ARIS SUMMARY SHEET

District Geologist, Kamloops Off Confidential: 89.04.07

ASSESSMENT REPORT 17556 MINING DIVISION: Kamloops

PROPERTY: Barn
LOCATION: LAT 50 38 00 LONG 120 07 00
UTM 10 5612800 703902
NTS 092I09E
CLAIM(S): Barn
OPERATOR(S): Jaguar Equities
AUTHOR(S): Roberts, A.F.
REPORT YEAR: 1988, 91 Pages
COMMODITIES SEARCHED FOR: Gold,Silver
GEOLOGICAL SUMMARY: Tertiary Kamloops Group sedimentary rocks strike 120 degrees and dip 75 degrees north. Altered feldspar porphyry with completely kaolinized amygdules and argillite are evident. Upper Triassic Nicola Group rocks occur west of the drilling area. To the extreme south, outcrops consist of granite and biotite-feldspar and feldspar porphyry. The drilled area is highly brecciated with leaching and pyritic quartz-carbonate filled fractures.
WORK DONE: Geophysical,Drilling
DIAD 361.8 m 6 hole(s);BQ
Map(s) - 2; Scale(s) - 1:10 000,1:800
EMGR 31.2 km;VLF
Map(s) - 2; Scale(s) - 1:2500
GEOL 576.0 ha
Map(s) - 1; Scale(s) - 1:12 000
LINE 21.6 km
MAGG 31.2 km
Map(s) - 1; Scale(s) - 1:2500
MINFILE: 092INE128

ASSESSMENT REPORT

ON THE

MAGNETIC SURVEY

VLF-EM SURVEY

DIAMOND DRILLING

ON THE

BARN CLAIM [12 UNITS]

KAMLOOPS M. D.

NTS 92I/9

Latitude 50°38'N Longitude 120°07'W

for

JAGUAR EQUITIES INC.
Vancouver, B. C.

by

A.F. ROBERTS, P.ENG.

July 1, 1988

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MAPS

Ref. No.

1] Fig. 1 Location Map, B.C. Road Map 1 cm = 24 KH2.....[Frontispiece]

2] Fig. 2 Topographic Map, NTS 92I/9, 1:50,000.....[Follows page 1]

3] Fig. 3 Claim Map, B.C. Department of Mines 92I/9, 1:50,000.....[Follows page 2]

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5] Fig. 5 Local Geology, after C.P. Purdy, P.Eng. 1" = 1,000 ft., 1973..... [Back Pocket]

6] Fig. 6 Magnetometer Survey Map, R.F. Sheldrake, Geophysicist, 1:5,000, 1988.....[Back Pocket]

8] Fig. 8 VLF-EM Total Field, R.F. Sheldrake, Geophysicist, 1:5,000, 1980.....[Back Pocket]

VLF-EM - Dip Angle, R.F. Sheldrake, Geophysicist, 1:5,000, 1988.....[Back Pocket]

11] Fig. 9 Vertical Projection of DD Holes looking north [Follows page 6]

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7] Appendix "A" Letter re Geophysical Surveys, from Ronald F. Sheldrake, Geophysicist.....[End of Report]

9] Appendix "B" Diamond Drill Logs.....[End of Report]

10] Appendix "C" Assay Certificates.....[End of Report]

REFERENCES

1] Assessment Report No. 3616, December 7, 1971 D.E. Hopkins, P. Eng.

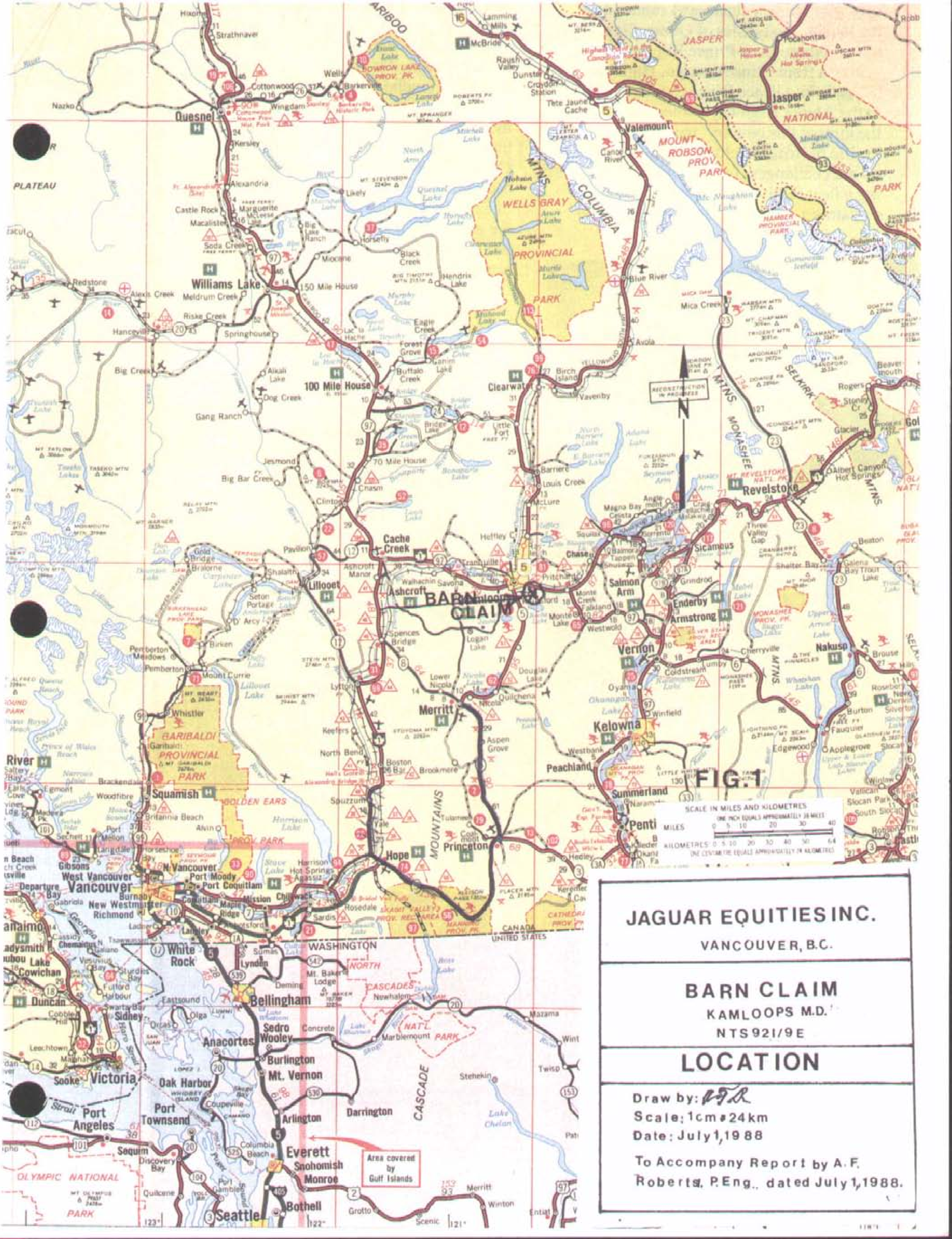
2] Assessment Report No. 4315, May 26, 1973, C.P. Purdy, Jr., P. Eng.

3] Report on the Carlin 2 Claim, Kamloops M.D., for United Mineral Services, J.B.P. Sawyer, P.Eng., May 11, 1976

4] Report on the Carlin 2 M.C. held by R. Dickenson; R. Dickenson-McLaren, October, 1975

5] Report on the Carlin 2 M.C. for T. Alexander; J.B.P. Sawyer, P. Eng., May 11, 1979

6] Geochemical-Geophysical Report on the Carlin 2 M.C. for Vantex Resources Inc.; A.F. Roberts, P.Eng., October 31, 1980



JAGUAR EQUITIES INC.

VANCOUVER, B.C.

BARN CLAIM

KAMLOOPS M.D.

NTS 92I/9E

LOCATION

Draw by: AFR

Scale: 1cm = 24km

Date: July 1, 1988

To Accompany Report by A.F. Roberts, P.Eng., dated July 1, 1988.

S U M M A R Y

The Company has completed VLF-EM surveys over the portion of the property covered by geochemical and EM anomalies located in 1980.

Six diamond drill holes located over the old geochemical gold anomalies have been drilled, with indeterminate results.

There are two ore grade intersections in DD holes #1 and #4. All holes have shown intersections with anomalous values.

It has not been possible to correlate these intersections from hole to hole, nor to correlate the rock types to date.

The magnetic survey has given a good structural picture of the property. The EM is rather indeterminate although more or less coinciding with the indicated faults.

Overall, it is an encouraging picture to date, therefore it is recommended that the Company continue with the drilling program.

Respectfully submitted,

A.F. Roberts, P.Eng.
July 1, 1988

ASSESSMENT REPORT ON THE

1] MAGNETIC SURVEY

2] VLF-EM SURVEY

3] DIAMOND DRILLING

on the

BARN CLAIM [12 UNITS]

KAMLOOPS M. D.

NTS 92I/9

Latitude 50°38'N Longitude 120°07'W

for

JAGUAR EQUITIES INC.
Vancouver, B. C.

by

A.F. ROBERTS, P.ENG.

July 1, 1988

INTRODUCTION:

This report is authorized by the Directors of the Company.

Its purpose is to fulfill the requirements of the Mining Act with respect to VLF-EM and Magnetic Surveys carried out in the last few months. In addition, the results of a short diamond drilling program will be reported, complete with drill logs, and assays.

This work was done since the beginning of March to the middle of June this year.

LOCATION,[1] ACCESS, TOPOGRAPHY:[2]

The property is reached by paved road a distance of approximately eight miles easterly and south of Kamloops to the village of Barnhartvale.

1] Fig. 1] Location Map; B.C. Road Map, 1 cm = 24 Km [Frontispiece]

2] Fig. 2] Topography; NTS 92I/9, 1:50,000 [Follows page 1]

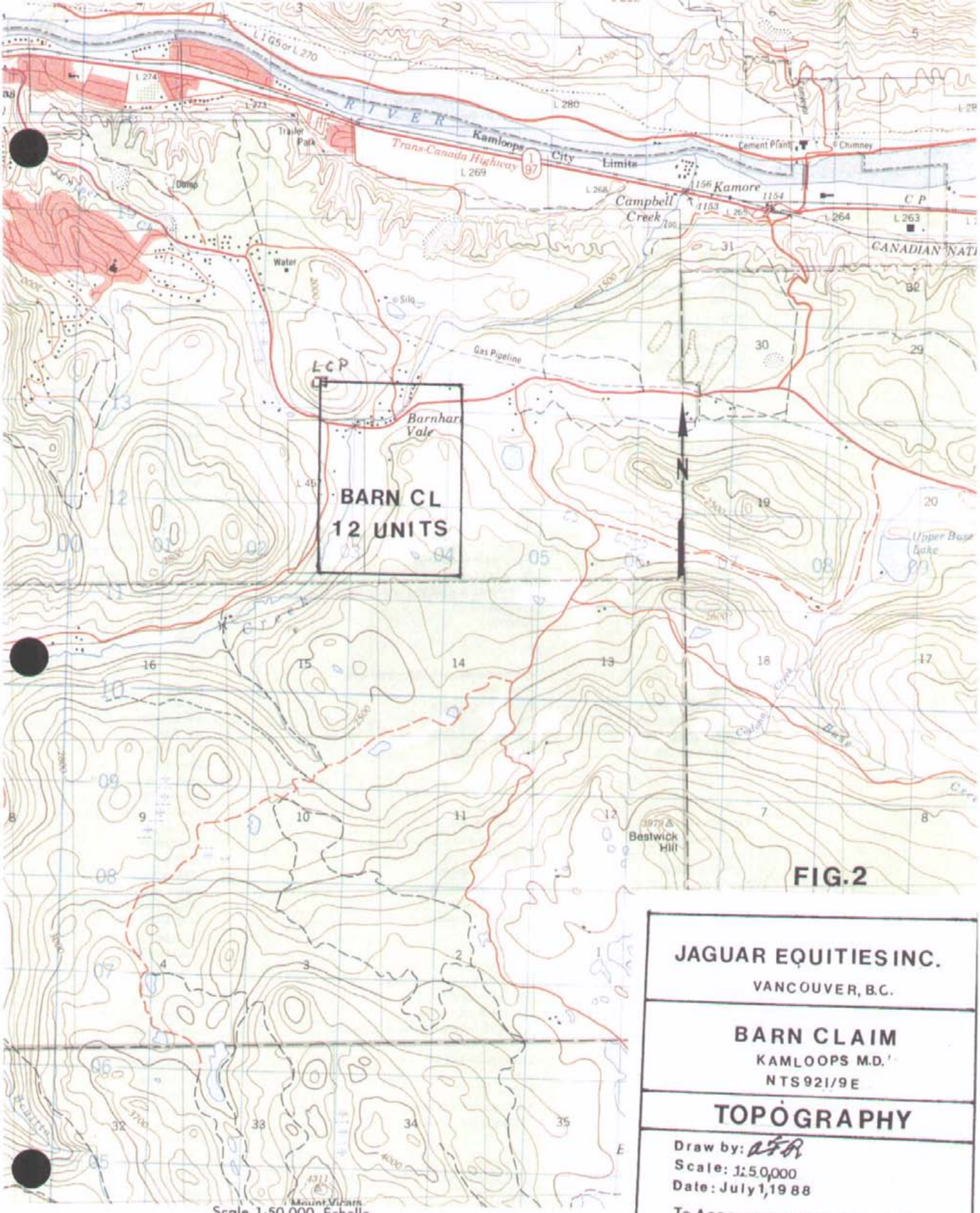


FIG.2

Scale 1:50 000 Echelle

0 1 2 3 Miles

Metres 1000 0 1000 2000 3000 4000 Mètres

Yards 1000 0 1000 2000 3000 4000 Verges

JAGUAR EQUITIES INC.

VANCOUVER, B.C.

BARN CLAIM

KAMLOOPS M.D.

NTS 92I/9E

TOPOGRAPHY

Draw by: ASR

Scale: 1:50,000

Date: July 1, 1988

To Accompany Report by A. F. Roberts, P.Eng., dated July 1, 1988.

A country road, south of the highway is followed up to the area of the claim. It is a good dirt road.

Generally, the country is open and rolling with only one small cone-shaped hill where the drilling is being done.

There is very little timber on the property, non-commercial, consisting of pine, hemlock, and spruce.

Water requirements for diamond drilling are being met by hauling with a tank truck from Campbell Creek.

There are very few rock exposures.

CLAIM: 5]

The claim is described as follows:

Name	Unit	Record No.	Expiry Date
BARN	12	6590	April 7, 1987

Sufficient work has been done and recorded to put the claim in good standing for several years.

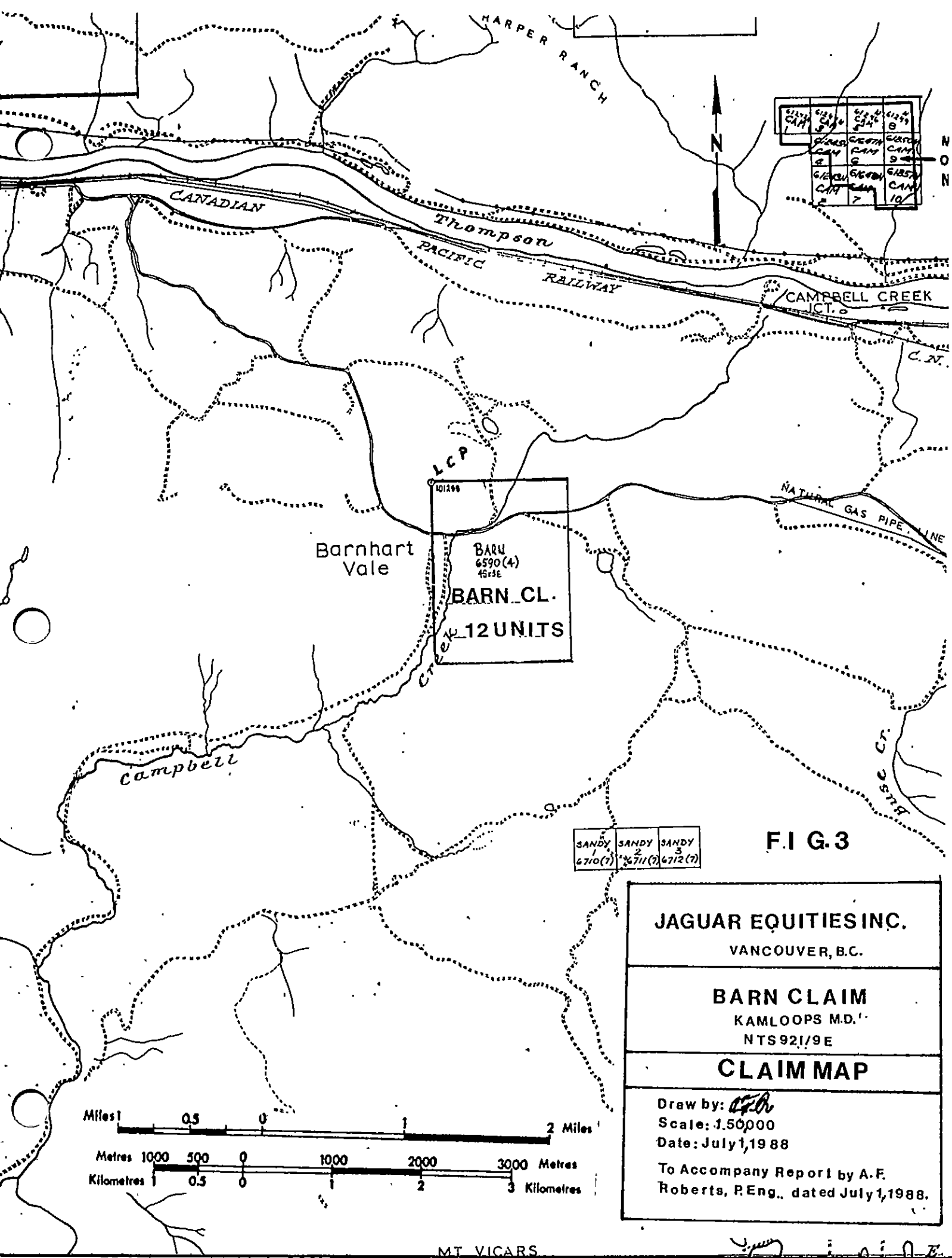
The exact location and the area covered can only be determined by a legal survey.

HISTORY: *

Trenching on the property suggests prospecting early in this century, as there are no known records of it.

3] Fig. 3 - Claim Map: B.C. Department of Mines & Energy, 92I/9, 1:50,000 [Follows page 2]

* See list of References on Index page



F.I G.3

JAGUAR EQUITIES INC.
VANCOUVER, B.C.

BARN CLAIM
KAMLOOPS M.D.
NTS 92I/9E

CLAIM MAP

Draw by:
Scale: 1:50,000
Date: July 1, 1988

To Accompany Report by A.F. Roberts, P.Eng., dated July 1, 1988.

In 1971, regional prospecting by Copper Range Exploration Company Inc., discovered anomalous copper-gold values. They staked 22 claims, MOT 9-30 inclusive.

Their follow-up work consisted of geological mapping, geochemical soil and rock chip analysis.

This work suggested an anomalous area about 300 ft. wide, with a possible east-west strike, open at both ends.

In 1973, a more detailed program indicated a total of three anomalous zones. Further work was recommended, but not carried out due to closure of the Vancouver Office.

The property was re-staked in 1975 by R.A. Dickenson, who carried out a small sampling program.

Vantex Resources Inc. optioned the property and carried out a full program of soil sampling, and VLF-EM surveys, which were successful in outlining good drilling targets. They did not follow-up, and allowed the property to lapse.

GEOLOGY, STRUCTURE: [4] [5]

The GSC MAP OF-980, indicates that the property is underlain by sediments of the Kamloops Group on the northeast side, and Nicola group rocks to the west and southwest, and a Jurassic granitic intrusion to the extreme southwest corner of the property.

