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**GEOLOGY · GEOPHYSICS
MINING ENGINEERING**

Suite #704-850 WEST HASTINGS STREET, VANCOUVER, B.C.
TELEPHONE (604) 681-0191 V6C 1E1

GEOCHEMICAL and GEOPHYSICAL REPORT

on the

LODE I-IV CLAIMS

FILMED

Similkameen Mining Division - British Columbia

Lat. $49^{\circ} 29'$ N.

Long. $120^{\circ} 50'$ W.

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for

INTER-CANADIAN DEVELOPMENT CORP.

**G E O L O G I C A L B R A N C H
A S S E S S M E N T R E P O R T**

17,819

by

D. G. Allen, P.Eng. (B.C.)

and

Douglas J. Brownlee, Geologist, B.Sc.

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Vancouver, B.C.

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SUMMARY

Inter-Canadian Development Corp. holds title to the LODE I, III and IV claims (58 units), and has a 90% interest in the LODE II (20 units) claim in the Tulameen River area of British Columbia. The properties are situated 9 kilometres west of Tulameen and 27 kilometres northwest of Princeton.

Principal lithologies in the claim area are the Nicola Group metavolcanic and metasedimentary rocks along the western margin of LODE I and LODE II and the Tulameen ultramafic complex underlying the remainder of the claim group. Potential mineral targets are copper/gold deposits associated with alkalic phases (similar to the Copper Mountain Intrusions) of the Tulameen Complex and platinum/nickel/chromite or massive iron deposits associated with ultramafic members of the Complex.

In late 1987 and early 1988 an exploration program comprising soil sampling, magnetometer and VLF-electromagnetic surveys, was conducted on 22 line kilometres of grid on the eastern half of the property. Results of this work indicate that multielement geochemical data and geophysical data are useful in mapping the differing lithologies of the Tulameen Complex underlying the property. This data has shown that the hornblende clinopyroxenite underlying the northeastern portion of the grid probably extends northwesterly across the grid. In addition, a chromium, nickel and platinum anomaly with an associated magnetic high possibly reflects a plug of olivine clinopyroxenite in the southwest central portion of the grid. Also, a possible compositional change in the gabbro to a sulphide-enriched hornblende gabbro in the northwest corner grid may be reflected in the increase in iron, calcium, barium, vanadium, phosphorous, manganese and titanium.

Four areas have been delineated by this exploration program as warranting follow-up work. The area of major interest is in the northwest corner of the grid where there is an 800 by 800 metre copper (up to 598 parts per million) anomaly in soil with associated scattered gold (up to 86 parts per billion) and palladium (up to 69 ppb) values.

In the east central portion of the grid is a 500 by 100 metre anomaly comprised of platinum (up to 61 ppb), palladium (up to 230 ppb) and copper (up to 282 ppm). Two separate chromium (up to 986 ppm) platinum (up to 62 ppb), nickel (up to 359 ppm) and arsenic (up to 138 ppm) anomalies lie in the southwest portion of the grid. The larger of these two anomalies overlies the olivine clinopyroxenite on the southern edge of the grid and is 400 by 400 metres in size. The second anomaly is roughly circular in shape with a diameter of about 150 metres in the southwest central portion of the grid.

A follow-up exploration program is proposed.

CONCLUSION

The utilization of the geochemistry and geophysics has greatly aided in defining the property geology and areas of interest on the eastern half of the LODE claims.

Four areas have been identified correlating to three potential target types:

- 1) a copper/gold anomaly occurring in the northwest corner of the grid overlying a possible sulphide-bearing hornblende gabbro may indicate an alkalic porphyry target similar to the nearby Copper Mountain deposit (56 million tons of 0.53% copper and 0.018 ounces per ton gold),
- 2) two platinum/chromium/nickel anomalies overlying the olivine clinopyroxenite in the southwest portion of the grid suggest possible chromite cumulates, and
- 3) a platinum/palladium/copper anomaly over the hornblende clinopyroxenite is a possible indication of sulphides. All major PGM (platinum group metals) world producers mine platinum from sulphide-rich horizons found in ultramafic intrusions and extrusions.

RECOMMENDATIONS

A two phase program is proposed to fully evaluate the mineral potential of the LODE property. Phase I will comprise continued geochemical and geophysical surveys on the western portion of the property which covers the Tulameen complex. It will also include geological mapping and trenching of the copper-gold, platinum-chromium-nickel and platinum-palladium-copper anomalies to determine bedrock sources of the anomalies and provide geological information. Rock geochemical sampling should be conducted on the magnetite occurrences on the western part of the claim group to investigate their potential to host platinum group element mineralization.

Depending on results of Phase I, a follow-up Phase II program of geological mapping and trenching on targets generated on the western portion of the property may be warranted. Estimated costs of Phase I and Phase II are \$70,000 and \$130,000, respectively, for a grand total of \$200,000.

ESTIMATED COST OF RECOMMENDATIONS

PHASE I Geochemical and geophysical surveys, geological mapping and trenching.

Salaries

Geologist	30 days @ \$350/day	\$ 10,500
3 Assistants	90 days @ \$200/day	18,000
Room and Board	120 days @ \$35/day	4,200
Vehicle Rental		2,000
Material and Camp Supplies		1,500
Instrument Rental		1,250
Geochemical Analyses (ICP, Au, Pt, Pd)	700 samples @ \$18.50 ea.	12,950
Backhoe for Trenching	80 hours @ \$75/hour	6,000
Report and Maps		7,500
	Subtotal	\$ 63,900
	Contingencies	<u>6,100</u>
	TOTAL PHASE I	\$ 70,000

PHASE II Geological mapping, trenching, diamond drilling.

Salaries

Geologist	30 days @ \$350/day	\$ 10,500
Assistant	30 days @ \$200/day	6,000
Room and Board	60 man days @ \$35/day	2,100
Vehicle Rental		2,000
Backhoe for Trenching	80 hours @ \$75/hour	6,000
Bulldozer Site Preparation	25 hours @ \$90/hour	2,250
Drilling (all incl.)	2,000 feet @ \$35/foot	70,000
Geochemical Analyses (ICP, Au, Pt, Pd)	250 samples @ \$18.50 ea.	4,625
Material and Supplies		2,500
Report and Maps		10,000
	Subtotal	115,975
	Contingencies	<u>14,025</u>
	TOTAL PHASE II	\$130,000
	GRAND TOTAL PHASES I AND II	\$200,000

INTRODUCTION

Inter-Canadian Development Corp. holds a 100% interest in the LODE I, III and IV claims and a 90% interest in the LODE II claims. The claim group covers part of the Tulameen ultramafic-syenogabbro intrusion in the Tulameen River region of British Columbia.

The Tulameen complex and surrounding Nicola Group rocks in the past have been the target of exploration for various commodities including gold, platinum, copper, nickel, chromium, iron and diamonds. Placer operations on the Tulameen River and several of its tributaries have recovered over 30,000 ounces of gold and 20,000 ounces of platinum since the turn of the century. Several companies, as well as the Provincial government (Nixon and Rublee, 1988; Hora and White, 1988) are currently evaluating the mineral potential of the complex. Newmont Exploration of Canada Ltd. is systematically sampling chromitite occurrences for platinum and palladium, and also conducting bulk sample tests in an effort to evaluate the foundry sand potential of the olivine-rich dunite. Tiffany Resources Ltd. is investigating the iron reserves on Lodestone Mountain (immediately southeast of the LODE III claim) for platinum group element potential.

A work program comprised of soil geochemical and magnetometer surveys was conducted on the LODE claims on behalf of Inter-Canadian by D. Morneau, B. Stewart, K. Stewart, and C. Hopping on September 11th to 15th, 1987. The survey area was subsequently expanded and additional geochemical, magnetometer and VLF-electromagnetic surveys were conducted during the period of November 16th to 27th 1987. This expanded work program was conducted by D. Morneau, G. Manning, D. Hebditch, D. Carstens, G. Avery, A. Foote and B. Dixie. Work was limited to the eastern part of the claim block because of relative ease of access and heavy snow conditions. In addition, the location of the Legal Corner Posts of the LODE I to IV claims was determined by a land survey by B. Winterburn. This report summarizes the results of these surveys, and reviews some of the literature pertaining to the geology and mineralization of the Tulameen Complex.

LOCATION, ACCESS AND PHYSIOGRAPHY

The LODE claims lie on the southern flank of Olivine Mountain, nine kilometres west-southwest of the town of Tulameen and 27 kilometres west-northwest of Princeton (Figures 1 and 2).

Access is via paved road to the town of Coalmont then by good logging roads to the claims.

Elevations of the claims range from 1400 metres (4,500 feet) to 1800 metres (6,000 feet). Slopes in general are gentle, except along the upper flanks of Olivine Mountain where the average slope is 30 degrees. The region has been logged over most of the claims but steeper slopes are covered by a virgin growth of fir, balsam and spruce. The climate is moderate with an average yearly snow pack of one to two metres which lasts until late May.

HISTORY

The Tulameen area is one of British Columbia's oldest placer mining camps, having been discovered prior to 1885. Platinum of economic concentrations was recognized in 1891. Recorded placer production from 1886 to 1941 was 37,422 ounces of gold (Holland, 1950) and an estimated 20,000 ounces of platinum (estimated by O'Neill and Gunning, 1934). Source of the gold and platinum is believed to be the Nicola Group rocks and Tulameen Complex, respectively. Higher grade pockets of platinum in bedrock have been noted by various government workers mapping the Tulameen Complex, e.g., Camsell (1913), Rice (1947), Eastwood (1959), Findlay (1969). Minor bedrock mining of platinum was attempted during the Second World War (H. Jones, personal communication). Exploration over the past decade has concentrated on the copper and iron potential in the area. Imperial Metals and Power Ltd. by 1972 had delineated by drilling 176.9 million tonnes grading 14.5% iron on Lodestone Mountain including 89.5 million tonnes grading 15.54% iron and 0.48% vanadium (B.C. Ministry of Mines Mineral Deposits File). Tiffany Resources has since acquired control of the Lodestone Mountain magnetite deposits and

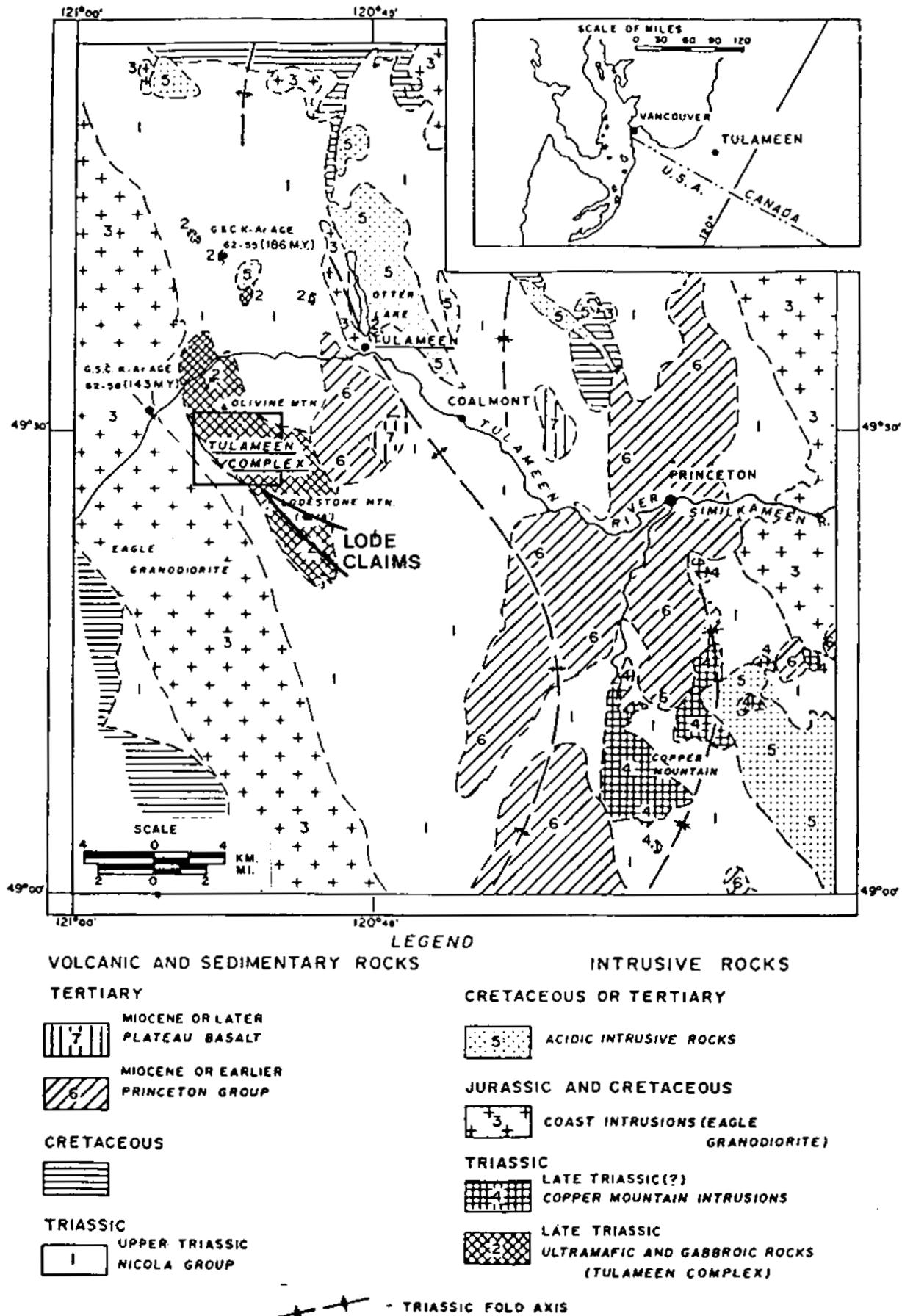
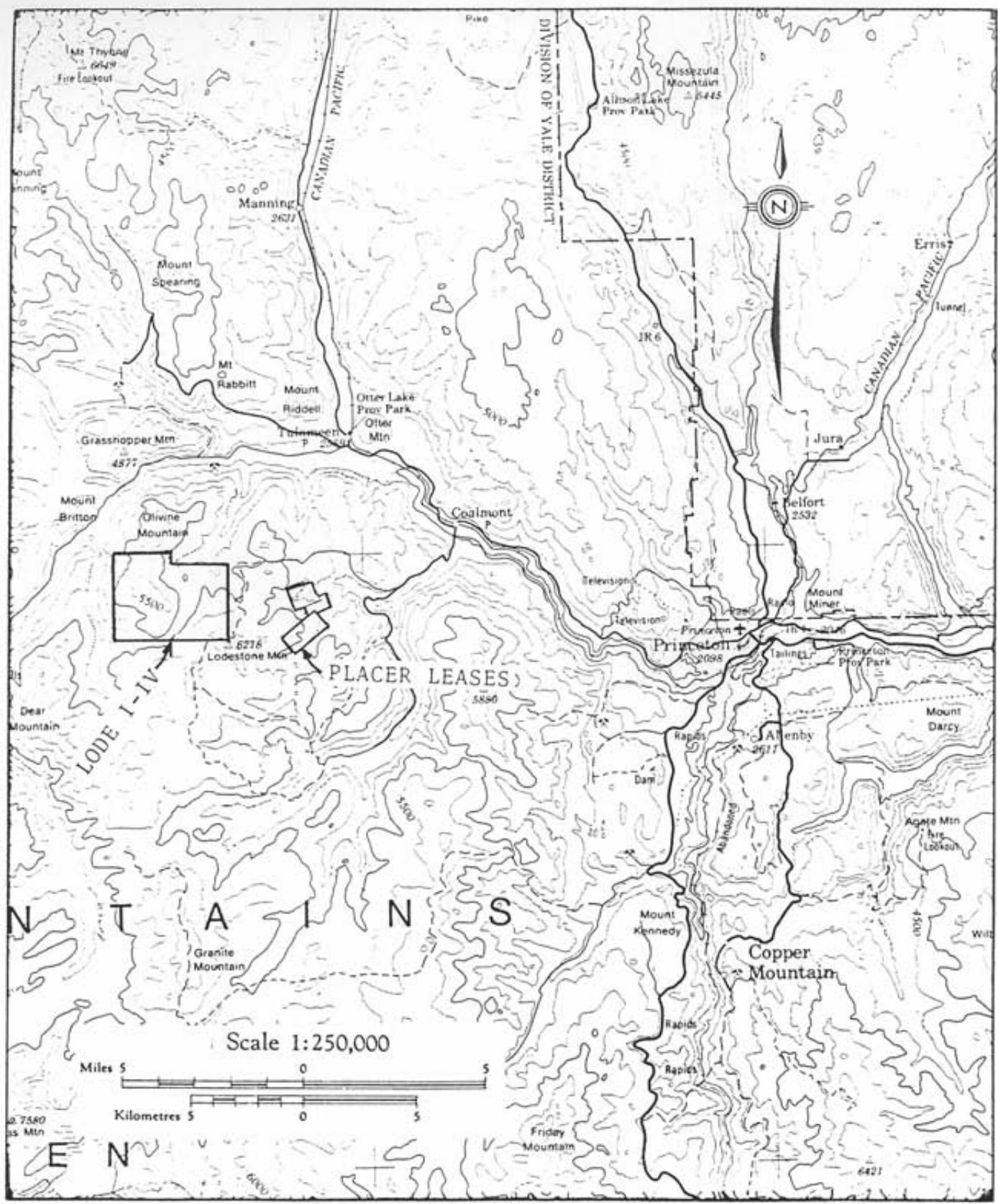


Figure 1. Location and regional geology of Tulameen River area (after Rice, 1947).



INTER-CANADIAN DEVELOPMENT CORP.

ACCESS MAP

TULAMEEN RIVER PROPERTIES

Similkameen Mining Division - British Columbia

 *Donald G. Allen*
exploration Ltd.

is re-assaying for their platinum group element potential. The recent increase in price of platinum has rekindled interest in the Tulameen Complex as a potential host for platinum deposits.

A drill site with some scattered drill core was found on the western part of the property but a search of government records has availed no systematic exploration of the LODE claims.

CLAIM DATA

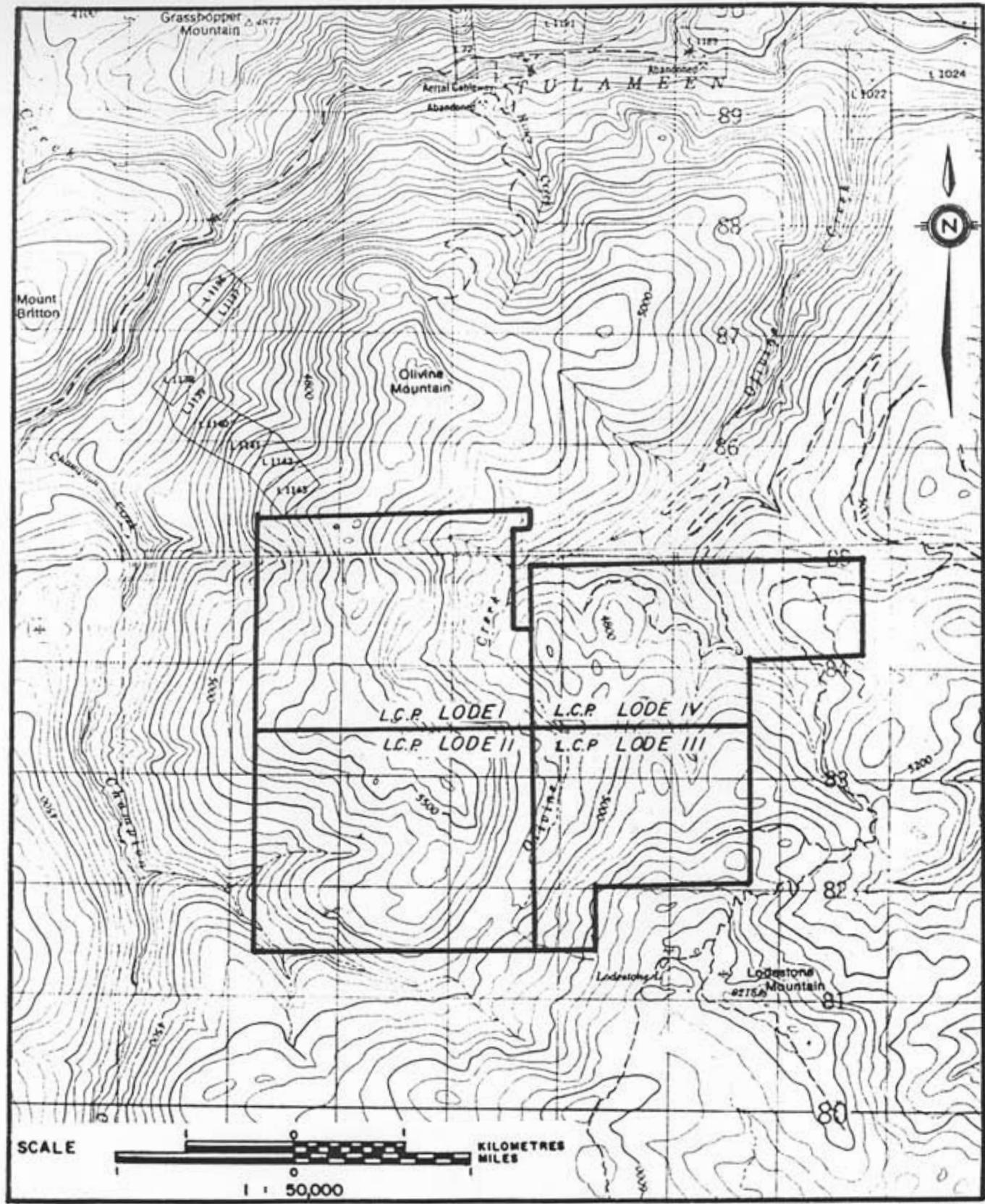
The LODE property comprises the following claims (Figure 5):

<u>Claim Name</u>	<u>No. of Units</u>	<u>Record No.</u>	<u>Expiry Date</u>
LODE I	20	1223 (11)	November 5, 1988
LODE II	20	1240 (11)	November 13, 1988
LODE III	20	1713 (9)	September 17, 1988
LODE IV	18	1712 (9)	September 17, 1988

GEOLOGY

Regional Geology

The Inter-Canadian Development properties are situated in the Princeton Map Area (Rice, 1947). The Tulameen River area is underlain by metasedimentary and metavolcanic schists of the Upper Triassic Nicola Group (unit 1, Figure 1) that have been intruded by syenogabbroic and ultramafic rocks of the Tulameen Complex. According to Findlay (1969), Nicola rocks in the Tulameen area are dominantly albite-epidote-amphibole schists and calcareous greenschists derived from andesitic to basaltic flows. Metasediments, including argillaceous quartzites, quartz-mica-plagioclase schists, and crystalline limestone bands, are subordinate. Other intrusions in the area include the Eagle granodiorite (a member of the Coast Plutonic Complex, unit 3) and the Copper Mountain intrusions (unit 4). The latter are indicated by Findlay to be related to the gabbroic phases of the Tulameen Complex. Tertiary sedimentary rocks (units 6 and 7) outcrop to the east and southeast of the complex.



INTER-CANADIAN DEVELOPMENT CORP

CLAIM MAP

LODE CLAIMS

Similkameen Mining Division - British Columbia

Local Geology

The LODE claims cover part of the Tulameen ultramafic-gabbroic complex and Nicola Group volcanic rocks on the west side of the complex (Figures 4 and 5). The geology and various aspects of the economic geology of the complex have been well described by Camsell (1913), Ruckmick (1956), Eastwood (1959), Findlay (1969), Roberts et al (1970), and Nixon and Rublee (1988).

The Tulameen Complex is an "Alaskan-type" ultramafic complex. According to Findlay:

"...the ultramafic units form an elongate body that dips steeply to the west and is bordered by, and partly overlain by gabbroic rocks (Fig. 2). Gabbroic and ultramafic rocks occur in about equal amounts, but their distribution is asymmetric, with the former mainly restricted to the eastern and southeastern parts of the complex. The total exposure area of the complex is about 22 sq. m. (57 km^2).

Ultramafic rocks outcrop in three areas within the complex...

The principal ultramafic rocks are dunite, olivine clinopyroxenite, and hornblende clinopyroxenite. Peridotite, clinopyroxenite, hornblende-olivine clinopyroxenite, and hornblendite are subordinate and generally not mappable units. A minor feldspathic rock - mafic pegmatite - is probably a late differentiate of the ultramafic suite.

In the northern part of the complex, the ultramafic units display the characteristic zonal pattern of similar intrusions in Alaska and U.S.S.R., comprising a dunite core surrounded by shells of olivine clinopyroxenite and hornblende clinopyroxenite. South of Olivine Mountain, where dunite is not exposed, the two main ultramafic zones contain a median zone of olivine clinopyroxenite bounded by hornblende clinopyroxenite. In the Tanglewood Hill area, hornblende clinopyroxenite is the principal ultramafic type exposed.

The principal gabbroic types are syenogabbro and syenodiorite with the former most abundant. In addition to forming the large mass lying to the east of Lodestone Mountain, gabbroic rocks occur elsewhere as smaller bands and lenses notably south of Olivine Mountain along the west margin of the complex, on the northeast flank of Olivine Mountain, and on Lodestone Mountain."

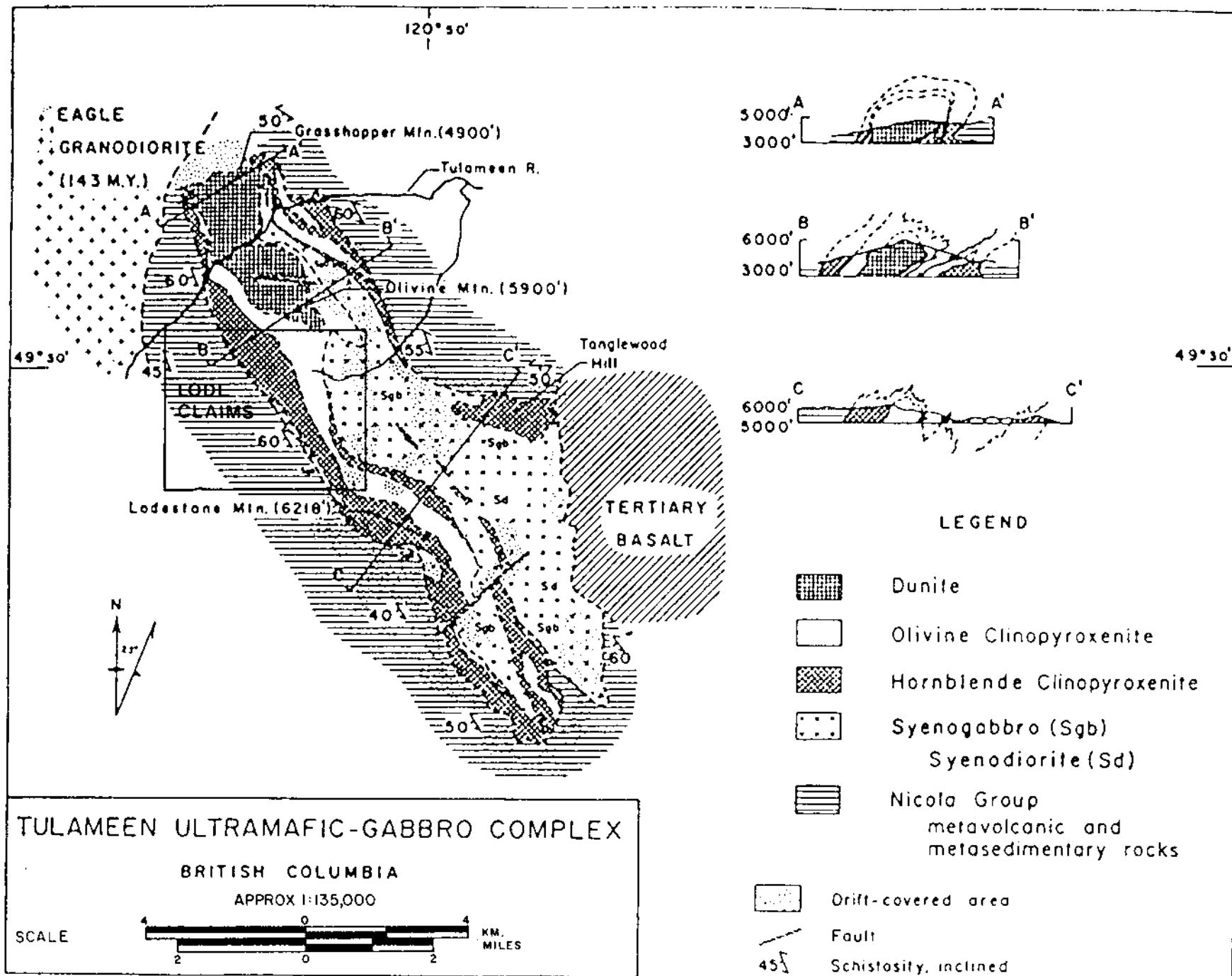


Figure 4. Geology and structure of Tulameen Complex (after Findlay, 1969).

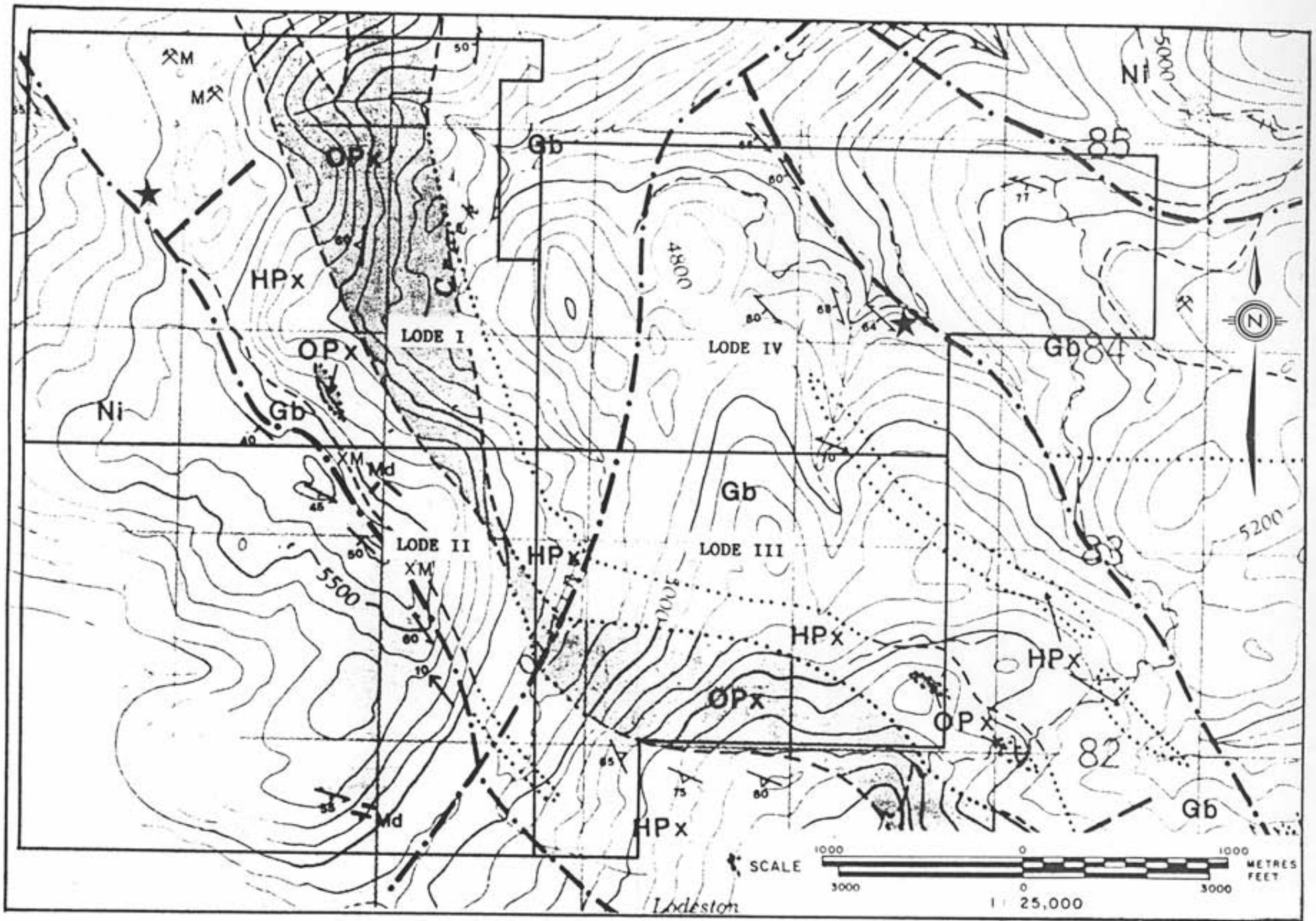


FIGURE 5

LEGEND

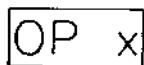
UPPER TRIASSIC (Carnian-Norian)

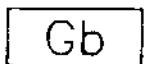
 Ni Nicola Group

LATE TRIASSIC

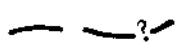
TULAMEEN ULTRAMAFIC COMPLEX

 HP x Hornblende clinopyroxenite

 OP x Olivine clinopyroxenite

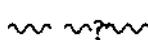
 Gb Gabbro-syenodiorite

SYMBOLS

 Geological contour;
Defined, Inferred.

S Sulphide showing.

M x Magnetite prospect.

 Fault; Defined, Inferred.

 L.C.P., Claim boundary.

 Topographical contours;
100 metre intervals.

Outcrops on the Lode claims are not abundant because of glacial drift and forest cover. Regional mapping by Nixon and Rublee (1988) indicate that the LODE claims are underlain mainly by syenogabbro, peridotite (olivine clinopyroxenite) and pyroxenite (hornblende clinopyroxenite) and Nicola Group metavolcanic rocks. Metavolcanic rocks observed by Allen (1986) in drill core and on surface on the LODE II claim are chlorite schists.

MINERALIZATION

Lode Deposits

In addition to the large tonnage low-grade iron deposits, minor amounts of copper, chromite, platinum, and diamonds have been reported in the ultramafic-gabbroic phases of the Tulameen Complex. However, except for drilling by Imperial Metals on the Lodestone Mountain magnetite deposit, there appears to have been little systematic exploration for such deposits until recently. This may in part be due to extensive forest cover and lack of outcrops.

Magnetite: magnetite in the Tulameen complex was studied by Eastwood (1959) and Ruckmick (1956). Abundant magnetite occurs in the pyroxenite phase and locally in the peridotite-dunite. Mapping by Ruckmick outlined a large area containing greater than 20% magnetite, including parts of the Lode claims. Drilling by Imperial Metals on Lodestone Mountain and Tanglewood Hill has outlined 176.9 million tonnes grading 14.5% iron. Two samples of magnetite-rich pyroxenite sampled by Allen (1986) from the LODE I and II were found to contain 15 to 20% Fe_2O_3 indicating that a large tonnage of similar material may be present on the Lode claims.

Copper: copper occurrences are reported in the Olivine Mountain area. According to Camsell (1913) they appear to be confined to east-west zones of shearing although chalcopyrite is a primary mineral in places. Several rusty shear zones have been examined and sampled by Allen (1986). Copper values obtained were up to 430 ppm (0.043% Cu).

Chromite: chromite occurs near the outer borders of the peridotite phase of the Tulameen Complex. It is a primary mineral and occurs as disseminated grains scattered throughout the peridotite and locally as irregular veins or masses up to 10-15 centimetres in diameter.

Platinum: the ultramafic complex is undoubtedly the source of platinoid minerals in the Tulameen placer deposits. Findlay (1963) studied the distribution of platinum in the major rock types of the complex and found highest concentrations (up to 0.0225 ppm Pt) in the dunites and peridotites. St Louis et al (1986) showed that platinum group elements occur in chromitite lenses in the dunite core of the intrusions and that palladium is concentrated in hornblende clinopyroxenite and gabbroic rocks. Tiffany Resources Inc. are currently sampling the magnetite deposits on Lodestone Mountain for their platinum group element potential.

Diamonds: Camsell (1913) reports the presence of diamonds, which are associated with chromite in the dunite. The diamonds are small and of good quality but break up on exposure to the atmosphere.

Placer Deposits

The Tulameen River area is well-known for its placer gold and platinum deposits. The placer deposits were described by Camsell (1913), O'Neill and Gunning (1934) and Raicevic and Cabri (1976). The placer leases held by Inter-Canadian Development Corp. cover tributaries of Granite Creek which was one of the most productive creeks in the Tulameen camp.

The gold and platinoid minerals in the camp are accompanied by chromite, magnetite and, in places, native copper. The platinoid minerals, chromite and magnetite, were derived by erosion of the ultramafic rocks of the Tulameen Complex. The gold is thought to have originated from gold-bearing veins in Nicola Group rocks in the vicinity of Grasshopper Mountain, but this has not been proven.

According to Raicevic and Cabri:

"The gold and platinum of the placers must have been released from the parent rocks in preglacial time and deposited in preglacial placers, because, since glacial times, although canyons have been cut in the floors of some of the valleys, erosion has not succeeded in removing the mantle of glacial debris over most of the area, much less eroding any quantity of the underlying rock. Some dissipation of preglacial placers must have occurred, as well as further concentration during postglacial times by reworked deposits in the present river beds. The ice-sheet also filled up some valleys with detritus so that, in some cases, the streams did not re-occupy their original channels after the retreat of the ice. There is, therefore, the possibility of the occurrence of buried placer deposits."

