ARIS SUMMARY SHEET

District Geologist, Kamloops   Off Confidential: 89.06.24

ASSESSMENT REPORT 17815   MINING DIVISION: Greenwood

PROPERTY: Sailor
LOCATION: LAT 49 06 36   LONG 119 11 24
UTM 11 5441774 340171
NTS 082E03E
CLAIM(S): Minnie Ha-Ha,Sailor,Diamond,Toledo,Snowshoe,Rover Fr.,Cariboo Fr.
Kamloops
OPERATOR(S): Nexus Res.
AUTHOR(S): Walker, J.E.
REPORT YEAR: 1988, 41 Pages
COMMODITIES
SEARCHED FOR: Gold,Silver,Copper,Lead,Zinc
GEOLOGICAL
SUMMARY: Late Permian to Early Triassic Anarchist Group rocks host quartz veins along an east trending fracture set. Mineralization consists of free gold with minor pyrite, sphalerite, galena, and chalcopyrite. Grades of up to 119 grams per tonne gold have been noted.
WORK
DONE: Physical,Geochemical
LINE 13.5 km
ROCK 31 sample(s) ;ME
Map(s) - 1; Scale(s) - 1:2000
SOIL 206 sample(s) ;ME
Map(s) - 6; Scale(s) - 1:2000
RELATED
REPORTS: 08153,09840
MINFILE: 082ESW045,082ESW046

CAMP MCKINNEY PROJECT 1988

ASSESSMENT REPORT
ON SOIL GEOCHEMICAL AND
ROCK SAMPLE SURVEYS OF
SAILOR CLAIM GROUP

GREENWOOD MINING DIVISION, BRITISH COLUMBIA

Claims:	Sailor, Minnie-Ha-Ha, Kamloops, Toledo, Diamond Rover Fr., Cariboo Fr., Snow Shoe
Total Claim Units:	8
Owner And Operator:	Nexus Resource Corporation
Location:	Greenwood Mining Division NTS: 82E/3E Latitude: 49°06' Longitude: 119°11' Bridesville Area South-Central British Columbia
Field Work:	June 10 - 22, 1988
By:	James E. Walker

TABLE OF CONTENTS

SUMMARY

In 1988, Nexus Resource Corporation conducted a two week exploration program on its Camp McKinney Property. The program was designed to assess the property's current state of development and to determine the feasibility of using soil geochemistry as an exploration tool in this area.

The property consists of 8 reverted crown grants. It has easy access by good gravel road. The area containing the claim block is of low relief. Vegetation is largely immature pine and spruce.

The area has a long mining history, dating back to the 1860's. The Cariboo-Amelia mine was the main producer in this camp with total production of 83,320 oz of gold and 21,860 oz of silver from 136,793 tons of ore mined between 1894 and 1963. The gold and silver occurs in a vein striking east-west and dipping vertically. The Nexus property is located some 300 metres south of the mine.

The geology present on the property is dominately Anarchist Group, a mainly meta-sedimentary sequence of Upper Permian or Triassic age. Gold mineralization occurs in east-west striking quartz vein systems which contain pyrite, galena, sphalerite, chalcopyrite and free gold. These veins vary in thickness from 30 cm to 120 cm in surface exposure.

Work conducted by Nexus in 1988 involved establishing 13.46 km of grid, and collecting 206 soil samples and 31 rock samples.

The soil survey delineated several anomalies which could indiate the strike projections of the vein between the Sailor and Minnie-Ha-Ha occurrences. Rock sampling of the dumps produced grab samples from the Sailor dump grading up to 073 oz/t Au and from the Minnie-Ha-Ha grading up to 3.47 oz/t Au.

A further work program is recommended for this property. It is estimated to cost $41,000. and take 7 weeks to complete.

INTRODUCTION

A. PURPOSE:

The purpose of this report is to relate the results of a two week program in June, 1988 designed as an initial evaluation of the Camp McKinney claims (Sailor Claim Group) 100% owned by Nexus Resource Corporation. The program was designed to examine the old workings on the property and provide a reference grid through which surveys done eight years previous could be related to any new work done. As well, soil samples were taken over the strike projections of the main quartz vein to determine its position.

B. LOCATION, ACCESS, TOPOGRAPHY AND VEGETATION:

The Camp McKinney property is located 21.5 km ENE of Osoyoos, British Columbia and is within the Greenwood Mining Division (N.T.S. 82E/3E).

The property is accessed by a good gravel road maintained for year-round use. The turnoff for this road is 3.0 km east of Bridesville. It follows the McKinney and Rice Creek watersheds to the ski resort on Baldy Mountain. The McKinney property is located about 7 km southeast of the resort. Portions of the claim block straddle this road.

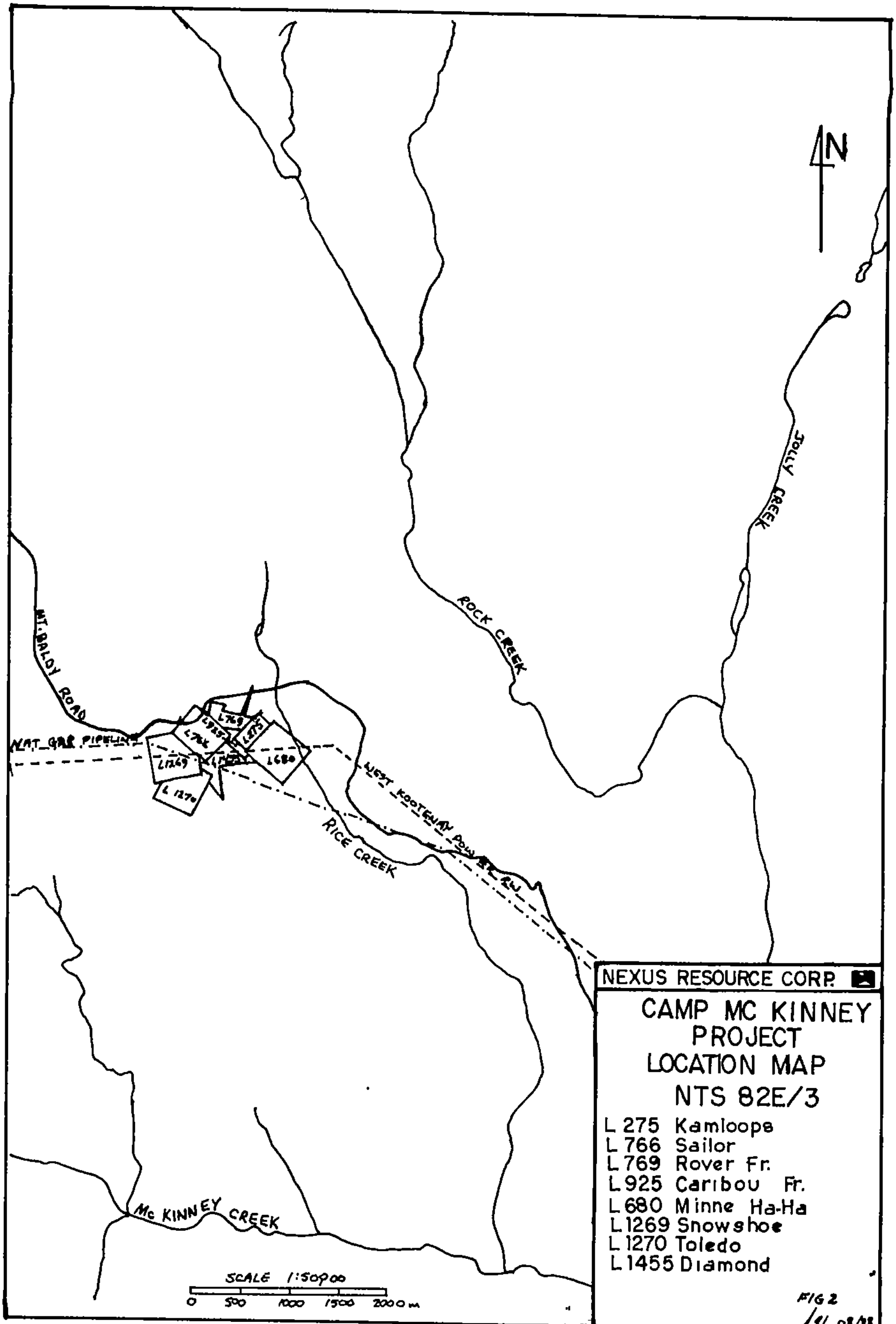
Within the claim block there are several access roads. Several access the Hydro lines or gas pipeline which cross the claims. These are maintained in a driveable condition for two or four wheel drive trucks.

Lodging is available in the town of Osoyoos or Rock Creek. Approximately 35 minutes is required for access from Osoyoos. Rock Creek is somewhat closer, but service facilities there are limited.

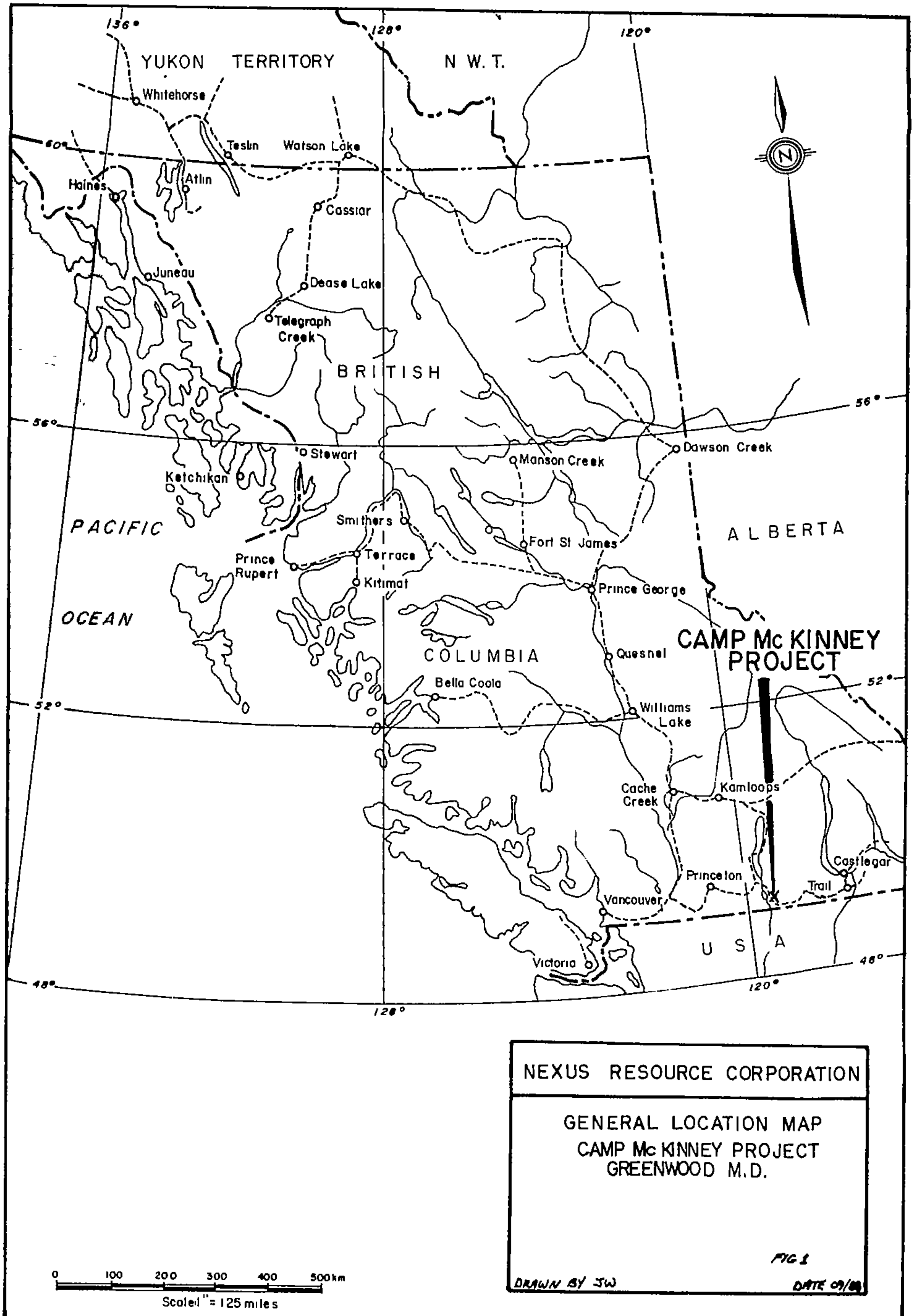
Camp McKinney is located in a area of relatively flat terrain in the Okanagan Highland, a plateau region with an average elevation of 1,300m. The claims are located between 1,280m and 1,340m elevation.

The area of the claim block is primarily second growth pine and spruce. A fire in 1932 burned most of the mature timber stands in the area. Consequently, certain portions of the claim block are covered by closely spaced trees under 10 cm in diametre.

Climate varies widely in the region around the claims. Over the interval of 20 km from Osoyoos to the claim blocks, annual rainfall varies from less than 20 cm to approximately 50 cm. Accumulations of snow can be expected in the area from November to early April.



N
JOLLY CREEK
ROCK CREEK
MT. BALDY ROAD
NAT. GAS PIPELINE
WEST KOOTENAY POWER R/W
RICE CREEK
L769
L766
L925
L1269
L 1270
L680
Mc KINNEY CREEK
SCALE 1:50000
0 500 1000 1500 2000 m
NEXUS RESOURCE CORP.
CAMP MC KINNEY PROJECT
LOCATION MAP
NTS 82E/3
L 275 Kamloops
L 766 Sailor
L 769 Rover Fr.
L 925 Caribou Fr.
L 680 Minne Ha-Ha
L 1269 Snowshoe
L 1270 Toledo
L 1455 Diamond
FIG 2



136°
128°
120°
YUKON TERRITORY
N. W. T.
Whitehorse
Teslin
Watson Lake
60°
Haines
Atlin
Cassiar
Juneau
Dease Lake
Telegraph Creek
BRITISH
56°
Stewart
Dawson Creek
Manson Creek
Ketchikan
PACIFIC
Smithers
ALBERTA
Fort St James
Prince Rupert
Terrace
Kitimat
Prince George
OCEAN
CAMP Mc KINNEY PROJECT
COLUMBIA
Quesnel
Bella Coola
52°
Williams Lake
Cache Creek
Kamloops
Castlegar
Princeton
Trail
Vancouver
U S A
Victoria
48°
NEXUS RESOURCE CORPORATION
GENERAL LOCATION MAP
CAMP Mc KINNEY PROJECT
GREENWOOD M.D.
FIG 1
0 100 200 300 400 500 km
Scale 1" = 125 miles
DRAWN BY JW
DATE 09/8

C. CLAIM INFORMATION:

The Sailor Group of claims is 100% owned by Nexus Resource Corporation. The Minnie-Ha-Ha claim is subject to a 10% net profit interest payable to Lode Resource Corporation, the former owner of the claim.

Claim	Record Number	Units	Date Recorded	Expiry Date*
Minnie-Ha-Ha	1620	1	June 27/79	06/95
Sailor	1621	1	June 27/79	06/94
Diamond	1622	1	June 27/79	06/93
Toledo	1623	1	June 27/79	06/93
Snowshoe	1624	1	June 27/79	06/93
Rover Fr.	1662	1	July 3/79	07/94
Cariboo Fr.	1663	1	July 3/79	07/94
Kamloops	1664	1	July 3/79	07/94

* Includes assessment work filed with this report.

D. EXPLORATION HISTORY:

Placer gold was mined from the Camp McKinney area from the early 1860's onward. Lode gold was first discovered in 1884 and the Cariboo-Amelia mine commenced operations in 1894. The Cariboo-Amelia mine operated until 1903 producing 123,457 tons at an average grade of 0.563 oz/ton gold and 0.052 oz/ton silver. Total profits in these years was $565,588. In 1940, the Cariboo-Amelia mine was reactivated and 2,044 tons of ore were mined until its closure in 1946. Average grade over this period was 0.850 oz/ton gold. The final production of the Cariboo-Amelia mine to date was in the years 1960-1962. Production totalled 11,292 tons grading 1.06 oz/ton gold and 1.26 oz/ton silver. Total production from 1894 to 1963 was 136,793 tons with an average grade of 0.61 oz/ton gold and 0.16 oz/ton silver. In total ounces, gold production was 83,320 oz. and silver production was 21,886 oz.

The Cariboo-Amelia mine produced all of its ore from a single vein, the Cariboo vein. This vein strikes roughly east-west and dips steeply south. The vein is highly transected by faults and shears. It generally varies between 0.9m and 2.4m, but thicknesses to 4.6m have been recorded.

Nexus Resource Corporation first acquired the Sailor Group in 1980. During that year, a VLF-EM and a magnetometer survey were conducted over the property. The survey was not particularly effective due to interference from the powerline and gas pipeline.

In 1981, Sawyer Consultants conducted a soil geochemistry and mapping project over the claims. Over 1,000 samples were collected, but they were only analyzed for lead and zinc. Only small spotty anomalies were located, possibly due to cultural contaminents.

GEOLOGY

A. INTRODUCTION:

The Camp McKinney area has been the subject of government surveys by W. E. Cockfield in 1935 and M. S. Hedley in 1940. A summary of the geology of the Camp McKinney area extracted from these two reports is presented below.

B. LITHOLOGY:

The Camp McKinney area is predominately underlain by rocks of the Anarchist Series, a package of greenstones, quartzites, amphibolites and limestones. In general, these rock types are complexly interbedded making stratigraphic correlations relatively ifficult over even short distances.

The greenstones are andesitic in composition. Most appear to be sedimentary in origin. They are often interlaminated with original carbonate layers. In some areas, the greenstone is massive and appears to be of igneous origin. The exact nature of their origin is not certain.

Quartzites are fine-grained, light grey rocks. They are finely laminated with dark laminae composed largely of biotite representing original bedding planes. These quartzites contain varying quantities of argillaceous material. Some contain over 50% argillaceous material; and others have only thin partings of biotite as meta-argillites.