Examination of old pits and trenches showed a rock that occurs as varied colour from weathering with amygdules totally white. This is believed to be the altered version

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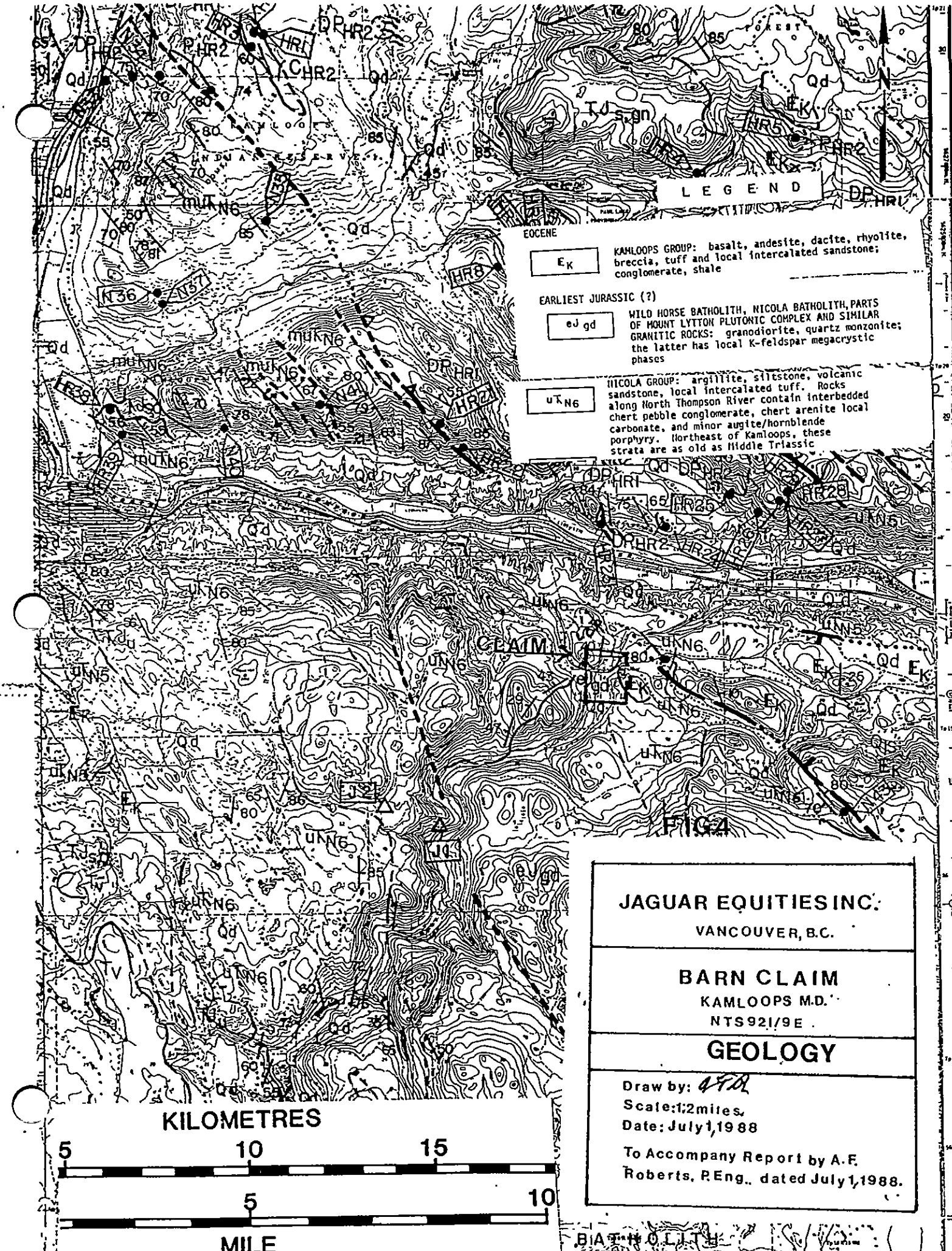
4] Fig. 4, GSC Map OF-980, 1:125,000 [Follows page 2]

5] Fig. 5, Local Geology, after C.P. Purdy, P.Eng., [1" = 1,000'], 1973 [Back Pocket]



JAGUAR EQUITIES INC.
VANCOUVER, B.C.

BARN CLAIM

KAMLOOPS M.D.
NTS 92I/9E

GEOLOGY

Draw by: AFR
Scale: 1:2 miles
Date: July 1, 1988

To Accompany Report by A.F. Roberts, P.Eng., dated July 1, 1988.

of the feldspar porphyry dikes of other reports, also found in the drill holes.

There is one outcrop of biotite feldspar porphyry very definitely, but no unaltered version of feldspar porphyry until the south end of the property is reached.

The most abundant rock is argillite everywhere. There is a magnetic soft rock on the extreme northeast corner of the claim.

One definite outcrop of fault breccia was located on the property northeast of DDH No. 6. This fits with the fault mapped by the GSC.

The whole area of the drilling, regardless of the rock, is brecciated, which shows up in the drill cores.

At the south end of the property, there are outcrops of feldspar porphyry, and biotite feldspar porphyry, limestone, and the intrusive granitic rocks.

Structurally, there is little to be seen other than the breccia previously mentioned, and no attitude was determined for this.

MAGNETOMETER SURVEY: 6] 7]

The geophysical surveys were done over a 25 metre by 25 metre grid.

The instrument used was a Geometrics Model G816 proton magnetometer with a resolution of 1 gamma.

6] Magnetic Survey Map, R.F. Sheldrake, Geophysicist, 1:2,500 [Back Pocket]

7] Geophysical Surveys, Letter Report by R. Sheldrake, Geophysicist, June 12, 1988 [Appendix A]

The field work was carried out by Kenneth Ellerbeck of Kamloops, B.C.

The interpretation was done by Ronald F. Sheldrake, Geophysicist, of Vancouver, B.C., using computerized equipment.

The drill holes completed to date are marked on the map.

The Gamma range over the area surveyed is rather small, 57,480 gammas to 57,200 gammas.

Reference is made to Mr. Sheldrake's letter covering the surveys, rather than the writer attempting an analysis.

However, the following statements may be useful:

1] The interpreted faults strike azimuth 35^{o} - 40^{o}.

2] The structures have a strike of azimuth 120^{o}.

3] The major fault structure indicated in the NW corner roughly coincides with the fault shown on GSC OF-980.

4] The intermediate contours are in the area being drilled - all in sediments, or highly altered dikes, as shown in the drill hole logs.

VLF-EM SURVEY: 8]

This survey was carried out over the same grid as the magnetic survey.

Fig. 8] Map VLF Survey, Total Field, R.F. Sheldrake, Geophysicist, 1988 [Back Pocket]

Map VLF Survey, Dip Angle, R.F. Sheldrake, Geophysicist, 1988 [Back Pocket]

The instrument used was Sabre Electronic Instruments Ltd., Sabre Model 27, using the Seattle Station operating on the frequency of 24.8 KHz.

The readings were taken by Mr. K. Ellerbeck of Kamloops, B.C.

Interpretation was again by Mr. R.F. Sheldrake, whose letter interpretation is enclosed.

The writer is not qualified to attempt an interpretation, although he has used Fraser's reduction of VLF-EM for interpretation on other properties.

It should be noted that -

1] Lineaments can be drawn on the maps that follow closely on those on the magnetic map.

2] The area of current drilling lies in the mid-range of the interpretation.

DIAMOND DRILLING: 9] 10] 11]

The diamond drilling hole locations were originally based on the geochemical and VLF-EM surveys of 1980.

However, the first hole locations were impossible due to topography that would require a major road building program.

9] Appendix "B" Diamond Drilling Logs [Back Pocket]

10] Appendix "C" Assay Certificates [Back Pocket]

11] Fig. 9, Vertical Projection, north, of DD Holes [Follows page 6]

Therefore, the hole locations were adjusted to the topography.

The vertical projections show the major rock types and geochemical gold values above 100 ppb.

Logging the core showed heavy leaching in all holes except #6, and the lower part of #4. The rocks were all brecciated, and fractured. The fractures were -

1] parallel to the core.
2] about 75^{o} to the vertical axis, and
3] 30^{o} to the vertical axis.

The fractures and breccia were healed with quartz, and quartz-carbonate. Mineralization consisted of disseminated crystals of iron pyrite, and extremely fine pyrite in the fractures, which is thought to be the mineralization carrier. The density of these latter fractures apparently varies as the gold values. Other than perhaps silver, no relationship appears to be related to the other mineralization.

At first, it was believed that the gold values would all occur in the altered dike material as it does in Pit #4, with galena, and in Pit #3. However, the occurrence in DDH #1 was entirely in silicified argillite; in DDH #4 - entirely in the altered dike; and in DDH #6 where it appears entirely in a heavily silicified argillite.

Future holes will be guided by the geophysical surveys.

So far there does not appear to be any sure correlation in the geology, or mineralization, from hole to hole.

Drilling has not been easy. Too many days have been lost due to ground problems. Hole #1 was lost at 185 feet, with stuck rods, and lost water. Hole #4 lost water but was able to continue drilling, and never did get water back. Drill Hole #6 was losing core to grinding, soft sandy spots, lost water, etc. Fortunately, the drill sludges were saved from surface to the end of the hole; as for some sections there is only sludge for assays. It is proposed that in future drilling "mud" will be used in place of water, to hopefully give a good core recovery.

Total footage drilled was 1,187 feet or 361.89 metres. Assays for part of DDH #6, are not all reported as they have not arrived in time for this report which is due at the Mining Recorder's Office in a few days.

CONCLUSION:

This property has been shown to contain gold values of economic importance in surface samples. Also, in the few holes drilled there have been values in sections of all holes that are definitely anomalous. Also, in DD Holes #1 and #4 each has had a section with ore values over mineable widths.

RECOMMENDATION:

It is recommended that the Company continue with its drilling program to try and outline sufficient ore to make production practical.

Respectfully submitted,

A.F. Roberts, P.Eng.
July 1, 1988

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
A. F. ROBERTS

C E R T I F I C A T E

I, A.F. Roberts of 8120 Fairbrook Crescent, Richmond, B.C., do hereby certify that:

[1] I am a graduate of the University of British Columbia [B.Ap.Sc.] in Mining Engineering, 1951.

[2] I am registered as a Professional Engineer of the Province of British Columbia, and am a member of The Canadian Institute of Mining and Metallurgy.

[3] I have practiced my profession since 1951 with Quatsino Copper Gold Mines Ltd., Giant Mascot Mines Ltd., Cochenour Willans Gold Mines Ltd., Mogul Mines Ltd., Kerr Addison Gold Mines Ltd., Atlantic Coast Copper Corporation Ltd., Wasamac Mines Ltd., Brenda Mines Ltd., and T. C. Explorations Ltd. Since January of 1970 I have been an independent Consultant.

Previous to, and during University, I worked as a miner underground, and on several exploration-development projects.

[4] The accompanying report is based entirely on my personal analysis of the reports and other data referred to in the text, and on a visit to the property in July 1980, and supervision of the current diamond drilling program.

[5] I have no interest, direct or indirect, in the Jaguar Equities Inc. property, or adjacent properties, nor have I any interest, direct or indirect, in any companies controlled by Jaguar Equities Inc. I have not, nor do I expect to receive any interest in the shares of the Company, in its securities, or in those of any company with which it may become associated.

[6] I consent to the use of this report, in or in connection with, a prospectus, or a statement of material facts relating to the raising of funds for this project.

DATED at Vancouver, British Columbia, this first day of July, 1988.

A.F. Roberts, P. Eng.

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
A. F. ROBERTS

WORK DONE FOR ASSESSMENT
BARN CLAIM, KAMLOOPS M.D.
RECORD NO. 6590
NTS 92 I/9

March 21, 1988 - Receipt No. 142240

The following work was filed and accepted:

Magnetometer, EM Grid		
Baseline 1.35 km @ $250.00/km		$ 337.50
Lines 10 km @ $150.00/km		1,500.00
	Total	1,837.50

April 7, 1988 - Receipt No. 1437105

Balance of Grid work 25 m. stations
25 m. line spacing

Grid 21.5 km at $150.00/km]		
Magnetometer 31.20 km @ $150.00/km]		7,912.50
Diamond Drilling:		
BQ wireline - 540 ft. @ $27.00/ft.		14,580.00
Water Truck, bulldozer		4,578.00
Supervision		7,300.00
Report to date		2,000.00
	Total	$36,370.50

This was applied: $13,200.00 for six years assessment
and $23,170.50 PAC Account

Since then more diamond drilling has been completed with attendant costs for at least an equal amount
$540 ft. @ $27.00 ft. $34,370.00

Plus assaying 241 samples @ $10.00 2,410.00

$36,780.00

Plus support costs

As the Company has no intention of applying these costs against further assessment, they are given only as a matter of record, and are not complete.

A.F. Roberts, P.Eng.

A. F. ROBERTS, P.ENG.
CONSULTING MINING ENGINEER

APPENDIX "A"

LETTER RE GEOPHYSICAL SURVEYS
FROM RONALD F. SHELDRAKE, GEOPHYSICIST

R. F. Sheldrake & Associates Ltd.
Geophysical Consultants

Suite 1500 - 409 Granville Street
Vancouver, British Columbia
Canada V6C 1T2
Telephone (604) 683-3671

Mr. Roy Roberts, Engineer
Jaguar Equities Inc.
Vancouver Hotel
Suite 211-900 W. Georgia Street
Vancouver, B.C.
V6C 2W6

June 12, 1988

Dear Roy,

re: Geophysical Surveys on the Barn Claims

Both magnetic and VLF EM readings were taken on the Barn Claims grid.

The data was collected by Mr. Ken Ellerbeck of Jaguar Equities Ltd. under the supervision of the writer. The writer has not visited the property.

The magnetic readings were taken using a Geometric G816 magnetometer and the VLF EM readings were taken with a Sabre Mk 27 electromagnetometer. Tilt angle and relative field strength (Seattle Tx.) were the specific parameters taken.

Both the magnetic and relative field strength readings were corrected for diurnal variations using the loop method.

Readings were taken on a 25 metre line interval and a 25 metre station interval to establish a non-biased data. The data were displayed as contour maps at appropriate contour intervals.

The North Grid data set (L10600-L10800) is too small to reliably interpret.

I. INTERPRETATION OF THE DATA

MAGNETIC DATA

The magnetometer survey measures the spatial variation of magnetic content in the subsurface rocks. Magnetic maps can indicate variations in rock types, and may also directly locate structures which may contain gold mineralization. For example, a quartz filled fracture zone is most likely to appear as a magnetic low, assuming that it is located in an intermediate (magnetically) volcanic rock.

The structures that one is interested in for gold exploration are normally quite subtle and special effort is made in collecting data to a resolution of a gamma or so. Naturally, both station and line interval must be of the order of the structure one is attempting to map, and because the direction of the structures is never predictable it is necessary to collect orthogonal data, ie line and station intervals are similar.

The data on this survey are compatible with the above specifications and are otherwise satisfactory. The data show no evidence of systematic error or faulty equipment. Maps at 1:2,500 scale using colour contours have been presented. The colour selection and contour intervals have been selected to identify structural features and assist in the interpretation of the data.

The magnetic data have delimited an abundance of features which may help unravel some of the geological complexity of the prospect. Magnetic "features" that strike NNW are probably indicative of varyingly magnetic sequences of volcanic flows. They are offset in several places indicating faulting.

The NW corner of the survey area, in the area of the present drilling, is quiet magnetically compared to the southern portion of the map. The zone where the magnetic character changes may be due to a regional contact zone striking NNE.

REMARK: This discussion is focused primarily on the area around the present drilling (since gold mineralization has been intersected) in an effort to help illuminate the situation there. It is hoped, that for other areas, the data set in the way that it has been presented on the map, speaks for itself.

Also it is noted that there is a relatively subtle lineament striking NW that is in the area of the the present drilling. This could indicate a structural weakness in that direction. The weak gold mineralization that you see in the drilling samples may be associated with this (inferred) feature.

ELECTROMAGNETIC DATA

The electromagnetic data serve to identify electrical discontinuities in the near surface rock (or overburden) materials. These are manifested as gradients in the Tilt Angle EM data. No conductors (ie crossover type responses) are expected in this geological regime, and indeed none are so interpreted.

VLF-EM data are drastically influenced by the direction of the field, so that when selecting a station one is discriminating against features in the orthogonal (secondary) direction. Information may be gained in the secondary direction, but it is gained obliquely.

There are a number of lineaments in the electromagnetic data, but unfortunately there are no significant features in the area of the drilling, other than a subtle disturbance in the relative field strength contours (striking NW). This may be related with the magnetic feature previously mentioned although they do not superimpose directly on one another.

The predominant NNE striking gradients appear to map faults or contacts. These roughly coincide with inferred lineaments from the magnetic data set. They are likely to have little meaning with respect to the supposed gold mineralization. However, they will assist greatly in mapping the area, although they may, in some cases, be caused by variations in the thickness of overburden.

II. CONCLUSIONS

The geophysical data by themselves identify no area that is singularly anomalous. However, they do assist in unravelling some of the geological complexity of the area, and provide guidance in the present drilling program, which otherwise would be purely stochastic.

The presence of gold mineralization (verbal communication, A.F. Roberts, June 1988) in the present drill holes indicates the area has been subjected to the appropriate geological regimes. The task is to establish a sound understanding of the geological nature of the area. Unfortunately the task is made more difficult by the depths involved. The (present) geophysical data sets can help in the task, but the data will have to be correlated closely with the "ground truth" as uncovered by the drilling program itself.

I encourage you to maintain close contact with me as "ground truth" unfolds.

Respectfully submitted,

Ronald F. Sheldrake

Ronald F. Sheldrake
Geophysicist

JAGUAR DATA

COLLECTED MAY 25/88
JUNE 8/88

June 1988.

STN.	LINE	MAG	NULL	VLF-EM F.S.
9750	9000	57325	9	43
9775	9000	57328	8	43
9800	9000	57327	10	45
9825	9000	57368	9	47
9850	9000	57376	10	48
9875	9000	57362	4	54
9900	9000	57336	0	47
9925	9000	57339	-1	47
9950	9000	57348	-1	47
9975	9000	57379	1	50
10000	9000	57352	5	52
10025	9000	57387	6	58
10050	9000	57351	-1	55
10075	9000	57338	0	53
10100	9000	57320	-1	52
10125	9000	57320	0	52
10150	9000	57331	2	52
10175	9000	57332	2	52
10200	9000	57327	2	47
10225	9000	57341	8	47
10250	9000	57366	10	52
10275	9000	57338	3	53
10300	9000	57358	4	52
10325	9000	57400	0	52
10350	9000	57368	-5	50
10375	9000	57447	5	45
10400	9000	57341	0	48
10425	9000	57350	2	47
10450	9000	57378	2	47
10475	9000	57442	3	52
10500	9000	57442	0	47
9750	9025	57353	10	42
9775	9025	57350	8	42
9800	9025	57349	6	42
9825	9025	57345	4	40
9850	9025	57356	9	42
9875	9025	57383	7	51
9900	9025	57327	-3	50
9925	9025	57346	-4	40
9950	9025	57465	0	38
9975	9025	57359	2	40
10000	9025	57353	8	53
10025	9025	57320	0	57
10050	9025	57354	1	58
10075	9025	57361	-3	55
10100	9025	57338	-4	47
10125	9025	57339	-1	52
10150	9025	57334	-1	52
10175	9025	57335	-3	41
10200	9025	57330	0	47
10225	9025	57382	3	47
10250	9025	57339	2	50
10275	9025	57328	1	50
10300	9025	57361	-3	50
10325	9025	57361	0	47

ORIGINAL READINGS REPRODUCED (FROM ORIGINAL FIELD DATA) BY R. SHELDRAKE.

