Lat. 49° 28'W
Long. 119° 07'W
NTS 82E/6

GEOLOGICAL, GEOCHEMICAL AND GEOPHYSICAL REPORT ON THE LUCKY BOY PROPERTY GREENWOOD MINING DIVISION BEAVERDELL AREA, BRITISH COLUMBIA

for

DRYDEN RESOURCE CORPORATION
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by

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February 29, 1988

SUMMARY

The Lucky Boy property consists of two mineral claims, one-2 post claim and five crown grants, totalling 18 units. The property is situated 3 kilometres northwest of the town of Beaverdell in south central British Columbia.

The claims lie within the historic Beaverdell mining camp. Teck Corporation's Highland Bell mine has been in continuous production since 1900. To date this mine has produced over 45 million ounces of silver. Exploration in the Beaverdell area remains active.

The subject property is underlain by Permian/Triassic metavolcanics and sediments which were intruded by Cretaceous granitic rocks. Mineralized quartz veins have been emplaced along 260 degree fractures within the granitic rocks. This geological environment is favourable for hosting silver-gold-base metal-bearing quartz veins.

Six showings, consisting of adits, trenches and shafts, have been located on the claims. Sampling to date has yielded significant results in silver (1 oz/ton to 11.54 oz/ton) and base metals from the Lucky Boy, Olympic, North and Boundary Showings. Gold assays increased on the southern portion of the claims at the South Showing (.012 oz/ton) and at the Boundary Showing (.200 oz/ton).

Geochemical soil sampling has outlined three anomalous areas. The first area surrounds the North Showing and is open to the north and west. The second area is situated at the Lucky Boy portal and trends to the southwest. The third area is located 100 metres east of the South Showing.

A limited geophysical induced polarization survey has outlined four separate anomalous zones in the Lucky Boy - South Showing area. Two of these zones suggest the Lucky Boy vein may continue along strike to the east.

A second and third-phase exploration program has been recommended. Phase II will consist of geological mapping, rock sampling, soil sampling, biogeochemical sampling, backhoe trenching and induced polarization geophysics at an estimated cost of $91,000. Phase III would be contingent upon favourable results from Phase II and would consist of backhoe trenching and diamond drilling at an estimated cost of $131,000.

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1. INTRODUCTION

This report was prepared at the request of Dryden Resource Corporation to describe and evaluate the results of geological, geochemical and geophysical surveys completed by Ashworth Explorations Limited on the Lucky Boy Claim Group, Beaverdell area, B.C.. The surveys were carried out February 9 - 29, 1988. The report also describes the regional geology, area history and previous work from both published and unpublished reports.

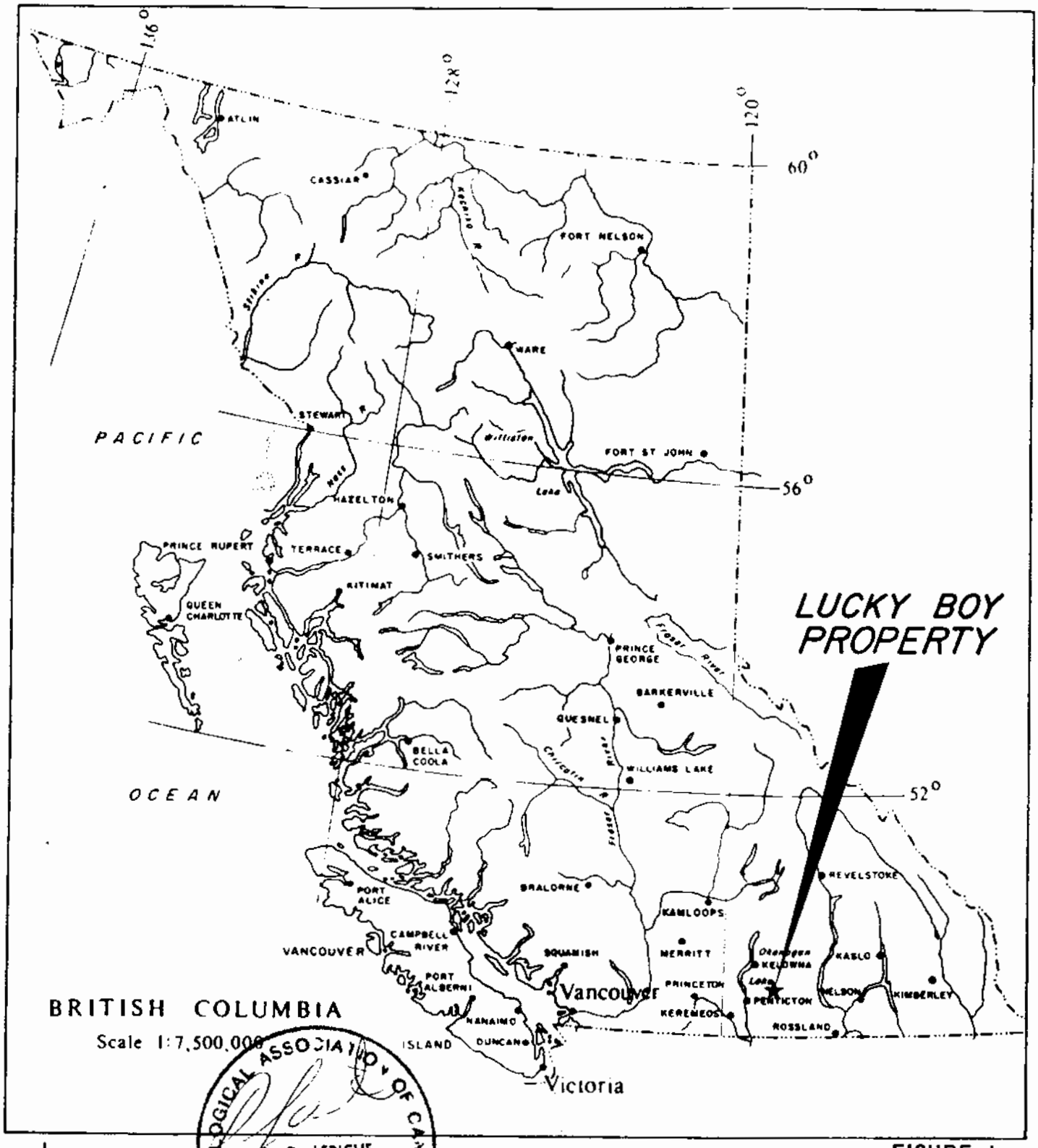
The main purpose of the project was to evaluate the known showings and area for economic silver-gold mineralization within epithermal-type quartz veins.

2. LOCATION, ACCESS AND TOPOGRAPHY

The centre of the property is approximately 3 kilometres northwest of the town of Beaverdell, B.C., and 36 kilometres east-southeast of Penticton, B.C.. It is located on the east side of Cranberry Ridge, and west of the West Kettle River and Kettle Valley railway line. The claims lie within the Greenwood Mining Division on NTS mapsheet 82E/6. The approximate coordinates are latitude 49° 28' North and longitude 119°07' West(see Figures 1, 2 and 3).

Access to the property is by a gravel road northwest from Beaverdell. The road leads north up the Kettle Valley railway line (abandoned) for 3.0 kilometres to the subject property. From there a dirt road leads west and switchbacks through the crown grants. Four wheel drive vehicles are recommended.

The subject claims lie on a moderate grade, east-dipping slope between Cranberry Ridge and the West Kettle River. Elevations range from 792 metres (2600 feet)



GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
— FELLOW —

FIGURE 1

DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

GENERAL LOCATION MAP

Scale: 1: 7,500,000	By: F.Y. Drn: G.T.
Date: February, 1988	NTS 82E6

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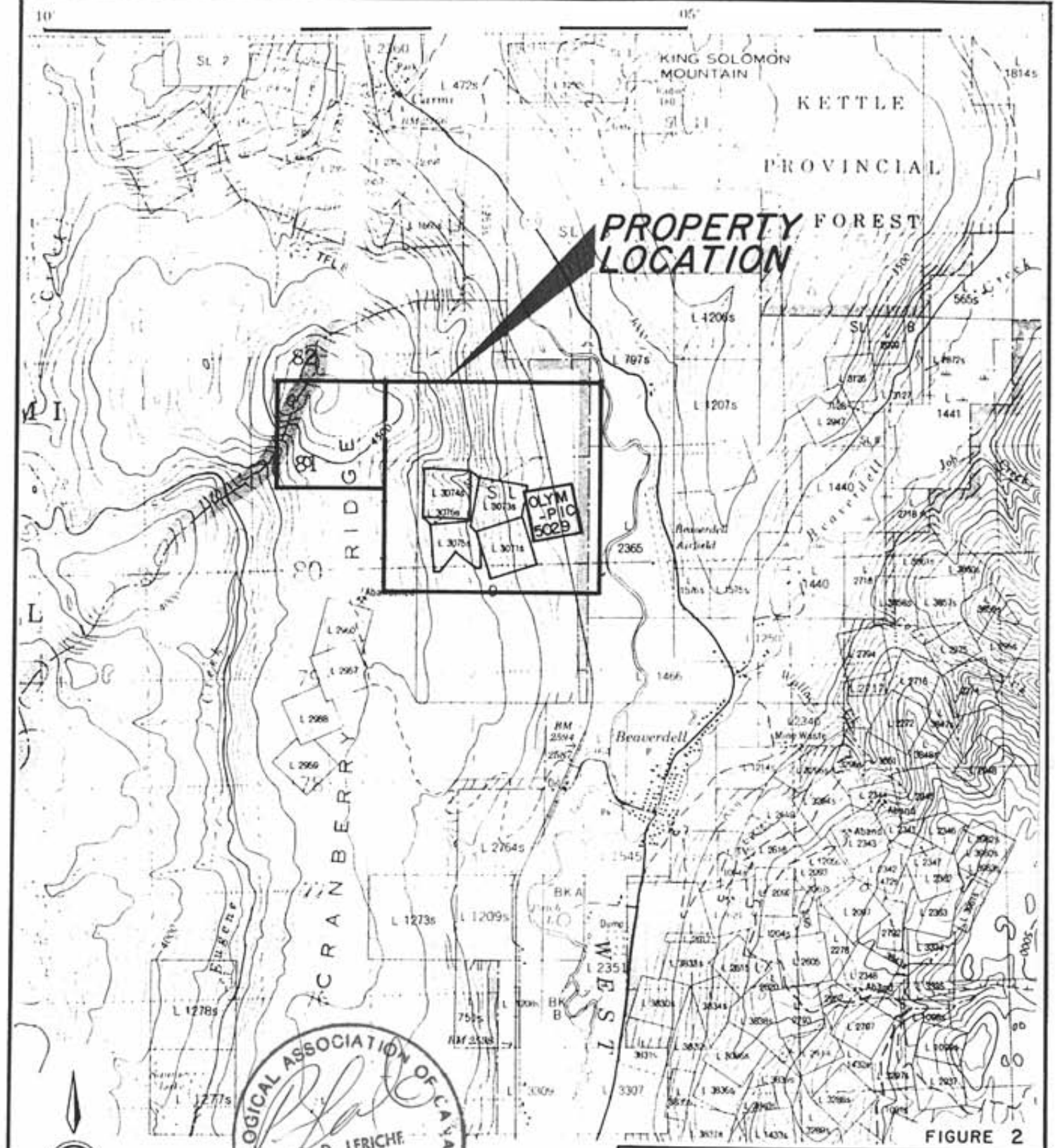

FIGURE 2

DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

TOPOGRAPHIC MAP

Scale:	By: F.Y. Drn: G.T.
Date: February, 1988	NTS 82E6

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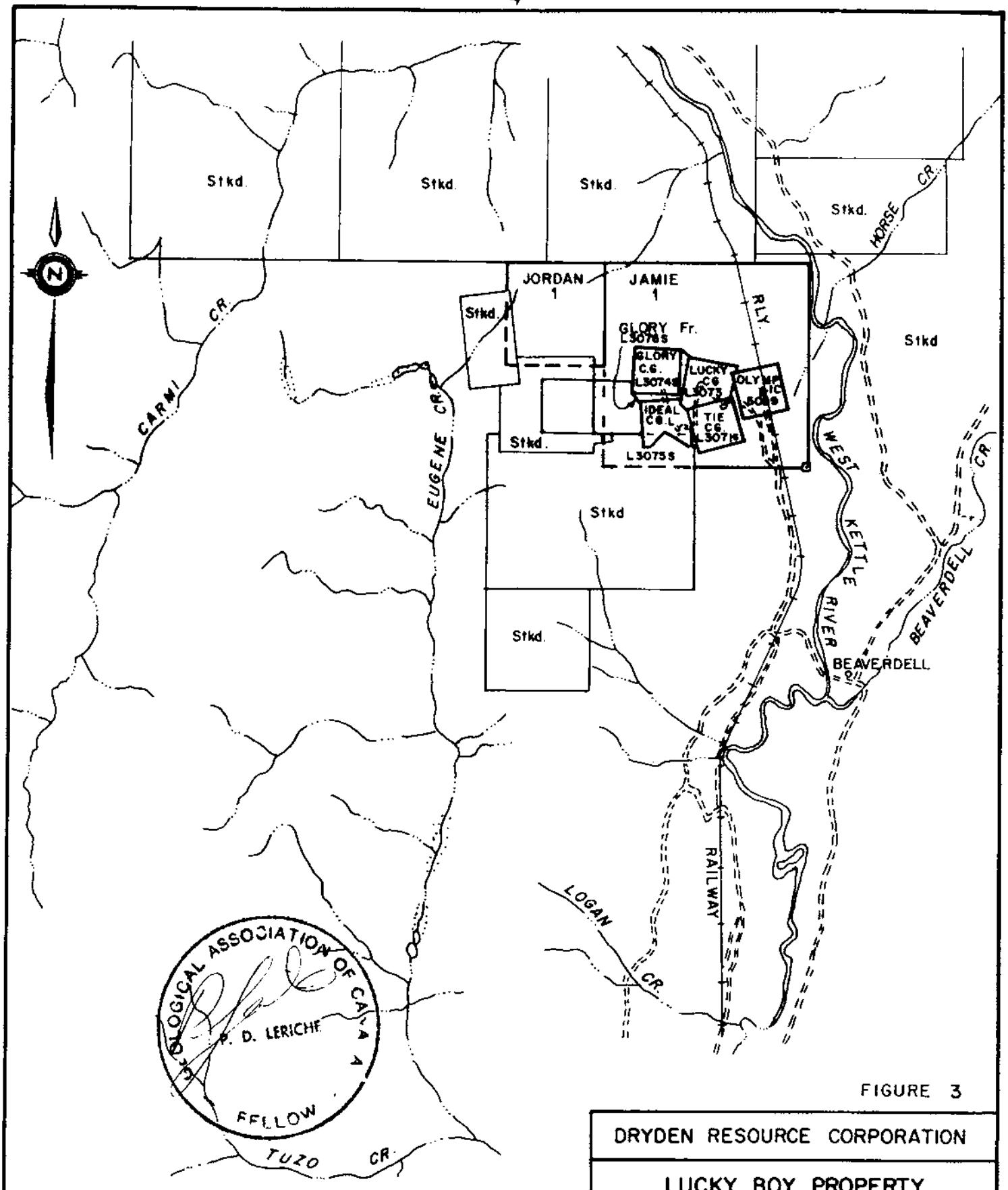

GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
FELLOW

FIGURE 3

DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

CLAIM MAP

Scale: 1:50,000	By: F.Y.	Drn: G.T.
Date: February, 1988	NTS 82E6	

Ashworth Explorations Limited

at the West Kettle River to 1463 metres (4800 feet) on Cranberry Ridge, giving a total relief of 671 metres (2200 feet). Vegetation consists mainly of Douglas fir and Ponderosa pine with minor underbrush.

3. PROPERTY STATUS

The Lucky Boy Claim Group consists of two mineral claims totalling 20 units, one 2-post claim, and five crown grants (see Figure 3). The total area, correcting for overlap, is approximately 18 units or 450 hectares(1111 acres).

Pertinent claim data is given below:

NAME	RECORD/ LOT #	UNITS	EXPIRY DATE	OWNER
Jamie I	Pending	16	Mar. 7/89	Dryden Resource Corporation
Jordan I	Pending	4	Mar. 7/89	" " "
Olympic	5029	1	Oct.19/88	Ellsworth Dickson
Lucky Boy C.G.	L3073S	1	"	Rene Doyharcabal
Glory C.G.	L3074S	1	"	" "
Ideal C.G.	L3075S	1	"	" "
Tie C.G.	L3071S	1	"	" "
Glory Fraction C.G.	L3076S	Fr.	"	" "

An option agreement, signed February 5, 1988, entitles Dryden Resource Corporation to a 60% interest in the crown grants and Olympic 2-post claim by expending $100,000. by February 29, 1988. Dryden can earn a further 20% interest by expending $100,000. by June 30, 1988. Further details of the agreement are beyond the scope of this report.

4. AREA HISTORY

Mining history in the Beaverdell area has centred around the Highland Bell (Beaverdell) mine, located on the west side of Mount Wallace, 4 kilometres

southeast of the subject claims. The following section on history, geology, mineralization and structure of the Highland Bell mine is taken from Christopher, 1975(pp. G30 - G33).

> HISTORY: Records indicate that prospecting and exploration in the Beaverdell mine area was in progress in the year 1889. Production of silver has been continuous since 1913, with intermittent production between 1900 and 1913.
>
> Several companies commenced production when the Kettle Valley Railway reached the village of Beaverdell in 1913. In 1936, the Bell and Highland Lass mines amalgamated to form the Highland Bell mine which in 1938 obtained control of the Beaver mine. In 1946 Leitch Gold Mines, Limited obtained control of Highland Bell, Limited, and the Sally mine property. In 1950 a 50-ton-per-day mill was constructed and the first concentrate shipments were made. Discovery of the faulted extension of the Lass vein system(Lower Lass) in 1954 led to the expansion of the mill capacity to the present rate of 108 tonnes per day.
>
> In 1970 Teck Corporation Ltd. acquired the Highland Bell mine and conducted an extensive exploration program with limited success. Faulted segments of known vein systems were outlined but no significant new reserves were located. At present the mining operation consists of reworking old stopes to recover remnants of low-grade sections.
>
> Production from the Beaverdell mine area since 1900 has totalled about 32 million ounces of silver, 24 million pounds of lead, 28 million pounds of zinc, with minor production of gold, cadmium, and copper. Gold values appear to increase in the eastern part of the Lower Lass mine but further exploration is required to outline an economic gold-silver part of the deposit. Complex faulting makes estimation of proven ore reserves tenuous and with the present day economics, the main requirement for continued production depends on maintaining mill heads above about 10 ounces of silver per ton.
>
> GEOLOGICAL SETTING: Detailed geology of the Highland Bell mine property has been reported by Reineck(1915), White(1949), Kidd and Perry(1957), and Verzosa and Goetting(1972). The mine area is mainly underlain by the Westkettle batholith(Nelson) and Beaverdell stock(Valhalla)? with contained pendants of Paleozoic or Early Mesozoic metamorphosed rocks of the Wallace Formation(Anarchist Group). Hypabyssal rocks occur in east-west and northeast fracture zones that are also occupied by the mineralized vein systems.

Vein systems of the Beaverdell mine occur mainly within quartz diorite or granodiorite of the Westkettle batholith. Five separate vein systems are situated in a 3-kilometre, northeast-trending, complexly faulted zone on the west slope of Mount Wallace. At the eastern end of the mineralized zone, the Westkettle batholith is overlain by metamorphosed sedimentary and volcanic rocks of the Wallace Formation while at the western end of the mineralized zone, porphyritic quartz monzonite(Beaverdell stock) has intruded the Westkettle batholith. Pre-mineral andesitic dykes(Wellington type) and syn or post-mineral quartz latite dykes(Idaho type) are spatially and temporally related to mineralization, often occupying the same structural zone.
Veins are essentially mineralized fissures that formed along either easterly or northeasterly trending faults. Mainly easterly trending veins occur in the western part of the mineralized zone(Wellington, Sally, and Rob Roy vein systems) while in the eastern part of the mineralized zone(Upper and Lower Lass systems), veins trend northeasterly. The Bell system in the central part of the mineralized zone has both easterly and northeasterly trending veins. Except for the mineralized 'black breccia'(probably a carbonaceous fault brecciated vein) mineralized lodes persist for only short distances into the Wallace Formation. The proximity of the Wallace Formation to mineral occurrences throughout the area suggests that the Wallace rocks acted as a dam to mineralizing solutions.

MINERALIZATION: Sulphide mineralization consists mainly of pyrite, galena, and sphalerite with lesser chalcopyrite, pyrrhotite, arsenopyrite, polybasite, argentite, and native silver(see Staples and Warren, 1946). Quartz, calcite, and rare fluorite are the main gangue minerals. Veins generally have a propylitic alteration halo that may be recognizable up to 10 metres from the main vein and may carry low-grade silver values.

Zoning is suggested by a change in the silver and gold content of the veins in the Lass system. Gold values increase and silver values decrease in the eastern part of the Lower Lass mine. Chalcopyrite and pyrrhotite are found in the Wellington and in the eastern part of the Lower Lass but are not generally found in other parts of the mine. Pyrargyrite is especially common in the Bell and Lass mines(Verzosa and Goetting, 1972).

STRUCTURAL SETTING: Faulting dominates the structural pattern at the Beaverdell mine and predicates mining and exploration procedures. Vein systems appear to have been continuous features that have been disrupted by at least five main fault systems(White, 1949; Kidd and Perry, 1954)

> including northerly striking, steeply east-dipping normal faults(Terminal faults) and northeasterly striking, moderately west-dipping normal faults causing the main disruptions.
>
> The East Terminal fault has been shown to have displaced the Lass vein by 210 metres(Kidd and Perry, 1954) but the extent of movement on the West Terminal fault has not been determined.

Production continues at the Highland Bell mine at a present rate of 120 tons per day with grades of approximately 10 ounces of silver per ton. Forty-five million ounces of silver have been produced since 1900. Lead and zinc continue to be recovered with grades of 1% each (Northern Miner Magazine, May, 1987).

The Inyo-Ackworth property (now the W1 and W2 claims) lies immediately to the west of the Glory crown grant, Glory fraction claim and Ideal crown grant of the Lucky Boy Claim Group. Work began around 1924, continuing sporadically to the present day. Early open-cuts, shallow shafts and trenches indicating gold and silver mineralization in quartz veins were sampled but grades were insufficient for economic recovery of metals. Two shallow shafts, with cross-cuts, are present on this property. The most recent shaft was sunk in 1924-1925 by the Dollar Mining Company. At depth, the predominant quartz vein varied from two inches to two feet in width over a 45 foot length. The main sulphides present are pyrite with occasional segregations of galena and silver. A sample of the pyrite assayed 0.30 oz/ton Au and 1.6 oz/ton Ag, and a sorted lead ore sample assayed 0.10 oz/ton Au, 8 oz/ton Ag and 22% Pb. A 14 ton shipment was made to the Trail smelter towards the end of 1925 (B.C.M.M., 1925).

Additional work in the '60's, '70's and '80's, completed by various companies and individuals, consisted of additional trenching, limited diamond drilling, surface mapping, VLF-EM survey and biogeochemical sampling. Indications show a general northeast-southwest trend on the property. This is observed in most of the old workings on the property which reveal a vertical shear zone striking N80E for 300 metres. A less well defined shear is also present which is subparallel to the main shear and lies 150 to 250 metres northwest of the main shear. Assays range from .021 oz/ton Au and 0.30 oz/ton Ag to .120 oz/ton Au and 3.46 oz/ton Ag in dump material samples with 5% to 10% pyrite, 5% galena and 3% to 5% sphalerite (Morrison, 1979).

The Nipper claims experienced work previous to, and around 1925, and were indicated to lie northwest of the Inyo-Ackworth property. It is difficult to locate these claims with respect to the Lucky Boy Claim Group. They were possibly located west of the current Jordan 1 claim. Various open-cuts, tunnels and shallow shafts indicated quartz veins striking northeast-southwest with Au, Ag and Pb-Zn mineralization present, as shown by two assays: 0.20 oz/ton Au, 26 oz/ton Ag, 32% Pb and .50 oz/ton Au, 3 oz/ton Ag, 0.5% Pb, 5% Zn(B.C.M.M., 1925).

A property which saw more recent work was the Arn Claim Group. It surrounded both the old Inyo-Ackworth property(present W1 and W2 claims) and the Lucky Boy claims to the west. A few soil geochemistry anomalies of Cu, Pb, Zn, Ag and Au were found in 1981. A VLF-EM survey, carried out in 1983 on the John claims(now the Jordan 1 and Jamie 1 claims) north of the Lucky Boy

and W1-W2 claims, located conductors on the southwest corner of the claims(Kregosky, 1981, 1983).

The Fran property(Deer Group), was located approximately 200 metres southwest from the southwest corner of the Jamie 1 claim of the Lucky Boy Claim Group. It was the subject of mapping, a rock chip sampling survey and a soil sampling survey done over VLF conductors. The soil sampling survey indicated a Ag-Cu anomaly located towards the Highland Bell mine. The VLF survey found east-west trends paralleling the vein system at the Highland Bell mine. The VLF trends also coincided with some of the soil survey's anomalous values.

IGF Metals Inc. has worked on its property on Wallace Mountain, located immediately to the south of the Highland Bell mine. Geochemical and rock chip surveys were followed by three diamond drill holes. Indications of a fault zone were good and two of the holes intersected a vein structure. Assays of the two intersections for Ag were 71.9 oz/ton over 1.06 feet and 39.3 oz/ton over 1.69 feet (Vancouver Stockwatch, February 11, 1988). Due to the encouraging results, a diamond drilling and trenching programme is indicated for the 1988 season.

5. PREVIOUS WORK

As with the other properties in the Cranberry Ridge area, exploration work dating back to the early 1900's has taken place. The presence of trenches, open-cuts, shallow shafts and short tunnels was reported in the B.C. Minister of Mines Annual Report of 1925. Four veins trending east-west were outlined in the exposures. A vein width of approximately six feet was reported on the Lucky Boy claim, with mineralization present in veinlets and segregations on the

hanging wall side of the vein. Mineralization was predominantly pyrite, galena, sphalerite, chalcopyrite, gold and silver in quartz. One sorted ore sample assayed trace Au, 141 oz/ton Ag and 5.3% Cu(B.C.M.M., 1925).

In August 1986, Mr. Clive Ashworth and Mr. Hugo Laanela, FGAC, of Ashworth Explorations Limited, visited the area. They were unable to locate the old Lucky Boy workings but found an adit and dump on the Olympic 2-post claim. Three samples were taken: two from the shear zone in the adit(one over a 12 inch width, the other over a 28 inch width) and one from the old dump. The 12 inch shear zone sample assayed 34.2 ppm Ag and trace Au.

In July 1987, Mr. E. E. Dickson located the Lucky Boy workings by following the strike of the shear zone westward from the Olympic adit. The workings were found near the boundary of the Lucky Boy and Glory crown grants. An adjacent dump containing mineralized rocks was sampled with the highest assay producing 6.92 oz/ton Ag (Dickson, 1987). Due to dangerous conditions, the adit could not be sampled but the shear zone was noted to contain visible mineralization.

6. REGIONAL GEOLOGY (FIGURE 4)

The basement (Precambrian?) unit, the Monashee Group, occurs in one location to the northwest of Cranberry Ridge. This unit is mainly paragneiss with minor schist, amphibolite, quartzite, marble and pegmatite. The next oldest unit in the area is the Anarchist Group, of Permian and/or Triassic age. It consists of greenstone, quartzite, graywacke, limestone and local paragneiss. The Anarchist Group was intruded by the Nelson Plutonic rocks (Cretaceous?). The intrusions

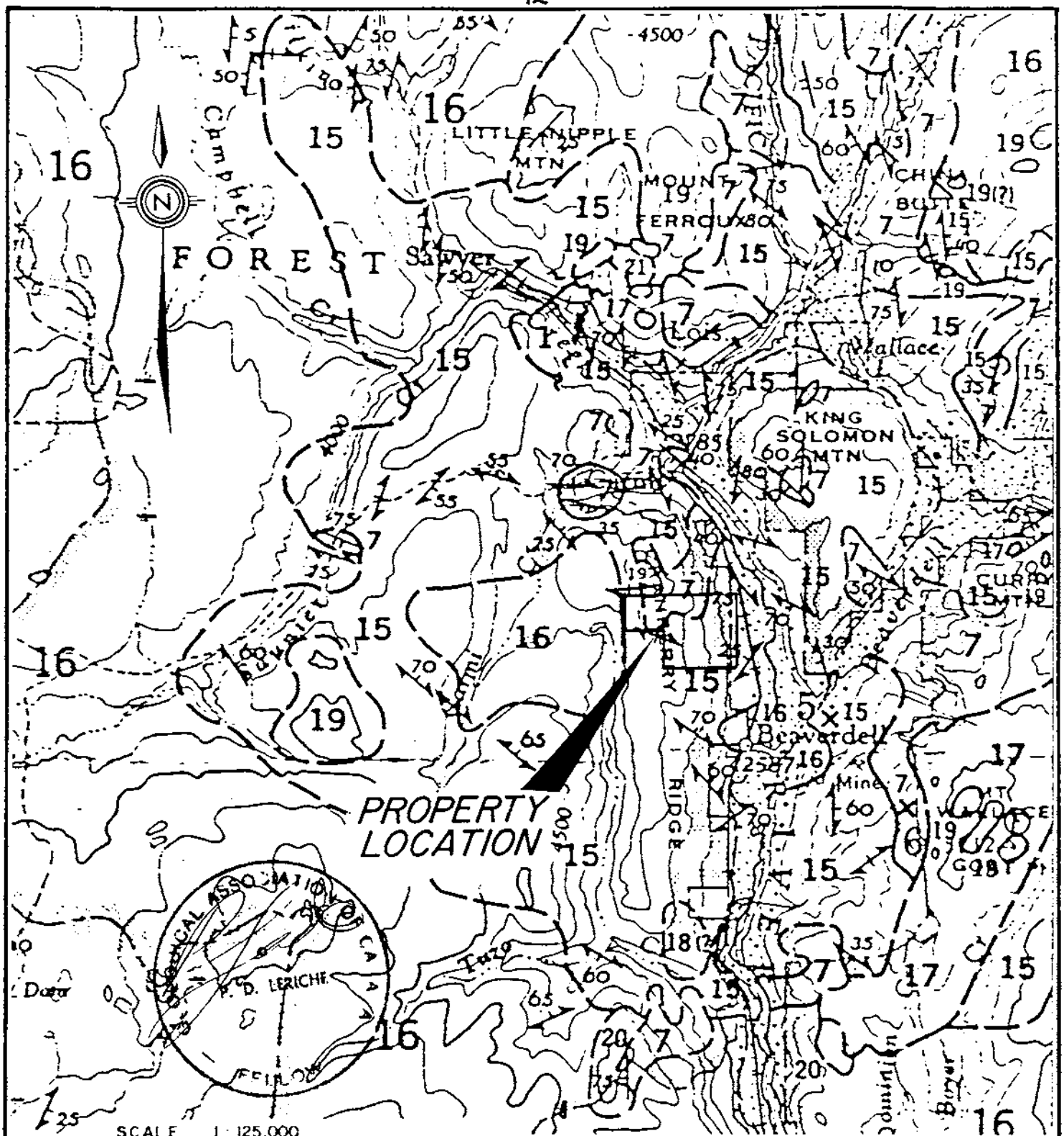

FIGURE 4

LEGEND

Geological boundary (defined, approximate)

Bedding (horizontal, inclined)

Bedding, tops unknown (inclined, vertical)

Gneissosity (inclined, vertical)

Schistosity (inclined, vertical)

Fault (defined, approximate, assumed)

Geology by H. W. Little, 1958 and 1959

DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

REGIONAL GEOLOGY

Scale: 1: 125,000	By: F.Y. Drn: G.T.
Date: February, 1988	NTS 82E6

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LEGEND

CENOZOIC

TERTIARY

MIOCENE (?)

21 — Basalt; minor olivine basalt

OLIGOCENE (?)

20 — CORYELL PLUTONIC ROCKS: syenite, granite; minor monzonite and shonkinite

EOCENE OR OLIGOCENE

19 — Andesite, trachyte, minor basalt; locally, interbedded tuff and shale; 19a, andesite and trachyte flows and agglomerate; 19b, conglomerate, sandstone, shale, tuff; minor agglomerate and breccia; coal; 19c, andesite and trachyte; 19d, agglomerate and conglomerate

PALEOCENE OR EOCENE

18 — Porphyritic granite and rhyolite

17 — Conglomerate, sandstone, shale, tuff

MESOZOIC

CRETACEOUS (?)

16 — VALHALLA PLUTONIC ROCKS: granite, granodiorite

15 — NELSON PLUTONIC ROCKS: granodiorite, quartz diorite, diorite; granite, quartz monzonite, syenite, monzonite

JURASSIC (?)

14 — 14a, pyroxenite; 14b, hornblendite; 14c, serpentinite

TRIASSIC OR JURASSIC

13 — Limestone

TRIASSIC

UPPER TRIASSIC

NICOLA GROUP

12 — Greenstone, tuff, quartzite, limestone, argillite, and schist

TRIASSIC OR EARLIER

8–11 — 8. BARSLOW FORMATION: argillite
9. INDEPENDENCE FORMATION: chert, greenstone
10. SHOEMAKER FORMATION: chert, some tuff and greenstone
11. OLD TOM FORMATION: greenstone, minor diorite

PERMIAN AND/OR TRIASSIC

ANARCHIST GROUP

7 — Greenstone, quartzite, greywacke, limestone; locally paragneiss

PALAEOZOIC

PERMIAN AND (?) PENNSYLVANIAN

5,6 — 5. CACHE CREEK GROUP: greenstone, quartzite, argillite, limest
6. BLIND CREEK FORMATION: limestone; limy argillite

CARBONIFEROUS (?)

KOBAU GROUP

4 — Quartzite, schist, greenstone

PRECAMBRIAN OR LATER

PRE-PERMIAN

3 — OLD DAVE INTRUSIONS: serpentinized ultrabasic rocks

CHAPPERON GROUP

2 — Chlorite schist, quartzite

MONASHEE GROUP

1 — Layered gneiss (paragneiss); minor schist, amphibolite, quartzite, marble, and pegmatite

range from granodiorite to quartz diorite, diorite, granite, quartz monzonite, syenite and monzonite. A final intrusive phase of this area is represented by the Valhalla Plutonic Rocks (Cretaceous), granite to granodiorite in composition. The Nelson and Valhalla units are distinguished solely on a lithologic basis.

The above units are overlain by the Curry Creek Formation (Paleocene or Eocene?) consisting of conglomerate, sandstone, shale and tuff. Possibly contemporaneous with these sediments is a unit of porphyritic granite to rhyolite, located on the southeast edge of Cranberry Ridge.

The next youngest formation is the Midway Volcanic Group of Eocene/Oligocene age. It is composed of andesite, trachyte, minor basalt and locally interbedded tuff and shale.

The Coryell Plutonic rocks (Oligocene?) are the youngest in the area and are sparsely represented in the area of Cranberry Ridge. The Coryell unit mainly consists of syenite and granite (Little, 1958-1959).

7. 1988 PROGRAM

7.1 SCOPE AND PURPOSE

During February 1988 a field crew consisting of two geologists, two geophysicists, and seven geotechnicans completed geological mapping, rock sampling, trenching, soil geochemical sampling plus magnetometer - VLF-EM-induced polarization geophysics over the Lucky Boy claim area.

The purpose of this program was twofold:

a) To find, map and systematically sample the showings on the property to evaluate their economic potential.

b) To locate mineralized structures along strike from the known showings or find parallel structures.

7.2 METHODS AND PROCEDURES

A grid was laid out and used as a control for all surveys (Map 1). A baseline was cut at azimuth 260° for 1.5 kilometres. Cross-lines were surveyed using compass, hipchain and flagging at 100 metre line spacings and 50 metre station spacings. Four additional cross-lines were added to provide more detailed coverage over the main Lucky Boy showings. Total line surveyed, including baseline, tie-lines, and cross-lines, was 31.5 kilometres.

Geological mapping was performed at a scale of 1:5000 over the property and at 1:200 over the showings. A total of 87 rock samples were collected and analyzed for gold and silver (fire assay) plus multi-element ICP by Vangeochem Lab Limited. See Appendix C for analytical techniques.

Five rock samples from host rock and vein structures were sent to Vancouver Petrographics Ltd. for thin section analysis. Appendix D is a complete report on each section and Map 2 shows their locations.

A Case 1450B bulldozer was used to plow and rehabilitate the property access road, and to dig three trenches. Grid coordinates were used for location control.

The grid was soil sampled at 50 metre station spacings, except the area around the Lucky Boy workings where a 25 metre spacing was used. The total number of soil samples taken was 525. Twelve additional soil samples were obtained from trenches to test the soil profiles. All soil samples were taken with a grub hoe from the B horizon (approximate depth of 25 cm), placed into marked Kraft-paper bags, field dried and sent to Vangeochem Lab, North Vancouver, B.C.. Samples were analyzed for gold (aqua regia) and multi-element ICP. Refer to Appendix C for description of analytical techniques.

The lab results for seven elements (Au, Ag, Cu, Pb, Zn, As, Ni) were computer-plotted on 1:5000 scale maps (Maps 9 to 15). To evaluate any existing geochemical anomalies, frequency distribution histograms based on lab data were prepared for each of the aforementioned elements. Anomalous values were chosen using natural breaks in each histogram. For interpretation purposes, correlation coefficients were calculated (Table 1) and anomalous ranges for each element were plotted using symbol maps (Figures 5 to 11). All statistical and plotting work was performed by Tony Clark Consulting Services.

An E.D.A. Omni Plus system was used to simultaneously measure total field magnetics data and VLF-EM data from the Seattle (24.8 KHz) transmitter. Parameters measured were total magnetic field strength, VLF-EM field strength, in-phase dip angle and quadrature (see Appendix F for Equipment Specifications).

The VLF-EM in-phase and quadrature results were corrected to have the operator facing north. There were no other calculations made to the VLF-EM data. Total field magnetic data was corrected for diurnal variation by the

internal programming of the Omni IV base station. The Omni IV program interpolates a base-station reading corresponding to the time of each field reading and corrects the field reading to a chosen datum value.

VLF-EM and magnetic values are presented in table form in Appendix F. A VLF-EM in-phase and quadrature profile map, VLF-EM total field profile map, magnetic contour map and VLF-magnetometer interpretation map (Maps 16 to 19) were plotted at a scale of 1:5000 by Interpretex Resources Inc..

Pacific Geophysical Limited was retained to perform an induced polarization and resistivity survey. A Phoenix IPV-1 IP and resistivity unit, together with a Phoenix Model IPT-1 IP and resistivity transmitter unit, was used to record the measurements. IP effects were recorded as Percent Frequency Effect (PFE) at operating frequencies of 4.0 Hz and 0.25 Hz, while apparent resistivity values were normalized in ohm-meters. Dipole-dipole array was employed exclusively using a basic inter-electrode distance of 25 metres in every case. A portion of Line 500N was also completed using 12.5 metre electrode intervals. Four dipole separations were measured in every case.

The interpreted IP results are illustrated on Map 20, a 1:2500 scale plan map of the Lucky Boy IP and resistivity grid, which also shows the contoured n=1 PFE readings. Map 21 is a 1:2500 scale plan map of the contoured n=1 apparent resistivity values.

8. RESULTS

8.1 GEOLOGICAL MAPPING & ROCK GEOCHEMISTRY

The following sections are based on geological mapping and rock sampling by the author and Mr. Fayz Yacoub, field geologist.

Geological mapping was inhibited by approximately 30 cm of snow cover. The focus of attention therefore was on mapping and sampling the old workings on the property.

8.1.1 Property Geology and Mineralization (Map 2)

The regional geology map (Figure 4) shows the subject claims to be underlain by Nelson plutonic rocks (Cretaceous) in contact with metasediments and metavolcanics of the Anarchist Group (Permian/Triassic). Limited mapping to date has located only the plutonic rocks. These rocks are medium-grained, granodiorite to quartz monzonite in composition, consisiting of 20 - 25% quartz, 40 - 45% plagioclase, 20 - 25% K-feldspar and 10% combined hornblende-biotite. Thin section samples P-1 and P-3 are representative of the property host rock and are described in Appendix D.

Mineralization on the property is related to four parallel shear zones which trend at 250° to 260°. The shear zones have been injected with quartz, mineralized with pyrite, chalcopyrite, galena and sphalerite.

8.1.2 Old Showings

Six showings which contain physical workings (trenches, pits, adits, shafts) were located on the claims and have been called the (1) Lucky Boy, (2) Rat, (3)

Olympic, (4) South, (5) North and (6) Boundary showings. The following is a description of each showing:

1) Lucky Boy Showing(Maps 5 and 6, Plates 2, 3, 4 and 5)

This is the main showing on the property. It consists of one adit (25 metres long), driven at 260 degrees, and numerous open cuts and trenches.

The main quartz vein was traced for 20 metres within the adit. The vein pinches and swells from 20 cm to 150 cm, strikes at 260 to 265 degrees and dips at 60 degrees to the south. The vein pinched out completely to the west near the face of the adit. Sulphide minerals (pyrite, chalcopyrite, sphalerite, minor galena) are disseminated within the quartz vein and the hanging wall. Thin section P-5 was taken from the Lucky Boy shear zone. Minerals observed in thin section include: 67% quartz, 25% sericite, trace chlorite, 2% barite, trace carbonate, 4% sphalerite, 2% pyrite, trace chalcopyrite and trace Pb-As sulphosalt (?).

Altogether 22 rock samples were taken across the vein and wallrock for a length of 20 metres with an average width of 51.4 cm. Silver values averaged 1.32 oz/ton, with a high assay of 3.90 oz/ton. Base metal values averaged 1763 ppm Cu, 714 ppm Pb, and 5213 ppm Zn.

Other significant results outside the Lucky Boy adit are summarized as follows:

Sample #	Description	Assays
R-76	Across 150 cm quartz vein outcrop, 10 metres north of Lucky Boy portal.	5.14 oz/ton Ag 1031 ppm Bi 1768 ppm Pb
R-77	Ore dump. Quartz with pyrite, galena, malachite staining.	11.54 oz/ton Ag 11790 ppm Cu 16221 ppm Pb 6424 ppm Zn 1078 ppm Bi
R-78	Ore dump. Quartz with disseminated pyrite, chalcopyrite, sphalerite, minor galena and malachite.	0.96 oz/ton Ag 8269 ppm Cu 23227 ppm Zn
R-79	Ore dump. Rusty quartz with pyrite and chalcopyrite.	2.80 oz/ton Ag 6534 ppm Cu 8584 ppm Zn
R-80	Ore dump. Quartz material with disseminated pyrite, chalcopyrite.	1.57 oz/ton Ag 5634 ppm Cu 9590 ppm Zn

Sampling of other outcrops or old trenches in the area was not possible due to snow conditions.

2) The Rat Showing (Maps 7 & 8)

This showing is located at 7+17W 0+96S. It consists of a trench, a small open cut and an adit which continues for 28.5 metres at 260 degrees.

Granodiorite is the host for a series of small shears, locally infilled with calcite. Two rock samples were taken from two of the shears. The results were not significant.

3) The Olympic Showing (Maps 7 & 8, Plates 6, 7 and 8)

Located at 4+75W and 0+25S, this showing consists of one vertical shaft

PLATE 1: Typical Granodiorite-Quartz Monzonite Host Rock on Lucky Boy Property.

PLATE 2: Lucky Boy Portal.

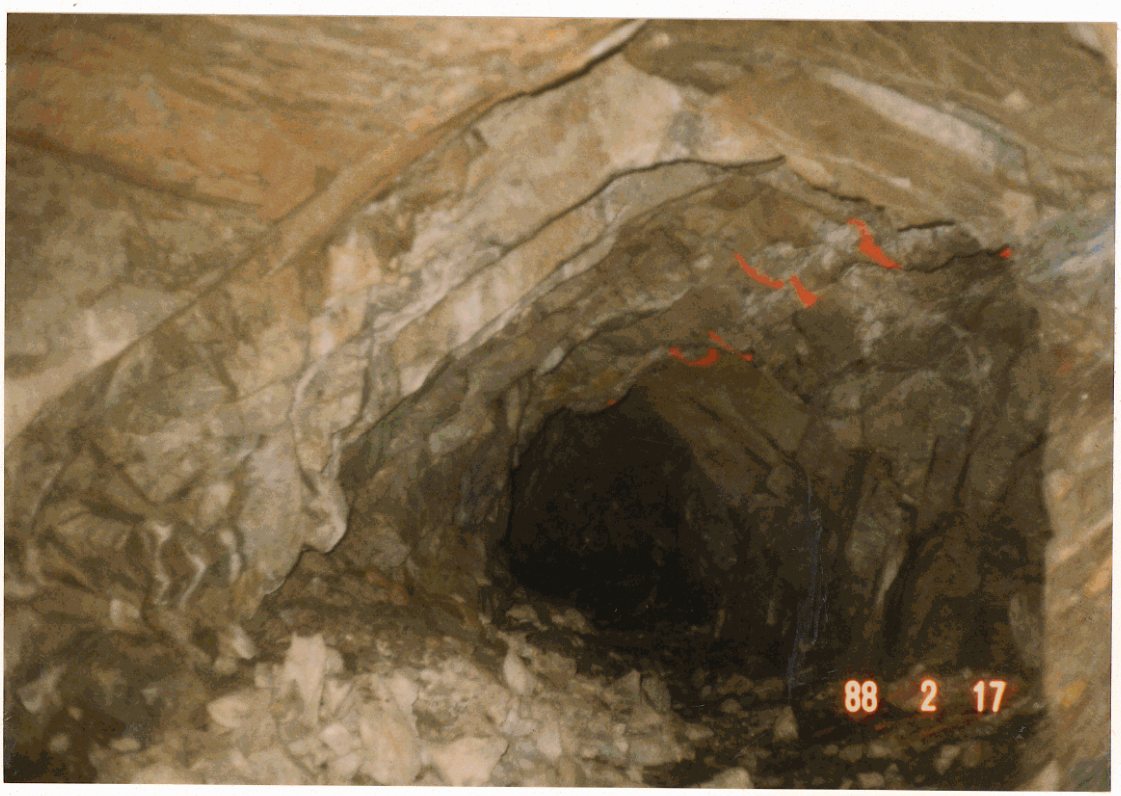


PLATE 3: Lucky Boy Adit. Note quartz vein along orange paint markings.

PLATE 4: Quartz Vein, 1.0 metres wide outside Lucky Boy Adit.

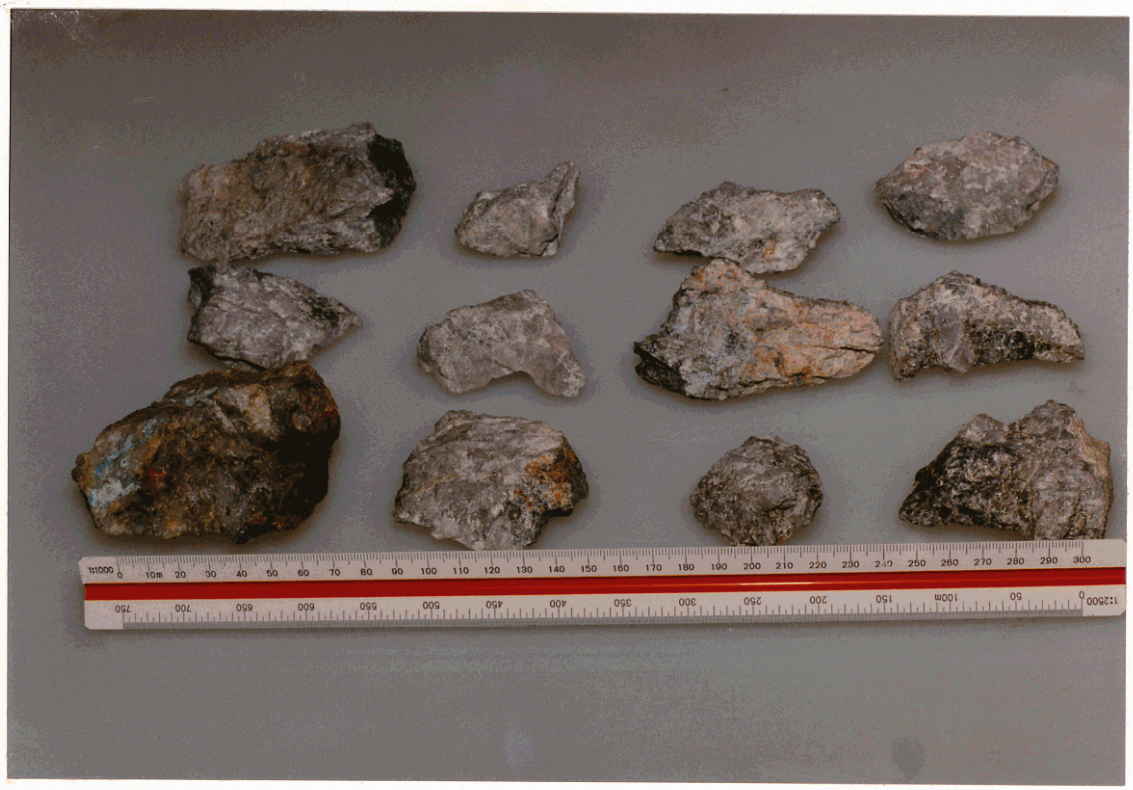


PLATE 5: Quartz Vein Specimens from Lucky Boy Vein.

PLATE 6: Olympic Portal.

PLATE 7: Olympic Shaft.

PLATE 8: Channel Samples in Olympic Adit.

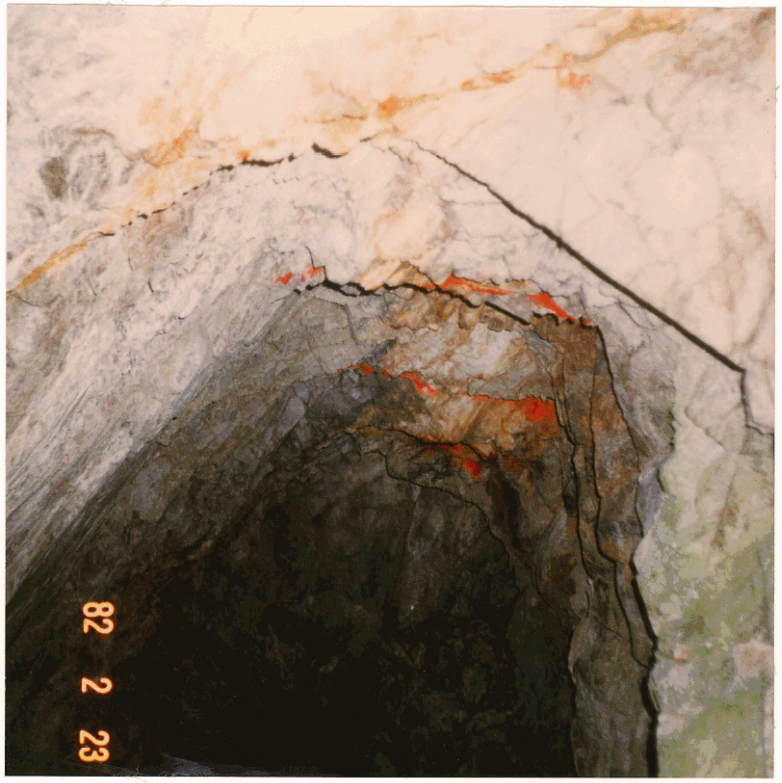


PLATE 9: North Showing Adit.

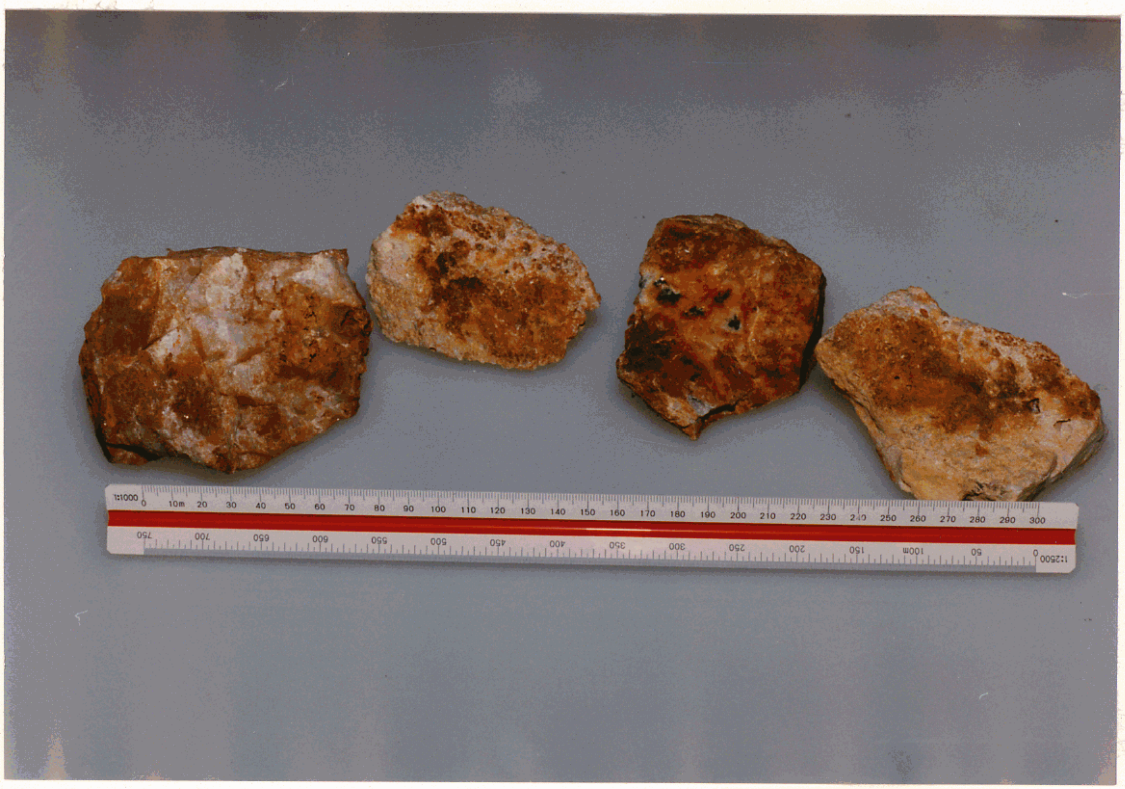


PLATE 10: Quartz Vein Specimens from North Showing.

PLATE 11: Boundary Showing. Note the seam of galena in centre of photo.

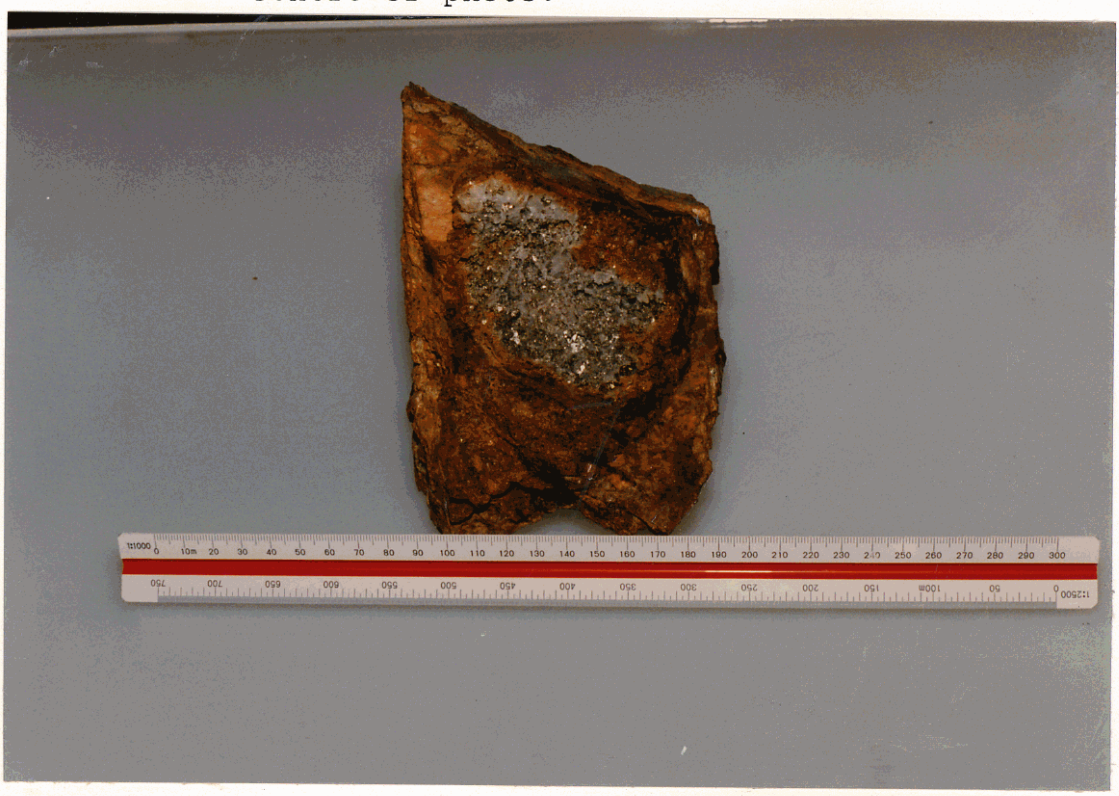


PLATE 12: Pyritic Quartz Vein Material from Boundary Showing.

PLATE 13: Sampling in Trench #1 (1988).

of unknown depth, a trench, plus an adit extending for 9.0 metres at a bearing of 260 degrees.

The adit continues along a 20 cm to 30 cm wide rusty shear zone, striking 260 degrees and dipping 65 degrees south. The host rock is a medium-grained granodiorite consisting of 10% to 20% quartz, 60% combined feldspars and 15% combined hornblende and biotite. Adjacent to the shear, the granodiorite shows a strong alteration of the mafic minerals to chlorite and the feldspars to sericite. Thin section sample P-4 was taken from the Olympic showing and was described as a brecciated, sericitized quartz diorite with quartz vein (see Appendix D).

Twenty-five rock samples were taken from the Olympic adit. Nineteen chip samples were collected along the shear over a length of 9.0 metres and an average width of 30 cm. The average silver grade was 1.41 oz/ton with a high result of 6.76 oz/ton (sample R-72).

4) The South Showing (Maps 3 & 4)

Consists of at least six trenches and one adit encompassing an area from L10+00W 3+25S to L8+00W 4+50S. The adit was not entered due to partial collapse of the entrance.

Three samples were taken from outside the adit and from dump material. Sample R-3, obtained from an altered shear, assayed .012

oz/ton Au. Sample R-4 was taken from rusty, quartz vein material in the dump and it assayed .012 oz/ton Au.

A 1.3 metre wide quartz vein was exposed for 12 metres within a trench at 9+65W 3+50S. Three samples were taken from the vein and host rock (granodiorite). The highest result was .010 oz/ton Au in friable granitic rock showing strong sericitic alteration.

5) The North Showing (Maps 7 & 8, Plates 9 and 10)

Located at 12+25W 7+30N, this showing consists of several pits and one adit 13 metres long, trending at 240 degrees.

The adit was drifted along a 0.6 metre to 1.5 metre wide quartz vein disseminated with pyrite and minor galena. The vein strikes at 240 degrees and dips 55 degrees southeast. The wallrock is granitic showing a strong alteration to chlorite and sericite.

Twelve samples were obtained along 8.5 metres of quartz vein and wallrock, over an average width of 50 cm. Lead results were the most consistent yielding an average grade of 2774 ppm. The highest precious metal value was .95 oz/ton Ag from sample R-20.

6) The Boundary Showing (Maps 7 & 8, Plates 11 and 12)

This showing consists of one adit, one shaft and ten trenches centred around L13+00W 4+75S. The adit extends 260 degrees for a length of 15 metres. A shaft of unknown depth exists at the face of the adit.

The working as plotted occurs at or near the southern boundary of the Ideal crown grant. A legal survey would be required to determine if the showing is on the subject claims.

A quartz vein 0.6 metres wide, striking 200 degrees with vertical dip, was followed for 6.5 metres outside the adit. A 5 cm wide seam of galena occurs along the western edge of the vein. The vein is faulted off by a 20 cm wide rusty shear, striking at 260 degrees and dipping vertically, at the portal of the adit. The adit was driven to follow the shear along strike.

A chip sample obtained across the 60 cm width of the quartz vein and the galena seam assayed .83 oz/ton Ag, 22831 ppm Pb and 15843 ppm Zn. Four samples taken along the shear zone assayed up to 24276 ppm Pb and 15994 ppm Zn.

Three samples of quartz vein material, disseminated with pyrite, chalcopyrite and galena, were taken from a small dump. The rock was originally from a trench located 150 metres west of the adit. Sample R-14 assayed .200 oz/ton Au, 1.36 oz/ton Ag, 571 ppm Cu and 1118 ppm Pb. This particular gold assay is the highest gold assay result encountered on the property to date. Sample R-12 assayed 4.92 oz/ton Ag, 7714 ppm Cu, 1911 ppm Pb and 41479 ppm Zn.

8.2 TRENCHING SURVEY (Maps 5 & 6, Plate 13)

Three trenches were made by a bulldozer to test the Lucky Boy vein along strike. None of the trenches were successful in intersecting the vein.

Trench #1 (1988)

Located 65 metres west of the Lucky Boy portal, with grid coordinates 10+27W 1+25S, this trench is 23 metres long, 3.5 metres wide and 4.5 metres deep (maximum). Overburden averaged over 3.0 metres before bedrock was encountered.

The exposed rock consisted of a medium-grained quartz monzonite with 15% quartz, 75% combined feldspars, 10% biotite and minor hornblende. In the centre of the trench, a rusty brown fracture 2 cm wide was found. Immediately adjacent to the seam the host rock shows strong alteration to chlorite and sericite. Two samples were taken from the rusty seam and assay results were not significant.

Trench #2 (1988)

This trench is located 23 metres west of the Lucky Boy portal, grid coordinates 9+72W 1+25S. Its dimensions are 28 metres long, 3.5 metres wide and 4.0 metres deep. The maximum depth is 5.6 metres at the centre of the trench. The trench was cut above the face of the Lucky Boy adit.

A small outcrop of fresh-looking quartz monzonite was exposed near the centre of the trench. One sample was taken from a piece of angular rusty, pyritic

float derived from the Lucky Boy vein or from uphill to the west. Significant values include 3.48 oz/ton Ag and 2613 ppm Pb.

Trench #3 (1988)

Located 50 metres east of the Lucky Boy portal, grid coordinates 9+20W 1+25S. The trench is 50 metres long, 3.5 metres wide and 1.0 metres deep.

Outcrop consisting of fresh medium-grained granodiorite was exposed along the entire length of the trench.

8.3 GEOCHEMICAL SOIL SURVEY

Breaks in the statistical histograms (Appendix E) were used to determine background and anomaly levels for each element. A correlation matrix (Table 1) and statistical report by Tony Clark, PhD. (Appendix E) aided in interpretation.

8.3.1 Soil Profiles

Twelve soil samples were taken from Trenches 1, 2 and 3 to geochemically test the soil horizons (see Report #8809253GA, Appendix B).

Trenches 1 and 2 each had over 4.0 metres of overburden, each. The upper 10 cm consisted of organic "A" horizon. Below that was 2.0 metres of light brown soil containing about 20% subangular-subrounded granitic fragments and minor round gray sedimentary fragments. The lowest horizon was a light gray soil (two metres thick) with 50% angular granitic fragments. A narrow (1 cm wide) clay seam separated the light brown and light gray horizons in Trench 1.

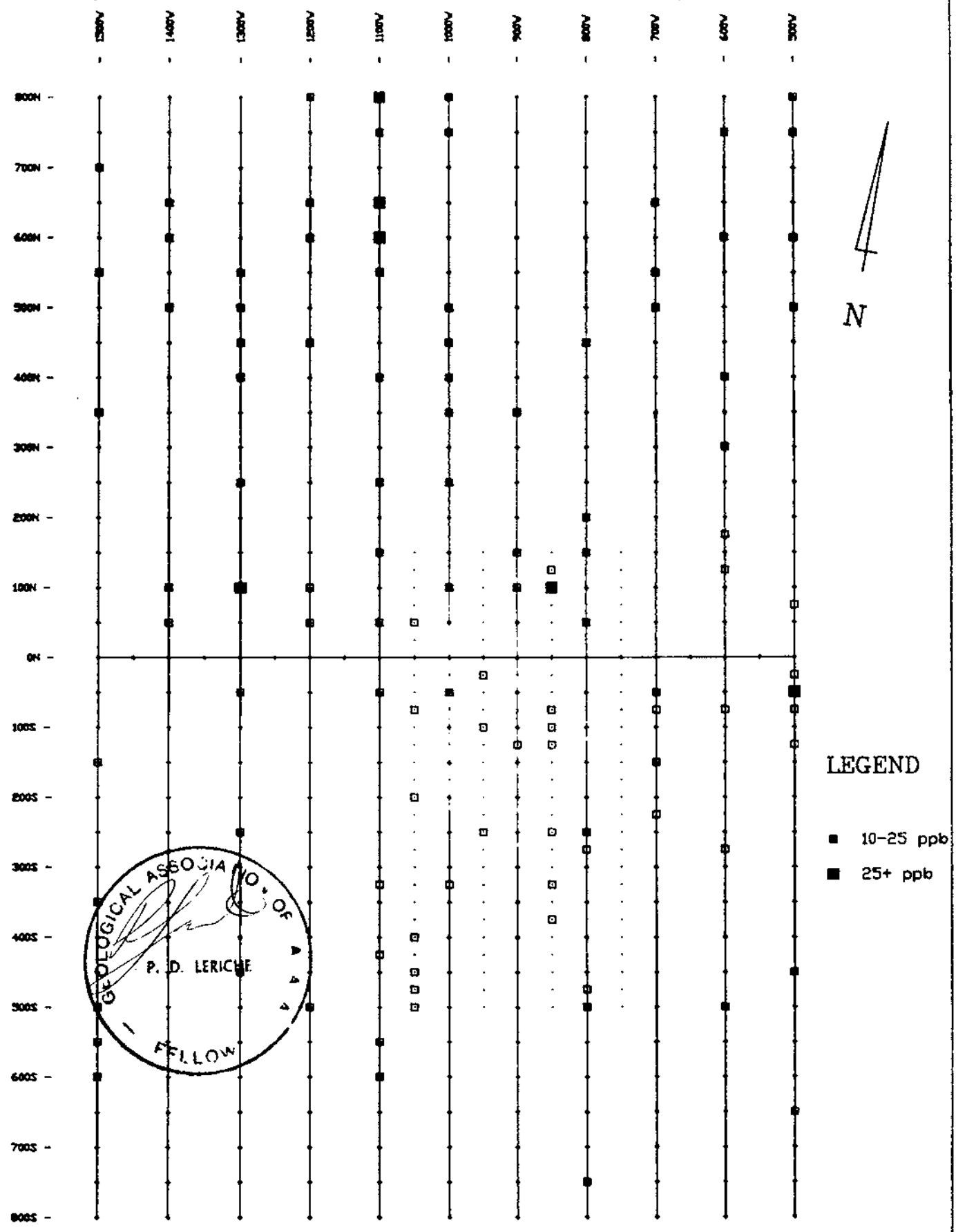
TABLE 1: Soil Sample Correlation Matrix

Lucky Boy Property   Soil Sample Correlation Matrix

	AGPPM	ALPCT	ASPPM	AUPPM	BAPPM	BIPPM	CAPCT	CDPPM	COPPM	CRPPM	CUPPM	FEPCT	KPCT	MGPCT	MNPPM	MOPPM	NAPCT	NIPPM	PPCT	PBPPM	PDPPM	SBPPM	SNPPM	SRPPM	WPPM	ZNPPM	AUPPB
AGPPM	1.00	0.10	0.46	0.15	0.20	0.17	0.37	0.33	0.32	0.39	0.40	0.32	0.40	0.33	0.02	0.35	0.01	0.43	0.03	0.27	0.08	0.11	0.26	0.20	0.01	0.33	0.20
ALPCT	0.10	1.00	0.18	0.16	0.32	0.07	0.42	0.15	0.59	0.42	0.42	0.63	0.42	0.61	0.37	0.38	0.02	0.42	0.20	0.05	0.09	0.33	0.02	0.58	0.07	0.27	0.10
ASPPM	0.46	0.18	1.00	0.19	0.22	0.11	0.61	0.35	0.40	0.62	0.73	0.48	0.37	0.52	0.24	0.57	0.00	0.71	0.05	0.29	0.07	0.06	0.39	0.41	0.05	0.31	0.41
AUPPM	0.15	0.16	0.19	1.00	0.17	0.00	0.21	0.23	0.13	0.11	0.13	0.01	0.39	0.09	0.05	0.16	0.04	0.17	0.13	0.01	0.02	0.02	0.13	0.09	0.03	0.09	0.02
BAPPM	0.20	0.32	0.22	0.17	1.00	0.00	0.04	0.06	0.00	0.09	0.19	0.07	0.01	0.06	0.57	0.09	0.04	0.07	0.62	0.06	0.05	0.25	0.06	0.22	0.02	0.22	0.15
BIPPM	0.17	0.07	0.12	0.00	0.00	1.00	0.10	0.01	0.07	0.06	0.12	0.07	0.04	0.00	0.11	0.00	0.02	0.13	0.03	0.07	0.13	0.16	0.02	0.06	0.22	0.03	0.05
CAPCT	0.37	0.42	0.61	0.21	0.04	0.10	1.00	0.41	0.64	0.67	0.65	0.63	0.66	0.72	0.53	0.53	0.01	0.67	0.00	0.10	0.02	0.10	0.43	0.00	0.06	0.33	0.31
CDPPM	0.33	0.15	0.35	0.23	0.06	-0.01	0.41	1.00	0.41	0.40	0.43	0.36	0.41	0.34	0.50	0.46	0.00	0.54	0.02	0.51	0.01	-0.11	0.12	0.29	-0.09	0.40	0.12
COPPM	0.32	0.59	0.40	0.13	0.00	-0.07	0.64	0.41	1.00	0.79	0.79	0.88	0.67	0.88	0.55	0.40	0.03	0.61	0.00	0.14	-0.00	-0.17	0.15	0.61	-0.05	0.36	0.22
CRPPM	0.39	0.42	0.62	0.11	-0.09	-0.06	0.67	0.40	0.79	1.00	0.73	0.81	0.59	0.44	0.41	0.62	0.02	0.81	0.04	0.26	0.05	-0.09	0.45	0.56	-0.04	0.31	0.25
CUPPM	0.40	0.42	0.73	0.13	-0.19	-0.12	0.65	0.43	0.79	0.73	1.00	0.75	0.55	0.75	0.38	0.50	0.01	0.82	-0.03	0.26	-0.04	-0.12	0.21	0.56	-0.06	0.40	0.34
FEPCT	0.32	0.63	0.48	0.01	-0.07	-0.07	0.63	0.36	0.88	0.81	0.75	1.00	0.64	0.92	0.44	0.46	0.04	0.75	0.03	0.10	0.10	-0.15	0.14	0.63	-0.06	0.32	0.26
KPCT	0.40	0.42	0.37	0.39	-0.01	0.04	0.66	0.41	0.67	0.59	0.55	0.64	1.00	0.68	0.46	0.50	0.01	0.57	-0.03	0.22	0.08	-0.00	0.16	0.61	-0.08	0.20	0.17
MGPCT	0.33	0.61	0.52	0.09	-0.06	-0.00	0.72	0.34	0.88	0.44	0.75	0.92	0.68	1.00	0.49	0.58	0.04	0.75	0.04	0.14	0.06	-0.17	0.19	0.73	-0.06	0.30	0.27
MNPPM	0.02	0.37	0.24	0.05	0.57	-0.11	0.53	0.50	0.55	0.41	0.38	0.44	0.46	0.49	1.00	0.43	0.04	0.49	0.29	0.25	-0.02	-0.19	0.06	0.57	-0.07	0.40	0.04
MOPPM	0.35	0.38	0.57	0.16	0.09	0.00	0.53	0.46	0.40	0.62	0.50	0.46	0.50	0.58	0.43	1.00	0.01	0.61	0.03	0.30	0.03	-0.13	0.37	0.38	-0.04	0.41	0.10
NAPCT	-0.01	0.02	0.00	-0.04	0.04	0.02	0.01	0.00	0.03	0.02	0.01	0.04	0.01	0.04	0.04	0.02	1.00	0.03	0.04	0.01	-0.05	0.02	0.00	0.03	0.01	0.02	0.03
NIPPM	0.43	0.42	0.71	0.17	-0.07	-0.13	0.67	0.54	0.61	0.81	0.82	0.75	0.57	0.75	0.49	0.61	0.03	1.00	0.07	0.30	-0.10	-0.15	0.30	0.53	-0.00	0.45	0.30
PPCT	-0.03	0.20	-0.05	-0.13	0.62	-0.03	0.08	0.02	0.00	0.04	-0.03	0.03	-0.03	0.04	0.29	0.03	0.04	0.07	1.00	-0.11	-0.16	-0.17	0.01	0.26	-0.01	0.20	-0.04
PBPPM	0.27	-0.05	0.29	0.01	-0.06	-0.07	0.10	0.51	0.14	0.26	0.26	0.10	0.22	0.14	0.25	0.30	0.01	0.30	-0.11	1.00	0.04	-0.05	0.19	0.04	-0.03	0.50	0.12
PDPPM	-0.08	0.09	-0.07	0.02	-0.05	0.13	-0.02	0.01	-0.00	0.05	-0.04	0.10	0.00	0.06	-0.02	0.03	-0.05	-0.10	-0.16	0.04	1.00	0.16	-0.06	0.02	0.00	-0.03	-0.13
SBPPM	0.11	-0.33	-0.06	-0.02	-0.25	0.16	-0.10	-0.11	-0.17	-0.09	-0.12	-0.15	-0.00	-0.17	-0.19	-0.13	0.02	-0.15	-0.17	-0.05	0.16	1.00	-0.02	-0.16	0.07	-0.20	-0.03
SNPPM	0.26	0.02	0.39	0.13	-0.06	-0.02	0.43	0.12	0.15	0.45	0.21	0.14	0.16	0.19	0.06	0.37	0.00	0.30	0.01	0.19	-0.06	-0.02	1.00	0.15	-0.01	0.09	0.13
SRPPM	0.20	0.58	0.41	0.09	0.22	-0.06	0.00	0.29	0.61	0.56	0.56	0.63	0.61	0.73	0.57	0.30	0.03	0.53	0.26	0.04	0.02	-0.16	0.15	1.00	-0.05	0.20	0.23
WPPM	0.01	-0.07	-0.05	0.03	-0.02	0.22	-0.06	-0.09	-0.05	-0.04	-0.06	-0.06	-0.08	-0.06	-0.07	-0.04	0.01	-0.00	-0.01	-0.03	0.00	0.07	-0.01	-0.05	1.00	-0.05	-0.04
ZNPPM	0.33	0.27	0.31	0.09	0.22	0.03	0.33	0.40	0.36	0.31	0.40	0.32	0.20	0.30	0.40	0.41	0.02	0.45	0.20	0.50	-0.03	-0.20	0.09	0.20	-0.05	1.00	0.11
AUPPB	0.20	0.10	0.41	-0.02	-0.15	-0.05	0.31	0.12	0.22	0.25	0.34	0.26	0.17	0.27	0.04	0.10	0.03	0.30	-0.04	0.12	-0.13	-0.03	0.13	0.23	-0.04	0.11	1.00

Tony Clark Consulting

Ashworth Explorations Limited



0 10 20 30
metres

SYMBOL MAP: Au ppb

Figure 5

Tony Clark Consulting

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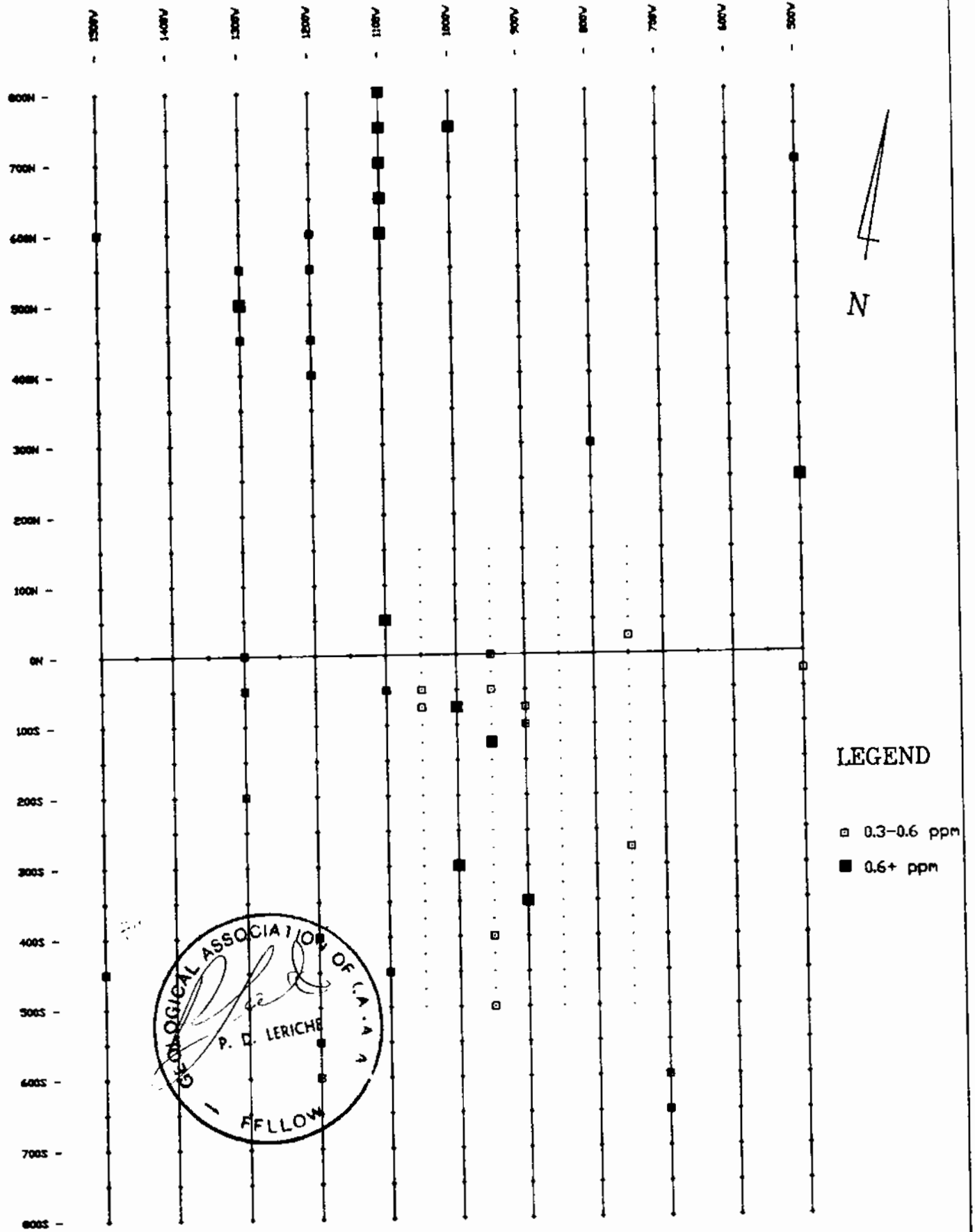