GEOCHEMICAL SURVEY

A soil sampling survey was undertaken on a 22 line kilometre grid with a 200 metre line spacing and a 50 metre station spacing. A total of 412 soil samples were collected, each sample comprising 0.25 to 0.5 kilograms of "B" horizon material collected from a depth of 20 to 40 centimetres. Overburden on the gentler slopes consists predominantly of glacial till. Colluvium and residual soils are found on the steeper slopes and hill tops. Samples were placed in Kraft paper bags and shipped to Acme Analytical Laboratories in Vancouver for 30 element analysis I.C.P. (inductively coupled plasma) spectrometry and fire assay concentration followed by mass spectrometry analyses for gold, platinum and palladium. The anomalous ranges for each element is determined by inspection of the data, previous experience in the area and basic statistical analysis of the data (Appendix II). Analytical data is presented in Appendix I and plots of selected elements presented in Figures 6a to 6t. Gold, platinum and palladium values are recorded in parts per billion (ppb), major elements in percent (%) and all others in parts per million (ppm).

Although till of various thickness overlies nearly all of the surveyed area, precious metals, base metals and minor element enrichments appear to define underlying rock units. The olivine clinopyroxenite (OPx, Figure 5), which underlies portions of lines 17S, 19S and 21S, is characterized by anomalous amounts of chromium (100 to 635 ppm), nickel (70 to 187 ppm), arsenic (20 to 136 ppm), platinum (10 to 72 ppb) and weak barium (100 to 424 ppm), calcium (0.79 to 1.1%) and manganese (700 to 1171 ppm). There is also a marked depletion of copper, strontium, phosphorous, aluminium, zinc, lead and silver.

The hornblende clinopyroxenite (HPx, Figure 5) adjoins the olivine clinopyroxenite in the southern portion of the grid and in the east central and northeast portion of the grid. This unit is characterized by magnesium (1.0 to 3.96%), barium (100 to 373 ppm), platinum (10 to 124 ppb), palladium (10-230 ppb), moderate vanadium (100 to 136 ppm), titanium (0.15 to 0.21%) and calcium (0.75 to 1.51%). The hornblende clinopyroxenite in the southern portion of the grid is also characterized by relatively high nickel (50 to 359 ppm), chromium (100 to 880 ppm) and arsenic (15 to 17 ppm) which do not characterize the hornblende clinopyroxenite in the central to northeast portion of the grid.

The geochemical pattern of the area underlain by gabbro appears to reflect a compositional change from the southwest portion of the grid to the trace of a northwest trending fault. This compositional change is shown in a north-northeasterly increase in iron (to 8.00%), calcium (to 1.81%), phosphorous (to 0.38%), barium (to 417 ppm), vanadium (to 255 ppm), manganese (to 2438 ppm), titanium (to 0.25%) and strontium (to 195 ppm). Additionally, palladium (to 69 ppb), cobalt (to 38 ppm), zinc (to 137 ppm), copper (to 598 ppm) and gold (to 86 ppb) reflect the compositional change in the gabbro and also show a general increase toward the northwest. The compositional change indicated by the geochemistry may indicate that a sulphide-enriched hornblende gabbro as described by Nixon and Rublee (1988) may underlie the northern portion of the grid.

LEGEND

- < 5.00
- 6 to 14
- 15 to 21
- 22 to 36
- 37 to 49
- > 50.00

Range of Values in parts per billion

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

SYMBOLS

— Geological contour; Defined, inferred.

S Sulphide showing.

M x Magnetite prospect.

~~ Fault; Defined, inferred.

L.C.P. Claim boundary.

~~~~ Topographical contours; 100 metre intervals.

### LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

### GEOCHEMICAL MAP GOLD

A&M exploration Ltd

FEBRUARY, 1988

N.T.S. 92 H/7.10

FIGURE 6a

### LEGEND

- < 10.00
- 11 to 19
- 20 to 29
- 30 to 39
- 40 to 49
- > 50.00

Range of Values in parts per million

### UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

### LATE TRIASSIC

#### TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

### SYMBOLS

- Geological contour; Defined, Inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~~~ Fault; Defined, Inferred.
- L.C.P., Claim boundary.
- 4800 Topographical contours; 100 metre intervals.

INTER-CANADIAN DEVELOPMENT CORP.

### LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

#### GEOCHEMICAL MAP PLATINUM

A.M exploration Ltd

FEBRUARY, 1988

N.T.S. 92 H/ 7.10

Ni

HPx

FIGURE 6D

### LEGEND

- < 10.00
- 11 to 19
- 20 to 29
- 30 to 39
- 40 to 49
- > 50.00

Range of Values in parts per billion.

### UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

### LATE TRIASSIC

#### TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

### SYMBOLS

— Geological contour,  
Defined, inferred.

S Sulphide showing.

M x Magnetite prospect.

~~~ Fault; Defined, inferred.

L.C.P. Claim boundary.

~~~~ Topographic contours,  
100 metre intervals.

LODE III LCP LCP LODE IV

HPx

Olivine

1000f

4800

GB

230

HPx

500

1250

0

1250

Metres

FEET

1 : 12,500

INTER-CANADIAN DEVELOPMENT CORP.

### LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

#### GEOCHEMICAL MAP PALLADIUM

A.M exploration Ltd

FEBRUARY, 1988

N.T.S. 92 H/ 7.10

Ni

HPx

FIGURE 6c

### LEGEND

- < 100
- 101 to 125
- 126 to 199
- 200 to 249
- 250 to 299
- > 300

Range of Values in parts per million

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

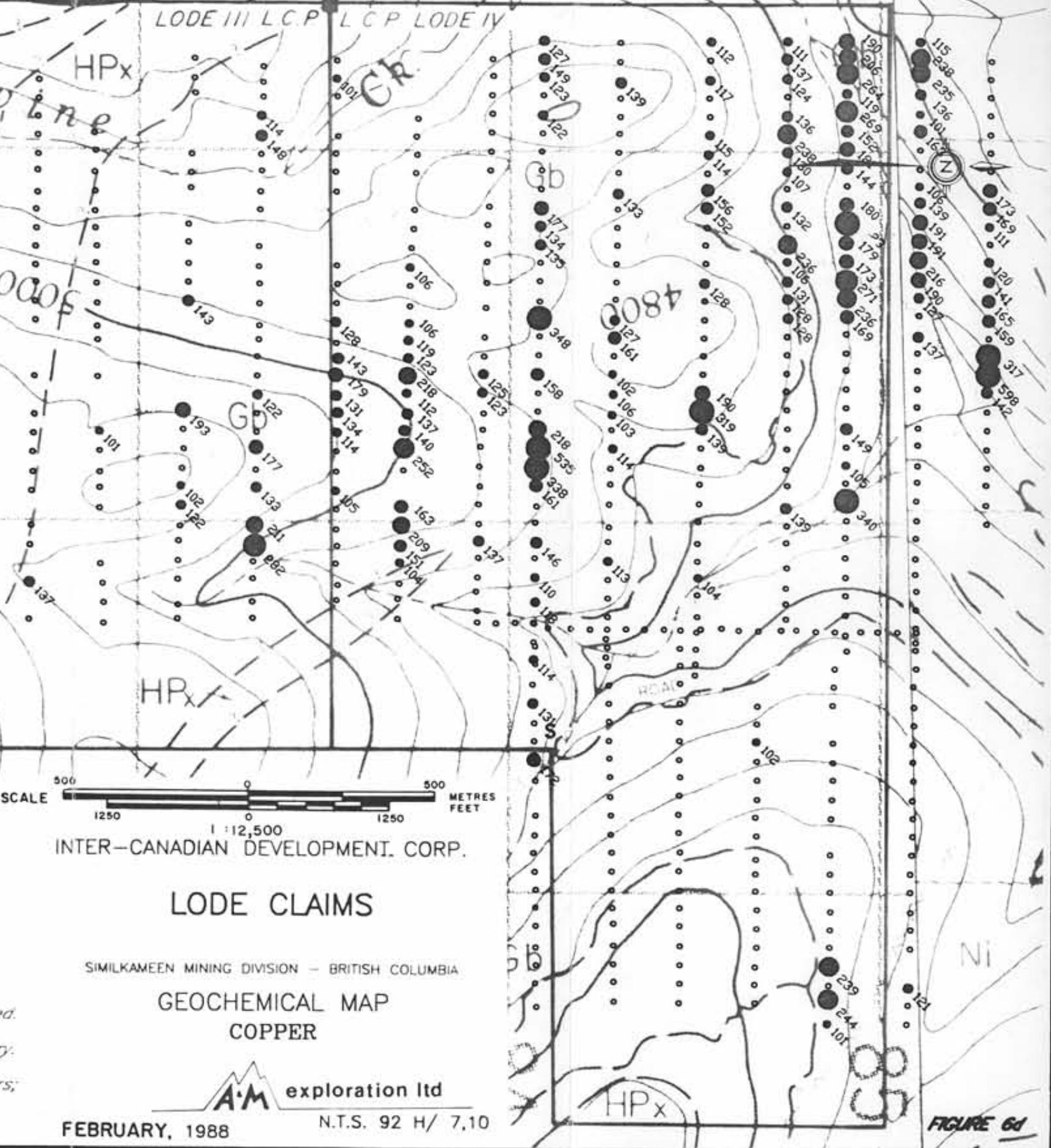
HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

### SYMBOLS

- Geological contour, Defined, inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~~ Fault, Defined, inferred.
- L.C.P., Claim boundary.
- ~~~~ Topographic contours, 100 metre intervals.



### LEGEND

- < 0.5
- 0.6 to 1.4
- 1.5 to 2.3
- 2.4 to 3.3
- 3.4 to 4.3
- > 4.4

Range of Values in parts per million

### UPPER TRIASSIC (Carnian-Norian)

**Ni** Nicola Group

### LATE TRIASSIC

#### TULAMEEN ULTRAMAFIC COMPLEX

**HP X** Hornblende clinopyroxenite

**OP X** Olivine clinopyroxenite

**Gb** Gabbro-syenodiorite

### SYMBOLS

—?— Geological contour, Defined, inferred.

S Sulphide showing.

M x Magnetite prospect.

~~~ Fault, Defined, inferred.

L.C.P. Claim boundary.

4800 Topographic contours, 100 metre intervals.

LODE III LCP LCP LODE IV

HPx

toadf

QP

HPx

?

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LEGEND

- < 10
- 11 to 19
- 20 to 29
- 30 to 39
- 40 to 49
- > 50

Range of Values in parts per million

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

SYMBOLS

- Geological contour, Defined, Inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~~ Fault, Defined, Inferred.
- L.C.P., Claim boundary.
- ~~~~ Topographical contours, 100 metre intervals.

INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP
LEAD

A.M exploration ltd

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N.T.S. 92 H/ 7.10

FIGURE 6

LEGEND

- < 100
- 101 to 199
- 200 to 299
- 300 to 399
- 400 to 499
- > 500

Range of Values in parts per million

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

- | | |
|------|----------------------------|
| HP x | Hornblende clinopyroxenite |
| OP x | Olivine clinopyroxenite |
| Gb | Gabbro-syenodiorite |

SYMBOLS

- Geological contour; Defined, Inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~~~ Fault; Defined, inferred.
- L.C.P. Claim boundary.
- 4800 Topographical contours; 100 metre intervals.

LODE III L.C.P. L.C.P. LODE IV

INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP
ZINC

A.M exploration ltd

FEBRUARY, 1988

N.T.S. 92 H/ 7.10

Ni

FIGURE 69

LEGEND

- < 20
- 21 to 26
- 27 to 33
- 34 to 40
- 41 to 48
- > 49

Range of Values in parts per million

UPPER TRIASSIC (Carnian-Norian)

Ni

Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x

Hornblende clinopyroxenite

OP x

Olivine clinopyroxenite

Gb

Gabbro-syenodiorite

SYMBOLS

- ?— Geological contour; Defined, Inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~~~ Fault; Defined, Inferred.
- L.C.P. Claim boundary.
- 4800 — Topographical contours; 100 metre intervals.

SCALE
0 500 500 METRES FEET
1250 0 1250
1 : 12,500
INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP
COBALT

A.M exploration ltd

FEBRUARY, 1988

N.T.S. 92 H/ 7.10

FIGURE 6A

LEGEND

- < 10
- 11 to 19
- 20 to 29
- 30 to 39
- 40 to 49
- > 50

Range of Values in parts per million

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

SYMBOLS

- ?— Geological contour; Defined, inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~?~~ Fault; Defined, inferred.
- L.C.P. Claim boundary.
- 4800 Topographical contours; 100 metre intervals.

INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP
ARSENIC

A.M exploration Ltd

FEBRUARY, 1988

N.T.S. 92 H / 7,10

Ni

HPx

FIGURE 61

LEGEND

- < 100
- 101 to 199
- 200 to 299
- 300 to 399
- 400 to 499
- > 500

Range of Values in parts per million

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

SYMBOLS

- Geological contour, Defined, Inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~~~ Fault, Defined, Inferred.
- L.C.P. Claim boundary.
- Topographical contours, 100 metre intervals.

INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP
CHROMIUM

AM exploration ltd

FEBRUARY, 1988

N.T.S. 92 H/ 7.10

FIGURE 6J

LEGEND

- < 50
- 51 to 126
- 127 to 203
- 204 to 280
- 281 to 358
- > 359

Range of Values in parts per million

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

SYMBOLS

- Geological contour, Defined, inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~ Fault, Defined, inferred.
- L.C.P. Claim boundary.
- 4800 Topographical contours, 100 metre intervals.

INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP
NICKEL

A.M exploration ltd

FEBRUARY, 1988

N.T.S. 92 H/ 7.10

Ni

FIGURE 6X

LEGEND

- < 5
- 5.1 to 5.9
- 6 to 6.9
- 7 to 8.9
- 9 to 9.9
- > 10

Range of Values in percent

UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

SYMBOLS

- Geological contour; Defined, Inferred.
- S Sulphide showing.
- M x Magnetite prospect.
- ~~~~ Fault; Defined, Inferred.
- L.C.P. Claim boundary.
- 4800 Topographical contours; 100 metre intervals.

INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP IRON

AM exploration ltd

FEBRUARY, 1988

N.T.S. 92 H/ 7.10

FIGURE 61

Additionally, the pattern for silver (up to 4.4 ppm), platinum (up to 32 ppb), palladium (up to 44 ppb), gold (up to 152 ppb), copper (up to 340 ppm) and lead (up to 205 ppm) appears to outline a parallel structure about 200 metres northeast of the projected trend of the eastern normal fault.

Gold (up to 287 ppb), silver (up to 3.6 ppm), copper (up to 244 ppm) and cobalt (up to 31 ppm) outline an anomalous zone in the northeast corner of the grid.

Chromium (up to 243 ppm), arsenic (up to 46 ppm), nickel (up to 268 ppm), strontium (up to 96 ppm), calcium (up to 1.15%) manganese (up to 4221 ppm) and titanium (up to 0.2%) outline a roughly circular zone north of the hornblende clinopyroxenite.

GEOPHYSICAL SURVEY

VLF-Electromagnetic Survey

A total of 19.5 line kilometres of a VLF-electromagnetic survey was completed on the LODE claims.

The VLF-electromagnetic method utilizes an electromagnetic field transmitted from radio stations in the 12 to 24 kilohertz range (long range submarine communication signals). The signals are propagated with the magnetic component of the field being parallel to the ground surface in undisturbed areas.

Conductivity contrasts (such as the presence of massive sulphides, graphitic shales or fault structures) in the earth's crust produce a local vertical component to the electromagnetic field and changes in field strength or amplitude. These conductive areas may be located and, to a degree, evaluated by measuring the various parameters of this electromagnetic field. A Sabre Model 27 VLF-electromagnetic receiver, tuned to Seattle, Washington, was used for all observations. This instrument is manufactured by Sabre Electronic Instruments. It measures the dip angle of the resultant field (in degrees) and the normalized horizontal component of the field strength (in relative percent).

Conductive zones are interpreted to underlie the point on a traverse line where changes in dip angle of the resultant field (from negative to positive - operator facing transmitter station) are associated with increased field strength. Data can be filtered by a technique described by Fraser (1969 - Geophysics, Vol. 34, No. 6, pp. 958-967) and can be presented in contour or profile form. Fraser filtered values, which are derived from dip angle measurements, show high positive values above a conductor. Results for the purposes of this report, including field strength and dip angle data are shown in profile form on Figures 7a to 7c.

Numerous weak to moderate conductors were located by the survey. All anomalies trend northwesterly and subparallel to the known geology and structure in the northern portion of the grid. The most consistent VLF-electromagnetic response is in the northeastern portion of the grid and is subparallel to the hornblende clinopyroxenite. They are interpreted as reflecting contacts of the major units and/or fault structures.

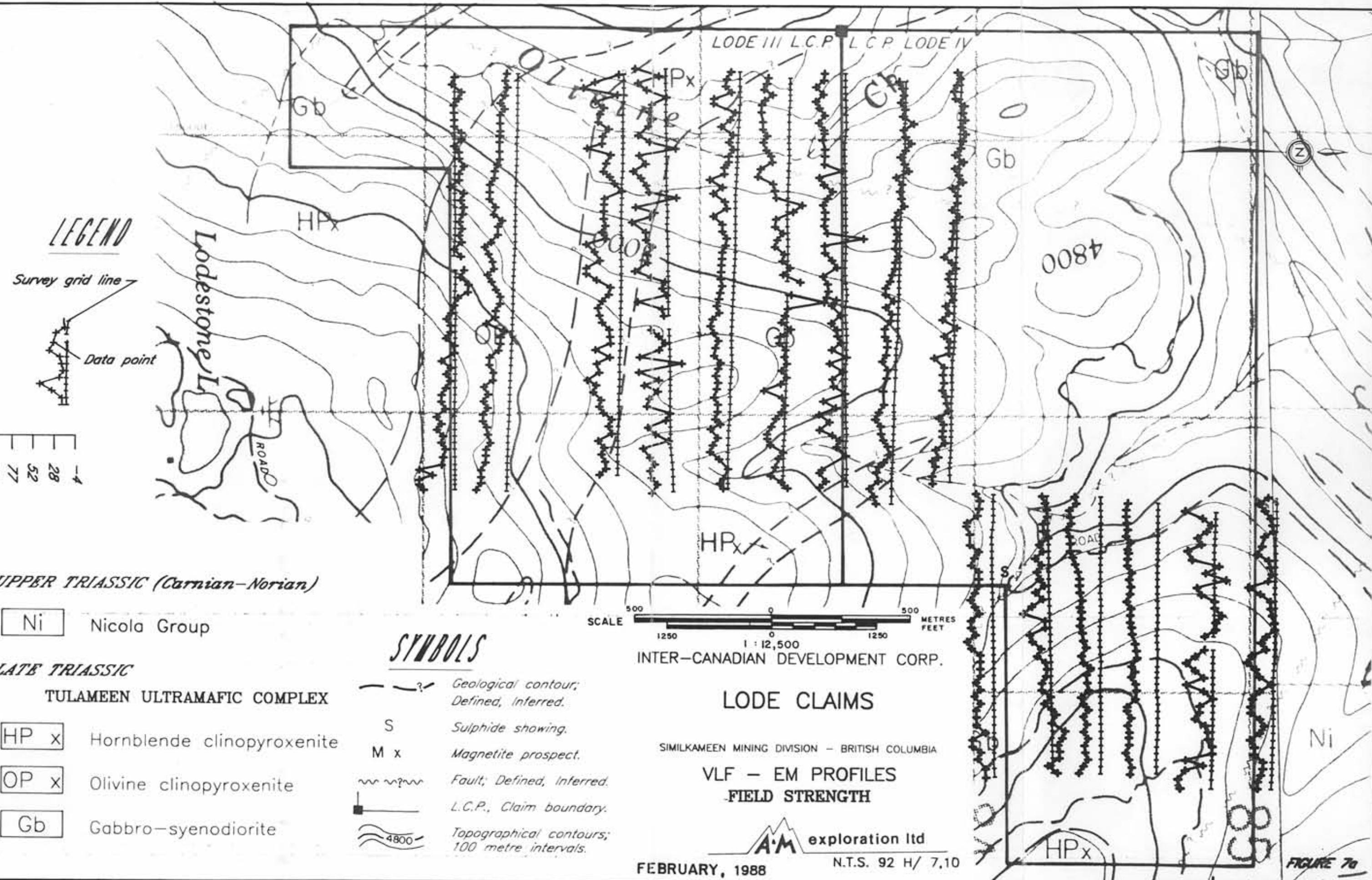
Magnetometer Survey

A magnetic survey of 22 line kilometres was run at 25 metre spacing utilizing a Scintrex MP-2 proton magnetometer. Data was corrected for diurnal variation and correlated with previous magnetometer data. The magnetometer data is presented in profile and contour form at a scale of 1:12,500 (Figures 8a and 8b) and as a 3D perspective (Figure 8c).

The magnetometer data reflects the underlying geology and structure of the property.

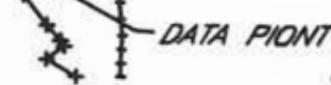
The hornblende clinopyroxenite which outcrops in the northeastern portion of the grid is shown to extend across the property, possibly not outcropping, by a 200 to 250 metre wide magnetic high (58,000 to 60,000 gammas).

The olivine clinopyroxenite in the southern portion of the property is reflected by a magnetic high (up to 65,000 gammas), while the flanking hornblende clinopyroxenite is reflected by moderately lower magnetic reading (up to 61,000 gammas).

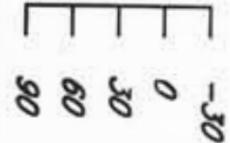


LEGEND

SURVEY GRID LINE



DATA POINT



UPPER TRIASSIC (Carnian-Norian)



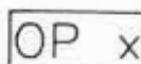
Nicola Group

LATE TRIASSIC

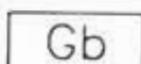
TULAMEEN ULTRAMAFIC COMPLEX



Hornblende clinopyroxenite



Olivine clinopyroxenite



Gabbro-syenodiorite

SYMBOLS

— ? Geological contour; Defined, Inferred.

S Sulphide showing.

M x Magnetite prospect.

~~?~~ Fault; Defined, Inferred.

L.C.P. Claim boundary.

4800 Topographical contours; 100 metre intervals.

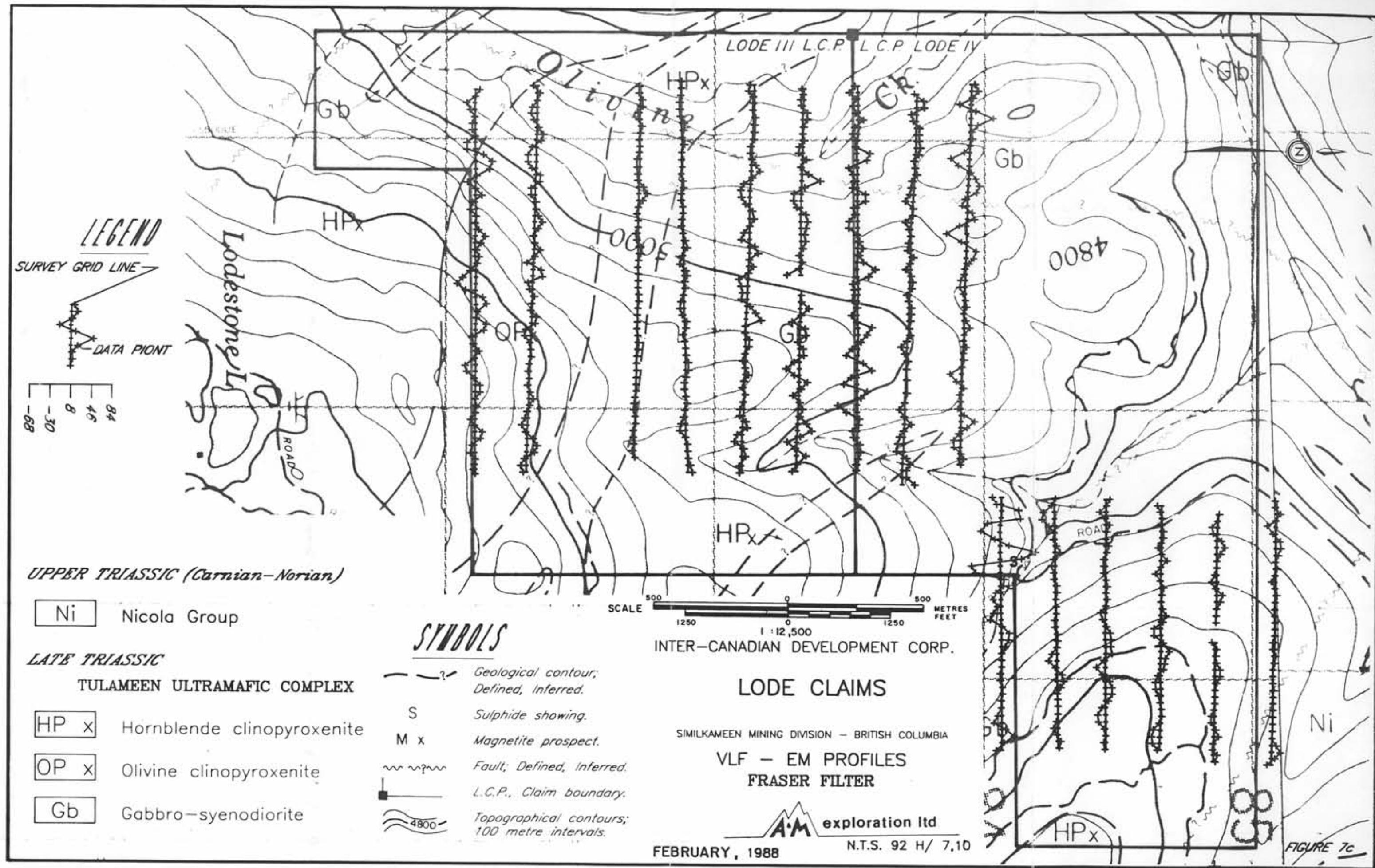
LODE III L.C.P. L.C.P. LODE IV

Px

OP

Gb

4800



The gabbro and the adjacent northwest trending fault covered by the central portion of the grid is reflected by a magnetic low (54,000 to 57,000 gammas) 300 to 400 metres wide.

The circular geochemical anomaly occurring in the southwest central portion of the grid is reflected by a magnetic high (to 61,000 gammas).

There are three magnetic lows trending north-northwest across the central and southern portions of the grid. These magnetic lows transect the olivine clinopyroxenite and also correspond with moderate VLF-electromagnetic anomalies and may represent fault structures.

DISCUSSION OF RESULTS

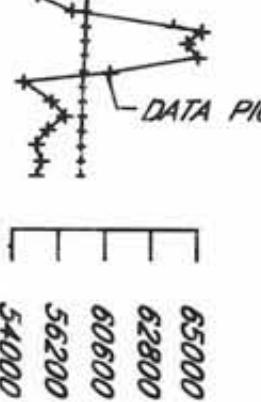
The geochemical and geophysical data obtained over the LODE grid mainly reflects the known geology of the property. Magnetic highs with related chromium, nickel, barium, calcium, manganese and minor vanadium and titanium reflected the hornblende and olivine clinopyroxenites and may be of economic interest in that the magnetite-rich unit may be a host for platinum group elements. The magnetic data was also able to trace the hornblende clinopyroxenite where it was hidden by overlying gabbro (Figure 9).

The gabbro is reflected by magnetic lows and associated iron, calcium, phosphorous, barium, vanadium, manganese, titanium and strontium. A compositional change in the gabbro from the southwest to northwest was shown by an increase in the above geochemical signature and a corresponding decrease in the magnetic field. This may reflect a compositional change to a sulphide-enriched hornblende gabbro as described by Nixon and Rublee (1988).

The platinum, nickel and chromium anomalies located in the southwestern portion of the grid indicate possible chromite cumulates in the olivine clinopyroxenite. The circular anomaly located in the southwest central portion of the grid with the associated magnetic high indicates a possible plug of olivine clinopyroxenite.

LEGEND

SURVEY GRID LINE



UPPER TRIASSIC (Carnian-Norian)

Ni Nicola Group

LATE TRIASSIC

TULAMEEN ULTRAMAFIC COMPLEX

HP x Hornblende clinopyroxenite

OP x Olivine clinopyroxenite

Gb Gabbro-syenodiorite

SYMBOLS

— Geological contour; Defined, Inferred.

S Sulphide showing.

M x Magnetite prospect.

~~~~ Fault; Defined, Inferred.

