ARIS SUMMARY SHEET

District Geologist, Kamloops — Off Confidential: 89.04.22

ASSESSMENT REPORT 17328 — MINING DIVISION: Kamloops

PROPERTY: Foghorn
LOCATION: LAT 51 31 54 LONG 119 57 39
UTM 11 5712888 294636
NTS 082M12W
CLAIM(S): Foghorn 1-5
OPERATOR(S): Gold Spring Res.
AUTHOR(S): Christopher, P.A.
REPORT YEAR: 1988, 46 Pages
COMMODITIES
SEARCHED FOR: Copper,Lead,Zinc,Silver,Gold
GEOLOGICAL
SUMMARY: The property is situated near the boundary of the Intermontane and Omineca Tectonic belts. The region is mainly underlain by a metamorphosed assemblage of sedimentary and volcanic rocks that range in age from Devonian through Permian age. Devonian-Permian Fennell Formation rocks are mainly mafic volcanics and related sedimentary rocks. Devonian-Mississippian Eagle Bay Formation rocks represent an Island Arc assemblage. Pyrite, chalcopyrite and pyrrhotite occur as massive to semi-massive layers in schists while argentiferous galena, sphalerite, chalcopyrite and pyrite occur in quartz veins.

\ _.K
DONE: Geochemical,Geophysical,Physical
EMGR 60.0 km;VLF
Map(s) - 4; Scale(s) - 1:5000
LINE 60.0 km
MAGG 60.0 km
Map(s) - 4; Scale(s) - 1:5000
ROCK 12 sample(s) ;ME
SOIL 510 sample(s) ;ME
Map(s) - 10; Scale(s) - 1:5000
MINFILE: 082M 029,082M 040,082M 108

GEOCHEMICAL, GEOLOGICAL AND GEOPHYSICAL REPORT ON THE FOGHORN MOUNTAIN PROPERTY

KAMLOOPS MINING DIVISION,
BIRCH ISLAND AREA, BRITISH COLUMBIA

LOCATION:

N.T.S.: 82-M-12W; 92-P-9E
LATITUDE: 51°32'N.
LONGITUDE: 119°54'W.

CLAIMS:

FOGHORN 1 TO 5 (# 7014 TO 7018)
FOGHORN 6 (# 7305)

REPORT FOR:

GOLD SPRING RESOURCES LTD.
300 - 800 WEST PENDER STREET
VANCOUVER, B.C. V6C 2V8

PREPARED BY:

Peter A. Christopher Ph.D., P.Eng.
PETER CHRISTOPHER AND ASSOCIATES INC.
3707 WEST 34TH AVENUE,
VANCOUVER, B.C. V6N 2K9

April 12, 1988

TABLE OF CONTENTS

LIST OF TABLES

LIST OF ILLUSTRATIONS

SUMMARY

The Foghorn Mountain Property, consisting of six metric claims totaling 108 units, covers about 2700 hectares in the Adams Plateau and Kamloops Mining Division about 100 kilometer north-northeast of Kamloops, British Columbia. Four wheel drive road access exists to the property from Birch Island. The area of interest is at about 1675 meters in a plateau between Foghorn Mountain and Granite Mountain.

The property is underlain by metamorphic rocks of the Eagle Bay and Fennell formations which host several mineral deposits under active exploration. The Foghorn Mountain Property covers several British Columbia Government mineral inventory occurrence with work on the Foghorn and Lydia starting about the turn of the century. The original Foghorn Showings are quartz veins with pods and lenses of nearly massive galena, sphalerite, pyrite and chalcopyrite from which about 75 tons shipped in 1916 had a net smelter return of about $3,500. The Lydia showing, a stratabound copper showing was explored prior to 1918 by over 900 feet of underground workings in two adit levels with the first 100 feet of the upper level reported to contain disseminated pyrite and chalcopyrite.

Exploration programs over the last 30 years by Rexspar Uranium and Metals Co. (1958), Anaconda (1967), Royal Canadian Ventures (1968-1969), Imperial Oil (1969-1970), Fennell Family (1970-1974), Noranda Exploration Co. (1972), Barrier Reef Resources (1979-1981), Craigmont Mines (1979-1982), Esso Resources (1982-1984) and Gold Spring Resources (1987) has consisted of geological, soil geochemical, airborne and ground magnetic survey, trenching and over 3,700 meters of diamond drilling. Previous exploration has mainly concentrated on the areas of the original Foghorn and Lydia showings with a number of additional, relatively untested conductors (A, B, C Figure G8) and soil geochemical anomalies (B and C in West Grid Area). Three AQ holes drilling in anomaly B by Craigmont Mines encouraged Esso to drill two NQ holes in order to obtain better core recovery. Esso's holes intersect an 8 meter wide mineralized zone which contained:

Hole 84-2	73.2-75.9m. (8.85')	@ 9.2% Pb, 1.56% Zn, 2.74 oz/t Ag
Hole 84-3	60.6-62.4m. (5.9')	@ 2.89% Pb, 0.45% Zn, 0.76 oz/t Ag.

Gold in soils up to 287 ppb obtained by Esso from the Foghorn 1 claim, up to 126 ppb obtained by Gold Spring from the Foghorn 4 claim and up to 650 ppb reported by Ostensoe (1985, A.R. 14054) from the Foghorn 6 claim provide justification for further analytical testing for gold.

The writer has outlined a success contingent, staged exploration program for further evaluation of the Foghorn Mountain Property. A recommended Stage I program of detailed geological mapping, geochemical follow-up, trenching and 1,000 feet (500 meters) of diamond drilling is recommended at an estimated cost of $ 95,000. Success contingent Stage II an Stage III, mainly drilling programs are estimated to cost $ 195,600 each.

INTRODUCTION

The Foghorn Mountain Property covers about 2700 hectares in the Kamloops Mining Division and Adams Plateau of southwestern-central British Columbia. The property was acquired by Gold Springs Resources Ltd. to further test the precious and base metal potential of multi element geochemical anomalies associated with several known mineral occurrences. The writer was retained by the management of Gold Springs Resources Ltd. to confirm the property location, evaluate the geological setting and recommend a program for further exploration of the property, if warranted. An extensive file of assessment reports and government reports covering nearly continuous exploration of the property over the past twenty years was reviewed to provide background for preparation of this report.

The writer examined and sampled the Foghorn Mountain Property on August 23, 1987 with Brent Jardine and property staker, Mr. Randy Hogg. This report outlines a success contingent, staged exploration program for further evaluation of the precious and base metal potential of the Foghorn Mountain Property.

LOCATION AND ACCESS (Figures 1 and 2)

The Foghorn Mountain Property is situated in the Adams Plateau and Kamloops Mining Division of south-central British Columbia about 100 kilometers north of Kamloops, British Columbia. The claims are in and the headwater area of Foghorn Creek between about 10 kilometers east of the North Thompson River and 6 kilometers and 11 kilometers southerly from Birch Island and Clearwater, respectively. The property covers Foghorn Mountain and the northern flank of Granite Mountain. The claims are centered at about geographic coordinates 51° 32'N latitude and 119° 54'W longitude in N.T.S. map sheets 82-M-12W and 92-P-9E.

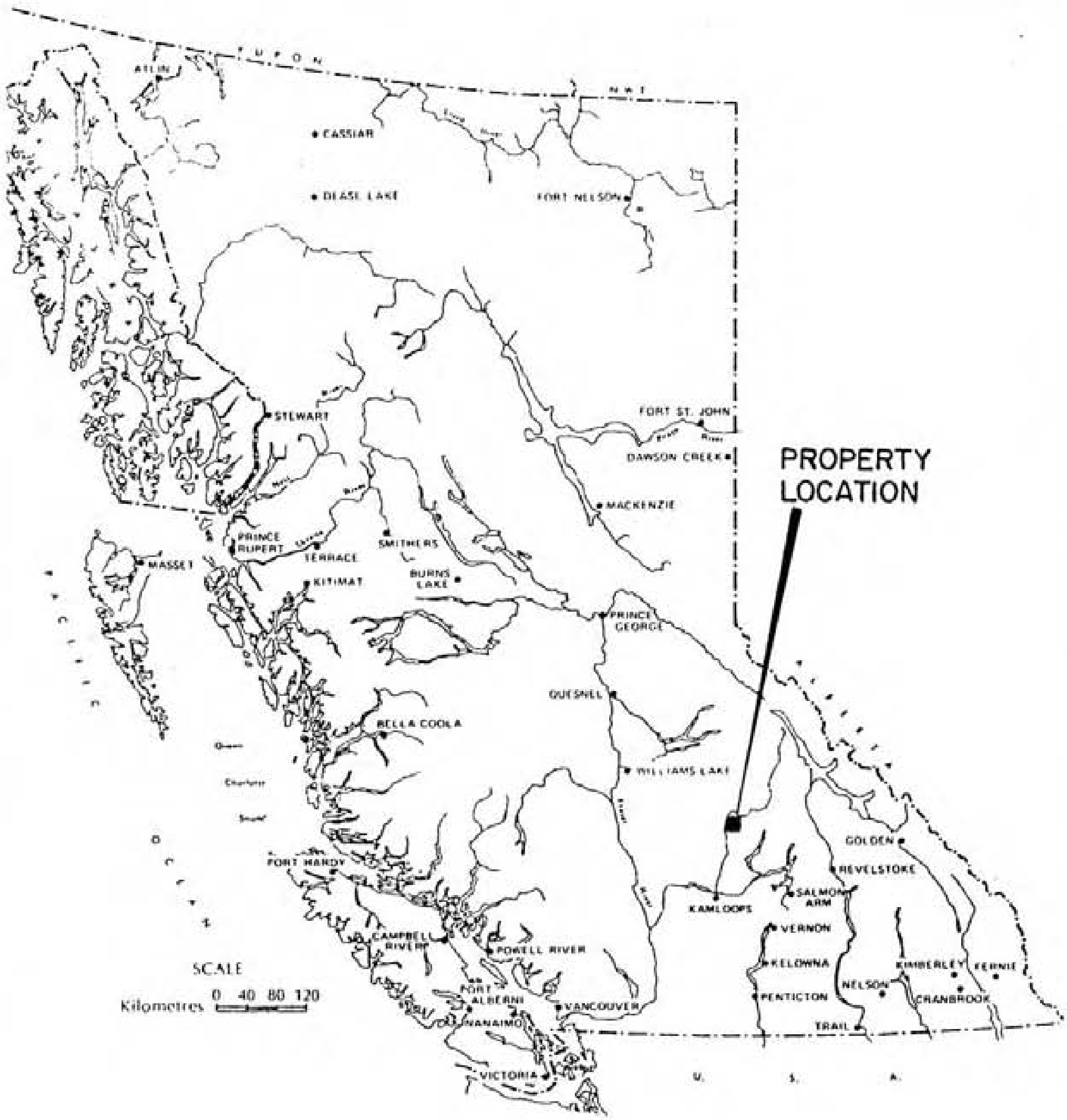
Access to the property is by four wheel drive vehicle via the Rexspar Property access road or via the Jones Creek logging road about 20 road kilometers from Birch Island.

TOPOGRAPHY AND VEGETATION

The Foghorn Mountain Property covers Foghorn Mountain and part of a northerly trending ridge lying between Foghorn Creek and Lute Creek. The southern part of the property is drained by Joseph Creek and the northwest part by McDougal Creek.

The area is part of the Shuswap Highland physiographic subdivision of the Interior System of British Columbia. Elevations range from about 6500 feet (1981 meters) on Foghorn Mountain to under 4000 feet (1220 meters) in Foghorn Creek with current exploration areas at elevations near 5,500 feet (1676 meters).

The lower parts of Foghorn Creek valley contain commercial stands of spruce, fir and cedar. The area around Foghorn Mountain and southern part of the property contain mainly alpine meadows with some alpine spruce and fir. Creeks occupy wide swampy valleys.



PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher

GOLD SPRING RESOURCES LTD.

FOGHORN PROPERTY

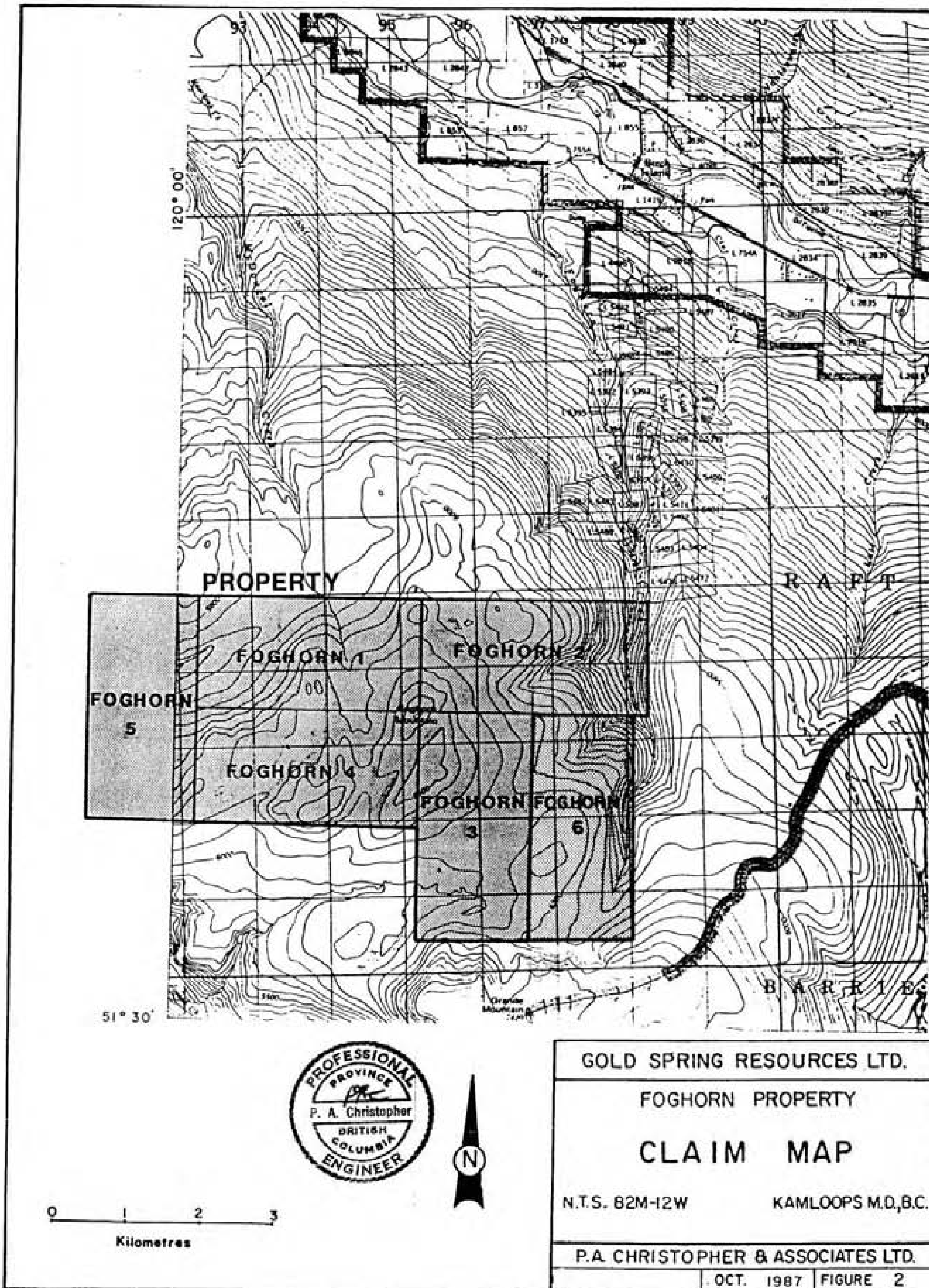
LOCATION MAP

N.T.S. 82M-12W KAMLOOPS M.D., B.C.

P.A. CHRISTOPHER & ASSOCIATES LTD.

OCT. 1987 FIGURE 1

CHONG



GOLD SPRING RESOURCES LTD.

FOGHORN PROPERTY

CLAIM MAP

N.T.S. 82M-12W KAMLOOPS M.D., B.C.

P.A. CHRISTOPHER & ASSOCIATES LTD.

OCT. 1987 FIGURE 2

CHONG

PROPERTY DEFINITION

The Foghorn Property, consisting of 6 metric claims totalling 108 units covers about 2700 hectares in the Kamloops Mining Division, British Columbia. The Foghorn 1 through 5 claims were staked by Randy Hogg of Kamloops, British Columbia between March 15 and March 17, 1987 and the Foghorn 6 claim was staked by Randy Hogg for Brera Holdings Ltd. on September 16, 1987. The claims were recorded on April 23, 1987 and October 15, 1987 within the 30 day period allowed for recording. The writer examined the common legal corner post for Foghorn 1 through 4 during a field examination of the property on August 23, 1987. The claim lines were well marked and the legal corner post for the Foghorn 1 through 4 claims correctly located in the field and on the government claim map.

Pertinent claim data for the Foghorn Property is shown in Table 1 with approximate claim locations shown on Figure 2.

TABLE 1. Pertinent Claim Data - Foghorn Property.

Claim	Record #	Units/Shape	Record Date	Expiry*	Staker
Foghorn 1	7014(4)	18/3Nx6W	April 23/87	1988	Randy Hogg
Foghorn 2	7015(4)	18/3Nx6E	April 23/87	1988	Randy Hogg
Foghorn 3	7016(4)	18/6Sx3E	April 23/87	1988	Randy Hogg
Foghorn 4	7017(4)	18/3Sx6W	April 23/87	1988	Randy Hogg
Foghorn 5	7018(4)	18/6Nx3W	April 23/87	1988	Randy Hogg
Foghorn 6	7305(10)	18/6Sx3E	Oct. 15/87	1988	Randy Hogg
	Total Units	108			

* Before recording 1987 work program.

HISTORY

The old Foghorn showings (MI 82M-29) were discovered in the early 1900's by George Fennell of Barriere, British Columbia with the showings held by the Fennell family almost continuously up to 1976. Work on the Foghorn property was first reported in the 1913 Annual Report of the Minister of Mines with reports of a crosscut tunnel being driven to intersect the downward projection of four narrow galena bearing quartz veins.

In 1915 development work consisted of 200 foot adit, a 40 foot vertical shaft with a 40 foot drift at the bottom, and two surface cuts on veins. Three main veins were reported to be 6-12 inches wide on surface and to carry almost solid galena. Veins exposed at the bottom of the shaft contained more sphalerite, pyrite and chalcopyrite with a representative vein sample reported to contain: trace gold, 16 oz Ag/ton, 16.7 % lead, 6.6% copper, 16.5% zinc and 17.5% iron.

In 1916, 2 carloads of ore, approximately 75 tons, brought a net smelter return of about $ 3,500. A third carload was reported by Singhai (1974) to have lost money and shipments were discontinued. The Foghorn showing remained idle till 1935 when George Fennell conducted further trenching and pitting.

Several vein-type showings referred to as the Chidgrin (MI 82M-040) were discovered in 1924 about 0.6 km north of the Foghorn showings. The veins have been explored by a number of deep trenches.

The area east of the Foghorn showings (Figure 5) has also received considerable attention with the Lydia stratiform copper showing (MI 82M-8) first worked in about 1913 with over 900 feet of drifting and crosscutting completed in two levels by 1918. The area of the Lydia showing has been explored by Anaconda, Royal Canadian Ventures Ltd., Imperial Oil Enterprises Ltd., Noranda and Barrier Reef Resources Ltd. during the past 20 years.

In 1968 and 1969 (Vollo, 1968a, 1968b, 1969) Royal Canadian Ventures Ltd. conducted geological, magnetic, electromagnetic, and soil geochemical surveys and constructed three bulldozer trenches totalling 700 feet in the area of the old Lydia showings. Imperial Oil is reported to have conduced 1,002 feet of surface and 1,560 feet of underground diamond drilling in 1970. In 1972 Noranda Exploration Company, Ltd. explored part of the property with soil, magnetic and geological surveys and drilled 5 holes totalling 2,294 feet.

The Shamrock (MI 82M-30) or FH prospect is situated north of the Lydia and covered ground between the Lydia and Foghorn showings. The 1917 Report of the Minister of Mines reported drifting on a 123 foot adit with considerable work on adjacent claims. The 1924 Report of the Minister of Mines states that, "considerable tunneling was done on the property in developing a quartz ledge which has a north-and-south strike conforming with the prevailing schist."

In 1958 the Foghorn Property was optioned to Rexspar Uranium and Metals Co. with access roads constructed from the Rexspar uranium deposit. Radiometric, self-potential, electromagnetic and geochemical surveys were conducted over the area of the old lead zinc showings with bulldozer trenching of the best anomalies.

A section of the property referred to as the Gopher (MI 82M-108) showing was explored with a 140 foot diamond drill hole by Barriere Explorations Ltd. in 1970 with trenching and geological investigations carried out by the Fennell family in 1974.

Following discovery of the CC massive sulphide-copper-zinc bearing deposit at Chu Chua by Craigmont Mines Ltd, Barrier Reef Resources Ltd. and Craigmont Mines Ltd. acquired land position in the Foghorn Mountain area. Exploration in 1979 with Dighem II airborne electromagnetic, resistivity and magnetic surveys was conducted by both Craigmont Mines Ltd. and Barrier Reef Resources Limited. The surveys indicated several conductive bands with strong electromagnetic response.

In October 1979 Craigmont optioned some of the Barrier Reef ground and drilled 4 AQ holes totalling 361 meters. The holes tested the strongest airborne electromagnetic conductor. The holes intersected chloritic and pyritic rhyolite of the Fennell Formation with small amounts of galena and sphalerite (see Figures 6a & 6b for Craigmont's drill hole locations).

In August-September, 1980 Craigmont drilled a further 7 holes totalling 646 meters to test altered graphitic tuffs associated with lead-zinc-copper soil geochemical anomalies and EM conductors in the eastern part of the present Foghorn 4 claim (then Foggy 2 and Foggy 3 Claims). The holes intersected weak lead-zinc-silver-gold mineralization with hole FH6 containing 4.1 meters grading 0.1% Cu, 0.15% Pb, 0.15% Zn and 0.48ppm Au. Holes JC-1 to 3, totalling 175 meters, were drilled to test a strong coincident EM Conductor and Pb, Zn, Cu soil geochemical anomaly in the western part of the present Foghorn 4 claim (Figure 6b). They intersected graphitic tuffite and erratic Pb, Cu, Ag, Au mineralization with hole JC-1 contained 0.87 ppm gold in a sludge sample and hole JC-2 contained 3.3 meters grading 0.27% Cu, 3.06% Pb, 0.53 ppm Au and 58.0 ppm Ag (the adjacent 1.7 meters section of core was not recovered).

In 1981 Craigmont drilled an additional 9 holes totaling over 600 meters and intersected thick sections of pyritic cherty tuffite and graphitic tuffite with traces of lead, zinc and copper mineralization. The drilling was conducted in the area of the present Foghorn 4 claim.

In 1982 Esso Resources Canada Limited consolidated the Foghorn Mountain area with options including the Foghorn Property of Barrier Reef Resources Ltd. and the Joseph Claims of Craigmont Mines Ltd. 1982. Esso's 1983 program consisted of road building, grid construction, 1305 soil samples analyzed for Cu, Pb, Zn, Ag, Au, 76.6 km of HLEM (Genie) and 68.9 km of proton magnetometer surveying. Soil geochemical anomalies and electromagnetic conductors, coincident with black graphitic argillites and pyritic mafic to felsic volcanic rocks of the Fennel Formation, were located.

In 1983 Esso completed 3 BQ holes (Figure 6b) totalling 401.5 meters in the central part of the present Foghorn 6 claim. Holes BBC 83-2 and 83-3 intersected semi-massive pyrite with minor base and precious metal values (Marr and Everett, 1984). In August 1984, Esso drilled two NQ holes totalling 173.7 meters in the western part of the present Foghorn 4 (then Joseph 9) claim to test down dip form Craigmont's hole JC-2 (3.3 meters of 3.06% Pb, 0.25% Zn, 0.27% Cu, 0.53 ppm Au and 58 ppm Ag). Esso's Hole 84-2 contained an interval from 73.2 to 75.9 meters grading 9.2% Pb, 1.56% Zn, and 2.74 oz/ton Ag and Hole 84-3 contained an interval from 60.6-62.4 meters grading 2.89% Pb, 0.45% Zn and 0.76 oz/ton Ag. The mineralization was reported to occur in baritic galena-pyrite-sphalerite veins in stratabound zone of quartz and carbonate.

In 1987 claims covering the Foghorn Mountain Property were allowed to lapse and the Foghorn 1 to 5 claims were staked in March of 1987 by Randy Hogg. In September of 1987, claims covering the old Lydia showing lapsed and the Foghorn 6 claim was staked. The property was acquired by Gold Spring Resources Ltd. to further test extensions of previous explored anomalous zones for precious metal enhanced vein or massive sulphide deposits. During August and September of 1987 fill-in soil geochemical, VLF-Em and magnetic surveys were conducted for Gold Spring Resources Ltd. by Renegade Mineral Exploration Services Ltd. The writer examined the Foghorn Property on August 23, 1987.

1987 WORK PROGRAM

The 1987 field program was conducted by personnel contracted from Renegade Mineral Exploration Services Ltd. with property exploration conducted between August 1, 1987 and October 31, 1987. The program consisted of constructing 4.2 kilometers of baseline and 60 kilometers of cross lines with flagged stations placed at 25 meter intervals and lines spaced at 50 or 100 meter intervals. Geometrics total field magnetometer (Proton Procession) coupled with an automatic recording base station and Geonics VLF-EM 16 readings were collected over the entire grid area. Geophysical data was computer plotted with the results interpreted by Ed Rockel of Interpretex Resources Ltd. Rockel's interpretation and Figures G1 to G8 are presented as Appendix A to this report.

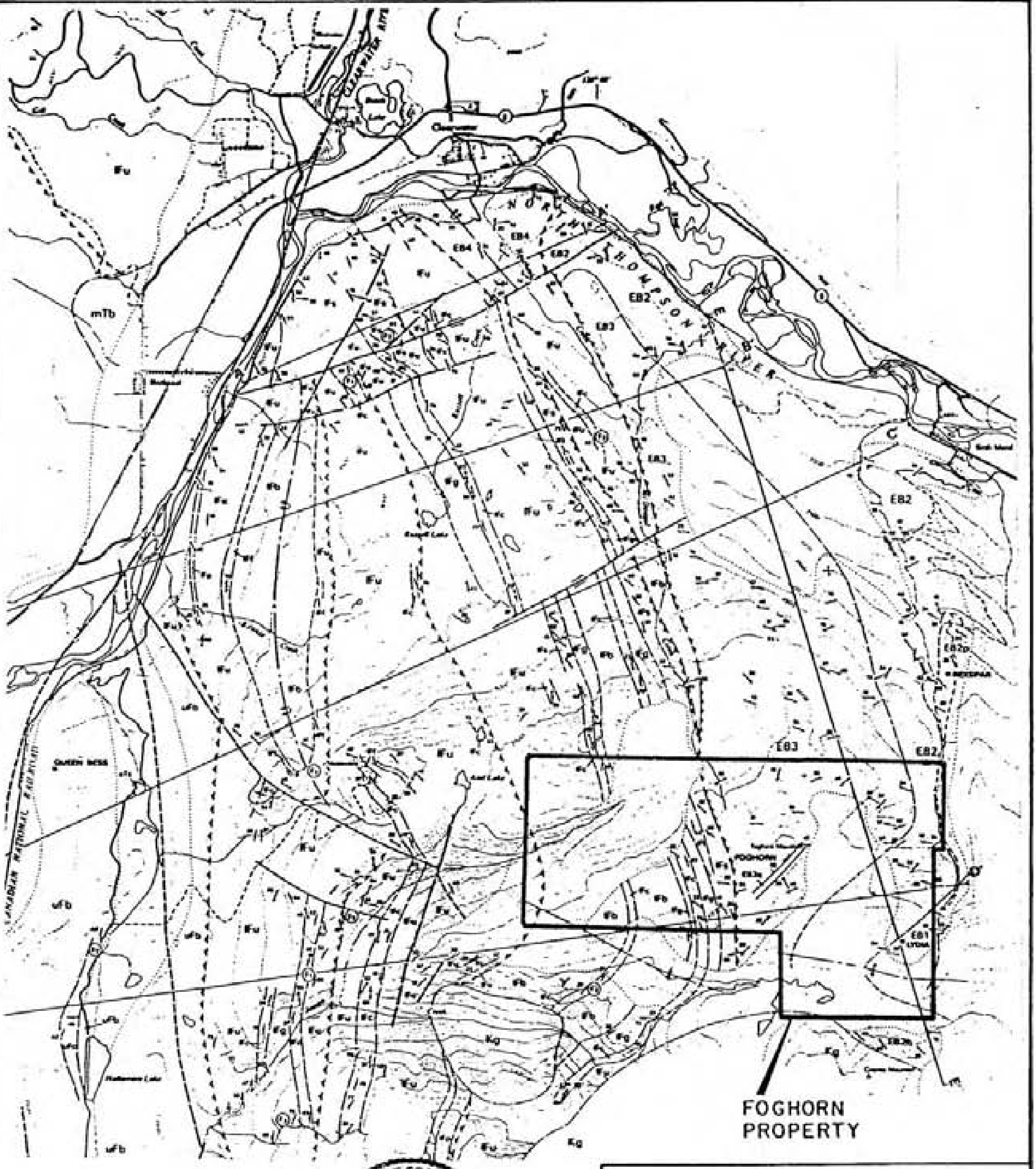
VLF-EM data is presented on plans as profiles and contoured Fraser Filtered with original assessment maps, at a scale of 1:50,000, presented as Figures G1 to G4. Magnetic values were corrected for drift with final magnetic values computer plotted, contoured at a 1:50,000 scale for summary presentation as Figures G5 and G6. Geophysical interpretation maps for the east and west grid areas are presented as Figures G7 and G8, respectively.

Soil samples were selectively taken over the grid area to extend and fill-in previous coverage in the grid areas by Esso Resources Canada Limited (Everett and Cooper, 1983a). A total of 510 soil samples were collected and submitted to Acme Analytical Laboratories for 30 Element ICP with 75 samples, containing anomalous base metals or silver, selected for gold analysis by atomic absorption. The writer collected 5 rock samples from the old Foghorn workings to check precious metal content of the showing. Contract crews submitted one additional sample from the Foghorn Shaft, three samples of Esso Resources drill hole 83-1 and six selected character samples to evaluate the ratio of base to precious metals. Geochemical values for the 1987 program are shown on Figures 6a to 10b with certificates of analysis presented as Appendix B. A cost statement for the 1987 exploration program is presented as Appendix C.

REGIONAL GEOLOGY (FIGURE 3 & 4)

The geology of the Foghorn Property and surrounding area has been mapped in detail by the B.C. Ministry of Energy Mines and Petroleum Resources with Figure 3 after Preliminary Map 53 and Geological Fieldwork 1982 (Schiarizza, 1982 a & b). The regional geology has been mapped by Campbell (1963), Preto et al. (1980), Preto (1979, 1981) and Okulitch (1979).

The area is referred to as the Adams Plateau and is situated near the boundary of the Intermontane and Omineca Crystalline Tectonic Belts. The region is mainly underlain by a metamorphosed assemblage of sedimentary and volcanic rocks that range in age from Devonian through Permian age. The Fennell Rocks are mainly basic volcanics and related sediments that represent an imbricated oceanic terrane thrust into its present position. The Eagle Bay Formation appears to represent the metamorphosed product of an island arc volcano -sedimentary environment. The Fennel and Eagle Bay formations are in fault contact.



PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher

0 1 2 3 4 Kilometres

Scale 1:100,000

GOLD SPRING RESOURCES LTD.		
FOGHORN PROPERTY		
REGIONAL GEOLOGY		
N.T.S. 82M-12W		KAMLOOPS M.D., B.C.
P.A. CHRISTOPHER & ASSOCIATES LTD.		
	OCT. 1987	FIGURE 3

CHONG

PRELIMINARY MAP NO. 53

GEOLOGY OF THE BARRIÈRE RIVER - CLEARWATER AREA

N.T.S. 82M/4, 5, 12; 92P/1, 8, 9

GEOLOGY BY PAUL SCHIARIZZA, 1978 - 1981, WITH ADDITIONAL DATA FROM B.C. MINISTRY OF ENERGY, MINES AND PETROLEUM RESOURCES MAPPING BY V. A. PRETO, G. P. McLAREN, AND L. J. DIAKOW 1975 - 1979
CONODONT IDENTIFICATIONS BY M. J. ORCHARD, GEOLOGICAL SURVEY OF CANADA, VANCOUVER
RADIOMETRIC DATING BY R. L. ARMSTRONG AND ... UNIVERSITY OF BRITISH COLUMBIA
CARTOGRAPHY BY [illegible]

LEGEND

MIOCENE AND/OR YOUNGER

mTb OLIVINE BASALT

EOCENE

KAMLOOPS GROUP

eTs SKULL HILL FORMATION: VESICULAR AND AMYGDALOIDAL ANDESITE

eTc CHU CHUA FORMATION: SANDSTONE, SHALE, CONGLOMERATE, MINOR AMOUNTS OF COAL

CRETACEOUS

BALDY BATHOLITH, RAFT BATHOLITH, AND RELATED ROCKS

Kg (±HORNBLENDE-) BIOTITE GRANITE AND GRANODIORITE

DEVONIAN TO PERMIAN

ALLOCHTHONOUS, INTERNALLY IMBRICATED OCEANIC TERRANE

FENNELL FORMATION

UPPER STRUCTURAL DIVISION

uFb GREY AND GREEN PILLOWED AND MASSIVE METABASALT; MINOR AMOUNTS OF BASALTIC BRECCIA AND TUFF, DIABASE, GABBRO, AND CHERT

uFc GREY AND GREEN BEDDED CHERT

LOWER STRUCTURAL DIVISION

lFb GREY AND GREEN MASSIVE AND PILLOWED METABASALT; MINOR AMOUNTS OF BASALTIC BRECCIA AND TUFF

lFc GREY AND GREEN BEDDED CHERT, CHERTY ARGILLITE, SLATE, AND PHYLLITE

lFg GABBRO, DIORITE, DIABASE

lFp LIGHT TO MEDIUM GREY QUARTZ-FELDSPAR PORPHYRY

lFs LIGHT TO DARK GREY SANDSTONE, SILTSTONE, SLATE, PHYLLITE, AND QUARTZITE; SOME CHERT; IN PLACES INCLUDES GREY TO GREEN QUARTZOSE AND/OR FELDSPATHIC PHYLLITE (METATUFF)

lFl LIMESTONE, MARBLE

lFf INTRAFORMATIONAL CONGLOMERATE - CLASTS DERIVED EXCLUSIVELY FROM FENNELL FORMATION LITHOLOGIES

lFu UNDIVIDED; MAINLY lFc, lFg AND lFb, BUT MAY INCLUDE ANY OR ALL OF ABOVE ROCK TYPES

MISSISSIPPIAN AND OLDER (?)

PARAUTOCHTHONOUS TERRANE

EAGLE BAY FORMATION

EB4 DARK GREY SLATE AND PHYLLITE WITH INTERBEDDED SILTSTONE, SANDSTONE, AND GRIT; LESSER CONGLOMERATE, LIMESTONE, METATUFF, AND METAVOLCANIC BRECCIA; EB4l: LIMESTONE; EB4v: METAVOLCANIC BRECCIA AND TUFF

EB3 LIGHT GREY, RUSTY WEATHERING FELDSPATHIC PHYLLITE (LARGELY METATUFF) AND PHYLLITIC VOLCANIC BRECCIA, EB3q: LIGHT GREY MASSIVE "CHERTY QUARTZITE" (SILICEOUS EXHALITE?)