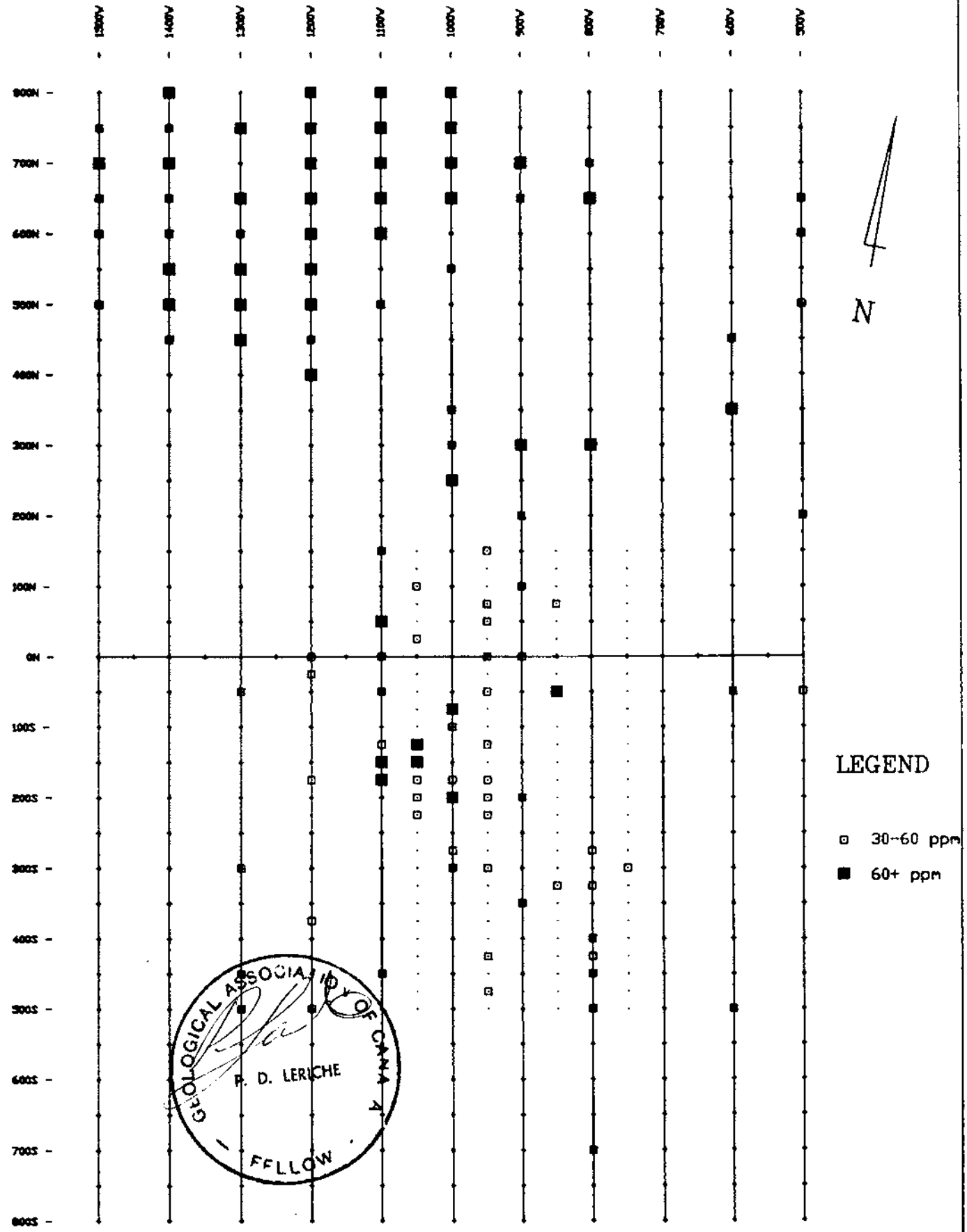
GEOLOGICAL ASSOCIATION OF C.A.A.
P. D. LERICHE
FELLOW

SYMBOL MAP: Ag ppm

Figure 6

Tony Clark Consulting

Ashworth Explorations Limited



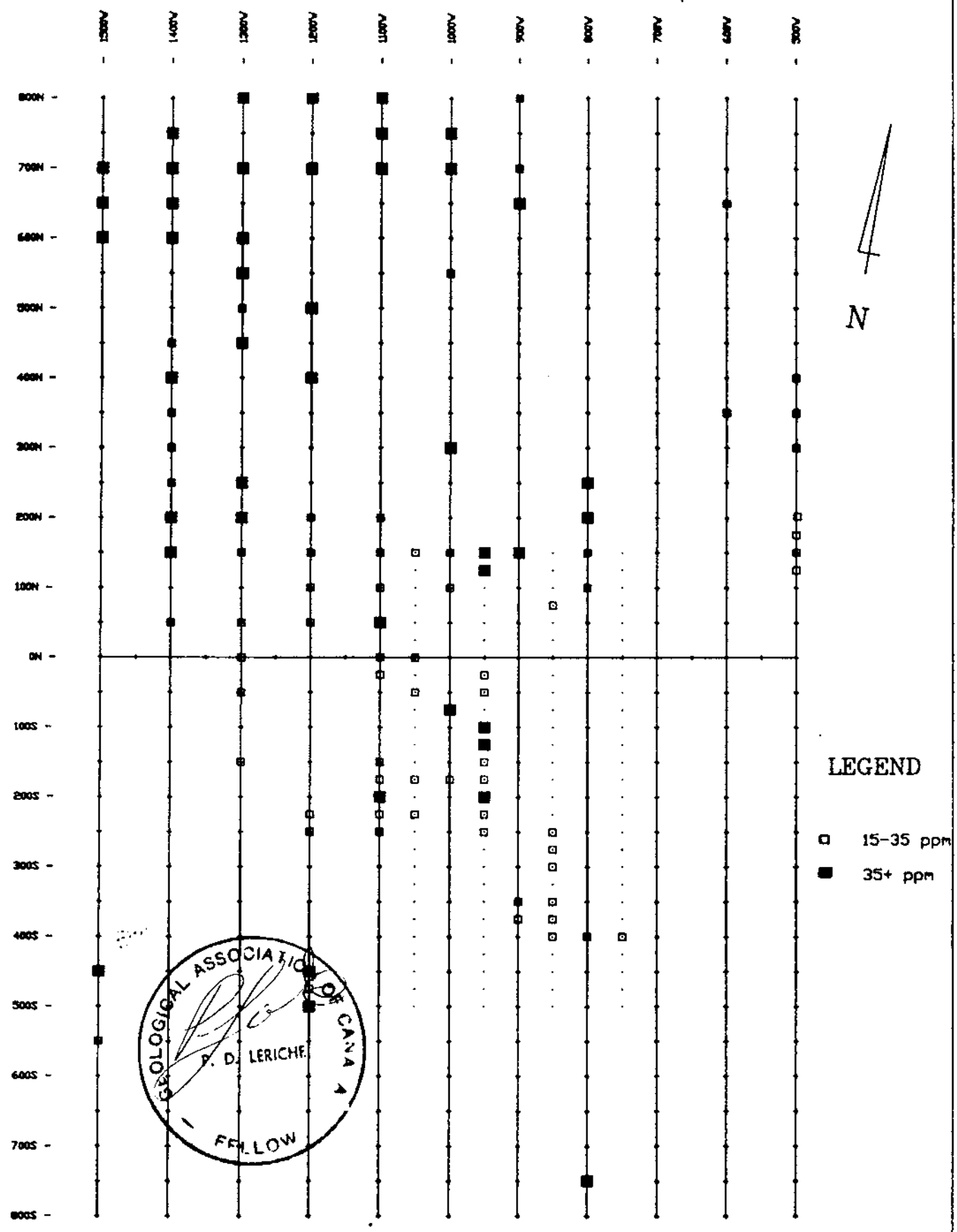
0 10 20 30
metres

SYMBOL MAP: Cu ppm

Figure 7

Tony Clark Consulting

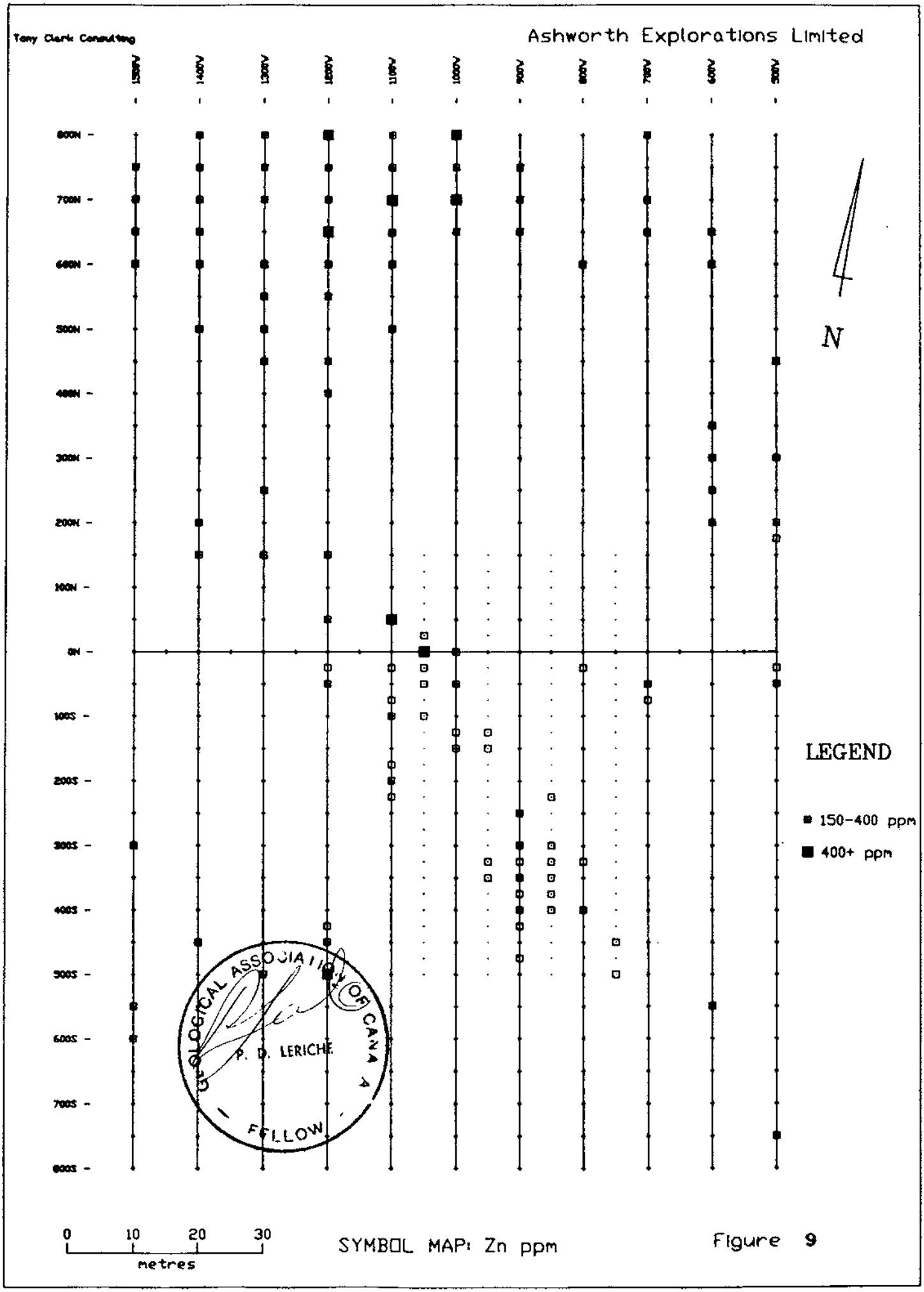
Ashworth Explorations Limited



0 10 20 30
metres

SYMBOL MAP: Pb ppm

Figure 8



SYMBOL MAP: Zn ppm

Figure 9

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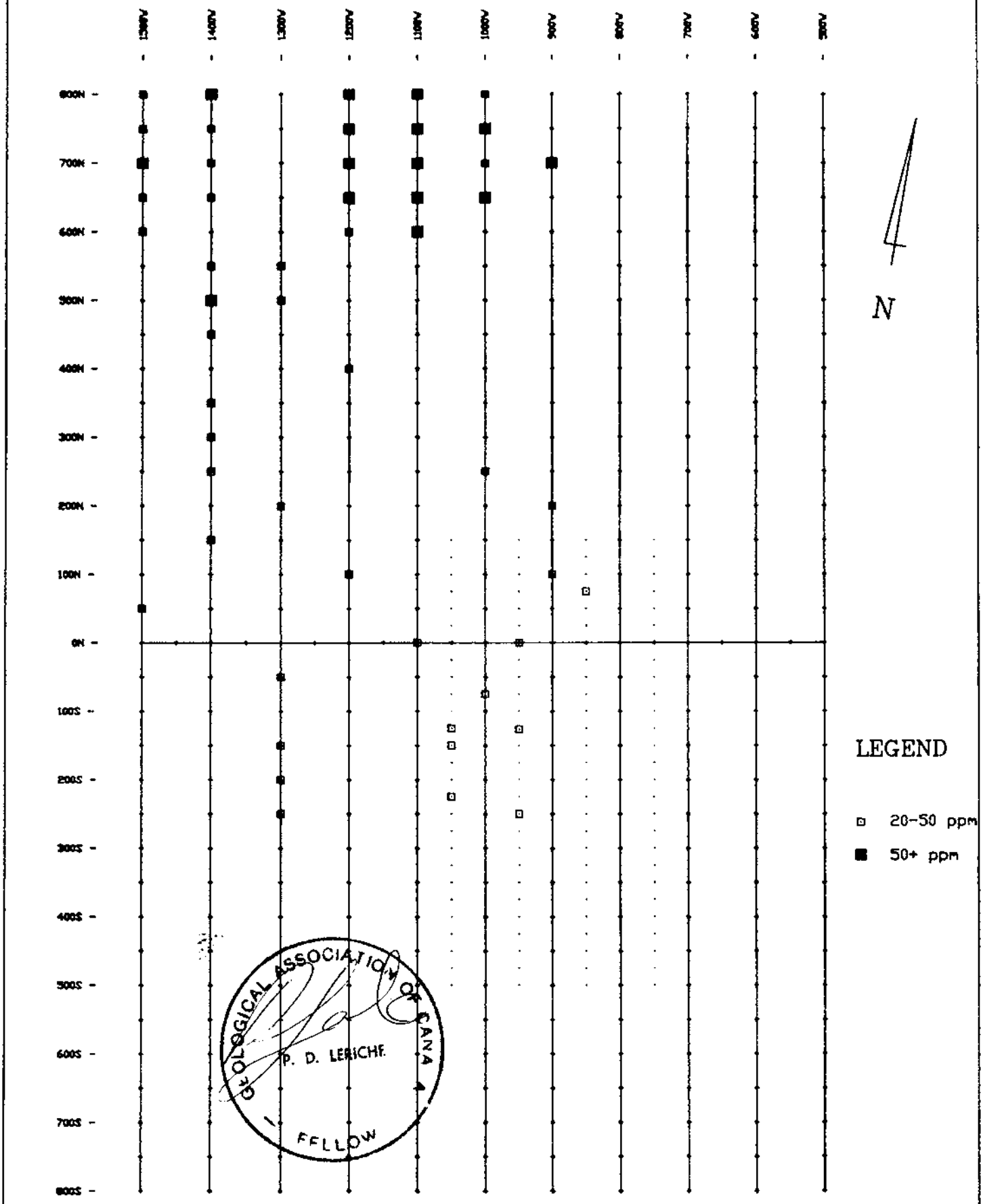
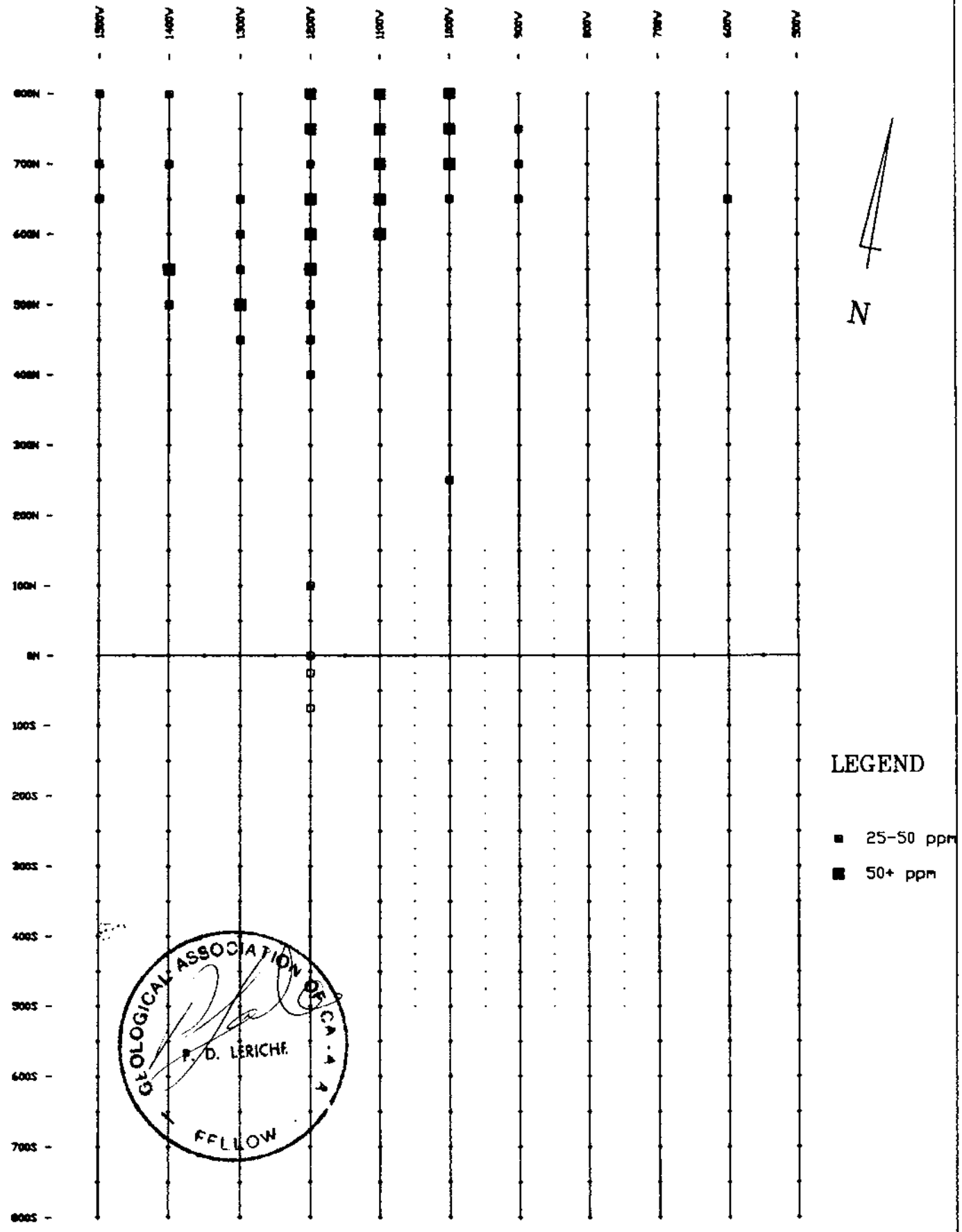


SYMBOL MAP: As ppm

Figure 10

Tony Clark Consulting

Ashworth Explorations Limited



SYMBOL MAP: Ni ppm

Figure 11

Trench 3 consisted of 20 cm of organic "A" horizon underlain by 0.7 metres of light brown "B" horizon.

In general, metal values (Au, Cu, Pb, Zn) all increase adjacent to outcrop in all the trenches. The thickness of material (over 4.0 metres in Trenches 1 and 2, which originated elsewhere), combined with a clay seam, is probably impeding the migration of metal ions to the surface. The thickness of overburden on the Lucky Boy claims is highly variable ranging from less than 1.0 metre to over 6.0 metres over relatively short distances. Therefore it is important to follow-up on subtle geochemical anomalies, especially when they correlate with other geochemical or geophysical anomalies.

8.3.2 Gold in Soil (Figure 5, Map 9)

Range:	Not detected to 45 ppb
Mean:	3.88
Standard Deviation:	5.60
Background:	0-10 ppb
Anomalous:	10-25 ppb
High Anomalous:	25+ ppb

Gold values are scattered and spotty. Three of the anomalous values occur on L11+00W 6+00-800N, just downslope from the North Showing. A weak correlation exists with arsenic, copper and nickel.

8.3.3 Silver in Soil (Figure 6, Map 10)

Range:	Not detected to 1.7 ppm
Mean:	0.15
Standard Deviation:	0.16
Background:	0-0.3 ppm
Anomalous:	0.3-0.6 ppm
High Anomalous:	0.6+ ppm

Two distinct anomalous groupings exist. The first group forms a fan-shape from L13+00W 5+00N to L11+00W 8+00N. It consists of seven high anomalous values and four lesser anomalous values. The group is downslope approximately 100 metres from the North Showing.

The second group is a small cluster of values situated around the Lucky Boy Showing and upslope (west) from the portal.

A moderate correlation exists with arsenic, copper and nickel and weak correlations with cadmium, cobalt, chromium and molybdenum.

8.3.4 Copper in Soil (Figure 7, Map 11)

Range:	Not detected to 292 ppm
Mean:	26.74
Standard Deviation:	31.17
Background:	0-30 ppm
Anomalous:	30-60 ppm
High Anomalous:	60+ ppm

High copper values occur in two distinct groups. The first group is in the northwest corner of the grid surrounding the North Showing. Most of the anomalies are in the high anomalous range. The area extends to L8+00W 6+50N and L12+00W 4+00N. The anomaly is open to both the north and the west. The five highest copper values (176, 183, 195, 254 and 292 ppm) occur on L11+00W 6+00N to 8+00N.

The second group is a cluster centred approximately 100 metres southeast and upslope from the Lucky Boy Showing (10+50W 1+50S).

The correlation matrix shows a strong correlation with arsenic, cobalt, chromium and nickel. A moderate correlation exists with silver, cadmium and molybdenum. There is a weak association with gold.

8.3.5 Lead in Soil (Figure 8, Map 12)

Range:	Not detected to 110 ppm
Mean:	12.26
Standard Deviation:	10.16
Background:	0-15 ppm
Anomalous:	15-35 ppm
High Anomalous:	35+ ppm

Lead anomalies are scattered over the grid and two main areas of interest stand out.

An east-west trending anomaly extends from 15+00W 6+50N to 9+00W 700N and averages about 100 metres wide. It remains open to both the north and the west.

A round-shaped anomaly begins at the Lucky Boy portal and extends 100 metres southwest.

There is moderate correlation with zinc.

8.3.6 Zinc in Soil (Figure 9, Map 13)

Range:	35-1254 ppm
Mean:	128.75
Standard Deviation:	82.39
Background:	0-150 ppm
Anomalous:	150-400 ppm
High Anomalous:	400+ ppm

The symbol plot for zinc indicates three groups of anomalous values.

The first group occurs in the north area near the North Showing and is very similar in character to the northern lead anomaly.

The second group is erratic and is clustered around the baseline at 10+00W.
The third group is round-shaped and centred around L9+00W 4+00S. This corresponds with the workings of the South Showing.

A moderate correlation exists with copper, lead, nickel and molybdenum. A weak correlation exists with silver and arsenic.

8.3.7 Arsenic in Soil (Figure 10, Map 14)

Range:	Not detected to 268 ppm
Mean:	12.30
Standard Deviation:	21.13
Background:	0-20 ppm
Anomalous:	20-50 ppm
High Anomalous:	50+ ppm

Two groups of anomalies occur on the north part of the grid.

The strongest group, consisting mostly of values above 50 ppm, occurs downslope from the North Showing. Its centre is L11+00W 7+00N and the anomaly is open to the north.

The second group is in the northwest corner of the grid and is open to the north and west.

Significant observations include moderate correlations with gold and silver plus

weak correlations with lead, tin and zinc. A weak to moderate correlation exists with nickel group elements (Ni, Co, Cr, Cu).

8.3.8 Nickel in Soil (Figure 11, Map 15)

Range:	8-111 ppm
Mean:	17.83
Standard Deviation:	11.87
Background:	8-25 ppm
Anomalous:	25-50 ppm
High Anomalous:	50+ ppm

One strong anomaly occurs in a broad fan-shape downslope from the North Showing. Nickel was plotted due to its strong correlation with silver, gold, arsenic, copper, lead and zinc. Scatter plots (Appendix E) were produced showing nickel versus silver, arsenic, zinc and gold. The plots show a strong correlation between low nickel values and other low values (Ag, As, Zn Au). A weak trend has been developed with zinc and arsenic.

8.3.9 Interpretation of Soil Survey

The 1988 soil survey has delineated three anomalous areas.

The first, and by far the strongest, occurs in the north area of the grid. The anomaly stretches from L15+00W 7+00N to L9+00W 7+00N and is open to the north and west. The anomaly consists of copper, lead, zinc, arsenic, nickel and silver (weak). The presence of nickel is unusual considering that the host environment is acidic in composition (i.e. granitic). Once possible explanation is that a basic body (possibly Anarchist metavolcanics) exists in the northern part of the grid and carries high background values of nickel.

Some of the northern anomaly is probably derived from the North Showing. However, anomalies were found upslope from the North Showing, suggesting that the showing continues along strike, or that other mineralized structures exist.

The second anomalous area occurs at the Lucky Boy portal and 100 to 200 metres southwest of the portal. It consists of anomalies in silver, copper, lead and zinc in a cluster. Most of the anomaly is topographically higher than the Lucky Boy vein indicating the source is uphill.

The third anomalous area is a cluster of zinc values around L9+00W 4+00S. This anomaly is considered significant because it correlates with the South Showing.

8.4 VLF-EM AND MAGNETOMETER GEOPHYSICAL SURVEYS

8.4.1 VLF-EM Survey (Maps 16 & 17)

Three weak VLF-EM conductors are present on the property.

The first conductor (A) occurs at L4+00W 6+30N. It consists of a parallel in-phase and quadrature response at a single point. Field strength results also show an anomaly at this point.

Conductor B extends from L8+00W 2+75N to L10+00W 2+10N and trends at 250°. The in-phase and quadrature responses are characterized by two parallel cross-overs which are similar on each line.

Conductor C is very weak but persistent, extending from L8+00W 0+50S to

9+50W 0+90S at a 250° trend. The in-phase and quadrature responses are parallel.

8.4.2 Magnetometer Survey (Map 18)

There seems to be a magnetic levelling problem between lines 11+00W and 12+00W. This could be caused from a magnetic change around the base station. Readings from L12+00W to L15+00W should probably be 150 to 200 gammas higher than what has been plotted. Based on observation of the map, the magnetic background level is approximately 57,000 gammas.

A linear magnetic low (M1) extends from L8+00W 3+00N to L12+00 3+00N. The low then shifts to the north from L13+00W 4+00N to L15+00W 4+00N. This shift is probably due to the levelling effect. The low is approximately 350 gammas below background.

A "bull's eye-shaped magnetic high (M2) occurs at L11+00W 4+35N, 500 gammas above background.

8.4.3 Interpretation of VLF-EM and Magnetometer Survey (Map 19)

Conductor A occurs in an area of very deep overburden, adjacent to the West Kettle River. It is not considered to be significant.

Conductor B is significant because it correlates with the linear magnetic low (M1). They both trend at 250° to 260° which is the orientation of all mineralized structures on the property, and could represent a structural shear

zone at shallow depth. The anomaly also coincides with a small creek valley, indicating that the source could be topographic.

Conductor C is very weak. However, it is considered significant because it trends at 250° and it is roughly coincident with the Lucky Boy shear zone. Geological mapping has confirmed a shear which correlates with the conductor.

The magnetic high (M2) is considered moderate (500 gammas). The probable cause is a local increase in accessory magnetite within the granitic rock.
The in-phase and quadrature values from L12+00W to L15+00W are very erratic, which is probably caused by noise. The noise could be caused by interference from a transmitter used by the IP crew on the same day.

8.5 INDUCED POLARIZATION AND RESISTIVITY SURVEY

The following summary is from Cartwright and Lockhart (1988) in their report to Ashworth Explorations Limited. The full report is included in Appendix H.

> Four zones of anomalous IP effects are interpreted to be present in the data, and are marked on Map 20.
>
> Zone A appears to strike northeasterly across the western portion of the survey grid. Generally speaking, this trend is the most anomalous of the four zones detected, with the data recorded between Station 150S and Station 50S on Line 1200W exhibiting the most encouraging response. Depth to the top of the IP source is indicated to be less than 25 meters subsurface in every case. A ragged zone of marginally lower than background apparent resistivity values can also be seen coincident with the anomalous IP effects that constitute Zone A.
>
> Zone B is best outlined by the IP data collected in the vicinity of Station 112.5S on Line 1000W. The source of this zone is thought to extend westward to beyond Line 1050W, and eastward to beyond Line 900W. In this latter

case, the zone is marked by only marginally anomalous IP effects. It is the authors' understanding that Zone B is coincident with the position of a narrow shear zone carrying elevated gold values.

Zone C is evident in the data collected on the extreme southern ends of Line 850W through to Line 750W. The zone is presently open in three directions, and may be composed of anomalous IP effects similar in magnitude to those which form Zone A.

Zone D is primarily outlined by somewhat anomalous IP effects together with slightly higher than background resistivity values, all of which trend roughly south-southwesterly across the eastern end of the grid until being truncated by IP Zone C. The region between Station 175S and Station 100S on Line 750W displays the most anomalous results recorded within the zone, the source of which appears to be more concentrated with increasing depth.

8.6 DISCUSSION OF RESULTS

Results from the 1988 field program delineated four areas of interest which will require follow-up work.

Area #1:

The first area is in the northwest part of the grid around the North Showing. This showing consists of a quartz vein, 0.6 to 1.5 metres wide and 8.5 metres long. Significant assays from rock samples were encountered in lead and silver (.95 oz/ton). A large soil geochemical anomaly occurs east and west of the North Showing consisting of copper, lead, zinc, arsenic, nickel and silver (weak). The anomaly remains open north and west of the present grid. The presence of elevated metal values uphill from the North Showing suggest the mineralized vein structure may continue along strike to the west.

Area #2:

The second area of interest occurs from the Lucky Boy portal (L9+50W 1+30S) to L12+00W 1+25S. It consists of the Lucky Boy vein, a cluster of soil geochemical anomalies and I.P. anomalies, A and B. The Lucky Boy vein was mapped as pinching-out to the west. The anomalous chargeability highs from L10+00W to 12+00W combined with soil geochemical anomalies (Ag, Cu, Pb, Zn) at Lines 10+00 and 11+00W, 1+00 to 2+00S, indicate the Lucky Boy vein may swell and exhibit mineralization to the west.

Area #3:

The third area of interest is at the South Showing, L10+00W 3+25S to L8+00W 4+50S, and chargeability high C (Lines 8+50W and 7+50W, 3+00S). Some of the higher gold values (.012 oz/ton) were taken from the adit dump and trench of the South Showing. I.P. anomaly C suggests that the South Showing may continue to the east. Geological mapping has inferred the Boundary and South showings may occur along the same structure. More detailed geological mapping is required to determine this.

Area #4:

The fourth area is at the Boundary Showing. Rock sampling from the adit yielded high values in silver, lead and zinc. Sampling of quartz vein material from a trench, 150 metres west of the adit, assayed .20 oz/ton Au and 1.36 oz/ton Ag. The Boundary adit may not be on the subject claims, however, the vein structure does continue along strike onto the claims. Due to the obtained gold value, this structure is worth follow-up work.

9. CONCLUSIONS

As the subject property is situated in a productive mining camp and is underlain by favourable geology, the author believes the claims have good potential for hosting an economic silver-gold deposit.

Geological mapping and rock sampling in 1988 has located six mineralized showings which yielded significant results in both precious and base metals.

Four areas of interest have been outlined from mapping, soil sampling, VLF-EM, magnetometer and induced polarization geophysics.

For these reasons, further exploration work is warranted and recommended.

10. RECOMMENDATIONS

Phase II

1) Geologically map and sample the entire property. This was not completed in February 1988 due to snow conditions. All old trenches and pits should be sampled, and the grid lines should be walked and carefully mapped. Special attention should be paid to the known vein structures (Areas 1, 2, 3, and 4) and their strike trend.

2) Extend the known grid lines (north and west) to include the Jamie and Jordan claims. Soil sample the new grid at 50 metre spacings. The grid around the North Showing should be tightened to line-spacings every 50

metres and station-spacings every 25 metres to better define the soil geochemical anomaly at Area #1.

3) Perform a biogeochemical orientation survey around the Lucky Boy vein. This type of survey was used effectively on the Inyo-Ackworth claims, 1.5 kilometres to the west. The varying thickness of overburden is negatively affecting soil sample results. If the orientation survey is successful then the remainder of the grid should be sampled biogeochemically.

4) An Induced Polarization survey should be continued over the existing grid and on selected parts of the extended grid. The focus of the survey should be over Area #1 (North Showing), Area #3 (South Showing) and Area #4 (Boundary Showing) to locate the mineralized structures along strike. Induced Polarization has been the most effective geophysical method used to date.

5) Perform backhoe trenching on the Lucky Boy, North, South and Boundary veins to follow the systems along strike. The Induced Polarization survey combined with geological mapping would be used to establish trenching targets.

Phase III

Phase III is contingent upon drill targets being established from Phase II. It would consist primarily of diamond drilling to test the down-dip extensions of the mineralized structures. A backhoe or bulldozer would be required to support the drill program and to perform more trenching.

11. PROPOSED BUDGETS

11.1 PROPOSED BUDGET PHASE II

(Two Geologists, Four Geotechnicians; 10 Field Days)

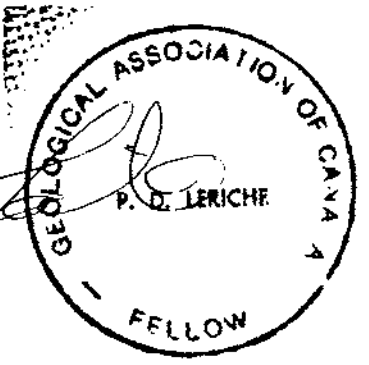
Project Preparation		$ 950
Mob/Demob		$ 4,450
Field Crew		$ 14,800
Field Costs		$ 7,700
Subcontractors:		
I.P. Survey - 20 line kilometres X $1,200/km	$ 24,000	
Mob/Demob	$ 2,000	
		$ 26,000
Backhoe - 60 hours X $60/hr	$ 3,600	
Mob/Demob	$ 500	
		$ 4,100
Lab Analysis:		
Say 550 soil samples @ $15/sample	$ 8,250	
Say 50 organic samples @ $15/sample	$ 750	
Say 100 rock samples @ $18/sample	$ 1,800	
		$ 10,800
Supervision and Report		$ 10,450
Sub-total		$ 79,250
Administration 15%		11,887
Total		$ 91,137
	(Say	$ 91,000)

11.2 PROPOSED BUDGET PHASE III

(Two Geologists, One Geotechnician; Estimated 20 Field Days)

Project Preparation		$ 1,300
Mob/Demob		$ 2,250
Field Crew		$ 16,200
Field Costs		$ 8,500
Backhoe - 100 hours X $60/hr	$ 6,000	
Mob/Demob	$ 500	
		$ 6,500
Diamond Drilling - 600 metres X $100/metre	$ 60,000	
Mob/Demob	$ 5,000	
		$ 65,000
Lab Analysis:		
Say 200 rock and core samples @ $18/sample	$ 3,600	$ 3,600
Supervision and Report		$ 10,900
Sub-total		$ 114,250
Administration 15%		17,137
Total		$ 131,387
	(Say	$ 131,000)

Respectfully submitted,



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B.Sc., F.G.A.C.

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CERTIFICATE

I, PETER D. LERICHE, of 3612 West 12th Avenue, Vancouver, B.C., V6K 2R7, do hereby state that:

1. I am a graduate of McMaster University, Hamilton, Ontario, with a Bachelor of Science Degree in Geology, 1980.

2. I am a Fellow in good standing with the Geological Association of Canada.

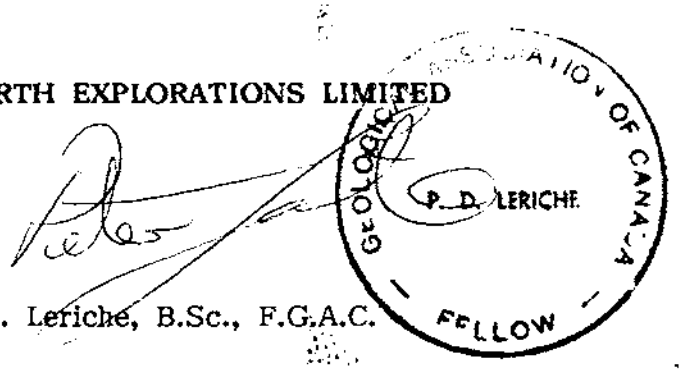
3. I have actively pursued my career as a geologist for nine years in British Columbia, Ontario, Yukon and Northwest Territories, Arizona, Nevada and California.

4. The information, opinions, and recommendations in this report are based on fieldwork carried out under my direction, published and unpublished literature. I was present on the subject property from February 18 to 21, 1988.

5. I have no interest, direct or indirect, in the subject claims or the securities of Dryden Resource Corporation.

6. I consent to the use of this report in a Prospectus or Statement of Material Facts for the purpose of private or public financing.

ASHWORTH EXPLORATIONS LIMITED



Peter D. Leriche, B.Sc., F.G.A.C.

Dated at Vancouver, B.C., February 29, 1988

ITEMIZED COST STATEMENT

Project Preparation			$ 950.00
Mob/Demob (includes transportation, freight and wages)			4,450.00
Field Crew			
Project Geologist $325/day X 4 days (February 18-21/88)	$	1,300.00	
Field Geologist $275/day X 11 days		3,025.00	
5 Geotechnicians $210/day X 60 mandays (February 10-22/88)		12,600.00	16,925.00
Field Costs			
Food and Accommodation $70/day X 75 mandays	$	5,250.00	
Communications $30/day X 12 days		360.00	
Supplies		1,200.00	
2 4X4 Trucks $110/day each X 24 days		2,640.00	9,450.00
Contractors			
Magnetometer - VLF-EM Survey	$	9,375.00	
I.P. Survey		19,000.00	
Bulldozer		3,500.00	
Vancouver Petrographics		325.00	32,200.00
Lab Analysis			
537 soil samples @ $12.85/sample (Geochem Au and multi ICP)	$	6,900.45	
87 rock samples @ $20.50/sample (Au,Ag Fire Assay and multi ICP)		1,783.50	8,683.95
Supervision and Report			$ 10,600.00
Sub-total			$ 83,258.95
Administration 15%			12,488.84
Total			$ 95,747.80

APPENDIX A

ROCK SAMPLE DESCRIPTIONS

LUCKY BOY PROJECT

ROCK SAMPLE DESCRIPTIONS

SAMPLE NO.	KIND OF SAMPLE	DESCRIPTIONS	WIDTHS
LB88 R-1	Chip	Calcite vein, strike 240, dipping 65 NW, intruded into hornblend, biotite granitic rock	25 cm
LB88 R-2	Chip	Shear zone, strike 310 , dipping 45 NE at the end of the adit	45 cm
LB88 R-3	Chip	Rusty, dark brown, altered rock within shear zone at L8+78W-3+97S, taken from the portal of the adit	10 cm
LB88 R-4	Grab	Dark brown, rusty quartz vein material with minor pyrite and chalcopyrite	-
LB88 R-5	Chip	Shear zone strike 255 and vertical No. visible textures or sulphides	25 cm
LB88 R-6	Chip	Shear zone of fine-grained green rock. No mineralization	25 cm
LB88 R-7	Chip	Rusty altered shear zone, Fe-oxide minor pyrite	25 cm
LB88 R-8	Chip	Altered shear zone with minor pyrite and chalcopyrite at the end of the adit	30 cm
LB88 R-9	Chip	Altered granitic rock with chlorite and sericite alteration onthe road cut at L8+50W, no mineralization	100 cm
LB88 R-10	Chip	Altered granitic rock taken from the road cut, at L4W 3+00S, sericite, muscovite, no sulphides	100 cm
LB88 R-11	Chip	Shear zone strike 260, altered, green, fine grained rock at L12W+5+00S	30 cm
LB88 R-12	Dump	Sample taken from dump material of trench at L14+50W 4+50S, quartz vein material with pyrite, chalcopyrite, rusty with minor malachite	-

SAMPLE NO.	KIND OF SAMPLE	DESCRIPTIONS	WIDTHS
LB88 R-13	Dump	Dump sample taken from the same spot (trench), quartz vein material with pyrite, chalcopyrite and galena	-
LB88 R-14	Dump	Dump quartz vein material, pyrite, chalcopyrite up to 30% and minor galena, dark brown, rusty sample	-
LB88 R-15	Chip	Quartz vein with pyrite crystals, fine grained galena, minor hematite (the north adit)	60 cm
LB88 R-16	Chip	Sample across the vein in the north adit, disseminated with pyrite, chalcopyrite and minor galena, trace of hematite	70 cm
LB88 R-17	Chip	The same vein, more galena, less pyrite and chalcopyrite, malachite	70 cm
LB88 R-18	Chip	Sample across the vein, vuggy, rusty, light brown with abundant disseminated pyrite, minor chalcopyrite and galena	60 cm
LB88 R-19	Chip	Quartz vein with light brown to yellow colour, 5% pyrite and chalcopyrite, minor galena and Fe-oxide	60 cm
LB88 R-20	Chip	Sample across the vein (the north adit), 5% pyrite crystals, minor galena	45 cm
LB88 R-21	Chip	Sample across the vein and the wall rock, pyrite crystals, galena, minor hematite and limonite staining (taken from the trench)	120 cm
LB88 R-22	Chip	Sample over the vein and the wallrock vuggy quartz with pyrite dissemination, altered granitic wallrock with minor sulphides	120 cm
LB88 R-23	Chip	Vuggy quartz vein with pyrite crystals, rusty on surface, minor galena and limonite, the wallrock is altered granite with trace of pyrite	120 cm
LB88 R-24	Chip	Sample over the vein and the wallrock. Rusty vuggy quartz with pyrite, chalcopyrite galena and limonite	120 cm
LB88 R-25	Chip	Sample over 150 cm of altered granitic rock (no vein) with sericitic and chloritic alteration	150 cm

SAMPLE NO.	KIND OF SAMPLE	DESCRIPTIONS	WIDTHS
LB88 R-51	Grab	Soft, weatered, brumbly coarse-grained granitic rock with chloritic and sericitic alteration no obvious mineralization (from the portal of the Olympic adit)	-
LB88 R-52	Grab	Soft, friable, weathered granitic rock, sericitic alteration, no mineralization	-
LB88 R-53	Grab	Weathered, altered granitic, granodioritic rock with fragments of fine grained grey volcanic, barren looking rock, no obvious sulphides	-
LB88 R-54	Grab	Barren quartz diorite to granodiorite, soft and crumbly with altered biotite	-
LB88 R-55	Grab	Soft crumbly, weathered granitic rock, no obvious mineralization	-
LB88 R-56	Chip	Rusty shear, and altered zone strike 260, bleached feldspar. Argilic alteration no sulphides	20 cm
LB88 R-57	Chip	Altered shear zone with bleached feldspar. No visible textures or sulphides	20 cm
LB88 R-58	Chip	Soft, altered, easily broken sheared rock. Same as 57	20 cm
LB88 R-59	Chip	The same shear zone with bleached feldspar. No visible texture or sulphides	20 cm
LB88 R-60	Chip	Sample over crumbly soft sheared, and altered zone in altered granitic rock. No mineralization.	20 cm
LB88 R-61	Chip	Sample across shear zone of friable, rusty rock with argilic alteration	15 cm
LB88 R-62	Chip	Rusty shear zone with bleached feldspar in barren granitic rock, no sulphides	20 cm
LB88 R-63	Chip	The same shear zone as #62, altered and bleached feldspar in barren looking granitic rock	25 cm
LB88 R-64	Chip	Sample over the same shear zone, minor rust limonite staining	25 cm

SAMPLE NO.	KIND OF SAMPLE	DESCRIPTIONS	WIDTHS
LB88 R-65	Chip	Sample over shear zone, argilic alteration rusty with no obvious mineralization	25 cm
LB88 R-66	Chip	Sample across the same shear zone adjacent to the portal of the adit, rusty, altered soft rock in altered granitic countary rock	25 cm
LB88 R-67	Chip	Sample across 60 cm of quartz diorite with argilic alteration, minor rust and limonite	60 cm
LB88 R-68	Chip	Shear zone with limonite, minor rust, no sulphides	30 cm
LB88 R-69	Chip	Shear xone as #68, soft crumbling in altered weathered granitic rock	-
LB88 R-70	Chip	Rusty shear zone with limonite, bleached feldspar, very rusty and crumbly rock	30 cm
LB88 R-71	Chip	Altered rock with bleached feldspar, limonite staining, dark brown, rusty and friable	30 cm
LB88 R-72	Chip	Shear zone exposed in a trench adjacent to the olympic adit, dark brown, crumbly rock with limonite staining, the sample is heavy	30 cm
LB88 R-73	Chip	Dark brown rusty sheared rock within granitic rock, limonite staining, iron oxide no sulphides high density	30 cm
LB88 R-74	Chip	Sample over 30 cm of altered, sheared granitic rock at the end of the adit strike 200	30 cm
LB88 R-75	Chip	Dark brown, altered shear zone with limonite staining, Fe oxide, high density rock	30 cm
LB88 R-76	Chip	Sample over 150 cm of quartz vein in the Lucky Boy adit, vuggy quartz with limonite, hematite malachite and minor pyrite, strike 260, dipping 50 N	150 cm
LB88 R-77	Grab	Quartz vein material taken from the dump of the adit, pyrite, malachite and minor galena	-
LB88 R-78	Grab	Quartz vein material disseminated with pyrite, chalcopyrite, minor galena and malachite	-

SAMPLE NO.	KIND OF SAMPLE	DESCRIPTIONS	WIDTHS
LB88 R-79	Grab	Vuggy, rusty quartz vein material disseminated with sulphides mainly pyrite and chalcopyrite 5%, malachite staining and minor galena	-
LB88 R-80	Grab	Quartz vein material disseminated with pyrite 5% chalcopyrite, 3% malachite staining and sphalerite	-
LB88 R-81	Chip	Sample across quartz vein in the Lucky Boy adit strike 265, disseminated with pyrite 2%, chalcopyrite 1%, malachite staining and hamatite	60 cm
LB88 R-82	Chip	The same vein, more malachite, less pyrite and chalcopyrite, trace of galena and sphalerite	45 cm
LB88 R-83	Chip	Lucky Boy vein, loaded with malachite staining, 2-5% pyrite and chalcopyrite trace of galena	45 cm
LB88 R-84	Chip	Sample over the Lucky Boy bein pyrite and chalcopyrite dissemination, trace of malachite and pyrite	45 cm
LB88 R-85	Chip	Quartz vein and the wallrock, both disseminated with 5% chalcopyrite, 2% pyrite, trace of malachite	30 cm
LB88 R-86	Chip	The vein in this spot is loaded with malachite 2-5% sulphides mainly chalocpyrite, the vein is rusty	60 cm
LB88 R-87	Chip	Sample over the vein and the wallrock. Pyrite chalcopyrite dissmination in quartz vein 30 cm with and the wallrock (30 cm), trace of galena in the vein	60 cm
LB88 R-88	Chip	Smokey quartz vein, less mineralization 1-2% sulphides, trace of galena, no copper staining	90 cm
LB88 R-89	Chip	Smokey quartz vein, disseminated with pyrite, chalcopyrite, sphalerite and trace of galena	90 cm

SAMPLE NO.	KIND OF SAMPLE	DESCRIPTIONS	WIDTHS
LB88 R-90	Chip	Smokey quartz vein with minor malachite less mineralization, sample over the vein and the wallrock	135 cm
LB88 R-91	Chip	Sample over the vein 60 cm and the wallrock 30 cm, pyrite, minor chalcopyrite within altered granitic rock	90 cm
LB88 R-92	Chip	Quartz vein with malachite staining, less pyrite an chalcopyrite, smokey quartz with minor oxides	75 cm
LB88 R-93	Chip	Sample over the vein and the wallrock smokey quartz with less sulphides within altered granitic rocky muscovite	-
LB88 R-94	Chip	Sample over the vein, less pyrite and chalcopyrite, no copper staining	30 cm
LB88 R-95	Chip	The vein in this spot strike 175 dipping 55 -S, minor sulphides	30 cm
LB88 R-96	Chip	Wallrock sample at the contact with the vein, 20% pyrite in altered granitic rock	30 cm
LB88 R-97	Chip	Smokey quartz vein with Fe oxide pyrite, chalcopyrite, and copper staining, sulphides dissemination within the wallrock	30 cm
LB88 R-98	Chip	Sample taken at the same spot as R-97 over the vein and the wallrock, pyrite chalcopyrite and minor copper staining	90 cm
LB88 R-99	Chip	Sample taken across 25 cm of quartz vein and 55 cm of the wallrock, both disseminated with pyrite, chalcopyrite and minor copper staining	60 cm
LB88 R-100	Chip	5-10% of disseminated sulphides mainly pyrite in smokey quartz vein	25 cm
LB88 R-101	Float	Float quartz vein material slightly disseminated with pyrite and trace of chalcopyrite	-
LB88 R-102	Chip	Chip sample across 120 cm of quartz vein strike 270, dipping 80 south, reddish, rusty, vesicular with muscouite and trace of pyrite	120 cm

SAMPLE NO.	KIND OF SAMPLE	DESCRIPTIONS	WIDTHS
LB88 R-103	Chip	Altered, weathered, crumbly granitic rock with sericitic alteration	30 cm
LB88 R-104	Chip	Sample across the vein as R-102, strike 270, dipping 75 S, reddish quartz slightly mineralized with sulphides, minor muscovite	90 cm
LB88 R-105	Chip	Soft, weathered, cumbly granitic rock, sericitic and chloritic alteration, no mineralization	150 cm
LB88 R-106	Chip	Rusty, altered granitic rock with chloritic alteration, biotite is altered to chlorite, rusty looking rock, strike 150	60 cm
LB88 R-107	Chip	Sample taken from the same rusty zone, deep dark brown rusty granitic rock with chlorite sericite alteration	60 cm
LB88 R-108	Chip	Altered granitic rock, pyrite dissemination, no vein	50 cm
LB88 R-109	Chip	Altered granitic rock slightly disseminated with pyrite, no vein	50 cm
LB88 R-110	Float	Quartz vein material from the wall of TR-2, loaded with sulphides mainly pyrite about 30% and 5-10% chalcopyrite with trace of galena	-
LR P1	Chip	Sample across quartz vein, loaded with galena, pyrite and chalcopyrite dissemination, strike 200 and vertical	60 cm

APPENDIX B

ANALYTICAL REPORTS
by
VANGEOCHEM LIMITED

Report #880249 AA (87 Rock Samples)
Report #880248 GA (525 Soil Samples)
Report #880253 GA (12 Soil Profile Samples)

VANGEOCHEM LAB LIMITED

MAIN OFFICE
1521 PEMBERTON AVE.
NORTH VANCOUVER, B.C V7P 2S3
(604) 986-5211 TELEX: 04-352578

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

ASSAY ANALYTICAL REPORT

CLIENT: ASHWORTH EXPLORATION LTD.
ADDRESS: Mez. Floor, 744 W. Hastings St.
: Vancouver, B.C.
: V6C 1A5

DATE: Mar 07 1988
REPORT#: 880249 AA
JOB#: 880249

PROJECT#: 192
SAMPLES ARRIVED: Feb 24 1988
REPORT COMPLETED: Mar 04 1988
ANALYSED FOR: Ag Au ICP

INVOICE#: 880249 NA
TOTAL SAMPLES: 87
REJECTS/PULPS: 90 DAYS/1 YR
SAMPLE TYPE: 87 Rock

SAMPLES FROM: Submitted by P. Leriche.
COPY SENT TO: All copies sent to Vancouver office.

PREPARED FOR: Mr. Peter Leriche

ANALYSED BY: David Chiu

SIGNED: _____
Registered Provincial Assayer

GENERAL REMARK: Data disk sent to Mr. Tony Clark.

VANGEOCHEM LAB LIMITED

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NORTH VANCOUVER, B.C. V7P 2S3
(604) 986-5211 TELEX: 04-352578

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

REPORT NUMBER: 880249 AA JOB NUMBER: 880249 ASHWORTH EXPLORATION LTD.

SAMPLE #	Ag oz/st	Au oz/st
LB 88 - R 1	.01	.005
LB 88 - R 2	.12	.005
LB 88 - R 3	.05	.012
LB 88 - R 4	.16	.012
LB 88 - R 5	.21	.005
LB 88 - R 6	.04	<.005
LB 88 - R 7	.43	.006
LB 88 - R 8	.19	.008
LB 88 - R 9	.01	.005
LB 88 - R10	<.01	<.005
LB 88 - R11	.03	.005
LB 88 - R12	4.92	<.005
LB 88 - R13	<.01	<.005
LB 88 - R14	1.36	.200
LB 88 - R15	.16	<.005
LB 88 - R16	.02	<.005
LB 88 - R17	.21	<.005
LB 88 - R18	<.01	<.005
LB 88 - R19	.43	<.005
LB 88 - R20	.95	<.005
DETECTION LIMIT	.01	.005

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed:

VANGEOCHEM LAB LIMITED

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(604) 986-5211 TELEX: 04-352578

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(604) 251-5656

SAMPLE #	Ag oz/st	Au oz/st
LB 88 - R21	.20	<.005
LB 88 - R22	.01	.005
LB 88 - R23	.01	.005
LB 88 - R24	.10	<.005
LB 88 - R25	.04	<.005
LB 88 - R26	.01	<.005
LB 88 - R51	.01	.005
LB 88 - R52	.02	<.005
LB 88 - R53	.03	<.005
LB 88 - R54	.03	<.005
LB 88 - R55	.01	<.005
LB 88 - R56	.37	.005
LB 88 - R57	.13	<.005
LB 88 - R58	.06	<.005
LB 88 - R59	.04	<.005
LB 88 - R60	1.17	<.005
LB 88 - R61	1.26	<.005
LB 88 - R62	.48	<.005
LB 88 - R63	.51	<.005
LB 88 - R64	1.19	.006
DETECTION LIMIT	.01	.005

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed:

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VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Ag oz/st	Au oz/st
LB 88 - R65	1.60	<.005
LB 88 - R66	.55	<.005
LB 88 - R67	.07	<.005
LB 88 - R68	1.91	.005
LB 88 - R69	1.03	<.005
LB 88 - R70	3.45	<.005
LB 88 - R71	.07	<.005
LB 88 - R72	6.76	.022
LB 88 - R73	3.10	.005
LB 88 - R74	.03	<.005
LB 88 - R75	.06	<.005
LB 88 - R76	5.14	<.005
LB 88 - R77	11.54	<.005
LB 88 - R78	.96	<.005
LB 88 - R79	2.80	.005
LB 88 - R80	1.57	.005
LB 88 - R81	2.40	.005
LB 88 - R82	3.90	.005
LB 88 - R83	.82	<.005
LB 88 - R84	.44	<.005
DETECTION LIMIT	.01	.005

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

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VANCOUVER, B.C V5L 1L6
(604) 251-5656

SAMPLE #	Ag oz/st	Au oz/st
LB 88 - R85	.06	<.005
LB 88 - R86	.10	<.005
LB 88 - R87	.29	<.005
LB 88 - R88	.24	<.005
LB 88 - R89	1.85	.005
LB 88 - R90	.27	<.005
LB 88 - R91	3.37	<.005
LB 88 - R92	3.46	.005
LB 88 - R93	.97	<.005
LB 88 - R94	.16	<.005
LB 88 - R95	.32	<.005
LB 88 - R96	.78	<.005
LB 88 - R97	3.27	.008
LB 88 - R98	2.59	.005
LB 88 - R99	2.71	<.005
LB 88 - R100	.29	<.005
LB 88 - R101	.05	<.005
LB 88 - R102	.10	<.005
LB 88 - R103	.16	.010
LB 88 - R104	.05	<.005
DETECTION LIMIT	.01	.005

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed:

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(604) 986-5211 TELEX: 04-352578

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1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Ag oz/st	Au oz/st
LB 88 - R105	.01	<.005
LB 88 - R106	.01	<.005
LB 88 - R107	.02	<.005
LB 88 - R108	.72	.020
LB 88 - R109	.11	<.005
LB 88 - R110	3.48	<.005
LB 88 - P 1	.83	<.005
DETECTION LIMIT	.01	.005

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed:

VANGEOCHEM LAB LIMITED

MAIN OFFICE: 1521 PEMBERTON AVE. N.VANCOUVER B.C. V7P 2S3 PH:(604)986-5211 TELEX:04-352578
BRANCH OFFICE: 1630 PANDORA ST. VANCOUVER B.C. V5L 1L6 PH:(604)251-5656

ICAP GEOCHEMICAL ANALYSIS

A .5 GRAM SAMPLE IS DIGESTED WITH 5 ML OF 3:1:2 HCL TO HNO3 TO H2O AT 95 DEG. C FOR 90 MINUTES AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR BA,FE,CA,P,CR,MG,BA,TI,B,AL,NA,K,W,PT AND SR. AU AND PD DETECTION IS 3 PPM.
IS= INSUFFICIENT SAMPLE, ND= NOT DETECTED, -= NOT ANALYZED

COMPANY: ASHWORTH EXPL. LTD.
ATTENTION: P. LERICHE
PROJECT: 192

REPORT#: 880249PA
JOB#: 880249
INVOICE#: 880249NA

DATE RECEIVED: 88/02/24
DATE COMPLETED: 88/03/11
COPY SENT TO:

ANALYST

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
LB 88-R1	.1	2.95	ND	ND	10	3	22.86	.2	6	7	21	.66	.08	.27	432	1	.01	7	.01	12	ND	ND	ND	ND	318	30	ND	17
LB 88-R2	3.5	1.97	ND	ND	64	4	2.52	1.2	20	30	1163	3.42	.08	.91	999	9	.01	21	.04	116	ND	ND	ND	ND	60	ND	ND	427
LB 88-R3	.8	1.39	4	ND	88	4	.32	1.2	9	52	296	3.13	.05	.68	1482	7	.01	19	.03	41	ND	ND	ND	ND	19	ND	ND	98
LB 88-R4	3.7	.81	ND	ND	83	ND	.05	.6	16	17	430	10.41	.08	.22	205	9	.01	40	.06	23	ND	ND	ND	ND	26	ND	ND	141
LB 88-R5	5.5	.97	41	ND	62	3	.81	11.3	14	56	108	2.66	.06	.30	1034	9	.01	16	.03	24276	ND	ND	3	ND	12	ND	ND	2315
LB 88-R6	.8	1.03	4	ND	62	5	.79	1.2	8	93	48	1.54	.05	.35	1070	4	.01	8	.03	780	ND	ND	ND	ND	12	ND	ND	423
LB 88-R7	12.3	.79	17	ND	32	14	2.09	6.5	36	46	719	3.02	.08	.30	1372	8	.01	18	.01	1388	ND	ND	ND	ND	22	ND	ND	1329
LB 88-R8	5.1	.91	12	ND	23	8	2.32	67.1	13	78	153	1.91	.07	.40	1628	11	.01	15	.01	3657	ND	ND	ND	ND	25	ND	ND	15994
LB 88-R9	.2	2.08	ND	ND	45	3	.89	.6	21	20	33	3.29	.05	1.60	920	ND	.01	28	.13	49	ND	ND	ND	ND	44	ND	ND	174
LB 88-R10	.1	3.16	ND	ND	29	5	1.41	.4	15	42	25	2.62	.06	.86	800	2	.01	18	.06	30	ND	ND	ND	ND	135	ND	ND	92
LB 88-R11	.6	.59	5	ND	17	3	3.70	3.2	10	85	19	1.77	.08	.28	1424	4	.01	12	.01	487	ND	ND	ND	ND	36	ND	ND	816
LB 88-R12	>100	.64	63	ND	2	985	.01	542.9	21	76	7714	5.90	.03	.07	242	34	.01	30	.01	1911	ND	ND	ND	ND	2	ND	144	41479
LB 88-R13	5.1	.85	48	ND	64	4	.24	4.1	6	43	150	8.03	.06	.28	235	4	.01	35	.04	51	ND	ND	ND	ND	44	ND	ND	394
LB 88-R14	42.2	.20	310	ND	20	38	.01	2.2	1	45	571	12.05	.07	.02	29	47	.01	47	.01	1118	ND	ND	ND	ND	3	ND	ND	384
LB 88-R15	4.5	.26	44	ND	20	7	.06	21.2	4	72	153	1.28	.03	.01	187	44	.01	6	.01	2037	ND	ND	ND	ND	3	ND	ND	2433
LB 88-R16	3.1	.24	50	ND	22	8	.07	1.7	3	59	85	1.31	.03	.01	66	39	.01	5	.01	906	ND	ND	ND	ND	2	ND	ND	250
LB 88-R17	6.1	.26	33	ND	18	6	.24	10.6	4	97	55	.81	.03	.02	445	8	.01	4	.01	4007	ND	ND	3	ND	6	ND	ND	911
LB 88-R18	2.7	.20	51	ND	14	5	.02	3.1	3	143	78	1.23	.02	.01	181	64	.01	8	.01	1150	ND	ND	ND	ND	1	ND	ND	555
LB 88-R19	15.6	.20	105	ND	16	3	.02	7.3	3	75	140	1.91	.03	.01	438	57	.01	9	.01	1908	ND	ND	ND	ND	1	ND	ND	935
LB 88-R20	29.7	.17	102	ND	11	9	.12	3.9	3	69	280	1.45	.02	.01	428	29	.01	9	.01	11336	ND	ND	11	ND	3	ND	ND	479
LB 88-R21	6.1	.32	95	ND	13	3	.07	3.1	3	107	306	2.58	.03	.03	161	74	.01	12	.01	2201	ND	ND	ND	ND	6	ND	ND	838
LB 88-R22	5.9	.22	114	ND	17	ND	.01	2.9	2	50	159	3.12	.03	.01	49	32	.01	11	.01	2984	ND	ND	ND	ND	2	ND	ND	623
LB 88-R23	10.6	.32	141	ND	25	9	.01	1.3	2	63	110	2.33	.03	.01	40	16	.01	8	.01	3981	ND	ND	ND	ND	1	ND	ND	384
LB 88-R24	3.2	.32	95	ND	27	5	.01	4.1	2	63	127	2.25	.04	.01	51	21	.01	8	.01	1475	ND	ND	ND	ND	1	ND	ND	627
LB 88-R25	.2	.48	15	ND	10	9	.17	2.2	3	23	21	.40	.02	.07	629	4	.01	2	.01	70	ND	ND	ND	ND	12	ND	ND	144
LB 88-R26	.1	.54	24	ND	9	5	.16	1.6	3	59	77	1.50	.03	.08	159	37	.01	9	.01	45	ND	ND	ND	ND	8	ND	ND	490
LB 88-R51	.2	3.50	ND	ND	21	7	1.35	.5	22	12	50	4.41	.07	1.72	1382	ND	.01	33	.11	2	ND	ND	ND	ND	110	ND	ND	120
LB 88-R52	.2	2.66	ND	ND	54	7	1.06	.5	11	67	26	2.20	.06	.75	815	3	.01	18	.05	10	ND	ND	ND	ND	86	ND	ND	173
LB 88-R53	.6	2.27	ND	ND	63	8	.86	.8	13	43	65	2.40	.06	.68	835	1	.01	18	.05	14	ND	ND	ND	ND	75	ND	ND	162
LB 88-R54	.2	2.00	ND	ND	45	8	.68	.8	10	25	23	2.25	.05	.65	940	ND	.01	12	.05	21	ND	ND	ND	ND	56	ND	ND	178
LB 88-R55	.1	1.33	3	ND	69	8	.35	.3	13	80	22	2.50	.04	.81	785	2	.01	18	.05	14	ND	ND	ND	1	21	ND	ND	53
LB 88-R56	11.8	3.00	ND	ND	62	44	1.45	1.8	16	31	27	3.75	.08	.63	892	12	.01	23	.03	115	ND	ND	ND	ND	147	ND	ND	274
LB 88-R57	3.1	2.33	ND	ND	68	13	1.82	1.7	12	46	21	2.62	.08	.63	1233	3	.01	16	.04	23	ND	ND	ND	ND	99	ND	ND	249
LB 88-R58	.4	1.62	ND	ND	92	7	1.51	3.1	11	71	42	2.02	.07	.60	956	2	.01	13	.05	13	ND	ND	ND	ND	53	ND	ND	458
LB 88-R59	.2	1.73	ND	ND	49	7	1.20	1.1	11	37	47	2.08	.06	.64	930	ND	.01	15	.04	13	ND	ND	ND	ND	64	ND	ND	144
LB 88-R60	36.7	2.50	ND	ND	54	118	1.06	1.8	15	16	40	2.52	.06	.56	862	3	.01	17	.04	156	ND	ND	ND	ND	91	ND	ND	314
LB 88-R61	36.7	2.99	ND	ND	50	124	1.29	2.9	16	39	32	2.95	.07	.63	845	6	.01	17	.03	192	ND	ND	ND	ND	129	ND	ND	432
LB 88-R62	15.3	1.89	ND	ND	55	43	.61	1.1	14	30	28	2.79	.05	.91	906	1	.01	20	.05	78	ND	ND	ND	ND	54	ND	ND	189
LB 88-R63	12.5	2.58	ND	ND	63	60	.94	1.1	13	52	30	2.70	.06	.81	970	2	.01	17	.05	69	ND	ND	ND	ND	160	ND	ND	259
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

CLIENT: ASHWORTH EXPL. LTD. JOB#: 880249 PROJECT: 192 REPORT: 880249PA DATE: 88/03/11

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
LB 88-R 64	31.1	1.69	7	ND	53	127	.63	2.7	9	44	38	2.17	.06	.46	583	4	.01	15	.04	142	ND	ND	ND	ND	45	ND	ND	480
LB 88-R 65	52.4	1.82	8	ND	45	207	.69	3.0	10	57	26	2.16	.05	.47	585	4	.01	15	.03	193	ND	ND	ND	ND	51	ND	ND	543
LB 88-R 66	17.6	2.19	4	ND	53	100	.92	1.8	9	25	64	2.19	.06	.45	611	5	.01	11	.05	87	ND	ND	ND	ND	85	ND	ND	338
LB 88-R 67	1.2	1.52	5	ND	57	4	.40	.9	10	73	44	2.37	.05	.77	737	3	.01	16	.05	18	ND	ND	ND	ND	27	ND	ND	160
LB 88-R 68	58.6	1.72	5	ND	83	163	.49	1.9	13	29	45	2.98	.05	.60	892	6	.01	17	.04	280	ND	ND	ND	ND	39	ND	ND	260
LB 88-R 69	36.7	1.43	7	ND	94	212	.69	1.9	9	44	35	2.53	.06	.57	752	6	.01	14	.03	156	ND	ND	ND	ND	26	ND	ND	285
LB 88-R 70	>100	1.73	4	ND	47	614	.63	1.7	19	29	74	3.79	.06	.38	667	18	.01	20	.02	558	ND	ND	ND	ND	49	ND	ND	277
LB 88-R 71	1.3	1.79	7	ND	43	7	.58	1.0	9	53	35	2.25	.05	.80	841	1	.01	15	.05	16	ND	ND	ND	ND	43	ND	ND	200
LB 88-R 72	>100	1.31	5	ND	71	859	.27	.8	7	55	37	5.09	.05	.39	493	22	.01	24	.01	1221	ND	ND	ND	ND	23	ND	ND	170
LB 88-R 73	>100	1.23	10	ND	42	360	.31	1.0	11	36	28	3.16	.04	.38	609	7	.01	16	.01	564	ND	ND	ND	ND	24	ND	ND	248
LB 88-R 74	1.3	1.74	6	ND	15	5	1.70	.3	9	42	11	2.17	.07	.74	602	ND	.01	15	.04	13	ND	ND	ND	ND	59	ND	ND	50
LB 88-R 75	1.2	1.37	11	ND	56	ND	.26	.8	11	58	44	2.18	.05	.57	831	3	.01	17	.05	58	ND	ND	ND	ND	16	ND	ND	137
LB 88-R 76	>100	.24	30	ND	6	1031	.01	1.1	1	130	957	3.43	.03	.03	70	44	.01	18	.01	1768	ND	ND	ND	ND	3	ND	ND	229
LB 88-R 77	>100	.57	49	ND	2	1078	.45	59.8	3	81	11790	3.37	.04	.10	300	77	.01	17	.01	16221	ND	ND	4	ND	8	ND	ND	6424
LB 88-R 78	34.2	.29	66	ND	4	796	.02	236.4	6	128	8269	5.80	.04	.05	179	27	.01	32	.01	484	ND	ND	ND	ND	ND	ND	34	23227
LB 88-R 79	92.2	.45	21	ND	2	378	1.29	72.2	9	68	6534	2.82	.06	.07	436	25	.01	14	.01	827	ND	ND	ND	ND	21	ND	ND	8584
LB 88-R 80	68.5	.84	39	ND	29	269	.38	71.8	4	111	5634	3.21	.05	.18	578	38	.01	20	.01	805	ND	ND	ND	ND	8	ND	ND	9580
LB 88-R 81	83.1	.41	26	ND	5	178	.40	25.1	3	65	2353	1.80	.04	.09	233	34	.01	9	.01	1690	ND	ND	ND	ND	9	ND	ND	4285
LB 88-R 82	>100	.42	19	ND	5	378	.58	16.0	5	64	1763	2.01	.04	.11	269	34	.01	10	.01	2392	ND	ND	ND	ND	12	ND	ND	2533
LB 88-R 83	27.9	.74	10	ND	51	115	1.37	5.9	4	36	1396	1.82	.07	.15	337	25	.01	9	.04	543	ND	ND	ND	ND	26	ND	ND	883
LB 88-R 84	19.2	.78	26	ND	32	48	2.29	6.0	4	75	800	2.06	.08	.23	937	12	.01	15	.03	277	ND	ND	ND	ND	35	ND	ND	652
LB 88-R 85	2.4	1.24	44	ND	34	3	.84	4.8	7	34	408	3.34	.08	.40	743	15	.01	19	.04	98	ND	ND	ND	ND	14	ND	ND	574
LB 88-R 86	3.1	.47	16	ND	29	4	.32	2.2	4	38	298	1.26	.04	.09	190	7	.01	9	.03	142	ND	ND	ND	ND	6	ND	ND	376
LB 88-R 87	9.3	.84	20	ND	37	20	3.79	3.6	12	66	773	2.21	.10	.21	1494	9	.01	12	.03	207	ND	ND	ND	ND	54	ND	ND	408
LB 88-R 88	8.8	.46	9	ND	22	38	.76	24.2	1	87	481	.70	.05	.10	430	126	.01	5	.01	170	ND	ND	ND	ND	13	ND	ND	3182
LB 88-R 89	67.5	.58	29	ND	21	869	.17	199.7	5	123	14747	4.39	.05	.13	362	25	.01	25	.01	645	ND	ND	ND	ND	3	ND	12	18783
LB 88-R 90	7.6	.42	13	ND	27	51	.64	13.2	3	43	253	1.02	.05	.10	325	12	.01	5	.02	143	ND	ND	ND	ND	10	ND	ND	1883
LB 88-R 91	>100	.62	16	ND	23	887	.71	30.2	6	105	2173	1.90	.05	.13	382	32	.01	11	.01	1776	ND	ND	ND	ND	13	ND	ND	3590
LB 88-R 92	>100	.47	16	ND	19	208	.66	10.9	3	88	288	1.22	.05	.10	354	32	.01	7	.01	1434	ND	ND	ND	ND	11	ND	5	1594
LB 88-R 93	32.9	.60	15	ND	35	52	1.17	24.7	2	39	1297	.99	.06	.12	609	345	.01	7	.03	1660	ND	ND	ND	ND	20	ND	ND	4061
LB 88-R 94	4.6	.71	25	ND	42	15	.44	11.9	4	34	466	2.16	.05	.17	331	12	.01	13	.04	292	ND	ND	ND	ND	6	ND	ND	1283
LB 88-R 95	10.1	.57	12	ND	27	21	.99	2.6	2	101	60	1.02	.06	.12	287	5	.01	5	.02	164	ND	ND	ND	ND	16	ND	ND	421
LB 88-R 96	32.7	1.14	65	ND	21	239	1.36	5.1	13	32	622	7.04	.10	.25	729	4	.01	35	.04	491	ND	ND	ND	ND	34	ND	ND	955
LB 88-R 97	>100	.43	65	ND	7	583	.69	259.9	9	107	3425	3.61	.06	.08	309	16	.01	21	.01	779	ND	ND	ND	ND	9	ND	75	27856
LB 88-R 98	83.7	.60	45	ND	18	393	.75	140.9	6	83	2038	2.77	.06	.14	341	11	.01	17	.01	676	ND	ND	ND	ND	12	ND	17	16538
LB 88-R 99	81.6	1.42	21	ND	34	315	1.39	35.5	29	54	2019	5.66	.10	.53	719	32	.01	27	.03	1632	ND	ND	ND	ND	26	ND	ND	5613
LB 88-R 100	13.5	.93	8	ND	39	58	2.03	32.3	3	47	586	1.61	.08	.28	776	15	.01	10	.03	195	ND	ND	ND	ND	48	ND	ND	4061
LB 88-R 101	2.2	.22	24	ND	21	5	.03	1.2	3	183	274	1.27	.03	.04	129	15	.01	11	.01	74	ND	ND	ND	ND	3	ND	ND	161
LB 88-R 102	3.4	.14	12	ND	32	80	.01	.4	1	73	26	1.39	.03	.02	49	22	.01	7	.01	101	ND	ND	ND	ND	3	ND	ND	70
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

CLIENT: ASHWORTH EXPL. LTD. JOB#: 880249 PROJECT: 192 REPORT: 880249PA DATE: 88/03/11

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
LB 88-R 103	5.7	.78	5	ND	58	33	.23	.6	6	111	77	2.72	.05	.46	327	15	.01	18	.03	70	ND	ND	ND	ND	10	ND	ND	128
LB 88-R 104	2.2	.15	5	ND	30	256	.02	.2	1	82	64	2.40	.03	.04	56	14	.01	12	.01	42	ND	ND	ND	ND	4	ND	ND	31
LB 88-R 105	.4	2.06	7	ND	36	4	.52	.5	13	44	26	2.97	.06	1.14	817	3	.01	24	.06	9	ND	ND	ND	ND	50	ND	ND	97
LB 88-R 106	.7	1.26	8	ND	36	4	.71	1.7	8	54	119	1.93	.06	.60	676	3	.01	15	.04	22	ND	ND	ND	ND	19	ND	ND	397
LB 88-R 107	.4	1.43	5	ND	28	ND	.83	1.2	10	33	84	2.34	.06	.79	692	1	.01	17	.05	14	ND	ND	ND	ND	32	ND	ND	281
LB 88-R 108	23.8	.77	11	ND	24	153	1.15	101.2	7	67	1354	1.97	.06	.19	396	19	.01	13	.02	199	ND	ND	ND	ND	27	ND	5	12598
LB 88-R 109	10.3	.78	6	ND	26	45	3.07	14.4	4	32	183	1.25	.09	.30	463	3	.01	10	.02	116	ND	ND	ND	ND	39	ND	ND	1770
LB 88-R 110	>100	.08	28	ND	8	228	.24	2.3	13	140	163	4.36	.04	.02	262	8	.01	20	.01	2613	ND	ND	ND	ND	9	ND	ND	185
LB 88-P 1	27.5	.38	89	ND	13	ND	.03	69.3	23	82	440	4.06	.03	.08	409	16	.01	23	.01	22831	ND	ND	22	ND	19	ND	11	15843
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

VGC

VANGEOCHEM LAB LIMITED

MAIN OFFICE
1521 PEMBERTON AVE.
NORTH VANCOUVER, B.C. V7P 2S3
(604) 986-5211 TELEX: 04-352578

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

GEOCHEMICAL ANALYTICAL REPORT

CLIENT: ASHWORTH EXPLORATION LTD.
ADDRESS: Mez. Floor, 744 W. Hastings St.
: Vancouver, B.C.
: V6C 1A5

DATE: Mar 09 1988
REPORT#: 880248 GA
JOB#: 880248

PROJECT#: 192
SAMPLES ARRIVED: Feb 24 1988
REPORT COMPLETED: Mar 09 1988
ANALYSED FOR: Au ICP

INVOICE#: 880248 NA
TOTAL SAMPLES: 525
SAMPLE TYPE: 525 Soil
REJECTS: DISCARDED

SAMPLES FROM: Submitted by Mr. P. Leriche.
COPY SENT TO: All copies sent to Vancouver office.

PREPARED FOR: Mr. Peter Leriche

ANALYSED BY: VGC Staff

SIGNED: _____

GENERAL REMARK: Data disk sent to Mr. Tony Clark.

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SAMPLE #	Au ppb
L 5+00W 0+00 BL	nd
L 5+00W 0+25N	nd
L 5+00W 0+50N	5
L 5+00W 0+75N	15
L 5+00W 1+00N	nd
L 5+00W 1+25N	nd
L 5+00W 1+50N	nd
L 5+00W 1+75N	nd
L 5+00W 2+00N	5
L 5+00W 2+50N	5
L 5+00W 3+00N	nd
L 5+00W 3+50N	nd
L 5+00W 4+00N	5
L 5+00W 4+50N	nd
L 5+00W 5+00N	10
L 5+00W 5+50N	nd
L 5+00W 6+00N	10
L 5+00W 6+50N	nd
L 5+00W 7+00N	nd
L 5+00W 7+50N	10
L 5+00W 8+00N	10
L 5+00W 0+25S	20
L 5+00W 0+50S	30
L 5+00W 0+75S	10
L 5+00W 1+00S	nd
L 5+00W 1+25S	15
L 5+00W 1+50S	5
L 5+00W 1+75S	5
L 5+00W 2+00S	nd
L 5+00W 2+25S	nd
L 5+00W 2+50S	nd
L 5+00W 2+75S	nd
L 5+00W 3+00S	nd
L 5+00W 3+50S	nd
L 5+00W 4+00S	nd
L 5+00W 4+50S	10
L 5+00W 5+00S	5
L 5+00W 5+50S	nd
L 5+00W 6+00S	nd
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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SAMPLE #	Au ppb
L 5+00W 6+50S	10
L 5+00W 7+00S	nd
L 5+00W 7+50S	nd
L 5+00W 8+00S	nd
L 6+00W 0+00 BL	5
L 6+00W 0+25N	nd
L 6+00W 0+50N	nd
L 6+00W 0+75N	nd
L 6+00W 1+00N	nd
L 6+00W 1+25N	10
L 6+00W 1+50N	nd
L 6+00W 1+75N	15
L 6+00W 2+00N	nd
L 6+00W 2+50N	nd
L 6+00W 3+00N	10
L 6+00W 3+50N	nd
L 6+00W 4+00N	15
L 6+00W 4+50N	nd
L 6+00W 5+00N	nd
L 6+00W 5+50N	nd
L 6+00W 6+00N	15
L 6+00W 6+50N	nd
L 6+00W 7+00N	nd
L 6+00W 7+50N	15
L 6+00W 8+00N	nd
L 6+00W 0+25S	nd
L 6+00W 0+50S	nd
L 6+00W 0+75S	15
L 6+00W 1+00S	nd
L 6+00W 1+25S	5
L 6+00W 1+50S	nd
L 6+00W 1+75S	nd
L 6+00W 2+00S	nd
L 6+00W 2+25S	5
L 6+00W 2+50S	5
L 6+00W 2+75S	10
L 6+00W 3+00S	nd
L 6+00W 3+50S	nd
L 6+00W 4+00S	5
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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SAMPLE #	Au ppb
L 6+00W 4+50S	nd
L 6+00W 5+00S	10
L 6+00W 5+50S	nd
L 6+00W 6+00S	nd
L 6+00W 6+50S	nd
L 6+00W 7+00S	nd
L 6+00W 7+50S	nd
L 6+00W 8+00S	nd
L 7+00W 0+25N	nd
L 7+00W 0+50N	5
L 7+00W 0+75N	nd
L 7+00W 1+00N	nd
L 7+00W 1+25N	nd
L 7+00W 1+50N	5
L 7+00W 1+75N	nd
L 7+00W 2+00N	nd
L 7+00W 2+50N	5
L 7+00W 3+00N	nd
L 7+00W 3+50N	nd
L 7+00W 4+00N	nd
L 7+00W 4+50N	nd
L 7+00W 5+00N	10
L 7+00W 5+50N	10
L 7+00W 6+00N	5
L 7+00W 6+50N	10
L 7+00W 7+00N	nd
L 7+00W 7+50N	nd
L 7+00W 8+00N	nd
L 7+00W 0+25S	nd
L 7+00W 0+50S	10
L 7+00W 0+75S	10
L 7+00W 1+00S	5
L 7+00W 1+25S	nd
L 7+00W 1+50S	10
L 7+00W 1+75S	nd
L 7+00W 2+00S	nd
L 7+00W 2+25S	10
L 7+00W 2+50S	nd
L 7+00W 2+75S	5
DETECTION LIMIT	5

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SAMPLE #	Au ppb
L 7+00W 3+00S	nd
L 7+00W 3+50S	nd
L 7+00W 4+00S	nd
L 7+00W 4+50S	5
L 7+00W 5+00S	nd
L 7+00W 5+50S	5
L 7+00W 6+00S	nd
L 7+00W 6+50S	nd
L 7+00W 7+00S	nd
L 7+00W 7+50S	nd
L 7+00W 8+00S	nd
L 7+50W 0+00 BL	5
L 7+50W 0+25N	nd
L 7+50W 0+50N	nd
L 7+50W 0+75N	nd
L 7+50W 1+00N	nd
L 7+50W 1+25N	5
L 7+50W 1+50N	nd
L 7+50W 0+25S	nd
L 7+50W 0+50S	nd
L 7+50W 0+75S	nd
L 7+50W 1+00S	nd
L 7+50W 1+25S	nd
L 7+50W 1+50S	nd
L 7+50W 1+75S	nd
L 7+50W 2+00S	nd
L 7+50W 2+25S	nd
L 7+50W 2+50S	nd
L 7+50W 2+75S	nd
L 7+50W 3+00S	nd
L 7+50W 3+25S	nd
L 7+50W 3+50S	nd
L 7+50W 3+75S	nd
L 7+50W 4+00S	nd
L 7+50W 4+25S	nd
L 7+50W 4+50S	nd
L 7+50W 4+75S	nd
L 7+50W 5+00S	nd
L 8+00W 0+00 BL	nd
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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SAMPLE #	Au ppb
L 8+00W 0+50N	10
L 8+00W 1+00N	5
L 8+00W 1+50N	15
L 8+00W 2+00N	15
L 8+00W 2+50N	5
L 8+00W 3+00N	5
L 8+00W 3+50N	nd
L 8+00W 4+00N	5
L 8+00W 4+50N	10
L 8+00W 5+00N	nd
L 8+00W 5+50N	nd
L 8+00W 6+00N	5
L 8+00W 6+50N	nd
L 8+00W 7+00N	nd
L 8+00W 7+50N	5
L 8+00W 8+00N	5
L 8+00W 0+25S	nd
L 8+00W 0+50S	nd
L 8+00W 0+75S	nd
L 8+00W 1+00S	nd
L 8+00W 1+25S	5
L 8+00W 1+50S	nd
L 8+00W 1+75S	nd
L 8+00W 2+00S	5
L 8+00W 2+25S	5
L 8+00W 2+50S	15
L 8+00W 2+75S	15
L 8+00W 3+00S	5
L 8+00W 3+25S	nd
L 8+00W 3+50S	nd
L 8+00W 3+75S	5
L 8+00W 4+00S	nd
L 8+00W 4+25S	nd
L 8+00W 4+50S	nd
L 8+00W 4+75S	10
L 8+00W 5+00S	10
L 8+00W 5+50S	nd
L 8+00W 6+00S	5
L 8+00W 6+50S	nd
DETECTION LIMIT	5

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SAMPLE #	Au ppb
L 8+00W 7+00S	nd
L 8+00W 7+50S	10
L 8+00W 8+00S	5
L 8+50W 0+00 BL	5
L 8+50W 0+25N	nd
L 8+50W 0+50N	nd
L 8+50W 0+75N	nd
L 8+50W 1+00N	35
L 8+50W 1+25N	20
L 8+50W 1+50N	5
L 8+50W 0+25S	nd
L 8+50W 0+50S	nd
L 8+50W 0+75S	10
L 8+50W 1+00S	15
L 8+50W 1+25S	15
L 8+50W 1+50S	5
L 8+50W 1+75S	5
L 8+50W 2+00S	nd
L 8+50W 2+25S	5
L 8+50W 2+50S	15
L 8+50W 2+75S	nd
L 8+50W 3+00S	nd
L 8+50W 3+25S	10
L 8+50W 3+50S	nd
L 8+50W 3+75S	10
L 8+50W 4+00S	5
L 8+50W 4+25S	5
L 8+50W 4+50S	5
L 8+50W 4+75S	nd
L 8+50W 5+00S	nd
L 9+00W 0+00 BL	nd
L 9+00W 0+50N	5
L 9+00W 1+00N	10
L 9+00W 1+50N	10
L 9+00W 2+00N	5
L 9+00W 2+50N	5
L 9+00W 3+00N	5
L 9+00W 3+50N	10
L 9+00W 4+00N	nd
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Au ppb
L 9+00W 4+50N	nd
L 9+00W 5+00N	nd
L 9+00W 5+50N	5
L 9+00W 6+00N	nd
L 9+00W 6+50N	nd
L 9+00W 7+00N	nd
L 9+00W 7+50N	5
L 9+00W 8+00N	nd
L 9+00W 0+25S	nd
L 9+00W 0+50S	5
L 9+00W 0+75S	nd
L 9+00W 1+00S	nd
L 9+00W 1+25S	10
L 9+00W 1+50S	nd
L 9+00W 1+75S	nd
L 9+00W 2+00S	nd
L 9+00W 2+25S	nd
L 9+00W 2+50S	5
L 9+00W 2+75S	nd
L 9+00W 3+00S	nd
L 9+00W 3+25S	nd
L 9+00W 3+50S	nd
L 9+00W 3+75S	nd
L 9+00W 4+00S	nd
L 9+00W 4+25S	nd
L 9+00W 4+50S	nd
L 9+00W 4+75S	nd
L 9+00W 5+00S	5
L 9+00W 5+50S	nd
L 9+00W 6+00S	nd
L 9+00W 6+50S	nd
L 9+00W 7+00S	5
L 9+00W 7+50S	5
L 9+00W 8+00S	5
L 9+50W 0+00 BL	nd
L 9+50W 0+25N	nd
L 9+50W 0+50N	nd
L 9+50W 0+75N	nd
L 9+50W 1+00N	5
DETECTION LIMIT	5

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SAMPLE #	Au ppb
L 9+50W 1+25N	nd
L 9+50W 1+50N	5
L 9+50W 0+25S	10
L 9+50W 0+50S	nd
L 9+50W 0+75S	nd
L 9+50W 1+00S	15
L 9+50W 1+25S	5
L 9+50W 1+50S	5
L 9+50W 1+75S	nd
L 9+50W 2+00S	5
L 9+50W 2+25S	5
L 9+50W 2+50S	20
L 9+50W 2+75S	5
L 9+50W 3+00S	nd
L 9+50W 3+25S	nd
L 9+50W 3+50S	5
L 9+50W 3+75S	5
L 9+50W 4+00S	5
L 9+50W 4+25S	nd
L 9+50W 4+50S	nd
L 9+50W 4+75S	5
L 9+50W 5+00S	5
L10+00W 0+00 BL	5
L10+00W 0+50N	nd
L10+00W 1+00N	10
L10+00W 1+50N	nd
L10+00W 2+00N	5
L10+00W 2+50N	10
L10+00W 3+00N	nd
L10+00W 3+50N	10
L10+00W 4+00N	10
L10+00W 4+50N	10
L10+00W 5+00N	10
L10+00W 5+50N	nd
L10+00W 6+00N	nd
L10+00W 6+50N	nd
L10+00W 7+00N	5
L10+00W 7+50N	10
L10+00W 8+00N	10
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

MAIN OFFICE
1521 PEMBERTON AVE.
NORTH VANCOUVER, B.C. V7P 2S3
(604) 986-5211 TELEX: 04-352578

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Au ppb
L10+00W 0+25S	nd
L10+00W 0+50S	10
L10+00W 0+75S	5
L10+00W 1+00S	nd
L10+00W 1+25S	nd
L10+00W 1+50S	nd
L10+00W 1+75S	nd
L10+00W 2+00S	nd
L10+00W 2+25S	5
L10+00W 2+50S	nd
L10+00W 2+75S	5
L10+00W 3+00S	nd
L10+00W 3+25S	10
L10+00W 3+50S	nd
L10+00W 3+75S	5
L10+00W 4+00S	5
L10+00W 4+25S	nd
L10+00W 4+50S	nd
L10+00W 4+75S	nd
L10+00W 5+00S	nd
L10+00W 5+50S	nd
L10+00W 6+00S	nd
L10+00W 6+50S	nd
L10+00W 7+00S	5
L10+00W 7+50S	5
L10+00W 8+00S	nd
L10+50W 0+00 BL	nd
L10+50W 0+25N	nd
L10+50W 0+50N	10
L10+50W 0+75N	nd
L10+50W 1+00N	nd
L10+50W 1+25N	nd
L10+50W 1+50N	nd
L10+50W 0+25S	nd
L10+50W 0+50S	nd
L10+50W 0+75S	10
L10+50W 1+00S	5
L10+50W 1+25S	5
L10+50W 1+50S	5
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Au ppb
L10+50W 1+75S	5
L10+50W 2+00S	10
L10+50W 2+25S	nd
L10+50W 2+50S	5
L10+50W 2+75S	5
L10+50W 3+00S	nd
L10+50W 3+25S	5
L10+50W 3+50S	5
L10+50W 3+75S	5
L10+50W 4+00S	10
L10+50W 4+25S	nd
L10+50W 4+50S	10
L10+50W 4+75S	10
L10+50W 5+00S	15
L11+00W 0+00 BL	5
L11+00W 0+50N	10
L11+00W 1+00N	nd
L11+00W 1+50N	10
L11+00W 2+00N	5
L11+00W 2+50N	10
L11+00W 3+00N	nd
L11+00W 4+00N	15
L11+00W 4+50N	5
L11+00W 5+00N	5
L11+00W 5+50N	10
L11+00W 6+00N	45
L11+00W 6+50N	25
L11+00W 7+00N	nd
L11+00W 7+50N	20
L11+00W 8+00N	30
L11+00W 0+25S	nd
L11+00W 0+50S	10
L11+00W 0+75S	nd
L11+00W 1+00S	nd
L11+00W 1+25S	nd
L11+00W 1+50S	nd
L11+00W 1+75S	nd
L11+00W 2+00S	nd
L11+00W 2+25S	nd
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Au ppb
L11+00W 2+50S	nd
L11+00W 2+75S	5
L11+00W 3+00S	nd
L11+00W 3+25S	10
L11+00W 3+50S	nd
L11+00W 3+75S	5
L11+00W 4+00S	nd
L11+00W 4+25S	10
L11+00W 4+50S	5
L11+00W 4+75S	nd
L11+00W 5+00S	nd
L11+00W 5+50S	15
L11+00W 6+00S	10
L12+00W 0+00 BL	5
L12+00W 0+50N	10
L12+00W 1+00N	10
L12+00W 1+50N	5
L12+00W 2+00N	nd
L12+00W 2+50N	5
L12+00W 3+00N	nd
L12+00W 3+50N	5
L12+00W 4+00N	nd
L12+00W 4+50N	10
L12+00W 5+00N	5
L12+00W 5+50N	nd
L12+00W 6+00N	10
L12+00W 6+50N	10
L12+00W 7+00N	5
L12+00W 7+50N	5
L12+00W 8+00N	10
L12+00W 0+25S	nd
L12+00W 0+50S	nd
L12+00W 0+75S	nd
L12+00W 1+00S	5
L12+00W 1+25S	nd
L12+00W 1+50S	nd
L12+00W 1+75S	nd
L12+00W 2+00S	nd
L12+00W 2+25S	nd
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

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(604) 251-5656

SAMPLE #	Au ppb
L12+00W 2+50S	5
L12+00W 2+75S	nd
L12+00W 3+00S	5
L12+00W 3+25S	nd
L12+00W 3+50S	5
L12+00W 3+75S	5
L12+00W 4+00S	5
L12+00W 4+25S	nd
L12+00W 4+50S	5
L12+00W 4+75S	nd
L12+00W 5+00S	10
L12+00W 5+50S	nd
L12+00W 6+00S	nd
L13+00W 0+00 BL	5
L13+00W 0+50N	nd
L13+00W 1+00N	25
L13+00W 1+50N	nd
L13+00W 2+00N	5
L13+00W 2+50N	10
L13+00W 3+00N	nd
L13+00W 3+50N	nd
L13+00W 4+00N	10
L13+00W 4+50N	10
L13+00W 5+00N	15
L13+00W 5+50N	10
L13+00W 6+00N	nd
L13+00W 6+50N	nd
L13+00W 7+00N	nd
L13+00W 7+50N	nd
L13+00W 8+00N	nd
L13+00W 0+50S	15
L13+00W 1+00S	nd
L13+00W 1+50S	nd
L13+00W 2+00S	5
L13+00W 2+50S	10
L13+00W 3+00S	5
L13+00W 3+50S	nd
L13+00W 4+00S	5
L13+00W 4+50S	10
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

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VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #	Au ppb
L13+00W 5+00S	nd
L14+00W 0+00 BL	nd
L14+00W 0+50N	15
L14+00W 1+00N	10
L14+00W 1+50N	5
L14+00W 2+00N	nd
L14+00W 2+50N	nd
L14+00W 3+00N	nd
L14+00W 3+50N	nd
L14+00W 4+00N	5
L14+00W 4+50N	nd
L14+00W 5+00N	10
L14+00W 5+50N	5
L14+00W 6+00N	20
L14+00W 6+50N	10
L14+00W 7+00N	5
L14+00W 7+50N	nd
L14+00W 8+00N	nd
L14+00W 0+50S	nd
L14+00W 1+00S	nd
L14+00W 1+50S	nd
L14+00W 2+00S	nd
L14+00W 2+50S	nd
L14+00W 3+00S	nd
L14+00W 3+50S	5
L14+00W 4+00S	nd
L14+00W 4+50S	nd
L14+00W 5+00S	nd
L15+00W 0+00 BL	nd
L15+00W 0+50N	nd
L15+00W 1+00N	nd
L15+00W 1+50N	nd
L15+00W 2+00N	nd
L15+00W 2+50N	nd
L15+00W 3+00N	nd
L15+00W 3+50N	10
L15+00W 4+00N	5
L15+00W 4+50N	5
L15+00W 5+00N	5
DETECTION LIMIT	5

nd = none detected -- = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

MAIN OFFICE
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NORTH VANCOUVER, B.C. V7P 2S3
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BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

SAMPLE #		Au ppb
L15+00W	5+50N	10
L15+00W	6+00N	nd
L15+00W	6+50N	5
L15+00W	7+00N	10
L15+00W	7+50N	nd
L15+00W	8+00N	nd
L15+00W	0+50S	nd
L15+00W	1+00S	5
L15+00W	1+50S	10
L15+00W	2+00S	5
L15+00W	2+50S	5
L15+00W	3+00S	5
L15+00W	3+50S	10
L15+00W	4+00S	nd
L15+00W	4+50S	nd
L15+00W	5+00S	15
L15+00W	5+50S	10
L15+00W	6+00S	15

DETECTION LIMIT 5
nd = none detected -- = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

MAIN OFFICE: 1521 PEMBERTON AVE. N.VANCOUVER B.C. V7P 2S3 PH:(604)986-5211 TELEX:04-352578
BRANCH OFFICE: 1630 PANDORA ST. VANCOUVER B.C. V5L 1L6 PH:(604)251-5656

ICAP GEOCHEMICAL ANALYSIS

A .5 GRAM SAMPLE IS DIGESTED WITH 5 ML OF 3:1:2 HCL TO HNO3 TO H2O AT 95 DEG. C FOR 90 MINUTES AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR SN,MN,FE,CA,P,CR,MG,BA,PD,AL,NA,K,W,PT AND SR. AU AND PD DETECTION IS 3 PPM.
IS= INSUFFICIENT SAMPLE, ND= NOT DETECTED, -= NOT ANALYZED

COMPANY: ASHWORTH EXPL LTD
ATTENTION:
PROJECT: 192

REPORT#: 880248PA
JOB#: 880248
INVOICE#: 880248NA

DATE RECEIVED: 88/02/24
DATE COMPLETED: 88/03/10
COPY SENT TO: P LERICHE

ANALYST

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 5+00N 0+00BL	.1	2.25	4	ND	240	ND	.20	.1	7	5	10	1.66	.04	.28	636	2	.01	15	.12	13	ND	ND	ND	ND	23	ND	ND	139
L 5+00N 0+25N	.1	1.83	7	ND	146	ND	.17	.1	7	5	8	1.70	.04	.26	374	2	.01	14	.10	12	ND	ND	ND	ND	17	ND	ND	104
L 5+00N 0+50N	.1	2.06	7	ND	142	ND	.24	.1	7	5	13	1.76	.04	.34	641	1	.01	13	.14	11	ND	ND	ND	ND	30	ND	ND	98
L 5+00N 0+75N	.1	2.00	4	ND	120	ND	.24	.1	8	5	18	1.91	.04	.34	392	1	.01	12	.05	8	ND	ND	ND	ND	24	ND	ND	77
L 5+00N 1+00N	.1	1.53	3	ND	134	ND	.25	.1	6	4	7	1.52	.05	.28	414	1	.01	15	.12	12	ND	ND	ND	ND	28	ND	ND	143
L 5+00N 1+25N	.1	1.41	4	ND	220	ND	.20	.1	6	4	6	1.39	.04	.26	1085	1	.01	11	.13	16	ND	ND	ND	ND	24	ND	ND	131
L 5+00N 1+50N	.1	1.35	3	ND	156	ND	.34	.1	7	5	10	1.73	.04	.39	1056	1	.01	12	.06	17	ND	ND	ND	ND	31	ND	ND	124
L 5+00N 1+75N	.1	1.41	ND	ND	242	ND	.34	.4	5	4	5	1.33	.03	.29	1475	1	.01	11	.05	16	ND	ND	ND	ND	30	ND	ND	188
L 5+00N 2+00N	.1	2.66	13	ND	166	ND	.25	.2	9	6	33	2.20	.04	.44	558	1	.01	20	.16	15	ND	ND	ND	ND	28	ND	ND	153
L 5+00N 2+50N	1.7	1.64	18	ND	95	ND	.15	.4	7	3	16	1.37	.11	.29	386	2	.01	15	.10	21	ND	ND	3	ND	15	ND	ND	116
L 5+00N 3+00N	.2	2.25	10	ND	162	ND	.32	.2	8	5	24	1.86	.05	.39	773	2	.01	16	.15	16	ND	ND	ND	ND	34	ND	ND	161
L 5+00N 3+50N	.1	1.98	6	ND	169	ND	.27	.1	8	5	14	1.92	.04	.44	640	1	.01	17	.05	17	ND	ND	ND	ND	29	ND	ND	136
L 5+00N 4+00N	.1	2.04	6	ND	169	ND	.27	.1	8	5	14	1.97	.04	.44	630	2	.01	16	.05	15	ND	ND	ND	ND	29	ND	ND	140
L 5+00N 4+50N	.1	1.73	ND	ND	199	ND	.26	.2	8	6	15	1.93	.04	.44	1525	1	.01	15	.08	12	ND	ND	ND	ND	21	ND	ND	187
L 5+00N 5+00N	.2	2.22	19	ND	88	ND	.39	.2	10	10	41	2.74	.05	.70	461	1	.01	23	.06	14	ND	ND	ND	ND	36	ND	ND	115
L 5+00N 5+50N	.2	2.12	4	ND	183	ND	.30	.3	9	6	13	2.02	.04	.41	812	2	.01	17	.15	10	ND	ND	ND	ND	36	ND	ND	148
L 5+00N 6+00N	.2	2.95	5	ND	107	ND	.46	.3	11	7	47	2.67	.06	.56	586	1	.01	20	.04	6	ND	ND	ND	ND	47	ND	ND	99
L 5+00N 6+50N	.2	2.95	ND	ND	107	ND	.45	.3	12	6	46	2.70	.06	.68	589	1	.01	20	.04	5	ND	ND	ND	ND	46	ND	ND	102
L 5+00N 7+00N	.3	2.27	6	ND	140	ND	.26	.3	10	7	15	2.24	.05	.46	629	1	.01	18	.08	10	ND	ND	ND	ND	29	ND	ND	137
L 5+00N 7+50N	.2	2.16	6	ND	97	ND	.36	.2	9	6	11	2.40	.05	.55	534	1	.01	17	.06	8	ND	ND	ND	ND	36	ND	ND	115
L 5+00N 8+00N	.1	2.13	ND	ND	82	ND	.45	.3	11	8	15	2.68	.06	.63	554	1	.01	19	.07	8	ND	ND	ND	ND	44	ND	ND	104
L 5+00N 0+25S	.3	2.58	5	ND	224	ND	.24	.3	9	6	36	1.88	.05	.34	532	1	.01	17	.14	12	ND	ND	ND	ND	27	ND	ND	168
L 5+00N 0+50S	.2	1.91	4	ND	201	ND	.25	.2	7	6	6	1.72	.04	.30	983	2	.01	15	.11	12	ND	ND	ND	ND	25	ND	ND	195
L 5+00N 0+75S	.1	2.22	4	ND	173	ND	.26	.3	7	5	20	1.68	.04	.29	703	1	.01	15	.17	8	ND	ND	ND	ND	28	ND	ND	131
L 5+00N 1+00S	.1	1.67	4	ND	206	ND	.17	.1	6	5	ND	1.58	.03	.24	629	1	.01	14	.16	8	ND	ND	ND	ND	17	ND	ND	141
L 5+00N 1+25S	.2	2.09	4	ND	174	ND	.19	.1	7	6	5	1.70	.04	.25	565	1	.01	16	.15	10	ND	ND	ND	ND	20	ND	ND	113
L 5+00N 1+50S	.2	1.79	ND	ND	176	ND	.17	.1	6	5	3	1.58	.04	.24	482	1	.01	11	.15	9	ND	ND	ND	ND	19	ND	ND	94
L 5+00N 1+75S	.1	2.07	ND	ND	150	ND	.19	.1	7	5	4	1.68	.04	.28	412	1	.01	13	.13	8	ND	ND	ND	ND	21	ND	ND	77
L 5+00N 2+00S	.1	2.34	ND	ND	137	ND	.34	.1	7	4	6	1.75	.05	.32	694	1	.01	12	.05	6	ND	ND	ND	ND	28	ND	ND	71
L 5+00N 2+25S	.2	2.25	3	ND	136	ND	.19	.1	7	5	3	1.72	.04	.29	434	1	.01	13	.12	7	ND	ND	ND	ND	22	ND	ND	82
L 5+00N 2+50S	.2	2.25	ND	ND	148	ND	.24	.1	7	5	3	1.76	.04	.32	538	1	.01	12	.13	9	ND	ND	ND	ND	27	ND	ND	97
L 5+00N 2+75S	.2	2.16	ND	ND	180	ND	.25	.1	7	4	3	1.62	.04	.29	637	1	.01	14	.14	9	ND	ND	ND	ND	29	ND	ND	89
L 5+00N 3+00S	.1	2.31	ND	ND	208	ND	.29	.1	8	5	4	1.95	.04	.40	619	1	.01	13	.14	7	ND	ND	ND	ND	41	ND	ND	115
L 5+00N 3+50S	.1	2.06	ND	ND	124	3	.32	.1	8	6	5	1.95	.05	.38	535	1	.01	11	.04	9	ND	ND	ND	ND	30	ND	ND	71
L 5+00N 4+00S	.1	2.37	3	ND	192	ND	.30	.1	8	6	16	1.85	.04	.34	695	2	.01	15	.11	11	ND	ND	ND	ND	28	ND	ND	125
L 5+00N 4+50S	.1	2.49	3	ND	222	ND	.20	.1	7	5	6	1.66	.04	.28	653	1	.01	14	.16	8	ND	ND	ND	ND	24	ND	ND	145
L 5+00N 5+00S	.2	2.12	5	ND	196	ND	.24	.1	7	5	13	1.62	.04	.32	665	1	.01	14	.12	9	ND	ND	ND	ND	30	ND	ND	117
L 5+00N 5+50S	.2	2.16	5	ND	206	ND	.26	.2	7	4	22	1.61	.04	.30	646	1	.01	14	.13	8	ND	ND	ND	ND	32	ND	ND	144
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	V PPM	ZN PPM
L 5+00W 6+00S	.2	1.81	3	ND	161	ND	.28	.3	8	5	18	1.86	.04	.40	560	2	.01	15	.05	8	ND	ND	ND	ND	28	ND	ND	113
L 5+00W 6+50S	.1	2.39	3	ND	178	ND	.30	.1	9	7	12	2.20	.04	.46	644	1	.01	17	.11	4	ND	ND	ND	ND	37	ND	ND	97
L 5+00W 7+00S	.1	1.28	4	ND	135	ND	.20	.1	6	5	3	1.81	.03	.38	638	1	.01	12	.05	6	ND	ND	ND	ND	20	ND	ND	89
L 5+00W 7+50S	.1	2.63	6	ND	239	ND	.41	.1	8	6	19	2.04	.04	.38	1014	1	.01	15	.17	4	ND	ND	ND	ND	39	ND	ND	150
L 5+00W 8+00S	.1	2.31	4	ND	154	ND	.22	.2	9	7	14	2.27	.03	.45	526	1	.01	16	.15	3	ND	ND	ND	ND	30	ND	ND	125
L 6+00W 0+00BL	.2	2.08	5	ND	173	ND	.22	.1	7	5	9	1.67	.04	.28	401	1	.01	13	.11	5	ND	ND	ND	ND	32	ND	ND	124
L 6+00W 0+25N	.1	2.06	4	ND	265	ND	.25	.2	6	5	4	1.62	.03	.25	673	1	.01	14	.28	6	ND	ND	ND	ND	40	ND	ND	144
L 6+00W 0+50N	.2	1.92	4	ND	211	ND	.17	.2	7	5	8	1.77	.04	.28	516	1	.01	15	.20	9	ND	ND	ND	ND	23	ND	ND	141
L 6+00W 0+75N	.1	1.85	7	ND	167	ND	.20	.2	6	5	7	1.70	.03	.27	551	1	.01	15	.11	8	ND	ND	ND	ND	25	ND	ND	131
L 6+00W 1+00N	.1	1.92	12	ND	130	ND	.20	.1	6	5	11	1.61	.03	.27	365	1	.01	13	.10	10	ND	ND	ND	ND	22	ND	ND	101
L 6+00W 1+25N	.1	1.46	ND	ND	139	ND	.17	.1	6	4	2	1.60	.03	.27	392	1	.01	12	.08	9	ND	ND	ND	ND	19	ND	ND	114
L 6+00W 1+50N	.1	1.81	10	ND	188	ND	.22	.1	7	6	7	1.58	.04	.28	714	1	.01	16	.13	11	ND	ND	ND	ND	30	ND	ND	122
L 6+00W 1+75N	.1	1.62	4	ND	167	ND	.30	.1	7	7	11	2.36	.04	.40	795	1	.01	15	.08	13	ND	ND	ND	ND	32	ND	ND	135
L 6+00W 2+00N	.1	2.04	6	ND	242	ND	.20	.1	7	5	13	1.85	.04	.34	720	1	.01	15	.20	11	ND	ND	ND	ND	31	ND	ND	165
L 6+00W 2+50N	.1	2.45	5	ND	206	ND	.32	.1	8	6	13	1.91	.04	.43	1064	1	.01	18	.08	13	ND	ND	ND	ND	36	ND	ND	200
L 6+00W 3+00N	.1	2.62	10	ND	287	ND	.22	.4	8	5	10	1.92	.04	.39	1710	2	.01	19	.11	13	ND	ND	ND	ND	28	ND	ND	269
L 6+00W 3+50N	.1	2.54	5	ND	190	ND	.46	.4	11	8	61	2.62	.06	.56	1492	1	.01	22	.06	16	ND	ND	ND	ND	35	ND	ND	158
L 6+00W 4+00N	.1	1.45	4	ND	133	ND	.32	.1	7	5	10	1.81	.04	.43	985	1	.01	12	.05	9	ND	ND	ND	ND	24	ND	ND	133
L 6+00W 4+50N	.1	1.95	7	ND	113	ND	.44	.4	9	7	44	2.23	.05	.48	834	1	.01	18	.05	14	ND	ND	ND	ND	26	ND	ND	121
L 6+00W 5+00N	.1	1.92	5	ND	239	ND	.20	.1	7	4	6	1.61	.03	.28	676	1	.01	11	.20	7	ND	ND	ND	ND	27	ND	ND	139
L 6+00W 5+50N	.1	1.87	6	ND	152	ND	.24	.2	6	4	7	1.46	.03	.29	590	1	.01	16	.10	5	ND	ND	ND	ND	29	ND	ND	96
L 6+00W 6+00N	.1	2.18	9	ND	135	ND	.22	.5	8	9	17	1.97	.04	.56	648	2	.01	24	.08	11	ND	ND	ND	ND	24	ND	ND	234
L 6+00W 6+50N	.1	2.08	15	ND	173	ND	.32	.5	8	6	17	1.83	.04	.44	1032	2	.01	28	.17	16	ND	ND	ND	ND	42	ND	ND	218
L 6+00W 7+00N	.2	2.16	7	ND	154	ND	.20	.2	7	3	7	1.54	.03	.27	551	2	.01	12	.10	5	ND	ND	ND	ND	24	ND	ND	167
L 6+00W 7+50N	.1	2.18	5	ND	123	ND	.27	.1	7	4	9	1.68	.04	.34	580	2	.01	14	.13	5	ND	ND	ND	ND	29	ND	ND	134
L 6+00W 8+00N	.2	1.41	3	ND	58	ND	.17	.1	7	5	6	1.68	.03	.39	277	1	.01	10	.02	6	ND	ND	ND	ND	16	ND	ND	100
L 6+00W 0+25S	.2	2.37	4	ND	153	ND	.22	.3	7	4	12	1.67	.04	.29	414	1	.01	12	.14	7	ND	ND	ND	ND	29	ND	ND	128
L 6+00W 0+50S	.1	1.95	3	ND	141	ND	.24	.2	8	5	34	1.95	.04	.38	609	1	.01	12	.05	7	ND	ND	ND	ND	25	ND	ND	147
L 6+00W 0+75S	.1	2.04	ND	ND	163	ND	.19	.1	7	5	7	1.63	.03	.27	521	1	.01	14	.13	6	ND	ND	ND	ND	27	ND	ND	123
L 6+00W 1+00S	.1	1.73	ND	ND	185	ND	.26	.1	6	4	4	1.54	.04	.29	525	1	.01	12	.10	6	ND	ND	ND	ND	35	ND	ND	112
L 6+00W 1+25S	.2	1.64	5	ND	137	ND	.28	.1	8	5	12	1.75	.04	.34	587	1	.01	14	.08	10	ND	ND	ND	ND	29	ND	ND	93
L 6+00W 1+50S	.1	1.91	ND	ND	138	ND	.22	.1	6	4	3	1.56	.04	.27	345	1	.01	12	.08	5	ND	ND	ND	ND	31	ND	ND	97
L 6+00W 1+75S	.1	1.85	ND	ND	168	ND	.20	.1	6	4	2	1.45	.03	.22	420	1	.01	11	.12	3	ND	ND	ND	ND	28	ND	ND	95
L 6+00W 2+00S	.1	1.98	ND	ND	168	ND	.19	.1	7	5	3	1.70	.04	.29	350	1	.01	14	.08	5	ND	ND	ND	ND	22	ND	ND	95
L 6+00W 2+25S	.2	2.02	5	ND	138	ND	.20	.1	7	5	4	1.63	.04	.28	349	1	.01	14	.17	5	ND	ND	ND	ND	28	ND	ND	98
L 6+00W 2+50S	.2	2.20	3	ND	154	ND	.22	.1	8	6	6	1.92	.04	.30	427	1	.01	17	.11	7	ND	ND	ND	ND	27	ND	ND	75
L 6+00W 2+75S	.1	1.41	ND	ND	126	ND	.16	.1	5	4	ND	1.52	.03	.20	171	1	.01	9	.05	5	ND	ND	ND	ND	19	ND	ND	47
L 6+00W 3+00S	.2	2.12	5	ND	123	ND	.22	.2	7	6	14	1.79	.03	.29	283	1	.01	15	.10	5	ND	ND	ND	ND	26	ND	ND	78
L 6+00W 3+25S	.1	1.88	13	ND	109	ND	.22	.1	8	6	13	2.24	.03	.32	316	1	.01	17	.13	10	ND	ND	ND	ND	25	ND	ND	100
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 6+00W 4+00S	.1	2.34	8	ND	164	ND	.24	.1	8	6	17	2.01	.03	.33	390	ND	.01	17	.10	5	ND	ND	ND	ND	26	ND	ND	84
L 6+00W 4+50S	.1	2.68	9	ND	226	ND	.26	.1	8	5	20	1.99	.03	.37	673	1	.01	18	.23	6	ND	ND	ND	ND	32	ND	ND	142
L 6+00W 5+00S	.1	1.46	5	ND	81	ND	.27	.3	9	9	32	2.78	.04	.63	414	ND	.01	17	.04	7	ND	ND	ND	ND	24	ND	ND	65
L 6+00W 5+50S	.1	2.25	12	ND	178	ND	.21	.1	8	6	22	2.12	.03	.38	678	1	.01	19	.15	10	ND	ND	ND	ND	23	ND	ND	166
L 6+00W 6+00S	.1	1.56	4	ND	85	ND	.19	.2	5	4	3	1.52	.02	.26	365	ND	.01	9	.01	5	ND	ND	ND	ND	17	ND	ND	52
L 6+00W 6+50S	.1	2.18	3	ND	134	ND	.24	.1	6	5	8	1.74	.02	.31	314	ND	.01	14	.04	6	ND	ND	ND	ND	24	ND	ND	73
L 6+00W 7+00S	.1	1.60	4	ND	90	ND	.26	.2	6	5	10	1.92	.02	.34	437	ND	.01	12	.04	7	ND	ND	ND	ND	23	ND	ND	65
L 6+00W 7+50S	.1	2.06	3	ND	144	ND	.26	.1	6	5	15	1.85	.02	.32	575	ND	.01	15	.04	6	ND	ND	ND	ND	24	ND	ND	95
L 6+00W 8+00S	.1	1.86	7	ND	153	ND	.22	.1	6	4	6	1.64	.02	.25	346	ND	.01	12	.09	5	ND	ND	ND	ND	23	ND	ND	95
L 7+00W 0+25N	.1	1.94	10	ND	154	ND	.21	.1	6	5	14	1.83	.02	.28	355	ND	.01	15	.14	9	ND	ND	ND	ND	25	ND	ND	102
L 7+00W 0+50N	.1	1.96	5	ND	135	ND	.23	.2	6	4	14	1.68	.02	.27	334	ND	.01	12	.12	6	ND	ND	ND	ND	28	ND	ND	101
L 7+00W 0+75N	.1	2.03	11	ND	125	ND	.20	.1	7	6	16	1.93	.02	.29	350	ND	.01	16	.17	12	ND	ND	ND	ND	31	ND	ND	112
L 7+00W 1+00N	.1	1.70	6	ND	122	ND	.21	.1	6	4	10	1.61	.03	.25	441	ND	.01	14	.08	7	ND	ND	ND	ND	23	ND	ND	104
L 7+00W 1+25N	.1	1.52	3	ND	161	ND	.23	.1	5	4	7	1.49	.02	.25	811	ND	.01	11	.07	10	ND	ND	ND	ND	29	ND	ND	136
L 7+00W 1+50N	.1	1.91	6	ND	139	ND	.20	.2	6	6	15	1.83	.02	.31	528	ND	.01	16	.14	13	ND	ND	ND	ND	22	ND	ND	131
L 7+00W 1+75N	.1	2.14	8	ND	173	ND	.22	.1	7	4	16	1.78	.02	.29	623	1	.01	15	.11	8	ND	ND	ND	ND	28	ND	ND	119
L 7+00W 2+00N	.1	1.89	ND	ND	143	ND	.21	.1	6	4	12	1.77	.03	.29	443	ND	.01	13	.06	6	ND	ND	ND	ND	25	ND	ND	75
L 7+00W 2+50N	.1	1.97	6	ND	125	ND	.23	.1	6	5	10	1.90	.03	.29	323	ND	.01	16	.07	8	ND	ND	ND	ND	25	ND	ND	82
L 7+00W 3+00N	.1	1.67	4	ND	126	ND	.21	.2	6	4	9	1.67	.02	.29	598	ND	.01	12	.08	7	ND	ND	ND	ND	22	ND	ND	93
L 7+00W 3+50N	.1	1.56	ND	ND	169	ND	.43	.1	7	5	13	1.93	.03	.44	1046	ND	.01	13	.07	13	ND	ND	ND	ND	28	ND	ND	136
L 7+00W 4+00N	.1	2.07	9	ND	121	ND	.24	.1	6	3	13	1.54	.02	.25	423	1	.01	14	.13	5	ND	ND	ND	ND	26	ND	ND	98
L 7+00W 4+50N	.1	1.54	ND	ND	174	ND	.22	.1	5	3	8	1.66	.03	.28	850	1	.01	10	.06	7	ND	ND	ND	ND	28	ND	ND	95
L 7+00W 5+00N	.1	1.96	4	ND	178	ND	.29	.1	8	8	13	2.28	.03	.43	542	ND	.01	16	.10	8	ND	ND	ND	ND	28	ND	ND	130
L 7+00W 5+50N	.1	1.84	7	ND	79	ND	.28	.1	8	5	15	2.16	.03	.38	297	ND	.01	15	.05	8	ND	ND	ND	ND	25	ND	ND	80
L 7+00W 6+00N	.1	1.60	5	ND	75	ND	.26	.2	8	6	19	2.15	.03	.42	344	ND	.01	15	.06	9	ND	ND	ND	ND	27	ND	ND	97
L 7+00W 6+50N	.1	2.35	15	ND	138	ND	.26	.2	7	6	24	1.76	.02	.44	388	1	.01	20	.12	14	ND	ND	ND	ND	31	ND	ND	161
L 7+00W 7+00N	.1	2.46	4	ND	158	ND	.36	.3	10	6	19	2.32	.04	.55	699	1	.01	18	.09	8	ND	ND	ND	ND	32	ND	ND	184
L 7+00W 7+50N	.1	2.05	3	ND	116	ND	.30	.3	9	6	17	2.28	.03	.44	503	ND	.01	17	.10	7	ND	ND	ND	ND	28	ND	ND	131
L 7+00W 8+00N	.1	2.36	ND	ND	153	ND	.29	.4	8	5	17	2.05	.03	.47	594	ND	.01	19	.15	13	ND	ND	ND	ND	39	ND	ND	190
L 7+00W 0+25S	.1	2.19	6	ND	168	ND	.22	.1	6	4	14	1.73	.03	.30	395	ND	.01	12	.12	7	ND	ND	ND	ND	30	ND	ND	137
L 7+00W 0+50S	.1	2.20	ND	ND	147	ND	.29	.3	7	5	28	2.02	.03	.38	488	ND	.01	14	.06	7	ND	ND	ND	ND	27	ND	ND	150
L 7+00W 0+75S	.1	2.50	7	ND	145	ND	.22	.3	7	7	17	1.88	.03	.32	340	ND	.01	18	.14	6	ND	ND	ND	ND	29	ND	ND	153
L 7+00W 1+00S	.1	2.24	9	ND	163	ND	.24	.2	7	5	20	1.94	.03	.31	539	ND	.01	17	.14	12	ND	ND	ND	ND	29	ND	ND	143
L 7+00W 1+25S	.1	2.29	8	ND	149	ND	.22	.2	8	5	17	1.98	.03	.32	417	ND	.01	17	.09	11	ND	ND	ND	ND	27	ND	ND	132
L 7+00W 1+50S	.1	1.95	3	ND	109	ND	.23	.2	6	4	14	1.75	.03	.27	285	ND	.01	13	.08	6	ND	ND	ND	ND	26	ND	ND	95
L 7+00W 1+75S	.1	1.82	4	ND	160	ND	.26	.1	6	4	12	1.67	.03	.27	388	ND	.01	13	.12	4	ND	ND	ND	ND	36	ND	ND	94
L 7+00W 2+00S	.1	1.72	5	ND	124	ND	.23	.2	6	4	14	1.66	.03	.26	399	ND	.01	12	.10	9	ND	ND	ND	ND	27	ND	ND	104
L 7+00W 2+25S	.1	1.84	ND	ND	153	ND	.19	.1	5	4	10	1.48	.02	.22	407	ND	.01	12	.13	8	ND	ND	ND	ND	28	ND	ND	114
L 7+00W 2+50S	.1	2.01	4	ND	137	ND	.18	.1	6	4	10	1.53	.02	.24	372	ND	.01	13	.10	8	ND	ND	ND	ND	23	ND	ND	96
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 7+00N 2+75S	.1	2.20	7	ND	180	ND	.20	.1	7	5	8	1.73	.04	.27	406	1	.01	15	.11	6	ND	ND	ND	ND	25	ND	ND	85
L 7+00N 3+00S	.1	1.85	3	ND	105	ND	.28	.5	8	6	12	1.98	.05	.39	346	1	.01	15	.04	8	ND	ND	ND	ND	27	ND	ND	81
L 7+00N 3+50S	.1	2.02	7	ND	150	ND	.22	.2	7	5	8	1.72	.05	.29	395	1	.01	12	.08	6	ND	ND	ND	ND	27	ND	ND	70
L 7+00N 4+00S	.1	2.62	10	ND	125	ND	.24	.4	10	9	22	2.47	.05	.44	404	2	.01	20	.10	8	ND	ND	ND	ND	27	ND	ND	101
L 7+00N 4+50S	.1	3.04	7	ND	151	ND	.29	.4	10	8	28	2.36	.05	.55	500	2	.01	18	.13	3	ND	ND	ND	ND	32	ND	ND	132
L 7+00N 5+00S	.1	2.70	ND	ND	152	ND	.28	.3	10	7	23	2.33	.05	.50	500	2	.01	16	.08	4	ND	ND	ND	ND	36	ND	ND	99
L 7+00N 5+50S	.1	2.75	6	ND	186	ND	.20	.3	9	6	23	2.06	.05	.38	559	2	.01	17	.16	4	ND	ND	ND	ND	27	ND	ND	143
L 7+00N 6+00S	.3	2.45	6	ND	128	ND	.30	.3	9	6	15	2.13	.05	.44	389	2	.01	15	.05	4	ND	ND	ND	ND	32	ND	ND	78
L 7+00N 6+50S	.3	2.16	5	ND	119	ND	.26	.3	9	6	15	2.13	.05	.40	344	1	.01	15	.04	5	ND	ND	ND	ND	26	ND	ND	75
L 7+00N 7+00S	.1	1.77	6	ND	107	ND	.20	.1	8	6	11	1.83	.04	.35	413	2	.01	13	.03	6	ND	ND	ND	ND	19	ND	ND	81
L 7+00N 7+50S	.1	2.90	4	ND	163	ND	.48	.5	12	8	11	2.62	.06	.77	921	2	.01	19	.08	1	ND	ND	ND	ND	59	ND	ND	132
L 7+00N 8+00S	.1	2.37	3	ND	103	ND	.45	.5	9	8	7	2.08	.05	.54	700	2	.01	15	.04	4	ND	ND	ND	ND	42	ND	ND	145
L 7+50N 0+00 BL	.1	1.14	ND	ND	89	ND	.27	.2	5	5	ND	1.46	.05	.22	412	1	.01	8	.03	7	ND	ND	ND	ND	28	ND	ND	64
L 7+50N 0+25N	.3	1.08	ND	ND	68	ND	.27	.3	6	6	2	1.82	.05	.25	325	1	.01	12	.05	5	ND	ND	ND	ND	28	ND	ND	51
L 7+50N 0+50N	.1	1.45	3	ND	173	ND	.20	.3	6	5	3	1.61	.04	.22	526	1	.01	11	.12	6	ND	ND	ND	ND	26	ND	ND	95
L 7+50N 0+75N	.1	1.51	ND	ND	140	ND	.30	.2	7	6	3	1.92	.06	.28	580	1	.01	11	.05	5	ND	ND	ND	ND	30	ND	ND	85
L 7+50N 1+00N	.1	1.39	4	ND	66	ND	.32	.2	7	6	6	1.97	.06	.28	245	1	.01	13	.06	6	ND	ND	ND	ND	27	ND	ND	54
L 7+50N 1+25N	.1	2.34	3	ND	115	ND	.32	.4	8	7	8	2.25	.06	.45	416	2	.01	16	.07	10	ND	ND	ND	ND	30	ND	ND	127
L 7+50N 1+50N	.1	2.00	ND	ND	142	ND	.30	.6	9	6	6	2.18	.06	.43	1130	2	.01	14	.04	14	ND	ND	ND	ND	31	ND	ND	127
L 7+50N 0+25S	.1	1.70	ND	ND	115	ND	.27	.4	8	7	11	1.97	.06	.30	503	1	.01	12	.04	6	ND	ND	ND	ND	25	ND	ND	83
L 7+50N 0+50S	.1	1.60	ND	ND	107	ND	.28	.4	7	7	6	1.92	.05	.30	521	1	.01	17	.04	6	ND	ND	ND	ND	28	ND	ND	72
L 7+50N 0+75S	.1	1.29	ND	ND	59	ND	.30	.3	8	7	7	2.22	.06	.44	293	1	.01	15	.06	5	ND	ND	ND	ND	28	ND	ND	54
L 7+50N 1+00S	.1	1.60	ND	ND	126	ND	.24	.3	6	7	4	1.68	.05	.25	366	1	.01	12	.05	6	ND	ND	ND	ND	28	ND	ND	79
L 7+50N 1+25S	.1	1.95	ND	ND	139	ND	.27	.2	7	6	5	1.77	.05	.27	292	1	.01	13	.07	4	ND	ND	ND	ND	28	ND	ND	86
L 7+50N 1+50S	.1	1.29	ND	ND	147	ND	.32	.2	5	5	2	1.56	.04	.22	548	1	.01	10	.07	6	ND	ND	ND	ND	38	ND	ND	72
L 7+50N 1+75S	.1	1.62	ND	ND	186	ND	.26	.4	7	5	1	1.64	.05	.28	923	1	.01	11	.07	4	ND	ND	ND	ND	29	ND	ND	112
L 7+50N 2+00S	.1	1.54	ND	ND	142	ND	.26	.1	6	5	2	1.58	.05	.25	561	1	.01	11	.05	4	ND	ND	ND	ND	27	ND	ND	81
L 7+50N 2+25S	.1	1.72	3	ND	120	ND	.24	.2	7	6	7	1.72	.04	.30	358	1	.01	11	.07	4	ND	ND	ND	ND	25	ND	ND	70
L 7+50N 2+50S	.1	1.93	ND	ND	188	ND	.26	.3	7	5	6	1.64	.04	.30	509	1	.01	14	.15	5	ND	ND	ND	ND	32	ND	ND	87
L 7+50N 2+75S	.4	2.29	9	ND	120	ND	.24	.3	10	8	23	2.31	.05	.40	349	1	.01	16	.07	8	ND	ND	ND	ND	28	ND	ND	81
L 7+50N 3+00S	.1	2.08	3	ND	127	ND	.30	.4	7	5	57	1.66	.04	.30	450	1	.01	12	.08	4	ND	ND	ND	ND	26	ND	ND	129
L 7+50N 3+25S	.1	1.67	9	ND	102	ND	.25	.3	9	9	25	2.47	.05	.48	346	1	.01	19	.05	8	ND	ND	ND	ND	25	ND	ND	83
L 7+50N 3+50S	.1	2.43	6	ND	162	ND	.30	.4	9	7	19	1.92	.05	.36	495	2	.01	18	.05	11	ND	ND	ND	ND	27	ND	ND	147
L 7+50N 3+75S	.1	2.45	7	ND	226	ND	.27	.2	8	6	14	1.75	.05	.30	708	2	.01	18	.08	8	ND	ND	ND	ND	29	ND	ND	126
L 7+50N 4+00S	.1	3.00	12	ND	212	ND	.35	.5	10	8	24	2.25	.06	.43	874	2	.01	20	.07	16	ND	ND	ND	ND	35	ND	ND	128
L 7+50N 4+25S	.1	2.62	5	ND	190	ND	.32	.4	9	7	11	2.02	.05	.40	738	2	.01	14	.17	5	ND	ND	ND	ND	36	ND	ND	127
L 7+50N 4+50S	.1	2.57	6	ND	137	ND	.24	.4	9	7	18	2.02	.05	.39	458	2	.01	17	.10	8	ND	ND	ND	ND	25	ND	ND	157
L 7+50N 4+75S	.1	1.89	4	ND	169	ND	.27	.3	8	6	8	1.75	.04	.35	676	1	.01	15	.10	7	ND	ND	ND	ND	28	ND	ND	125
L 7+50N 5+00S	.1	1.95	ND	ND	166	ND	.24	.4	8	6	9	1.62	.04	.32	587	2	.01	13	.08	5	ND	ND	ND	ND	27	ND	ND	187
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 8+00N 0+00 BL	.2	1.73	3	ND	124	ND	.34	.1	8	6	16	2.08	.05	.32	429	1	.01	15	.04	10	ND	ND	ND	ND	29	ND	3	80
L 8+00N 0+50N	.1	1.66	5	ND	88	ND	.29	.1	8	6	18	2.02	.04	.32	378	1	.01	13	.05	10	ND	ND	ND	ND	26	ND	ND	70
L 8+00N 1+00N	.1	1.47	3	ND	92	ND	.27	.1	7	5	14	1.93	.04	.30	581	1	.01	11	.05	18	ND	ND	ND	ND	25	ND	ND	81
L 8+00N 1+50N	.1	1.68	7	ND	99	ND	.30	.1	8	7	19	2.07	.04	.35	459	2	.01	16	.07	17	ND	ND	ND	ND	28	ND	ND	101
L 8+00N 2+00N	.1	1.72	10	ND	115	ND	.30	.2	8	8	28	2.07	.04	.36	554	1	.01	17	.04	24	ND	ND	ND	ND	27	ND	ND	102
L 8+00N 2+50N	.2	1.52	13	ND	104	ND	.24	.1	8	8	25	1.95	.04	.38	346	1	.01	16	.02	21	ND	ND	ND	ND	23	ND	ND	80
L 8+00N 3+00N	.4	2.00	3	ND	90	ND	.68	.1	9	7	83	2.27	.06	.55	692	1	.01	16	.07	8	ND	ND	ND	ND	63	ND	ND	87
L 8+00N 3+50N	.1	2.72	3	ND	84	ND	.58	.3	11	7	25	2.70	.07	.68	581	1	.01	18	.05	5	ND	ND	ND	ND	48	ND	ND	82
L 8+00N 4+00N	.1	1.79	ND	ND	78	ND	.22	.1	8	5	10	1.98	.04	.38	300	1	.01	11	.04	7	ND	ND	ND	ND	21	ND	ND	75
L 8+00N 4+50N	.2	2.49	ND	ND	99	ND	.39	.2	10	5	14	2.32	.05	.58	418	1	.01	13	.05	12	ND	ND	ND	ND	32	ND	ND	133
L 8+00N 5+00N	.2	1.77	5	ND	97	ND	.26	.2	8	6	16	2.00	.04	.32	361	1	.01	14	.04	11	ND	ND	ND	ND	23	ND	ND	80
L 8+00N 5+50N	.1	1.54	6	ND	87	ND	.29	.2	9	6	20	2.27	.04	.44	514	1	.01	16	.04	12	ND	ND	ND	ND	23	ND	ND	81
L 8+00N 6+00N	.1	2.49	5	ND	181	ND	.40	.5	11	8	20	2.37	.05	.60	903	2	.01	16	.12	8	ND	ND	ND	ND	39	ND	ND	162
L 8+00N 6+50N	.1	3.34	5	ND	117	ND	.59	.2	13	10	60	2.97	.05	.76	658	2	.01	22	.05	9	ND	ND	ND	ND	47	ND	ND	147
L 8+00N 7+00N	.1	3.62	3	ND	171	ND	.60	.4	13	8	30	2.87	.07	.73	1114	2	.01	22	.09	5	ND	ND	ND	ND	47	ND	ND	141
L 8+00N 7+50N	.1	2.83	ND	ND	126	ND	.52	.1	10	5	23	2.54	.06	.60	828	2	.01	15	.04	6	ND	ND	ND	ND	35	ND	ND	102
L 8+00N 8+00N	.1	3.25	ND	ND	165	ND	.53	.5	11	7	22	2.63	.07	.65	923	2	.01	18	.07	8	ND	ND	ND	ND	46	ND	ND	145
L 8+00N 0+25S	.1	1.79	5	ND	207	ND	.30	.2	6	5	14	1.62	.04	.32	564	1	.01	12	.19	10	ND	ND	ND	ND	39	ND	ND	175
L 8+00N 0+50S	.1	.96	ND	ND	53	ND	.28	.1	7	5	12	1.82	.04	.32	368	ND	.01	10	.04	8	ND	ND	ND	ND	23	ND	ND	58
L 8+00N 0+75S	.1	.93	3	ND	73	ND	.36	.1	6	5	9	1.53	.04	.26	434	ND	.01	10	.03	10	ND	ND	ND	ND	26	ND	ND	51
L 8+00N 1+00S	.2	1.29	5	ND	114	ND	.29	.2	7	5	12	1.72	.04	.28	519	1	.01	14	.05	10	ND	ND	ND	ND	33	ND	ND	83
L 8+00N 1+25S	.1	1.70	7	ND	132	ND	.24	.2	7	5	16	1.68	.03	.27	514	1	.01	13	.07	10	ND	ND	ND	ND	30	ND	ND	90
L 8+00N 1+50S	.1	1.63	8	ND	115	ND	.28	.1	7	5	13	1.72	.04	.27	462	1	.01	11	.06	8	ND	ND	ND	ND	35	ND	ND	91
L 8+00N 1+75S	.1	1.37	8	ND	124	ND	.27	.1	7	6	16	1.91	.04	.32	460	1	.01	14	.04	12	ND	ND	ND	ND	29	ND	ND	70
L 8+00N 2+00S	.1	2.15	9	ND	133	ND	.30	.1	8	6	17	2.00	.04	.36	502	1	.01	15	.07	10	ND	ND	ND	ND	31	ND	ND	99
L 8+00N 2+25S	.1	1.86	7	ND	146	ND	.27	.1	7	6	15	1.91	.04	.34	632	1	.01	13	.05	8	ND	ND	ND	ND	29	ND	ND	93
L 8+00N 2+50S	.1	1.82	10	ND	87	ND	.32	.1	8	7	20	2.11	.04	.40	269	1	.01	14	.05	9	ND	ND	ND	ND	33	ND	ND	56
L 8+00N 2+75S	.2	2.84	ND	ND	115	ND	.61	.2	13	8	57	3.06	.06	.86	453	1	.01	18	.08	4	ND	ND	ND	ND	64	ND	ND	65
L 8+00N 3+00S	.1	2.16	4	ND	157	ND	.35	.2	9	6	21	2.13	.05	.45	802	1	.01	14	.04	13	ND	ND	ND	ND	31	ND	ND	88
L 8+00N 3+25S	.1	2.36	9	ND	137	ND	.40	.4	9	6	31	1.98	.04	.41	807	1	.01	14	.05	12	ND	ND	ND	ND	31	ND	ND	154
L 8+00N 3+50S	.1	2.40	10	ND	187	ND	.22	.2	8	5	26	1.81	.03	.32	785	2	.01	14	.07	13	ND	ND	ND	ND	25	ND	ND	144
L 8+00N 3+75S	.1	2.04	7	ND	164	ND	.36	.1	8	6	21	1.95	.04	.36	808	1	.01	15	.02	14	ND	ND	ND	ND	27	ND	ND	118
L 8+00N 4+00S	.1	2.72	12	ND	198	ND	.34	.4	10	7	41	2.31	.04	.48	753	2	.01	18	.14	17	ND	ND	ND	ND	39	ND	ND	166
L 8+00N 4+25S	.2	3.20	10	ND	173	ND	.28	.2	12	8	52	2.79	.04	.59	717	2	.01	19	.08	14	ND	ND	ND	ND	33	ND	ND	137
L 8+00N 4+50S	.1	2.52	5	ND	148	ND	.27	.3	10	7	38	2.45	.04	.52	447	1	.01	17	.06	14	ND	ND	ND	ND	30	ND	ND	106
L 8+00N 4+75S	.1	2.49	14	ND	155	ND	.27	.2	9	6	27	2.07	.04	.43	393	1	.01	17	.05	14	ND	ND	ND	ND	31	ND	3	108
L 8+00N 5+00S	.1	2.36	8	ND	142	ND	.36	.3	10	6	38	2.41	.04	.54	722	1	.01	18	.07	9	ND	ND	ND	ND	35	ND	ND	100
L 8+00N 5+50S	.1	1.95	9	ND	143	ND	.25	.2	8	5	18	1.92	.03	.40	535	1	.01	14	.08	10	ND	ND	ND	ND	26	ND	ND	120
L 8+00N 6+00S	.1	2.02	7	ND	70	ND	.30	.1	11	7	29	2.58	.04	.69	515	1	.01	16	.04	8	ND	ND	ND	ND	29	ND	ND	85
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPB	PT PPB	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 8+00W 6+50S	.2	1.85	10	ND	114	ND	.28	.1	8	7	18	2.17	.04	.42	442	1	.01	16	.03	11	ND	ND	ND	ND	29	ND	ND	92
L 8+00W 7+00S	.1	2.66	13	ND	133	ND	.31	.3	9	7	46	2.24	.04	.48	456	1	.01	16	.12	11	ND	ND	ND	ND	41	ND	ND	95
L 8+00W 7+50S	.1	2.74	15	ND	166	ND	.25	.3	9	7	28	2.35	.04	.51	431	2	.01	20	.13	26	ND	ND	ND	ND	28	ND	ND	114
L 8+00W 8+00S	.1	2.05	7	ND	158	ND	.73	.3	7	4	14	1.57	.05	.31	489	1	.01	13	.05	6	ND	ND	ND	ND	57	ND	ND	113
L 8+50W 0+00 BL	.1	1.94	9	ND	125	ND	.34	.3	8	6	24	2.03	.04	.34	544	1	.01	16	.05	11	ND	ND	ND	ND	28	ND	ND	91
L 8+50W 0+25N	.1	1.33	11	ND	103	ND	.30	.1	6	5	15	1.70	.04	.26	634	1	.01	13	.05	9	ND	ND	ND	ND	25	ND	ND	92
L 8+50W 0+50N	.1	1.44	12	ND	91	ND	.31	.1	7	6	17	1.94	.04	.30	402	1	.01	13	.04	9	ND	ND	ND	ND	24	ND	ND	74
L 8+50W 0+75N	.1	1.43	23	ND	71	ND	.29	.1	8	6	34	2.07	.03	.35	339	1	.01	16	.05	15	ND	ND	ND	ND	24	ND	ND	60
L 8+50W 1+00N	.1	1.64	17	ND	95	ND	.30	.3	8	6	22	2.08	.04	.35	442	1	.01	15	.08	12	ND	ND	ND	ND	29	ND	ND	81
L 8+50W 1+25N	.1	1.72	15	ND	86	ND	.30	.2	8	6	25	2.12	.04	.34	371	1	.01	15	.05	13	ND	ND	ND	ND	25	ND	ND	79
L 8+50W 1+50N	.1	1.45	13	ND	112	ND	.31	.3	7	6	14	1.87	.03	.31	578	1	.01	12	.04	12	ND	ND	ND	ND	25	ND	ND	96
L 8+50W 0+25S	.1	1.73	7	ND	217	ND	.36	.4	7	5	21	1.65	.04	.28	1099	1	.01	12	.16	10	ND	ND	ND	ND	40	ND	ND	139
L 8+50W 0+50S	.1	1.81	12	ND	117	ND	.26	.2	8	7	19	1.91	.04	.34	355	1	.01	15	.04	13	ND	ND	ND	ND	25	ND	ND	87
L 8+50W 0+75S	.2	3.52	15	ND	84	ND	.89	.4	10	7	65	2.71	.06	.69	416	2	.01	18	.04	7	ND	ND	ND	ND	78	ND	ND	95
L 8+50W 1+00S	.1	2.68	10	ND	148	ND	.32	.4	9	6	28	2.00	.04	.38	374	1	.01	15	.11	11	ND	ND	ND	ND	31	ND	ND	135
L 8+50W 1+25S	.1	2.79	13	ND	154	ND	.34	.1	9	7	23	2.22	.04	.44	331	1	.01	17	.04	9	ND	ND	ND	ND	34	ND	ND	84
L 8+50W 1+50S	.1	2.08	8	ND	122	ND	.29	.2	8	6	15	1.99	.04	.41	544	1	.01	14	.03	7	ND	ND	ND	ND	27	ND	ND	79
L 8+50W 1+75S	.1	2.56	11	ND	189	ND	.43	.4	9	7	23	2.07	.04	.40	862	2	.01	15	.07	13	ND	ND	ND	ND	43	ND	ND	132
L 8+50W 2+00S	.1	2.43	15	ND	161	ND	.26	.3	9	6	23	1.93	.03	.35	550	2	.01	15	.18	13	ND	ND	ND	ND	35	ND	ND	121
L 8+50W 2+25S	.1	2.42	14	ND	241	ND	.32	.3	9	7	18	1.99	.03	.37	1250	2	.01	18	.10	11	ND	ND	ND	ND	36	ND	ND	152
L 8+50W 2+50S	.1	2.30	12	ND	207	ND	.35	.4	8	6	19	2.00	.04	.38	1053	2	.01	22	.07	16	ND	ND	ND	ND	34	ND	ND	150
L 8+50W 2+75S	.1	2.13	12	ND	100	ND	.30	.1	8	7	28	2.14	.04	.38	482	1	.01	18	.05	15	ND	ND	ND	ND	28	ND	ND	98
L 8+50W 3+00S	.1	1.99	11	ND	140	ND	.33	.2	8	6	20	1.90	.03	.36	547	1	.01	19	.14	15	ND	ND	ND	ND	38	ND	ND	161
L 8+50W 3+25S	.1	1.70	7	ND	119	ND	.97	1.0	8	6	32	1.88	.06	.35	580	1	.01	15	.02	11	ND	ND	ND	ND	40	ND	ND	207
L 8+50W 3+50S	.1	2.10	16	ND	163	ND	.31	.4	9	7	19	2.02	.04	.40	541	1	.01	19	.04	16	ND	ND	ND	ND	26	ND	ND	255
L 8+50W 3+75S	.1	2.24	14	ND	189	ND	.32	.6	9	7	27	2.22	.04	.45	934	1	.01	19	.07	18	ND	ND	ND	ND	32	ND	ND	166
L 8+50W 4+00S	.1	2.61	10	ND	144	ND	.35	.2	9	8	26	2.32	.04	.44	509	1	.01	21	.06	17	ND	ND	ND	ND	31	ND	ND	162
L 8+50W 4+25S	.1	2.71	13	ND	239	ND	.35	.3	9	7	24	2.13	.04	.47	1011	1	.01	16	.10	8	ND	ND	ND	ND	38	ND	ND	134
L 8+50W 4+50S	.1	2.65	11	ND	171	ND	.59	.4	10	9	24	2.38	.05	.55	833	1	.01	19	.06	8	ND	ND	ND	ND	55	ND	ND	92
L 8+50W 4+75S	.1	2.71	11	ND	157	ND	.35	.2	11	10	19	2.60	.04	.65	560	1	.01	19	.05	7	ND	ND	ND	ND	33	ND	ND	106
L 8+50W 5+00S	.1	1.98	10	ND	136	ND	.23	.1	8	6	14	2.00	.03	.39	641	1	.01	13	.05	13	ND	ND	ND	ND	22	ND	ND	101
L 9+00W 0+00 BL	.1	1.69	9	ND	82	ND	.27	.2	7	6	30	1.83	.04	.31	271	ND	.01	14	.05	12	ND	ND	ND	ND	23	ND	ND	72
L 9+00W 0+50N	.1	1.76	12	ND	141	ND	.25	.3	7	6	22	1.83	.03	.31	634	1	.01	16	.09	11	ND	ND	ND	ND	25	ND	ND	109
L 9+00W 1+00N	.2	1.51	20	ND	43	ND	.56	.1	8	7	44	2.20	.05	.55	347	ND	.01	15	.10	9	ND	ND	ND	ND	37	ND	ND	54
L 9+00W 1+50N	.1	1.61	9	ND	95	ND	.27	.2	7	6	16	1.95	.04	.35	527	1	.01	14	.08	21	ND	ND	ND	ND	23	ND	ND	106
L 9+00W 2+00N	.2	1.42	20	ND	48	ND	.43	.3	7	7	36	2.07	.04	.40	296	1	.01	15	.05	12	ND	ND	ND	ND	31	ND	ND	61
L 9+00W 2+50N	.1	1.01	7	ND	66	ND	.18	.2	5	5	8	1.40	.03	.24	263	ND	.01	10	.01	9	ND	ND	ND	ND	18	ND	ND	56
L 9+00W 3+00N	.1	2.77	5	ND	327	ND	1.20	.4	12	10	114	2.60	.07	.81	1797	1	.01	21	.25	1	ND	ND	ND	ND	103	ND	ND	141
L 9+00W 3+50N	.1	1.51	9	ND	68	ND	.32	.3	9	6	20	2.14	.04	.49	584	ND	.01	15	.03	7	ND	ND	ND	ND	26	ND	ND	60
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 9+00N 4+00W	.2	1.37	5	ND	128	ND	.44	.6	5	4	11	1.30	.04	.24	632	1	.01	11	.07	8	ND	ND	ND	ND	31	ND	ND	128
L 9+00N 4+50W	ND	2.41	ND	ND	227	ND	.43	.5	8	5	20	1.92	.05	.36	1380	2	.01	16	.06	10	ND	ND	ND	ND	40	ND	ND	122
L 9+00N 5+00W	.2	2.05	5	ND	138	ND	.24	.4	7	5	17	1.78	.04	.33	425	1	.01	14	.06	10	ND	ND	ND	ND	25	ND	ND	104
L 9+00N 5+50W	.1	1.51	3	ND	139	ND	.26	.4	6	5	12	1.73	.03	.32	773	1	.01	13	.06	8	ND	ND	ND	ND	25	ND	ND	121
L 9+00N 6+00W	.1	1.59	9	ND	95	ND	.27	.4	7	5	15	1.88	.03	.36	404	1	.01	13	.06	7	ND	ND	ND	ND	24	ND	ND	97
L 9+00N 6+50W	ND	2.82	17	ND	204	ND	.53	1.4	13	12	43	2.91	.06	.75	1737	4	.01	33	.08	37	ND	ND	ND	ND	52	ND	ND	268
L 9+00N 7+00W	.1	2.19	55	ND	116	ND	.50	1.3	11	12	66	2.81	.06	.72	1249	3	.01	42	.06	19	ND	ND	ND	ND	45	ND	ND	209
L 9+00N 7+50W	ND	3.05	12	ND	232	ND	.51	.9	12	8	24	2.76	.07	.74	1582	2	.01	25	.10	11	ND	ND	ND	ND	48	ND	ND	176
L 9+00N 8+00W	.1	2.58	9	ND	126	ND	.32	.5	11	7	25	2.56	.05	.55	871	3	.01	23	.06	16	ND	ND	ND	ND	30	ND	ND	140
L 9+00N 0+25S	.1	1.76	10	ND	153	ND	.23	.4	7	6	23	1.81	.04	.31	722	1	.01	14	.11	13	ND	ND	ND	ND	25	ND	ND	114
L 9+00N 0+50S	.2	1.86	8	ND	152	ND	.30	.6	8	7	26	1.99	.04	.38	620	1	.01	15	.08	11	ND	ND	ND	ND	30	ND	ND	127
L 9+00N 0+75S	.3	1.49	3	ND	96	ND	.26	.5	7	6	15	1.91	.05	.38	469	1	.01	14	.04	8	ND	ND	ND	ND	22	ND	ND	125
L 9+00N 1+00S	.3	2.12	8	ND	127	ND	.27	.5	9	10	27	2.24	.04	.43	453	1	.01	16	.06	9	ND	ND	ND	ND	26	ND	ND	87
L 9+00N 1+25S	.2	2.48	7	ND	151	ND	.26	.4	10	7	17	2.20	.04	.45	718	2	.01	17	.06	8	ND	ND	ND	ND	26	ND	ND	98
L 9+00N 1+50S	.1	2.66	7	ND	189	ND	.37	.5	9	8	24	2.07	.04	.43	863	2	.01	16	.07	8	ND	ND	ND	ND	37	ND	ND	105
L 9+00N 1+75S	.2	2.49	9	ND	139	ND	.34	.6	9	6	22	2.23	.04	.42	629	1	.01	15	.09	8	ND	ND	ND	ND	37	ND	ND	103
L 9+00N 2+00S	.1	2.25	10	ND	211	ND	.34	.4	10	7	31	2.34	.05	.49	1135	2	.01	21	.09	11	ND	ND	ND	ND	34	ND	ND	139
L 9+00N 2+25S	.2	2.40	6	ND	141	ND	.32	.3	9	6	22	2.15	.04	.44	819	2	.01	15	.03	11	ND	ND	ND	ND	26	ND	ND	95
L 9+00N 2+50S	ND	2.73	5	ND	235	ND	.42	.5	9	7	15	2.01	.04	.50	936	1	.01	15	.19	5	ND	ND	ND	ND	46	ND	ND	152
L 9+00N 2+75S	.1	3.03	3	ND	94	ND	.51	.3	10	9	25	2.33	.04	.64	430	2	.01	18	.06	3	ND	ND	ND	ND	53	ND	ND	118
L 9+00N 3+00S	.2	2.49	5	ND	197	ND	.48	.7	8	7	16	1.77	.04	.39	739	1	.01	16	.15	11	ND	ND	ND	ND	39	ND	ND	164
L 9+00N 3+25S	ND	2.75	4	ND	184	ND	.35	.4	10	8	16	2.28	.04	.49	1082	2	.01	15	.08	12	ND	ND	ND	ND	33	ND	ND	165
L 9+00N 3+50S	1.0	2.49	12	ND	161	ND	.35	.5	10	7	30	2.43	.05	.53	823	2	.01	16	.06	16	ND	ND	ND	ND	34	ND	ND	180
L 9+00N 3+75S	.1	2.86	7	ND	249	ND	.44	.7	12	8	22	2.77	.05	.66	1843	2	.01	20	.08	16	ND	ND	ND	ND	42	ND	ND	198
L 9+00N 4+00S	.1	2.82	3	ND	187	ND	.37	.6	11	8	19	2.68	.04	.59	1117	2	.01	19	.07	12	ND	ND	ND	ND	34	ND	ND	189
L 9+00N 4+25S	ND	2.16	ND	ND	263	ND	.42	1.1	9	7	19	2.34	.05	.52	1756	1	.01	16	.07	10	ND	ND	ND	ND	46	ND	ND	212
L 9+00N 4+50S	ND	1.98	5	ND	223	ND	.35	.3	7	6	13	1.90	.04	.38	1375	2	.01	13	.06	7	ND	ND	ND	ND	33	ND	ND	134
L 9+00N 4+75S	.1	2.05	ND	ND	217	ND	.43	1.0	9	7	21	2.08	.05	.39	1294	1	.01	14	.05	9	ND	ND	ND	ND	34	ND	ND	181
L 9+00N 5+00S	ND	1.70	ND	ND	106	ND	.26	.4	7	6	13	1.89	.03	.33	473	1	.01	12	.02	6	ND	ND	ND	ND	20	ND	ND	76
L 9+00N 5+50S	ND	2.48	3	ND	179	ND	.42	.6	9	7	17	2.21	.04	.48	956	2	.01	16	.07	11	ND	ND	ND	ND	33	ND	ND	137
L 9+00N 6+00S	ND	2.12	ND	ND	189	ND	.30	.5	8	6	13	1.86	.04	.34	1162	1	.01	12	.07	6	ND	ND	ND	ND	27	ND	ND	134
L 9+00N 6+50S	.1	2.67	4	ND	181	ND	.31	.3	9	8	16	2.25	.04	.44	960	2	.01	16	.05	7	ND	ND	ND	ND	31	ND	ND	115
L 9+00N 7+00S	.1	2.98	ND	ND	204	ND	.41	.5	9	6	18	2.24	.05	.47	859	1	.01	16	.08	4	ND	ND	ND	ND	40	ND	ND	115
L 9+00N 7+50S	ND	1.90	ND	ND	119	ND	.33	.5	8	6	14	1.98	.04	.45	647	1	.01	12	.03	6	ND	ND	ND	ND	26	ND	ND	96
L 9+00N 8+00S	.1	2.15	ND	ND	137	ND	.26	.4	8	6	19	1.96	.04	.38	488	1	.01	13	.04	4	ND	ND	ND	ND	25	ND	ND	73
L 9+50N 0+00 BL	.3	1.57	27	ND	74	ND	.31	.4	8	6	46	2.07	.04	.35	281	1	.01	16	.05	14	ND	ND	ND	ND	25	ND	ND	63
L 9+50N 0+25N	.1	2.50	12	ND	112	ND	.34	.4	9	6	28	2.27	.04	.41	435	1	.01	16	.13	13	ND	ND	ND	ND	31	ND	ND	102
L 9+50N 0+50N	ND	1.68	18	ND	76	ND	.26	.2	10	8	40	2.57	.04	.49	375	1	.01	20	.09	12	ND	ND	ND	ND	24	ND	ND	89
L 9+50N 0+75N	.1	1.19	10	ND	45	ND	.29	.3	6	5	32	1.97	.03	.35	230	ND	.01	11	.06	9	ND	ND	ND	ND	21	ND	ND	52
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 9+50N 1+00N	.1	1.87	12	ND	128	NB	.22	.1	7	5	22	1.80	.03	.31	257	1	.01	15	.06	14	NB	NB	NB	NB	24	NB	ND	88
L 9+50N 1+25N	.1	2.06	13	ND	112	NB	.29	.2	8	5	26	1.96	.04	.32	340	1	.01	16	.09	20	NB	NB	NB	NB	33	NB	NB	89
L 9+50N 1+50N	.1	2.06	16	ND	99	ND	.28	.2	9	7	35	2.37	.04	.43	512	1	.01	18	.05	20	NB	NB	NB	NB	26	NB	NB	91
L 9+50N 0+25S	.1	1.59	16	NB	91	NB	.24	.2	8	5	26	1.96	.04	.33	345	1	.01	17	.06	16	NB	NB	NB	NB	25	NB	NB	112
L 9+50N 0+50S	.3	1.93	15	ND	90	ND	.25	.3	8	6	32	2.06	.04	.33	365	1	.01	16	.13	15	NB	NB	NB	NB	29	NB	NB	134
L 9+50N 0+75S	.1	1.21	8	NB	46	NB	.22	.3	7	5	19	1.83	.03	.30	181	NB	.01	12	.03	12	NB	NB	NB	NB	16	NB	ND	70
L 9+50N 1+00S	.1	1.44	11	ND	60	NB	.22	.5	7	5	21	1.99	.03	.34	250	1	.01	14	.03	23	NB	NB	NB	NB	19	NB	NB	138
L 9+50N 1+25S	1.5	1.34	26	ND	48	NB	.25	.9	8	7	51	2.23	.04	.43	287	1	.01	20	.03	46	NB	NB	NB	NB	22	NB	NB	247
L 9+50N 1+50S	.1	1.57	11	ND	103	NB	.25	.9	6	5	24	1.79	.03	.33	500	1	.01	13	.06	19	NB	NB	NB	NB	25	NB	NB	198
L 9+50N 1+75S	.1	1.62	17	NB	74	NB	.24	.3	8	6	39	2.03	.03	.35	372	1	.01	14	.05	18	NB	NB	NB	NB	20	NB	NB	118
L 9+50N 2+00S	.1	2.23	17	NB	123	NB	.27	.2	9	6	30	2.16	.03	.39	407	1	.01	16	.06	22	NB	NB	NB	NB	27	NB	NB	125
L 9+50N 2+25S	.1	1.92	15	ND	80	NB	.21	.2	9	6	31	2.30	.03	.41	333	1	.01	19	.03	16	NB	NB	NB	NB	22	NB	NB	75
L 9+50N 2+50S	.1	2.27	20	NB	139	NB	.20	.1	9	7	23	2.25	.03	.40	564	1	.01	17	.06	17	NB	NB	NB	NB	20	NB	NB	124
L 9+50N 2+75S	.1	1.86	9	NB	107	NB	.22	.2	7	6	15	1.92	.03	.38	364	1	.01	15	.03	13	NB	NB	NB	NB	20	NB	NB	107
L 9+50N 3+00S	.1	3.46	4	ND	88	NB	.68	.4	10	7	50	2.67	.06	.70	392	1	.01	19	.03	4	NB	NB	NB	NB	51	NB	NB	106
L 9+50N 3+25S	.1	3.16	5	ND	206	NB	.32	.2	9	7	21	2.41	.04	.54	449	2	.01	20	.07	11	NB	NB	NB	NB	28	NB	NB	193
L 9+50N 3+50S	.1	3.27	8	ND	263	NB	.49	.3	11	8	28	2.67	.05	.66	820	2	.01	21	.09	10	NB	NB	NB	NB	58	NB	NB	164
L 9+50N 3+75S	.1	2.14	8	NB	99	NB	.30	.1	9	7	20	2.24	.04	.48	307	1	.01	16	.04	9	NB	NB	NB	NB	27	NB	NB	86
L 9+50N 4+00S	.3	2.20	8	ND	96	NB	.25	.1	9	7	21	2.29	.04	.48	275	1	.01	17	.04	10	NB	NB	NB	NB	25	NB	NB	87
L 9+50N 4+25S	.1	1.95	5	ND	102	NB	.24	.3	8	7	30	2.16	.04	.42	271	1	.01	16	.02	12	NB	NB	NB	NB	23	NB	NB	98
L 9+50N 4+50S	.1	2.55	9	ND	136	NB	.29	.1	9	8	22	2.41	.05	.45	395	1	.01	22	.05	10	NB	NB	NB	NB	28	NB	NB	94
L 9+50N 4+75S	.1	3.79	4	ND	193	NB	.90	.4	13	9	42	3.13	.08	.73	1192	2	.01	20	.04	11	NB	NB	NB	NB	73	NB	NB	149
L 9+50N 5+00S	.3	2.12	6	ND	110	NB	.29	.2	9	7	20	2.21	.05	.42	312	1	.01	17	.03	9	NB	NB	NB	NB	26	NB	NB	76
L 10+00N 0+00 BL	.1	1.57	8	ND	149	NB	.30	.4	6	5	17	1.60	.03	.34	1258	1	.01	14	.05	11	NB	NB	NB	NB	26	NB	NB	175
L 10+00N 0+50N	.1	1.80	10	ND	154	ND	.29	.2	7	5	16	1.83	.04	.34	789	1	.01	14	.04	12	NB	NB	NB	NB	26	NB	NB	83
L 10+00N 1+00N	.1	1.71	14	ND	211	NB	.35	.2	8	6	17	1.75	.03	.30	1007	2	.01	15	.07	18	NB	NB	NB	ND	30	NB	NB	116
L 10+00N 1+50N	.1	1.38	12	NB	130	NB	.35	.2	7	6	18	1.82	.03	.31	569	1	.01	15	.04	17	NB	NB	NB	NB	30	ND	NB	79
L 10+00N 2+00N	.1	.97	7	ND	65	NB	.20	.2	6	6	10	1.57	.02	.29	327	1	.01	9	.02	11	NB	NB	NB	NB	21	NB	NB	52
L 10+00N 2+50N	.1	2.14	37	ND	68	NB	.47	.1	10	11	70	2.83	.04	.76	506	2	.01	25	.06	13	NB	NB	NB	NB	43	ND	NB	98
L 10+00N 3+00N	.1	1.41	12	NB	155	NB	.51	.1	10	13	35	1.92	.05	.45	1146	1	.01	22	.16	22	NB	NB	NB	NB	47	NB	NB	130
L 10+00N 3+50N	.1	3.00	4	ND	66	ND	.75	.1	10	5	53	2.49	.06	.67	435	1	.01	14	.04	1	NB	NB	NB	NB	72	NB	NB	68
L 10+00N 4+00N	.1	2.43	6	NB	167	NB	.29	.1	8	6	19	2.08	.04	.36	735	1	.01	16	.05	8	NB	NB	NB	NB	26	NB	NB	103
L 10+00N 4+50N	.1	2.39	5	ND	127	NB	.31	.2	8	6	20	2.16	.04	.44	426	1	.01	16	.05	7	NB	NB	NB	NB	25	NB	NB	106
L 10+00N 5+00N	.1	3.06	5	NB	151	NB	.53	.1	9	5	18	2.38	.05	.56	717	1	.01	18	.04	1	NB	NB	NB	NB	45	NB	NB	84
L 10+00N 5+50N	.1	3.34	5	ND	160	NB	.41	.3	10	7	32	2.66	.05	.56	806	2	.01	19	.03	16	NB	NB	NB	NB	37	NB	NB	141
L 10+00N 6+00N	.1	3.27	9	NB	212	NB	.57	.2	9	4	19	2.37	.05	.51	1492	2	.01	16	.12	3	NB	NB	NB	NB	50	NB	NB	120
L 10+00N 6+50N	.1	3.39	69	NB	117	NB	.67	.7	17	10	80	3.34	.05	.83	1482	3	.01	46	.05	9	NB	NB	NB	NB	68	NB	NB	299
L 10+00N 7+00N	.1	2.67	35	NB	126	NB	.87	2.5	13	15	85	3.04	.06	.85	1720	3	.01	57	.09	55	NB	NB	NB	NB	63	NB	NB	460
L 10+00N 7+50N	.6	3.39	112	NB	88	NB	.72	1.2	14	15	167	3.90	.06	.95	900	4	.01	100	.04	28	NB	NB	NB	NB	59	NB	NB	347
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L10+00W 0+00N	.1	2.36	35	ND	189	ND	.83	1.5	16	10	92	2.81	.06	.57	2397	3	.01	77	.09	11	ND	ND	ND	ND	64	ND	ND	431
L10+00W 0+25S	.1	1.88	15	ND	140	ND	.28	.4	7	5	21	1.80	.04	.30	540	1	.01	13	.06	9	ND	ND	ND	ND	26	ND	ND	140
L10+00W 0+50S	.2	1.39	8	ND	119	ND	.23	.5	6	4	18	1.57	.03	.28	328	1	.01	10	.05	11	ND	ND	ND	ND	23	ND	ND	200
L10+00W 0+75S	.6	2.30	25	ND	93	ND	.38	.4	10	7	76	2.34	.04	.44	339	1	.01	21	.03	20	ND	ND	ND	ND	32	ND	ND	144
L10+00W 1+00S	.2	1.66	16	ND	79	ND	.26	.6	8	6	33	1.96	.03	.38	348	1	.01	12	.07	13	ND	ND	ND	ND	25	ND	ND	126
L10+00W 1+25S	.1	1.95	12	ND	138	ND	.20	.9	8	6	23	1.90	.03	.33	577	2	.01	15	.09	13	ND	ND	ND	ND	20	ND	ND	220
L10+00W 1+50S	.1	1.72	13	ND	134	ND	.30	.5	8	5	26	1.80	.04	.32	739	2	.01	12	.04	13	ND	ND	ND	ND	26	ND	ND	168
L10+00W 1+75S	.2	1.74	17	ND	129	ND	.32	.6	11	7	32	2.36	.04	.46	929	2	.01	16	.06	16	ND	ND	ND	ND	26	ND	ND	147
L10+00W 2+00S	.1	1.84	12	ND	98	ND	.39	.3	7	4	62	1.67	.03	.30	625	1	.01	12	.04	11	ND	ND	ND	ND	28	ND	ND	144
L10+00W 2+25S	.1	1.22	10	ND	117	ND	.19	.2	6	4	11	1.47	.02	.25	545	1	.01	8	.04	11	ND	ND	ND	ND	19	ND	ND	125
L10+00W 2+50S	.1	1.92	11	ND	112	ND	.24	.3	7	6	16	1.82	.03	.36	421	1	.01	14	.06	10	ND	ND	ND	ND	24	ND	ND	116
L10+00W 2+75S	.1	2.10	16	ND	111	ND	.27	.3	9	7	30	2.18	.03	.44	412	1	.01	16	.08	13	ND	ND	ND	ND	27	ND	ND	117
L10+00W 3+00S	.6	2.46	7	ND	93	ND	.26	.3	9	7	46	2.09	.04	.44	288	2	.01	13	.04	5	ND	ND	ND	ND	29	ND	ND	80
L10+00W 3+25S	.1	1.81	11	ND	80	ND	.26	.3	8	9	24	2.16	.03	.44	280	1	.01	12	.03	6	ND	ND	ND	ND	27	ND	ND	67
L10+00W 3+50S	.1	1.47	5	ND	107	ND	.23	.3	6	5	11	1.59	.03	.31	296	1	.01	10	.03	5	ND	ND	ND	ND	19	ND	ND	114
L10+00W 3+75S	.1	1.40	5	ND	119	ND	.22	.3	6	6	9	1.39	.03	.25	456	1	.01	9	.05	5	ND	ND	ND	ND	22	ND	ND	88
L10+00W 4+00S	.1	1.65	8	ND	147	ND	.29	.3	7	6	12	1.51	.03	.29	510	2	.01	11	.05	7	ND	ND	ND	ND	26	ND	ND	93
L10+00W 4+25S	.2	1.26	4	ND	145	ND	.25	.3	6	6	11	1.54	.03	.29	591	1	.01	9	.03	6	ND	ND	ND	ND	22	ND	ND	89
L10+00W 4+50S	.1	1.01	4	ND	126	ND	.26	.3	6	5	11	1.42	.03	.27	641	1	.01	8	.02	6	ND	ND	ND	ND	24	ND	ND	91
L10+00W 4+75S	.1	1.48	7	ND	130	ND	.34	.3	8	7	17	1.73	.04	.32	633	2	.01	10	.03	7	ND	ND	ND	ND	23	ND	ND	106
L10+00W 5+00S	.1	1.26	6	ND	137	ND	.29	.2	7	6	12	1.61	.04	.31	619	1	.01	10	.02	8	ND	ND	ND	ND	26	ND	ND	83
L10+00W 5+50S	.1	.94	7	ND	89	ND	.23	.3	6	6	11	1.48	.04	.28	351	1	.01	8	.02	8	ND	ND	ND	ND	22	ND	ND	57
L10+00W 6+00S	.1	1.22	9	ND	94	ND	.26	.1	7	6	12	1.58	.03	.30	519	1	.01	10	.03	6	ND	ND	ND	ND	22	ND	ND	65
L10+00W 6+50S	.2	2.26	12	ND	155	ND	.25	.2	8	7	23	1.94	.04	.33	308	1	.01	15	.06	7	ND	ND	ND	ND	28	ND	ND	95
L10+00W 7+00S	.1	1.48	8	ND	189	ND	.29	.3	6	5	14	1.55	.04	.25	743	1	.01	12	.05	8	ND	ND	ND	ND	32	ND	ND	103
L10+00W 7+50S	.2	1.97	9	ND	115	ND	.40	.4	8	7	25	1.80	.04	.35	380	1	.01	14	.05	8	ND	ND	ND	ND	28	ND	ND	79
L10+00W 8+00S	.1	1.27	9	ND	133	ND	.35	.2	6	5	16	1.54	.04	.26	628	1	.01	8	.04	7	ND	ND	ND	ND	33	ND	ND	84
L10+50W 0+00 BL	.2	2.13	11	ND	146	ND	.27	2.0	8	5	27	2.08	.04	.37	566	1	.01	13	.05	17	ND	ND	ND	ND	27	ND	ND	539
L10+50W 0+25N	.2	2.28	13	ND	150	ND	.49	1.4	8	5	51	1.93	.05	.32	687	2	.01	13	.13	11	ND	ND	ND	ND	41	ND	ND	259
L10+50W 0+50N	.1	1.44	12	ND	99	ND	.21	.8	8	5	17	1.84	.04	.35	486	1	.01	13	.04	11	ND	ND	ND	ND	20	ND	ND	135
L10+50W 0+75N	.1	1.50	13	ND	95	ND	.25	.5	7	5	20	1.86	.04	.34	399	1	.01	13	.05	13	ND	ND	ND	ND	26	ND	ND	107
L10+50W 1+00N	.1	2.09	15	ND	96	ND	.30	.4	8	7	32	2.26	.04	.41	341	1	.01	13	.03	13	ND	ND	ND	ND	30	ND	ND	70
L10+50W 1+25N	.1	2.00	11	ND	166	ND	.32	.5	8	6	24	2.07	.04	.37	804	2	.01	15	.07	14	ND	ND	ND	ND	30	ND	ND	115
L10+50W 1+50N	.1	1.61	12	ND	85	ND	.29	.4	8	5	18	1.92	.04	.37	481	1	.01	12	.02	18	ND	ND	ND	ND	26	ND	ND	73
L10+50W 0+25S	.2	1.76	13	ND	124	ND	.26	.6	7	5	19	1.95	.03	.35	567	1	.01	11	.06	13	ND	ND	ND	ND	26	ND	ND	300
L10+50W 0+50S	.4	1.55	11	ND	98	ND	.23	.4	7	5	23	1.72	.04	.32	466	1	.01	13	.04	16	ND	ND	ND	ND	20	ND	ND	207
L10+50W 0+75S	.4	1.84	12	ND	87	ND	.22	.3	8	6	24	2.01	.04	.35	335	1	.01	15	.05	13	ND	ND	ND	ND	21	ND	ND	136
L10+50W 1+00S	.2	1.91	12	ND	137	ND	.28	.3	8	6	26	2.00	.04	.35	474	1	.01	18	.15	14	ND	ND	ND	ND	35	ND	ND	158
L10+50W 1+25S	.2	2.13	23	ND	87	ND	.41	.3	9	7	111	2.27	.05	.44	597	1	.01	19	.03	14	ND	ND	ND	ND	27	ND	ND	127
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L 10+50N 1+50S	.1	1.90	22	ND	74	ND	.27	.2	9	6	78	2.21	.04	.42	368	1	.01	18	.03	13	ND	ND	ND	ND	24	ND	ND	112
L 10+50N 1+75S	.1	1.95	17	ND	83	ND	.24	.4	9	5	38	2.21	.04	.43	299	1	.01	16	.04	15	ND	ND	ND	ND	25	ND	ND	80
L 10+50N 2+00S	.1	2.19	9	ND	93	ND	.25	.3	8	6	35	2.16	.03	.40	299	1	.01	14	.04	9	ND	ND	ND	ND	21	ND	ND	95
L 10+50N 2+25S	.1	2.22	24	ND	127	ND	.25	.3	10	8	30	2.25	.04	.39	273	1	.01	23	.06	16	ND	ND	ND	ND	28	ND	ND	136
L 10+50N 2+50S	.1	2.30	15	ND	124	ND	.28	.4	9	6	19	2.26	.05	.43	327	2	.01	18	.04	13	ND	ND	ND	ND	26	ND	ND	114
L 10+50N 2+75S	.1	2.12	9	ND	127	ND	.31	.2	9	6	22	2.08	.05	.43	485	2	.01	16	.07	10	ND	ND	ND	ND	30	ND	ND	125
L 10+50N 3+00S	.1	1.77	9	ND	86	ND	.39	.3	10	8	26	2.24	.06	.48	366	1	.01	14	.03	7	ND	ND	ND	ND	32	ND	ND	73
L 10+50N 3+25S	.1	3.30	7	ND	103	ND	.97	.4	11	8	23	2.66	.08	.69	600	2	.01	18	.07	1	ND	ND	ND	ND	116	ND	ND	86
L 10+50N 3+50S	.2	1.61	11	ND	98	ND	.24	.4	7	6	15	1.80	.04	.34	212	1	.01	15	.05	10	ND	ND	ND	ND	22	ND	ND	84
L 10+50N 3+75S	.1	1.70	13	ND	116	ND	.21	.4	9	7	17	1.96	.05	.36	281	1	.01	18	.07	10	ND	ND	ND	ND	21	ND	ND	113
L 10+50N 4+00S	.2	1.27	13	ND	80	ND	.27	.4	8	6	16	1.79	.05	.36	261	1	.01	14	.03	10	ND	ND	ND	1	22	ND	ND	67
L 10+50N 4+25S	.1	1.58	9	ND	149	ND	.24	.2	7	5	15	1.65	.05	.28	427	2	.01	14	.05	8	ND	ND	ND	ND	22	ND	ND	120
L 10+50N 4+50S	.1	1.28	7	ND	94	ND	.25	.3	7	6	11	1.73	.04	.32	344	1	.01	12	.02	8	ND	ND	ND	ND	19	ND	ND	69
L 10+50N 4+75S	.1	1.25	7	ND	87	ND	.37	.4	9	7	18	2.08	.05	.42	471	1	.01	16	.05	8	ND	ND	ND	ND	27	ND	ND	65
L 10+50N 5+00S	.1	1.49	8	ND	97	ND	.25	.4	7	6	13	1.71	.05	.30	308	1	.01	13	.03	9	ND	ND	ND	ND	22	ND	ND	78
L 11+00N 0+00 BL	.1	1.46	22	ND	61	ND	.24	.2	9	7	30	2.17	.05	.39	346	2	.01	17	.04	15	ND	ND	ND	ND	22	ND	ND	102
L 11+00N 0+50N	1.1	2.39	12	ND	209	3	.53	6.2	10	8	63	2.45	.06	.42	1261	2	.01	20	.16	45	ND	ND	ND	ND	48	ND	ND	1254
L 11+00N 1+00N	.1	1.87	19	ND	220	ND	.37	.5	9	6	28	2.07	.05	.40	846	3	.01	19	.15	18	ND	ND	ND	ND	47	ND	ND	142
L 11+00N 1+50N	.1	1.62	18	ND	120	ND	.33	.6	10	6	31	2.05	.05	.39	839	2	.01	17	.05	17	ND	ND	ND	ND	28	ND	ND	114
L 11+00N 2+00N	.1	1.21	9	ND	80	ND	.32	.4	7	6	18	1.52	.05	.31	631	2	.01	11	.02	15	ND	ND	ND	ND	26	ND	ND	75
L 11+00N 2+50N	.1	1.93	10	ND	103	ND	.30	.5	8	9	20	1.93	.05	.39	520	2	.01	19	.06	11	ND	ND	ND	ND	26	ND	ND	91
L 11+00N 3+00N	.1	2.06	5	ND	383	ND	1.42	.6	11	9	28	2.07	.07	.65	2849	1	.01	16	.24	7	ND	ND	ND	ND	129	ND	ND	124
L 11+00N 4+00N	.1	3.75	3	ND	92	ND	.88	.4	13	6	26	3.03	.07	.80	602	2	.01	20	.05	ND	ND	ND	ND	ND	88	ND	ND	76
L 11+00N 4+50N	.1	1.15	9	ND	53	ND	.29	.4	9	5	17	2.07	.05	.38	489	1	.01	13	.01	14	ND	ND	ND	ND	23	ND	ND	61
L 11+00N 5+00N	.1	2.10	8	ND	501	ND	.90	1.2	11	5	32	2.06	.06	.54	2335	3	.01	17	.18	11	ND	ND	ND	ND	77	ND	ND	277
L 11+00N 5+50N	.1	3.33	12	ND	162	ND	.65	.3	11	5	29	2.56	.07	.58	1165	2	.01	19	.10	2	ND	ND	ND	ND	56	ND	ND	114
L 11+00N 6+00N	.6	3.51	268	ND	17	ND	1.23	.2	16	14	292	4.39	.07	1.36	976	3	.01	56	.06	ND	ND	ND	ND	ND	141	ND	ND	172
L 11+00N 6+50N	.7	3.88	107	ND	55	ND	.86	1.0	21	21	254	4.02	.07	1.32	910	4	.01	98	.04	14	ND	ND	ND	ND	59	ND	ND	266
L 11+00N 7+00N	1.1	3.48	89	ND	77	ND	.78	2.0	18	22	183	4.04	.08	1.32	1036	9	.01	71	.05	60	ND	ND	ND	ND	55	ND	ND	405
L 11+00N 7+50N	1.1	2.23	203	ND	60	ND	2.51	1.7	19	37	176	3.93	.09	1.28	1116	9	.01	100	.08	57	ND	ND	ND	25	84	ND	ND	302
L 11+00N 8+00N	1.3	2.47	232	ND	68	ND	2.77	1.9	21	21	195	4.30	.10	1.40	1246	7	.01	97	.08	27	ND	ND	ND	ND	93	ND	ND	325
L 11+00N 0+25S	.1	1.64	11	ND	147	ND	.31	.6	8	6	22	1.91	.05	.34	638	2	.01	20	.14	15	ND	ND	ND	ND	36	ND	ND	193
L 11+00N 0+50S	.3	2.09	14	ND	92	ND	.36	.4	9	6	51	2.15	.05	.42	354	2	.01	21	.04	12	ND	ND	ND	ND	27	ND	ND	104
L 11+00N 0+75S	.1	1.86	8	ND	127	ND	.23	.3	8	6	18	1.85	.04	.33	458	2	.01	17	.09	13	ND	ND	ND	ND	24	ND	ND	183
L 11+00N 1+00S	.1	1.88	9	ND	117	ND	.25	.3	8	5	25	1.69	.04	.31	468	2	.01	16	.09	12	ND	ND	ND	ND	22	ND	ND	207
L 11+00N 1+25S	.1	1.35	11	ND	58	ND	.21	.4	8	6	36	1.73	.04	.34	313	2	.01	15	.02	13	ND	ND	ND	ND	16	ND	ND	98
L 11+00N 1+50S	.2	1.78	8	ND	101	ND	.33	.4	10	7	77	2.07	.05	.44	600	2	.01	16	.02	15	ND	ND	ND	ND	27	ND	ND	98
L 11+00N 1+75S	.1	1.85	12	ND	91	ND	.50	.5	8	7	81	2.04	.05	.38	809	2	.01	17	.05	15	ND	ND	ND	ND	30	ND	ND	154
L 11+00N 2+00S	.1	1.74	7	ND	119	ND	.19	.5	7	4	19	1.84	.04	.33	606	2	.01	13	.07	25	ND	ND	ND	ND	20	ND	ND	177
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L11+00W 2+25S	.1	1.64	8	ND	95	ND	.17	.5	7	4	15	1.76	.04	.33	341	1	.01	17	.03	16	ND	ND	ND	ND	16	ND	ND	158
L11+00W 2+50S	.1	1.54	12	ND	130	ND	.32	.4	6	3	18	1.54	.04	.26	633	1	.01	16	.05	16	ND	ND	ND	ND	32	ND	ND	127
L11+00W 2+75S	.1	1.17	9	ND	91	ND	.20	.2	5	4	17	1.60	.04	.32	466	1	.01	16	.02	10	ND	ND	ND	ND	21	ND	ND	52
L11+00W 3+00S	.1	1.20	12	ND	88	ND	.18	.2	6	5	12	1.59	.04	.29	389	1	.01	16	.02	9	ND	ND	ND	ND	16	ND	ND	87
L11+00W 3+25S	.2	1.27	10	ND	97	ND	.23	.3	6	5	10	1.45	.04	.27	375	1	.01	14	.04	8	ND	ND	ND	ND	20	ND	ND	74
L11+00W 3+50S	.2	1.81	10	ND	106	ND	.21	.4	8	6	17	1.82	.04	.34	342	1	.01	20	.05	9	ND	ND	ND	ND	20	ND	ND	86
L11+00W 3+75S	.2	1.27	8	ND	68	ND	.24	.4	6	6	12	1.60	.05	.32	266	1	.01	15	.02	7	ND	ND	ND	ND	18	ND	ND	82
L11+00W 4+00S	.2	1.42	8	ND	115	ND	.25	.2	7	6	14	1.74	.05	.33	414	1	.01	16	.05	10	ND	ND	ND	ND	21	ND	ND	99
L11+00W 4+25S	.1	1.63	10	ND	152	ND	.28	.3	7	5	15	1.60	.04	.29	705	2	.01	18	.11	13	ND	ND	ND	ND	25	ND	ND	120
L11+00W 4+50S	.5	1.94	18	ND	94	ND	.36	.5	9	6	37	1.89	.06	.34	281	1	.01	22	.06	12	ND	ND	ND	ND	27	ND	ND	106
L11+00W 4+75S	.2	1.59	11	ND	122	ND	.27	.4	7	7	12	1.56	.05	.27	563	2	.01	20	.07	12	ND	ND	ND	ND	25	ND	ND	83
L11+00W 5+00S	.2	1.69	14	ND	105	ND	.18	.2	7	6	13	1.66	.05	.28	305	1	.01	23	.14	11	ND	ND	ND	ND	21	ND	ND	112
L11+00W 5+50S	.1	1.19	10	ND	76	ND	.25	.2	6	4	14	1.49	.04	.23	295	1	.01	16	.05	7	ND	ND	ND	ND	20	ND	ND	77
L11+00W 6+00S	.1	1.53	14	ND	92	ND	.29	.2	6	4	10	1.40	.04	.21	351	1	.01	18	.05	10	ND	ND	ND	ND	21	ND	ND	83
L12+00W 0+00 BL	.2	2.19	17	ND	101	ND	.38	.5	10	7	37	2.11	.05	.40	470	1	.01	34	.04	12	ND	ND	ND	ND	26	ND	ND	75
L12+00W 0+50N	.2	1.58	17	ND	150	ND	.32	.5	8	6	25	1.99	.05	.36	615	1	.01	22	.07	15	ND	ND	ND	ND	37	ND	ND	173
L12+00W 1+00N	.1	1.85	20	ND	135	ND	.27	.3	9	6	27	2.07	.05	.36	587	1	.01	25	.08	15	ND	ND	ND	ND	27	ND	ND	129
L12+00W 1+50N	.1	1.52	17	ND	158	ND	.31	.5	8	5	22	1.82	.05	.32	739	1	.01	22	.08	17	ND	ND	ND	ND	35	ND	ND	153
L12+00W 2+00N	.2	1.37	15	ND	105	ND	.32	.4	8	6	23	1.85	.05	.36	724	1	.01	22	.03	17	ND	ND	ND	ND	26	ND	ND	103
L12+00W 2+50N	.2	1.40	7	ND	117	ND	.21	.4	6	5	10	1.37	.04	.24	378	1	.01	21	.04	9	ND	ND	ND	ND	23	ND	ND	119
L12+00W 3+00N	.2	2.30	3	ND	101	ND	.31	.3	9	7	12	2.05	.05	.55	335	ND	.01	21	.04	3	ND	ND	ND	ND	32	ND	ND	78
L12+00W 3+50N	.2	2.45	7	ND	71	ND	.43	.4	9	6	22	2.26	.06	.54	353	1	.01	24	.04	5	ND	ND	ND	ND	43	ND	ND	78
L12+00W 4+00N	.4	3.58	20	ND	136	ND	.77	.7	17	13	85	3.81	.09	1.14	1498	1	.01	42	.06	21	ND	ND	ND	ND	58	ND	ND	181
L12+00W 4+50N	.4	2.98	ND	ND	249	ND	1.15	.6	17	8	33	3.46	.08	1.16	1400	ND	.01	35	.14	ND	ND	ND	ND	ND	70	ND	ND	151
L12+00W 5+00N	.2	2.20	13	ND	72	ND	.43	.6	12	7	61	2.81	.06	.63	580	1	.01	27	.03	25	ND	ND	ND	ND	39	ND	ND	148
L12+00W 5+50N	.4	3.29	6	ND	106	ND	.69	1.1	20	10	180	3.44	.07	.81	1187	1	.01	53	.09	9	ND	ND	ND	ND	60	ND	ND	266
L12+00W 6+00N	.5	3.06	23	ND	56	ND	1.00	1.2	42	20	233	5.32	.08	1.62	1925	1	.01	91	.10	ND	ND	ND	ND	ND	73	ND	ND	252
L12+00W 6+50N	.1	3.02	63	ND	130	ND	.85	2.5	22	8	124	3.34	.07	.79	2312	2	.01	55	.09	11	ND	ND	ND	ND	52	ND	ND	432
L12+00W 7+00N	.2	2.13	54	ND	95	ND	.40	1.1	13	7	79	2.71	.06	.46	1117	3	.01	32	.04	35	ND	ND	ND	ND	27	ND	ND	243
L12+00W 7+50N	.1	2.46	133	ND	114	ND	.49	1.6	24	18	100	3.14	.06	.93	1876	4	.01	65	.07	13	ND	ND	ND	ND	37	ND	ND	263
L12+00W 8+00N	.2	1.81	50	ND	159	ND	.92	5.4	17	14	106	3.29	.07	.60	2362	5	.01	111	.10	35	ND	ND	ND	ND	49	ND	ND	433
L12+00W 0+25S	.1	2.07	7	ND	218	ND	.45	.7	10	7	33	2.27	.06	.45	1147	1	.01	27	.16	13	ND	ND	ND	ND	49	ND	ND	156
L12+00W 0+50S	.1	2.06	11	ND	235	ND	.35	.4	9	6	26	1.98	.05	.37	1279	1	.01	23	.11	13	ND	ND	ND	ND	35	ND	ND	152
L12+00W 0+75S	.1	1.96	13	ND	147	ND	.35	.2	9	5	26	1.99	.05	.41	662	1	.01	25	.07	11	ND	ND	ND	ND	31	ND	ND	73
L12+00W 1+00S	.1	2.06	10	ND	143	ND	.31	.4	10	6	24	2.31	.05	.44	613	1	.01	24	.06	13	ND	ND	ND	ND	26	ND	ND	88
L12+00W 1+25S	.1	2.06	15	ND	205	ND	.34	.5	10	5	26	2.11	.05	.41	1038	1	.01	21	.10	12	ND	ND	ND	ND	32	ND	ND	124
L12+00W 1+50S	.1	2.05	11	ND	177	ND	.35	.2	9	6	25	2.13	.05	.43	822	1	.01	24	.09	11	ND	ND	ND	ND	35	ND	ND	112
L12+00W 1+75S	.1	1.85	17	ND	89	ND	.39	.3	7	4	39	1.56	.05	.32	479	1	.01	18	.07	8	ND	ND	ND	ND	28	ND	ND	74
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L12+00N 2+00S	.1	1.81	12	ND	125	ND	.22	.1	6	4	22	1.64	.03	.31	477	1	.01	14	.07	11	ND	ND	ND	ND	21	ND	ND	106
L12+00N 2+25S	.1	1.40	14	ND	243	ND	.58	.4	7	4	17	1.57	.04	.33	1738	1	.01	16	.12	17	ND	ND	ND	ND	54	ND	ND	147
L12+00N 2+50S	.1	1.94	12	ND	98	ND	.23	.3	8	5	20	2.09	.04	.39	459	1	.01	17	.03	15	ND	ND	ND	ND	21	ND	ND	95
L12+00N 2+75S	.1	1.91	9	ND	109	ND	.24	.4	8	5	20	1.84	.04	.33	513	1	.01	15	.03	14	ND	ND	ND	ND	22	ND	ND	93
L12+00N 3+00S	.1	1.93	12	ND	167	ND	.24	.2	8	5	24	1.86	.04	.36	691	1	.01	19	.06	14	ND	ND	ND	ND	25	ND	ND	118
L12+00N 3+25S	.1	1.94	9	ND	155	ND	.25	.4	7	4	18	1.75	.03	.35	666	1	.01	15	.10	11	ND	ND	ND	ND	24	ND	ND	108
L12+00N 3+50S	.1	2.20	11	ND	142	ND	.26	.2	8	5	24	1.94	.04	.37	608	1	.01	19	.08	11	ND	ND	ND	ND	27	ND	ND	117
L12+00N 3+75S	.1	2.12	12	ND	96	ND	.26	.3	9	6	35	2.26	.04	.46	305	1	.01	19	.03	14	ND	ND	ND	ND	27	ND	ND	103
L12+00N 4+00S	.3	1.84	11	ND	151	ND	.31	.6	7	4	16	1.62	.03	.33	723	1	.01	15	.09	14	ND	ND	ND	ND	37	ND	ND	146
L12+00N 4+25S	.1	1.94	9	ND	141	ND	.31	.5	8	5	21	1.95	.03	.36	660	1	.01	19	.08	14	ND	ND	ND	ND	33	ND	ND	155
L12+00N 4+50S	.1	1.76	8	ND	78	ND	.18	.4	7	5	21	1.87	.03	.34	311	1	.01	17	.02	21	ND	ND	ND	ND	17	ND	ND	204
L12+00N 4+75S	.1	2.02	11	ND	155	ND	.33	.6	8	4	27	1.82	.04	.33	750	1	.01	17	.13	19	ND	ND	ND	ND	35	ND	ND	127
L12+00N 5+00S	.1	1.25	12	ND	41	ND	.54	.7	7	4	37	1.97	.04	.50	391	ND	.01	13	.06	60	ND	ND	ND	ND	30	ND	ND	538
L12+00N 5+50S	.3	1.43	13	ND	84	ND	.22	.2	6	4	13	1.46	.04	.23	261	ND	.01	12	.07	12	ND	ND	ND	ND	21	ND	ND	103
L12+00N 6+00S	.3	1.73	15	ND	99	ND	.21	.1	7	4	18	1.56	.03	.24	349	1	.01	16	.07	14	ND	ND	ND	ND	19	ND	ND	118
L13+00N 0+00 BL	.3	1.79	14	ND	123	ND	.23	.4	8	5	16	1.76	.04	.29	352	1	.01	16	.04	15	ND	ND	ND	ND	22	ND	ND	125
L13+00N 0+50N	.1	1.27	11	ND	133	ND	.31	.5	6	4	16	1.46	.04	.26	593	1	.01	14	.04	18	ND	ND	ND	ND	27	ND	ND	123
L13+00N 1+00N	.1	1.31	10	ND	94	ND	.28	.3	6	4	16	1.50	.03	.28	346	1	.01	12	.05	13	ND	ND	ND	ND	26	ND	ND	108
L13+00N 1+50N	.1	1.29	13	ND	261	ND	.22	.8	6	4	16	1.38	.03	.21	1015	1	.01	16	.17	19	ND	ND	ND	ND	31	ND	ND	208
L13+00N 2+00N	.1	1.59	23	ND	94	ND	.32	.3	7	5	24	1.75	.04	.30	547	1	.01	18	.06	24	ND	ND	ND	ND	24	ND	ND	131
L13+00N 2+50N	.1	1.63	19	ND	182	ND	.29	.6	7	5	20	1.60	.04	.26	736	1	.01	21	.12	22	ND	ND	ND	ND	34	ND	ND	179
L13+00N 3+00N	.1	.83	5	ND	123	ND	.32	.3	6	5	12	1.39	.04	.30	648	1	.01	11	.03	11	ND	ND	ND	ND	29	ND	ND	77
L13+00N 3+50N	.1	1.10	11	ND	99	ND	.28	.4	5	5	12	1.33	.03	.29	427	ND	.01	10	.02	11	ND	ND	ND	ND	26	ND	ND	72
L13+00N 4+00N	.1	3.23	ND	ND	106	ND	1.12	.4	11	4	20	2.65	.07	.76	1299	ND	.01	18	.07	1	ND	ND	ND	ND	64	ND	ND	80
L13+00N 4+50N	.3	3.04	10	ND	164	ND	.72	.8	14	9	68	3.44	.07	.56	1127	1	.01	35	.06	46	ND	ND	ND	ND	67	ND	ND	338
L13+00N 5+00N	.9	3.18	27	ND	84	ND	.64	.9	25	19	213	5.91	.08	1.16	884	2	.01	68	.06	19	ND	ND	ND	ND	48	ND	ND	243
L13+00N 5+50N	.3	2.05	33	ND	130	ND	.38	1.4	15	14	74	3.39	.07	.88	1192	2	.01	35	.03	57	ND	ND	ND	ND	29	ND	ND	212
L13+00N 6+00N	.1	2.77	17	ND	168	ND	.38	1.6	12	7	50	2.57	.06	.45	1395	2	.01	27	.03	89	ND	ND	ND	ND	33	ND	ND	268
L13+00N 6+50N	.1	2.50	14	ND	111	ND	.51	.6	19	16	125	3.79	.07	.99	1137	2	.01	42	.13	11	ND	ND	ND	ND	31	ND	ND	141
L13+00N 7+00N	.1	2.37	10	ND	82	ND	.35	.7	6	5	28	1.89	.05	.33	379	2	.01	16	.01	65	ND	ND	ND	ND	43	ND	ND	199
L13+00N 7+50N	.1	2.94	8	ND	101	ND	.51	1.1	9	6	64	2.23	.06	.47	799	2	.01	23	.03	14	ND	ND	ND	ND	63	ND	ND	199
L13+00N 8+00N	.1	2.25	12	ND	104	ND	.42	1.0	7	6	29	1.84	.05	.38	1285	5	.01	19	.03	44	ND	ND	ND	ND	36	ND	ND	251
L13+00N 0+50S	.3	1.24	40	ND	59	ND	.31	.2	7	7	44	2.43	.04	.41	275	1	.01	20	.03	15	ND	ND	ND	ND	21	ND	ND	64
L13+00N 1+00S	.1	1.73	13	ND	124	ND	.21	.2	7	4	18	1.66	.03	.26	448	1	.01	16	.07	12	ND	ND	ND	ND	25	ND	ND	109
L13+00N 1+50S	.1	1.48	22	ND	118	ND	.25	.4	8	5	22	1.99	.03	.33	559	1	.01	20	.06	16	ND	ND	ND	ND	24	ND	ND	133
L13+00N 2+00S	.3	1.97	21	ND	123	ND	.30	.4	7	5	26	1.73	.03	.31	241	ND	.01	17	.05	11	ND	ND	ND	ND	28	ND	ND	102
L13+00N 2+50S	.1	2.15	33	ND	116	ND	.21	.2	8	5	28	2.02	.03	.33	390	1	.01	18	.14	13	ND	ND	ND	ND	22	ND	ND	118
L13+00N 3+00S	.1	1.63	18	ND	113	ND	.30	.3	7	4	36	1.77	.03	.32	478	1	.01	18	.04	13	ND	ND	ND	ND	26	ND	ND	78
L13+00N 3+50S	.1	1.35	9	ND	93	ND	.23	.2	6	4	14	1.48	.03	.27	383	1	.01	11	.02	11	ND	ND	ND	ND	20	ND	ND	75
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L13+00W 4+00S	.2	1.97	18	ND	153	ND	.23	.5	7	4	19	1.77	.04	.30	691	1	.01	14	.12	8	ND	ND	ND	ND	25	ND	ND	112
L13+00W 4+50S	.1	1.85	12	ND	86	ND	.24	.9	7	4	57	1.69	.04	.34	495	1	.01	14	.05	10	ND	ND	ND	ND	21	ND	ND	121
L13+00W 5+00S	.1	2.20	8	ND	141	ND	.30	1.4	8	5	39	1.84	.04	.36	484	1	.01	14	.05	9	ND	ND	ND	ND	29	ND	ND	361
L14+00W 0+00 BL	.2	2.41	16	ND	107	ND	.34	.5	8	5	29	1.93	.05	.31	386	1	.01	16	.03	14	ND	ND	ND	ND	23	ND	ND	140
L14+00W 0+50N	.1	1.66	19	ND	120	ND	.18	.3	7	4	18	1.57	.03	.25	314	1	.01	16	.11	18	ND	ND	ND	ND	20	ND	ND	142
L14+00W 1+00N	.2	1.45	15	ND	103	ND	.22	.4	6	4	16	1.42	.04	.23	346	1	.01	14	.05	13	ND	ND	ND	ND	23	ND	ND	105
L14+00W 1+50N	.2	1.64	28	ND	124	ND	.30	.7	8	5	28	1.80	.04	.31	569	1	.01	21	.06	26	ND	ND	ND	ND	33	ND	ND	163
L14+00W 2+00N	.2	1.46	15	ND	100	ND	.26	.4	6	5	14	1.53	.04	.28	408	1	.01	16	.04	22	ND	ND	ND	ND	23	ND	ND	157
L14+00W 2+50N	.2	1.25	21	ND	86	ND	.25	.3	5	4	17	1.39	.04	.23	451	ND	.01	12	.05	19	ND	ND	ND	ND	26	ND	ND	125
L14+00W 3+00N	.1	1.02	24	ND	93	ND	.22	.6	5	4	16	1.44	.04	.25	442	1	.01	13	.04	19	ND	ND	ND	ND	23	ND	ND	114
L14+00W 3+50N	.2	1.13	21	ND	80	ND	.21	.3	5	4	14	1.46	.04	.24	334	1	.01	13	.04	19	ND	ND	ND	ND	22	ND	ND	97
L14+00W 4+00N	.2	1.52	16	ND	100	ND	.29	.5	9	12	25	1.98	.05	.53	542	1	.01	22	.03	21	ND	ND	ND	ND	29	ND	ND	92
L14+00W 4+50N	.2	1.53	22	ND	96	ND	.40	.6	9	10	32	2.13	.06	.52	651	1	.01	22	.06	18	ND	ND	ND	ND	33	ND	ND	100
L14+00W 5+00N	.1	3.22	50	ND	39	ND	.81	1.3	16	20	93	5.20	.07	1.58	1160	5	.01	49	.10	7	ND	ND	ND	ND	53	ND	ND	169
L14+00W 5+50N	.2	3.11	23	ND	73	ND	1.01	.8	22	26	65	5.35	.08	1.95	1324	1	.01	54	.15	2	ND	ND	ND	ND	148	ND	ND	112
L14+00W 6+00N	.1	1.68	16	ND	206	ND	.57	2.3	8	9	30	2.47	.07	.52	1856	3	.01	21	.08	110	ND	ND	ND	ND	48	ND	ND	304
L14+00W 6+50N	.2	1.60	39	ND	50	ND	.33	1.1	8	7	53	2.50	.06	.49	494	4	.01	20	.02	47	ND	ND	ND	ND	33	ND	ND	217
L14+00W 7+00N	.2	2.81	28	ND	135	ND	.50	.7	12	10	69	2.71	.07	.60	939	1	.01	27	.06	24	ND	ND	ND	ND	50	ND	ND	182
L14+00W 7+50N	.2	1.80	45	ND	131	ND	.31	1.7	8	6	36	1.85	.05	.39	1115	1	.01	19	.04	45	ND	ND	ND	ND	29	ND	ND	284
L14+00W 8+00N	.1	2.42	57	ND	78	ND	.70	.9	15	15	104	3.41	.07	.85	1450	1	.01	45	.10	6	ND	ND	ND	ND	43	ND	ND	187
L14+00W 0+50S	.2	1.15	11	ND	96	ND	.27	.4	6	4	14	1.47	.04	.27	416	1	.01	13	.05	12	ND	ND	ND	ND	22	ND	ND	90
L14+00W 1+00S	.2	.86	10	ND	61	ND	.29	.4	5	4	12	1.37	.04	.23	297	ND	.01	8	.02	8	ND	ND	ND	ND	23	ND	ND	46
L14+00W 1+50S	.2	1.63	13	ND	132	ND	.24	.5	6	4	14	1.50	.04	.22	291	1	.01	13	.04	10	ND	ND	ND	ND	23	ND	ND	83
L14+00W 2+00S	.2	1.66	12	ND	85	ND	.31	.4	6	5	18	1.50	.04	.24	262	1	.01	11	.03	9	ND	ND	ND	ND	21	ND	ND	100
L14+00W 2+50S	.2	.73	10	ND	43	ND	.25	.3	5	3	10	1.24	.04	.22	212	ND	.01	8	.02	8	ND	ND	ND	ND	19	ND	ND	35
L14+00W 3+00S	.2	1.23	10	ND	104	ND	.24	.4	5	3	14	1.34	.04	.20	441	ND	.01	9	.03	8	ND	ND	ND	ND	21	ND	ND	104
L14+00W 3+50S	.2	1.44	13	ND	90	ND	.20	.3	6	4	11	1.38	.04	.21	229	1	.01	13	.04	10	ND	ND	ND	ND	17	ND	ND	77
L14+00W 4+00S	.2	1.54	12	ND	105	ND	.26	.5	6	4	19	1.55	.04	.23	259	1	.01	12	.06	13	ND	ND	ND	ND	20	ND	ND	133
L14+00W 4+50S	.2	1.62	11	ND	135	ND	.30	2.4	6	4	17	1.55	.04	.26	428	1	.01	13	.06	10	ND	ND	ND	ND	28	ND	ND	239
L14+00W 5+00S	.2	1.92	19	ND	144	ND	.27	.8	8	5	25	1.88	.04	.34	447	1	.01	17	.10	11	ND	ND	ND	ND	28	ND	ND	144
L15+00W 0+00 BL	.1	2.05	13	ND	129	ND	.26	.4	7	4	17	1.74	.04	.30	594	1	.01	13	.09	13	ND	ND	ND	ND	26	ND	ND	102
L15+00W 0+50N	.2	2.55	21	ND	148	ND	.26	.3	8	5	25	2.01	.05	.34	359	1	.01	17	.08	11	ND	ND	ND	ND	28	ND	ND	84
L15+00W 1+00N	.1	1.74	15	ND	120	ND	.34	.8	7	4	23	1.75	.04	.31	620	1	.01	13	.06	10	ND	ND	ND	ND	29	ND	ND	147
L15+00W 1+50N	.1	2.25	6	ND	133	ND	.41	.6	7	3	27	1.89	.05	.37	827	1	.01	12	.05	9	ND	ND	ND	ND	33	ND	ND	107
L15+00W 2+00N	.2	1.45	11	ND	67	ND	.24	.5	6	4	16	1.65	.04	.28	241	ND	.01	10	.03	10	ND	ND	ND	ND	20	ND	ND	89
L15+00W 2+50N	.2	1.26	10	ND	65	ND	.24	.3	6	4	14	1.39	.04	.23	317	ND	.01	9	.04	9	ND	ND	ND	ND	24	ND	ND	58
L15+00W 3+00N	.1	1.06	11	ND	76	ND	.20	.2	5	4	12	1.33	.03	.23	355	ND	.01	10	.07	14	ND	ND	ND	ND	23	ND	ND	111
L15+00W 3+50N	.2	.92	15	ND	56	ND	.36	.3	7	4	29	1.73	.04	.32	433	ND	.01	11	.06	10	ND	ND	ND	ND	27	ND	ND	54
L15+00W 4+00N	.2	1.18	8	ND	62	ND	.27	.4	6	4	13	1.52	.04	.26	313	ND	.01	12	.03	6	ND	ND	ND	ND	23	ND	ND	59
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
L15+00N 4+50W	.1	.96	10	ND	53	ND	.34	.3	6	4	19	1.59	.05	.25	280	ND	.01	13	.03	10	ND	ND	ND	ND	22	ND	ND	51
L15+00N 5+00W	.1	.96	17	ND	51	ND	.41	.3	7	5	33	1.85	.05	.31	359	ND	.01	15	.03	10	ND	ND	ND	ND	26	ND	ND	53
L15+00N 5+50W	.1	1.31	12	ND	117	ND	.33	.5	6	5	26	1.87	.05	.32	641	ND	.01	16	.04	9	ND	ND	ND	ND	28	ND	ND	118
L15+00N 6+00W	.3	1.39	20	ND	70	ND	.33	.7	9	6	37	2.24	.06	.50	610	1	.01	20	.02	64	ND	ND	ND	ND	26	ND	ND	168
L15+00N 6+50W	.1	2.24	43	ND	81	ND	.42	.9	9	9	46	2.44	.06	.49	611	2	.01	25	.03	27	ND	ND	ND	ND	28	ND	ND	356
L15+00N 7+00W	.1	2.13	52	ND	158	ND	.43	2.0	14	9	60	2.58	.05	.50	1843	2	.01	30	.08	49	ND	ND	ND	ND	35	ND	ND	284
L15+00N 7+50W	.1	2.02	41	ND	104	ND	.36	.3	12	8	44	2.50	.06	.51	751	1	.01	24	.06	10	ND	ND	ND	ND	32	ND	ND	153
L15+00N 8+00W	.1	2.71	32	ND	206	ND	.44	.4	17	15	98	3.56	.08	.95	1133	1	.01	36	.06	3	ND	ND	ND	ND	33	ND	ND	138
L15+00N 0+50S	.1	1.76	11	ND	63	ND	.19	.1	7	4	15	1.79	.04	.33	244	1	.01	13	.03	12	ND	ND	ND	ND	16	ND	ND	74
L15+00N 1+00S	.1	1.49	8	ND	112	ND	.19	.3	5	2	12	1.44	.03	.25	571	1	.01	13	.04	13	ND	ND	ND	ND	19	ND	ND	112
L15+00N 1+50S	.1	1.65	10	ND	110	ND	.21	.4	6	4	17	1.55	.04	.25	307	1	.01	14	.09	13	ND	ND	ND	ND	20	ND	ND	107
L15+00N 2+00S	.1	.86	9	ND	93	ND	.23	.2	4	2	9	1.08	.03	.17	476	1	.01	8	.02	8	ND	ND	ND	ND	19	ND	ND	77
L15+00N 2+50S	.1	1.27	11	ND	85	ND	.22	.2	6	4	13	1.56	.04	.24	261	1	.01	12	.01	10	ND	ND	ND	ND	18	ND	ND	52
L15+00N 3+00S	.1	1.58	15	ND	91	ND	.22	.2	6	3	13	1.50	.04	.26	334	1	.01	11	.07	11	ND	ND	ND	ND	19	ND	ND	171
L15+00N 3+50S	.1	1.02	12	ND	59	ND	.22	.2	6	4	12	1.73	.04	.34	294	ND	.01	11	.02	12	ND	ND	ND	ND	18	ND	ND	71
L15+00N 4+00S	.1	1.51	11	ND	53	ND	.27	.4	6	3	17	1.71	.04	.30	292	1	.01	14	.02	11	ND	ND	ND	ND	19	ND	ND	78
L15+00N 4+50S	.3	1.55	10	ND	47	ND	.29	.4	9	4	15	2.33	.05	.51	350	ND	.01	16	.02	22	ND	ND	ND	ND	23	ND	ND	97
L15+00N 5+00S	.1	1.42	7	ND	103	ND	.26	.4	7	4	12	1.77	.04	.34	473	1	.01	12	.02	9	ND	ND	ND	ND	25	ND	ND	93
L15+00N 5+50S	.1	1.68	10	ND	173	ND	.28	.9	6	3	17	1.72	.04	.29	692	1	.01	13	.10	15	ND	ND	ND	ND	27	ND	ND	228
L15+00N 6+00S	.1	1.60	14	ND	95	ND	.19	.4	6	3	17	1.42	.03	.23	338	1	.01	12	.03	12	ND	ND	ND	ND	15	ND	ND	211
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

