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PRELIMINARY REPORT

ON THE

IDEAL PROJECT

ALBERNI MINING DIVISION BRITISH COLUMBIA

FOR

METAXA RESOURCES LIMITED Suite 13 - 1155 Melville Street Vancouver, British Columbia

NTS Sheet : 092F 6E / 7W Latitude : 49 degrees 17 minutes Longitude : 125 degrees 02 minutes

GEOLOGICAL BRANCH ASSESSMENT REPORT

R. Tim Henneberry , FGAC

Consulting Geologist October 26, 1987

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SUMMARY

Metaxa Resources Limited has under option 6 two-post mineral claims and 3 modified grid mineral claims totaling 1350 hectares, collectively known as the Ideal Property, in the Alberni Mining Division of Vancouver Island. The Ideal Property hosts several quartz vein/shear zones. The most important is the Ideal Vein yielding gold values to 0.875 ounces per ton over 0.40 metres from a 125 metre exposure open at both ends.

An exploration program consisting of detailed Ideal Vein sampling, property wide mapping and sampling, property wide silt sampling and detailed geochemical sampling was undertaken from April to September, 1987. Indications of important gold mineralization were obtained, as all surveys located significant anomalies.

Three potential ore shoots were outlined on the Ideal Vein. Three additional linear soil anomalies resulted from the geochemistry. All drainages tested returned gold values in the 1000 to 2000 parts per billion range.

An exploration program consisting of diamond drilling on the Ideal Vein, prospecting and examination of all anomalies and follow up trenching and diamond drilling is recommended at an estimated cost of 191,000.00

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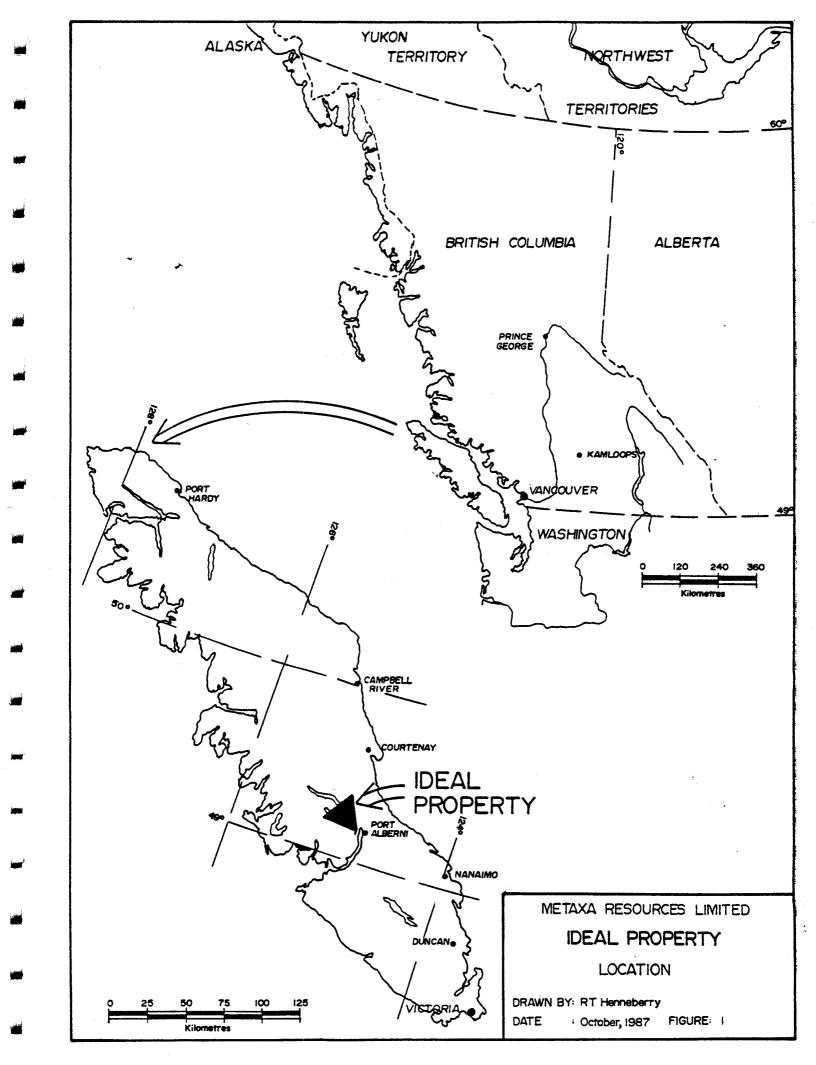
Full size copies of the following figures are located in map pockets :

Figures 4 through 8. Figures 9 through 13. -iii-

INTRODUCTION

The Ideal Property, consisting of 6 two-post claims and 58 contiguous units, lies within the Alberni Mining Division of Vancouver Island on the south slope of the Great Divide, the ridge between Sproat Lake and Great Central Lake. The Great Divide, hosting several mineral occurrences, has intermittently active since the been discovery of auriferous quartz sulfide veins on the Morning and Apex crown grants off the west end of Sproat Lake in the early 1900's. The resurgence of the Kennedy River Gold Belt the southwest) in (25 kilometres to the early 1980's, combined with the relatively steady price of gold has led to prospecting and re-evaluation of the quartz sulfide veins and copper showings for gold.

The purpose of this report is to document the recently completed exploration program on the Ideal Property.

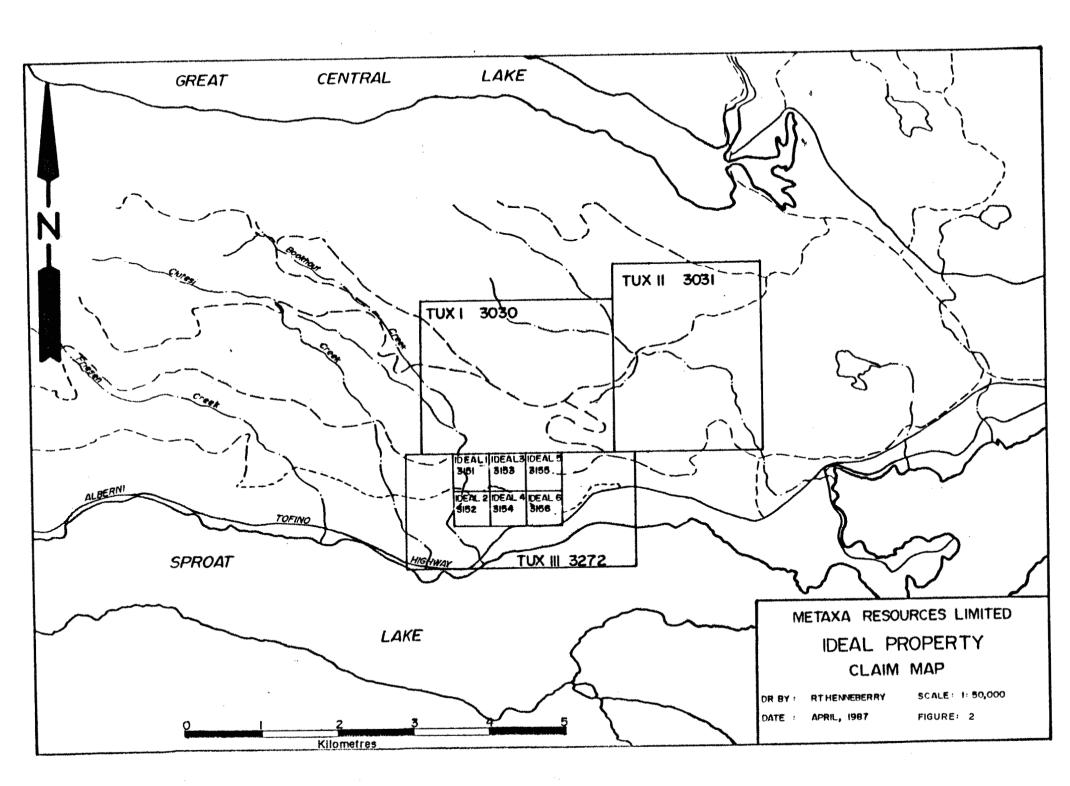


LOCATION, ACCESS

The Ideal property is located approximately 20 kilometres west of Port Alberni, in the Alberni Mining Division of Vancouver Island (Figure 1). The claim block lies on the south slope of the Great Divide between Sproat Lake and Great Central Lake.

Access is provided by logging roads leaving the Alberni - Tofino Highway approximately 18 kilometres west of Port Alberni. Inactive logging roads criss-cross the property providing reasonable access to all points. The main showing (the Ideal Vein) lies in a road cut ditch along one of these logging roads.

Exploration is quite feasible year round, with property elevations ranging from 100 to 700 metres. Rainfall is heavy in the winter, with occasional snow at the higher elevations. A large part of the claim group has been logged with second generation timber present. Water for diamond drilling should be available from the numerous streams cutting the south slope of the Great Divide.



OWNERSHIP

	lowing claims r operty (Figure 2)		Metaxa Resources
₹ *			
Name	Record Number	Units	Expiry Date
Tux I	3030	20	November 5, 1987
Tux II	3031	20	November 5, 1987
Tux III	3272	18	July 10, 1988
Ideal 1	3151	l	March 18, 1988
Ideal 2	3152	1	March 18, 1988
Ideal 3	3153	1	March 18, 1988
Ideal 4	3154	1	March 18, 1988
Ideal 5	3155	1	March 18, 1988
Ideal 6	3156	1	March 18, 1988

The Ideal 1 to 6 two-post mineral claims (record numbers 3151 to 3156) are held by R. Bilquist of Gabriola Island. The Tux I and Tux II mineral claims (record numbers 3030 and 3031) and the Tux III mineral claim (record number 3272) are held by Geo P.C. Services Inc. of Vancouver (Figure 2).

HISTORY

The exploration history of the Ideal Vein has been brief. The only previous exploration program of record was carried out for Royalon Petroleum Corporation in 1985 (Caulfield and Ikona, 1985). This exploration program consisted of geological mapping and sampling concentrated primarily on the Ideal Vein. Gold values as high as 0.272 ounces per ton were obtained from selected sites along the strike of the vein. A fairly comprehensive exploration program was recommended, but a record of this program does not exist, leading to speculation as to whether it was ever carried out.

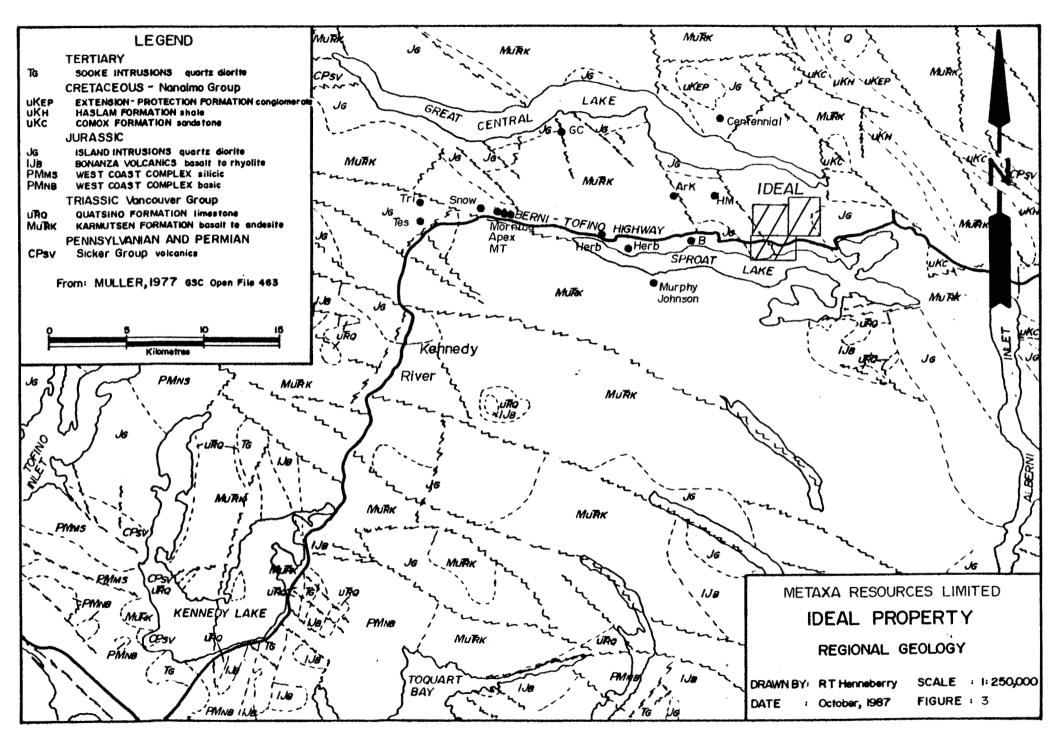
Regional Mineral Occurrences

Property	MINFI	LE	Commodity
Morning	092F	119 `*	gold
Apex	092F	150	gold
MT	092F	212	gold
HM (Ark)	092F	230	gold
Herb, Moon	092F	232	copper
Murphy Johnson	092F	249	gold
Tri	092F	281	copper
Centennial	092F	293	copper
HM 32	092F	306	copper
HM 28	092F	307	copper
R	092F	341	copper
B, Dede	092F	356	copper
Herb	092F	362	copper
Tes	092F	391	copper
G.C.	092F		gold

Several mineral showings have been documented on the Great Divide (Figure 3). The largest percentage of these showings were located for copper within the Karmutsen Formation basalts and andesites. Minimal attention has been paid to the gold potential of these properties.

The south slope of the Great Divide hosts at least 5 distinct shear hosted gold occurrences. Significant concentrations have been documented on 4 of the 5 properties. Values to 0.75 ounces per ton gold have been obtained from a quartz carbonate stockwork alteration zone associated with a northeast trending shear zone have been obtained from the G.C. Property (Bilquist, 1986).

Values to 2.78 ounces over 1.2 metres have been reported from a shear hosted quartz sulfide vein on Casau Explorations Snow Property (J.C.Stephen, pers com). The Morning, Apex and M.T. Properties have all recorded values in excess of 1 ounce per ton gold from shear hosted quartz sulfide veins (Harder, 1984; Cukor, 1985). Considerable antimony-mercury has been reported from the Ark Property, believed to be the upper reaches of a buried epithermal system (Henneberry, 1986; 1987).



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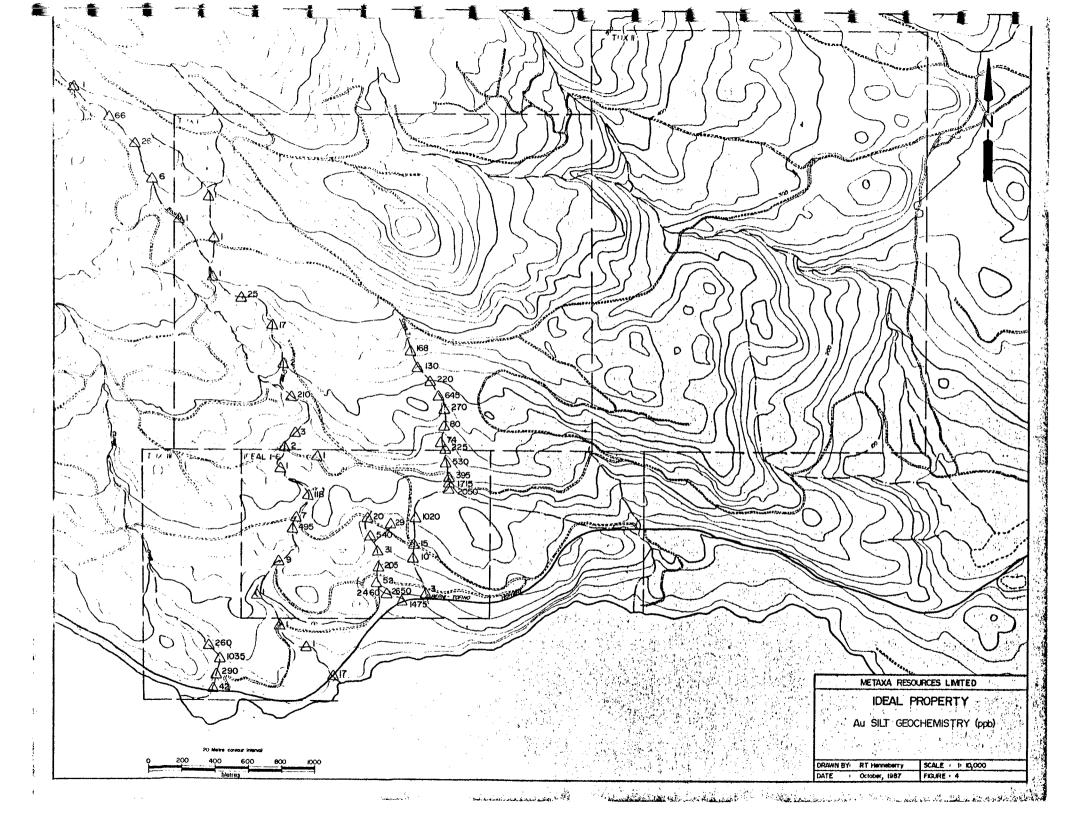
REGIONAL GEOLOGY

The geology of the Great Divide consists primarily of rocks of the Vancouver Group intruded by plutons of the Island Intrusions. A later episode of faulting has resulted in a series of northwest trending regional shear zone / faults (Figure 3). (Muller, 1977).

rocks are the basaltic to The oldest andesitic pillowed flows and tuffs of the Triassic Karmutsen Formation of the Vancouver Group. Locally, shale/slate seams have been documented interstitially with the individual pillows and flows. Bedding attitudes are difficult to obtain from the lavas. Alteration consists primarily of greenschist facies chlorite and carbonate, with stronger alteration assemblages associated with the contacts of the intruding plutons.

A quartz diorite member of the Jurassic Island Intrusions outcrops regularly at lower elevations on both sides of the Great Divide. The intrusive varies from fresh to moderately altered proximal to the contacts and to the northeast trending shear zones. The alteration assemblage includes chlorite, carbonate, argillization and silicification. Locally, sericite has been noted with the shear zones.

Post-Island Intrusion faulting has resulted in a series of sub-parallel shear/fault zones striking to the northwest, now occupying several of the present creek drainages. Limited exploration suggests these zones are anomalous in gold. The shear/fault zones are the target of the present exploration program.



1987 PROGRAM

A detailed exploration program, undertaken on the Ideal Project from April to October, consisted of property wide mapping and prospecting, property wide silt sampling, detailed mapping and sampling of the Ideal Vein, and expanded soil sampling of the Ideal Vein strike projections.

Silt Sampling (Figure 4):

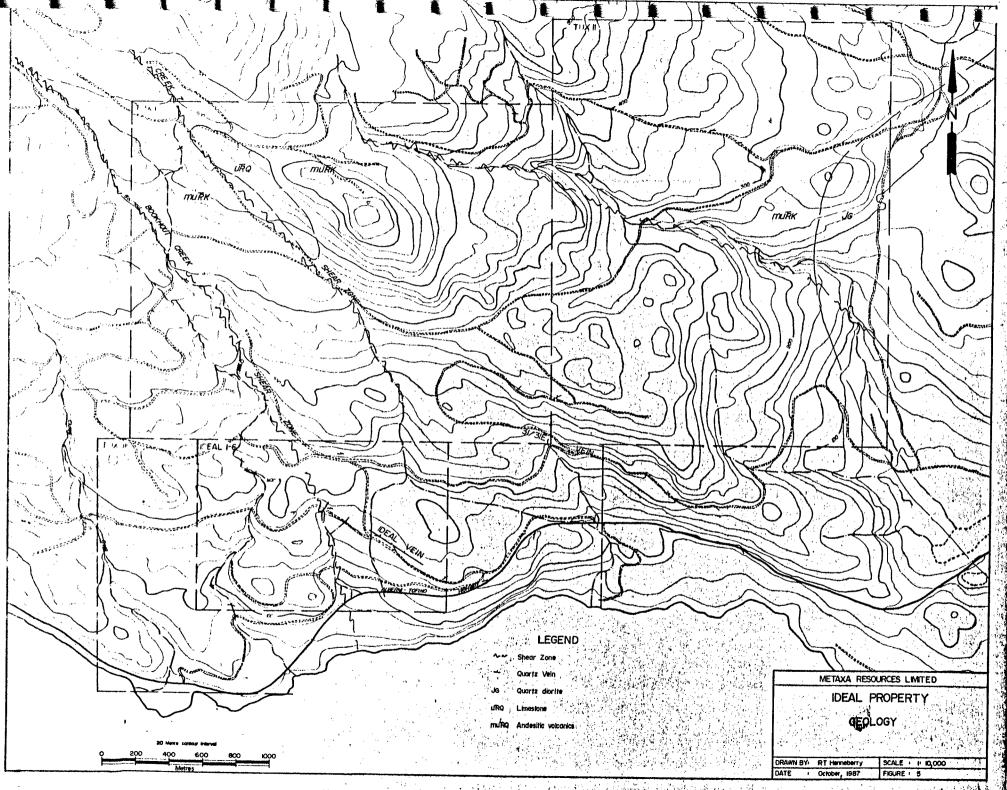
The silt sampling program was concentrated on the western half of the property, with one major drainage remaining to be sampled. Drainages flow southeast for the most part, following the trace of the northwest trending shear zone / faults. Where possible moss was collected from the stream and sieved at 80 mesh. The resulting fine silt was placed in a kraft soil bag and sent to the lab for analysis.

The analytical results from the streams sampled are very encouraging. All drainages tested are anomalous in gold. Gold was found downstream in all drainages cutting the strike projection of the Ideal Vein. Significant gold was also located in the upper Creek 7 drainage, indicating a source distinct from the Ideal Vein, whose strike projection is well below the anomalous zone. Upper Bookhout Creek is also sporadically anomalous in gold, again suggesting sources distinct from the Ideal Vein. A concentration of anomalous values at the mouth of Clutesi Creek are as yet unexplained.

Silt sampling should be undertaken on Clutesi Creek looking for strike continuations of the anomalous values located in Bookhout Creek and Creek 7. Additional ground to the west should be staked based on the results. The drainages on the eastern half of the claim group should also be tested. Check samples taken at several sites verify the earlier results. Detailed prospecting is required to locate the sources of these gold anomalies.

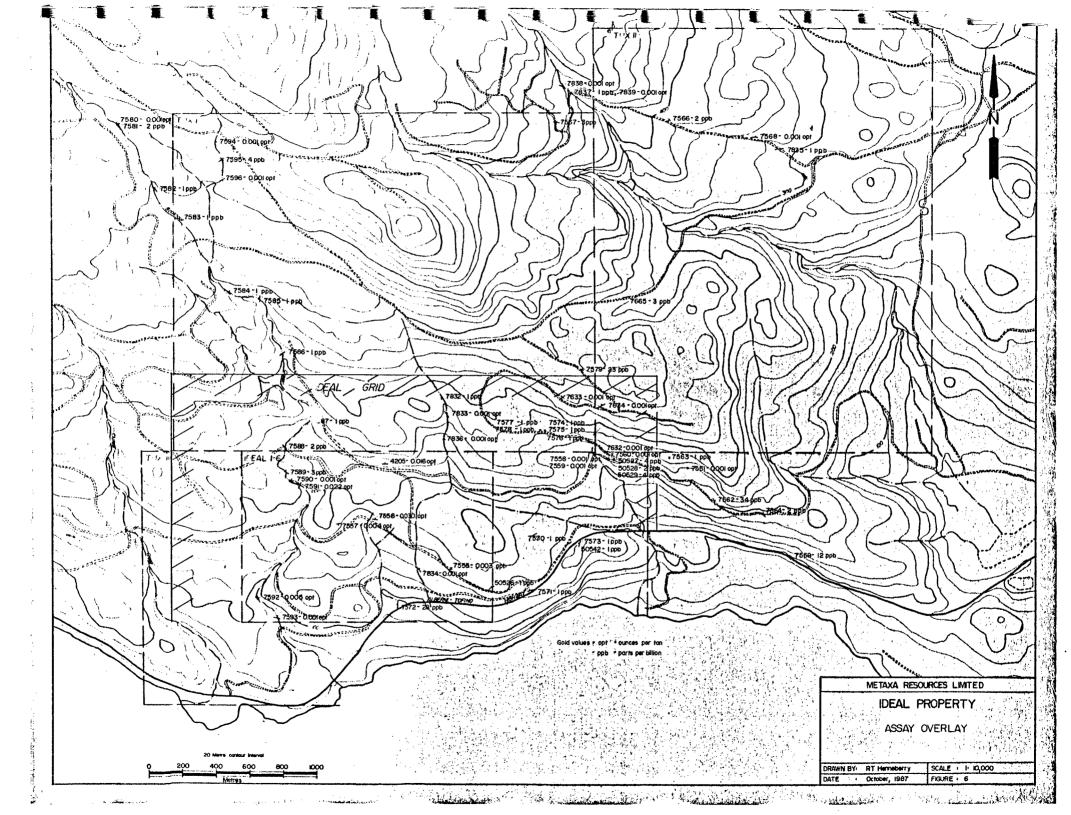
Property Mapping and Sampling (Figures 5 and 6):

Considerable outcrop exposure was noted throughout the claim group. Andesitic pillowed to massive flows and tuffs form the primary rock unit. A small lenses of limestone was mapped in the northeast corner of Tux I. Quartz diorite was noted proximal to the eastern boundary of Tux II. Traverses down Bookhout Creek and Creek 7 located significant shear zones in the creek valleys. The 61 samples taken during



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prospecting consisted of 36 quartz vein samples, 7 shear zone samples, 10 stockwork zone samples, 3 float samples and 5 undocumented samples.

The Karmutsen volcanics, underlying most of the claim group, exhibit a weathered dull brown appearance. Fresh exposurés indicate an andesitic composition, though no distinct phenocrysts are noted. Locally, small highly deformed shale/slate bands are mapped between the pillows. Several of these bands are cut by a stockwork of carbonate veinlets and stringers that do not continue into the lavas. The lavas are propylitically altered, consisting of chlorite, local carbonate and pyrite. Stronger alteration consisting of silicification, argillization and local sericitization is noted haloing shear zones and larger (+10 centimetre) guartz veins.

Quatsino limestone outcrops as a small lens on the hanging wall of the Creek 7 Shear Zone. Exposures are grey in color and well brecciated. Calcareous siltstones are interbedded with the limestone. Very little alteration or mineralization was noted.

A weakly altered quartz diorite was mapped on the eastern boundary of the claim group. The actual quartz diorite / volcanic contact does not outcrop. Alteration consists of weak chloritization of feldspars, and chlorite and carbonate along fractures. Traces of pyrite were also noted on fractures.

Fifteen samples were taken from Bookhout Creek. Samples 7580 to 7585 traced the Bookhout Creek Shear Zone 1200 metres to a point where it appears to leave the creek. Discontinuous quartz veins (to 15 centimetres in width) and stockwork zones characterize the zone. Alteration silicification, of chloritization and with consists local hematite. Disseminated pyrite was noted in the quartz veins and stockwork. Gouge zones were not mapped indicating the true width of the shear zone has not been exposed. Anomalous silt samples in the range of 25 to 210 ppb gold were recorded from this section of Bookhout Creek. The 6 rock samples taken returned background gold values. The remaining 9 samples were taken from parallel and cross lower in the creek, also identified by the soil veins Sample 7591, a flat lying quartz vein geochemistry. striking 020 degrees assayed 0.022 ounces per ton. The remaining samples did not exceed background.

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505W			50.5W	IDEAL VEIN GEOLOGY / ASSAY PLAN
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Four samples were taken from Creek 7. Samples 7632 and 7633 were taken from the Creek 7 Shear Zone. Limited outcrop exposure resulted in only one 4 centimetre quartz vein being sampled. The shear zone exhibits chlorite and silicification. Gouge zones were not mapped. Anomalous silt samples to 2050 ppb gold have been recorded in the drainagé. All rock samples taken did not exceed background.

Five samples were taken from a vein located at the junction of roads 31 and 31E. The 31/31E Junction Vein (285/55 N) is 10 to 40 centimetres in width and is exposed semi-continuously for a strike length of 25 metres. Intense limonite masks the vein through its entire strike length. Hematite also occurs regularly within the vein, as well as within 15 centimetres of the footwall contact. Other than limonite and hematite, no other alteration is noted in the wall rock. Gold values did not exceed background.

The remaining samples were taken from structures identified primarily in creeks and roadcuts. Sample 4205 assayed 0.016 ounces per ton gold from a malachite stained quartz vein (270/?) located as a result of following up soil geochemistry Anomaly B.

Prospecting of creeks has met with limited success. The shear zones do not appear to carry anomalous gold though they do show signs of hydrothermal alteration. The strongest vein structures appear to be east west trending, suggesting gold may be localized in the splay structures of the shear zone/faults and not the faults themselves. Soil geochemistry has yielded results verifying this observation.

Ideal Vein:

The primary showing on the claim group, the Ideal Vein (125/62 NE), strikes along road C-18 for a semi-continuous length of 110 metres (Figure 7). After considerable hand trenching only 50 percent of the exposure is presently covered by talus and/or overburden. Vein widths range from 20 to 50 centimetres. The vein pinches and swells quite regularly. The strike projection goes under overburden cover in both directions.

Andesitic volcanics of the Karmutsen Formation host the Ideal Vein. They are locally well-brecciated within the vein channel. There is not a distinct alteration associated with the Ideal Vein. Perhaps the regional alteration of the Karmutsen Formation masks any

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hydrothermal alteration associated with the emplacement of the Ideal Vein.

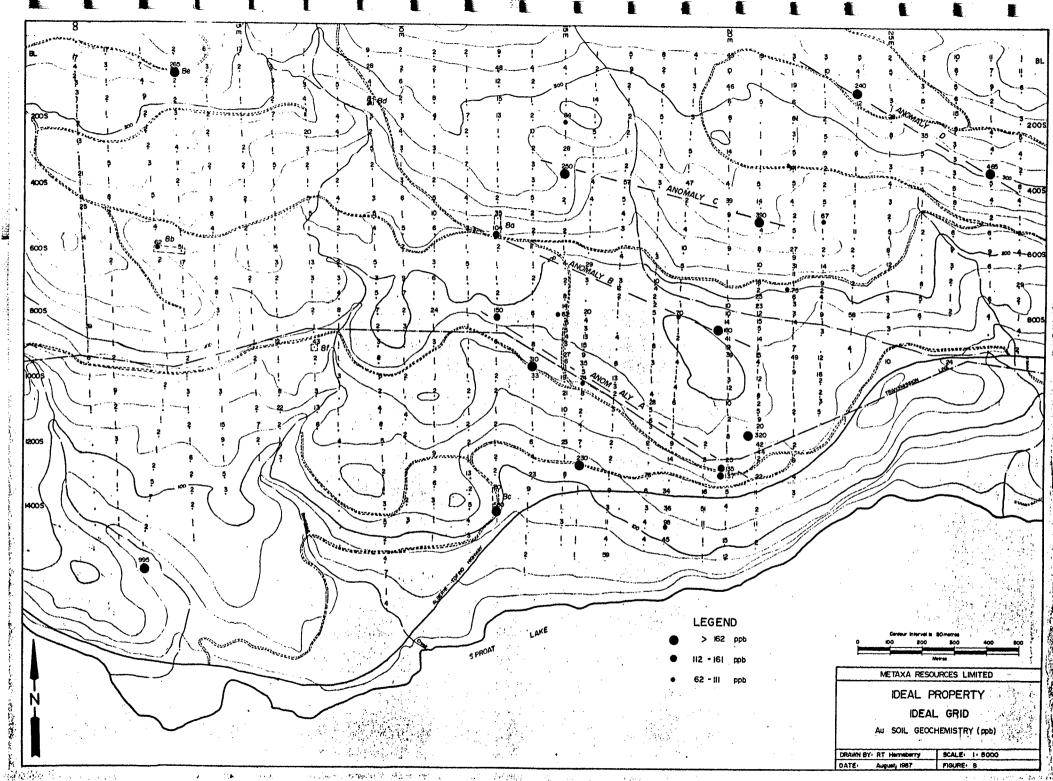
Mineralization is concentrated within the quartz, though not necessarily confined to either one contact or the other. Sulfide mineralization occurring as pods and dissemifiations, is predominantly pyrite, with lesser chalcopyrite and traces of arsenopyrite. (Percentages 2.5-3 % pyrite, 0-0.5 % chalcopyrite). Malachite (and in on occurrence azurite) staining is noted with the presence of chalcopyrite.

Where exposed, sample spacing is 2 metres or less. Values as high as 0.845 ounces per ton over 0.40 metres have been recorded. Of the 43 samples taken only 13 returned distinct values that are not considered anomalous. Two shoots appear to be outlined by the sampling to ore date, at either end of the present exposure. Based on this authors experience gold veins on Vancouver and elsewhere have been a partially to completely Island leached zone at surface, with a considerable improvement concentration immediately (ie. 1 metre) below in surface. Hand-trenching and blasting to obtain a depth of 50 centimetres is strongly recommended before drilling commences.

Soil Geochemistry:

Initially a small grid was recommended for strike projection of the Ideal Vein. The discovery the of 31/31E Junction Vein necessitated expansion of the the recommended grid to cover both structures, and to explore for additional veins. A baseline of 2900 metres was cut at 090 degrees, 400 metres north of the 31/31E Junction exposure. Cross lines, spaced at 100 metres, were cut at 180 degrees from the baseline to just short of the Sample spacing was 50 metres except in the highway. immediate area of the Ideal Vein where the spacing was tightened up to 25 metres. Soil samples were taken from the "B" Horizon and placed in Kraft Soil Bags for shipment to Analytical Labs in Vancouver for analysis. The Acme resulting 850 samples were analyzed for Au, Ag, As, Hg, Sb, Pb and Cu. Plots have been made for all elements except Sb. Simple statistics have been performed to determine the threshold values for each element.

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	Au ppb	Ag mqq	As ppm	Hg ppb	Sb ppm	Pb ppm	Cu ppm
Count	897	850	850	850	850	850	850
Maximum	995	1.7	125	430	13	40	487
Minimum	l	0.1	2	20	2	2	14
Meán	11.4	0.18	5.3	92	2.3	11.9	97.5
Std Dev	50.3	0.14	6.7	42.2	l	6.3	51.5
M + SD	62	0.32	11	134	3	18	149
M + 2SD	112	0.46	18	176	4	24	201
M + 3SD	162	0.58	26	218	6	30	252

Gold (Figure 8): 897 samples were analyzed for gold, with a mean of 11.4 ppb and a standard deviation of 50.3 ppb. Values in excess of 62 ppb were considered anomalous. Four linear anomalies and several spot anomalies were identified by the survey. Anomaly A is the Ideal Vein, traced a total of 850 metres. Anomaly B, running between lines 13E and 20 E, is a linear anomaly parallel to the Ideal Vein. Anomaly C, between lines 15E and 21E, is also a linear anomaly parallel to the Ideal Vein. Anomaly C could be the strike continuation of the 31/31E Junction vein. Anomaly D, a linear anomaly between lines 24E and 29E, parallels the Ideal Vein as well.

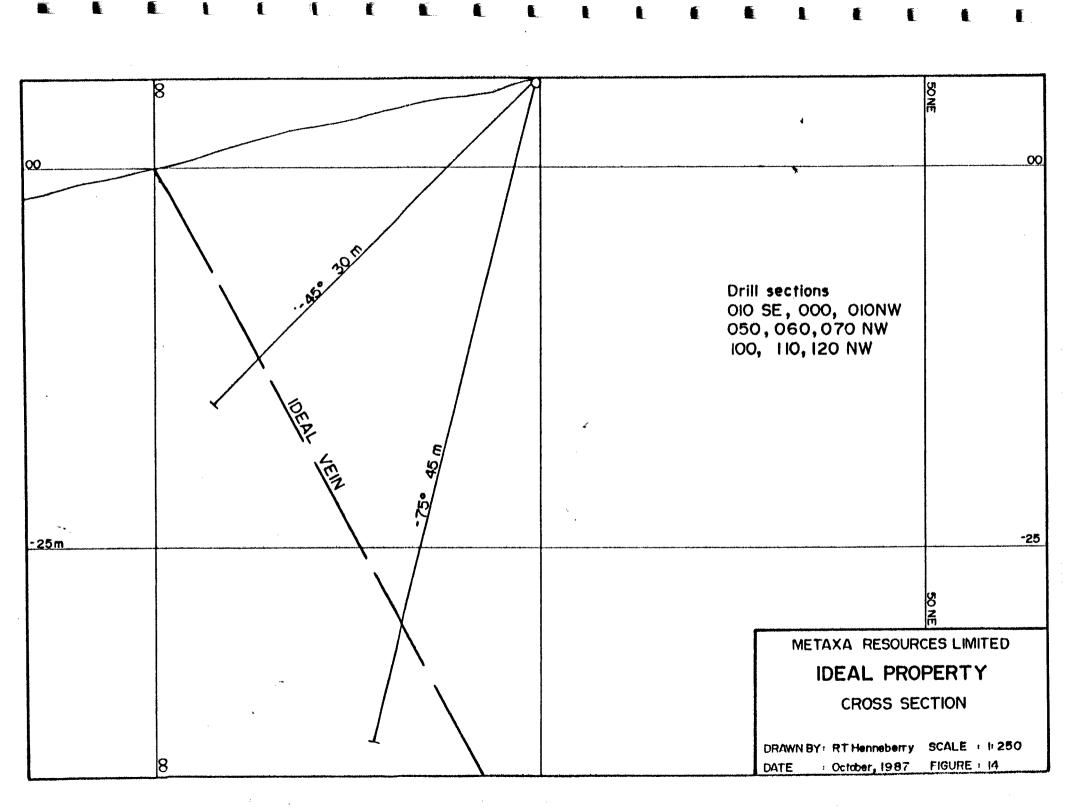
In an effort to test some of the spot anomalies 6 detailed soil grids were initiated (8a to 8f on Figure 8). Samples were taken at 5 metre centres from a 20 by 20 metre grid centred on the existing anomalous value. Only 1 of the 6 grids were successful (Figure 8a), with the original anomalous value being surrounded by strong gold responses. This location is at the western end of Anomaly B. In the other 5 locations (Figures 8b to 8f), the original values were not even duplicated.

Silver (Figure 9): 850 samples were analyzed for silver, with a mean of 0.18 ppm and a standard deviation of 0.14 ppm. Values in excess of 0.3 ppm were considered anomalous. The continuous anomalous values on lines 12E, 13E and 14E are considered to be contamination. Gold anomalies B, C and D are also anomalous in silver, while the Ideal Vein is not. The anomalous gold values are displaced 25 to 50 metres down slope with respect to silver. Linear Anomaly B lies between lines 15E and 23E. Anomaly C is represented as a spot anomaly on line 23E. Anomaly D, running between lines 18E and 29E, exhibits the strongest silver responses. Arsenic (Figure 10): 580 samples were analyzed for arsenic, with a mean of 5.3 ppm and a standard deviation of 6.7 ppm. Values above 12 ppm were considered anomalous. The Ideal Vein, Anomaly A, lies between lines 12E and 20E. Anomaly B runs between lines 12E and 22E. Anomaly C lies between lines 14E and 26E. Anomaly D lies between lines 18E and 29E. Arsenic responses correlate well with gold. All linear anomalies have been extended along strike by the arsenic responses. As with gold, several spot anomalies exist over the remainder of the soil grid.

11): 850 samples were analyzed (Figure Mercury for mercury, with a mean of 92 ppb and a standard deviation of 42.1 ppb. values in excess of 134 ppb were considered anomalous. As with silver, the Ideal Vein is not anomalous in mercury. Anomaly B lies between lines 18E and 22E, a considerably shorter strike length than the from gold, silver and arsenic anomalies. Anomaly C runs line 21E to 28E. Anomaly D runs from line 16E to 29E. Unlike the previous three elements a considerable concentration of anomalous mercury values lie on the western half of the grid.

for Lead (Figure 12): 850 samples were analyzed lead, with a mean of 11.9 ppm and a standard deviation of 6.3 ppm. Values in excess of 18 ppm were considered The Ideal Vein, Anomaly A, is anomalous in h lines 14E and 19E. Anomaly B, between anomalous. lead between lines 15E and 22E, is weakly anomalous in lead, as is Anomaly C between lines 18E and 27E and Anomaly D between lines 18E and 29E. In a situation similar to mercury, a considerable concentration of anomalous lead values lie on the western half of the grid, though a lead-mercury correlation is not readily evident. Surprisingly, lead and silver do not exhibit a positive correlation.

Copper (Figure 13): 850 samples were analyzed for copper, with a mean of 97.5 ppm and a standard deviation of 51.5 ppm. Values in excess of 149 ppm were considered anomalous. Although there is considerable scatter in the plotted copper results, the four linear anomalies are still evident. Anomaly A lies between lines 15E and 21E. Anomaly B lies between lines 13E and 22E. Anomaly C lies between lines 17E and 29E. Anomaly D lies between lines 18E and 29E. The south end of line OE is also interesting as this local is anomalous in all elements except gold and silver.



DISCUSSION

The recently completed exploration program has indicated the Ideal Property has potential to host economic concentrations of gold mineralization. Economic grade mineralfzation has been established on the Ideal Vein. Soil geochemistry has identified three distinct linear anomalies, displaying characteristics similar to the Ideal Vein. Silt geochemistry has located considerable and presently unexplained gold within all drainages sampled.

The Ideal Vein, a quartz sulfide vein splaying from a regional shear zone fault, has yielded values to 0.875 ounces per ton gold over a width of 40 centimetres. Sampling of semi-continuous exposure over a strike length of 120 metres has identified two potential ore shoots. The west ore shoot is open to the northwest from 105 NW. The east ore shoot is open to the southeast from 010 NW. Indications of a potential ore shoot to the northwest of 60 NW are also suggested from the sampling.

Blasting is initially recommended to remove the weathered surface and obtain fresh exposure for sampling. Follow up diamond drilling is recommended to initially test the potential ore shoots to a depth of 30 metres below surface. A total of 18 drill holes totaling 1000 metres is recommended to initially test the Ideal Vein (Figure 14).

The large percentage of anomalous silt values recorded during the survey need to be heavily prospected. Shear zones have been mapped in the creek valleys on both Bookhout and 7 Creeks. Several cross veins parallel to the strikes of the soil anomalies have also been mapped. Comparison of the gold soil geochemistry and geochemistry silt geochemistry suggests the source of gold the Creek 7 could be the strike continuous anomaly in projections of linear anomalies B, C and D. The large creek on the Tux II claim parallels the strike of the Ideal Vein and the linear anomalies. This creek needs to be silt sampled and prospected.

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The soil sampling located 4 distinct linear anomalies as well as several lesser spot anomalies. A preliminary examination was made of the major linear anomalies. Anomaly A is the strike projection of the Ideal Vein. Traverses along strike of anomalies B, C, and D located considerable outcropping with a hummock-like appearance, ie. a series of steps, or valleys and ridges with suspected structures lying beneath cover in the valleys. Though structure with very little mineralization or quartz was located in most instances, a large area of angular quartz float was noted, with one small outcrop exposure at the west end of Anomaly B. Hand-trenching and mechanical trenching will be required to evaluate these anomalies. 500 metres of diamond drilling is budgeted for anomaly follow-up.

Finally, the 31/31E Junction Vein and a presently unmapped vein located on the eastern half of the Tux II mineral claim should be tested. The character of the 31/31E Vein is noticeably different from the Ideal Vein. The 31/31E Vein exhibits considerable limonite and hematite, as well as a quartz carbonate nature. At this time blasting to obtain fresh surfaces and sampling is recommended.

RECOMMENDATIONS

Based on the results of the initial exploration program, further exploration is recommended.

Phase A - Ideal Vein

- 1) Blast the present exposure to obtain fresh surfaces and sample every 2 metres.
- 2) Diamond drill to test the three potential ore shoots to a depth of 30 metres. Three sections of 2 holes each are recommended at 10 metre spacings for each of the shoots.

Estimated cost of Phase A is 93,800.00

Phase B - Anomaly Prospecting

- 1) Silt sample and prospect the Tux II creek.
- 2) Prospect all silt anomalies.
- 3) Prospect and hand-trench the soil anomalies.
- 4) Blast and sample the 31/31E Junction Vein and the east Tux Vein.

Estimated cost of Phase B is 32,210.00

Phase C - Anomaly Trenching

Excavator trench the linear anomalies where required.
 Estimated cost of Phase C is 18,990.00

Phase D - Diamond Drilling

Diamond drill, based on the results of Phases B and C.
 Estimated cost of Phase D is 45,490.00

Total estimated cost of the recommended exploration program is 191,000.00. Phases A and B can run concurrently. Phase C is for the most part based on the results of Phase B. Phase D is based on the results of Phases B and C. This offering will raise funds for Phases A through C only.

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COST ESTIMATES

Phase A - Ideal Vein

Drill mobilization/demobilization	5,000.00
Footage [*] charges	60,000.00
Geologist	7,500.00
Room and Board	4,500.00
Transportation	1,800.00
Analysis	4,000.00
Field Supplies	3,500.00
Contingency	7,500.00
SUB-TOTAL	93,800.00

Phase B - Anomaly Prospecting

5,250.00 4,200.00 3,150.00 3,150.00 4,200.00 1,260.00 6,000.00 1,000.00 4,000.00
32,210.00

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Phase C - Anomaly Trenching

Mobilization/Demobilization	2,000.00
Excavator trenching	5,000.00
Geelogist	3,750.00
Room and Board	1,400.00
Transportation	840.00
Analysis	3,000.00
Field Supplies	1,000.00
Contingency	2,000.00
SUB-TOTAL	18,990.00

Phase D - Anomaly Drilling

Footage charges	30,000.00
Geologist	3,750.00
Room and Board	1,400.00
Transportation	840.00
Analysis	3,000.00
Field Supplies	2,500.00
Contingency	4,000.00
SUB-TOTAL	45,490.00

Phase A	93,800.00
Phase B	32,210.00
Phase C	18,990.00
Phase D	45,490.00
TOTAL	190,490.00

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STATEMENT OF QUALIFICATIONS

I, R.Tim Henneberry, am a consulting geologist residing at 4054 Dundas Street, Burnaby, B.C.

I 'earned a Bachelor of Science Degree majoring in geology from Dalhousie University, graduating in May, 1980.

I have practiced my profession continuously since graduation.

I am a Fellow of the Geological Association of Canada.

I have no interest, either direct or indirect, in Metaxa Resources Limited.

This report is based on an exploration program supervised by the author. The initial property evaluation was made April 01 to 02, 1986. Progress of the program was monitored on August 15, 1987. Initial prospecting of soil anomalies was undertaken from September 03 to 05, 1987.

I hereby grant my permission for Metaxa Resources Limited to use this report for filing with the Vancouver Stock Exchange as partial requirement of a Statement of Material Facts or for any legal purposes normal to the business of Metaxa Resources Limited.

day of Abventor in city of the Dated this Vancouver, British Columbia. SSOCIA; FELLON

REFERENCES

Bilquist,R.J. (1986). Prospecting report on the G.C. #1 Claim. British Columbia Ministry of Energy, Mines and Petroleum Resources Assessment Report 15,354.

Caulfield, D.A. and Ikona, C.E. (1985). Geological Report on the Ideal Claims for Royalon Petroleum Corporation. British Columbia Ministry of Energy, Mines and Petroleum Resources Assessment Report 13,539.

Cukor, V. (1985). Geological, Geophysical and Geochemical Report on the Tay Group. British Columbia Ministry of Energy, Mines and Petroleum Resources Assessment Report 14,121.

Harder, D.G. (1984). Report on Diamond Drilling Program, Tay Gold Property. British Columbia Ministry of Energy, Mines and Petroleum Resources Assessment Report 14,601.

Henneberry, R.T. (1986). Preliminary report on the Ark Project, Alberni Mining Division, British Columbia. Ascot Resources Limited private report.

Henneberry, R.T. (1987). Final Phase I and II Report on the Ark Property, Alberni Mining Division, British Columbia. Ascot Resources Limited private report.

Muller, J.E. (1977). Geology of Vancouver Island. Geological Survey of Canada Open File 463.

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34 Statement of Cost

Reference: Geological mapping, Geochemical sampling Ideal Property - June 22 - June 30, 1987

PERSONNEL:

l	Supervisor - 5 days @ \$300/day	\$ 1,500.00
l	Geologist - 8 days @ \$225/day	1,800.00
1	Prospector - 1 day @ \$225/day	225.00
l	Technicians' Chief - 8 days @ \$200/day	1,600.00
2	Field Tecnincians -	
	4.5 mandays @ \$150/manday	675.00
		\$ 5,800.00

TRANSPORATION:

1 4x4 Bronco - 1 week @ \$250	/week \$ 250.00
516 kms @ \$0.18/km	92.88
Ferries, Gas, Oil	431.85
	\$ 774.73

SUPPORT:

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Camp Cost - 25 mandays @ \$15/manday	\$ 375.00
Hotel Accommodations	79.38
Food	304.28
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ANALYSIS:

17	rock	samples	a	\$14.25	/sample	\$ 242.25

MISCELLANEOUS:

Equipment Rental	\$ 60.00)
Supplies	179.13	\$
Communications	150.00)
	\$ 389.13	ļ

- Sub-Total: \$ 7,964.77
- 10% Administrative Overhead: 796.48

Total: \$ 8,761.25

	35	
Reference:	Geological Mapping, Gecchemical S line cutting and Grid Preparation IDEAL Property July 01 - 31, 987	
PERSONNEL		
1 Geol 1 Pros 2 Chie	ervisor - 2 mandays @ \$300/manday ogist - 30 mandays @ \$225/manday opector - 3 mandays @ \$225/manday of Technicians - 18.5 mandays @ \$200/manday of Technicians - 90 mandays @ \$150/manday - 19 mandays @ \$100/manday	675.00
TRANSPORTATION	TRAVEL	
1 Brone	Pickup - 1 week @ \$250/week co - 4 weeks @ \$250/week km @ \$0.18/km ies	\$ 250.00 1,000.00 554.22 111.50 282.06 \$ 2,197.78
SUPPORT		
Camp Costs Food	s - 160.5 mandays 3 \$15/manday	\$ 2,407.50 1,515.66
ANALYSIS		\$ 3,923.16
54 Rock ar	nd Soil Samples	\$ 621.50
MISCELLANECUS		
Supplies a	ainsaws - 9 days @ \$25/day	\$ 450.00 1,204.35 600.00 2,549.26 \$ 4,303.61
	Sub-Total:	\$38,671.05

Sub-Total: \$33,671.05 10% Administrative Overhead: 3,367.11

Total: \$42,538.16

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Sample Location Number	Description	Width Metres	oz/t Au	ppb ['] Au
	IDEAL VEIN Henneberry Sampling			•
50537 Stn +50.0 50538 Stn +88.0	10% py 12% py, 1% cpy 1% py 4% py 2% py No visible min 8% py, 2% cpy 2% py No visible min 1% py	0.22 0.25 0.15 0.18 0.30 0.25 0.50 0.38 0.30 0.40 0.40		
	IDEAL VEIN Robb Sampling			
7801 Stn + 02 7802 Stn + 04 7803 Stn + 06 7804 Stn + 08 7805 Stn + 10 7806 Stn + 12 7807 Stn + 14 7808 Stn + 16 7809 Stn + 18	· · ·	0.25 0.22 0.25 0.25 0.25 0.20 0.15 0.18 0.25	0.016 0.117 0.205 0.029 0.114 0.015 0.001 0.006 0.070	490 3630
7810 Stn + 20 7811 Stn + 22 7812 Stn + 24 7813 Stn + 26 7814 Stn + 28		0.30 0.28 0.25 0.25 0.30	0.007 0.003 0.011 0.014 0.014	220 89 450

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Sample Number	Location	Description	Width Metres	oz/t Au	ppb Au
7815	Stn + 30)	0.25	0.002	76
7816	Stn + 32		0.30	0.023	730
7817	Stn + 34		0.30	0.007	207
7818	Stn + 36		0.30	0.001	4
7819	Stn + 50		0.40	0.018	570
7820	Stn + 54		0.50	0.017	520
7821	Stn + 50		0.50	0.001	21
7822	Stn + 60		0.40	0.006	
7823	Stn + 61		0.50	0.726	
7824	Stn + 62		0.40	0.035	
7825	Stn + 99		0.38	0.004	115
7826	Stn +102		0.35	0.002	67
7827	Stn +104		0.30	0.001	•
7828	Stn +106		0.40	0.001	
7829	Stn +108		0.40	0.845	
7830	Stn +110		0.40	0.065	
7831	Stn +112		0.30	0.078	

PROPERTY Robb Sampling

7613 7632 Br 31 7633 Br 31 7634 Br 31	100/71N shear gouge zone 065/85NW qtz vn/shear 072/86NW qtz vn	0.20 0.20 0.60	0.001 0.001 0.001
7555 Br 18	Qtz vein	0.70	0.003
7556 Br 18	108/60N qtz vein vis py	grab	0.030
7557 Br 18	083/79S qtz vn with diss py	grab	0.004
7558 Br 31E	098/73N qtz vn	0.15	0.001
7559 Br 31E	100/73N qtz vn	grab	0.001
7560 Br 31	Qtz vein	0.12	0.001

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Sample Number	Location	Description	Width Metr e s	oz/t Au	ppb ['] Au
7562 7563 7564 7565 7566 7567 7568 7569 7570 7571 7572 7573 7573 7574	Br 31 Br 31 Br 31 Br 31 High Level Br 6 Br 6 Br 6 Highway Highway Highway Highway Br 31 Br 31	Cb/ep stockwork with diss py 161/78NE shear zone with hem Calcite stockwork 121/65NE shear zone 068/? qtz vein cb stockwork 093/70N qtz vn/fault 084/70N qtz vn/fault with py 135/23NE cb stockwork 060/70NW qtz vein 070/60NW qtz/gouge vn 178/07W qtz vein 020/68NW siliceous gossan	grab 0.90 grab 0.40 0.90 1.00 1.30 0.60 grab 0.05 0.12 0.10 grab	0.001	34 1 2 3 2 3 12 1 1 28 1 1
7576 7577	Br 31 Br 31 Br 31 Br 31	· · · · · · · · · · · · · · · · · · ·	4		1 1 1 1 1
7580 7581 7582 7583 7584 7585 7585 7586 7587 7588 7589 7589	Br 31 Bookhout Ck Bookhout Ck Bookhout Ck Bookhout Ck Bookhout Ck Bookhout Ck Bookhout Ck Bookhout Ck Bookhout Ck Bookhout Ck	160/83NE qtz vn with py 144/74SE qtz vn Oxidized qtz stockwork 120/86NE qtz vn 180/68W siliceous dyke 062/18SE siliceous bed 060/32SE qtz vn 143/71S qtz vn 117/? shear zone/fault 119/66NE qtz infilling with p		0.001	23 2 1 1 1 1 1 2 3
7592 7593	Bookhout Ck Bookhout Ck Bookhout Ck E Ck	020/18SE qtz vn with py 150/88NE qtz vn with py 105/74N qtz vein with py Siliceous volc's with py	0.50 0.06 0.20 0.40	0.005	

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Sample Number	Location	Description	Width Metres	oz/t Au	ppb Au
7595 7596	E Ck E Ck	058/42SE qtz infilling 070/80S qtz infill py	0.40 0.25	0.001	`4
7833	Ck 7 Ck 7 Ck 2E	Sulfide float 125/68? qtz vn with py 290/40NE qtz vn	grab 0.04 0.20	0.001 0.001	1
7835 7836	Br 6 Ck 7 Br 6	090/90 Altered dyke Qtz float 154/90 fault/qtz str with py	0.31 grab grab	0.001	1
7838	Br 6 Br 6	280/82N lim qtz flt gouge HW volc from 7837	grab grab	0.001	*

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PROPERTY Henneberry Sampling

50528 31/31E Vein	285/45N lim/qtz vn 5% vugs 285/55N lim/qtz vn - east 285/55N lim/qtz vn - centre 285/55N lim/qtz vn - west Siliceous gossan	grab 0.15 0.20 0.20 grab		1 4 2 4 1
4205 1290E 560S	270/? qtz vn with 2% py-cpy and malachite staining	grab	0.016	

ACME ANALYHICAL LABU TORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011 DA DA RECEIVED: JUL 28 179/

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DATE REPORT MAILED:

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: SOILS -BO MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE. H6 ANALYSIS BY FLAMLESS AA.

ASSAYER: . N. My. DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCES PROJECT-IDEAL File # 87-2792 Page 1

SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L4+00 10+00S	41	14	. 4	2	2	1	80
L4+00 10+50S	104	21	. 1	4	2	ŝ	130
L4+00 11+00S	94	15	. 1	2	2	1	80
L4+00 11+50S	70	21	.1	4	2	15	70
L4+00 12+00S	67	20	.2	2	2	5	60
L-1.00 12.000	G 7	<i></i>	• dia		alara.	,	0.0
L4+00 12+50S	57	12	. 1	2	2	1	80
L4+00 13+00S	73	8	.2	2	2	5	100
L4+00 13+50S	119	13	. 1	2	2	3	20
L5+00 9+50S	73	10	. 1	2	2	2	60
L5+00 10+00S	94	13	× • 1	2	2	1	130
L5+00 10+50S	104	15	. 1	5	2	1	90
L5+00 11+00S	124	15	. 1	2	2	2	80
L5+00 11+50S	109	18	.3	5	2	7	110
L5+00 12+00S	81	18	. 1	4	2	2	80
L5+00 12+50S	68	16	. 1	3	2	1	70
L6+00 9+50S	45	21	. 1	2	2	1	50
L6+00 10+00S	78	20	.3	4	2	1	70
L6+00 10+50S	87	17	.2	2	2	8	60
L6+00 11+00S	86	12	. 1	4	2	22	50
L6+00 11+50S	130	10	. 1	5	2	2	90
به مورد المراجع و المراجع و ا	~~						
L6+00 12+00S	22	12	.1	4	3	1	40
L6+00 12+50S	125	14	- 1	5	2	3	100
L7+00 0+00S	113	3	. 1	5	2	1	100
L7+00 0+50S	83	16	.3	5	2	1	90
L7+00 1+00S	16	13	. 1	5	2	3	40
L7+00 1+50S	137	23	. 1	3	2	4	130
L7+00 2+005	88	12	.1	4	3	11	180
L7+00 2+50S	123	14	. 1	2	2	20	80
L7+00 3+005	52	7	.1	2	2	3	100
L7+00 3+50S	72	16	.2	4	2	2	100 90
L/HV0 0H000	14	10	سک ہ	-1	می <i>ک</i> د.	*	/0
L7+00 4+00S	82	17	. 1	2	2	1	110
L7+00 4+50S	196	21	. 1	11	2	5	130
L7+00 5+00S	115	15	. 1	4	2	5	140
L7+00 5+50S	140	23	. 1	6	2	1	90
L7+00 6+00S	51	17	. 1	3	2	1	70
and a constant of the second second				-			
L7+00 6+50S	90	15	. 1	4	2	13	80
STD C/AU-S	58	40	6.9	40	<i>i</i> 17	53	1500

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS , PPM (SB PPM	AU* PPB	HG PPB
L7+00 7+00S	55	13	.2	6	2	3	150
L7+00 7+50S	45	13	.3	6	2	1	90
L7+00 8+00S	40	11	.1	2	2	2	70
L7+00 8+50S		14	.1	2	2	1	70
L7+00 9+00S	64	14	.1	2	2	43	
27400 94003	0**	11	• 1	ii.	<u>~</u>	40	50
L7+00 9+50S	45	4	. 1	4	3	2	60
L7+00 10+00S	76	10	.1	2	2	1	80
L7+00 10+50S	69	21	.2	.2	2	3	60
L7+00 11+00S	115	6	. 1	2	2	13	80
L7+00 11+50S	44	15	.2	ប	23	6	70
L8+00 0+00S	91	10	.2	3	2	3	140
L8+00 0+50S	67	5	. 1	2	2	1	60
L8+00 1+00S	37	14	.2	2	2 2 3	5	50
L8+00 1+50S	59	4	. 1	2	5	1	70
L8+00 2+005	115	2	.2	2	2	4	220
	110	đin	10 dim	din.	<u>~</u>	-	220
L8+00 2+50S	142	9	. 1	7	2	4	90
L8+00 3+00S	81	18	.2	3	2	1	160
L8+00 3+50S	75	10	`.1	5.	2	1	90
L8+00 4+00S	78	10	.3	2	2	2	110
L8+00 4+50S	134	4	.2	6	2	4	130
L8+00 5+00S	115	14	.3	2	2	1	80
L8+00 5+50S	117	7	. 1	4	2	ź	140
L8+00 6+00S	93	13	. 1	4	3	ī	90
L8+00 6+50S	50	8	. 1	3	3	2	80
L8+00 7+005	74	14	.1	7	2	Ĵ	90
	74	T-4	• 1	/	4	U.	70
L8+00 7+50S	107	9	. 1	6	2	4	110
L8+00 8+00S	59	13	.2	2	2	8	90
L8+00 8+50S	122	12	. 1	6	2	1	70
L9+00 0+00S	97	11	. 1	3	2	9	160
L9+00 0+50S	65	16	. 4	6	4	28	80
L9+00 1+00S	132	5	. 1	4	2	4	70
L9+00 1+50S	102	13	. 1	6	2	81	80
L9+00 2+005	112	10	. 1	6	2	3	90
L9+00 2+50S	74	6	. 1	4	2	2	70 '
L9+00 3+00S	95	9	.2	8	2	5	100
L9+00 3+50S	101	13	. 1	7	2	2	160
STD C/AU-S	60	41	7.2	41	17	49	1300
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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L9+00 4+00S L9+00 4+50S L9+00 5+00S L9+00 5+50S L9+00 6+00S	78 102 93 52 58	21 28 22 20 32	. 1 . 1 . 1 . 1	2 2 2 4 2	2 N N N N N N N N N N N N N N N N N N N	1 3 5 4 1	80 70 60 50 90
L9+00 6+50S L9+00 7+00S L9+00 7+50S L9+00 8+00S L9+00 8+50S	102 119 117 68 56	20 24 18 25 28	. 1 . 1 . 1 . 1 . 1	4 3 4 2 2	N N N N N N	5357 Q	100 70 80 60 70
L9+00 9+00S L9+00 9+50S L9+00 10+00S L9+00 10+50S L9+00 11+00S	71 122 74 90 88	28 8 24 27 24	. 1 . 1 . 1 . 1	2 7 5 2 5	2 2 2 3 2 3	3 8 6 2 4	100 110 70 200 130
L9+00 11+50S L9+00 12+00S L9+00 12+50S L9+00 13+00S L9+00 13+50S	51 68 89 67 58	15 11 19 22 13	.1 .1 .1 .1	2 5 3 4	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	8 5 1 2 1	60 100 200 220 90
L9+00 14+00S L9+00 14+50S L9+00 15+00S STD C/AU-S L9+00 15+50S	72 145 89 58 55	28 24 19 40 14	.1 .1 7.1 .1	2 2 38 2	2 2 16 2	3 5 2 54 4	70 80 60 1300 60
L9+00 16+00S L9+00 16+50S L9+00 17+00S L10+00 0+00S L10+00 0+50S	103 48 52 42 77	13 13 16 13 18	.1 .3 .3 .1	5 5 2 3 10	2 4 2 4 2	7 1 4 2 2	50 90 100 70 60
L10+00 1+00S L10+00 1+50S L10+00 2+00S L10+00 2+50S L10+00 3+00S	68 126 70 79 82	18 12 22 16 17	.1 .1 .2 .1 .1	ద ర ర ర	2 2 2 2 2 2	6 2 3 4 3	80 110 120 110 ' 80
L10+00 3+50S L10+00 4+00S L10+00 4+50S	57 71 101	17 12 15	.2 .1 .2	ර ර 4	2 2 2	1 3 6	60 70 160

SAMFLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L10+00 5+00S	72	6	. 1	2	2	1	190
L10+00 5+50S	145	13	. 1	2	2	5	60
L10+00 6+00S	106	4	.3	2	2	2	70
L10+00 6+50S	82	9	.2	2	2 2	1	40
L10+00 7+00S	55	10	.2	5	2	9	80
			• •	-			
L10+00 7+50S	62	10	. 1	3	2	2	70
L#0+00 8+00S	82	2	. 1	3	2	2	90
L10+00 8+505	63	16	. 1	4	2	3	100
L10+00 9+005	49	17	.2	5	2	1	110
L10+00 9+50S	41	6	. 1	7	2	1	70
				-	-	-	00
L10+00 10+00S	57	13	.1	2 4	2	2	80 90
L10+00 10+50S	61	15	. 1		2	1 4	
L10+00 11+005	67	14	. 1	6	2 3		60 80
L10+00 11+50S	88	12	.1	2 2	2	2 1	90 120
L10+00 12+00S	133	18	.2	2	<u></u>	T	120
L10+00 12+50S	93	5	. 1	4	2	2	80
L10+00 13+00S	65	16	. 1	3	2	1	90
L10+00 13+50S	154	` 8	۰.2	2	2	2	110
L10+00 14+00S	129	4	. 1	2. 2	2	3	90
L11+00 0+00S	81	14	. 1	2	2	2	70
STD C/AU-S	59	41	7.0	39	18	48	1400
L11+00 0+50S	103	11	. 1	3	2	2	80
L11+00 1+00S	42	6	.2	2	3	1	50
L11+00 1+50S	64	12	. 1	2	2	8	9 0
L11+00 2+00S	86	12	.3	2	2	4	100
L11+00 3+00S	7 8	10	.2	6	2	3	80
L11+00 3+50S	57	10	.2	6	3	- 1	90
L11+00 4+00S	36	6	. 1	6	4	2	70
L11+00 4+50S	95	15	. 1	5	2	5	90
L11+00 5+00S	85	16	. 1	2	2	10	50
L11+00 5+50S	95	7	. 1	6	2	6	100
L11+00 6+00S	130	20	. 1	7	2	1	80
L11+00 6+50S	66	7	.2	3	2	3	50
L11+00 7+00S	82	12	. 1	2	2	6	100
L11+00 7+50S	94	4	. 1	7	2	1	90
L11+00 8+00S	62	10	. 1	5	2	24	110
L11+00 8+50S	70	6	. 1	2	2	1	120
L11+00 9+00S	45	10	.2	4	2	3	80

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ACME ANALYTICAL LABORATORIES DATE RECEIVED: JUL 24 1987 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED:

GEOCHEMICAL ICP ANALYSIS

.500 GRAN SAMPLE IS DIGESTED WITH 3NL 3-1-2 HCL-HN03-H20 AT 95 DEB.C FOR ONE HOUR AND IS DILUTED TO 10 NL WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-6 SOILS P7-SILT _____ AU&_ANALYSIS BY AA FROM 10 GRAM SAMPLE. H6 ANALYSIS BY FLAMLESS AA.

STETSON RESOURCES PROJECT-IDEAL File # 87-2685 Page 1

SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L0+00 0+25S	44	2	. 1	2	2	17	90
L0+00 0+50S	16	2	. 1	2	2	4	60
L0+00 0+755	46	3	.2	2	2	2	70
L0+00 1+00S	117	4	. 1	2	2	3	110
L0+00 1+25S	84	6	. 1	2	2	Ĵ	120
			• -			-	
L0+00 1+50S	84	2	.2	2	2	1	80
L0+00 1+75S	125	10	.2	4	2	1	100
L0+00 2+00S	96	3	.1	4	2	• 1	60
L0+00 2+25S	63	12	. 1	4	2	2	130
L0+00 2+50S	70	20	×.1	3	2	1	80
L0+00 2+755	72	12	. 1	4	2	13	70
L0+00 3+255	146	18	.2	2	2	10	60
L0+00 3+205	44	16	.2	2	2	1	80
L0+00 3+75S	73	10	.1	5	2	21	70
L0+00 4+00S	81	19	.1	2	2	- 1	60
20100 41003	01	17	• 1	<i></i>	- Aire	1	00
L0+00 4+25S	44	17	.2	2 '	2	1	110
L0+00 4+5 0S	65	18	. 1	2	2	2	80
L0+00 4+75S	81	9	.2	7	2	25	100
L0+00 5+00S	96	11	.1	4	2	1	90
L0+00 5+25S	19	8	. 1	2	2	1	110
L0+00 5+50S	78	13	. 1	2	2	1	100
L0+00 5+75S	55	21	.2	7	2	14	70
L0+00 6+005	118	25	.2	5	2	1	70
L0+00 6+25S	60	16	. 1	3	4	1	60
L0+00 6+50S	38	11	.1	3	2	1	150
						-	1
L0+00 6+75S	94	23	.3	5	4	1	110
L0+00 7+00S	108	32	. 1	3	2	1	90
L0+00 7+25S	77	25	.2	3	3	1	160
L0+00 7+50S	50	24	. 1	2	2	1	50
L0+00 7+75S	61	18	. 1	2	2	1	130
L0+00 8+005	114	32	. 1	5	2	1	100
L0+00 8+25S	202	25	.2	4	2	1	110
L0+00 8+205	157	34	.1	8	2	39	100
L0+00 8+75S	128	29	.2	2	3	1	130
L0+00 9+00S	128	35	.1	5	2	1	120
20400 94003	100		• 1	<u>ل</u>	din.	*	an ann "c"
L0+00 9+25S	234	40	.2	6	2	1	240
STD C/AU-S	57	40	7.3	37	i 17	50	1300

SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L1+00 0+005 L1+00 0+505 L1+00 1+005 L1+00 1+505 L1+00 2+005	114 36 48 101 64	10 2 5 4 4	.3 .1 .1 .2 .2	33 2 2 2 2	2 2 2 2 2 2	17 3 1 2 1	120 70 140 80 150
L1+00 2+50S L1+00 3+00S L1+00 3+50S L1+00 4+00S L1+00 4+50S	58 79 60 52 43	11 4 8 12 13	.2 .1 .3 .3	3 2 4 2 2	2 2 2 2 2 2 2	1 5 1 8	70 90 70 110 100
L1+00 5+00S L1+00 5+50S L1+00 6+00S L1+00 6+50S L1+00 7+00S	144 33 18 71 70	10 7 6 5 12	.3 .1 .1 .1	7 2 3 5 5	2 2 2 2 2 2	2 1 1 2 1	70 80 90 130 180
L1+00 7+50S L1+00 8+00S L1+00 8+50S L1+00 9+00S L1+00 9+50S	86 135 97 131 87	11 4 17 12 5	×.2 .2 .2 .3 .3	659 946	2 2 2 2 2 2 2	1 1 1 2	150 100 140 60 130
L1+00 10+00S L1+00 10+50S L1+00 11+00S L1+00 11+50S L1+00 12+00S	126 73 59 52 79	2 2 2 7 7	.3 .2 .3 .3 .3	833 750 750	2 2 2 2 2 2 2 2	1 9 2 1 3	110 80 70 80 60
L1+00 12+50S L1+00 13+00S L1+00 13+50S L1+00 14+00S L1+00 14+50S	85 77 39 109 25	5 13 3 4 6	.3 .3 .1 .3	8 6 2 4 5	2 2 2 2 2	1 1 1 1	120 90 70 160 50
L1+00 15+00S L2+00 0+00S L2+00 0+50S L2+00 1+00S L2+00 1+50S	153 110 145 105 69	9 6 2 5 8	.1 .2 .1 .1 .2	5 5 10 5 5	2 2 2 4	1 7 4 9	110 120' 110 130 100
L2+00 2+00 S STD C/AU-S	97 59	6 40	.2 6.7	3 38	4 17	2 54	90 1400

SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L2+00 2+50S L2+00 3+00S L2+00 3+50S L2+00 4+00S L2+00 4+50S	60 59 37 15 53	13 18 12 11 14	. 1 . 1 . 1 . 1 . 1	- 5 2 2 2 2	2 2 2 2 2 2 2 2	2 2 3 1 5	160 170 100 30 50
L2+00 5+00S L2+00 5+50S L2+00 6+00S L2+00 6+50S L2+00 7+00S	41 41 111 49 49	7 9 21 16 6	. 1 . 1 . 2 . 1 . 1	2 2 7 4 3	2 2 4 2 2	1 4 62 2 1	50 80 130 120 120
L2+00 7+50S L2+00 8+00S L2+00 8+50S L2+00 9+00S L2+00 9+50S	45 74 85 120 60	13 14 15 19 16	. 1 . 1 . 1 . 1 . 1	2 2 2 4	2 2 2 2 2 2 2	1 1 1 1	80 130 100 70 90
L2+00 10+00S L2+00 10+50S L2+00 11+00S L2+00 11+50S L2+00 12+00S	105 88 140 41 115	18 17 23 13 18	.1 .2 .1	52725	2 2 2 2 2 2 2	1 2 1 1 2	130 90 90 70 90
L2+00 12+50S L2+00 13+00S L2+00 13+50S L2+00 14+00S L2+00 15+00S	52 26 126 92 76	12 13 18 22 18	.2 .1 .1 .1 .1	2 5 3 2 3	N N N N N N N N	1 2 5 2 2	60 60 100 70 80
L2+00 15+50S L2+00 16+00S L3+00 0+00S L3+00 0+50S L3+00 0+50S A	106 50 36 237 238	21 18 17 23 24	.1 .1 .1 .2	័្រភេខ។ខ	3 2 2 2 2 2	1 995 265 3	120 70 150 60 70
L3+00 1+00S L3+00 1+50S L3+00 2+00S L3+00 2+00S A L3+00 3+00S	81 120 50 73 63	18 23 14 15 15	.1 .1 .1 .2	2 4 3 4	2 2 3 2 2 2	2 2 3 4 4	60 110 130 420 120
L3+00 3 +50S STD C/AU-S	25 62	11 40	.1 7.2	4 38	3 17	11 53	60 1300

SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L3+00 4+00S	104	14	. 1	З	2	2	120
L3+00 4+50S	100	14	. 1	2	2	1	100
L3+00 5+50S	117	12	. 1	4	2	1	110
L3+00 6+00S	55	9	. 1	2	2	51	130
L3+00 6+50S	27	13	. 1	2	2	17	110
#-							
L3+00 7+00S	82	14	. 1	2	2	1	220
L3+00 7+50S	56	20	.2	4	2	1	100
L3+00 8+00S	77	13	. 1	4	2	1	120
L3+00 8+50S	56	13	. 1	3	2	1	150
L3+00 9+00S	43	16	.2	4	2	1	90
L3+00 9+50S	152	21	. 1	4	2	2	120
L3+00 10+00S	83	11	. 1	4	2	1	70
L3+00 10+50S	71	15	. 1	5	2	3	80
L3+00 11+00S	80	7	. 1	2	2	1	110
L3+00 11+50S	96	18	. 1	5	2	2	80
L3+00 12+00S	59	11	×.2	2	2	1	90
L3+00 12+50S	70	8	. 1	3.1	2	6	60
L3+00 13+00S	24	7	. 1	2	3	2	40
L3+00 13+50S	140	14	. 1	2	2	2	110
L3+00 14+00S	67	8	. 1	4	3	2	140
L3+00 14+50S	63	12	. 1	2	2	1	110
L3+00 15+00S	140	18	. 1	4	2	1	130
L4+00 0+00S	132	11	. 1	6 '	2	6	100
L4+00 0+50S	90	18	.2	5	3	3	90
L4+00 1+00S	123	15	. 1	5	2	2	150
L4+00 1+50S	37	9	. 1	2	2	1	120
L4+00 2+00S	182	13	. 1	7	2 2	2	110
L4+00 2+50S	39	10	.1	2	2	2	50
L4+00 3+00S	130	14	.2	2	2	1	80
L4+00 3+50S	106	9	- 1	3	2	2	200
L4+00 4+00S	35	14	.3	2	2	1	80
L4+00 4+50S	32	10	.2	3	2	3	90'
L4+00 5+00S	49	12	. 1	2	5	6	60
L4+00 5+50S	69	15	. 1	4	3	4	170
L4+00 6+00S	109	15	. 1	5	2	1	100
L4+00 6+50S	108	12	.2	8	2	1	130
STD C/AU-S	62	41	7.4	41	17	51	1400

SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L4+00 7+00S	115	6	.2	6	2	4	160
L4+00 7+50S	79	11	.3	2	2	8	140
L4+00 8+00S	52		. 1	2	2	3	150
L4+00 8+50S	44	6	.2	2	3	1	160
L4+00 9+005	24	6	.1	2	2	1	60
	۳ ⁻ ۳	6	• ±	4	d	*	00
L4+00 9+50S	107	15	.2	2	2	1	120
L5+00 0+00S	73	10	.2	3	3	17	90
L5+00 0+50S	72	15	.3	2	2	2	130
L5+00 1+00S	29	8	.2	2	2	1	80
L5+00 1+50S	38	12	.3	2,	2	1	100
L5+00 2+00S	178	26	.2	9	2	1	70
L5+00 2+50S	33	14	.4	ź	3	1	110
L5+00 3+00S	76	13	.1	3	2	2	100
L5+00 3+50S	115	21	.2	3	2	2	210
L5+00 4+005	79	17	.2	7	2	1	210 90
LJ+00 4+005	/7	17	• ***	/	<u>~</u>	Ţ	70
L5+00 4+50S	34	11	.2	3	2	2	70
L5+00 5+00S	109	14	. 1	2	2	1	120
L5+00 5+50S	134	21	. 1	6	2	2	100
L5+00 6+00S	115	22	. 4	4	2	1	230
L5+00 6+50S	122	25	`. 2	8	2	1	110
L5+00 7+00S	77	22	. 1	5	2	2	100
L5+00 7+50S	61	19	.3	6	2	1	80
L5+00 8+00S	39	10	. 1	2	$\overline{2}$	1	60
L5+00 8+50S	57	17	. 1	2	2	1	120
L5+00 9+005	40	22	.1	3	2	1	90
	10	alan alan	• -		-	*	
L6+00 0+00S	118	19	. 4	5	2	1	110
L6+00 0+50S	132	24	.2	2	2	2	120
L6+00 1+00S	124	25	.2	2	2	3	130
L6+00 1+50S	53	16	. 1	2	2	2	110
L6+00 2+00S	107	23	. 1	2	2	7	100
L6+00 2+50S	119	21	.2	4	2	1	120
L6+00 3+00S	117	21	.2	5	2	1	70
L6+00 3+50S	82	19	. 1	4	2	5	60
L6+00 4+00S	112	29	.2	2	2 2	1	130
L6+00 4+50S	20	12	.2	2	3	1	100,
unn uar thattar 8 thad faithad		e , d		-	-	-	!
L6+00 5+00S	110	24	. 1	4	2	1	110
STD C/AU-S	60	40	7.4	41	16	48	1500

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SAMPLE#	CU	PB	AG	AS	SB	AU*	HG
	PPM	PPM	PPM	PPM	PPM	PPB	PPB
L6+00 5+50S L6+00 6+00S L6+00 6+50S L6+00 7+00S ▲6+00 7+50S	66 49 146 85 92	2 10 5 11 12	.4 .2 .4 .3	6 8 10 3	5 4 8 7	1 14 3 2 1	100 120 180 150 130
L6+00 8+00S	98	14	.2	11	6	1	70
L6+00 8+50S	60	12	.1	3	4	1	50
L6+00 9+00S	92	16	.3	5	3	12	100
STD C/AU-S	61	40	7.0	38	17	48	1400

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SAMPLEN	NO Ppn	CU PPM	PB PPM	ZN PPM	AG PPH	NI PP N	CO PPN	MN PPH	FE Z	AS PPN	U PPN	AU Ppn	TH PPN	SR PPN	CD PPN	SB PPN	BI PPM	V PPH	CA Z	P Z	LA PPN	CR PPM	MG X	BA PPM	11 7	B PPM	AL Z	NA Z	K Z	N PPM	AU# PPB	
1A-CR-2-ET 0+00		115	20	75		47		445	4 43			ыņ	.	17		2	•	100		420		00	· · ·	~~ 17			2.04	47	A7	1	3	
18-CR-1-EAST 0-M'S	1	180	15	111	.1 .1	63 66	22 23		6.62 6.81	5	5	NÐ ND	2	23 35		2	2	190		.029	5		2.16	23	.43 .38		2.94 3.31	.03	.03	2	2650	
2A-CR-2-ET 0+250	1	113	13	68	.1	58	23		6.89	3	5	ND	4	23	1	2	3 2	200	1.19		5		1.97 2.07	39 23	. 46		3.00	.03 .03	.03 .02	1	2030	
3A-CR-2-ET 0+500	1	168	13	85	.1	80		1398		3	5	ND		23 32	1	2	2				7		2.50	23 54	. 10			.03	.02	1		
4A-CR-2-ET 1+000	1		11	92	.1	70	31		9.62	14	5	ND	2	28	1	2	2		1.09		6		2.50	34 37	.27		4.00 3.41	.02	.04		2050	
4M-CK-2-E1 14000	1	217		12	• •	70	31	073	7.02	14	3	80	2	20	1	2	2	701	1.11	.040	0	77	2.00	37	. 37	7	3.41	. VI		3	2030	
5A-CR-2-ET 1+250	1	231	17	94	.1	68	31	910	9.29	13	5	ND	1	26	1	2	2	257	1.03	.038	6	89	2.69	37	.35	8	3.57	.02	.05	2	225	
SILT 41 OH'S	2	124	14	62	.1	38	21		6.62	6	6	ND	2	38	1	2	2	171		.045	6		1.93	40	.26		3.07	.02	.04	2		
SILT #2 0+250	i	147	9	86	.1	53	26	874	7.71	6	5	ND	1	35	1	2	2	224	1.08	.030	5	64	2.22	27	.47	8	3.28	.02	.04	1	1	
SILT #3 0+500	1	144	13	80	.1	52	25	888	7.37	7	5	ND	2	36	1	2	2	218	1.17	.032	- 4	67	2.11	27	.47	9	3.22	.02	.03	2	66	
SILT #4 0+750	1	137	7	83	.2	55	26	853	7.89	3	5	ND	1	37	1	2	2	238	1.20	.029	4	73	2.23	30	.51	7	3.28	.02	.03	3	26	
SILT #5 1+000	1	153	10	82	.1	53	25		7.18	6	5.	ND	1	40	1	- 4	2			.034	5		2.16	31	.45		3.44	.02	.05	1	6	• •.
SILT #6 1+200	2	129	9	63	.1	46	23	960	6.66	9	5	ND	<u></u> 1	41	1	3	2	161			8		2.26	42	.14		3.51	.02	.07	1	61	
SILT #7 1+250	1	129	6	82	.1	49	26	848	7.63	6	5	ND	2	36	1	2	2	218	1.12	.032	5	63	2.25	32	.44	?	3.35	.02	.04	2	1	
SILT #8A 1+565	1	111	9	89	.1	45	26	850	6.98	- 4	5	ND	2	28	1	2	2	166	1.01	.035	5	57	2.72	34	.34	9	3.51	.03	.06	1	1	
SILT #9 1+750	1	134	5	79	.1	45	24	891	7.79	5	5	ND	1	38	1	2	2	221	1.09	.042	6	64	2.17	37	.36	7	3.33	.02	.05	1	1	
SILT #10 2+000	1	121	15	79		= 1	-05	045	7.00		E	AUD.		70		•				470			0.50	•,	**	-	7 17	47			05	
SILT #11 2+250	1	130	15	86	.1	51 49	25 26		7.98	4	5 5	ND ND	1	39 37	1	2		226		.032	5	67	2.29 2.38	36	.33 .39		3.47 3.27	.03	.04		25 17	
SILT #12 2+500	1	125	5	78	.1	47 55	25		6.98	7	ວ 5		1	-	1	23	23				3			33				.03		1		
SILT #13 2+750	1	120	16	70	.1	58	26		B.0 0	6	5 5	ND,		38 36	1	-	2	190 237		.028	2 5		2.38 2.43	35	.35 .39		3.38	.03	.04	2		
SILT #13 3+000	2		8	76	.1	69	25		7.95	7	5	ND		30		2	2							31	.37		3.21 3.33	.03 .03	.05	1		
31C1 #13 37000	4	120		/0	•1	67	23	/ 33	7.73	3	9	ND	1	31	1	2	4	231	1.08	.034	5	101	2.55	31	. 37	17	3.33	.03	.03	1	ు	
SILT #15 3+250	1	119	6	79	.1	62	26	791	7.80	3	5	NÐ	1	38	1	2	2	226	1.10	.040	5	92	2.56	31	.41	19	3.34	04	.04	1	1	
SILT #16 3+500	1	126	14	78	.1	63	25	841	8.04	. 9	5	ND	2	39	1	2	- 4	236	1.17	.046	6	97	2.50	33	.41	16	3.36	.04	.05	1	118	
SILT #17 3+750	1	124	17	74	.1	59	26	779	8.44	7	5	ND	1	46	1	2	2	266	1.28	.048	6	98	2.55	32	.44	16	3.24	,07	.04	2	495	
SILT #18 4+000	£	128	12	76	.1	67	24	769	7.54	5	5	ND	2	45	1	2	2	223	1.28	.039	5	103	2.69	33	.42	16	3.35	.07	.04	1	9	
SILT #19 4+250	1	124	13	76	.1	69	25	779	7.86	8	5	ND	2	47	1	2	2	232	1.33	.047	5	103	2.77	36	.42	- 14	3.43	.07	.04	1	1	
SILT #20 4+500		104	.,	77	•			770	7		,					-	-				-											
SILT #20 4+300 SILT #21 4+750	1	104	16	73	.2	64	24		7.08	4	5	ND	1	45	1	2	2		1.27		5		2.84	33	.39		3.38		.04	1	. 1	
	2	106	11	63	.1	63	22		6.17	2	5	ND	2	43	1	2	2		1.26		5		2.43	32	.37		3.05	.06	.04	1	. 1	
SILT #22 5+000	1	115	3	74	.1	65	22		6.97	5	5	ND	2	46	1	2	2		1.36		5		2.55	31	.43		3.11	.07	.05	1	17	
STD C/AU-S	18	62	40	128	7.4	68	28	944	4.05	41	19	8	39	52	18	18	21	57	.51	.086	39	60	.92	185	.08	36	1.75	.07	.14	12	53	

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DATE RECEIVED: ACME ANALYTICAL LABORATORIES LTD. OCT 5 1987 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE (604) 253-3158 FAX (604) 253-1716 DATE REPORT MAILED:

GEOCHEMICAL ICP ANALYSIS

- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER:

Dauges. DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON Page 1

l	RESOURCES File # 87-	4765
	SAMPLE# Ideal	AU* ppb
	CLOUTSIE CK STA 0+00 CLOUTSIE CK STA 0+00A CLOUTSIE CK STA 0+00B CLOUTSIE CK STA 1+00 CLOUTSIE CK STA 1+00A	18 22 42 290 69
	CLOUTSIE CK STA 1+00B CLOUTSIE CK STA 2+00 CLOUTSIE CK STA 2+00A CLOUTSIE CK STA 2+00B CLOUTSIE CK STA 2+00B CLOUTSIE CK STA 3+00	11 55 49 1035 9
	CLOUTSIE CK STA 3+00A CLOUTSIE CK STA 3+00B CR #7 STA 0+00 CR #7 STA 0+00A CR #7 STA 0+00B	260 12 102 190 1715
	CR #7 STA 1+00 CR #7 STA 1+00A CR #7 STA 1+00B CR #7 STA 2+00 CR #7 STA 3+00	530 205 28 74 80
	CR #7 STA 4+00 CR #7 STA 4+00A CR #7 STA 4+00B CR #7 STA 5+00 CR #7 STA 5+00A	270 29 180 39 49
	CR #7 STA 5+00B CR #7 STA 6+00 CR #7 STA 6+00A CR #7 STA 6+00B CR #7 STA 6+00B	645 220 79 35 117
:	CR #7 STA 7+00A CR #7 STA 7+00B CR #7 STA 8+00 CR #7 STA 8+00A CR #13 STA 0+00	130 23 50 168 1475
	CR #13 STA 0+00A	835

SAMPLE#	AU* ppb
CR #13 STA 0+00B CR #13 STA 1+00 CR #13 STA 1+00A CR #13 STA 1+00B CR #13 STA 1+00B CR #13 STA 2+00	18 890 2460 525 36
CR #13 STA 2+00A	52
CR #13 STA 2+00B	25
CR #13 STA 3+00	205
CR #13 STA 3+00A	107
CR #13 STA 3+00B	67
CR #13 STA 4+00	31
CR #13 STA 4+00A	22
CR #13 STA 4+00B	30
CR #13 STA 5+00	540
CR #13 STA 5+00A	265
CR #13 STA 5+00B	41
L1+90E STA 5+90S	3
L1+90E STA 5+95S	1
L1+90E STA 6+00S	1
L1+90E STA 6+05S	9
L1+90E STA 6+10S	3
L1+95E STA 5+90S	5
L1+95E STA 6+00S	1
L1+95E STA 6+05S	44
L1+95E STA 6+10S	23
L2+00E STA 5+90S	1
L2+00E STA 5+95S	210
L2+00E STA 6+00S	1
L2+00E STA 6+05S	1
L2+00E STA 6+10S	1
L2+05E STA 5+90S	1
L2+05E STA 5+95S	• 1
L2+05E STA 6+00S	49
L2+05E STA 6+05S	42
L2+05E STA 6+10S	1
L2+10E STA 5+90S	11

SAMPLE#

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pob	

L2+10E	STA	5+955	1
L2+10E	STA	6+00S	1
L2+10E	STA	6+055	1
L2+10E			1
L2+90E			2
han din ' / 'n' han	UIH	.	-
L2+90E	STO	54050	8
L2+90E			1
L2+90E			1
L2+90E			1
L2+90E	STA	455	1
L2+90E	STA	SAC	1
L2+90E			1
L2+90E			
			1
L2+95E			22
L2+95E	STA	5+955	1
L2+95E	стл	44000	59
L2+95E			1
		``	
L2+95E			1
L2+95E			1
L2+95E	STA	45S	34
L2+95E	CTA	500	5
L2+95E			12
L2+95E			12
L3+00E			10
L3+00E			10
LSTUDE	BIH	3+735	1
L3+00E	STA	6+005	1
L3+00E			1
L3+00E			13
L3+00E			1
L3+00E		455	1
	w r i i	1,202	- .
L3+00E	STA	50S	1
L3+00E	STA	555	2
L3+00E	STA	60S	1
L3+05E	ST 5	5+90S	8
L3+05E	ST 5	5+955	1
L3+05E	ST é	6+00S	5

SAMPLE	ŧ	AU* ppb
L3+05E L3+05E L3+05E	ST 6+05S ST 6+10S ST 40S ST 45S ST 50S	9 1 2 3 3
L3+05E L3+10E L3+10E	ST 555 ST 605 ST 5+905 ST 5+955 ST 6+005	2 1 1 5
L3+10E L3+10E L3+10E	ST 6+05S ST 6+10S STA 40S STA 45S STA 50S	1 2 1 14
L3+10E L6+90E L6+90E		1 1 2 1 6
L6+90E L6+90E L6+95E L6+95E L6+95E	9+10S 8+90S 8+95S	1 1 6 10
L6+95E L6+95E L7+00E L7+00E L7+00E	9+10S 8+90S 8+90S	2 1 14 12 2
L7+00E L7+00E L7+05E L7+05E L7+05E		2 2 1 2 2

L7+05E 9+05S

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terf (1.2. 3.1. term that it	ppb
L7+05E 9+10S L7+10E 8+90S L7+10E 8+95S L7+10E 9+00S L7+10E 9+05S	1 2 1 1
L7+10E 9+10S L8+90E ST 1+40S L8+90E ST 1+45S L8+90E ST 1+50S L8+90E ST 1+55S	2 2 2 2 2 2
L8+90E ST 1+60S L8+95E ST 1+40S L8+95E ST 1+45S L8+95E ST 1+50S L8+95E ST 1+55S	2 5 64 2 1
L8+95E ST 1+60S L9+00E ST 1+40S L9+00E ST 1+45S L9+00E ST 1+50S L9+00E ST 1+55S	3 2 3 3 2 3 2
L9+00E ST 1+60S L9+05E ST 1+40S L9+05E ST 1+45S L9+05E ST 1+50S L9+05E ST 1+55S	5 2 18 4 1
L9+05E ST 1+60S L9+10E ST 1+40S L9+10E ST 1+45S L9+10E ST 1+50S L9+10E ST 1+55S	5 40 2 2 1
L9+10E ST 1+60S L12+90E ST 4+90S L12+90E ST 4+95S L12+90E ST 5+00S L12+90E ST 5+05S	1 1 2 2 2
L12+90E ST 5+10S	2

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SAMF'LE#		AU* ppb
L12+90E L12+90E L12+90E L12+90E L12+90E L12+90E	5+45S 5+50S	80 4 17 12 5
L12+90E L12+90E L12+90E L12+90E L12+90E L12+90E	12+90S 12+95S 13+00S 13+05S 13+10S	1 3 1 8 2
L12+90E L12+90E L12+90E L12+90E L12+90E L12+90E	13+40S 13+45S 13+50S 13+55S 13+60S	1 4 1 2 15
L12+95E L12+95E L12+95E L12+95E L12+95E	ST 4+90S ST 4+95S ST 5+00S ST 5+05S ST 5+05S ST 5+10S	3 1 1 3 1
L12+95E L12+95E L12+95E L12+95E L12+95E	ST 5+40S ST 5+45S ST 5+50S ST 5+55S ST 5+60S	1 260 36 250 72
L12+95E L12+95E L12+95E L12+95E L12+95E L12+95E	12+95S 13+00S 13+05S	2 18 8 12 1
L12+95E L12+95E L12+95E L12+95E L12+95E L12+95E	13+45S 13+50S 13+55S	9 1 3 1
L13E 124	-905	1

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SHULCH	ppb
L13E 12+95S L13E 13+00S L13E 13+05S L13E 13+10S L13E 13+10S L13+00E ST 4+90S	1 1 4 1
L13+00E ST 4+95S L13+00E ST 5+00S L13+00E ST 5+05S L13+00E ST 5+10S L13+00E ST 5+40S	1 1 1 18
L13+00E ST 5+45S L13+00E ST 5+50S L13+00E ST 5+55S L13+00E ST 5+60S L13+00E ST 13+40S	6 25 189 102 9
L13+00E ST 13+45S L13+00E ST 13+50S L13+00E 13+55S L13+00E 13+60S L13+05E ST 4+90S	3 1 5 1 2
L13+05E ST 4+95S L13+05E ST 5+00S L13+05E ST 5+05S L13+05E ST 5+10S L13+05E ST 5+40S	1 1 2 1
L13+05E ST 5+45S L13+05E ST 5+50S L13+05E ST 5+55S L13+05E ST 5+60S L13+05E 12+90S	1 192 128 5
L13+05E 12+95S L13+05E 13+00S L13+05E 13+05S L13+05E 13+10S L13+05E 13+40S	14 1 51 25 4
L13+05E 13+45S	2

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		ppo
L13+05E L13+05E L13+05E L13+10E L13+10E	13+55S 13+60S	1 2 5 1 1
L13+10E L13+10E L13+10E L13+10E L13+10E L13+10E	ST 5+008 ST 5+058 ST 5+108 ST 5+408 ST 5+458	3 1 10 31 96
L13+10E L13+10E L13+10E L13+10E L13+10E	ST 5+50S ST 5+55S ST 5+60S 12+90S 12+95S	158 149 108 4 1
L13+10E L13+10E L13+10E L13+10E L13+10E L13+10E	13+05S 13+10S	7 4 5 1 4
L13+10E L13+10E L13+10E L13+00E L14+00E L14+00E	13+50S 13+55S 13+60S STA 14+00S STA 14+50S	1 1 1 1 1
L14+00E L14+00E L14+00E L15+00E L15+00E	STA 15+00S STA 15+50S STA 16+00S STA 13+50S STA 14+00S	1 2 1 1 1
	12+955	3 1 1 1 4
L15+90E	13+055	1

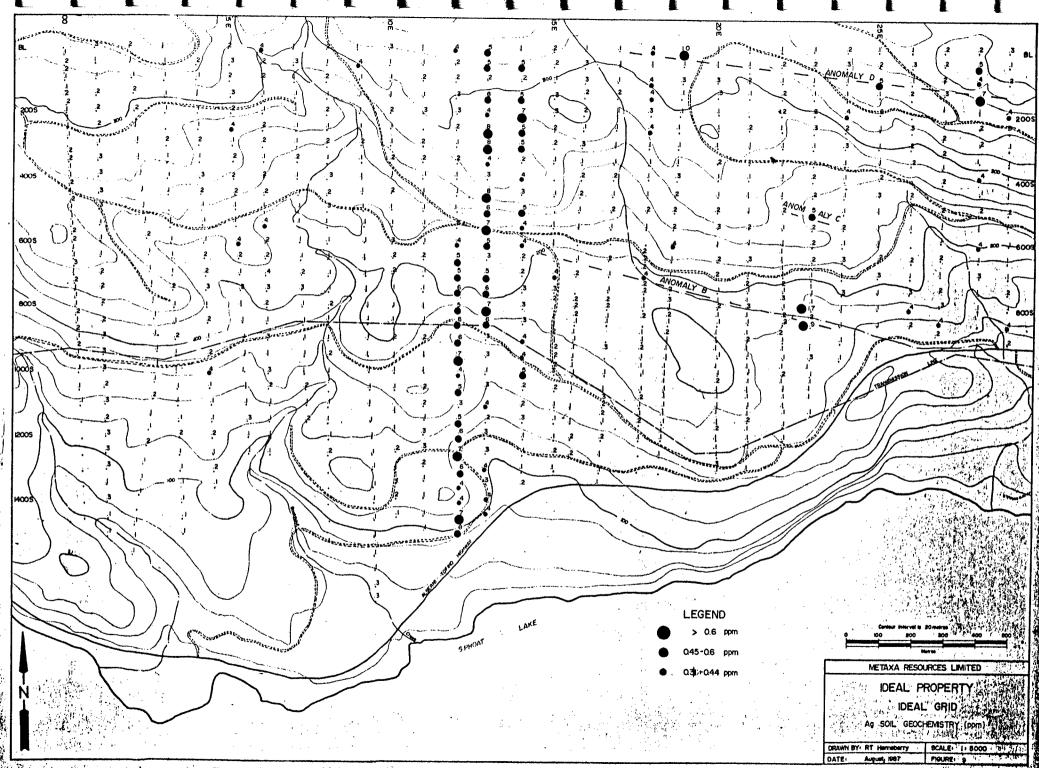
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		ppb
L15+90E L15+95E L15+95E L15+95E L15+95E	12+905 12+955 13+005	1 3 1 6 3
L15+95E L16+00E L16+00E L16+00E L16+00E	12+905 12+905A 12+955	4 2 7 2 4
L16+00E L16+00E L16+00E L16+00E L16+05E	14+50S 15+00S 15+50S	1 1 1 4
L16+05E L16+05E L16+05E L16+10E L16+10E	13+05S 13+10S >	5 5 3 4 2
L16+10E L17+00E L17+00E L17+00E L17+00E	13+50S 14+00S 14+50S	3 9 3 11 4
L17+00E L18+00E L18+00E L18+00E L18+00E	STA 13+00S STA 13+50S	59 76 6 3 4
L18+00E L19+00E L19+00E L19+00E L19+00E L19+00E	13+50S 14+00S 14+50S	4 34 36 98 45
L19+50E	12+005	2

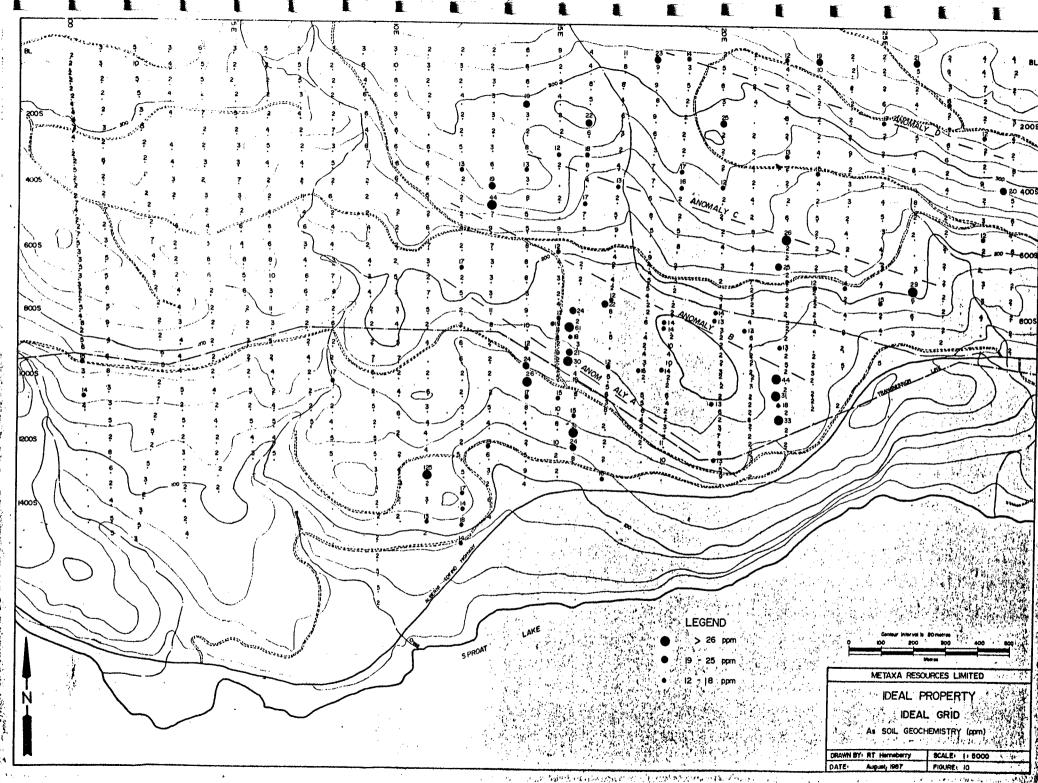
SAMPLE#	AU* ppb
L19+50E 12+50S	2
L19+50E 13+00S	1
L19+50E 13+50S	16
L19+50E 14+00S	51
L19+50E 14+50S	11
L19+50E 15+00S	1
L19+50E 15+50S	1
L20+00E 13+50S	5
L20+00E 14+00S	4
L20+00E 14+50S	1
L20+00E 15+00S	15
L20+00E 15+50S	12
L21E 13+50S	11
L21E 14+00S	2
L21E 14+50S	11
L21E 15+00S	2
L22E 12+50S	9
L22E 13+00S >	4
L22E 13+50S	3

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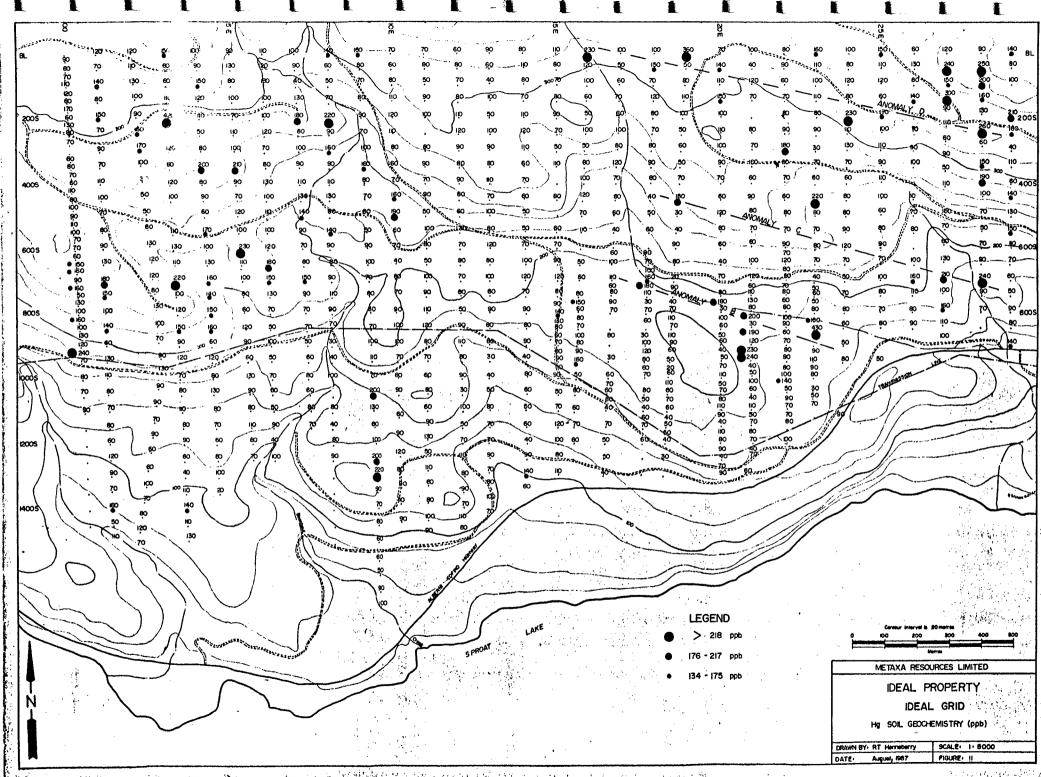
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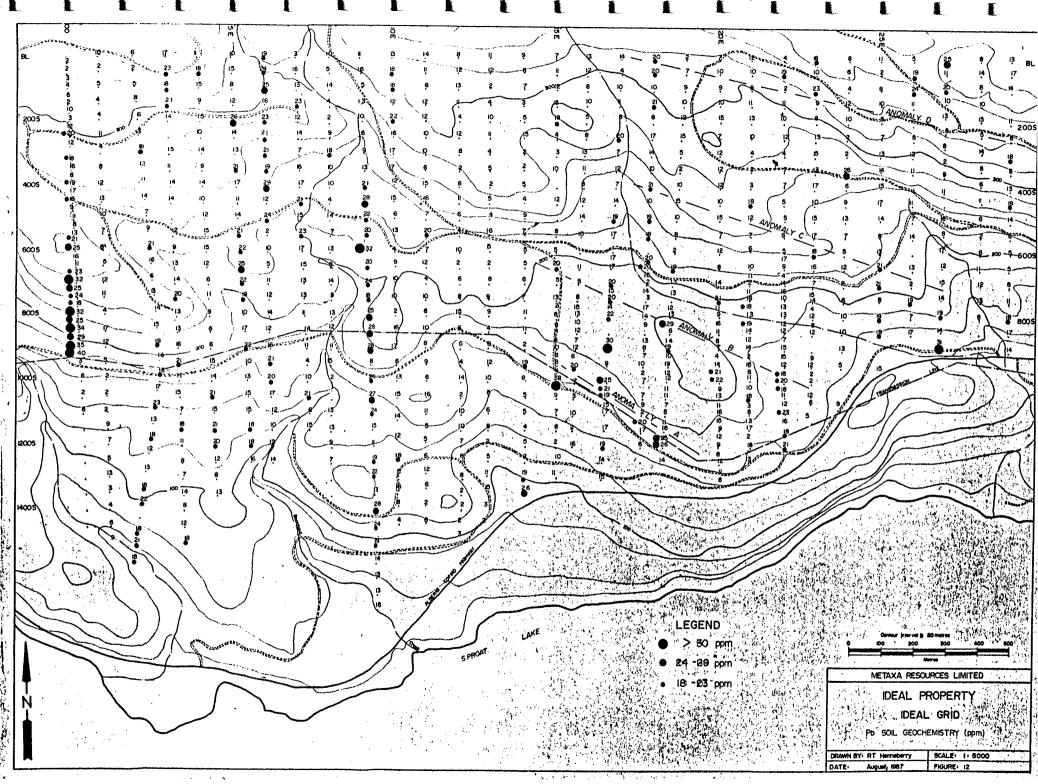
the second states that the second states of the state between the states of the second states and the second states of the second state

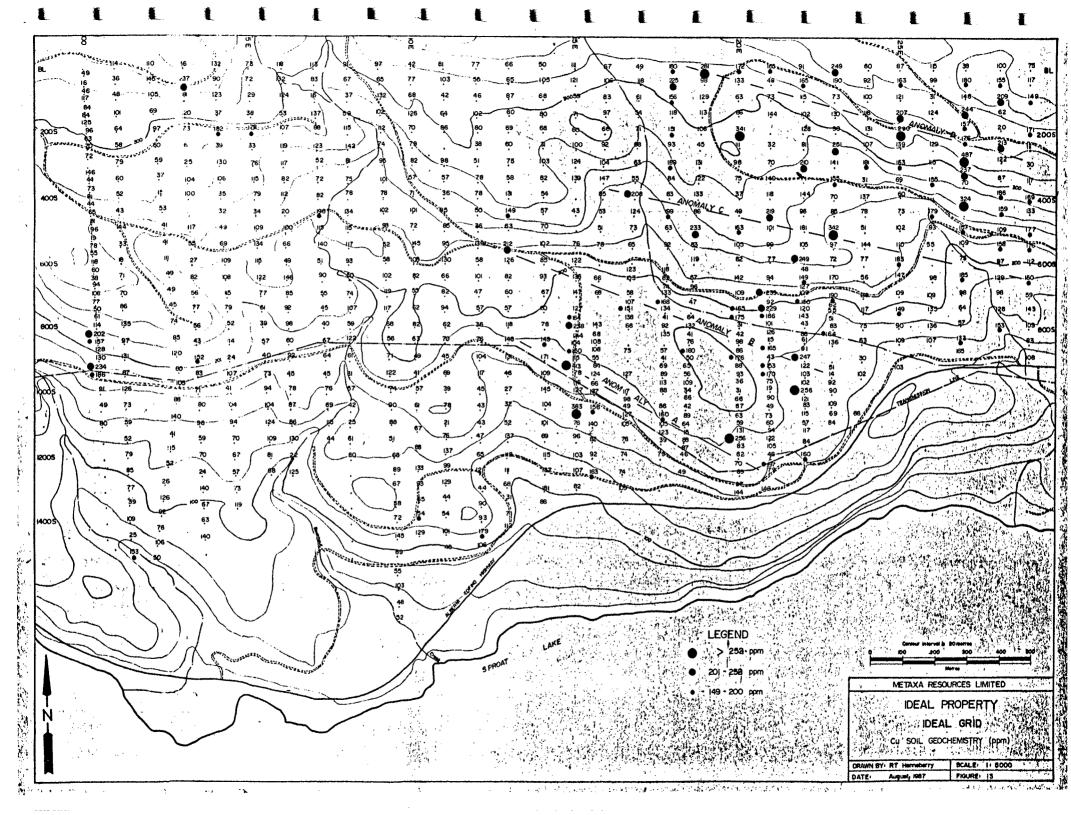
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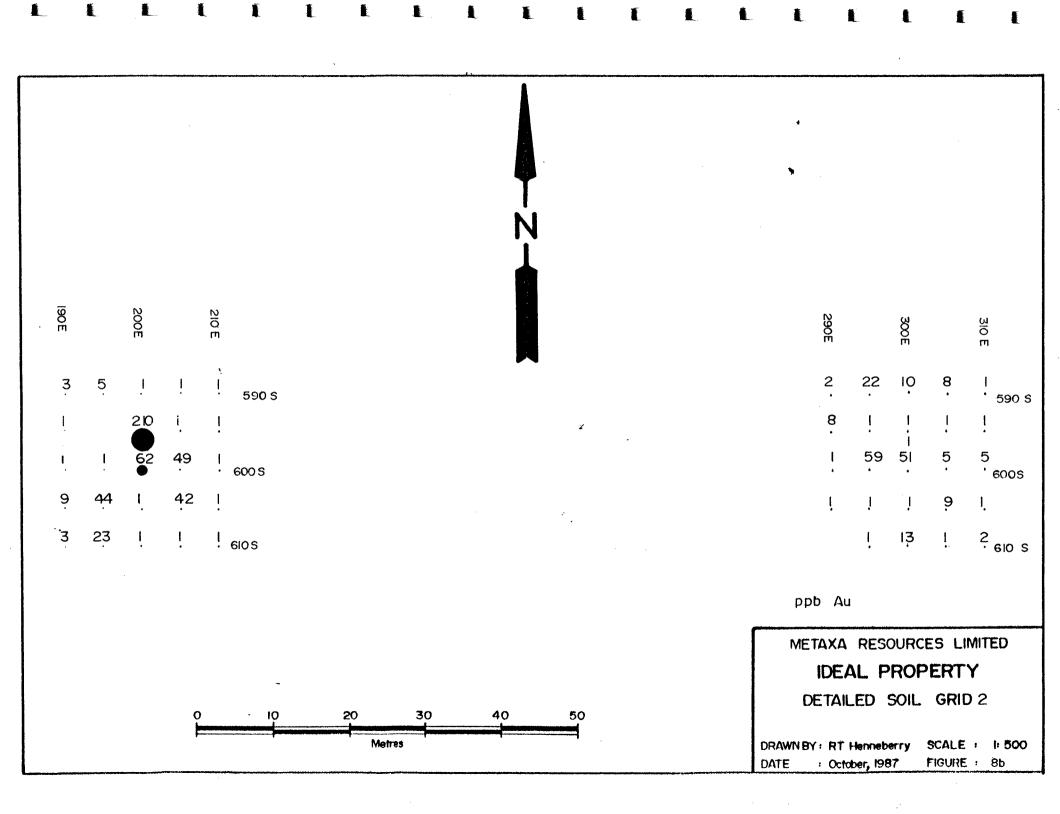


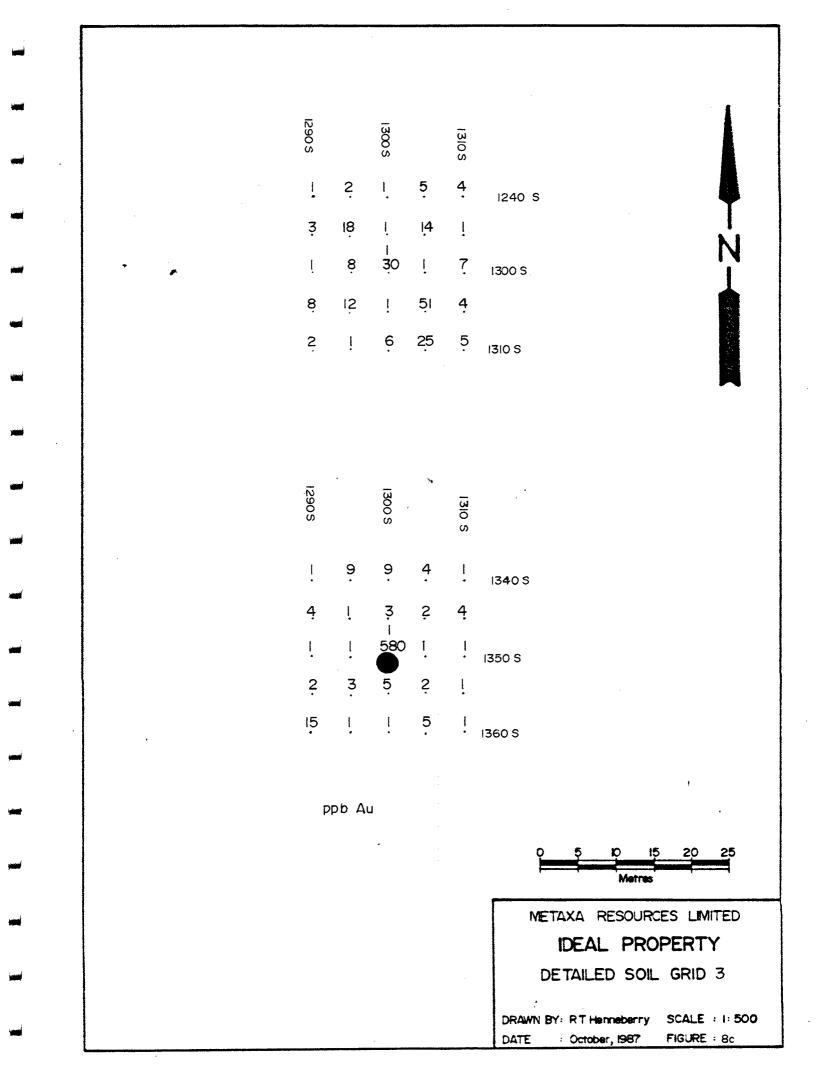
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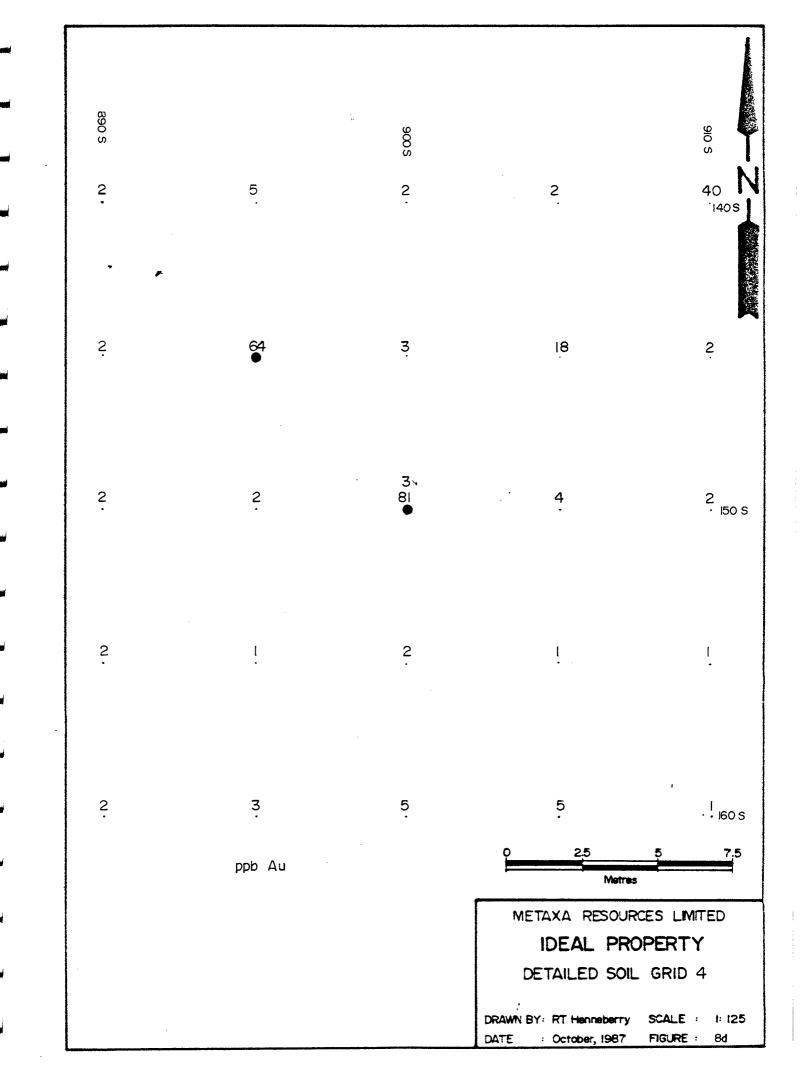
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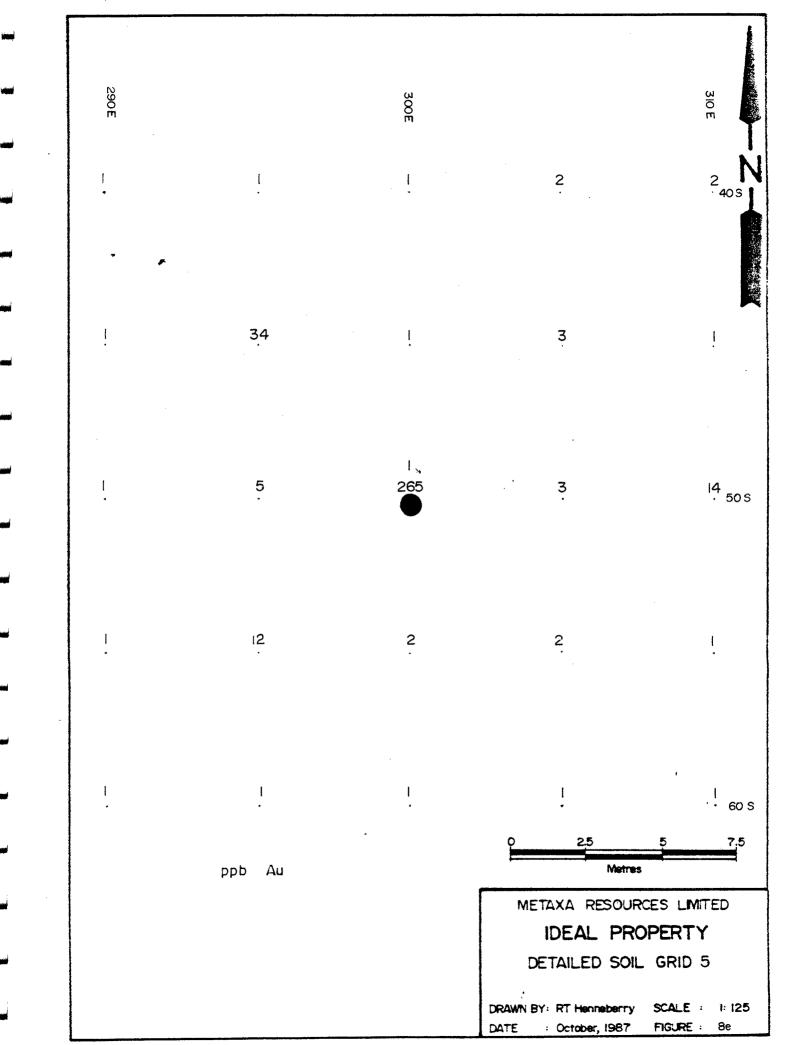




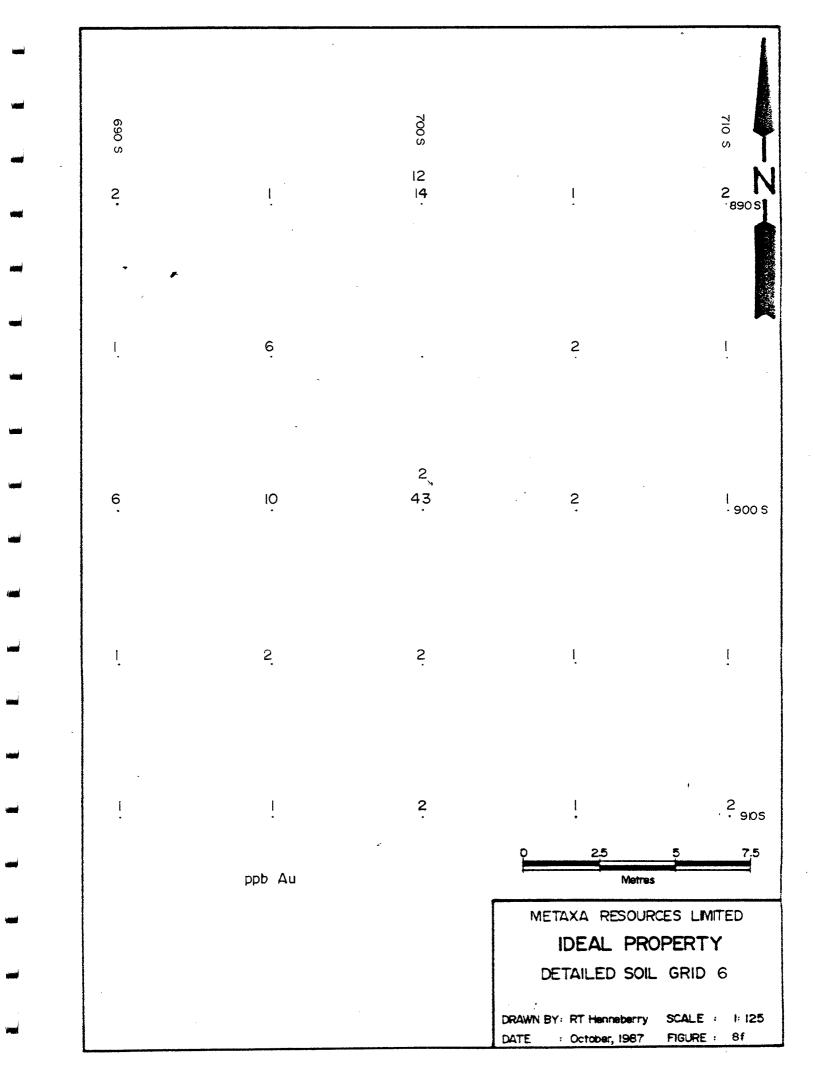


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ACME ANALYTICAL LABORATORIES DATE RECEIVED: APRIL 6,1987 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED: 48/87

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips

ASSAYER: DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCES MANAGEMENT PROJECT-IDEAL File # 87-0907A

SAMPLE#	AG**	AU**
	OZ/T	OZ/T
50530	.02	.040
50531	.02	.042
50532	.03	.189
50533	.09	.027
50534	.02	.019
50535	.01	.019
50536	.01	.001
50537	`. 03	.039
50538	.01	.009
50539	.01	.001
50540	.02	.074
50541	.01	.309

ACME ANALYTICAL LABORATORIES

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 FHONE 253-3158

DATA LINE 251-1011

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GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P CR MG BA TI B AL NA K W SI ZR CE SN Y NB AND TA. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: Rock Chips Aut ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: APRIL 6 1987 DATE REPORT MAILED: 4088/87 ASSAYER

STETSON RESOURCES MANAGEMENT PROJECT - IDEAL File # 87-0907

SAMPLE#	ND PPM		PB PPM	ZN PPM	AG PPM	NI PPM	CO PPN	MN PPH	FE %	AS PPM	U PPM	AU PPM	TH Ppm	SR PPH	CD PPM	SB Ppn	BI PPM	V PPM	CA %	P X	LA PPM	CR PPM	M5 %	BA PPM	11 %	B PPM	AL 7.	NA 7.	K Z	W PPM	au‡ PPB
50526	1	81	2	31	.1	55	13	608	4.00	4	5	ND	1	1	1	5	2	117	.08	.022	2	98	. 49	2	.01	3	1.59	.01	.01	1	1
50527	1	502	7	93	.3	41	23	1228	6.66	26	11	ND	3	29	i	14	2	176	3.96	.058	5	33	1.00	13	.01	3	.55	.03	.02	1	4
50528	1	221	7	87	.1	33	24	1047	6.68	34	8	ND	3	38	1	6				.040		28	1.12	11	.01	2	1.10	.04	.04	2	2
50529	1	59	6	65	.1	26	18	1131	6.04	11	5	ND	5	63	1	15	2		11.78		4		2.15	7	.01	2	.44	.06	.05	3	4
50542	1	12	3	86	.1	36	18	1561	6.50	8	5	ND	5	138	1	2	2			.016	2		4.90	3	.01		.11	.04	.01	3	t
STD C/AU-R	22	58	39	133	7.2	70	28	1009	3.96	40	18	7	35	48	18	17	21	64	.46	.102	36	58	. 88	180	.08	35	1.72	.07	.13	14	500

DATE RECEIVED: ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED:

JUNE 29 1987 July 4

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips AU++ AND AG++ BY FIRE ASSAY. 1 A.T

ASSAYER:

LIM. DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCE PROJECT-IDEAL File # 87-2066

SAMF'LE#	AG** OZ/T	AU** OZ/T
7555 7556 7557 7558 7559	.02 .01 .01 .01	.003 .030 .004 .001 .001
7560 7632 7633 7634	.01 .01 .02 .01	.001 .001 .001 .001

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GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH JML 3-1-2 HCL-HM03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MW FE CA P LA CR NG BA TI O W AND LINITED FOR NA AND K. AU DETECTION LINIT BY ICP IS 3 PPN. - SAMPLE TYPE: SILTS AUS ANALYSIS BY AA FROM 10 GRAM SAMPLE.

					- 9	HUR LE	11161	91L 19		IA MUNE									Δ	Λ											
DATE RE	CEIV	ED 1	JUL	29 19	187	DA	TE				.ED I ESOL		ly PRO	1	•				U # 1	- 1		DEAN	1 TO	YE,	CERI	r I F I	ED I	9.C.	A69	ЗАҮЕ	R
SAMPLE	NO PPN	CU PPM	P8 PPN	ZN PPH	A6 PPN	NI PPH	CO PPN	NN PPH	FE X	AS PPN	U PPN	AU Pph	TH PPN	SR PPH	CD PPM	SB PPM	BI PPM	V PPM	CA X	P	LA PFN	CR PPN	NG Z	8A PPN	11 X	B PPN	AL 1	NA Z	K Z	N PPN	AUS PPB
CKI	1	105	5	64	.1	53	19	590	5.20	5	7	ND	2	17	t	3	2	168	.71	.024	4	n	1.78	20	. 38	3	2.53	.02	.01	1	15
CK2	1	231	13	89	.1	61	24	1148	5.86	12	5	ND	2	30	1	6	2	173	.96	.031	7	- 79	1.96	43	. 32	4	2.95	. 02	.02	1	29
CK3	1	145	11	75	.1	90	24	948	5.55	14	5	ND	2	40	1	7	2	146	.78	.026	6	90	2.20	39	.23	2	3.45	.02	.02	1	20
CK4	1	115	8	86	.1	58	24	810	7.17	10	8	ND	2.	31	1	6	2	221		.030	4	83	2.57	29	.35	14	3.00	.03	.03	1	1
CK5	1	109	8	83	.1	54	23	843	6.14	7	6	ND	2	34	1	4	2	178	.93	.033	5	68	2.37	32	. 32	11	3.05	.02	.02	1	2
CK6	1	86	3	59	.1	56	19	698	5.73	5	5	NO	2	26	1	5	2	196	. 65	.030	5	75	1.84	30	. 42	3	2.76	. 02	.01	1	1
CK7	1	207	6	91	.1	67	26	1032	6.59	- 14	5	ND	2	29	1	4	2	185	.86	.027	6	81	2.35	43	. 28	2	3.19	.01	.03	1	395
CKB	1	221	5	81	.1	49	24	1022	6.97	8	5	ND	2	32	1	5	2	214	1.15	.028	7	60	1.95	33	.34	5	3.31	.01	.02	1	2
CK9	1	107	9	92	.1	39	21	1070	6.60	7	5	NÐ	2	25	1	5	2	190	.57	.026	7	48	1.52	45	.19	2	3.27	.03	.06	1	2

ACME ANALYTICAL LABORATORIES

CK6

CK7

CK8

CK9

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207

1 221

1 107

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91

.1 56 19

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698 5.73

26 1032 6.59

24 1022 6.97

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GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. This leach is partial for MN FE CA P LA CR H5 BA TI D W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IB 3 PPM. -- Sample type: Gilts Aug Analysis by AA FROM 10 GRAM SAMPLE.

ASBAYER. D. Jugg. DEAN TOYE, CERTIFIED B.C. ABBAYER DATE REPORT MAILED, July 4 DATE RECEIVED: JUL 29 1987 STETSON RESOURCE PROJECT-IDEAL File # 87-2065 SAMPLE KO CU PB AG NI CO MN FE AS U AU TH SR CD SB BI V CA P LA CR MG BA 11 AL N AUT ZN 8 PPN PPB I PPN PPN PPN рри рри рри рри рри у у рри рри Z PPH Ż 1 Z PPN PPN PPR PPN PPH PPN PPH PPH PPM 1 CK 1 168 .71 .024 71 1.78 20 . 38 3 2.53 .02 .01 15 53 19 590 5.28 17 2 1 105 .1 -5 2 ٦ 2 173 .96 .031 43 .32 4 2.95 .02 .02 29 CK2 231 24 1148 5.86 12 30 7 79 1.96 1 1 13 89 .1 61 5 ND 2 1 6 CK3 145 11 75 .1 90 24 948 5.55 14 5 ND 2 40 7 2 146 .78 .026 6 90 2.20 39 .23 2 3.45 .02 .02 1 20 1 1 29 .35 1 115 58 24 810 7.17 10 8 ND 2 . 31 2 221 .90 .030 4 83 2.57 14 3.00 .03 .03 1 7 CX4 8 86 .1 1 6 CK5 68 2.37 32 .32 11 3.05 .02 .02 2 1 109 A 83 .1 54 23 843 6.14 1 ND 2 -34 2 178 .93 .033 5 1 6 1 4

1 4

5

2 196

.85 .030

2 185 .86 .027

5

6

7

75 1.84

81 2.35

60 1.95

7 48 1.52 45 .19

30 .42

33 .34

43

.28

3 2.76

2 3.19

.02 .01

.01 .03

5 3.31 .01 .02

2 3.27 .03 .06

8 5 ND 2 32 5 2 214 1.15 .028 1 7 5 ND 2 25 1 5 2 190 .57 .026

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2 28

DATE RECEIVED JUL 07 1987 ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS, VANCOUVER B.C. DATE REPORTS MAILED Kuly PH: (604) 253-3158 COMPUTER LINE: 251-1011 GEOCHEMICAL ASSAY CERTIFICATE SAMPLE TYPE : ROCK - CRUSHED AND PULVERIZED TO -100 MESH. Aut - 10 5H, JENITED, HOT AQUA REGIA LEACHED, MIBK EXTRACTION, AA ANALYSIS. <u>PLM</u>__DEAN TOYE , CERTIFIED B.C. ASSAYER ASSAYER STETSON RESOURCES PROJECT IDEAL FILE# 87-2265 PAGE# 1 SAMPLE Au* ppb

ACME ANALYTICAL LABORATORIES DATE RECEIVED: JULY 7 1987 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED: July 13/87.

A/T)

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips AU++ AND AG++ BY FIRE ASSAY (1 A.T.)

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SAMPLE#	AG** OZ/T	AU** OZ/T
7561	.01	.001
7568	.03	.001
7580	.02	.001
7590	.3.02	.001
7591	.01	.022
7592	.04	.005
7593	、.03	.001
7594	.02	.001
7596	.02	.001

ACME ANALYTICAL LABORATORIES DATE RECEIVED: JULY 7 1987 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED: July 13/67.

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips AU** AND A6** BY FIRE ASSAY (1 A T)

ASSAYER: . A. Aufl. DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCES PROJECT - IDEAL File # 87-2265A

A/T)

SAMPLE#	AG★★ OZ∕T	AU★★ OZ∕T
7561 7568 7580 7590 7591	.01 .03 .02 .02 .01	.001 .001 .001 .001
7592 7593 7594 7596	× .04 .03 .02 .02	.005 .001 .001 .001

ACME ANALYTICAL LABORATORIES DATE RECEIVED: AUG 6 1987 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED:

ASSAY CERTIFICATE

- SANPLE TYPE: ROCK AU** AND AG** BY FIRE ASSAY.

ASSAYER:

DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCES PROJECT-IDEAL File # 87-2996

SAMPLE#	AG**	
	OZ/T	OZ/T
منتب إحدار إحدر علاجه		And
7803	.06	.205
7804	.01	.029
7805	.04	.114
7806	.05	.015
7807	.01	.001
7808		.006
7809	• O 1	.070
7812	.01	.011
7813	.01	.014
7822	× .01	.006
7823	.07	.726
7824	.02	.035
7827	.02	.001
7828	.01	.001
7829	.13	.845
7830	.02	.065
7831	.01	.078
7833	01	.001
7834	.01	.001
7836	.01	.001
7838	.01	.001
7839	.01	.001

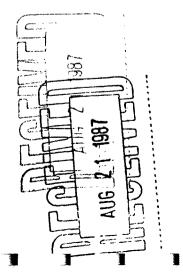
ACME ANALYTICAL LABORATORIES

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GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3HL 3-1-2 HCL-HN03-H20 AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. This leach is partial for MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-ROCK P2-SILT P3-17 SOIL AUS ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE REC	CEIV	ED:	AU5	6 1987	1	DAT	TE R	EPO	RT M	AIL	ED:	au	91	14 /8	37	AS	BAYE	R. /	Q.	kip,	źD	EAN	точ	E, C	ERT	IFIG	ED B	.c.	ASS	AYEF	R
							STE	TSO	N RE	SOUF	RCES	FRC) JEC	т–1С	EAL	F	ile	# 1	37-2	996	i	Page	≥ 1								
SAMPLE#	NO Pph	CU PPN	PB PPM	ZN PPK	AG PPN	NI PPN	CO PPN	MN PPM	FE X	AS PP N	U PPN	AU PPN	TH PPN	SR PPN	CD PPM	SB PPN	BI PPM	V PPN	CA Z	. P X	LA PPN	CR PPN	HG 2	BA PPN	TI X	B PPM	AL Z	NA Z	K X	N PPN	AU S PPB
7579	1	242	84	176	.2	18	24	479	4.36	34	5	ND	1	10	1	2	2	89	.66	.014	2	10	. 83	9	.15	2	1.38	.01	.03	1	23
7801	1	237	268	469	.4	40	18	474	5.55	- 4	5	ND	1	14	2	2	2	104	.48	.023	3	49	1.22	10	.24	2	2.18	.02	.06	1	490
7802	1	457	35	94	3.6	20	13	344	6.42	17	5	15	1	2	1	2	2	87	.15	.017	2	44	.76	4	.18	2	1.66	.01	.02	1	3630
7810	1	173	56	90	.3	25	13	291	2.98	2	5	ND	1	. 3	1	2	2	48	.11	.014	2	36	.85	9	.04	2	1.08	.01	.07	1	220
7811	2	322	22	99	.1	56	26	574	6.19	3	5	ND	1	18	1	2	2	Í 155	.57	.031	4	101	1.92	15	.34	2	2.94	.03	.07	1	89
7814	1	989	36	79	.4	23	10	91	2.97	2	5	ND	1	2	1	2	2	21	.09	.016	2	20	.17	11	.05	7	.42	.01	.10	i	450
7815	1	1541	14	48	.4	35	17	441	4.12	3	5	ND	1	7	1	2	2	95	.25	.021	3	57	1.26	11	.13	- 4	1.80	.01	.07	2	76
7816	1	247	26	47	.1	46	19	249	3.76	7	5	NÐ	1	- 4	1	2	2	80	.30	.035	3	59	.87	13	.19	2	1.36	.01	.10	1	730
7817	2	1112	17	31	.6	23	12	249	2.96	7	5	ND	1	4	1	2	2	50	.14	.006	2	28	.67	3	.11	2	1.00	.01	.03	1	207
7818	i	192	26	105	.1	86	41	1039	10.98	2	5	NÐ	1	33	1	2	2	302	2.82	.043	7	162	5.07	13	.50	2	5.71	.02	.03	2	4
													7.																		
7819	4	434	18	53	.1	33	14	335	3.05	11	5	ND	1	14	1	2	2	63	.48	.024	3	51	.78	7	.07	2	1.43	.01	.06	1	570
7820	1	769	17	84	.1	78	28	878	6.38	2	5	NÐ	1	43	1	2	2	171	6.87	.037	7	163	2.53	21	.07	2	3.55	.01	.09	2	520
7821	1	462	15	47	.1	38	14	643	3.92	3	5	NÐ	1	31	1	2	2	81	10.15	.018	3	69	1.63	4	.01	2	1.95	.01	.04	1	21
7825	1	145	19	103	.1	75	36	889	8.13	6	5	ND	1	6	1	2	2	166	.20	.041	4	117	2.87	17	.08	2	3.72	.01	.08	2	115
7826	13	53	15	30	.2	58	21	233	4.71	14	5	ND	i	4	1	2	2	61	.21	.029	2	40	.66	9	.23	2	1.27	.01	.07	1	67
7832	1	20	5	41	.1	67	24	1167	5.25	2	5	ND	1	77	1	2	2	60	15.08	.005	2	31	4.44	29	.01	2	.26	.01	.01	1	1
7835	1	- 44	19	76	.1	11	19	820	6.37	2	5	NÐ	1	27	1	2	2	152	1.14	.059	7	10	1.93	42	.17	5	2.11	.03	.09	1	1
7837	1	112	12	100	1	14	28	866	7.32	3	5	ND	1	11	1	2	2	175	.66	.072	6	7	2.43	26	.20	10	2.78	.05	.05	1	1
STD C/AU-R	19	57	41	131	7.0	67	28	905	3.95	40	19	7	38	50	17	17	21	55	.47	.081	37	58	.87	176	.08	38	1.87	.06	.13	13	490



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SAMPLE			PB PPN	÷.,					FE L	-									CA X													
10	1	216	12	107	.3	42	28	914	9.30	10	5	ND	3	20	1	2	2	245	1.02	.037	6	40	1.71	35	.53	8	2.86	.05	. 02	1	66	
20																			.72													
7A	1	266	7	155	.4	56	28	1113	7.84	14	5	NÐ	2	27	1	4	2	175	.84	.034	6	70	2.39	48	.25	4	3.62	.05	.05	1	445	
SILT#1 BRIN RD6 TUX1	1	232	18	96	.3	37	26	1310	8.18	15	5	ND	2	23	1	3	2	217	1.12	.047	6	35	1.50	36	.57	13	2.76	.06	.02	3	6	
STD C	19	60	42	136	7.9	74	29	1021	4.01	48	14	7	40	52	19	14	24	61	.48	.093	40	65	. 88	105	.08	34	1.84	.09	.15	13	-	

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L0+00 9+50S	186	3	. 1	15	7	6	70
L0+00 10+00S	91	6	- 1	3	3	1	80
L0+00 10+50S	49	2	. 1	14	2	1	70
L0+00 11+00S	80	6	. 1	4	2	1	90
L8+00E 9+00S	61	11	. 1	2	2	1	30
L8+00E 9+50S	31	1.5	.2	2	2	1	40
Ľ 8+00E 10+00S	57	2	. 1	17	5	3	100
L8+00E 11+00S	42	13	. 1	2	2	1	80
L8+00E 11+50S	25	13	. 1	4	2	1	40
L8+00E 12+00S	61	9	. 1	5	2	4	80
L8+00E 12+50S	80	7	.2	5	2	1	90
L11E 9+50S	. 69	8	. 1	3	4	1	70
L11E 10+00S	39	9	. 1	2	2	1	60
L11E 10+50S	78	6	.2	6	З	2	80
L11E 11+00S	21	16	.2	N	2	1	60
L11E 11+50S	76	11	. 1	4	4	1	90
L11E 12+00S	137	5	. 3	4	3	1	130
L11E 12+50S	9 9	5	× .3	4	2	9.	50
L11E 13+00S	129	6	.2	125	2	3	110
L11E 13+50S	44	12	. 1	2	2	6	60
L11E 14+00S	54	6	. 1	3	2	3	80
L11E 14+50S	101	2	. 1	13	8	1	100
L11E 15+00S	48	6	. 1	2	2	1	90
L12E 0+00S	77	8	.4	2	2	2	60
L12E 0+50S	55	12	.2	3	3	1	80
L12E 1+00S	,46	13	.2	2	2	1	70
L12E 1+50S	102	11	.3	4	3 3	1	80
L12E 2+00S	80	4	.3	2		7	110
L12E 2+50S	38	12	.2	2	2	2	120
L12E 3+00S	51	8	. 1	5	2	1	90
L12E 3+50S	78	2	.2	13	7	7	80
L12E 4+00S	78	6	. 1	2	2	1	90
L12E 4+50S	50	11	. 1	2	3	4	80
L12E 5+00S	36	6	. 1	2	2	1	60
L12E 5+50S	139	4	.2	4	3	2	120 .
L12E 6+00S	58	10	. 4	2	2	1	70
STD C/AU-S	58	41	7.3	37	15	49	1300

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L12E 6+50S	101	2	.5	17	2	5	80
L12E 7+00S	47	6	.5	2	2	1	70
L12E 7+50S	57	8	.6	5	2	1	60
L12E 8+00S	36	15	.5	2	2	1	50
L12E 8+50S	76	6	.6	2	2	1	90
L12E 9+00S	104	6	. 6	6	2	1	110
L12E 9+50S	117	4	. 7	6	2	1	80
L12E 10+00S	45	14	. 4	2	2	1.	90
L12E 10+50S	43	2	.5	2	2	2	30
L12E 11+00S	43	10	.3	5	2	1	100
L12E 11+50S	47	10	.5	2	2	2	50
L12E 12+00S	65	7	. 6	2	2	2	70
L12E 12+50S	121	6	. 7	5	2	1	110
L12E 13+00S	44	8	.6	5	2	13	80
L12E 13+50S	90	2	. 4	17	4	2	90
L12E 14+00S	93	2	. 4	14	2	5	70
L12E 14+50S	179	2	.7	18	2	4	110
L12E 15+00S	106	3	1.6	14.	2	3	80
L13E 0+00S	66	11	.5	2	2	9	90
L13E 0+50S	65	12	.5	2	2	48	60
L13E 1+00S	87	2	.2	3	2	12	40
L13E 1+50S	60	4	. 6	3	2	15	100
L13E 2+00S	69	10	. 4	3	2	13	50
L13E 2+50S	60	11	-8	2	2	1	100
L13E 3+00S	75	4	.8	3	2	1	90
L13E 3+50S	58	5	. 4	6	2	1	80
L13E 4+00S	131	2	.3	19	2	1	110
L13E 4+50S	149	5	.8	44	2	2	70
L13E 5+00S	63	4	. 6	7	3	35	100
L13E 5+50S	212	16	.7	9	2	104	80
L13E 6+00S	126	15	.5	7	2	2	120
L13E 6+50S	82	2	.3	3	2	1	80
L13E 7+00S	60	8	.5	3	2	1	100
L13E 7+50S	57	9	- 6	3	2	2	60
L13E 8+00S	118	9	.7	11	2	150	90
L13E 8+50S	148	4	.6	8	2	1	80

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L13E9+50S4612.322130L13E10+00S2710.122240L13E11+00S526.452180L13E11+00S526.452180L13E11+50S1378.242270L13E12+00S1122.3133170L13E12+50S1115.362290L13E13+00S6811.432270L13E13+50S3115.3223080L13E14+50S1123.462580100L14E14+50S1123.462580100L14E14+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+50S3115.52210120L14E2+50S3115.52210120L14E2+50S1032.582210L14E2+50S1027.432370L14E2+50S1	L13E 9+00S	131	8	.3	2	2	6	80
L13E10+00S2710.122240L13E10+50S328.322250L13E11+00S526.452180L13E11+50S1378.242270L13E12+00S1122.3133170L13E12+50S1115.362290L13E13+00S6811.432270L13E13+50S3115.3223080L13E14+50S1123.442170L14E0+50S1058.5624110L14E0+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+50S1052210120L14E2+50S1052210120L14E2+50S1052210120L14E2+50S102743825L14E2+50S102743825L14E4+50S754382100L								
L13E10+50S328.3222250L13E11+00S526.452180L13E11+50S1122.3133170L13E12+50S1115.362290L13E12+50S1115.362270L13E13+0S6811.432270L13E13+0S5115.3223080L13E14+50S1123.442170L14E0+0S509.162180L14E0+50S1058.5624110L14E1+0OS687.162280L14E1+50S803.5192170L14E2+50S3115.52210102L14E2+50S822.2132360L14E2+50S822.2132360L14E2+50S1027.432250L14E5+50S1027.432250L14E5+50S1027.452250L14E5+50S102 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>_</td> <td></td>							_	
L13E11+00S526.452180L13E11+50S1378.242270L13E12+00S1122.3133170L13E12+50S1115.362290L13E13+00S6811.432270L13E13+50S3115.3223080L13E14+00S763.462580100L13E14+50S1123.442170L14E0+00S509.1624110L14E0+50S1058.5624110L14E1+00S687.162280L14E1+00S685.7322100L14E2+50S1032.5822110L14E3+50S822.2132360L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S1032.5821100L14E5+50S1027.452250L14E5+50S1027<								
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L13E12+50S1115.362290L13E13+00S6811.432270L13E13+50S3115.3223080L13E14+00S763.462580100L13E14+50S1123.442170L14E0+00S509.162180L14E0+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+50S3115.52210120L14E2+50S3115.52210120L14E2+50S1032.5822110L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S1027.452250L14E4+50S1027.452250L14E5+50S1027.452170L14E6+50S935.2821170L14E6+50S78		137		.2	4		2	70
L13E13+00S6811.432270L13E13+50S3115.3223080L13E14+00S763.462580100L13E14+50S1123.442170L14E0+00S509.162180L14E0+50S1058.5624110L14E1+50S803.5192170L14E1+50S803.5192170L14E2+50S3115.52210120L14E3+50S822.2132360L14E3+50S822.2132360L14E3+50S822.2132360L14E3+50S822.2132360L14E3+50S1027.452250L14E4+50S709.552250L14E5+50S1027.452250L14E5+50S1027.452250L14E5+50S1027.452250L14E6+50S7811<	L13E 12+00S	112		.3	13		1	70
L13E13+50S3115.3223080L13E14+00S763.462580100L13E14+50S1123.442170L14E0+00S509.162180L14E0+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+50S3115.52210120L14E2+50S3115.52210120L14E3+50S822.2132360L14E3+50S822.2132360L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S709.552250L14E5+50S1027.452250L14E6+50S7811.392690L14E6+50S7811.392690L14E7+50S109172.4122890L14E6+50S109	L13E 12+50S	111	5	.3	6		2	90
L13E13+50S3115.3223080L13E14+00S763.462580100L13E14+50S1123.442170L14E0+00S509.162180L14E0+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+50S3115.52210120L14E2+50S3115.52210120L14E3+50S822.2132360L14E3+50S822.2132360L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S709.552250L14E5+50S1027.452250L14E6+50S7811.392690L14E6+50S7811.392690L14E7+50S109172.4122890L14E6+50S109	L13E 13+00S	68	11	. 4	3	2	2	70
L13E14+50S1123.442170L14E0+00S509.162180L14E0+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+00S685.7322110L14E2+50S3115.52210120L14E3+00S1032.5822110L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S574.382560L14E5+50S1027.452250L14E5+50S1027.452250L14E6+50S7811.31021100L14E7+50S607.332170L14E8+50S14911.3102160L14E9+50S10919.424231040L14E9+50S1045.2172160L14E9+50S1045	L13E 13+508	31	15	.3	2	2	20	80
L13E14+50S1123.442170L14E0+00S509.162180L14E0+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+00S685.7322110L14E2+50S3115.52210120L14E3+00S1032.5822110L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S574.382560L14E5+50S1027.452250L14E5+50S1027.452250L14E6+50S7811.31021100L14E7+50S607.332170L14E8+50S14911.3102160L14E9+50S10919.424231040L14E9+50S1045.2172160L14E9+50S1045	113E 14+008	74	7	А	۷.	2	500	100
L14E0+00S509.162180L14E0+50S1058.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+00S685.7322110L14E2+50S3115.52210120L14E3+00S1032.5822110L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S574.382560L14E5+50S1027.452250L14E5+50S1027.452250L14E6+50S935.2821100L14E7+50S607.332170L14E8+50S14911.3102160L14E9+00S1712.4122890L14E9+00S1458.52633380L14E9+50S1045.2172160L14E9+50S1045 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
L14E0+50S10S8.5624110L14E1+00S687.162280L14E1+50S803.5192170L14E2+50S3115.52210120L14E2+50S3115.52210120L14E3+00S1032.5822110L14E3+50S822.2132360L14E4+60S545.432560L14E5+50S1027.452250L14E5+50S1027.452250L14E6+00S855.4821170L14E6+50S935.2821100L14E7+50S607.332170L14E6+50S14911.3102160L14E8+50S14911.3102160L14E9+00S1712.4122890L14E8+50S10919.424231040L14E9+00S1458.52633380L14E10+00S145 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>								
L14E1+00S687.162280L14E1+50S803.5192170L14E2+00S685.7322110L14E2+50S3115.52210120L14E3+00S1032.5822110L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S574.382560L14E5+50S1027.452250L14E5+50S1027.452250L14E6+00S855.4821170L14E6+50S935.2832120L14E7+50S607.332170L14E7+50S10711.3102160L14E8+50S1712.4122890L14E9+50S10919.424231040L14E10+60S1458.52633380L14E10+60S1045.2172160L14E10+60S104 <t< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td></t<>							-	
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L14E2+50S3115 \cdot 52210120L14E3+00S1032 \cdot 5822110L14E3+50S822 \cdot 2132360L14E4+00S545 \cdot 432370L14E4+50S574 \cdot 382560L14E5+00S709 \cdot 552250L14E5+50S1027 \cdot 452250L14E6+00S855 \cdot 4821170L14E6+00S855 \cdot 4821170L14E6+50S935 \cdot 2832120L14E7+00S 67 67 \cdot 332170L14E7+50S607 \cdot 332170L14E8+00S7811 \cdot 3102160L14E8+00S14711 \cdot 3102160L14E9+00S1712 \cdot 4122890L14E9+00S1458 5 2633380L14E10+00S1458 5 2633380L14E10+00S1458 5 26333 <td< td=""><td>L14E 1+50S</td><td>80</td><td></td><td>.5</td><td>19</td><td>2</td><td>1</td><td>70</td></td<>	L14E 1+50S	80		.5	19	2	1	70
L14E2+50S3115.52210120L14E3+00S1032.5822110L14E3+50S822.2132360L14E4+00S545.432370L14E4+50S574.382560L14E5+50S1027.452250L14E5+50S1027.452250L14E6+00S855.4821170L14E6+50S935.2832120L14E7+50S607.332170L14E8+00S7811.3792690L14E8+50S14711.3102160L14E9+00S1712.4122890L14E9+50S10919.424231040L14E10+00S1458.52633380L14E10+00S1458.52633380L14E10+50S1045.2172160L14E11+50S694.342160	L14E 2+00S	68	5	.7	3	2	2	110
L14E $3+50S$ 82 2 $.2$ 13 2 3 60 L14E $4+00S$ 54 5 $.4$ 3 2 3 70 L14E $4+50S$ 57 4 $.3$ 8 2 5 60 L14E $5+00S$ 70 9 $.5$ 5 2 2 50 L14E $5+50S$ 102 7 $.4$ 5 2 2 50 L14E $5+50S$ 102 7 $.4$ 5 2 2 50 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+00S$ 67 6 2 8 3 2 120 L14E $7+00S$ 67 6 2 8 3 2 120 L14E $7+50S$ 60 7 $.3$ 3 2 1 70 L14E $8+00S$ 78 11 $.3$ 10 2 1 60 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 145 8 $.5$ 26 3 33 80 L14E $10+00S$ 145 8 $.5$ 26 3 33 80 L14E<	L14E 2+50S	31	15	`.5	2.	2	10	120
L14E $3+50S$ 82 2 $.2$ 13 2 3 60 L14E $4+00S$ 54 5 $.4$ 3 2 3 70 L14E $4+50S$ 57 4 $.3$ 8 2 5 60 L14E $5+00S$ 70 9 $.5$ 5 2 2 50 L14E $5+50S$ 102 7 $.4$ 5 2 2 50 L14E $5+50S$ 102 7 $.4$ 5 2 2 50 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+00S$ 67 6 2 8 3 2 120 L14E $7+00S$ 67 6 2 8 3 2 120 L14E $7+50S$ 60 7 $.3$ 3 2 1 70 L14E $8+00S$ 78 11 $.3$ 10 2 1 60 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 145 8 $.5$ 26 3 33 80 L14E $10+00S$ 145 8 $.5$ 26 3 33 80 L14E<	L14E 3+00S	103	2	.5	8	2	2	110
L14E $4+50S$ 57 4 $.3$ 8 2 5 60 L14E $5+50S$ 102 7 $.4$ 5 2 2 50 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+50S$ 93 5 $.2$ 8 2 1 100 L14E $7+00S$ 67 6 $.2$ 8 3 2 120 L14E $7+50S$ 60 7 $.3$ 3 2 1 70 L14E $8+00S$ 78 11 $.3$ 9 2 6 90 L14E $8+50S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $10+00S$ 145 8 $.5$ 26 3 33 80 L14E $10+00S$ 104 5 $.2$ 17 2 1 60 L14E $11+00S$ 101 5 $.2$ 8 2 1 50 L14E $11+00S$ 101 5 $.2$ 8 2 1 60 <td>L14E 3+50S</td> <td>82</td> <td>2</td> <td></td> <td>13</td> <td></td> <td></td> <td></td>	L14E 3+50S	82	2		13			
L14E $4+50S$ 57 4 $.3$ 8 2 5 60 L14E $5+50S$ 102 7 $.4$ 5 2 2 50 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+50S$ 93 5 $.2$ 8 2 1 100 L14E $7+00S$ 67 6 $.2$ 8 3 2 120 L14E $7+50S$ 60 7 $.3$ 3 2 1 70 L14E $8+00S$ 78 11 $.3$ 9 2 6 90 L14E $8+50S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $10+00S$ 145 8 $.5$ 26 3 33 80 L14E $10+00S$ 104 5 $.2$ 17 2 1 60 L14E $11+00S$ 101 5 $.2$ 8 2 1 50 L14E $11+00S$ 101 5 $.2$ 8 2 1 60 <td>114F 4+00S</td> <td>54</td> <td>=</td> <td>Д</td> <td>7</td> <td>2</td> <td>-7</td> <td>70</td>	114F 4+00S	54	=	Д	7	2	-7	70
L14E5+00S709.552250L14E5+50S1027.452250L14E6+00S855.4821170L14E6+50S935.2821100L14E7+00S676.2832120L14E7+50S607.332170L14E8+00S7811.392690L14E8+50S14911.3102160L14E9+50S10919.424231040L14E10+00S1458.52633380L14E10+50S1045.2172160L14E11+50S694.342160								
L14E5+50S1027.4522250L14E $6+00S$ 855.4821170L14E $6+50S$ 935.2821100L14E $7+00S$ 67 6.2832120L14E $7+50S$ 607.332170L14E $8+00S$ 7811.392690L14E $8+50S$ 14911.3102160L14E $9+00S$ 1712.4122890L14E $9+00S$ 1712.412231040L14E $9+00S$ 10919.424231040L14E $10+00S$ 1458.52633380L14E $10+00S$ 1045.2172160L14E $11+00S$ 1015.282150L14E $11+50S$ 694.342160								
L14E $6+00S$ 85 5 $.4$ 8 2 11 70 L14E $6+50S$ 93 5 $.2$ 8 2 1 100 L14E $7+00S$ 67 6 2 8 3 2 120 L14E $7+50S$ 60 7 $.3$ 3 2 1 70 L14E $8+00S$ 78 11 $.3$ 9 2 6 90 L14E $8+50S$ 149 11 $.3$ 10 2 1 60 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 145 8 $.5$ 26 3 33 80 L14E $10+00S$ 145 8 $.5$ 26 3 33 80 L14E $10+50S$ 104 5 $.2$ 17 2 1 60 L14E $11+00S$ 101 5 $.2$ 8 2 1 50 L14E $11+50S$ 69 4 $.3$ 4 2 1 60								
L14E $6+50S$ 93 5 $.2$ 8 2 1 100 L14E $7+00S$ 67 6 $.2$ 8 3 2 120 L14E $7+50S$ 60 7 $.3$ 3 2 1 70 L14E $8+00S$ 78 11 $.3$ 9 2 6 90 L14E $8+50S$ 149 11 $.3$ 10 2 1 60 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+00S$ 171 2 $.4$ 12 2 8 90 L14E $9+50S$ 109 19 $.4$ 24 2 310 40 L14E $10+00S$ 145 8 $.5$ 26 3 33 80 L14E $10+50S$ 104 5 $.2$ 17 2 1 60 L14E $11+00S$ 101 5 $.2$ 8 2 1 50								
L14E 7+005 67 6 .2 8 3 2 120 L14E 7+505 60 7 .3 3 2 1 70 L14E 8+005 78 11 .3 9 2 6 90 L14E 8+505 149 11 .3 10 2 1 60 L14E 9+005 171 2 .4 12 2 8 90 L14E 9+505 109 19 .4 24 2 310 40 L14E 10+005 145 8 .5 26 3 33 80 L14E 10+005 145 8 .5 26 3 33 80 L14E 10+505 104 5 .2 17 2 1 60 L14E 11+005 101 5 .2 8 2 1 50 L14E 11+505 69 4 .3 4 2 1 60 <td>LI4E 07005</td> <td>80</td> <td>0</td> <td>. 4</td> <td>8</td> <td><u></u></td> <td>11</td> <td>70</td>	LI4E 07005	80	0	. 4	8	<u></u>	11	70
L14E 8+00S 78 11 .3 9 2 6 90 L14E 8+50S 149 11 .3 10 2 1 60 L14E 9+00S 171 2 .4 12 2 8 90 L14E 9+50S 109 19 .4 24 2 310 40 L14E 10+00S 145 8 .5 26 3 33 80 L14E 10+50S 104 5 .2 17 2 1 60 L14E 10+50S 104 5 .2 8 2 1 50 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60		93	5		8		1	100
L14E 8+00S 78 11 .3 9 2 6 90 L14E 8+50S 149 11 .3 10 2 1 60 L14E 9+00S 171 2 .4 12 2 8 90 L14E 9+50S 109 19 .4 24 2 310 40 L14E 10+00S 145 8 .5 26 3 33 80 L14E 10+50S 104 5 .2 17 2 1 60 L14E 10+50S 104 5 .2 8 2 1 50 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60			6			3		120
L14E B+50S 149 11 .3 10 2 1 60 L14E 9+00S 171 2 .4 12 2 8 90 L14E 9+50S 109 19 .4 24 2 310 40 L14E 10+00S 145 B .5 26 3 33 80 L14E 10+50S 104 5 .2 17 2 1 60 L14E 10+50S 104 5 .2 8 2 1 50 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60	L14E 7+50S	60	7				1	70
L14E 9+00S 171 2 .4 12 2 8 90 L14E 9+50S 109 19 .4 24 2 310 40 L14E 10+00S 145 8 .5 26 3 33 80 L14E 10+50S 104 5 .2 17 2 1 60 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60	L14E 8+00S	78	11	.3	9	2	6	90
L14E 9+50S 109 19 .4 24 2 310 40 L14E 10+00S 145 8 .5 26 3 33 80 L14E 10+50S 104 5 .2 17 2 1 60 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60	L14E 8+50S	149	11	. 3	10	2 -	1	60
L14E 9+50S 109 19 .4 24 2 310 40 L14E 10+00S 145 8 .5 26 3 33 80 L14E 10+50S 104 5 .2 17 2 1 60 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60	L14E 9+00S	171	2	. 4	12	2	8	90
L14E 10+00S 145 8 .5 26 3 33 80 L14E 10+50S 104 5 .2 17 2 1 60 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60								
L14E 10+50S 104 5 .2 17 2 1 60 L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60								
L14E 11+00S 101 5 .2 8 2 1 50 L14E 11+50S 69 4 .3 4 2 1 60								,
L14E 11+50S 69 4 .3 4 2 1 60								
	ստեղըները են է չչչչչչչչչ։	a vera)	سند ه	L L	<u>.</u>	Ŧ	00
	L14E 11+50S	69	4	.3	4	2	1	60
	STD C/AU-S	59	28	7.5	38		47	1300

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L14E 12+00S	115	5	. 1	2	2	6	40
L14E 12+50S	137	2	. 1	5	2	4	90 90
	181		. 1		2		140
		19				23	
L14E 13+50S	86	26	.2	4	2	9	60
L15E 0+00S	111	7	.2	9	2	1	110
L15E 0+50S	121	11	.2	2	2	4	80
L15E 1+00S	59	12	. 1	2	2	1	70
L15E 1+50S	71	15	.3	4	2	1	80
L15E 2+00S	60	18	.3	2	2	84	90
L15E 2+50S	100	4	.2	2		1	70
L15E 3+005	124	3	.2	12	2	28	50
L15E 3+50S	139	10	. 1	2	2	250	110
L15E 4+50S	43	12	. 1	2	2	2	80
L15E 5+50S	76	8	. 1	9	2	2	60
L15E 6+00S	122	5	. 1	12	2	1	70
			• •	4. au-	****	-	у т <u>и</u> т
L15E 6+50S	136	20	. 1	4	2	4	90
L15E 7+00S	147	5	. 4	3	2	2	120
L15E 7+50S	127	13	`. 3	2.	2	8	80
L15E 7+75S	164	2	.2	4	2	14	90
L15E 8+00S	238	8	. 1	17	2	62	140
L15E 8+25S	144	9	. 1	13	5	5	130
L15E 8+50S	104	4	. 1	4	2	5	80
L15E 8+75S	150	8	.2	8	2	14	60
L15E 9+00S	115	10	. 1	2	2	3	70
L15E 9+25S	413	8	.2	9	2	27	80
L15E 9+50S	78	8	.2	2	2	6	90
L15E 9+75S	116	4	.2	2	2	1	110
L15E 10+00S	127	38	.3	5	2	19	90
L15E 10+50S	383		.2	15	2	21	50
L15E 11+00S	76	7	. 1	10	2	10	70
tean de tead hann de de 'ng'ne'tead	,	,		444 (A.)		10	
L15E 11+50S	96	6	. 1	8	2	1	120
L15E 12+00S	103	2	. 1	10	2	23	100
L15E 12+50S	107	10	.2	2	2	1	80
L15E 13+00S	82	11	. 1	2	2	8	110'
L16E 0+00S	67	13	. 1	4	2	1	230
L16E 0+50S	106	12	.3	4	2	2	120
STD C/AU-S	59	41	7.3	39	18	48	1400