EB2 LIGHT SILVER GREY QUARTZ PHYLLITE AND MUSCOVITE-QUARTZ SCHIST (DERIVED LARGELY FROM ACID VOLCANIC ROCKS), SOME DARK GREY PHYLLITE, GREEN CHLORITIC PHYLLITE, AND SCHISTOSE VOLCANIC BRECCIA; EB2f: FELDSPAR PORPHYRY, FELDSPATHIC SCHIST, PYRITIC SERICITE-QUARTZ SCHIST, METAVOLCANIC BRECCIA; EB2h: EQUIVALENT(?) ROCKS ADJACENT TO BALDY BATHOLITH - BIOTITE-PLAGIOCLASE-QUARTZ SCHIST AND GNEISS, BIOTITE-QUARTZ HORNFELS, AMPHIBOLITE

EB1 MEDIUM TO DARK GREEN CHLORITIC PHYLLITE, SCHIST, AND SCHISTOSE VOLCANIC BRECCIA; LESSER LIMESTONE, DOLOSTONE, QUARTZITE, PHYLLITE, AND MINOR AMOUNTS OF CONGLOMERATE; EB1l: MASSIVE WHITE FINELY CRYSTALLINE LIMESTONE; EB1q: LIGHT GREY TO WHITE QUARTZITE

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher

GOLD SPRING RESOURCES LTD.

FOGHORN PROPERTY

LEGEND FOR REGIONAL GEOLOGY

N.T.S. 82M-12W | KAMLOOPS M.D, B.C.

P.A. CHRISTOPHER & ASSOCIATES LTD.

OCT. 1987 | FIGURE 4

CHONG

The Cretaceous Baldy Batholith was emplaced along the southern boundary of the Foghorn Property. A satellite granitic stock with about a 2 km diameter outcrop in the Joseph Creek valley occurs northwest of the main batholith.

Conglomerate, sandstone and shale of the Eocene Chu Chua Formation and overlying vesicular andesite of the Skull Hill Formation overlie the Fennell Formation north of Dunn Lake with a small exposure of the Skull Hill Formation about 6 km west of the Foghorn property.

Structurally rocks units have a northwesterly trend and have been affected by four phases of deformation (Preto, 1979). Schiarizza (1982 a & b) defined three periods of folding in the Foghorn Mountain area with early folds generally plunging northwest, second phase folds plunging northwest or southeast and third phase folds plunging at low angles east or westward. An overturned, phase 1 syncline in the Lower Fennell Formation is the dominate structure on the west flank of Foghorn Mountain with Eagle Bay Formation on Foghorn Mountain forming a relatively flat plate to gentle northerly plunging synform.

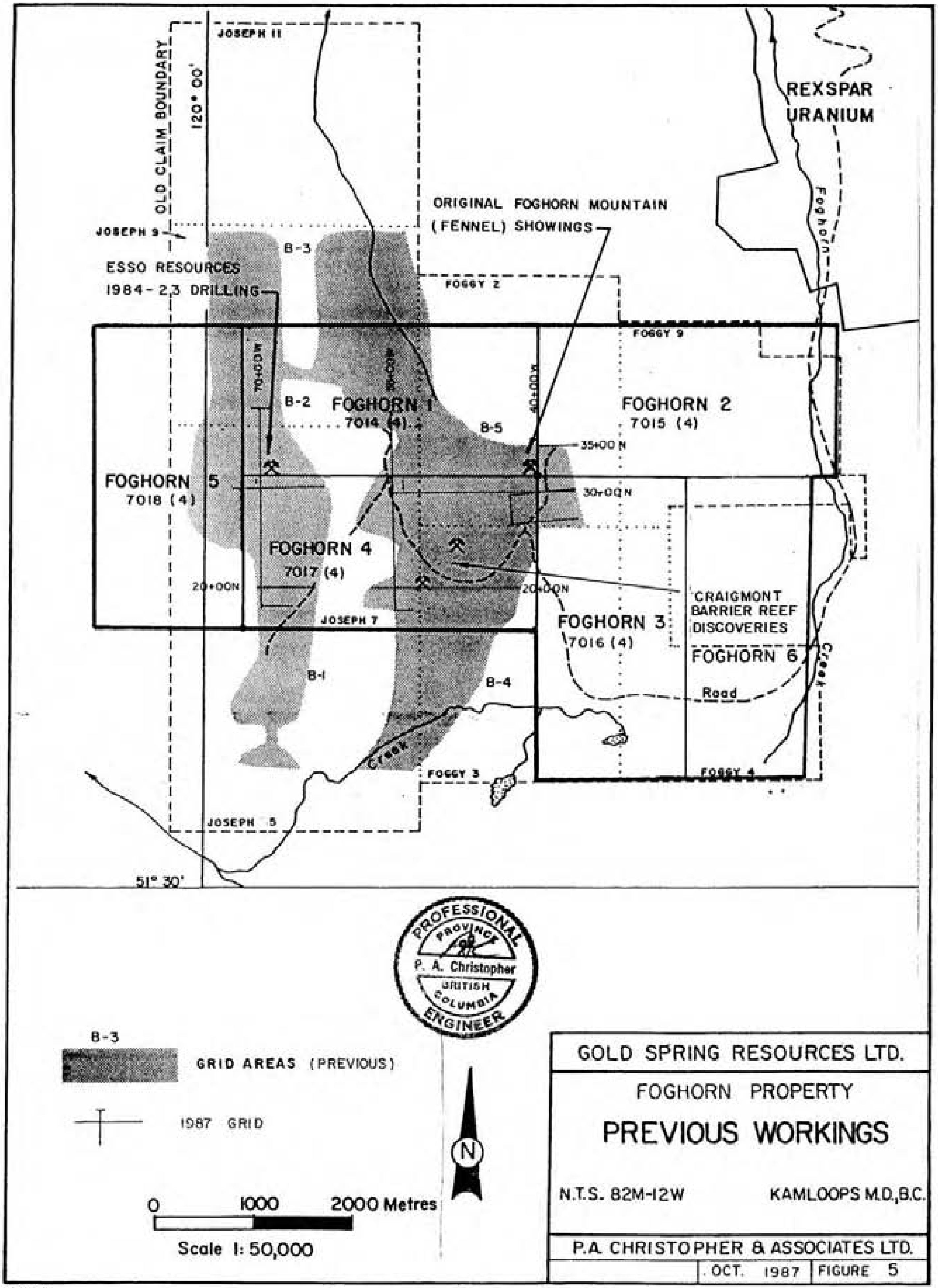
Two main fault direction are apparent with northerly trending late faults forming breccia zones and occupying main drainages and northeast-trending faults inferred on the basis of abrupt truncation of stratigraphic units to be late features (Schiarizza, 1982a).

MINERALIZATION (Figures 6a & 6b)

The Foghorn Mountain prospects have experienced several episodes of exploration because of the exposures of favourably mineralized and altered pyritic schists, presence of a variety of mineral occurrence types, and proximity to the Rexspar uranium-fluorite-rare earth deposits (3 km north), Harper Creek copper deposits (4 km east) and CC massive sulphide deposits on Chu Chua Mountain (15 km south -southwest). The present Foghorn property covers several B.C. Government Mineral Inventory occurrences including 82M-008 (FH, Foghorn, Lydia), 82M-029 (Foghorn), 82M-30 (Shamrock, FH), 82M-40 (Chidgrin), 82M-41 (Kelly's, FH?) and 82M-108 (Gopher).

The Lydia showings, a conformable, semi-massive to disseminated layer of suphides is reported to consist of pyrite, chalcopyrite and pyrrhotite occurring along the northwest dipping and northeast striking schistosity of the host metamorphic rocks. The upper adit is reported in the 1923 Report of the Minister of Mines to have drifted on schist mineralized with iron and copper pyrites for 100 feet before encountering a fault zone. A hole drilled by Noranda in 1972 encountered 30 feet grading 0.30% copper (Dawson, 1979). Claims covering the Lydia workings lapsed and the old Lydia workings were staked as the Foghorn 6 claim. A soil sample from the northwest area of the claim is reported by Ostensoe (1985 in A.R. 14054) to contain 650 ppb gold.

At the original Foghorn showings argentiferous galena, sphalerite, chalcopyrite, and pyrite are exposed by old workings on quartz veins and fissures in a sequence of metavolcanic rocks of the Paleozoic Eagle Bay Formation. Dawson (1980a) suggests that a mineralized zone, 400 meters long by up to 150 meters wide, occurs in buff to orange tuff at an abrupt, probable fault contact with quartz veined massive


JOSEPH 11
OLD CLAIM BOUNDARY
120° 00'
REXSPAR URANIUM
Foghorn
ORIGINAL FOGHORN MOUNTAIN (FENNEL) SHOWINGS
JOSEPH 9
B-3
ESSO RESOURCES 1984- 2,3 DRILLING
FOGGY 2
FOGGY 9
70+00W
B-2
FOGHORN 1
7014 (4)
B-5
40+00W
FOGHORN 2
7015 (4)
35+00 N
FOGHORN 5
7018 (4)
30+00 N
FOGHORN 4
7017 (4)
20+00N
20+00N
CRAIGMONT BARRIER REEF DISCOVERIES
JOSEPH 7
FOGHORN 3
7016 (4)
FOGHORN 6
Creek
B-1
B-4
Road
Creek
FOGGY 3
FOGGY 4
JOSEPH 5
51° 30'
PROFESSIONAL ENGINEER
PROVINCE
P. A. Christopher
BRITISH COLUMBIA
B-3
GRID AREAS (PREVIOUS)
1987 GRID
N
0
1000
2000 Metres
Scale 1: 50,000
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
PREVIOUS WORKINGS
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
P.A. CHRISTOPHER & ASSOCIATES LTD.
OCT. 1987
FIGURE 5

CHONG

chert. The zone contains over 20 narrow, discontinuous, steeply dipping, quartz veinlets containing spotty to sub-massive lenses of galena and sphalerite with lesser amounts of pyrite and chalcopyrite. Values up to 50.41 oz Ag/ton were obtained from a selected sample (01028) of massive sulphide. Five samples were collected by the writer from the old Foghorn working to test for enhanced precious metal content. Table 2 summaries Foghorn Showing sample results:

Table 2. Summary of Foghorn Showing Samples Results.

Sample#	Type	Width	Location	%Cu	%Pb	%Zn	oz/ton Ag	oz/ton Au
K0361	Grab	-	Foghorn Shaft	0.01	5.18	0.24	1.28	.001
K0362	Select	-	" "	0.05	17.97	8.17	5.07	.003
K0375	Select	-	" "	1.26	4.36	6.09	3.33	.002
K0377	Chip	50 cm.	60m. N. Shaft	0.10	1.07	1.46	0.30	.001
K0378	Chip	40 cm.	280m. N30E "	0.60	20.71	2.34	26.04	.001
E25051	Select*	-	Foghorn Shaft	0.07	18.34	5.28	3.85	.002
01028	Select**	-	"	0.72	33.50	9.85	50.41	.008
01029	Select**	-	"	1.10	46.40	5.95	46.88	.014
01031	Select**	-	"	1.32	20.15	16.13	37.64	.014
01033	Select**	-	"	1.04	82.10	2.39	52.65	.018

* Select Sample by R. Hogg during writer August 23/87 examination.
** Select Sample by Renegade crew.

Several vein-type lead-zinc-copper showings (Chingrin MI 82-M-40) occur 0.6km north of the Foghorn showings. The Chingrin showings have been developed by a number of deep trenches.

On the old Foggy 11 (Kelly's MI 82M-41) claim an outcrop of semi-massive sulphides occurs within quartz-sericite schists, sericitic quartzites and chloritic pyrite schists of the Upper Fennell Formation. Drill hole JC-2 by Craigmont (Vollo, 1980) intersected 3.3 meters grading 0.27% Cu, 0.15% Zn, 3.06% Pb, 58ppm Ag and 0.53ppm Au with no recovery in the adjacent 1.7 meters. Sludge from hole JC-1 (31 meters west) contained 0.87ppm gold. In 1984, Esso Resources drilled NQ holes 84-2 and 84-3 to test a north south oriented zone of anomalous soil geochemistry in the area of the Craigmont drill holes.

Table 3. Significant Drill Intersections.

Hole	Year	Company	Interval	%Cu	%Pb	%Zn	Au (ppm)	Ag (ppm)	Grid Location
FH 6	1980	Craigmont	60.0-64.1m	0.10	0.15	0.15	0.41	9.0	2220N 4498W
FH 7	1980	Craigmont	21.0-25.0m	0.39	0.10	0.04	0.14	38.0	2220N 4429W
JC 2	1980	Craigmont	17.7-21.0m	0.27	3.06	0.15	0.53	58.0	2820N 6738W
							oz/ton		
84-2	1984	Esso	68.2-69.2m	0.03	1.20	2.92	0.004	1.18	2810N 6838W
			69.2-70.3m	0.022	1.07	1.75	0.005	0.65	
			73.2-74.1m	0.03	8.94	2.56	0.005	4.55	
			74.1-75.0m	0.014	7.21	0.15	0.005	1.52	
			75.0-75.9m	0.015	11.45	1.97	0.006	2.15	
84-3	1984	Esso	43.2-44.1m	0.012	1.38	0.14	0.001	0.65	3008N 6916W
			49.5-50.4m	-	0.76	1.20	0.002	0.76	
			60.6-62.4m	-	2.89	0.45	0.001	0.76	
			62.4-63.6m	-	0.25	0.05	0.017	0.17	
			65.4-66.3m	0.074	1.20	0.68	0.001	1.15	

GEOCHEMICAL PROGRAM "B" horizons sampled at 15-25 cm depths.

The 1987 geochemical program consisted of confirmation, extension and fill-in of the 1983 Esso Resources Canada Ltd. sampling program. Samples were selectively collected over the 60km grid constructed for systematic VLF-EM and magnetic coverage. A total of 510 soil samples were analyzed for 30 element ICP with 75 sample pulps selected for atomic absorption gold analysis. Gold-silver, arsenic, copper, lead and zinc values were plotted and contoured on Figures 6a to 10b, respectively. The anomalous zones established by Esso Resources are shown for comparison. Certificates of analysis are presented as Appendix B.

Gold

Gold values were obtained from samples containing anomalous contents for base metals or silver. Gold values varied from the 1 ppb detection limit to 126 ppb with 18 values between 10 and 40 ppb and five stongly anomalous values over 40 ppb. Esso obtained values up to 287 ppb from the Foghorn 1 claim area and Ostensoe (1985, AR 14054) reported values up to 650 ppb gold from the Foghorn 6 claim area.

Silver

Silver values varied from the detection limit of 1 ppm to 42.2 ppm with 48 values of 2 ppm or more considered strongly anomalous contoured on Figure 6a (East Half) and 6b (West Half). The strongest silver responses, obtained from lines 20+50N, 25+50N and 27+50N in the east grid support and extend Esso's anomalies H and I. Anomalous silver values, obtained from the west grid generally support and extend Esso's anomalous zones C and D.

Arsenic

Arsenic values varied from 2 to 366 ppm with values over 30 ppm considered anomalous. The strongest arsenic values appear to be associated with a northeast trending belt of strong silver values and the three strongest gold responses that include anomalies H and I.

Copper

Copper values varied from 7 ppm to 1492 ppm with 33 copper values of 100 ppm or more outlined on Figures 8a and 8b. Copper values generally occur with lead, zinc or silver in the southeast part of the east grid.

Lead

Lead values varied from 11 to 5655 ppm with 66 strongly anomalous values of 100 ppm or more outlined on Figures 9a and 9b. The strongest lead responses support Esso's anomalies H and I in the east grid area and support and extend Esso's anomaly C in the west grid.

Zinc

Zinc values varied from 23 to 6226 ppm with 60 strongly anomalous values of 200 ppm or more outlined on Figures 10a and 10b. Zinc values support Esso's anomaly I but not anomalies G or K in the east grid. Zinc values in the west grid closely follow lead and expand the C anomaly but provide little support for the B anomaly.

GEOPHYSICAL SURVEY

A detailed discussion of the magnetic and VLF-Em data obtained during the 1987 field survey is provided by Ed Rochel as Appendix A to this report. Figures G1 through G8 (in pockets) summarize electromagnetic and magnetic results.

The magnetic data in the eastern grid area is generally flat with little apparent correlation with conductors. The west grid area has stronger magnetic relief with a number of northerly trending highs shown on Figure 6. A north-northwest trending magnetic low appears to correspond with the strongly conductive section of conductor axis B and possibly curves southerly to follow conductor axis C.

Conductors have two main trends with a conductive zone containing A to A7 and B to B1 having a north-northwest trend in the east grid and conductors A1, A2, and A3 having northeasterly segments. Conductors D, E, F, and G have a northeast trend and intersect the A and B conductive zones in the area of geochemical anomalies G, H and K. Conductors E, F and G pass through geochemical anomaly I in the area of the original Foghorn workings.

In the western grid area strong conductors A, B, and C parallel the north-northwest stratigraphic and structural trends with Craigmont's holes JC-1 to 3 and Esso's holes 84-3 and 84-4 testing anomaly anomaly B between lines 28N and 30N. Marr (1984) suggested that Esso's holes intersected an 8 meter wide zone of stratabound veins of galena with pyrite and sphalerite. Anomalies A and C have associated soil geochemical anomalies and may result from stratabound mineralization.

CONCLUSIONS AND RECOMMENDATIONS

The Foghorn Mountain Property, covering several named mineral occurrences, is situated in a geological environment that host the nearby Rexspar uranium-fluorite-rare earth deposits, Harper Creek copper deposits, CC (a massive pyrite deposit containing 2,500,000 tonnes grading 2% copper, 0.5% zinc, 0.5 grams/tonne gold, 9 grams/tonne silver and 0.05% cobalt), Rea Gold's Concession Zone (266,200 tons grading 0.19 oz/ton gold, 2.14oz/ton silver, 2.15% lead, 2.25% zinc and 0.527% copper) and the Minnova-Rea Gold Samatosum silver deposit (661,000 tons grading 32.08 oz/ton silver, 0.052 oz/ton gold, 3.50% zinc, 1.70% lead and 1.20% copper). The property has several soil geochemical anomalies (Figure 6 to 10) with coincident conductive trends (Figures G1 to G8, Appendix A). Trenching, geological mapping and geochemical sampling is required to define specific drill sites for testing coincident geophysical and geochemical anomalous trends.

A recommended Stage 1 program of trenching, geological mapping, geochemical sampling and 500 meter diamond drill program is estimate to cost $ 95,000. Success contingent Stage 2 and Stage 3, 1200 meter diamond drill programs are estimated to cost $ 195,600 each.

COST ESTIMATES

STAGE 1. GEOPHYSICAL, GEOCHEMICAL, TRENCHING, DRILLING

Mobilization/Project Preparation		$ 2,000
Trenching & Road Building		6,000
Personnel		
Project Manager	5 days @ $300/day..............	1,500
Project Geologist	20 days @ 300/day..............	6,000
Assistant/Sampler	30 days @ 150/day..............	4,500
Geophysical Operator	10 days @ 175/day..............	1,750
Engineer	3 days @ 400/day..............	1,200
Room & Board	70 man days @ $40/day...........	2,800
Transporation/Communication		
Airfares		500
4x4 trucks	30 truck days @ $75ea............	2,250
Fuel		500
Phone		200
Diamond Drilling		
500 meters @ $ 80/meter..............................		40,000
Equipment Rental		500
Geochemical Costs		
300 soil or rock geochem samples @ $12ea................		3,600
100 assays @ $25ea..............................		2,500
Expendables		1,000
Report Preparation..............................		4,000
Recording Costs	say 5% on $80,000................	4,000
Contingency		10,200
	Stage 1 Total	$ 95,000

STAGE 2. DIAMOND DRILLING (Contingent)

Mobilization/Project Preparation		$ 2,000
Site Preparation, Road Building & Reclamation		10,000
Personnel Costs		
Project Manager	10 days @ $300/day..........	3,000
Project Geologist	50 days @ 300/day..........	15,000
Assistant	50 days @ 150/day..........	7,500
Engineer	4 days @ 400/day..........	1,600
Room & Board	110 man days @ 40/man day.......	4,400
Transporation		6,000
Communication		500
Diamond Drilling		
1200 meters @ $80/meter..............................		96,000
Expendables		2,000
Equipment Rentals		2,000
Geochemical Costs		
400 assays @ $25ea..............................		10,000
Report Preparation		5,000
Recording Costs	5% on $100,000..............	5,000
Contingency		25,600
	Stage 2 Total	$ 195,600

STAGE 3. DIAMOND DRILLING (Contingent)

Mobilization/Project Preparation		$ 2,000
Site Preparation, Road Building & Reclamation		10,000
Personnel Costs		
Project Manager	10 days @ $300/day..........	3,000
Project Geologist	50 days @ 300/day..........	15,000
Assistant	50 days @ 150/day..........	7,500
Engineer	4 days @ 400/day..........	1,600
Room & Board	110 man days @ 40/man day.......	4,400
Transporation		6,000
Communication		500
Diamond Drilling		
1200 meters @ $80/meter................................		96,000
Expendables		2,000
Equipment Rentals		2,000
Geochemical Costs		
400 assays @ $25ea....................................		10,000
Report Preparation		5,000
Recording Costs	5% on $100,000..............	5,000
Contingency		25,600
	Stage 3 Total	$ 195,600

Stage 1.	$ 95,000
Stage 2.	195,600
Stage 3.	195,600

$ 486,200 Total Stages 1, 2, and 3

Peter A. Christopher, Ph.D., P.Eng.
April 12, 1988

BIBLIOGRAPHY

British Columbia Dept. of Mines: Annual Reports 1913, 1915, 1916, 1917, 1923, 1924; GEM 1970, 1974; Exploration 1983, 1984; Minfile 82M/8 FH (Foghorn, Lydia), 29 Foghorn, 30 Shamrock (FH), 40 Chidgrin, 41 Kelly's (FH?), 108 Gopher; Assessment Reports 1597, 1624, 1924, 3820, 4876, 7404, 7757, 7758, 7813, 7990, 8530, 9008, 9537, 9716, 11381, 11503, 12904, 13054, 14054.

Campbell, R.B., 1963. Adams Lake. Geol. Surv. Can., Map 48-1963.

Cartwright, Paul A., 1981. Report om I.P. and Resistivity Survey, Foggy 11 Claim. Assessment Report 9537 for Barrier Reef Resources dated Oct. 1, 1981.

Dawson, J.M., 1979. Report on Diamond Drilling on the Foghorn Mountain Property, Kamloops Mining Division, British Columbia. Assessment Report 7758 for Barrier Reef Resources Dated November 1979.

Dawson, J.M., 1980a. Geological, Geochemical and Geophysical Report on the Foghorn Showings. Assessment Report 7813 for Barrier Reef Resources Dated Jan. 4, 1980.

Dawson, J.M., 1980b. Geological, Geochemical and Geophysical Report on the Foggy No. 11 Claim. Assessment Report 7990 for Barrier Reef Resources dated April 15,1980.

Dawson, J.M., 1981. Geochemical and Geophysical Report on the Foggy #11 Claim, Kamloops Mining Division, British Columbia. Assessment Report 9008 for Barrier Reef Resources Dated Jan. 4, 1980.

Everett, C.C. and Cooper, W.G., 1983a. Geochemical and Geophysical Report on Foggy B, Foggy C, Foggy D, Foggy E Groups. Assessment Report 11,381 for Esso Resources Canada dated November 7, 1983.

Everett, C.C. and Cooper, W.G., 1983b. Geochemical and Geophysical Report on Foggy A Group. Assessment Report 11,503 for Esso Resources Canada dated August 25, 1983.

Fraser, D.C. and Dvorak, Z., 1979. Dighem Survey Foghorn Mountain. for Barrier Reef Resources, Assessment Report 7404 dated June 15, 1979.

Heim, R.C., Knauer, J.D., Walker, J.T., and Belik, G.D., 1972. Geochemical Survey, Geophysical Survey and Geological Survey on the FH 1-6, FH 9-10, FH 14-18, FH 20, FH 22 and Foghorn Fraction Mineral Calims. For Noranda Exploration Company, Limited, As. Report 3820.

Marr, J.M. and Everett, 1984. Drilling Assessment Report on the Foggy A Group. Assessment Report 12,904 for Esso Resources Canada Ltd. dated November 10, 1984.

Marr, J.M., 1984. Drilling Assessment Report on Joseph 84 Group. Assessment Report 13,054 for Esso Resources Canada Ltd. Nov. 8, 1984.

McMillan, W.J., 1980. CC Prospect, Chu Chua Mountain, B.C. Min. Energy Mines & Pet. Res., Geological Fieldwork, 1979, papaer 1980-1, pp. 37-48.

Okulitch, A.V., 1979. Thompson-Shuswap-Okanagan. Geol. Surv. Can. Open File 637.

Preto, V.A., 1978. Rexspar Uranium Deposit (82M/12W), B.C. Min. Energy Mines & Pet. Res., Geological Fieldwork, 1977, Paper 1978-8, pp. 19-22.

Preto, V.A., 1979. Barriere Lakes - Adams Plateau Area (82L/13E; 82M/4, 5W; 92P/1E, 8E). B.C. Min. Energy Mines & Pet. Res., Geological Fieldwork, 1978, Paper 1979-1, pp. 15-23.

Preto, V.A., 1981. Barriere Lakes - Adams Plateau Area (82M/4, 5W; 92P/1E). B.C. Min. Energy Mines & Pet. Res., Geological Fieldwork, 1980, Paper 1981-1, pp. 15-23.

Preto, V.A., McLaren, G.P., and Schiarizza, P.A., 1980. Barriere Lakes -Adams Plateau Area (82L/13E; 82M/4, 5W; 92P/8E, 9E) . B.C. Min. Energy Mines & Pet. Res., Geological Fieldwork, 1979, Paper 1980-1, pp. 28-36.

Sampson, Chris J., 1987. Report on Geology and Exploration Potential Foghorn Claims, Kamloops Mining Division Near Birch Island, British Columbia. For Gold Spring Resources Ltd.

Schiarizza, P.A., 1981. Clearwater Area (82M/12W; 92P/8E, 9E). B.C. Min. Energy, Mines & Pet. Res., Feological Fieldwork, 1980, Paper 1981-1, pp. 159-164.

Schiarizza, P.A., 1982a. Clearwater Area (82M/12W; 92P/8E, 9E). B.C. Min. Energy, Mines & Pet. Res., Feological Fieldwork, 1981, Paper 1982-1, pp. 59-67.

Schiarizza, P.A., 1982b. Geology of the Barriere River -Clearwater Area (82M/4, 5, 12 ; 92P/1, 8, 9). B.C. Min. Energy, Mines & Pet. Res., Preliminary Map No. 53.

Singhai, G.C., 1974. Report on Foghorn Mineral Claims. for Sandy and Marston Fennell dated Sept. 1974.

Vollo, N.B., 1979. Diamond Drilling, Foggy 2 and 3 Claims. Assessment Report 7757 for Craigmont Mines Linited dated Dec. 17, 1979.

Vollo, N.B., 1980. Diamond Drilling, Foggy 2 and 3 and Joseph 7. Assessment Report 8530 for Craigmont Mines Limited dated Oct. 3, 1980.

Vollo, N.B., 1981. Diamond Drilling, Foggy 2 and 3 and Joseph 7. Assessment Report 9716 for Craigmont Mines Limited dated Sept. 16, 1981.

Vollo, N.B., 1968a. Geophysical Report on an EM-16 Survey of the 82M/12 FH Group. for Royal Canadian Ventures Ltd. As. Report 1597 dated Aug. 19, 1968.

Vollo, N.B., 1968b. Geophysical Report on a Magnetometer Survey of the 82M/12 FH Group. for Royal Canadian Ventures Ltd. As. Report 1624 dated Aug. 10, 1968.

Vollo, N.B., 1969. Geochemical Report on the 82M/12 FH Group at Birch Island, B.C. for Royal Canadian Ventures Ltd. As. Report 1924 dated May 28, 1969.

White, G.E., undated, Geophysical Responses Chu Chua Massive Sulphide Deposits, Barriere Area, B.C.

CERTIFICATE

I, Peter A. Christopher, with business address at 3707 West 34th Avenue, Vancouver, British Columbia, do hereby certify that:

1) I am a consulting geological engineer registered with the Association of Professional Engineers of British Columbia since 1976.

2) I am a Fellow of the Geological Association of Canada and a member of the Society of Economic Geologists.

3) I hold a B.Sc. (1966) from the State University of New York at Fredonia, a M.A. (1968) from Dartmouth College and a Ph.D. (1973) from the University of British Columbia.

4) I have been practising my profession as a Geologist for over 20 years.

5) I have no direct or indirect interest, nor do I expect to receive any interest directly or indirectly in the property or securities of Gold Spring Resources Ltd.

6) I have based this report on previous exploration experience in the area of the Foghorn Mountain Property, a review of government and company reports listed in the bibliography, a field examination conducted by me on August 23, 1987 and on the results of an exploration program conducted for Gold Spring Resources Ltd. in 1987.

7) I consent to the use of this report by for any Filing Statement, Statement of Material Facts, Prospectus or assessment work by Gold Spring Resources Ltd.

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher

Peter A. Christopher, Ph.D., P.Eng.
April 12, 1988

FOGHORN PROJECT APPENDIX REPORT

ON

1987 GEOPHYSICAL SURVEY RESULTS

DECEMBER, 1987
VANCOUVER, B.C.

E.R. ROCKEL
INTERPRETEX RESOURCES LTD.

FOGHORN PROJECT APPENDIX REPORT
ON
1987 GEOPHYSICAL SURVEY RESULTS

1. DISCUSSION

Two grid areas were surveyed using a Geonics EM-16 VLF receiver and a Geometrics total field magnetometer. The "east" grid was described by lines 1800N to 3900N from stations 3300W to 5500W. The "west" grid was described by lines 1800N to 3400N from stations 5500W to 7500W.

VLF EM data from the "east" and "west" grids have been profiled on plan maps at a scale of 1:5000. In phase VLF EM values have been Fraser Filtered and presented as contours on plan maps at a scale of 1:5000. VLF EM in-phase anomaly amplitudes ranged from strong through moderate to weak. Little evidence of topography induced positive and negative bias could be seen in these data. VLF EM anomalies have been grouped into conductor systems according to profile character similarities and, where possible, with the aid of magnetic trends. Conductor axes have been interpreted between survey lines to form conductive trends. Significant conductor systems have been labelled for further discussion.

Magnetic activity in the Foghorn survey area was mainly flat in the east grid and slightly more active in the west area. Total field magnetic data were controlled by automatic recording of magnetic values every 30 seconds at a stationary base station. Field magnetic readings were individually corrected for drift using base station values recorded at the same time of day. Certain readings which were observed to be incorrect were deleted. Additional magnetic level corrections were made mathematically to resolve level changes on some lines induced by battery changes in the magnetometer. Final magnetic values were contoured by computer on plan maps at a scale of 1:5000.

2. CONCLUSIONS

2.1 East Grid

Magnetic results in this area show no large magnetic anomalies although some weak trends can be seen. The weak magnetic activity seen here is probably due to a relatively homogeneous nonmagnetic rock type. Small lows and highs can be seen but do not correlate with VLF EM conductors. These small features may be due to fractures and local changes in magnetic susceptibility.

VLF electromagnetic results in the east grid show a complicated conductive pattern between approximately 4700W and 5300W trending roughly northerly. This complicated zone has been labelled "A" to "A7" and "B" to "B1". VLF EM profile character indicates that most conductors are near surface and that conductivity occurs in relatively short discontinuous and multiple systems rather than in a long continuous body as suggested by Fraser Filter contours. Although most of the complicated zone trends northerly, conductors "A1", "A2", "A3", "A5" and "A7" strike more towards the east of north and appear to

...2

intersect or cross cut the main strike direction. The main zone, striking more northerly, is believed to represent a fracture zone. VLF EM profiles infer that conductance (conductivity-thickness product) of many of the stronger anomalies within systems "A", "A4" and "B" is relatively high, suggesting, in turn, the presence of conductive sulphide mineralization within the main fracture zone. Low magnetic activity and no apparent magnetic correlation with conductivity indicates that pyrrhotite is probably not present. The cross cutting features, mentioned above, are believed to represent complimentary fractures related to the main fracture trend. Sulphide mineralization may also be present in these systems, however, lower conductance indicates that the sulphide occurences would be narrow, probably in thin veins.

Conductors "C" and "D" are believed to be related to the main zone, "A" through "B1" to the north, but seem to be cut or offset from the main zone. An interpreted fault has been shown to explain the offset and also the apparent abrupt change in the strike direction of system "D". Evidence of higher conductance in "D" again suggests the presence of sulphides.

East of about 4700W a series of conductors have been outlined and labelled "E", "F" and "G". This group of conductors has a strike direction similar to that of the systems cross cutting the main zone "A" through "B1". Systems labelled "E" seem to create a long discontinuous trend and is believed to be caused by a fracture or shear zone. Anomalies in "E" on line 1800N through 2100N show slightly higher conductance and therefore are better candidates for the presence of conductive sulphides than the rest of "E". Conductors "F" and "G" are weak systems and are probably caused by wet fractures rather than sulphide mineralization.

2.2 West Grid

Magnetic contours show northerly and northwesterly trends. Many of the weaker northerly trends may have resulted from contouring unrelated anomalies accross the large (200 meters) separation between lines. Stronger magnetic high trends are probably due to a more basic rock type. These magnetic highs do not appear to be related to VLF EM conductivity. A vague magnetic low trend seems to cut through the magnetic highs striking north-northwest. This low trend roughly follows a VLF EM conductor system. No other magnetic feature seem to be related to conductivity.

VLF EM data show a number of conductor systems in the west grid. Three strong systems, trending mainly northwesterly, have been labelled "A", "B" and "C". Other weaker unlabelled systems in the area trend north to northeasterly.

Conductor "A" varies from strong to weak along its strike, possibly fading out south of line 2200N. A strong anomaly on line 2500N and moderate strength anomalies on lines 3000N and 3200N show slightly

...3

higher conductance than the rest of the system. These anomalies may be targets for additional exploration for conductive sulphide minerals.

The apparent correlation of conductors "B" and "C" with a wide and rather vague magnetic low trend may indicate that these systems reflect conductivity within a fault zone. The double conductor formed by "B" and "C" on lines 2400 and 2600 may represent the hanging wall and foot wall of the fault zone. VLF EM profiles show higher conductance on stronger anomalies within both systems. Profile character suggests that the dip of systems "B" and "C" is westerly from line 2400N to the north and is easterly on conductor "C" south of line 2400N. Strong anomalies within both conductor systems are considered good targets for exploration for conductive sulphide minerals.

Unlabelled weaker conductor systems in the west grid are believed to be caused by near surface features such as water soaked fractures or conductive overburden material.

3. RECOMMENDATIONS

From a geophysical standpoint the best targets for follow-up are the VLF EM anomalies in the main complex conductive zone within the east grid, described by systems "A" through "B1". Next in priority for follow-up exploration are the conductors "B" and "C", in the west grid, which appear to be associated with a fault zone. Third priority targets are the strong anomalies within conductor "A" in the west grid.

Information about other VLF EM anomalies within both areas should be obtained on the ground to determine if anomalies are surficial or bonafied bedrock conductors. If no evidence of conductive overburden can be found then these anomalies should be explored in more detail to determine if a geological cause of significance to mineral exploration can be determined.

Ground exploration should include geological mapping and geochemical sampling to help determine geological priorities for further exploration by trenching or drilling.

Magnetic survey results should be correlated with geological information in order to assess the importance of magnetic features and to aid geological mapping.

E.R. Rockel
Interpretex Resources Ltd.
Vancouver, B.C.
December, 1987

Respectfully submitted

INTERPRETEX RESOURCES LTD.

Vancouver, British Columbia

E. R. ROCKEL

Consulting Geophysicist

THE ASSOCIATION OF
PROFESSIONAL ENGINEERS,
GEOLOGISTS and GEOPHYSICISTS
OF ALBERTA
PERMIT NUMBER
P 3100
INTERPRETEX
RESOURCES LTD.

CERTIFICATE

I, Edwin Ross Rockel, Geophysicist of Vancouver, British Columbia, Canada, hereby certify that:

1. I received a B.Sc. degree in Geophysics from the University of British Columbia in 1966.

2. I am a Consulting Geophysicist and owner of Interpretex Resources Ltd. of Box 48239, Bentall P.O., in the City of Vancouver, in the Province of British Columbia.

3. I currently reside at 6571 Cooney Rd., in the City of Richmond, in the Province of British Columbia.

4. I have been practising my profession since graduation.

5. I am a Professional Geophysicist registered in the Province of Alberta.

6. I am a Professional Engineer registered in the Province of Saskatchewan.

7. I am a Certified Professional Geological Scientist registered in the United States of America.

8. This report may be used for the development of the property, provided that no portion will be used out of context in such a manner as to convey meanings different from that set out in the whole.

