ARIS SUMMARY SHEET

District Geologist, Prince George Off Confidential: 89.04.22

ASSESSMENT REPORT 17457 MINING DIVISION: Omineca

PROPERTY: Heidi-Lay
LOCATION: LAT 56 27 30 LONG 125 46 20
UTM 10 6260325 329173
NTS 094C05W 094C05E
CLAIM(S): Heidi 1-2,Lay 1-4
OPERATOR(S): Skylark Res.
AUTHOR(S): McAtee, C.L.
REPORT YEAR: 1988, 35 Pages
GEOLOGICAL
SUMMARY: Upper Triassic Takla Group rocks are in fault contact with Mississippian Slide Mountain Group volcanic and sedimentary rocks intruded by quartz-biotite porphyry dykes or plugs. Low precious metal values occur in narrow quartz and quartz-carbonate vein systems.

WORK
DONE: Geological,Geochemical
GEOL 2300.0 ha
ROCK 44 sample(s) ;ME
SILT 9 sample(s) ;ME
SOIL 342 sample(s) ;ME
MINFILE: 094C 010,094C 011,094C 012,094C 013

GEOLOGICAL REPORT

ON THE

HEIDI - LAY MINERAL CLAIMS

Aiken Lake Area
Omineca Mining Division, British Columbia
94 C/5 E + W

56°28'45" N. Latitude
125°47'18" W. Longitude

For

OPERATOR:

Skylark Resources Ltd.
#902-837 West Hastings Street
Vancouver, B.C.
V6C 1B6

OWNER:

John M. Mirko
Vancouver, B.C.

By

Christopher L. McAtee, B.Sc., M.Sc.

April, 1988

TABLE OF CONTENTS

ILLUSTRATIONS

INTRODUCTION

Location and Access

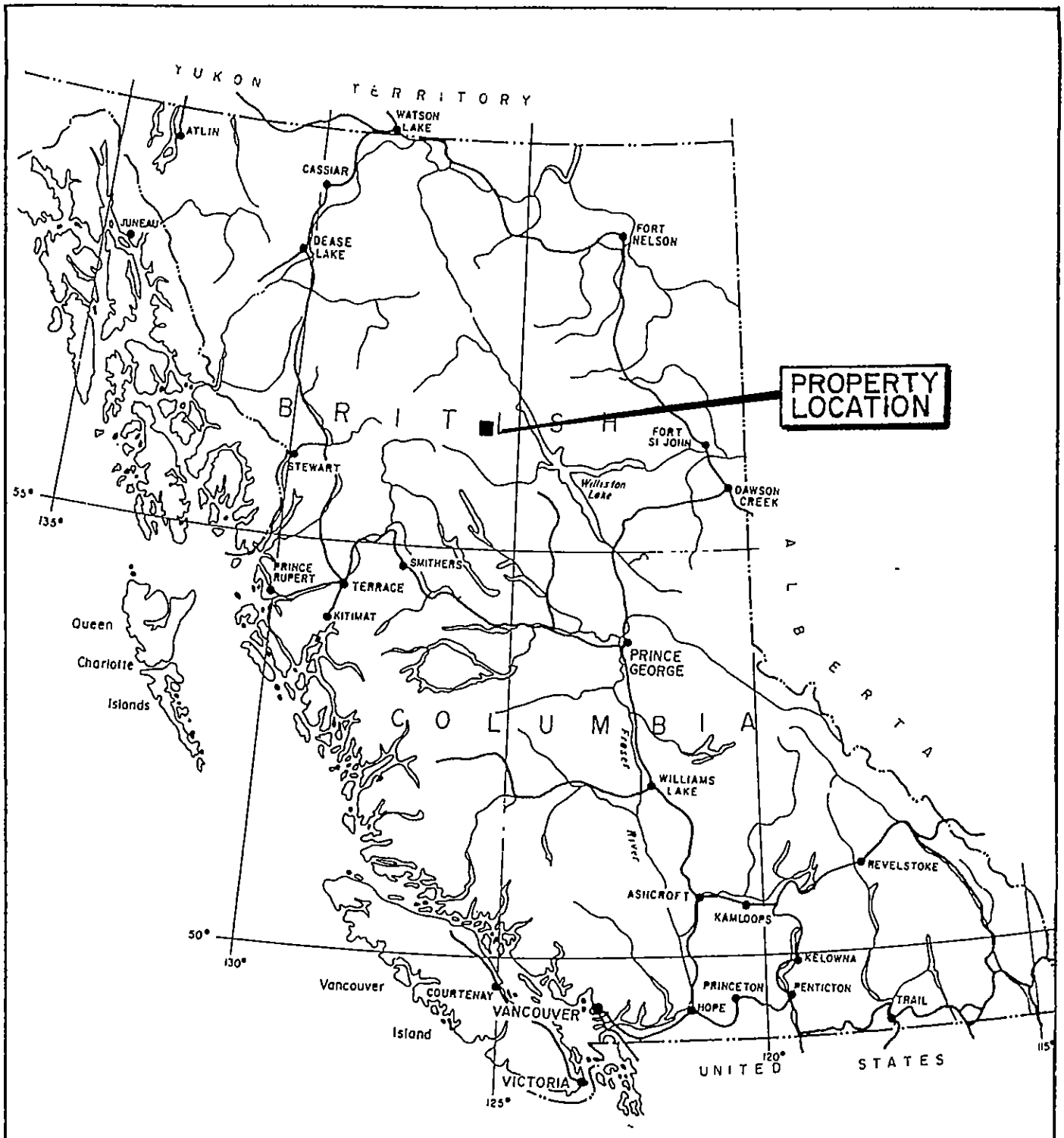
The Heidi-Lay claim group is located 345 kms. northwest of Prince George, B.C., at 56°28'45" north latitude and 125° 47'18" west longitude. Lay Creek flows southeasterly across the property into the Mesilinka River, which in turn flows into the Omineca Arm of Williston Lake (Figures 1 and 2).

Access to the area is by road 400 kms. north from Fort St. James, B.C. This road runs SE-NW across the Lay #2, Heidi #1, and Heidi #2 claims.

Physiography

The Heidi-Lay claim group lies within the Omineca Mountains of the Central Plateau and Mountain area of the Canadian Cordillera. The area is gently rolling to mountainous with elevations from 980 to 1880 metres a.s.l. The Lay Creek canyon, which is 100 to 150 metres deep, runs in a NW-SE direction across the claim group. Also, a smaller canyon is developed on Polaris Creek, a south flowing tributary of Lay Creek (Figures 2 and 3).

Rock exposure is poor to excellent on the claim group. Glacial deposits mantle the valley slopes up to about 1300 metres a.s.l. Rock exposure is very good in the Polaris and Lay Creek canyons, as well as the rugged mountainous area of the Heidi #2 claim.



SKYLARK RESOURCES LTD.

HEIDI - LAY CLAIM GROUP

LOCATION MAP

N.T.S. 94C-5 OMINECA M.D., B.C.

0 100 200 500 KM.

SCALE AS SHOWN	DATE : FEB. 1988
DRAWN BY: C.M.	FIGURE Nº. 1

CHONG

Property Claim Status

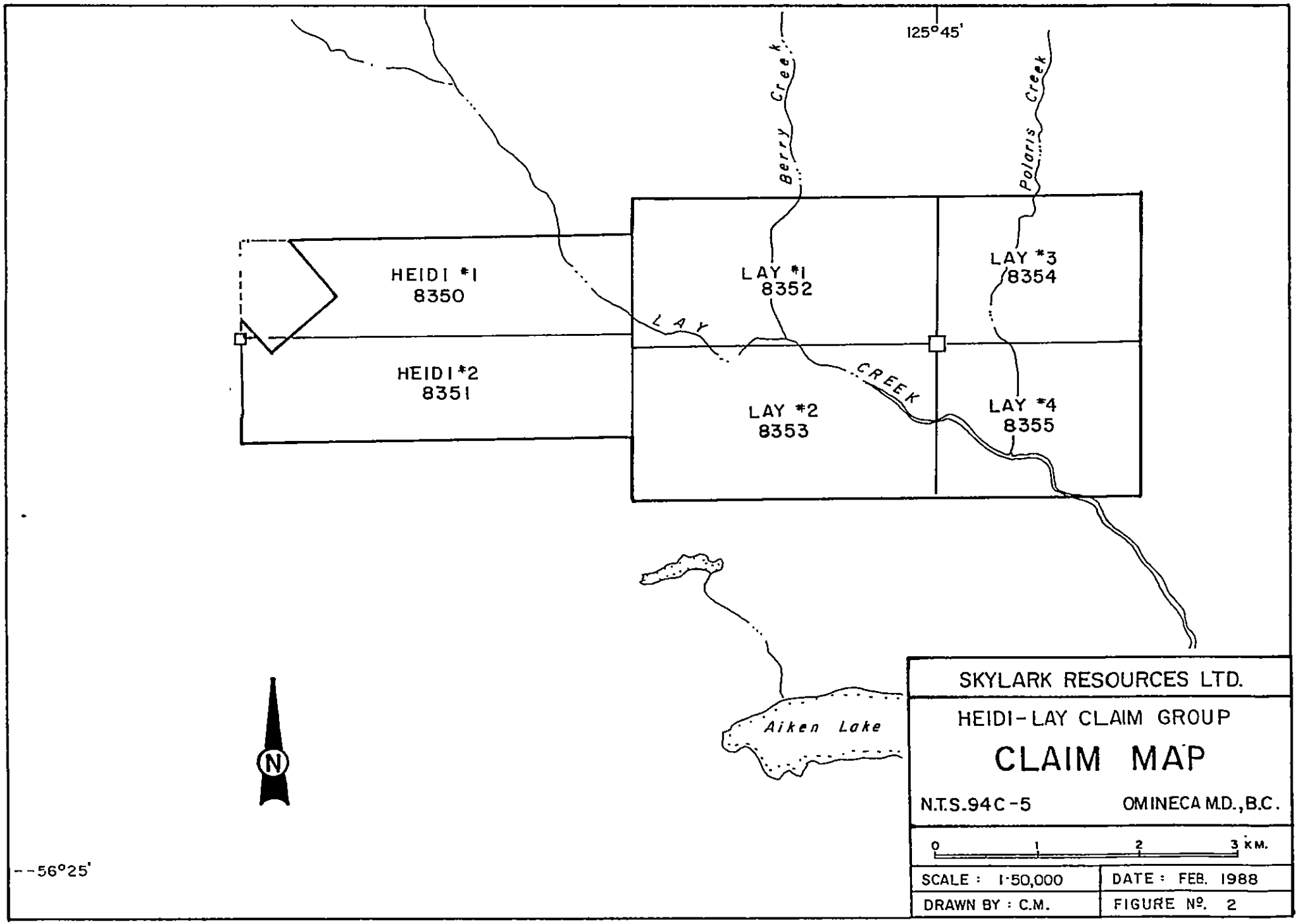
The Heidi-Lay claim group is owned by John M. Mirko, of 451 Hermosa Ave., North Vancouver, B.C.

The claim group consists of the following claims:

Claim	Units	Record No.	Anniversary Date
Heidi #1	16	8350	April 23, 1988
Heidi #2	16	8351	April 23, 1988
Lay #1	18	8352	April 23, 1988
Lay #2	18	8353	April 23, 1988
Lay #3	12	8354	April 23, 1988
Lay #4	12	8355	April 23, 1988

Property History

Prospecting has been active in the area since the turn of the century when placer gold deposits were worked on Jim May Creek and on the Igenika River. Much prospecting and development work was carried out by Cominco in the 1930's and 1940's. A few major and junior mining companies explored for porphyry copper-molybdenum and Mississippi valley lead-zinc type deposits in the 1960's and 1970's. Some exploration for precious metals was done in the late 1970's and 80's, but was soon eclipsed by new gold discoveries in the Toodoggone area. No economic ore bodies have been developed in the Aiken Lake area to date.


125°45'
Berry Creek
Polaris Creek
HEIDI #1
8350
HEIDI #2
8351
LAY #1
8352
LAY #2
8353
LAY #3
8354
LAY #4
8355
LAY
CREEK
Aiken Lake
N
--56°25'
SKYLARK RESOURCES LTD.
HEIDI-LAY CLAIM GROUP
CLAIM MAP
N.T.S. 94C-5
OMINECA M.D., B.C.
0 1 2 3 KM.
SCALE : 1:50,000
DATE : FEB. 1988
DRAWN BY : C.M.
FIGURE Nº. 2

CHONG

EXPLORATION PROCEDURE

Field work was carried out by Chris McAtee, geologist, Doug Hopper and John Sveen, prospectors, as well as Tom Smith, assistant, from July 8 to August 5, 1987.

Geological mapping, prospecting, rock chip sampling, and geochemical soil and silt sampling were carried out on the claims as follows: Soil samples were taken from the "B" horizon where available at 15-30 cm depths.

Area	Claims	Work Program
Jupiter	Lay #1, #2	5 soil samples 6 rock samples
Polaris	Lay #3, #4	23 soil samples 9 rock samples
South of Jupiter	Lay #2, #4	295 soil samples 3 silt samples 19 rock samples 13.6 kms. lines
Granite Basin	Heidi #1, #2	19 soil samples 6 silt samples 10 rock samples

Jupiter

Reconnaisance work was carried out in the area of the old Jupiter workings. The main adit, which is on the west side of Jupiter Creek, was open and in fairly good condition. No samples were taken underground due to unsafe conditions. Rock chip samples were taken on the steep east-facing cliff above the Jupiter portal and across Berry Creek to the east. Also a short soil sample line was run above the steep south-facing cliff on the east side of the creek (Figure 4).

Polaris

Soil samples were taken every 100 metres along the bluff on either side of the Polaris Creek canyon. Rock chip samples were also collected. (Figure 3).

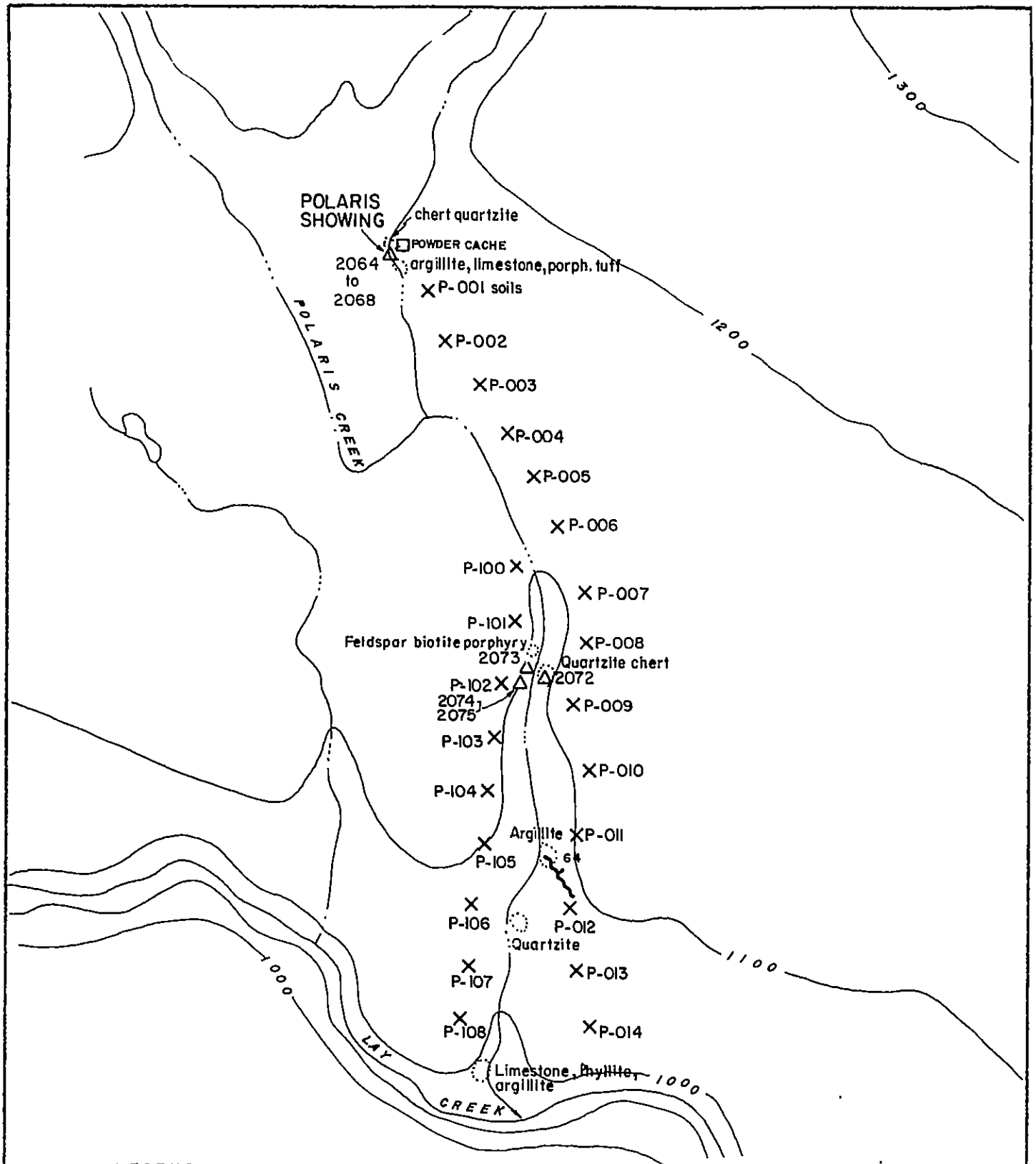
South of Jupiter

A 13.6 km. soils grid (Lay grid) was put in south of the Jupiter showing on the south side of the Lay Creek canyon. The Omineca road was used as a baseline with lines 200 metres apart and stations 50 metres along the lines (Figure 5). Soil samples were taken at all stations along the lines and at 50 metre intervals between the ends of the lines. Also, the baseline was sampled for soils at 50 metre intervals. A soil sample line, with a few rock chip samples, was also run along the south bluff overlooking Lay Creek west of the Berry Creek road (Lay # series - Figure 5).

At the north end of the Berry Creek road, a series of switchbacks exposes fresh bedrock and several new mineralized showings (Figures 4 and 6). Rock chip samples were taken and the veins and showings mapped.

Granite Basin

Reconnaissance work was undertaken on the Heidi #1 and Heidi #2 claims, where several traverses were run for soil and silt geochemistry (Figure 7).



LEGEND

- × Soil sample location
- △ Rock " "
- ~64~ Shear zone
- ~1000~ Contour in metres
- ⋯ Outcrop

SKYLARK RESOURCES LTD.

HEIDI-LAY CLAIM GROUP

POLARIS CREEK AREA

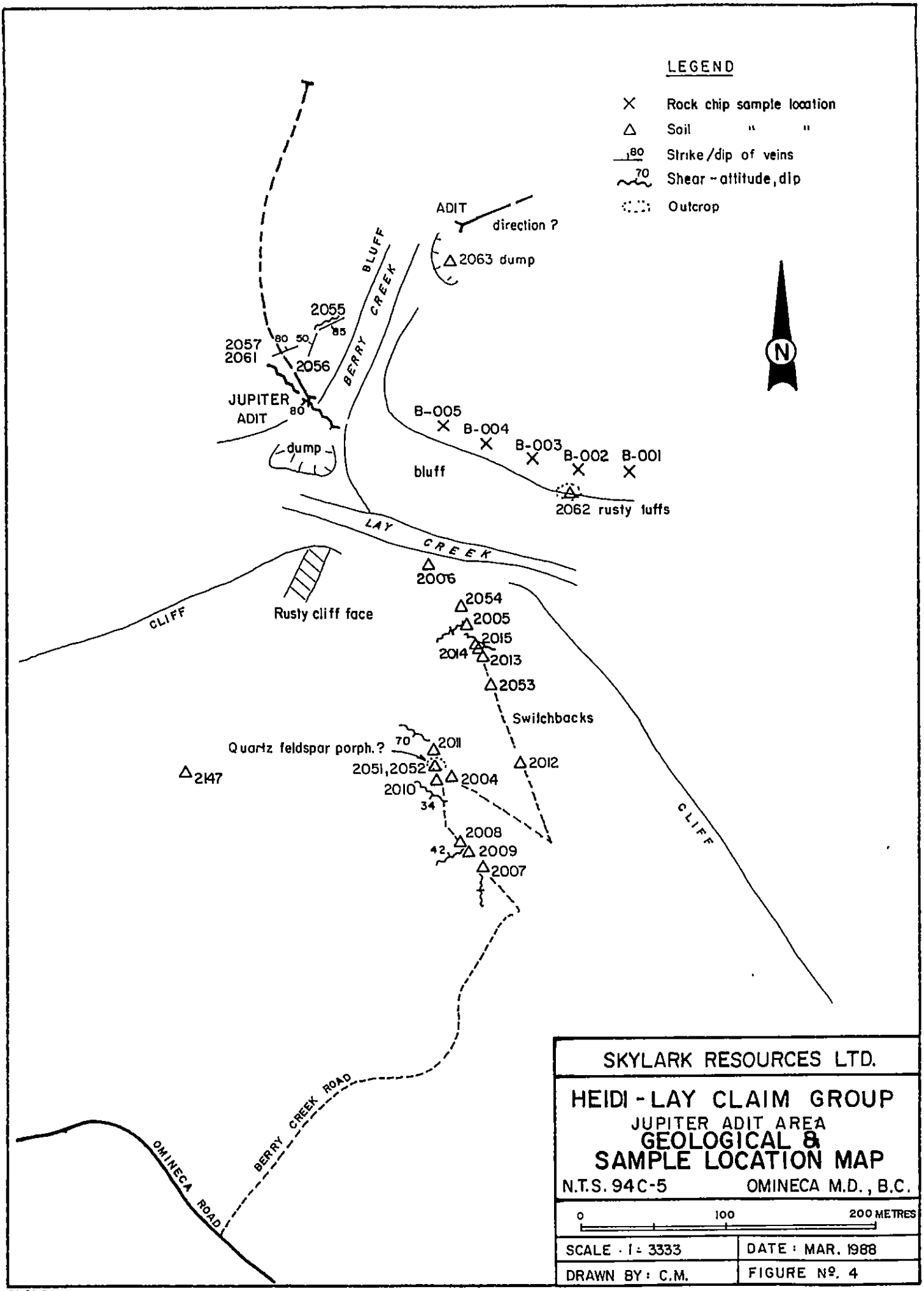
GEOLOGICAL AND SAMPLE LOCATION MAP

N.T.S. 94 C-5 OMINECA M.D., B.C.

