ARIS SUMMARY SHEET

District Geologist, Kamloops   Off Confidential: 89.05.30

ASSESSMENT REPORT 17143   MINING DIVISION: Kamloops

PROPERTY: Deadman
LOCATION: LAT 50 54 52   LONG 120 57 25
UTM 10 5642080 643622
NTS 092I15W
CLAIM(S): Cayuse,Cayuse 2,Goldgiant 1,G.I. Joey 1-2
OPERATOR(S): Stetson Res. Management
AUTHOR(S): Freeze, J.C.
REPORT YEAR: 1988, 127 Pages
COMMODITIES
SEARCHED FOR: Antimony,Mercury
GEOLOGICAL
SUMMARY: Triassic Nicola volcanic rocks are overlain by Cretaceous sedimentary rocks, and intruded by Upper Cretaceous igneous rocks. Cinnabar, stibnite, pyrite and sphalerite occur in quartz-carbonate veins, stockwork zones and breccias.
WORK
DONE: Geological,Geochemical
GEOL 250.0 ha
HMIN 19 sample(s) ;CU,AG,NI,AS,SB,AU
ROCK 26 sample(s) ;CU,AG,NI,AS,SB,AU
SOIL 1453 sample(s) ;CU,AG,NI,AS,SB,AU
RELATED
REPORTS: 11477,12288,15227,16819
MINFILE: 092INE063

0830

GEOLOGICAL AND GEOCHEMICAL

ASSESSMENT REPORT

ON THE

DEADMAN PROPERTY

CAYUSE, CAYUSE 2, GOLDGIANT 1, G.I.JOEY 1 & 2

KAMLOOPS MINING DIVISION

SOUTHERN CENTRAL, BRITISH COLUMBIA

FILMED

NTS 92I/15W

50° 57'N 120° 55'W

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FOR

BU-MAX GOLD CORP.

SUITE 13 - 1155 MELVILLE STREET

VANCOUVER, BRITISH COLUMBIA

V6E 4C4

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,143

PREPARED BY

STILLWATER ENTERPRISES LTD.

2891 WEST 14TH AVENUE

VANCOUVER, BRITISH COLUMBIA

V6K 2X3

JOANNE C. FREEZE, F.G.A.C.

MAY, 1988

SUMMARY

The Deadman property comprises five claims, totalling 76 units, situated in the Kamloops mining division in southern central British Columbia. The nearest communities are Kamloops, 50 air kilometres to the southeast and Savona, 20 air kilometres to the south. The property is situated in the southern part of the Interior Plateau. The region has a semi-arid climate. The claims lie between 550 and 1100 metres above sea level covering a total of 19 square km. Sufficient timber and water resources for exploration and develpment purposes are available from the Criss Creek and Deadman River valleys.

The most significant precious metal mineralization discovered in the area is the Vidette Mine on Vidette Lake 30 kilometres north of the Deadman River property. The Vidette is an epithermal gold silver and base metal deposit which averaged 0.55 oz per ton gold, 0.84 oz per ton silver and 0.09% copper in a total of 12,352 tons milled in the 1930's.

The area presently covered by the Deadman property has been staked by various claims since 1896. The initial claim was staked to cover a mercury showing; limited underground work included excavation of an adit and the installation of tracks. This showing was recently recognized as the upper level to an epithermal quartz-carbonate vein system similar to those hosting bonanza type precious metal ore bodies. Several other similar showings have been found on the Deadman property. The claims are held under option to Bu-Max Gold Corp. On behalf of Bu-Max, Stetson Resource Management Corp. carried out an exploration program under the direction of the writer in 1987 and 1988.

Cinnabar, stibnite, pyrite and sphalerite mineralization occurs in quartz - carbonate veins, stockword zones and breccias. Several zones of anomalous copper, arsenic, antimony, nickel, gold and silver concentrations have been delineated in soils. Anomalous concentrations of gold and barium have been found in several creeks draining the property.

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TABLES

FIGURES AND MAPS

1. INTRODUCTION

This report discusses the geology, physiography and economic potential of a precious metal prospect covered by the Deadman property under option to Bu-Max Gold Corp. The report is based on a detailed geochemical and geological exploration program conducted by Stetson Resource Management Corp., under the direction of the writer and on public assessment reports from previous exploration on the property. Further exploration is recommended to test the economic potential of the property.

1.1 Location and Access

The Deadman property is situated in the Kamloops mining division in southern central British Columbia, approximately 50 air kilometres west-northwest of Kamloops, and 20 air kilometres north of the village of Savona. The claim blocks cover 19 square kilometres centred at 50° 57'N and 120° 55'W on NTS map sheet 92I/15W.

Distance by road from Kamloops to the property is 55 kilometres via the Trans Canada Highway and Deadman River Road, an all weather gravel road. Range roads cover most of the claims, providing excellent summer access and good four wheel drive access during the winter.

1.2 Property

The Deadman property covers five claims totalling 76 units situated in the Kamloops mining division. Bu-Max Gold Corp. has an option to earn 100% interest in the Goldgiant 1, and Cayuse 2 claims and 75% interest in the Cayuse claim. The G.I. Joey 1 and 2 claims are held by location. Claim locations were verified by legal (and other) corner posts and blazed - flagged lines.

TABLE 1.2
Deadman Property

Claim Name	Record No.	Record Date	Expiry Date	No. Units
Cayuse	2986	Sept 24/80	Sept 89	12
Cayuse 2	6841	Nov 7/86	Nov 89	4
Goldgiant 1	6840	Nov 7/86	Nov 89	20
G.I. Joey 1	7053	May 29/87	May 89	20
G.I. Joey 2	7054	May 29/87	May 89	20

BU–MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

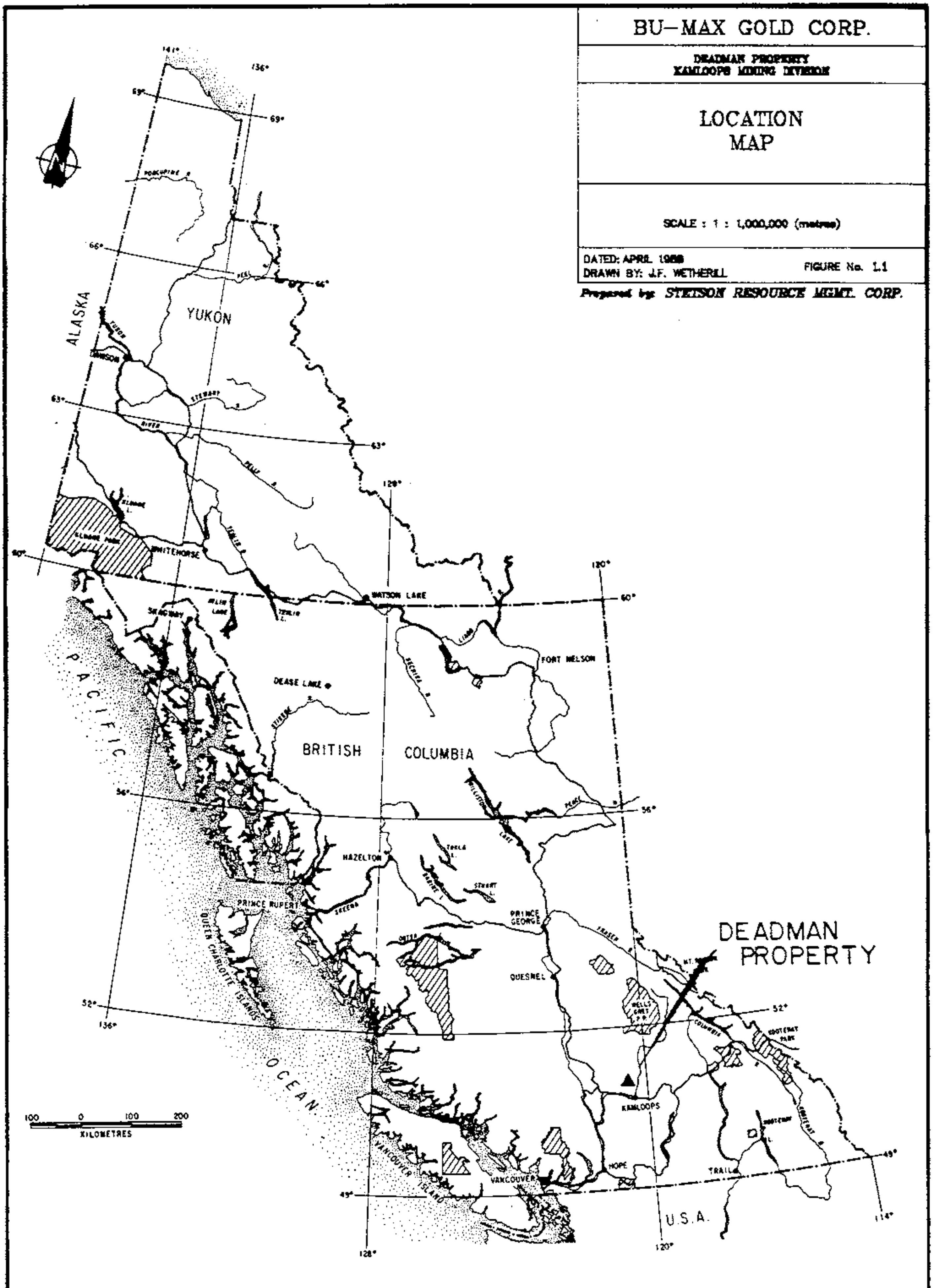
LOCATION MAP

SCALE : 1 : 1,000,000 (metres)

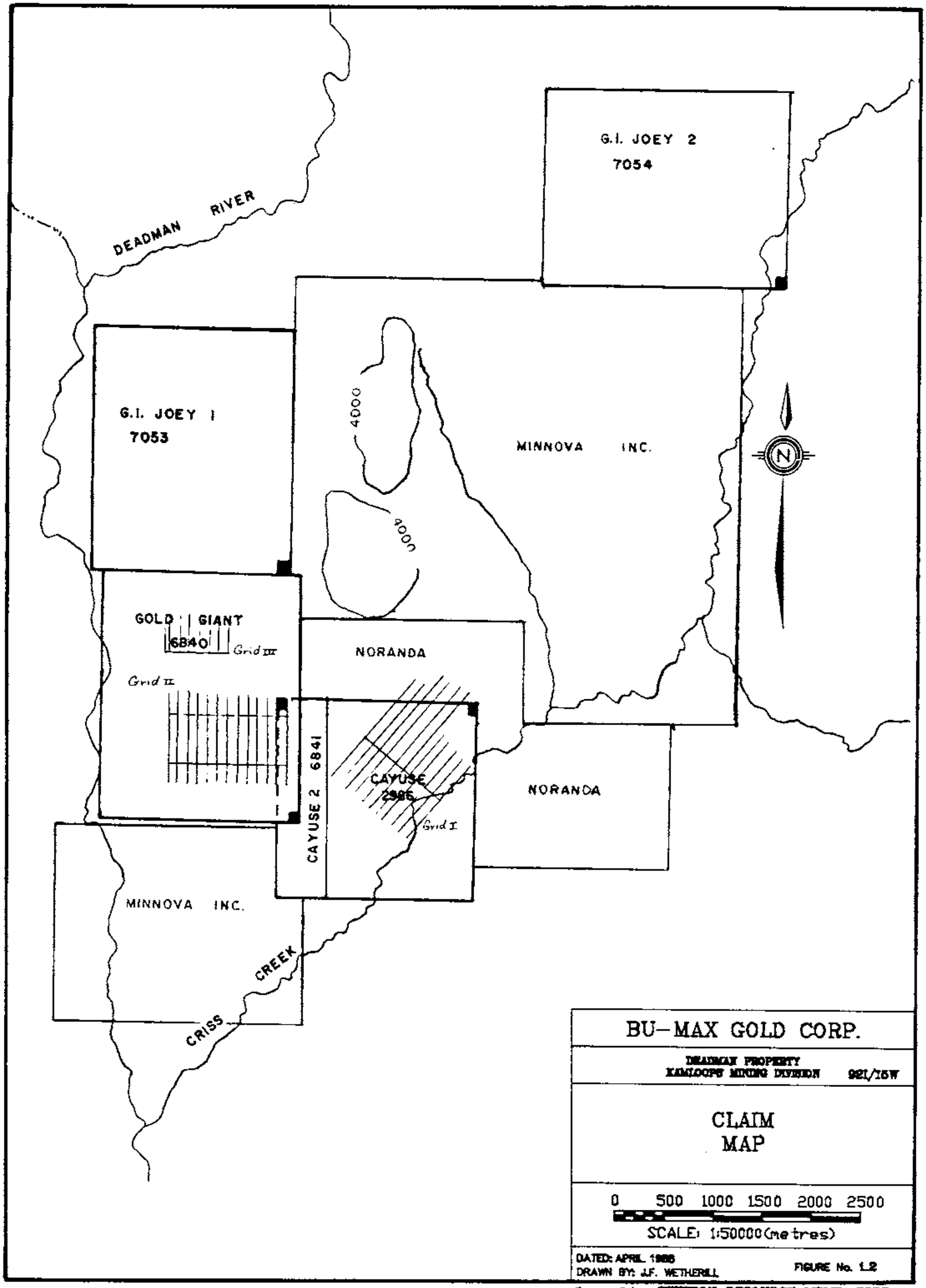
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL

FIGURE No. 1.1

Prepared by: STETSON RESOURCE MGMT. CORP.



R W R MINERAL GRAPHICS LTD.



Prepared by: STETSON RESOURCE MGMT. CORP.

1.3 Physiography, Vegetation and Climate

The claims are situated in the southern part of the Interior Plateau within the Intermontane Belt. The region has a semi-arid climate; mean annual precipitation in the area ranges between 30 and 40 centimetres. Temperatures reach a low of -30°C in winter and exceed 40°C in summer. Elevations on the property range from 550 metres to 1100 metres above sea level; and the terrain is characterized by generally broad, forested hills and locally, steep sided valleys.

Vegetation consists of open grasslands at lower elevations with Ponderosa pine, fir and deciduous trees near drainages and at higher elevations.

1.4 History

The Deadman property area has been prospected since the late 1800's. Initially the area was explored for gold and copper. Independent placer operations worked Deadman River and Criss Creek intermittently up to the 1940's. Two lode prospects, the Veron and the Diamond S contained pyrite mineralization, with minor copper, molybdenum, zinc and lead. Two mercury showings have been worked on the north side of Criss Creek above Criss Creek road. Exploration included the construction of short adits, pits and trenches.

Recent exploration over the area covered by the Deadman property has included geological mapping, geochemical, rock and soil sampling, and diamond drilling by Andex Mines Ltd. in 1972 and by Guichon Explorco Ltd. in 1981 and 1982. Anomalous gold, silver and arsenic zones were delineated in the soils. These zones were covered by the 1987 grids to confirm and further delineate the geochemical anomalies.

1.5 1987 Exploration Program

In 1987 an exploration program was undertaken by geologists, prospectors and field technicians employed by Stetson Resource Management Corp. under the direction of J.C. Freeze of Stillwater Enterprises Ltd. Approximately $78,000 was spent carrying out the following surveys between November 12, 1987 and February 2, 1988:

1) Geological mapping was carried out over the centre portion of the property at a scale of 1:10,000 (see Figure 2.3);

2) Rock chip sampling of quartz and calcite veins, quartz-carbonate stockwork zones, hydrothermal alteration zones and all pyritic rocks was carried out (see Figure 3.2);

3) Grid preparation and 'B' horizon soil sampling was carried out over 3 areas of the claim block. A total of 1453 samples were collected at 25 metre stations along grid lines spaced 50 and 100 metres apart;

4) Heavy minera [illegible] ng was carried out on all major [illegible] operty area.

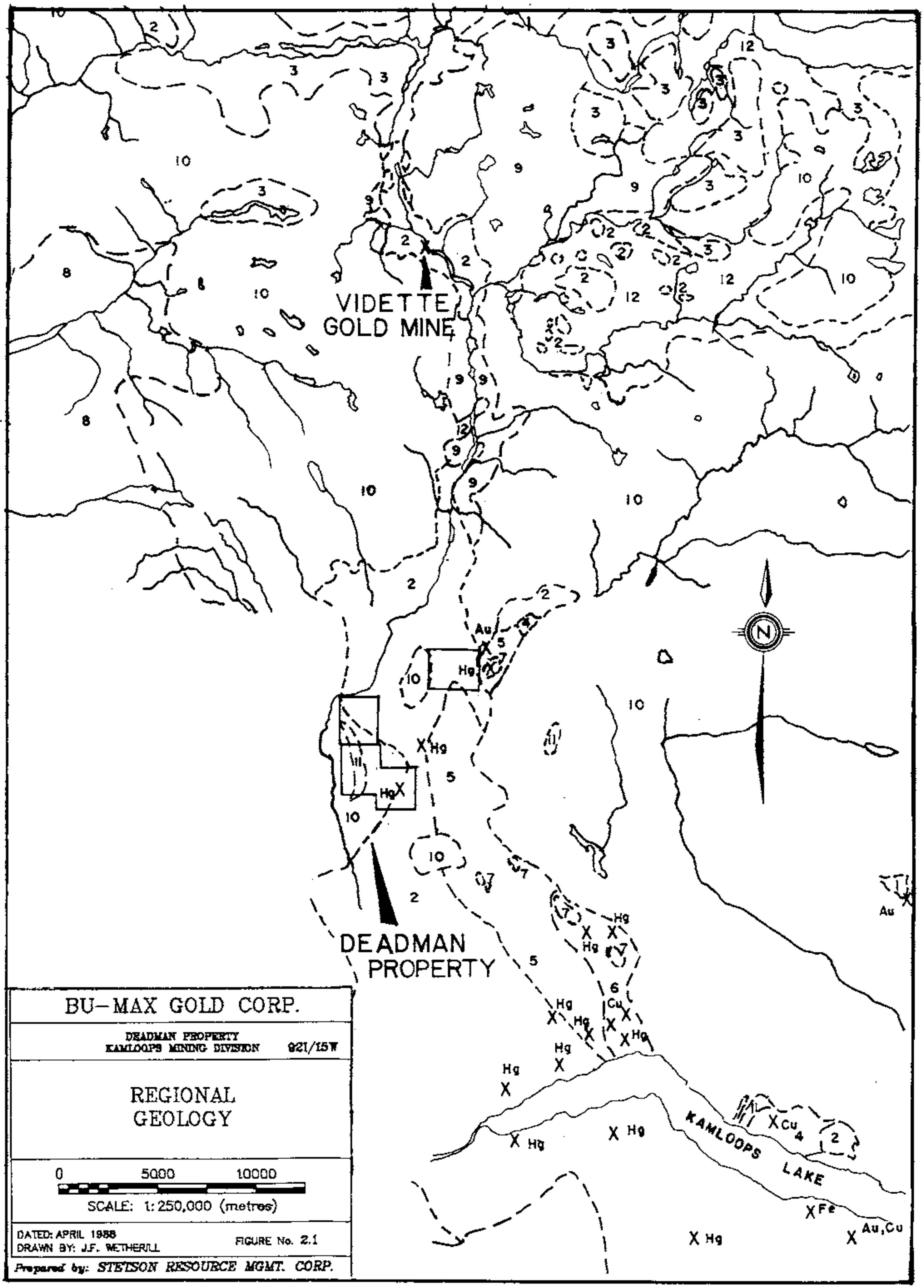
5) Stream sedi [illegible] arried out at two locations i [illegible]

Double Sided

2. GEOLOGY

2.1 Regional Geology

The Deadman River valley was mapped as part of the Nicola Map Sheet No. 886A by W. E. Cockfield of the Geological Survey of Canada between 1939 and 1943. The oldest units in the area are the Triassic volcanic and sedimentary rocks of the Nicola group. These rocks are now considered the southern equivalent of the Takla volcanics which comprise the Quesnel Trough. The Nicola group is overlain by Cretaceous sediments which have been intruded by Upper Cretaceous igneous rocks known as the Copper Creek Intrusions. The Cretaceous sediments and Copper Creek Intrusions are overlain by Tertiary volcanic rocks of the Kamloops group. Overlying the Kamloops group volcanics is a small wedge of thin bedded Tertiary sediments known locally as the Tranquille Beds.



BU-MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION 92I/15W

REGIONAL
GEOLOGY

DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 2.1

Prepared by: STETSON RESOURCE MGMT. CORP.

2.2 Regional Mineralization

Both the Nicola and Takla volcanic packages host several base and precious metal occurrences and deposits. A significant deposit of precious and accessory base metal mineralization is located on Vidette Lake 30 kilometres north of the Deadman property. During the 1930's the mine produced 29,869 oz of gold, 45,573 oz of silver, 96,614 lbs of copper and 356 lbs of lead from 54,199 tons milled. The average grade of the deposit was 0.55 oz per ton gold, 0.84 oz per ton silver, 0.09% copper and 0.0003% lead.

Ore deposits in the mine are described by Cockfield (1935) and B.C.M.M.A.R.(1936) as narrow continuous veins of quartz and sulphide clusters hosted by augite andesites of the Triassic Nicola group. The Nicola group is crosscut by granitic dykes indicating that a deeper seated intrusive body lies at depth.

Wall rock alteration is not considered important in the mine and leaching is rare. A steeply dipping northwesterly trending fault, Tertiary or younger in age, appears to control the mineralization. (R. Myers, B.C.M.E.M.P.R., Geological Survey, Personal Communication). Several episodes of faulting are apparent at the mine. The gold and silver is believed to be part of a chalcopyrite - quartz - telluride mineralization phase which followed both the original quartz - pyrite fissure filling and subsequent brecciation caused by fault movement. Further episodes of faulting truncated and brecciated the ore shoots. Barren calcite veins also crosscut the ore shoots. Films of crystalline gypsum covering joint planes in quartz are believed to have precipitated from circulating meteoric waters which acidified under pyrite oxidation and dissolved calcium carbonate from the wall rocks and veins and precipitated it as calcium sulphate.

The Vidette ore body is believed to fit an epithermal deposit model called the Closed-cell convection type which is characterized by the following features:

1) An extensive steeply dipping structure that acts as a channel way for mineralizing fluids.

2) Episodic brecciation and faulting followed by silicification and carbonate precipitation.

3) The presence of meteoric waters heated by cooling intrusive bodies at depth.

4) Impermeable host rocks that restrict meteoric fluids to the main structure.

2.3 Property Geology

The oldest rocks on the Deadman property belong to the Triassic Nicola group. These comprise andesite volcanics and cherty sediments. The volcanic assemblage consists of medium to dark green andesite flows, tuffs and breccias. The flows and tuffs are generally fine grained; breccia clasts vary in size up to 20 centimetres. Breccia clasts comprise Nicola volcanic flow rock and minor amounts of rhyolite and siliceous sediment clasts, both exhibiting dissolution features.

The volcanics are generally chloritized with varying degrees of epidote alteration in the form of stringers and blebs.

Nicola group sedimentary rocks comprise two distinct units. Unit 'L' is a grey bedded limestone sequence marked at bedding contacts by grey siltstone and shale beds. Unit 'C' is a cherty siltstone with a variable calcareous component.

Kamloops group volcanics and sediments of Miocene age or earlier unconformably overlie the Nicola group forming the cliffs and hoodoos found on the west side of the property and at higher elevations on the east side. The volcanics comprise predominantly andesite breccias with some andesite tuffs and flows and minor rhyolitic tuffs and breccias. Haematite coats extensive fracture surfaces, oxidizing to form deep red soils and gossans covering the western portions of the property. The sediments are called the Tranquille Beds which comprise a white granite cobble conglomerate grading up into a white cross-bedded sandstone unit.

Dark green and purple Miocene or later basalt flows are found at higher elevations on the property. Small sills of basalts similar in color and composition were observed at lower elevations crosscutting Nicola volcanics. The vesicles are filled by amygdules of zeolites and quartz. A flat lying basalt unit lies in fault contact with a quartz-carbonate alteration zone on the Cayuse claim suggesting a Tertiary age for the hydrothermal fluids or at least the controlling structure.

Cretaceous or Tertiary felsic stocks intrude Nicola volcanics and sediments. The intrusions are medium to fine grained, pale pink to buff in color, possibly granodioritic. Chlorite, clay alteration and pervasive weathering makes identification difficult. Haematite and limonite staining occurs in fractures in these rocks also.

2.4 Property Mineralization and Alteration

Epigenetic pyrite occurs in quartz stringers throughout the Nicola volcanics, but does not appear to have any associated anomalous metal concentrations.

Dolomite - quartz - carbonate veins are prevalent in the volcanics on the Cayuse claims. Limonite occurs within the veins and invades the country rock somewhat. Haematite occurs on fracture surfaces. These veins may be genetically related to an intense quartz-carbonate alteration zone controlled by a Tertiary fault structure on the east side of the Cayuse claims. Within this zone an east-southeasterly trending shear zone contains anomalous arsenic and antimony concentrations.

Stibnite mineralization occurs in limonitic quartz-dolomite veins and stockwork hosted by a brecciated andesite flow. Stibnite heals brecciated wall rock and crosscuts dolomite veins. In general the zone strikes northwesterly and can be traced for 120 metres in shallow old trenches. The dolomite hosts fine grained pyrite and occasional pods of stibnite up to 15 cm along the long axis. Metal values reach 0.5 ppm silver, 32 ppm copper, 94 ppm arsenic, and 27425 ppm antimony.

Pyrite and cinnabar ± sphalerite mineralization occurs in silicified dolomite-calcite veins and breccias with haematite and limonite staining. Episodic silicification is evidenced by crosscutting features in the breccias. Realgar is also reported to occur in this showing but was not observed by the writer.

3. GEOCHEMISTRY

3.1 Rock Chip Sampling

3.1.1 Sampling, Sample Preparation and Analytical Procedures

Rock chip samples were collected from all outcrops with visible mineralization, boxwork, iron staining or silicification, and from all quartz ± carbonate stockwork veins and alteration halos on Grid I.

Selected samples were taken where the width of the zone of interest could not be determined. Chip samples were taken at regular intervals (according to the size of the unit) across: the width of lenses and veins; wallrock to beds and veins; and gossanous, siliceous or pyritic zones. Larger chip sample widths were divided into 1.5 metre intervals. A total of 26 rock samples were collected and were sent for analysis.

The samples were places in numbered plastic bags and sent to Acme Analytical Laboratories Ltd. in Vancouver for analysis. In the laboratory, samples were put through primary and secondary crushers. A sub-sample of approximately 250 gm was then pulverized to minus 100 mesh. The pulp was then analyzed for gold by Atomic Absorption and for silver, copper, nickel, antimony and arsenic by ICP (Inductively Coupled Plasma).

3.1.2 Presentation and Discussion of Results

As discussed in section 2.4 three main zones of mineralization and alteration have been delineated on the Deadman property. Assay results, locations and descriptions of samples are given in Table 3.1 and shown on Map 3.1.

In addition to the mineralized zones several quartz-carbonate veins, stockwork zones and breccias contain anomalous levels of antimony and arsenic.

TABLE 3.1
Locations, Descriptions and Analytical Results for Rock Samples

Samp No.	Location	Rock Type With Mineralization	Width	Attd	Au ppb	Ag ppm	Cu ppm	Pb ppm	Ni ppm	Sb ppm	As ppm
	Grid I *										
7301	L10+00N 2+70W	Calcareous Chl andesite Brxx w/Rhy frags, vis Su's	slct		1	.2	6		3	2	6
7302	L9+00N 3+00W	Qz-Cb vein, Hem & Lim alt. Ci & Sphl in FW/HW	20cm	105/77N	2	.3	28		1	35	24
7303	L8+50N 0+00	Qz-Do banded vn sil'd host Rx, no vis Py	slct		1	.3	7		3	4	2
7304	L8+00N 1+60W	Qz-Do vn w/ HW/FW Brxx vis Py, Ci	106cm	130/66S	1	.4	5			3	10
7305	L10+00N 6+80E	Qz-Do vn, Lim vis Py	slct		1	.4	27			2	13
7306	L9+00N 6+25E	Limonitic Do no vis Su's	grab		2	.1		6		2	6
7307	L5+00N 1+00E	Limonitic Do w/ gry Lst frags no vis Su's	slct		2	.5	6			31	22
7308	L3+00N 2+50W	Do vn w/ HW/FW Brxx Lim & Hem alt	25cm	118/80S	1	.3	38			22	246
7309	L6+00N	Qz-Cb Brxx Chl, Hem, Lim altd vis Su	slct		1	.3	28			5	71
7310	L6+00N 3+00E	Buff subvolc vis Su, Lim alt	1.50cm		1	.4	51		3	2	61
7311	"	see 7310	"		1	.3	58		5	2	39
7312	L6+00N 5+00E	Shear zn Chl, Hem alt bslt FW, hydroth alt HW volc	30cm	119/40N	2	.3	20		74	2	15

***All Rocks Are From Grid I**

Samp No.	Location	Rock Type With Mineralization	Width	Attd	Au ppb	Ag ppm	Cu ppm	Pb ppm	Ni ppm	Sb ppm	As ppm
7313	L5+50N 1+00E	Qz/Cal vn no vis Su Hem alt	5cm	130/90	1	.4	7		1	20	68
7314	Criss Ck	Qz-Do Stwk Hem, Lim, Chl alt no vis Su	30cm	014/79E	1	.5	31		10	6	33
7315	L5+20N 0+75E	Msv Stbn Qz vn andesite Brxx wall Rx	slct		1	.2	22		13	20124	94
7316	L5+30N 0+75E	Stbn/Do pod Lim alt vis Su	15cm	165/35W	4	.4	32		9	27425	28
7317	"	Do vein Lim alt No vis Su	7.5cm	176/55W	1	.5	19		11	848	36
7318	Criss Creek Rd	Qz/Cb alt volc Lim, Hem no vis Su's	1.50cm	110/64S	1	.2	4		4	300	4
7319	Criss Ck Rd	Qz/Cb alt vol w/gouge Do vns Hgm, Lim no vis Su	1.50cm	90/74N	1	.4	47		5	31	38
7320	"	see 7319	"		2	.3	10		27	8	8
7321	"	Qz/Cb alt vol Lim alt FW gouge no vis Su	"	100/79S	1	.1	2		9	2	168
7322	"	"	"		1	.2	2		8	10	74
7323	"	"	"		1	.1	2		2	2	45
7324	"	"	"		4	.1	5		1	2	21
7325	"	" w/HW gouge	"	100/79S	1	.3	22		12	2	31
7326	"	Qz/Cb alt vol w/ FW gouge Lim alt	"	155/71E	1	.2	35		16	3	18

3.2 Soil Sampling

3.2.1 Sampling, Sample Preparation and Analytical Procedures

On the Deadman property soil samples were collected at 25 metre stations over three grids. Grid I comprises lines trending 040° spaced 100 metres apart. This grid was tied into a prominent knoll along the Criss Creek road 4.8 kilometres from the Deadman River road intersection. Grid I was oriented perpendicular to the general strike of quartz veins in the area. Grid II and III comprise lines trending north spaced 100 and 50 metres apart. Grid II was tied into an old reservoir and its access road, which intersects the Deadman River road just west of the river. Grid III was tied into Grid II at L850mW 700mN and a major drainage.

A total of 1,453 samples were collected from the "B" soil horizon at an average depth of 10-15 centimetres using a lightweight mattock. All samples were sent to Acme Analytical Laboratories Ltd. in Vancouver for analysis.

In the laboratory, samples were oven-dried at approximately 60°C. The dried samples were ring pulverized to minus 20 mesh and were analyzed for silver, copper, nickle antimony and arsenic by ICP (Inductively Coupled Plasma). To analyze for gold, the samples were ignited at 60°C, digested with hot concentrated nitric-aqua-regia, extracted by MIBK (organic solvent) and analyzed by graphite furnace AA (atomic absorption). Mercury has been shown to occur pervasively in soils covering most of the property by previous exploration programs.

TABLE 3.2
Statistical Data For Metal Values in "B" Horizon Soil Samples

Metal	N	Mean(x) pop.1	Mean(x) pop.2	Threshold	Anomalous
Grid I					
Au ppb	565	5	88	22	205
Ag ppm	565	0.2		0.4	1.1
Cu ppm	565	71	114	85	152
Ni ppm	565	23		31	51
Sb ppm	565	2		10	
As ppm	565	8	70	36	107

*Results show too much scatter; levels were chosen by visual examination.

Metal	N	Mean(x) pop.1	pop.2	Threshold	Anomalous
Grid II					
Au ppb	692	10		30	100
Ag ppm	692	*		0.5	
Cu ppm	692	90		128	200
Ni ppm	692	35		52	
Sb ppm	692	*		20	50
As ppm	692	8	63	27	218
Grid III					
Au ppb	196	*		10	30
Ag ppm	196	*		0.5	
Cu ppm	196	*		75	100
Ni ppm	196	*		50	
Sb ppm	196	*		10	
As ppm	196	*		100	

3.2.2 Treatment and Presentation of Results

In assessing the soil geochemical results, a frequency distribution, modelling program, Probplot by C. Stanley, was utilized. Elements which displayed single population characteristics had threshold and anomalous metal concentrations determined at the mean plus two standard deviations and the mean plus three standard deviations, respectively. Multi-population elements were separated into anomalous and background populations by threshold values of two standard deviations. Elements which displayed excessive scatter were separated into threshold and anomalous zones by regular interval levels. This data is given in Appendix II. Threshold and anomalous levels are shown in Table 3.2.

Sample locations and analytical results are shown on Figures 3.2.I.1 to 3.2.III.6.

3.2.3 Discussion of Results

Grid I

Anomalous levels of copper, nickel and arsenic occur in several zones in the soils. Anomalous levels of gold, silver and arsenic occur as only one or two station anomalies.

Anomalous copper values are the most widespread occurring in four large and several small zones south of line 500mN and in a few small zones over the rest of the grid. Arsenic shows a moderate correlation with copper in that anomalous arsenic levels occur mostly within the copper anomalies south of line 500mN.

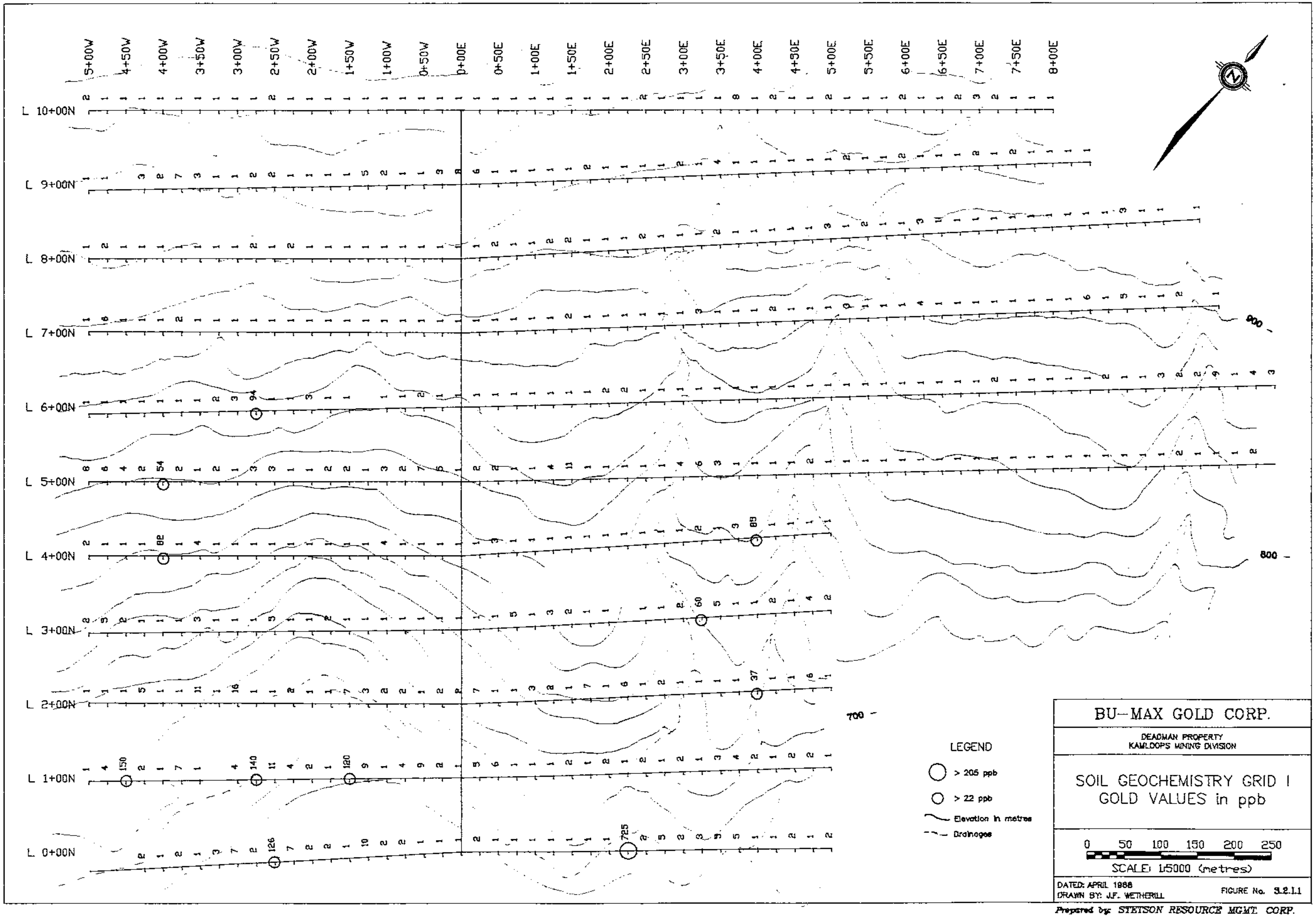
An epithermal dolomite vein with siliceous breccias in both the hanging wall and footwall occurs within the copper - arsenic anomaly at 300mN and 220mW. A selected sample from the vein contains 246 ppm arsenic.