THIS PRINTOUT IS AN EXACT DUPLICATE OF ORIGINAL FIELD DATA, AS COLLECTED BY K. ELLERBECK MAY 25/88 to JUNE 8/88

KEN ELLERBECK
NOV. 23/88

VLF-EM

STN.	LINE	MAG	NULL	F.S
10350	9025	57431	-3	52
10375	9025	57381	-1	45
10400	9025	57355	-3	45
10425	9025	57342	3	45
10450	9025	57364	3	46
10475	9025	57467	5	48
10500	9025	57438	3	50
9750	9050	57716	11	40
9775	9050	57512	10	42
9800	9050	57352	6	45
9825	9050	57288	3	40
9850	9050	57323	12	40
9875	9050	57363	4	47
9900	9050	57330	-4	40
9925	9050	57346	1	39
9950	9050	57365	3	40
9975	9050	57349	7	40
10000	9050	57394	5	42
10025	9050	57356	1	53
10050	9050	57370	0	53
10075	9050	57327	-3	45
10100	9050	57334	3	45
10125	9050	57362	4	50
10150	9050	57384	-3	48
10175	9050	57397	-4	50
10200	9050	57357	-2	45
10225	9050	57380	2	47
10250	9050	57367	1	47
10275	9050	57462	-3	47
10300	9050	57479	-5	50
10325	9050	57348	-3	45
10350	9050	57367	-1	44
10375	9050	57390	-1	45
10400	9050	57366	-1	47
10425	9050	57372	-1	42
10450	9050	57444	2	45
10475	9050	57464	0	42
10500	9050	57359	3	45
10000	9075	57353	9	58
10025	9075	57318	-3	56
10050	9075	57335	-5	52
10075	9075	57322	-3	47
10100	9075	57332	3	47
10125	9075	57335	5	52
10150	9075	57335	1	50
10175	9075	57364	-2	55
10200	9075	57354	0	44
10225	9075	57402	-1	46
10250	9075	57387	-2	47
10275	9075	57393	-3	48
10300	9075	57369	0	44
10325	9075	57502	-5	47
10350	9075	57544	-1	43
10375	9075	57336	-3	44
10400	9075	57381	0	47

VLF-EM

STN.	LINE	MAG.	NULL	FS.
10425	9075	57550	-3	47
10450	9075	57389	-1	42
10475	9075	57355	-4	43
10500	9075	57419	2	40
9750	9100	57206	17	40
9775	9100	57196	17	40
9800	9100	57257	5	43
9825	9100	57302	6	38
9850	9100	57311	9	37
9875	9100	57338	9	40
9900	9100	57342	3	38
9925	9100	57363	3	38
9950	9100	57346	7	38
9975	9100	57345	11	42
10000	9100	57344	5	45
10025	9100	57310	-5	54
10050	9100	57376	-5	49
10075	9100	57348	-3	47
10100	9100	57336	5	47
10125	9100	57342	7	53
10150	9100	57360	1	54
10175	9100	57357	0	52
10200	9100	57370	1	48
10225	9100	57366	-1	48
10250	9100	57333	-1	47
10275	9100	57367	0	46
10300	9100	57437	1	45
10325	9100	57474	5	50
10350	9100	57437	-2	52
10375	9100	57374	-5	45
10400	9100	57407	-5	44
10425	9100	57490	-1	43
10450	9100	57601	-3	42
10475	9100	57328	-2	43
10500	9100	57339	1	41
10000	9125	57327	2	56
10025	9125	57366	-6	52
10050	9125	57337	-1	45
10075	9125	57310	-1	42
10100	9125	57346	7	45
10125	9125	57337	6	53
10150	9125	57355	2	47
10175	9125	57343	-1	50
10200	9125	57365	-3	47
10225	9125	57481	1	44
10250	9125	57479	-1	46
10275	9125	57381	-1	43
10300	9125	57569	2	42
10325	9125	57275	2	43
10350	9125	57393	3	52
10375	9125	57355	6	42
10400	9125	57643	-4	48
10425	9125	57368	-1	43
10450	9125	57368	-2	44
10475	9125	57351	-1	42

VLF-EM

STN.	LINE	MAG.	NULL	F.S.
10500	9125	57336	-7	43
9750	9150	57298	21	40
9775	9150	57269	6	46
9800	9150	57178	6	41
9825	9150	56554	8	39
9850	9150	57334	7	39
9875	9150	57384	7	40
9900	9150	57405	7	40
9925	9150	57390	9	42
9950	9150	57356	11	43
9975	9150	57404	10	53
10000	9150	57418	4	40
10025	9150	57345	-3	37
10050	9150	57346	-3	32
10075	9150	57346	1	30
10100	9150	57333	9	32
10125	9150	57334	4	40
10150	9150	57351	2	37
10175	9150	57420	0	38
10200	9150	57461	1	35
10225	9150	57286	0	33
10250	9150	57424	-1	33
10275	9150	57300	3	34
10300	9150	57327	5	33
10325	9150	57351	-1	37
10350	9150	57361	2	34
10375	9150	57443	-1	33
10400	9150	57400	4	35
10425	9150	57303	1	36
10450	9150	57332	-1	36
10475	9150	57379	-3	36
10500	9150	57380	-7	34
10000	9175	57393	5	53
10025	9175	57365	0	52
10050	9175	57341	-2	45
10075	9175	57355	1	42
10100	9175	57364	9	42
10125	9175	57337	5	52
10150	9175	57340	0	47
10175	9175	57366	1	45
10200	9175	57328	4	43
10225	9175	57390	1	47
10250	9175	57271	-1	40
10275	9175	57341	2	42
10300	9175	57353	3	40
10325	9175	57386	2	50
10350	9175	57394	-2	38
10375	9175	57350	-3	37
10400	9175	57420	2	37
10425	9175	57336	3	35
10450	9175	57355	-3	35
10475	9175	57343	4	34
10500	9175	57390	9	40
9750	9200	57373	20	41
9775	9200	57397	13	45

VLF-EM

STN.	LINE	MAG.	NHLL	F.S.
9800	9200	57303	6	40
9825	9200	57345	7	38
9850	9200	57327	9	40
9875	9200	57333	5	40
9900	9200	57384	9	38
9925	9200	57334	12	37
9950	9200	57339	16	44
9975	9200	57347	7	44
10000	9200	57382	5	53
10025	9200	57370	3	53
10050	9200	57371	-1	50
10075	9200	57350	-2	41
10100	9200	57328	9	43
10125	9200	57319	5	45
10150	9200	57373	-1	45
10175	9200	57329	-3	40
10200	9200	57389	3	40
10225	9200	57363	6	47
10250	9200	57439	-3	40
10275	9200	57394	-3	38
10300	9200	57366	1	36
10325	9200	57368	5	37
10350	9200	57482	3	45
10375	9200	57481	-9	40
10400	9200	57385	-5	33
10425	9200	57336	0	34
10450	9200	57394	3	37
10475	9200	57427	-3	37
10500	9200	57310	3	34
10000	9225	57364	8	44
10025	9225	57461	2	45
10050	9225	57399	-1	45
10075	9225	57350	-1	38
10100	9225	57339	9	38
10125	9225	57391	3	42
10150	9225	57595	-1	42
10175	9225	57350	-1	40
10200	9225	57323	-1	37
10225	9225	57318	1	35
10250	9225	57352	1	38
10275	9225	57390	-1	38
10300	9225	57379	-5	35
10325	9225	57401	0	34
10350	9225	57466	4	35
10375	9225	57544	5	47
10400	9225	57353	-6	38
10425	9225	57354	-2	34
10450	9225	57390	0	34
10475	9225	57343	3	40
10500	9225	57354	-3	34
9750	9250	57383	15	35
9775	9250	57284	10	35
9800	9250	57248	10	35
9825	9250	57440	14	34
9850	9250	57440	17	40

VLF-EM

STN	LINE	MAG	NULL	FIL
9875	9250	57395	14	44
9900	9250	57341	8	42
9925	9250	57319	7	43
9950	9250	57324	8	43
9975	9250	57361	8	40
10000	9250	57369	9	44
10025	9250	57600	5	47
10050	9250	57282	4	48
10075	9250	57341	0	42
10100	9250	57333	3	42
10125	9250	57367	5	47
10150	9250	57345	2	43
10175	9250	57342	-3	43
10200	9250	57315	-1	40
10225	9250	57351	3	39
10250	9250	57391	-3	44
10275	9250	57374	-1	38
10300	9250	57451	5	48
10325	9250	57568	-3	40
10350	9250	57510	1	39
10375	9250	57314	6	45
10400	9250	57334	5	43
10425	9250	57287	0	37
10450	9250	57388	0	40
10475	9250	57379	0	44
10500	9250	57321	-5	36
10000	9275	57304	10	44
10025	9275	57310	7	50
10050	9275	57313	7	50
10075	9275	57345	0	44
10100	9275	57359	1	45
10125	9275	57339	5	48
10150	9275	57338	2	47
10175	9275	57363	-4	50
10200	9275	57348	-3	40
10225	9275	57391	0	42
10250	9275	57404	1	47
10275	9275	57415	-1	37
10300	9275	57478	1	45
10325	9275	57452	1	48
10350	9275	57327	1	38
10375	9275	57342	4	42
10400	9275	57334	0	39
10425	9275	57369	-5	47
10450	9275	57356	-3	42
10475	9275	57362	1	40
10500	9275	57389	1	40
9750	9300	57320	14	31
9775	9300	57419	13	33
9800	9300	57432	14	34
9825	9300	57271	19	34
9850	9300	57275	23	38
9875	9300	57279	22	42
9900	9300	57312	18	42
9925	9300	57357	10	48

STN	LINE	MAG.	VLF-EM NULL	VLF-EM F.S
9950	9300	57313	9	44
9975	9300	57322	7	44
10000	9300	57327	10	39
10025	9300	57316	8	47
10050	9300	57338	8	49
10075	9300	57366	0	45
10100	9300	57418	4	45
10125	9300	57361	0	46
10150	9300	57401	3	45
10175	9300	57394	0	49
10200	9300	57392	-4	39
10225	9300	57471	-2	39
10250	9300	57589	-1	38
10275	9300	57300	2	38
10300	9300	57369	3	48
10325	9300	57322	-1	40
10350	9300	57306	-5	38
10375	9300	57308	-2	40
10400	9300	57331	3	39
10425	9300	57340	2	42
10450	9300	57391	-2	44
10475	9300	57428	-5	40
10500	9300	57363	-3	38
10000	9325	57292	8	49
10025	9325	57336	6	53
10050	9325	57336	7	55
10075	9325	57353	0	50
10100	9325	57391	7	50
10125	9325	57397	4	59
10150	9325	57370	1	54
10175	9325	57413	-3	57
10200	9325	57561	-3	48
10225	9325	57475	-5	43
10250	9325	57320	-1	48
10275	9325	57383	0	44
10300	9325	57485	4	50
10325	9325	57298	-1	39
10350	9325	57345	-1	44
10375	9325	57339	-3	42
10400	9325	57358	4	48
10425	9325	57348	2	40
10450	9325	57374	-1	40
10475	9325	57392	-3	39
10500	9325	57372	-5	38
9750	9350	57251	7	25
9775	9350	57248	16	28
9800	9350	57294	17	29
9825	9350	57275	22	30
9850	9350	57322	23	35
9875	9350	57323	21	40
9900	9350	57288	17	49
9925	9350	57278	13	47
9950	9350	57301	7	45
9975	9350	57312	7	40
10000	9350	57306	8	49

VLF-EM

STN.	LINE	MAG.	NULL	F.S.
10025	9350	57366	7	54
10050	9350	57338	10	54
10075	9350	57356	0	49
10100	9350	57399	6	49
10125	9350	57398	6	59
10150	9350	57373	5	55
10175	9350	57415	-2	57
10200	9350	57564	-4	49
10225	9350	57472	-3	45
10250	9350	57324	-2	45
10275	9350	57388	1	44
10300	9350	57492	-4	45
10325	9350	57299	1	44
10350	9350	57388	-3	50
10375	9350	57347	-1	45
10400	9350	57398	0	54
10425	9350	57374	3	47
10450	9350	57416	1	50
10475	9350	57370	-4	42
10500	9350	57385	-3	39
10000	9375	57340	9	44
10025	9375	57342	3	45
10050	9375	57324	8	46
10075	9375	57368	-1	46
10100	9375	57366	5	45
10125	9375	57364	7	50
10150	9375	57375	4	50
10175	9375	57631	-3	50
10200	9375	57336	-3	45
10225	9375	57352	-4	44
10250	9375	57324	-1	39
10275	9375	57353	0	43
10300	9375	57345	-2	42
10325	9375	57385	-1	40
10350	9375	57331	0	42
10375	9375	57353	0	42
10400	9375	57370	2	42
10425	9375	57405	-4	44
10450	9375	57433	-4	44
10475	9375	57471	1	44
10500	9375	57453	-4	40
9750	9400	57339	3	29
9775	9400	57240	9	24
9800	9400	57267	15	24
9825	9400	57297	22	26
9850	9400	57283	19	30
9875	9400	57311	18	36
9900	9400	57316	20	39
9925	9400	57327	15	45
9950	9400	57319	11	44
9975	9400	57318	7	44
10000	9400	57297	7	47
10025	9400	57362	2	45
10050	9400	57327	8	44
10075	9400	57325	3	46

VLF-EM

STN.	LINE	MAG.	NULL	FS.
10100	9400	57344	8	42
10125	9400	57385	9	52
10150	9400	57391	2	47
10175	9400	57484	3	49
10200	9400	57341	-1	48
10225	9400	57350	-2	44
10250	9400	57344	-4	39
10275	9400	57365	0	42
10300	9400	57410	-5	39
10325	9400	57401	2	40
10350	9400	57393	-3	42
10375	9400	57398	4	45
10400	9400	57451	-3	47
10425	9400	57411	3	42
10450	9400	57400	-4	45
10475	9400	57374	-2	40
10500	9400	57386	-1	40
10000	9425	57335	8	47
10025	9425	57360	1	45
10050	9425	57355	6	46
10075	9425	57344	1	42
10100	9425	57428	7	44
10125	9425	57379	7	55
10150	9425	57450	2	48
10175	9425	57321	0	45
10200	9425	57319	-3	48
10225	9425	57344	-4	44
10250	9425	57351	0	39
10275	9425	57403	-3	40
10300	9425	57375	-5	39
10325	9425	57354	1	39
10350	9425	57404	1	49
10375	9425	57433	-4	42
10400	9425	57437	2	42
10425	9425	57418	4	42
10450	9425	57390	4	39
10475	9425	57301	-3	42
10500	9425	57407	-1	39
9750	9450	57397	4	30
9775	9450	57255	5	22
9800	9450	57324	15	23
9825	9450	57400	19	25
9850	9450	57281	23	30
9875	9450	57300	20	33
9900	9450	57583	17	42
9925	9450	57307	15	45
9950	9450	57317	11	45
9975	9450	57331	10	44
10000	9450	57300	9	49
10025	9450	57320	7	48
10050	9450	57340	3	48
10075	9450	57326	7	44
10100	9450	57335	7	44
10125	9450	57344	8	46
10150	9450	57359	4	54

10175	9450	57332	-3	45
10200	9450	57337	-1	47
10225	9450	57348	-4	42
10250	9450	57388	1	42
10275	9450	57394	-1	45
10300	9450	57379	-3	39
10325	9450	57402	7	40
10350	9450	57369	-2	39
10375	9450	57388	5	44
10400	9450	57405	-5	38
10425	9450	57401	-4	35
10450	9450	57442	3	42
10475	9450	57452	-3	40
10500	9450	57456	-3	39
10000	9475	57328	11	45
10025	9475	57348	2	45
10050	9475	57325	5	41
10075	9475	57364	5	40
10100	9475	57349	5	40
10125	9475	57329	3	45
10150	9475	57386	3	54
10175	9475	57343	1	42
10200	9475	57324	-1	42
10225	9475	57374	2	44
10250	9475	57401	0	40
10275	9475	57393	-5	40
10300	9475	57374	-2	35
10325	9475	57391	-1	42
10350	9475	57433	-1	40
10375	9475	57405	0	40
10400	9475	57433	-7	39
10425	9475	57446	-3	34
10450	9475	57545	-5	40
10475	9475	57588	-4	37
10500	9475	57674	-1	42
9750	9500	57406	9	29
9775	9500	57373	8	30
9800	9500	57389	10	28
9825	9500	57366	14	25
9850	9500	57470	17	28
9875	9500	57505	19	33
9900	9500	57376	18	35
9925	9500	57314	17	42
9950	9500	57324	9	44
9975	9500	57296	13	44
10000	9500	57287	11	45
10025	9500	57353	2	49
10050	9500	57303	5	39
10075	9500	57361	5	40
10100	9500	57340	6	40
10125	9500	57358	7	40
10150	9500	57347	7	49
10175	9500	57340	-4	42
10200	9500	57360	-3	39
10225	9500	57373	-1	42

10250	9500	57381	-5	38
10275	9500	57401	-2	34
10300	9500	57343	-11	34
10325	9500	57369	-4	37
10350	9500	57468	0	43
10375	9500	57422	-1	40
10400	9500	57509	-7	39
10425	9500	57655	-7	37
10450	9500	57570	-3	34
10475	9500	57444	3	39
10500	9500	57475	-3	39
10000	9525	57298	12	48
10025	9525	57290	7	50
10050	9525	57308	3	45
10075	9525	57365	2	42
10100	9525	57331	4	40
10125	9525	57343	7	40
10150	9525	57346	5	43
10175	9525	57411	3	45
10200	9525	57378	1	44
10225	9525	57388	4	42
10250	9525	57390	-4	43
10275	9525	57405	-6	40
10300	9525	57385	-2	34
10325	9525	57388	-9	35
10350	9525	57426	-1	36
10375	9525	57469	-5	40
10400	9525	57793	-4	37
10425	9525	57389	-3	33
10450	9525	57382	-3	34
10475	9525	57398	3	33
10500	9525	57429	-4	42
10000	9550	57311	13	42
10025	9550	57313	7	42
10050	9550	57322	3	40
10075	9550	57326	6	39
10100	9550	57372	1	36
10125	9550	57350	2	35
10150	9550	57338	3	36
10175	9550	57358	4	35
10200	9550	57419	3	40
10225	9550	57382	2	35
10250	9550	57391	3	42
10275	9550	57374	-3	35
10300	9550	57393	-3	35
10325	9550	57380	-1	34
10350	9550	57417	-3	33
10375	9550	57439	-10	33
10400	9550	57362	-7	30
10425	9550	57470	-6	32
10450	9550	57420	-3	30
10475	9550	57468	4	30
10500	9550	57472	2	40
10000	9575	57311	13	35
10025	9575	57357	12	42

10050	9575	57359	2	35
10075	9575	57355	1	35
10100	9575	57347	-2	30
10125	9575	57401	0	30
10150	9575	57366	2	27
10175	9575	57361	5	27
10200	9575	57405	1	36
10225	9575	57344	4	25
10250	9575	57369	-3	35
10275	9575	57399	-4	30
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10325	9575	57535	1	35
10350	9575	57436	-4	35
10375	9575	57485	-7	32
10400	9575	57417	0	35
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10450	9575	57546	-2	30
10475	9575	57586	-3	33
10500	9575	57438	-3	33
10000	9600	57322	13	37
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10050	9600	57413	3	40
10075	9600	57330	3	37
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10125	9600	57354	-2	35
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10175	9600	57373	5	31
10200	9600	57458	3	42
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10300	9600	57433	1	34
10325	9600	57489	1	34
10350	9600	57479	-1	40
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10475	9600	57435	0	32
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10075	9625	57337	6	40
10100	9625	57386	5	50
10125	9625	57398	-7	45
10150	9625	57370	-4	32
10175	9625	57377	-3	30
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10300	9625	57388	1	35
10325	9625	57361	4	38
10350	9625	57418	4	37

10375	9625	57409	-1	36
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10425	9625	57382	-1	34
10450	9625	57385	-5	35
10475	9625	57387	9	35
10500	9625	57411	-5	35
10000	9650	57389	13	40
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10050	9650	57342	8	47
10075	9650	57372	5	40
10100	9650	57396	13	45
10125	9650	57395	-3	50
10150	9650	57398	-3	35
10175	9650	57409	0	37
10200	9650	57341	-1	34
10225	9650	57339	2	40
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10275	9650	57335	5	40
10300	9650	57461	-1	38
10325	9650	57350	1	37
10350	9650	57384	-1	40
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10400	9650	57380	-3	40
10425	9650	57372	0	35
10450	9650	57342	-6	30
10475	9650	57389	4	30
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10000	9675	57312	12	39
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10050	9675	57345	7	40
10075	9675	57420	6	40
10100	9675	57531	5	42
10125	9675	57546	-3	38
10150	9675	57348	3	37
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10200	9675	57391	1	40
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10325	9675	57437	-1	37
10350	9675	57423	2	40
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10400	9675	57393	-1	40
10425	9675	57360	-6	39
10450	9675	57422	-3	32
10475	9675	57395	3	32
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9900	9700	57267	8	30
9925	9700	57302	11	29
9950	9700	57308	11	35
9975	9700	57311	9	33
10000	9700	57414	12	40

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10075	9700	57696	3	41
10100	9700	57399	-2	40
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10150	9700	57345	2	35
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10325	9700	57363	3	35
10350	9700	57351	3	40
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10400	9700	57397	1	40
10425	9700	57358	-1	38
10450	9700	57395	-7	35
10475	9700	57384	1	32
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10025	9725	57426	3	48
10050	9725	57434	1	43
10075	9725	57414	3	50
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10150	9725	57403	4	42
10175	9725	57387	1	36
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10325	9775	57351	2	37
10350	9775	57395	6	42
10375	9775	57366	8	44
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10450	9800	57392	-5	50
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10350	9825	57384	7	44
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10450	9825	57381	-6	50
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10150	9875	57413	8	45
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10275	9875	57375	-3	45
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10425	9950	57823	-3	44
10450	9950	57528	-6	35
10475	9950	57679	-7	34
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10150	10000	57308	3	30
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10325	10000	58044	-3	35
10350	10000	57775	3	34
10375	10000	57848	5	39
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10425	10000	58119	0	47
10450	10000	57131	-13	37
10475	10000	57593	-14	34
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10000	10025	57320	8	40
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10075	10025	57307	2	35
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10150	10025	57296	3	35
10175	10025	57298	5	34
10200	10025	57318	7	34
10225	10025	57410	10	38
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10275	10025	57810	4	44
10300	10025	57245	6	44
10325	10025	58042	1	46
10350	10025	57802	0	39
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10400	10025	58240	1	46
10425	10025	57924	-10	46
10450	10025	57402	-15	35
10475	10025	57672	-17	30
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10000	10050	57331	9	35
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10225	10050	57665	9	35
10250	10050	57849	7	39
10275	10050	57899	7	37
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10325	10050	57856	5	40
10350	10050	57962	5	37
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10400	10050	58243	-6	45
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10475	10050	57545	-11	30
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10000	10075	57325	10	34
10025	10075	57321	10	36
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10075	10075	57315	8	34
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10125	10075	57308	10	34
10150	10075	57316	7	34
10175	10075	57360	10	33
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10225	10075	57527	9	35
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10125	10100	57278	11	30
10150	10100	57276	12	34
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	SLN.	LINE	MAG.	VLF-EM RULL	F.S.
	10200	10100	57454	13	33
	10225	10100	57441	14	39
	10250	10100	57443	7	40
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	10300	10100	57408	12	36
	10325	10100	57403	8	40
	10350	10100	57724	6	46
	10375	10100	57641	2	39
	10400	10100	57583	-1	43
	10425	10100	57525	-9	39
	10450	10100	56974	-4	38
	10475	10100	57067	-9	34
	10500	10100	57192	-9	34
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	10050	10150	57323	8	35
	10075	10150	57311	7	32
	10100	10150	57316	9	29
	10125	10150	57265	11	29
	10150	10150	57258	17	30
	10175	10150	57248	18	32
	10200	10150	57320	20	38
	10225	10150	57345	14	39
	10250	10150	57259	13	40
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	10350	10150	57348	4	39
	10375	10150	57262	1	41
	10400	10150	57363	-3	40
	10425	10150	57211	0	37
	10450	10150	57443	3	39
	10475	10150	57191	-2	35
NORTH GRID →	10500	10150	57276	-3	35
	9300	10600	57321	-9	34
	9325	10600	57321	-8	34
	9350	10600	57322	-9	33
	9375	10600	57302	-8	33
	9400	10600	57329	-9	32
	9425	10600	57288	-9	32
	9450	10600	57302	-9	30
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	9500	10600	57300	-7	33
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	9625	10600	57310	-16	35
	9650	10600	57306	-19	26
	9675	10600	57284	-23	25
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	9750	10600	57277	-17	24
	9775	10600	57284	-15	24
	9300	10625	57331	-7	34

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9375	10625	57330	-9	34
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9375	10650	57324	-8	35
9400	10650	57310	-10	34
9425	10650	57309	-9	34
9450	10650	57296	-10	32
9475	10650	57315	-11	32
9500	10650	57305	-9	30
9525	10650	57273	-9	32
9550	10650	57280	-7	32
9575	10650	57283	-7	32
9600	10650	57292	-7	35
9625	10650	57334	-10	38
9650	10650	57615	-15	35
9675	10650	57252	-18	25
9700	10650	57280	-17	25
9725	10650	57291	-16	24
9750	10650	57284	-19	23
9775	10650	57290	-17	22
9300	10675	57303	-6	38
9325	10675	57318	-5	35
9350	10675	57337	-5	32
9375	10675	57302	-5	32
9400	10675	57320	-7	32
9425	10675	57314	-7	32
9450	10675	57299	-9	30
9475	10675	57299	-10	29
9500	10675	57288	-7	28
9525	10675	57318	-9	26
9550	10675	57272	-7	30
9575	10675	57283	-7	30
9600	10675	57296	-8	30
9625	10675	57293	-9	32
9650	10675	57268	-8	30
9675	10675	57243	-17	30

VLF-EM

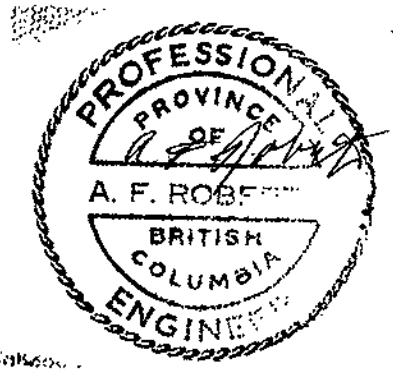
STN.	LINE	MAG.	NULL	F.S
9700	10675	57266	-15	24
9725	10675	57299	-16	25
9750	10675	57291	-16	25
9775	10675	57287	-14	24
9300	10700	57317	-2	34
9325	10700	57254	-9	34
9350	10700	57308	-3	34
9375	10700	57307	-5	32
9400	10700	57328	-7	36
9425	10700	57311	-7	34
9450	10700	57323	-10	32
9475	10700	57263	-8	30
9500	10700	57280	-7	30
9525	10700	57299	-7	29
9550	10700	57271	-5	32
9575	10700	57258	-7	30
9600	10700	57168	-9	30
9625	10700	57230	-10	30
9650	10700	57224	-10	30
9675	10700	57244	-16	30
9700	10700	57264	-15	28
9725	10700	57210	-11	25
9750	10700	57309	-17	22
9775	10700	57272	-15	22
9300	10725	57349	0	34
9325	10725	57284	1	34
9350	10725	57283	-1	38
9375	10725	57325	-3	34
9400	10725	57330	-3	34
9425	10725	57383	-5	34
9450	10725	57351	-10	32
9475	10725	57322	-9	30
9500	10725	57300	-7	30
9525	10725	57390	-6	30
9550	10725	57334	-7	30
9575	10725	57304	-7	34
9600	10725	57312	-5	33
9625	10725	57537	-10	34
9650	10725	57347	-11	30
9675	10725	57317	-15	30
9700	10725	57446	-17	25
9725	10725	57313	-11	26
9750	10725	57245	-15	24
9775	10725	57284	-14	22
9300	10750	57357	1	34
9325	10750	57362	0	33
9350	10750	57330	0	34
9375	10750	57313	-1	34
9400	10750	57306	0	34
9425	10750	57276	-5	37
9450	10750	57335	-5	34
9475	10750	57320	-4	30
9500	10750	57294	-6	30
9525	10750	57293	-3	29
9550	10750	57312	-3	33

VLF-EM

STN.	LINE	MAG.	NULL	F.S
9575	10750	57302	-1	34
9600	10750	57292	-3	39
9625	10750	57276	-6	40
9650	10750	57194	-17	30
9675	10750	57275	-17	28
9700	10750	57295	-12	30
9725	10750	57267	-11	29
9750	10750	57315	-11	29
9775	10750	57363	-9	32
9300	10775	57233	3	40
9325	10775	57275	3	39
9350	10775	57270	3	39
9375	10775	57288	3	39
9400	10775	57292	2	36
9425	10775	57335	-3	39
9450	10775	57358	-3	38
9475	10775	57260	-7	35
9500	10775	57894	-9	32
9525	10775	57275	-4	32
9550	10775	57270	0	32
9575	10775	57360	1	34
9600	10775	57403	2	46
9625	10775	57349	-11	47
9650	10775	57249	-23	30
9675	10775	57251	-16	29
9700	10775	57299	-12	30
9725	10775	57280	-10	28
9750	10775	57362	-9	30
9775	10775	57354	-9	31

APPENDIX "B"

DIAMOND DRILL LOGS



DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 85 E m
DEP. 10,000 + ON m
ELEVATION 2,150' 655.49 metres
AZIMUTH -80° Westerly

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM Core Storage
HOLE NO. DDH JAG 1/88 From Loops
COMMENCED March 15/88 1854 Breakenridge
FINISHED March 21/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE Meters	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO	FROM	TO	WIDTH	ASSAY	WIDTH X ASSAY	SAMPLE NO.	FROM	TO	ASSAY
0 - 13 @3.96M	Casing				1.37m		Au	Ag	Cu	Pb	Zn
13 - 15 -4.56	Limestone, Broken soft, limonite veinlets qtz-carb.	751	15	19.5	4.5	-	ppb	ppm	ppm	ppm	ppm
Recovery 80%	1/16" - ¼", vuggy after pyrite (?)						9	.6	63	21	74
	Irregularly soft and hard Breccia										
15 - 19.5 -5.95		752	19.5	22	0.76M 2.5		1	.1	44	7	100
Recovery 90%	Limestone Hematite stained throughout. Veinlets - hairline										
	to ⅛". No visible pyrite, pyrite vugs.										
19.5 - 22 -6.70											
Recovery 95%	Limonite stained, black quartz veinlets, carbonate. This	753	22	25	0.9 3		107	.6	81	21	76
	core is a breccia feldspar after porphyry was altered.										
	The many veinlets which do not cut the core healing the	754	25	-32	2.13 7		16	.6	90	9	70
	fractures - discontinuous										
22 - 27 -8.27											
Recovery 95%	The colour of the core changing to grey, otherwise as a bore	755	32	38	1.8 6		1	.2	57	7	101
	(altered feldspar porphyry dyke)	756	38	41	0.90 3		6	.4	103	6	125
27 - 32 -9.75	Grey no oxidation. The veinlets and quartz-carbonate	757	41	46	1.52 5		3	.1	28	81	114
Rec. 80%	patches continue	758	46	51	1.52 5		7	.4	67	2	76
32 - 38 -11.6	Core colour changed from grey to yellow, then reddish.										
Recovery 85%	Still veinlets. No visible mineralization.										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 85 E
DEP. 10,000 + ON
ELEVATION 2,150'
AZIMUTH -80° Westerly

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. DDH JAG 1/88
COMMENCED March 15/88
FINISHED March 21/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE M.	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH M.	ASSAY ~~Au~~/ppb	WIDTH X ASSAY ~~Au~~/ppb Ag	SAMPLE NO. Cu/ppm Ag	FROM ~~Cu~~/ppm	TO ~~Pb~~/ppm	ASSAY Zn
38 – 41 12.5	Much the same as previous										
Rec. 100%	Quartz-carbonate veins continuing										
41 – 46 14.0	At 41.5 Gouge for 4" with rock buttons										
Rec. 100%	Generally greyish with the quartz-carbonate veinlets										
46 – 51 15.5	As previous except occasional rare pyrite. Some leaching										
Rec. 100%	on the fractures.										
51 – 56 17.0	Same rock – more broken – more limonite staining all	759	51	56	1.52 5		3	.5	114	3	94
Rec. 90%	through. Some leaching.										
56 – 60 18.0	As above but 58-60 very broken and leached in the										
Rec. 90%	last foot.										
60 – 65 19.52	Same as above. Fairly well oxidized.	760	56	60	1.23 4		1	.6	54	9	114
Rec. 90%	Much more pyrite vugs. Some parts are nearly "knife hard".	761	60	65	1.52 5		1	.2	67	4	99
65 – 70 21.34	Mostly badly broken										
Rec. 80%	Heavy limonite	762	65	70	1.52 5		6	.5	114	4	98
76 – 75 22.9	Broken, oxidized, leached	763	70	75	1.52 5		1	.3	48	3	108
Rec. 90%											
75 – 80 24.3	As previous	764	75	80	1.52 5		5	.5	118	3	104
Rec. 80-65%											

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 85 E
DEP. 10,000 + ON
ELEVATION 2,150'
AZIMUTH -80° westerly

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. DDH JAG 1/88
COMMENCED March 15/88
FINISHED March 21/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH	ASSAY Au/ppb	WIDTH X ASSAY Ag/ppm	SAMPLE NO. Cu/ppm	FROM Pb/ppm	TO Zn/ppm	ASSAY
80 - 85 - 25.9 M	Black - some hard sections. Argillaceous										
Rec. 80%	breccia partly silicified	765	80	85	1.52 5	3	.5	76	8	112	
85 - 90 27.4	Mostly argillaceous breccia	766	85	90	1.52 5	3	.4	62	7	88	
Rec. 90%	NOTE: For all core. Fracture banding almost parallel										
	to core and at 30° and 60° fractures generally are										
	healed by quartz-carbonate filling from hairline up.										
90 - 95 28.96	As above, a little more broken	767	90	95	1.52 5	2	.4	87	6	105	
Rec. 95%	Well fractured and broken. Altered feldspar porphyry										
95 - 100 30.49	As above, badly broken for one foot, then argillite breccia.	768	95	100	1.52 5	1	.5	62	7	111	
Rec. 95%	Last foot is massive, grey coloured, sandy appearance.										
100 - 105 32.0	Argillaceous - broken	769	100	110	3.05 10	2	.6	71	7	75	
Rec. 80%											
105 - 110 33.54	Very badly broken										
Rec. 60%	Argillite fragments										
110 - 115 ~~33.53~~ 35.66	Argillaceous, badly broken, limonite veining and	770	110	115	1.52 5	10	.7	64	11	76	
Rec. 80%	Veining and hairline fracturing continues										
115 - 120 ~~35.58~~ 37.18	As above. Broken argillite	772	115	120	1.52 5	1	.4	46	15	64	
Rec. 90%											

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 85 E
DEP. 10,000 + ON
ELEVATION 2,150'
AZIMUTH -80° westerly

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. DDH JAG 1/88
COMMENCED March 15/88
FINISHED March 21/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH	ASSAY Au/ppb	WIDTH X ASSAY Ag/ppm	SAMPLE NO. Cu/ppm	FROM Pb/ppm	TO Zn/ppm	ASSAY
120 - 125 - 38,1 m.	As above. Broken Argillite	773	120	125	1.52 (5')	5	.6	44	10	75	
Rec. 90%											
125 - 130 - 39,63	Argillite breccia - completely broken	774	125	130	1.52	7	.6	72	11	107	
85% Recovery											
130 - 135 41,15	Argillite. Handful of buckshot sized pieces	775	130	135	1.52	.11	.8	77	12	129	
75%	Breccia fractures still sealed with quartz-carbonate.	776	135	140	1.52	78	1.2	61	23	187	
	Occasional patches of quartz	777	140	145	1.52	8640	4.4	82	56	222	
135 - 160 48.78	As above										
Rec. poor											
75% ?											
160 - 170 51,82	Altered feldspar porphyry amygdules kaolinized	779	150	155	1.52	8	.7	53	12	999	
	squarish shape (after pyrite ?)	780	155	160	1.52	.23	.8	61	10	95	
	Argillite at 169'	781	160	165	1.52	174	.7	15	5	120	
170 - 185 56,4	All argillite breccia, badly broken	782	165	170	1.52	15	.7	88	8	99	
	sections of core completely washed	783	170	175	1.52	7	1.0	76	14	219	
	out. Some pyrite casts are quartz filled	784	175	180	1.52	9	1.1	61	11	127	
		785	180	185	1.52	14	1.0	88	13	161	
	END OF HOLE										

DIAMOND DRILL LOG

COLLAR:—

LAT. 99 + 85 E

DEP. 10,000 + ON

ELEVATION 2,150'

AZIMUTH -80° westerly

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM

HOLE NO. DDH JAG 1/88

COMMENCED March 15/88

FINISHED March 21/88

PURPOSE OF HOLE Test Mineralization

LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH	ASSAY	WIDTH X ASSAY	SAMPLE NO.	FROM	TO	ASSAY
	At 185 lost water. Rods stuck. Spent two days trying to recover them.										
	Lost: Rods 60 ft. of BX wire line										
	1 - 10 ft. core barrel										
	1 - diamond bit										
	NOTE: After splitting, it was noted that there was more quartz than observed on the raw core. Veinlets around breccia fragments are quartz-carbonate filled.										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N m
DEP. 99 + 57 E m
ELEVATION 2120' 646.34 metres
AZIMUTH -55° N 30° W
Core stored at 1834 Breakenridge Court, Kamloops

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY: BARN CLAIM
HOLE NO.: DDH JAG 2/88
COMMENCED: March 24, 1988
FINISHED: March 29, 1988
PURPOSE OF HOLE: Test for mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
M											
0 – 15 4.57	Casing										
15 – 20 6.10	All altered feldspar prophyry, broken, brecciated	786	15	20	1.52 5		6	.6	48	10	38
	Heavy limonite. No apparent mineralization.										
20 – 25 7.62	As above – some pyrite casts	787	20	25	1.52 5		340	1.3	91	173	44
25 – 30 8.14	As above. All the core in the box is spotted with tiny	788	25	30	1.52 5		37	.5	54	7	44
	white carbonate spots that are nearly square, kaolinized	789	30	32	0.60 2		31	.5	50	6	87
	altered amygdules ?										
30 – 35 10.16	Change of rock. Probably silicified	790	32	35	0.90 3		15	.3	63	8	31
30 – 32 9.76	Pyrite plentiful in 1/16" veinlets, plus possible galena.										
	small spots of very fine pyrite, considerable quartz.										
	Silicified brecciated argellite. Reverted to altered										
	feldspar porphyry breccia, some quartz, leaching										
35 – 40 12.20	Brecciated. Pyrite casts, heavy oxidation	791	35	40	1.52 5		18	.6	48	9	46
	Altered feldspar porphyry										
40 – 45 13.72	As above. Very fine pyrite bordering the quartz veinlets	792	40	45	1.52 5		8	.5	70	6	36
45 – 50 15.24	As above	793	45	50	1.52 5		21	.4	106	7	42
50 – 55 16.76	As above. Note that attitude of quartz veinlets parallels	794	50	55	1.52 5		1	.3	103	6	64
	the core fracturing @ 90°, 30° , 60°.										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120
AZIMUTH -55° N 30° W

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY: BARN CLAIM
HOLE NO.: DDH JAG 2/88
COMMENCED: March 24, 1988
FINISHED: March 29, 1988
PURPOSE OF HOLE: Test for mineralization
LOGGED BY: A.F. Roberts

FOOTAGE (M)	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH (M)	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
55 - 60 18.0	Continuing in breccia, heavily oxidized, pyrite casts, some quartz veinlets	795	55	60	5 (1.52)		9	.4	119	5	70
60 - 64 19.2	As previous										
64 - 70 21.34	At 64, brecciated silicified argillite	796	60	64	4 (1.20)		35	.4	50	9	56
Recov. 90%	Hard. Possible extremely fine pyrite associated with quartz veinlets	797	64	70	6 (1.80)		41	.8	75	10	60
70 - 75 22.86	Few inches of brown tuff - soft. Then hard argillite.	798	70	75	5 (1.52)		19	.9	33	5	58
Recov. 90%	Brecciation not too definite. Some fine pyrite										
75 - 80 24.30	18" silicified argillite. Balance is silicified, altered	799	75	77	2 (6.60)	X	720	1.3	38	41	68
Rec. 95%	feldspar porphyry. Hard, brecciation concealed. No	800	77	78	1 (0.30)		63	.6	36	8	39
	core leaching. Some extremely fine pyrite in frac-	742	78	80	2 (0.60)		34	.3	44	5	38
	tures. Some pyrite casts										
80 - 85 25.82	Same as above to end of hole. The rock is altered feldspar	743	80	80	5 (1.52)		15	.3	52	6	46
95%	porphyry that is silicified to the appearance of a massive	744	85	90	5 (1.52)		1	.4	42	5	52
	rock. Far more patches of pyrite and fracture filling.										
	This pyrite is extremely fine and hard to see										
85 - 90 27.34	As previous - silicified and then brecciated and healed by	745	90	95	5 (1.52)		41	.6	63	15	64
Recov. 95%	the silica.. Argillite has been added and appears in small	746	95	100	5 (1.52)		8	.7	82	7	79
	sections, and smeared through the altered porphyry	747	100	105	5 (1.52)		36	.3	31	12	38

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120
AZIMUTH -55° N 30° W

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. DDH JAG 2/88
COMMENCED March 24, 1988
FINISHED March 29, 1988
PURPOSE OF HOLE Test for mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
M.		SAMPLE NO.	FROM	TO	WIDTH	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
32.62					1.52						
90 - 107	Core is solid to 107 as in previous sample - silicified	748	105	111	5		58	.1	25	5	33
Recov. 95%	altered porphyry and argillite. Considerable fine pyrite										
	filling, pyrite casts and in quartz filled fractures.	--									
	fair amount of oxidation in soft section of tuff.										
33.84											
107 - 111	Buttons - have 1 ft. of fragments	N.S.									
Rec. 10%											
34.14											
111 - 112	A few buttons	N.S.									
	END OF HOLE										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120' 646.34 metres
AZIMUTH -90°
Core stored at 1834 Breakenridge Court, Kamloops

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 3/88
COMMENCED March 29/88
FINISHED April 6/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE ft. / m.	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH m	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
0 – 12 3.66	Casing										
12 – 15 4.54	As in other holes, a brecciated, altered feldspar porphyry.	61	12	15	3 0.90		15	.6	83	17	102
Recov. 75%	Very rusty. Some metallics in fractures.										
15 – 20 ~~7.62~~ 6.09	As above. Some metallics in surface fractures.	62	15	20	5 1.52		2	.4	113	6	111
	very fine pyrite, possible galena.										
20 – 25 7.62	As above. Trouble - grinding core	63	20	25	5 1.52		1	.6	109	3	91
Recov. 40%											
25 – 30 9.15	As above. Minor Metallics	64	25	30	5 1.52		5	.4	93	3	126
Recov. 90%											
30 – 35 10.66	Brecciated feldspar porphyry	65	30	35	5 1.52		68	.4	48	4	129
Recov. 90%	No visible metallics										
35 – 40 12.24	As above	66	35	40	5 1.52		9	.5	80	7	136
Recov. 95%											
40 – 44 13.40	As above	67	40	44	4 1.20		3	.2	62	7	121
Recov. 95%											
44 – 50 15.20	Feldspar porphyry. Breccia. Variable amount of silicifica-	68	44	50	6 1.80		15	.5	84	7	90
Recov. 100%	tion. Minor metallics										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120
AZIMUTH -90°

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 3/88
COMMENCED March 29/88
FINISHED April 6/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH m.	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
50 – 55 16.7	Lost water. Recovered by using heavy grease.										
Recov. 75%	Core badly broken and washed out. Balance of core O.K.	69	50	55	1.52 5		330	1.1	71	33	80
	Little silicification beyond 51 ft., save metallics.										
55 – 60 18.29	Altered feldspar porphyry. Breccia. Still light coloured.	70	55	60	1.52 5		7	.4	59	8	65
95%	Some leaching. Patchy silicification. Possible mineral-										
	ization in fractures (?)										
60 – 65 19.81	Variable colour. Turned grey and hard for 18" @ 61, and 64	71	60	65	1.52 5		102	.9	62	16	73
100%	for 3½ ft. Metallics visible in fractures. Few pyrite										
	casts. All well brecciated, and then fractured.										
65 – 70 21.30	Mostly grey, patchy hardness. Some Pb-pyrite mineralization.	72	65	70	1.52 5		13	.2	39	8	82
	Note that all fractures are filled (black quartz ?) regard-										
	less of direction or hardness. At 68 core changes to a										
	pinkish-sandy appearance. Very fine grained – little										
	quartz.										
70 – 75 22.82	Same as above. The same fracture system persists all	73	70	75	1.52 5		34	.2	39	12	84
	through the core.										
75 – 80 24.34	As previous, but grey to 77 ft., then changing	74	75	80	1.52 5		5	.4	102	7	103
95%	gradually – mostly brownish with increasing quartz.										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120'
AZIMUTH -90°

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 3/88
COMMENCED March 29/88
FINISHED April 6/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
M		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
80 - 85 25.90	As previous. Some pitting. At about 83 ft. changing to	75	80	85	1.52 5		7	.6	91	5	162
95%	grey, very hard - silicified. Increasing mineralization										
85 - 90 27.43	Similar to above. Sections light grey to dark grey with	76	85	90	1.52 5		290	1.9	88	238	75
95%	plenty of mineralization.										
90 - 95 28.96	As above. All the rock is a brecciated feldspar porphyry	77	90	95	1.52 5		1	.3	93	2	55
95%											
95 - 100 30.49	As above. Hardness of core varies from quartz, hard to	78	95	100	1.52 5		3	.4	114	9	76
95%	limestone hardness. Some pyrite mineralization. Maybe										
	very fine galena.										
100 - 105 32.0	Very broken, but similar to above. Little mineralization	79	100	105	1.52 5		1	.4	68	9	76
75%											
105 - 110 33.52	Very broken. Some soft, brown, muddy looking material	80	105	110	1.52 5		8	.6	72	6	91
50%											
110 - 115 35.04	Completely broken. Mostly a reddish brown and sandy	81	110	115	1.52 5		15	.2	61	15	118
50%											
115 - 120 36.59	Soft, brown. Obvious leaching	82	115	120	1.52 5		153	.8	63	31	149
30%	Some faint mineralization (?)										
120 - 125 38.11	Completely broken. Some soft material	83	120	125	1.52 5		87	1.2	94	63	208
0%											

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120
AZIMUTH -90°

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 3/88
COMMENCED March 29/88
FINISHED April 6/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE (M)	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
125 – 130 39.63	As above										
40%		84	125	130	1.52 5		29	1.0	101	40	181
130 – 135 41.15	All dark. Badly broken. Argillite breccia with some	85	130	135	1.52 5		12	.7	94	16	93
40%	alteration										
135 – 140 42.68	One foot as above. Then transition to limey, hard, tough,	86	135	140	1.52 5		16	.4	60	13	64
80%	Turned soft at 143.										
140 – 145 44.20	As above. 146 – 142 – Soft, pyrite with black stain	87	140	145	1.52 5		36	.3	38	13	61
80%	Argellitic	26750	145	147	0.60 2		75	.3	29	43	50
145 – 150 45.72	First 18", as above, some mineral (?).	88	147	150	0.96 3		18	.9	84	29	88
80%	Change to argillite breccia, rather clayey look.										
150 – 155 47.24	As above	89	150	155	1.52 5		41	1.0	150	22	120
80%	Very broken										
155 – 160 48.76	As above. Last foot almost completely washed out.	90	155	160	1.52 5		19	.6	84	9	105
75%											
160 – 165 50.22	Argellitic, very broken. Washed out. All core in this and	91	160	165	1.52 5		13	.8	96	12	147
40%	previous boxes coated with mud.										
165 – 170 51.74	Argillitic, some washed out. Brecciation visible only	92	165	170	1.52 5		163	.7	70	7	124
90%	because of filled fractures between fragments.										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120
AZIMUTH 90°

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 3/88
COMMENCED March 29/88
FINISHED April 6/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE M	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
170 – 175 -53.35	Same as previous										
90%	Fractures filled	93	170	175	5 M 1.52		15	.3	247	14	225
175 – 180 -54.88	All in small pieces, but still argillitic fractures filled.	94	175	180	5 1.52		4	.6	108	10	141
	Small section of hematized core near 175 ft.										
180 – 185 56.40	Badly broken, more large pieces than above. Last foot –	95	180	185	5 1.52		10	.5	88	9	94
	speckled breccia										
185 – 189 -57.60	Back to the spotted, altered feldspar porphyry breccia.	96	185	189	4 1.20		6	.2	39	10	90
	Kaolinized amygdules. Colour is reddish. Fractures										
	and veinlets filled quartz calcite.										
189 – 192 -58.50	Altered feldspar porphyry breccia, spotted with white calcite	97	189	192	3 0.90		9	.2	28	9	87
95%	amygdules over entire length. A short bleached white										
	section contains fine pyrite. Little leaching.										
192 – 200 -60.98	Argillitic breccia with quartz carbonate fracture filling.	98	192	200	8 2.43		14	.6	114	14	132
95%	Some leaching in places heavy leaching.										
200 – 206 -62.80	Argillitic breccia. More broken. More leaching.	99	200	206	6 1.8		11	.6	79	11	99
85%											
206 – 209 -63.70	Brownish altered feldspar porphyry breccia. Still fine	100	206	209	3 0.90		8	.1	29	9	130
100%	mineralization in filled fractures.										

DIAMOND DRILL LOG

COLLAR:—
LAT. 99 + 80 N
DEP. 99 + 57 E
ELEVATION 2120
AZIMUTH -90°

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 3/88
COMMENCED March 29/88
FINISHED April 6/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE M.	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
209 – 215 (65.55)	Argillitic breccia. Slightly broken. Strong leaching with										
90%	heavy pitting. Fractures filled.	878	209	215	6 (1.80)		31	1.5	83	33	117
215 – 220 (67.07)	Argillitic	879	215	220	5 (1.52)		30	1.1	90	13	116
95%	Considerable pitting										
220 – 225 (68.59)	Argillitic. More solid than last	880	220	225	5 (1.52)		6	.8	89	11	127
95%											
225 – 230 (70.12)	Argillitic. Short lengths. Slight pitting	881	225	230	5 (1.52)		1	.8	90	11	99
95%											
230 – 235 (71.64)	Argillitic. Badly broken 231 – 234	882	230	235	5 (1.52)		14	.8	84	9	97
95%											
235 – 239 (72.87)	As above to 237. Then balance is dense black. Some	883	235	239	4 (1.20)		1	1.0	84	10	99
95%	pitting. No quartz stringers.										
239 – 245 (74.70)	Argillitic breccia. Broken. Considerable leaching. Some	884	239	245	6 (1.80)		3	.9	90	10	86
90%	quartz carbonate in fine veinlets.										
245 – 250 (76.22)	Similar to above, but much blacker. Possible carbonaceous.	885	245	250	5 (1.52)		11	1.0	92	9	95
	Clean to handle.										
	END OF HOLE										

Core stored at 1834 Breakenridge Court, Kamloops

DIAMOND DRILL LOG

COLLAR:— 000
LAT. 10,+30N m
DEP. 10,080+10E m
ELEVATION 2120 Our base station.
AZIMUTH —90° 640.24 metres
Set altimeter to 2100 ft. at Jag 4/88
April 8/88 at 10:00 A.M.

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM, BARNHART VALE
HOLE NO. JAG 4/88
COMMENCED April 17/88
FINISHED May 2/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE M	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH M.	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
0 – 6' 1.8	Casing										
6 – 12' 3.66	Ground away. No recovery										
12 – 20' 6.00	Grey argellitic breccia. Surface washed	887	12	20	2.43 8		5	.2	74	4	66
90%	Out in places. A few pyrite casts. A few scattered pyrite crystals. Fractures rusty. Same sets of fractures as in previous holes.										
20 – 25 7.52	As above	888	20	25	1.52 5		1	.5	76	7	79
90%											
25 – 29 8.84	As above	889	25	30			3	.1	66	5	195
90%											
29 – 35 10.67	Hematized altered feldspar porphyry - darker in filled	890	30	35	1.52 5		2	.1	32	2	156
100%	fractures. This is spotted with kaolinized amygdules as in previous cores. Lots of limonite										
35 – 40 12.0	Grey argillitic again. Broken, ~~considerable washing out of~~	891	35	40	1.52 5		5	.5	83	3	70
90%	core										
40 – 45 13.52	8 inches of red altered dyke, then argillaceous material	892	40	45	1.52 5		6	.1	74	6	66
50%	extremely leached so that rock fragments are exposed. The red altered dyke, when split, showed minor pyrite.										

DIAMOND DRILL LOG

COLLAR:—
LAT.
DEP.
ELEVATION 2110 Our base station
AZIMUTH -90°
Set altimeter to 2100 ft. at Jag 4/88
April 8/88 at 10:00 A.M.

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM, JAG 4/88
HOLE NO.
COMMENCED April 17/88
FINISHED May 2/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH m	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag /ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
45 – 50 15,20	Grey altered dyke. Argillitic fragments more massive,										
80%	less leaching than last section. The general fracture	893	45	50	1.52 5						
	system still persists with quartz-carbonate filling, some										
	of which are black.										
50 – 55 16,72	As above broken	894	50	55	1.52 5		9	.3	75	15	109
90%	Some of the reddish altered dyke										
55 – 60 18,24	As previous. Broken.	895	55	60	1.52 5		7	.6	101	18	121
90%	It appears to have more quartz in some pieces.										
60 – 65 19,76	61-62 40% recovery. Broken, hard, grey, fragmental,	896	60	65	1.52 5		8	.9	67	41	133
85%	Veinlets persist and usually quartz-carbonate filled.										
	No mineral observed.										
65 – 70 21,22	Short lengths. Broken as above. Tan coloured,	897	65	70	1.52 5		31	1.2	99	124	233
90%	hard.										
70 – 75 22,74	As above, but a lighter tan. Sandy appearance. Breccia	804	70	75	1.52 5		24	.1	65	3	70
95%	still with few veinlets. Then abrupt changes to argel-										
	litic breccia.										
75 – 80 24,26	Argellitic breccia. Hard. Some leaching. Minor galena	805	75	80	1.52 5		6	.1	59	2	84
95%	showing in fractures. Heavily oxidized.										

DIAMOND DRILL LOG

COLLAR:—
LAT. —
DEP. —
ELEVATION 2110 Our base station
AZIMUTH -90°
Set altimeter to 2100 ft. at Jag 4/88
April 8/88 at 10:00 A.M.

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 4/88
COMMENCED April 1/88
FINISHED May 2/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH M.	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
80 – 85 25,41	Very broken. Washed out. Tan coloured breccia										
50%	Fairly hard	806	80	85	1.52 5		14	.2	146	2	136
85 – 90 27.40	Very broken breccia. Tan coloured. Last two feet becoming	807	85	90	1.52 5		2	.1	56	3	106
60%	argillitic. Hard to 90 ft.										
90 – 95 28.92	Argillitic breccia. Not too broken. Hard-quartz ?	808	90	95	1.52 5		2	.1	34	5	85
95%	Galena – very fine. Yellow oxide of lead ?										
95 – 100 30.44	Manganese stain ? Limonite or Pb oxide ?	809	95	100	1.52 5		1	.9	7	6	141
50%	Argillitic breccia – very hard.										
100 – 105 31.96	Argillitic breccia, some leaching, leaving breccia fragments	810	100	105	1.52 5		1	.4	82	9	165
90%	exposed. More quartz (?)										
105 – 110 33.48	As previous. More quartz. More leaching.	811	105	110	1.52 5		5	.3	79	18	157
85%	108–110 Extremely broken.										
110 – 115 35.10	As above.	812	110	115	1.52 5		1	.4	81	9	106
60%	Very badly broken.										
115 – 120 36.52	Still argillitic, hard, completely broken up.	813	115	120	1.52 5		4	1.3	109	13	140
50%	Core loss very high.										
120 – 126 38.40	No core. Handful of argillitic chips. Will start using	814	120	125	1.52 5		1	.5	88	11	148
10%	mud for drilling. Have lost water, and may be caving.										

DIAMOND DRILL LOG

COLLAR:—
LAT. .....
DEP. .....
ELEVATION ..... 2110 Our Base station
AZIMUTH ..... -90°
Set altimeter to 2100 ft. at Jag 4/88
April 8/88 at 10:00 A.M.

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY . BARN CLAIM
HOLE NO. . . JAG 4/88
COMMENCED April 17/88
FINISHED May 2/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO.	Ag/ppm	Cu/ppm	Pb/ppm	Zn/ppm
126 – 129 39.33	This 3 ft. section has some mineralization all through.											
85%	The only fair section to date in this hole. Heavy quartz	815	126	129	6,90 3		X 225		1.0	80	98	463
	in argillitic breccia, and in the last foot changed to											
	porphyritic breccia. Hard silicified. Lost water											
	completely.											
129 – 133 41.55	Greyish argillitic breccia. Well fractured. More quartz	816	129	135	1,20 4		10		1.0	51	9	92
95%	than usual, less limonite.											
133 – 140 42.69	Hematized altered dyke breccia. Softer than knife blade.	817	133	140	2,13 7		5		1.0	120	6	67
95%	Fracture fillings also red, little limonite.											
140 – 145 44.20	Argillitic breccia. Fairly hard, good silicification.	818	140	145	1,52 5		3		4.7	99	6	105
90%	Little limonite.											
145 – 150 45.73	Argillitic breccia. Very hard silicified-quartz plentiful.	819	145	150	1,52 5		X 126		2.3	74	23	62
100%	Some mineralization. Less limonite than usual.											
150 – 155 47.26	Hematized altered dyke. Breccia, very hard and dense	820	150	155	1,52 5		19		.4	97	99	44
100%	(Jasper ?). Well fractured and fracture-filled with											
	quartz-calcite. Slight leaching. Far less limonite than											
	upper footage. Minor pyrite in a few spots, and in frac-											
	tures.											

DIAMOND DRILL LOG

COLLAR:—
LAT.
DEP.
ELEVATION 2110 Our Base station
AZIMUTH -90°
Set altimeter to 2100 ft. at Jag 4/88
April 8/88 at 10:00 A.M.

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 4/88
COMMENCED April 17/88
FINISHED May 2/88
PURPOSE OF HOLE Test Mineralization
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO	FROM	TO	WIDTH M.	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag /ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
155 -160 42.70 M.	8" hematized dyke (?). Then blended with argillite.										
75%	Some broken, in place, badly. Heavy hairline fractures.	821	155	160	1.52 5		2	.7	74	10	79
	calcite-quartz filled.										
160 - 165 56.30	As previous. Mixed sandstone-argillite 50 - 50. Fair	822	160	165	1.52 5		31	1.0	77	11	91
90%	pyrite. More quartz than usual. Hard										
165 - 170 51.83	Argillite breccia. Broken leached.	823	165	170	1.52 5		4	.9	73	8	96
95%	Some pyrite.										
170 - 176 53.66	Argillite breccia. Broken. Massive quartz	824	170	176	1.80 6		1	.7	76	13	99
90%	at 171										
176 - 180 54.88	As above. Very broken. Argillitic with yellow to grey	825	176	180	1.40 4		1	.5	69	9	88
90%	sandy material mixed in some sections to 181 ft.										
180 - 185 56.46	Argillitic material as previous. Generally softer,	826	180	185	1.52 5		2	.7	84	10	93
90%	Leached. Broken.										
185 - 190 57.92	Argillitic, some leaching. Tendency to be banded, by	827	185	190	1.52 5		5	.6	60	7	68
95%	mixed rocks, or sets of fractures at 60° to core axis,										
	also some at 30°. At 188, heavy graphite on 30° fracture.										
190 - 195 59.44	Argillitic. Banded as previous.	828	190	195	1.52 5		3	.6	98	13	115
95%											
195 - 200 60.98	As previous	829	195	200	1.52 5		1	.5	83	10	118

DIAMOND DRILL LOG

COLLAR:—

LAT. .....

DEP. .....

ELEVATION ..... 2110 Our Base station

AZIMUTH ..... -90°

Set altimeter to 2100 ft. at Jag 4/88
April 8/88 at 10:00 A.M.

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY ..... BARN CLAIM

HOLE NO. ..... JAG 4/88

COMMENCED ..... April 17/88

FINISHED ..... May 2/88

PURPOSE OF HOLE ..... Test Mineralization

LOGGED BY: ..... A.F. Roberts

FOOTAGE M.	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH M.	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
200 - 208 63,4	Argillaceous. Black to grey , soft, broken -										
90%	lacks any metallics.	830	200	208	2,43 8		1	.5	86	9	97
208 - 216 65,85	Handful of argillitic pebbles. lost core.	831	208	216	2,43 8		1	.5	62	7	101
-											
216 - 218 66,46	As above, but a lot of pyrite, arsenopyrite (?),	832	216	218	2 0.60		27	1.6	209	26	88
-	Galena (?)										
218 - 220 67.66	As above but little metallics	833	218	220	2 0.66		4	.7	77	10	71
-											
220 - 223 67.99	Argillitic - Grey, some quartz-pyrite. Sharp contact	834	220	223	3 0.90		2	.6	99	9	98
95%	change to altered feldspar dyke at 223.										
223 - 227 69.20	N.B. Feldspar dyke. Same as other sections further up the	835	223	227	4 1,20		+450	2.1	65	31	28
95%	hole. Apparently massive, brecciation not visible. Hard,										
	siliceous quartz veinlets. Very little limonite. Pyrite -										
	far more visible than elsewhere in this and other holes.										
227 - 229 69.82	As above. Heavy pyrite. Special sample	836	227	229	2 0,60		+520	2.6	56	51	37
95%											
229 - 230 70.12	As above. Special sample	837	229	230	1 0,30		+610	.6	27	18	59
98%											
230 - 235 71,65	As above. Broken oxidized at 231 and 233 feet. At 231 -	838	230	235	5 1,52		4	.4	23	10	57
%	some hematized material.										

DIAMOND DRILL LOG

COLLAR:—

LAT.

DEP.

ELEVATION 2110 Our Base station

AZIMUTH -90°

Set altimeter to 2100 ft. at Jag 4/88

April 8/88 at 10:00 A.M.

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM

HOLE NO. JAG. 4/88

COMMENCED April 17/88

FINISHED May 2/88

PURPOSE OF HOLE Test. Mineralization

LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au/ppb	SAMPLE NO. Ag/ppm	FROM Cu/ppm	TO Pb/ppm	ASSAY Zn/ppm
235 - 240 M. 73.17	As above. Some limonite stain.										
90%	Some very good pyrite at 235	839	235	240	1.52 5	X	305	1.8	51	47	42
240 - 245 74.70	As above. Mostly a reddish colour.	840	240	245	1.52 5	X	5,990	4.0	35	17	58
90%	Softer rock										
245 - 250 76.22	As above, badly broken. Both grey and reddish altered dyke.	841	245	250	1.52 5	X	205	0.6	39	14	44
85%	Some good mineralization.										
250 - 258 78.66	Lost core barrel. Lost core. Eventually recovered core	842	250	258	2.43 8	X	1,660	3.8	77	72	38
10%	barrel. All cores sent to assay. Altered dyke. Some										
	mineralization. Sharp contact with argillites.										
258 - 265 80.79	Massive argillite. Hard, siliceous. Massive quartz veinlets.	843	258	265	2.13 7		1	0.4	41	5	70
90%	Few specks of pyrite.										
265 - 270 82.32	As above. Note some gouge on slips at all broken	844	265	270	1.52 5		5	0.3	61	6	133
90%	angles.										
270 - 280 85.37	Massive argillite. Badly broken. Driller lost core.	845	270	280	3.09 10		6	0.4	87	8	89
20%	Had to pull rods for any recovery. Hole stopped.										
	END OF HOLE										

NOTE: This argillite has consistently shown very fine pyrite, fairly evenly distributed through the core. Some gouge on fractures seldom more than 1/4". Note displacement on fracture.

DIAMOND DRILL LOG

COLLAR:—
LAT. 10030 N m
DEP. 10060 E m
ELEVATION 2040' 621.95 metres
AZIMUTH -90°

Core stored at 1834 Braeburn Road Court, Kamloops

DIP TEST		
FOOTAGE	ANGLE	
	READING	CORRECTED

PROPERTY BARN CLAIM
HOLE NO. JAG 6/88
COMMENCED June 6/88
FINISHED June 17/88
PURPOSE OF HOLE Mineral Exploration
LOGGED BY: A.F. Roberts

FOOTAGE	DESCRIPTION	CORE SAMPLES								
		SAMPLE NO.	FROM	TO	WIDTH	ASSAY	WIDTH X ASSAY	SAMPLE NO.	FROM	TO	ASSAY
0 - 12 M 3.66	No core. Sludge to 12 ft. (1-8) & (8-12)										
12 - 20 6.09	2 ft. of pebbles, mixed argillite, red sandstone with minor										
10%	quartz veining in last inch.										
20 - 26 7.93	Broken, mostly pebbles. Slight pyrite in quartz. 4" red										
50%	sandstone, then all argillite 5% quartz brecciated. Note,										
	the possibility of the feldspar dike being altered and										
	hematized.										
26 - 30 9.0	Argillite, some red sandstone inclusions. Fracture filling -										
25%	hematized quartz calcite fractures 30°- 45° and parallel										
	to core axis.										
30 - 35 10.67	Broken, mostly pebbles of argillite. Some hematite staining.										
22%	Breccia										
35 - 45 12.19	Argillite breccia with quartz carbonate veining. Hematite										
85%	and limonite staining.										
46 - 61 13.71	Brecciated argillite. Inclusions of undetermined sediments.										
80%	Hematite and limonite staining. Ends with partial blending										
	with red sandstone.										