Southeast of the property occurs a large intrusion composed of granodiorite which has a width of over 3 km and a northwesterly-trend.

C. STRUCTURE:

In general, most meta-sediments on the property have a southeasterly strike and a northeasterly dip. Some evidence of tight folding was encountered on the property as well.

Cross faulting of the vein appears to be important in the area. In the Cariboo-Amelia mine, many of the problems encountered during mining involved fault offsets of the quartz vein. Apparent northerly offsets in the main vein from east to west may be a result of cross faulting. Faults are difficult to observe directly on surface but geochemical patterns may help to identify these offsets.

D. MINERALIZATION:

On the Sailor group, gold mineralization has been identified in one main quartz vein. The vein occurs along an old fault or joint set, and has a general strike and dip of about $115^0/80^0$ NE. Widths of the quartz vein are inferred from float and observed in place to vary from less than 30 cm to about 120 cm.

Most quartz vein specimens with high grade have from 1-2% galena and sphalerite. Pyrite is also present in quantities between 2% and 5%. Free gold occurs locally as very fine specks in quartz. It may also occur in a pyrite matrix.

In the Sailor dump there are considerable quantities of a carbonate altered rock bearing some mariposite and possibly some annabergite. This rock contains anomalous quantities of nickel and chromium which may yield a distinct geochemical signature, producing high nickel, chromium and arsenic values in soil samples.

1988 EXPLORATION PROGRAM

A. INTRODUCTION:

Twenty-nine man days were spent on the Sailor property from June 9 - 22, 1988. During this period, both a rock chip sample program and a soil sample program were conducted.

To provide control points for subsequent surveys, 13.46 km of flagged grid was established using hip chain and compass. The grid was established with a baseline 1,500 metres long having crosslines at 50 metre intervals. Stations were established at 15 metre intervals on the crosslines. The base map was produced from old survey notes and location of cultural features during gridding.

Rock chip samples were taken of mineralized quartz vein material in from any workings found, and their dumps. These samples were analyzed using ICP techniques for 30 elements with a further analyses for gold performed using a fire assay with an AA "finish". A total of 31 samples were taken.

A total of 206 soil samples were taken from areas within the grid along strike projections from the Minnie-Ha-Ha and Sailor workings. Samples were taken all of good B horizon material. The soil samples were analyzed using ICP techniques for 30 elements. Gold analyses were accomplished by an acid digestion with an AA "finish".

B. ROCK SAMPLING SURVEY:

The program of rock sampling and prospecting was undertaken with the purpose of determining nature and quantity of mineralization associated with old workings for which only limited information is available.

A total of 31 rock samples were taken and analyzed. Listed below are the most significant results:

SAMPLE	ANALYSES	LOCATION
8801	3635 ppb Au; 148 ppm Cu, 121 ppm Zn and 106 ppm Ni	Minnie-Ha-Ha, Main Dump
8803	119,060 ppb Au, 459 ppm Cu, 6,377 ppm Pb, 1,697 ppm Zn and 30.0 ppm Ag	Minnie-Ha-Ha, Main Dump
8804	6,526 ppb Au, 193 ppm Zn	Minnie-Ha-Ha, Main Dump
8806	4,684 ppb Au, 147 ppm Cu, 308 ppm Pb, 671 ppm Zn and 3.3 ppm Ag	Vein at Minnie-Ha-Ha Main Shaft
8807	24,930 ppb Au, 9,533 ppm Pb, 1,569 ppm Zn and 19.7 ppm Ag	Sailor, Main Dump
8820	1,256 ppb Au and 1,035 ppm Pb	Sailor, Main Dump

The main mode of significant gold mineralization is a quartz vein up to 1m wide with accessory calcite in veinlets and chloritic partings. In close association with this vein are zones of mariposite-sericite-quartz-carbonate alteration.

The quartz veins may contain galena, chalcopyrite, sphalerite and native gold. These minerals are typically present in quantities of less than 1%, as fine widely disseminated grains. The sphalerite is very fine grained and honey colored. Pyrite is also present, often in quantities of up to 5%.

In carbonate alteration surrounding the vein, traces of arsenopyrite may be present.

Seven workings located had only low background concentrations of gold. Commonly these workings were not located on quartz veins at all, but on quartz "sweats" or on silicified limestones. Examples of this kind of working are found at 200W 215N, 200W 270N, 650W 360S and 130W BLO. Other similar workings probably exist.

Of the most economic potential are the Sailor and Minnie-Ha-Ha shafts. Development work exceeded 100m of drifts on three levels from a shaft extending 53m deep on the Sailor shaft and over 180m of drifts on three levels extending to a depth of 61m on the Minnie-Ha-Ha shaft. The dumps surrounding these workings are of considerable size. Samples taken from these dumps produced analyses as high as 3.47 oz/ton calculated from geochemical data from the Minnie-Ha-Ha dump and 0.73 oz/ton from the Sailor dump. The workings are inaccessible in both cases due to caving of the tops of the shafts. At the Minnie-Ha-Ha shaft, the quartz vein is exposed at the collar. The width of the exposure is 30 cm and a channel sample taken across this width returned a value of 0.137 oz/ton gold (calculated from geochemical data). Free gold was identified in one sample taken at the Minnie-Ha-Ha dump. (Sample CM8803 with 3.47 oz/ton Au).

C. <u>SOIL GEOCHEMISTRY SURVEY:</u>

The purpose of the soil geochemistry survey was to cover the area between known workings in order to determine the extent of the mineralized quartz vein as well as its characteristic geochemical signature for use as a prospecting tool elsewhere.

A total of 206 samples were collected at 15m x 50m intervals and analyzed for 30 elements by ICP and for gold by acid digestion with an AA "finish". Probability plots were prepared for copper, lead, zinc, arsenic and gold. The following analytical values were determined as anomalous for the following elements:

Element	Average Value (ppm)	Standard Deviation (ppm)	Possibly Anomalous (ppm)	Anomalous (ppm)
Cu	24.5	32.75	44.0	90.0
Pb	14.75	9.63	26.5	34.0
Zn	80	88.0	135	256
As	7	21.5	215	500
Au	3 ppb	51.5 ppb	14 ppb	106 ppb

Three significant anomalous zones were defined by the survey. Zone A is a one line anomaly located between L450W 105N and L450W 150N which is associated with the Sailor shaft. The highest values in soil for gold, copper, lead, zinc, arsenic and chromium are found here. There is a possibility that high values in this area are actually caused by contamination from waste rock at the shaft.

Zone B is located between 350W 150N and 250W 120N. Anomalous levels of copper, lead and zinc are found in this zone. Possibly anomalous values for gold are also present in this area.

Zone C, the third geochemically anomalous area, occurs in the area of the Minnie-Ha-Ha shaft. The area directly over the shaft does not show any anomalous values. This is likely due to the thick layer of barren waste material from the shaft. Samples taken from 0+15N to 0+45S on line 0+00W were taken off of this dump, and it is reasonable to assume that any surface anomaly would be masked by the waste pile.

D. INTEGRATION WITH PREVIOUS SURVEYS:

In May and June of 1980, Glen E. White Geophysical Consulting and Services conducted a magnetometer and VLF-EM survey on the Sailor Group.

The VLF-EM survey conducted at that time produced a weak VLF anomaly which ran from the western edge of the Sailor claim to the western edge of the Kamloops claim along a strike of 97 . The base map produced for this survey did not show shaft locations, however, plotting the shaft location on the Sailor claim relative to the claim boundaries shows a coincidence between the anomaly and the shaft. Unfortunately, there are errors in the 1980 base map, mainly in the claim boundaries. The claim outlines which are the most distorted on the 1980 map are the Rover Fr., the Cariboo Fr., the Diamond, and the Toledo. These errors cause difficulties in further integrating the old data.

Similar problems crop up in trying to integrate 1981 soil sample grid with the 1988 work as the grid and base map used in 1980 and 1981 use the same base map. Also, the soil sampling performed in 1981 does not have anomaly patterns which closely resemble those delineated in 1988.

RECOMMENDATIONS

Results of the 1988 work program on the Camp McKinney Project were, in general, encouraging. Samples of quartz vein material recovered from the dumps at the Sailor and Minnie-Ha-Ha shaft produced grades of gold in excess of 0.5 oz/ton. Soil sampling identified three small anomalous features which could serve as targets for an immediate trenching program.

Recommended for the Camp McKinney Project is a program designed to operate in several stages with a modest first stage, leading to greater expenditures contingent upon results.

Stage I should involve the completion of the grid over the remainder of the property. Soil samples should be taken at 15m x 50m intervals. The property should be mapped in detail, with particular attention paid to structural offsets in the stratigraphy in the Minnie-Ha-Ha and Sailor areas. VLF-EM and magnetometer surveys should be done at a 15m spacing. Stage I should require about 3 weeks to complete for a two man crew and cost about $25,000.

Stage II of the program should begin with about 250m of trenching around the Minnie-Ha-Ha and Sailor shafts and in the area of soil anomaly "B". Contingent on results, this program can be expanded to provide the necessary surface definition to define a series of diamond drilling targets. Stage II would require about 4 weeks and cost $16,000.

Stage III would involve diamond drilling of selected targets developed during Stages I and II. No more than 1,000m of drilling should be contemplated for the first round of drilling.

It should be stressed that later stages contemplated for this property should be made contingent on results from prior programs. The Camp McKinney area is structurally very complex and the key to any successful program of mineral exploration in this area will be the understanding of this puzzle.

Respectfully Submitted

James E. Walker

CERTIFICATE

I, James Walker, of Vancouver, British Columbia, hereby declare that:

1. I am currently in the employ of Nexus Resource Corporation.

2. I hold a Bachelor of Science degree majoring in geology from the University of British Columbia.

3. I have practiced in the field of mineral exploration both prior and post gaduation since 1984.

James E. Walker, B.Sc.

20/09/88
Date

STATEMENT OF EXPENDITURES

Personnel

G. Benvenuto, Exploration Manager	
2 Days @ $250./day	$ 500.00
J. Walker, Geologist	
14 Days @ $115./day	$1,610.00
T. Baines, Assistant	
13 Days @ $115./day	$1,495.00
	$3,605.00

Accommodation

Room - 25 Man Days @ $18.58/Man Day	$ 464.50
Board - 26 Man Days @ $23.46/Man Day	$ 609.96
	$1,074.46

Transportation

4WD Truck - 14 Days @ $30.75/Day	$ 430.50
Fuel And Oil	$ 241.29
	$ 671.79

Supplies

$ 138.50

Analyses

31 Rock Samples @ $15.25	$ 472.75
206 Soil Samples @ $11.60	$2,389.60
	$2,862.35

Report

Geologist - 5 Days	$ 115.00
Draftsman - 4 Days	$ 115.00
Reproduction	$ 250.00
Typing	$ 100.00
	$ 580.00

TOTAL: $8,932.10

PROPOSED BUDGET
STAGE I

Objective: Complete soil sampling grid over property, conduct VLF-EM and magnetometer survey over grid and geologically map property at 1:1000 scale.

Personnel:		
Geologist	20 man days @ $120/day	$ 2,400.00
Soil Samplers	30 man days @ $90/day	$ 2,700.00
Geophysical Technicians	10 man days @ $90/day	$ 900.00
		$ 6,000.00
Accommodation:		
Room	60 man days @ $25/day	$ 1,500.00
Board	60 man days @ $25/day	$ 1,500.00
		$ 3,000.00
Transportation:		
4WD Truck	20 days @ $30.75/day	$ 615.00
Fuel and Oil		$ 345.00
		$ 960.00
Supplies:		$ 200.00
Analyses:		
100 Rock Samples @ $15.25		$ 1,525.00
550 Soil Samples @ $11.60		$ 6,380.00
		$ 7,905.00
Instrument Rental:		
VLF and Magnetometer		$ 400.00
Report:		
Geologist	15 days @ $120/day	$ 1,800.00
Draftsman	10 days @ $120/day	$ 1,200.00
Reproduction		$ 300.00
Typing		$ 100.00
		$ 3,400.00
Contingency:	15% of Field Costs	$ 2,935.00
TOTAL COST:		$24,800.00

PROPOSED BUDGET STAGE II

Objective: Locate and trench suitable zones near old workings and soil/geophysical anomalies.

Personnel:		
Geologist	30 man days @ $120/day	$ 3,600.00
Accommodations:		
Room	30 man days @ $25/day	$ 750.00
Board	30 man days @ $25/day	$ 750.00
		$ 1,500.00
Transportation:		
4 x 4 Truck	30 days @ $30.75/day	$ 922.00
Fuel and Oil		$ 518.00
		$ 1,440.00
Analyses:		
200 Samples @ $15.25		$ 3,050.00
Excavation:		
375 metres @ $6/metre		$ 2,250.00
Contingencies: At 15% of Field Costs		$ 1,776.00
Report:		
Geologist	15 man days @ $120/day	$ 1,800.00
Drafting	10 days @ $120/day	$ 1,200.00
Reproduction		$ 400.00
Typing		$ 100.00
		$ 3,500.00
TOTAL COST:		$15,340.00

TOTAL COST FOR PHASE I AND II APPROXIMATELY: $40,200.00

APPENDIX III

ROCK SAMPLE DESCRIPTIONS

SAMPLE NO.	DESCRIPTION	SELECTED ANALYSES Au(ppb)	Other(ppm)
CM8801	Quartz, vein float on Minnie-Ha-Ha shaft dump. Inferred width of 15 cm. Weak, chloritic partings. Traces of sphalerite present in quartz. Pyrite occurs as selvages. Host rock is massive greenstone.	3635	148 Cu 121 Zn 106 Ni
CM8802	Chlorite sericite schist with thin laminations to 0.5 cm. Alternate lamina are composed of semi massive pyrite with interstitial chlorite. Pyrite comprises 15% of total rock volume. Traces of chalcopyrite present. Calcite occurs in fracture filling. Rock weathers to dark orange-brown color. Sample taken from dump at Minnie-Ha-Ha shaft.	112	502 Cu 111 Zn 1.0 Ag 106 Ni
CM8803	Greenstone with quartz carbonate veining. Abundant disseminated galena with traces of chalcopyrite and sphalerite. Two specks of free gold visible. Float from Minnie-Ha-Ha dump.	119,060	459 Cu 6377 Pb 1697 Zn 30.0 Ag
CM8804	Quartz vein containing 5% blebs of coarse grained pyrite up to 1 cm in size. Also containing up to 10% chlorite as "clasts" up to 2 cm in size. Traces of sphalerite are present from Minnie-Ha-Ha dump.	6526	193 Zn
CM8805	Greenstone with quartz carbonate veining. Traces of pyrite and galena. From Minnie-Ha-Ha dump.	235	

SAMPLE NO.	DESCRIPTION	SELECTED ANALYSES Au(ppb)	Other(ppm)
CM8806	Quartz vein from Minnie-Ha-Ha shaft. Vein has width of 30 cm and attitude $116^0/81^0$ N. Footwall portion of vein is primarily white bull quartz with no visible sulphide mineralization present. Hangwall has chloritic partings and disseminated pyrite (5%), sphalerite (.5%), galena (trace) and chalcopyrite (trace). Chip sample across 30cm.	4684	147 Cu 308 Pb 671 Zn 3.3 Ag
CM8807	Representative chip sample from quartz dump at shaft on Sailor claim. Quartz material contains abundant pyrite with minor associated sphalerite and galena. Mineralization primarily confined to selvages. Sample weathers crimson red.	24,930	9533 Pb 1569 Zn 19.7 Ag
CM8808R	Epidote, sericite, quartz alteration in greenstone at Kamloops main shaft. Contains approximately 2% pyrite and traces of galena.	98	
CM8809	Fine to medium grained green intrusive rock with color index indicating andesitic composition. Pervasive disseminated fine grained pyrite.	42	
CM8810R	Quartz vein, in place, on secondary shaft at Kamloops claim. Contains substantial (15%) boxwork voids. Weathers rusty orange. Vein approximately 20 cm thick.	88	
CM8811R	Fine grained, med. gray, highly siliceous tuff with approximately 5% pyrite. Has strike of 22^0.	7	211 Cu
CM8812R	Bull quartz from dump at shallow shaft on Minnie-Ha-Ha claim. Sample has no visible sulphide minerals.	1	

SAMPLE NO.	DESCRIPTION	SELECTED ANALYSES Au(ppb)	Other(ppm)
CM8813R	Banded quartzite from shaft at 200W,60N on Kamloops claim. Bands alternate between light and dark. Minor carbonate alteration.	1	
CM8814R	Milky quartz from Sailor dump. Vein material has chloritic partings. Has 5% sulphides, total volume. Principle sulphide minerals are pyrite (3%), galena (1.5%) and sphalerite (0.5%).	179	298 Pb 133 Zn 1.7 Ag
CM8815	Dark gray to white banded recrystallized limestone. Contains about 0.5% pyrite. Located on dump at small shaft on line 200W,195N.	7	
CM8816	Milky to vitreous quartz with traces of galena (<0.5%). Occurs in shear zone with attitude of 006° / 74°W located near BLO, 3+75E. Trench is 5m long 1.5m wide. Vein has width of 20 cm.	6	
CM8817	Fine grained, medium green basaltic? tuff. Contains about 2-5% pyrite. Located in bed of Rice Creek at 3+50E, 0+40S.	3	
CM8818	Chip sample across quartz float at secondary shaft, Kamloops claim (100W, 045N). Quartz is locally vuggy (boxwork). No remaining unweathered sulphides are present.	205	
CM8819	Quartz float at (1+35N, 2+50W). No visible sulphide mineralization.	1	
CM8820	Composite sample of quartz dump at Sailor shaft. Dump contains both high sulphide and low sulphide quartz. Vein width appears to vary between 50 cm and 1m.	1256	1035 Pb