0 200 400 600 METRES

SCALE - 1:10,000	DATE : MAR. 1988
DRAWN BY : C.M.	FIGURE Nº. 3

CHONG


LEGEND
Rock chip sample location
Soil " "
Strike/dip of veins
Shear - attitude, dip
Outcrop
ADIT
direction ?
2063 dump
BLUFF
BERRY CREEK
2055
2057
2061
2056
JUPITER
ADIT
dump
B-005
B-004
B-003
B-002
B-001
bluff
2062 rusty tuffs
LAY CREEK
2006
CLIFF
Rusty cliff face
2054
2005
2015
2014
2013
2053
Switchbacks
Quartz feldspar porph.?
2011
2147
2051, 2052
2004
2012
2010
2008
2009
2007
CLIFF
BERRY CREEK ROAD
OMINECA ROAD
N
SKYLARK RESOURCES LTD.
HEIDI - LAY CLAIM GROUP
JUPITER ADIT AREA
GEOLOGICAL & SAMPLE LOCATION MAP
N.T.S. 94C-5
OMINECA M.D., B.C.
0
100
200 METRES
SCALE - 1 : 3333
DATE : MAR. 1988
DRAWN BY : C.M.
FIGURE Nº. 4
CHONG

REGIONAL GEOLOGY

The Heidi-Lay claim group occurs within the 1:253,440 scale, Aiken Lake map area (Roots, 1954).

Regionally, Tenakihi group metamorphic rocks, Takla group sedimentary and volcanic rocks, and unnamed interbedded volcanic and sedimentary rocks are intruded by Omineca intrusives of Mesozoic age. Northeast of Blackpine Lake, Wolverine Complex amphibolites, quartzites, and skarns are present.

Structurally, beds of the Tenakihi group have been deformed into a series of compound folds that have overwhelmed earlier more north-trending folds. Northwesterly faulting plays a major role in localizing mineralization, both regionally and locally.

PROPERTY GEOLOGY

Rocks exposed on the Heidi-Lay claim group consist of tuffs, andesites, limestone, argillite, and chert, with numerous small dykes and stocks of acidic to intermediate composition.

The Polaris Creek Canyon shows a complex assemblage of slaty argillites, impure limestone, tuffs, and andesitic flows intruded by quartz biotite porphyry dykes or plugs.

All other rocks on the property are green or grey tuffs and andesites, sometimes interbedded with limestone.

Structure is complex, as evidenced by fresh exposed bedrock in a series of switchbacks just south of the old Jupiter workings.

MINERALIZATION

The Heidi #1 and #2 claims cover the old Halquinn and Red Dyke groups which were staked in 1947 on the extension of the Granite Basin zone. This zone contains four wide pyritized bands exposed within a horizontal distance of about 600 metres contained in porphyritic andesites and diorite porphyry.

The Lay #1 to #4 claims cover the old Jupiter and Polaris groups held and worked by Cominco from 1936 to the 1940's. Early exploratory work on the Jupiter group consisted of two adits, one on either side of Berry Creek near its confluence with Lay Creek.

On the old Jupiter group, two distinct types of mineral deposits have been found in altered andesites and tuffs. The first is represented by a brecciated fault zone, the second by well defined quartz-calcite fissure veins mineralized with sphalerite, tetrahedrite, galena, and minor chalcopyrite, covellite, and pyrrhotite.

The old Polaris group, which is situated about one kilometre east of the Jupiter workings, consists of several showings. Networks of quartz and quartz-calcite veins are mineralized with bands of blebby pyrite, arsenopyrite, pyrrhotite, and minor chalcopyrite. Also found along Polaris Creek are several lens-like bodies of pyrrhotite, pyrite, and chalcopyrite near a quartz-biotite porphyry plug or dyke.

The object of the 1987 work was to further explore the area for precious metals mineralization.

RESULTS

Jupiter

Sample locations and assay results from the rock chip and soil-silt program are shown on Figure 4 and Appendix 2.

A quartz-carbonate vein containing fine grained galena, malachite, and azurite returned 114 ppb Au, 160.8 ppm (160.8 g/tonne) Ag, 710 ppm Cu, and 1.6% combined Pb plus Zn across 127 cms. This vein (assay #2057, #2061) is brecciated and fractured, with fault gouge on both the hanging wall and foot wall as well as within the vein itself. The vein most likely corresponds with underground vein #1 or vein #3 mentioned in Roots' report (Roots, 1954).

Thirty-five metres northeast of the above mentioned vein, a 6.0 cm wide quartz vein (#2055) strikes 240 and dips 85 SE. A rock chip sample of vein material containing pyrrhotite, galena, and other unidentifiable sulphides returned 294.4 ppm (294.4 g/tonne) Ag, 0.8% Pb plus Zn, and anomalous Cu and Sb values. In the same vicinity a 5.7 cm wide banded quartz-carbonate vein with pyrite and chalcopyrite (#2056) gave 260 ppb Au and 243 ppm As.

The adit on the east side of Berry Creek was found to be sloughed. One sample of picked material from the dump (#2063) gave values of 145 ppb Au, 69.4 ppm Ag, 3.8% Pb plus Zn, and 345 ppm Cu. The picked sample consists of vein quartz with very fine grained galena and possibly tetrahedrite. An anomalous value of 4.8 ppm Ag was returned from a soil sample (B-002) above rusty tuffs approximately 200 metres ESE of the main Jupiter adit.

Polaris

Low assay values were returned from the Polaris area (Figure 3 and Appendices 1 and 2).

Five rock chip samples, each across 165 cms, at the main Polaris showing gave only mildly anomalous values of 223 to 371 ppm Zn. At the showing, highly fractured silicified rocks with 1 X 1 metre patches of yellow and orange stain contain thin quartz fracture fillings. The only visible sulphide is fine grained pyrite in 4 X 10 mm blebs.

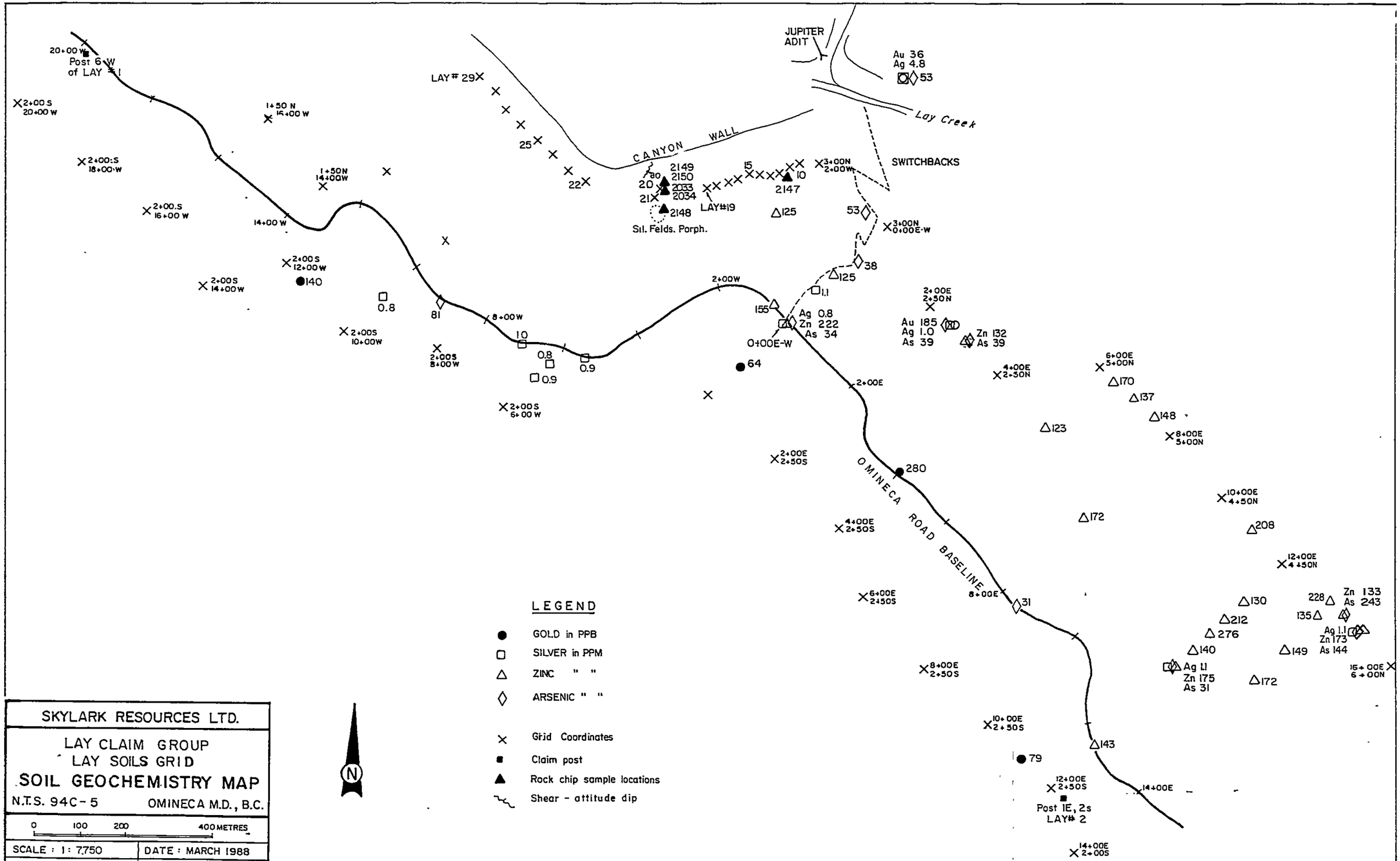
A 33 cm wide rusty zone in silicified grey quartzite and green cherts strikes 168/62°E and outcrops on either side of Polaris Creek (#2072 and #2703, Figure 4). The zone, which contains massive pyrrhotite and pyrite, is probably related to a feldspar-biotite porphyry dyke or plug found 50 metres upstream. Values of 60 ppb Au and 685 ppm Cu were returned for assay #2073.

Soil samples numbered P-012 and P-103 gave assay values of 1.9 ppm Ag and 835 ppb Au respectively. Neither of these samples were taken in proximity to any mineral showing seen by the writer.

South of Jupiter

Spot high precious metal values, as well as a few high base metal areas are found on the Lay soils grid (Figure 5).

Gold values of 280, 185, 140, and 79 ppb over a distance of 1900 metres were returned. Also, five samples southeast of the Berry Creek road and four samples in a 100 X 150 metre area near 6+00 West showed values around 1.0 ppm silver.


20+00W
Post 6 W of LAY #1
2+00S 20+00W
1+50N 16+00W
2+00S 18+00W
1+50N 14+00W
2+00S 16+00W
14+00W
2+00S 12+00W
140
2+00S 14+00W
0.8
81
8+00W
2+00S 10+00W
10
0.8
0.9
0.9
2+00S 8+00W
2+00S 6+00W
LAY # 29
25
22
CANYON WALL
2149
2150
2033
2034
2148
Sil. Felds. Porph.
80
20
21
15
10
2147
LAY #19
125
JUPITER ADIT
Au 36
Ag 4.8
53
Lay Creek
SWITCHBACKS
3+00N 2+00W
53
3+00N 0+00E-W
38
125
1.1
2+00W
155
Ag 0.8
Zn 222
As 34
0+00E-W
64
2+00E
2+00E 2+50N
Au 185
Ag 1.0
As 39
Zn 132
As 39
4+00E 2+50N
6+00E 5+00N
170
137
148
123
8+00E 5+00N
2+00E 2+50S
280
OMINECA ROAD BASELINE
10+00E 4+50N
172
208
4+00E 2+50S
12+00E 4+50N
6+00E 2+50S
8+00E
31
130
228
Zn 133
As 243
135
212
276
Ag 1.1
Zn 173
As 144
140
149
Ag 1.1
Zn 175
As 31
172
16+00E 6+00N
8+00E 2+50S
10+00E 2+50S
143
79
12+00E 2+50S
Post 1E, 2s LAY# 2
14+00E
14+00E 2+00S
LEGEND
GOLD in PPB
SILVER in PPM
ZINC " "
ARSENIC " "
Grid Coordinates
Claim post
Rock chip sample locations
Shear - attitude dip
N
SKYLARK RESOURCES LTD.
LAY CLAIM GROUP
LAY SOILS GRID
SOIL GEOCHEMISTRY MAP
N.T.S. 94C-5
OMINECA M.D., B.C.
0 100 200 400 METRES
SCALE : 1: 7,750
DATE : MARCH 1988
DRAWN BY : C.M.
FIGURE Nº. 5
CHONG .

Spot high arsenic values of 144 ppm (coincident with 1.1 ppm Ag) and 243 ppm were returned. Also, mildly anomalous values of 125 to 276 ppm zinc were received.

Rock chip samples from veins in tuffs and andesites exposed in the series of switchbacks at the north end of the Berry Creek road gave low assay values (Figures 4 and 6, Appendix 2.)

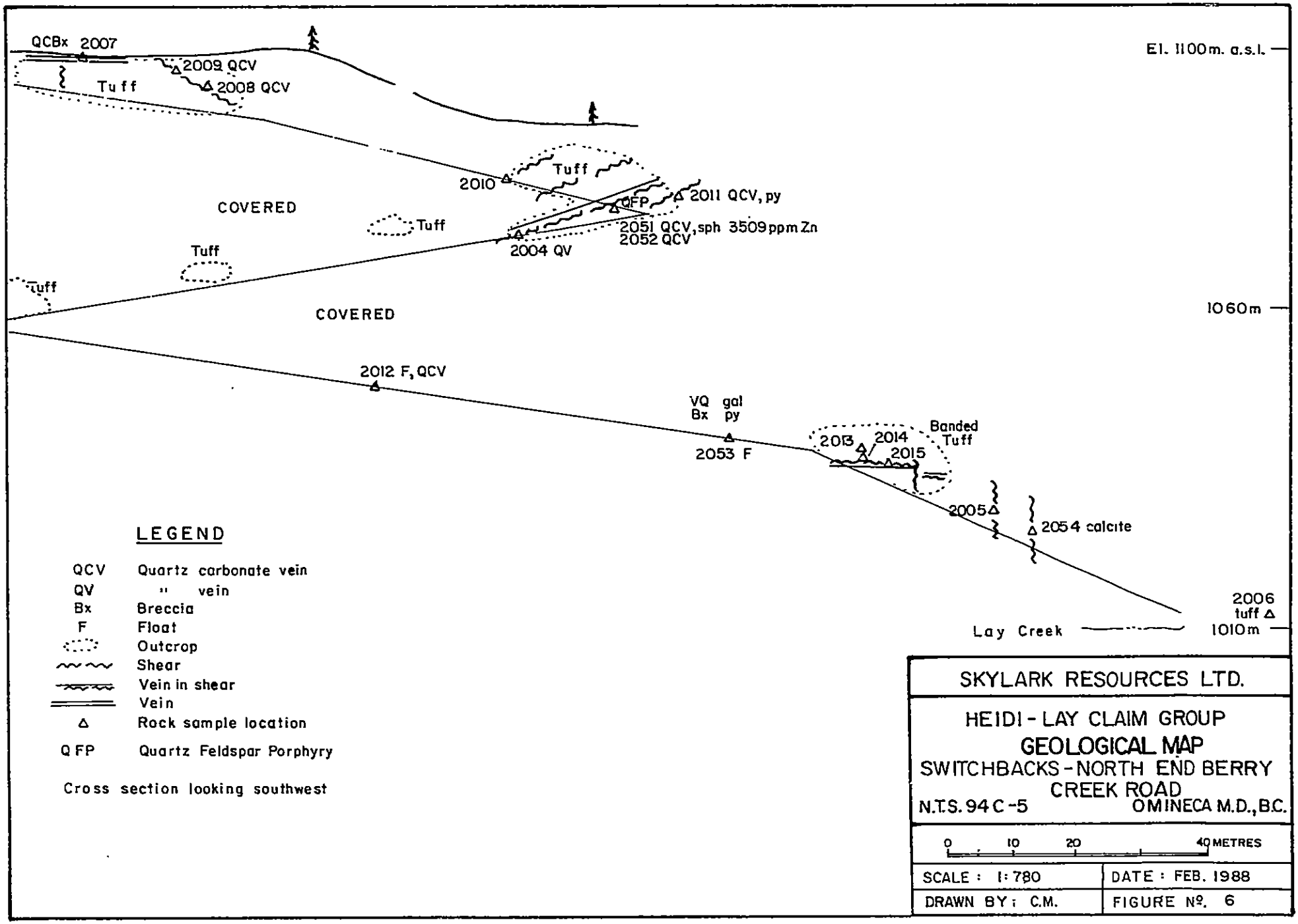
Here, sub-parallel shallow dipping barren quartz-carbonate veins are cut by many near vertical shears. A 30 X 45 cm boulder of angular float containing fine grained galena and pyrite (#2053) returned 2.2 ppm Ag, 395 ppm Zn, and 193 ppm Pb. The only other interesting value is 3509 ppm Zn in a 10 cm thick quartz-carbonate vein (#2051). No anomalous rock chip or soil assay values were obtained from the line run along the south bluff overlooking Lay Creek west of the Berry Creek road.

Granite Basin

A series of soil samples taken along a steep east-facing ridge (H-001 to H-005) and down "Heidi Creek" (H-006 to H-010), gave the following results:

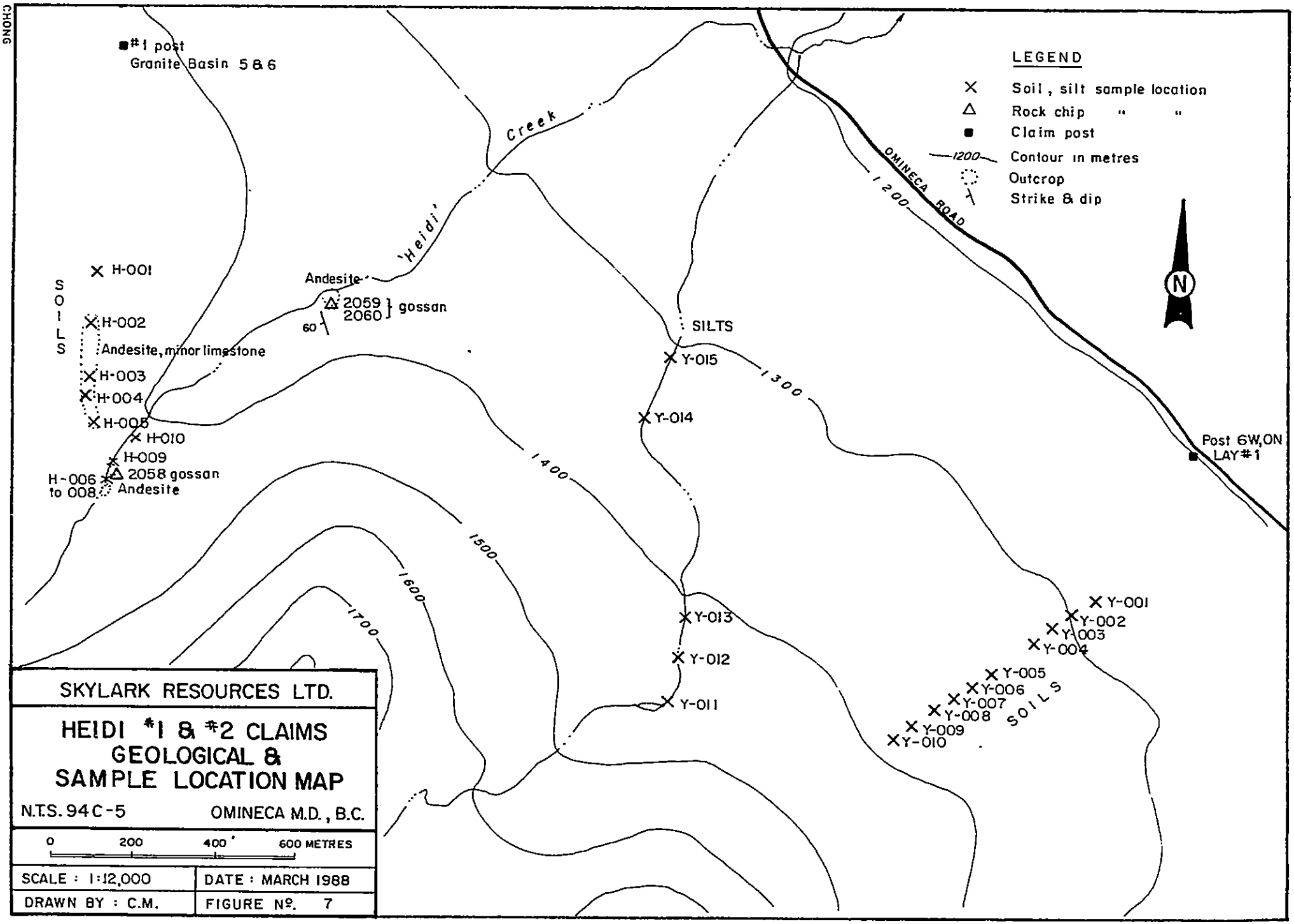
	Ag ppm	Au ppb	
H - 001	2.0	49	
H - 002	0.6	345	
H - 003	1.0	158	
H - 008	0.4	134	near #2058 rock chip sample
H - 009	2.0	91	

Locations are shown on Figure 7.