9. Consent is hereby given to the company for which this report was prepared to reproduce the report or any part of it for the purposes of development of the property, or facts relating to the raising of funds by way of a prospectus and/or statement of material facts.

Date: Dec. 11, 1987 Signed: [signature]

Vancouver,
British Columbia

Edwin Ross Rockel
B.Sc., P.Geoph., P. Eng.

APPENDIX B

CERTIFICATES OF ANALYSIS

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE (604) 253-3158 FAX (604) 253-1716

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-4 SOIL P5-SILT P6-ROCK

DATE RECEIVED: OCT 5 1987 DATE REPORT MAILED: Oct 20/87 ASSAYER. D. Toye. DEAN TOYE, CERTIFIED B.C. ASSAYER

GOLD SPRING RESOURCES File # 87-4749 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L36+00N 40+00W	1	11	28	33	.4	6	4	75	1.78	4	5	ND	1	52	1	2	2	30	.10	.055	31	23	.41	63	.03	2	1.37	.01	.05	1
L36+00N 39+50W	1	13	16	44	.2	11	5	169	1.85	3	5	ND	1	55	1	2	2	28	.15	.051	37	24	.49	118	.03	2	1.31	.01	.05	1
L36+00N 39+00W	1	13	18	41	.2	9	5	223	1.97	2	5	ND	1	50	1	2	2	32	.13	.040	33	22	.43	126	.03	3	1.55	.02	.05	1
L36+00N 38+50W	1	10	13	28	.3	5	3	48	1.36	2	5	ND	1	27	1	2	2	28	.10	.048	19	18	.18	57	.03	4	1.72	.02	.02	1
L36+00N 38+00W	1	14	13	39	.2	8	5	140	2.36	2	5	ND	1	69	1	2	2	36	.16	.036	39	23	.58	102	.04	5	1.48	.01	.06	1
L36+00N 37+50W	1	23	15	113	.3	8	5	377	1.88	2	6	ND	1	194	1	2	2	33	.49	.063	40	23	.65	206	.06	6	2.22	.02	.06	1
L36+00N 37+00W	1	8	13	48	.1	12	6	221	1.87	2	5	ND	1	144	1	2	3	34	.27	.051	38	26	.73	90	.07	4	1.37	.02	.08	1
L36+00N 36+50W	1	16	16	61	.2	9	6	252	1.96	6	5	ND	1	178	1	2	2	35	.42	.054	43	24	.76	127	.04	4	1.51	.02	.06	1
L36+00N 36+00W	1	15	29	48	.4	8	5	102	2.25	3	5	ND	1	74	1	2	2	34	.10	.035	36	20	.54	76	.05	2	1.25	.01	.05	1
L36+00N 35+50W	1	13	29	43	.6	6	3	83	1.63	3	5	ND	1	54	1	2	2	27	.12	.043	24	19	.35	47	.03	2	1.16	.01	.03	1
L36+00N 35+00W	1	9	29	55	.7	9	4	151	1.76	2	5	ND	1	97	1	2	2	32	.27	.053	32	21	.53	95	.03	2	1.12	.01	.06	1
L35+00N 40+00W	3	258	29	562	.2	14	8	375	2.52	13	22	ND	5	87	2	2	2	40	.16	.076	71	39	.76	74	.11	5	2.77	.02	.05	1
L35+00N 39+50W	2	30	36	95	.2	13	6	237	2.40	5	6	ND	1	134	1	2	2	38	.26	.050	45	33	.81	135	.05	2	1.63	.01	.07	1
L35+00N 39+00W	1	14	20	40	.3	8	3	125	1.83	2	5	ND	1	50	1	2	2	28	.12	.040	26	20	.31	78	.04	4	1.42	.01	.04	1
L35+00N 38+50W	2	66	40	239	.4	16	9	620	2.49	6	7	ND	1	302	3	2	2	32	.66	.102	47	30	.57	180	.04	7	2.37	.02	.06	1
L35+00N 38+00W	1	13	18	35	.2	7	3	95	1.53	4	5	ND	1	38	1	2	2	27	.06	.037	34	15	.29	76	.03	2	1.06	.01	.04	1
L35+00N 37+50W	1	10	17	42	.5	7	4	95	1.72	2	5	ND	1	34	1	2	2	27	.05	.037	33	16	.26	77	.03	3	.85	.01	.05	1
L35+00N 37+00W	1	17	13	52	.3	10	6	229	2.60	5	5	ND	1	95	1	2	2	37	.19	.071	49	24	.85	89	.03	3	1.35	.01	.09	1
L35+00N 36+50W	1	11	14	34	.2	5	4	88	1.58	4	5	ND	1	69	1	3	2	30	.09	.041	41	16	.48	68	.05	3	1.19	.01	.07	1
L35+00N 36+00W	1	11	16	42	.3	6	5	90	1.84	2	5	ND	1	63	1	2	3	32	.10	.039	40	20	.58	60	.05	4	1.46	.01	.06	1
L35+00N 35+50W	1	13	24	40	.1	7	5	201	1.99	4	5	ND	1	63	1	2	2	37	.10	.041	41	20	.69	60	.04	4	1.46	.01	.06	1
L35+00N 35+00W	1	31	26	69	.3	11	8	267	2.68	9	5	ND	1	89	1	2	2	35	.17	.060	44	22	.82	92	.04	3	1.64	.01	.09	1
L34+00N 40+00W	1	14	14	48	.2	12	8	472	2.18	2	5	ND	1	242	1	2	2	44	.32	.054	48	40	1.06	70	.08	2	1.69	.01	.09	1
L34+00N 39+50W	1	11	16	36	.1	8	4	103	1.64	2	5	ND	1	132	1	2	3	34	.15	.049	37	28	.56	48	.07	9	1.37	.02	.06	1
L34+00N 39+00W	1	9	14	32	.1	6	3	100	1.60	2	5	ND	1	85	1	2	2	33	.11	.036	32	21	.46	49	.06	5	1.18	.02	.05	1
L34+00N 38+50W	1	15	24	46	.3	9	5	164	1.88	2	5	ND	1	129	1	2	2	34	.14	.050	42	23	.59	69	.05	3	1.52	.01	.06	1
L34+00N 38+00W	1	12	21	44	.2	6	4	188	1.68	7	5	ND	1	94	1	2	2	30	.09	.040	38	17	.38	66	.04	2	1.15	.01	.05	1
L34+00N 37+50W	2	24	52	125	.3	11	7	453	2.84	26	5	ND	1	79	1	2	2	33	.15	.072	45	24	.57	82	.02	2	1.46	.01	.07	1
L34+00N 37+00W	1	26	76	333	.6	13	7	364	2.44	2	5	ND	1	263	5	2	3	42	.39	.049	53	30	.80	157	.05	5	1.65	.01	.07	1
L34+00N 36+50W	1	10	22	36	.2	6	3	101	2.01	3	5	ND	1	46	1	2	2	34	.05	.045	31	15	.30	72	.04	2	1.13	.01	.04	1
L34+00N 36+00W	1	25	22	64	.4	7	6	349	2.59	5	5	ND	1	131	1	2	2	37	.19	.058	43	21	.63	82	.05	6	1.57	.01	.10	1
L34+00N 35+50W	1	18	23	80	.4	7	5	145	2.10	8	5	ND	1	162	1	2	2	30	.36	.065	39	17	.50	83	.04	5	1.68	.01	.09	1
L34+00N 35+00W	2	20	52	57	.1	8	5	159	2.26	9	5	ND	1	99	1	2	2	31	.12	.061	47	19	.55	67	.04	11	1.24	.01	.07	1
L33+50N 40+00W	1	18	26	55	.1	12	7	261	2.28	7	5	ND	1	187	1	2	2	39	.26	.059	47	32	.95	75	.05	5	1.36	.01	.07	1
L33+50N 39+50W	1	18	21	61	.1	10	6	234	2.13	6	5	ND	1	144	1	2	4	42	.23	.056	51	33	.96	68	.04	2	1.57	.02	.06	1
L33+50N 39+00W	1	14	19	39	.1	8	5	220	2.01	2	5	ND	1	100	1	2	2	36	.21	.049	43	22	.58	68	.05	6	1.21	.02	.07	1
STD C	19	61	40	132	7.7	70	29	1077	4.10	41	23	8	39	53	19	18	20	60	.48	.088	40	61	.91	180	.07	35	1.89	.06	.15	13

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L33+50N 38+50W	2	17	18	38	.2	5	3	96	1.97	3	5	ND	1	90	1	2	2	28	.15	.058	34	16	.31	53	.03	2	.86	.02	.06	1
L33+50N 38+00W	1	14	23	42	.1	7	4	232	1.84	6	5	ND	1	130	1	2	2	35	.22	.062	43	24	.58	59	.05	3	1.06	.02	.08	1
L33+50N 37+50W	2	14	35	44	.5	5	3	116	1.67	12	5	ND	1	63	1	2	2	29	.09	.047	29	21	.32	43	.03	2	1.38	.02	.04	2
L33+50N 37+00W	2	17	47	99	.4	6	5	209	2.22	11	5	ND	1	73	1	2	2	31	.15	.056	40	20	.51	100	.03	5	1.23	.01	.05	1
L33+50N 36+50W	2	62	58	176	.7	6	4	224	1.86	11	7	ND	1	148	2	2	2	28	.23	.053	44	17	.40	101	.03	2	1.41	.01	.06	1
L33+50N 36+00W	2	20	33	72	.5	7	5	237	2.31	11	5	ND	1	75	1	2	2	31	.18	.075	35	19	.40	90	.02	2	1.02	.01	.08	1
L33+50N 35+50W	2	38	31	79	.7	10	7	213	2.64	10	5	ND	1	137	1	2	2	36	.30	.088	49	25	.86	71	.04	4	1.58	.01	.12	1
L33+50N 35+00W	1	22	20	57	.5	9	6	203	2.36	9	5	ND	1	165	1	2	2	36	.34	.083	44	21	.89	66	.05	3	1.49	.01	.09	2
L33+00N 40+00W	1	19	26	63	.1	10	7	221	2.65	12	5	ND	1	132	1	2	2	37	.27	.093	51	30	.93	53	.05	2	1.55	.01	.07	1
L33+00N 39+50W	2	15	18	50	.1	11	6	289	2.27	4	5	ND	2	85	1	2	2	36	.19	.051	40	34	.70	65	.06	2	1.68	.01	.05	2
L33+00N 39+00W	2	15	20	44	.2	8	5	180	2.15	5	5	ND	1	99	1	2	2	32	.16	.049	37	26	.67	62	.05	3	1.45	.01	.06	1
L33+00N 38+50W	1	17	32	71	.2	10	7	218	2.92	9	5	ND	2	177	1	2	2	39	.34	.056	42	31	.88	101	.07	2	1.70	.01	.08	1
L33+00N 38+00W	1	18	35	87	.1	9	6	269	2.35	8	5	ND	1	191	1	2	2	37	.30	.059	42	23	.74	112	.05	2	1.40	.01	.09	1
L33+00N 37+50W	2	14	55	70	.8	7	4	373	1.88	3	5	ND	1	115	1	2	2	31	.27	.119	36	21	.44	74	.04	2	1.11	.01	.08	1
L33+00N 37+00W	4	157	269	813	1.5	20	15	951	3.41	41	5	ND	3	165	4	2	2	33	.30	.138	70	24	.68	152	.05	5	2.50	.01	.10	2
L33+00N 36+50W	2	21	136	184	.4	8	5	238	2.34	9	5	ND	1	87	1	2	2	32	.18	.052	35	21	.45	86	.03	3	1.18	.01	.05	1
L33+00N 36+00W	3	28	87	174	.3	9	6	211	2.58	11	5	ND	1	60	1	2	2	32	.12	.065	47	20	.52	101	.02	2	1.16	.01	.07	1
L33+00N 35+50W	2	27	51	77	.5	8	4	145	2.39	8	5	ND	1	66	1	2	2	26	.14	.058	41	16	.44	92	.02	2	1.06	.01	.05	1
L33+00N 35+00W	2	18	43	48	.5	7	5	196	2.35	4	5	ND	1	67	1	2	2	31	.09	.056	37	19	.51	73	.03	3	1.33	.01	.06	1
L32+50N 40+00W	2	14	27	60	.2	14	6	244	1.96	4	5	ND	1	158	1	2	3	33	.21	.062	38	34	.90	64	.04	2	1.28	.01	.06	1
L32+50N 39+50W	2	15	20	55	.1	11	6	272	2.07	5	5	ND	1	137	1	2	2	42	.19	.057	41	37	.89	82	.04	6	1.34	.01	.07	1
L32+50N 39+00W	2	18	33	47	.2	10	4	171	1.87	7	5	ND	1	91	1	2	2	29	.14	.062	37	29	.61	56	.03	3	1.28	.01	.06	3
L32+50N 38+50W	2	14	20	49	.1	9	5	192	1.90	7	5	ND	1	107	1	2	2	33	.19	.057	38	25	.71	81	.03	4	1.08	.01	.08	2
L32+50N 38+00W	2	18	34	75	.1	11	7	427	2.40	9	5	ND	1	119	1	2	2	39	.29	.063	46	31	.86	118	.04	5	1.39	.01	.10	1
L32+50N 37+50W	2	18	22	103	.3	11	6	456	2.09	4	5	ND	1	181	1	2	2	38	.46	.184	40	28	.90	133	.04	3	1.31	.02	.14	1
L32+50N 37+00W	2	45	143	212	.7	14	8	347	2.59	10	5	ND	2	294	1	2	3	38	.44	.122	63	32	1.00	110	.06	4	1.83	.02	.11	1
L32+50N 36+50W	2	20	73	92	.3	8	5	247	2.03	8	5	ND	1	198	1	2	2	33	.25	.059	41	21	.56	84	.05	2	1.13	.01	.08	1
L32+50N 36+00W	2	26	80	124	.6	11	7	195	2.27	11	5	ND	1	95	1	2	2	31	.21	.067	46	24	.61	132	.02	5	1.10	.01	.06	1
L32+50N 35+50W	1	17	36	86	.3	9	6	262	2.29	5	5	ND	1	101	1	2	2	34	.26	.075	49	21	.93	142	.03	2	1.31	.01	.07	1
L32+50N 35+00W	1	17	63	40	.1	4	2	70	1.30	4	5	ND	1	46	1	2	2	19	.08	.048	31	12	.17	90	.02	2	.69	.01	.04	1
L28+50N 74+00W	2	29	28	47	.1	9	4	109	2.68	15	5	ND	1	19	1	2	2	52	.06	.028	17	21	.30	67	.07	2	1.44	.01	.04	3
L28+50N 73+75W	1	26	23	53	.5	10	6	178	3.23	6	5	ND	2	13	1	2	2	54	.15	.031	9	19	.22	54	.11	3	1.13	.01	.02	1
L28+50N 73+50W	2	59	29	89	.3	17	9	196	4.17	11	5	ND	2	30	1	2	2	57	.40	.047	19	29	.51	197	.07	2	1.98	.01	.05	1
L28+50N 73+25W	2	380	48	102	.6	30	13	713	3.31	26	5	ND	3	34	1	2	2	40	.70	.062	33	28	.48	250	.09	4	3.23	.02	.06	1
L28+50N 73+00W	2	165	60	128	.1	26	14	841	3.48	16	5	ND	2	39	1	2	2	46	.65	.069	28	32	.61	408	.04	2	2.01	.01	.06	2
L28+50N 72+75W	2	28	76	77	.3	12	6	177	3.11	11	5	ND	1	35	1	2	2	44	.17	.065	27	22	.47	180	.03	2	1.47	.01	.07	1
STD C	20	62	37	133	7.5	72	29	1070	4.15	38	18	8	40	52	19	17	19	59	.49	.092	40	63	.92	181	.07	34	1.81	.06	.14	12

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L28+50N 72+50W	1	27	109	87	.5	15	6	219	3.22	16	5	ND	1	38	1	2	3	57	.17	.103	26	27	.53	242	.03	2	1.78	.01	.09	1
L28+50N 72+25W	1	199	181	660	1.6	56	11	1275	3.34	12	5	ND	2	55	5	2	2	43	.77	.104	33	24	.54	511	.07	4	3.42	.02	.06	1
L28+50N 72+00W	1	117	275	1159	1.0	95	16	1072	4.13	26	5	ND	2	58	9	2	2	61	.49	.099	31	33	.70	887	.06	3	2.89	.01	.07	1
L28+50N 71+75W	1	39	175	411	.7	33	9	340	4.00	18	5	ND	1	29	2	2	2	58	.17	.052	22	24	.53	336	.06	2	2.24	.01	.05	1
L28+50N 71+50W	1	32	206	310	.6	21	10	487	4.65	16	5	ND	1	30	1	2	2	70	.15	.065	25	23	.60	254	.06	3	2.05	.01	.06	1
L28+50N 71+25W	1	33	64	363	.3	16	6	170	2.94	14	5	ND	1	22	4	2	2	43	.13	.035	25	16	.24	267	.06	2	1.50	.01	.04	1
L28+50N 71+00W	1	15	38	59	.1	6	4	105	3.05	12	5	ND	1	19	1	3	2	40	.08	.038	24	15	.29	71	.05	5	1.07	.01	.04	1
L28+50N 70+75W	1	10	60	48	.1	4	4	142	2.61	5	5	ND	1	14	1	3	2	32	.07	.025	15	13	.19	67	.05	2	1.05	.02	.02	1
L28+50N 70+50W	2	24	101	539	.3	16	8	462	2.79	10	5	ND	4	49	1	2	2	28	.35	.070	35	19	.46	214	.05	2	1.95	.01	.05	1
L28+50N 70+25W	2	94	299	2767	1.0	34	14	1582	4.33	11	5	ND	2	127	15	2	2	44	1.05	.104	25	29	.55	624	.06	3	3.49	.02	.05	5
L28+50N 70+00W	1	18	53	147	.4	7	5	1771	2.24	21	5	ND	1	26	1	2	3	24	.07	.070	38	15	.32	92	.02	2	1.26	.01	.08	1
L28+50N 52+00W	1	33	242	924	.4	19	13	344	4.41	19	5	ND	2	39	2	2	2	63	.20	.046	25	28	.62	323	.07	4	2.22	.01	.04	1
L19+00N 51+50W	1	17	67	131	1.3	7	4	122	2.34	20	5	ND	1	19	1	2	2	26	.05	.060	27	15	.25	87	.01	3	1.38	.01	.06	1
L19+00N 51+00W	1	27	60	55	.7	9	5	262	2.82	25	5	ND	1	15	1	2	2	30	.03	.066	28	17	.31	73	.01	2	1.55	.01	.07	1
L19+00N 50+50W	1	37	52	66	1.5	9	5	295	2.67	20	5	ND	1	19	1	2	2	26	.04	.083	23	16	.32	78	.01	2	1.38	.01	.07	1
L19+00N 50+00W	1	40	59	68	.3	10	6	234	3.01	23	5	ND	1	20	1	2	2	24	.04	.078	33	16	.34	69	.01	2	1.39	.01	.08	1
L19+00N 49+50W	1	93	84	123	.5	19	12	492	4.55	27	5	ND	2	54	1	2	2	36	.25	.115	42	24	.55	143	.01	4	1.95	.01	.10	1
L19+00N 49+00W	1	30	32	43	.2	6	3	136	1.95	11	5	ND	1	21	1	2	2	20	.06	.082	24	14	.23	59	.01	3	1.12	.01	.07	1
L19+00N 48+50W	1	57	61	80	.2	11	7	256	3.07	20	5	ND	1	29	1	2	2	22	.05	.080	31	14	.35	83	.01	2	1.33	.01	.06	1
L19+00N 48+00W	1	133	66	112	2.9	23	15	218	3.41	16	5	ND	1	27	1	2	2	26	.08	.110	31	21	.44	103	.02	2	2.07	.01	.09	1
L19+00N 47+50W	1	28	42	42	.6	5	4	115	2.15	12	5	ND	1	25	1	2	2	19	.05	.070	32	11	.20	57	.01	2	1.44	.01	.04	1
L19+00N 47+00W	1	57	39	66	.8	14	6	151	3.62	20	5	ND	1	27	1	2	2	22	.02	.076	32	15	.27	80	.01	3	1.55	.01	.06	1
L19+00N 46+00W	2	63	33	144	1.0	17	11	167	3.17	13	5	ND	1	39	1	2	2	24	.10	.107	31	19	.41	177	.01	2	1.88	.01	.06	1
L19+00N 45+00W	1	24	52	51	.7	7	4	168	2.23	14	5	ND	1	40	1	2	2	24	.04	.104	33	15	.27	73	.01	3	1.06	.01	.05	1
L19+00N 44+50W	1	16	51	40	.4	8	3	102	2.03	14	5	ND	1	62	1	2	2	28	.07	.070	39	23	.41	61	.02	2	1.30	.01	.06	1
L19+00N 44+00W	1	31	102	94	.4	15	8	297	3.00	26	5	ND	1	128	1	2	2	41	.28	.090	49	30	.88	120	.04	2	1.82	.01	.10	1
L19+00N 43+50W	1	28	63	72	.3	10	7	292	2.68	18	5	ND	1	93	1	2	2	33	.13	.080	45	28	.61	122	.02	3	1.21	.01	.09	1
L19+00N 43+00W	1	16	38	42	.4	7	4	154	2.12	11	5	ND	1	49	1	2	2	30	.05	.059	41	20	.37	67	.02	2	1.14	.01	.06	1
L19+00N 42+50W	1	21	47	56	.1	7	5	280	2.34	9	5	ND	1	62	1	2	2	31	.11	.102	42	23	.49	82	.03	2	1.66	.01	.08	1
L19+00N 42+00W	1	17	37	67	.5	10	6	329	2.12	8	5	ND	1	83	1	2	2	33	.12	.093	45	33	.81	81	.02	5	1.97	.01	.08	1
L18+00N 52+00W	1	15	33	42	.6	5	4	270	2.14	10	5	ND	1	20	1	2	2	27	.03	.076	26	16	.32	52	.02	2	1.38	.01	.07	1
L18+00N 51+50W	1	15	35	38	.7	4	3	114	1.82	13	5	ND	1	19	1	2	3	26	.04	.083	29	17	.32	62	.02	3	1.61	.01	.06	1
L18+00N 51+00W	1	59	52	90	.9	19	9	355	3.61	35	5	ND	1	20	1	2	2	27	.02	.107	31	17	.31	83	.01	3	1.30	.01	.08	1
L18+00N 50+50W	1	59	54	80	.6	11	7	352	3.64	42	5	ND	1	20	1	2	2	30	.05	.092	28	18	.37	103	.01	4	1.71	.01	.08	1
L18+00N 50+00W	1	33	45	78	.4	9	7	497	2.98	24	5	ND	1	24	1	2	2	28	.05	.096	31	15	.29	156	.01	3	1.21	.01	.08	1
L18+00N 49+50W	1	46	53	60	.4	8	6	335	2.70	19	5	ND	1	24	1	2	2	25	.04	.089	30	15	.30	84	.01	2	1.18	.01	.07	1
STD C	20	62	37	132	7.4	67	28	1066	4.16	40	22	8	40	52	18	17	19	58	.49	.088	39	61	.92	178	.07	34	1.82	.06	.14	12

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	[illegible]	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L18+00N 47+50W	4	141	119	252	.1	30	16	664	3.88	32	5	ND	6	113	2	2	2	19	.37	.113	55	20	.67	106	.02	2	1.18	.01	.10	1
L18+00N 47+00W	2	40	52	51	.1	7	3	152	2.09	14	5	ND	1	21	1	2	2	16	.06	.081	23	10	.18	57	.01	2	1.11	.01	.04	1
L18+00N 46+50W	3	38	39	98	.1	11	6	373	2.32	14	5	ND	1	57	1	2	2	20	.20	.119	22	14	.26	104	.01	2	1.20	.01	.06	1
L18+00N 45+50W	2	28	53	46	.5	8	4	129	2.46	17	5	ND	1	27	1	2	3	26	.04	.066	27	16	.22	71	.01	3	.86	.01	.05	1
L18+00N 45+00W	3	24	61	42	.3	8	4	99	1.98	11	5	ND	1	39	1	2	3	25	.05	.054	30	18	.26	81	.02	2	.87	.01	.05	1
L18+00N 44+50W	2	17	51	47	.2	7	4	242	1.78	9	5	ND	1	34	1	2	2	23	.05	.068	31	17	.33	67	.01	12	1.14	.01	.05	1
L18+00N 44+00W	2	13	52	47	.2	7	4	151	1.83	8	5	ND	1	58	1	2	2	26	.09	.073	37	22	.41	56	.02	2	1.18	.01	.06	1
L18+00N 43+50W	2	15	48	43	.5	5	3	126	1.57	8	5	ND	1	34	1	2	2	24	.07	.065	27	17	.31	48	.02	3	1.26	.01	.05	1
L18+00N 43+00W	2	21	78	63	.3	9	5	187	2.21	13	5	ND	1	55	1	2	3	30	.08	.059	31	23	.55	64	.02	2	1.27	.01	.07	1
L18+00N 42+50W	2	19	65	59	.8	8	4	174	1.99	14	5	ND	1	55	1	2	3	25	.11	.074	33	19	.44	83	.01	2	1.02	.01	.07	1
L18+00N 42+00W	1	12	46	59	.3	9	4	174	1.58	5	5	ND	1	135	1	2	3	24	.45	.081	29	22	.52	153	.01	2	.96	.01	.08	1
STD C	20	62	39	132	7.7	69	29	1110	4.22	43	19	9	40	55	19	14	20	60	.51	.095	41	65	.94	181	.07	36	1.85	.07	.15	13

CERTIFICATE

I, Edwin Ross Rockel, Geophysicist of Vancouver, British Columbia, Canada, hereby certify that:

1. I received a B.Sc. degree in Geophysics from the University of British Columbia in 1966.

2. I am a Consulting Geophysicist and owner of Interpretex Resources Ltd. of Box 48239, Bentall P.O., in the City of Vancouver, in the Province of British Columbia.

3. I currently reside at 6571 Cooney Rd., in the City of Richmond, in the Province of British Columbia.

4. I have been practising my profession since graduation.

5. I am a Professional Geophysicist registered in the Province of Alberta.

6. I am a Professional Engineer registered in the Province of Saskatchewan.

7. I am a Certified Professional Geological Scientist registered in the United States of America.

8. This report may be used for the development of the property, provided that no portion will be used out of context in such a manner as to convey meanings different from that set out in the whole.

9. Consent is hereby given to the company for which this report was prepared to reproduce the report or any part of it for the purposes of development of the property, or facts relating to the raising of funds by way of a prospectus and/or statement of material facts.

Date: Dec. 11, 1987 Signed: [signature]

Vancouver,
British Columbia

Edwin Ross Rockel
B.Sc., P.Geoph., P. Eng.

APPENDIX B

CERTIFICATES OF ANALYSIS

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-4 SOIL P5-SILT P6-ROCK

DATE RECEIVED: OCT 5 1987 DATE REPORT MAILED: Oct 20/87 ASSAYER. D.Toye ..DEAN TOYE, CERTIFIED B.C. ASSAYER

GOLD SPRING RESOURCES File # 87-4749 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L36+00N 40+00W	1	11	28	33	.4	6	4	75	1.78	4	5	ND	1	52	1	2	2	30	.10	.055	31	23	.41	63	.03	2	1.37	.01	.05	1
L36+00N 39+50W	1	13	16	44	.2	11	5	169	1.85	3	5	ND	1	55	1	2	2	28	.15	.051	37	24	.49	118	.03	2	1.31	.01	.05	1
L36+00N 39+00W	1	13	18	41	.2	9	5	223	1.97	2	5	ND	1	50	1	2	2	32	.13	.040	33	22	.43	126	.03	3	1.55	.02	.05	1
L36+00N 38+50W	1	10	13	25	.3	5	3	48	1.36	2	5	ND	1	27	1	2	2	28	.10	.048	19	18	.18	57	.03	4	1.72	.02	.02	1
L36+00N 38+00W	1	14	13	39	.2	8	5	140	2.36	2	5	ND	1	69	1	2	2	36	.16	.036	39	23	.58	102	.04	5	1.48	.01	.06	1
L36+00N 37+50W	1	23	15	113	.3	8	5	377	1.88	2	6	ND	1	194	1	2	2	33	.49	.063	40	23	.65	206	.06	6	2.22	.02	.06	1
L36+00N 37+00W	1	8	13	48	.1	12	6	221	1.87	2	5	ND	1	144	1	2	3	34	.27	.051	38	26	.73	90	.07	4	1.37	.02	.08	1
L36+00N 36+50W	1	16	16	61	.2	9	6	252	1.96	6	5	ND	1	178	1	2	2	35	.42	.054	43	24	.76	127	.04	4	1.51	.02	.06	1
L36+00N 36+00W	1	15	29	48	.4	8	5	102	2.25	3	5	ND	1	74	1	2	2	34	.10	.035	36	20	.54	76	.05	2	1.25	.01	.05	1
L36+00N 35+50W	1	13	29	43	.6	6	3	83	1.63	3	5	ND	1	54	1	2	2	27	.12	.043	24	19	.35	47	.03	2	1.16	.01	.03	1
L36+00N 35+00W	1	9	29	55	.7	9	4	151	1.76	2	5	ND	1	97	1	2	2	32	.27	.053	32	21	.53	95	.03	2	1.12	.01	.06	1
L35+00N 40+00W	3	258	29	562	.2	14	8	375	2.52	13	22	ND	5	87	2	2	2	40	.16	.076	71	39	.76	74	.11	5	2.77	.02	.05	1
L35+00N 39+50W	2	30	36	95	.2	13	6	237	2.40	5	6	ND	1	134	1	2	2	38	.26	.050	45	33	.81	135	.05	2	1.63	.01	.07	1
L35+00N 39+00W	1	14	20	40	.3	8	3	125	1.83	2	5	ND	1	50	1	2	2	28	.12	.040	26	20	.31	78	.04	4	1.42	.01	.04	1
L35+00N 38+50W	2	66	40	239	.4	16	9	620	2.49	6	7	ND	1	302	3	2	2	32	.66	.102	47	30	.57	180	.04	7	2.37	.02	.06	1
L35+00N 38+00W	1	13	18	35	.2	7	3	95	1.53	4	5	ND	1	38	1	2	2	27	.06	.037	34	15	.29	76	.03	2	1.06	.01	.04	1
L35+00N 37+50W	1	10	17	42	.5	7	4	95	1.72	2	5	ND	1	34	1	2	2	27	.05	.037	33	16	.26	77	.03	3	.85	.01	.05	1
L35+00N 37+00W	1	17	13	52	.3	10	6	229	2.60	5	5	ND	1	95	1	2	2	37	.19	.071	49	24	.85	89	.03	3	1.35	.01	.09	1
L35+00N 36+50W	1	11	14	34	.2	5	4	88	1.58	4	5	ND	1	69	1	3	2	30	.09	.041	41	16	.48	68	.05	3	1.19	.01	.07	1
L35+00N 36+00W	1	11	16	42	.3	6	5	90	1.84	2	5	ND	1	63	1	2	3	32	.10	.039	40	20	.58	60	.05	4	1.46	.01	.06	1
L35+00N 35+50W	1	13	24	40	.1	7	5	201	1.99	4	5	ND	1	63	1	2	2	37	.10	.041	41	20	.69	60	.04	4	1.46	.01	.06	1
L35+00N 35+00W	1	31	26	69	.3	11	8	267	2.68	9	5	ND	1	89	1	2	2	35	.17	.060	44	22	.82	92	.04	3	1.64	.01	.09	1
L34+00N 40+00W	1	14	14	48	.2	12	8	472	2.18	2	5	ND	1	242	1	2	2	44	.32	.054	48	40	1.06	70	.08	2	1.69	.01	.09	1
L34+00N 39+50W	1	11	16	36	.1	8	4	103	1.64	2	5	ND	1	132	1	2	3	34	.15	.049	37	28	.56	48	.07	9	1.37	.02	.06	1
L34+00N 39+00W	1	9	14	32	.1	6	3	100	1.60	2	5	ND	1	85	1	2	2	33	.11	.036	32	21	.46	49	.06	5	1.18	.02	.05	1
L34+00N 38+50W	1	15	24	46	.3	9	5	164	1.88	2	5	ND	1	129	1	2	2	34	.14	.050	42	23	.59	69	.05	3	1.52	.01	.06	1
L34+00N 38+00W	1	12	21	44	.2	6	4	188	1.68	7	5	ND	1	94	1	2	2	30	.09	.040	38	17	.38	66	.04	2	1.15	.01	.05	1
L34+00N 37+50W	2	24	52	125	.3	11	7	453	2.84	26	5	ND	1	79	1	2	2	33	.15	.072	45	24	.57	82	.02	2	1.46	.01	.07	1
L34+00N 37+00W	1	26	76	333	.6	13	7	364	2.44	2	5	ND	1	263	5	2	3	42	.39	.049	53	30	.80	157	.05	5	1.65	.01	.07	1
L34+00N 36+50W	1	10	22	36	.2	6	3	101	2.01	3	5	ND	1	46	1	2	2	34	.05	.045	31	15	.30	72	.04	2	1.13	.01	.04	1
L34+00N 36+00W	1	25	22	64	.4	7	6	349	2.59	5	5	ND	1	131	1	2	2	37	.19	.058	43	21	.63	82	.05	6	1.57	.01	.10	1
L34+00N 35+50W	1	18	23	80	.4	7	5	145	2.10	8	5	ND	1	162	1	2	2	30	.36	.065	39	17	.50	83	.04	5	1.68	.01	.09	1
L34+00N 35+00W	2	20	52	57	.1	8	5	159	2.26	9	5	ND	1	99	1	2	2	31	.12	.061	47	19	.55	67	.04	11	1.24	.01	.07	1
L33+50N 40+00W	1	18	26	55	.1	12	7	261	2.28	7	5	ND	1	187	1	2	2	39	.26	.059	47	32	.95	75	.05	5	1.36	.01	.07	1
L33+50N 39+50W	1	18	21	61	.1	10	6	234	2.13	6	5	ND	1	144	1	2	4	42	.23	.056	51	33	.96	68	.04	2	1.57	.02	.06	1
L33+50N 39+00W	1	14	19	39	.1	8	5	220	2.01	2	5	ND	1	100	1	2	2	36	.21	.049	43	22	.58	68	.05	6	1.21	.02	.07	1
STD C	19	61	40	132	7.7	70	29	1077	4.10	41	23	8	39	53	19	18	20	60	.48	.088	40	61	.91	180	.07	35	1.89	.06	.15	13