SAMPLE NO.	DESCRIPTION	SELECTED ANALYSES Au(ppb)	Other(ppm)
CM8822	Fuchsite-sericite-quartz-carbonate alteration in dump at Sailor shaft. Rock is highly altered, original rock type not discernable.	4	571 Ni 143 Cr 467 As
CM8828	Quartz vein in massive green meta-sandstone at 4+75E, 0+30N. Vein is 20 cm thick.	10	
CM8830	Representative random sample of quartz material from dump at Minnie-Ha-Ha shaft.	2273	
CM8832	Silicified wall rock from 1+95W, 0+40N. Sample is originally inferred to be quartzite. Contains trace amounts of pyrite and sphalerite. Rock has very thin chloritic partings.	104	
CM8834	Quartz-carbonate altered boulder. No remnant textures. Minimum dimension 26 cm.	13	
CM8836	Iron stained quartz veinlet 4 cm thick in float near shaft at (2+08W, 0+53N). Silicified quartzite is host rock.	2	
CM8838	Altered limestone with alternating light and dark layers from trench at 2+60W, 0+90N.	1	
CM8840	Chip sample across quartz float 23 cm in width at 2+40W, 1+40N. Quartz appears barren.	1	
CM8842	Argillaceous quartzite from dump the shaft at 250W, 230N.	1	

SAMPLE NO.	DESCRIPTION	SELECTED ANALYSES Au(ppb)	Other(ppm)
CM8844R	Quartz vein 15 cm thick in shear on south side of small creek at (200E, 1+55S).	1	
CM8846	Andradite garnet-mica schist from small glory hole on line 650W, 355S.	1	

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

[redacted]

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P6 SOIL P7 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JUN 23 1988 DATE REPORT MAILED: June 30/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