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PROPERTY: BARN CLAIM
HOLE NO.: JAG 6/88
COMMENCED: June 6/88
FINISHED: June 17/88
PURPOSE OF HOLE: Mineral Exploration
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FOOTAGE	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH	ASSAY	WIDTH X ASSAY	SAMPLE NO.	FROM	TO	ASSAY
61 - 71 (M) 21.65	Red sandstone, changing to the altered feldspar porphyry										
85%	dike in which the emygdules have been altered to kaolin										
	saturated with hematite. Very little quartz. Brecciated.										
71 - 76 23.17	Altered dike - hematized. Some argillite inclusions.										
85%	No mineralization up to this point in the hole.										
76 - 84 25.61	Sharp contact with argillite - brecciated. Some leaching.										
80%											
84 - 90 27.40	Argillite. Mud inclusions in the argillite. 87 ft.										
95%	fragments cemented to form arkose.										
~~90 - 100~~ 30.40	~~Argillite. Hematite increasing to 100 ft.~~										
85%											
100 - 102 31.10	Hematized altered dyke (sandstone ?). Changes to a light										
95%	brown bleached material, fine grained, (mudstone ?).										
	Contact with argillite.										
102 - 110 33.54	Argillite. All broken. Limonite stained. Several 4" - 6"										
75%	sections. Arkose.										
110 - 111 33.84	Short length of sandy material (mudstone) between sections										
95%	of argillite.										
111 - 121 36.88 ~~33.84~~	Argillite breccia. Both limonite and hematite staining.										

NOT sampled

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FOOTAGE (M)	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH (M)	ASSAY	WIDTH X ASSAY Au ppb	SAMPLE NO. Ag ppm	FROM Cu ppm	TO Pb ppm	ASSAY Zn ppm
121 – 123 375	Argillite breccia stained reddish and brownish with black										
95%	argillite inclusions.	8608	122	123	10.3 121		4	.5	71	9	74
123 – 128 39.02	6" of green mud, mottled – chloritized and altered dyke,	8609	123	128	5 6' 1.52		1	.3	111	10	67
	then solid to 128' with a sharp argillite contact. More						1				
	greyish from 125'. Brecciated. Calcite healing of										
	fractures.										
128 – 131 39.94	Argillite.										
95%	Contacts are sharp.										
131 – 134 40.85	Altered feldspar porphyry dyke. Partially chloritized.	8610	131	134	6.90 3'		1	.3	191	87	77
85%	Fractures are calcite filled.										
134 – 136 41.45	Sandy material – altered dyke. Generally grey. Some										
85%	chloritic sections. Calcite in fractures. (Note that										
	fractures feel talcy.) for 1 ft., change to argillite.										
136 – 145 44.21	Altered dyke chloritic, sandy, grey when split. Heavy	8605	136	145	12.74 9'		2	.4	121 8	8	74
95%	calcite in fractures. Heavily fractured. Pyrite										
	disseminated through core. Considerable pyrrhotite.										
	Last foot – sand.										
145 – 151 46.04	Argillite, 1 ft. of sand. Badly broken										
35%											

DIAMOND DRILL LOG

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FOOTAGE (M)	DESCRIPTION	CORE SAMPLES										
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au ppb	SAMPLE NO. Ag	FROM Cu	TO Pb	ASSAY Zn
151 – 164 50.0	Argillite fragments. Slight pyrite. Siliceous. Balance				0.60						
30%	in sludge – fragment	8606	161	163	2	→	265	.7	55	9	116
164 – 169 51.5	Siliceous. Argillite fragments Sludge	8682	155	160	5 1.52	→	~~320~~ 480	~~188~~ 59	~~69~~ 169	~~118~~	
20%						→	480	3.8	188	69	118
169 – 175 53.35	No core – washed or ground out. Sludge	8683	160	165	5 1.52	→	127	.8	126	11	106
0%											
175 – 177 53.96	Siliceous argillite fragments, some pyrite	8607	177	179	2 0.66		1	.9	59	6	58
10%											
177 – 179 54.57	Argillite. Siliceous fragments pyrite.										
10%											
179 – 182 55.49	Argillite broken – short pieces. Pyrite										
50%											
184 – 210 64.02	Badly broken short sections, fairly hard, some pyrite,	8618	179	184	5 1.52		1	.9	72	7	79
30%	~~Some pitting.~~										
	Some red sludges. Some hematite	8619	210	215	5 1.52		1	1.0	41	6	81
210 – 225 68.60	Amygdules, similar to altered feldspar porphyry. Similar	8620	215	220	5 1.52		1	.9	53	8	94
95%	pieces scattered through the core for 10 ft.										
	Much pyrite in veinlets and disseminated through the core.	8621	220	225	5 1.52		2	1.0	70	8	102
225–232 70.73	Washed out.										

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FOOTAGE M	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au ppb	SAMPLE NO. Ag ppm	FROM Cu ppm	TO Pb ppm	ASSAY Zn ppm
232 – 247 75.30	Good core as above, but sections washed out.				4.57						
20%	sludge	8622	232	247	15		2	.9	69	9	80
247 – 253 77.13	Argillite, badly broken. Quartz-carbonate filling veinlets.	8623	290	295	1.52 5		2	.8	65	8	108
80%	Very hard, some pyrite in fractures, and disseminated.										
253 – 268 81.7	As above. Very hard.										
20%											
268 – 290 88.41	No core recovered.										
0%	All in sludges.										
290 – 295 89.93	Perfect recovery to 300 ft.										
95%	Silicified argillite. Sections showing brecciation over										
	1" – 2". Veinlets filled with quartz, plenty of pyrite.										
	Occasional graphite on slips. Also some slips broken and										
	displaced for 1/4" – 1/2".										
295 – 298 90.85	Argillite, quartz filling 25% of core. Pyrite in fractures,	8624	295	298	0.90 3		2	.8	50	5	64
95%	and disseminated.										
298 – 300 91.45	As above, but not nearly as much pyrite.	8625	298	300	0.60 2		1	.7	72	8	103
95%											
300 – 305 92.97	Argillite. Fractures quartz filled. Pyrite plentiful in	8626	300	305	1.52 5		5	.9	63	10	99
95%	fractures and disseminated										

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FOOTAGE M	DESCRIPTION	CORE SAMPLES						Ag ppm / Au ppb			
		SAMPLE NO.	FROM	TO	WIDTH M	ASSAY	WIDTH X ASSAY Au ppb	SAMPLE NO.	FROM Cu ppm	TO Pb ppm	ASSAY Zn ppm
305–307 93.60	As previous. This 2 ft. much more pyrite than usual										
95%		8627	305	307	2 0.66		4	.8	75	11	79
307 – 310 94.15	As above	8628	307	310	3 0.96		5	.6	116	11	105
95%											
310 – 315 96.03	As above, but decreasing amount of quartz-carbonate	8629	310	315	5 1.52		3	.7	79	9	105
95%											
315 – 320 97.55	As above										
95%		8630	315	320	5 1.52		1	.7	37	6	63
320 – 325 99.07	NOTE: At 320 to 321. short mottled sections with tiny										
	amygdules suggest possibility of being altered dyke	8631	320	325	5 1.52		2	1.1	112	11	148
	absorbed in argillite.										
	Large number of slips with graphite. The sludges are										
	very black.										
325 – 326 99.37	Argillite quartz filled ~~fractures.~~ Hard, some pyrite in	~~8632~~	~~325~~	~~326~~	~~1.52~~ 1 0.30		1	1.1	~~67~~ 88	~~9~~ 11	~~110~~ 144
95%	veinlets and disseminated.										
326 – 336 102.43	Appears to be argillite. But under the glass has a very	8633	326	336	10 3.04		1	.5	18	2	41
18" for 10 ft.	fine grain, with an overall appearance of granite										
15%	(Aplite ?)										
336 – 344 104.88	No core.										

DIAMOND DRILL LOG

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LAT. .....

DEP. .....

ELEVATION .....

AZIMUTH .....

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PROPERTY ..... BARN CLAIM

HOLE NO. ..... JAG 6/88

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FINISHED ..... June 17/88

PURPOSE OF HOLE ..... Mineral Exploration

LOGGED BY: ..... A.F. Roberts

FOOTAGE (M)	DESCRIPTION	CORE SAMPLES									
		SAMPLE NO.	FROM	TO	WIDTH (M)	ASSAY	WIDTH X ASSAY Au ppb	SAMPLE NO. Ag ppm	FROM Cu ppm	TO Pb ppm	ASSAY Zn ppm
344 – 347 (105.79)	6" argillite	8634	347	351	1.26 (4)		5	1.1	88	11	193
1%											
347 – 354 (107.93)	Argillite – Last foot heavily graphitic.										
60%											
354 – 360 (109.76)	Sludge only.										
0 %											
	END OF HOLE										

APPENDIX "C"

ASSAY CERTIFICATES

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1 ROCK/CORE P2 CUTTING AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JUN 20 1988 DATE REPORT MAILED: June 24/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAQUAR EQUITIES File # 88-2093 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
U 8601 ROCK	1	32	5	103	.3	90	11	522	3.37	2	7	ND	5	103	1	2	2	73	1.72	.254	51	88	1.35	108	.16	37	.59	.04	.23	1	1
U 8602 ROCK	1	29	11	46	.5	10	4	797	2.53	347	5	ND	1	207	1	2	2	38	2.45	.057	8	13	.90	399	.01	17	.60	.01	.08	2	41
U 8603 ROCK	1	29	9	45	.7	9	5	962	3.26	214	5	ND	1	752	1	2	2	27	7.74	.049	8	15	3.05	233	.01	15	.51	.01	.10	2	5
U 8604 ROCK	1	38	8	51	1.4	5	5	669	3.38	161	5	ND	1	169	1	2	2	41	3.15	.069	12	10	.21	157	.01	9	.62	.02	.14	2	1280
U 8605 CORE	1	121	8	74	.4	102	32	1078	5.60	2	5	ND	1	212	1	2	2	94	3.59	.105	6	96	2.62	461	.09	7	1.84	.03	.61	1	2
U 8606 CORE	1	55	9	116	.7	28	6	1465	2.92	8	5	ND	1	518	1	3	2	31	9.67	.061	10	27	2.38	318	.01	17	.29	.01	.02	1	265
U 8607 CORE	1	59	6	68	.9	30	7	1398	2.19	2	5	ND	1	919	1	2	2	25	10.75	.050	10	23	.54	167	.01	10	.34	.01	.06	1	1
U 8608 CORE	1	71	9	74	.5	76	20	1904	5.06	3	5	ND	1	898	1	3	2	80	10.54	.074	8	111	1.26	362	.01	13	.34	.01	.02	1	4
U 8609 CORE	1	111	10	67	.3	96	32	1115	5.19	2	5	ND	1	236	1	2	2	104	3.82	.115	8	96	1.89	374	.10	7	1.39	.01	.40	1	1
U 8610 CORE	1	111	9	77	.3	97	33	1021	5.60	2	5	ND	1	305	1	2	2	96	2.54	.114	8	77	2.48	346	.13	7	1.74	.01	.53	1	1
U 8611 ROCK	1	80	5	35	.4	10	6	682	2.68	5	5	ND	1	162	1	2	2	38	3.42	.040	6	11	1.17	116	.01	5	.42	.01	.09	1	1
U 8612 ROCK	1	26	30	57	1.4	27	4	1292	2.02	12	5	ND	2	808	1	2	2	34	10.20	.061	9	38	2.90	135	.01	11	.38	.01	.02	1	1220
U 8613 ROCK	1	7	6	43	.3	7	5	485	2.31	3	5	ND	1	33	1	2	2	45	1.02	.036	6	18	.83	252	.04	7	1.14	.02	.14	2	3
U 8614 ROCK	7	38	11	86	.2	167	24	854	4.32	2	5	ND	1	103	1	2	2	45	2.53	.140	18	89	1.17	69	.01	18	.70	.01	.03	1	1
U 8615 ROCK	1	89	7	106	.9	69	8	713	1.92	76	5	ND	1	54	1	11	2	34	1.43	.069	14	49	.53	73	.01	10	.44	.01	.05	1	4
U 8616 ROCK	1	65	9	88	.4	34	6	377	2.48	53	5	ND	1	137	1	16	2	35	1.51	.085	7	33	.68	98	.01	8	.44	.01	.03	1	7
U 8617 CORE	1	84	13	100	.4	57	16	785	3.50	4	5	ND	1	317	1	2	2	63	4.60	.074	9	63	1.85	290	.07	4	1.04	.01	.23	1	1
U 8618 CORE	1	72	7	79	.9	30	7	1835	1.69	2	5	ND	2	696	1	2	2	29	10.95	.048	12	18	.60	189	.01	5	.50	.01	.10	1	1
U 8619 CORE	1	41	6	81	1.0	28	5	1057	1.88	28	5	ND	1	961	1	2	2	26	14.60	.088	9	21	.46	168	.01	7	.40	.01	.05	1	1
U 8620 CORE	1	53	8	94	.9	36	6	1133	1.82	2	5	ND	1	804	1	2	2	43	12.09	.093	10	39	.90	182	.01	12	.70	.01	.19	1	1
U 8621 CORE	1	70	8	102	1.0	38	7	951	2.26	2	5	ND	1	640	1	2	2	44	8.28	.076	11	33	1.07	143	.02	10	1.02	.01	.35	1	2
U 8622 CORE	1	60	9	80	.9	39	7	1097	2.03	3	5	ND	1	671	1	2	2	36	8.81	.079	10	34	.87	177	.01	9	.73	.01	.23	1	2
U 8623 CORE	1	65	10	108	.8	46	7	891	2.74	16	5	ND	2	502	1	5	2	24	7.37	.062	6	25	.78	121	.01	11	.37	.01	.08	1	2
U 8624 CORE	1	50	5	64	.7	28	5	875	1.76	45	5	ND	1	782	1	4	2	15	9.68	.043	5	16	1.70	130	.01	5	.30	.01	.09	1	2
U 8625 CORE	1	72	8	103	.7	49	8	1127	2.05	95	5	ND	1	606	1	14	2	20	8.77	.074	9	29	1.58	135	.01	10	.40	.01	.11	1	1
U 8626 CORE	1	63	10	99	.9	43	7	1305	2.25	34	5	ND	1	704	1	8	2	21	8.40	.065	8	26	1.40	154	.01	12	.38	.01	.10	1	5
U 8627 CORE	1	75	11	79	.8	48	10	1036	4.45	72	5	ND	1	213	1	43	2	31	3.39	.066	8	37	1.13	44	.01	10	.44	.01	.07	1	4
U 8628 CORE	1	116	11	105	.6	82	15	379	2.76	13	5	ND	1	107	1	7	2	34	1.27	.073	16	32	.27	127	.01	7	.65	.01	.11	1	5
U 8629 CORE	1	79	9	105	.7	59	9	909	2.64	6	5	ND	1	431	1	3	2	34	6.61	.058	9	30	.59	138	.01	7	.46	.01	.09	1	3
U 8630 CORE	1	37	6	63	.7	22	4	1492	1.73	2	5	ND	1	1024	1	2	2	23	15.22	.069	8	20	1.11	220	.01	9	.36	.01	.03	1	1
U 8631 CORE	1	112	11	148	1.1	49	11	696	2.75	3	5	ND	1	346	1	4	2	32	5.10	.072	8	28	.65	126	.01	7	.54	.01	.12	1	2
U 8632 CORE	1	67	9	110	1.1	32	7	900	2.46	21	5	ND	2	854	1	5	2	27	9.60	.080	9	27	.83	152	.01	5	.50	.01	.08	1	1
U 8633 CORE	1	18	2	41	.5	13	2	1429	.96	7	5	ND	2	1309	1	4	2	11	20.18	.042	6	11	.91	178	.01	4	.16	.01	.01	3	1
U 8634 CORE	2	88	11	199	1.1	81	11	1223	2.54	9	5	ND	2	287	1	6	2	31	4.63	.053	5	33	1.47	213	.01	7	.52	.01	.13	1	5
STD C/AU-R	18	58	41	132	7.1	66	27	1035	3.85	38	16	6	36	45	16	16	19	55	.49	.086	36	55	.90	173	.06	32	1.89	.06	.14	13	520

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
U 8680	2	529	38	195	1.0	76	29	1459	5.49	14	5	ND	1	393	1	2	2	67	6.38	.098	12	91	1.58	284	.01	10	.46	.04	.10	88	11
U 8681	2	223	22	227	1.3	56	21	1260	3.79	24	5	ND	1	336	2	2	2	54	6.41	.087	12	58	1.47	281	.01	18	.44	.02	.06	167	28
U 8682	2	188	69	118	3.8	54	17	1344	3.32	65	5	ND	1	551	1	2	2	38	8.22	.071	10	48	.92	225	.01	12	.31	.01	.06	147	480
U 8683	1	120	11	106	.8	69	21	1895	5.45	20	5	ND	1	367	1	2	2	67	8.34	.073	10	86	2.95	567	.01	11	.46	.02	.06	65	127
U 8684	2	159	13	134	.6	85	37	1655	5.92	17	5	ND	1	377	1	5	2	79	6.39	.092	10	120	2.28	400	.03	9	.81	.05	.27	73	7
U 8685	1	146	10	121	.7	79	29	1101	4.53	9	5	ND	1	233	1	2	2	69	3.80	.093	11	107	1.33	575	.02	8	.71	.02	.21	44	4
U 8686	1	153	9	118	.9	66	24	936	3.66	10	5	ND	1	263	1	2	2	61	4.22	.079	13	86	.95	462	.02	14	.74	.02	.20	40	7
U 8687	1	115	10	106	.6	74	30	1292	4.55	5	5	ND	1	403	1	2	2	77	6.34	.110	11	123	1.63	522	.03	6	.90	.01	.32	8	2
U 8688	2	141	9	111	.6	82	30	1149	4.90	14	5	ND	1	331	1	4	2	77	5.13	.122	10	128	1.63	723	.02	8	.83	.02	.24	18	5
U 8689	2	136	8	122	.8	66	24	1081	4.00	11	5	ND	1	297	1	2	2	63	4.73	.122	11	101	1.54	1115	.01	13	.67	.03	.16	36	5
U 8690	2	104	9	96	.7	59	22	929	3.66	9	5	ND	1	255	1	2	2	58	3.60	.130	10	95	1.21	1409	.01	23	.66	.02	.15	12	3
U 8691	1	116	9	102	.5	75	27	917	4.03	8	5	ND	1	306	1	2	2	73	4.32	.119	12	121	1.34	1016	.02	13	.82	.03	.24	9	3
U 8692	1	105	8	95	.5	67	25	1072	4.24	8	5	ND	2	324	1	2	2	66	4.94	.119	10	104	1.49	987	.02	13	.68	.01	.23	6	2
U 8693	1	133	8	111	.7	79	31	1126	4.29	11	5	ND	1	567	1	2	2	71	7.85	.115	10	119	1.53	665	.02	8	.72	.04	.20	16	1
U 8694	1	108	6	90	.6	70	27	1161	4.24	7	5	ND	1	438	1	2	2	73	6.61	.118	10	123	1.57	452	.02	21	.81	.03	.26	2	2
U 8695	1	142	11	110	.7	88	35	1332	5.30	8	5	ND	1	454	1	2	2	89	6.89	.132	12	153	1.89	366	.02	9	.95	.02	.29	3	3
U 8696	1	128	9	102	.6	86	31	1152	4.84	6	5	ND	1	307	1	2	2	74	4.95	.117	11	129	1.53	294	.02	12	.74	.02	.18	6	4
U 8697	1	121	9	112	.7	84	28	1195	4.92	7	5	ND	1	291	1	2	2	73	4.96	.118	11	125	1.57	226	.02	10	.71	.03	.18	4	7
U 8698	1	110	11	107	.7	70	19	1085	3.86	35	5	ND	1	370	1	5	2	48	5.76	.099	9	68	1.14	160	.01	11	.59	.04	.18	17	12
U 8699	1	94	10	100	.7	58	17	1249	3.30	43	5	ND	1	594	1	2	2	43	8.34	.090	9	64	1.07	227	.01	11	.50	.02	.14	15	1
U 8700	1	105	8	105	.6	73	23	1126	3.87	37	5	ND	1	417	1	2	2	55	6.30	.097	9	93	1.20	217	.01	16	.62	.02	.18	10	6
STD C/AU-R	18	60	38	132	6.9	68	29	1072	4.03	40	18	7	37	50	18	16	19	58	.49	.084	40	59	.92	181	.07	30	2.00	.05	.13	12	480

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Core AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: MAY 04 1988 DATE REPORT MAILED: May 10/88 ASSAYER C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAGUAR EQUITIES File # 88-1269

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
060839	1	51	47	42	1.8	7	7	825	3.36	2419	5	ND	1	292	1	7	6	16	4.32	.059	6	4	1.33	66	.01	4	.36	.01	.13	2	305
060840	1	35	17	58	4.0	10	7	810	3.47	188	5	8	2	162	1	4	2	40	2.79	.069	11	12	.86	66	.01	8	.46	.01	.10	1	5990
060841	1	39	14	44	.6	10	7	921	3.35	210	5	ND	2	287	1	6	2	21	4.01	.066	8	6	1.26	59	.01	9	.44	.01	.13	1	205
060842	1	77	72	38	3.8	10	6	698	3.18	3247	5	2	2	252	1	6	4	19	3.27	.065	6	6	1.06	56	.01	5	.44	.01	.12	1	1660
060843	1	41	5	70	.4	27	4	2185	1.59	13	5	ND	1	853	1	3	2	39	12.95	.064	7	39	1.49	130	.01	2	.30	.01	.03	1	1
060844	1	61	6	133	.3	52	7	1111	2.20	27	5	ND	2	727	2	2	2	32	9.61	.081	7	43	.88	116	.01	13	.39	.01	.09	1	5
060845	1	87	3	89	.4	57	10	666	2.43	37	5	ND	2	386	1	13	2	39	5.84	.059	8	39	1.15	110	.01	8	.48	.01	.13	1	6

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: MAY 02 1988 DATE REPORT MAILED: May 6/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAGUAR EQUITIES File # 88-1244

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
060820	1	97	3	44	.4	125	31	1730	4.30	204	5	ND	2	1086	1	33	2	65	7.27	.111	7	140	3.39	109	.01	11	.52	.01	.12	2	19
060821	1	74	10	79	.7	75	16	3735	4.10	75	5	ND	1	434	1	25	2	40	7.39	.078	7	63	3.20	107	.01	6	.44	.01	.11	1	2
060822	1	77	11	94	1.0	86	15	1809	3.80	126	5	ND	2	714	1	34	2	34	6.59	.062	7	49	3.03	286	.01	5	.42	.01	.15	1	31
060823	1	73	8	96	.9	47	8	1564	2.98	66	5	ND	2	424	1	13	2	24	4.44	.074	11	27	1.93	178	.01	9	.45	.01	.17	1	4
060824	1	76	13	99	.7	52	9	1169	2.88	83	5	ND	2	321	1	18	2	28	3.73	.090	13	30	1.33	117	.01	11	.52	.01	.17	1	1
060825	2	69	3	88	.5	47	8	1184	2.15	53	5	ND	1	135	1	15	2	28	3.10	.102	9	42	.62	111	.01	3	.46	.01	.11	1	1
060826	1	84	10	93	.7	42	8	1090	2.49	53	5	ND	2	187	1	13	2	33	2.69	.079	8	43	.77	164	.01	4	.52	.01	.11	1	2
060827	1	69	7	68	.6	40	6	1449	2.57	158	5	ND	2	574	1	11	2	19	5.98	.043	6	24	2.45	251	.01	7	.36	.01	.13	1	5
060828	2	98	13	115	.6	70	9	1133	2.69	59	5	ND	2	297	1	22	2	40	3.11	.089	10	40	1.03	226	.01	4	.57	.01	.14	1	3
060829	2	83	10	118	.5	65	9	1275	2.86	41	5	ND	3	271	1	25	2	36	4.09	.087	11	44	1.35	130	.01	4	.57	.01	.16	1	1
060830	1	86	9	97	.5	51	9	1371	2.79	26	5	ND	1	228	1	22	2	36	3.47	.095	10	43	1.19	133	.01	8	.59	.01	.14	1	1
060831	1	52	7	101	.5	41	7	1848	2.85	28	5	ND	1	389	1	14	2	43	5.01	.093	9	72	1.90	196	.01	2	.46	.01	.11	1	1
060832	7	209	26	98	1.6	79	37	984	7.75	51	5	ND	2	201	1	15	3	26	3.48	.064	4	27	1.20	34	.01	3	.51	.01	.15	1	27
060833	1	77	10	71	.7	38	7	1163	2.99	439	5	ND	1	387	1	9	2	21	4.82	.058	10	18	1.81	90	.01	9	.54	.01	.24	1	4
060834	2	99	9	98	.6	49	9	1035	2.98	155	5	ND	1	425	1	35	2	22	5.07	.062	11	20	1.96	100	.01	6	.45	.01	.19	1	2
060835	1	65	31	28	2.1	7	5	945	2.86	218	5	ND	1	269	1	2	2	19	3.46	.067	7	7	1.12	70	.01	4	.42	.01	.13	1	450
060836	1	50	51	37	2.6	6	8	783	2.55	740	5	ND	2	178	1	2	2	29	2.85	.070	10	10	.90	79	.01	5	.47	.01	.15	2	520
060837	1	27	18	59	.6	7	10	1019	3.14	145	5	ND	1	179	1	2	2	35	2.83	.073	11	11	.92	135	.01	5	.62	.01	.14	1	610
060838	1	23	10	57	.4	5	7	1348	3.81	236	5	ND	2	287	1	7	2	30	1.42	.067	11	8	1.48	72	.01	17	.50	.01	.14	1	4
STD C/AU-R	19	62	40	132	7.5	71	30	1125	4.18	42	23	8	39	53	20	20	21	61	.50	.089	42	61	.88	181	.07	34	1.77	.06	.13	12	490

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716 DATE RECEIVED: MAY 17 1988
DATE REPORT MAILED: May 20/88.

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp
AU** AND AG** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: C. Leong .. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAGUAR EQUITIES File # 88-1269R

SAMPLE#	Ag** OZ/T	Au** OZ/T
060840	.09	.181 ✓
060841	.02	.005
060842	.11	.043 ✓

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: MAY 17 1988
DATE REPORT MAILED: May 20/88.

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp

ASSAYER: C. Leong ..... D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAGUAR EQUITIES File # 88-1007R

SAMPLE#	Ag** OZ/T
50777	.12
26747	.26
26748	.81
26749	.26

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: MAY 17 1988
DATE REPORT MAILED: May 20/88

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp
AU** AND AG** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: C. Leong D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAGUAR EQUITIES File # 88-1244R

SAMPLE#	Ag** OZ/T	Au** OZ/T
060836	.08	.014
060837	.05	.016

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: APR 24 1988
DATE REPORT MAILED: April 27/88

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp AU** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: C. Leong D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAGUAR EQUITIES File # 88-1007R

	SAMPLE#	AU** oz/t	
Jag 1	60775	.001	130 - 135
	60776	.002	135 - 140
	60777	.224	140 - 145
	60778	.016	140 - 150
Jag 2	60798	.001	70 - 75
	60799	.010	75 - 77
	60800	.002	77 - 78
Jag 3	60878	.007	209 - 215
	69	.008	50 - 55
	76	.007	85 - 90
	82	.010	115 - 120
	83	.002	120 - 125
	84	.003	125 - 130
	100	.001	206 - 209
Pit #3	26747 6ft	.117	
Pit #4	26748 select	.554	
Pit #4	26749	.033	

Pits

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CORE/ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: APR 15 1988 DATE REPORT MAILED: April 19/88 ASSAYER: C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

KENNETH ELLERBECK File # 88-1091

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
060804	3	65	3	70	.1	62	15	1443	3.40	680	5	ND	1	637	1	5	2	47	5.52	.061	9	62	2.83	109	.01	3	.34	.01	.10	1	24
060805	2	59	2	84	.1	41	6	1918	2.63	58	5	ND	1	218	1	6	2	34	4.64	.085	7	26	2.16	105	.01	2	.25	.01	.07	1	6
060806	4	146	2	136	.2	92	13	1424	2.41	57	5	ND	1	111	1	9	4	49	1.42	.099	10	57	.53	155	.01	6	.41	.01	.02	1	14
060807	2	56	3	106	.1	62	10	1689	2.28	140	5	ND	1	147	1	3	2	47	2.65	.082	6	39	.74	103	.01	2	.30	.01	.01	1	2
060808	2	34	5	85	.1	61	6	2588	2.68	78	5	ND	1	139	1	19	2	28	4.03	.123	5	23	1.31	134	.01	2	.29	.01	.01	1	2
060809	2	71	6	141	.9	73	9	1832	2.61	84	5	ND	1	156	1	10	2	40	3.22	.103	12	44	1.11	140	.01	4	.43	.01	.16	1	1
060810	2	82	9	165	.4	100	12	1198	2.62	75	5	ND	1	117	1	18	2	51	2.09	.107	14	58	.72	177	.01	2	.47	.01	.13	1	1
060811	2	79	18	157	.3	56	10	1411	2.67	69	5	ND	1	185	1	2	2	33	3.29	.076	14	30	1.27	136	.01	2	.41	.01	.16	1	5
060812	2	81	9	106	.4	54	8	816	2.20	62	5	ND	1	148	1	4	2	29	2.28	.066	13	32	.62	101	.01	2	.36	.01	.15	1	1
060813	3	109	13	140	1.3	64	11	804	2.40	96	5	ND	3	244	1	4	2	21	2.61	.106	20	27	1.06	123	.01	2	.43	.01	.22	1	4
060814	3	88	11	148	.5	69	10	1207	3.48	126	5	ND	1	246	1	2	2	19	3.81	.107	17	24	1.09	138	.01	6	.49	.01	.21	1	1
060815	2	80	98	463	1.0	43	9	1403	3.53	335	5	ND	1	395	4	8	2	21	3.77	.092	11	20	1.87	86	.01	6	.39	.01	.09	1	225
060816	1	51	9	92	1.0	41	6	1497	2.72	109	5	ND	1	455	1	3	2	17	4.92	.070	9	20	2.49	142	.01	2	.30	.01	.09	1	10
060817	1	120	6	67	.1	140	35	1471	5.25	18	5	ND	1	676	1	2	2	121	6.18	.125	8	217	3.58	281	.01	2	.48	.01	.01	1	5
060818	2	99	6	105	4.7	87	10	1247	3.08	155	5	ND	1	656	1	14	2	18	5.91	.115	10	24	3.16	137	.01	5	.33	.01	.10	1	3
060819	1	74	23	62	2.3	112	21	1221	3.87	339	5	ND	1	1120	1	5	2	28	6.44	.066	5	58	3.47	192	.01	2	.24	.01	.11	1	126
060883	1	84	4	89	.1	36	10	1134	2.05	17	5	ND	1	79	1	2	2	45	1.72	.065	11	44	.63	99	.01	2	.38	.01	.01	1	5
060887	1	74	4	66	.2	28	6	1179	1.90	29	5	ND	1	80	1	4	2	36	2.46	.047	8	32	.92	88	.01	2	.32	.01	.08	1	5
060888	2	76	7	79	.5	40	8	1049	2.48	46	5	ND	1	109	1	10	2	45	2.91	.111	11	54	.83	174	.01	2	.35	.01	.04	1	1
060889	2	66	5	195	.1	43	25	1086	5.44	11	5	ND	1	107	1	4	2	131	1.80	.129	13	24	.89	207	.01	8	.61	.01	.10	1	3
060890	3	31	2	156	.1	23	25	1711	8.80	11	5	ND	1	94	1	2	2	216	1.36	.167	13	20	.34	242	.01	4	.73	.02	.15	1	2
060891	2	83	3	70	.5	35	11	1235	2.42	42	5	ND	3	94	1	4	2	54	1.46	.074	13	44	.67	118	.01	2	.43	.01	.06	1	5
060892	2	74	6	66	.1	41	12	1181	2.43	44	5	ND	2	88	1	2	2	66	1.26	.099	10	48	.52	154	.01	2	.46	.01	.04	1	6
060894	2	75	15	109	.3	47	11	895	2.77	53	5	ND	1	78	1	3	3	43	1.47	.081	15	39	.59	104	.01	3	.47	.02	.01	1	9
060895	2	101	18	121	.6	41	9	1361	2.29	37	5	ND	3	104	1	5	2	50	2.28	.066	16	42	.90	81	.01	2	.58	.01	.04	1	7
060896	3	67	41	133	.9	37	6	1908	2.56	43	5	ND	3	93	1	2	2	41	3.64	.093	13	51	1.42	51	.01	10	.36	.01	.02	1	8
060897	6	99	124	233	1.2	47	7	1388	2.04	38	5	ND	1	82	5	2	2	48	1.95	.110	13	50	.53	63	.01	7	.41	.01	.01	1	31
Hatfield Creek 1	1	796	2461	11	20.5	2	1	202	.46	2	5	ND	1	24	1	2	34	3	.17	.003	2	3	.01	27	.01	2	.02	.01	.01	2	105
2	1	207	528	4	6.5	2	1	38	.34	4	6	ND	1	5	1	2	11	2	.03	.002	2	2	.01	12	.01	5	.02	.03	.02	2	31
3	2	3305	7100	17	62.3	2	1	374	.84	9	5	ND	1	61	2	2	90	6	.62	.003	6	4	.01	211	.01	2	.02	.01	.01	2	660
STD C/AU-R	19	62	38	132	8.1	70	31	1055	4.02	37	22	7	40	53	19	20	21	60	.48	.088	41	61	.96	180	.07	37	1.70	.06	.15	13	485

—Assay required for correct result — Ag > 360 ppm

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Core AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: APR 06 1988 DATE REPORT MAILED: April 18/88 ASSAYER.. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

JAGUAR EQUITIES File # 88-1007 Page 1

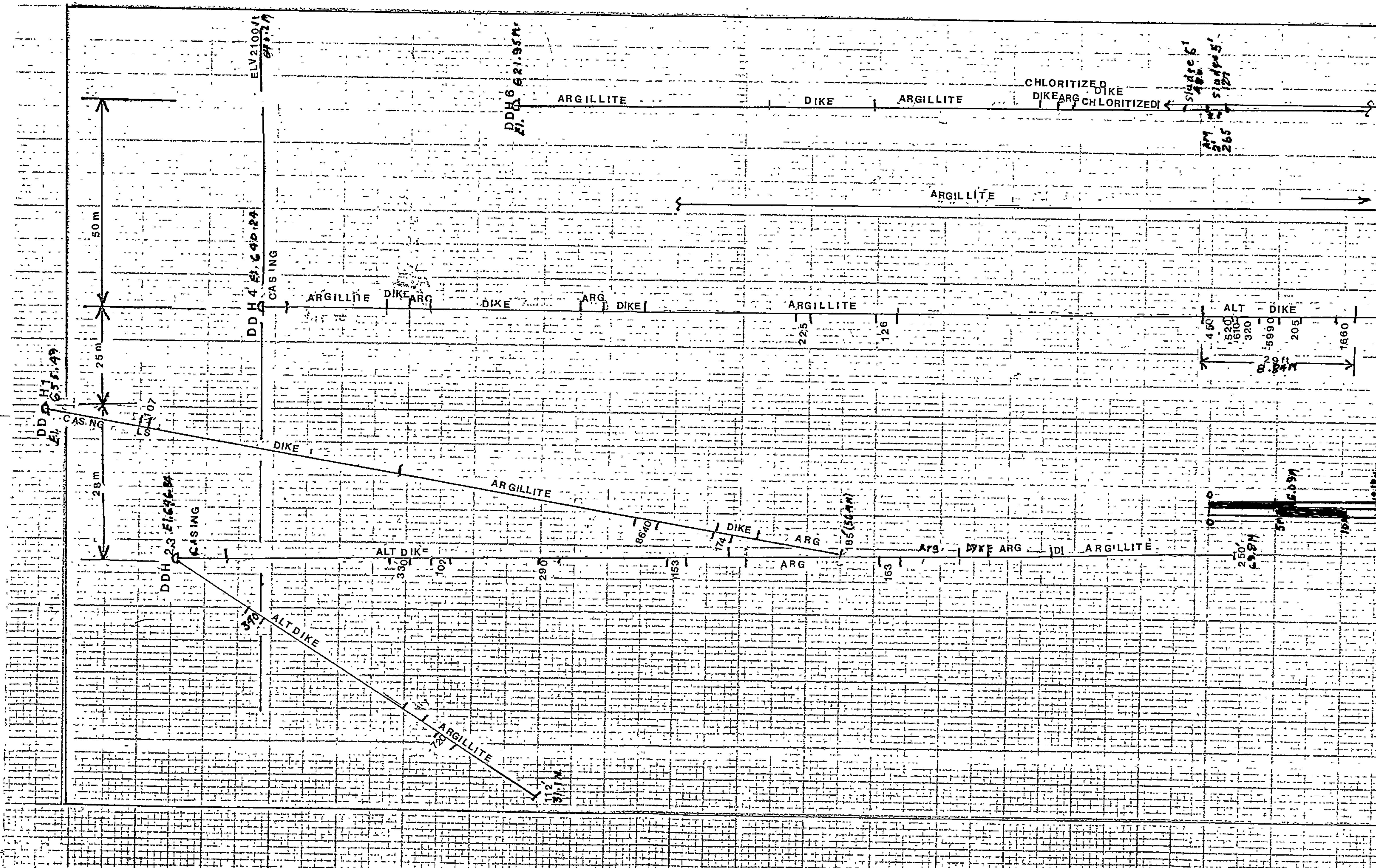
SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
60742	1	44	5	38	.3	8	8	535	2.85	12	5	ND	2	235	1	2	2	50	3.89	.061	11	28	1.05	109	.01	12	.80	.01	.08	2	34
60743	3	52	6	48	.3	31	7	758	2.39	26	5	ND	3	506	1	2	2	44	9.64	.112	12	31	.80	123	.01	8	.64	.01	.07	2	15
60744	2	42	2	52	.4	30	5	1010	1.68	11	5	ND	1	807	1	2	2	30	10.24	.112	11	29	.55	138	.01	12	.38	.01	.05	1	1
60745	10	63	15	60	.6	43	9	690	1.98	28	5	ND	3	410	1	2	2	46	9.06	.113	14	43	.62	110	.01	7	.56	.01	.07	3	41
60746	3	82	7	79	.7	42	10	515	2.67	22	5	ND	3	212	1	2	2	49	4.78	.079	13	39	.52	175	.01	14	.75	.01	.14	1	8
60747	1	31	12	38	.3	9	7	475	2.95	35	5	ND	2	170	1	3	2	49	3.01	.065	13	26	.57	132	.01	7	.70	.01	.09	2	36
60748	3	25	5	33	.1	9	6	500	2.53	20	5	ND	3	170	1	2	2	52	4.12	.062	10	37	.90	61	.01	2	1.10	.01	.08	3	58
60749	18	68	2	46	.3	45	8	359	1.85	2	5	ND	4	88	1	2	2	27	2.83	.092	10	26	.19	96	.09	2	.99	.01	.06	6	1
60751	3	63	21	74	.6	33	6	2242	2.98	36	5	ND	2	230	1	2	2	57	9.99	.070	10	44	.42	104	.01	17	.40	.01	.04	1	9
60752	3	44	7	100	.1	<36	18	1566	5.72	8	5	ND	5	149	1	2	2	97	3.62	.175	37	44	.28	170	.01	5	.69	.01	.03	1	1
60753	2	81	21	76	.6	34	6	1372	2.20	17	5	ND	3	738	1	2	2	41	10.55	.050	11	39	1.96	111	.01	18	.35	.01	.02	1	107
60754	3	90	9	70	.6	39	7	1049	1.82	13	5	ND	3	569	1	2	2	41	9.67	.061	12	32	.95	134	.01	16	.38	.01	.03	1	16
60755	3	57	7	101	.2	30	14	1193	4.37	12	5	ND	4	338	1	2	2	70	7.16	.138	33	23	.51	207	.01	8	.45	.01	.07	1	1
60756	6	103	6	125	.4	118	16	955	2.23	41	5	ND	4	406	1	2	2	69	6.42	.054	16	53	.86	159	.01	11	.46	.01	.03	1	6
60757	3	28	8	114	.1	30	20	1222	5.92	15	5	ND	6	111	1	2	2	98	2.76	.201	53	32	.44	92	.01	10	.96	.01	.06	1	3
60758	3	67	2	76	.4	66	7	1195	2.01	15	5	ND	3	675	1	2	2	51	11.10	.074	13	51	.94	95	.01	9	.35	.01	.02	1	7
60759	7	114	3	94	.5	68	10	1065	2.34	22	5	ND	4	531	1	2	2	57	6.17	.075	15	59	1.43	138	.01	12	.53	.01	.06	1	3
60760	7	54	9	174	.6	50	8	1169	1.88	30	5	ND	4	566	1	3	2	45	8.13	.070	11	53	1.37	145	.01	15	.43	.01	.04	1	1
60761	22	67	4	99	.2	58	8	1388	2.68	18	6	ND	3	1030	1	2	2	55	8.72	.071	11	60	2.86	162	.01	17	.52	.01	.02	1	1
60762	4	114	4	98	.5	98	12	1001	2.47	14	5	ND	4	423	1	2	3	60	6.48	.092	15	73	.77	132	.01	8	.50	.01	.03	1	6
60763	3	48	3	108	.3	76	9	1340	1.90	23	5	ND	4	348	1	2	2	63	9.40	.108	15	65	.49	100	.01	11	.46	.01	.02	1	1
60764	3	118	3	104	.5	99	12	783	2.45	10	5	ND	4	161	1	2	2	53	3.67	.095	16	81	.43	114	.01	15	.62	.01	.05	1	5
60765	3	76	8	112	.5	65	9	1326	2.44	11	5	ND	4	362	1	4	2	49	7.50	.074	13	65	1.06	108	.01	11	.51	.01	.07	1	3
60766	2	62	7	88	.4	50	7	1098	2.25	5	5	ND	3	402	1	2	2	40	6.77	.073	12	52	.91	121	.01	7	.52	.01	.10	1	3
60767	2	87	6	105	.4	58	10	752	2.75	2	5	ND	3	276	1	3	2	40	5.10	.058	13	44	.59	336	.01	7	.53	.01	.07	1	2
60768	1	62	7	111	.5	40	7	1043	2.68	5	5	ND	3	402	1	2	2	24	8.11	.044	11	13	.41	149	.01	2	.59	.01	.13	1	1
60769	2	71	7	75	.6	35	7	611	2.07	3	5	ND	3	209	1	2	2	38	3.80	.058	11	30	.89	105	.01	2	.53	.01	.14	1	2
60770	4	64	11	76	.7	33	6	1014	1.98	33	6	ND	3	434	1	2	2	41	6.46	.059	11	47	1.75	192	.01	13	.52	.01	.09	1	10
60771	1	35	4	51	.4	24	4	1026	2.24	14	5	ND	1	914	1	2	2	30	8.93	.044	8	29	4.07	269	.01	17	.39	.01	.06	1	3
60772	1	46	15	64	.6	25	4	1697	1.82	7	5	ND	2	662	1	2	2	37	11.94	.055	9	35	1.43	170	.01	2	.35	.01	.02	1	1
60773	1	44	10	75	.6	38	6	1445	2.00	8	5	ND	3	501	1	2	2	38	8.77	.053	9	46	1.26	160	.01	7	.39	.01	.06	1	5
60774	1	72	11	107	.8	54	8	1175	2.40	13	5	ND	2	496	1	2	2	43	6.30	.073	13	44	1.55	398	.01	2	.51	.01	.10	1	7
60775	2	77	17	129	.8	65	9	912	2.61	17	5	ND	3	188	1	3	2	34	2.82	.070	14	34	1.07	148	.01	8	.54	.01	.14	1	11
60776	2	61	23	187	1.2	54	8	>1847	3.16	76	5	ND	2	499	2	17	2	27	7.11	.062	9	27	2.86	184	.01	8	.39	.01	.11	1	78
60777	2	82	56	222	4.4	63	8	>2366	3.43	63	5	3	3	587	2	16	2	32	7.84	.100	13	34	3.14	227	.01	4	.47	.01	.12	1	8640
60778	1	52	47	95	1.2	41	7	1186	2.70	69	5	ND	2	272	1	17	2	27	4.46	.074	9	38	1.43	107	.01	2	.40	.01	.12	1	490
STD C/AU-R	19	62	39	132	7.8	72	30	1064	4.20	42	19	8	40	52	19	21	22	60	.50	.091	42	61	.89	180	.07	33	1.92	.06	.14	12	505