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GEOCHEMICAL ANALYTICAL REPORT

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DATE: Mar 07 1988
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JOB#: 880253

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REPORT COMPLETED: Mar 07 1988
ANALYSED FOR: Au ICP

INVOICE#: 880253 NA
TOTAL SAMPLES: 12
SAMPLE TYPE: 12 Soil
REJECTS: DISCARDED

SAMPLES FROM: Submitted by Mr. P. Leriche.
COPY SENT TO: All copies sent to Vancouver office.

PREPARED FOR: Mr. Peter Leriche

ANALYSED BY: VGC Staff

SIGNED: _____

GENERAL REMARK: Data disk sent to Mr. Tony Clark.

VANGEOCHEM LAB LIMITED

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REPORT NUMBER: 880253 GA JOB NUMBER: 880253 ASHWORTH EXPLORATION LTD.

SAMPLE #	Au ppb
TR 1 - S 1	5
TR 1 - S 2	nd
TR 1 - S 3	10
TR 1 - S 4	25
TR 2 - S 1	20
TR 2 - S 2	20
TR 2 - S 3	5
TR 2 - S 4	5
TR 2 - S 5	40
TR 3 - S 1	5
TR 3 - S 2	nd
TR 3 - S 3	15

DETECTION LIMIT 5

nd = none detected -- = not analysed is = insufficient sample

VANGEOCHEM LAB LIMITED

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BRANCH OFFICE: 1630 PANDORA ST. VANCOUVER B.C. V5L 1L6 PH:(604)251-5656

ICAP GEOCHEMICAL ANALYSIS

A .5 GRAM SAMPLE IS DIGESTED WITH 5 ML OF 3:1:2 HCL TO HNO3 TO H2O AT 95 DEG. C FOR 90 MINUTES AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN,FE,CA,P,CR,MG,BA,PD,AL,NA,K,W,PT AND SR. AU AND PD DETECTION IS 3 PPM.
IS= INSUFFICIENT SAMPLE, ND= NOT DETECTED, -= NOT ANALYZED

COMPANY: ASHWORTH EXPL LTD
ATTENTION:
PROJECT: 192

REPORT#: 880253PA
JOB#: 880253
INVOICE#: 880253NA

DATE RECEIVED: 88/02/24
DATE COMPLETED: 88/03/10
COPY SENT TO: P LERICHE

ANALYST

SAMPLE NAME	AG PPM	AL %	AS PPM	AU PPM	BA PPM	BI PPM	CA %	CD PPM	CO PPM	CR PPM	CU PPM	FE %	K %	MG %	MN PPM	MO PPM	NA %	NI PPM	P %	PB PPM	PD PPM	PT PPM	SB PPM	SN PPM	SR PPM	U PPM	W PPM	ZN PPM
TR 1-S 1	.1	1.78	7	ND	122	ND	.27	.4	8	6	29	2.16	.04	.43	503	1	.01	18	.04	9	ND	ND	ND	ND	24	ND	ND	152
TR 1-S 2	.1	1.83	11	ND	85	ND	.28	.2	9	6	38	2.32	.04	.47	377	1	.01	17	.04	11	ND	ND	ND	ND	28	ND	ND	95
TR 1-S 3	.3	1.32	14	ND	32	ND	.30	.2	8	4	43	2.57	.04	.52	424	1	.01	17	.04	13	ND	ND	ND	ND	23	ND	ND	68
TR 1-S 4	.3	1.24	12	ND	33	ND	.44	1.6	9	4	152	2.69	.04	.59	724	1	.01	16	.08	54	ND	ND	ND	ND	27	ND	ND	332
TR 2-S 1	.1	1.82	11	ND	140	ND	.26	.7	9	6	30	1.98	.03	.38	644	1	.01	20	.10	11	ND	ND	ND	ND	28	ND	ND	203
TR 2-S 2	.1	1.12	26	ND	42	ND	.23	.2	7	7	34	2.12	.03	.39	277	1	.01	19	.03	7	ND	ND	ND	ND	21	ND	ND	66
TR 2-S 3	.9	1.50	21	ND	42	ND	.47	.1	8	6	110	2.57	.04	.50	390	ND	.01	16	.03	15	ND	ND	ND	ND	36	ND	ND	60
TR 2-S 4	.3	1.01	31	ND	39	ND	.84	.4	9	5	68	2.39	.05	.42	532	1	.01	15	.09	25	ND	ND	ND	ND	41	ND	ND	86
TR 2-S 5	.1	.73	21	ND	20	ND	.44	2.8	8	4	189	2.12	.04	.35	490	ND	.01	13	.07	21	ND	ND	ND	ND	28	ND	ND	504
TR 3-S 1	.1	2.45	13	ND	147	ND	.29	2.6	9	6	41	2.21	.04	.46	578	1	.01	17	.11	10	ND	ND	ND	ND	30	ND	ND	316
TR 3-S 2	.1	2.98	16	ND	133	ND	.36	2.1	11	7	54	2.45	.04	.56	428	1	.01	19	.09	6	ND	ND	ND	ND	33	ND	ND	213
TR 3-S 3	.1	1.86	14	ND	76	ND	.35	.4	9	7	35	2.28	.04	.48	318	1	.01	15	.04	7	ND	ND	ND	ND	32	ND	ND	82
DETECTION LIMIT	.1	.01	3	3	1	3	.01	.1	1	1	1	.01	.01	.01	1	1	.01	1	.01	2	3	5	2	2	1	5	3	1

APPENDIX C

ANALYTICAL TECHNIQUES

VGC

VANGEOCHEM LAB LIMITED

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December 1st, 1987

TO: Peter Leriche
ASHWORTH EXPLORATION LTD.
Mezz Flr - 744 W. Hastings St.
Vancouver, B.C. V6C 1A5

FROM: Vangeochem Lab Limited
1521 Pemberton Avenue
North Vancouver, British Columbia
V7P 2S3

SUBJECT: Analytical procedure used to determine gold by fire assay method and detect by atomic absorption spectrophotometry in geological samples.

1. Method of Sample Preparation

(a) Geochemical soil, silt or rock samples were received at the laboratory in high wet-strength, 4" x 6", Kraft paper bags. Rock samples would be received in poly ore bags.

(b) Dried soil and silt samples were sifted by hand using an 8" diameter, 80-mesh, stainless steel sieve. The plus 80-mesh fraction was rejected. The minus 80-mesh fraction was transferred into a new bag for subsequent analyses.

(c) Dried rock samples were crushed using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for subsequent analyses.

2. Method of Extraction

(a) 20.0 to 30.0 grams of the pulp samples were used. Samples were weighed out using a top-loading balance and deposited into individual fusion pots.

(b) A flux of litharge, soda ash, silica, borax, and, either flour or potassium nitrite is added. The samples are then fused at 1900 degrees Farenhiet to form a lead "button".

(c) The gold is extracted by cupellation and parted with diluted nitric acid.

VGC

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(d) The gold bead is retained for subsequent measurement.

3. Method of Detection

(a) The gold bead is dissolved by boiling with sodium cyanide, hydrogen peroxide and ammonium hydroxide.

(b) The detection of gold was performed with a Techtron model AA5 Atomic Absorption Spectrophotometer with a gold hollow cathode lamp. The results were read out on a strip chart recorder. The gold values, in parts per billion, were calculated by comparing them with a set of known gold standards.

4. Analysts

The analyses were supervised or determined by Mr. Conway Chun or Mr. David Chiu and his laboratory staff.

David Chiu
VANGEOCHEM LAB LIMITED

VGC

VANGEOCHEM LAB LIMITED

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December 1st, 1987

TO: Peter Leriche
ASHWORTH EXPLORATION LTD.
Mezz Flr - 744 W. Hastings St.
Vancouver, B.C. V6C 1A5

FROM: Vangeochem Lab Limited
1521 Pemberton Avenue
North Vancouver, British Columbia
V7P 2S3

SUBJECT: Analytical procedure used to determine hot acid soluble for 28 element scan by inductively Coupled Plasma Spectrophotometry in geochemical silt and soil samples.

1. Method of Sample Preparation

(a) Geochemical soil, silt or rock samples were received at the laboratory in high wet-strength, 4" x 6", Kraft paper bags. Rock samples would be received in poly ore bags.

(b) Dried soil and silt samples were sifted by hand using an 8" diameter, 80-mesh, stainless steel sieve. The plus 80-mesh fraction was rejected. The minus 80-mesh fraction was transferred into a new bag for subsequent analyses.

(c) Dried rock samples were crushed using a jaw crusher and pulverized to 100-mesh or finer by using a disc mill. The pulverized samples were then put in a new bag for subsequent analyses.

2. Method of Digestion

(a) 0.50 gram portions of the minus 80-mesh samples were used. Samples were weighed out using an electronic balance.

(b) Samples were digested with a 5 ml solution of HCL:HNO3:H2O in the ratio of 3:1:2 in a 95 degree Celsius water bath for 90 minutes.

(c) The digested samples are then removed from the bath and bulked up to 10 ml total volume with dimineralized water and thoroughly mixed.

VGC

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3. Method of Analyses

The ICP analyses elements were determined by using a Jarrel-Ash ICAP model 9000 directly reading the spectrophotometric emissions. All major matrix and trace elements are interelement corrected. All data are subsequently stored onto disk.

4. Analysts

The analyses were supervised or determined by either Mr. Eddie Tang, and, the laboratory staff.

Eddie Tang
VANGEOCHEM LAB LIMITED

APPENDIX D

PETROGRAPHIC DESCRIPTIONS

Vancouver Petrographics Ltd.

JAMES VINNELL, Manager
JOHN G. PAYNE, Ph.D. Geologist
A.L. LITTLEJOHN, M.Sc. Geologist
JEFF HARRIS, Ph.D. Geologist

P.O. BOX 39
8887 NASH STREET
FORT LANGLEY, B.C.
VOX 1JO

PHONE (604) 888-1323

Invoice #7201

March 7th, 1988

Report for: Fayz Yacoub,
Ashworth Explorations Ltd.,
Mezzanine Floor,
744 West Hastings St.,
Vancouver, B.C.
V6C 1A5

Samples:

5 rock samples, numbered P-1 to P-5, for sectioning and petrographic descriptions.

Summary:

Samples P-1 and P-3 are medium-grained instrusives of granodiorite to quartz monzonite composition. Accessory hornblende shows partial late-magmatic conversion to secondary biotite. P-1 is essentially unaltered, but P-3 shows mild epidotization.

Samples P-2 and P-4 are finer-grained rocks of diorite to quartz diorite composition. P-2 is incipiently foliated and shows weak to moderate epidotization, partially structurally controlled. P-4 is cut by a mylonite-bounded quartz vein and shows strong microbreccia-controlled sericitization and limonitization.

Sample P-5 is a granulated, sheeted quartz vein or shear rock, with sinuous schlieren of sericite. It is mineralized with sphalerite and pyrite as small wisps and pockets. It is cut by barite-filled, hairline fractures.

Individual petrographic descriptions are attached.

J.F. Harris Ph.D.

(phone: 929-5867)

Sample P-1 GRANODIORITE

Estimated mode

Quartz	25
Plagioclase	42
K-feldspar	20
Sericite	1
Biotite	7
Chlorite	1
Hornblende	3
Epidote	trace
Sphene	trace
Apatite	trace
Opaques	1

This is a medium-grained rock showing a typical granitic texture.

Of the three principal constituents, plagioclase occurs as clumps of subhedral prismatic grains, 0.5 - 3.0mm in size; K-feldspar forms coarse anhedral areas, often with included plagioclase crystals; and quartz forms irregular pockets of anhedral, often crenulate mosaic, of grain size 0.2 - 2.0mm.

The plagioclase is of composition oligoclase-andesine; it locally shows a very light flecking of sericitic alteration.

The K-spar is cryptoperthitic orthoclase, and is totally fresh.

Mafics are relatively sparse. They occur as scattered clumps interstitial to the quartzo-feldspathic components. They include biotite (now weakly chloritized) and hornblende (now quite extensively replaced by fine-grained, secondary biotite with a little chlorite and epidote).

Sphene is seen as scattered, individual, well-formed grains, to 1mm in size, and as small granules in biotite.

Scattered subhedral opaques - probably mainly magnetite - occur, generally in close association with the mafic silicates.

The rock is a normal, essentially unaltered granodiorite.

Sample P-2 FOLIATED FINE-GRAINED DIORITE

Estimated mode

Quartz	8
Plagioclase	48
K-feldspar	4
Sericite	1
Biotite	12
Chlorite	1
Hornblende	6
Epidote	18
Sphene	1
Apatite	trace
Carbonate	trace
Opaques	1

In comparison with P-1, this is a notably finer-grained rock. It also contains considerably less quartz and K-spar and more mafics. It is of dioritic composition.

Plagioclase is the principal constituent, occurring as an aggregate of anhedral-subhedral grains, 0.2 - 1.0mm in size.

Accessory K-feldspar occurs as sporadic clumps.

Quartz forms small pockets and semi-connected networks of finely granular anhedral mosaic.

The plagioclase shows sporadic development of mild sericite, carbonate and epidote alteration, as fine-grained flecks. Epidote concentrates as core zones to a few plagioclase grains.

Mafics are abundant, occurring rather evenly dispersed as clumps and intergranular impregnations throughout the plagioclase aggregate. The dispersed appearance of the mafics under the microscope is increased by the fact that much of the original hornblende is now replaced by clusters of fine-grained olive-green biotite with granules of epidote and sphene.

Clumps of more or less compact, fine-grained epidote are locally developed - sometimes after primary mafics, sometimes in feldspar adjacent to pockets of quartz. This effect is notably concentrated in a central, 1cm wide band, within which the quartz and epidote are locally segregated as veinlets.

This central zone is clearly the locus of incipient fracturing and alteration, probably developed late in the intrusion history. It parallels a weak but perceptible foliation defined by the distribution of mafics throughout the rock.

Sparse disseminated opaques in this rock include some sulfides (pyrite or pyrrhotite).

Sample P-3 QUARTZ MONZONITE

Estimated mode

Quartz	20
Plagioclase	44
K-feldspar	26
Sericite	trace
Biotite	4
Epidote	5
Hornblende	1
Sphene	trace
Apatite	trace
Opaques	trace

This is a medium-grained intrusive of very similar general character to P-1. It appears to have slightly more K-spar and slightly less quartz than P-1, and probably falls in the compositional field of quartz monzonite.

As in the other sample, plagioclase is generally subhedral - prismatic, K-spar is coarse anhedral, and quartz is as polygranular mosaic pockets interstitial to the feldspars.

Some of the plagioclase grains in this rock are sieved with small inclusions of quartz. K-spar occasionally exhibits microcline twinning, though the majority is the untwinned cryptoperthitic type seen in P-1.

Primary mafics appear to have consisted of biotite and hornblende. Some relatively coarse grains of brown primary-type biotite are present, as well as clusters of finer, greenish biotite which often develop around and within remnants of hornblende, and are clearly a secondary (late magmatic reaction) product.

Epidote is more abundant in this sample than in P-1. It occurs as small granules intergrown with clusters of secondary biotite; as disseminated flecks representing a weak pervasive epidotization of certain plagioclase grains; and as a few coarse compact patches which appear to be the result of localized total replacement of mafics or feldspar. Occasionally the epidote shows concentration as short strings of granules, representing mobilization into incipient microfractures.

Sphene is a less prominent accessory than in the previous samples, and is present only as fine-grained traces. Opaques are likewise.

Sample P-4 BRECCIATED, SERICITIZED QUARTZ DIORITE WITH QUARTZ VEIN

Estimated mode

Quartz	24
Plagioclase	27
K-feldspar	4
Sericite	14
Secondary biotite	trace
Limonite	1
Vein	
Quartz	24
Sericite	4
Limonite	2

This is a rock of quartz dioritic composition which shows strong fracturing and alteration.

It consists of an aggregate of subhedral plagioclase, of grain size 0.2 - 1.0mm, with sporadic patches of coarser K-spar and notably abundant quartz. This occurs as extensive pockets (1 - 10mm in size) of sub-polygonal mosaic of grain size 0.1 - 0.5mm.

Sericite is abundant, occurring as intergranular wisps and networks of micro-breccia-controlled permeations. It is also developed as moderate to strong pervasive alteration of plagioclase marginal to the above. Some of the sericitic wisps follow limonitic microfractures.

It is notable that the quartz pockets in the rock are often cross-cut by vein-like bodies of fine-grained plagioclase and associated sericite, suggesting that the brecciation and alteration took place, at least in part, at an early stage of the cooling history, with the redistribution of still-fluid, residual magmatic material.

This rock contains essentially no mafics, other than occasional tiny pockets of pale secondary biotite associated with the dominant sericite.

The slide includes an apparent quartz vein which shows strong strain polarization. It is locally granulated and permeated by breccia fillings and intergranular pockets of strongly limonitic sericite. The contact of the vein is delineated by a thin mylonitic zone of felted sericite with rounded quartz remnants.

Sample P-5 QUARTZ SERICITE SHEAR VEIN WITH SULFIDES

Estimated mode

Quartz	67
Sericite	25
Chlorite	trace
Barite	2
Carbonate	trace
Sphalerite	4
Pyrite	2
Chalcopyrite	trace
Pb-As sulfosalt(?)	trace

This sample is a typical shear zone rock. It consists predominantly of quartz, as an intensely strained, granulated aggregate, ranging in grain size from about 2.0mm down to 20 microns. The fine-grained mosaics clearly result from intergranular recrystallization of original coarser material, and concentrate as sinuous, sub-parallel streaks and networks throughout the crenulate-margined aggregate.

Sericite, of fine felted to foliaceous form, is a prominent accessory, occurring as sub-parallel schlieren and locally contorted masses which delineate a crude, platy foliation.

Sulfides form small lenses, clusters and disseminations, generally conformable to the deformational foliation in the host, but locally expanding to more discordant pockets and networks.

They consist principally of sphalerite - typically packed with micron-sized, sub-oriented exsolution blebs of chalcopyrite - and pyrite. The two commonly occur together with the pyrite,forming euhedral grains (50 - 300 microns) and coalescent clumps in a matrix of sphalerite, or as clusters of pyrite euhedra cemented and moulded around by sphalerite.

Chalcopyrite occasionally concentrates as discrete pockets, closely associated with sphalerite or with another minor constituent of uncertain identity. The latter has the colour of galena, but is strongly anisotropic; it is probably a Pb-Sb or Pb-Sb-Cu sulfosalt. This phase is sometimes also seen as tiny disseminated inclusions in sphalerite.

The rock is cut by a system of late transverse fractures, crosscutting the foliation. These are filled by barite with minor associated carbonate. These fractures mostly appear to postdate the sulfides, though locally the more discordant form of sulfide impregnation partially follows the crosscutting structure. A few isolated pockets of barite occur independent of the fractures.

APPENDIX E

STATISTICAL REPORT AND HISTOGRAMS

BY TONY CLARK CONSULTING

REPORT
ON A
STATISTICAL INTERPRETATION
OF
SOIL SAMPLE ANALYSES
FROM THE
LUCKY BOY PROPERTY
BRITISH COLUMBIA

FOR

ASHWORTH EXPLORATIONS LIMITED
Mezzanine Floor,
744 WEST HASTINGS ST.
VANCOUVER, BC
V6C 1A5

A.M.S.Clark
Ph.D, P.Geol(Alta)
17 March 1988

(604)942-7172

TONY CLARK CONSULTING
218 Roger's Building
470 Granville St
Vancouver, BC
V6C 1V5

CONTENTS

INTRODUCTION

This report is prepared at the request of Ashworth Explorations. The analytical results were supplied by Vangeochem Lab Limited of North Vancouver. The author was not involved in either the collection of the samples or the analysis of the samples, and has not visited the property. The intent of this report is to evaluate the inter-relationships of the elements in order to determine patterns that may help in guiding further field-work.

GENERAL DISCUSSION

The correlation coefficients are given as a matrix table of values (Table 2) relating each element with the others- note that each correlation occurs twice in the table, eg. PBPPM/ZNPPM and ZNPPM/PBPPM but, of course, has the same correlation.

Two elements, platinum and uranium, were not included in the calculations as all values were nil ppm, making correlation meaningless.

Correlations of around zero indicate no correlation between elements; correlations of increasing value indicate increasing correlation between elements, with positive values being positive correlations (as one element increases so does the other) and negative values being negative correlations (as one element increases so the other element decreases). Correlations of about .3 are considered weak, but in geochemistry may be significant, correlations of about .5 are moderate and significant, and correlations of .7 or higher are

strong and indicate a direct relationship of one element with another.

In discussing the histograms, and in the maps (located in the main body of the report), the term 'anomalous' is defined separately for each element based on an interpretation of the histograms. Although 'anomalous' is frequently taken in geochemistry to be 'de facto' those samples that are greater in value than twice the standard deviation of the suite of samples being considered, as there is no mathematical definition for 'anomalous' and as it is best to use values that can guide the continuing field exploration, the use of twice the standard deviation is not used here: the terms used are 'high' for values including approximately the upper 25% of the data set to the approximate end of the gaussian curve, and 'anomalous' for those samples that appear at the highest end of the gaussian curve and beyond as determined by inspection of the histograms.

Although all the elements are probably distributed logarithmically, as there was no particular reason to plot histograms of the logarithms of the values in this data-set, only histograms of the normal values are used.

The discussion below should be considered as a guide to further field checking for more definite answers. Although weak or stronger correlations are mentioned, only those on which some degree of interpretation can be placed are discussed.

DETAILED DISCUSSION

The correlation coefficient table is included as Table 2 at the end of the report. Scatter plots of some values are included where necessary to show that there is no 'single-sample' effect to bias the correlations.

Ag ppm:

Histograms of the normal distribution of the samples indicate a lognormal distribution (as expected). A more detailed histogram was plotted showing the main suite of samples, and the diagram indicates a main population and a few high outliers that may be a second population. All values are relatively low, but a threshold of 0.3 ppm for 'high' values and another at 0.6 ppm for 'anomalous' values were chosen and plotted as a symbol map to determine possible patterns of distribution. The results (see main body of report for symbol maps) indicate two areas of interest: one area in the north part of the grid, and a lesser one in the south-central part of the grid. The northern area of interest is in the vicinity of an old adit (Peter Leriche, pers. comm), and should be checked for mineralised extensions to the adit working area, or a possible 'original' outcrop higher than the adit that the adit may have been testing. It is possible the anomalies reflect material from the adit, but a possible original bedrock source should be checked, particularly as other elements (As, Cu, Pb) show anomalous values above the position of the adit. Further checking should be undertaken- this can consist of soil investigation (source of the soil and clasts), detailed soil sampling on lines 50-metres apart and the same station spacing as used already, and any other menthods deemed

useful under the circumstances (eg. ground geophysics, trenching, etc.). A moderate correlation between silver and arsenic is expected in a felsic volcanic terrain. A moderate correlation between silver and nickel and other nickel-association metals (Co, Cr, Cu) is unusual, and a scatter plot of silver and nickel was undertaken to check. The scatter plot indicates the correlation is not the result of a single high-value sample distorting the correlation, but is genuine for many samples- however, there is no distinct or obvious distribution trend on the scatter plot. The geological setting for such a correlation of nickel and silver is not known and should be checked in the field. The scatter plot does show an unusual possible trend parallel to the y-axis. As there are no known basic rocks in the area this could be from basic dykes (frequently recessively eroded) that that have a fixed nickel content but a variable silver content due to incorporation from the country rock, however this is at present only a suggestion for further field investigation.

Al %:

Apart from expected correlations (Ca, K, Sr) there is a moderate correlation with nickel, cobalt, chromium, copper and iron. No significance is placed on these correlations.

As ppm:

The arsenic values are generally low, but with some high values above the normally expected soil background of about 25 to 50 ppm. For the purpose of plotting the symbol map, high values were taken as above 20 ppm and anomalous values as

above 50 ppm. As with silver there are two areas of interest- the northern area about the adit, and a south-central area. The northern area shows anomalous values above the position of the adit which may reflect an above-adit bedrock source: prospecting should be undertaken in this area. The south-central area is very weakly shown in these sample results. There is a moderate correlation with silver and gold (Au ppb), and a weak correlation with lead, tin and zinc. There is a weak to moderate correlation between arsenic and the nickel group or elements (Ni, Co, Cr, Cu) that may again be related to the same origin as the silver-nickel correlation. The scatter plot of arsenic and nickel shows that the correlation is valid and not the result of a single or small group of exceptionally high assays, and though the pattern is indistinct pattern it does show that as nickel increases so does arsenic.

Au ppm:

Because of the inaccuracy of gold analysis by ICP these correlations will not be discussed. Gold by fire assay will be discussed later.

Ba ppm:

Barium shows no significant correlations apart from the expected correlations with manganese and phosphorous.

Bi ppm:

No significant correlations.

Ca %:

No unusual correlations apart from a moderate correlation with both the nickel group of elements and also with arsenic.

Cd ppm:

No unexpected correlations.

Co ppm:

A strong correlation with the same nickel group of elements as above (Ni, Cr, Cu, Fe) as well as a moderate correlation with arsenic.

Cr ppm:

No unusual correlations apart for a moderate to strong correlation with arsenic.

Cu ppm:

Values are all low, with 'high' values taken as above 20 ppm and 'anomalous' values above 50 ppm for the purposes of plotting the symbol map. The map again shows the two areas of interest, with the higher values being in the northern area. The correlation matrix indicates no unusual correlations apart from a moderate correlation with silver and a strong correlation with arsenic.

Fe %:

A strong correlation with the nickel association elements and a moderate correlation with arsenic.

K %:

No noteworthy correlations.

Mg %:

A moderate correlation with arsenic, otherwise no unusual correlations.

Mn ppm:

No unusual correlations.

Mo ppm:

A moderate correlation with nickel and its associated elements, otherwise no unusual correlations.

Na %:

Sodium has a very low to nil correlation with all elements suggesting it is not part of the rock-forming suite of elements. If these are felsic volcanic rocks this would be unusual and therefore the rock-types in the area should be investigated petrographically.

Ni ppm:

The soil sample values for nickel are only the expected background and slightly above, with threshold values chosen as above 25 ppm ('high') and above 50 ppm ('anomalous'). The unusual correlation of nickel with silver and arsenic has already been mentioned. The symbol map of nickel shows an association only with the northern area of interest around the adit. This suggests the rock types in this area may be more

basic than previously thought, or may have a larger basic component that realised. The area should be checked carefully and petrographically sampled by a geologist, particularly the adit area and above, as this may be the clue to the mineralisation the adit was intended to check.

P %:

There are no unusual correlations.

Pb ppm:

Values for lead are generally low, with thresholds of 15 ppm ('high') and 35 ppm ('anomalous') being chosen for the symbol map. There is the suggestion of a second population in the histogram, but there are too few samples to follow up on this possibility (10 samples out of 525). Lead also defines the two areas of interest, but with more highs and anomalous valous in the intervening area. There are no significant correlations.

Pd ppm:

No correlations.

Pt ppm:

Not in the correlation matrix as all assays of this element were nil.

Sb ppm:

No significant correlations.

Sn pm:

A weak correlation with arsenic and nickel, and a moderate correltion with chromium that is unusual.

Sr ppm:

A moderate correlation with arsenic and also with the nickel associated elements that may signify alkalic basic rocks.

U ppm:

Not in the correlation matrix as all assays of this element were nil.

W ppm:

No correlations.

Zn ppm:

Weak correlation with silver and arsenic, and weak to moderate correlation with the nickel associated elements. Values of sample analyses are generally low to moderate for soils, but some high values extend to the 1300 ppm range. In the symbol map 'high' values were taken as above 150 ppm and 'anomalous' values as above 400 ppm. The map indicates both the northern (adit) and the central areas of interest. A scatter plot of zinc verses nickel indicates the correlation is significant, cith with very little range.

Au ppb(FA):

Values are low, and only weak correlations with arsenic and some of the nickel associated elements are recognised. The symbol map ('high' above 10 ppm and 'anomalous' above 25 ppm) shows no local association which is as expected with such low values (the detection limit is only 5 ppm). A scatter plot of gold against nickel is not suggestive of an association, though it does show an apparent 'grouping' about the 20 ppm Ni range that is similar to that recognised for silver.

CONCLUSIONS:

The unusual correlation of nickel and its associated elements (Co,Cd,Cu) with silver, arsenic, etc. should be checked merely because it is unusual. At present there is no reason to think it has exploration significance.

The area of the adit (the northern area of interest) consistently has higher soil values than the central area of interest, suggesting a different lithological suite in the area.

The correlation of the nickel associated elements with potassium and strontium suggests a possible alkalic basic igneous suite in the area that may have significance for other elements and minerals not presently being considered.

TABLE 1.
List of Elements

Ag	ppm
Al	%
As	ppm
Au	ppm
Ba	ppm
Bi	ppm
Ca	%
Cd	ppm
Co	ppm
Cr	ppm
Cu	ppm
Fe	%
K	%
Mg	%
Mn	ppm
Mo	ppm
Na	%
Ni	ppm
P	%
Pb	ppm
Pd	ppm
Pt	ppm
Sb	ppm
Sn	ppm
Sr	ppm
U	ppm
W	ppm
Zn	ppm
Au	ppb(Fire assay)

CERTIFICATE

I, Anthony M. S. Clark, residing at 2988 Fleet St. in the Municipality of Coquitlam, Province of British Columbia, hereby certify that:

1. I received a Bachelor of Science degree in geology from the University of Cape Town, Cape Town, South Africa, in 1963, and a Doctor of Philosophy degree in geology from the Memorial University of Newfoundland, St.John's, Newfoundland in 1974.

2. I practised the profession of exploration geologist from 1963 to 1986, since when I have undertaken consulting in the fields of mineral exploration, and computer applications to exploration.

3. I am a Fellow of the Geological Association of Canada and Registered as a Professional Geologist with the Association of Professional Engineers, Geologists and Geophysicists of Alberta.