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L33+50N 38+50W	2	17	18	38	.2	5	3	96	1.97	3	5	ND	1	90	1	2	2	28	.15	.058	34	16	.31	53	.03	2	.85	.02	.06	1
L33+50N 38+00W	1	14	23	42	.1	7	4	232	1.84	6	5	ND	1	130	1	2	2	35	.22	.062	43	24	.58	59	.05	3	1.06	.02	.08	1
L33+50N 37+50W	2	14	35	44	.5	5	3	116	1.67	12	5	ND	1	63	1	2	2	29	.09	.047	29	21	.32	43	.03	2	1.38	.02	.04	2
L33+50N 37+00W	2	17	47	99	.4	6	5	209	2.22	11	5	ND	1	73	1	2	2	31	.15	.056	40	20	.51	100	.03	5	1.23	.01	.05	1
L33+50N 36+50W	2	62	58	176	.7	6	4	224	1.86	11	7	ND	1	148	2	2	2	28	.23	.053	44	17	.40	101	.03	2	1.41	.01	.06	1
L33+50N 36+00W	2	20	33	72	.5	7	5	237	2.31	11	5	ND	1	75	1	2	2	31	.18	.075	35	19	.40	90	.02	2	1.02	.01	.08	1
L33+50N 35+50W	2	38	31	79	.7	10	7	213	2.64	10	5	ND	1	137	1	2	2	36	.30	.088	49	25	.86	71	.04	4	1.58	.01	.12	1
L33+50N 35+00W	1	22	20	57	.5	9	6	203	2.36	9	5	ND	1	165	1	2	2	36	.34	.083	44	21	.89	66	.05	3	1.49	.01	.09	2
L33+00N 40+00W	1	19	26	63	.1	10	7	221	2.65	12	5	ND	1	132	1	2	2	37	.27	.093	51	30	.93	53	.05	2	1.55	.01	.07	1
L33+00N 39+50W	2	15	18	50	.1	11	6	289	2.27	4	5	ND	2	85	1	2	2	36	.19	.051	40	34	.70	65	.06	2	1.68	.01	.05	2
L33+00N 39+00W	2	15	20	44	.2	8	5	180	2.15	5	5	ND	1	99	1	2	2	32	.16	.049	37	26	.67	62	.05	3	1.45	.01	.06	1
L33+00N 38+50W	1	17	32	71	.2	10	7	218	2.92	9	5	ND	2	177	1	2	2	39	.34	.056	42	31	.88	101	.07	2	1.70	.01	.08	1
L33+00N 38+00W	1	18	35	87	.1	9	6	269	2.35	8	5	ND	1	191	1	2	2	37	.30	.059	42	23	.74	112	.05	2	1.40	.01	.09	1
L33+00N 37+50W	2	14	55	70	.8	7	4	373	1.88	3	5	ND	1	115	1	2	2	31	.27	.119	36	21	.44	74	.04	2	1.11	.01	.08	1
L33+00N 37+00W	4	157	269	813	1.5	20	15	951	3.41	41	5	ND	3	165	4	2	2	33	.50	.138	70	24	.68	152	.05	5	2.50	.01	.10	2
L33+00N 36+50W	2	21	136	184	.4	8	5	238	2.34	9	5	ND	1	87	1	2	2	32	.18	.052	35	21	.45	86	.03	3	1.18	.01	.05	1
L33+00N 36+00W	3	28	87	174	.3	9	6	211	2.58	11	5	ND	1	60	1	2	2	32	.12	.065	47	20	.52	101	.02	2	1.16	.01	.07	1
L33+00N 35+50W	2	27	51	77	.5	8	4	145	2.39	8	5	ND	1	66	1	2	2	26	.14	.058	41	16	.44	92	.02	2	1.06	.01	.05	1
L33+00N 35+00W	2	18	43	48	.5	7	5	196	2.35	4	5	ND	1	67	1	2	2	31	.09	.056	37	19	.51	73	.03	3	1.33	.01	.06	1
L32+50N 40+00W	2	14	27	60	.2	14	6	244	1.96	4	5	ND	1	158	1	2	3	33	.21	.062	38	34	.90	64	.04	2	1.28	.01	.06	1
L32+50N 39+50W	2	15	20	55	.1	11	6	272	2.07	5	5	ND	1	137	1	2	2	42	.19	.057	41	37	.89	82	.04	6	1.34	.01	.07	1
L32+50N 39+00W	2	18	33	47	.2	10	4	171	1.87	7	5	ND	1	91	1	2	2	29	.14	.062	37	29	.61	56	.03	3	1.28	.01	.06	3
L32+50N 38+50W	2	14	20	49	.1	9	5	192	1.90	7	5	ND	1	107	1	2	2	33	.19	.057	38	25	.71	81	.03	4	1.08	.01	.08	2
L32+50N 38+00W	2	18	34	75	.1	11	7	427	2.40	9	5	ND	1	119	1	2	2	39	.29	.063	46	31	.86	118	.04	5	1.39	.01	.10	1
L32+50N 37+50W	2	18	22	103	.3	11	6	456	2.09	4	5	ND	1	181	1	2	2	38	.46	.184	40	28	.90	133	.04	3	1.31	.02	.14	1
L32+50N 37+00W	2	45	143	212	.7	14	8	347	2.59	10	5	ND	2	294	1	2	3	38	.44	.122	63	32	1.00	110	.06	4	1.83	.02	.11	1
L32+50N 36+50W	2	20	73	92	.3	8	5	247	2.03	8	5	ND	1	198	1	2	2	33	.25	.059	41	21	.56	84	.05	2	1.13	.01	.08	1
L32+50N 36+00W	2	26	80	124	.6	11	7	195	2.27	11	5	ND	1	95	1	2	2	31	.21	.067	46	24	.61	132	.02	5	1.10	.01	.06	1
L32+50N 35+50W	1	17	36	86	.3	9	6	262	2.29	5	5	ND	1	101	1	2	2	34	.26	.075	49	21	.93	142	.03	2	1.31	.01	.07	1
L32+50N 35+00W	1	17	63	40	.1	4	2	70	1.30	4	5	ND	1	46	1	2	2	19	.08	.048	31	12	.17	90	.02	2	.69	.01	.04	1
L28+50N 74+00W	2	29	28	47	.1	9	4	109	2.68	15	5	ND	1	19	1	2	2	52	.06	.028	17	21	.30	67	.07	2	1.44	.01	.04	3
L28+50N 73+75W	1	26	23	53	.5	10	6	178	3.23	6	5	ND	2	13	1	2	2	54	.15	.031	9	19	.22	54	.11	3	1.13	.01	.02	1
L28+50N 73+50W	2	59	29	89	.3	17	9	196	4.17	11	5	ND	2	30	1	2	2	57	.40	.047	19	29	.51	197	.07	2	1.98	.01	.05	1
L28+50N 73+25W	2	380	48	102	.6	30	13	713	3.31	26	5	ND	3	34	1	2	2	40	.70	.062	33	28	.48	250	.09	4	3.23	.02	.06	1
L28+50N 73+00W	2	165	60	128	.1	26	14	841	3.48	16	5	ND	2	39	1	2	2	46	.65	.069	28	32	.61	408	.04	2	2.01	.01	.06	2
L28+50N 72+75W	2	28	76	77	.3	12	6	177	3.11	11	5	ND	1	35	1	2	2	44	.17	.065	27	22	.47	180	.03	2	1.47	.01	.07	1
STD C	20	62	37	133	7.5	72	29	1070	4.15	38	18	8	40	52	19	17	19	59	.49	.092	40	63	.92	181	.07	34	1.81	.06	.14	12

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L28+50N 72+50W	1	27	109	87	.5	15	6	219	3.22	16	5	ND	1	38	1	2	3	57	.17	.103	26	27	.53	242	.03	2	1.78	.01	.08	1
L28+50N 72+25W	1	199	181	660	1.6	56	11	1275	3.34	12	5	ND	2	55	5	2	2	43	.77	.104	33	24	.54	511	.07	4	3.42	.02	.06	1
L28+50N 72+00W	1	117	275	1159	1.0	95	16	1072	4.13	26	5	ND	2	58	9	2	2	61	.49	.099	31	33	.70	887	.06	3	2.89	.01	.07	1
L28+50N 71+75W	1	39	175	411	.7	33	9	340	4.00	18	5	ND	1	29	2	2	2	58	.17	.052	22	24	.53	336	.06	2	2.24	.01	.05	1
L28+50N 71+50W	1	32	206	310	.6	21	10	487	4.65	16	5	ND	1	30	1	2	2	70	.15	.065	25	23	.60	254	.06	3	2.05	.01	.06	1
L28+50N 71+25W	1	33	64	363	.3	16	6	170	2.94	14	5	ND	1	22	4	2	2	43	.13	.035	25	16	.24	267	.06	2	1.50	.01	.04	1
L28+50N 71+00W	1	15	38	59	.1	6	4	105	3.05	12	5	ND	1	19	1	3	2	40	.08	.038	24	15	.29	71	.05	5	1.07	.01	.04	1
L28+50N 70+75W	1	10	60	48	.1	4	4	142	2.61	5	5	ND	1	14	1	3	2	32	.07	.025	15	13	.19	67	.05	2	1.05	.02	.02	1
L28+50N 70+50W	2	24	101	539	.3	16	8	462	2.79	10	5	ND	4	49	1	2	2	28	.35	.070	35	19	.46	214	.05	2	1.95	.01	.05	1
L28+50N 70+25W	2	94	299	2767	1.0	34	14	1582	4.33	11	5	ND	2	127	15	2	2	44	1.05	.104	25	29	.55	624	.06	3	3.49	.02	.05	5
L28+50N 70+00W	1	18	53	147	.4	7	5	1771	2.24	21	5	ND	1	26	1	2	3	24	.07	.070	38	15	.32	92	.02	2	1.26	.01	.08	1
L28+50N 52+00W	1	33	242	924	.4	19	13	344	4.41	19	5	ND	2	39	2	2	2	63	.20	.046	25	28	.62	323	.07	4	2.22	.01	.04	1
L19+00N 51+50W	1	17	67	131	1.3	7	4	122	2.34	20	5	ND	1	19	1	2	2	26	.05	.060	27	15	.25	87	.01	3	1.38	.01	.06	1
L19+00N 51+00W	1	27	60	55	.7	9	5	262	2.82	25	5	ND	1	15	1	2	2	30	.03	.066	28	17	.31	73	.01	2	1.55	.01	.07	1
L19+00N 50+50W	1	37	52	66	1.5	9	5	295	2.67	20	5	ND	1	19	1	2	2	26	.04	.083	23	16	.32	78	.01	2	1.38	.01	.07	1
L19+00N 50+00W	1	40	59	68	.3	10	6	234	3.01	23	5	ND	1	20	1	2	2	24	.04	.078	33	16	.34	69	.01	2	1.39	.01	.08	1
L19+00N 49+50W	1	93	84	123	.5	19	12	492	4.55	27	5	ND	2	54	1	2	2	36	.25	.115	42	24	.55	143	.01	4	1.95	.01	.10	1
L19+00N 49+00W	1	30	32	43	.2	6	3	136	1.95	11	5	ND	1	21	1	2	2	20	.06	.082	24	14	.23	59	.01	3	1.12	.01	.07	1
L19+00N 48+50W	1	57	61	80	.2	11	7	256	3.07	20	5	ND	1	29	1	2	2	22	.05	.080	31	14	.35	83	.01	2	1.33	.01	.06	1
L19+00N 48+00W	1	133	66	112	2.9	23	15	218	3.41	16	5	ND	1	27	1	2	2	26	.08	.110	31	21	.44	103	.02	2	2.07	.01	.09	1
L19+00N 47+50W	1	28	42	42	.6	5	4	115	2.15	12	5	ND	1	25	1	2	2	19	.05	.070	32	11	.20	57	.01	2	1.44	.01	.04	1
L19+00N 47+00W	1	57	39	66	.8	14	6	151	3.62	20	5	ND	1	27	1	2	2	22	.02	.076	32	15	.27	80	.01	3	1.55	.01	.06	1
L19+00N 46+00W	2	63	33	144	1.0	17	11	167	3.17	13	5	ND	1	39	1	2	2	24	.10	.107	31	19	.41	177	.01	2	1.88	.01	.06	1
L19+00N 45+00W	1	24	52	51	.7	7	4	168	2.23	14	5	ND	1	40	1	2	2	24	.04	.104	33	15	.27	73	.01	3	1.06	.01	.05	1
L19+00N 44+50W	1	16	51	40	.4	8	3	102	2.03	14	5	ND	1	62	1	2	2	28	.07	.070	39	23	.41	61	.02	2	1.30	.01	.06	1
L19+00N 44+00W	1	31	102	94	.4	15	8	297	3.00	26	5	ND	1	128	1	2	2	41	.28	.090	49	30	.88	120	.04	2	1.82	.01	.10	1
L19+00N 43+50W	1	28	63	72	.3	10	7	292	2.68	18	5	ND	1	93	1	2	2	33	.13	.080	45	28	.61	122	.02	3	1.21	.01	.09	1
L19+00N 43+00W	1	16	38	42	.4	7	4	154	2.12	11	5	ND	1	49	1	2	2	30	.05	.059	41	20	.37	67	.02	2	1.14	.01	.06	1
L19+00N 42+50W	1	21	47	56	.1	7	5	280	2.34	9	5	ND	1	62	1	2	2	31	.11	.102	42	23	.49	82	.03	2	1.66	.01	.08	1
L19+00N 42+00W	1	17	37	67	.5	10	6	329	2.12	8	5	ND	1	83	1	2	2	33	.12	.093	45	33	.81	81	.02	5	1.97	.01	.08	1
L18+00N 52+00W	1	15	33	42	.6	5	4	270	2.14	10	5	ND	1	20	1	2	2	27	.03	.076	26	16	.32	52	.02	2	1.38	.01	.07	1
L18+00N 51+50W	1	15	35	38	.7	4	3	114	1.82	13	5	ND	1	19	1	2	3	26	.04	.083	29	17	.32	62	.02	3	1.61	.01	.06	1
L18+00N 51+00W	1	59	52	90	.9	19	9	355	3.61	35	5	ND	1	20	1	2	2	27	.02	.107	31	17	.31	83	.01	3	1.30	.01	.08	1
L18+00N 50+50W	1	59	54	80	.6	11	7	352	3.64	42	5	ND	1	20	1	2	2	30	.05	.092	28	18	.37	103	.01	4	1.71	.01	.08	1
L18+00N 50+00W	1	33	45	78	.4	9	7	497	2.98	24	5	ND	1	24	1	2	2	28	.05	.096	31	15	.29	156	.01	3	1.21	.01	.08	1
L18+00N 49+50W	1	46	53	60	.4	8	6	335	2.70	19	5	ND	1	24	1	2	2	25	.04	.089	30	15	.30	84	.01	2	1.18	.01	.07	1
STD C	20	62	37	132	7.4	67	28	1066	4.16	40	22	8	40	52	18	17	19	58	.49	.088	39	61	.92	178	.07	34	1.82	.06	.14	12

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	[illegible]	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
L18+00N 47+50W	4	141	119	252	.1	30	16	664	3.88	32	5	ND	6	113	2	2	2	19	.37	.113	55	20	.67	106	.02	2	1.18	.01	.10	1
L18+00N 47+00W	2	40	52	51	.1	7	3	152	2.09	14	5	ND	1	21	1	2	2	16	.06	.081	23	10	.18	57	.01	2	1.11	.01	.04	1
L18+00N 46+50W	3	38	39	98	.1	11	6	373	2.32	14	5	ND	1	57	1	2	2	20	.20	.119	22	14	.26	104	.01	2	1.20	.01	.06	1
L18+00N 45+50W	2	28	53	46	.5	8	4	129	2.46	17	5	ND	1	27	1	2	3	26	.04	.066	27	16	.22	71	.01	3	.86	.01	.05	1
L18+00N 45+00W	3	24	61	42	.3	8	4	99	1.98	11	5	ND	1	39	1	2	3	25	.05	.054	30	18	.26	81	.02	2	.87	.01	.05	1
L18+00N 44+50W	2	17	51	47	.2	7	4	242	1.78	9	5	ND	1	34	1	2	2	23	.05	.068	31	17	.33	67	.01	12	1.14	.01	.05	1
L18+00N 44+00W	2	15	52	47	.2	7	4	151	1.83	8	5	ND	1	58	1	2	2	26	.09	.073	37	22	.41	56	.02	2	1.18	.01	.06	1
L18+00N 43+50W	2	15	48	43	.5	5	3	126	1.57	8	5	ND	1	34	1	2	2	24	.07	.065	27	17	.31	48	.02	3	1.26	.01	.05	1
L18+00N 43+00W	2	21	78	63	.3	9	5	187	2.21	13	5	ND	1	55	1	2	3	30	.08	.059	31	23	.55	64	.02	2	1.27	.01	.07	1
L18+00N 42+50W	2	19	65	59	.8	8	4	174	1.99	14	5	ND	1	55	1	2	3	25	.11	.074	33	19	.44	83	.01	2	1.02	.01	.07	1
L18+00N 42+00W	1	12	46	59	.3	9	4	174	1.58	5	5	ND	1	135	1	2	3	24	.45	.081	29	22	.52	153	.01	2	.96	.01	.08	1
STD C	20	62	39	132	7.7	69	29	1110	4.22	43	19	9	40	55	19	14	20	60	.51	.095	41	65	.94	181	.07	36	1.85	.07	.15	13

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Pulp AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: OCT 9 1987 DATE REPORT MAILED: Oct 16/87 ASSAYER. D. Toye. DEAN TOYE, CERTIFIED B.C. ASSAYER

GOLD SPRING RESOURCES File # 87-3961 R Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
L-39N 55+00W	2	29	31	91	.8	18	5	131	3.25	15	5	ND	4	52	1	3	2	33	.15	.050	37	25	.54	122	.03	2	1.53	.02	.08	1	-
L-39N 54+75W	1	21	32	86	2.1	17	4	96	2.64	9	5	ND	2	32	1	2	2	33	.15	.038	25	19	.28	147	.03	2	1.61	.02	.08	1	-
L-39N 54+25W	2	21	36	76	.8	12	3	111	3.11	30	5	ND	2	36	1	2	2	29	.20	.054	20	16	.22	124	.04	2	1.30	.03	.08	1	-
L-39N 54+00W	1	17	30	53	.8	10	3	76	2.25	18	5	ND	2	39	1	2	2	24	.15	.036	26	15	.22	62	.03	6	1.08	.02	.04	1	-
L-39N 53+75W	3	26	84	72	.5	15	3	67	2.83	63	5	ND	2	20	1	7	2	24	.05	.053	20	16	.10	46	.03	2	.80	.01	.03	1	-
L-39N 53+50W	2	29	48	105	.6	21	6	234	3.36	54	5	ND	3	36	1	3	2	34	.09	.055	33	23	.43	57	.04	2	1.39	.02	.05	1	-
L-39N 53+25W	1	11	29	50	.7	7	2	85	1.69	13	5	ND	2	52	1	2	2	26	.18	.037	29	14	.18	78	.03	2	1.06	.02	.04	2	-
L-39N 53+00W	1	13	20	35	.2	6	2	84	1.71	2	5	ND	2	16	1	2	2	27	.06	.037	30	16	.15	75	.04	4	.93	.02	.03	1	-
L-37N 55+00W	2	18	28	47	.5	10	3	71	3.42	11	5	ND	2	22	1	2	2	27	.09	.052	29	15	.17	56	.03	2	1.26	.01	.04	2	-
L-37N 54+75W	1	15	23	40	.7	10	3	73	2.67	11	5	ND	2	18	1	2	2	25	.03	.033	30	13	.12	59	.04	5	.94	.02	.03	1	-
L-37N 54+50W	2	17	26	59	1.0	15	4	87	4.12	13	5	ND	2	19	1	2	2	32	.07	.075	18	15	.14	41	.05	2	1.38	.02	.02	1	-
L-37N 54+25W	1	11	15	37	.7	6	2	35	1.73	2	5	ND	1	15	1	2	2	25	.08	.031	15	10	.06	55	.05	2	.93	.02	.02	2	-
L-37N 53+00W	3	28	83	108	1.1	20	4	218	3.14	99	5	ND	1	17	1	2	2	27	.05	.072	17	14	.11	78	.02	2	1.23	.02	.03	1	-
L-37N 52+75W	2	23	68	95	.5	15	5	241	2.86	50	5	ND	2	42	1	2	2	32	.16	.065	22	17	.29	83	.03	2	1.61	.02	.04	1	-
L-37N 52+50W	2	29	52	62	1.7	9	5	316	3.44	25	5	ND	4	49	1	2	2	20	.14	.151	46	10	.11	106	.01	4	.79	.02	.06	1	-
L-37N 52+25W	1	17	30	39	.7	8	4	129	2.48	13	5	ND	3	35	1	2	2	24	.09	.075	40	9	.08	107	.01	4	.71	.02	.03	1	-
L-37N 52+00W	2	45	37	108	.9	22	8	641	2.42	26	5	ND	2	65	1	2	2	28	.31	.089	31	18	.23	160	.03	3	1.65	.02	.04	1	-
L-37N 51+50W	1	12	24	35	.6	8	3	66	1.90	5	5	ND	2	69	1	2	2	28	.09	.048	38	18	.41	77	.03	5	1.17	.02	.05	1	-
L-37N 51+25W	1	16	37	47	.9	9	3	81	1.83	6	5	ND	3	80	1	2	2	27	.11	.051	42	19	.43	135	.04	5	1.29	.02	.06	1	-
L-37N 51+00W	1	37	51	81	1.0	18	7	217	2.69	9	5	ND	4	104	1	3	2	35	.19	.082	63	30	.83	409	.03	2	1.70	.02	.10	1	-
L-35N 55+00W	4	22	35	52	.5	10	3	67	2.50	10	5	ND	2	21	1	2	2	22	.05	.059	38	12	.16	86	.02	2	1.25	.02	.03	1	-
L-35N 54+75W	5	17	30	51	.6	10	3	73	2.99	12	5	ND	2	25	1	2	2	23	.07	.067	34	11	.17	57	.02	2	.96	.01	.03	1	-
L-35N 54+50W	14	35	52	93	1.8	18	4	92	3.80	35	5	ND	2	18	1	2	2	24	.02	.059	39	14	.14	58	.02	2	1.12	.01	.02	1	-
L-35N 52+50W	2	68	50	784	11.9	115	9	953	4.17	28	5	ND	2	65	8	4	2	25	.51	.098	21	18	.29	149	.08	2	4.62	.04	.05	1	11
L-35N 52+25W	2	88	69	660	7.6	103	8	1024	2.89	25	5	ND	2	100	7	6	2	22	.78	.092	18	21	.42	132	.11	7	3.30	.05	.04	1	7
L-35N 52+00W	3	49	118	399	1.5	52	12	674	3.66	80	5	ND	4	108	4	7	2	21	.63	.128	34	15	.47	139	.02	7	1.45	.02	.08	1	3
L-35N 51+50W	1	36	67	178	1.5	34	5	341	2.38	16	5	ND	2	57	1	2	2	19	.24	.124	36	14	.22	247	.04	2	2.93	.02	.03	1	4
L-35N 51+25W	1	30	48	53	.8	10	3	92	1.77	10	5	ND	2	25	1	3	2	23	.06	.067	37	16	.26	183	.03	2	1.68	.02	.04	1	-
L-35N 51+00W	1	14	26	43	.7	7	2	80	1.65	6	5	ND	2	71	1	2	2	25	.09	.051	39	17	.27	149	.03	2	1.00	.02	.04	1	-
L-34N 75+00W	2	19	48	51	.8	10	5	272	2.21	8	5	ND	2	49	1	2	2	35	.13	.083	33	21	.36	49	.06	2	1.26	.02	.03	2	-
L-34N 74+75W	1	25	83	62	1.0	12	6	278	2.86	15	5	ND	2	55	1	2	2	37	.20	.095	31	26	.42	64	.07	13	1.69	.02	.03	1	-
L-34N 74+50W	1	26	79	71	.9	14	9	320	3.40	14	5	ND	4	72	1	2	2	39	.31	.114	40	23	.59	73	.07	2	1.40	.02	.04	1	-
L-34N 74+25W	2	90	238	402	.5	41	14	726	3.82	17	5	ND	4	57	3	2	2	52	.23	.104	48	39	.85	451	.05	4	2.13	.02	.09	1	9
L-34N 74+00W	2	56	253	159	.9	27	13	602	3.64	19	5	ND	4	104	2	3	2	53	.64	.141	34	33	.83	780	.08	2	1.77	.03	.05	1	14
L-34N 73+75W	3	81	129	140	1.8	31	14	1195	3.34	10	5	ND	5	126	3	2	2	42	.85	.197	51	30	.75	705	.06	2	1.82	.03	.05	1	-
L-34N 73+50W	1	17	48	47	.5	10	5	108	2.46	8	5	ND	3	51	1	2	2	42	.14	.041	33	22	.41	105	.08	4	1.10	.02	.02	1	-
STD C	18	57	45	132	7.1	67	26	1032	3.93	40	16	7	37	49	17	17	19	55	.47	.088	36	57	.86	174	.08	32	1.81	.08	.11	11	-