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
60779	2	53	12	99	.7	58	9	1916	3.26	44	5	ND	3	322	1	14	2	34	5.67	.098	15	47	2.43	188	.01	8	.48	.01	.15	1	8
60780	2	61	10	95	.8	56	9	1029	2.89	70	5	ND	3	257	1	11	2	22	3.97	.077	12	28	1.79	127	.01	16	.43	.01	.17	1	23
60781	2	55	15	120	.9	47	17	1288	4.57	98	5	ND	3	249	1	12	2	63	3.68	.098	11	25	1.45	259	.01	2	.64	.01	.18	1	174
60782	2	88	8	99	.7	46	11	924	2.61	28	5	ND	3	280	1	9	2	32	3.78	.081	15	39	1.42	183	.01	10	.65	.01	.19	1	15
60783	1	76	69	219	1.0	50	9	1102	2.73	28	5	ND	3	367	4	14	2	31	4.61	.060	10	36	2.00	210	.01	9	.54	.01	.16	1	7
60784	2	61	11	121	1.1	56	8	1136	2.36	65	5	ND	4	317	1	13	3	18	4.29	.071	10	23	2.04	213	.01	11	.41	.01	.12	1	9
60785	4	88	13	161	1.0	59	10	1001	3.26	80	5	ND	3	261	2	14	2	20	3.55	.069	12	23	1.67	190	.01	2	.47	.01	.17	1	14,795
60786	1	48	10	38	.6	10	8	807	3.50	13	5	ND	3	107	1	2	2	41	4.14	.055	12	21	.26	78	.01	4	.55	.01	.07	2	6
60787	2	91	173	44	1.3	10	9	806	3.57	35	5	ND	3	66	1	2	2	42	2.78	.061	12	20	.14	109	.01	2	.53	.01	.08	2	340
60788	1	54	7	44	.5	8	9	807	3.38	24	5	ND	4	194	1	2	2	44	3.89	.061	13	21	.46	99	.01	5	.49	.01	.08	1	37
60789	7	50	6	87	.5	14	7	1157	3.14	22	5	ND	3	810	1	4	2	39	7.63	.061	11	23	2.86	110	.01	11	.59	.01	.07	1	31
60790	3	63	8	31	.3	15	10	821	3.15	8	5	ND	3	257	1	2	2	47	3.70	.066	12	25	.76	118	.01	8	.72	.01	.06	1	15
60791	3	48	9	46	.6	14	11	668	3.98	14	5	ND	3	79	1	2	2	53	2.62	.068	12	25	.14	83	.01	2	.71	.01	.07	1	18
60792	3	70	6	36	.5	11	11	625	3.72	30	5	ND	3	91	1	2	2	54	3.38	.068	12	25	.17	86	.01	7	.73	.01	.08	1	8
60793	9	106	7	42	.4	9	11	661	3.76	17	5	ND	3	147	1	2	2	56	2.95	.065	13	28	.41	103	.01	9	.70	.01	.06	1	21
60794	13	103	6	64	.3	12	11	651	3.57	5	5	ND	4	68	1	2	2	58	2.71	.068	15	27	.15	124	.01	2	.63	.01	.07	1	1
60795	3	119	6	70	.4	15	10	648	3.72	7	5	ND	3	58	1	2	2	55	2.35	.069	11	27	.10	164	.01	2	.66	.01	.06	1	9
60796	5	50	9	56	.4	17	9	745	3.23	30	5	ND	3	123	1	2	2	51	4.16	.070	13	26	.13	157	.01	2	.68	.01	.08	1	35
60797	3	75	10	60	.8	28	7	928	2.34	27	5	ND	3	415	1	2	2	37	12.58	.072	12	24	.09	87	.01	2	.40	.01	.06	1	41
60798	3	33	5	58	.9	22	4	800	1.74	23	5	ND	2	523	1	3	2	29	17.37	.094	9	28	.10	124	.01	11	.33	.01	.03	1	19
60799	3	38	41	68	1.3	34	6	1962	1.85	31	5	ND	2	448	1	2	2	41	10.57	.099	11	29	.38	134	.01	13	.38	.01	.05	1	720
60800	8	36	8	39	.6	17	8	788	2.74	22	5	ND	3	464	1	2	2	40	7.22	.074	11	22	.92	223	.01	11	.57	.01	.10	1	83
60878	2	85	33	117	1.5	42	10	957	2.99	94	5	ND	2	272	1	10	2	29	3.38	.090	9	26	.65	252	.01	8	.51	.01	.14	1	310
60879	2	90	13	116	1.1	67	10	824	2.80	55	5	ND	4	442	1	18	2	32	3.46	.112	12	45	.84	182	.01	15	.62	.01	.18	1	30
60880	1	89	11	127	.8	53	10	1114	2.90	17	5	ND	3	421	1	24	2	40	4.86	.091	12	55	1.66	198	.01	14	.54	.01	.15	1	6
60881	1	90	11	99	.8	49	9	1213	3.04	48	5	ND	2	484	1	19	2	29	5.21	.094	10	39	2.12	203	.01	15	.49	.01	.14	1	1
60882	1	84	9	97	.8	47	9	1181	3.06	90	5	ND	3	436	1	11	2	22	5.24	.082	8	27	1.97	195	.01	17	.44	.01	.14	1	19
60883	1	84	10	99	1.0	58	10	1080	2.87	79	5	ND	3	382	1	16	2	24	4.43	.094	10	32	1.95	164	.01	2	.47	.01	.16	1	1
60884	1	90	10	86	.9	48	9	765	2.89	106	5	ND	3	369	1	15	2	16	3.93	.071	6	19	1.78	156	.01	14	.40	.01	.17	1	3
60885	1	92	9	95	1.0	50	10	798	2.96	143	5	ND	3	337	1	17	3	18	3.53	.065	7	21	1.57	120	.01	2	.43	.01	.16	1	11
61	2	83	17	102	.6	72	10	1499	3.78	32	5	ND	4	255	1	2	2	63	5.18	.090	13	65	.56	116	.01	8	.58	.01	.05	1	15
62	1	113	6	111	.4	83	11	1389	3.63	9	5	ND	4	640	1	2	2	64	6.20	.087	14	84	1.96	172	.01	8	.62	.01	.02	1	2
63	2	109	3	91	.6	78	13	660	2.76	12	5	ND	4	130	1	2	2	49	1.91	.069	12	48	.25	89	.01	3	.67	.01	.03	1	1
64	12	98	3	126	.4	66	11	995	3.15	15	5	ND	4	531	1	2	2	55	5.26	.060	15	66	1.85	130	.01	2	.65	.01	.04	1	5
65	13	48	4	129	.4	56	9	1113	2.25	13	5	ND	3	607	1	2	2	49	8.92	.072	13	65	1.61	123	.01	6	.48	.01	.03	1	68
66	6	80	7	136	.5	61	10	998	2.74	14	5	ND	4	303	1	2	2	59	6.83	.070	15	63	.89	145	.01	4	.55	.01	.02	1	9
STD C/AU-R	18	59	36	132	7.5	70	30	1074	4.04	42	21	8	39	51	18	21	21	61	.48	.086	39	60	.94	181	.07	35	1.80	.06	.13	12	510

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
67	12	62	7	121	.2	66	9	1122	2.72	21	5	ND	4	302	1	2	2	43	8.36	.064	14	61	.77	110	.01	2	.43	.01	.05	1	3
68	5	84	7	90	.5	54	8	854	2.35	23	5	ND	5	387	1	2	2	50	6.82	.082	14	50	1.20	157	.01	5	.53	.01	.06	1	15
69	24	71	33	80	1.1	37	6	933	2.32	19	5	ND	2	374	1	2	2	42	7.12	.063	11	46	1.17	121	.01	4	.51	.01	.08	1	330
70	2	59	8	65	.4	30	5	881	1.72	7	8	ND	3	544	1	2	2	36	12.01	.090	10	38	.96	159	.01	7	.44	.01	.03	1	7
71	4	62	16	73	.9	26	7	763	2.24	31	5	ND	2	474	1	2	3	31	8.83	.076	10	22	.89	184	.01	5	.36	.01	.06	1	102
72	4	39	8	82	.2	28	15	911	3.75	15	5	ND	5	406	1	2	2	61	8.13	.136	32	31	.67	425	.01	2	.53	.01	.07	2	13
73	3	39	12	84	.2	28	13	863	4.39	30	5	ND	4	331	1	2	2	74	7.92	.158	34	34	.12	214	.01	12	.52	.01	.06	1	34
74	4	102	7	103	.4	55	9	789	2.23	12	5	ND	3	476	1	2	2	45	9.16	.093	13	36	.40	146	.01	9	.39	.01	.06	1	5
75	2	91	5	162	.6	49	9	834	2.47	2	5	ND	2	446	1	2	2	50	8.96	.080	10	36	.58	212	.01	2	.40	.01	.06	1	2
76	2	85	238	75	1.9	48	6	1051	2.07	32	6	ND	3	648	1	2	2	40	12.36	.082	11	32	.76	214	.01	8	.42	.01	.07	1	290
77	14	93	2	55	.3	50	6	872	1.82	2	5	ND	3	650	1	2	2	33	12.88	.085	12	30	.46	96	.01	5	.29	.01	.05	1	1
78	2	114	9	76	.4	58	9	640	2.58	11	5	ND	3	465	1	2	2	51	7.88	.092	13	46	.70	152	.01	3	.69	.01	.12	1	3
79	4	68	9	76	.4	46	7	988	1.77	3	5	ND	2	702	1	2	2	30	14.89	.135	10	32	.08	136	.01	2	.46	.01	.06	1	1
80	2	72	6	91	.6	43	7	960	2.09	14	5	ND	2	662	1	2	2	30	13.89	.123	12	27	.08	114	.01	3	.45	.01	.08	1	8
81	2	61	15	118	.2	37	21	1157	6.46	16	5	ND	5	226	1	2	2	96	2.03	.233	47	31	.07	320	.01	12	.81	.01	.05	1	15
82	2	63	31	148	.8	51	9	1404	2.68	27	5	ND	2	138	3	2	2	55	4.71	.151	9	48	.12	319	.01	13	.59	.01	.06	1	153
83	3	94	63	208	1.2	69	10	585	2.17	56	5	ND	2	120	4	18	2	34	2.57	.161	8	51	.07	133	.01	16	.59	.01	.12	1	87
84	4	101	40	181	1.0	86	10	599	2.45	36	5	ND	3	119	2	12	2	38	3.66	.158	7	51	.09	138	.01	14	.58	.01	.12	1	29
85	3	94	16	93	.7	54	8	317	1.65	20	5	ND	2	131	1	15	3	28	1.31	.186	15	44	.05	113	.01	20	.55	.01	.14	1	12
86	1	60	13	64	.4	26	10	681	3.35	30	5	ND	2	56	1	10	2	45	.30	.098	13	31	.05	86	.01	2	.53	.01	.10	1	16
87	1	38	15	61	.3	12	10	513	4.10	19	5	ND	2	77	1	11	2	38	.56	.065	10	24	.05	75	.01	2	.46	.01	.10	1	36
88	2	84	29	88	.9	59	14	1188	3.74	40	5	ND	3	105	1	35	2	61	1.90	.156	15	48	.08	140	.01	15	.55	.01	.12	1	18
89	2	150	22	120	1.0	62	11	691	2.57	197	5	ND	3	135	2	42	3	36	2.44	.135	17	38	.08	197	.01	12	.60	.01	.17	1	41
90	2	84	9	105	.6	54	9	936	2.40	33	5	ND	2	105	1	35	2	33	3.04	.155	11	38	.09	174	.01	18	.54	.01	.15	1	19
91	2	96	12	147	.8	51	9	1033	2.49	102	5	ND	3	107	2	21	2	36	2.95	.135	13	40	.08	141	.01	18	.54	.01	.14	1	13
92	2	70	7	124	.7	61	9	516	1.87	37	5	ND	1	111	1	39	2	29	2.21	.131	5	36	.06	99	.01	19	.51	.01	.12	1	163
93	2	247	14	225	.3	99	21	568	4.15	46	5	ND	2	311	1	30	2	59	.75	.144	18	51	.06	159	.01	15	1.35	.01	.11	1	15
94	2	108	10	141	.6	65	11	927	2.99	17	5	ND	2	93	3	24	3	36	1.57	.091	10	44	.06	115	.01	12	.50	.01	.09	1	4
95	1	88	9	94	.5	47	14	1111	3.77	35	5	ND	2	71	1	15	2	53	1.21	.086	11	51	.06	95	.01	2	.81	.01	.09	1	10
96	1	39	10	90	.2	15	14	705	4.44	5	5	ND	2	52	1	2	2	64	1.19	.076	12	54	.06	86	.01	4	.54	.01	.08	1	6
97	2	28	8	87	.2	19	15	814	3.67	13	5	ND	2	54	1	2	2	60	1.29	.078	12	54	.09	71	.01	2	.55	.01	.08	1	9
98	2	114	14	132	.6	50	11	1015	2.86	58	5	ND	2	170	1	22	2	44	3.17	.098	12	48	.24	166	.01	2	.56	.01	.13	1	14
99	2	79	11	99	.5	43	9	1266	2.79	39	5	ND	2	210	1	13	3	43	4.17	.149	13	43	.15	166	.01	9	.64	.01	.11	1	11
100	1	29	9	130	.1	25	21	1416	7.89	9	5	ND	2	142	1	2	2	201	1.90	.147	11	21	.17	232	.01	2	.86	.01	.16	1	8
STD C/AU-R	20	62	41	132	7.8	72	31	1082	4.30	40	20	8	39	53	20	22	20	60	.51	.092	42	63	.91	180	.07	37	1.98	.06	.14	13	510

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM	AU* PPB
PIT #1 8' 26745	1	24	17	85	.2	22	7	690	2.47	38	5	ND	3	125	1	5	2	34	2.02	.042	8	26	.80	71	.01	2	.44	.01	.10	1	24
PIT #2 6' 26746	1	62	12	56	.6	21	9	625	2.84	21	5	ND	3	164	1	2	2	43	4.13	.072	12	27	.51	121	.01	8	.50	.01	.09	1	42
PIT #3 6' 26747	4	208	1687	86	5.6	40	7	498	2.43	42	5	2	3	234	1	2	2	37	4.83	.065	12	40	.61	199	.01	12	.28	.01	.07	1	4890
✓Select 26748	8	428	10003	201	22.7	28	5	106	5.49	127	5	11	2	73	1	5	7	33	.14	.045	8	29	.03	225	.01	9	.24	.01	.28	1	22400
PIT #3 (Dup). 26749	52	152	1749	1199	3.8	42	6	881	2.40	33	5	ND	2	294	28	2	2	45	7.24	.058	8	57	.90	83	.01	14	.72	.01	.05	1	1465
PDH'3 26750	1	29	43	50	.3	14	9	575	2.96	61	5	ND	2	101	1	7	2	45	.71	.079	11	24	.05	79	.01	14	.50	.01	.08	1	25
145-176 STD C/AU-R	19	60	39	133	6.8	71	31	1095	4.16	39	19	8	40	53	20	16	18	60	.49	.089	41	60	.98	180	.07	37	1.82	.06	.14	13	500

BIT #3 + HILLS
PIT #4



ELV 2100 ft
DDH 6
ARGILLITE
DIKE
ARGILLITE
CHLORITIZED DIKE
CHLORITIZED
ARGILLITE
50 m
DDH 4
CASING
ARGILLITE
DIKE
ARG
DIKE
ARG
DIKE
ARGILLITE
ALT DIKE
29 ft
25 m
DDH 1
CASING
LS
DIKE
ARGILLITE
DIKE
ARG
28 m
DDH 23
CASING
ALT DIKE
ARG
ARG
DIKE
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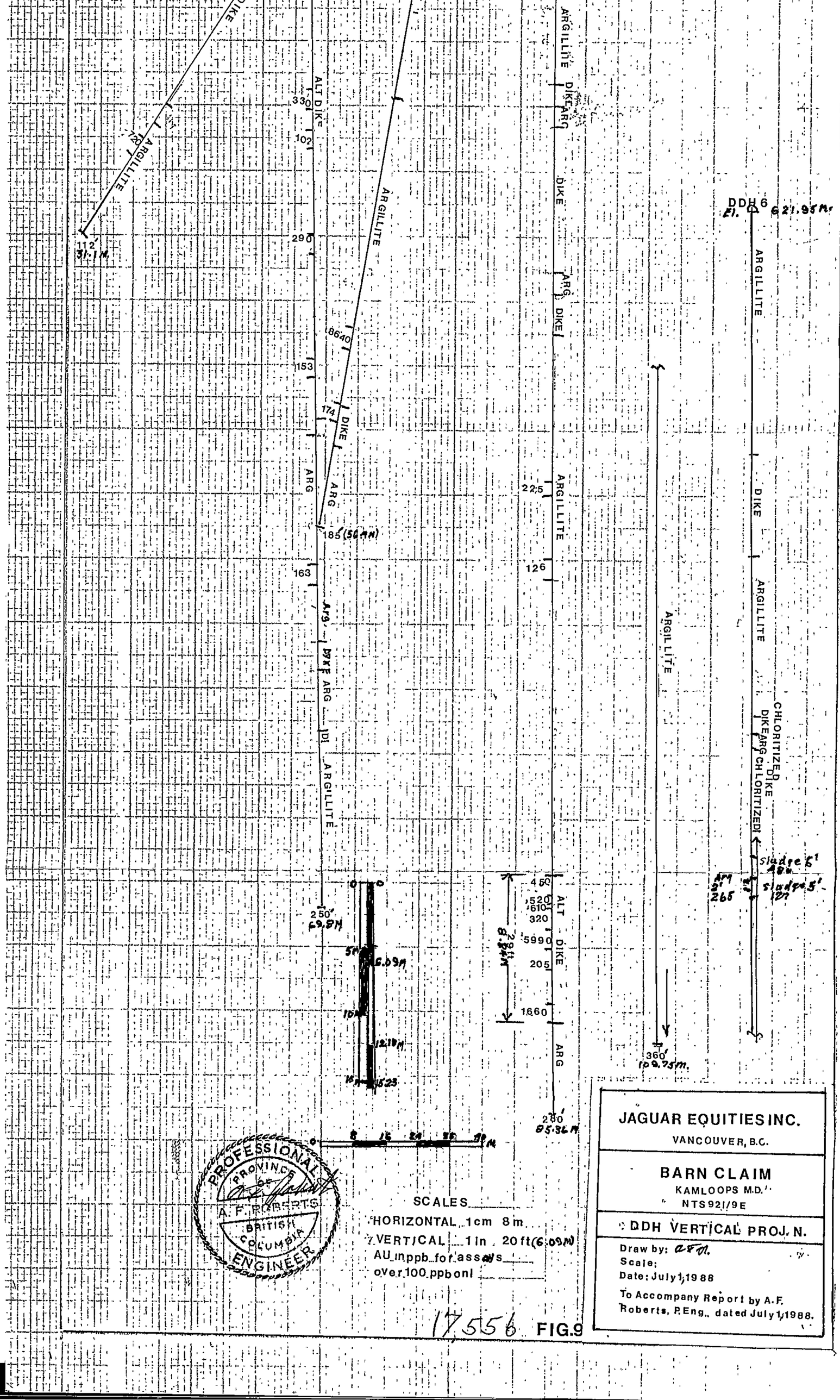

JAGUAR EQUITIES INC.
VANCOUVER, B.C.

BARN CLAIM
KAMLOOPS M.D.
NTS 92I/9E

DDH VERTICAL PROJ. N.

Drawn by: A.F.R.
Scale:
Date: July 1, 1988

To Accompany Report by A.F. Roberts, P.Eng., dated July 1, 1988.

17556 FIG. 9