L.C.P., Claim boundary.

~~~~ Topographical contours; 100 metre intervals.

LODE III L.C.P. L.C.P. LODE IV

HPx

Gb

4800

SCALE 500 0 500 METRES FEET
1 : 12,500
INTER-CANADIAN DEVELOPMENT CORP.

LODE CLAIMS

SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA

MAGNETOMETER PROFILES
GAMMAS



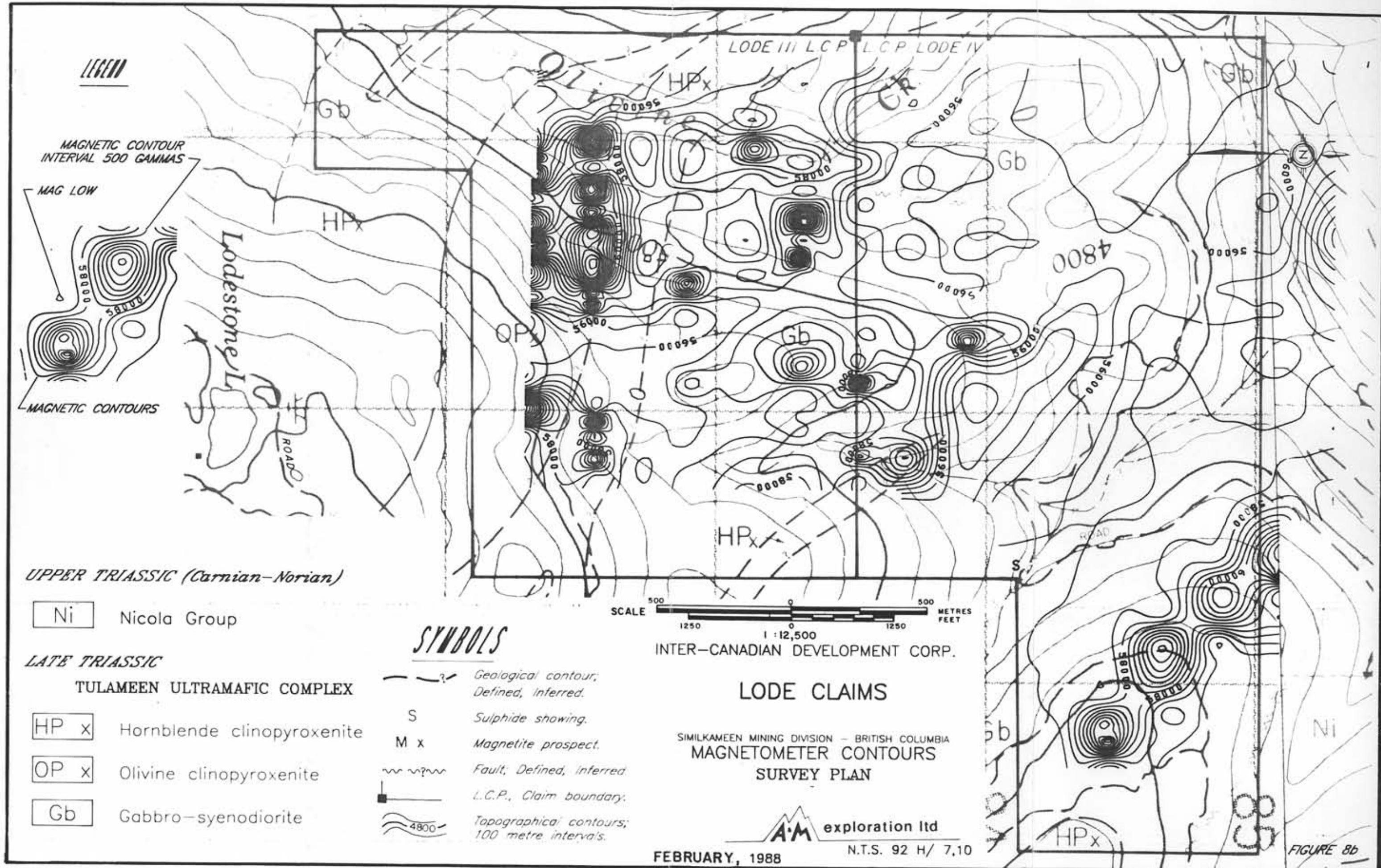
FEBRUARY, 1988

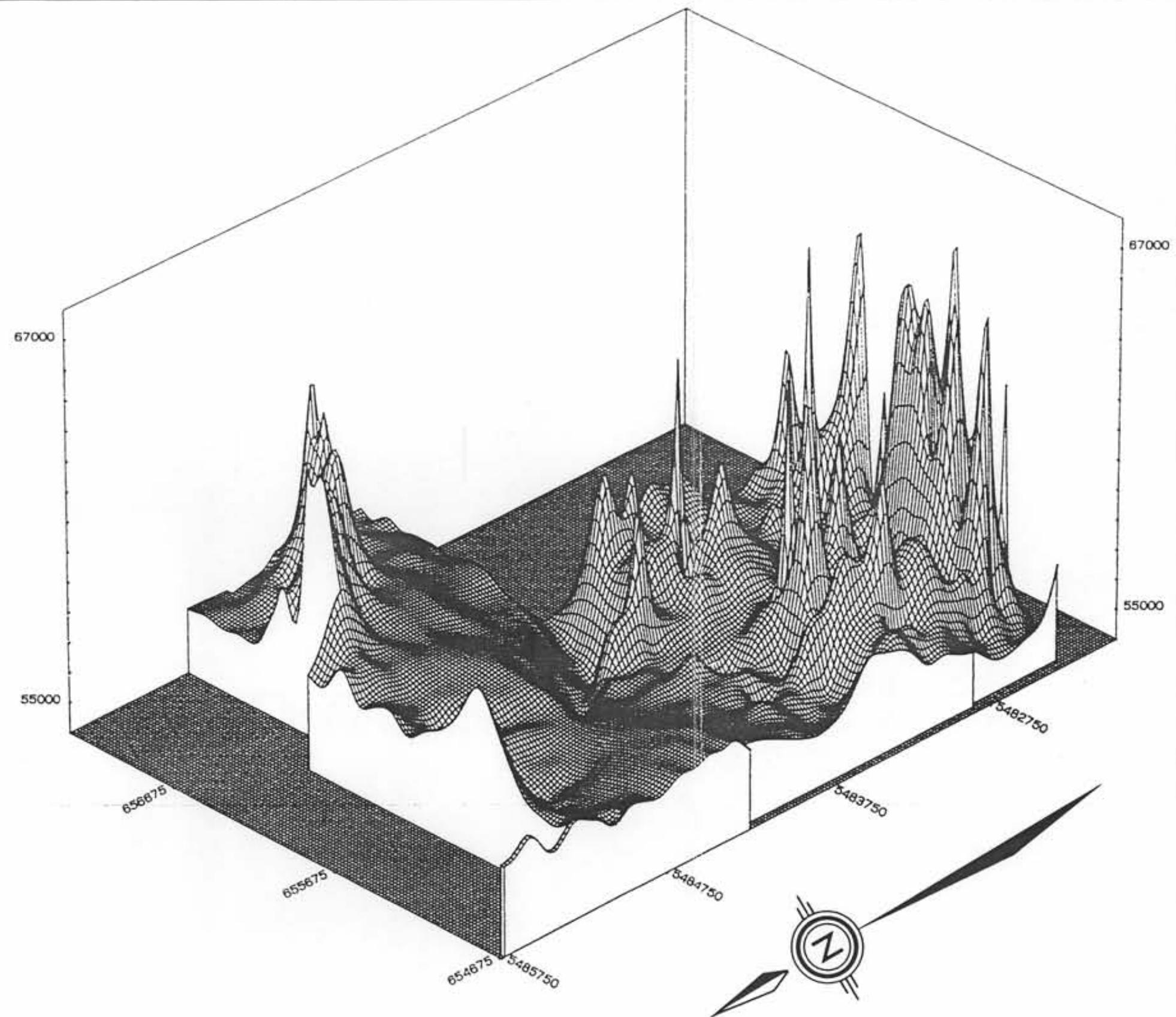
N.T.S. 92 H / 7.10

Ni

HPx

FIGURE 80





INTER-CANADIAN DEVELOPMENT CORP.
LODE CLAIMS
SIMILKAMEEN MINING DIVISION - BRITISH COLUMBIA
MAGNETOMETER SURVEY
3D PERSPECTIVE

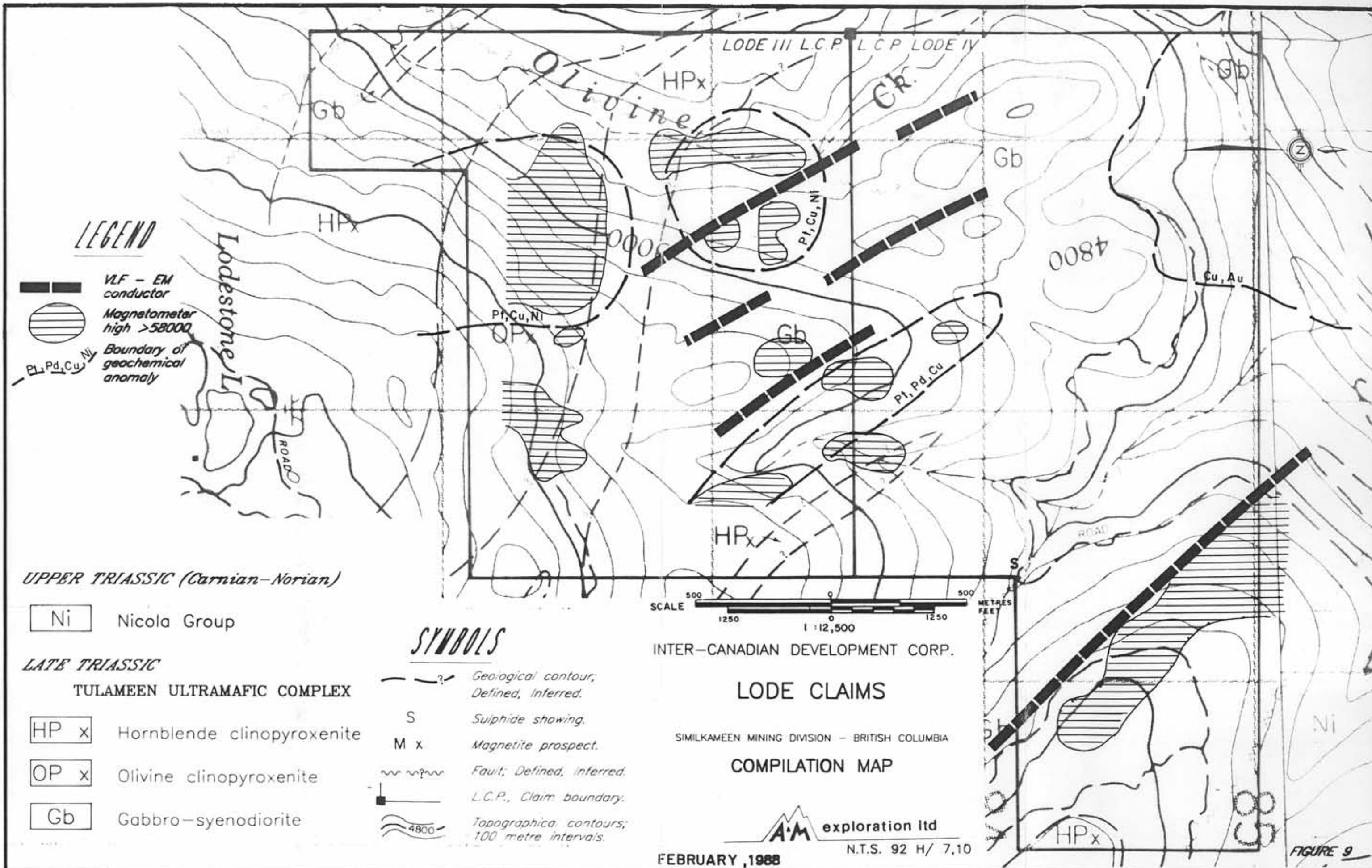
FEBRUARY ,1988

N.T.S. 92 H/ 7.10

FIGURE 8c

A platinum, palladium and copper anomaly overlying the central hornblende clinopyroxenite may indicate sulphides.

A handwritten signature in black ink, appearing to read "Douglas Brownlee". The signature is fluid and cursive, with a prominent 'D' at the beginning.



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CERTIFICATE

I, Douglas J. Brownlee, do hereby certify that:

1. I am a geologist residing at Suite 101, 2615 Lonsdale Avenue, North Vancouver, British Columbia.
2. I am a graduate in Geology Specialization from the University of Alberta (1980).
3. I have practised my profession in British Columbia since January, 1980.
4. This report is based on fieldwork completed by D. Morneau, B. Stewart, K. Stewart, C. Hopping during the period September 11th to 15th, 1987; and by D. Morneau, G. Manning, D. Hebditch, D. Carstens, G. Avery, A. Foote and B. Dixie during the period November 16th to 27th 1987; and on information listed in the references.
5. I hold no interest, nor do I expect to receive any, in the LODE claims nor in Inter-Canadian Development Corp.
6. I consent to the use of my name and this report in a Statement of Material Facts or in a Prospectus by Inter-Canadian Development Corp.

February 21, 1988
Vancouver, B.C.



Douglas J. Brownlee,
B. Sc.

CERTIFICATE

I, Donald G. Allen, certify that:

1. I am a Consulting Geological Engineer with offices at Suite 704, 850 West Hastings Street, Vancouver, British Columbia.
2. I am a graduate of the University of British Columbia with degrees in Geological Engineering (B.A.Sc., 1964; M.A.Sc., 1966).
3. I have been practising my profession since 1964.
4. I am a member in good standing of the Association of Professional Engineers of British Columbia.
5. This report is based on fieldwork completed by D. Morneau, B. Stewart, K. Stewart, C. Hopping during the period September 11th to 15th, 1987; and by D. Morneau, G. Manning, D. Hebditch, D. Carstens, G. Avery, A. Foote and B. Dixie during the period November 16th to 27th 1987; and on information listed in the references.
6. I hold no interest, nor do I expect to receive any, in the LODE claims nor in Inter-Canadian Development Corp.
7. I consent to the use of my name and this report in a Statement of Material Facts or in a Prospectus by Inter-Canadian Development Corp.

February 21, 1988
Vancouver, B.C.

Donald G. Allen,
P. Eng. (B.C.)

APPENDIX I

Analytical Results

ACME ANALYTICAL LABORATORIES
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE 253-3158

DATE RECEIVED: NOV 13 1987

DATA LINE 251-1011 DATE REPORT MAILED:

Dec 1/87....

GEOCHEMICAL ICP-MS ANALYSIS

10 GRAM SAMPLE FIRE ASSAY AND ANALYSIS BY ICP MASS SPECTROMETER.

- SAMPLE TYPE: Pulp

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

A & M EXPLORATION File # 87-5618 Page 1

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------------|-----------|-----------|-----------|
| 903001 | 2 | 2 | 15 |
| 903002 | 3 | 3 | 26 |
| 903003 | 5 | 3 | 15 |
| 903004 | 2 | 3 | 12 |
| 903005 | 3 | 2 | 15 |
| 903006 | 3 | 3 | 10 |
| 903007 | 5 | 2 | 16 |
| 903008 | 4 | 3 | 31 |
| 903009 | 2 | 3 | 11 |
| 903010 | 3 | 3 | 10 |
| 903011 | 84 | 2 | 69 |
| 903012 | 3 | 3 | 8 |
| 903013 | 2 | 3 | 8 |
| 903014 | 1 | 5 | 15 |
| 903015 | 1 | 3 | 9 |
| 903016 | 1 | 2 | 6 |
| 903017 | 1 | 2 | 2 |
| 903018 | 1 | 2 | 3 |
| 903019 | 1 | 4 | 3 |
| 903020 | 1 | 2 | 2 |
| 903021 | 1 | 2 | 2 |
| 903022 | 3 | 2 | 2 |
| 903023 | 2 | 15 | 8 |
| 903024 | 1 | 3 | 4 |
| 903025 | 1 | 2 | 2 |
| 903026 | 1 | 3 | 5 |
| 903027 | 1 | 2 | 2 |
| 903028 | 2 | 2 | 2 |
| 903029 | 1 | 2 | 2 |
| 903030 | 2 | 4 | 6 |
| 903031 | 3 | 3 | 2 |
| 903032 | 152 | 2 | 2 |
| 903033 | 1 | 2 | 2 |
| 903034 | 5 | 2 | 2 |
| 903035 | 1 | 2 | 3 |
| 903036 | 1 | 2 | 4 |
| DETECTION LIMIT | 1 | 2 | 2 |

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------------|-----------|-----------|-----------|
| 903037 | 1 | 2 | 7 |
| 903038 | 1 | 2 | 5 |
| 903039 | 1 | 2 | 14 |
| 903040 | 2 | 2 | 10 |
| 903041 | 1 | 2 | 4 |
| 903042 | 2 | 4 | 7 |
| 903043 | 1 | 2 | 8 |
| 903044 | 2 | 53 | 6 |
| 903045 | 1 | 2 | 7 |
| 903046 | 1 | 2 | 10 |
| 903047 | 2 | 4 | 10 |
| 903048 | 1 | 3 | 8 |
| 903049 | 2 | 5 | 9 |
| 903050 | 2 | 2 | 9 |
| 903051 | 1 | 3 | 14 |
| 903052 | 1 | 2 | 11 |
| 903053 | 1 | 2 | 4 |
| 903054 | 27 | 2 | 3 |
| 903055 | 1 | 2 | 3 |
| 903056 | 1 | 61 | 4 |
| 903057 | 2 | 7 | 7 |
| 903058 | 1 | 3 | 5 |
| 903059 | 2 | 4 | 6 |
| 903060 | 1 | 4 | 13 |
| 903061 | 1 | 2 | 5 |
| 903062 | 1 | 2 | 3 |
| 903063 | 1 | 2 | 3 |
| 903064 | 1 | 18 | 8 |
| 903065 | 1 | 4 | 10 |
| 903066 | 5 | 4 | 4 |
| 903067 | 1 | 3 | 2 |
| 903068 | 1 | 2 | 2 |
| DETECTION LIMIT | 1 | 2 | 2 |

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 93 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR Mn Fe Ca P La Cr Mg Ba Ti B W AND LIMITED FOR Na K AND Al. Au DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: SOLUTION

DATE RECEIVED: DEC 7 1987 DATE REPORT MAILED: Dec 10/87 ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

ROSSBACHER LABORATORY PROJECT-87842 File # 87-6066 Page 1 #yz1

| SAMPLE# | Mo
PPM | Cu
PPM | Pb
PPM | Zn
PPM | Ag
PPM | Mn
PPM | Fe
PPM | As
PPM | U
PPM | Au
PPM | Th
PPM | SR
PPM | Co
PPM | Sb
PPM | Bi
PPM | V
PPM | Ca
PPM | P
PPM | La
PPM | Cr
PPM | Mg
PPM | Ba
PPM | Ti
PPM | B
PPM | Al
PPM | Na
PPM | K
PPM | W
PPM | | |
|-------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|----------|----------|-----|----|
| S L9N 1600E | 1 | .31 | .5 | .56 | .2 | .22 | 11 | 301 | 2.97 | 5 | 5 | ND | 1 | 16 | 1 | 2 | 2 | .50 | .23 | .068 | 3 | .29 | .74 | .60 | .11 | 2 | 1.78 | .03 | .06 | 1 |
| S L9N 1650E | 1 | .43 | .9 | .51 | .3 | .23 | 11 | 486 | 3.09 | 5 | 5 | ND | 2 | 30 | 1 | 2 | 2 | .59 | .33 | .049 | 8 | .32 | 1.03 | .60 | .11 | 2 | 1.59 | .03 | .06 | 1 |
| S L9N 1700E | 1 | .23 | .5 | .68 | .3 | .17 | 8 | 349 | 2.67 | 3 | 5 | ND | 1 | 20 | 1 | 2 | 2 | .42 | .35 | .058 | 3 | .20 | .50 | .108 | .07 | 2 | 1.89 | .03 | .05 | 1 |
| S L9N 1750E | 1 | .36 | .6 | .60 | .2 | .20 | 12 | 330 | 3.36 | 4 | 5 | ND | 1 | 17 | 1 | 2 | 2 | .63 | .28 | .080 | 3 | .27 | .80 | .59 | .10 | 2 | 2.15 | .03 | .05 | 1 |
| S L9N 1800E | 1 | .26 | .5 | .49 | .3 | .18 | 10 | 226 | 2.86 | 5 | 5 | ND | 2 | 14 | 1 | 2 | 2 | .50 | .21 | .060 | 3 | .23 | .59 | .70 | .10 | 2 | 2.01 | .03 | .04 | 2 |
| S L9N 1850E | 1 | .30 | .7 | .65 | .6 | .30 | 13 | 382 | 3.48 | 5 | 5 | ND | 3 | 22 | 1 | 2 | 2 | .57 | .38 | .056 | 12 | .35 | .90 | .197 | .10 | 2 | 2.29 | .03 | .06 | 1 |
| S L9N 1900E | 1 | .42 | .7 | .61 | .4 | .23 | 15 | 693 | 3.93 | 7 | 5 | ND | 2 | 35 | 1 | 2 | 2 | .83 | .70 | .120 | 10 | .30 | 1.19 | .182 | .09 | 2 | 1.95 | .04 | .09 | 1 |
| S L9N 1950E | 1 | .16 | .5 | .37 | .2 | .13 | 8 | 210 | 2.52 | 2 | 5 | ND | 1 | 12 | 1 | 2 | 2 | .44 | .17 | .095 | 3 | .20 | .49 | .82 | .07 | 2 | 1.88 | .02 | .05 | 2 |
| S L9N 2000E | 1 | .38 | .7 | .69 | .3 | .23 | 14 | 421 | 3.57 | 2 | 5 | ND | 2 | 17 | 1 | 2 | 2 | .63 | .28 | .103 | 4 | .31 | 1.04 | .81 | .07 | 2 | 2.20 | .02 | .06 | 1 |
| S L9N 2050E | 1 | .25 | .8 | .66 | .2 | .16 | 10 | 327 | 3.10 | 3 | 5 | ND | 2 | 18 | 1 | 2 | 2 | .57 | .25 | .095 | 4 | .22 | .74 | .87 | .07 | 2 | 2.16 | .03 | .04 | 1 |
| S L9N 2100E | 1 | .48 | .10 | .59 | .6 | .23 | 10 | 807 | 3.17 | 3 | 5 | ND | 2 | 53 | 1 | 2 | 2 | .44 | 1.16 | .029 | 19 | .27 | .61 | .403 | .08 | 2 | 2.67 | .04 | .06 | 1 |
| S L9N 2150E | 1 | .33 | .8 | .74 | .3 | .26 | 9 | 685 | 2.65 | 2 | 5 | ND | 2 | 36 | 1 | 2 | 2 | .38 | .46 | .064 | 8 | .25 | .50 | .178 | .08 | 2 | 2.57 | .03 | .05 | 1 |
| S L9N 2200E | 1 | .68 | .3 | .97 | .2 | .13 | 18 | 541 | 4.22 | 3 | 5 | ND | 2 | 30 | 1 | 2 | 2 | .101 | .36 | .117 | 3 | .14 | 1.64 | .58 | .16 | 2 | 2.87 | .03 | .06 | 1 |
| S L9N 2250E | 1 | .27 | .8 | .85 | .4 | .21 | 12 | 356 | 3.12 | 3 | 5 | ND | 1 | 15 | 1 | 2 | 2 | .48 | .22 | .074 | 4 | .34 | .72 | .76 | .09 | 2 | 1.87 | .02 | .04 | 1 |
| S L9N 2300E | 1 | .40 | .6 | .75 | .3 | .24 | 11 | 253 | 3.57 | 6 | 5 | ND | 1 | 15 | 1 | 2 | 2 | .57 | .23 | .104 | 3 | .36 | .73 | .73 | .09 | 2 | 2.21 | .03 | .04 | 1 |
| S L9N 2350E | 1 | .43 | .8 | .65 | .4 | .26 | 11 | 285 | 3.22 | 2 | 5 | ND | 2 | 20 | 1 | 2 | 2 | .51 | .31 | .031 | 4 | .35 | .79 | .59 | .09 | 2 | 2.20 | .03 | .05 | 1 |
| S L9N 2400E | 1 | .38 | .7 | .47 | .2 | .23 | 9 | 206 | 3.20 | 5 | 5 | ND | 1 | 12 | 1 | 2 | 2 | .56 | .18 | .057 | 3 | .30 | .59 | .46 | .10 | 2 | 1.91 | .02 | .08 | 2 |
| S L9N 2450E | 1 | .63 | .6 | .59 | .4 | .26 | 9 | 201 | 3.12 | 5 | 5 | ND | 2 | 12 | 1 | 2 | 2 | .48 | .16 | .054 | 4 | .31 | .57 | .63 | .10 | 2 | 2.16 | .03 | .04 | 1 |
| S L9N 2550E | 2 | .121 | .9 | .63 | 1.0 | .58 | 19 | 1809 | 3.15 | 10 | 5 | ND | 5 | .69 | 1 | 2 | 2 | .64 | .96 | .036 | 33 | .71 | 1.02 | .179 | .02 | 2 | 3.65 | .03 | .08 | 1 |
| S L9N 2600E | 1 | .40 | .7 | .64 | .3 | .27 | 11 | 367 | 3.27 | 4 | 5 | ND | 1 | 26 | 1 | 2 | 2 | .51 | .47 | .038 | 7 | .39 | .93 | .78 | .09 | 2 | 1.86 | .03 | .05 | 1 |
| S L9N 2850E | 1 | .48 | .7 | .72 | .3 | .35 | 16 | 1004 | 3.56 | 9 | 5 | ND | 2 | 42 | 1 | 2 | 2 | .57 | .78 | .062 | 11 | .45 | 1.10 | .81 | .10 | 2 | 1.90 | .03 | .11 | 1 |
| S L7N 1700E | 1 | .55 | .6 | .67 | .3 | .29 | 14 | 611 | 3.58 | 7 | 5 | ND | 2 | 29 | 1 | 2 | 2 | .62 | .45 | .058 | 6 | .42 | 1.06 | .68 | .12 | 2 | 1.87 | .03 | .08 | 1 |
| S L7N 1750E | 1 | .19 | .10 | .66 | .3 | .17 | 9 | 338 | 2.78 | 2 | 5 | ND | 1 | 19 | 1 | 2 | 2 | .51 | .30 | .081 | 3 | .26 | .65 | .62 | .08 | 2 | 1.47 | .03 | .06 | 1 |
| S L7N 1800E | 1 | .39 | .12 | .70 | .2 | .24 | 14 | 598 | 3.66 | 3 | 5 | ND | 1 | 34 | 1 | 2 | 2 | .74 | .66 | .073 | 8 | .36 | 1.15 | .75 | .12 | 2 | 1.67 | .03 | .06 | 1 |
| S L7N 1900E | 1 | .33 | .6 | .66 | .3 | .23 | 12 | 440 | 3.54 | 6 | 5 | ND | 2 | 24 | 1 | 2 | 2 | .70 | .39 | .134 | 4 | .24 | .80 | .102 | .10 | 2 | 2.34 | .04 | .07 | 1 |
| S L7N 1950E | 1 | .31 | .4 | .65 | .2 | .21 | 15 | 563 | 4.08 | 2 | 5 | ND | 2 | 35 | 1 | 2 | 2 | .94 | .56 | .090 | 5 | .26 | 1.13 | .106 | .13 | 2 | 1.83 | .03 | .09 | 1 |
| S L7N 2000E | 1 | .24 | .6 | .64 | .3 | .17 | 12 | 322 | 3.51 | 2 | 5 | ND | 2 | 24 | 1 | 2 | 2 | .74 | .30 | .107 | 3 | .21 | .89 | .109 | .11 | 2 | 2.18 | .03 | .07 | 1 |
| S L7N 2050E | 1 | .38 | .5 | .59 | .2 | .21 | 13 | 471 | 3.78 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | .86 | .32 | .041 | 3 | .24 | .93 | .122 | .14 | 2 | 2.11 | .03 | .04 | 1 |
| S L7N 2100E | 1 | .28 | .12 | .91 | .4 | .19 | 19 | 874 | 5.16 | 2 | 5 | ND | 1 | 39 | 1 | 2 | 2 | .142 | .82 | .043 | 6 | .19 | 1.37 | .191 | .20 | 2 | 2.46 | .04 | .07 | 1 |
| S L7N 2200E | 1 | .21 | .10 | .44 | .5 | .12 | 10 | 509 | 2.89 | 2 | 5 | ND | 3 | 37 | 1 | 2 | 2 | .65 | .61 | .090 | 8 | .14 | .65 | .186 | .14 | 2 | 2.84 | .05 | .06 | 2 |
| S L7N 2250E | 1 | .18 | .5 | .55 | .2 | .11 | 11 | 335 | 3.35 | 3 | 5 | ND | 2 | 24 | 1 | 2 | 2 | .73 | .19 | .122 | 3 | .19 | .64 | .74 | .10 | 2 | 2.45 | .03 | .06 | 2 |
| S L7N 2300E | 1 | .32 | .4 | .87 | .2 | .13 | 13 | 457 | 3.62 | 2 | 5 | ND | 1 | 24 | 1 | 2 | 2 | .71 | .23 | .095 | 3 | .17 | .89 | .80 | .11 | 2 | 2.63 | .03 | .08 | 2 |
| S L7N 2350E | 1 | .54 | .7 | .84 | .5 | .19 | 12 | 525 | 3.46 | 2 | 5 | ND | 3 | 31 | 1 | 2 | 2 | .68 | .52 | .048 | 10 | .21 | .86 | .250 | .09 | 2 | 2.94 | .03 | .09 | 1 |
| S L7N 2400E | 1 | .50 | .8 | .124 | .2 | .11 | 21 | 1007 | 4.52 | 2 | 5 | ND | 1 | 47 | 1 | 3 | 2 | .131 | .48 | .120 | 3 | .13 | 2.19 | .67 | .22 | 2 | 2.88 | .03 | .25 | 1 |
| S L7N 2450E | 1 | .44 | .4 | .102 | .3 | .17 | 14 | 649 | 3.66 | 3 | 5 | ND | 2 | 26 | 1 | 2 | 2 | .72 | .31 | .147 | 3 | .22 | 1.02 | .62 | .12 | 2 | 2.73 | .03 | .07 | 1 |
| S L7N 2500E | 1 | .239 | .7 | .85 | .5 | .21 | 25 | 879 | 5.46 | 6 | 5 | ND | 1 | 53 | 1 | 2 | 2 | .136 | .95 | .167 | 8 | .24 | 1.75 | .114 | .13 | 5 | 2.36 | .04 | .48 | 1 |
| S L7N 2550E | 1 | .79 | .11 | .82 | .3 | .37 | 12 | 336 | 4.09 | 7 | 5 | ND | 2 | 26 | 1 | 2 | 2 | .71 | .31 | .074 | 5 | .49 | 1.05 | .64 | .13 | 2 | 2.58 | .03 | .06 | 1 |
| S L7N 2600E | 1 | .244 | .11 | .87 | .5 | .81 | 16 | 528 | 4.06 | 13 | 5 | ND | 2 | 49 | 1 | 2 | 2 | .73 | .36 | .042 | 5 | .41 | .81 | .82 | .12 | 2 | 2.95 | .03 | .06 | 1 |
| S L7N 2650E | 1 | .101 | .9 | .78 | .9 | .56 | 15 | 1138 | 4.27 | 6 | 3 | ND | 3 | 99 | 1 | 2 | 2 | .63 | .17 | .052 | 21 | .64 | 1.06 | .305 | .05 | 2 | 3.57 | .04 | .10 | 1 |
| STD C | 18 | .58 | .38 | .130 | 7.3 | .68 | 28 | 1053 | 4.10 | 39 | 17 | 8 | 38 | 51 | 18 | 17 | 20 | .57 | .49 | .082 | 38 | .60 | .91 | .178 | .08 | 39 | 1.85 | .08 | .14 | 12 |

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Page 2

| SAMPLE# | MO | CU | PB | ZN | A6 | NI | CO | MN | FE | AS | U | AU | TH | SR | CD | J | BI | V | CN | P | LA | CR | M6 | I | BA | T1 | B | AL | NA | K | W |
|-------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|----|---|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | | |
| S LSN 1800E | 1 | 46 | 4 | 46 | .3 | 31 | 11 | 502 | 3.29 | 2 | 5 | ND | 3 | 46 | 1 | 2 | 2 | 71 | .75 | .020 | 8 | .39 | .72 | 219 | .17 | 2 | 2.80 | .05 | .09 | 2 | |
| S LSN 1850E | 1 | 45 | 5 | 68 | .4 | 29 | 14 | 755 | 4.35 | 2 | 5 | ND | 3 | 49 | 1 | 2 | 2 | 96 | .83 | .044 | 10 | .32 | .95 | 174 | .17 | 2 | 3.02 | .05 | .10 | 1 | |
| S LSN 1900E | 1 | 102 | 10 | 77 | .6 | 54 | 15 | 900 | 4.99 | 6 | 5 | ND | 4 | 52 | 1 | 2 | 2 | 95 | .90 | .066 | 20 | .49 | .98 | 230 | .14 | 4 | 4.86 | .05 | .13 | 1 | |
| S LSN 1950E | 1 | 43 | 5 | 60 | .3 | 26 | 13 | 441 | 4.12 | 6 | 5 | ND | 2 | 49 | 1 | 2 | 2 | 92 | .71 | .083 | 7 | .30 | .80 | 113 | .15 | 2 | 2.61 | .08 | .08 | 1 | |
| S LSN 2000E | 1 | 33 | 3 | 69 | .3 | 28 | 14 | 348 | 4.34 | 3 | 5 | ND | 2 | 46 | 1 | 2 | 2 | 102 | .54 | .080 | 4 | .31 | .99 | 96 | .18 | 2 | 2.92 | .05 | .10 | 1 | |
| S LSN 2050E | 1 | 40 | 2 | 62 | .3 | 25 | 19 | 631 | 5.62 | 4 | 5 | ND | 3 | 77 | 1 | 4 | 2 | 142 | 1.15 | .121 | 7 | .33 | 1.75 | 142 | .16 | 2 | 2.52 | .05 | .18 | 1 | |
| S LSN 2100E | 1 | 54 | 3 | 78 | .4 | 45 | 15 | 479 | 4.64 | 3 | 5 | ND | 3 | 52 | 1 | 2 | 2 | 105 | .85 | .054 | 9 | .30 | 1.24 | 374 | .20 | 2 | 4.17 | .06 | .12 | 1 | |
| S LSN 2150E | 1 | 28 | 3 | 74 | .2 | 20 | 20 | 597 | 5.34 | 3 | 5 | ND | 2 | 84 | 1 | 5 | 2 | 139 | 1.09 | .113 | 5 | .24 | 1.88 | 198 | .18 | 2 | 2.64 | .06 | .15 | 1 | |
| S LSN 2200E | 1 | 44 | 9 | 68 | .6 | 27 | 11 | 597 | 3.61 | 2 | 8 | ND | 5 | 34 | 1 | 2 | 2 | 74 | .64 | .116 | 7 | .18 | .88 | 462 | .19 | 3 | 4.54 | .06 | .12 | 1 | |
| S LSN 2250E | 1 | 32 | 2 | 70 | .2 | 16 | 19 | 484 | 5.01 | 5 | 5 | ND | 2 | 87 | 1 | 3 | 2 | 144 | .78 | .139 | 5 | .19 | 1.61 | 181 | .23 | 2 | 3.23 | .08 | .15 | 1 | |
| S LSN 2300E | 1 | 39 | 8 | 72 | .4 | 24 | 17 | 1017 | 5.26 | 4 | 5 | ND | 3 | 70 | 1 | 2 | 2 | 156 | 1.06 | .044 | 13 | .29 | 1.36 | 637 | .18 | 2 | 4.06 | .05 | .20 | 1 | |
| S LSN 2350E | 1 | 23 | 4 | 64 | .2 | 17 | 15 | 1104 | 4.36 | 4 | 5 | ND | 2 | 90 | 1 | 2 | 2 | 146 | 1.09 | .040 | 7 | .24 | 1.27 | 406 | .18 | 3 | 3.68 | .05 | .11 | 1 | |
| S LSN 2400E | 1 | 10 | 4 | 82 | .3 | 12 | 22 | 761 | 4.97 | 5 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 157 | .81 | .081 | 2 | .9 | 2.20 | 89 | .30 | 2 | 2.88 | .09 | .17 | 1 | |
| S LSN 2450E | 1 | 42 | 5 | 81 | .2 | 17 | 15 | 704 | 4.02 | 2 | 5 | ND | 2 | 63 | 1 | 2 | 2 | 96 | .58 | .099 | 5 | .23 | 1.05 | 156 | .13 | 2 | 3.43 | .04 | .13 | 1 | |
| S LSN 2500E | 1 | 32 | 2 | 88 | .2 | 11 | 31 | 778 | 6.08 | 3 | 5 | ND | 2 | 42 | 1 | 4 | 2 | 195 | 1.20 | .174 | 5 | .10 | 2.66 | 170 | .18 | 2 | 2.95 | .06 | .91 | 1 | |
| S LSN 2550E | 1 | 40 | 6 | 88 | .3 | 21 | 12 | 354 | 4.13 | 4 | 5 | ND | 2 | 45 | 1 | 2 | 2 | 91 | .43 | .091 | 4 | .32 | 1.06 | 80 | .16 | 2 | 3.17 | .03 | .08 | 1 | |
| S LSN 2600E | 1 | 25 | 5 | 57 | .1 | 21 | 9 | 279 | 3.30 | 4 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 63 | .35 | .104 | 3 | .38 | .68 | 66 | .13 | 2 | 2.42 | .03 | .06 | 1 | |
| S LSN 1600E | 1 | 30 | 3 | 47 | .1 | 21 | 10 | 209 | 4.09 | 2 | 5 | ND | 6 | 47 | 1 | 2 | 2 | 96 | .46 | .112 | 4 | .47 | .85 | 66 | .13 | 2 | 2.02 | .04 | .06 | 2 | |
| S LSN 1650E | 1 | 52 | 3 | 37 | .1 | 24 | 12 | 264 | 3.80 | 4 | 5 | ND | 2 | 54 | 1 | 2 | 2 | 94 | .62 | .103 | 6 | .46 | .89 | 70 | .11 | 2 | 1.74 | .04 | .05 | 1 | |
| S LSN 1700E | 1 | 69 | 6 | 54 | .5 | 43 | 15 | 769 | 4.19 | 9 | 5 | ND | 3 | 92 | 1 | 2 | 2 | 83 | .90 | .038 | 16 | .57 | .94 | 174 | .13 | 2 | 3.03 | .04 | .09 | 1 | |
| S LSN 1800E | 1 | 54 | 10 | 63 | .2 | 41 | 17 | 647 | 4.18 | 6 | 5 | ND | 3 | 74 | 1 | 2 | 2 | 82 | 1.15 | .041 | 8 | .58 | .99 | 132 | .12 | 2 | 2.86 | .05 | .10 | 1 | |
| S LSN 1850E | 1 | 40 | 3 | 77 | .5 | 33 | 12 | 248 | 3.80 | 5 | 5 | ND | 2 | 46 | 1 | 2 | 2 | 75 | .57 | .102 | 6 | .45 | .83 | 95 | .12 | 2 | 2.61 | .04 | .08 | 1 | |
| S LSN 1900E | 1 | 38 | 3 | 78 | .3 | 33 | 11 | 279 | 3.77 | 3 | 5 | ND | 2 | 46 | 1 | 2 | 2 | 78 | .59 | .083 | 6 | .39 | .78 | 107 | .13 | 2 | 2.54 | .04 | .08 | 1 | |
| S LSN 1950E | 1 | 39 | 2 | 70 | .4 | 29 | 11 | 526 | 3.42 | 4 | 5 | ND | 2 | 43 | 1 | 2 | 2 | 70 | .57 | .122 | 6 | .34 | .87 | 113 | .12 | 2 | 2.43 | .04 | .11 | 1 | |
| S LSN 2000E | 1 | 38 | 10 | 50 | .1 | 26 | 13 | 325 | 3.68 | 3 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 84 | .76 | .071 | 6 | .36 | .95 | 97 | .16 | 2 | 2.26 | .04 | .09 | 3 | |
| S LSN 2050E | 1 | 37 | 3 | 52 | .2 | 30 | 11 | 237 | 3.72 | 6 | 5 | ND | 2 | 34 | 1 | 2 | 2 | 78 | .42 | .095 | 6 | .34 | .68 | 96 | .13 | 2 | 2.78 | .04 | .07 | 1 | |
| S LSN 2100E | 1 | 25 | 8 | 52 | .2 | 27 | 11 | 289 | 3.65 | 4 | 5 | ND | 2 | 46 | 1 | 2 | 2 | 82 | .67 | .043 | 5 | .31 | .80 | 183 | .17 | 2 | 2.51 | .05 | .08 | 1 | |