SAMPLE#		CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU*
	.	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L-34N 73+25W	1	42	77	77	.5	24	12	349	3.67	9	5	ND	4	35	1	2	2	60	.26	.091	21	39	1.11	72	.07	2	1.49	.02	.03	1	-
L-34N 73+00W	4	43	198	112	.6	21	7	197	3.46	43	5	ND	2	62	1	5	2	59	.33	.146	21	28	.54	227	.05	2	1.06	.02	.03	1	-
L-34N 72+75W	1	19	41	54	.4	11	6	131	3.19	9	5	ND	2	27	1	2	2	71	.13	.034	16	21	.39	121	.11	2	1.24	.02	.02	1	-
L-34N 72+50W	2	17	46	71	.4	7	3	64	2.53	8	5	ND	3	35	1	2	2	44	.07	.023	26	16	.21	248	.08	3	1.13	.02	.02	1	-
L-34N 72+25W	4	21	68	83	.4	13	6	154	4.10	39	5	ND	7	36	1	4	2	58	.12	.080	23	25	.36	95	.09	2	1.03	.02	.04	1	-
L-34N 72+00W	2	21	59	102	.7	16	9	224	4.59	12	5	ND	3	32	1	2	2	67	.18	.078	24	33	.72	107	.08	2	1.59	.02	.03	1	-
L-34N 71+75W	2	23	35	71	.9	10	6	579	2.58	6	5	ND	3	65	1	2	2	35	.37	.056	29	17	.38	324	.08	6	1.10	.03	.04	1	-
L-34N 71+50W	2	74	96	497	.8	35	12	644	3.34	24	5	ND	5	92	5	2	2	39	.63	.113	43	22	.63	288	.06	2	1.75	.03	.06	1	54
L-34N 71+25W	2	102	145	1083	1.4	65	11	946	3.01	17	6	ND	3	102	9	2	2	35	.73	.118	48	26	.69	545	.04	2	2.13	.03	.08	1	1
L-34N 71+00W	2	71	44	251	1.3	29	10	903	2.83	10	5	ND	3	94	2	2	2	33	.60	.095	46	23	.64	349	.06	2	1.91	.03	.05	1	2
L-34N 70+75W	1	24	32	58	.3	10	6	99	2.87	12	5	ND	6	53	1	2	2	39	.11	.040	30	24	.36	143	.07	4	1.19	.02	.04	1	-
L-34N 70+50W	1	25	40	58	.6	9	5	102	3.45	10	5	ND	4	54	1	2	2	34	.14	.054	32	20	.38	110	.09	2	1.61	.02	.03	1	-
L-34N 70+25W	2	50	41	126	1.2	25	12	323	3.24	15	8	ND	7	105	1	3	2	33	.52	.118	51	27	.80	197	.05	10	1.99	.03	.08	1	-
L-34N 70+00W	2	40	39	223	1.4	19	9	543	2.60	6	5	ND	2	103	1	2	2	34	.54	.075	49	22	.58	420	.04	8	2.64	.03	.10	1	-
L-33N 53+75W	14	18	77	34	.7	5	2	156	2.49	14	5	ND	4	28	1	3	2	26	.02	.047	95	9	.09	69	.02	6	1.27	.02	.03	1	-
L-33N 53+50W	8	20	79	43	.7	9	2	82	2.93	28	5	ND	2	13	1	2	2	23	.03	.051	26	7	.06	30	.01	2	.98	.01	.02	1	-
L-33N 53+00W	4	21	25	67	1.2	24	3	120	3.23	22	5	ND	1	5	1	2	2	17	.01	.033	13	7	.04	40	.02	2	.98	.01	.02	1	-
L-33N 52+75W	3	17	27	36	1.7	10	2	32	2.08	12	5	ND	1	5	1	2	2	18	.01	.033	14	8	.03	38	.02	2	1.02	.01	.02	1	-
L-33N 52+50W	6	20	34	77	1.1	21	4	73	3.08	12	5	ND	1	16	1	2	2	21	.07	.035	15	7	.05	53	.02	2	.83	.01	.02	1	-
L-33N 51+50W	2	14	24	39	1.1	7	2	83	1.79	5	5	ND	1	6	1	2	2	17	.01	.056	12	7	.05	45	.02	2	1.24	.01	.02	1	-
L-33N 51+25W	3	28	110	76	1.0	12	4	207	2.60	23	5	ND	1	18	1	3	2	24	.05	.074	26	13	.20	75	.01	3	1.18	.01	.04	1	-
L-33N 51+00W	1	14	35	38	.8	7	2	109	1.54	8	5	ND	2	17	1	2	2	20	.04	.079	30	14	.32	65	.01	8	1.17	.02	.05	2	-
L-33N 50+50W	2	32	54	70	1.1	14	6	301	2.39	15	5	ND	2	41	1	2	2	24	.17	.123	40	19	.48	157	.01	2	1.22	.02	.07	1	-
L-33N 50+25W	2	26	59	54	.8	9	3	146	2.48	8	5	ND	3	22	1	3	2	24	.04	.060	32	17	.25	117	.02	3	1.49	.01	.04	1	-
L-33N 50+00W	1	19	29	45	.7	10	3	91	1.87	7	5	ND	2	24	1	2	2	22	.05	.060	28	17	.33	162	.02	2	1.33	.02	.04	2	-
L-33N 49+75W	1	16	21	39	.4	8	3	103	1.89	7	5	ND	2	54	1	2	2	27	.10	.051	33	16	.37	146	.02	2	1.09	.02	.04	1	-
L-33N 49+50W	1	14	24	60	.5	10	3	567	1.86	3	5	ND	2	114	1	2	2	29	.23	.068	34	19	.66	140	.03	2	1.13	.02	.06	1	-
L-33N 49+25W	1	16	31	69	.5	10	6	233	2.11	6	5	ND	3	83	1	3	2	30	.17	.066	41	20	.64	222	.04	2	1.65	.02	.06	1	-
L-33N 49+00W	2	37	44	72	.5	15	10	440	2.56	10	5	ND	4	59	1	2	2	27	.13	.080	45	22	.68	97	.02	2	1.44	.02	.08	1	-
L-32N 75+00W	2	28	51	105	.6	15	9	188	3.96	17	5	ND	6	73	1	2	2	44	.18	.056	36	26	.65	113	.09	2	1.77	.02	.06	1	-
L-32N 74+75W	2	81	57	138	2.1	19	8	182	3.09	10	5	ND	4	62	1	2	2	40	.42	.065	49	31	.53	659	.05	2	2.10	.02	.08	1	1
L-32N 74+50W	1	72	49	99	1.7	14	5	105	2.87	6	5	ND	2	31	1	2	2	39	.26	.042	41	20	.26	544	.05	2	1.64	.02	.05	1	-
L-32N 74+25W	1	27	32	62	.3	10	3	78	2.18	8	5	ND	3	43	1	2	2	35	.23	.026	25	18	.25	274	.06	4	.95	.02	.07	1	-
L-32N 74+00W	2	99	66	117	.6	27	12	541	2.92	17	6	ND	8	90	1	2	2	31	.77	.125	55	30	.77	585	.05	3	1.77	.03	.11	1	-
L-32N 73+75W	2	42	73	107	1.0	23	10	196	3.11	16	7	ND	10	94	1	2	2	35	.37	.100	49	33	.89	207	.04	8	1.73	.02	.11	1	-
L-32N 73+25W	2	85	270	641	.8	54	14	808	3.57	19	6	ND	3	71	5	3	2	49	.66	.111	37	36	.85	778	.04	3	2.07	.03	.09	1	12
STD C	18	58	42	132	7.1	68	27	1024	3.92	37	23	8	37	49	18	16	20	58	.47	.088	38	59	.86	174	.07	36	1.82	.06	.15	12	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
L-32N 73+00W	2	36	73	85	.5	16	8	210	3.55	21	5	ND	7	81	1	2	2	41	.31	.084	44	23	.56	87	.08	2	1.13	.02	.07	1	-
L-32N 72+75W	1	18	40	50	.6	9	4	105	2.09	5	5	ND	3	64	1	2	2	39	.31	.036	35	16	.31	154	.09	5	.93	.02	.04	1	-
L-32N 72+50W	1	12	45	40	.4	6	3	114	3.27	9	5	ND	2	36	1	2	2	47	.19	.057	19	16	.24	74	.09	2	1.25	.02	.03	2	-
L-32N 72+25W	2	18	42	67	.1	10	6	211	3.87	11	5	ND	3	48	1	2	2	68	.23	.052	22	17	.49	98	.11	2	1.04	.02	.04	1	-
L-32N 72+00W	3	42	107	413	.8	33	7	370	2.50	14	5	ND	4	80	2	2	2	44	.58	.108	47	24	.61	536	.05	2	1.91	.03	.08	2	1
L-32N 71+00W	1	12	28	47	.4	5	3	75	1.90	8	5	ND	2	31	1	2	2	41	.13	.028	21	12	.28	74	.08	2	.85	.02	.03	2	-
L-32N 70+75W	1	12	24	41	.2	6	4	75	1.89	4	5	ND	1	17	1	2	2	74	.12	.027	12	10	.18	49	.10	2	.55	.02	.03	1	-
L-32N 70+50W	1	7	31	25	.3	4	2	61	1.59	4	5	ND	1	11	1	2	2	63	.11	.023	5	8	.09	43	.12	2	.44	.02	.03	1	-
L-32N 70+25W	1	11	23	51	.3	7	4	221	2.49	6	5	ND	1	20	1	2	2	79	.23	.021	11	12	.23	81	.12	2	.92	.02	.03	2	-
L-32N 70+00W	1	163	249	332	.9	52	17	886	4.43	25	5	ND	6	51	2	2	2	71	.53	.075	32	31	.74	270	.08	3	2.43	.03	.11	1	1
L-31N 55+00W	4	34	418	246	.6	23	11	758	4.18	11	5	ND	4	19	1	2	2	27	.15	.072	27	17	.27	111	.03	2	2.51	.02	.04	1	12
L-31N 54+50W	2	20	183	123	.4	15	8	444	3.09	6	5	ND	2	24	1	2	2	31	.19	.048	19	14	.25	109	.05	2	2.39	.02	.04	1	1
L-31N 54+25W	1	27	134	70	.7	12	4	190	2.18	3	5	ND	2	20	1	2	2	24	.20	.050	19	15	.19	195	.04	2	2.63	.02	.03	2	-
L-31N 53+75W	2	31	82	73	.5	19	7	196	3.39	9	5	ND	4	18	1	2	2	31	.07	.040	29	20	.23	248	.03	3	2.31	.02	.06	1	-
L-31N 53+50W	7	40	153	118	.3	28	6	376	4.11	24	5	ND	3	19	1	2	2	28	.14	.043	23	13	.13	244	.03	2	1.44	.01	.04	1	-
L-31N 53+25W	3	17	40	66	.2	12	5	719	2.72	7	5	ND	2	14	1	2	2	29	.08	.044	19	9	.11	111	.03	2	1.17	.02	.04	1	-
L-31N 53+00W	2	20	37	62	.4	12	5	268	3.76	7	5	ND	3	7	1	2	2	26	.03	.045	27	13	.14	65	.03	2	2.12	.01	.03	1	-
L-31N 52+75W	2	45	58	58	1.4	12	4	465	1.94	9	5	ND	1	32	1	2	2	21	.21	.077	19	9	.15	94	.04	2	2.70	.03	.03	1	-
L-31N 52+50W	3	14	42	50	.5	5	2	170	2.57	3	5	ND	2	11	1	2	2	26	.04	.046	26	7	.08	102	.02	2	.93	.01	.04	1	-
L-31N 52+25W	5	16	67	50	.5	7	3	256	2.74	10	5	ND	2	9	1	2	2	28	.02	.039	25	11	.12	51	.03	2	1.54	.02	.03	2	-
L-31N 51+50W	7	23	36	93	1.0	22	4	87	4.01	18	5	ND	2	14	1	2	2	23	.04	.048	19	10	.08	56	.02	2	1.07	.01	.02	1	-
L-31N 51+00W	2	29	45	87	.8	16	6	254	2.58	19	5	ND	2	22	1	2	2	25	.03	.078	23	12	.16	77	.01	2	1.15	.01	.05	1	-
L-31N 50+50W	2	19	54	50	.7	8	2	44	2.37	21	5	ND	1	9	1	2	2	20	.01	.055	18	10	.07	68	.02	2	1.28	.01	.02	2	-
L-31N 50+25W	3	23	84	69	1.0	11	3	81	2.98	43	5	ND	2	20	1	3	2	18	.06	.058	25	12	.17	68	.02	2	1.12	.01	.04	1	-
L-31N 50+00W	2	24	104	53	1.5	7	2	56	1.86	20	5	ND	3	21	1	3	2	19	.05	.058	33	14	.23	76	.01	3	1.60	.02	.05	1	-
L-31N 49+75W	2	27	60	63	.4	13	4	159	2.56	17	5	ND	3	27	1	3	2	28	.05	.053	35	16	.28	98	.02	3	1.11	.02	.06	1	-
L-31N 49+50W	1	26	64	69	.5	13	5	458	2.38	16	5	ND	4	34	1	2	2	27	.07	.067	47	23	.46	124	.02	3	1.45	.02	.07	1	-
L-31N 49+25W	1	16	49	54	1.0	8	3	116	2.11	23	5	ND	2	27	1	2	2	20	.05	.069	32	15	.25	74	.01	2	1.22	.01	.05	1	-
L-31N 49+00W	1	13	27	54	.6	7	3	240	1.72	8	5	ND	2	19	1	2	2	28	.05	.071	25	13	.23	59	.02	5	1.43	.02	.05	1	-
L-30N 75+00W	1	10	11	29	.2	5	2	70	1.23	2	5	ND	1	9	1	3	2	42	.06	.017	7	14	.08	34	.11	2	.41	.02	.03	1	-
L-30N 74+75W	1	33	31	78	.4	16	9	412	5.18	21	5	ND	1	13	1	2	2	82	.15	.066	7	34	.66	62	.09	3	1.59	.02	.05	1	-
L-30N 74+50W	1	12	14	37	.2	6	3	102	1.78	2	5	ND	1	11	1	2	2	61	.11	.027	8	20	.19	53	.11	2	.60	.02	.03	2	-
L-30N 74+25W	1	14	20	35	.3	7	3	105	2.24	6	5	ND	1	25	1	2	2	49	.11	.035	15	14	.21	71	.08	2	.72	.02	.04	2	-
L-30N 74+00W	1	16	24	33	.2	6	3	105	1.78	5	5	ND	2	31	1	2	2	43	.18	.024	20	13	.17	94	.08	2	.87	.02	.02	1	-
L-30N 73+75W	1	14	28	32	.3	6	3	77	1.71	3	5	ND	2	30	1	2	2	41	.14	.032	18	17	.21	102	.07	2	.83	.02	.04	1	-
L-30N 73+50W	1	137	60	111	.5	22	10	1148	3.03	10	5	ND	2	45	1	2	2	43	.86	.078	29	28	.54	683	.05	2	2.66	.03	.09	1	-
STD C	18	57	44	132	7.1	67	26	1031	3.95	38	24	7	37	48	17	15	18	55	.47	.087	36	58	.87	173	.08	32	1.82	.08	.12	11	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	Pro	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
L-30N 73+25W	1	11	12	26	.3	5	2	64	1.20	2	5	ND	3	40	1	2	2	28	.09	.020	26	11	.12	81	.05	9	.75	.02	.06	1	-
L-30N 73+00W	1	43	50	95	.6	19	9	316	2.73	12	5	ND	12	95	1	2	2	30	.34	.117	65	28	.82	127	.05	4	1.64	.02	.18	1	-
L-30N 72+75W	3	64	53	206	3.0	27	9	794	3.32	8	9	ND	4	103	2	2	2	45	.90	.097	53	37	.60	805	.05	4	3.71	.04	.23	2	1
L-30N 72+50W	1	22	38	79	.5	12	5	223	2.35	6	5	ND	3	57	1	2	2	38	.18	.064	37	24	.51	231	.05	3	1.48	.02	.17	1	-
L-30N 72+25W	1	11	23	40	.4	7	3	86	1.45	2	5	ND	3	64	1	2	2	29	.12	.034	36	18	.33	126	.05	3	.99	.02	.09	1	-
L-30N 72+00W	1	11	26	43	.5	7	3	101	1.70	3	5	ND	3	57	1	2	2	30	.10	.047	33	17	.34	91	.04	2	1.10	.02	.10	2	-
L-30N 71+75W	1	19	34	92	.7	13	5	201	2.65	7	5	ND	4	86	1	2	2	31	.27	.066	43	26	.72	228	.04	2	1.60	.02	.14	1	-
L-30N 71+50W	1	8	41	47	.3	4	2	149	1.41	2	5	ND	1	21	1	2	2	37	.13	.035	12	15	.21	80	.07	9	.81	.02	.04	1	-
L-30N 71+25W	3	75	173	648	.4	56	10	669	3.03	18	6	ND	5	76	4	2	2	54	.34	.139	73	29	.75	492	.05	12	2.20	.03	.11	1	41
L-30N 71+00W	1	14	57	63	.4	7	4	132	2.28	3	5	ND	3	20	1	2	2	53	.08	.046	14	16	.25	111	.14	3	.85	.03	.02	1	-
L-28+50N 37+00W	1	16	42	78	.5	8	6	419	2.33	12	5	ND	3	115	1	2	2	39	.14	.052	40	20	.49	140	.06	2	1.15	.02	.06	1	-
L-28+50N 36+75W	1	49	74	516	.9	12	8	488	2.54	56	12	ND	4	357	7	2	2	33	.62	.084	47	23	.58	309	.05	2	1.81	.03	.06	2	1
L-28+50N 36+50W	2	57	76	1373	.8	22	13	833	2.66	19	18	ND	4	307	7	2	2	40	.44	.092	67	24	.62	205	.06	2	1.95	.03	.06	1	1
L-28+50N 36+25W	1	20	66	210	.7	10	5	172	2.54	33	5	ND	4	143	1	2	2	37	.20	.054	46	23	.54	102	.05	2	1.42	.02	.05	1	-
L-28+50N 36+00W	2	20	69	278	.6	9	4	239	2.38	31	5	ND	3	109	1	2	2	35	.14	.063	34	21	.41	90	.05	2	1.48	.02	.06	1	-
L-28+50N 35+75W	1	20	86	97	.5	7	4	166	2.17	44	5	ND	3	81	1	2	2	28	.14	.065	37	17	.32	68	.04	4	1.15	.02	.06	1	-
L-28+50N 35+50W	1	317	101	594	1.5	32	25	1264	2.07	24	26	ND	2	461	7	2	2	27	.38	.095	131	17	.35	160	.04	3	1.70	.04	.04	1	2
L-28+50N 35+25W	1	31	60	68	.6	6	4	109	2.33	28	5	ND	3	68	1	2	2	27	.06	.040	35	12	.18	68	.04	2	1.08	.02	.03	1	-
L-28+50N 35+00W	2	33	109	116	.5	11	6	125	3.06	34	5	ND	4	123	1	2	2	32	.11	.063	52	16	.35	93	.04	2	1.14	.02	.05	1	-
L-27+50N 43+00W	1	16	31	60	.4	10	4	145	2.26	10	5	ND	3	137	1	2	2	37	.15	.062	45	26	.46	86	.04	7	1.17	.02	.08	1	-
L-27+50N 42+75W	1	13	27	51	.7	7	3	151	1.66	8	5	ND	3	133	1	2	2	34	.16	.066	40	20	.39	62	.04	5	1.03	.02	.07	1	-
L-27+50N 42+50W	1	19	78	76	.6	8	4	204	1.98	6	5	ND	3	130	1	2	2	33	.17	.076	41	23	.40	52	.03	2	1.38	.02	.06	1	-
L-27+50N 42+25W	1	37	49	95	.6	12	7	293	2.82	10	6	ND	5	159	1	2	2	38	.23	.073	52	28	.71	81	.07	7	2.04	.02	.09	1	-
L-27+50N 42+00W	1	14	30	61	.4	8	4	131	1.71	4	5	ND	3	148	1	2	2	30	.16	.074	38	20	.45	85	.03	2	1.23	.02	.07	1	-
L-27+50N 41+75W	1	19	31	60	.3	11	6	276	2.33	8	5	ND	4	165	1	2	2	35	.17	.058	47	24	.63	91	.05	7	1.51	.02	.08	1	-
L-27+50N 41+50W	2	61	142	831	1.2	14	8	399	2.67	20	6	ND	5	215	27	2	2	33	.23	.070	59	26	.68	149	.05	2	1.65	.02	.11	1	-
L-27+50N 41+25W	2	126	516	391	2.0	17	15	692	3.12	34	16	ND	10	386	4	5	2	31	.29	.090	87	27	.76	186	.04	3	1.62	.02	.17	1	126
L-27+50N 41+00W	1	28	44	103	.6	13	8	305	2.74	8	7	ND	5	272	1	2	2	38	.26	.066	55	27	.80	128	.06	8	1.90	.03	.11	1	-
L-27+50N 40+75W	1	38	176	303	1.0	16	11	763	3.23	24	7	ND	6	257	2	2	2	35	.33	.081	65	27	.76	210	.04	6	2.04	.03	.11	1	-
L-27+50N 40+50W	2	150	3696	1121	8.4	16	9	710	3.40	57	5	ND	6	200	3	9	2	38	.29	.108	59	28	.73	89	.06	2	1.81	.02	.10	2	19
L-27+50N 40+25W	1	67	1167	731	3.6	14	8	521	2.59	19	5	ND	5	205	2	3	2	37	.28	.082	57	28	.80	103	.06	2	1.90	.02	.10	1	1
L-27+50N 40+00W	1	45	694	860	1.6	12	7	436	2.90	23	5	ND	5	161	2	2	2	36	.22	.076	56	25	.62	95	.05	11	2.14	.02	.09	2	1
L-27+50N 39+75W	1	15	98	148	.9	8	5	417	1.86	13	5	ND	3	134	1	2	2	31	.16	.073	36	19	.41	66	.04	2	1.43	.02	.06	1	-
L-27+50N 39+50W	1	15	85	148	1.9	9	6	518	2.18	20	5	ND	3	149	1	2	2	35	.15	.067	42	21	.50	58	.05	8	1.39	.02	.07	1	-
L-27+50N 39+25W	1	26	95	417	.8	11	7	383	2.37	42	5	ND	4	200	3	2	2	35	.26	.059	47	23	.60	111	.06	2	1.56	.02	.07	1	-
L-27+50N 39+00W	1	32	88	569	.6	13	6	271	2.09	23	6	ND	4	172	5	2	2	33	.25	.076	45	26	.60	123	.06	2	1.93	.03	.06	1	2
STD C	18	58	40	132	7.1	68	27	1023	3.98	38	18	7	38	49	18	18	21	58	.48	.087	38	58	.88	175	.08	36	1.84	.06	.15	12	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	Ppm	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
L-27+50N 38+75W	1	68	140	1802	.7	20	11	1159	2.86	56	18	ND	7	277	14	5	2	36	.47	.108	53	33	1.01	190	.06	4	2.80	.03	.08	1	-
L-27+50N 38+25W	1	32	186	666	.9	12	7	285	2.82	108	5	ND	5	234	4	3	2	39	.34	.054	42	28	.67	187	.08	4	2.20	.03	.06	1	-
L-27+50N 38+00W	1	26	349	427	1.3	10	7	386	2.61	146	6	ND	4	177	2	2	2	35	.27	.071	46	22	.65	96	.06	2	1.55	.02	.09	1	-
L-27+50N 37+75W	1	32	118	165	.9	11	8	354	2.40	43	5	ND	5	150	1	2	2	31	.28	.096	52	22	.68	68	.05	13	1.50	.02	.08	1	-
L-27+50N 37+50W	1	21	194	52	3.5	4	2	55	1.73	18	5	ND	3	41	1	2	2	23	.06	.050	34	12	.18	66	.02	2	1.43	.02	.05	1	1
L-27+50N 37+25W	1	9	42	38	.6	5	3	115	1.87	6	5	ND	2	62	1	2	2	30	.08	.044	28	16	.29	42	.05	2	1.22	.02	.05	2	-
L-27+50N 37+00W	1	19	51	68	1.4	10	5	157	2.26	12	5	ND	4	141	1	2	2	33	.24	.085	48	25	.76	74	.05	2	1.57	.02	.07	1	-
L-27+50N 36+75W	9	22	481	57	4.4	7	3	116	1.99	19	5	ND	3	120	1	2	39	29	.18	.105	44	19	.40	58	.02	2	1.27	.02	.07	1	1
L-27+50N 36+50W	1	19	46	64	.6	11	5	140	2.27	12	5	ND	3	117	1	2	2	34	.19	.069	45	32	.73	71	.04	2	1.70	.02	.08	1	-
L-27+50N 36+25W	1	37	37	66	.7	13	7	233	2.62	17	5	ND	4	204	1	2	2	35	.30	.073	49	27	.95	74	.07	4	1.56	.02	.13	1	-
L-27+50N 36+00W	1	23	47	97	1.7	10	6	286	2.99	19	5	ND	3	145	1	2	2	34	.21	.070	43	25	.66	96	.04	2	1.40	.02	.09	1	-
L-27+50N 35+75W	2	14	43	99	.7	9	4	257	1.99	9	5	ND	3	154	1	2	2	33	.20	.057	37	23	.56	111	.06	2	1.34	.02	.07	1	-
L-27+50N 35+50W	2	32	105	150	.6	10	6	267	2.83	14	5	ND	4	158	1	2	2	38	.21	.058	46	26	.63	107	.07	8	1.29	.02	.08	1	-
L-27+50N 35+25W	2	44	328	235	.8	15	7	219	2.79	13	5	ND	4	233	2	2	2	38	.40	.080	43	31	.66	164	.06	2	1.49	.03	.07	1	-
L-27+50N 35+00W	1	21	113	90	1.6	6	3	73	1.66	10	5	ND	3	76	1	2	2	27	.11	.050	36	16	.36	55	.04	2	1.10	.02	.06	1	-
L-27+00N 72+50W	3	122	83	106	.6	14	9	1939	2.62	6	5	ND	2	36	1	2	2	47	.65	.077	45	19	.34	738	.06	2	2.08	.03	.05	1	-
L-27+00N 72+25W	1	13	34	49	.1	7	3	97	2.63	6	5	ND	1	22	1	2	2	53	.14	.032	17	13	.22	156	.10	2	.90	.02	.05	1	-
L-27+00N 72+00W	1	31	54	73	.2	12	6	203	2.72	6	5	ND	3	22	1	3	2	55	.12	.030	19	20	.39	379	.08	4	1.20	.02	.06	1	-
L-27+00N 71+75W	2	87	175	381	1.9	31	5	166	2.63	12	5	ND	2	40	3	3	2	41	.40	.057	20	19	.35	399	.08	2	2.41	.03	.05	1	2
L-27+00N 71+50W	2	14	42	37	.3	5	1	35	1.08	3	5	ND	1	12	1	2	2	33	.05	.013	14	8	.05	70	.08	2	.57	.02	.02	1	-
L-27+00N 71+25W	2	24	55	52	.3	11	3	65	2.94	7	5	ND	2	19	1	2	2	58	.06	.039	17	17	.18	92	.06	3	.94	.02	.03	1	-
L-27+00N 71+00W	14	87	62	380	.7	59	9	770	3.35	33	5	ND	1	50	4	2	2	52	.31	.056	21	22	.34	462	.05	3	1.62	.03	.05	1	-
L-27+00N 70+75W	8	111	110	311	2.2	65	6	210	2.28	65	25	ND	2	87	3	2	2	58	.58	.085	54	20	.30	898	.04	4	1.95	.03	.04	1	3
L-27+00N 70+50W	6	118	504	1313	2.4	107	11	1269	3.53	45	11	ND	3	128	7	2	2	50	1.02	.121	38	25	.60	699	.05	11	2.72	.04	.10	1	14
L-27+00N 70+25W	3	24	294	184	.8	14	6	439	3.73	7	5	ND	2	32	1	3	2	62	.15	.050	18	21	.48	230	.08	2	1.37	.02	.05	1	-
L-27+00N 70+00W	1	11	88	71	.2	7	3	115	1.92	5	5	ND	2	24	1	2	2	42	.10	.035	19	17	.27	135	.07	2	1.08	.02	.04	1	-
L-25+50N 52+00W	1	31	40	132	.8	17	6	354	2.67	5	5	ND	3	78	1	2	2	30	.75	.105	24	15	.34	193	.05	2	2.52	.04	.06	1	-
L-25+50N 51+75W	1	28	50	121	.7	15	7	432	2.78	5	5	ND	3	51	1	2	2	29	.46	.098	23	17	.35	264	.04	2	2.62	.03	.06	1	-
L-25+50N 51+50W	2	22	49	48	.7	7	2	74	2.34	5	5	ND	2	20	1	2	2	23	.04	.055	24	11	.16	86	.02	2	1.29	.01	.04	1	-
L-25+50N 51+25W	2	25	49	123	.6	18	6	1043	2.48	8	5	ND	2	67	2	2	2	30	.35	.143	25	16	.37	234	.02	2	1.59	.03	.09	1	-
L-25+50N 51+00W	3	64	41	162	1.1	24	7	688	2.97	7	5	ND	2	81	1	2	2	39	.76	.141	25	16	.45	180	.04	2	1.85	.04	.08	1	-
L-25+50N 50+75W	3	49	45	73	1.8	11	3	101	2.06	5	5	ND	2	39	1	2	2	27	.31	.089	26	15	.27	132	.02	2	1.73	.02	.06	1	1
L-25+50N 50+50W	2	40	49	51	.5	8	3	110	2.41	9	5	ND	2	19	1	2	2	24	.07	.057	28	11	.17	59	.02	14	1.12	.02	.06	2	-
L-25+50N 50+25W	3	35	53	62	.4	12	4	200	3.33	12	5	ND	3	17	1	2	2	27	.02	.061	30	14	.18	67	.02	2	1.14	.01	.05	1	-
L-25+50N 50+00W	2	40	35	50	.4	9	3	195	2.19	7	5	ND	2	21	1	2	2	22	.08	.073	29	13	.19	60	.01	2	.89	.01	.05	1	-
L-25+50N 49+75W	2	35	30	50	.8	7	3	169	1.92	6	5	ND	3	21	1	2	2	20	.06	.074	35	12	.18	66	.01	6	1.19	.02	.06	1	-
STD C	17	57	43	132	7.2	68	26	1031	3.96	35	25	7	38	49	18	18	21	55	.48	.087	36	61	.87	175	.08	31	1.82	.07	.13	12	-

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L-25+50N 49+50W	3	134	73	215	2.6	41	23	1159	3.44	12	15	ND	4	129	1	2	2	24	.67	.147	31	17	.38	171	.05	2	3.43	.03	.06	1	4
L-25+50N 49+25W	3	139	1372	291	1.3	42	44	741	14.76	13	24	ND	10	119	2	2	2	11	.30	.119	83	16	.18	90	.02	6	3.52	.02	.03	5	2
L-25+50N 49+00W	2	33	133	63	2.1	10	6	111	2.53	9	5	ND	2	21	1	2	2	18	.05	.079	24	10	.16	78	.01	2	1.25	.01	.03	1	1
L-25+50N 48+75W	2	23	41	36	1.4	6	2	45	2.02	6	5	ND	1	12	1	2	2	20	.02	.052	18	11	.12	55	.01	2	1.03	.01	.03	1	-
L-25+50N 48+50W	3	26	32	45	.9	9	2	44	2.25	10	5	ND	1	11	1	2	2	19	.01	.047	23	9	.09	55	.01	2	.80	.01	.03	1	-
L-25+50N 48+25W	1	22	31	36	.9	7	2	57	1.84	9	5	ND	1	13	1	2	2	18	.03	.062	21	11	.14	51	.01	5	.94	.01	.02	1	-
L-25+50N 48+00W	1	12	21	23	.5	4	1	44	1.37	3	5	ND	1	7	1	2	2	18	.01	.048	13	9	.05	36	.02	2	.96	.01	.02	1	-
L-25+50N 47+75W	2	17	32	39	1.0	7	2	64	2.08	7	5	ND	2	9	1	2	2	19	.02	.058	17	9	.14	40	.01	2	1.35	.01	.03	1	-
L-25+50N 47+50W	2	18	31	44	.6	7	2	115	2.06	10	5	ND	1	14	1	2	2	20	.03	.068	21	12	.18	46	.01	2	1.24	.01	.04	1	-
L-25+50N 47+25W	1	13	40	33	.5	6	2	114	1.99	13	5	ND	1	13	1	2	2	19	.02	.080	21	11	.14	34	.01	2	.89	.01	.03	1	-
L-25+50N 47+00W	1	13	60	30	1.0	4	1	64	1.52	6	5	ND	2	21	1	2	3	17	.04	.063	27	10	.14	53	.01	2	1.03	.01	.02	1	-
L-25+50N 43+00W	1	28	28	86	.4	10	5	159	2.02	7	5	ND	3	105	1	2	2	30	.20	.075	33	22	.62	78	.03	2	1.26	.02	.06	1	-
L-25+50N 42+75W	1	20	31	75	.4	11	5	290	2.16	8	5	ND	2	110	1	2	2	30	.21	.081	34	26	.58	82	.03	2	1.23	.02	.08	1	-
L-25+50N 42+50W	1	18	36	68	.5	10	5	315	2.07	4	5	ND	2	113	1	2	2	33	.15	.074	34	25	.58	63	.03	2	1.25	.02	.06	1	-
L-25+50N 42+25W	1	12	31	60	.6	8	3	194	1.49	7	5	ND	2	80	1	2	2	26	.12	.069	26	18	.35	59	.02	2	1.16	.02	.04	1	-
L-25+50N 42+00W	1	55	130	274	.7	16	11	394	3.27	28	8	ND	8	88	1	3	2	33	.18	.086	50	30	.86	84	.03	2	2.15	.02	.10	1	-
L-25+50N 41+75W	2	1492	5655	3344	42.2	10	6	200	6.29	366	8	ND	4	71	48	48	2	31	.12	.105	24	20	.57	64	.04	2	.84	.02	.09	6	1
L-25+50N 41+50W	5	737	4462	3779	16.1	21	21	1307	5.56	113	11	ND	12	163	16	51	2	21	.31	.152	54	15	.48	134	.02	3	1.15	.02	.12	7	71
L-25+50N 41+25W	1	75	867	559	3.1	10	6	183	2.42	23	8	ND	3	86	2	5	2	28	.15	.076	38	19	.39	65	.02	2	1.19	.02	.07	1	1
L-25+50N 41+00W	3	251	332	6226	4.4	22	8	655	2.39	14	25	ND	4	261	53	3	2	30	.72	.124	50	24	.65	146	.04	2	1.86	.03	.07	7	4
L-25+50N 40+75W	1	90	133	1096	1.4	29	12	352	3.19	27	13	ND	18	137	5	3	2	34	.33	.091	98	31	1.04	191	.05	8	2.03	.02	.15	1	16
L-25+50N 40+50W	1	20	44	106	.5	8	3	102	1.94	5	5	ND	3	54	2	2	2	25	.08	.058	31	18	.32	65	.04	2	1.50	.02	.05	1	-
L-25+50N 40+25W	1	22	73	143	1.1	8	5	209	1.71	8	5	ND	2	69	2	2	2	26	.13	.082	31	17	.41	95	.02	5	1.56	.02	.06	1	-
L-25+50N 40+00W	1	25	87	235	1.2	10	4	154	1.91	7	7	ND	3	115	2	3	2	25	.24	.075	32	22	.65	149	.03	2	2.04	.02	.05	3	1
L-25+50N 39+75W	1	28	42	239	1.6	12	4	129	1.75	5	15	ND	3	344	5	2	2	22	.61	.083	24	19	.49	234	.07	2	3.32	.03	.03	1	1
L-25+50N 39+50W	1	63	22	133	1.0	19	1	122	1.13	2	47	ND	1	119	2	2	2	13	.27	.069	39	4	.11	56	.10	2	4.09	.03	.01	2	-
L-25+50N 39+25W	3	412	44	416	1.4	92	77	525	2.24	10	217	ND	1	236	2	2	2	22	.53	.096	622	21	.57	148	.08	2	2.94	.04	.04	1	5
L-25+50N 39+00W	1	19	34	70	.5	8	5	106	1.56	2	5	ND	2	65	1	2	2	27	.09	.050	32	15	.35	51	.05	2	1.26	.02	.04	1	-
L-25+50N 38+75W	1	30	36	82	.6	14	8	231	3.01	20	6	ND	5	136	1	2	2	33	.22	.074	48	28	.90	70	.06	3	1.70	.02	.10	1	-
L-25+50N 38+50W	1	13	28	39	.5	7	3	78	1.48	7	5	ND	2	85	1	2	2	23	.10	.049	30	17	.39	50	.03	2	1.12	.02	.04	2	-
L-25+50N 38+25W	1	29	37	81	.6	11	7	294	2.01	14	5	ND	3	74	1	3	2	26	.12	.092	35	22	.58	63	.04	2	1.76	.02	.05	1	-
L-25+50N 38+00W	1	16	36	61	.4	8	4	242	1.91	10	5	ND	3	84	1	2	2	29	.10	.056	30	18	.51	65	.03	2	1.23	.02	.06	1	-
L-25+50N 37+75W	1	12	26	44	.4	7	3	119	1.56	7	5	ND	2	78	1	2	2	24	.08	.059	29	19	.41	56	.02	2	1.02	.02	.04	2	-
L-25+50N 37+50W	1	17	38	52	.9	9	5	306	1.89	11	5	ND	3	91	1	2	2	25	.13	.070	33	20	.52	76	.02	2	1.08	.02	.06	1	-
L-25+50N 37+25W	1	15	53	64	.8	8	5	302	1.99	13	6	ND	3	92	1	2	2	27	.13	.049	33	17	.50	66	.03	2	1.10	.02	.05	1	-
L-25+50N 37+00W	1	12	63	58	.5	6	3	147	1.49	17	5	ND	2	53	1	2	2	22	.06	.046	27	15	.28	53	.02	2	.96	.01	.03	1	-
STD C	19	60	40	133	7.0	70	27	1024	3.97	38	18	7	38	49	18	17	21	58	.48	.088	38	57	.87	175	.07	36	1.84	.06	.15	12	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	[illegible] PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU. PPB
L-25+50N 36+75W	1	29	144	173	1.0	12	7	395	2.81	44	5	ND	5	146	1	3	2	35	.18	.076	55	26	.68	104	.03	2	1.81	.02	.11	1	-
L-25+50N 36+50W	2	22	91	110	1.1	10	6	333	2.64	32	8	ND	5	194	1	2	2	36	.25	.065	54	28	.65	135	.04	2	1.54	.02	.10	1	-
L-25+50N 36+25W	4	53	164	373	1.5	13	13	1132	2.88	25	29	ND	5	174	2	2	2	41	.37	.074	103	28	.70	149	.05	19	2.53	.04	.08	1	-
L-25+50N 36+00W	4	27	129	312	1.1	13	7	350	3.16	25	5	ND	5	138	1	3	2	43	.19	.052	51	28	.71	131	.05	6	2.04	.03	.11	1	-
L-25+00N 72+50W	1	10	34	41	.3	6	3	145	1.89	2	5	ND	2	25	1	2	2	49	.09	.031	20	16	.22	104	.09	2	1.00	.02	.04	1	-
L-25+00N 72+25W	1	16	41	57	.4	11	4	182	3.04	8	5	ND	2	19	1	2	2	65	.09	.040	16	25	.34	100	.11	2	1.46	.02	.03	1	-
L-25+00N 72+00W	1	16	45	61	.4	11	4	187	2.76	4	5	ND	2	23	1	2	2	63	.07	.048	23	24	.45	141	.05	2	1.42	.02	.06	1	-
L-25+00N 71+75W	1	15	50	40	.2	8	3	119	2.29	3	5	ND	2	22	1	2	2	43	.06	.048	22	17	.27	157	.04	2	1.19	.02	.04	2	-
L-25+00N 71+50W	2	95	463	763	2.2	78	11	609	3.49	19	5	ND	3	46	6	2	2	39	.35	.105	31	32	.54	576	.05	2	3.13	.03	.08	1	10
L-25+00N 71+00W	8	26	83	142	.7	17	5	111	3.86	14	5	ND	3	37	1	2	2	47	.12	.043	33	29	.45	324	.05	3	1.96	.02	.06	2	-
L-25+00N 70+75W	14	46	126	558	2.1	60	10	828	3.14	12	5	ND	2	84	5	4	2	41	.55	.085	26	23	.61	709	.05	2	2.23	.03	.08	1	3
L-25+00N 70+50W	17	105	205	1041	2.2	133	12	1256	3.69	22	23	ND	3	78	6	2	2	55	.51	.118	32	32	.77	767	.06	6	3.07	.04	.11	1	2
L-25+00N 70+25W	3	33	114	192	.7	27	11	456	4.42	19	5	ND	3	38	1	2	2	78	.17	.068	26	33	.75	305	.07	2	2.25	.02	.07	1	-
L-25+00N 70+00W	2	12	66	77	.1	11	5	212	2.78	6	5	ND	1	26	1	2	2	75	.13	.033	17	16	.34	254	.10	2	1.06	.02	.03	1	-
L-25+00N 68+50W	1	9	13	34	.2	5	2	67	1.38	2	5	ND	1	10	1	3	2	36	.04	.023	10	10	.07	53	.06	2	.45	.02	.02	2	-
L-25+00N 68+25W	1	19	26	59	.3	7	5	204	2.51	7	5	ND	1	23	1	2	2	66	.16	.043	9	10	.22	230	.07	2	.88	.02	.03	1	-
L-25+00N 67+75W	1	13	36	54	.4	9	4	114	2.03	8	5	ND	1	21	1	2	2	51	.06	.051	17	15	.16	240	.05	2	.84	.01	.03	1	-
L-25+00N 67+50W	1	15	19	28	1.3	5	1	29	.97	4	5	ND	1	19	1	2	2	17	.03	.052	12	10	.04	458	.02	2	.83	.02	.02	2	-
L-25+00N 67+25W	3	18	25	40	6.5	7	1	37	1.73	28	5	ND	1	31	1	2	2	35	.08	.083	13	17	.12	844	.02	2	2.94	.02	.04	3	4
L-25+00N 67+00W	3	18	22	43	2.7	6	2	60	1.64	10	5	ND	1	33	1	2	2	31	.04	.085	10	14	.05	899	.01	2	1.23	.02	.02	1	2
L-25+00N 66+75W	8	27	43	74	5.5	18	4	95	3.47	66	5	ND	2	47	1	3	2	51	.13	.480	16	29	.25	1602	.02	2	1.95	.02	.05	2	6
L-25+00N 66+50W	5	31	59	85	1.6	17	5	186	3.55	40	5	ND	2	39	1	3	2	51	.11	.158	23	32	.31	941	.02	2	1.97	.02	.06	1	-
L-25+00N 66+25W	3	22	47	73	1.4	13	4	143	2.71	11	5	ND	2	32	1	2	2	37	.08	.179	26	24	.39	471	.01	2	1.52	.02	.08	1	-
L-25+00N 66+00W	10	41	38	219	2.2	48	7	327	2.59	52	5	ND	2	56	3	6	2	39	.39	.179	30	27	.58	1572	.02	2	2.09	.03	.11	2	4
L-25+00N 65+75W	1	20	38	54	.3	9	4	178	2.81	10	5	ND	2	24	1	2	2	38	.09	.046	27	22	.34	98	.04	2	1.60	.02	.06	2	-
L-25+00N 65+50W	1	12	24	44	.3	6	2	86	1.51	4	5	ND	3	23	1	2	2	35	.05	.033	34	18	.24	64	.03	4	.95	.02	.06	2	-
L-25+00N 65+25W	1	17	29	48	.6	8	4	125	2.59	8	5	ND	2	27	1	2	2	43	.05	.052	23	18	.25	65	.04	2	1.18	.02	.04	3	-
L-25+00N 65+00W	1	22	37	65	.3	10	5	236	2.48	12	5	ND	3	36	1	2	2	40	.12	.061	31	23	.35	114	.02	2	1.01	.02	.07	1	-
L-23+50N 52+00W	1	16	47	50	.6	7	3	158	2.49	8	5	ND	2	32	1	2	2	30	.05	.060	28	16	.29	66	.03	2	1.71	.02	.05	2	-
L-23+50N 51+75W	1	20	47	92	.6	10	5	350	2.39	10	5	ND	2	47	1	2	2	26	.15	.081	33	15	.34	121	.02	10	1.54	.02	.08	1	-
L-23+50N 51+50W	3	39	64	151	1.4	45	9	545	3.22	14	6	ND	3	72	1	2	2	28	.41	.120	38	19	.49	281	.02	2	1.95	.03	.10	2	-
L-23+50N 51+25W	1	31	42	37	1.4	6	2	56	1.52	7	5	ND	2	17	1	2	2	22	.04	.046	30	10	.15	72	.02	3	1.31	.02	.05	1	-
L-23+50N 51+00W	2	53	34	64	.7	10	6	213	3.12	14	5	ND	3	25	1	2	2	29	.10	.064	30	11	.20	72	.01	2	1.00	.01	.06	1	-
L-23+50N 50+75W	2	36	42	41	.4	6	3	168	2.33	13	5	ND	2	18	1	2	2	28	.03	.045	28	13	.21	56	.02	2	1.37	.02	.05	2	-
L-23+50N 50+50W	2	30	42	50	.7	7	3	153	2.48	9	5	ND	2	22	1	2	2	27	.02	.056	31	11	.22	54	.02	2	1.25	.02	.07	2	-
L-23+50N 50+25W	2	24	39	53	.7	8	3	179	2.48	10	5	ND	3	27	1	2	2	25	.04	.061	33	13	.24	68	.02	2	1.17	.01	.06	1	-
STD C	18	57	41	132	7.1	68	26	1030	3.97	40	21	7	37	48	18	16	21	55	.48	.087	36	60	.87	173	.08	32	1.83	.08	.13	13	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	[illegible]	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU PPB
L-23+50N 50+00W	2	215	61	102	1.0	19	10	400	4.01	29	5	ND	3	16	1	2	2	31	.03	.076	24	19	.40	60	.01	2	1.40	.01	.05	1	-
L-23+50N 49+75W	1	43	32	46	.4	9	3	105	2.64	15	5	ND	2	11	1	2	2	26	.02	.048	27	11	.17	53	.02	2	1.20	.01	.03	1	-
L-23+50N 49+00W	2	136	39	202	.7	35	21	391	3.14	11	10	ND	5	115	1	2	2	27	.43	.093	34	19	.53	147	.05	2	2.24	.03	.08	1	-
L-23+00N 71+00W	1	31	75	113	.5	21	8	191	3.74	23	5	ND	3	27	1	3	2	43	.09	.060	29	24	.48	164	.05	2	1.70	.02	.06	1	-
L-23+00N 70+75W	1	21	47	65	.1	15	5	121	3.34	20	5	ND	2	22	1	2	2	47	.05	.051	24	21	.32	199	.04	2	1.10	.01	.05	1	-
L-23+00N 70+50W	1	20	26	48	.2	13	4	93	2.94	11	5	ND	2	14	1	2	2	41	.04	.043	19	21	.27	84	.06	2	1.14	.01	.03	1	-
L-23+00N 70+25W	1	17	41	51	.4	10	4	108	3.02	17	5	ND	2	20	1	2	2	44	.04	.054	25	19	.24	91	.05	2	1.05	.01	.04	1	-
L-23+00N 70+00W	1	17	38	60	.3	12	6	154	3.26	18	5	ND	3	34	1	2	2	42	.08	.067	32	19	.33	128	.04	3	1.19	.02	.06	1	-
L-23+00N 69+75W	1	25	60	83	.4	16	8	149	4.10	32	5	ND	4	42	1	3	2	36	.08	.094	41	24	.47	134	.03	2	1.42	.02	.08	1	-
L-23+00N 69+50W	1	19	52	63	.5	11	6	197	4.70	25	5	ND	4	32	1	3	2	53	.05	.074	32	23	.38	118	.06	2	1.69	.02	.06	2	-
L-23+00N 69+25W	2	30	38	33	.8	8	3	88	2.51	29	5	ND	2	36	1	2	2	27	.04	.178	17	17	.14	222	.02	3	1.20	.02	.03	1	-
L-23+00N 69+00W	1	18	34	33	.8	6	2	70	2.60	20	5	ND	1	26	1	2	2	33	.04	.078	22	17	.16	174	.03	2	1.67	.01	.03	1	-
L-23+00N 68+75W	4	28	40	65	1.8	17	4	185	3.21	48	5	ND	1	72	1	4	2	35	.09	.218	16	19	.18	399	.04	2	1.94	.02	.04	1	-
L-23+00N 68+50W	1	20	45	56	.7	8	4	216	2.97	21	5	ND	2	31	1	2	2	32	.04	.096	28	17	.25	128	.02	2	1.24	.02	.06	1	-
L-23+00N 68+25W	1	20	33	58	.2	12	5	180	3.04	13	5	ND	2	21	1	3	2	43	.05	.059	23	25	.31	119	.03	2	1.18	.01	.05	1	-
L-23+00N 67+75W	1	19	38	51	1.0	9	3	97	2.67	10	5	ND	2	28	1	2	2	37	.19	.045	22	18	.26	184	.04	3	1.28	.02	.05	2	-
L-23+00N 67+50W	1	31	48	75	1.5	14	5	123	3.09	16	5	ND	2	19	1	3	2	38	.07	.047	23	25	.36	129	.04	2	1.73	.02	.05	1	-
L-23+00N 67+25W	1	51	49	116	1.3	23	8	204	4.37	27	5	ND	3	19	1	2	2	43	.07	.070	26	28	.45	89	.06	3	1.81	.01	.05	1	-
L-23+00N 67+00W	1	34	30	75	1.1	14	3	74	3.76	32	5	ND	1	7	1	2	2	39	.03	.042	13	15	.12	66	.06	2	.90	.01	.03	1	-
L-23+00N 66+75W	1	19	37	45	.7	11	4	86	2.93	12	5	ND	2	15	1	2	2	39	.03	.039	19	20	.22	73	.05	2	1.01	.01	.04	2	-
L-23+00N 66+50W	1	23	37	61	.7	11	4	98	3.31	18	5	ND	2	19	1	2	2	41	.04	.086	25	21	.32	76	.04	3	1.07	.02	.05	1	-
L-23+00N 66+25W	1	21	50	71	.6	12	4	81	2.45	9	5	ND	2	21	1	2	2	35	.09	.043	32	22	.39	217	.03	2	1.82	.02	.07	1	-
L-23+00N 66+00W	1	47	52	182	.9	24	10	333	3.64	19	5	ND	4	45	1	4	2	48	.58	.081	32	41	.75	340	.04	2	2.97	.03	.07	1	-
L-23+00N 65+75W	1	41	44	105	2.9	14	7	323	2.92	21	5	ND	3	42	1	2	2	34	.83	.061	28	30	.33	193	.06	2	3.06	.03	.06	1	33
L-23+00N 65+50W	1	34	32	69	.4	18	7	187	3.13	12	5	ND	3	19	1	3	2	37	.11	.053	19	27	.46	111	.06	2	2.12	.02	.04	1	-
L-23+00N 65+25W	1	28	35	67	.3	10	6	191	3.02	12	5	ND	2	32	1	2	2	43	.43	.052	25	18	.27	132	.06	2	1.60	.02	.04	1	-
L-23+00N 65+00W	1	19	26	42	.3	7	4	88	2.46	10	5	ND	2	23	1	2	2	37	.08	.040	24	14	.22	66	.05	4	1.10	.02	.04	1	-
L-22+50N 51+25W	2	20	46	55	.4	11	3	121	2.88	13	5	ND	2	19	1	2	2	26	.02	.044	27	13	.15	66	.02	2	1.08	.01	.04	1	-
L-22+50N 51+00W	1	36	41	56	.4	10	4	154	2.48	11	5	ND	2	16	1	2	2	27	.02	.048	28	15	.17	56	.02	2	1.08	.01	.04	1	-
L-22+50N 50+75W	1	30	40	53	.3	10	3	118	2.19	11	5	ND	2	14	1	2	2	24	.02	.054	25	17	.18	56	.02	2	1.17	.01	.04	1	-
L-22+50N 50+50W	1	27	42	50	.4	7	3	110	2.32	12	5	ND	2	19	1	2	2	24	.02	.061	25	11	.18	55	.02	2	1.12	.01	.05	2	-
L-22+50N 50+25W	1	150	50	178	1.2	19	6	265	2.67	11	5	ND	2	40	1	2	2	28	.27	.077	24	14	.28	134	.03	2	2.45	.02	.07	1	-
L-22+50N 50+00W	1	61	65	86	1.0	12	4	95	2.86	12	5	ND	2	35	1	2	2	29	.16	.059	24	16	.31	110	.02	2	1.74	.02	.06	1	-
L-22+50N 49+75W	2	474	76	227	4.6	48	15	850	5.04	25	8	ND	6	144	1	3	2	35	.63	.077	64	28	.54	320	.10	2	4.39	.04	.12	1	1
L-22+50N 48+00W	1	54	63	65	.8	12	4	235	2.26	10	5	ND	2	32	1	2	2	25	.08	.076	27	11	.19	89	.02	3	1.14	.02	.07	1	-
L-22+50N 47+75W	2	48	52	91	1.6	13	3	74	2.67	13	5	ND	3	25	1	2	2	28	.05	.055	42	20	.28	101	.03	2	1.93	.01	.05	1	-
STD C	17	59	43	133	7.0	68	27	1035	3.99	41	17	8	38	49	19	15	23	56	.48	.090	37	59	.87	177	.08	32	1.84	.08	.14	13	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
L-21+50N 47+50W	1	80	178	28	2.6	4	1	24	1.46	5	5	ND	2	10	1	2	2	14	.03	.050	20	12	.06	35	.06	2	2.51	.02	.03	1	10
L-21+50N 46+75W	3	71	133	109	1.7	22	6	124	3.74	21	5	ND	5	31	1	2	2	23	.07	.051	42	18	.36	106	.02	2	1.91	.01	.08	1	16
L-21+50N 46+50W	2	34	81	75	.6	14	5	118	3.49	26	5	ND	4	33	1	3	2	23	.06	.062	39	18	.39	57	.02	2	1.49	.01	.07	1	-
L-21+50N 46+25W	2	32	106	59	.5	9	4	155	2.61	16	5	ND	4	61	1	2	2	23	.06	.081	36	15	.33	70	.04	2	2.17	.02	.06	1	-
L-21+50N 46+00W	3	31	122	76	2.0	13	6	212	3.10	29	5	ND	4	41	1	3	2	27	.07	.067	37	22	.46	83	.02	2	1.56	.02	.07	1	54
L-21+50N 45+75W	2	26	119	88	.8	15	5	177	3.66	27	5	ND	5	50	1	5	4	31	.10	.070	39	28	.53	84	.04	2	1.65	.02	.06	1	-
L-21+50N 45+50W	1	33	68	66	1.2	10	4	142	3.35	15	5	ND	3	50	1	2	2	34	.07	.056	33	25	.35	75	.07	2	2.31	.02	.03	1	-
L-21+50N 45+25W	1	18	56	40	3.2	9	3	83	2.17	6	5	ND	2	62	1	7	5	31	.06	.054	29	18	.20	130	.03	2	.90	.01	.04	1	4
L-21+50N 45+00W	2	23	54	63	1.6	11	5	146	2.94	10	5	ND	3	55	1	2	2	37	.07	.049	43	23	.42	129	.04	2	1.45	.01	.05	1	-
L-21+00N 71+00W	1	26	25	50	.2	13	5	139	2.82	7	5	ND	2	17	1	2	2	50	.08	.041	16	25	.26	141	.08	2	1.01	.02	.02	2	-
L-21+00N 70+75W	1	14	20	39	.2	7	3	69	1.86	5	5	ND	2	18	1	2	2	36	.11	.039	17	16	.12	120	.07	2	.68	.01	.02	1	-
L-21+00N 70+50W	2	22	47	61	.3	12	7	124	4.08	19	5	ND	5	37	1	2	2	46	.08	.066	37	25	.39	85	.06	2	1.66	.02	.05	1	-
L-21+00N 70+25W	1	18	32	51	.3	9	4	149	2.81	7	5	ND	2	25	1	2	2	37	.07	.052	22	23	.27	92	.04	2	1.68	.02	.04	2	-
L-21+00N 69+00W	1	31	33	43	.4	9	3	73	2.63	11	5	ND	2	21	1	2	2	32	.04	.044	26	20	.23	58	.04	2	1.45	.01	.04	1	-
L-21+00N 68+75W	1	16	31	50	1.0	8	3	237	2.58	9	5	ND	2	19	1	2	2	34	.13	.062	17	15	.20	69	.06	3	1.85	.01	.04	2	-
L-21+00N 68+50W	1	21	40	52	.4	9	4	118	2.72	14	5	ND	2	22	1	2	2	32	.05	.065	25	18	.24	144	.03	2	1.34	.01	.05	1	-
L-21+00N 68+25W	1	27	37	64	.3	15	4	114	2.87	11	5	ND	2	20	1	2	2	39	.03	.054	22	23	.26	86	.03	2	.95	.01	.05	1	-
L-21+00N 67+75W	1	16	28	34	.3	9	2	55	2.04	9	5	ND	2	18	1	2	2	33	.03	.045	23	20	.12	57	.03	2	.82	.01	.04	1	-
L-21+00N 67+50W	1	18	42	43	.4	7	2	79	2.18	5	5	ND	2	17	1	2	2	30	.04	.047	22	18	.21	61	.02	2	1.44	.01	.04	2	-
L-21+00N 67+25W	1	16	45	52	1.5	10	3	105	2.28	4	5	ND	1	14	1	2	2	32	.02	.061	18	16	.20	67	.02	2	1.20	.01	.04	1	-
L-21+00N 66+75W	1	32	73	39	2.1	7	2	38	1.06	2	5	ND	1	9	1	2	2	16	.03	.044	14	16	.14	128	.05	2	2.29	.02	.03	1	1
L-21+00N 66+25W	1	19	40	45	.9	9	3	195	2.61	11	5	ND	2	19	1	2	2	37	.03	.046	20	22	.21	61	.04	2	1.09	.01	.04	1	-
L-21+00N 66+00W	1	21	38	58	1.0	11	4	148	2.17	6	5	ND	2	23	1	2	2	29	.07	.077	25	19	.38	139	.02	2	1.58	.02	.06	1	-
L-21+00N 65+75W	1	24	41	67	.9	12	4	146	2.51	8	5	ND	2	23	1	2	2	29	.07	.058	28	20	.43	132	.03	3	1.73	.02	.07	1	-
L-21+00N 65+50W	1	18	33	49	.7	7	4	112	2.22	7	5	ND	3	24	1	2	2	26	.06	.055	28	14	.30	89	.02	2	1.49	.01	.06	2	-
L-21+00N 64+75W	1	23	47	52	.4	8	4	84	2.17	10	5	ND	2	24	1	2	2	27	.06	.062	26	15	.30	71	.02	2	1.50	.01	.06	2	-
L-21+00N 64+50W	1	22	41	55	.4	8	4	150	2.76	12	5	ND	3	26	1	2	2	30	.05	.054	31	15	.32	67	.02	2	1.28	.01	.06	1	-
L-21+00N 64+25W	1	40	23	160	2.0	13	4	187	2.22	7	5	ND	3	24	1	2	2	26	.30	.107	26	20	.33	181	.08	2	5.77	.03	.05	1	1
L-21+00N 64+00W	1	19	35	58	.3	8	4	142	2.14	5	5	ND	2	36	1	2	2	26	.19	.062	24	14	.32	99	.02	2	1.29	.02	.06	1	-
L-21+00N 63+75W	1	17	43	49	.4	8	4	180	2.72	7	5	ND	2	23	1	2	2	31	.07	.054	24	17	.26	64	.03	2	1.38	.02	.05	1	-
L-21+00N 63+50W	1	47	41	191	2.6	18	5	433	2.61	14	9	ND	4	48	1	2	2	27	.87	.125	31	20	.48	237	.07	2	4.32	.04	.08	1	3
L-20+50N 47+50W	2	146	72	133	3.0	20	6	300	3.35	18	5	ND	4	25	1	2	2	28	.10	.081	45	23	.42	237	.03	4	2.91	.02	.08	1	1
L-20+50N 47+25W	1	221	55	56	2.3	11	7	65	1.12	4	10	ND	3	11	1	2	2	13	.04	.094	38	10	.10	48	.05	2	5.28	.02	.03	1	1
L-20+50N 47+00W	5	90	1809	87	3.5	20	12	340	7.08	30	5	ND	9	124	1	3	2	30	.07	.135	38	22	.50	344	.04	2	1.19	.02	.22	1	19
L-20+50N 46+75W	15	91	1157	39	9.9	7	3	79	11.62	45	5	ND	3	18	1	6	2	33	.02	.132	16	20	.15	65	.05	2	1.35	.02	.07	2	10
L-20+50N 46+50W	45	164	1383	73	7.5	7	4	102	25.31	118	5	ND	6	19	1	15	2	39	.02	.186	15	20	.20	95	.07	2	.88	.02	.19	1	4
STD C	18	57	42	132	7.1	67	26	1027	3.88	40	22	8	37	48	18	16	21	58	.47	.087	38	59	.86	172	.07	36	1.79	.06	.15	1	-