QCBx 2007
2009 QCV
2008 QCV
Tuff
El. 1100m. a.s.l.
Tuff
2010
QFP
2011 QCV, py
COVERED
Tuff
2051 QCV, sph 3509ppm Zn
2052 QCV
2004 QV
Tuff
Tuff
1060m
COVERED
2012 F, QCV
VQ gal
Bx py
2053 F
Banded
Tuff
2013
2014
2015
2005
2054 calcite
2006
tuff
1010m
Lay Creek
LEGEND
QCV Quartz carbonate vein
QV " vein
Bx Breccia
F Float
Outcrop
Shear
Vein in shear
Vein
Rock sample location
QFP Quartz Feldspar Porphyry
Cross section looking southwest
SKYLARK RESOURCES LTD.
HEIDI - LAY CLAIM GROUP
GEOLOGICAL MAP
SWITCHBACKS - NORTH END BERRY CREEK ROAD
N.T.S. 94 C-5
OMINECA M.D., B.C.
0 10 20 40 METRES
SCALE : 1:780
DATE : FEB. 1988
DRAWN BY : C.M.
FIGURE Nº. 6

CHONG

Bedrock exposed here is massive green andesite with minor limestone. Pyrite occurs in 3 X 4 mm blebs and with calcite in fracture fillings, as well as with up to 2% disseminated pyrrhotite. No significant assay values were obtained from a soil-silt traverse of two creeks tributary to Lay Creek (Y-001 to 015 series).


#1 post
Granite Basin 5 & 6
Creek
'Heidi'
OMINECA ROAD
1200
LEGEND
Soil, silt sample location
Rock chip " "
Claim post
1200 Contour in metres
Outcrop
Strike & dip
N
H-001
SOILS
H-002
Andesite, minor limestone
H-003
H-004
H-005
H-010
H-009
H-006 to 008
2058 gossan
Andesite
Andesite
2059
2060
gossan
60
SILTS
Y-015
Y-014
1300
1400
1500
1600
1700
Post 6W, ON LAY #1
Y-013
Y-012
Y-011
Y-001
Y-002
Y-003
Y-004
Y-005
Y-006
Y-007
Y-008
Y-009
Y-010
SOILS
SKYLARK RESOURCES LTD.
HEIDI #1 & #2 CLAIMS
GEOLOGICAL &
SAMPLE LOCATION MAP
N.T.S. 94C-5
OMINECA M.D., B.C.
0 200 400 600 METRES
SCALE : 1:12,000
DATE : MARCH 1988
DRAWN BY : C.M.
FIGURE Nº. 7

CONCLUSIONS AND RECOMMENDATIONS

Work on the Heidi-Lay claim group has shown that low precious metal values are found in quartz and quartz-carbonate vein systems. Several high lead and zinc values were returned for soil and rock samples.

Recommendations for further work include:

1. Jupiter - Prospecting, rock and silt sampling on Berry Creek.

2. Polaris - Prospecting, rock and possibly silt sampling to the north of work already done on Polaris Creek.

3. Reconnaisance and prospecting, soil and rock sampling, on several traverses between Berry and Polaris Creeks.

4. South of Jupiter (Lay Grid) - Extend the grid to the southwest and possibly fill soil lines between existing lines.

5. Southwest corner of Heidi #2 claim - Prospecting and rock sampling above tree-line. Very steep area.

With the exception of the Lay grid which has excellent road access, the work recommended here is best done with helicopter setouts.

ITEMIZED COST STATEMENT

HEIDI-LAY CLAIM GROUP

Field Wages -	1 prospector 8 days @ $130/day	1,040.00
	1 geologist 14 days @ 135/day	1,890.00
	1 assistant 9 days @ $130/day	1,170.00
	1 assistant 14 days @ $95/day	1,330.00
Report/Drafting/Wordprocessing		1,270.00
Mob/Demob - Vehicle - Fuel - Equipment		245.00
Camp 42 man days @ $35/day		1,470.00
Assays - 395 @ $13.25/each		5,233.75
	TOTAL	$ 13,648.75

QUALIFICATIONS

I, **CHRISTOPHER L. MCATEE**, certify that:

1. I am a minerals exploration geologist.

2. I am a graduate of Brock University, St Catharines, Ontario with a degree in geological Sciences (M.Sc., 1977), and a graduate of Wright State University, Dayton, Ohio, with a degree in Geology (B.Sc., 1972).

3. I have spent the past ten years in mineral exploration and development in Canada and the United States.

4. I personally examined the property and directed the geophysical program conducted by Skylark Resources Ltd. in 1987.

Christopher L. McAtee

Vancouver, B.C.
April, 1988

Christopher L. McAtee
Geologist

REFERENCE

Roots, E.F. (1954) Geology and Mineral Deposits of Aiken Lake Map - Area, British Columbia. Geological Survey of Canada Memoir 274, 246 pp.

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-SOIL P2-ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JUL 30 1987 DATE REPORT MAILED: Aug 10/87 ASSAYER..D. Toye..DEAN TOYE, CERTIFIED B.C. ASSAYER

SKYLARK RESOURCES PROJECT-FIRESTEEL GRUBSTAKE File # 87-2858 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
B-001	1	129	27	129	2.2	40	27	1409	9.62	164	5	ND	2	23	1	5	3	159	.72	.045	10	56	.62	310	.04	5	1.67	.01	.07	1	53
B-002	1	150	69	184	4.8	33	23	1047	7.37	87	5	ND	3	17	2	12	2	128	.34	.027	8	45	.19	255	.01	3	1.66	.01	.07	1	36
B-003	1	103	18	89	.2	35	28	1219	6.41	48	5	ND	1	22	1	2	2	120	.44	.032	5	53	1.04	218	.05	5	2.32	.01	.06	1	3
B-004	1	104	12	82	.6	42	23	1009	4.98	48	5	ND	1	33	1	2	2	108	.76	.043	4	56	1.00	117	.09	9	2.39	.01	.07	1	9
B-005	1	180	21	94	.2	37	34	1444	7.30	74	5	ND	2	29	1	2	2	157	.86	.032	8	63	2.15	132	.05	5	3.29	.01	.12	1	15
H-001	1	55	51	156	2.0	19	10	590	5.38	20	8	ND	2	72	1	2	3	64	.50	.093	3	43	.86	166	.13	2	5.60	.01	.06	1	49
H-002	1	89	36	163	.6	26	18	609	5.21	28	5	ND	2	100	1	2	2	65	.70	.056	2	51	1.38	105	.14	2	6.49	.01	.07	1	345
H-003	1	82	30	139	1.0	30	17	523	4.89	15	5	ND	2	57	1	2	2	81	.63	.056	3	59	1.44	109	.20	5	5.53	.02	.04	1	158
H-004	1	72	21	125	.9	27	15	587	4.47	10	5	ND	1	72	1	2	2	58	.65	.066	2	46	1.13	94	.12	2	3.97	.01	.05	1	57
H-005	1	27	25	126	.3	19	13	982	5.30	9	5	ND	2	69	1	2	2	94	.40	.059	4	44	.96	146	.18	5	2.50	.02	.05	1	30
H-006	1	130	7	106	.2	40	22	895	4.76	14	5	ND	2	90	1	2	3	98	1.98	.079	3	75	2.16	59	.16	2	3.38	.02	.07	1	19
H-007	1	138	15	117	.2	41	24	893	4.52	12	5	ND	2	101	1	2	2	78	1.00	.054	4	59	1.59	85	.19	2	3.10	.03	.04	1	12
H-008	1	30	19	71	.4	24	13	460	7.11	9	5	ND	3	38	1	2	2	193	.38	.045	4	64	1.22	59	.33	2	2.52	.01	.03	1	134
H-009	4	176	20	90	2.0	37	19	805	9.60	58	5	ND	3	590	1	2	2	68	1.31	.054	3	65	1.21	143	.18	2	3.08	.10	.09	1	91
H-010	1	176	17	139	.4	38	21	925	4.54	18	6	ND	1	109	1	2	2	109	2.32	.100	5	80	1.92	78	.11	5	3.45	.03	.07	1	11
P-001	2	54	16	133	.3	48	17	472	4.86	45	5	ND	2	24	1	2	3	91	.41	.109	4	58	1.08	101	.10	2	2.95	.01	.04	1	2
P-002	1	85	7	95	.3	36	12	585	3.29	22	5	ND	1	108	1	2	2	63	2.49	.060	6	55	1.15	182	.11	13	2.03	.02	.05	1	1
P-003	4	32	11	83	.1	23	8	264	4.01	51	5	ND	2	29	1	5	2	112	.45	.024	4	39	.59	93	.09	3	1.47	.01	.05	1	1
P-004	4	32	11	105	.1	27	11	593	4.31	71	5	ND	1	24	1	6	2	88	.36	.043	4	42	.56	142	.07	5	1.40	.01	.09	1	2
P-005	1	47	10	59	.4	30	10	234	2.86	27	5	ND	2	51	1	2	2	65	.75	.021	6	79	.94	79	.07	4	2.43	.08	.05	1	5
P-006	1	61	6	56	.1	28	14	454	3.16	13	5	ND	2	37	1	2	2	68	.97	.025	4	36	1.03	60	.18	2	1.68	.02	.02	1	3
P-007	1	124	6	78	.1	32	13	499	2.89	8	5	ND	1	82	1	2	2	57	2.46	.058	5	38	1.09	104	.14	10	1.56	.03	.04	1	12
P-008	3	49	15	118	.3	27	14	356	5.71	27	5	ND	2	24	1	3	2	103	.47	.096	4	43	.71	77	.14	6	2.09	.01	.04	1	9
P-009	2	73	14	121	.7	41	19	522	4.66	19	5	ND	2	32	1	2	3	90	.66	.013	6	46	1.00	102	.18	4	2.60	.02	.04	1	8
P-010	2	72	11	135	.5	40	26	636	5.50	30	5	ND	2	25	1	2	2	92	.55	.059	4	45	.91	81	.18	5	2.19	.01	.04	1	6
P-011	2	61	16	113	.2	42	20	334	5.30	23	5	ND	2	26	1	3	2	97	.52	.039	4	46	.82	94	.20	2	2.29	.01	.04	1	14
P-012	5	184	18	211	1.9	107	31	673	6.83	35	6	ND	4	22	1	2	2	83	.35	.029	7	43	1.16	97	.20	5	2.75	.01	.05	1	6
P-013	2	140	19	244	.3	58	37	1012	6.06	40	5	ND	2	27	1	3	2	106	.48	.065	5	49	1.00	122	.21	2	2.74	.01	.05	1	6
P-014	3	206	12	144	.6	120	34	530	5.96	26	5	ND	4	28	1	2	2	89	.40	.021	7	57	1.36	110	.19	3	2.94	.01	.03	1	12

SKYLARK RESOURCES PROJECT-FIRESTEEL/GRUBSTAKE FILE # 87-3214

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY #10	1	38	2	88	.2	33	15	361	5.14	9	5	ND	2	31	1	2	2	133	.87	.066	3	79	1.25	49	.26	2	2.48	.02	.03	2	1
LAY #11	1	63	5	76	.1	46	21	387	4.61	2	5	ND	2	34	1	2	2	124	1.02	.050	3	84	1.59	46	.29	2	3.35	.02	.04	1	7
LAY #12	1	36	2	47	.1	38	15	430	3.63	5	5	ND	1	38	1	2	2	106	1.30	.046	4	65	1.53	30	.28	4	2.63	.02	.02	1	17
LAY #13	1	31	4	68	.1	26	13	280	4.88	8	5	ND	1	27	1	2	3	133	.70	.070	3	70	.90	47	.26	3	2.67	.02	.03	1	12
LAY #15	1	26	2	72	.1	27	13	311	5.26	3	5	ND	2	29	1	2	2	146	.78	.037	3	80	1.01	49	.32	2	2.62	.02	.03	1	8
LAY #16	1	31	4	57	.1	35	14	312	5.45	8	5	ND	1	33	1	2	3	159	.92	.038	3	90	1.26	60	.36	6	2.75	.02	.03	1	1
LAY #17	1	40	2	66	.1	42	17	350	5.21	5	5	ND	1	31	1	2	2	151	.93	.047	3	89	1.33	44	.33	4	3.41	.02	.02	1	9
LAY #19	1	147	4	63	.1	53	20	457	4.26	9	5	ND	1	35	1	2	2	117	1.18	.029	3	77	1.80	58	.29	5	3.03	.02	.04	1	12
LAY #20	1	103	4	60	.3	52	25	754	3.58	30	5	ND	1	51	1	29	2	53	4.79	.018	2	35	.76	145	.01	13	.69	.01	.12	1	1
LAY #22	1	102	3	164	.2	78	43	2444	5.91	3	5	ND	1	43	2	2	4	135	.92	.145	3	146	1.69	255	.18	6	3.05	.01	.04	1	1
LAY #23	1	44	2	99	.1	26	20	830	6.74	14	5	ND	1	41	1	2	2	167	.79	.060	4	49	1.58	179	.29	2	3.15	.01	.06	1	15
LAY #24	1	67	2	80	.1	45	17	530	4.54	7	5	ND	1	41	1	2	2	117	.91	.054	2	81	1.78	63	.28	2	2.87	.02	.05	1	13
LAY #25	1	189	7	134	.3	52	35	1263	7.45	38	5	ND	1	41	1	2	2	129	1.41	.065	7	76	2.67	157	.21	4	3.92	.02	.11	1	4
LAY #26	1	170	6	96	.2	73	27	969	4.76	16	5	ND	1	64	1	2	2	102	1.72	.056	4	100	2.05	239	.20	7	3.43	.03	.26	1	1
LAY #27	1	136	2	93	.1	48	25	879	5.03	10	5	ND	1	49	1	2	2	121	1.01	.047	5	83	2.13	104	.29	4	3.61	.04	.09	1	3
LAY #28	1	58	6	83	.1	62	19	401	5.23	14	5	ND	1	36	1	2	2	145	.86	.047	3	134	1.70	39	.31	2	2.71	.01	.03	1	4
LAY #29	1	62	9	70	.1	330	33	452	6.54	2	5	ND	1	20	1	2	2	182	.54	.012	3	496	5.05	24	.11	5	4.92	.01	.02	2	1
P .100	5	66	11	135	.4	39	17	391	6.99	51	5	ND	1	25	1	2	2	124	.35	.041	6	50	.69	100	.13	2	2.45	.01	.05	1	12
P .101	3	43	12	162	.5	31	16	607	5.45	38	5	ND	1	23	1	3	2	103	.35	.068	6	48	.61	107	.13	2	2.35	.01	.05	1	3
P .102	9	94	11	194	.1	49	24	441	7.93	41	5	ND	1	24	1	3	8	110	.37	.053	5	54	.94	114	.22	2	3.27	.01	.05	2	7
P .103	4	93	8	241	.4	63	34	945	6.73	17	5	ND	1	30	1	2	2	103	.56	.042	5	48	1.09	98	.26	2	3.18	.02	.05	1	835
P .104	2	158	8	192	.3	65	36	933	6.91	37	5	ND	1	28	1	2	2	111	.51	.073	5	56	.94	110	.25	2	3.41	.02	.07	1	8
P .105	3	116	12	210	.5	59	35	591	6.67	38	5	ND	1	29	1	2	5	118	.53	.056	5	55	.97	118	.23	6	3.04	.02	.08	1	3
P .106	5	121	17	351	.5	70	40	768	8.03	30	5	ND	2	29	1	2	5	112	.44	.101	5	43	.91	103	.23	4	3.76	.02	.07	3	8
P .107	3	46	9	146	.2	43	19	359	5.49	57	5	ND	1	22	1	3	2	103	.36	.059	4	59	.86	101	.13	2	2.51	.01	.04	1	5
P .108	4	65	16	223	.4	35	25	656	8.23	28	5	ND	2	29	1	2	3	141	.39	.058	5	49	1.04	66	.30	6	2.70	.01	.05	2	9
Y .001	1	47	2	97	.3	39	18	521	6.70	6	5	ND	2	39	1	2	2	185	.84	.054	3	88	1.52	51	.46	4	4.44	.02	.05	1	1
Y .002	1	26	19	50	.4	21	11	351	5.81	10	5	ND	2	35	1	2	2	216	.71	.067	4	64	1.03	50	.58	5	2.72	.02	.03	1	8
Y .003	1	34	7	71	.4	22	12	349	7.02	10	5	2	2	34	1	2	2	257	.71	.048	4	71	1.09	63	.54	4	2.96	.01	.03	1	2
Y .004	1	52	8	56	.4	33	16	397	6.82	18	5	ND	3	34	1	2	2	208	.65	.044	3	86	1.28	64	.53	10	4.66	.02	.04	1	2
Y .005	1	93	18	76	.3	44	20	933	4.44	4	5	ND	2	56	1	2	2	109	1.68	.026	4	76	1.70	101	.40	3	3.36	.03	.06	2	1
Y .006	1	24	15	45	.3	19	9	274	5.19	9	5	ND	1	30	1	2	2	217	.59	.085	5	55	.76	54	.47	4	2.25	.01	.04	1	1
Y .007	1	41	10	66	.3	30	13	392	4.52	2	5	ND	1	50	1	2	2	170	.72	.036	3	72	1.56	103	.59	2	3.12	.02	.04	1	9
Y .008	1	84	2	65	.3	55	18	473	6.70	6	5	ND	2	51	1	2	2	171	.55	.054	3	126	2.06	110	.54	2	4.24	.02	.07	1	1
Y .009	1	84	14	75	.2	30	16	348	7.84	22	5	ND	2	23	1	2	2	210	.25	.051	2	79	.80	74	.13	2	2.43	.01	.06	1	2
Y .010	1	53	13	69	.1	27	18	293	6.38	30	5	ND	2	12	1	2	2	107	.12	.033	3	65	.61	153	.01	3	3.00	.01	.09	1	1
Y .011	1	117	11	85	.3	57	23	797	4.53	8	5	ND	2	100	1	2	2	124	1.49	.082	4	117	2.30	112	.30	3	3.53	.03	.13	1	5
Y .012	1	125	9	91	.3	54	20	861	4.12	8	5	ND	2	99	1	2	2	111	1.90	.092	4	114	2.11	102	.26	2	3.27	.03	.14	1	9
Y .013	1	142	12	66	.4	32	14	1073	2.40	12	5	ND	1	89	1	2	2	71	3.04	.126	6	118	1.11	75	.10	7	2.27	.02	.10	1	1
Y .014	1	294	9	71	.9	25	12	1193	2.33	9	5	ND	1	98	1	2	2	63	4.84	.154	14	83	.78	114	.05	6	2.51	.02	.06	1	1
Y .015	1	232	10	75	.7	26	11	1403	1.92	8	5	ND	1	86	1	2	2	61	4.25	.127	8	119	.70	72	.06	7	1.62	.02	.08	1	2

