

ARIS SUMMARY SHEET

District Geologist, Prince George

Off Confidential: 89.02.17

ASSESSMENT REPORT 17080

MINING DIVISION: Clinton

PROPERTY: Newmac
LOCATION: LAT 51 45 00 LONG 124 40 00
UTM 10 5734329 384946
NTS 092N10E 092N15E
CLAIM(S): Newmac, Newmac 1-3
OPERATOR(S): Jacqueline Gold
AUTHOR(S): Morton, J.W.; Chapman, J.; Tregaskis, S.
REPORT YEAR: 1988, 71 Pages

COMMODITIES

SEARCHED FOR: Gold, Silver

GEOLOGICAL

SUMMARY: Early Cretaceous volcanic and volcaniclastic rocks have been intruded by Late Cretaceous to Early Tertiary diorite plugs. Gold and silver values are associated with quartz-carbonate or quartz-manganese veins. A gold-copper occurrence in mafic volcanics may be related to a separate event.

WORK

DONE: Geochemical
ROCK 139 sample(s) ;ME
Map(s) - 1; Scale(s) - 1:2000
SOIL 878 sample(s) ;ME
Map(s) - 2; Scale(s) - 1:5000, 1:2000
MINFILE: 092N

LOG NO: 0219	RD.
ACTION:	2/89
FILE NO:	

PRELIMINARY GEOLOGIC REPORT
 on the
NEWMAC CLAIM, BRITISH COLUMBIA
 for
JACQUELINE GOLD CORP. (OWNER & OPERATOR)
 by
MINCORD EXPLORATION CONSULTANTS LTD.

FILE NO.

<u>Claim Name</u>	<u>Record Number</u>	<u>Units</u>
St. Teresa 1	13414	1
St. Teresa 6	15531	1
Newmac	2301	20
Newmac 1	2409	20
Newmac 2	2410	30
Newmac 3	2424	15
		<u>77</u>

CAL BRANCH
 ASSESSMENT REPORT

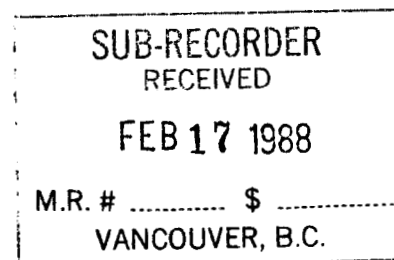
17,080

Clinton Mining Division
 Southwestern British Columbia
 Lat.: 51 degrees, 44 minutes North
 Long.: 124 degrees, 39 minutes West
 NTS Sheets: 92N/10E and 15E

Jim Chapman
 Scott W. Tregaskis
 J. W. Morton
 January, 1988

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A. SUMMARY

During September 1987, a program of rock and soil geochemical sampling, mapping and limited trenching was carried out on the Newmac Claim group for Jacqueline Gold Corp. This work was carried out under the supervision of Mincord Exploration Consultants Ltd.

Previous work on the property by Noranda Exploration Ltd. and Imperial Metals Corporation had outlined two anomalous areas. The objective of the current program was to further define these zones and test for additional mineralized trends.

As a result of the 1987 work, three discrete anomalous trends were delineated. The previously known Cow Trail vein, located on the A grid, was enlarged and a new quartz-sulfide stockwork zone, the Goat Trail zone, was outlined. Samples from this new zone returned values up to 14.0 oz/t silver and 0.03 oz/t gold.

Additional soils collected over the previously known copper anomaly on the B grid defined a strong coherent copper-gold zone with dimension exceeding 1300 metres in length and 50-400 metres in width. Float samples from this area contained up to 2% copper and 0.06 oz/t gold.

The third zone, known as the Road Gossan, shows a north-south trending gold, silver, copper, zinc anomaly with dimensions exceeding 600 metres in length and 200 metres in width.

A two phase exploration program is proposed for 1988. Phase I will entail additional geochemical sampling, mapping, trenching, geophysical surveys and drilling. The estimated cost of this program will be \$100,000.00. Contingent upon favorable results from this program, a Phase II program of diamond drilling, estimated to cost approximately \$210,000.00 would be warranted.

B. INTRODUCTION

In November 1987, J. Chapman, consulting geologist, was commissioned by Canevex Resources Ltd. to write a summary report of the company's Newmac property situated in the Niut Range of southwestern British Columbia.

The upper Chilcotan region has to date remained quite isolated from early prospecting rushes largely due to its inaccessibility. The copper porphyry exploration programs of the 1960's and 1970's saw the earliest systematic work in the area. During this period several copper, gold and silver showings were located and some of the earliest claims staked. Interest in the gold potential of the region prompted renewed



BRITISH COLUMBIA

Scale 1 : 7,500,000 approx.

Jacqueline Gold Corp.		
NEWMAC PROJECT Clinton M.D.; B.C.		
GENERAL LOCATION MAP		
	Scale : see above	N.T.S. 92N(10/B)
	Date : Jan '88	Figure :
	By :	1

exploration in the 1980's. It is as a result of this continued search that the present discoveries are attributed.

This report is based upon the writer's knowledge of the area and upon an on site examination of the property.

C. LOCATION AND ACCESS

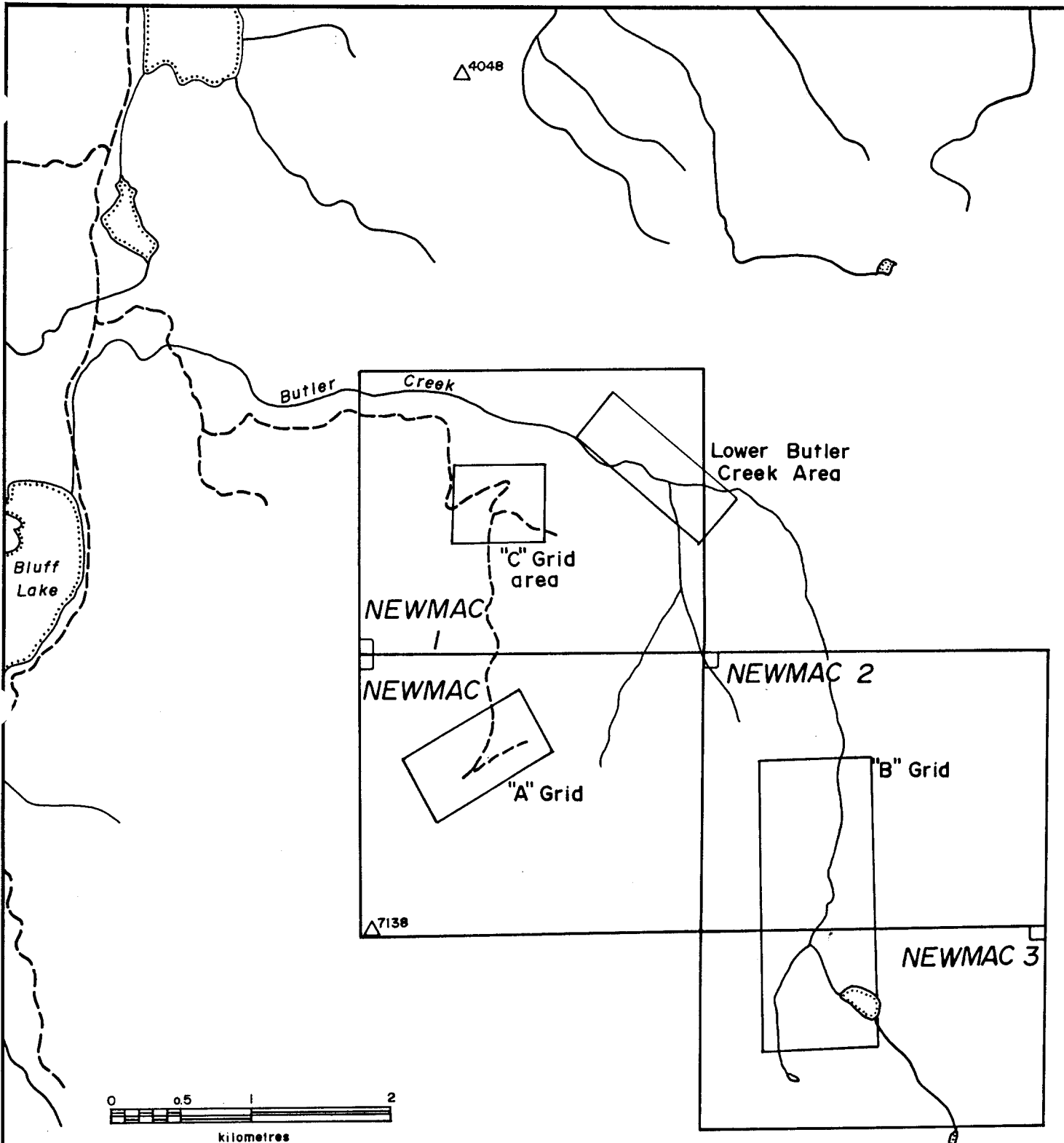
The Newmac property is centered at 51 degrees 44' North latitude, 124 degrees 39' West longitude on NTS sheets 92N/10 E and 15 E (Figure 1). This lies within the Clinton Mining Division of southwestern British Columbia. The property is located approximately 180 kilometers west of Williams Lake and 23 kilometers south of the village of Tatla Lake. The claims are situated three kilometers east of Bluff Lake and south of lower Butler Creek. Elevations range from 3500 feet on lower Butler Creek to 7500 feet at the southwest corner of the Newmac 3 claim. Terrain is steep and contains rugged rocky cliffs along the western flanks of the mountain. The south and central portions of the claims are vegetated by open, grassy alpine meadows. Below 5000 feet, the claims are covered with thick Lodgepole Pine thickets.

Good quality paved and gravel roads provide year round access from Williams Lake to within three kilometers of the western edge of the claims. A steep, rocky jeep trail provides access to the western portions of the claims but is accessible only to 4 X 4 vehicles. Access to the eastern portions of the claims is by foot or helicopter.

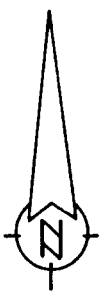
D. PROPERTY STATUS

The Newmac group of claims consists of six claims totalling seventy-seven units (Figure 2). All claims are owned by Jacqueline Gold Corp. through an option agreement with Canevex Resources Ltd.

The following table summarizes pertinent data for the claim block:



Jacqueline Gold Corp.		
NEWMAC PROJECT Clinton M.D.; B.C.		
CLAIM and GRID LOCATION MAP		
	Scale: 1:40,000	N.T.S. 92N(10/15)
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	By:	



Di Chapman

Table 1

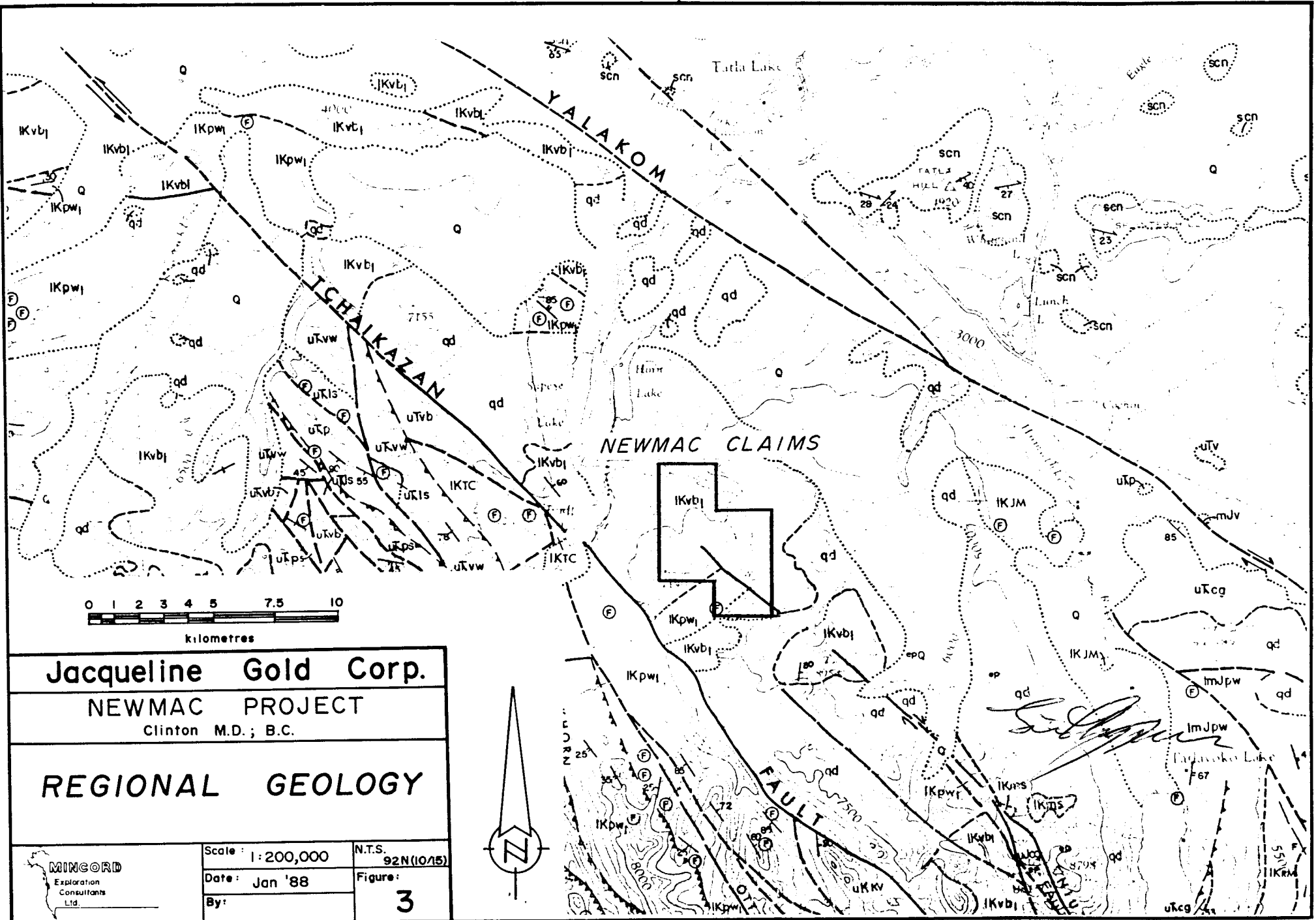
<u>Claim Name</u>	<u>Record Number</u>	<u>Units</u>	<u>Recording Date</u>	<u>Expiry Date</u>
St. Teresa 1	13414	1	66/13/07	88/13/07
St. Teresa 6	15531	1	67/25/07	88/25/07
Newmac	2301	20	87/18/06	88/18/06
Newmac 1	2409	20	87/22/09	88/22/09
Newmac 2	2410	20	87/22/09	88/22/09
Newmac 3	2424	<u>15</u>	87/26/10	88/26/10

77

E. HISTORY AND PREVIOUS WORK

The first known claims in the area were the "St. Teresa Claims" which were staked in about 1966 by A. McDonald. McDonald spent the next 18 years building the access road to the Cow Trail vein on the St. Teresa 6 claim then passed away shortly after completing it. Noranda was the first company to attempt a systematic exploration program during a porphyry copper exploration program in 1972. Noranda staked their 37 B.U. claims around Butler Creek and Butler Lake (approximately two kilometres west of the Cow Trail vein) then conducted a geochemical grid soil survey, a geological survey and an I.P. survey. This work defined a broad copper geochemical anomaly and a good geophysical I.P. response. Noranda, who are thought not to have analysed samples for gold content, dropped the claims without conducting any follow up work. The area in which Noranda worked saw little activity for the next ten year period.

In 1984, Ryan Explorations (a subsidiary of U.S. Borax) staked the M.S.B. claims in upper Butler Creek after silt sampling detected anomalous copper and arsenic concentrations. In 1984, Imperial Metals staked the Mac claims after acquiring an option on the St. Teresa claims. After grid soil sampling the Cow Trail vein area and conducting some bulldozer trenching, Imperial Metals drilled two diamond drill holes on the Cow Trail vein (to 67.7 metres [200 feet] and 66.1 metres [217 feet] respectively). The assay results from the drilling were disappointing and Imperial Metals subsequently dropped its option on the property. In 1987, Canevex Resources Ltd. staked the Newmac claims and purchased the St. Teresa claims from the estate of A. McDonald. Canevex optioned the property to Jacqueline



Jacqueline Gold Corp.

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REGIONAL GEOLOGY



Scale: 1:200,000
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N.T.S.
92N(10/15)
Figure:
3

Gold Corporation in the fall of 1987 and Jacqueline Gold contracted Mincord Exploration Consultants to conduct a preliminary exploration program on the property.

During October 1987, a senior geologist and three geotechnicians spent fourteen days on the property conducting geochemical soil grid surveys, mapping, and backhoe trenching. This program was successful in defining extensions to the "Cow Trail vein" and additionally located a quartz-sulfide stockwork zone in the "A grid" area. Soil sampling outlined a 1300 meter long copper-gold anomaly in the "B grid" area and reconnaissance sampling indicated a new zone of gold, silver, copper and zinc mineralization in the "Road Gossan - C grid" area.

F. GEOLOGY

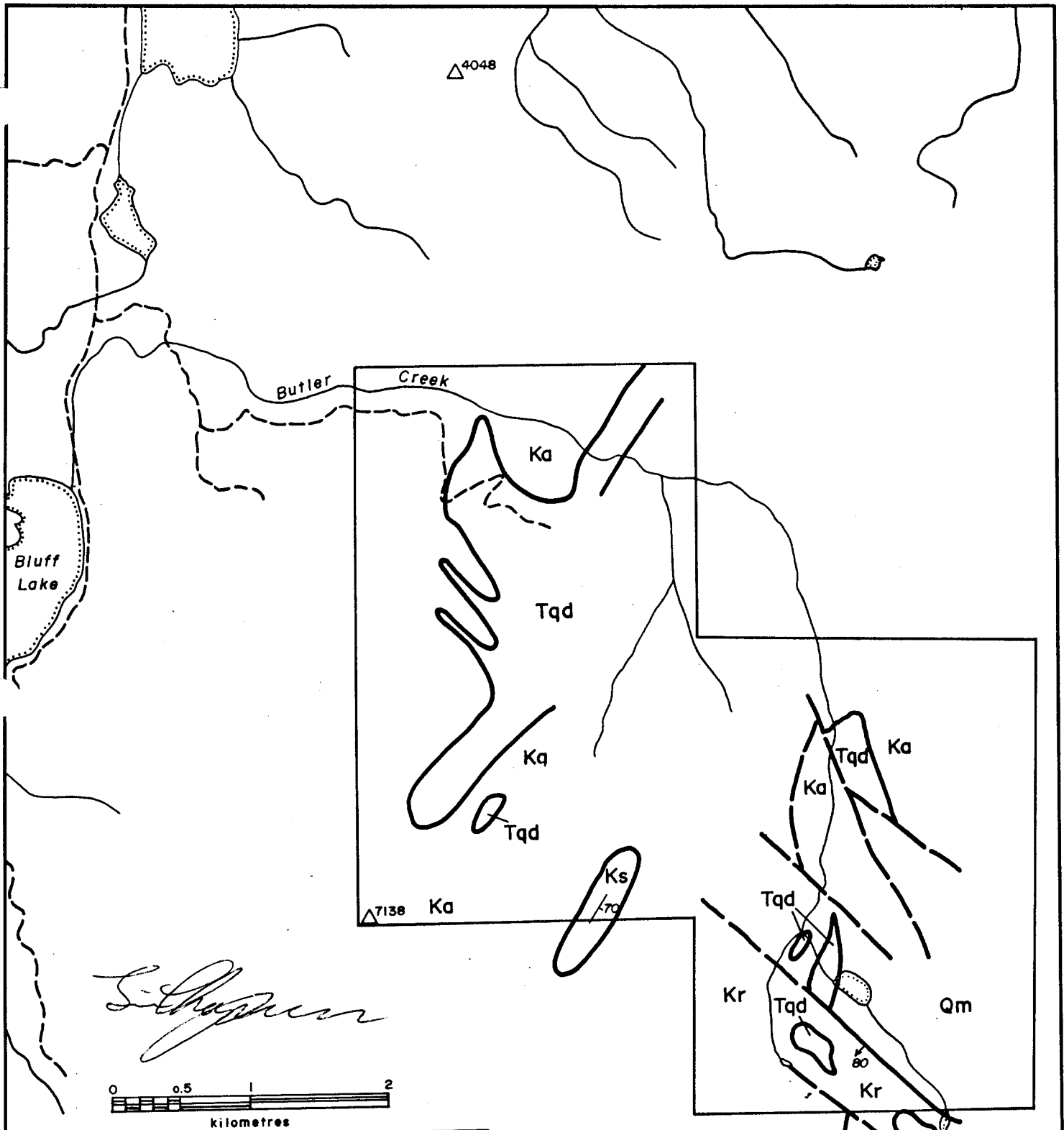
1. Regional

The Newmac property is located in a structural block between the right-lateral strike-slip Yalakom Fault and the left-lateral strike-slip Tchaikazan Fault. The early Tertiary/Tchaikazan Fault has an apparent displacement of about 32 kilometers, and a splay fault known as the Niut Fault runs through the heart of the property (Roddick et al, 1979). The Yalakom Fault trends northwest and is situated about 5 kilometers northeast of the claims. The transcurrent Yalakom fault is at least 225 kilometers long, has an apparent displacement of 130 to 190 kilometers and divides the Coast Mountains plutonic complex from the Intermontane Belt (Figure 3).

2. Property

The Newmac property covers a thick sequence of Early Cretaceous volcanics and volcanic sediments which have been intruded by Late Cretaceous to Early Tertiary diorites and quartz diorites related to the Coast Mountains plutonic complex (Figure 4).

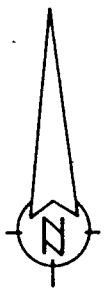
The lowermost portions of the volcanic sequence consist largely of andesitic tuffs, tuff breccias and porphyritic flows. The andesites are typically pervasively propylitically altered to dark green chloritic rocks with epidote clots and quartz-calcite fracture fillings. Pyrite and pyrrhotite occur as fracture fillings and disseminations and are present in amounts up to 10-15% in silicified structural zones. Overlying the andesites, possibly as a structural block, is a thick sequence of rhyodacites which form the cliffs to the south of Bulter Lake. The rhyodacites consist of flows, flow domes and tuffs cut by the Nait Fault and small bodies of quartz



Jacqueline Gold Corp.	
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GENERALIZED PROPERTY GEOLOGY	
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N.T.S. 92N(10/15)	Figure: 4

LEGEND

- Qm Glacial moraine
- Tqb Diabase dykes
- Tqd Quartz diorite - diorite
- Ks Volcanic grits, wackes
- Kr Rhyodacite flows, domes, tuffs
- Ka Andesite flows, tuffs, tuff breccias
- Fault



diorite. The rhyodacites show pervasive propylitic alteration as evidenced by fine fractures filled with chlorite, epidote and calcite. The rhyodacites contain up to 5% pyrite adjacent to diorite dikes. Locally the rhyodacites have been intruded by diabase dikes which were subsequently cut by low and high angle faults. The next youngest portion of the volcanic sequence, displayed in a conspicuous ridge situated in upper Butler Creek, consists of volcanic sandstone. This clastic package is cut by a few high angle barren quartz veins but shows only weak alteration. Probably the youngest volcanic rock known is a thin layer of fresh vesicular basalt which occurs on the ridge due south of Butler Lake. Much of the area around Butler Lake, and the B grid, is covered by a mantle of glacial moraine which probably ranges from 5 - 20 meters in thickness.

The project area was intruded by a series of quartz-diorite to diorite intrusives in late Cretaceous to early Tertiary time. The largest exposure of intrusive is located in the western portion of the claims and can be followed intermittently from the Cow Trail vein (A grid) area down through the C grid area to Butler Creek. The diorite ranges from finely to coarsely crystalline but is typically a medium crystalline, medium-dark green porphyritic diorite to quartz diorite. Most exposures exhibit a moderate pervasive propylitic alteration but trenching has exposed some intensely argillized zones adjacent to mineralized structures. Other structures show intense quartz-sericite-pyrite alteration over zones ranging from a few centimeters to tens of meters and are common within the C and B grid areas.

3. Mineralization

Mineralization is thought to be directly associated with the diorite to quartz-diorite intrusives where it occurs in the form of discrete quartz veins. These veins contain chalcopyrite, galena, sphalerite and pyrite in structural zones such as the Cow Trail vein as well as in quartz manganese stockworks, and silicified, pyritized zones related to structures and intrusive contacts.

Four mineralized areas were investigated during the 1987 program and will be discussed separately in the following section.

G. GEOCHEMICAL PROGRAM

1. Introduction

A total of 878 soil samples and 139 rock samples were collected over the three main grid areas and additional reconnaissance traverses. All soil samples were taken from the B horizon where possible. These were packaged in paper sample bags and shipped to Acme Analytical Laboratories in Vancouver, B.C. for analysis by I.C.P. Samples which exceeded the threshold values for lead, zinc and silver were then assayed.

Rock samples collected during the work program were also analyzed by I.C.P. and assayed if significant results were obtained geochemically.

2. Discussion

2(a) A Grid Area

The A grid area was the focus of most of the work conducted by Imperial Metals. Imperial Metals was successful in delineating the trace of the Cow Trail vein and located quartz vein samples which contained up to 0.355 oz/ton gold, 33.3 oz/ton silver with 2.0% lead and 3.7% zinc. Recent work (1987) entailed enlarging the soil grid and backhoe trenching across projections of the Cow Trail vein. The grid sampling was successful in defining several new anomalous zones which contained significant gold, zinc and lead values. The most encouraging anomaly is a 350 metres long, northwest trending soil gold anomaly with values up to 395 ppb gold and which is open in both directions (Figure 5). A second anomaly was detected in the canyon above the Cow Trail vein consisting of a 125 metre by 50 metre zone with coincident gold, silver, lead and zinc values. Prospecting in this area located a series of quartz-galena sphalerite veins named the Goat Trail zone. These contained up to 14.0 oz/t silver, .026 oz/ton gold, 2% lead and 6.8% zinc. The veins in this zone are typically from .1 to 1 metre thick but could potentially form a stockwork system. A third zinc-lead anomaly with dimensions of approximately 200 metres by 75 metres was partially delineated in the northeast portion of the grid (Figure 6). Little is known of this area and the lack of gold or silver geochemistry is not understood.

Trenching along the Cow Trail spur road was successful in exposing mineralization in trenches 2, 3, 4 and 5 (Figure 7). Trench 2 exposed strongly argillized diorite with abundant quartz-manganese veinlets. Channel samples indicate widespread gold, silver, copper, zinc and arsenic mineralization, although of subeconomic grades. Trench 3 cut argillized diorite with abundant quartz-manganese veinlets. Channel sampling returned anomalous gold, silver and arsenic values.

Trench 4 cut the Cow Trail vein and a wide zone of intense quartz-manganese veining. Ten vertical channel samples taken across this area show a 7 metre wide zone which carries an average of 1.4 oz/ton silver and anomalous gold, lead, zinc and arsenic. As this anomaly has a significant width, it may offer a bulk tonnage, stockwork type target. Trench 5 was on the original Cow Trail vein exposure. Recent sampling confirmed the original high silver values and indicated widespread zinc, lead, silver mineralization over at least a 15 metre wide structural zone.

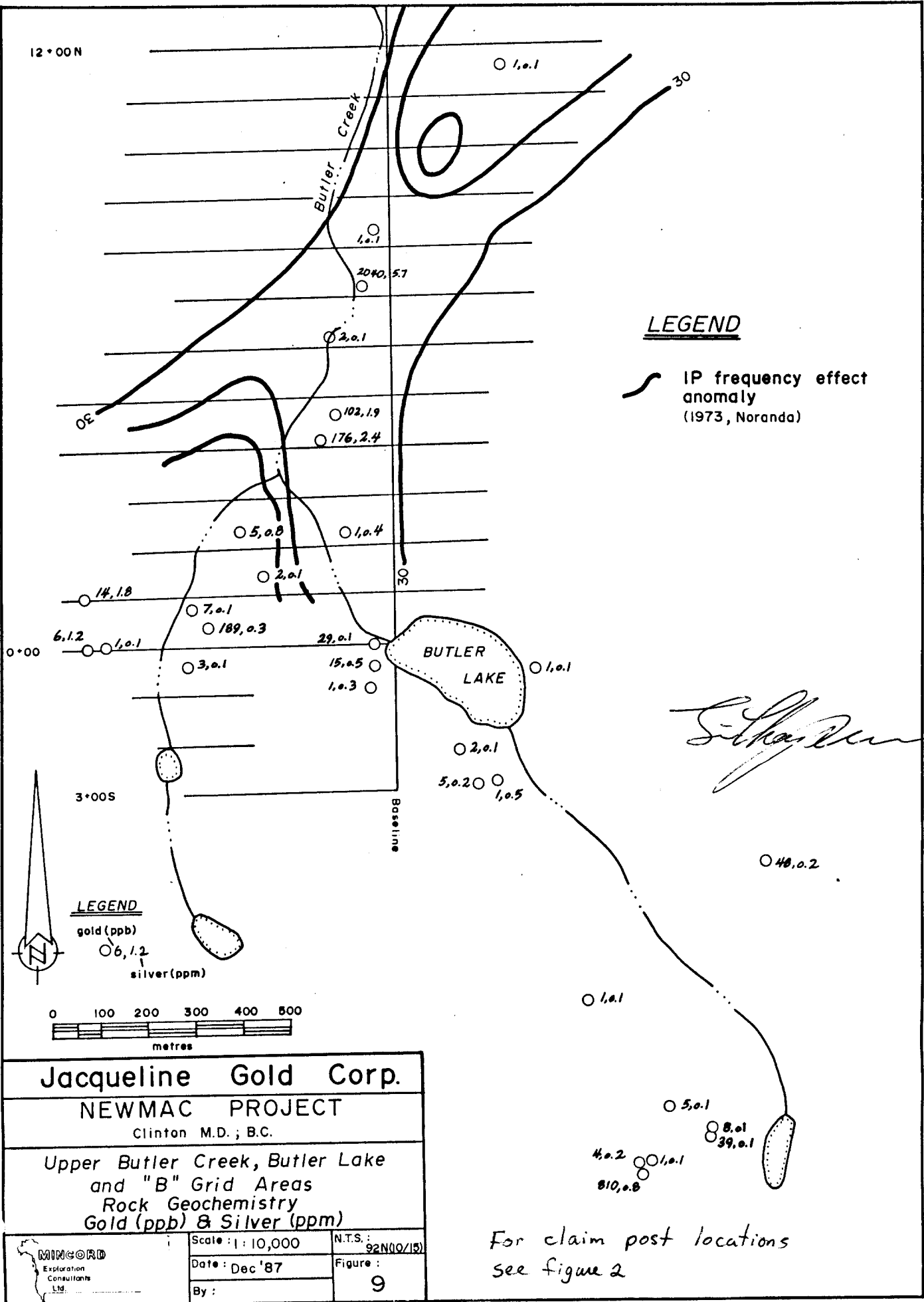
2(b) B Grid Area

The B grid is situated along upper Butler Creek and runs from Butler Lake for 1800 metres to the north. The terrain is fairly open, alpine shrubs and grasses on moderately to gently rolling hills. Much of the grid area is covered with a mantle of glacial moraine material, but limited outcrop exposures of goethite stained diorite and andesitic volcanics are found along the creek bottom. Results of the geochemical analyses of the soil grid defined a minimum 1300 metre long copper-gold anomaly, still open to the north (Figure 8). Outcrop and float sampling along the creek has confirmed an in situ-bedrock source for the copper-gold mineralization, and one rock sample from the middle of the anomaly contained 0.06 oz/t gold and 2% copper (Figure 9). The Induced Polarization survey conducted by Noranda in 1973 also indicated a coincident Frequency Effect anomaly over the copper-gold geochemical anomaly (Figure 9). This Zone offers an exciting exploration target and additional follow-up work is needed.

2(c) C Grid Area

Two short 600 metre rock and soil lines were conducted along the lower access road through an area with strongly iron-stained soil. A series of rock chip samples were taken from the most strongly silicified and pyritized

12°00N

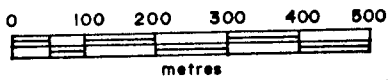


LEGEND

~ IP frequency effect anomaly (1973, Noranda)

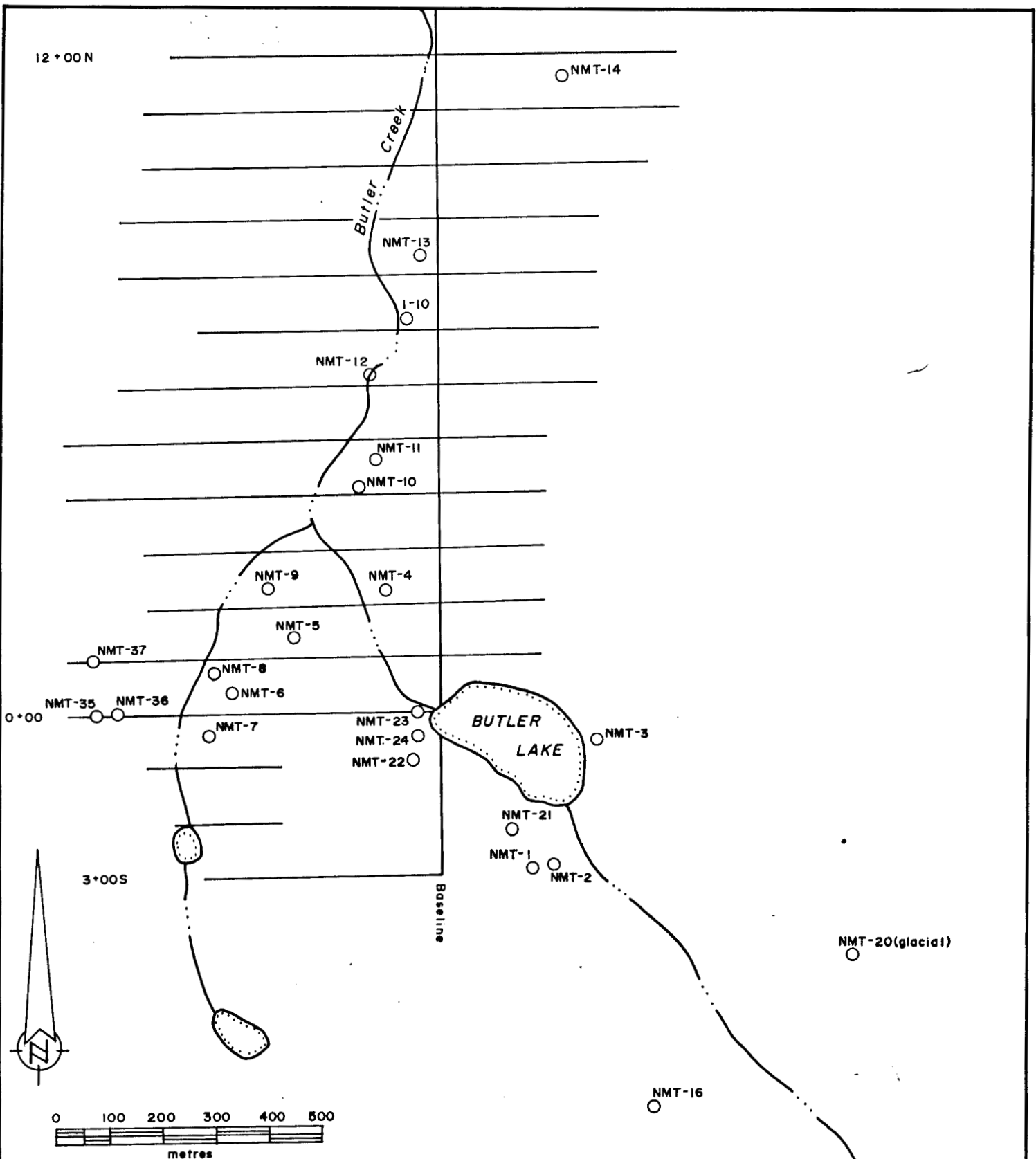
LEGEND

gold (ppb)
○ 6.1.2
silver (ppm)