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD		BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W	AU*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	Pm	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L-20+50N 46+25W	48	69	802	46	27.5	7	3	94	7.66	90	5	ND	3	14	1	19	2	37	.04	.113	15	13	.10	60	.04	2	1.56	.02	.05	3	10
L-20+50N 46+00W	6	155	124	91	3.5	18	8	229	5.96	44	5	ND	4	38	1	3	2	27	.15	.100	33	14	.28	109	.02	2	1.13	.02	.07	1	12
L-20+50N 45+75W	2	20	55	41	2.2	8	3	69	2.16	10	5	ND	2	18	1	2	2	27	.03	.039	28	12	.14	64	.02	2	1.06	.01	.03	1	3
L-20+50N 45+50W	3	34	120	85	1.7	14	6	256	2.97	18	5	ND	3	44	1	2	2	26	.16	.081	39	17	.34	103	.02	2	1.29	.02	.08	1	2
L-20+50N 45+25W	2	22	67	53	2.2	8	4	158	2.24	12	5	ND	3	34	1	2	2	23	.06	.068	34	15	.29	77	.02	2	1.25	.01	.06	1	11
L-20+50N 45+00W	1	22	59	79	1.3	12	4	134	2.55	17	5	ND	3	67	1	2	2	24	.12	.076	33	27	.50	102	.01	2	1.41	.02	.08	1	-
L-20+50N 44+75W	1	23	77	72	2.4	9	4	164	2.67	15	5	ND	3	67	1	2	2	23	.10	.076	31	16	.31	96	.02	2	1.57	.02	.07	1	4
L-20+50N 44+50W	1	20	49	57	1.3	7	4	172	2.10	11	5	ND	3	43	1	2	2	22	.09	.102	32	15	.31	78	.02	2	1.42	.02	.07	1	-
L-19+50N 47+00W	2	70	60	78	.7	13	5	133	2.78	16	5	ND	2	26	1	3	2	21	.06	.080	35	15	.31	61	.01	2	1.34	.01	.05	1	-
L-19+50N 46+75W	4	107	86	114	.9	19	9	257	3.25	19	5	ND	4	112	1	2	2	19	.16	.179	48	16	.35	172	.01	3	1.17	.02	.09	1	-
L-19+50N 46+50W	1	23	31	40	.6	7	2	105	1.89	8	5	ND	2	18	1	2	2	24	.03	.048	23	10	.13	42	.02	2	1.23	.01	.04	1	-
L-19+50N 46+25W	3	41	51	67	1.0	11	5	184	2.61	14	5	ND	3	26	1	2	2	25	.03	.083	31	13	.22	92	.01	2	1.08	.01	.06	1	-
L-19+50N 44+50W	4	68	124	195	2.5	26	14	970	3.40	26	5	ND	8	270	1	5	2	37	.84	.145	67	42	1.13	258	.06	2	2.32	.03	.14	1	2
L-19+50N 44+25W	3	78	103	180	2.5	20	11	628	3.03	18	5	ND	6	284	2	2	2	35	.93	.099	57	34	.69	262	.08	2	2.76	.04	.08	1	3
L-19+50N 44+00W	2	31	86	96	.4	13	6	155	3.32	16	5	ND	5	75	1	3	2	34	.13	.062	47	31	.65	96	.04	2	1.65	.02	.09	1	-
L-19+00N 70+00W	1	28	49	231	1.0	18	7	551	2.62	8	5	ND	3	40	1	4	2	31	.37	.113	28	26	.54	545	.03	2	2.38	.03	.10	1	-
L-19+00N 69+75W	1	18	39	47	.2	8	3	107	2.46	9	5	ND	2	19	1	2	2	32	.04	.047	25	18	.24	118	.03	2	1.25	.01	.06	1	-
L-19+00N 69+50W	1	44	64	79	1.4	14	5	182	2.43	10	5	ND	2	25	1	2	2	34	.11	.082	31	23	.41	312	.03	2	2.37	.02	.08	1	-
L-19+00N 69+25W	1	17	27	35	.3	7	3	153	2.23	6	5	ND	2	17	1	2	2	39	.05	.042	18	14	.17	90	.04	2	.83	.01	.04	1	-
L-19+00N 69+00W	1	18	37	47	.2	8	3	112	2.30	8	5	ND	2	24	1	2	2	34	.07	.052	25	17	.20	102	.03	2	.85	.01	.05	1	-
L-19+00N 68+75W	1	17	40	36	.5	8	3	75	2.06	9	5	ND	2	21	1	2	2	28	.03	.051	24	17	.22	97	.02	2	1.05	.01	.05	1	-
L-19+00N 68+50W	1	19	39	40	.5	9	4	108	2.36	10	5	ND	2	21	1	2	2	32	.06	.060	22	16	.22	125	.02	2	.97	.01	.05	1	-
L-19+00N 68+25W	1	30	55	52	.5	10	5	201	2.38	16	5	ND	2	28	1	2	2	29	.08	.057	28	15	.21	265	.02	2	1.00	.01	.06	1	-
L-19+00N 67+75W	1	44	54	99	.9	16	6	164	2.64	19	5	ND	4	36	1	2	2	32	.11	.077	39	27	.55	176	.03	2	1.81	.02	.10	1	-
L-19+00N 67+50W	1	21	40	41	.9	8	3	80	2.06	7	5	ND	2	18	1	2	2	29	.04	.052	24	17	.24	71	.02	2	1.39	.01	.05	2	-
L-19+00N 67+25W	1	15	33	28	.3	5	2	76	1.88	8	5	ND	2	21	1	2	2	27	.03	.037	26	15	.18	54	.02	2	1.23	.01	.04	1	-
L-19+00N 67+00W	1	21	36	30	.2	6	2	68	1.88	5	5	ND	2	20	1	2	2	29	.02	.040	24	15	.17	52	.02	3	1.16	.01	.05	1	-
L-19+00N 66+75W	1	20	33	48	1.2	10	3	80	2.11	10	5	ND	2	16	1	2	2	30	.04	.051	20	19	.22	63	.03	2	1.66	.01	.04	2	-
L-19+00N 66+50W	2	26	64	62	1.0	12	3	103	2.48	19	5	ND	2	20	1	2	2	32	.04	.058	23	17	.25	87	.02	2	1.31	.01	.05	1	-
L-19+00N 66+25W	1	24	42	61	.6	14	4	271	2.64	15	5	ND	2	20	1	2	2	36	.03	.042	26	19	.24	137	.03	2	1.09	.01	.05	1	-
L-19+00N 66+00W	2	27	29	56	.7	10	3	131	2.91	11	5	ND	2	26	1	2	2	33	.33	.066	13	16	.12	151	.04	2	1.01	.02	.04	1	-
L-19+00N 65+75W	1	25	42	63	.6	10	6	231	2.40	20	5	ND	2	21	1	2	2	32	.06	.076	24	18	.33	103	.02	2	1.49	.01	.06	1	-
L-19+00N 65+50W	1	28	50	67	.6	10	5	189	2.64	18	5	ND	2	24	1	2	2	31	.07	.074	28	22	.34	97	.02	2	1.42	.02	.07	1	-
L-19+00N 65+25W	1	25	40	59	.6	9	4	97	2.49	15	5	ND	2	24	1	2	2	34	.12	.052	23	18	.26	159	.03	5	1.21	.02	.05	1	-
L-19+00N 65+00W	1	41	49	141	1.1	14	7	480	2.66	19	5	ND	3	42	1	2	2	32	.48	.092	29	22	.42	223	.03	5	2.00	.02	.08	1	-
L-19+00N 64+75W	1	23	31	53	.5	10	4	127	2.21	11	5	ND	2	20	1	2	2	33	.04	.060	21	18	.28	94	.02	2	1.33	.01	.05	1	-
STD C	18	57	43	132	7.0	67	26	1031	3.92	37	18	7	37	49	17	14	18	55	.47	.087	36	57	.86	173	.08	32	1.80	.08	.13	13	-

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
L-19+00N 64+50W	1	14	37	38	.5	5	3	132	2.12	10	5	ND	2	21	1	2	2	30	.11	.080	20	13	.20	62	.02	2	.93	.01	.05	2	-
L-19+00N 64+25W	1	17	31	63	1.0	8	4	242	2.10	11	5	ND	1	21	1	2	2	31	.07	.058	19	16	.33	64	.03	2	1.30	.01	.04	1	-
L-19+00N 64+00W	1	15	28	44	.2	7	4	90	2.23	10	5	ND	1	26	1	2	2	28	.10	.043	24	13	.28	53	.03	2	1.01	.01	.03	1	-
L-19+00N 63+75W	1	13	23	38	.3	5	2	83	1.68	6	5	ND	1	26	1	2	2	29	.18	.050	20	13	.14	63	.03	2	.70	.02	.03	2	-
L-19+00N 63+50W	1	14	27	32	.5	6	3	139	2.14	8	5	ND	2	17	1	2	2	35	.04	.040	21	17	.19	76	.03	2	1.00	.01	.03	1	-
L-18+00N 70+00W	1	15	38	31	.5	6	2	76	1.95	13	5	ND	2	20	1	2	2	27	.04	.045	27	15	.18	76	.03	2	1.11	.01	.04	2	-
L-18+00N 69+75W	1	43	60	80	.6	21	8	270	2.56	12	5	ND	3	24	1	3	2	33	.12	.080	28	29	.57	111	.04	5	1.83	.02	.07	3	-
L-18+00N 69+50W	1	28	43	56	.4	10	4	112	2.36	12	5	ND	2	20	1	2	2	30	.04	.056	25	19	.28	232	.02	2	1.54	.01	.05	1	-
L-18+00N 69+25W	1	27	53	98	.6	13	8	531	2.58	12	5	ND	3	25	1	2	2	31	.14	.062	28	23	.45	340	.03	2	2.26	.02	.07	1	-
L-18+00N 69+00W	1	54	58	168	.7	28	12	660	3.37	17	5	ND	4	45	1	2	2	36	.51	.133	28	33	.90	581	.03	2	1.97	.02	.08	1	-
L-18+00N 68+75W	2	98	70	222	1.3	27	11	810	3.57	21	5	ND	3	37	1	2	2	37	.25	.097	36	28	.53	642	.03	2	2.63	.02	.12	1	-
L-18+00N 68+50W	1	40	49	115	.7	14	6	147	3.31	22	5	ND	3	39	1	2	2	31	.18	.089	38	22	.48	220	.03	2	1.91	.02	.08	1	-
L-18+00N 68+25W	2	48	241	111	.9	21	7	237	3.45	25	5	ND	3	36	1	2	2	30	.09	.074	33	30	.47	138	.02	14	1.47	.02	.09	1	-
L-18+00N 68+00W	1	36	60	58	3.0	11	4	93	1.94	9	5	ND	1	21	1	2	2	30	.07	.073	26	21	.36	149	.03	3	2.06	.02	.05	1	7
L-18+00N 67+75W	1	23	36	50	1.0	10	3	101	1.93	8	5	ND	1	24	1	2	2	26	.06	.061	22	20	.28	124	.02	8	1.17	.02	.05	2	-
L-18+00N 67+50W	1	23	29	52	.6	13	3	108	2.39	7	5	ND	1	14	1	2	2	29	.04	.056	15	17	.20	60	.03	2	1.31	.01	.04	1	-
L-18+00N 67+25W	1	17	30	43	.5	8	3	91	2.54	12	5	ND	1	14	1	2	2	31	.03	.037	21	16	.22	53	.04	2	1.58	.01	.04	3	-
L-18+00N 67+00W	2	31	39	65	1.1	13	4	268	2.79	17	5	ND	2	17	1	2	2	30	.05	.084	22	21	.29	60	.03	2	1.33	.01	.06	1	-
L-18+00N 66+75W	1	23	59	75	1.2	10	5	185	2.95	16	5	ND	2	22	1	2	2	31	.05	.059	29	19	.34	79	.02	2	1.92	.01	.06	1	-
L-18+00N 66+50W	1	33	56	105	.8	14	7	227	3.17	27	5	ND	3	29	1	2	2	31	.09	.061	32	22	.43	125	.02	2	1.77	.02	.08	1	-
L-18+00N 66+25W	1	52	41	335	3.9	50	3	136	1.94	17	5	ND	3	33	2	2	2	19	.50	.107	29	14	.29	351	.09	2	5.55	.03	.06	1	11
L-18+00N 66+00W	1	37	61	151	1.8	14	7	193	2.93	25	5	ND	4	54	1	3	2	36	.71	.066	33	23	.43	370	.04	2	2.60	.03	.07	1	16
L-18+00N 65+75W	1	44	64	244	1.1	18	11	843	3.07	22	5	ND	4	56	2	2	2	31	.86	.124	28	21	.59	327	.03	2	2.28	.03	.10	1	-
L-18+00N 65+50W	1	24	47	78	1.0	11	6	271	2.69	18	5	ND	3	27	1	2	2	32	.12	.063	26	20	.34	103	.03	2	1.53	.02	.06	1	-
L-18+00N 65+25W	1	39	49	117	.9	17	9	332	3.22	22	5	ND	3	38	1	2	2	37	.50	.070	26	24	.52	207	.04	2	2.08	.02	.08	1	-
L-18+00N 65+00W	1	41	53	123	1.9	14	7	253	2.94	35	5	ND	4	54	1	2	2	30	.81	.095	29	19	.52	183	.04	2	2.28	.03	.08	1	3
L-18+00N 64+75W	1	25	42	94	.5	10	6	178	2.97	21	5	ND	3	30	1	2	2	33	.18	.053	27	19	.49	118	.03	12	1.95	.02	.06	1	-
L-18+00N 64+50W	1	40	41	85	.2	19	10	244	3.83	22	5	ND	3	19	1	2	2	54	.11	.049	21	28	.66	83	.08	2	1.76	.02	.06	1	-
L-18+00N 64+25W	1	18	29	48	.7	8	3	118	2.78	8	5	ND	1	18	1	2	2	42	.09	.045	16	16	.23	71	.05	3	1.05	.02	.04	2	-
L-18+00N 64+00W	1	27	30	66	.4	17	7	192	3.42	14	5	ND	2	19	1	2	2	43	.10	.060	21	28	.50	68	.06	4	1.71	.02	.04	1	-
L-18+00N 63+50W	1	55	56	142	1.3	19	11	1005	2.99	27	5	ND	4	50	1	2	2	33	.68	.109	32	24	.54	156	.05	2	2.48	.03	.08	2	-
STD C	18	58	40	132	7.2	68	27	1036	4.04	39	18	8	39	50	18	15	21	56	.49	.090	37	59	.89	177	.07	36	1.87	.06	.15	12	-

ACME ANALYTICAL LABORATORIES DATE RECEIVED: AUG 27 1987
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED: Sept 7/87...

ASSAY CERTIFICATE

- SAMPLE TYPE: Rock Chips

ASSAYER: .D. Toye.. DEAN TOYE, CERTIFIED B.C. ASSAYER

GOLD SPRING RES. File # 87-3674

SAMPLE#	CU	PB	ZN	AG	AU
	%	%	%	OZ/T	OZ/T
E 25051	.07	18.34	5.28	3.83	.002
K 0361	.01	5.18	.24	1.28	.001
K 0362	.05	17.97	8.17	5.07	.003
K 0375	1.26	4.36	6.09	3.33	.002
K 0377	.10	1.07	1.46	.30	.001
K 0378	.60	20.71	2.34	26.04	.003

ACME ANALYTICAL LABORATORIES DATE RECEIVED: AUG 17 1987
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158 DATA LINE 251-1011 DATE REPORT MAILED: Aug.30/87.....

ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK

ASSAYER: .D.Toye.. DEAN TOYE, CERTIFIED B.C. ASSAYER

RENEGADE MINERAL PROJECT-FOGHORN File # 87-3377

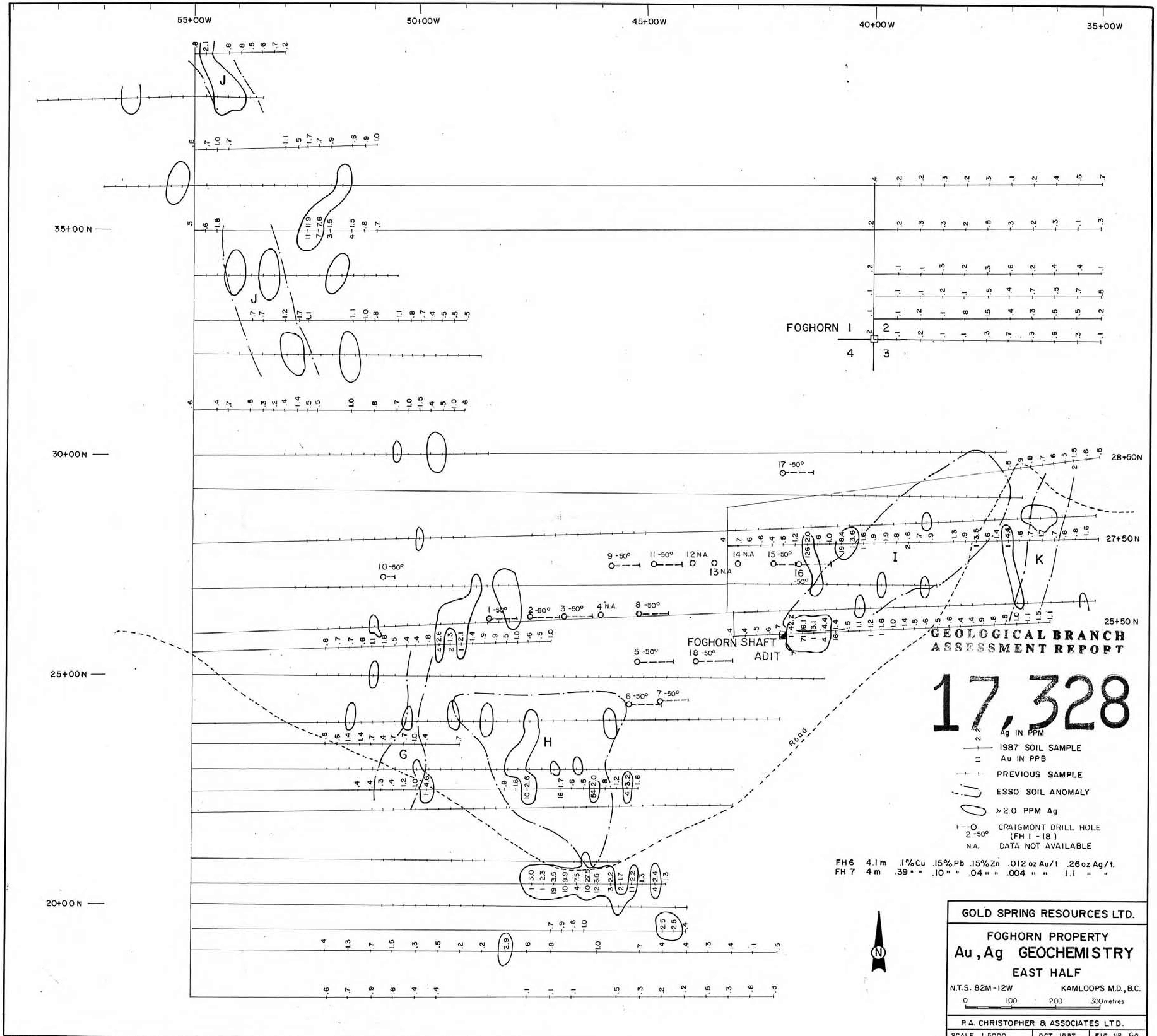
SAMPLE#	CU %	PB %	ZN %	AG OZ/T	AS %	AU OZ/T
01028	.72	33.50	9.85	50.41	.09	.008
01029	1.10	46.40	5.95	46.88	.10	.014
01030	.74	6.11	1.31	5.90	.09	.001
01031	1.32	20.15	16.13	37.64	.09	.014
01032	.32	22.60	2.52	12.71	.13	.004
01033	1.04	82.10	2.39	52.65	.10	.018

TYPE OF WORK IN THIS REPORT	EXTENT OF WORK (IN METRIC UNITS)	ON WHICH CLAIMS	COST APPORTIONED
GEOLOGICAL (scale, area)			
Ground			
Photo			
GEOPHYSICAL (line-kilometres)			
Ground			
Magnetic	60 km	Foghorn 1 to 5 claims	8,733.00
Electromagnetic	60 km	Foghorn 1 to 5 claims	8,733.00
Induced Polarization			
Radiometric			
Seismic			
Other			
Airborne			
GEOCHEMICAL (number of samples analysed for ....)			
Soil	510 soils- 30 element ICP (75 Au by AA)	Foghorn 1 to 5 claims	4,400.00
Silt			
Rock	12 rock samples	Foghorn 1 to 4 claims	243.00
Other			
DRILLING (total metres; number of holes, size)			
Core			
Non-core			
RELATED TECHNICAL			
Sampling/assaying			
Petrographic			
Mineralogic			
Metallurgic			
PROSPECTING (scale, area)		Foghorn 1 to 5 claims	3,799.00
PREPARATORY/PHYSICAL			
Legal surveys (scale, area)			
Topographic (scale, area)			
Photogrammetric (scale, area)			
Line/grid (kilometres)	60 km flagged & chained	Foghorn 1 to 5 claims	19,234.00
Road, local access (kilometres)			
Trench (metres)			
(XXXXXXXXXXXX) Peter Christopher & Associates Inc. (property visit and qualifying (VSE) Report)			3,200.00
		TOTAL COST	$48,342.00

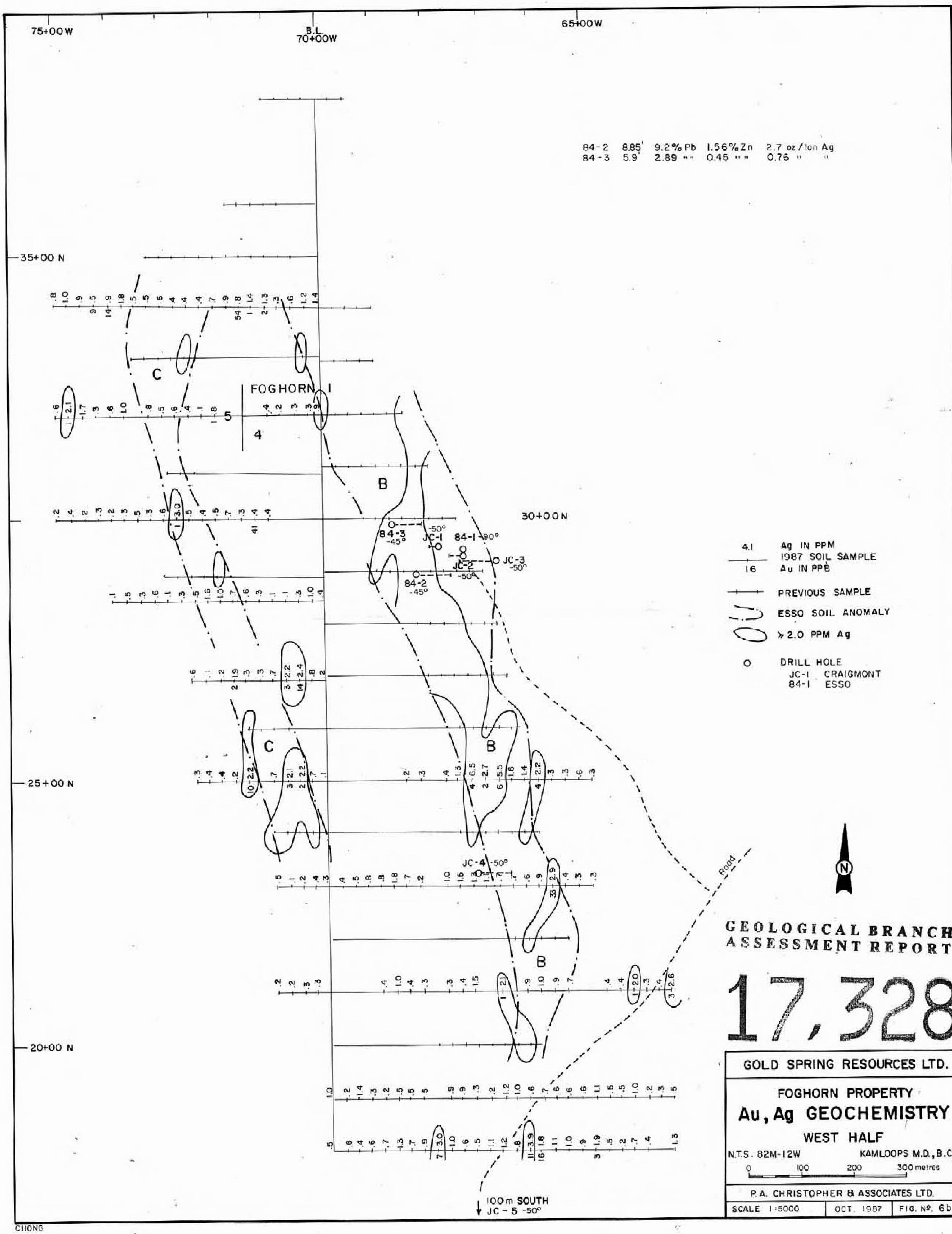
FOR MINISTRY USE ONLY	NAME OF PAC ACCOUNT	DEBIT	CREDIT	REMARKS:
Value work done (from report)				
Value of work approved				
Value claimed (from statement)				
Value credited to PAC account				
Value debited to PAC account				
Accepted .... Date	Rept. No.			Information Class