| S LSN 2150E | 1 | 31 | 4 | 59 | .3 | 28 | 13 | 359 | 4.11 | 2 | 5 | ND | 2 | 40 | 1 | 2 | 2 | 89 | .62 | .080 | 3 | .31 | .83 | 142 | .16 | 2 | 2.75 | .05 | .09 | 1 | |
| S LSN 2200E | 1 | 74 | 7 | 88 | .3 | 37 | 20 | 363 | 5.17 | 6 | 5 | ND | 2 | 42 | 1 | 2 | 2 | 123 | .61 | .170 | 6 | .26 | 1.42 | 291 | .15 | 2 | 4.33 | .04 | .14 | 1 | |
| S LSN 2250E | 1 | 31 | 6 | 61 | .2 | 22 | 14 | 522 | 3.97 | 2 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 97 | .70 | .068 | 5 | .22 | 1.14 | 169 | .16 | 2 | 2.47 | .05 | .08 | 1 | |
| S LSN 2300E | 1 | 27 | 7 | 62 | .3 | 15 | 13 | 403 | 4.60 | 5 | 5 | ND | 1 | 62 | 1 | 2 | 2 | 113 | .77 | .168 | 4 | .27 | 1.30 | 103 | .15 | 2 | 2.35 | .06 | .14 | 1 | |
| S LSN 2350E | 1 | 19 | 6 | 83 | .2 | 13 | 13 | 399 | 4.26 | 2 | 5 | ND | 1 | 48 | 1 | 2 | 2 | 98 | .57 | .211 | 3 | .22 | .93 | 95 | .15 | 2 | 2.66 | .05 | .09 | 1 | |
| S LSN 2400E | 1 | 25 | 7 | 66 | .2 | 18 | 14 | 575 | 3.98 | 4 | 5 | ND | 1 | 66 | 1 | 2 | 2 | 105 | .97 | .076 | 5 | .21 | 1.08 | 329 | .15 | 2 | 2.79 | .05 | .18 | 1 | |
| S LSN 2450E | 1 | 17 | 9 | 67 | .3 | 17 | 12 | 498 | 3.78 | 2 | 5 | ND | 1 | 48 | 1 | 2 | 2 | 86 | .44 | .101 | 3 | .31 | .81 | 92 | .15 | 2 | 2.56 | .04 | .08 | 1 | |
| S LSN 2500E | 1 | 17 | 8 | 65 | .2 | 12 | 11 | 346 | 3.77 | 3 | 5 | ND | 1 | 41 | 1 | 2 | 2 | 84 | .33 | .220 | 3 | .18 | .76 | 99 | .13 | 2 | 2.59 | .04 | .09 | 1 | |
| S LSN 2550E | 1 | 16 | 6 | 77 | .2 | 17 | 16 | 542 | 4.27 | 4 | 5 | ND | 1 | 42 | 1 | 2 | 2 | 107 | .55 | .152 | 2 | .18 | 1.41 | 92 | .18 | 2 | 2.54 | .06 | .08 | 1 | |
| S LSN 2600E | 1 | 23 | 6 | 55 | .2 | 19 | 10 | 292 | 3.21 | 4 | 5 | ND | 1 | 34 | 1 | 2 | 2 | 67 | .38 | .082 | 4 | .28 | .62 | 101 | .14 | 2 | 2.39 | .03 | .09 | 1 | |
| S LIN 1650E | 1 | 49 | 5 | 65 | .3 | 27 | 15 | 368 | 4.74 | 5 | 5 | ND | 2 | 58 | 1 | 2 | 2 | 114 | .58 | .109 | 5 | .55 | 1.03 | 102 | .14 | 2 | 2.10 | .04 | .08 | 1 | |
| S LIN 1700E | 1 | 41 | 6 | 48 | .2 | 23 | 14 | 282 | 4.75 | 4 | 5 | ND | 1 | 51 | 1 | 2 | 2 | 108 | .53 | .075 | 5 | .46 | .79 | 73 | .15 | 2 | 2.34 | .04 | .05 | 2 | |
| STD C | 18 | 58 | 37 | 131 | 7.3 | 67 | 27 | 1052 | 4.07 | 39 | 16 | 8 | 37 | 50 | 18 | 17 | 20 | 56 | .49 | .081 | 38 | .60 | .90 | 177 | .08 | 38 | 1.93 | .08 | .13 | 12 | |

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Page 3

| SAMPLE | Mo
PPM | Cu
PPM | Pb
PPM | Zn
PPM | Ag
PPM | Ni
PPM | Co
PPM | Mn
PPM | Fe
% | As
PPM | U
PPM | Au
PPM | Th
PPM | SR
PPM | CD
PPM | SB
PPM | Si
PPM | V
PPM | Ca
PPM | P
PPM | La
PPM | Cr
PPM | Mg
PPM | Ba
PPM | Ti
PPM | B
PPM | Al
PPM | Na
PPM | K
PPM | N
PPM |
|-------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|----------|----------|
| S LIN 1750E | 1 | 28 | 4 | 31 | .2 | 15 | 8 | 244 | 3.33 | 2 | 5 | ND | 2 | 29 | 1 | 2 | 2 | 76 | .36 | .068 | 3 | 34 | .55 | 79 | .11 | 2 | 1.56 | .03 | .03 | 1 |
| S LIN 1800E | 1 | 53 | 6 | 49 | .2 | 23 | 11 | 522 | 3.31 | 4 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 69 | .55 | .091 | 5 | 31 | .75 | 114 | .10 | 2 | 1.79 | .03 | .06 | 2 |
| S LIN 1850E | 1 | 69 | 5 | 52 | .1 | 21 | 14 | 713 | 3.55 | 3 | 5 | ND | 2 | 69 | 1 | 2 | 2 | 84 | .86 | .119 | 8 | 28 | 1.02 | 116 | .10 | 2 | 1.54 | .04 | .13 | 1 |
| S LIN 1900E | 1 | 59 | 6 | 52 | .2 | 27 | 14 | 682 | 4.03 | 5 | 5 | ND | 2 | 54 | 1 | 2 | 2 | 89 | .83 | .109 | 9 | 40 | 1.05 | 91 | .11 | 2 | 1.68 | .04 | .15 | 2 |
| S LIN 1950E | 1 | 45 | 7 | 46 | .3 | 28 | 12 | 582 | 3.43 | 4 | 5 | ND | 3 | 48 | 1 | 2 | 2 | 73 | .90 | .029 | 8 | 32 | .79 | 166 | .16 | 2 | 2.71 | .05 | .06 | 1 |
| S LIN 2000E | 1 | 74 | 8 | 38 | .4 | 29 | 10 | 661 | 3.26 | 3 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 63 | 1.07 | .044 | 15 | 31 | .60 | 146 | .12 | 2 | 2.72 | .05 | .06 | 1 |
| S LIN 2050E | 1 | 29 | 7 | 47 | .1 | 23 | 11 | 275 | 3.53 | 5 | 5 | ND | 2 | 34 | 1 | 2 | 2 | 73 | .46 | .080 | 5 | 33 | .71 | 85 | .14 | 2 | 2.28 | .04 | .07 | 1 |
| S LIN 2100E | 1 | 31 | 10 | 70 | .4 | 24 | 10 | 1111 | 2.94 | 2 | 5 | ND | 1 | 62 | 1 | 2 | 2 | 63 | .94 | .080 | 6 | 26 | .84 | 208 | .11 | 3 | 1.79 | .04 | .07 | 1 |
| S LIN 2150E | 1 | 45 | 9 | 61 | .1 | 28 | 13 | 571 | 3.72 | 3 | 5 | ND | 2 | 48 | 1 | 2 | 2 | 83 | .69 | .088 | 8 | 30 | .83 | 133 | .13 | 2 | 2.24 | .04 | .07 | 1 |
| S LIN 2200E | 1 | 41 | 7 | 56 | .1 | 29 | 14 | 691 | 3.99 | 6 | 5 | ND | 2 | 48 | 1 | 2 | 2 | 92 | .69 | .076 | 8 | 33 | .92 | 101 | .14 | 2 | 2.00 | .05 | .08 | 1 |
| S LIN 2250E | 1 | 28 | 6 | 49 | .1 | 26 | 10 | 262 | 3.29 | 3 | 5 | ND | 2 | 25 | 1 | 2 | 2 | 67 | .36 | .082 | 4 | 25 | .57 | 78 | .11 | 2 | 2.02 | .03 | .06 | 1 |
| S LIN 2300E | 1 | 29 | 8 | 47 | .1 | 25 | 11 | 245 | 3.67 | 2 | 5 | ND | 3 | 29 | 1 | 2 | 2 | 77 | .39 | .081 | 4 | 30 | .77 | 70 | .12 | 2 | 1.91 | .03 | .07 | 2 |
| S LIN 2350E | 1 | 32 | 8 | 51 | .2 | 25 | 12 | 265 | 3.93 | 3 | 5 | ND | 2 | 37 | 1 | 2 | 2 | 84 | .49 | .108 | 6 | 27 | .80 | 104 | .13 | 2 | 2.25 | .04 | .06 | 2 |
| S LIN 2400E | 1 | 49 | 7 | 47 | .2 | 26 | 9 | 608 | 3.07 | 2 | 5 | ND | 2 | 45 | 1 | 2 | 2 | 63 | .83 | .042 | 9 | 20 | .63 | 235 | .16 | 2 | 2.76 | .05 | .05 | 1 |
| S LIN 2450E | 1 | 45 | 8 | 58 | .2 | 23 | 13 | 315 | 4.04 | 4 | 5 | ND | 2 | 50 | 1 | 2 | 2 | 85 | .68 | .103 | 7 | 24 | .85 | 161 | .15 | 2 | 2.87 | .04 | .10 | 1 |
| S LIN 2500E | 1 | 44 | 11 | 69 | .2 | 28 | 14 | 380 | 4.04 | 4 | 5 | ND | 3 | 47 | 1 | 2 | 2 | 94 | .69 | .044 | 5 | 30 | 1.06 | 375 | .18 | 2 | 3.32 | .05 | .10 | 1 |
| S LIN 2550E | 1 | 29 | 8 | 55 | .2 | 23 | 14 | 365 | 4.06 | 2 | 5 | ND | 2 | 51 | 1 | 2 | 2 | 95 | .81 | .039 | 6 | 24 | 1.07 | 266 | .18 | 2 | 2.44 | .04 | .07 | 1 |
| S LIN 2600E | 1 | 18 | 5 | 72 | .2 | 20 | 19 | 364 | 5.12 | 4 | 5 | ND | 1 | 46 | 1 | 2 | 2 | 136 | .69 | .121 | 3 | 18 | 1.43 | 124 | .20 | 2 | 2.60 | .07 | .09 | 1 |
| S LIS 1650E | 1 | 82 | 5 | 68 | .4 | 43 | 10 | 531 | 3.20 | 4 | 5 | ND | 3 | 43 | 1 | 2 | 2 | 60 | .63 | .033 | 8 | 35 | .70 | 193 | .12 | 2 | 2.93 | .04 | .08 | 1 |
| S LIS 1700E | 1 | 90 | 6 | 104 | .2 | 20 | 19 | 515 | 4.54 | 3 | 5 | ND | 2 | 62 | 1 | 2 | 2 | 111 | .41 | .084 | 4 | 16 | 1.56 | 106 | .14 | 2 | 3.52 | .03 | .18 | 1 |
| S LIS 1750E | 1 | 45 | 7 | 63 | .2 | 32 | 15 | 458 | 3.52 | 2 | 5 | ND | 2 | 29 | 1 | 2 | 2 | 66 | .35 | .062 | 7 | 40 | .84 | 103 | .11 | 2 | 2.64 | .03 | .07 | 1 |
| S LIS 1800E | 1 | 131 | 8 | 65 | 1.0 | 26 | 12 | 980 | 3.62 | 4 | 5 | ND | 3 | 68 | 1 | 2 | 2 | 75 | .66 | .044 | 19 | 22 | .81 | 147 | .14 | 2 | 3.33 | .04 | .05 | 1 |
| S LIS 1850E | 1 | 38 | 8 | 60 | .3 | 18 | 10 | 415 | 3.23 | 3 | 5 | ND | 2 | 35 | 1 | 2 | 2 | 72 | .39 | .083 | 4 | 26 | .75 | 87 | .11 | 2 | 2.01 | .03 | .07 | 1 |
| S LIS 1900E | 1 | 46 | 8 | 52 | .2 | 21 | 10 | 349 | 3.08 | 3 | 5 | ND | 2 | 32 | 1 | 2 | 2 | 62 | .40 | .061 | 6 | 33 | .64 | 74 | .12 | 2 | 2.20 | .03 | .05 | 1 |
| S LIS 1950E | 1 | 172 | 3 | 80 | .2 | 20 | 12 | 293 | 3.45 | 4 | 5 | ND | 2 | 62 | 1 | 2 | 2 | 76 | .69 | .096 | 5 | 27 | .86 | 106 | .14 | 2 | 2.50 | .04 | .07 | 1 |
| S LIS 2000E | 1 | 82 | 205 | 54 | 4.4 | 32 | 13 | 816 | 3.49 | 8 | 5 | ND | 2 | 105 | 1 | 2 | 2 | 70 | 1.38 | .050 | 13 | 37 | .78 | 171 | .07 | 2 | 2.18 | .04 | .07 | 1 |
| S LIS 2100E | 1 | 65 | 4 | 44 | .5 | 29 | 12 | 449 | 3.88 | 5 | 5 | ND | 3 | 69 | 1 | 2 | 2 | 86 | .91 | .052 | 12 | 36 | .70 | 126 | .12 | 2 | 2.47 | .04 | .06 | 1 |
| S LIS 2150E | 1 | 39 | 6 | 37 | .2 | 20 | 10 | 299 | 3.40 | 4 | 5 | ND | 2 | 91 | 1 | 2 | 2 | 75 | 1.06 | .070 | 7 | 32 | .65 | 105 | .10 | 2 | 1.73 | .04 | .05 | 1 |
| S LIS 2200E | 1 | 26 | 7 | 42 | .1 | 18 | 9 | 223 | 3.13 | 2 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 65 | .41 | .066 | 4 | 28 | .70 | 91 | .09 | 2 | 1.66 | .03 | .05 | 1 |
| S LIS 2250E | 1 | 15 | 7 | 38 | .2 | 15 | 7 | 175 | 3.43 | 4 | 5 | ND | 2 | 28 | 1 | 2 | 2 | 72 | .38 | .148 | 3 | 28 | .42 | 58 | .12 | 2 | 2.20 | .03 | .06 | 1 |
| S LIS 2300E | 1 | 48 | 8 | 52 | .2 | 26 | 13 | 326 | 4.00 | 4 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 85 | .38 | .087 | 4 | 34 | .94 | 112 | .12 | 2 | 2.43 | .03 | .08 | 1 |
| S LIS 2350E | 1 | 16 | 7 | 38 | .1 | 14 | 7 | 204 | 2.70 | 3 | 5 | ND | 1 | 31 | 1 | 2 | 2 | 82 | .45 | .053 | 3 | 20 | .47 | 59 | .12 | 2 | 1.34 | .03 | .05 | 2 |
| S LIS 2400E | 1 | 39 | 7 | 54 | .3 | 23 | 13 | 266 | 4.14 | 5 | 5 | ND | 2 | 48 | 1 | 2 | 2 | 92 | .58 | .109 | 6 | 28 | .89 | 119 | .14 | 2 | 2.69 | .04 | .10 | 1 |
| S LIS 2450E | 1 | 31 | 9 | 54 | .2 | 22 | 11 | 720 | 3.56 | 2 | 5 | ND | 1 | 64 | 1 | 2 | 2 | 79 | .82 | .052 | 8 | 30 | .73 | 136 | .15 | 2 | 2.04 | .04 | .13 | 1 |
| S LIS 2500E | 1 | 25 | 5 | 47 | .2 | 20 | 11 | 275 | 3.34 | 4 | 5 | ND | 1 | 52 | 1 | 2 | 2 | 81 | .61 | .051 | 4 | 27 | .88 | 116 | .15 | 2 | 1.87 | .04 | .08 | 1 |
| S LIS 2550E | 1 | 46 | 2 | 50 | .3 | 29 | 13 | 548 | 3.74 | 4 | 5 | ND | 3 | 55 | 1 | 2 | 2 | 80 | .86 | .084 | 9 | 38 | 1.03 | 130 | .12 | 2 | 1.90 | .04 | .14 | 2 |
| S LIS 2600E | 1 | 47 | 7 | 53 | .3 | 34 | 13 | 575 | 3.87 | 5 | 5 | ND | 2 | 49 | 1 | 2 | 2 | 88 | .88 | .055 | 9 | 32 | .99 | 159 | .14 | 2 | 2.38 | .05 | .09 | 1 |
| S LIS 1000E | 1 | 84 | 7 | 70 | .2 | 19 | 14 | 373 | 4.51 | 4 | 5 | ND | 2 | 46 | 1 | 2 | 2 | 115 | .43 | .158 | 4 | 36 | 1.15 | 42 | .15 | 2 | 2.37 | .03 | .04 | 1 |
| S LIS 1500E | 1 | 43 | 6 | 62 | .2 | 15 | 10 | 256 | 3.48 | 3 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 83 | .28 | .093 | 2 | 26 | .71 | 44 | .15 | 2 | 1.80 | .03 | .05 | 1 |
| STD C | 18 | 60 | 38 | 132 | 7.5 | 67 | 27 | 1046 | 4.06 | 39 | 14 | 8 | 37 | 50 | 18 | 16 | 20 | 56 | .48 | .081 | 38 | 59 | .90 | 175 | .08 | 38 | 1.91 | .08 | .13 | 11 |

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| SAMPLE# | MQ | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | CD | SB | BI | V | CA | P | LA | CR | MG | BA | TI | B | AL | NA | K | N |
|-------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|----|
| | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | |
| S L3S 200E | 1 | 57 | 10 | .68 | .2 | 21 | 13 | 328 | 3.90 | 4 | 5 | ND | 1 | 54 | 1 | 2 | 2 | 101 | .40 | .096 | 2 | 36 | .93 | 46 | .18 | 2 | 2.04 | .03 | .05 | 1 |
| S L3S 250E | 1 | 89 | 7 | .76 | .2 | 29 | 17 | 319 | 4.62 | 5 | 5 | ND | 1 | 64 | 1 | 2 | 2 | 117 | .45 | .125 | 3 | 42 | 1.03 | 68 | .21 | 2 | 2.70 | .03 | .05 | 1 |
| S L3S 300E | 1 | 61 | 10 | .67 | .4 | 20 | 14 | 318 | 4.24 | 3 | 5 | ND | 1 | 89 | 1 | 2 | 2 | 111 | .47 | .117 | 3 | 33 | .99 | 44 | .18 | 2 | 2.28 | .03 | .06 | 1 |
| S L3S 350E | 1 | 78 | 9 | .82 | .3 | 19 | 16 | 647 | 3.80 | 4 | 5 | ND | 1 | 78 | 1 | 2 | 2 | 102 | .52 | .113 | 3 | 29 | 1.20 | 109 | .18 | 2 | 2.50 | .03 | .08 | 1 |
| S L3S 400E | 1 | 93 | 7 | .84 | .3 | 22 | 16 | 422 | 4.59 | 4 | 5 | ND | 2 | 82 | 1 | 2 | 2 | 118 | .51 | .111 | 4 | 40 | 1.15 | 82 | .20 | 2 | 2.60 | .03 | .09 | 1 |
| S L3S 500E | 1 | 70 | 6 | .74 | .2 | 20 | 14 | 383 | 4.57 | 4 | 5 | ND | 1 | 79 | 1 | 2 | 2 | 125 | .44 | .123 | 3 | 40 | 1.26 | 61 | .20 | 2 | 2.69 | .03 | .06 | 1 |
| S L3S 550E | 1 | 75 | 6 | .75 | .1 | 14 | 13 | 699 | 3.78 | 2 | 5 | ND | 1 | 78 | 1 | 2 | 2 | 110 | .43 | .135 | 3 | 24 | .99 | 44 | .19 | 2 | 2.38 | .03 | .08 | 1 |
| S L3S 600E | 1 | 39 | 9 | .69 | .4 | 14 | 10 | 605 | 3.45 | 2 | 5 | ND | 2 | 41 | 1 | 2 | 2 | 88 | .28 | .097 | 4 | 26 | .73 | 57 | .14 | 3 | 2.37 | .03 | .06 | 1 |
| S L3S 650E | 1 | 57 | 7 | .77 | .2 | 24 | 17 | 581 | 4.84 | 3 | 5 | ND | 2 | 80 | 1 | 2 | 2 | 136 | .42 | .118 | 3 | 49 | 1.42 | 73 | .19 | 2 | 2.46 | .03 | .07 | 1 |
| S L3S 700E | 1 | 78 | 8 | 107 | .4 | 28 | 21 | 688 | 4.86 | 3 | 5 | ND | 3 | 115 | 1 | 2 | 2 | 139 | .69 | .177 | 6 | 45 | 1.55 | 72 | .17 | 2 | 2.57 | .04 | .08 | 1 |
| S L3S 750E | 1 | 65 | 7 | .83 | .2 | 33 | 19 | 495 | 4.82 | 2 | 5 | ND | 1 | 72 | 1 | 2 | 2 | 115 | .52 | .150 | 4 | 67 | 1.47 | 73 | .17 | 2 | 2.17 | .03 | .07 | 1 |
| S L3S 800E | 1 | 68 | 7 | .86 | .3 | 27 | 18 | 478 | 4.84 | 5 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 146 | .49 | .132 | 4 | 43 | 1.82 | 79 | .17 | 2 | 2.64 | .03 | .07 | 1 |
| S L3S 900E | 1 | 80 | 6 | .78 | .2 | 23 | 15 | 428 | 4.49 | 2 | 5 | ND | 2 | 62 | 1 | 2 | 2 | 118 | .57 | .123 | 3 | 37 | 1.31 | 48 | .16 | 2 | 2.00 | .03 | .06 | 1 |
| S L3S 950E | 1 | 125 | 12 | 102 | .2 | 30 | 21 | 512 | 5.43 | 6 | 5 | ND | 2 | 75 | 1 | 2 | 2 | 151 | .60 | .149 | 4 | 76 | 2.02 | 67 | .23 | 2 | 1.19 | .03 | .11 | 1 |
| S L3S 1000E | 1 | 123 | 9 | .92 | .2 | 24 | 19 | 617 | 5.24 | 4 | 5 | ND | 2 | 95 | 1 | 2 | 2 | 134 | .63 | .142 | 4 | 29 | 1.69 | 54 | .17 | 2 | 3.27 | .03 | .06 | 1 |
| S L3S 1050E | 1 | 44 | 48 | .64 | .3 | 12 | 12 | 574 | 3.85 | 2 | 5 | ND | 1 | 46 | 1 | 2 | 2 | 94 | .43 | .137 | 3 | 21 | .99 | 56 | .15 | 2 | 2.33 | .04 | .04 | 1 |
| S L3S 1100E | 1 | 54 | 8 | .59 | .1 | 13 | 13 | 443 | 4.07 | 2 | 5 | ND | 1 | 45 | 1 | 2 | 2 | 110 | .46 | .065 | 2 | 24 | 1.11 | 49 | .21 | 2 | 2.04 | .05 | .04 | 1 |
| S L3S 1150E | 1 | 95 | 9 | .75 | .3 | 17 | 15 | 549 | 4.75 | 3 | 5 | ND | 1 | 40 | 1 | 2 | 2 | 121 | .36 | .097 | 2 | 31 | 1.30 | 75 | .18 | 2 | 2.68 | .03 | .05 | 1 |
| S L3S 1200E | 1 | 81 | 7 | 120 | .3 | 19 | 22 | 726 | 5.72 | 3 | 5 | ND | 1 | 48 | 1 | 3 | 2 | 158 | .48 | .109 | 3 | 31 | 2.43 | 98 | .19 | 2 | 3.50 | .03 | .05 | 1 |
| S L3S 1250E | 1 | 27 | 9 | .76 | .3 | 11 | 11 | 1009 | 3.35 | 2 | 5 | ND | 1 | 61 | 1 | 2 | 2 | 80 | .40 | .075 | 3 | 21 | .90 | 85 | .15 | 2 | 2.15 | .03 | .06 | 1 |
| S L3S 1300E | 1 | 42 | 9 | .71 | .3 | 12 | 14 | 446 | 3.95 | 3 | 5 | ND | 1 | 51 | 1 | 2 | 2 | 98 | .42 | .079 | 2 | 18 | 1.40 | 74 | .19 | 2 | 2.54 | .03 | .06 | 1 |
| S L3S 1350E | 1 | 67 | 8 | .89 | .4 | 12 | 13 | 449 | 3.85 | 4 | 5 | ND | 1 | 61 | 1 | 2 | 2 | 96 | .48 | .120 | 2 | 21 | 1.39 | 111 | .17 | 2 | 2.40 | .03 | .09 | 1 |
| S L3S 1400E | 1 | 137 | 10 | .72 | .9 | 14 | 15 | 826 | 3.99 | 4 | 5 | ND | 2 | 78 | 1 | 2 | 2 | 102 | .76 | .060 | 14 | 23 | 1.24 | 222 | .18 | 3 | 3.09 | .04 | .12 | 1 |
| S L3S 1450E | 1 | 65 | 5 | .84 | .2 | 13 | 17 | 789 | 4.41 | 5 | 5 | ND | 1 | 93 | 1 | 2 | 2 | 111 | .69 | .107 | 4 | 21 | 1.66 | 131 | .16 | 2 | 2.88 | .03 | .21 | 1 |
| S L3S 1500E | 1 | 43 | 8 | .49 | .2 | 27 | 16 | 410 | 5.29 | 5 | 5 | ND | 2 | 64 | 1 | 2 | 2 | 121 | .67 | .089 | 5 | 63 | .94 | 104 | .15 | 2 | 2.06 | .04 | .08 | 1 |
| S L3S 1550E | 1 | 69 | 8 | .52 | .4 | 32 | 13 | 401 | 3.83 | 7 | 5 | ND | 2 | 68 | 1 | 2 | 2 | 83 | 1.13 | .041 | 13 | 49 | .94 | 151 | .12 | 2 | 2.38 | .04 | .08 | 2 |
| S L3S 1600E | 1 | 41 | 4 | .57 | .5 | 26 | 12 | 255 | 3.88 | 6 | 5 | ND | 3 | 45 | 1 | 2 | 2 | 81 | .67 | .034 | 9 | 40 | .66 | 120 | .15 | 2 | 2.53 | .04 | .07 | 1 |
| S L5S 250E | 1 | 77 | 8 | .62 | .2 | 20 | 15 | 392 | 4.57 | 4 | 5 | ND | 1 | 81 | 1 | 2 | 2 | 125 | .63 | .129 | 4 | 46 | 1.14 | 49 | .15 | 2 | 2.01 | .03 | .06 | 1 |
| S L5S 300E | 1 | 68 | 10 | .75 | .2 | 35 | 21 | 485 | 6.36 | 3 | 5 | ND | 2 | 85 | 1 | 2 | 2 | 163 | .78 | .130 | 4 | 74 | 1.41 | 48 | .18 | 2 | 2.32 | .03 | .06 | 1 |
| S L5S 350E | 1 | 67 | 8 | .73 | .2 | 25 | 17 | 639 | 4.68 | 5 | 5 | ND | 2 | 89 | 1 | 2 | 2 | 123 | .63 | .122 | 4 | 54 | 1.28 | 73 | .14 | 3 | 2.44 | .04 | .07 | 1 |
| S L5S 400E | 1 | 92 | 7 | .67 | .1 | 24 | 17 | 391 | 4.64 | 7 | 5 | ND | 2 | 72 | 1 | 2 | 2 | 125 | .55 | .136 | 4 | 59 | 1.40 | 87 | .17 | 2 | 2.27 | .03 | .15 | 1 |
| S L5S 500E | 1 | 76 | 9 | .67 | .2 | 38 | 17 | 516 | 4.20 | 4 | 5 | ND | 1 | 83 | 1 | 2 | 2 | 108 | .64 | .073 | 3 | 93 | 1.35 | 107 | .18 | 2 | 1.96 | .04 | .07 | 1 |
| S L5S 550E | 1 | 65 | 7 | .70 | .2 | 29 | 17 | 410 | 5.39 | 2 | 5 | ND | 2 | 74 | 1 | 2 | 2 | 150 | .60 | .128 | 4 | 61 | 1.23 | 79 | .19 | 2 | 2.14 | .03 | .06 | 1 |
| S L5S 600E | 1 | 89 | 7 | .92 | .3 | 28 | 19 | 603 | 5.23 | 4 | 5 | ND | 2 | 105 | 1 | 2 | 2 | 148 | .70 | .170 | 4 | 52 | 1.29 | 53 | .16 | 3 | 2.27 | .04 | .07 | 1 |
| S L5S 650E | 1 | 106 | 9 | 112 | .3 | 19 | 19 | 814 | 5.01 | 5 | 5 | ND | 2 | 118 | 1 | 2 | 2 | 158 | .95 | .192 | 4 | 23 | 1.37 | 71 | .17 | 2 | 2.25 | .03 | .14 | 1 |
| S L5S 700E | 1 | 86 | 8 | .87 | .3 | 16 | 16 | 405 | 4.89 | 4 | 5 | ND | 2 | 111 | 1 | 2 | 2 | 140 | .55 | .187 | 4 | 26 | 1.08 | 40 | .16 | 2 | 2.33 | .03 | .05 | 1 |
| S L5S 750E | 1 | 49 | 11 | .85 | .4 | 18 | 13 | 425 | 3.87 | 5 | 5 | ND | 2 | 76 | 1 | 2 | 2 | 94 | .67 | .119 | 6 | 33 | 1.04 | 90 | .13 | 2 | 2.35 | .04 | .10 | 1 |
| S L5S 800E | 1 | 106 | 5 | .75 | .2 | 20 | 18 | 443 | 4.85 | 4 | 5 | ND | 2 | 147 | 1 | 2 | 2 | 159 | .73 | .149 | 5 | 34 | 1.45 | 49 | .19 | 2 | 2.33 | .03 | .12 | 1 |
| S L5S 850E | 1 | 119 | 9 | .90 | .3 | 17 | 19 | 602 | 4.72 | 6 | 5 | ND | 3 | 146 | 1 | 2 | 2 | 148 | .67 | .110 | 5 | 25 | 1.48 | 86 | .18 | 3 | 2.76 | .04 | .09 | 1 |
| STD C | 18 | 60 | 41 | 131 | 7.3 | 65 | 27 | 1048 | 4.04 | 39 | 16 | 7 | 38 | 50 | 18 | 16 | 19 | 56 | .48 | .081 | 38 | 59 | .89 | 178 | .08 | 38 | 1.92 | .07 | .13 | 11 |

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Page 5

| SAMPLE# | Mo
PPM | Cu
PPM | Pb
PPM | Zn
PPM | Ag
PPM | Ni
PPM | Co
PPM | Mn
PPM | Fe
% | As
PPM | U
PPM | Au
PPM | Th
PPM | SR
PPM | Cd
PPM | pb
PPM | Bi
PPM | V
PPM | Ca
PPM | P
PPM | La
PPM | Cr
PPM | Mg
PPM | Ba
PPM | Tl
PPM | B
PPM | Al
PPM | Na
PPM | K
PPM | N
PPM |
|-------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|----------|----------|
| S LSS 900E | 1 | 123 | 5 | 112 | .4 | 17 | 19 | 610 | 5.56 | 2 | 5 | ND | 2 | 105 | 1 | 2 | 2 | 167 | .70 | .194 | 7 | 26 | 1.68 | 83 | .21 | 4 | 2.74 | .04 | .13 | 1 |
| S LSS 950E | 1 | 218 | 4 | 101 | .2 | 27 | 23 | 707 | 6.13 | 2 | 5 | ND | 3 | 92 | 1 | 2 | 2 | 184 | .87 | .151 | 6 | 35 | 1.99 | 53 | .18 | 2 | 2.83 | .04 | .20 | 1 |
| S LSS 1000E | 1 | 112 | 2 | 97 | .3 | 16 | 19 | 698 | 4.83 | 2 | 5 | ND | 2 | 53 | 1 | 2 | 2 | 137 | .52 | .150 | 6 | 17 | 1.59 | 75 | .16 | 2 | 2.54 | .03 | .12 | 1 |
| S LSS 1050E | 1 | 137 | 2 | 100 | .4 | 28 | 21 | 736 | 4.78 | 3 | 5 | ND | 2 | 68 | 1 | 2 | 2 | 143 | .64 | .115 | 5 | 38 | 1.77 | 60 | .19 | 3 | 2.46 | .03 | .07 | 1 |
| S LSS 1100E | 1 | 140 | 5 | 106 | .4 | 19 | 19 | 1018 | 4.86 | 2 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 148 | .90 | .137 | 6 | 31 | 1.60 | 64 | .21 | 2 | 2.16 | .06 | .18 | 1 |
| S LSS 1150E | 1 | 252 | 4 | 92 | .5 | 25 | 18 | 1469 | 4.42 | 2 | 5 | ND | 3 | 79 | 1 | 2 | 2 | 120 | .81 | .057 | 7 | 32 | 1.33 | 79 | .21 | 2 | 3.02 | .05 | .06 | 1 |