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
R2001	1	78	27	52	.1	92	24	526	4.37	3	5	ND	3	19	1	2	2	112	2.65	.044	2	53	3.26	6	.34	10	3.17	.02	.02	1	2
R2002	1	62	16	37	.1	39	13	487	2.66	9	5	ND	1	111	1	2	2	83	12.18	.059	2	37	1.38	3	.23	10	2.52	.02	.01	2	1
R2003	1	66	9	52	.3	10	14	587	3.62	2	5	ND	2	217	1	2	2	119	2.05	.091	3	10	1.85	11	.20	15	2.35	.08	.05	1	1
R2004	1	31	57	53	1.3	3	7	783	2.54	19	5	ND	1	502	1	2	2	11	5.70	.053	4	3	.88	663	.01	7	.38	.01	.21	1	1
R2005	1	61	19	77	2.5	15	17	974	4.91	59	5	ND	1	167	1	6	2	55	8.74	.027	3	10	1.38	415	.01	8	.53	.01	.22	1	25
R2006	1	66	8	84	.4	48	23	902	5.91	20	5	ND	2	58	1	2	2	135	4.25	.034	3	129	2.89	40	.06	7	3.28	.02	.09	1	2
R2007	1	15	2	47	.3	22	8	1424	3.57	14	5	ND	5	183	1	2	2	49	24.54	.009	2	35	2.55	185	.01	6	.63	.01	.04	1	1
R2008	1	113	5	66	.3	53	25	689	5.23	11	5	ND	1	71	1	2	2	94	10.47	.052	2	67	1.16	71	.01	12	2.57	.01	.14	1	3
R2009	1	33	4	35	.2	46	12	1087	2.81	40	5	ND	3	135	1	2	2	45	19.46	.017	2	46	1.74	260	.01	7	.80	.01	.08	1	1
R2010	1	69	5	62	.6	19	16	851	4.44	11	5	ND	1	114	1	2	2	63	10.43	.044	5	18	1.26	270	.01	14	1.37	.01	.19	1	1
R2011	2	65	9	85	.6	23	14	812	4.68	11	5	ND	1	276	1	2	2	40	7.48	.047	6	12	1.89	417	.01	15	1.00	.01	.17	1	1
R2012	26	16	10	74	1.3	10	7	1075	4.14	8	5	ND	2	221	1	2	2	14	17.29	.010	2	4	4.78	804	.01	8	.16	.01	.06	1	1
R2013	1	61	2	49	.3	45	15	781	3.82	12	5	ND	2	232	1	2	2	104	11.75	.033	4	73	3.05	19	.01	5	.56	.01	.06	1	1
R2014	1	60	4	51	.3	276	24	829	4.23	8	5	ND	1	269	1	2	2	82	9.62	.056	5	219	3.16	269	.01	8	.53	.01	.02	1	2
R2015	1	65	4	81	.4	38	18	920	5.31	14	5	ND	2	121	1	2	2	73	6.50	.038	3	31	2.32	384	.01	12	.57	.01	.13	1	1
R2016	6	77	5	54	.6	14	13	385	3.94	4	5	ND	2	121	1	2	2	47	1.01	.056	2	14	.71	46	.18	5	2.11	.24	.10	1	65
R-2017	2	44	154	564	1.9	14	12	895	5.69	15	5	ND	2	168	2	6	2	43	1.19	.040	2	33	1.38	68	.18	3	2.97	.16	.11	1	121
R-2018	1	23	82	203	1.0	4	8	1096	4.93	2	5	ND	1	73	1	4	2	34	1.23	.032	2	10	1.98	48	.14	3	3.51	.21	.14	1	54
R-2019	1	15	39	44	.°	5	10	628	5.47	5	5	ND	1	62	1	5	2	27	.74	.036	2	10	.82	39	.17	2	2.07	.20	.13	1	75
R-2020	1	18	25	67	.5	8	12	795	5.23	3	5	ND	1	61	1	4	2	27	1.00	.035	2	9	1.00	41	.16	5	2.86	.30	.13	1	58
R-2021	1	17	34	50	.6	5	12	937	5.17	4	5	ND	1	73	1	5	2	31	1.36	.035	2	11	1.02	49	.14	2	3.15	.37	.13	1	109
R-2022	1	41	5	41	.3	22	10	367	4.17	5	5	ND	1	51	1	3	2	34	.79	.052	2	34	.80	69	.23	2	1.37	.05	.08	1	36
R-2023	1	86	15	91	.8	15	17	346	5.70	11	5	ND	1	97	1	4	2	43	1.68	.040	2	10	.46	46	.19	3	3.05	.36	.15	1	32
R-2024	1	44	10	78	.4	25	12	313	5.50	15	5	ND	1	50	1	5	2	30	.71	.048	2	22	.47	64	.21	2	2.28	.17	.17	1	87
R-2025	1	48	2	41	.3	6	7	189	5.68	2	5	ND	1	314	1	3	2	52	2.44	.030	2	9	.24	67	.15	2	5.38	.37	.13	1	39
R-2026	1	44	5	73	.1	11	18	295	5.69	10	5	ND	1	181	1	4	2	39	2.40	.036	2	9	.30	64	.11	2	4.48	.56	.12	2	47
R-2027	1	23	15	49	.4	6	10	266	5.13	22	5	ND	1	24	1	2	2	28	1.33	.039	2	6	.39	59	.16	3	1.85	.06	.17	1	57
R-2028	1	36	7	68	.1	5	10	284	3.28	10	5	ND	1	78	1	2	2	38	2.12	.041	2	4	.53	65	.14	3	3.40	.18	.11	1	23
R-2029	2	28	16	60	.3	3	10	217	4.02	18	5	ND	1	123	1	3	2	22	.75	.042	2	1	.48	110	.10	3	2.32	.21	.13	1	61
R-2033	1	49	8	57	.1	55	24	1037	5.83	5	5	ND	1	141	1	2	2	65	9.44	.037	3	52	3.30	98	.01	5	.34	.01	.10	1	6
R-2034	1	65	14	46	.1	233	27	845	4.67	8	6	ND	1	202	1	2	2	115	11.57	.038	3	319	6.01	32	.01	3	1.93	.01	.04	1	6

ACME ANALYTICAL LABORATORIES - 852 East Hastings Street Vancouver, B.C. V6A 1R6

Appendix 2 - Assay results - HEIDI - LAY CLAIM GROUP - ROCKS

R2051	15	23	37	3509	1.8	6	5	1086	3.39	9	5	ND	1	207	25	2	2	9	10.72	.003	2	3	2.07	435	.01	4	.14	.01	.07	16	1
R2052	1	31	47	94	1.0	4	8	841	2.91	9	5	ND	3	272	1	7	2	14	5.47	.080	8	4	.44	495	.01	14	.46	.01	.24	1	1
R2053	18	42	193	395	2.2	7	5	896	2.69	10	5	ND	1	108	3	2	2	12	9.96	.006	2	4	2.46	561	.01	6	.15	.01	.04	1	3
R2054	1	50	6	66	1.0	18	11	957	3.81	33	5	ND	1	257	1	2	2	54	12.38	.018	3	19	1.88	474	.01	7	.32	.01	.12	1	20
R-2055	4	609	2357	5875	294.4	10	6	709	2.22	61	5	ND	1	97	105	391	2	11	7.00	.002	2	5	.79	25	.01	6	.43	.01	.07	1	39
R-2056	1	10	7	15	1.0	2	3	1374	1.18	243	5	ND	1	468	1	2	5	7	29.62	.004	3	4	.22	27	.01	2	.31	.01	.05	1	260
R-2057	15	331	849	21648	126.2	3	5	372	.62	10	5	ND	1	21	555	103	4	3	1.97	.001	2	3	.06	21	.01	2	.17	.01	.02	6	59
R-2058	86	58	27	100	1.0	10	13	322	17.34	27	5	ND	1	27	1	6	2	76	.56	.023	2	50	.65	18	.29	2	1.29	.02	.03	1	29
R-2059	1	91	12	478	1.0	10	11	1233	6.23	2	5	ND	1	45	4	4	2	93	1.15	.031	2	20	2.71	39	.16	2	3.66	.10	.06	1	6
R-2060	1	61	9	193	.3	12	20	1095	5.81	2	5	ND	1	129	1	4	2	76	1.62	.031	2	14	2.15	51	.17	2	4.03	.13	.07	1	9
R-2061	10	710	2485	13076	140.8	4	4	377	.92	16	5	ND	1	30	323	178	2	7	2.58	.001	2	4	.11	161	.01	3	.32	.01	.03	5	114
R-2062	1	78	5	126	.4	13	17	938	5.00	15	5	ND	1	140	2	2	2	78	7.35	.030	3	19	1.50	200	.01	5	.69	.01	.09	1	5
R-2063	6	345	2979	7671	69.4	8	5	1069	2.84	57	5	ND	1	184	130	73	6	7	13.19	.003	2	2	.95	89	.01	3	.10	.01	.02	1	145
R-2064	1	113	15	71	.2	13	8	343	4.54	4	5	ND	1	46	1	3	2	83	.66	.055	9	26	1.38	93	.32	4	1.82	.12	.11	2	7
R-2065	1	148	47	223	.8	15	8	300	4.30	2	5	ND	1	69	4	2	4	59	1.75	.045	8	16	1.00	73	.27	4	1.42	.15	.13	2	5
R-2066	1	154	11	371	.1	20	14	459	5.25	2	5	ND	1	42	5	2	2	89	1.13	.060	8	23	1.32	65	.26	2	1.65	.09	.12	1	7
R-2067	1	120	16	234	.1	17	10	603	5.45	2	5	ND	1	47	3	3	4	97	1.35	.084	10	21	1.54	88	.40	3	2.08	.11	.22	2	2
R-2068	1	102	10	72	.1	6	6	393	4.48	3	5	ND	2	31	1	2	2	45	.84	.041	11	12	.69	82	.22	4	1.13	.07	.10	1	8
R-2072	1	441	10	25	.2	13	18	697	13.42	2	5	ND	2	43	1	2	5	95	4.34	.068	5	32	.69	10	.17	2	.99	.04	.03	24	6
R-2073	1	685	19	36	.5	23	23	1026	18.99	2	5	ND	1	67	1	2	7	48	6.05	.055	6	14	.51	7	.06	12	.72	.02	.03	109	40
R-2074	2	239	18	14	.1	17	20	251	10.56	2	5	ND	2	70	1	2	2	62	.87	.123	5	26	.41	25	.18	10	1.06	.14	.08	10	1
R-2075	30	190	13	12	.1	6	8	242	8.18	5	5	ND	2	98	1	2	2	86	1.17	.117	5	24	.46	20	.22	6	1.34	.09	.05	11	3
R-2095	1	138	7	71	.3	13	13	785	5.87	4	5	ND	2	202	1	2	8	155	2.60	.096	4	28	1.61	108	.28	11	6.84	.76	1.17	2	7
R-2147	3	208	21	39	.1	35	14	539	5.96	2	5	ND	2	34	1	2	3	226	5.59	.061	3	53	2.28	19	.45	28	5.91	.02	.01	2	6
R-2148	1	33	8	48	.1	39	16	1235	4.72	20	9	ND	1	231	1	2	2	61	13.57	.010	2	40	4.71	241	.01	6	.23	.01	.04	1	1
R-2149	1	35	9	68	.1	47	18	1259	5.49	16	6	ND	1	240	1	2	2	56	14.29	.015	2	27	5.37	223	.01	7	.37	.01	.06	1	1
R-2150	1	62	5	48	.1	79	24	929	4.99	2	5	ND	1	170	1	2	2	153	8.67	.038	4	83	4.70	74	.01	6	.56	.03	.03	1	1

ACME ANALYTICAL LABORATORIES - 852 East Hastings Street Vancouver, B.C. V6A 1R6

Appendix 2 - Assay results - HEIDI - LAY CLAIM GROUP - ROCKS

ACME ANALYTICAL LABORATORIES 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE 253-3158 DATA LINE 251-1011

GEOCHEMICAL ICP ANALYSIS

.500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG.C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA AND K. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-B SOIL P9-SILT P10-ROCK AU# ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: JUL 24 1987 DATE REPORT MAILED: July 31/87 ASSAYER. D. Toye .DEAN TOYE, CERTIFIED B.C. ASSAYER

SKYLARK RESOURCES PROJECT-FIRESTEEL File # 87-2679 Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU# PPB
LAY 6+00N 14+50E	2	98	21	133	.5	323	42	428	10.31	243	5	ND	2	16	1	5	2	135	.18	.041	4	236	2.14	77	.01	12	3.75	.01	.06	1	1
LAY 6+00N 15+00E	1	46	35	173	1.1	23	23	526	9.52	144	5	ND	2	9	1	2	2	102	.10	.068	6	27	.52	122	.01	7	2.53	.01	.08	1	5
LAY 6+00N 15+50E	2	31	3	93	.3	20	13	380	5.17	22	5	ND	2	28	1	2	2	144	.50	.058	3	43	.77	66	.20	10	1.99	.01	.04	1	6
LAY 6+00N 16+00E	1	57	14	62	.2	35	17	484	4.52	23	5	ND	2	29	1	2	2	117	.64	.049	3	57	1.18	60	.22	4	2.82	.02	.03	1	16
LAY 5+00N 6+50E	2	89	13	170	.7	66	23	510	5.69	28	5	ND	2	34	1	2	2	136	.58	.049	3	64	1.28	67	.24	6	2.81	.02	.04	1	6
LAY 5+00N 7+00E	1	67	2	137	.4	31	18	529	6.38	30	5	ND	3	26	1	2	2	153	.44	.076	2	51	1.44	46	.25	13	2.80	.01	.04	1	1
LAY 5+00N 7+50E	1	103	11	148	.2	53	30	588	6.24	26	5	ND	2	40	1	2	2	156	.54	.026	3	72	1.76	54	.35	14	3.40	.01	.06	1	1
LAY 4+50N 10+50E	1	41	4	107	.8	27	14	342	4.59	17	5	ND	1	29	1	2	2	120	.42	.046	4	50	.93	53	.26	4	1.91	.01	.05	1	1
LAY 4+50N 11+00E	1	48	15	208	.3	35	20	1033	5.21	18	5	ND	2	33	1	2	2	120	.52	.076	3	62	1.40	74	.20	7	2.53	.02	.04	1	18
LAY 4+50N 11+50E	1	39	9	130	.4	22	15	602	5.32	11	5	ND	1	28	1	2	2	134	.40	.095	3	49	1.08	42	.24	5	2.25	.02	.04	1	2
LAY 3+00N 2+00W	1	46	17	72	.5	35	17	280	5.14	9	5	ND	2	28	1	2	2	157	.88	.036	3	75	1.17	52	.29	13	2.59	.02	.02	1	16
LAY 3+00N 1+50W	1	53	5	72	.3	37	18	362	6.25	19	5	ND	2	29	1	2	2	166	.62	.057	3	69	1.34	48	.26	11	2.73	.02	.03	1	25
LAY 3+00N 1+00W	1	35	9	77	.1	30	13	369	4.34	16	5	ND	2	29	1	2	2	127	.78	.060	3	57	1.08	45	.24	14	2.41	.02	.03	1	2
LAY 3+00N 0+50W	1	67	6	62	.1	50	17	441	7.16	53	5	ND	1	22	1	2	5	182	.62	.069	2	103	1.31	65	.14	10	2.98	.01	.03	1	75
LAY 3+00N 2+50E	1	48	15	99	1.0	28	16	332	6.16	39	5	ND	1	25	1	2	2	139	.54	.054	3	60	1.05	150	.13	9	2.47	.01	.04	1	185
LAY 3+00N 3+00E	2	87	17	132	.2	35	20	624	5.89	39	5	ND	2	17	1	2	2	120	.32	.029	3	58	.95	204	.03	13	2.58	.01	.04	1	5
LAY 3+00N 3+50E	1	33	12	88	.3	15	9	280	4.59	12	5	ND	2	22	1	2	2	134	.45	.040	3	40	.94	83	.17	5	2.29	.02	.05	1	2
LAY 3+00N 4+00E	1	67	14	51	.3	24	15	272	3.67	16	5	ND	1	22	1	2	2	93	.51	.033	2	43	.97	55	.14	10	2.39	.02	.03	1	13
LAY 1+50N 15+50W	1	125	8	72	.1	60	25	515	6.25	31	7	ND	1	39	2	2	2	186	1.24	.032	2	78	2.15	57	.27	14	3.84	.02	.04	6	1
LAY 1+50N 15+00W	1	47	21	84	.3	35	14	437	6.17	24	5	ND	2	34	1	2	2	180	.86	.082	3	78	1.42	56	.33	7	3.29	.02	.03	2	1
LAY 1+50N 14+50W	1	68	16	65	.5	45	18	404	6.51	21	5	ND	2	31	1	2	2	213	1.19	.035	2	79	1.89	34	.35	16	3.21	.02	.03	1	1
LAY 1+00N 11+50W	1	29	18	47	.4	28	10	263	5.00	11	5	ND	2	29	1	2	2	179	.90	.049	3	64	1.08	35	.36	11	2.35	.02	.02	1	5
LAY 1+00N 11+00W	1	131	13	52	.1	60	20	695	5.01	23	6	ND	3	16	1	2	2	155	.58	.022	9	103	2.57	16	.16	7	2.63	.01	.02	3	2
LAY 1+00N 10+50W	1	20	21	47	.4	17	8	228	3.90	7	5	ND	2	30	1	2	2	197	1.04	.021	3	46	.74	36	.41	11	2.07	.01	.01	1	1
LAY 2+00S 19+50W	1	50	16	77	.2	53	22	510	6.86	15	5	ND	3	22	1	2	2	205	1.28	.075	2	95	2.30	33	.46	16	4.13	.02	.02	2	6
LAY 2+00S 19+00W	1	63	16	69	.1	66	19	421	6.17	24	5	ND	2	28	1	2	2	196	1.75	.071	2	98	2.18	44	.37	14	4.01	.02	.02	3	39
LAY 2+00S 18+50W	1	21	17	67	.1	22	9	330	5.15	10	5	ND	1	37	1	2	2	182	.90	.085	3	56	.94	53	.28	6	2.68	.02	.03	1	2
LAY 2+00S 18+00W	1	28	21	75	.4	38	14	344	5.97	16	5	ND	2	26	1	2	2	197	1.14	.072	3	77	1.37	34	.38	4	3.15	.02	.03	2	6
LAY 2+00S 17+50W	1	89	16	64	.1	49	21	499	4.94	24	5	ND	2	33	1	2	2	169	1.40	.019	2	71	1.82	53	.35	10	3.72	.02	.03	3	3
LAY 2+00S 17+00W	1	85	18	53	.2	43	16	372	4.60	13	5	ND	2	25	1	2	2	156	1.42	.035	2	65	1.70	44	.30	2	3.35	.02	.02	2	1
LAY 2+00S 14+50W	1	56	12	92	.2	30	19	617	5.03	13	5	ND	2	25	1	2	2	182	1.28	.042	3	57	1.16	61	.31	19	2.57	.02	.03	1	2
LAY 2+00S 11+50W	1	39	12	85	.5	38	18	370	5.42	24	5	ND	2	24	1	2	2	187	.99	.071	4	67	1.32	45	.38	2	3.52	.02	.02	3	140
LAY 2+00S 11+00W	1	68	21	94	.2	56	22	542	6.90	17	5	ND	3	33	1	2	2	199	1.57	.033	2	96	2.54	30	.46	16	4.08	.01	.01	1	5
LAY 2+00S 10+50W	1	36	15	88	.4	34	17	398	5.30	11	5	ND	2	26	1	2	2	170	1.08	.074	3	67	1.54	47	.36	9	3.38	.02	.03	1	4
LAY 2+00S 7+50W	1	31	5	83	.3	42	15	425	6.10	9	5	ND	1	24	1	2	3	201	1.40	.118	3	73	1.53	45	.36	15	3.09	.02	.02	1	2
LAY 2+00S 7+00W	1	59	16	65	.4	67	18	428	5.54	15	5	ND	1	23	1	2	4	166	1.20	.116	3	90	2.09	47	.31	16	3.81	.01	.03	1	1