TYPE OF WORK IN THIS REPORT	EXTENT OF WORK (IN METRIC UNITS)	ON WHICH CLAIMS	COST APPORTIONED
GEOLOGICAL (scale, area)			
Ground			
Photo			
GEOPHYSICAL (line-kilometres)			
Ground			
Magnetic	60 km	Foghorn 1 to 5 claims	8,733.00
Electromagnetic	60 km	Foghorn 1 to 5 claims	8,733.00
Induced Polarization			
Radiometric			
Seismic			
Other			
Airborne			
GEOCHEMICAL (number of samples analysed for ....)			
Soil	510 soils- 30 element ICP (75 Au by AA)	Foghorn 1 to 5 claims	4,400.00
Silt			
Rock	12 rock samples	Foghorn 1 to 4 claims	243.00
Other			
DRILLING (total metres; number of holes, size)			
Core			
Non-core			
RELATED TECHNICAL			
Sampling/assaying			
Petrographic			
Mineralogic			
Metallurgic			
PROSPECTING (scale, area)		Foghorn 1 to 5 claims	3,799.00
PREPARATORY/PHYSICAL			
Legal surveys (scale, area)			
Topographic (scale, area)			
Photogrammetric (scale, area)			
Line/grid (kilometres)	60 km flagged & chained	Foghorn 1 to 5 claims	19,234.00
Road, local access (kilometres)			
Trench (metres)			
(XXXXXXXXXXXXX) Peter Christopher & Associates Inc. (property visit and qualifying (VSE) Report)			3,200.00
		TOTAL COST	$48,342.00

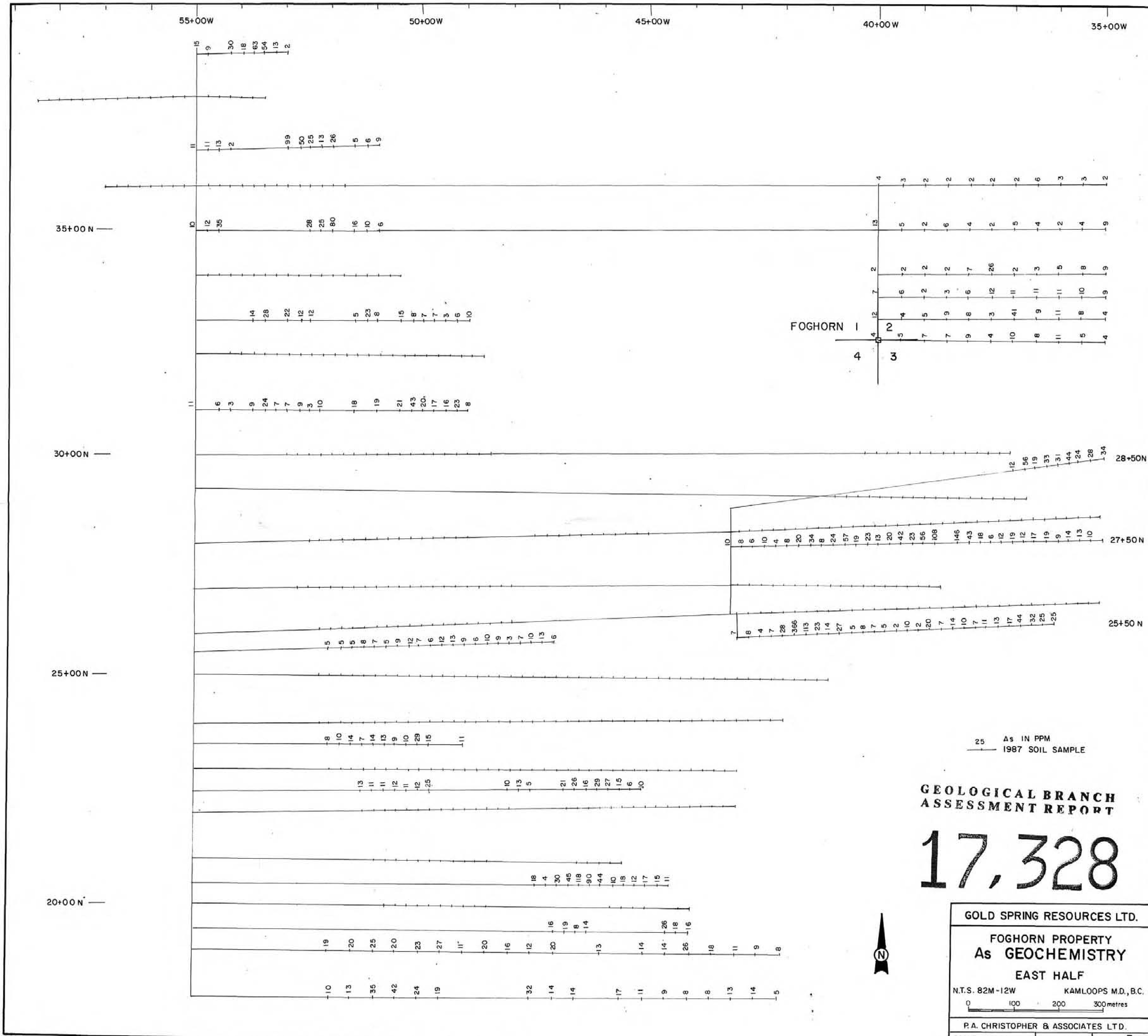
FOR MINISTRY USE ONLY	NAME OF PAC ACCOUNT	DEBIT	CREDIT	REMARKS:
Value work done (from report)				
Value of work approved				
Value claimed (from statement)				
Value credited to PAC account				
Value debited to PAC account				
Accepted .... Date	Rept. No.			Information Class

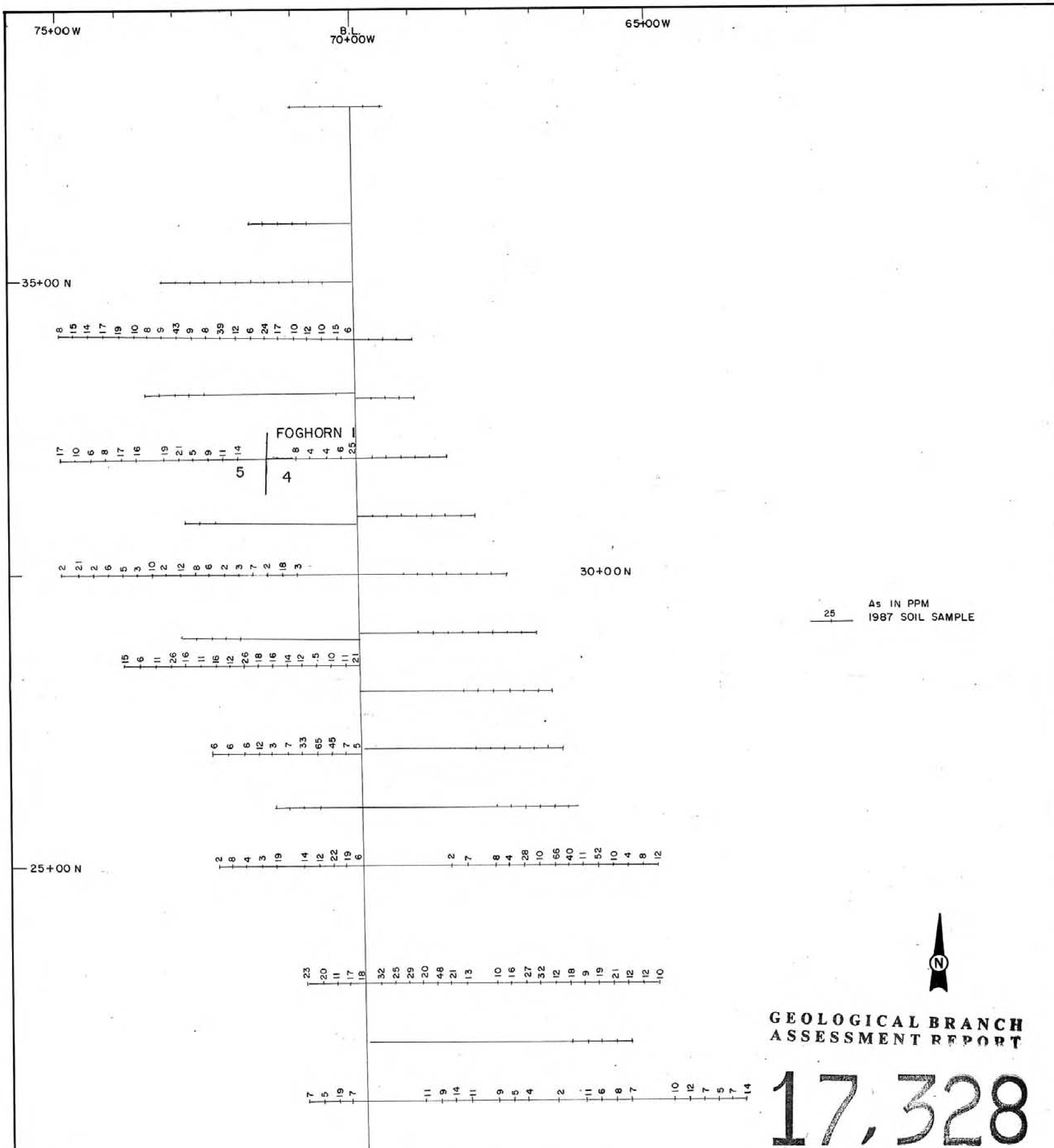


55+00W
50+00W
45+00W
40+00W
35+00W
35+00N
30+00N
25+00N
20+00N
28+50N
27+50N
25+50N
FOGHORN 1 2
4 3
FOGHORN SHAFT
ADIT
Road
J
I
K
G
H
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
Ag IN PPM
1987 SOIL SAMPLE
Au IN PPB
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
≥ 2.0 PPM Ag
CRAIGMONT DRILL HOLE (FH 1 - 18)
N.A. DATA NOT AVAILABLE
FH6 4.1 m .1% Cu .15% Pb .15% Zn .012 oz Au/t .26 oz Ag/t.
FH 7 4 m .39 " " .10 " " .04 " " .004 " " 1.1 " "
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Au, Ag GEOCHEMISTRY
EAST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. Nº. 60
CHONG



75+00 W
B.L. 70+00W
65+00W
84-2 8.85' 9.2% Pb 1.56% Zn 2.7 oz/ton Ag
84-3 5.9' 2.89 " " 0.45 " " 0.76 " "
35+00 N
30+00 N
25+00 N
20+00 N
FOGHORN 1
C
B
84-3 -45°
JC-1
84-1 -90°
JC-2 -50°
JC-3 -50°
84-2 -45°
JC-4 -50°
Road
100 m SOUTH
JC-5 -50°
4.1 Ag IN PPM
1987 SOIL SAMPLE
16 Au IN PPB
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
≥ 2.0 PPM Ag
DRILL HOLE
JC-1 CRAIGMONT
84-1 ESSO
N
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Au, Ag GEOCHEMISTRY
WEST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. Nº. 6b
CHONG


55+00W
50+00W
45+00W
40+00W
35+00W
35+00 N
30+00 N
25+00 N
20+00 N
28+50N
27+50 N
25+50 N
FOGHORN 1 2
4 3
25 As IN PPM
1987 SOIL SAMPLE
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
As GEOCHEMISTRY
EAST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. No. 7a
CHONG



GOLD SPRING RESOURCES LTD.

FOGHORN PROPERTY

As GEOCHEMISTRY

WEST HALF

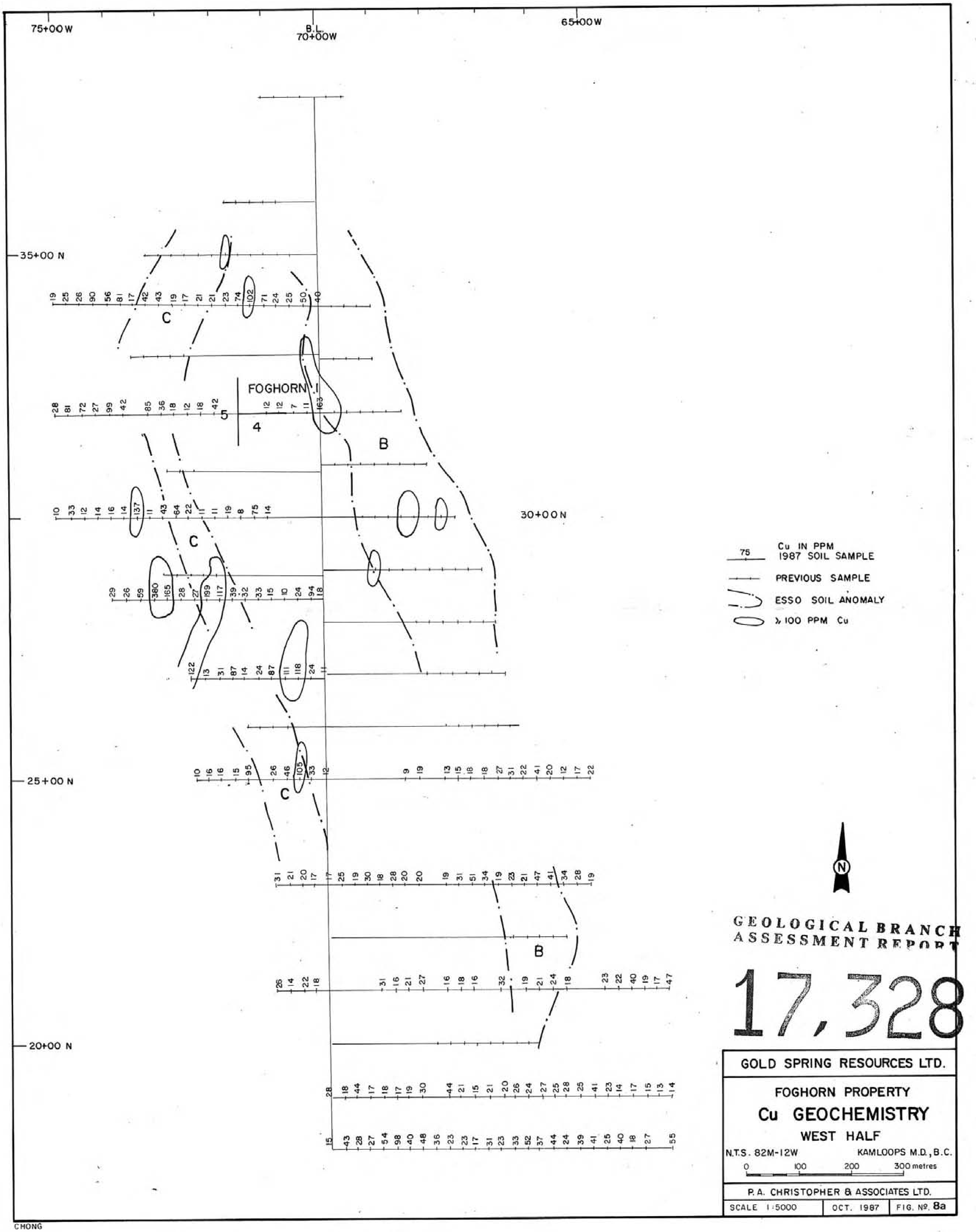
N.T.S. 82M-12W — KAMLOOPS M.D., B.C.

0 100 200 300 metres

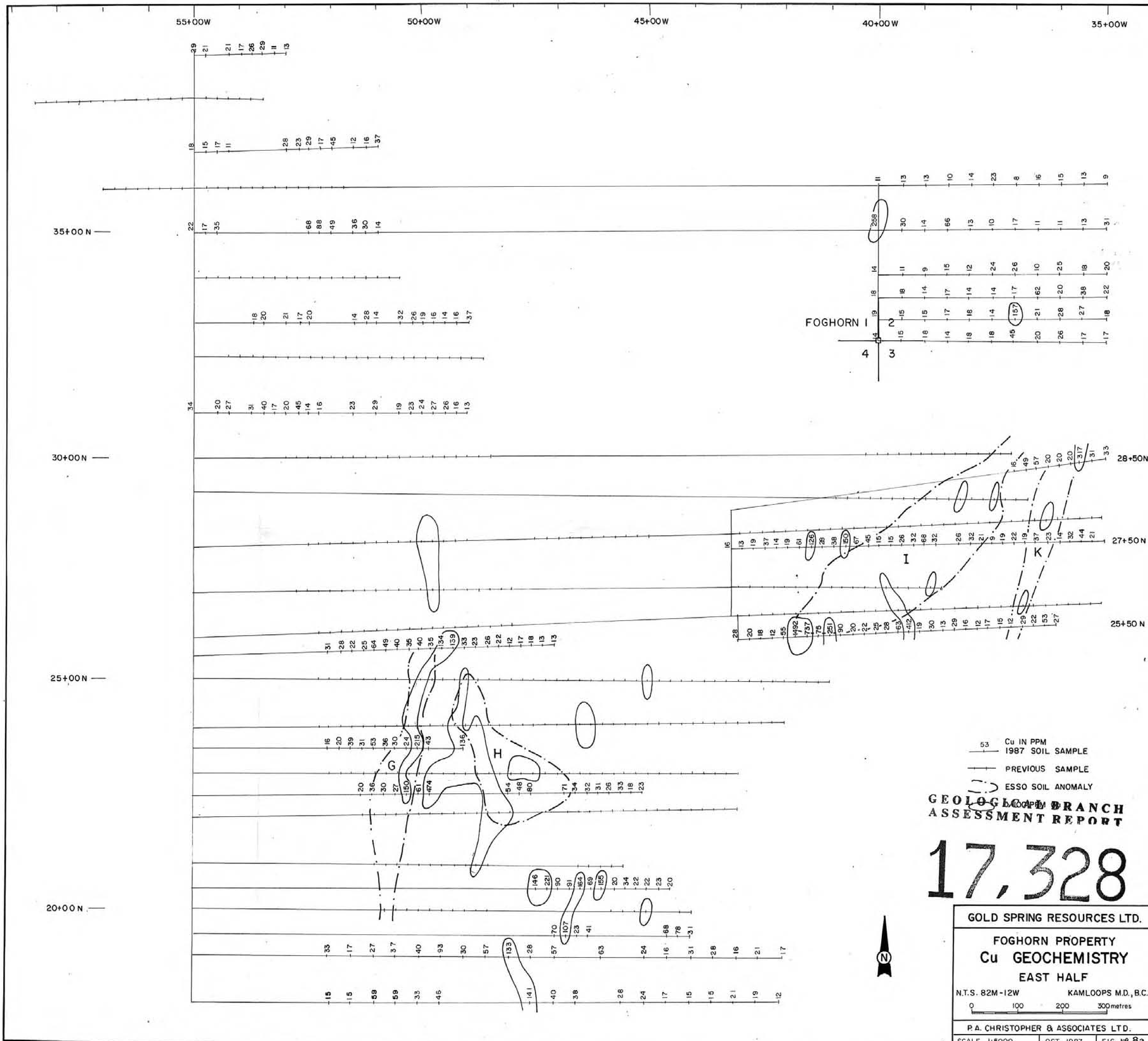
P.A. CHRISTOPHER & ASSOCIATES LTD.

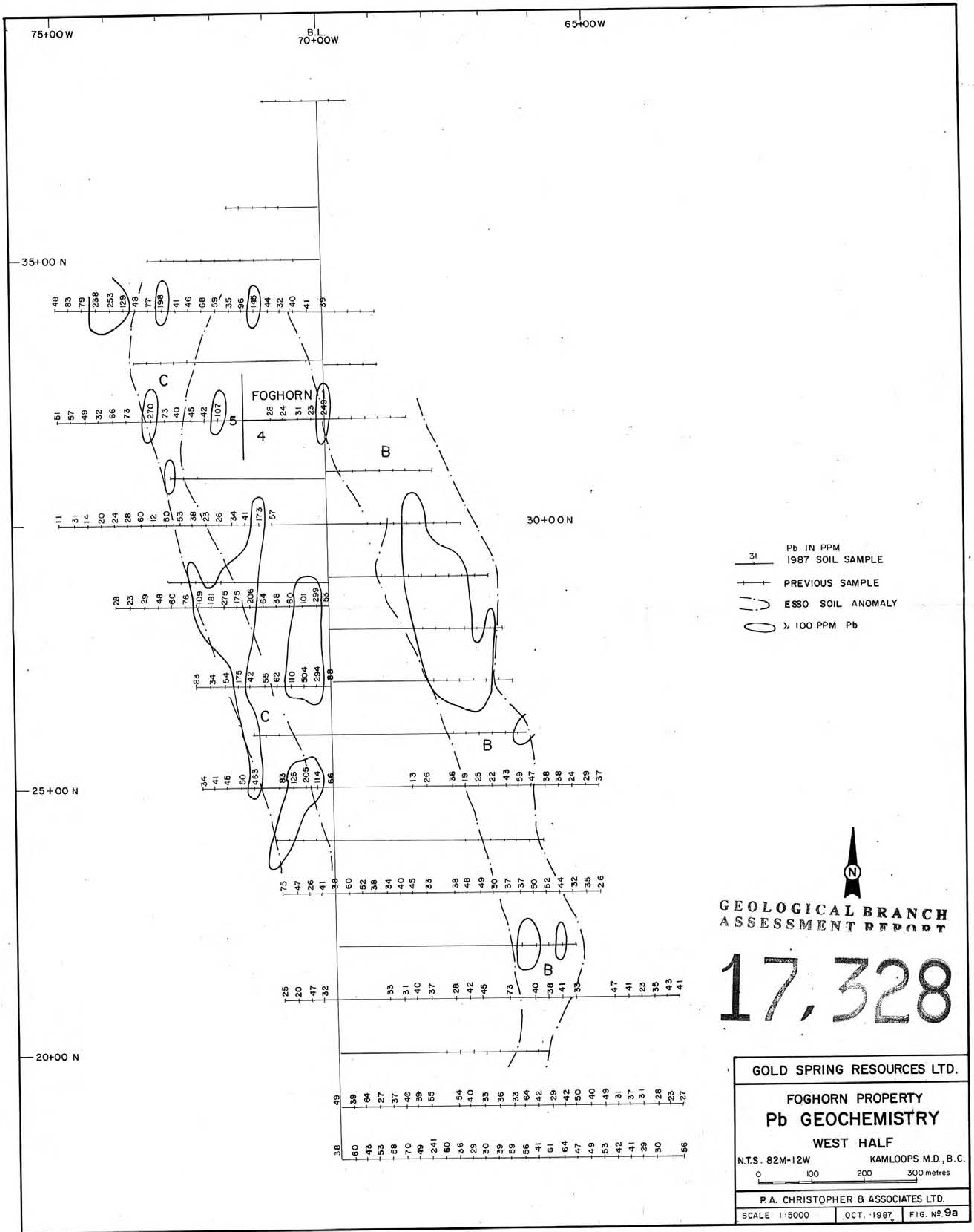
SCALE 1:5000	OCT. 1987	FIG. Nº. 7b

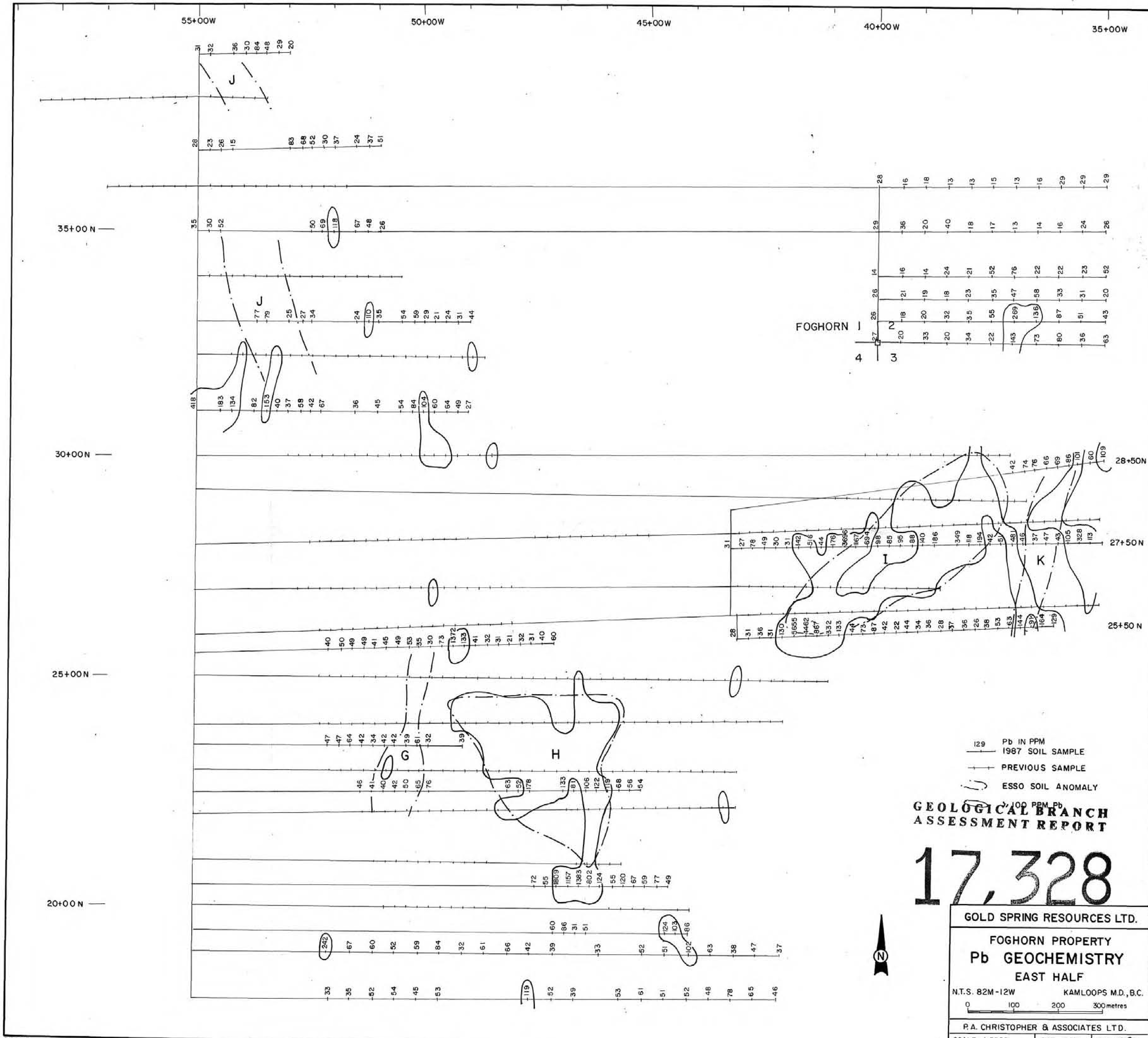
CHONG



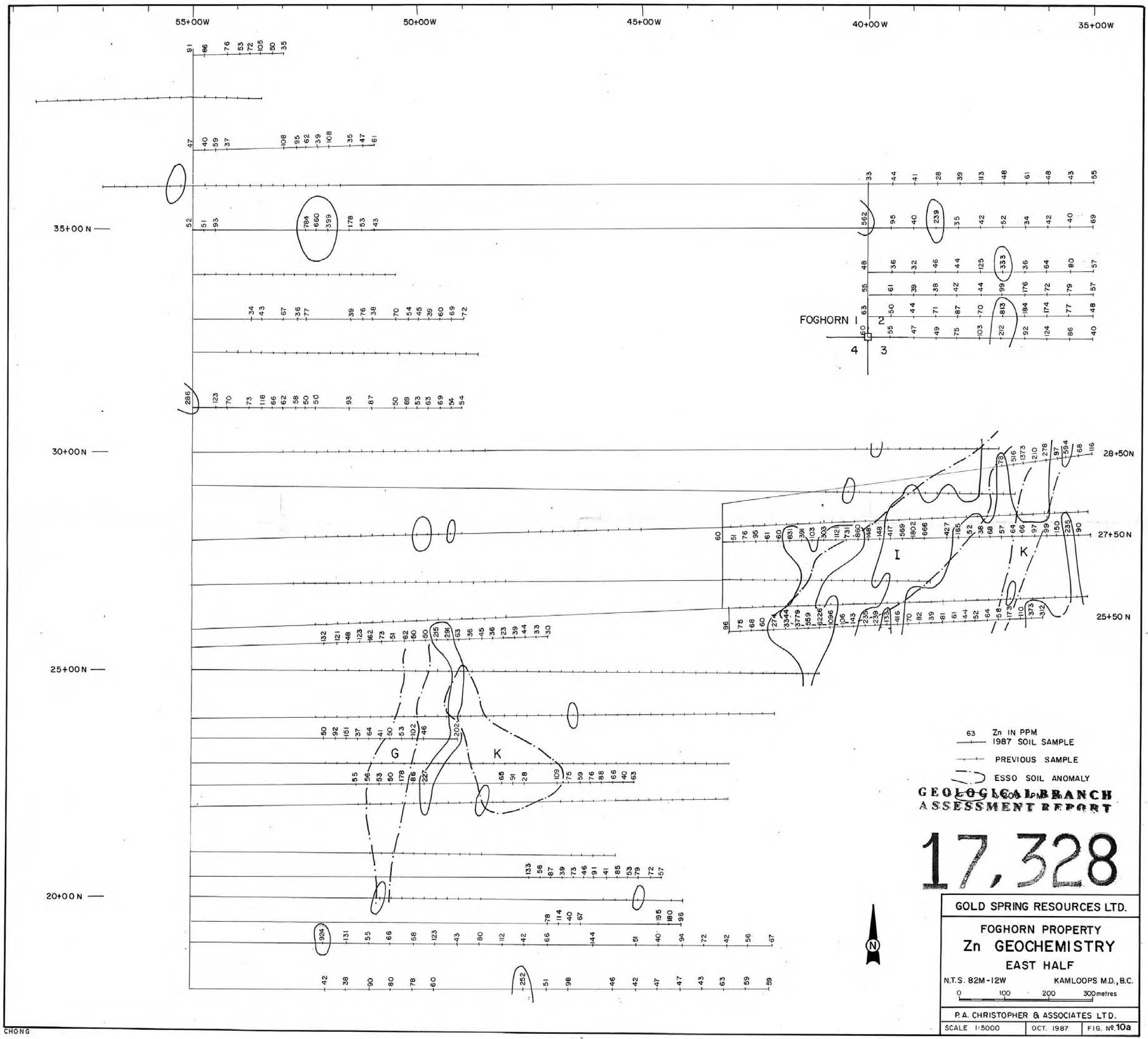
75+00 W
B.L.
70+00W
65+00W
35+00 N
30+00 N
25+00 N
20+00 N
FOGHORN I
5
4
C
B
Cu IN PPM
75
1987 SOIL SAMPLE
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
≥ 100 PPM Cu
N
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Cu GEOCHEMISTRY
WEST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0
100
200
300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. Nº. 8a
CHONG


55+00W
50+00W
45+00W
40+00W
35+00W
35+00N
30+00N
25+00N
20+00N
28+50N
27+50N
25+50 N
FOGHORN I
2
4
3
G
H
I
K
53 Cu IN PPM
1987 SOIL SAMPLE
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Cu GEOCHEMISTRY
EAST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. Nº 8a
CHONG

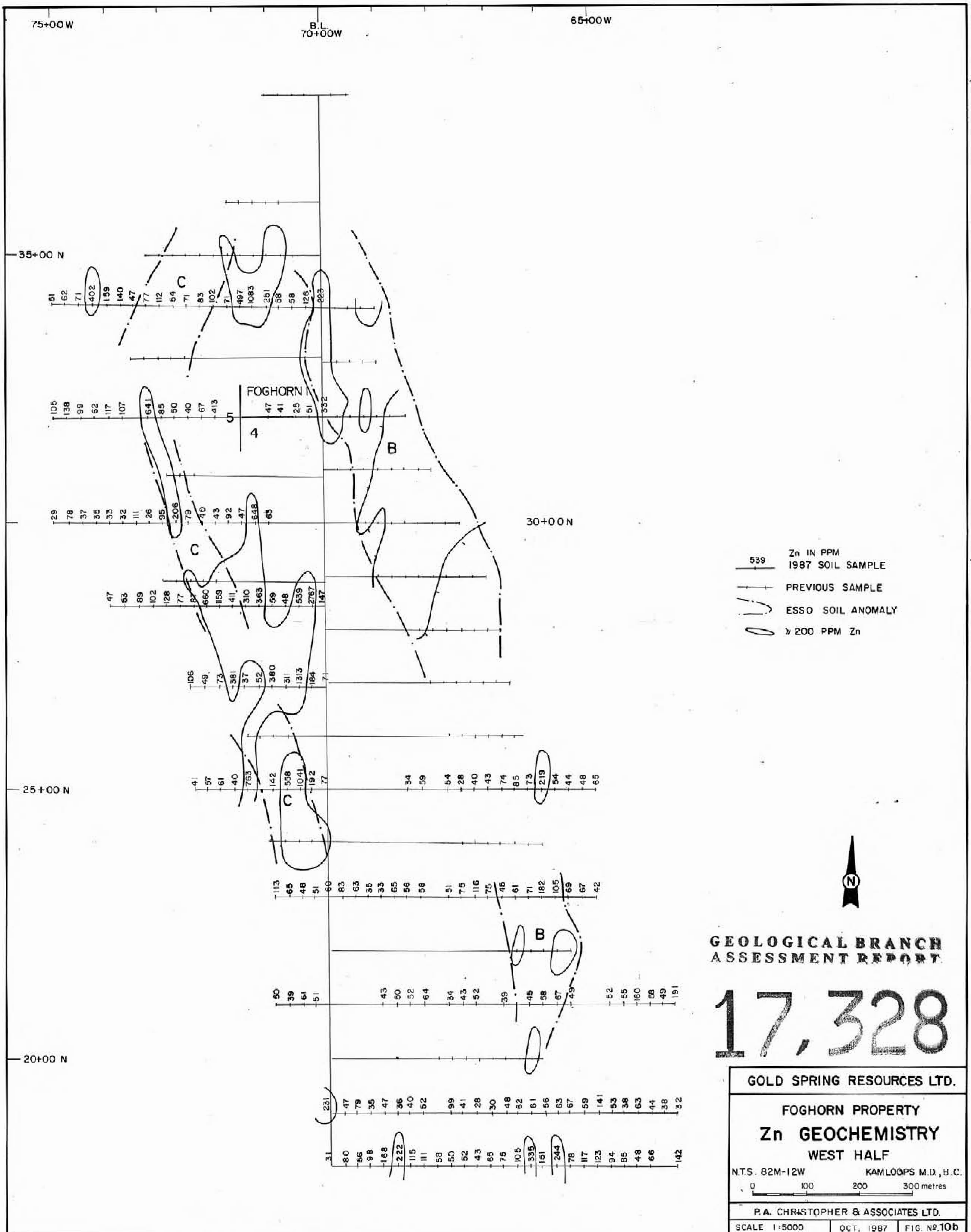

75+00 W
B.L.
70+00 W
65+00 W
35+00 N
30+00 N
25+00 N
20+00 N
FOGHORN
5
4
B
C
Pb IN PPM
1987 SOIL SAMPLE
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
≥ 100 PPM Pb
N
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Pb GEOCHEMISTRY
WEST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. Nº 9a
CHONG