| S LSS 1200E | 1 | 97 | 2 | 81 | .2 | 18 | 21 | 760 | 5.42 | 3 | 5 | ND | 1 | 50 | 1 | 2 | 2 | 115 | 1.06 | .216 | 4 | 36 | 1.15 | 76 | .10 | 4 | 2.10 | .04 | .04 | 1 |
| S LSS 1250E | 1 | 163 | 6 | 71 | .2 | 23 | 16 | 573 | 4.42 | 2 | 5 | ND | 1 | 51 | 1 | 2 | 2 | 114 | .96 | .115 | 5 | 35 | 1.13 | 77 | .16 | 4 | 2.50 | .05 | .07 | 1 |
| S LSS 1300E | 1 | 209 | 3 | 63 | .3 | 26 | 15 | 453 | 4.36 | 3 | 5 | ND | 2 | 51 | 1 | 2 | 2 | 101 | .51 | .044 | 4 | 34 | 1.08 | 109 | .19 | 2 | 2.78 | .04 | .04 | 1 |
| S LSS 1350E | 1 | 151 | 7 | 50 | .5 | 22 | 12 | 532 | 3.57 | 2 | 5 | ND | 2 | 91 | 1 | 2 | 2 | 78 | .93 | .052 | 11 | 32 | .83 | 99 | .15 | 2 | 2.01 | .05 | .04 | 1 |
| S LSS 1400E | 1 | 104 | 7 | 67 | .3 | 25 | 17 | 603 | 4.31 | 2 | 5 | ND | 2 | 87 | 1 | 2 | 2 | 106 | .88 | .053 | 6 | 36 | 1.12 | 119 | .18 | 3 | 2.15 | .05 | .07 | 1 |
| S LSS 1500E | 1 | 17 | 2 | 38 | .3 | 14 | 7 | 169 | 3.84 | 2 | 5 | ND | 1 | 38 | 1 | 2 | 2 | 96 | .39 | .052 | 3 | 43 | .55 | 58 | .15 | 2 | 1.12 | .03 | .04 | 1 |
| S LSS 1550E | 1 | 71 | 5 | 55 | .3 | 28 | 18 | 1197 | 5.29 | 4 | 5 | ND | 2 | 70 | 1 | 2 | 2 | 138 | .90 | .059 | 7 | 51 | 1.28 | 117 | .17 | 2 | 2.01 | .05 | .13 | 1 |
| S LSS 1600E | 1 | 43 | 4 | 59 | .1 | 20 | 15 | 405 | 4.92 | 2 | 5 | ND | 2 | 61 | 1 | 2 | 2 | 125 | .64 | .110 | 4 | 39 | .99 | 109 | .18 | 2 | 1.68 | .05 | .08 | 1 |
| S L7S 100E | 1 | 87 | 5 | 75 | .2 | 27 | 16 | 414 | 4.05 | 2 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 93 | .67 | .061 | 4 | 45 | 1.21 | 120 | .19 | 2 | 2.45 | .04 | .06 | 1 |
| S L7S 150E | 1 | 101 | 5 | 76 | .3 | 36 | 18 | 518 | 4.73 | 2 | 5 | ND | 2 | 70 | 1 | 2 | 2 | 115 | .95 | .093 | 6 | 73 | 1.42 | 146 | .17 | 2 | 2.38 | .04 | .06 | 1 |
| S L7S 200E | 1 | 36 | 2 | 52 | .3 | 25 | 12 | 293 | 4.77 | 4 | 5 | ND | 1 | 63 | 1 | 2 | 2 | 112 | .52 | .130 | 3 | 75 | .91 | 53 | .13 | 2 | 1.44 | .03 | .03 | 1 |
| S L7S 300E | 1 | 40 | 2 | 54 | .2 | 32 | 15 | 295 | 4.53 | 2 | 5 | ND | 1 | 63 | 1 | 2 | 2 | 100 | .38 | .097 | 3 | 95 | 1.06 | 88 | .15 | 2 | 1.83 | .03 | .04 | 1 |
| S L7S 350E | 1 | 42 | 3 | 59 | .2 | 48 | 17 | 339 | 4.56 | 2 | 5 | ND | 2 | 60 | 1 | 2 | 2 | 106 | .37 | .105 | 2 | 147 | 1.50 | 80 | .16 | 2 | 1.93 | .03 | .06 | 1 |
| S L7S 400E | 1 | 37 | 4 | 60 | .3 | 28 | 12 | 272 | 4.06 | 2 | 5 | ND | 1 | 40 | 1 | 2 | 2 | 84 | .37 | .094 | 3 | 101 | .82 | 72 | .13 | 2 | 1.82 | .03 | .05 | 1 |
| S L7S 450E | 1 | 34 | 4 | 57 | .2 | 31 | 13 | 317 | 4.14 | 2 | 5 | ND | 2 | 51 | 1 | 2 | 2 | 102 | .43 | .073 | 3 | 101 | 1.03 | 55 | .17 | 2 | 1.84 | .04 | .04 | 1 |
| S L7S 650E | 1 | 88 | 4 | 85 | .2 | 97 | 19 | 1085 | 4.17 | 2 | 5 | ND | 2 | 108 | 1 | 2 | 2 | 107 | .73 | .041 | 4 | 124 | 1.49 | 190 | .16 | 2 | 2.00 | .04 | .06 | 1 |
| S L7S 700E | 1 | 43 | 5 | 53 | .1 | 51 | 17 | 306 | 4.52 | 2 | 5 | ND | 1 | 81 | 1 | 2 | 2 | 110 | .59 | .076 | 2 | 125 | 1.37 | 71 | .15 | 2 | 1.46 | .04 | .05 | 1 |
| S L7S 750E | 1 | 39 | 6 | 54 | .2 | 45 | 14 | 289 | 3.69 | 2 | 5 | ND | 1 | 67 | 1 | 2 | 2 | 100 | .46 | .077 | 2 | 65 | 1.20 | 54 | .16 | 2 | 1.45 | .03 | .04 | 1 |
| S L7S 800E | 1 | 128 | 4 | 74 | .2 | 21 | 17 | 483 | 4.06 | 2 | 5 | ND | 1 | 66 | 1 | 2 | 2 | 120 | .56 | .139 | 4 | 36 | 1.49 | 66 | .17 | 4 | 2.13 | .03 | .15 | 1 |
| S L7S 850E | 1 | 78 | 4 | 62 | .2 | 13 | 14 | 420 | 3.86 | 2 | 5 | ND | 1 | 57 | 1 | 2 | 2 | 109 | .40 | .127 | 3 | 24 | 1.19 | 75 | .17 | 2 | 1.89 | .03 | .08 | 1 |
| S L7S 900E | 1 | 143 | 3 | 80 | .4 | 21 | 22 | 372 | 5.13 | 4 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 157 | .65 | .156 | 4 | 36 | 1.94 | 126 | .18 | 2 | 2.54 | .03 | .35 | 1 |
| S L7S 950E | 1 | 179 | 4 | 92 | .7 | 32 | 18 | 689 | 4.53 | 2 | 5 | ND | 3 | 60 | 1 | 2 | 2 | 131 | .58 | .106 | 7 | 64 | 1.43 | 87 | .19 | 2 | 2.49 | .04 | .16 | 1 |
| S L7S 1000E | 1 | 131 | 3 | 56 | .2 | 29 | 16 | 534 | 4.18 | 3 | 5 | ND | 2 | 88 | 1 | 2 | 2 | 112 | .80 | .136 | 6 | 69 | 1.38 | 59 | .15 | 2 | 1.26 | .03 | .26 | 1 |
| S L7S 1050E | 1 | 134 | 4 | 90 | .3 | 35 | 20 | 844 | 4.86 | 3 | 5 | ND | 3 | 65 | 1 | 2 | 2 | 128 | .88 | .133 | 6 | 58 | 1.61 | 118 | .16 | 2 | 2.27 | .04 | .29 | 1 |
| S L7S 1100E | 1 | 114 | 7 | 77 | .5 | 29 | 16 | 760 | 4.45 | 2 | 5 | ND | 3 | 78 | 1 | 2 | 2 | 107 | .62 | .047 | 8 | 48 | 1.04 | 261 | .18 | 2 | 2.36 | .04 | .07 | 1 |
| S L7S 1150E | 3 | 79 | 8 | 54 | .6 | 18 | 11 | 620 | 3.30 | 2 | 5 | ND | 2 | 111 | 1 | 2 | 2 | 74 | 1.22 | .066 | 6 | 28 | .71 | 194 | .10 | 2 | 1.92 | .04 | .06 | 1 |
| S L7S 1200E | 1 | 66 | 6 | 56 | .3 | 23 | 13 | 370 | 4.19 | 5 | 5 | ND | 2 | 63 | 1 | 2 | 2 | 94 | .62 | .085 | 6 | 39 | .81 | 173 | .11 | 2 | 1.91 | .04 | .09 | 1 |
| S L7S 1250E | 1 | 105 | 5 | 53 | .2 | 15 | 11 | 315 | 3.59 | 2 | 5 | ND | 1 | 117 | 1 | 2 | 2 | 98 | .68 | .054 | 3 | 24 | .90 | 107 | .15 | 2 | 1.61 | .03 | .03 | 1 |
| S L7S 1300E | 1 | 41 | 6 | 54 | .2 | 23 | 12 | 302 | 4.05 | 4 | 5 | ND | 2 | 55 | 1 | 2 | 2 | 102 | .62 | .096 | 5 | 47 | 1.00 | 66 | .13 | 2 | 1.48 | .04 | .07 | 1 |
| S L7S 1350E | 1 | 60 | 9 | 54 | .2 | 30 | 19 | 489 | 4.46 | 6 | 5 | ND | 3 | 56 | 1 | 2 | 2 | 104 | .71 | .075 | 9 | 54 | 1.12 | 105 | .12 | 2 | 1.90 | .05 | .08 | 1 |
| S L7S 1400E | 1 | 26 | 6 | 46 | .1 | 16 | 8 | 189 | 3.80 | 2 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 91 | .31 | .060 | 4 | 36 | .64 | 57 | .15 | 2 | 1.61 | .03 | .05 | 1 |
| S L7S 1450E | 1 | 47 | 5 | 69 | .2 | 26 | 16 | 451 | 4.37 | 5 | 5 | ND | 2 | 40 | 1 | 2 | 2 | 97 | .53 | .111 | 7 | 47 | 1.13 | 69 | .13 | 2 | 1.80 | .04 | .07 | 1 |
| S L7S 1500E | 1 | 26 | 6 | 51 | .2 | 19 | 9 | 229 | 3.38 | 2 | 5 | ND | 2 | 35 | 1 | 2 | 2 | 80 | .38 | .076 | 6 | 43 | .69 | 84 | .18 | 2 | 1.47 | .04 | .05 | 2 |
| STD C | 1B | 57 | 38 | 133 | 7.3 | 66 | 27 | 1059 | 4.13 | 39 | 21 | 8 | 37 | 50 | 18 | 17 | 19 | 56 | .49 | .081 | 38 | 59 | .92 | 176 | .08 | 31 | 1.86 | .08 | .14 | 12 |

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| SAMPLER | NO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | Cu | LB | BI | V | CA | P | LA | CR | M6 | BA | Tl | B | AL | NA | K | N |
|-------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|
| | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | I | I | PPM | PPM | I | PPM | I | PPM | I | PPM | I | PPM |
| S L75 1550E | 1 | 60 | 11 | .39 | .2 | 34 | 16 | 567 | 4.27 | 7 | 5 | ND | 4 | 88 | 1 | 2 | 2 | 93 | .86 | .080 | 14 | 60 | 1.15 | 143 | .09 | 2 | 2.06 | .05 | .14 | 1 |
| S L95 100E | 1 | 37 | 6 | .57 | .2 | 26 | 10 | 276 | 3.50 | 2 | 5 | ND | 2 | 86 | 1 | 2 | 2 | 86 | .71 | .046 | 5 | 73 | .91 | 94 | .16 | 2 | 1.84 | .04 | .05 | 1 |
| S L95 150E | 1 | 52 | 9 | .60 | .2 | 29 | 13 | 479 | 4.12 | 2 | 5 | ND | 2 | 77 | 1 | 2 | 2 | 95 | .63 | .091 | 5 | 72 | .92 | 93 | .14 | 2 | 2.27 | .04 | .06 | 1 |
| S L95 200E | 1 | 39 | 10 | .53 | .1 | 22 | 10 | 270 | 4.01 | 2 | 5 | ND | 1 | 68 | 1 | 2 | 2 | 96 | .50 | .100 | 4 | 56 | .95 | 53 | .16 | 2 | 2.25 | .04 | .05 | 1 |
| S L95 250E | 1 | 114 | 9 | .86 | .4 | 45 | 17 | 765 | 4.58 | 6 | 5 | ND | 1 | 96 | 1 | 2 | 2 | 108 | 1.15 | .083 | 11 | 88 | 1.26 | 183 | .12 | 2 | 2.45 | .05 | .07 | 1 |
| S L95 300E | 2 | 148 | 10 | .56 | .6 | 148 | 30 | 4221 | 5.88 | 33 | 5 | ND | 3 | 80 | 1 | 2 | 2 | 140 | .76 | .058 | 14 | 208 | 1.45 | 234 | .16 | 2 | 2.87 | .05 | .05 | 1 |
| S L95 350E | 1 | 48 | 6 | .62 | .1 | 43 | 13 | 316 | 4.86 | 2 | 5 | ND | 1 | 77 | 1 | 2 | 2 | 114 | .48 | .083 | 4 | 134 | 1.11 | 90 | .18 | 2 | 1.98 | .04 | .04 | 1 |
| S L95 400E | 1 | 23 | 5 | .53 | .2 | 43 | 15 | 240 | 5.54 | 2 | 5 | ND | 1 | 63 | 1 | 2 | 2 | 117 | .38 | .081 | 3 | 174 | .88 | 56 | .20 | 2 | 1.92 | .04 | .03 | 1 |
| S L95 450E | 1 | 30 | 7 | .50 | .1 | 49 | 14 | 222 | 5.17 | 2 | 5 | ND | 1 | 58 | 1 | 2 | 2 | 113 | .40 | .049 | 2 | 173 | .91 | 53 | .17 | 2 | 1.44 | .03 | .02 | 1 |
| S L95 500E | 1 | 44 | 10 | .66 | .2 | 70 | 13 | 605 | 3.39 | 4 | 5 | ND | 1 | 69 | 1 | 2 | 2 | 82 | .77 | .048 | 3 | 88 | 1.01 | 106 | .14 | 3 | 1.76 | .04 | .05 | 1 |
| S L95 550E | 1 | 30 | 7 | .54 | .1 | 31 | 13 | 248 | 5.20 | 2 | 5 | ND | 1 | 107 | 1 | 2 | 2 | 114 | .32 | .100 | 3 | 118 | .90 | 63 | .15 | 2 | 1.43 | .04 | .03 | 1 |
| S L95 650E | 1 | 42 | 5 | .76 | .1 | 80 | 26 | 442 | 6.49 | 5 | 5 | ND | 1 | 93 | 1 | 4 | 2 | 135 | .74 | .081 | 3 | 243 | 2.01 | 67 | .18 | 2 | 2.02 | .05 | .06 | 1 |
| S L95 700E | 1 | 22 | 8 | .57 | .1 | 41 | 14 | 283 | 4.73 | 3 | 5 | ND | 1 | 70 | 1 | 2 | 2 | 94 | .54 | .140 | 2 | 163 | 1.09 | 60 | .13 | 2 | 1.52 | .06 | .03 | 1 |
| S L95 750E | 1 | 35 | 3 | .50 | .1 | 63 | 19 | 341 | 4.82 | 2 | 5 | ND | 1 | 81 | 1 | 2 | 2 | 100 | .75 | .067 | 3 | 203 | 1.57 | 59 | .15 | 2 | 1.59 | .08 | .06 | 2 |
| S L95 800E | 1 | 22 | 10 | .47 | .1 | 33 | 11 | 396 | 3.27 | 2 | 5 | ND | 1 | 50 | 1 | 2 | 2 | 68 | .51 | .089 | 3 | 135 | .90 | 116 | .12 | 2 | 1.66 | .05 | .05 | 2 |
| S L95 850E | 1 | 35 | 8 | .56 | .1 | 21 | 11 | 494 | 3.69 | 5 | 5 | ND | 2 | 54 | 1 | 2 | 2 | 95 | .48 | .062 | 5 | 58 | .96 | 125 | .14 | 2 | 1.99 | .03 | .08 | 1 |
| S L95 900E | 1 | 54 | 5 | .58 | .1 | 17 | 14 | 336 | 3.75 | 2 | 5 | ND | 1 | 92 | 1 | 2 | 2 | 106 | .58 | .113 | 4 | 27 | 1.18 | 75 | .18 | 2 | 2.21 | .03 | .14 | 1 |
| S L95 950E | 1 | 40 | 9 | .69 | .2 | 18 | 16 | 536 | 4.11 | 2 | 5 | ND | 2 | 65 | 1 | 2 | 2 | 112 | .50 | .105 | 5 | 28 | 1.20 | 67 | .16 | 2 | 2.46 | .03 | .08 | 1 |
| S L95 1000E | 1 | 122 | 5 | .74 | .3 | 16 | 14 | 604 | 4.01 | 3 | 5 | ND | 2 | 51 | 1 | 2 | 2 | 103 | .45 | .127 | 4 | 23 | 1.13 | 68 | .16 | 2 | 2.30 | .03 | .08 | 1 |
| S L95 1050E | 1 | 72 | 6 | .72 | .2 | 13 | 14 | 648 | 3.95 | 2 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 105 | .37 | .137 | 3 | 17 | 1.02 | 45 | .15 | 2 | 1.89 | .03 | .05 | 1 |
| S L95 1100E | 1 | 99 | 8 | .80 | .2 | 20 | 17 | 517 | 4.33 | 4 | 5 | ND | 2 | 89 | 1 | 2 | 2 | 118 | .62 | .129 | 6 | 29 | 1.31 | 79 | .18 | 2 | 3.14 | .04 | .12 | 1 |
| S L95 1150E | 1 | 177 | 8 | .93 | .2 | 19 | 19 | 349 | 4.59 | 2 | 5 | ND | 2 | 88 | 1 | 2 | 2 | 123 | .65 | .140 | 4 | 24 | 1.53 | 69 | .22 | 2 | 3.08 | .04 | .12 | 1 |
| S L95 1200E | 1 | 52 | 6 | .66 | .1 | 52 | 20 | 461 | 3.27 | 2 | 5 | ND | 1 | 61 | 1 | 2 | 2 | 121 | .55 | .121 | 2 | 152 | 2.04 | 79 | .20 | 2 | 2.30 | .03 | .08 | 1 |
| S L95 1250E | 1 | 133 | 9 | .64 | .3 | 25 | 19 | 415 | 6.17 | 3 | 5 | ND | 1 | 62 | 1 | 2 | 2 | 144 | .68 | .220 | 3 | 48 | 1.21 | 77 | .14 | 2 | 2.21 | .06 | .06 | 1 |
| S L95 1350E | 1 | 211 | 8 | .69 | .2 | 46 | 30 | 523 | 7.28 | 4 | 5 | ND | 2 | 60 | 1 | 4 | 2 | 201 | .89 | .111 | 5 | 68 | 2.47 | 180 | .24 | 2 | 2.84 | .05 | .21 | 1 |
| S L95 1400E | 1 | 282 | 7 | 108 | .2 | 36 | 25 | 567 | 3.66 | 2 | 5 | ND | 2 | 100 | 1 | 3 | 2 | 157 | .79 | .169 | 4 | 58 | 1.67 | 157 | .21 | 2 | 2.69 | .04 | .09 | 1 |
| S L95 1450E | 1 | 71 | 7 | .53 | .3 | 29 | 14 | 454 | 4.73 | 4 | 5 | ND | 2 | 60 | 1 | 2 | 2 | 115 | .71 | .076 | 10 | 46 | .85 | 104 | .12 | 2 | 1.99 | .04 | .06 | 1 |
| S L95 1500E | 1 | 44 | 6 | .42 | .1 | 20 | 11 | 254 | 4.19 | 2 | 5 | ND | 1 | 42 | 1 | 2 | 2 | 105 | .44 | .090 | 3 | 49 | .76 | 55 | .14 | 2 | 1.55 | .04 | .06 | 1 |
| S L95 1550E | 1 | 38 | 6 | .44 | .1 | 20 | 11 | 452 | 2.94 | 2 | 5 | ND | 1 | 39 | 1 | 2 | 2 | 73 | .44 | .037 | 4 | 32 | .71 | 64 | .13 | 2 | 1.42 | .04 | .04 | 1 |
| S L95 1600E | 1 | 35 | 4 | .50 | .1 | 19 | 10 | 385 | 3.50 | 3 | 5 | ND | 1 | 37 | 1 | 2 | 2 | 83 | .42 | .089 | 3 | 37 | .71 | 73 | .13 | 2 | 1.47 | .03 | .05 | 1 |
| S L115 100E | 1 | 72 | 9 | .74 | .2 | 43 | 14 | 620 | 3.83 | 2 | 5 | ND | 2 | 83 | 1 | 2 | 2 | 91 | .69 | .039 | 5 | 86 | 1.03 | 116 | .20 | 2 | 2.42 | .05 | .06 | 1 |
| S L115 150E | 1 | 40 | 7 | .54 | .2 | 26 | 11 | 251 | 4.12 | 2 | 5 | ND | 1 | 77 | 1 | 2 | 2 | 95 | .46 | .131 | 3 | 77 | .81 | 58 | .15 | 2 | 1.92 | .04 | .04 | 1 |
| S L115 175E | 1 | 58 | 3 | .61 | .2 | 30 | 14 | 402 | 3.48 | 2 | 5 | ND | 1 | 96 | 1 | 2 | 2 | 90 | .80 | .053 | 3 | 56 | 1.15 | 99 | .19 | 2 | 2.14 | .04 | .08 | 1 |
| S L115 150E | 1 | 25 | 7 | .72 | .1 | 77 | 14 | 357 | 3.73 | 15 | 5 | ND | 2 | 62 | 1 | 2 | 2 | 82 | .62 | .047 | 3 | 126 | .96 | 80 | .17 | 2 | 1.90 | .05 | .03 | 1 |
| S L115 400E | 1 | 17 | 6 | .76 | .2 | 55 | 16 | 339 | 3.72 | 5 | 5 | ND | 1 | 65 | 1 | 2 | 2 | 74 | .43 | .072 | 3 | 104 | .84 | 97 | .16 | 2 | 1.54 | .04 | .03 | 1 |
| S L115 450E | 1 | 8 | 2 | .55 | .1 | 57 | 14 | 229 | 3.82 | 2 | 5 | ND | 1 | 42 | 1 | 2 | 2 | 66 | .31 | .024 | 3 | 113 | .86 | 42 | .17 | 2 | 1.31 | .04 | .03 | 1 |
| S L115 550E | 1 | 44 | 8 | .43 | .2 | 85 | 16 | 410 | 4.07 | 33 | 5 | ND | 3 | 54 | 1 | 2 | 2 | 93 | .46 | .025 | 5 | 140 | .90 | 129 | .17 | 2 | 2.56 | .05 | .04 | 1 |
| S L115 600E | 1 | 59 | 5 | .59 | .3 | 268 | 16 | 1177 | 4.04 | 46 | 5 | ND | 1 | 59 | 1 | 2 | 2 | 86 | .88 | .037 | 7 | 232 | 1.19 | 155 | .14 | 3 | 2.91 | .04 | .06 | 1 |
| S L115 650E | 1 | 28 | 6 | .51 | .1 | 96 | 13 | 213 | 3.46 | 8 | 5 | ND | 1 | 50 | 1 | 2 | 2 | 78 | .41 | .032 | 2 | 117 | .81 | 68 | .16 | 2 | 1.55 | .04 | .02 | 1 |
| STD C | 18 | 39 | 39 | 131 | 7.2 | 67 | 27 | 1039 | 4.05 | 37 | 20 | 7 | 37 | 49 | 18 | 17 | 20 | 55 | .48 | .087 | 38 | 58 | .90 | 172 | .08 | 31 | 1.91 | .07 | .13 | 11 |

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| SAMPLE# | MO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | CD | R | SI | V | CA | P | LA | CR | ME | BA | TI | B | AL | NA | X | N |
|--------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|-----|-----|------|-----|-----|-----|------|-----|-----|----|
| | PPM | % | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | PPM | |
| S L11S 700E | 1 | 55 | 9 | 76 | .1 | 108 | 19 | 365 | 4.60 | 2 | 5 | ND | 1 | 50 | 1 | 2 | 2 | 106 | .48 | .062 | 3 | 138 | 1.25 | 78 | .20 | 2 | 2.26 | .04 | .05 | 1 |
| S L11S 950E | 1 | 143 | 6 | 65 | .2 | 15 | 14 | 302 | 4.01 | 2 | 5 | ND | 1 | 52 | 1 | 2 | 2 | 115 | .43 | .147 | 3 | 23 | 1.33 | 131 | .18 | 2 | 2.32 | .03 | .25 | 1 |
| S L11S 1000E | 1 | 193 | 8 | 86 | .2 | 17 | 17 | 720 | 4.23 | 3 | 5 | ND | 1 | 41 | 1 | 2 | 2 | 114 | .46 | .123 | 3 | 18 | 1.47 | 103 | .21 | 2 | 2.91 | .03 | .10 | 1 |
| S L11S 1050E | 1 | 88 | 10 | 83 | .2 | 26 | 15 | 578 | 3.95 | 3 | 5 | ND | 2 | 45 | 1 | 2 | 2 | 96 | .46 | .130 | 4 | 34 | 1.13 | 103 | .14 | 2 | 2.71 | .03 | .08 | 1 |
| S L11S 1100E | 1 | 70 | 6 | 71 | .1 | 20 | 13 | 372 | 3.76 | 2 | 5 | ND | 1 | 56 | 1 | 2 | 2 | 90 | .38 | .117 | 3 | 27 | .95 | 54 | .17 | 2 | 2.43 | .03 | .04 | 1 |
| S L11S 1150E | 1 | 55 | 3 | 85 | .3 | 24 | 13 | 1487 | 3.63 | 2 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 81 | .30 | .087 | 4 | 36 | .86 | 120 | .15 | 2 | 2.63 | .03 | .06 | 1 |
| S L11S 1200E | 1 | 102 | 8 | 87 | .2 | 21 | 14 | 333 | 4.22 | 2 | 5 | ND | 1 | 42 | 1 | 2 | 2 | 106 | .44 | .107 | 4 | 31 | 1.12 | 66 | .17 | 2 | 2.41 | .03 | .07 | 1 |
| S L11S 1250E | 1 | 122 | 7 | 89 | .3 | 46 | 22 | 1297 | 4.87 | 2 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 129 | .68 | .074 | 5 | 90 | 1.82 | 101 | .21 | 2 | 2.85 | .04 | .06 | 1 |
| S L11S 1300E | 1 | 72 | 7 | 65 | .3 | 37 | 17 | 337 | 4.78 | 3 | 5 | ND | 2 | 31 | 1 | 2 | 2 | 117 | .29 | .095 | 4 | 79 | 1.28 | 78 | .17 | 2 | 2.22 | .03 | .04 | 1 |
| S L11S 1350E | 1 | 19 | 5 | 73 | .1 | 35 | 18 | 361 | 4.59 | 3 | 5 | ND | 1 | 44 | 1 | 2 | 2 | 113 | .62 | .203 | 4 | 61 | 1.50 | 109 | .13 | 2 | 1.95 | .05 | .07 | 1 |
| S L11S 1400E | 1 | 37 | 3 | 50 | .1 | 37 | 17 | 346 | 4.35 | 2 | 5 | ND | 1 | 37 | 1 | 2 | 2 | 97 | .35 | .085 | 2 | 93 | 1.31 | 36 | .13 | 2 | 1.38 | .02 | .22 | 1 |
| S L11S 1450E | 1 | 26 | 7 | 44 | .1 | 20 | 9 | 178 | 3.60 | 3 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 79 | .24 | .080 | 3 | 43 | .65 | 52 | .12 | 2 | 1.67 | .03 | .03 | 1 |
| S L11S 1500E | 1 | 28 | 10 | 44 | .3 | 19 | 9 | 175 | 3.75 | 3 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 85 | .27 | .073 | 4 | 31 | .62 | 59 | .13 | 2 | 1.94 | .03 | .05 | 1 |
| S L11S 1550E | 1 | 50 | 8 | 59 | .1 | 25 | 10 | 313 | 3.06 | 2 | 5 | ND | 1 | 38 | 1 | 2 | 2 | 70 | .45 | .032 | 6 | 28 | .82 | 107 | .14 | 2 | 2.18 | .04 | .04 | 1 |
| S L11S 1600E | 1 | 44 | 5 | 55 | .2 | 35 | 12 | 480 | 3.31 | 2 | 5 | ND | 2 | 46 | 1 | 2 | 2 | 77 | .56 | .043 | 6 | 43 | 1.18 | 102 | .15 | 2 | 2.09 | .04 | .04 | 1 |
| S L13S 300E | 1 | 33 | 7 | 74 | .2 | 40 | 12 | 534 | 2.82 | 2 | 5 | ND | 1 | 52 | 1 | 2 | 2 | 83 | .56 | .049 | 5 | 68 | 1.00 | 82 | .14 | 2 | 1.81 | .04 | .04 | 1 |
| S L13S 350E | 1 | 36 | 9 | 41 | .2 | 37 | 12 | 212 | 3.64 | 23 | 5 | ND | 1 | 34 | 1 | 2 | 2 | 88 | .32 | .040 | 3 | 108 | .80 | 56 | .13 | 2 | 1.65 | .03 | .03 | 1 |
| S L13S 400E | 1 | 17 | 5 | 31 | .1 | 20 | 8 | 126 | 3.50 | 2 | 5 | ND | 1 | 27 | 1 | 2 | 2 | 73 | .25 | .096 | 2 | 70 | .46 | 59 | .11 | 2 | 1.21 | .03 | .03 | 1 |
| S L13S 450E | 1 | 28 | 6 | 31 | .2 | 26 | 7 | 172 | 2.61 | 2 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 59 | .35 | .058 | 4 | 45 | .52 | 70 | .11 | 2 | 1.19 | .03 | .04 | 1 |
| S L13S 500E | 1 | 40 | 6 | 43 | .1 | 38 | 12 | 394 | 2.60 | 2 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 56 | .37 | .027 | 3 | 62 | .82 | 65 | .09 | 2 | 1.24 | .03 | .03 | 1 |
| S L13S 550E | 1 | 31 | 5 | 43 | .2 | 26 | 12 | 212 | 3.14 | 2 | 5 | ND | 1 | 31 | 1 | 2 | 2 | 75 | .32 | .045 | 3 | 54 | .83 | 55 | .13 | 2 | 1.31 | .03 | .04 | 1 |
| S L13S 600E | 1 | 23 | 6 | 30 | .1 | 22 | 9 | 175 | 2.37 | 24 | 5 | ND | 1 | 59 | 1 | 2 | 2 | 64 | .62 | .072 | 2 | 38 | .65 | 93 | .11 | 2 | 1.08 | .03 | .03 | 1 |
| S L13S 650E | 1 | 11 | 3 | 28 | .1 | 55 | 13 | 165 | 3.98 | 12 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 45 | .10 | .026 | 2 | 236 | .74 | 24 | .09 | 2 | .58 | .03 | .01 | 1 |
| S L13S 700E | 1 | 23 | 7 | 36 | .1 | 46 | 11 | 197 | 3.20 | 4 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 69 | .25 | .039 | 2 | 86 | .67 | 63 | .13 | 2 | 1.25 | .03 | .02 | 1 |
| S L13S 750E | 1 | 47 | 6 | 50 | .1 | 26 | 12 | 239 | 3.79 | 3 | 5 | ND | 2 | 28 | 1 | 2 | 2 | 93 | .26 | .069 | 3 | 48 | .90 | 55 | .16 | 2 | 2.12 | .03 | .04 | 2 |
| S L13S 800E | 1 | 43 | 7 | 59 | .1 | 21 | 12 | 283 | 3.27 | 3 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 79 | .32 | .068 | 3 | 45 | .82 | 75 | .14 | 2 | 1.76 | .03 | .05 | 1 |
| S L13S 850E | 1 | 36 | 7 | 49 | .1 | 24 | 9 | 241 | 3.35 | 3 | 5 | ND | 1 | 27 | 1 | 2 | 2 | 74 | .24 | .109 | 2 | 70 | .77 | 52 | .12 | 2 | 1.58 | .03 | .04 | 1 |