Signature

For claim post locations see figure 2

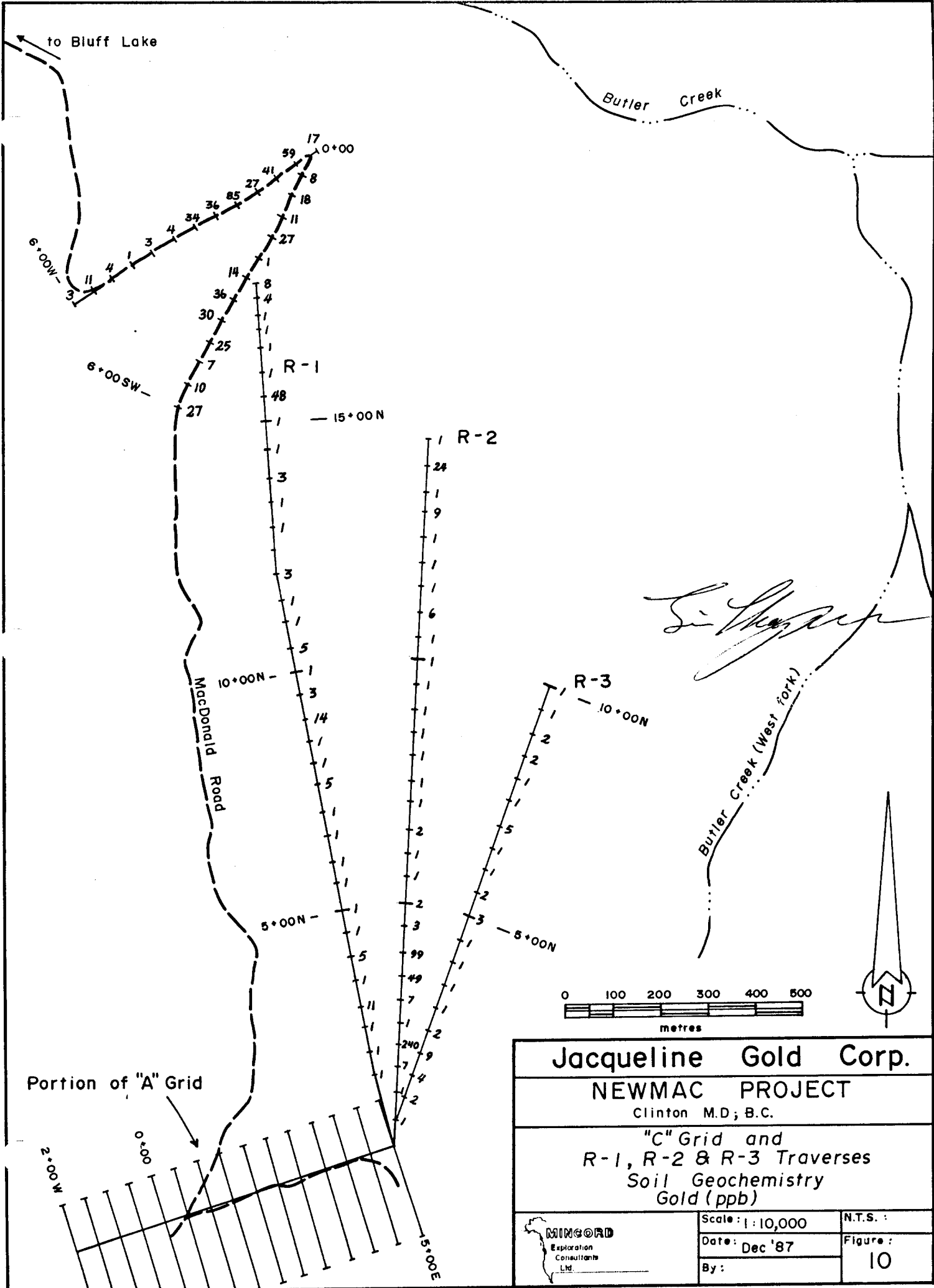


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*Upper Butler Creek, Butler Lake
 and "B" Grid Areas*
Rock Chip Sample Locations

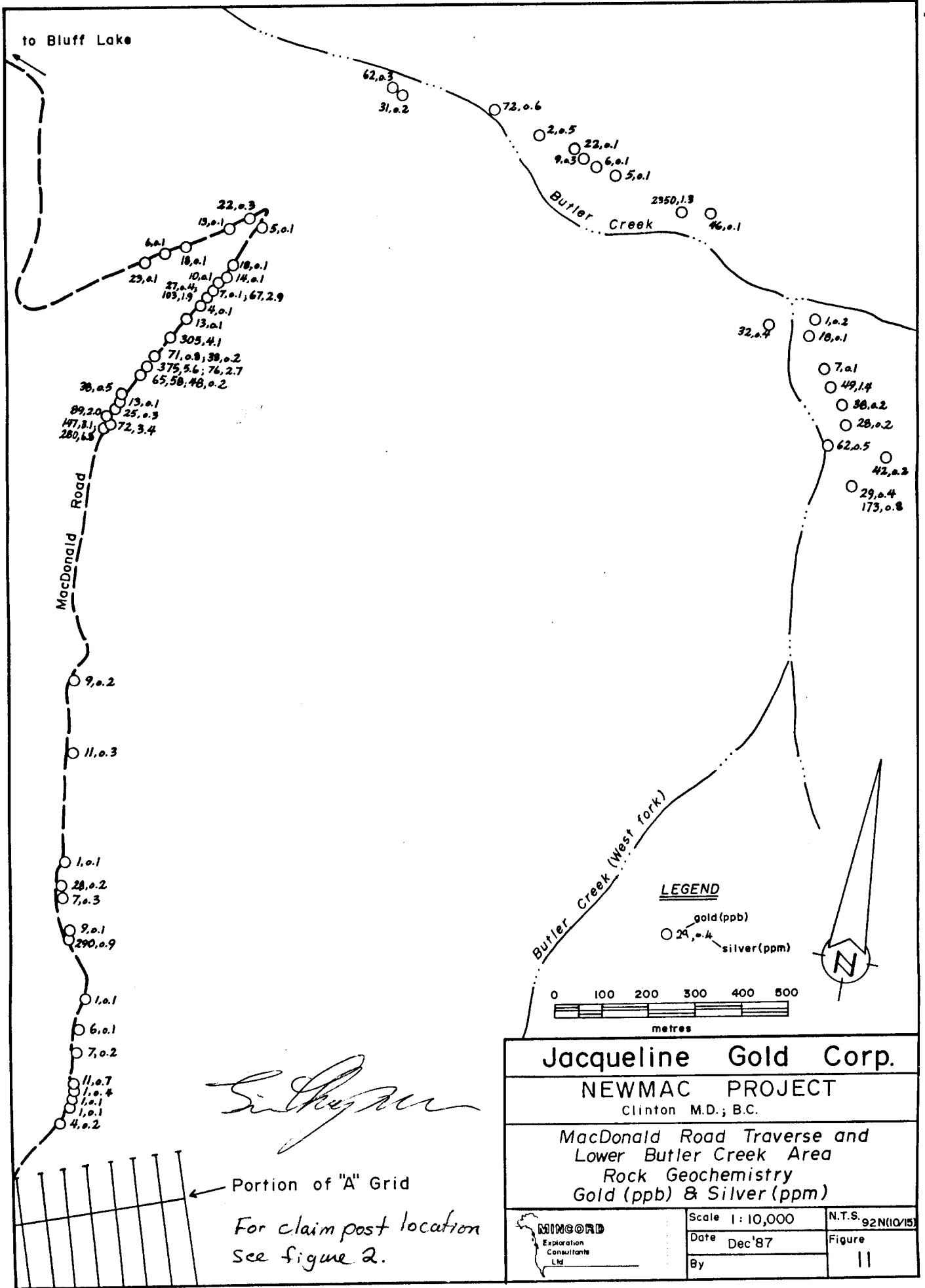
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	Date: Dec '87	Figure: Appendix
	By:	

For claim post location see figure 2.



Li. Harper

Jacqueline Gold Corp.		
NEWMAC PROJECT		
Clinton M.D; B.C.		
"C" Grid and R-1, R-2 & R-3 Traverses Soil Geochemistry Gold (ppb)		
	Scale: 1:10,000	N.T.S.:
	Date: Dec '87	Figure:
	By:	10



to Bluff Lake

Butler Creek (West fork)

MacDonal Road

LEGEND

○ gold(ppb)

○ 29, a.4 silver(ppm)

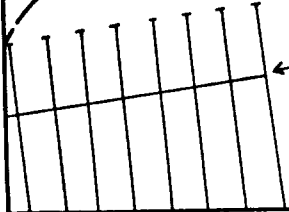
0 100 200 300 400 500 metres

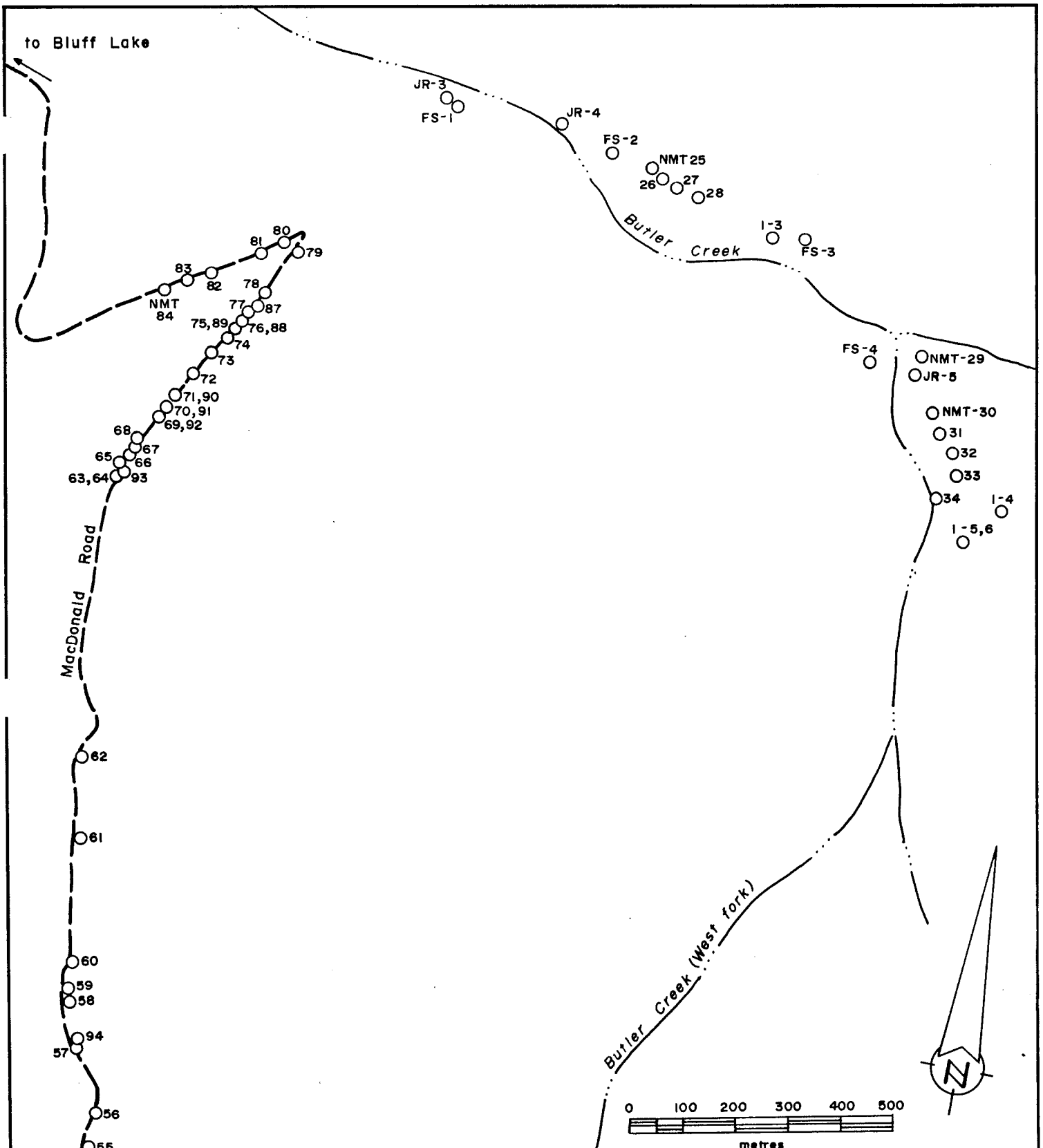


Jacqueline Gold Corp.		
NEWMAC PROJECT Clinton M.D.; B.C.		
MacDonal Road Traverse and Lower Butler Creek Area Rock Geochemistry Gold (ppb) & Silver (ppm)		
	Scale 1: 10,000	N.T.S. 92N(10/15)
	Date Dec '87	Figure 11
	By	

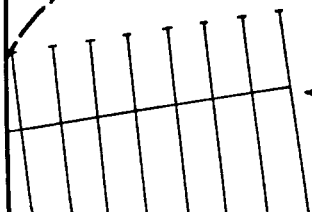
S. J. [Signature]

Portion of "A" Grid
For claim post location
See figure 2.





Note: all sample location numbers not otherwise prefixed are headed, "NMT"



Portion of "A" Grid
For claim post location see figure 2.

Jacqueline Gold Corp.
NEWMAC PROJECT
 Clinton M.D.; B.C.
 MacDonal Road Traverse and
 Lower Butler Creek Area
 Rock Chip Sample Locations



Scale 1:10,000	N.T.S. 92N(10/15)
Date Dec '87	Figure
By	Appendix

outcrops and a series of shallow pits were dug on the gossanous zones. Although this sampling was almost reconnaissance in nature, it served to show that the zone contained anomalous gold, silver, copper and zinc values over an area of at least 600 metres by 200 metres and that additional sampling is warranted (Figure 10).

2(d) Lower Butler Creek

A brief reconnaissance survey was conducted along Butler Creek in an attempt to find a rumored bornite showing (Figure 11). Widespread shearing and pyritization in altered diorites and andesites was found, but none of the samples were anomalous. One chip sample (I-3) from a quartz-pyrite-arsenopyrite shear zone along the creek contained 0.07 oz/t gold and anomalous copper, zinc and arsenic and may indicate a new gold zone. The area is steep and covered with extremely dense deadfall, Lodgepole Pine and alder, lines would need to be cut for a grid survey.

H. CONCLUSIONS AND RECOMMENDATIONS

The Newmac property contains several promising copper-gold exploration targets at this time. On the A grid the Cow Trail and Goat Trail veins, while narrow in themselves, contain significant precious metal values and have associated wide stockwork and structural zones which may offer a bulk tonnage potential.

The copper-gold anomaly on the B grid is extremely encouraging due to the extent and magnitude of the coincident anomalies. Chloritic andesites with pyrite chalcopyrite mineralization have returned values as high as 2% copper and 0.06 oz/t gold indicating a significant trend.

Preliminary mapping and sampling, mostly along the road, on the C grid has returned anomalous gold values from both soil and rock samples. Further sampling and mapping are warranted to outline this zone.

Additionally, much of the claim block has had little or no systematic work completed over it and this should be carried out during the more detailed programs on the established anomalies.

A two-phase, success contingent exploration program is recommended.

1. Phase I

- 1(a) Conduct geologic reconnaissance mapping over the entire claim block to determine the intrusive/volcanic contact relationships and to locate additional exploration targets.
- 1(b) Conduct additional soil and silt reconnaissance surveys in the central portions of the claim block.
- 1(c) Extend the A grid to the north and south between L0+00 and L5+00 E.
- 1(d) Extend the B grid to the north along Butler Creek for an additional 1000 meters.
- 1(e) Conduct detailed fill-in soil and rock sampling within the main copper-gold anomaly on the B grid and attempt hand trenching to find a bedrock source. Additional IP, magnetometer and VLF-EM geophysical surveys could better define mineralization.
- 1(f) Complete a grid soil survey over the C grid area.
- 1(g) Improved access on the A grid would facilitate further trenching operations.
- 1(h) An initial diamond drilling program on the best targets to provide down dip information.

2. Phase II

This program is contingent upon favorable results from the Phase I program.

- 2(a) Diamond drilling of the best targets in the A and B grid
- 2(b) Fill-in sampling, additional grid sampling of any new targets generated during the Phase I work.

I. BUDGET ESTIMATE

Costs for the Phase I program are estimated at \$100,000.00 with an additional \$210,000.00 for Phase II if warranted. Details of these costs are outlined as follows:

1. Phase

Soil Sampling, Labour & Analyses	\$ 16,250
IP Surveys	8,000
Geologic Mapping	9,000
Room & Board (90 man days @ \$60/day)	5,400
Transportation & Communications	3,000
Helicopter (3 hrs @ \$550/hr)	1,650
Bulldozer Work (40 hrs @ \$55/hr)	2,200
Line Cutting	1,500
Technical Report	3,000
Diamond Drilling - All Inclusive (1000 ft @ \$50/ft)	<u>50,000</u>
	<u>\$100,000</u>

2. Phase II

Geological,, Geochemical, Geophysical Surveys to follow up Phase I generated anomalies	\$ 30,150
Diamond Drilling (300 ft @ \$50/ft)	150,000
Geologist, Assist	15,000
Transportation	1,500
Room & Board (60 man days @ \$60/day)	3,600
Helicopter (15 hrs @ \$550/hr)	8,250
Technical Report	<u>1,500</u>
	<u>\$210,000</u>

APPENDIX 1: Statements of Qualification

STATEMENT OF QUALIFICATIONS

I, Jim Chapman, of 580 West 17th Avenue, Vancouver, British Columbia hereby certify:

1. I am a graduate of the University of British Columbia (1976) and hold a BSc. degree in geology.
2. I am presently self-employed as a consulting geologist.
3. I have been employed in my profession by various mining companies since graduation.
4. I am a professional geologist with the Association of Professional Engineers, Geologists, and Geophysicists of Alberta.
5. The information contained in this report was obtained from on site examination of the property and a review of data listed in the bibliography.
6. I do not have, nor expect to receive, direct or indirect interest in the property or in the securities of Jacqueline Gold Corp. or any of its subsidiaries.
7. I consent to and authorize the use of the attached report and my name in the Company's Prospectus, Statement of Material Facts or other public document.



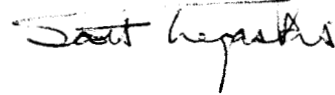
Jim Chapman
Consulting Geologist

Dated at Vancouver, British Columbia, this 4th day of January, 1988.

STATEMENT OF QUALIFICATIONS

I, Scott W. Tregaskis, residing at 11065 Broken Hill Road, city of Reno, Nevada, do hereby certify:

1. I am a practising geologist and have been since 1975 after completing a B. Sc. in Geology at Oregon University including the period during which I completed a M. Sc. in Geochemistry from Pennsylvania State University (1979).
2. I am a fellow member of the Society of Exploration Geologists and the Society of Geochemical Explorationists.
3. The conclusions and statements made in this report are my own and are the results of my own fieldwork and data interpretation.



S. W. Tregaskis
Consulting Geologist

Dated at Reno, Nevada, USA, this 13 of January, 1988.

STATEMENT OF QUALIFICATIONS

I, James William Morton, of 955 Braeside, West Vancouver, British Columbia, hereby certify:

1. I graduated from Carleton University, Ottawa, in 1971 with a Bachelor of Science in Geology.
2. I graduated from the University of British Columbia, Vancouver, in 1976 with a Master of Science in Soil Science.
3. I have worked for various mining and exploration companies since graduation.
4. I supervised the work described in this report.



J. W. Morton, M. Sc.
Geologist

Dated at Vancouver, British Columbia, this 27th day of January, 1988.

APPENDIX 2: Statement of Expenditures

STATEMENT OF EXPENDITURES

Professional Services:

S. W. Tregaskis	28 days @ \$300/day	\$ 8,400.00
J. Chapman	3 days @ \$300/day	900.00
J. W. Morton	5 days @ \$300/day	1,500.00
G. L. Garratt	3 days @ \$300/day	900.00

Field Personnel:

J. Green	18 days @ \$200/day	3,600.00
I. Hayton	14 days @ \$200/day	2,800.00
F. Sivertz	18 days @ \$200/day	3,600.00
T. MacKenzie	5 days @ \$250/day	1,250.00

Truck Rental	28 days @ \$50/day	1,400.00
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Helicopter Charter	3.3 hrs @ \$545/hr	1,798.50
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Communications:

Radio Rental	\$ 614.80	
Telephone	72.88	
Courier	<u>61.00</u>	748.68

Drafting		670.00
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Analyses:

1065 Sample Determinations @ Approximately \$11.52/sample		12,266.00
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Freight		287.70
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Field Equipment & Consumables		687.79
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Recording Fees		95.00
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Room & Board		4,436.14
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Fuel		663.68
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Airfare		772.08
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Map & Report Copying		355.79
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Miscellaneous Expenses		241.14
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Secretarial		<u>400.00</u>
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TOTAL EXPENDITURES		<u>\$47,772.50</u>
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FIELD DATES

Tregaskis	October 8 - November 25, 1987
Chapman	November 13 - 15, 1987
Morton	November 13 - 15, 1987
Green	October 3, October 10 - 26, 1987
Hayton	October 13 - 27, 1987
Sivertz	August 31, September 1 - 3, October 13 - 17, 1987
MacKenzie	August 31, September 1 - 3, 1987

APPENDIX 3: Rock Sample Descriptions

<u>SAMPLE</u>	<u>LOCATION</u>	<u>ROCK SAMPLE DESCRIPTIONS</u>	<u>SAMPLE TYPE & WIDTH</u>
(NMT-)			
1	B Grid Area	N10E80W vuggy qtz-epidote veins in rhyodacite	2 m chip
2	"	Mafic gabbro dike w/qtz, calcite, tr. py veining	grab
3	"	Potassically altered diorite cut by qtz-calcite veining	20 m grab
4	"	Strongly silicified andesite tuff 1-5% py, tr cpy	3 m chip
5	"	Silicified andesite tuff 3% py	grab
6	"	Silicified andesite 2-5% py	2 m chip
7	"	Sheared, silicified andesite N10E structure 1-2 cm py veinlets	2 m chip
8	"	Strongly silicified andesite w/py veinlets	2 m chip
9	"	Strong N40E zone of py veining adjacent to fresh rhyodacite	1 m chip
10	"	N60W structure in dark green chloritic tuff, strong silicification, 5% py	1 m chip
11	"	Weakly pyritic, partially foliated diorite	2 m chip
12	"	Andesite in creek, 1% py - unmineralized	2 m chip
13	"	Strongly fractured, goethitic andesite, possibly glacial	grab
14	"	NW Grid area, Hornblende diorite, hematite stained	grab
15	"	Bleached dacite, 1-2% py, po	grab
16	Butler LK Ridge	N55W90 structure cutting cliffs of rhyodacite	5 m chip
17	"	Diorite porphyry dike into rhyodacite	grab
18	"	Silicified, hematitic rhyodacite contact zone w/diorite	grab
19	"	N50W90 structure cutting rhyodacite, bleached, moderately silicified, strongly goethitic	10 m chip
20	Upper Butler	Glacial erratics - strongly pyritic, goethitic rhyodacite	grab
21	Butler LK	Strongly pyritic diorite dike	5 m chip
22	B Grid	Fine grained diorite, .5-1% diss. po. N90W shear	3 m chip
23	0+00N-0+50W	Fine grained diorite dike, .5-1% diss. po.	grab
24	0+50S-0+50W	Sheared diorite, diss & units of po.	2 m chip

<u>SAMPLE</u>	<u>LOCATION</u>	<u>ROCK SAMPLE DESCRIPTIONS</u>	<u>SAMPLE TYPE & WIDTH</u>
(NMT-) 25	Lower Butler Creek	Large cliff of flat lying andesite, locally silicified 2% py	3 m chip
26	"	"	"
27	"	"	"
28	"	"	"
29	Mouth South FK of Butler CK "Bornite Show"	Large zone of sheared, silicified, goethitic diorite w/1-2% py on fractures	5 m chip
30	"	"	"
31	"	"	"
32	"	"	"
33	"	"	"
34	"	Very strong fracturing and goethite	grab
35	B Grid	Goethitic, weakly qtz veined rhyodacite	grab
36	"	Goethitic rhyodacite	2 m chip
37	"	Goethitic rhyodacite	
38	A Grid	Silicified diorite w/2-3% py	
39	"	N60W75S qtz-galena vein, terminated by flat fault	.2 m chip
40	"	Float boulders of qtz vein w/diorite frags 1% py 1% gal, 2% sph	
41	"	Float below drill site - coarsely Xtlm qtz diorite	
42	"	N50E35N shear zone 4-5 m thick, silicified, py, goethitic diorite	
43	A Grid Creek Bottom	"	
44	"	"	
45	"	"	
46	McDonald Road	Mod-strongly pyritic rhyodacite, diorite, andesite float	
47	"		

<u>SAMPLE</u>	<u>LOCATION</u>	<u>ROCK SAMPLE DESCRIPTIONS</u>	<u>SAMPLE TYPE & WIDTH</u>
(NMT-) 48	McDonald Road	Mod-strongly pyritic rhyodacite, diorite, andesite float	
49	"	"	
50	"	Pyritic diorite and rhyodacite float	
51	"	"	
52	"	"	
53	Drill Site	High grade qtz vein float	
54	McDonald Road	Green andesite tuff, tuff breccia, locally bleached	2 m chip
55	"	Andesite tuff, bleached, fractured goethitic	7 m chip
56	"	Pyritic diorite, rhyolite breccia, andesite float	
57	"	Vuggy qtz vein w/tr gal, sph float	
58	"	Med xtaline sericitic, pyritic qtz diorite	3 m chip
59	"	Felsic chloritic volcanic, 1-3% py, pink matrix	2 m chip
60	"	Densely silicified andesite/diorite 5-10% py	5 m chip
61	"	Pervasively silicified felsic volcanic 5-8% dess. py	7 m chip
62	"	Med gray diorite, pervasive qtz-ser-py alt 5-10% py minor brecciation	3 m chip
63	Top of Road Gossan McDonald Road C Grid	Coarsely xtaline diorite, weak argillite alt 3-5% py	3 m chip
64	"	Vitreous qtz veining adjacent to diorite dike 1-3% py	grab
65	"	Qtz vein, fractured, minor goethite	1 m chip
66	"	Coarsely xtaline pyritic diorite, mod qtz veining, strong goethitic	3 m chip
67	"	"	2 m chip
68	"	Strongly goethitic, qtz-ser-py altered qtz diorite?volcanic?	3 m chip
69	"	Coarsely xtaline diorite, strong argillic	2 m chip
70	C Grid	Vuggy qtz vein, some chalcedony with fine dissem. pyrite, MnOx in vugs, subcrop	grab
71	"	Silicified, slightly pyritic qtz diorite, outcrop	grab
72	"	Silicified qtz diorite w/vuggy qtz-pyrite-magnetite veinlets	2 m chip

<u>SAMPLE</u>	<u>LOCATION</u>	<u>ROCK SAMPLE DESCRIPTIONS</u>	<u>SAMPLE TYPE & WIDTH</u>
(NMT-) 73	"	Coarsely xtaline diorite w/1-2% py, mod. argillic alt.	2 m chip
74	"	Qtz diorite dike w/locally strong qtz-ser-py alteration	2 m grab
75	"	"	
76	C Grid	Qtz diorite dike w/locally strong qtz-ser-py alteration	2 m grab
77	"	Strong propylitically altered diorite	
78	"	"	
79	"	Chloritic, silicified diorite w/1-3% diss. py	50 m grab
80	"	Diorite w/Qtz-ser-py alteration	
81	"	Strongly silicified med. gray diorite 2-5% py	2 m chip
82	"	Mod. silicified pyritic diorite float	
83	"	Strongly Qtz-ser-py altered diorite	2 m chip
84	"	Silicified diorite w/Qtz pyrite veinlets	2 m chip
85	Lower McDonald Road Backhoe Trenches	9' pit into rotten andesites WK goethite	pit sample
86	"	Strong N90W 30S shear in diorite strong goethite	5 m chip
87	"	Strongly Qtz-seriate-py altered diorite next to NMT-87-77	pit grab
88	"	N65W70S silicified shear in argillized diorite	3 m chip
89	"	Mod. silicified, pyritic diorite	
90	"	Mod. silicified N85E90	
91	"	Strong N85E shear, strong py, silicification	
92	"	Fresh diorite	
93	"	Qtz vein cutting argillically altered diorite	
94	"	Propylitically altered diorite	
95	Goat Trail Zone	6" calcite, Qtz, py vein in andesite	
96	"	Qtz-galena-pyrite vein, outcrop in creek N35W90-65W 3-6" thick	
97-102	"	Qtz-galena-sphalerite veins 3 - 10"	chips along veins
103	"	Sidebank slump with abundant float of Qtz-galenz-sphalerite veins	

APPENDIX 4: References

REFERENCES

Heim, R.C. et al, 1973: Geological Survey, Induced Polarization and Resistivity survey and Geochemical Survey of the B.U. claims, Noranda Exploration Co, Ltd. Assessment Report 4540

Morton, J.W., 1985: MAC - St. Teresa Summary Report of Geology and Drilling Results, Imperial Metals Ltd. Summary Report.

Roddick, J.A. et al, 1985: Mt. Waddington Geologic Map Sheet 92N, OF 1163

APPENDIX 5: Certificates of Analysis

Soil samples collected from the 'B horizon' at an average depth of 30 cm.

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: P1-2 ROCK P3-17 SOIL AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 21 1987

DATE REPORT MAILED: Nov 3/87

ASSAYER: *D. Jones* DEAN TOYE, CERTIFIED B.C. ASSAYER

MINCORD EXPLORATION PROJECT-NEW MAC File # 87-5150 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NMT-87-1	1	13	12	72	.2	29	6	977	2.51	19	5	ND	1	43	1	3	2	41	8.82	.024	2	60	1.14	6	.12	5	1.36	.01	.05	1	5
NMT-87-2	1	22	13	78	.5	69	12	674	2.96	3	5	ND	1	48	1	2	2	59	5.22	.042	2	119	1.14	4	.35	10	2.33	.02	.01	1	1
NMT-87-3	1	8	11	89	.1	9	3	1072	2.09	4	5	ND	1	24	1	2	2	9	3.27	.030	2	14	.89	52	.01	4	1.56	.04	.08	1	1
NMT-87-4	1	323	7	36	.4	28	12	383	6.71	5	5	ND	1	21	1	2	2	41	1.29	.065	2	62	.55	6	.22	6	1.67	.10	.02	1	1
NMT-87-5	2	189	6	40	.1	27	18	555	5.84	5	5	ND	1	33	1	2	2	97	2.44	.068	2	25	1.14	9	.14	8	2.86	.17	.05	1	2
NMT-87-6	7	253	6	28	.3	16	7	378	5.34	98	5	ND	1	15	1	2	2	74	1.34	.056	3	64	.83	9	.15	5	2.13	.11	.02	1	189
NMT-87-7	3	159	9	29	.1	21	9	459	4.92	4	5	ND	1	7	1	2	2	64	1.39	.042	2	67	.95	9	.24	8	2.04	.08	.01	1	3
NMT-87-8	7	372	6	31	.1	33	15	389	5.10	21	5	ND	1	11	1	2	2	65	1.37	.061	2	57	.87	5	.15	5	1.94	.08	.02	1	7
NMT-87-9	7	1271	6	29	.8	12	19	346	7.47	2	5	ND	1	19	1	2	2	70	1.67	.034	2	7	1.07	8	.08	7	3.14	.09	.01	3	5
NMT-87-10	13	1672	53	40	2.4	120	14	238	5.37	4	5	ND	1	32	1	2	2	44	1.30	.041	2	159	1.15	9	.18	14	2.47	.14	.05	1	176
NMT-87-11	20	1355	7	32	1.9	11	9	208	3.03	2	5	ND	1	9	1	2	2	43	.83	.047	2	14	1.00	4	.09	10	1.60	.08	.02	1	102
NMT-87-12	1	178	8	35	.1	36	13	717	4.25	15	5	ND	1	23	1	2	2	62	2.90	.116	2	74	1.18	3	.18	2	1.59	.08	.02	1	2
NMT-87-13	1	116	19	43	.1	17	14	359	3.62	18	5	ND	1	26	1	2	2	36	2.20	.033	2	62	.57	3	.27	10	2.38	.04	.01	1	1
STD C/AU-R	20	57	40	131	7.5	67	28	1040	3.96	39	19	7	39	49	18	17	21	55	.47	.086	37	55	.88	172	.07	35	1.87	.08	.15	13	510
NMT-87-14	1	33	4	25	.1	2	2	280	2.75	2	5	ND	1	45	1	2	2	52	1.27	.036	2	22	.83	9	.09	7	2.38	.20	.04	1	1
NMT-87-15	1	22	24	111	.1	4	4	453	4.10	29	5	ND	1	8	1	2	2	13	.11	.016	19	4	1.06	43	.01	2	1.82	.05	.05	1	1
NMT-87-16	2	12	2	58	.1	2	3	522	2.69	9	5	ND	1	14	1	2	2	9	1.66	.046	3	1	.54	21	.04	3	1.22	.05	.08	1	1
NMT-87-17	1	6	5	66	.2	10	14	870	4.14	2	5	ND	1	28	1	2	2	72	1.82	.034	2	26	1.92	30	.07	4	2.33	.09	.03	1	4
NMT-87-18	6	9	15	131	.8	9	5	1118	4.65	44	5	ND	1	19	1	2	2	37	1.59	.019	2	11	4.01	43	.01	4	3.43	.03	.04	1	810
NMT-87-19	4	31	14	103	.1	3	2	946	4.73	20	5	ND	1	4	1	2	2	30	.03	.035	4	8	1.71	60	.01	2	1.83	.03	.10	1	5
NMT-87-20	5	44	10	33	.2	1	1	440	3.12	24	5	ND	1	5	1	2	2	5	.07	.021	4	2	.32	63	.01	3	.58	.02	.13	1	48
NMT-87-21	1	87	4	57	.1	85	17	813	7.58	20	5	ND	1	24	1	2	2	59	1.66	.033	2	159	1.18	7	.29	6	2.37	.19	.14	1	2
NMT-87-22	1	264	5	39	.3	47	22	590	4.11	9	5	ND	1	19	1	2	2	56	2.25	.057	2	70	.85	8	.22	9	1.88	.16	.05	3	1
NMT-87-23	1	7	8	49	.1	76	18	729	3.03	45	5	ND	1	34	1	2	2	85	3.64	.066	2	141	1.02	6	.37	10	2.14	.27	.10	1	29
NMT-87-24	1	249	5	31	.5	35	22	472	4.54	25	5	ND	1	26	1	2	2	60	1.66	.083	2	101	.71	5	.17	4	1.96	.06	.04	1	15
NMT-87-25	2	22	9	65	.1	4	7	827	3.33	15	9	ND	1	43	1	2	2	42	.67	.041	2	6	1.59	13	.18	5	1.92	.06	.05	1	22
NMT-87-26	2	19	13	57	.3	2	5	764	3.62	19	5	ND	1	34	1	2	2	35	.52	.038	2	4	1.28	22	.18	5	1.69	.06	.05	1	9
NMT-87-27	2	31	29	71	.1	5	7	724	3.54	24	5	ND	1	50	1	2	2	51	.78	.032	2	11	1.77	16	.21	5	2.34	.05	.05	1	6
NMT-87-28	1	13	7	45	.1	1	3	841	4.38	32	5	ND	1	19	1	2	2	28	.58	.046	2	1	1.13	34	.11	3	1.97	.10	.13	1	5
NMT-87-29	1	151	5	23	.2	5	5	684	4.65	3	5	ND	1	50	1	2	2	86	1.09	.032	2	20	1.50	12	.15	5	3.33	.08	.02	1	1
NMT-87-30	4	158	2	35	.1	31	9	643	4.07	17	5	ND	1	10	1	2	2	86	2.17	.031	2	96	1.90	12	.23	10	3.74	.05	.03	1	7
NMT-87-31	2	448	4	20	1.4	26	7	246	5.30	2	5	ND	1	22	1	2	2	52	1.16	.025	2	140	.80	27	.23	6	2.22	.15	.11	1	49
NMT-87-32	11	229	2	34	.2	19	5	284	3.74	2	5	ND	1	13	1	2	2	83	1.40	.023	2	204	1.08	9	.31	8	2.18	.09	.09	1	38
NMT-87-33	8	70	5	19	.2	4	3	460	3.21	4	5	ND	1	6	1	2	2	56	2.62	.036	2	19	.85	6	.15	8	3.22	.05	.03	1	28
NMT-87-34	4	178	7	44	.5	93	23	431	6.85	9	5	ND	1	8	1	2	2	77	3.41	.034	2	298	.91	3	.23	11	3.46	.04	.02	1	62
NMT-87-35	1	454	10	133	1.2	3	2	130	7.86	630	5	ND	1	10	1	2	9	32	.11	.026	4	4	.19	27	.10	2	.70	.07	.04	1	6
NMT-87-36	1	154	6	56	.1	4	4	407	4.51	64	5	ND	1	19	1	2	2	55	.42	.017	2	10	.94	34	.08	5	1.99	.11	.06	1	1