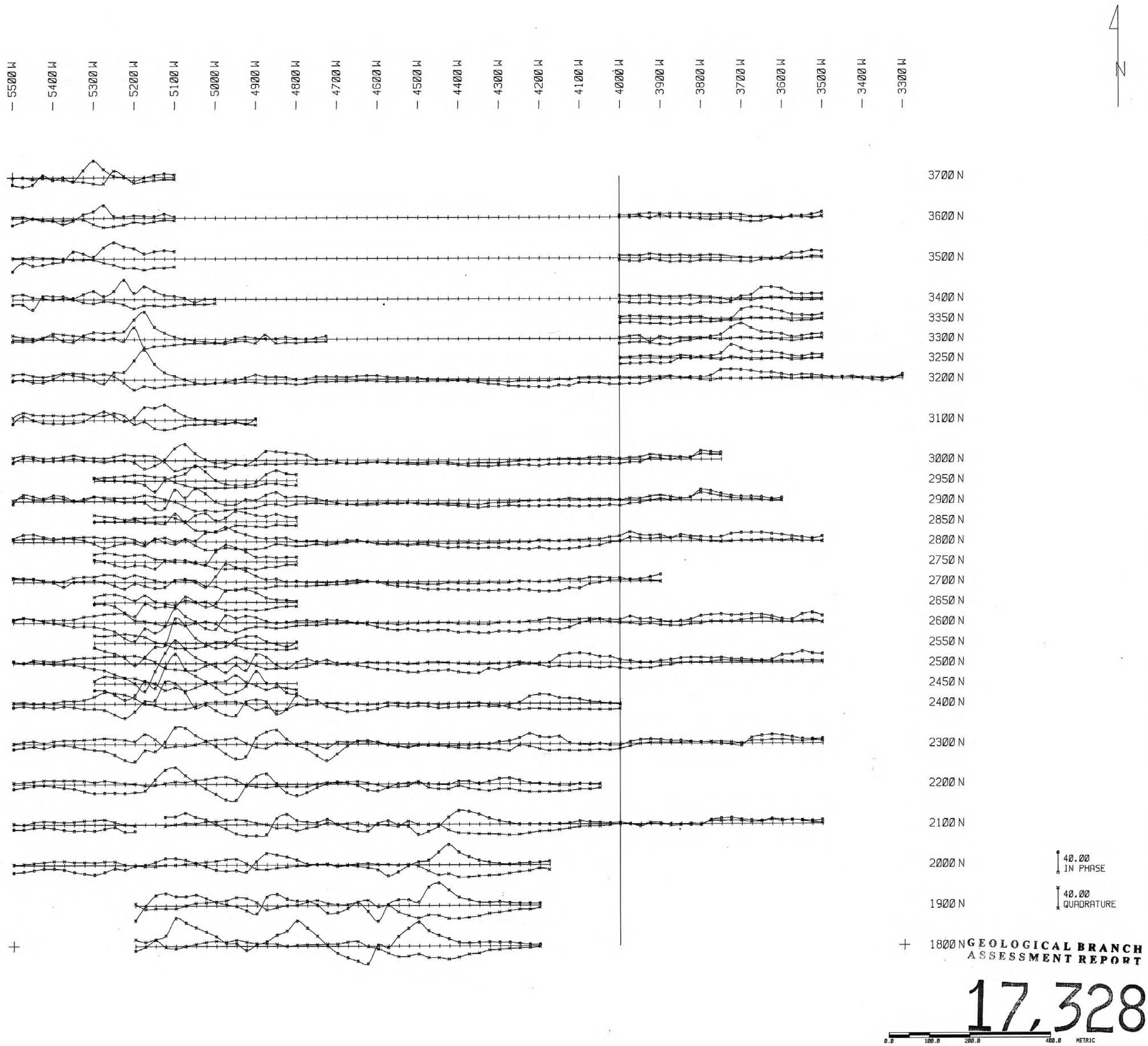


55+00W
50+00W
45+00W
40+00W
35+00W
35+00 N
30+00N
25+00N
20+00N
28+50N
27+50N
25+50 N
FOGHORN 1 2
4 3
J
G
H
I
K
129 Pb IN PPM 1987 SOIL SAMPLE
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
>100 PPM Pb
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Pb GEOCHEMISTRY
EAST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. No. 9a
CHONG



55+00W
50+00W
45+00W
40+00W
35+00W
35+00N
30+00N
25+00N
20+00N
28+50N
27+50N
25+50N
FOGHORN 1 2
4 3
I
K
G
K
63 Zn IN PPM
1987 SOIL SAMPLE
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
N
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Zn GEOCHEMISTRY
EAST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. No. 10a
CHONG

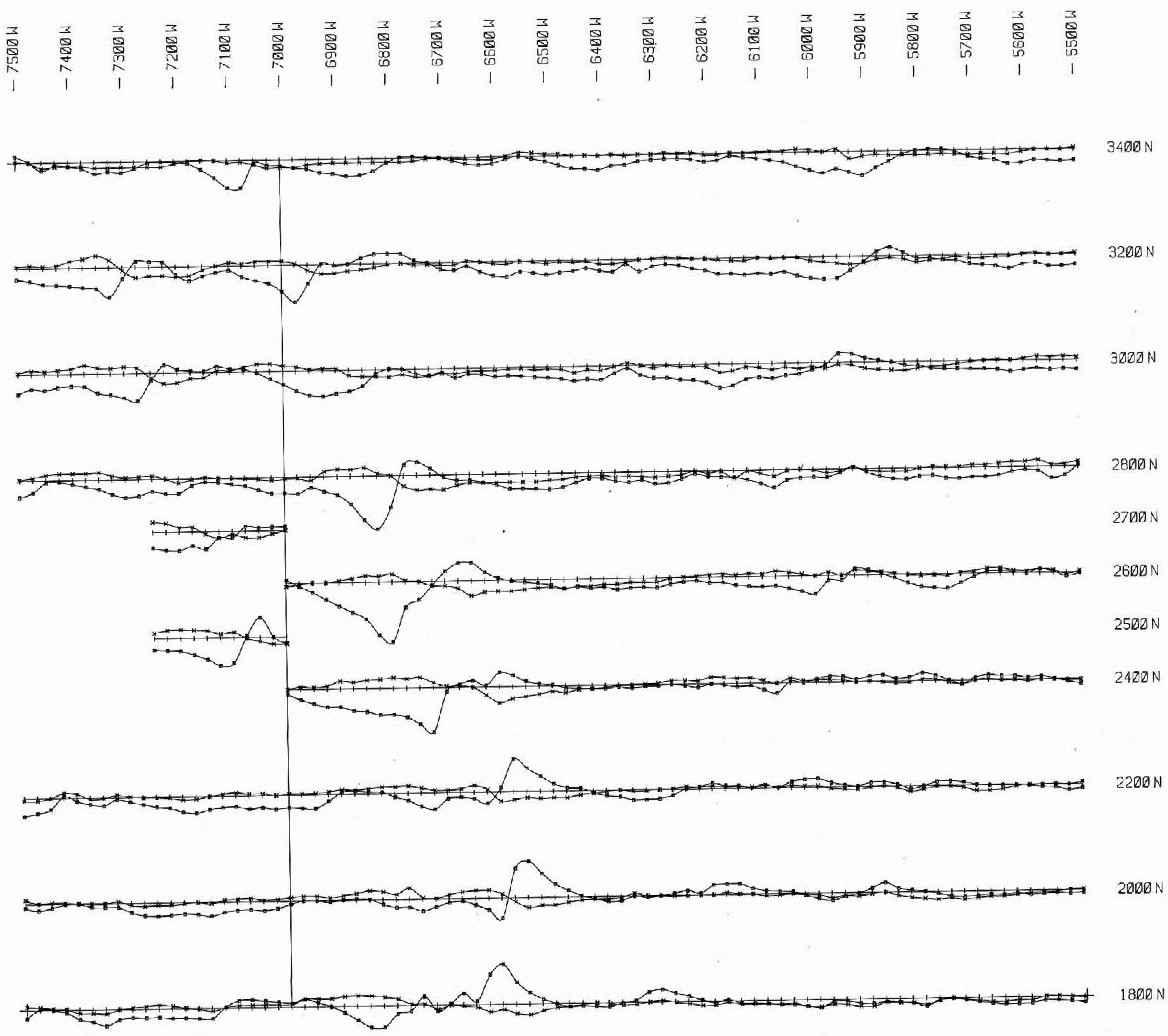

75+00W
B.L. 70+00W
65+00W
35+00 N
30+00N
25+00 N
20+00 N
FOGHORN
5
4
C
B
Zn IN PPM
539 1987 SOIL SAMPLE
PREVIOUS SAMPLE
ESSO SOIL ANOMALY
≥ 200 PPM Zn
N
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,328
GOLD SPRING RESOURCES LTD.
FOGHORN PROPERTY
Zn GEOCHEMISTRY
WEST HALF
N.T.S. 82M-12W
KAMLOOPS M.D., B.C.
0 100 200 300 metres
P.A. CHRISTOPHER & ASSOCIATES LTD.
SCALE 1:5000
OCT. 1987
FIG. No. 10b
CHONG



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,328

SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD.	FOGHORN EAST GRID VLF-EM PROFILES	SCALE: 1:5000
GEONICS EM-16 & SEATTLE VLF TRANSMITTER	DATE: DEC. 2, 1987	VANCOUVER, B.C.	TO ACCOMPANY REPORT BY: E.R. ROCKEL INTERPRETEX RESOURCES LTD. VANCOUVER, B.C.	PROJECT NO.: 87428
OPERATOR FACED WESTERLY WHILE READING	FIGURE = G-1			N.T.S. NO.: 82 M/12W



N

40.00 IN PHASE

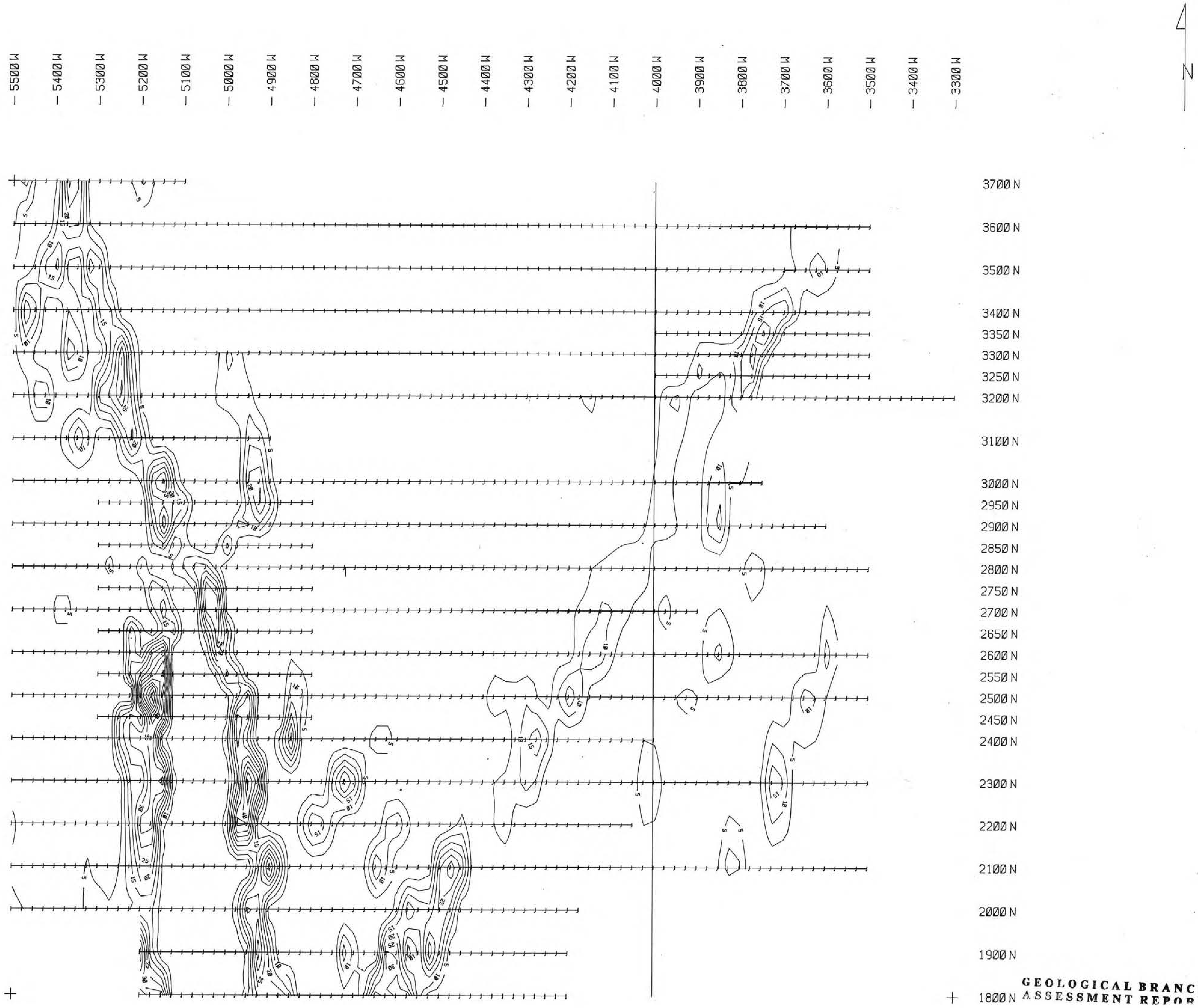
40.00 QUADRATURE

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,328

0.0 100.0 200.0 400.0 METRIC

SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD. VANCOUVER, B.C.	FOGHORN WEST GRID VLF-EM PROFILES	SCALE: 1:5000
GEONICS EM-16 & SEATTLE VLF TRANSMITTER	DATE: DEC. 2, 1987		TO ACCOMPANY REPORT BY: E.R. ROCKEL INTERPRETEX RESOURCES LTD. VANCOUVER, B.C.	PROJECT NO.: 87428
OPERATOR FACED WESTERLY WHILE READING	FIGURE # G-2			N.T.S. NO.: 82 M/12W

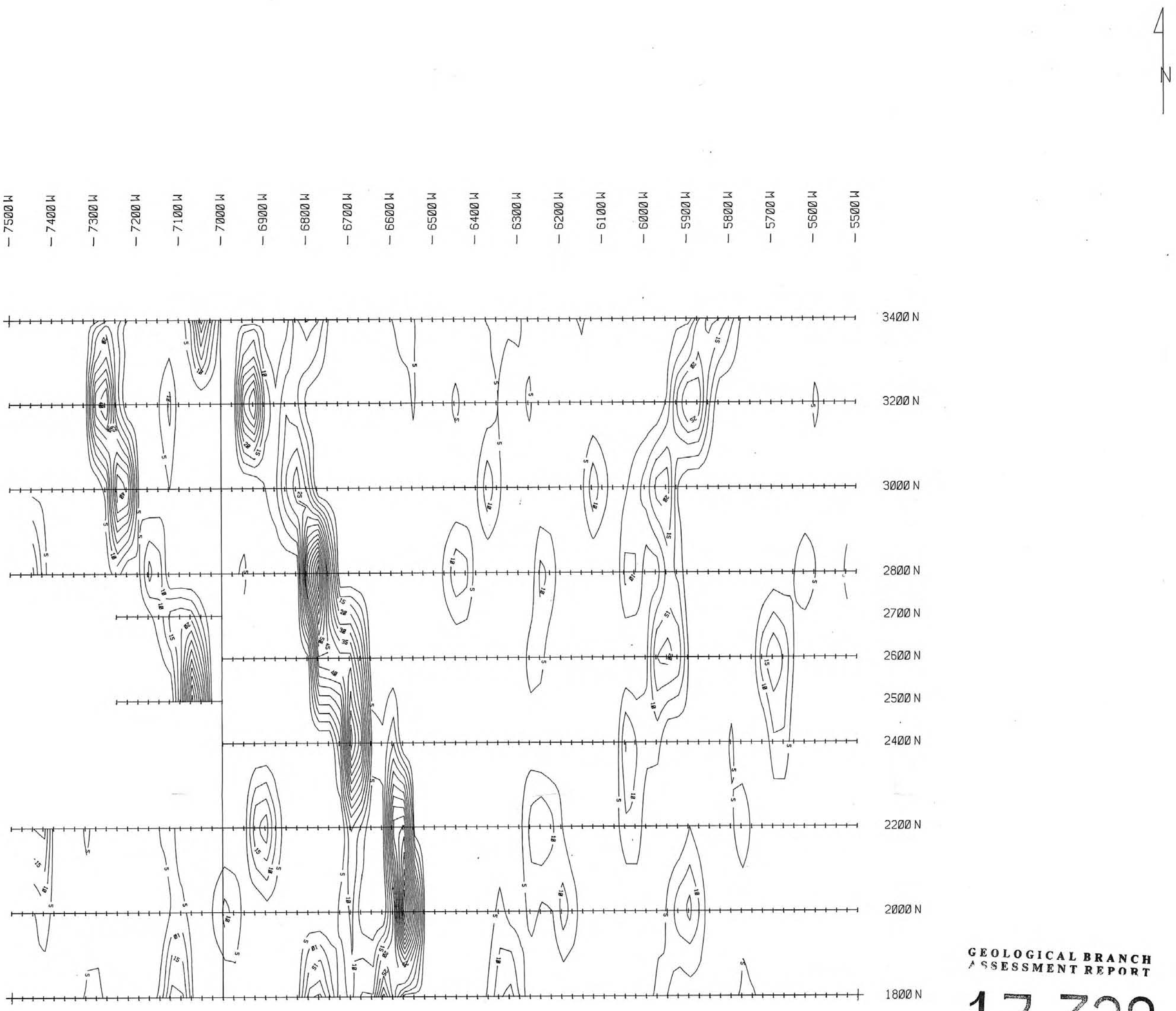


GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,328

0.0 100.0 200.0 400.0 METRIC

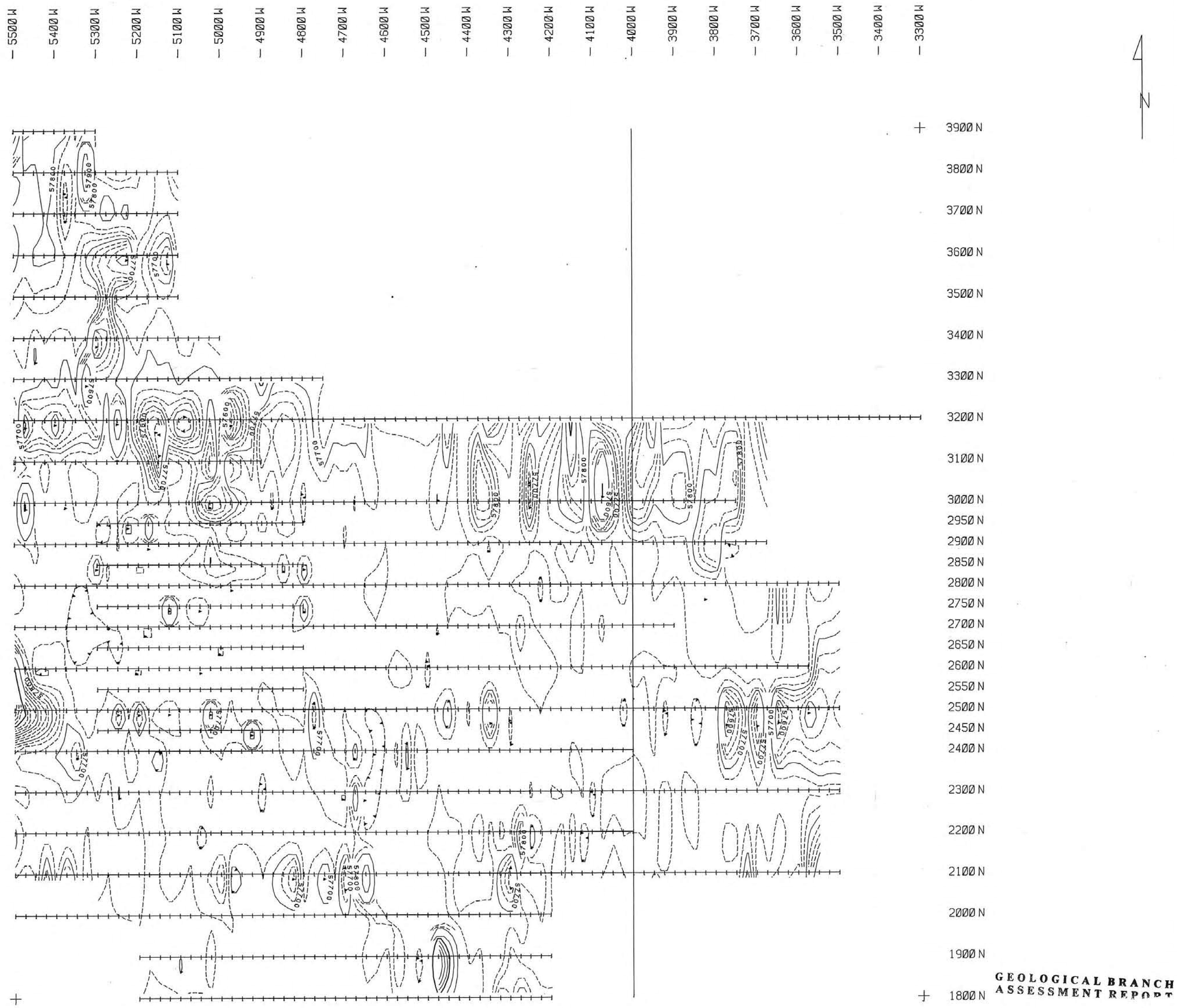
SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD. VANCOUVER, B.C.	FOGHORN EAST - FRASER FILTER CONTOURS TO ACCOMPANY REPORT BY: E.R. ROCKEL INTERPRETEX RESOURCES LTD. VANCOUVER, B.C.	SCALE: 1:5000
GEONICS EM-16 & SEATTLE VLF TRANSMITTER	DATE: DEC. 2, 1987			PROJECT NO.: 87428
OPERATOR FACED WESTERLY WHILE READING	FIGURE # G-3			N.T.S. NO.: 82 M/12W



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,328

SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD. VANCOUVER, B.C.	FOGHORN WEST - FRASER FILTER CONTOURS TO ACCOMPANY REPORT BY: E.R. ROCKEL INTERPRETEX RESOURCES LTD. VANCOUVER, B.C.	SCALE: 1:5000
GEONICS EM-16 & SEATTLE VLF TRANSMITTER	DATE: DEC. 2, 1987			PROJECT NO.: 87428
OPERATOR FACED WESTERLY WHILE READING	FIGURE # G-4			N.T.S. NO.: 82 M/12W

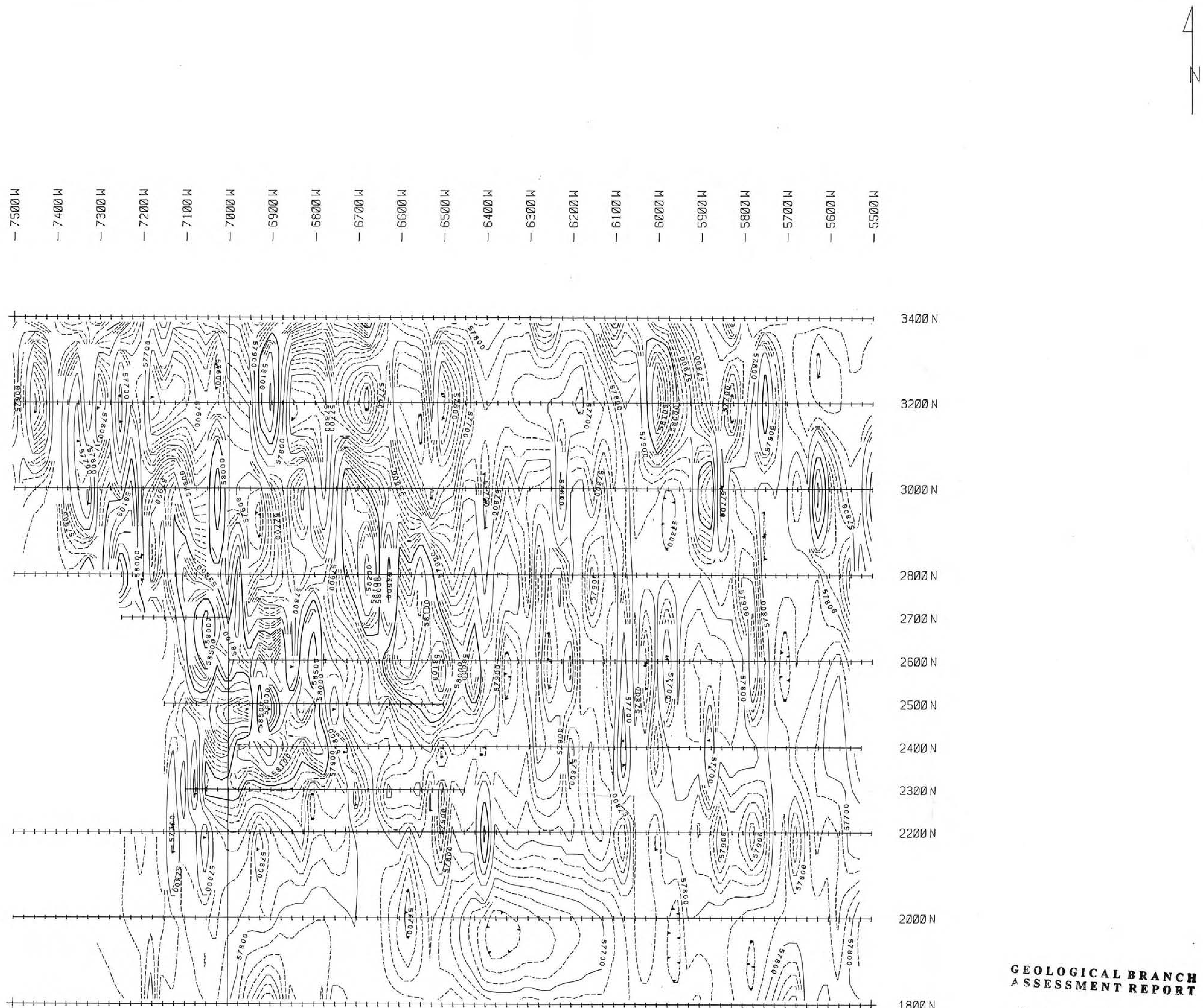


GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,328

0.0 100.0 200.0 400.0 METRIC

SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD. VANCOUVER, B.C.	FOGHORN EAST GRID MAGNETIC CONTOURS TO ACCOMPANY REPORT BY: E.R. ROCKEL INTERPRETEX RESOURCES LTD. VANCOUVER, B.C.	SCALE: 1:5000
GEOMETRICS G-816 MAGNETOMETER AND	DATE: DEC. 2, 1987			PROJECT NO.: 87428
G-856 MAGNETOMETER BASE STATION	FIGURE # G-5			N.T.S. NO.: 82 M/12W

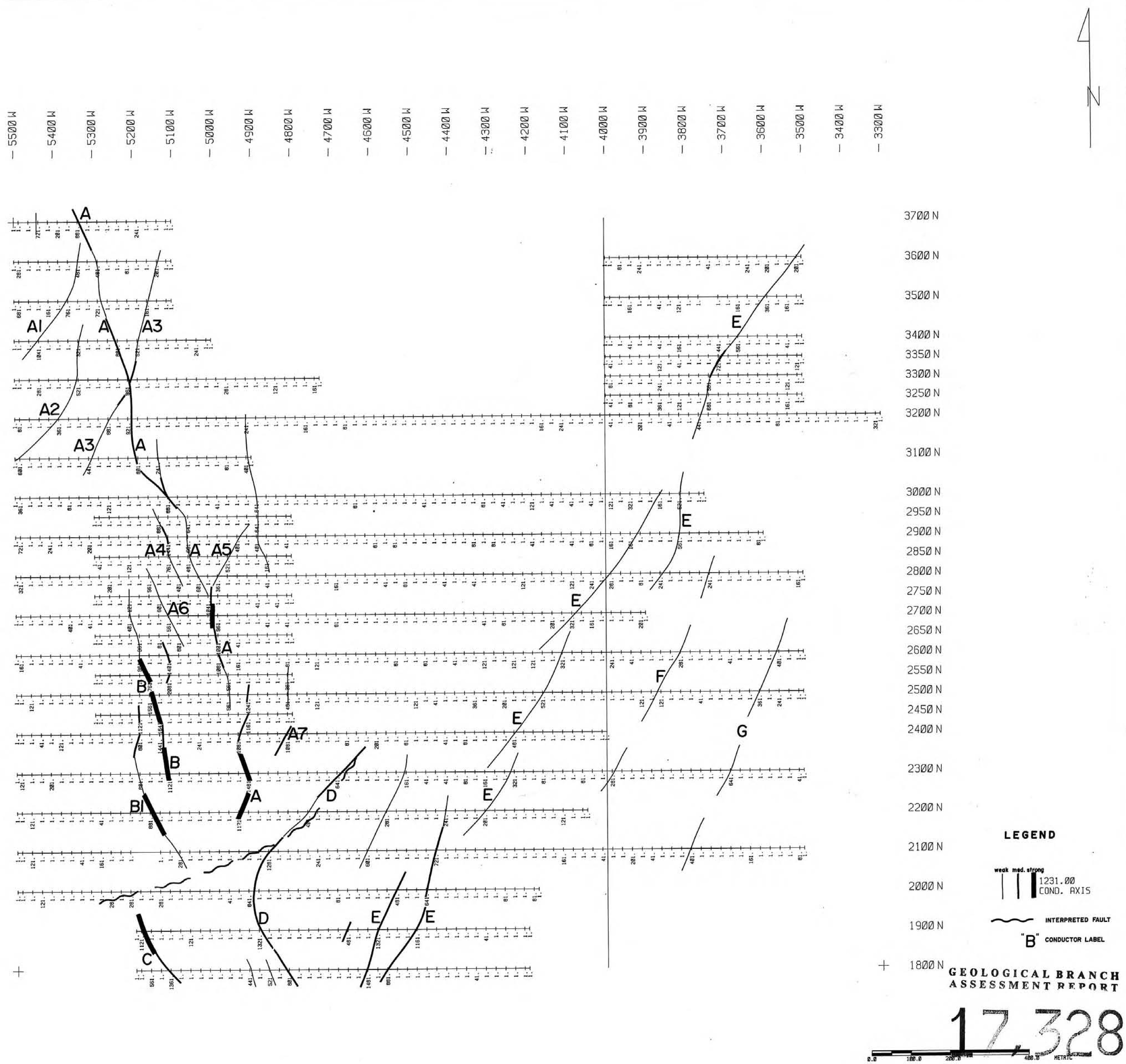


GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,328

0.0 100.0 200.0 400.0 METRIC

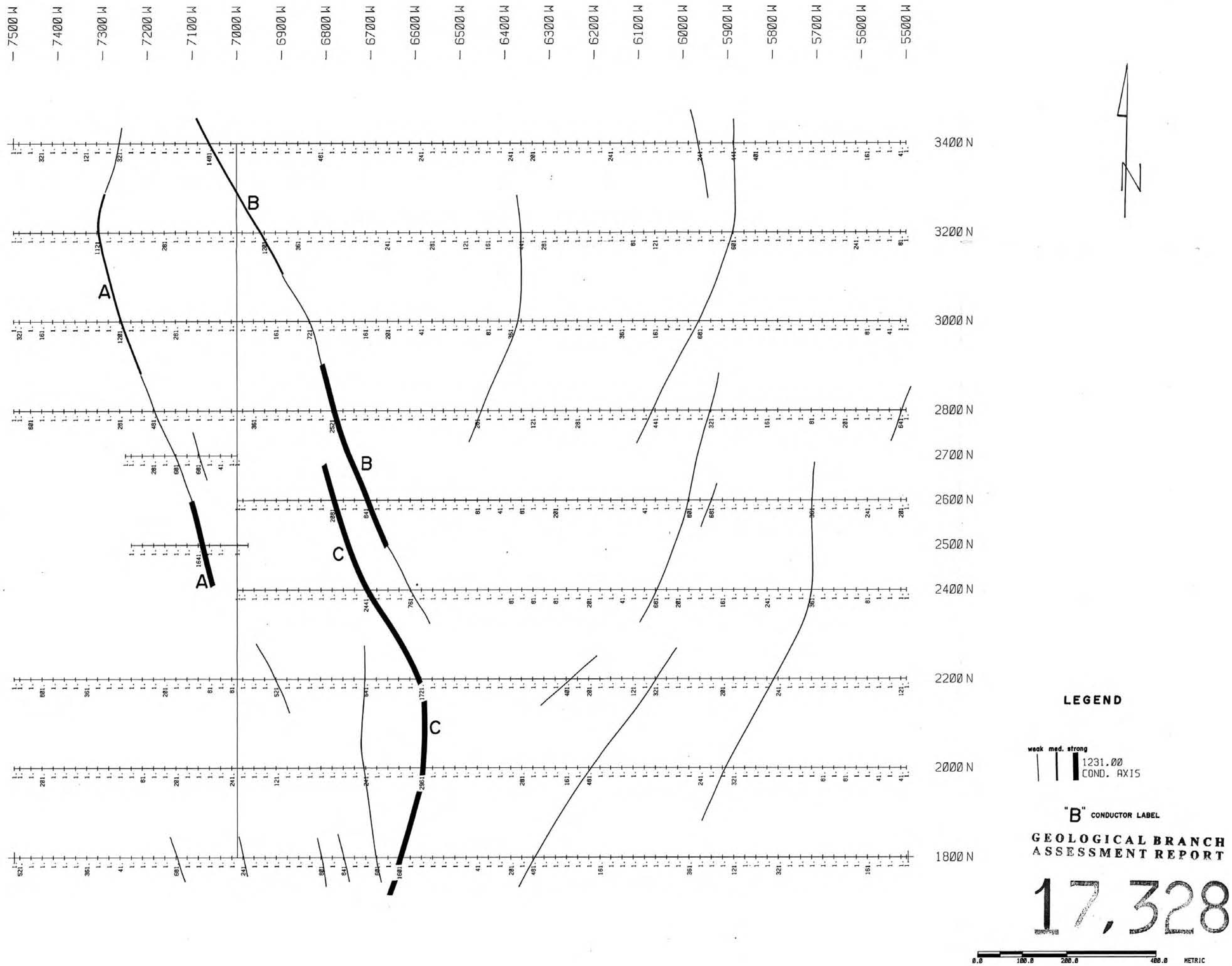
SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD.	FOGHORN WEST GRID MAGNETIC CONTOURS	SCALE: 1:5000
GEOMETRICS G-816 MAGNETOMETER AND	DATE: DEC. 2, 1987	VANCOUVER, B.C.	TO ACCOMPANY REPORT BY: E.R. ROCKEL, INTERPRETEX RESOURCES LTD., VANCOUVER, B.C.	PROJECT NO.: 87428
G-856 MAGNETOMETER BASE STATION	FIGURE # G-6			N.T.S. NO.: 82 M/12W



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,328

SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD. VANCOUVER, B.C.	FOGHORN EAST GEOPHYSICAL INTERPRETATION TO ACCOMPANY REPORT BY: E.R. ROCKEL INTERPRETEX RESOURCES LTD. VANCOUVER, B.C.	SCALE: 1:5000
LEGEND: COND AXIS = 1ST DERIV PEAK VALUE	DATE: DEC. 2, 1987			PROJECT NO.: 87428
MAG ANOMALY = "+M" (HI), "-M" (LO)	FIGURE # G-7			N.T.S. NO.: 82 M/12W



SURVEYED BY: RENEGADE MINERAL EXPL. SERVICES LTD.	DRAWN BY: E.R. ROCKEL	GOLDSPRING RESOURCES LTD. VANCOUVER, B.C.	FOGHORN WEST GEOPHYSICAL INTERPRETATION TO ACCOMPANY REPORT BY: E.R. ROCKEL INTERPRETEX RESOURCES LTD. VANCOUVER, B.C.	SCALE: 1:5000
LEGEND: COND AXIS = 1ST DERIV PEAK VALUE	DATE: DEC. 2, 1987			PROJECT NO.: 87428
MAG ANOMALY = "+H" (HI), "-H" (LO)	FIGURE # G-8			N.T.S. NO.: 82 M/12W