NEXUS RESOURCES CORP. PROJECT-CM88 File # 88-2186 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
CM88L550W 210N	1	16	18	98	.1	38	10	467	2.38	4	5	ND	4	22	1	2	2	40	.24	.146	11	52	.44	145	.10	4	2.13	.02	.09	1	6
CM88L550W 195N	1	9	12	76	.1	34	8	606	2.11	4	5	ND	4	29	1	2	2	35	.35	.108	9	46	.40	200	.09	2	1.49	.02	.11	1	5
CM88L550W 180N	1	9	10	49	.3	37	9	188	1.92	9	5	ND	3	29	1	4	2	33	.35	.021	10	32	.35	111	.10	4	1.91	.02	.13	1	1
CM88L550W 165N	1	30	14	63	.2	69	14	393	2.80	10	7	ND	6	39	1	2	3	49	.45	.017	23	74	.68	165	.14	7	2.32	.02	.11	1	4
CM88L550W 150N	1	20	13	58	.1	46	11	231	2.45	6	5	ND	3	21	1	2	-2	40	.24	.061	12	50	.51	131	.11	2	2.20	.02	.09	1	2
CM88L550W 135N	1	15	18	47	.1	31	8	165	2.20	9	5	ND	5	18	1	2	2	41	.19	.025	8	24	.37	91	.11	2	1.68	.02	.07	1	1
CM88L550W 120N	1	30	11	28	.1	31	6	279	1.66	6	5	ND	1	45	1	2	2	27	.62	.022	13	18	.29	156	.08	2	1.81	.03	.07	1	2
CM88L550W 105N	1	28	5	13	.1	12	1	49	.61	2	5	ND	1	31	1	3	2	14	.48	.016	9	6	.10	73	.04	8	.58	.04	.05	1	1
CM88L550W 45N	1	16	10	83	.1	67	18	131	2.71	7	5	ND	1	12	1	4	2	63	.19	.014	8	119	1.21	76	.12	6	1.67	.02	.06	1	2
CM88L500W 195N	1	14	20	103	.1	31	10	474	2.08	4	5	ND	3	16	1	2	4	36	.16	.130	8	38	.39	150	.10	4	1.66	.02	.09	1	1
CM88L500W 180N	1	17	10	59	.1	40	10	277	2.34	5	5	ND	1	22	1	2	2	39	.27	.058	9	45	.46	116	.10	7	2.05	.02	.11	1	1
CM88L500W 165N	1	16	11	35	.2	40	7	270	1.68	6	7	ND	3	39	1	2	2	30	.60	.020	9	28	.37	102	.08	4	1.46	.02	.07	1	1
CM88L500W 150N	1	36	10	35	.1	42	8	181	1.85	9	5	ND	3	38	1	2	2	31	.43	.023	16	23	.39	177	.09	6	1.98	.03	.10	1	1
CM88L500W 105N	1	37	11	47	.1	31	8	197	1.71	2	5	ND	1	46	1	2	2	29	1.11	.041	25	24	.35	184	.08	9	1.78	.03	.10	2	1
CM88L500W 75N	1	18	16	50	.1	31	11	215	2.35	4	5	ND	3	21	1	2	2	43	.25	.073	10	34	.54	107	.11	8	1.77	.02	.13	1	1
CM88L500W 60N	1	9	10	39	.2	14	6	170	1.66	5	5	ND	3	14	1	2	2	29	.19	.087	6	17	.23	103	.09	9	1.70	.02	.07	1	1
CM88L500W 45N	1	13	11	39	.1	27	7	174	2.13	5	5	ND	10	17	1	2	2	38	.20	.109	8	35	.35	103	.10	5	1.88	.02	.08	1	1
CM88L450W 195N	1	25	21	63	.2	48	10	361	2.50	6	5	ND	5	28	1	2	2	46	.33	.093	24	69	.61	133	.10	5	1.88	.02	.12	1	1
CM88L450W 180N	1	16	6	14	.1	8	3	88	.91	2	5	ND	1	70	1	4	4	19	1.45	.016	6	10	.11	114	.05	8	.55	.02	.06	1	2
CM88L450W 165N	1	19	22	41	.1	23	5	319	1.19	6	5	ND	1	101	1	3	2	21	1.99	.056	12	15	.25	129	.05	13	1.13	.02	.07	1	3
CM88L450W 150N	3	123	764	713	3.0	337	49	1016	7.06	221	7	ND	3	132	12	2	2	140	2.95	.084	9	404	4.04	49	.02	7	3.25	.01	.09	1	1050
CM88L450W 135N	33	211	28	216	.9	190	45	1365	6.51	76	5	ND	5	164	1	2	2	108	4.98	.140	12	133	1.82	69	.02	7	1.90	.01	.08	1	41
CM88L450W 120N	9	88	234	432	1.1	307	41	713	4.59	216	5	ND	1	144	5	2	2	36	1.68	.057	5	115	2.39	31	.01	15	1.29	.01	.06	1	310
CM88L450W 105N	1	19	63	194	.4	29	8	678	2.11	16	5	ND	3	11	1	6	2	34	.12	.068	6	40	.31	103	.08	2	.93	.02	.05	2	131
CM88L450W 0+90N	1	16	20	55	.1	45	13	191	2.72	7	5	ND	5	22	1	2	2	51	.29	.024	14	63	.63	100	.14	8	2.19	.02	.08	1	6
CM88L450W 0+75N	1	16	13	52	.1	56	16	230	2.97	10	5	ND	6	26	1	2	3	54	.40	.029	16	71	.72	131	.15	2	2.55	.02	.12	1	4
CM88L450W 0+60N	1	9	12	48	.1	37	8	340	2.35	6	5	ND	3	16	1	2	4	39	.23	.118	9	50	.46	139	.10	7	1.96	.02	.15	1	7
CM88L450W 0+45N	1	13	9	59	.1	37	9	260	2.40	6	5	ND	2	15	1	2	4	40	.22	.102	9	51	.48	141	.11	2	2.06	.02	.08	1	12
CM88L400W 0+195N	1	47	13	97	.2	71	17	444	3.42	6	5	ND	6	29	1	2	2	63	.31	.152	21	85	.96	203	.15	12	2.96	.02	.25	1	7
CM88L400W 0+180N	1	42	23	67	.4	80	15	495	2.57	31	5	ND	3	48	1	5	2	43	.53	.085	22	67	.62	158	.09	2	1.92	.02	.14	1	27
CM88L400W 0+165N	1	18	7	23	.2	23	7	209	1.41	3	5	ND	1	43	1	3	2	24	.64	.026	11	15	.22	103	.07	2	1.43	.02	.07	1	3
CM88L400W 0-150N	1	9	12	56	.1	13	6	105	1.69	2	5	ND	3	15	1	4	4	28	.15	.122	5	18	.20	78	.09	2	1.47	.02	.04	1	2
CM88L400W 0+135N	1	19	11	43	.5	33	9	246	2.17	2	5	ND	4	74	1	3	2	34	1.19	.024	16	36	.42	140	.09	7	2.04	.03	.10	1	1
CM88L400W 0+120N	1	20	13	137	.2	61	16	243	3.09	9	5	ND	11	21	1	3	2	55	.25	.073	14	79	.71	124	.14	14	2.72	.02	.09	1	310
CM88L400W 0+105N	1	14	17	126	.1	43	12	646	2.67	5	5	ND	6	19	1	3	2	46	.23	.162	12	63	.60	143	.11	2	2.15	.02	.08	1	5
CM88L400W 0+90N	1	12	9	54	.2	41	11	185	2.66	2	5	ND	6	16	1	3	4	44	.19	.100	10	56	.50	96	.12	2	2.45	.02	.10	1	1
STD C/AU-S	18	57	38	132	6.7	70	30	1091	4.03	41	14	8	37	48	18	17	19	59	.46	.082	41	59	.94	180	.07	33	1.95	.07	.14	13	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
CM88L400W 75N	1	21	13	57	.1	44	11	216	2.77	8	5	ND	3	16	1	2	3	46	.21	.091	11	57	.53	107	.13	9	2.72	.02	.10	1	1
CM88L400W 60N	1	19	12	55	.1	38	10	233	2.47	6	9	ND	5	15	1	2	2	45	.22	.083	10	55	.55	99	.11	13	1.95	.02	.10	1	1
CM88L400W 45N	1	30	21	80	.1	62	16	422	3.21	5	5	ND	6	18	1	2	2	57	.28	.092	11	86	.91	136	.14	14	2.96	.02	.14	1	5
CM88L400W 30N	1	26	14	31	.1	59	17	623	3.03	7	5	ND	1	14	1	2	4	51	.24	.147	9	77	.80	134	.12	10	2.56	.02	.13	1	6
CM88L350W 180N	1	21	18	73	.1	38	9	171	2.19	6	5	ND	13	39	1	2	2	35	.56	.024	8	28	.41	142	.12	4	2.24	.02	.11	1	1
CM88L350W 165N	1	46	13	58	.1	85	13	395	2.40	7	5	ND	2	50	1	2	2	35	.72	.028	8	44	.57	181	.11	11	2.13	.03	.16	1	9
CM88L350W 150N	1	63	27	128	.3	224	43	1853	6.10	53	5	ND	2	51	1	2	4	126	1.26	.162	15	393	3.09	263	.15	13	3.22	.01	.84	1	6
CM88L350W 135N	1	32	10	126	.1	90	21	239	3.20	8	5	ND	4	22	1	2	2	72	.34	.018	10	150	1.38	125	.19	3	2.22	.02	.13	2	38
CM88L350W 120N	1	32	16	119	.3	56	15	436	2.94	8	5	ND	6	20	1	2	4	52	.27	.132	14	73	.77	176	.12	5	2.60	.02	.14	1	12
CM88L350W 105N	1	18	11	76	.2	44	10	381	2.43	5	5	ND	5	19	1	2	2	42	.22	.132	9	54	.53	129	.11	2	2.06	.02	.12	1	3
CM88L350W 95N	1	20	14	66	.4	47	11	472	2.66	4	5	ND	5	17	1	2	3	45	.26	.128	9	60	.57	138	.11	2	2.20	.02	.12	1	4
CM88L350W 80N	1	21	12	80	.1	48	12	467	2.64	8	5	ND	3	15	1	2	2	44	.20	.135	9	61	.58	105	.11	12	2.43	.02	.11	1	3
CM88L350W 60N	1	29	11	70	.1	57	16	305	3.01	6	5	ND	4	19	1	2	2	50	.28	.129	10	71	.68	153	.12	10	2.83	.03	.13	1	1
CM88L350W 45N	1	21	10	61	.1	44	12	268	2.55	9	5	ND	1	16	1	2	4	40	.29	.219	7	59	.55	124	.11	12	2.50	.03	.11	1	1
CM88L350W 30N	1	67	10	29	.2	125	10	362	1.94	8	5	2	1	36	1	2	3	34	.59	.026	15	73	.53	217	.09	10	1.91	.03	.10	1	2
CM88L350W 30NA	1	31	10	54	.1	57	13	687	2.64	3	5	ND	1	25	1	2	2	52	.53	.045	12	79	.84	143	.13	6	1.83	.03	.17	1	17
CM88L350W 15N	1	21	11	43	.1	39	8	214	2.19	3	6	ND	3	27	1	2	4	37	.49	.057	12	51	.50	120	.10	10	1.88	.03	.12	1	4
CM88L350W 00N	1	23	10	38	.1	75	8	311	1.95	7	5	ND	1	29	1	2	2	32	.41	.129	10	55	.44	178	.08	11	1.79	.02	.10	1	2
CM88L300W 180N	1	54	27	255	.6	215	30	517	5.90	15	5	ND	2	57	1	2	2	120	1.24	.051	10	351	3.25	283	.24	6	4.44	.02	.41	1	1
CM88L300W 165N	1	28	11	200	.1	75	20	701	2.65	12	5	ND	3	35	1	2	3	38	.36	.283	7	64	.58	306	.10	9	2.29	.02	.12	1	2
CM88L300W 150N	1	54	17	257	.3	81	28	981	3.85	6	5	ND	2	37	1	2	5	60	.63	.179	5	129	.95	260	.11	6	2.47	.02	.28	1	1
CM88L300W 135N	1	55	19	204	.1	46	22	939	4.08	3	5	ND	1	31	1	2	2	79	.48	.124	5	63	1.17	215	.14	2	2.84	.02	.35	1	69
CM88L300W 120N	1	36	14	114	.2	75	19	462	3.47	7	5	ND	6	33	1	2	2	65	.51	.032	15	103	1.00	214	.14	6	2.17	.02	.16	1	3
CM88L300W 105N	1	30	17	134	.3	69	16	683	2.93	10	5	ND	5	21	1	2	5	50	.29	.120	11	80	.81	157	.11	12	2.25	.03	.13	1	2
CM88L300W 90N	1	25	9	106	.1	56	15	592	2.88	7	5	ND	4	21	1	2	6	49	.29	.163	9	76	.74	183	.12	6	2.20	.02	.11	1	1
CM88L300W 75N	1	28	16	60	.1	57	14	268	2.91	8	5	ND	3	18	1	2	2	50	.29	.099	8	81	.73	132	.13	4	2.76	.03	.09	1	2
CM88L300W 60N	1	25	13	58	.4	60	10	389	2.26	6	8	ND	4	14	1	2	2	37	.22	.127	8	66	.54	145	.10	3	2.02	.03	.09	1	2
CM88L300W 45N	1	26	13	29	.1	69	9	408	2.05	4	5	ND	2	29	1	2	4	34	.58	.025	13	71	.55	149	.10	5	1.98	.03	.10	1	2
CM88L300W 15N	1	90	11	46	.5	201	14	330	2.41	18	10	ND	7	42	1	3	2	40	.65	.023	23	107	.74	195	.11	10	2.27	.03	.10	1	3
CM88L300W 00N	1	28	9	99	.1	121	17	413	2.68	16	5	ND	2	17	1	2	3	46	.20	.209	9	153	.99	146	.10	8	2.75	.02	.09	1	1
CM88L250W 165N	1	32	9	21	.1	24	5	155	1.36	2	5	ND	1	37	1	2	2	27	.51	.016	11	24	.23	134	.07	4	.98	.03	.11	1	1
CM88L250W 150N	1	25	10	92	.3	95	21	270	3.36	6	5	ND	1	21	1	2	2	62	.46	.075	5	199	1.64	164	.16	2	2.45	.02	.26	1	1
CM88L250W 135N	1	62	15	83	.2	107	20	252	3.89	9	5	ND	3	24	1	2	2	92	.39	.058	10	161	1.68	277	.20	6	2.87	.02	.33	1	1
CM88L250W 120N	1	96	17	148	.3	228	38	389	5.94	2	5	ND	3	23	1	2	2	101	.74	.151	9	437	3.68	395	.23	7	4.58	.02	.43	1	2
CM88L250W 105N	1	47	17	265	.5	152	32	538	5.58	8	5	ND	4	26	1	2	2	111	.55	.242	13	271	2.58	295	.15	2	3.93	.02	.17	1	2
CM88L250W 90N	1	34	11	120	.1	78	18	464	3.06	6	5	ND	2	27	1	2	2	53	.42	.090	13	109	.93	173	.12	4	2.16	.03	.14	1	12
STD C/AU-S	18	63	42	132	6.8	72	29	1038	4.04	42	16	8	38	48	18	16	24	59	.46	.086	41	59	.95	181	.07	30	1.94	.07	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
CM88L250W 75N	1	26	15	104	.3	66	16	795	2.81	5	5	ND	5	22	1	2	2	45	.31	.150	11	92	.80	144	.10	2	2.18	.02	.11	1	1
CM88L250W 60N	1	33	15	101	.1	122	22	479	3.60	10	5	ND	5	25	1	2	2	58	.42	.170	9	160	1.41	266	.13	6	2.85	.02	.25	1	3
CM88L250W 45N	1	25	12	77	.4	142	15	257	2.61	13	5	ND	6	33	1	2	2	44	.51	.037	12	117	.91	156	.12	3	2.41	.02	.17	1	1
CM88L250W 30N	1	21	15	52	.1	89	11	224	2.34	8	5	ND	4	20	1	2	2	36	.34	.051	7	106	.66	127	.10	2	1.93	.02	.08	1	5
CM88L250W 15N	1	26	14	70	.1	111	17	247	2.67	11	5	ND	6	17	1	2	2	43	.29	.101	10	137	.93	156	.11	9	2.65	.02	.08	1	5
CM88L250W 00N	1	22	19	82	.2	89	17	308	2.87	9	5	ND	3	17	1	2	4	49	.27	.087	10	112	.85	141	.12	6	2.60	.02	.12	1	4
CM88L250W 15S	1	28	15	75	.1	88	19	375	3.05	6	5	ND	4	17	1	2	2	55	.33	.062	13	154	1.38	175	.15	2	2.01	.01	.16	1	62
CM88L200W 1+50N	1	19	17	114	.3	49	12	222	2.57	9	6	ND	12	17	1	2	2	38	.20	.115	8	45	.48	141	.11	6	3.11	.02	.11	1	2
CM88L200W 1+35N	1	15	15	124	.2	48	11	190	2.62	9	5	ND	3	16	1	5	3	41	.16	.073	5	49	.49	129	.12	6	2.82	.02	.13	1	1
CM88L200W 1+20N	1	17	20	157	.1	38	12	253	2.52	7	5	ND	4	17	1	2	2	41	.19	.159	6	47	.45	113	.12	5	2.63	.02	.08	1	2
CM88L200W 1+05N	1	37	13	75	.2	62	11	200	2.45	5	5	ND	6	31	1	2	6	35	.41	.016	22	45	.53	159	.13	4	2.78	.02	.10	1	2
CM88L200W 0+90N	1	37	14	127	.2	96	20	435	3.22	9	5	ND	6	16	1	2	2	57	.23	.110	9	120	1.03	163	.14	4	3.41	.02	.14	1	10
CM88L200W 0+75N	1	35	17	116	.3	105	18	366	3.13	26	5	ND	4	22	1	2	2	53	.26	.129	10	129	1.05	189	.13	3	2.90	.02	.14	2	24
CM88L200W 0+60N	1	42	15	122	.1	99	20	459	3.07	20	5	ND	5	22	1	2	2	52	.29	.084	22	101	.89	200	.13	5	2.88	.02	.13	1	1
CM88L200W 0+45N	1	37	22	237	.4	95	20	1228	3.56	22	5	ND	4	20	1	2	2	64	.22	.223	10	114	.97	267	.12	10	3.05	.02	.07	3	2
CM88L200W 0+30N	1	29	15	197	.1	44	11	1225	2.20	12	5	ND	2	28	1	2	3	36	.32	.217	8	45	.42	265	.08	7	1.90	.02	.05	1	8
CM88L200W 0+15N	1	28	14	82	.1	67	13	401	2.70	7	5	ND	4	32	1	2	2	46	.36	.158	18	103	.82	182	.10	9	2.06	.02	.12	1	1
CM88L200W 0+00N	1	31	15	79	.1	120	18	219	3.11	12	5	ND	3	23	1	2	2	52	.32	.109	9	118	.91	210	.13	10	3.06	.02	.13	1	18
CM88L200W 0+15S	1	20	15	93	.1	62	10	440	2.38	10	5	ND	3	20	1	2	2	39	.20	.159	10	71	.54	181	.10	3	2.48	.02	.09	1	2
CM88L200W 0+30S	1	25	13	115	.2	54	9	766	2.48	11	5	ND	5	22	1	3	2	40	.20	.233	11	63	.55	224	.10	3	2.51	.01	.12	1	1
CM88L1+50W 1+05N	1	27	19	94	.1	70	20	172	3.20	7	5	ND	8	32	1	2	2	54	.42	.018	13	73	.80	170	.16	10	3.15	.02	.08	1	1
CM88L1+50W 0+90N	1	26	9	99	.1	70	16	288	2.93	9	5	ND	5	17	1	2	2	48	.21	.158	10	101	.83	125	.12	8	2.38	.02	.11	1	2
CM88L1+50W 0+75N	1	26	9	74	.4	70	12	484	2.55	6	5	ND	5	16	1	2	2	43	.22	.099	8	98	.81	173	.11	5	2.20	.02	.09	1	25
CM88L1+50W 0+60N	1	31	16	94	.2	116	20	313	3.24	12	5	ND	12	19	1	2	2	57	.26	.129	11	155	1.29	188	.13	15	2.58	.02	.14	1	55
CM88L1+50W 0+45N	1	28	10	96	.3	85	16	506	3.00	5	5	ND	5	23	1	2	4	52	.32	.071	9	122	1.10	237	.12	8	2.22	.02	.20	1	1
CM88L1+50W 0+30N	1	28	16	132	.1	65	14	825	2.62	3	5	ND	2	30	1	2	2	43	.36	.116	10	81	.77	205	.10	7	2.26	.02	.14	1	1
CM88L1+50W 0+15N	1	28	16	140	.5	83	19	477	2.94	10	5	ND	5	24	1	2	2	50	.35	.076	13	149	1.08	202	.12	13	2.31	.02	.11	1	1
CM88L1+50W 0+00N	1	22	12	97	.4	69	12	465	2.34	3	5	ND	5	21	1	2	2	38	.23	.115	9	108	.75	209	.09	7	1.93	.01	.13	1	1
CM88L1+50W 0+15S	1	32	10	86	.4	70	10	345	2.55	6	5	ND	5	23	1	2	2	43	.22	.095	14	87	.74	195	.10	2	2.25	.01	.18	1	2
CM88L1+50W 0+30S	1	21	12	80	.3	57	9	370	2.40	6	5	ND	4	24	1	2	2	37	.23	.105	8	64	.57	248	.09	5	2.13	.01	.13	1	2
CM88L1+50W 0+45S	1	26	13	90	.1	57	10	396	2.57	8	5	ND	5	22	1	2	2	40	.25	.096	13	61	.57	206	.11	11	2.58	.02	.14	1	2
CM88L1+50W 0+60S	1	26	17	88	.2	58	9	477	2.44	8	5	ND	5	29	1	4	2	35	.32	.179	10	56	.49	337	.09	5	2.25	.02	.13	1	13
CM88L1+00W 1+20N	1	23	14	68	.4	53	18	147	3.00	10	5	ND	9	20	1	5	2	50	.25	.038	7	52	.59	106	.14	9	3.07	.02	.10	1	2
CM88L1+00W 1+05N	1	21	16	76	.2	58	15	153	2.71	8	5	ND	6	34	1	4	2	42	.44	.016	15	55	.60	159	.13	5	2.87	.02	.10	2	1
CM88L1+00W 0+90N	1	28	23	118	.4	87	19	187	3.19	37	5	ND	9	26	1	2	2	55	.34	.023	11	90	.87	157	.12	14	2.73	.02	.09	1	18
CM88L1+00W 0+75N	1	84	22	124	.1	158	25	450	4.67	24	5	ND	1	34	1	2	2	84	.59	.030	13	183	1.70	217	.16	3	2.88	.02	.55	1	14
STD C/AU-S	18	59	39	130	6.8	73	30	1029	3.98	40	19	7	37	47	18	16	18	58	.46	.080	40	58	.93	178	.07	34	1.96	.06	.14	12	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
CM88L1+00W 0+60N	1	38	13	85	.2	120	18	242	2.86	17	5	ND	2	42	1	2	2	43	.71	.016	11	70	.76	154	.11	6	2.30	.03	.06	1	10
CM88L1+0CW 0+45N	1	29	16	129	.2	83	20	325	3.08	12	5	ND	2	30	1	2	2	58	.42	.030	10	91	1.00	161	.12	10	2.59	.02	.07	1	34
CM88L1+00W 0+30N	1	32	40	227	.1	58	17	796	3.74	9	5	ND	1	27	1	2	2	52	.27	.264	12	57	.62	250	.09	5	2.44	.03	.08	1	152
CM88L1+00W 0+15N	1	31	12	134	.1	85	15	543	2.63	5	5	ND	3	27	1	2	7	45	.39	.084	12	71	.77	146	.12	9	2.80	.03	.06	1	1
CM88L1+00W 0+00N	1	42	13	133	.1	124	22	710	2.84	2	5	ND	1	48	1	2	4	51	.97	.039	12	114	1.10	193	.13	9	2.08	.03	.17	1	4
CM88L1+00W 0+15S	1	28	17	120	.3	53	11	300	2.61	6	5	ND	5	31	1	2	2	45	.42	.084	20	73	.64	153	.11	7	2.17	.02	.10	1	1
CM88L1+00W 0+30S	1	19	10	103	.3	53	10	507	2.43	2	5	ND	7	23	1	2	4	38	.24	.189	15	63	.59	222	.09	7	2.01	.02	.08	1	59
CM88L1+00W 0+45S	1	16	10	92	.2	49	9	520	2.27	3	5	ND	5	25	1	2	2	36	.22	.251	12	66	.51	243	.08	4	2.04	.02	.09	1	1
CM88L1+00W 0+60S	1	18	13	52	.1	55	8	242	2.34	7	5	ND	4	23	1	2	2	36	.27	.061	12	62	.47	205	.10	2	2.42	.02	.08	1	1
CM88L0+50W 1+05N	1	27	14	51	.1	45	11	185	2.43	16	5	ND	1	20	1	2	2	38	.30	.018	7	39	.44	82	.10	4	2.03	.02	.08	1	5
CM88L0+50W 0+90N	1	32	51	274	.1	89	18	510	4.44	264	5	ND	3	24	1	3	2	44	.24	.112	8	52	.67	153	.10	7	2.00	.02	.08	2	101
CM88L0+50W 0+75N	1	28	23	163	.1	74	20	526	3.48	98	5	ND	5	19	1	2	2	57	.19	.220	10	94	1.00	176	.12	9	2.85	.02	.10	1	17