| S L13S 900E | 1 | 56 | 6 | 45 | .1 | 11 | 9 | 229 | 3.02 | 2 | 5 | ND | 1 | 35 | 1 | 2 | 2 | 74 | .32 | .073 | 3 | 32 | .75 | 77 | .12 | 2 | 1.40 | .02 | .06 | 1 |
| S L13S 1100E | 1 | 101 | 4 | 75 | .1 | 17 | 15 | 530 | 3.57 | 3 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 91 | .31 | .126 | 3 | 21 | 1.30 | 84 | .13 | 2 | 2.12 | .02 | .12 | 1 |
| S L13S 1150E | 1 | 59 | 2 | 46 | .2 | 8 | 10 | 265 | 2.95 | 2 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 82 | .24 | .065 | 2 | 11 | .94 | 56 | .13 | 2 | 1.62 | .02 | .06 | 1 |
| S L13S 1200E | 1 | 63 | 4 | 68 | .3 | 16 | 13 | 599 | 3.56 | 2 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 85 | .23 | .116 | 3 | 28 | .85 | 54 | .14 | 2 | 2.18 | .03 | .04 | 1 |
| S L13S 1250E | 1 | 39 | 7 | 54 | .3 | 15 | 10 | 229 | 3.29 | 2 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 74 | .24 | .099 | 3 | 24 | .67 | 52 | .12 | 2 | 1.62 | .03 | .04 | 1 |
| S L13S 1300E | 1 | 26 | 4 | 44 | .2 | 13 | 8 | 200 | 3.00 | 2 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 66 | .27 | .098 | 2 | 25 | .59 | 61 | .10 | 2 | 1.13 | .03 | .04 | 1 |
| S L13S 1450E | 1 | 47 | 7 | 41 | .2 | 24 | 9 | 310 | 3.36 | 2 | 5 | ND | 2 | 49 | 1 | 2 | 2 | 72 | .50 | .028 | 6 | 32 | .65 | 169 | .10 | 2 | 2.09 | .04 | .06 | 1 |
| S L13S 1500E | 1 | 46 | 7 | 43 | .2 | 28 | 12 | 311 | 3.30 | 2 | 5 | ND | 2 | 41 | 1 | 2 | 2 | 64 | .40 | .029 | 7 | 28 | .56 | 133 | .09 | 2 | 2.70 | .04 | .06 | 1 |
| S L13S 1550E | 1 | 46 | 5 | 42 | .4 | 24 | 15 | 554 | 3.39 | 2 | 5 | ND | 1 | 44 | 1 | 2 | 2 | 68 | .48 | .046 | 11 | 27 | .72 | 115 | .09 | 2 | 2.44 | .04 | .05 | 1 |
| S L13S 1600E | 1 | 47 | 9 | 55 | .1 | 22 | 12 | 482 | 3.46 | 3 | 5 | ND | 1 | 48 | 1 | 2 | 2 | 87 | .57 | .038 | 7 | 32 | .89 | 138 | .11 | 2 | 2.01 | .04 | .05 | 1 |
| S L13S 1700E | 1 | 36 | 3 | 38 | .1 | 26 | 10 | 215 | 3.12 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 74 | .22 | .074 | 2 | 71 | .84 | 48 | .10 | 2 | 1.44 | .02 | .02 | 1 |
| STD C | 18 | 60 | 39 | 131 | 7.4 | 67 | 27 | 1047 | 4.07 | 38 | 24 | 8 | 38 | 50 | 18 | 18 | 20 | 56 | .48 | .082 | 38 | 59 | .91 | 174 | .08 | 31 | 1.93 | .08 | .13 | 11 |

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| SAMPLE | NO | CU | PB | ZN | AG | NI | CO | MN | FE | AS | U | AU | TH | SR | CU | SB | BT | V | CA | P | LA | CR | Mg | BA | Tl | B | AL | NA | K | N |
|--------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|
| | PPM | I | PPM | I | I | PPM | PPM | I | PPM | I | PPM | I | PPM | I | PPM |
| S L155 200E | 1 | 93 | 9 | 73 | .3 | 163 | 16 | 889 | 4.52 | 15 | 5 | ND | 2 | 79 | 1 | 2 | 2 | 113 | .82 | .032 | 6 | 105 | 1.22 | 171 | .21 | 3 | 2.83 | .05 | .06 | 1 |
| S L155 250E | 1 | 28 | 4 | 47 | .2 | 39 | 13 | 256 | 4.31 | 2 | 5 | ND | 1 | 65 | 1 | 2 | 2 | 92 | .45 | .078 | 3 | 126 | .90 | 44 | .16 | 2 | 1.93 | .04 | .05 | 1 |
| S L155 300E | 1 | 24 | 5 | 48 | .2 | 32 | 12 | 321 | 4.45 | 5 | 5 | ND | 1 | 75 | 1 | 2 | 2 | 101 | .48 | .084 | 3 | 111 | .90 | 63 | .18 | 2 | 1.82 | .04 | .04 | 1 |
| S L155 350E | 1 | 24 | 5 | 37 | .1 | 31 | 13 | 281 | 4.41 | 2 | 5 | ND | 1 | 82 | 1 | 2 | 2 | 104 | .51 | .063 | 3 | 103 | .92 | 54 | .19 | 2 | 1.84 | .04 | .04 | 1 |
| S L155 400E | 1 | 23 | 10 | 49 | .1 | 24 | 10 | 647 | 3.58 | 2 | 5 | ND | 1 | 91 | 1 | 2 | 2 | 94 | .56 | .098 | 3 | 65 | .85 | 85 | .16 | 2 | 1.72 | .04 | .04 | 1 |
| S L155 450E | 1 | 23 | 6 | 52 | .2 | 38 | 13 | 275 | 4.30 | 8 | 5 | ND | 1 | 90 | 1 | 2 | 2 | 101 | .56 | .073 | 3 | 113 | .85 | 52 | .17 | 2 | 1.53 | .05 | .04 | 1 |
| S L155 500E | 1 | 23 | 6 | 46 | .1 | 33 | 13 | 386 | 3.75 | 2 | 5 | ND | 1 | 62 | 1 | 2 | 2 | 87 | .46 | .053 | 2 | 116 | .98 | 59 | .17 | 2 | 1.31 | .04 | .05 | 1 |
| S L155 550E | 1 | 53 | 7 | 65 | .1 | 359 | 49 | 795 | 6.32 | 2 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 101 | 1.51 | .027 | 2 | 237 | 3.95 | 29 | .19 | 3 | 1.98 | .03 | .01 | 1 |
| S L155 600E | 1 | 20 | 6 | 40 | .1 | 26 | 10 | 217 | 4.00 | 2 | 5 | ND | 2 | 57 | 1 | 2 | 2 | 100 | .48 | .069 | 3 | 93 | .84 | 53 | .16 | 2 | 1.62 | .04 | .04 | 1 |
| S L155 650E | 1 | 54 | 10 | 57 | .2 | 58 | 13 | 195 | 3.00 | 4 | 5 | ND | 1 | 41 | 1 | 2 | 2 | 70 | .30 | .064 | 3 | 48 | .74 | 83 | .16 | 2 | 2.13 | .04 | .04 | 1 |
| S L155 700E | 1 | 59 | 4 | 60 | .3 | 99 | 15 | 379 | 3.69 | 15 | 5 | ND | 2 | 80 | 1 | 2 | 2 | 94 | .75 | .050 | 4 | 69 | 1.05 | 122 | .21 | 2 | 2.27 | .04 | .05 | 1 |
| S L155 750E | 1 | 15 | 6 | 35 | .1 | 52 | 13 | 243 | 2.88 | 3 | 5 | ND | 1 | 48 | 1 | 2 | 2 | 62 | .44 | .018 | 2 | 157 | 1.04 | 61 | .15 | 2 | .93 | .03 | .04 | 1 |
| S L155 900E | 1 | 19 | 7 | 56 | .2 | 29 | 8 | 141 | 2.82 | 9 | 5 | ND | 1 | 40 | 1 | 2 | 2 | 66 | .42 | .025 | 3 | 103 | .51 | 92 | .17 | 2 | 1.78 | .04 | .03 | 1 |
| S L155 1000E | 1 | 18 | 7 | 93 | .1 | 20 | 8 | 245 | 2.69 | 3 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 63 | .75 | .029 | 4 | 53 | .70 | 155 | .13 | 2 | 1.86 | .05 | .04 | 1 |
| S L155 1050E | 1 | 71 | 7 | 64 | .4 | 42 | 15 | 565 | 4.29 | 5 | 5 | ND | 2 | 74 | 1 | 2 | 2 | 96 | .71 | .059 | 7 | 74 | 1.07 | 123 | .14 | 2 | 2.49 | .04 | .07 | 1 |
| S L155 1100E | 1 | 55 | 6 | 71 | .1 | 17 | 12 | 336 | 3.98 | 2 | 5 | ND | 1 | 99 | 1 | 2 | 2 | 115 | .56 | .098 | 4 | 32 | 1.06 | 57 | .22 | 2 | 2.57 | .04 | .08 | 1 |
| S L155 1150E | 1 | 20 | 6 | 61 | .2 | 19 | 9 | 209 | 4.46 | 2 | 5 | ND | 1 | 63 | 1 | 2 | 2 | 100 | .45 | .099 | 3 | 63 | .65 | 73 | .18 | 2 | 1.75 | .05 | .05 | 1 |
| S L155 1200E | 1 | 48 | 3 | 49 | .2 | 11 | 9 | 244 | 3.94 | 2 | 5 | ND | 1 | 91 | 1 | 2 | 2 | 113 | .53 | .098 | 3 | 26 | .80 | 42 | .22 | 2 | 1.88 | .04 | .04 | 1 |
| S L155 1250E | 1 | 79 | 5 | 65 | .1 | 17 | 13 | 364 | 4.55 | 2 | 5 | ND | 2 | 72 | 1 | 2 | 2 | 127 | .44 | .139 | 5 | 28 | 1.24 | 70 | .17 | 2 | 1.95 | .04 | .08 | 1 |
| S L155 1350E | 1 | 14 | 9 | 36 | .2 | 10 | 5 | 137 | 3.02 | 2 | 5 | ND | 1 | 38 | 1 | 2 | 2 | 90 | .35 | .022 | 3 | 26 | .37 | 44 | .21 | 2 | 1.02 | .04 | .05 | 1 |
| S L155 1400E | 1 | 41 | 5 | 75 | .2 | 22 | 12 | 489 | 3.51 | 2 | 5 | ND | 1 | 58 | 1 | 2 | 2 | 100 | .59 | .031 | 4 | 25 | .81 | 124 | .20 | 2 | 2.34 | .05 | .07 | 1 |
| S L155 1500E | 1 | 137 | 7 | 86 | .4 | 23 | 15 | 391 | 4.93 | 7 | 5 | ND | 2 | 84 | 1 | 2 | 2 | 139 | .59 | .074 | 5 | 35 | 1.24 | 75 | .22 | 2 | 3.16 | .04 | .09 | 1 |
| S L155 1600E | 1 | 56 | 10 | 88 | .3 | 24 | 13 | 453 | 4.29 | 6 | 5 | ND | 2 | 32 | 1 | 2 | 2 | 99 | .48 | .064 | 5 | 32 | .86 | 214 | .18 | 2 | 3.32 | .05 | .13 | 1 |
| S L175 100E | 1 | 9 | 7 | 30 | .1 | 27 | 8 | 141 | 3.08 | 3 | 5 | ND | 1 | 45 | 1 | 2 | 2 | 68 | .35 | .044 | 3 | 135 | .57 | 42 | .16 | 2 | 1.23 | .04 | .03 | 1 |
| S L175 150E | 1 | 38 | 7 | 40 | .2 | 49 | 17 | 277 | 5.21 | 4 | 5 | ND | 2 | 72 | 1 | 2 | 2 | 120 | .64 | .083 | 4 | 150 | 1.00 | 67 | .16 | 2 | 1.89 | .05 | .05 | 2 |
| S L175 200E | 1 | 20 | 8 | 43 | .2 | 28 | 10 | 182 | 4.03 | 4 | 5 | ND | 1 | 61 | 1 | 2 | 2 | 94 | .43 | .067 | 3 | 80 | .64 | 40 | .20 | 2 | 1.69 | .04 | .03 | 1 |
| S L175 250E | 1 | 3 | 6 | 32 | .1 | 23 | 7 | 102 | 3.23 | 3 | 5 | ND | 1 | 17 | 1 | 2 | 2 | 60 | .13 | .058 | 2 | 108 | .29 | 19 | .13 | 2 | 1.20 | .04 | .01 | 1 |
| S L175 300E | 1 | 18 | 7 | 45 | .2 | 56 | 14 | 188 | 4.08 | 3 | 5 | ND | 1 | 40 | 1 | 2 | 2 | 81 | .33 | .059 | 2 | 161 | .85 | 38 | .17 | 2 | 1.55 | .03 | .03 | 1 |
| S L175 350E | 1 | 4 | 8 | 48 | .1 | 79 | 13 | 140 | 4.24 | 19 | 5 | ND | 1 | 12 | 1 | 2 | 2 | 53 | .26 | .027 | 2 | 276 | .59 | 33 | .17 | 2 | 1.98 | .04 | .02 | 2 |
| S L175 400E | 1 | 54 | 7 | 57 | .2 | 148 | 19 | 265 | 4.22 | 19 | 5 | ND | 2 | 41 | 1 | 2 | 2 | 90 | .50 | .036 | 3 | 136 | 1.01 | 111 | .18 | 2 | 2.78 | .04 | .04 | 1 |
| S L175 450E | 1 | 32 | 6 | 63 | .1 | 161 | 22 | 364 | 4.34 | 24 | 5 | ND | 2 | 59 | 1 | 2 | 2 | 97 | .50 | .037 | 3 | 122 | 1.08 | 91 | .20 | 2 | 2.13 | .05 | .04 | 1 |
| S L175 500E | 1 | 113 | 9 | 44 | .3 | 132 | 20 | 486 | 4.57 | 117 | 5 | ND | 2 | 62 | 1 | 2 | 2 | 127 | .79 | .043 | 7 | 489 | 1.29 | 166 | .15 | 2 | 2.13 | .05 | .05 | 1 |
| S L175 550E | 1 | 41 | 6 | 67 | .2 | 85 | 14 | 258 | 3.42 | 13 | 5 | ND | 2 | 56 | 1 | 2 | 2 | 89 | .50 | .023 | 4 | 109 | .88 | 142 | .19 | 2 | 2.30 | .05 | .05 | 1 |
| S L175 600E | 1 | 30 | 8 | 37 | .1 | 31 | 10 | 199 | 3.45 | 2 | 5 | ND | 1 | 53 | 1 | 2 | 2 | 87 | .40 | .037 | 3 | 104 | .77 | 49 | .21 | 2 | 1.63 | .04 | .04 | 1 |
| S L175 650E | 1 | 8 | 6 | 29 | .1 | 33 | 9 | 116 | 3.83 | 2 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 74 | .16 | .019 | 2 | 140 | .50 | 37 | .21 | 2 | 1.64 | .04 | .02 | 1 |
| S L175 700E | 1 | 23 | 7 | 33 | .1 | 37 | 10 | 157 | 4.30 | 2 | 5 | ND | 1 | 32 | 1 | 2 | 2 | 97 | .30 | .012 | 3 | 211 | .93 | 50 | .21 | 2 | 1.69 | .03 | .03 | 1 |
| S L175 750E | 1 | 50 | 5 | 30 | .4 | 167 | 15 | 937 | 3.22 | 78 | 5 | ND | 2 | 25 | 1 | 2 | 2 | 59 | .68 | .028 | 10 | 506 | 1.14 | 270 | .08 | 3 | 2.00 | .04 | .06 | 1 |
| S L175 800E | 1 | 48 | 4 | 25 | .3 | 121 | 12 | 422 | 2.32 | 156 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 50 | 1.04 | .035 | 9 | 412 | .53 | 224 | .08 | 4 | 1.59 | .05 | .04 | 1 |
| S L175 850E | 1 | 6 | 4 | 21 | .1 | 71 | 16 | 246 | 2.26 | 6 | 5 | ND | 1 | 11 | 1 | 2 | 2 | 28 | .38 | .008 | 2 | 297 | 1.57 | 73 | .07 | 2 | .63 | .02 | .02 | 1 |
| STD C | 18 | 59 | 38 | 127 | 7.3 | 67 | 27 | 1051 | 4.08 | 38 | 22 | 8 | 37 | 49 | 18 | 17 | 20 | 56 | .48 | .081 | 38 | 59 | .90 | 173 | .08 | 37 | 1.85 | .08 | .13 | 12 |

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| SAMPLE# | MO
PPM | CU
PPM | PB
PPM | ZN
PPM | A6
PPM | NI
PPM | CD
PPM | MN
PPM | FE
PPM | AS
PPM | U
PPM | AU
PPM | TH
PPM | SR
PPM | CD
PPM | Ud
PPM | BI
PPM | V
PPM | CA
PPM | P
PPM | LA
PPM | CR
PPM | M6
PPM | BA
PPM | TI
PPM | B
PPM | AL
PPM | NA
PPM | K
PPM | M
PPM |
|--------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|----------|----------|
| S L17S 900E | 1 | 5 | 4 | 40 | .1 | 67 | 13 | 155 | 3.02 | 6 | 5 | ND | 1 | 12 | 1 | 2 | 2 | .48 | .32 | .024 | 2 | 200 | 1.06 | .58 | .13 | 2 | 1.28 | .03 | .02 | 1 |
| S L17S 950E | 1 | 14 | 4 | 35 | .2 | 99 | 19 | 628 | 2.63 | 5 | 5 | ND | 1 | 20 | 1 | 2 | 2 | .47 | .32 | .023 | 2 | 150 | 1.19 | .66 | .09 | 2 | 1.24 | .03 | .03 | 1 |
| S L17S 1000E | 1 | 12 | 3 | 65 | .1 | 149 | 18 | 741 | 3.17 | 11 | 5 | ND | 1 | 21 | 1 | 2 | 2 | .50 | .24 | .026 | 2 | 127 | .93 | .59 | .11 | 2 | 1.86 | .04 | .03 | 1 |
| S L17S 1050E | 1 | 23 | 4 | 54 | .2 | 74 | 14 | 496 | 3.12 | 4 | 5 | ND | 1 | 36 | 1 | 2 | 2 | .68 | .47 | .032 | 3 | 70 | .88 | 109 | .12 | 2 | 1.83 | .04 | .04 | 1 |
| S L17S 1100E | 1 | 94 | 3 | 34 | .6 | 143 | 10 | 631 | 2.81 | 71 | 5 | ND | 2 | 37 | 1 | 2 | 2 | .59 | .74 | .048 | 14 | 880 | .89 | 365 | .08 | 2 | 2.32 | .05 | .06 | 2 |
| S L17S 1150E | 1 | 34 | 8 | 51 | .4 | 32 | 15 | 548 | 3.97 | 40 | 5 | ND | 2 | 63 | 1 | 2 | 2 | 111 | .70 | .033 | 6 | 105 | 1.06 | 170 | .14 | 2 | 2.06 | .05 | .07 | 1 |
| S L17S 1200E | 1 | 50 | 6 | 50 | .4 | 27 | 14 | 446 | 4.48 | 20 | 5 | ND | 2 | 62 | 1 | 2 | 2 | 102 | .74 | .045 | 7 | 95 | 1.06 | 126 | .11 | 2 | 2.09 | .04 | .08 | 1 |
| S L17S 1250E | 1 | 40 | 4 | 67 | .2 | 27 | 14 | 409 | 4.17 | 3 | 5 | ND | 2 | 46 | 1 | 2 | 2 | .95 | .59 | .072 | 5 | 55 | 1.03 | 108 | .11 | 2 | 1.93 | .04 | .06 | 1 |
| S L17S 1300E | 1 | 22 | 7 | 39 | .2 | 21 | 10 | 190 | 4.19 | 6 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 103 | .29 | .055 | 2 | 72 | .70 | 57 | .11 | 2 | 1.25 | .03 | .04 | 1 |
| S L17S 1350E | 1 | 39 | 7 | 52 | .4 | 30 | 14 | 285 | 4.77 | 6 | 5 | ND | 1 | 48 | 1 | 2 | 2 | 106 | .56 | .068 | 7 | 85 | .92 | 96 | .10 | 2 | 1.83 | .04 | .05 | 1 |
| S L17S 1400E | 1 | 57 | 4 | 67 | .3 | 41 | 18 | 657 | 4.41 | 6 | 5 | ND | 2 | 57 | 1 | 2 | 2 | 111 | .52 | .056 | 6 | 63 | 1.14 | 144 | .10 | 2 | 2.31 | .04 | .07 | 1 |
| S L17S 1450E | 1 | 51 | 5 | 62 | .2 | 31 | 15 | 372 | 4.14 | 6 | 5 | ND | 1 | 44 | 1 | 2 | 2 | 103 | .49 | .075 | 4 | 55 | 1.14 | 93 | .11 | 2 | 1.46 | .04 | .08 | 1 |
| S L17S 1500E | 1 | 32 | 4 | 45 | .1 | 91 | 20 | 417 | 4.40 | 4 | 5 | ND | 1 | 30 | 1 | 2 | 2 | .63 | .43 | .019 | 2 | 374 | 1.80 | 51 | .10 | 2 | 1.49 | .04 | .04 | 2 |
| S L17S 1550E | 1 | 13 | 4 | 46 | .1 | 98 | 20 | 282 | 3.96 | 2 | 5 | ND | 1 | 19 | 1 | 2 | 2 | .57 | .22 | .029 | 2 | 166 | 1.52 | 46 | .09 | 2 | .92 | .03 | .02 | 2 |
| S L17S 1600E | 1 | 10 | 6 | 40 | .1 | 52 | 11 | 185 | 3.30 | 3 | 5 | ND | 1 | 14 | 1 | 2 | 2 | .55 | .17 | .033 | 2 | 162 | .99 | 30 | .10 | 2 | 1.02 | .02 | .01 | 2 |
| S L19S 100E | 1 | 7 | 6 | 27 | .2 | 20 | 7 | 118 | 2.41 | 3 | 5 | ND | 1 | 17 | 1 | 2 | 2 | .58 | .21 | .031 | 2 | 79 | .48 | 35 | .14 | 2 | .78 | .03 | .03 | 1 |
| S L19S 150E | 1 | 2 | 7 | 21 | .1 | 15 | 4 | 99 | 2.46 | 3 | 5 | ND | 1 | 10 | 1 | 2 | 2 | .71 | .13 | .026 | 2 | 118 | .37 | 14 | .12 | 2 | .41 | .02 | .02 | 1 |
| S L19S 200E | 1 | 9 | 8 | 32 | .1 | 24 | 7 | 123 | 3.94 | 3 | 5 | ND | 1 | 13 | 1 | 2 | 2 | .90 | .12 | .082 | 2 | 121 | .50 | 39 | .18 | 2 | .92 | .02 | .02 | 1 |
| S L19S 250E | 1 | 41 | 7 | 37 | .2 | 105 | 12 | 310 | 3.07 | 36 | 5 | ND | 1 | 23 | 1 | 2 | 2 | .74 | .51 | .031 | 3 | 124 | .82 | 147 | .10 | 2 | 1.67 | .03 | .06 | 1 |
| S L19S 300E | 1 | 22 | 6 | 31 | .1 | 43 | 11 | 152 | 3.34 | 5 | 5 | ND | 1 | 14 | 1 | 2 | 2 | .64 | .13 | .040 | 2 | 141 | .67 | 41 | .12 | 2 | 1.51 | .02 | .02 | 1 |
| S L19S 350E | 1 | 21 | 5 | 33 | .1 | 34 | 10 | 160 | 3.19 | 13 | 5 | ND | 1 | 24 | 1 | 2 | 2 | .79 | .21 | .031 | 2 | 76 | .62 | 54 | .15 | 2 | 1.35 | .02 | .03 | 1 |
| S L19S 400E | 1 | 14 | 4 | 39 | .2 | 54 | 11 | 173 | 3.34 | 11 | 5 | ND | 1 | 12 | 1 | 2 | 2 | .58 | .13 | .029 | 2 | 175 | .66 | 46 | .12 | 2 | 1.23 | .02 | .02 | 2 |
| S L19S 450E | 1 | 14 | 5 | 24 | .1 | 63 | 10 | 115 | 2.41 | 30 | 5 | ND | 1 | 17 | 1 | 2 | 2 | .59 | .31 | .013 | 2 | 161 | .56 | 100 | .11 | 2 | 1.33 | .03 | .02 | 2 |
| S L19S 500E | 1 | 22 | 4 | 50 | .2 | 51 | 13 | 197 | 4.13 | 9 | 5 | ND | 1 | 14 | 1 | 2 | 2 | .81 | .14 | .040 | 2 | 162 | .86 | 35 | .13 | 2 | 2.03 | .03 | .03 | 3 |
| S L19S 550E | 1 | 39 | 8 | 32 | .3 | 135 | 13 | 1057 | 3.04 | 21 | 5 | ND | 1 | 28 | 1 | 2 | 2 | .65 | .53 | .043 | 8 | 213 | 1.03 | 189 | .09 | 2 | 2.50 | .04 | .04 | 1 |
| S L19S 600E | 1 | 4 | 2 | 27 | .1 | 52 | 20 | 326 | 2.26 | 2 | 5 | ND | 1 | 7 | 1 | 2 | 2 | .19 | .30 | .017 | 2 | 155 | 1.07 | 51 | .05 | 2 | .46 | .02 | .02 | 1 |
| S L19S 650E | 1 | 12 | 3 | 48 | .1 | 48 | 13 | 166 | 3.80 | 3 | 5 | ND | 1 | 8 | 1 | 2 | 2 | .53 | .11 | .033 | 2 | 177 | .73 | 49 | .12 | 2 | 1.85 | .02 | .02 | 2 |
| S L19S 700E | 1 | 14 | 8 | 50 | .2 | 54 | 12 | 199 | 4.86 | 8 | 5 | ND | 1 | 8 | 1 | 2 | 2 | .51 | .14 | .040 | 2 | 296 | .76 | 31 | .11 | 2 | 1.76 | .02 | .02 | 3 |
| S L19S 750E | 1 | 37 | 4 | 57 | .3 | 49 | 14 | 342 | 3.41 | 15 | 5 | ND | 1 | 18 | 1 | 2 | 2 | .65 | .28 | .043 | 7 | 96 | .95 | 103 | .07 | 2 | 2.05 | .03 | .04 | 1 |
| S L19S 800E | 1 | 5 | 2 | 27 | .1 | 47 | 15 | 326 | 2.09 | 3 | 5 | ND | 1 | 3 | 1 | 2 | 2 | .17 | .05 | .025 | 2 | 181 | .85 | 18 | .04 | 2 | .40 | .01 | .01 | 1 |
| S L19S 850E | 1 | 22 | 5 | 32 | .3 | 94 | 10 | 377 | 2.38 | 128 | 5 | ND | 1 | 37 | 1 | 2 | 2 | .64 | 1.10 | .032 | 8 | 986 | .84 | 428 | .08 | 2 | 2.02 | .04 | .05 | 3 |
| S L19S 900E | 1 | 15 | 2 | 42 | .2 | 105 | 9 | 654 | 2.28 | 38 | 5 | ND | 1 | 19 | 1 | 2 | 2 | .52 | .34 | .021 | 5 | 139 | .55 | 181 | .09 | 2 | 1.74 | .03 | .04 | 1 |
| S L19S 950E | 1 | 15 | 2 | 39 | .1 | 94 | 11 | 332 | 2.78 | 15 | 5 | ND | 1 | 16 | 1 | 2 | 2 | .52 | .19 | .018 | 3 | 222 | .79 | 131 | .08 | 2 | 1.77 | .03 | .02 | 2 |
| S L19S 1000E | 1 | 25 | 5 | 42 | .2 | 55 | 12 | 234 | 3.10 | 6 | 5 | ND | 1 | 24 | 1 | 2 | 2 | .68 | .46 | .023 | 3 | 237 | 1.00 | 112 | .10 | 2 | 1.55 | .03 | .04 | 2 |
| S L19S 1050E | 1 | 32 | 5 | 54 | .2 | 26 | 16 | 632 | 4.04 | 17 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 107 | .60 | .040 | 5 | 87 | 1.17 | 130 | .12 | 2 | 1.91 | .05 | .06 | 1 |
| S L19S 1100E | 1 | 26 | 6 | 54 | .4 | 19 | 15 | 453 | 4.24 | 26 | 5 | ND | 1 | 53 | 1 | 2 | 2 | 123 | .80 | .093 | 7 | 73 | 1.20 | 139 | .10 | 2 | 1.79 | .05 | .07 | 1 |
| S L19S 1150E | 1 | 34 | 7 | 64 | .3 | 17 | 20 | 1171 | 4.27 | 5 | 5 | ND | 1 | 37 | 1 | 2 | 2 | .98 | .33 | .100 | 5 | 33 | .82 | 136 | .08 | 2 | 2.10 | .04 | .06 | 1 |
| S L19S 1200E | 1 | 23 | 6 | 50 | .2 | 20 | 14 | 449 | 4.37 | 7 | 5 | ND | 2 | 50 | 1 | 2 | 2 | 116 | .59 | .092 | 7 | 38 | 1.09 | 115 | .08 | 2 | 1.59 | .04 | .10 | 2 |
| S L19S 1300E | 1 | 85 | 7 | 53 | .3 | 46 | 16 | 1457 | 4.18 | 39 | 5 | ND | 2 | 48 | 1 | 2 | 2 | .96 | .68 | .059 | 10 | 91 | 1.13 | 247 | .09 | 2 | 2.30 | .04 | .10 | 1 |
| STD C | 18 | 58 | 39 | 132 | 7.5 | 66 | 28 | 1056 | 4.11 | 42 | 20 | 8 | 37 | 50 | 18 | 16 | 21 | 57 | .48 | .082 | 38 | 60 | .91 | 176 | .08 | 30 | 1.86 | .08 | .13 | 13 |

ROSSBACHER LABORATORY PROJECT #97842 FILE # 87-6066

Page 10

| SAMPLE# | Mo
PPM | Cu
PPM | Pb
PPM | Zn
PPM | Ag
PPM | Ni
PPM | Co
PPM | Mn
PPM | Fe
PPM | As
PPM | U
PPM | Au
PPM | Th
PPM | SR
PPM | Cd
PPM | SB
PPM | Bi
PPM | V
PPM | Ca
PPM | P
PPM | La
PPM | Er
PPM | Mg
PPM | Ba
PPM | Ti
PPM | S
PPM | Al
% | Na
% | K
PPM | M
PPM |
|--------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|---------|---------|----------|----------|
| S L19S 1350E | 1 | .51 | 7 | 70 | .1 | 34 | 17 | 682 | 4.50 | 6 | 5 | ND | 1 | 43 | 1 | 2 | 2 | 116 | .51 | .069 | 5 | 65 | 1.20 | 132 | .13 | 2 | 1.91 | .04 | .06 | 1 |
| S L19S 1400E | 1 | .59 | 4 | 70 | .2 | 40 | 16 | 604 | 4.50 | 9 | 5 | ND | 1 | 42 | 1 | 2 | 2 | 111 | .47 | .063 | 5 | 68 | 1.13 | 165 | .14 | 2 | 2.15 | .05 | .07 | 1 |
| S L19S 1450E | 1 | .43 | 3 | 48 | .1 | 28 | 19 | 730 | 4.55 | 4 | 5 | ND | 2 | 64 | 1 | 2 | 2 | 125 | .76 | .132 | 5 | 61 | 1.24 | 67 | .09 | 2 | 1.25 | .05 | .15 | 1 |
| S L19S 1500E | 1 | .30 | 2 | 59 | .1 | 37 | 12 | 311 | 3.75 | 3 | 5 | ND | 1 | 44 | 1 | 2 | 2 | 84 | .48 | .055 | 4 | 74 | 1.14 | 74 | .13 | 2 | 1.47 | .04 | .04 | 1 |
| S L19S 1550E | 1 | .46 | 3 | 56 | .1 | 39 | 17 | 453 | 4.25 | 4 | 5 | ND | 1 | 57 | 1 | 2 | 2 | 98 | .57 | .095 | 5 | 94 | 1.34 | 61 | .13 | 2 | 1.74 | .04 | .05 | 1 |
| S L19S 1600E | 1 | .49 | 3 | 67 | .1 | 55 | 29 | 1372 | 4.18 | 2 | 5 | ND | 1 | 51 | 1 | 2 | 2 | 86 | .48 | .069 | 5 | 103 | 1.62 | 81 | .11 | 2 | 1.81 | .03 | .04 | 1 |