MINCORD EXPLORATION PROJECT- IMAC FILE # 87-5150

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NMT-87-37	1	274	7	52	1.8	22	12	337	6.84	14	5	ND	2	33	1	2	5	82	.17	.037	11	57	.61	19	.05	7	1.33	.02	.09	2	14
NMT-87-38	1	58	6	97	.3	18	15	831	4.55	37	5	ND	1	33	1	2	2	96	1.65	.041	3	39	1.83	39	.16	5	2.85	.21	.04	1	4
NMT-87-39	5	57	822	1605	.8	16	13	1201	3.78	58	5	ND	1	46	8	2	2	55	5.48	.033	3	27	1.20	91	.10	7	2.26	.10	.06	1	27
NMT-87-40	11	441	1063	3780	42.6	3	4	2597	1.77	56	5	ND	1	87	33	13	2	3	15.84	.009	2	1	.11	7	.01	3	.18	.01	.05	1	205
NMT-87-41	3	4	8	62	.1	12	11	585	5.30	9	5	ND	1	54	1	2	2	107	1.91	.019	2	16	1.57	26	.15	3	5.17	.25	.01	2	1
NMT-87-42	2	36	15	30	.4	2	3	144	4.52	72	5	ND	1	3	1	2	6	22	.14	.046	2	8	.38	19	.01	4	.64	.03	.12	1	4
NMT-87-43	2	35	7	32	.3	3	8	373	6.20	100	5	ND	1	3	1	2	2	45	.21	.044	2	7	1.09	19	.03	6	1.32	.03	.11	1	23
NMT-87-44	5	29	9	43	.2	7	6	346	4.07	15	6	ND	1	9	1	2	2	62	.64	.038	2	17	1.21	66	.18	4	1.95	.05	.09	1	19
NMT-87-45	2	35	6	22	.1	4	4	235	4.36	26	5	ND	1	13	1	2	2	44	.27	.041	2	14	.70	42	.20	7	1.15	.04	.11	1	7
NMT-87-46	4	46	110	48	.7	4	5	294	4.32	23	5	ND	1	10	1	2	2	45	.25	.034	2	8	.53	51	.08	5	1.41	.06	.08	1	11
NMT-87-47	2	59	5	114	.4	14	19	1210	6.28	9	5	ND	1	14	1	2	2	96	.26	.031	2	27	1.94	20	.06	4	3.37	.08	.07	1	1
NMT-87-48	2	70	5	87	.1	15	17	1027	5.34	13	5	ND	1	63	1	2	2	103	1.68	.032	2	29	1.39	18	.20	2	5.07	.36	.02	1	1
NMT-87-49	1	86	4	64	.1	19	14	797	5.10	18	5	ND	1	30	1	2	2	104	1.00	.034	2	43	1.25	42	.18	4	3.19	.17	.06	1	1
NMT-87-50	1	68	3	93	.2	13	19	904	5.72	13	6	ND	1	31	1	2	2	142	.84	.028	2	22	1.21	18	.17	4	2.79	.21	.06	1	4
NMT-87-51	1	69	2	60	.1	58	17	708	4.02	8	5	ND	1	27	1	2	2	60	.99	.030	3	50	2.14	47	.16	7	2.41	.08	.05	1	1
NMT-87-52	1	25	5	47	.1	15	9	639	3.19	2	5	ND	1	22	1	2	2	57	1.04	.025	2	31	1.28	19	.16	3	2.20	.14	.03	1	2
NMT-87-53	25	1953	2864	2203	80.2	3	6	844	5.32	69	5	ND	1	14	19	152	2	6	4.58	.010	2	4	.16	5	.02	2	.35	.01	.04	1	111
NM-FS-1	1	23	4	68	.2	1	3	1072	3.84	9	5	ND	1	31	1	2	2	39	1.10	.051	2	1	1.23	24	.15	5	2.88	.06	.09	1	31
NM-FS-2	2	21	21	56	.5	1	4	843	3.86	18	5	ND	1	21	1	2	2	30	.91	.041	2	2	1.29	14	.15	7	1.93	.06	.04	1	2
NM-FS-3	1	12	5	42	.1	3	2	506	1.91	240	5	ND	1	28	1	2	2	2	3.43	.009	2	1	.21	15	.01	13	.21	.03	.06	2	46
NM-FS-4	3	197	7	57	.4	67	20	840	4.93	4	5	ND	1	12	1	2	2	94	1.48	.036	2	174	1.69	13	.26	12	2.90	.09	.07	1	32
NM-JR-1	1	2	2	84	.1	1	4	736	3.13	2	5	ND	1	8	1	2	2	11	.05	.012	3	2	1.04	168	.01	2	1.71	.04	.04	1	8
NM-JR-2	1	11	10	41	.1	4	3	215	1.67	6	5	ND	1	18	1	2	2	4	.08	.007	2	1	.24	1273	.01	4	.70	.02	.06	2	39
NM-JR-3	1	22	6	49	.3	1	3	754	3.74	11	5	ND	1	35	1	2	2	36	1.29	.048	2	1	.92	37	.14	3	2.80	.05	.08	2	62
NM-JR-4	4	53	10	43	.6	7	13	678	4.00	33	7	ND	1	19	1	2	2	32	5.29	.032	2	9	.91	34	.01	9	1.02	.03	.09	1	72
NM-TR-5	2	2209	17	56	1.6	13	16	224	37.90	6	5	ND	4	5	1	2	2	82	.63	.016	2	6	.37	10	.07	2	1.06	.04	.04	4	88
I-3A	3	298	23	330	1.3	5	15	1284	6.90	274	7	ND	1	75	3	2	2	5	7.10	.008	3	1	.83	15	.01	4	1.11	.01	.04	1	2350
I-4	2	225	2	27	.2	21	13	387	2.95	2	6	ND	1	12	1	2	2	63	1.59	.029	2	48	.88	19	.20	9	1.97	.09	.05	1	42
I-5	3	274	4	31	.4	8	16	291	4.97	509	5	ND	1	57	1	2	2	47	3.40	.035	2	10	1.39	16	.01	7	1.78	.04	.06	2	29
I-6	3	746	9	52	.8	12	19	1263	6.84	1031	5	ND	2	120	1	2	29	50	11.37	.013	3	6	1.43	8	.01	2	1.97	.01	.04	1	173
I-10	4	19224	3	135	5.7	51	32	179	5.28	7	5	ND	1	70	2	2	2	33	2.09	.034	2	133	.58	11	.15	9	2.95	.16	.04	1	2040
R-5	1	41	11	37	.1	5	7	424	2.96	5	5	ND	1	18	1	2	2	37	1.19	.041	2	10	.77	24	.10	3	1.52	.12	.04	1	18
RK-12	1	157	2	93	.1	7	18	1462	4.86	6	5	ND	1	88	1	2	2	113	4.61	.035	3	3	1.93	14	.29	2	8.22	.03	.03	1	24
STD C/AU-R	19	58	39	133	7.0	68	27	1030	3.99	42	17	7	38	50	18	18	20	56	.48	.086	37	61	.84	177	.08	35	1.80	.08	.14	13	490

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	%	%	%	%	PPH	PPB
NMA L1+50E 2+00N	1	28	19	93	.2	12	8	201	4.12	12	5	ND	1	15	1	4	2	86	.19	.029	3	28	.44	34	.07	3	2.69	.02	.01	1	1
NMA L1+50E 1+80N	1	31	13	77	.1	16	10	233	4.23	17	5	ND	2	14	1	2	2	80	.19	.024	3	32	.59	36	.07	3	3.06	.02	.02	1	1
NMA L1+50E 1+60N	1	23	12	74	.5	12	10	219	3.76	13	5	ND	2	14	1	2	2	78	.28	.022	3	25	.48	38	.06	3	2.54	.02	.02	1	1
NMA L1+50E 1+40N	1	31	14	66	.6	12	10	243	4.23	21	5	ND	2	17	1	2	2	81	.25	.027	3	26	.63	32	.07	3	2.92	.02	.02	1	1
NMA L1+50E 1+20N	1	41	10	72	.1	16	13	329	4.65	21	5	ND	1	14	1	2	2	89	.22	.024	2	30	.93	41	.10	3	3.26	.03	.01	1	1
NMA L1+50E 1+00N	1	31	11	70	.2	13	11	247	4.07	19	5	ND	2	12	1	3	2	84	.22	.023	3	25	.70	27	.08	3	3.00	.02	.03	1	360
NMA L1+50E 0+80N	1	39	12	65	.2	14	11	280	4.12	25	5	ND	2	12	1	2	2	78	.16	.023	3	26	.79	33	.07	4	3.27	.03	.02	1	33
NMA L1+50E 0+60N	1	28	13	82	.9	12	10	224	3.78	11	5	ND	1	14	1	2	2	78	.22	.026	3	25	.66	26	.08	8	2.78	.03	.03	1	2
NMA L1+50E 0+40N	1	35	15	61	.4	13	10	235	3.98	16	5	ND	1	13	1	2	2	74	.20	.036	3	27	.64	33	.08	2	3.26	.02	.03	1	1
NMA L1+75E 1+00N	1	27	11	62	.1	12	9	236	3.96	15	5	ND	2	15	1	2	2	82	.20	.021	3	26	.61	38	.07	3	2.61	.02	.03	1	2
NMA L1+75E 0+60N	1	36	9	71	.1	15	13	262	4.31	21	5	ND	1	15	1	2	2	85	.21	.025	2	30	.76	33	.08	6	3.18	.03	.02	1	14
NMA L1+75E 0+80N	1	28	9	65	.1	10	8	225	3.88	18	5	ND	1	16	1	2	2	81	.22	.022	3	21	.60	33	.06	4	2.63	.02	.02	1	2
NMA L2+00E 1+00N	1	29	11	73	.1	13	10	284	4.27	20	5	ND	1	15	1	2	2	85	.22	.022	3	26	.67	42	.09	4	2.99	.03	.04	2	1
NMA L2+00E 0+80N	1	28	12	58	.1	13	9	218	3.87	10	5	ND	1	14	1	2	2	86	.21	.021	3	23	.62	29	.09	3	2.70	.03	.03	1	11
NMA L2+00E 0+60N	1	36	7	64	.2	14	11	289	4.30	14	5	ND	2	16	1	2	2	90	.21	.024	3	27	.73	37	.11	6	3.35	.03	.03	1	1
NMA L2+00E 0+40N	1	19	10	50	.1	9	7	207	3.51	6	5	ND	1	18	1	2	2	85	.23	.015	3	23	.50	37	.09	3	2.16	.02	.01	3	1
NMA L2+00E 0+30S	2	42	11	77	.6	13	12	301	4.24	39	5	ND	1	11	1	2	2	70	.15	.033	3	21	.62	30	.07	4	2.89	.02	.04	1	1
NMA L2+00E 0+35S	1	24	8	55	.5	9	7	207	3.24	22	5	ND	1	12	1	2	2	67	.17	.023	3	22	.55	29	.07	9	2.60	.02	.03	2	1
NMA L2+00E 0+40S	1	30	9	57	.2	14	9	236	3.61	17	5	ND	1	13	1	2	2	75	.19	.030	3	27	.63	30	.09	3	2.91	.02	.02	1	3
NMA L2+00E 0+45S	1	41	10	62	.3	16	14	287	4.35	20	5	ND	2	13	1	2	2	84	.21	.026	3	32	.91	38	.12	3	3.50	.03	.03	1	28
NMA L2+00E 0+50S	1	19	6	93	.1	9	5	154	3.06	19	5	ND	1	13	1	2	2	68	.19	.030	2	25	.41	23	.07	3	2.12	.02	.03	1	1
NMA L2+00E 0+55S	1	26	7	54	.2	12	7	191	3.30	26	5	ND	1	15	1	2	2	70	.22	.025	3	27	.55	28	.08	3	2.47	.02	.03	1	5
NMA L2+00E 0+60S	1	31	8	58	.1	15	10	242	3.95	22	5	ND	2	15	1	2	2	80	.21	.021	3	32	.76	34	.11	4	3.01	.03	.02	2	1
NMA L2+00E 0+65S	1	25	7	53	.7	11	8	232	3.70	18	5	ND	2	18	1	2	2	83	.28	.025	3	25	.61	35	.10	3	2.55	.03	.04	1	1
NMA L2+00E 0+70S	1	36	8	60	.1	15	12	265	4.26	21	5	ND	1	15	1	2	2	85	.21	.026	3	31	.86	42	.12	3	3.51	.03	.02	3	1
STD C/AU-S	19	60	36	133	7.6	68	28	1028	4.01	40	21	8	39	50	18	18	21	57	.48	.086	38	60	.84	172	.07	38	1.80	.08	.14	14	48
NMA L2+00E 0+75S	1	31	8	56	.2	13	11	231	3.78	16	5	ND	2	14	1	2	2	77	.20	.021	3	27	.77	41	.12	3	3.46	.03	.03	1	1
NMA L2+00E 0+80S	1	21	7	47	.1	12	7	200	3.31	21	5	ND	1	16	1	2	2	75	.22	.022	3	28	.55	30	.09	4	2.56	.02	.01	1	1
NMA L2+00E 1+00S	1	23	7	56	.1	11	8	211	3.33	15	5	ND	1	14	1	2	2	74	.20	.023	3	25	.61	33	.10	3	2.60	.02	.02	1	1
NMA L2+00E 1+20S	1	22	5	49	.1	12	7	253	3.30	8	5	ND	1	16	1	2	2	79	.21	.017	3	25	.60	36	.12	4	2.50	.03	.02	2	1
NMA L2+00E 1+40S	1	31	8	71	.1	23	11	233	3.81	6	5	ND	1	14	1	2	2	79	.21	.028	3	38	.78	36	.12	4	3.47	.03	.02	1	2
NMA L2+00E 1+60S	1	29	4	65	.3	15	11	253	3.92	2	5	ND	1	16	1	2	2	84	.24	.031	3	32	.79	35	.12	4	3.53	.03	.02	1	1
NMA L2+00E 1+80S	1	34	7	66	.3	15	11	306	4.14	8	5	ND	1	15	1	2	2	89	.22	.030	3	28	.93	33	.13	4	3.68	.03	.03	1	8
NMA L2+00E 2+00S	1	37	7	74	.1	17	13	598	4.49	6	5	ND	1	18	1	2	2	99	.27	.020	3	35	1.00	60	.14	4	3.55	.03	.02	2	2
NMA L2+25E 1+00N	2	35	8	82	.1	13	10	257	4.21	18	5	ND	1	14	1	4	2	79	.16	.029	3	29	.66	36	.08	2	2.96	.02	.03	1	1
NMA L2+25E 0+80N	1	35	12	74	.2	13	12	247	4.37	17	5	ND	1	17	1	2	2	86	.22	.028	3	28	.70	37	.08	3	3.26	.02	.04	1	4
NMA L2+25E 0+60N	1	25	7	60	.1	11	8	207	3.85	11	5	ND	1	14	1	2	2	84	.19	.023	3	27	.57	31	.10	5	2.86	.02	.03	1	2

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NMA L2+25E 1+05S	1	20	9	59	.5	11	7	227	3.33	33	5	ND	1	15	1	2	2	72	.21	.026	3	26	.52	39	.10	2	2.24	.02	.03	1	3
NMA L2+25E 1+10S	1	21	9	72	.8	9	7	379	3.42	28	5	ND	2	16	1	2	2	75	.23	.030	3	20	.52	33	.10	2	2.31	.03	.04	1	1
NMA L2+25E 1+15S	1	33	7	64	1.0	14	11	297	3.68	59	5	ND	1	15	1	2	2	71	.22	.029	3	24	.76	47	.12	2	2.96	.03	.04	1	14
NMA L2+25E 1+20S	1	18	5	48	.2	8	6	320	2.87	12	5	ND	1	18	1	2	2	71	.25	.024	3	18	.44	35	.10	3	1.87	.03	.04	1	1
NMA L2+25E 1+25S	1	26	5	62	.2	11	9	234	3.51	20	5	ND	2	15	1	2	2	75	.23	.030	3	24	.65	32	.11	3	2.80	.03	.02	1	2
NMA L2+25E 1+40S	1	25	2	57	.1	12	9	247	3.62	17	5	ND	1	18	1	2	2	81	.23	.026	3	27	.73	34	.12	2	2.81	.03	.02	1	1
NMA L2+25E 1+60S	1	23	3	56	.6	12	8	262	3.19	5	8	ND	1	18	1	2	2	70	.24	.027	3	25	.71	36	.12	3	2.65	.03	.04	1	1
NMA L2+25E 1+80S	1	29	3	63	.2	14	9	305	3.54	4	5	ND	2	14	1	2	2	75	.20	.036	3	26	.84	38	.13	2	3.13	.03	.02	1	9
NMA L2+25E 2+00S	1	16	5	51	.3	9	6	320	2.79	5	5	ND	1	17	1	2	2	63	.22	.026	3	21	.60	33	.11	2	2.27	.03	.03	1	1
NMA L2+50E 2+00N	1	49	31	117	.9	12	11	296	5.69	19	5	ND	1	14	1	2	2	87	.12	.037	3	26	.59	32	.05	3	3.21	.03	.06	1	2
NMA L2+50E 1+80N	1	40	42	137	.6	12	10	311	5.25	17	5	ND	2	14	1	2	2	86	.13	.036	3	22	.60	40	.04	2	3.18	.02	.06	1	1
NMA L2+50E 1+60N	1	48	25	141	.5	10	10	355	5.93	27	5	ND	1	13	1	2	2	90	.12	.045	2	19	.55	43	.05	4	3.39	.03	.06	1	1
NMA L2+50E 1+40N	1	35	15	80	.4	13	11	321	4.25	16	5	ND	1	15	1	2	2	75	.19	.031	3	26	.71	32	.07	2	2.73	.03	.05	1	1
NMA L2+50E 1+20N	1	21	12	69	.4	9	7	257	3.56	10	6	ND	2	14	1	2	2	77	.20	.025	3	20	.47	35	.07	2	2.27	.03	.04	1	118
NMA L2+50E 1+00N	1	46	11	71	.1	17	13	321	4.82	20	5	ND	2	15	1	2	2	86	.19	.031	4	28	.87	41	.11	2	3.33	.03	.02	1	7
NMA L2+50E 0+90N	2	34	12	80	.4	13	11	322	4.70	20	5	ND	1	14	1	2	2	86	.18	.031	4	25	.68	41	.09	2	2.91	.03	.04	1	5
NMA L2+50E 0+80N	2	54	18	82	.1	16	15	382	4.90	23	5	ND	1	18	1	2	2	85	.22	.025	3	31	.97	44	.12	4	3.35	.03	.03	1	10
NMA L2+50E 0+70N	1	28	12	73	.2	12	9	306	4.21	17	5	ND	2	16	1	2	2	85	.22	.023	4	23	.62	37	.10	2	2.68	.03	.03	1	72
NMA L2+50E 0+60N	1	34	7	67	.3	15	12	268	4.25	9	5	ND	2	17	1	2	2	88	.25	.020	3	31	.91	30	.13	2	3.34	.03	.03	1	6
NMA L2+50E 0+50N	1	30	8	74	.4	15	11	291	4.17	10	5	ND	1	15	1	2	2	91	.23	.024	3	30	.79	41	.12	4	3.05	.03	.02	1	3
NMA L2+50E 0+45N	1	26	12	65	.1	13	9	290	3.80	10	5	ND	2	16	1	2	2	84	.23	.024	3	24	.74	43	.12	2	2.82	.03	.03	1	1
NMA L2+50E 0+40N	1	28	7	71	.1	13	10	281	3.87	11	5	ND	2	14	1	2	2	82	.21	.028	3	28	.74	32	.12	3	2.95	.03	.03	1	2
NMA L2+50E 0+35N	1	20	14	71	.5	11	7	224	3.87	13	5	ND	2	16	1	2	2	91	.23	.021	3	26	.60	45	.09	2	2.53	.02	.03	1	1
NMA L2+50E 0+30N	1	32	17	97	.4	14	10	275	4.40	19	5	ND	1	13	1	2	2	92	.19	.026	3	26	.77	35	.09	3	3.09	.03	.02	1	53
NMA L2+50E 0+40S	1	31	8	56	.6	13	9	219	3.87	20	5	ND	1	13	1	2	2	77	.17	.037	3	23	.64	28	.09	3	2.90	.03	.04	1	71
NMA L2+50E 0+60S	1	18	6	47	.4	9	6	189	3.33	14	5	ND	1	19	1	2	2	80	.25	.028	3	19	.51	29	.07	2	2.13	.03	.03	1	136
NMA L2+50E 0+80S	1	28	6	53	.2	17	8	202	3.55	21	5	ND	1	15	1	2	2	72	.22	.032	3	33	.58	27	.10	2	2.71	.03	.03	1	18
NMA L2+50E 1+00S	1	21	5	47	.2	11	7	184	3.22	14	5	ND	1	15	1	2	2	72	.25	.024	3	23	.59	30	.09	2	2.52	.03	.02	1	5
NMA L2+50E 1+20S	1	34	6	66	.2	17	12	271	4.08	22	5	ND	1	14	1	2	2	83	.20	.030	3	31	.83	41	.13	2	3.20	.03	.03	1	4
NMA L2+50E 1+40S	1	30	7	57	.4	14	10	241	3.69	33	5	ND	1	13	1	2	2	70	.20	.031	3	26	.72	40	.11	3	3.17	.03	.03	1	69
NMA L2+50E 1+60S	1	22	8	54	.1	11	7	207	3.38	11	5	ND	1	16	1	2	2	71	.21	.031	3	27	.54	34	.09	2	2.67	.03	.03	3	1
NMA L2+50E 1+80S	1	24	5	59	.2	11	7	220	3.19	5	5	ND	1	14	1	2	2	64	.20	.042	4	20	.61	29	.09	3	2.96	.03	.04	1	3
NMA L2+50E 2+00S	1	29	2	61	.1	13	10	217	3.37	3	5	ND	1	14	1	2	2	70	.19	.032	3	25	.74	33	.11	3	3.36	.03	.04	1	2
NMA L2+75E 1+00N	2	30	23	178	.1	14	12	719	4.34	21	5	ND	1	13	1	2	2	67	.52	.034	3	23	.64	38	.01	2	3.11	.03	.05	1	15
NMA L2+75E 0+90N	2	75	18	115	.4	17	19	469	5.65	29	5	ND	1	12	1	2	2	79	.14	.036	3	22	.83	40	.05	3	3.41	.03	.02	1	31
NMA L2+75E 0+80N	1	32	9	76	.3	12	9	239	3.95	12	5	ND	2	13	1	2	2	75	.18	.031	3	23	.59	32	.07	3	3.02	.03	.05	1	1
STD C/AU-S	18	57	39	133	7.1	69	27	1029	3.97	42	22	7	39	50	18	17	22	57	.47	.089	37	64	.88	177	.08	37	1.79	.08	.14	13	47

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NMA L2+75E 0+70N	1	26	19	65	.2	11	8	241	3.94	14	5	ND	1	15	1	4	2	83	.22	.023	3	22	.65	27	.07	2	2.77	.03	.03	1	1
STD C/AU-S	19	58	40	126	7.0	66	27	1016	3.87	42	20	7	39	49	18	17	19	56	.47	.083	37	58	.89	172	.07	36	1.83	.08	.16	14	47
NMA L2+75E 0+60N	1	26	9	60	.1	10	8	336	3.72	10	5	ND	1	21	1	2	2	82	.26	.029	3	22	.58	37	.07	2	2.60	.03	.03	1	2
NMA L2+75E 0+60S	1	27	9	56	.2	11	9	223	3.78	27	5	ND	2	17	1	2	2	75	.20	.030	4	22	.57	33	.08	2	2.68	.02	.04	1	45
NMA L2+75E 0+80S	1	24	9	40	.1	9	7	175	3.36	19	5	ND	1	15	1	2	2	75	.23	.021	3	20	.51	32	.09	2	2.33	.03	.02	1	25
NMA L2+75E 1+00S	1	25	3	56	.1	10	7	235	3.38	15	5	ND	1	15	1	2	2	74	.20	.029	3	23	.61	31	.08	3	2.52	.03	.02	1	395
NMA L2+75E 1+20S	2	25	6	73	.1	10	9	1115	3.65	12	5	ND	1	15	1	2	2	69	.20	.062	4	20	.63	42	.08	2	2.66	.03	.03	2	11
NMA L2+75E 1+40S	1	22	6	63	.1	11	5	178	2.52	11	5	ND	1	14	1	2	2	53	.22	.042	3	23	.43	40	.05	2	2.23	.03	.03	1	18
NMA L2+75E 1+60S	1	22	8	56	.3	9	6	310	3.07	23	5	ND	2	14	1	2	2	66	.22	.042	4	16	.46	41	.06	3	2.23	.03	.04	1	10
NMA L2+75E 1+80S	2	28	8	56	.1	14	8	305	3.34	28	5	ND	1	14	1	2	2	57	.22	.045	4	25	.64	46	.08	4	2.71	.03	.03	1	6
NMA L2+75E 2+00S	1	25	5	57	.1	12	8	243	3.46	5	5	ND	1	14	1	2	2	67	.21	.034	3	23	.71	40	.09	3	2.91	.03	.02	1	4
NMA L4+25E 1+00N	1	48	22	69	.1	11	7	252	5.15	21	5	ND	2	12	1	2	2	85	.12	.034	3	25	.56	37	.05	2	2.83	.02	.04	1	11
NMA L4+25E 0+80N	2	69	45	82	.3	11	8	268	5.89	24	5	ND	1	13	1	2	2	87	.10	.045	3	23	.61	51	.06	2	3.41	.02	.05	1	5
NMA L4+25E 0+60N	1	62	45	89	.6	12	9	327	5.02	19	5	ND	1	14	1	2	2	74	.13	.039	3	21	.62	46	.06	2	3.34	.03	.06	1	3
NMA L4+25E 0+40N	2	69	13	73	.1	18	12	402	5.47	19	5	ND	1	17	1	2	2	90	.17	.031	3	32	.98	46	.10	2	3.55	.03	.03	1	4
NMA L4+25E 0+20N	1	39	8	79	.5	11	10	260	4.13	18	5	ND	2	14	1	2	2	78	.18	.027	3	24	.62	34	.06	2	3.09	.03	.05	1	1
NMA L4+25E 0+20S	1	30	4	86	.6	15	11	266	3.39	2	5	ND	1	14	1	2	2	67	.19	.027	3	24	.76	38	.07	2	3.20	.03	.04	1	1
NMA L4+25E 0+40S	1	45	4	67	.1	14	13	275	4.26	17	5	ND	1	13	1	2	2	76	.16	.030	3	27	.70	45	.08	2	3.54	.03	.03	1	19
NMA L4+25E 0+60S	1	34	5	61	.1	15	12	275	3.91	5	5	ND	1	14	1	2	2	82	.18	.020	3	26	.88	35	.09	2	3.32	.03	.02	1	4
NMA L4+25E 0+80S	1	43	5	66	.1	18	16	284	4.23	11	5	ND	1	13	1	2	2	90	.19	.023	2	36	1.06	40	.14	2	3.99	.03	.02	2	4
NMA L4+25E 1+00S	1	26	3	60	.1	13	10	232	3.32	5	5	ND	2	15	1	2	2	71	.19	.021	3	24	.71	36	.10	2	3.10	.03	.02	1	3
NMA L4+25E 1+20S	1	35	7	63	.2	17	13	297	4.36	10	5	ND	1	15	1	2	2	96	.24	.022	2	33	1.02	49	.11	2	3.60	.03	.03	2	2
NMA L4+25E 1+40S	1	31	5	65	.1	15	10	269	4.41	12	5	ND	2	14	1	3	2	94	.19	.026	3	29	.92	44	.11	2	3.50	.03	.02	1	1
NMA L4+25E 1+60S	1	23	6	67	.4	12	8	254	3.56	5	5	ND	1	12	1	2	2	79	.17	.024	3	22	.74	34	.09	2	3.14	.03	.03	1	1
NMA L4+25E 1+80S	1	18	7	47	.1	9	6	202	2.80	4	5	ND	1	14	1	2	2	68	.19	.016	3	21	.59	53	.09	2	2.38	.02	.03	1	1
NMA L4+25E 2+00S	1	23	5	63	.3	11	9	213	3.08	2	5	ND	1	13	1	2	2	67	.18	.020	3	24	.73	37	.10	4	3.11	.03	.03	1	2
NMA L4+50E 1+00N	1	77	20	80	.5	10	7	285	6.32	28	5	ND	1	9	1	2	2	86	.08	.064	2	21	.60	31	.03	2	2.96	.02	.05	2	3
NMA L4+50E 0+80N	2	76	28	85	.1	14	11	315	5.66	28	5	ND	1	12	1	2	2	87	.10	.041	2	24	.83	38	.06	2	3.48	.03	.03	1	1
NMA L4+50E 0+60N	1	33	108	77	.4	6	4	172	3.83	18	5	ND	1	10	1	2	2	58	.11	.044	2	13	.34	35	.02	2	2.20	.02	.05	1	6
NMA L4+50E 0+60S	1	34	8	68	.3	12	10	293	3.93	22	5	ND	1	13	1	2	2	75	.18	.029	3	23	.73	36	.06	2	3.01	.02	.03	1	62
NMA L4+50E 0+80S	1	29	5	70	.1	11	10	280	3.63	24	5	ND	1	15	1	2	2	70	.23	.029	2	22	.66	43	.05	2	3.02	.03	.04	1	61
NMA L4+50E 1+00S	1	28	8	57	.9	10	9	242	3.37	11	5	ND	1	14	1	2	2	66	.19	.027	3	19	.61	42	.06	2	2.84	.03	.04	1	8
NMA L4+50E 1+20S	1	34	4	61	.1	15	11	260	4.00	10	5	ND	1	12	1	2	2	81	.17	.028	3	25	.94	43	.10	2	3.69	.03	.03	1	11
NMA L4+50E 1+40S	1	26	6	69	.5	11	9	209	3.26	12	5	ND	1	11	1	3	2	65	.14	.034	3	20	.63	31	.05	2	3.05	.02	.03	1	1
NMA L4+50E 1+60S	1	33	9	61	.3	15	11	272	3.93	11	5	ND	1	13	1	2	2	80	.17	.024	3	24	.93	51	.09	2	3.71	.03	.03	1	2
NMA L4+50E 1+80S	2	25	7	62	.2	11	9	224	3.23	5	5	ND	1	12	1	2	2	64	.17	.037	3	22	.66	33	.07	2	3.08	.03	.03	1	1
NMA L4+50E 2+00S	1	28	6	60	.1	11	10	226	3.50	8	5	ND	1	12	1	2	2	69	.17	.042	3	21	.65	35	.07	2	3.64	.03	.03	1	1

MINCORD EXPLORATION PROJECT- MAC FILE # 87-5150

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM	PPB
NMA L4+50E 2+20S	1	23	5	74	.1	12	10	383	3.61	7	5	ND	1	14	1	2	2	70	.23	.037	3	25	.80	48	.07	2	3.00	.03	.04	1	8
NMA L4+50E 2+40S	1	35	6	81	.2	14	11	370	3.88	4	5	ND	2	11	1	2	2	70	.16	.056	3	29	.99	39	.06	2	3.92	.03	.04	1	1
NMA L4+75E 1+00N	2	55	16	92	.3	12	9	326	5.30	48	5	ND	2	11	1	2	2	80	.14	.050	2	24	.64	34	.02	2	2.92	.02	.08	1	1
NMA L4+75E 0+80N	2	78	13	104	.1	17	11	422	7.25	40	5	ND	1	9	1	2	2	79	.08	.073	2	25	.65	44	.02	2	3.29	.02	.06	1	1
NMA L4+75E 0+60N	2	39	40	94	.4	9	7	261	4.64	17	5	ND	2	11	1	2	2	70	.12	.047	3	21	.48	42	.04	2	2.94	.02	.06	2	1
NMA L4+75E 0+40N	1	32	11	63	.4	10	9	223	4.00	15	6	ND	3	12	1	2	2	73	.14	.029	3	19	.56	37	.05	3	2.88	.02	.06	1	1
NMA L4+75E 0+20N	1	32	11	78	.6	11	11	208	3.63	10	5	ND	2	13	1	2	2	63	.15	.036	3	22	.46	42	.05	2	3.58	.02	.08	1	1
NMA L4+75E 0+20S	1	43	6	73	.7	15	11	286	4.27	10	5	ND	1	12	1	2	2	80	.17	.031	3	30	.80	47	.09	2	2.99	.02	.05	1	1
NMA L4+75E 0+40S	1	34	4	67	.2	15	13	278	4.06	3	5	ND	2	14	1	2	2	88	.19	.021	2	31	.93	43	.12	2	3.49	.03	.03	1	1
NMA L4+75E 0+60S	1	28	6	63	.6	11	9	224	3.71	8	5	ND	1	14	1	2	2	76	.21	.024	3	23	.60	33	.08	2	2.57	.02	.03	1	1
NMA L4+75E 0+80S	1	48	6	68	.1	16	14	336	4.69	18	5	ND	2	15	1	2	2	92	.21	.029	2	33	1.08	48	.08	2	3.63	.03	.04	1	1
NMA L4+75E 1+00S	2	34	9	62	.4	10	9	289	3.81	23	5	ND	2	13	1	2	3	66	.18	.033	3	17	.65	48	.03	2	2.74	.02	.05	1	1
NMA L4+75E 1+20S	1	34	7	71	.3	10	10	255	3.59	15	5	ND	2	13	1	2	2	62	.16	.032	3	19	.66	47	.03	2	2.90	.02	.05	1	1
NMA L4+75E 1+40S	1	21	7	48	.3	9	6	201	3.17	18	5	ND	1	13	1	2	2	64	.20	.042	3	19	.50	42	.04	2	2.14	.02	.03	2	1
NMA L4+75E 1+60S	1	27	8	62	.1	11	10	285	3.85	13	5	ND	2	13	1	2	2	76	.21	.042	3	22	.75	51	.05	2	2.84	.02	.05	1	7
NMA L4+75E 1+80S	1	30	3	72	.1	13	11	279	4.02	8	5	ND	1	15	1	2	2	80	.21	.036	2	24	.83	51	.08	3	3.37	.03	.02	1	1
NMA L4+75E 2+00S	1	21	6	61	.2	11	8	295	3.41	7	5	ND	2	13	1	2	2	71	.22	.028	3	22	.65	46	.06	2	2.67	.02	.03	1	4
NMA L5+00E 1+00N	3	63	20	83	.1	8	6	279	5.36	25	5	ND	1	8	1	2	2	68	.07	.064	3	18	.48	41	.01	2	3.00	.02	.06	1	1
NMA L5+00E 0+80N	1	39	18	73	.2	6	5	275	4.98	11	5	ND	2	11	1	2	2	77	.10	.051	3	17	.48	36	.03	2	2.60	.02	.05	1	1
NMA L5+00E 0+60N	1	51	17	88	.1	14	10	297	4.72	18	5	ND	2	10	1	2	2	76	.11	.041	3	25	.64	43	.05	2	3.29	.02	.05	1	3
NMA L5+00E 0+60S	1	53	10	55	.1	12	10	252	4.96	33	5	ND	1	9	1	2	2	69	.11	.040	3	22	.56	52	.06	2	2.90	.02	.05	1	63
NMA L5+00E 0+80S	1	34	8	62	.1	14	12	261	4.10	14	5	ND	2	10	1	2	2	78	.14	.027	2	29	.81	38	.08	2	3.27	.02	.04	1	6
NMA L5+00E 1+00S	1	33	9	59	.1	10	7	233	4.36	18	5	ND	2	11	1	2	2	68	.13	.045	3	22	.54	52	.06	3	2.91	.02	.04	1	1
NMA L5+00E 1+20S	1	40	9	52	.1	9	7	225	4.44	19	5	ND	1	12	1	2	2	74	.12	.042	3	17	.53	48	.07	2	3.00	.02	.03	2	1
NMA L5+00E 1+40S	1	24	7	60	.1	10	8	228	3.92	19	5	ND	1	12	1	2	2	75	.16	.037	3	19	.61	38	.05	2	2.55	.02	.04	1	1
NMA L5+00E 1+60S	1	29	12	60	.1	11	9	242	4.19	35	5	ND	1	11	1	2	2	71	.15	.026	3	21	.59	53	.02	2	2.77	.02	.04	1	3
NMA L5+00E 1+80S	1	21	7	62	.1	9	8	283	3.35	23	5	ND	2	12	1	2	2	67	.17	.024	3	20	.54	44	.02	2	2.31	.02	.06	1	1
NMA L5+00E 2+00S	1	28	8	73	.3	14	10	330	3.75	7	5	ND	2	14	1	2	2	73	.25	.043	2	26	.86	37	.05	2	3.07	.03	.04	1	1
NMA L2+00W 1+00N	1	43	7	70	.1	13	11	396	4.28	21	5	ND	2	15	1	2	2	79	.26	.038	4	25	.85	42	.07	2	3.00	.03	.05	1	1
NMA L2+00W 0+80N	1	58	6	66	.1	16	14	563	4.20	15	5	ND	2	22	1	2	2	81	.40	.036	4	32	1.10	39	.12	2	3.21	.03	.04	1	5
NMA L2+00W 0+60N	1	66	10	71	.1	16	14	652	4.18	19	5	ND	3	32	1	2	2	78	.52	.041	5	29	1.10	45	.13	2	3.13	.04	.04	1	3
NMA L2+00W 0+40N	2	26	7	49	.1	10	6	182	3.20	9	5	ND	2	11	1	2	2	76	.17	.021	3	23	.59	24	.12	2	2.02	.02	.03	1	1
NMA L2+00W 0+20N	1	21	7	46	.1	9	6	151	2.81	4	5	ND	1	11	1	2	2	68	.16	.021	3	24	.53	24	.09	2	2.19	.02	.04	1	1
NMA L2+00W 0+00	1	35	5	58	.1	12	9	236	3.35	8	5	ND	2	10	1	2	2	70	.17	.034	3	25	.64	32	.10	2	2.66	.02	.02	1	1
NMA L2+00W 0+20S	1	24	7	52	.1	9	6	196	2.94	12	5	ND	1	13	1	2	2	66	.17	.017	3	19	.53	29	.09	2	1.93	.02	.03	1	4
NMA L2+00W 0+40S	2	31	5	51	.1	9	7	190	2.85	11	5	ND	1	12	1	2	2	62	.20	.021	2	16	.49	32	.07	2	2.55	.02	.01	1	1
STD C/AU-S	18	57	40	133	7.1	67	27	1029	3.95	37	19	7	38	50	18	18	18	56	.47	.087	37	58	.87	177	.08	34	1.79	.08	.16	12	50

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NMA L2+00W 0+60S	2	36	8	70	.1	11	9	333	3.46	14	5	ND	1	14	1	2	2	63	.22	.038	3	22	.63	50	.07	4	2.61	.03	.04	1	1
NMA L2+00W 0+80S	2	25	6	50	.1	9	6	175	3.32	8	5	ND	2	12	1	2	2	74	.18	.021	3	20	.51	28	.11	3	2.51	.02	.01	1	12
NMA L2+00W 1+00S	2	39	10	63	.1	12	9	273	3.60	12	5	ND	1	14	1	2	2	71	.22	.031	3	24	.72	38	.09	3	2.70	.03	.02	1	1
NMA L2+00W 1+20S	1	33	13	49	.1	10	8	201	2.98	8	5	ND	1	12	1	2	2	61	.19	.026	3	20	.59	34	.09	3	2.62	.03	.03	1	1
NMA L2+00W 1+40S	2	38	10	64	.1	12	9	257	3.57	16	5	ND	1	12	1	2	2	69	.21	.032	3	24	.69	38	.09	3	3.08	.03	.02	1	1
NMA L2+00W 1+60S	2	27	10	62	.1	10	8	257	3.12	9	5	ND	1	16	1	2	2	66	.31	.029	3	22	.63	34	.07	2	2.65	.03	.03	1	1
NMA L2+00W 1+80S	1	37	8	66	.1	12	10	285	3.54	35	5	ND	1	13	1	2	2	68	.28	.034	4	24	.73	32	.08	3	3.82	.03	.03	2	1
NMA L2+00W 2+00S	1	48	6	64	.1	14	12	291	3.87	15	5	ND	2	12	1	2	2	72	.23	.027	3	27	.90	39	.11	4	3.92	.03	.02	1	1
NMA L1+75W 1+00N	2	51	11	66	.1	16	14	597	4.26	12	5	ND	1	18	1	2	2	82	.40	.037	3	34	1.13	38	.13	3	2.97	.04	.03	1	1
NMA L1+75W 0+80N	1	32	10	58	.1	12	9	246	3.68	5	5	ND	1	15	1	2	2	85	.26	.024	4	25	.74	33	.12	4	2.57	.03	.01	1	1
NMA L1+75W 0+60N	2	36	10	66	.1	11	10	236	3.38	25	5	ND	1	13	1	2	2	66	.23	.023	2	25	.76	36	.07	3	3.07	.03	.03	1	1
NMA L1+75W 0+40N	2	35	12	82	.1	12	9	278	3.61	18	5	ND	1	15	1	2	2	67	.37	.041	3	24	.73	38	.06	4	2.84	.03	.03	1	1
NMA L1+75W 0+20N	1	42	9	118	.1	12	11	349	3.44	49	5	ND	1	23	1	2	2	63	.60	.045	3	27	.78	39	.06	3	2.95	.04	.04	1	3
NMA L1+75W 0+00	1	19	9	44	.1	6	4	165	2.47	6	5	ND	1	12	1	2	2	59	.18	.024	3	15	.39	27	.07	3	1.68	.02	.03	2	1
NMA L1+75W 0+20S	2	21	11	49	.1	7	5	206	3.06	7	5	ND	1	13	1	2	2	77	.19	.030	4	17	.45	27	.10	4	2.04	.02	.03	2	1
NMA L1+75W 0+40S	1	34	6	45	.1	10	8	229	3.18	9	5	ND	1	13	1	2	2	67	.21	.018	3	23	.67	37	.11	2	2.47	.02	.01	2	1
NMA L1+75W 0+80S	1	25	8	51	.1	8	5	166	2.91	5	5	ND	1	12	1	2	2	65	.18	.025	3	16	.48	24	.08	2	2.47	.02	.02	3	1
NMA L1+75W 1+00S	1	31	10	53	.1	9	8	196	3.44	8	5	ND	1	13	1	2	2	75	.19	.024	3	19	.59	31	.10	4	2.95	.02	.02	2	1
NMA L1+75W 1+20S	1	35	7	58	.1	12	10	275	3.66	11	5	ND	1	13	1	2	2	75	.21	.022	3	26	.81	31	.11	2	2.72	.03	.02	1	1
NMA L1+75W 1+40S	1	30	11	59	.1	11	9	248	3.34	7	5	ND	1	15	1	2	2	70	.23	.022	3	21	.70	41	.10	3	2.52	.03	.02	1	1
NMA L1+75W 1+60S	1	33	11	65	.1	11	9	288	3.62	11	5	ND	1	14	1	2	2	69	.23	.033	2	23	.72	39	.07	5	2.78	.03	.02	2	1
NMA L1+75W 1+80S	2	31	11	64	.1	11	8	238	3.40	11	5	ND	1	16	1	2	2	70	.26	.031	3	22	.64	36	.08	4	2.44	.03	.03	1	1
NMA L1+75W 2+00S	2	36	6	69	.1	13	9	264	3.62	11	5	ND	1	13	1	2	2	71	.19	.041	3	23	.75	36	.10	3	2.66	.03	.04	1	1
NMA L1+50W 1+00N	2	38	7	59	.1	14	13	262	3.97	13	5	ND	1	12	1	2	2	72	.20	.032	3	26	.80	42	.10	2	3.65	.03	.02	4	11
NMA L1+50W 1+20S	1	25	24	80	1.4	10	8	216	3.52	10	5	ND	1	13	1	2	2	72	.19	.024	3	20	.66	32	.10	2	2.38	.02	.02	1	1
NMA L1+50W 1+40S	1	35	9	59	.1	13	9	246	3.58	12	5	ND	1	12	1	2	2	69	.22	.035	3	24	.75	34	.11	4	2.76	.03	.03	1	4
NMA L1+50W 1+60S	2	32	11	57	.3	10	7	226	3.50	11	5	ND	2	12	1	5	2	72	.21	.033	3	20	.62	28	.10	4	2.56	.03	.04	2	1
NMA L1+50W 1+80S	1	24	9	53	.1	9	7	202	3.34	13	5	ND	1	12	1	2	2	70	.20	.023	3	20	.59	27	.10	3	2.24	.03	.02	1	1
NMA L1+50W 2+00S	2	28	7	51	.1	12	8	225	3.58	12	5	ND	1	14	1	2	2	77	.21	.022	3	22	.73	29	.11	2	2.30	.03	.02	2	1
NMA L1+25W 1+00N	2	18	11	53	.1	6	5	197	2.65	10	5	ND	1	16	1	2	2	67	.26	.025	3	15	.42	40	.09	3	1.62	.03	.04	1	1
NMA L1+25W 0+80N	2	22	16	62	.1	8	6	198	3.07	11	5	ND	1	14	1	2	2	65	.23	.029	3	17	.55	42	.07	3	2.08	.03	.03	2	8
NMA L1+25W 0+60N	1	23	12	59	.3	9	7	226	3.61	15	5	ND	1	16	1	2	2	75	.28	.024	3	20	.66	34	.07	3	2.29	.03	.04	1	1
NMA L1+25W 0+40N	2	30	11	58	.1	11	9	256	3.53	10	5	ND	2	12	1	2	2	76	.20	.019	3	22	.71	36	.11	2	2.72	.03	.03	2	1
NMA L1+25W 0+20N	2	31	10	72	.2	12	10	284	3.70	10	5	ND	1	12	1	2	2	72	.21	.031	3	21	.77	35	.11	4	2.81	.03	.03	1	1
STD C/AU-S	18	57	40	130	6.9	67	27	1024	3.91	38	20	6	38	48	18	18	21	54	.46	.084	37	56	.90	178	.08	36	1.85	.08	.13	13	47
NMA L1+25W 0+00	2	30	11	58	.1	11	8	246	3.87	11	5	ND	1	15	1	2	2	81	.23	.022	3	22	.68	37	.11	3	2.34	.03	.01	1	1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	M6 %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
L15+00N 3+50W	2	62	6	90	.1	14	8	383	4.04	43	5	ND	1	10	1	2	2	55	.16	.043	3	25	.81	43	.06	2	2.37	.02	.03	1	1
L15+00N 3+25W	1	18	9	131	.1	10	6	221	2.54	8	5	ND	1	9	1	2	2	46	.14	.064	3	22	.48	27	.05	2	1.91	.02	.02	3	1
L15+00N 3+00W	2	29	7	126	.2	15	7	310	4.28	17	5	ND	1	9	1	2	2	64	.16	.109	4	31	.72	41	.04	2	2.55	.02	.04	2	3
L15+00N 2+75W	2	32	7	105	.1	21	10	400	4.06	17	5	ND	1	10	1	2	2	66	.19	.095	3	40	.68	35	.08	3	2.49	.02	.05	2	1
L15+00N 2+50W	2	42	10	81	.1	20	8	266	3.54	17	5	ND	2	10	1	3	2	64	.17	.079	4	37	.71	32	.07	2	2.48	.03	.03	1	1
L15+00N 2+25W	4	103	10	95	.1	26	12	360	5.21	38	5	ND	1	9	1	2	2	86	.19	.081	3	41	.95	49	.07	2	3.26	.02	.03	3	1
L15+00N 2+00W	7	226	34	75	.1	41	16	365	5.71	68	5	ND	1	13	1	2	2	85	.22	.051	3	47	1.09	54	.08	2	3.88	.03	.02	2	2
L15+00N 1+75W	3	187	11	74	.2	27	11	384	4.82	52	5	ND	2	9	1	2	2	78	.22	.076	2	42	1.05	29	.07	3	3.06	.03	.02	2	1
L15+00N 1+50W	3	114	8	87	.2	26	10	340	4.20	33	5	ND	2	10	1	2	2	76	.19	.054	4	40	.82	33	.07	2	2.48	.02	.03	1	1
L15+00N 1+25W	4	199	15	87	.1	34	14	486	5.55	82	5	ND	1	11	1	2	2	93	.28	.068	3	47	1.13	51	.07	2	3.32	.03	.02	3	1
L15+00N 1+00W	5	291	10	84	.3	27	15	430	5.04	65	5	ND	1	12	1	2	2	83	.31	.058	3	33	1.02	43	.07	3	3.08	.03	.05	1	1
L15+00N 0+75W	3	67	10	97	.2	18	13	618	4.12	30	5	ND	1	13	1	2	2	75	.28	.057	3	31	.65	45	.08	2	2.07	.03	.05	1	4
L15+00N 0+50W	3	79	9	95	.2	26	11	357	4.29	29	5	ND	2	13	1	2	3	82	.30	.054	3	42	.80	52	.08	5	2.51	.03	.05	1	3
L15+00N 0+25W	3	222	9	72	.1	35	11	320	4.24	49	5	ND	1	10	1	2	2	73	.22	.057	3	56	.96	40	.07	5	2.93	.03	.03	2	1
L15+00N 0+00W	6	435	6	68	.5	31	16	510	4.90	75	5	ND	1	17	1	2	2	74	.41	.064	4	52	1.10	47	.05	5	2.50	.03	.04	1	14
L15+00N 0+25E	3	183	5	66	.1	52	15	487	4.06	37	5	ND	1	14	1	2	2	65	.32	.040	4	62	1.22	60	.09	3	2.92	.03	.03	3	2
L15+00N 0+50E	6	350	17	123	.5	53	13	915	4.35	77	5	ND	2	24	1	3	2	72	.73	.034	6	90	1.01	112	.06	4	3.90	.04	.05	1	1
L15+00N 0+75E	4	162	5	74	.1	40	9	314	2.81	17	5	ND	1	16	1	2	2	50	.46	.014	5	53	1.05	64	.07	2	2.34	.03	.03	1	1
L15+00N 1+00E	4	36	7	72	.1	21	8	281	3.94	12	5	ND	2	15	1	2	2	67	.37	.026	5	33	.77	73	.05	2	2.24	.03	.05	1	1
L15+00N 1+25E	4	179	9	88	.4	43	12	333	4.64	40	5	ND	2	11	1	2	2	79	.27	.035	4	70	1.19	59	.07	3	2.93	.03	.05	1	3
L15+00N 1+50E	3	118	4	72	.4	87	17	285	4.28	30	5	ND	1	11	1	2	2	93	.51	.027	3	136	1.60	39	.10	3	2.90	.04	.05	1	2
L15+00N 1+75E	3	200	9	102	.1	35	13	339	3.81	28	5	ND	1	11	1	2	2	74	.28	.043	4	59	.79	59	.08	3	2.50	.03	.03	1	11
L15+00N 2+00E	3	119	5	88	.1	67	16	354	4.28	30	5	ND	1	12	1	2	2	91	.51	.049	3	107	1.43	62	.10	3	2.79	.03	.02	2	3
L15+00N 2+50E	3	137	10	166	.2	38	16	655	4.35	79	5	ND	1	14	1	2	2	73	.32	.037	4	50	.99	77	.07	5	2.75	.03	.07	1	4
L14+00N 4+50W	2	48	6	71	.1	114	19	584	3.93	7	5	ND	1	19	1	2	2	82	.88	.024	3	190	2.64	41	.12	6	3.01	.04	.02	1	1
L14+00N 4+00W	2	19	9	81	.2	14	5	191	3.63	17	5	ND	1	10	1	2	2	64	.15	.049	4	30	.55	28	.04	4	2.04	.02	.02	2	1
L14+00N 3+50W	2	25	7	161	.1	17	8	269	3.19	9	5	ND	1	9	1	2	2	48	.15	.089	3	30	.57	34	.06	2	2.82	.03	.03	1	1
L14+00N 3+25W	1	34	4	121	.2	19	8	296	3.03	14	5	ND	2	8	1	2	2	48	.13	.064	3	33	.68	37	.06	5	2.54	.02	.04	1	1
L14+00N 3+00W	1	30	5	113	.2	15	7	336	3.70	22	5	ND	1	12	1	2	2	58	.17	.070	4	29	.76	45	.06	5	2.54	.02	.03	1	1
L14+00N 2+75W	2	35	9	95	.1	17	7	284	3.79	18	5	ND	1	10	1	2	2	67	.13	.070	4	31	.72	34	.06	3	2.40	.02	.03	1	1
L14+00N 2+50W	1	21	6	94	.1	10	5	229	3.26	14	5	ND	1	9	1	2	2	62	.12	.044	4	22	.51	33	.06	4	2.10	.02	.02	1	18
L14+00N 2+25W	2	62	8	116	.1	24	10	350	4.30	30	5	ND	1	11	1	3	2	74	.19	.082	4	36	.86	34	.07	3	2.52	.03	.02	1	1
L14+00N 2+00W	3	60	8	97	.1	26	10	319	4.53	33	5	ND	2	11	1	2	2	85	.20	.032	4	39	.89	49	.07	5	2.77	.03	.03	1	1
L14+00N 1+75W	4	53	3	91	.3	15	9	269	4.51	33	5	ND	1	11	1	2	2	87	.22	.050	2	26	.59	27	.07	2	2.01	.02	.03	2	2
L14+00N 1+50W	4	77	8	100	.2	17	10	387	4.71	44	5	ND	1	13	1	2	2	90	.29	.034	3	29	.72	41	.06	2	2.24	.03	.03	1	4
L14+00N 1+25W	4	98	9	89	.5	31	10	317	4.71	47	5	ND	2	10	1	3	2	86	.19	.041	4	53	.93	45	.08	5	2.82	.03	.03	1	1
STD C/AU-5	19	57	40	131	7.2	67	27	1030	3.95	40	20	7	37	50	17	17	19	57	.47	.085	38	57	.87	178	.08	38	1.79	.08	.16	13	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	PPB	
L14+00N 1+00W	3	181	9	83	.3	38	15	394	5.48	75	5	ND	2	13	1	2	2	96	.22	.041	4	55	1.20	62	.11	2	4.19	.03	.05	2	86
L14+00N 0+75W	3	129	7	92	.1	35	14	386	4.55	46	5	ND	1	14	1	2	2	81	.27	.036	4	48	.93	46	.09	6	3.22	.03	.05	1	16
L14+00N 0+50W	2	67	3	82	.3	19	7	297	3.39	27	6	ND	1	13	1	2	2	66	.26	.047	4	37	.60	37	.09	5	2.22	.03	.03	1	5
L14+00N 0+25W	7	209	12	87	.1	22	9	242	5.37	85	5	ND	1	15	1	2	2	91	.34	.129	4	41	.74	48	.07	3	2.52	.03	.06	1	22
L14+00N 0+25E	6	335	7	73	.9	25	12	501	4.95	69	5	ND	1	17	1	2	2	79	.41	.070	4	44	1.07	42	.06	3	2.83	.03	.04	1	40
L14+00N 0+50E	3	147	9	93	.3	38	12	330	4.40	46	5	ND	1	11	1	2	2	74	.21	.065	4	61	1.03	49	.08	6	3.50	.03	.04	1	1
L14+00N 0+75E	3	309	3	111	.2	45	12	314	4.02	51	5	ND	1	10	1	2	2	61	.21	.071	4	59	1.03	47	.07	2	3.59	.03	.05	1	11
L14+00N 1+00E	3	286	5	112	.5	28	11	398	4.19	45	5	ND	1	12	1	2	2	70	.22	.054	3	42	.85	35	.09	2	3.07	.02	.04	1	7
L14+00N 1+25E	4	262	7	164	.2	41	13	355	4.42	82	5	ND	1	11	1	2	2	71	.22	.045	4	58	1.08	51	.07	6	3.55	.03	.04	1	27
L14+00N 1+50E	2	38	7	102	.2	18	7	213	3.40	20	5	ND	1	11	1	2	2	67	.24	.053	3	41	.54	40	.07	2	2.26	.03	.04	1	1
L14+00N 1+75E	3	99	9	86	.1	33	10	285	5.03	77	5	ND	1	13	1	2	2	95	.28	.031	4	54	.92	50	.09	3	2.74	.03	.06	2	4
L14+00N 2+00E	6	87	4	97	.3	21	9	247	3.59	88	5	ND	1	17	1	2	2	83	.54	.023	5	44	.75	52	.07	5	2.12	.03	.04	1	5
NM L13 3+75W	1	30	7	78	.1	19	8	469	3.11	12	5	ND	1	11	1	2	2	54	.19	.060	4	37	.68	33	.07	6	2.19	.03	.04	1	1
NM L13 3+25W	1	18	8	78	.1	9	5	345	3.14	10	5	ND	1	12	1	2	2	55	.14	.047	4	21	.47	26	.06	2	1.78	.02	.03	1	1
NM L13 2+75W	1	26	5	114	.2	12	6	303	3.29	15	5	ND	1	13	1	2	2	59	.21	.044	5	25	.57	33	.05	5	1.97	.02	.04	1	1
NM L13 2+50W	1	39	6	104	.2	18	8	421	3.53	20	5	ND	1	15	1	2	2	58	.28	.064	4	32	.73	38	.06	2	2.58	.02	.05	1	5
NM L13 2+25W	2	60	8	123	.1	22	12	640	3.85	35	5	ND	2	15	1	2	2	55	.27	.063	3	34	.92	70	.07	2	2.87	.03	.05	1	1
NM L13 2+00W	1	16	7	115	.2	10	5	636	2.78	8	5	ND	1	17	1	2	2	56	.30	.038	4	20	.55	44	.05	2	1.81	.02	.04	1	1
NM L13 1+75W	1	17	5	78	.2	15	6	240	2.99	10	5	ND	1	10	1	2	2	62	.23	.023	3	31	.55	34	.05	2	2.13	.03	.06	1	43
NM L13 1+50W	3	63	6	95	.2	17	9	362	4.70	35	5	ND	1	15	1	2	2	87	.32	.037	3	35	.62	36	.08	2	2.62	.03	.03	1	11
NM L13 1+25W	3	83	9	84	.3	20	9	622	4.58	44	5	ND	1	12	1	2	2	79	.22	.065	4	35	.79	38	.07	2	2.57	.03	.05	1	4
NM L13 1+00W	2	44	10	120	.4	18	8	291	3.93	24	5	ND	1	13	1	2	2	74	.24	.049	4	35	.63	38	.08	5	2.31	.02	.04	1	1
NM L13 0+75W	2	21	9	60	.2	9	5	383	2.64	9	5	ND	1	17	1	2	2	62	.29	.045	4	18	.42	51	.06	3	1.50	.02	.05	1	1
NM L13 0+50W	8	258	12	74	.4	21	9	440	4.71	80	5	ND	2	13	1	2	2	83	.27	.062	3	44	.88	45	.05	5	2.51	.03	.05	1	15
NM L13 0+25W	2	39	8	74	.4	10	5	272	3.03	19	5	ND	2	13	1	2	2	61	.19	.047	4	24	.39	27	.07	3	1.72	.02	.03	1	1
NM L13 0+00	8	511	9	77	.9	27	12	654	5.86	87	5	ND	1	14	1	2	2	93	.31	.081	3	46	1.10	57	.06	3	3.06	.03	.04	1	36
NM L13 0+25E	4	267	8	87	.4	27	14	882	4.36	53	5	ND	1	16	1	2	2	75	.44	.069	2	46	1.25	48	.07	3	2.24	.04	.07	1	5
NM L13 0+50E	2	270	8	123	.3	22	7	413	2.88	39	5	ND	1	24	1	2	2	55	.81	.059	4	45	.67	59	.03	3	2.36	.03	.07	2	4
NM L13 0+75E	4	400	9	77	.3	22	8	311	4.37	65	5	ND	1	11	1	2	2	75	.30	.054	3	43	.88	39	.05	3	2.38	.03	.06	2	5
NM L13 1+00E	2	61	8	91	.5	23	7	260	3.36	21	5	ND	2	13	1	2	2	58	.22	.056	5	42	.69	48	.08	3	2.41	.02	.05	1	68
NM L13 1+25E	3	92	8	90	.1	27	9	307	3.77	34	5	ND	2	14	1	2	2	67	.23	.039	4	48	.88	41	.08	6	2.64	.03	.05	1	4
NM L13 1+50E	2	184	9	80	.2	28	12	493	3.89	36	5	ND	2	11	1	2	2	70	.19	.024	3	42	1.14	56	.08	2	2.72	.03	.05	1	13
NM L13 1+75E	2	60	4	78	.1	19	8	285	3.35	19	5	ND	2	11	1	2	2	69	.19	.016	4	33	.70	38	.07	3	1.92	.02	.06	1	21
NM L13 2+00E	2	81	8	82	.1	25	10	452	3.58	30	5	ND	2	12	1	2	2	74	.23	.016	4	40	.86	40	.07	3	2.17	.03	.06	1	1
NM L13 2+25E	2	73	3	87	.3	27	10	357	3.41	35	5	ND	1	11	1	2	2	69	.23	.017	4	43	.88	49	.04	2	2.36	.02	.06	1	18
NM L13 2+50E	2	61	5	110	.2	34	11	732	3.77	19	5	ND	1	12	1	2	2	83	.30	.048	3	64	.89	43	.09	2	2.19	.03	.06	1	6
STD C/AU-S	18	57	40	132	7.2	67	27	1020	3.93	37	22	6	39	49	18	17	22	56	.47	.086	36	57	.87	176	.08	38	1.87	.08	.14	13	49

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	A PPB	
NM L13 2+75E	2	90	14	89	.4	45	14	548	4.28	127	5	ND	1	14	1	2	2	83	.33	.026	3	72	.93	48	.06	3	2.65	.03	.04	1	37
NM L13 3+00E	3	92	10	137	.1	27	18	2120	4.77	147	5	ND	1	17	1	2	3	67	.24	.060	8	38	.64	89	.04	2	2.54	.03	.06	1	900
NM L13 3+50E	2	147	14	101	.3	20	20	2758	4.88	17	5	ND	2	20	1	2	2	91	.38	.057	13	31	1.53	115	.08	2	3.31	.03	.10	1	11
NM L13 4+00E	2	121	13	102	.6	9	19	2128	5.22	26	5	ND	3	30	1	2	2	76	.51	.063	12	14	1.57	73	.10	4	3.35	.04	.12	1	3
NM L12 5+00W	1	29	13	86	.3	18	6	396	3.17	9	5	ND	1	18	1	2	2	58	.23	.042	6	25	.48	78	.04	3	1.67	.02	.05	1	1
NM L12 4+50W	1	25	6	88	.5	13	8	396	3.19	9	5	ND	1	17	1	2	2	56	.29	.065	4	28	.55	38	.05	2	2.26	.02	.05	1	32
NM L12 4+00W	1	21	5	70	.1	12	5	269	3.16	11	5	ND	1	11	1	2	2	55	.16	.048	4	29	.46	31	.05	2	1.99	.02	.04	1	4
NM L12 3+50W	1	21	5	82	.2	15	7	325	3.08	9	5	ND	1	12	1	2	2	54	.21	.062	4	32	.54	32	.07	6	2.01	.03	.04	1	1
NM L12 3+00W	1	27	10	118	.4	18	7	355	3.72	15	5	ND	1	12	1	2	2	61	.20	.093	5	36	.62	40	.06	2	2.48	.03	.03	1	1
NM L12 2+50W	2	36	10	129	.4	18	9	451	3.76	19	5	ND	1	11	1	2	2	61	.16	.064	4	29	.71	42	.07	2	2.66	.02	.05	1	2
NM L12 2+00W	1	23	9	89	.3	11	5	635	2.91	12	5	ND	1	14	1	2	3	55	.22	.053	5	23	.45	30	.07	3	1.78	.03	.03	1	1
STD C/AU-S	20	58	39	135	7.3	70	28	1075	4.01	38	20	8	40	50	18	17	22	57	.49	.086	38	57	.85	184	.08	36	1.86	.09	.13	13	51
NM L12 1+50W	2	41	10	124	.4	17	9	806	3.97	25	5	ND	2	19	1	2	2	79	.39	.053	5	28	.67	61	.08	2	2.25	.03	.09	1	5
NM L12 1+00W	2	46	10	94	.1	19	8	325	4.84	35	5	ND	1	11	1	2	2	85	.16	.084	4	44	.75	31	.08	2	2.60	.03	.03	1	6
NM L12 0+50W	6	632	10	67	.9	21	14	401	4.11	120	5	ND	2	20	1	2	4	79	.44	.083	6	319	.50	52	.06	5	2.14	.03	.04	1	12
NM L12 0+00W	9	759	9	87	.6	33	22	690	6.10	119	5	ND	1	24	1	2	2	84	.72	.070	4	51	1.22	55	.05	5	2.90	.04	.06	2	24
NM L12 0+00E	11	966	8	96	.9	41	20	488	6.49	121	5	ND	2	18	1	2	2	95	.44	.069	4	55	1.35	62	.07	3	3.67	.03	.05	2	36
NM L12 0+25E	4	229	15	76	.5	28	18	753	4.71	79	5	ND	2	22	1	2	2	89	.46	.065	6	69	1.08	49	.09	4	2.54	.04	.04	1	9
NM L12 0+50E	2	48	8	69	.5	20	8	312	3.46	32	5	ND	1	18	1	2	2	70	.35	.051	5	48	.85	53	.08	3	2.46	.03	.05	1	25
NM L12 0+75E	2	58	7	85	.5	25	9	354	3.43	25	5	ND	1	18	1	2	2	65	.37	.043	5	45	.93	53	.08	3	2.30	.03	.04	1	2
NM L12 1+00E	2	100	10	97	.3	27	9	365	3.31	18	5	ND	1	19	1	2	2	55	.38	.037	6	42	.86	70	.07	5	2.48	.03	.04	1	2
NM L12 1+25E	3	303	7	101	.4	47	13	413	4.37	50	5	ND	1	14	1	2	2	72	.26	.068	6	68	1.16	62	.09	3	3.25	.03	.04	1	11
NM L12 1+50E	3	57	11	112	.2	21	9	357	6.18	26	5	ND	1	11	1	2	2	88	.16	.138	5	49	.89	48	.07	2	3.02	.03	.08	1	1
NM L12 1+75E	3	1369	13	184	.9	43	12	734	4.20	42	5	ND	2	34	1	2	2	67	1.03	.064	18	48	.90	94	.06	5	3.87	.04	.08	2	25
NM L12 2+00E	2	1519	5	166	.1	37	11	925	3.96	31	5	ND	1	28	1	2	2	66	.72	.039	19	39	.82	85	.07	3	3.61	.04	.01	1	1
NM L12 2+25E	3	358	13	139	.5	19	10	693	3.40	24	5	ND	1	25	1	2	2	74	.68	.027	9	24	.79	48	.08	6	2.57	.04	.04	1	1
NM L12 2+50E	3	119	7	169	.5	37	10	511	3.32	37	5	ND	1	22	1	2	2	62	.47	.029	6	38	.81	58	.09	4	2.58	.04	.06	1	9
NM L12 2+75E	3	250	9	80	.5	43	13	409	4.40	52	5	ND	2	14	1	2	2	84	.28	.030	4	58	1.08	68	.09	8	3.08	.03	.05	1	5
NM L12 3+00E	4	398	11	124	.5	38	23	884	6.99	94	5	ND	2	14	1	2	2	72	.29	.080	4	38	1.01	57	.05	7	4.56	.03	.10	1	2
NM L12 3+25E	19	374	7	88	.3	26	12	353	8.11	77	5	ND	1	11	1	2	2	77	.17	.068	3	37	.87	45	.02	2	3.59	.03	.03	3	8
NM L12 3+50E	10	420	10	80	.5	70	19	408	11.60	83	5	ND	1	9	1	2	2	101	.13	.090	3	136	1.18	44	.04	2	4.34	.03	.05	2	25
NM L12 3+75E	23	474	10	59	.8	53	16	340	10.85	39	5	ND	2	9	1	4	2	100	.13	.074	4	104	1.08	38	.06	3	3.60	.02	.04	3	36
NM L12 4+00E	31	378	7	55	.2	66	15	524	9.57	35	5	ND	2	15	1	2	2	102	.16	.072	4	149	1.39	76	.02	2	3.32	.02	.05	1	122
NM L12 4+50E	2	59	9	132	.6	14	14	2611	3.82	8	5	ND	2	32	1	2	2	62	.45	.171	5	20	1.06	120	.08	4	2.91	.03	.16	1	6
NM L11N 5+50W	1	30	8	124	.4	15	8	278	3.37	9	5	ND	2	12	1	2	2	51	.15	.106	5	30	.55	38	.07	2	2.76	.02	.05	1	6
NM L11N 5+00W	1	16	4	47	.1	7	3	172	2.29	7	5	ND	2	10	1	2	2	43	.13	.042	4	17	.34	22	.02	3	1.48	.02	.04	1	2
NM L11N 4+50W	1	23	5	102	.3	24	7	221	3.08	11	5	ND	1	12	1	2	2	56	.13	.061	5	57	.69	37	.06	3	2.26	.03	.04	1	130

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NM L11N 4+00W	1	24	7	86	.1	14	5	178	4.01	15	5	ND	1	10	1	2	2	61	.15	.070	4	31	.51	31	.05	2	2.38	.02	.04	1	4
NM L11N 3+50W	1	50	8	87	.4	23	10	305	3.99	18	5	ND	1	7	1	2	2	60	.15	.055	3	37	.95	37	.02	2	2.92	.02	.04	1	9
NM L11N 3+00W	1	24	8	120	.3	13	7	296	3.41	16	5	ND	1	12	1	2	2	55	.16	.065	5	26	.53	43	.06	2	2.69	.02	.04	2	2
NM L11N 2+50W	1	15	10	158	.3	9	6	510	3.14	10	5	ND	2	13	1	2	2	52	.18	.053	5	22	.43	37	.06	2	2.05	.02	.04	1	1
NM L11N 2+00W	2	23	10	117	.3	15	9	417	3.38	12	5	ND	2	14	1	2	2	64	.27	.035	5	30	.58	35	.08	3	2.19	.03	.05	1	1
NM L11N 1+50W	1	53	8	103	.1	22	9	406	4.13	27	5	ND	1	11	1	2	2	69	.18	.060	5	37	.79	35	.08	3	2.86	.03	.03	2	6
NM L11N 1+25W	1	50	10	90	.1	23	8	288	4.24	29	5	ND	1	9	1	2	2	69	.16	.056	4	42	.84	36	.07	3	2.79	.03	.04	1	1
NM L11N 1+00W	3	104	10	86	.1	26	9	295	4.37	171	5	ND	1	11	1	2	2	74	.20	.059	5	51	.72	33	.08	3	2.55	.03	.03	1	9
NM L11N 0+75W	3	124	8	76	.2	15	7	252	4.28	41	5	ND	1	12	1	2	2	78	.23	.049	3	29	.62	27	.08	4	2.58	.03	.03	1	7
NM L11N 0+50W	2	118	12	90	.1	46	17	344	5.38	26	5	ND	2	14	1	2	2	102	.23	.061	4	67	1.03	55	.24	6	4.12	.03	.05	1	3
STD C/AU-S	19	60	37	133	7.4	68	27	1024	4.03	41	21	8	40	50	18	18	21	57	.48	.088	38	61	.84	172	.08	35	1.83	.08	.15	13	47
NM L11N 0+25W	3	349	13	120	.5	32	14	426	4.66	54	5	ND	2	12	1	2	2	79	.20	.049	5	48	1.06	53	.10	3	3.23	.03	.06	1	49
NM L11N 0+00E	14	1003	8	86	.6	37	24	521	7.18	182	5	ND	1	28	1	2	2	99	.65	.053	4	49	1.34	71	.05	4	3.95	.04	.06	2	32
NM L11N 0+25E	2	90	11	79	.3	23	8	288	3.83	28	5	ND	1	14	1	2	2	70	.24	.051	5	41	.69	36	.08	2	2.49	.03	.04	1	10
NM L11N 0+50E	2	93	14	93	.3	30	9	385	4.55	33	5	ND	1	16	1	2	2	71	.29	.099	5	48	.91	45	.08	3	2.56	.03	.06	1	5
NM L11N 0+75E	2	43	11	43	.3	15	5	152	2.62	23	5	ND	1	14	1	2	2	56	.30	.084	5	31	.48	36	.07	3	1.63	.03	.05	2	6
NM L11N 1+00E	2	23	8	43	.3	11	4	145	1.96	12	5	ND	1	16	1	2	2	49	.28	.027	4	22	.41	38	.07	2	1.26	.03	.05	1	2
NM L11N 1+25E	1	38	9	98	.1	20	11	695	4.19	23	5	ND	1	17	1	2	2	79	.29	.091	5	37	.89	45	.08	3	2.27	.03	.04	1	9
NM L11N 1+50E	1	38	5	72	.2	20	10	608	3.47	22	5	ND	1	24	1	2	2	67	.53	.049	5	37	.95	61	.09	3	1.97	.04	.06	1	4
NM L11N 1+75E	2	34	11	84	.5	20	9	440	3.84	26	6	ND	2	18	1	2	2	74	.33	.068	4	41	.97	60	.08	3	2.29	.03	.06	1	24
NM L11N 2+00E	2	76	12	88	.3	24	9	383	4.15	32	5	ND	2	14	1	2	2	70	.20	.055	6	42	.87	52	.08	3	2.96	.03	.05	1	1
NM L11N 2+25E	2	79	7	95	.1	24	9	333	4.16	31	5	ND	2	13	1	2	2	72	.18	.045	5	41	.85	43	.08	4	2.92	.03	.04	1	107
NM L11N 2+50E	2	22	9	70	.1	10	4	164	3.25	9	5	ND	1	15	1	2	2	68	.19	.040	5	28	.40	34	.09	2	2.03	.02	.01	1	10
NM L11N 2+75E	3	51	9	62	.4	16	6	199	3.71	30	5	ND	2	14	1	2	2	78	.20	.037	6	34	.57	45	.07	2	2.20	.03	.04	1	9
NM L11N 3+00E	2	187	10	150	.3	22	10	440	3.23	26	5	ND	1	28	1	2	2	68	.65	.036	7	34	.81	67	.08	4	2.51	.04	.04	1	1
NM L11N 3+25E	4	464	13	91	.4	20	10	1202	3.42	22	5	ND	1	32	1	2	2	63	.76	.049	19	29	.77	81	.06	4	2.75	.04	.04	1	5
NM L11N 3+50E	6	362	11	109	.3	26	11	633	2.92	37	5	ND	1	23	1	2	2	58	.64	.035	9	38	.64	68	.05	4	2.44	.04	.04	1	5
NM L11N 3+75E	3	36	8	84	.2	10	6	247	3.76	12	5	ND	2	20	1	2	2	90	.27	.043	4	22	.64	42	.10	3	2.31	.03	.03	1	3
NM L11N 4+00E	2	619	9	91	.4	21	10	834	3.66	29	5	ND	1	28	1	2	2	71	.54	.026	12	28	.83	58	.08	4	2.82	.03	.06	1	6
NM L11N 4+50E	7	167	8	86	.4	24	9	294	4.35	26	5	ND	2	15	1	2	2	78	.27	.035	6	44	.81	50	.09	4	2.63	.03	.04	1	3
NMB L10+00N 5+50W	2	34	7	100	.4	12	6	326	3.61	17	5	ND	1	11	1	2	2	52	.13	.067	4	25	.52	31	.05	4	2.69	.03	.04	1	2
NMB L10+00N 5+25W	2	58	7	110	.2	17	7	337	4.58	47	5	ND	1	10	1	2	2	59	.14	.076	5	31	.74	42	.06	3	2.98	.03	.04	1	18
NMB L10+00N 5+00W	2	51	10	137	.4	23	9	313	4.41	37	5	ND	2	10	1	2	2	60	.14	.070	6	41	.81	51	.07	3	3.10	.03	.03	2	2
NMB L10+00N 4+75W	1	27	9	79	.2	12	5	191	3.01	16	5	ND	1	11	1	2	2	47	.13	.052	5	26	.51	33	.06	2	2.46	.02	.03	1	2
NMB L10+00N 4+50W	1	43	7	116	.3	17	7	292	3.98	30	5	ND	1	12	1	2	2	56	.15	.057	6	32	.62	47	.06	2	2.78	.02	.03	1	8
NMB L10+00N 4+25W	2	75	7	118	.3	18	7	331	4.79	58	5	ND	2	10	1	2	2	56	.11	.063	5	29	.80	46	.07	4	2.89	.02	.03	1	2
NMB L10+00N 4+00W	1	32	11	108	.2	16	7	279	3.67	21	5	ND	2	13	1	2	2	56	.16	.064	6	30	.67	40	.07	2	2.53	.02	.03	1	3

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NMB L10+00N 3+50W	1	19	7	155	.1	14	7	289	3.75	14	5	ND	1	10	1	2	2	52	.13	.067	4	33	.57	35	.06	5	2.76	.02	.03	1	11
NMB L10+00N 3+00W	1	14	8	122	.1	8	4	189	2.96	9	5	ND	1	10	1	2	2	47	.17	.072	4	21	.37	22	.05	3	2.23	.02	.02	2	1
NMB L10+00N 2+50W	1	45	9	132	.2	14	7	260	3.87	23	5	ND	2	10	1	2	2	54	.12	.072	4	26	.61	37	.07	3	3.09	.02	.04	3	4
NMB L10+00N 2+00W	1	36	10	142	.2	16	8	453	3.57	20	5	ND	1	11	1	2	2	58	.16	.047	4	30	.69	36	.06	3	2.46	.03	.03	1	1
NMB L10+00N 1+50W	1	34	8	101	.2	29	9	293	4.13	13	5	ND	1	11	1	2	2	75	.23	.071	5	54	.93	35	.08	3	2.57	.03	.05	1	1
STD C/AU-5	19	60	39	131	7.3	68	27	1053	3.94	39	21	8	39	48	18	18	23	55	.46	.085	37	59	.90	171	.07	36	1.86	.08	.15	14	48
NMB L10+00N 1+00W	3	233	11	84	.3	24	9	337	4.38	33	5	ND	1	14	1	2	2	76	.23	.072	4	45	.71	40	.07	2	3.92	.03	.03	2	31
NMB L10+00N 0+50W	11	1033	9	89	.4	36	22	536	6.26	139	5	ND	1	31	1	2	2	89	.76	.046	4	51	1.45	61	.05	5	3.90	.04	.03	2	565
NMB L10+00N 0+00	1	41	7	72	.5	18	7	221	3.60	8	5	ND	2	11	1	2	2	63	.19	.065	4	40	.55	29	.06	2	2.53	.02	.03	1	13
NMB L10+00N 0+50E	1	54	9	114	.1	23	8	245	3.66	18	5	ND	1	11	1	2	2	63	.21	.083	4	40	.73	36	.09	3	3.06	.03	.04	1	6
NMB L10+00N 1+00E	2	64	12	142	.1	36	11	292	4.09	34	5	ND	1	13	1	2	2	71	.30	.066	4	48	.79	41	.11	4	3.05	.03	.03	1	25
NMB L10+00N 1+50E	1	54	8	65	.2	17	6	191	2.89	13	5	ND	1	12	1	2	2	57	.19	.046	5	32	.58	43	.07	2	2.26	.03	.03	1	6
NMB L10+00N 2+00E	2	84	11	98	.4	30	9	302	4.40	46	5	ND	2	11	1	2	2	71	.19	.069	5	57	.93	40	.08	4	3.34	.03	.04	2	3
NMB L10+00N 2+50E	2	50	8	103	.1	27	8	258	4.11	16	5	ND	1	11	1	2	2	73	.21	.054	5	60	.86	35	.09	3	2.74	.03	.03	1	4
NMB L10+00N 3+00E	1	36	9	83	.4	22	10	685	3.26	16	5	ND	1	21	1	2	2	63	.44	.045	4	41	1.09	52	.08	7	2.09	.04	.05	1	6
NMB L10+00N 3+50E	2	159	8	73	.1	30	9	383	3.52	28	5	ND	2	14	1	2	2	59	.22	.056	4	49	1.09	52	.08	3	2.77	.03	.04	4	7
NMB L10+00N 4+00E	16	470	7	178	.3	179	29	439	6.31	294	5	ND	1	11	1	2	2	88	.31	.067	4	200	2.05	48	.10	5	4.06	.03	.02	2	8
NMB L9+00N 5+50W	2	35	8	91	.1	13	5	218	3.11	23	5	ND	1	10	1	2	2	47	.14	.049	5	26	.59	36	.04	2	2.34	.02	.03	1	4
NMB L9+00N 5+00W	2	37	9	159	.2	21	10	494	3.84	25	6	ND	2	12	1	2	2	55	.15	.057	5	31	.74	58	.07	3	3.06	.03	.04	1	1
NMB L9+00N 4+50W	1	21	5	91	.1	9	5	245	2.84	10	5	ND	1	12	1	2	2	45	.13	.054	4	24	.49	32	.05	2	2.25	.02	.03	1	1
NMB L9+00N 4+00W	3	120	12	127	.1	25	9	445	4.30	29	5	ND	1	15	1	2	2	66	.25	.068	5	43	.84	53	.07	14	2.78	.03	.03	2	1
NMB L9+00N 3+50W	2	47	7	160	.4	14	8	352	4.46	47	5	ND	2	9	1	2	2	55	.11	.073	4	28	.78	38	.06	3	3.28	.03	.04	1	17
NMB L9+00N 3+00W	2	32	7	126	.1	8	5	347	3.59	30	5	ND	1	9	1	2	2	44	.11	.095	4	18	.49	31	.05	2	2.85	.02	.03	1	1
NMB L9+00N 2+50W	1	42	5	203	.4	19	11	532	3.74	26	5	ND	2	14	1	2	2	57	.19	.076	5	29	.75	48	.06	6	3.23	.03	.03	2	1
NMB L9+00N 2+00W	2	32	8	150	.1	16	7	260	3.77	27	5	ND	2	11	1	2	2	59	.14	.066	5	33	.71	42	.06	2	2.80	.03	.03	4	4
NMB L9+00N 1+50W	2	43	10	144	.2	18	9	342	4.19	18	5	ND	1	15	1	2	2	74	.25	.081	4	29	.60	32	.09	3	3.63	.03	.04	3	1
NMB L9+00N 1+00W	13	888	12	84	1.8	32	23	652	7.17	133	5	ND	1	23	1	2	2	83	.57	.077	3	41	1.32	34	.06	5	3.25	.04	.04	2	44
NMB L9+00N 0+50W	1	125	8	88	.5	50	11	305	4.41	24	5	ND	2	12	1	2	2	82	.29	.059	4	84	1.18	42	.10	7	3.35	.03	.04	1	6
NMB L9+00N 0+50E	3	132	10	107	.1	31	10	477	4.40	33	5	ND	1	15	1	2	2	74	.31	.068	5	60	.94	58	.07	3	2.90	.03	.04	1	1
NMB L9+00N 1+00E	2	67	12	110	.4	28	8	270	3.89	40	5	ND	2	10	1	2	2	62	.18	.049	5	48	.89	39	.07	8	3.29	.03	.03	1	6
NMB L9+00N 1+50E	11	246	8	140	.6	58	12	266	5.27	215	5	ND	2	15	1	2	2	84	.28	.045	4	91	.95	32	.10	5	3.20	.03	.04	1	31
NMB L9+00N 2+00E	2	32	10	91	.1	21	9	505	4.28	10	5	ND	1	12	1	2	2	63	.16	.050	4	38	1.47	72	.05	5	3.77	.03	.05	1	10
NMB L9+00N 2+50E	1	51	7	131	.4	72	17	667	4.32	9	5	ND	1	17	1	2	2	88	.71	.057	4	101	1.70	42	.08	3	3.00	.04	.04	1	2
NMB L9+00N 3+00E	2	93	9	100	.1	29	8	277	4.46	11	5	ND	1	11	1	2	2	79	.20	.052	4	57	.90	45	.08	2	3.00	.03	.02	1	3
NMB L8+00N 6+00W	1	29	7	112	.1	16	6	245	3.30	15	5	ND	1	13	1	2	2	50	.16	.049	6	26	.54	39	.06	4	2.49	.03	.02	1	7
NMB L8+00N 5+50W	1	18	9	91	.1	11	5	401	2.59	7	5	ND	1	12	1	2	2	44	.16	.058	4	21	.49	41	.05	2	1.96	.02	.03	1	12
NMB L8+00N 5+00W	2	42	11	146	.1	17	9	615	4.12	34	5	ND	2	12	1	2	2	59	.15	.049	4	27	.90	51	.07	3	3.08	.03	.04	1	1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU1 PPB
NMB L9 4+50W	1	29	9	161	.2	17	8	362	3.62	17	5	ND	1	11	1	2	2	56	.15	.067	4	34	.79	37	.06	2	2.88	.03	.01	2	6
NMB L8 4+00W	1	25	9	117	.1	18	7	1471	3.18	12	5	ND	1	17	1	2	2	53	.24	.068	4	34	.70	60	.05	2	2.46	.03	.03	2	8
NMB L8 3+50W	2	18	6	113	.4	11	6	982	2.72	8	5	ND	1	15	1	2	2	46	.23	.064	4	26	.53	48	.04	2	2.12	.02	.03	2	7
NMB L8 3+00W	1	20	8	112	.2	11	7	909	2.91	13	5	ND	1	16	1	2	2	50	.22	.065	4	23	.51	49	.05	2	2.00	.02	.04	1	1
NMB L8 2+50W	1	18	10	137	.5	11	6	601	3.23	8	5	ND	2	12	1	2	2	55	.17	.102	5	28	.55	34	.06	2	2.02	.02	.03	2	2
NMB L8 2+00W	1	72	11	125	.3	22	9	353	4.11	35	5	ND	1	11	1	2	2	65	.16	.068	5	37	.94	42	.06	2	2.87	.03	.01	1	1
NMB L8 1+50W	2	40	9	124	.1	28	8	391	3.75	15	5	ND	1	13	1	2	2	75	.27	.065	5	58	.95	39	.09	2	2.65	.03	.04	1	1
NMB L8 1+00W	3	152	11	90	.4	25	11	537	3.97	30	5	ND	1	18	1	2	2	66	.32	.060	7	40	.81	62	.07	2	2.39	.03	.04	3	3
STD C/AU-S	18	58	38	128	7.2	67	27	1029	3.88	40	21	7	38	49	18	17	20	56	.47	.085	38	60	.89	176	.07	37	1.84	.08	.13	12	52
NMB L8 0+50W	1	39	6	100	.5	25	8	624	3.82	13	5	ND	1	14	1	2	2	71	.25	.070	4	51	.81	44	.08	3	2.31	.03	.02	1	1
NMB L8 0+00W	1	61	8	84	.4	47	11	590	4.10	15	5	ND	1	13	1	2	2	86	.33	.039	4	91	1.23	42	.10	3	2.56	.03	.02	1	1
NMB L8 0+50E	1	23	8	91	.3	18	6	268	3.71	11	5	ND	1	12	1	2	2	69	.21	.052	4	43	.61	32	.08	4	2.05	.03	.02	1	1
NMB L8 1+00E	1	20	9	97	.2	16	5	320	3.48	12	5	ND	1	13	1	2	3	61	.23	.066	4	32	.61	47	.09	3	1.90	.03	.02	1	5
NMB L8 1+50E	1	11	6	67	.2	9	4	365	2.85	4	5	ND	1	14	1	2	2	57	.23	.041	4	18	.51	36	.05	2	1.80	.03	.05	1	2
NMB L8 2+00E	1	17	8	79	.1	16	7	430	3.61	9	5	ND	1	12	1	2	2	60	.17	.030	3	28	1.06	38	.05	2	2.63	.02	.02	1	1
NMB L8 2+50E	1	27	9	98	.1	17	10	707	3.38	5	5	ND	1	18	1	2	2	61	.25	.026	6	32	1.05	71	.05	2	2.89	.03	.05	1	1
NMB L8 3+00E	1	12	9	62	.3	9	4	352	3.15	3	5	ND	1	14	1	2	2	65	.18	.037	4	18	.45	39	.05	2	1.81	.02	.04	2	11
NMB L7+00N 4+50W	1	28	6	117	.2	18	7	292	3.13	16	5	ND	1	11	1	2	2	51	.13	.058	5	33	.68	38	.06	3	2.69	.03	.03	2	1
NMB L7+00N 4+00W	1	46	12	116	.3	29	9	305	4.17	25	5	ND	1	11	1	2	2	63	.13	.079	6	53	.87	52	.08	3	3.35	.03	.03	1	2
NMB L7+00N 3+50W	1	19	8	111	.2	8	5	336	2.87	13	5	ND	1	11	1	2	2	49	.12	.061	5	22	.41	29	.05	2	2.31	.02	.01	1	2
NMB L7+00N 3+00W	1	15	6	80	.2	12	5	215	2.52	10	5	ND	1	12	1	2	2	49	.14	.044	5	32	.50	31	.06	2	1.90	.02	.02	2	17
NMB L7+00N 2+50W	1	50	8	155	.1	39	12	485	3.94	21	5	ND	2	12	1	2	2	68	.20	.057	6	58	1.15	51	.07	2	3.23	.03	.04	1	1
NMB L7+00N 2+00W	1	38	7	242	.1	20	11	409	4.19	26	5	ND	1	14	1	2	2	69	.26	.095	5	32	.91	49	.07	2	2.76	.03	.03	1	1
NMB L7+00N 1+50W	2	193	11	118	.3	31	12	671	4.75	36	5	ND	1	13	1	2	2	76	.23	.097	5	46	.99	63	.09	3	3.81	.03	.04	2	16
NMB L7+00N 1+00W	2	118	11	103	.4	19	8	362	4.09	20	5	ND	1	13	1	2	2	63	.19	.083	5	33	.76	46	.07	3	2.96	.03	.03	1	12
NMB L7+00N 0+50W	4	1200	9	85	.4	61	16	549	5.04	131	5	ND	1	16	1	2	2	72	.30	.053	4	75	1.73	52	.07	5	4.00	.03	.02	2	63
NMB L7+00N 0+00W	2	428	8	85	.8	44	10	367	4.29	24	5	ND	1	15	1	2	2	79	.23	.063	4	81	1.05	38	.11	3	2.65	.03	.02	1	41
NMB L7+00N 0+50E	1	27	10	68	.1	16	6	338	3.19	10	5	ND	1	14	1	3	2	66	.23	.043	3	35	.74	33	.07	4	2.34	.03	.02	1	1
NMB L7+00N 1+00E	1	23	6	78	.5	13	6	231	2.26	8	5	ND	1	16	1	2	2	41	.24	.029	5	26	.56	39	.06	3	2.01	.03	.03	1	24
NMB L7+00N 1+50E	1	49	8	106	.1	29	8	395	4.80	23	5	ND	1	12	1	2	2	62	.19	.068	4	45	.97	49	.07	2	3.33	.03	.03	1	14
NMB L7+00N 2+00E	1	24	7	108	.1	18	6	412	3.70	13	5	ND	1	13	1	2	2	53	.19	.054	5	28	.86	47	.06	4	2.37	.03	.03	1	10
NMB L7+00N 2+50E	1	24	3	74	.1	16	6	331	3.07	6	5	ND	1	14	1	2	2	58	.19	.025	5	31	.90	48	.06	3	2.27	.03	.02	1	12
NMB L7+00N 3+00E	1	20	7	103	.1	19	8	523	4.17	10	5	ND	1	12	1	2	2	58	.14	.039	4	32	1.39	53	.05	3	2.84	.03	.05	1	7
NMB L6 6+00W	1	31	9	72	.2	9	4	274	3.25	26	5	ND	1	10	1	2	2	49	.11	.050	4	18	.50	33	.03	3	1.93	.02	.04	1	1
NMB L6 5+50W	1	36	6	144	.2	13	10	1172	3.33	25	5	ND	1	12	1	2	2	50	.14	.071	4	24	.62	49	.05	4	2.47	.03	.04	1	34
NMB L6 5+00W	1	46	9	122	.1	20	8	489	3.67	26	5	ND	1	13	1	2	2	54	.19	.073	5	38	.69	41	.06	4	2.60	.03	.05	2	8
NMB L6 4+50W	1	25	5	99	.3	11	5	410	3.62	24	5	ND	1	12	1	2	2	57	.13	.076	4	27	.50	38	.07	3	2.17	.03	.03	2	1

SAMPLE#	MO	CU	PB	ZN	AG	NI	CD	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AUX
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NMB L6 4+00W	1	25	11	149	.2	18	10	1444	3.77	22	5	ND	1	15	1	2	2	68	.29	.058	4	27	.77	50	.05	2	2.54	.03	.07	1	31
NMB L6 3+50W	1	18	7	134	.1	15	7	591	2.89	9	6	ND	1	15	1	2	2	59	.23	.046	4	32	.52	45	.06	3	1.88	.03	.05	1	7
NMB L6 3+00W	1	27	8	162	.1	26	13	1127	3.83	17	5	ND	3	19	1	2	2	74	.40	.034	4	46	.87	66	.07	3	2.47	.03	.09	1	4
NMB L6 2+50W	1	38	7	117	.1	99	19	398	5.01	13	5	ND	2	11	1	2	2	121	.21	.030	3	192	2.30	37	.08	3	3.43	.03	.04	1	2
NMB L6 2+00W	3	115	9	107	.3	26	9	394	4.26	28	5	ND	1	12	1	2	2	71	.19	.059	5	46	.81	45	.07	3	3.20	.03	.03	1	62
NMB L6 1+50W	11	717	8	78	.8	25	15	642	7.00	133	5	ND	2	22	1	2	2	95	.50	.074	3	35	1.18	57	.06	4	4.13	.04	.04	2	36
NMB L6 1+00W	10	865	7	87	1.0	26	15	611	6.18	134	5	ND	2	21	1	2	2	90	.49	.090	2	38	1.14	72	.06	5	3.91	.03	.07	1	13
NMB L6 0+50W	5	1744	10	97	1.3	73	27	783	5.68	51	5	ND	2	15	1	2	3	80	.31	.062	3	87	1.26	45	.09	5	3.98	.04	.05	1	95
NMB L6 0+00	2	101	10	88	.1	24	8	367	3.29	28	5	ND	2	15	1	2	2	59	.29	.047	4	37	.59	52	.08	2	2.08	.03	.02	1	15
NMB L6 0+50E	1	16	4	48	.1	11	3	189	1.78	10	5	ND	1	15	1	2	2	46	.24	.025	4	21	.27	32	.09	2	1.19	.02	.04	3	1
NMB L6 1+00E	2	14	7	51	.2	9	3	197	2.40	7	5	ND	1	13	1	2	2	55	.20	.034	4	19	.32	30	.08	2	1.38	.02	.03	2	7
NMB L6 1+50E	1	23	10	76	.1	17	5	227	3.38	18	5	ND	2	12	1	2	2	55	.18	.031	5	32	.53	34	.08	2	2.32	.03	.01	1	8
NMB L6 2+00E	2	31	9	77	.2	18	6	280	3.57	13	5	ND	2	13	1	2	4	61	.19	.046	4	29	.66	46	.07	2	2.16	.02	.03	1	1
NMB L6 2+50E	1	26	7	74	.2	16	5	264	3.57	20	5	ND	1	13	1	2	2	62	.19	.044	4	29	.61	41	.06	3	2.19	.03	.04	1	8
NMB L6 3+00E	2	94	9	98	.2	22	7	401	3.55	23	5	ND	1	16	1	2	2	60	.25	.050	5	38	.64	54	.06	2	2.25	.03	.03	1	9
NMB L5N 7+00W	1	23	6	73	.1	11	5	208	2.84	13	5	ND	1	10	1	2	2	45	.10	.036	5	17	.50	35	.05	3	2.23	.02	.01	1	2
NMB L5N 6+50W	1	35	8	87	.3	13	6	216	2.86	21	5	ND	2	9	1	2	2	42	.09	.057	5	24	.49	36	.07	3	3.06	.02	.02	1	7
NMB L5N 6+00W	1	65	8	82	.1	15	7	283	3.91	45	5	ND	1	10	1	2	2	53	.10	.043	5	24	.57	39	.07	2	2.54	.03	.03	1	4
NMB L5N 5+50W	1	29	5	76	.1	13	5	253	2.55	15	5	ND	1	9	1	2	2	41	.09	.034	4	20	.62	29	.04	2	2.33	.03	.02	1	1
NMB L5N 5+00W	2	39	4	68	.1	20	7	264	4.04	15	5	ND	1	15	1	2	2	75	.25	.043	4	36	.68	38	.09	3	2.72	.03	.04	1	18
NMB L5N 4+50W	1	43	6	102	.4	22	7	204	3.29	16	5	ND	1	15	1	2	2	55	.22	.047	4	33	.52	31	.07	3	2.60	.03	.04	1	1
NMB L5N 4+25W	1	68	7	105	.1	42	11	387	4.23	23	5	ND	1	13	1	2	2	61	.27	.053	3	57	1.02	42	.09	3	3.40	.03	.04	1	17
NMB L5N 4+00W	2	38	6	93	.5	35	10	500	4.29	24	6	ND	1	16	1	3	2	70	.27	.056	4	49	1.00	51	.08	4	2.98	.03	.06	1	23
NMB L5N 3+50W	1	25	4	69	.2	17	6	216	3.57	16	5	ND	2	16	1	2	3	64	.31	.052	4	37	.50	43	.07	3	2.15	.03	.05	1	7
NMB L5N 3+00W	2	121	8	71	.2	30	9	289	3.68	17	5	ND	1	15	1	2	2	67	.24	.036	3	38	.76	42	.09	4	2.49	.03	.04	1	1
NMB L5N 2+50W	3	584	6	83	-1.1	44	9	313	4.82	54	5	ND	1	13	1	2	2	73	.21	.060	4	64	.89	40	.08	5	3.17	.03	.06	1	8
NMB L5N 2+00W	11	707	6	73	1.5	23	10	387	6.12	110	5	ND	2	15	1	4	2	86	.27	.085	2	33	1.03	50	.05	4	3.92	.03	.03	2	5
NMB L5N 1+50W	12	823	9	87	1.7	23	16	417	7.07	127	5	ND	2	16	1	2	2	90	.37	.077	3	33	1.10	45	.05	4	4.23	.03	.04	3	5
NMB L5N 1+00W	4	74	8	146	.5	24	8	286	5.49	63	8	ND	2	11	1	2	2	74	.16	.063	5	43	.74	49	.07	2	3.41	.02	.03	1	13
NMB L5N 0+50W	2	100	8	139	.4	31	10	455	5.97	56	5	ND	2	13	1	2	2	80	.30	.233	4	54	.99	49	.06	2	4.20	.03	.05	1	6
NMB L5N 0+00W	1	27	6	128	.1	17	8	333	3.48	17	5	ND	1	15	1	2	2	68	.25	.034	6	28	.67	44	.06	2	2.43	.03	.04	1	76
NMB L5N 0+50E	1	55	5	106	.3	23	9	314	4.36	33	5	ND	1	12	1	2	2	71	.17	.067	5	38	.79	52	.06	3	3.29	.03	.03	1	3
NMB L5N 1+00E	1	40	8	134	.2	15	6	270	3.40	30	6	ND	1	11	1	2	2	53	.16	.080	5	28	.60	42	.04	3	2.78	.02	.04	1	4
NMB L5N 1+50E	1	45	8	138	.1	13	6	363	3.52	43	5	ND	1	13	1	2	2	49	.16	.059	4	22	.54	42	.05	2	2.47	.03	.02	1	3
NMB L5N 2+00E	1	48	9	95	.1	16	6	235	3.78	35	5	ND	1	11	1	2	2	50	.11	.043	6	28	.53	55	.08	2	2.77	.02	.03	1	1
NMB L4N 7+00W	1	55	5	129	.3	12	7	283	3.70	42	5	ND	1	10	1	3	2	44	.10	.072	4	22	.53	38	.05	3	3.11	.03	.03	1	12
STD C/AU-S	18	57	39	132	7.3	68	27	1025	3.98	40	21	8	38	50	18	18	20	56	.48	.085	38	59	.84	177	.08	34	1.89	.08	.13	13	47

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NMB L4 6+50W	1	43	10	88	.1	15	7	410	3.84	56	5	ND	2	13	1	2	2	57	.18	.065	4	22	.60	43	.05	2	2.17	.03	.03	1	1
NMB L4 6+00W	2	95	11	121	.1	15	8	738	3.91	69	5	ND	2	14	1	2	2	43	.22	.091	4	22	.66	48	.05	2	3.00	.03	.04	3	2
NMB L4 5+50W	1	37	12	106	.1	13	6	322	3.83	38	5	ND	2	14	1	2	2	53	.14	.069	5	24	.51	49	.07	2	2.58	.02	.03	1	1
NMB L4 5+00W	1	29	11	111	.1	13	6	804	3.35	27	5	ND	2	12	1	2	2	52	.14	.067	5	25	.51	53	.07	2	2.52	.03	.02	1	5
NMB L4 4+50W	1	23	8	110	.1	12	6	295	3.01	20	5	ND	2	13	1	2	2	51	.17	.035	5	23	.51	39	.07	2	2.11	.02	.05	1	2
STD C/AU-S	18	60	38	130	7.0	67	27	1064	3.94	42	18	7	39	49	17	17	21	55	.48	.087	37	57	.87	176	.08	38	1.86	.08	.14	13	52
NMB L4 4+00W	2	74	13	126	.1	18	8	1080	3.54	25	5	ND	1	16	1	2	2	58	.25	.063	4	31	.62	63	.07	2	2.32	.03	.07	1	5
NMB L4 3+50W	1	22	8	99	.2	8	5	762	2.39	9	5	ND	2	16	1	2	2	49	.29	.045	4	16	.46	52	.05	2	1.62	.02	.07	1	8
NMB L4 3+00W	6	284	13	174	.2	27	12	387	4.17	40	5	ND	3	15	1	2	2	71	.38	.015	4	31	1.07	40	.07	2	3.07	.03	.03	1	6
NMB L4 2+50W	4	223	13	115	.2	25	10	519	4.44	43	5	ND	1	16	1	2	2	66	.29	.061	4	36	.84	58	.07	2	2.84	.03	.03	1	8
NMB L4 2+00W	8	382	12	87	.6	17	7	386	3.76	53	5	ND	1	18	1	2	2	62	.36	.085	5	32	.68	39	.05	2	2.69	.03	.06	1	9
NMB L4 1+50W	2	411	7	93	.4	15	8	445	3.76	32	5	ND	1	16	1	2	2	60	.20	.047	4	28	.86	48	.05	2	2.86	.03	.05	1	39
NMB L4 1+00W	2	614	16	101	.5	26	12	718	4.12	29	5	ND	1	16	1	2	2	66	.28	.053	4	42	1.12	53	.08	3	2.89	.03	.05	1	16
NMB L4 0+50W	1	67	10	96	.3	21	10	1245	3.43	16	5	ND	1	16	1	2	2	59	.30	.053	3	34	.79	51	.07	2	2.25	.03	.06	1	14
NMB L4 0+00	2	52	11	94	.1	39	11	384	4.28	29	5	ND	1	17	1	2	2	66	.30	.050	3	55	.98	48	.09	3	3.17	.03	.05	1	42
NMB L4 0+50E	1	22	8	95	.3	23	7	558	3.30	13	5	ND	1	14	1	2	2	48	.23	.043	3	35	.86	60	.08	2	2.38	.03	.04	1	9
NMB L4 1+00E	1	27	8	81	.1	30	8	344	3.75	21	5	ND	1	15	1	2	2	63	.27	.032	4	47	.91	34	.10	2	2.60	.03	.03	2	23
NMB L4 1+50E	1	19	9	65	.1	10	4	639	2.03	7	5	ND	1	21	1	2	2	41	.39	.046	4	15	.36	68	.06	2	1.49	.03	.06	1	5
NMB L4 2+00E	1	27	12	130	.2	24	8	581	4.02	16	5	ND	2	15	1	2	2	55	.37	.085	3	39	.91	43	.07	2	2.79	.03	.06	1	24
NMB L3 5+50W	1	18	8	51	.1	7	3	205	2.68	17	5	ND	2	13	1	2	2	50	.12	.031	6	17	.36	34	.06	2	2.02	.02	.02	3	2
NMB L3 5+00W	2	26	12	102	.1	9	5	220	2.94	20	5	ND	2	12	1	2	2	46	.12	.044	6	19	.43	43	.06	2	2.58	.02	.03	1	1
NMB L3 4+50W	2	83	9	170	.1	19	11	497	4.43	68	5	ND	1	11	1	2	2	54	.17	.095	4	31	.83	44	.05	2	3.66	.03	.03	1	18
NMB L3 4+00W	1	24	4	144	.1	11	6	290	3.28	18	5	ND	2	12	1	2	2	59	.19	.055	5	20	.57	36	.05	2	2.39	.02	.05	2	4
NMB L3 3+50W	4	60	12	130	.3	17	8	332	4.32	59	5	ND	2	12	1	2	2	71	.20	.034	5	28	.73	41	.07	2	2.71	.03	.04	2	1
NMB L3 3+25W	9	233	14	133	.1	23	19	897	6.77	108	5	ND	2	15	1	2	2	100	.27	.083	4	37	1.13	51	.08	2	3.77	.03	.05	4	19
NMB L3 3+00W	46	919	10	41	.7	12	30	388	7.07	136	5	ND	4	36	1	2	2	47	.58	.057	9	12	.66	20	.02	4	2.96	.03	.04	7	17
NMB L3 2+75W	11	539	11	82	.2	25	18	592	7.59	132	5	ND	2	21	1	2	2	106	.36	.058	4	34	1.26	47	.09	2	4.08	.03	.04	3	12
NMB L3 2+50W	4	114	12	94	.3	25	10	345	5.27	78	5	ND	1	14	1	2	2	74	.24	.053	5	42	.96	42	.08	12	3.22	.03	.03	1	6
NMB L3 2+00W	6	748	9	93	.3	39	17	692	4.55	98	5	ND	2	18	1	2	2	82	.39	.035	4	61	1.22	75	.07	3	3.32	.04	.09	1	12
NMB L3 1+50W	2	66	12	83	.5	22	12	503	4.22	24	5	ND	2	15	1	2	2	77	.29	.029	4	34	.99	36	.09	2	2.65	.03	.07	1	7
NMB L3 1+00W	1	38	9	82	.4	25	10	388	3.79	22	5	ND	2	19	1	2	2	65	.34	.045	4	44	.82	35	.08	2	2.51	.03	.05	2	1
NMB L3 0+50W	1	32	8	109	.1	21	8	383	3.53	17	5	ND	1	16	1	2	2	59	.25	.042	4	33	.67	47	.08	2	2.69	.03	.04	1	11
NMB L3 0+00W	1	28	9	86	.3	22	8	438	3.85	17	5	ND	2	20	1	2	2	68	.34	.041	4	36	.95	47	.06	2	2.62	.03	.07	2	10
NMB L3 0+50E	1	28	8	107	.1	36	9	352	4.00	19	5	ND	2	14	1	2	2	65	.24	.050	3	62	.99	38	.08	3	3.31	.03	.05	1	41
NMB L3 1+00E	1	27	8	98	.1	25	8	438	3.50	21	5	ND	1	15	1	2	2	49	.25	.058	3	37	.89	39	.09	2	2.77	.03	.05	1	50
NMB L3 1+50E	1	38	9	87	.1	33	10	655	3.37	17	5	ND	1	18	1	2	2	53	.38	.054	4	42	.74	52	.08	2	2.31	.03	.07	1	18
NMB L3 2+00E	1	17	6	66	.2	16	5	266	3.37	14	5	ND	1	14	1	2	2	59	.23	.040	4	33	.54	36	.09	2	1.98	.03	.05	1	31

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NMB L2N 5+50W	1	34	12	130	.2	11	7	383	3.51	20	5	ND	1	14	1	2	2	51	.20	.063	5	22	.51	37	.06	2	2.03	.02	.06	1	25
NMB L2N 5+00W	1	23	6	104	.3	9	5	241	2.82	15	5	ND	1	13	1	2	2	45	.15	.044	5	16	.44	27	.05	3	1.90	.02	.05	1	9
NMB L2N 4+50W	2	28	11	191	.4	11	7	361	3.56	17	5	ND	2	12	1	2	2	57	.15	.063	5	23	.59	44	.05	2	2.10	.02	.05	1	3
NMB L2N 4+00W	4	51	9	182	.3	19	11	582	4.71	42	5	ND	1	16	1	2	2	70	.35	.075	5	32	.89	42	.05	4	3.58	.03	.05	2	5
NMB L2N 3+50W	8	258	9	70	.6	10	7	378	9.59	20	5	ND	2	14	1	2	2	85	.18	.123	3	16	.45	38	.07	3	2.89	.03	.05	3	32
NMB L2N 3+00W	5	216	11	79	.5	28	14	374	5.78	313	5	ND	1	12	1	2	2	73	.19	.061	3	38	.93	45	.07	3	4.26	.03	.03	1	23
NMB L2N 2+50W	2	47	10	76	.4	13	7	316	4.05	41	5	ND	1	14	1	2	2	88	.22	.037	4	25	.59	34	.08	3	2.40	.03	.06	1	5
STD C/AU-S	19	61	38	129	7.2	69	28	1047	3.98	38	24	7	39	50	18	17	19	56	.48	.086	38	60	.84	176	.08	38	1.81	.08	.14	12	49
NMB L2N 2+00W	1	51	9	93	.3	23	10	540	3.79	18	5	ND	1	19	1	2	2	69	.34	.043	4	35	1.19	49	.07	3	3.06	.03	.08	1	5
NMB L2N 1+50W	4	71	7	126	.3	18	10	367	5.08	50	5	ND	1	15	1	2	2	83	.31	.057	3	31	.78	45	.07	4	2.70	.03	.05	1	60
NMB L2N 1+00W	1	20	8	72	.1	10	6	426	3.19	8	5	ND	1	18	1	2	2	55	.22	.051	3	20	.66	57	.04	2	2.51	.03	.07	1	14
NMB L2N 0+50W	1	41	6	90	.3	24	9	328	3.82	15	5	ND	2	15	1	2	2	62	.21	.043	4	39	.87	41	.08	4	2.97	.03	.05	1	1
NMB L2N 0+00W	1	30	8	84	.2	25	8	314	3.76	23	8	ND	1	16	1	2	2	60	.25	.059	3	43	.75	43	.07	4	2.53	.03	.05	1	23
NMB L2N 0+50E	1	28	9	83	.2	35	9	357	3.84	18	5	ND	1	14	1	2	2	63	.24	.047	3	63	1.00	40	.08	4	3.01	.03	.05	1	21
NMB L2N 1+00E	1	27	4	87	.4	33	9	336	3.56	15	5	ND	1	17	1	2	2	54	.30	.057	4	51	.85	40	.08	3	2.95	.03	.06	1	26
NMB L2N 1+50E	1	28	9	92	.1	38	9	352	4.14	26	5	ND	1	15	1	2	2	71	.27	.043	3	62	.94	43	.10	4	2.73	.03	.05	1	35
NMB L2N 2+00E	2	28	6	100	.1	27	8	362	3.48	22	5	ND	1	14	1	2	2	56	.24	.046	4	42	.72	42	.07	4	2.39	.03	.04	1	42
NMB L1 0+00E	1	35	9	93	.3	31	11	356	3.44	16	5	ND	1	15	1	2	2	60	.22	.042	4	41	.92	49	.08	3	3.17	.03	.04	1	18
NMB L1 0+50E	1	30	9	79	.3	29	10	347	3.40	10	5	ND	1	16	1	2	2	58	.24	.037	3	49	.92	46	.06	2	2.87	.03	.04	1	29
NMB L1 1+00E	1	47	6	107	.2	42	14	933	3.99	32	5	ND	1	21	1	2	2	62	.46	.069	3	60	1.01	60	.07	5	2.89	.03	.10	1	113
NMB L1 1+50E	2	31	7	124	.2	30	9	391	4.09	23	8	ND	1	22	1	2	2	66	.40	.050	4	45	.97	50	.07	3	2.46	.03	.08	1	24
NMB L1 2+00E	2	42	5	131	.1	29	9	466	4.55	47	5	ND	1	11	1	2	2	55	.19	.083	4	39	1.05	45	.05	3	3.12	.03	.05	1	20
NMB 300S 4+50W	2	26	10	108	.1	14	10	885	3.83	6	5	ND	1	24	1	2	2	70	.36	.059	4	25	.78	75	.04	3	2.72	.03	.08	1	1
NMB 300S 4+00W	1	18	16	126	.1	15	9	635	3.67	7	7	ND	1	21	1	2	2	68	.35	.044	4	26	.90	39	.07	3	2.50	.03	.06	1	20
NMB 300S 3+50W	2	25	15	122	.1	14	8	743	4.29	11	5	ND	1	19	1	2	2	72	.20	.042	4	25	.73	59	.06	3	2.28	.03	.07	1	2
NMB 300S 3+00W	2	61	11	91	.1	19	8	482	3.57	23	5	ND	1	18	1	2	2	61	.32	.048	5	31	.75	51	.07	3	2.31	.03	.05	1	1
NMB 300S 2+50W	2	52	11	96	.1	17	7	475	3.57	16	5	ND	1	17	1	2	2	56	.24	.062	4	29	.68	51	.06	2	2.44	.03	.05	1	16
NMB 300S 2+00W	1	42	15	88	.1	19	9	854	3.37	11	5	ND	2	23	1	2	2	52	.37	.050	7	27	.94	90	.08	3	2.54	.03	.06	1	1
NMB 300S 1+00W	2	23	11	91	.2	11	6	447	3.49	7	8	ND	1	18	1	2	2	58	.21	.058	4	25	.75	51	.06	2	2.32	.03	.05	1	1
NMB 300S 0+50W	1	18	9	84	.1	10	7	961	3.29	2	5	ND	1	19	1	2	2	68	.24	.058	4	19	.70	89	.07	2	1.97	.03	.05	1	1
NMB 2+00S 5+00W	3	82	15	123	.1	21	11	720	3.94	48	5	ND	1	19	1	2	2	65	.30	.098	6	42	.77	70	.05	2	2.78	.03	.05	1	1
NMB 2+00S 4+50W	1	61	9	120	.1	29	13	645	4.25	18	5	ND	1	23	1	2	2	77	.39	.047	4	46	1.30	58	.08	3	3.53	.03	.08	1	15
NMB 2+00S 4+00W	1	24	13	105	.1	28	10	724	3.69	13	5	ND	1	20	1	2	2	72	.31	.048	4	36	.99	58	.07	2	2.54	.03	.04	1	5
NMB 2+00S 3+50W	1	27	12	114	.1	19	12	864	4.05	8	5	ND	1	19	1	2	2	83	.30	.042	4	35	1.08	56	.09	3	2.80	.03	.06	1	1
NMB 2+00S 3+00W	1	23	14	122	.1	29	11	662	3.96	8	5	ND	1	19	1	2	2	74	.35	.044	4	46	1.38	39	.08	2	2.82	.03	.05	1	1
NMB 1+00N 7+00W	1	61	8	130	.1	18	9	610	3.68	48	5	ND	1	13	1	4	2	63	.13	.047	6	30	.71	51	.04	4	2.30	.02	.03	2	1
NMB 1+00N 6+50W	1	40	8	93	.3	11	5	423	3.13	37	5	ND	1	14	1	2	2	57	.14	.056	5	22	.48	48	.04	3	2.16	.02	.04	1	11

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AUX PPB
NMB 1+00N 6+00W	1	36	8	86	.2	10	5	258	3.58	45	5	ND	1	13	1	2	2	60	.11	.040	5	23	.48	55	.05	2	2.07	.02	.04	1	4
NMB 1+00N 5+50W	1	57	6	121	.3	10	5	388	4.02	50	5	ND	1	13	1	2	2	58	.12	.057	5	21	.52	47	.04	3	2.20	.02	.03	1	1
NMB 1+00N 5+00W	2	49	7	108	.1	10	6	282	3.90	41	5	ND	1	10	1	2	2	67	.09	.039	4	24	.59	37	.04	3	2.21	.02	.03	1	1
NMB 1+00N 4+50W	1	48	9	161	.4	16	10	413	4.32	37	5	ND	1	13	1	2	2	57	.17	.095	5	28	.62	42	.05	3	3.23	.02	.05	2	6
NMB 1+00N 4+00W	1	40	14	114	.1	24	13	596	4.03	25	5	ND	1	15	1	2	2	73	.20	.040	2	35	1.09	44	.04	2	2.54	.01	.03	1	1
NMB 1+00N 3+50W	2	73	13	106	.1	26	16	842	4.68	21	5	ND	2	16	1	2	2	88	.21	.055	4	40	1.08	51	.09	3	3.15	.03	.04	1	5
NMB 1+00N 3+00W	2	43	10	89	.1	24	12	522	4.16	13	5	ND	1	16	1	2	2	88	.19	.028	4	36	.98	49	.10	3	2.93	.03	.03	1	1
NMB 1+00N 2+50W	3	87	11	108	.4	23	9	528	3.97	33	5	ND	1	16	1	2	2	65	.24	.058	5	40	.76	58	.06	5	2.50	.03	.04	1	7
NMB 1+00N 2+00W	1	14	8	73	.1	12	6	475	2.69	5	5	ND	1	15	1	2	2	61	.19	.042	4	26	.63	39	.07	2	1.76	.03	.03	1	1
NMB 1+00N 1+50W	1	25	10	149	.2	13	8	1076	3.66	8	5	ND	1	16	1	2	2	58	.19	.068	4	21	.70	62	.05	3	2.22	.02	.05	1	3
NMB 1+00N 1+00W	1	17	8	96	.2	12	7	393	3.19	5	5	ND	1	16	1	2	2	62	.23	.055	4	23	.79	37	.05	2	2.21	.03	.06	1	1
NMB 1+00N 0+50W	2	35	8	105	.1	18	9	503	3.76	9	5	ND	1	19	1	2	2	65	.28	.074	3	31	.87	52	.05	3	2.96	.03	.04	2	5
NMB 1+00S 5+50W	3	48	8	132	.3	11	6	524	2.64	40	5	ND	1	15	2	2	2	39	.18	.099	5	20	.42	44	.02	6	2.26	.02	.04	1	3
NMB 1+00S 5+00W	3	57	12	172	.5	17	16	1738	5.38	103	7	ND	1	20	1	2	2	84	.29	.153	5	42	.70	59	.02	4	2.63	.02	.07	2	1
NMB 1+00S 4+50W	2	70	10	112	.1	21	10	633	3.96	23	5	ND	1	17	1	2	2	69	.28	.065	4	36	.84	57	.05	3	2.52	.03	.04	2	1
STD C/AU-S	18	59	38	128	7.4	66	28	1046	3.92	38	21	7	39	49	18	18	19	56	.46	.085	38	57	.81	174	.07	36	1.75	.08	.13	12	48
NMB 1+00S 4+00W	2	57	14	97	.3	15	7	432	3.26	18	5	ND	1	17	1	2	2	60	.26	.050	4	26	.62	62	.05	3	2.00	.03	.05	2	4
NMB 1+00S 3+50W	1	18	12	92	.1	10	6	386	3.31	4	7	ND	1	13	1	2	2	62	.17	.056	3	23	.62	34	.05	2	1.86	.02	.04	1	1
NMB 1+00S 3+00W	2	49	12	94	.3	17	7	446	3.46	13	5	ND	2	16	1	2	2	69	.23	.048	5	29	.67	67	.06	2	2.15	.02	.04	2	8
NMB 0+00N 6+50W	2	88	19	124	.4	19	9	511	3.22	38	5	ND	1	19	1	2	2	51	.29	.062	7	33	.62	109	.05	3	1.99	.03	.05	2	8
NMB 0+00N 6+00W	2	60	9	126	.2	16	9	766	3.73	30	5	ND	1	18	1	2	2	62	.22	.068	5	28	.74	59	.05	3	2.25	.03	.05	1	8
NMB 0+00N 5+50W	3	51	17	121	.1	16	6	478	3.39	29	5	ND	1	18	1	2	2	47	.42	.058	6	25	.58	71	.04	7	2.04	.03	.04	1	7
NMB 0+00N 5+00W	2	27	10	110	.2	10	6	522	3.34	14	6	ND	1	15	1	2	2	61	.12	.037	5	20	.52	51	.05	2	1.91	.02	.05	2	4
NMB 0+00N 4+50W	2	55	11	99	.4	19	8	483	3.32	15	5	ND	1	19	1	2	2	68	.28	.043	6	32	.62	81	.06	3	2.00	.03	.05	1	3
NMB 0+00N 4+00W	2	26	9	96	.2	12	8	737	3.04	12	5	ND	1	21	1	2	2	66	.31	.048	4	21	.55	56	.06	2	1.82	.03	.05	2	6
NMB 0+00N 3+50W	2	66	19	102	.5	21	7	526	2.87	13	5	ND	3	21	1	2	2	49	.32	.049	11	34	.48	113	.06	2	1.80	.03	.07	1	4
NMB 0+00N 3+00W	1	39	8	70	.1	22	11	543	3.56	8	5	ND	2	12	1	2	2	70	.25	.036	4	40	1.16	44	.12	3	2.39	.03	.03	1	1
NMB 0+00N 2+50W	2	29	9	88	.1	21	10	517	4.19	9	5	ND	1	14	1	2	2	94	.18	.047	4	39	.94	43	.10	3	2.69	.03	.03	2	1

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-10 SOIL P11-13 ROCK AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 29 1987 DATE REPORT MAILED: Nov 13/87 ASSAYER: D. J. DEAN TOYE, CERTIFIED B.C. ASSAYER

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SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NM-A L1+50W 0+60S	1	22	6	61	.1	8	7	234	3.84	12	5	ND	2	16	1	2	2	84	.25	.033	3	18	.50	34	.08	2	2.46	.01	.03	1	1
NM-A L1+50W 0+70S	1	36	9	69	.2	10	10	307	4.05	17	5	ND	2	14	1	2	2	76	.24	.043	3	22	.66	35	.09	4	3.13	.01	.03	1	1
NM-A L1+50W 0+80S	1	23	12	53	.1	9	7	198	3.44	11	5	ND	1	14	1	2	2	67	.22	.026	3	19	.48	27	.07	2	2.69	.01	.03	1	1
NM-A L1+50W 0+90S	1	16	4	43	.1	6	5	171	2.69	6	5	ND	1	15	1	2	2	64	.23	.020	3	15	.37	29	.07	3	1.82	.01	.03	2	2
NM-A L1+50W 1+00S	1	23	12	60	.1	7	7	224	3.54	12	5	ND	1	14	1	2	2	75	.21	.031	3	18	.49	32	.08	2	2.23	.01	.03	1	1
NM-A L1+25W 0+20S	2	24	12	63	.3	9	8	233	3.55	12	5	ND	1	15	1	2	2	73	.26	.024	3	20	.61	27	.06	2	2.57	.01	.03	1	1
NM-A L1+25W 0+40S	1	36	6	61	.1	10	9	265	4.13	20	5	ND	1	15	1	2	2	79	.25	.033	3	21	.62	31	.08	2	2.90	.01	.02	1	1
NM-A L1+25W 0+60S	1	45	13	61	.1	14	13	344	4.24	20	5	ND	1	13	1	2	2	78	.22	.029	3	26	.90	30	.10	2	3.39	.01	.03	1	2
NM-A L1+25W 0+80S	1	32	13	54	.1	10	9	276	3.80	14	5	ND	1	13	1	2	2	75	.22	.020	3	22	.66	35	.09	3	2.85	.01	.02	1	1
NM-A L1+25W 1+00S	1	31	6	65	.1	10	10	259	3.90	22	5	ND	2	13	1	3	2	69	.18	.027	3	21	.61	34	.09	2	3.07	.01	.02	1	1
NM-A L1+25W 1+20S	1	35	10	60	.1	12	11	291	4.13	19	5	ND	1	15	1	2	2	80	.26	.025	2	23	.75	31	.09	2	2.96	.01	.03	1	1
NM-A L1+25W 1+40S	1	29	6	54	.1	9	8	266	3.83	14	5	ND	1	16	1	2	2	77	.25	.023	3	21	.67	34	.09	4	2.45	.01	.03	2	1
NM-A L1+25W 1+60S	1	38	9	67	.1	13	12	317	4.24	22	5	ND	1	14	1	2	2	80	.26	.030	3	24	.84	33	.09	2	2.76	.01	.03	1	1
NM-A L1+25W 1+80S	2	40	11	65	.1	12	12	377	4.41	23	5	ND	1	18	1	2	2	80	.35	.024	2	24	.94	36	.09	5	2.82	.01	.02	1	1
NM-A L1+25W 2+00S	1	52	13	77	.1	11	17	665	4.55	24	5	ND	2	26	1	2	2	79	.54	.034	3	25	.99	36	.10	3	3.29	.01	.04	1	4
NM-A L1+00W 1+00N	1	39	12	66	.1	13	12	319	3.95	16	5	ND	2	15	1	2	2	72	.24	.035	3	24	.83	41	.08	2	3.26	.01	.03	1	5
NM-A L1+00W 0+80N	1	16	14	60	.1	6	6	329	2.54	9	5	ND	1	18	1	2	2	57	.32	.024	3	14	.43	47	.05	2	1.74	.01	.03	1	7
NM-A L1+00W 0+70N	1	19	10	75	.1	8	6	196	3.19	16	5	ND	1	12	1	2	2	63	.19	.028	3	17	.49	29	.05	2	2.01	.01	.03	1	1
NM-A L1+00W 0+60N	1	19	15	70	.1	7	6	247	3.03	13	5	ND	2	15	1	2	2	62	.23	.020	3	17	.50	42	.06	4	1.87	.01	.04	1	7
NM-A L1+00W 0+70S	1	37	23	63	.1	12	10	278	4.07	16	5	ND	1	15	1	2	2	77	.26	.024	3	23	.72	37	.09	2	2.86	.01	.02	1	5
NM-A L1+00W 0+80S	1	20	13	50	.1	7	7	232	3.27	12	5	ND	2	15	1	2	2	72	.25	.015	3	18	.54	38	.07	4	2.20	.01	.04	2	1
NMA L1+00W 0+90S	1	20	5	47	.1	6	6	198	3.23	9	5	ND	1	13	1	2	2	69	.19	.018	3	18	.46	25	.07	2	2.35	.01	.02	1	6
NMA L1+00W 1+00S	1	35	9	55	.1	11	11	284	4.16	20	5	ND	2	13	1	2	2	79	.21	.023	3	24	.73	36	.10	3	3.02	.01	.02	1	14
NMA L1+00W 1+20S	1	29	15	49	.1	8	8	242	3.62	16	5	ND	2	14	1	2	2	74	.24	.019	3	19	.60	36	.08	3	2.36	.01	.03	1	6
NMA L1+00W 1+40S	1	42	12	68	.1	13	13	468	4.15	22	5	ND	2	18	1	2	2	75	.33	.026	3	25	.91	48	.09	2	2.73	.01	.03	1	1
NMA L1+00W 1+60S	1	42	10	64	.1	12	13	408	4.21	19	5	ND	2	17	1	2	2	76	.33	.029	3	25	.91	32	.09	3	2.54	.01	.05	1	10
NMA L1+00W 1+80S	5	68	14	49	.2	10	26	667	5.22	16	5	ND	3	161	1	2	2	77	1.23	.028	2	19	.98	65	.10	3	4.33	.02	.03	2	5
NMA L1+00W 2+00S	1	57	15	81	.1	14	18	782	4.55	39	5	ND	2	41	1	2	2	76	.79	.039	4	24	1.09	53	.10	4	3.11	.02	.07	1	34
NMA L0+75W 1+00N	1	16	16	49	.1	6	5	239	2.68	14	5	ND	1	19	1	2	2	60	.27	.024	3	14	.40	38	.04	3	1.76	.01	.04	1	1
NMA L0+75W 0+80N	1	44	20	72	.3	15	13	412	4.03	19	5	ND	2	16	1	2	2	73	.24	.020	4	30	.95	44	.08	4	3.00	.01	.03	2	40
NMA L0+75W 0+60N	1	18	17	47	.1	6	6	185	2.99	11	5	ND	1	13	1	3	2	70	.18	.015	3	17	.45	34	.06	3	1.97	.01	.03	2	7
NMA L0+75W 0+40N	1	14	16	40	.1	4	4	161	2.45	9	5	ND	1	11	1	2	2	66	.16	.010	3	13	.35	31	.07	3	1.61	.01	.02	1	1
NMA L0+75W 0+20N	1	31	17	64	.1	8	9	290	3.77	16	5	ND	1	16	1	2	2	74	.23	.020	3	21	.65	35	.08	2	2.78	.01	.02	1	1
NMA 0+75W BL	2	33	19	57	.1	8	9	269	4.06	18	5	ND	2	14	1	2	2	82	.21	.021	3	20	.62	38	.07	2	2.73	.01	.03	1	1
NMA L0+75W 0+20S	1	40	26	77	.2	10	11	346	3.96	21	5	ND	2	11	1	2	2	73	.20	.019	3	21	.78	35	.05	4	2.97	.01	.03	1	1
NMA L0+75W 0+40S	2	20	14	48	.2	6	6	195	2.86	13	9	ND	1	12	1	2	2	66	.17	.015	3	15	.46	26	.06	5	1.98	.01	.02	2	1
NMA L0+75W 0+60S	2	21	18	49	.2	5	5	188	2.58	11	8	ND	1	11	1	2	2	57	.21	.024	3	14	.38	28	.05	4	1.66	.01	.03	1	7
STD C/AU-S	19	58	39	130	7.0	67	28	1040	4.12	39	20	7	37	49	17	17	21	55	.47	.083	37	58	.87	178	.06	37	1.93	.06	.13	13	47

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	V PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	HG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NMA LO+75W 0+80S	1	47	14	71	.3	13	14	351	4.60	39	5	ND	1	20	1	2	2	70	.36	.053	3	25	.80	22	.07	2	3.42	.01	.02	1	2
NMA LO+75W 1+00S	1	36	8	59	.1	12	10	306	4.10	15	5	ND	1	13	1	2	2	80	.25	.040	3	24	.76	26	.08	2	2.34	.01	.02	1	1
NMA LO+75W 1+20S	1	56	4	69	.1	11	20	804	4.72	15	5	ND	1	44	1	2	2	79	.64	.044	3	22	.92	42	.09	2	2.90	.01	.08	1	1
NMA LO+75W 1+40S	1	45	7	68	.1	12	13	463	4.11	16	5	ND	1	27	1	2	2	73	.45	.035	3	25	.88	41	.09	4	2.91	.01	.03	1	1
NMA LO+75W 1+60S	2	63	23	67	.1	14	17	626	5.48	21	5	ND	1	42	1	2	2	79	.50	.032	4	24	.98	41	.11	2	3.21	.01	.02	1	3
NMA LO+75W 1+80S	1	39	10	62	.1	12	12	374	3.85	13	5	ND	1	15	1	2	2	73	.28	.021	3	24	.89	36	.09	2	2.45	.01	.03	1	1
NMA LO+75W 2+00S	1	38	8	56	.1	12	12	355	3.89	8	5	ND	1	13	1	2	4	75	.19	.017	4	25	.88	39	.10	2	2.45	.01	.01	1	1
NMA LO+50W 0+90N	1	45	19	76	.1	14	13	540	4.37	20	5	ND	1	15	1	2	2	78	.30	.025	3	25	.97	35	.08	3	2.50	.01	.03	1	1
NMA LO+50W 0+80N	1	32	17	70	.1	9	9	371	3.89	17	5	ND	1	14	1	2	2	74	.25	.025	2	21	.81	33	.06	2	2.30	.01	.02	1	2
NMA LO+50W 0+60N	1	35	13	60	.1	12	10	305	4.09	17	5	ND	1	12	1	2	2	79	.20	.022	3	24	.77	34	.09	3	2.61	.01	.02	1	4
NMA LO+50W 0+40N	1	40	12	70	.2	11	11	359	4.20	20	5	ND	1	13	1	2	2	80	.24	.022	3	22	.80	39	.08	3	2.69	.01	.03	1	1
NMA LO+50W 0+40S	1	30	19	56	.1	9	8	258	3.72	17	5	ND	1	13	1	2	2	75	.24	.014	3	20	.62	33	.06	3	2.03	.01	.03	1	1
NMA LO+50W 0+60S	1	46	11	59	.1	16	13	356	4.11	13	5	ND	1	14	1	3	3	74	.25	.021	3	29	.95	40	.10	2	2.86	.01	.02	1	1
NMA LO+50W 0+80S	1	34	18	56	.1	9	9	307	3.54	25	5	ND	1	18	1	2	2	64	.37	.030	3	18	.62	38	.07	2	2.03	.01	.03	1	7
NMA LO+50W 1+00S	1	45	15	68	.2	13	14	550	4.17	54	5	ND	1	23	1	2	2	74	.61	.039	4	26	.88	22	.08	3	2.39	.02	.03	1	3
NMA LO+50W 1+20S	1	47	9	67	.1	13	13	570	3.98	12	5	ND	1	21	1	2	3	72	.36	.033	4	26	.98	36	.09	2	2.42	.01	.02	1	2
NMA LO+50W 1+40S	1	39	9	63	.1	13	11	321	4.11	16	5	ND	1	13	1	2	2	78	.20	.020	3	25	.83	36	.09	2	2.72	.01	.02	1	5
NMA LO+50W 1+60S	1	32	13	61	.1	11	10	382	3.85	13	5	ND	1	12	1	2	2	76	.21	.022	3	23	.77	34	.08	2	2.47	.01	.02	1	2
NMA LO+50W 1+80S	1	42	11	66	.1	13	12	509	4.20	17	5	ND	1	14	1	2	2	79	.25	.032	3	27	.91	42	.10	6	2.84	.01	.03	1	1
NMA LO+50W 2+00S	1	35	3	61	.1	12	11	503	3.76	10	5	ND	1	15	1	2	3	73	.30	.033	3	23	.81	40	.09	2	2.17	.01	.03	1	1
NMA LO+25W 1+00S	1	52	6	78	.1	15	18	856	4.91	25	5	ND	1	22	1	2	2	89	.47	.029	4	31	1.19	33	.10	2	2.67	.01	.04	1	2
NMA LO+25W 1+20S	1	46	34	80	.2	13	13	592	4.51	25	5	ND	1	17	1	2	2	75	.33	.036	4	26	.94	43	.08	3	2.61	.01	.04	1	1
NMA LO+25W 1+40S	1	44	11	69	.1	14	14	610	4.03	19	5	ND	1	15	1	2	2	73	.28	.031	3	26	.96	37	.09	3	2.61	.01	.03	1	4
NMA LO+25W 1+60S	1	44	9	71	.1	13	14	503	4.36	18	5	ND	1	18	1	2	2	78	.32	.025	3	25	.95	34	.08	2	2.69	.01	.03	1	1
NMA LO+25W 1+80S	1	50	11	102	.1	14	14	860	4.43	29	5	ND	3	21	1	2	2	78	.56	.097	6	24	1.08	86	.15	3	2.29	.01	.24	1	3
NMA LO+25W 2+00S	1	51	9	74	.1	14	15	689	4.31	31	5	ND	1	35	1	2	2	71	.52	.038	6	26	.90	48	.11	2	2.49	.01	.05	1	21
NMA LO+00E 1+00N	1	31	18	129	.1	12	13	535	3.78	20	5	ND	1	23	1	2	2	65	.45	.034	3	23	.74	48	.06	3	2.41	.01	.04	1	26
NMA LO+00E 0+80N	1	36	18	94	.1	12	13	718	4.00	14	5	ND	1	17	1	2	2	72	.36	.038	3	23	.76	64	.06	2	2.50	.01	.03	1	11
NMA LO+00E 0+60N	1	54	14	76	.2	16	18	797	4.55	24	5	ND	1	21	1	3	3	79	.38	.027	4	29	1.13	57	.10	2	2.92	.01	.02	1	42
NMA LO 0+60S	1	52	18	75	.2	13	13	974	4.05	21	5	ND	1	33	1	2	2	70	1.17	.033	3	24	.85	86	.07	2	3.66	.01	.03	1	5
NMA LO 0+80S	1	49	13	72	.1	15	15	609	4.72	19	5	ND	1	21	1	2	2	87	.38	.024	4	30	.99	49	.09	3	2.94	.01	.03	1	2
NMA LO 1+00S	1	48	6	77	.1	15	15	441	4.82	20	5	ND	1	19	1	2	3	87	.30	.019	3	31	1.06	36	.10	2	3.12	.01	.02	1	1
NMA LO 1+20S	1	57	12	92	.2	15	15	574	4.69	22	5	ND	1	21	1	2	2	82	.68	.030	5	29	1.10	46	.07	2	3.03	.02	.03	1	110
NMA LO 1+60S	4	152	169	250	1.3	22	55	4353	6.80	96	5	ND	1	17	3	7	4	59	.33	.048	5	16	.73	34	.05	2	2.10	.01	.05	1	93
NMA LO 1+80S	5	219	91	314	3.4	13	49	3872	11.40	85	8	ND	1	12	4	15	4	46	.26	.095	5	8	.63	24	.02	2	1.91	.01	.06	1	27
NMA LO 2+00S	1	115	16	102	.2	15	19	1025	6.04	13	5	ND	2	84	1	2	2	60	1.11	.057	2	15	.78	51	.07	2	4.84	.03	.05	1	11
STD C/AU-S	18	60	44	133	7.3	69	28	1132	4.26	39	16	B	39	52	18	16	20	57	.49	.088	38	61	.90	180	.07	30	1.81	.07	.14	10	53

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BT PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# FPB
NMA L0+25E 1+00N	1	40	19	112	.1	14	14	444	4.35	21	5	ND	1	20	1	2	2	87	.36	.022	3	27	.84	52	.08	12	3.30	.01	.05	1	5
NMA L0+25E 0+80N	2	32	14	97	.1	11	13	388	3.87	40	5	ND	1	20	1	2	2	71	.39	.027	3	23	.71	52	.05	7	2.86	.01	.05	1	1
NMA L0+25E 0+60N	1	34	9	98	.2	9	11	768	3.67	8	5	ND	1	19	1	2	2	68	.48	.088	3	20	.62	55	.08	6	2.64	.01	.09	1	2
NMA L0+25E 0+40N	2	31	17	135	.1	12	13	360	4.03	17	5	ND	1	17	1	2	2	77	.35	.031	3	23	.71	60	.07	6	2.91	.01	.05	1	3
NMA L0+25E 0+40S	2	32	17	117	1.4	10	11	377	4.40	20	5	ND	1	15	1	2	2	84	.27	.038	3	23	.71	32	.05	6	2.68	.01	.05	1	62
NMA L0+25E 0+80S	1	50	12	80	.1	10	10	464	3.97	9	5	ND	1	17	1	2	2	79	.32	.032	3	22	.67	42	.04	7	2.71	.01	.05	1	1
STD C/AU-S	19	59	37	127	7.3	64	29	1073	3.95	38	18	8	38	50	18	16	21	57	.49	.088	39	60	.88	174	.07	34	1.91	.06	.14	14	47
NMA L0+25E 0+80S	1	41	10	79	.1	13	13	707	4.46	14	5	ND	1	18	1	2	2	82	.33	.030	3	26	.78	39	.07	6	3.24	.01	.05	1	2
NMA L0+25E 1+00S	1	35	7	72	.1	15	13	382	4.27	5	5	ND	1	18	1	2	2	88	.30	.024	3	27	.75	36	.09	4	3.05	.01	.04	1	3
NMA L0+25E 1+20S	1	28	6	64	.1	11	11	528	3.80	4	5	ND	1	24	1	2	2	86	.42	.020	3	26	.70	40	.09	5	2.65	.01	.04	1	1
NMA L0+25E 1+40S	1	59	17	90	.2	16	20	752	5.41	24	5	ND	1	29	1	2	2	102	.55	.029	5	37	1.24	38	.13	6	3.38	.02	.04	1	3
NMA L0+25E 1+60S	1	53	9	69	.1	15	18	652	4.91	18	5	ND	1	27	1	2	2	99	.43	.023	4	34	1.15	40	.13	6	3.39	.01	.03	1	6
NMA L0+25E 1+80S	1	60	12	76	.1	17	22	814	5.56	24	5	ND	1	28	1	2	2	104	.51	.033	3	37	1.30	36	.12	4	3.54	.01	.06	1	430
NMA L0+25E 2+00S	1	51	11	72	.1	16	19	1000	4.73	14	5	ND	1	27	1	2	2	93	.54	.060	4	34	1.12	49	.10	6	3.39	.01	.07	1	1
NMA L0+50E 1+00N	2	16	15	92	.4	6	8	246	3.38	18	5	ND	1	16	1	2	2	61	.27	.050	3	18	.39	36	.03	4	2.44	.01	.06	1	102
NMA L0+50E 0+80N	3	31	20	89	.1	9	13	408	3.69	40	5	ND	1	21	1	2	2	58	.52	.031	3	15	.61	39	.02	4	2.72	.01	.07	1	1
NMA L0+50E 0+60N	1	31	10	105	.1	13	13	363	4.04	22	5	ND	1	17	1	2	2	75	.28	.027	3	25	.70	45	.07	6	2.84	.01	.04	1	10
NMA L0+50E 0+40N	1	55	16	78	.3	16	17	420	4.66	34	5	ND	1	27	1	2	2	77	.44	.029	3	28	.99	47	.07	6	3.90	.01	.05	1	5
NMA L0+50E 0+40S	1	50	11	90	.1	15	14	619	4.63	29	5	ND	1	21	1	2	2	83	.44	.029	3	27	.81	48	.03	5	3.41	.01	.06	1	45
NMA L0+50E 0+60S	2	33	26	109	.1	9	12	571	4.68	19	5	ND	1	18	1	2	2	87	.36	.029	3	24	.72	42	.05	4	2.97	.01	.05	1	2
NMA L0+50E 1+00S	2	38	12	83	.1	14	14	937	4.34	7	5	ND	1	19	1	2	2	87	.35	.040	4	26	.84	60	.07	6	3.18	.01	.06	1	1
NMA L0+50E 1+20S	1	35	8	78	.1	14	13	437	4.10	6	5	ND	1	19	1	2	2	86	.32	.023	3	28	.87	43	.10	9	3.08	.01	.05	1	1
NMA L0+50E 1+40S	1	29	8	66	.1	12	13	304	3.99	3	5	ND	1	20	1	2	2	90	.32	.023	3	30	.81	30	.11	5	3.08	.01	.04	1	37
NMA L0+50E 1+60S	1	39	5	72	.1	16	13	351	4.29	13	5	ND	1	18	1	2	2	86	.28	.031	3	30	.91	32	.10	6	3.40	.01	.05	1	2
NMA L0+50E 1+80S	1	33	3	61	.1	13	12	300	4.09	9	5	ND	1	16	1	2	2	85	.22	.029	3	29	.78	29	.09	3	3.24	.01	.03	1	44
NMA L0+50E 2+00S	1	42	6	63	.2	13	14	368	4.39	20	5	ND	1	17	1	2	2	83	.25	.037	3	29	.87	36	.08	7	3.62	.01	.03	1	3
NMA L0+75E 1+00N	2	29	11	78	.2	8	10	256	3.82	40	5	ND	1	15	1	2	2	61	.20	.032	3	18	.66	34	.02	5	2.79	.01	.05	1	1
NMA L0+75E 0+80N	1	16	9	49	.4	6	5	172	2.64	11	5	ND	1	14	1	2	2	54	.18	.018	4	17	.38	25	.05	4	2.15	.01	.04	1	1
NMA L0+75E 0+60N	1	28	31	107	.5	11	11	281	3.68	30	5	ND	1	18	1	2	2	67	.21	.027	3	23	.64	31	.05	3	2.89	.01	.04	1	6
NMA L0+75E 0+40N	1	25	16	100	.1	10	11	271	3.66	18	5	ND	1	18	1	2	2	71	.22	.021	3	22	.63	32	.07	6	2.87	.01	.04	1	1
NMA L0+75E 0+40S	2	42	14	70	.2	12	16	645	4.63	48	5	ND	1	22	1	2	2	83	.36	.025	3	24	.76	42	.06	2	3.08	.01	.05	1	2
NMA L0+75E 0+60S	3	51	12	97	.1	15	15	375	4.76	21	5	ND	1	19	1	2	2	80	.31	.030	4	25	.68	51	.07	3	3.87	.01	.05	1	5
NMA L0+75E 0+80S	3	72	179	1020	.4	16	16	701	4.83	41	5	ND	1	16	1	4	2	70	.43	.027	4	24	.95	64	.02	8	3.69	.01	.07	1	4
NMA L0+75E 1+00S	2	41	17	88	.1	15	13	551	4.47	11	5	ND	6	16	1	2	2	92	.32	.028	4	30	.89	49	.08	5	3.36	.01	.05	1	1
NMA L0+75E 1+20S	1	38	9	67	.1	15	13	341	4.32	7	5	ND	1	17	1	3	2	91	.28	.016	4	34	.92	36	.10	6	3.31	.01	.04	1	2
NMA L0+75E 1+40S	1	25	8	66	.1	13	11	302	3.83	3	5	ND	1	19	1	2	2	85	.28	.015	3	29	.77	33	.10	5	2.92	.01	.04	1	1
NMA L0+75E 1+60S	1	27	4	86	.1	13	13	296	3.80	4	5	ND	1	20	1	2	2	81	.26	.019	3	30	.83	33	.11	5	3.22	.01	.04	1	1

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM	
NMA L0+75E 1+80S	1	21	10	52	.1	10	8	232	3.45	9	5	ND	1	17	1	2	2	76	.24	.021	3	26	.59	28	.08	4	2.43	.01	.04	1	1
NMA L0+75E 2+00S	1	28	10	58	.1	11	10	337	3.67	12	5	ND	1	17	1	5	2	79	.23	.021	4	24	.68	31	.09	2	2.74	.01	.04	2	48
NMA L1+00E 1+00N	1	22	15	61	.4	8	8	215	3.08	19	5	ND	1	13	1	2	2	60	.20	.024	3	18	.56	29	.05	2	2.58	.01	.04	1	1
NMA L1+00E 0+80N	1	42	18	70	.5	11	13	304	4.38	57	5	ND	1	13	1	3	2	68	.21	.028	3	21	.73	41	.04	4	3.23	.01	.04	1	1
NMA L1+00E 0+60N	1	24	17	71	.1	11	10	259	3.85	24	5	ND	1	14	1	2	2	72	.21	.023	3	21	.64	27	.06	2	2.73	.01	.03	1	5
NMA L1+00E 0+40N	1	23	11	66	.1	8	9	247	3.58	18	5	ND	1	14	1	2	2	72	.20	.020	3	20	.55	32	.06	4	2.47	.01	.04	1	1
NMA L1+00E 0+40S	1	29	21	58	.3	9	10	266	3.86	28	5	ND	1	15	1	2	2	75	.25	.019	3	20	.62	36	.03	4	2.82	.01	.05	1	7
NMA L1+00E 0+60S	2	33	18	59	.1	12	11	285	3.93	19	5	ND	1	16	1	2	2	80	.25	.018	3	25	.74	38	.10	3	3.27	.01	.03	2	1
NMA L1+00E 0+80S	1	32	11	65	.1	11	11	463	3.96	15	5	ND	1	16	1	3	2	85	.26	.021	4	25	.72	50	.08	4	2.84	.01	.04	1	3
NMA L1+00E 1+00S	1	35	13	65	.1	13	12	357	4.15	13	5	ND	1	15	1	2	2	89	.25	.021	3	28	.89	37	.10	2	3.12	.01	.04	1	21
NMA L1+00E 1+20S	1	30	8	63	.1	14	13	376	4.18	10	5	ND	1	21	1	2	2	93	.33	.019	3	30	.96	38	.11	5	3.05	.01	.04	1	6
NMA L1+00E 1+40S	1	26	8	73	.1	12	12	336	3.53	6	5	ND	1	17	1	2	2	76	.28	.018	2	27	.90	32	.10	4	3.09	.01	.03	1	1
NMA L1+00E 1+60S	1	32	12	77	.1	14	15	340	4.02	49	5	ND	1	17	1	2	2	79	.26	.019	3	27	.83	39	.07	2	3.07	.01	.04	1	10
NMA L1+00E 1+80S	1	40	7	63	.1	17	14	327	4.36	15	5	ND	2	18	1	4	2	90	.28	.021	3	38	1.12	42	.11	3	3.45	.01	.03	1	2
NMA L1+00E 2+00S	1	27	13	57	.1	12	11	271	3.53	7	5	ND	1	14	1	2	2	77	.20	.018	3	25	.72	32	.10	4	2.84	.01	.05	1	4
NMA L1+25E 1+00N	2	18	14	48	.2	6	6	194	2.82	14	5	ND	1	15	1	2	2	62	.23	.018	3	16	.47	29	.04	2	2.06	.01	.03	2	3
NMA L1+25E 0+80N	1	29	17	60	.5	10	9	245	3.56	23	5	ND	1	14	1	2	2	62	.19	.024	4	21	.61	31	.07	3	2.90	.01	.04	1	2
NMA L1+25E 0+60N	1	26	26	64	.1	10	10	281	3.90	25	5	ND	1	15	1	2	2	79	.20	.023	3	23	.65	33	.06	4	2.68	.01	.05	1	4
NMA L1+25E 0+40N	1	30	18	66	.3	12	10	252	4.14	20	5	ND	1	16	1	2	2	80	.21	.022	3	25	.67	35	.07	2	2.96	.01	.03	1	3
NMA L1+25E 0+40S	1	30	9	58	.2	11	10	242	3.83	13	5	ND	1	14	1	2	2	79	.20	.026	3	25	.66	32	.09	2	3.03	.01	.04	1	1
NMA L1+25E 0+60S	1	32	11	58	.1	14	11	284	4.04	10	5	ND	1	14	1	2	2	89	.19	.019	3	28	.86	33	.11	5	3.10	.01	.03	1	3
NMA L1+25E 0+80S	1	24	8	51	.2	13	9	230	3.40	7	5	ND	1	14	1	2	2	79	.20	.015	3	25	.74	34	.10	2	2.94	.01	.03	1	2
NMA L1+25E 1+00S	1	25	10	53	.1	11	9	248	3.51	5	5	ND	1	14	1	2	2	79	.18	.013	3	25	.73	32	.11	5	2.80	.01	.03	1	1
NMA L1+25E 1+20S	1	28	15	58	.1	13	11	268	3.79	10	5	ND	1	13	1	2	2	79	.17	.026	3	27	.80	44	.10	2	3.15	.01	.03	1	8
NMA L1+25E 1+40S	1	36	15	69	.1	15	14	405	4.18	7	5	ND	1	18	1	2	2	90	.28	.021	3	33	1.06	48	.10	3	3.52	.01	.03	1	4
NMA L1+25E 1+60S	1	31	5	61	.1	14	12	273	3.78	5	5	ND	1	16	1	2	2	80	.24	.021	3	31	.94	35	.11	5	3.00	.01	.03	1	2
NMA L1+25E 1+80S	1	25	13	62	.1	12	11	238	3.47	5	5	ND	1	16	1	2	2	73	.23	.030	3	27	.72	29	.10	4	2.97	.01	.04	1	1
NMA L1+25E 2+00S	1	27	10	69	.1	13	12	519	3.79	6	5	ND	1	17	1	2	2	81	.24	.024	3	30	.88	38	.11	4	2.96	.01	.04	1	4
NMA L1+50E 0+40S	1	26	9	51	.1	12	9	259	3.57	10	5	ND	1	15	1	2	2	77	.18	.015	3	27	.84	35	.11	2	2.79	.01	.02	1	3
NMA L1+50E 0+60S	1	28	10	51	.3	11	10	269	3.77	12	5	ND	2	15	1	2	2	81	.20	.022	3	27	.71	33	.09	4	2.87	.01	.03	1	1
NMA L1+50E 0+80S	1	32	9	62	.1	13	10	297	3.87	18	5	ND	1	14	1	2	2	77	.20	.030	3	26	.75	26	.08	2	2.87	.01	.03	1	2
NMA L1+50E 1+00S	1	25	9	54	.2	11	9	241	3.51	12	5	ND	1	14	1	2	2	73	.18	.025	3	23	.64	32	.08	4	2.79	.01	.03	1	9
NMA L1+50E 1+20S	1	29	8	55	.1	12	9	275	3.58	10	5	ND	1	14	1	2	2	74	.17	.023	3	26	.72	35	.08	4	2.87	.01	.02	1	5
NMA L1+50E 1+40S	1	23	8	48	.1	10	9	232	3.33	8	5	ND	1	15	1	2	2	78	.20	.017	3	24	.66	31	.10	5	2.62	.01	.02	1	1
NMA L1+50E 1+60S	1	20	13	48	.1	10	8	208	3.21	9	5	ND	1	16	1	2	2	74	.20	.017	3	24	.64	35	.09	3	2.44	.01	.02	2	1
NMA L1+50E 1+80S	1	37	5	58	.1	16	14	299	4.10	6	5	ND	1	19	1	2	2	87	.21	.016	3	34	1.10	43	.13	4	3.52	.01	.02	1	1
STD C/AU-S	18	59	39	132	7.4	68	29	1035	4.07	41	20	8	39	52	18	18	19	57	.48	.084	39	61	.90	179	.07	32	1.91	.07	.14	10	49