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L16E 1+00S	83	8	.3	8	2	1	100
L16E 1+50S	97	10	.2	5	2	14	60
L16E 2+00S	66	5	.2	22	2	1	50
L16E 2+50S	92	8	. 1	6	2	5	100
L16E 3+00S	104	13	.3	18	2	1	50
L16E 3+50S	147	11	. 1	8	2	1	80
L16E 4+00S	85	8	.2	4	2	4	100
L16E 4+50S	53	12	.2	7	13	4	120
STD C/AU-S	62	41	7.8	42	18	53	1300
L16E 5+00S	51	14	. 1	7	2	1	70
L16E 5+50S	78	10	. 1	5	2	1	110
L16E 6+50S	66	11	. 1	2	2	29	50
L16E 7+00S	68	5	.2	2	2	3	60
L16E 8+00S	143	8	.2	24	2	20	80
L16E 8+255	68	15	.2	2	2	4	150
L16E 8+50S	108	13	. 1	61	2	3	60
L16E 8+75S	108	10	. 1	18	2	13	80
L16E 9+00S	55	12	1	3.	4	15	70
L16E 9+25S	84	7	. 1	21	2	9	100
L16E 9+50S	124	12	- 1	30	2	35	80
L16E 9+75S	66	6	. 1	4	2	5	90
L16E 10+00S	137	20	. 1	10	2	74	110
L16E 10+50S	156	7	. 1	6	2	8	50
L16E 11+00S	140	3	. 1	15	2	2	80
L16E 11+50S	82	10	. 1	31	2	1	60
L16E 12+00S	92	2	.2	24	2	7	70
L16E 12+50S	163	16	.2	8	2 3	230	60
L17E 0+00S	49	14	. 1	11	3	5	100
L17E 0+50S	118	4	. 1	8	2	9	50
L17E 1+00S	61	10	. 1.	8	2	2	60
L17E 1+50S	54	11	.2	4	2	1	70
L17E 2+00S	71	8	. 1	6	2	2	60
L17E 2+50S	88	20	.2	3	2	2	100
L17E 3+00S	63	7	. 1	2	2	1	8 0
L17E 3+50S	55	12	. 1	4	2	2	120
L17E 4+00S	208	7	. 1	13	2	57	70
L17E 4+50S	124	14	. 1	2	2	5	60

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
	£ f 1. f	FFIT		F F 11		1112	11.0
L17E 5+00S	73	19	• 2	5	3	4	60
L17E 5+50S	65	17	. 1	9	2	3	40
L17E 6+25S	123	17	.2	4	3	4	60
L17E 6+50S	103	17	. 1	2	2	1	100
L17E 7+00S	58	20	. 1	4	2	3	110
LI/E /+005	00	مند منه ا	• 1	-1	din.	·1	110
L17E 7+25S	107	15	.2	2	2	12	6Ŭ
L17E 7+50S	151	20	.2	12	2	2	80
L17E 7+75S	138	14	. 1	22	2	1	90
L17E 7+75SA	126	25	. 1	4	2	1	80
L17E 8+00S		22	. 1	8	2	1	70
	00	ساله ساله	u J.	0	din	+	7.0
L17E 8+75S	75	30	.3	5	2	4	80
L17E 9+50S	127	9	. 1	12	2	6	30
L17E 10+00S	117	25	. 1	5	2	13	60
L17E 10+25S	9 8	21	.3	5	2	3	70
L17E 10+50S	49	19	.2	6	2	2	60
tana da 2 kana da 121 Y tan2 121 Yan2	.,	1 /	•	0	-		
L17E 10+75S	127	15	.2	3	2	· 1	80
L17E 11+00S	105	17	. 1	8	2	3	40
L17E 11+50S	76	17	1.2	2.	2	1	70
L17E 12+00S	74	19	. 1	2	2	2	50
L17E 12+505	74	14	.1	2	2	2	50
LI/E 12+305	/4	T ++	• 1	<i></i> .	£.	đ.	00
L17E 13+00S	109	15	. 1	16	2	1	40
L18E 0+00S	180	20	.4	23	2	8	100
L18E 0+50S	225	20	. 1	9	2	2	150
L18E 1+00S	156	10	. 4	9	2	6	70
L18E 1+50S	118	21	.4	8	2	1	120
	* * **	4 A	•	0	ation.	+	44.0
L18E 2+00S	151	8	.3	9	2	5	80
L18E 2+50S	93	17	. 4	6	2	1	70
L18E 3+00S	189	14	. 1	3	2	1	80
L18E 3+50S	84	10	. 1	7	2	3	9 0
L18E 4+00S	83	21	. 1	7	2	3	60
L18E 4+50S	199	10	. 1	6	2	1	40
L18E 5+00S	63	19	.2	8	2	1	50
L18E 5+50S	92	18	. 1	5	2	1	60
L18E 6+25S	118	20	.2	9	2	3	9ď
STD C/AU-S	59	42	6.9	39	17	46	1300
L18E 6+50S	82	16	.2	4	2	1	70
			.2	4	2	1	100
L18E 6+75S	74	17	• 44	~1		T	100

SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L18E 7+00S	133	2	. 4	5	2	10	160
L18E 7+25S	168	14	.2	5	2	4	180
	134	3	.2	4	2	2	110
L18E 7+50S					3		
L18E 7+75S	41	17	. 1	2		2	30
L18E 8+00S	- 92	14	- 1	2	2	5	70
L18E 8+25S	135	9	.2	6	3	1	60
118E 8+75S	57	13	. 1	4	ద	1	30
L18E 9+00S	41	6	. 1	2	2	8	100
L18E 9+25S	69	7	.2	4	2	1	120
L18E 9+50S	89	10	. 1	3	3	3	80
	ω,		s .1.		* _ _*	·	And the
L18E 9+75S	113	2	. 1	16	3	1	60
L18E 10+00S	(88	7	. 1	2	3	1	70
L18E 10+50S	86	7	. 1	5	2	4	80
L18E 10+75S	160	9	.2	5	2	28	50
L18E 11+00S	105	2	. 1	6	2	5	40
L18E 11+25S	123	20	. 1	4	2	6	പ
L18E 11+50S	39	17	.2	2	2	3	70
L18E 12+00S	79	- 6	`.1	2.	2	2	60
L19E 0+00S	281	2	1.0	14	3	4	360
	201 98	~ 7		3	2		50
L19E 0+50S	70	1	. 1		<i>4</i> .	T	00
L19E 1+00S	129	5	.3	5	2	3	80
L19E 1+50S	113	10	. 1	2	2	1	110
L19E 2+00S	106	12	.1	2	2	3	100
L19E 2+50S	45	15	. 1	2	2	1	50
L19E 3+00S	131	5	. 1	6	2	5	60
and all if balls for the factor	100 - 100 - 100						
L19E 3+50S	122	2	. 1	17	3	1	50
L19E 4+00S	133	1 Ö	.3	16	2	47	70
L19E 4+50S	86	15	.2	2	2	2	180
L19E 5+00S	233	10	.2	2	2	1	30
L19E 5+50S	83	8	.2	5	2	4	40
L19E 6+00S	119	2	. 4	8	2	10	90
L19E 6+50S	57	19	. 1	2	2	5	80
			• 1	3	2	1	20
L19E 7+00S	96	13				-	
L19E 7+25S	47	13	.2	2	2	1	90 90
L19E 7+75S	64	12	• 3	2	2	1	40
L19E 8+00S	132	13	. 1	2	2	70	70
STD C/AU-S	58	43	7.0	36	14	53	1300

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
	41	20	.2	1.4	2	4	110
L19E 8+258		29		14		1	110
L19E 8+50S	76	6	. 1	14	2	1	70
L19E 8+75S	160	14	.2	2	2	2	110
L19E 9+00S	50	19	- 1	10	2	1	90
L19E 9+25S	65	10	. 1	4	2	1	60
L19E 9+50S	56	19	. 1	10	4	4	50
L19E 9+755	109	12	. 1	14	2	1	20
L19E 10+00S	34	12	. 1.	2	2	1	60
L19E 10+25S	66	11	. 1	2	2	4	110
L19E 10+50S	42	11	. 1.	6	2	1	60
L19E 10+75S	89	7	. 1	4	2	6	70
L19E 11+00S	64	5	. 1	2	2	1	60
L19E 11+003	15		. 1	7	3	1	40
		11					
L19E 11+50S	88	16	. 1	3	2	1	50
L19E 11+75S	87	25	- 1	3	2	7	50
L19E 12+00S	116	26	. 1	11	2	9	40
L19E 12+50S	49	14	. 1	10	2	14	30
L20E 0+00S	172	7	`_1 .	2.	2	45	70
L20E 0+50S	133	10	. 1	5	2	10	140
L20E 1+00S	63	9	.3	8	2	46	110
L20E 1+50S	86	10	.3	3	2	6	150
L20E 2+00S	341	15	. 1	25	2	6	100
L20E 2+50S	111	7	. 1	2	2	1	110
L20E 3+00S	98	12	.1	ž	2	14	100
L20E 3+50S	75	12	.2	2	2	1	100 90
CZOC 37008	1	* 4	يته ه	يئه	din.	1	70
L20E 4+00S	37	12	. 1	12	2	4	70
L20E 4+50S	49	10	. 1	2	3	39	60
L20E 5+00S	163	15	.2	2	2	9	120
L20E 5+50S	105	7	.3	2	2	1	80
L20E 6+00S	62	12	. 1	4	3	9	60
L20E 6+50S	142	8	.2	3	2	1	40
L20E 7+00S	109	14	. 2	2	2	1	70
L20E 7+50S	165	21	. 1	2	2	1	80
L20E 7+75S	175	11	. 1	11	2	10	180
L20E 8+00S	31	5	•	14	2	10	30
ann aine an Chuire - Ann Chuir Ann Ann Ann A	·' 4	7	a sin	л. т т	4	τ	-512
L20E 8+25S	42	16	. 1	13	3	14	100
STD C/AU-S	58	39	7.2	40	15	52	1300

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB FPM	AU¥ PPB	HG PPB
L20E 8+50S	98	11	. 1		2	180	60
L20E 8+75S	86	8	• • • •	2	2	41	50
L20E 9+00S	.176	7	. 1	2	2	15	60
L20E 9+25S	88	4	- 1	2	2	39	40
L20E 9+50S	93	14	. 1	2	2	1	50
L20E 9+75S	36	21	. 1	3	3	1	70
120E 10+00S	31	22	. 1	2	2	3	110
L20E 10+25S	66		.2	2	2	12	50
L20E 10+50S	87	13	. 1	2	2	1	70
L20E 10+75S	63	11	.1	13	2	10	80
	<u>с</u>	11	• 1	1	÷-	10	00
L20E 11+00S	59	16	. 1	6	2	1	110
L20E 11+25S	131	15	. 1	2	2	2	90
L20E 11+50S	256	9	.1	3	2	1	40
L20E 11+75S	83	12	.2	7	2	8	110
L20E 12+00S	62	9	. 1	2	2	1	80
L20E 12+25S	70	8	. 1	8	2	1	90
L20E 12+50S	89	12	. 1	13	2	25	40
L20E 12+75S	97	11	`.3	5.	2	135	70
L20E 13+00S	144	6	. 1	9	2	137	90
L21E 0+00S	165	12	. 1	2	2	19	100
	4.00	10			C 3		40
L21E 0+50S	48	10	. 1	5	2	1	40
L21E 1+00S	73	8	.2	2	2	1	120
L21E 1+50S	144	11	. 1	4	2	5	70
L21E 2+50S	32	13	.2	2	3	1	80
L21E 3+00S	70	10	. 1	2	2	1	70
L21E 3+50S	140	4	. 1	4	2	1	100
L21E 4+00S	118		. 1	2	2	5	60
L21E 4+50S	219	2 3	. 1	4		14	90
L21E 5+00S	101	18	. 1	2	2	390	80
L21E 5+50S	99	12	.2	8	2	4	70
Beau aluas etc Beaus - Lyaf ' Laad fa' Lead		4. 494	• •	<u> </u>		·	· ·
L21E 6+00S	77	7	. 1	4	2	8	60
L21E 6+50S	94	6	.3	4	2	10	100
L21E 7+00S	235	10	. 1	7	2	18	120
L21E 7+25S	92	11	.2	2	2	2	ക്ക്
L21E 7+50S	229	2	. 1	3	2	25	110
L21E 7+75S	186	11	. 1	2	2	23	130
STD C/AU-S	57	38	6.7	42	16	20 51	1600
510 C/HU-5	U7	40 10	© ∎ /	** .	тO	01	1000

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SAMPLE#	CU	ΡB	AG	AS	SB	AU×	HG
	PPM	PPM	PPM	PPM	PPM	PPB	PPB
L21E 8+005	101	16	.3	3	2	12	80
L21E 8+25S	126	18	. 1	4	2	15	200
L21E 8+50S	115	13	. 1	13	2	5	30
L21E 8+75S	165	19	. 1	6	2	14	190
L21E 9+005	43	14	.2	4	2	1	120
L21E 9+25S	153	12	. 1	2	2	15	230
L21E 9+50S	170	14	.2	2	2	4	240
L21E 9+75S	75	2	. 1	2	2	1	40
L21E 10+00S	19	16	. 1	2	2	12	50
L21E 10+25S	90	8	. 1	3	2	1	100
L21E 10+50S	49	11	. 1	2	2	8	60
L21E 10+75S	73	10	. 1	2	2	2	40
L21E 11+00S	60	18	. 1	2	2	5	110
L21E 11+25S	94	3	. 1	8	2	9	50
L21E 11+50S	122	8	.2	2	2	20	70
L21E 11+75S	105	13	. 1	2	2	320	80
L21E 12+00S	48	17	. 1	2	3	42	70
L21E 12+25S	197	2	`.1	2.	2	44	40
L21E 12+50S	79	16	. i	3	3	2	70
L21E 13+00S	146	13	- 1	2	2	22	60
L22E 0+00S	91	4	. 1	12	2	3	80
L22E 0+50S	165	19	. 2	4	2	. 1	90
L22E 1+00S	115	2	. 1	2	2	19	60
L22E 1+50S	102	11	.2	2	2	6	70
L22E 2+00S	128	10	.2	3	2	8	80
L22E 2+50S	81	12	. 1	2	2	3	90
L22E 3+00S	210	4	. 1	13	2	5	180
L22E 3+50S	71	7	. 1	2	2	41	60
L22E 4+00S	144	7	1	2	2	5	70
L22E 4+50S	96	5	. 1	2	2	4	60
L22E 5+00S	181	5	.2	6	2	2	80
L22E 5+50S	105	8	. 1	26	2	5	70
L22E 6+00S	249	5	. 1	2	2	27	90
L22E 6+25S	48	17	. 1	2	4	9	70
L22E 6+50S	149	9	.2	25	2	31	120
L22E 6+75S	127	4	. 1	2	2	11	80
STD C/AU-S	57	42	7.2	39	16	52	1300

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SAMF'LE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU∗ ₽₽₿	HG PPB
L22E 7+00S	107	14	. 1	2	2	i	50
L22E 7+25S	150	16	.2	2	5	75	70
L22E 7+50S	120	10	. 1	4	2	6	80
L22E 7+75S	143	13	.3	2	2	3	60
L22E 8+00S	43	13	. 1	2	2	3	80
L22E 8+25S	88	12	.2	3	2	14	100
122E 8+50S	61	12	.2	2	2	1	90
L22E 8+75S	91	7	.2	2	2	1	60
L22E 9+00S	247	15	. 1	13	2	7	70
L22E 9+25S	122	15	. 1	2	2	49	80
L22E 9+50S	103	12	. 1	5	2	1	90
L22E 9+75S	102	18	. 1	2	2	9	80
L22E 10+00S	256	20	.2	44	2	1	100
L22E 10+25S	121	18	. 1	2	2	1	140
L22E 10+50S	83	11	. 1	31	2	1	50
L22E 10+75S	115	12	. 1	18	2	1	90
L22E 11+00S	57	23	. 1	2	2	2	70
L22E 11+25S	117	16	• L	33.	2	1	70
L22E 11+50S	84	18	. 1	2	2	1	80
L22E 12+00S	160	21	. 1	2	2	2	100
L23E 0+00S	249	18	. 1	19	2	3	160
L23E 0+50S	190	10	.2	10	2	10	110
L23E 1+00S	73	23	. 1	2	2	1	100
L23E 1+50S	130	9	- 1	2	2	1	110
L23E 2+00S	90	8	.2	2	2	2	80
L23E 2+50S	251	13	.3	2	2	5	90
L23E 3+00S	141	15	. 1	4	2	19	30
L23E 3+50S	155	13	. 1	15	2	2	70
L23E 4+00S	70	17	.2	4	3	2	60
L23E 4+50S	85	10	.2	2	4	5	220
L23E 5+00S	342	15	.5	5	2	67	80
L23E 5+50S	97	17	.2	2	2	1	70
L23E 6+00S	72	18	.2	2	2	2	80
L23E 6+50S	170	1.6	- 2	2	2	14	70
L23E 7+00S	190	7	. 1	12	2	9	90
L23E 7+25S	62	15	. 1	2	2	2	50
STD C/AU-S	58	40	7.2	39	14	51	1300

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L23E 7+50S	55	14	. 1	2	2	4	60
L23E 7+75S	51	4	. 1	2	2	1	50
L23E 8+00S	83	12	1.7	2	2	9	80
L23E 8+25S	164	8	. 2	5	6	1	160
L23E 8+50S	136	12	.9	4	2	3	430
L23E 9+25S	51	9	. 1	2	2	12	90
123E 9+50S	14	12	.3	2	2	1	110
L23E 9+75S	92	2	. 1.	3	3	16	90
L23E 10+00S	90	2	- 1	2	2	2	80
L23E 10+50S	109	12	- 1	2	2	2	30
L23E 10+75S	69	6	. 1	2	2	3	50
L23E 11+00S	84	5	. 1	2	4	1	70
L24E 0+00S	60	8	.2	2	2	5	100
L24E 0+50S	92	6	. 3	2	2	4	80
L24E 1+00S	100	4	. 1	8	4	240	120
L24E 1+50S	116	12	. 1	2	2	12	80
L24E 2+00S	131	10	. 4	2	2	1	230
L24E 2+50S	107	2	2	2	2	1	110
L24E 3+00S	181	2	.3	9 .	8	6	130
L24E 3+50S	31	26	. 1	2	2	1	70
L24E 4+00S	137	6	. 1	3	5	1	60
L24E 4+50S	78	9	. 1	3	2	11	80
L24E 5+00S	51	13	. 1	2	2	1	80
L24E 5+50S	144	7	. 2	4	2	11	90
L24E 6+00S	77	5	. 1	2	2	2	120
L24E 6+50S	56	12	.3	2	2	2	70
L24E 7+00S	139	2	. 1	14	10	2	50
L24E 7+50S	117	6	.3	2	2	1	70
L24E 8+00S	75	10	. 1	4	2	58	80
L24E 8+50S	63	10	. 1	2	2	1	60
L24E 9+005	30	13	. 1	2	2	4	50
L24E 9+50S	102	5	. 1	5	2 ·	1	80
L24E 11+25S	66	9	. 1	2	2	1	90
L25E 0+00S	87	11	- 1	2	2	2	150
L25E 0+50S	163	2	.2	2	3	5	110
L25E 1+00S	121	8	. 5	2	2	1	120
STD C/AU-S	62	42	7.7	38	16	49	1300

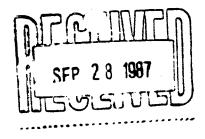
SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L25E 1+50S	207	10	. 1	6	7	3	60 170
L25E 2+00S	290	5 7	.2. .1	17 2	4 3	28 8	170 100
L25E 2+50S L25E 3+00S	139 163	13	. 1	2	2	1	110
L25E 3+50S	69	14	. 1	3	2	3	90
L25E 4+00S	60	15	.2	2	2	4	110
€25E 4+50S	73	17	.3	4	2	3	100
L25E 5+00S	102	14 8	.1 .1	5 5	3 2	2 5	60 80
L25E 5+50S L25E 6+00S	110 183	13	- 1 - 1	4	4	с 8	90
LŹ5E 6+50S	147	21	• 2	2	2	12	70
L25E 7+00S	109	21	.3	4	3	1	100
L25E 7+50S	149	8	. 1	15	7	3	80
L25E 8+00S	90	19	. 1	2	2	2	70
L25E 8+50S	109	19	. 1	4	2	3	80
L25E 9+50S	103	15	. 1	5	2	10	50
L26E 0+00S	115	5	. 1	21	10	2	60
L26E 0+50S	99	19	13	5	. 2	1 3	430 80
L26E 1+00S L26E 1+50S	31 124	24 11	.1 .2	2 4	2	15	140
han din tad han - dir 5 Kad Sart Kad							
L26E 2+50S	129	8	.3	5	3	35	70
L26E 3+00S	115	13	.2	4	4	5	90 100
L26E 3+50S	155	11	.2	5 8	2 2	3 1	$\frac{100}{110}$
L26E 4+50S L26E 5+00S	179 93	11 7	.2 .1	2	ž	1	70
L26E 5+50S	55	14	. 1	2	3	2	80
L26E 6+50S		13	.2	3	5	1	100
L26E 7+00S	109	2	. 1	29	7	8	160
L26E 7+50S	135	19	.3	6	5	5	110
L26E 8+00S	136	7	. 4	6	7	6	80
L26E 8+50S	107	17	.2	3	2	1	90
L27E 0+00S	38	25	.2	2	2	10	120
L27E 0+50S	180	11	.2	9 3	6	6 5	240
L27E 1+00S	146	20 10	.2 .3	د 16	2 8		150 300
L27E 1+50S	244	τO	• •			C	
L27E 2+00S	157	13	. 1		2	15	90
STD C/AU-S	59	43	7.3	38	17	47	1200

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L27E 2+50S	176	5	. 1	7	4	5	110
L27E 3+00S	487	8	. 2	6	6	3	60
L27E 3+50S	237	2	.21	ර	3	3	90
L27E 4+00S	70	9	. 1	2	2	5	50
L27E 4+50S	324	11	.2	4	2	8	110
L27E 5+50S	157	16	.3	2	2	6	160
127E 6+00S	109	8	. 1	2	2	9	70
L27E 6+50S	75	17	. 1	2	2	3	60
L27E 7+00S	185	12	.2	2	2	2	130
L27E 7+50S	98	15	. 1	2	2	1.	210
L27E 8+005	64	14	.2	2	2	2	100
L27E 8+50S	57	19	.3	2	2	2	160
L27E 9+00S	133	14	. 4	2	2	3	110
L27E 9+50S	165	31	.2	2	2	24	100
L28E 0+00S	100	8	.2	4	3	11	90
L28E 0+50S	155	14	.5	4	2	7	250
L28E 1+00S	209	8	. 4	7	6	9	200
L28E 1+50S	62	10	<u>,</u> 7	2	2	2	160
L28E 2+00S	20	15	. 1	2	· 2	1	130
L28E 2+50S	213	5	.2	12	3	4	260
L28E 3+005	122	14	.2	2	- 2	4	60
L28E 3+50S	87	8	. 1	2	2	465	150
L28E 4+00S	186	6	. 4	9	5	5	190
L28E 4+50S	159	11	- 1	2	3	4	100
L28E 5+00S	109	6	.2	3	- 3	2	70
L28E 5+50S	158	2	. 1	12	6	6	50
L28E 6+00S	97	6	. 4	2	2	9	70
L28E 6+50S	129	11	. 1	2	2	6	90
L28E 7+00S	96	12	• 2	3	2	1	240
L28E 7+50S	126	13	. 1	3	2	6	90
L28E 8+005	153	8	. 1	4	3	4	70
L29E 0+00S	75	13	.3	4	2	1	140
L29E 0+50S	117	17	. 1	2	2	11	80
L29E 1+00S	149	14	.2	2	2	6	100
L29E 2+00S	171	11	. 4	3	2	2	210
L29E 2+50S	111	8		4	5	5	160
STD C/AU-S	61	43	7.4	37	15	51	1300