| S L21S 100E | 1 | .10 | 5 | 40 | .1 | 49 | 16 | 219 | 5.46 | 9 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 146 | .26 | .041 | 2 | 182 | 1.01 | 51 | .19 | 2 | 1.43 | .03 | .02 | 1 |
| S L21S 150E | 1 | .19 | 4 | 40 | .1 | 50 | 16 | 201 | 5.11 | 3 | 7 | ND | 1 | 15 | 1 | 2 | 2 | 122 | .28 | .017 | 2 | 150 | .93 | 77 | .22 | 2 | 2.50 | .03 | .02 | 1 |
| S L21S 200E | 1 | .12 | 4 | 55 | .1 | 39 | 25 | 221 | 7.78 | 3 | 5 | ND | 1 | 8 | 1 | 2 | 2 | 238 | .28 | .020 | 2 | 77 | 1.80 | 102 | .32 | 2 | 2.19 | .03 | .06 | 1 |
| S L21S 250E | 1 | .18 | 3 | 42 | .1 | 41 | 15 | 183 | 5.53 | 2 | 5 | ND | 1 | 14 | 1 | 2 | 2 | 148 | .23 | .022 | 2 | 129 | 1.09 | 33 | .22 | 2 | 1.60 | .03 | .03 | 1 |
| S L21S 300E | 1 | .9 | 5 | 79 | .2 | 34 | 34 | 592 | 7.77 | 8 | 5 | ND | 1 | 11 | 1 | 2 | 2 | 269 | .45 | .015 | 2 | 36 | 2.37 | 130 | .34 | 2 | 2.30 | .03 | .05 | 1 |
| S L21S 350E | 1 | .10 | 6 | 86 | .1 | 48 | 37 | 852 | 9.58 | 28 | 5 | ND | 1 | 10 | 1 | 2 | 2 | 269 | .28 | .026 | 2 | 123 | 1.99 | 189 | .12 | 2 | 2.82 | .02 | .15 | 1 |
| S L21S 400E | 1 | .7 | 6 | 46 | .1 | 24 | 13 | 409 | 5.09 | 4 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 126 | .15 | .028 | 2 | 79 | .53 | 48 | .16 | 2 | 1.69 | .03 | .02 | 1 |
| S L21S 450E | 1 | .10 | 7 | 63 | .1 | 76 | 24 | 621 | 10.80 | 57 | 5 | ND | 1 | 5 | 1 | 2 | 2 | 208 | .06 | .033 | 2 | 208 | .93 | 50 | .03 | 2 | 1.79 | .02 | .02 | 1 |
| S L21S 500E | 1 | .19 | 3 | 42 | .2 | 70 | 14 | 579 | 4.48 | 99 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 134 | 1.09 | .039 | 4 | 227 | .86 | 150 | .09 | 2 | 1.73 | .04 | .03 | 1 |
| S L21S 550E | 1 | .12 | 2 | 39 | .1 | 46 | 15 | 443 | 4.60 | 5 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 101 | .32 | .033 | 2 | 204 | 1.28 | 67 | .13 | 2 | 1.59 | .03 | .02 | 1 |
| S L21S 600E | 1 | .9 | 3 | 38 | .1 | 27 | 14 | 190 | 6.19 | 3 | 5 | ND | 1 | 11 | 1 | 2 | 2 | 190 | .33 | .021 | 2 | 50 | .64 | 70 | .24 | 2 | 1.38 | .04 | .03 | 1 |
| S L21S 650E | 1 | .14 | 6 | 61 | .2 | 36 | 19 | 302 | 7.54 | 2 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 237 | .26 | .030 | 2 | 37 | 1.01 | 54 | .26 | 2 | 2.03 | .03 | .03 | 1 |
| S L21S 700E | 1 | .16 | 7 | 74 | .1 | 23 | 14 | 663 | 4.92 | 4 | 5 | ND | 2 | 12 | 1 | 2 | 2 | 114 | .21 | .032 | 3 | 42 | .70 | 70 | .17 | 2 | 1.88 | .03 | .04 | 1 |
| S L21S 750E | 1 | .35 | 5 | 76 | .2 | 44 | 16 | 863 | 4.70 | 7 | 5 | ND | 2 | 21 | 1 | 2 | 2 | 103 | .34 | .043 | 6 | 83 | 1.09 | 116 | .13 | 2 | 2.78 | .03 | .05 | 1 |
| S L21S 800E | 1 | .10 | 6 | 70 | .1 | 29 | 16 | 374 | 5.94 | 2 | 5 | ND | 1 | 11 | 1 | 2 | 2 | 173 | .28 | .029 | 2 | 48 | .92 | 105 | .26 | 2 | 1.77 | .04 | .04 | 1 |
| S L21S 850E | 1 | .15 | 6 | 58 | .1 | 27 | 12 | 338 | 5.06 | 4 | 5 | ND | 2 | 11 | 1 | 2 | 2 | 117 | .18 | .034 | 3 | 70 | .74 | 84 | .17 | 2 | 2.04 | .03 | .03 | 1 |
| S L21S 900E | 1 | .24 | 4 | 68 | .1 | 28 | 12 | 345 | 4.52 | 5 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 90 | .16 | .030 | 3 | 59 | .83 | 80 | .11 | 2 | 2.24 | .02 | .04 | 1 |
| S L21S 950E | 1 | .21 | 8 | 48 | .1 | 28 | 9 | 281 | 3.56 | 4 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 70 | .19 | .048 | 3 | 93 | .82 | 52 | .11 | 2 | 2.13 | .03 | .04 | 1 |
| S L21S 1000E | 1 | .49 | 6 | 54 | .6 | 31 | 6 | 241 | 2.67 | 2 | 6 | ND | 1 | 35 | 1 | 2 | 2 | 52 | .88 | .096 | 14 | 39 | .63 | 138 | .05 | 2 | 2.37 | .04 | .05 | 1 |
| S L21S 1050E | 1 | .31 | 8 | 58 | .1 | 32 | 11 | 789 | 3.39 | 82 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 77 | .62 | .045 | 7 | 82 | .83 | 155 | .08 | 2 | 2.19 | .04 | .06 | 1 |
| S L21S 1100E | 1 | .26 | 7 | 70 | .2 | 42 | 11 | 506 | 3.72 | 16 | 5 | ND | 1 | 27 | 1 | 2 | 2 | 74 | .40 | .043 | 6 | 61 | .88 | 109 | .10 | 2 | 2.22 | .03 | .05 | 1 |
| S L21S 1150E | 1 | .27 | 5 | 63 | .1 | 51 | 13 | 1048 | 3.66 | 16 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 71 | .42 | .049 | 7 | 118 | .93 | 123 | .08 | 2 | 2.00 | .03 | .04 | 1 |
| S L21S 1200E | 1 | .20 | 6 | 46 | .1 | 16 | 7 | 220 | 3.55 | 5 | 5 | ND | 1 | 26 | 1 | 2 | 2 | 79 | .28 | .069 | 3 | 43 | .68 | 63 | .11 | 2 | 1.63 | .03 | .03 | 1 |
| S L21S 1250E | 1 | .28 | 4 | 57 | .2 | 42 | 17 | 1039 | 3.93 | 3 | 5 | ND | 1 | 43 | 1 | 2 | 2 | 90 | .42 | .048 | 5 | 118 | 1.13 | 87 | .12 | 2 | 1.63 | .04 | .05 | 1 |
| S L21S 1300E | 1 | .24 | 5 | 55 | .2 | 19 | 8 | 299 | 2.80 | 11 | 5 | ND | 1 | 38 | 1 | 2 | 2 | 69 | .59 | .040 | 4 | 52 | .73 | 122 | .08 | 2 | 1.19 | .04 | .04 | 1 |
| S L21S 1350E | 1 | .38 | 5 | 64 | .3 | 23 | 12 | 599 | 3.99 | 6 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 87 | .33 | .072 | 5 | 46 | .94 | 80 | .11 | 2 | 2.07 | .03 | .06 | 1 |
| S L21S 1400E | 1 | .4 | 5 | 25 | .1 | 34 | 16 | 478 | 2.39 | 12 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 31 | .17 | .041 | 2 | 150 | .93 | 47 | .07 | 2 | .41 | .03 | .02 | 1 |
| S L21S 1450E | 1 | .25 | 6 | 33 | .3 | 147 | 14 | 643 | 2.61 | 69 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 62 | .87 | .040 | 6 | 635 | 1.34 | 256 | .09 | 3 | 1.69 | .04 | .04 | 2 |
| S L21S 1500E | 1 | .17 | 8 | 43 | .1 | 62 | 13 | 585 | 3.00 | 9 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 75 | .38 | .016 | 4 | 169 | 1.16 | 107 | .18 | 2 | 1.79 | .04 | .03 | 1 |
| S L21S 1550E | 1 | .13 | 6 | 39 | .1 | 78 | 19 | 368 | 3.72 | 2 | 5 | ND | 1 | 12 | 1 | 2 | 2 | 85 | .36 | .021 | 2 | 471 | 2.15 | 47 | .13 | 2 | .99 | .03 | .03 | 1 |
| S L21S 1575E | 1 | .14 | 8 | 33 | .1 | 52 | 12 | 203 | 3.45 | 3 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 69 | .22 | .022 | 2 | 244 | 1.17 | 40 | .15 | 2 | 1.54 | .04 | .03 | 1 |
| S BL 2150E | 1 | .16 | 10 | 53 | .3 | 110 | 19 | 526 | 3.79 | 12 | 8 | ND | 2 | 23 | 1 | 2 | 2 | 74 | .34 | .009 | 3 | 269 | 1.29 | 141 | .16 | 2 | 2.06 | .04 | .03 | 1 |
| S BL 300S | 1 | .65 | 5 | 55 | .2 | 32 | 13 | 343 | 3.82 | 7 | 5 | ND | 2 | 45 | 1 | 2 | 2 | 79 | .60 | .082 | 8 | 41 | .95 | 98 | .11 | 2 | 1.98 | .04 | .09 | 1 |
| STD C | 18 | .58 | .38 | 133 | 7.4 | 67 | 27 | 1058 | 4.14 | 40 | 24 | 7 | 38 | 50 | 18 | 18 | 20 | 56 | .49 | .082 | 38 | 60 | .91 | 174 | .08 | 30 | 1.87 | .07 | .13 | 12 |

ROSSBACHER LABORATORY PROJECT-87842 FILE # 87-6066

Page 11

| SAMPLE | 10
PPM | CU
PPM | PB
PPM | ZN
PPM | AG
PPM | NI
PPM | CO
PPM | NN
PPM | FE
PPM | AS
PPM | U
PPM | AU
PPM | TH
PPM | SR
PPM | CD
PPM | BI
PPM | V
PPM | CA
PPM | P
PPM | LA
PPM | CR
PPM | MG
PPM | BA
PPM | TI
PPM | B
PPM | AL
PPM | NA
PPM | K
PPM | N
PPM | |
|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|----------|-----------|-----------|-----------|-----------|-----------|----------|-----------|-----------|----------|----------|----|
| S BL 250S | 1 | 23 | 8 | .35 | .2 | 16 | 8 | 148 | 3.18 | 2 | 5 | ND | 1 | 14 | 1 | 2 | 3 | .59 | .23 | .030 | 4 | .25 | .43 | 104 | .12 | 2 | 1.86 | .02 | .04 | 2 |
| S BL 200S | 1 | 61 | 6 | .59 | .3 | 32 | 16 | 746 | 3.68 | 7 | 5 | ND | 3 | 40 | 1 | 2 | 2 | .68 | .77 | .077 | 9 | .45 | 1.20 | 116 | .09 | 2 | 1.71 | .03 | .14 | 1 |
| S BL 150S | 1 | 21 | 3 | .46 | .2 | 21 | 8 | 200 | 2.94 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | .57 | .36 | .059 | 3 | .33 | .71 | 105 | .09 | 2 | 1.50 | .03 | .06 | 2 |
| S BL 100S | 1 | 30 | 8 | .53 | .3 | 30 | 11 | 275 | 3.56 | 2 | 5 | ND | 2 | 22 | 1 | 2 | 2 | .63 | .31 | .083 | 4 | .40 | .80 | 92 | .09 | 2 | 2.10 | .03 | .06 | 1 |
| S BL 050S | 1 | 47 | 4 | .54 | .2 | 29 | 11 | 299 | 2.99 | 2 | 5 | ND | 2 | 33 | 1 | 2 | 2 | .62 | .51 | .068 | 7 | .39 | .87 | 90 | .09 | 2 | 1.64 | .03 | .07 | 1 |
| S BL 000 | 1 | 51 | 2 | .44 | .2 | 25 | 14 | 594 | 4.24 | 4 | 5 | ND | 1 | 45 | 1 | 2 | 2 | .96 | .69 | .101 | 5 | .53 | .88 | 112 | .07 | 2 | .96 | .03 | .12 | 2 |
| S BL 050N | 1 | 44 | 5 | .90 | .1 | 9 | 12 | 470 | 3.26 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | .79 | .29 | .088 | 2 | .12 | 1.17 | 46 | .12 | 2 | 1.62 | .02 | .07 | 1 |
| S BL 100N | 1 | 31 | 8 | .50 | .2 | 21 | 9 | 257 | 3.37 | 5 | 5 | ND | 1 | 17 | 1 | 2 | 2 | .61 | .27 | .096 | 3 | .35 | .86 | 55 | .07 | 2 | 1.37 | .02 | .05 | 3 |
| S BL 150N | 1 | 50 | 6 | .87 | .1 | 14 | 13 | 419 | 3.90 | 3 | 5 | ND | 1 | 17 | 1 | 2 | 2 | .86 | .24 | .090 | 3 | .18 | 1.33 | 65 | .10 | 2 | 2.51 | .02 | .06 | 1 |
| S BL 200N | 1 | 54 | 4 | .56 | .3 | 18 | 11 | 335 | 3.22 | 3 | 5 | ND | 1 | 27 | 1 | 2 | 2 | .63 | .37 | .030 | 4 | .23 | .80 | 192 | .09 | 2 | 2.19 | .03 | .04 | 1 |
| S BL 250N | 1 | 42 | 4 | .50 | .3 | 28 | 12 | 694 | 3.29 | 4 | 5 | ND | 2 | 35 | 1 | 2 | 2 | .57 | .62 | .054 | 9 | .39 | .99 | 135 | .09 | 2 | 1.65 | .03 | .09 | 1 |
| S BL 300N | 1 | 24 | 3 | .36 | .1 | 16 | 8 | 148 | 3.23 | 2 | 5 | ND | 1 | 16 | 1 | 2 | 2 | .67 | .22 | .094 | 2 | .31 | .48 | 35 | .07 | 2 | 1.38 | .02 | .02 | 2 |
| S BL 350N | 1 | 52 | 3 | .48 | .1 | 27 | 12 | 330 | 3.56 | 7 | 5 | ND | 1 | 27 | 1 | 2 | 2 | .66 | .39 | .074 | 5 | .40 | .97 | 57 | .08 | 2 | 1.56 | .03 | .05 | 2 |
| S BL 400N | 1 | 30 | 4 | .55 | .1 | 24 | 10 | 221 | 3.07 | 4 | 5 | ND | 2 | 16 | 1 | 2 | 2 | .55 | .23 | .068 | 4 | .35 | .69 | 65 | .08 | 2 | 1.82 | .02 | .04 | 1 |
| S BL 450N | 1 | 22 | 5 | .54 | .3 | 19 | 10 | 246 | 3.11 | 2 | 5 | ND | 1 | 17 | 1 | 3 | 2 | .57 | .23 | .093 | 3 | .26 | .62 | 68 | .09 | 2 | 2.03 | .02 | .05 | 1 |
| S BL 500N | 1 | 16 | 4 | .44 | .1 | 15 | 9 | 391 | 2.73 | 3 | 5 | ND | 1 | 25 | 1 | 2 | 2 | .58 | .43 | .050 | 3 | .25 | .75 | 73 | .08 | 2 | 1.24 | .03 | .04 | 1 |
| S BL 550N | 1 | 30 | 5 | .69 | .4 | 19 | 9 | 441 | 2.73 | 4 | 5 | ND | 1 | 36 | 1 | 2 | 2 | .47 | .72 | .060 | 5 | .26 | .67 | 94 | .07 | 2 | 1.55 | .03 | .06 | 1 |
| S BL 600N | 1 | 33 | 4 | .71 | .2 | 24 | 10 | 293 | 2.95 | 2 | 5 | ND | 1 | 21 | 1 | 2 | 2 | .47 | .34 | .049 | 4 | .28 | .76 | 86 | .07 | 2 | 1.83 | .03 | .05 | 1 |
| S BL 650N | 1 | 17 | 3 | .47 | .2 | 17 | 8 | 234 | 2.66 | 2 | 5 | ND | 1 | 11 | 1 | 2 | 2 | .45 | .17 | .055 | 2 | .22 | .57 | 42 | .07 | 2 | 1.34 | .02 | .04 | 1 |
| S BL 700N | 1 | 31 | 4 | .56 | .4 | 21 | 10 | 304 | 2.77 | 2 | 5 | ND | 1 | 17 | 1 | 2 | 2 | .44 | .29 | .056 | 3 | .26 | .70 | 72 | .07 | 2 | 1.68 | .02 | .05 | 1 |
| S BL 750N | 1 | 36 | 3 | .73 | .4 | 26 | 11 | 285 | 3.30 | 4 | 5 | ND | 1 | 16 | 1 | 2 | 3 | .53 | .25 | .082 | 3 | .33 | .74 | 69 | .08 | 2 | 2.06 | .02 | .05 | 1 |
| S BL 800N | 1 | 56 | 8 | .59 | .2 | 26 | 14 | 672 | 3.45 | 6 | 5 | ND | 1 | 28 | 1 | 2 | 2 | .58 | .53 | .078 | 8 | .34 | 1.05 | 71 | .08 | 2 | 1.72 | .03 | .08 | 1 |
| S BL 850N | 1 | 38 | 7 | .63 | .2 | 24 | 10 | 424 | 3.00 | 2 | 5 | ND | 1 | 21 | 1 | 2 | 2 | .46 | .26 | .059 | 8 | .35 | .77 | 73 | .07 | 2 | 1.94 | .02 | .07 | 1 |
| NO,NOE | 1 | 42 | 7 | .50 | .3 | 14 | B | 191 | 3.25 | 3 | 5 | ND | 1 | 30 | 1 | 2 | 2 | .69 | .37 | .053 | 4 | .28 | .63 | 72 | .08 | 2 | 1.41 | .03 | .04 | 2 |
| STD C | 18 | 39 | 39 | 130 | 7.2 | 67 | 27 | 1041 | 4.12 | 41 | 17 | 8 | 36 | 49 | 18 | 17 | 20 | .56 | .48 | .080 | 38 | .59 | .91 | 173 | .08 | 31 | 1.85 | .07 | .13 | 12 |

ACME ANALYTICAL LABORATORIES

DATE RECEIVED: DEC 4 1987

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE 253-3158

DATA LINE 251-1011 DATE REPORT MAILED: Dec. 17/87

GEOCHEMICAL ICP-MS ANALYSIS

10 GRAM SAMPLE FIRE ASSAY AND ANALYSIS BY ICP MASS SPECTROMETER.

- SAMPLE TYPE: Pulp

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

A & M EXPLORATION PROJECT-421 File # 87-6035 Page 1

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------------|-----------|-----------|-----------|
| L9N 1600E | 1 | 3 | 2 |
| L9N 1650E | 4 | 3 | 3 |
| L9N 1700E | 1 | 2 | 2 |
| L9N 1750E | 1 | 2 | 5 |
| L9N 1800E | 1 | 2 | 2 |
| L9N 1850E | 5 | 2 | 2 |
| L9N 1900E | 1 | 3 | 15 |
| L9N 1950E | 1 | 2 | 6 |
| L9N 2000E | 5 | 2 | 4 |
| L9N 2050E | 4 | 2 | 2 |
| L9N 2100E | 1 | 2 | 4 |
| L9N 2150E | 1 | 2 | 2 |
| L9N 2200E | 3 | 3 | 6 |
| L9N 2250E | 1 | 2 | 2 |
| L9N 2300E | 17 | 2 | 2 |
| L9N 2350E | 2 | 2 | 2 |
| L9N 2400E | 1 | 2 | 2 |
| L9N 2450E | 1 | 3 | 2 |
| L9N 2550E | 35 | 2 | 5 |
| L9N 2600E | 1 | 2 | 2 |
| L9N 2650E | 1 | 2 | 3 |
| L7N 1700E | 1 | 2 | 2 |
| L7N 1750E | 1 | 2 | 5 |
| L7N 1800E | 1 | 3 | 3 |
| L7N 1900E | 1 | 2 | 2 |
| L7N 1950E | 1 | 4 | 3 |
| L7N 2000E | 1 | 2 | 3 |
| L7N 2050E | 1 | 2 | 2 |
| L7N 2100E | 3 | 10 | 3 |
| L7N 2200E | 3 | 3 | 6 |
| L7N 2250E | 3 | 2 | 3 |
| L7N 2300E | 287 | 2 | 4 |
| L7N 2350E | 3 | 2 | 4 |
| L7N 2400E | 1 | 3 | 8 |
| L7N 2450E | 3 | 2 | 4 |
| DETECTION LIMIT | 1 | 2 | 2 |

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------------|-----------|-----------|-----------|
| L7N 2500E | 3 | 6 | 9 |
| L7N 2550E | 11 | 2 | 2 |
| L7N 2600E | 1 | 2 | 2 |
| L7N 2650E | 5 | 2 | 5 |
| L5N 1800E | 1 | 2 | 2 |
| L5N 1850E | 1 | 6 | 2 |
| L5N 1900E | 2 | 2 | 2 |
| L5N 1950E | 1 | 2 | 2 |
| L5N 2000E | 3 | 3 | 2 |
| L5N 2050E | 2 | 5 | 3 |
| L5N 2100E | 1 | 2 | 3 |
| L5N 2150E | 1 | 6 | 3 |
| L5N 2200E | 4 | 2 | 3 |
| L5N 2250E | 3 | 5 | 3 |
| L5N 2300E | 1 | 3 | 6 |
| L5N 2350E | 3 | 2 | 7 |
| L5N 2400E | 19 | 7 | 4 |
| L5N 2450E | 4 | 2 | 5 |
| L5N 2500E | 1 | 13 | 6 |
| L5N 2550E | 1 | 2 | 3 |
| L5N 2600E | 1 | 2 | 2 |
| L3N 1600E | 14 | 3 | 3 |
| L3N 1650E | 6 | 11 | 8 |
| L3N 1700E | 2 | 3 | 3 |
| L3N 1800E | 5 | 4 | 2 |
| L3N 1850E | 10 | 2 | 2 |
| L3N 1900E | 1 | 4 | 2 |
| L3N 1950E | 2 | 2 | 2 |
| L3N 2000E | 2 | 2 | 2 |
| L3N 2050E | 1 | 2 | 2 |
| L3N 2100E | .5 | 6 | 2 |
| L3N 2150E | 1 | 3 | 2 |
| L3N 2200E | 2 | 5 | 4 |
| L3N 2250E | 4 | 3 | 3 |
| L3N 2300E | 8 | 14 | 5 |
| L3N 2350E | 2 | 4 | 3 |
| DETECTION LIMIT | 1 | 2 | 2 |

A & M EXPLORATION PROJECT-421 FILE # 87-6035 Page 3

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------------|-----------|-----------|-----------|
| L3N 2400E | 115 | 5 | 4 |
| L3N 2450E | 2 | 15 | 4 |
| L3N 2500E | 1 | 2 | 4 |
| L3N 2550E | 1 | 10 | 3 |
| L3N 2600E | 1 | 2 | 2 |
|
 | | | |
| L1N 1650E | 1 | 9 | 8 |
| L1N 1700E | 5 | 32 | 9 |
| L1N 1750E | 1 | 4 | 4 |
| L1N 1800E | 7 | 2 | 2 |
| L1N 1850E | 2 | 7 | 6 |
|
 | | | |
| L1N 1900E | 2 | 6 | 44 |
| L1N 1950E | 1 | 3 | 2 |
| L1N 2000E | 1 | 2 | 5 |
| L1N 2050E | 1 | 2 | 2 |
| L1N 2100E | 3 | 4 | 2 |
|
 | | | |
| L1N 2150E | 1 | 3 | 2 |
| L1N 2200E | 3 | 3 | 4 |
| L1N 2250E | 4 | 3 | 4 |
| L1N 2300E | 8 | 6 | 4 |
| L1N 2350E | 1 | 4 | 5 |
|
 | | | |
| L1N 2400E | 2 | 2 | 2 |
| L1N 2450E | 1 | 24 | 7 |
| L1N 2500E | 3 | 3 | 3 |
| L1N 2550E | 2 | 3 | 4 |
| L1N 2600E | 3 | 11 | 16 |
|
 | | | |
| L1S 1650E | 1 | 2 | 2 |
| L1S 1700E | 7 | 3 | 6 |
| L1S 1750E | 1 | 2 | 2 |
| L1S 1800E | 2 | 2 | 7 |
| L1S 1850E | 1 | 3 | 5 |
|
 | | | |
| L1S 1900E | 3 | 2 | 2 |
| L1S 1950E | 5 | 2 | 6 |
| L1S 2000E | 1 | 3 | 6 |
| L1S 2100E | 14 | 4 | 3 |
| L1S 2150E | 1 | 3 | 2 |
|
 | | | |
| L1S 2200E | 2 | 3 | 2 |
| DETECTION LIMIT | 1 | 2 | 2 |

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------|-----------|-----------|-----------|
| L1S 2250E | 1 | 2 | 2 |
| L1S 2300E | 1 | 3 | 4 |
| L1S 2350E | 6 | 3 | 2 |
| L1S 2400E | 16 | 3 | 3 |
| L1S 2450E | 1 | 3 | 3 |
| L1S 2500E | 2 | 3 | 4 |
| L1S 2550E | 1 | 5 | 4 |
| L1S 2600E | 1 | 5 | 5 |
| L3S 100E | 1 | 2 | 8 |
| L3S 150E | 1 | 2 | 4 |
| L3S 200E | 1 | 2 | 6 |
| L3S 250E | 1 | 2 | 6 |
| L3S 300E | 1 | 3 | 5 |
| L3S 350E | 1 | 2 | 5 |
| L3S 400E | 1 | 2 | 6 |
| L3S 500E | 16 | 2 | 6 |
| L3S 550E | 1 | 2 | 4 |
| L3S 600E | 4 | 2 | 3 |
| L3S 650E | 1 | 4 | 5 |
| L3S 700E | 1 | 3 | 12 |
| L3S 750E | 1 | 2 | 8 |
| L3S 850E | 1 | 3 | 7 |
| L3S 900E | 1 | 3 | 13 |
| L3S 950E | 1 | 3 | 8 |
| L3S 1000E | 1 | 2 | 5 |
| L3S 1050E | 1 | 9 | 7 |
| L3S 1100E | 3 | 10 | 7 |
| L3S 1150E | 2 | 3 | 4 |
| L3S 1200E | 1 | 3 | 5 |
| L3S 1250E | 1 | 2 | 3 |
| L3S 1300E | 1 | 3 | 6 |
| L3S 1350E | 2 | 3 | 5 |
| L3S 1400E | 1 | 2 | 12 |
| L3S 1450E | 1 | 3 | 6 |
| L3S 1500E | 1 | 13 | 12 |
| L3S 1550E | 1 | 3 | 5 |

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------|-----------|-----------|-----------|
| L3S 1600E | 2 | 3 | 3 |
| L5S 250E | 1 | 2 | 8 |
| L5S 300E | 1 | 4 | 31 |
| L5S 350E | 7 | 2 | 6 |
| L5S 400E | 1 | 3 | 8 |
| L5S 500E | 1 | 4 | 5 |
| L5S 550E | 1 | 3 | 5 |
| L5S 600E | 1 | 4 | 11 |
| L5S 650E | 1 | 9 | 11 |
| L5S 700E | 1 | 2 | 9 |
| L5S 750E | 1 | 2 | 5 |
| L5S 800E | 1 | 2 | 11 |
| L5S 850E | 1 | 2 | 9 |
| L5S 900E | 1 | 2 | 10 |
| L5S 950E | 1 | 2 | 11 |
| L5S 1000E | 2 | 5 | 9 |
| L5S 1050E | 1 | 2 | 8 |
| L5S 1100E | 1 | 2 | 43 |
| L5S 1150E | 1 | 2 | 7 |
| L5S 1200E | 1 | 61 | 230 |
| L5S 1250E | 2 | 8 | 8 |
| L5S 1300E | 1 | 4 | 6 |
| L5S 1350E | 15 | 4 | 8 |
| L5S 1400E | 3 | 7 | 7 |
| L5S 1500E | 1 | 6 | 5 |
| L5S 1550E | 1 | 7 | 7 |
| L5S 1600E | 3 | 24 | 8 |
| L7S 100E | 3 | 2 | 6 |
| L7S 150E | 1 | 3 | 16 |
| L7S 200E | 1 | 4 | 7 |
| L7S 300E | 1 | 4 | 5 |
| L7S 350E | 1 | 8 | 6 |
| L7S 400E | 1 | 3 | 4 |
| L7S 450E | 4 | 3 | 8 |
| L7S 650E | 1 | 3 | 8 |
| L7S 700E | 1 | 6 | 15 |

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------|-----------|-----------|-----------|
| L7S 750E | 1 | 7 | 6 |
| L7S 800E | 1 | 3 | 37 |
| L7S 850E | 1 | 2 | 8 |
| L7S 900E | 1 | 2 | 8 |
| L7S 950E | 3 | 3 | 11 |
| L7S 1000E | 2 | 4 | 17 |
| L7S 1050E | 2 | 2 | 12 |
| L7S 1100E | 1 | 10 | 8 |
| L7S 1150E | 1 | 2 | 10 |
| L7S 1200E | 2 | 4 | 6 |
| L7S 1250E | 3 | 4 | 7 |
| L7S 1300E | 2 | 6 | 5 |
| L7S 1350E | 6 | 6 | 6 |
| L7S 1400E | 1 | 5 | 3 |
| L7S 1450E | 1 | 4 | 7 |
| L7S 1500E | 1 | 4 | 5 |
| L7S 1550E | 2 | 6 | 5 |
| L9S 100E | 1 | 3 | 4 |
| L9S 150E | 1 | 3 | 6 |
| L9S 200E | 1 | 3 | 5 |
| L9S 250E | 4 | 3 | 8 |
| L9S 300E | 2 | 5 | 15 |
| L9S 350E | 1 | 4 | 5 |
| L9S 400E | 1 | 6 | 4 |
| L9S 450E | 1 | 6 | 6 |
| L9S 500E | 1 | 3 | 5 |
| L9S 550E | 1 | 4 | 7 |
| L9S 650E | 1 | 6 | 3 |
| L9S 700E | 1 | 6 | 3 |
| L9S 750E | 1 | 7 | 7 |
| L9S 800E | 1 | 3 | 3 |
| L9S 850E | 1 | 2 | 4 |
| L9S 900E | 1 | 2 | 6 |
| L9S 950E | 1 | 2 | 8 |
| L9S 1000E | 1 | 2 | 8 |
| L9S 1050E | 1 | 2 | 9 |
| L9S 1100E | 1 | 2 | 6 |

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|------------|-----------|-----------|-----------|
| L9S 1150E | 2 | 2 | 10 |
| L9S 1200E | 1 | 4 | 7 |
| L9S 1250E | 2 | 25 | 34 |
| L9S 1350E | 3 | 16 | 49 |
| L9S 1400E | 1 | 4 | 11 |
| L9S 1450E | 1 | 9 | 10 |
| L9S 1500E | 6 | 6 | 5 |
| L9S 1550E | 1 | 6 | 3 |
| L9S 1600E | 1 | 12 | 4 |
| L11S 100E | 2 | 3 | 11 |
| L11S 150E | 1 | 3 | 6 |
| L11S 175E | 1 | 3 | 6 |
| L11S 350E | 1 | 5 | 4 |
| L11S 400E | 5 | 23 | 3 |
| L11S 450E | 1 | 62 | 2 |
| L11S 550E | 1 | 4 | 5 |
| L11S 600E | 1 | 4 | 5 |
| L11S 650E | 1 | 6 | 4 |
| L11S 700E | 1 | 5 | 30 |
| L11S 950E | 1 | 2 | 6 |
| L11S 1000E | 1 | 2 | 5 |
| L11S 1050E | 1 | 2 | 5 |
| L11S 1100E | 1 | 3 | 6 |
| L11S 1150E | 1 | 2 | 5 |
| L11S 1200E | 1 | 2 | 6 |
| L11S 1250E | 1 | 3 | 7 |
| L11S 1300E | 3 | 8 | 7 |
| L11S 1350E | 1 | 8 | 11 |
| L11S 1400E | 1 | 9 | 35 |
| L11S 1450E | 1 | 9 | 5 |
| L11S 1500E | 1 | 4 | 6 |
| L11S 1550E | 1 | 3 | 4 |
| L11S 1600E | 1 | 8 | 5 |
| L13S 300E | 1 | 3 | 4 |
| L13S 350E | 1 | 6 | 7 |
| L13S 400E | 1 | 4 | 7 |

A & M EXPLORATION PROJECT-421 FILE # 87-6035 Page B

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|------------|-----------|-----------|-----------|
| L13S 450E | 1 | 5 | 2 |
| L13S 500E | 2 | 8 | 4 |
| L13S 550E | 7 | 6 | 6 |
| L13S 600E | 1 | 4 | 3 |
| L13S 650E | 1 | 33 | 2 |
| L13S 700E | 1 | 11 | 4 |
| L13S 750E | 1 | 6 | 5 |
| L13S 800E | 1 | 3 | 3 |
| L13S 850E | 1 | 3 | 3 |
| L13S 950E | 1 | 2 | 6 |
| L13S 1100E | 1 | 2 | 6 |
| L13S 1150E | 1 | 2 | 6 |
| L13S 1200E | 1 | 7 | 5 |
| L13S 1250E | 1 | 2 | 5 |
| L13S 1300E | 2 | 3 | 6 |
| L13S 1450E | 1 | 3 | 3 |
| L13S 1500E | 1 | 2 | 2 |
| L13S 1550E | 1 | 6 | 3 |
| L13S 1600E | 1 | 3 | 4 |
| L15S 150E | 1 | 5 | 4 |
| L15S 200E | 1 | 5 | 7 |
| L15S 250E | 1 | 6 | 4 |
| L15S 300E | 1 | 7 | 4 |
| L15S 350E | 1 | 5 | 6 |
| L15S 400E | 1 | 7 | 6 |
| L15S 450E | 2 | 5 | 5 |
| L15S 500E | 1 | 9 | 5 |
| L15S 550E | 2 | 11 | 5 |
| L15S 600E | 1 | 8 | 9 |
| L15S 650E | 1 | 22 | 4 |
| L15S 700E | 1 | 9 | 5 |
| L15S 750E | 1 | 16 | 4 |
| L15S 900E | 1 | 5 | 5 |
| L15S 1000E | 1 | 3 | 3 |
| L15S 1050E | 1 | 4 | 5 |

A & M EXPLORATION PROJECT-421 FILE # 87-6035 Page 9

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|------------|-----------|-----------|-----------|
| L15S 1100E | 3 | 2 | 4 |
| L15S 1150E | 1 | 8 | 3 |
| L15S 1200E | 1 | 2 | 5 |
| L15S 1250E | 2 | 3 | 5 |
| L15S 1300E | 6 | 3 | 2 |
| L15S 1400E | 1 | 2 | 3 |
| L15S 1500E | 2 | 2 | 5 |
| L15S 1600E | 1 | 4 | 6 |
| L17S 100E | 2 | 10 | 2 |
| L17S 150E | 68 | 7 | 3 |
| L17S 200E | 1 | 5 | 3 |
| L17S 250E | 1 | 8 | 2 |
| L17S 300E | 4 | 17 | 2 |
| L17S 350E | 1 | 10 | 2 |
| L17S 400E | 31 | 5 | 4 |
| L17S 450E | 2 | 6 | 2 |
| L17S 500E | 1 | 5 | 15 |
| L17S 550E | 1 | 4 | 2 |
| L17S 600E | 1 | 6 | 3 |
| L17S 650E | 1 | 10 | 2 |
| L17S 700E | 3 | 5 | 4 |
| L17S 750E | 3 | 11 | 17 |
| L17S 800E | 2 | 10 | 14 |
| L17S 850E | 1 | 33 | 2 |
| L17S 900E | 1 | 46 | 4 |
| L17S 950E | 1 | 12 | 2 |
| L17S 1000E | 1 | 8 | 2 |
| L17S 1050E | 2 | 6 | 2 |
| L17S 1100E | 3 | 9 | 17 |
| L17S 1150E | 4 | 4 | 7 |
| L17S 1200E | 2 | 6 | 21 |
| L17S 1250E | 2 | 4 | 7 |
| L17S 1300E | 1 | 5 | 5 |
| L17S 1350E | 1 | 5 | 3 |
| L17S 1400E | 2 | 52 | 9 |
| L17S 1450E | 2 | 7 | 8 |

A & M EXPLORATION PROJECT-421 FILE # 87-6035 Page 10

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|------------|-----------|-----------|-----------|
| L17S 1500E | 2 | 7 | 3 |
| L17S 1550E | 1 | 13 | 3 |
| L17S 1600E | 1 | 9 | 3 |
| L19S 100E | 1 | 12 | 3 |
| L19S 150E | 1 | 26 | 2 |
| L19S 200E | 3 | 8 | 3 |
| L19S 250E | 1 | 12 | 6 |
| L19S 300E | 47 | 8 | 2 |
| L19S 350E | 1 | 4 | 4 |
| L19S 400E | 1 | 16 | 2 |
| L19S 450E | 2 | 15 | 3 |
| L19S 500E | 2 | 17 | 2 |
| L19S 550E | 1 | 9 | 3 |
| L19S 600E | 1 | 54 | 2 |
| L19S 650E | 1 | 18 | 2 |
| L19S 700E | 2 | 20 | 2 |
| L19S 750E | 1 | 25 | 4 |
| L19S 800E | 1 | 72 | 2 |
| L19S 850E | 1 | 47 | 17 |
| L19S 900E | 1 | 2 | 3 |
| L19S 950E | 2 | 25 | 2 |
| L19S 1000E | 2 | 16 | 4 |
| L19S 1050E | 5 | 5 | 13 |
| L19S 1100E | 2 | 5 | 6 |
| L19S 1150E | 2 | 5 | 6 |
| L19S 1200E | 6 | 6 | 8 |
| L19S 1300E | 1 | 5 | 6 |
| L19S 1350E | 1 | 5 | 5 |
| L19S 1400E | 2 | 5 | 8 |
| L19S 1450E | 6 | 10 | 8 |
| L19S 1500E | 4 | 8 | 4 |
| L19S 1550E | 2 | 22 | 37 |
| L19S 1600E | 2 | 9 | 5 |
| L21S 100E | 1 | 33 | 3 |
| L21S 150E | 1 | 17 | 4 |
| L21S 200E | 2 | 20 | 13 |

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| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|------------|-----------|-----------|-----------|
| L21S 250E | 2 | 9 | 3 |
| L21S 300E | 2 | 10 | 7 |
| L21S 350E | 4 | 14 | 9 |
| L21S 400E | 1 | 6 | 2 |
| L21S 450E | 2 | 34 | 2 |
| L21S 500E | 1 | 12 | 2 |
| L21S 550E | 2 | 62 | 11 |
| L21S 600E | 1 | 14 | 2 |
| L21S 650E | 1 | 12 | 9 |
| L21S 700E | 2 | 6 | 11 |
| L21S 750E | 1 | 13 | 4 |
| L21S 800E | 1 | 53 | 4 |
| L21S 850E | 1 | 2 | 2 |
| L21S 900E | 5 | 4 | 2 |
| L21S 950E | 1 | 2 | 2 |
| L21S 1000E | 2 | 2 | 4 |
| L21S 1050E | 3 | 2 | 2 |
| L21S 1100E | 2 | 2 | 4 |
| L21S 1150E | 17 | 2 | 27 |
| L21S 1200E | 1 | 5 | 3 |
| L21S 1250E | 1 | 4 | 3 |
| L21S 1300E | 4 | 3 | 4 |
| L21S 1350E | 1 | 3 | 4 |
| L21S 1400E | 2 | 26 | 2 |
| L21S 1450E | 3 | 8 | 10 |
| L21S 1500E | 2 | 7 | 2 |
| L21S 1550E | 1 | 12 | 2 |
| L21S 1575E | 3 | 124 | 21 |
| BL 2150E | 1 | 26 | 3 |
| BL 05 | 4 | 6 | 10 |
| BL 50S | 13 | 2 | 5 |
| BL 100S | 6 | 3 | 3 |
| BL 150S | 2 | 3 | 2 |
| BL 200S | 11 | 5 | 5 |
| BL 250S | 3 | 2 | 3 |
| BL 300S | 4 | 2 | 6 |

A & M EXPLORATION PROJECT-421 FILE # 87-6035 Page 12

| SAMPLE# | Au
PPB | Pt
PPB | Pd
PPB |
|-----------|-----------|-----------|-----------|
| BL 850N | 1 | 2 | 2 |
| BL 800N | 1 | 2 | 2 |
| BL 750N | 1 | 2 | 2 |
| BL 700N | 2 | 2 | 2 |
| BL 650N | 3 | 2 | 2 |
| BL 600N | 2 | 2 | 2 |
| BL 550N | 1 | 2 | 2 |
| BL 500N | 1 | 2 | 2 |
| BL 450N | 1 | 2 | 2 |
| BL 400N | 1 | 2 | 25 |
| BL 350N | 1 | 2 | 2 |
| BL 300N | 1 | 5 | 2 |
| BL 250N | 6 | 2 | 3 |
| BL 200N | 1 | 2 | 2 |
| BL 150N | 1 | 2 | 4 |
| BL 100N | 1 | 2 | 2 |
| BL 50N | 1 | 2 | 2 |
| NO NUMBER | 2 | 2 | 3 |

APPENDIX II

Statistics

ROSSBACHER LABORATORY LTD.

STATISTICAL REPORT

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: CU

Sample Type: Soil

| CLASS INTERVAL | CLASS FREQUENCY | RELATIVE FREQUENCY% | CUMULATIVE FREQUENCY% | CLASS MEAN |
|----------------|-----------------|---------------------|-----------------------|------------|
| 0 - 25 | 4 | 1.73 | 1.73 | 17.50 |
| 26 - 50 | 45 | 19.49 | 21.21 | 41.64 |
| 51 - 75 | 49 | 21.21 | 42.42 | 62.92 |
| 76 - 100 | 41 | 17.75 | 60.17 | 86.85 |
| 101 - 125 | 25 | 10.82 | 70.99 | 112.08 |
| 126 - 150 | 27 | 11.69 | 82.68 | 135.59 |
| 151 - 175 | 13 | 5.63 | 88.31 | 162.38 |
| 176 - 200 | 9 | 3.90 | 92.21 | 185.44 |
| 201 - 225 | 2 | 0.87 | 93.08 | 211.00 |
| 226 - 250 | 5 | 2.16 | 95.24 | 236.60 |
| 251 - 275 | 3 | 1.30 | 96.54 | 268.00 |
| 276 - 300 | 0 | 0.00 | 96.54 | 0.00 |
| 301 - 325 | 2 | 0.87 | 97.41 | 318.00 |
| 326 - 350 | 3 | 1.30 | 98.71 | 342.00 |
| 351 - 375 | 0 | 0.00 | 98.71 | 0.00 |
| 376 - 400 | 0 | 0.00 | 98.71 | 0.00 |
| 401 - 425 | 1 | 0.43 | 99.14 | 423.00 |
| 426 - 450 | 0 | 0.00 | 99.14 | 0.00 |
| 451 - 475 | 0 | 0.00 | 99.14 | 0.00 |
| 476 - 500 | 0 | 0.00 | 99.14 | 0.00 |
| 501 - 525 | 0 | 0.00 | 99.14 | 0.00 |
| 526 - 550 | 0 | 0.00 | 99.14 | 0.00 |
| 551 - 575 | 1 | 0.43 | 99.57 | 565.00 |
| 576 - 600 | 1 | 0.43 | 100.00 | 589.00 |

For Statistics

For All Data

| | | |
|----------------------|---------------|---------------|
| Number of Samples: | 231 | 231 |
| Arithmetic Mean : | 105.97 | N.A. |
| Standard Deviation : | 79.23001 | N.A. |
| Minimum Value : | 11 | 11 |
| Maximum Value : | 589 | 589 |
| Range : | 1 -- 9999 PPM | 11 -- 589 PPM |

File(s) used for Statistics:

874678 875600 874492

ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

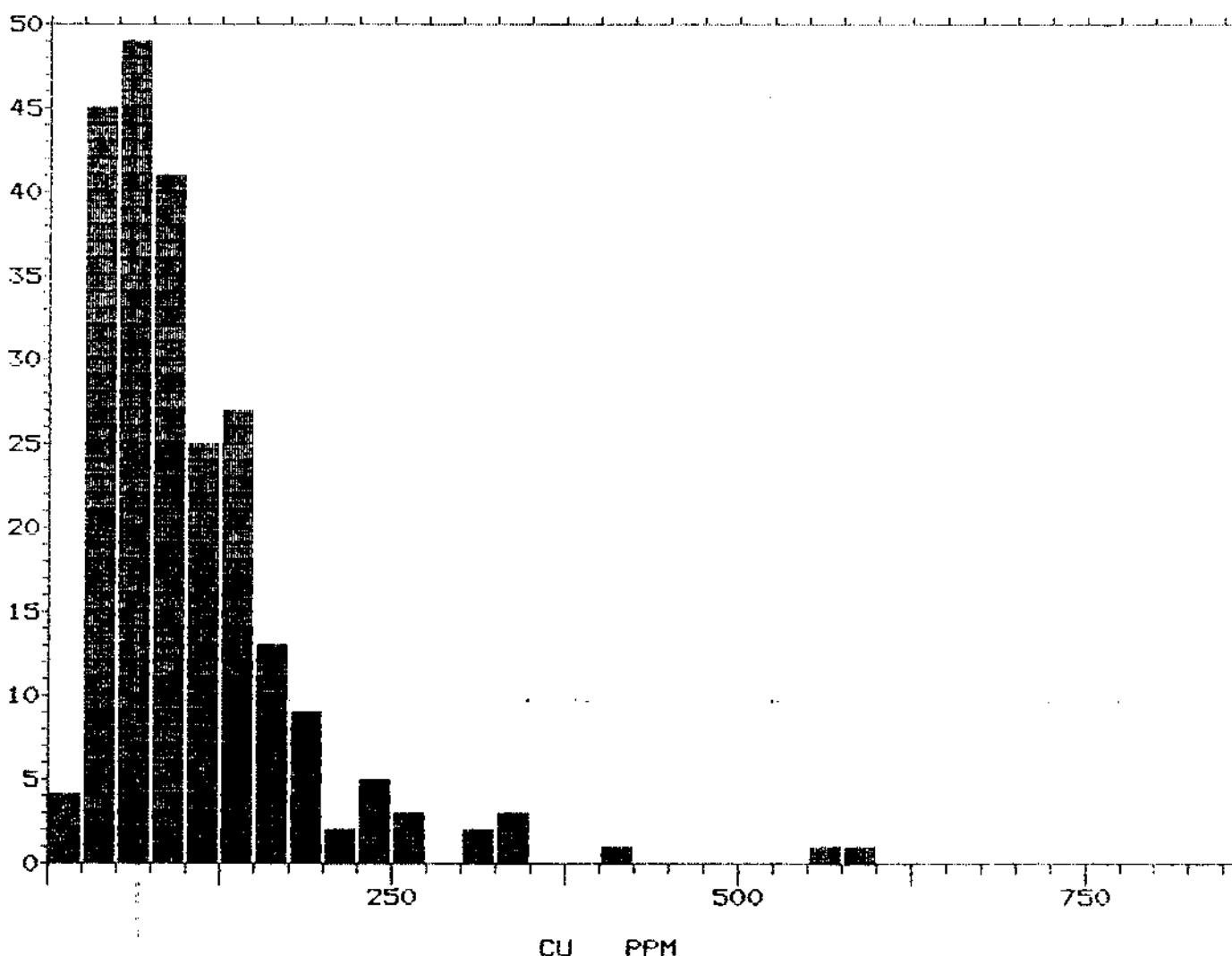
To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: CU

Sample Type: Soil

Frequency Histogram



ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE

BURNABY, B.C. V5B 3N1

TEL : (604) 299 - 6910

STATISTICAL REPORT

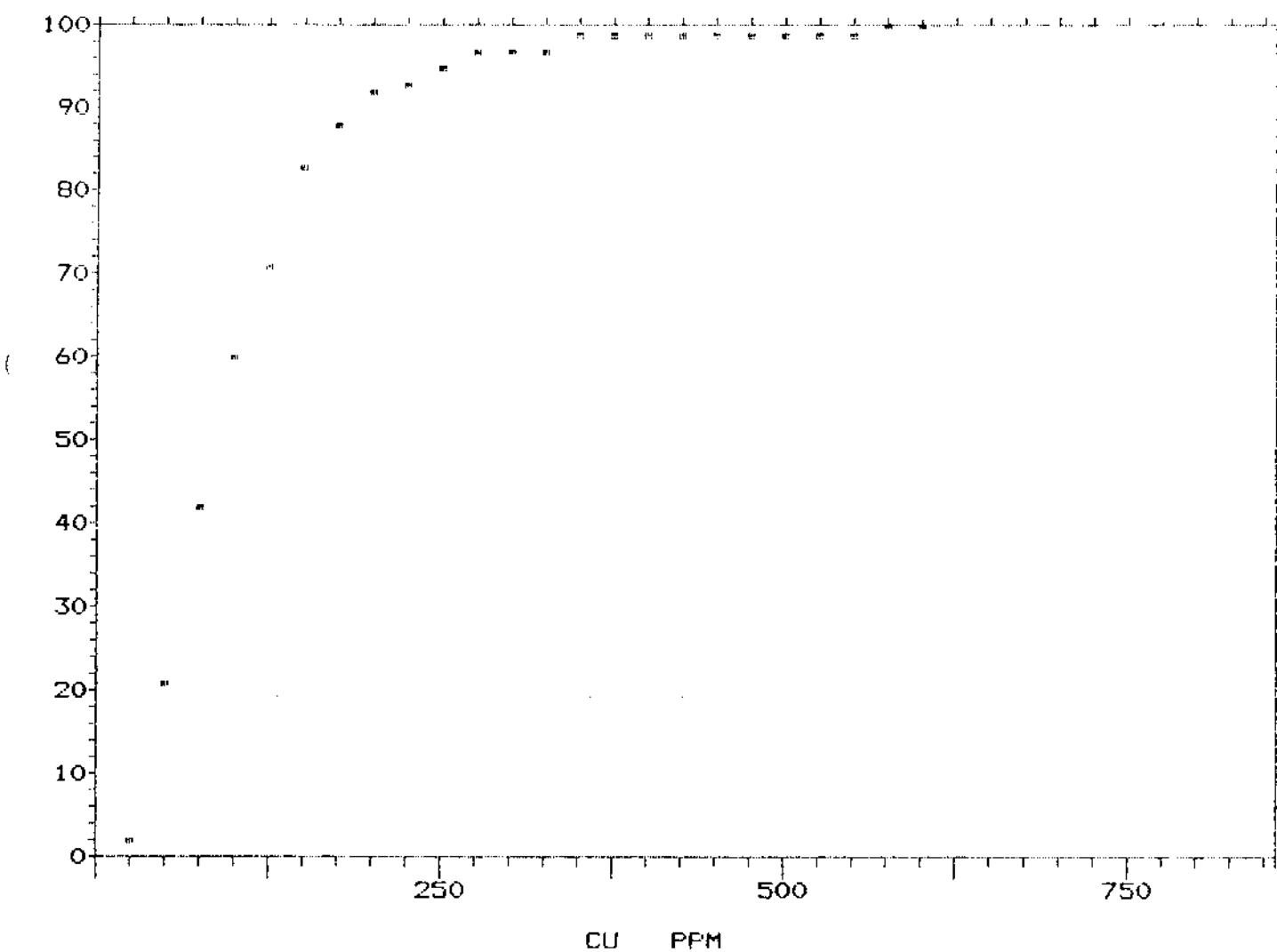
To: A&M EXPLORATION LTD.
214-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: 100E CLAIMS
Date: 09-01-85

Element: CU

Sample Type: Soil

Cumulative Frequency Histogram



ROSSBACHER LABORATORY LTD.**STATISTICAL REPORT**

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: ZN

Sample Type: Soil

| CLASS INTERVAL | CLASS FREQUENCY | RELATIVE FREQUENCY% | CUMULATIVE FREQUENCY% | CLASS MEAN |
|----------------|-----------------|---------------------|-----------------------|------------|
| 0 - 7 | 0 | 0.00 | 0.00 | 0.00 |
| 8 - 14 | 1 | 0.44 | 0.44 | 14.00 |
| 15 - 21 | 0 | 0.00 | 0.44 | 0.00 |
| 22 - 28 | 0 | 0.00 | 0.44 | 0.00 |
| 29 - 35 | 0 | 0.00 | 0.44 | 0.00 |
| 36 - 42 | 0 | 0.00 | 0.44 | 0.00 |
| 43 - 49 | 3 | 1.31 | 1.75 | 46.67 |
| 50 - 56 | 7 | 3.06 | 4.81 | 53.43 |
| 57 - 63 | 9 | 3.93 | 8.74 | 60.67 |
| 64 - 70 | 16 | 6.99 | 15.73 | 66.38 |
| 71 - 77 | 25 | 10.92 | 26.65 | 74.24 |
| 78 - 84 | 22 | 9.61 | 36.26 | 81.18 |
| 85 - 91 | 28 | 12.23 | 48.49 | 88.04 |
| 92 - 98 | 33 | 14.41 | 62.90 | 94.91 |
| 99 - 105 | 27 | 11.79 | 74.69 | 102.11 |
| 106 - 112 | 15 | 6.55 | 81.24 | 109.00 |
| 113 - 119 | 11 | 4.80 | 86.04 | 116.18 |
| 120 - 126 | 9 | 3.93 | 89.97 | 122.56 |
| 127 - 133 | 9 | 3.93 | 93.90 | 129.89 |
| 134 - 140 | 5 | 2.18 | 96.08 | 137.40 |
| 141 - 147 | 2 | 0.87 | 96.95 | 141.50 |
| 148 - 154 | 3 | 1.31 | 98.26 | 151.67 |
| 155 - 161 | 3 | 1.31 | 99.57 | 157.00 |
| 162 - 168 | 1 | 0.44 | 100.00 | 167.00 |

For Statistics**For All Data**

| | | |
|----------------------|--------------|----------------|
| Number of Samples: | 229 | 231 |
| Arithmetic Mean : | 93.36 | N.A. |
| Standard Deviation : | 24.13 | N.A. |
| Minimum Value : | 14 | 11 |
| Maximum Value : | 167 | 2766 |
| Range : | 1 -- 300 PPM | 11 -- 2766 PPM |

File(s) used for Statistics:

874678 875600 874492

ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

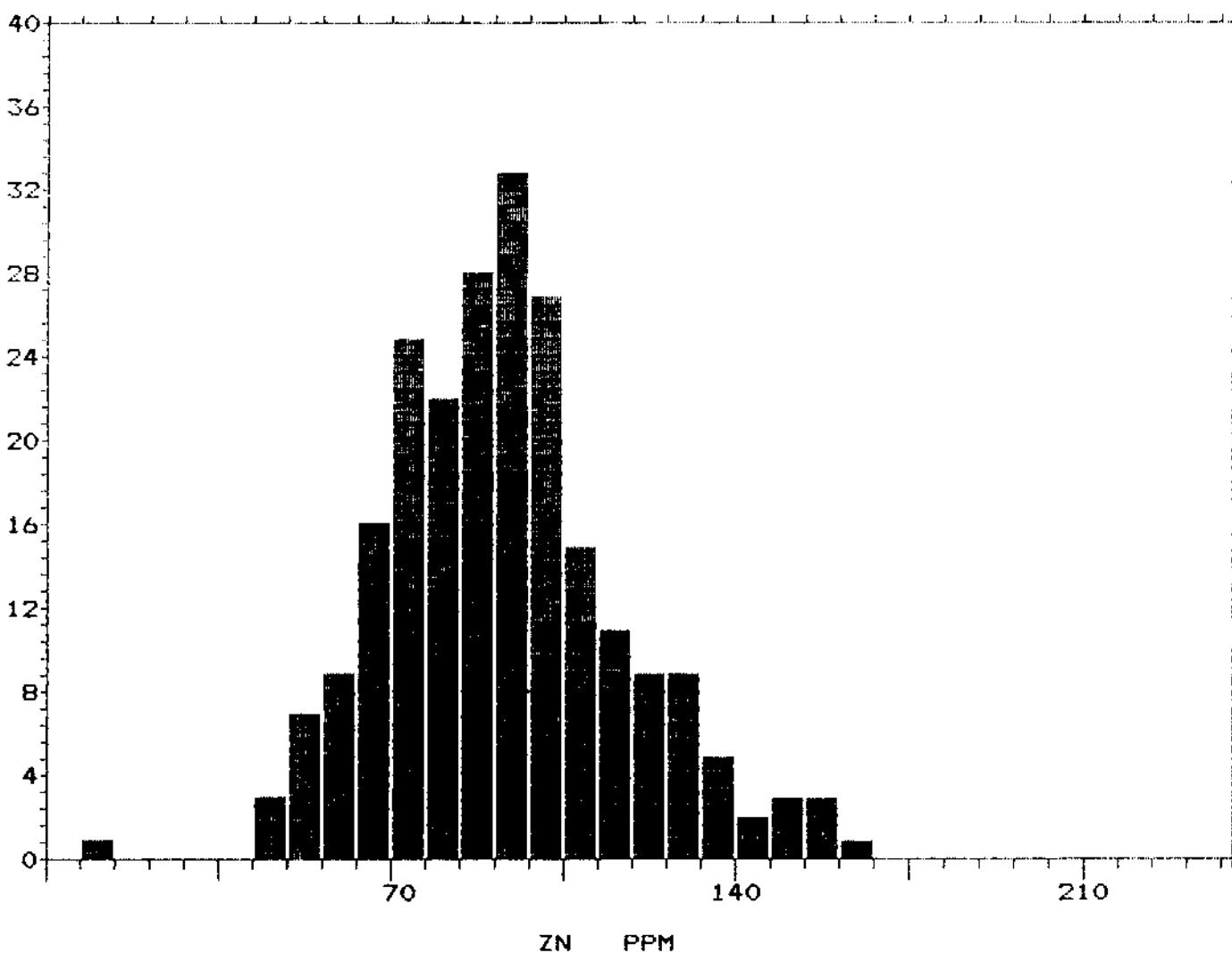
STATISTICAL REPORT

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 07-12-85

Element: ZN

Sample Type: Soil

Frequency Histogram

ROSSBACHER LABORATORY LTD.**STATISTICAL REPORT**

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

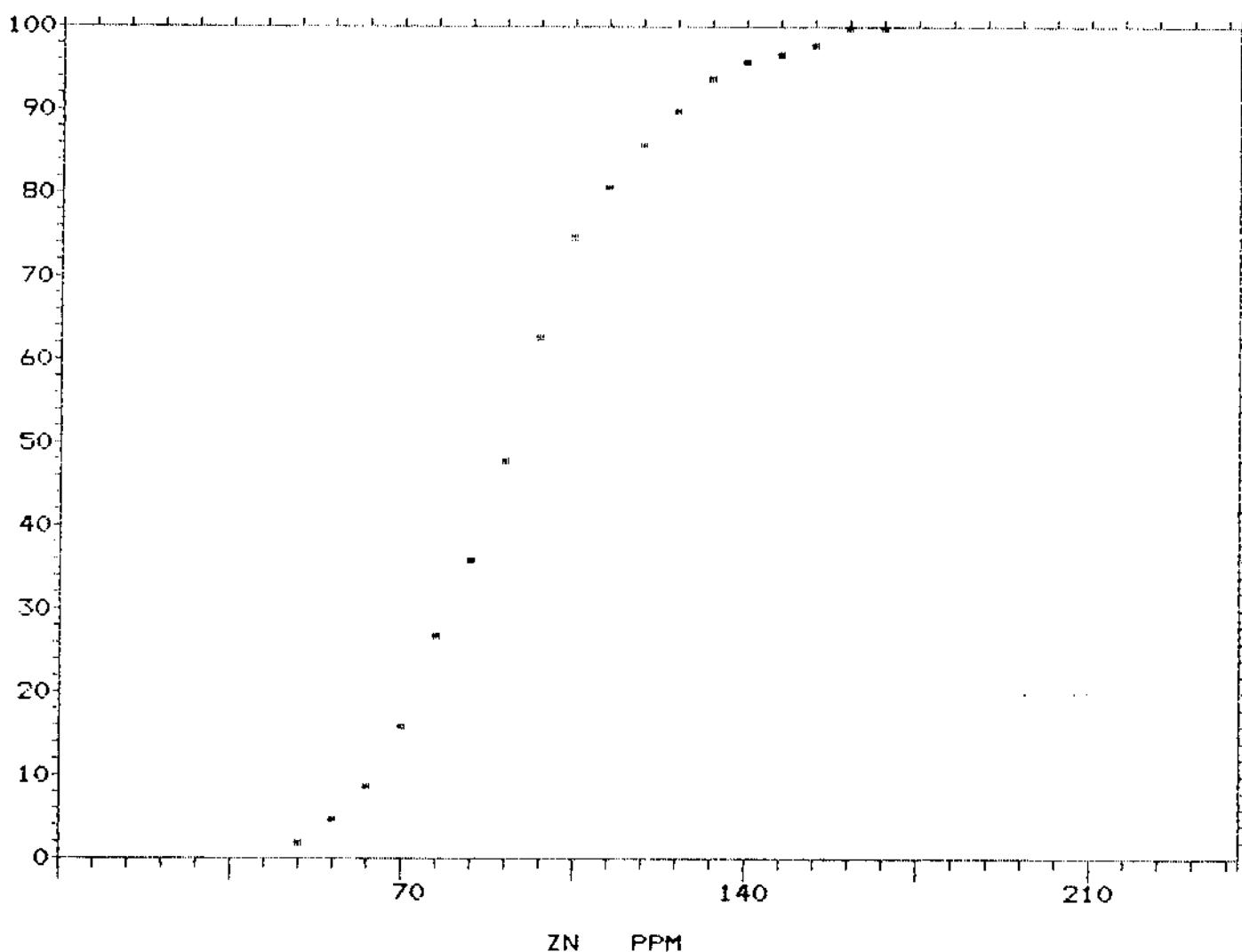
To: A&H EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: ZN

Sample Type: Soil

Cumulative Frequency Histogram



ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: NI

Sample Type: Soil

| CLASS INTERVAL | CLASS FREQUENCY | RELATIVE FREQUENCY% | CUMULATIVE FREQUENCY% | CLASS MEAN |
|----------------|-----------------|---------------------|-----------------------|------------|
| 0 - 4 | 0 | 0.00 | 0.00 | 0.00 |
| 5 - 8 | 4 | 1.73 | 1.73 | 6.50 |
| 9 - 12 | 15 | 6.49 | 8.22 | 10.80 |
| 13 - 16 | 15 | 6.49 | 14.71 | 14.80 |
| 17 - 20 | 34 | 14.72 | 29.43 | 18.91 |
| 21 - 24 | 34 | 14.72 | 44.15 | 22.44 |
| 25 - 28 | 38 | 16.45 | 60.60 | 26.29 |
| 29 - 32 | 19 | 8.23 | 68.83 | 30.53 |
| 33 - 36 | 26 | 11.26 | 80.09 | 34.23 |
| 37 - 40 | 7 | 3.03 | 83.12 | 37.86 |
| 41 - 44 | 14 | 6.06 | 89.18 | 42.43 |
| 45 - 48 | 4 | 1.73 | 90.91 | 46.00 |
| 49 - 52 | 8 | 3.46 | 94.37 | 49.88 |
| 53 - 56 | 3 | 1.30 | 95.67 | 53.67 |
| 57 - 60 | 3 | 1.30 | 96.97 | 58.33 |
| 61 - 64 | 1 | 0.43 | 97.40 | 61.00 |
| 65 - 68 | 1 | 0.43 | 97.83 | 65.00 |
| 69 - 72 | 1 | 0.43 | 98.26 | 70.00 |
| 73 - 76 | 1 | 0.43 | 98.69 | 76.00 |
| 77 - 80 | 1 | 0.43 | 99.12 | 79.00 |
| 81 - 84 | 0 | 0.00 | 99.12 | 0.00 |
| 85 - 88 | 1 | 0.43 | 99.55 | 85.00 |
| 89 - 92 | 1 | 0.43 | 99.98 | 90.00 |
| 93 - 96 | 0 | 0.00 | 100.00 | 0.00 |

For Statistics**For All Data**

| | | |
|----------------------|--------------|-------------|
| Number of Samples: | 231 | 231 |
| Arithmetic Mean : | 28.52 | N.A. |
| Standard Deviation : | 13.82 | N.A. |
| Minimum Value : | 5 | 5 |
| Maximum Value : | 90 | 90 |
| Range : | 1 -- 500 PPM | 5 -- 90 PPM |

File(s) used for Statistics:

874678

875600

874492

ROSSBACHER LABORATORY LTD.**STATISTICAL REPORT**

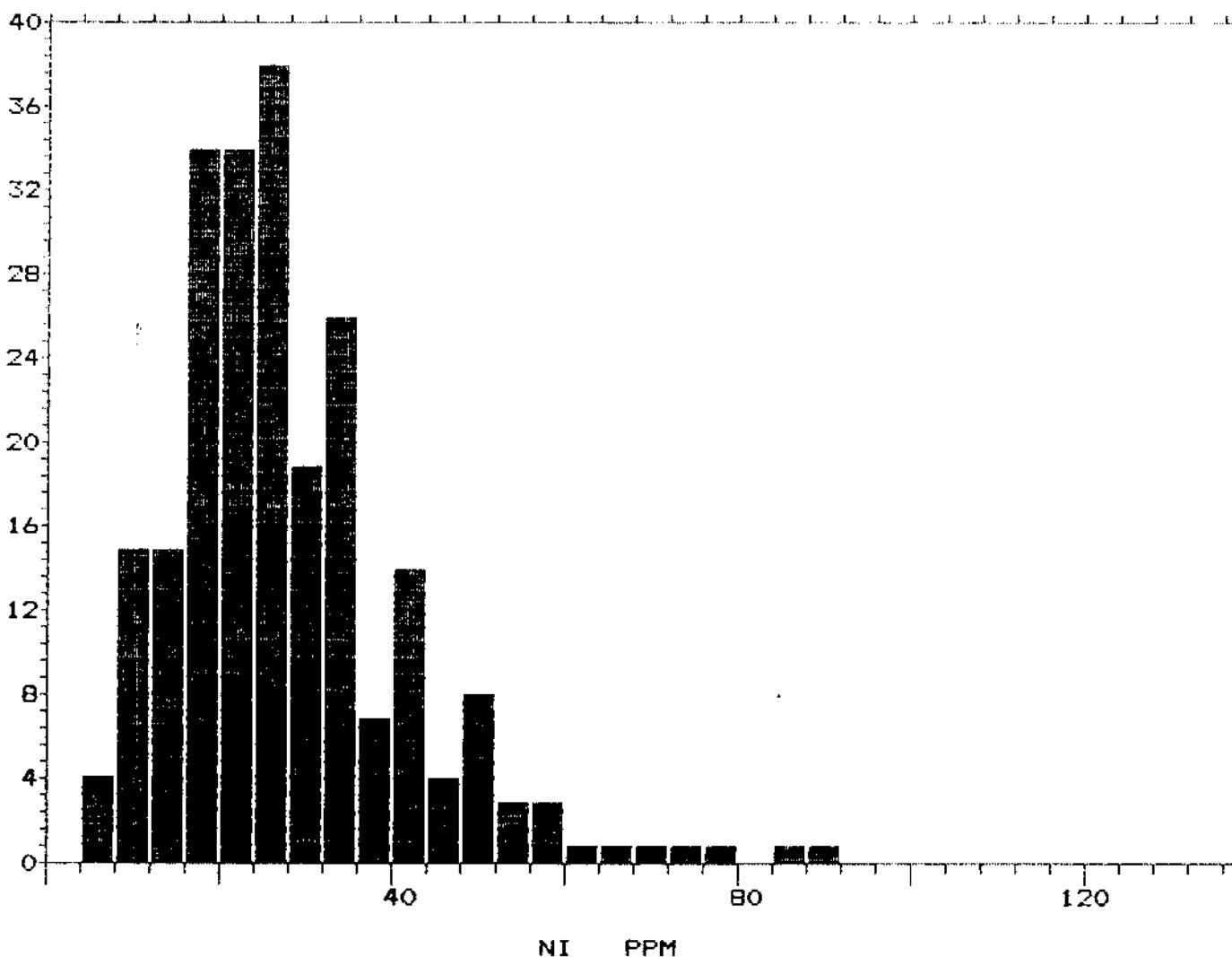
2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-10-05

Element: NI

Sample Type: Soil

Frequency Histogram

POSSBACHER LABORATORY LTD.

STATISTICAL REPORT

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

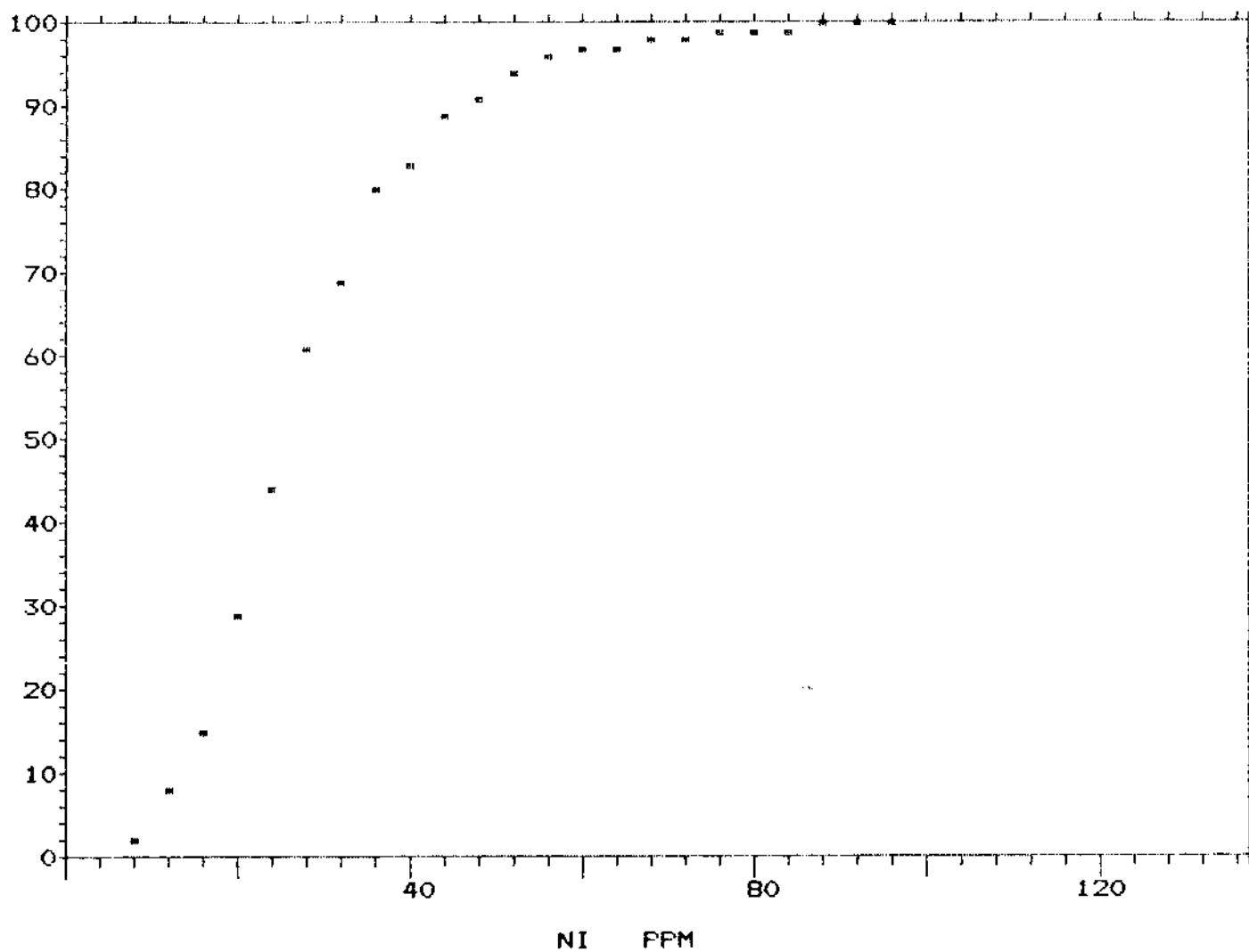
To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-10-06

Element: NI

Sample Type: Soil

Cumulative Frequency Histogram



POSSBACHER LABORATORY LTD.

STATISTICAL REPORT

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: CR

Sample Type: Soil

| CLASS INTERVAL | CLASS FREQUENCY | RELATIVE FREQUENCY% | CUMULATIVE FREQUENCY% | CLASS MEAN |
|----------------|-----------------|---------------------|-----------------------|------------|
| 0 - 8 | 5 | 2.16 | 2.16 | 5.60 |
| 9 - 16 | 13 | 5.63 | 7.79 | 12.38 |
| 17 - 24 | 20 | 8.66 | 16.45 | 20.85 |
| 25 - 32 | 34 | 14.72 | 31.17 | 28.03 |
| 33 - 40 | 43 | 18.61 | 49.78 | 35.95 |
| 41 - 48 | 36 | 15.58 | 65.36 | 44.00 |
| 49 - 56 | 19 | 8.23 | 73.59 | 53.16 |
| 57 - 64 | 15 | 6.49 | 80.08 | 61.67 |
| 65 - 72 | 9 | 3.90 | 83.98 | 68.33 |
| 73 - 80 | 6 | 2.60 | 86.58 | 75.67 |
| 81 - 88 | 10 | 4.33 | 90.91 | 84.10 |
| 89 - 96 | 6 | 2.60 | 93.51 | 92.67 |
| 97 - 104 | 4 | 1.73 | 95.24 | 100.00 |
| 105 - 112 | 2 | 0.87 | 96.11 | 112.00 |
| 113 - 120 | 2 | 0.97 | 96.98 | 115.50 |
| 121 - 128 | 2 | 0.87 | 97.85 | 124.50 |
| 129 - 136 | 1 | 0.43 | 98.28 | 134.00 |
| 137 - 144 | 1 | 0.43 | 98.71 | 139.00 |
| 145 - 152 | 1 | 0.43 | 99.14 | 145.00 |
| 153 - 160 | 0 | 0.00 | 99.14 | 0.00 |
| 161 - 168 | 1 | 0.43 | 99.57 | 162.00 |
| 169 - 176 | 0 | 0.00 | 99.57 | 0.00 |
| 177 - 184 | 1 | 0.43 | 100.00 | 180.00 |
| 185 - 192 | 0 | 0.00 | 100.00 | 0.00 |

For Statistics

For All Data

| | | |
|----------------------|---------------|--------------|
| Number of Samples: | 231 | 231 |
| Arithmetic Mean : | 47.42 | N.A. |
| Standard Deviation : | 29.01 | N.A. |
| Minimum Value : | 1 | 1 |
| Maximum Value : | 180 | 180 |
| Range : | 1 -- 9999 PPM | 1 -- 180 PPM |

File(s) used for Statistics:

874678

875600

874492

ROSSBACHER LABORATORY LTD.**STATISTICAL REPORT**

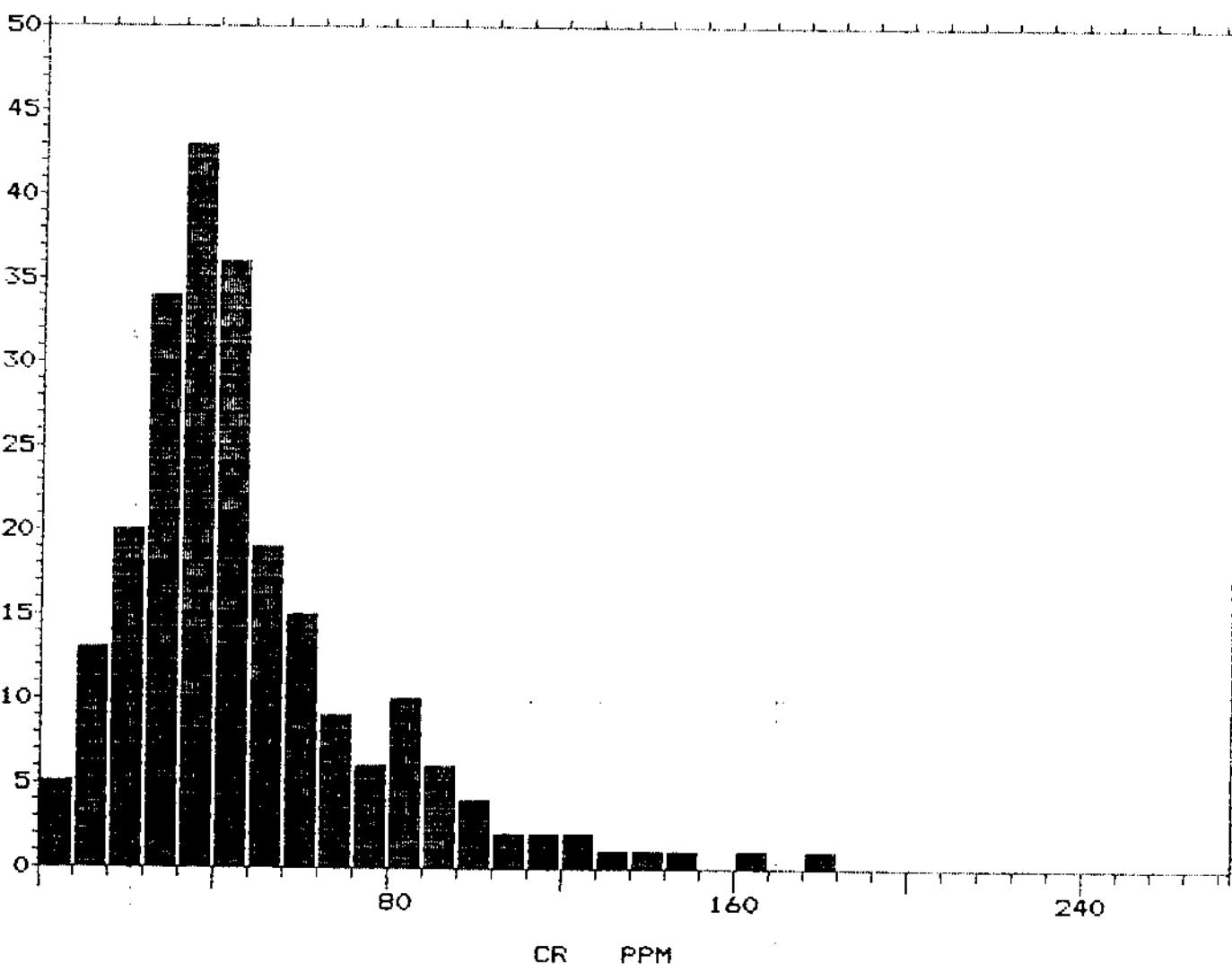
2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

To: A&M EXPLORATION LTD.
714-650 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODGE CLAIMS
Date: 87-12-05

Element: CR

Sample Type: Soil

Frequency Histogram

ROSSBACHER LABORATORY LTD.**STATISTICAL REPORT**

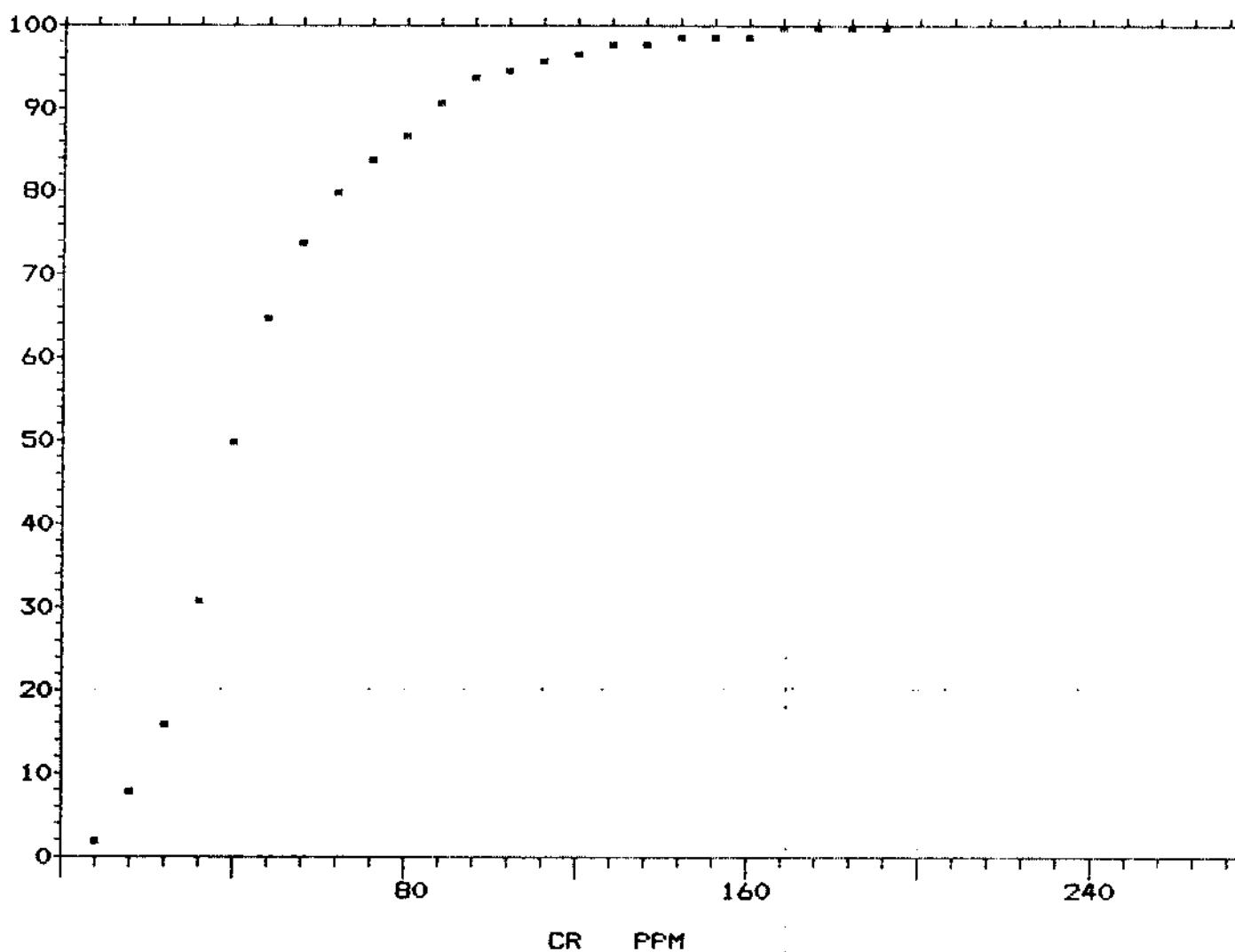
2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: CR

Sample Type: Soil

Cumulative Frequency Histogram

OSSBACHER LABORATORY LTD.

STATISTICAL REPORT

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: Pd

Sample Type: Soil

| CLASS INTERVAL | CLASS FREQUENCY | RELATIVE FREQUENCY% | CUMULATIVE FREQUENCY% | CLASS MEAN |
|----------------|-----------------|---------------------|-----------------------|------------|
| 0 - 3 | 72 | 31.03 | 31.03 | 2.26 |
| 4 - 6 | 59 | 25.43 | 56.46 | 4.97 |
| 7 - 9 | 47 | 20.26 | 76.72 | 7.74 |
| 10 - 12 | 28 | 12.07 | 88.79 | 10.79 |
| 13 - 15 | 14 | 6.03 | 94.82 | 14.36 |
| 16 - 18 | 4 | 1.72 | 96.54 | 16.75 |
| 19 - 21 | 3 | 1.29 | 97.83 | 19.67 |
| 22 - 24 | 1 | 0.43 | 98.26 | 24.00 |
| 25 - 27 | 1 | 0.43 | 98.69 | 26.00 |
| 28 - 30 | 0 | 0.00 | 98.69 | 0.00 |
| 31 - 33 | 2 | 0.86 | 99.55 | 31.00 |
| 34 - 36 | 0 | 0.00 | 99.55 | 0.00 |
| 37 - 39 | 0 | 0.00 | 99.55 | 0.00 |
| 40 - 42 | 0 | 0.00 | 99.55 | 0.00 |
| 43 - 45 | 0 | 0.00 | 99.55 | 0.00 |
| 46 - 48 | 0 | 0.00 | 99.55 | 0.00 |
| 49 - 51 | 0 | 0.00 | 99.55 | 0.00 |
| 52 - 54 | 0 | 0.00 | 99.55 | 0.00 |
| 55 - 57 | 0 | 0.00 | 99.55 | 0.00 |
| 58 - 60 | 0 | 0.00 | 99.55 | 0.00 |
| 61 - 63 | 0 | 0.00 | 99.55 | 0.00 |
| 64 - 66 | 0 | 0.00 | 99.55 | 0.00 |
| 67 - 69 | 1 | 0.43 | 99.98 | 69.00 |
| 70 - 72 | 0 | 0.00 | 100.00 | 0.00 |

For Statistics

For All Data

| | | |
|----------------------|-----------|---------|
| Number of Samples: | 232 | 232 |
| Arithmetic Mean : | 7.03 | N.A. |
| Standard Deviation : | 6.46 | N.A. |
| Minimum Value : | 2 | 2 |
| Maximum Value : | 69 | 69 |
| Range : | 1 -- 1000 | 2 -- 69 |

File(s) used for Statistics:

LODE-PD

874678

875600

874492

ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

(**STATISTICAL REPORT**

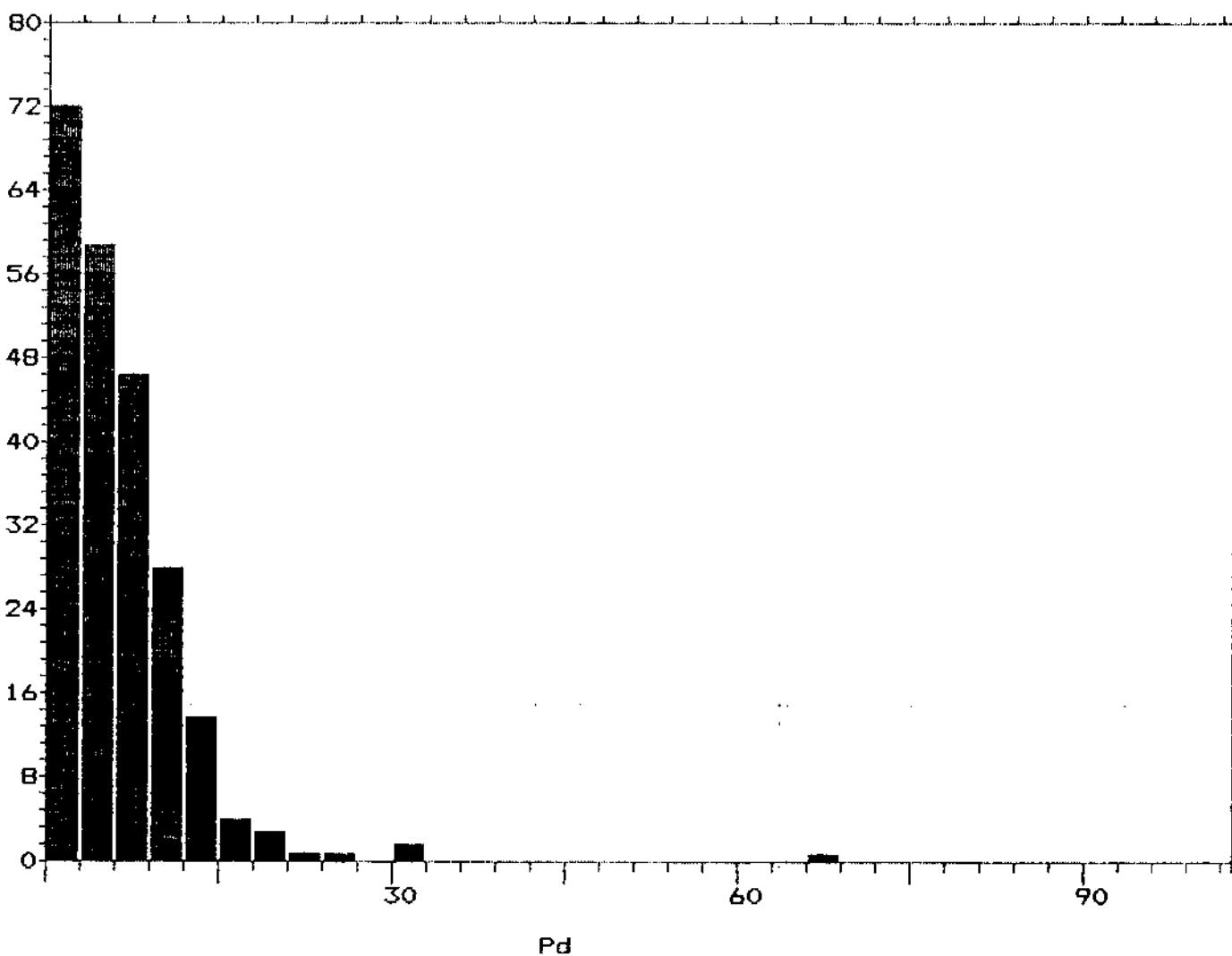
To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: Pd

Sample Type: Soil

Frequency Histogram



ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

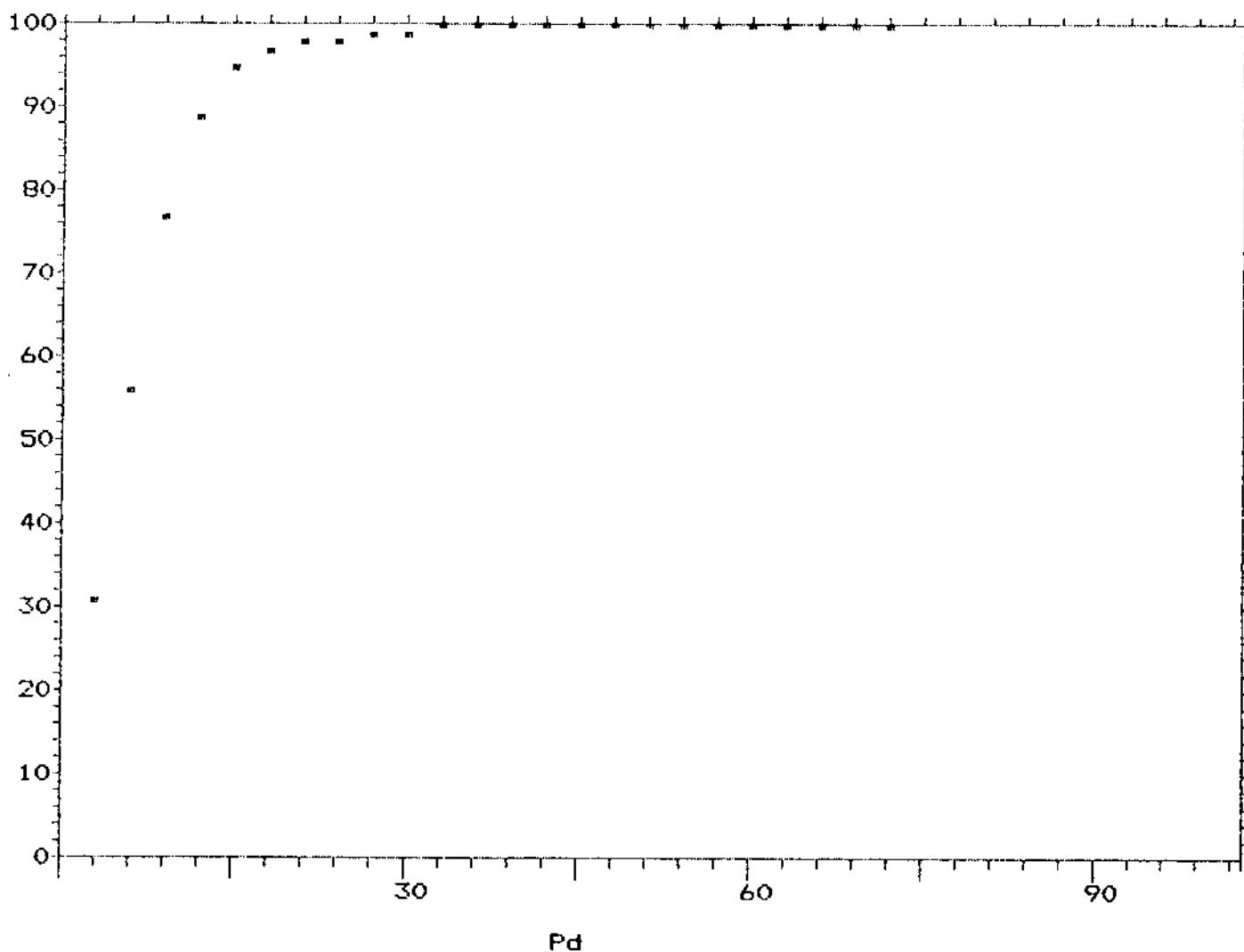
STATISTICAL REPORT

To: A&M EXPLORATION LTD.
714-850 WEST HASTINGS STREET
VANCOUVER, B.C.

Project: LODE CLAIMS
Date: 87-12-05

Element: Pd

Sample Type: Soil

Cumulative Frequency Histogram

APPENDIX III

Affidavit of Expenses

AFFIDAVIT OF EXPENSES

During the period of November 16, 1987 to November 27, 1987 work was performed on the LODE I-IV claims, located in the Similkameen Mining Division in the Tulameen River area of British Columbia.

FIELD

Personnel

| | |
|------------------|----------|
| Don Allen | \$ 1,350 |
| Gary Allen | 900 |
| Geoff Manning | 2,100 |
| Bruce Winterburn | 2,975 |
| Doug Morneau | 3,500 |
| Darwin Carstens | 2,200 |
| Diane Hebditch | 720 |
| Brian Dixie | 720 |
| Alan Foote | 1,080 |
| Gordon Avery | 900 |
| Chris Hopping | 1,260 |
| Andrew Hamilton | 1,200 |
| D. H. | 720 |

Consulting

Airborne Geophysical Survey by
Dighem Surveys and Processing Inc.

28,500

Not in this report

Geochemical Analyses

| | | |
|------|--|-------|
| Soil | 412 samples (Au, Pt, Pd by
fire assay & mass spec.) | 4,120 |
| | 412 samples (30 elem. I.C.P.) | 5070 |

Equipment Rental

| | | |
|--------------|--------------------|-----|
| Magnetometer | 11 days @ \$30/day | 330 |
| VLF-EM Unit | 11 days @ \$15/day | 165 |

Equipment Leasing

265

Field Supplies

1,160

Communication

110

Room & Board

3,530

Transportation

3,075

Stationery/Supplies

50

Subtotal **\$66,000**

AFFIDAVIT OF EXPENSES (Cont'd.)

| | Balance Forward | \$66,000 |
|---------------------|-----------------------|------------------------------|
| REPORT | | |
| Personnel | | |
| Don Allen | 2 days @ \$450/day | 900 |
| Doug Brownlee | 10 days @ \$300/day | 3,000 |
| Drafting | | |
| Draftsmen | 100 hours @ \$20/hour | 2,000 |
| Maps | | 500 |
| Supplies | | 50 |
| Computer Processing | 25 hours @ \$20/hour | 500 |
| Typing/Compilation | | 400 |
| Stationery/Supplies | | 75 |
| | | TOTAL \$73,425 |