A copper - arsenic anomaly centred at 350mN and 150mE may be related to a Cretaceous - Tertiary felsic intrusive body.

An arsenic - copper anomaly centred at 900mN and 600mE fringes a gulley which is suspected to follow the structural control for the Cayuse Iron Carbonate Zone. A quartz - dolomite vein is exposed within this zone.

Nickel occurs almost exclusively from copper. Anomalous nickel values occur predominantly in an extensive southeastery zone just west of the Iron Carbonate Zone. The nickel zone is bound on both sides by parallel creeks, the easterly of which contacts the western edge of the Iron Carbonate Zone.

Anomalous gold and silver occur coincidently at two sites, one within the anomalous nickel zone and the other within the anomalous copper zone. Both anomalies occur on line 0mN proximal to Criss Creek and may be attributed to placer concentrations.


BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID I
GOLD VALUES in ppb
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.1.1
Prepared by: STETSON RESOURCE MGMT. CORP.
LEGEND
> 205 ppb
> 22 ppb
Elevation in metres
Drainages
L 10+00N
L 9+00N
L 8+00N
L 7+00N
L 6+00N
L 5+00N
L 4+00N
L 3+00N
L 2+00N
L 1+00N
L 0+00N
5+00W
4+50W
4+00W
3+50W
3+00W
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8+00E
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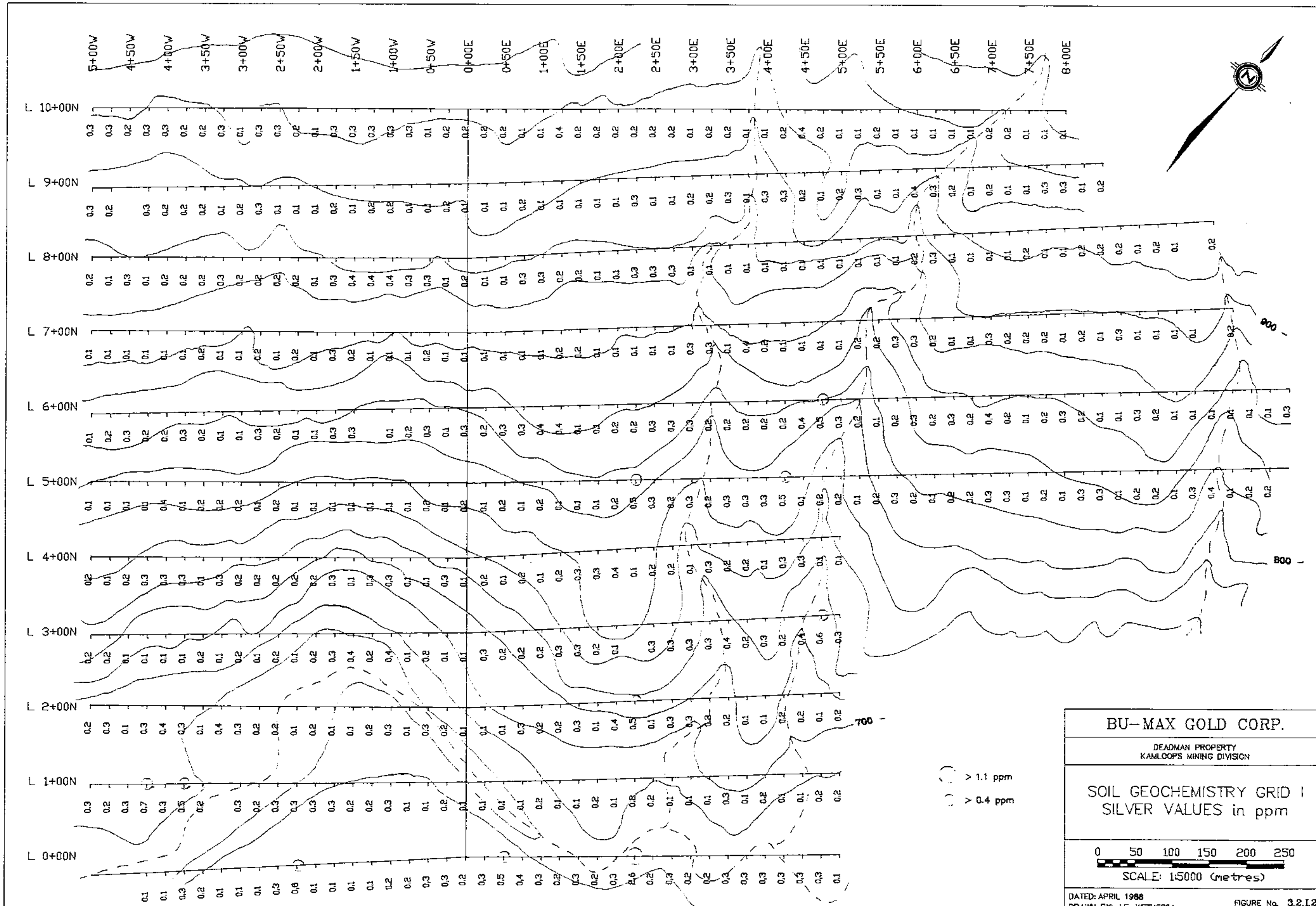
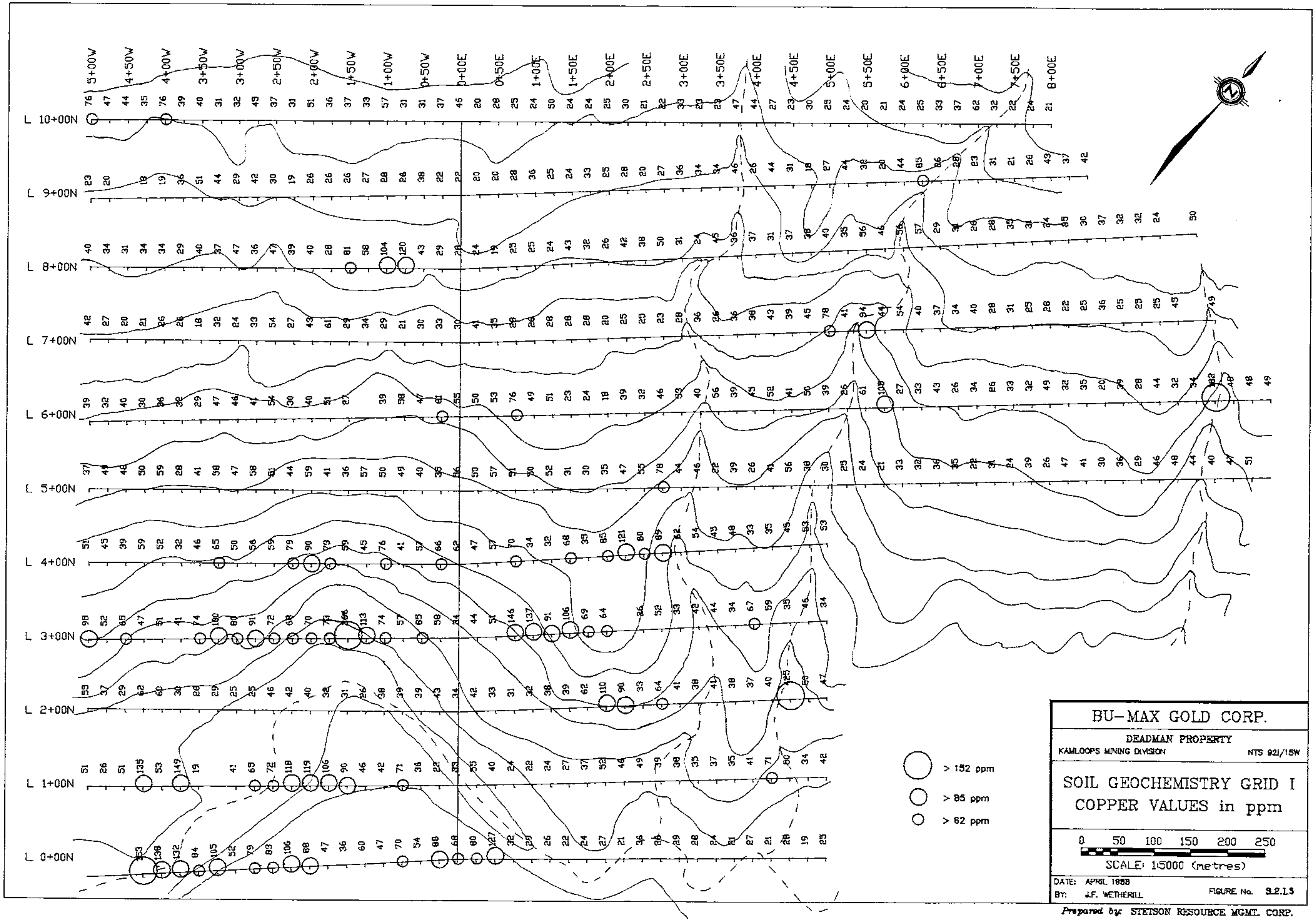


Prepared by: STETSON RESOURCE MGMT. CORP.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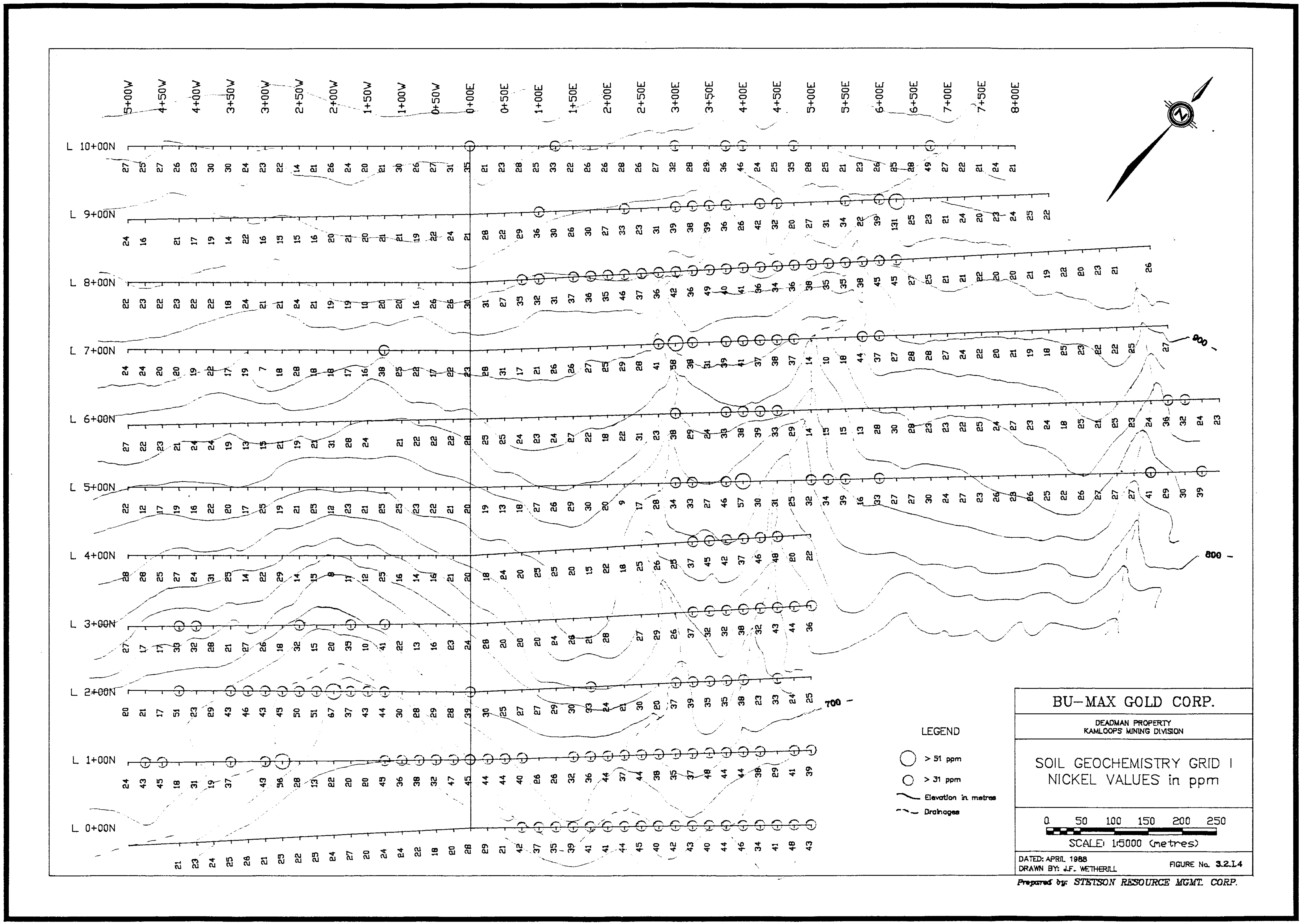
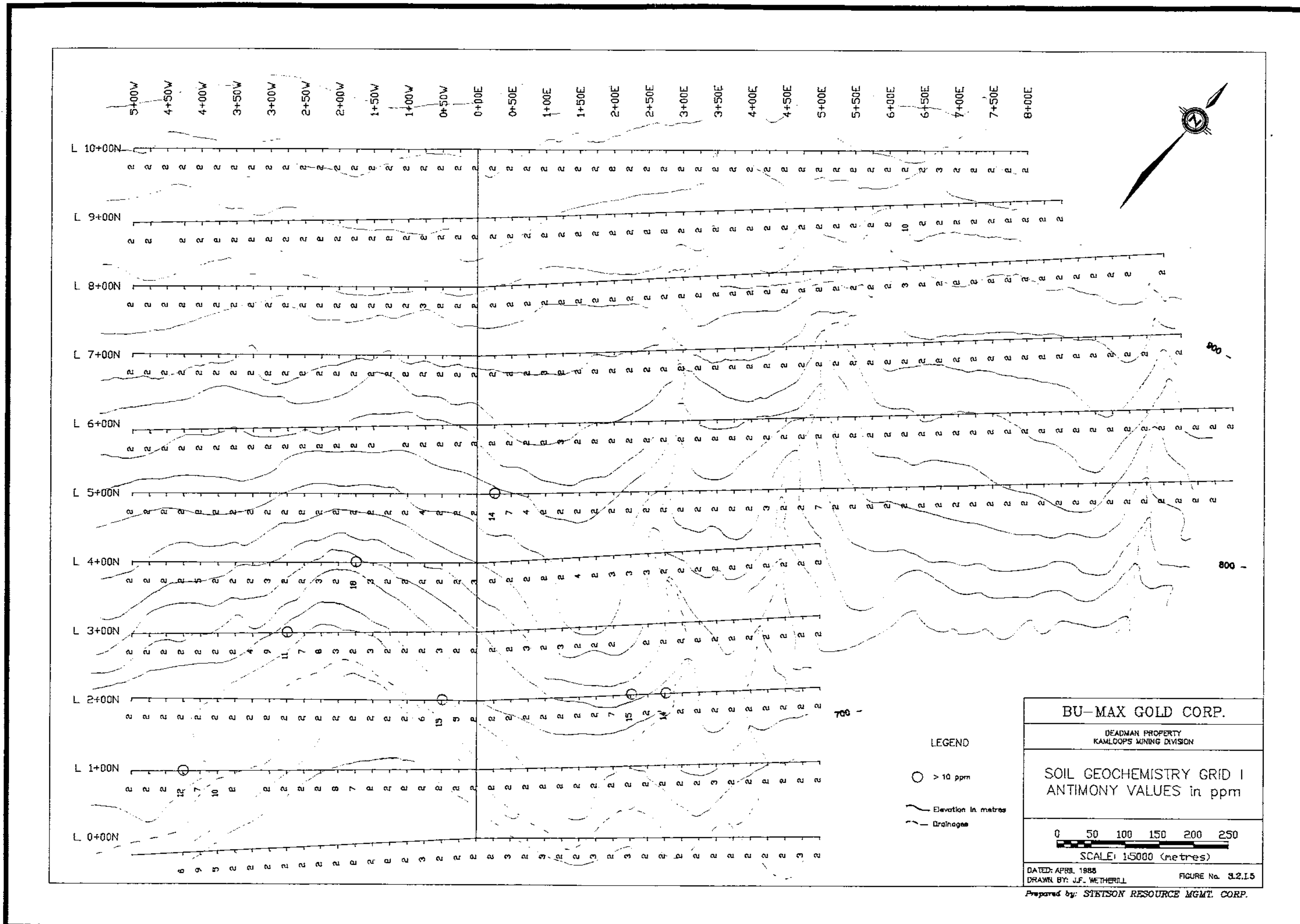
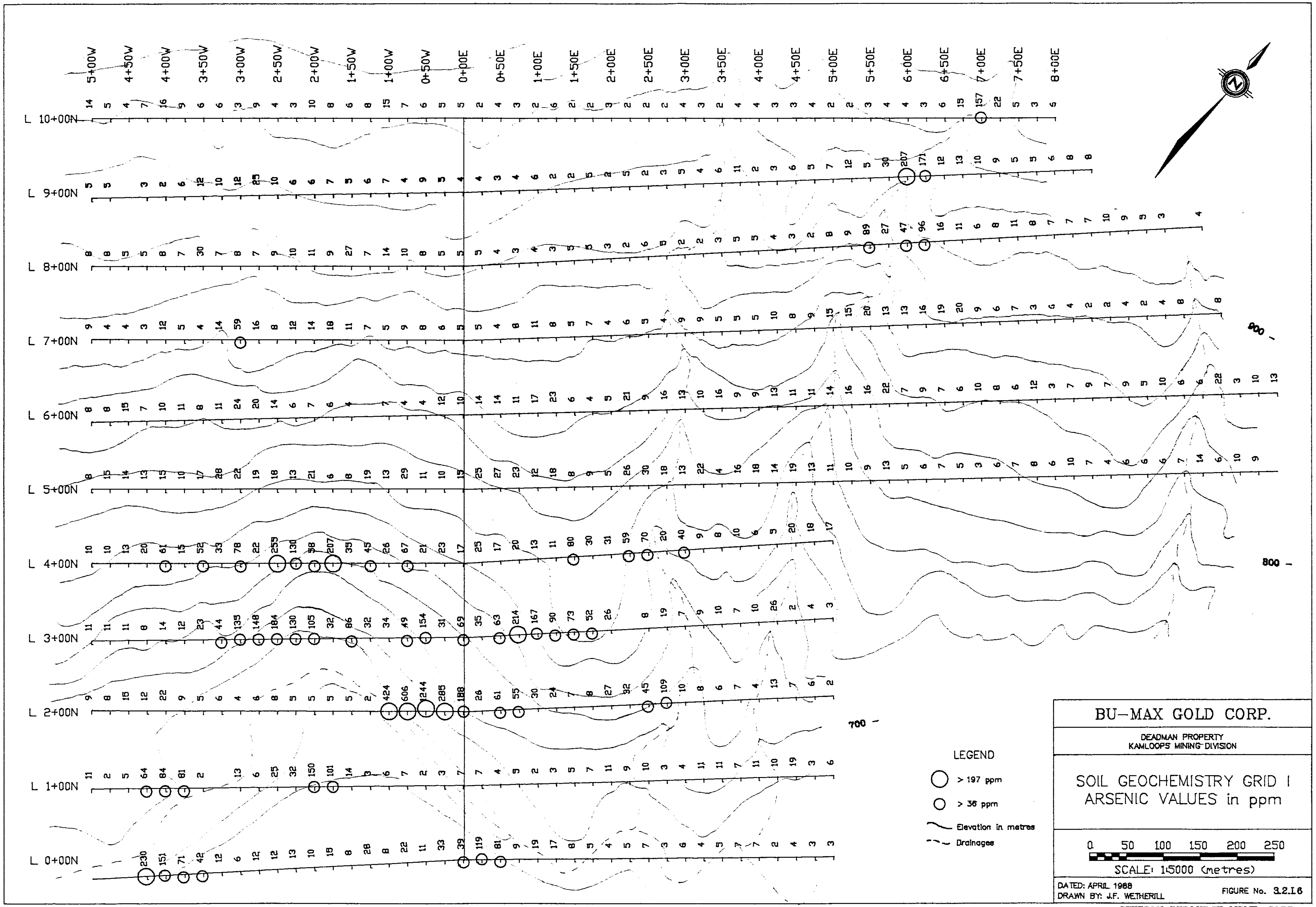
2+00E
2+50E
3+00E
3+50E
4+00E
4+50E
5+00E
5+50E
6+00E
6+50E
7+00E
7+50E
8+00E
N
> 152 ppm
> 85 ppm
> 62 ppm
BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
NTS 92I/15W
SOIL GEOCHEMISTRY GRID I
COPPER VALUES in ppm
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATE: APRIL 1988
BY: J.F. WETHERILL
FIGURE No. 3.2.1.3
Prepared by: STETSON RESOURCE MGMT. CORP.


BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID I
NICKEL VALUES in ppm
SCALE: 1:5000 (metres)
0 50 100 150 200 250
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.1.4
Prepared by: STETSON RESOURCE MGMT. CORP.
LEGEND
> 51 ppm
> 31 ppm
Elevation in metres
Drainages
L 10+00N
L 9+00N
L 8+00N
L 7+00N
L 6+00N
L 5+00N
L 4+00N
L 3+00N
L 2+00N
L 1+00N
L 0+00N
5+00W
4+50W
4+00W
3+50W
3+00W
2+50W
2+00W
1+50W
1+00W
0+50W
0+00E
0+50E
1+00E
1+50E
2+00E
2+50E
3+00E
3+50E
4+00E
4+50E
5+00E
5+50E
6+00E
6+50E
7+00E
7+50E
8+00E
900
800
700


5+00W 4+50W 4+00W 3+50W 3+00W 2+50W 2+00W 1+50W 1+00W 0+50W 0+00E 0+50E 1+00E 1+50E 2+00E 2+50E 3+00E 3+50E 4+00E 4+50E 5+00E 5+50E 6+00E 6+50E 7+00E 7+50E 8+00E
L 10+00N
L 9+00N
L 8+00N
L 7+00N
L 6+00N
L 5+00N
L 4+00N
L 3+00N
L 2+00N
L 1+00N
L 0+00N
900
800
700
LEGEND
> 10 ppm
Elevation in metres
Drainages
BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID I
ANTIMONY VALUES in ppm
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.1.5
Prepared by: STETSON RESOURCE MGMT. CORP.



Prepared by: STETSON RESOURCE MGMT. CORP.

Grid II

Anomalous arsenic concentrations were found in soils covering the central portion of Grid II from 200mW to 850mW between 025mN and 625mN. Anomalous copper levels occur within this area in two smaller zones.

A few small anomalous arsenic zones also occur at 025mN and 600mN on line 1000mW.

Anomalous antimony concentrations were found in soils covering four small zones having a moderate correlation with copper.

Silver values are generally low; most anomalous levels occur at isolated sites. One small anomalous silver zone occurs within the central arsenic - copper anomaly.

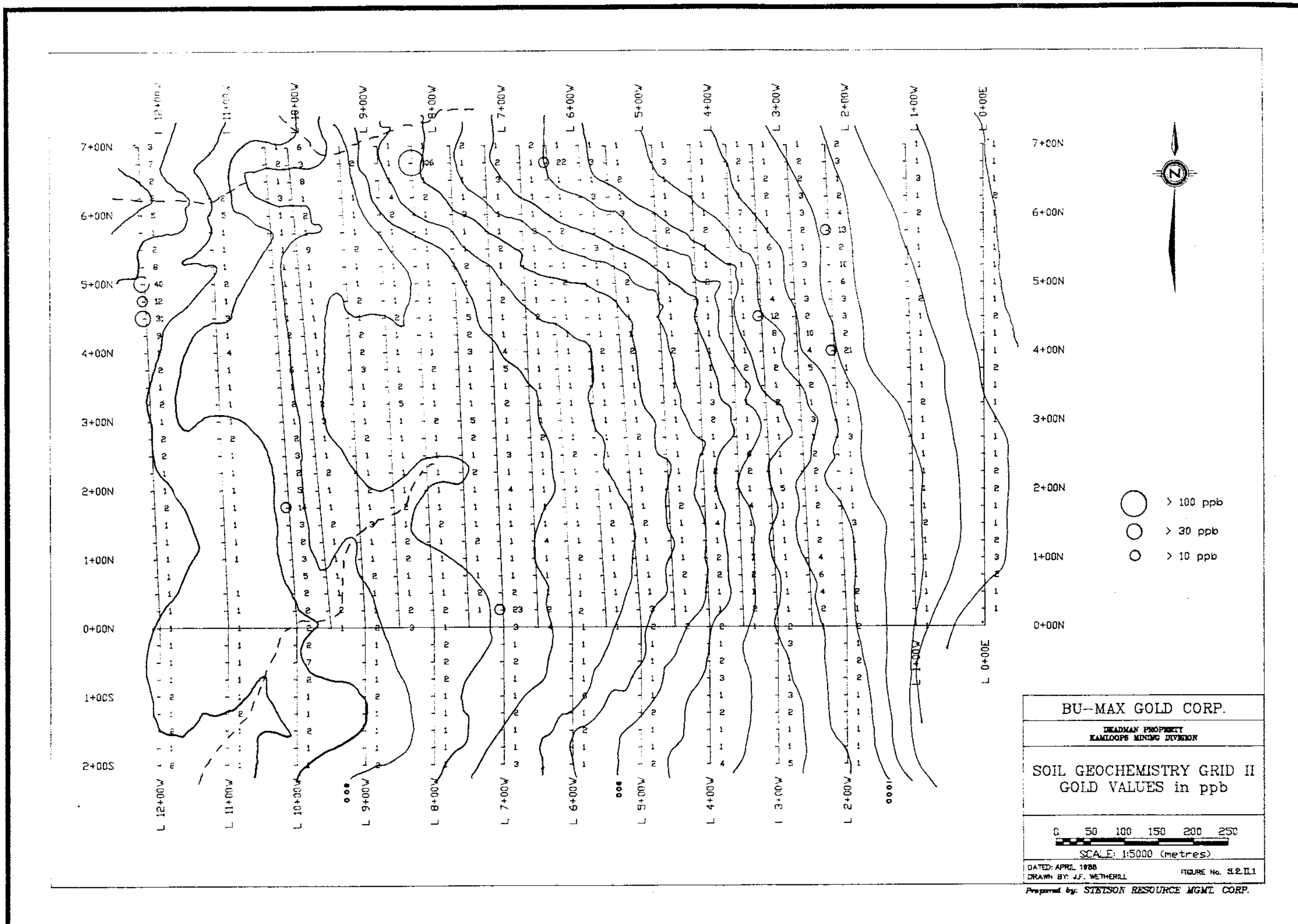
Both gold and nickel show no correlation with other elements. Anomalous levels of each usually occur as one or two station anomalies. A three station gold anomaly occurs from 450mN to 500mN on line 1200mW at the western edge of the grid.

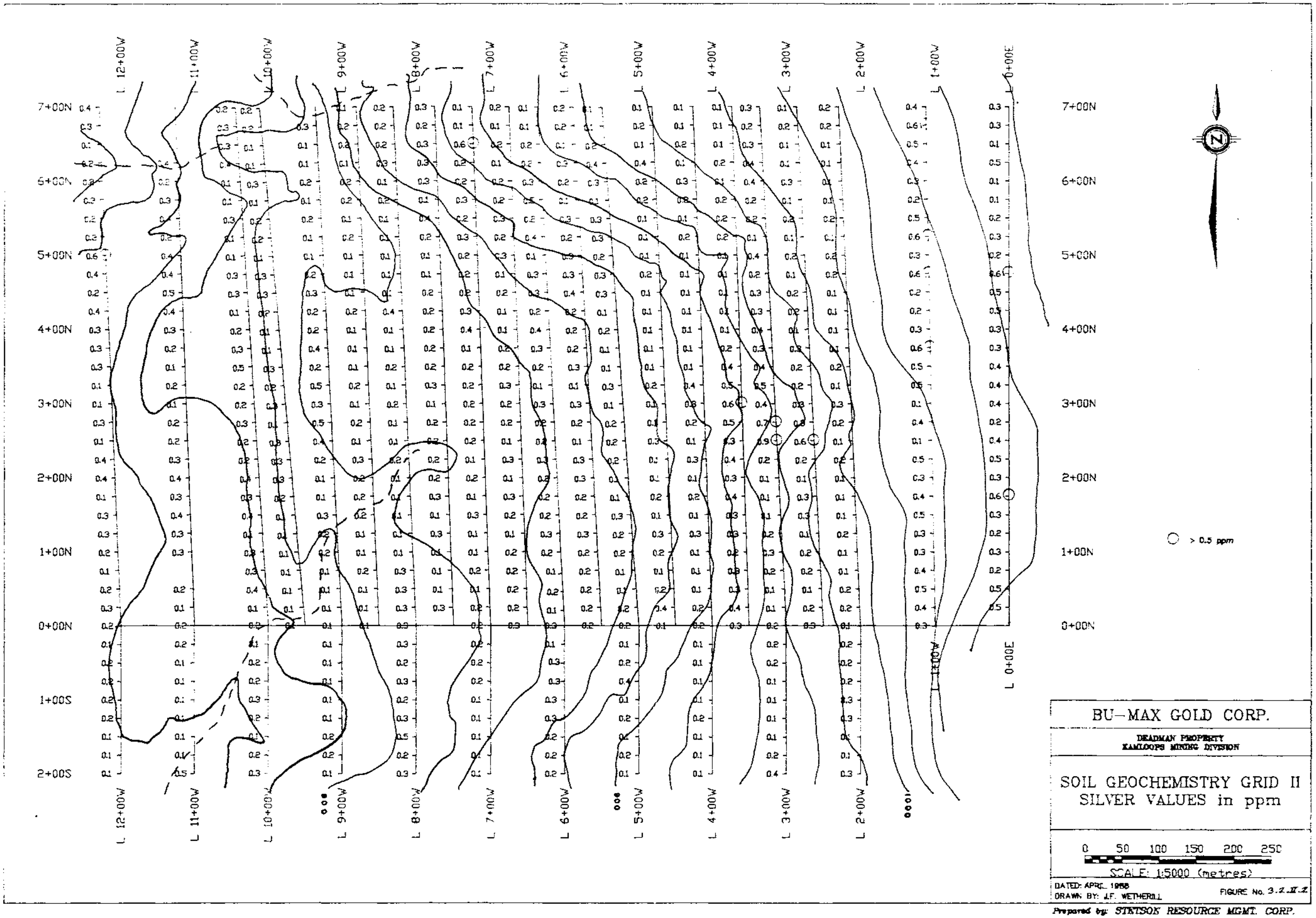
The eastern edge of the antimony - copper anomaly is believed to indicate the contact between the Miocene basalts and the underlying Triassic Nicola group. The highest arsenic and copper values occur proximal to a felsic intrusive belonging to the Cretaceous - Tertiary Kamloops group. A few anomalous nickel values also occur on the northern edge of this intrusive body.

Grid III

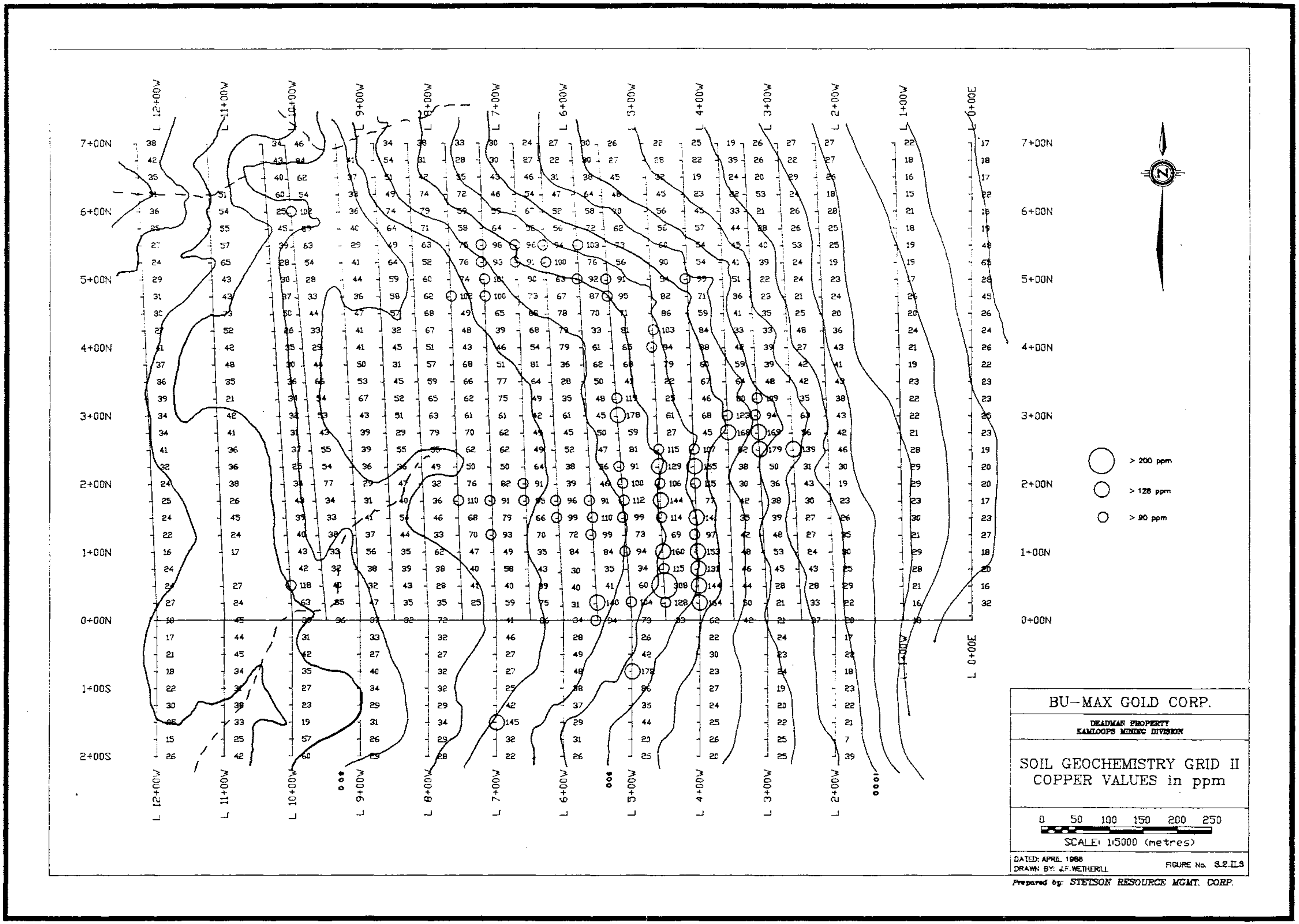
Anomalous levels of arsenic, copper and nickel occur in several zones which show a general zoning pattern from southwest to northeast. Silver occurs in anomalous concentrations in small zones within the larger nickel and copper anomalies. Zones of anomalous levels of antimony occur proximal to the copper anomalies. Anomalous gold values occur at two isolated sites, one of wich lies within an arsenic anomaly on the edge of a fault.