SKYLARK RESOURCES PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY 12+00N 1+00N	1	35	15	70	.3	35	18	405	5.47	5	5	ND	2	28	1	2	2	179	1.00	.037	3	65	1.35	37	.36	14	3.19	.01	.03	1	7
LAY 12+00N 0+50N	1	50	11	67	.5	48	18	426	4.77	14	5	ND	3	27	1	2	2	165	1.24	.071	3	67	1.63	44	.35	14	3.86	.01	.03	2	3
LAY 12+00N 0+00BL	1	50	2	67	.5	39	21	411	4.69	12	5	ND	3	30	1	2	2	153	1.05	.085	2	72	1.64	46	.32	12	3.87	.02	.02	1	6
LAY 12+00N 0+50S	1	32	11	68	.5	28	13	359	5.64	2	5	ND	3	26	1	2	2	202	.95	.094	3	71	1.28	45	.42	2	3.28	.02	.04	1	5
LAY 12+00N 1+00S	1	44	15	76	.7	41	16	398	6.07	11	5	ND	2	26	1	2	2	192	.88	.065	3	88	1.66	44	.42	7	3.87	.01	.01	1	1
LAY 12+00N 1+50S	1	36	3	80	.5	47	17	405	6.03	13	5	ND	3	25	1	2	2	190	.87	.074	3	87	1.63	41	.43	2	4.38	.02	.02	1	6
LAY 12+00N 2+00S	1	27	17	61	.6	39	12	320	5.03	8	5	ND	1	25	1	2	2	182	.79	.058	3	69	1.24	41	.39	9	3.02	.01	.03	1	22
LAY 10+00N 1+00N	1	43	3	62	.3	49	17	437	5.79	21	5	ND	3	27	1	2	2	220	1.26	.024	2	83	1.60	40	.42	13	3.39	.01	.01	1	5
LAY 10+00N 0+50N	1	33	3	72	.4	45	16	350	5.02	8	5	ND	2	27	1	2	2	170	1.08	.047	2	76	1.36	48	.38	2	3.56	.02	.02	1	2
LAY 10+00N 0+50S	1	23	10	82	.3	21	12	409	5.80	11	5	ND	3	25	1	3	2	195	.87	.161	4	67	.93	34	.41	9	2.69	.01	.06	1	10
LAY 10+00N 1+00S	1	34	2	78	.8	34	16	386	5.60	9	5	ND	2	26	1	2	2	206	1.24	.066	3	64	1.29	32	.44	11	3.19	.01	.02	3	3
LAY 10+00N 1+50S	1	54	10	68	.4	42	17	403	4.56	9	5	ND	3	27	1	2	2	155	1.23	.091	2	66	1.48	42	.34	8	3.71	.02	.02	1	18
LAY 10+00N 2+00S	1	28	10	69	.5	27	14	339	5.63	5	5	ND	1	25	1	2	2	208	.90	.066	3	71	1.08	44	.45	2	3.18	.02	.03	1	7
LAY 8+00N 1+00S	1	37	14	51	.4	32	14	343	5.05	2	5	ND	1	25	1	2	2	203	1.21	.063	3	71	1.32	56	.43	2	3.34	.02	.02	1	1
LAY 8+00N 1+50S	1	79	12	55	.1	55	20	431	4.53	12	7	ND	1	23	1	2	2	159	1.42	.087	2	70	1.80	37	.34	5	4.35	.02	.03	1	2
LAY 8+00N 2+00S	1	56	12	68	.5	51	18	437	5.64	14	5	ND	2	21	1	2	2	182	1.18	.115	2	92	1.75	40	.37	6	4.48	.01	.02	1	3
LAY 6+00N 0+50S	1	65	9	107	.8	57	21	498	6.25	29	5	ND	2	34	1	2	2	173	.98	.079	3	94	1.95	53	.36	12	3.67	.01	.03	1	1
LAY 6+00N 1+00S	2	70	10	116	.9	40	19	587	6.28	29	5	ND	1	22	1	2	2	165	.59	.063	3	53	1.60	69	.18	11	3.67	.01	.04	1	22
LAY 6+00N 1+50S	1	40	18	73	.4	46	17	402	5.13	10	5	ND	2	23	1	2	2	175	1.40	.067	3	78	1.55	38	.39	11	3.56	.01	.02	1	12
LAY 6+00N 2+00S	1	42	7	79	.4	27	15	477	5.99	7	5	ND	1	27	1	2	2	192	.81	.080	3	61	1.11	71	.36	10	2.90	.01	.02	1	2
LAY 2+00N 2+50N	1	62	17	90	.4	35	17	426	5.41	13	5	ND	2	23	1	2	2	143	.48	.123	3	67	1.13	60	.27	5	3.79	.02	.04	3	8
LAY 2+00N 2+00N	1	34	6	69	.5	27	12	301	4.99	7	5	ND	2	29	1	2	2	165	.59	.074	4	67	.97	52	.37	9	3.29	.02	.03	1	10
LAY 2+00N 1+50N	1	25	16	125	.4	29	17	504	5.66	12	5	ND	2	24	1	2	2	152	.75	.129	3	70	1.09	52	.31	10	3.15	.01	.03	1	2
LAY 2+00N 1+00N	1	25	5	85	.2	31	13	334	5.00	12	5	ND	2	29	1	2	2	162	.89	.047	2	80	1.16	35	.33	11	2.72	.01	.03	1	4
LAY 2+00N 0+50N	1	25	12	59	.1	23	10	270	4.53	6	5	ND	1	25	1	2	2	164	.88	.057	3	44	.89	36	.33	6	2.31	.01	.02	1	5
LAY 2+00N 0+00BL	1	33	14	84	.5	39	17	446	4.72	12	5	ND	1	26	1	2	2	148	.90	.080	3	72	1.28	58	.30	7	2.98	.02	.04	1	40
LAY 2+00N 0+50S	1	42	3	66	.1	43	18	366	4.16	12	5	ND	1	25	1	2	2	135	.88	.045	2	71	1.26	46	.29	9	3.13	.02	.02	1	5
LAY 2+00N 1+00S	1	29	11	101	.3	41	16	604	5.23	10	5	ND	2	24	1	3	2	168	.83	.092	4	79	1.19	67	.32	11	2.76	.01	.02	2	6
LAY 2+00N 2+50S	1	31	9	111	.4	53	21	484	5.38	10	5	ND	1	25	1	2	2	159	.86	.077	3	82	1.42	60	.32	8	3.35	.01	.03	1	3
LAY BL 0+00E/N 3+00N	1	46	2	82	.3	33	17	555	5.18	10	5	ND	1	28	1	2	2	151	.66	.119	3	69	1.31	60	.29	15	2.65	.02	.04	1	9
LAY BL 0+00E/N 2+50N	2	27	9	118	.4	33	17	515	5.68	7	5	ND	1	22	1	2	2	199	1.03	.057	4	71	1.01	65	.47	8	2.78	.01	.03	1	5
LAY BL 0+00E/N 2+00N	1	24	13	102	.5	31	13	405	5.78	7	8	ND	2	24	1	2	2	191	1.18	.075	3	73	1.20	32	.38	10	2.84	.01	.02	1	1
LAY BL 0+00E/N 1+50N	1	18	2	125	.1	24	14	469	4.76	3	5	ND	2	24	1	3	2	177	1.14	.091	4	54	.89	44	.40	8	2.41	.01	.03	1	15
LAY BL 0+00E/N 0+50S	1	32	2	85	.2	34	14	363	5.60	9	5	ND	2	20	1	2	2	175	.82	.093	3	65	1.10	42	.29	12	2.81	.01	.03	1	1
LAY BL 0+00E/N 1+00S	2	48	10	58	.1	30	12	381	4.13	13	5	ND	3	27	1	2	2	119	.59	.104	3	60	1.02	49	.26	4	3.22	.02	.03	1	8
LAY BL 0+00E/N 1+50S	3	65	13	64	.4	38	17	318	7.86	21	5	ND	1	27	1	3	2	221	.88	.034	4	105	1.10	40	.47	11	4.10	.01	.03	1	2
STD C/AU-S	19	60	42	131	7.1	68	26	936	3.95	38	20	7	36	47	16	17	18	59	.47	.083	35	56	.86	173	.09	36	1.81	.04	.15	13	50

SKYLARK RESOURCES LTD PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY 2+00S 4+50W	1	52	19	75	.2	53	21	434	5.07	2	5	ND	3	23	1	2	2	178	1.21	.126	3	82	1.61	35	.29	8	4.21	.01	.02	1	3
LAY 2+50S 1+50W	1	22	19	69	.1	33	12	407	5.09	3	5	ND	2	22	1	2	2	187	.69	.084	3	79	.93	38	.19	4	2.33	.01	.02	1	2
LAY 2+50S 1+00W	1	98	18	52	.1	75	22	554	4.85	4	5	ND	3	33	1	2	2	159	2.05	.034	4	84	1.98	52	.21	18	3.82	.02	.01	1	19
LAY 2+50S 0+50W	1	42	19	109	.1	49	17	337	4.88	6	5	ND	2	23	1	2	2	164	.87	.072	3	79	1.21	42	.25	10	3.46	.02	.02	1	1
LAY 2+50S 2+50E	1	85	28	109	.1	43	19	411	5.94	31	5	ND	2	24	1	3	2	190	.60	.036	5	81	1.46	68	.16	8	3.15	.01	.04	1	3
LAY 2+50S 3+00E	1	58	17	79	.1	31	16	379	4.78	2	5	ND	1	31	1	2	2	157	.74	.042	2	59	1.13	59	.23	7	2.59	.02	.03	1	12
LAY 2+50S 3+50E	1	72	15	65	.1	41	18	360	4.17	2	7	ND	2	30	1	2	2	132	.77	.065	3	62	1.27	38	.22	8	2.79	.02	.02	1	9
LAY 2+50S 6+50E	1	17	16	59	.1	17	9	304	3.53	2	5	ND	1	21	1	7	2	127	.44	.076	4	46	.68	35	.23	5	1.76	.01	.03	1	1
LAY 2+50S 7+00E	1	26	17	63	.1	24	11	242	4.72	2	5	ND	2	25	1	5	2	181	.51	.065	4	50	.73	53	.26	3	2.23	.02	.02	1	1
LAY 2+50S 7+50E	1	29	12	107	.1	24	14	330	4.49	5	5	ND	2	32	1	3	2	147	.60	.065	3	54	.90	66	.23	5	2.28	.02	.03	1	36
LAY 2+50S 10+50E	1	61	25	57	.1	33	15	374	4.12	2	5	ND	2	35	1	2	2	133	.65	.030	2	49	1.13	61	.23	4	2.65	.02	.03	1	6
LAY 2+50S 11+00E	1	22	25	48	.1	23	12	266	3.91	2	5	ND	2	31	1	2	2	148	.52	.025	2	48	.83	32	.25	6	1.77	.02	.03	1	79
LAY 2+50S 11+50E	1	53	21	88	.1	37	17	431	4.72	2	5	ND	2	30	1	2	2	144	.66	.077	3	64	1.22	53	.22	4	2.58	.02	.03	1	7
LAY 20+00W 0+50S	1	48	29	90	.1	33	16	391	5.56	5	5	ND	2	31	1	2	2	173	.70	.034	3	70	1.28	53	.34	2	3.51	.02	.03	1	4
LAY 20+00W 1+00S	1	25	25	60	.1	23	9	280	4.44	3	5	ND	2	32	1	4	2	219	.84	.029	3	56	.93	59	.37	2	2.19	.01	.01	1	9
LAY 20+00W 1+50S	1	52	27	98	.1	71	24	588	6.29	3	5	ND	1	33	1	2	2	201	1.36	.056	2	115	2.45	37	.33	7	3.81	.02	.02	1	4
LAY 20+00W 2+00S	1	44	23	70	.2	65	20	487	6.02	6	5	ND	1	26	1	2	2	202	1.09	.054	3	104	2.26	31	.35	6	3.76	.02	.01	3	7
LAY 19+50W 19+50N	1	83	31	69	.4	39	17	484	4.20	8	5	ND	2	66	1	2	2	125	1.73	.037	3	68	1.67	71	.22	2	3.54	.05	.03	1	12
LAY 18+00W 0+36N	1	42	36	70	.2	45	17	689	4.46	4	5	ND	3	29	1	5	2	163	1.14	.068	3	69	1.52	55	.27	7	3.29	.02	.01	1	10
LAY 18+00W 0+50S	1	74	31	82	.1	41	21	512	7.07	19	5	ND	1	39	1	4	2	253	1.03	.043	2	80	1.53	69	.34	6	3.60	.02	.02	3	1
LAY 18+00W 1+00S	1	51	23	79	.2	41	19	424	4.98	2	5	ND	2	32	1	3	5	172	.98	.034	3	71	1.56	41	.30	6	3.47	.02	.03	3	4
LAY 18+00W 1+50S	1	52	38	86	.2	41	17	443	7.12	7	5	ND	3	20	2	4	2	244	.77	.077	2	91	1.60	31	.41	8	4.22	.01	.01	1	4
LAY 18+00W 2+00S	1	108	35	96	.1	71	26	622	6.13	2	7	ND	2	25	2	2	2	204	.87	.048	3	90	2.21	56	.33	3	4.50	.01	.03	1	5
LAY 16+00W 1+50N	1	61	32	65	.2	39	18	419	6.38	19	5	ND	3	29	1	2	2	278	1.02	.057	3	83	1.39	33	.39	7	3.14	.01	.02	1	2
LAY 16+00W 1+00N	1	37	26	65	.1	27	12	418	5.55	3	5	ND	3	27	1	4	2	195	.82	.087	3	70	1.15	42	.31	2	2.92	.01	.02	1	8
LAY 16+00W 0+50N	1	74	33	63	.4	45	17	477	5.54	11	5	ND	2	26	1	3	2	196	1.20	.079	3	75	1.74	56	.31	2	3.43	.01	.05	3	3
LAY 16+00W 0+50S	1	35	35	73	.1	39	16	383	5.22	2	7	ND	3	26	1	3	2	184	.93	.050	3	78	1.35	49	.32	4	3.81	.02	.02	1	5
LAY 16+00W 1+00S	1	60	42	113	.1	41	21	498	5.70	4	6	ND	2	29	1	2	2	181	.93	.104	3	78	1.37	61	.27	2	3.59	.01	.02	3	7
LAY 16+00W 1+50S	1	50	38	74	.3	47	18	563	5.16	2	5	ND	1	22	1	2	4	193	1.26	.058	2	72	1.79	40	.34	7	3.90	.01	.02	1	2
LAY 14+00W 1+50N	1	65	46	84	.7	47	20	453	6.40	8	7	ND	2	28	1	2	2	207	.88	.059	3	79	1.57	54	.29	2	4.32	.02	.02	3	5
LAY 14+00W 1+00N	1	38	41	77	.2	31	16	416	6.42	11	5	ND	3	24	1	2	2	222	.69	.046	2	75	1.30	75	.27	2	3.35	.01	.03	1	8
LAY 14+00W 0+00BL	1	17	19	62	.1	23	8	313	4.90	6	5	ND	2	24	1	4	.2	198	.79	.103	5	62	.84	38	.39	2	2.40	.01	.03	1	3
LAY 14+00W 0+50S	1	46	41	76	.2	45	16	470	5.40	3	5	ND	3	26	1	7	2	188	.95	.095	3	71	1.59	46	.34	2	3.80	.02	.02	1	16
LAY 14+00W 1+00S	1	50	40	66	.4	39	16	394	6.22	2	5	ND	2	23	1	2	2	222	.92	.085	3	79	1.39	54	.41	2	4.25	.02	.03	1	4
LAY 14+00W 1+50S	1	42	35	78	.3	41	15	386	5.00	2	5	ND	2	28	1	2	2	185	1.08	.085	4	65	1.41	45	.33	4	3.71	.02	.02	2	6
LAY 14+00W 2+00S	1	23	33	91	.1	27	13	496	6.49	2	5	ND	2	22	1	4	2	290	.88	.063	3	56	1.24	36	.46	2	2.97	.01	.02	1	11
STD C/AU-S	20	63	39	131	7.2	69	25	938	3.72	37	20	7	37	47	17	16	18	61	.47	.083	35	58	.85	176	.08	36	1.79	.06	.14	12	49

SKYLARK RESOURCES PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY BL 0+00E/N 2+00S	1	39	2	121	.4	51	20	397	5.70	6	5	ND	2	23	1	2	3	179	1.20	.038	3	78	1.52	39	.35	17	3.32	.02	.03	1	5
LAY BL 0+00E/N 2+50S	1	59	6	71	.3	52	20	388	4.89	2	5	ND	1	22	1	2	3	145	1.04	.099	3	74	1.56	33	.28	11	3.62	.02	.03	1	64
LAY BL 0+00W 1+00N	1	58	18	66	.5	62	23	388	4.59	3	5	ND	1	26	1	2	2	127	1.08	.046	3	82	1.68	37	.23	14	3.28	.02	.02	1	10
LAY BL 0+00W 0+50N	1	29	3	76	.3	21	12	324	4.67	6	5	ND	1	21	1	2	2	135	.67	.073	3	56	.85	40	.20	3	2.07	.01	.02	1	4
LAY BL 0+00W 0+00BL	1	70	5	36	.2	12	8	358	2.29	2	5	ND	2	36	1	2	2	66	1.12	.025	2	33	.57	25	.08	2	1.35	.03	.02	1	9
LAY BL 0+00E 3+50N	1	38	2	84	.5	21	13	333	6.33	9	5	ND	2	24	1	2	5	172	.40	.033	4	57	.98	52	.36	3	2.64	.01	.04	1	1
LAY BL 0+00E 3+00N	1	133	20	66	.4	43	17	354	3.57	8	5	ND	2	39	1	2	2	96	.90	.016	5	57	1.24	50	.23	15	2.89	.02	.02	1	1
LAY BL 0+00E 2+50N	1	38	21	114	.6	33	18	416	5.66	11	6	ND	2	26	1	2	3	131	.40	.034	3	54	1.41	49	.27	11	2.63	.01	.04	1	1
LAY BL 0+00E 2+00N	1	52	2	109	.4	29	18	377	5.61	38	5	ND	1	23	1	2	3	127	.36	.059	3	68	1.15	52	.18	12	2.56	.01	.04	2	2
LAY BL 0+00E 1+50N	1	27	2	72	.1	10	12	261	3.21	27	5	ND	1	21	1	2	2	79	.36	.027	2	30	.66	55	.12	2	1.36	.01	.03	1	9
LAY BL 0+00E 1+00N	1	95	8	112	1.1	33	25	484	6.07	22	5	ND	1	35	1	2	2	111	.48	.042	3	49	1.52	107	.19	15	3.61	.01	.04	2	3
LAY BL 0+00E 0+50N	1	30	5	48	.1	25	12	243	3.52	7	5	ND	2	28	1	2	2	108	.73	.019	2	56	.98	64	.22	10	2.04	.01	.02	1	2
LAY 2+00E 2+50N	1	32	2	92	.3	23	17	471	5.22	12	5	ND	2	20	1	2	2	132	.48	.028	3	51	1.17	119	.13	4	2.41	.01	.04	1	1
LAY 2+00E 2+00N	1	69	12	66	.3	42	19	414	4.77	4	5	ND	1	27	1	2	2	133	.71	.031	3	65	1.34	48	.23	2	2.71	.02	.04	3	5
LAY 2+00E 1+50N	1	19	11	52	.4	12	8	219	3.65	5	5	ND	1	26	1	2	2	150	.48	.044	3	39	.53	67	.27	7	1.47	.01	.03	1	3
LAY 2+00E 1+00N	1	51	11	92	.6	35	18	409	4.66	6	5	ND	1	27	1	2	2	138	.90	.065	3	59	1.15	74	.26	8	2.50	.01	.03	1	2
LAY 2+00E 0+50N	1	34	5	65	.4	25	13	341	4.62	2	5	ND	2	25	1	2	2	137	.82	.089	3	60	1.08	39	.23	15	2.34	.01	.03	1	2
LAY 2+00E 0+50S	1	40	13	127	.6	33	20	340	5.97	5	8	ND	2	20	1	2	2	147	.56	.128	4	78	.99	52	.24	15	3.68	.01	.03	2	1
LAY 2+00E 1+00S	1	46	14	96	.6	42	19	676	5.07	3	6	ND	3	24	1	2	2	138	1.08	.099	3	76	1.49	33	.24	4	2.97	.01	.03	1	1
LAY 2+00E 1+50S	1	46	11	109	.3	42	21	538	4.91	2	5	ND	3	24	1	2	3	135	1.05	.100	3	79	1.41	34	.25	3	3.04	.01	.02	4	18
LAY 2+00E 2+00S	1	51	8	69	.3	31	18	479	5.10	2	5	ND	1	26	1	2	2	152	1.33	.079	3	60	1.26	51	.26	7	2.59	.01	.04	3	1
LAY 2+00E 2+50S	1	55	12	95	.3	37	20	466	6.69	4	5	ND	3	26	1	2	3	216	1.73	.046	3	86	1.84	39	.36	6	3.32	.01	.04	5	2
LAY 4+00E 2+00N	1	51	10	55	.1	23	11	407	3.40	3	5	ND	1	18	1	2	2	79	.37	.072	2	42	.80	72	.09	8	1.90	.01	.03	1	1
LAY 4+00E 1+50N	1	28	18	79	.1	25	14	362	5.62	5	5	ND	2	24	1	2	2	181	.48	.046	4	82	.99	82	.19	16	2.00	.01	.05	1	2
LAY 4+00E 1+00N	1	27	18	75	.6	31	13	291	5.09	6	5	ND	2	24	1	2	2	146	.45	.049	4	88	1.27	80	.17	2	2.21	.02	.04	1	1
LAY 4+00E 0+50N	1	23	10	51	.2	18	12	272	5.06	2	6	ND	2	25	1	2	2	150	.38	.051	4	70	.57	52	.15	9	1.74	.01	.03	1	7
LAY 4+00E 0+00BL	1	34	2	40	.1	37	13	250	4.75	2	5	ND	2	25	1	2	2	135	.49	.012	3	67	1.12	70	.21	12	2.46	.01	.03	1	1
LAY 4+00E 1+00S	1	35	11	37	.2	31	12	226	3.65	3	5	ND	1	26	1	2	2	138	.59	.010	3	59	1.21	54	.35	4	1.83	.04	.05	1	1
LAY 4+00E 1+50S	1	38	2	72	.4	31	14	307	4.66	2	5	ND	3	25	1	2	2	122	.53	.102	3	66	1.14	41	.26	2	2.99	.02	.03	3	6
LAY 4+00E 2+00S	1	51	2	80	.1	31	16	330	4.41	4	5	ND	2	28	1	7	2	117	.61	.078	4	58	1.08	55	.23	3	2.70	.02	.04	2	2
LAY 4+00E 2+50S	1	75	14	65	.2	25	16	331	4.32	2	6	ND	2	31	1	2	3	122	.75	.050	3	56	1.20	45	.23	2	2.42	.02	.04	1	7
LAY 6+00E 4+50N	1	123	10	113	.7	22	16	562	5.95	2	8	ND	2	24	1	2	2	106	.51	.022	2	37	1.88	34	.50	8	3.13	.01	.03	4	1
LAY 6+00E 4+00N	1	36	12	95	.4	20	13	375	3.98	16	8	ND	2	22	1	2	2	90	.39	.064	3	43	.86	33	.22	6	1.60	.01	.05	2	2
LAY 6+00E 3+50N	1	86	2	84	.7	27	20	432	5.40	15	9	ND	2	29	1	2	2	115	.54	.092	3	55	1.32	54	.18	12	3.00	.01	.04	2	1
LAY 6+00E 3+00N	1	66	13	123	.6	29	18	459	6.00	18	6	ND	2	26	1	3	2	123	.42	.056	4	55	1.40	84	.20	10	3.11	.01	.04	6	9
LAY 6+00E 2+50N	1	30	5	94	.1	20	13	327	4.92	9	7	ND	2	30	1	2	2	117	.52	.035	3	46	.92	115	.11	7	2.29	.01	.04	1	10
STD C/AU-S	20	62	43	131	7.1	68	28	918	3.90	38	18	7	39	50	18	17	22	59	.49	.085	38	59	.89	179	.09	36	1.71	.06	.13	12	48

SKYLARK RESOURCES PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY 6+00E 2+00N	1	45	3	84	.2	16	12	345	4.85	14	5	ND	2	21	1	2	2	114	.43	.038	2	36	.90	97	.04	9	2.24	.01	.11	1	3
LAY 6+00E 1+50N	1	69	9	47	.3	29	16	335	3.99	10	5	ND	2	45	1	2	2	92	1.10	.028	3	50	1.18	231	.11	9	3.22	.02	.04	3	5
LAY 6+00E 1+00N	1	14	11	49	.3	21	10	368	3.77	2	5	ND	1	31	1	2	2	122	.60	.042	3	41	.63	225	.18	6	1.56	.01	.04	1	3
LAY 6+00E 0+50N	1	26	16	44	.4	25	10	286	4.38	2	5	ND	2	25	1	2	3	126	.44	.063	4	79	.98	42	.25	5	1.92	.01	.03	1	2
LAY 6+00E 0+50S	1	45	12	67	.3	23	15	583	5.02	5	5	ND	2	36	1	2	2	158	.98	.029	3	52	.99	72	.27	6	2.16	.02	.06	1	16
LAY 6+00E 1+00S	1	28	9	72	.3	24	11	369	4.84	4	5	ND	1	27	1	2	2	156	.72	.086	3	57	.87	80	.22	7	2.35	.01	.04	1	22
LAY 6+00E 1+50S	1	44	19	84	.3	32	15	421	6.41	11	5	ND	2	28	1	2	2	196	.69	.036	3	69	1.29	85	.31	9	3.11	.01	.04	2	14
LAY 6+00E 2+00S	1	58	16	72	.3	32	16	411	5.64	4	5	ND	2	27	1	2	3	180	.74	.029	3	63	1.19	89	.26	11	2.92	.01	.04	1	1
LAY 6+00E 2+50S	1	33	19	74	.3	23	14	319	5.14	3	5	ND	2	28	1	2	2	164	.70	.049	3	60	.91	64	.29	8	2.41	.01	.03	1	1
LAY 8+00E 5+00N	1	26	13	116	.8	19	13	511	4.57	9	5	ND	2	34	1	2	2	111	.48	.069	3	46	.93	73	.26	11	2.27	.01	.04	1	2
LAY 8+00E 4+50N	1	57	16	80	.5	26	16	375	5.31	5	5	ND	2	35	1	2	3	135	.58	.028	4	54	1.10	54	.20	11	2.52	.02	.05	1	1
LAY 8+00E 4+00N	1	39	15	70	.3	19	13	447	5.62	10	5	ND	1	29	1	3	2	152	.55	.025	3	46	.93	160	.15	7	2.47	.01	.02	1	2
LAY 8+00E 3+50N	1	36	12	84	.4	24	13	615	5.29	10	5	ND	1	18	1	3	2	126	.32	.037	3	56	.89	58	.09	10	2.07	.01	.03	1	1
LAY 8+00E 3+00N	1	24	13	94	.5	16	11	347	4.96	10	5	ND	2	24	1	3	2	120	.37	.044	4	40	.92	65	.15	11	2.52	.01	.03	1	4
LAY 8+00E 2+50N	1	27	9	172	.3	20	14	465	5.02	9	5	ND	1	26	1	2	2	111	.47	.072	3	46	1.05	56	.16	4	2.73	.01	.04	2	9
LAY 8+00E 2+00N	1	112	10	92	.4	29	18	461	4.72	17	5	ND	2	34	1	2	3	102	.66	.055	4	50	1.29	77	.17	7	2.99	.02	.04	2	29
LAY 8+00E 1+50N	1	30	15	69	.2	16	13	315	4.44	7	5	ND	1	28	1	2	2	116	.48	.023	4	38	.73	84	.16	10	2.08	.02	.04	1	1
LAY 8+00E 1+00N	1	46	15	70	.3	21	14	454	5.59	21	5	ND	2	23	1	2	2	123	.43	.067	3	47	.95	60	.10	6	2.52	.01	.04	1	3
LAY 8+00E 0+50N	1	83	14	84	.6	34	19	443	5.63	14	5	ND	2	26	1	2	4	120	.47	.080	3	52	1.20	135	.16	9	3.45	.02	.06	1	5
LAY 8+00E 0+00BL	1	27	9	90	.3	17	12	359	5.33	10	5	ND	1	24	1	5	2	126	.31	.045	3	38	.42	119	.05	9	1.69	.01	.05	1	2
LAY 8+00E 0+50S	1	38	15	77	.4	31	14	377	5.69	7	5	ND	1	25	1	2	2	182	.64	.046	4	75	1.05	77	.32	11	2.85	.01	.04	1	1
LAY 8+00E 1+00S	1	31	15	76	.2	21	15	468	4.74	5	5	ND	1	31	1	2	2	123	.68	.082	4	50	.96	63	.21	7	2.32	.01	.07	1	6
LAY 8+00E 1+50S	1	38	12	75	.3	19	11	639	3.76	3	5	ND	2	27	1	2	4	100	.58	.078	4	41	.92	71	.22	8	2.10	.03	.06	1	24
LAY 8+00E 2+00S	1	41	13	65	.3	22	12	351	4.52	3	5	ND	1	27	1	2	2	117	.54	.092	4	49	.85	48	.21	9	2.32	.02	.04	1	2
LAY 8+00E 2+50S	1	32	13	76	.3	15	10	258	4.82	3	5	ND	2	28	1	3	3	139	.57	.087	4	54	.73	54	.24	8	2.01	.01	.03	1	1
LAY 10+00E 4+50N	1	75	11	74	.4	37	16	424	4.82	8	5	ND	2	31	1	2	2	109	.58	.106	3	58	1.31	63	.20	10	3.40	.02	.04	2	8
LAY 10+00E 4+00N	1	98	15	62	.5	38	16	432	4.16	14	5	ND	1	31	1	2	3	97	.63	.040	3	58	1.49	71	.21	9	2.99	.02	.05	1	1
LAY 10+00E 0+50S	1	30	7	92	.2	27	13	398	4.59	4	5	ND	1	25	1	2	2	113	.62	.075	4	56	1.07	54	.22	10	2.61	.01	.03	1	4
LAY 10+00E 1+00S	1	24	19	84	.2	27	13	374	4.92	7	5	ND	2	27	1	2	2	165	.64	.022	3	52	.99	68	.30	9	2.53	.02	.04	1	2
LAY 10+00E 1+50S	1	23	15	112	.3	22	13	482	4.80	7	5	ND	2	20	1	2	2	123	.62	.129	5	56	.87	61	.22	11	2.90	.01	.04	2	1
LAY 10+00E 2+00S	1	52	17	59	.2	24	16	410	4.70	3	5	ND	2	28	1	2	2	115	.53	.055	3	53	1.19	53	.24	10	2.61	.02	.04	1	2
LAY 10+00E 2+50S	1	48	16	63	.2	24	14	317	5.00	4	5	ND	1	29	1	2	2	130	.54	.073	4	53	1.07	54	.23	8	2.57	.02	.05	1	1
LAY 12+00E 4+50N	3	47	15	130	.4	32	18	524	5.08	13	5	ND	1	23	1	3	2	114	.40	.054	4	47	1.04	59	.11	12	2.69	.01	.05	1	1
LAY 12+00E 4+00N	2	69	28	212	.3	45	22	1523	6.08	19	5	ND	1	24	1	2	2	113	.39	.157	4	58	1.29	57	.17	15	3.09	.01	.04	1	1
LAY 12+00E 3+50N	2	69	20	276	.5	51	28	678	5.59	16	5	ND	2	36	1	2	2	113	.52	.070	4	66	1.12	70	.27	10	2.78	.02	.04	1	2
LAY 12+00E 3+00N	1	52	16	68	.2	36	15	353	4.41	9	5	ND	1	27	1	2	4	105	.62	.044	3	53	1.14	49	.20	7	2.86	.02	.03	1	31
STD C/AU-S	20	59	40	131	7.2	67	26	952	3.83	39	19	7	37	48	17	17	19	55	.48	.080	35	57	.87	177	.08	36	1.83	.06	.13	12	53

SKYLARK RESOURCES PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY BL 18+00W(SILT)	1	177	3	73	.3	36	15	794	3.84	13	5	ND	1	53	1	2	2	120	2.53	.050	4	78	1.53	67	.17	12	2.79	.02	.03	1	1
LAY BL 15+50W(SILT)	1	258	3	67	.3	28	7	784	1.28	18	5	ND	1	69	1	2	3	44	4.18	.085	2	45	.74	39	.04	34	1.04	.01	.08	1	1
LAY BL 11+00W(SILT)	8	135	11	94	.4	176	24	973	5.23	17	5	ND	2	31	1	2	2	161	3.19	.059	4	202	2.24	22	.31	16	3.79	.01	.04	2	3

SKYLARK RESOURCES LTD PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY BL 2+50E	1	65	2	115	.3	59	31	671	7.55	12	5	ND	2	20	1	2	3	191	1.26	.050	3	126	2.31	62	.22	16	3.98	.01	.03	1	5
LAY BL 3+00E	1	33	2	110	.1	37	17	364	4.29	3	5	ND	1	28	1	2	2	112	1.04	.065	4	60	1.33	52	.27	12	2.72	.01	.03	1	2
LAY BL 3+50E	1	28	9	83	.3	22	14	420	5.93	5	5	ND	2	25	1	2	2	169	.93	.083	4	58	.87	39	.33	12	2.20	.01	.03	1	19
LAY BL 4+00E	2	77	2	61	.2	34	16	351	5.20	4	5	ND	2	28	1	2	2	119	.62	.081	4	67	1.37	58	.24	8	3.48	.02	.04	1	3
LAY BL 4+50E	1	54	2	60	.1	31	15	340	4.36	5	5	ND	1	30	1	2	2	110	.70	.053	3	59	1.21	58	.23	10	2.77	.02	.04	1	280
LAY BL 5+00E	1	45	3	63	.2	43	16	331	5.02	6	5	ND	1	30	1	2	2	130	.65	.042	3	74	1.27	60	.21	11	2.49	.02	.04	1	11
LAY BL 5+50E	1	46	5	59	.2	33	15	327	5.32	5	5	ND	2	30	1	2	2	132	.57	.083	4	73	1.32	60	.22	8	2.90	.02	.03	1	4
LAY BL 6+00E	1	48	2	112	.4	30	18	358	5.05	8	5	ND	2	26	1	2	2	108	.51	.107	5	62	1.08	66	.22	11	3.21	.02	.04	1	6
LAY BL 6+50E	1	46	4	70	.2	47	19	406	5.06	4	5	ND	1	32	1	2	2	115	.75	.051	4	96	1.49	56	.25	9	2.70	.02	.03	1	2
LAY BL 7+00E	2	45	2	98	.1	31	18	388	5.02	4	5	ND	2	24	1	3	2	111	.54	.102	5	61	1.12	60	.21	7	3.46	.02	.04	1	14
LAY BL 7+50E	1	60	2	48	.2	46	16	401	4.42	5	5	ND	1	37	1	2	3	125	1.28	.030	3	71	1.73	73	.26	10	2.93	.02	.02	1	6
LAY BL 8+00E	1	44	2	90	.1	57	22	375	5.82	7	5	ND	1	24	1	2	2	149	.46	.040	4	151	2.52	75	.20	9	3.44	.02	.05	1	3
LAY BL 8+50E	2	54	5	92	.2	41	21	426	5.94	31	5	ND	2	26	1	2	2	146	.71	.089	4	75	1.36	79	.25	11	3.49	.02	.04	1	27
LAY BL 9+00E	1	49	5	91	.3	34	18	456	6.08	9	5	ND	2	25	1	2	2	148	.65	.144	5	77	1.35	88	.25	7	3.22	.02	.03	1	1
LAY BL 9+50E	1	20	4	66	.4	17	10	300	4.06	2	5	ND	2	28	1	2	2	127	.62	.033	4	44	.76	94	.22	9	1.93	.02	.03	1	1
LAY BL 10+00E	1	37	5	82	.2	26	15	352	5.57	8	5	ND	2	25	1	5	2	137	.61	.080	5	58	1.00	211	.13	6	2.59	.01	.04	1	8
LAY BL 10+50E	2	46	8	85	.3	43	19	393	5.92	11	5	ND	2	28	1	3	2	146	.75	.078	3	76	1.40	78	.26	7	3.37	.02	.03	1	4
LAY BL 11+00E	1	47	2	113	.2	35	19	425	5.99	9	5	ND	2	24	1	2	2	144	.62	.153	4	69	1.25	79	.24	9	3.60	.02	.03	1	5
LAY BL 11+50E	1	61	2	67	.1	31	18	366	4.56	11	5	ND	1	30	1	2	2	107	.56	.036	4	53	1.12	68	.20	10	2.55	.02	.04	1	2
LAY BL 12+00E	1	20	5	71	.2	12	9	303	3.38	3	5	ND	2	25	1	2	2	86	.44	.061	5	34	.55	41	.19	6	1.64	.02	.03	1	12
LAY BL 12+50E	1	40	12	143	.4	26	19	614	4.68	6	5	ND	2	32	1	2	2	109	.63	.065	5	51	1.14	95	.21	8	2.61	.02	.06	1	9
LAY BL 13+00E	1	66	3	58	.4	35	18	376	5.20	9	5	ND	2	32	1	2	2	115	.58	.072	4	63	1.20	97	.19	5	3.03	.02	.03	2	7
LAY BL 13+50E	1	22	8	79	.1	19	11	312	3.91	2	5	ND	1	28	1	2	2	103	.47	.049	6	44	.88	52	.26	5	1.75	.02	.04	1	1
LAY BL 14+00E	1	42	12	59	.3	27	15	341	5.55	10	5	ND	2	33	1	2	2	119	.48	.046	3	54	1.14	79	.19	9	2.44	.02	.05	1	7
STD C/AU-S	19	61	39	133	7.3	71	28	944	4.04	38	16	8	39	52	18	17	18	58	.51	.090	39	61	.92	182	.08	37	1.79	.07	.15	12	48

SKYLARK RESOURCES PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY BL 16+00W	1	46	24	71	.6	36	17	389	7.64	24	5	ND	1	29	1	2	2	238	.90	.027	3	94	1.77	31	.40	2	3.17	.01	.02	2	10
LAY BL 15+50W	1	51	26	99	.7	82	25	835	6.93	11	5	ND	1	21	1	2	2	222	1.25	.098	3	110	2.94	40	.35	2	3.59	.01	.02	1	5
LAY BL 15+00W	1	42	22	71	.5	49	16	336	4.97	11	5	ND	1	22	1	2	2	178	.98	.077	4	83	1.80	30	.32	4	3.78	.01	.02	1	8
LAY BL 14+50W	1	40	16	93	.2	55	23	432	4.91	15	5	ND	1	29	1	2	2	163	.92	.081	3	91	1.96	36	.30	14	4.03	.02	.01	2	5
LAY BL 14+00W	1	88	22	65	.3	55	20	478	5.20	19	8	ND	1	30	1	2	2	177	1.23	.060	2	86	2.33	46	.26	2	4.03	.01	.02	1	2
LAY BL 13+50W	1	40	21	71	.6	48	17	402	6.13	14	5	ND	1	24	1	2	2	226	1.02	.063	2	100	2.08	41	.40	2	3.37	.01	.02	1	4
LAY BL 13+00W	1	52	24	73	.4	53	19	442	5.33	23	5	ND	1	24	1	2	2	176	1.05	.078	2	84	1.96	51	.32	2	4.41	.02	.02	1	1
LAY BL 12+50W	1	28	18	55	.6	28	11	290	5.58	9	5	ND	1	27	1	2	2	213	.90	.054	3	71	1.19	37	.36	8	2.79	.01	.02	1	11
LAY BL 12+00W	1	70	23	56	.5	45	17	434	4.53	13	5	ND	1	27	1	2	2	161	1.20	.055	2	71	1.83	47	.29	2	3.69	.02	.01	1	5
LAY BL 11+50W	1	69	28	53	.2	42	16	404	3.92	19	6	ND	1	29	1	2	2	143	1.24	.037	2	68	1.80	38	.28	7	3.50	.02	.01	1	13
LAY BL 11+00W	1	21	12	53	.1	23	11	225	3.06	2	5	ND	1	16	1	2	2	121	.78	.025	2	36	.83	24	.21	2	1.80	.01	.01	1	1
LAY BL 10+50W	1	16	2	38	.1	18	7	175	3.25	6	5	ND	1	12	1	2	2	108	.48	.045	2	38	.62	17	.18	7	1.47	.01	.01	1	4
LAY BL 10+00W	1	39	24	72	.4	37	16	356	5.51	14	5	ND	1	23	1	2	2	186	1.15	.146	2	78	1.49	35	.30	2	3.49	.02	.02	3	3
LAY BL 9+50W	1	50	38	92	.6	65	23	428	5.50	20	5	ND	1	26	1	2	2	183	1.22	.049	3	102	1.90	35	.31	2	4.11	.02	.03	2	6
LAY BL 9+00W	1	69	9	56	.5	98	22	458	5.44	81	5	ND	1	20	1	6	2	177	1.09	.046	3	126	1.93	39	.26	8	3.63	.02	.02	1	12
LAY BL 8+50W	1	20	14	62	.5	24	10	277	5.22	8	5	ND	1	27	1	2	2	223	1.09	.047	3	64	1.00	44	.37	9	2.35	.01	.02	2	6
LAY BL 8+00W	1	33	13	73	.2	41	16	348	4.81	13	5	ND	1	23	1	2	2	176	1.10	.073	3	74	1.32	37	.31	2	3.14	.01	.02	1	15
LAY BL 7+50W	1	41	17	81	.3	53	19	450	5.54	9	7	ND	1	23	1	2	2	196	1.23	.046	4	91	1.89	30	.35	4	3.50	.01	.04	1	8
LAY BL 7+00W	1	52	26	74	1.0	60	20	409	6.13	24	5	ND	1	25	1	2	2	198	1.16	.077	3	107	2.12	44	.31	15	3.77	.02	.02	1	25
LAY BL 6+50W	1	31	11	95	.6	37	18	410	5.45	14	5	ND	1	26	1	2	2	180	.99	.080	4	76	1.27	67	.30	4	2.96	.02	.03	1	12
LAY BL 6+00W	2	36	2	116	.6	38	16	403	6.58	23	7	ND	1	28	1	2	2	210	.87	.046	4	75	1.22	78	.25	3	3.13	.01	.03	2	8
LAY BL 5+50W	1	66	22	90	.9	43	19	394	5.82	25	6	ND	1	23	1	2	2	169	.85	.076	3	96	1.56	58	.22	8	3.33	.01	.04	1	39
LAY BL 5+00W	1	46	16	80	.5	50	18	415	5.82	24	5	ND	1	26	1	3	2	166	.66	.085	3	109	1.70	61	.23	5	3.20	.01	.03	2	2
LAY BL 4+50W	1	56	16	75	.7	57	21	455	5.55	23	6	ND	1	22	1	2	2	146	.69	.065	3	100	1.80	47	.21	5	3.28	.01	.03	1	2
LAY BL 4+00W	1	38	20	98	.5	45	19	470	5.67	20	5	ND	1	22	1	2	2	175	.87	.091	2	88	1.52	52	.23	11	2.89	.01	.04	1	1
LAY BL 3+50W	1	46	18	81	.5	42	18	447	5.06	15	5	ND	1	23	1	2	2	162	.94	.084	3	81	1.39	52	.22	2	3.01	.01	.03	1	31
LAY BL 3+00W	1	62	22	70	.4	52	19	434	4.98	22	5	ND	1	24	1	2	2	153	1.01	.065	3	88	1.68	44	.24	2	3.30	.02	.02	1	7
LAY BL 2+50W	1	72	20	64	.3	58	21	458	4.83	31	6	ND	1	23	1	2	2	147	.93	.077	2	82	1.71	47	.22	2	3.03	.02	.03	1	9
LAY BL 2+00W	1	21	16	63	.4	22	11	276	4.61	15	5	ND	1	22	1	2	2	160	.87	.078	3	56	.78	36	.23	6	2.08	.01	.02	1	7
LAY BL 1+50W	1	53	4	58	.4	42	16	382	4.84	6	5	ND	1	27	1	2	2	166	1.37	.058	3	66	1.46	34	.28	2	2.92	.01	.05	1	10
LAY BL 1+00W	1	26	4	63	.4	30	14	346	4.74	12	5	ND	1	25	1	2	2	169	1.05	.052	3	61	1.14	40	.26	3	2.33	.01	.02	3	2
LAY BL 0+50W	1	38	10	155	.5	33	15	380	5.55	19	5	ND	3	20	1	2	2	164	.79	.110	5	68	1.12	60	.25	4	2.73	.01	.04	1	1
LAY BL 0+00W	4	319	20	222	.8	76	37	1195	6.19	34	7	ND	2	30	2	2	2	135	.63	.025	6	69	1.53	63	.24	2	3.35	.02	.04	2	3
LAY BL 0+50E	1	92	18	88	.5	46	18	374	4.83	15	5	ND	1	38	1	2	2	134	1.33	.024	6	73	1.43	103	.19	9	3.03	.02	.04	1	13
LAY BL 1+00E	1	24	15	53	.2	17	10	225	3.53	5	5	ND	2	26	1	2	2	120	.66	.072	4	45	.62	38	.21	4	1.88	.01	.03	1	37
LAY BL 1+50E	1	47	8	98	.5	54	18	364	5.27	13	5	ND	1	21	1	6	2	159	1.08	.075	3	82	1.55	40	.28	7	3.08	.01	.02	2	2
LAY BL 2+00E	1	50	8	83	.4	46	23	360	4.13	7	5	ND	2	29	1	2	2	121	.88	.058	4	79	1.45	39	.26	5	3.26	.02	.02	1	11
STD C/AU-S	19	61	40	131	7.3	70	27	905	3.96	38	20	7	37	50	18	18	20	63	.49	.081	37	60	.90	178	.08	39	1.75	.04	.13	12	50

SKYLARK RESOURCES LTD PROJECT-FIRESTEEL FILE # 87-2679

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
LAY 12+00E 2+50N	1	56	13	175	1.1	32	20	1054	5.54	31	5	ND	2	24	1	2	2	120	.43	.202	4	62	1.14	84	.18	2	3.98	.02	.04	3	2
LAY 12+00E 2+00N	1	38	10	76	.7	17	13	393	5.51	13	6	ND	2	31	1	2	2	135	.60	.106	3	54	.98	48	.25	2	2.01	.02	.05	1	4
LAY 12+00E 1+50N	1	35	12	51	.8	21	13	329	4.36	16	5	ND	1	32	1	2	2	121	.61	.028	3	48	1.01	71	.19	3	2.33	.02	.04	1	4
LAY 12+00E 1+00N	1	52	17	74	.6	34	18	414	4.87	21	5	ND	1	33	1	2	2	124	.57	.054	3	52	1.21	76	.23	2	2.58	.02	.07	3	7
LAY 12+00E 0+50N	1	49	9	111	.3	42	18	514	4.72	15	5	ND	1	31	1	2	3	131	.59	.044	3	93	1.50	76	.29	4	2.30	.02	.04	1	2
LAY 12+00E 0+50S	1	55	2	76	.6	26	13	327	5.14	11	5	ND	1	33	1	2	2	140	.57	.040	3	55	1.07	66	.28	2	2.40	.02	.04	3	1
LAY 12+00E 1+50S	1	55	11	70	.5	30	15	338	4.58	13	5	ND	1	33	1	2	2	135	.62	.031	3	55	1.20	60	.30	2	2.14	.02	.05	1	10
LAY 12+00E 2+00S	1	53	4	66	.5	32	16	353	4.25	14	5	ND	2	29	1	2	2	113	.60	.080	3	59	1.00	55	.21	2	2.48	.02	.04	1	6
LAY 12+00E 2+50S	1	30	15	85	.2	23	8	219	3.49	5	5	ND	1	44	1	2	2	114	1.15	.038	4	51	.66	114	.22	2	1.50	.02	.04	1	2
LAY 14+00E 6+00N	5	47	7	228	.7	37	25	1984	6.59	27	5	ND	2	23	2	2	2	135	.38	.067	4	51	.91	128	.19	2	2.10	.02	.06	1	1
LAY 14+00E 5+50N	5	56	19	135	.7	44	20	433	6.14	26	5	ND	2	28	1	2	2	122	.43	.063	4	57	1.15	55	.24	7	2.55	.01	.05	2	1
LAY 14+00E 5+00N	1	31	7	109	.3	19	13	312	4.59	18	5	ND	1	32	1	2	2	127	.55	.054	3	48	.90	69	.27	10	1.82	.02	.04	1	1
LAY 14+00E 4+50N	1	73	17	149	.5	37	22	419	5.08	16	5	ND	2	30	1	2	2	117	.53	.048	3	58	1.33	57	.25	5	3.13	.02	.04	1	1
LAY 14+00E 4+00N	1	65	12	72	.7	53	17	540	4.94	22	5	ND	2	34	1	2	2	146	1.12	.042	3	84	1.80	55	.32	2	3.42	.02	.04	1	2
LAY 14+00E 3+50N	1	55	9	172	.6	50	24	447	6.00	25	5	ND	3	22	1	2	2	147	.68	.116	4	84	1.47	75	.29	13	4.60	.02	.04	1	1
LAY 14+00E 3+00N	1	59	12	140	.7	21	20	470	6.24	22	5	ND	2	32	1	2	2	151	.51	.050	4	48	.97	55	.40	3	2.05	.01	.04	1	8
LAY 14+00E 2+50N	1	18	9	81	.5	19	13	535	4.15	12	5	ND	1	25	1	3	2	130	.52	.048	3	40	1.31	84	.33	2	2.10	.03	.07	2	3
LAY 14+00E 2+00N	1	23	13	47	.1	14	10	243	4.17	13	5	ND	1	26	1	2	2	130	.43	.062	3	39	.72	40	.29	5	1.68	.02	.03	1	28
LAY 14+00E 1+50N	1	46	7	61	.4	23	13	320	4.01	9	5	ND	2	31	1	2	2	108	.51	.047	3	46	.82	54	.23	2	2.07	.02	.03	1	2
LAY 14+00E 1+00N	1	53	16	75	.3	26	15	376	4.70	16	5	ND	1	26	1	2	2	110	.48	.080	3	49	1.07	82	.19	2	2.42	.02	.05	1	2
LAY 14+00E 0+50N	1	71	18	62	.2	26	17	376	4.39	22	5	ND	2	38	1	2	2	104	.61	.048	3	56	1.27	70	.23	5	2.78	.03	.04	1	6
LAY 16+00E 5+50N	1	58	14	58	.3	37	16	505	4.07	12	5	ND	1	37	1	2	2	111	.88	.023	3	64	1.49	59	.32	2	2.90	.02	.05	1	5
LAY 16+00E 5+00N	1	26	16	52	.3	21	14	351	3.53	10	5	ND	1	33	1	2	2	106	.79	.029	3	44	.91	56	.24	4	1.83	.02	.04	1	1
LAY 16+00E 4+50N	1	38	25	119	.2	28	14	362	4.52	17	5	ND	1	30	1	2	2	119	.71	.056	3	57	1.15	54	.27	2	2.52	.02	.03	1	4
LAY 16+00E 2+50N	1	40	7	127	.3	30	17	359	4.44	14	5	ND	1	29	1	2	2	112	.65	.057	3	56	1.11	58	.26	9	2.44	.02	.04	1	1
LAY 16+00E 2+00N	1	79	20	69	.2	33	16	371	4.18	11	5	ND	1	32	1	2	2	115	.58	.022	3	53	1.23	106	.24	2	2.35	.02	.04	1	1
LAY 16+00E 1+50N	1	40	22	76	.3	21	13	427	4.53	15	5	ND	1	31	1	2	2	119	.51	.046	4	48	.94	73	.24	8	2.24	.02	.04	2	12
LAY 16+00E 1+00N	1	69	8	106	.4	28	17	505	5.04	15	5	ND	2	27	1	2	2	111	.49	.187	3	57	1.28	68	.22	2	3.00	.02	.06	4	1
LAY 16+00E 0+50N	1	52	12	60	.4	24	18	1102	3.64	15	5	ND	2	43	1	2	2	108	.89	.027	3	48	1.00	134	.22	7	1.85	.02	.05	1	1
LAY BL 20+00N	1	32	19	92	.5	35	17	427	7.40	21	5	ND	1	23	1	2	2	222	.84	.050	3	82	1.38	43	.42	8	3.20	.01	.04	1	6
LAY BL 19+00N	1	37	2	85	.4	28	15	418	5.50	16	5	ND	2	29	1	2	2	168	.81	.069	3	67	1.28	51	.38	7	3.46	.02	.04	1	25
LAY BL 18+50N	1	49	18	84	.1	48	23	637	5.80	24	5	ND	2	53	1	2	2	166	1.30	.046	3	89	2.19	45	.35	8	4.13	.02	.04	1	1
LAY BL 18+00N	1	71	12	116	.2	35	21	719	6.23	23	5	ND	2	29	1	2	2	164	.94	.078	3	74	1.61	80	.31	3	3.62	.01	.05	1	8
LAY BL 17+50N	1	68	19	64	.3	50	22	502	5.30	22	5	ND	1	34	1	2	2	146	.90	.060	2	78	1.84	41	.33	7	3.92	.02	.04	1	1
LAY BL 17+00N	1	34	12	61	.5	37	15	434	5.30	30	8	ND	1	27	1	2	2	154	.85	.078	2	74	1.41	36	.34	7	3.14	.01	.04	1	3
LAY BL 16+50N	1	30	17	55	.4	31	14	341	4.51	17	5	ND	1	22	1	2	2	148	.76	.014	2	55	1.28	27	.31	8	2.40	.01	.02	1	2
STD C/AU-S	20	63	40	132	7.5	68	29	1027	4.01	41	17	8	39	51	19	18	23	58	.50	.094	41	59	.91	182	.09	36	1.73	.07	.15	13	52

BL0+00 1+00E 2+00E 3+00E 4+00E 5+00E 6+00E 7+00E 8+00E 9+00E 10+00E

L10+00N

L9+00N

L8+00N

L7+00N

L6+00N

L5+00N

L4+00N

L3+00N

L2+00N

L1+00N

L0+00

CH 2 SC 1

CH 4 CH 11

○ Indicates anomalous values

Sb ≥ 7 ppm

As ≥ 12 ppm

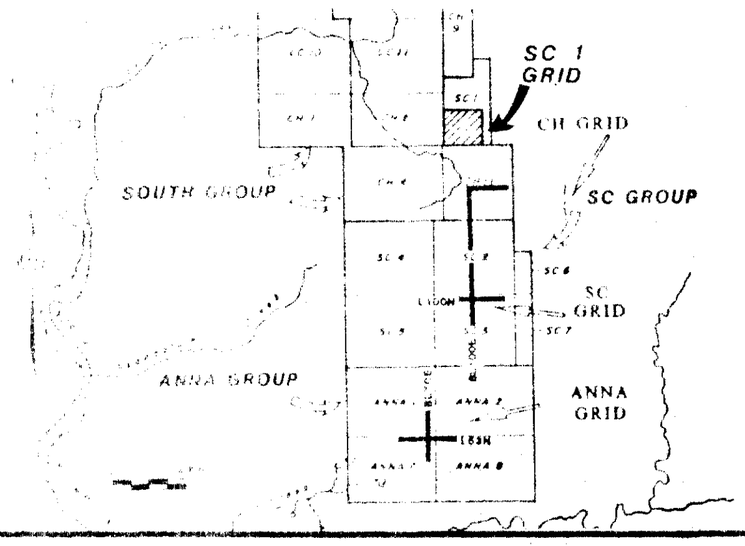
4 , 3 As , Sb ppm

073 soil sample location and number

All soil sample numbers prefixed by SC1SS

Creek Swamp

Road Claim line



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,475

MINNOVA Inc.

BAR PROJECT

SC 1 GRID

SOIL GEOCHEMISTRY

As, Sb ppm

50 100 150 200 250m

SCALE 1 2500

N.T.S. 92P/8,82M/5		MAP 7
DRAWN BY KS/sg		
DATE DEC 1987		

BL0+00 1+00E 2+00E 3+00E 4+00E 5+00E 6+00E 7+00E 8+00E 9+00E 10+00E

L10+00N

L9+00N

L8+00N

L7+00N

L6+00N

L5+00N

L4+00N

L3+00N

L2+00N

L1+00N

L0+00

CH 2 SC 1

CH 4 CH 11

17,475

◯ Indicates anomalous values

Au ≥ 15 ppb

Ag ≥ 1.2 ppm

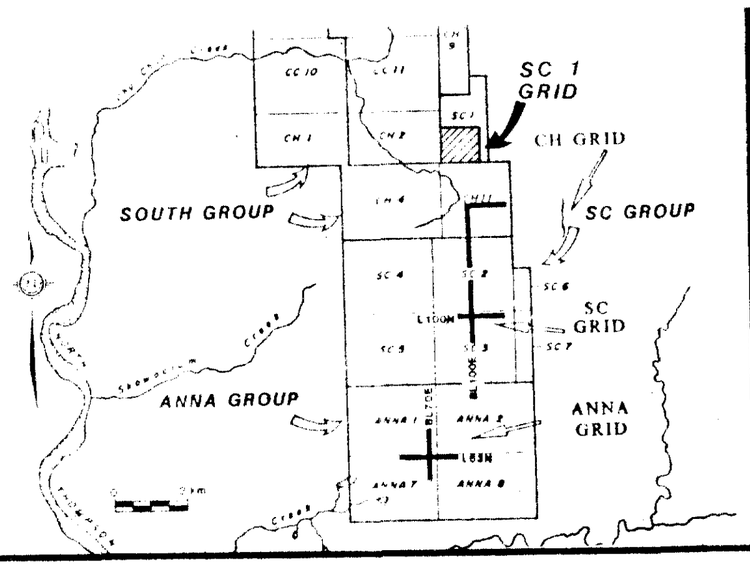
0.4, 5 Ag ppm, Au ppb

073 soil sample location and number

All soil sample numbers prefixed by SC1SS

Creek Swamp

Road Claim line



MINNOVA Inc.

BAR PROJECT

SC 1 GRID

SOIL GEOCHEMISTRY

Ag ppm, Au ppb

0 50 100 150 200 250m

SCALE 1: 2500

N.T.S. 92P/8,82M/5		MAP 6
DRAWN BY: KS/sg		
DATE DEC.1987		

BL0+00 1+00E 2+00E 3+00E 4+00E 5+00E 6+00E 7+00E 8+00E 9+00E 10+00E

L10+00N L9+00N L8+00N L7+00N L6+00N L5+00N L4+00N L3+00N L2+00N L1+00N L0+00

CH 2 SC 1 CH 4 CH 11

○ Indicates anomalous values

Cu≥30 ppm

Zn≥70 ppm

Pb≥20 ppm

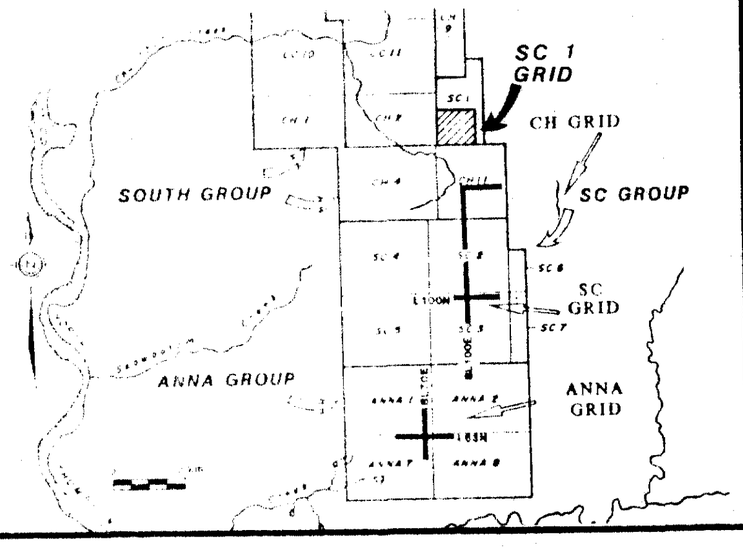
9, 17, 13
Cu, Pb, Zn ppm

073
soil sample location and number

All soil sample numbers prefixed by SC1SS

Creek Swamp

Road Claim line



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,475

MINNOVA Inc.

BAR PROJECT

SC 1 GRID

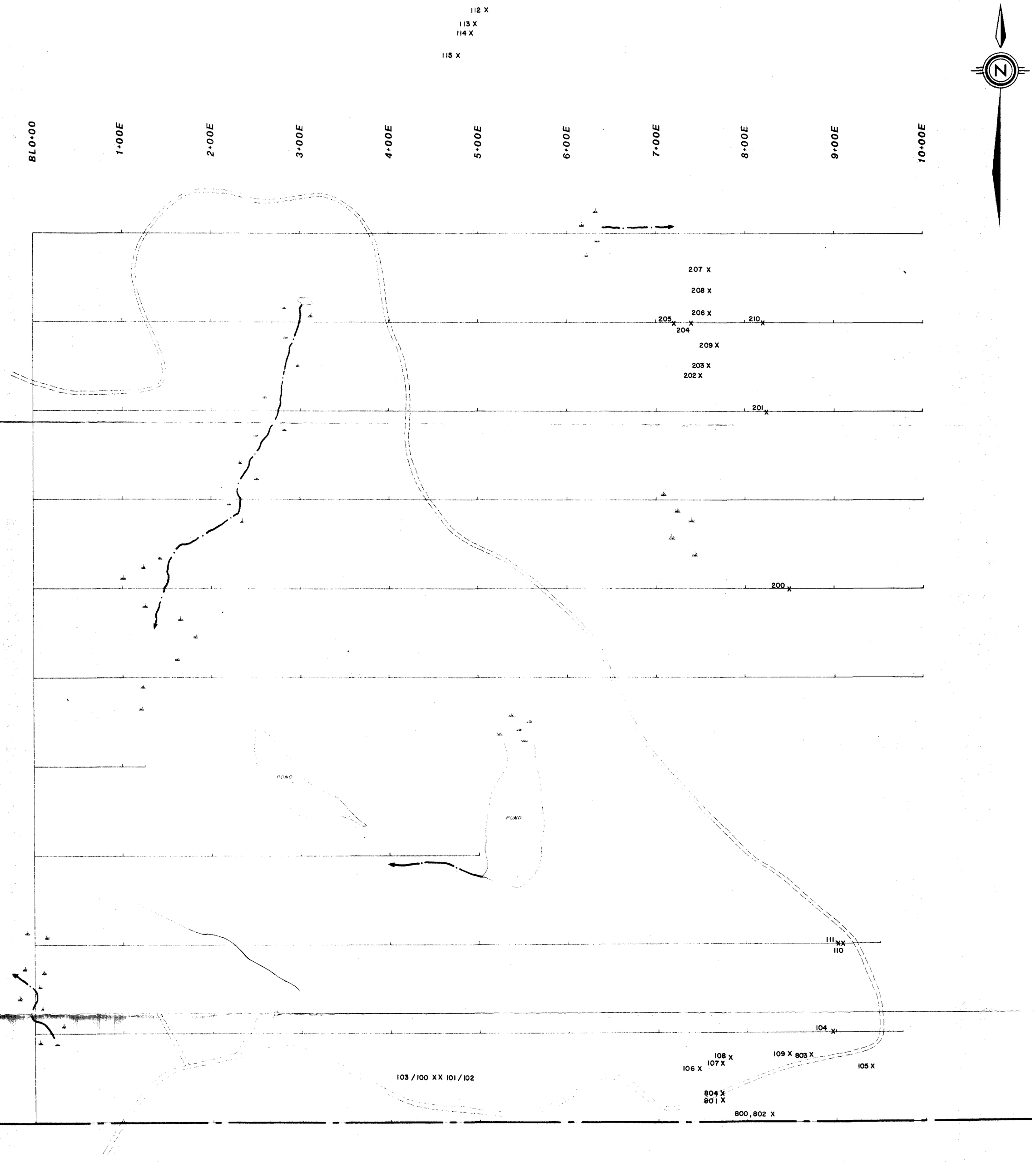
SOIL GEOCHEMISTRY

Cu, Pb, Zn ppm

0 50 100 150 200 250m

SCALE 1:2500

N.T.S. 92P/8,82M/5		MAP 5
DRAWN BY KS/sg		
DATE DEC.1987		



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,475

Sample #	Al2O3%	BaX	CaO%	Fe2O3%	K2O%	MgO%	MnO2%	Na2O%	SiO2%	TiO2%	ZrX	As ppm	Au ppm	Cu ppm	Pb ppm	Sb ppm	Zn ppm	Au ppb
SC1 87 100	7.32	0.041	1.68	4.86	0.24	2.56	0.24	0.88	78.68	0.42	0.005	0.8	8	114	17	1	78	5
SC1 87 101	11.05	0.320	1.07	4.12	2.52	3.27	0.10	0.01	73.51	0.70	0.019	0.7	19	17	4	1	89	5
SC1 87 102	-	-	-	-	-	-	-	-	-	-	-	0.9	4	21	9	1	50	5
SC1 87 103	15.41	0.914	7.22	10.00	0.76	6.93	0.42	2.78	50.62	1.71	0.006	2.0	24	42	12	2	71	5
SC1 87 104	5.13	0.082	0.18	4.80	0.86	1.48	0.05	0.01	84.81	0.27	0.005	0.3	2	19	6	3	73	5
SC1 87 105	15.47	0.400	0.16	2.29	4.32	0.93	0.01	0.07	72.90	0.77	0.008	0.8	1	13	18	2	102	10
SC1 87 106	15.31	0.915	10.25	10.69	0.07	7.17	0.27	3.09	48.96	1.52	0.006	0.8	11	39	7	1	60	5
SC1 87 107	13.54	0.315	0.20	5.70	2.95	1.90	0.06	0.04	71.75	0.87	0.011	0.6	8	22	4	1	72	10
SC1 87 108	17.16	0.359	0.10	8.71	3.40	3.32	0.10	0.09	63.17	0.91	0.016	0.5	6	19	7	6	101	15
SC1 87 109	17.08	0.316	0.18	8.48	3.30	2.99	0.10	0.04	63.78	0.87	0.010	2.0	32	104	13	8	78	5
SC1 87 110	15.25	0.556	0.03	5.51	3.69	2.57	0.04	0.07	69.04	0.66	0.016	1.0	16	5	8	1	73	10
SC1 87 111	16.39	0.432	0.03	3.82	4.33	1.81	0.03	0.07	69.25	0.76	0.008	0.4	5	27	11	1	98	5
SC1 87 112	3.10	0.834	0.04	1.71	0.67	0.60	0.10	0.14	89.73	0.17	0.005	0.6	3	10	7	1	40	5
SC1 87 113	4.22	0.295	0.10	1.86	0.80	0.97	0.08	0.21	88.73	0.26	0.005	0.6	9	8	4	2	47	5
SC1 87 114	4.72	0.653	0.11	3.30	1.25	0.57	0.04	0.23	86.02	0.29	0.005	0.6	7	10	16	2	17	10
SC1 87 115	4.62	0.779	0.16	2.12	1.28	1.24	0.11	0.32	86.22	0.26	0.005	0.6	5	33	10	1	15	20
SC1 87 200	5.99	0.529	0.05	4.20	0.86	1.33	0.03	0.54	83.47	0.35	0.005	0.8	9	123	10	1	15	15
SC1 87 201	7.98	0.973	0.32	3.58	1.96	1.69	0.06	0.07	79.77	0.52	0.013	0.4	1	6	3	2	73	5
SC1 87 202	8.21	1.141	0.73	3.15	1.57	2.05	0.15	0.28	78.84	0.51	0.013	1.0	3	22	8	2	81	5
SC1 87 203	-	-	-	-	-	-	-	-	-	-	-	0.3	8	35	10	1	71	5
SC1 87 204	7.61	0.760	0.36	3.01	1.55	1.10	0.06	0.38	81.64	0.49	0.009	1.1	4	38	3	1	76	5
SC1 87 205	1.57	0.397	0.02	1.10	0.48	0.14	0.03	0.01	93.68	0.07	0.005	0.6	11	11	8	1	11	10
SC1 87 206	9.39	0.214	0.48	4.46	0.65	2.12	0.17	0.14	73.35	0.62	0.005	1.2	10	15	7	2	66	25
SC1 87 207	8.00	0.703	2.34	3.43	1.82	2.99	0.08	0.62	75.76	0.57	0.022	1.2	11	18	8	1	85	15
SC1 87 208	6.68	0.425	2.63	3.47	1.33	2.95	0.08	0.30	77.76	0.43	0.009	0.4	6	17	12	1	81	10
SC1 87 209	5.86	0.809	2.63	2.79	1.20	2.07	0.10	0.15	79.92	0.34	0.005	0.4	2	17	7	2	80	5
SC1 87 210	5.79	0.661	0.44	3.47	1.51	1.81	0.11	0.13	83.02	0.31	0.005	0.4	9	3	5	1	69	5
SC1 87 800	4.98	0.129	5.99	2.48	0.92	2.19	0.17	0.10	77.57	0.29	0.007	0.2	1	18	11	1	52	5
SC1 87 801	13.47	0.429	0.96	1.85	3.45	1.86	0.06	0.09	74.60	0.13	0.007	0.5	6	2	7	3	26	5
SC1 87 802	6.46	0.164	0.64	3.49	1.19	2.08	0.07	0.04	82.87	0.31	0.005	0.8	12	37	10	6	82	5
SC1 87 803	14.96	0.011	1.49	2.12	0.04	0.98	0.04	7.66	68.80	0.72	0.012	2.5	16	19	14	1	26	5
SC1 87 804	9.87	0.230	0.29	10.44	2.30	0.87	0.01	0.06	73.43	0.85	0.013	0.7	41	44	57	5	51	30

MINNOVA Inc.

BAR PROJECT

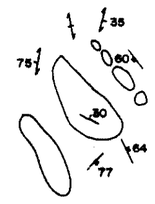
SC 1 GRID

LITHOGEOCHEMISTRY

0 50 100 150 200 250m

SCALE: 1: 2500

N.T.S. 92P/8,82M/5		MAP. 2
DRAWN BY: KS/sg		
DATE: DEC.1987		



(200 m North)
3.3, 6.1
cherty ash tuff (interbedded)
locally 5% py as weathered
out cubic crystals, interstitial,
locally folded

BL 0+00 | 1+00E | 2+00E | 3+00E | 4+00E | 5+00E | 6+00E | 7+00E | 8+00E | 9+00E | 10+00E

L 10+00N | L 9+00N | L 8+00N | L 7+00N | L 6+00N | L 5+00N | L 4+00N | L 3+00N | L 2+00N | L 1+00N | L 0+00

mainly tuffaceous chert ?

1.1

3.3(6.1)

6.5,6.9

3.3

6.1,1.1

POND

POND

× 4.1/1.1
× 5% diss py

× 1.1/1.4 | × 1.1 | ×× 1.1 | × 1.1/4.1 | × 6.8

3.3 0 | 3.3 tr py | 3.3 1% tr py | 3.3 3% py | 3.3 × | 2.3/3.3

6.1, 6.11 | 6.11, 6.2 | 6.1 | 1.1

6.5 debris flow | 6.9 rusty weathering | 4.1? 5% py | 4.1? 1.1 1% py, po wk cb locally cherty | chert pebble conglomerate | arg conglomerate debris flow | sulphide blebs to 20cm lenses with cubic py

6.5 3.3 fine ash tuff | 6.5 arg | 6.5 debris flow arg | 6.5 2% py

BL 100 E (Chu Chua Grid)

CH SC 1 | CH 2 | CH CH 11 | CH 4

LEGEND

ROCK TYPE

1. MAFIC VOLCANICS
2. INTERMEDIATE VOLCANICS
3. FELSIC VOLCANICS
4. MAFIC INTRUSION
5. FELSIC INTRUSION
6. SEDIMENT

ROCK TYPE TEXTURAL CODES

1. Massive flows
2. Pillowed flows, breccia
3. Tuff, ash tuff
4. Lapilli tuff, lapilli and ash
5. Agglomerate (block size frags >64mm)
6. Tuff breccia
7. Debris flow (1,2, or 3 depending on predominant fragment types)

1. Diorite
2. Gabbro
3. Diabase

1. QFP

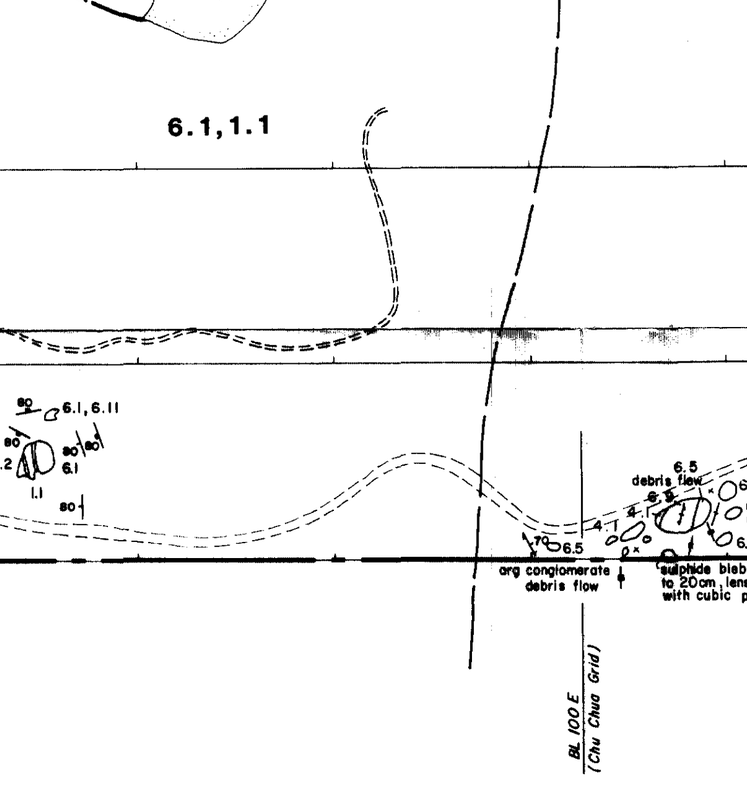
1. Chert, ribbon chert, chert breccia
2. Chert with argillite
3. Quartzite argillite fgr wacke
4. Quartz pebble conglomerate.
5. Argillite/phyllite
6. Limestone
7. Greywacke (fgr quartz wackes)/ or greenwacke (contingent on chl content)
8. Limestone cobble breccia
9. Coarse wackes: ± grits; ± sandstones
10. Multilithic pebble conglomerates (with micaceous clasts, argillite clasts etc.)
11. Siltstone
12. Debris flow

ABBREVIATIONS

ank-ankerite, arg-wacke, po-pyrrhotite, gp-graphite, bx-breccia, gl-galena, plag-plagioclase, sed-sediment, qv-quartz vein, mod-moderate, blk-black, QFP-quartz feldspar porphyry, bx-breccia, chl-chlorite, epi-epidote, arg-argillite, carb-carbonate, py-pyrite, frags-fragments, alt-altered, tr-trace, fl-float, sil-siliceous, stwk-stockwork, grn-green, vol-volcanic, fgr/mgr/cgr-fine, medium, coarse grained, qtz-quartz, monz-monzonite, metam-metamorphism, clas-diorite, spy-chalcopyrite, congl-conglomerate

SYMBOLS

Outcrop | Bedding
Subcrop | Geological contact (conformable)
Fragments | Geological contact (intrusive)
Foliation | Break in slope
Schistosity | Creek
Jointing | Road
Massive conductor axis (1988)
Fault | Float



MINNOVA Inc.

BAR PROJECT

SC 1 GRID

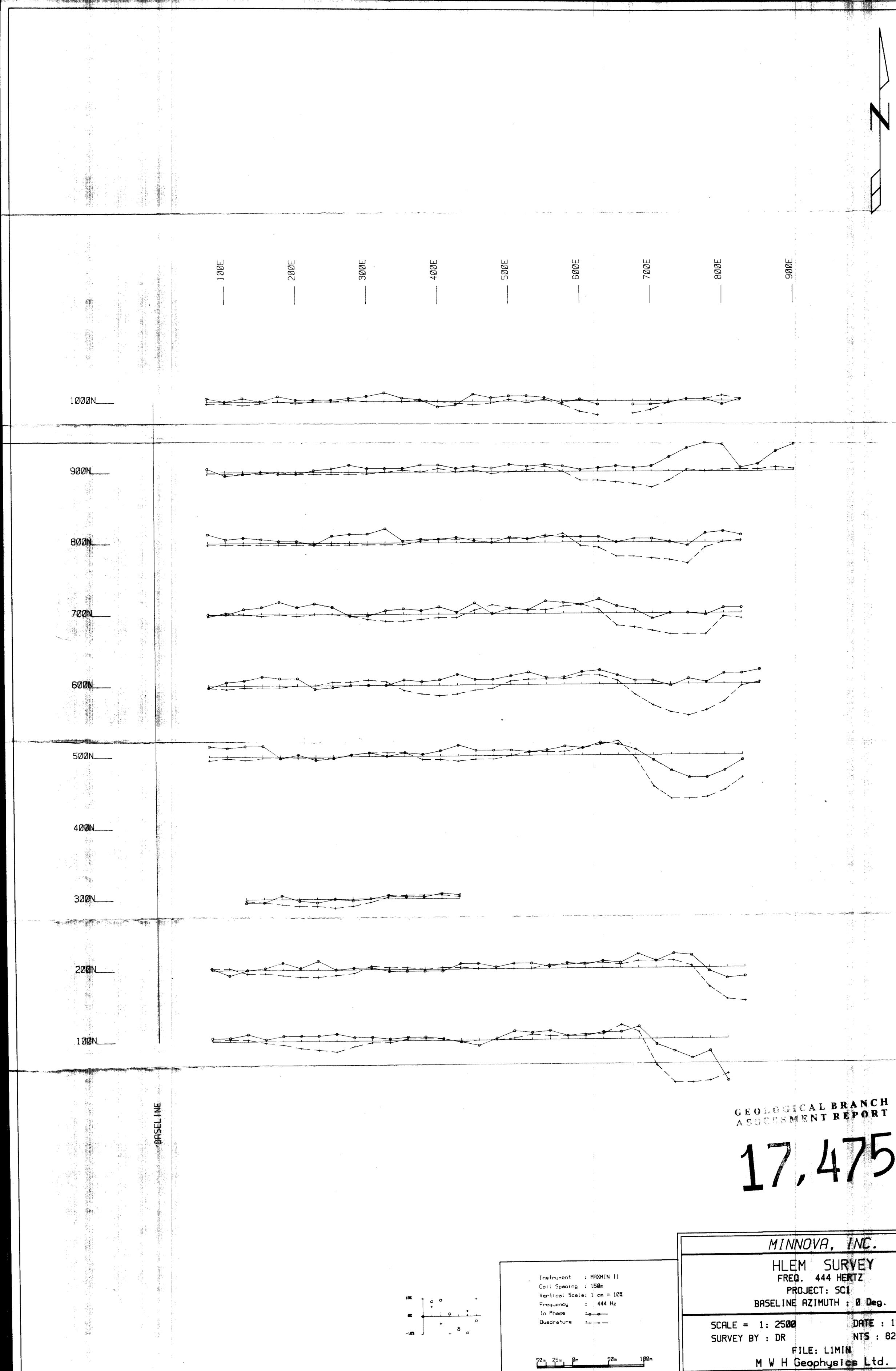
GEOLOGY

0 50 100 150 200 250m

SCALE: 1: 2500

N.T.S. 92P/8,82M/5
DRAWN BY: KS/sg
DATE: DEC.1987

MAP: 1



Instrument : MAXMIN II
Coil Spacing : 150m
Vertical Scale: 1 cm = 10%
Frequency : 444 Hz
In Phase
Quadrature

50m 25m 0m 50m 100m

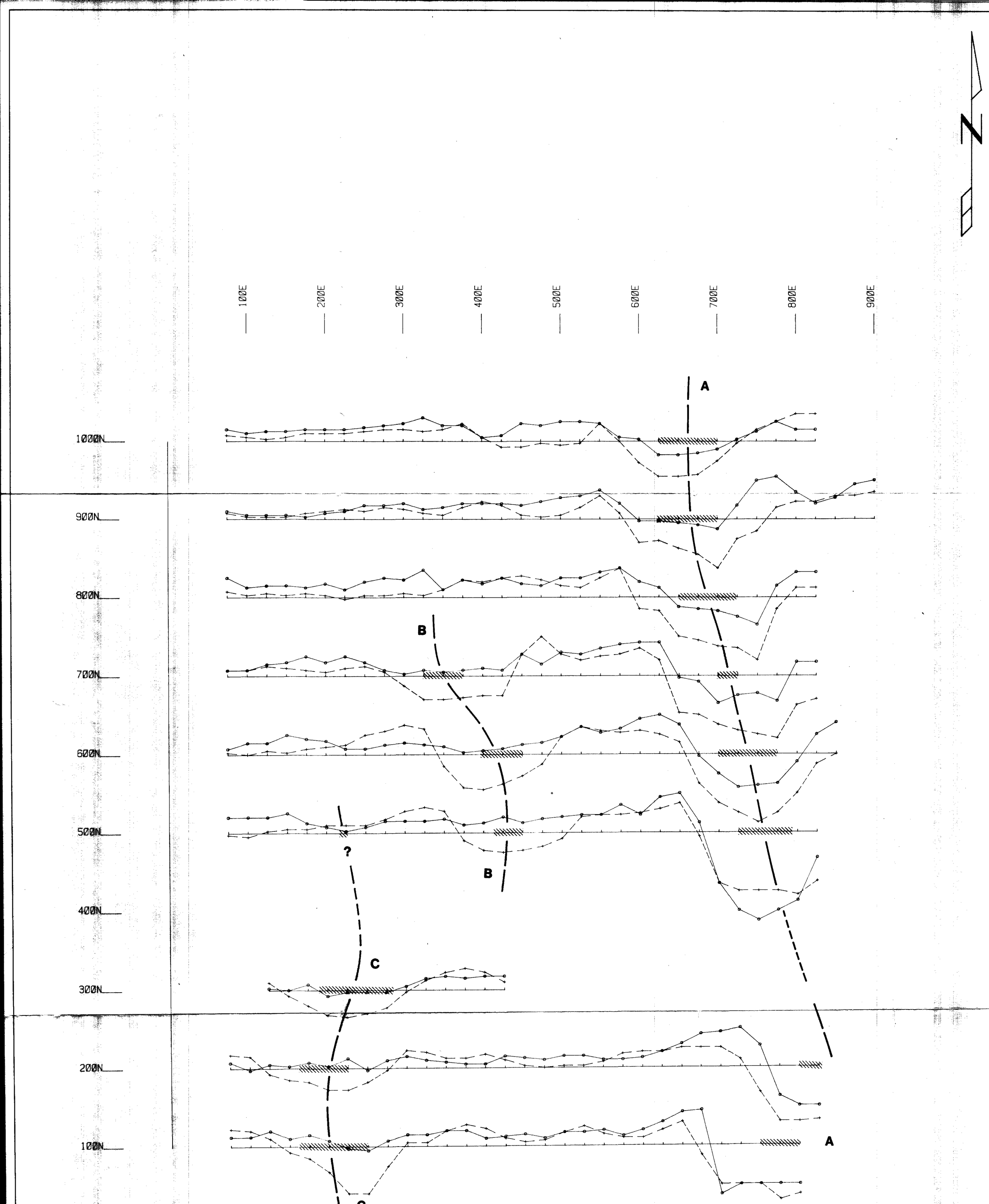
GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,475

MINNOVA, INC.

HLEM SURVEY
FREQ. 444 HERTZ
PROJECT: SC1
BASELINE AZIMUTH : 0 Deg.

SCALE = 1: 2500 DATE : 10/11/87
SURVEY BY : DR NTS : 82M
FILE: L1MIN
M W H Geophysics Ltd.



Instrument : MAXMIN II
Coil Spacing : 150m
Vertical Scale: 1 cm = 10%
Frequency : 1777 Hz
In Phase
Quadrature

50m 25m 0m 50m 100m

MINNOVA, INC.

HLEM SURVEY
FREQ. 1777 HERTZ
PROJECT: SC1
BASELINE AZIMUTH : 0 Deg.

SCALE = 1: 2500 DATE : 10/11/87
SURVEY BY : DR NTS : 82M
FILE: H1MIN
M W H Geophysics Ltd.