CM88L0+50W 0+60N	1	31	20	103	.1	71	16	475	3.00	17	5	ND	8	24	1	2	2	53	.29	.148	14	82	.84	147	.11	11	2.44	.02	.12	1	1
CM88L0+50W 0+45N	1	23	13	93	.1	57	10	349	2.80	9	5	ND	3	21	1	2	3	49	.23	.118	14	65	.66	229	.12	11	2.53	.02	.10	1	1
CM88L0+50W 0+30N	1	12	10	67	.1	49	11	230	2.51	2	5	ND	2	18	1	2	3	49	.26	.020	8	71	.74	84	.14	2	1.93	.01	.09	1	14
CM88L0+50W 0+15N	1	39	14	61	.6	68	10	189	2.38	5	9	ND	4	30	1	2	2	36	.48	.012	15	53	.51	115	.11	10	1.93	.03	.08	2	4
CM88L0+50W 0+00N	1	96	20	92	.1	194	19	610	3.25	10	5	ND	8	43	1	2	2	46	.57	.013	20	82	.78	272	.15	3	3.46	.03	.19	1	4
CM88L0+50W 0+15S	1	191	16	71	.6	200	17	727	2.84	15	5	ND	5	43	1	2	4	43	.66	.013	37	75	.70	215	.13	10	2.84	.03	.15	1	3
CM88L0+50W 0+30S	1	34	72	138	.4	67	16	370	3.11	14	5	ND	7	30	1	4	2	56	.33	.065	23	93	.93	157	.12	6	1.95	.02	.27	1	163
CM88L0+50W 0+60S	1	28	11	67	.4	51	12	238	2.60	4	5	ND	4	31	1	2	2	46	.41	.040	18	78	.76	162	.12	6	2.04	.02	.08	1	1
CM88L0+50W 0+75S	1	32	16	100	.1	61	15	393	2.78	6	5	ND	4	20	1	2	2	45	.28	.098	14	82	.82	166	.12	9	2.54	.02	.09	1	3
CM88L0+00E 0+75N	1	26	12	74	.1	60	15	314	2.79	33	5	ND	7	22	1	2	2	49	.22	.124	12	59	.62	166	.11	8	2.31	.02	.10	1	3
CM88L0+00E 0+60N	1	17	13	73	.1	39	9	305	2.57	14	5	ND	6	18	1	2	2	43	.18	.130	12	48	.46	121	.11	6	2.15	.02	.08	1	1
CM88L0+00E 0+45N	1	22	12	81	.4	67	13	353	2.71	8	8	ND	7	20	1	2	2	48	.22	.107	14	78	.72	162	.12	4	2.48	.02	.10	1	1
CM88L0+00E 0+30N	1	21	6	66	.1	48	9	363	2.40	4	5	ND	8	21	1	3	2	42	.22	.123	16	65	.59	149	.10	8	1.95	.02	.11	1	2
CM88L0+00E 0+15N	1	16	11	62	.1	33	8	343	2.23	6	5	ND	8	21	1	6	4	39	.20	.120	13	40	.42	120	.10	11	1.84	.02	.07	1	1
CM88L0+00E 0+00N	1	43	18	78	.1	90	18	557	3.75	5	5	ND	8	58	1	2	5	72	.60	.115	39	154	1.60	198	.14	6	2.01	.02	.41	1	4
CM88L0+00E 0+15S	1	7	6	75	.1	34	7	632	1.77	2	5	ND	2	25	1	3	3	32	.25	.093	9	47	.45	136	.09	12	1.28	.02	.08	1	1
CM88L0+00E 0+30S	1	10	10	67	.3	42	8	335	2.16	2	8	ND	3	17	1	4	4	38	.21	.080	10	70	.62	93	.10	3	1.29	.02	.10	2	3
CM88L0+00E 0+45S	1	28	10	97	.1	88	18	355	3.25	2	5	ND	4	28	1	2	3	55	.29	.079	13	123	1.09	215	.14	7	2.69	.02	.19	1	1
CM88L0+00E 0+60S	1	37	15	113	.1	91	19	566	3.11	9	5	ND	4	24	1	2	2	52	.28	.073	12	109	.96	274	.13	2	2.84	.02	.20	2	1
CM88L0-00E 0+75S	1	19	11	54	.2	58	14	260	2.39	3	5	ND	3	30	1	2	3	42	.44	.014	8	76	.71	163	.11	2	1.95	.02	.11	1	12
CM88L0+50E 0+75N	1	26	13	92	.1	62	10	547	2.43	11	7	ND	8	25	1	2	2	42	.27	.172	15	56	.53	137	.11	9	2.45	.02	.12	1	9
CM88L0+50E 0+60N	1	21	12	87	.3	55	11	358	2.51	11	7	ND	8	19	1	6	3	44	.18	.208	12	62	.57	211	.10	9	2.15	.02	.11	2	4
CM88L0+50E 0+45N	1	17	12	66	.2	79	13	322	2.82	10	5	ND	5	20	1	2	3	50	.22	.143	13	85	.76	149	.11	5	2.25	.02	.10	1	1
CM88L0+50E 0+30N	1	3	7	28	.2	24	5	440	1.13	4	5	ND	4	10	1	6	6	22	.11	.067	4	30	.24	84	.06	8	.76	.02	.06	1	1
STD C/AU-S	18	59	38	132	6.6	71	30	1044	4.04	42	17	8	40	48	18	15	21	60	.47	.090	41	60	.94	182	.07	35	1.98	.07	.13	13	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
CM88L0+50E 0+15N	1	24	9	54	.1	99	15	273	2.61	13	5	ND	4	21	1	3	4	44	.30	.042	10	97	.84	117	.11	6	2.24	.02	.12	1	4
CM88L0+50E 0+00N	1	22	11	74	.1	59	9	500	2.53	3	5	ND	6	17	1	4	2	42	.21	.112	12	64	.61	141	.11	11	2.38	.02	.11	1	1
CM88L0+50E 0+15S	1	23	15	80	.1	68	10	331	2.66	6	5	ND	6	18	1	2	2	46	.20	.101	12	74	.70	141	.11	7	2.49	.01	.11	1	8
CM88L0+50E 0+30S	1	29	15	94	.2	73	14	458	2.85	3	5	ND	4	20	1	2	2	49	.21	.128	11	85	.88	184	.11	2	2.46	.01	.11	1	7
CM88L0+50E 0+45S	1	30	13	79	.2	67	15	474	2.88	2	5	ND	6	19	1	4	2	48	.25	.128	12	78	.85	209	.12	2	2.62	.01	.14	1	5
CM88L0+50E 0+60S	1	25	21	90	.2	59	12	772	2.53	2	5	ND	3	19	1	3	2	40	.24	.106	10	61	.70	165	.10	2	2.17	.01	.12	1	2
CM88L0+50E 0+75S	1	32	14	91	.1	82	16	341	3.00	2	5	ND	9	17	1	2	2	52	.23	.069	11	98	1.04	149	.12	2	2.74	.01	.12	1	17
CM88L1+00E 0+75N	1	31	15	77	.1	85	15	236	2.80	7	5	ND	10	20	1	3	2	50	.24	.105	15	118	1.01	116	.11	8	2.55	.01	.11	1	5
CM88L1+00E 0+60N	1	20	14	169	.2	165	27	691	3.29	8	5	ND	5	24	1	2	2	64	.31	.098	9	247	2.07	220	.14	6	2.65	.01	.13	1	2
CM88L1+00E 0+45N	1	29	18	104	.1	139	19	423	3.00	10	5	ND	5	22	1	3	2	57	.28	.130	12	142	1.31	198	.13	4	3.09	.02	.13	1	9
CM88L1+00E 0+30N	1	28	16	84	.1	49	8	289	2.49	4	5	ND	3	21	1	2	4	68	.20	.063	9	64	.86	150	.11	2	1.80	.02	.12	1	1
CM88L1+00E 0+15N	1	31	8	66	.1	130	18	457	2.84	7	5	ND	2	17	1	2	2	52	.22	.080	6	128	1.23	138	.13	5	2.58	.02	.14	1	2
CM88L1+00E 0+00N	1	22	9	70	.1	49	9	891	2.21	9	5	ND	3	15	1	2	3	35	.16	.146	6	56	.57	178	.11	5	2.62	.02	.05	1	1
CM88L1+00E 0+15S	1	33	13	83	.1	59	11	326	2.97	8	5	ND	7	21	1	2	4	51	.21	.166	13	68	.78	124	.12	2	2.52	.01	.12	1	3
CM88L1+00E 0+30S	1	21	18	55	.1	103	11	189	2.47	19	5	ND	4	18	1	4	2	40	.22	.071	8	53	.54	109	.11	12	2.68	.02	.09	1	2
CM88L1+00E 0+45S	1	19	9	63	.4	71	9	203	2.13	30	5	ND	10	24	1	2	4	35	.30	.025	13	50	.53	101	.11	6	2.20	.02	.10	1	1
CM88L1+00E 0+60S	1	18	12	72	.2	33	8	531	2.12	8	5	ND	4	19	1	2	2	33	.19	.151	13	40	.38	140	.09	12	2.27	.02	.09	1	1
CM88L1+00E 0+75S	1	15	12	69	.2	34	7	446	2.15	7	5	ND	5	18	1	2	2	36	.17	.166	12	42	.38	148	.09	15	2.09	.02	.07	1	1
CM88L1+50E 0+75N	1	23	10	96	.3	60	11	548	2.44	3	5	ND	7	19	1	2	6	41	.20	.164	12	60	.55	181	.10	2	2.14	.01	.11	1	1
CM88L1+50E 0+60N	1	12	7	101	.3	50	9	725	2.22	2	5	ND	7	21	1	6	5	35	.20	.180	11	52	.48	244	.09	7	1.85	.01	.12	1	1
CM88L1+50E 0+45N	1	19	10	78	.1	39	9	306	2.36	4	5	ND	6	20	1	2	2	39	.19	.175	11	48	.43	153	.10	14	2.16	.02	.09	1	1
CM88L1+50E 0+30N	1	17	8	81	.3	34	8	439	2.08	2	5	ND	5	21	1	2	2	33	.16	.139	9	42	.36	204	.09	4	1.53	.01	.07	1	1
CM88L1+50E 0+15N	1	31	17	129	.2	68	17	471	3.09	4	5	ND	5	26	1	5	5	57	.26	.089	12	75	.87	147	.14	4	2.25	.02	.15	1	1
CM88L1+50E 0+00N	1	13	11	57	.1	33	8	288	2.13	2	5	ND	4	17	1	4	2	36	.17	.109	9	41	.39	142	.09	2	1.59	.01	.07	1	1
CM88L1+50E 0+15S	1	14	12	39	.1	39	7	216	2.14	5	5	ND	5	19	1	2	6	37	.19	.048	10	44	.43	102	.09	2	1.58	.01	.08	1	5
CM88L1+50E 0+30S	1	18	9	51	.1	49	8	215	2.31	5	5	ND	9	19	1	2	2	39	.20	.082	12	48	.47	95	.09	4	1.75	.01	.09	1	1
CM88L1+50E 0+45S	1	26	14	82	.3	47	9	586	2.49	3	5	ND	13	24	1	2	6	44	.25	.129	17	47	.56	182	.11	6	1.98	.01	.13	1	2
CM88L1+50E 0+60S	1	17	15	65	.1	32	7	438	1.95	6	5	ND	5	30	1	2	2	35	.28	.114	12	37	.40	118	.08	4	1.39	.01	.07	1	1
CM88L1+50E 0+75S	1	21	9	54	.1	30	7	249	1.92	6	5	ND	6	22	1	3	2	34	.22	.121	15	35	.36	97	.08	2	1.38	.01	.06	1	4
CM88L1+50E 0+90S	1	19	12	58	.4	30	8	240	2.11	7	5	ND	7	19	1	2	2	35	.19	.131	13	31	.33	99	.09	4	2.02	.01	.06	2	1
CM88L1+50E 1+05S	1	21	8	79	.4	19	6	1202	1.40	8	5	ND	1	21	1	2	2	26	.22	.139	5	20	.24	234	.06	3	1.10	.02	.07	1	1
CM88L1+50E 1+20S	1	33	11	71	.3	46	10	355	2.61	7	5	ND	8	24	1	2	7	45	.21	.108	16	53	.57	177	.11	2	2.45	.02	.10	1	1
CM88L1+50E 1+35S	1	33	10	105	.1	44	9	673	2.50	6	5	ND	4	19	1	2	5	41	.19	.076	10	46	.54	179	.08	3	1.54	.01	.10	3	2
CM88L1+50E 1+50S	1	42	17	112	.3	71	15	580	3.29	12	5	ND	10	28	1	2	2	57	.27	.160	18	76	.81	249	.11	3	2.54	.01	.19	5	11
CM88L1+50E 1+65S	1	35	9	141	.1	68	13	608	2.94	5	5	ND	3	38	1	2	2	52	.41	.188	16	69	.72	264	.10	4	2.09	.01	.15	1	5
CM88L1+50E 1+80S	1	20	10	118	.2	39	10	523	2.49	6	5	ND	4	32	1	2	2	42	.28	.192	15	54	.50	195	.08	9	1.57	.01	.09	1	2
STD C/AU-S	18	58	41	132	6.6	68	30	1036	4.00	41	15	8	37	48	18	16	21	59	.46	.081	40	57	.94	182	.07	30	1.96	.07	.14	11	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
CM88L1+50E 1+95S	1	16	12	58	.1	39	8	267	2.23	2	5	ND	6	31	1	3	4	39	.27	.104	13	49	.41	117	.09	2	1.85	.03	.09	2	1
CM88L1+50E 2+10S	1	19	13	66	.1	52	7	329	2.43	11	7	ND	4	21	1	3	2	42	.18	.082	12	49	.46	120	.12	7	2.77	.02	.09	1	1
CM88L1+50E 2+10SA	1	24	18	75	.1	63	11	411	2.62	7	5	ND	5	25	1	2	6	47	.24	.085	17	76	.73	160	.11	10	2.31	.02	.13	1	1
CM88L1+50E 2+25S	1	17	13	73	.1	67	8	500	2.43	3	5	ND	5	29	1	2	2	45	.28	.071	15	68	.65	142	.11	11	2.08	.02	.13	1	8
CM88L1+50E 2+55S	1	24	35	114	1.8	73	10	416	2.58	6	5	3	5	24	1	2	2	47	.25	.072	17	83	.82	180	.11	10	2.24	.02	.15	1	1
CM88L1+50E 2+70S	1	17	18	89	.1	45	8	674	2.07	3	5	ND	2	22	1	2	6	36	.20	.112	11	46	.48	160	.08	12	1.80	.02	.09	2	1
CM88L2+00E 0+75N	1	18	12	47	.1	59	10	174	2.80	3	5	ND	9	37	1	4	5	48	.40	.012	19	64	.56	140	.12	2	2.03	.02	.10	1	1
CM88L2+00E 0+60N	1	33	9	41	.3	100	8	352	2.38	17	5	ND	6	37	1	2	4	38	.36	.020	22	52	.50	108	.11	9	2.24	.03	.11	1	1
CM88L2+00E 0+45N	1	21	12	105	.1	22	7	326	2.28	3	5	ND	3	22	1	2	2	36	.18	.178	9	33	.35	189	.09	4	1.58	.02	.11	1	10
CM88L2+00E 0+30N	1	10	13	114	.1	30	8	744	2.21	4	5	ND	5	23	1	2	2	35	.19	.212	11	47	.38	176	.09	8	1.64	.02	.09	1	1
CM88L2+00E 0+15N	1	19	12	70	.1	49	9	396	2.25	3	5	ND	7	21	1	2	2	40	.19	.113	13	55	.48	139	.10	12	1.88	.02	.08	1	1
CM88L2+00E 0+00N	1	24	14	90	.1	62	11	521	2.55	2	5	ND	7	25	1	2	2	45	.23	.161	14	63	.59	160	.10	2	2.11	.02	.12	1	1
CM88L2+00E 0+15S	1	15	11	69	.1	54	9	308	2.03	2	5	ND	4	20	1	4	2	37	.19	.107	11	71	.51	103	.09	15	1.40	.02	.08	1	1
CM88L2+00E 0+30S	1	25	6	82	.2	96	13	375	2.73	4	5	ND	4	24	1	2	2	49	.22	.101	14	124	.81	181	.11	4	2.16	.02	.12	1	2
CM88L2+00E 0+45S	1	30	11	80	.1	99	12	398	2.74	5	5	ND	9	20	1	2	2	48	.20	.090	14	136	.87	166	.12	14	2.68	.02	.10	1	1
CM88L2+00E 0+45SA	1	32	15	83	.2	88	14	305	2.71	5	5	ND	5	30	1	2	2	48	.26	.072	17	91	.83	171	.12	10	2.21	.02	.16	1	1
CM88L2+00E 0+60S	1	52	11	126	.2	260	28	603	3.20	21	5	ND	3	25	1	2	2	56	.28	.052	9	525	2.69	204	.14	20	2.84	.01	.16	1	1
CM88L2+00E 0+75S	1	42	9	97	.3	121	16	503	2.85	12	5	ND	7	21	1	2	2	52	.21	.106	14	112	.99	210	.14	16	3.00	.02	.17	1	3
CM88L2+50E 0+75N	1	25	14	87	.1	52	10	258	2.60	4	5	ND	5	25	1	4	2	46	.25	.080	12	59	.58	117	.12	14	2.20	.02	.11	1	1
CM88L2+50E 0+60N	1	13	11	73	.2	52	10	207	2.33	4	5	ND	8	21	1	2	2	39	.21	.060	14	63	.40	87	.08	15	1.44	.02	.08	1	1
CM88L2+50E 0+45N	1	23	12	69	.1	53	9	294	2.54	2	5	ND	12	24	1	2	2	44	.23	.143	19	56	.48	127	.10	14	2.07	.02	.09	1	6
CM88L2+50E 0+30N	1	19	11	73	.3	55	9	472	2.25	4	8	ND	8	18	1	2	2	38	.17	.121	12	53	.45	135	.10	4	2.17	.02	.10	1	2
CM88L2+50E 0+15N	1	20	10	85	.5	69	11	350	2.65	3	5	ND	6	20	1	2	2	45	.20	.105	13	76	.63	92	.11	2	2.06	.01	.11	1	1
CM88L2+50E 0+00N	1	35	13	81	.1	94	13	422	2.69	2	5	ND	4	22	1	2	2	47	.21	.129	14	112	.89	164	.11	12	2.23	.02	.12	2	3
CM88L2+50E 0+15S	1	15	12	70	.3	83	9	423	2.09	5	5	ND	4	18	1	2	2	36	.16	.072	10	101	.63	128	.10	3	1.68	.02	.08	1	1
CM88L2+50E 0+30S	1	25	8	66	.1	77	10	209	2.45	4	5	ND	4	23	1	2	2	42	.22	.094	14	85	.65	143	.11	11	2.24	.02	.09	1	1
CM88L2+50E 0+60S	1	20	12	91	.5	86	11	480	2.42	3	7	ND	3	20	1	2	2	43	.20	.060	11	93	.73	132	.11	6	1.87	.02	.13	1	3
CM88L2+50E 0+75S	1	23	12	76	.3	107	12	252	2.60	4	5	ND	3	24	1	2	2	46	.21	.059	14	105	.80	183	.12	12	2.19	.02	.13	1	1
STD C/AU-S	19	62	41	132	6.7	68	30	1039	4.03	41	20	8	37	48	18	16	22	59	.46	.083	40	59	.93	181	.07	32	1.98	.07	.16	12	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au** PPB	Cu %
CM88-1	1	148	15	121	.3	106	22	617	3.28	2	5	2	1	93	1	2	2	85	3.44	.040	2	109	1.22	160	.17	18	1.18	.02	.23	5	3635	-
CM88-2	7	502	30	111	1.0	106	35	457	8.90	7	5	ND	1	29	1	2	4	162	1.63	.230	6	86	1.17	54	.13	10	1.17	.02	.10	2	112	-
CM88-3	1	459	6377	1697	30.0	18	8	363	2.80	2	5	103	1	54	16	2	10	74	1.65	.041	3	13	.68	23	.08	16	.61	.03	.09	6	119060	-
CM88-4	1	61	54	193	.2	19	5	136	.96	2	5	ND	1	35	2	2	3	7	.87	.003	2	8	.12	1	.01	17	.11	.01	.02	2	6526	-
CM88-5	1	86	43	15	.1	22	12	222	1.14	2	5	ND	1	75	1	2	3	8	3.13	.036	2	16	.12	8	.04	3	.20	.02	.04	2	235	-
CM88-6	1	147	308	671	3.3	13	9	758	2.71	2	5	6	1	197	20	2	2	27	4.31	.039	2	4	.76	31	.01	2	.67	.02	.09	1	4684	-
CM88-7	1	83	9533	1569	19.7	58	9	245	2.91	22	5	15	1	60	59	2	2	2	.44	.002	2	9	.48	5	.01	15	.04	.01	.03	7	24930	-
CM88-8R	1	86	13	74	.1	39	22	1088	4.76	5	5	ND	1	213	1	2	2	69	7.86	.068	6	57	2.50	17	.01	5	.62	.02	.13	1	98	-
CM88-9	1	82	60	54	.5	2	4	416	3.44	2	5	ND	1	22	1	2	6	91	.27	.065	3	9	1.05	180	.13	13	1.25	.04	.26	2	42	-
CM88-10R	2	32	14	29	.1	12	2	110	2.82	6	5	ND	1	11	1	2	4	40	.19	.062	11	23	.50	115	.01	2	.76	.01	.14	2	68	-
CM88-11	1	211	14	34	.1	7	18	315	3.54	2	5	ND	1	43	1	2	4	65	.69	.043	2	5	.98	126	.08	8	1.04	.04	.17	1	7	-
CM88-12R	1	10	4	3	.1	3	1	35	.34	2	5	ND	1	1	1	2	2	1	.01	.001	2	3	.02	4	.01	2	.01	.01	.02	1	1	-
CM88-13	1	11	10	40	.2	50	12	842	2.02	6	5	ND	1	683	1	2	4	47	19.78	.040	5	84	1.12	235	.08	15	.98	.01	.22	1	1	-
CM88-14R	1	23	298	133	1.7	58	5	238	1.31	27	5	ND	1	184	2	2	2	10	1.70	.012	3	26	1.12	15	.01	19	.29	.01	.04	1	179	-
CM88-15	18	26	17	77	.3	35	4	323	1.80	5	5	ND	1	201	1	2	2	63	5.66	.036	8	41	.63	70	.03	19	.62	.01	.09	2	7	-
CM88-16	4	77	9	78	.1	31	3	134	1.36	7	5	ND	1	4	1	2	2	10	.07	.028	5	8	.22	61	.01	20	.45	.01	.06	1	6	-
CM88-17	1	71	5	83	.1	31	7	305	3.31	2	5	ND	1	7	1	2	4	129	.22	.056	5	65	1.21	140	.14	2	1.32	.03	.67	1	3	-
CM88-18	1	13	12	15	.1	7	1	50	.87	2	5	ND	1	5	1	3	2	9	.04	.020	3	4	.11	24	.01	2	.16	.01	.05	1	205	-
CM88-19	1	26	2	28	.1	14	4	262	1.55	3	5	ND	2	4	1	2	2	16	.05	.018	8	19	.43	69	.03	14	.77	.01	.24	1	1	-
CM88-20	1	12	1035	31	2.2	16	2	152	.83	11	5	ND	1	39	1	2	2	3	.38	.005	2	5	.26	10	.01	18	.06	.01	.02	1	1256	-
CM88-22	1	13	13	95	.3	571	34	1045	4.23	467	5	ND	1	518	1	4	2	13	5.94	.026	2	143	8.54	28	.01	22	.31	.01	.12	1	4	-
CM88-28	1	16	11	15	.1	19	2	79	.90	10	5	ND	1	16	1	2	2	3	.15	.008	2	8	.23	33	.01	2	.13	.01	.07	1	10	-
CM88-30	1	44	13	44	.4	44	6	483	1.30	3	5	ND	1	168	1	2	2	22	6.61	.032	2	37	.38	26	.06	4	.34	.01	.06	2	2273	-
CM88-32	2	49	13	75	.4	30	6	375	1.97	2	5	ND	2	23	1	2	2	34	.37	.071	11	17	.76	106	.01	2	.77	.01	.12	1	104	-
CM88-34	1	30	4	75	.1	6	6	556	3.02	2	5	ND	2	13	1	2	2	36	.31	.069	13	3	.83	106	.01	6	1.31	.02	.24	1	13	-
CM88-36	1	9	44	19	.1	9	2	295	.65	2	5	ND	1	6	1	2	2	8	.08	.007	2	3	.12	19	.01	4	.12	.01	.03	1	2	-
CM88-38	5	42	9	45	.1	94	20	906	2.51	32	5	ND	1	802	1	2	2	84	22.64	.084	11	243	1.07	359	.02	2	1.14	.01	.34	1	1	-
CM88-40	1	4	4	22	.1	18	3	238	1.24	2	5	ND	1	5	1	2	2	33	.17	.042	6	25	.45	26	.01	16	.45	.02	.01	1	1	-
CM88-42	1	30	13	77	.1	37	4	184	1.58	2	5	ND	1	47	1	2	2	51	1.50	.086	13	49	1.03	73	.01	2	.92	.01	.11	1	1	-
CM88-44R	1	25	7	19	.4	19	3	248	.98	4	5	ND	2	4	1	3	2	26	.08	.025	8	18	.31	96	.01	5	.40	.01	.12	1	1	-
CM88-46	1	48	10	37	.1	17	6	442	2.18	2	5	ND	3	5	1	2	2	39	.07	.021	11	30	1.15	89	.02	10	1.12	.02	.16	1	1	-
DM1	4	29592✓	189	39	11.6	128	42	61	16.44	67	5	ND	1	5	1	62	8	1	.58	.001	2	1	.36	2	.01	9	.02	.01	.03	1	4	3.16
DM2	12	99999✓	255	282	6.4	265	124	23	28.24	1107	12	ND	1	1	1	1637	2	5	.10	.066	2	1	.07	5	.01	4	.04	.01	.02	1	1	27.65
STD C/AU-R	18	63	39	132	6.8	73	30	1043	4.05	40	17	8	38	48	18	17	23	60	.46	.081	41	60	.93	178	.07	33	1.96	.07	.14	11	520	-