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SAMPLE#	CU PPM	PB PPM	AG PPM	AS PPM	SB PPM	AU* PPB	HG PPB
L29E 3+00S	30	18	. 1	2	2	4	40
L29E 3+50S	117	6	. 1	8	2	2	110
L29E 4+00S	169	13	. 1	20	2	8	60
L29E 4+50S	133	19	. 1	5	2	4	140
L29E 5+00S	177	14	.2	చ	2	1	130
L29E 5+50S	176	8	. 1	4	2	9	150
129E 6+00S	112	5	. 1	6	2	4	110
L29E 6+50S	160	5	. 1	2	2	2	70
L29E 7+00S	59	6	. 1	2	2	29	60
L29E 7+50S	143	11	.2	2	2	2	50
L29E 8+00S	103	18	. 1	4	2	1	90
L29E 8+50S	83	17	. 4	2	2	4	80
L29E 9+00S	108	14	.2	3	2	2	140
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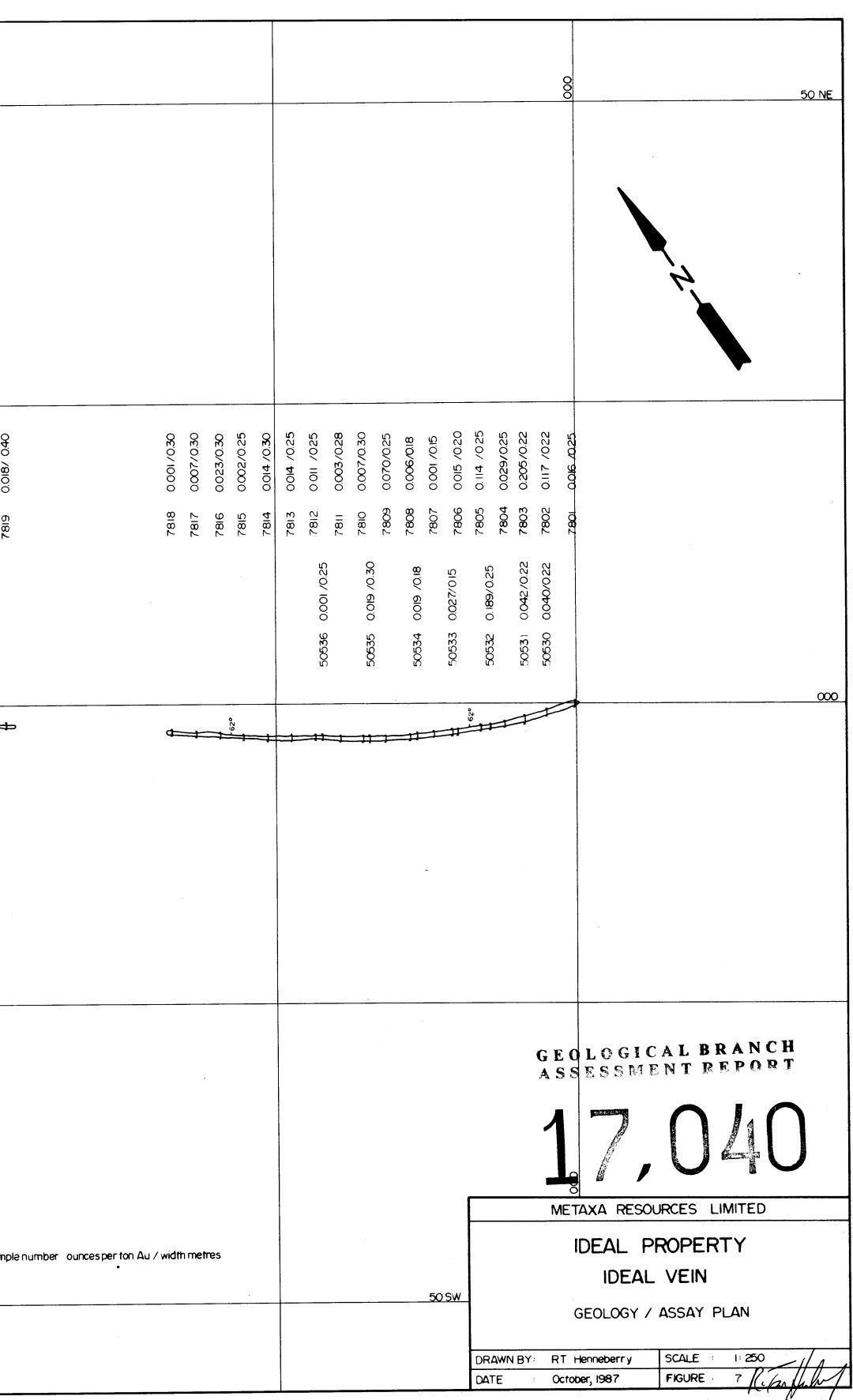
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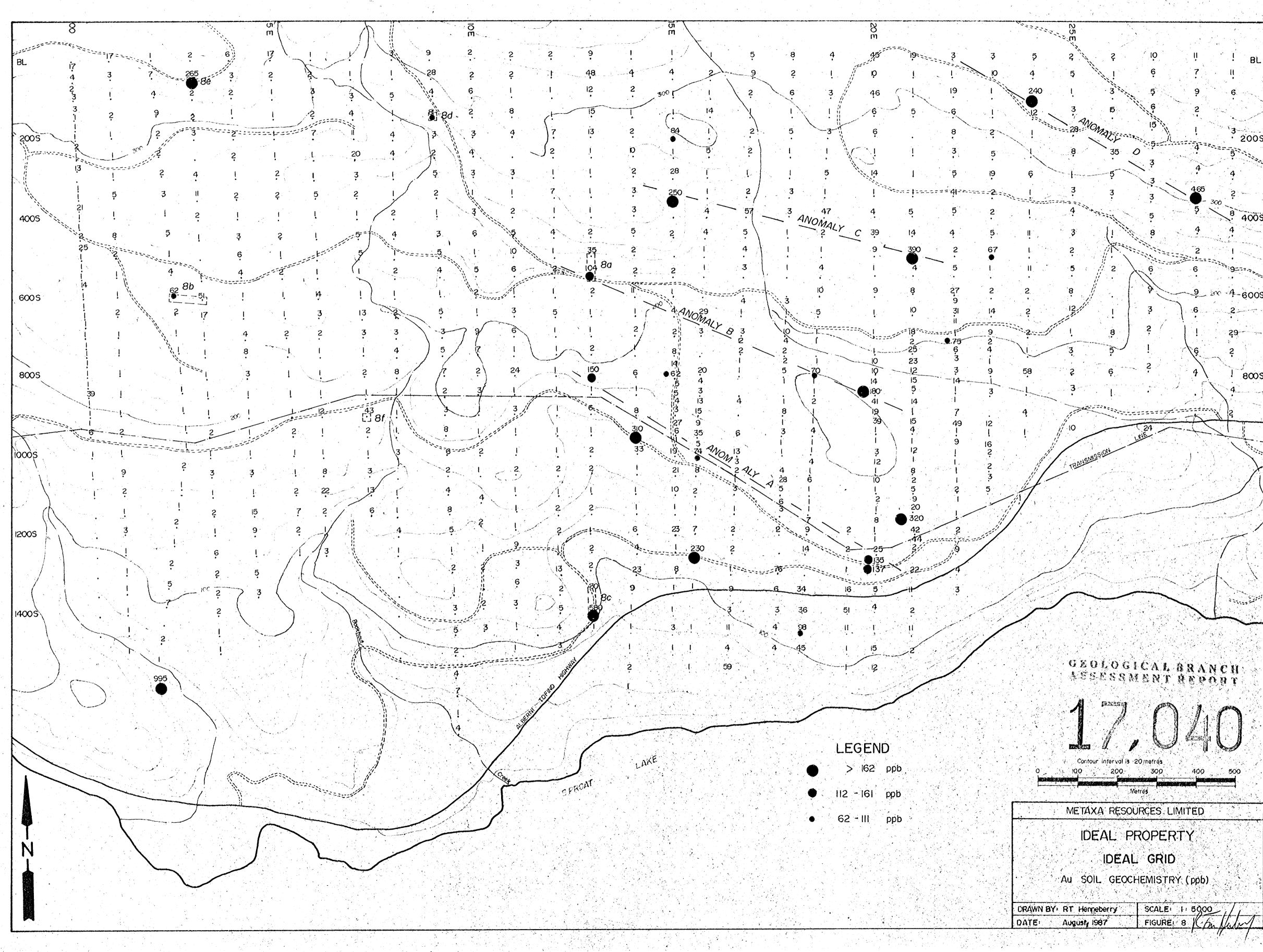
	ACME ANALYTICAL LABURATURIES LID. DATE 852 E. HASTINGS, VANCOUVER B.C. PH: (604)253-3158 COMPUTER LINE:251-1011 DATE	REPORTS MAILED
	ASSAY CERTIFICA	те / / /
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j.	STETSON RESSOURCES PROJECT EFIC-AIRTREC FI	LE# 87-4126 PAGE# 1
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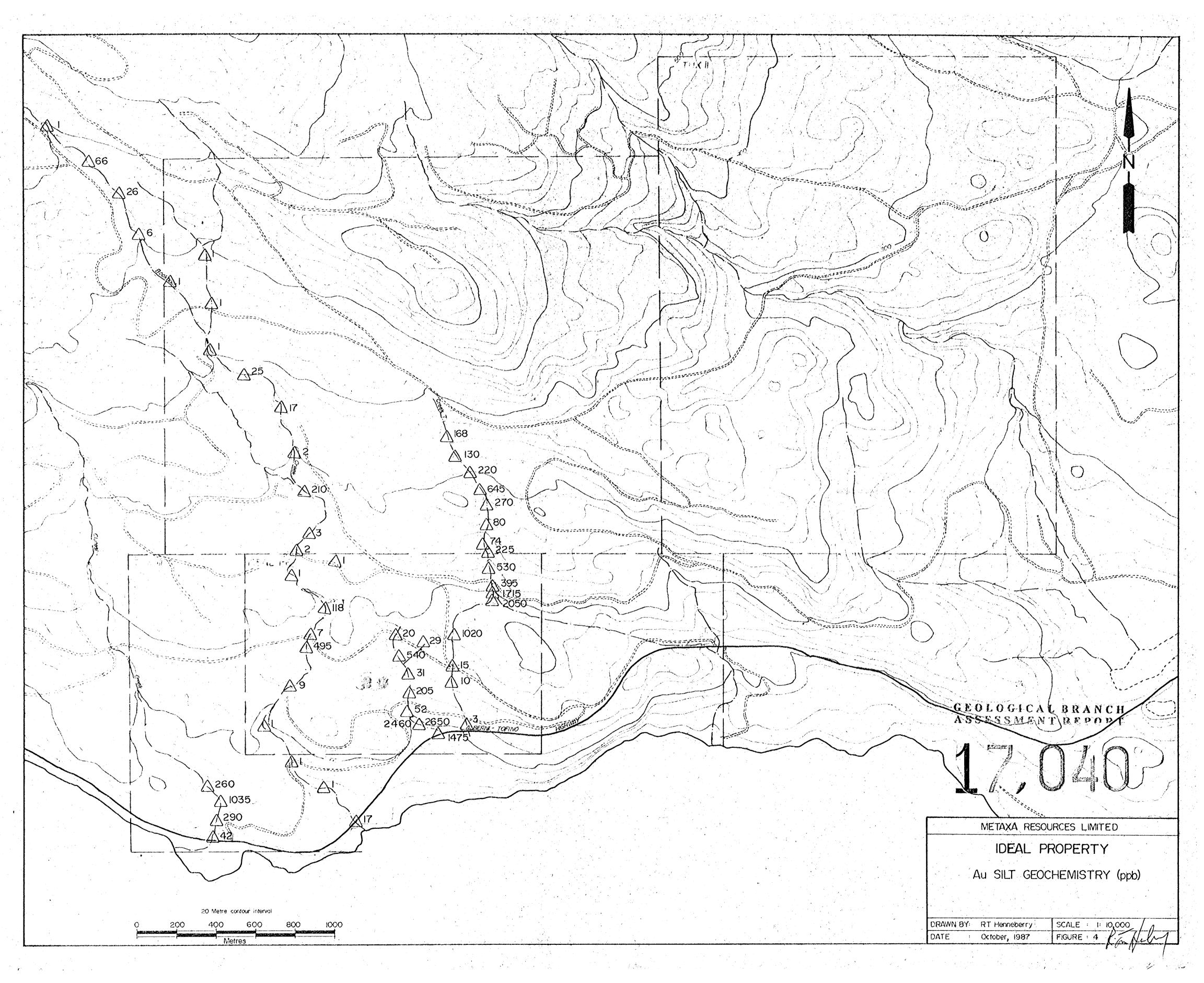


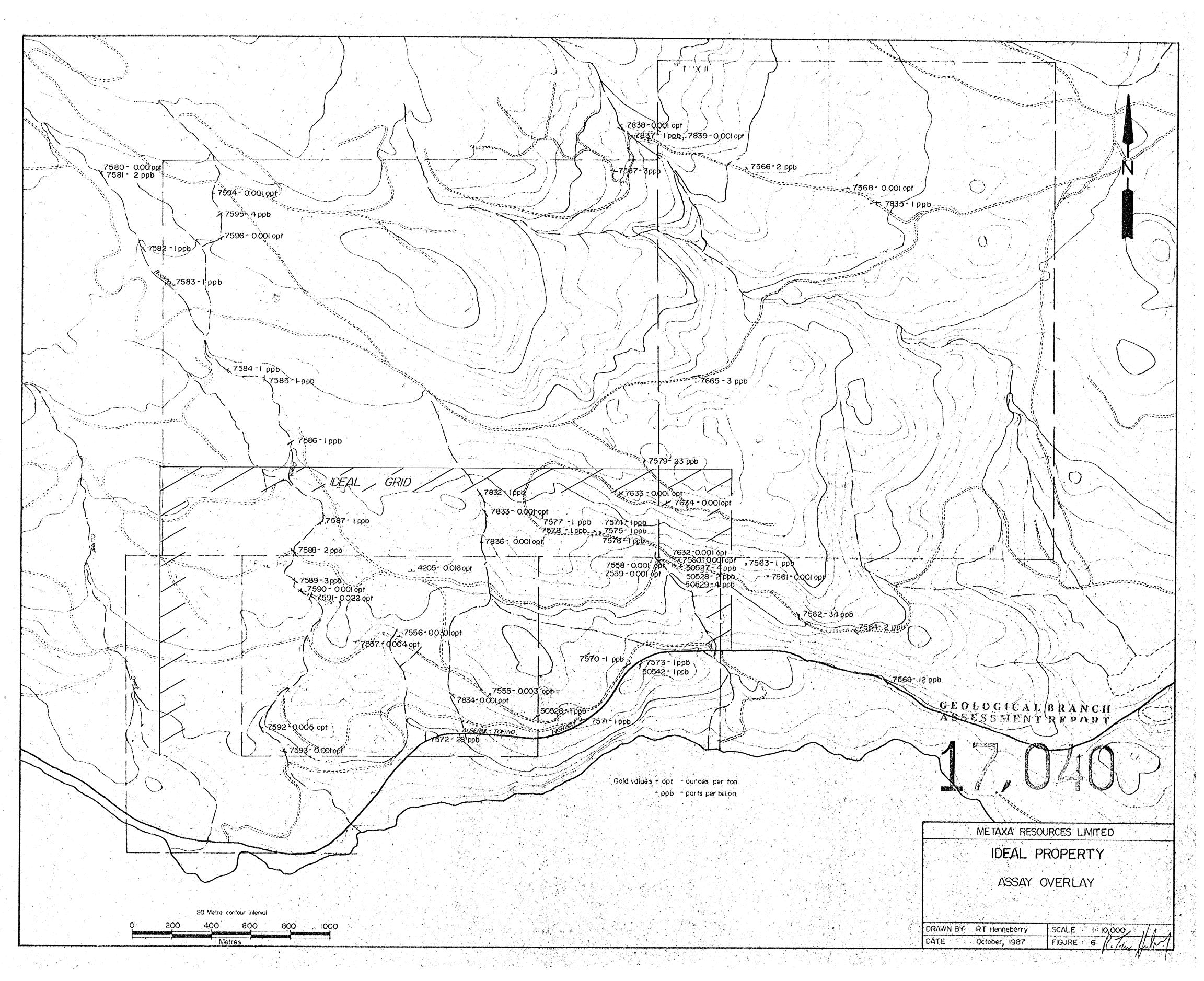
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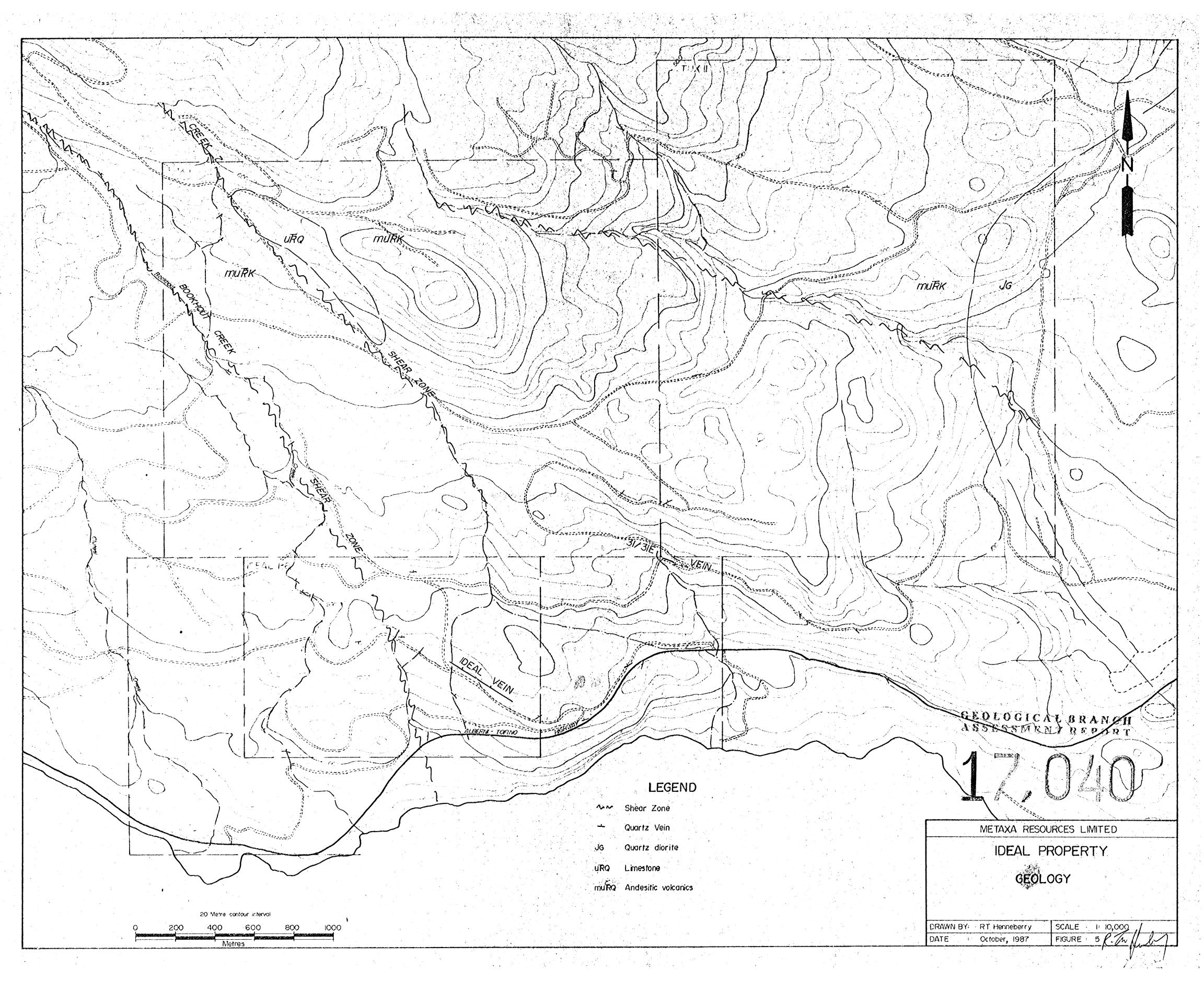
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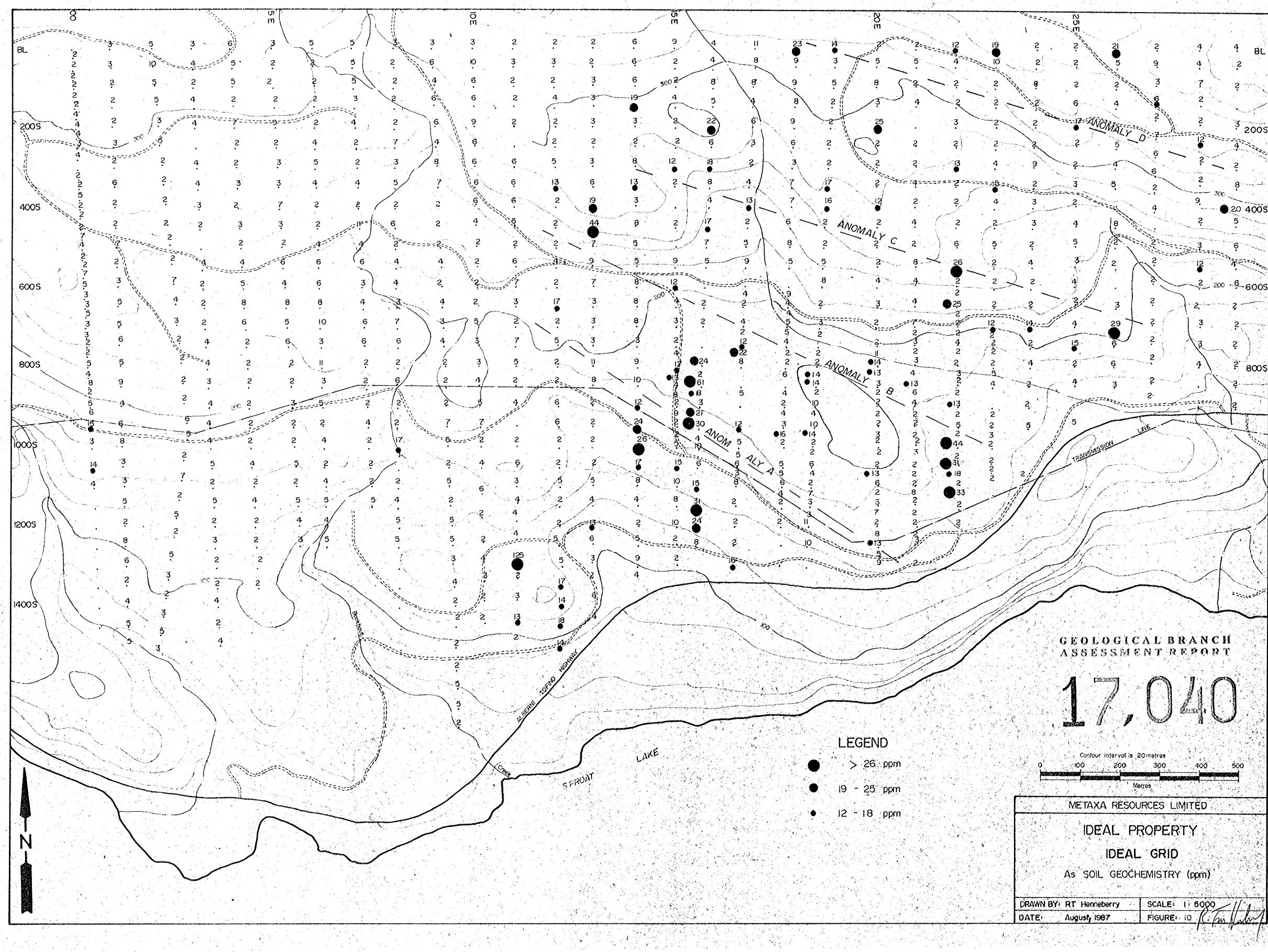






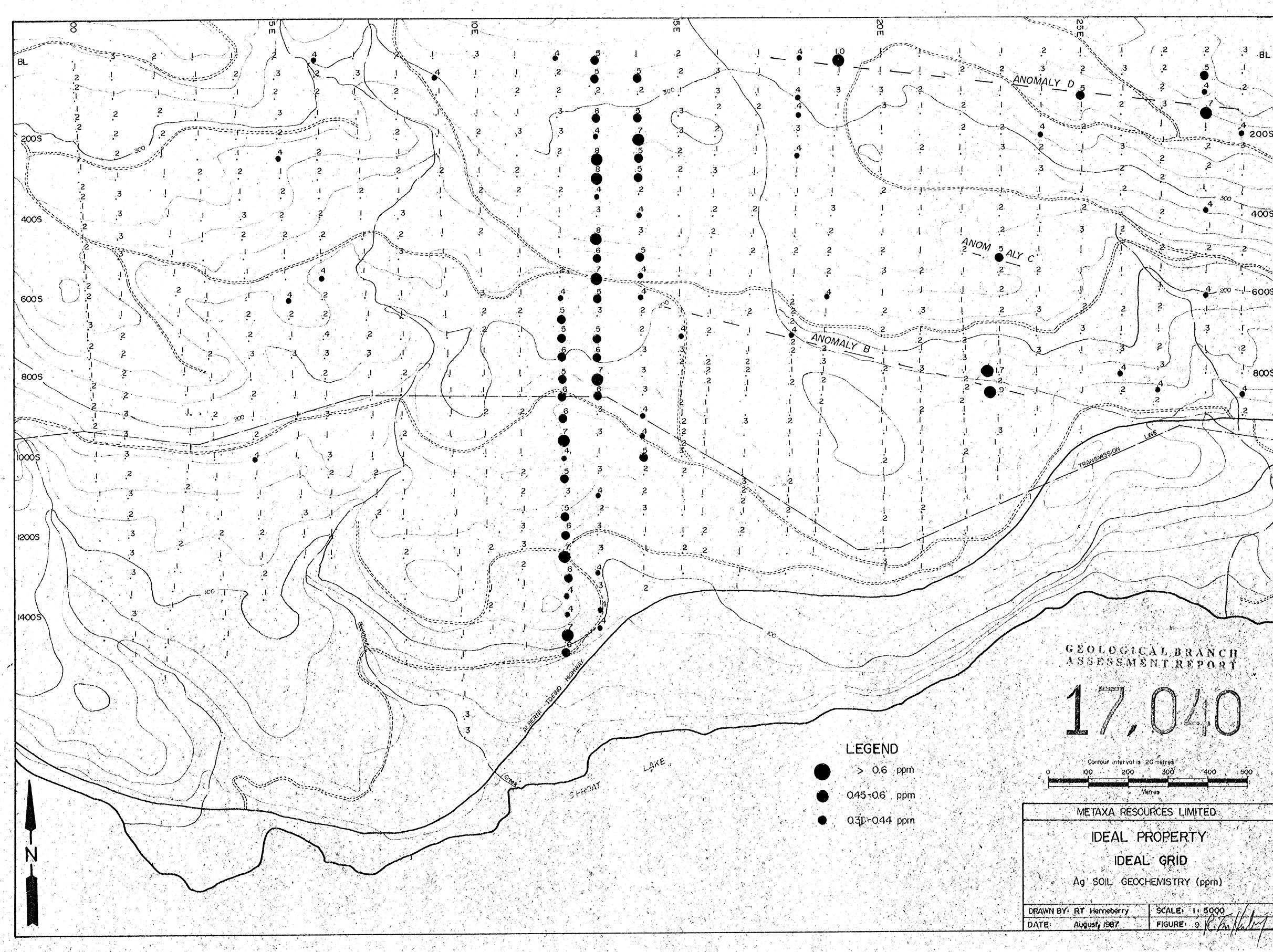






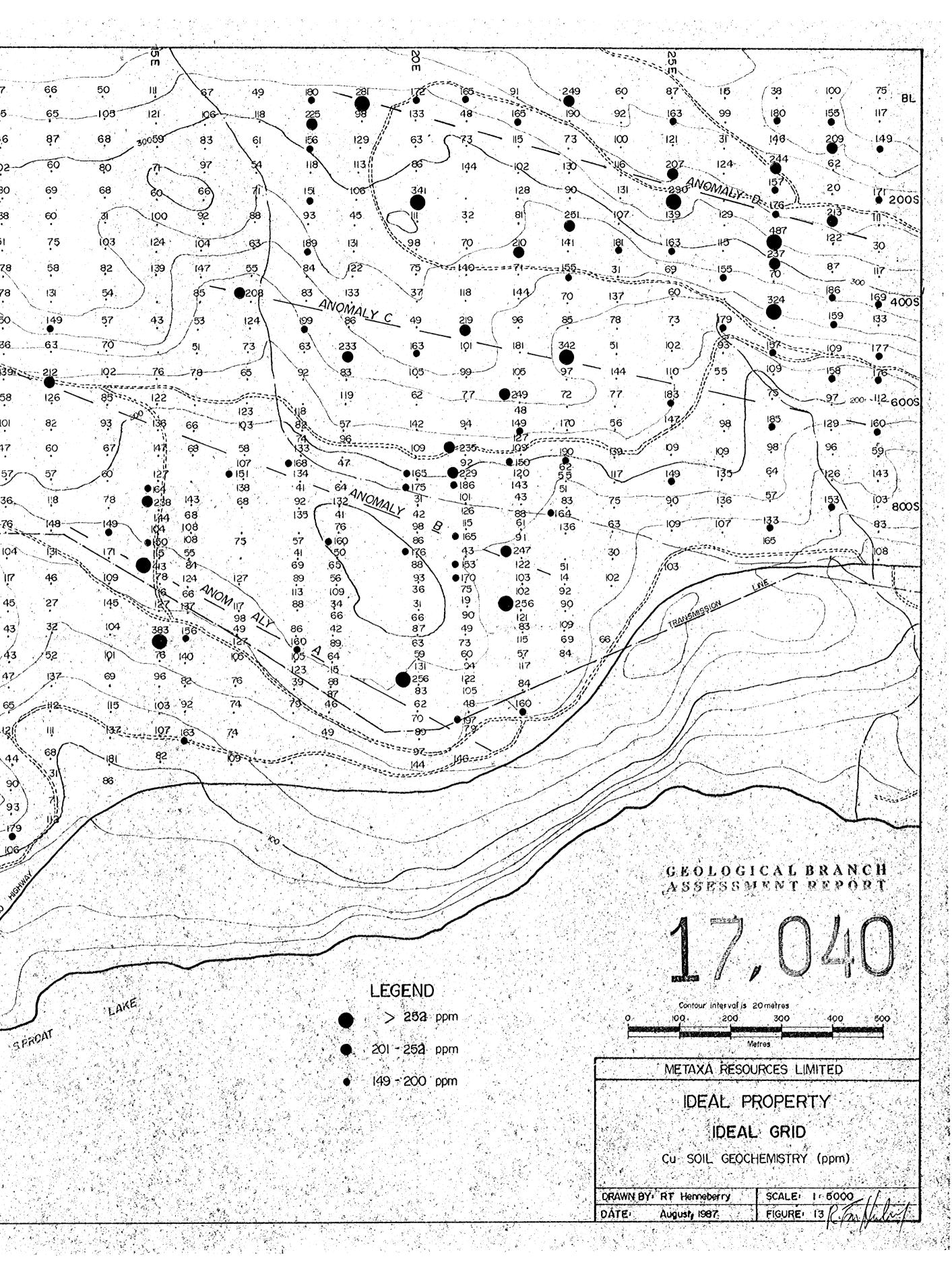
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