4. I am self-employed and undertake my profession under the name of TONY CLARK CONSULTING.

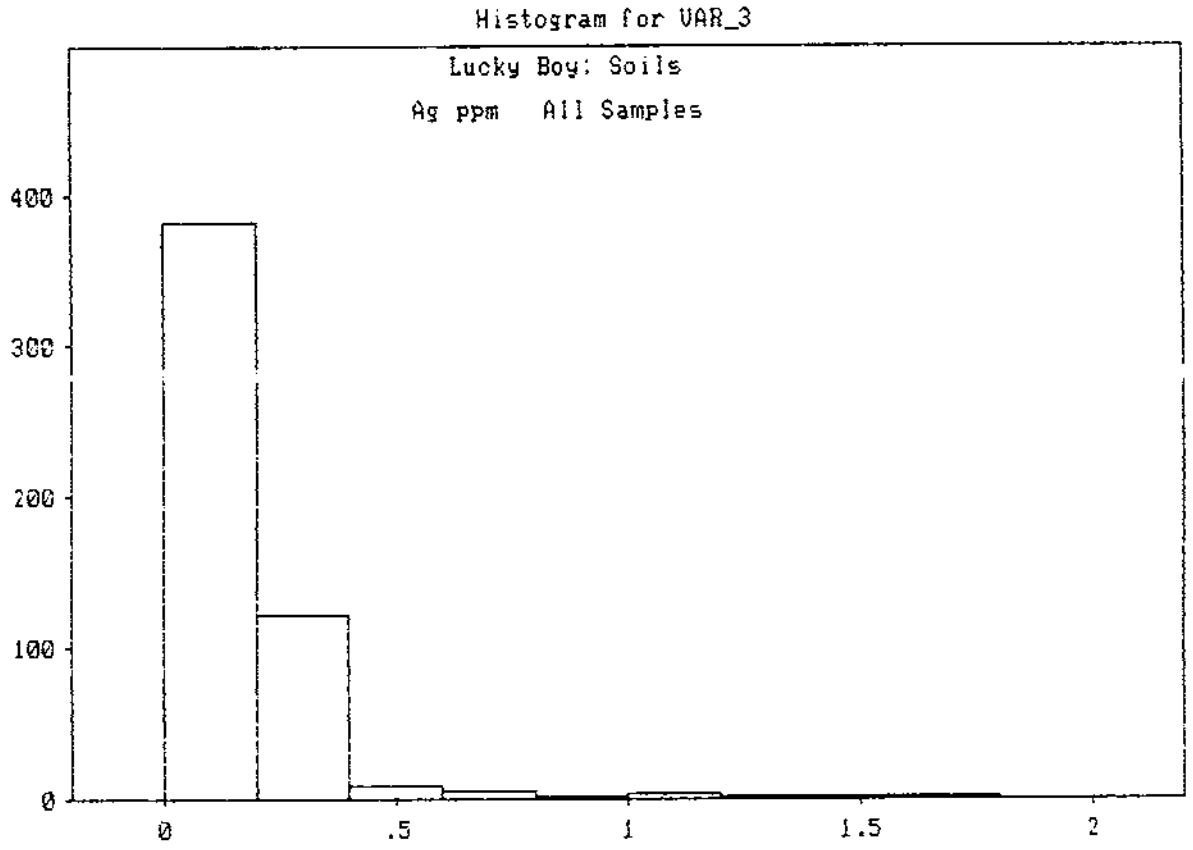
5. This report is produced at the request of Ashworth Explorations Limited of Vancouver. The sample analytical data is from Vangeochem Lab in North Vancouver. I have not visited the property, and this report is based on the analytical results and discussions with Ashworth personnel only. The report is intended to determine element relationships in the samples so as to aid further work on the property.

Date:

19 March 1988

A.M.S.Clark,Ph.D.
FGAC, P.Geol(Alta).

Coquitlam,British Columbia



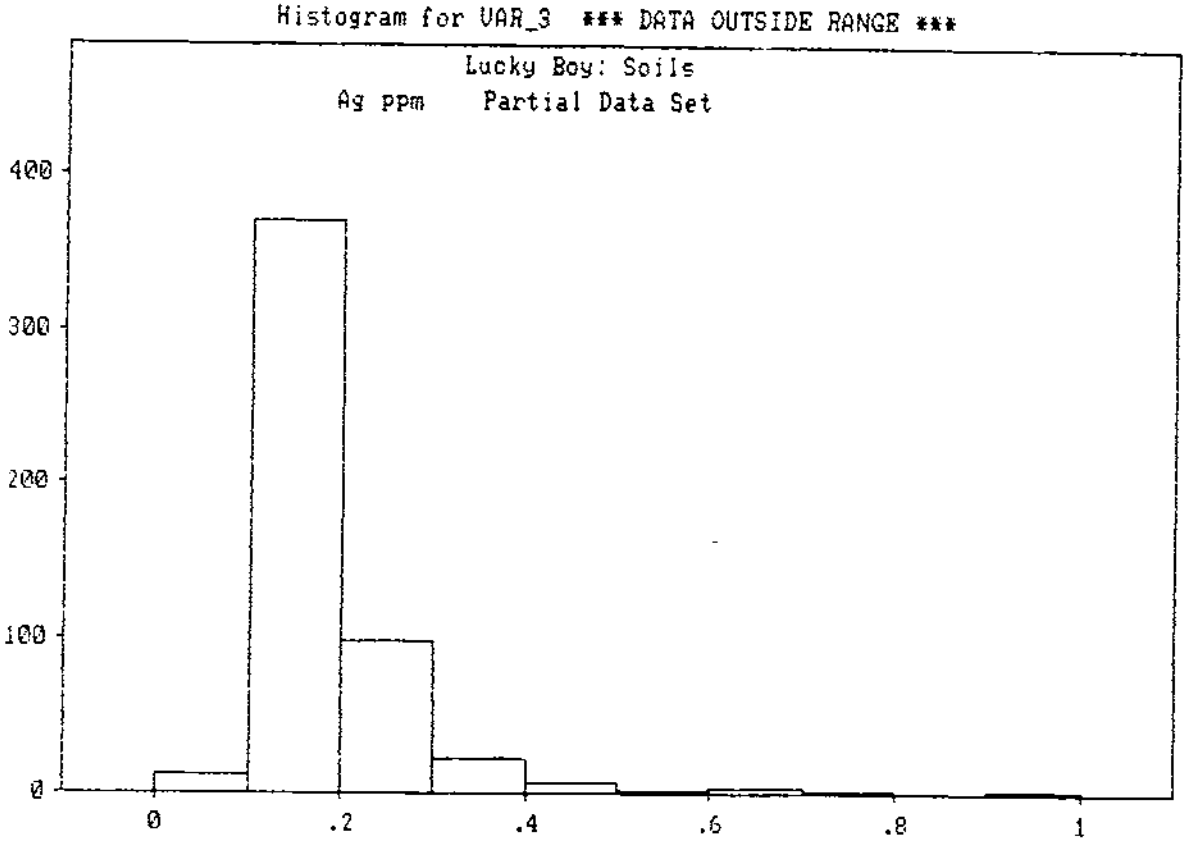
Mean = .15238 Variance = .02532
Standard Deviation = .1591 Skewness = 5.662

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	0.17	382	73	382	73	Mean
0.17	0.34	121	23	503	96	
0.34	0.51	9	2	512	98	
0.51	0.68	4	1	516	98	
0.68	0.85	1	0	517	98	
0.85	1.02	2	0	519	99	
1.02	1.19	3	1	522	99	
1.19	1.36	1	0	523	100	
1.36	1.53	1	0	524	100	
1.53	1.7	1	0	525	100	

Data elements inside histogram 525
Data elements outside histogram 0

Descriptive Statistics

Mean	0.1523801
Variance	0.025324
Standard Deviation	0.1591336
Skewness	5.661828

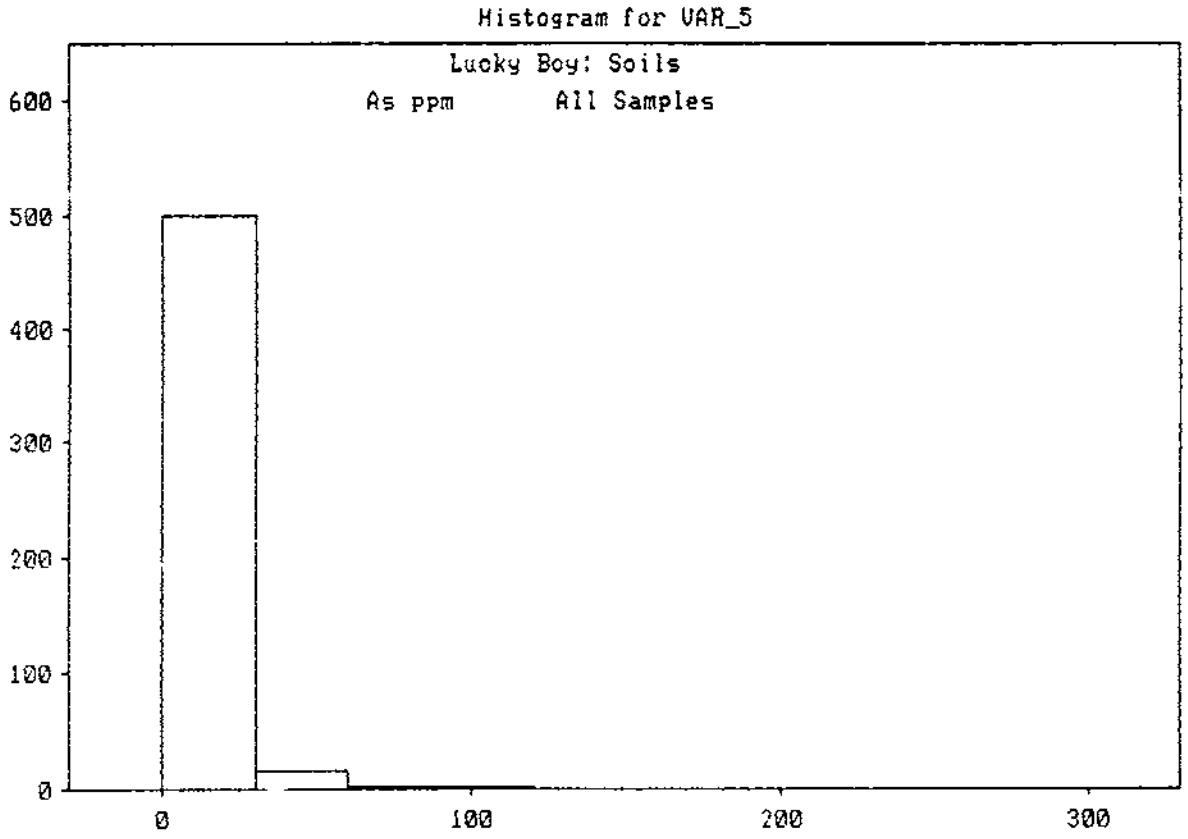


Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	0.1	12	2	12	2	
0.1	0.2	370	70	382	73	Mean
0.2	0.3	99	19	481	92	
0.3	0.4	22	4	503	96	
0.4	0.5	7	1	510	97	
0.5	0.6	2	0	512	98	
0.6	0.7	4	1	516	98	
0.7	0.8	1	0	517	98	
0.8	0.9	0	0	517	98	
0.9	1	2	0	519	99	

Data elements inside histogram 519
Data elements outside histogram 6

Descriptive Statistics

Mean	0.1523801
Variance	0.025324
Standard Deviation	0.1591336
Skewness	5.661828



Mean = 12.303 Variance = 446.4
Standard Deviation = 21.13 Skewness = 7.921

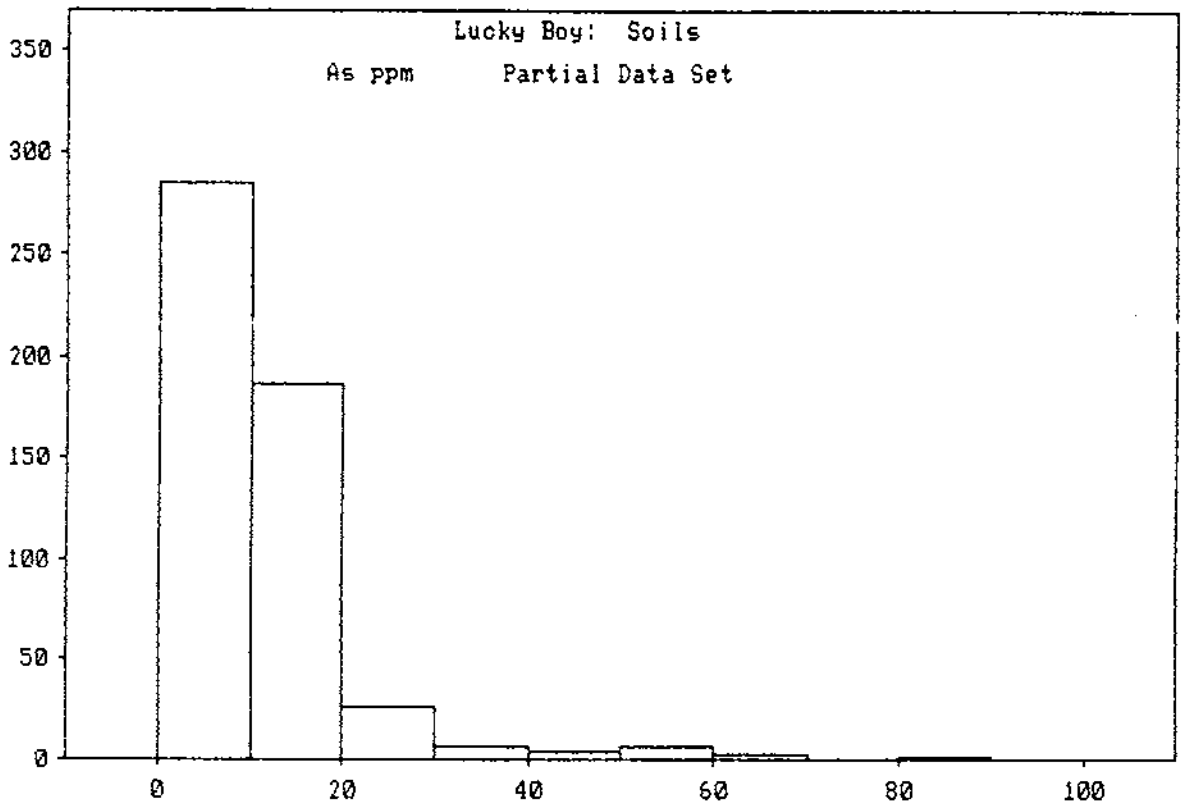
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	30	499	95	499	95	Mean
30	60	17	3	516	98	
60	90	3	1	519	99	
90	120	2	0	521	99	
120	150	1	0	522	99	
150	180	0	0	522	99	
180	210	1	0	523	100	
210	240	1	0	524	100	
240	270	1	0	525	100	
270	300	0	0	525	100	

Data elements inside histogram 525
Data elements outside histogram 0

Descriptive Statistics

Mean	12.30286
Variance	446.3796
Standard Deviation	21.1277
Skewness	7.920547

Histogram for VAR_5 *** DATA OUTSIDE RANGE ***



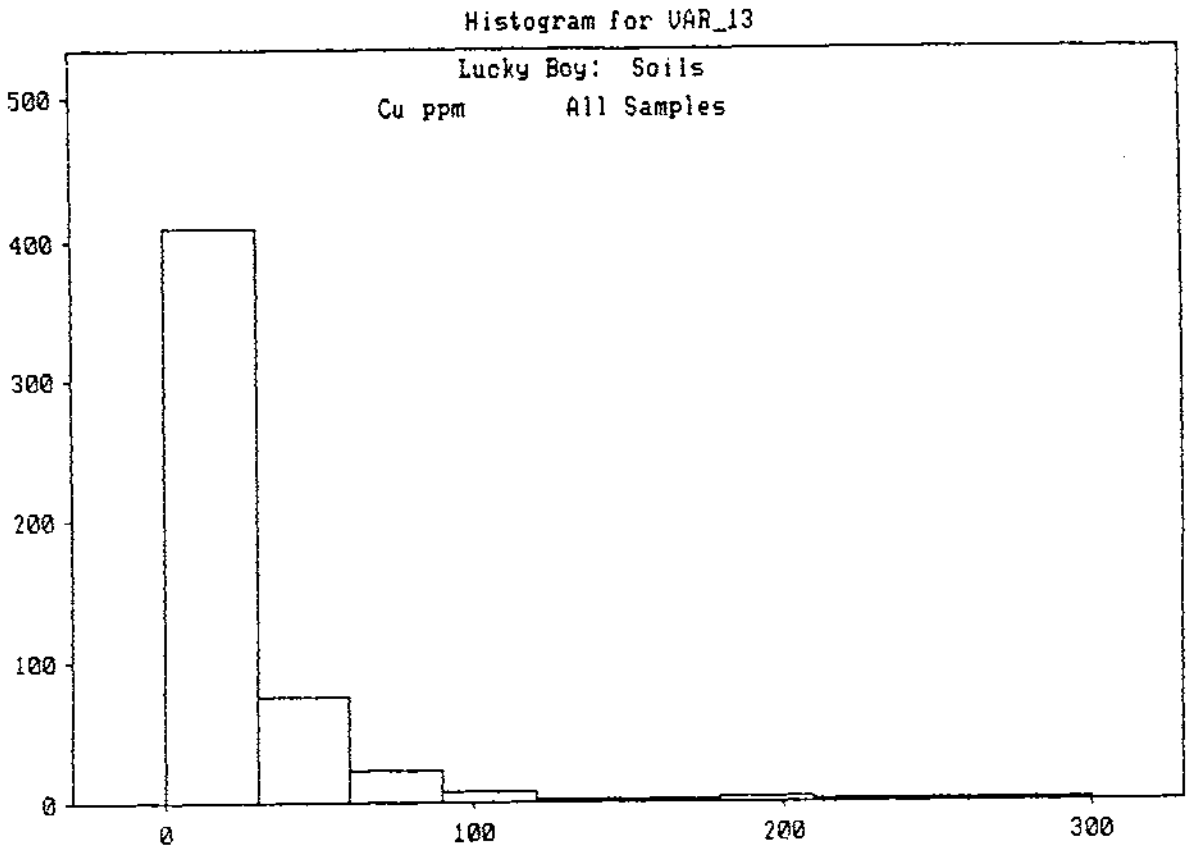
Mean = 12.303 Variance = 446.4
Standard Deviation = 21.13 Skewness = 7.921

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	10	285	54	285	54	
10	20	187	36	472	90	Mean
20	30	27	5	499	95	
30	40	7	1	506	96	
40	50	4	1	510	97	
50	60	6	1	516	98	
60	70	2	0	518	99	
70	80	0	0	518	99	
80	90	1	0	519	99	
90	100	0	0	519	99	

Data elements inside histogram 519
Data elements outside histogram 6

Descriptive Statistics

Mean	12.30286
Variance	446.3796
Standard Deviation	21.1277
Skewness	7.920547



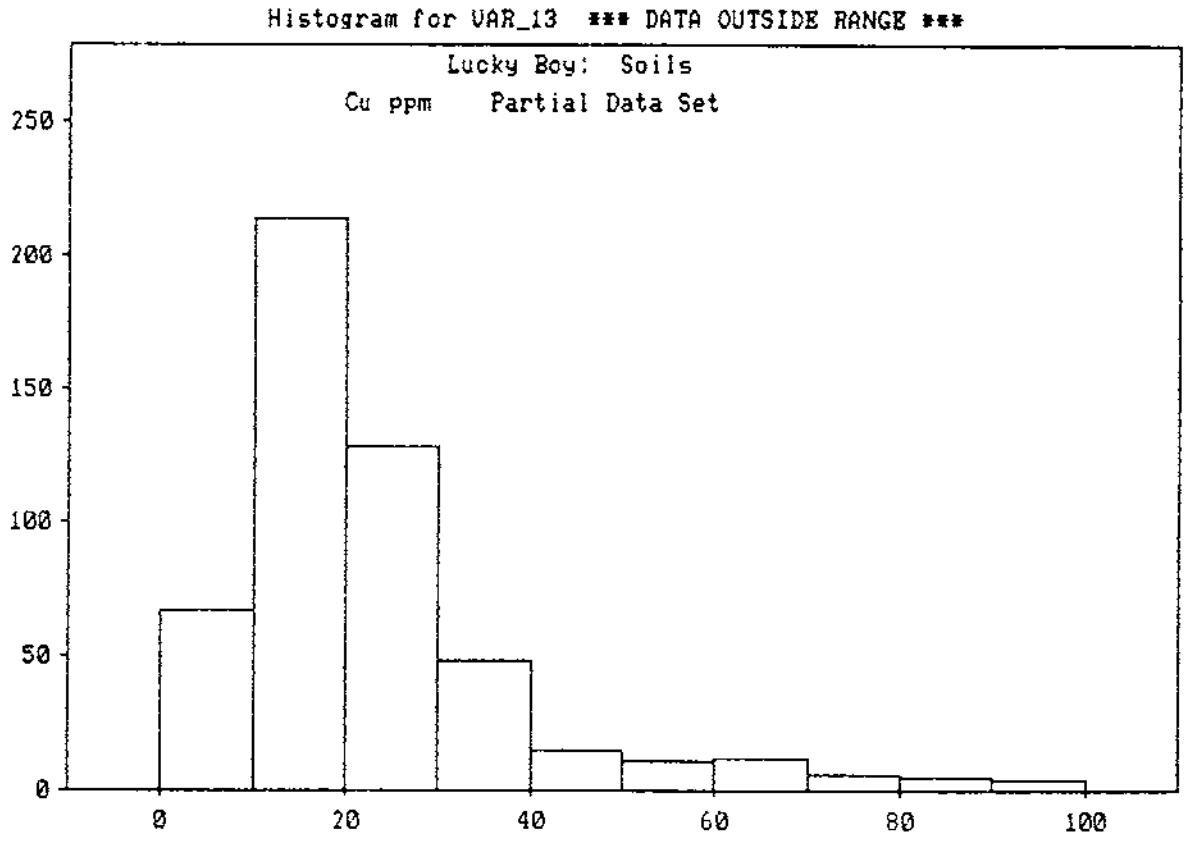
Mean = 26.741 Variance = 971.3
Standard Deviation = 31.16 Skewness = 4.463

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	30	409	78	409	78	Mean
30	60	74	14	483	92	
60	90	23	4	506	96	
90	120	8	2	514	98	
120	150	2	0	516	98	
150	180	2	0	518	99	
180	210	3	1	521	99	
210	240	2	0	523	100	
240	270	1	0	524	100	
270	300	1	0	525	100	

Data elements inside histogram 525
Data elements outside histogram 0

Descriptive Statistics

Mean	26.74095
Variance	971.2609
Standard Deviation	31.16506
Skewness	4.463239

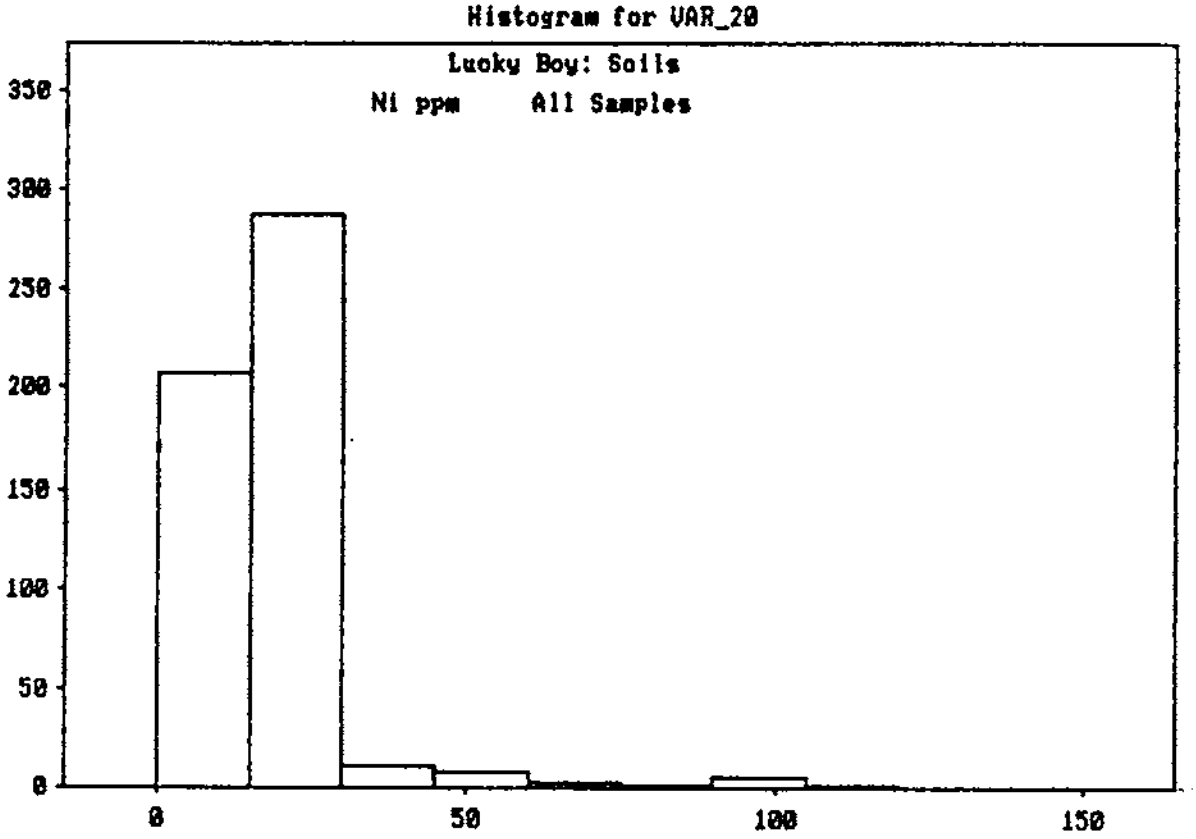


Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	10	67	13	67	13	
10	20	214	41	281	54	
20	30	128	24	409	78	Mean
30	40	48	9	457	87	
40	50	15	3	472	90	
50	60	11	2	483	92	
60	70	12	2	495	94	
70	80	6	1	501	95	
80	90	5	1	506	96	
90	100	4	1	510	97	

Data elements inside histogram 510
Data elements outside histogram 15

Descriptive Statistics

Mean	26.74095
Variance	971.2609
Standard Deviation	31.16506
Skewness	4.463239



Mean = 17.834 Variance = 140.8
Standard Deviation = 11.87 Skewness = 4.892

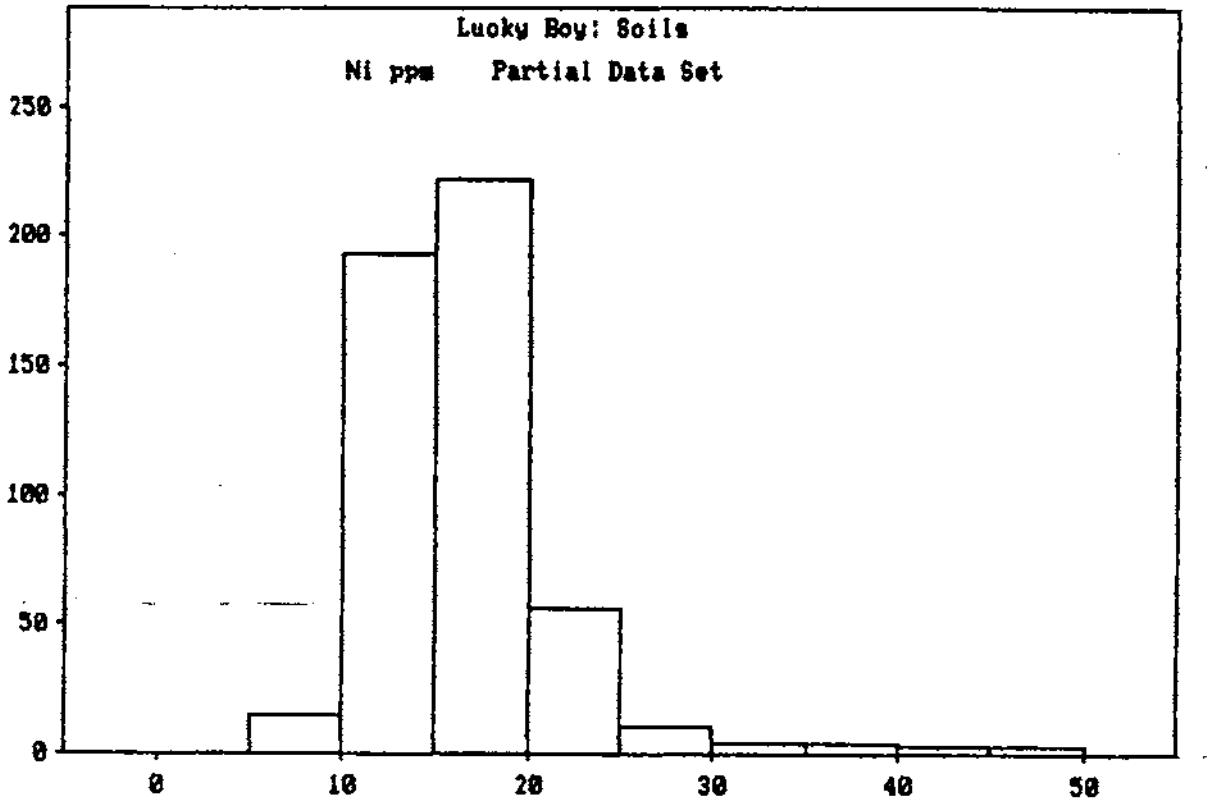
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	15	208	40	208	40	
15	30	288	55	496	94	Mean
30	45	11	2	507	97	
45	60	8	2	515	98	
60	75	3	1	518	99	
75	90	1	0	519	99	
90	105	5	1	524	100	
105	120	1	0	525	100	
120	135	0	0	525	100	
135	150	0	0	525	100	

Data elements inside histogram 525
Data elements outside histogram 0

Descriptive Statistics

Mean	17.83429
Variance	140.7836
Standard Deviation	11.86523
Skewness	4.892026

Histogram for VAR_20 *** DATA OUTSIDE RANGE ***



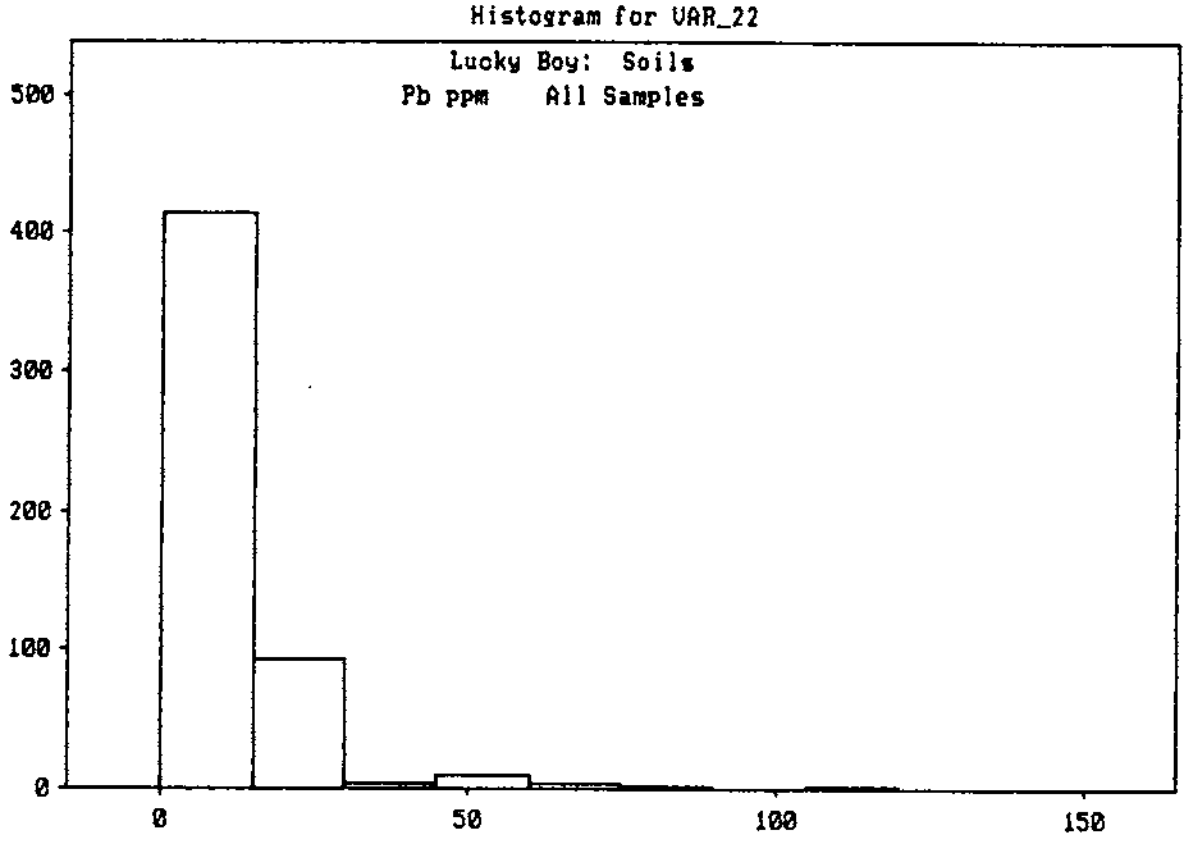
Mean = 17.834 Variance = 140.8
Standard Deviation = 11.87 Skewness = 4.892

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	5	0	0	0	0	
5	10	15	3	15	3	
10	15	193	37	208	40	
15	20	222	42	430	82	Mean
20	25	56	11	486	93	
25	30	10	2	496	94	
30	35	4	1	500	95	
35	40	4	1	504	96	
40	45	3	1	507	97	
45	50	3	1	510	97	

Data elements inside histogram 510
Data elements outside histogram 15

Descriptive Statistics

Mean	17.83429
Variance	140.7836
Standard Deviation	11.86523
Skewness	4.892026



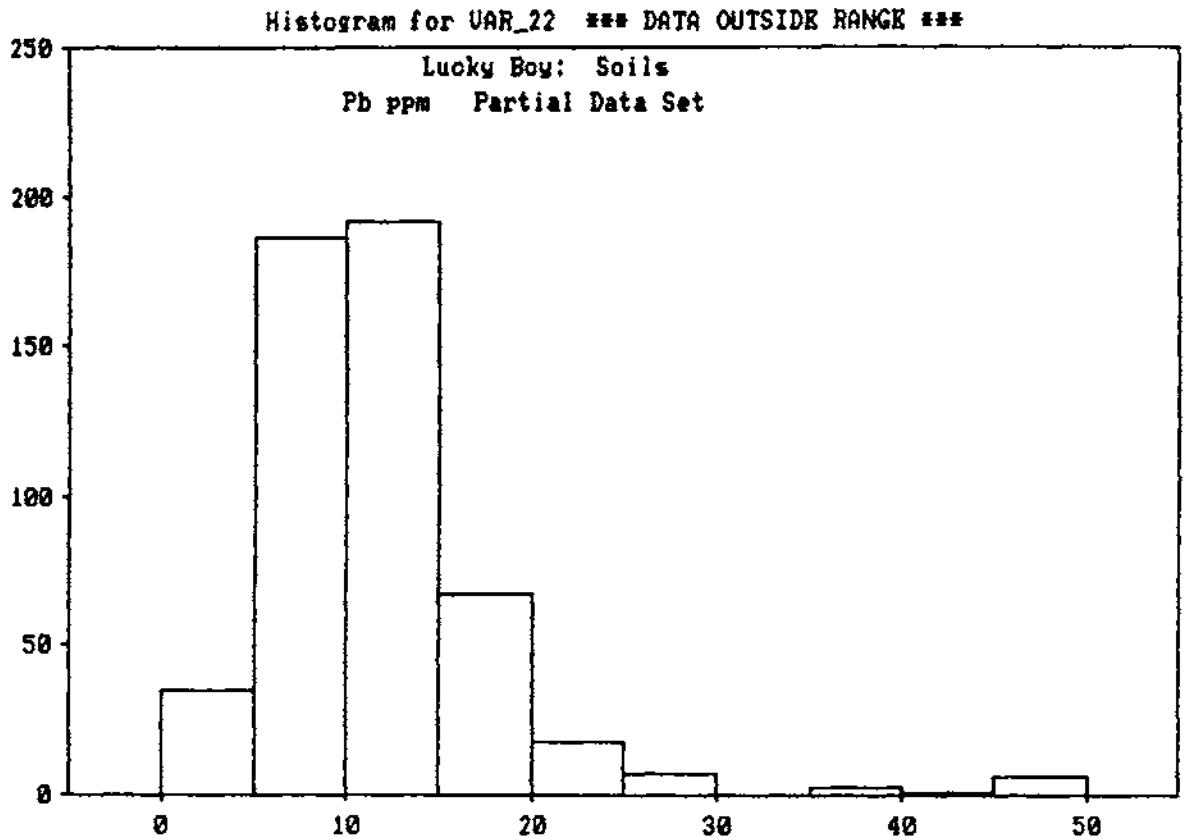
Mean = 12.263 Variance = 103.1
Standard Deviation = 10.16 Skewness = 4.441

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	15	414	79	414	79	Mean
15	30	92	18	506	96	
30	45	4	1	510	97	
45	60	9	2	519	99	
60	75	4	1	523	100	
75	90	1	0	524	100	
90	105	0	0	524	100	
105	120	1	0	525	100	
120	135	0	0	525	100	
135	150	0	0	525	100	

Data elements inside histogram 525
Data elements outside histogram 0

Descriptive Statistics

Mean	12.26286
Variance	103.133
Standard Deviation	10.15544
Skewness	4.440813



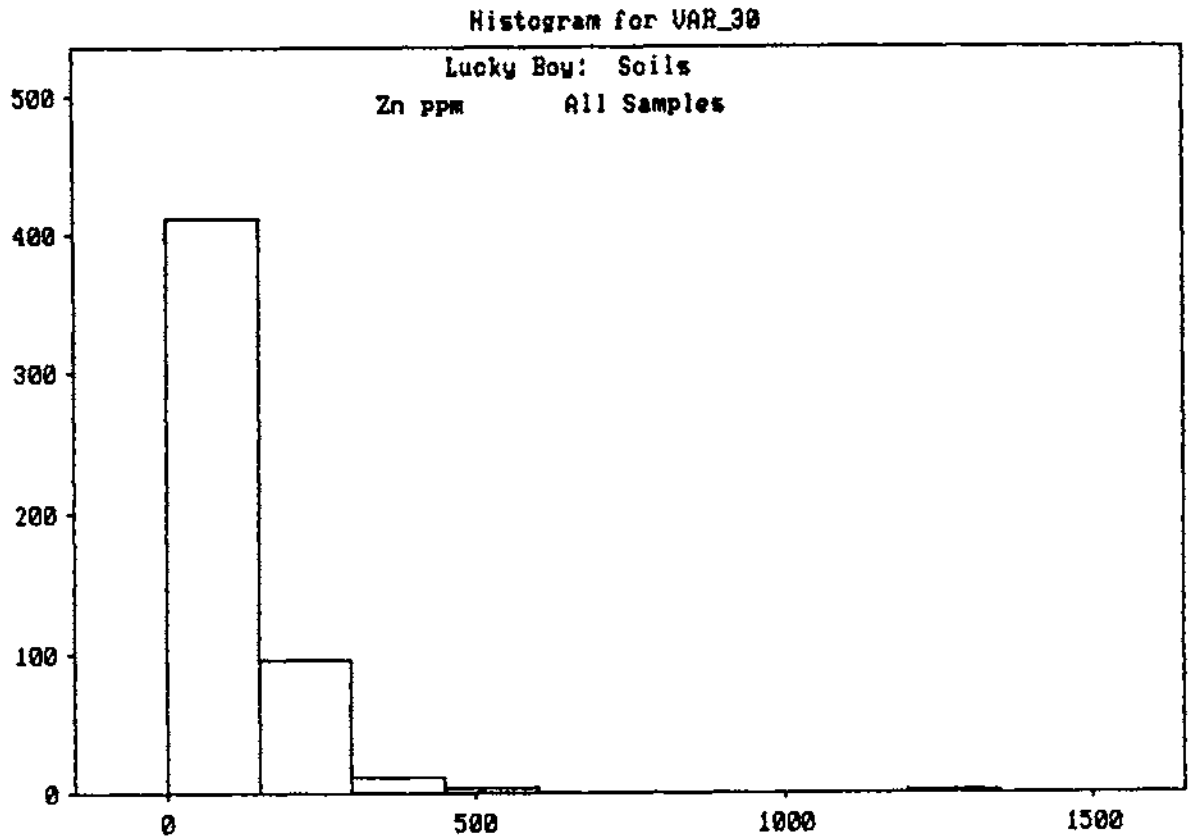
Mean = 12.263 Variance = 103.1
Standard Deviation = 10.16 Skewness = 4.441

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	5	35	7	35	7	
5	10	187	36	222	42	
10	15	192	37	414	79	Mean
15	20	67	13	481	92	
20	25	18	3	499	95	
25	30	7	1	506	96	
30	35	0	0	506	96	
35	40	3	1	509	97	
40	45	1	0	510	97	
45	50	6	1	516	98	

Data elements inside histogram 516
Data elements outside histogram 9

Descriptive Statistics

Mean	12.26286
Variance	103.133
Standard Deviation	10.15544
Skewness	4.440813



Mean = 128.75 Variance = 6786
Standard Deviation = 82.38 Skewness = 6.141

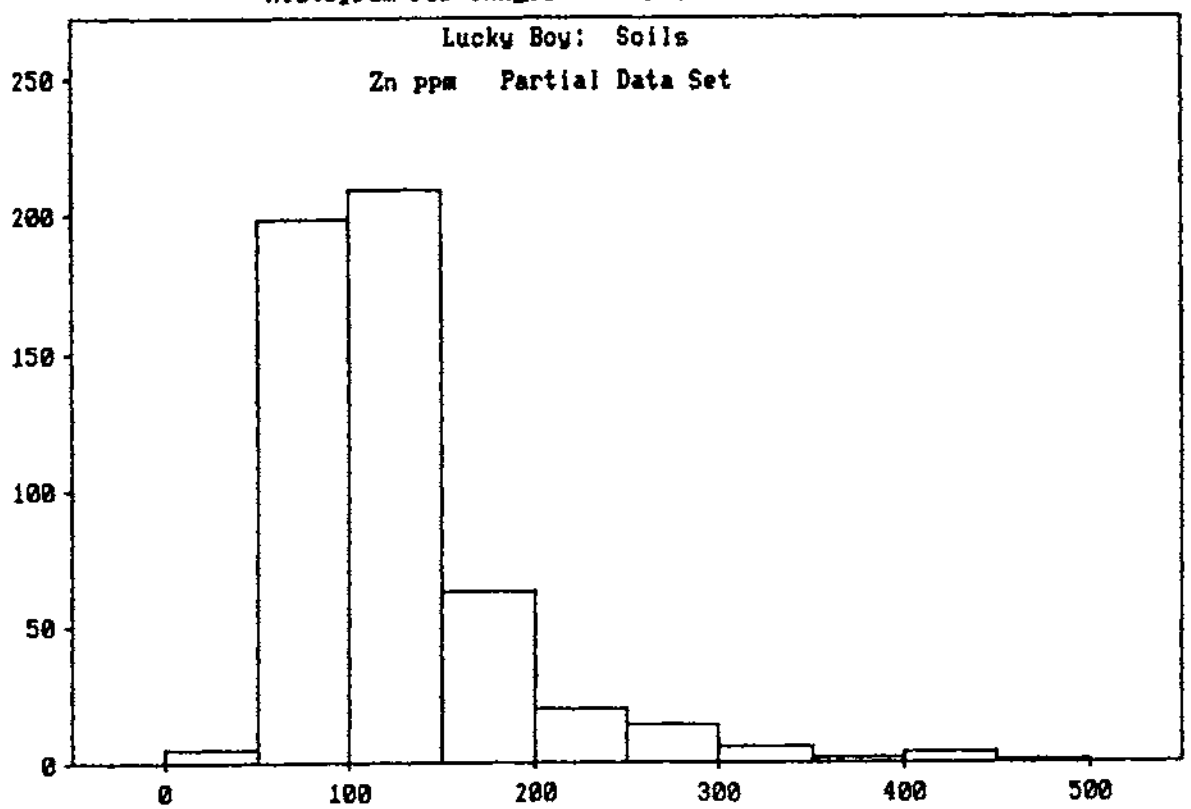
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	150	412	78	412	78	Mean
150	300	97	18	509	97	
300	450	12	2	521	99	
450	600	3	1	524	100	
600	750	0	0	524	100	
750	900	0	0	524	100	
900	1050	0	0	524	100	
1050	1200	0	0	524	100	
1200	1350	1	0	525	100	
1350	1500	0	0	525	100	

Data elements inside histogram 525
Data elements outside histogram 0

Descriptive Statistics

Mean	128.7486
Variance	6786.225
Standard Deviation	82.37855
Skewness	6.140551

Histogram for VAR_30 *** DATA OUTSIDE RANGE ***



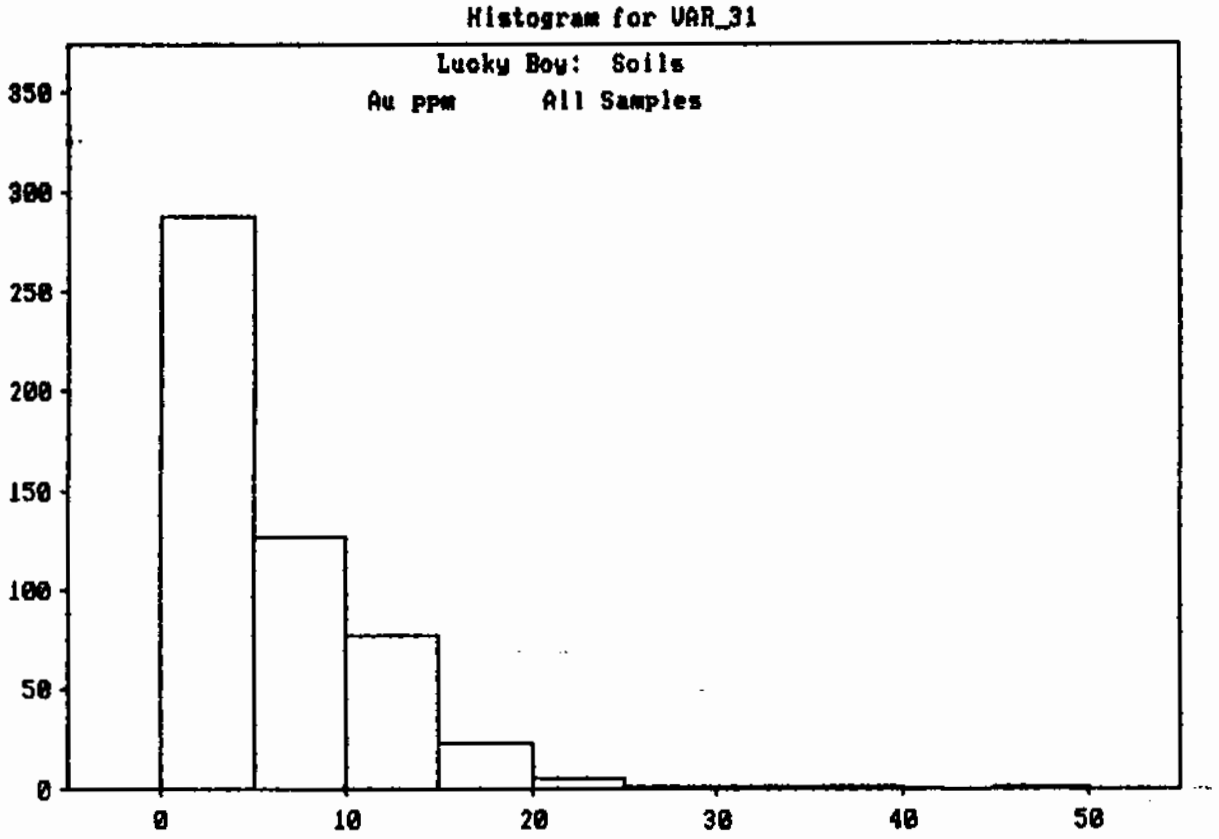
Mean = 128.75 Variance = 6786
Standard Deviation = 82.38 Skewness = 6.141

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	50	5	1	5	1	
50	100	198	38	203	39	
100	150	209	40	412	78	Mean
150	200	63	12	475	90	
200	250	20	4	495	94	
250	300	14	3	509	97	
300	350	6	1	515	98	
350	400	2	0	517	98	
400	450	4	1	521	99	
450	500	1	0	522	99	

Data elements inside histogram 522
Data elements outside histogram 3

Descriptive Statistics

Mean	128.7486
Variance	6786.225
Standard Deviation	82.37855
Skewness	6.140551



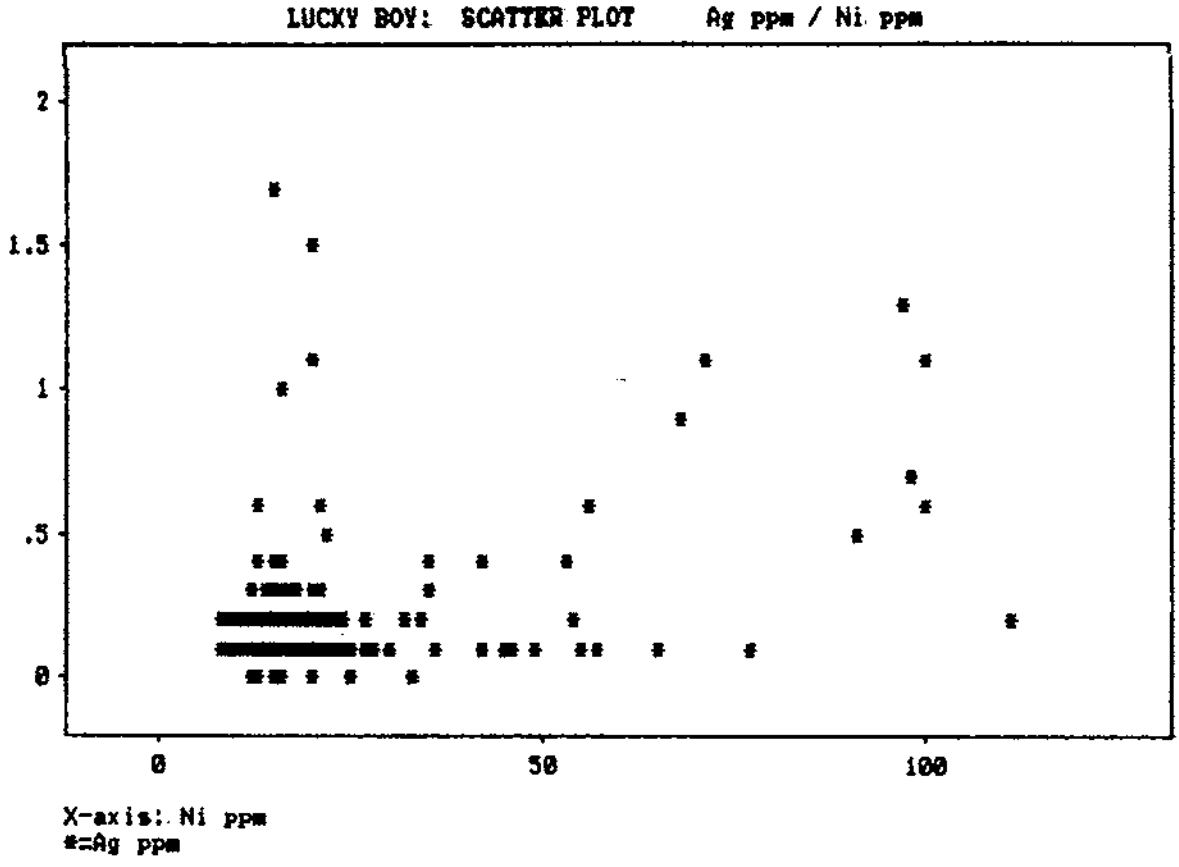
Mean = 3.8762 Variance = 31.37
Standard Deviation = 5.601 Skewness = 2.261

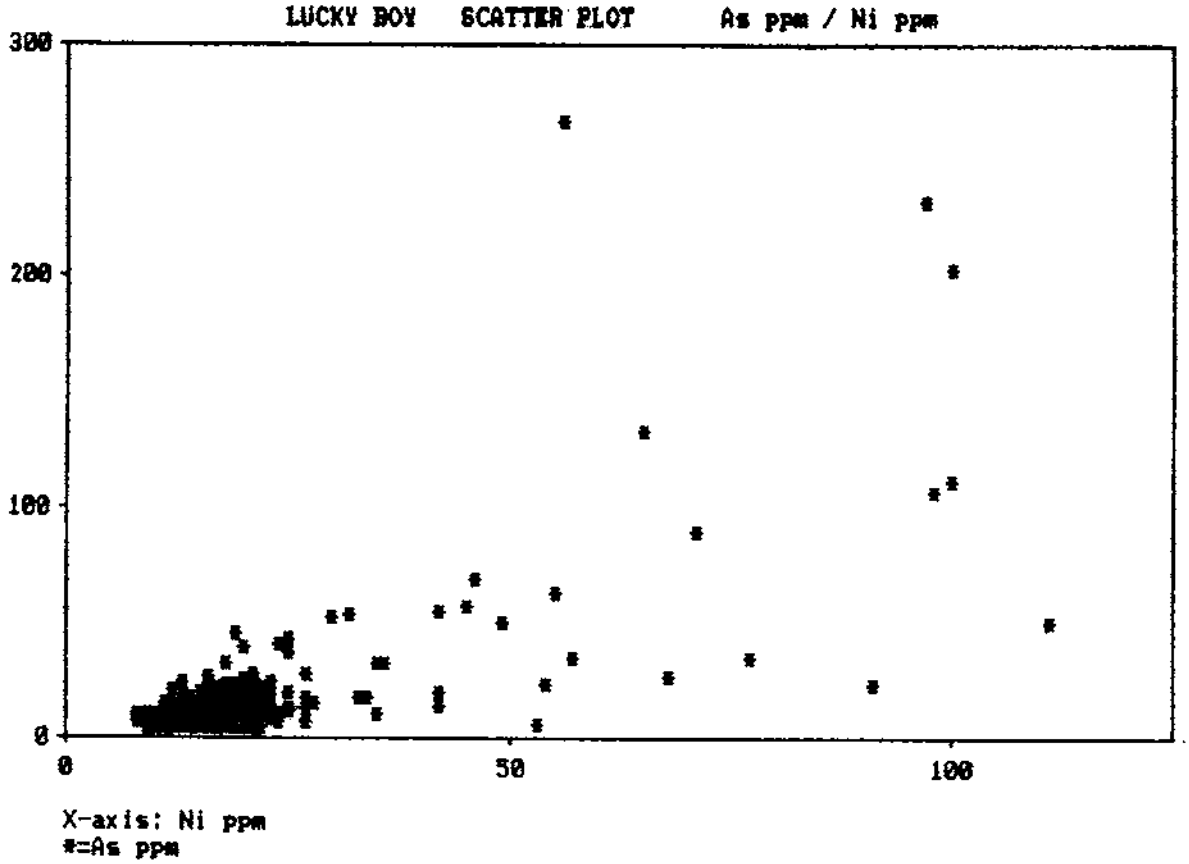
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	5	288	55	288	55	Mean
5	10	126	24	414	79	
10	15	77	15	491	94	
15	20	23	4	514	98	
20	25	5	1	519	99	
25	30	2	0	521	99	
30	35	2	0	523	100	
35	40	1	0	524	100	
40	45	0	0	524	100	
45	50	1	0	525	100	

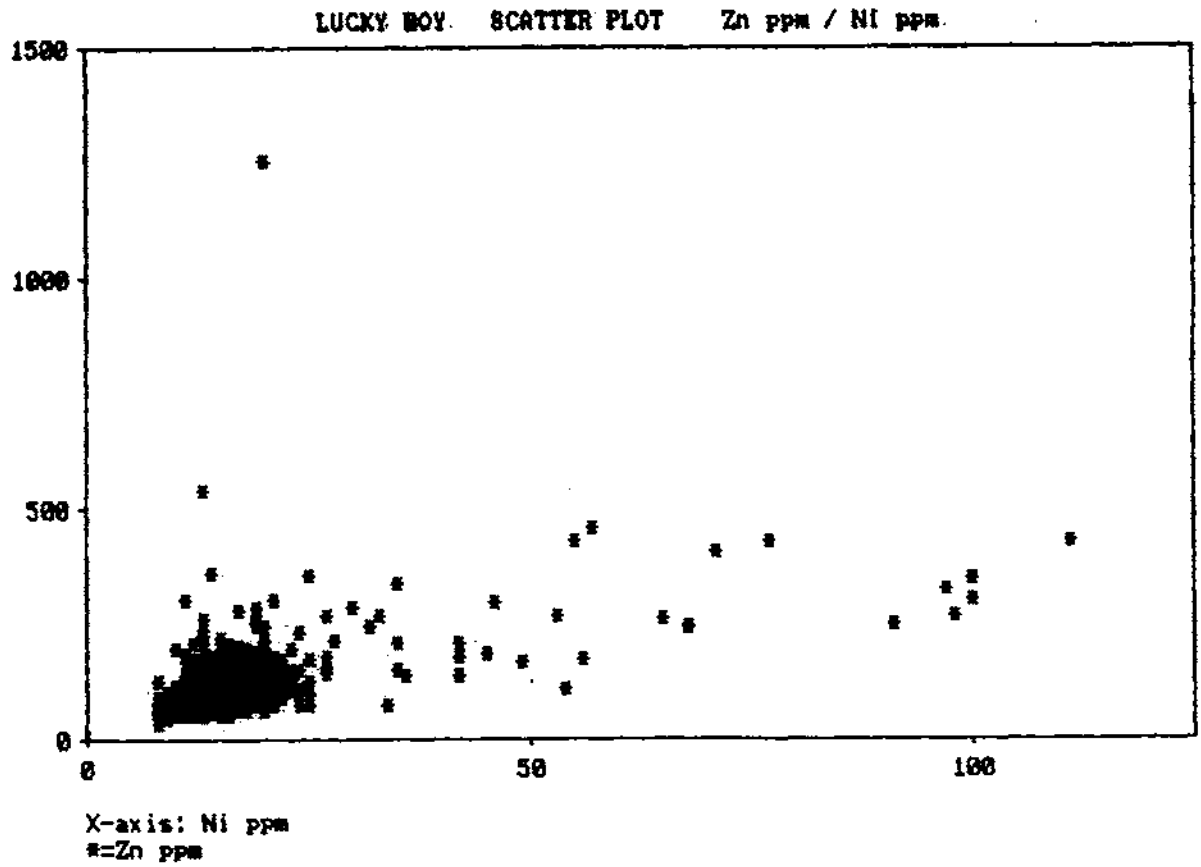
Data elements inside histogram 525
Data elements outside histogram 0

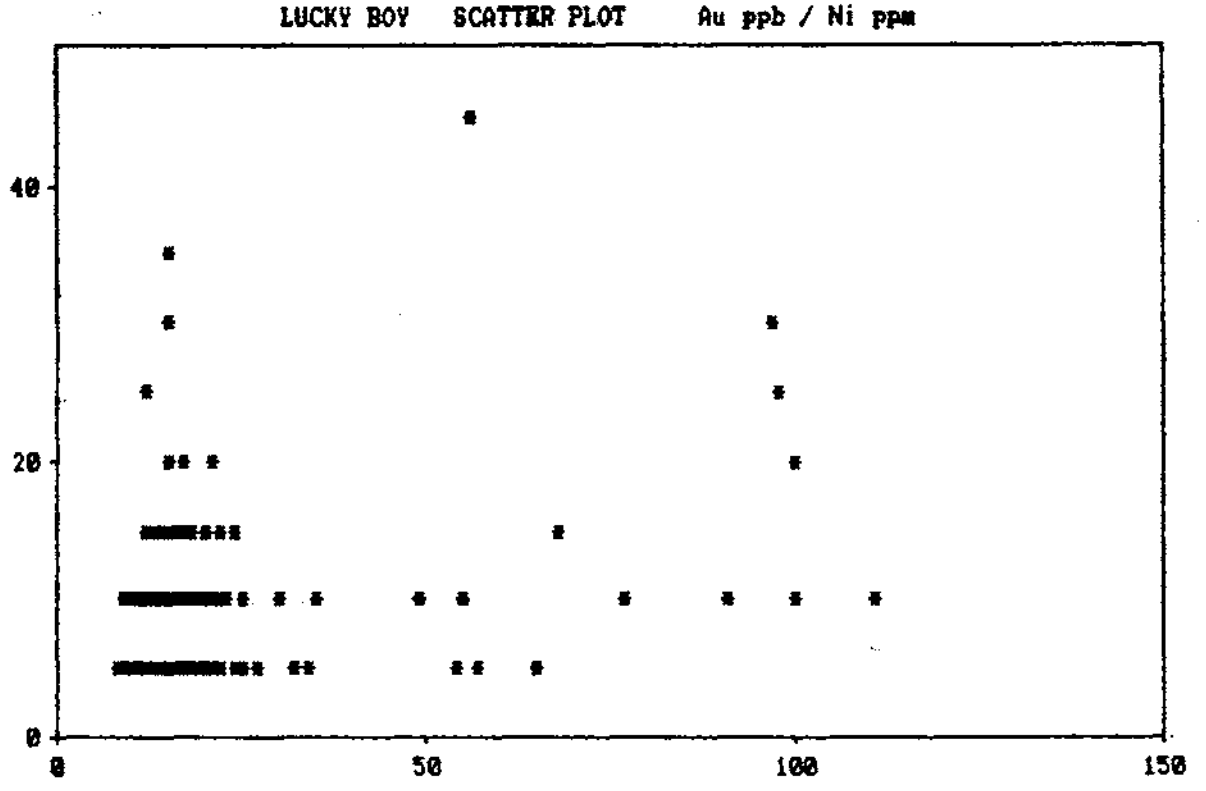
Descriptive Statistics

Mean	3.87619
Variance	31.36824
Standard Deviation	5.600736
Skewness	2.260639


LUCKY BOY: SCATTER PLOT Ag ppm / Ni ppm
2
1.5
1
.5
0
0
50
100
X-axis: Ni ppm
*=Ag ppm


LUCKY BOY SCATTER PLOT As ppm / Ni ppm
300
200
100
0
0
50
100
X-axis: Ni ppm
*=As ppm


LUCKY BOY SCATTER PLOT Zn ppm / Ni ppm
1500
1000
500
0
0
50
100
X-axis: Ni ppm
*=Zn ppm


LUCKY BOY SCATTER PLOT Au ppb / Ni ppm
40
20
0
0
50
100
150
X-axis: Ni ppm
*=Au ppb

APPENDIX F

MAGNETOMETER AND VLF-EM

FIELD DATA WORKSHEETS

AND EQUIPMENT SPECIFICATIONS

INTERPRETEX RESOURCES LTD. Data listing (Line & Station + = Northing/Easting, - = Southing/Westing)

Current File Name: LBDATA.WRI
From File: LBA.DAT
LBSMAGA.XYZ

Area: BEAVERDELL
Grid: LUCKY BOY PROPERTY
Date: March 11, 1988

DATA TYPE(S):	INSTRUMENT TYPE:	DATA DETAILS:
# 1. VLF-EM In-Phase Values	EDA VLF-EM/Magnetic System	Facing northerly using Seattle Transmitter
# 2. VLF-EM Quadrature (Out-of-Phase)	" " " "	Facing northerly using Seattle Transmitter
# 3. VLF-EM Field Strength	" " " "	Seattle total field strength
# 4.		
# 5. line number (Magnetic Values)		
# 6. station no. " "		
# 7. Total Field Magnetic Values	EDA VLF-EM/Magnetic System	Corrected total magnetic field
# 8.		
# 9.		
# 10.		

LINE #	STATION	# 1.	# 2.	# 3.	# 4.	# 5.	# 6.	# 7.
-1500	-587.5	19.3	5.2	180.1		-1500	-600.0	56114
-1500	-575.0	21.2	7.0	184.8		-1500	-587.5	56792
-1500	-562.5	21.5	7.1	176.9		-1500	-575.0	56808
-1500	-550.0	22.4	7.9	181.8		-1500	-562.5	56823
-1500	-537.5	23.8	8.0	181.9		-1500	-550.0	56824
-1500	-525.0	24.9	8.4	186.6		-1500	-537.5	56815
-1500	-512.5	25.5	9.6	192.2		-1500	-525.0	56785
-1500	-500.0	24.4	7.6	192.9		-1500	-512.5	56851
-1500	-487.5	24.9	7.6	193.0		-1500	-500.0	56761
-1500	-475.0	24.3	7.6	201.0		-1500	-487.5	56732
-1500	-462.5	25.1	7.1	196.7		-1500	-475.0	56736
-1500	-450.0	25.7	5.8	195.0		-1500	-462.5	56707
-1500	-437.5	26.4	4.0	191.3		-1500	-450.0	56710
-1500	-425.0	25.4	1.7	188.0		-1500	-437.5	56760
-1500	-412.5	26.5	3.0	187.2		-1500	-425.0	56767
-1500	-400.0	25.8	6.2	194.2		-1500	-412.5	56752
-1500	-387.5	26.9	3.0	185.3		-1500	-400.0	56743
-1500	-375.0	24.8	6.3	191.1		-1500	-387.5	56777
-1500	-362.5	25.9	2.1	188.6		-1500	-375.0	56830
-1500	-350.0	25.1	6.1	193.2		-1500	-362.5	56827
-1500	-337.5	25.5	3.8	196.4		-1500	-350.0	56839
-1500	-325.0	26.3	6.0	196.2		-1500	-337.5	56765
-1500	-312.5	25.1	4.3	193.7		-1500	-325.0	56740
-1500	-300.0	26.9	2.0	190.5		-1500	-312.5	56713
-1500	-287.5	25.6	5.8	199.3		-1500	-300.0	56713
-1500	-275.0	26.5	1.0	197.1		-1500	-287.5	56698
-1500	-262.5	26.5	5.2	208.9		-1500	-275.0	56769
-1500	-250.0	24.9	4.0	218.7		-1500	-262.5	56738
-1500	-237.5	20.8	1.6	224.1		-1500	-250.0	56783
-1500	-225.0	18.8	-0.1	221.2		-1500	-237.5	56798
-1500	-212.5	17.9	1.1	220.6		-1500	-225.0	56801
-1500	-200.0	18.1	0.7	211.9		-1500	-212.5	56837
-1500	-187.5	18.6	0.8	207.4		-1500	-200.0	56812
-1500	-175.0	18.1	2.2	202.5		-1500	-187.5	56840
-1500	-162.5	18.1	2.2	206.9		-1500	-175.0	56847
-1500	-150.0	16.5	0.8	207.9		-1500	-162.5	56867
-1500	-137.5	14.7	0.6	205.6		-1500	-150.0	56805
-1500	-125.0	12.9	-1.6	200.7		-1500	-137.5	56783

-1500	-112.5	13.0	-1.2	192.7	-1500	-125.0	56818
-1500	-100.0	13.8	-0.8	192.1	-1500	-112.5	56818
-1500	-87.5	14.2	0.3	187.7	-1500	-100.0	56814
-1500	-75.0	14.5	0.8	187.2	-1500	-87.5	56767
-1500	-62.5	15.7	2.2	186.2	-1500	-75.0	56748
-1500	-50.0	16.6	2.6	182.4	-1500	-62.5	56791
-1500	-37.5	17.5	2.5	183.7	-1500	-50.0	56803
-1500	-25.0	17.1	2.6	183.9	-1500	-37.5	56801
-1500	-12.5	18.0	2.4	181.9	-1500	-25.0	56787
-1500	0.0	17.9	0.7	178.0	-1500	-12.5	56800
-1500	12.5	18.8	3.1	179.5	-1500	0.0	56784
-1500	25.0	19.0	0.9	172.6	-1500	12.5	56805
-1500	37.5	20.0	2.4	174.7	-1500	25.0	56873
-1500	50.0	20.2	1.6	179.5	-1500	37.5	56872
-1500	62.5	20.8	0.4	171.9	-1500	50.0	56864
-1500	75.0	20.9	1.9	169.9	-1500	62.5	56820
-1500	87.5	23.5	3.3	167.4	-1500	75.0	56818
-1500	100.0	23.9	3.9	169.0	-1500	87.5	56893
-1500	112.5	26.4	-1.6	162.2	-1500	100.0	56808
-1500	125.0	27.4	0.1	163.5	-1500	112.5	56835
-1500	137.5	28.9	3.8	171.9	-1500	125.0	56857
-1500	150.0	29.0	4.1	176.5	-1500	137.5	56810
-1500	162.5	26.5	2.4	179.3	-1500	150.0	56731
-1500	175.0	26.9	2.7	181.2	-1500	162.5	56795
-1500	187.5	25.2	0.9	187.7	-1500	175.0	56841
-1500	200.0	24.3	-0.7	187.3	-1500	187.5	56820
-1500	212.5	22.2	-1.1	189.0	-1500	200.0	56759
-1500	225.0	20.3	-3.6	187.7	-1500	212.5	56753
-1500	237.5	18.1	-4.1	182.0	-1500	225.0	56819
-1500	250.0	15.7	-6.6	172.9	-1500	237.5	56782
-1500	262.5	12.9	-6.3	169.4	-1500	250.0	56798
-1500	275.0	14.4	-6.2	164.2	-1500	262.5	56799
-1500	287.5	15.4	-5.6	164.3	-1500	275.0	56797
-1500	300.0	18.0	-5.1	168.0	-1500	287.5	56806
-1500	312.5	19.3	-4.6	166.9	-1500	300.0	56828
-1500	325.0	16.9	-6.9	167.1	-1500	312.5	56856
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-1500	350.0	16.3	-10.0	155.4	-1500	337.5	56743
-1500	362.5	24.6	-4.3	152.8	-1500	350.0	56725
-1500	375.0	21.7	-7.9	159.3	-1500	362.5	56749
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-1500	400.0	28.3	-8.2	148.9	-1500	387.5	56685
-1500	412.5	35.0	-7.7	153.5	-1500	400.0	56643
-1500	425.0	39.0	-11.2	158.4	-1500	412.5	56817
-1500	437.5	43.1	-7.8	165.0	-1500	425.0	56727
-1500	450.0	40.4	-9.7	170.0	-1500	437.5	56732
-1500	462.5	39.0	-9.4	171.3	-1500	450.0	56898
-1500	475.0	39.2	-11.0	176.3	-1500	462.5	56961
-1500	487.5	41.8	-9.8	175.6	-1500	475.0	56840
-1500	500.0	44.5	-5.7	177.2	-1500	487.5	56719
-1500	512.5	51.0	-3.1	182.3	-1500	500.0	56698
-1500	525.0	49.1	-3.1	182.1	-1500	512.5	56766
-1500	537.5	47.4	-4.4	183.5	-1500	525.0	56790
-1500	550.0	48.4	-7.4	173.6	-1500	537.5	56772
-1500	562.5	51.8	-4.7	175.2	-1500	550.0	56728
-1500	575.0	54.1	-5.5	178.9	-1500	562.5	56739

-1500	587.5	54.2	-5.1	188.0	-1500	575.0	56719
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-1500	612.5	43.9	-6.5	194.5	-1500	600.0	56780
-1500	625.0	38.0	-0.6	198.6	-1500	612.5	56779
-1500	637.5	34.5	-6.1	189.6	-1500	625.0	56758
-1500	650.0	32.4	-5.2	189.1	-1500	637.5	56771
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-1500	675.0	33.2	-6.2	182.2	-1500	662.5	56766
-1500	687.5	35.2	0.0	185.3	-1500	675.0	56771
-1500	700.0	34.3	-5.5	180.0	-1500	687.5	56776
-1500	712.5	36.0	1.6	182.9	-1500	700.0	56761
-1500	725.0	38.0	1.9	180.2	-1500	712.5	56758
-1500	737.5	43.4	5.9	188.6	-1500	725.0	56749
-1500	750.0	43.2	4.9	211.8	-1500	737.5	56744
-1500	762.5	43.5	2.5	216.7	-1500	750.0	56773
-1500	775.0	41.1	2.3	227.7	-1500	762.5	56758
-1500	787.5	36.9	0.6	220.8	-1500	775.0	56757
-1500	800.0	37.1	1.5	220.6	-1500	787.5	56760
-1400	-500.0	15.8	-6.1	128.2	-1500	800.0	56768
-1400	-487.5	15.4	-6.6	125.9	-1400	-500.0	56770
-1400	-475.0	16.4	-6.0	126.5	-1400	-487.5	56764
-1400	-462.5	16.3	6.0	127.1	-1400	-475.0	56698
-1400	-450.0	14.7	-9.4	132.1	-1400	-462.5	56704
-1400	-437.5	16.1	4.2	130.9	-1400	-450.0	56680
-1400	-425.0	14.8	-7.5	136.5	-1400	-437.5	56641
-1400	-412.5	15.8	-8.4	140.3	-1400	-425.0	56631
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-1400	-387.5	15.2	-7.2	153.8	-1400	-400.0	56803
-1400	-375.0	14.7	-4.7	159.5	-1400	-387.5	56817
-1400	-362.5	12.3	-2.3	166.0	-1400	-375.0	56813
-1400	-350.0	12.1	-0.7	164.8	-1400	-362.5	56814
-1400	-337.5	12.4	-2.3	164.8	-1400	-350.0	56821
-1400	-325.0	15.3	-2.2	166.3	-1400	-337.5	56751
-1400	-312.5	16.8	-2.3	169.9	-1400	-325.0	56761
-1400	-300.0	18.9	-4.9	175.4	-1400	-312.5	56805
-1400	-287.5	19.7	-2.8	175.4	-1400	-300.0	56733
-1400	-275.0	19.4	-3.2	178.8	-1400	-287.5	56692
-1400	-262.5	18.5	-2.4	176.6	-1400	-275.0	56723
-1400	-250.0	21.9	-6.0	179.7	-1400	-262.5	56678
-1400	-237.5	23.0	-6.3	178.5	-1400	-250.0	56836
-1400	-225.0	23.8	-5.0	181.8	-1400	-237.5	56806
-1400	-212.5	23.2	-5.9	186.2	-1400	-225.0	56872
-1400	-200.0	25.1	-7.4	185.3	-1400	-212.5	56792
-1400	-187.5	27.8	-9.5	183.1	-1400	-200.0	56658
-1400	-175.0	27.8	-10.1	193.4	-1400	-187.5	56639
-1400	-162.5	21.7	-5.5	194.4	-1400	-175.0	56770
-1400	-150.0	22.0	-8.9	198.1	-1400	-162.5	56779
-1400	-137.5	19.1	-6.1	202.0	-1400	-150.0	56801
-1400	-125.0	15.8	-5.5	202.8	-1400	-137.5	56832
-1400	-112.5	11.7	-4.7	197.4	-1400	-125.0	56837
-1400	-100.0	16.2	-6.7	193.6	-1400	-112.5	56759
-1400	-87.5	12.8	-3.7	198.4	-1400	-100.0	56839
-1400	-75.0	11.6	-3.7	190.1	-1400	-87.5	56838
-1400	-62.5	14.0	-6.2	194.3	-1400	-75.0	56753
-1400	-50.0	11.5	-5.0	194.7	-1400	-62.5	56825
-1400	-37.5	10.1	-2.8	188.9	-1400	-50.0	56789

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-1400	12.5	7.6	-0.9	182.9	-1400	0.0	56725
-1400	25.0	9.2	-1.0	179.5	-1400	12.5	56719
-1400	37.5	9.7	-2.4	180.7	-1400	25.0	56711
-1400	50.0	10.8	-2.1	180.3	-1400	37.5	56726
-1400	62.5	12.9	-4.8	177.2	-1400	50.0	56733
-1400	75.0	13.9	-5.2	177.8	-1400	62.5	56773
-1400	87.5	15.7	-4.5	176.7	-1400	75.0	56822
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-1400	112.5	16.4	-6.0	177.1	-1400	100.0	56817
-1400	125.0	18.9	-5.9	173.9	-1400	112.5	56850
-1400	137.5	21.2	-6.7	176.1	-1400	125.0	56811
-1400	150.0	19.5	-6.4	178.3	-1400	137.5	56893
-1400	162.5	20.0	-6.4	179.2	-1400	150.0	56877
-1400	175.0	19.2	-5.8	180.1	-1400	162.5	56877
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-1400	212.5	16.3	-5.2	176.8	-1400	200.0	56797
-1400	225.0	17.7	-6.6	172.0	-1400	212.5	56753
-1400	237.5	18.8	-6.0	173.5	-1400	225.0	56717
-1400	250.0	16.4	-5.6	167.9	-1400	237.5	56839
-1400	262.5	22.1	-8.8	168.4	-1400	250.0	56745
-1400	275.0	19.4	-11.1	173.3	-1400	262.5	56807
-1400	287.5	17.0	-7.7	173.1	-1400	275.0	56899
-1400	300.0	16.8	-6.9	170.6	-1400	287.5	56882
-1400	312.5	16.0	5.1	169.4	-1400	300.0	56912
-1400	325.0	12.8	-3.0	169.1	-1400	312.5	56909
-1400	337.5	9.6	8.0	163.3	-1400	325.0	56865
-1400	350.0	5.0	6.2	157.6	-1400	337.5	56829
-1400	362.5	9.1	9.4	151.2	-1400	350.0	56816
-1400	375.0	5.5	9.0	144.8	-1400	362.5	56895
-1400	387.5	10.2	14.6	130.3	-1400	375.0	56764
-1400	400.0	22.3	-5.4	137.1	-1400	387.5	56686
-1400	412.5	28.5	-11.7	137.8	-1400	400.0	56531
-1400	425.0	37.1	10.0	134.5	-1400	412.5	56483
-1400	437.5	41.4	-14.6	150.3	-1400	425.0	56587
-1400	450.0	38.7	-8.5	164.2	-1400	437.5	56665
-1400	462.5	36.1	-7.4	167.9	-1400	450.0	56645
-1400	475.0	41.6	13.3	162.8	-1400	462.5	56625
-1400	487.5	47.1	-14.0	169.0	-1400	475.0	56738
-1400	500.0	54.3	9.8	173.7	-1400	487.5	56807
-1400	512.5	52.3	-9.1	178.5	-1400	500.0	56865
-1400	525.0	55.6	-9.2	176.6	-1400	512.5	56862
-1400	537.5	54.8	-10.6	171.1	-1400	525.0	56864
-1400	550.0	55.4	-10.9	170.7	-1400	537.5	56856
-1400	562.5	57.3	-10.0	177.9	-1400	550.0	56842
-1400	575.0	58.8	-10.1	180.9	-1400	562.5	56835
-1400	587.5	60.9	-11.6	185.8	-1400	575.0	56833
-1400	600.0	61.3	-10.7	200.8	-1400	587.5	56833
-1400	612.5	55.7	-10.2	205.2	-1400	600.0	56841
-1400	625.0	49.9	-7.4	222.0	-1400	612.5	56837
-1400	637.5	44.6	-5.4	220.8	-1400	625.0	56831
-1400	650.0	39.3	-2.6	222.4	-1400	637.5	56834
-1400	662.5	36.9	-3.7	217.0	-1400	650.0	56827

-1400	675.0	35.0	-2.4	220.1	-1400	662.5	56832
-1400	687.5	32.8	-2.0	214.2	-1400	675.0	56823
-1400	700.0	32.3	-2.2	210.5	-1400	687.5	56822
-1400	712.5	31.9	-3.2	212.8	-1400	700.0	56820
-1400	725.0	31.1	-0.1	207.4	-1400	712.5	56821
-1400	737.5	31.6	-0.9	205.9	-1400	725.0	56821
-1400	750.0	32.3	-2.9	204.8	-1400	737.5	56816
-1400	762.5	34.2	-2.5	203.0	-1400	750.0	56813
-1400	775.0	34.4	-3.2	200.2	-1400	762.5	56810
-1400	787.5	35.9	-4.3	201.2	-1400	775.0	56798
-1400	800.0	37.4	-8.3	205.6	-1400	787.5	56778
-1300	-500.0	17.3	11.0	115.4	-1400	800.0	56802
-1300	-487.5	17.6	10.6	118.5	-1300	-500.0	56794
-1300	-475.0	18.6	9.1	119.2	-1300	-487.5	56761
-1300	-462.5	19.3	9.4	119.3	-1300	-475.0	56803
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-1300	-412.5	18.9	7.6	124.0	-1300	-425.0	56817
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-1300	-387.5	19.6	6.9	122.0	-1300	-400.0	56754
-1300	-375.0	19.9	8.3	124.3	-1300	-387.5	56765
-1300	-362.5	18.0	9.3	127.3	-1300	-375.0	56739
-1300	-350.0	16.9	7.3	128.0	-1300	-362.5	56705
-1300	-337.5	17.9	6.2	128.9	-1300	-350.0	56834
-1300	-325.0	19.2	6.9	128.5	-1300	-337.5	56947
-1300	-312.5	20.1	6.8	128.7	-1300	-325.0	56991
-1300	-300.0	20.6	10.0	132.6	-1300	-312.5	57002
-1300	-287.5	21.9	6.0	132.0	-1300	-300.0	56951
-1300	-275.0	22.1	7.7	133.6	-1300	-287.5	56796
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-1300	-250.0	23.9	10.9	154.0	-1300	-262.5	56799
-1300	-237.5	24.1	10.1	156.9	-1300	-250.0	56801
-1300	-225.0	24.6	10.3	158.2	-1300	-237.5	56765
-1300	-212.5	24.2	8.9	161.5	-1300	-225.0	56716
-1300	-200.0	24.1	9.4	163.3	-1300	-212.5	56781
-1300	-187.5	25.5	9.1	162.8	-1300	-200.0	56751
-1300	-175.0	26.5	9.5	161.3	-1300	-187.5	56640
-1300	-162.5	30.7	14.3	170.3	-1300	-175.0	56611
-1300	-150.0	32.1	14.4	172.9	-1300	-162.5	56618
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-1300	-125.0	35.4	18.8	180.4	-1300	-137.5	56764
-1300	-112.5	37.4	18.8	184.6	-1300	-125.0	56777
-1300	-100.0	37.2	18.3	187.4	-1300	-112.5	56818
-1300	-87.5	38.5	18.6	184.8	-1300	-100.0	56819
-1300	-75.0	41.6	20.8	196.0	-1300	-87.5	56783
-1300	-62.5	39.7	16.7	205.0	-1300	-75.0	56851
-1300	-50.0	36.3	14.9	202.3	-1300	-62.5	56807
-1300	-37.5	39.0	16.6	202.8	-1300	-50.0	56726
-1300	-25.0	40.5	18.2	205.3	-1300	-37.5	56735
-1300	-12.5	36.8	12.2	207.5	-1300	-25.0	56754
-1300	0.0	32.1	10.9	206.7	-1300	-12.5	56767
-1300	12.5	29.7	9.9	198.3	-1300	0.0	56807
-1300	25.0	37.8	14.5	203.4	-1300	12.5	56788
-1300	37.5	28.3	9.1	208.5	-1300	25.0	56775
-1300	50.0	23.1	7.9	209.2	-1300	37.5	56761

-1300	62.5	19.9	6.8	200.1
-1300	75.0	17.1	6.1	192.4
-1300	87.5	19.6	8.7	189.7
-1300	100.0	20.8	8.7	183.7
-1300	112.5	21.3	11.2	183.4
-1300	125.0	21.3	10.8	188.3
-1300	137.5	19.1	10.3	190.8
-1300	150.0	17.9	10.8	192.1
-1300	162.5	18.4	9.9	197.1
-1300	175.0	9.8	5.7	190.0
-1300	187.5	9.6	5.6	186.4
-1300	200.0	10.2	4.9	183.3
-1300	212.5	10.6	4.6	179.8
-1300	225.0	10.1	4.1	177.5
-1300	237.5	11.6	4.6	173.9
-1300	250.0	12.2	4.6	174.4
-1300	262.5	13.3	5.3	177.3
-1300	275.0	9.6	2.2	181.5
-1300	287.5	2.7	-2.8	175.3
-1300	300.0	10.6	1.6	162.5
-1300	312.5	4.4	-2.1	166.1
-1300	325.0	8.2	-0.5	159.4
-1300	337.5	11.0	0.5	156.0
-1300	350.0	15.0	1.9	153.7
-1300	362.5	17.8	4.0	150.0
-1300	375.0	22.5	4.8	145.8
-1300	387.5	23.9	6.6	141.7
-1300	400.0	27.9	8.9	136.1
-1300	412.5	31.6	11.0	132.2
-1300	425.0	39.3	13.3	127.6
-1300	437.5	42.4	19.0	132.7
-1300	450.0	42.6	16.2	132.8
-1300	462.5	46.6	16.6	132.8
-1300	475.0	50.3	19.2	135.7
-1300	487.5	55.0	19.9	139.4
-1300	500.0	57.4	20.1	151.1
-1300	512.5	56.9	18.3	155.6
-1300	525.0	55.1	17.2	163.4
-1300	537.5	54.4	15.4	169.1
-1300	550.0	52.5	13.3	176.9
-1300	562.5	47.8	9.3	179.4
-1300	575.0	45.4	7.0	180.1
-1300	587.5	43.8	5.9	181.0
-1300	600.0	42.0	3.3	181.9
-1300	612.5	40.0	2.6	187.5
-1300	625.0	40.3	3.5	183.6
-1300	637.5	40.8	3.9	188.1
-1300	650.0	40.5	3.7	190.0
-1300	662.5	40.6	3.6	193.5
-1300	675.0	39.5	3.9	196.1
-1300	687.5	37.4	2.3	196.0
-1300	700.0	36.3	2.0	195.0
-1300	712.5	35.8	2.5	193.4
-1300	725.0	34.8	2.7	194.6
-1300	737.5	34.5	1.9	194.0
-1300	750.0	34.9	2.8	194.0

-1300	50.0	56709
-1300	62.5	56716
-1300	75.0	56737
-1300	87.5	56712
-1300	100.0	56780
-1300	112.5	56803
-1300	125.0	56797
-1300	137.5	56813
-1300	150.0	56825
-1300	162.5	56811
-1300	175.0	56783
-1300	187.5	56789
-1300	200.0	56787
-1300	212.5	56820
-1300	225.0	56859
-1300	237.5	56892
-1300	250.0	56901
-1300	262.5	56853
-1300	275.0	56900
-1300	287.5	56782
-1300	300.0	56837
-1300	312.5	56749
-1300	325.0	56706
-1300	337.5	56669
-1300	350.0	56644
-1300	362.5	56639
-1300	375.0	56517
-1300	387.5	56537
-1300	400.0	56504
-1300	412.5	56446
-1300	425.0	56612
-1300	437.5	56654
-1300	450.0	56643
-1300	462.5	56692
-1300	475.0	56794
-1300	487.5	56994
-1300	500.0	57012
-1300	512.5	56943
-1300	525.0	56908
-1300	537.5	56889
-1300	550.0	56869
-1300	562.5	56895
-1300	575.0	56884
-1300	587.5	56875
-1300	600.0	56875
-1300	612.5	56865
-1300	625.0	56862
-1300	637.5	56860
-1300	650.0	56856
-1300	662.5	56856
-1300	675.0	56854
-1300	687.5	56857
-1300	700.0	56858
-1300	712.5	56854
-1300	725.0	56848
-1300	737.5	56849

-1300	762.5	31.9	2.7	196.6	-1300	750.0	56852
-1300	775.0	29.9	2.0	196.6	-1300	762.5	56845
-1300	787.5	28.6	2.8	193.9	-1300	775.0	56842
-1300	800.0	27.5	2.4	192.9	-1300	787.5	56848
-1200	-600.0	9.4	-3.8	145.7	-1300	800.0	56838
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-1200	-575.0	5.6	-1.7	147.7	-1200	-587.5	56702
-1200	-562.5	3.9	0.4	147.4	-1200	-575.0	56724
-1200	-550.0	1.6	2.3	147.9	-1200	-562.5	56733
-1200	-537.5	-0.7	2.3	146.7	-1200	-550.0	56720
-1200	-525.0	-2.6	3.2	140.9	-1200	-537.5	56714
-1200	-512.5	-2.7	1.7	139.0	-1200	-525.0	56679
-1200	-500.0	-1.0	1.2	136.5	-1200	-512.5	56664
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-1200	-462.5	0.4	-0.9	133.5	-1200	-475.0	56679
-1200	-450.0	2.2	-1.3	131.3	-1200	-462.5	56750
-1200	-437.5	3.0	-3.2	130.5	-1200	-450.0	56787
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-1200	-412.5	6.5	-4.1	131.7	-1200	-425.0	56809
-1200	-400.0	5.7	-3.7	130.7	-1200	-412.5	56741
-1200	-387.5	5.6	-3.8	130.9	-1200	-400.0	56732
-1200	-375.0	5.3	-4.1	128.7	-1200	-387.5	56747
-1200	-362.5	6.0	-4.6	127.9	-1200	-375.0	56750
-1200	-350.0	6.3	-6.2	128.2	-1200	-362.5	56751
-1200	-337.5	7.1	-4.1	128.2	-1200	-350.0	56794
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-1200	-287.5	7.8	-5.6	125.1	-1200	-300.0	56728
-1200	-275.0	8.6	-6.1	125.6	-1200	-287.5	56697
-1200	-262.5	9.1	-5.9	125.6	-1200	-275.0	56717
-1200	-250.0	10.1	-6.8	125.2	-1200	-262.5	56734
-1200	-237.5	10.4	-5.9	126.8	-1200	-250.0	56698
-1200	-225.0	10.6	-6.9	127.3	-1200	-237.5	56656
-1200	-212.5	11.1	-7.1	128.9	-1200	-225.0	56596
-1200	-200.0	13.7	-8.9	131.3	-1200	-212.5	56515
-1200	-187.5	12.9	-7.5	132.4	-1200	-200.0	56522
-1200	-175.0	11.9	-7.2	134.2	-1200	-187.5	56601
-1200	-162.5	11.5	-5.8	135.5	-1200	-175.0	56640
-1200	-150.0	11.2	-6.6	135.1	-1200	-162.5	56705
-1200	-137.5	11.7	-6.6	134.4	-1200	-150.0	56721
-1200	-125.0	11.6	-6.0	135.6	-1200	-137.5	56667
-1200	-112.5	12.4	-6.0	134.8	-1200	-125.0	56686
-1200	-100.0	12.9	-6.7	134.7	-1200	-112.5	56761
-1200	-87.5	13.6	-8.4	135.4	-1200	-100.0	56750
-1200	-75.0	14.0	-8.0	134.7	-1200	-87.5	56790
-1200	-62.5	14.1	-8.7	134.6	-1200	-75.0	56701
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-1200	-25.0	15.8	-10.3	133.1	-1200	-37.5	56797
-1200	-12.5	16.1	-10.8	132.0	-1200	-25.0	56790
-1200	0.0	16.9	-11.5	134.1	-1200	-12.5	56793
-1200	12.5	17.7	-11.0	135.2	-1200	0.0	56801
-1200	25.0	16.5	-10.5	137.6	-1200	12.5	56768
-1200	37.5	16.1	-10.3	137.9	-1200	25.0	56732

-1200	50.0	15.5	-9.6	138.5	-1200	37.5	56701
-1200	62.5	14.8	-9.5	138.4	-1200	50.0	56709
-1200	75.0	14.5	-9.4	138.4	-1200	62.5	56708
-1200	87.5	15.1	-9.9	138.5	-1200	75.0	56753
-1200	100.0	16.5	-12.3	143.0	-1200	87.5	56862
-1200	112.5	17.5	-11.7	144.9	-1200	100.0	56951
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-1200	137.5	17.3	-11.0	147.5	-1200	125.0	56895
-1200	150.0	17.3	-10.8	148.9	-1200	137.5	56889
-1200	162.5	16.7	-11.1	151.8	-1200	150.0	56907
-1200	175.0	16.1	-10.5	152.9	-1200	162.5	56915
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-1200	200.0	15.2	-10.2	157.1	-1200	187.5	56935
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-1200	262.5	1.0	4.3	145.3	-1200	250.0	56568
-1200	275.0	1.7	2.0	143.9	-1200	262.5	56569
-1200	287.5	4.6	0.9	141.5	-1200	275.0	56545
-1200	300.0	7.5	1.0	144.7	-1200	287.5	56493
-1200	312.5	9.3	0.0	141.3	-1200	300.0	56583
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-1200	337.5	13.7	-0.8	135.9	-1200	325.0	56517
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-1200	362.5	19.9	-7.1	138.2	-1200	350.0	56390
-1200	375.0	22.6	-10.8	135.3	-1200	362.5	56441
-1200	387.5	24.9	-9.3	131.7	-1200	375.0	56567
-1200	400.0	28.8	-13.0	133.0	-1200	387.5	56654
-1200	412.5	29.9	-14.3	136.4	-1200	400.0	56704
-1200	425.0	31.3	-15.4	138.0	-1200	412.5	56709
-1200	437.5	31.2	-12.5	139.6	-1200	425.0	56716
-1200	450.0	31.4	-15.0	141.0	-1200	437.5	56662
-1200	462.5	31.8	-15.1	141.5	-1200	450.0	56792
-1200	475.0	33.2	-12.0	142.3	-1200	462.5	56814
-1200	487.5	34.5	-15.5	142.6	-1200	475.0	56889
-1200	500.0	34.8	-17.9	146.7	-1200	487.5	56984
-1200	512.5	36.4	-19.0	151.0	-1200	500.0	57154
-1200	525.0	35.5	-17.8	151.8	-1200	512.5	57240
-1200	537.5	35.2	-15.2	155.6	-1200	525.0	57245
-1200	550.0	34.2	-14.1	158.5	-1200	537.5	57132
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-1200	612.5	24.9	-5.8	151.9	-1200	600.0	56913
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-1200	712.5	33.2	-11.9	175.5	-1200	700.0	56772
-1200	725.0	30.9	-11.4	181.8	-1200	712.5	56955
-1200	737.5	29.6	-7.8	183.2	-1200	725.0	56904

-1200	750.0	28.5	-8.7	188.0	-1200	737.5	56883
-1200	762.5	25.2	-5.8	196.1	-1200	750.0	56862
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-1200	787.5	18.4	-3.5	199.4	-1200	775.0	56879
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-1100	-562.5	10.8	3.1	149.2	-1100	-575.0	57152
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-1100	-525.0	6.4	1.8	158.3	-1100	-537.5	57119
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-1100	-500.0	1.0	-0.3	156.9	-1100	-512.5	57106
-1100	-487.5	-1.2	-0.2	150.4	-1100	-500.0	57067
-1100	-475.0	-1.9	-0.5	152.0	-1100	-487.5	56998
-1100	-462.5	-7.4	-3.1	149.7	-1100	-475.0	57078
-1100	-450.0	-8.0	-3.8	144.9	-1100	-462.5	57095
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-1100	-400.0	-1.5	-1.4	146.8	-1100	-412.5	57102
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-1100	-375.0	-2.5	-2.9	151.5	-1100	-387.5	57014
-1100	-362.5	-4.3	-4.3	146.1	-1100	-375.0	56994
-1100	-350.0	-1.5	-2.8	143.6	-1100	-362.5	56935
-1100	-337.5	-1.5	-2.9	144.3	-1100	-350.0	56974
-1100	-325.0	-0.4	-2.5	140.9	-1100	-337.5	56961
-1100	-312.5	3.0	0.2	143.6	-1100	-325.0	56914
-1100	-300.0	2.9	-1.0	145.9	-1100	-312.5	56971
-1100	-287.5	5.0	0.9	145.8	-1100	-300.0	56924
-1100	-275.0	4.6	0.2	150.1	-1100	-287.5	56921
-1100	-262.5	3.4	-0.6	147.0	-1100	-275.0	56946
-1100	-250.0	4.6	0.5	146.9	-1100	-262.5	56930
-1100	-237.5	4.8	0.2	145.8	-1100	-250.0	56947
-1100	-225.0	5.0	0.1	145.8	-1100	-237.5	56964
-1100	-212.5	5.3	0.2	145.2	-1100	-225.0	56981
-1100	-200.0	4.8	-0.1	144.2	-1100	-212.5	56961
-1100	-187.5	5.1	-0.5	139.6	-1100	-200.0	56987
-1100	-175.0	5.9	0.4	138.5	-1100	-187.5	56940
-1100	-162.5	7.5	1.4	140.5	-1100	-175.0	56941
-1100	-150.0	8.3	1.1	141.2	-1100	-162.5	56895
-1100	-137.5	9.0	3.6	145.1	-1100	-150.0	56812
-1100	-125.0	10.9	3.9	147.9	-1100	-137.5	57025
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-1100	-100.0	11.2	3.5	151.3	-1100	-112.5	57136
-1100	-87.5	11.7	2.9	152.2	-1100	-100.0	57201
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-1100	-62.5	13.2	3.6	152.8	-1100	-75.0	57115
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-1100	-12.5	14.6	4.6	154.8	-1100	-25.0	57065
-1100	0.0	14.2	4.6	156.8	-1100	-12.5	57095
-1100	12.5	14.7	4.3	165.6	-1100	0.0	57088
-1100	25.0	13.9	3.8	166.5	-1100	12.5	56980
-1100	37.5	13.4	3.6	166.5	-1100	25.0	57015
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-1100	62.5	11.8	3.0	163.4	-1100	50.0	57048
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-1100	200.0	8.9	-0.8	168.4	-1100	187.5	56982
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-1100	225.0	6.0	-3.4	166.2	-1100	212.5	56885
-1100	237.5	5.1	-4.8	163.4	-1100	225.0	56924
-1100	250.0	5.6	-4.6	160.0	-1100	237.5	56873
-1100	262.5	6.2	-5.0	154.6	-1100	250.0	56964
-1100	275.0	6.7	-3.6	150.2	-1100	262.5	56966
-1100	287.5	7.8	-2.8	145.5	-1100	275.0	56770
-1100	300.0	9.1	0.0	139.5	-1100	287.5	56742
-1100	312.5	11.6	0.7	134.5	-1100	300.0	56725
-1100	325.0	14.2	5.2	132.7	-1100	312.5	56683
-1100	337.5	16.6	9.3	135.4	-1100	325.0	56733
-1100	350.0	20.6	10.9	139.8	-1100	337.5	57003
-1100	362.5	22.6	12.0	145.1	-1100	350.0	57161
-1100	375.0	25.6	14.1	148.0	-1100	362.5	57182
-1100	387.5	27.2	13.7	154.1	-1100	375.0	57171
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-1100	425.0	22.4	7.3	155.1	-1100	412.5	57258
-1100	437.5	21.7	6.1	157.7	-1100	425.0	57385
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-1100	462.5	21.1	5.0	160.3	-1100	450.0	57516
-1100	475.0	20.7	3.7	161.1	-1100	462.5	57386
-1100	487.5	21.4	4.1	160.6	-1100	475.0	57287
-1100	500.0	22.2	4.3	162.9	-1100	487.5	57284
-1100	512.5	23.0	5.1	164.6	-1100	500.0	57212
-1100	525.0	22.5	4.6	167.5	-1100	512.5	57141
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-1100	550.0	22.7	4.1	172.1	-1100	537.5	57059
-1100	562.5	22.5	4.3	172.4	-1100	550.0	56997
-1100	575.0	22.6	4.4	175.2	-1100	562.5	57087
-1100	587.5	22.6	4.4	173.9	-1100	575.0	57123
-1100	600.0	23.2	4.2	177.7	-1100	587.5	57124
-1100	612.5	23.3	3.1	179.7	-1100	600.0	57116
-1100	625.0	22.6	2.9	182.1	-1100	612.5	57049
-1100	637.5	21.6	2.8	181.1	-1100	625.0	57080
-1100	650.0	22.6	3.2	182.4	-1100	637.5	57115
-1100	662.5	22.2	3.8	184.1	-1100	650.0	57157
-1100	675.0	23.3	4.6	185.1	-1100	662.5	57204
-1100	687.5	22.7	4.9	184.8	-1100	675.0	57196
-1100	700.0	22.7	5.3	190.6	-1100	687.5	57187
-1100	712.5	20.9	3.9	197.6	-1100	700.0	57133
-1100	725.0	20.6	3.9	196.2	-1100	712.5	57123
-1100	737.5	22.9	4.9	193.2	-1100	725.0	57147
-1100	750.0	24.9	6.4	198.7	-1100	737.5	57226

-1100	762.5	24.7	6.1	203.3
-1100	775.0	23.8	5.5	205.2
-1100	787.5	22.1	4.4	205.4
-1100	800.0	22.1	4.1	204.8
-1050	-487.5	11.9	15.3	133.6
-1050	-475.0	13.0	15.9	147.4
-1050	-462.5	8.2	9.6	148.5
-1050	-450.0	4.1	5.7	148.7
-1050	-437.5	4.6	7.9	142.8
-1050	-425.0	3.9	6.2	143.5
-1050	-412.5	5.4	9.2	144.3
-1050	-400.0	3.0	7.0	145.6
-1050	-387.5	2.0	6.0	143.6
-1050	-375.0	1.2	2.2	141.0
-1050	-362.5	1.3	3.1	136.9
-1050	-350.0	1.9	4.0	132.7
-1050	-337.5	3.4	5.9	129.1
-1050	-325.0	6.7	8.5	128.1
-1050	-312.5	8.3	9.5	133.0
-1050	-300.0	8.9	10.0	133.6
-1050	-287.5	9.8	8.4	137.4
-1050	-275.0	7.6	6.1	134.6
-1050	-262.5	10.3	7.5	132.3
-1050	-250.0	10.6	10.5	134.9
-1050	-237.5	11.3	9.7	134.1
-1050	-225.0	10.8	10.8	134.7
-1050	-212.5	10.6	8.5	135.7
-1050	-200.0	10.4	10.9	134.2
-1050	-187.5	11.1	11.1	138.2
-1050	-175.0	9.9	12.9	141.9
-1050	-162.5	11.8	11.3	144.5
-1050	-150.0	13.5	12.4	146.1
-1050	-137.5	14.0	10.8	155.2
-1050	-125.0	14.4	11.0	158.3
-1050	-112.5	15.0	10.7	158.6
-1050	-100.0	15.8	10.8	159.0
-1050	-87.5	17.3	13.0	156.5
-1050	-75.0	18.6	14.5	157.8
-1050	-62.5	19.3	13.2	156.9
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-1050	-37.5	17.2	11.9	153.1
-1050	-25.0	18.9	11.9	148.8
-1050	-12.5	18.0	12.2	147.6
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-1050	12.5	18.1	12.6	148.4
-1050	25.0	18.3	11.9	148.3
-1050	37.5	16.3	11.4	151.1
-1050	50.0	16.4	11.6	149.8
-1050	62.5	15.4	11.4	149.6
-1050	75.0	16.2	10.2	152.5
-1050	87.5	16.4	11.9	153.5
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-1050	112.5	15.5	8.5	157.1
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-1050	150.0	14.7	5.6	162.0

-1100	750.0	57220
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-1100	775.0	57172
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-1100	800.0	57141
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-1050	-475.0	57110
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-1050	50.0	57046
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-1000	-712.5	1.8	10.3	136.2	-1000	-725.0	57125
-1000	-700.0	-1.0	8.6	136.3	-1000	-712.5	57146
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-1000	-675.0	-1.3	6.7	133.4	-1000	-687.5	57189
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-1000	-500.0	-1.7	2.1	162.8	-1000	-512.5	57035
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-1000	-475.0	2.3	5.7	136.6	-1000	-487.5	56943
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-1000	-250.0	7.1	5.5	154.2	-1000	-262.5	57014
-1000	-237.5	7.0	5.4	154.7	-1000	-250.0	57010
-1000	-225.0	7.9	6.1	154.0	-1000	-237.5	57035
-1000	-212.5	8.7	6.4	153.0	-1000	-225.0	57004
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-1000	25.0	8.9	5.3	157.9	-1000	12.5	57033
-1000	37.5	9.8	5.8	158.4	-1000	25.0	57161
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-1000	62.5	10.2	5.9	161.4	-1000	50.0	57139
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-1000	100.0	10.7	5.5	163.0	-1000	87.5	57293
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-1000	275.0	6.3	-0.2	139.3	-1000	262.5	56620
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-1000	775.0	16.6	1.8	184.9	-1000	762.5	57015
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-950	50.0	11.3	7.7	176.4	-950	37.5	57007
-950	62.5	11.7	7.1	170.8	-950	50.0	57060
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-950	137.5	10.5	7.0	165.8	-950	125.0	56973
-950	150.0	11.6	8.0	167.0	-950	137.5	56915
-900	-800.0	0.7	8.2	134.3	-950	150.0	57012
-900	-787.5	1.3	8.6	132.9	-900	-800.0	57155
-900	-775.0	2.5	8.7	134.8	-900	-787.5	57167
-900	-762.5	2.8	8.8	134.7	-900	-775.0	57179
-900	-750.0	3.1	8.8	134.8	-900	-762.5	57135
-900	-737.5	3.1	8.4	134.7	-900	-750.0	56982
-900	-725.0	2.1	7.4	133.2	-900	-737.5	57026
-900	-712.5	3.0	7.5	132.6	-900	-725.0	57044
-900	-700.0	3.4	7.9	132.2	-900	-712.5	56997
-900	-687.5	3.7	7.1	135.2	-900	-700.0	57067
-900	-675.0	3.7	7.3	135.9	-900	-687.5	57076
-900	-662.5	1.6	6.2	133.9	-900	-675.0	57062
-900	-650.0	1.5	5.5	132.9	-900	-662.5	57084
-900	-637.5	1.3	5.8	131.3	-900	-650.0	57100
-900	-625.0	2.0	5.2	132.5	-900	-637.5	57147
-900	-612.5	1.4	4.5	129.2	-900	-625.0	57087
-900	-600.0	3.1	5.8	128.1	-900	-612.5	57045
-900	-587.5	3.3	5.6	127.2	-900	-600.0	56991
-900	-575.0	4.0	6.2	127.6	-900	-587.5	57021
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-900	-550.0	3.2	5.2	127.7	-900	-562.5	56988
-900	-537.5	4.2	5.9	124.4	-900	-550.0	56937
-900	-525.0	6.7	7.2	128.3	-900	-537.5	56918
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-900	-500.0	6.9	7.0	130.0	-900	-512.5	56973
-900	-487.5	6.2	6.4	128.8	-900	-500.0	56986
-900	-475.0	6.0	5.9	126.6	-900	-487.5	56988
-900	-462.5	5.8	5.2	126.4	-900	-475.0	56915
-900	-450.0	5.9	5.7	124.2	-900	-462.5	56965
-900	-437.5	7.2	6.3	124.6	-900	-450.0	57001
-900	-425.0	7.7	6.7	124.3	-900	-437.5	56998
-900	-412.5	8.8	7.0	123.6	-900	-425.0	57036
-900	-400.0	8.2	6.9	125.6	-900	-412.5	56984
-900	-387.5	7.5	7.2	123.4	-900	-400.0	56919
-900	-375.0	7.1	7.5	122.9	-900	-387.5	56930
-900	-362.5	7.9	6.6	126.2	-900	-375.0	56941
-900	-350.0	7.1	6.4	126.0	-900	-362.5	56905
-900	-337.5	7.3	6.5	125.6	-900	-350.0	56958
-900	-325.0	7.4	5.7	127.8	-900	-337.5	57001
-900	-312.5	8.1	5.5	127.8	-900	-325.0	56969
-900	-300.0	7.8	5.5	126.3	-900	-312.5	56927
-900	-287.5	8.2	5.7	126.0	-900	-300.0	56948

-900	-275.0	9.5	6.2	126.5	-900	-287.5	57029
-900	-262.5	10.9	7.5	130.6	-900	-275.0	57068
-900	-250.0	10.7	6.9	132.1	-900	-262.5	57008
-900	-237.5	10.8	7.1	133.4	-900	-250.0	56929
-900	-225.0	11.1	7.3	135.8	-900	-237.5	56898
-900	-212.5	11.3	7.1	141.9	-900	-225.0	57015
-900	-200.0	11.1	6.6	141.7	-900	-212.5	56958
-900	-187.5	10.4	6.1	143.2	-900	-200.0	56995
-900	-175.0	9.4	5.4	142.9	-900	-187.5	57004
-900	-162.5	9.3	5.4	142.9	-900	-175.0	57068
-900	-150.0	9.7	5.3	142.4	-900	-162.5	57050
-900	-137.5	8.5	4.5	141.3	-900	-150.0	57002
-900	-125.0	7.7	3.9	142.1	-900	-137.5	57023
-900	-112.5	6.9	3.5	141.5	-900	-125.0	57035
-900	-100.0	6.2	3.0	139.5	-900	-112.5	57041
-900	-87.5	7.0	3.5	135.9	-900	-100.0	57075
-900	-75.0	9.9	5.1	140.4	-900	-87.5	57061
-900	-62.5	5.1	2.7	140.6	-900	-75.0	57046
-900	-50.0	5.6	2.8	139.2	-900	-62.5	57102
-900	-37.5	3.9	1.9	136.5	-900	-50.0	57052
-900	-25.0	4.3	2.1	133.1	-900	-37.5	57059
-900	-12.5	6.1	3.7	130.4	-900	-25.0	57012
-900	0.0	7.7	5.1	131.8	-900	-12.5	57167
-900	12.5	7.7	4.7	136.6	-900	0.0	57160
-900	25.0	6.6	3.6	136.8	-900	12.5	57153
-900	37.5	7.5	4.4	135.4	-900	25.0	57092
-900	50.0	6.7	4.6	140.0	-900	37.5	57013
-900	62.5	5.8	4.1	138.1	-900	50.0	56937
-900	75.0	4.9	3.5	137.4	-900	62.5	57071
-900	87.5	3.7	3.4	134.5	-900	75.0	56972
-900	100.0	3.1	2.9	135.1	-900	87.5	57169
-900	112.5	3.1	3.3	133.3	-900	100.0	57140
-900	125.0	1.5	1.8	130.7	-900	112.5	57062
-900	137.5	1.2	2.4	126.9	-900	125.0	57032
-900	150.0	3.3	3.6	125.1	-900	137.5	56976
-900	162.5	2.8	2.8	127.1	-900	150.0	56930
-900	175.0	1.6	1.9	126.3	-900	162.5	56943
-900	187.5	1.6	2.7	125.7	-900	175.0	56977
-900	200.0	2.1	2.3	125.7	-900	187.5	57036
-900	212.5	1.0	1.9	127.6	-900	200.0	57088
-900	225.0	0.6	0.5	127.1	-900	212.5	57059
-900	237.5	-1.8	-1.4	128.0	-900	225.0	57068
-900	250.0	-6.4	-5.2	123.7	-900	237.5	57072
-900	262.5	-5.2	-5.4	116.6	-900	250.0	56878
-900	275.0	-3.1	-3.9	114.4	-900	262.5	56801
-900	287.5	-1.3	-2.9	113.1	-900	275.0	56782
-900	300.0	0.9	0.0	117.2	-900	287.5	56696
-900	312.5	2.3	2.5	114.9	-900	300.0	56655
-900	325.0	5.3	5.0	116.8	-900	312.5	56908
-900	337.5	7.2	6.7	123.4	-900	325.0	57190
-900	350.0	9.5	6.3	127.7	-900	337.5	57353
-900	362.5	5.8	3.6	128.4	-900	350.0	57391
-900	375.0	4.4	2.3	127.2	-900	362.5	57236
-900	387.5	5.3	3.0	127.6	-900	375.0	57151
-900	400.0	3.6	2.3	128.1	-900	387.5	57105
-900	412.5	2.1	0.9	126.2	-900	400.0	57121

-900	425.0	2.0	1.3	123.0	-900	412.5	57081
-900	437.5	2.5	1.3	121.9	-900	425.0	57097
-900	450.0	5.6	2.6	122.0	-900	437.5	57094
-900	462.5	3.4	2.4	120.5	-900	450.0	57048
-900	475.0	5.2	3.2	119.8	-900	462.5	57080
-900	487.5	5.3	3.2	118.8	-900	475.0	57050
-900	500.0	4.6	3.1	117.6	-900	487.5	56970
-900	512.5	3.1	2.6	116.5	-900	500.0	56945
-900	525.0	3.9	2.9	118.3	-900	512.5	56947
-900	537.5	3.6	2.6	115.8	-900	525.0	56962
-900	550.0	0.2	1.9	108.2	-900	537.5	57006
-900	562.5	0.6	1.7	106.5	-900	550.0	56979
-900	575.0	1.9	2.0	105.8	-900	562.5	57019
-900	587.5	1.8	2.0	106.2	-900	575.0	57021
-900	600.0	2.1	2.9	104.2	-900	587.5	56983
-900	612.5	3.3	3.2	105.0	-900	600.0	57006
-900	625.0	4.5	4.5	105.6	-900	612.5	57047
-900	637.5	4.5	4.7	104.3	-900	625.0	57029
-900	650.0	5.6	5.2	103.9	-900	637.5	57048
-900	662.5	6.1	5.4	103.9	-900	650.0	57085
-900	675.0	6.6	5.9	103.7	-900	662.5	57055
-900	687.5	7.7	6.2	103.5	-900	675.0	57088
-900	700.0	9.4	7.2	105.5	-900	687.5	57139
-900	712.5	9.5	7.3	105.0	-900	700.0	57107
-900	725.0	9.1	5.7	106.8	-900	712.5	57101
-900	737.5	9.2	6.5	105.9	-900	725.0	57036
-900	750.0	8.1	5.6	104.7	-900	737.5	57105
-900	762.5	7.9	6.5	104.2	-900	750.0	57033
-900	775.0	8.4	7.1	104.2	-900	762.5	57128
-900	787.5	8.3	7.2	103.3	-900	775.0	57038
-900	800.0	8.7	8.3	103.5	-900	787.5	57035
-850	-500.0	13.1	8.5	160.9	-900	800.0	57043
-850	-487.5	12.2	8.8	165.2	-850	-500.0	57060
-850	-475.0	12.1	7.8	165.4	-850	-487.5	56991
-850	-462.5	12.2	7.5	165.4	-850	-475.0	57025
-850	-450.0	12.2	7.9	166.1	-850	-462.5	56874
-850	-437.5	13.5	8.0	167.5	-850	-450.0	56978
-850	-425.0	14.6	9.1	168.2	-850	-437.5	56989
-850	-412.5	14.4	8.9	170.1	-850	-425.0	56968
-850	-400.0	14.6	8.7	171.8	-850	-412.5	56954
-850	-387.5	15.5	8.5	167.4	-850	-400.0	56890
-850	-375.0	16.0	10.4	165.4	-850	-387.5	56935
-850	-362.5	18.7	11.2	163.9	-850	-375.0	57135
-850	-350.0	18.6	12.0	167.3	-850	-362.5	57144
-850	-337.5	19.1	11.3	166.5	-850	-350.0	57081
-850	-325.0	19.6	12.0	168.0	-850	-337.5	57049
-850	-312.5	19.5	11.5	168.7	-850	-325.0	57055
-850	-300.0	18.2	9.4	166.9	-850	-312.5	56996
-850	-287.5	18.0	9.6	166.1	-850	-300.0	57021
-850	-275.0	18.7	10.2	161.2	-850	-287.5	57035
-850	-262.5	19.3	10.9	164.1	-850	-275.0	57081
-850	-250.0	18.8	11.6	164.4	-850	-262.5	57067
-850	-237.5	18.7	11.6	164.2	-850	-250.0	56916
-850	-225.0	19.0	11.2	165.3	-850	-237.5	57087
-850	-212.5	17.5	10.4	164.5	-850	-225.0	57122
-850	-200.0	17.2	10.8	164.1	-850	-212.5	57075

-850	-187.5	16.3	9.9	163.7	-850	-200.0	57092
-850	-175.0	16.2	10.1	161.9	-850	-187.5	57059
-850	-162.5	16.1	11.5	162.7	-850	-175.0	57122
-850	-150.0	15.9	10.9	163.6	-850	-162.5	57107
-850	-137.5	16.3	10.0	165.0	-850	-150.0	57088
-850	-125.0	15.2	9.3	166.5	-850	-137.5	57108
-850	-112.5	14.8	8.6	164.6	-850	-125.0	57083
-850	-100.0	12.6	6.0	166.2	-850	-112.5	57094
-850	-87.5	12.2	6.7	163.7	-850	-100.0	57053
-850	-75.0	14.1	7.5	159.1	-850	-87.5	57015
-850	-62.5	14.9	9.1	167.0	-850	-75.0	56997
-850	-50.0	11.7	5.0	168.6	-850	-62.5	57008
-850	-37.5	9.5	4.2	162.7	-850	-50.0	57029
-850	-25.0	10.3	5.4	158.3	-850	-37.5	56955
-850	-12.5	12.8	8.3	160.8	-850	-25.0	56927
-850	0.0	12.8	8.6	163.8	-850	-12.5	57038
-850	12.5	11.8	7.8	168.2	-850	0.0	57059
-850	25.0	10.8	6.0	165.5	-850	12.5	57100
-850	37.5	12.0	7.2	164.2	-850	25.0	56978
-850	50.0	12.6	7.2	165.2	-850	37.5	57011
-850	62.5	12.0	6.7	167.9	-850	50.0	57040
-850	75.0	12.0	6.3	168.1	-850	62.5	57066
-850	87.5	12.5	7.1	168.7	-850	75.0	56996
-850	100.0	11.4	7.3	169.5	-850	87.5	57006
-850	112.5	11.2	8.3	171.2	-850	100.0	57072
-850	125.0	11.0	6.9	169.3	-850	112.5	56993
-850	137.5	12.2	6.6	168.2	-850	125.0	57021
-850	150.0	11.7	7.6	169.7	-850	137.5	57018
-800	-800.0	0.0	3.2	155.5	-850	150.0	57017
-800	-787.5	-0.7	3.1	152.3	-800	-800.0	56939
-800	-775.0	-0.7	3.2	150.0	-800	-787.5	56987
-800	-762.5	0.2	3.5	148.7	-800	-775.0	57054
-800	-750.0	1.4	4.2	149.8	-800	-762.5	57058
-800	-737.5	0.6	3.6	150.3	-800	-750.0	57041
-800	-725.0	2.3	4.5	150.3	-800	-737.5	57024
-800	-712.5	1.8	3.4	153.9	-800	-725.0	57126
-800	-700.0	1.6	3.4	149.9	-800	-712.5	57029
-800	-687.5	2.6	3.6	149.4	-800	-700.0	57020
-800	-675.0	2.7	3.7	149.2	-800	-687.5	57039
-800	-662.5	2.4	3.1	148.3	-800	-675.0	57068
-800	-650.0	4.6	4.2	147.3	-800	-662.5	57030
-800	-637.5	5.2	4.5	148.2	-800	-650.0	57029
-800	-625.0	4.9	3.8	149.0	-800	-637.5	57081
-800	-612.5	5.9	4.2	147.4	-800	-625.0	57053
-800	-600.0	7.2	4.8	147.6	-800	-612.5	57062
-800	-587.5	9.9	7.5	146.2	-800	-600.0	57003
-800	-575.0	9.8	6.3	151.8	-800	-587.5	56964
-800	-562.5	7.4	4.1	153.1	-800	-575.0	57045
-800	-550.0	7.1	4.4	151.0	-800	-562.5	56961
-800	-537.5	7.0	3.7	150.6	-800	-550.0	56914
-800	-525.0	6.3	3.3	151.1	-800	-537.5	56916
-800	-512.5	6.2	2.7	151.7	-800	-525.0	56976
-800	-500.0	5.6	2.7	147.9	-800	-512.5	56987
-800	-487.5	7.3	3.9	146.7	-800	-500.0	56949
-800	-475.0	7.3	3.6	146.8	-800	-487.5	56913
-800	-462.5	6.6	3.9	146.5	-800	-475.0	56906

-800	-450.0	7.6	3.9	144.4	-800	-462.5	56838
-800	-437.5	7.4	4.0	143.7	-800	-450.0	56883
-800	-425.0	7.9	4.3	142.8	-800	-437.5	56928
-800	-412.5	8.1	5.1	145.0	-800	-425.0	56936
-800	-400.0	9.0	4.9	145.3	-800	-412.5	57087
-800	-387.5	9.3	5.2	144.8	-800	-400.0	57035
-800	-375.0	9.7	5.5	146.0	-800	-387.5	57005
-800	-362.5	10.4	5.7	145.3	-800	-375.0	57023
-800	-350.0	11.1	6.2	143.9	-800	-362.5	57020
-800	-337.5	12.3	6.5	145.5	-800	-350.0	56950
-800	-325.0	11.7	6.4	146.9	-800	-337.5	56898
-800	-312.5	11.6	6.5	147.7	-800	-325.0	56895
-800	-300.0	12.8	6.8	150.7	-800	-312.5	56989
-800	-287.5	12.0	6.9	152.2	-800	-300.0	56909
-800	-275.0	12.4	7.1	152.5	-800	-287.5	57146
-800	-262.5	12.8	7.8	154.2	-800	-275.0	57217
-800	-250.0	13.2	7.9	154.1	-800	-262.5	57220
-800	-237.5	13.6	8.4	153.5	-800	-250.0	57159
-800	-225.0	13.2	8.2	156.2	-800	-237.5	57189
-800	-212.5	13.1	8.2	158.1	-800	-225.0	57175
-800	-200.0	12.3	7.4	158.9	-800	-212.5	57117
-800	-187.5	11.9	7.1	159.9	-800	-200.0	57130
-800	-175.0	11.2	6.9	159.3	-800	-187.5	57054
-800	-162.5	10.3	6.3	157.0	-800	-175.0	57075
-800	-150.0	10.2	7.4	156.1	-800	-162.5	57088
-800	-137.5	10.9	7.7	155.5	-800	-150.0	57097
-800	-125.0	10.6	7.5	157.2	-800	-137.5	57116
-800	-112.5	7.0	5.6	157.7	-800	-125.0	57100
-800	-100.0	5.6	4.2	156.0	-800	-112.5	57060
-800	-87.5	6.5	5.1	152.3	-800	-100.0	57080
-800	-75.0	5.6	4.0	151.4	-800	-87.5	57132
-800	-62.5	8.5	6.5	147.6	-800	-75.0	57052
-800	-50.0	8.1	5.9	153.7	-800	-62.5	57060
-800	-37.5	5.8	4.8	146.0	-800	-50.0	57070
-800	-25.0	9.0	6.5	144.4	-800	-37.5	56940
-800	-12.5	11.6	7.4	147.5	-800	-25.0	56974
-800	0.0	11.2	6.2	151.8	-800	-12.5	57019
-800	12.5	7.2	3.5	153.3	-800	0.0	57007
-800	25.0	8.1	3.8	147.0	-800	12.5	56909
-800	37.5	9.2	5.0	151.6	-800	25.0	56847
-800	50.0	8.0	3.9	154.9	-800	37.5	56994
-800	62.5	7.0	2.5	155.2	-800	50.0	56959
-800	75.0	6.9	3.0	152.6	-800	62.5	56921
-800	87.5	8.2	3.3	154.2	-800	75.0	56962
-800	100.0	7.0	2.5	154.1	-800	87.5	56951
-800	112.5	6.4	2.4	154.4	-800	100.0	56944
-800	125.0	6.8	2.8	153.6	-800	112.5	56915
-800	137.5	6.5	2.4	152.9	-800	125.0	56863
-800	150.0	7.1	1.8	153.3	-800	137.5	56936
-800	162.5	6.3	1.8	154.7	-800	150.0	56905
-800	175.0	6.5	2.5	151.1	-800	162.5	56904
-800	187.5	6.5	2.6	153.8	-800	175.0	56846
-800	200.0	6.4	2.1	153.5	-800	187.5	56955
-800	212.5	6.3	2.1	153.5	-800	200.0	56913
-800	225.0	6.7	2.6	153.2	-800	212.5	56918
-800	237.5	6.7	2.7	152.4	-800	225.0	56947

-800	250.0	6.7	2.6	152.5	-800	237.5	56960
-800	262.5	6.8	2.0	151.2	-800	250.0	57011
-800	275.0	6.3	1.4	150.7	-800	262.5	57029
-800	287.5	3.2	-1.2	149.4	-800	275.0	57033
-800	300.0	3.3	-1.1	143.9	-800	287.5	56935
-800	312.5	5.2	1.0	140.3	-800	300.0	56676
-800	325.0	4.9	1.9	140.5	-800	312.5	56585
-800	337.5	6.3	3.7	141.0	-800	325.0	56838
-800	350.0	6.7	4.0	141.5	-800	337.5	57035
-800	362.5	6.8	3.2	144.3	-800	350.0	56984
-800	375.0	6.1	2.7	142.6	-800	362.5	56977
-800	387.5	5.2	2.7	142.6	-800	375.0	56970
-800	400.0	6.3	3.2	143.2	-800	387.5	56959
-800	412.5	6.5	3.4	146.1	-800	400.0	57005
-800	425.0	6.1	3.1	144.4	-800	412.5	56997
-800	437.5	4.8	2.1	144.3	-800	425.0	56874
-800	450.0	4.4	2.1	141.9	-800	437.5	56865
-800	462.5	4.3	2.7	141.7	-800	450.0	56802
-800	475.0	2.5	1.2	139.6	-800	462.5	56835
-800	487.5	2.5	1.7	138.7	-800	475.0	56841
-800	500.0	3.8	2.3	145.5	-800	487.5	56956
-800	512.5	3.7	1.7	144.4	-800	500.0	56926
-800	525.0	2.3	0.7	142.7	-800	512.5	56920
-800	537.5	3.4	2.2	138.7	-800	525.0	56925
-800	550.0	5.8	3.4	139.2	-800	537.5	56938
-800	562.5	5.3	2.7	141.2	-800	550.0	56928
-800	575.0	4.0	2.0	137.2	-800	562.5	56981
-800	587.5	6.3	3.3	139.2	-800	575.0	56897
-800	600.0	7.9	3.4	139.1	-800	587.5	56841
-800	612.5	7.3	2.8	140.5	-800	600.0	56805
-800	625.0	7.6	3.1	138.4	-800	612.5	56875
-800	637.5	9.1	3.7	137.9	-800	625.0	57026
-800	650.0	11.0	4.5	138.2	-800	637.5	56976
-800	662.5	12.3	5.1	137.3	-800	650.0	56865
-800	675.0	13.4	5.4	137.5	-800	662.5	56808
-800	687.5	14.0	5.0	138.0	-800	675.0	56812
-800	700.0	15.1	5.1	137.8	-800	687.5	56844
-800	712.5	16.4	6.3	142.0	-800	700.0	56848
-800	725.0	17.0	6.3	143.4	-800	712.5	56835
-800	737.5	18.3	6.5	144.9	-800	725.0	56856
-800	750.0	18.7	6.6	148.7	-800	737.5	56869
-800	762.5	18.5	6.3	150.8	-800	750.0	56863
-800	775.0	19.1	6.3	150.8	-800	762.5	56934
-800	787.5	18.7	5.6	158.5	-800	775.0	56937
-800	800.0	16.9	4.6	157.7	-800	787.5	56902
-750	-500.0	-0.4	15.4	61.3	-800	800.0	56918
-750	-487.5	-0.9	16.2	62.5	-750	-500.0	56980
-750	-475.0	-1.5	15.5	64.3	-750	-487.5	57088
-750	-462.5	-2.5	14.1	65.7	-750	-475.0	57052
-750	-450.0	-2.4	14.1	67.3	-750	-462.5	57077
-750	-437.5	-3.3	12.8	68.1	-750	-450.0	57049
-750	-425.0	-0.8	13.0	68.8	-750	-437.5	57045
-750	-412.5	0.3	12.3	69.1	-750	-425.0	57034
-750	-400.0	1.5	14.0	69.6	-750	-412.5	57056
-750	-387.5	2.6	12.8	71.0	-750	-400.0	57037
-750	-375.0	0.0	11.3	71.5	-750	-387.5	56901

-750	-362.5	2.6	13.9	73.2	-750	-375.0	57018
-750	-350.0	2.6	13.9	73.9	-750	-362.5	57178
-750	-337.5	2.1	13.0	74.3	-750	-350.0	57162
-750	-325.0	2.8	13.6	75.6	-750	-337.5	57120
-750	-312.5	2.1	11.2	77.0	-750	-325.0	57141
-750	-300.0	2.7	11.3	77.0	-750	-312.5	57139
-750	-287.5	1.8	13.1	78.4	-750	-300.0	57016
-750	-275.0	1.1	10.8	77.2	-750	-287.5	57101
-750	-262.5	0.9	11.1	77.0	-750	-275.0	57074
-750	-250.0	2.2	10.5	77.0	-750	-262.5	57085
-750	-237.5	2.3	12.8	77.2	-750	-250.0	57101
-750	-225.0	2.2	11.3	78.7	-750	-237.5	57083
-750	-212.5	1.3	11.5	80.7	-750	-225.0	57061
-750	-200.0	-3.5	10.5	81.5	-750	-212.5	56999
-750	-187.5	-4.5	8.9	79.6	-750	-200.0	57054
-750	-175.0	-4.0	10.3	80.4	-750	-187.5	57032
-750	-162.5	-6.8	10.2	79.5	-750	-175.0	57037
-750	-150.0	-7.9	10.2	78.8	-750	-162.5	56992
-750	-137.5	-6.3	11.9	78.9	-750	-150.0	57077
-750	-125.0	-7.6	12.5	79.4	-750	-137.5	57041
-750	-112.5	-6.7	13.4	79.7	-750	-125.0	57037
-750	-100.0	-8.1	12.5	80.1	-750	-112.5	57072
-750	-87.5	-8.4	10.1	80.1	-750	-100.0	57023
-750	-75.0	-8.0	10.0	79.2	-750	-87.5	56987
-750	-62.5	-4.6	12.0	80.5	-750	-75.0	56996
-750	-50.0	-6.1	9.2	82.5	-750	-62.5	56994
-750	-37.5	-7.5	9.2	83.8	-750	-50.0	56997
-750	-25.0	-7.5	11.0	84.1	-750	-37.5	56953
-750	-12.5	-9.0	8.9	85.6	-750	-25.0	57081
-750	0.0	2.3	-5.0	101.0	-750	-12.5	57027
-750	12.5	2.4	-4.8	93.9	-750	0.0	57017
-750	25.0	-1.3	-7.4	95.2	-750	12.5	56949
-750	37.5	1.8	-5.1	96.0	-750	25.0	57071
-750	50.0	2.5	-6.8	88.3	-750	37.5	57035
-750	62.5	-0.2	-8.1	87.5	-750	50.0	57009
-750	75.0	-2.6	-8.0	89.2	-750	62.5	56937
-750	87.5	-3.3	-7.8	90.7	-750	75.0	56975
-750	100.0	-5.0	-7.9	90.5	-750	87.5	56839
-750	112.5	-5.6	-6.3	92.1	-750	100.0	56926
-750	125.0	-7.6	-8.0	93.4	-750	112.5	56880
-750	137.5	-7.1	-7.1	95.2	-750	125.0	56884
-750	150.0	-5.0	-7.1	95.6	-750	137.5	56996
-700	-800.0	3.3	5.4	152.1	-750	150.0	56961
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-700	-775.0	4.4	5.2	151.5	-700	-787.5	57051
-700	-762.5	5.2	5.0	155.5	-700	-775.0	57035
-700	-750.0	3.9	4.8	153.4	-700	-762.5	57065
-700	-737.5	4.4	3.9	158.3	-700	-750.0	57006
-700	-725.0	4.0	3.1	158.3	-700	-737.5	56977
-700	-712.5	3.8	3.0	158.6	-700	-725.0	56976
-700	-700.0	3.9	3.8	159.0	-700	-712.5	56979
-700	-687.5	3.2	3.5	161.1	-700	-700.0	56983
-700	-675.0	1.7	2.6	158.8	-700	-687.5	56985
-700	-662.5	1.1	2.3	157.9	-700	-675.0	56936
-700	-650.0	-0.7	1.9	157.4	-700	-662.5	56931
-700	-637.5	-1.9	1.4	157.1	-700	-650.0	56935

-700	-625.0	-3.5	0.5	159.1	-700	-637.5	56959
-700	-612.5	-3.5	-0.2	154.1	-700	-625.0	56976
-700	-600.0	-3.6	-0.7	152.4	-700	-612.5	56964
-700	-587.5	-4.0	-0.7	151.4	-700	-600.0	56924
-700	-575.0	-4.0	-1.0	150.6	-700	-587.5	56928
-700	-562.5	-3.2	-0.3	149.5	-700	-575.0	56785
-700	-550.0	-2.2	-0.1	147.3	-700	-562.5	56748
-700	-537.5	-2.7	-0.1	147.2	-700	-550.0	56901
-700	-525.0	-1.5	0.0	148.0	-700	-537.5	56892
-700	-512.5	-0.1	0.5	147.5	-700	-525.0	56904
-700	-500.0	0.5	0.8	146.6	-700	-512.5	57015
-700	-487.5	1.6	1.1	147.4	-700	-500.0	57087
-700	-475.0	1.8	1.1	147.1	-700	-487.5	57034
-700	-462.5	2.8	1.3	146.1	-700	-475.0	57010
-700	-450.0	2.6	1.5	148.7	-700	-462.5	57018
-700	-437.5	3.5	1.6	149.7	-700	-450.0	57020
-700	-425.0	3.3	1.6	148.1	-700	-437.5	57000
-700	-412.5	4.3	1.6	148.2	-700	-425.0	56994
-700	-400.0	5.0	2.9	150.3	-700	-412.5	56981
-700	-387.5	6.8	3.8	151.4	-700	-400.0	57070
-700	-375.0	6.9	3.6	155.5	-700	-387.5	57086
-700	-362.5	6.6	3.2	153.5	-700	-375.0	57054
-700	-350.0	6.3	3.1	154.2	-700	-362.5	57038
-700	-337.5	6.1	2.6	155.3	-700	-350.0	57025
-700	-325.0	6.2	2.6	152.3	-700	-337.5	56990
-700	-312.5	9.5	5.2	154.2	-700	-325.0	56917
-700	-300.0	8.7	4.2	157.9	-700	-312.5	57081
-700	-287.5	7.0	3.3	160.5	-700	-300.0	57074
-700	-275.0	6.5	2.8	160.1	-700	-287.5	57069
-700	-262.5	5.3	2.4	158.5	-700	-275.0	57054
-700	-250.0	4.6	2.1	160.0	-700	-262.5	57014
-700	-237.5	3.4	1.8	160.1	-700	-250.0	57013
-700	-225.0	2.8	1.7	160.4	-700	-237.5	57032
-700	-212.5	1.4	1.2	160.2	-700	-225.0	57018
-700	-200.0	0.0	0.9	160.0	-700	-212.5	57016
-700	-187.5	-0.9	1.0	160.6	-700	-200.0	57031
-700	-175.0	-1.9	0.5	157.6	-700	-187.5	57028
-700	-162.5	-2.1	0.5	156.9	-700	-175.0	57047
-700	-150.0	-2.8	0.4	155.5	-700	-162.5	57065
-700	-137.5	-3.2	0.8	154.5	-700	-150.0	57047
-700	-125.0	-2.9	0.7	155.1	-700	-137.5	57025
-700	-112.5	-3.7	0.4	153.1	-700	-125.0	56998
-700	-100.0	-3.4	0.2	154.3	-700	-112.5	57026
-700	-87.5	-3.6	0.8	152.0	-700	-100.0	56996
-700	-75.0	-3.1	1.2	149.4	-700	-87.5	57005
-700	-62.5	-1.9	1.5	151.5	-700	-75.0	57059
-700	-50.0	-1.1	1.5	152.5	-700	-62.5	57068
-700	-37.5	-2.9	0.7	151.5	-700	-50.0	57080
-700	-25.0	-3.1	0.6	151.1	-700	-37.5	57062
-700	-12.5	-2.6	0.1	148.4	-700	-25.0	56993
-700	0.0	-5.4	2.0	106.3	-700	-12.5	57013
-700	12.5	-4.5	2.1	105.2	-700	0.0	57015
-700	25.0	-3.5	2.1	104.5	-700	12.5	57066
-700	37.5	-1.6	2.3	106.4	-700	25.0	57053
-700	50.0	-2.5	1.5	105.7	-700	37.5	57082
-700	62.5	-1.2	1.8	104.3	-700	50.0	57065

-700	75.0	-0.3	1.3	106.9
-700	87.5	-0.9	0.7	106.6
-700	100.0	1.6	1.5	107.5
-700	112.5	2.4	1.1	108.7
-700	125.0	4.8	1.6	110.7
-700	137.5	5.7	1.5	113.4
-700	150.0	7.4	1.9	116.4
-700	162.5	11.5	3.5	118.8
-700	175.0	10.2	2.2	126.7
-700	187.5	6.9	0.8	125.3
-700	200.0	5.7	0.2	126.1
-700	212.5	5.0	0.6	125.1
-700	225.0	5.0	0.8	124.2
-700	237.5	5.1	1.2	125.8
-700	250.0	3.9	1.3	129.0
-700	262.5	2.6	0.9	130.2
-700	275.0	1.2	0.6	130.1
-700	287.5	0.0	0.3	132.2
-700	300.0	-0.5	0.5	127.7
-700	312.5	0.5	2.0	128.6
-700	325.0	1.4	2.2	132.7
-700	337.5	-0.6	1.0	136.7
-700	350.0	-3.1	-0.1	133.7
-700	362.5	-5.1	-1.1	133.4
-700	375.0	-6.0	-1.8	130.6
-700	387.5	-6.7	-1.9	129.5
-700	400.0	-5.2	-1.0	128.9
-700	412.5	-4.9	-0.1	130.1
-700	425.0	-4.9	0.2	129.6
-700	437.5	-2.2	1.8	129.5
-700	450.0	1.1	4.0	132.6
-700	462.5	0.0	3.5	134.1
-700	475.0	-0.4	3.2	135.1
-700	487.5	-1.5	2.7	133.9
-700	500.0	-1.6	2.6	133.3
-700	512.5	-0.3	3.9	133.4
-700	525.0	-0.8	3.6	135.3
-700	537.5	-0.4	4.0	134.7
-700	550.0	-1.3	3.2	138.2
-700	562.5	-3.3	2.1	137.0
-700	575.0	-3.4	1.3	136.0
-700	587.5	-3.4	1.9	135.3
-700	600.0	-3.3	1.3	135.3
-700	612.5	-3.2	1.0	133.7
-700	625.0	-2.1	1.5	133.2
-700	637.5	-1.3	1.7	132.2
-700	650.0	-0.2	2.0	133.8
-700	662.5	0.9	1.9	131.4
-700	675.0	2.2	3.0	130.7
-700	687.5	4.3	3.6	132.3
-700	700.0	5.9	4.4	132.1
-700	712.5	7.8	4.4	135.1
-700	725.0	8.9	4.2	136.4
-700	737.5	9.0	4.2	137.4
-700	750.0	10.1	4.2	139.2
-700	762.5	11.6	4.3	142.8

-700	62.5	57057
-700	75.0	57063
-700	87.5	57072
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-700	112.5	57063
-700	125.0	57071
-700	137.5	57105
-700	150.0	57079
-700	162.5	56983
-700	175.0	56942
-700	187.5	56950
-700	200.0	56924
-700	212.5	56936
-700	225.0	56966
-700	237.5	56969
-700	250.0	56949
-700	262.5	56911
-700	275.0	56890
-700	287.5	56891
-700	300.0	56983
-700	312.5	56998
-700	325.0	57014
-700	337.5	57034
-700	350.0	57032
-700	362.5	57008
-700	375.0	56980
-700	387.5	56923
-700	400.0	56832
-700	412.5	56921
-700	425.0	56939
-700	437.5	56953
-700	450.0	56897
-700	462.5	56898
-700	475.0	56910
-700	487.5	56865
-700	500.0	56891
-700	512.5	56883
-700	525.0	56992
-700	537.5	56937
-700	550.0	56926
-700	562.5	56920
-700	575.0	56847
-700	587.5	56856
-700	600.0	56861
-700	612.5	56857
-700	625.0	56870
-700	637.5	56886
-700	650.0	56909
-700	662.5	56898
-700	675.0	56926
-700	687.5	56908
-700	700.0	56944
-700	712.5	56953
-700	725.0	56883
-700	737.5	56929
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-700	775.0	12.5	4.7	145.0	-700	762.5	56984
-700	787.5	12.8	4.6	147.1	-700	775.0	56952
-700	800.0	13.0	5.1	146.4	-700	787.5	56912
-600	-800.0	5.8	7.2	132.3	-700	800.0	56874
-600	-787.5	6.1	6.7	130.8	-600	-800.0	57108
-600	-775.0	6.0	6.1	131.3	-600	-787.5	57099
-600	-762.5	5.6	6.1	130.5	-600	-775.0	57130
-600	-750.0	5.6	6.1	133.1	-600	-762.5	57118
-600	-737.5	5.6	6.0	133.2	-600	-750.0	57055
-600	-725.0	3.7	5.1	134.6	-600	-737.5	57022
-600	-712.5	2.5	4.4	136.7	-600	-725.0	57042
-600	-700.0	2.5	3.8	137.4	-600	-712.5	57032
-600	-687.5	1.4	3.3	137.8	-600	-700.0	57028
-600	-675.0	2.0	3.1	139.5	-600	-687.5	57002
-600	-662.5	2.2	2.6	140.5	-600	-675.0	57034
-600	-650.0	1.3	2.0	140.6	-600	-662.5	57036
-600	-637.5	1.2	1.6	141.0	-600	-650.0	57024
-600	-625.0	1.8	1.6	139.0	-600	-637.5	57024
-600	-612.5	2.1	1.5	138.5	-600	-625.0	57025
-600	-600.0	2.6	1.3	139.5	-600	-612.5	57008
-600	-587.5	2.3	0.8	140.4	-600	-600.0	57028
-600	-575.0	2.3	0.2	139.3	-600	-587.5	57020
-600	-562.5	2.0	0.0	138.5	-600	-575.0	57044
-600	-550.0	2.5	-0.3	139.6	-600	-562.5	57002
-600	-537.5	1.9	-1.2	136.5	-600	-550.0	57043
-600	-525.0	2.9	-0.8	134.4	-600	-537.5	57001
-600	-512.5	3.1	-1.0	133.7	-600	-525.0	56990
-600	-500.0	4.5	0.0	131.9	-600	-512.5	56975
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-600	-475.0	6.6	1.3	133.0	-600	-487.5	56948
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-600	-387.5	14.5	4.3	143.0	-600	-400.0	56979
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-600	-362.5	15.5	4.5	148.9	-600	-375.0	56998
-600	-350.0	12.4	3.0	148.0	-600	-362.5	57047
-600	-337.5	11.2	1.8	148.1	-600	-350.0	57040
-600	-325.0	11.4	2.2	145.3	-600	-337.5	56987
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-600	-300.0	10.0	1.6	148.2	-600	-312.5	57005
-600	-287.5	8.9	1.3	150.9	-600	-300.0	56989
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-600	-262.5	6.2	2458.1	152.5	-600	-275.0	56988
-600	-250.0	4.5	-0.5	151.4	-600	-262.5	57010
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-600	-225.0	3.0	-1.2	150.1	-600	-237.5	57021
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-600	-175.0	3.1	-0.4	147.9	-600	-187.5	57027
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-600	-75.0	-0.1	0.2	150.6
-600	-62.5	-0.1	0.3	150.5
-600	-50.0	-0.4	0.1	151.4
-600	-37.5	-0.4	0.3	151.5
-600	-25.0	-1.4	-0.3	149.5
-600	-12.5	-1.8	-0.6	148.7
-600	0.0	-4.0	1.7	120.0
-600	12.5	-3.7	2.1	118.8
-600	25.0	-3.5	1.7	116.9
-600	37.5	-3.2	2.5	115.1
-600	50.0	-2.5	2.4	113.8
-600	62.5	-0.9	2.6	111.4
-600	75.0	0.8	3.0	109.5
-600	87.5	2.2	3.3	108.7
-600	100.0	3.9	3.5	108.2
-600	112.5	5.3	4.1	108.0
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-600	137.5	8.5	3.7	110.0
-600	150.0	9.3	4.0	109.9
-600	162.5	9.4	3.5	111.0
-600	175.0	9.4	2.5	112.5
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-600	200.0	12.2	4.1	115.0
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-600	237.5	11.9	3.5	119.8
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-600	287.5	5.3	2.7	121.7
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-600	375.0	0.4	4.4	117.2
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-600	425.0	-3.8	1.4	113.7
-600	437.5	-5.1	1.2	114.1
-600	450.0	-6.0	0.6	111.3
-600	462.5	-6.6	1.3	110.9
-600	475.0	-6.9	1.4	109.1
-600	487.5	-5.9	1.2	106.5
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-600	512.5	-4.0	3.9	105.4
-600	525.0	-3.6	5.3	104.4
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-600	-150.0	56990
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-600	-50.0	57033
-600	-37.5	57024
-600	-25.0	57039
-600	-12.5	57046
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-600	12.5	57096
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-600	37.5	57049
-600	50.0	57071
-600	62.5	57069
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-600	87.5	57049
-600	100.0	57026
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-600	137.5	57008
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-600	162.5	56984
-600	175.0	56999
-600	187.5	57019
-600	200.0	57007
-600	212.5	57009
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-600	237.5	56970
-600	250.0	56970
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-600	475.0	56928
-600	487.5	56923
-600	500.0	56927
-600	512.5	56931
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-600	562.5	-1.1	7.3	105.1	-600	550.0	56986
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-600	600.0	1.1	8.0	104.5	-600	587.5	56970
-600	612.5	1.9	7.7	104.7	-600	600.0	56935
-600	625.0	1.9	6.9	105.0	-600	612.5	56922
-600	637.5	1.7	7.1	104.3	-600	625.0	56908
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-600	662.5	0.6	6.3	103.6	-600	650.0	56916
-600	675.0	0.0	4.5	102.5	-600	662.5	56890
-600	687.5	0.0	3.9	101.8	-600	675.0	56907
-600	700.0	1.1	5.0	100.9	-600	687.5	56917
-600	712.5	0.9	5.4	102.0	-600	700.0	56892
-600	725.0	1.4	4.7	103.6	-600	712.5	56884
-600	737.5	2.4	4.5	103.6	-600	725.0	56893
-600	750.0	3.4	6.7	104.9	-600	737.5	56908
-600	762.5	4.6	7.4	105.9	-600	750.0	56915
-600	775.0	5.1	6.6	109.0	-600	762.5	56869
-600	787.5	4.5	6.2	110.1	-600	775.0	56869
-600	800.0	5.3	6.2	113.5	-600	787.5	56887
-500	-800.0	-7.7	4.3	137.2	-600	800.0	56901
-500	-787.5	-6.3	5.2	135.9	-500	-800.0	57037
-500	-775.0	-5.4	5.2	136.3	-500	-787.5	57085
-500	-762.5	-5.5	4.6	133.5	-500	-775.0	57061
-500	-750.0	-6.6	3.6	134.1	-500	-762.5	57088
-500	-737.5	-6.5	3.5	131.6	-500	-750.0	57079
-500	-725.0	-6.4	3.3	130.4	-500	-737.5	57048
-500	-712.5	-5.7	3.2	129.9	-500	-725.0	57025
-500	-700.0	-5.5	2.8	129.5	-500	-712.5	57025
-500	-687.5	-4.5	2.7	130.8	-500	-700.0	57062
-500	-675.0	-4.0	2.9	126.5	-500	-687.5	57024
-500	-662.5	-3.0	3.2	127.5	-500	-675.0	57026
-500	-650.0	-1.2	3.9	126.6	-500	-662.5	57081
-500	-637.5	-0.1	4.0	127.6	-500	-650.0	57065
-500	-625.0	0.4	3.7	128.1	-500	-637.5	57051
-500	-612.5	1.1	3.5	127.3	-500	-625.0	57112
-500	-600.0	1.1	3.0	127.6	-500	-612.5	57098
-500	-587.5	1.3	2.8	127.1	-500	-600.0	57093
-500	-575.0	2.2	2.4	127.5	-500	-587.5	57120
-500	-562.5	2.4	2.4	128.9	-500	-575.0	57101
-500	-550.0	2.8	2.1	128.7	-500	-562.5	57070
-500	-537.5	4.0	2.2	129.8	-500	-550.0	57048
-500	-525.0	3.5	1.7	128.8	-500	-537.5	57073
-500	-512.5	4.1	1.2	130.2	-500	-525.0	57078
-500	-500.0	4.7	1.2	130.0	-500	-512.5	57045
-500	-487.5	4.2	0.4	130.2	-500	-500.0	57032
-500	-475.0	4.3	0.3	130.5	-500	-487.5	57031
-500	-462.5	3.6	-0.5	133.6	-500	-475.0	57053
-500	-450.0	3.2	-0.8	128.1	-500	-462.5	57054
-500	-437.5	3.3	-1.0	129.5	-500	-450.0	57046
-500	-425.0	2.9	-1.3	128.2	-500	-437.5	57044
-500	-412.5	2.9	-1.1	127.3	-500	-425.0	57081
-500	-400.0	3.5	-0.9	126.2	-500	-412.5	57122
-500	-387.5	3.6	-0.5	128.9	-500	-400.0	57132
-500	-375.0	3.7	-0.7	127.0	-500	-387.5	57139
-500	-362.5	4.2	0.0	127.1	-500	-375.0	57148

-500	-350.0	4.4	0.1	129.1	-500	-362.5	57087
-500	-337.5	2.1	-0.8	129.1	-500	-350.0	57049
-500	-325.0	2.6	-0.6	129.5	-500	-337.5	56996
-500	-312.5	0.7	-1.1	130.1	-500	-325.0	57005
-500	-300.0	-0.5	-1.4	129.8	-500	-312.5	57098
-500	-287.5	-0.8	-1.5	129.1	-500	-300.0	57105
-500	-275.0	-2.0	-2.0	128.1	-500	-287.5	57125
-500	-262.5	-2.4	-2.1	131.0	-500	-275.0	57106
-500	-250.0	-3.3	-2.5	127.4	-500	-262.5	57085
-500	-237.5	-3.9	-2.9	127.2	-500	-250.0	57065
-500	-225.0	-3.6	-3.1	126.8	-500	-237.5	57103
-500	-212.5	-3.7	-3.3	128.5	-500	-225.0	57114
-500	-200.0	-5.2	-4.2	127.5	-500	-212.5	57108
-500	-187.5	-5.3	-4.5	126.1	-500	-200.0	57092
-500	-175.0	-4.9	-4.4	124.8	-500	-187.5	57099
-500	-162.5	-3.4	-3.9	122.2	-500	-175.0	57051
-500	-150.0	-1.1	-2.7	122.0	-500	-162.5	56995
-500	-137.5	0.0	-2.1	121.9	-500	-150.0	56991
-500	-125.0	0.8	-2.0	123.0	-500	-137.5	57006
-500	-112.5	-0.4	-2.4	124.6	-500	-125.0	56997
-500	-100.0	-2.8	-3.4	122.4	-500	-112.5	57019
-500	-87.5	-3.6	-3.7	121.3	-500	-100.0	57046
-500	-75.0	-2.9	-3.5	119.1	-500	-87.5	57024
-500	-62.5	-2.1	-3.0	119.3	-500	-75.0	57051
-500	-50.0	-1.2	-2.6	118.6	-500	-62.5	57086
-500	-37.5	1.5	-1.2	119.9	-500	-50.0	57100
-500	-25.0	2.8	-0.3	126.0	-500	-37.5	57029
-500	-12.5	3.7	-0.4	124.9	-500	-25.0	56999
-500	12.5	7.1	0.0	156.7	-500	-12.5	56935
-500	25.0	5.1	-1.4	156.1	-500	12.5	56962
-500	37.5	4.3	-1.8	151.5	-500	25.0	56957
-500	50.0	4.5	-1.6	149.6	-500	37.5	56894
-500	62.5	4.3	-1.0	150.0	-500	50.0	56866
-500	75.0	1.1	-2.8	148.4	-500	62.5	56870
-500	87.5	1.6	-2.9	143.1	-500	75.0	56907
-500	100.0	4.6	-1.1	141.0	-500	87.5	56962
-500	112.5	6.5	-0.4	141.6	-500	100.0	56989
-500	125.0	7.6	-0.4	140.4	-500	112.5	57039
-500	137.5	9.3	0.0	139.0	-500	125.0	57045
-500	150.0	11.1	0.9	140.3	-500	137.5	57028
-500	162.5	11.4	0.9	139.4	-500	150.0	57055
-500	175.0	11.0	0.4	141.1	-500	162.5	57050
-500	187.5	11.6	1.1	139.1	-500	175.0	57037
-500	200.0	12.2	1.3	141.1	-500	187.5	57002
-500	212.5	12.6	1.1	141.0	-500	200.0	56993
-500	225.0	13.3	1.3	140.8	-500	212.5	56936
-500	237.5	13.7	1.4	144.5	-500	225.0	56977
-500	250.0	12.6	1.2	144.1	-500	237.5	56974
-500	262.5	11.7	1.3	148.1	-500	250.0	56969
-500	275.0	10.4	0.9	150.6	-500	262.5	56964
-500	287.5	9.1	0.6	151.2	-500	275.0	56972
-500	300.0	8.1	0.1	149.9	-500	287.5	56974
-500	312.5	7.2	0.7	151.3	-500	300.0	56979
-500	325.0	7.0	0.7	151.7	-500	312.5	56978
-500	337.5	5.9	0.7	150.4	-500	325.0	56950
-500	350.0	4.9	0.6	152.7	-500	337.5	56964

-500	362.5	4.8	0.4	149.9	-500	350.0	56935
-500	375.0	4.1	0.5	147.2	-500	362.5	56918
-500	387.5	4.5	0.8	143.7	-500	375.0	56880
-500	400.0	4.1	0.9	142.8	-500	387.5	56931
-500	412.5	4.3	0.6	142.1	-500	400.0	56926
-500	425.0	4.1	1.4	142.2	-500	412.5	56914
-500	437.5	3.7	0.8	138.8	-500	425.0	56917
-500	450.0	3.0	0.5	140.1	-500	437.5	56912
-500	462.5	3.7	0.9	136.5	-500	450.0	56891
-500	475.0	2.1	0.7	136.5	-500	462.5	56897
-500	487.5	1.1	0.0	134.2	-500	475.0	56893
-500	500.0	-1.1	0.3	130.1	-500	487.5	56916
-500	512.5	-3.0	-0.2	129.2	-500	500.0	56891
-500	525.0	-1.3	0.6	126.6	-500	512.5	56916
-500	537.5	-1.3	1.2	128.2	-500	525.0	56916
-500	550.0	-3.4	0.7	127.3	-500	537.5	56930
-500	562.5	-2.1	1.8	124.8	-500	550.0	56955
-500	575.0	-1.7	2.5	123.8	-500	562.5	56924
-500	587.5	0.1	3.7	121.0	-500	575.0	56981
-500	600.0	1.5	4.3	121.3	-500	587.5	56976
-500	612.5	2.3	4.7	121.8	-500	600.0	56980
-500	625.0	2.2	4.6	121.3	-500	612.5	56947
-500	637.5	2.3	3.5	119.3	-500	625.0	56970
-500	650.0	3.0	4.5	117.5	-500	637.5	56956
-500	662.5	4.4	7.1	118.3	-500	650.0	56986
-500	675.0	5.5	7.9	116.9	-500	662.5	57006
-500	687.5	6.9	7.7	118.1	-500	675.0	56976
-500	700.0	5.7	6.1	118.1	-500	687.5	56950
-500	712.5	6.6	6.4	118.7	-500	700.0	57065
-500	725.0	5.3	5.7	121.4	-500	712.5	57086
-500	737.5	3.5	4.8	120.2	-500	725.0	57083
-500	750.0	4.5	4.3	119.7	-500	737.5	57096
-500	762.5	3.9	3.3	119.1	-500	750.0	57046
-500	775.0	3.8	3.0	117.8	-500	762.5	57036
-500	787.5	3.4	3.3	117.4	-500	775.0	56948
-500	800.0	3.8	3.5	117.8	-500	787.5	56906
-400	-800.0	2.5	3.2	161.9	-500	800.0	56994
-400	-787.5	2.7	3.6	158.1	-400	-800.0	57141
-400	-775.0	4.0	4.0	158.6	-400	-787.5	57156
-400	-762.5	3.1	3.6	159.0	-400	-775.0	57264
-400	-750.0	4.7	4.5	158.4	-400	-762.5	57223
-400	-737.5	4.9	5.2	159.9	-400	-750.0	57327
-400	-725.0	5.4	5.7	162.8	-400	-737.5	57219
-400	-712.5	5.4	5.0	162.0	-400	-725.0	57218
-400	-700.0	5.1	4.8	163.6	-400	-712.5	57133
-400	-687.5	5.6	4.5	166.1	-400	-700.0	57125
-400	-675.0	4.7	3.3	165.7	-400	-687.5	57145
-400	-662.5	4.6	2.1	165.8	-400	-675.0	57147
-400	-650.0	4.6	2.4	168.4	-400	-662.5	57135
-400	-637.5	5.3	2.2	166.7	-400	-650.0	57135
-400	-625.0	5.4	2.2	169.4	-400	-637.5	57104
-400	-612.5	5.7	2.3	167.2	-400	-625.0	57094
-400	-600.0	5.6	2.0	167.1	-400	-612.5	57150
-400	-587.5	5.6	1.2	169.4	-400	-600.0	57096
-400	-575.0	5.3	1.5	167.2	-400	-587.5	57100
-400	-562.5	5.5	1.2	169.4	-400	-575.0	57139

-400	-550.0	5.7	0.5	167.8
-400	-537.5	4.1	-0.6	168.2
-400	-525.0	5.2	-1.2	166.6
-400	-512.5	2.6	-0.5	167.5
-400	-500.0	5.2	0.3	167.0
-400	-487.5	5.4	0.0	167.4
-400	-475.0	5.7	1.3	167.6
-400	-462.5	5.5	0.6	168.9
-400	-450.0	5.8	1.2	170.1
-400	-437.5	6.4	2.1	172.3
-400	-425.0	4.9	0.7	170.6
-400	-412.5	5.6	1.4	172.5
-400	-400.0	5.8	1.4	172.5
-400	-387.5	5.5	0.8	171.1
-400	-375.0	4.8	0.3	174.5
-400	-362.5	5.1	0.1	171.1
-400	-350.0	4.9	0.2	172.3
-400	-337.5	5.2	0.4	173.2
-400	-325.0	5.1	0.2	174.8
-400	-312.5	5.9	0.2	174.6
-400	-300.0	4.8	0.5	177.7
-400	-287.5	5.3	0.0	179.2
-400	-275.0	4.7	-0.5	178.8
-400	-262.5	4.4	-0.1	180.4
-400	-250.0	4.0	0.2	183.1
-400	-237.5	4.0	0.1	180.6
-400	-225.0	4.9	0.2	181.1
-400	-212.5	4.4	-0.4	182.5
-400	-200.0	4.4	-0.6	182.3
-400	-187.5	4.6	-0.7	183.0
-400	-175.0	6.7	0.3	182.1
-400	-162.5	7.7	0.8	185.9
-400	-150.0	7.3	-0.8	190.8
-400	-137.5	4.4	-1.3	194.6
-400	-125.0	3.2	-3.2	191.7
-400	-112.5	2.3	-2.5	192.6
-400	-100.0	2.3	-2.6	191.0
-400	-87.5	2.6	-2.1	187.7
-400	-75.0	3.4	-0.9	187.5
-400	-62.5	4.6	-0.7	190.6
-400	-50.0	5.8	0.0	194.0
-400	-37.5	7.6	0.6	191.3
-400	-25.0	8.2	0.1	199.5
-400	-12.5	5.4	-1.2	202.1
-400	0.0	5.6	-1.1	197.8
-400	12.5	7.3	-0.2	197.8
-400	25.0	7.7	0.3	205.0
-400	37.5	3.3	-2.9	205.7
-400	50.0	5.6	-1.4	198.3
-400	62.5	7.4	-0.3	201.7
-400	75.0	8.7	0.0	205.7
-400	87.5	8.0	-0.2	207.7
-400	100.0	8.4	-0.6	209.4
-400	112.5	7.4	-1.1	209.7
-400	125.0	6.2	-1.2	210.8
-400	137.5	4.7	-1.6	212.5

-400	-562.5	57149
-400	-550.0	57148
-400	-537.5	57168
-400	-525.0	57180
-400	-512.5	57169
-400	-500.0	57149
-400	-487.5	57096
-400	-475.0	57166
-400	-462.5	57148
-400	-450.0	57116
-400	-437.5	57142
-400	-425.0	57021
-400	-412.5	57031
-400	-400.0	57031
-400	-387.5	57027
-400	-375.0	57052
-400	-362.5	57101
-400	-350.0	57097
-400	-337.5	57117
-400	-325.0	57098
-400	-312.5	56968
-400	-300.0	57106
-400	-287.5	57114
-400	-275.0	57142
-400	-262.5	57131
-400	-250.0	57132
-400	-237.5	57130
-400	-225.0	57076
-400	-212.5	57036
-400	-200.0	57020
-400	-187.5	56922
-400	-175.0	57001
-400	-162.5	57007
-400	-150.0	56934
-400	-137.5	56929
-400	-125.0	56894
-400	-112.5	56912
-400	-100.0	56962
-400	-87.5	56973
-400	-75.0	56989
-400	-62.5	56990
-400	-50.0	56989
-400	-37.5	56988
-400	-25.0	56981
-400	-12.5	57007
-400	0.0	57012
-400	12.5	57021
-400	25.0	57028
-400	37.5	57051
-400	50.0	57050
-400	62.5	57019
-400	75.0	57006
-400	87.5	56994
-400	100.0	56984
-400	112.5	56975
-400	125.0	56962

-400	150.0	4.2	-2.1	209.2
-400	162.5	4.2	-1.8	207.0
-400	175.0	5.2	-1.5	206.6
-400	187.5	4.7	-0.9	207.8
-400	200.0	5.9	-0.8	206.1
-400	212.5	6.6	-0.1	205.8
-400	225.0	7.9	0.4	207.1
-400	237.5	8.3	0.8	207.8
-400	250.0	8.7	1.1	210.0
-400	262.5	8.9	0.4	213.8
-400	275.0	7.8	0.6	213.9
-400	287.5	8.0	0.3	215.7
-400	300.0	7.4	1.5	217.9
-400	312.5	6.4	0.0	224.3
-400	325.0	4.6	0.8	230.1
-400	337.5	2.3	-0.1	232.4
-400	350.0	-0.5	-0.8	235.6
-400	362.5	-4.1	-1.7	232.8
-400	375.0	-4.8	-0.9	227.9
-400	387.5	-4.2	0.0	221.4
-400	400.0	-2.5	0.7	223.1
-400	412.5	-1.7	2.2	223.6
-400	425.0	-3.0	1.9	225.7
-400	437.5	-3.1	1.9	224.0
-400	450.0	-3.5	2.1	222.5
-400	462.5	-4.2	2.5	225.4
-400	475.0	-3.7	2.9	224.1
-400	487.5	-4.2	2.3	225.2
-400	500.0	-4.4	2.2	226.9
-400	512.5	-5.2	2.3	217.8
-400	525.0	-6.2	2.5	215.8
-400	537.5	-5.6	2.8	210.1
-400	550.0	-2.8	4.3	207.2
-400	562.5	-1.6	5.0	207.0
-400	575.0	0.1	6.0	204.9
-400	587.5	2.8	6.5	205.6
-400	600.0	5.7	8.1	209.3
-400	612.5	4.7	7.2	217.7
-400	625.0	-4.9	1.7	229.2
-400	637.5	-19.1	-6.0	218.2
-400	650.0	-16.3	-5.4	198.7
-400	662.5	-11.7	-2.2	188.6
-400	675.0	-8.6	-0.3	185.0
-400	687.5	-5.6	1.4	181.5
-400	700.0	-2.9	3.7	179.1
-400	712.5	0.8	5.2	181.3
-400	725.0	1.1	5.2	183.4
-400	737.5	2.2	5.3	184.3
-400	750.0	2.6	5.4	182.8
-400	762.5	3.1	5.2	186.1
-400	775.0	1.0	3.9	188.3
-400	787.5	-0.6	2.4	188.3
-400	800.0	-1.5	1.3	185.9

-400	137.5	56976
-400	150.0	56979
-400	162.5	56986
-400	175.0	56989
-400	187.5	56980
-400	200.0	56985
-400	212.5	56975
-400	225.0	56982
-400	237.5	56999
-400	250.0	57007
-400	262.5	57014
-400	275.0	57017
-400	287.5	57004
-400	300.0	56988
-400	312.5	56990
-400	325.0	56996
-400	337.5	56982
-400	350.0	56970
-400	362.5	56975
-400	375.0	56977
-400	387.5	56976
-400	400.0	56967
-400	412.5	56969
-400	425.0	56982
-400	437.5	56972
-400	450.0	56982
-400	462.5	56982
-400	475.0	56962
-400	487.5	56962
-400	500.0	56969
-400	512.5	56951
-400	525.0	56937
-400	537.5	56948
-400	550.0	56949
-400	562.5	56953
-400	575.0	56947
-400	587.5	56952
-400	600.0	56957
-400	612.5	56949
-400	625.0	56899
-400	637.5	56856
-400	650.0	56908
-400	662.5	56976
-400	675.0	56999
-400	687.5	56930
-400	700.0	56955
-400	712.5	57012
-400	725.0	56998
-400	737.5	56964
-400	750.0	56927
-400	762.5	56874
-400	775.0	56815
-400	787.5	56876
-400	800.0	56938

Specifications

Frequency Tuning Range	15 to 30 kHz, with bandwidth of 150 Hz; tuning range accommodates new Puerto Rico station at 28.5 kHz.
Transmitting Stations Measured	Up to 3 stations can be automatically measured at any given grid location within frequency tuning range.
Recorded VLF Magnetic Parameters	Vertical in-phase, vertical quadrature (out-of-phase), total field strength (or optional horizontal amplitude), dip angle.
Standard Memory Capacity	1300 combined VLF magnetic and VLF electric measurements as well as gradiometer and magnetometer readings.
Display	Custom designed, ruggedized liquid crystal display with built-in heater and an operating temperature range from −40°C to +55°C. The display contains six numeric digits, decimal point, battery status monitor, signal strength status monitor and function descriptors.
RS232C Serial I/O Interface	Variable baud rate from 300 to 9600 baud, 8 data bits, 2 stop bits, no parity.
Test Mode	A. Diagnostic Testing (data and programmable memory). B. Self Test (hardware).
Sensor Head	Contains 3 orthogonally mounted coils with automatic tilt compensation.
Operating Environmental Range	−40°C to +55°C; 0 – 100% relative humidity; Weatherproof.
Power Supply	Non-magnetic rechargeable sealed lead-acid 18V DC battery cartridge or belt; 18V DC disposable battery belt; 12V DC external power source for base station operation only.
Weights and Dimensions	
Instrument Console	3.8 kg, 122 x 246 x 210 mm.
Sensor Head	0.9 kg, 140 dia. x 130 mm.
VLF Electronics Module	1.7 kg, 280 x 190 x 60 mm.
Lead Acid Battery Cartridge	1.8 kg, 138 x 95 x 75 mm.
Lead Acid Battery Belt	1.8 kg, 540 x 100 x 40 mm.
Disposable Battery Belt	1.2 kg, 540 x 100 x 40 mm.