✓ ASSAY REQUIRED FOR CORRECT RESULT -

ANALYTICAL TECHNIQUES

A. Sample Preparation:

1. Soil/Silt Geochemistry: Samples are dried out and sifted to minus 80 mesh, through stainless steel or nylon screens.

2. Rock Geochemistry: Samples are dried, crushed to minus 1/4 inch, split and pulverized to minus 100 mesh.

3. Rock Assay: Samples are dried, crushed to minus 1/8 inch, split and pulverized to minus 150 mesh.

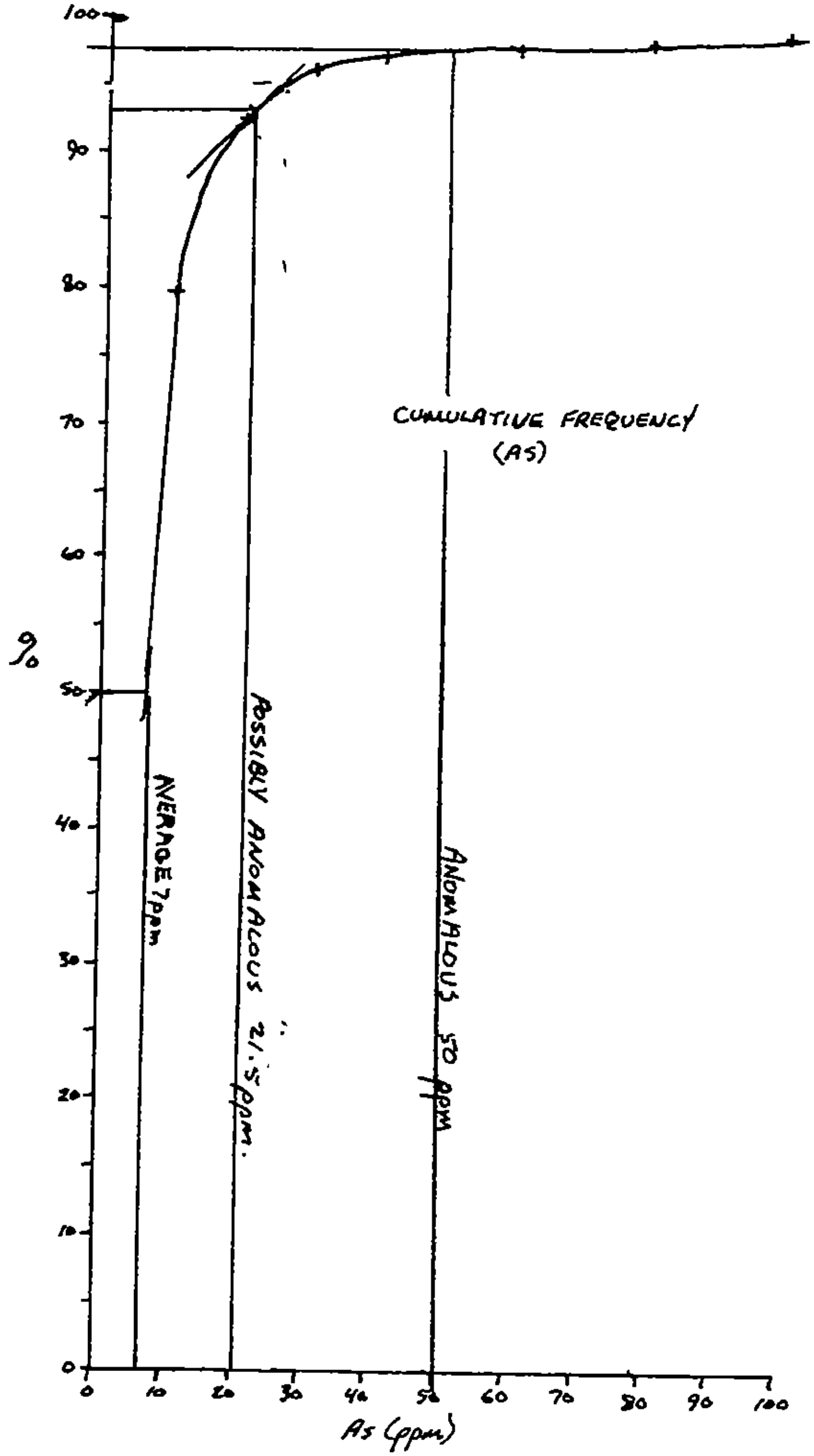
B. Methods of Analysis:

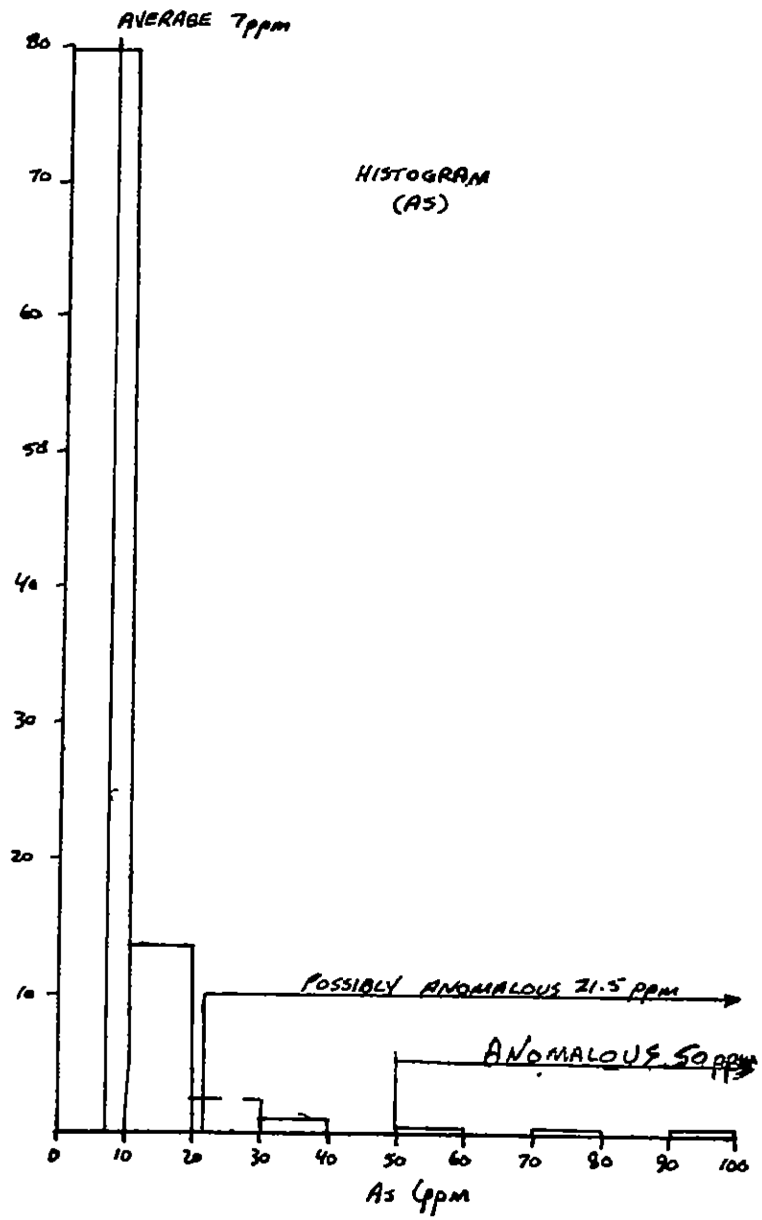
1. Geochemical Gold: A 10 gram sample is roasted at 550C and digested with aqua regia. The dissolved gold is then extracted with methyl isobutyl ketone, and the resulting solution analyzed using atomic absorption spectroscopy.

2. Fire Assay Gold: A 15 or 30 gram sample is fused using standard fire assay fluxes, the resulting gold/silver/lead button is cupelled, and the gold/silver bead analyzed using atomic absorption or a gravimetric finish.

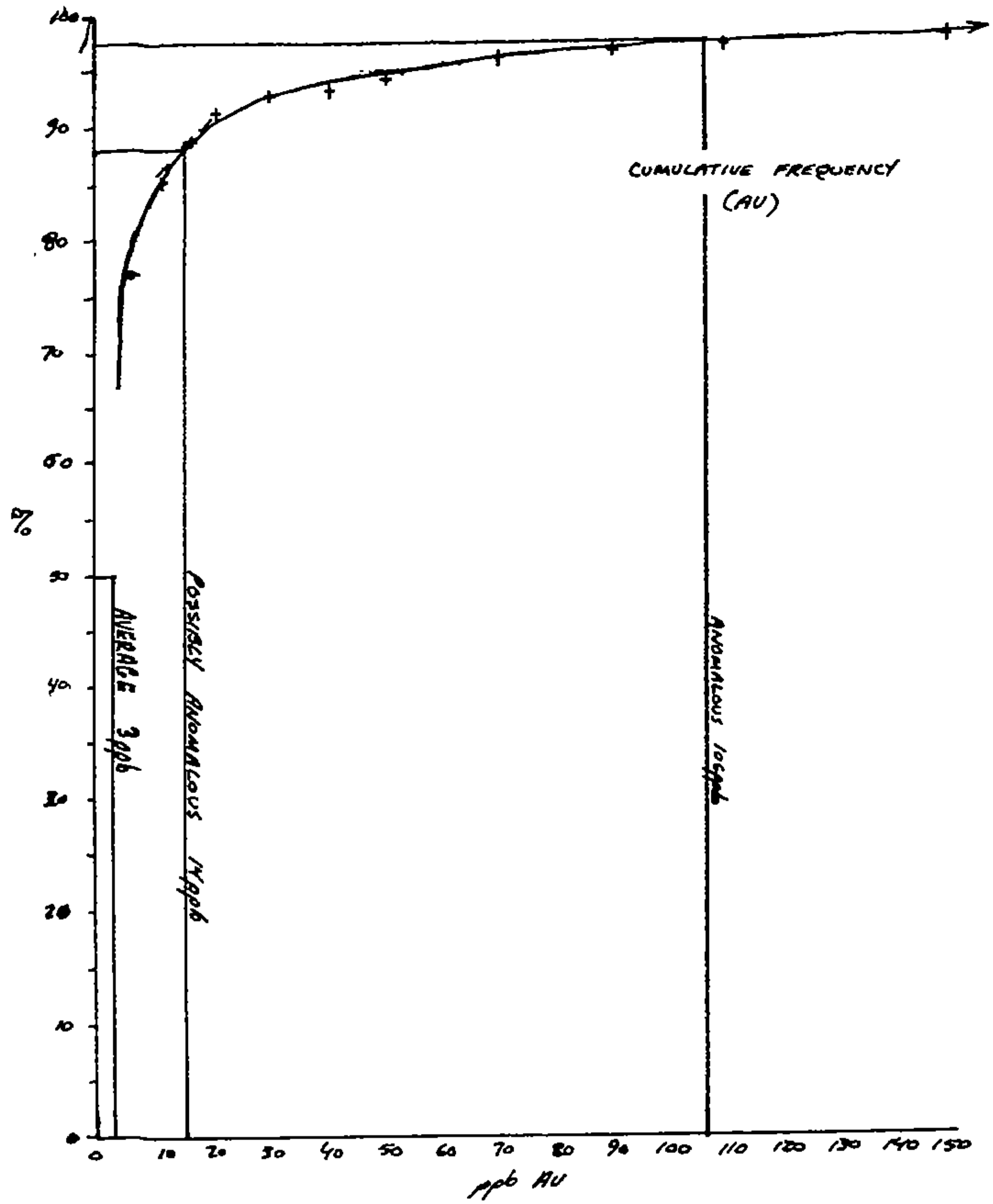
3. Multi-Element ICP: A 0.5 gram sample is digested with a 3-1-2 dilute aqua regia mixture and analyzed using inductively coupled plasma spectroscoy.

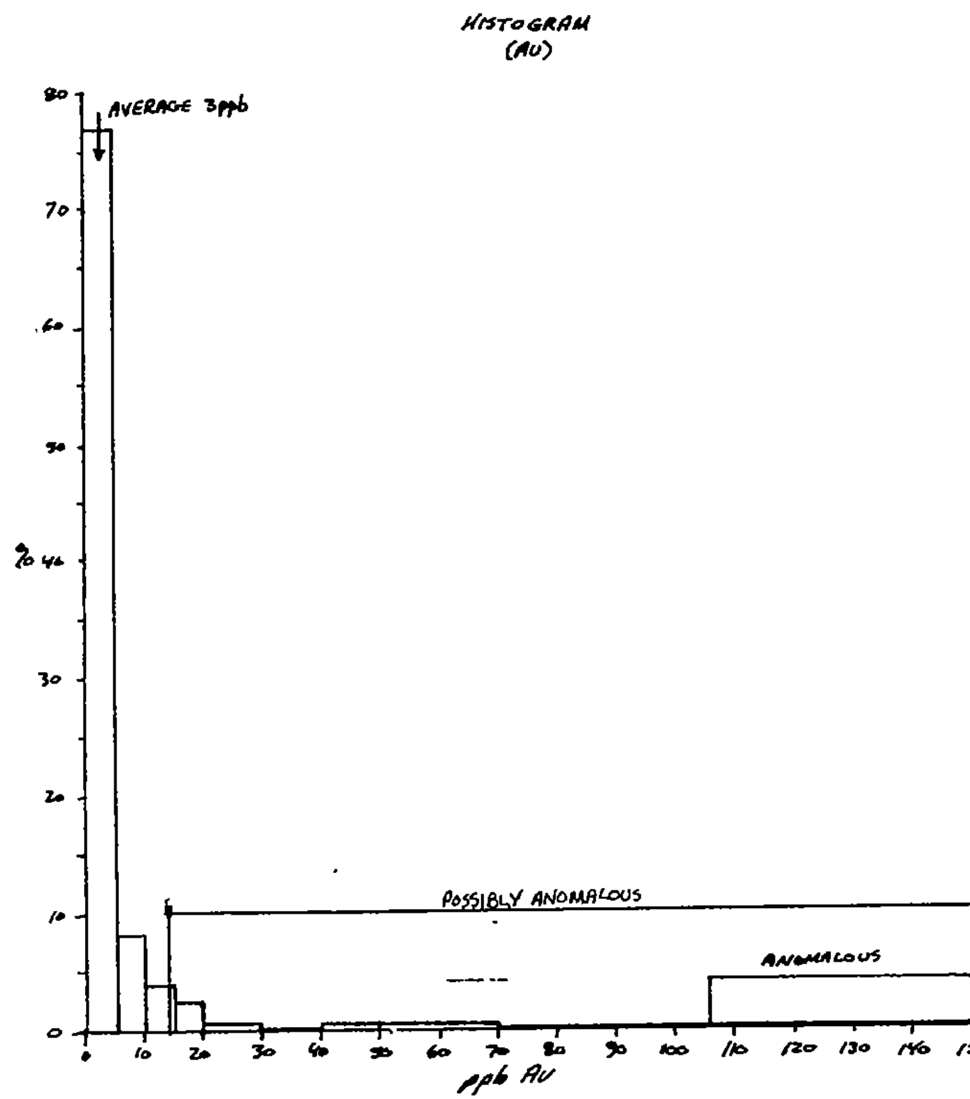
STATISTICAL PLOTS (AS)