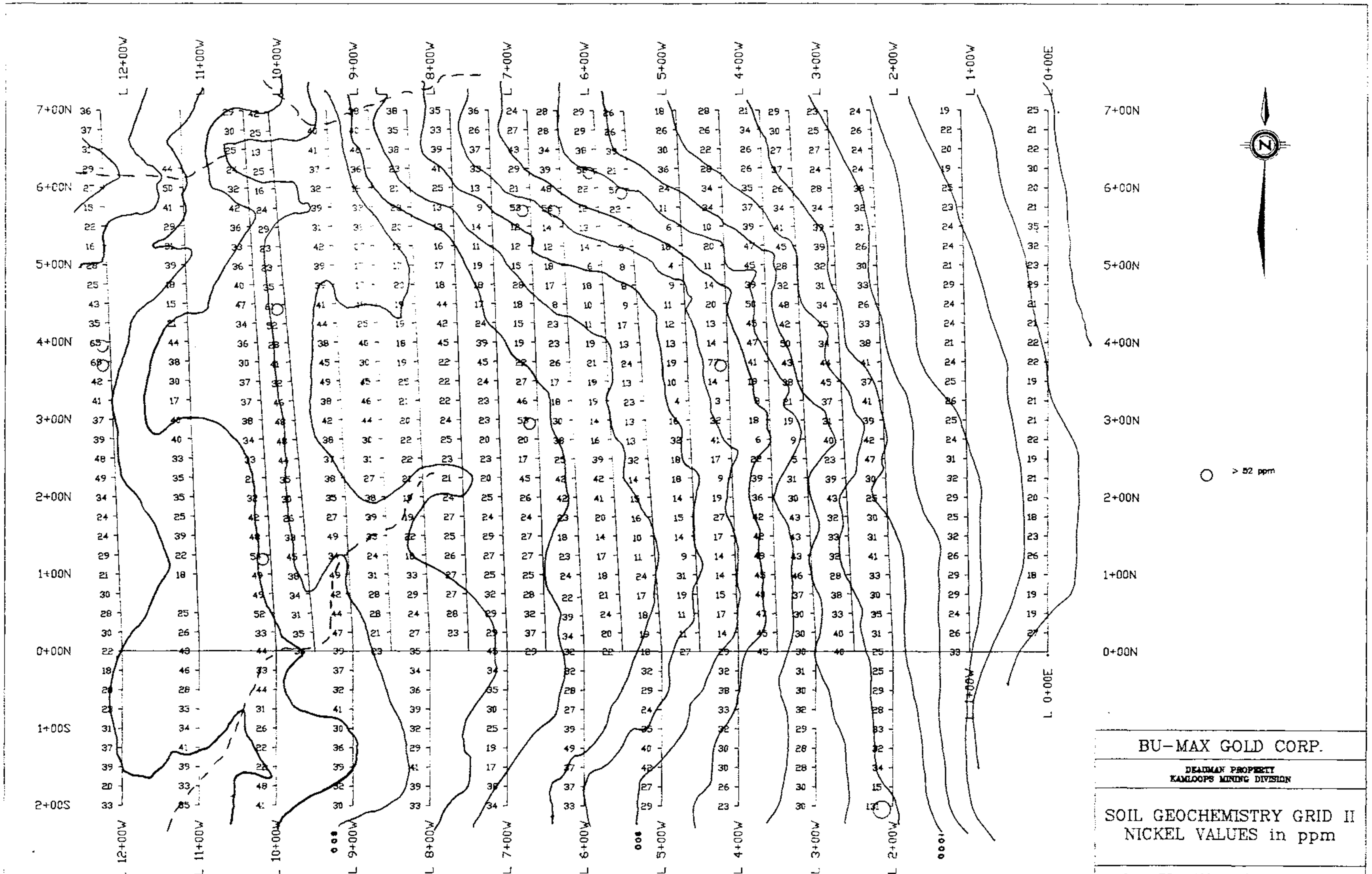
The copper - antimony anomalies occur in soils overlying the Tertiary Tranquille Beds. A few copper anomalies occur over both Tertiary and Triassic volcanics. The other elements show no affinity to lithology.


BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID II
GOLD VALUES in ppb
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.II.1
Prepared by: STETSON RESOURCE MGMT. CORP.
> 100 ppb
> 30 ppb
> 10 ppb
N
7+00N
6+00N
5+00N
4+00N
3+00N
2+00N
1+00N
0+00N
1+00S
2+00S
L 12+00W
L 11+00W
L 10+00W
L 9+00W
L 8+00W
L 7+00W
L 6+00W
L 5+00W
L 4+00W
L 3+00W
L 2+00W
L 1+00W
L 0+00E



L 12+00W
L 11+00W
L 10+00W
L 9+00W
L 8+00W
L 7+00W
L 6+00W
L 5+00W
L 4+00W
L 3+00W
L 2+00W
L 1+00W
L 0+00E
7+00N
6+00N
5+00N
4+00N
3+00N
2+00N
1+00N
0+00N
1+00S
2+00S
N
> 0.5 ppm
BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID II
SILVER VALUES in ppm
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.II.2
Prepared by: STETSON RESOURCE MGMT. CORP.


BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID II
COPPER VALUES in ppm
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.II.3
Prepared by: STETSON RESOURCE MGMT. CORP.
> 200 ppm
> 128 ppm
> 90 ppm
N
7+00N
6+00N
5+00N
4+00N
3+00N
2+00N
1+00N
0+00N
1+00S
2+00S
L 12+00W
L 11+00W
L 10+00W
L 9+00W
L 8+00W
L 7+00W
L 6+00W
L 5+00W
L 4+00W
L 3+00W
L 2+00W
L 1+00W
L 0+00E



BU-MAX GOLD CORP.

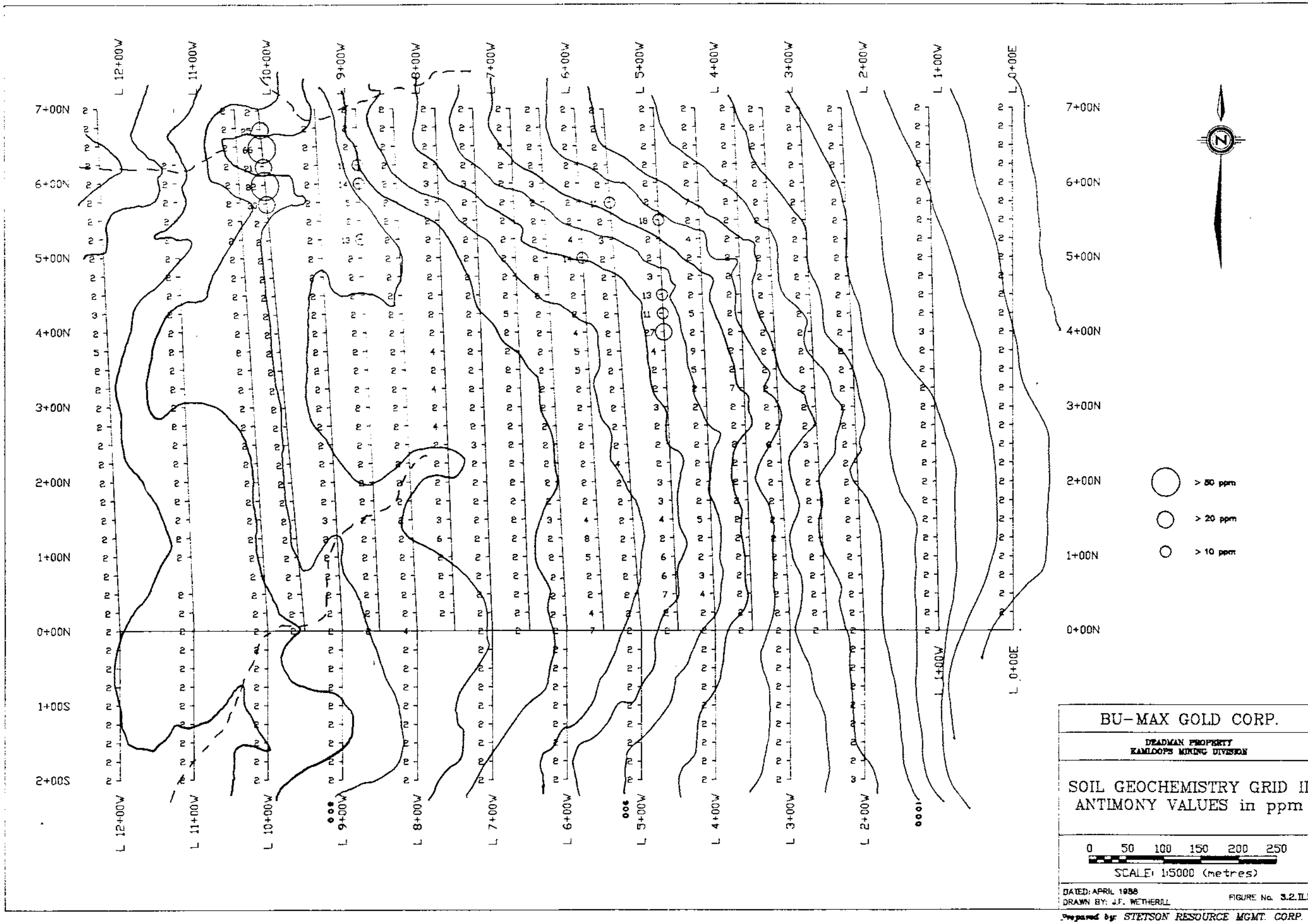
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

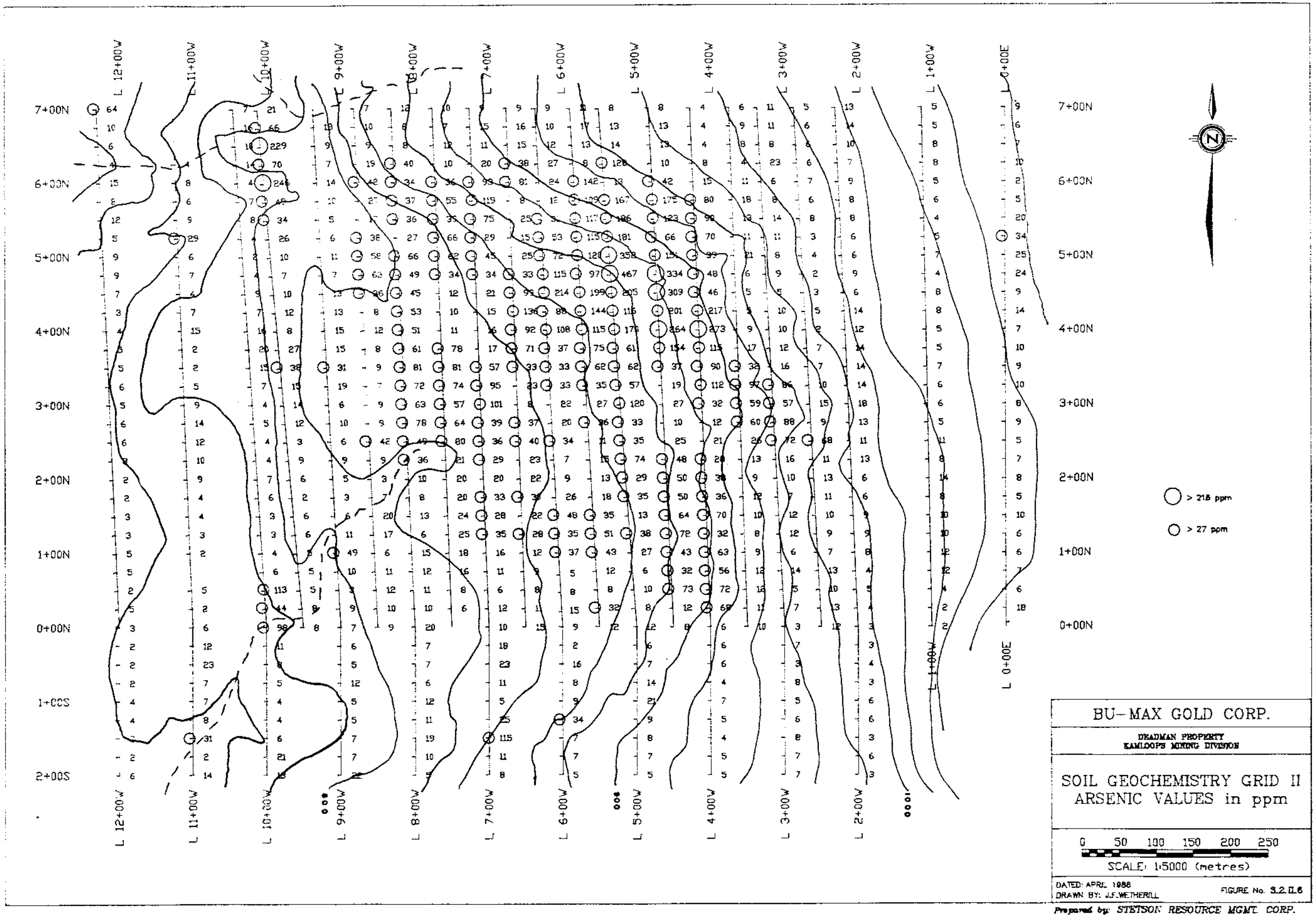
SOIL GEOCHEMISTRY GRID II
NICKEL VALUES in ppm

0 50 100 150 200 250
SCALE: 1:5000 (metres)

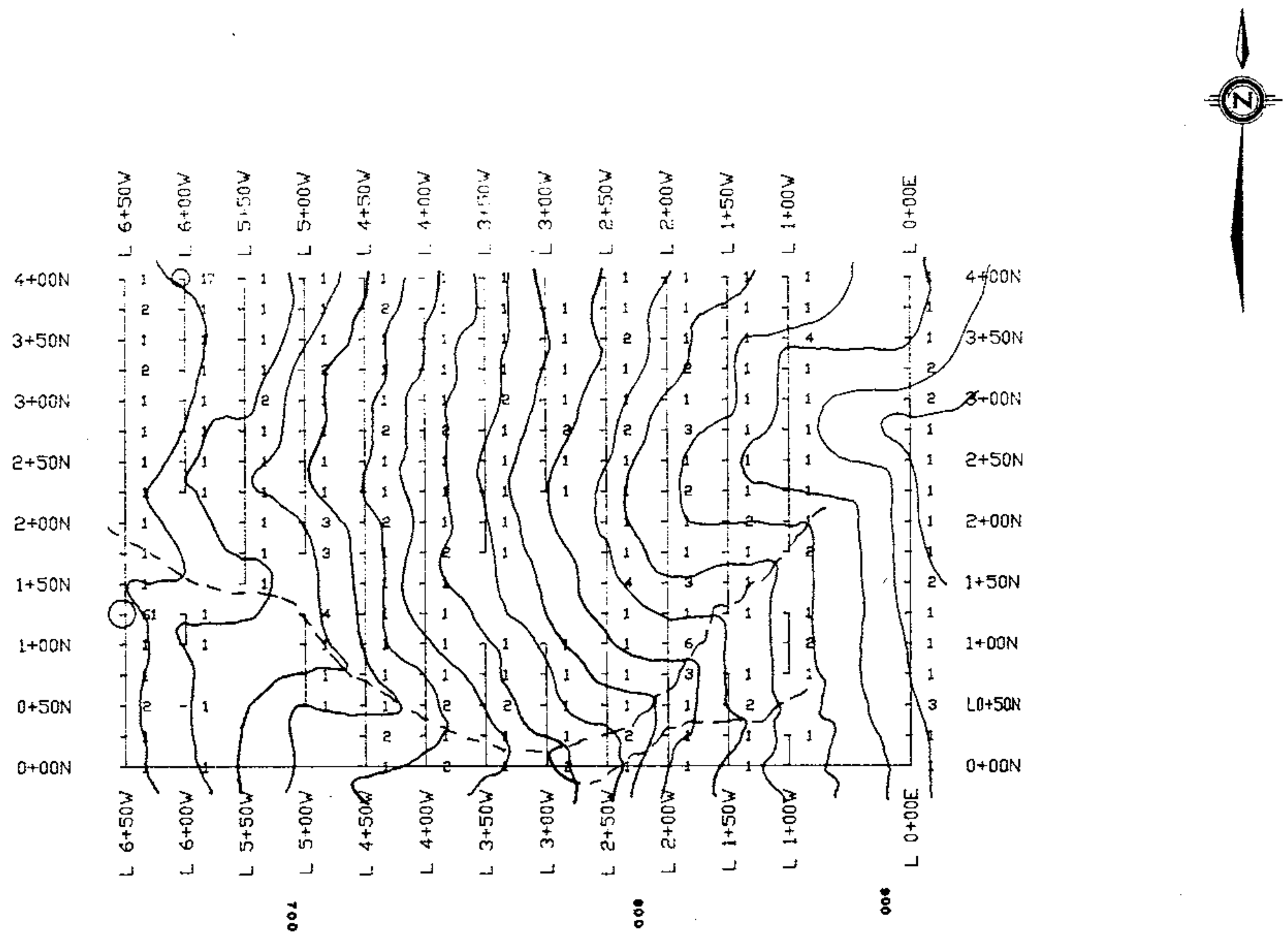
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.II.4

Prepared by: STETSON RESOURCE MGMT. CORP.


BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID II
ANTIMONY VALUES in ppm
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL
FIGURE No. 3.2.II.5
Prepared by: STETSON RESOURCE MGMT. CORP.
> 50 ppm
> 20 ppm
> 10 ppm
N
L 12+00W
L 11+00W
L 10+00W
L 9+00W
L 8+00W
L 7+00W
L 6+00W
L 5+00W
L 4+00W
L 3+00W
L 2+00W
L 1+00W
L 0+00E
7+00N
6+00N
5+00N
4+00N
3+00N
2+00N
1+00N
0+00N
1+00S
2+00S



BU-MAX GOLD CORP.
DEADMAN PROPERTY
KAMLOOPS MINING DIVISION
SOIL GEOCHEMISTRY GRID II
ARSENIC VALUES in ppm
0 50 100 150 200 250
SCALE: 1:5000 (metres)
DATED: APRIL 1988
DRAWN BY: J.F.WETHERILL
FIGURE No. 3.2.II.6
Prepared by: STETSON RESOURCE MGMT. CORP.
> 218 ppm
> 27 ppm
N
L 12+00W
L 11+00W
L 10+00W
L 9+00W
L 8+00W
L 7+00W
L 6+00W
L 5+00W
L 4+00W
L 3+00W
L 2+00W
L 1+00W
L 0+00E
7+00N
6+00N
5+00N
4+00N
3+00N
2+00N
1+00N
0+00N
1+00S
2+00S



> 30 ppm

> 10 ppm

BU–MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

SOIL GEOCHEMISTRY GRID III
GOLD VALUES in ppb

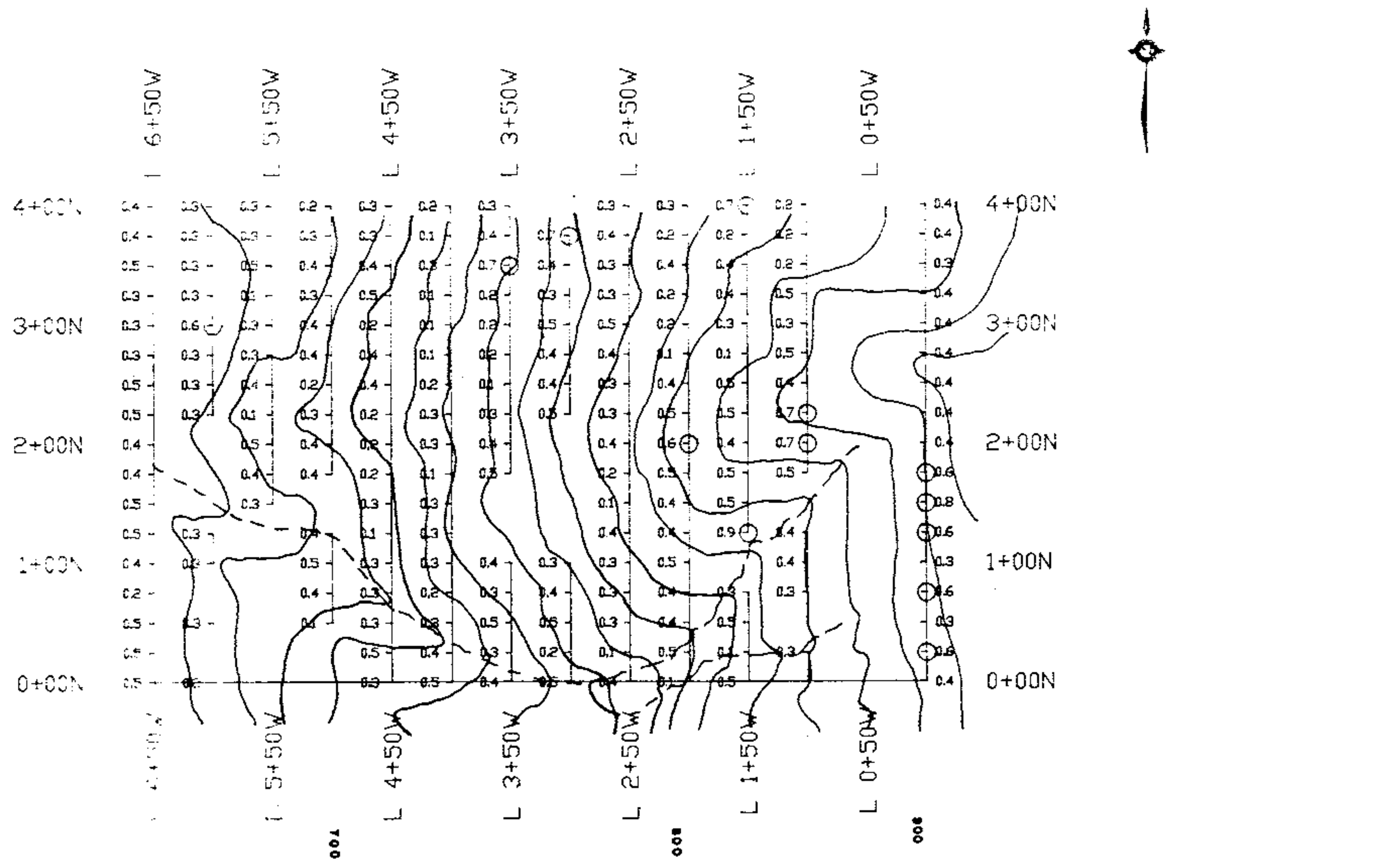
0 50 100 150 200 250

SCALE: 1:5000 (metres)

DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL

FIGURE No. S.2.III.4

Prepared by: STETSON RESOURCE MGMT. CORP.



BU–MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

SOIL GEOCHEMISTRY GRID III
SILVER VALUES in ppm

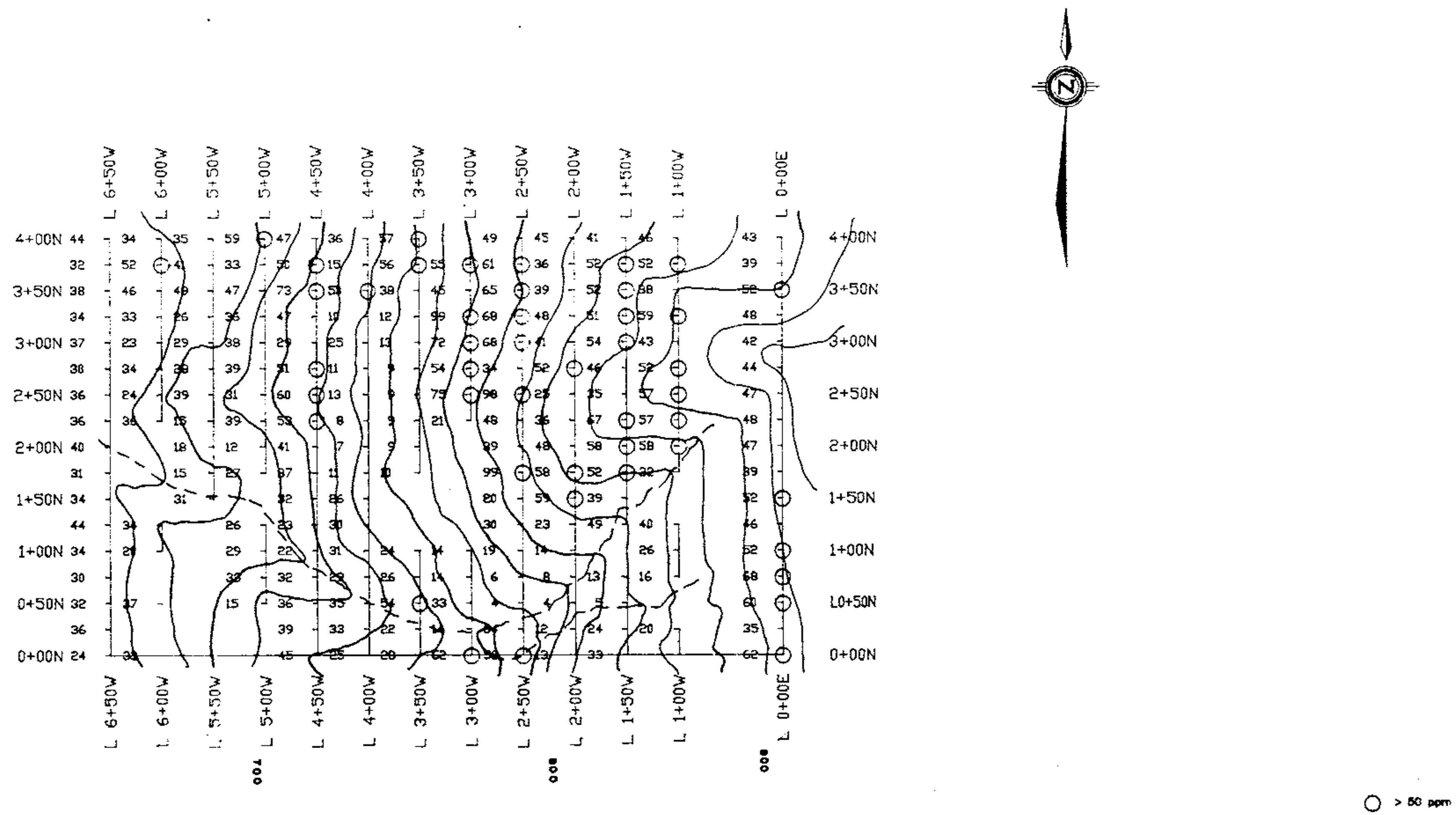
0 50 100 150 200 250

SCALE: 1:5000 (metres)

DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL

FIGURE No. 8.2.III.2

Prepared by: STETSON RESOURCE MGMT. CORP.



BU-MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

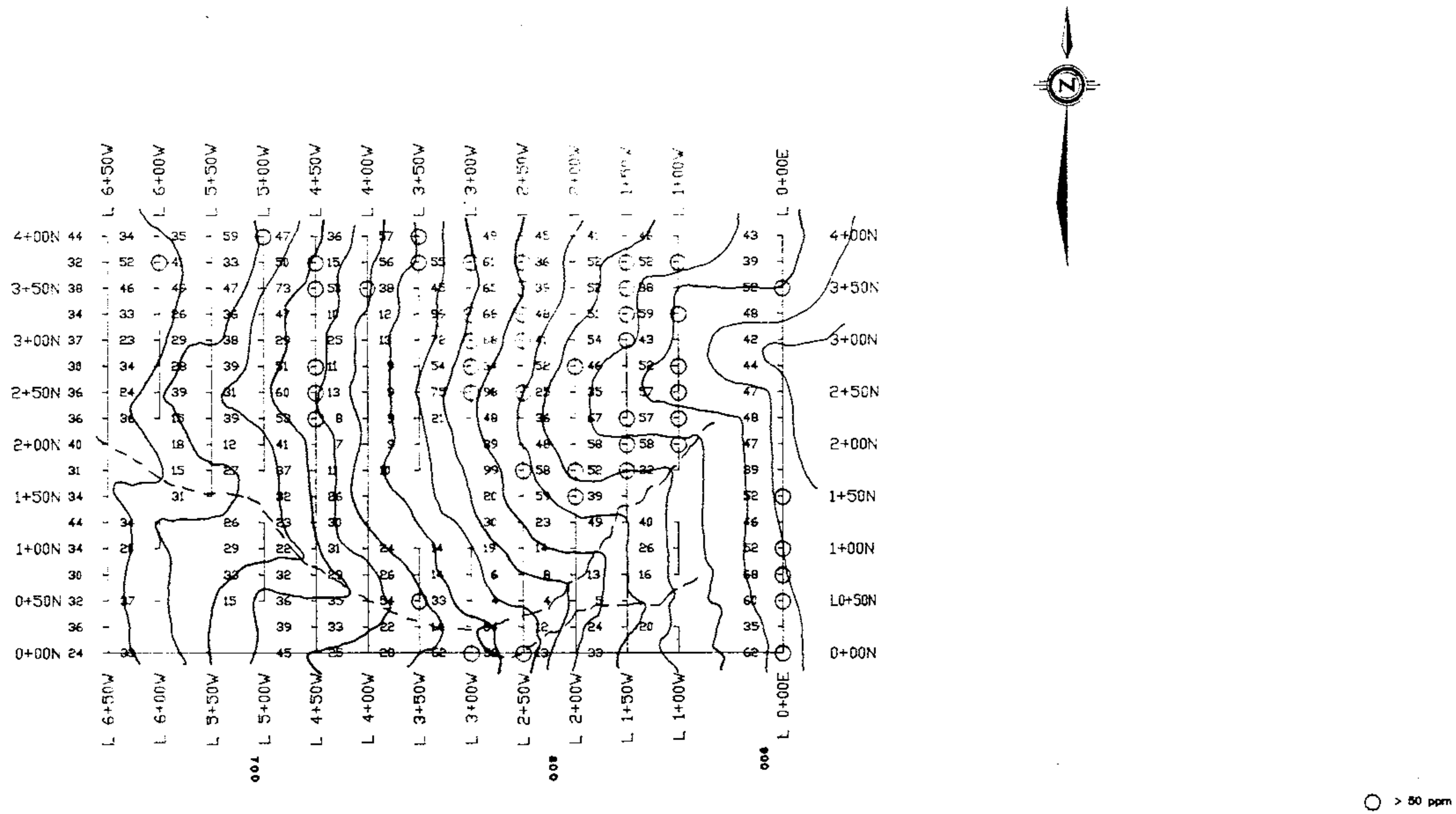
SOIL GEOCHEMISTRY GRID III
NICKEL VALUES in ppm

0 50 100 150 200 250
SCALE 1:5000 (metres)

DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL

FIGURE No. 3.2.III.4

Prepared by: STETSON RESOURCE MGMT. CORP.



BU-MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

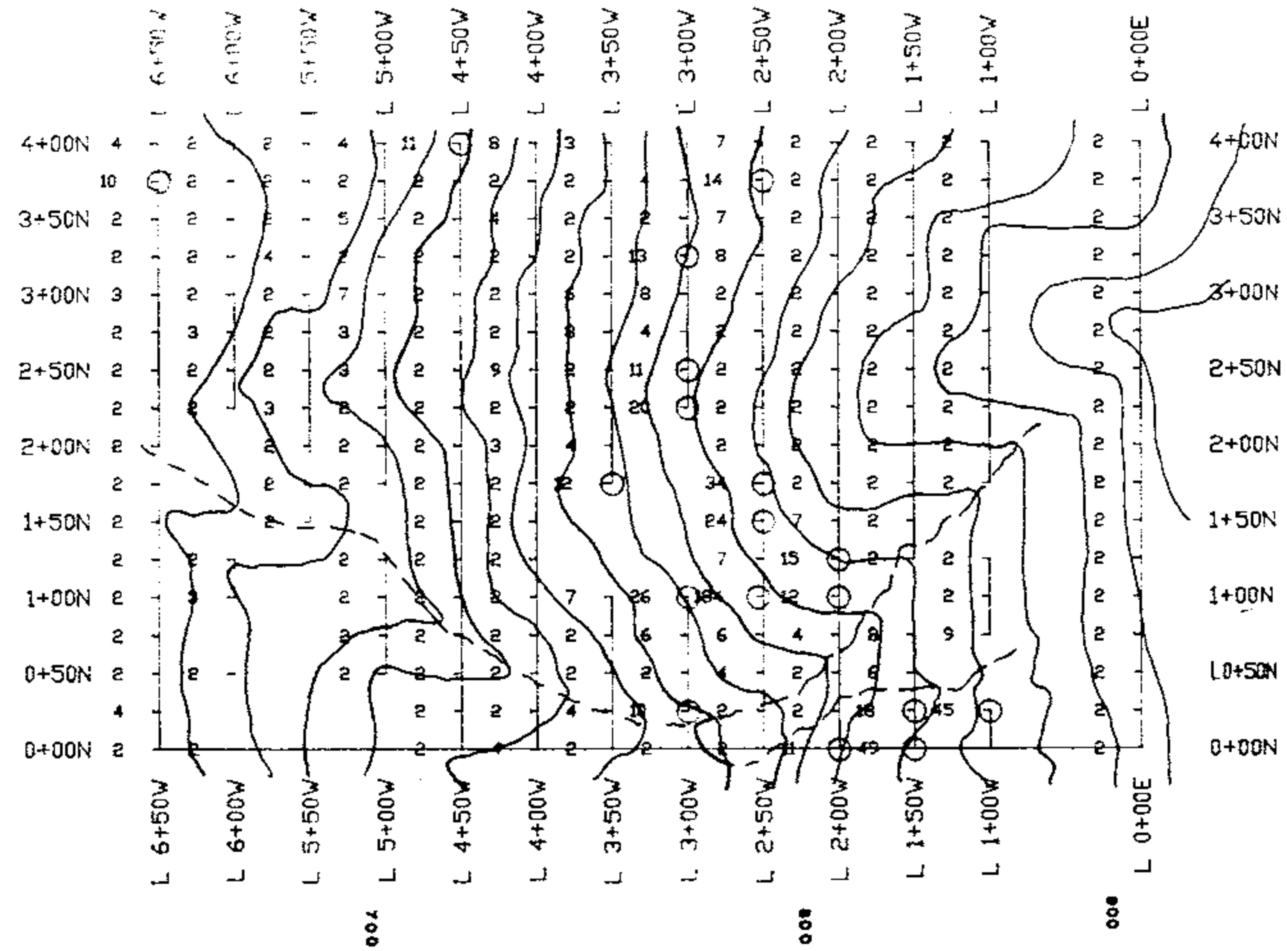
SOIL GEOCHEMISTRY GRID III
NICKEL VALUES in ppm

0 50 100 150 200 250
SCALE: 1:5000 (metres)

DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL

FIGURE No. 3.2.III.4

Prepared by: STETSON RESOURCE MGMT. CORP.