EDA Instruments Inc
4 Thorncliffe Park Drive
Toronto, Ontario
Canada M4H 1H1
Telex: 06 23222 EDA TOR
Cables: Instruments Toronto
Telephone: (416) 425-7800
Fax: (416) 425-8135

In USA,
EDA Instruments Inc
5151 Ward Road
Wheat Ridge, Colorado
U.S.A. 80033
Telephone (303) 422-9112

nted in Canada

Physical Dimensions	Wt(kg):	w x h x d(mm)
Instrument console only	3.8:	122 x 246 x 210
Battery belt	1.8:	540 x 100 x 40
Battery cartridge	1.8:	138 x 95 x 75
Sensors		
Magnetometer remote sensor	1.2:	56 dia x 220
Magnetometer gradient sensor	2.1:	56 dia x 790
VLF sensor module	2.6:	280 x 190 x 60

Environment

Electronics
- Operating temperature range... -40 C to +55 C
- Relative humidity..... 0 to 100% (weather-proof)

Magnetometer Sensors
- Temperature range..... -45 C to +55 C
- Relative humidity..... 0 to 100% (weather-proof)

VLF Sensor
- Temperature range..... -45 C to +55 C
- Relative humidity..... 0 to 100% (weather-proof)

Standard Memory Capacity

Field unit	1300 sets of readings
Tie-line points	100 sets of readings
Base staion	5500 sets of readings

Electronics

RS-232C serial I/O	300 to 9600 baud(programmable); 8 data bits, 2 stop bits; no parity
Electronics console	Enclosure contains electronics and battery pack (if not contained in separate belt). Front panel includes liquid crystal display (LCD), and keypad.
Power Supply	Internal battery pack or external battery belt; or 12V car battery (base station).

Table 1-1 Technical Summary

APPENDIX G

INDUCED POLARIZATION AND RESISTIVITY REPORT

BY PACIFIC GEOPHYSICAL LIMITED

PACIFIC Geophysical Limited

224-744 WEST HASTINGS STREET, VANCOUVER, B.C. V6C 1A5 TELEPHONE (604) 669-1070

TO: Peter Leriche, Ashworth Explorations Ltd.

FROM: Paul A. Cartwright and Grant D. Lockhart

RE: Induced Polarization and Resistivity Survey;
Lucky Boy Property, Greenwood M.D., B.C.

i) Summary of Results

An induced polarization (IP) and resistivity survey has been carried out on the Lucky Boy property, Greenwood M.D., B.C. by Pacific Geophysical Ltd., on behalf of Ashworth Explorations Limited, property managers for Dryden Resource Corporation.

A Phoenix Model IPV-1 IP and resistivity receiver unit was used to record the measurements, together with a Phoenix Model IPT-1 IP and resistivity transmitter unit powered by a 2 kw motor-generator. IP effects were recorded as Percent Frequency Effect (PFE) at operating frequencies of 4.0 Hz and 0.25 Hz, while apparent resistivity values were normalized in ohm-meters. Dipole-dipole array was employed exclusively using a basic inter-electrode distance of 25 meters in every case. A portion of Line 500N was also completed using 12.5 meter electrode intervals. Four dipole separations were measured in every case.

The interpreted IP results are illustrated on Dwg. No. I.P.P.-3012, a 1:2500 scale plan map of the Lucky Boy IP and resistivity grid, which also shows the contoured n=1 PFE readings. Dwg. No. R.P.-3012 is a 1:2500 scale plan map of the contoured n=1 apparent resistivity values.

Four zones of anomalous IP effects are interpreted to be present in the data, and are marked on Dwg. No. I.P.P.-3012.

Zone A appears to strike northeasterly across the western portion of the survey grid. Generally speaking, this trend is the most anomalous of the four zones detected, with the data recorded between Station 150S and Station 50S on Line 1200W exhibiting the most encouraging response. Depth to the top of the IP source is indicated to be less than 25 meters sub-surface in every case. A ragged zone of marginally lower than background apparent resistivity values can also be seen coincident with the anomalous IP effects that constitute Zone A.

Zone B is best outlined by the IP data collected in the vicinity of Station 112.5S on Line 1000W. The source of this zone is thought to extend westward to beyond Line 1050W, and eastward to beyond Line 900W. In this latter case, the zone is marked by only marginally anomalous IP effects. It is the authors' understanding that Zone B is coincident with the position of a narrow shear zone carrying elevated gold values.

Zone C is evident in the data collected on the extreme southern ends of Line 850W through to Line 750W. The zone is presently open in three directions, and may be composed of anomalous IP effects similar in magnitude to those which form Zone A.

Zone D is primarily outlined by somewhat anomalous IP effects together with slightly higher than background resistivity values, all of which trend roughly south-southwesterly across the eastern end of the grid until being truncated by IP Zone C. The region between Station 175S and Station 100S on Line 750W displays the most anomalous results recorded within the zone, the source of which appears to be more concentrated with increasing depth.

ii) Recommendations

Four separate anomalous zones are interpreted to be present in the induced polarization and resistivity data recorded on the Lucky Boy IP

grid. As any of these features could be outlining gold-bearing structures or zones, it is recommended that further work be considered to better evaluate the source of all of the IP zones.

Drilling and/or trenching should be considered to test the sources of Zone A, Zone B, and Zone D, with individual priorities being decided upon after correlating the IP data with other available information. It is the authors' understanding that Zone B may already have been trenched, in which case care should be taken to insure that the source of Zone B has actually been intersected or exposed.

In the case of IP Zone C, additional work should first take the form of further IP and resistivity work to better define the southern margin of the zone. Drill testing or trenching could then be carried out to physically evaluate the source of the IP response.

PACIFIC GEOPHYSICAL LTD.

Paul A. Cartwright, P.Geoph.

Grant D. Lockhart, B.Sc.

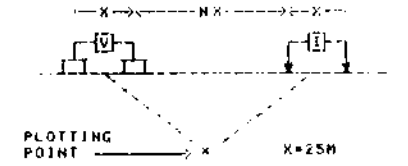
Dated: 29 February 1988

ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D /8 C.

LINE NO -1400W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1.-1.5 -2.-3.-5.-7 5.-10 PLUS EACH 0 25 FROM 0 5 TO 2 0

DWG NO -1 F 5856-1

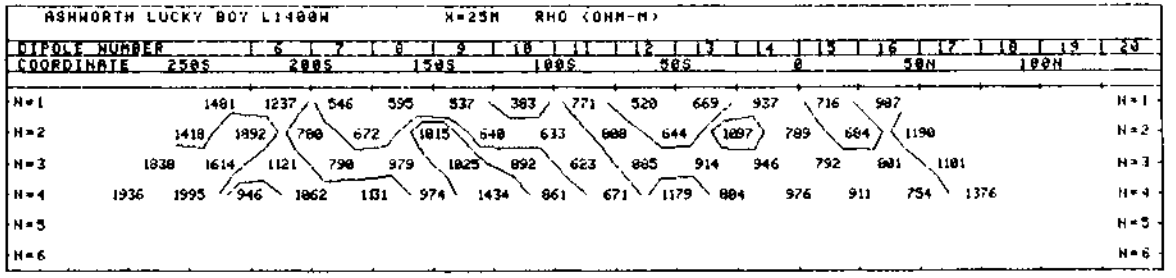
DATE SURVEYED FEB/86

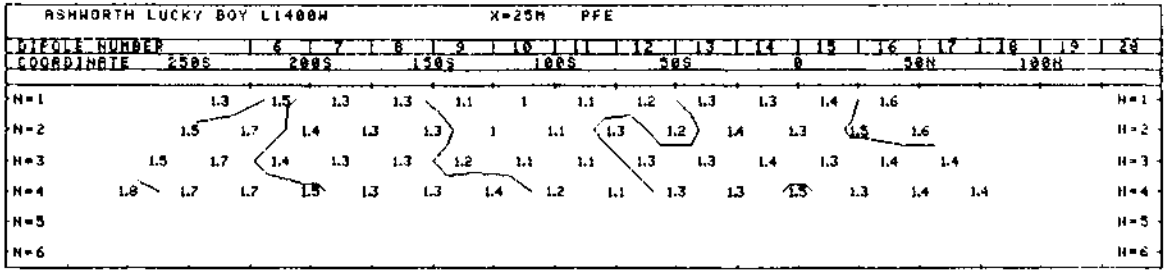
APPROVED PAK

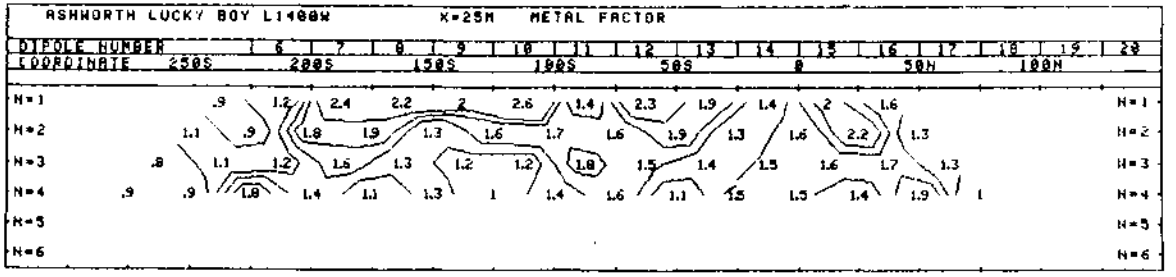
DATE FEB 27/86

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





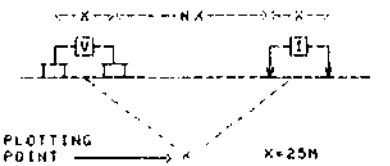


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D /B.C

LINE NO.-1300W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

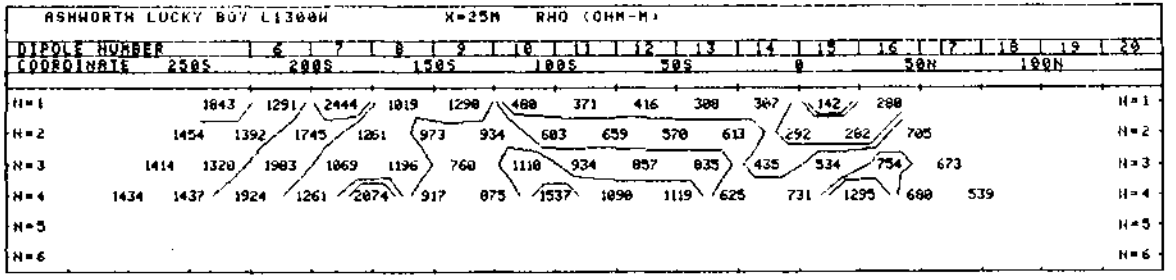
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7 5,-10 PLUS EACH 0 25 FROM 0 5 TO 2 0

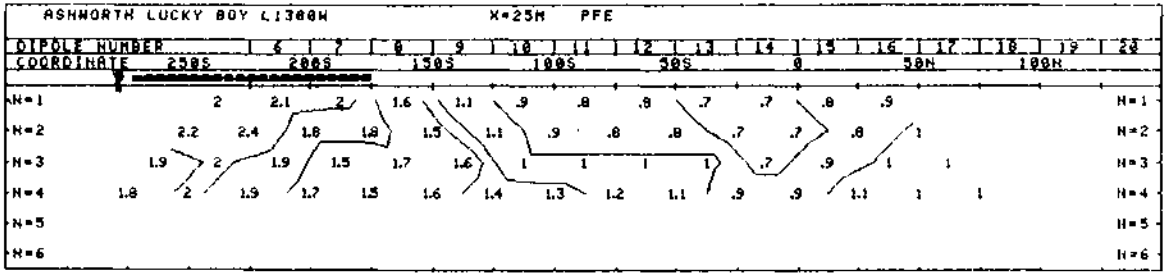
DWG NO -I P -5885 2

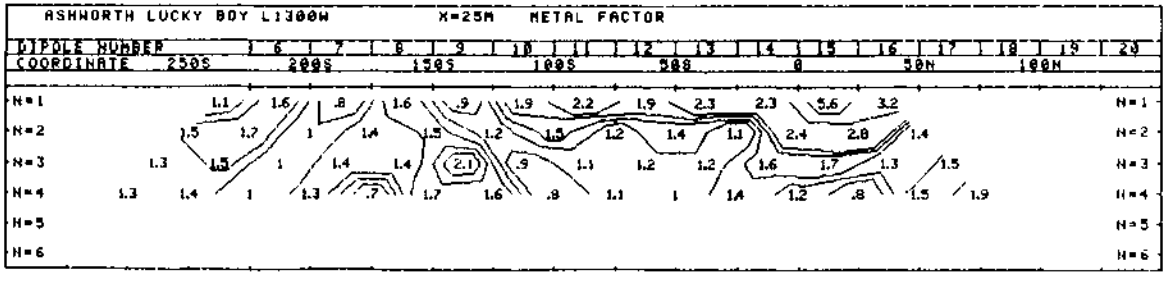
DATE SURVEYED FEB '88
APPROVED PAC
DATE FEB 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





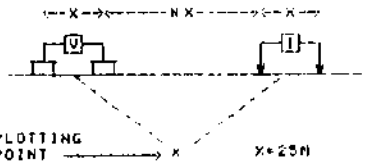


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M.D. (B.C.)

LINE NO. -1200N



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

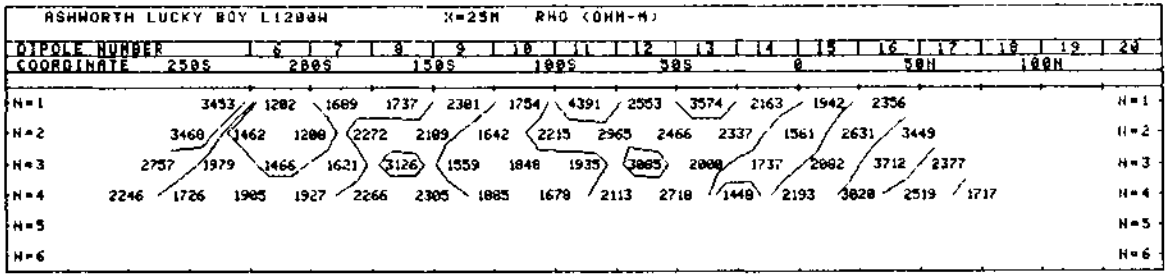
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

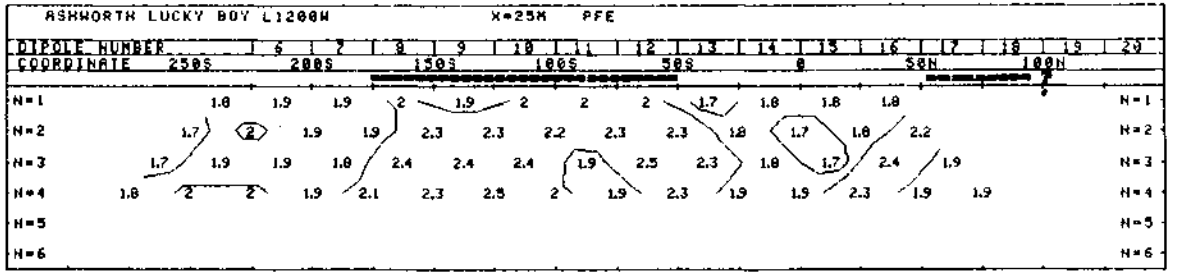
DWG NO -1 P 5000.3

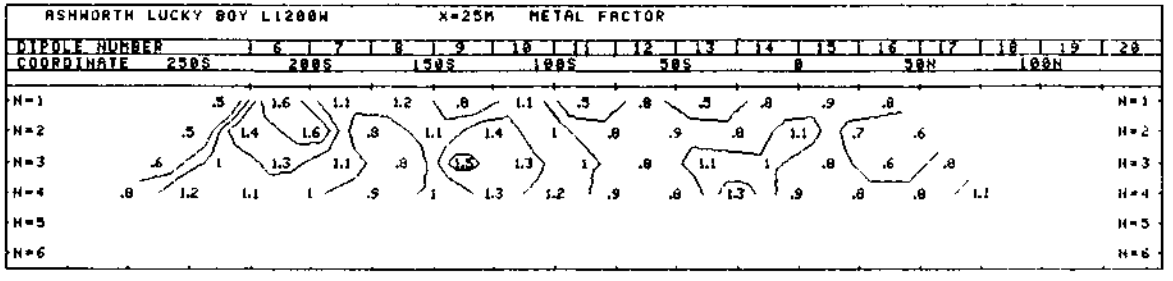
DATE SURVEYED FEB/88
APPROVED PAC
DATE FEB 27/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





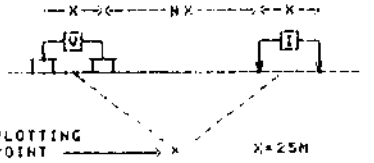


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D /8 C

LINE NO -1100N



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0/0 25

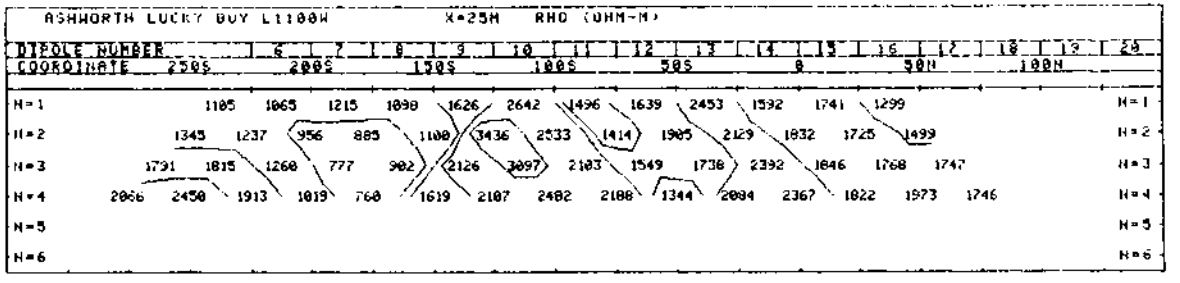
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1 5 -2,-3,-5,-7 5,-10 PLUS EACH 0 25 FROM 0 5 TO 2 0

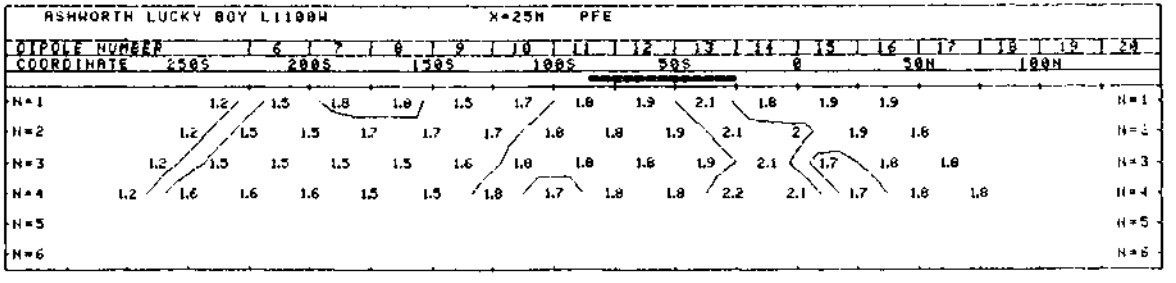
DWG NO -I P 5660 4

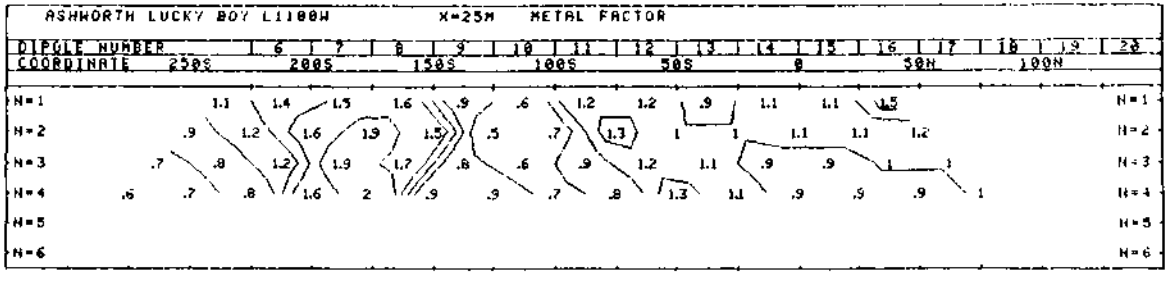
DATE SURVEYED FEB 88
APPROVED PAC
DATE FEB 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





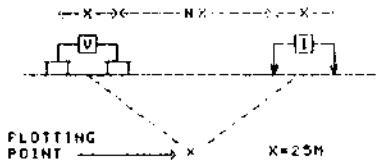


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D (B C

LINE NO -1050W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

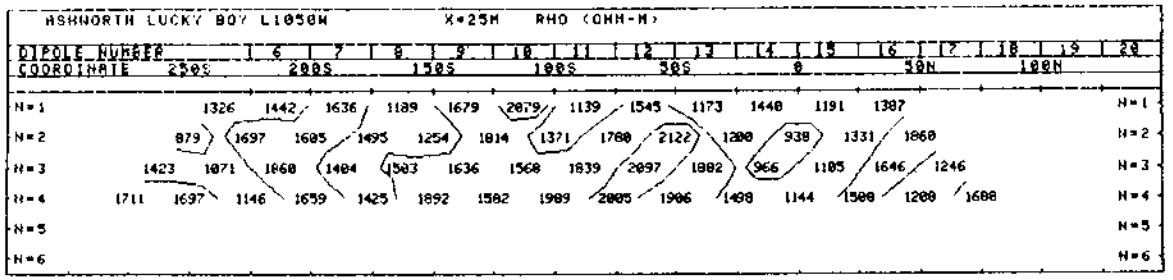
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

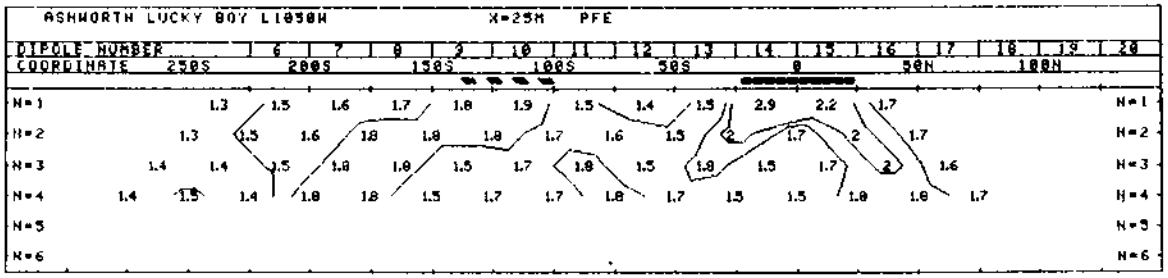
DWG NO (I.P. 5868.5

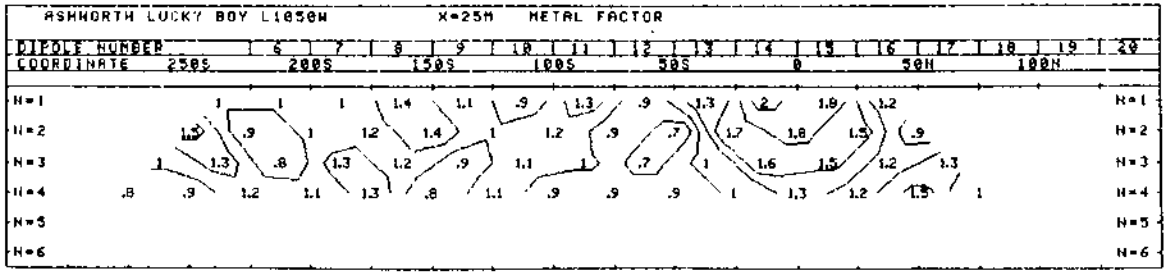
DATE SURVEYED FEB/88
APPROVED PAC
DATE FEB. 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





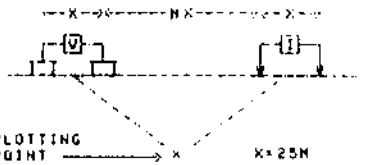


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D /B C

LINE NO -1000W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.8 25

NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

DWG NO 5 P -568a &

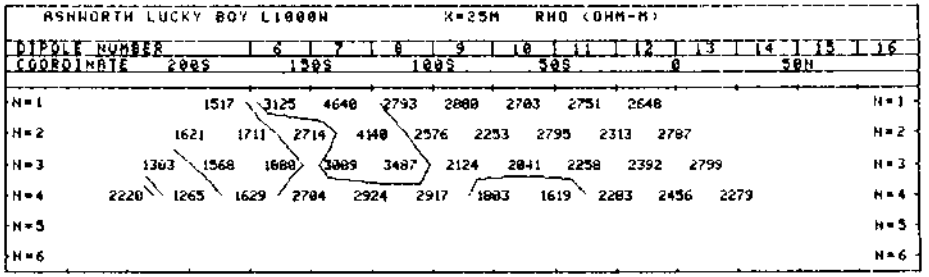
DATE SURVEYED FEB 88

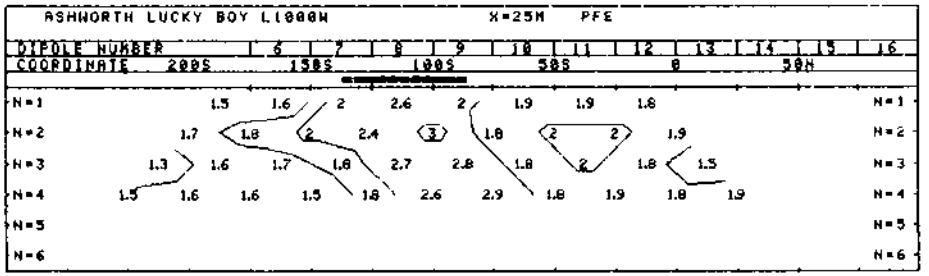
APPROVED PAC

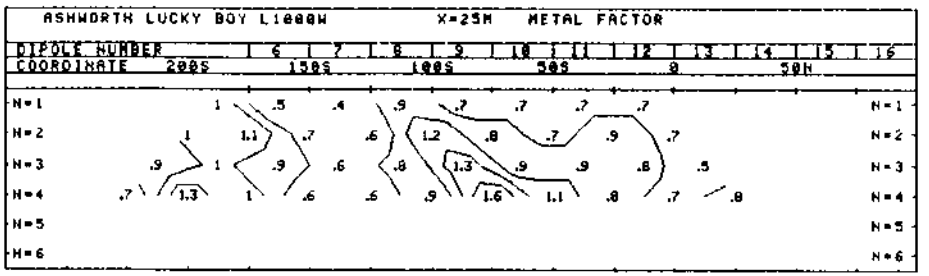
DATE FEB 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





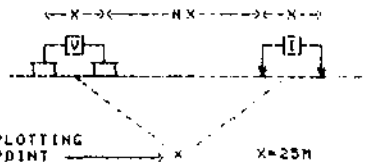


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D 18 C

LINE NO -950W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

DWG NO -1 P -5808-7

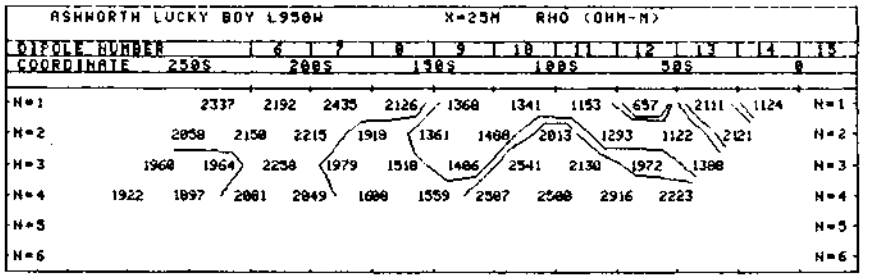
DATE SURVEYED FEB 08

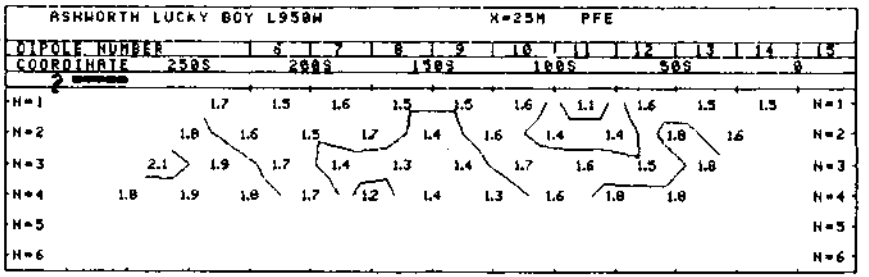
APPROVED PMC

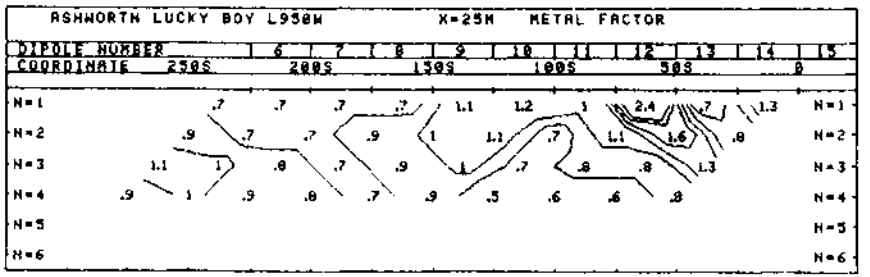
DATE Feb 27/08

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





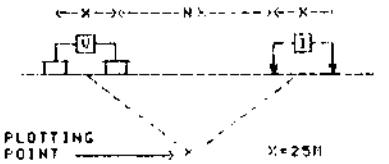


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D 18 C

LINE NO -900W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

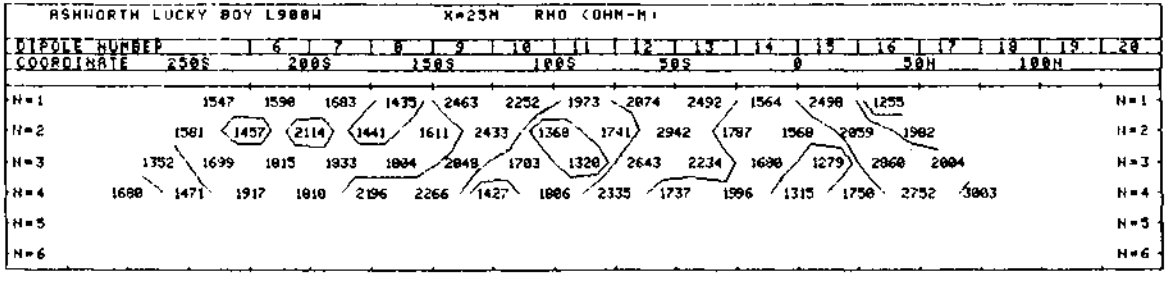
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

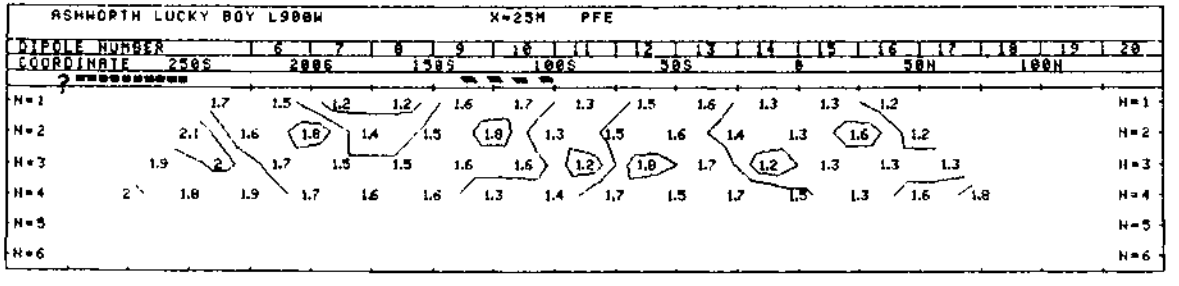
DWG NO [illegible]

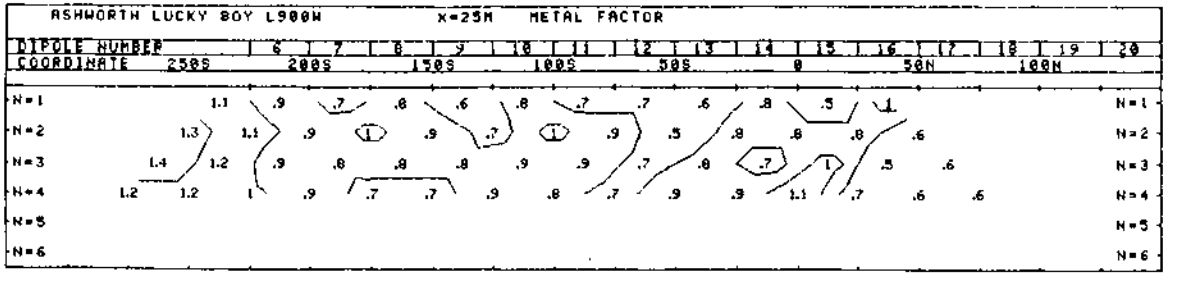
DATE SURVEYED FEB 88
APPROVED PAC
DATE FEB 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





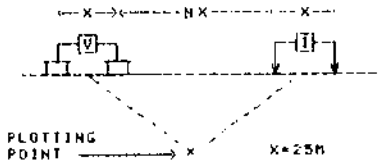


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D , B C

LINE NO -850W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

NOTE- CONTOURS AT LOGARITHMIC INTERVALS. 1,-1.5 -2.-3.-5.-7.5.-10 PLUS EACH 0 25 FROM 0 5 TO 2 0

DWG NO -1 F 588-3

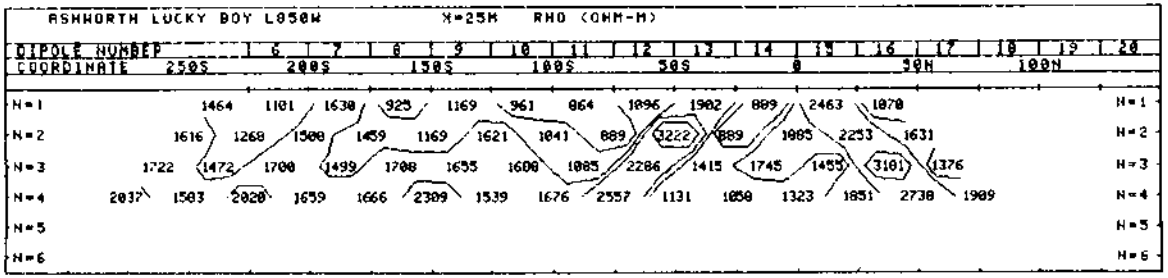
DATE SURVEYED FEB '88

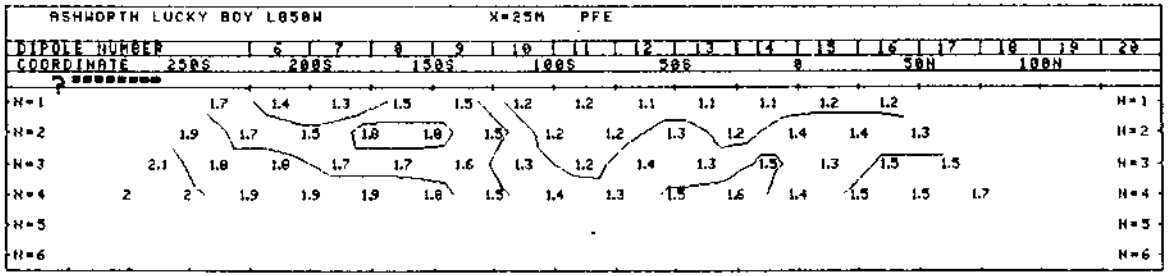
APPROVED VAC

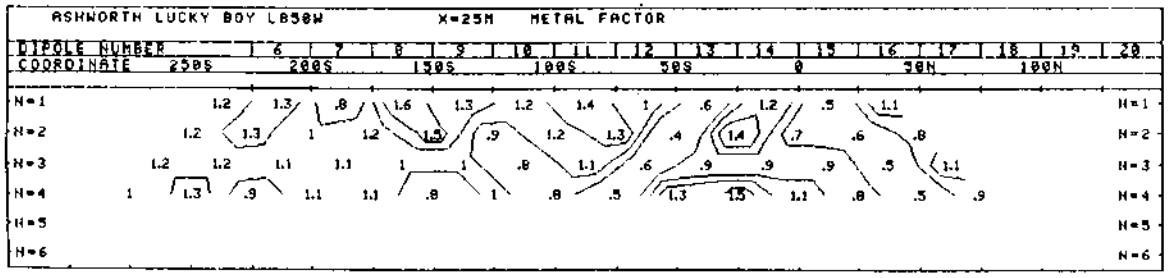
DATE FEB 22/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





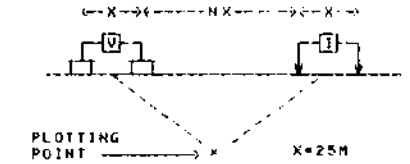


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D 18 C

LINE NO -800W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

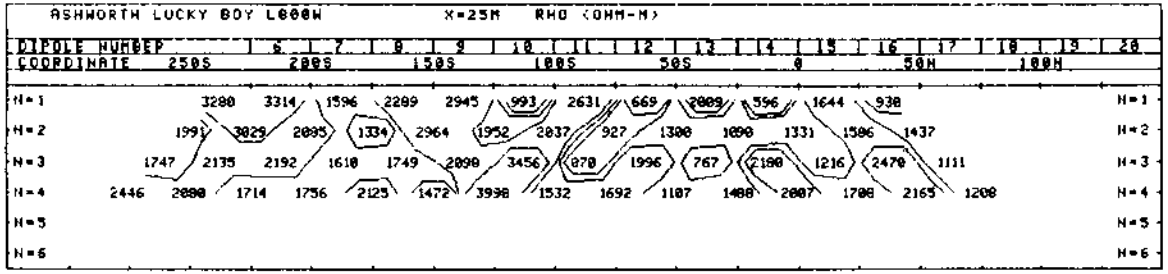
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

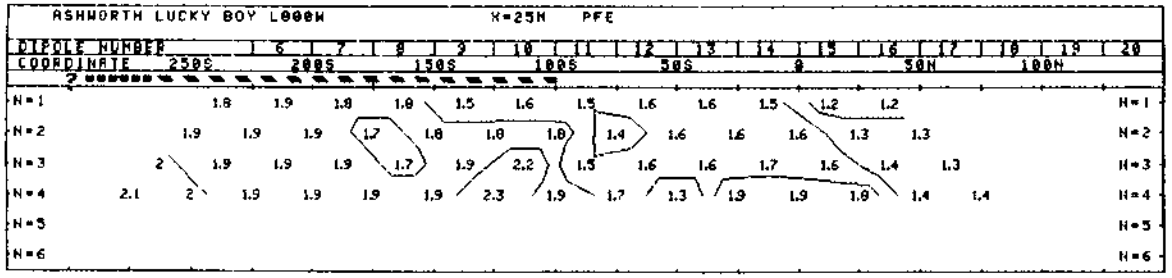
DWG NO -1 P [illegible] 10

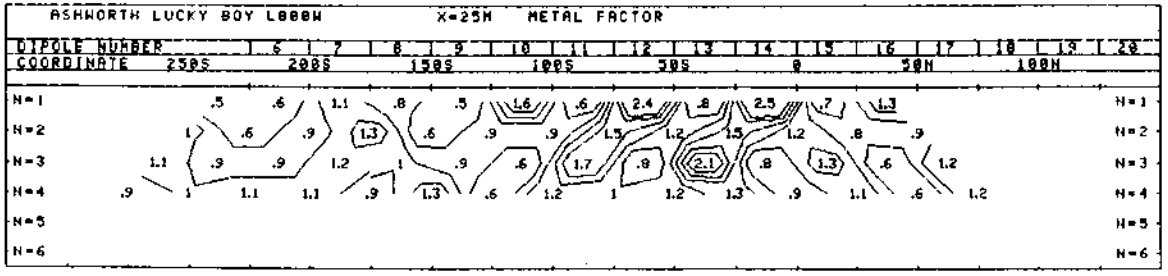
DATE SURVEYED FEB-88
APPROVED PAC
DATE FEB 27/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





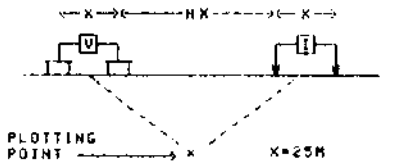


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D ,B C

LINE NO -750W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

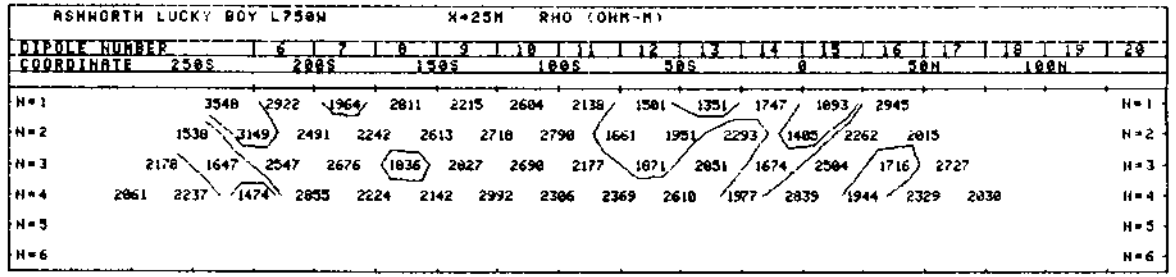
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1 5 -2,-3,-5,-7 5,-10 PLUS EACH 0.25 FROM 0 5 TO 2.0

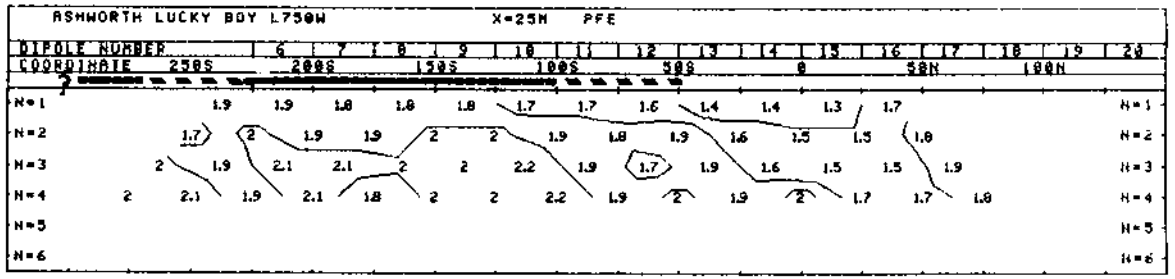
DWG NO I P -5666 11

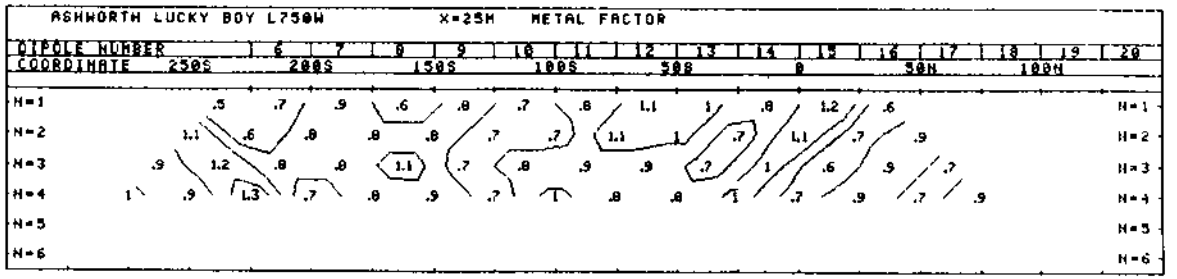
DATE SURVEYED FEB 88
APPROVED PAC
DATE FEB 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





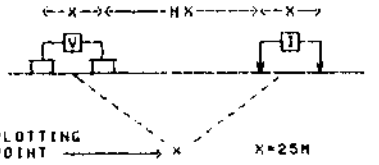


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D .B C

LINE NO -700N



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4.0.0 25

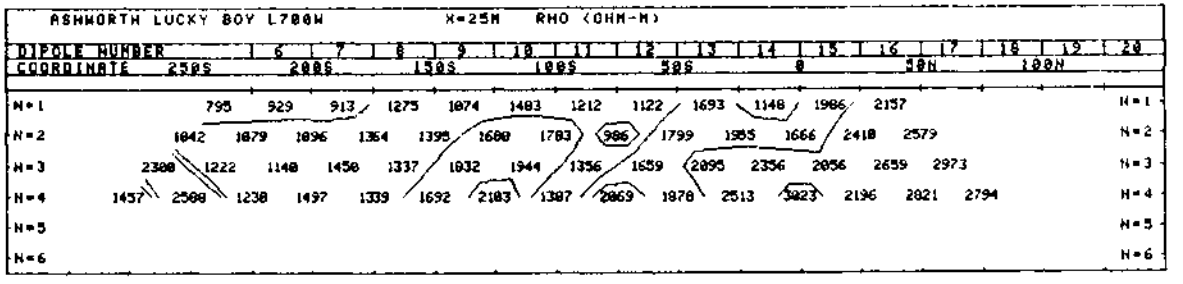
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7 5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

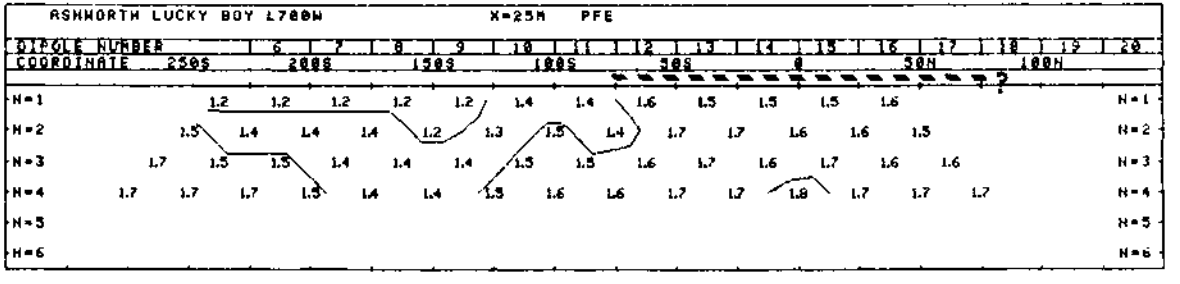
DWG NO -1 F 5866 I.

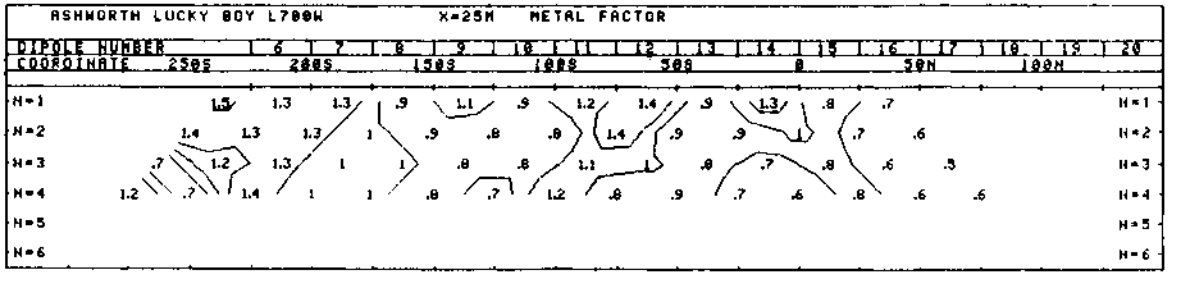
DATE SURVEYED FEB 88
APPROVED PAC
DATE FEB 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





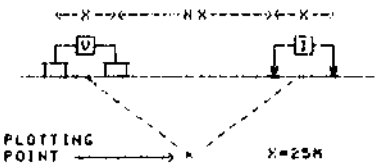


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D , B C.

LINE NO.-600N



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

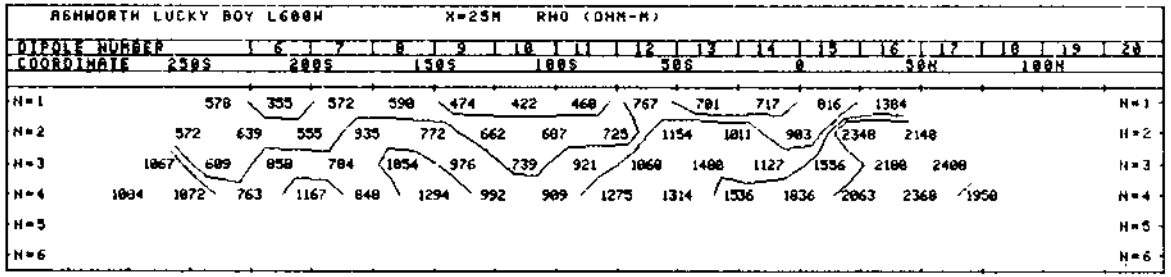
NOTE- CONTOURS AT LOGARITHMIC INTERVALS 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

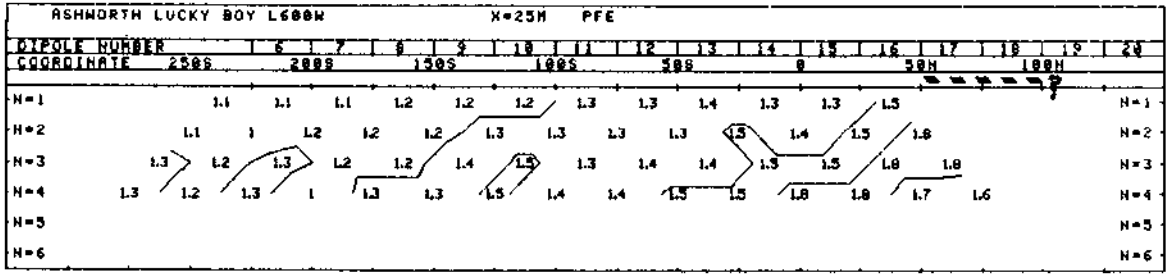
DDG NO -1 F -5688 13

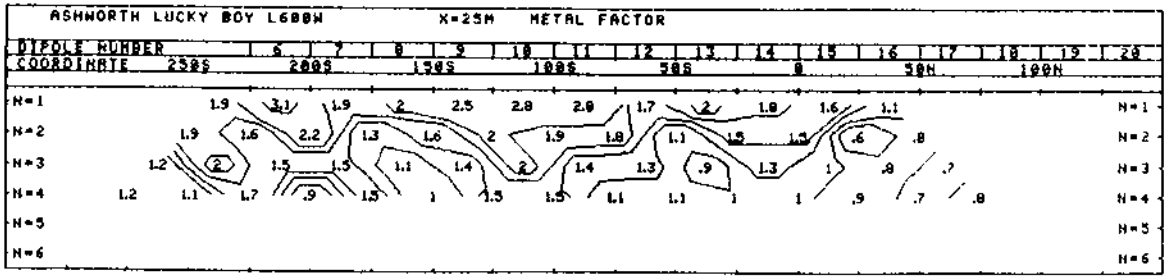
DATE SURVEYED FEB-68
APPROVED PAC
DATE FEB 29/68

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





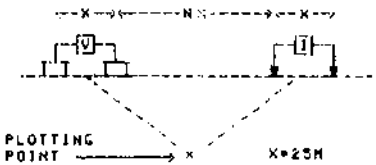


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D /B C.

LINE NO.-500W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0/8 25

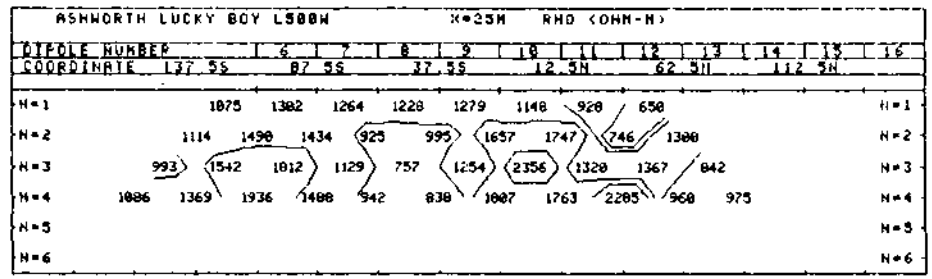
NOTE- CONTOURS AT LOGARITHMIC INTERVALS. 1,-1.5 -2,-3,-5,-7.5,-10 PLUS EACH 0.25 FROM 0.5 TO 2.0

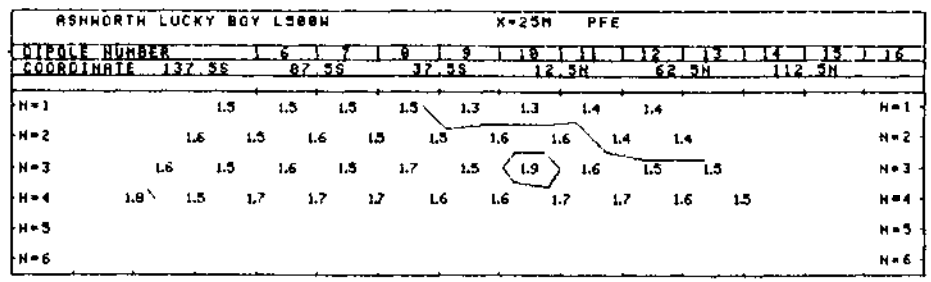
DWG NO -1 F 5800 14

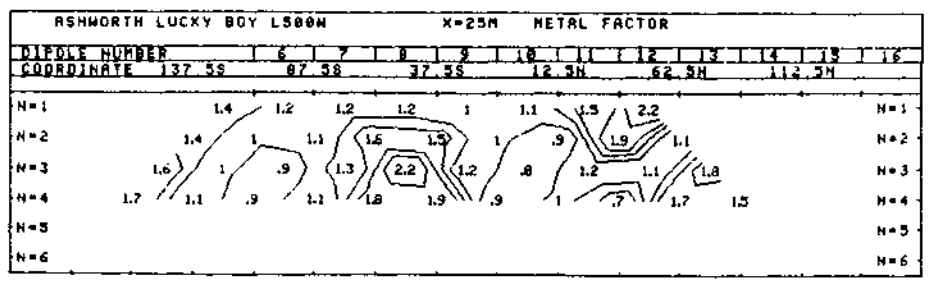
DATE SURVEYED FEB 88
APPROVED PAC
DATE FEB 29/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY





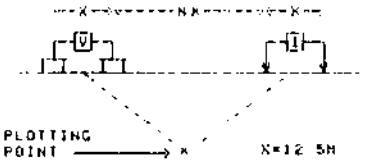


ASHWORTH EXPLORATIONS LIMITED

LUCKY BOY PROPERTY

GREENWOOD M D (B C

LINE NO -500W



SURFACE PROJECTION OF ANOMALOUS ZONE

DEFINITE
PROBABLE
POSSIBLE

FREQUENCY (HERTZ)
4 0.0 25

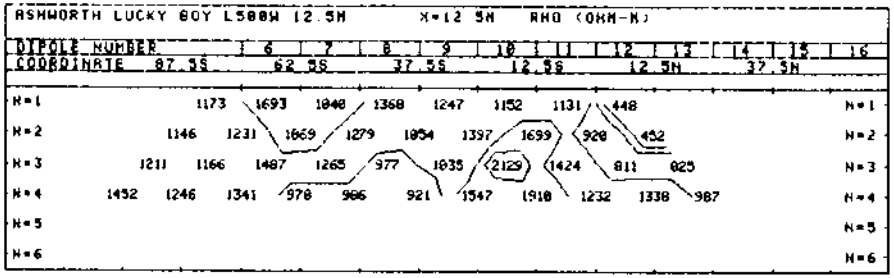
NOTE- CONTOURS
AT LOGARITHMIC
INTERVALS 1,-1 5
-2,-3,-5,-7 5,-10
PLUS EACH 0 25
FROM 0.5 TO 2 0

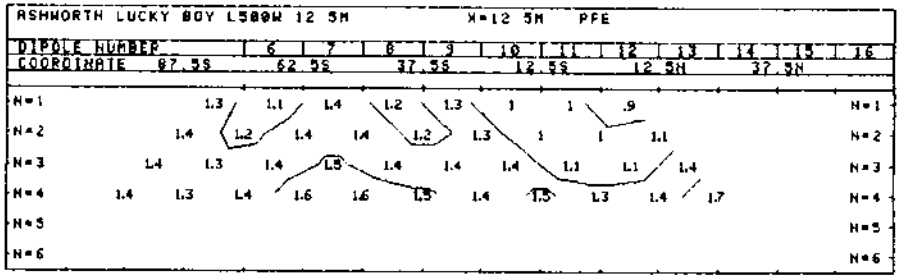
DWG NO I P 5-85 15

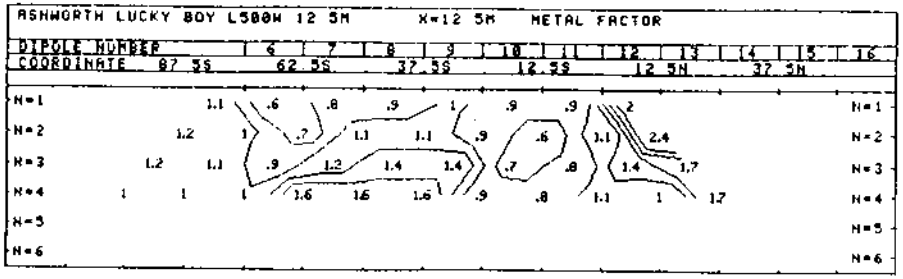
DATE SURVEYED FEB 88
APPROVED PAC
DATE FEB 24/88

PACIFIC GEOPHYSICAL LTD.

INDUCED POLARIZATION AND RESISTIVITY SURVEY







Legend

- FLAGGED GRID LINE (50m STATIONS)
- 300 — TOPOGRAPHICAL CONTOUR, INTERVAL 500 feet
- CREEK
- SECONDARY ROAD
- RAILWAY TRACK
- CROWN GRANTS, TWO POST CLAIM BOUNDARY
- CLAIM BOUNDARY AND LEGAL CORNER POST
- QUARTZ VEIN
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- AREA OF DETAILED ROCK SAMPLING

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
FELLOW

SCALE
0 100 200 300 400 METRES

MAP I

DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

SHOWINGS AND GRID MAP

Scale 1:5000	By F.Y. Drn. G.T.
Date February, 1988	NTS 92E6

Ashworth Explorations Limited

4000
3500
3000
4500
4000
L15W L14W L13W L12W L11W L10W L9W L8W L7W L6W L5W L4W L3W L2W L1W L0W
RAILWAY
WEST KETTLE RIVER
TL 500N
BASELINE 260°
THE NORTH SHOWING
py, gal, hem
cho, mal
gne
55°
THE RAT SHOWING
THE OLYMPIC SHOWING
THE LUCKY BOY SHOWING
py
cho
gal
mal
sph
THE SOUTH SHOWING
80°
THE BOUNDARY SHOWING
gal
py
cho
85°
P-1
P-2
P-3
P-4
P-5
R-9
R-10
R-101
R-102
R-103
R-104
R-105
R-3, R-4
R-12
R-13
R-14
chl.
ser.
65°
FL 5005
4000
3500
3000

Abbreviations

chl.	CHLORITIZATION	py	PYRITE
ser.	SERICITIZATION	cho	CHALCOPYRITE
mal	MALACHITE	gal	GALENA
sph	SPHALERITE	hem	HEMATITE
gne	GNEISSOSITY		

Legend

- FLAGGED GRID LINE (50m STATIONS)
- 300 — TOPOGRAPHICAL CONTOUR, INTERVAL 500 feet
- CREEK
- SECONDARY ROAD
- RAILWAY TRACK
- CROWN GRANTS, TWO POST CLAIM BOUNDARY
- CLAIM BOUNDARY AND LEGAL CORNER POST
- QUARTZ VEIN
- GRANITE, GRANODIORITE, QUARTZ MONZONITE
- SHEAR ZONE
- AREA OF OUTCROP
- 65° STRIKE AND DIP
- AREA OF DETAILED ROCK SAMPLING
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- R-10 ROCK SAMPLE LOCATION & SAMPLE NUMBER
- P-5 ROCK SAMPLE LOCATION (THIN SECTION)

GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
FELLOW

SCALE
0 100 200 300 400 500 METRES

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

MAP 2

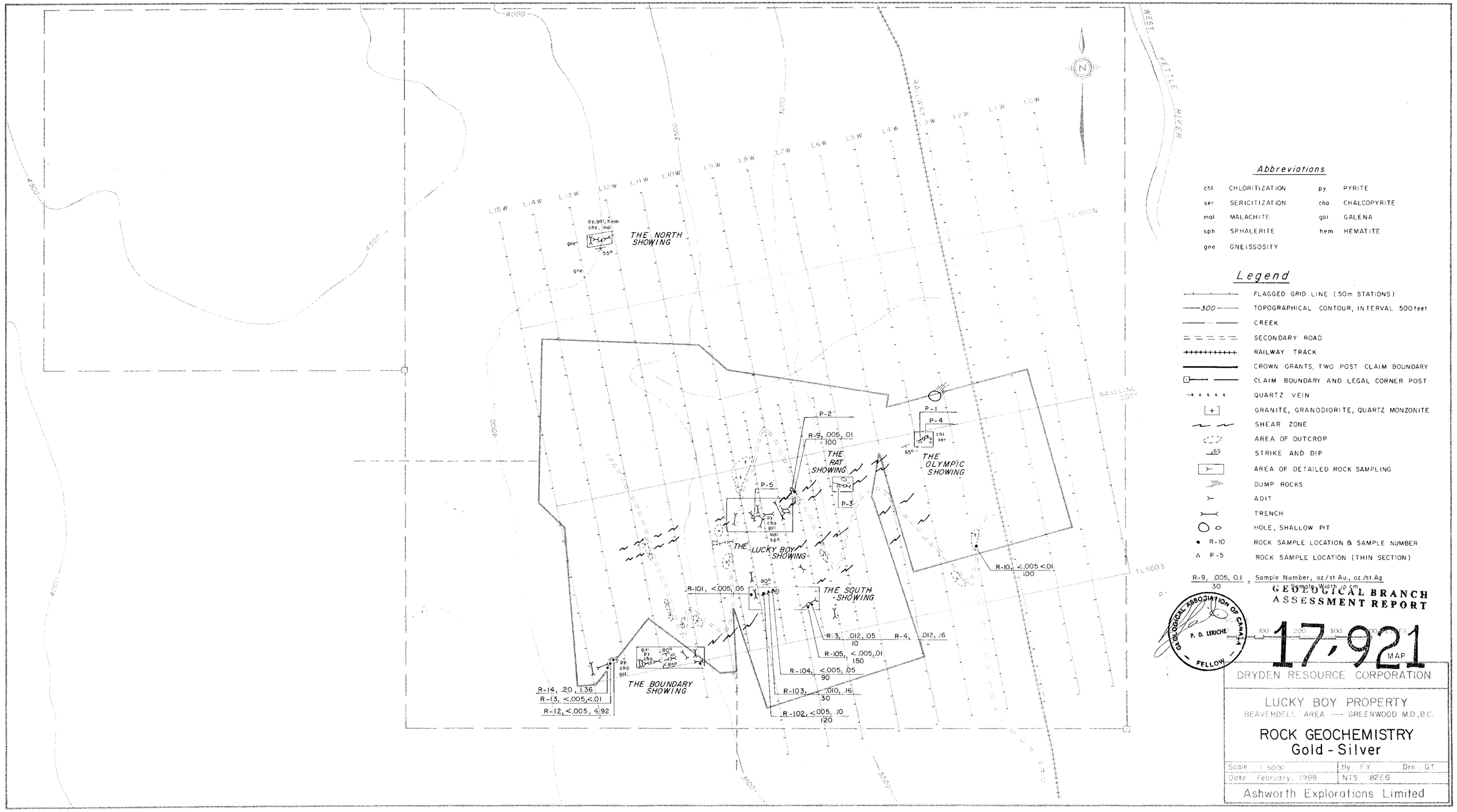
DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

GEOLOGY & ROCK SAMPLE LOCATIONS

Scale: 1:5000	By: F.Y. Drn: G.T.
Date: February, 1988	NTS 82E6

Ashworth Explorations Limited



Abbreviations

chl.	CHLORITIZATION	py	PYRITE
ser.	SERICITIZATION	cha	CHALCOPYRITE
mal	MALACHITE	gal	GALENA
sph	SPHALERITE	hem	HEMATITE
gne	GNEISSOSITY		

Legend

- FLAGGED GRID LINE (50m STATIONS)
- 300 — TOPOGRAPHICAL CONTOUR, INTERVAL 500 feet
- CREEK
- SECONDARY ROAD
- RAILWAY TRACK
- CROWN GRANTS, TWO POST CLAIM BOUNDARY
- CLAIM BOUNDARY AND LEGAL CORNER POST
- QUARTZ VEIN
- GRANITE, GRANODIORITE, QUARTZ MONZONITE
- SHEAR ZONE
- AREA OF OUTCROP
- STRIKE AND DIP
- AREA OF DETAILED ROCK SAMPLING
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- R-10 ROCK SAMPLE LOCATION & SAMPLE NUMBER
- P-5 ROCK SAMPLE LOCATION (THIN SECTION)

R-9, .005, 0.1 / 30 = Sample Number, oz/st Au., oz/st Ag / Sample Width 10 cm.

GEOLOGICAL ASSOCIATION OF CANADA — P. D. LERICHE — FELLOW

0 100 200 300 400 500 FEET

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

MAP

DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

ROCK GEOCHEMISTRY
Gold - Silver

Scale 1:5000	By. F.Y. Drn. G.T.
Date February, 1988	NTS 82E6

Ashworth Explorations Limited

Overstaked Claim Boundary

THE NORTH SHOWING

THE RAT SHOWING

THE OLYMPIC SHOWING

THE LUCKY BOY SHOWING

THE SOUTH SHOWING

THE BOUNDARY SHOWING

RAILWAY

WEST KETTLE RIVER

BASELINE 280°

TL 600N

TL 500S

R-9, 33, 49, 174
100

R-10, 25, 30, 92
100

R-101, 274, 74, 161

R-3, 296, 116, 427
10

R-4, 430, 23, 141

R-105, 26, 9, 97
150

R-104, 64, 42, 31
90

R-103, 77, 70, 128
30

R-102, 26, 101, 70
120

R-14, 571, 118, 384

R-13, 150, 51, 394

R-12, 7714, 191, 41479

Abbreviations

chl.	CHLORITIZATION	py	PYRITE
ser.	SERICITIZATION	cha	CHALCOPYRITE
mal	MALACHITE	gal	GALENA
sph	SPHALERITE	hem	HEMATITE
gne	GNEISSOSITY		

Legend

- FLAGGED GRID LINE (50m STATIONS)
- 300 TOPOGRAPHICAL CONTOUR, INTERVAL 500 feet
- CREEK
- SECONDARY ROAD
- RAILWAY TRACK
- CROWN GRANTS, TWO POST CLAIM BOUNDARY
- CLAIM BOUNDARY AND LEGAL CORNER POST
- QUARTZ VEIN
- GRANITE, GRANODIORITE, QUARTZ MONZONITE
- SHEAR ZONE
- AREA OF OUTCROP
- 65° STRIKE AND DIP
- AREA OF DETAILED ROCK SAMPLING
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- R-10 ROCK SAMPLE LOCATION & SAMPLE NUMBER
- P-5 ROCK SAMPLE LOCATION (THIN SECTION)

R-9, 33, 49, 174 / 100 — Sample Number, Cu/ppm, Pb/ppm, Zn/ppm / Grade Width in cm

SCALE 100 200 300 400 METRES

GEOLOGICAL ASSOCIATION OF CANADA — P. D. LERICHE — FELLOW

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

MAP 4

DRYDEN RESOURCE CORPORATION

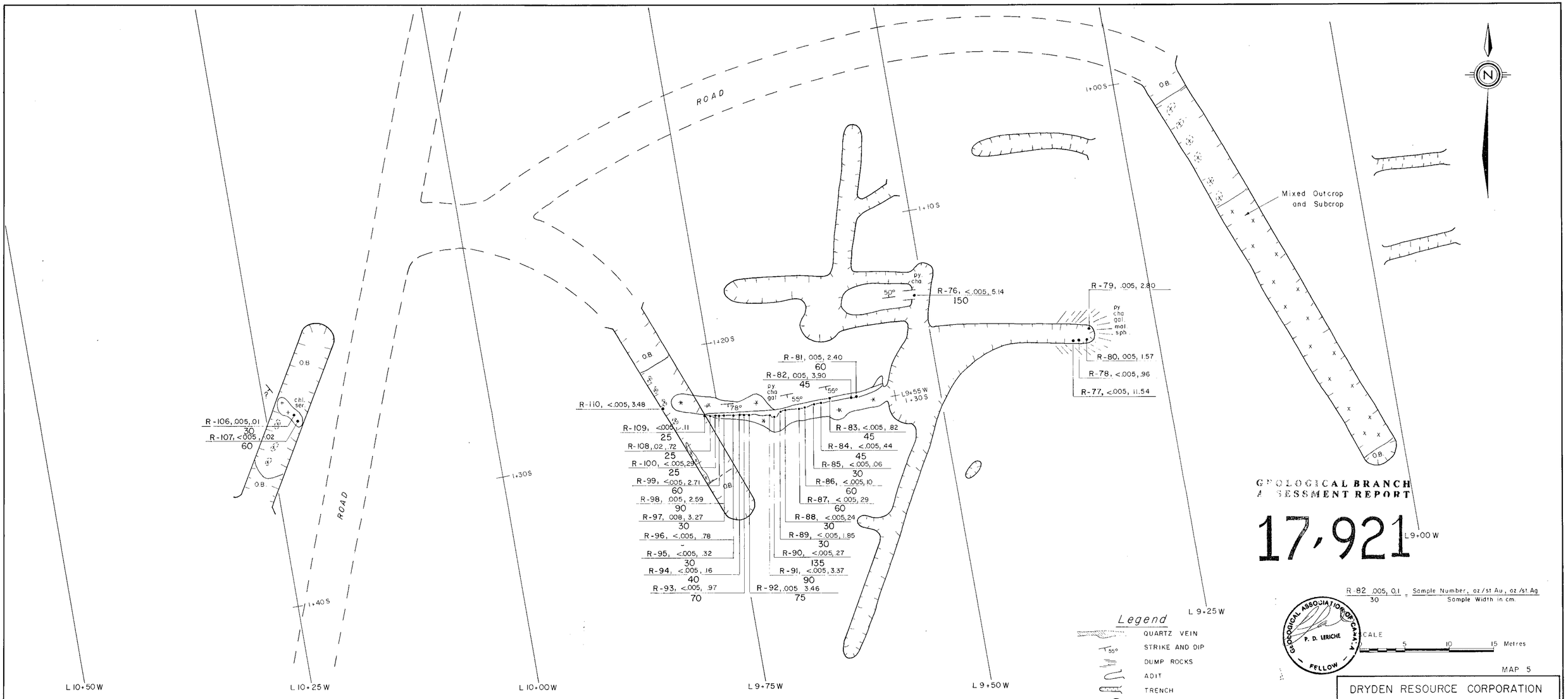
LUCKY BOY PROPERTY

BEAVERDELL AREA — GREENWOOD M.D., B.C.

ROCK GEOCHEMISTRY
Copper, Lead & Zinc

Scale 1:5000	By F.Y. Drn. G.T.
Date February, 1988	NTS 82E6

Ashworth Explorations Limited



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

R-82 .005, 0.1 = Sample Number, oz/st Au, oz/st Ag
30 = Sample Width in cm.

GEOLOGICAL ASSOCIATION OF CANADA — P. D. LERICHE — FELLOW

SCALE 0 5 10 15 Metres

MAP 5

Legend

- QUARTZ VEIN
- 55° STRIKE AND DIP
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- R-90 ROCK SAMPLE LOCATION & SAMPLE NUMBER
- OUTCROP, SUBCROP IN TRENCH
- x x BIOTITE HORNBLEND GRANITE IN ADIT

chl.	CHLORITIZATION	py	PYRITE
ser.	SERICITIZATION	cha	CHALCOPYRITE
mal	MALACHITE	gal	GALENA
sph	SPHALERITE		

DRYDEN RESOURCE CORPORATION

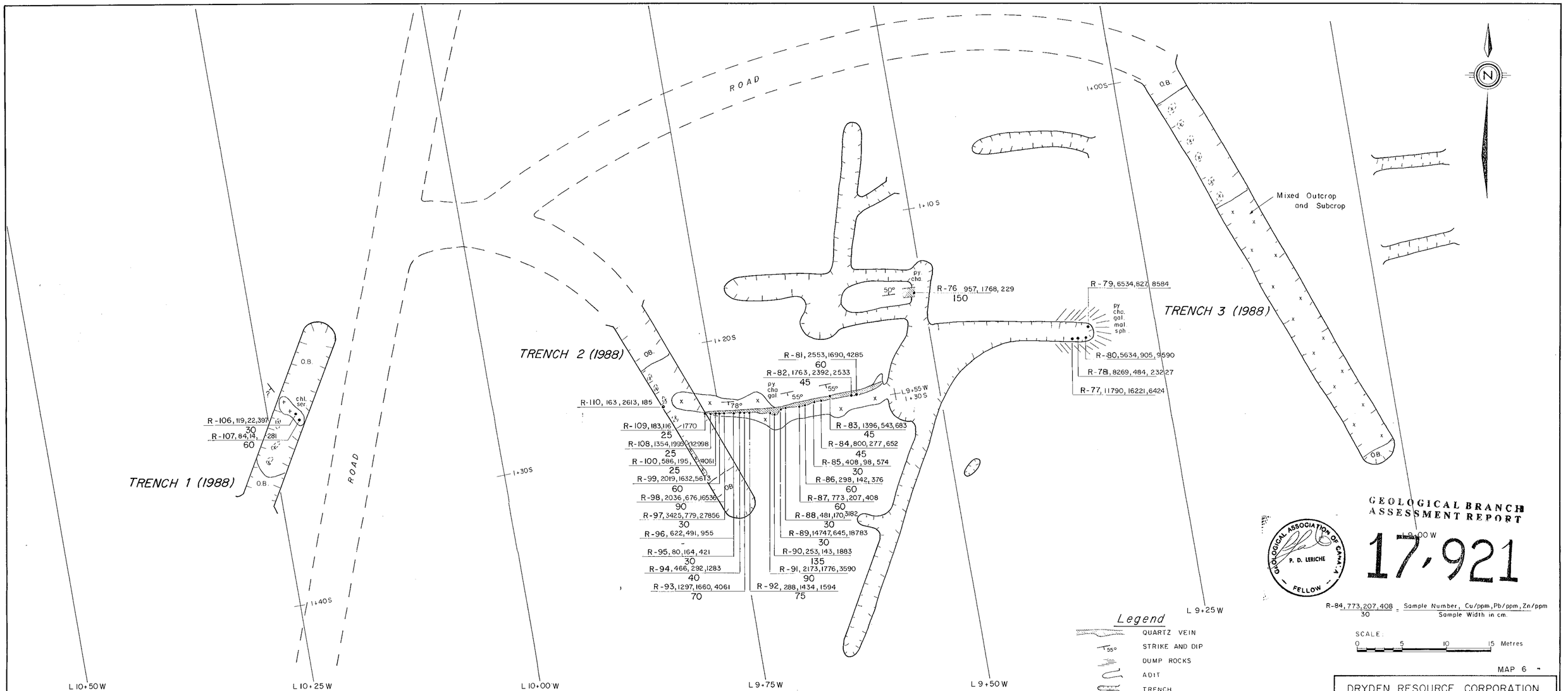
LUCKY BOY PROPERTY

BEAVERDELL AREA — GREENWOOD M.D., B.C.

LUCKY BOY SHOWING
PLAN AND ASSAY RESULTS
Gold - Silver

Scale: 1: 200	By: F.Y. Drn.: G.T.
Date: February, 1988	NTS 82E6

Ashworth Explorations Limited



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA — P. D. LERICHE — FELLOW

R-84, 773, 207, 408 / 30 = Sample Number, Cu/ppm, Pb/ppm, Zn/ppm / Sample Width in cm.

SCALE
0 5 10 15 Metres

Legend

- QUARTZ VEIN
- 55° STRIKE AND DIP
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- R-90 ROCK SAMPLE LOCATION & SAMPLE NUMBER
- OUTCROP, SUBCROP IN TRENCH
- x x BIOTITE HORNBLEND GRANITE IN ADIT

chl.	CHLORITIZATION	py	PYRITE
ser.	SERICITIZATION	cha	CHALCOPYRITE
mal	MALACHITE	gal	GALENA
sph	SPHALERITE		

MAP 6

DRYDEN RESOURCE CORPORATION

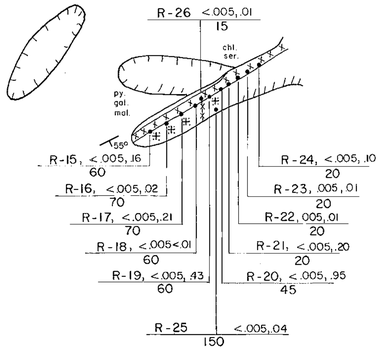
LUCKY BOY PROPERTY

BEAVERDELL AREA — GREENWOOD M.D., B.C.

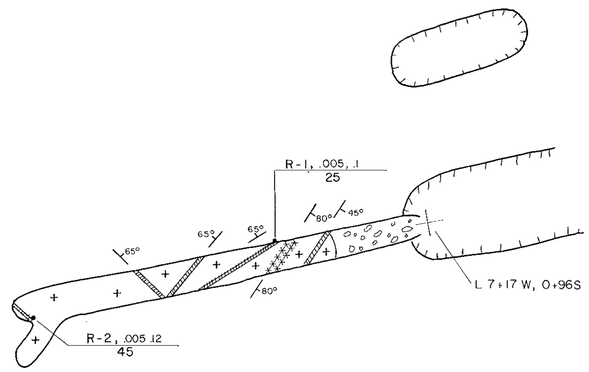
LUCKY BOY SHOWING
PLAN AND ASSAY RESULTS
Copper, Lead & Zinc

Scale: 1: 200	By: F.Y. Drn: G.T.
Date: February, 1988	NTS 82E6

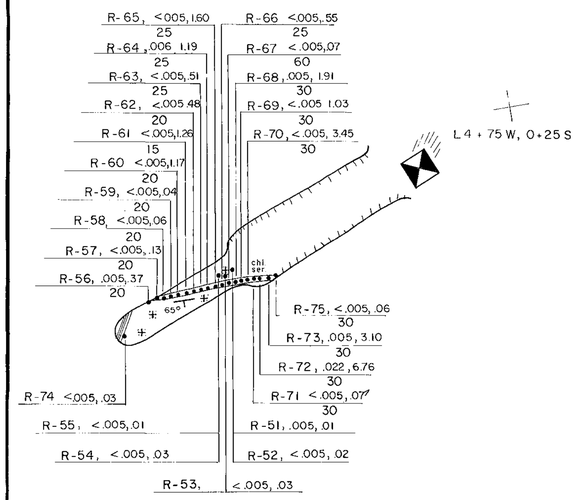
Ashworth Explorations Limited



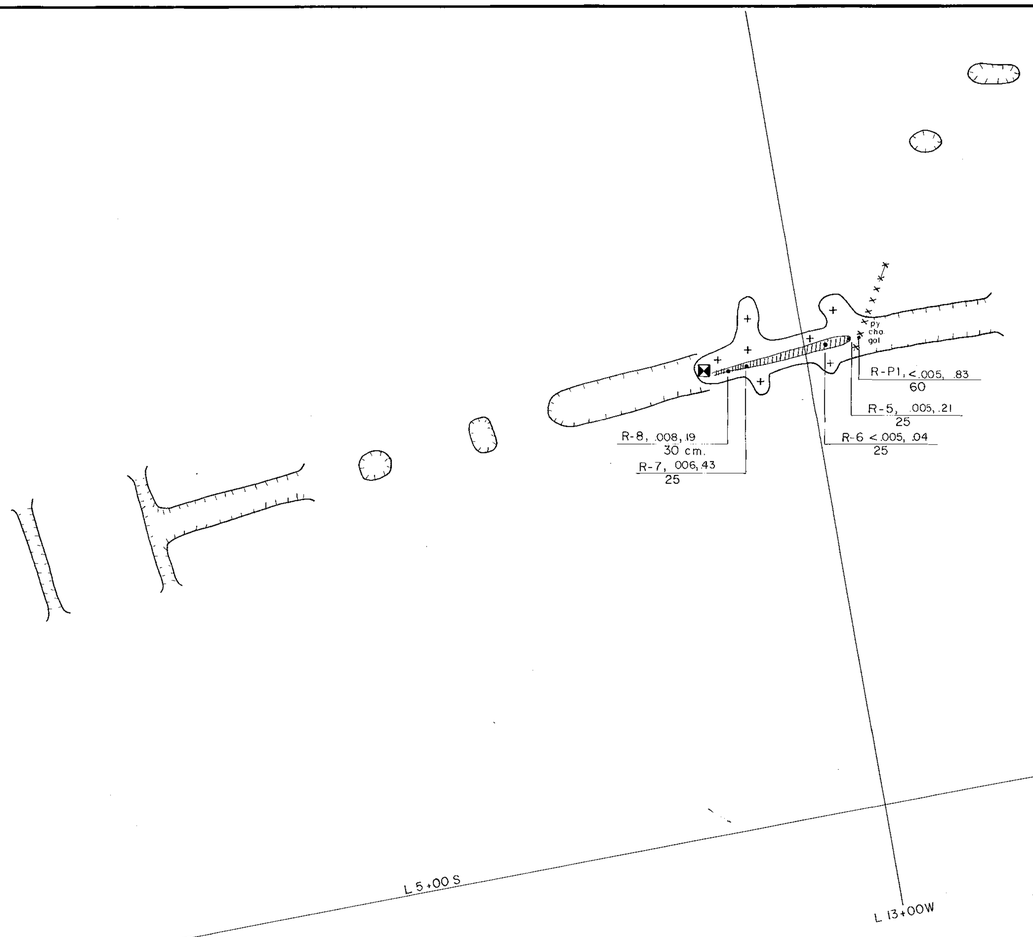
THE NORTH SHOWING



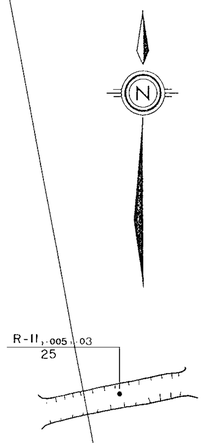
THE RAT SHOWING



THE OLYMPIC SHOWING



THE BOUNDARY SHOWING



L 7+00 W

L 12+50 W

L 12+00 W

Legend

- 65° STRIKE AND DIP
- SHEAR ZONE
- SHAFT
- SECONDARY ROAD
- QUARTZ VEIN
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- • R-20 ROCK SAMPLE LOCATION & SAMPLE NUMBER
- GRAVEL, SAND AND ALLUVIUM
- ALTERED GRANITIC ROCK IN ADIT
- + + BIOTITE HORNBLEND GRANITE IN ADIT

Abbreviations

chl.	CHLORITIZATION
ser.	SERICITIZATION
mal	MALACHITE
py	PYRITE
cha	CHALCOPYRITE
gal.	GALENA

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
FELLOW

R-72, .022,6.76 / 30 = Sample Number, oz/st Au, oz/st Ag / Sample Width in cm.

SCALE
0 5 10 15 Metres

MAP 7

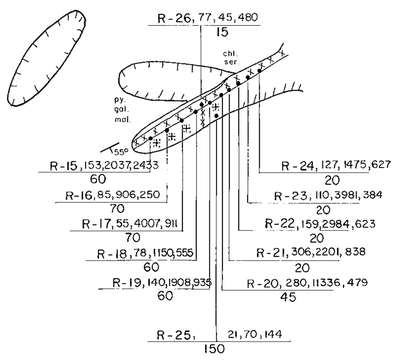
DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

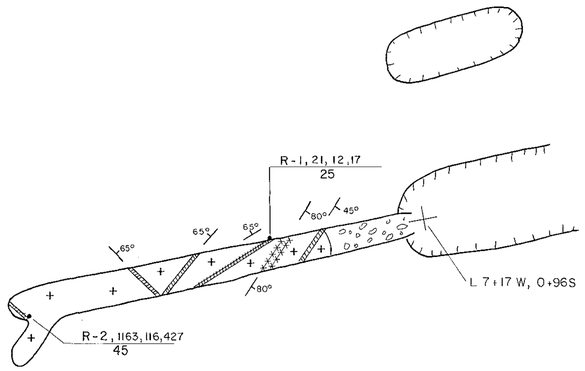
OLD SHOWINGS
PLAN AND ASSAY RESULTS
Gold - Silver

Scale: 1: 200	By: F.Y. Drn: G.T.
Date: February, 1988	NTS 82E6

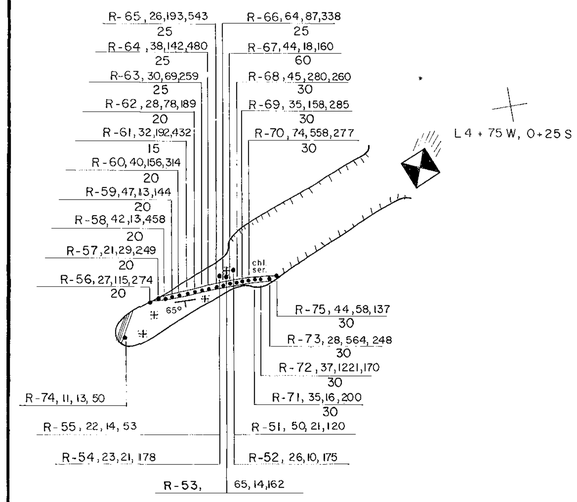
Ashworth Explorations Limited



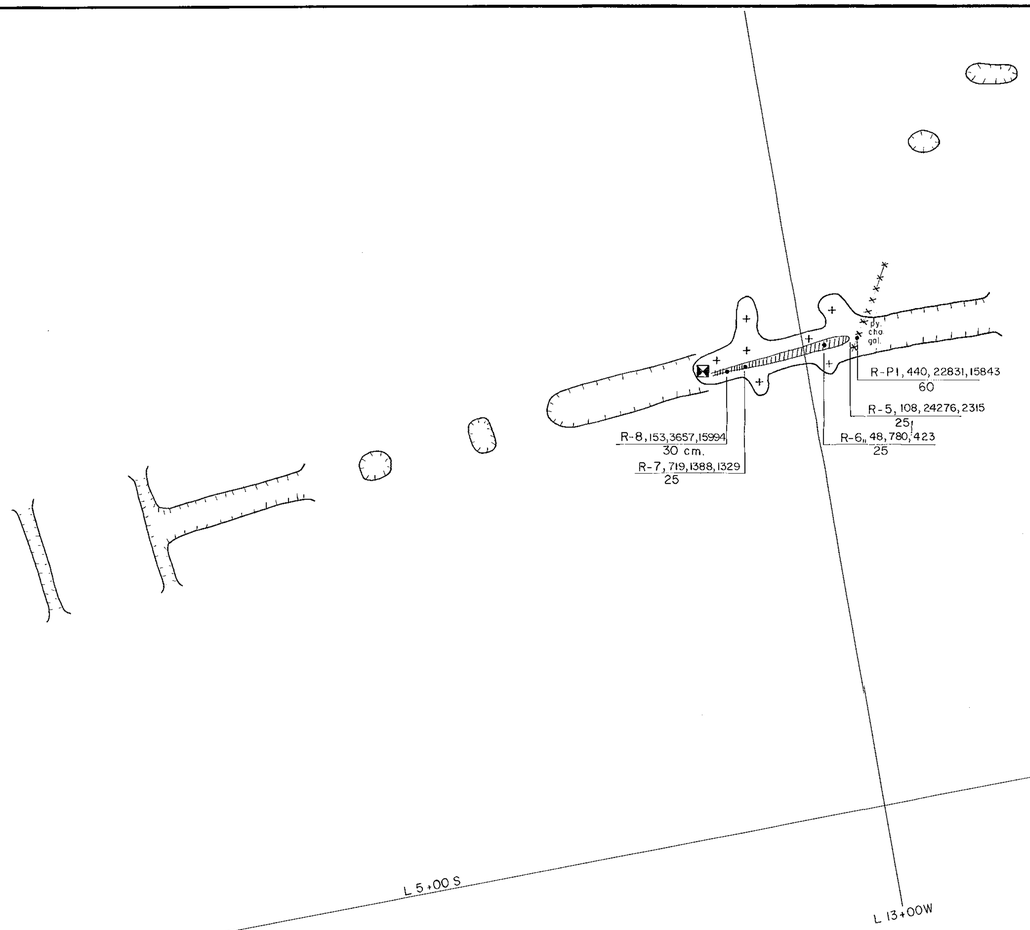
THE NORTH SHOWING



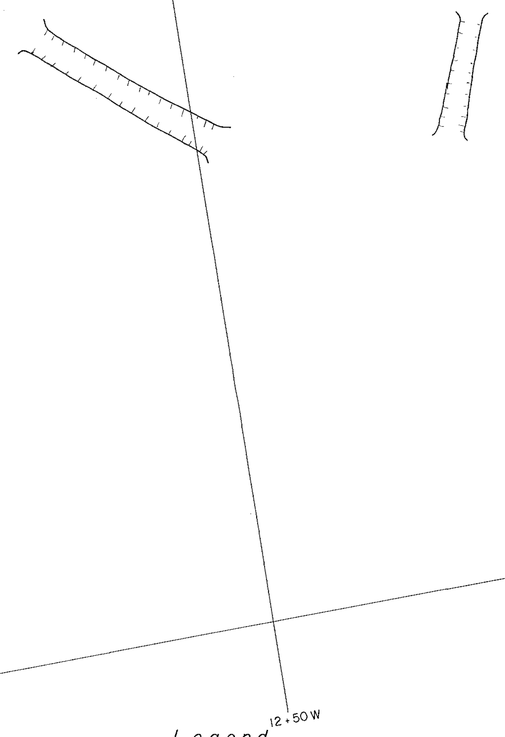
THE RAT SHOWING

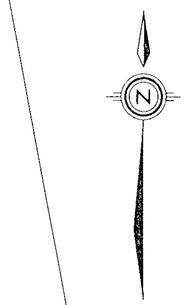


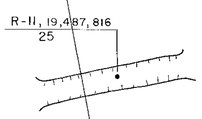
THE OLYMPIC SHOWING



THE BOUNDARY SHOWING







L 12+00W

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
FELLOW

R-5, 108, 24276, 2315 / 30 = Sample Number, Cu/ppm, Pb/ppm, Zn/ppm / Sample Width in cm.

SCALE
0 5 10 15 Metres

Legend

- STRIKE AND DIP
- SHEAR ZONE
- SHAFT
- SECONDARY ROAD
- QUARTZ VEIN
- DUMP ROCKS
- ADIT
- TRENCH
- HOLE, SHALLOW PIT
- R-20 ROCK SAMPLE LOCATION & SAMPLE NUMBER
- GRAVEL, SAND AND ALLUVIUM
- ALTERED GRANITIC ROCK IN ADIT
- BIOTITE HORNBLENDE GRANITE IN ADIT

Abbreviations

- chl. CHLORITIZATION
- ser. SERICITIZATION
- mal MALACHITE
- py PYRITE
- cha CHALCOPYRITE
- gal. GALENA

MAP 8

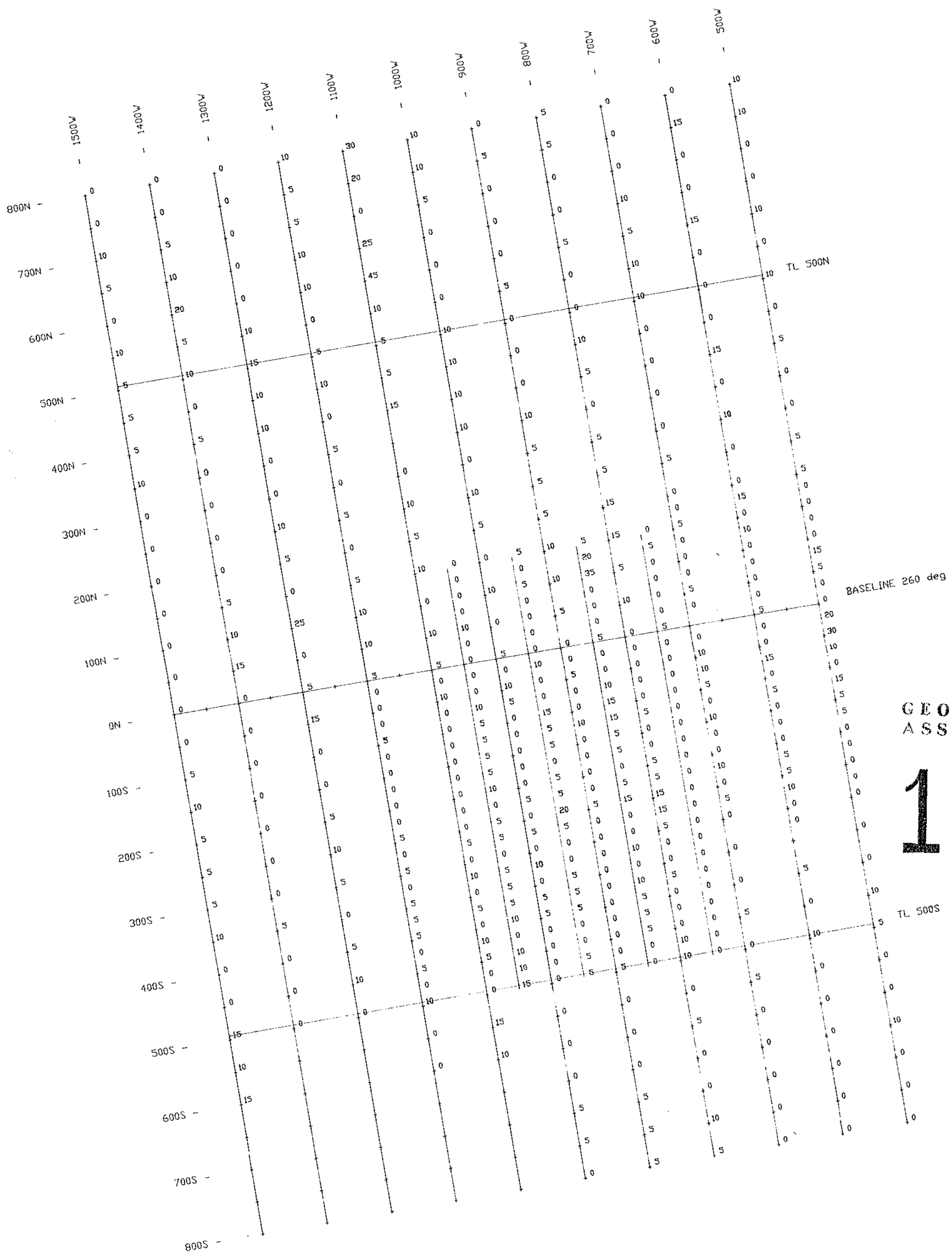
DRYDEN RESOURCE CORPORATION

LUCKY BOY PROPERTY
BEAVERDELL AREA — GREENWOOD M.D., B.C.

OLD SHOWINGS
PLAN AND ASSAY RESULTS
Copper Lead & Zinc

Scale: 1:200	By: F.Y. Drn: G.T.
Date: February, 1988	NTS 82E6

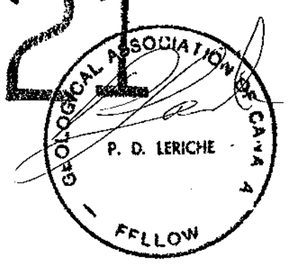
Ashworth Explorations Limited



N

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921



0 100 200 300 400 500

metres

MAP 9

DRYDEN RESOURCE CORPORATION

ASHWORTH EXPLORATIONS LIMITED
LUCKY BOY PROJECT
Beaverdell Area

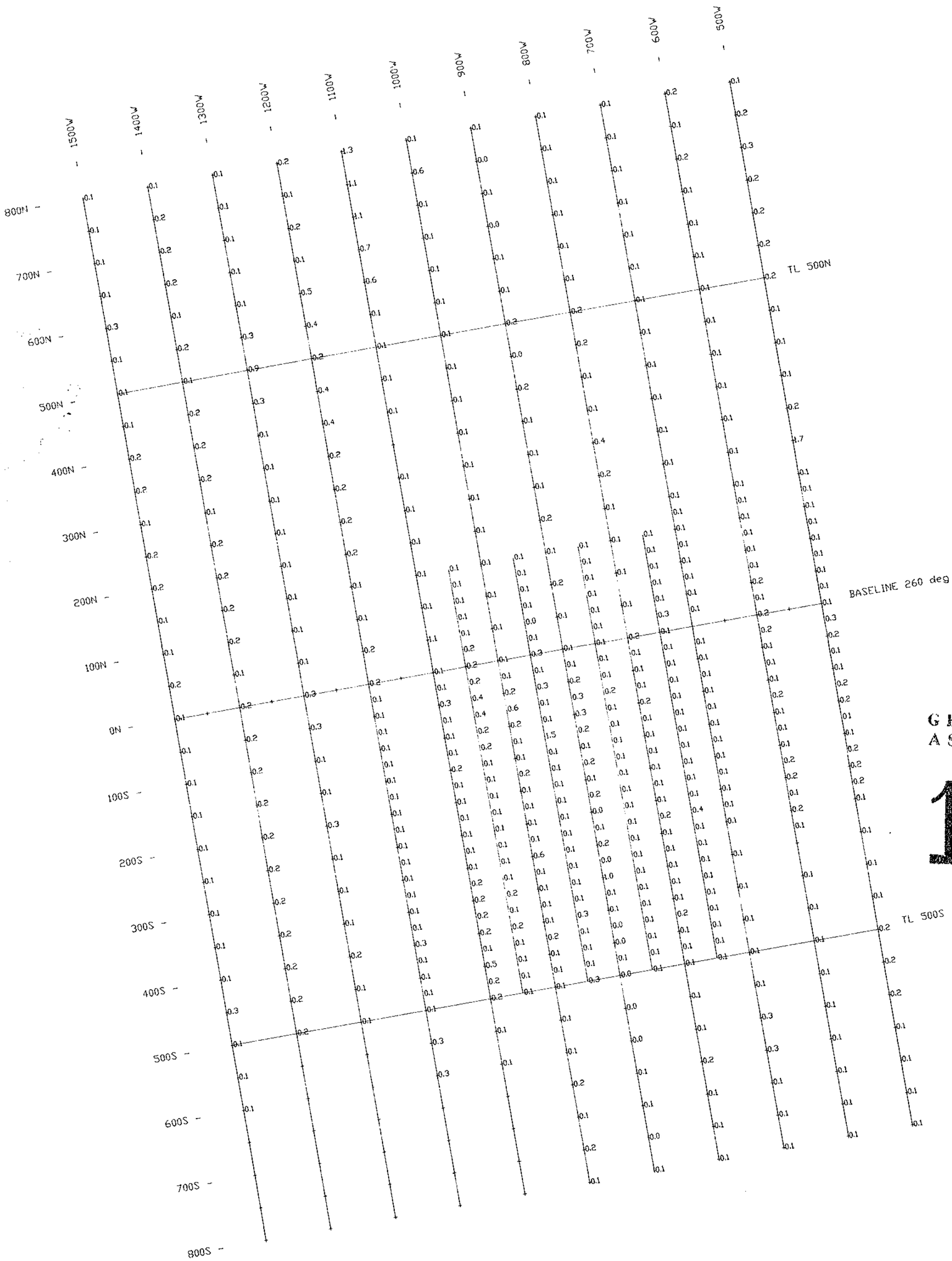
SOIL GEOCHEMISTRY

Gold

Greenwood M.D. N.T.S. 82E/6

DATE: 18 March 1988 SCALE: 1 : 5000

DRAWN BY: Tony Clark Consulting



N

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
FELLOW

0 100 200 300 400 500
metres

MAP 10

DRYDEN RESOURCE CORPORATION

ASHWORTH EXPLORATIONS LIMITED
LUCKY BOY PROJECT
Beaverdell Area

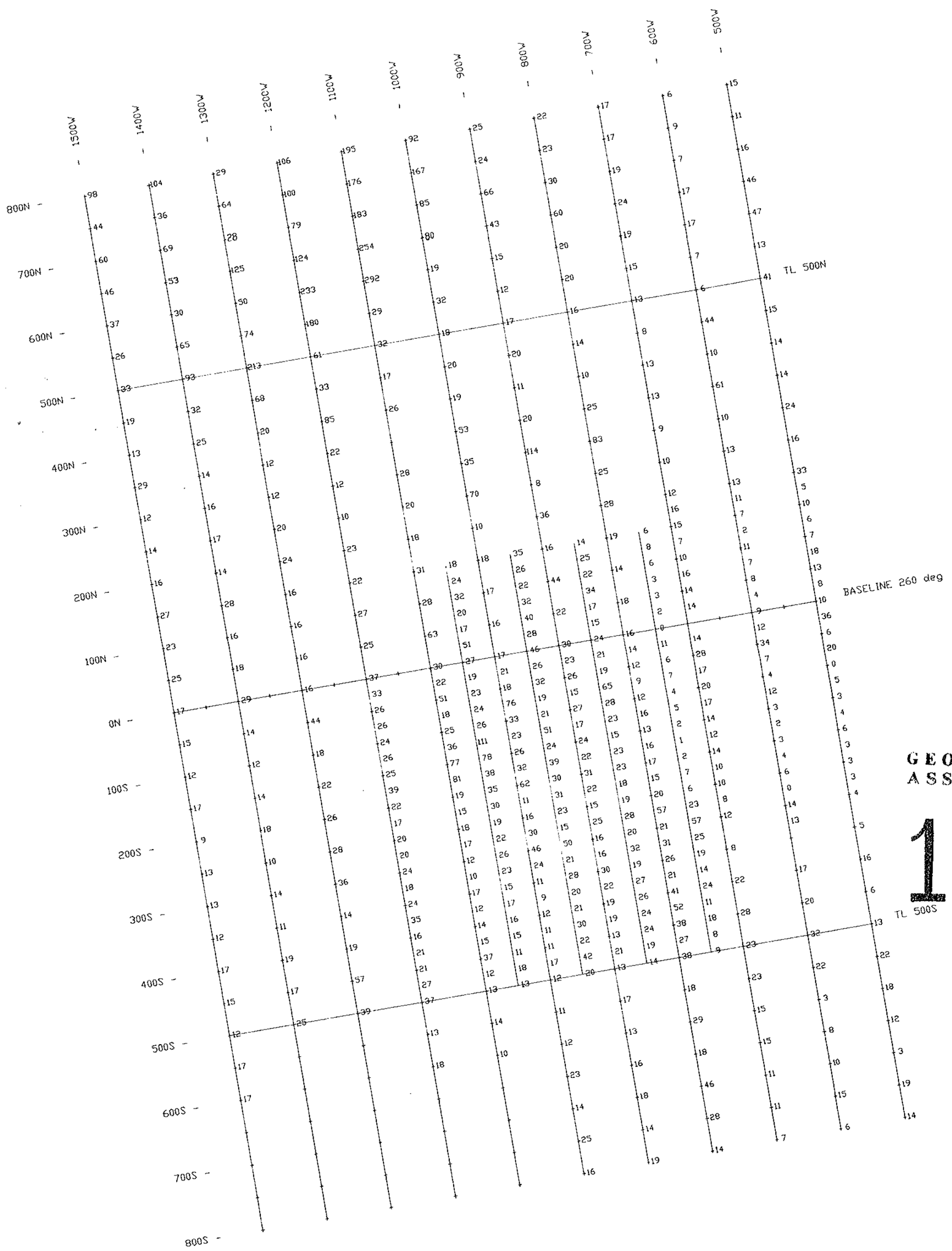
SOIL GEOCHEMISTRY

Silver

Greenwood M.D. N.T.S. 82E/6

DATE: 18 March 1988 | SCALE: 1 : 5000

DRAWN BY: Tony Clark Consulting



N

42 Cu ppm

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA — P. D. JERICHE — FELLOW

0 100 200 300 400 500

metres

MAP II

DRYDEN RESOURCE CORPORATION

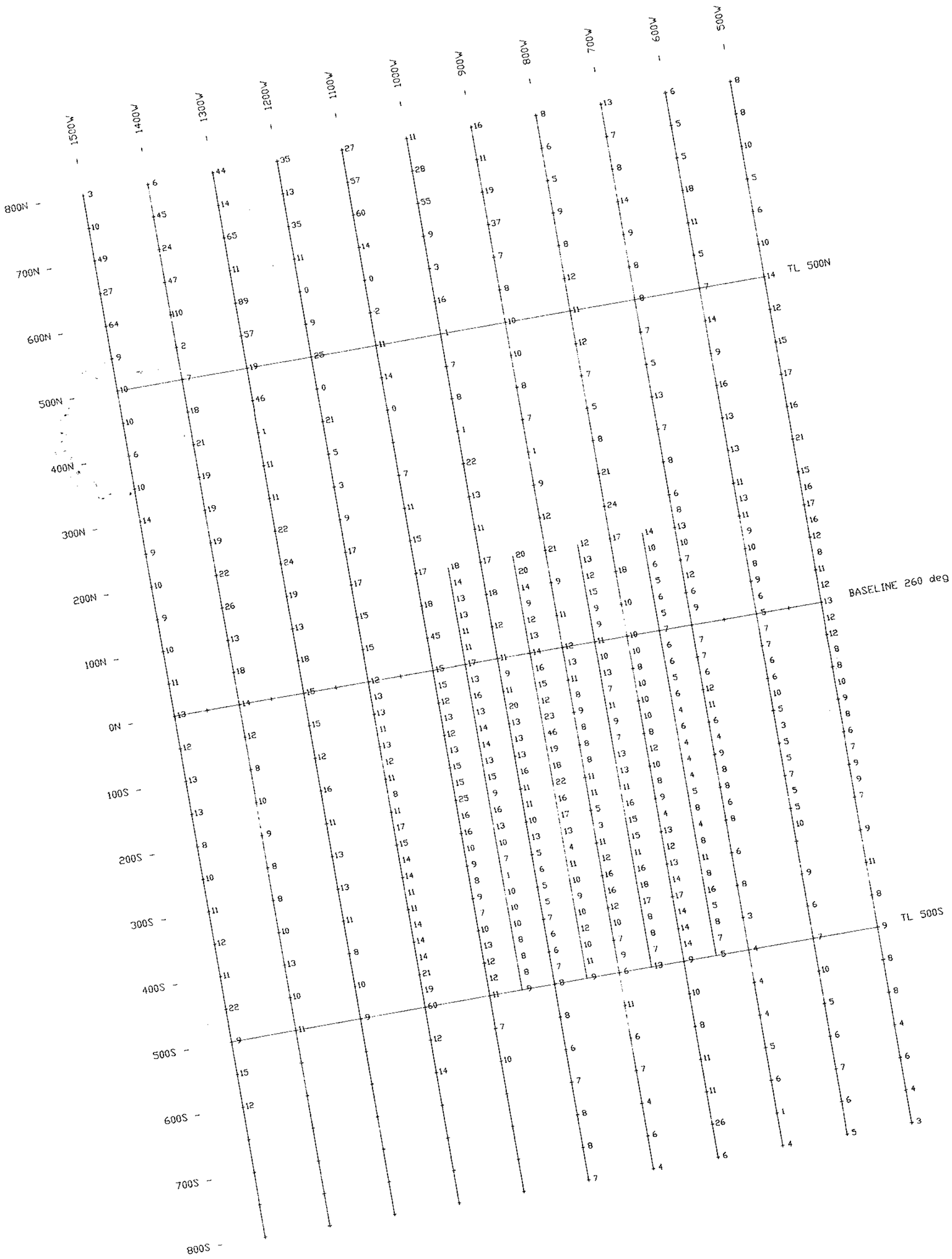
ASHWORTH EXPLORATIONS LIMITED
LUCKY BOY PROJECT
Beaverdell Area

SOIL GEOCHEMISTRY
Copper

Greenwood M.D. N.T.S. 82E/6

DATE: 18 March 1988 | SCALE: 1 : 5000

DRAWN BY: Tony Clark Consulting



N

32 Pb ppm

0 100 200 300 400 500

metres

MAP 12

DRYDEN RESOURCE CORPORATION

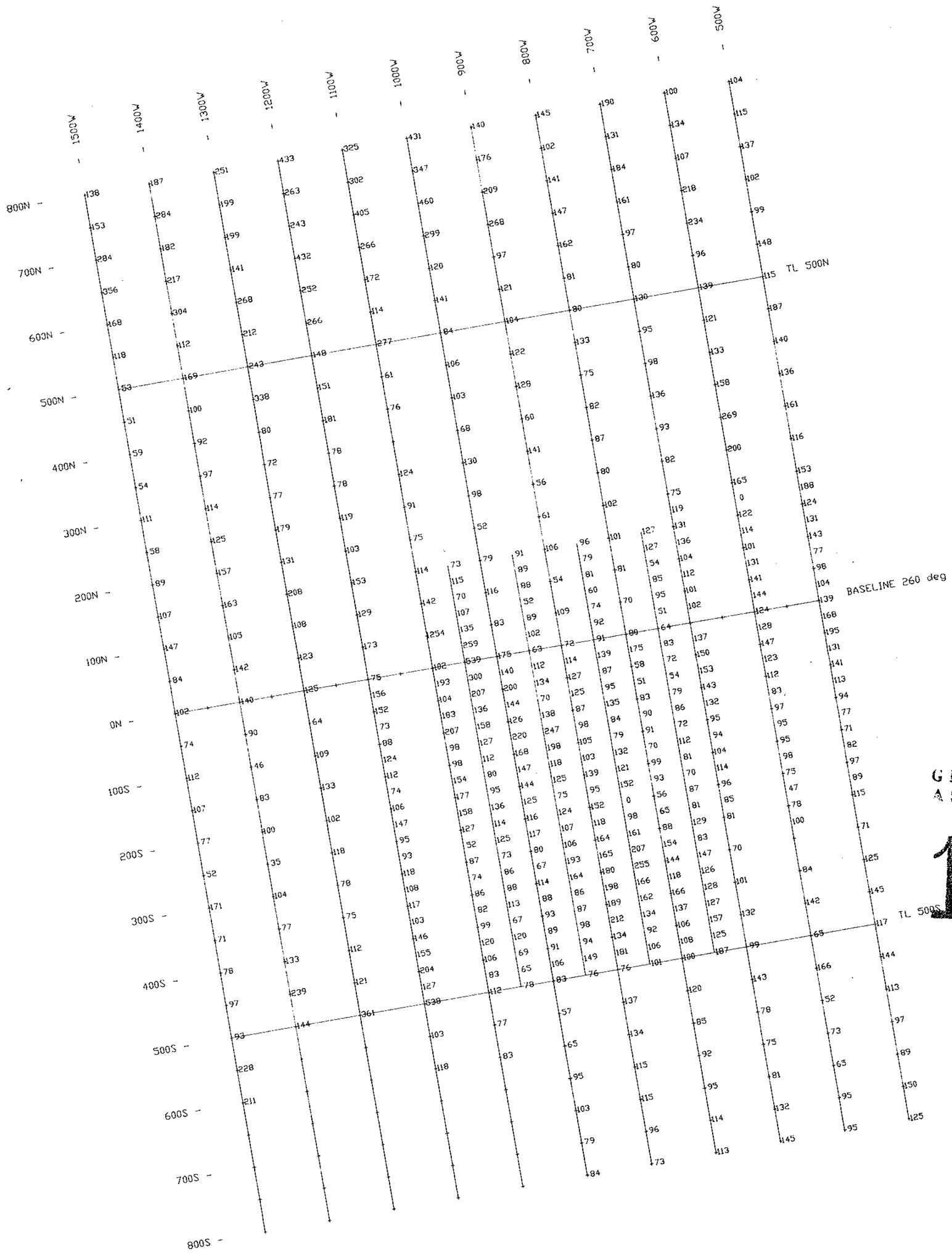
ASHWORTH EXPLORATIONS LIMITED
LUCKY BOY PROJECT
Beaverdell Area

SOIL GEOCHEMISTRY

Greenwood M.D. Lead N.T.S. 82E/6

DATE: 18 March 1988 | SCALE: 1 : 5000

DRAWN BY: Tony Clark Consulting



N

251 Zn ppm

0 100 200 300 400 500

metres

MAP 13

DRYDEN RESOURCE CORPORATION

ASHWORTH EXPLORATIONS LIMITED
LUCKY BOY PROJECT
Beaverdell Area

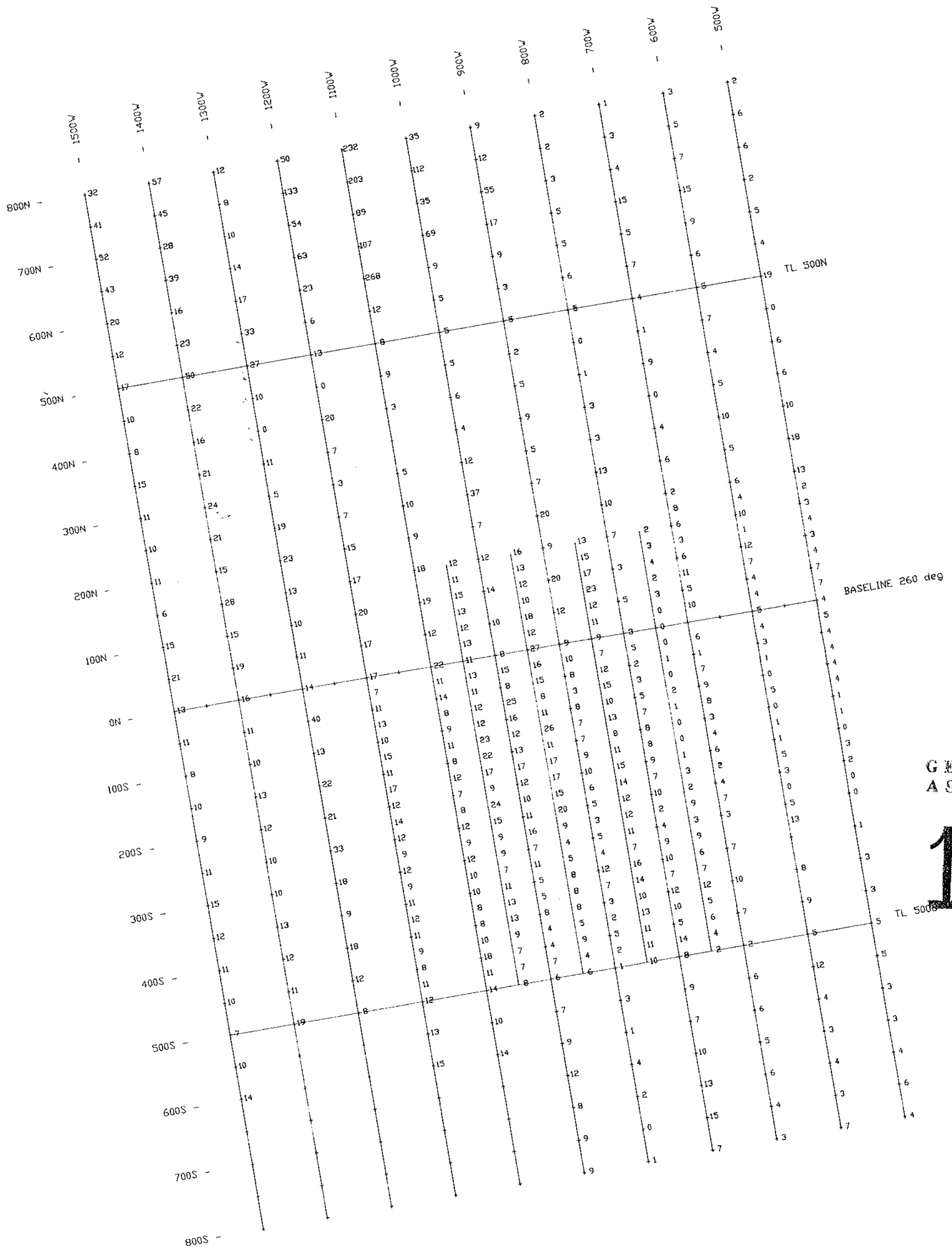
SOIL GEOCHEMISTRY

Zinc

Greenwood M.D. N.T.S. 82E/6

DATE: 18 March 1988 | SCALE: 1 : 5000

DRAWN BY: Tony Clark Consulting



N

23 As ppm

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA
D. LERICHE
FELLOW

0 100 200 300 400 500

metres

MAP 14

DRYDEN RESOURCE CORPORATION

ASHWORTH EXPLORATIONS LIMITED
LUCKY BOY PROJECT
Beaverdell Area

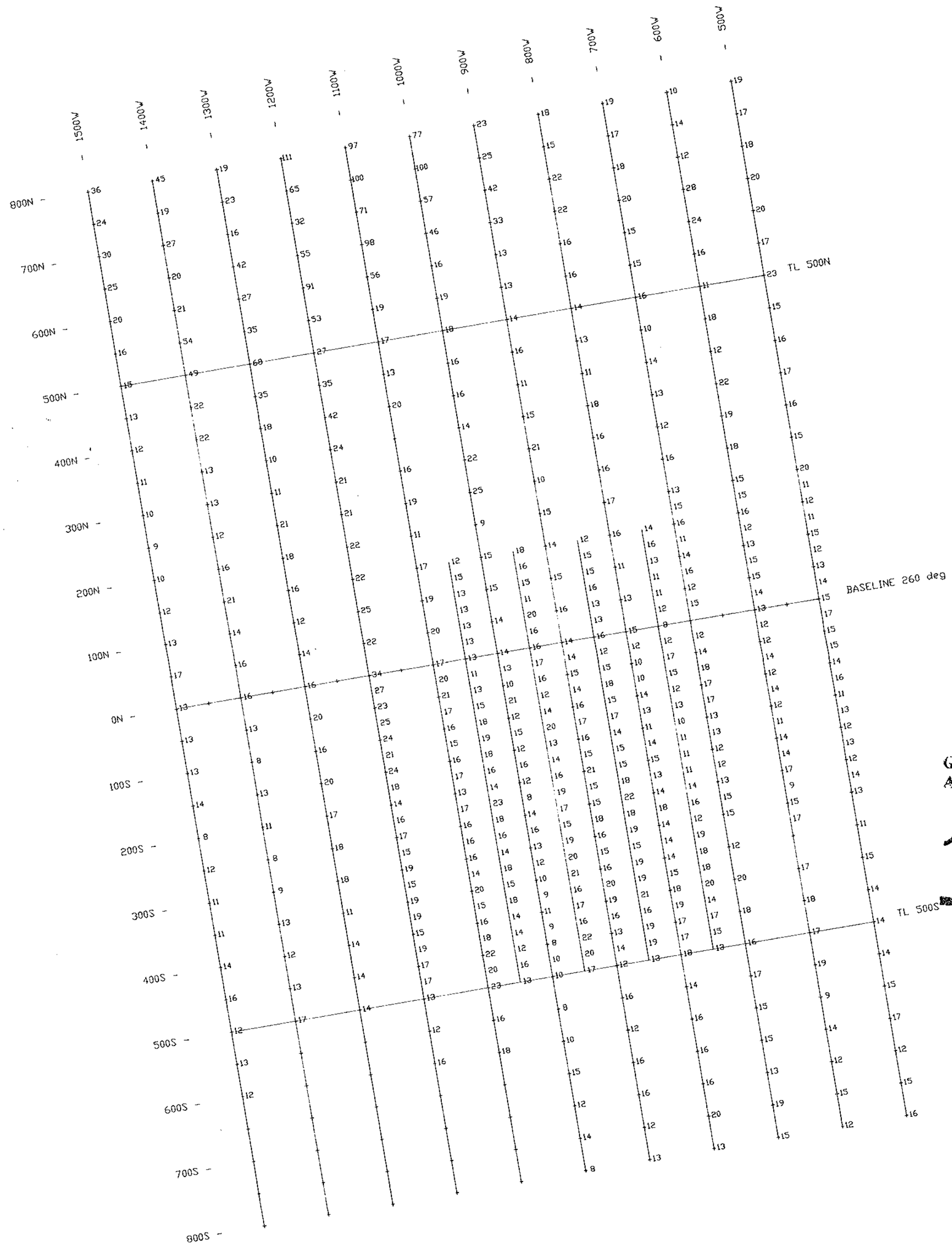
SOIL GEOCHEMISTRY

Arsenic

Greenwood M.D. N.T.S. 82E/6

DATE: 18 March 1988 | SCALE: 1 : 5000

DRAWN BY: Tony Clark Consulting



N

27 Ni ppm

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA
P.D. LERICHE
FELLOW

0 100 200 300 400 500

metres

MAP 15

DRYDEN RESOURCE CORPORATION

ASHWORTH EXPLORATIONS LIMITED
LUCKY BOY PROJECT
Beaverdell Area

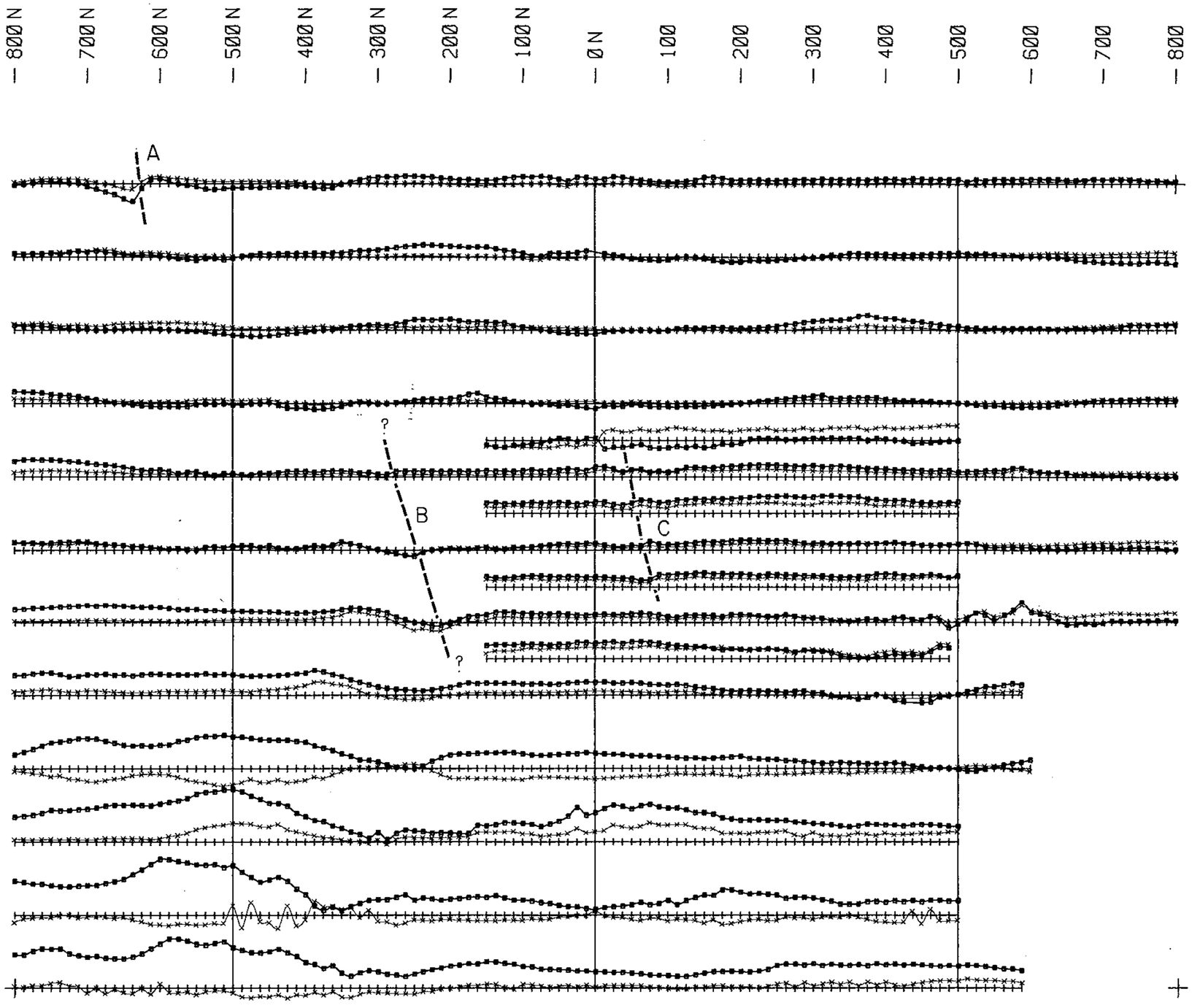
SOIL GEOCHEMISTRY

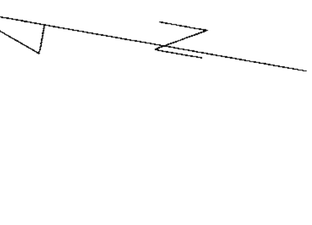
Nickel

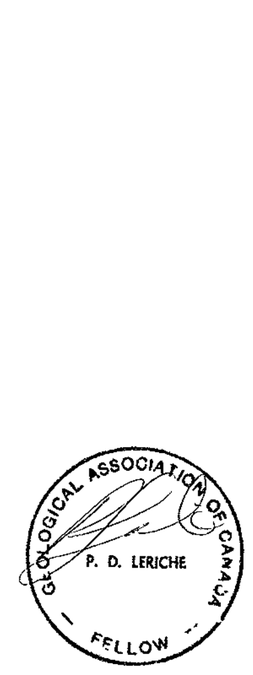
Greenwood M.D. N.T.S. 82E/6

DATE: 18 March 1988 | SCALE: 1 : 5000

DRAWN BY: Tony Clark Consulting







40.00
IN-PHASE

40.00
QUADRATURE

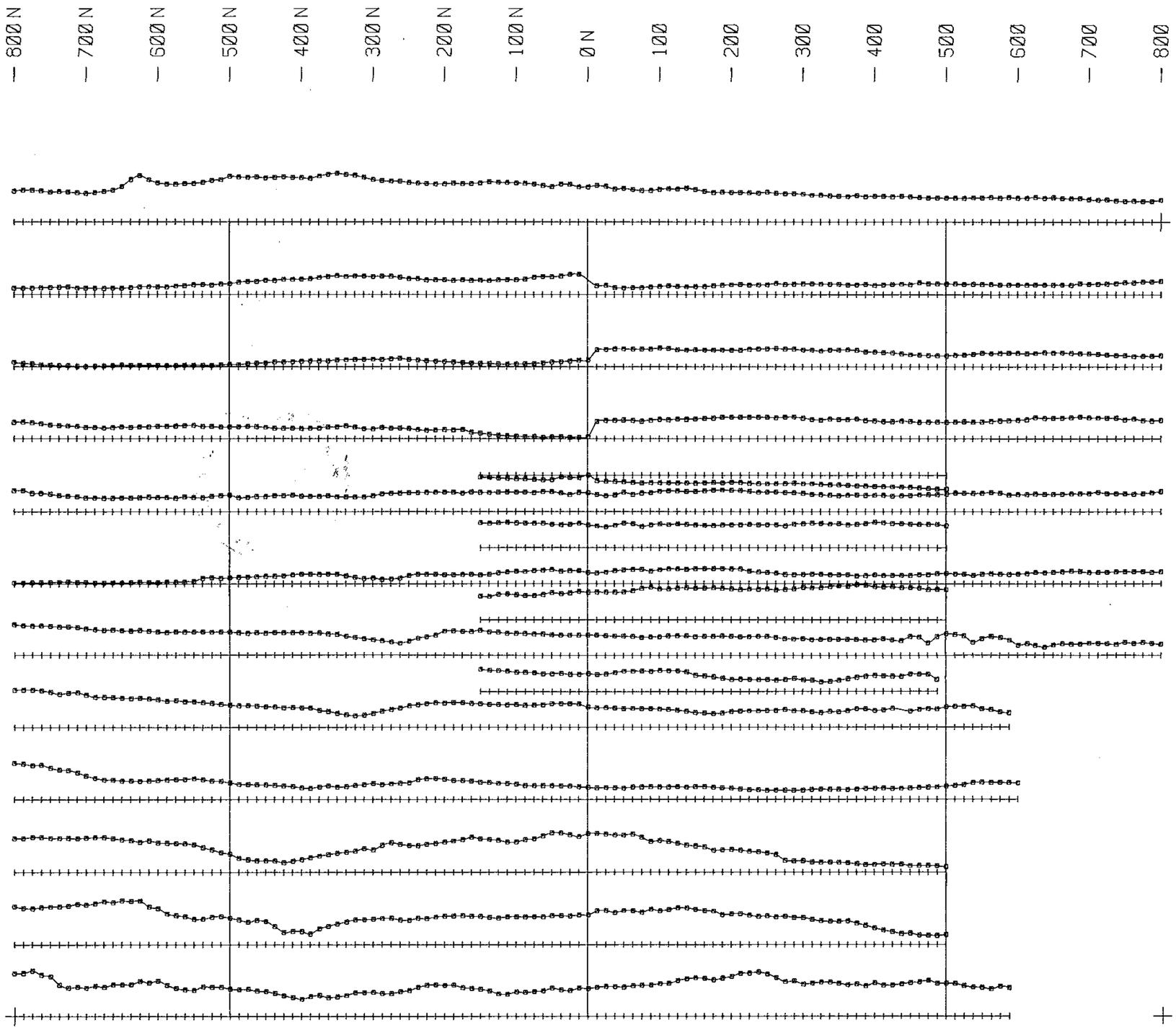
GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

0.0 100.0 200.0 400.0 METRIC

MAP 16

SURVEYED BY: ASHWORTH EXPLORATIONS LIMITED	DRAWN BY: INTERPRETEX	DRYDEN RESOURCE CORPORATION VANCOUVER, B.C.	VLF-EM IN-PHASE & QUADRATURE PROFILE MAP BEAVERDELL AREA - GREENWOOD MINING DIVISION, B.C. LUCKY BOY PROPERTY REPORT BY: PETER LERICHE ASHWORTH EXPLORATIONS LIMITED, VAN, B.C.	SCALE: 1:5000
EDA OMNI PLUS VLF-EM/MAGNETIC SYSTEM	DATE: MAR. 11/88			PROJECT NO.: 192
USING SEATTLE TRANSMITTER, FACING NORTH	FIGURE #			N.T.S. NO.: 82 E/6



N

GEOLOGICAL ASSOCIATION OF CANADA
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100.00
FLD STRNTH

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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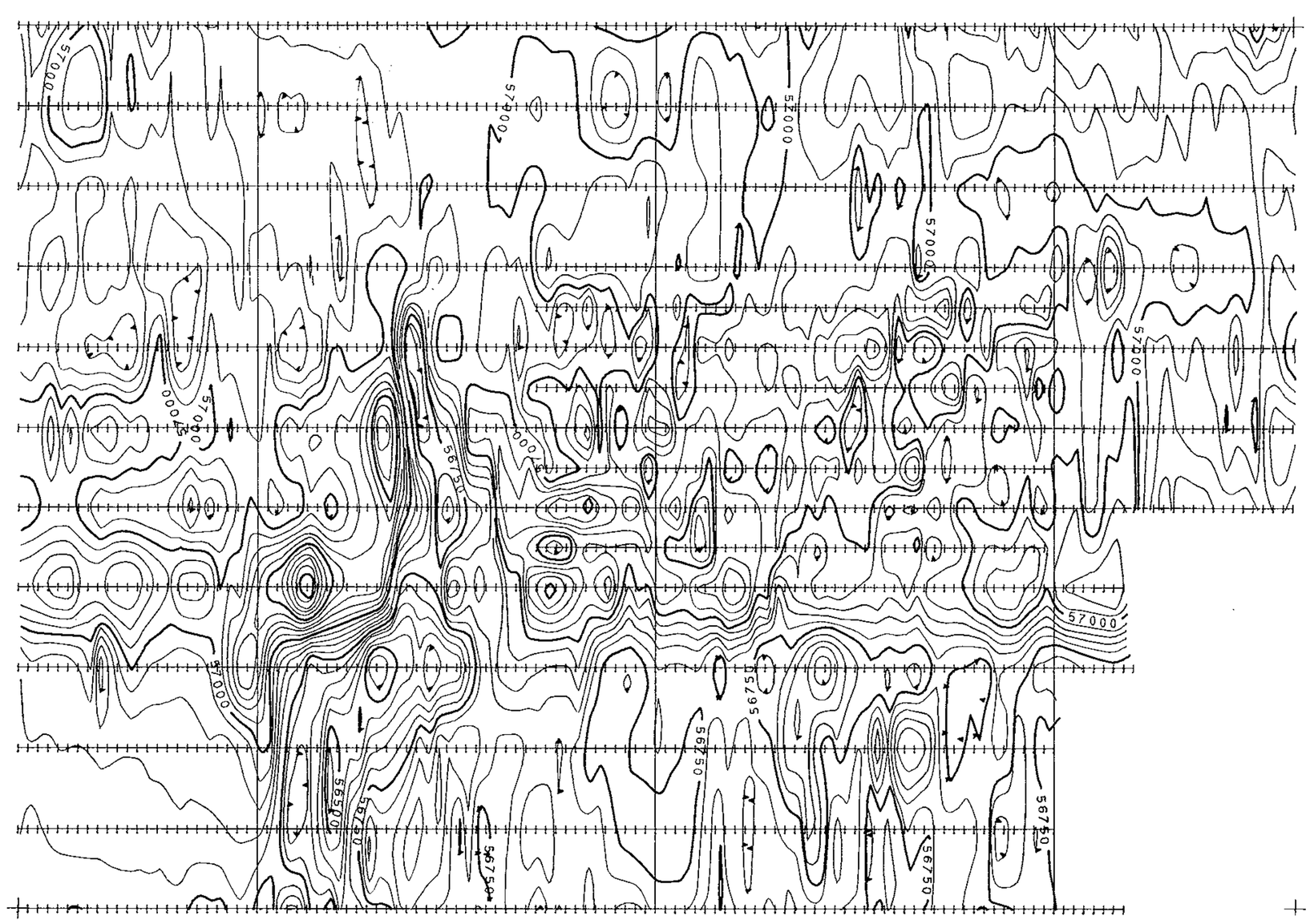
0.0 100.0 200.0 400.0 METRIC

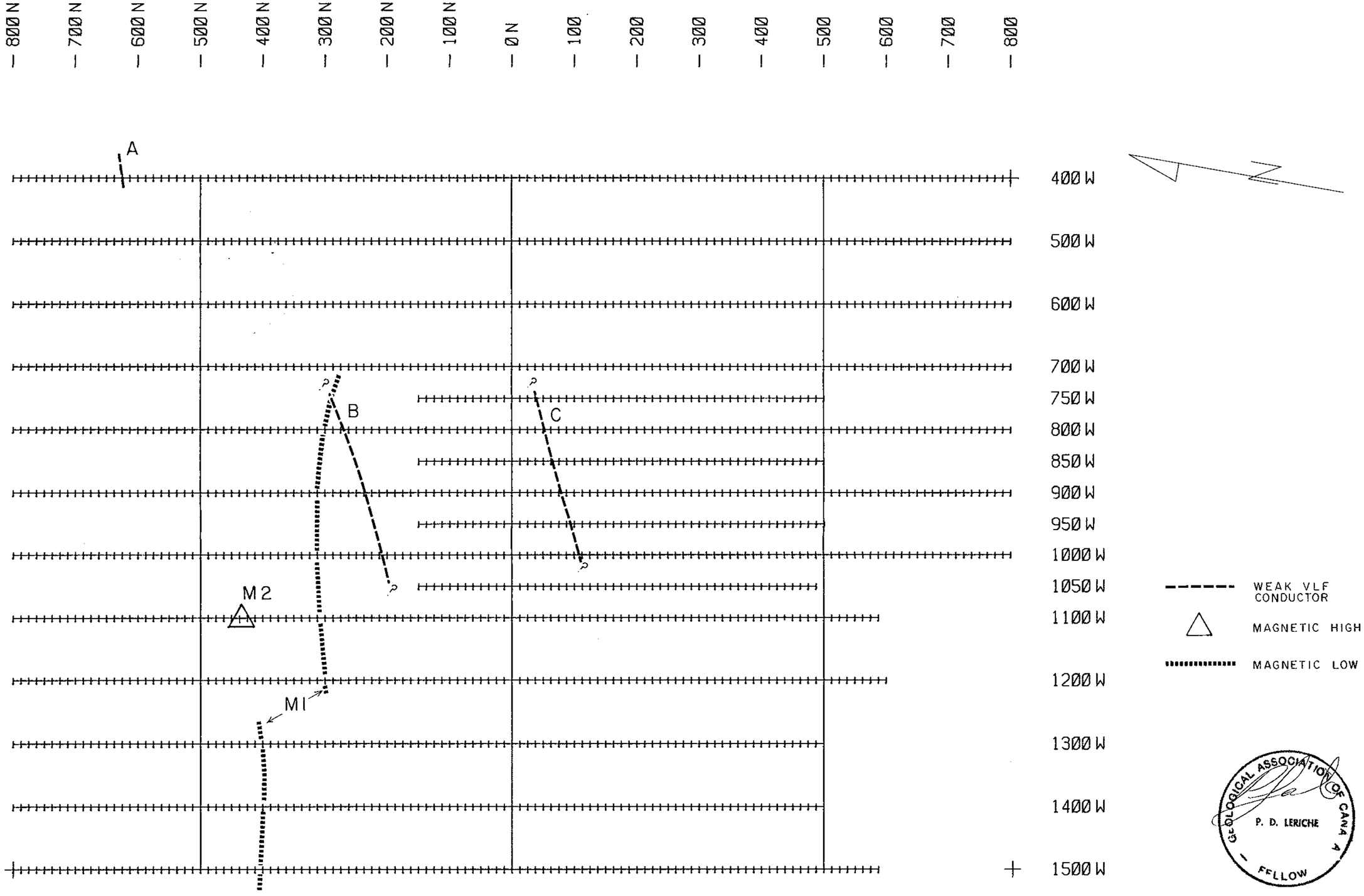
MAP 17

SURVEYED BY: ASHWORTH EXPLORATIONS LIMITED	DRAWN BY: INTERPRETEX	DRYDEN RESOURCE CORPORATION VANCOUVER, B.C.	VLF-EM FIELD STRENGTH PROFILE MAP BEAVERDELL AREA - GREENWOOD MINING DIVISION, B.C. LUCKY BOY PROPERTY REPORT BY: PETER LERICHE ASHWORTH EXPLORATIONS LIMITED, VAN, B.C.	SCALE: 1:5000
EDA OMNI PLUS VLF-EM/MAGNETIC SYSTEM	DATE: MAR. 11/88			PROJECT NO.: 192
USING SEATTLE TX, 100 UNITS SUBTRACTED	FIGURE #			N.T.S. NO.: 82 E/6



MAP 18

SURVEYED BY: ASHWORTH EXPLORATIONS LIMITED	DRAWN BY: INTERPRETEX	DRYDEN RESOURCE CORPORATION VANCOUVER, B.C.	TOTAL FIELD MAGNETIC CONTOUR MAP BEAVERDELL AREA - GREENWOOD MINING DIVISION, B.C. LUCKY BOY PROPERTY REPORT BY: PETER LERICHE ASHWORTH EXPLORATIONS LIMITED, VAN, B.C.	SCALE: 1:5000
EDA OMNI PLUS VLF-EM/MAGNETIC SYSTEM	DATE: MAR. 11/88			PROJECT NO.: 192
CONTOUR INTERVAL = 50 GAMMAS	FIGURE #			N.T.S. NO.: 82 E/6



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0.0 100.0 200.0 400.0 METRIC

GEOLOGICAL BRANCH
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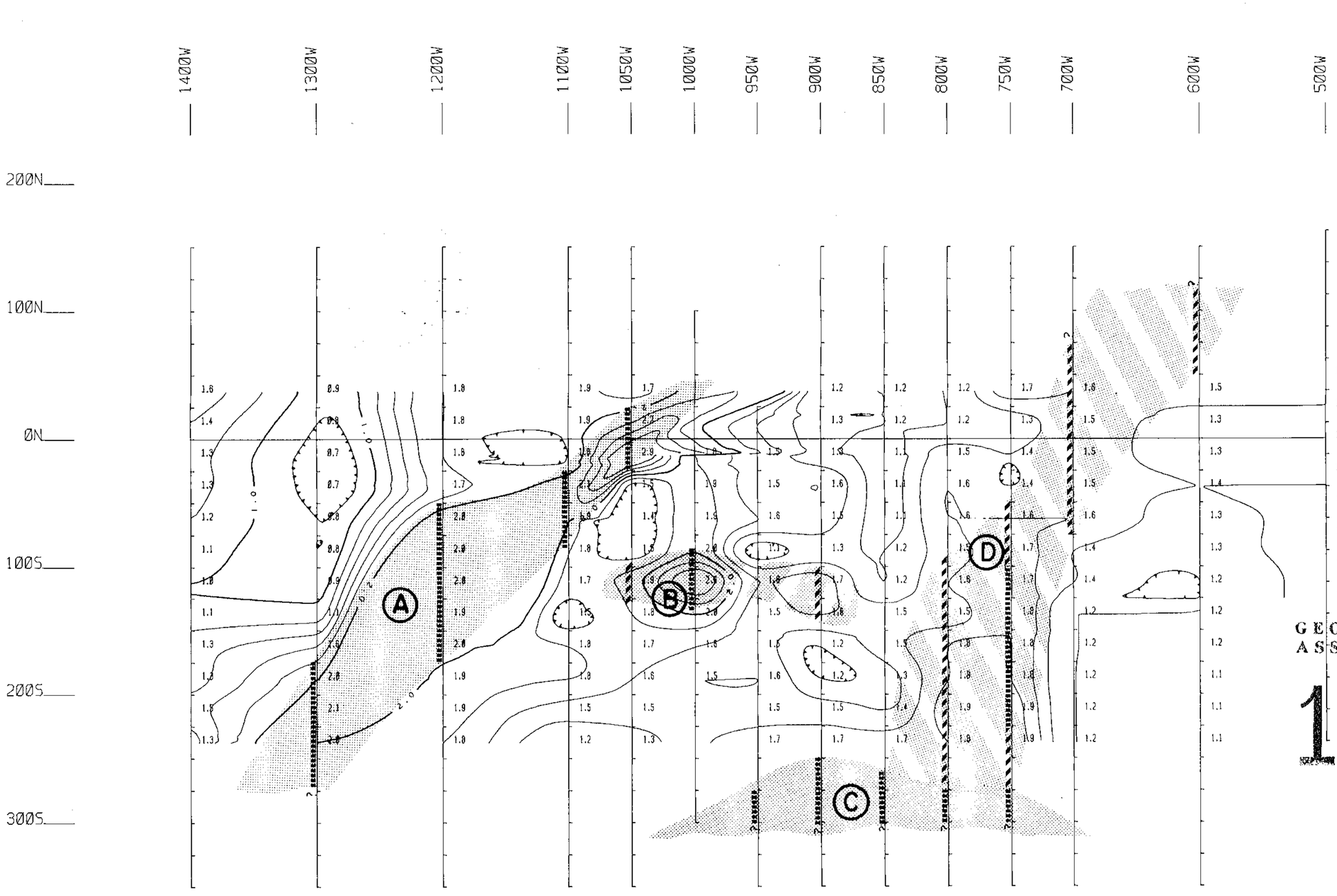
MAP 19

SURVEYED BY: ASHWORTH EXPLORATIONS LIMITED	DRAWN BY: INTERPRETEX	DRYDEN RESOURCE CORPORATION VANCOUVER, B.C.	INTERPRETATION MAP BEAVERDELL AREA - GREENWOOD MINING DIVISION, B.C. LUCKY BOY PROPERTY REPORT BY: PETER LERICHE ASHWORTH EXPLORATIONS LIMITED, VAN, B.C.	SCALE: 1:5000
EDA OMNI PLUS VLF-EM/MAGNETIC SYSTEM	DATE: MAR. 11/88			PROJECT NO.: 192
	FIGURE #			N.T.S. NO.: 82 E/6



50m 25m 0m 50m 100m

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MAP 20

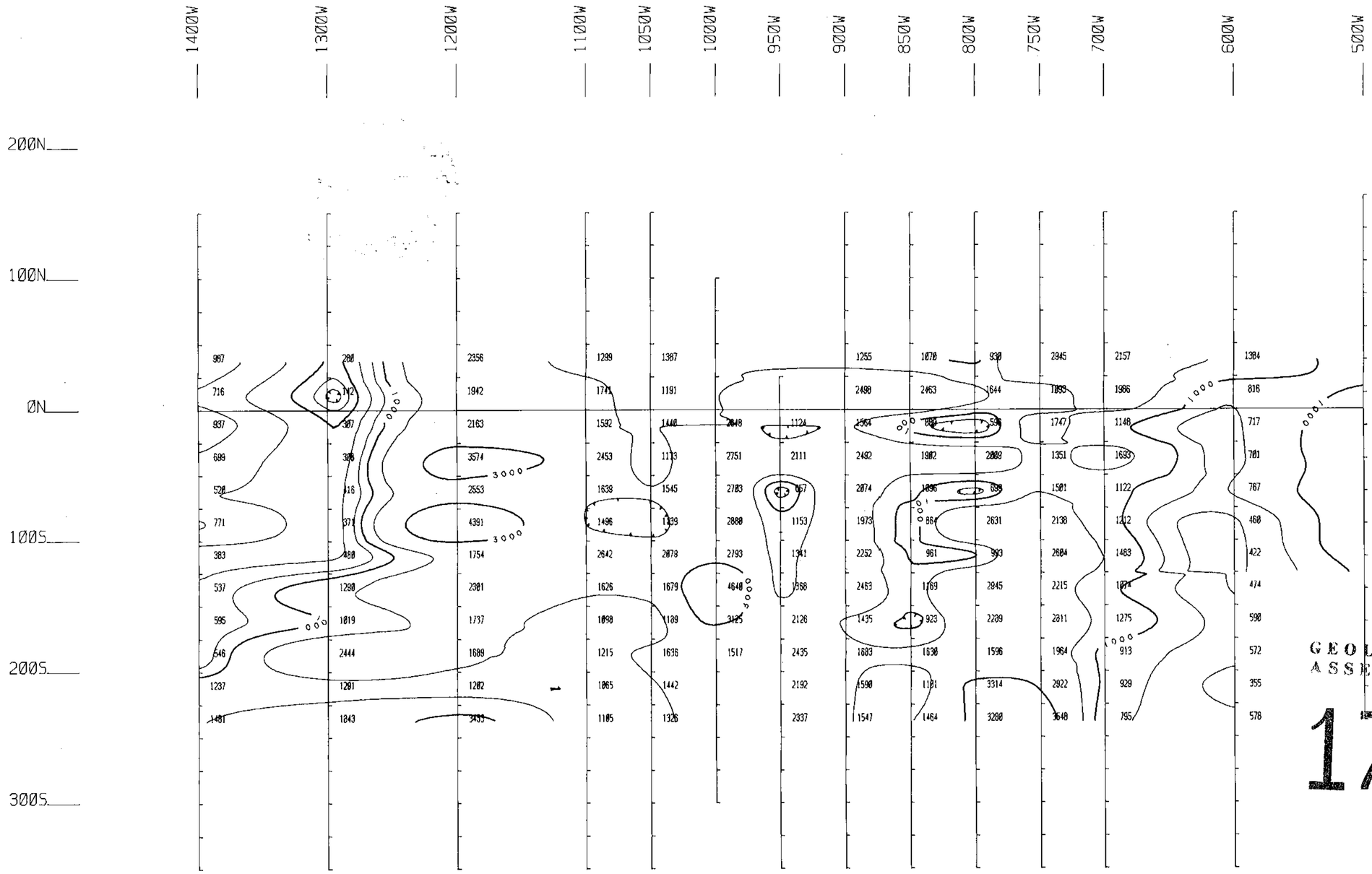
To Accompany Pacific Geophysical Report By
: P.A.CARTWRIGHT, P.Geoph.
: G.D.LOCKHART, B.Sc.

ANOMALY CLASS : Definite
: Probable
: Possible
CONTOUR INTERVAL : 0.2% PFE
ELECTRODE ARRAY : Dipole-Dipole X=25m N=1
/ 1 pass through a 3 pt. Hanning Filter./
/ 1 pass through a 9 pt. Hanning Filter./
OUTLINE OF ANOMALOUS ZONES

DRYDEN RESOURCE CORPORATION

INDUCED POLARIZATION SURVEY
(FILTERED CONTOUR PRESENTATION)
LUCKY BOY PROPERTY: GREENWOOD M.D.,B.C.
BASELINE AZIMUTH : 260 Deg.

SCALE = 1: 2500 DATE : 2/29/88
SURVEY BY : GDL NTS : 82E6
FILE: MIIPDRY Dwg.No.:I.P.P.-3012
Ashworth Explorations Limited



GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,921

GEOLOGICAL ASSOCIATION OF CANADA
P. D. LERICHE
FELLOW

MAP 21

To Accompany Pacific Geophysical Report By
: P.A.CARTWRIGHT, P.Geoph.
: G.D.LOCKHART, B.Sc.

CONTOUR INTERVAL : 150/200/300/500/750/1000 ohmm

ELECTRODE ARRAY : Dipole-Dipole X=25m N=1

( ) pass through a 3 pt. Hanning Filter.)
( ) pass through a 9 pt. Hanning Filter.)

DRYDEN RESOURCE CORPORATION

RESISTIVITY SURVEY
(FILTERED CONTOUR PRESENTATION)
LUCKY BOY PROPERTY: GREENWOOD M.D.,B.C.
BASELINE AZIMUTH : 260 Deg.

SCALE = 1: 2500 DATE : 2/29/88
SURVEY BY : GDL NTS : 82E6
FILE: MRPDRY Dwg.No.: R.P.-3012
Ashworth Explorations Limited