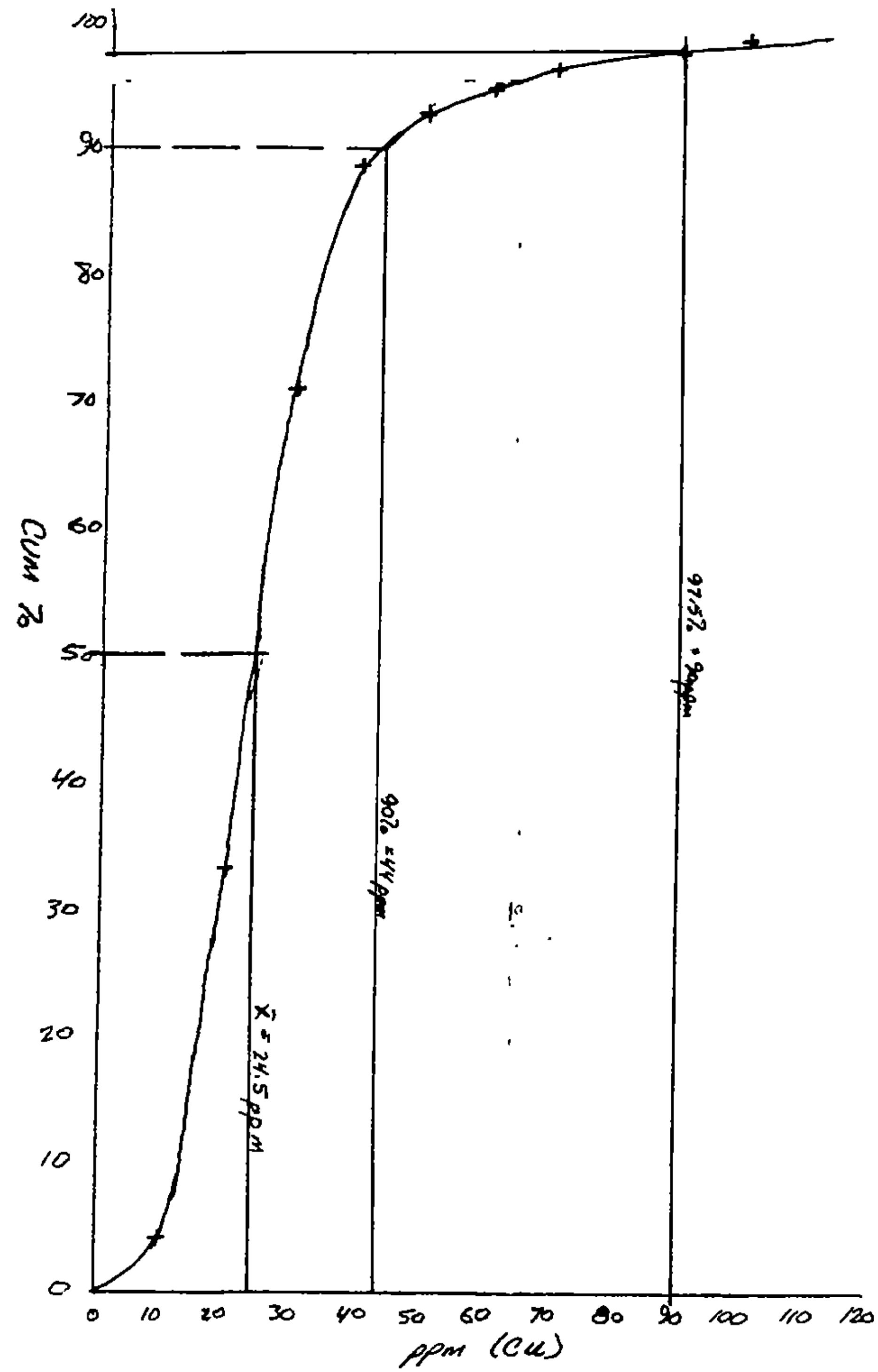


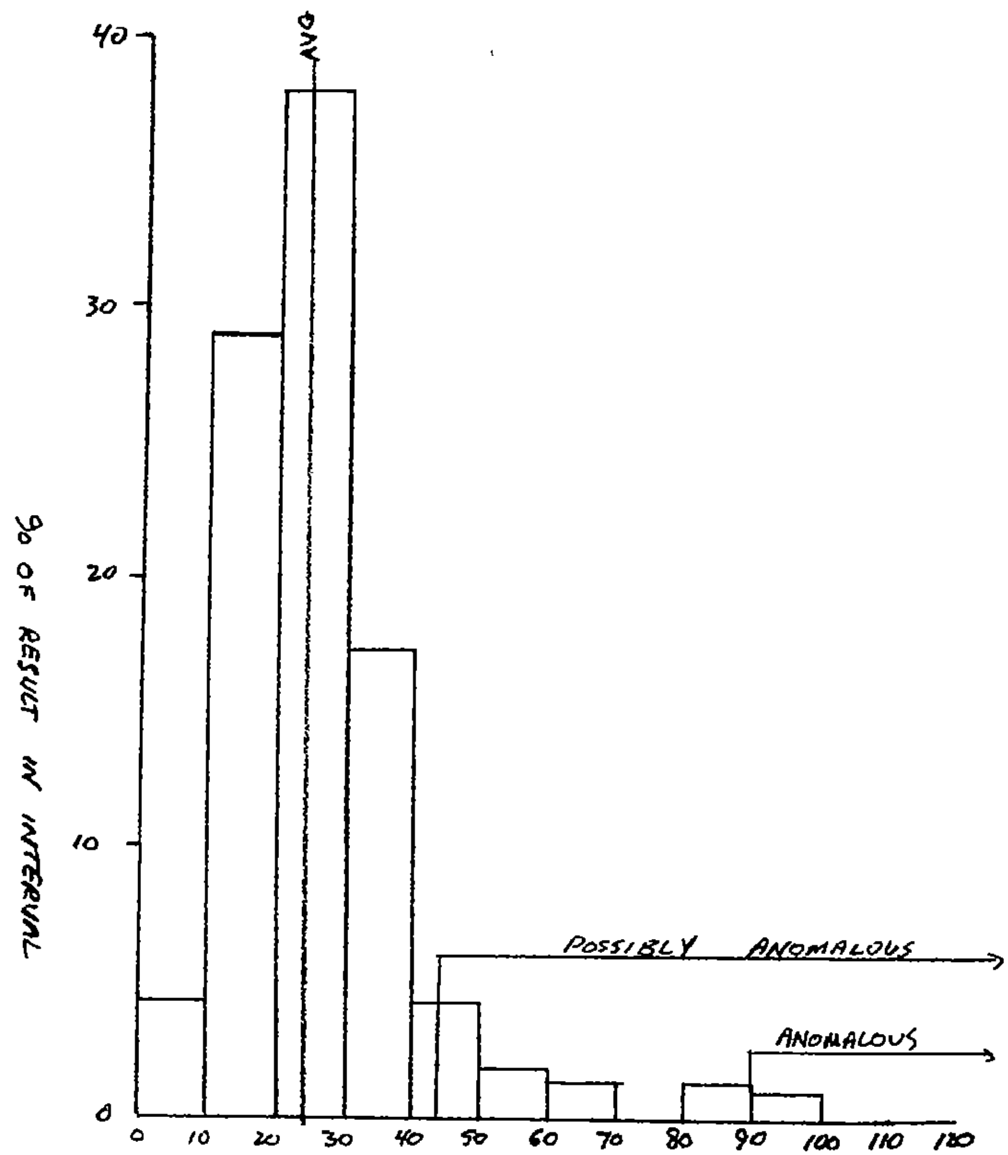


STATISTICAL PLOTS (AU)

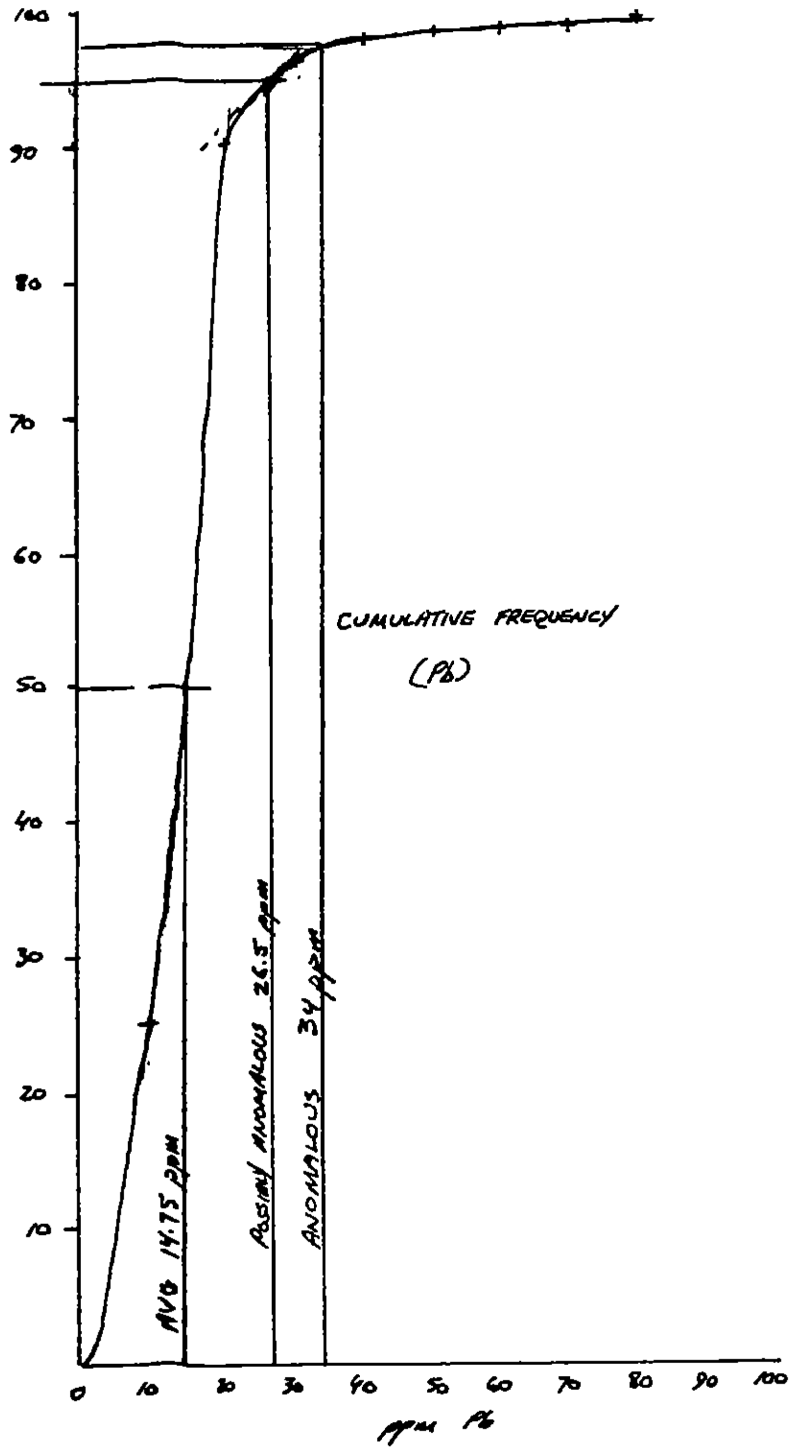


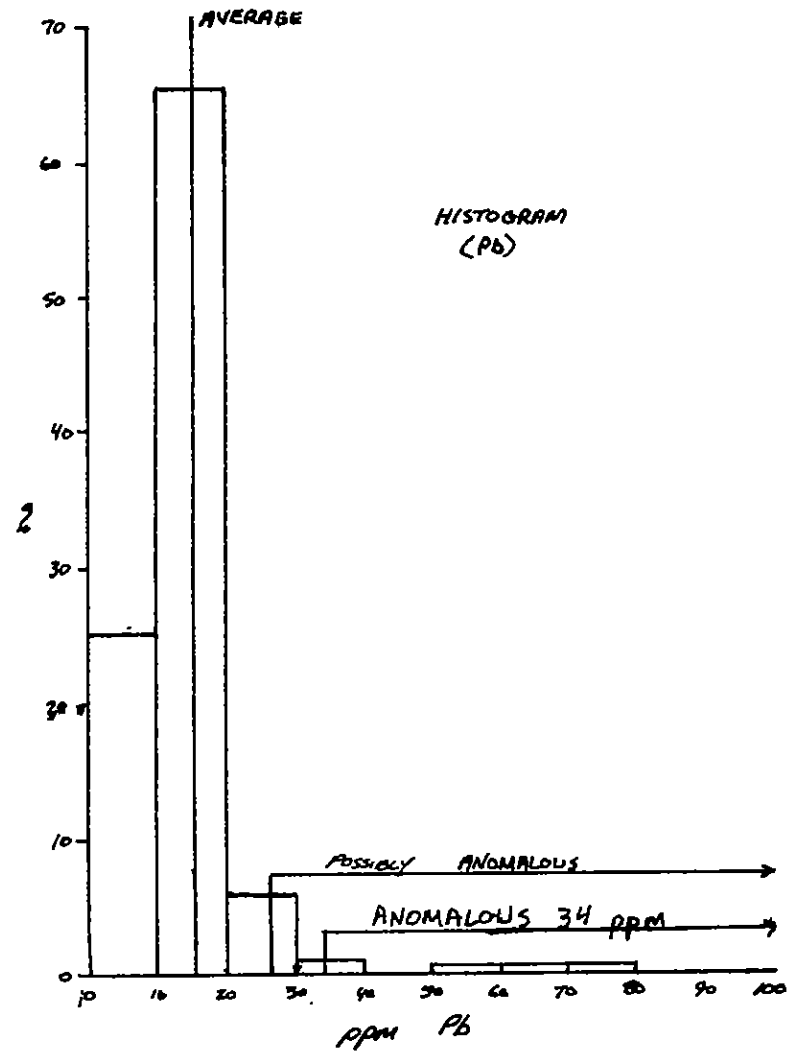



CUM %
X̄ = 24.5 PPM
90% = 44 ppm
97.5% = 90 ppm
PPM (CU)

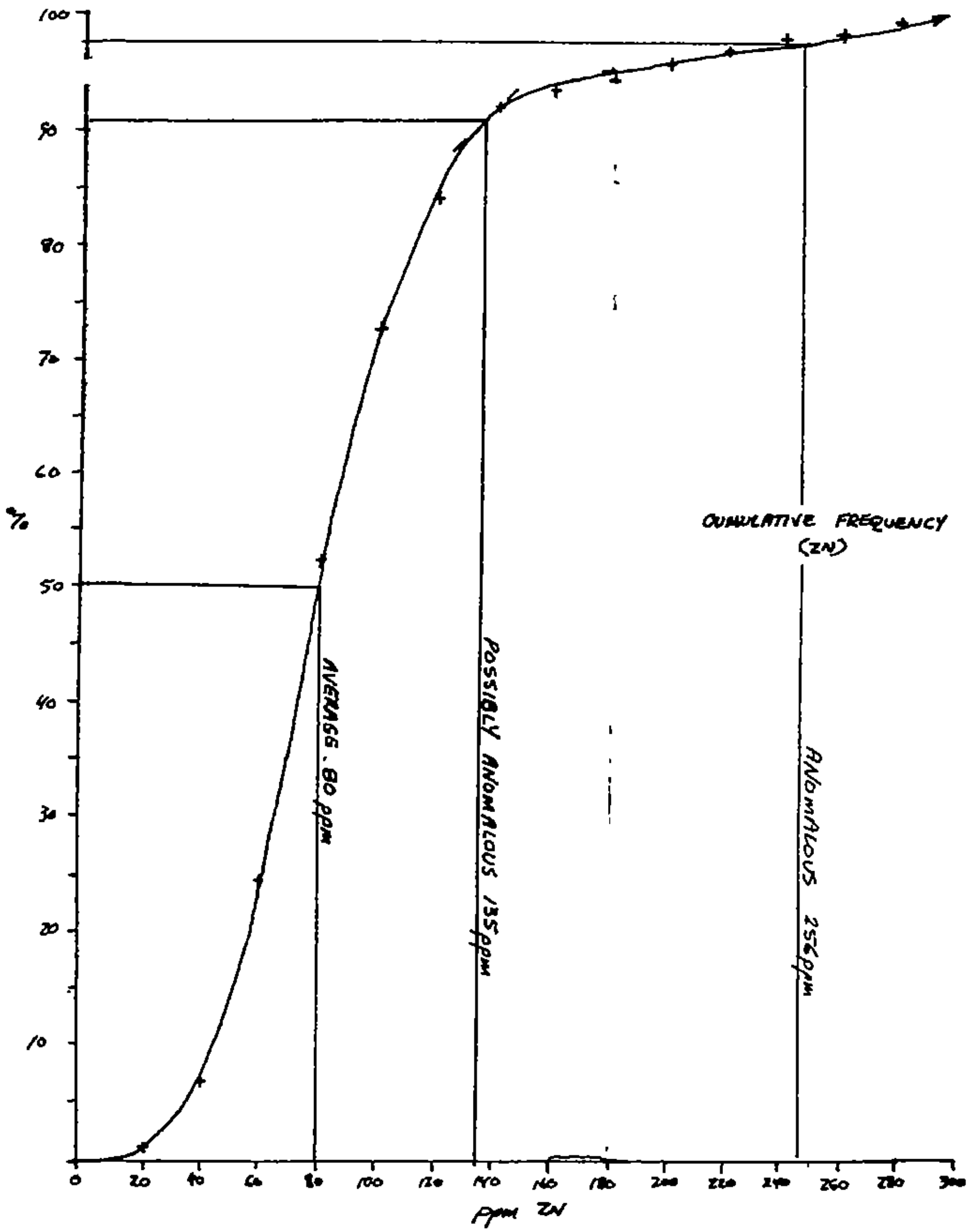

AVG
% OF RESULT IN INTERVAL
POSSIBLY ANOMALOUS
ANOMALOUS

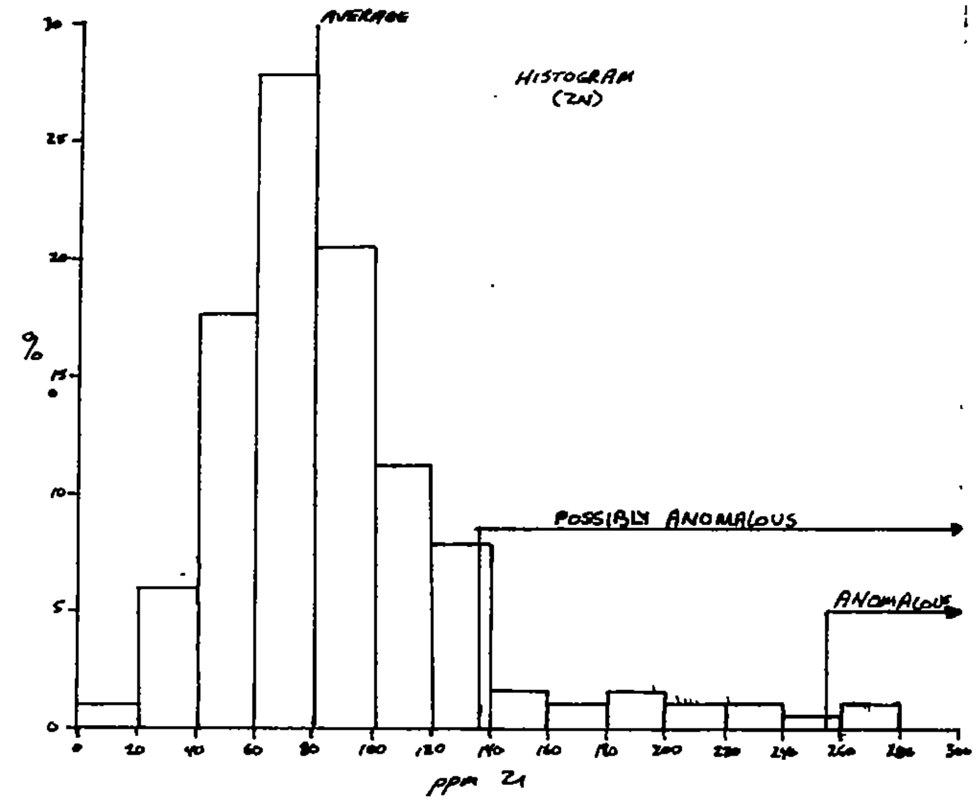
STATISTICAL PLOTS (Pb)