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE PPM	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA PPM	P PPM	LA PPM	CR PPM	MG PPM	BA PPM	TI PPM	B PPM	AL PPM	NA PPM	K PPM	W PPM	AU# PPB
NMA L1+50E 2+00S	1	35	8	63	.1	17	13	308	3.88	4	5	ND	1	17	1	2	2	81	.22	.032	3	30	.98	43	.12	2	3.19	.01	.03	1	4
NMA L1+75E 0+60S	1	19	2	37	.4	6	5	167	2.59	8	5	ND	2	17	1	2	2	63	.20	.022	3	18	.41	30	.05	2	2.03	.01	.04	3	2
NMA L1+75E 0+80S	1	34	9	52	.2	13	10	292	3.86	25	5	ND	2	16	1	2	2	78	.22	.029	4	24	.72	38	.08	4	2.93	.01	.03	1	8
NMA L1+75E 1+00S	1	32	2	54	.2	15	12	265	3.74	13	5	ND	2	14	1	2	2	79	.19	.018	3	25	.84	39	.10	5	3.10	.01	.02	1	1
NMA L1+75E 1+20S	1	33	2	55	.1	14	11	303	3.86	14	5	ND	1	13	1	2	2	80	.18	.027	3	25	.79	34	.09	2	3.03	.01	.03	1	1
NMA L1+75E 1+40S	1	31	2	51	.1	15	10	254	3.49	7	5	ND	1	14	1	2	2	76	.18	.019	3	27	.82	32	.10	3	2.95	.01	.02	1	7
NMA L1+75E 1+60S	1	27	2	61	.1	13	11	259	3.54	6	5	ND	1	15	1	2	2	78	.21	.021	3	25	.76	30	.11	3	3.06	.01	.03	1	3
NMA L1+75E 1+80S	1	29	8	57	.1	13	10	281	3.70	11	5	ND	1	17	1	2	2	79	.22	.033	3	26	.73	33	.09	4	2.96	.01	.03	1	1
NMA L1+75E 2+00S	1	40	7	60	.1	17	14	385	4.19	6	5	ND	2	22	1	2	2	92	.26	.018	3	33	1.15	49	.12	2	3.17	.01	.03	1	1
NMA L3E 1+00N	1	62	20	126	.8	16	16	414	5.36	31	5	ND	2	17	1	2	2	85	.13	.048	3	24	.70	28	.07	5	3.37	.01	.06	1	2
NMA L3E 0+80N	1	62	19	88	.6	13	14	347	5.33	25	5	ND	2	12	1	2	2	82	.09	.043	3	23	.64	30	.05	4	3.20	.01	.05	1	32
NMA L3E 0+60N	1	26	14	71	.3	10	9	262	3.89	12	5	ND	2	15	1	2	2	81	.17	.026	3	21	.57	28	.06	2	2.69	.01	.05	1	1
NMA L3E 0+40N	1	52	3	71	.3	16	16	372	4.91	23	5	ND	2	14	1	2	3	91	.17	.028	3	29	.95	44	.09	2	3.50	.01	.04	1	1
NMA L3E 0+40S	1	44	4	66	.1	17	15	347	4.46	13	5	ND	1	17	1	2	2	93	.21	.020	3	33	1.10	44	.12	4	3.37	.01	.03	1	1
NMA L3E 0+60S	1	31	6	61	.2	13	12	280	3.65	10	5	ND	1	14	1	2	2	78	.18	.023	3	25	.75	32	.10	4	3.07	.01	.03	1	1
NMA L3E 0+80S	1	44	9	58	.2	15	15	334	4.22	16	5	ND	2	14	1	2	2	84	.17	.015	3	31	1.08	40	.12	2	3.37	.01	.03	1	5
NMA L3E 1+00S	1	34	12	57	.1	13	12	275	3.85	15	5	ND	1	14	1	2	2	79	.19	.024	3	26	.79	29	.10	2	3.15	.01	.02	1	12
NMA L3E 1+20S	1	36	8	59	.2	14	11	270	3.60	18	5	ND	1	12	1	2	2	71	.15	.028	3	24	.73	33	.09	2	3.01	.01	.03	1	118
NMA L3E 1+40S	1	27	5	56	.2	10	9	272	3.46	23	5	ND	1	12	1	2	2	69	.16	.031	3	20	.58	30	.07	2	2.66	.01	.02	1	130
NMA L3E 1+60S	1	29	3	51	.3	12	9	256	3.30	27	5	ND	2	11	1	2	2	61	.17	.036	4	21	.59	32	.06	2	2.69	.01	.03	1	34
NMA L3E 1+80S	1	30	6	57	.1	13	11	280	3.68	21	5	ND	1	12	1	2	2	71	.19	.034	3	23	.68	36	.07	5	3.26	.01	.03	1	13
NMA L3E 2+00S	1	35	3	61	.4	14	12	299	3.90	12	5	ND	2	13	1	2	2	78	.22	.040	3	25	.89	41	.09	2	3.47	.01	.03	1	1
NMA L3+25E 1+00N	1	75	47	221	.3	20	23	600	6.38	29	5	ND	1	18	1	2	2	99	.16	.042	3	28	.85	42	.09	2	4.06	.01	.05	1	3
NMA L3+25E 0+80N	1	69	25	146	.4	18	20	516	5.65	39	5	ND	2	17	1	2	2	87	.16	.041	3	26	.78	44	.08	4	3.90	.01	.06	1	16
NMA L3+25E 0+60N	1	53	20	91	.4	14	11	342	5.43	27	5	ND	2	14	1	2	2	92	.11	.035	3	24	.63	39	.05	2	3.48	.01	.05	1	2
NMA L3+25E 0+40N	1	58	15	97	.4	16	17	408	4.92	24	5	ND	1	11	1	2	2	86	.13	.032	3	26	.82	34	.08	6	3.63	.01	.05	1	3
NMA L3+25E 0+20N	1	30	11	60	.3	12	10	254	3.51	10	5	ND	1	14	1	2	2	76	.18	.019	3	23	.64	28	.08	4	2.65	.01	.04	1	16
NMA L3+25E BL	1	32	3	60	.1	15	13	276	4.01	9	5	ND	2	13	1	2	2	88	.18	.023	2	27	.86	35	.10	3	3.16	.01	.04	1	3
NMA L3+25E 0+20S	1	36	7	59	.2	14	13	289	4.18	13	5	ND	1	14	1	3	2	87	.18	.027	3	26	.77	28	.09	2	3.14	.01	.04	1	19
NMA L3+25E 0+40S	1	44	5	56	.3	17	15	317	4.34	14	5	ND	1	15	1	2	2	86	.18	.026	3	28	.94	38	.09	3	3.39	.01	.03	2	1
NMA L3+25E 0+60S	1	35	4	53	.1	16	13	305	4.36	9	5	ND	1	15	1	2	2	94	.19	.023	3	29	.95	42	.10	4	3.23	.01	.02	1	13
NMA L3+25E 0+80S	1	26	6	59	.3	14	11	257	3.54	7	5	ND	2	16	1	3	2	77	.20	.025	3	24	.70	29	.09	3	3.01	.01	.04	1	1
NMA L3+25E 1+00S	1	31	4	58	.2	13	12	266	3.68	12	5	ND	1	13	1	2	2	80	.17	.026	3	24	.74	28	.10	5	3.15	.01	.03	2	2
NMA L3+25E 1+20S	1	27	6	49	.2	11	10	245	3.41	15	5	ND	1	13	1	2	2	71	.18	.024	3	21	.64	33	.08	4	2.86	.01	.03	1	35
NMA L3+25E 1+40S	1	32	5	58	.5	13	10	250	3.52	24	5	ND	1	11	1	2	2	64	.18	.041	3	21	.58	30	.07	3	3.13	.01	.03	1	52
NMA L3+25E 1+60S	1	22	9	42	.2	12	8	222	2.80	20	6	ND	2	11	1	3	2	52	.19	.025	4	18	.53	33	.06	3	2.24	.01	.03	2	1
STD C/AU-S	19	60	41	131	7.4	71	30	1079	4.05	41	21	8	38	54	19	17	23	59	.48	.088	40	58	.89	180	.07	34	1.92	.07	.13	13	47

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM	PPB
NMA L3+25E 1+80S	1	35	3	58	.1	14	12	298	4.03	6	5	ND	1	12	1	2	2	88	.20	.026	2	26	.96	44	.10	3	3.66	.01	.02	1	1
NMA L3+25E 2+00S	1	42	2	62	.1	15	15	354	4.46	7	5	ND	1	13	1	2	2	95	.22	.027	3	30	1.19	48	.11	4	3.97	.01	.02	1	78
NMA L3+50E 1+00N	1	75	247	125	1.9	11	13	360	5.68	29	5	ND	1	12	1	2	2	99	.11	.043	3	21	.67	37	.05	3	3.97	.01	.08	1	3
NMA L3+50E 0+80N	1	79	101	108	.4	14	12	454	6.24	29	5	ND	1	20	1	2	2	93	.12	.044	4	26	.84	31	.08	2	3.30	.01	.04	1	15
NMA L3+50E 0+80N	1	54	86	109	1.5	13	13	380	5.20	24	5	ND	1	16	1	2	2	87	.15	.038	3	22	.70	42	.05	2	3.36	.01	.06	1	27
NMA L3+50E 0+60S	1	48	7	67	.2	16	15	384	4.83	8	5	ND	1	17	1	2	2	105	.25	.022	3	34	1.32	48	.12	2	4.14	.01	.02	1	1
NMA L3+50E 0+90S	1	28	5	57	.1	10	10	371	3.75	6	5	ND	1	16	1	2	2	83	.23	.023	4	25	.76	35	.09	2	2.93	.01	.03	1	1
NMA L3+50E 1+00S	1	34	3	70	.2	15	12	289	4.00	8	5	ND	1	14	1	5	2	86	.22	.027	3	27	.91	32	.10	7	3.76	.01	.03	1	1
NMA L3+50E 1+20S	1	36	4	64	.1	13	12	297	4.23	11	5	ND	1	14	1	3	2	87	.22	.028	3	27	.90	37	.10	2	3.70	.01	.03	1	1
NMA L3+50E 1+40S	1	39	2	59	.1	13	12	334	4.27	35	5	ND	1	13	1	2	2	79	.21	.036	4	24	.82	34	.07	3	3.35	.01	.04	1	1
NMA L3+50E 1+60S	1	28	11	59	.3	11	10	274	3.68	15	5	ND	1	14	1	4	2	71	.21	.032	4	22	.69	35	.07	3	3.17	.01	.04	1	2
NMA L3+50E 1+80S	1	24	2	54	.1	11	10	264	3.68	16	5	ND	1	14	1	2	2	80	.24	.021	4	22	.75	36	.06	2	2.94	.01	.03	1	1
NMA L3+50E 2+00S	1	42	2	64	.1	15	14	360	4.39	7	5	ND	1	13	1	2	2	92	.20	.030	2	31	1.18	45	.11	5	4.12	.01	.02	1	1
NMA L3+75E 1+00N	1	42	41	70	.7	8	7	250	4.37	19	5	ND	1	12	1	2	2	80	.10	.028	3	15	.47	37	.04	2	2.98	.01	.06	1	4
NMA L3+75E 0+80N	2	98	417	146	.6	11	10	392	6.82	40	5	ND	1	16	1	3	2	92	.09	.057	4	20	.63	40	.05	4	3.24	.02	.06	1	1
NMA L3+75E 0+60N	1	46	35	89	.2	12	10	311	4.81	20	5	ND	1	14	1	2	2	90	.14	.030	3	20	.59	40	.05	2	3.45	.01	.06	1	3
NMA L3+75E 0+40N	1	49	16	82	.1	12	12	337	4.72	21	5	ND	1	15	1	2	2	83	.15	.033	3	19	.64	38	.06	3	3.22	.01	.04	1	2
NMA L3+75E 0+20N	1	35	9	112	.3	11	12	485	3.73	6	5	ND	1	17	1	3	2	94	.32	.045	4	23	.76	32	.11	6	2.93	.01	.06	1	1
NMA L3+75E 0+20S	1	41	8	68	.6	17	16	359	4.51	7	5	ND	1	15	1	2	3	96	.23	.025	2	32	1.14	35	.10	2	3.73	.01	.04	1	2
NMA L3+75E 0+40S	1	39	5	71	.2	18	15	374	4.33	8	5	ND	1	16	1	2	2	87	.25	.031	3	31	1.17	34	.08	2	3.57	.01	.04	1	4
NMA L3+75E 0+60S	1	25	3	59	.1	13	11	346	3.83	5	5	ND	1	17	1	2	2	84	.30	.042	3	26	.85	31	.09	3	3.06	.01	.05	1	3
NMA L3+75E 0+80S	1	34	10	63	.1	14	13	318	4.43	10	5	ND	1	19	1	2	2	91	.26	.030	3	26	.92	36	.08	3	3.55	.01	.04	1	1
NMA L3+75E 1+00S	1	25	7	60	.1	13	10	287	3.96	3	5	ND	1	19	1	2	2	89	.28	.030	3	25	.83	31	.09	5	3.24	.01	.04	1	1
NMA L3+75E 1+20S	1	32	2	58	.2	13	11	295	4.11	17	5	ND	1	14	1	2	2	85	.20	.030	3	25	.87	36	.08	5	3.31	.01	.03	1	8
NMA L3+75E 1+40S	1	24	6	50	.1	10	8	235	3.42	48	5	ND	1	13	1	4	2	59	.20	.036	5	20	.57	34	.05	3	2.93	.01	.03	1	5
NMA L3+75E 1+60S	1	23	5	61	.2	9	8	284	3.79	23	5	ND	1	14	1	2	2	77	.25	.026	3	18	.60	34	.04	4	2.81	.01	.05	1	3
NMA L3+75E 1+80S	1	26	3	58	.1	11	10	257	3.45	25	5	ND	1	12	1	2	2	71	.18	.021	3	21	.68	38	.04	3	3.29	.01	.03	1	4
NMA L3+75E 2+00S	1	32	5	63	.1	13	10	297	3.85	7	5	ND	1	14	1	2	2	81	.22	.039	3	25	.88	39	.07	3	3.33	.01	.03	1	1
NMA L4+00E 1+00N	1	83	27	83	.1	12	11	447	6.42	35	5	ND	1	16	1	3	2	91	.11	.047	3	21	.66	52	.10	2	4.20	.01	.06	1	6
NMA L4+00E 0+80N	1	92	163	110	.5	14	11	385	6.88	36	5	ND	1	19	1	2	2	93	.10	.052	3	26	.73	42	.09	3	3.35	.02	.06	1	1
NMA L4+00E 0+60N	1	88	47	86	.3	16	12	435	6.00	28	5	ND	1	14	1	2	2	87	.09	.042	3	27	.83	47	.08	2	3.77	.01	.05	1	15
NMA L4+00E 0+60S	1	40	4	73	.1	17	14	388	4.50	7	5	ND	1	16	1	2	2	91	.26	.032	3	31	1.16	33	.07	5	3.66	.01	.04	1	9
NMA L4+00E 0+80S	1	29	2	64	.1	13	10	264	3.84	6	5	ND	2	17	1	2	2	84	.26	.043	3	25	.78	33	.10	3	3.12	.01	.04	1	1
NMA L4+00E 1+00S	1	18	3	48	.3	9	8	204	2.79	3	5	ND	1	15	1	2	2	66	.19	.018	3	20	.57	31	.08	4	2.65	.01	.03	1	2
NMA L4+00E 1+20S	1	33	9	63	.5	14	11	278	3.84	22	5	ND	1	17	1	2	2	77	.23	.041	4	23	.73	32	.07	4	3.24	.01	.04	1	40
NMA L4+00E 1+40S	1	24	4	60	.1	9	9	262	3.73	15	5	ND	1	14	1	2	2	81	.21	.038	4	22	.61	35	.07	3	2.80	.01	.04	1	1
STD C/AU-S	19	62	42	132	7.4	73	31	1068	4.05	42	19	7	40	52	19	18	19	58	.50	.088	39	62	.93	180	.07	34	1.97	.07	.14	11	48

MINCORD EXPLORATION FILE # 87-5766

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NMA L4+00E 1+20S	1	21	11	52	.2	9	7	224	3.15	6	5	ND	1	12	1	3	2	74	.21	.016	3	24	.61	27	.09	6	2.53	.01	.02	1	10
NMA L4+00E 1+20S	1	27	8	55	.2	12	9	258	3.51	10	5	ND	2	12	1	2	2	74	.18	.025	3	26	.70	34	.08	4	3.25	.01	.02	1	6
NMA L4+00E 2+20S	1	20	11	54	.1	10	7	215	3.41	10	5	ND	2	15	1	2	2	75	.21	.025	3	23	.55	30	.09	3	2.54	.01	.02	1	1
NMC 6+00W	1	31	17	75	.3	11	8	286	3.49	9	5	ND	1	17	1	2	2	72	.31	.027	4	23	.65	35	.08	6	2.96	.01	.03	1	3
NMC 5+50W	1	43	12	112	.2	9	8	460	2.71	13	5	ND	1	21	1	2	2	41	.46	.019	4	17	.66	38	.07	5	2.08	.01	.06	1	11
NMC 5+00W	1	53	13	190	.2	15	8	455	3.23	23	5	ND	1	21	1	2	2	48	.49	.020	3	18	.83	51	.10	3	2.30	.01	.07	1	4
NMC 4+50W	1	60	19	85	.1	9	9	461	3.61	30	5	ND	2	23	1	2	2	47	.45	.022	3	18	.92	60	.09	2	2.56	.01	.08	1	1
NMC 4+00W	2	51	14	66	.3	10	8	352	3.30	25	6	ND	2	17	1	4	2	49	.40	.019	3	18	.72	60	.07	3	2.48	.01	.07	2	3
NMC 3+50W	2	58	18	179	.3	20	10	414	3.48	24	5	ND	1	20	1	2	2	49	.35	.023	3	20	.62	73	.07	4	2.97	.01	.06	1	4
NMC 3+00W	15	54	20	140	.4	22	13	276	7.52	38	5	ND	2	11	1	5	2	47	.26	.042	3	22	.55	44	.07	3	2.89	.01	.06	1	34
NMC 2+50W	16	71	20	93	.2	12	9	370	5.09	46	6	ND	3	14	1	4	2	55	.24	.067	4	22	.71	69	.09	3	3.40	.01	.05	1	36
NMC 2+00W	6	191	34	77	.4	9	9	363	7.01	67	5	ND	1	16	1	3	2	52	.20	.090	5	19	.54	49	.12	3	2.61	.02	.05	1	85
NMC 1+50W	3	83	23	92	.4	15	11	538	4.92	45	5	ND	2	23	1	2	2	54	.38	.045	3	27	.99	113	.09	5	3.64	.01	.09	1	27
NMC 1+00W	3	82	20	71	.1	12	9	405	4.45	33	5	ND	1	19	1	2	2	51	.31	.040	3	24	.81	74	.09	3	3.01	.01	.05	1	41
NMC 0+50W	2	114	21	103	.7	38	15	395	4.44	32	5	ND	2	13	1	2	2	49	.22	.046	6	35	.86	54	.07	2	4.26	.01	.05	1	59
NMC 0+00SW	2	134	28	74	.3	31	14	518	4.98	41	5	ND	2	25	1	2	2	54	.37	.038	4	26	1.08	156	.08	4	4.11	.01	.08	1	17
NMC 0+50SW	2	98	19	118	.1	30	12	344	4.69	33	5	ND	2	13	1	4	3	52	.17	.031	4	29	.76	62	.06	4	3.16	.01	.04	1	8
NMC 1+00SW	2	144	31	71	.1	14	8	370	6.67	40	5	ND	2	10	1	2	3	59	.15	.065	4	25	.76	48	.10	2	2.98	.01	.04	1	18
NMC 1+50SW	2	48	24	84	.2	12	7	331	4.26	28	5	ND	2	10	1	2	2	47	.14	.043	3	20	.64	62	.07	7	2.80	.01	.04	1	11
NMC 2+00SW	3	42	24	103	.5	15	11	375	5.41	35	7	ND	2	12	1	2	2	55	.19	.042	3	22	.63	54	.08	5	2.99	.01	.06	1	27
NMC 2+50SW	4	41	29	244	.5	8	6	367	4.52	39	5	ND	1	14	1	2	2	48	.27	.029	4	18	.66	35	.07	5	1.91	.01	.04	1	1
NMC 3+00SW	3	52	21	214	.1	11	10	535	4.78	46	5	ND	1	14	1	4	2	46	.30	.029	3	20	.87	32	.07	4	2.00	.01	.06	1	14
NMC 3+50SW	9	68	26	288	.8	17	12	504	5.08	61	5	ND	1	17	1	2	2	54	.42	.042	2	22	.79	47	.08	2	3.23	.01	.08	1	36
NMC 4+00SW	10	139	39	94	1.0	5	6	401	4.54	56	5	ND	1	17	1	3	2	43	.23	.041	3	17	.74	51	.06	2	2.12	.01	.05	1	30
NMC 4+50SW	5	108	31	67	3.0	7	7	369	4.35	37	5	ND	1	15	1	2	2	49	.19	.041	3	20	.78	68	.07	3	2.79	.01	.05	1	25
NMC 5+00SW	3	51	18	92	1.9	12	8	305	3.78	23	5	ND	2	16	1	2	2	47	.22	.033	3	19	.66	53	.06	5	2.72	.01	.05	1	7
NMC 5+50SW	5	54	22	55	.6	5	6	265	4.81	39	6	ND	1	13	1	2	2	43	.14	.046	3	16	.61	47	.05	2	2.28	.01	.05	1	10
NMC 6+00SW	16	91	35	65	.8	3	5	289	7.40	79	5	ND	1	11	1	14	2	52	.12	.082	3	24	.66	44	.03	2	2.15	.01	.06	1	27
NM R1 19+00N	6	69	25	182	.4	14	10	366	4.87	49	5	ND	1	15	1	4	2	55	.22	.048	3	21	.69	74	.07	6	3.18	.01	.06	1	22
NM R1 18+50N	4	68	22	225	.6	11	12	460	4.08	45	5	ND	1	16	1	2	2	55	.26	.035	3	20	.62	67	.06	2	2.62	.01	.06	1	5
NM R1 18+00N	5	88	29	172	.6	9	11	485	3.79	38	5	ND	2	19	1	2	2	53	.28	.035	3	17	.52	91	.05	3	2.65	.01	.07	1	8
NM R1 17+50N	3	56	13	131	.1	10	15	531	3.32	21	5	ND	1	20	1	2	2	52	.35	.031	3	16	.47	66	.05	5	1.90	.01	.07	1	4
NM R1 17+00N	5	33	54	239	.2	9	19	638	3.22	25	5	ND	2	28	1	2	2	53	.45	.033	4	17	.43	70	.06	4	1.82	.01	.06	1	1
NM R1 16+50N	1	28	16	236	.2	12	16	1259	2.89	13	5	ND	1	21	1	2	2	46	.39	.036	4	17	.58	69	.09	5	1.74	.02	.07	1	1
NM R1 16+00N	1	35	11	107	.3	14	11	432	3.11	19	5	ND	1	18	1	3	2	50	.38	.027	3	18	.65	44	.09	3	2.05	.01	.05	1	1
NM R1 15+50N	2	25	8	157	.1	12	9	352	3.16	17	5	ND	1	13	1	2	2	54	.29	.021	3	18	.57	31	.09	4	1.76	.01	.05	1	1
STD C/AU-S	18	58	40	132	7.1	67	29	1044	3.98	42	17	7	38	51	17	16	18	56	.48	.086	38	61	.89	179	.07	34	1.88	.06	.14	11	48

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NM R1 15+00N	1	25	4	101	.2	11	10	389	3.13	22	5	ND	1	20	1	2	2	52	.45	.034	3	18	.62	31	.09	4	1.98	.01	.08	1	1
NM R1 14+50N	1	67	4	277	.1	21	9	416	3.31	21	5	ND	1	20	1	2	2	54	.49	.022	3	20	.73	33	.08	2	2.12	.02	.04	1	1
NM R1 14+00N	2	29	10	73	.1	8	10	428	3.51	16	5	ND	2	20	1	2	2	63	.40	.029	3	17	.58	44	.08	2	2.19	.01	.05	1	3
NM R1 13+50N	1	26	5	104	.1	13	10	550	3.37	23	5	ND	2	17	1	2	2	58	.31	.025	3	19	.61	55	.09	4	2.33	.01	.07	1	1
NM R1 13+00N	2	34	15	72	.1	10	11	433	4.18	42	5	ND	2	32	1	2	2	71	.61	.038	3	21	.66	38	.09	7	2.22	.01	.08	1	1
NM R1 12+00N	1	24	5	99	.1	14	13	605	3.51	31	5	ND	1	18	1	2	2	60	.32	.028	3	20	.64	45	.08	4	2.56	.01	.07	1	3
NM R1 11+50N	1	29	11	86	.1	14	11	388	3.81	36	5	ND	1	20	1	2	2	62	.39	.023	3	21	.73	46	.08	4	2.74	.01	.07	1	1
NM R1 11+00N	1	16	8	92	.1	8	10	342	2.74	11	5	ND	1	19	1	2	2	54	.37	.026	3	16	.43	52	.07	3	1.80	.01	.08	1	1
NM R1 10+50N	2	31	5	106	.1	13	11	431	3.70	35	5	ND	1	18	1	2	2	64	.38	.034	3	23	.73	41	.07	6	2.30	.01	.06	1	5
NM R1 10+00N	2	18	5	122	.1	9	10	418	3.12	19	5	ND	1	16	1	2	2	57	.35	.030	3	20	.48	43	.06	5	2.25	.01	.06	1	1
NM R1 9+50N	2	48	5	73	.1	10	10	500	3.41	54	5	ND	1	13	1	2	2	47	.37	.015	3	17	.71	46	.02	4	2.21	.01	.08	1	3
NM R1 9+00N	1	16	5	177	.1	12	11	625	2.86	15	5	ND	1	20	1	2	2	54	.42	.022	3	18	.54	86	.08	6	2.22	.02	.10	1	14
NM R1 8+50N	1	18	4	79	.1	7	8	246	3.22	14	5	ND	2	15	1	2	2	62	.25	.027	4	16	.48	30	.06	3	1.87	.01	.05	1	1
NM R1 8+00N	1	21	7	65	.1	9	9	290	3.81	24	5	ND	1	14	1	2	2	72	.26	.031	4	18	.54	37	.04	3	2.31	.01	.05	1	1
NM R1 7+50N	1	17	5	57	.1	8	7	245	3.40	18	5	ND	1	13	1	2	2	63	.22	.032	4	17	.48	33	.04	3	2.16	.01	.05	1	5
NM R1 7+00N	1	20	7	64	.1	9	7	289	3.05	12	5	ND	1	13	1	2	2	57	.24	.028	4	19	.53	31	.05	2	2.04	.01	.05	1	1
NM R1 6+50N	1	14	2	76	.1	8	8	238	2.68	8	5	ND	2	13	1	2	2	50	.27	.064	4	19	.45	41	.04	3	1.86	.01	.08	1	1
NM R1 6+00N	1	17	3	56	.2	8	7	231	3.27	11	5	ND	1	13	1	2	2	62	.27	.037	3	17	.44	42	.04	5	2.05	.01	.06	1	1
NM R1 5+50N	1	21	10	51	.1	9	8	308	2.93	20	5	ND	1	13	1	2	2	48	.25	.022	4	16	.55	45	.02	3	1.87	.01	.05	1	1
NM R1 5+00N	1	17	3	52	.1	8	8	241	2.80	11	5	ND	1	13	1	2	2	50	.26	.032	3	17	.51	30	.03	4	1.93	.01	.06	1	1
NM R1 4+50N	1	16	2	51	.3	7	7	224	2.78	10	5	ND	1	13	1	2	2	54	.20	.021	3	14	.41	33	.02	3	1.81	.01	.06	1	1
NM R1 4+00N	1	19	3	46	.1	6	7	250	3.28	12	5	ND	1	15	1	2	2	60	.21	.022	4	15	.52	30	.02	4	2.00	.01	.04	1	5
NM R1 3+50N	1	20	12	61	.1	10	9	306	3.48	9	5	ND	2	16	1	2	2	62	.31	.023	4	19	.57	43	.02	3	2.36	.01	.08	1	1
NM R1 3+00N	1	26	5	55	.1	9	9	327	3.37	22	5	ND	2	14	1	2	2	54	.26	.027	4	19	.63	48	.03	4	2.30	.01	.06	1	11
NM R1 2+50N	1	48	3	123	.4	8	7	629	4.31	2	5	ND	1	18	1	2	2	66	.66	.050	8	11	.68	40	.01	6	2.93	.02	.05	1	1
NM R1 2+00N	1	56	6	38	.3	5	6	164	5.59	12	5	ND	2	7	1	2	2	68	.07	.071	2	17	.27	31	.01	6	2.06	.01	.05	1	1
NM R1 1+50N	1	68	12	72	.3	11	12	302	5.46	16	5	ND	2	16	1	2	2	69	.12	.057	4	20	.53	49	.02	4	3.60	.01	.08	1	1
NM-A R2 14+00N	4	45	26	58	.1	9	9	369	4.89	95	5	ND	2	18	1	3	2	59	.27	.041	3	18	.62	49	.03	4	2.27	.01	.07	1	24
NM-A R2 13+50N	2	19	11	37	.2	7	5	221	3.61	30	5	ND	1	12	1	3	2	55	.16	.028	3	13	.44	31	.03	6	1.88	.01	.06	1	1
NM-A R2 13+00N	2	30	10	52	.2	8	9	293	4.37	34	5	ND	1	12	1	2	2	70	.17	.041	3	20	.61	43	.05	3	2.56	.01	.04	1	9
NM-A R2 12+50N	2	33	2	47	.1	11	10	375	4.34	30	5	ND	1	11	1	2	2	67	.30	.028	3	22	.76	35	.03	6	2.39	.01	.06	2	1
NM-A R2 12+00N	2	16	13	51	.1	6	7	325	2.79	13	5	ND	1	10	1	2	2	55	.19	.019	2	13	.49	25	.02	5	1.79	.01	.03	1	1
NM-A R2 11+50N	1	16	9	114	.1	9	8	634	2.88	13	5	ND	1	11	1	2	2	55	.20	.025	3	18	.52	29	.03	3	1.74	.01	.04	1	1
NM-A R2 11+00N	1	23	6	86	.1	12	13	612	3.34	28	5	ND	1	14	1	2	2	60	.24	.032	3	21	.63	62	.06	4	2.56	.01	.05	1	6
NM-A R2 10+50N	1	25	7	107	.1	14	13	646	3.10	13	5	ND	1	17	1	2	2	59	.39	.028	3	22	.68	55	.07	4	2.51	.01	.05	1	1
NM-A R2 10+00N	2	46	7	89	.1	12	11	380	5.06	31	5	ND	2	12	1	3	2	73	.16	.051	3	33	.78	49	.04	4	3.05	.01	.06	1	1
STD C/AU-S	18	59	40	132	7.2	67	29	1038	4.03	39	19	8	38	52	18	17	18	57	.49	.084	39	60	.89	179	.07	37	2.01	.07	.14	12	52

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
NM-A R2 9+50N	1	21	11	61	.1	15	9	360	3.42	15	5	ND	2	20	1	2	2	58	.34	.021	6	24	.61	65	.07	4	2.49	.01	.05	1	1
NM-A R2 9+00N	1	25	11	150	.1	13	14	1231	3.31	13	5	ND	1	17	1	2	2	56	.36	.034	4	21	.62	68	.06	7	2.60	.01	.05	1	1
NM-A R2 8+50N	1	24	6	47	.1	11	10	371	3.58	11	5	ND	1	16	1	2	2	65	.40	.015	3	21	.69	46	.06	2	2.43	.01	.05	1	1
NM-A R2 8+00N	1	14	3	61	.1	8	8	274	2.79	3	5	ND	1	14	1	2	2	54	.24	.019	3	18	.51	54	.05	2	2.12	.01	.04	1	1
NM-A R2 7+50N	1	25	6	73	.1	11	9	722	3.27	15	5	ND	1	15	1	2	2	59	.34	.034	3	19	.59	89	.05	3	2.80	.01	.05	1	1
NM-A R2 7+00N	1	31	5	68	.1	14	11	382	3.56	9	5	ND	1	13	1	4	2	54	.22	.062	4	21	.71	45	.07	5	2.70	.01	.05	1	1
NM-A R2 6+50N	1	17	7	54	.1	9	7	265	3.00	6	5	ND	2	12	1	2	2	57	.27	.037	4	18	.49	34	.06	2	2.06	.01	.03	1	2
NM-A R2 6+00N	1	20	9	67	.1	12	9	483	3.25	8	5	ND	2	16	1	2	2	59	.37	.028	4	22	.59	55	.06	4	2.54	.01	.05	1	1
NM-A R2 5+50N	1	25	8	67	.1	13	9	466	3.32	9	5	ND	1	14	1	2	2	54	.32	.066	3	24	.58	51	.06	9	2.49	.01	.04	1	1
NM-A R2 5+00N	1	23	10	59	.1	10	8	315	3.59	14	5	ND	1	14	1	2	2	59	.22	.039	3	19	.50	54	.02	3	2.38	.01	.04	1	2
NM-A R2 4+50N	1	10	3	39	.1	4	4	189	2.30	14	5	ND	1	8	1	2	2	43	.11	.013	3	11	.30	40	.01	2	1.62	.01	.03	1	3
NM-A R2 4+00N	1	31	12	81	.1	10	8	386	3.62	21	5	ND	1	11	1	2	2	51	.21	.027	4	18	.54	45	.03	3	2.35	.01	.05	1	99
NM-A R2 3+50N	1	21	9	90	.2	11	10	860	3.40	7	5	ND	2	12	1	2	2	52	.19	.031	4	20	.59	69	.03	5	2.42	.01	.05	1	49
NM-A R2 3+00N	1	18	6	83	.1	10	8	657	3.16	2	5	ND	1	12	1	2	2	49	.25	.023	3	19	.61	53	.03	5	2.11	.01	.05	1	7
NM-A R2 2+50N	1	16	9	59	.1	6	6	374	2.58	4	5	ND	1	12	1	2	2	42	.18	.019	3	13	.43	50	.02	4	1.80	.01	.05	1	1
NM-A R2 2+00N	1	182	12	90	.1	17	42	800	4.73	16	5	ND	1	19	1	2	3	69	.20	.031	6	16	.60	78	.04	4	4.12	.01	.05	1	240
NM-A R2 1+50N	1	34	8	65	.1	5	5	302	4.42	7	5	ND	1	8	1	2	2	45	.09	.046	2	9	.37	38	.01	3	2.14	.01	.05	1	7
NM-A R2 1+00N	1	36	6	63	.3	18	12	352	4.31	5	5	ND	1	15	1	2	2	76	.23	.032	2	33	.97	39	.04	4	3.23	.01	.04	1	1
NM-A R2 0+50N	1	40	22	68	.6	8	6	327	5.56	14	5	ND	1	12	1	3	2	88	.10	.056	3	21	.47	54	.03	3	2.77	.01	.05	1	56
NM- R3 10+00N	1	25	9	77	.1	12	11	339	3.61	6	5	ND	1	13	1	3	2	62	.26	.040	3	21	.63	47	.06	6	2.56	.01	.04	1	1
NM- R3 9+50N	1	29	3	58	.1	14	11	360	4.09	14	5	ND	1	10	1	2	2	65	.26	.029	2	26	.77	31	.04	2	2.45	.01	.04	1	1
NM- R3 9+00N	1	34	9	63	.1	13	11	360	4.25	19	5	ND	1	11	1	3	2	65	.22	.055	3	24	.77	38	.03	4	2.61	.01	.04	1	2
NM- R3 8+50N	1	35	4	60	.1	14	11	463	4.15	7	5	ND	1	13	1	2	2	71	.51	.014	3	26	.90	52	.05	7	2.95	.01	.03	1	2
NM- R3 8+00N	1	36	2	52	.3	11	11	338	4.14	12	5	ND	1	15	1	2	2	71	.36	.021	3	23	.73	43	.04	5	2.73	.01	.03	1	1
NM- R3 7+50N	1	18	3	50	.1	8	7	199	2.99	3	5	ND	1	12	1	2	2	51	.20	.043	4	18	.38	34	.05	2	2.31	.01	.03	1	1
NM- R3 7+00N	1	31	7	57	.1	12	11	323	3.90	8	5	ND	1	12	1	2	2	62	.22	.053	3	22	.71	38	.06	7	2.79	.01	.03	1	5
NM- R3 6+50N	1	34	3	53	.1	11	10	395	3.75	6	5	ND	1	14	1	2	3	66	.41	.018	4	21	.76	40	.05	8	2.40	.01	.03	1	1
NM- R3 6+00N	1	29	5	48	.1	10	10	361	3.67	5	5	ND	1	14	1	2	2	63	.37	.017	4	19	.71	54	.04	3	2.42	.01	.03	1	1
NM- R3 5+50N	1	29	7	54	.1	9	8	283	3.79	7	5	ND	1	11	1	2	2	65	.20	.024	3	18	.57	45	.04	2	2.32	.01	.03	1	2
NM- R3 5+00N	1	19	4	54	.1	8	7	321	2.72	5	5	ND	1	12	1	2	2	49	.36	.011	4	15	.66	63	.04	2	1.94	.01	.03	1	3
NM- R3 4+50N	1	16	3	58	.1	9	6	259	2.43	2	5	ND	1	14	1	2	2	42	.22	.014	4	15	.55	45	.04	2	1.86	.01	.03	1	1
NM- R3 4+00N	1	29	6	73	.1	10	8	401	3.66	6	5	ND	1	12	1	2	2	57	.24	.021	4	19	.70	69	.04	2	2.44	.01	.03	1	1
NM- R3 3+50N	1	60	7	76	.2	12	12	421	5.52	15	5	ND	1	9	1	2	2	67	.10	.052	3	20	.71	51	.04	5	3.21	.01	.04	1	1
NM- R3 3+00N	1	40	3	66	.1	11	10	323	4.30	6	5	ND	1	10	1	2	2	57	.10	.032	3	23	.57	34	.03	3	2.55	.01	.03	1	1
NM- R3 2+50N	1	42	15	63	.4	9	8	315	5.34	10	5	ND	1	10	1	2	2	63	.07	.052	3	23	.48	41	.04	5	2.70	.01	.04	1	2
NM- R3 2+00N	1	39	6	60	.2	11	9	281	4.34	9	5	ND	2	11	1	3	2	62	.10	.041	3	23	.65	51	.03	2	2.88	.01	.04	1	9
STD C/AU-S	18	56	37	132	7.1	70	28	1074	4.08	39	18	7	37	50	17	17	18	56	.47	.081	37	60	.86	179	.06	33	1.92	.06	.14	11	49

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU#
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NM-R3 1+50N	1	42	22	66	.4	7	8	248	4.23	21	5	ND	1	9	1	2	2	59	.08	.043	3	15	.44	36	.02	2	2.32	.01	.04	1	4
NM-R3 1+00N	1	41	19	32	1.0	1	4	178	6.36	17	5	ND	1	8	1	2	2	59	.03	.081	2	10	.27	32	.01	2	1.99	.01	.04	1	2
NM-R3 0+50N	1	57	18	67	.6	12	12	333	5.11	26	5	ND	1	12	1	2	2	72	.11	.042	3	22	.65	44	.05	2	2.95	.01	.03	1	1
NO NUMBER	1	37	13	62	.3	14	13	350	4.11	38	5	ND	1	17	1	2	2	64	.25	.026	3	21	.68	41	.08	4	2.31	.01	.04	1	1

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU**
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	Z	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	Z	Z	PPM	PPM	Z	PPM	Z	PPM	Z	Z	Z	PPM	PPB
3-T-4	5	7	6	8	.4	2	3	2514	1.34	33	5	ND	1	104	1	2	2	7	17.60	.006	3	1	.14	5	.01	4	.28	.01	.06	1	41
IR-11	1	17	7	76	.1	5	25	1142	6.67	2	5	ND	1	35	1	2	2	33	1.63	.041	2	2	.83	25	.07	11	2.22	.25	.07	1	1
NM-A IR 12	2	44	11	60	.2	7	17	1098	5.06	4	5	ND	2	62	1	2	2	41	1.37	.025	2	4	1.17	35	.01	7	4.93	.35	.14	1	1
NM-A LD1+675	1	12	9	48	.1	7	22	1406	6.79	8	5	ND	2	17	1	2	2	106	2.71	.033	3	11	1.50	13	.01	12	2.81	.02	.13	1	1
NM-A LD1+905	6	77	367	106	32.1	3	13	710	6.45	76	5	ND	1	4	1	38	2	16	.12	.039	2	1	.36	15	.01	13	1.05	.01	.14	1	39
✓ NM-FS-5	37	1570	1856	1535	396.0	1	1	100	1.02	175	5	ND	1	2	24	1963	2	1	.09	.005	2	1	.02	3	.01	3	.11	.01	.04	1	92
NM-JR-6	1	38	13	53	1.1	7	9	728	6.31	2	5	ND	1	35	1	2	2	97	1.76	.039	2	16	1.56	16	.13	6	4.22	.07	.04	2	1
NM-JR-7	2	48	20	55	7.3	12	12	1325	4.02	109	5	ND	1	18	1	14	2	36	4.30	.035	5	19	1.12	16	.02	12	1.29	.01	.11	1	50
NMT-2-1	2	93	33	656	4.8	19	27	2304	6.82	150	5	ND	1	7	6	8	2	73	.52	.037	3	11	1.12	18	.01	7	1.62	.01	.11	1	82
NMT-2-2	2	101	38	768	6.0	10	30	2593	7.77	151	5	ND	1	6	8	7	2	123	.37	.043	3	13	1.89	13	.01	7	2.32	.01	.13	1	320
NMT-2-3	2	196	47	737	9.4	10	36	1693	6.72	158	5	ND	1	4	6	14	2	41	.26	.022	3	6	.70	16	.01	11	1.48	.01	.15	1	113
NMT-2-4	3	112	42	675	7.7	7	21	2894	6.22	83	5	ND	1	4	8	9	2	61	.36	.036	4	4	.94	16	.01	12	1.51	.01	.14	1	91
NMT-2-5	2	105	18	745	3.5	7	26	2761	6.84	77	5	ND	1	4	5	7	2	58	.38	.030	3	3	1.51	17	.01	7	2.40	.01	.13	1	42
NMT-2-6	3	60	16	786	2.1	15	24	2420	5.91	201	5	ND	1	5	9	11	2	54	.32	.046	4	21	1.27	17	.01	12	1.57	.01	.13	1	45
NMT-3-1	4	101	13	68	.9	10	30	1786	7.45	128	5	ND	1	5	1	4	2	95	.15	.041	3	14	1.26	13	.01	6	2.62	.01	.13	1	96
NMT-3-2	4	47	26	104	1.4	11	22	2797	5.00	141	5	ND	1	5	1	3	2	43	.09	.029	3	9	.65	10	.01	5	1.25	.01	.11	1	87
NMT-3-3	5	82	21	212	4.4	21	27	6106	5.28	132	5	ND	1	11	4	3	2	86	.15	.040	5	11	1.19	17	.01	8	2.06	.01	.10	1	395
NMT-87-54	1	52	12	64	.2	9	8	559	5.29	6	5	ND	1	28	1	2	2	97	.47	.026	2	16	.78	19	.29	4	2.75	.04	.06	1	7
NMT-87-55	1	71	5	78	.1	7	8	841	8.04	10	5	ND	1	31	1	2	2	115	.62	.043	2	35	.63	18	.27	6	2.58	.04	.04	1	6
NMT-87-56	1	24	2	78	.1	5	12	868	4.98	10	5	ND	1	13	1	2	2	69	.50	.050	3	10	.97	23	.11	8	2.06	.03	.08	1	1
NMT-87-57	9	66	155	336	.9	5	9	810	3.06	34	5	ND	1	11	8	2	3	36	.29	.019	2	12	.56	11	.07	6	1.15	.02	.06	1	290
NMT-87-58	1	28	3	47	.3	9	9	590	4.04	39	5	ND	1	10	1	2	2	39	.24	.018	2	17	1.21	20	.10	9	1.72	.02	.08	1	7
NMT-87-59	1	65	11	84	.2	3	10	1085	5.15	92	5	ND	1	10	1	2	2	66	.33	.042	2	3	1.43	13	.25	8	2.10	.02	.07	1	28
NMT-87-60	3	24	3	54	.1	11	12	342	5.57	18	5	ND	1	16	1	2	2	49	.57	.028	2	31	1.66	101	.13	7	2.50	.04	.04	1	1
NMT-87-61	1	37	7	71	.3	2	10	888	5.43	50	5	ND	1	9	1	2	2	83	.18	.030	2	2	1.20	15	.27	9	1.59	.03	.05	1	11
NMT-87-62	1	40	44	86	.2	10	6	1081	3.97	14	5	ND	1	20	1	2	2	72	.52	.022	2	33	1.72	88	.15	6	2.50	.04	.04	1	9
NMT-87-63	4	36	123	104	3.1	6	7	363	3.64	107	5	ND	1	6	1	2	2	39	.26	.027	3	23	1.18	61	.04	10	1.62	.02	.11	1	147
NMT-87-64	16	33	174	149	6.8	1	3	74	2.57	39	5	ND	1	4	1	3	2	6	.03	.013	2	4	.04	46	.03	5	.28	.01	.09	1	280
NMT-87-65	16	66	9	22	2.0	3	4	97	2.27	50	5	ND	1	4	1	2	2	8	.03	.010	2	5	.08	26	.03	3	1.43	.01	.10	2	89
NMT-87-66	3	37	11	38	.3	8	9	420	4.04	50	5	ND	1	8	1	4	2	55	.13	.021	2	30	1.77	20	.07	11	1.75	.04	.09	1	25
STD C/AU-R	18	59	40	128	7.3	68	28	1084	3.92	39	19	8	37	47	17	17	20	58	.45	.081	36	57	.89	160	.06	31	1.82	.06	.14	13	520
NMT-87-67	2	29	3	18	.1	1	4	251	4.68	11	5	ND	1	12	1	2	2	33	.25	.031	2	19	1.09	22	.08	4	1.54	.03	.07	1	13
NMT-87-68	6	123	19	51	.5	5	6	757	3.90	38	5	ND	1	11	1	2	2	55	.39	.032	2	20	1.54	61	.12	3	1.78	.05	.10	1	38
NMT-87-69	12	95	24	58	1.0	3	3	287	2.97	79	5	ND	1	8	1	24	2	29	.10	.024	5	9	.68	42	.01	5	.98	.02	.12	1	65
NMT-87-70	13	27	11	12	5.6	1	2	54	1.60	52	5	ND	1	4	1	7	2	2	.02	.010	4	2	.02	21	.01	2	.26	.01	.10	1	375
NMT-87-71	5	34	49	34	.8	3	3	260	2.98	50	5	ND	1	6	1	3	2	19	.03	.016	2	9	.89	28	.12	5	.91	.01	.11	2	71
NMT-87-72	7	35	52	25	4.1	4	4	261	2.16	51	5	ND	1	4	1	2	2	12	.06	.011	2	9	.40	12	.05	9	.42	.01	.08	2	305
NMT-87-73	1	26	8	71	.1	10	7	1020	3.62	24	5	ND	1	6	1	5	2	69	.10	.034	3	39	2.76	52	.01	5	2.42	.02	.11	1	13

Rocks.
Asby FA/AA

MINCORD EXPLORATION

FILE # 87-5366

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU**
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
NMT-87-74	1	23	19	101	.1	16	11	1203	4.16	21	5	ND	1	11	1	2	2	58	.33	.030	2	45	2.07	35	.01	3	1.78	.07	.05	1	4
NMT-87-75	1	36	37	105	.4	9	10	1181	4.18	40	5	ND	1	6	1	3	2	42	.18	.016	2	20	1.95	25	.09	5	1.84	.02	.09	1	27
NMT-87-76	1	25	77	63	.1	6	7	728	4.42	21	5	ND	1	18	1	2	2	43	.21	.034	2	21	1.62	43	.13	9	1.60	.04	.18	1	7
NMT-87-77	1	43	10	80	.1	9	8	610	4.34	20	5	ND	1	6	1	3	2	32	.06	.031	2	22	1.61	25	.01	4	1.81	.01	.11	1	10
NMT-87-78	1	40	14	88	.1	17	10	724	4.30	38	5	ND	1	10	1	2	2	51	.39	.039	2	39	1.67	57	.11	8	1.75	.04	.11	1	18
NMT-87-79	1	27	2	75	.1	8	9	871	3.30	17	5	ND	1	29	1	2	2	36	.90	.031	2	25	1.59	38	.09	3	2.27	.06	.04	1	5
NMT-87-80	1	36	4	111	.3	22	9	915	4.52	35	5	ND	1	11	1	2	2	65	.39	.038	2	53	2.47	51	.10	4	2.23	.04	.07	1	22
NMT-87-81	1	22	9	101	.1	23	12	962	4.00	44	5	ND	1	14	1	2	2	59	.65	.031	2	53	2.15	41	.11	6	2.03	.95	.04	1	13
NMT-87-82	2	31	8	55	.1	14	10	528	3.98	29	5	ND	1	12	1	2	2	35	.53	.056	2	18	1.28	39	.08	6	1.77	.06	.09	1	18
NMT-87-83	32	33	9	74	.1	5	11	621	4.39	22	5	ND	1	14	1	2	2	41	1.04	.036	2	11	1.16	55	.11	5	1.95	.05	.07	1	6
NMT-87-84	4	15	8	53	.1	11	8	398	3.87	18	5	ND	1	13	1	2	2	37	.42	.030	2	39	1.82	23	.10	8	1.82	.04	.09	1	23
NMT-87-85	3	82	9	234	.1	17	22	1459	6.69	52	5	ND	1	21	1	2	2	139	.57	.031	2	15	1.19	22	.11	3	3.03	.08	.06	1	9
NMT-87-87	2	26	12	146	.1	8	6	882	4.18	27	5	ND	1	3	1	2	2	40	.10	.032	2	24	2.36	20	.02	4	2.58	.01	.09	1	14
NMT-87-88	4	58	101	83	2.9	6	10	969	4.40	41	5	ND	1	6	1	2	2	40	.14	.023	2	15	1.39	21	.10	6	1.28	.01	.09	1	67
NMT-87-89	6	31	24	38	1.9	2	2	258	2.38	74	5	ND	1	5	1	2	2	17	.18	.014	2	14	.51	16	.09	6	.84	.01	.13	1	103
NMT-87-90	6	89	13	83	.2	7	4	617	3.70	38	5	ND	1	8	1	2	2	59	.12	.026	2	33	2.21	20	.10	6	2.23	.02	.10	1	38
NMT-87-91	11	52	21	25	2.7	2	2	71	2.24	62	5	ND	1	3	1	40	2	7	.01	.014	3	3	.12	19	.01	7	.41	.02	.10	1	76
NMT-87-92	8	89	12	62	.2	4	4	579	3.90	62	5	ND	1	5	1	2	5	47	.11	.035	2	16	1.23	25	.02	3	1.60	.02	.10	1	48
NMT-87-93	8	27	13	42	3.4	4	3	129	1.35	36	5	ND	1	7	1	5	2	8	.09	.011	2	4	.17	16	.02	7	.59	.01	.05	1	72
NMT-87-94	1	79	8	93	.1	17	24	1443	5.82	28	5	ND	1	11	1	2	2	69	.47	.019	2	19	1.59	20	.08	9	3.04	.02	.09	1	9
✓ NMT-87-96	42	1363	21282	68567	215.3	5	7	1512	3.14	100	5	ND	1	33	593	337	2	9	7.61	.012	3	5	.27	8	.01	11	.39	.01	.06	1	890
NMT-87-97	1	17	44	145	1.7	3	5	3034	3.56	47	5	ND	1	118	1	2	2	17	13.39	.004	2	3	1.10	2	.01	7	1.20	.01	.02	1	34
✓ NMT-87-98	20	339	6847	21399	167.4	8	11	1208	2.23	119	5	ND	1	10	226	113	2	6	2.43	.027	3	4	.11	14	.01	13	.47	.01	.14	2	135
NMT-87-99	4	51	299	594	17.3	10	12	553	2.89	102	5	ND	1	17	5	13	2	11	3.45	.033	3	8	.25	13	.02	12	.49	.01	.11	1	132
✓ NMT-87-100	23	466	6676	14745	187.0	2	3	2453	1.48	56	5	ND	1	76	132	135	2	2	15.48	.007	4	2	.09	7	.01	7	.18	.01	.04	3	480
NMT-87-101	5	106	136	191	9.6	8	9	991	3.26	76	5	ND	1	21	2	2	2	18	6.71	.024	4	8	.61	10	.01	13	.91	.01	.08	1	29
NMT-87-102	1	52	56	185	1.5	6	11	969	5.20	9	5	ND	1	9	1	2	2	33	1.48	.046	2	2	.80	18	.01	11	2.15	.03	.15	1	25
✓ NMT-87-103	14	486	1226	1385	478.3	2	4	134	2.04	116	5	ND	1	2	17	949	2	2	.06	.012	2	2	.07	6	.01	8	.27	.01	.05	2	91
✓ T-2-7	5	92	654	831	50.9	12	23	4167	4.27	143	5	ND	1	4	14	25	2	21	.24	.030	4	7	.48	20	.01	14	.85	.01	.10	1	295
✓ T-4-01	14	120	607	633	40.0	9	15	2567	2.57	145	5	ND	1	6	10	14	2	6	.14	.022	3	4	.06	17	.01	16	.35	.01	.07	1	72
✓ T-4-02	22	354	2309	1161	77.5	14	35	7026	3.00	197	5	ND	1	8	24	24	2	8	.09	.021	3	3	.07	31	.01	6	.54	.01	.07	1	104
✓ T-4-03	10	157	1350	761	26.2	6	16	1964	3.45	233	5	ND	1	8	6	15	2	10	.07	.025	3	3	.15	19	.01	6	.58	.01	.09	1	52
✓ T-4-04	6	123	444	947	11.7	11	15	1748	4.48	202	5	ND	1	10	7	10	2	23	.15	.039	5	9	.56	23	.01	6	1.10	.01	.09	1	38
✓ T-4-05	22	255	2637	5284	56.6	9	12	10955	3.98	142	5	ND	1	11	101	19	2	27	.21	.034	7	8	.76	45	.01	11	1.58	.01	.08	1	450
✓ T-4-06	9	158	12880	1429	76.2	8	16	4473	4.12	98	5	ND	1	8	14	12	3	41	.18	.038	6	12	1.13	33	.01	10	1.70	.01	.11	1	460
✓ T-4-07	4	52	399	597	5.0	8	17	2438	4.07	118	5	ND	2	12	8	4	2	32	.19	.030	6	11	.86	208	.01	13	1.36	.01	.10	1	46
STD C/AU-R	18	58	39	131	7.4	68	28	1034	4.04	43	20	8	39	52	17	17	17	56	.52	.085	38	62	.91	178	.07	34	1.89	.07	.13	12	490

- ASSAY REQUIRED FOR CORRECT RESULT
 * Pb > 10,000 PPM
 Zn > 20,000 PPM
 Ag > 35 PPM

MINCORD EXPLORATION FILE # 87-5366

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU** PPB
T4-08	3	53	740	462	3.5	11	13	3410	3.94	82	5	ND	2	9	5	2	3	32	.19	.037	7	11	.94	30	.01	2	1.48	.01	.10	1	33
T4-09	7	253	528	1222	7.6	10	16	7037	5.33	148	5	ND	1	12	17	2	3	39	.22	.035	9	9	1.16	220	.01	10	1.94	.01	.10	1	78
T4-10	2	112	295	724	30.3	9	11	3707	3.62	77	5	ND	1	51	7	2	2	40	7.39	.029	5	11	.99	69	.01	8	1.43	.01	.09	1	54
T4-11A	7	190	3150	6740	28.5	1	1	6090	1.03	61	5	ND	1	130	76	10	2	1	21.73	.001	2	1	.10	5	.01	2	.08	.01	.01	1	360
✓ T4-11B	40	645	20230	64111	295.5	2	3	5178	1.69	178	5	ND	1	10	711	51	2	2	2.53	.003	3	2	.08	4	.01	6	.17	.01	.02	1	605
✓ T4-12	4	186	1151	2893	31.4	1	1	5504	.93	44	5	ND	1	102	28	7	2	1	16.20	.001	2	1	.10	9	.01	7	.10	.01	.01	2	210
✓ T4-12A	7	71	2987	5351	81.9	1	1	10370	.94	57	5	ND	1	145	50	5	2	1	27.39	.001	2	1	.11	3	.01	5	.05	.01	.01	2	205
T-5-1	2	41	98	235	2.6	11	18	1469	4.63	55	5	ND	2	13	2	2	2	52	.64	.023	4	11	1.09	25	.01	7	1.66	.03	.11	1	27
T-5-2	1	35	82	318	2.6	8	10	3602	3.08	61	5	ND	1	70	3	2	2	22	11.46	.020	6	8	.55	20	.01	3	1.08	.02	.10	1	26
T-5-3	1	62	229	386	4.0	14	16	1776	4.58	23	5	ND	1	29	3	2	2	70	2.02	.032	4	23	1.72	23	.01	3	2.69	.09	.06	1	16
T-5-4	1	39	33	143	.7	7	15	1285	4.74	5	5	ND	1	26	1	2	2	63	1.84	.051	5	6	1.73	20	.05	3	2.74	.08	.05	1	1
✓ T-5-5	6	194	2548	2681	93.8	7	10	3756	3.01	93	5	ND	1	5	32	15	2	17	.40	.025	3	8	.49	11	.01	10	.73	.01	.07	2	720
T-5-6	9	94	1580	3189	22.4	5	7	2148	2.58	142	5	ND	1	20	32	6	2	3	4.27	.017	2	3	.12	7	.01	14	.28	.01	.07	2	380
T-5-7	8	78	362	524	6.8	6	9	2546	2.75	81	5	ND	2	9	7	2	2	20	1.39	.023	5	7	.60	16	.01	9	1.07	.01	.09	1	103
T-5-8	1	79	35	219	.8	7	17	1826	5.19	15	5	ND	2	24	1	2	2	96	2.82	.036	6	3	2.02	20	.01	5	3.45	.06	.09	1	3
T-5-9	1	55	40	116	1.1	12	15	1333	4.34	46	5	ND	1	12	1	2	4	55	.30	.031	6	14	1.22	22	.01	6	1.92	.02	.10	1	10
T-5-10	1	42	31	101	.5	14	17	1269	4.91	39	5	ND	1	17	1	2	2	77	.93	.037	4	23	1.79	20	.06	9	2.10	.10	.10	1	9
STD C/AU-R	19	59	39	132	7.2	69	29	1040	3.96	40	17	8	39	52	18	15	18	57	.47	.084	39	60	.88	180	.07	33	1.88	.07	.14	12	515

F. I. E. ANALYTICAL LABORATORIES LTD. DATE RECEIVED: NOV 17 1987
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE (604) 253-3158 FAX (604) 253-1716 DATE REPORT MAILED: *Dec. 3/87.*

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp AU** BY FIRE ASSAY (1 A/T)

ASSAYER: .. *D. Toyne* DEAN TOYE, CERTIFIED B.C. ASSAYER

MINCORD EXPLORATION File # 87-5366 R

SAMPLE#	AU** oz/t
NM-FS-5	.002
NMT-87-96	.017
NMT-87-98	.005
NMT-87-100	.023
NMT-87-103	.003
T-2-7	.009
T-4-01	.002
T-4-02	.003
T-4-03	.001
T-4-04	.001
T-4-05	.011
T-4-06	.017
T-4-07	.001
T-4-08	.001
T4-11B	.022
T4-12	.007
T4-12A	.008
T-5-5	.021

ATME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: DEC 8 1987
E. E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE (604) 253-3158 FAX (604) 253-1716 DATE REPORT MAILED: *Dec 10/87*

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

MINCORD EXPLORATION File # 87-5366 R

SAMPLE#	AG OZ/T
NM-FS-5	29.52
NMT-87-96	6.30
NMT-87-98	4.78
NMT-87-100	5.50
NMT-87-103	28.19
T-2-7	1.51
T-4-01	1.18
T-4-02	2.25
T-4-03	.78
T-4-04	.38
T-4-05	1.79
T-4-06	2.30
T-4-07	.11
T-4-08	.11
T-4-11B	8.96
T-4-12	.78
T-4-12A	2.31
T-5-5	2.79

F. Z ANALYTICAL LABORATORIES LTD. DATE RECEIVED: NOV 17 1987
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE (604) 253-3158 FAX (604) 253-1716 DATE REPORT MAILED: *Dec. 3/87.*

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp AU** BY FIRE ASSAY (1 A/T)

ASSAYER: .. *D. Toyer* .. DEAN TOYE, CERTIFIED B.C. ASSAYER

MINCORD EXPLORATION PROJECT-NEW MAC File # 87-5150 R

SAMPLE#	AU** oz/t
NMT-87-53	.002
I-3A	.065
I-10	.065

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: DEC 8 1987
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE (604)253-3158 FAX (604)253-1716 DATE REPORT MAILED: *Dec. 10/87*

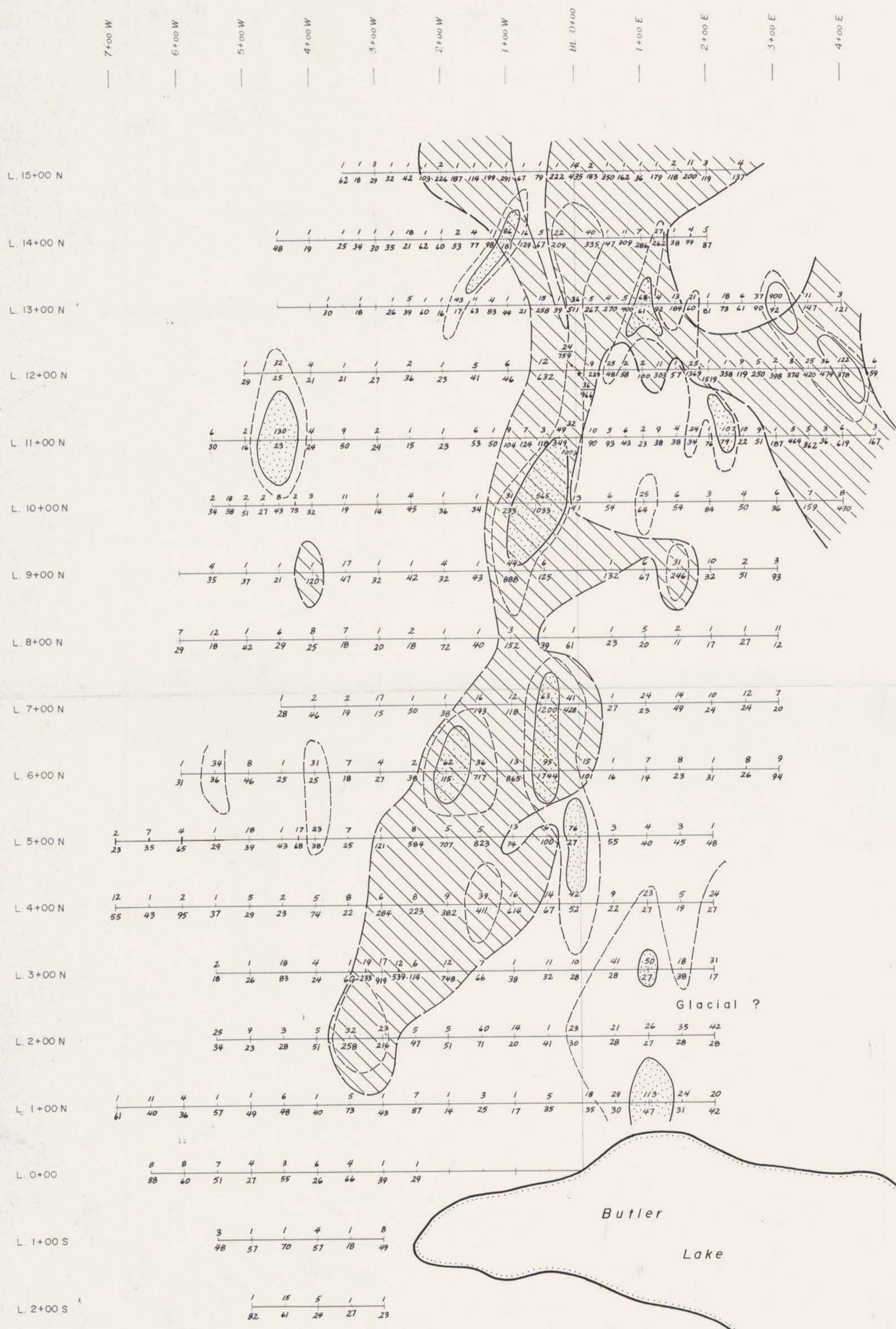
ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

MINCORD EXPLORATION PROJECT-NEW MAC File # 87-5150 R

SAMPLE#	AG OZ/T
NMT-87-53	2.23
I-3A	.03
I-10	.15

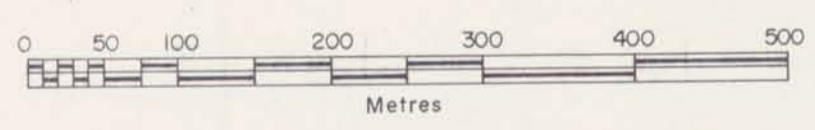


**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

17,080
8 Au (ppb)
23 Cu (ppm)

Gold values (ppb) Copper values (ppm)

○ 20 ppb ○ >100 ppm
● >50 ppb ○ (diagonal lines)



Jacqueline Gold Corp.		
NEWMAC PROJECT		
Clinton M.D.; B.C.		
- Grid B -		
SOIL GEOCHEMISTRY		
Gold (ppb), Copper (ppm)		
 MINCORD Exploration Consultants Ltd.	Scale :	1 : 5000
	Date :	November 1987
	By :	J.W.M. / S.T.
N.T.S. 92-N(10/15)E		Figure :
		8

For claim post location see figure 2

L. 2+00 W L. 1+50 W L. 1+00 W L. 0+50 W L. 0+00 L. 0+50 E L. 1+00 E L. 1+50 E L. 2+00 E L. 2+50 E L. 3+00 E L. 3+50 E L. 4+00 E L. 4+50 E L. 5+00 E

2+00 N
1+00 N
BL 0+00
1+00 S
2+00 S



Outline of area soil sampled by Imperial Metals Corporation (1984)

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

17,080

Jacqueline Gold Corp.

NEWMAC PROJECT

Clinton M.D., B.C.

- Grid A -

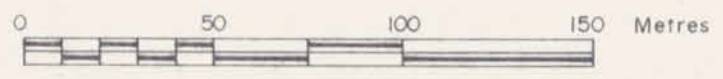
SOIL GEOCHEMISTRY
Gold (ppb), Silver (ppm)



Gold values (ppb)

- 20 ppb
- >50 ppb

Au (ppb)
Ag (ppm)

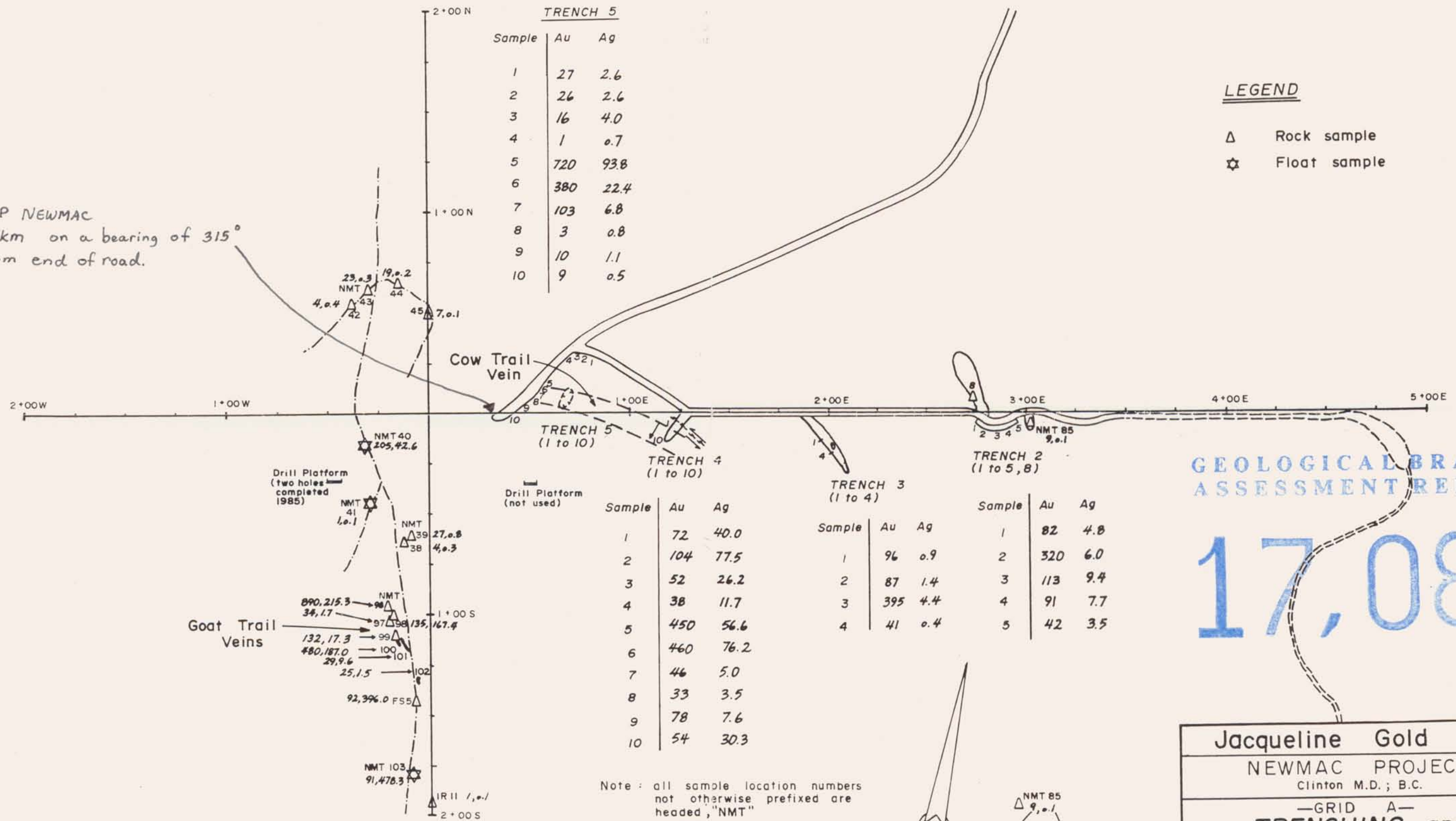


For claim post location see figure 2.



Scale:	1 : 2000	N.T.S.	92-N(10/15)E
Date:	November 1987	Figure:	5
By:	J.W.M. / S.T.		

LCP NEWMAC
1.5 km on a bearing of 315°
From end of road.



TRENCH 5

Sample	Au	Ag
1	27	2.6
2	26	2.6
3	16	4.0
4	1	0.7
5	720	93.8
6	380	22.4
7	103	6.8
8	3	0.8
9	10	1.1
10	9	0.5

LEGEND

- △ Rock sample
- ☆ Float sample

TRENCH 4 (1 to 10)

Sample	Au	Ag
1	72	40.0
2	104	77.5
3	52	26.2
4	38	11.7
5	450	56.6
6	460	76.2
7	46	5.0
8	33	3.5
9	78	7.6
10	54	30.3

TRENCH 3 (1 to 4)

Sample	Au	Ag
1	96	0.9
2	87	1.4
3	395	4.4
4	41	0.4

TRENCH 2 (1 to 5, 8)

Sample	Au	Ag
1	82	4.8
2	320	6.0
3	113	9.4
4	91	7.7
5	42	3.5

Note: all sample location numbers not otherwise prefixed are headed, "NMT"



NMT 85
9,0.1
gold (ppb) silver (ppm)

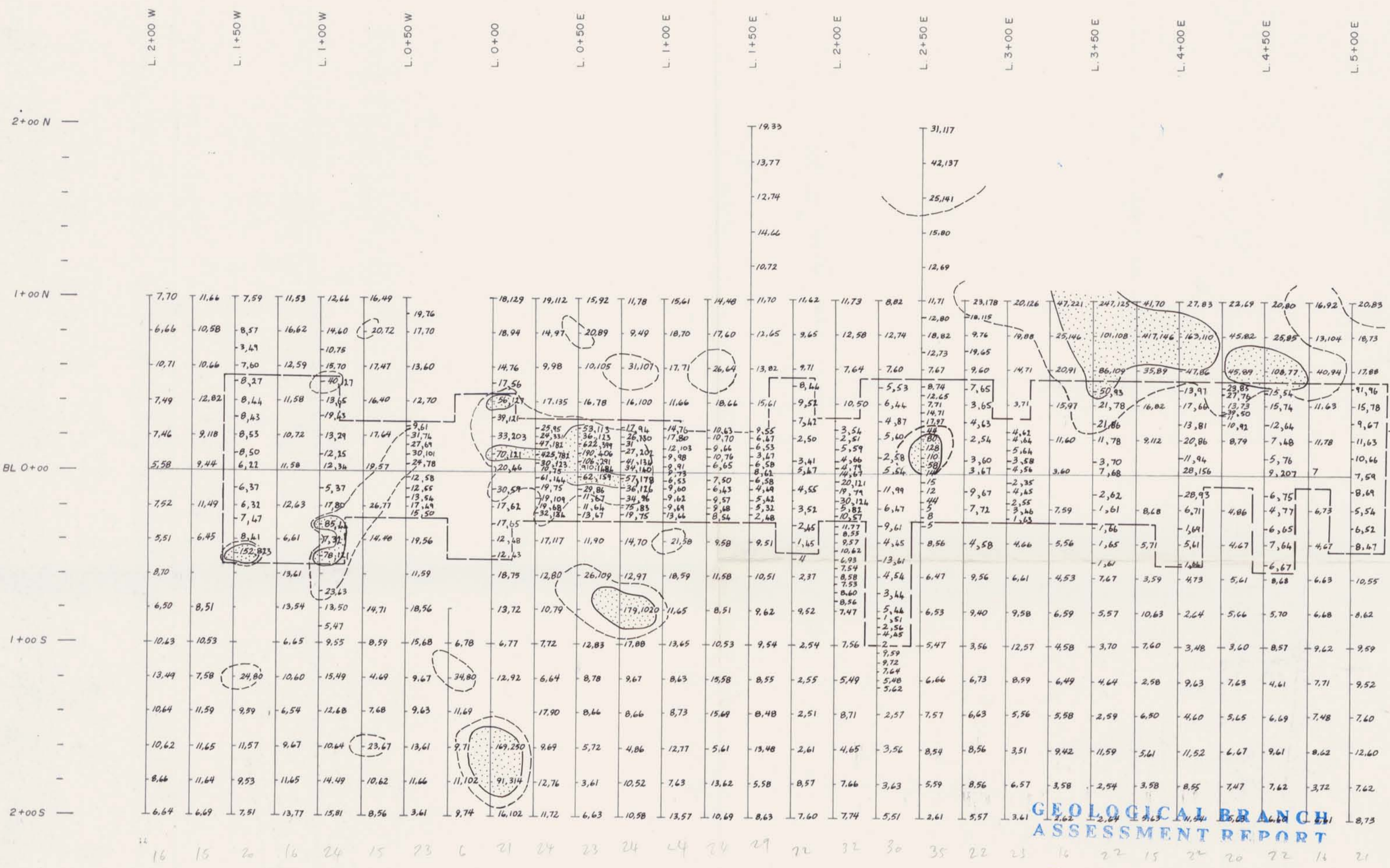


GEOLOGICAL BRANCH ASSESSMENT REPORT

17,080

Jacqueline Gold Corp	
NEWMAC PROJECT Clinton M.D.; B.C.	
—GRID A— TRENCHING and ROCK SAMPLING	
Scale 1:2,000	N.T.S. 92 N(10/15) E
Date Dec. 1987	Figure
By	7



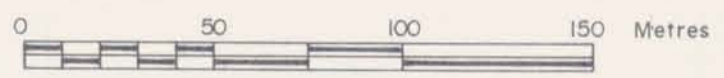


Outline of area soil sampled by Imperial Metals Corporation (1984)

GEOLOGICAL BRANCH ASSESSMENT REPORT

17,080

Lead values (ppm)
 ○ 20 ppm
 ● > 50 ppm
 ← Pb (ppm)
 ← Zn (ppm)



For claim post locations see figure 2.

Jacqueline Gold Corp.		
NEWMAC PROJECT		
Clinton M.D.; B.C.		
- Grid A -		
SOIL GEOCHEMISTRY		
Lead (ppm), Zinc (ppm)		
Scale:	1 : 2000	N.T.S. 92-N(10/15)E
Date:	November 1987	Figure:
By:	J.W.M. / S.T.	6