○ > 10 ppm

BU-MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

SOIL GEOCHEMISTRY GRID III
ANTIMONY VALUES in ppm

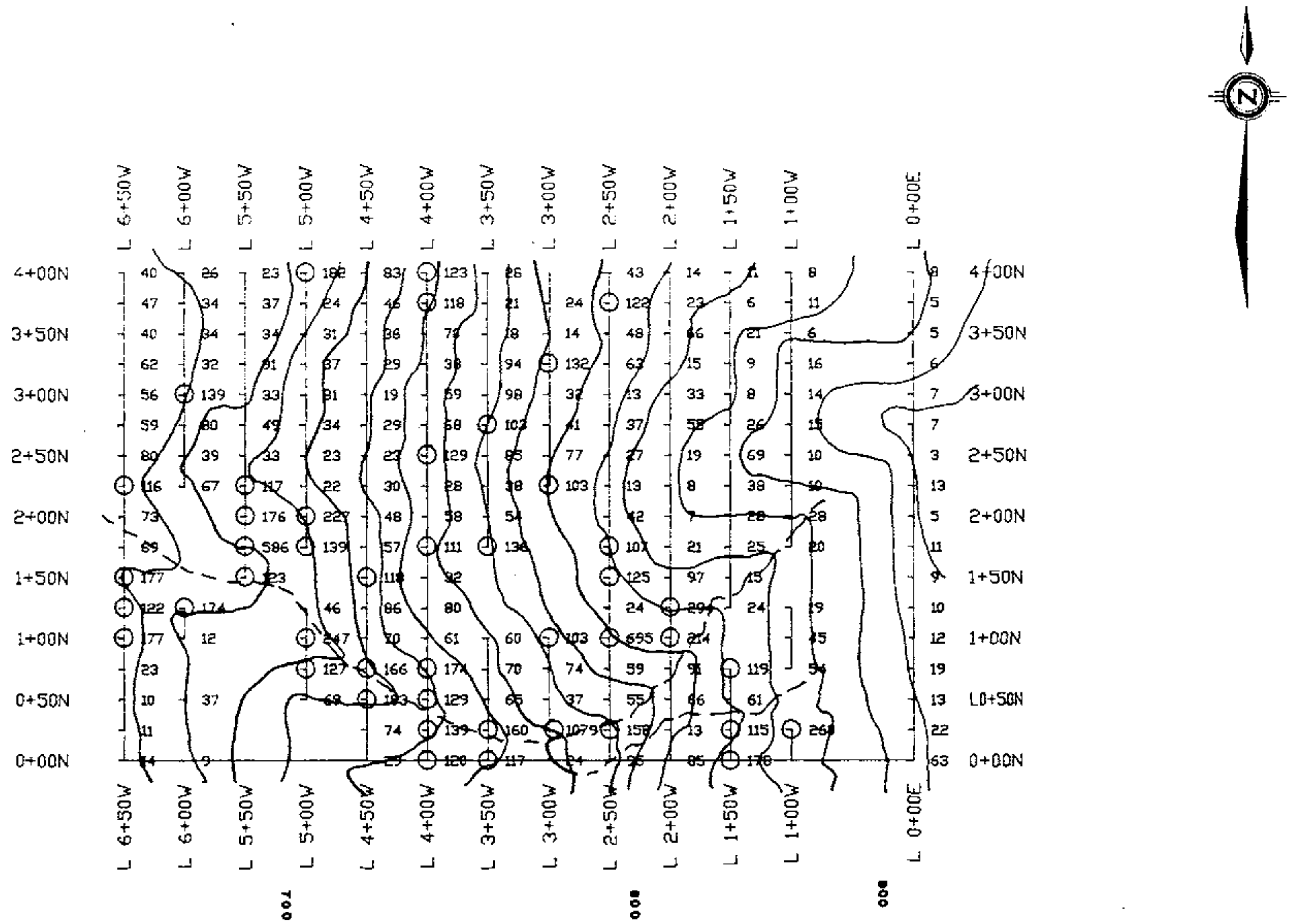
0 50 100 150 200 250

SCALE: 1:5000 (metres)

DATED: APRIL 1988
DRAWN BY: J.F. WETHERILL

FIGURE No. 3.2.III.5

Prepared by: STETSON RESOURCE MGMT. CORP.



○ > 100 ppm

BU-MAX GOLD CORP.

DEADMAN PROPERTY
KAMLOOPS MINING DIVISION

SOIL GEOCHEMISTRY GRID III
ARSENIC VALUES in ppm

0 50 100 150 200 250
SCALE: 1:5000 (metres)

DATED: APRIL 1988
DRAWN BY: J.F.WETHERILL

FIGURE No. 5.2.III.6

Prepared by: STETSON RESOURCE MGMT. CORP.

3.3 Heavy Mineral Concentrate Sampling

3.3.1 Sampling, Sample Preparation and Analysis

Heavy mineral concentrate samples must be collected where predominantly high density materials are deposited in the stream bed. These sites include: gravel bars, the inside of bends, stretches below the confluence of two streams, mouths of canyons and areas around obstacles or traps in the active channel. In the field a 50 to 100 kg sample of stream gravel was taken at 19 sites. At 18 sites the sample was dry-seived to minus 20 mesh, the coarse fractin discarded and the remaining fine fraction (approximately 16 kg) was placed in a numbered plastic bag. At one site, where water was available, the sample was wet-sieved to minus 80 mesh, the coarse fraction discarded and the remaining fraction (approximately 10 kg) was placed a numbered plastic bag.

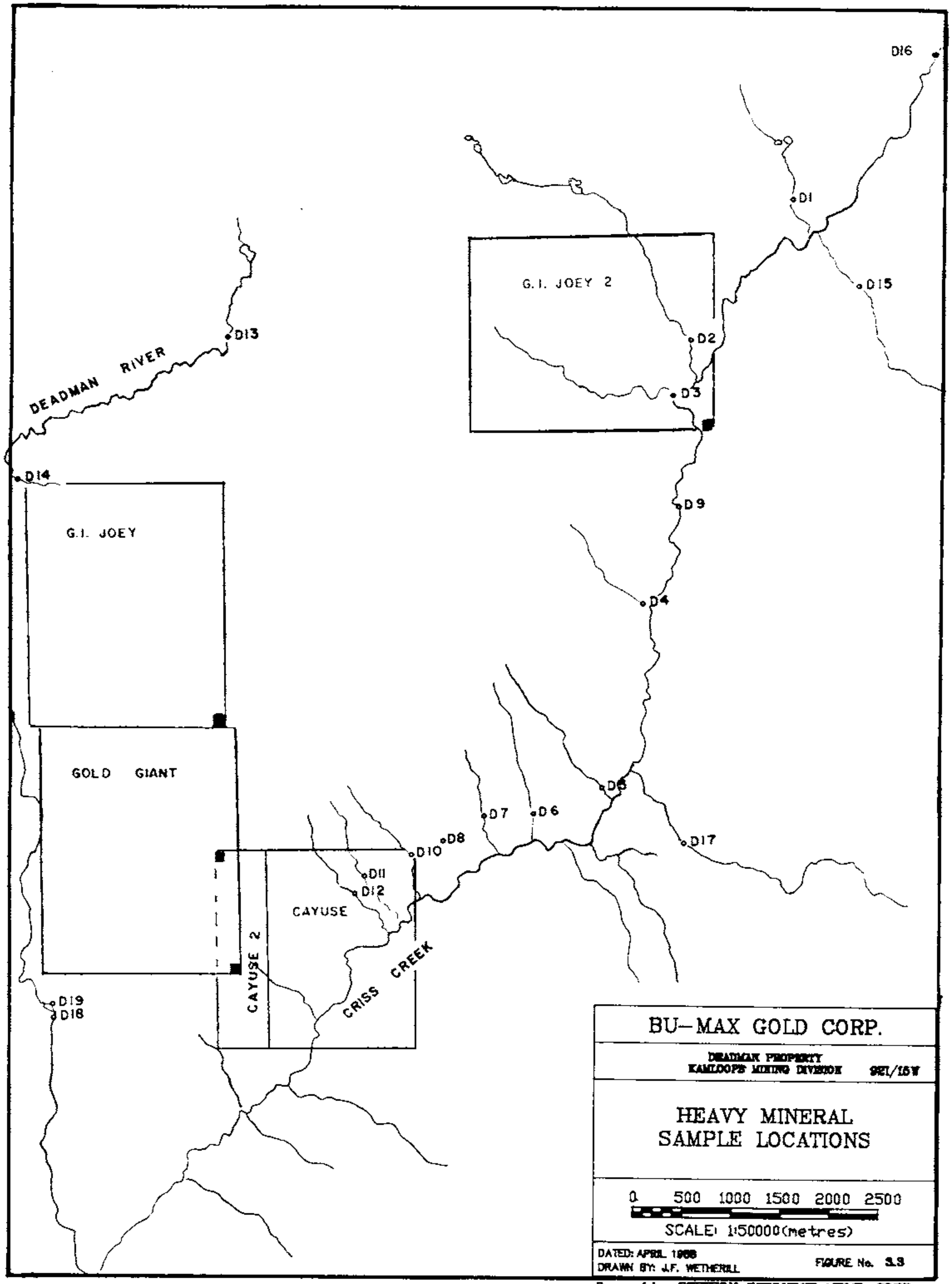
All samples were sent to the C.F. Mineral Research Ltd. laboratory in Kelowna for preparation. In the laboratory, the samples were washed and wet sieved to -20 +35, -35 +60 and -60 mesh sizes. The coarse and intermediate fractions were jigged to separate by gravity. A 2000 gm sample from each of the -20 +35 and -35 +60 mesh size heavy fractions and all of the -60 mesh size were dried and separated further by two heavy liquid separations: 1) Tetrabromoethane and 2) Methylene Iodide. The heaviest fractions from the -20 +150 and -150 mesh sizes were each submitted to 3 electromagnetic separations: 1) heavy magnetic (HM), 2) heavy paramagnetic (HP) and 3) nonmagnetic (HN).

The samples were placed in vials; the -20 +150 HN and the -150HN samples were sent to Nuclear Activation Services in Hamilton, Ontario for analysis. In the nuclear laboratory each sample was irradiated in a nuclear reactor. The samples were analysed for gold plus 26 elements by neutron activation.

3.3.2 Discussion of Results

Anomalous levels of gold were obtained from several samples. The fine fractions from samples collected on the parallel creeks draining the Cayuse claim contain 1500 and 2300 ppb gold with 9200 and 4800 ppm barium. A creek draining the northern portion of the G.I. Joey I claim contains 6300 ppb gold and 1800 ppm barium in the fine fraction.

Creeks draining the G. I. Joey II claim contain up to 93000 ppb gold and 2000 ppm barium in the fine fraction and up to 4300 ppb gold and 10000 ppm barium in the coarse fraction.



Prepared by: STETSON RESOURCE MGMT. CORP.

CONCLUSIONS

Cinnabar (and apparently realgar), pyrite ± sphalerite and stibnite mineralization occurs in quartz - dolomite - calcite vein stockwork zones and breccias often seen in crosscutting relationships.

Small zones of anomalous antimony, gold and silver concentrations occur within extensive zones of anomalous mercury, arsenic, copper and nickel levels in soils covering the Deadman property.

Gold and barium also occur in anomalous concentrations in heavy mineral concentrate samples from streams draining the property.

The geological environment underlying the Deadman property is believed to have excellent potential for hosting epithermal precious metal ore bodies for the following reasons:

1. The Triassic - Jurassic volcanic - sedimentary host rocks are well known to contain copper, lead, zinc, silver and gold mineral occurrences and deposits in a northwesterly trending belt referred to as the Quesnel Trough. The volcanics themselves may be the gold source.

2. Cretaceous - Tertiary intrusive bodies intruding the Nicola volcanics provided temperatures required to heat meteoric waters allowing them to dissolve elements including gold from the volcanics and redeposit (precipitate) them in higher concentrations.

3. Alteration and mineralization is found in association with extensive structures, often Tertiary in age. These structures play an important role in acting as conduits for ascending mineralizing fluids.

4. The geochemical signature (antimony - arsenic - mercury - barium) of both the rocks and soils fits that of the upper levels of a typical hotspring epithermal deposit.

5. Episodic brecciation and silicification evident in some of the showings is characteristic of overpressured systems and often represents hydrothermal flues in which sulphide and precious metal bearing quartz veins form. This process of sealing followed by brecciation is evident in multiple cycles in productive epithermal systems such as Round Mountain, Nevada and McLaughlin, California (Eimon, 1983).

The Vidette deposit, 30 kilometres north of the Deadman property, lies in the same geological belt and is also believed to be an epithermal deposit. The Vidette ore body differs from the Deadman prospect in that it seems to fit the Closed - Cell Convection epithermal model. These deposits form at a greater depth than a hot spring deposit however they both form in epithermal systems.

RECOMMENDATIONS

Based on the conclusions stated the following two phased exploration programme is recommended. The decision to proceed with Phase II is contingent upon favourable results from Phase I.

Phase I

1) Detailed mapping and rock chip sampling of the three main showings on the Cayuse claim. Special attention should be paid to evidence indicating direction of depth extensions for drilling targets.

2) All geochemical anomalies delineated in soils should be followed up by field examination followed by trenching where the source of the anomaly is indicated by topography.

3) All geochemical anomalies delineated in heavy mineral concentrates should be followed up by investigation upstream of the anomalies.

Phase II

Diamond drilling should be carried out to test the depth extent to mineralized showings and investigate the potential for precious metal horizons.

Respectfully Submitted,
STILLWATER ENTERPRISES LTD.

J.C. Freeze, F.G.A.C.

COST STATEMENT

Project Preparation:			
J.F.Wetherill	1 day @ $250/day/man	$	250.00
Field Costs:			
J.E.Dupuis	10 days @ $300 day/man		3,000.00
W.J.Dynes	6 days @ $225 day/man		1,350.00
J.C.Freeze	8 days @ $300/day/man		2,400.00
J.F.Wetherill	35 days @ $250/day/man		8,750.00
Field Technicians	61 days @ $175/day/man		10,675.00
		$	26,175.00
Support Costs:			
Accommodation in town of Cache Creek			
Motel and Meals			1,051.01
Camp: Room	89 mandays @ $25/day		2,225.00
Board	89 mandays @ $20/day		1,780.00
Communication			266.43
Supplies			2,758.74
Shipping			354.30
		$	8,435.48
Transportation:			
Ford Bronco w/winch	36 days @ $60/day		2,160.00
	6875 km @ $.25/km		1,718.75
Ford Bronco	10 days @ $60/day		600.00
	3124 KM @ $.25/km		781.00
4 x 4 Truck			294.00
EPS, Tolls			740.59
		$	6,294.34
Equipment Rental:			
Mobile Radio	19 days @ $ 35/day		665.00
Kitchen	19 days @ $ 50/day		950.00
Field Gear	119 days mandays @ $10/day		1,190.00
Tools	24 days @ $ 10/day		240.00
Generator	19 days @ $ 25/day		475.00
Computer	23 days @ $ 25/day		575.00
Paloma	19 days @ $ 20/day		480.00
Chainsaw	19 days @ $ 15/day		285.00
Pump (Shindawa)	19 days @ $ 15/day		285.00
Trailer	21 days @ $ 25/day		525.00
		$	5,670.00
Contract Services:			
G.Medford		$	975.00

Analysis:		14,284.25
HMC Sample Prep/Separation		2,650.65
14 element Nuclear Act. Analysis		543.50
		$ 17,478.40
Report Writing:		
J. C. Freeze	10 days at $300/day	3,000.00
Typing		400.00
Drafting and Reproduction		1,500.00
		$ 4,900.00
	SUBTOTAL	$ 70,178.22
	12.5% Administration Fee	8,772.28
	TOTAL	$ 78,950.50

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----------, 1982 — Summary of the Diamond Drilling on the D.M. claims for Guichon Explorco Limited, Assessment Report No. 10215.

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STATEMENT OF QUALIFICATIONS

NAME:	Freeze, J.C., (nee Ridley), F.G.A.C.
PROFESSION:	Consulting Geologist
EDUCATION:	1981 B. Sc. Geology - University of British Columbia
	1978 B.A. Geography - University of Western Ontario
PROFESSIONAL ASSOCIATIONS:	Fellow of the Geological Association of Canada
EXPERIENCE:	1987 - Present: Consulting Geologist with Stillwater Enterprises Ltd. Directing exploration programs and reviewing properties in Canada and U.S.A.
	1985 - 1986: Project Coordinator - Geologist with White Geophysical Inc. Coordinating mineral exploration projects involving geology, geochemistry, geophysics and diamond drilling in B.C. and Yukon.
	1981 - 1985: Project Geologist with Mark Management Ltd. Hughes-Lang Group. Responsible for precious metals exploration programs involving geology, geochmistry, geophysics and diamond drilling in Western Canada.
	1979 - 1981: Summer and part-time Geologist involved with coal exploration in N.E. B.C. with Utah Mines Ltd.

APPENDIX I

Rock Geochemistry Results

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
P 7301	6	.2	3	6	2	1
P 7302	28	.3	1	24	35	2
P 7303	7	.3	3	2	4	1
P 7304	5	.4	4	10	3	1
P 7305	27	.4	6	13	2	1
P 7306	6	.1	14	6	2	2
P 7307	6	.5	1	22	31	2
P 7308	38	.3	5	246	22	1
P 7309	28	.3	2	71	5	1
P 7310	51	.4	3	61	2	1
P 7311	58	.3	5	39	2	1
P 7312	20	.3	74	15	2	2
P 7313	7	.4	1	68	20	1
P 7314	31	.5	10	33	6	1
P 7315	22	.2	13	94	20124 ✓	1
P 7316	32	.4	9	28	27425 ✓	4
P 7317	19	.5	11	36	848	1
P 7318	4	.2	4	4	300	1
P 7319	47	.4	5	38	31	1
P 7320	10	.3	27	8	8	2
P 7321	2	.1	9	168	2	1
P 7322	2	.2	8	74	10	1
P 7323	2	.1	2	45	2	1
P 7324	5	.1	1	21	2	4
P 7325	22	.3	12	31	2	1
P 7326	35	.2	16	18	3	1
3575M	61	.6	4	28	2	1
STD C/AU-R	57	7.4	71	43	15	520

- ASSAY REQUIRED FOR CORRECT RESULT -

APPENDIX II

Soil Geochemistry Results and Graphical Statistics

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: DEC 17 1987
DATE REPORT MAILED: Jan 5, 1988

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-22 SOIL P23-ROCK P24-H.M. CONS. AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: ..[signature] DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCE PROJECT-DEADMAN File # 87-6238 Page 1

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L10+00N 5+00W	76	.3	27	14	2	2
G1 L10+00N 4+75W	47	.3	25	5	2	1
G1 L10+00N 4+50W	44	.2	27	4	2	1
G1 L10+00N 4+25W	35	.3	26	7	2	1
G1 L10+00N 4+00W	76	.3	23	16	2	1
G1 L10+00N 3+75W	39	.2	30	9	2	1
G1 L10+00N 3+50W	40	.2	30	6	2	1
G1 L10+00N 3+25W	31	.3	24	6	2	1
G1 L10+00N 3+00W	32	.1	23	3	2	1
G1 L10+00N 2+75W	45	.3	22	9	2	1
G1 L10+00N 2+50W	37	.3	14	4	2	2
G1 L10+00N 2+25W	31	.2	21	3	2	1
G1 L10+00N 2+00W	51	.1	26	10	2	1
G1 L10+00N 1+75W	36	.3	24	8	2	1
G1 L10+00N 1+50W	37	.3	20	6	2	1
G1 L10+00N 1+25W	33	.3	21	8	2	1
G1 L10+00N 1+00W	57	.3	30	15	2	1
G1 L10+00N 0+75W	31	.3	26	7	2	1
G1 L10+00N 0+50W	31	.1	27	6	2	1
G1 L10+00N 0+25W	37	.2	31	5	2	1
G1 L10+00N 0+00W	46	.2	35	5	2	1
G1 L10+00N 0+25E	20	.2	21	2	2	1
G1 L10+00N 0+50E	28	.2	23	4	2	1
G1 L10+00N 0+75E	25	.1	28	3	2	1
G1 L10+00N 1+00E	24	.1	25	2	2	1
G1 L10+00N 1+25E	50	.4	33	6	2	1
G1 L10+00N 1+50E	24	.2	22	2	2	1
G1 L10+00N 1+75E	24	.2	26	2	2	1
G1 L10+00N 2+00E	25	.2	26	3	2	1
G1 L10+00N 2+25E	30	.2	28	2	2	1
G1 L10+00N 2+50E	21	.2	26	2	2	2
G1 L10+00N 2+75E	22	.2	27	2	2	1
G1 L10+00N 3+00E	33	.1	32	4	2	1
G1 L10+00N 3+25E	23	.2	28	3	2	1
G1 L10+00N 3+50E	23	.2	29	2	2	1
G1 L10+00N 3+75E	47	.1	36	4	2	8
STD C/AU-S	58	7.5	67	41	20	50

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L10+00N 4+00E	44	.1	46	4	2	1
G1 L10+00N 4+25E	27	.2	24	3	2	2
G1 L10+00N 4+50E	23	.4	25	3	2	1
G1 L10+00N 4+75E	30	.2	35	4	2	1
G1 L10+00N 5+00E	25	.1	28	2	2	2
G1 L10+00N 5+25E	24	.1	25	2	2	1
G1 L10+00N 5+50E	20	.2	21	3	2	1
G1 L10+00N 5+75E	21	.1	23	4	2	1
G1 L10+00N 6+00E	24	.1	26	4	2	2
G1 L10+00N 6+25E	25	.1	25	3	2	1
G1 L10+00N 6+50E	33	.1	28	6	2	1
G1 L10+00N 6+75E	37	.1	49	15	3	2
G1 L10+00N 7+00E	62	.2	27	157	2	3
G1 L10+00N 7+25E	32	.2	22	22	2	2
G1 L10+00N 7+50E	22	.1	21	5	2	1
G1 L10+00N 7+75E	24	.1	24	3	2	1
G1 L10+00N 8+00E	21	.1	21	6	2	1
G1 L9+00N 5+00W	23	.3	24	5	2	1
G1 L9+00N 4+75W	20	.2	16	5	2	1
G1 L9+00N 4+25W	18	.3	21	3	2	3
G1 L9+00N 4+00W	19	.2	17	2	2	2
G1 L9+00N 3+75W	36	.2	19	6	2	7
G1 L9+00N 3+50W	51	.2	14	12	2	3
G1 L9+00N 3+25W	44	.1	22	10	2	1
G1 L9+00N 3+00W	29	.2	16	12	2	1
G1 L9+00N 2+75W	42	.3	15	25	2	2
G1 L9+00N 2+50W	30	.1	15	10	2	2
G1 L9+00N 2+25W	19	.1	16	6	2	1
G1 L9+00N 2+00W	26	.1	20	6	2	1
G1 L9+00N 1+75W	26	.2	21	7	2	1
G1 L9+00N 1+50W	26	.1	20	5	2	1
G1 L9+00N 1+25W	27	.2	21	6	2	5
G1 L9+00N 1+00W	28	.2	21	7	2	2
G1 L9+00N 0+75W	26	.1	19	4	2	1
G1 L9+00N 0+50W	38	.1	22	9	2	1
G1 L9+00N 0+25W	22	.2	24	5	2	3
STD C/AU-S	57	7.6	68	42	19	52

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L9+00N 0+00W	18	.1	18	4	2	1
G1 L9+00N 0+00E	22	.2	21	7	2	3
G1 L9+00N 0+25E	20	.1	28	4	2	6
G1 L9+00N 0+50E	20	.1	22	3	2	1
G1 L9+00N 0+75E	28	.2	29	4	2	1
G1 L9+00N 1+00E	36	.1	36	6	2	1
G1 L9+00N 1+25E	25	.1	30	2	2	1
G1 L9+00N 1+50E	24	.1	26	2	2	1
G1 L9+00N 1+75E	33	.1	30	5	2	2
G1 L9+00N 2+00E	25	.1	27	2	2	1
G1 L9+00N 2+25E	28	.3	33	5	2	1
G1 L9+00N 2+50E	20	.1	23	2	2	1
G1 L9+00N 2+75E	27	.1	31	3	2	1
G1 L9+00N 3+00E	36	.2	39	5	2	2
G1 L9+00N 3+25E	34	.2	38	4	2	1
G1 L9+00N 3+50E	34	.3	39	6	2	4
G1 L9+00N 3+75E	46	.1	36	11	2	1
G1 L9+00N 4+00E	26	.3	26	2	2	1
G1 L9+00N 4+25E	44	.3	42	3	2	1
G1 L9+00N 4+50E	31	.2	32	6	2	1
G1 L9+00N 4+75E	18	.1	20	5	2	1
G1 L9+00N 5+00E	27	.2	27	7	2	1
G1 L9+00N 5+25E	44	.3	31	12	2	2
G1 L9+00N 5+50E	32	.1	34	5	2	1
G1 L9+00N 5+75E	20	.1	22	30	2	1
G1 L9+00N 6+00E	44	.4	39	207	2	2
G1 L9+00N 6+25E	57	.3	45	96	3	3
G1 L9+00N 6+25EA	85	.3	131	171	10	1
G1 L9+00N 6+50E	29	.1	27	16	2	1
G1 L9+00N 6+50EA	26	.2	25	12	2	1
G1 L9+00N 6+75E	31	.1	25	11	2	1
G1 L9+00N 6+75EA	28	.1	23	13	2	1
G1 L9+00N 7+00E	23	.2	21	10	2	2
G1 L9+00N 7+25E	31	.1	24	9	2	1
G1 L9+00N 7+50E	21	.1	20	5	2	2
G1 L9+00N 7+75E	26	.3	23	5	2	1
STD C/AU-S	58	7.6	70	42	17	50

36

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L9+00N 8+00E	43	.3	24	6	2	1
G1 L9+00N 8+25E	37	.1	25	8	2	1
G1 L9+00N 8+50E	42	.2	22	8	2	1
G1 L8+00N 5+00W	40	.2	22	8	2	1
G1 L8+00N 4+75W	34	.1	23	8	2	2
G1 L8+00N 4+50W	31	.3	22	5	2	1
G1 L8+00N 4+25W	34	.1	23	5	2	1
G1 L8+00N 4+00W	34	.2	22	8	2	1
G1 L8+00N 3+75W	29	.2	22	7	2	1
G1 L8+00N 3+50W	40	.2	18	30	2	1
G1 L8+00N 3+25W	37	.3	24	7	2	1
G1 L8+00N 3+00W	47	.2	21	8	2	1
G1 L8+00N 2+75W	36	.2	21	7	2	2
G1 L8+00N 2+50W	47	.2	24	9	2	1
G1 L8+00N 2+25W	39	.2	21	10	2	2
G1 L8+00N 2+00W	40	.1	19	11	2	1
G1 L8+00N 1+75W	28	.3	19	9	2	1
G1 L8+00N 1+50W	81	.4	10	27	2	1
G1 L8+00N 1+25W	58	.4	20	7	2	1
G1 L8+00N 1+00W	104	.4	20	14	2	1
G1 L8+00N 0+75W	120	.3	16	10	3	1
G1 L8+00N 0+50W	43	.3	26	8	2	1
G1 L8+00N 0+25W	29	.1	26	5	2	1
G1 L8+00N 0+00W	32	.2	30	4	2	1
G1 L8+00N 0+00E	28	.2	30	5	2	1
G1 L8+00N 0+25E	24	.1	31	5	2	1
G1 L8+00N 0+50E	19	.1	27	4	2	2
G1 L8+00N 0+75E	25	.3	35	3	2	1
G1 L8+00N 1+00E	25	.3	32	4	2	1
G1 L8+00N 1+25E	24	.2	31	3	2	2
G1 L8+00N 1+50E	43	.2	37	5	2	2
G1 L8+00N 1+75E	32	.1	36	5	2	1
G1 L8+00N 2+00E	26	.1	35	3	2	1
G1 L8+00N 2+25E	42	.3	46	2	2	1
G1 L8+00N 2+50E	38	.3	37	6	2	2
G1 L8+00N 2+75E	50	.3	36	5	2	1
STD C/AU-S	58	7.5	67	44	17	49

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L8+00N 3+00E	31	.1	42	2	2	1
G1 L8+00N 3+25E	24	.1	36	2	2	1
G1 L8+00N 3+50E	45	.1	49	3	2	2
G1 L8+00N 3+75E	36	.1	40	5	2	1
G1 L8+00N 4+00E	37	.1	41	5	2	1
G1 L8+00N 4+25E	31	.1	36	4	2	1
G1 L8+00N 4+50E	37	.1	34	3	2	1
G1 L8+00N 4+75E	38	.1	36	2	2	1
G1 L8+00N 5+00E	40	.1	38	8	2	3
G1 L8+00N 5+25E	35	.1	35	9	2	1
G1 L8+00N 5+50E	56	.1	35	89	2	2
G1 L8+00N 5+75E	46	.1	38	27	2	1
G1 L8+00N 6+00E	56	.2	45	47	2	1
G1 L8+00N 7+00E	26	.1	21	6	2	1
G1 L8+00N 7+25E	28	.1	21	8	2	1
G1 L8+00N 7+50E	35	.2	22	11	2	1
G1 L8+00N 7+75E	31	.1	20	8	2	1
G1 L8+00N 8+00E	24	.1	20	7	2	1
G1 L8+00N 8+25E	35	.2	21	7	2	1
G1 L8+00N 8+50E	30	.2	19	7	2	1
G1 L8+00N 8+75E	37	.2	22	10	2	1
G1 L8+00N 9+00E	32	.1	20	9	2	3
G1 L8+00N 9+25E	32	.2	23	5	2	1
G1 L8+00N 9+50E	24	.1	21	3	2	1
G1 L8+00N 10+00E	50	.2	26	4	2	1
G1 L7+00N 5+00W	42	.1	24	9	2	1
G1 L7+00N 4+75W	27	.1	24	4	2	6
G1 L7+00N 4+50W	20	.1	20	4	2	1
G1 L7+00N 4+25W	21	.1	20	3	2	1
G1 L7+00N 4+00W	26	.1	19	12	2	1
G1 L7+00N 3+75W	26	.1	22	5	2	2
G1 L7+00N 3+50W	18	.2	17	4	2	1
G1 L7+00N 3+25W	32	.1	19	14	2	1
G1 L7+00N 3+00W	24	.1	7	59	2	1
G1 L7+00N 2+75W	33	.2	18	16	2	1
G1 L7+00N 2+50W	54	.1	28	8	2	1
STD C/AU-S	57	7.3	67	39	18	48

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L7+00N 2+25W	27	.2	18	12	2	1
G1 L7+00N 2+00W	43	.1	18	14	2	1
G1 L7+00N 1+75W	61	.3	17	18	2	1
G1 L7+00N 1+50W	29	.2	16	11	2	1
G1 L7+00N 1+25W	34	.1	38	7	2	1
G1 L7+00N 1+00W	29	.1	25	5	2	1
G1 L7+00N 0+75W	21	.1	22	9	2	1
G1 L7+00N 0+50W	30	.2	17	8	2	1
G1 L7+00N 0+25W	33	.1	22	6	2	1
G1 L7+00N 0+00W	24	.1	23	5	2	1
G1 L7+00N 0+00E	30	.1	23	5	2	1
G1 L7+00N 0+25E	41	.1	28	5	2	1
G1 L7+00N 0+50E	35	.1	31	4	2	1
G1 L7+00N 0+75E	28	.1	17	8	2	1
G1 L7+00N 1+00E	26	.1	21	11	3	1
G1 L7+00N 1+25E	28	.2	26	8	2	1
G1 L7+00N 1+50E	28	.2	26	5	2	2
G1 L7+00N 1+75E	28	.1	27	7	2	1
G1 L7+00N 2+00E	20	.1	25	4	2	1
G1 L7+00N 2+25E	25	.1	29	6	2	1
G1 L7+00N 2+50E	25	.1	28	5	2	1
G1 L7+00N 2+75E	23	.1	41	4	2	1
G1 L7+00N 3+00E	28	.3	58	9	2	1
G1 L7+00N 3+25E	36	.3	38	9	2	3
G1 L7+00N 3+50E	26	.1	31	5	2	1
G1 L7+00N 3+75E	36	.4	39	5	2	1
G1 L7+00N 4+00E	38	.2	41	5	2	1
G1 L7+00N 4+25E	43	.1	37	10	2	2
G1 L7+00N 4+50E	39	.1	38	8	2	1
G1 L7+00N 4+75E	45	.1	37	9	2	1
G1 L7+00N 5+00E	78	.1	14	15	2	1
G1 L7+00N 5+25E	41	.2	10	15	2	3
G1 L7+00N 5+50E	94	.2	18	20	2	1
G1 L7+00N 5+75E	44	.3	44	13	2	1
G1 L7+00N 6+00E	54	.3	37	13	2	1
G1 L7+00N 6+25E	40	.2	27	16	2	4
STD C/AU-S	58	7.4	68	40	17	49

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L7+00N 6+50E	37	.1	28	19	2	1
G1 L7+00N 6+75E	34	.1	28	20	2	1
G1 L7+00N 7+00E	40	.3	27	9	2	1
G1 L7+00N 7+25E	28	.2	24	6	2	1
G1 L7+00N 7+50E	31	.2	22	7	2	1
G1 L7+00N 7+75E	25	.2	20	3	2	1
G1 L7+00N 8+00E	28	.1	21	6	2	1
G1 L7+00N 8+25E	22	.2	19	4	2	1
G1 L7+00N 8+50E	25	.1	18	2	2	6
G1 L7+00N 8+75E	36	.3	25	2	2	1
G1 L7+00N 9+00E	25	.1	23	4	2	5
G1 L7+00N 9+25E	25	.1	22	2	2	1
G1 L7+00N 9+50E	25	.1	22	4	2	1
G1 L7+00N 9+75E	45	.1	25	8	2	2
G1 L7+00N 10+25E	49	.2	27	8	2	1
G1 L6+00N 5+00W	39	.1	27	8	2	1
G1 L6+00N 4+75W	32	.2	22	8	2	1
G1 L6+00N 4+50W	40	.3	23	15	2	1
G1 L6+00N 4+25W	30	.2	21	7	2	1
G1 L6+00N 4+00W	36	.2	24	10	2	1
G1 L6+00N 3+75W	32	.3	24	11	2	1
G1 L6+00N 3+50W	29	.2	19	8	2	1
G1 L6+00N 3+25W	47	.1	13	11	2	2
G1 L6+00N 3+00W	46	.1	15	24	2	3
G1 L6+00N 2+75W	41	.3	21	20	2	94
G1 L6+00N 2+50W	54	.2	19	14	2	1
G1 L6+00N 2+25W	30	.1	21	6	2	1
G1 L6+00N 2+00W	40	.1	31	7	2	3
G1 L6+00N 1+75W	51	.3	28	6	2	1
G1 L6+00N 1+50W	27	.3	24	4	2	1
G1 L6+00N 1+00W	39	.1	21	7	2	1
G1 L6+00N 0+75W	58	.2	22	4	2	1
G1 L6+00N 0+50W	47	.3	22	4	2	2
G1 L6+00N 0+25W	81	.1	22	12	2	1
G1 L6+00N 0+00W	48	.1	29	10	3	1
G1 L6+00N 0+00E	55	.3	28	9	2	1
STD C/AU-S	57	7.5	68	39	17	51

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L6+00N 0+25E	50	.2	25	14	2	1
G1 L6+00N 0+50E	53	.3	25	14	2	1
G1 L6+00N 0+75E	76	.3	24	11	2	1
G1 L6+00N 1+00E	49	.4	23	17	2	1
G1 L6+00N 1+25E	51	.4	24	23	3	1
G1 L6+00N 1+50E	23	.1	27	6	2	1
G1 L6+00N 1+75E	24	.1	22	4	2	1
G1 L6+00N 2+00E	18	.2	18	5	2	2
G1 L6+00N 2+25E	39	.2	22	21	2	2
G1 L6+00N 2+50E	32	.3	31	9	2	1
G1 L6+00N 2+75E	46	.3	23	16	2	1
G1 L6+00N 3+00E	53	.3	38	13	2	1
G1 L6+00N 3+25E	40	.2	29	10	2	1
G1 L6+00N 3+50E	56	.2	24	16	2	1
G1 L6+00N 3+75E	39	.2	33	9	2	1
G1 L6+00N 4+00E	45	.2	38	9	2	1
G1 L6+00N 4+25E	52	.2	39	13	2	1
G1 L6+00N 4+50E	41	.4	33	11	2	1
G1 L6+00N 4+75E	50	.5	29	11	2	1
G1 L6+00N 5+00E	39	.3	14	14	2	1
G1 L6+00N 5+25E	26	.2	15	16	2	1
G1 L6+00N 5+50E	61	.1	15	16	2	1
G1 L6+00N 5+75E	105	.2	13	22	2	1
G1 L6+00N 6+00E	27	.3	28	7	2	1
G1 L6+00N 6+25E	33	.2	30	9	2	1
G1 L6+00N 6+50E	43	.3	28	7	2	1
G1 L6+00N 6+75E	26	.2	23	6	2	1
G1 L6+00N 7+00E	34	.4	23	10	2	1
G1 L6+00N 7+25E	26	.2	22	8	2	2
G1 L6+00N 7+50E	33	.1	25	6	2	1
G1 L6+00N 7+75E	32	.2	24	12	2	1
G1 L6+00N 8+00E	49	.3	27	3	2	1
G1 L6+00N 8+25E	32	.2	23	7	2	1
G1 L6+00N 8+50E	35	.1	24	9	2	1
G1 L6+00N 8+75E	20	.1	18	7	2	2
G1 L6+00N 9+00E	39	.3	25	9	2	1
STD C/AU-S	58	7.5	68	43	17	51

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L6+00N 9+25E	28	.2	21	5	2	1
G1 L6+00N 9+50E	44	.1	25	10	2	3
G1 L6+00N 9+75E	32	.1	23	6	2	2
G1 L6+00N 10+00E	34	.1	24	6	2	2
G1 L6+00N 10+25E	182	.1	36	22	2	9
G1 L6+00N 10+50E	48	.1	32	3	2	1
G1 L6+00N 10+75E	48	.1	24	10	2	4
G1 L6+00N 11+00E	49	.3	23	13	2	3
G1 L5+00N 5+00W	37	.1	22	8	2	8
G1 L5+00N 4+75W	49	.1	12	15	2	6
G1 L5+00N 4+50W	48	.1	17	14	2	4
G1 L5+00N 4+25W	50	.1	19	13	2	2
G1 L5+00N 4+00W	59	.4	16	15	2	54
G1 L5+00N 3+75W	28	.1	22	10	2	2
G1 L5+00N 3+50W	41	.2	20	17	2	1
G1 L5+00N 3+25W	58	.2	17	28	2	2
G1 L5+00N 3+00W	47	.2	25	22	2	1
G1 L5+00N 2+75W	58	.1	19	19	2	3
G1 L5+00N 2+50W	51	.2	21	18	2	3
G1 L5+00N 2+25W	44	.1	25	13	2	1
G1 L5+00N 2+00W	59	.1	12	21	2	1
G1 L5+00N 1+75W	41	.1	23	6	2	2
G1 L5+00N 1+50W	36	.1	21	8	2	2
G1 L5+00N 1+25W	57	.1	25	19	2	1
G1 L5+00N 1+00W	50	.1	25	13	2	3
G1 L5+00N 0+75W	49	.1	23	29	4	2
G1 L5+00N 0+50W	40	.2	22	11	2	7
G1 L5+00N 0+25W	35	.1	21	10	2	5
G1 L5+00N 0+00W	70	.2	20	15	2	1
G1 L5+00N 0+00E	56	.2	20	13	2	1
G1 L5+00N 0+25E	50	.1	19	25	14	2
G1 L5+00N 0+50E	57	.2	13	27	7	2
G1 L5+00N 0+75E	51	.1	18	23	4	1
G1 L5+00N 1+00E	50	.2	27	12	2	1
G1 L5+00N 1+25E	52	.1	26	18	2	4
G1 L5+00N 1+50E	31	.1	29	8	2	11
STD C/AU-S	57	7.5	67	40	18	48

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L5+00N 1+75E	30	.1	30	9	2	1
G1 L5+00N 2+00E	35	.2	20	5	2	1
G1 L5+00N 2+25E	47	.5	9	26	2	1
G1 L5+00N 2+50E	55	.3	17	30	2	1
G1 L5+00N 2+75E	78	.2	28	18	2	1
G1 L5+00N 3+00E	44	.3	34	13	2	4
G1 L5+00N 3+25E	46	.2	33	22	2	6
G1 L5+00N 3+50E	22	.3	27	4	2	3
G1 L5+00N 3+75E	39	.3	46	16	2	1
G1 L5+00N 4+00E	26	.3	57	18	2	1
G1 L5+00N 4+25E	41	.5	30	14	3	1
G1 L5+00N 4+50E	56	.1	31	19	2	1
G1 L5+00N 4+75E	38	.2	25	13	2	2
G1 L5+00N 5+00E	30	.2	32	11	7	1
G1 L5+00N 5+25E	25	.1	34	10	2	1
G1 L5+00N 5+50E	24	.2	39	9	2	1
G1 L5+00N 5+75E	21	.3	16	13	2	1
G1 L5+00N 6+00E	33	.2	33	5	2	1
G1 L5+00N 6+25E	32	.1	27	6	2	1
G1 L5+00N 6+50E	36	.2	27	7	2	1
G1 L5+00N 6+75E	35	.2	30	5	2	1
G1 L5+00N 7+00E	22	.3	24	3	2	1
G1 L5+00N 7+25E	31	.3	27	6	2	1
G1 L5+00N 7+50E	24	.1	23	7	2	1
G1 L5+00N 7+75E	39	.2	26	8	2	1
G1 L5+00N 8+00E	26	.1	23	6	2	1
G1 L5+00N 8+25E	47	.3	26	10	2	1
G1 L5+00N 8+50E	41	.3	25	7	2	1
G1 L5+00N 8+75E	30	.1	22	4	2	1
G1 L5+00N 9+00E	36	.2	26	6	2	1
G1 L5+00N 9+25E	29	.2	27	6	2	1
G1 L5+00N 9+50E	46	.1	27	6	2	1
G1 L5+00N 9+75E	48	.3	27	7	2	2
G1 L5+00N 10+00E	44	.4	40	13	2	1
G1 L5+00N 10+25E	40	.1	29	6	2	1
G1 L5+00N 10+50E	47	.2	30	10	2	1
STD C/AU-S	57	7.4	68	38	18	49

STETSON RESOURCE PROJECT-DEADMAN FILE # 87-6238 Page 11

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L5+00N 10+75E	51	.2	39	9	2	2
G1 L5+00N 10+00E	53	.3	41	14	2	1
G1 L4+00N 5+00W	51	.2	28	10	2	2
G1 L4+00N 4+75W	45	.1	29	10	2	1
G1 L4+00N 4+50W	39	.2	25	13	2	1
G1 L4+00N 4+25W	59	.3	27	20	2	1
G1 L4+00N 4+00W	52	.3	24	61	5	82
G1 L4+00N 3+75W	32	.3	31	15	2	1
G1 L4+00N 3+50W	46	.1	25	52	2	4
G1 L4+00N 3+25W	65	.3	14	33	2	1
G1 L4+00N 3+00W	50	.2	22	78	3	1
G1 L4+00N 2+75W	56	.2	29	22	2	1
G1 L4+00N 2+50W	59	.2	14	255	2	1
G1 L4+00N 2+25W	79	.2	15	130	3	1
G1 L4+00N 2+00W	90	.2	8	58	2	1
G1 L4+00N 1+75W	73	.3	11	207	18	1
G1 L4+00N 1+50W	59	.1	12	35	3	1
G1 L4+00N 1+25W	45	.3	25	45	2	1
G1 L4+00N 1+00W	76	.3	16	26	2	4
G1 L4+00N 0+75W	41	.1	14	67	2	1
G1 L4+00N 0+50W	57	.1	16	21	2	1
G1 L4+00N 0+25W	66	.3	21	23	2	1
G1 L4+00N 0+00W	62	.1	20	17	3	1
G1 L4+00N 0+25E	47	.2	18	25	2	1
G1 L4+00N 0+50E	57	.1	24	17	2	3
G1 L4+00N 0+75E	70	.2	20	20	2	1
G1 L4+00N 1+00E	34	.1	25	13	2	1
G1 L4+00N 1+25E	32	.2	25	11	2	1
G1 L4+00N 1+50E	68	.3	20	80	4	1
G1 L4+00N 1+75E	35	.3	15	30	2	1
G1 L4+00N 2+00E	85	.4	22	31	3	1
G1 L4+00N 2+25E	121	.1	18	59	3	1
G1 L4+00N 2+50E	80	.2	25	70	3	1
G1 L4+00N 2+75E	89	.2	26	20	2	1
G1 L4+00N 3+00E	62	.1	25	40	2	1
G1 L4+00N 3+25E	54	.3	37	9	2	2
STD C/AU-S	57	7.4	67	39	18	49

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L4+00N 3+50E	45	.2	45	8	2	1
G1 L4+00N 3+75E	48	.2	42	10	2	3
G1 L4+00N 4+00E	33	.1	37	6	2	85
G1 L4+00N 4+25E	35	.3	46	5	2	1
G1 L4+00N 4+50E	45	.3	48	20	2	1
G1 L4+00N 4+75E	53	.1	20	18	2	1
G1 L4+00N 5+00E	53	.1	22	17	2	1
G1 L3+00N 5+00W	95	.2	27	11	2	2
G1 L3+00N 4+75W	52	.2	17	11	2	5
G1 L3+00N 4+50W	65	.1	17	11	2	2
G1 L3+00N 4+25W	47	.1	33	8	2	1
G1 L3+00N 4+00W	51	.1	32	14	2	1
G1 L3+00N 3+75W	41	.1	28	12	2	1
G1 L3+00N 3+50W	74	.2	21	23	2	3
G1 L3+00N 3+25W	100	.1	27	44	4	1
G1 L3+00N 3+00W	80	.2	26	135	9	1
G1 L3+00N 2+75W	91	.1	18	148	11	1
G1 L3+00N 2+50W	72	.2	32	184	7	5
G1 L3+00N 2+25W	68	.1	15	130	8	1
G1 L3+00N 2+00W	70	.2	20	105	3	1
G1 L3+00N 1+75W	73	.3	35	32	2	2
G1 L3+00N 1+50W	366	.4	10	86	3	1
G1 L3+00N 1+25W	113	.2	41	32	2	1
G1 L3+00N 1+00W	74	.4	22	34	2	1
G1 L3+00N 0+75W	57	.1	13	49	2	1
G1 L3+00N 0+50W	85	.2	16	154	3	1
G1 L3+00N 0+25W	58	.1	23	31	2	1
G1 L3+00N 0+00W	34	.1	24	69	2	1
G1 L3+00N 0+25E	44	.3	28	35	2	1
G1 L3+00N 0+50E	51	.2	20	63	2	1
G1 L3+00N 0+75E	146	.2	20	214	3	5
G1 L3+00N 1+00E	137	.2	20	167	2	1
G1 L3+00N 1+25E	91	.3	24	90	3	3
G1 L3+00N 1+50E	106	.3	26	73	2	2
G1 L3+00N 1+75E	69	.2	21	52	2	1
G1 L3+00N 2+00E	64	.1	28	26	2	1
STD C/AU-S	57	7.2	68	43	18	50

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L3+00N 2+25E	44	.2	19	22	2	1
G1 L3+00N 2+50E	26	.3	27	8	2	1
G1 L3+00N 2+75E	52	.3	29	19	2	1
G1 L3+00N 3+00E	33	.3	26	7	2	2
G1 L3+00N 3+25E	42	.3	37	9	2	60
G1 L3+00N 3+50E	44	.4	32	10	2	5
G1 L3+00N 3+75E	34	.2	32	7	2	1
G1 L3+00N 4+00E	67	.3	38	10	2	1
G1 L3+00N 4+25E	59	.2	32	26	2	2
G1 L3+00N 4+50E	35	.4	43	2	2	1
G1 L3+00N 4+75E	46	.6	44	4	2	4
G1 L3+00N 5+00E	34	.3	36	3	2	2
G1 L2+00N 5+00W	55	.2	20	9	2	1
G1 L2+00N 4+75W	37	.3	21	8	2	1
G1 L2+00N 4+50W	29	.1	17	15	2	1
G1 L2+00N 4+25W	62	.3	51	12	2	5
G1 L2+00N 4+00W	60	.4	23	22	2	1
G1 L2+00N 3+75W	30	.3	29	9	2	1
G1 L2+00N 3+50W	26	.1	43	5	2	11
G1 L2+00N 3+25W	29	.4	46	6	2	1
G1 L2+00N 3+00W	25	.3	43	4	2	16
G1 L2+00N 2+75W	25	.2	45	6	2	1
G1 L2+00N 2+50W	46	.2	50	8	2	1
G1 L2+00N 2+25W	42	.1	51	5	2	2
G1 L2+00N 2+00W	40	.2	67	5	2	1
G1 L2+00N 1+75W	32	.1	37	5	2	1
G1 L2+00N 1+50W	31	.1	43	5	2	7
G1 L2+00N 1+25W	26	.2	44	2	2	3
G1 L2+00N 1+00W	38	.3	30	424	2	2
G1 L2+00N 0+75W	39	.1	28	606	6	2
G1 L2+00N 0+50W	39	.3	29	1244	15	1
G1 L2+00N 0+25W	43	.2	28	285	5	2
G1 L2+00N 0+00W	34	.1	39	123	2	1
G1 L2+00N 0+00E	29	.1	28	158	2	2
G1 L2+00N 0+25E	42	.1	30	26	2	7
G1 L2+00N 0+50E	33	.1	25	61	2	1
G1 L2+00N 0+75E	31	.3	27	55	2	1
STD C/AU-S	57	7.3	68	42	16	52

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 L2+00N 1+00E	32	.2	27	30	2	3
G1 L2+00N 1+25E	38	.2	29	24	2	2
G1 L2+00N 1+50E	39	.3	30	7	2	1
G1 L2+00N 1+75E	62	.1	33	8	2	7
G1 L2+00N 2+00E	110	.4	24	27	7	1
G1 L2+00N 2+25E	90	.5	21	32	15	6
G1 L2+00N 2+50E	33	.1	30	45	2	1
G1 L2+00N 2+75E	64	.3	20	109	14	2
G1 L2+00N 3+00E	41	.3	37	10	2	1
G1 L2+00N 3+25E	38	.2	39	8	2	1
G1 L2+00N 3+50E	41	.2	35	6	2	1
G1 L2+00N 3+75E	38	.1	35	7	2	1
G1 L2+00N 4+00E	37	.1	38	4	2	37
G1 L2+00N 4+25E	40	.2	23	13	2	1
G1 L2+00N 4+50E	425	.2	33	7	2	1
G1 L2+00N 4+75E	50	.1	24	6	2	6
G1 L2+00N 5+00E	47	.2	25	2	2	1
G1 L1+00N 5+00W	51	.3	24	11	2	1
G1 L1+00N 4+75W	26	.2	43	2	2	4
G1 L1+00N 4+50W	51	.3	45	5	2	150
G1 L1+00N 4+25W	135	.7	18	64	12	2
G1 L1+00N 4+00W	53	.3	31	84	7	1
G1 L1+00N 3+75W	149	.5	19	81	10	7
G1 L1+00N 3+50W	19	.2	37	2	2	1
G1 L1+00N 3+00W	41	.3	43	13	2	4
G1 L1+00N 2+75W	65	.2	56	6	2	140
G1 L1+00N 2+50W	72	.3	28	25	2	11
G1 L1+00N 2+25W	118	.3	13	32	2	4
G1 L1+00N 2+00W	119	.3	22	150	8	2
G1 L1+00N 1+75W	106	.3	20	101	7	1
G1 L1+00N 1+50W	90	.2	20	14	2	120
G1 L1+00N 1+25W	46	.2	45	3	2	9
G1 L1+00N 1+00W	42	.3	36	6	2	1
G1 L1+00N 0+75W	71	.1	38	7	2	4
G1 L1+00N 0+50W	36	.1	32	2	2	9
G1 L1+00N 0+25W	22	.2	47	3	2	2
STD C/AU-S	58	7.3	68	39	18	48

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G1 LO+00N 0+75W	70	.2	22	22	3	2
G1 LO+00N 0+50W	54	.3	18	11	2	1
G1 LO+00N 0+25W	88	.3	20	33	2	1
G1 LO+00N 0+00E	68	.2	28	39	2	1
G1 LO+00N 0+25E	80	.3	29	119	2	2
G1 LO+00N 0+50E	127	.5	21	81	3	1
G1 LO+00N 0+75E	32	.4	42	9	2	1
G1 LO+00N 1+00E	29	.3	37	19	3	1
G1 LO+00N 1+25E	26	.2	35	17	2	1
G1 LO+00N 1+50E	22	.3	39	8	2	1
G1 LO+00N 1+75E	24	.2	41	5	3	1
G1 LO+00N 2+00E	27	.3	41	4	2	1
G1 LO+00N 2+25E	21	2.6	44	5	3	725
G1 LO+00N 2+50E	36	.2	45	7	2	2
G1 LO+00N 2+75E	26	.3	40	3	2	5
G1 LO+00N 3+00E	29	.2	42	6	2	2
G1 LO+00N 3+25E	28	.2	43	4	2	3
G1 LO+00N 3+50E	24	.3	40	5	2	5
G1 LO+00N 3+75E	21	.3	44	7	2	5
G1 LO+00N 4+00E	27	.3	46	7	2	1
G1 LO+00N 4+25E	21	.3	34	2	2	1
G1 LO+00N 4+50E	28	.3	41	4	2	2
G1 LO+00N 4+75E	19	.3	48	3	3	1
G1 LO+00N 5+00E	25	.1	43	3	2	2
STD C/AU-S	57	7.3	68	41	19	49

2A

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE (604) 253-3158 FAX (604) 253-1716
DATE RECEIVED: DEC 17 1987
DATE REPORT MAILED: Dec. 14, 1988

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOILS -80 MESH AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: .... DEAN TOYE, CERTIFIED B.C. ASSAYER

STETSON RESOURCES PROJECT - DEADMAN File # 87-6238A Page 1

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L12+00W 7+00N	38	.4	36	64	2	3
G2 L12+00W 6+75N	42	.3	37	10	2	7
G2 L12+00W 6+50N	35	.1	31	6	2	2
G2 L12+00W 6+25N	31	.2	29	4	2	3
G2 L12+00W 6+00N	36	.2	27	15	2	5
G2 L12+00W 5+75N	25	.3	15	8	2	1
G2 L12+00W 5+50N	27	.2	22	12	2	2
G2 L12+00W 5+25N	24	.3	16	5	2	8
G2 L12+00W 5+00N	29	.6	28	9	2	40
G2 L12+00W 4+75N	31	.4	25	9	2	12
G2 L12+00W 4+50N	30	.2	43	7	2	31
G2 L12+00W 4+25N	27	.4	35	3	3	9
STD C/AU-S	57	7.3	68	41	19	49

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L12+00W 4+00N	41	.3	65	4	2	1
G2 L12+00W 3+75N	37	.3	69	5	5	2
G2 L12+00W 3+50N	36	.3	42	5	2	1
G2 L12+00W 3+25N	39	.1	41	6	2	2
G2 L12+00W 3+00N	34	.1	37	5	2	1
G2 L12+00W 2+75N	34	.3	39	6	2	2
G2 L12+00W 2+50N	41	.1	48	6	2	2
G2 L12+00W 2+25N	32	.4	49	3	2	1
G2 L12+00W 2+00N	24	.4	34	2	2	1
G2 L12+00W 1+75N	25	.1	24	2	2	2
G2 L12+00W 1+50N	24	.3	24	3	2	1
G2 L12+00W 1+25N	22	.3	29	3	2	1
G2 L12+00W 1+00N	16	.2	21	5	2	1
G2 L12+00W 0+75N	24	.1	30	5	2	1
G2 L12+00W 0+50N	24	.2	28	2	2	1
G2 L12+00W 0+25N	27	.3	30	5	2	1
G2 L12+00W 0+00N	18	.1	22	3	2	1
G2 L12+00W 0+00S	22	.2	25	3	2	1
G2 L12+00W 0+25S	17	.1	18	2	2	1
G2 L12+00W 0+50S	21	.2	28	2	2	1
G2 L12+00W 0+75S	18	.2	23	2	2	1
G2 L12+00W 1+00S	22	.2	31	4	2	2
G2 L12+00W 1+25S	30	.2	37	4	2	1
G2 L12+00W 1+50S	35	.1	39	7	2	2
G2 L12+00W 1+75S	15	.1	20	2	2	1
G2 L12+00W 2+00S	26	.1	33	6	2	2
G2 L11+00W 6+25N	51	.4	44	4	2	2
G2 L11+00W 6+00N	54	.2	50	8	2	5
G2 L11+00W 5+75N	55	.3	41	6	2	1
G2 L11+00W 5+50N	57	.4	29	9	2	1
G2 L11+00W 5+25N	65	.2	31	29	2	1
G2 L11+00W 5+00N	43	.4	39	6	2	2
G2 L11+00W 4+75N	43	.4	18	7	2	1
G2 L11+00W 4+50N	73	.5	15	4	2	3
G2 L11+00W 4+25N	52	.4	21	7	2	1
G2 L11+00W 4+00N	42	.3	44	15	2	4
STD C/AU-S	58	7.5	68	43	17	47

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L11+00W 3+75N	48	.2	38	2	2	1
G2 L11+00W 3+50N	35	.1	30	2	2	1
G2 L11+00W 3+25N	21	.2	17	5	2	1
G2 L11+00W 3+00N	42	.1	40	9	2	1
G2 L11+00W 2+75N	41	.2	40	14	2	2
G2 L11+00W 2+50N	36	.2	33	12	2	1
G2 L11+00W 2+25N	36	.3	35	10	2	1
G2 L11+00W 2+00N	38	.4	35	9	2	1
G2 L11+00W 1+75N	26	.3	25	4	2	1
G2 L11+00W 1+50N	45	.4	39	4	2	1
G2 L11+00W 1+25N	24	.3	22	3	2	1
G2 L11+00W 1+00N	17	.3	18	2	2	1
G2 L11+00W 0+50N	27	.2	25	5	2	1
G2 L11+00W 0+25N	24	.1	26	2	2	1
G2 L11+00W 0+00S	45	.2	43	6	2	1
G2 L11+00W 0+25S	44	.2	46	12	2	1
G2 L11+00W 0+50S	45	.1	28	23	2	1
G2 L11+00W 0+75S	34	.1	33	7	2	1
G2 L11+00W 1+00S	31	.1	34	7	2	1
G2 L11+00W 1+25S	38	.1	41	8	2	2
G2 L11+00W 1+50S	33	.1	39	31	2	1
G2 L11+00W 1+75S	25	.1	33	2	2	1
G2 L11+00W 2+00S	42	.5	35	14	2	1
G2 L10+00W 7+00N	34	.2	29	7	2	1
G2 L10+00W 6+75N	43	.3	30	16	2	2
G2 L10+00W 6+50N	40	.3	25	10	2	1
G2 L10+00W 6+25N	60	.4	24	14	2	3
G2 L10+00W 6+00N	25	.1	32	4	2	1
G2 L10+00W 5+75N	45	.1	42	7	2	1
G2 L10+00W 5+50N	39	.3	36	8	2	1
G2 L10+00W 5+25N	28	.1	33	4	2	1
G2 L10+00W 5+00N	30	.1	36	2	2	1
G2 L10+00W 4+75N	37	.3	40	4	2	1
G2 L10+00W 4+50N	50	.3	47	9	2	1
G2 L10+00W 4+25N	26	.1	34	7	2	2
G2 L10+00W 4+00N	35	.2	36	16	2	1
STD C/AU-S	58	7.6	68	38	18	50

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L10+00W 3+75N	30	.3	30	20	2	6
G2 L10+00W 3+50N	36	.5	37	15	2	1
G2 L10+00W 3+25N	34	.2	37	7	2	2
G2 L10+00W 3+00N	32	.2	38	4	2	1
G2 L10+00W 2+75N	31	.3	34	5	2	2
G2 L10+00W 2+50N	37	.2	33	4	2	3
G2 L10+00W 2+25N	25	.2	21	4	2	2
G2 L10+00W 2+00N	34	.4	32	7	2	5
G2 L10+00W 1+75N	43	.3	42	6	2	14
G2 L10+00W 1+50N	39	.4	48	3	2	3
G2 L10+00W 1+25N	40	.1	54	3	2	2
G2 L10+00W 1+00N	43	.3	49	4	2	3
G2 L10+00W 0+75N	42	.3	49	6	2	5
G2 L10+00W 0+50N	118	.4	52	113	2	2
G2 L10+00W 0+25N	63	.1	33	44	2	2
G2 L10+00W 0+00N	49	.2	44	98	2	1
G2 L10+00W 0+00S	39	.3	35	8	2	2
G2 L10+00W 0+25S	31	.1	33	11	2	2
G2 L10+00W 0+50S	42	.2	44	8	2	7
G2 L10+00W 0+75S	35	.2	31	5	2	2
G2 L10+00W 1+00S	27	.3	26	4	2	1
G2 L10+00W 1+25S	23	.2	22	4	2	1
G2 L10+00W 1+50S	19	.1	22	6	2	2
G2 L10+00W 1+75S	57	.2	48	21	2	1
G2 L10+00W 2+00S	60	.3	41	13	2	1
G2 L9+00W 7+00N	46	.2	42	21	2	6
G2 L9+00W 6+75N	84	.2	25	66	25	3
G2 L9+00W 6+75NA	41	.3	40	13	2	2
G2 L9+00W 6+50N	62	.1	13	229	66	8
G2 L9+00W 6+50NA	37	.1	41	9	2	1
G2 L9+00W 6+25N	54	.1	25	70	21	1
G2 L9+00W 6+25NA	33	.1	37	7	2	1
G2 L9+00W 6+00N	102	.3	16	246	82	2
G2 L9+00W 6+00NA	36	.2	32	14	2	1
G2 L9+00W 5+75N	89	.1	24	49	30	1
G2 L9+00W 5+75NA	40	.1	39	10	2	1
G2 L9+00W 5+50N	63	.2	29	34	2	9
STD C/AU-S	58	7.4	68	43	18	50

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L9+00W 5+50NA	29	.2	31	5	2	2
G2 L9+00W 5+25N	54	.2	23	26	2	1
G2 L9+00W 5+25NA	41	.1	42	6	2	1
G2 L9+00W 5+00N	28	.1	23	10	2	1
G2 L9+00W 5+00NA	44	.1	39	11	2	1
G2 L9+00W 4+75N	33	.3	35	7	2	1
G2 L9+00W 4+75NA	36	.2	39	7	2	2
G2 L9+00W 4+50N	44	.3	61	10	2	1
G2 L9+00W 4+50NA	47	.3	41	13	2	1
G2 L9+00W 4+25N	33	.2	52	12	2	1
G2 L9+00W 4+25NA	41	.2	44	13	2	2
G2 L9+00W 4+00N	29	.1	28	8	2	1
G2 L9+00W 4+00NA	41	.2	38	15	2	2
G2 L9+00W 3+75N	44	.1	41	27	2	1
G2 L9+00W 3+75NA	50	.4	45	15	2	3
G2 L9+00W 3+50N	66	.3	32	38	2	1
G2 L9+00W 3+50NA	53	.2	49	31	2	1
G2 L9+00W 3+25N	54	.2	46	15	2	2
G2 L9+00W 3+25NA	67	.5	38	19	2	1
G2 L9+00W 3+00N	53	.3	48	14	2	3
G2 L9+00W 3+00NA	43	.3	42	6	2	1
G2 L9+00W 2+75N	43	.1	48	12	2	1
G2 L9+00W 2+75NA	39	.5	38	10	2	2
G2 L9+00W 2+50N	55	.3	44	3	2	1
G2 L9+00W 2+50NA	39	.4	37	6	2	1
G2 L9+00W 2+25N	36	.2	38	9	2	1
G2 L9+00W 2+25NA	54	.3	35	9	2	2
G2 L9+00W 2+25NB	38	.1	43	8	2	1
G2 L9+00W 2+00N	77	.3	30	6	2	1
G2 L9+00W 2+00NA	29	.1	35	5	2	2
G2 L9+00W 1+75N	34	.2	26	2	2	1
G2 L9+00W 1+75NA	31	.1	27	3	2	1
G2 L9+00W 1+50N	33	.1	33	6	2	2
G2 L9+00W 1+50NA	41	.3	49	6	3	3
G2 L9+00W 1+25N	38	.1	45	6	2	1
G2 L9+00W 1+25NA	37	.2	34	11	2	1
STD C/AU-S	58	7.6	67	40	16	52

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L9+00W 1+00N	33	.1	38	5	2	1
G2 L9+00W 1+00NA	56	.2	49	49	2	1
G2 L9+00W 0+75N	32	.1	34	5	2	1
G2 L9+00W 0+75NA	38	.1	42	10	2	2
G2 L9+00W 0+50N	40	.1	31	5	2	1
G2 L9+00W 0+50NA	32	.1	44	3	2	1
G2 L9+00W 0+25N	35	.1	35	8	2	2
G2 L9+00W 0+25NA	47	.1	47	9	2	1
G2 L9+00W 0+00N	36	.1	36	8	2	1
G2 L9+00W 0+00NA	37	.1	39	7	2	2
G2 L9+00W 0+25S	33	.1	37	6	2	1
G2 L9+00W 0+50S	27	.1	32	5	2	1
G2 L9+00W 0+75S	40	.1	41	12	2	1
G2 L9+00W 1+00S	34	.1	30	5	2	2
G2 L9+00W 1+25S	29	.1	36	5	2	1
G2 L9+00W 1+50S	31	.2	39	7	2	1
G2 L9+00W 1+75S	26	.2	32	7	2	1
G2 L9+00W 2+00S	29	.1	30	22	2	2
G2 L8+50W 7+00N	34	.1	38	7	2	1
G2 L8+50W 6+75N	54	.2	40	10	2	1
G2 L8+50W 6+50N	51	.2	46	9	2	1
G2 L8+50W 6+25N	49	.1	36	19	11	4
G2 L8+50W 6+00N	74	.2	19	42	14	2
G2 L8+50W 5+75N	64	.2	33	27	5	1
G2 L8+50W 5+50N	49	.1	32	17	2	1
G2 L8+50W 5+25N	64	.2	27	38	13	1
G2 L8+50W 5+00N	59	.1	17	58	2	1
G2 L8+50W 4+75N	58	.1	17	63	2	1
G2 L8+50W 4+50N	57	.1	19	36	2	2
G2 L8+50W 4+25N	32	.2	25	8	2	1
G2 L8+50W 4+00N	45	.1	40	12	2	1
G2 L8+50W 3+75N	31	.1	30	8	2	1
G2 L8+50W 3+50N	45	.1	45	9	2	2
G2 L8+50W 3+25N	52	.2	46	7	2	5
G2 L8+50W 3+00N	51	.1	44	9	2	1
G2 L8+50W 2+75N	29	.2	30	9	2	1
STD C/AU-S	57	7.3	68	41	18	49

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L8+50W 2+50N	55	.1	31	42	2	1
G2 L8+50W 2+25N	36	.3	27	9	2	1
G2 L8+50W 2+00N	47	.2	38	3	2	1
G2 L8+50W 1+75N	40	.2	39	7	2	2
G2 L8+50W 1+50N	54	.2	33	20	2	1
G2 L8+50W 1+25N	44	.1	24	17	2	2
G2 L8+50W 1+00N	35	.1	31	6	2	2
G2 L8+50W 0+75N	39	.2	28	11	2	1
G2 L8+50W 0+50N	43	.1	28	12	2	1
G2 L8+50W 0+25N	35	.1	21	10	2	2
G2 L8+50W 0+00N	32	.1	23	9	2	3
G2 L8+00W 7+00N	38	.2	38	12	2	1
G2 L8+00W 6+75N	31	.2	35	8	2	106
G2 L8+00W 6+50N	42	.2	38	8	2	1
G2 L8+00W 6+25N	74	.3	23	40	2	2
G2 L8+00W 6+00N	79	.1	21	34	2	1
G2 L8+00W 5+75N	71	.2	23	37	2	1
G2 L8+00W 5+50N	63	.1	20	36	2	1
G2 L8+00W 5+25N	52	.1	19	27	2	1
G2 L8+00W 5+00N	60	.1	17	66	2	1
G2 L8+00W 4+75N	62	.1	20	49	2	1
G2 L8+00W 4+50N	68	.1	19	45	2	1
G2 L8+00W 4+25N	67	.4	19	53	2	1
G2 L8+00W 4+00N	51	.1	18	51	2	1
G2 L8+00W 3+75N	57	.1	19	61	2	2
G2 L8+00W 3+50N	59	.2	25	81	2	1
G2 L8+00W 3+25N	65	.1	21	72	2	1
G2 L8+00W 3+00N	63	.2	20	63	2	2
G2 L8+00W 2+75N	79	.1	22	78	2	1
G2 L8+00W 2+50N	55	.1	22	49	2	1
G2 L8+00W 2+25N	49	.2	21	36	2	1
G2 L8+00W 2+00N	32	.1	19	10	2	1
G2 L8+00W 1+75N	36	.1	19	8	2	1
G2 L8+00W 1+50N	46	.1	22	13	2	2
G2 L8+00W 1+25N	33	.1	18	6	2	1
G2 L8+00W 1+00N	62	.1	33	15	2	1
STD C/AU-S	58	7.6	68	40	19	48

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L8+00W 0+75N	38	.3	29	12	2	1
G2 L8+00W 0+50N	28	.3	24	11	2	1
G2 L8+00W 0+25N	35	.3	27	10	2	2
G2 L8+00W 0+00N	72	.3	35	20	4	1
G2 L8+00W 0+25S	32	.3	34	7	2	2
G2 L8+00W 0+50S	27	.2	36	7	2	2
G2 L8+00W 0+75S	32	.3	39	6	2	2
G2 L8+00W 1+00S	32	.2	32	12	2	1
G2 L8+00W 1+25S	29	.3	29	11	2	1
G2 L8+00W 1+50S	34	.5	41	19	2	1
G2 L8+00W 1+75S	29	.2	39	10	2	1
G2 L8+00W 2+00S	28	.3	33	5	2	1
G2 L7+50W 7+00N	33	.3	35	10	2	2
G2 L7+50W 6+75N	28	.2	33	7	2	1
G2 L7+50W 6+50N	35	.3	39	12	2	1
G2 L7+50W 6+25N	72	.3	41	10	2	1
G2 L7+50W 6+00N	59	.3	25	36	3	3
G2 L7+50W 5+75N	58	.1	13	55	3	1
G2 L7+50W 5+50N	75	.4	13	39	2	1
G2 L7+50W 5+25N	76	.2	16	66	2	2
G2 L7+50W 5+00N	74	.1	17	62	2	1
G2 L7+50W 4+75N	102	.1	18	34	2	1
G2 L7+50W 4+50N	49	.2	44	12	2	5
G2 L7+50W 4+25N	48	.2	42	10	2	2
G2 L7+50W 4+00N	43	.2	45	11	2	3
G2 L7+50W 3+75N	68	.2	22	78	4	1
G2 L7+50W 3+50N	66	.2	22	81	2	1
G2 L7+50W 3+25N	62	.3	22	74	4	1
G2 L7+50W 3+00N	61	.1	24	57	2	5
G2 L7+50W 2+75N	70	.2	25	64	4	2
G2 L7+50W 2+50N	62	.2	23	80	2	1
G2 L7+50W 2+25N	50	.2	21	21	2	2
G2 L7+50W 2+00N	76	.2	24	20	2	1
G2 L7+50W 1+75N	110	.3	27	20	2	1
G2 L7+50W 1+50N	68	.1	25	24	3	1
G2 L7+50W 1+25N	70	.3	26	25	6	2
STD C/AU-S	57	7.4	67	40	18	48

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L7+50W 1+00N	47	.1	27	18	2	1
G2 L7+50W 0+75N	40	.1	27	16	2	1
G2 L7+50W 0+50N	41	.1	28	8	2	2
G2 L7+50W 0+25N	25	.3	23	6	2	1
G2 L7+00W 7+00N	30	.1	36	9	2	1
G2 L7+00W 6+75N	30	.1	26	15	2	2
G2 L7+00W 6+50N	43	.6	37	11	2	3
G2 L7+00W 6+25N	46	.2	33	20	2	1
G2 L7+00W 6+00N	59	.2	13	93	3	1
G2 L7+00W 5+75N	64	.3	9	119	2	1
G2 L7+00W 5+50N	98	.2	14	75	2	2
G2 L7+00W 5+25N	93	.3	11	29	2	1
G2 L7+00W 5+00N	101	.2	19	45	2	1
G2 L7+00W 4+75N	100	.2	18	34	2	2
G2 L7+00W 4+50N	65	.2	17	21	2	1
G2 L7+00W 4+25N	39	.3	24	15	2	1
G2 L7+00W 4+00N	46	.4	39	16	2	4
G2 L7+00W 3+75N	51	.1	45	17	2	5
G2 L7+00W 3+50N	77	.2	24	57	2	1
G2 L7+00W 3+25N	75	.2	23	95	2	2
G2 L7+00W 3+00N	61	.2	23	101	2	1
G2 L7+00W 2+75N	62	.2	20	39	2	1
G2 L7+00W 2+50N	62	.2	23	36	3	3
G2 L7+00W 2+25N	50	.1	20	29	2	1
G2 L7+00W 2+00N	82	.2	25	20	2	4
G2 L7+00W 1+75N	91	.1	24	33	2	1
G2 L7+00W 1+50N	79	.3	29	28	2	1
G2 L7+00W 1+25N	93	.1	27	35	2	1
G2 L7+00W 1+00N	49	.1	25	16	2	1
G2 L7+00W 0+75N	58	.2	32	11	2	1
G2 L7+00W 0+50N	40	.1	29	6	2	2
G2 L7+00W 0+25N	59	.2	29	12	2	23
G2 L7+00W 0+00N	41	.2	45	10	2	3
G2 L7+00W 0+25S	46	.2	34	18	2	1
G2 L7+00W 0+50S	27	.2	35	23	2	2
G2 L7+00W 0+75S	27	.2	30	11	2	1
STD C/AU-S	58	7.6	68	41	16	52

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L7+00W 1+00S	25	.1	25	5	2	1
G2 L7+00W 1+25S	42	.1	19	25	2	2
G2 L7+00W 1+50S	145	.1	17	115	2	1
G2 L7+00W 1+75S	32	.1	38	11	2	1
G2 L7+00W 2+00S	22	.1	34	8	2	3
G2 L6+50W 7+00N	24	.2	24	9	2	2
G2 L6+50W 6+75N	27	.1	27	16	2	1
G2 L6+50W 6+50N	46	.2	43	15	2	1
G2 L6+50W 6+25N	54	.1	29	38	2	1
G2 L6+50W 6+00N	67	.2	21	81	2	1
G2 L6+50W 5+75N	52	.2	53	8	2	3
G2 L6+50W 5+50N	96	.3	12	25	2	1
G2 L6+50W 5+25N	91	.2	12	15	2	1
G2 L6+50W 5+00N	90	.3	15	25	2	1
G2 L6+50W 4+75N	73	.1	28	33	2	1
G2 L6+50W 4+50N	68	.2	18	99	2	2
G2 L6+50W 4+25N	68	.1	15	136	5	1
G2 L6+50W 4+00N	54	.1	19	92	2	1
G2 L6+50W 3+75N	81	.2	22	71	2	1
G2 L6+50W 3+50N	64	.2	27	33	2	1
G2 L6+50W 3+25N	49	.3	46	23	2	1
G2 L6+50W 3+00N	42	.2	53	8	2	1
G2 L6+50W 2+75N	49	.2	20	37	2	2
G2 L6+50W 2+50N	49	.1	17	40	2	1
G2 L6+50W 2+25N	64	.3	45	23	2	1
G2 L6+50W 2+00N	91	.1	26	22	2	1
G2 L6+50W 1+75N	95	.3	24	30	2	1
G2 L6+50W 1+50N	66	.2	27	22	2	1
G2 L6+50W 1+25N	70	.1	27	28	2	4
G2 L6+50W 1+00N	35	.2	25	12	2	1
G2 L6+50W 0+75N	43	.2	28	9	2	1
G2 L6+50W 0+50N	39	.2	32	8	2	1
G2 L6+50W 0+25N	75	.2	37	11	2	2
G2 L6+50W 0+00N	86	.3	29	15	2	4
G2 L6+00W 7+00N	27	.1	28	9	2	1
G2 L6+00W 6+75N	22	.1	28	10	2	22
STD C/AU-S	57	7.4	68	39	17	49

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L6+00W 6+50N	31	.2	34	12	2	1
G2 L6+00W 6+25N	47	.2	39	27	2	1
G2 L6+00W 6+00N	52	.3	48	24	3	1
G2 L6+00W 5+75N	56	.5	56	12	2	2
G2 L6+00W 5+50N	94	.2	14	31	2	1
G2 L6+00W 5+25N	100	.4	12	53	2	1
G2 L6+00W 5+00N	63	.1	18	72	2	2
G2 L6+00W 4+75N	67	.3	17	115	8	1
G2 L6+00W 4+50N	78	.3	8	214	8	1
G2 L6+00W 4+25N	79	.2	23	88	2	1
G2 L6+00W 4+00N	79	.4	23	108	2	1
G2 L6+00W 3+75N	36	.3	26	37	2	1
G2 L6+00W 3+50N	28	.2	17	33	2	1
G2 L6+00W 3+25N	35	.1	18	33	2	1
G2 L6+00W 3+00N	61	.3	30	22	2	1
G2 L6+00W 2+75N	45	.2	38	20	2	1
G2 L6+00W 2+50N	52	.2	25	34	2	2
G2 L6+00W 2+25N	38	.3	42	7	2	1
G2 L6+00W 2+00N	39	.2	42	9	2	1
G2 L6+00W 1+75N	96	.2	23	26	2	1
G2 L6+00W 1+50N	99	.2	18	48	3	1
G2 L6+00W 1+25N	72	.3	23	35	2	1
G2 L6+00W 1+00N	84	.2	24	37	2	2
G2 L6+00W 0+00N	34	.3	32	9	2	1
G2 L6+00W 0+25S	28	.1	22	2	2	1
G2 L6+00W 0+25SA	30	.1	32	5	2	1
G2 L6+00W 0+50S	49	.3	39	16	2	1
G2 L6+00W 0+50SA	40	.2	28	8	2	1
G2 L6+00W 0+75S	31	.1	34	8	2	2
G2 L6+00W 0+75SA	48	.3	27	15	2	1
G2 L6+00W 1+00S	38	.3	39	9	2	6
G2 L6+00W 1+25S	37	.3	49	34	2	1
G2 L6+00W 1+50S	29	.2	37	7	2	2
G2 L6+00W 1+75S	31	.2	37	7	2	1
G2 L6+00W 2+00S	26	.2	33	5	2	1
G2 L5+50W 7+00N	30	.2	29	11	2	1
STD C/AU-S	58	7.6	68	41	16	51

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L5+50W 6+75N	30	.2	29	17	2	3
G2 L5+50W 6+50N	38	.1	38	13	2	1
G2 L5+50W 6+25N	64	.3	58	8	2	3
G2 L5+50W 6+00N	58	.2	22	142	2	1
G2 L5+50W 5+75N	72	.1	12	109	2	1
G2 L5+50W 5+50N	103	.3	13	117	2	3
G2 L5+50W 5+25N	76	.2	14	115	4	1
G2 L5+50W 5+00N	92	.3	6	120	14	1
G2 L5+50W 4+75N	87	.3	18	97	2	1
G2 L5+50W 4+50N	70	.4	10	199	2	1
G2 L5+50W 4+25N	33	.2	11	144	2	1
G2 L5+50W 4+00N	61	.2	19	115	4	2
G2 L5+50W 3+75N	62	.2	21	75	5	1
G2 L5+50W 3+50N	50	.3	19	62	5	1
G2 L5+50W 3+25N	48	.1	19	35	2	1
G2 L5+50W 3+00N	45	.3	14	27	2	1
G2 L5+50W 2+75N	50	.2	16	36	2	1
G2 L5+50W 2+50N	47	.1	39	11	2	1
G2 L5+50W 2+25N	56	.3	42	15	2	1
G2 L5+50W 2+00N	46	.3	41	13	2	1
G2 L5+50W 1+75N	91	.2	20	18	2	1
G2 L5+50W 1+50N	110	.2	14	35	4	2
G2 L5+50W 1+25N	99	.3	17	51	8	1
G2 L5+50W 1+00N	84	.2	18	43	5	1
G2 L5+50W 0+75N	35	.2	21	12	2	1
G2 L5+50W 0+50N	41	.2	24	8	2	1
G2 L5+50W 0+25N	140	.2	20	32	4	1
G2 L5+50W 0+00N	94	.2	22	12	7	1
G2 L5+00W 7+00N	26	.1	26	8	2	1
G2 L5+00W 6+75N	27	.1	26	13	2	1
G2 L5+00W 6+50N	45	.2	39	14	2	2
G2 L5+00W 6+25N	48	.4	21	128	2	1
G2 L5+00W 6+00N	70	.3	57	13	2	3
G2 L5+00W 5+75N	62	.1	22	167	11	1
G2 L5+00W 5+50N	73	.3	7	186	2	1
G2 L5+00W 5+25N	56	.3	3	181	3	1
STD C/AU-S	57	7.6	68	41	19	49

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L5+00W 5+00N	91	.2	8	352	2	2
G2 L5+00W 4+75N	95	.3	8	467	2	1
G2 L5+00W 4+50N	71	.3	9	205	2	1
G2 L5+00W 4+25N	81	.1	17	116	2	1
G2 L5+00W 4+00N	65	.2	13	170	2	2
G2 L5+00W 3+75N	68	.1	24	61	2	1
G2 L5+00W 3+50N	41	.1	13	62	2	1
G2 L5+00W 3+25N	119	.3	23	57	2	1
G2 L5+00W 3+00N	178	.1	13	120	2	1
G2 L5+00W 2+75N	59	.2	13	33	2	2
G2 L5+00W 2+50N	81	.2	32	35	2	1
G2 L5+00W 2+25N	91	.2	14	74	4	1
G2 L5+00W 2+00N	100	.1	15	29	2	1
G2 L5+00W 1+75N	112	.1	16	35	2	1
G2 L5+00W 1+50N	99	.3	10	13	2	2
G2 L5+00W 1+25N	73	.2	11	38	2	1
G2 L5+00W 1+00N	94	.2	24	27	2	1
G2 L5+00W 0+75N	34	.1	17	6	2	1
G2 L5+00W 0+50N	60	.1	18	10	2	1
G2 L5+00W 0+25N	104	.2	19	8	2	3
G2 L5+00W 0+00N	73	.2	18	12	2	2
G2 L5+00W 0+25S	26	.1	32	6	2	1
G2 L5+00W 0+50S	42	.2	29	7	2	1
G2 L5+00W 0+75S	178	.4	24	14	2	1
G2 L5+00W 1+00S	86	.1	35	21	2	1
G2 L5+00W 1+25S	35	.2	40	9	2	2
G2 L5+00W 1+50S	44	.1	42	8	2	1
G2 L5+00W 1+75S	20	.2	27	7	2	1
G2 L5+00W 2+00S	25	.1	29	5	2	2
G2 L4+50W 7+00N	22	.1	18	8	2	1
G2 L4+50W 6+75N	28	.2	26	13	2	3
G2 L4+50W 6+50N	32	.1	30	13	2	1
G2 L4+50W 6+25N	45	.4	36	10	2	1
G2 L4+50W 6+00N	56	.2	24	42	2	1
G2 L4+50W 5+75N	56	.2	11	175	2	2
G2 L4+50W 5+50N	60	.1	6	123	18	1
STD C/AU-S	57	7.4	67	43	18	48

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L3+50W 3+75N	59	.2	41	17	2	2
G2 L3+50W 3+50N	64	.4	19	32	2	1
G2 L3+50W 3+25N	80	.5	8	97	7	1
G2 L3+50W 3+00N	123	.6	18	59	2	1
G2 L3+50W 2+75N	168	.5	6	60	2	1
G2 L3+50W 2+50N	82	.3	22	26	2	6
G2 L3+50W 2+25N	38	.4	39	13	2	2
G2 L3+50W 2+00N	30	.3	36	9	2	1
G2 L3+50W 1+75N	42	.4	42	12	2	4
G2 L3+50W 1+50N	35	.3	42	10	2	1
G2 L3+50W 1+25N	42	.3	49	8	2	1
G2 L3+50W 1+00N	48	.2	45	9	2	7
G2 L3+50W 0+75N	46	.3	40	12	2	2
G2 L3+50W 0+50N	44	.3	47	12	2	1
G2 L3+50W 0+25N	50	.4	45	11	2	2
G2 L3+50W 0+00N	42	.3	45	10	2	1
G2 L3+00W 7+00N	26	.3	29	11	2	1
G2 L3+00W 6+75N	26	.2	30	11	2	1
G2 L3+00W 6+50N	20	.3	27	8	2	2
G2 L3+00W 6+25N	53	.4	37	23	2	2
G2 L3+00W 6+00N	21	.4	26	6	2	1
G2 L3+00W 5+75N	28	.2	34	8	2	1
G2 L3+00W 5+50N	40	.2	41	14	2	6
G2 L3+00W 5+25N	39	.1	45	11	2	1
G2 L3+00W 5+00N	22	.4	28	8	2	1
G2 L3+00W 4+75N	23	.2	32	9	2	4
G2 L3+00W 4+50N	35	.3	48	5	2	12
G2 L3+00W 4+25N	33	.3	42	10	2	8
G2 L3+00W 4+00N	39	.4	50	10	2	1
G2 L3+00W 3+75N	39	.3	43	12	2	2
G2 L3+00W 3+50N	48	.4	38	16	2	1
G2 L3+00W 3+25N	109	.5	21	86	2	2
G2 L3+00W 3+00N	94	.4	19	57	2	1
G2 L3+00W 2+75N	169	.7	9	88	2	1
G2 L3+00W 2+50N	179	.9	5	72	6	1
G2 L3+00W 2+25N	50	.2	31	16	2	1
STD C/AU-S	58	7.5	67	40	18	49

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L3+00W 2+00N	36	.1	30	10	2	5
G2 L3+00W 1+75N	38	.1	43	7	2	1
G2 L3+00W 1+50N	39	.1	43	12	2	1
G2 L3+00W 1+25N	48	.2	43	12	2	1
G2 L3+00W 1+00N	53	.3	46	6	2	1
G2 L3+00W 0+75N	45	.2	37	14	2	1
G2 L3+00W 0+50N	28	.1	30	5	2	1
G2 L3+00W 0+25N	21	.1	30	7	2	1
G2 L3+00W 0+00N	21	.2	30	3	2	2
G2 L3+00W 0+25S	24	.2	31	7	2	3
G2 L3+00W 0+50S	23	.2	30	3	2	1
G2 L3+00W 0+75S	24	.1	32	8	2	1
G2 L3+00W 1+00S	19	.1	29	5	2	3
G2 L3+00W 1+25S	20	.1	28	6	2	2
G2 L3+00W 1+50S	22	.1	28	8	2	1
G2 L3+00W 1+75S	25	.2	30	7	2	1
G2 L3+00W 2+00S	25	.4	30	7	2	5
G2 L2+50W 7+00N	27	.1	23	5	2	1
G2 L2+50W 6+75N	22	.2	25	6	2	2
G2 L2+50W 6+50N	29	.1	27	6	2	2
G2 L2+50W 6+25N	24	.1	24	6	2	3
G2 L2+50W 6+00N	26	.3	28	7	2	3
G2 L2+50W 5+75N	26	.1	34	6	2	2
G2 L2+50W 5+50N	53	.2	39	8	2	1
G2 L2+50W 5+25N	24	.1	39	3	2	3
G2 L2+50W 5+00N	24	.2	32	4	2	1
G2 L2+50W 4+75N	21	.1	31	2	2	3
G2 L2+50W 4+50N	25	.2	34	3	2	2
G2 L2+50W 4+25N	48	.2	45	5	2	10
G2 L2+50W 4+00N	27	.1	34	2	2	4
G2 L2+50W 3+75N	42	.3	44	7	2	5
G2 L2+50W 3+50N	42	.2	45	7	2	2
G2 L2+50W 3+25N	35	.2	37	10	2	1
G2 L2+50W 3+00N	63	.3	31	15	2	3
G2 L2+50W 2+75N	56	.3	40	9	2	1
G2 L2+50W 2+50N	139	.6	23	68	3	2
STD C/AU-S	57	7.5	67	40	18	47

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L2+50W 2+25N	31	.2	39	11	2	2
G2 L2+50W 2+00N	43	.1	43	13	2	1
G2 L2+50W 1+75N	30	.3	32	11	2	2
G2 L2+50W 1+50N	27	.3	33	10	2	1
G2 L2+50W 1+25N	27	.1	32	9	2	2
G2 L2+50W 1+00N	24	.2	28	7	2	4
G2 L2+50W 0+75N	43	.2	38	13	2	6
G2 L2+50W 0+50N	28	.1	33	10	2	4
G2 L2+50W 0+25N	33	.2	40	13	2	2
G2 L2+50W 0+00N	37	.3	40	12	2	1
G2 L2+00W 7+00N	27	.2	24	13	2	2
G2 L2+00W 6+75N	27	.2	26	14	2	3
G2 L2+00W 6+50N	26	.1	24	10	2	1
G2 L2+00W 6+25N	18	.1	24	7	2	2
G2 L2+00W 6+00N	28	.1	38	9	2	4
G2 L2+00W 5+75N	25	.1	32	8	2	13
G2 L2+00W 5+50N	25	.2	31	8	2	2
G2 L2+00W 5+25N	19	.1	26	6	2	10
G2 L2+00W 5+00N	23	.2	30	6	2	6
G2 L2+00W 4+75N	24	.2	33	9	2	3
G2 L2+00W 4+50N	20	.1	26	6	2	3
G2 L2+00W 4+25N	36	.1	33	14	2	2
G2 L2+00W 4+00N	43	.1	38	12	2	21
G2 L2+00W 3+75N	41	.1	41	14	2	1
G2 L2+00W 3+50N	43	.2	37	14	2	1
G2 L2+00W 3+25N	38	.1	41	14	2	1
G2 L2+00W 3+00N	43	.3	39	18	2	1
G2 L2+00W 2+75N	42	.2	42	13	2	3
G2 L2+00W 2+50N	46	.1	47	11	2	1
G2 L2+00W 2+25N	30	.2	30	13	2	1
G2 L2+00W 2+00N	19	.1	25	6	2	1
G2 L2+00W 1+75N	23	.1	30	6	2	1
G2 L2+00W 1+50N	26	.1	31	9	2	3
G2 L2+00W 1+25N	35	.2	41	9	2	1
G2 L2+00W 1+00N	30	.1	33	8	2	1
G2 L2+00W 0+75N	25	.1	30	4	2	1
STD C/AU-S	58	7.4	69	40	16	50

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L2+00W 0+50N	29	.2	35	5	2	2
G2 L2+00W 0+25N	22	.2	31	4	2	1
G2 L2+00W 0+00N	20	.1	25	3	2	2
G2 L2+00W 0+25S	17	.2	25	3	2	1
G2 L2+00W 0+50S	22	.2	29	4	2	2
G2 L2+00W 0+75S	18	.2	28	3	2	2
G2 L2+00W 1+00S	23	.3	33	6	2	1
G2 L2+00W 1+25S	22	.3	32	6	2	1
G2 L2+00W 1+50S	21	.1	34	3	2	1
G2 L2+00W 1+75S	7	.1	15	6	2	1
G2 L2+00W 2+00S	39	.3	131	3	3	1
STD C/AU-S	58	7.3	69	40	17	52

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
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DATE RECEIVED: JAN 14 1988
DATE REPORT MAILED: Jan. 18/88.

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL PULP AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: C. Leong .... D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

STETSON RESOURCE PROJECT-DEADMAN File # 88-0108 Page 1

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 L1W 7+00N	22	.4	19	5	2	1
G2 L1W 6+75N	18	.6	22	5	2	1
G2 L1W 6+50N	16	.5	20	8	2	3
G2 L1W 6+25N	15	.4	19	8	2	1
G2 L1W 6+00N	21	.3	25	5	2	2
G2 L1W 5+75N	18	.2	23	6	2	1
G2 L1W 5+50N	19	.5	24	4	2	1
G2 L1W 5+25N	19	.6	24	5	2	1
G2 L1W 5+00N	17	.3	21	7	2	1
G2 L1W 4+75N	26	.6	29	4	2	2
G2 L1W 4+50N	20	.2	24	8	2	1
G2 L1W 4+25N	24	.2	24	8	2	1
G2 L1W 4+00N	21	.3	21	5	3	1
G2 L1W 3+75N	19	.6	24	5	2	1
G2 L1W 3+50N	23	.5	25	7	2	1
G2 L1W 3+25N	22	.5	26	6	2	2
G2 L1W 3+00N	22	.1	25	6	2	1
G2 L1W 2+75N	21	.4	24	5	2	1
G2 L1W 2+50N	28	.1	31	11	2	1
G2 L1W 2+25N	29	.5	32	8	2	1
G2 L1W 2+00N	29	.3	29	14	2	1
G2 L1W 1+75N	23	.4	25	8	2	1
G2 L1W 1+50N	30	.5	32	10	2	2
G2 L1W 1+25N	21	.3	26	10	2	1
G2 L1W 1+00N	29	.3	29	12	2	1
G2 L1W 0+75N	28	.4	29	12	2	1
G2 L1W 0+50N	21	.5	24	4	2	1
G2 L1W 0+25N	16	.4	26	2	2	1
G2 L1W 0+00N	18	.3	33	2	2	1
G2 L0W 7+00N	17	.3	25	9	2	1
G2 L0W 6+75N	18	.3	21	6	2	1
G2 L0W 6+50N	17	.1	22	7	2	1
G2 L0W 6+25N	22	.5	30	10	2	2
G2 L0W 6+00N	16	.1	20	2	2	1
G2 L0W 5+75N	19	.1	21	5	2	1
G2 L0W 5+50N	48	.2	35	20	2	1
STD C/AU-S	58	7.2	67	37	18	51

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G2 LOW 5+25N	65	.3	32	34	2	1
G2 LOW 5+00N	28	.2	23	25	2	1
G2 LOW 4+75N	45	.6	29	24	2	1
G2 LOW 4+50N	26	.5	21	9	2	2
G2 LOW 4+25N	24	.5	21	14	2	1
G2 LOW 4+00N	26	.3	22	7	2	1
G2 LOW 3+75N	22	.3	22	10	2	2
G2 LOW 3+50N	23	.4	19	9	2	1
G2 LOW 3+25N	23	.4	21	10	2	1
G2 LOW 3+00N	25	.4	21	8	2	1
G2 LOW 2+75N	23	.2	22	9	2	1
G2 LOW 2+50N	19	.4	19	5	2	1
G2 LOW 2+25N	20	.5	21	7	2	2
G2 LOW 2+00N	20	.3	20	8	2	2
G2 LOW 1+75N	17	.6	18	5	2	1
G2 LOW 1+50N	23	.3	23	10	2	1
G2 LOW 1+25N	27	.2	26	6	2	2
G2 LOW 1+00N	18	.3	18	6	2	3
G2 LOW 0+75N	20	.2	19	7	2	2
G2 LOW 0+50N	16	.5	19	6	2	1
G2 LOW 0+25N	32	.5	27	18	2	1
STD C/AU-S	57	7.3	68	38	18	48

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G3 L6+50W 4+00N	48	.4	44	40	4	1
G3 L6+50W 3+75N	54	.4	32	47	10	2
G3 L6+50W 3+50N	43	.5	38	40	2	1
G3 L6+50W 3+25N	49	.3	34	62	2	2
G3 L6+50W 3+00N	69	.3	37	56	3	1
G3 L6+50W 2+75N	64	.3	30	59	2	1
G3 L6+50W 2+50N	51	.5	36	80	2	1
G3 L6+50W 2+25N	52	.5	36	116	2	1
G3 L6+50W 2+00N	49	.4	40	73	2	1
G3 L6+50W 1+75N	82	.4	31	69	2	1
G3 L6+50W 1+50N	37	.5	34	177	2	1
G3 L6+50W 1+25N	25	.5	44	122	2	61
G3 L6+50W 1+00N	35	.4	34	177	2	1
G3 L6+50W 0+75N	19	.2	30	23	2	1
G3 L6+50W 0+50N	29	.5	32	10	2	2
G3 L6+50W 0+25N	25	.5	36	11	4	1
G3 L6+50W 0+00N	24	.5	24	14	2	1
G3 L6+00W 4+00N	45	.3	34	26	2	17
G3 L6+00W 3+75N	49	.3	52	34	2	1
G3 L6+00W 3+50N	56	.3	46	34	2	1
G3 L6+00W 3+25N	40	.3	33	32	2	1
G3 L6+00W 3+00N	21	.6	23	139	2	1
G3 L6+00W 2+75N	51	.3	34	80	3	1
G3 L6+00W 2+50N	39	.3	24	39	2	1
G3 L6+00W 2+25N	52	.3	36	67	2	1
STD C/AU-S	58	7.3	69	40	17	52

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G3 L6+00W 1+25N	43	.3	34	174	2	1
G3 L6+00W 1+00N	14	.3	20	12	3	1
G3 L6+00W 0+50N	32	.3	37	37	2	1
G3 L6+00W 0+00N	38	.2	33	9	2	1
G3 L5+50W 4+00N	51	.3	35	23	2	1
G3 L5+50W 3+75N	43	.3	41	37	2	1
G3 L5+50W 3+50N	43	.5	49	34	2	1
G3 L5+50W 3+25N	49	.1	26	91	4	1
G3 L5+50W 3+00N	55	.3	29	33	2	2
G3 L5+50W 2+75N	40	.3	28	49	2	1
G3 L5+50W 2+50N	44	.4	39	33	2	1
G3 L5+50W 2+25N	63	.1	15	117	3	1
G3 L5+50W 2+00N	18	.5	18	176	2	1
G3 L5+50W 1+75N	14	.4	15	586	2	1
G3 L5+50W 1+50N	30	.3	31	123	2	1
G3 L5+00W 4+00N	91	.2	59	182	4	1
G3 L5+00W 3+75N	39	.3	33	24	2	1
G3 L5+00W 3+50N	40	.4	47	31	5	1
G3 L5+00W 3+25N	33	.3	36	37	2	2
G3 L5+00W 3+00N	54	.4	38	81	7	1
G3 L5+00W 2+75N	43	.4	39	34	3	1
G3 L5+00W 2+50N	33	.2	31	23	3	1
G3 L5+00W 2+25N	41	.3	39	22	2	1
G3 L5+00W 2+00N	15	.4	12	227	2	3
G3 L5+00W 1+75N	36	.4	27	139	2	3
G3 L5+00W 1+25N	38	.4	26	46	2	4
G3 L5+00W 1+00N	44	.5	29	247	2	1
G3 L5+00W 0+75N	35	.4	33	127	2	1
G3 L5+00W 0+50N	19	.1	15	69	2	1
G3 L4+50W 4+00N	62	.3	47	83	11	1
G3 L4+50W 3+75N	27	.3	50	46	2	2
G3 L4+50W 3+50N	53	.4	73	36	2	1
G3 L4+50W 3+25N	43	.5	47	29	2	1
G3 L4+50W 3+00N	45	.2	29	19	2	1
G3 L4+50W 2+75N	46	.4	51	29	2	2
G3 L4+50W 2+50N	45	.4	60	23	2	1
STD C/AU-S	58	7.7	69	41	16	47

SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G3 L4+50W 2+25N	35	.2	53	30	2	1
G3 L4+50W 2+00N	43	.2	41	48	2	2
G3 L4+50W 1+75N	40	.2	37	57	2	1
G3 L4+50W 1+50N	43	.3	32	118	2	1
G3 L4+50W 1+25N	26	.1	23	86	2	1
G3 L4+50W 1+00N	30	.3	22	70	2	1
G3 L4+50W 0+75N	33	.3	32	166	2	1
G3 L4+50W 0+50N	40	.3	36	183	2	1
G3 L4+50W 0+25N	39	.5	39	74	2	2
G3 L4+50W 0+00N	34	.3	45	29	2	1
G3 L4+00W 4+00N	63	.2	36	123	8	1
G3 L4+00W 3+75N	85	.1	15	118	2	1
G3 L4+00W 3+50N	74	.3	50	70	4	1
G3 L4+00W 3+25N	81	.1	10	38	2	1
G3 L4+00W 3+00N	23	.1	25	59	2	1
G3 L4+00W 2+75N	68	.1	11	68	2	2
G3 L4+00W 2+50N	53	.2	13	129	9	1
G3 L4+00W 2+25N	66	.3	8	28	2	1
G3 L4+00W 2+00N	65	.3	7	58	3	1
G3 L4+00W 1+75N	73	.1	11	111	2	2
G3 L4+00W 1+50N	82	.3	26	32	2	1
G3 L4+00W 1+25N	38	.3	30	80	2	1
G3 L4+00W 1+00N	37	.3	31	61	2	1
G3 L4+00W 0+75N	32	.2	29	174	2	1
G3 L4+00W 0+50N	65	.3	35	129	2	2
G3 L4+00W 0+25N	52	.4	33	139	2	1
G3 L4+00W 0+00N	25	.5	25	120	4	2
G3 L3+50W 4+00N	55	.3	57	28	3	1
G3 L3+50W 3+75N	83	.4	56	21	2	1
G3 L3+50W 3+50N	63	.7	38	18	2	1
G3 L3+50W 3+25N	32	.2	12	94	2	1
G3 L3+50W 3+00N	42	.2	13	98	6	2
G3 L3+50W 2+75N	42	.2	9	103	8	1
G3 L3+50W 2+50N	55	.1	9	85	2	1
G3 L3+50W 2+25N	74	.3	9	38	2	1
G3 L3+50W 2+00N	80	.4	9	54	4	1
STD C/AU-S	58	7.5	68	40	17	49

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G3 L3+50W 1+75N	55	.5	10	136	12	1
G3 L3+50W 1+00N	65	.4	24	60	7	1
G3 L3+50W 0+75N	49	.3	26	70	2	1
G3 L3+50W 0+50N	42	.5	54	65	2	2
G3 L3+50W 0+25N	41	.3	22	160	4	1
G3 L3+50W 0+00N	30	.4	28	117	2	1
G3 L3+00W 3+75N	60	.7	55	24	4	1
G3 L3+00W 3+50N	57	.4	45	14	2	1
G3 L3+00W 3+25N	45	.3	99	132	13	1
G3 L3+00W 3+00N	70	.5	72	32	8	1
G3 L3+00W 2+75N	62	.4	54	41	4	2
G3 L3+00W 2+50N	65	.4	75	77	11	1
G3 L3+00W 2+25N	70	.5	21	103	20	1
G3 L3+00W 1+00N	77	.3	14	103	26	1
G3 L3+00W 0+75N	72	.4	14	74	6	1
G3 L3+00W 0+50N	37	.5	33	37	2	1
G3 L3+00W 0+25N	50	.2	14	1079	10	1
G3 L3+00W 0+00N	60	.5	62	24	2	2
G3 L2+50W 4+00N	37	.3	49	43	7	1
G3 L2+50W 3+75N	43	.4	61	122	14	1
G3 L2+50W 3+50N	51	.3	65	48	7	2
G3 L2+50W 3+25N	53	.3	68	63	8	1
G3 L2+50W 3+00N	81	.5	68	13	2	1
G3 L2+50W 2+75N	68	.4	34	37	2	2
G3 L2+50W 2+50N	81	.3	98	27	2	1
G3 L2+50W 2+25N	65	.3	48	13	2	1
G3 L2+50W 2+00N	54	.4	39	42	2	1
G3 L2+50W 1+75N	62	.2	99	107	34	1
G3 L2+50W 1+50N	22	.1	20	125	24	4
G3 L2+50W 1+25N	258	.4	30	24	7	1
G3 L2+50W 1+00N	67	.3	19	695	184	1
G3 L2+50W 0+75N	65	.3	6	59	6	1
G3 L2+50W 0+50N	44	.3	4	55	4	1
G3 L2+50W 0+25N	59	.1	34	158	2	2
G3 L2+50W 0+00N	48	.4	58	95	2	1
G3 L2+00W 4+00N	60	.3	45	14	2	1
STD C/AU-S	58	7.6	67	40	14	48

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G3 L2+00W 3+75N	41	.2	36	23	2	1
G3 L2+00W 3+50N	62	.4	39	66	2	1
G3 L2+00W 3+25N	49	.2	48	15	2	2
G3 L2+00W 3+00N	47	.2	41	33	2	1
G3 L2+00W 2+75N	54	.1	52	55	2	3
G3 L2+00W 2+50N	59	.4	25	19	2	1
G3 L2+00W 2+25N	81	.5	36	8	2	2
G3 L2+00W 2+00N	64	.6	48	7	2	1
G3 L2+00W 1+75N	75	.5	58	21	2	1
G3 L2+00W 1+50N	76	.4	59	97	7	3
G3 L2+00W 1+25N	24	.4	23	294	15	1
G3 L2+00W 1+00N	47	.5	14	214	12	6
G3 L2+00W 0+75N	38	.4	8	91	4	3
G3 L2+00W 0+50N	143	.4	4	66	2	1
G3 L2+00W 0+25N	228	.5	12	13	2	1
G3 L2+00W 0+00N	99	.1	13	85	11	1
G3 L1+50W 4+00N	63	.7	41	11	2	1
G3 L1+50W 3+75N	46	.2	52	6	2	1
G3 L1+50W 3+50N	56	.4	52	21	2	1
G3 L1+50W 3+25N	54	.4	51	9	2	1
G3 L1+50W 3+00N	60	.3	54	8	2	1
G3 L1+50W 2+75N	50	.1	46	26	2	1
G3 L1+50W 2+50N	50	.5	35	69	2	1
G3 L1+50W 2+25N	90	.5	67	38	2	1
G3 L1+50W 2+00N	88	.4	58	28	2	2
G3 L1+50W 1+75N	64	.5	52	25	2	1
G3 L1+50W 1+50N	74	.5	39	15	2	1
G3 L1+50W 1+25N	89	.9	49	24	2	1
G3 L1+50W 0+75N	66	.3	13	119	8	1
G3 L1+50W 0+50N	109	.5	5	61	6	2
G3 L1+50W 0+25N	85	.1	24	115	18	1
G3 L1+50W 0+00N	37	.5	33	178	49	1
G3 L1+00W 4+00N	41	.2	46	8	2	1
G3 L1+00W 3+75N	53	.2	52	11	2	1
G3 L1+00W 3+50N	38	.2	38	6	2	4
G3 L1+00W 3+25N	75	.5	59	16	2	1
STD C/AU-S	57	7.2	67	37	15	52

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SAMPLE#	CU PPM	AG PPM	NI PPM	AS PPM	SB PPM	AU* PPB
G3 L1+00W 3+00N	34	.3	43	14	2	1
G3 L1+00W 2+75N	52	.5	52	15	2	1
G3 L1+00W 2+50N	52	.4	57	10	2	1
G3 L1+00W 2+25N	55	.7	57	10	2	1
G3 L1+00W 2+00N	57	.7	58	28	2	1
G3 L1+00W 1+75N	77	.5	32	20	2	2
G3 L1+00W 1+25N	71	.4	40	19	2	1
G3 L1+00W 1+00N	72	.4	26	45	2	2
G3 L1+00W 0+75N	79	.3	16	54	9	1
G3 L1+00W 0+25N	124	.3	20	260	45	1
G3 L0+00W 4+00N	31	.4	43	8	2	1
G3 L0+00W 3+75N	27	.4	39	5	2	1
G3 L0+00W 3+50N	45	.3	52	5	2	1
G3 L0+00W 3+25N	40	.4	48	6	2	2
G3 L0+00W 3+00N	34	.4	42	7	2	2
G3 L0+00W 2+75N	38	.4	44	7	2	1
G3 L0+00W 2+50N	40	.4	47	3	2	1
G3 L0+00W 2+25N	38	.4	48	13	2	1
G3 L0+00W 2+00N	37	.4	47	5	2	1
G3 L0+00W 1+75N	51	.6	39	11	2	1
G3 L0+00W 1+50N	56	.8	52	9	2	2
G3 L0+00W 1+25N	48	.6	46	10	2	1
G3 L0+00W 1+00N	49	.3	52	12	2	1
G3 L0+00W 0+75N	63	.6	68	19	2	1
G3 L0+00W 0+50N	51	.3	60	13	2	3
G3 L0+00W 0+25N	57	.6	35	22	2	1
G3 L0+00W 0+00N	38	.4	62	63	2	1
STD C/AU-S	57	7.6	70	41	17	49

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##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR1PLOT.TXT

Variable = AU   Unit = PPB   N = 39
N CI = 20

Transform = Logarithmic   Number of Populations = 2

# of Missing Observations = 0.

474 Observations Were Below the Minimum Value of 2.1000
1 Observations Were Above the Maximum Value of 200.0000

==

Raw Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -5.628

Parameterized Degrees of Freedom = 3

Population	Mean		Std Dev	Percentage
1	4.658	-	3.070	88.65
		+	7.070	
2	87.571	-	57.148	11.35
		+	134.191	

==

User Defined Thresholds.

Thresholds
205.636
22.542
2.023

##

##

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = AU   Unit = PPB   N = 89

Mean =	0.8099	Min =	0.4771	1st Quartile =	0.4771
Std. Dev. =	0.4435	Max =	2.1761	Median =	0.6990
CV % =	54.7626	Skewness =	1.8968	3rd Quartile =	0.8451

Anti-Log Mean = 6.455   Anti-Log Std. Dev. : (-) 2.325
(+) 17.922

%	cum %	antilog	cls int	(# of bins = 20 - bin size = 0.0894)
0.00	0.56	2.707	0.4324	
30.34	30.56	3.325	0.5218	***************************
15.73	46.11	4.086	0.6113	**************
13.48	59.44	5.020	0.7007	************
8.99	68.33	6.167	0.7901	********
8.99	77.22	7.577	0.8795	********
5.62	82.78	9.310	0.9689	*****
4.49	87.22	11.438	1.0583	****
0.00	87.22	14.053	1.1478	
1.12	88.33	17.266	1.2372	*
0.00	88.33	21.213	1.3266	
0.00	88.33	26.063	1.4160	
0.00	88.33	32.022	1.5054	
1.12	89.44	39.343	1.5949	*
0.00	89.44	48.337	1.6843	
1.12	90.56	59.389	1.7737	*
1.12	91.67	72.966	1.8631	*
2.25	93.89	89.648	1.9525	**
1.12	95.00	110.144	2.0420	*
2.25	97.22	135.326	2.1314	**
2.25	99.44	166.265	2.2208	**

0 1 2 3 4

##

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SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = AG Unit = PPM N = 564

Mean =	-0.7560	Min =	-1.0000	1st Quartile =	-1.0000
Std. Dev. =	0.2195	Max =	0.4150	Median =	-0.6990
CV % =	29.0328	Skewness =	0.3634	3rd Quartile =	-0.5229

Anti-Log Mean = 0.175 Anti-Log Std. Dev. : (-) 0.106
(+) 0.291

%	cum %	antilog	cls int	(# of bins = 28 - bin size = 0.0524)
0.00	0.09	0.094	-1.0262	
39.18	39.20	0.106	-0.9738	****************************** --> 90
0.00	39.20	0.120	-0.9214	
0.00	39.20	0.135	-0.8690	
0.00	39.20	0.153	-0.8166	
0.00	39.20	0.172	-0.7642	
0.00	39.20	0.194	-0.7118	
32.27	71.42	0.219	-0.6594	****************************** --> 74
0.00	71.42	0.247	-0.6070	
0.00	71.42	0.279	-0.5545	
22.87	94.25	0.315	-0.5021	****************************** --> 53
0.00	94.25	0.355	-0.4497	
3.90	98.14	0.401	-0.3973	*********
0.00	98.14	0.452	-0.3449	
1.06	99.20	0.510	-0.2925	**
0.00	99.20	0.575	-0.2401	
0.35	99.56	0.649	-0.1877	*
0.18	99.73	0.732	-0.1353	
0.00	99.73	0.826	-0.0829	
0.00	99.73	0.932	-0.0305	
0.00	99.73	1.052	0.0219	
0.00	99.73	1.187	0.0743	
0.00	99.73	1.339	0.1267	
0.00	99.73	1.511	0.1791	
0.00	99.73	1.704	0.2316	
0.00	99.73	1.923	0.2840	
0.00	99.73	2.170	0.3364	
0.00	99.73	2.448	0.3888	
0.18	99.91	2.762	0.4412	

0 1 2 3 4

Each "*" represents approximately 2.4 observations.

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SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = CU Unit = PPM N = 564

Mean =	1.6005	Min =	1.2553	1st Quartile =	1.4624
Std. Dev. =	0.1963	Max =	2.6284	Median =	1.5798
CV % =	12.2625	Skewness =	1.0149	3rd Quartile =	1.7076

Anti-Log Mean = 39.855 Anti-Log Std. Dev. : (-) 25.364
(+) 62.623

%	cum %	antilog	cls int	(# of bins = 36 - bin size = 0.0392)
0.00	0.09	17.205	1.2357	
0.89	0.97	18.832	1.2749	**
2.66	3.63	20.612	1.3141	******
3.55	7.17	22.561	1.3534	********
4.96	12.12	24.694	1.3926	***********
9.57	21.68	27.028	1.4318	**********************
5.67	27.35	29.583	1.4710	*************
8.51	35.84	32.380	1.5103	********************
7.80	43.63	35.441	1.5495	******************
7.27	50.88	38.792	1.5887	*****************
9.57	60.44	42.460	1.6280	**********************
7.27	67.70	46.474	1.6672	*****************
7.09	74.78	50.867	1.7064	****************
6.03	80.80	55.676	1.7457	**************
4.61	85.40	60.940	1.7849	***********
2.30	87.70	66.701	1.8241	*****
2.66	90.35	73.007	1.8634	******
1.77	92.12	79.910	1.9026	****
1.77	93.89	87.464	1.9418	****
1.77	95.66	95.733	1.9811	****
0.35	96.02	104.784	2.0203	*
1.24	97.26	114.690	2.0595	***
0.71	97.96	125.533	2.0988	**
0.71	98.67	137.401	2.1380	**
0.53	99.20	150.391	2.1772	*
0.18	99.38	164.609	2.2165	
0.00	99.38	180.171	2.2557	
0.18	99.56	197.205	2.2949	
0.00	99.56	215.849	2.3341	
0.00	99.56	236.255	2.3734	
0.00	99.56	258.591	2.4126	
0.00	99.56	283.038	2.4518	
0.00	99.56	309.797	2.4911	
0.00	99.56	339.085	2.5303	
0.18	99.73	371.143	2.5695	
0.00	99.73	406.231	2.6088	
0.18	99.91	444.636	2.6480	

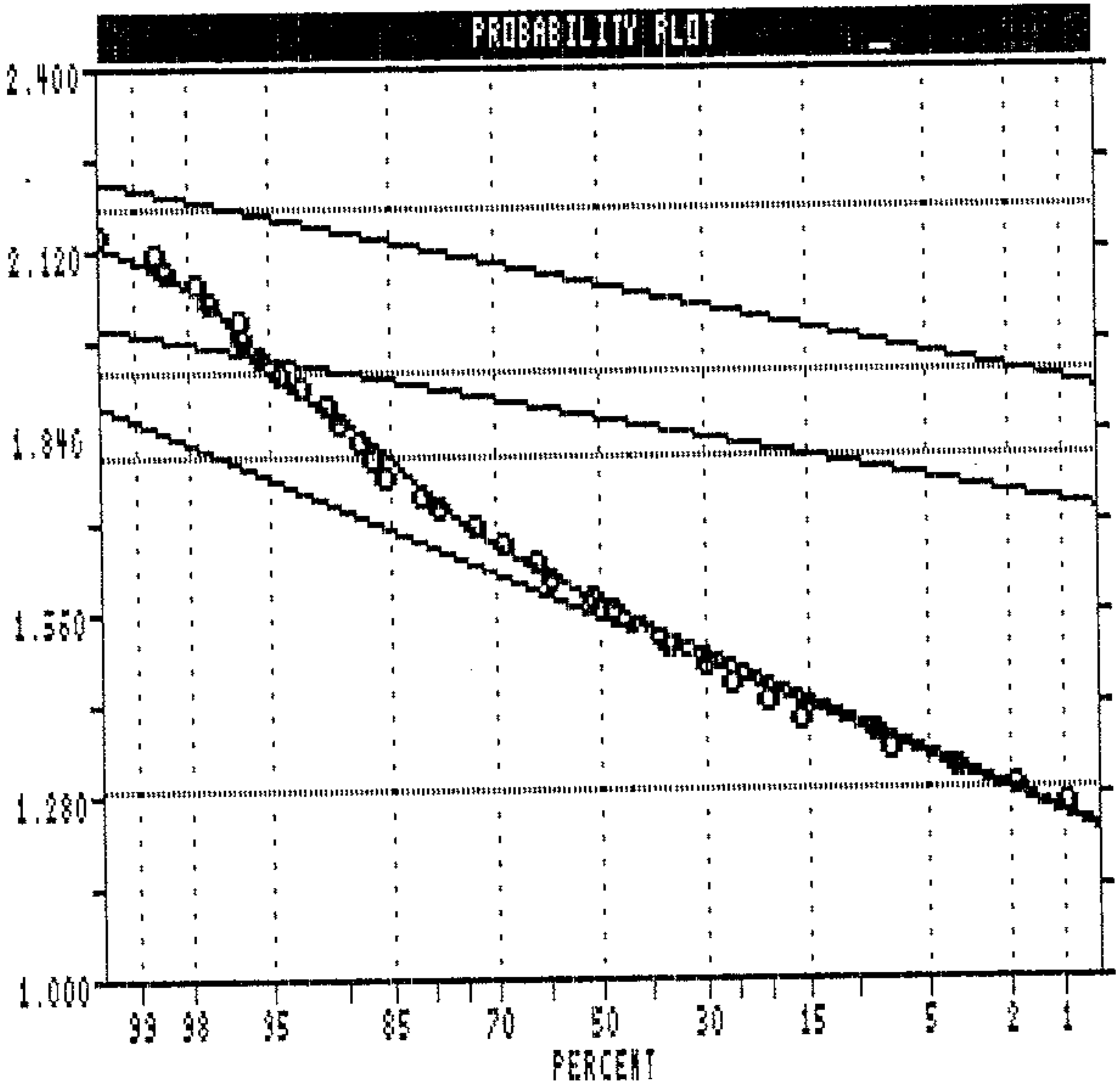
0 1 2 3 4

Each "*" represents approximately 2.4 observations.

##

13:11:17
03/23/88

BUMAX DEADMAN PROJECT 1987 GRID 1



LOGARITHMIC VALUES

VARIABLE = CU
UNIT = PPM
N = 561
N CI = 36

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	1.5454	0.1306	86.0
2	1.8550	0.0560	10.0
3	2.0562	0.0631	4.0

THRESHOLDS

2.1823 1.9299
1.7963 1.2841

CLASS INTERVAL ML
PARAMETER ESTIMATES

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR1PLOT.TXT

Variable = CU Unit = PPM N = 561
N CI = 36

Transform = Logarithmic Number of Populations = 3

# of Missing Observations = 0.

0 Observations Were Below the Minimum Value of 1.0000
3 Observations Were Above the Maximum Value of 180.0000

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1854.994

Parameterized Degrees of Freedom = 5

Population	Mean		Std Dev	Percentage
1	35.111	-	25.989	86.00
		+	47.433	
2	71.610	-	62.949	10.00
		+	81.463	
3	113.807	-	98.422	4.00
		+	131.597	

User Defined Thresholds.

Thresholds
152.160
95.094
62.360
19.235

##

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = NI Unit = PPM N = 563

Mean =	1.4158	Min =	0.8451	1st Quartile =	1.3222
Std. Dev. =	0.1425	Max =	1.8261	Median =	1.3979
CV % =	10.0674	Skewness =	-0.2121	3rd Quartile =	1.5152

Anti-Log Mean = 26.052 Anti-Log Std. Dev. : (-) 18.763
(+) 36.172

%	cum %	antilog	cls int	(# of bins = 36 - bin size = 0.0280)
0.00	0.09	6.778	0.8311	
0.18	0.27	7.230	0.8591	
0.00	0.27	7.712	0.8871	
0.18	0.44	8.226	0.9152	
0.00	0.44	8.774	0.9432	
0.18	0.62	9.359	0.9712	
0.00	0.62	9.983	0.9993	
0.53	1.15	10.648	1.0273	*
0.18	1.33	11.358	1.0553	
0.53	1.86	12.115	1.0833	*
0.00	1.86	12.923	1.1114	
0.89	2.75	13.785	1.1394	**
1.24	3.99	14.703	1.1674	***
1.42	5.41	15.684	1.1954	***
1.78	7.18	16.729	1.2235	****
1.95	9.13	17.844	1.2515	****
5.15	14.27	19.034	1.2795	************
5.51	19.77	20.303	1.3076	*************
6.57	26.33	21.656	1.3356	***************
11.90	38.21	23.100	1.3636	****************************
6.22	44.41	24.640	1.3916	**************
10.66	55.05	26.283	1.4197	*************************
10.12	65.16	28.035	1.4477	************************
2.66	67.82	29.904	1.4757	******
4.97	72.78	31.897	1.5038	***********
4.62	77.39	34.024	1.5318	***********
4.09	81.47	36.292	1.5598	*********
4.80	86.26	38.711	1.5878	***********
4.44	90.69	41.292	1.6159	**********
4.26	94.95	44.045	1.6439	**********
2.66	97.61	46.981	1.6719	******
1.24	98.85	50.113	1.6999	***
0.36	99.20	53.454	1.7280	*
0.36	99.56	57.017	1.7560	*
0.18	99.73	60.818	1.7840	
0.00	99.73	64.873	1.8121	
0.18	99.91	69.197	1.8401	

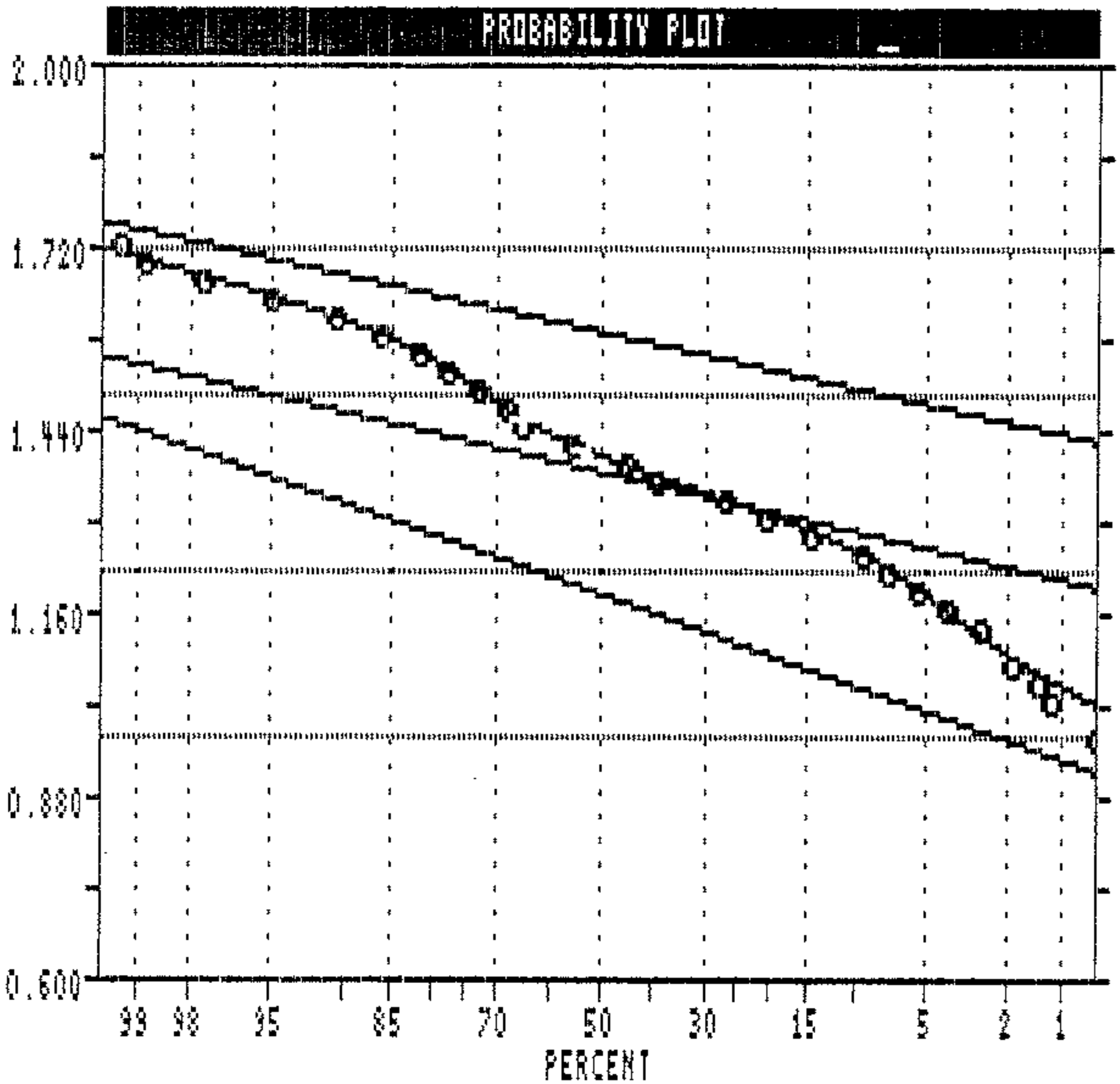
0 1 2 3 4

Each "*" represents approximately 2.4 observations.

##

13:34:20
03/23/88

BUMAX DEADMAN PROJECT 1987   GRID 1



LOGARITHMIC VALUES

VARIABLE = NI
UNIT = PPM
N = 563
N CI = 36

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	1.1837	0.1096	9.2
2	1.3714	0.0706	62.2
3	1.5807	0.0671	28.7

THRESHOLDS

1.7149	1.4950
1 2169	0.9645

INCOMPLETE ITERATION
PARAMETER ESTIMATES

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR1PLOT.TXT

Variable = NI   Unit = PPM   N = 563
N CI = 36

Transform = Logarithmic   Number of Populations = 3

# of Missing Observations = 0.

0 Observations Were Below the Minimum Value of 1.0000
1 Observations Were Above the Maximum Value of 100.0000

Incomplete Iteration Parameter Estimates

Population	Mean		Std Dev	Percentage
1	15.265	-	11.860	9.17
		+	19.648	
2	23.517	-	19.990	62.17
		+	27.666	
3	38.082	-	32.630	28.66
		+	44.444	

User Defined Thresholds.

Thresholds
51.868
31.261
16.478
9.215

##

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = SB Unit = PPM N = 564

Mean =	0.3383	Min =	0.3010	1st Quartile =	0.3010
Std. Dev. =	0.1377	Max =	1.2553	Median =	0.3010
CV % =	40.6972	Skewness =	4.3367	3rd Quartile =	0.3010

Anti-Log Mean = 2.179 Anti-Log Std. Dev. : (-) 1.587
(+) 2.992

%	cum %	antilog	cls int	(# of bins = 28 - bin size = 0.0353)
0.00	0.09	1.920	0.2834	
90.43	90.35	2.083	0.3187	****************************** --> 206
0.00	90.35	2.260	0.3540	
0.00	90.35	2.451	0.3894	
0.00	90.35	2.659	0.4247	
0.00	90.35	2.884	0.4601	
4.61	94.96	3.129	0.4954	***********
0.00	94.96	3.394	0.5308	
0.00	94.96	3.682	0.5661	
0.00	94.96	3.994	0.6014	
0.71	95.66	4.333	0.6368	**
0.00	95.66	4.700	0.6721	
0.53	96.19	5.099	0.7075	*
0.00	96.19	5.531	0.7428	
0.00	96.19	6.000	0.7782	
0.35	96.55	6.509	0.8135	*
1.06	97.61	7.061	0.8488	**
0.00	97.61	7.659	0.8842	
0.35	97.96	8.308	0.9195	*
0.35	98.32	9.013	0.9549	*
0.00	98.32	9.777	0.9902	
0.35	98.67	10.606	1.0255	*
0.18	98.85	11.505	1.0609	
0.18	99.03	12.481	1.0962	
0.00	99.03	13.539	1.1316	
0.35	99.38	14.686	1.1669	*
0.35	99.73	15.932	1.2023	*
0.00	99.73	17.282	1.2376	
0.18	99.91	18.748	1.2729	

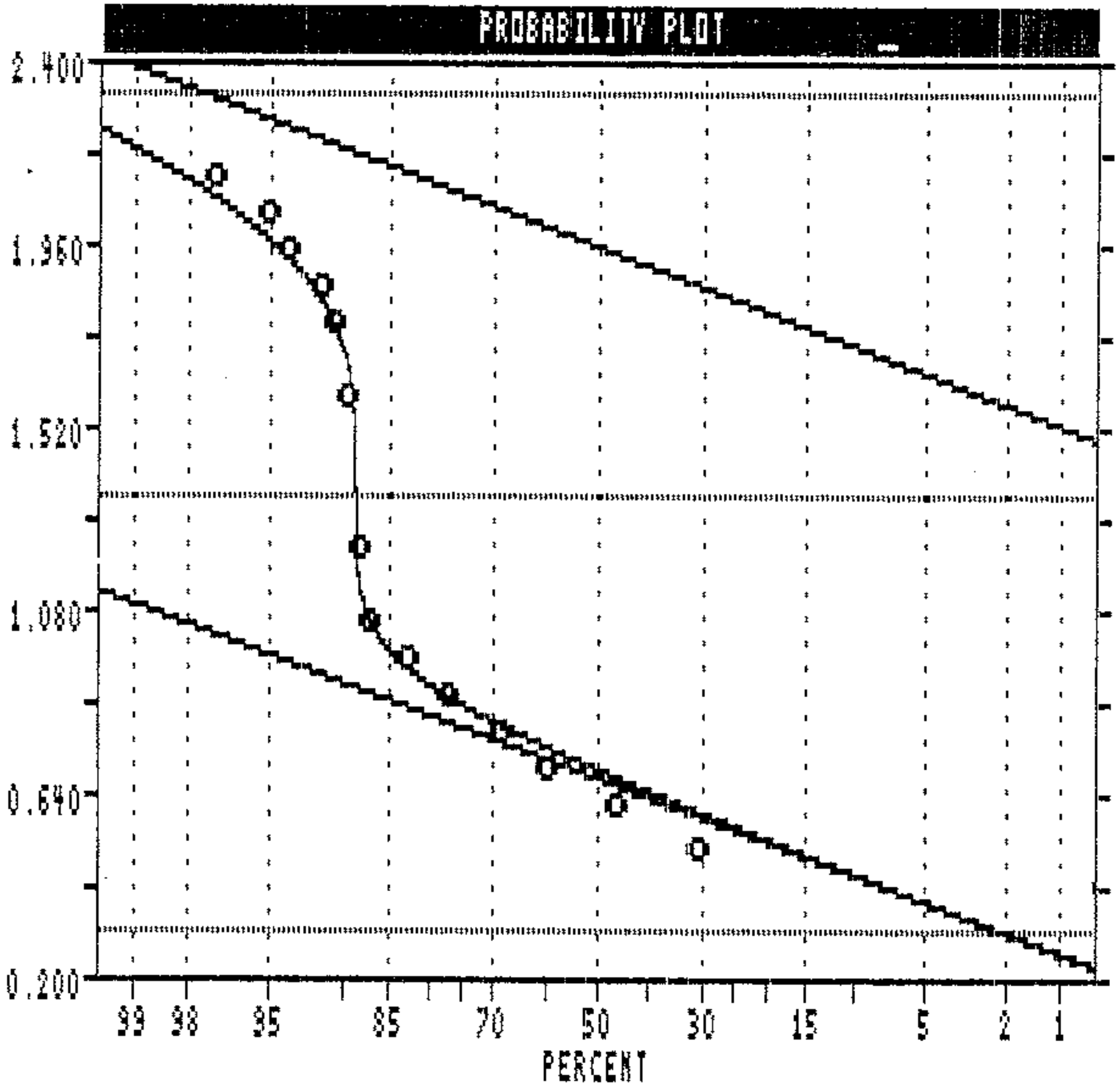
0 1 2 3 4

Each "*" represents approximately 2.4 observations.

##

16:58:36
03/23/88

BUHAX DEADMAN PROJECT 1987 GRID 1



LOGARITHMIC VALUES

VARIABLE = AU
UNIT = PPB
N = 89
N CI = 20

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	0.6682	0.1812	88.6
2	1.9424	0.1854	11.4

THRESHOLDS

2.3131 1.3530
0.3059

RAW DATA ML
PARAMETER ESTIMATES

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = AS Unit = [illegible] N = 524

Mean =	1.0201	Min =	[illegible]	1st Quartile =	0.7782
Std. Dev. =	0.3890	Max =	2.3148	Median =	[illegible]
C.V. =	[illegible]	Skewness =	[illegible]	3rd Quartile =	[illegible]

Antilog Mean = 10.475 Antilog Std. Dev. (-) 4.277

(+) 25.656

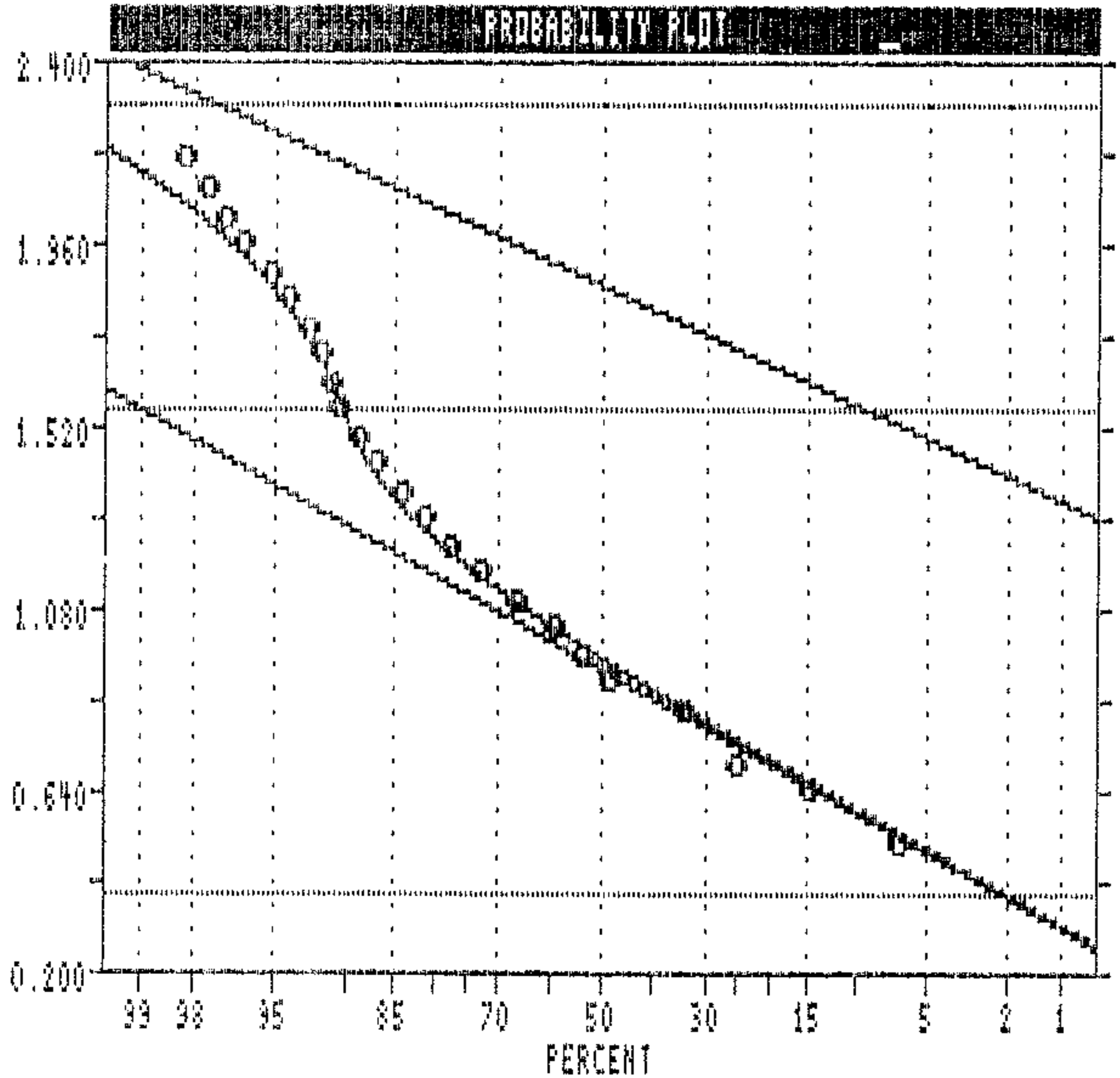
%	cum %	antilog	cls inc	# of bins = 28 -- bin size = 0.0662
0.00	0.10	2.780	0.4440	
6.49	6.57	3.238	0.5102	**************
0.00	6.57	3.771	0.5764	
8.02	14.37	4.392	0.6426	******************
10.11	24.67	5.115	0.7089	***********************
0.00	24.67	5.958	0.7751	
8.78	33.43	6.939	0.8413	*******************
14.69	48.10	8.082	0.9075	********************************
5.73	53.81	9.412	0.9737	************
5.53	59.33	10.963	1.0399	************
7.06	66.38	12.768	1.1061	***************
6.11	72.48	14.871	1.1723	*************
4.96	77.43	17.320	1.2385	***********
3.82	81.24	20.172	1.3048	********
2.86	84.10	23.495	1.3710	******
2.86	86.95	27.364	1.4372	******
1.91	88.56	31.871	1.5034	****
1.72	90.57	37.120	1.5696	****
0.57	91.14	43.233	1.6358	*
0.95	92.10	50.353	1.7020	**
0.76	92.86	58.646	1.7682	**
1.34	94.19	68.304	1.8344	***
0.95	95.14	79.553	1.9007	**
1.34	96.48	92.655	1.9669	***
0.57	97.05	107.913	2.0331	*
0.57	97.62	125.657	2.0993	*
0.57	98.19	146.387	2.1655	*
1.34	99.52	171.495	2.2317	***
0.38	99.90	198.574	2.2979	*

0 1 2 3 4

Each '*' represents approximately 0.5 observations.

16:33:19
03/23/88

BUMAX DEADMAN PROJECT 1987 GRID 1



LOGARITHMIC VALUES

VARIABLE = AS
UNIT = PPM
N = 524
N CI = 28

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	0.9253	0.2675	90.0
2	1.8503	0.2229	10.0

THRESHOLDS

2.2960 1.5628
0.3903

CLASS INTERVAL ML
PARAMETER ESTIMATES

PARAMETRIC SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = [illegible]

Variable = AG   Units = PPM   N = [illegible]

Transform = Logarithmic   Number of Populations = 2

# of Missing Observations = 0.

31 Observations Were Below the Minimum Value of [illegible]
7 Observations Were Above the Maximum Value of [illegible]

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1604.221

Parameterized Degrees of Freedom = 5

Population	Mean		Std Dev	Percentage
1	8.419	-	4.548	90.00
		+	15.588	
2	70.935	-	42.402	10.00
		+	118.[illegible]	

User Defined Thresholds.

Thresholds
[illegible]
[illegible]
[illegible]

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = AU Unit = PPM N = 94

Mean =	0.6882	Min =	0.4771	1st Quartile =	0.4771
Std. Dev. =	0.2898	Max =	2.0253	Median =	0.6021
CV % =	42.1099	Skewness =	2.0147	3rd Quartile =	0.7782

Anti-Log Mean = 4.677 Anti-Log Std. Dev. : (-) 2.503
(+) 9.505

%	cum %	antilog	cls int	(# of bins = 36 - bin size = 0.0442)
0.00	0.53	2.851	0.4550	
43.62	43.68	3.157	0.4992	******************************* --> 41
0.00	43.68	3.495	0.5435	
0.00	43.68	3.870	0.5877	
14.89	58.42	4.285	0.6319	**************
0.00	58.42	4.744	0.6762	
11.70	70.00	5.253	0.7204	***********
0.00	70.00	5.816	0.7646	
7.45	77.37	6.440	0.8089	*******
4.26	81.58	7.130	0.8531	****
0.00	81.58	7.895	0.8973	
3.19	84.74	8.741	0.9416	***
2.13	86.84	9.679	0.9858	**
2.13	88.95	10.716	1.0300	**
0.00	88.95	11.865	1.0743	
3.19	92.11	13.137	1.1185	***
1.06	93.16	14.546	1.1627	*
0.00	93.16	16.106	1.2070	
0.00	93.16	17.833	1.2512	
0.00	93.16	19.745	1.2954	
1.06	94.21	21.862	1.3397	*
2.13	96.32	24.206	1.3839	**
0.00	96.32	26.801	1.4281	
0.00	96.32	29.674	1.4724	
1.06	97.37	32.856	1.5166	*
0.00	97.37	36.379	1.5609	
1.06	98.42	40.280	1.6051	*
0.00	98.42	44.598	1.6493	
0.00	98.42	49.380	1.6936	
0.00	98.42	54.675	1.7378	
0.00	98.42	60.537	1.7820	
0.00	98.42	67.028	1.8263	
0.00	98.42	74.214	1.8705	
0.00	98.42	82.172	1.9147	
0.00	98.42	90.982	1.9590	
0.00	98.42	100.737	2.0032	
1.06	99.47	111.536	2.0474	*

0 1 2 3 4

##

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR2PLOT.TXT

Variable = AG Unit = PPM N = 692
N CI = 29

Transform = Logarithmic Number of Populations = 1

# of Missing Observations = 0.

==

Users Visual Parameter Estimates

Population	Mean		Std Dev	Percentage
1	0.166	-	0.095	100.00
		+	0.288	

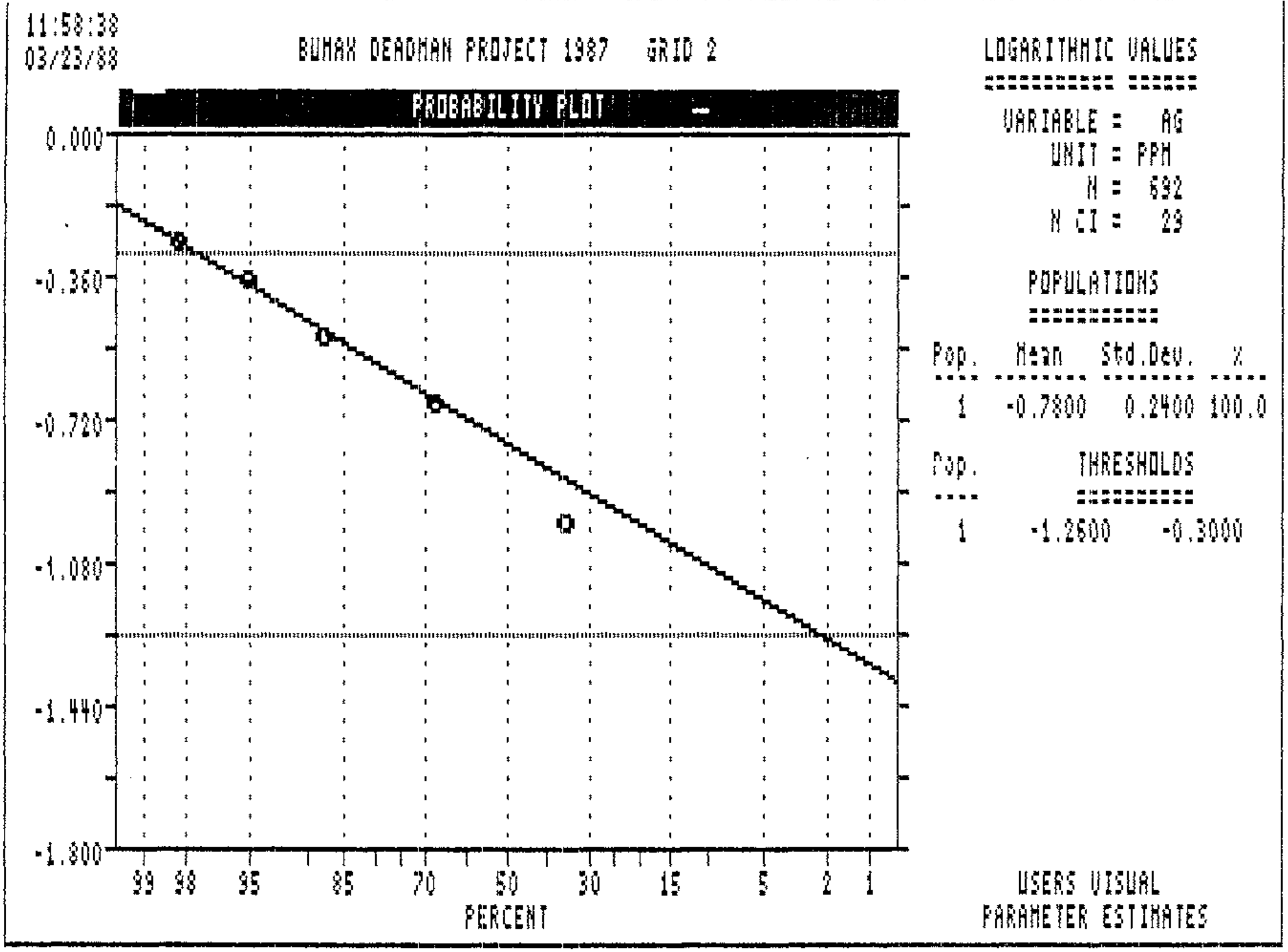
==

Default Thresholds.

Standard Deviation Multiplier = 2.0

Pop.	Thresholds	
1	0.055	0.501

##


11:58:38
03/23/88
BUMAX DEADMAN PROJECT 1987 GRID 2
PROBABILITY PLOT
0.000
-0.360
-0.720
-1.080
-1.440
-1.800
99 98 95 85 70 50 30 15 5 2 1
PERCENT
LOGARITHMIC VALUES
VARIABLE = AG
UNIT = PPM
N = 692
N CI = 29
POPULATIONS
Pop. Mean Std.Dev. %
1 -0.7800 0.2400 100.0
Pop. THRESHOLDS
1 -1.2600 -0.3000
USERS VISUAL
PARAMETER ESTIMATES

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = CU Unit = PPM N = 691

Mean =	1.6210	Min =	0.8451	1st Quartile =	1.4472
Std. Dev. =	0.2251	Max =	2.2529	Median =	1.6074
CV % =	13.8891	Skewness =	0.3523	3rd Quartile =	1.7782

Anti-Log Mean = 41.787 Anti-Log Std. Dev. : (-) 24.883
(+) 70.177

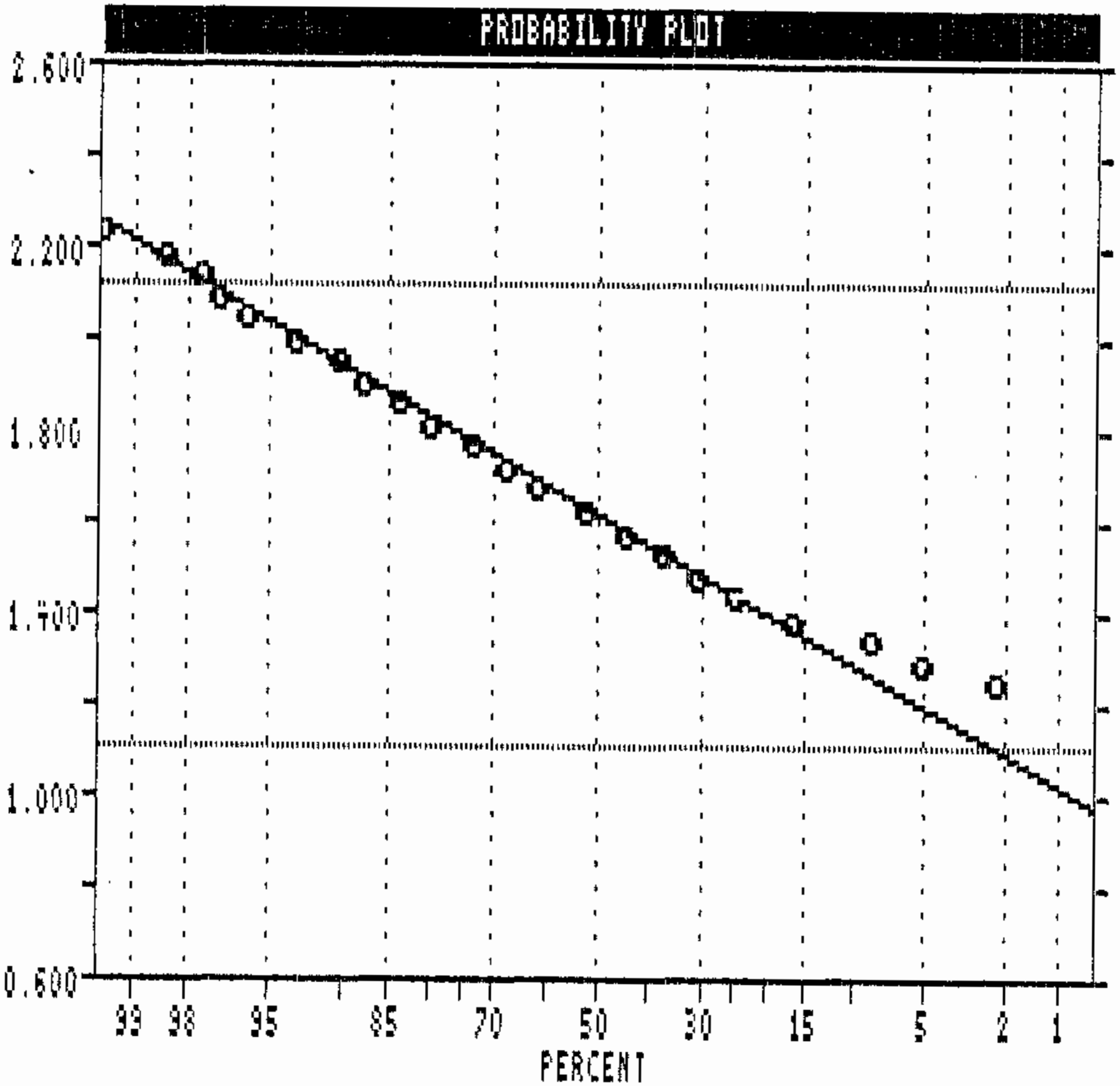
%	cum %	antilog	cls int	(# of bins = 29 - bin size = 0.0503)
0.00	0.07	6.606	0.8200	
0.14	0.22	7.417	0.8702	
0.00	0.22	8.327	0.9205	
0.00	0.22	9.350	0.9708	
0.00	0.22	10.497	1.0211	
0.00	0.22	11.785	1.0713	
0.00	0.22	13.232	1.1216	
0.00	0.22	14.856	1.1719	
1.01	1.23	16.679	1.2222	***
2.32	3.54	18.726	1.2725	******
4.78	8.31	21.025	1.3227	************
5.07	13.37	23.605	1.3730	*************
7.81	21.17	26.502	1.4233	********************
7.38	28.54	29.755	1.4736	*******************
7.96	36.49	33.407	1.5238	*********************
7.67	44.15	37.507	1.5741	********************
10.42	54.55	42.111	1.6244	***************************
7.96	62.50	47.279	1.6747	*********************
6.51	69.00	53.082	1.7249	*****************
5.79	74.78	59.597	1.7752	***************
6.08	80.85	66.911	1.8255	****************
5.21	86.05	75.123	1.8758	**************
3.47	89.52	84.344	1.9261	*********
3.18	92.70	94.696	1.9763	********
2.89	95.59	106.318	2.0266	********
1.59	97.18	119.367	2.0769	****
0.58	97.76	134.017	2.1272	**
0.87	98.63	150.466	2.1774	**
0.72	99.35	168.933	2.2277	**
0.58	99.93	189.667	2.2780	**

0 1 2 3 4

Each "*" represents approximately 2.6 observations.

11:07:15
03/23/88

BUMAX DEADMAN PROJECT GRID 2



LOGARITHMIC VALUES

VARIABLE = CU P
UNIT = PM
N = 692
N CI = 36

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	1.6100	0.2550	100.0

THRESHOLDS

2.1200 1.1000

USERS VISUAL
PARAMETER ESTIMATES

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR2PLOT.TXT .

Variable = CU Unit = PPM N = 691
N CI = 29

Transform = Logarithmic Number of Populations = 1

# of Missing Observations = 0.

0 Observations Were Below the Minimum Value of 5.0000
1 Observations Were Above the Maximum Value of 200.0000

Users Visual Parameter Estimates

Population	Mean		Std Dev	Percentage
1	40.738	-	22.909	100.00
		+	72.444	

Default Thresholds.

Standard Deviation Multiplier = 2.0

Pop.	Thresholds	
1	12.882	128.825

##

##

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = NI P   Unit = PM   N = 692

Mean =	1.4294	Min =	0.4771	1st Quartile =	1.3222
Std. Dev. =	0.1924	Max =	2.1173	Median =	1.4624
CV % =	13.4571	Skewness =	-1.1251	3rd Quartile =	1.5682

Anti-Log Mean = 26.878   Anti-Log Std. Dev. : (-) 17.260
(+) 41.855

%	cum %	antilog	cls int	(# of bins = 36 - bin size = 0.0469)
0.00	0.07	2.842	0.4537	
0.29	0.36	3.166	0.5006	*
0.00	0.36	3.527	0.5474	
0.00	0.36	3.929	0.5943	
0.29	0.65	4.377	0.6411	*
0.00	0.65	4.875	0.6880	
0.14	0.79	5.431	0.7349	
0.43	1.23	6.050	0.7817	*
0.00	1.23	6.739	0.8286	
0.14	1.37	7.507	0.8754	
0.58	1.95	8.362	0.9223	**
0.87	2.81	9.315	0.9692	**
0.58	3.39	10.376	1.0160	**
1.16	4.55	11.558	1.0629	***
0.72	5.27	12.875	1.1098	**
3.61	8.87	14.342	1.1566	*********
1.16	10.03	15.976	1.2035	***
3.18	13.20	17.797	1.2503	********
6.94	20.13	19.824	1.2972	******************
8.67	28.79	22.083	1.3441	***********************
7.51	36.29	24.599	1.3909	********************
9.68	45.96	27.402	1.4378	*************************
10.69	56.64	30.524	1.4846	****************************
12.72	69.34	34.002	1.5315	*********************************
6.50	75.83	37.876	1.5784	*****************
13.01	88.82	42.192	1.6252	**********************************
5.78	94.59	46.999	1.6721	***************
3.76	98.34	52.354	1.7189	**********
0.87	99.21	58.319	1.7658	**
0.14	99.35	64.964	1.8127	
0.29	99.64	72.366	1.8595	*
0.14	99.78	80.611	1.9064	
0.00	99.78	89.796	1.9533	
0.00	99.78	100.027	2.0001	
0.00	99.78	111.424	2.0470	
0.00	99.78	124.120	2.0938	
0.14	99.93	138.262	2.1407	

0 1 2 3 4

Each "*" represents approximately 2.6 observations.

##

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR2PLOT.TXT

Variable = NI Unit = PPM N = 414
N CI = 27

Transform = Logarithmic Number of Populations = 1

# of Missing Observations = 0.

277 Observations Were Below the Minimum Value of 25.0000
1 Observations Were Above the Maximum Value of 100.0000

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1219.612

Parameterized Degrees of Freedom = 1

Population	Mean		Std Dev	Percentage
1	35.387	-	29.039	100.00
		+	43.123	

Default Thresholds.

Standard Deviation Multiplier = 2.0

Pop.	Thresholds	
1	23.830	52.551

##

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = SB   Unit = PPM   N = 66

Mean =	0.7746	Min =	0.4771	1st Quartile =	0.4771
Std. Dev. =	0.3302	Max =	1.9138	Median =	0.6990
CV % =	42.6283	Skewness =	1.4844	3rd Quartile =	0.9031

Anti-Log Mean = 5.951   Anti-Log Std. Dev. : (-) 2.782
(+) 12.729

%	cum %	antilog	cls int	(# of bins = 36 - bin size = 0.0410)
0.00	0.75	2.862	0.4566	
27.27	27.61	3.145	0.4976	******************
0.00	27.61	3.457	0.5387	
0.00	27.61	3.800	0.5797	
19.70	47.01	4.176	0.6208	*************
0.00	47.01	4.590	0.6618	
13.64	60.45	5.045	0.7029	*********
0.00	60.45	5.545	0.7439	
6.06	66.42	6.095	0.7850	****
0.00	66.42	6.699	0.8260	
6.06	72.39	7.363	0.8671	****
4.55	76.87	8.093	0.9081	***
0.00	76.87	8.896	0.9492	
1.52	78.36	9.777	0.9902	*
0.00	78.36	10.747	1.0313	
4.55	82.84	11.812	1.0723	***
0.00	82.84	12.983	1.1134	
6.06	88.81	14.270	1.1544	****
0.00	88.81	15.684	1.1955	
0.00	88.81	17.239	1.2365	
1.52	90.30	18.948	1.2776	*
0.00	90.30	20.826	1.3186	
1.52	91.79	22.891	1.3597	*
1.52	93.28	25.160	1.4007	*
1.52	94.78	27.654	1.4418	*
1.52	96.27	30.395	1.4828	*
0.00	96.27	33.408	1.5239	
0.00	96.27	36.720	1.5649	
0.00	96.27	40.360	1.6060	
0.00	96.27	44.361	1.6470	
0.00	96.27	48.758	1.6880	
0.00	96.27	53.592	1.7291	
0.00	96.27	58.904	1.7701	
0.00	96.27	64.743	1.8112	
1.52	97.76	71.161	1.8522	*
0.00	97.76	78.215	1.8933	
1.52	99.25	85.968	1.9343	*

0 1 2 3 4

11:26:01 BUMAX DEADMAN PROJECT GRID 2 03/23/88

##
SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable =	AS P	Unit =	PM			N =	692
Mean =	1.1448	Min =	0.3010	1st Quartile =	0.8451		
Std. Dev. =	0.4698	Max =	2.6693	Median =	1.0414		
CV % =	41.0354	Skewness =	0.6570	3rd Quartile =	1.4624		

Anti-Log Mean = 13.958 Anti-Log Std. Dev. : (−) 4.732
(+) 41.171

%	cum %	antilog	cls int	(# of bins = 36 − bin size = 0.0677)
0.00	0.07	1.850	0.2672	
2.89	2.96	2.162	0.3349	********
0.00	2.96	2.527	0.4025	
0.00	2.96	2.953	0.4702	
3.18	6.13	3.450	0.5379	********
4.34	10.46	4.032	0.6055	***********
0.00	10.46	4.712	0.6732	
6.50	16.96	5.506	0.7409	*****************
7.66	24.60	6.435	0.8085	********************
6.50	31.10	7.519	0.8762	*****************
7.08	38.17	8.787	0.9439	*******************
10.84	48.99	10.269	1.0115	****************************
8.09	57.07	12.000	1.0792	*********************
5.20	62.27	14.023	1.1468	**************
3.61	65.87	16.387	1.2145	*********
2.02	67.89	19.150	1.2822	*****
2.89	70.78	22.379	1.3498	********
2.46	73.23	26.152	1.4175	******
2.17	75.40	30.561	1.4852	******
3.90	79.29	35.714	1.5528	**********
3.18	82.47	41.735	1.6205	********
1.73	84.20	48.772	1.6882	*****
1.73	85.93	56.995	1.7558	*****
3.18	89.11	66.604	1.8235	********
2.31	91.41	77.833	1.8912	******
1.73	93.15	90.956	1.9588	*****
1.16	94.30	106.291	2.0265	***
2.17	96.46	124.211	2.0942	******
0.58	97.04	145.153	2.1618	**
0.43	97.47	169.626	2.2295	*
0.58	98.05	198.225	2.2972	**
0.87	98.92	231.645	2.3648	**
0.29	99.21	270.700	2.4325	*
0.29	99.49	316.340	2.5002	*
0.29	99.78	369.674	2.5678	*
0.00	99.78	432.000	2.6355	
0.14	99.93	504.835	2.7031	

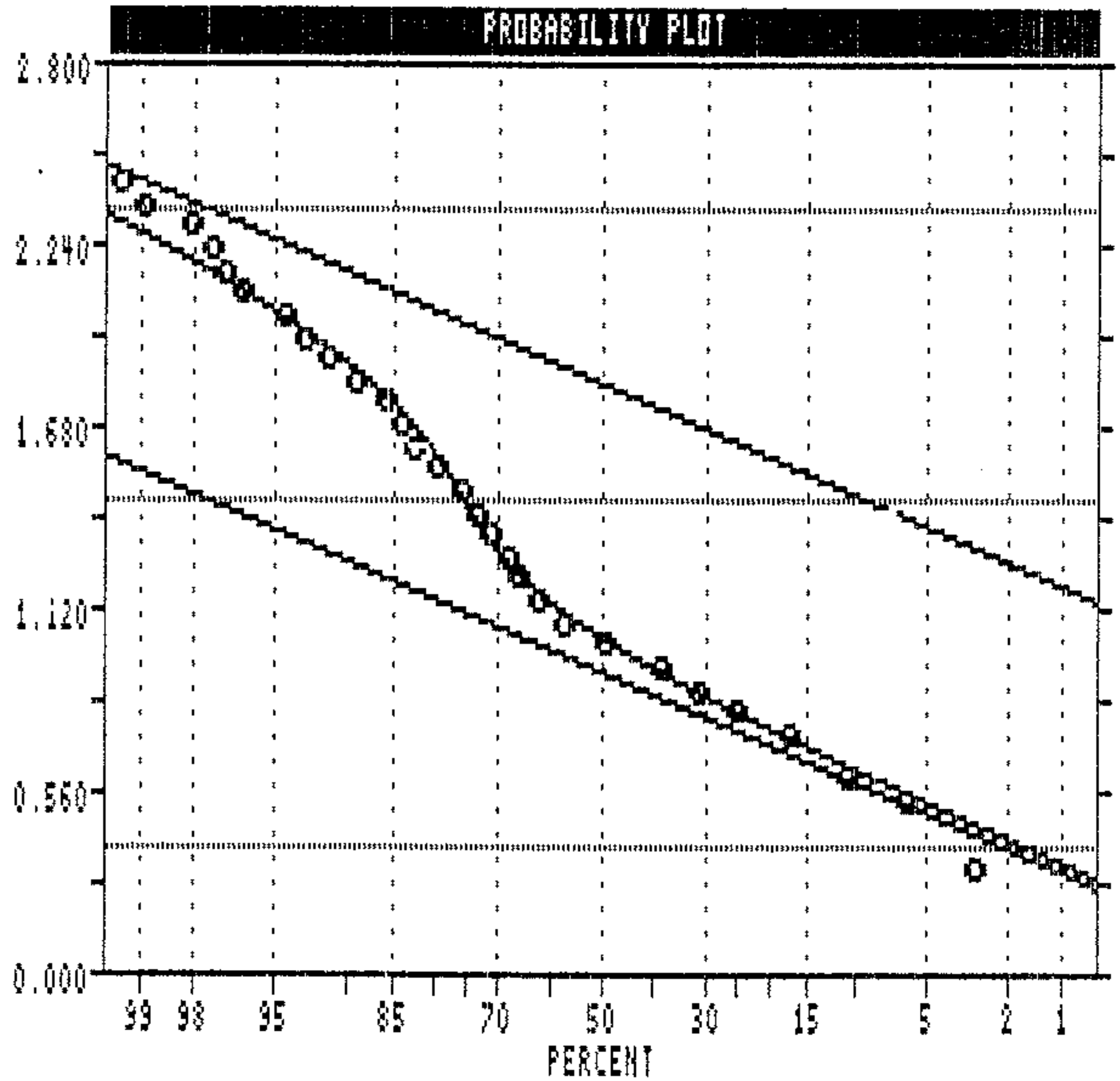
0 1 2 3 4

Each "*" represents approximately 2.6 observations.

##

11:35:42
03/23/88

BUMAX DEADMAN   PROJECT GRID 2



LOGARITHMIC VALUES

VARIABLE = AS P
UNIT = PM
N = 692
N CI = 36

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	0.9149	0.2617	74.3
2	1.8030	0.2682	25.7

THRESHOLDS

2.3395   1.4383
0.3915

CLASS INTERVAL ML
PARAMETER ESTIMATES

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR2PLOT.TXT

Variable = AS P Unit = PM N = 692
N CI = 36

Transform = Logarithmic Number of Populations = 2

# of Missing Observations = 0.

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -2254.600

Parameterized Degrees of Freedom = 3

Population	Mean		Std Dev	Percentage
1	8.220	-	4.500	74.25
		+	15.017	
2	63.540	-	34.263	25.75
		+	117.836	

User Defined Thresholds.

Thresholds
218.524
27.435
2.463

##

##
SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = CU   Unit = PPM   N = 185

Mean =	1.6922	Min =	1.3222	1st Quartile =	1.5993
Std. Dev. =	0.1427	Max =	1.9956	Median =	1.6990
CV % =	8.4327	Skewness =	-0.2459	3rd Quartile =	1.7993

Anti-Log Mean = 49.223   Anti-Log Std. Dev. : (-) 35.438
(+) 68.369

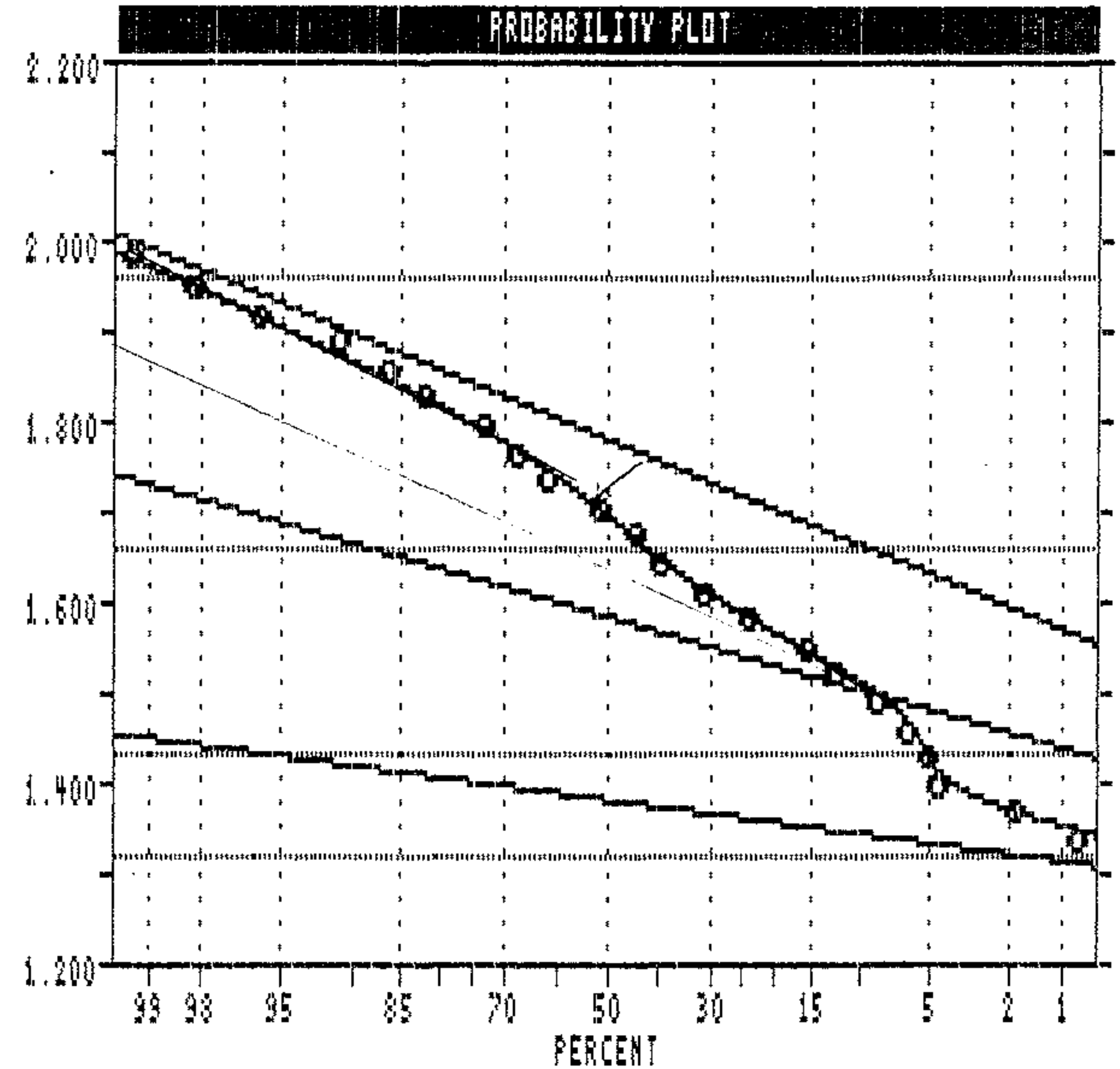
%	cum %	antilog	cls int	(# of bins = 23 - bin size = 0.0306)
0.00	0.27	20.273	1.3069	
0.54	0.81	21.753	1.3375	*
1.08	1.88	23.342	1.3681	*
2.70	4.57	25.046	1.3987	****
0.54	5.11	26.875	1.4294	*
1.08	6.18	28.838	1.4600	*
2.16	8.33	30.944	1.4906	***
3.78	12.10	33.203	1.5212	*****
3.24	15.32	35.628	1.5518	****
8.11	23.39	38.230	1.5824	***********
7.57	30.91	41.022	1.6130	**********
8.11	38.98	44.017	1.6436	***********
4.86	43.82	47.232	1.6742	******
7.03	50.81	50.681	1.7048	*********
10.81	61.56	54.382	1.7355	**************
5.95	67.47	58.353	1.7661	********
5.41	72.85	62.614	1.7967	*******
9.19	81.99	67.186	1.8273	************
4.32	86.29	72.093	1.8579	******
4.86	91.13	77.357	1.8885	******
4.86	95.97	83.006	1.9191	******
2.16	98.12	89.068	1.9497	***
1.08	99.19	95.572	1.9803	*
0.54	99.73	102.551	2.0109	*

0 1 2 3 4

##

15:08:38
03/26/88

BUMAX DEADMAN PROJECT 1987 GRID 3



LOGARITHMIC VALUES

VARIABLE = CU
UNIT = PPM
N = 185
N CI = 23

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	1.3756	0.0296	4.9
2	1.5810	0.0636	34.5
3	1.7759	0.0913	60.6

THRESHOLDS

1.9585 1.6548
1.4295 1.3164

CLASS INTERVAL ML
PARAMETER ESTIMATES

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR3PLOT.TXT

Variable = CU Unit = PPM N = 185
N CI = 23

Transform = Logarithmic Number of Populations = 3

# of Missing Observations = 0.

6 Observations Were Below the Minimum Value of 20.0000
5 Observations Were Above the Maximum Value of 100.0000

==

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -535.688

Parameterized Degrees of Freedom = 5

Population	Mean		Std Dev	Percentage
1	23.744	-	22.180	4.90
		+	25.419	
2	38.109	-	32.921	34.49
		+	44.115	
3	59.688	-	48.373	60.61
		+	73.651	

==

User Defined Thresholds.

Thresholds

90.887
45.165
26.384
20.720

##

##

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = NI   Unit = PPM   N = 183

Mean =	1.5527	Min =	1.0414	1st Quartile =	1.4624
Std. Dev. =	0.1993	Max =	1.9956	Median =	1.5662
CV % =	12.8383	Skewness =	-0.6287	3rd Quartile =	1.6968

Anti-Log Mean = 35.706   Anti-Log Std. Dev. : (-) 22.563
(+) 56.506

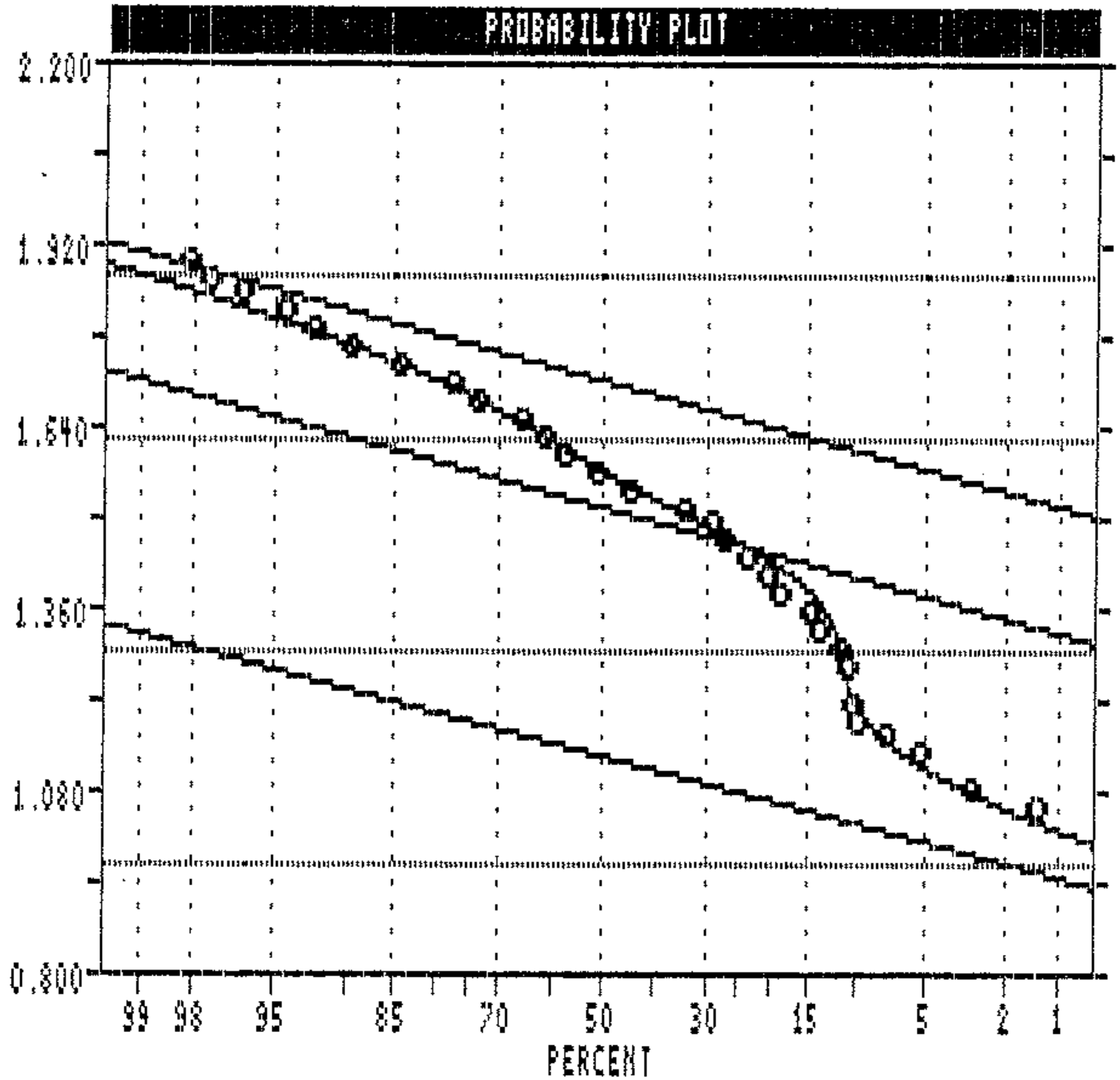
%	cum %	antilog	cls int	(# of bins = 36 - bin size = 0.0273)
0.00	0.27	10.660	1.0278	
1.09	1.36	11.351	1.0550	*
1.64	2.99	12.086	1.0823	**
0.00	2.99	12.869	1.1096	
2.19	5.16	13.703	1.1368	***
2.19	7.34	14.591	1.1641	***
2.19	9.51	15.536	1.1913	***
0.55	10.05	16.543	1.2186	*
0.00	10.05	17.615	1.2459	
0.55	10.60	18.756	1.2731	*
0.55	11.14	19.971	1.3004	*
2.19	13.32	21.265	1.3277	***
1.09	14.40	22.643	1.3549	*
3.83	18.21	24.110	1.3822	*****
1.64	19.84	25.672	1.4095	**
3.28	23.10	27.335	1.4367	****
3.28	26.36	29.106	1.4640	****
2.19	28.53	30.992	1.4912	***
4.92	33.42	33.000	1.5185	******
10.38	43.75	35.138	1.5458	*************
6.56	50.27	37.415	1.5730	********
7.10	57.34	39.839	1.6003	*********
3.83	61.14	42.420	1.6276	*****
4.37	65.49	45.168	1.6548	******
7.65	73.10	48.095	1.6821	**********
3.83	76.90	51.211	1.7094	*****
7.65	84.51	54.529	1.7366	**********
4.92	89.40	58.062	1.7639	******
3.28	92.66	61.824	1.7912	****
1.64	94.29	65.829	1.8184	**
2.19	96.47	70.094	1.8457	***
1.09	97.55	74.636	1.8729	*
0.55	98.10	79.471	1.9002	*
0.00	98.10	84.620	1.9275	
0.00	98.10	90.103	1.9547	
0.00	98.10	95.941	1.9820	
1.64	99.73	102.157	2.0093	**

0 1 2 3 4

##

15:29:24
03/26/88

BUMAX DEADMAN PROJECT 1987 GRID 3



LOGARITHMIC VALUES

VARIABLE = NI
UNIT = PPM
N = 183
N CI = 36

POPULATIONS

Pop.	Mean	Std.Dev.	%
1	1.1225	0.0802	11.1
2	1.5090	0.0842	48.1
3	1.7070	0.0830	40.8

THRESHOLDS

1.8730	1.6140
1.2864	0.9621

CLASS INTERVAL ML
PARAMETER ESTIMATES

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR3PLOT.TXT

Variable = NI Unit = PPM N = 183
N CI = 36

Transform = Logarithmic Number of Populations = 3

# of Missing Observations = 0.

13 Observations Were Below the Minimum Value of 10.0000
0 Observations Were Above the Maximum Value of 100.0000

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -587.921

Parameterized Degrees of Freedom = 5

Population	Mean		Std Dev	Percentage
1	13.260	-	11.023	11.15
		+	15.951	
2	32.288	-	26.597	48.07
		+	39.197	
3	50.933	-	42.073	40.78
		+	61.660	

User Defined Thresholds.

Thresholds
74.645
41.115
19.337
9.164

##

###

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = AS Unit = PPM N = 167

Mean =	1.6802	Min =	1.0414	1st Quartile =	1.4022
Std. Dev. =	0.3375	Max =	2.2625	Median =	1.6812
CV % =	20.0860	Skewness =	-0.0982	3rd Quartile =	1.9590

Anti-Log Mean = 47.883 Anti-Log Std. Dev. : (-) 22.014
(+) 104.152

%	cum %	antilog	cls int	(# of bins = 36 - bin size = 0.0349)
0.00	0.30	10.567	1.0239	
2.40	2.68	11.451	1.0588	***
1.20	3.87	12.409	1.0937	*
2.99	6.85	13.447	1.1286	****
2.40	9.23	14.571	1.1635	***
1.80	11.01	15.790	1.1984	**
0.60	11.61	17.111	1.2333	*
0.60	12.20	18.542	1.2682	*
2.99	15.18	20.093	1.3030	****
1.80	16.96	21.774	1.3379	**
4.19	21.13	23.595	1.3728	*****
3.59	24.70	25.569	1.4077	****
1.80	26.49	27.708	1.4426	**
4.79	31.25	30.025	1.4775	******
2.40	33.63	32.537	1.5124	***
4.19	37.80	35.258	1.5473	*****
5.39	43.15	38.207	1.5821	******
2.40	45.54	41.403	1.6170	***
1.20	46.73	44.866	1.6519	*
3.59	50.30	48.619	1.6868	****
0.60	50.89	52.686	1.7217	*
3.59	54.46	57.093	1.7566	****
4.19	58.63	61.869	1.7915	*****
4.19	62.80	67.044	1.8264	*****
4.19	66.96	72.652	1.8612	*****
2.40	69.35	78.729	1.8961	***
4.19	73.51	85.314	1.9310	*****
1.80	75.30	92.450	1.9659	**
2.40	77.68	100.183	2.0008	***
2.40	80.06	108.563	2.0357	***
2.99	83.04	117.644	2.0706	****
5.99	88.99	127.485	2.1055	*******
2.40	91.37	138.148	2.1403	***
1.80	93.15	149.704	2.1752	**
1.20	94.35	162.226	2.2101	*
1.80	96.13	175.795	2.2450	**
3.59	99.70	190.500	2.2799	****

0 1 2 3 4

###

##

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = A:GR3PLOT.TXT

Variable = AS Unit = PPM N = 176
N CI = 23

Transform = Logarithmic Number of Populations = 3

# of Missing Observations = 0.

17 Observations Were Below the Minimum Value of 10.0000
3 Observations Were Above the Maximum Value of 500.0000

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -530.825

Parameterized Degrees of Freedom = 5

Population	Mean		Std Dev	Percentage
1	12.424	-	10.801	10.88
		+	14.292	
2	28.670	-	20.195	35.87
		+	40.702	
3	90.692	-	55.559	53.25
		+	148.042	

User Defined Thresholds.

Thresholds
241.657
45.909
15.524
9.389

##

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = SB Unit = PPM N = 55

Mean =	0.8599	Min =	0.4771	1st Quartile =	0.6021
Std. Dev. =	0.3112	Max =	1.6902	Median =	0.8451
CV % =	36.1968	Skewness =	0.7934	3rd Quartile =	1.0414

Anti-Log Mean = 7.242 Anti-Log Std. Dev. : (-) 3.537
(+) 14.829

%	cum %	antilog	cls int	(# of bins = 18 - bin size = 0.0714)
0.00	0.89	2.763	0.4414	
14.55	15.18	3.257	0.5128	********
0.00	15.18	3.838	0.5842	
21.82	36.61	4.524	0.6555	************
1.82	38.39	5.332	0.7269	*
7.27	45.54	6.284	0.7982	****
10.91	56.25	7.406	0.8696	******
9.09	65.18	8.729	0.9409	*****
7.27	72.32	10.287	1.0123	****
9.09	81.25	12.124	1.0837	*****
3.64	84.82	14.289	1.1550	**
1.82	86.61	16.841	1.2264	*
1.82	88.39	19.849	1.2977	*
1.82	90.18	23.393	1.3691	*
3.64	93.75	27.571	1.4404	**
0.00	93.75	32.494	1.5118	
1.82	95.54	38.297	1.5832	*
1.82	97.32	45.135	1.6545	*
1.82	99.11	53.195	1.7259	*

0 1 2 3 4

##