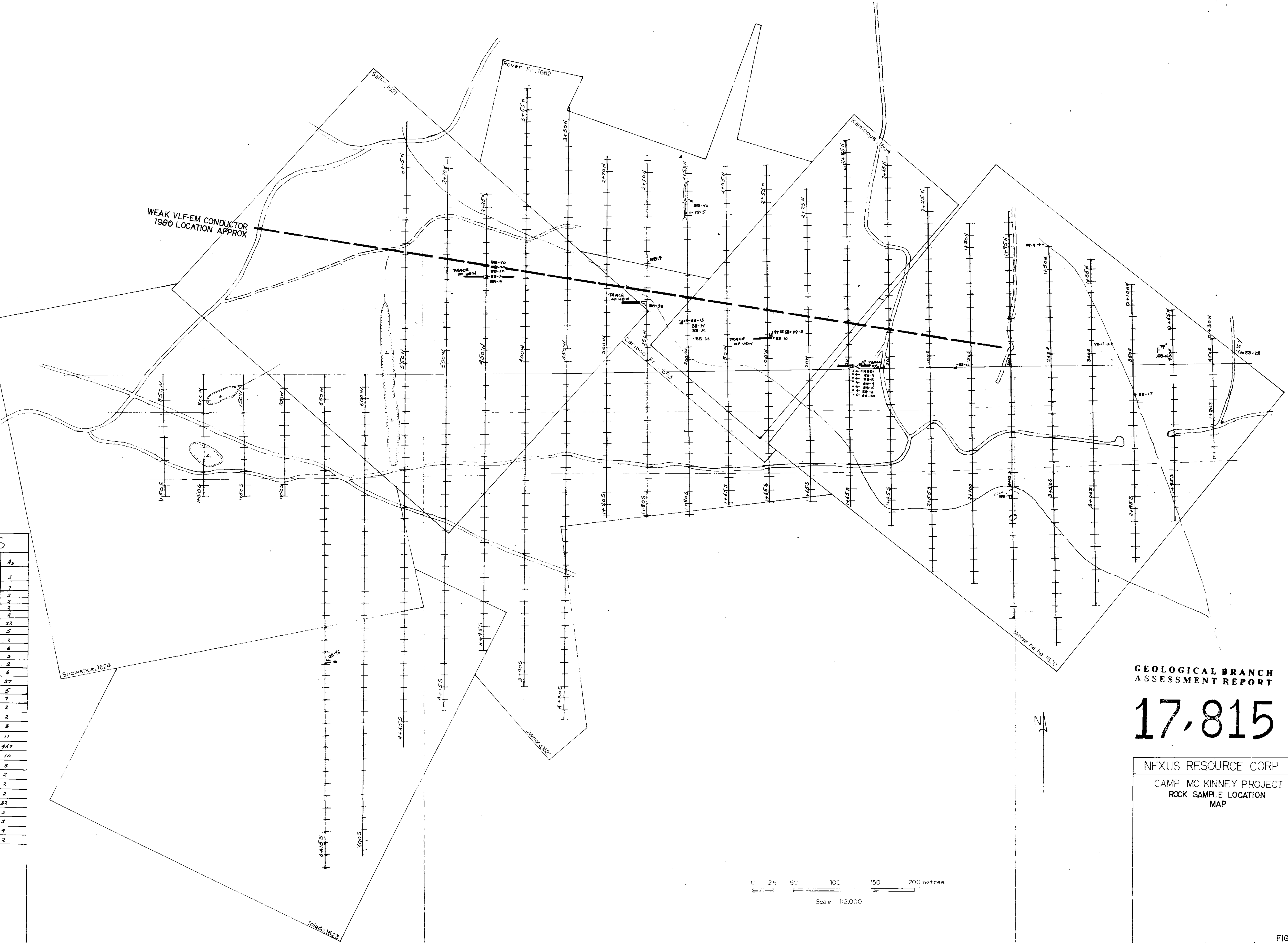




STATISTICAL PLOTS (ZN)







ROCK SAMPLE ASSAYS

SAMPLE #	Au (PPB)	Cu	Pb	Zn	As
CM88-1	3635	148	15	121	2
CM88-2	112	502	30	111	7
CM88-3	119060	459	6377	1697	2
CM88-4	6526	61	54	193	2
CM88-5	235	86	43	15	2
CM88-6	4684	147	308	671	2
CM88-7	24930	83	9533	1569	22
CM88-8R	98	86	13	79	5
CM88-9	42	82	60	59	2
CM88-10R	68	32	14	29	6
CM88-11	7	211	14	34	2
CM88-12R	1	10	4	3	2
CM88-13	1	11	10	40	6
CM88-14R	179	23	298	133	27
CM88-15	7	26	17	77	5
CM88-16	6	77	9	78	7
CM88-17	3	71	5	83	2
CM88-18	205	13	12	15	2
CM88-19	1	26	2	28	3
CM88-20	1256	12	1035	31	11
CM88-22	4	13	13	95	467
CM88-28	10	16	11	15	10
CM88-30	2273	44	13	44	3
CM88-32	104	49	13	75	2
CM88-34	13	30	4	75	2
CM88-36	2	9	44	19	2
CM88-38	1	42	9	45	32
CM88-40	1	4	4	22	2
CM88-42	1	30	13	77	2
CM88-44R	1	25	7	19	4
CM88-46	1	48	10	37	2

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17,815

NEXUS RESOURCE CORP

CAMP MC KINNEY PROJECT
ROCK SAMPLE LOCATION
MAP

FIG. 3

Work By: JW Drafted By: JW Date 15/09/88


WEAK VLF-EM CONDUCTOR
(1980, LOCATION APPROX)
Sailor 1621
Rover Fr. 1662
Kamloops 1664
Cariboo 1663
Snowshoe 1624
Toledo 1623
Diamond 1622
Minnie ha ha 1620
N
0 25 50 100 150 200 metres
Scale: 1:2,000
GEOLOGICAL BRANCH
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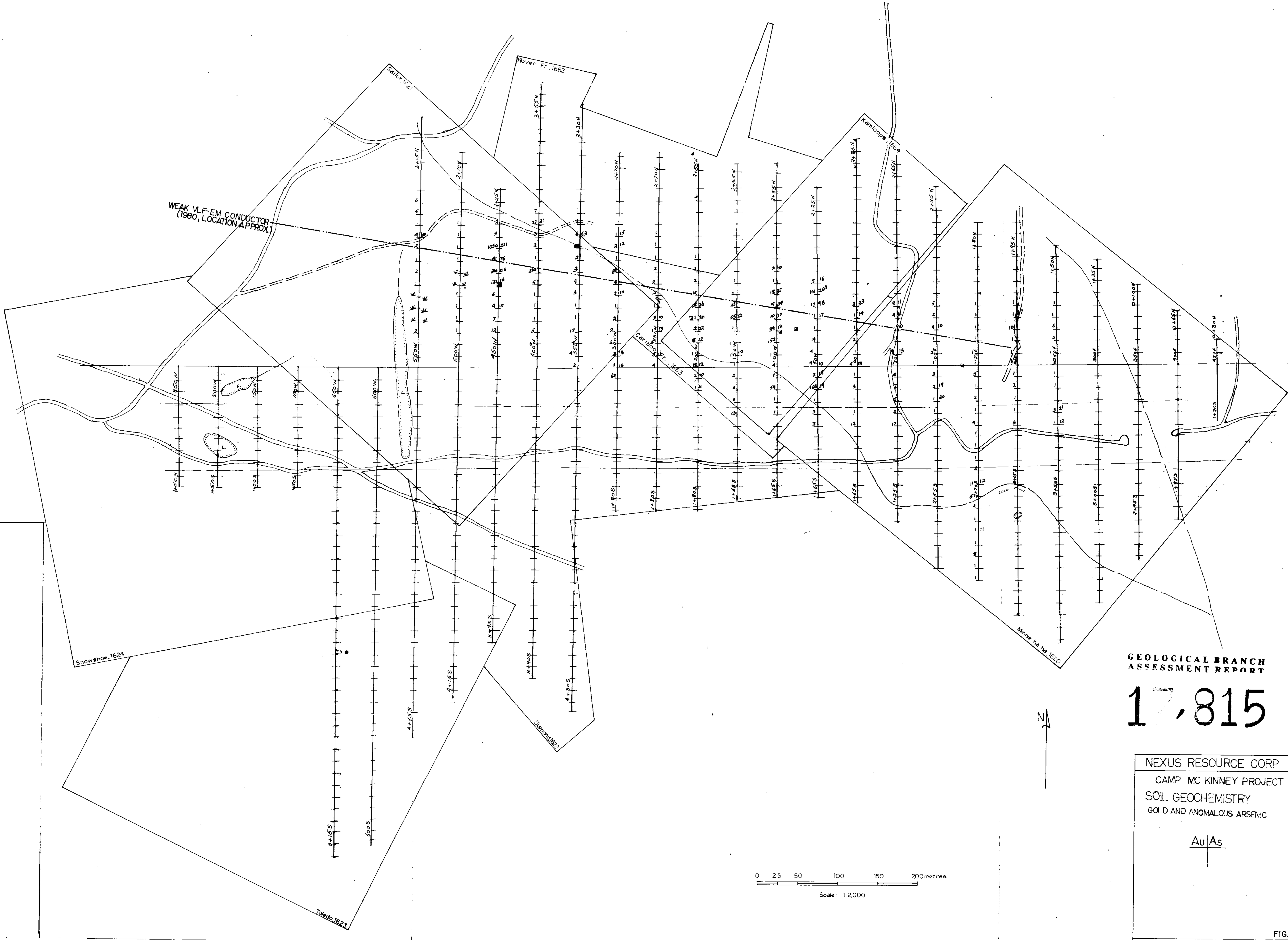
17,815
NEXUS RESOURCE CORP
CAMP MC KINNEY PROJECT
SOIL GEOCHEMISTRY
COPPER LEAD ZINC VALUES
Cu | Pb
Zn
FIG.4
Work By: TSB Drafted By: TSB



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CAMP MC KINNEY PROJECT

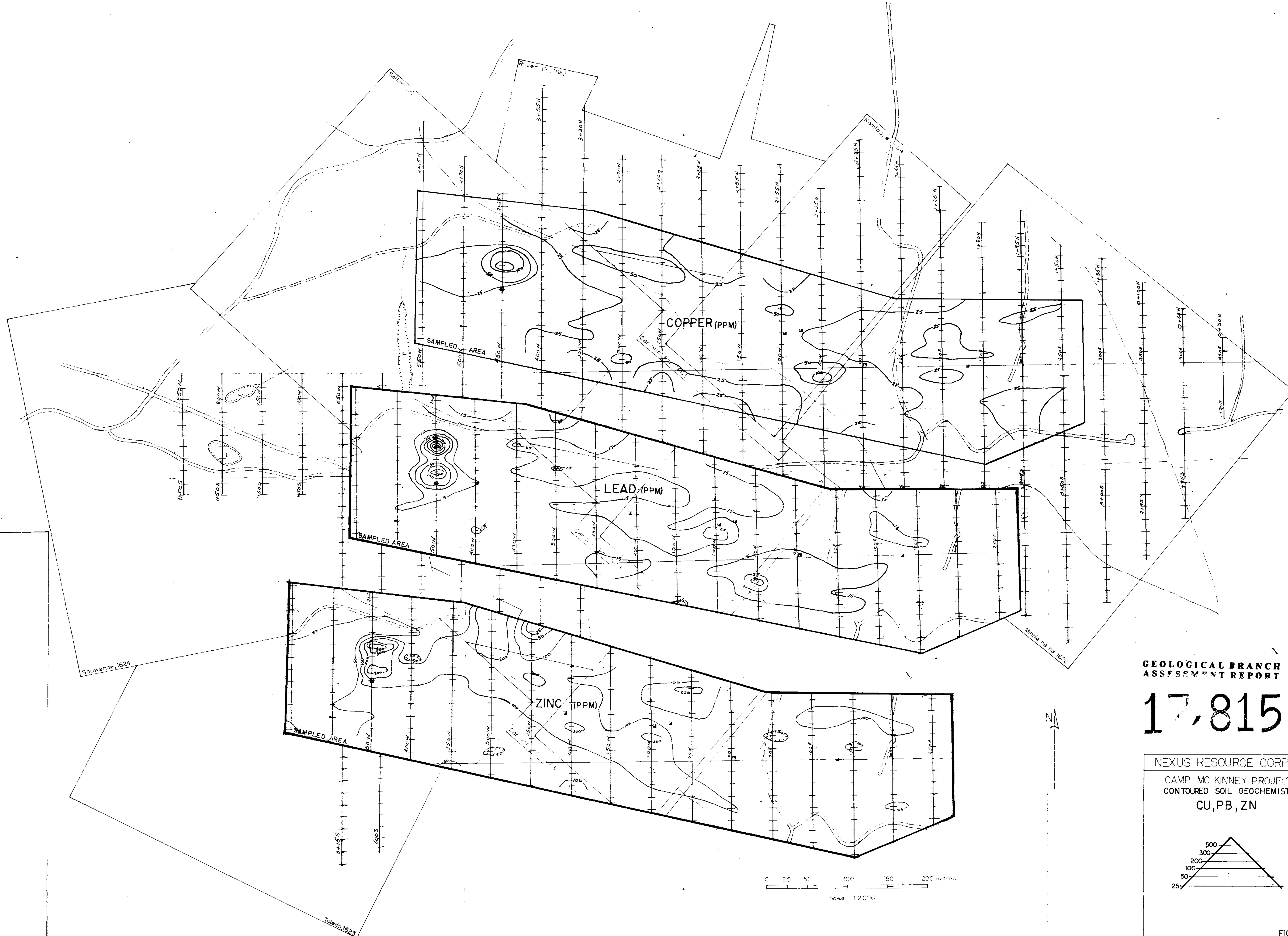
SOIL GEOCHEMISTRY

GOLD AND ANOMALOUS ARSENIC

Au | As

FIG. 5

Work By: 78 Drafted By: 738 Date: 07/88



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17,815

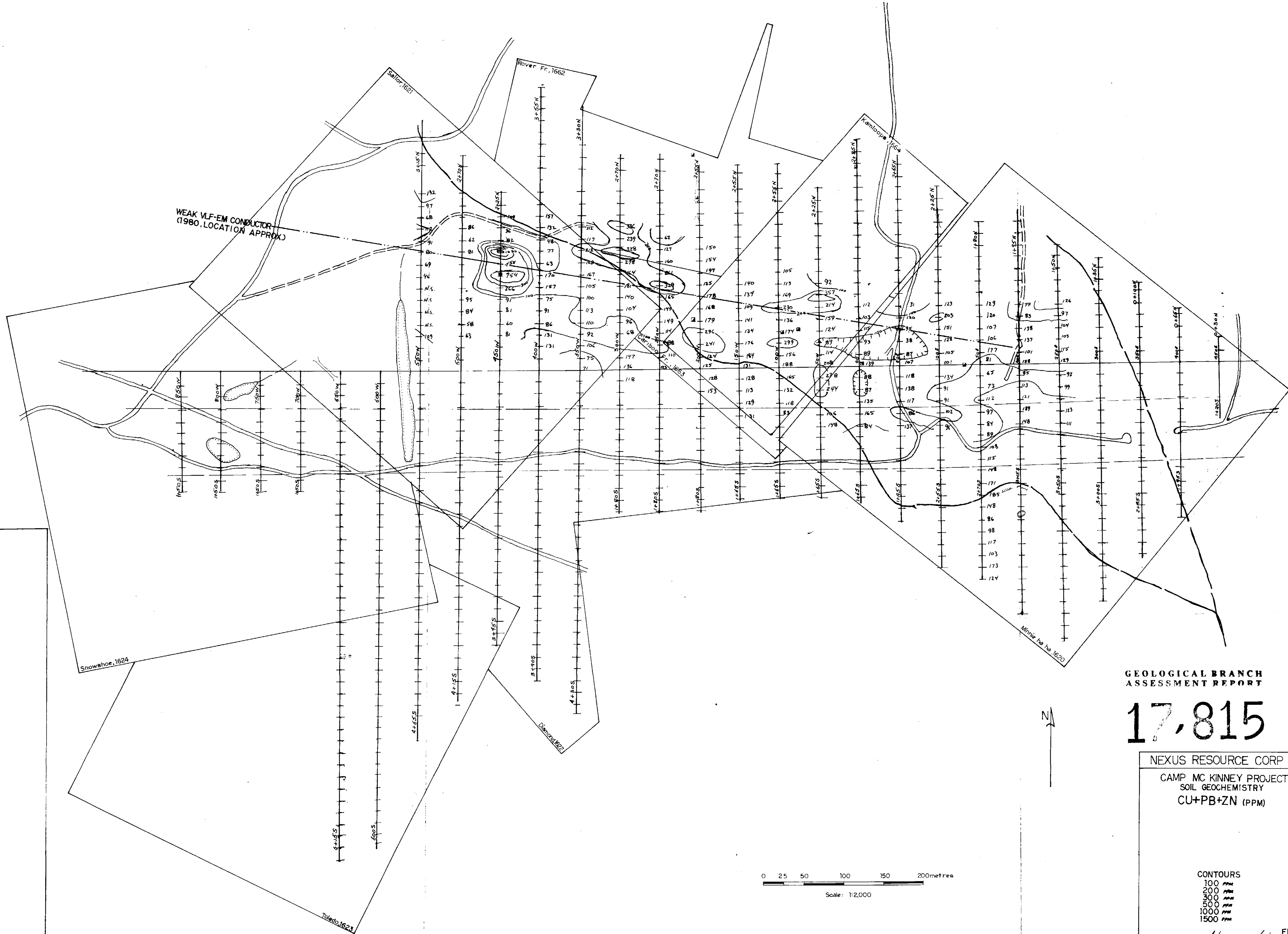
NEXUS RESOURCE CORP

CAMP MC KINNEY PROJECT
CONTOURED SOIL GEOCHEMISTRY
CU, PB, ZN

500
300
200
100
50
25

FIG.6

Work By: J.W. Drafted By: J.W. Date: 15/07/88



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,815

NEXUS RESOURCE CORP

CAMP MC KINNEY PROJECT
SOIL GEOCHEMISTRY
CU+PB+ZN (PPM)

FIG.7

Work By: Drafted By: Date: