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GEOLOGICAL - GEOCHEMICAL - GEOPHYSICAL REPORT

SUE CLAIMS

SOO RIVER, WHISTLER AREA

VANCOUVER, MINING DIVISION

92 J / 2 E

for

DECADE INTERNATIONAL DEVELOPMENT LTD.
1520 West 6th Avenue
Vancouver, B.C.
V6J 1R2

by

HAROLD M. JONES, P.ENG.
HAROLD M. JONES AND ASSOCIATES INC.

May 31, 1988

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*Revised Figures 3, 4, 5 and 6 in pocket

SUMMARY

The Sue 1-6 claims are located in southwestern British Columbia along the Soo River, approximately 15 kilometers due north of the Whistler ski village and 108 km north of Vancouver. They are accessible from Vancouver by a paved highway and a short section of logging road.

Work on and in the vicinity of the Sue 1 to 4 claims by Riocanex between 1978-1980 was successful in locating areas of coincident copper - zinc - lead geochemical anomalies. Later geochemical work by the present claim owner located an area anomalous in cobalt which was coincident with a large Cu - Zn - Pb anomaly located by Riocanex.

Between May 4-22, 1988 Decade International Development Ltd. conducted a program consisting of geological mapping, geochemical soil sampling and UTEM (time domain electromagnetic) surveying on the Sue claims. This work was centered around the area from which significant cobalt geochemical assays were obtained. The object of the program was to check the possibility that cobalt in the soils might be reflecting a buried massive sulphide deposit.

The claims are located within a roof pendant of Lower Cretaceous Gambier Group volcanic and sedimentary rocks in the Coast Range Plutonic Complex.

The surveyed area is underlain by a package of volcanic pyroclastic rocks ranging from rhyolitic to andesitic. They include tuffs, lapilli tuffs and volcanic breccias. Granitic intrusives crop out on the southeast edge of the surveyed area.

The volcanics appear to be in poorly defined groups. Rhyolitic - dacitic rocks dominate in the central part of the area, grading northeasterly into dacitic - andesitic units and finally into dominantly andesitic units.

Geochemical assay results indicate that cobalt, copper and zinc anomalous values transect all rock units, indicating a possible structural control not recognized to date. Cobalt is more widespread than originally thought.

Geophysical data indicates several conductors which are most likely due to geological contacts and one major but weak one not attributed to a contact. The cause of the latter one is unknown.

A follow-up exploration program, based on the results of the recently completed field work, is recommended. This work will attempt to determine the limits and significance of the cobalt geochemical anomalies, check for possible cross-cutting structures not seen in the UTEM survey and to explore for the source of the major conductor. This program would consist of prospecting, soil sampling, VLF-EM surveying, geological mapping and backhoe trenching. It is estimated that the program would cost approximately $40,000.

Upon completion of the above work, all results should be assessed. If a drill target is indicated, it should be diamond drilled. If not, consideration should be given to an expanded basic exploration program similar to that recently completed.

Two alternative programs are proposed, based on the results obtained from the above work. Stage II(a) consists of diamond drilling and is estimated to cost $115,000; Stage II(b) consists of expanded geological, geochemical and geophysical surveys and is estimated to cost $75,000.

INTRODUCTION

The writer prepared a report on the Sue claims dated October 15, 1987 in which he reviewed the geology, the previous work conducted on the property by Riocanex Ltd., and some more recent soil sampling by the property owner. This latter work located an area significantly anomalous in cobalt, which was interpreted by the writer as possibly indicating the presence of massive sulphides in the area. An exploration program was recommended to investigate this possibility.

A field program consisting of geological mapping, geochemical soil sampling and UTEM surveying was undertaken to explore for a possible massive sulphide body in the vicinity of the cobalt anomaly. To facilitate these surveys a grid was laid out using Silva compass, hip chain and flagging to cover an area approximately 2,000 m x 1,300 m, centered around the area from which anomalous cobalt samples were obtained. The grid consisted of lines at 100 m separations trending N30°E. Samples were collected along each line at 25 m intervals. The same grid was used for the UTEM survey. The grid totalled approximately 24.5 line kilometers.

The southwest end of the grid lines terminated in the swampy Soo River valley bottom or near the river itself. Because of this natural barrier and the grid orientation, line lengths are variable.

This report describes the results of the above exploration program.

Location and Access

50° 14' North Latitude	)	to centre of claims
122° 58' West Longitude	)	

The claims are located in the Vancouver Mining Division approximately 15 km due north of the village of Whistler and 108 km north of Vancouver. They lie immediately north of Soo River, an east-flowing tributary of Green River (Figure 1).

0 100 200 300 MILES

0 100 200 300 400 500 KM.

DECADE INTERNATIONAL DEVELOPMENT LTD.

H. M. JONES & ASSOCIATES INC. VANCOUVER, B.C.

SUE CLAIMS

LOCATION MAP

SOO RIVER, WHISTLER AREA

N.T.S. 92J-2W VANCOUVER M.D., B.C.

SCALE AS SHOWN	MAY 1988	FIG. 1
H. M. JONES		

The claims are readily accessible from Whistler Village by taking Highway 99 northward for approximately 18 km, then the Soo River logging road for approximately 8 km. This road passes through the southern part of the property. Only one short logging road provides limited access to the centre of the claims.

Topography and Vegetation

The claims lie on the south slope of the ridge separating Soo River from Rutherford Creek. Stopes are moderate to steep and fairly uniform, except toward the height of land where they are cliff-forming. The slopes are traversed by a number of creeks, some of which follow deeply incised, steep-walled gulleys and canyons. Elevations range from Soo River at 610 m to the ridge top at 1,675 m.

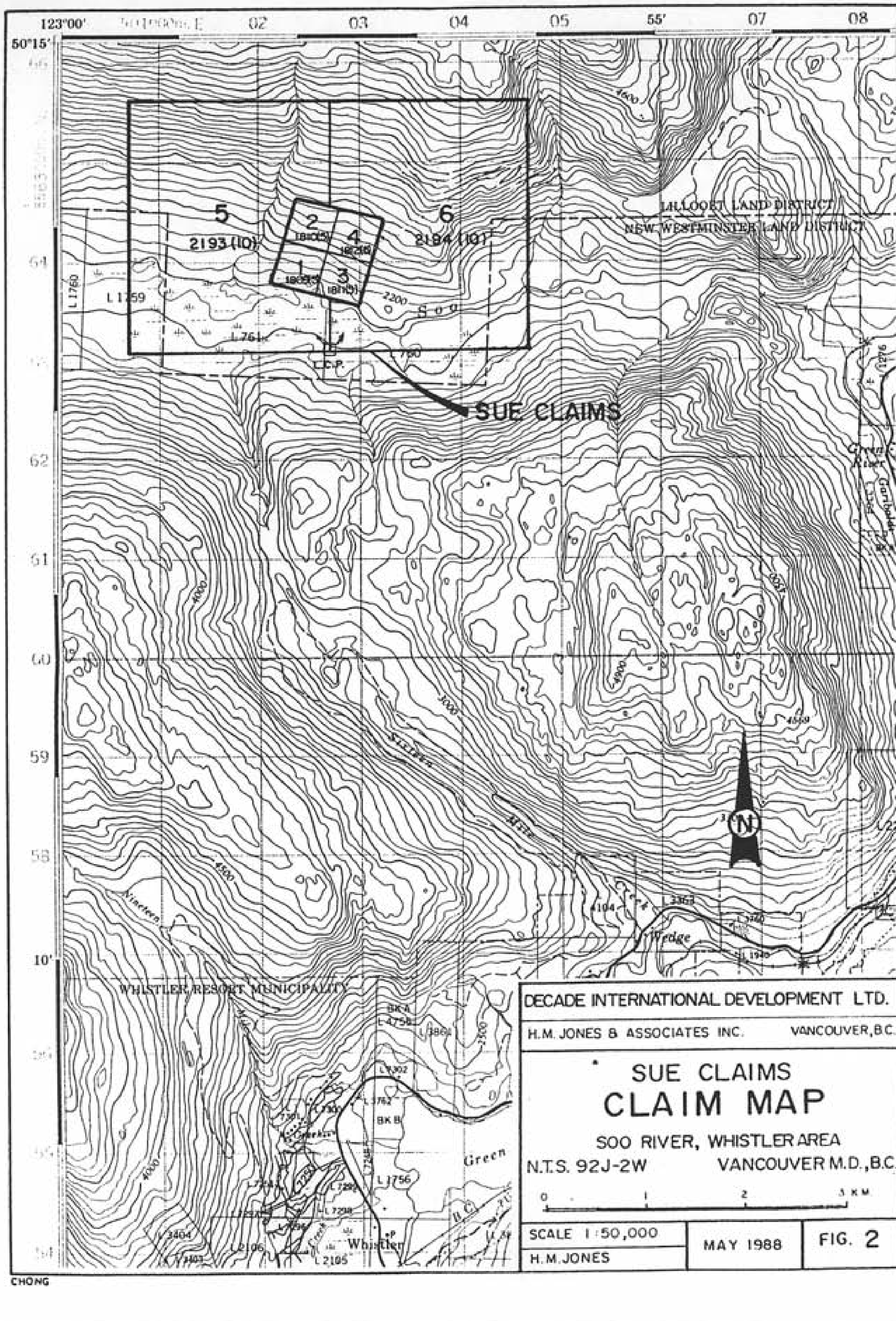
The Soo River valley is an active logging area. Sue 1 claim has been essentially completely clear-cut. The remainder of the property is well forested with commercial-sized fir and cedar.

Property

The property consists of six claims (Figure 2). They are:

Claim Name	No. of Units	Record No.	Date of Record	Expiry Date
Sue 1	1	1809	May 28, 1985	May 28, 1990
Sue 2	1	1810	"	"
Sue 3	1	1811	"	"
Sue 4	1	1812	"	"
Sue 5	20	2193	October 28, 1987	October 28, 1988
Sue 6	20	2194	October 28, 1987	October 28, 1988

Sue 1 to 4 claims are owned by M.P. Warshawski, 6326 Montgomery Street, Vancouver, B.C. and held under an option agreement by Decade International Development Ltd.



123°00'
02
03
04
05
55'
07
08
50°15'
64
62
61
60
59
58
10'
5
2193 (10)
6
2194 (10)
2
4
1
3
L 1760
L 1759
L 761
L 760
L.C.P.
Soo
SUE CLAIMS
LILLOOET LAND DISTRICT
NEW WESTMINSTER LAND DISTRICT
Green River
Wedge
L 3363
Nineteen
WHISTLER RESORT MUNICIPALITY
Whistler
Green
L 1756
L 2106
L 2105
L 3404
CHONG
DECADE INTERNATIONAL DEVELOPMENT LTD.
H.M. JONES & ASSOCIATES INC.
VANCOUVER, B.C.
SUE CLAIMS
CLAIM MAP
SOO RIVER, WHISTLER AREA
N.T.S. 92J-2W
VANCOUVER M.D., B.C.
0
1
2
3 KM
SCALE 1:50,000
H.M. JONES
MAY 1988
FIG. 2

Sue 5 and 6 are beneficially owned by Decade International Development Ltd., 1520 West 6th Avenue, B.C.

History

There is very little history on the Soo River area. During 1976-1977, Rainbow Syndicate conducted prospecting and reconnaissance geological mapping in the vicinity of the Sue claims. They located minor chalcopyrite as veinlets in metavolcanics within a pendant in the Coast Plutonic Complex.

In 1978, Riocanex examined the Soo River area as part of a regional program of exploring the Gambier Group rocks. The presence of rhyolitic and dacitic rocks in the area prompted them to conduct a stream silt sampling program. This work resulted in them locating one stream anomalous in copper and zinc. Further sampling was conducted in 1979, the results of which indicated that the anomalous portions of the creek was restricted to the section underlain by volcanic rocks. Four claims, Soo A, B, C and D were staked in late 1979 to cover the area of interest.

In 1980, Riocanex conducted a program of geological mapping, geochemical soil sampling, and electromagnetic and magnetic geophysical surveys. The results of this work indicated one large and a number of smaller areas anomalous in copper with partially coincident zinc and lead anomalies. The VLF-EM and Max-Min geophysical surveys generally reflected the northwest geological trend. However, both surveys recorded a "high" at one station. This occurred within a large zinc geochemical anomaly and upslope from the large copper anomaly. The survey area was underlain by volcanics of rhyolitic, dacitic and andesitic composition. Epidote stringers occurred throughout, some of which contained minor chalcopyrite. Pyrite occurred throughout as minor disseminations and up to 5% in quartz sericite schists.

Mike Warshawski, prospecting in the area in 1983, tested many streams in the area using a heavy metals kit. He found one creek within the Riocanex property as being anomalous. Assays from silts in this creek revealed that it was anomalous in cobalt as well as copper and zinc. He collected a number of soil samples which also returned anomalous cobalt assays.

In 1985, four two-post claims - Sue 1 to 4 - were staked for M. Warshawski. A number of soil samples were collected and assayed by the I.C.P. method. The results indicated a significant cobalt anomaly coincident with Riocanex's copper and zinc anomalies.

GEOLOGY

Regional Geology

The Sue claims are underlain by Lower Cretaceous Gambier Group rocks which form a pendant within the Cretaceous to Tertiary Coast Plutonic Complex.

The Gambier Group rocks consist of intermediate to acid marine volcanics and sediments. Andesites dominate the volcanic portion of the pendant in the claims area. They range in lithology from flows and flow breccias to tuffs, lapilli tuffs, and agglomerates. Dacites, principally tuffs but also flows, flow breccias, lapilli tuff, agglomerates and crystal tuffs represent less than 10% of the volcanic portion of the pendant, although locally they are the dominant rocks. Most of the dacites contain minor disseminated pyrite with local concentrations up to 2-3%. Rhyolites form a minor part of the volcanic section.

Sediments comprise a substantial proportion of the exposed rocks in the pendant. They include shales, greywackes, quartzites, and arkosic quartzites and cherts. Minor disseminated pyrite is common throughout the sediments.

The Gambier Group rocks host the Britannia Mine, a volcanogenic massive sulphide deposit which was a successful producer of copper for many years.

Property Geology

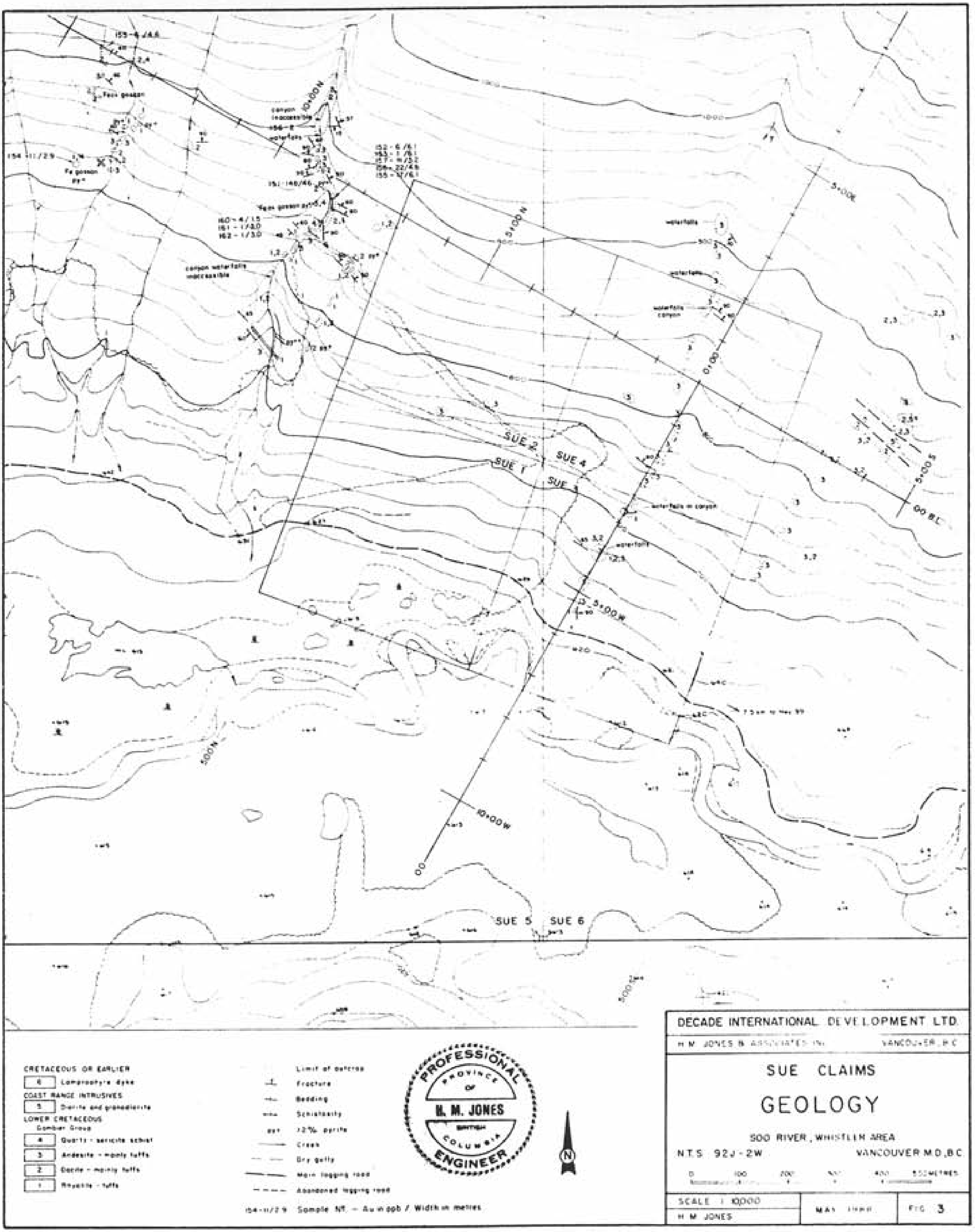
Outcrop is very sparse on the property except in the northeast corner of Sue 6 claim where precipitous cliffs are common. Other than in this area, outcrop is mostly restricted to creek gulleys and canyons. While creeks are common and are often in deeply incised gulleys, many do not expose bedrock.

The claims are underlain primarily by volcanic rocks which are rhyolitic, dacitic or andesitic in composition. Most appear to be pyroclastics, and include tuffs, lapilli tuffs and volcanic breccias. Some flow units may also be present. All units are interbedded and difficult to correlate due to the poor outcrop exposures. Contacts and bedding are rarely seen but where observed they strike north 40-50° west and dip 60-65° to the northeast.

Rhyolitic and dacitic tuffs, often mapped in the field as rhyodacites, with lesser andesitic tuffs form a distinct unit trending through the central part of the grid. They are well exposed along a creek which lies between lines 7N and 9N and a small parallel stream lying to the southeast of it. The rhyolitic and dacitic rocks are locally strongly fractured, heavily iron-stained and well mineralized with disseminated pyrite (2-5% pyrite), especially near line 8N from 0W to 1W. Quartz-sericite schist, also very pyritic, occurs in areas of shearing.

This unit grades into an andesitic-dacitic unit near line 8+50N, at 0+50E. Upstream from this point the creek is within a steep-walled canyon characterized by massive volcanics as compared to the highly fractured rhyolite-dacite unit located immediately downstream.

Similar rhyolitic and dacitic rocks occur at the lower end of the creek which follows grid line 1S, but the andesitic content is higher. In this creek, the rhyolite-dacite unit grades upward into mostly interbedded andesites and dacites. Further upstream massive andesite is the dominant rock.


SUE 1
SUE 2
SUE 3
SUE 4
SUE 5
SUE 6
10+00N
5+00N
0+00
5+00E
5+00S
00 BL
5+00W
10+00W
500N
canyon inaccessible
waterfalls
canyon waterfalls inaccessible
waterfalls in canyon
Fe gossan
154-11/2.9
CRETACEOUS OR EARLIER
6 Lamprophyre dyke
COAST RANGE INTRUSIVES
5 Diorite and granodiorite
LOWER CRETACEOUS
Gambier Group
4 Quartz - sericite schist
3 Andesite - mainly tuffs
2 Dacite - mainly tuffs
1 Rhyolite - tuffs
Limit of outcrop
Fracture
Bedding
Schistosity
Creek
Dry gully
Main logging road
Abandoned logging road
154-11/2.9 Sample Nº. - Au in ppb / Width in metres
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
H. M. JONES
N
DECADE INTERNATIONAL DEVELOPMENT LTD.
VANCOUVER, B.C.
SUE CLAIMS
GEOLOGY
SOO RIVER, WHISTLER AREA
N.T.S. 92J-2W
VANCOUVER M.D., B.C.
0 100 200 300 400 500 METRES
SCALE 1:10,000
H. M. JONES
FIG. 3

CHONG

Medium to coarse grained granite outcrops near line 4S, 1E. It appears to be dyke-like and striking approximately N50°W. Slightly northeast of here a dacite outcrop is feldspathized, has a somewhat granitic texture, and may contain a granite dyke. This area appears to be altered due to its close proximity to the contact between the pendant and the Coast Range Plutonic Complex.

ALTERATION AND MINERALIZATION

Rhyolitic rocks within the rhyolite-dacite unit are locally strongly sheared and altered to quartz-sericite schists, occasionally accompanied by narrow quartz veinlets.

Andesitic rocks are often weakly to moderately chloritized. Several small exposures were seen where shearing altered these rocks to chlorite schist.

Epidote is common throughout the andesitic and to a lesser degree the dacitic rocks as small grains and masses as well as fine stringers, some accompanied by quartz.

Pyrite is ubiquitous throughout all rocks, but commonly is much more abundant in the highly fractured rhyolitic and dacitic units and in the quartz-sericite schists. Pyrite concentrations from 2% to 5% are common in these rocks, especially is the schists.

Minor chalcopyrite was seen on the property by Riocanex personnel during their work in 1980. It occurred in narrow quartz-epidote stringers.

ROCK SAMPLE AND ASSAYS

Twelve rock samples were taken from areas of heavy iron gossans and/or well pyritized rhyolite, dacite and quartz-sericite schists, primarily to check on their possible gold content. For locations, see Figure 3, and for full set of assays, see Appendix I. The following is a list of the samples.

Sample No.	Type	Length(m)	Assay Au ppb	Assay Ag ppm	Description
151	chip	1.5	146	0.9	Rhyolite tuffs with quartz masses and pyrite veinlets, also diss. pyrite
152	chip	6.1	6	0.1	Rhyodacitic tuff, heavy FeOx, est 3%-5% diss. pyrite
153	chip	6.1	1	0.1	Similar to previous, but includes some chloritized andesite, est 3% pyrite
154	chip	2.4	11	0.1	Rhyolitic tuffs, approaching qtz-sericite schist, heavy FeOx, est 3%-5% pyrite
155	chip	4.5	6	0.7	Dacite tuff and qtz-sericite schist, FeOx, est 3% pyrite
156	grab	-	2	0.2	Rhyodacite rubble from shear zone possibly 1.0 m wide, below possible old working in cliff(?)
157	chip	5.2	11	0.2	Andesite tuff, FeOx on fractures, 1%-2% pyrite
158	chip	4.6	22	0.2	Shattered rhyolitic and dacitic tuff, estimate 3%-5% pyrite
159	chip	6.1	17	0.2	Strongly fractured, chloritized andesitic tuff, locally sheared, FeOx in fractures, est 2% pyrite.
160	chip	1.5	4	0.2	Mixed qtz-sericite schist and schistose dacite, est 2% pyrite
161	chip	3.0	1	0.2	Rhyolitic tuff, approaching qtz-sericite schist, est 3% pyrite
162	chip	3.0	1	0.2	Qtz-sericite schist, est pyrite 3%-5%

Note: Samples 152, 153, 157, 158 and 159 represent a continuous section over 28.1 meters true width, and samples 160, 161 and 162 represent a section over 7.5 meters true width.

These samples were taken from in most cases, very strongly fractured, well pyritized rhyolitic to dacitic rocks, often accompanied by strong iron gossans. Their assays indicate that the sulphides are not accompanied by precious metals.

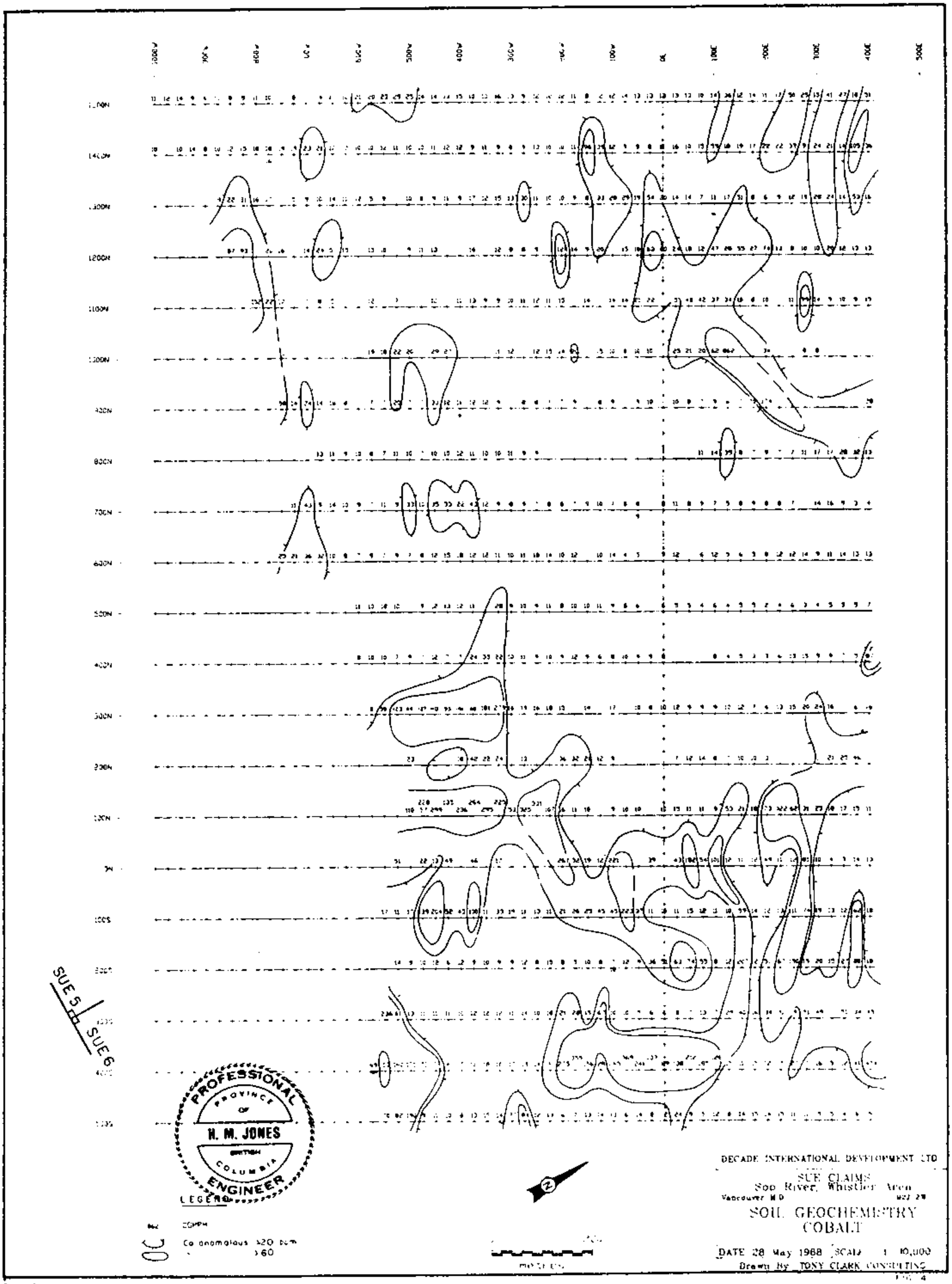
GEOCHEMISTRY

A soil sampling program was conducted over the grid, which was described under "Introduction". A total of 823 samples were collected. No samples were obtained from some grid points due to deep organic cover, creek canyons, etc. All samples were taken from the "B" horizon, using a mattock, from depths ranging from 10 cm to 30 cm, placed in Kraft paper bags and sent to Acme Analytical Laboratories in Vancouver for analysis. All samples were assayed by the I.C.P. method for Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K and W. Each was also assayed for Au by the atomic absorption method.

The above assay data totals 24,690 individual assay values. In order to review this large amount of data, Tony Clark Consulting, a geological and computer consultant, was requested to do a computerized study of the data and produce maps of the more significant elements. The object of this study was to determine which elements might be the most significant in indicating the presence of a buried massive sulphide deposit. He concluded that copper and cobalt are the most significant elements in the data.

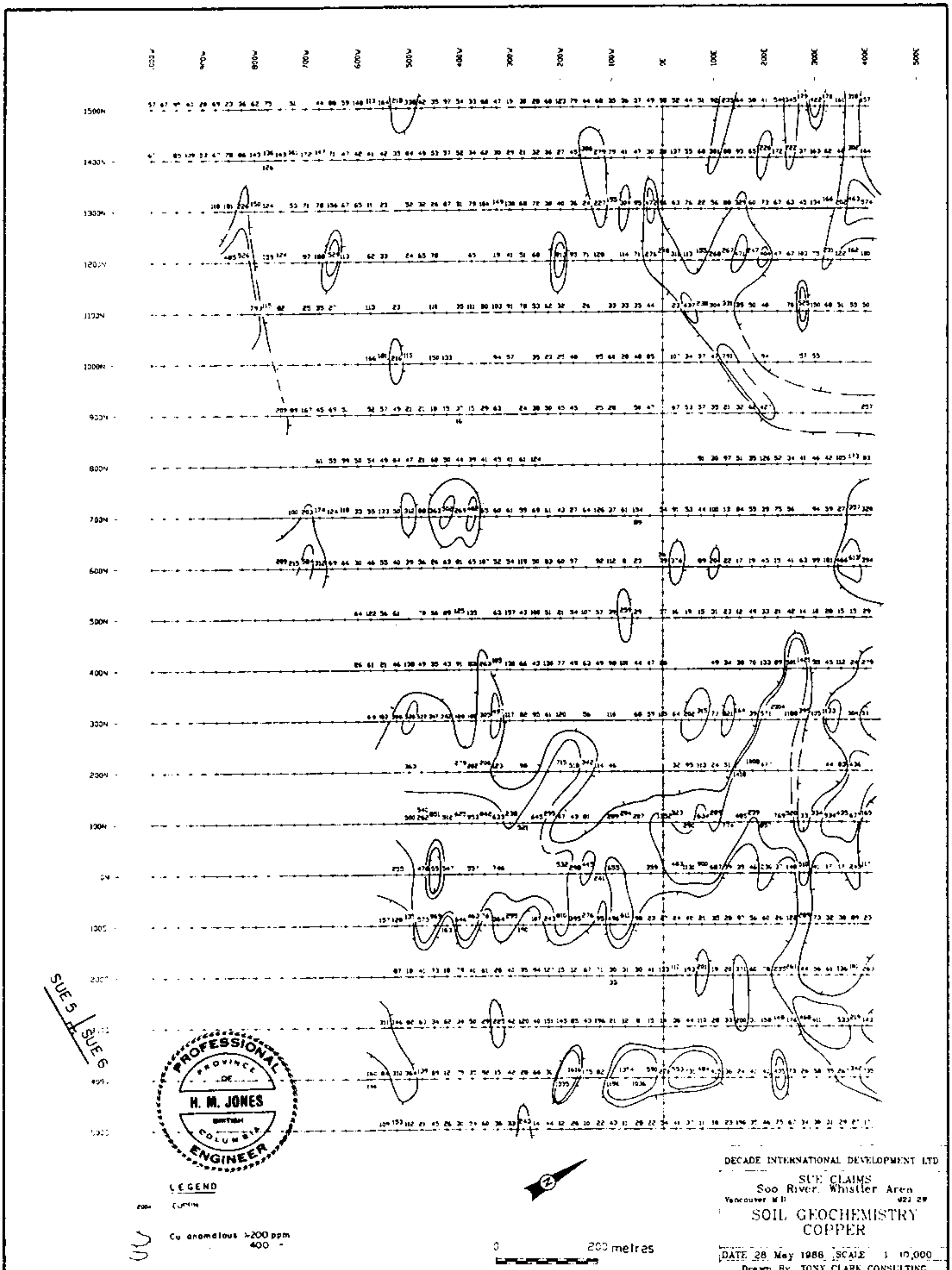
Cobalt and copper anomalous values shows a fairly good correlation (correlation coefficient Co/Cu 0.57). Most of the anomalous Co and Cu values are clustered in the southeastern part of the grid between lines 300W and 400S and are elongate in a north to northeast trend. This is coincident with the slope of the topography, consequently the anomalies are probably greatly exaggerated in this direction due to down slope migration (Figures 4 and 5).

Zinc, which should correlate well with copper in a massive sulphide environment, has a low correlation coefficient (Zn/Cu = 0.15) i.e. low zinc in proportion to copper. Similarly, with cobalt, its correlation coefficient is low (Zn/Co = 0.25). While being relatively low, zinc anomalies correlated with both cobalt and copper but are smaller in area than the other two elements.



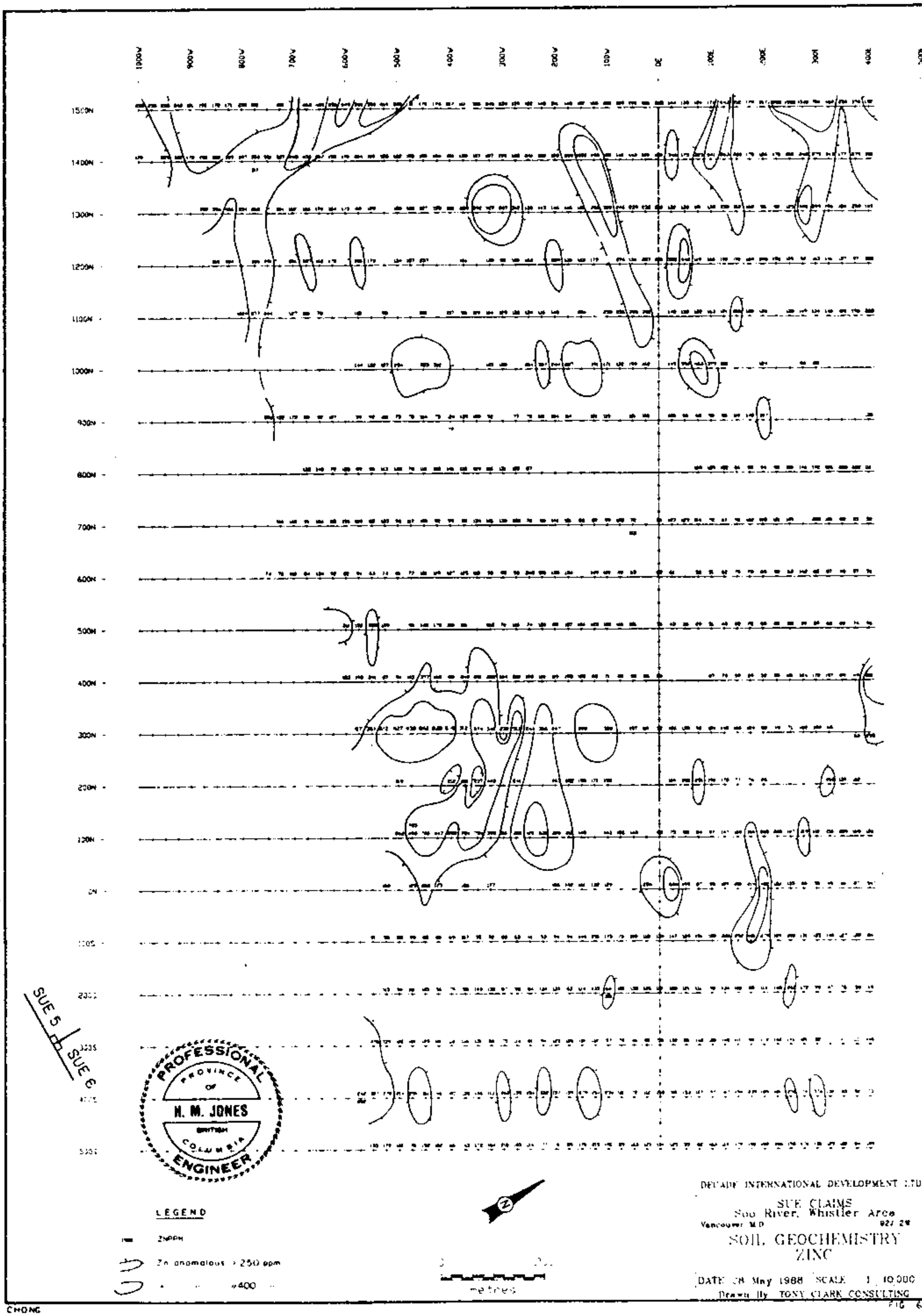
SUE 5
SUE 6
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
H. M. JONES
LEGEND
Co ppm
Co anomalous >20 ppm
>60
DECADE INTERNATIONAL DEVELOPMENT LTD
SUE CLAIMS
Soo River, Whistler Area
Vancouver M.D
92J 2W
SOIL GEOCHEMISTRY
COBALT
DATE 28 May 1988
SCALE 1:10,000
Drawn By TONY CLARK CONSULTING
FIG. 4

CHONG



1500N
1400N
1300N
1200N
1100N
1000N
900N
800N
700N
600N
500N
400N
300N
200N
100N
0N
SUE 5
SUE 6
PROFESSIONAL
PROVINCE OF
H. M. JONES
BRITISH COLUMBIA
ENGINEER
LEGEND
Cu anomalous >200 ppm
400
0
200 metres
DECADE INTERNATIONAL DEVELOPMENT LTD
SUE CLAIMS
Soo River, Whistler Area
Vancouver M.D.
92J 2W
SOIL GEOCHEMISTRY
COPPER
DATE 28 May 1986
SCALE 1:10,000
Drawn By TONY CLARK CONSULTING
FIG. 5

CHONG


1000W
900W
800W
700W
600W
500W
400W
300W
200W
100W
0E
100E
200E
300E
400E
500E
1500N
1400N
1300N
1200N
1100N
1000N
900N
800N
700N
600N
500N
400N
300N
200N
100N
0N
SUE 5
SUE 6
PROFESSIONAL
PROVINCE OF
H. M. JONES
BRITISH COLUMBIA
ENGINEER
LEGEND
ZnPPM
Zn anomalous > 250 ppm
400
metres
DECADE INTERNATIONAL DEVELOPMENT LTD
SUE CLAIMS
Soo River, Whistler Area
Vancouver M.D
92J 2W
SOIL GEOCHEMISTRY
ZINC
DATE 28 May 1988 SCALE 1:10,000
Drawn By TONY CLARK CONSULTING
FIG 6
CHONG

The central part of the sampled area is notably absent of anomalous geochemical values, giving the impression that different geology is present in this area. There is no geological evidence to suggest this. It is suggested that this geochemically low area is a reflection of deep glacial till.

GEOPHYSICS

A UTEM (Time Domain Electromagnetic) survey was run over the grid, the purpose of which was to search for a buried massive sulphide deposit. This survey was conducted by Syd J. Visser, S.J.V. Consultants Ltd. His report accompanies this report as Appendix II.

If a well mineralized zone or structure, water-filled or graphitic fault zone, etc. is present within the survey area, this would be reflected by the survey data as an electrical conductor. This survey method is said to penetrate 600 meters or more in depth.

A number of weak shallow (< 150 meters below surface) conductors and contact zones were located (see Plate 88-1, Appendix II). One shallow, weak conductor, extending from approximately line 1500N, 250W to line 300N, 650W and probably continuing to line 100S, 800W is considered by Visser as being a major feature. It is open along strike to both the northwest and southeast, the latter direction being under the swampy Soo River valley bottom.

The source of this conductor is not known. It angles up the lower south-facing slope on Sue 5 claim in an area completely covered by glacial till. The geochemical data does not reflect a mineralized zone in this area but this could be largely due to the overburden cover.

A well defined conductor was located extending from approximately line 500S, 400W to approximately line 500N, 100EW after which it disappears or is difficult to trace. Visser interprets this as a contact zone, with rock of higher conductivity laying to the northeast.

This inferred contact zone approximates the contact noted in the creek canyon near line 800W between rhyolitic and dacitic rocks to the southwest and massive andesite rocks to the northeast. The acidic rocks near the contact area are highly fractured and very pyritic. It would appear that the geology confirms this geophysical interpretation.

A second conductor, interpreted as a contact zone, is parallel to the above and extends from approximately line 100N, 275E to line 700N, 300E.

A number of weak, shallow crossovers and contact areas were recorded in the central part of the grid. They were interpreted as being small discontinuous conductors or due to changes in conductive overburden.

Visser concludes that no strong conductors indicating the presence of massive sulphides were recorded in the survey area.

DISCUSSION

The anomalous geochemical assays are somewhat scattered but may be grouped into fairly large irregular anomalies, especially in the southeastern part of the grid. Here, they trend approximately North to N30°E perpendicular to the slope and transect all rock types.

Bright orange limonite-rich mud, associated with springs, occur in the clear cut logging area between lines 400N and 0N as well as near line 100S at 300E. Similar material is exposed in road cuts along the main logging road, indicting a downslope migration of this material by surface run-off. This limonitic material is anomalous to highly anomalous in cobalt as well as copper and zinc. These anomalies are either exaggerated in length due to topography or are related to a northeasterly striking mineralized structure(?). The latter can not be ruled out since the anomalies tend to follow two creeks, both of which trend approximately N30°E. These streams may reflect mineralized shear structures(?).

The geochemical anomalies at the northwest end of the grid are more scattered and localized. Their source is not obvious.

The conductor inferred to be a major feature from the UTEM survey has only a weak correlation with the geochemical anomalies. This may(?) be a reflection of heavy overburden. Prospecting to the northwest may locate the source of this conductor.

The results of the recently completed exploration program indicates several areas contain coincident Co, Cu, and Zn geochemical anomalies and one electromagnetic conductor considered to be of interest. The source of the anomalies and conductor is not obvious. The geophysical results do not, however, indicate a massive sulphide deposit being present in the surveyed area but does not preclude one being present in or adjacent to the claims area.

CONCLUSIONS

The Sue claims are underlain by acid and basic pyroclastic volcanic rocks which comprise a part of a roof pendant enclosed within the Coast Plutonic Complex. While the geological setting is favourable for hosting massive sulphide mineralization, only pyrite was observed. It is abundant as disseminations and narrow veinlets, especially in highly fractured and sheared rhyolitic and dacitic tuffs and quartz-sericite schists.

The source of the geochemical anomalies and electrical conductors is not known. Additional exploration is warranted to investigate these features, especially the source of cobalt anomalies.

RECOMMENDATIONS

Using the results of the recently completed exploration program, a follow-up program of detailed prospecting, rock and soil sampling and backhoe trenching should be conducted within the cobalt-copper anomalous area to search for the source of the mineralization. Since anomalous cobalt values in the soil are more widespread than expected, additional soil sampling is warranted to define its limits.

Reconnaissance VLF-EM survey lines should be run perpendicular to the existing grid to check on possible north trending mineralized zones at the southeast end of the grid. These lines should extend from approximately 400N to 500S on the existing grid.

Similar exploration should also be conducted at the northwest end of the grid to search for a source of the conductor crossing line 1500N at 250W. Creek gulleys along this trend might expose some useful geology.

All results should be assessed upon completion of the follow-up program. If a drilling target is defined, it should be drilled. If not, consideration should be given to acquire additional claims and expand the basic exploration program along strike of the favourable geology.

COST ESTIMATE

Stage I - Follow-up program	
Reconnaissance geological mapping and prospecting, including 500 soil samples and 50 rock samples, by one geologist and two assistants	$ 25,000
Backhoe trenching - allow	15,000
Total Stage I	$ 40,000
Stage II(a) - Diamond Drilling - Contingent on Stage I	
Say 1,000 m @ $115/meter all inclusive	$ 115,000
Stage II(b) - Contingent on Stage I	
Additional geological-geochemical-geophysical surveys on expanded claim block, allow	$ 75,000

Respectively submitted,

Harold M. Jones, P.Eng.

REFERENCES

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Assessment Reports 6573, 6581 and 8576.

CERTIFICATE

I, Harold M. Jones, of the City of Vancouver, British Columbia, do hereby certify that:

1. I am a Consulting Geological Engineer with offices at 605 - 602 West Hastings Street, Vancouver, British Columbia.
2. I am a graduate of the University of British Columbia in Geological Engineering, 1956.
3. I have practised my profession as a Geological Engineer for over 30 years.
4. I am a member of the Association of Professional Engineers of British Columbia, Registration No. 4681.
5. I conducted geological mapping on the Sue claims and supervised the geochemical - geophysical program which was conducted on the property between May 4 - 22, 1988.
6. I have no interest in, nor do I expect to receive any interest, direct or indirect, in the Sue claims or in the securities of Decade International Development Ltd.
7. Decade International Development Ltd. is hereby given permission to reproduce this report, or any part of it, in a Prospectus, Statement of Material Facts or other documents as required by the regulating authorities, provided, however, that no portion may be used out of context in such a manner as to convey a meaning differing from that set out in the whole.

Dated at Vancouver, B.C. this 31st day of May, 1988.

PROFESSIONAL ENGINEER
H. M. JONES
BRITISH COLUMBIA

Harold M. Jones, P.Eng.

ADDENDUM

SUPPLEMENTAL REPORT

HAROLD M. JONES & ASSOCIATES INC.

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SUPPLEMENTAL REPORT
SUE CLAIMS
SOO RIVER, WHISTLER AREA
VANCOUVER MINING DISTRICT

Introduction

During the period September 25 - 29, 1988 a follow-up program was conducted on the Sue claims. The purpose of this work was to check areas of interest generated from the May 4 - 22, 1988 geological - geochemical - geophysical program conducted on the claims. Results of the geochemical survey indicated areas which were anomalous in one or more of copper, zinc and cobalt; the geophysical survey areas which contained possible electromagnetic conductors; and the geological survey areas which were well mineralized with pyrite, and several areas which contained a concentration of limonitic gossanous - looking material.

Fieldwork

1. Geology and Rock Samples

Outcrop is poorly exposed in most of the area surveyed, consequently the cause of the geophysical conductors is not obvious. The best exposures of geology are located along two creeks in the western part of the property on Sue 5 claim. Both follow deeply incised creek canyons, the walls of which, locally, are often nearly continuous outcrop or rubble. The geology observed during this recent survey is shown on revised Figure 3.

Both canyons expose similar geology. It consists of rhyolitic, dacitic and andesitic tuffs, often strongly fractured, and locally sheared or faulted. Rhyolitic and dacitic rocks usually are well mineralized with finely disseminated pyrite while the andesitic rocks appear to contain much less pyrite. The rocks in the vicinity of the conductors or their projections are strongly sheared, leached, white, schistose rhyolitic tuffs well mineralized with pyrite. The shears are about 5 feet wide. The conductors may be reflecting these shear or fault zones rather than mineralization. There are no indications of massive sulphides or mineralized veins in the creek canyons in the vicinity of the conductors.

Fourteen rock samples were taken from areas of interest. They were taken primarily to check on the presence of precious metals. Their locations are shown on Figure 3.

Sample No.	Type	Width(m)	Assay Au(ppb)	Assay Ag(ppm)	Description
181	Chip	17.0	1	0.2	Str. fr'd, limonitic rhyodacite, abund. py.
182	Chip	11.0	3	0.3	Similar to above, weakly chloritic, abund. py.
183	Chip	-	1	0.2	Similar to above, abund. py
184	Grabs	2.0	3	0.1	Rhyolite rubble, possible shear, abund. py.
185	Chip	1.5	1	0.2	Sheared rhyolite, heavy limonite
186	Chip	2.1	1	0.1	Chloritized andesite tuff, minor pyrite
187	Chip	1.8	1	0.1	Rhyolite shear, sericite alt'n, abund. pyrite
188	Chip	1.8	1	0.1	Similar to above
189	Chip	4.0	2	0.1	Chloritized dacite tuff, minor pyrite
190	Chip	9.0	35	1.4	Rhyodacite, locally silicified and with narrow quartz veinlets, abundant pyrite, minor Zn S. (Assayed 4,187 ppm Zn and 1,696 ppm Pb)

Sample No.	Type	Width(m)	Assay Au(ppb)	Ag(ppm)	Description
191	Chip	8.0	6	2.8	Sheared rhyolite, kaolinized, irreg. quartz alt'n, heavy limonite, abund. pyrite (assayed 720 ppm Zn and 249 ppm Cu)
192	Chip	8.0	9	0.1	Andesitic tuff, minor pyrite
193	Chip	2.0	1	0.3	Andesitic tuff, very minor pyrite
194	Grab	-	1	0.1	Ferricrete at 3N, 2+75E (assayed 287 ppm Zn and 922 ppm Cu)

The above samples confirm that while the rhyolitic and dacitic units are well pyritized, they do not contain significant values in precious metals. Samples 190, 191 and 194 returned anomalous values in zinc and copper. This weak mineralization could account for some of the soil geochemical anomalies.

2. Geochemistry

The main significant cobalt soil anomalies were checked in the field. Most occur in areas of damp ground - water seeps, creeks, swampy drainages, etc. Also, many are associated with a hematitic red soil.

Hematitic red soils are well exposed on Sue 1-4 claims in the clear-cut logging area. At several locations, limonitic-rich gossanous material is associated with these soils. This material is either a true iron gossan or ferricrete, a gossan-like material formed by the deposition of limonite by ground water. The source of the iron could be a pyrite or pyrrhotite-rich zone, i.e. mineralized fault or a rock unit, up-slope containing appreciable pyrite and/or pyrrhotite.

Fill-in soil samples were taken to better define the copper-zinc-cobalt anomalies on Sue 1 and 3 claims. A total of 73 soil samples were taken and assayed by Acme Analytical Laboratories by I.C.P. for Cu, Pb, Zn, Co and Ag and by fire assay for Au. Figures 4, 5 and 6 were revised to include these additional assays. As with the previous samples, both gold and silver assays were low and were not plotted.

It is interesting to note that the gossanous areas seen in the field occur both within and beyond the limits of the geochemical anomalies i.e., the limonitic float or ferricrete may not be from the same source as the copper, zinc and cobalt found in the soils.

3. Geophysics

The gossanous material was traced up-slope from the clear-cut for approximately 200 meters as scattered pieces of float. It may continue further but is hidden by moss, organic forest debris, etc.

The writer considered that these gossanous zones might be related to northerly-striking sulphide-rich shear zones. A VLF-EM survey was run due east-west over this area on lines at 125 meter separations. Six lines totalling 5.85 kms were surveyed, with readings taken at each 25 meter station. Results of this survey are shown in profile form on Figure 7.

The VLF-EM data shows a number of weak possible conductors, none of which are thought to reflect a well mineralized shear zone. (S. Vissar - Personal Communication).

4. Miscellaneous

Richmond Plywood Co., the loggers in the area, plan to build new logging roads above and to the east of the present clear-cut. This work might serve the purpose of trenching and open up new rock exposures within a part of the geochemically anomalous areas.

Conclusions

The results of the follow-up field program indicate that the geochemical soil anomalies are probably transported from a source either up slope, along the regional strike, or at depth. While several rock samples did assay anomalous in copper and zinc, many did not, suggesting that the underlying rock is not sufficiently well mineralized to be the source of the anomalies.

Additional exploration is warranted to explore up slope from the present grid. This work should consist of geochemical rock and soil sampling followed by induced polarization surveys in areas of interest.

Respectfully submitted

Harold M. Jones, P.Eng.

October 25, 1988

APPENDIX I

ASSAY CERTIFICATES AND HISTOGRAMS

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P21 SOIL P22 ROCK AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: MAY 13 1988 DATE REPORT MAILED: May 19/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

HAROLD M. JONES PROJECT-WHISTLER File # 88-1426 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L15+00N 10+00W	1	57	20	235	.1	9	11	874	2.93	2	5	ND	2	25	1	2	3	61	.25	.041	4	13	1.23	112	.20	6	2.85	.02	.17	1	1
L15+00N 9+75W	1	67	22	258	.1	10	12	774	3.43	9	5	ND	2	25	1	2	2	71	.24	.050	3	11	1.32	118	.19	3	3.36	.02	.14	1	1
L15+00N 9+50W	1	95	24	255	.2	12	14	855	3.75	2	5	ND	2	29	1	2	2	75	.27	.083	3	10	1.57	177	.19	2	4.38	.02	.18	1	1
L15+00N 9+25W	1	40	28	242	.4	7	9	672	3.05	2	5	ND	2	19	1	2	2	58	.17	.108	3	10	1.18	113	.19	5	2.91	.01	.08	1	11
L15+00N 9+00W	1	28	22	151	.1	6	6	694	2.96	2	5	ND	2	18	1	2	2	61	.17	.099	3	10	.97	69	.19	2	1.86	.01	.07	1	3
L15+00N 8+75W	1	69	28	190	.3	7	10	748	3.56	2	5	ND	2	21	1	2	2	73	.18	.085	3	12	1.25	123	.19	2	3.41	.02	.11	1	2
L15+00N 8+50W	1	23	15	172	.1	5	8	1131	2.56	2	5	ND	1	16	1	2	3	53	.16	.052	3	10	.99	77	.18	3	2.27	.01	.06	1	1
L15+00N 8+25W	1	36	29	171	.1	6	9	824	3.16	2	5	ND	2	24	1	2	2	67	.18	.077	3	11	1.10	114	.19	2	2.80	.02	.09	1	1
L15+00N 8+00W	1	62	30	232	.3	9	11	1199	3.25	2	5	ND	2	23	1	2	3	65	.21	.062	4	12	1.38	150	.20	8	3.24	.01	.11	1	1
L15+00N 7+75W	1	75	36	156	.1	8	10	811	3.61	8	5	ND	3	20	1	2	2	75	.18	.050	4	12	1.31	108	.21	2	3.46	.01	.08	1	1
L15+00N 7+25W	1	51	22	185	.3	7	8	868	2.92	2	5	ND	2	20	1	2	2	60	.19	.060	3	10	1.07	101	.18	5	2.84	.01	.09	1	1
L15+00N 6+75W	1	44	35	463	.4	7	14	2602	2.90	2	5	ND	2	24	1	2	2	50	.26	.118	4	10	.99	191	.13	2	2.50	.01	.10	1	1
L15+00N 6+50W	2	88	67	469	.6	8	17	1463	3.39	2	5	ND	2	28	1	7	3	55	.25	.103	4	11	1.16	194	.13	2	3.00	.01	.13	1	1
L15+00N 6+25W	2	59	43	256	.2	5	10	895	2.72	2	5	ND	2	24	1	2	2	46	.24	.062	3	9	1.13	102	.12	2	1.70	.02	.11	1	1
L15+00N 6+00W	2	148	64	645	.4	10	21	4411	3.92	6	5	ND	3	32	3	2	2	53	.32	.105	6	9	1.21	224	.14	7	2.87	.02	.22	1	6
L15+00N 5+75W	3	113	88	366	.5	8	20	2028	3.83	2	5	ND	3	36	1	2	2	47	.31	.110	6	11	1.28	148	.13	2	2.73	.01	.15	1	9
L15+00N 5+50W	2	164	91	556	.8	11	23	2330	3.88	2	5	ND	2	65	3	2	2	50	.89	.120	9	10	1.20	240	.13	10	2.83	.02	.21	1	16
L15+00N 5+25W	4	218	73	614	.6	12	29	2057	5.16	7	5	ND	3	29	1	2	2	55	.27	.113	9	10	1.39	159	.14	2	3.26	.01	.14	1	7
L15+00N 5+00W	4	338	66	803	.6	12	25	1620	4.46	7	5	ND	4	35	1	2	2	59	.32	.082	11	12	1.39	162	.15	3	3.18	.02	.15	1	6
L15+00N 4+75W	1	42	16	191	.1	8	14	1006	3.02	2	5	ND	3	27	1	2	3	59	.26	.052	3	21	1.08	122	.17	6	2.86	.02	.08	1	1
L15+00N 4+50W	1	35	17	170	.1	8	14	926	2.93	2	5	ND	2	26	1	2	2	58	.25	.043	3	12	1.02	112	.17	4	2.77	.01	.07	1	3
L15+00N 4+25W	1	97	15	174	.1	10	13	960	3.49	4	5	ND	2	28	1	8	3	71	.26	.051	4	13	1.43	135	.20	2	3.32	.01	.13	1	2
L15+00N 4+00W	1	54	13	217	.1	11	15	1028	3.52	4	5	ND	1	26	1	2	2	69	.24	.085	3	14	1.42	188	.19	2	3.30	.01	.12	1	1
L15+00N 3+75W	1	33	13	111	.3	7	10	1060	2.88	2	5	ND	1	27	1	2	2	62	.24	.039	4	10	.96	120	.17	2	1.78	.01	.09	1	1
L15+00N 3+50W	1	68	13	156	.1	7	10	1099	2.95	2	5	ND	2	29	1	2	2	62	.26	.040	3	11	1.34	106	.19	2	2.75	.01	.16	1	1
L15+00N 3+25W	1	47	14	246	.1	9	16	1047	3.20	2	5	ND	2	29	1	3	2	62	.28	.053	3	12	1.21	151	.19	5	3.00	.01	.11	1	1
L15+00N 3+00W	1	19	10	230	.1	6	13	2202	2.57	2	5	ND	1	31	1	2	4	52	.27	.062	4	9	.69	229	.16	2	1.71	.01	.09	1	1
L15+00N 2+75W	1	30	15	159	.1	7	9	2594	2.47	2	5	ND	1	31	1	2	2	52	.31	.097	3	13	.76	140	.14	3	1.54	.01	.11	1	4
L15+00N 2+50W	1	28	8	182	.1	7	12	2031	2.64	3	5	ND	1	29	1	2	2	50	.29	.081	3	11	1.01	187	.14	2	1.85	.01	.16	1	1
L15+00N 2+25W	1	68	13	148	.1	7	12	1165	2.76	2	5	ND	2	29	1	2	2	53	.27	.083	4	11	1.16	137	.15	4	2.75	.01	.15	1	1
L15+00N 2+00W	1	122	14	211	.1	12	12	951	3.66	8	5	ND	1	39	1	2	4	66	.35	.146	4	13	1.53	195	.18	2	3.41	.01	.22	1	9
L15+00N 1+75W	1	79	12	148	.1	9	11	1778	3.05	2	5	ND	2	29	1	2	2	61	.28	.083	4	12	1.14	174	.15	2	2.91	.01	.14	1	2
L15+00N 1+50W	1	44	11	197	.1	6	8	1624	2.28	2	5	ND	1	25	1	2	2	48	.23	.064	4	10	.71	125	.13	2	1.70	.01	.10	1	3
L15+00N 1+25W	1	66	17	168	.1	8	12	1013	3.64	7	5	ND	2	23	1	2	2	73	.24	.096	3	13	1.48	133	.22	2	3.38	.01	.11	1	1
L15+00N 1+00W	1	35	18	202	.1	7	12	4110	2.75	2	5	ND	1	25	1	2	2	56	.26	.082	4	11	1.05	239	.18	2	2.72	.02	.11	1	2
L15+00N 0+75W	1	36	13	239	.1	9	14	2280	2.93	2	5	ND	1	21	1	2	3	56	.24	.112	3	12	1.06	159	.18	2	2.77	.01	.08	1	6
STD C/AU-S	20	64	42	132	7.4	72	31	1070	4.04	41	22	7	40	52	19	17	23	64	.47	.093	39	60	.95	181	.08	33	1.81	.07	.14	14	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L15+00N 1+50W	1	37	13	136	.1	6	13	2178	3.04	2	5	ND	1	22	1	2	3	58	.24	.112	3	10	1.07	155	.16	2	2.74	.01	.08	1	1
L15+00N 1+25W	1	49	14	136	.1	10	13	2104	3.30	2	5	ND	1	25	1	2	2	58	.28	.083	3	14	1.26	176	.20	2	2.74	.01	.09	1	1
L15+00N 1+00W	1	35	26	240	.1	8	13	4334	2.83	2	5	ND	1	26	1	2	2	37	.27	.083	3	10	.98	384	.07	2	2.09	.02	.12	1	3
L14+00N 10+00W	3	67	107	170	.4	5	10	854	3.20	2	5	ND	1	28	1	4	3	36	.19	.075	4	9	1.02	70	.09	2	1.41	.01	.09	1	17
L14+00N 9+50W	3	65	90	229	.4	7	10	906	3.31	2	5	ND	2	28	1	2	3	42	.29	.107	4	10	.93	101	.10	2	1.45	.01	.21	1	27
L14+00N 9+25W	1	109	47	302	.4	8	14	2002	3.25	2	5	ND	3	40	2	2	3	53	.46	.107	6	11	1.12	155	.13	4	2.52	.02	.18	1	14
L14+00N 9+00W	2	53	70	172	.3	5	8	1837	2.55	2	5	ND	1	29	1	2	2	32	.33	.068	4	8	.94	79	.05	5	1.13	.01	.11	1	12
L14+00N 8+75W	3	57	84	196	.4	5	10	1752	2.95	2	5	ND	1	31	1	2	3	31	.38	.096	4	8	1.08	76	.08	5	1.34	.01	.12	1	18
L14+00N 8+50W	3	78	95	220	.3	6	12	1696	3.65	5	5	ND	1	33	1	2	2	37	.38	.121	5	9	1.39	73	.09	5	1.57	.01	.13	1	16
L14+00N 8+25W	4	66	109	309	.5	7	15	1294	3.73	2	5	ND	1	28	1	2	2	34	.31	.053	5	10	1.21	112	.09	2	1.55	.01	.11	1	35
L14+00N 8+00W	3	140	75	397	.5	10	18	1873	3.31	2	5	ND	1	47	1	2	3	44	.52	.089	7	12	1.11	132	.11	2	1.79	.01	.18	1	7
L14+00N 7+75W A	2	136	84	332	.5	9	18	1813	3.57	2	5	ND	1	35	2	2	2	46	.29	.097	7	10	1.25	132	.11	2	2.26	.01	.15	1	8
L14+00N 7+75W B	3	125	91	317	.2	11	16	1682	3.53	6	5	ND	1	41	1	2	2	43	.53-	.102	6	11	1.26	139	.11	2	1.83	.01	.20	1	3
L14+00N 7+50W	2	143	84	351	.8	9	19	1611	3.55	2	5	ND	1	34	1	2	2	45	.27	.085	7	13	1.24	136	.10	2	2.47	.01	.26	1	1
L14+00N 7+25W	4	161	101	327	.4	9	19	1698	3.88	2	5	ND	1	42	1	2	3	42	.41	.105	8	11	1.34	122	.11	2	2.25	.01	.23	1	27
L14+00N 7+00W	3	172	55	446	.1	10	23	2108	4.04	2	5	ND	2	29	1	22	2	51	.31	.115	5	11	1.36	152	.12	2	2.94	.01	.15	1	16
L14+00N 6+75W	2	147	73	456	.2	5	21	2629	3.80	2	5	ND	1	30	1	2	2	49	.37	.132	5	10	1.27	134	.11	2	2.85	.01	.14	1	1
L14+00N 6+50W	1	71	16	207	.3	8	12	1908	2.74	2	5	ND	1	26	1	2	3	47	.30	.069	4	10	1.03	122	.12	3	1.43	.01	.11	1	3
L14+00N 6+25W	1	47	22	156	.2	7	10	1812	2.62	2	5	ND	1	25	1	2	4	51	.29	.054	2	9	.99	113	.15	7	2.46	.01	.10	1	3
L14+00N 6+00W	1	42	12	170	.1	8	10	943	3.25	2	5	ND	1	28	1	2	2	65	.27	.090	2	11	1.01	136	.15	2	2.91	.01	.10	1	1
L14+00N 5+75W	1	41	24	204	.1	11	10	634	3.15	2	5	ND	1	22	1	2	2	61	.28	.064	3	12	.96	104	.18	2	2.90	.01	.08	1	1
L14+00N 5+50W	1	42	14	150	.2	9	12	710	3.21	2	5	ND	2	28	1	6	2	64	.27	.065	3	14	1.17	116	.19	5	2.90	.01	.11	1	1
L14+00N 5+25W	1	35	15	133	.1	8	11	692	3.02	2	5	ND	1	27	1	2	2	61	.27	.074	3	11	1.07	115	.18	6	2.71	.01	.10	1	1
L14+00N 5+00W	1	84	17	122	.1	4	10	613	3.10	2	5	ND	2	28	1	2	2	62	.25	.044	3	12	1.19	123	.18	2	3.06	.01	.12	1	1
L14+00N 4+75W	1	49	9	152	.1	8	10	757	2.91	2	5	ND	1	22	1	2	2	56	.21	.087	3	11	1.01	117	.15	2	2.84	.01	.09	1	1
L14+00N 4+50W	1	53	10	109	.1	7	11	659	3.02	2	5	ND	1	32	1	2	3	64	.27	.024	3	10	1.04	92	.17	2	2.34	.01	.09	1	1
L14+00N 4+25W	1	57	11	134	.1	9	12	1050	3.32	2	5	ND	1	27	1	16	2	67	.29	.085	3	13	1.54	136	.20	2	3.04	.02	.12	1	1
L14+00N 4+00W	1	52	3	156	.1	8	12	1775	3.35	2	5	ND	1	25	1	6	2	66	.24	.065	3	12	.98	117	.17	2	3.09	.01	.10	1	2
L14+00N 3+75W	1	34	10	123	.1	7	9	759	3.29	2	5	ND	1	23	1	2	2	71	.24	.083	3	12	.94	94	.18	2	2.78	.01	.10	1	1
L14+00N 3+50W	1	52	12	187	.1	10	11	1053	1.65	2	5	ND	2	25	1	2	2	68	.26	.205	3	13	1.32	143	.20	2	3.52	.01	.12	1	1
L14+00N 3+25W	1	30	15	157	.3	9	9	1054	2.62	2	5	ND	2	20	1	2	3	53	.27	.083	3	11	.72	120	.17	3	2.46	.01	.06	1	1
L14+00N 3+00W	1	25	13	155	.1	6	8	813	2.86	2	5	ND	1	22	1	2	2	60	.24	.080	3	10	1.03	119	.19	2	2.67	.01	.08	1	1
L14+00N 2+75W	1	21	12	122	.1	5	9	731	2.52	2	5	ND	1	19	1	2	3	49	.20	.049	3	9	.71	104	.15	2	1.62	.01	.06	2	5
L14+00N 2+50W	1	32	20	241	.1	9	13	1055	2.89	2	5	ND	1	20	1	2	2	57	.24	.042	3	11	1.19	113	.22	2	2.30	.01	.07	1	1
L14+00N 2+25W	1	35	16	206	.1	7	10	1340	2.82	2	5	ND	1	20	1	2	2	55	.25	.063	3	11	1.13	144	.16	2	2.64	.01	.10	1	6
L14+00N 2+00W	1	27	15	132	.1	6	10	1539	2.83	2	5	ND	1	18	2	2	2	53	.20	.141	3	9	.98	91	.18	2	2.46	.01	.06	1	2
STD C/AU-S	19	63	42	132	7.4	72	31	1064	4.05	36	21	8	40	51	18	17	21	62	.47	.096	39	61	.96	180	.28	33	1.50	.07	.14	14	49

HAROLD M. JONES PROJECT-WHISTLER FILE # 88-1426

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L14+00N 1+75W	1	45	20	288	.1	10	11	1050	3.19	5	5	ND	1	28	1	2	2	63	.28	.048	4	12	1.33	130	.17	2	2.31	.02	.09	1	1
L14+00N 1+50W	8	386	29	1058	.1	22	96	4001	6.97	7	5	ND	1	46	3	2	2	55	.48	.069	24	9	1.13	180	.13	17	3.88	.01	.16	1	3
L14+00N 1+25W	5	279	27	498	.1	12	39	1387	4.58	3	5	ND	1	36	1	2	2	57	.32	.049	10	10	1.25	138	.15	3	3.28	.01	.14	1	2
L14+00N 1+00W	1	79	19	158	.1	13	12	1006	3.62	2	5	ND	1	29	1	2	2	67	.26	.044	4	8	1.35	125	.18	2	3.02	.01	.14	1	1
L14+00N 0+75W	1	41	21	146	.1	7	9	1297	3.15	2	5	ND	1	27	1	2	3	58	.25	.089	4	10	1.11	156	.15	2	2.51	.01	.12	1	9
L14+00N 0+50W	1	47	16	143	.1	10	9	974	3.56	2	5	ND	1	27	1	2	2	69	.24	.055	3	8	1.40	139	.18	8	2.90	.02	.10	1	2
L14+00N 0+25W	1	30	18	109	.2	7	8	1025	2.94	3	5	ND	1	27	1	2	5	57	.23	.069	4	6	.91	184	.14	2	2.19	.01	.12	1	53
L14+00N 0+00W	1	39	19	139	.1	11	9	1488	3.46	2	5	ND	1	28	1	2	2	69	.28	.056	4	12	1.25	142	.18	5	2.67	.02	.12	1	1
L13+00N 8+75W	3	118	92	392	1.0	10	19	1968	3.73	12	5	ND	1	41	1	2	2	42	.48	.106	7	8	1.25	141	.09	5	2.27	.01	.18	1	8
L13+00N 8+50W	4	181	99	396	.6	15	22	1772	4.09	15	5	ND	1	34	1	2	2	39	.30	.098	10	17	1.43	115	.09	4	2.47	.01	.19	1	17
L13+00N 8+25W	3	226	108	406	.9	11	31	2364	4.07	10	5	ND	1	43	1	2	3	41	.46	.117	13	10	1.20	149	.08	8	2.57	.01	.20	2	28
L13+00N 8+00W	3	150	87	354	.1	12	16	1283	3.58	8	5	ND	1	34	1	2	2	40	.30	.078	7	16	1.29	109	.10	10	1.90	.01	.20	1	10
L13+00N 7+75W	4	124	139	268	.6	9	17	1522	4.30	13	5	ND	1	35	1	2	2	42	.35	.081	7	8	1.56	107	.11	4	2.44	.01	.18	1	21
L13+00N 7+25W	3	53	71	184	.2	3	5	1412	2.97	11	5	ND	1	24	1	2	2	39	.18	.076	4	7	.86	86	.08	7	1.77	.01	.09	2	2
L13+00N 7+00W	1	71	28	112	.2	9	9	1248	3.62	6	5	ND	1	37	1	2	2	70	.21	.142	5	12	1.00	157	.12	5	2.95	.01	.15	1	1
L13+00N 6+75W	1	78	15	166	.2	11	10	983	3.18	2	5	ND	2	24	1	2	2	62	.21	.056	4	10	1.16	106	.15	3	3.23	.01	.09	1	1
L13+00N 6+50W	1	156	13	170	.1	12	14	827	3.85	2	5	ND	1	32	1	2	2	74	.25	.050	5	11	1.40	155	.17	5	3.77	.01	.20	2	12
L13+00N 6+25W	1	67	22	164	.2	12	11	690	3.65	2	5	ND	1	23	1	2	2	71	.21	.040	3	9	1.37	104	.18	2	3.46	.01	.10	1	1
L13+00N 6+00W	1	65	23	173	.1	14	12	536	3.36	2	5	ND	1	20	1	2	3	64	.18	.024	3	16	1.07	87	.17	2	3.03	.01	.07	1	3
L13+00N 5+75W	1	11	15	65	.1	9	5	420	1.96	2	5	ND	1	19	1	2	2	46	.17	.020	3	14	.39	48	.14	2	1.15	.01	.05	2	1
L13+00N 5+50W	1	23	17	125	.1	8	9	521	2.85	2	5	ND	1	19	1	2	2	56	.16	.024	3	7	.73	81	.16	5	2.23	.01	.06	1	1
L13+00N 5+00W	1	52	16	155	.1	9	10	786	3.36	2	5	ND	1	23	1	2	4	67	.23	.039	4	9	1.17	129	.16	6	3.05	.01	.10	1	1
L13+00N 4+75W	1	32	10	188	.1	7	8	1053	3.23	2	5	ND	1	23	1	2	4	63	.23	.060	3	11	1.05	127	.18	5	2.58	.01	.08	1	1
L13+00N 4+50W	1	26	15	187	.1	9	9	1180	3.08	2	5	ND	1	22	1	2	2	61	.22	.048	3	11	1.00	130	.18	2	2.39	.01	.07	2	26
L13+00N 4+25W	1	87	24	159	.1	8	11	1574	3.37	2	5	ND	1	33	1	2	2	65	.34	.120	4	9	1.29	207	.15	2	3.25	.02	.18	1	5
L13+00N 4+00W	1	31	15	152	.1	9	9	895	2.80	2	5	ND	1	26	1	2	4	55	.25	.062	4	9	.93	117	.15	2	2.22	.01	.09	1	3
L13+00N 3+75W	1	79	20	239	.1	13	17	1208	3.18	2	5	ND	1	27	1	2	2	59	.25	.045	4	12	1.07	130	.16	2	3.24	.01	.07	1	1
L13+00N 3+50W	2	104	29	592	.2	16	12	1263	3.41	2	5	ND	1	45	3	2	2	60	.48	.054	5	25	1.30	162	.14	6	2.60	.02	.29	1	1
L13+00N 3+25W	2	149	20	907	.1	8	15	1123	3.78	2	5	ND	1	53	3	2	2	67	.53	.048	6	10	1.57	198	.16	3	3.03	.02	.40	2	6
L13+00N 3+00W	2	130	24	887	.2	11	13	1145	3.68	2	5	ND	2	57	3	2	2	66	.58	.047	6	11	1.57	190	.16	7	2.90	.02	.42	1	1
L13+00N 2+75W	3	68	23	312	.1	7	30	987	13.08	10	5	ND	2	35	1	2	2	64	.30	.064	10	8	.83	126	.14	2	3.55	.01	.11	1	2
L13+00N 2+50W	1	72	15	138	.2	7	11	906	3.28	2	5	ND	2	35	1	2	2	60	.29	.056	6	10	1.25	129	.15	5	2.72	.01	.14	1	1
L13+00N 2+25W	1	38	20	143	.1	7	10	868	2.97	3	5	ND	1	31	1	2	2	30	.26	.072	4	8	1.09	130	.14	3	2.25	.01	.08	2	1
L13+00N 2+00W	1	40	16	146	.1	8	10	922	2.99	2	5	ND	1	31	1	2	2	51	.26	.073	4	8	1.09	134	.15	8	2.31	.01	.06	1	1
L13+00N 1+75W	1	36	22	146	.2	9	9	932	2.93	2	5	ND	2	31	1	2	4	50	.27	.074	4	9	1.06	131	.14	6	2.22	.01	.08	1	3
L13+00N 1+50W	1	24	11	121	.1	5	8	2567	2.56	2	5	ND	1	29	1	2	2	50	.28	.042	3	8	.82	147	.14	5	1.77	.01	.08	1	10
STD C/AU-S	19	59	41	132	7.1	71	30	1067	3.97	39	19	8	39	51	18	16	23	61	.45	.088	41	60	.93	180	.07	37	1.88	.07	.14	13	50

HAROLD M. JONES PROJECT-WHISTLER FILE # 88-1426

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L13+00N 1+25W	2	227	47	396	.1	12	33	2002	3.79	2	5	ND	2	39	1	2	2	61	.33	.052	7	13	1.47	202	.18	2	3.40	.01	.25	1	3
L13+00N 1+00W	1	155	20	502	.1	12	28	814	3.46	2	5	ND	2	28	1	6	3	56	.26	.033	4	11	1.20	133	.18	3	3.25	.01	.12	1	1
L13+00N 0+75W	2	304	17	245	.1	11	29	957	3.67	2	5	ND	2	31	1	4	3	60	.28	.033	7	12	1.46	138	.17	3	3.36	.01	.15	1	1
L13+00N 0+50W	1	95	14	239	.6	9	19	1191	3.15	2	5	ND	1	27	1	20	2	55	.23	.047	4	12	1.31	172	.17	5	3.35	.01	.12	1	1
L13+00N 0+25W	3	472	24	228	.3	15	54	1075	3.82	2	5	ND	3	27	1	2	2	57	.21	.051	11	12	1.22	174	.26	2	4.30	.01	.13	1	4
L13+00N 0+00W	1	96	13	216	.5	9	20	1145	3.00	2	5	ND	2	25	1	9	3	53	.22	.040	4	10	1.26	166	.16	5	3.23	.01	.12	1	1
L12+00N 8+50W	2	435	18	810	.7	24	67	4155	6.09	2	5	ND	4	67	5	2	2	52	.71	.191	39	13	1.25	259	.21	2	4.43	.01	.32	1	2
L12+00N 8+25W	2	526	20	904	.8	27	93	4421	6.20	2	5	ND	5	60	6	2	2	49	.59	.100	39	13	1.18	236	.12	2	4.62	.01	.29	1	5
L12+00N 7+75W	2	159	19	336	.3	9	20	1130	4.25	2	5	ND	2	42	1	2	2	59	.38	.079	8	12	1.21	179	.13	2	3.03	.02	.35	1	91
L12+00N 7+50W	2	124	15	291	.3	8	16	569	2.82	2	5	ND	1	39	1	2	2	56	.36	.071	5	12	1.16	165	.12	2	2.69	.01	.32	1	4
L12+00N 7+00W	1	97	12	231	.2	6	14	698	3.35	4	5	ND	2	30	1	2	2	53	.27	.059	5	11	1.00	116	.11	5	1.74	.02	.28	1	15
L12+00N 6+75W	2	188	17	237	.1	10	24	1635	4.15	2	5	ND	1	28	1	2	2	61	.21	.070	7	12	1.27	172	.16	2	3.53	.01	.19	1	1
L12+00N 6+50W	6	529	20	162	.5	10	57	1903	9.48	2	5	ND	6	22	2	2	2	58	.22	.082	21	14	.89	117	.15	2	4.49	.01	.14	1	2
L12+00N 6+25W	1	113	17	170	.1	9	15	769	4.20	5	5	ND	1	23	1	2	2	79	.20	.088	4	12	1.56	134	.23	2	4.13	.01	.10	1	11
L12+00N 5+75W	1	62	16	281	.3	9	13	1603	3.53	2	5	ND	1	28	1	16	2	64	.26	.098	3	12	1.27	157	.18	2	3.39	.01	.11	1	3
L12+00N 5+50W	1	23	10	173	.1	6	10	1342	2.37	5	5	ND	1	23	1	2	3	45	.24	.072	3	9	.93	128	.12	2	1.95	.01	.07	1	1
L12+00N 5+00W	1	24	11	134	.1	6	9	478	2.62	3	5	ND	1	17	1	2	2	52	.17	.020	3	10	.75	93	.16	2	1.92	.01	.05	1	1
L12+00N 4+75W	1	65	23	157	.1	8	11	802	3.47	2	5	ND	1	27	1	2	2	60	.24	.116	3	13	1.22	132	.17	6	3.28	.01	.13	1	3
L12+00N 4+50W	1	78	36	237	.1	7	13	1804	2.76	8	5	ND	1	32	2	2	2	41	.35	.075	3	9	.84	155	.10	2	1.85	.01	.13	1	10
L12+00N 3+75W	1	65	13	161	.1	9	16	806	2.99	2	5	ND	2	24	2	2	2	50	.18	.102	4	11	1.00	103	.14	2	3.22	.01	.09	1	12
L12+00N 3+25W	1	15	12	133	.1	6	12	1125	2.13	2	5	ND	1	18	1	2	2	40	.18	.059	3	9	.52	101	.12	2	1.51	.01	.07	1	10
L12+00N 3+00W	1	41	14	95	.1	6	8	696	2.44	4	5	ND	1	23	1	2	2	44	.20	.036	3	10	.80	100	.12	2	1.74	.01	.08	1	9
L12+00N 2+75W	1	51	17	103	.1	7	8	723	2.66	5	5	ND	1	25	1	2	2	48	.21	.035	3	10	.91	112	.13	2	1.96	.01	.08	1	1
L12+00N 2+50W	1	68	18	162	.1	8	9	770	2.89	2	5	ND	1	34	1	2	2	54	.28	.035	3	11	1.29	126	.16	2	3.23	.01	.13	1	2
L12+00N 2+00W	6	813	30	289	.4	12	124	4395	8.78	2	5	ND	3	52	2	2	2	68	.30	.078	17	14	1.12	178	.12	2	3.46	.01	.13	1	5
L12+00N 1+75W	1	95	15	136	.1	7	14	895	3.02	2	5	ND	1	30	1	2	2	53	.25	.051	4	11	1.17	114	.14	2	3.05	.01	.13	1	1
L12+00N 1+50W	1	71	20	123	.1	8	9	920	3.13	2	5	ND	1	48	1	2	3	55	.29	.062	4	11	1.30	202	.15	2	3.12	.01	.18	1	2
L12+00N 1+25W	1	128	22	175	.1	8	20	922	3.45	2	5	ND	1	30	1	2	2	56	.21	.053	4	11	1.08	121	.15	2	2.99	.01	.09	1	1
L12+00N 0+75W	2	114	17	276	.1	10	15	828	3.50	2	5	ND	1	27	1	22	2	61	.23	.035	5	12	1.31	124	.18	2	3.30	.01	.11	1	1
L12+00N 0+50W	1	71	15	134	.1	7	10	878	3.19	2	5	ND	1	33	1	2	3	59	.29	.037	3	13	1.39	168	.17	3	2.96	.01	.11	1	2
L12+00N 0+25W	3	275	30	227	.1	12	63	2332	4.20	2	5	ND	1	34	1	2	2	58	.27	.068	5	13	.99	230	.15	2	3.42	.01	.10	1	1
L12+00N 0+00W	2	248	33	231	.1	11	60	3047	4.04	2	5	ND	2	38	1	8	2	56	.30	.062	5	11	.95	249	.15	2	3.27	.01	.10	1	1
L11+00N 8+00W	3	793	19	1024	.5	38	102	4893	7.63	3	5	ND	5	32	5	2	2	58	.26	.110	54	15	1.23	239	.14	2	5.36	.01	.18	1	5
L11+00N 7+75W	1	115	21	277	.1	10	22	1604	3.99	2	5	ND	1	25	1	18	2	59	.19	.071	6	12	1.00	168	.15	2	3.23	.01	.10	1	1
L11+00N 7+50W	1	62	16	244	.2	8	17	1189	3.38	2	5	ND	1	25	1	2	2	51	.18	.071	3	11	.92	154	.13	2	2.94	.01	.10	1	1
L11+00N 7+00W	1	25	14	127	.1	5	7	742	2.94	4	5	ND	1	15	1	2	2	56	.14	.030	2	9	.85	62	.15	2	1.92	.01	.05	1	1
STD C/AU-S	19	63	38	132	7.4	72	31	1070	4.13	38	19	6	40	52	18	17	21	63	.48	.091	39	61	.97	180	.06	31	1.34	.07	.14	13	50

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L11+00N 6+75W	1	35	18	116	.1	7	8	871	3.26	2	5	ND	1	25	1	8	4	64	.16	.089	3	10	.93	121	.18	2	3.28	.01	.09	1	1
L11+00N 6+50W	1	27	19	78	.2	5	5	411	3.10	2	5	ND	2	18	1	2	2	62	.13	.112	4	9	.64	79	.19	4	2.70	.01	.08	1	1
L11+00N 5+75W	1	113	18	115	.1	7	12	795	3.57	2	5	ND	1	42	1	2	2	60	.24	.059	5	11	1.17	176	.16	2	3.10	.01	.33	1	4
L11+00N 5+25W	1	23	8	93	.1	5	7	952	2.25	2	5	ND	1	19	1	2	2	48	.17	.036	3	6	.68	75	.15	6	1.67	.01	.07	1	1
L11+00N 4+50W	1	110	25	115	.6	11	12	1129	3.08	2	5	ND	3	29	1	2	2	55	.22	.032	5	13	1.31	152	.19	5	3.69	.01	.12	1	2
L11+00N 4+00W	1	35	20	157	.3	9	11	1224	2.82	2	5	ND	1	34	1	2	3	52	.23	.055	4	11	.96	139	.15	2	3.02	.01	.07	1	1
L11+00N 3+75W	1	111	17	98	.1	8	13	791	3.09	2	5	ND	1	37	1	2	2	60	.24	.063	4	12	1.35	184	.15	6	3.41	.01	.39	1	2
L11+00N 3+50W	1	80	16	119	.2	7	9	1479	2.74	2	5	ND	1	68	1	2	5	52	.45	.045	4	11	1.10	204	.12	12	3.05	.01	.27	1	7
L11+00N 3+25W	1	103	15	104	.1	8	9	841	3.07	2	5	ND	1	62	1	2	2	57	.35	.045	5	11	1.22	235	.14	2	3.16	.01	.46	1	1
L11+00N 3+00W	1	91	12	129	.1	9	10	1703	3.06	2	5	ND	1	54	1	2	5	56	.21	.080	4	12	1.23	213	.15	4	3.25	.01	.30	1	29
L11+00N 2+75W	1	78	24	128	.1	9	11	1540	2.86	2	5	ND	1	35	1	2	2	54	.30	.060	4	11	1.18	173	.15	3	3.19	.01	.19	1	2
L11+00N 2+50W	1	53	19	134	.1	9	12	1038	3.07	2	5	ND	1	26	1	6	2	55	.25	.039	3	12	1.10	154	.17	6	3.21	.01	.07	1	1
L11+00N 2+25W	1	62	16	116	.2	9	11	749	3.00	2	5	ND	2	22	1	2	2	57	.19	.041	3	10	.97	105	.15	2	3.23	.01	.08	1	1
L11+00N 2+00W	1	32	17	148	.1	8	15	1149	2.52	7	5	ND	1	23	1	2	2	47	.19	.035	4	9	.73	106	.15	5	1.57	.01	.06	1	1
L11+00N 1+50W	1	26	10	204	.1	8	14	1017	3.16	2	5	ND	1	22	1	2	2	68	.21	.042	3	12	1.07	95	.22	2	3.17	.01	.06	1	1
L11+00N 1+00W	1	33	12	235	.1	8	14	680	3.56	2	5	ND	1	24	1	2	2	73	.21	.050	3	12	1.05	105	.24	2	3.11	.01	.07	1	2
L11+00N 0+75W	1	33	15	236	.2	10	14	1025	2.97	2	5	ND	1	22	1	2	2	61	.22	.023	3	13	1.16	80	.21	2	3.13	.01	.08	1	1
L11+00N 0+50W	1	35	11	395	.1	14	21	1432	3.17	2	5	ND	1	26	1	25	2	62	.24	.041	3	12	1.11	116	.21	2	3.46	.01	.08	1	1
L11+00N 0+25W	1	44	13	392	.1	13	22	1979	3.30	2	5	ND	1	21	1	2	2	62	.17	.097	4	13	1.00	149	.19	2	3.32	.01	.05	1	1
L10+00N 5+75W	2	166	16	144	.3	8	19	762	4.08	2	5	ND	3	47	1	2	2	65	.20	.069	12	11	1.21	223	.17	3	3.44	.01	.21	1	4
L10+00N 5+50W	3	181	18	152	.2	8	18	630	4.49	4	5	ND	2	32	1	2	2	69	.17	.101	9	12	1.09	141	.20	8	3.75	.01	.13	1	2
L10+00N 5+25W	3	216	19	127	.5	9	22	684	4.55	2	5	ND	2	41	1	2	2	69	.21	.062	9	13	1.20	197	.16	2	3.72	.02	.16	1	5
L10+00N 5+00W	2	115	19	254	.3	12	20	761	3.89	2	5	ND	2	31	1	2	4	65	.21	.061	5	12	1.17	147	.18	2	3.83	.01	.11	1	1
L10+00N 4+50W	2	150	21	323	.1	14	29	806	4.12	2	5	ND	2	33	1	2	2	65	.22	.075	6	13	1.16	153	.18	2	5.00	.01	.12	1	16
L10+00N 4+25W	2	133	15	312	.1	14	27	847	4.01	2	5	ND	1	31	1	2	2	65	.21	.074	6	14	1.13	146	.18	2	4.50	.01	.12	1	1
L10+00N 3+25W	1	94	8	103	.2	9	11	655	3.93	2	5	ND	2	90	1	2	2	78	.31	.075	4	15	1.13	263	.15	8	3.54	.01	.35	1	1
L10+00N 3+00W	1	57	22	155	.1	9	12	736	2.84	2	5	ND	1	29	1	2	2	49	.24	.068	3	12	1.02	88	.14	5	3.23	.01	.10	1	4
L10+00N 2+50W	1	35	12	214	.1	7	12	2184	2.53	6	5	ND	1	27	1	2	2	47	.24	.087	3	10	.86	173	.14	2	1.86	.01	.07	1	1
L10+00N 2+25W	1	23	8	367	.1	8	15	1195	2.59	6	5	ND	2	32	1	2	2	47	.30	.077	3	11	.81	107	.14	9	1.97	.01	.09	1	1
L10+00N 2+00W	1	25	13	244	.2	9	14	2519	2.46	2	5	ND	1	36	1	2	2	46	.33	.066	3	13	.75	145	.14	5	1.71	.01	.10	1	1
L10+00N 1+75W	1	48	11	287	.1	10	20	1560	2.94	2	5	ND	1	37	1	2	2	53	.28	.042	3	10	.96	162	.15	4	2.47	.01	.10	1	2
L10+00N 1+25W	1	95	18	391	.1	13	15	1441	3.12	2	5	ND	1	52	1	2	2	58	.35	.046	4	13	1.13	167	.16	2	3.03	.01	.13	1	1
L10+00N 1+00W	1	60	8	171	.1	9	10	758	2.97	2	5	ND	1	42	1	2	2	64	.30	.024	3	14	1.16	145	.16	5	3.19	.01	.12	1	3
L10+00N 0+75W	1	28	8	132	.1	6	8	1543	2.32	2	5	ND	1	31	1	2	2	50	.26	.028	3	10	.74	131	.13	2	1.65	.01	.16	1	1
L10+00N 0+50W	1	48	12	199	.1	8	10	759	2.48	6	5	ND	1	41	1	2	2	49	.28	.030	3	11	.94	151	.14	2	1.96	.01	.10	1	5
L10+00N 0+25W	1	85	15	162	.1	10	10	1026	3.19	2	5	ND	1	44	1	2	2	59	.27	.065	5	15	1.06	182	.15	6	3.03	.01	.12	1	3
STD C/AU-S	20	62	41	132	7.1	72	31	1097	4.18	38	18	8	40	53	19	16	22	60	.49	.099	40	61	.88	183	.08	34	1.87	.07	.14	13	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L10+00N 0+25E	2	107	12	149	.1	10	25	1059	3.43	5	5	ND	1	29	1	2	2	59	.24	.065	4	7	1.32	153	.13	7	2.81	.01	.15	1	1
L10+00N 0+50E	1	34	8	390	.1	7	21	1346	3.07	2	5	ND	1	36	1	2	3	45	.23	.135	3	6	.83	207	.11	6	1.30	.01	.12	1	1
L10+00N 0+75E	1	37	7	463	.1	9	20	2703	3.18	6	5	ND	1	31	2	2	2	52	.28	.077	3	7	.92	199	.12	4	1.80	.01	.12	2	1
L10+00N 1+00E	2	47	7	379	.1	10	62	1754	4.26	2	5	ND	1	21	2	2	3	51	.18	.019	6	5	.74	121	.12	4	1.86	.01	.09	2	1
L10+00N 1+25E	26	791	2	221	.6	8	862	9627	20.62	4	8	ND	2	10	2	3	2	6	.11	.088	25	1	.05	39	.01	4	7.19	.01	.02	1	2
L10+00N 2+00E	1	54	4	124	.2	7	34	1604	3.14	5	5	ND	1	31	1	3	2	55	.25	.075	3	7	1.05	323	.10	6	2.22	.03	.14	1	1
L10+00N 2+75E	1	57	5	30	.2	5	8	668	2.76	5	5	ND	2	28	1	2	2	58	.20	.057	3	6	.96	141	.11	5	1.92	.01	.16	1	1
L10+00N 3+00E	1	55	5	82	.1	5	8	722	2.75	2	5	ND	1	29	1	2	3	57	.22	.060	3	6	.97	142	.11	8	1.92	.02	.15	1	43
L9+00N 7-50W	3	205	13	256	.3	12	58	2202	5.84	12	5	ND	1	39	1	5	3	54	.29	.070	11	7	1.05	145	.09	5	2.35	.02	.21	1	1
L9+00N 7+25W	1	89	11	152	.2	7	14	1109	2.62	2	5	ND	1	34	1	2	2	45	.25	.066	4	5	.37	150	.09	6	1.34	.02	.14	1	1
L9-00N 7+00W	2	267	15	172	.2	9	24	1677	3.58	2	5	ND	1	35	1	2	2	57	.26	.119	5	7	1.10	214	.11	6	2.44	.01	.12	1	1
L9+00N 6+75W	1	45	7	80	.1	7	14	505	2.60	2	5	ND	1	23	1	2	2	55	.17	.030	2	8	.89	66	.13	10	1.93	.01	.07	1	2
L9+00N 6+50W	1	69	7	92	.2	9	18	634	3.10	2	5	ND	2	25	1	2	2	60	.16	.028	3	9	1.00	89	.14	11	2.60	.02	.07	1	1
L9+00N 6+25W	1	51	8	107	.1	7	8	606	3.23	2	5	ND	1	24	1	2	3	66	.18	.070	2	10	.90	113	.12	6	2.45	.01	.08	1	1
L9+00N 5+75W	1	52	6	99	.2	7	7	601	2.95	2	5	ND	1	24	1	2	2	59	.17	.066	2	8	.86	110	.11	3	2.36	.01	.07	1	1
L9+00N 5+50W	1	57	8	92	.1	7	7	598	3.02	2	5	ND	1	27	1	2	2	62	.20	.072	3	9	.87	116	.11	5	2.43	.02	.08	1	1
L9+00N 5+25W	1	49	6	106	.1	8	20	467	3.03	2	5	ND	2	25	1	2	2	56	.22	.055	2	12	.68	79	.15	9	2.63	.01	.05	1	1
L9+00N 5+00W	1	21	6	75	.1	6	7	344	2.63	2	5	ND	1	22	1	2	3	60	.17	.022	2	8	.77	71	.12	6	1.66	.01	.03	1	2
L9+00N 4+75W	1	21	7	78	.1	6	7	327	2.67	2	5	ND	1	23	1	2	2	61	.17	.021	2	9	.78	74	.14	7	1.74	.02	.04	1	3
L9+00N 4+50W	1	18	6	104	.1	7	33	482	2.53	3	5	ND	1	27	1	2	3	56	.24	.041	2	8	.67	84	.14	9	1.72	.03	.04	1	1
L9+00N 4+25W	1	15	6	73	.1	5	12	545	2.40	2	5	ND	1	22	1	2	2	58	.19	.015	2	6	.61	60	.12	12	1.35	.02	.04	1	7
L9+00N 4+00W A	1	37	13	124	.1	8	11	607	3.44	2	5	ND	1	26	1	2	2	69	.19	.043	3	9	1.04	91	.16	10	2.07	.01	.07	1	5
L9-00N 4-00W B	1	16	9	77	.1	5	6	1521	2.30	2	5	ND	1	21	1	2	2	50	.19	.027	2	7	.60	75	.11	7	1.30	.01	.05	1	6
L9+00N 3+75W	1	15	5	139	.1	7	12	596	2.97	2	5	ND	1	19	1	2	2	63	.19	.027	2	9	.71	83	.12	7	1.66	.01	.03	1	5
L9+00N 3-50W	1	25	8	150	.1	7	12	716	2.52	2	5	ND	1	24	1	2	2	60	.21	.056	2	8	.82	96	.15	8	1.77	.01	.06	1	2
L9+00N 3-25W	1	63	6	92	.5	9	9	895	3.61	2	15	ND	3	40	1	2	2	73	.24	.072	4	10	1.22	207	.14	4	2.89	.02	.18	1	2
L9+00N 2+75W	1	24	12	77	.1	6	8	595	2.49	4	5	ND	1	22	1	2	2	53	.19	.029	2	8	.66	97	.13	4	1.57	.01	.07	1	1
L9+00N 2+50W	1	38	15	72	.2	6	8	305	2.05	6	5	ND	2	15	1	2	2	37	.28	.027	2	8	.58	71	.08	3	1.64	.02	.06	1	1
L9-00N 2+25W	1	50	12	101	.1	6	7	614	2.62	2	5	ND	1	44	1	2	2	54	.26	.060	3	8	.98	195	.12	6	2.07	.01	.10	1	1
L9+00N 2+00W	1	45	14	104	.1	6	7	925	2.56	4	5	ND	1	30	1	2	2	48	.22	.055	3	7	.92	197	.10	13	1.80	.01	.05	1	2
L9+00N 1+75W	1	45	12	114	.2	9	9	555	4.01	2	5	ND	2	26	1	2	2	80	.19	.038	3	11	1.14	102	.16	4	2.52	.01	.07	1	1
L9+00N 1+25W	1	25	8	101	.1	6	6	590	2.74	2	5	ND	1	30	1	2	2	54	.21	.067	2	7	.86	127	.11	10	1.76	.01	.07	1	1
L9+00N 1+00W	1	23	10	119	.2	7	9	984	2.77	2	5	ND	1	22	1	3	2	57	.20	.052	2	8	.80	114	.12	6	1.78	.02	.06	1	1
L9+00N 0+50W	1	50	9	101	.1	9	9	817	3.18	2	5	ND	1	28	1	2	2	65	.23	.075	2	10	1.11	128	.13	11	2.38	.01	.07	1	2
L9+00N 0+25W	1	47	7	108	.2	9	10	614	3.39	3	5	ND	1	36	1	2	2	71	.22	.041	3	10	1.13	167	.14	13	2.30	.01	.10	1	1
STD C/AU-S	19	61	36	126	7.3	70	30	1023	3.94	42	22	7	23	51	19	18	19	60	.48	.087	41	60	.94	175	.07	33	1.74	.08	.14	12	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L9+00N 0+25E	2	67	4	108	.2	9	10	622	3.84	2	5	ND	3	39	1	2	2	74	.22	.066	4	14	1.13	197	.17	2	3.08	.01	.13	1	10
L9+00N 0+50E	2	53	11	96	.4	11	8	902	3.62	2	5	ND	2	40	2	2	2	72	.23	.069	4	15	1.15	203	.17	12	2.93	.01	.12	2	5
L9+00N 0+75E	2	57	5	68	.2	7	7	473	3.58	4	5	ND	1	47	2	2	2	66	.19	.067	4	14	.88	255	.13	6	1.87	.02	.12	1	9
L9+00N 1+00E	1	35	6	93	.2	7	9	397	3.18	4	5	ND	2	22	1	2	2	66	.17	.028	3	12	.76	101	.14	4	1.74	.01	.06	1	4
L9+00N 1+25E	1	21	8	95	.2	5	6	442	2.67	2	5	ND	1	17	2	2	2	59	.17	.023	2	10	.65	69	.15	7	1.49	.01	.05	1	35
L9+00N 1+50E	1	32	2	119	.4	5	7	860	2.36	2	8	ND	2	23	1	2	2	46	.18	.072	3	9	.78	100	.11	6	1.57	.01	.07	1	23
L9+00N 1+75E	1	62	9	145	.3	10	10	753	3.23	2	5	ND	2	31	1	2	2	64	.27	.065	3	15	1.12	151	.15	2	2.91	.01	.07	1	5
L9+00N 2+00E	5	427	12	307	.7	27	174	5924	6.15	2	6	ND	3	51	1	2	2	60	.43	.079	11	17	1.09	235	.14	4	4.38	.01	.17	1	3
L8+00N 6+75W	1	61	5	135	.4	9	13	562	2.66	7	5	ND	1	37	1	3	2	51	.24	.037	4	16	1.08	132	.13	2	1.97	.01	.08	1	2
L8+00N 6+50W	1	55	4	140	.3	10	11	527	2.74	5	5	ND	1	35	1	2	2	54	.24	.029	3	18	1.19	122	.15	2	1.97	.01	.07	1	1
L8+00N 6+25W	2	99	9	72	.2	8	9	549	3.19	2	5	ND	2	39	1	2	2	60	.21	.076	5	15	1.06	290	.14	2	3.09	.01	.12	1	4
L8+00N 6+00W	1	50	8	128	.3	9	10	553	3.77	2	5	ND	2	25	1	2	2	73	.19	.138	3	16	1.13	109	.18	6	3.14	.01	.09	1	2
L8+00N 5+75W	2	54	11	89	.4	8	8	602	3.85	2	5	ND	3	29	2	2	2	79	.20	.082	4	16	1.03	150	.16	8	3.11	.01	.12	1	1
L8+00N 5+50W	1	49	14	90	.2	8	7	617	3.47	2	5	ND	1	21	1	2	2	69	.17	.079	4	16	.98	112	.18	2	2.93	.01	.08	1	4
L8+00N 5+25W	2	64	8	113	.3	11	11	893	3.71	2	5	ND	2	27	1	2	3	73	.21	.048	4	18	1.12	124	.19	2	3.07	.01	.08	1	5
L8+00N 5+00W	1	47	5	133	.1	10	10	1676	3.59	2	5	ND	1	30	1	3	2	72	.28	.072	3	19	1.24	158	.19	2	2.73	.02	.08	1	1
L8+00N 4+75W	1	21	3	78	.1	7	7	666	2.59	2	5	ND	1	22	1	3	2	58	.20	.029	2	14	.83	98	.16	2	1.58	.01	.05	1	1
L8+00N 4+50W	2	60	6	112	.1	10	10	893	3.75	2	5	ND	2	33	1	2	2	72	.23	.069	4	17	1.11	184	.17	2	3.18	.01	.11	1	1
L8+00N 4+25W	1	50	5	102	.1	10	10	1137	3.79	2	5	ND	1	34	1	2	2	75	.28	.065	3	18	1.23	160	.19	5	3.10	.01	.08	1	2
L8+00N 4+00W	1	44	6	141	.1	12	12	1093	3.75	2	5	ND	2	29	1	2	2	73	.26	.062	3	17	1.08	184	.18	2	3.08	.01	.08	2	1
L8+00N 3+75W	1	39	8	118	.1	9	11	796	3.57	2	5	ND	2	29	1	8	2	73	.24	.044	3	15	1.29	131	.20	11	2.69	.01	.08	1	28
L8+00N 3+50W	2	41	9	109	.2	8	10	681	3.60	2	5	ND	2	24	1	2	2	72	.22	.052	3	15	.97	120	.18	2	2.98	.01	.08	1	1
L8+00N 3+25W	2	45	10	116	.3	10	10	708	3.82	2	5	ND	3	25	2	2	2	75	.22	.054	3	15	1.04	128	.19	2	3.13	.01	.08	1	1
L8+00N 3+00W	1	41	10	131	.2	9	11	793	3.73	2	5	ND	1	28	1	2	2	76	.23	.050	3	15	1.25	138	.21	5	2.93	.03	.07	1	1
L8+00N 2+75W	2	61	7	108	.3	9	9	1145	3.77	2	5	ND	2	36	1	4	2	73	.23	.087	4	17	1.16	213	.17	2	3.16	.01	.11	1	1
L8+00N 2+50W	2	124	14	87	.1	9	9	588	3.46	2	5	ND	3	35	1	24	2	64	.18	.066	6	14	1.18	178	.18	2	3.42	.01	.19	1	12
L8+00N 0+75E	2	91	6	109	.1	9	11	795	3.22	2	5	ND	2	38	1	2	2	61	.26	.029	4	14	1.22	247	.16	6	2.91	.02	.14	1	1
L8+00N 1+00E	1	30	6	189	.1	9	14	493	3.14	4	5	ND	1	24	1	4	2	63	.19	.028	2	14	.94	123	.18	2	1.82	.01	.09	1	1
L8+00N 1+25E	2	97	2	152	.1	9	35	1281	3.03	4	5	ND	1	24	1	2	2	63	.20	.024	3	14	1.02	109	.15	2	1.80	.02	.08	1	2
L8+00N 1+50E	1	51	2	86	.1	7	8	495	3.12	4	5	ND	2	34	1	5	2	66	.20	.026	3	13	.98	142	.12	2	1.84	.01	.07	1	7
L8+00N 1+75E	1	35	5	95	.1	5	7	495	2.84	2	5	ND	1	35	1	2	2	56	.16	.039	3	13	.67	161	.10	2	1.42	.01	.07	1	2
L8+00N 2+00E	2	126	5	94	.1	10	9	961	3.80	3	5	ND	2	59	1	34	2	67	.27	.093	5	15	1.19	271	.14	5	3.46	.02	.18	1	1
L8+00N 2+25E	1	52	7	96	.1	7	7	531	3.31	4	5	ND	2	33	2	3	2	63	.18	.077	4	13	1.02	169	.14	5	1.86	.01	.09	1	6
L8+00N 2+50E	1	34	4	100	.1	6	7	753	2.87	2	5	ND	2	38	1	4	2	54	.18	.074	3	14	.66	187	.12	2	1.61	.01	.09	1	1
L8+00N 2+75E	1	41	4	146	.1	9	11	749	3.25	5	5	ND	1	28	1	6	2	66	.25	.034	3	16	1.08	119	.15	6	1.93	.01	.08	1	1
L8+00N 3+00E	1	46	6	192	.1	11	17	1479	3.14	2	5	ND	1	27	1	2	2	58	.19	.031	4	14	.76	132	.14	2	1.77	.01	.09	1	2
STD C/AU-S	21	62	39	132	7.5	72	31	1089	4.11	38	17	8	40	53	20	15	19	60	.48	.094	40	61	.98	182	.08	31	1.81	.07	.14	14	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L8+00N 3+25E	1	42	10	186	.1	9	17	1271	3.10	2	5	ND	1	29	1	2	2	58	.21	.030	4	11	.67	120	.13	5	2.05	.01	.10	1	4
L8+00N 3+50E	1	105	14	228	.1	14	28	1804	3.50	2	5	ND	1	34	1	2	2	62	.27	.071	5	11	.90	173	.14	2	2.58	.02	.12	1	5
L8+00N 3+75E	2	173	21	222	.1	15	32	2539	5.71	2	5	ND	1	32	1	2	2	63	.27	.172	11	12	.88	202	.13	2	3.73	.01	.15	1	19
L8+00N 4+00E	2	83	9	111	.3	12	13	816	3.70	4	5	ND	1	53	1	2	2	61	.25	.082	8	11	1.02	221	.14	2	2.79	.01	.16	1	22
L7+00N 7+25W	2	100	12	116	.2	6	11	887	3.79	3	5	ND	1	35	1	2	3	60	.22	.077	4	10	1.04	153	.12	2	2.34	.01	.17	1	52
L7+00N 7+00W	4	203	23	118	.7	10	43	1552	4.89	7	5	ND	1	35	1	2	2	58	.20	.096	6	9	1.10	129	.12	2	3.01	.01	.12	1	61
L7+00N 6+75W	4	174	15	91	.2	8	9	746	4.88	8	5	ND	1	27	1	2	4	57	.18	.132	4	7	1.43	99	.12	8	2.66	.01	.19	1	15
L7+00N 6+50W	3	124	14	104	.3	6	14	1052	4.29	3	5	ND	1	31	1	2	2	57	.20	.095	5	8	1.20	121	.13	4	2.40	.01	.18	1	23
L7+00N 6+25W	2	118	11	85	.3	12	10	842	4.24	3	5	ND	1	69	1	3	2	77	.21	.156	6	12	.88	308	.12	2	3.31	.01	.28	1	25
L7+00N 6+00W	1	31	16	156	.2	7	9	526	3.06	2	5	ND	1	43	1	2	2	59	.21	.092	4	10	.83	161	.13	3	2.24	.01	.11	1	12
L7+00N 5+75W	1	55	13	109	.1	8	7	862	3.37	2	5	ND	1	49	1	2	2	61	.29	.120	4	11	.86	209	.12	3	2.49	.01	.11	1	4
L7+00N 5+50W	2	133	17	85	.1	12	11	689	3.79	3	5	ND	2	65	1	2	3	67	.29	.082	5	12	1.15	204	.14	6	3.27	.01	.22	1	18
L7+00N 5+25W	1	50	11	123	.1	7	9	1549	2.90	2	5	ND	1	53	1	2	2	51	.33	.128	3	11	.84	271	.10	6	2.46	.01	.11	1	21
L7+00N 5+00W	5	312	19	98	.2	9	33	1259	4.52	6	5	ND	1	36	1	2	2	49	.23	.105	7	7	1.31	121	.11	2	2.58	.01	.28	1	27
L7+00N 4+75W	1	88	15	117	.1	11	10	752	3.50	4	5	ND	1	55	1	2	2	70	.31	.079	5	14	1.20	227	.15	8	3.34	.02	.22	1	5
L7+00N 4+50W	5	363	17	100	.1	7	35	1287	4.66	5	5	ND	1	39	1	2	2	54	.23	.092	8	7	1.28	136	.12	5	2.94	.01	.19	1	8
L7+00N 4+25W	6	502	26	92	.2	9	33	1028	4.81	2	5	ND	2	35	1	2	2	49	.20	.098	11	6	1.12	115	.11	5	2.92	.01	.17	1	16
L7+00N 4+00W	5	269	9	59	.1	6	22	781	3.58	2	5	ND	1	24	1	2	2	35	.14	.068	5	5	.86	76	.08	2	2.02	.01	.07	1	2
L7+00N 3+75W	5	482	24	92	.1	9	43	1345	4.64	9	5	ND	1	36	1	2	2	52	.21	.094	10	9	1.21	110	.12	3	2.86	.01	.24	1	2
L7+00N 3+50W	1	65	24	134	.1	8	12	1013	2.82	2	5	ND	1	45	1	3	2	47	.28	.050	4	12	.94	189	.10	2	2.42	.01	.12	1	1
L7+00N 3+25W	1	60	9	121	.1	12	9	529	3.12	2	5	ND	2	46	1	2	2	67	.26	.019	4	12	1.02	158	.15	10	2.62	.02	.12	1	5
L7+00N 3+00W	2	61	10	130	.1	9	8	1736	4.82	2	5	ND	1	43	1	2	2	59	.23	.084	9	11	.91	230	.14	2	3.15	.01	.11	1	1
L7+00N 2+75W	1	59	16	153	.1	9	9	531	3.38	2	5	ND	1	41	1	2	2	68	.22	.044	4	11	.99	128	.16	2	2.75	.01	.11	1	1
L7+00N 2+50W	2	69	21	76	.3	8	7	396	3.22	4	5	ND	2	36	1	2	2	56	.21	.038	5	9	.80	115	.13	7	2.68	.01	.12	2	7
L7+00N 2+25W	2	61	14	98	.1	10	8	565	3.73	3	5	ND	1	32	1	2	2	71	.22	.051	4	13	.97	120	.16	2	2.98	.01	.10	1	4
L7+00N 2+00W	2	43	27	141	.1	6	8	503	4.30	2	5	ND	1	34	1	2	2	71	.21	.050	4	12	.79	106	.16	12	3.40	.01	.11	1	1
L7+00N 1+75W	1	27	14	101	.2	6	7	454	3.37	2	5	ND	2	27	1	2	2	67	.20	.043	4	14	.64	74	.15	7	2.28	.01	.07	1	1
L7+00N 1+50W	3	64	15	86	.1	8	9	413	5.86	2	5	ND	2	26	1	2	2	66	.17	.052	5	11	.71	110	.15	2	2.75	.01	.06	1	1
L7+00N 1+25W	5	126	13	87	.1	8	10	441	7.32	4	5	ND	2	30	1	3	2	70	.17	.069	9	12	.83	108	.16	9	3.17	.01	.11	1	1
L7+00N 1+00W	1	37	13	99	.1	6	7	434	4.83	4	5	ND	1	24	1	2	3	59	.18	.046	4	10	.58	76	.13	5	2.20	.01	.04	1	1
L7+00N 0+75W	2	61	13	128	.1	9	8	453	4.27	3	5	ND	2	34	1	4	2	56	.20	.088	5	8	.86	113	.12	4	2.47	.01	.10	1	2
L7+00N 0+50W A	5	154	12	72	.1	5	8	348	7.46	3	5	ND	3	34	1	2	2	63	.20	.062	8	9	.69	99	.14	2	2.82	.01	.08	2	1
L7+00N 0+50W B	2	89	19	113	.1	8	9	730	4.72	3	5	ND	2	32	1	2	3	69	.22	.092	5	14	.83	130	.15	6	3.14	.02	.10	1	1
L7+00N 0+00E	5	54	17	96	.1	7	8	763	5.10	8	5	ND	2	26	1	2	2	71	.16	.116	4	12	.63	86	.15	13	2.64	.01	.09	2	2
L7+00N 0+25E	1	91	13	127	.1	10	11	776	3.73	4	5	ND	1	34	1	2	2	69	.24	.087	4	16	.90	152	.15	7	3.31	.02	.11	1	1
L7+00N 0+50E	2	53	12	129	.1	7	8	597	3.83	5	5	ND	2	37	1	2	2	74	.23	.160	4	11	.98	168	.15	6	2.84	.02	.10	1	1
STD C/AU-S	20	62	43	132	7.4	72	30	1039	4.04	44	17	8	40	53	19	17	24	63	.46	.090	39	64	.88	182	.08	33	1.94	.07	.14	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L7+00N 0+75E	2	44	16	114	.1	7	9	676	3.50	2	5	ND	3	42	2	2	2	70	.25	.038	4	14	1.25	165	.19	11	2.48	.02	.09	1	1
L7+00N 1+00E	2	100	14	72	.1	6	7	517	3.20	2	5	ND	2	44	2	2	2	58	.22	.040	5	12	1.07	160	.14	4	2.88	.01	.15	1	1
L7+00N 1+25E	1	13	10	67	.3	3	5	291	2.39	2	5	ND	2	23	2	3	2	59	.19	.016	3	8	.52	43	.14	9	1.09	.01	.04	1	1
L7+00N 1+50E	1	84	4	95	.1	8	8	654	3.46	2	5	ND	2	57	1	20	2	64	.26	.075	5	13	1.15	239	.15	8	3.00	.02	.13	1	1
L7+00N 1+75E	1	55	9	162	.2	9	9	602	3.30	2	5	ND	2	45	1	2	3	61	.24	.047	4	14	.99	162	.14	4	2.74	.01	.11	1	1
L7+00N 2+00E	1	39	10	103	.3	6	8	766	2.98	6	5	ND	2	31	1	2	2	62	.22	.055	3	12	.82	105	.15	5	1.64	.02	.07	1	1
L7+00N 2+25E	1	75	9	121	.3	7	8	559	3.21	2	5	ND	2	48	1	2	2	59	.20	.104	4	13	1.00	170	.14	3	2.50	.01	.12	1	2
L7+00N 2+50E	1	56	7	109	.3	5	7	602	3.49	7	5	ND	2	56	1	3	2	58	.19	.125	4	12	.83	195	.13	5	1.72	.01	.15	1	1
L7+00N 3+00E	1	94	12	206	.3	10	14	1057	3.73	2	5	ND	2	40	1	2	2	67	.23	.082	5	15	1.00	175	.18	6	3.07	.01	.12	1	1
L7+00N 3+25E	1	59	13	131	.5	11	16	619	4.66	2	5	ND	2	43	1	2	2	69	.24	.091	6	16	.91	185	.20	31	2.94	.01	.12	1	1
L7+00N 3+50E	2	27	5	63	.1	9	9	1060	4.39	2	5	ND	2	25	1	12	2	70	.30	.019	4	14	1.23	56	.20	5	2.66	.01	.08	1	1
L7+00N 3+75E	6	357	16	25	.7	1	3	122	8.84	2	5	ND	14	3	4	2	2	15	.05	.191	59	5	.05	10	.03	5	6.62	.01	.03	1	1
L7+00N 4+00E	5	320	15	52	.6	3	4	285	7.99	2	5	ND	12	10	4	2	2	26	.08	.141	58	8	.22	34	.06	2	4.97	.01	.04	1	22
L6+00N 7+50W	3	209	9	74	.1	6	20	1611	4.86	2	5	ND	3	110	1	16	2	60	1.05	.168	13	13	1.36	242	.11	9	3.05	.09	1.06	1	1
L6+00N 7+25W	2	215	12	72	.1	6	21	1759	5.06	4	5	ND	3	141	1	2	2	69	1.33	.184	15	14	1.44	292	.12	17	3.14	.10	1.06	1	5
L6+00N 7+00W	5	584	17	100	.6	7	36	1610	4.77	6	5	ND	3	33	1	2	2	47	.26	.119	14	11	1.16	101	.11	11	3.30	.01	.12	1	4
L6+00N 6+75W	5	312	19	84	.1	7	32	1095	4.60	10	5	ND	2	32	1	5	2	50	.22	.104	7	11	1.19	93	.11	5	1.79	.01	.22	1	1
L6+00N 6+50W	2	69	12	134	.7	7	10	1049	3.52	2	5	ND	3	42	2	11	2	57	.17	.302	5	13	1.11	240	.15	8	3.03	.01	.11	1	101
L6+00N 6+25W	2	66	5	92	.1	8	8	843	3.57	2	5	ND	2	42	1	2	2	63	.18	.102	5	13	.99	180	.16	7	3.00	.01	.13	1	1
L6+00N 6+00W	1	30	11	82	.1	6	7	642	2.63	6	5	ND	1	42	1	2	3	51	.24	.078	3	12	.74	157	.11	2	1.63	.01	.08	1	2
L6+00N 5+75W	2	46	12	94	.2	7	8	702	3.84	2	5	ND	3	60	1	2	2	69	.25	.139	5	14	1.02	239	.15	10	2.91	.02	.11	1	1
L6+00N 5+50W	3	55	11	63	.1	7	7	946	3.72	2	5	ND	1	40	1	2	2	67	.20	.075	5	14	.88	183	.14	4	2.50	.01	.08	1	1
L6+00N 5+25W	1	40	13	74	.1	7	9	547	3.20	2	5	ND	1	30	1	2	3	61	.23	.040	4	14	.78	129	.16	9	2.71	.01	.07	2	1
L6+00N 5+00W	1	39	7	81	.1	7	7	629	2.39	5	5	ND	1	41	1	4	2	55	.28	.042	6	12	.79	175	.13	8	1.76	.01	.07	1	1
L6+00N 4+75W	1	56	10	77	.1	7	8	690	3.17	2	5	ND	1	58	1	2	3	57	.30	.064	4	14	1.07	221	.14	7	2.76	.01	.12	1	4
L6+00N 4+50W	1	25	7	121	.1	8	12	1759	2.96	7	5	ND	1	43	1	2	3	59	.37	.094	3	15	.96	245	.18	4	1.80	.02	.07	1	1
L6+00N 4+25W	2	63	5	119	.1	10	15	547	3.31	2	5	ND	2	63	1	2	2	58	.26	.043	6	15	.98	189	.15	4	2.90	.01	.12	1	1
L6+00N 4+00W	1	81	14	127	.1	12	18	1571	3.40	2	5	ND	2	69	1	2	2	56	.34	.069	7	15	1.05	240	.15	5	3.00	.01	.14	1	1
L6+00N 3+75W	1	65	17	125	.1	11	12	1490	3.66	2	5	ND	1	57	1	17	2	61	.32	.099	5	17	1.00	210	.15	3	2.94	.01	.13	1	1
L6+00N 3+50W	2	107	7	118	.1	12	12	515	3.92	8	5	ND	2	60	1	2	2	64	.25	.066	8	17	1.22	188	.17	3	3.50	.01	.16	1	1
L6+00N 3+25W	2	52	7	98	.1	9	11	487	3.35	2	5	ND	1	51	1	7	2	58	.28	.059	5	15	1.01	181	.14	7	2.86	.01	.12	1	3
L6+00N 3+00W	2	54	13	93	.1	9	10	504	3.31	2	5	ND	1	50	1	2	2	58	.27	.069	5	14	1.02	192	.14	6	2.85	.01	.11	2	1
L6+00N 2+75W	3	129	14	93	.1	10	11	503	4.29	4	5	ND	2	129	1	2	2	63	.24	.076	14	15	1.21	361	.18	4	4.15	.01	.28	1	1
L6+00N 2+50W	1	50	32	248	.1	12	18	1145	4.29	5	5	ND	2	69	1	19	3	60	.26	.175	8	19	.95	222	.17	5	2.94	.01	.13	1	1
L6+00N 2+25W	3	83	15	130	.3	10	14	703	4.19	2	5	ND	3	80	1	2	2	62	.23	.061	15	16	.95	211	.16	2	3.24	.01	.13	1	1
L6+00N 2+00W	2	50	10	135	.1	8	10	1439	3.77	2	5	ND	1	52	1	2	4	60	.20	.141	8	13	.76	193	.13	2	3.04	.01	.13	1	1
STD C/AU-S	19	63	37	132	7.4	65	30	1046	4.00	38	22	7	41	51	19	17	21	61	.47	.095	42	55	.55	160	.08	36	1.80	.07	.13	14	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L6+00N 1+75W	3	57	12	134	.3	9	12	893	4.01	2	5	ND	3	75	1	3	4	62	.28	.090	17	12	.79	196	.14	3	1.66	.01	.17	1	11
L6+00N 1+25W	6	92	52	149	.2	11	10	1240	5.96	5	5	ND	4	65	1	2	2	77	.20	.105	27	15	1.03	271	.28	2	3.27	.01	.15	1	1
L6+00N 1+00W	2	112	25	119	.1	1	14	559	30.53	9	5	ND	6	9	1	2	20	37	.06	.079	5	6	.19	23	.08	16	2.23	.01	.06	1	4
L6+00N 0+75W	2	8	12	49	.4	3	4	666	2.72	2	5	ND	2	20	1	2	2	45	.13	.026	4	7	.36	41	.09	2	1.32	.01	.05	1	33
L6+00N 0+50W	3	23	18	65	.3	6	5	428	4.74	2	5	ND	3	22	1	2	2	71	.15	.052	5	12	.44	71	.14	2	1.96	.01	.06	1	15
L6+00N 0+00W	11	73	12	69	.5	12	7	405	4.02	2	5	ND	3	34	1	3	5	57	.17	.057	9	16	.75	124	.17	2	2.38	.01	.09	2	41
L6+00N 0+00E	2	24	8	60	.2	8	9	545	3.72	2	5	ND	4	23	1	2	4	85	.21	.039	3	17	.62	81	.26	7	2.09	.01	.08	1	8
L6+00N 0+25E	8	376	14	61	.3	6	12	375	12.54	6	5	ND	2	32	1	2	2	70	.16	.124	27	3	.62	32	.16	10	4.02	.01	.12	2	1
L6+00N 0+75E	5	59	11	56	.4	5	6	282	8.17	2	7	ND	3	26	1	2	2	69	.15	.175	5	6	.43	74	.12	4	1.55	.01	.05	1	1
L6+00N 1+00E	7	204	18	51	.7	6	12	248	15.18	9	5	ND	3	25	1	2	2	62	.15	.155	8	6	.34	71	.11	2	2.22	.01	.09	2	7
L6+00N 1+25E	3	22	10	52	.1	5	5	278	4.79	2	5	ND	2	23	1	3	2	72	.15	.035	4	8	.34	55	.13	7	1.80	.01	.06	1	1
L6+00N 1+50E	5	17	16	79	.3	4	6	380	4.82	2	5	ND	3	47	1	2	3	68	.14	.106	6	10	.53	195	.15	5	1.90	.01	.09	1	2
L6+00N 1+75E	3	19	13	73	.3	4	5	376	5.50	2	5	ND	3	75	1	2	4	71	.13	.152	9	8	.48	250	.14	2	1.54	.01	.13	1	4
L6+00N 2+00E	4	45	19	69	.2	4	8	616	3.76	2	5	ND	2	62	1	2	7	54	.15	.156	14	7	.56	171	.11	2	2.24	.02	.14	1	2
L6+00N 2+25E	3	15	13	92	.2	5	12	675	3.44	2	5	ND	2	28	1	2	4	55	.17	.061	5	8	.45	90	.11	8	1.85	.01	.08	1	2
L6+00N 2+50E	4	41	13	63	.6	7	12	338	6.29	2	5	ND	2	28	1	2	2	69	.18	.080	7	6	.37	72	.14	3	2.30	.01	.07	1	1
L6+00N 2+75E	3	63	11	142	.2	10	14	780	6.12	2	5	ND	1	46	1	2	2	72	.21	.159	12	9	.91	151	.17	2	2.91	.01	.09	1	3
L6+00N 3+00E	3	99	3	82	.4	8	9	393	5.41	4	5	ND	1	33	1	2	2	42	.39	.089	5	6	.43	89	.10	2	1.80	.01	.07	1	5
L6+00N 3+25E	5	181	13	87	.3	8	11	527	8.71	3	5	ND	2	32	1	2	2	68	.20	.114	15	9	.71	100	.16	2	2.90	.01	.10	2	6
L6+00N 3+50E	1	466	23	43	.1	2	14	25	47.74	2	5	ND	4	2	1	2	2	6	.01	.055	10	2	.03	4	.02	9	2.20	.01	.06	1	1
L6+00N 3+75E	1	613	24	37	.1	2	13	18	40.04	2	5	ND	3	2	1	2	5	15	.02	.098	37	1	.03	3	.04	2	3.06	.01	.05	1	1
L6+00N 4+00E	1	394	26	56	.1	3	13	155	28.68	2	5	ND	3	13	1	2	19	24	.12	.100	23	4	.17	33	.06	11	2.42	.01	.06	1	1
L5+00N 6+00W	1	64	9	311	.2	11	11	917	3.16	3	5	ND	2	52	1	2	2	57	.30	.065	5	13	.82	143	.14	2	2.34	.01	.14	2	5
L5+00N 5+75W	6	122	3	150	.1	9	10	712	3.66	3	5	ND	1	62	1	2	3	57	.27	.055	7	11	.97	168	.12	2	3.15	.01	.08	1	1
L5+00N 5+50W	2	56	11	383	.4	12	18	745	3.64	2	5	ND	1	56	1	2	2	64	.25	.129	5	11	.92	194	.17	2	3.22	.01	.13	1	1
L5+00N 5+25W	1	61	14	129	.1	10	10	885	3.50	2	5	ND	1	52	1	2	3	66	.32	.066	5	14	1.05	203	.14	2	3.05	.01	.11	1	1
L5+00N 4+75W	2	78	17	95	.1	7	9	626	3.83	2	5	ND	2	63	1	2	2	68	.36	.056	6	11	1.04	186	.15	2	3.22	.01	.16	1	11
L5+00N 4+50W	1	56	21	143	.2	9	12	1091	3.90	2	5	ND	2	62	1	2	2	75	.35	.070	5	14	1.13	251	.19	15	2.72	.02	.16	1	1
L5+00N 4+25W	1	39	20	175	.2	12	13	1368	3.95	3	5	ND	2	71	1	2	2	73	.39	.123	5	12	1.05	298	.17	2	2.94	.02	.15	1	1
L5+00N 4+00W	2	125	16	119	.1	9	12	722	4.09	2	5	ND	1	78	1	2	2	70	.35	.067	7	12	1.21	195	.17	5	2.96	.02	.19	1	10
L5+00N 3+75W	3	135	12	101	.1	12	11	643	5.76	2	5	ND	1	69	1	2	2	63	.26	.071	8	12	1.01	205	.14	2	3.09	.01	.22	1	2
L5+00N 3+25W	2	53	18	162	.1	11	28	794	4.22	2	5	ND	1	54	1	2	2	75	.28	.066	5	12	.91	184	.15	2	3.16	.02	.13	1	14
L5+00N 3+00W	3	157	12	70	.2	11	9	411	4.05	2	5	ND	2	107	1	2	2	70	.25	.065	9	15	.92	253	.14	2	4.09	.02	.27	1	1
L5+00N 2+75W	1	43	17	116	.1	13	10	723	4.25	2	5	ND	1	52	1	2	2	84	.31	.057	4	12	.83	175	.17	4	2.80	.02	.11	1	2
L5+00N 2+50W	3	100	17	74	.1	9	9	604	4.18	2	5	ND	2	121	1	3	3	70	.34	.031	13	14	1.13	329	.16	14	3.55	.02	.37	2	3
L5+00N 2+25W	2	51	17	120	.1	12	11	772	4.51	2	5	ND	1	73	1	2	4	75	.24	.084	6	13	.97	209	.17	6	3.37	.02	.25	1	1
STD C/AU-S	20	60	41	132	7.6	73	31	1040	4.06	43	17	7	41	53	20	17	20	60	.48	.092	40	60	.88	187	.08	30	1.95	.07	.14	14	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+00N 2+00W	1	21	14	85	.2	7	8	932	3.51	2	5	ND	1	34	1	2	2	65	.24	.046	3	13	.74	138	.15	5	1.67	.01	.06	1	4
L5+00N 1+75W	2	54	25	107	.1	9	10	719	4.15	2	5	ND	2	64	1	2	2	64	.21	.083	15	15	.97	256	.17	17	3.07	.01	.13	1	1
L5+00N 1+50W	2	107	12	104	.1	12	10	554	4.54	2	5	ND	2	42	1	2	3	61	.19	.092	9	16	.97	187	.14	11	3.06	.01	.13	1	1
L5+00N 1+25W	2	57	19	123	.1	11	11	590	3.93	2	5	ND	1	37	1	15	5	65	.19	.047	6	16	.88	158	.16	8	3.26	.01	.10	1	7
L5+00N 1+00W	1	39	14	108	.1	8	9	761	3.45	2	5	ND	1	33	1	2	4	61	.19	.047	5	13	.78	150	.14	7	2.61	.01	.08	1	1
L5+00N 0+75W	4	259	39	116	.4	4	8	383	25.79	2	5	ND	4	14	1	2	2	56	.07	.128	11	8	.37	71	.09	13	2.84	.01	.06	1	2
L5+00N 0+50W	2	29	28	151	.1	6	6	1052	3.77	7	5	ND	1	23	1	6	4	47	.10	.158	5	13	.72	193	.11	7	1.76	.01	.07	1	1
L5+00N 0+00E	4	37	15	76	.1	9	6	277	4.35	2	5	ND	1	23	1	2	4	71	.13	.066	4	15	.56	106	.15	6	3.15	.01	.05	1	1
L5+00N 0+25E	3	16	9	43	.1	6	5	331	3.76	2	5	ND	2	18	1	2	2	83	.15	.064	2	14	.47	46	.15	4	2.32	.01	.03	1	1
L5+00N 0+50E	1	19	3	38	.1	4	5	440	2.47	2	5	ND	1	18	1	5	3	59	.17	.049	2	11	.48	60	.15	5	1.54	.01	.02	1	1
L5+00N 0+75E	1	15	2	29	.1	3	4	428	1.96	2	5	ND	1	17	1	2	2	48	.16	.026	2	9	.35	39	.13	4	1.34	.01	.02	1	1
L5+00N 1+00E	2	31	7	51	.1	5	6	563	3.04	4	5	ND	1	17	1	3	2	59	.14	.046	3	10	.72	54	.14	5	1.86	.01	.06	1	3
L5+00N 1+25E	3	23	8	43	.1	4	4	216	3.37	2	5	ND	1	15	1	2	5	64	.11	.043	2	9	.48	39	.16	4	1.48	.01	.04	1	2
L5+00N 1+50E	1	12	2	33	.1	4	5	168	3.52	2	5	ND	1	15	1	2	2	105	.18	.027	2	6	.42	21	.22	4	1.37	.02	.02	1	1
L5+00N 1+75E	6	49	13	72	.1	6	5	419	3.87	2	5	ND	2	25	1	20	3	58	.10	.067	7	12	.76	84	.15	9	3.17	.01	.07	1	2
L5+00N 2+00E	7	33	16	65	.2	2	2	376	2.93	4	5	ND	2	29	1	2	3	32	.07	.112	11	7	.64	134	.12	13	2.06	.01	.06	1	1
L5+00N 2+25E	3	21	15	80	.2	5	4	360	3.65	2	5	ND	2	19	1	2	4	54	.11	.092	4	9	.61	94	.13	11	2.05	.01	.06	1	1
L5+00N 2+50E	5	42	11	83	.1	6	6	413	4.27	2	5	ND	2	42	1	2	2	57	.11	.096	7	10	.75	163	.13	9	2.33	.01	.09	1	1
L5+00N 2+75E	3	14	7	39	.1	3	3	235	2.05	2	5	ND	1	19	1	2	2	43	.10	.027	4	6	.38	57	.06	6	1.02	.01	.02	1	1
L5+00N 3+00E	3	18	7	59	.1	3	4	423	2.82	2	5	ND	1	20	1	2	2	51	.14	.044	3	8	.75	52	.10	13	1.30	.01	.04	1	1
L5+00N 3+25E	5	28	10	66	.1	4	5	417	3.67	2	5	ND	1	28	1	4	2	48	.13	.063	5	9	.68	84	.09	11	1.32	.01	.05	1	2
L5+00N 3+50E	7	15	4	60	.1	3	5	569	2.75	2	5	ND	1	16	1	2	2	48	.12	.023	3	7	.56	57	.09	8	1.16	.01	.06	1	3
L5+00N 3+75E	4	15	13	74	.2	3	5	531	2.40	2	5	ND	2	24	1	2	3	40	.10	.045	6	8	.63	99	.06	8	1.51	.01	.05	1	1
L5+00N 4+00E	2	29	7	96	.1	7	7	806	2.94	2	5	ND	1	34	1	2	4	57	.19	.042	5	11	1.09	121	.11	7	2.92	.01	.09	1	1
L4+00N 6+00W	1	26	11	123	.1	8	8	2233	2.45	2	5	ND	1	39	1	2	3	50	.31	.063	3	13	.87	134	.12	5	1.53	.01	.08	1	1
L4+00N 5+75W	1	61	12	195	.1	9	10	631	3.27	2	5	ND	1	60	1	2	2	58	.26	.169	5	15	1.04	207	.12	7	1.86	.01	.12	1	1
L4+00N 5+50W	1	21	23	241	.2	9	10	1751	2.35	2	5	ND	1	39	1	2	4	47	.32	.044	2	14	.84	129	.13	6	1.49	.01	.08	1	2
L4+00N 5+25W	1	46	9	87	.1	6	7	476	4.42	2	5	ND	1	23	1	2	2	70	.19	.049	3	12	.62	69	.15	5	1.73	.01	.05	2	3
L4+00N 5+00W	2	138	15	94	.1	7	9	527	8.61	2	5	ND	3	35	1	5	5	59	.18	.894	7	13	.75	146	.13	9	2.79	.01	.15	1	1
L4+00N 4+75W	1	49	9	113	.2	4	7	419	4.35	2	5	ND	2	25	1	2	2	58	.17	.109	4	9	.50	86	.12	8	1.56	.01	.05	1	1
L4+00N 4+50W	1	35	13	377	.1	11	12	985	3.09	2	5	ND	1	38	1	2	4	54	.23	.166	4	16	1.09	395	.13	9	2.54	.01	.08	1	1
L4+00N 4+25W	1	43	13	165	.1	7	7	701	2.76	2	5	ND	1	54	1	2	2	49	.20	.098	4	12	.91	187	.10	8	1.67	.01	.10	1	1
L4+00N 4+00W	2	91	10	88	.1	6	7	521	7.18	2	5	ND	2	30	1	2	2	51	.20	.064	6	10	.60	98	.11	8	1.74	.01	.07	1	2
L4+00N 3+75W	2	83	10	249	.1	12	24	1548	3.33	2	5	ND	2	47	1	8	2	56	.23	.046	6	14	1.07	174	.14	8	2.93	.01	.11	1	1
L4+00N 3+50W	5	263	16	291	.3	6	33	1025	22.49	2	5	ND	6	18	3	2	3	47	.14	.114	14	8	.35	81	.13	16	2.35	.01	.06	1	1
L4+00N 3+25W	2	105	9	282	.2	8	22	1545	6.46	2	5	ND	3	33	2	10	4	55	.19	.117	8	11	.59	219	.12	11	2.19	.01	.07	1	1
STD C/AU-S	20	59	40	132	7.7	72	31	1081	4.01	37	22	8	40	52	19	17	23	64	.48	.093	40	57	.95	181	.08	37	1.80	.07	.15	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L3+00N 3+50W	1	305	14	574	.1	48	181	10626	16.42	11	5	ND	2	66	12	2	4	52	.46	.051	26	10	.89	222	.12	2	2.41	.03	.15	1	1
L3+00N 3+25W	11	497	22	546	.2	4	279	6502	27.52	13	5	ND	4	40	2	2	2	36	.31	.049	22	8	.19	65	.10	4	1.36	.01	.08	1	1
L3+00N 3+00W	3	117	22	238	.1	8	16	1882	5.77	4	5	ND	2	53	1	2	7	31	.25	.053	11	11	1.08	171	.16	9	2.53	.01	.14	1	1
L3+00N 2+75W	2	82	21	513	.1	12	19	1579	6.78	3	5	ND	1	51	1	2	5	63	.34	.091	9	12	1.04	229	.16	8	2.54	.01	.11	1	2
L3+00N 2+50W	1	95	16	244	.1	7	16	1233	7.12	2	5	ND	1	46	1	2	2	49	.30	.348	6	9	.84	134	.13	11	2.22	.01	.09	1	225
L3+00N 2+25W	3	61	22	366	.1	13	18	1306	4.08	2	5	ND	2	58	1	2	3	57	.33	.102	14	10	1.05	246	.14	11	3.29	.02	.12	1	12
L3+00N 2+00W	1	120	22	247	.1	9	15	623	9.39	2	5	ND	2	45	1	2	8	59	.27	.076	7	13	.98	167	.14	6	1.90	.01	.10	1	5
L3+00N 1+50W	1	56	13	393	.1	9	14	863	3.37	3	5	ND	1	63	1	2	2	56	.48	.135	7	14	1.92	214	.14	12	2.59	.02	.15	1	2
L3+00N 1+00W	1	116	14	365	.1	8	17	952	9.22	5	5	ND	2	33	1	2	6	52	.24	.085	6	10	.85	114	.13	4	2.24	.01	.19	1	37
L3+00N 0+50W	2	68	11	197	.1	8	10	955	5.60	3	5	ND	1	43	1	3	2	54	.27	.073	4	11	.91	159	.12	4	2.43	.01	.10	1	2
L3+00N 0+25W	3	59	21	110	.1	8	8	780	3.74	2	5	ND	1	47	1	2	2	60	.26	.066	6	12	1.09	193	.13	2	2.93	.01	.12	1	3
L3+00N 0+00W	2	115	12	92	.1	6	10	532	7.83	2	5	ND	2	39	1	2	2	54	.22	.084	6	9	.86	109	.13	2	2.72	.01	.11	1	1
L3+00N 0+25E	2	54	16	186	.4	14	12	687	4.26	3	5	ND	1	40	1	3	2	74	.30	.055	5	18	1.36	143	.15	2	4.03	.01	.10	1	1
L3+00N 0+50E	2	202	22	135	.4	11	9	688	4.13	5	5	ND	2	36	1	2	5	63	.25	.073	7	17	1.11	135	.13	2	3.34	.01	.10	1	1
L3+00N 0+75E	8	315	35	92	.4	7	9	280	7.24	17	5	ND	3	27	1	3	3	69	.11	.162	16	16	.59	66	.16	4	4.67	.01	.05	1	1
L3+00N 1+00E	3	77	32	124	.3	9	9	647	4.25	6	5	ND	2	36	1	2	2	70	.23	.073	8	15	1.14	116	.17	5	3.44	.01	.09	1	6
L3+00N 1+25E	5	321	34	142	.1	11	10	748	5.31	10	5	ND	3	40	1	4	5	72	.24	.086	10	20	1.57	114	.19	3	5.31	.01	.12	1	1
L3+00N 1+50E	1	164	13	160	.2	14	12	423	3.46	5	5	ND	2	32	1	3	2	65	.28	.064	4	21	.94	94	.16	7	3.25	.02	.05	2	1
L3+00N 1+75E	1	39	14	124	.1	7	7	718	3.81	2	5	ND	2	36	1	2	7	59	.25	.102	3	12	.92	75	.11	4	2.93	.01	.07	1	1
L3+00N 2+00E	2	576	25	38	.4	7	6	220	2.34	2	5	ND	3	17	1	2	5	48	.19	.219	10	20	.70	37	.20	2	5.60	.02	.04	1	1
L3+00N 2+25E	1	2004	36	49	.1	1	13	44	40.26	2	5	ND	3	1	1	2	2	11	.02	.175	26	3	.04	6	.03	2	2.95	.01	.05	1	3
L3+00N 2+50E	2	1168	26	71	.3	3	15	392	35.27	6	5	ND	5	11	1	2	2	46	.10	.173	12	8	.18	62	.15	2	2.77	.01	.07	1	2
L3+00N 2+75E	5	395	48	182	.3	10	20	1357	7.44	2	5	ND	2	52	1	2	5	57	.23	.252	9	14	1.46	285	.13	2	3.15	.01	.12	1	1
L3+00N 3+00E	2	105	24	332	.5	8	24	2053	4.34	3	5	ND	2	55	1	2	2	51	.25	.072	6	10	1.24	227	.16	6	2.38	.01	.11	1	1
L3+00N 3+25E	9	1130	48	66	3.5	2	16	227	13.99	6	5	ND	2	13	1	2	4	34	.06	.113	27	3	.30	44	.05	2	4.32	.01	.05	1	2
L3+00N 3+75E	1	304	14	63	.3	5	6	235	2.51	2	5	ND	1	29	1	4	2	39	.26	.093	11	11	.48	56	.12	2	2.72	.01	.05	1	1
L3+00N 4+00E	1	33	15	255	.1	5	19	3796	3.27	2	5	ND	1	36	1	2	5	43	.24	.138	4	10	.95	179	.10	5	2.07	.01	.11	1	1
L2+00N 5+00W	4	351	21	319	.1	11	23	1244	4.04	6	5	ND	2	59	2	2	2	58	.53	.109	19	15	.92	102	.15	6	3.53	.01	.08	1	2
L2+00N 4+00W	2	279	20	212	.2	11	18	821	3.61	3	5	ND	2	50	1	3	2	58	.25	.116	13	15	1.08	161	.13	7	3.73	.01	.11	1	3
L2+00N 3+75W	3	202	18	401	.1	12	42	2803	5.16	7	5	ND	1	49	3	2	3	59	.37	.070	21	14	.97	119	.15	4	3.98	.01	.11	1	1
L2+00N 3+50W	3	206	21	237	.1	9	22	1109	7.04	3	5	ND	2	51	1	2	5	58	.29	.108	17	13	1.07	145	.15	4	3.32	.01	.15	1	1
L2+00N 3+25W	2	122	18	445	.2	13	24	1584	4.90	5	5	ND	2	42	1	2	2	56	.25	.075	8	14	1.02	135	.15	6	3.23	.01	.10	1	1
L2+00N 2+75W	1	93	16	241	.1	10	23	2355	4.14	6	5	ND	2	44	1	2	2	59	.24	.315	6	14	.97	195	.12	4	3.25	.01	.12	1	6
L2+00N 2+00W	2	713	39	257	.1	9	35	695	23.32	2	5	ND	2	28	1	2	3	41	.13	.068	60	8	.48	94	.11	2	4.32	.01	.09	1	1
L2+00N 1+75W	1	515	29	222	.1	6	32	1090	16.54	5	5	ND	3	31	1	2	6	43	.15	.069	47	9	.61	107	.12	2	3.75	.01	.10	1	3
L2+00N 1+50W	2	342	25	195	.1	5	21	1157	9.04	2	5	ND	2	35	1	2	4	53	.23	.097	10	12	.78	120	.12	6	2.93	.01	.16	1	4
STD C/AU-S	20	61	44	132	7.4	72	31	1075	4.15	42	17	8	40	52	19	16	23	60	.47	.085	40	61	.92	153	.08	36	1.99	.07	.15	14	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L2+00N 1+25W	1	114	7	171	.1	9	12	599	2.65	5	5	ND	1	49	1	2	5	49	.22	.041	9	16	1.16	149	.13	4	1.91	.01	.08	1	1
L2+00N 1+00W	1	46	19	158	.1	8	9	804	2.88	8	5	ND	1	43	1	3	2	42	.22	.058	6	14	1.14	181	.10	3	1.90	.01	.11	1	1
L2+00N 0+25E	12	32	26	114	.1	8	7	743	2.75	6	5	ND	1	25	1	2	4	46	.18	.056	4	17	.95	103	.10	2	1.72	.01	.07	1	1
L2+00N 0+50E	2	95	44	202	.1	16	12	550	3.79	3	5	ND	1	26	1	10	4	66	.22	.065	4	26	1.09	97	.14	2	3.36	.01	.09	1	1
L2+00N 0+75E	1	113	38	251	.1	15	14	3153	3.30	3	5	ND	1	22	1	2	2	55	.26	.121	5	20	1.07	137	.11	6	3.43	.01	.08	1	1
L2+00N 1+00E	1	24	61	190	.1	7	8	846	3.00	2	5	ND	1	24	1	2	2	47	.18	.089	3	14	.56	99	.11	5	2.38	.01	.05	1	1
L2+00N 1+25E	1	51	114	178	.1	8	7	496	2.31	6	5	ND	1	26	1	2	2	40	.18	.041	4	14	.89	96	.09	4	1.84	.01	.06	1	2
L2+00N 1+50E	1	1418	19	77	.1	1	10	170	42.52	2	5	ND	10	2	1	2	2	12	.02	.174	22	6	.04	8	.01	2	4.09	.01	.02	1	1
L2+00N 1+75E	5	1008	36	76	.1	3	10	208	33.14	2	5	ND	9	7	3	2	2	27	.05	.189	26	8	.27	32	.05	2	4.14	.01	.03	1	1
L2+00N 2+00E	14	477	29	26	.1	2	3	42	8.95	2	5	ND	10	10	3	2	2	22	.09	.430	61	3	.08	21	.01	2	2.97	.01	.04	1	1
L2+00N 3+25E	2	44	48	260	.1	8	21	686	4.68	4	5	ND	2	22	1	2	2	48	.15	.236	5	14	.61	113	.09	2	1.84	.01	.05	1	2
L2+00N 3+50E	4	83	644	130	.1	5	25	642	4.65	2	5	ND	1	32	1	2	2	35	.13	.123	8	9	.49	158	.09	3	1.32	.01	.07	1	1
L2+00N 3+75E	6	436	46	162	.1	13	46	808	10.64	2	5	ND	4	45	1	2	2	66	.23	.101	20	18	1.06	157	.17	2	3.15	.01	.08	1	1
L1+00N 5+00W	7	500	29	262	.1	11	110	2832	15.46	2	5	ND	7	35	1	2	3	42	.26	.107	23	13	.64	100	.10	2	4.63	.01	.06	1	2
L1+00N 4+75W A	4	252	17	493	.1	16	57	1548	7.39	2	5	ND	3	47	2	2	2	51	.34	.063	14	18	1.13	110	.13	2	3.36	.01	.08	1	1
L1+00N 4+75W B	12	540	16	793	.1	25	228	4844	9.08	42	5	ND	13	28	7	2	2	39	.14	.096	43	16	.54	73	.07	6	8.05	.01	.05	1	1
L1+00N 4+50W	8	851	24	703	.9	23	299	7740	9.51	48	11	ND	24	20	12	2	2	24	.12	.215	93	15	.38	92	.04	2	7.64	.01	.04	1	1
L1+00N 4+25W	12	512	18	447	.1	13	135	3611	13.74	76	5	ND	11	13	4	2	2	19	.07	.098	33	10	.29	44	.04	2	8.21	.01	.04	1	1
L1+00N 4+00W	11	625	16	392	.1	12	236	6548	11.37	23	5	ND	14	16	8	2	6	11	.14	.075	72	10	.14	31	.01	10	8.98	.01	.03	1	2
L1+00N 3+75W	13	953	24	724	.5	24	264	6925	13.07	2	5	ND	17	31	12	2	2	25	.25	.088	83	14	.43	70	.06	2	6.79	.01	.07	1	3
L1+00N 3+50W	13	842	24	724	.1	23	295	8595	12.53	2	5	ND	13	43	11	2	2	19	.46	.088	74	15	.30	82	.04	4	5.47	.01	.05	1	1
L1+00N 3+25W	10	633	30	395	.1	10	225	6300	15.78	4	5	ND	11	21	4	2	2	17	.13	.095	36	11	.26	54	.03	8	6.81	.01	.06	1	3
L1+00N 3+00W	6	238	12	86	.1	2	53	1398	9.44	16	5	ND	5	5	1	9	2	3	.04	.034	18	3	.02	6	.01	5	9.74	.01	.01	1	4
L1+00N 2+75W	9	521	13	380	.1	10	325	9617	12.54	2	7	ND	19	22	10	2	5	9	.21	.065	28	9	.13	38	.01	2	11.32	.01	.04	1	2
L1+00N 2+50W	9	645	20	419	.1	14	331	9650	7.75	2	5	ND	17	21	9	8	3	12	.36	.072	29	12	.22	41	.02	11	9.45	.01	.04	1	9
L1+00N 2+25W	6	295	21	631	.1	16	107	4176	7.34	2	5	ND	5	41	4	2	2	39	.26	.070	33	14	.72	120	.09	2	3.08	.01	.08	1	1
L1+00N 2+00W	2	47	21	308	.1	9	16	1827	3.68	5	5	ND	1	54	1	2	2	48	.27	.043	5	14	.81	157	.13	4	1.67	.01	.09	1	19
L1+00N 1+75W	1	43	7	312	.1	8	11	2186	3.63	4	5	ND	1	34	1	2	2	48	.25	.056	3	13	.70	140	.11	7	1.53	.01	.06	1	1
L1+00N 1+50W	2	81	12	149	.1	10	10	650	3.50	6	5	ND	1	52	1	2	4	45	.23	.066	7	14	.98	182	.10	3	1.65	.01	.11	1	2
L1+00N 1+00W	7	209	29	143	.1	9	9	592	4.18	3	5	ND	3	31	1	2	2	49	.24	.061	17	17	.84	102	.10	2	2.09	.01	.07	1	1
L1+00N 0+75W	2	204	22	156	.1	11	10	572	3.37	2	5	ND	1	34	1	10	2	48	.25	.018	6	18	1.43	122	.16	4	3.24	.01	.10	1	8
L1+00N 0+50W	2	207	19	143	.1	11	10	551	3.43	2	5	ND	1	36	1	17	2	47	.25	.017	6	18	1.42	120	.16	2	3.21	.01	.09	1	1
L1+00N 0+00W	1	1352	24	82	.1	1	10	195	41.18	2	5	ND	10	2	1	2	2	12	.03	.178	32	5	.05	10	.02	2	3.63	.01	.02	1	1
L1+00N 0+25E	4	323	20	75	.1	5	15	229	21.57	2	5	ND	9	57	1	2	2	27	.45	.044	58	11	.43	87	.06	2	1.49	.01	.04	1	1
L1+00N 0+50E	6	290	35	88	.1	8	11	398	6.42	2	5	ND	4	56	1	4	2	57	.20	.042	36	14	1.06	130	.17	2	2.90	.01	.07	1	1
L1+00N 0+75E	10	634	46	84	.1	8	11	429	9.29	2	5	ND	4	41	1	2	2	56	.17	.129	33	14	.83	131	.13	2	4.63	.01	.07	1	1
STD C/AU-S	20	63	40	132	6.6	72	31	1075	4.06	38	18	8	40	52	19	17	23	64	.48	.091	39	60	.92	181	.08	35	1.81	.07	.14	11	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L1+00N 1+00E	5	239	30	57	.1	5	9	570	10.20	2	5	ND	3	36	1	2	2	49	.15	.101	17	7	1.11	125	.16	10	2.47	.01	.07	1	4
L1+00N 1+25E	10	774	43	147	.4	9	53	1522	9.03	2	5	ND	1	57	1	2	2	45	.29	.066	53	8	.99	129	.12	10	3.22	.01	.09	1	10
L1+00N 1+50E	8	495	46	166	.1	13	21	759	7.89	2	5	ND	3	56	1	2	2	75	.35	.036	21	14	1.25	143	.16	7	3.28	.01	.09	1	7
L1+00N 1+75E	2	239	71	316	.1	11	18	819	3.62	2	5	ND	2	66	1	2	2	44	.33	.058	25	13	1.35	200	.13	15	2.45	.01	.12	2	91
L1+00N 2+00E	8	857	59	108	.9	8	73	689	11.39	4	5	ND	1	32	1	3	2	41	.16	.101	51	9	.53	82	.09	7	4.45	.01	.07	1	10
L1+00N 2+25E	13	769	40	105	.6	9	322	5760	13.40	13	5	ND	4	29	1	2	3	34	.17	.113	33	7	.34	60	.07	17	5.55	.02	.06	1	3
L1+00N 2+50E	15	520	35	147	.2	10	52	576	5.70	4	5	ND	1	51	1	3	2	54	.21	.052	38	12	.78	146	.10	19	4.10	.02	.06	1	1
L1+00N 2+75E	1	32	10	319	.1	10	31	3541	2.36	2	5	ND	1	34	1	2	2	53	.32	.039	4	11	.65	102	.13	7	1.65	.02	.07	1	1
L1+00N 3+00E	3	334	31	110	.3	7	23	1273	3.28	2	5	ND	1	52	1	2	2	22	.48	.034	37	5	.42	120	.07	13	2.62	.02	.05	1	5
L1+00N 3+25E	2	534	42	210	.6	7	18	611	3.89	2	5	ND	1	46	1	2	2	50	.56	.168	62	9	.54	108	.07	9	2.70	.01	.05	1	3
L1+00N 3+50E	1	435	36	209	.5	7	17	644	6.42	2	5	ND	1	46	1	2	2	40	.53	.194	53	8	.46	100	.05	11	2.32	.01	.07	1	2
L1+00N 3+75E	2	677	31	169	.7	6	15	574	4.51	2	5	ND	1	42	1	2	2	32	.52	.206	77	6	.36	83	.04	7	2.49	.01	.05	1	1
L1+00N 4+00E	2	165	10	156	.2	12	11	493	4.42	2	5	ND	2	50	1	2	2	69	.28	.099	14	15	1.03	154	.12	15	2.65	.01	.09	1	1
L0+00N 5+25W	5	255	29	168	.4	10	51	1176	7.80	2	5	ND	2	31	1	2	2	62	.25	.103	10	13	.53	85	.11	11	2.74	.01	.06	1	1
L0+00N 4+75W	4	476	16	125	.4	11	22	779	8.10	4	5	ND	2	38	1	2	2	78	.27	.092	22	15	1.02	125	.16	2	3.31	.01	.11	1	1
L0+00N 4+50W	1	55	8	258	.1	10	13	758	3.14	2	5	ND	1	34	1	2	2	76	.31	.066	2	14	.92	96	.13	10	2.06	.01	.07	1	7
L0+00N 4+25W	5	547	35	175	.4	8	49	772	7.65	2	5	ND	1	32	1	2	2	48	.21	.136	31	10	.59	91	.09	2	3.42	.01	.05	1	1
L0+00N 3+75W	5	557	38	186	.4	9	46	907	9.40	2	5	ND	2	31	1	2	2	54	.20	.189	30	10	.67	98	.10	2	3.57	.01	.06	1	1
L0+00N 3+25W	6	748	26	177	.2	9	17	1239	12.52	4	5	ND	4	32	1	4	2	64	.20	.215	12	12	.76	122	.11	7	4.47	.02	.03	1	2
L0+00N 2+00W	9	532	31	186	.3	7	267	5925	13.45	9	5	ND	2	35	1	2	2	38	.41	.119	22	7	.42	89	.07	13	3.95	.01	.08	1	1
L0+00N 1+75W	2	293	22	142	.1	12	32	836	6.17	2	5	ND	2	41	1	2	2	64	.30	.100	8	15	1.28	115	.12	8	3.40	.01	.10	1	2
L0+00N 1+50W	3	445	23	161	.3	15	19	627	5.65	2	5	ND	2	44	1	2	2	67	.33	.087	20	15	1.35	139	.14	4	3.70	.01	.12	1	1
L0+00N 1+25W	4	241	14	132	.1	9	12	1279	7.22	2	5	ND	2	38	1	2	2	65	.34	.055	8	10	.89	141	.12	3	2.34	.01	.09	1	1
L0+00N 1+00W	7	655	28	129	.7	5	221	4218	21.74	9	5	ND	2	24	1	2	2	24	.23	.121	46	4	.21	51	.04	16	3.21	.03	.05	1	8
L0+00N 0+25W	5	359	27	254	.1	10	39	1015	9.44	5	5	ND	3	52	1	2	2	48	.38	.200	13	13	.95	118	.10	2	2.81	.01	.10	1	1
L0+00N 0+25E	5	463	25	665	.5	15	43	1257	6.85	2	5	ND	2	59	2	2	2	51	.52	.079	21	12	.83	104	.09	13	3.64	.05	.13	4	1
L0+00N 0+50E	5	1131	43	199	.4	11	182	3940	9.09	2	5	ND	1	21	1	2	2	25	.20	.091	31	15	.36	44	.06	2	6.02	.02	.06	1	1
L0+00N 0+75E	5	500	152	87	.7	1	54	1319	27.22	6	5	ND	1	11	1	3	2	14	.11	.064	41	1	.09	16	.01	15	3.39	.01	.03	1	1
L0+00N 1+00E	6	667	202	95	.9	3	102	2018	26.34	2	5	ND	1	17	1	2	2	18	.17	.058	50	3	.14	25	.02	11	3.05	.01	.04	1	1
L0+00N 1+25E	1	39	16	109	.1	4	12	1466	2.73	2	5	ND	1	36	1	2	2	38	.31	.021	6	7	.59	58	.10	2	1.29	.02	.06	1	1
L0+00N 1+50E	1	35	14	201	.1	10	11	881	2.71	2	5	ND	1	49	1	2	2	45	.34	.065	5	12	1.13	149	.10	3	2.27	.02	.10	1	1
L0+00N 1+75E	1	46	14	214	.2	9	12	1738	2.86	2	5	ND	2	34	1	2	2	51	.23	.078	4	11	.91	124	.11	2	2.06	.01	.05	1	1
L0+00N 2+00E	16	235	21	482	.2	15	49	1085	6.40	2	5	ND	3	55	1	2	2	65	.39	.072	10	17	.97	85	.11	2	2.36	.02	.09	2	2
L0+00N 2+25E	3	37	26	120	.3	9	11	554	3.62	2	5	ND	5	36	1	2	2	59	.31	.061	4	12	1.21	89	.12	6	1.94	.01	.11	1	1
L0+00N 2+50E	9	145	111	155	.4	10	12	419	5.72	6	5	ND	2	30	1	2	3	73	.17	.107	7	16	.60	73	.13	2	2.63	.01	.06	2	1
L0+00N 2+75E	12	512	12	88	.4	10	81	793	6.41	2	5	ND	2	35	1	3	2	53	.22	.101	25	11	.97	82	.10	4	4.04	.02	.09	1	2
STD C AU-S	19	61	40	130	7.2	70	31	1029	3.94	41	16	8	39	52	19	18	16	62	.48	.087	41	59	.94	177	.07	33	1.73	.06	.14	13	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L0+00N 3+00E	5	41	12	55	.1	6	10	330	4.73	2	5	ND	1	50	1	2	2	49	.13	.090	6	12	.80	282	.12	2	2.11	.01	.10	1	6
L0+00N 3+25E	2	17	10	49	.2	4	4	270	2.85	2	5	ND	1	62	1	2	2	37	.11	.064	7	6	.55	356	.08	2	1.41	.01	.10	1	4
L0+00N 3+50E	3	17	5	46	.2	1	3	164	3.52	2	5	ND	1	38	1	2	2	44	.06	.144	5	8	.35	283	.09	6	1.68	.01	.04	2	1
L0+00N 3+75E	3	245	18	87	.1	5	14	444	6.27	2	5	ND	1	26	1	2	2	50	.16	.103	34	8	.62	98	.10	2	2.64	.01	.07	1	3
L0+00N 4+00E	1	117	13	94	.1	7	13	418	2.99	2	5	ND	1	27	1	2	2	56	.23	.060	19	12	.64	78	.09	3	2.05	.01	.05	2	4
L1+00S 5+50W	1	157	6	91	.1	10	17	683	3.98	2	5	ND	1	32	1	2	2	77	.25	.102	7	19	.99	151	.11	2	3.30	.01	.09	1	1
L1+00S 5+25W	2	129	2	55	.1	2	11	485	2.72	2	5	ND	1	32	1	2	2	51	.29	.061	2	10	.92	232	.09	2	2.55	.04	1.43	1	2
L1+00S 5+00W	4	135	14	83	.1	11	17	701	4.14	2	5	ND	1	35	1	2	2	57	.29	.074	4	13	1.16	109	.10	2	2.68	.01	.10	1	1
L1+00S 4+75W	19	573	31	99	.1	6	139	1625	6.10	3	5	ND	1	28	1	2	2	49	.18	.099	24	9	.85	87	.07	6	5.05	.01	.07	1	1
L1+00S 4+50W	11	969	28	88	.1	11	204	2682	5.68	4	5	ND	1	27	1	2	2	40	.14	.097	46	5	.62	82	.06	5	6.46	.01	.06	1	1
L1+00S 4+25W	5	163	29	80	.1	7	52	1293	4.33	2	5	ND	1	41	1	2	4	45	.39	.093	7	9	1.22	109	.07	8	2.17	.01	.07	1	2
L1+00S 4+00W	11	646	19	69	.1	6	43	530	5.15	3	5	ND	1	30	1	2	2	50	.22	.097	32	8	.83	62	.07	2	4.97	.01	.06	2	1
L1+00S 3+75W	9	463	22	107	.1	9	100	1424	6.50	2	5	ND	1	60	1	2	2	44	.56	.095	27	8	.86	125	.07	13	3.89	.01	.10	1	1
L1+00S 3+50W	2	76	8	35	.1	4	11	282	3.00	2	5	ND	1	37	1	2	2	69	.29	.017	5	14	.77	68	.10	7	1.72	.02	.07	1	2
L1+00S 3+25W	9	364	19	92	.3	7	33	434	7.34	2	5	ND	2	27	1	2	3	52	.18	.091	9	12	.78	96	.09	2	3.43	.01	.07	1	1
L1+00S 3+00W	11	295	29	88	.1	3	19	367	9.15	2	5	ND	1	24	1	2	2	56	.13	.100	8	9	.81	75	.09	6	3.02	.01	.06	1	1
L1+00S 2+75W	2	190	19	65	.1	11	11	386	3.69	2	5	ND	1	35	1	2	2	63	.25	.064	7	16	1.03	131	.12	2	3.07	.01	.08	1	1
L1+00S 2+50W	1	107	8	41	.1	7	13	318	3.27	2	5	ND	2	43	1	2	2	74	.34	.037	5	13	.87	102	.09	14	1.99	.03	.08	2	2
L1+00S 2+25W	2	243	10	53	.1	5	11	423	6.42	2	5	ND	1	30	1	2	2	57	.28	.064	6	12	.91	80	.09	6	2.31	.01	.10	1	1
L1+00S 2+00W	6	410	26	94	.1	10	21	392	10.40	3	5	ND	2	26	1	2	2	51	.15	.109	13	9	.78	90	.12	4	3.84	.01	.08	1	1
L1+00S 1+75W	3	395	14	94	.1	9	26	596	3.59	2	5	ND	2	50	1	2	4	51	.28	.039	11	13	1.32	175	.11	5	3.05	.01	.09	1	6
L1+00S 1+50W	10	276	23	144	.1	8	25	489	7.04	2	5	ND	2	29	1	2	2	67	.17	.056	7	9	.71	44	.12	3	2.42	.01	.05	1	1
L1+00S 1+25W	2	95	8	210	.3	9	45	688	3.35	2	5	ND	1	29	1	2	2	47	.21	.049	4	11	.74	65	.09	7	2.02	.01	.05	1	2
L1+00S 1+00W	8	496	30	175	.4	9	45	949	10.41	2	5	ND	2	36	2	2	2	48	.23	.203	14	9	.67	124	.11	4	3.59	.01	.09	1	1
L1+00S 0+75W	11	611	22	70	.1	7	223	3772	4.98	2	5	ND	1	53	1	2	2	34	.61	.157	33	5	.57	72	.04	5	4.15	.01	.06	1	1
L1+00S 0+50W	3	98	12	109	.1	10	37	681	3.70	2	5	ND	1	44	1	2	2	64	.36	.035	5	15	.93	106	.10	5	2.57	.01	.06	1	1
L1+00S 0+25W	2	23	9	118	.1	6	11	1016	2.35	2	5	ND	1	34	1	2	2	43	.28	.026	3	8	.81	58	.11	2	1.49	.01	.05	1	1
L1+00S 0+00E	1	27	8	134	.1	10	10	1400	2.59	2	5	ND	1	31	1	2	2	49	.31	.024	3	31	1.16	89	.13	3	1.73	.01	.07	1	1
L1+00S 0+25E	1	24	6	147	.1	7	11	695	2.35	2	5	ND	1	23	1	2	2	39	.22	.032	3	8	1.12	55	.13	10	1.60	.01	.07	1	2
L1+00S 0+50E	1	40	12	169	.1	10	15	1577	3.13	2	5	ND	1	32	1	2	2	58	.28	.026	3	14	1.27	89	.15	5	2.08	.01	.09	1	1
L1+00S 0+75E	1	21	8	191	.1	6	12	749	2.37	2	5	ND	1	36	1	2	2	44	.30	.015	4	9	.91	81	.12	5	1.52	.01	.05	1	1
L1+00S 1+00E	2	35	6	108	.1	7	11	569	2.08	5	5	ND	1	34	1	3	5	43	.26	.010	3	9	.64	73	.11	4	1.48	.01	.04	1	1
L1+00S 1+25E	1	28	8	220	.1	6	10	487	2.49	2	5	ND	1	30	1	2	2	52	.25	.017	3	10	1.01	57	.15	10	1.77	.01	.06	1	1
L1+00S 1+50E	12	97	15	292	.1	17	59	855	6.12	2	5	ND	1	28	1	2	4	76	.22	.058	6	17	1.09	76	.13	5	3.14	.01	.04	1	2
L1+00S 1+75E	1	56	27	401	.1	10	14	623	2.57	2	5	ND	1	28	1	2	3	50	.25	.014	3	16	1.12	75	.14	2	2.09	.01	.06	1	1
L1+00S 2+00E	1	60	16	279	.1	12	12	995	2.80	2	5	ND	1	38	1	2	2	52	.26	.046	4	12	1.12	134	.11	3	2.10	.01	.08	1	2
STD C/AU-S	20	62	40	131	7.3	71	31	1050	4.01	43	18	8	40	53	20	16	23	61	.46	.085	40	60	.95	185	.08	34	1.92	.07	.14	14	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L1+00S 1+25E	1	26	10	109	.1	7	13	532	3.35	4	5	ND	1	30	1	2	2	56	.22	.032	3	12	.76	92	.13	4	1.61	.01	.07	1	1
L1+00S 1+50E	15	122	6	200	.1	17	111	1466	8.20	26	5	ND	2	38	1	2	2	76	.36	.083	16	11	.87	125	.10	2	3.79	.01	.07	1	1
L1+00S 1+75E	14	283	11	131	.1	16	74	4888	5.39	16	5	ND	2	39	1	2	2	47	.29	.059	16	11	.78	150	.10	9	4.30	.01	.07	1	10
L1+00S 2+00E	4	73	17	125	.1	14	19	1559	6.75	10	5	ND	1	37	1	2	2	47	.19	.055	7	11	.63	140	.13	12	2.40	.01	.07	1	1
L1+00S 2+25E	5	32	33	140	.1	8	13	1078	6.68	9	5	ND	2	45	1	3	2	42	.14	.124	6	6	.47	207	.15	9	1.90	.01	.09	2	1
L2+00S 3+50E	1	38	18	127	.1	13	12	523	3.46	3	5	ND	1	42	1	2	2	58	.22	.052	3	28	1.25	137	.15	7	2.03	.01	.08	1	1
L2+00S 3+75E	3	59	10	122	.1	11	62	2572	4.73	5	5	ND	1	105	1	3	2	35	1.66	.072	10	15	.59	147	.06	14	1.75	.01	.05	1	22
L1+00S 4+00E	1	23	9	84	.1	12	18	1141	2.77	2	5	ND	1	32	1	2	2	68	.48	.014	2	22	1.35	190	.24	13	1.90	.02	.12	1	1
L2+00S 5+25W	1	87	10	113	.1	12	14	715	3.11	2	5	ND	1	42	1	2	2	56	.37	.096	3	19	.96	115	.13	6	2.96	.01	.06	1	1
L2+00S 5+00W	1	28	4	94	.1	4	9	378	1.71	2	5	ND	1	31	1	8	2	37	.30	.022	3	11	.42	50	.12	18	1.29	.01	.04	1	1
L2+00S 4+75W	1	41	12	111	.1	10	10	558	2.84	2	5	ND	1	35	1	2	4	56	.33	.075	3	16	.86	59	.13	5	2.41	.01	.07	1	1
L2+00S 4+50W	1	73	5	103	.1	9	12	759	3.07	2	5	ND	1	33	1	2	2	58	.29	.051	3	17	.98	85	.11	9	2.34	.01	.06	1	1
L2+00S 4+25W	1	13	5	56	.1	6	6	346	2.05	2	5	ND	1	25	1	2	3	46	.21	.026	2	9	.45	38	.10	5	1.26	.01	.03	1	1
L2+00S 4+00W	2	79	7	79	.1	11	12	1088	2.75	3	5	ND	1	31	1	2	3	54	.33	.044	2	14	.86	65	.11	2	2.63	.01	.07	1	4
L2+00S 3+75W	1	41	7	93	.1	9	9	534	2.57	2	5	ND	1	33	1	3	2	50	.30	.018	2	12	.95	77	.16	3	2.03	.01	.06	1	2
L2+00S 3+50W	1	61	8	143	.1	9	10	1632	2.61	2	5	ND	1	34	1	2	3	47	.29	.087	4	12	.74	205	.10	6	2.34	.01	.07	1	1
L2+00S 3+25W	1	26	7	132	.1	8	9	1468	2.09	2	5	ND	1	32	1	2	2	36	.27	.068	2	9	.59	174	.09	8	1.80	.01	.07	1	1
L2+00S 3+00W	1	40	13	87	.2	9	9	403	3.23	7	5	ND	1	27	1	2	2	61	.24	.046	3	13	1.03	92	.13	2	2.79	.01	.06	1	2
L2+00S 2+75W	1	35	7	95	.1	9	12	636	2.87	4	5	ND	1	34	1	2	2	57	.28	.031	3	15	.74	99	.14	8	2.72	.01	.05	1	2
L2+00S 2+50W	1	34	7	84	.1	10	8	644	2.76	3	5	ND	1	27	1	2	2	55	.27	.063	2	15	.63	58	.11	8	2.54	.01	.05	1	1
L2+00S 2+25W	1	127	15	134	.3	18	15	708	3.47	3	5	ND	1	38	1	2	2	54	.31	.063	4	21	1.30	135	.12	10	3.25	.01	.09	1	4
L2+00S 2+00W	1	15	10	132	.3	6	8	970	2.06	2	5	ND	1	27	1	2	2	37	.25	.034	3	10	.52	93	.03	11	1.68	.01	.05	1	2
L2+00S 1+75W	1	12	7	63	.2	5	5	705	2.02	2	5	ND	1	28	1	2	2	38	.23	.044	2	7	.57	78	.10	5	1.34	.01	.05	1	3
L2+00S 1+50W	1	67	14	114	.1	9	10	650	2.94	2	5	ND	1	29	1	2	2	45	.24	.080	3	14	.90	110	.10	8	2.51	.01	.09	1	1
L2+00S 1+25W	2	71	23	133	.2	10	8	510	3.91	6	5	ND	2	27	1	2	2	52	.19	.214	4	15	.82	95	.12	7	2.96	.01	.06	1	1
L2+00S 1+00W A	1	30	12	64	.3	8	7	316	2.36	3	5	ND	1	31	1	2	2	51	.24	.048	3	14	.58	71	.10	6	2.13	.01	.06	1	4
L2+00S 1+00W B	2	33	22	301	.1	9	10	476	3.16	2	5	ND	1	39	1	2	2	45	.27	.034	4	12	.82	126	.13	2	2.49	.01	.07	1	1
L2+00S 0+75W	1	31	20	100	.1	7	12	566	2.59	2	5	ND	1	33	1	2	2	48	.27	.051	3	13	.88	84	.11	3	1.98	.01	.05	1	1
L2+00S 0+50W	1	30	13	135	.1	10	9	1151	2.75	2	5	ND	1	29	1	2	2	45	.28	.124	3	12	.61	101	.10	3	2.05	.01	.06	1	5
L2+00S 0+25W	4	41	12	126	.1	12	36	564	3.06	2	5	ND	1	35	1	2	2	48	.30	.029	3	12	.62	75	.13	5	1.93	.01	.05	1	1
L2+00S 0+00W	3	133	5	110	.2	21	51	500	3.84	2	5	ND	1	34	1	2	2	65	.31	.031	5	15	.79	76	.12	17	3.33	.02	.05	2	1
L2+00S 0+25E	3	112	7	158	.1	23	63	817	4.10	5	5	ND	1	41	1	2	2	64	.41	.030	5	14	.76	113	.13	17	3.42	.02	.05	2	1
L2+00S 0+50E	6	153	[illegible]	[illegible]	.2	22	74	1105	3.54	7	5	ND	1	47	1	2	2	54	.47	.024	16	12	.61	114	.11	7	3.31	.02	.06	1	1
L2+00S 0+75E	6	111	5	111	.1	19	55	549	4.75	7	5	ND	2	35	1	2	2	66	.29	.020	5	15	.58	81	.14	13	2.80	.02	.07	1	2
L2+00S 1+00E	1	13	11	50	.1	7	8	351	2.81	2	5	ND	1	36	1	2	2	65	.33	.015	2	10	.51	62	.14	10	1.67	.01	.04	1	1
L2+00S 1+25E	1	11	8	114	.1	10	12	476	3.35	3	5	ND	1	30	1	2	2	77	.29	.130	2	14	.61	63	.15	14	1.82	.01	.06	1	1
STD C/AU-S	20	62	41	132	7.4	72	32	1067	4.15	42	19	8	41	52	20	17	22	61	.47	.089	40	64	.88	182	.08	36	2.02	.07	.15	15	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L2+00S 1+50E	9	371	2	118	.6	19	207	4706	3.01	3	5	ND	1	101	1	2	3	41	1.43	.080	45	6	.48	162	.05	4	3.25	.04	.04	1	1
L2+00S 1+75E	2	60	6	85	.1	10	12	344	3.61	2	5	ND	1	46	1	2	2	93	.34	.030	4	13	.80	72	.17	6	2.09	.05	.05	1	19
L2+00S 2+00E	7	78	7	114	.4	12	51	406	4.20	2	5	ND	1	44	1	2	2	87	.32	.024	4	13	.78	62	.17	7	2.16	.04	.05	1	3
L2+00S 2+25E	7	235	6	148	.5	19	67	544	4.33	2	5	ND	1	46	1	2	2	78	.39	.025	9	14	.94	100	.17	6	3.81	.05	.05	1	1
L2+00S 2+50E	5	261	2	261	.3	31	190	2195	4.94	4	5	ND	1	44	1	2	2	74	.39	.044	13	12	.79	123	.14	5	3.46	.02	.04	1	1
L2+00S 2+75E	1	44	2	172	.4	10	15	481	3.50	2	5	ND	1	39	1	2	2	78	.33	.077	3	13	1.04	91	.15	2	2.51	.02	.05	1	1
L2+00S 3+00E	1	56	4	99	.4	12	20	782	3.80	2	5	ND	1	46	1	2	2	90	.42	.035	4	16	.94	115	.15	11	2.26	.05	.07	1	1
L2+00S 3+25E	2	61	2	47	.1	9	15	301	3.72	2	5	ND	1	43	1	3	2	104	.34	.017	4	14	.67	51	.12	8	2.12	.06	.01	3	2
L2+00S 3+50E	2	136	2	78	.1	12	27	416	3.78	2	5	ND	1	48	1	2	4	101	.40	.020	5	16	.85	90	.14	12	2.45	.04	.01	1	1
L2+00S 3+75E	7	181	3	158	.1	11	80	1007	3.34	2	5	ND	1	38	1	2	2	73	.31	.025	6	12	.64	52	.13	4	2.25	.02	.03	1	1
L2+00S 4+00E	16	263	14	49	.1	4	18	266	2.78	9	5	ND	1	20	1	2	2	51	.27	.075	22	4	.24	37	.05	8	13.03	.01	.01	2	2
L3+00S 5+50W	4	311	11	376	.2	32	236	2019	3.61	5	5	ND	1	48	2	2	2	64	.38	.047	14	17	.82	151	.13	6	8.22	.03	.06	2	1
L3+00S 5+25W	5	146	6	159	.1	17	61	1085	3.85	2	5	ND	1	56	1	2	2	78	.42	.041	10	15	.86	160	.14	8	3.37	.02	.06	1	1
L3+00S 5+00W	1	82	4	102	.2	11	13	423	3.34	2	5	ND	1	48	1	2	2	83	.42	.038	4	16	1.08	98	.18	6	2.65	.06	.10	1	82
L3+00S 4+75W	1	63	5	101	.1	9	11	1136	2.86	2	5	ND	1	49	1	2	2	70	.44	.040	3	13	.94	132	.13	2	2.45	.05	.05	1	1
L3+00S 4+50W	1	34	6	125	.1	8	11	1963	2.52	2	5	ND	1	44	1	2	2	60	.36	.077	3	14	.87	113	.12	2	1.93	.03	.03	1	2
L3+00S 4+25W	1	62	5	101	.1	10	11	475	3.29	2	5	ND	1	51	1	2	2	74	.36	.122	5	15	1.07	133	.13	4	2.92	.06	.07	1	4
L3+00S 4+00W	1	34	4	112	.1	8	10	1726	2.53	2	5	ND	1	37	1	2	2	62	.29	.084	3	13	.82	129	.13	4	2.04	.03	.02	1	2
L3+00S 3+75W	1	50	4	116	.1	11	12	510	3.25	2	5	ND	1	46	1	2	2	77	.39	.103	3	17	.96	107	.14	2	3.18	.03	.04	1	22
L3+00S 3+50W	1	29	6	131	.3	10	12	434	2.83	2	5	ND	1	44	1	2	2	67	.35	.060	4	14	.84	115	.14	2	2.37	.02	.04	1	1
L3+00S 3+25W	1	225	5	86	.1	11	12	1200	2.79	2	5	ND	1	52	1	2	2	67	.44	.025	4	16	1.10	146	.15	7	2.72	.03	.06	1	13
L3+00S 3+00W	1	42	8	75	.1	9	11	488	2.72	2	5	ND	1	53	1	2	2	64	.45	.032	3	14	.87	126	.13	5	2.19	.03	.06	1	1
L3+00S 2+75W	1	120	6	116	.1	16	14	724	3.68	3	5	ND	1	59	1	2	2	78	.51	.041	4	24	1.33	146	.16	5	3.55	.01	.10	1	2
L3+00S 2+50W	1	40	6	81	.1	4	10	449	2.71	2	5	ND	1	45	1	2	2	68	.36	.035	2	14	.67	69	.15	6	1.86	.01	.01	1	1
L3+00S 2+25W	3	151	7	94	.1	15	18	590	4.11	2	5	ND	1	51	1	2	2	83	.39	.046	4	17	1.25	144	.15	2	3.67	.03	.06	1	1
L3+00S 2+00W	1	145	8	123	.2	15	21	685	4.47	2	5	ND	1	61	1	2	2	93	.54	.146	4	25	1.54	137	.15	2	4.10	.05	.13	1	3
L3+00S 1+75W	1	85	10	126	.1	14	28	682	3.53	2	5	ND	1	48	1	2	2	77	.40	.049	3	15	1.00	99	.16	4	2.76	.02	.05	1	2
L3+00S 1+50W	1	43	6	110	.1	10	15	490	2.93	2	5	ND	1	45	1	2	2	74	.38	.045	3	14	.73	79	.14	2	2.04	.02	.03	1	1
L3+00S 1+25W	4	196	12	112	.1	26	67	1775	4.09	3	5	ND	1	104	1	2	2	77	.96	.029	22	27	1.56	308	.17	2	4.56	.04	.11	1	3
L3+00S 1+00W	1	21	4	57	.1	5	10	341	2.82	2	5	ND	1	44	1	2	4	76	.45	.011	3	4	.88	73	.25	2	1.67	.02	.07	1	1
L3+00S 0+75W	1	12	6	79	.1	5	10	935	2.56	2	5	ND	1	43	1	3	2	61	.39	.025	2	6	1.04	110	.21	2	1.54	.01	.09	1	1
L3+00S 0+50W	1	8	4	46	.1	4	5	503	1.70	2	5	ND	1	40	1	2	2	45	.38	.010	2	6	.47	56	.16	8	.86	.01	.02	1	1
L3+00S 0+25W	1	15	7	80	.1	6	6	440	2.08	3	5	ND	1	41	1	3	2	52	.38	.039	3	8	.72	91	.13	2	1.36	.05	.05	1	1
L3+00S 0+00W	1	14	8	58	.1	5	6	349	2.20	2	5	ND	1	36	1	2	2	57	.30	.026	3	9	.67	61	.16	8	1.66	.01	.02	1	1
L3+00S 0+25E	1	30	6	132	.1	10	8	451	3.32	4	5	ND	1	42	1	2	2	71	.32	.121	4	16	.71	115	.13	4	3.44	.02	.04	1	5
L3+00S 0+50E	1	44	16	86	.1	7	7	674	2.70	2	5	ND	1	49	1	2	2	55	.31	.050	5	11	.77	129	.13	3	2.25	.02	.06	1	2
STD C/AU-S	20	63	41	132	7.7	73	31	1088	4.00	42	17	8	40	56	20	18	20	61	.48	.090	40	60	.95	182	.08	37	1.84	.06	.14	13	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L3+00S 0+75E	1	110	23	142	.1	15	13	607	4.43	2	5	ND	3	42	1	2	2	80	.33	.148	4	28	1.24	122	.18	5	4.35	.02	.11	1	1
L3+00S 1+00E	1	28	17	108	.2	7	7	251	3.35	2	5	ND	1	33	1	2	2	62	.25	.089	4	15	.53	75	.14	3	2.20	.02	.05	1	4
L3+00S 1+25E	1	32	10	168	.1	10	29	684	2.67	2	5	ND	1	31	1	2	4	54	.26	.114	4	15	.54	75	.15	10	2.05	.02	.06	1	1
L3+00S 1+50E	2	200	15	111	.1	11	40	1239	2.94	2	5	ND	1	31	1	7	2	60	.23	.160	10	16	.60	36	.12	10	2.60	.02	.06	1	1
L3+00S 1+75E	1	31	8	96	.1	7	16	809	2.14	2	5	ND	1	35	1	2	4	53	.30	.049	3	14	.59	68	.13	6	1.49	.02	.05	1	1
L3+00S 2+00E	1	153	12	172	.3	14	34	1762	3.35	2	5	ND	2	29	1	2	2	57	.24	.203	5	18	.82	53	.14	8	3.89	.02	.09	1	1
L3+00S 2+25E	1	145	17	143	.1	12	31	751	3.16	2	5	ND	1	37	1	2	2	64	.27	.063	8	18	.84	112	.16	6	5.15	.03	.08	1	1
L3+00S 2+50E	1	176	13	141	.1	19	19	698	3.66	2	5	ND	2	43	1	2	2	71	.36	.055	6	25	1.44	143	.19	8	3.94	.02	.14	1	3
L3+00S 2+75E	4	465	17	102	.5	12	51	764	3.19	2	5	ND	5	25	1	2	2	60	.24	.036	18	19	.75	55	.15	13	5.22	.01	.06	1	2
L3+00S 3+00E	7	411	13	92	.2	10	49	368	3.07	2	5	ND	2	27	1	2	2	47	.22	.037	13	15	.60	43	.13	2	4.79	.01	.05	3	1
L3+00S 3+50E	12	532	6	47	.3	5	51	726	2.21	7	5	ND	3	20	1	2	2	24	.25	.081	17	7	.30	37	.04	2	9.85	.01	.03	3	1
L3+00S 3+75E	8	223	11	111	.1	11	34	1205	4.25	2	5	ND	1	46	1	30	2	58	.31	.218	4	16	1.06	119	.10	3	3.35	.02	.08	3	1
L3+00S 4+00E	4	143	19	146	.1	9	45	2193	4.46	2	5	ND	1	28	1	2	2	59	.21	.095	5	14	.57	104	.13	2	3.31	.02	.05	1	4
L4+00S 5+75W A	2	150	15	242	.1	16	59	2274	2.66	2	5	ND	2	36	1	11	2	50	.34	.261	5	20	.73	110	.12	2	2.88	.02	.08	1	9
L4+00S 5+75W B	1	146	16	252	.1	16	66	2276	2.75	2	5	ND	3	37	1	8	2	52	.32	.293	4	22	.79	116	.13	14	3.70	.02	.09	1	4
L4+00S 5+50W	1	54	9	327	.2	17	50	3077	2.55	2	5	ND	2	35	2	7	2	49	.29	.200	4	21	.75	131	.12	4	3.62	.02	.07	1	1
L4+00S 5+25W	1	310	11	270	.4	17	160	2788	2.66	2	5	ND	4	27	3	2	2	35	.25	.257	10	16	.43	102	.09	7	7.76	.01	.06	1	1
L4+00S 5+00W	5	364	12	214	.2	15	171	3558	2.90	2	5	ND	3	27	1	2	2	44	.23	.245	13	17	.55	93	.11	3	7.72	.01	.06	1	1
L4+00S 4+75W	2	139	11	291	.1	19	72	1716	2.75	2	5	ND	2	31	1	2	2	48	.27	.150	5	17	.50	126	.13	4	5.65	.01	.06	2	1
L4+00S 4+50W	1	89	4	321	.1	12	79	2224	2.58	2	5	ND	1	33	1	2	2	51	.26	.140	4	16	.73	153	.16	4	2.10	.02	.08	1	6
L4+00S 4+25W	1	12	6	46	.1	4	6	287	1.71	2	5	ND	1	39	1	2	2	47	.30	.015	3	10	.49	54	.15	6	1.14	.02	.06	2	1
L4+00S 4+00W	2	75	11	105	.1	11	15	493	3.62	2	5	ND	2	40	1	5	3	77	.32	.095	4	18	.95	111	.13	3	3.26	.01	.07	1	1
L4+00S 3+75W	1	35	7	125	.1	10	12	592	2.64	2	5	ND	1	40	1	2	2	61	.34	.028	3	18	.97	108	.19	11	1.89	.02	.05	1	5
L4+00S 3+50W	1	92	13	146	.1	22	18	704	3.79	2	5	ND	1	64	1	2	2	74	.55	.035	4	37	1.47	150	.22	4	4.21	.02	.10	1	1
L4+00S 3+25W	1	15	6	113	.1	6	10	982	1.99	2	5	ND	1	40	1	2	2	47	.35	.020	3	12	.67	93	.19	7	1.33	.02	.07	1	1
L4+00S 3+00W	1	42	9	260	.1	13	17	1483	2.79	2	5	ND	1	40	1	2	2	54	.28	.047	4	21	.87	134	.16	12	1.89	.02	.07	1	1
L4+00S 2+75W	1	28	10	159	.1	10	13	740	2.55	2	5	ND	1	41	1	2	2	56	.36	.025	3	17	.73	124	.18	10	1.86	.02	.08	1	1
L4+00S 2+50W	1	66	5	154	.1	12	14	542	2.83	2	5	ND	1	49	1	2	2	63	.42	.020	3	21	1.07	74	.17	4	2.04	.02	.07	1	2
L4+00S 2+25W	1	30	9	352	.1	14	37	1084	2.08	2	5	ND	1	40	1	2	2	44	.33	.021	4	15	.53	102	.19	7	1.74	.02	.07	1	1
L4+00S 2+00W	5	1035	11	157	.9	17	275	2017	2.45	2	5	ND	12	28	3	2	2	27	.27	.137	44	13	.31	60	.05	8	12.51	.01	.03	1	1
L4+00S 1+75W	6	1625	14	159	.8	23	355	4055	1.75	2	5	ND	6	28	4	2	2	23	.28	.126	57	16	.32	54	.05	11	10.15	.01	.04	1	1
L4+00S 1+50W	3	175	10	279	.1	17	156	1673	2.37	2	5	ND	2	30	2	2	2	36	.29	.054	6	14	.31	98	.09	8	5.71	.01	.05	1	1
L4+00S 1+25W	2	82	14	251	.1	20	29	1158	2.99	2	5	ND	1	55	1	2	2	54	.43	.041	4	21	1.07	122	.15	4	3.35	.02	.09	1	4
L4+00S 1+00W	7	1195	14	236	1.0	18	265	3831	2.91	2	5	ND	7	27	3	2	2	35	.21	.107	57	15	.44	57	.08	10	9.08	.01	.05	1	5
L4+00S 0+75W	10	1354	14	101	1.2	17	369	3132	2.10	2	5	ND	11	41	4	2	2	25	.32	.069	72	27	.41	63	.06	8	10.02	.01	.05	1	1
L4+00S 0+50W	10	1038	15	72	1.0	10	241	2663	2.27	2	5	ND	6	33	2	2	2	29	.28	.074	53	25	.41	43	.06	11	8.61	.01	.05	1	1
STD C/AU-S	20	60	41	132	7.3	70	31	1092	4.00	38	23	7	40	53	20	16	22	60	.47	.094	41	60	.93	182	.08	36	1.80	.07	.14	14	49

HAROLD M. JONES PROJECT-WHISTLER FILE # 88-1426

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L4+00S 0+25W	10	590	7	110	.3	15	133	966	3.11	2	9	ND	1	45	1	2	2	33	.49	.039	29	7	.38	42	.06	13	6.42	.04	.06	1	8
L4+00S 0+00W	5	276	5	213	.2	16	89	743	3.00	2	7	ND	1	29	1	2	2	42	.27	.059	6	9	.50	74	.09	11	5.53	.01	.06	1	2
L4+00S 0+25E	9	553	4	39	.5	13	138	943	2.63	2	6	ND	1	17	1	2	2	25	.17	.042	35	6	.29	39	.06	9	9.63	.02	.03	1	1
L4+00S 0+50E	9	731	3	153	.7	16	232	2066	2.98	11	5	ND	1	14	2	2	2	26	.12	.071	29	6	.28	55	.05	15	10.09	.02	.02	1	2
L4+00S 0+75E	5	454	4	107	.2	9	185	2546	2.58	2	5	ND	1	22	1	2	2	32	.19	.028	24	7	.33	40	.08	9	4.05	.03	.05	1	1
L4+00S 1+00E	3	415	3	97	.6	11	126	1791	2.71	3	8	ND	2	18	1	2	2	27	.14	.060	33	6	.42	47	.07	6	7.89	.03	.06	1	1
L4+00S 1+25E	1	35	5	167	.1	8	15	1722	2.38	2	5	ND	1	33	1	2	2	46	.30	.024	3	10	.70	97	.09	11	1.56	.04	.06	1	5
L4+00S 1+50E	1	24	9	154	.1	6	11	1545	1.43	2	7	ND	2	37	1	2	2	40	.23	.059	4	8	.89	118	.09	9	1.65	.04	.06	1	1
L4+00S 1+75E	1	40	5	239	.1	12	15	1324	2.25	2	5	ND	2	40	1	2	2	39	.42	.051	3	12	.89	98	.12	7	1.61	.01	.12	1	1
L4+00S 2+00E	1	43	13	185	.1	11	12	365	3.29	2	5	ND	1	45	1	2	2	53	.23	.079	5	14	.95	133	.21	5	1.91	.02	.09	1	1
L4+00S 2+25E	21	405	14	101	.1	10	15	426	7.54	8	5	ND	1	33	1	2	4	64	.23	.038	12	12	1.05	70	.19	10	3.35	.05	.09	1	1
L4+00S 2+50E	1	73	5	252	.1	11	27	785	2.01	5	5	ND	1	30	1	2	2	43	.27	.015	5	10	.54	57	.11	11	1.96	.04	.05	1	1
L4+00S 2+75E	1	26	7	74	.1	4	7	993	1.69	2	5	ND	1	30	1	2	2	36	.20	.036	3	7	.44	91	.07	14	.97	.02	.05	1	3
L4+00S 3+00E	1	59	6	376	.1	13	16	1068	2.92	2	5	ND	1	32	1	2	5	51	.29	.035	3	14	1.30	97	.12	8	2.19	.02	.06	1	1
L4+00S 3+25E	2	35	10	102	.1	5	5	460	3.57	2	5	ND	1	20	1	2	3	59	.21	.060	3	11	.56	62	.15	8	1.43	.01	.08	1	1
L4+00S 3+50E	3	267	8	83	.3	11	12	418	2.83	4	5	ND	1	24	1	2	2	37	.24	.107	19	14	.54	78	.09	2	5.06	.03	.05	1	4
L4+00S 3+75E	21	342	21	92	.8	4	41	587	13.95	30	10	ND	1	10	1	2	13	30	.05	.125	13	4	.16	25	.05	8	7.65	.05	.02	1	1
L4+00S 4+00E	27	705	12	73	1.3	5	454	5823	5.76	118	6	ND	1	20	1	2	5	17	.50	.165	45	2	.13	33	.02	9	10.75	.04	.03	1	1
L5+00S 5+50W	10	109	11	133	.2	13	70	1533	2.56	7	5	ND	1	66	1	2	2	55	.71	.039	14	16	.84	121	.10	6	2.91	.02	.09	1	1
L5+00S 5+25W	19	153	14	172	.3	20	82	4487	3.91	2	7	ND	2	66	2	2	3	71	.52	.020	13	24	1.25	224	.11	5	4.26	.03	.15	1	1
L5+00S 5+00W	8	112	10	100	.2	11	190	1934	2.56	2	5	ND	1	38	1	2	2	50	.33	.043	11	14	.75	77	.09	6	2.95	.04	.08	1	1
L5+00S 4+75W	1	21	5	79	.2	6	9	416	1.68	2	5	ND	2	23	1	2	2	35	.20	.062	3	11	.41	61	.07	6	1.25	.01	.04	1	3
L5+00S 4+50W	1	45	6	152	.1	12	11	464	2.44	2	5	ND	2	42	1	3	2	47	.35	.040	4	15	1.19	116	.10	7	2.50	.02	.07	1	6
L5+00S 4+25W	1	26	6	102	.1	7	10	324	2.17	2	5	ND	1	38	1	2	2	42	.28	.028	3	10	.78	100	.11	10	1.45	.01	.05	1	2
L5+00S 4+00W	1	30	2	66	.1	8	8	451	2.05	2	5	ND	2	45	1	2	2	40	.39	.046	3	11	.87	91	.08	12	2.01	.03	.07	1	1
L5+00S 3+75W	1	54	8	143	.1	11	13	625	2.43	2	5	ND	1	48	1	2	2	46	.42	.044	3	14	1.11	124	.09	13	2.40	.04	.07	1	1
L5+00S 3+50W	1	60	5	172	.1	11	15	2380	2.28	2	5	ND	1	38	1	2	3	43	.30	.042	4	12	.85	195	.06	15	2.10	.02	.08	1	6
L5+00S 3+25W	1	36	7	164	.1	11	14	593	2.52	2	5	ND	1	38	1	2	2	48	.33	.026	3	12	.97	78	.11	5	1.91	.02	.05	1	3
L5+00S 3+00W	1	33	6	218	.1	11	27	805	2.13	2	5	ND	1	33	1	2	2	43	.31	.022	3	12	.67	74	.10	7	1.56	.01	.06	1	3
L5+00S 2+75W	5	143	6	185	.1	13	34	824	2.53	2	6	ND	2	25	1	2	2	43	.22	.048	13	10	.48	51	.09	9	3.04	.02	.06	1	1
L5+00S 2+50W	1	14	5	114	.1	5	11	1237	1.59	2	5	ND	1	28	1	2	2	32	.29	.025	3	7	.38	93	.09	10	.89	.01	.06	1	1
L5+00S 2+25W	1	44	12	177	.1	12	12	2071	2.18	2	5	ND	2	42	1	2	2	44	.31	.100	4	17	1.30	177	.09	6	1.30	.02	.08	2	1
L5+00S 2+00W	1	11	7	76	.1	7	6	359	1.85	2	5	ND	1	29	1	2	2	32	.23	.023	4	11	.47	62	.06	3	1.02	.01	.07	2	1
L5+00S 1+75W	1	16	4	63	.1	7	7	331	1.89	2	5	ND	1	28	1	2	2	40	.26	.027	3	10	.83	71	.11	8	1.49	.01	.04	1	3
L5+00S 1+50W	1	10	6	100	.1	5	10	515	1.64	2	5	ND	2	33	1	2	2	29	.29	.102	2	7	.49	122	.07	16	1.39	.02	.06	1	1
L5+00S 1+25W	1	11	3	115	.1	11	14	577	2.56	2	5	ND	2	25	1	2	2	48	.21	.022	3	13	.74	103	.13	2	1.46	.01	.06	1	2
STD C/AU-S	19	63	39	131	7.3	71	31	1049	3.94	42	22	9	39	50	19	17	24	59	.48	.086	42	61	.97	180	.07	34	1.77	.08	.13	14	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+00S 1+00W	1	45	12	190	.1	5	13	617	2.86	2	5	ND	1	45	1	2	2	31	.39	.042	3	12	1.07	95	.15	4	1.86	.01	.06	2	1
L5+00S 0+75W	1	11	12	59	.1	6	6	425	2.38	2	5	ND	1	36	1	2	2	49	.28	.022	3	9	.63	82	.14	2	1.46	.03	.04	1	1
L5+00S 0+50W	1	18	13	165	.3	10	14	697	2.81	2	5	ND	2	49	1	2	2	53	.38	.016	5	14	.91	141	.15	3	2.16	.01	.06	1	2
L5+00S 0+25W	1	22	15	102	.1	7	8	631	2.37	2	5	ND	1	45	1	2	2	48	.31	.021	3	8	.65	77	.15	8	1.70	.01	.03	1	1
L5+00S 0+00W	2	54	21	114	.3	8	12	1327	2.71	2	5	ND	3	52	1	2	2	44	.35	.059	7	10	.87	132	.11	2	2.03	.01	.07	1	1
L5+00S 0+25E	1	41	19	125	.1	8	24	553	2.38	2	5	ND	1	27	1	2	2	43	.24	.064	5	11	.55	103	.12	4	1.71	.02	.05	1	1
L5+00S 0+50E	1	37	6	55	.1	6	9	512	2.64	2	5	ND	1	36	1	2	2	44	.31	.026	3	6	1.07	74	.14	2	1.78	.01	.10	1	4
L5+00S 0+75E	1	11	8	32	.1	5	5	1468	1.90	2	5	ND	1	35	1	2	2	33	.40	.030	2	6	.61	90	.12	2	1.04	.02	.08	1	5
L5+00S 1+00E	1	15	15	163	.1	7	12	811	2.35	2	5	ND	1	37	1	2	2	45	.31	.038	4	9	.62	191	.12	2	1.61	.01	.04	2	1
L5+00S 1+25E	1	23	15	119	.1	3	8	726	2.42	2	5	ND	1	43	1	2	2	63	.30	.072	4	14	.88	172	.16	2	1.98	.01	.07	1	1
L5+00S 1+50E	2	136	17	170	.3	16	14	1263	4.19	7	5	ND	3	41	1	2	2	60	.30	.119	8	19	1.41	143	.16	2	4.76	.02	.11	1	13
L5+00S 1+75E	1	35	13	199	.1	12	15	1247	3.11	2	5	ND	1	29	1	2	2	51	.27	.084	3	17	.76	71	.15	5	2.48	.02	.07	2	1
L5+00S 2+00E	1	45	11	182	.1	10	14	1640	3.74	2	5	ND	1	33	1	2	2	46	.28	.025	4	13	.80	84	.16	7	1.97	.02	.05	1	6
L5+00S 2+25E	1	75	17	209	.7	15	15	705	4.84	3	5	ND	1	31	1	2	2	61	.25	.056	5	16	.55	97	.16	2	3.12	.01	.10	2	2
L5+00S 2+50E	2	57	21	199	.2	12	11	1614	4.47	2	5	ND	1	37	1	2	2	62	.26	.093	5	16	.89	167	.15	2	3.14	.01	.07	1	1
L5+00S 2+75E	1	24	11	176	.2	8	11	1009	3.89	2	5	ND	1	37	1	2	3	76	.37	.044	2	15	1.75	78	.23	2	2.70	.01	.11	1	3
L5+00S 3+00E	1	30	29	136	.3	6	5	454	3.93	2	5	ND	1	34	1	3	2	53	.20	.081	6	9	.67	103	.13	2	3.50	.01	.07	1	1
L5+00S 3+25E	3	31	27	125	.4	7	5	526	4.64	4	5	ND	3	37	1	4	2	58	.18	.092	6	12	.85	85	.17	5	3.64	.01	.08	1	22
L5+00S 3+50E	2	29	23	100	.4	6	4	527	3.98	5	5	ND	2	36	1	3	2	49	.17	.107	8	12	.65	75	.14	5	3.13	.01	.06	1	2
L5+00S 3+75E	2	27	25	94	.5	10	6	499	3.42	2	5	ND	1	52	1	2	2	54	.21	.091	8	19	1.14	113	.16	5	2.29	.03	.09	1	7
L5+00S 4+00E	1	17	25	109	.2	5	5	921	3.06	2	5	ND	1	39	1	2	2	39	.25	.075	5	7	.62	90	.13	4	1.59	.01	.07	1	2
STD C/AU-S	19	63	39	132	7.4	71	31	1053	3.96	40	17	7	39	53	19	18	23	59	.48	.086	42	61	.96	181	.07	32	1.82	.06	.14	14	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
U 0151	23	33	9	11	.9	4	4	64	3.29	3	5	ND	1	24	1	2	3	3	.04	.018	2	2	.10	37	.01	6	.29	.01	.15	1	146
U 0152	10	135	12	52	.1	2	8	309	5.56	9	5	ND	1	7	1	2	2	15	.05	.031	4	2	.87	36	.05	7	1.01	.02	.12	1	5
U 0153	5	34	5	54	.1	17	9	627	3.78	3	5	ND	2	24	1	2	2	36	.97	.044	3	25	2.04	23	.09	3	1.95	.02	.12	1	1
U 0154	3	51	3	55	.1	1	7	216	6.13	20	5	ND	1	11	1	2	2	14	.10	.139	5	1	.92	18	.01	2	1.20	.01	.14	1	11
U 0155	9	98	30	95	.7	3	4	924	4.03	3	5	ND	1	54	1	2	2	61	.29	.072	6	15	1.39	71	.27	4	1.35	.03	.26	1	6
U 0156	2	13	6	16	.2	5	8	111	3.70	23	5	ND	3	2	1	2	2	13	.05	.021	2	3	.37	54	.17	2	.50	.01	.16	1	2
U 0157	11	391	17	60	.1	5	9	270	10.75	11	5	ND	2	9	1	2	2	20	.15	.057	6	2	.82	34	.06	2	1.37	.02	.12	1	11
U 0158	8	31	5	23	.2	4	7	191	3.75	9	5	ND	3	4	1	2	2	10	.11	.079	2	1	.73	37	.03	2	.91	.01	.17	1	22
U 0159	11	33	6	71	.1	2	7	569	3.53	8	5	ND	2	8	1	2	2	29	.21	.078	4	4	1.59	38	.05	2	1.65	.02	.11	1	17
U 0160	3	15	5	12	.2	2	2	124	1.73	2	5	ND	1	5	1	2	3	5	.01	.020	2	1	.33	24	.05	5	.50	.01	.13	1	6
U 0161	1	8	11	4	.2	3	1	44	.95	5	5	ND	1	15	1	2	2	3	.01	.021	3	2	.14	31	.01	10	.35	.01	.17	1	1
U 0162	3	6	15	5	.2	2	1	37	1.80	3	5	ND	3	14	1	3	2	2	.01	.011	2	1	.10	33	.01	3	.30	.01	.15	1	1

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: MAY 16 1988 DATE REPORT MAILED: May 20/88 ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

HAROLD M. JONES File # 88-1462 Page 1 PROJECT WHISTLER

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L15+00N 0+00W	1	51	23	210	.2	6	12	1445	3.06	4	5	ND	1	31	1	2	7	47	.30	.111	3	8	1.04	209	.13	3	2.62	.01	.12	1	1
L15+00N 0+25E	1	52	13	144	.1	8	13	602	3.46	6	5	ND	1	28	1	2	2	54	.27	.074	3	6	1.21	120	.15	2	2.76	.01	.10	2	11
L15+00N 0+50E	1	44	22	133	.4	8	13	931	3.44	2	5	ND	1	25	1	2	2	54	.24	.066	3	8	1.14	135	.15	2	2.65	.01	.09	1	1
L15+00N 0+75E	1	51	13	124	.1	7	10	1100	3.43	10	5	ND	1	24	1	3	2	49	.25	.162	3	6	1.22	161	.13	3	2.80	.01	.08	2	1
L15+00N 1+00E	2	92	21	174	.1	5	14	827	3.48	5	5	ND	1	30	1	2	2	53	.27	.076	3	9	1.21	141	.15	2	2.81	.01	.13	1	2
L15+00N 1+25E	4	235	28	643	.2	8	36	838	4.28	2	5	ND	1	25	1	3	2	58	.22	.026	4	8	1.31	118	.17	8	3.48	.01	.13	1	2
L15+00N 1+50E	1	64	25	212	.1	8	12	1170	3.68	2	5	ND	1	30	1	2	2	58	.31	.088	3	8	1.18	203	.16	2	2.73	.01	.11	1	1
L15+00N 1+75E	1	58	22	179	.1	5	14	1191	3.60	2	5	ND	1	23	1	2	4	55	.21	.109	3	8	1.05	150	.16	2	2.65	.01	.14	1	2
L15+00N 2+00E	1	41	30	217	.1	5	11	2599	3.30	2	5	ND	1	39	1	3	7	37	.30	.130	5	6	.74	369	.12	2	2.00	.01	.12	1	1
L15+00N 2+25E	3	56	35	588	.3	7	17	1970	3.37	4	5	ND	1	31	1	2	5	37	.20	.133	4	7	.89	231	.13	2	2.11	.01	.11	1	1
L15+00N 2+50E	5	345	60	1922	.4	46	50	1422	4.79	5	5	ND	1	42	3	2	2	41	.40	.070	8	7	1.10	182	.13	2	3.43	.01	.08	1	3
L15+00N 2+75E	4	179	41	1530	.2	31	25	1075	4.13	8	5	ND	1	48	2	2	3	44	.61	.034	4	8	.95	105	.14	2	2.76	.01	.08	1	1
L15+00N 3+00E	4	422	138	704	.1	14	15	700	3.72	4	5	ND	1	44	1	2	2	43	.44	.054	6	6	1.13	132	.16	2	2.62	.01	.12	1	3
L15+00N 3+25E	4	170	88	460	.3	12	41	3120	6.39	18	5	ND	2	36	1	2	2	51	.24	.236	13	7	.84	311	.15	7	2.90	.01	.18	1	1
L15+00N 3+50E	3	161	26	250	.2	18	27	2980	4.69	12	5	ND	1	35	1	2	2	58	.35	.134	7	9	1.11	242	.16	2	3.15	.01	.16	1	1
L15+00N 3+75E	5	318	29	370	.7	12	19	1085	3.48	8	5	ND	1	28	1	2	2	36	.23	.094	30	7	.60	114	.10	2	4.17	.01	.21	1	1
L15+00N 4+00E	1	157	16	192	.4	13	51	3328	4.56	5	5	ND	1	38	1	2	2	54	.37	.233	5	8	1.09	209	.14	7	3.26	.01	.21	1	15
L14+00N 0+00E	1	71	23	191	.3	8	11	1054	3.92	2	5	ND	1	43	1	2	5	65	.24	.098	4	8	1.26	284	.18	2	2.68	.02	.14	1	6
L14+00N 0+25E	2	137	33	346	.1	8	16	1022	3.92	2	5	ND	1	31	1	2	2	62	.28	.026	5	9	1.16	148	.18	2	2.80	.02	.13	1	3
L14+00N 0+50E	1	55	26	175	.1	6	10	924	3.83	3	5	ND	1	37	1	3	2	64	.24	.064	4	9	1.23	239	.18	5	2.61	.01	.12	1	12
L14+00N 0+75E	1	68	38	325	.1	7	15	1543	3.14	5	5	ND	1	28	1	2	8	48	.21	.106	4	8	1.02	250	.15	2	2.45	.01	.08	2	1
L14+00N 1+00E	2	381	64	641	.1	16	59	1001	3.54	3	5	ND	1	25	1	2	2	54	.21	.069	5	8	1.11	156	.15	2	3.04	.01	.10	1	1
L14+00N 1+25E	1	88	12	263	.1	8	18	1171	3.08	4	5	ND	1	30	1	2	8	52	.25	.057	3	8	1.15	163	.15	2	2.61	.02	.14	1	3
L14+00N 1+50E	1	93	18	222	.2	9	19	2395	3.13	2	5	ND	1	28	1	2	5	51	.25	.072	4	9	1.12	179	.16	7	2.73	.01	.16	1	1
L14+00N 1+75E	1	65	17	178	.2	8	17	1898	3.28	2	5	ND	1	29	1	2	2	53	.23	.098	4	7	1.08	206	.14	2	2.71	.01	.14	1	4
L14+00N 2+00E	1	226	12	126	.1	8	22	1084	4.03	3	5	ND	1	37	1	2	2	66	.30	.061	4	9	1.62	282	.18	2	3.73	.01	.41	2	2
L14+00N 2+25E	1	172	21	176	.1	11	22	1472	3.87	2	5	ND	1	34	1	2	2	62	.27	.052	4	9	1.39	199	.17	4	3.28	.01	.21	1	4
L14+00N 2+50E	2	222	23	212	.1	9	33	949	3.75	2	5	ND	1	31	1	2	2	56	.24	.033	4	8	1.25	142	.15	2	3.28	.01	.20	1	1
L14+00N 2+75E	4	37	17	248	.1	6	9	1441	3.41	2	5	ND	1	57	1	2	3	32	.36	.096	6	5	.99	200	.13	2	1.64	.01	.09	1	1
L14+00N 3+00E	4	163	18	275	.2	7	24	1074	3.59	2	5	ND	2	30	1	2	2	38	.14	.045	7	6	1.01	145	.11	2	2.44	.01	.10	1	1
L14+00N 3+25E	1	62	56	343	.1	9	21	1716	4.19	2	5	ND	1	31	1	2	2	47	.23	.106	4	8	.85	196	.15	2	2.48	.01	.12	1	1
L14+00N 3+50E	1	46	15	177	.1	7	14	868	3.35	2	5	ND	1	26	1	2	2	55	.23	.067	3	8	.97	161	.16	6	2.53	.01	.12	1	1
L14+00N 3+75E	1	302	19	279	.3	11	105	2984	3.14	5	5	ND	1	26	1	2	4	51	.24	.041	9	8	.98	181	.14	4	3.45	.01	.17	1	2
L14+00N 4+00E	1	164	19	300	.5	23	36	1517	4.36	5	5	ND	1	45	1	2	5	56	.49	.124	7	12	1.07	271	.13	2	3.82	.01	.13	1	1
L13+00N 0+25E	1	63	14	132	.1	6	14	976	2.98	2	5	ND	1	27	1	4	2	51	.23	.065	3	8	.93	145	.14	2	2.45	.01	.11	2	2
L13+00N 0+50E	1	76	18	130	.2	10	14	722	4.12	2	5	ND	1	31	1	2	2	73	.24	.054	3	9	1.29	169	.18	2	3.20	.01	.16	1	1
STD C/AU-S	20	63	45	132	7.5	72	30	1047	4.16	41	23	8	40	53	20	16	21	58	.46	.089	40	60	.89	186	.08	35	1.94	.07	.16	15	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L13+00N 0+75E	1	22	14	101	.1	6	7	571	2.84	2	5	ND	1	32	1	2	2	58	.32	.050	3	8	1.04	149	.17	2	1.77	.01	.12	1	1
L13+00N 1+00E	1	56	22	135	.1	8	11	1060	3.74	4	5	ND	1	37	1	2	2	73	.32	.096	3	9	1.37	229	.19	8	2.98	.02	.13	1	2
L13+00N 1+25E	1	88	28	238	.1	9	17	1207	3.98	2	5	ND	1	36	1	2	2	74	.27	.074	4	11	1.49	331	.18	11	3.00	.02	.21	1	1
L13+00N 1+50E	4	329	38	312	.1	15	51	1175	5.01	8	5	ND	1	45	1	2	3	66	.39	.036	7	9	1.53	186	.19	2	3.76	.01	.16	1	1
L13+00N 1+75E	4	60	25	168	.1	8	8	666	4.12	3	5	ND	1	45	1	2	2	50	.25	.130	8	9	.82	297	.13	6	2.11	.01	.13	1	4
L13+00N 2+00E	5	73	32	96	.1	7	6	1018	4.50	5	5	ND	1	77	1	3	2	43	.21	.170	9	7	.85	472	.13	4	2.13	.02	.22	2	5
L13+00N 2+25E	1	67	20	95	.1	7	9	2282	3.72	5	5	ND	1	45	1	2	2	70	.28	.059	5	11	1.18	270	.15	3	2.60	.01	.17	1	7
L13+00N 2+50E	1	63	27	125	.1	7	12	779	4.24	3	5	ND	1	36	1	2	2	83	.24	.051	4	11	1.51	214	.19	2	3.11	.01	.18	2	1
L13+00N 2+75E	1	45	22	426	.1	11	19	1282	3.99	3	5	ND	1	33	1	3	3	72	.28	.153	3	9	1.59	230	.19	8	3.18	.01	.16	1	1
L13+00N 3+00E	2	134	25	399	.1	13	28	3499	3.79	3	5	ND	1	41	1	2	2	62	.36	.044	7	9	1.10	260	.18	2	2.94	.02	.15	1	5
L13+00N 3+25E	2	166	25	196	.1	8	24	1348	3.99	2	5	ND	1	43	1	2	2	72	.41	.151	6	9	1.61	268	.27	4	3.39	.02	.24	1	1
L13+00N 3+50E	4	202	37	180	.1	7	18	729	5.07	4	5	ND	2	25	1	2	2	49	.21	.064	7	8	1.16	117	.21	3	2.25	.01	.10	1	1
L13+00N 3+75E	2	463	28	238	.3	13	53	3325	3.95	10	5	ND	1	53	1	2	2	64	.49	.085	11	9	1.25	215	.16	5	3.55	.01	.29	1	4
L13+00N 4+00E	2	574	21	145	.3	16	16	1207	3.47	7	5	ND	1	45	1	2	2	61	.36	.114	12	7	.88	140	.12	2	2.39	.01	.14	1	6
L12+00N 0+25E	6	311	46	328	.1	18	24	987	5.61	14	5	ND	1	34	1	2	2	58	.28	.063	12	7	1.09	131	.14	2	3.07	.01	.12	1	1
L12+00N 0+50E	1	113	19	448	.1	9	18	1119	3.19	4	5	ND	1	46	1	2	2	58	.29	.063	6	8	1.20	244	.14	2	2.50	.01	.12	1	1
L12+00N 0+75E	1	155	17	219	.1	6	12	1089	3.07	4	5	ND	1	33	1	2	2	70	.24	.036	6	8	1.72	226	.19	9	3.34	.01	.41	1	1
L12+00N 1+00E	3	268	21	166	.2	16	47	2169	5.10	6	5	ND	1	39	1	2	2	57	.26	.106	8	10	1.04	212	.14	14	2.78	.01	.16	1	1
L12+00N 1+25E	2	267	28	190	.2	15	28	1159	4.25	6	5	ND	1	32	1	2	3	76	.26	.028	8	14	1.57	178	.19	2	3.17	.02	.17	1	1
L12+00N 1+50E	3	471	36	150	.1	9	55	1548	3.81	3	5	ND	1	33	1	2	2	65	.25	.039	11	9	1.14	221	.16	2	3.49	.02	.25	2	1
L12+00N 1+75E	2	247	30	269	.2	10	27	1356	3.98	7	5	ND	1	63	1	2	2	67	.28	.110	9	8	1.31	301	.15	7	3.26	.01	.25	1	1
L12+00N 2+00E	2	404	31	208	.1	12	74	2454	3.57	5	5	ND	1	32	1	3	2	61	.26	.109	9	9	1.08	210	.15	4	3.33	.01	.12	1	2
L12+00N 2+25E	1	47	12	156	.1	3	13	707	3.22	3	5	ND	1	27	1	2	2	64	.22	.076	3	10	1.00	349	.16	4	2.38	.01	.07	2	1
L12+00N 2+50E	1	67	17	109	.1	4	8	1298	3.23	3	5	ND	1	32	1	3	4	64	.19	.126	4	9	.98	179	.14	3	2.50	.01	.10	1	1
L12+00N 2+75E	1	103	16	92	.1	5	10	687	3.64	3	5	ND	1	49	1	2	2	70	.26	.083	5	10	1.08	216	.14	2	3.01	.01	.17	1	1
L12+00N 3+00E	1	75	17	163	.1	7	10	761	3.34	3	5	ND	2	26	1	4	2	65	.20	.079	4	9	1.11	142	.15	2	2.66	.01	.14	1	3
L12+00N 3+25E	2	231	17	141	.1	6	20	770	3.14	3	5	ND	1	32	1	2	2	59	.22	.039	8	7	1.16	129	.14	2	2.84	.01	.17	1	1
L12+00N 3+50E	1	122	29	137	.1	4	12	996	3.46	3	5	ND	1	74	1	2	2	59	.67	.143	5	8	1.13	225	.13	2	2.42	.01	.21	2	1
L12+00N 3+75E	2	162	12	97	.2	8	13	918	2.32	3	5	ND	1	59	1	4	4	33	.70	.056	5	6	.89	106	.07	2	2.08	.01	.13	1	6
L12+00N 4+00E	2	100	20	220	.3	9	13	1039	3.11	8	5	ND	1	51	1	3	2	58	.60	.056	4	12	1.32	153	.13	2	2.38	.01	.16	1	3
L11+00N 0+25E	1	23	16	148	.1	6	5	591	2.74	5	5	ND	2	23	1	2	5	54	.17	.128	3	7	.75	232	.16	2	1.88	.01	.07	1	1
L11+00N 0+50E	3	437	15	132	.2	13	48	1462	3.97	6	5	ND	1	41	1	2	2	60	.32	.060	11	7	1.15	162	.15	2	3.21	.01	.21	1	4
L11+00N 0+75E	5	238	23	122	.1	7	42	1250	3.73	6	5	ND	1	47	1	2	2	49	.40	.052	9	8	1.03	122	.11	3	2.48	.01	.16	1	1
L11+00N 1+00E	3	304	19	163	.1	9	37	2872	3.61	4	5	ND	1	51	1	2	5	63	.39	.042	10	7	1.18	171	.16	2	3.16	.01	.20	1	1
L11+00N 1+25E	2	331	22	121	.3	9	34	1731	3.16	2	5	ND	1	36	1	2	2	56	.26	.048	10	7	1.08	161	.13	4	2.79	.01	.16	2	5
L11+00N 1+50E	1	79	13	156	.1	8	14	1117	3.40	2	5	ND	1	56	1	3	2	63	.39	.161	4	10	1.16	218	.14	2	2.67	.01	.21	1	1
STD C/AU-S	20	63	41	132	7.5	73	30	1041	4.01	43	20	8	40	53	19	19	22	60	.46	.087	40	59	.95	185	.08	39	1.91	.07	.15	14	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L11+00N 1+50E	1	35	17	219	.1	5	11	1651	2.48	3	5	ND	1	36	1	2	2	50	.32	.082	3	8	.92	248	.14	12	1.85	.01	.12	1	1
L11+00N 1+75E	1	50	15	103	.3	6	8	624	2.69	3	5	ND	1	31	1	2	2	56	.19	.093	3	7	.98	147	.12	3	2.06	.01	.11	1	10
L11+00N 2+00E	1	48	8	126	.1	7	10	1436	2.35	2	5	ND	1	34	1	2	2	49	.30	.069	3	6	.98	194	.13	7	1.93	.01	.09	1	1
L11+00N 2+50E	1	70	9	136	.1	4	11	947	2.86	2	5	ND	1	31	1	2	2	58	.28	.119	3	8	1.18	210	.13	2	2.34	.01	.15	1	1
L11+00N 2+75E	3	525	16	149	.1	26	99	4183	2.76	7	5	ND	1	42	1	2	2	40	.39	.076	7	8	.89	163	.08	8	2.20	.01	.14	1	1
L11+00N 3+00E	1	150	15	134	.1	12	14	1115	3.19	2	5	ND	1	43	1	2	2	67	.32	.036	4	8	1.28	188	.15	5	2.47	.01	.16	1	2
L11+00N 3+25E	1	68	13	140	.1	7	9	1062	2.85	2	5	ND	1	39	1	2	3	58	.37	.178	3	6	1.05	223	.12	3	2.26	.01	.16	1	1
L11+00N 3+50E	1	51	13	183	.1	6	10	689	3.09	3	5	ND	1	39	1	2	2	60	.30	.263	3	9	1.03	190	.13	8	2.30	.01	.15	1	1
L11+00N 3+75E	1	55	13	198	.1	4	9	1059	2.55	2	5	ND	1	56	1	2	2	54	.47	.150	3	6	1.17	267	.13	13	2.13	.02	.22	1	1
L11+00N 4+00E	1	50	10	228	.1	6	15	2859	2.63	3	5	ND	1	60	1	3	2	44	.59	.184	3	8	.65	413	.13	2	1.80	.01	.17	1	1
L9+00N 6+00E	6	257	30	135	.9	7	28	939	5.85	16	5	ND	2	19	1	2	2	39	.18	.113	10	9	.67	97	.08	3	2.07	.01	.09	1	13
STD C/AU-S	20	57	38	133	7.1	69	28	1056	3.72	44	24	9	41	52	17	17	20	63	.46	.092	38	60	.88	197	.08	31	1.75	.07	.13	13	51

Correlation Coefficients of all Soil Samples

	MOPPM	CUPPM	PBPPM	ZNPPM	AGPPM	NIPPM	COPPM	MNPPM	FEPCT	ASPPM	UPPM	AUPPM	THPPM	SRPPM	CDPPM	SBPPM	BIPPM	VPPM	CAPCT	PPCT	LAPPM	CRPPM	MGPCT	BAPPM	TIPCT	BPPM	ALPCT	NAPCT	KPCT	WPPM	AUPPB
MOPPM	1.00	0.51	0.10	0.10	0.32	0.15	0.62	0.37	0.25	0.45	0.23	0.15	0.33	0.01	0.27	-0.02	0.06	-0.29	0.02	0.18	0.55	-0.12	-0.32	-0.22	-0.44	0.10	0.53	0.10	-0.11	0.08	-0.02
CUPPM	0.51	1.00	0.14	0.15	0.42	0.18	0.57	0.35	0.60	0.20	0.10	0.15	0.50	-0.10	0.33	-0.04	0.02	-0.44	-0.03	0.31	0.75	-0.15	-0.33	-0.24	-0.49	0.05	0.58	-0.00	-0.04	-0.00	-0.03
PBPPM	0.10	0.14	1.00	0.19	0.19	-0.02	0.01	0.06	0.14	0.05	-0.04	0.00	0.01	-0.04	0.01	-0.02	0.01	-0.20	-0.01	0.16	0.12	-0.10	0.03	0.02	-0.14	-0.05	-0.02	-0.11	0.04	0.00	0.06
ZNPPM	0.10	0.15	0.19	1.00	0.09	0.60	0.25	0.51	0.06	0.16	0.02	0.08	0.18	0.10	0.51	0.00	-0.00	-0.13	0.22	0.09	0.19	0.02	0.18	0.19	-0.00	-0.09	0.15	-0.06	0.12	-0.01	0.01
AGPPM	0.32	0.42	0.19	0.09	1.00	0.08	0.30	0.14	0.12	0.21	0.19	0.08	0.21	-0.07	0.12	-0.04	0.02	-0.23	0.01	0.20	0.41	-0.10	-0.17	-0.13	-0.27	0.05	0.33	0.03	-0.03	0.01	0.09
NIPPM	0.15	0.18	-0.02	0.60	0.08	1.00	0.37	0.45	-0.11	0.11	0.06	0.01	0.13	0.30	0.43	0.02	-0.10	0.14	0.35	-0.01	0.22	0.45	0.24	0.18	0.10	-0.01	0.37	0.13	0.04	0.01	-0.03
COPPM	0.62	0.57	0.01	0.25	0.30	0.37	1.00	0.73	0.22	0.36	0.24	0.17	0.44	-0.02	0.50	-0.03	-0.01	-0.38	0.11	0.12	0.57	-0.06	-0.31	-0.17	-0.41	0.13	0.63	0.08	-0.10	-0.03	-0.04
MNPPM	0.37	0.35	0.06	0.51	0.14	0.45	0.73	1.00	0.17	0.31	0.15	0.22	0.40	0.08	0.70	-0.00	0.01	-0.32	0.21	0.18	0.41	-0.04	-0.11	0.12	-0.27	0.01	0.38	0.01	0.05	-0.08	-0.01
FEPCT	0.25	0.60	0.14	0.06	0.12	-0.11	0.22	0.17	1.00	0.13	0.04	0.08	0.38	-0.20	0.19	-0.04	0.21	-0.37	-0.21	0.25	0.38	-0.27	-0.41	-0.24	-0.39	0.05	0.13	-0.06	-0.09	-0.04	-0.02
ASPPM	0.45	0.20	0.05	0.16	0.21	0.11	0.36	0.31	0.13	1.00	0.18	0.17	0.23	-0.07	0.23	-0.03	0.11	-0.20	-0.00	0.16	0.27	-0.12	-0.15	-0.08	-0.22	0.02	0.33	0.06	-0.03	-0.00	-0.02
UPPM	0.23	0.10	-0.04	0.02	0.19	0.06	0.24	0.15	0.04	0.18	1.00	0.09	0.20	-0.05	0.16	-0.02	0.08	-0.11	-0.04	0.05	0.15	-0.07	-0.11	-0.06	-0.15	0.04	0.21	0.13	-0.03	-0.03	-0.01
AUPPM	0.15	0.15	0.00	0.08	0.08	0.01	0.17	0.22	0.08	0.17	0.09	1.00	0.27	-0.01	0.24	0.00	0.02	-0.17	-0.02	0.15	0.22	-0.12	-0.13	0.01	-0.17	0.01	0.16	-0.04	0.00	0.05	-0.02
THPPM	0.33	0.50	0.01	0.18	0.21	0.13	0.44	0.40	0.38	0.23	0.20	0.27	1.00	-0.13	0.67	0.01	0.06	-0.36	-0.13	0.25	0.62	0.02	-0.33	-0.20	-0.35	0.01	0.52	-0.08	-0.08	-0.03	-0.01
SRPPM	0.01	-0.10	-0.04	0.10	-0.07	0.30	-0.02	0.08	-0.20	-0.07	-0.05	-0.01	-0.13	1.00	0.00	0.04	-0.07	0.27	0.64	0.04	0.03	0.30	0.33	0.59	0.12	0.09	-0.03	0.31	0.43	0.03	0.07
CDPPM	0.27	0.33	0.01	0.51	0.12	0.43	0.50	0.70	0.19	0.23	0.16	0.24	0.67	0.00	1.00	-0.03	0.01	-0.27	0.04	0.14	0.51	0.01	-0.20	-0.06	-0.27	-0.00	0.38	-0.03	-0.02	-0.03	-0.02
SBPPM	-0.02	-0.04	-0.02	0.00	-0.04	0.02	-0.03	-0.00	-0.04	-0.03	-0.02	0.00	0.01	0.04	-0.03	1.00	-0.01	0.05	-0.00	0.06	-0.06	0.13	0.12	0.07	0.09	-0.03	0.06	0.03	0.08	0.02	0.01
BIPPM	0.06	0.02	0.01	-0.00	0.02	-0.10	-0.01	0.01	0.21	0.11	0.08	0.02	0.06	-0.07	0.01	-0.01	1.00	-0.12	-0.09	0.07	0.03	-0.11	-0.10	-0.02	-0.08	0.05	0.03	-0.01	-0.03	-0.06	0.00
VPPM	-0.29	-0.44	-0.20	-0.13	-0.23	0.14	-0.38	-0.32	-0.37	-0.20	-0.11	-0.17	-0.36	0.27	-0.27	0.05	-0.12	1.00	0.09	-0.16	-0.45	0.43	0.55	0.32	0.74	-0.09	-0.20	0.17	0.17	0.04	-0.01
CAPCT	0.02	-0.03	-0.01	0.22	0.01	0.35	0.11	0.21	-0.21	-0.00	-0.04	-0.02	-0.13	0.64	0.04	-0.00	-0.09	0.09	1.00	-0.03	0.06	0.21	0.28	0.25	0.02	0.09	-0.00	0.39	0.33	0.02	0.05
PPCT	0.18	0.31	0.16	0.09	0.20	-0.01	0.12	0.18	0.25	0.16	0.05	0.15	0.25	0.04	0.14	0.06	0.07	-0.16	-0.03	1.00	0.28	-0.06	-0.12	0.20	-0.24	-0.03	0.23	-0.04	0.10	-0.01	0.04
LAPPM	0.55	0.75	0.12	0.19	0.41	0.22	0.57	0.41	0.38	0.27	0.15	0.22	0.62	0.03	0.51	-0.06	0.03	-0.45	0.06	0.28	1.00	-0.11	-0.38	-0.19	-0.50	0.09	0.57	0.01	-0.08	-0.01	-0.02
CRPPM	-0.12	-0.15	-0.10	0.02	-0.10	0.45	-0.06	-0.04	-0.27	-0.12	-0.07	-0.12	0.02	0.30	0.01	0.13	-0.11	0.43	0.21	-0.06	-0.11	1.00	0.35	0.12	0.36	-0.01	0.11	0.15	0.03	0.01	-0.03
MGPCT	-0.32	-0.33	0.03	0.18	-0.17	0.24	-0.31	-0.11	-0.41	-0.15	-0.11	-0.13	-0.33	0.33	-0.20	0.12	-0.10	0.55	0.28	-0.12	-0.38	0.35	1.00	0.51	0.63	-0.21	-0.13	0.03	0.44	-0.05	0.07
BAPPM	-0.22	-0.24	0.02	0.19	-0.13	0.18	-0.17	0.12	-0.24	-0.08	-0.06	0.01	-0.20	0.59	-0.06	0.07	-0.02	0.32	0.25	0.20	-0.19	0.12	0.51	1.00	0.33	-0.09	-0.10	0.01	0.48	-0.02	0.04
TIPCT	-0.44	-0.49	-0.14	-0.00	-0.27	0.10	-0.41	-0.27	-0.39	-0.22	-0.15	-0.17	-0.35	0.12	-0.27	0.09	-0.08	0.74	0.02	-0.24	-0.50	0.36	0.63	0.33	1.00	-0.18	-0.22	-0.02	0.14	-0.03	-0.01
BPPM	0.10	0.05	-0.05	-0.09	0.05	-0.01	0.13	0.01	0.05	0.02	0.04	0.01	0.01	0.09	-0.00	-0.03	0.05	-0.09	0.09	-0.03	0.09	-0.01	-0.21	-0.09	-0.18	1.00	0.04	0.19	-0.05	0.03	0.03
ALPCT	0.53	0.58	-0.02	0.15	0.33	0.37	0.63	0.38	0.13	0.33	0.21	0.16	0.52	-0.03	0.38	0.06	0.03	-0.20	-0.00	0.23	0.57	0.11	-0.13	-0.10	-0.22	0.04	1.00	0.06	-0.01	0.05	-0.04
NAPCT	0.10	-0.00	-0.11	-0.06	0.03	0.13	0.08	0.01	-0.06	0.06	0.13	-0.04	-0.08	0.31	-0.03	0.03	-0.01	0.17	0.39	-0.04	0.01	0.15	0.03	0.01	-0.02	0.19	0.06	1.00	0.26	0.07	0.02
KPCT	-0.11	-0.04	0.04	0.12	-0.03	0.04	-0.10	0.05	-0.09	-0.03	-0.03	0.00	-0.08	0.43	-0.02	0.08	-0.03	0.17	0.33	0.10	-0.08	0.03	0.44	0.48	0.14	-0.05	-0.01	0.26	1.00	-0.01	0.08
WPPM	0.08	-0.00	0.00	-0.01	0.01	0.01	-0.03	-0.08	-0.04	-0.00	-0.03	0.05	-0.03	0.03	-0.03	0.02	-0.06	0.04	0.02	-0.01	-0.01	0.01	-0.05	-0.02	-0.03	0.03	0.05	0.07	-0.01	1.00	0.02
AUPPB	-0.02	-0.03	0.06	0.01	0.09	-0.03	-0.04	-0.01	-0.02	-0.02	-0.01	-0.02	-0.01	0.07	-0.02	0.01	0.00	-0.01	0.05	0.04	-0.02	-0.03	0.07	0.04	-0.01	0.03	-0.04	0.02	0.08	0.02	1.00

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: OCT 12 1988
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: Oct. 19/88..

GEOCHEMICAL ANALYSIS CERTIFICATE

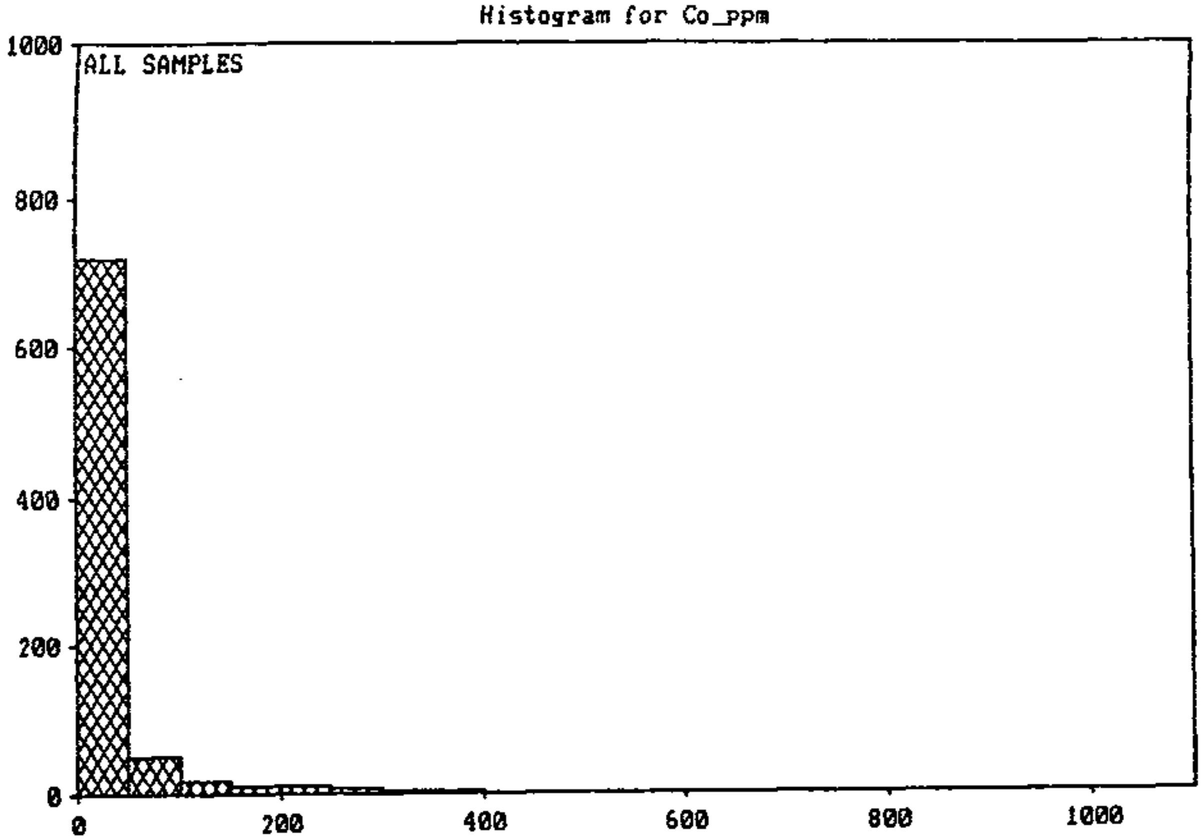
ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Pulp AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

SIGNED BY Bernard Chan .... D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

HAROLD M. JONES & ASSOC. INC. FILE # 88-4881R Page 1

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Cr PPM	Au* PPB
L3+50N 6+00W	43	7	244	.4	13	1
L3+50N 5+75W	161	17	467	.4	13	1
L3+50N 5+50W	152	13	429	.3	16	2
L3+50N 5+25W	233	23	284	.3	21	2
L3+50N 5+00W	128	10	982	.3	13	1
L3+50N 4+75W	155	11	816	.4	15	1
L3+50N 4+50W	113	8	181	1.2	14	3
L3+50N 4+25W	169	13	588	.3	14	1
L3+50N 4+00W	160	13	250	.4	14	1
L3+50N 4+00W B	109	14	804	.4	12	1
L3+50N 3+75W	76	19	666	.4	14	2
L3+50N 3+50W	195	7	949	.4	9	1
L3+50N 3+25W	416	15	309	.2	12	1
L3+50N 3+00W	210	14	678	.4	10	1
L3+00N 3+00W	90	32	564	.4	9	2
L2+50N 6+00W	490	16	1002	.2	9	3
L2+50N 5+75W	144	17	238	.3	16	1
L2+50N 5+50W	227	12	638	.4	13	18
L2+50N 5+25W	125	7	819	.2	10	1
L2+50N 5+00W	138	16	717	.5	7	1
L2+50N 4+75W	335	5	158	2.4	8	1
L2+50N 4+50W	939	13	1699	2.3	12	1
L2+50N 4+25W	979	30	619	.6	9	2
L2+50N 4+00W	141	12	1079	.5	13	1
L2+50N 3+75W	404	30	383	.7	13	2
L2+50N 3+50W	89	17	473	.3	15	1
L2+50N 3+25W	80	21	188	.3	16	1
L2+50N 3+00W	110	24	687	.3	9	1
L2+50N 3+00W B	102	15	171	.3	11	1
L2+50N 2+75W	38	21	539	.1	11	2
L2+50N 2+50W	187	14	531	.1	8	1
L2+50N 2+25W	119	14	261	.1	11	1
L2+50N 2+00W	558	10	140	.1	1	2
L2+50N 1+75W	448	19	338	.2	2	1
L2+50N 1+50W	240	24	369	.3	6	2
L2+50N 1+25W	100	58	244	.1	17	1
STD C/AU-S	61	39	132	7.1	57	49

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Cr PPM	Au* PPB
L1+50N 5+00W	195	22	414	.5	12	2
L1+50N 4+75W	183	18	480	.7	11	1
L1+50N 4+50W	294	24	540	.8	10	2
L1+50N 4+25W	296	27	560	.5	8	1
L1+50N 4+00W	297	33	589	.8	9	1
L1+50N 3+75W	167	23	228	.7	10	1
L1+50N 3+50W	668	29	270	.4	1	1
L1+50N 3+00W	258	23	114	.3	6	4
L1+50N 2+75W	451	34	120	.5	3	2
L1+50N 2+50W	119	23	128	.3	10	2
L1+50N 2+25W	423	26	108	.3	2	1
L1+50N 2+00W	677	29	169	.2	2	1
L1+50N 1+75W	430	28	210	.3	3	1
L1+50N 1+50W	1088	7	194	1.5	7	2
L1+50N 1+25W	1264	20	538	.5	2	1
L1+50N 1+00W	2348	43	349	1.9	11	5
L1+50N 0+75W	56	36	135	.3	9	3
L1+50N 0+50W	35	39	184	.4	10	1
L1+50N 0+25W	198	29	667	.3	11	4
L1+50N 0+00W	34	10	280	.4	12	8
L1+00N 1+25W	348	27	188	.3	9	21
L1+00N 0+25W	80	16	55	.1	9	7
L0+50N 5+25W	1015	27	441	.4	4	10
L0+50N 5+00W	578	16	306	.1	13	1
L0+50N 4+75W	109	7	551	.2	10	5
L0+50N 4+50W	570	22	341	.3	10	4
L0+50N 4+25W	1473	19	320	.5	11	5
L0+50N 4+00W	165	13	227	.3	10	6
L0+50N 3+75W	687	17	258	.4	15	7
L0+50N 3+50W	804	20	207	.2	8	1
L0+50N 3+25W	822	27	329	.1	6	2
L0+50N 3+00W	370	18	151	.1	13	4
L0+50N 2+75W	347	27	141	.3	11	7
L0+50N 2+50W	132	28	84	.2	12	3
L0+50N 2+25W	295	15	156	.3	14	1
L0+50N 2+00W	205	40	147	.2	14	1
HJ-1	61	45	417	.4	8	2
STD C/AU-S	59	38	132	6.8	56	48



Mean = 29.706 Variance = 3436
Standard Deviation = 58.62 Skewness = 6.215

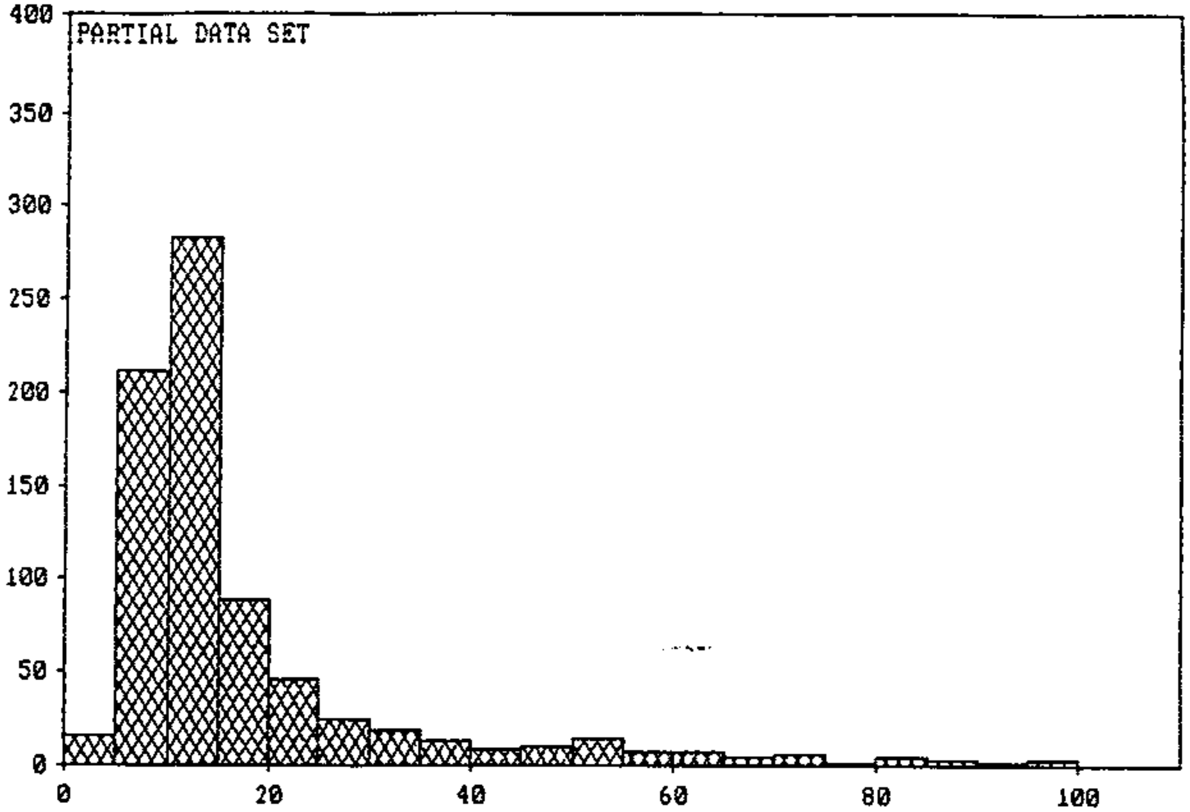
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	50	720	87	720	87	Mean
50	100	51	6	771	94	
100	150	19	2	790	96	
150	200	9	1	799	97	
200	250	10	1	809	98	
250	300	7	1	816	99	
300	350	3	0	819	100	
350	400	2	0	821	100	
400	450	0	0	821	100	
450	500	1	0	822	100	
500	550	0	0	822	100	
550	600	0	0	822	100	
600	650	0	0	822	100	
650	700	0	0	822	100	
700	750	0	0	822	100	
750	800	0	0	822	100	
800	850	0	0	822	100	
850	900	1	0	823	100	
900	950	0	0	823	100	
950	1000	0	0	823	100	

Data elements inside histogram 823
Data elements outside histogram 0

Descriptive Statistics

Mean	29.70595
Variance	3435.968
Standard Deviation	58.61713
Skewness	6.215026

Histogram for Co_ppm *** DATA OUTSIDE RANGE ***



Mean = 29.706 Variance = 3436
Standard Deviation = 58.62 Skewness = 6.215

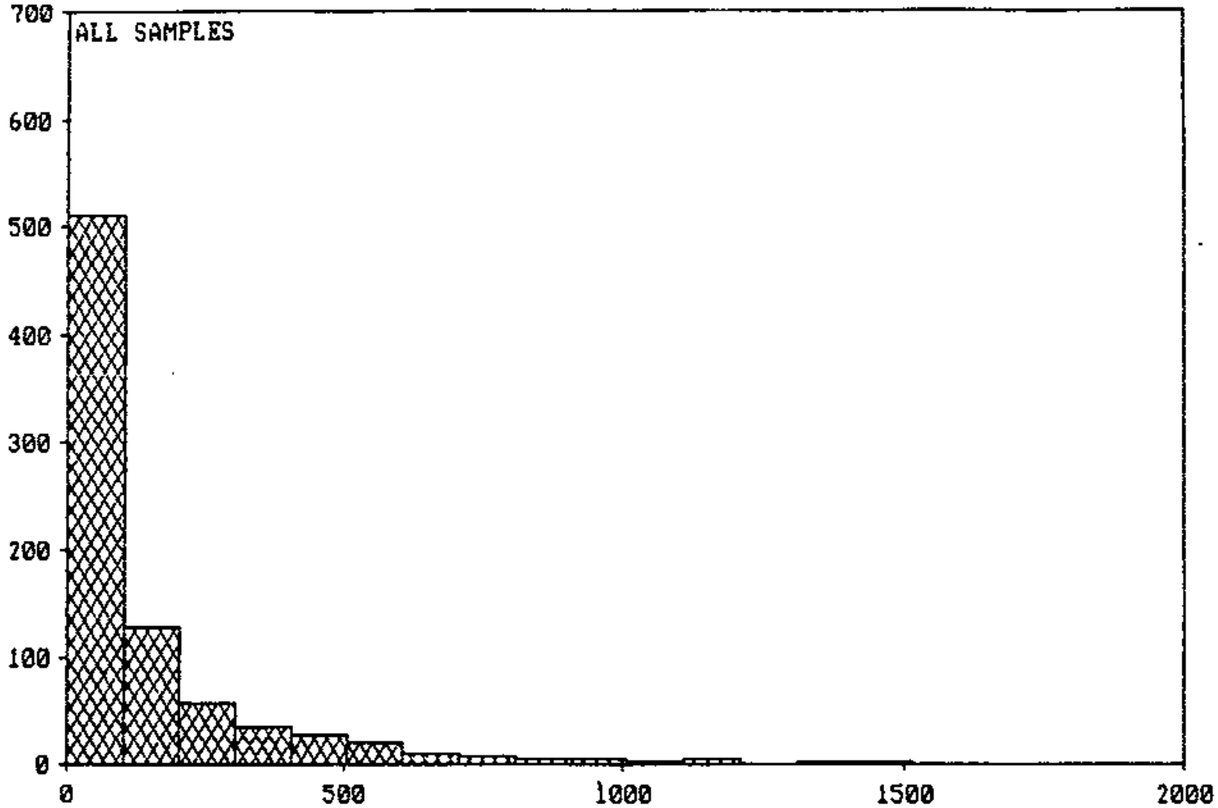
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	5	16	2	16	2	
5	10	211	26	227	28	
10	15	283	34	510	62	
15	20	89	11	599	73	
20	25	46	6	645	78	
25	30	24	3	669	81	Mean
30	35	19	2	688	84	
35	40	13	2	701	85	
40	45	9	1	710	86	
45	50	10	1	720	87	
50	55	15	2	735	89	
55	60	7	1	742	90	
60	65	7	1	749	91	
65	70	4	0	753	91	
70	75	6	1	759	92	
75	80	1	0	760	92	
80	85	4	0	764	93	
85	90	3	0	767	93	
90	95	2	0	769	93	
95	100	3	0	772	94	

Data elements inside histogram	772
Data elements outside histogram	51

Descriptive Statistics

Mean	29.70595
Variance	3435.968
Standard Deviation	58.61713
Skewness	6.215026

Histogram for Cu_ppm



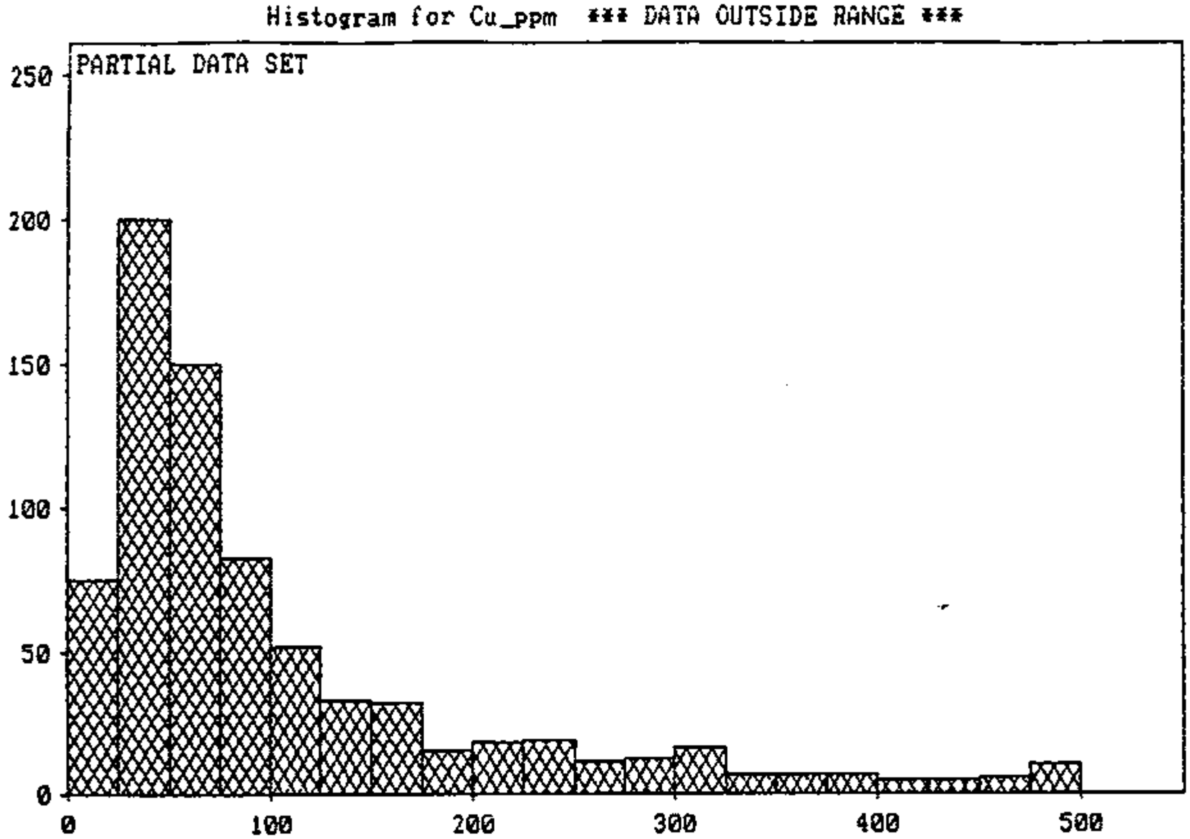
Mean = 159.57 Variance = 50500
Standard Deviation = 224.7 Skewness = 3.268

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	101	511	62	511	62	
101	202	129	16	640	78	Mean
202	303	59	7	699	85	
303	404	36	4	735	89	
404	505	28	3	763	93	
505	606	20	2	783	95	
606	707	11	1	794	96	
707	808	7	1	801	97	
808	909	6	1	807	98	
909	1010	4	0	811	99	
1010	1111	2	0	813	99	
1111	1212	4	0	817	99	
1212	1313	0	0	817	99	
1313	1414	2	0	819	100	
1414	1515	2	0	821	100	
1515	1616	0	0	821	100	
1616	1717	1	0	822	100	
1717	1818	0	0	822	100	
1818	1919	0	0	822	100	
1919	2020	1	0	823	100	

Data elements inside histogram 823
Data elements outside histogram 0

Descriptive Statistics

Mean	159.5723
Variance	50498.04
Standard Deviation	224.7177
Skewness	3.268079



Mean = 159.57 Variance = 50500
Standard Deviation = 224.7 Skewness = 3.268

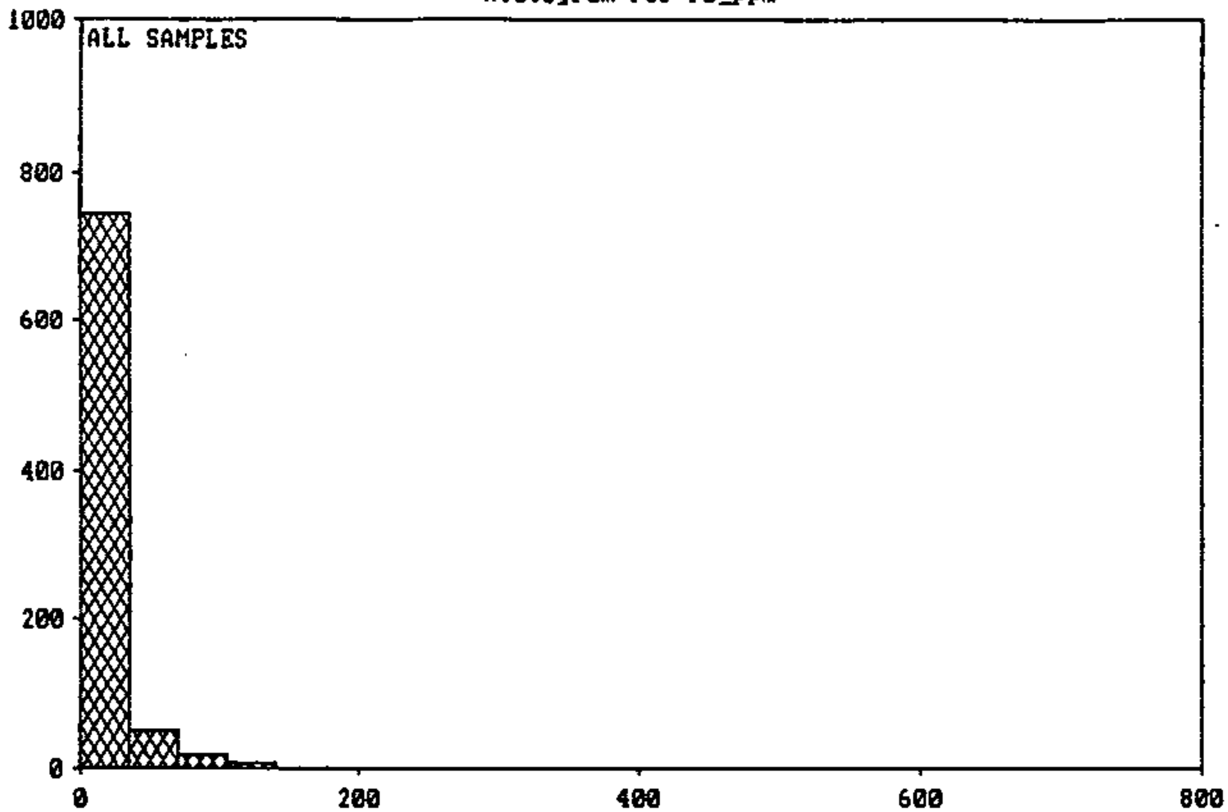
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	25	75	9	75	9	
25	50	200	24	275	33	
50	75	150	18	425	52	
75	100	82	10	507	62	
100	125	51	6	558	68	
125	150	33	4	591	72	
150	175	32	4	623	76	Mean
175	200	15	2	638	78	
200	225	18	2	656	80	
225	250	19	2	675	82	
250	275	11	1	686	83	
275	300	12	1	698	85	
300	325	16	2	714	87	
325	350	7	1	721	88	
350	375	7	1	728	88	
375	400	7	1	735	89	
400	425	5	1	740	90	
425	450	5	1	745	91	
450	475	6	1	751	91	
475	500	10	1	761	92	

Data elements inside histogram 761
Data elements outside histogram 62

Descriptive Statistics

Mean	159.5723
Variance	50498.04
Standard Deviation	224.7177
Skewness	3.268079

Histogram for Pb_ppm



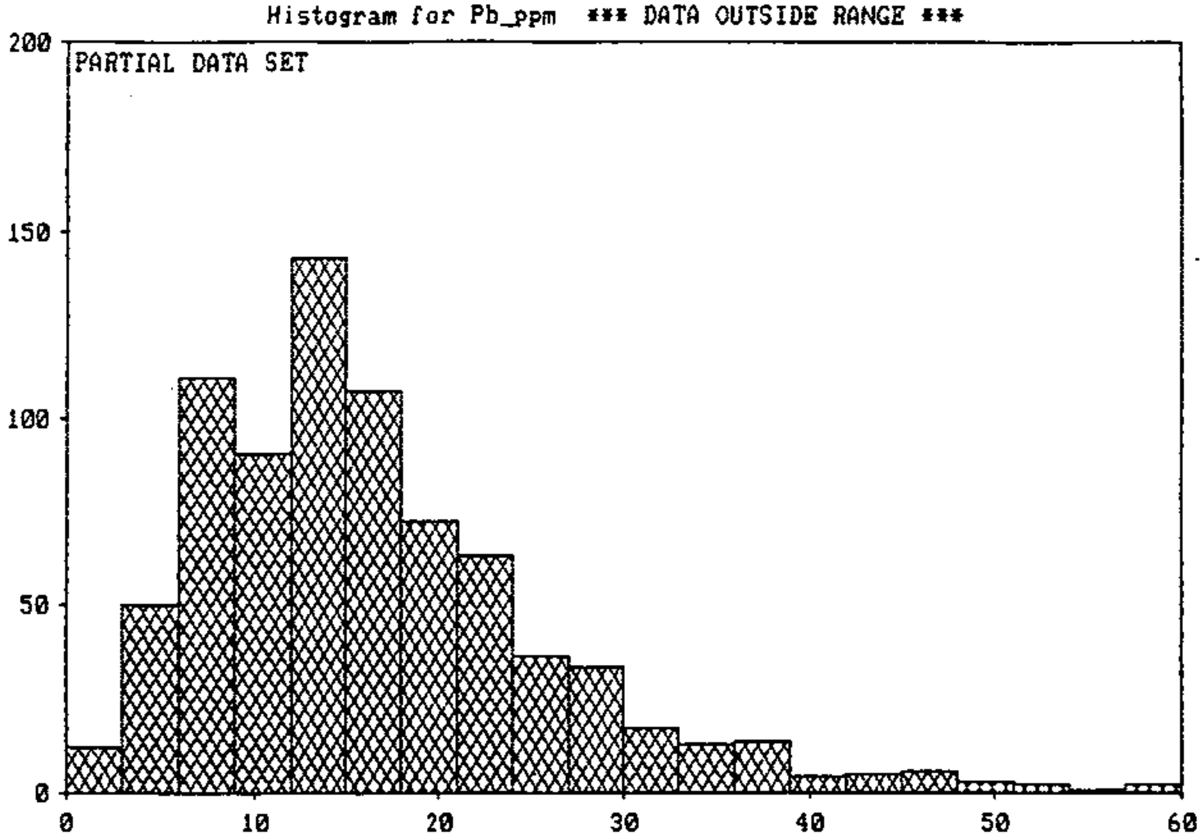
Mean = 20.067 Variance = 832.2
Standard Deviation = 28.85 Skewness = 13.39

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	35	744	90	744	90	Mean
35	70	50	6	794	96	
70	105	19	2	813	99	
105	140	7	1	820	100	
140	175	1	0	821	100	
175	210	1	0	822	100	
210	245	0	0	822	100	
245	280	0	0	822	100	
280	315	0	0	822	100	
315	350	0	0	822	100	
350	385	0	0	822	100	
385	420	0	0	822	100	
420	455	0	0	822	100	
455	490	0	0	822	100	
490	525	0	0	822	100	
525	560	0	0	822	100	
560	595	0	0	822	100	
595	630	0	0	822	100	
630	665	1	0	823	100	
665	700	0	0	823	100	

Data elements inside histogram 823
Data elements outside histogram 0

Descriptive Statistics

Mean	20.06683
Variance	832.245
Standard Deviation	28.84866
Skewness	13.3909



Mean = 20.067 Variance = 832.2
Standard Deviation = 28.85 Skewness = 13.39

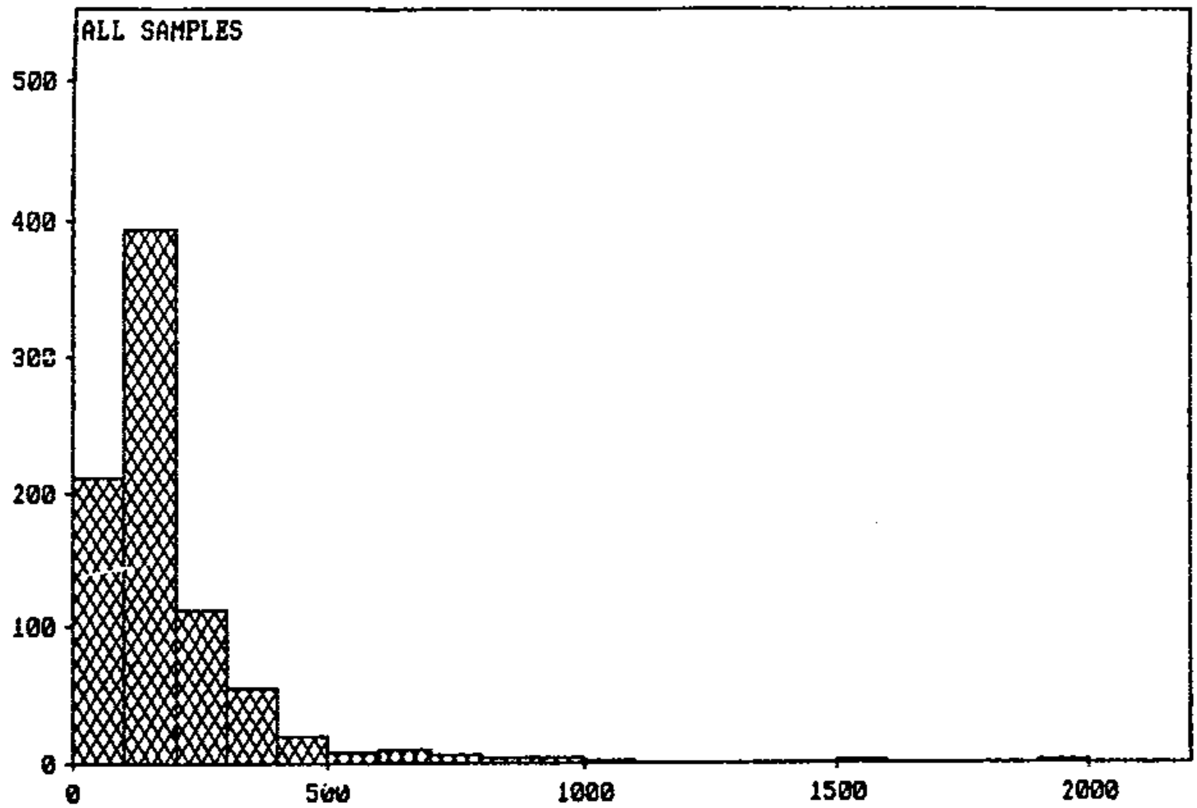
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	3	12	1	12	1	
3	6	50	6	62	8	
6	9	111	13	173	21	
9	12	91	11	264	32	
12	15	143	17	407	49	
15	18	107	13	514	62	
18	21	73	9	587	71	Mean
21	24	63	8	650	79	
24	27	37	4	687	83	
27	30	34	4	721	88	
30	33	17	2	738	90	
33	36	13	2	751	91	
36	39	14	2	765	93	
39	42	4	0	769	93	
42	45	5	1	774	94	
45	48	6	1	780	95	
48	51	3	0	783	95	
51	54	2	0	785	95	
54	57	1	0	786	96	
57	60	2	0	788	96	

Data elements inside histogram 788
Data elements outside histogram 35

Descriptive Statistics

Mean	20.06683
Variance	832.245
Standard Deviation	28.84866
Skewness	13.3909

Histogram for Zn_ppm



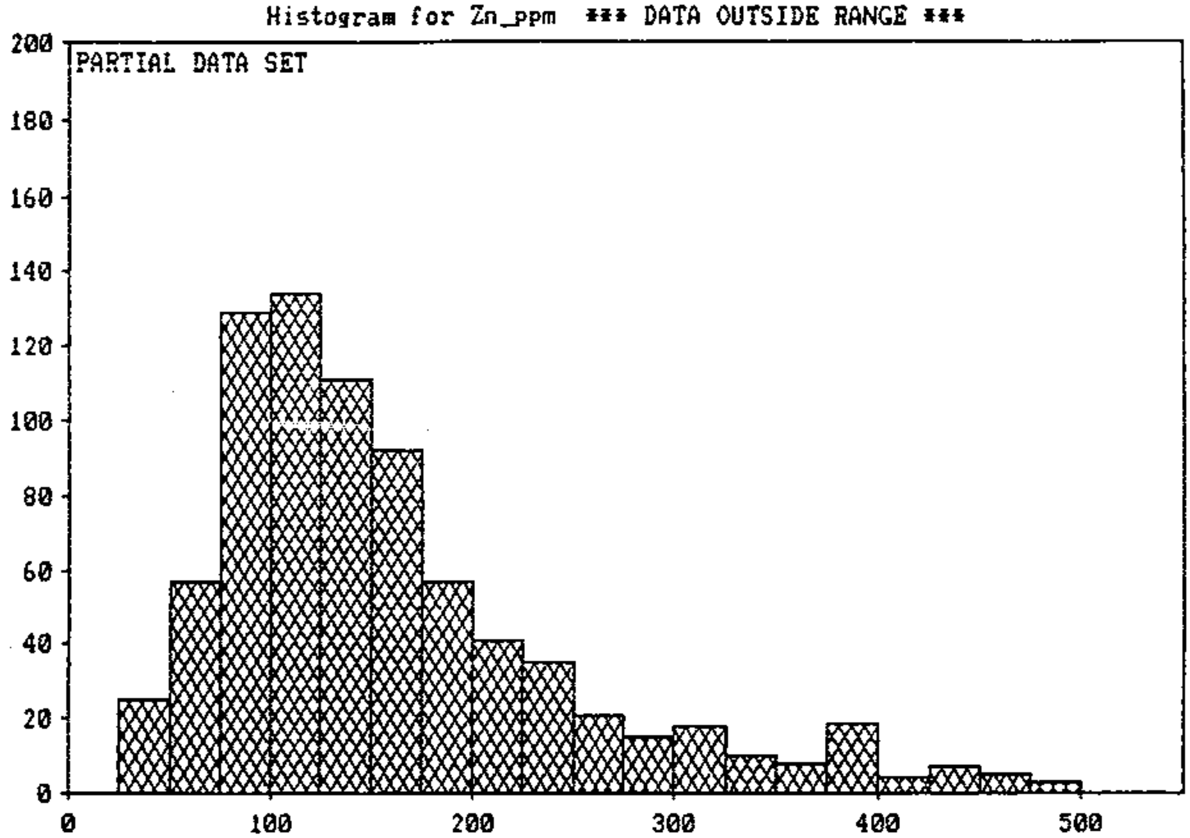
Mean = 183.44 Variance = 25230
Standard Deviation = 158.8 Skewness = 4.14

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	100	211	26	211	26	
100	200	394	48	605	74	Mean
200	300	112	14	717	87	
300	400	55	7	772	94	
400	500	19	2	791	96	
500	600	7	1	798	97	
600	700	9	1	807	98	
700	800	5	1	812	99	
800	900	4	0	816	99	
900	1000	3	0	819	100	
1000	1100	2	0	821	100	
1100	1200	0	0	821	100	
1200	1300	0	0	821	100	
1300	1400	0	0	821	100	
1400	1500	0	0	821	100	
1500	1600	1	0	822	100	
1600	1700	0	0	822	100	
1700	1800	0	0	822	100	
1800	1900	0	0	822	100	
1900	2000	1	0	823	100	

Data elements inside histogram	823
Data elements outside histogram	0

Descriptive Statistics

Mean	183.4399
Variance	25232.68
Standard Deviation	158.848
Skewness	4.140355



Mean = 183.44 Variance = 25230
Standard Deviation = 158.8 Skewness = 4.14

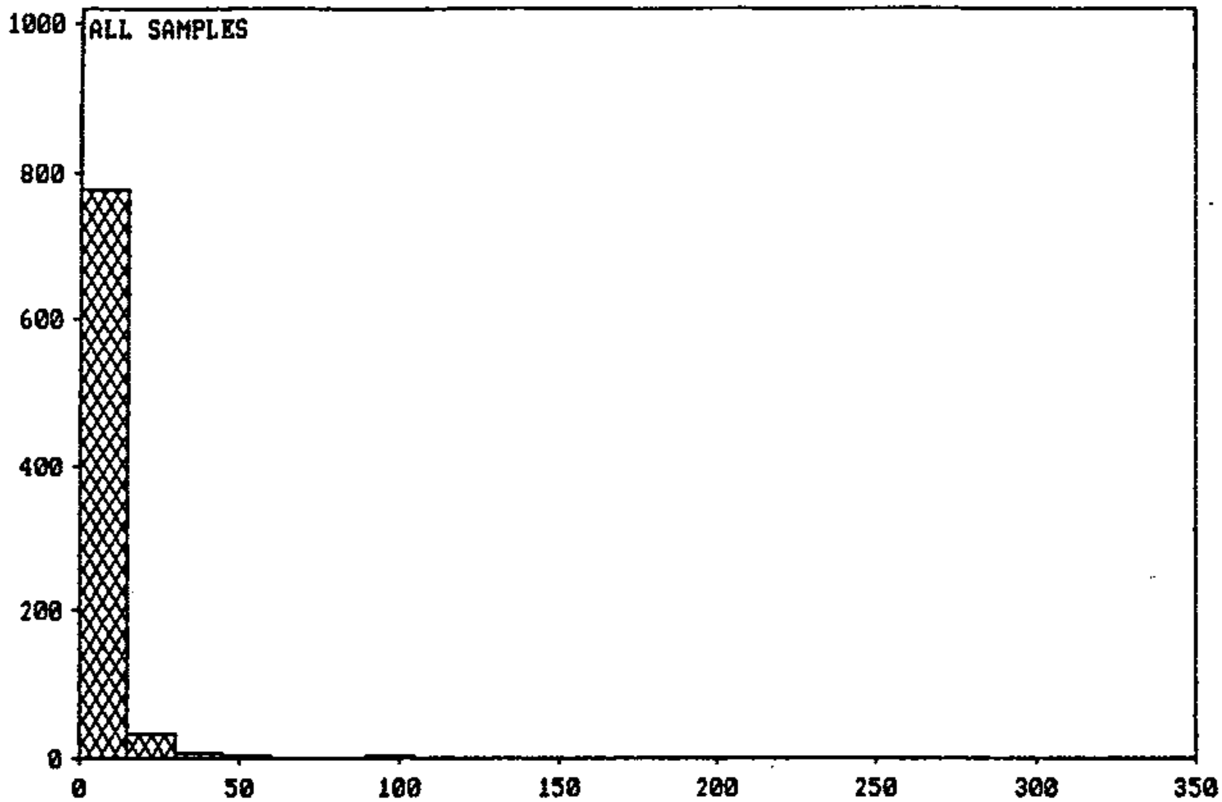
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	25	0	0	0	0	
25	50	25	3	25	3	
50	75	57	7	82	10	
75	100	129	16	211	26	
100	125	134	16	345	42	
125	150	111	13	456	55	
150	175	92	11	548	67	
175	200	57	7	605	74	Mean
200	225	41	5	646	78	
225	250	35	4	681	83	
250	275	21	3	702	85	
275	300	15	2	717	87	
300	325	18	2	735	89	
325	350	10	1	745	91	
350	375	8	1	753	91	
375	400	19	2	772	94	
400	425	4	0	776	94	
425	450	7	1	783	95	
450	475	5	1	788	96	
475	500	3	0	791	96	

Data elements inside histogram 791
Data elements outside histogram 32

Descriptive Statistics

Mean	183.4399
Variance	25232.68
Standard Deviation	158.848
Skewness	4.140355

Histogram for Au_ppb



Mean = 4.2151 Variance = 139.6
Standard Deviation = 11.82 Skewness = 11.64

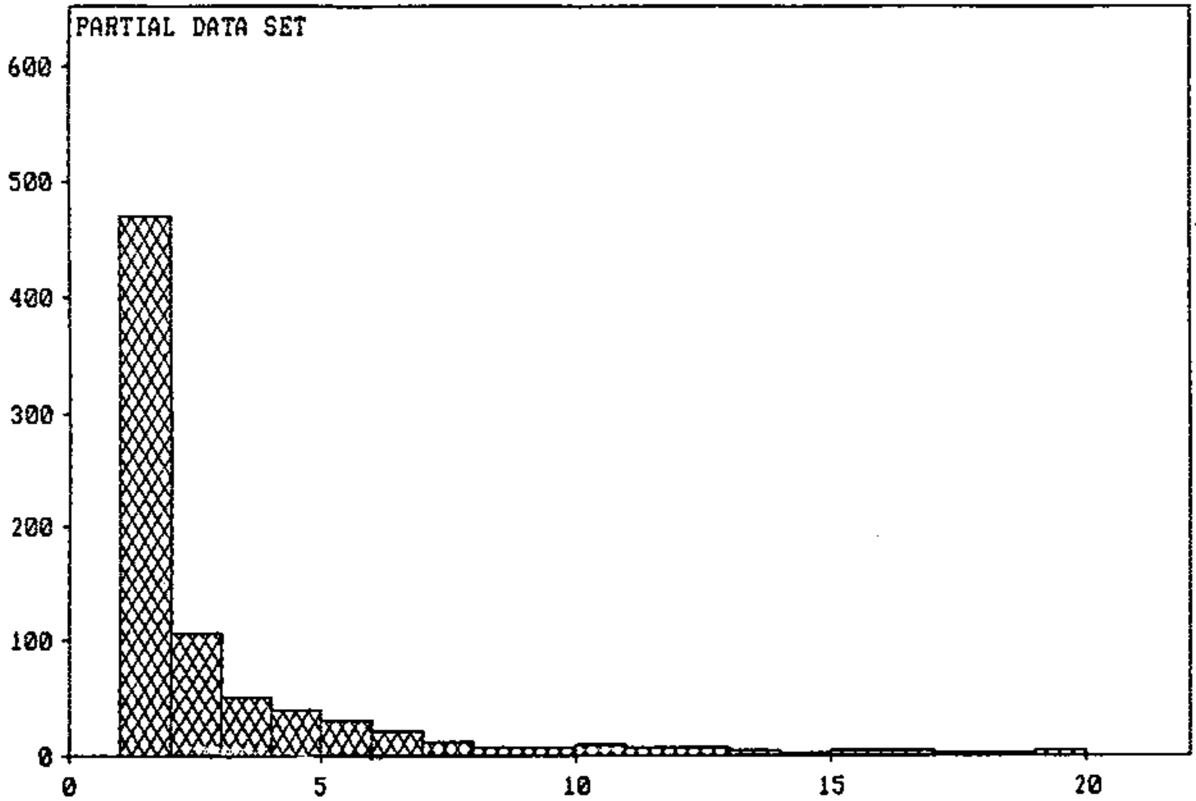
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	15	777	94	777	94	Mean
15	30	32	4	809	98	
30	45	6	1	815	99	
45	60	2	0	817	99	
60	75	1	0	818	99	
75	90	1	0	819	100	
90	105	3	0	822	100	
105	120	0	0	822	100	
120	135	0	0	822	100	
135	150	0	0	822	100	
150	165	0	0	822	100	
165	180	0	0	822	100	
180	195	0	0	822	100	
195	210	0	0	822	100	
210	225	0	0	822	100	
225	240	1	0	823	100	
240	255	0	0	823	100	
255	270	0	0	823	100	
270	285	0	0	823	100	
285	300	0	0	823	100	

Data elements inside histogram 823
Data elements outside histogram 0

Descriptive Statistics

Mean	4.215067
Variance	139.6409
Standard Deviation	11.81698
Skewness	11.63524

Histogram for Au_ppb *** DATA OUTSIDE RANGE ***



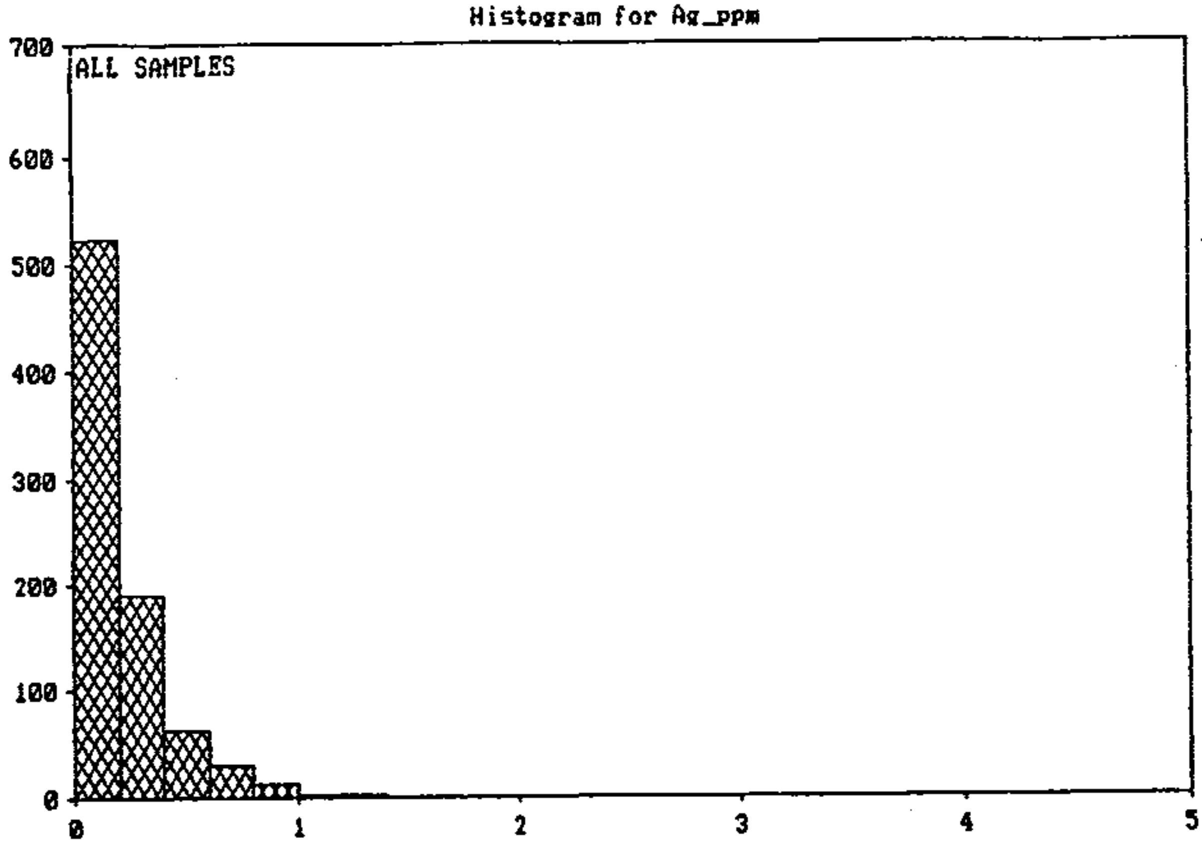
Mean = 4.2151 Variance = 139.6
Standard Deviation = 11.82 Skewness = 11.64

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	1	0	0	0	0	
1	2	470	57	470	57	
2	3	108	13	578	70	
3	4	52	6	630	77	
4	5	40	5	670	81	Mean
5	6	30	4	700	85	
6	7	20	2	720	87	
7	8	12	1	732	89	
8	9	8	1	740	90	
9	10	7	1	747	91	
10	11	10	1	757	92	
11	12	7	1	764	93	
12	13	6	1	770	94	
13	14	4	0	774	94	
14	15	3	0	777	94	
15	16	4	0	781	95	
16	17	4	0	785	95	
17	18	2	0	787	96	
18	19	3	0	790	96	
19	20	4	0	794	96	

Data elements inside histogram 794
Data elements outside histogram 29

Descriptive Statistics

Mean	4.215067
Variance	139.6409
Standard Deviation	11.81698
Skewness	11.63524



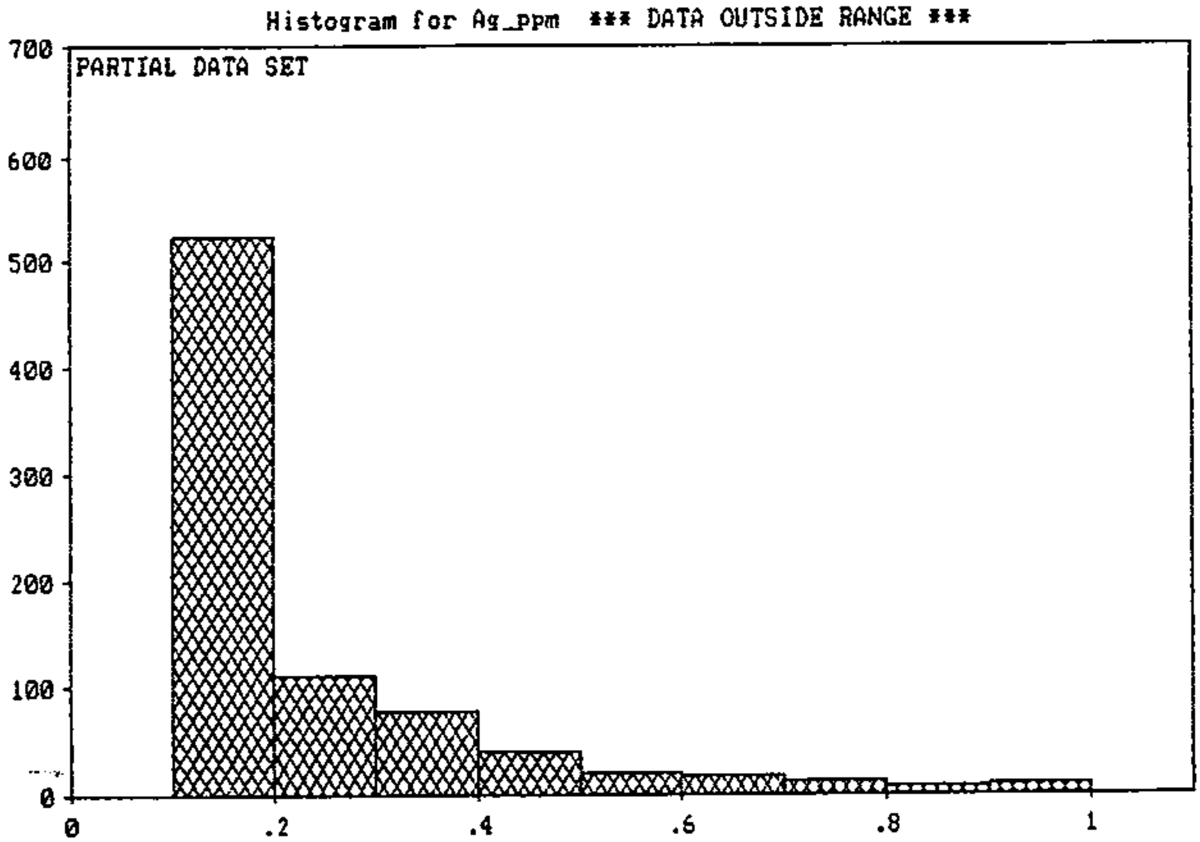
Mean = .19891 Variance = .04349
Standard Deviation = .2085 Skewness = 6.245

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	0.2	523	64	523	64	Mean
0.2	0.4	190	23	713	87	
0.4	0.6	62	8	775	94	
0.6	0.8	29	4	804	98	
0.8	1	13	2	817	99	
1	1.2	3	0	820	100	
1.2	1.4	2	0	822	100	
1.4	1.6	0	0	822	100	
1.6	1.8	0	0	822	100	
1.8	2	0	0	822	100	
2	2.2	0	0	822	100	
2.2	2.4	0	0	822	100	
2.4	2.6	0	0	822	100	
2.6	2.8	0	0	822	100	
2.8	3	0	0	822	100	
3	3.2	0	0	822	100	
3.2	3.4	0	0	822	100	
3.4	3.6	1	0	823	100	
3.6	3.8	0	0	823	100	
3.8	4	0	0	823	100	

Data elements inside histogram 823
Data elements outside histogram 0

Descriptive Statistics

Mean	0.1989065
Variance	0.043490
Standard Deviation	0.2085432
Skewness	6.245083



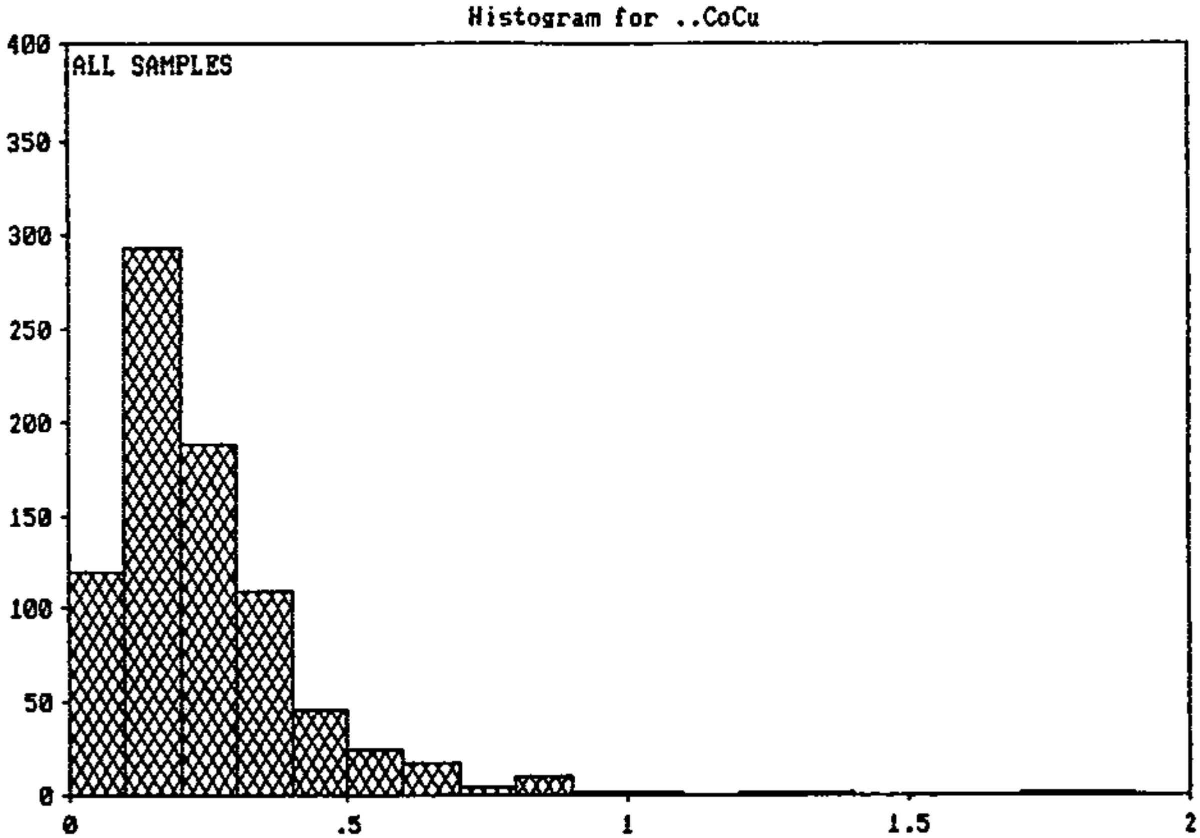
Mean = .19891 Variance = .04349
Standard Deviation = .2085 Skewness = 6.245

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	0.1	0	0	0	0	
0.1	0.2	523	64	523	64	Mean
0.2	0.3	111	13	634	77	
0.3	0.4	79	10	713	87	
0.4	0.5	41	5	754	92	
0.5	0.6	21	3	775	94	
0.6	0.7	17	2	792	96	
0.7	0.8	12	1	804	98	
0.8	0.9	7	1	811	99	
0.9	1	9	1	820	100	

Data elements inside histogram	820
Data elements outside histogram	3

Descriptive Statistics

Mean	0.1989065
Variance	0.043490
Standard Deviation	0.2085432
Skewness	6.245083



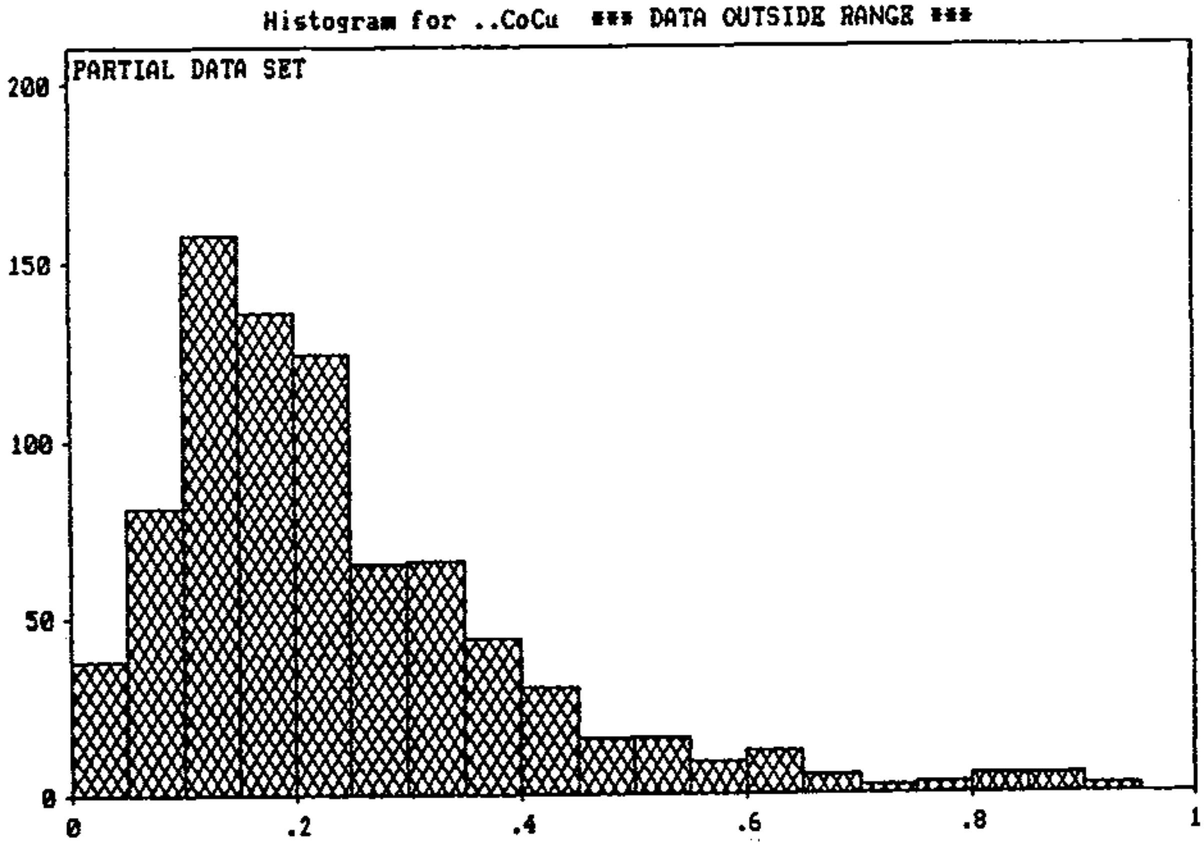
Mean = .2396 Variance = .03586
Standard Deviation = .1894 Skewness = 2.839

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	0.1	119	14	119	14	
0.1	0.2	294	36	413	50	
0.2	0.3	189	23	602	73	Mean
0.3	0.4	110	13	712	87	
0.4	0.5	46	6	758	92	
0.5	0.6	25	3	783	95	
0.6	0.7	17	2	800	97	
0.7	0.8	5	1	805	98	
0.8	0.9	10	1	815	99	
0.9	1	2	0	817	99	
1	1.1	1	0	818	99	
1.1	1.2	0	0	818	99	
1.2	1.3	1	0	819	100	
1.3	1.4	2	0	821	100	
1.4	1.5	0	0	821	100	
1.5	1.6	0	0	821	100	
1.6	1.7	0	0	821	100	
1.7	1.8	1	0	822	100	
1.8	1.9	1	0	823	100	
1.9	2	0	0	823	100	

Data elements inside histogram 823
Data elements outside histogram 0

Descriptive Statistics

Mean	0.2395991
Variance	0.035861
Standard Deviation	0.1893707
Skewness	2.838677



Mean = .2396 Variance = .03586
Standard Deviation = .1894 Skewness = 2.839

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	0.05	38	5	38	5	
0.05	0.1	81	10	119	14	
0.1	0.15	158	19	277	34	
0.15	0.2	136	17	413	50	
0.2	0.25	124	15	537	65	Mean
0.25	0.3	65	8	602	73	
0.3	0.35	66	8	668	81	
0.35	0.4	44	5	712	87	
0.4	0.45	30	4	742	90	
0.45	0.5	16	2	758	92	
0.5	0.55	16	2	774	94	
0.55	0.6	9	1	783	95	
0.6	0.65	12	1	795	97	
0.65	0.7	5	1	800	97	
0.7	0.75	2	0	802	97	
0.75	0.8	3	0	805	98	
0.8	0.85	5	1	810	98	
0.85	0.9	5	1	815	99	
0.9	0.95	2	0	817	99	
0.95	1	0	0	817	99	

Data elements inside histogram 817
Data elements outside histogram 6

Descriptive Statistics

Mean	0.2395991
Variance	0.035861
Standard Deviation	0.1893707
Skewness	2.838677

UTEM SURVEY

FOR

DECADE INTERNATIONAL DEVELOPMENT LTD.

ON THE SUE CLAIMS

SURVEY BY

HAROLD M. JONES & ASSOCIATES INC.

AND

S.J.V. CONSULTANTS LTD.

Vancouver M.D. N.T.S. 92J/2W

MAY 1988

Report By
Syd J. Visser
S.J.V. Consultants LTD.

APPENDIX II

UTEM SURVEY

FOR

DECADE INTERNATIONAL DEVELOPMENT LTD.

ON THE SUE CLAIMS

SURVEY BY

HAROLD M. JONES & ASSOCIATES INC.

AND

S.J.V. CONSULTANTS LTD.

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May, 1988

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S.J.V. Consultants Ltd.

TABLE OF CONTENTS

INTRODUCTION

A UTEM (Time Domain Electromagnetic) survey was completed on the Sue claims between May 10 and May 22, 1988. The Sue claims are located approx 20 Km north of Whistler on the Soo River.

The purpose of the UTEM survey was to search for massive sulfides at depth greater than 100 metres.

DESCRIPTION OF UTEM SYSTEM

UTEM is an acronym for "University of Toronto ElectroMagnetometer". The system was developed by Dr. Y. Lamontagne (1975) while he was a graduate student of that University.

The field procedure consist of first laying out a large loop of single strand insulated wire and energizing it with current from a transmitter which is powered by a 2.2 kW motor generator. Survey lines are generally oriented perpendicular to one side of the loop and surveying can be performed both inside and outside the loop.

The transmitter loop is energized with a precise triangular current waveform at a carefully controlled frequency (30.974 Hz for this survey). The receiver system includes a sensor coil and backpack portable receiver module which has a digital recording facility on cassette magnetic tape. The time synchronization between transmitter and receiver is achieved through quartz crystal clocks in both units which must be accurate to about one second in 50 years.

The receiver sensor coil measures the vertical magnetic component of the electromagnetic field and responds to its time derivative. Since the transmitter current waveform is triangular, the receiver coil will sense a perfect square wave in the absence of geologic conductors. Deviations from a perfect square wave are caused by electrical conductors which may be geologic or cultural in origin. The receiver stacks any pre-set number of cycles in order to increase the signal to noise ratio.

The UTEM receiver gathers and records 9 channels of data at each station. The higher number channels (7-8-9) correspond to short time or high frequency while the lower number channels (1-2-3) correspond to long time or low frequency. Therefore, poor or weak conductors will respond on channels 9, 8, 7, and 6. Progressively better conductors will give responses on progressively lower number channels as well. For example, massive, highly conducting sulfides or graphite will produce a response on all nine channels.

It was mentioned above that the UTEM receiver records data digitally on a cassette. This tape is played back into a computer at the base camp. The computer processes the data and controls the plotting on an 11" x 15" graphics plotter. Data are portrayed on data sections as profiles of each of the nine channels, one section for each survey line.

FIELD WORK

The field crew consisted of 3 helpers and one geophysicist for the first half of the survey and 2 helpers and two geophysicist (Syd Visser and Rolf Krawinkel) for the remainder of the survey. The crew stayed in Whistler and commuted by truck to the survey area each day.

A total of approx. 26Km were surveyed from 4 separate loops (see plate 88-1). Ten separate time channels from the vertical (Hz) component of the electromagnetic field was measured and recorded at each station. The station spacing along the survey lines varied from 25M to 50M. The 25M station spacing was used in some areas to more clearly outline near surface conductors or contact zones.

DATA PRESENTATION

The results of the survey are presented on one compilation map and 63 data sections (Appendix II).

The maps are listed as follows:

Plate 88-1	UTEM Compilation Map
(in envelope)	Scale 1:5,000

Legends for the UTEM data sections are also attached (Appendix I).

In order to reduce the field data, the theoretical primary field of the loop must be computed at each station. The normalization of the data is a follows:

a) For Channel 1:

$$\% \text{ Ch.1 anomaly} = \frac{\text{Ch.1} - P}{N_1} \times 100$$

where P is the primary field from the loop at the station and Ch.1 is the observed amplitude of Channel 1

b) For remaining channels (n = 2 to 9)

$$\% \text{ Ch.n anomaly} = \frac{(\text{Ch.n} - \text{Ch.1})}{N_1} \times 100$$

where Ch.n is the observed amplitude of Channel n (2 to 9)

N_1 = Ch.1 for Ch1 normalized

N_1 = P for primary field normalized

i is the data station for continuous normalized (each reading normalized by different primary field)

i is the station below the arrow on the data sections for point normalized (each reading normalized by the same primary field)

INTERPRETATION

A number of weak shallow (<150M) conductors and contact zones were located in the survey area (plate 88-1). The major feature is a shallow weak conductor extending from approx. 250W on line 1500N to 650W on line 500N. This weak conductor is open to the north and probable extends further south since a similar conductor is noted at approx 800W on line 100S. Loop 5 was placed on the west side of this conductor to detail lines 1000N, 1200N, 1400N and 1500N. The results from both loop 5 and loop 2 indicated the same shallow weak conductor along with a possibility of the conductive axis also being a contact zone.

A well defined contact zone, with the higher conductivity rocks laying to the east, can be traced from approx 400W on line 500S to approx. 100W on line 500N, after which the contact disappears or is difficult to trace. A similar contact zone extends from approx. 275E on line 100N to approx. 300E on line 700N.

A number of weak very shallow crossovers and contact area are seen in the center part of the grid (Plate 88-1) which are small discontinues conductors or due to changes in conductive overburden.

No strong conductors indicating the existence of massive sulfide were found in the survey area.

CONCLUSION

A number of weak shallow conductors and contact zones were located in the survey area. There is no indication of any strong conductors expected from massive sulfides.

Syd Visser F.G.A.C.
Geophysicist

S.J.V. Consultants LTD.

APPENDIX I

LEGEND

Channel	Mean delay time	Plotting symbol
1	12.8 ms	1
2	6.4	/
3	3.2	\
4	1.6	□
5	0.8	5
6	0.4	∡
7	0.2	7
8	0.1	⧖
9	0.05	△
10	0.025	◇

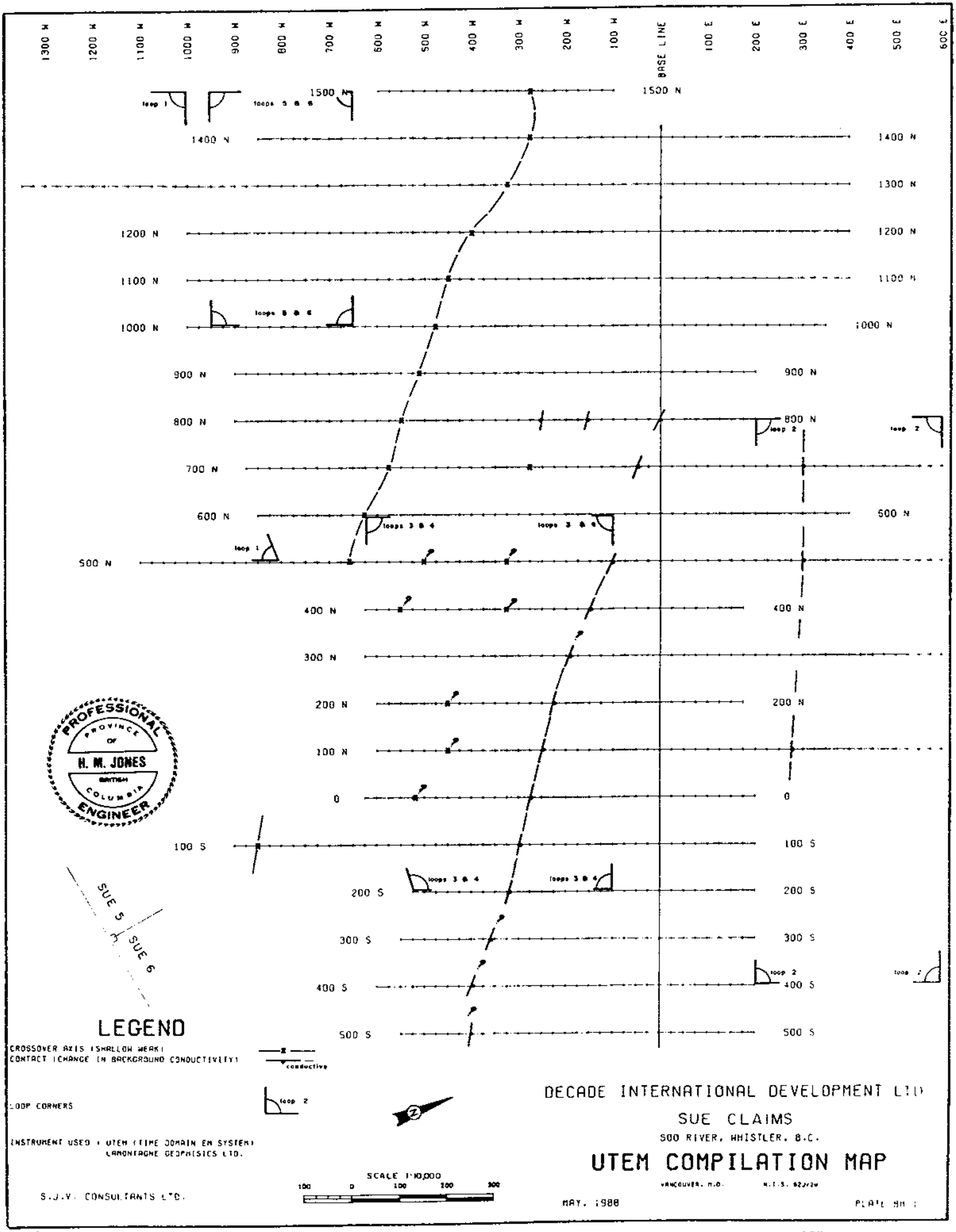
APPENDIX II

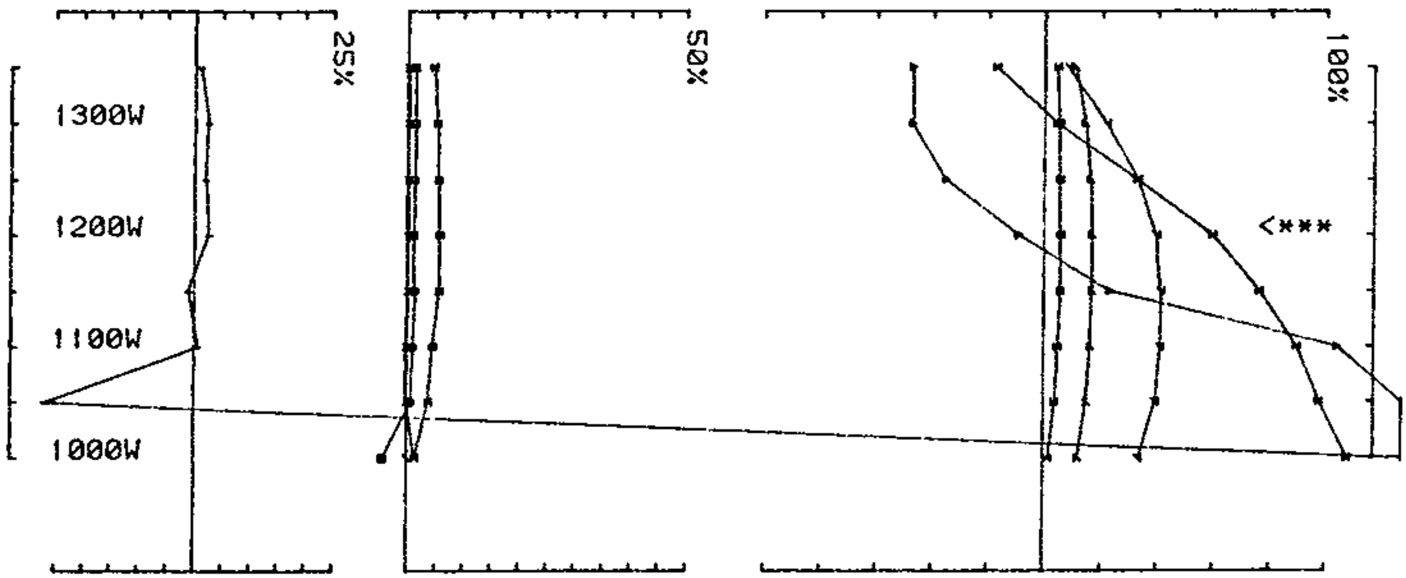
COMPILATION MAP AND SECTIONS

APPENDIX II

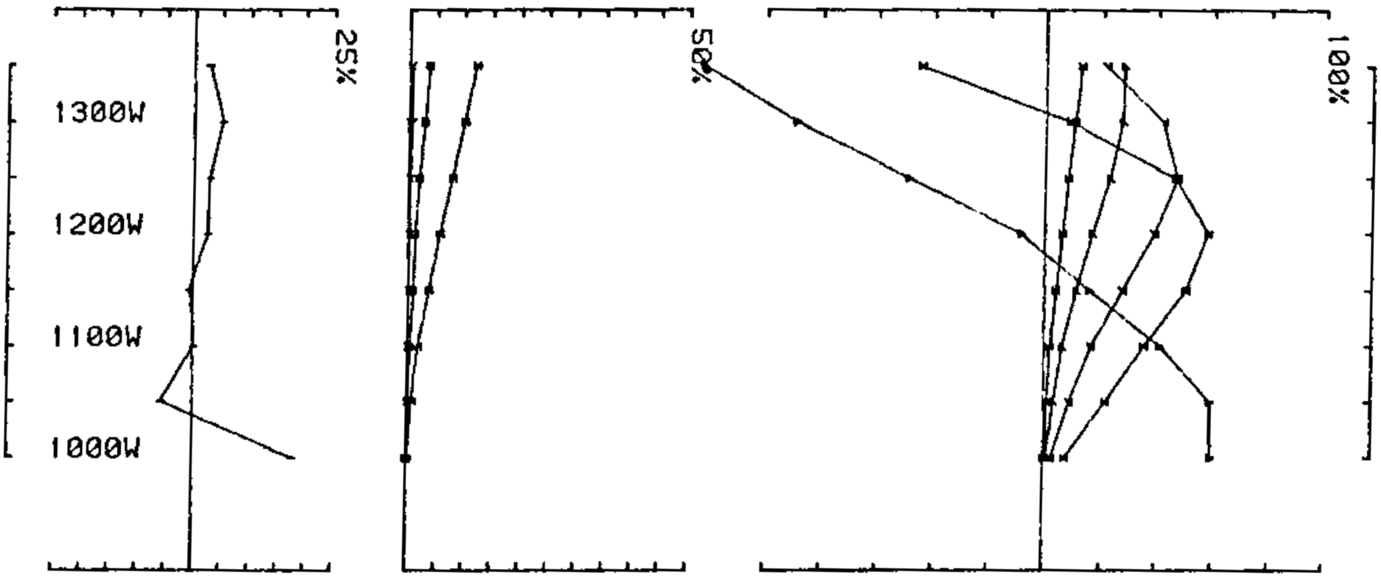
APPENDIX II

COMPILATION MAP AND SECTIONS


1300 W
1200 W
1100 W
1000 W
900 W
800 W
700 W
600 W
500 W
400 W
300 W
200 W
100 W
BASE LINE
100 E
200 E
300 E
400 E
500 E
600 E
1500 N
1400 N
1300 N
1200 N
1100 N
1000 N
900 N
800 N
700 N
600 N
500 N
400 N
300 N
200 N
100 N
0
100 S
200 S
300 S
400 S
500 S
loop 1
loops 5 & 6
loops 3 & 4
loop 2
SUE 5
SUE 6
PROFESSIONAL
PROVINCE OF
H. M. JONES
BRITISH COLUMBIA
ENGINEER
LEGEND
CROSSOVER AXIS (SHALLOW WEAK)
CONTACT (CHANGE IN BACKGROUND CONDUCTIVITY)
conductive
LOOP CORNERS
INSTRUMENT USED : UTEM (TIME DOMAIN EM SYSTEM)
LAMONTAGNE GEOPHYSICS LTD.
S.J.V. CONSULTANTS LTD.
SCALE 1:10,000
100
0
100
200
300
DECADE INTERNATIONAL DEVELOPMENT LTD
SUE CLAIMS
SOO RIVER, WHISTLER, B.C.
UTEM COMPILATION MAP
MAY, 1988



UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
conducted by S.J.V. CONSULTANTS LTD. job 8805 base freq (hz) 30.974
loop no 6 line 1300N component Hz secondary field Ch 1 point norm.



UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
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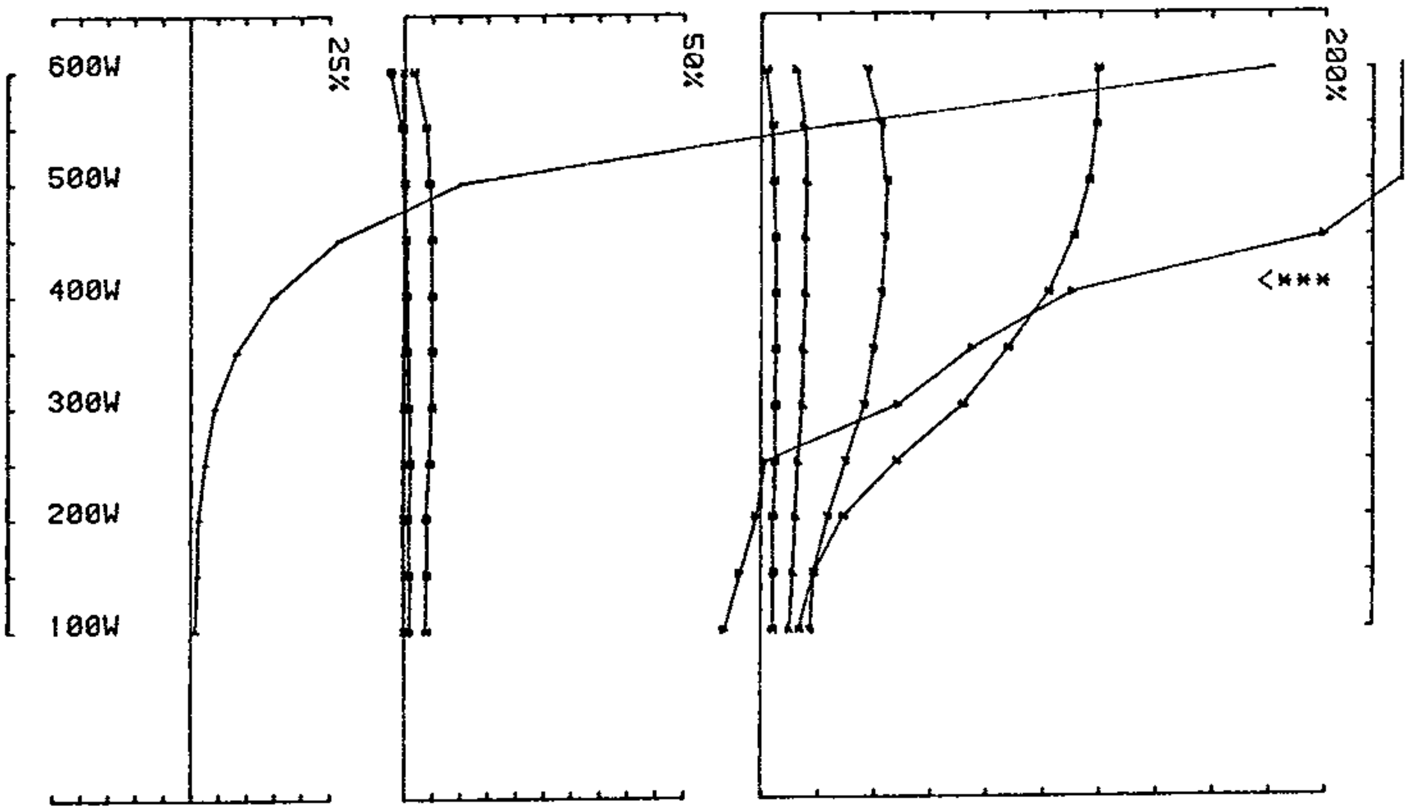
loop no 6 line 1300N component Hz secondary field Ch 1 contin. norm.



UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
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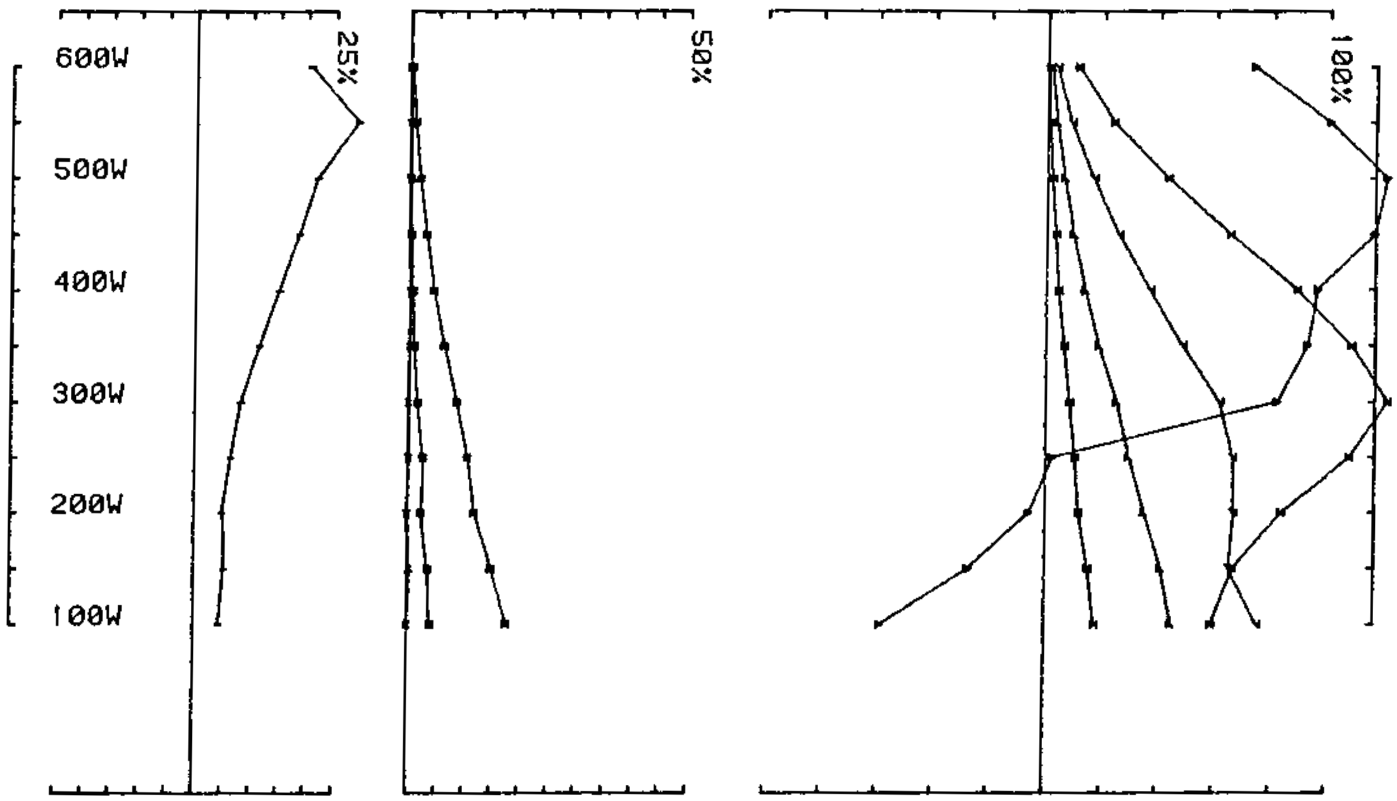

UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
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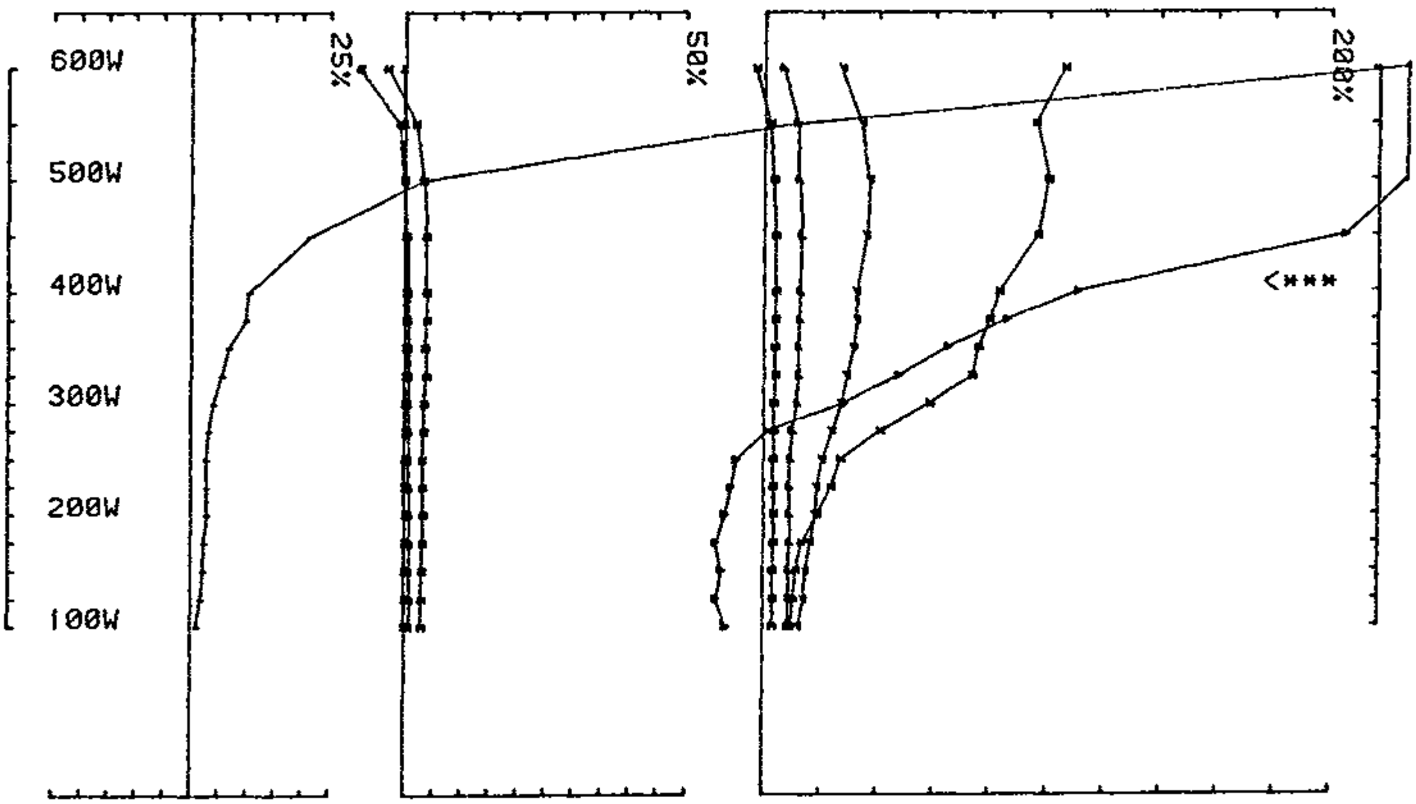

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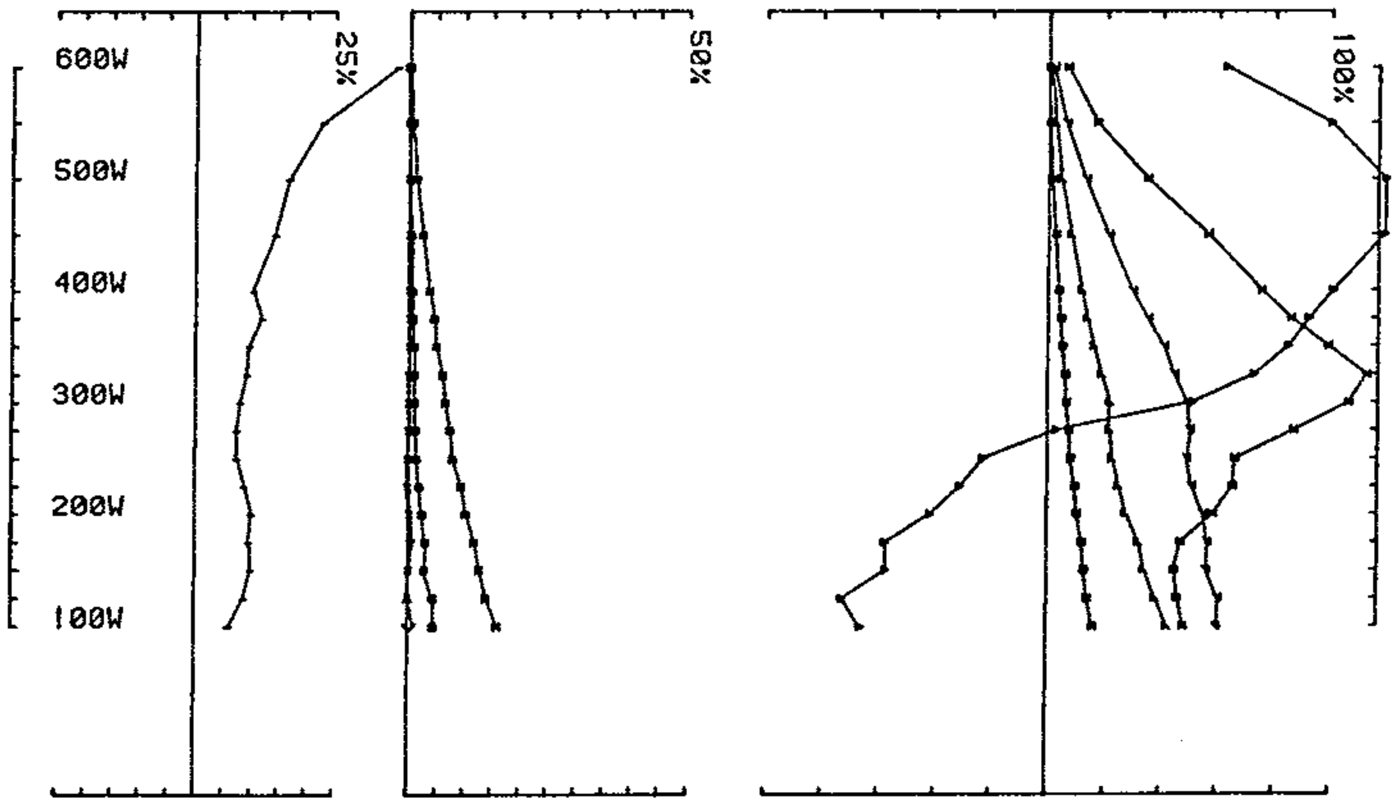

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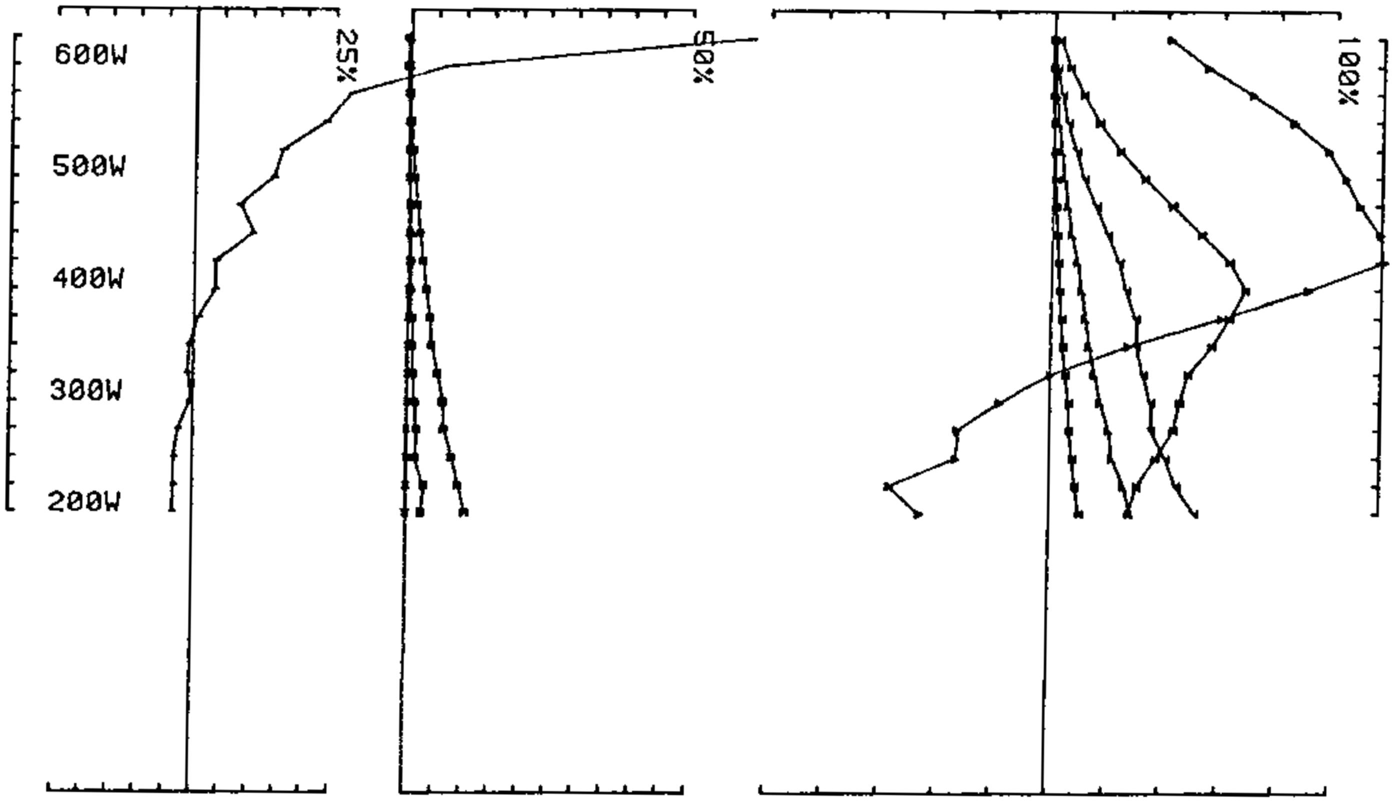

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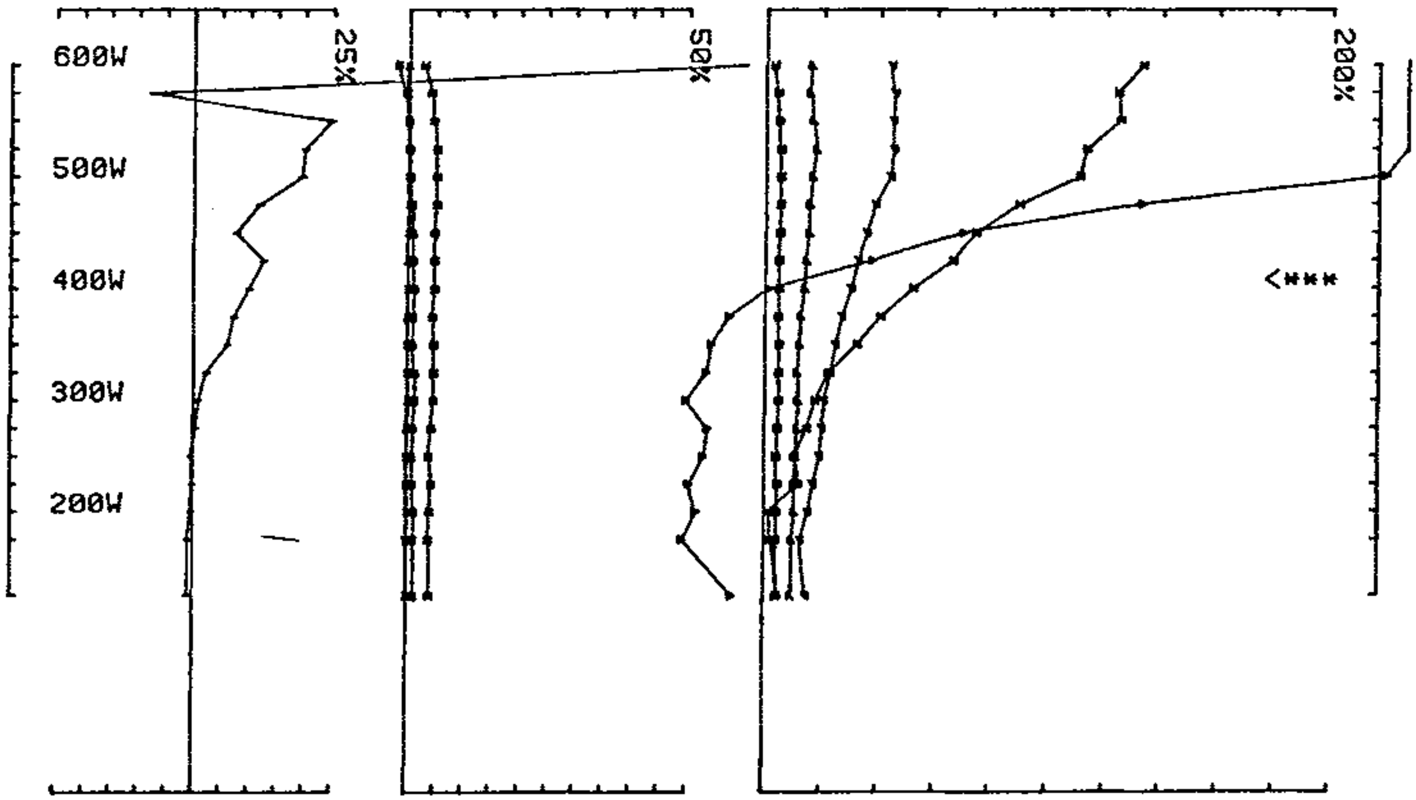

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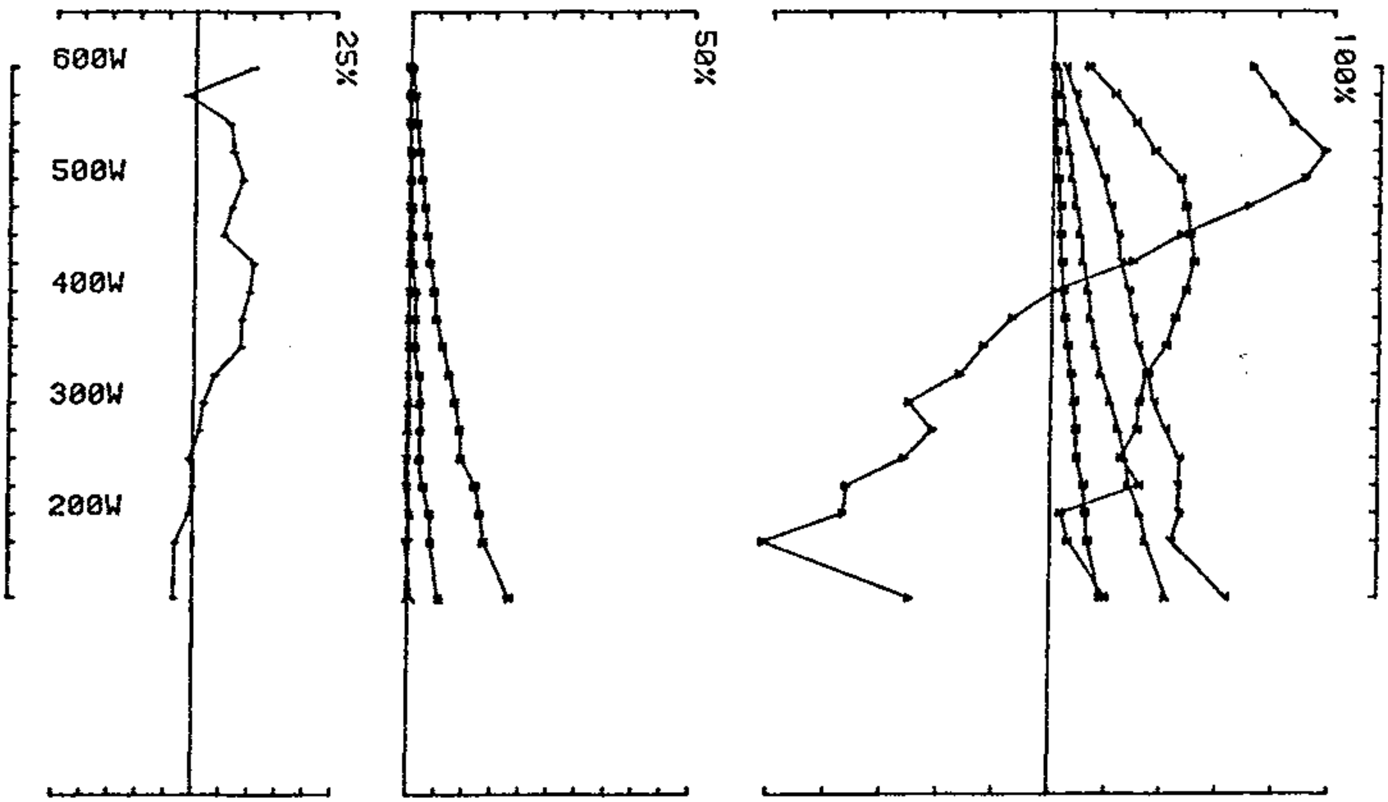

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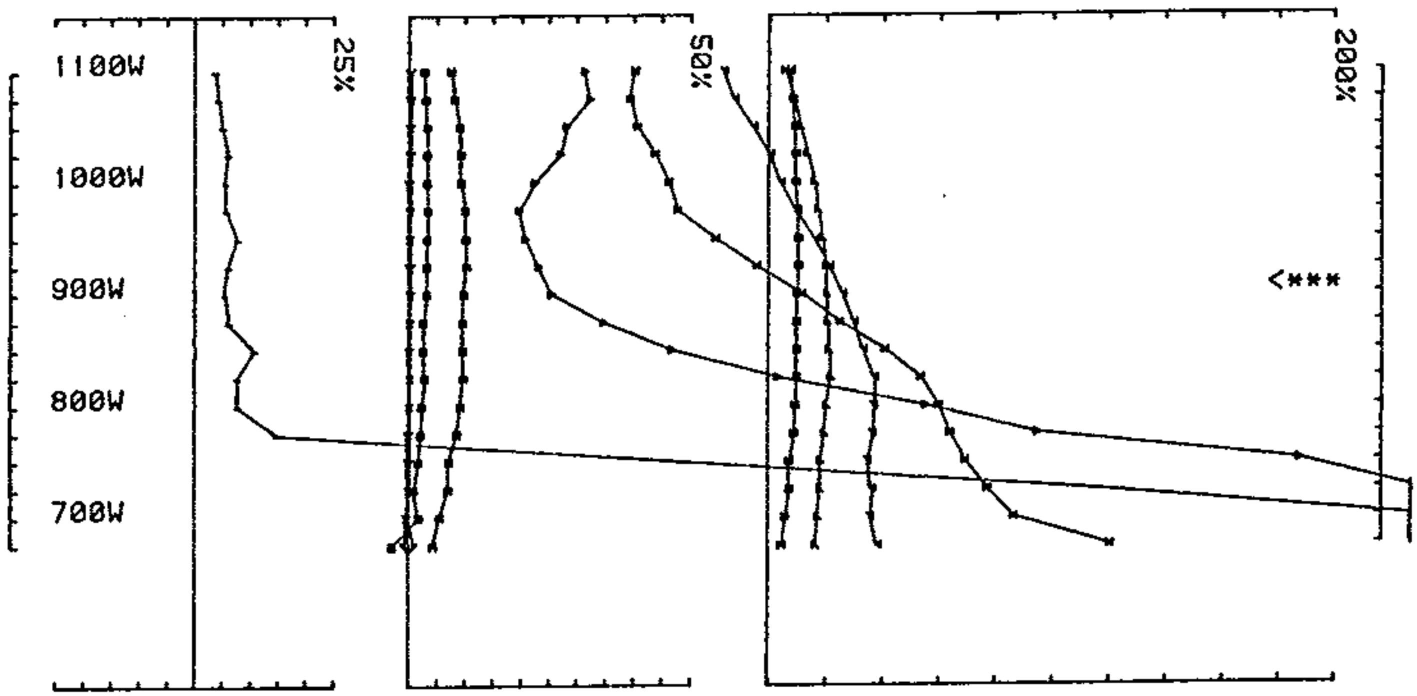

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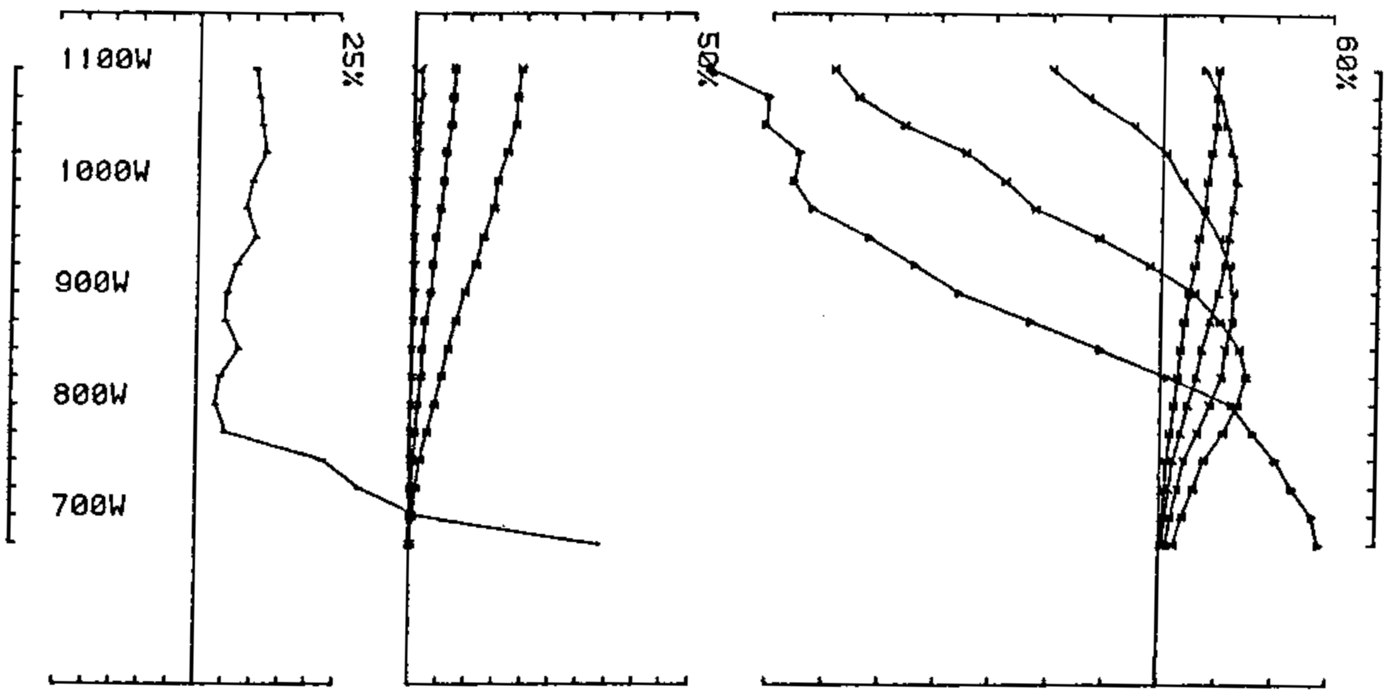

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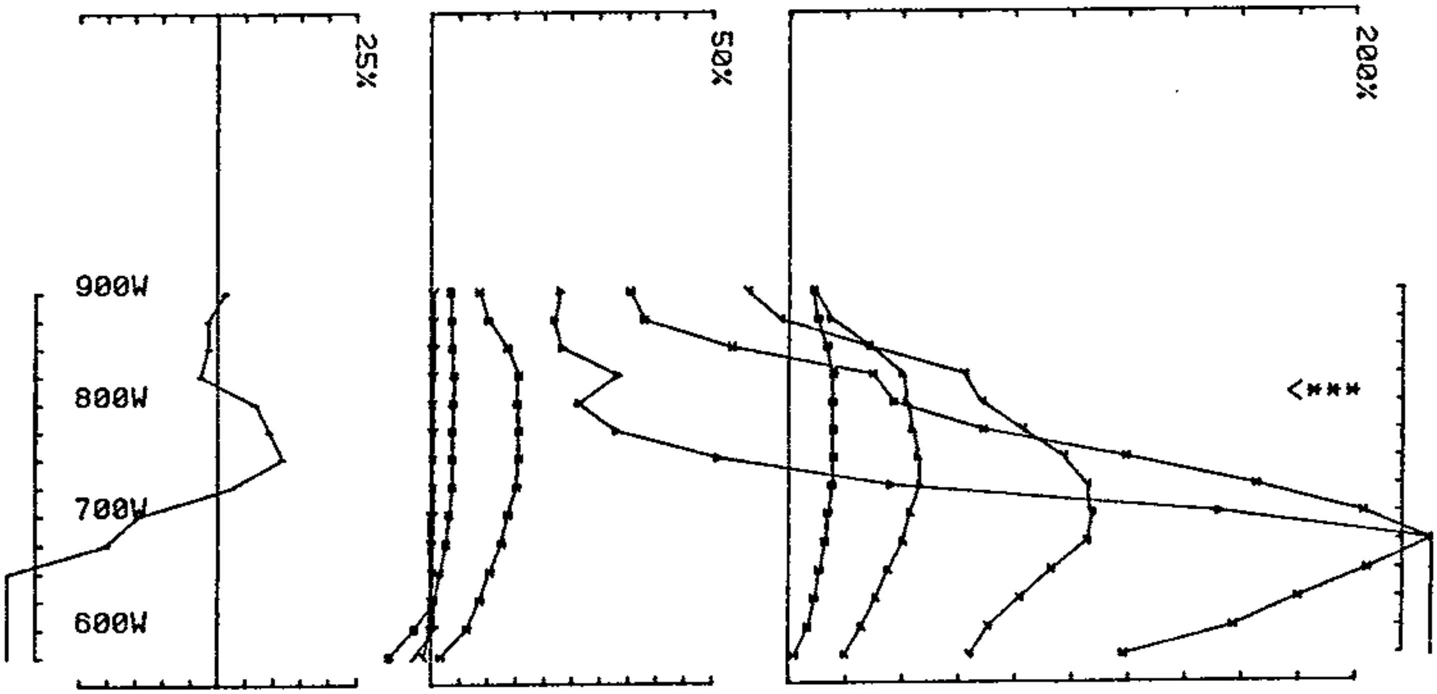

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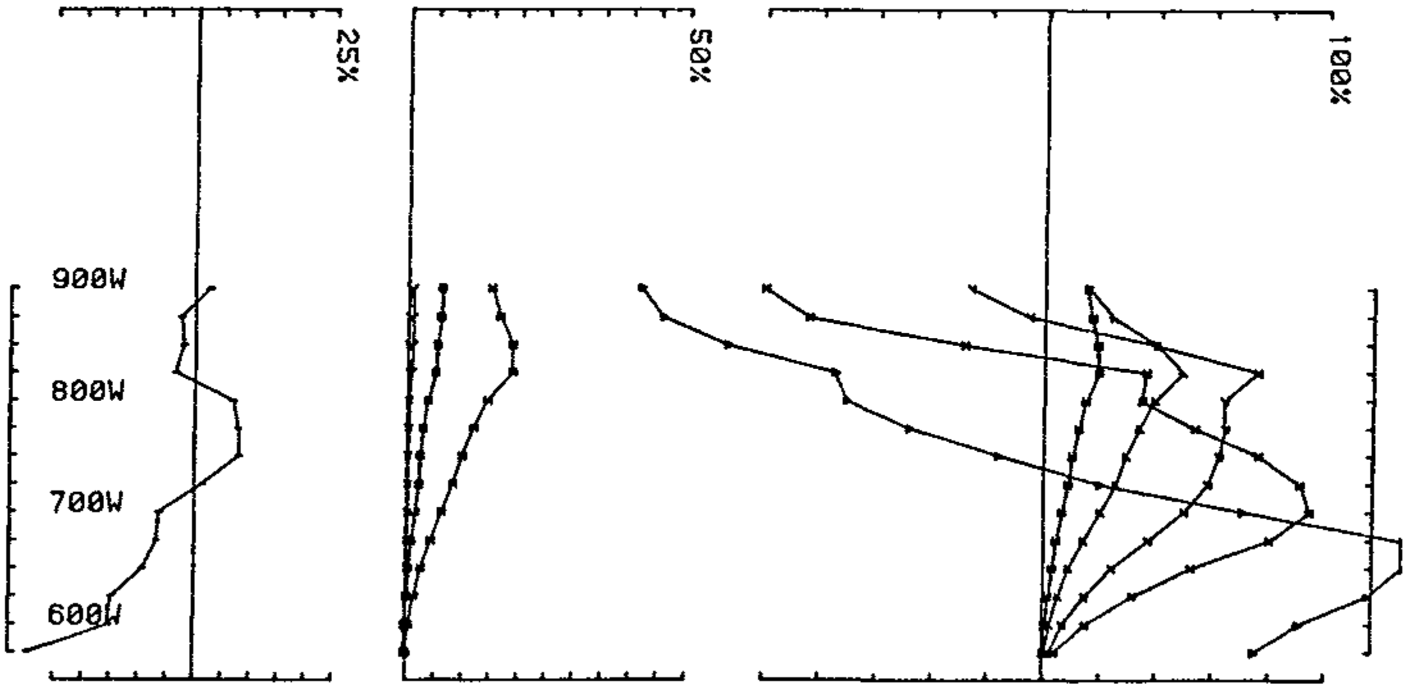

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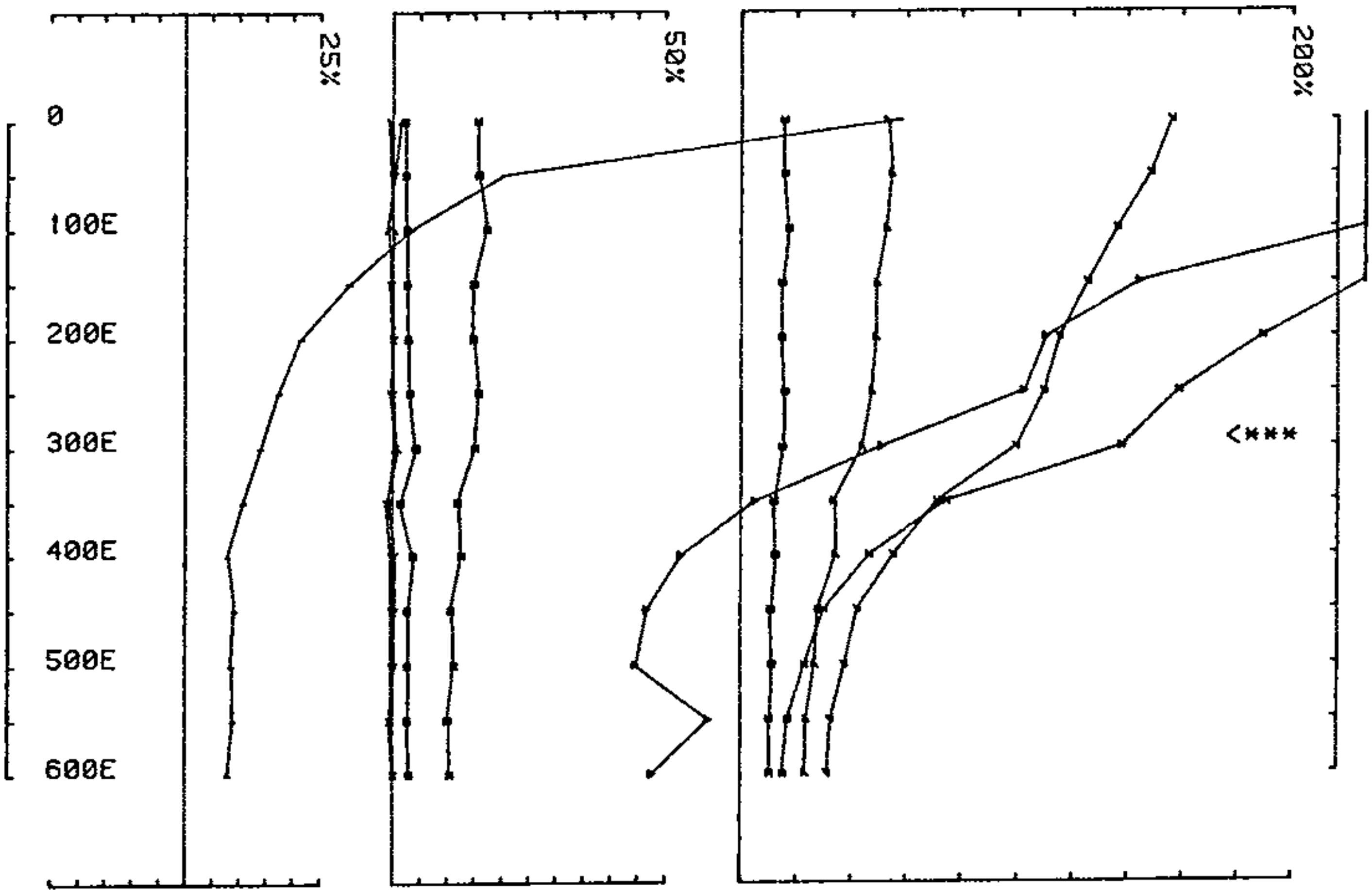

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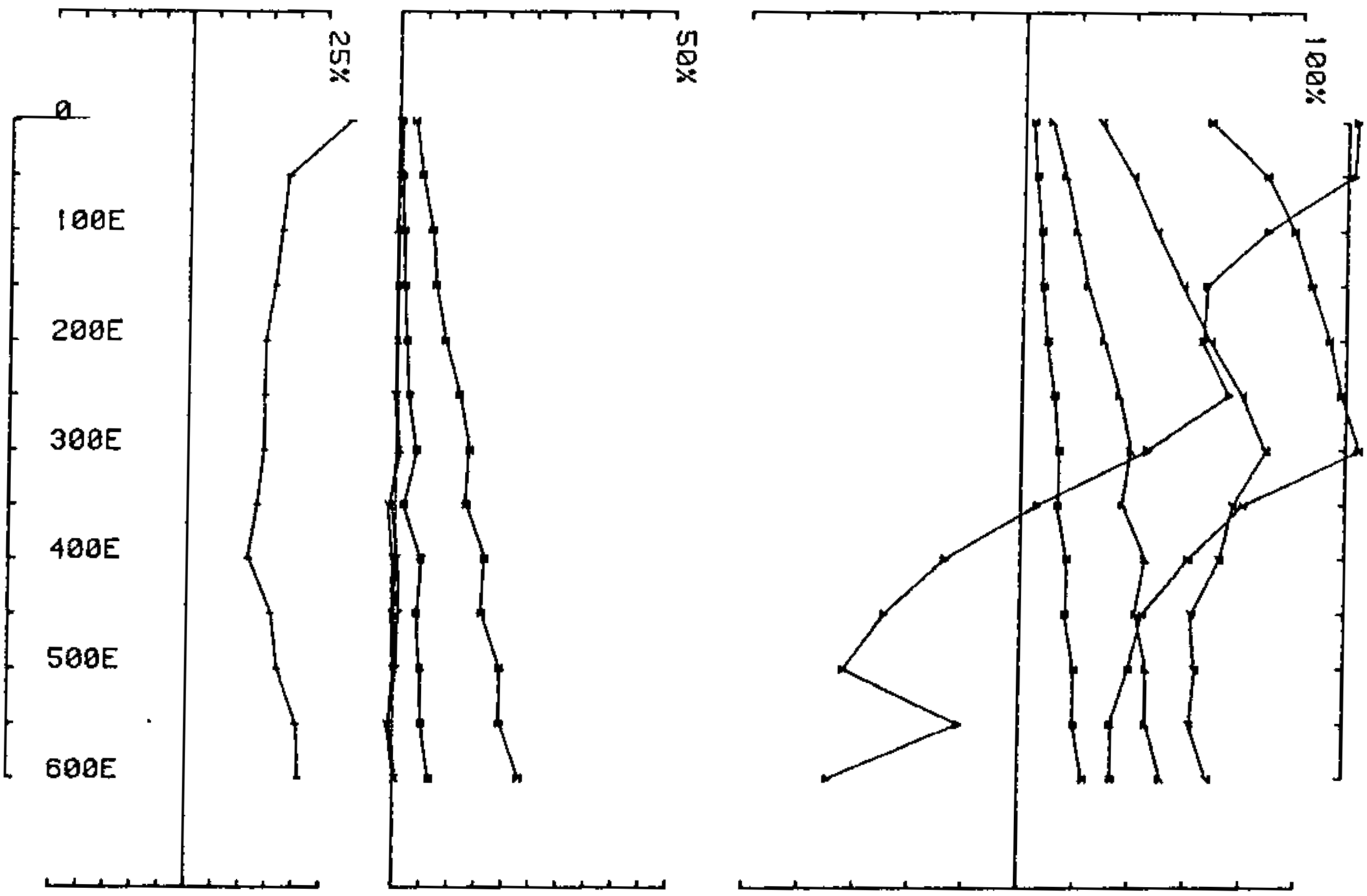

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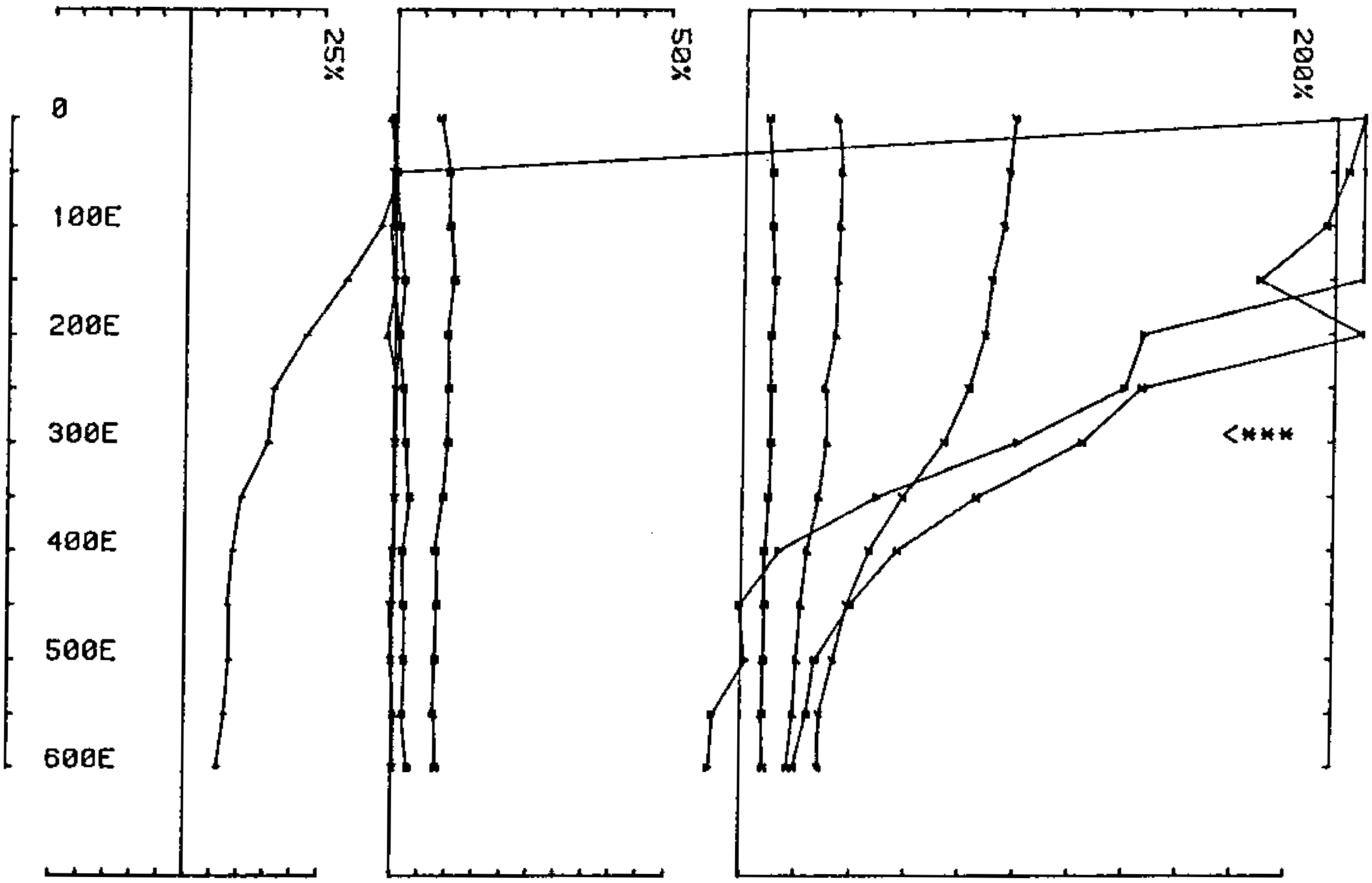

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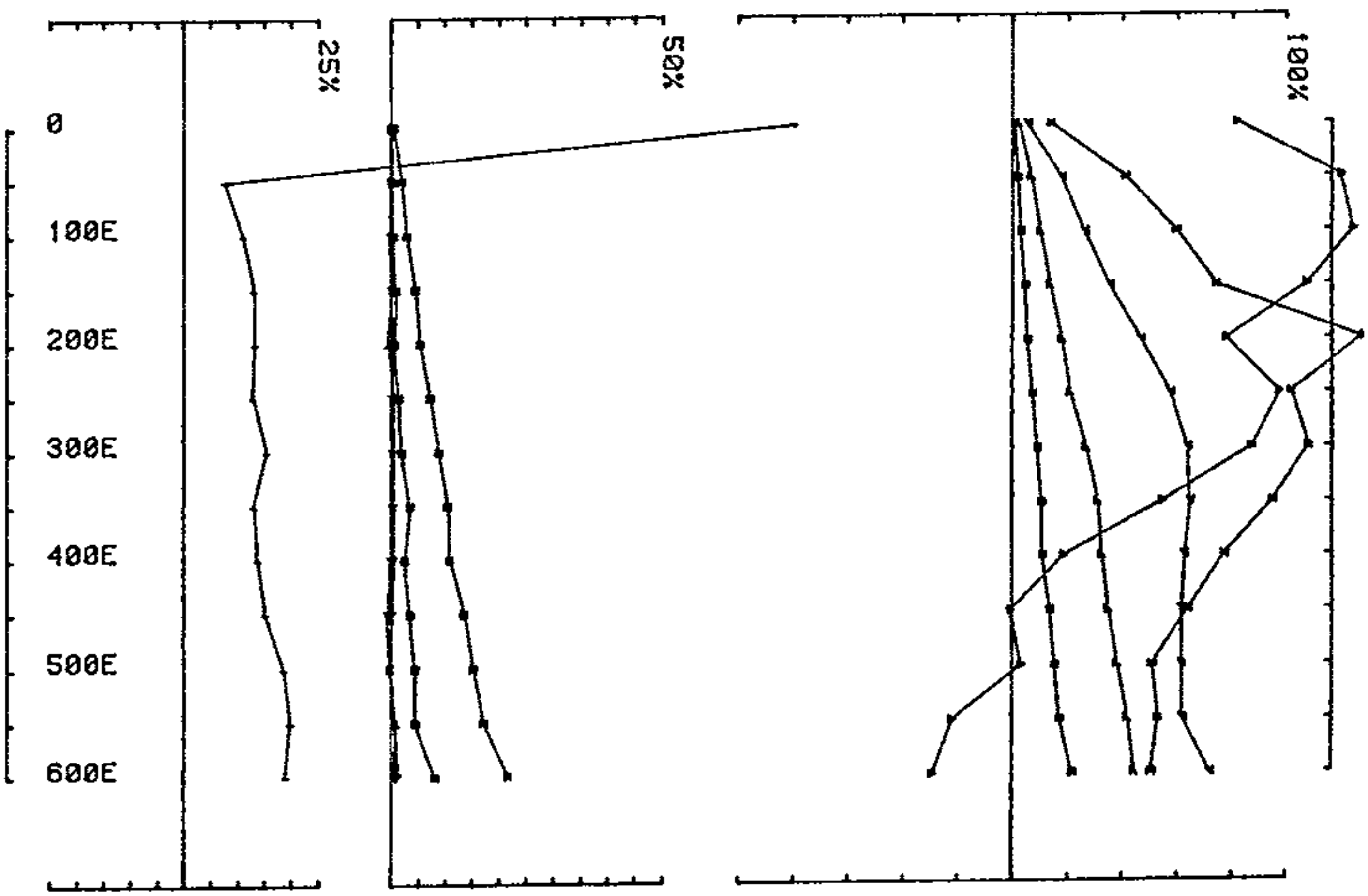

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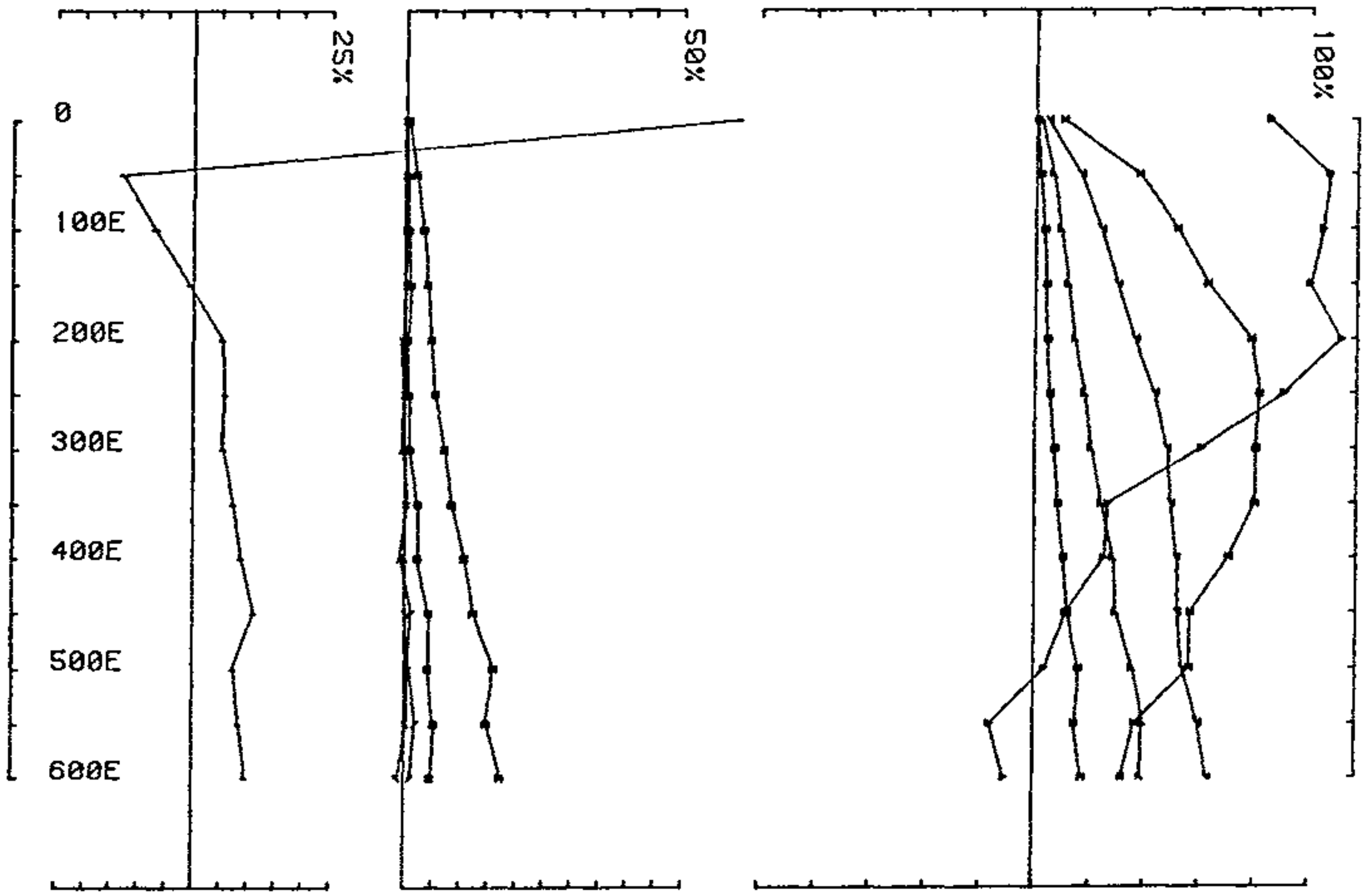

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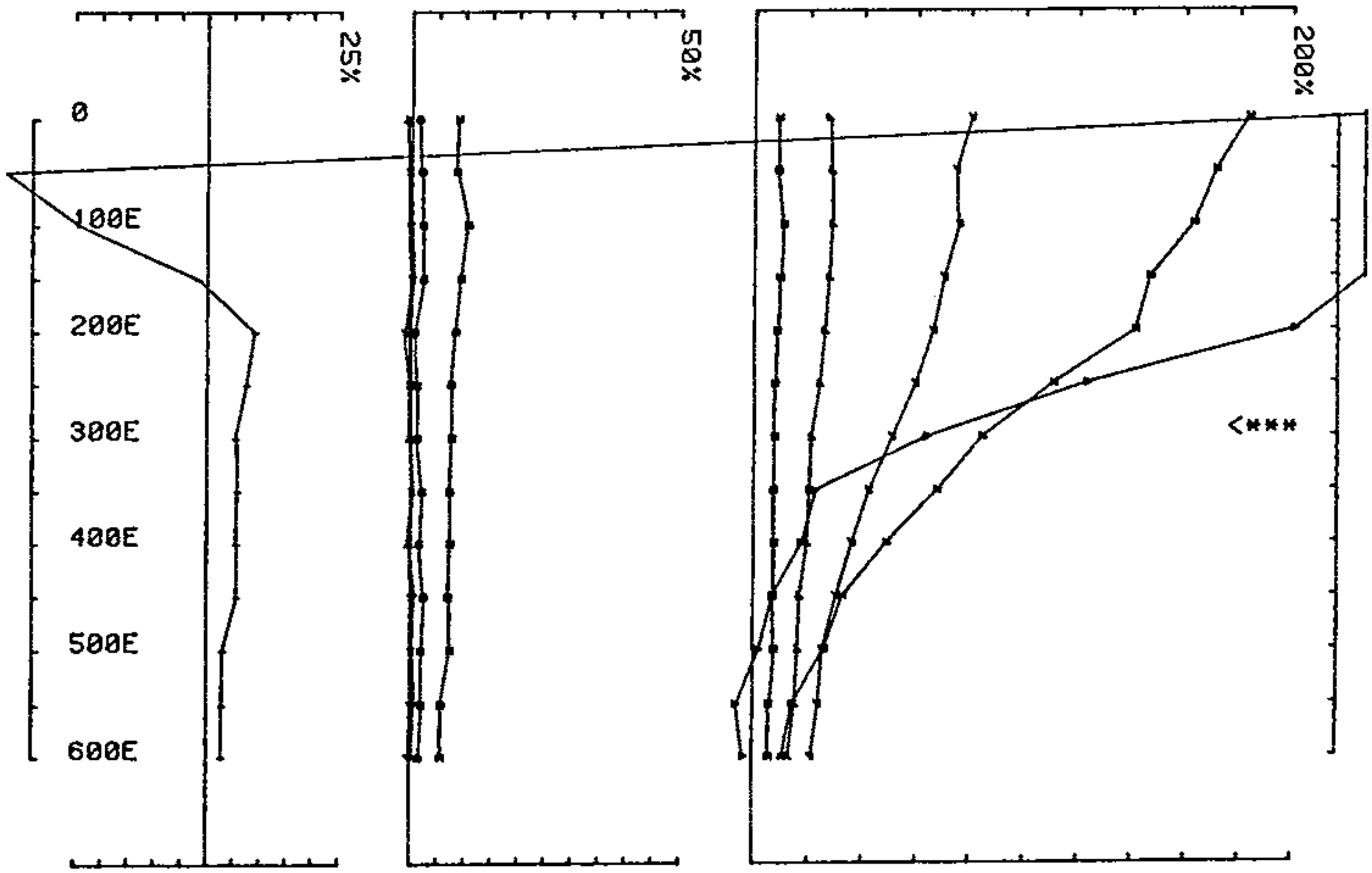

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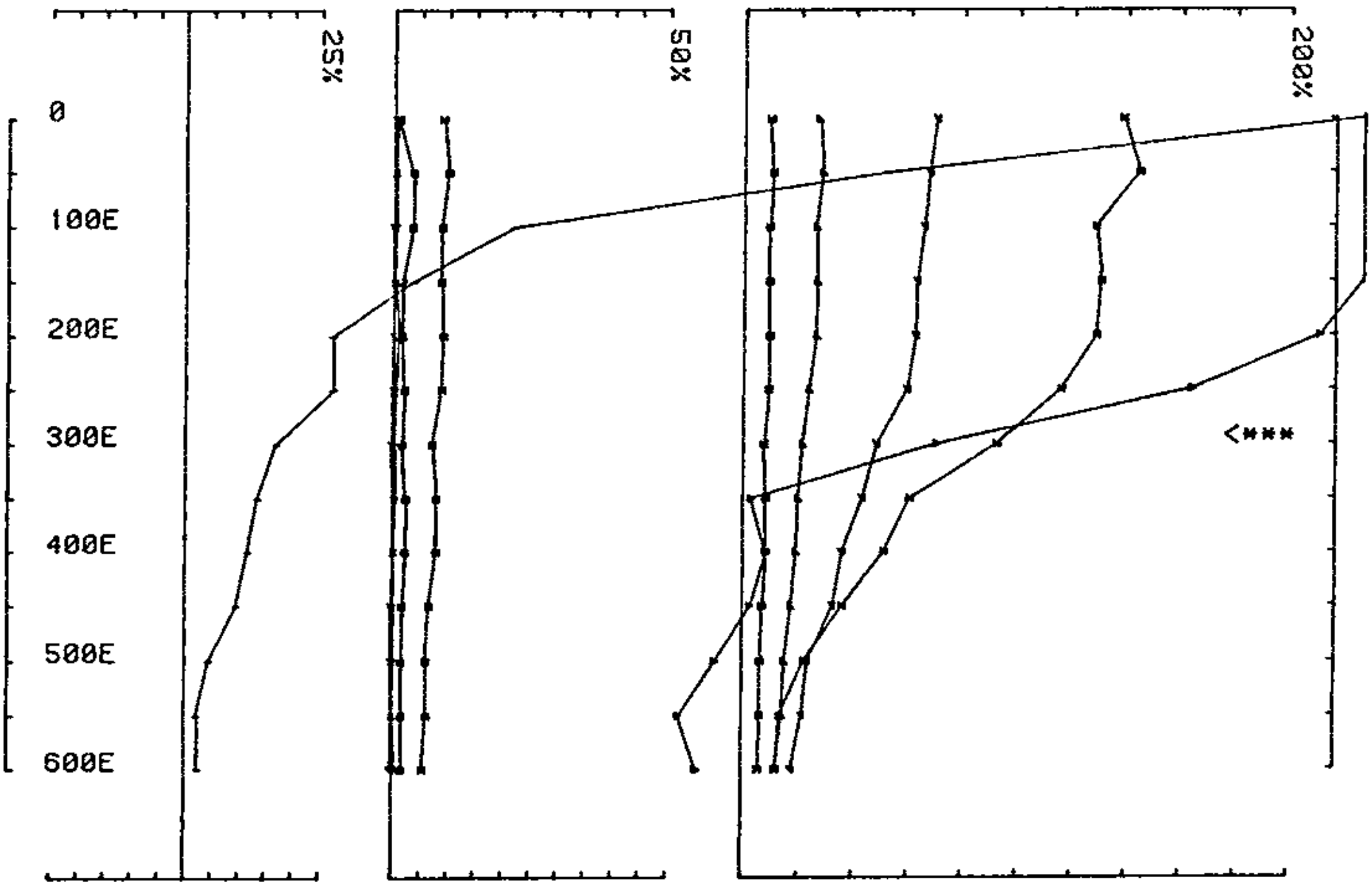

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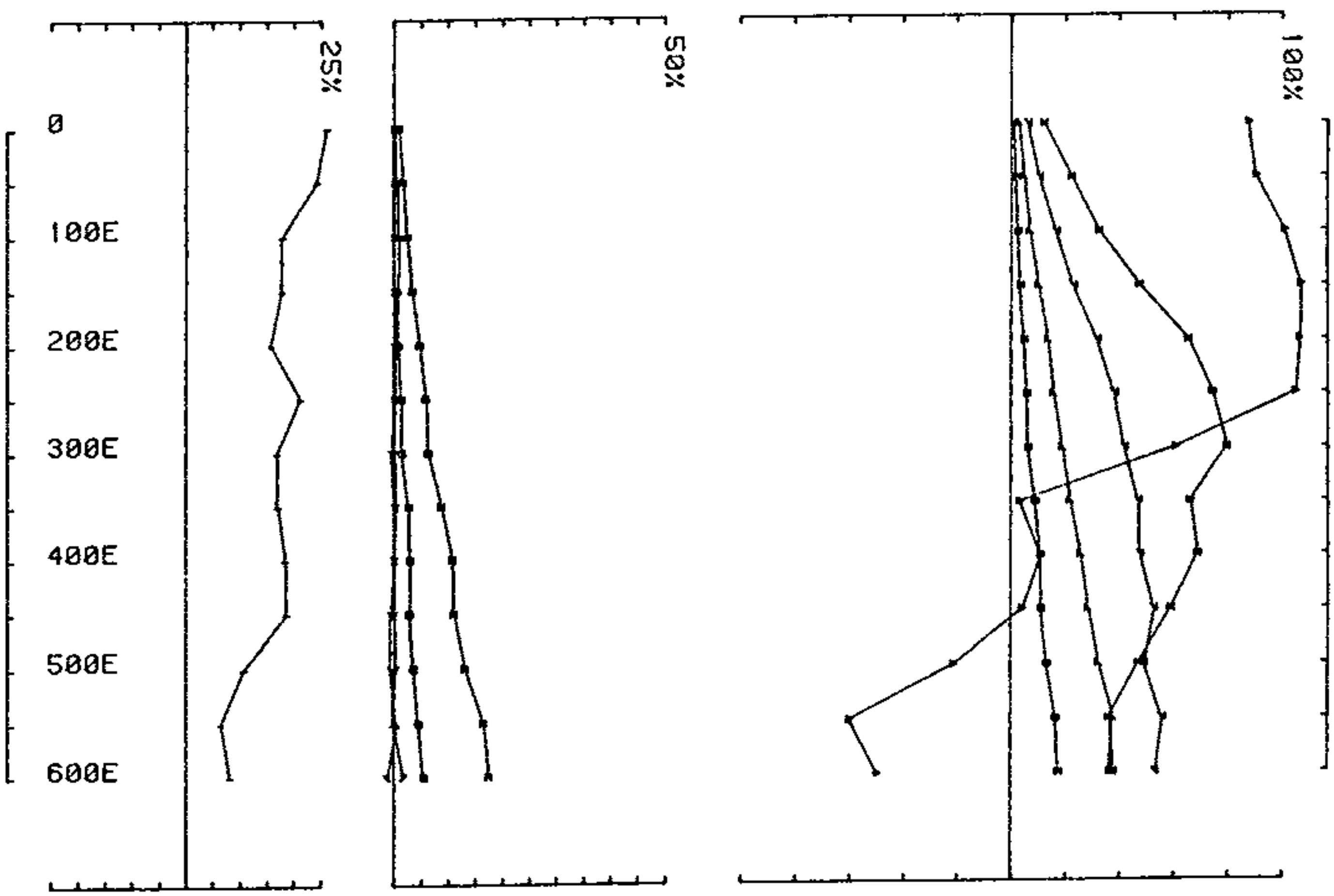

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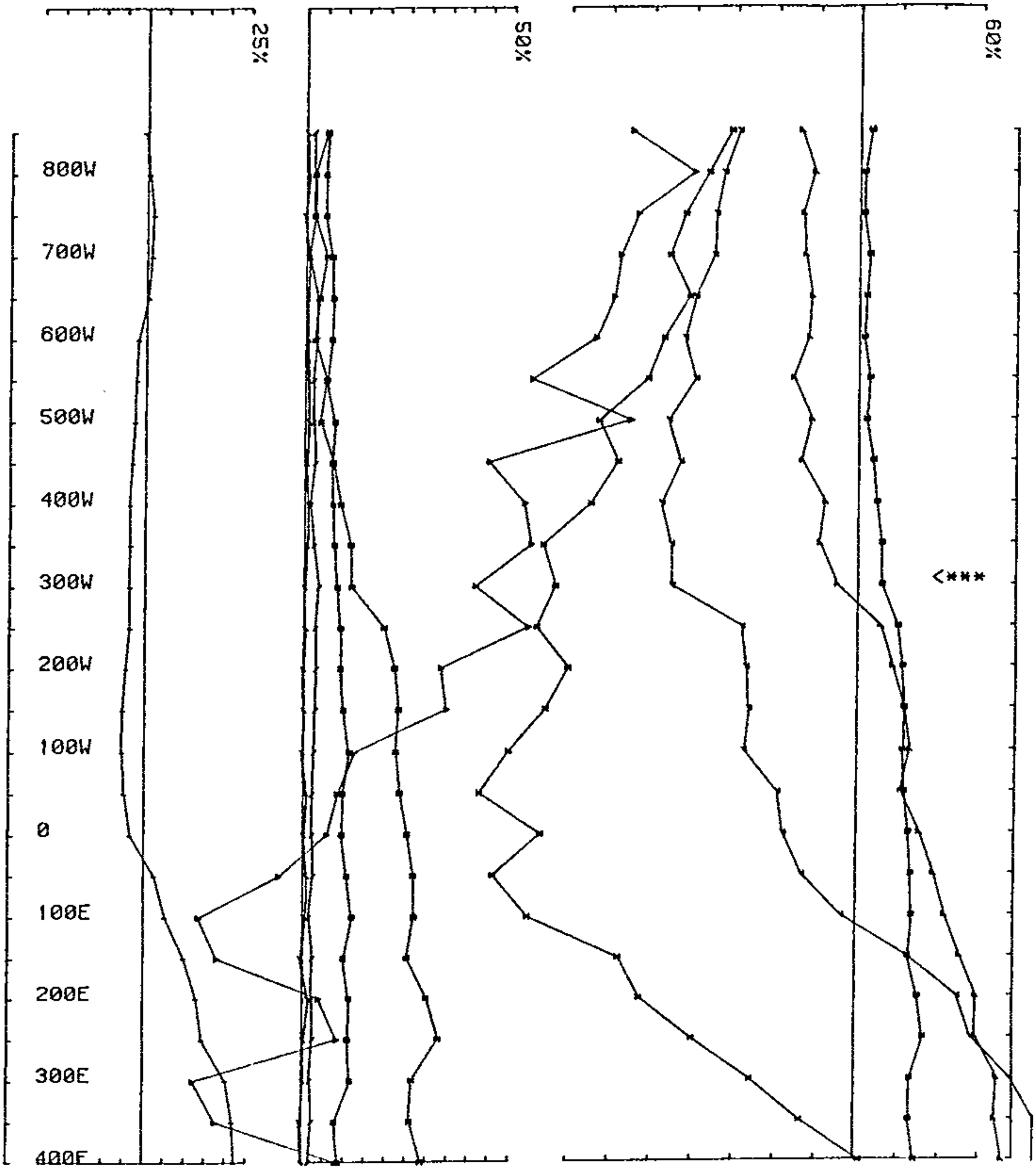

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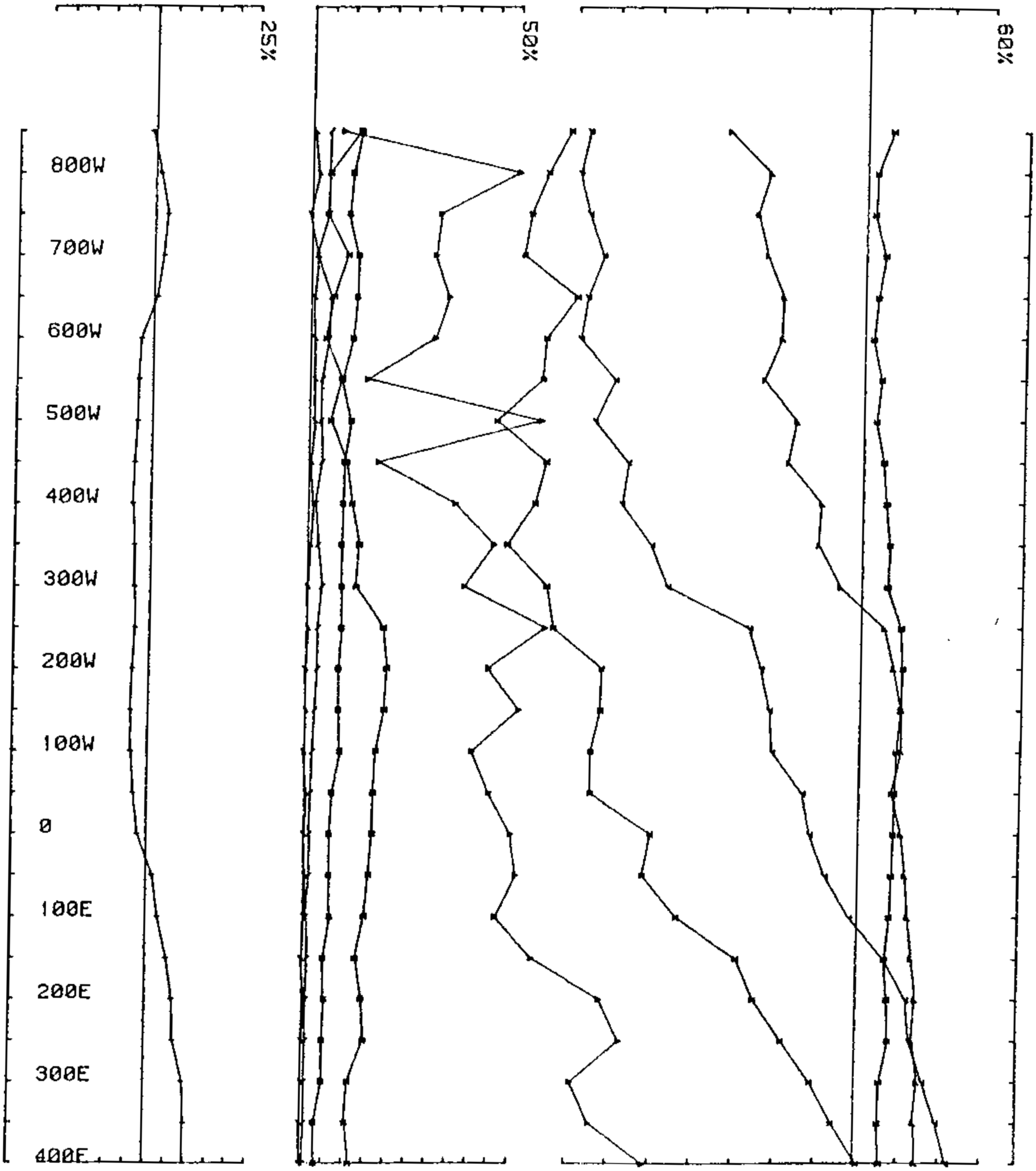

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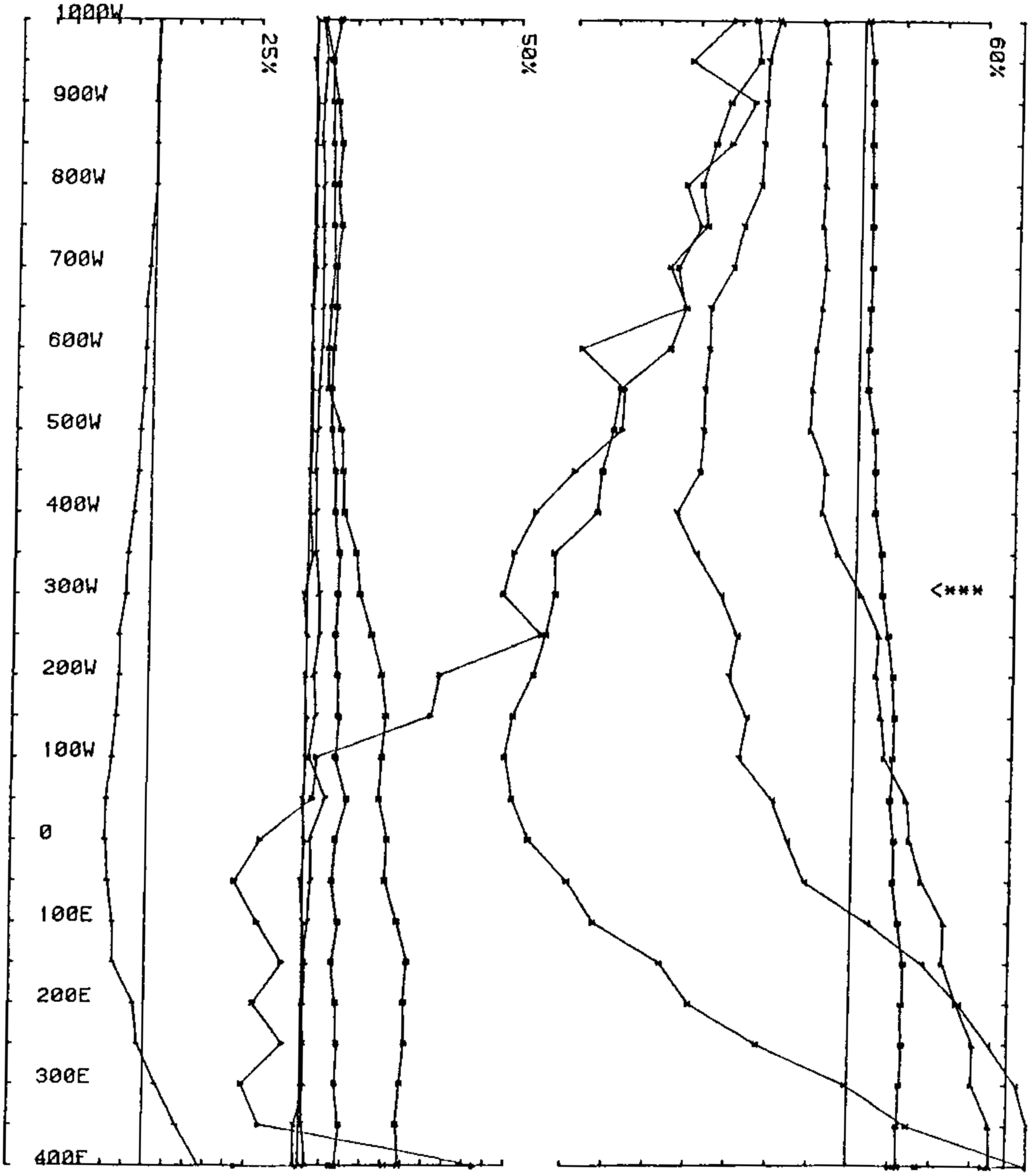

UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
conducted by S.J.V. CONSULTANTS LTD. job 8805 base freq (hz) 30.974
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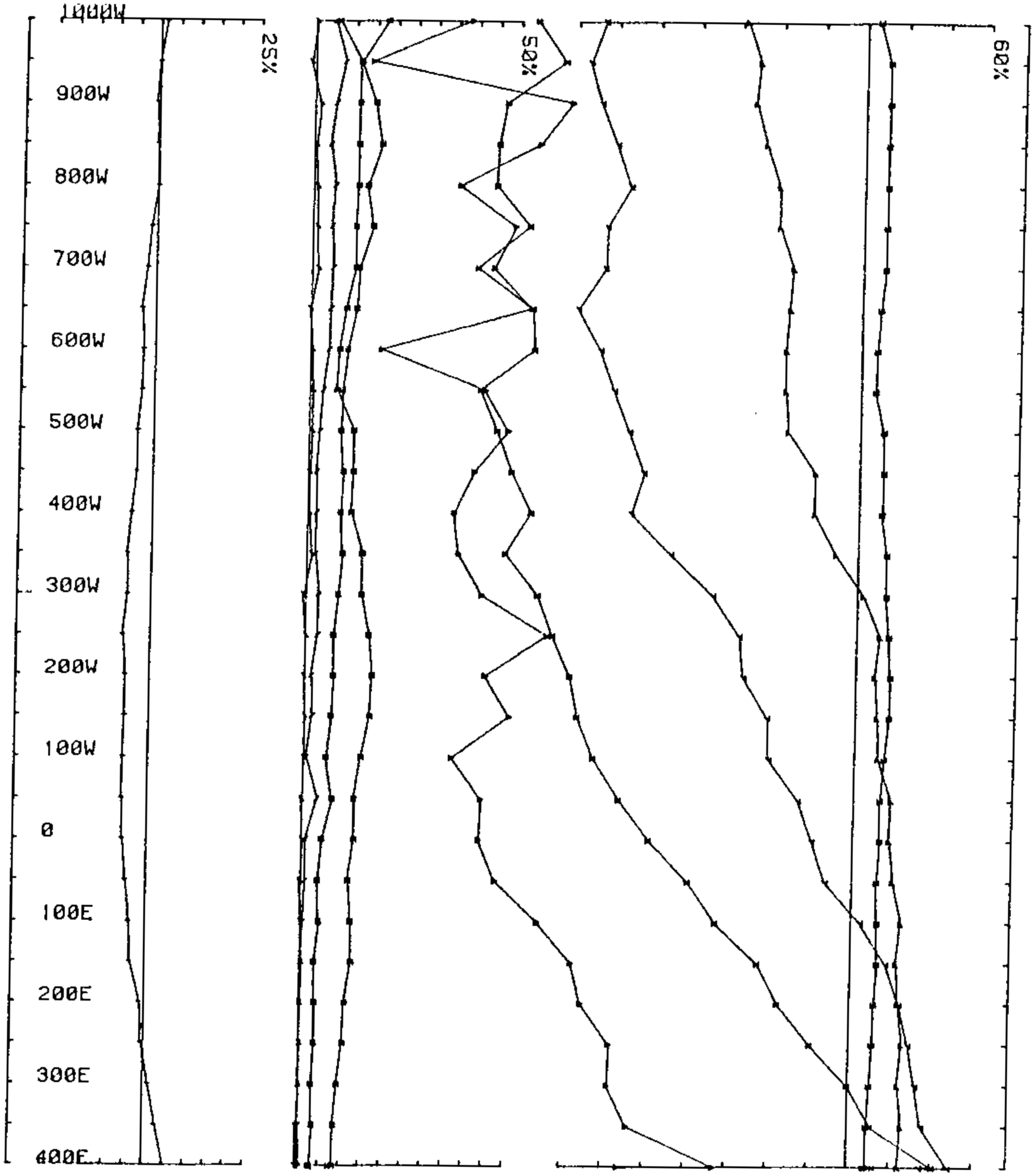

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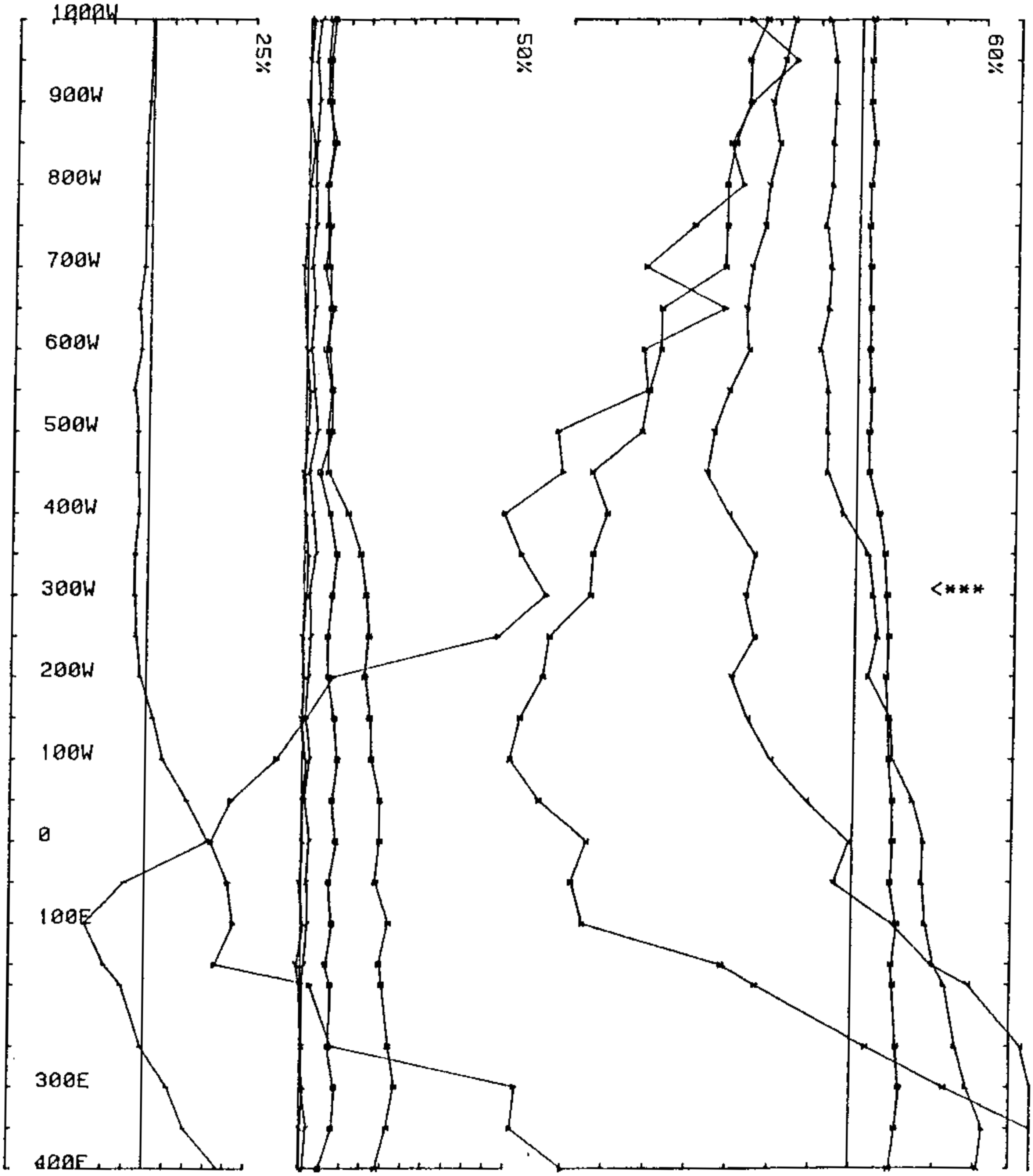

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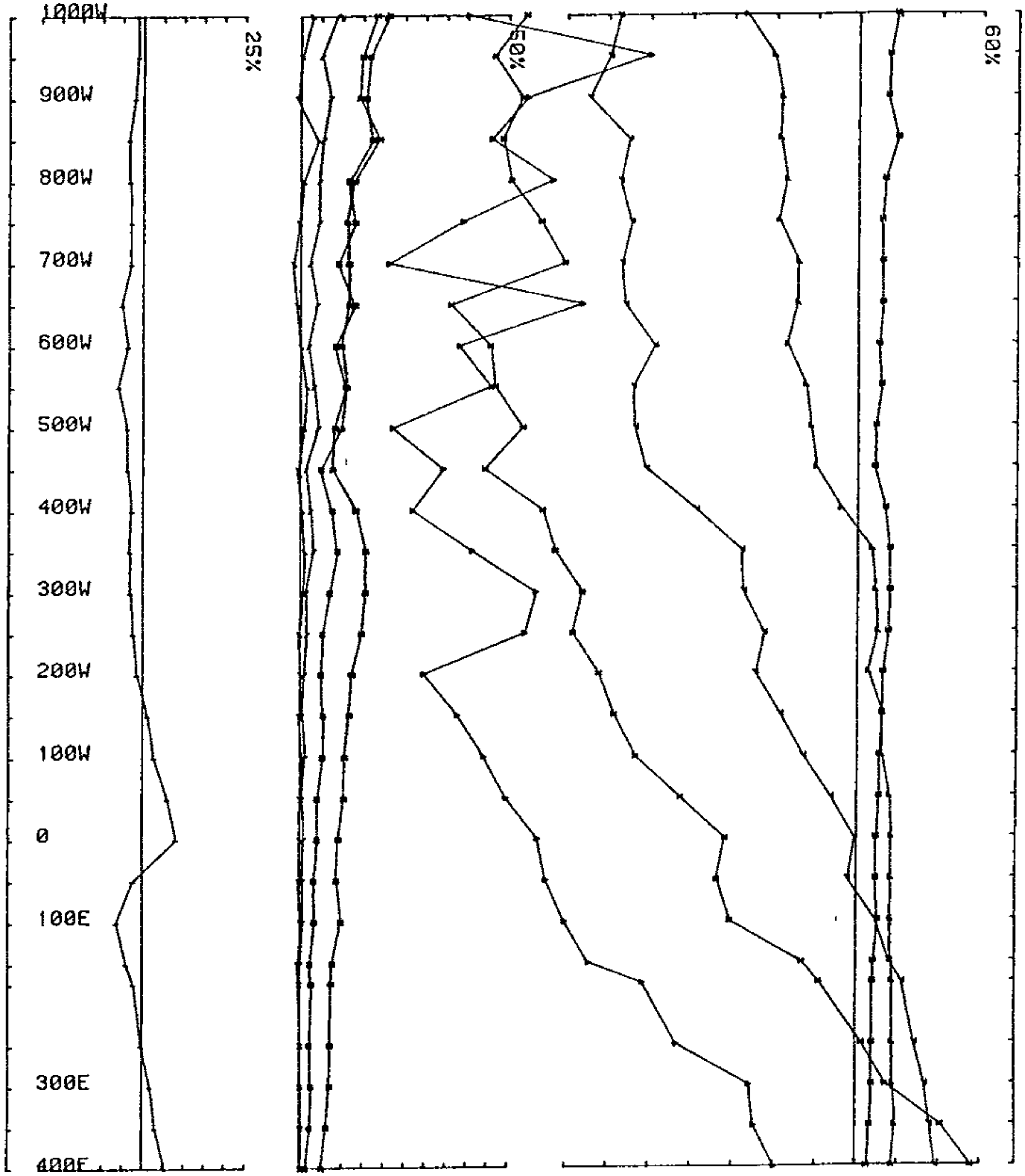

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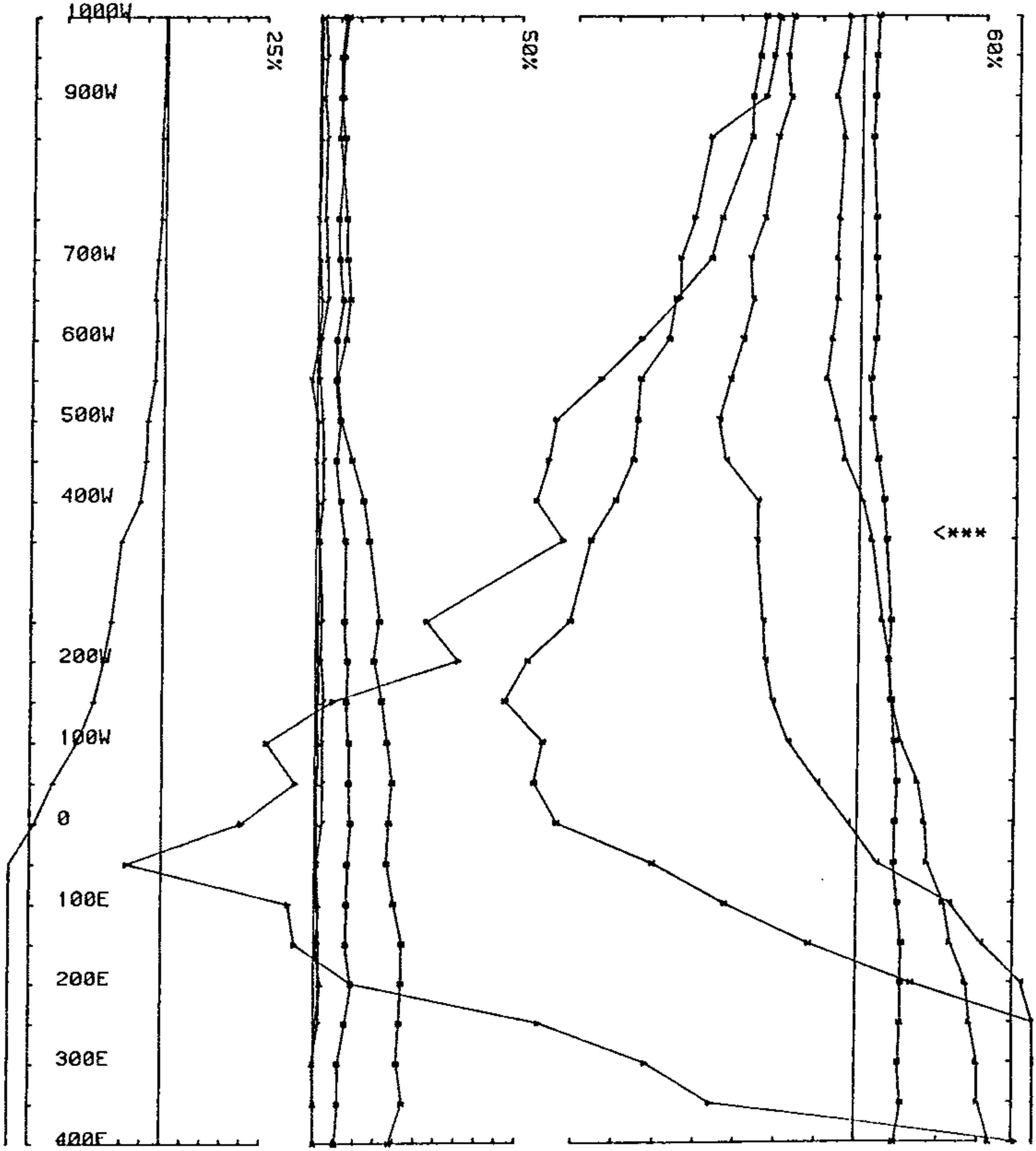

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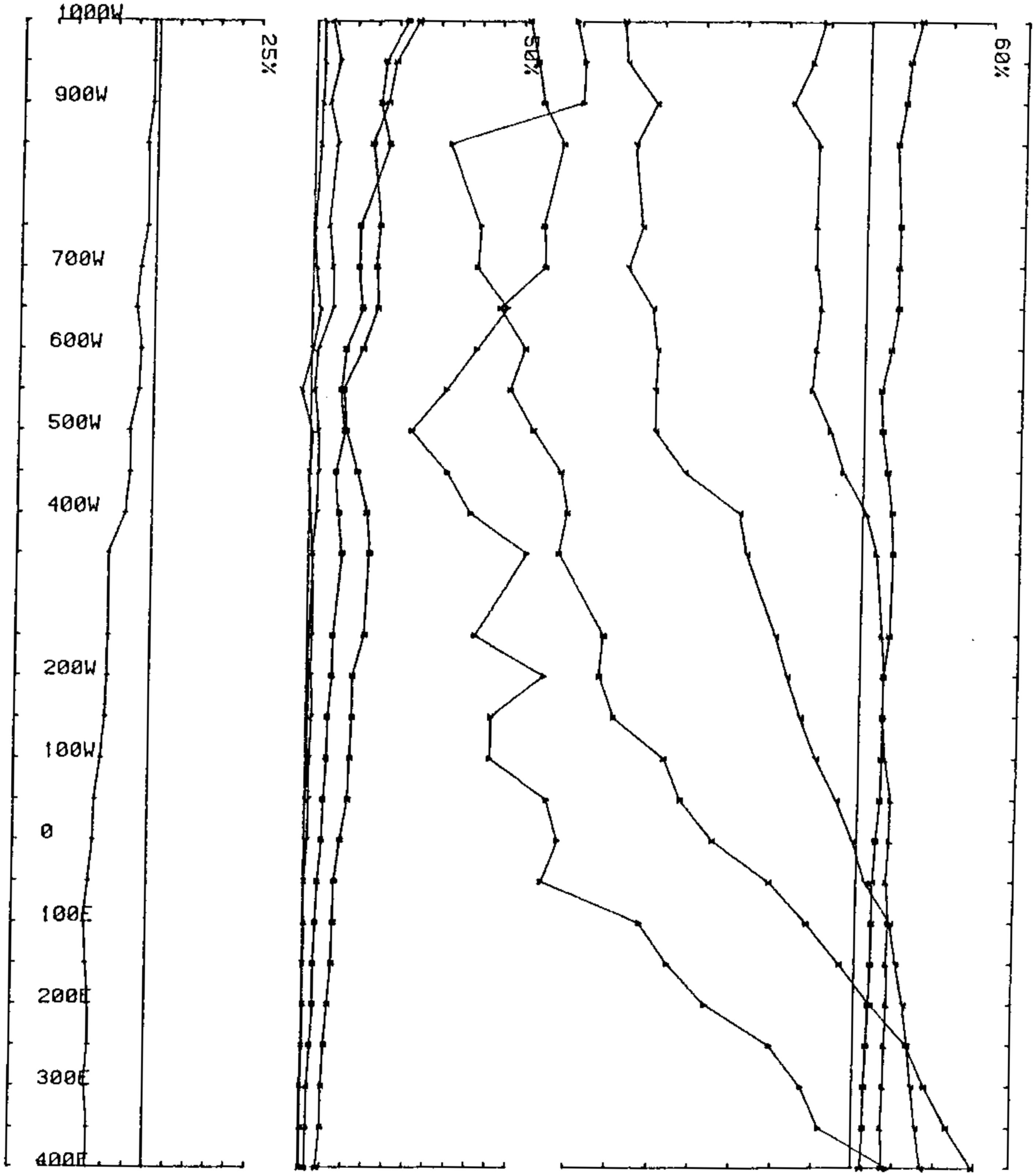

UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.

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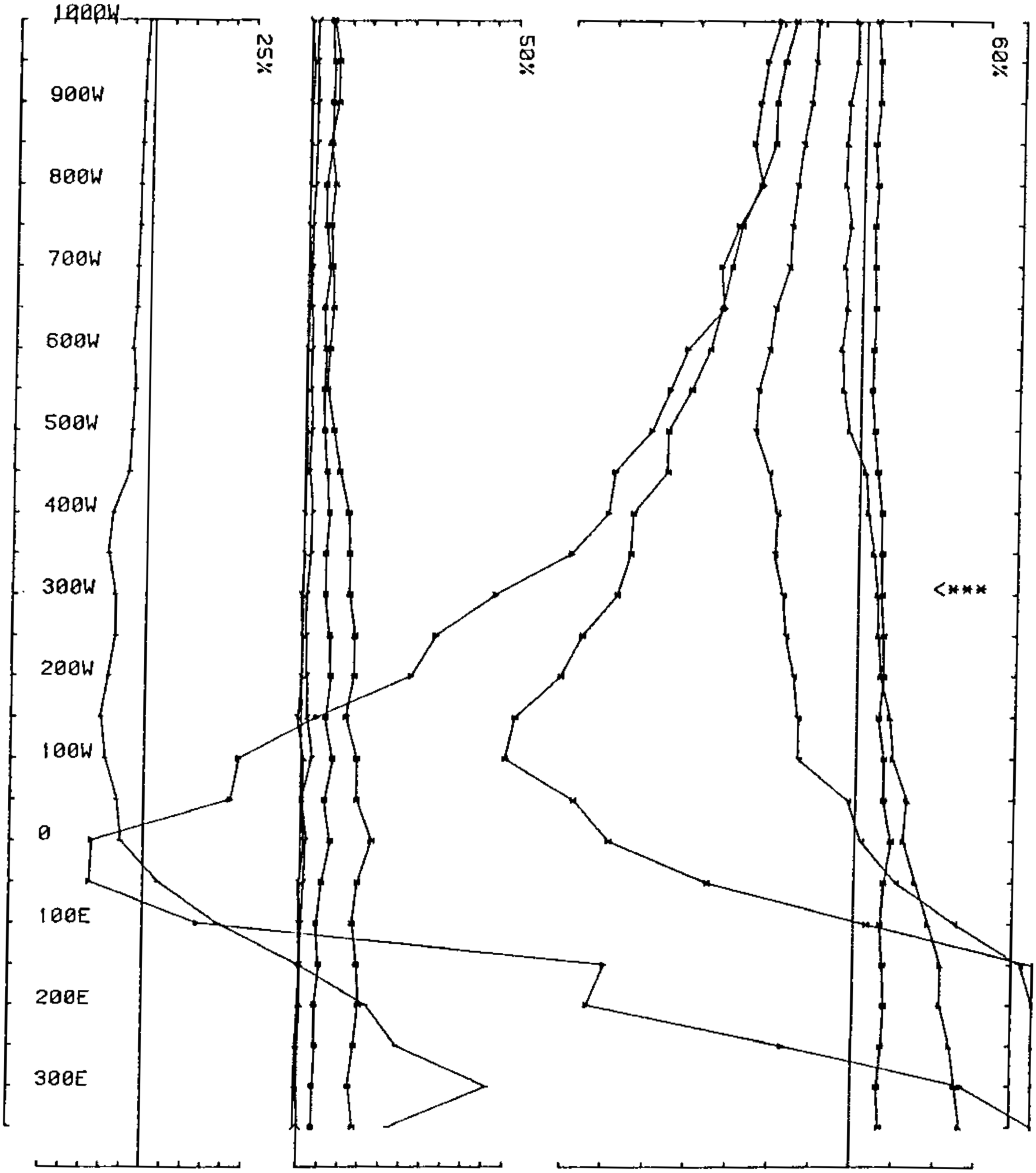

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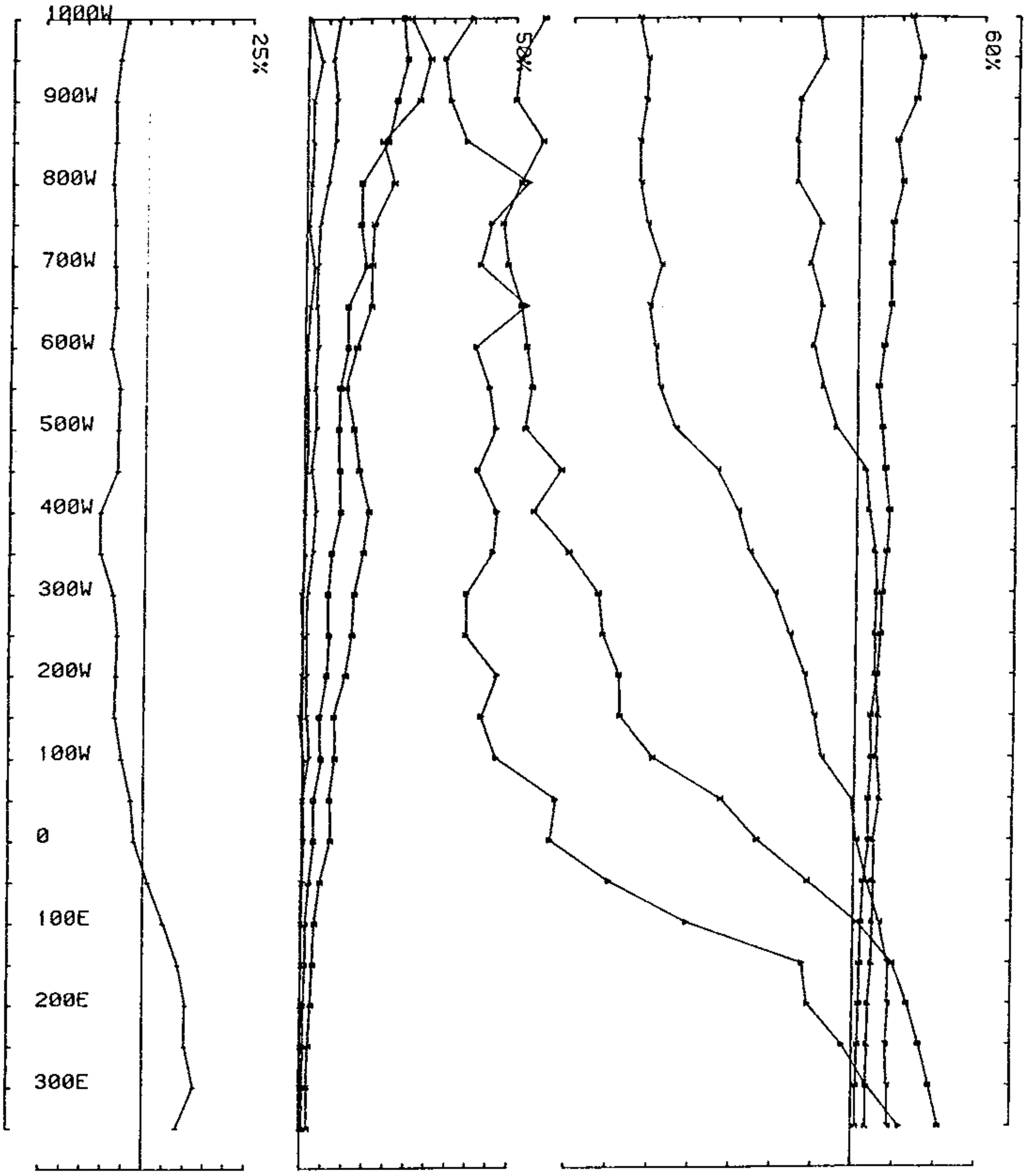

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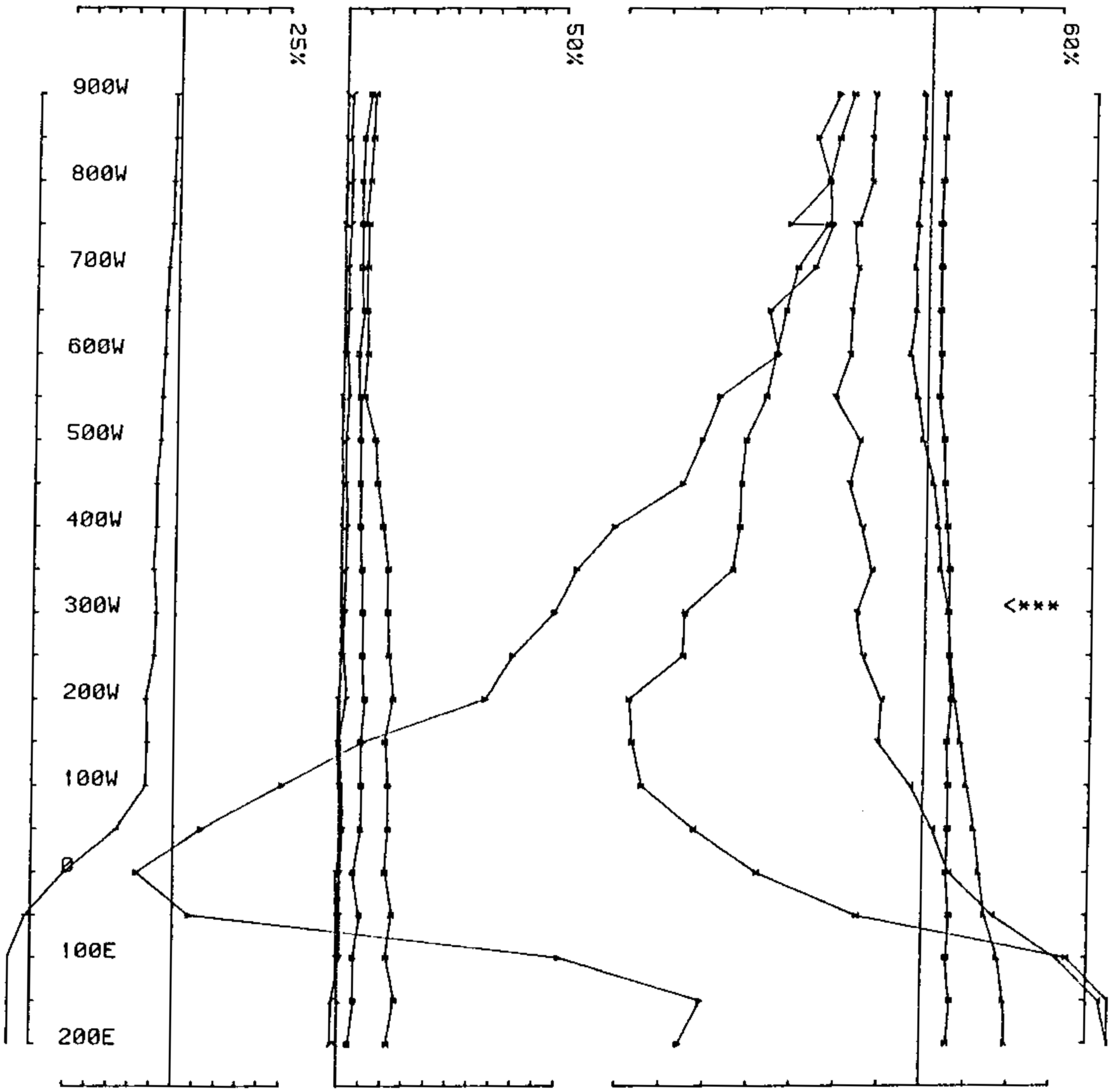

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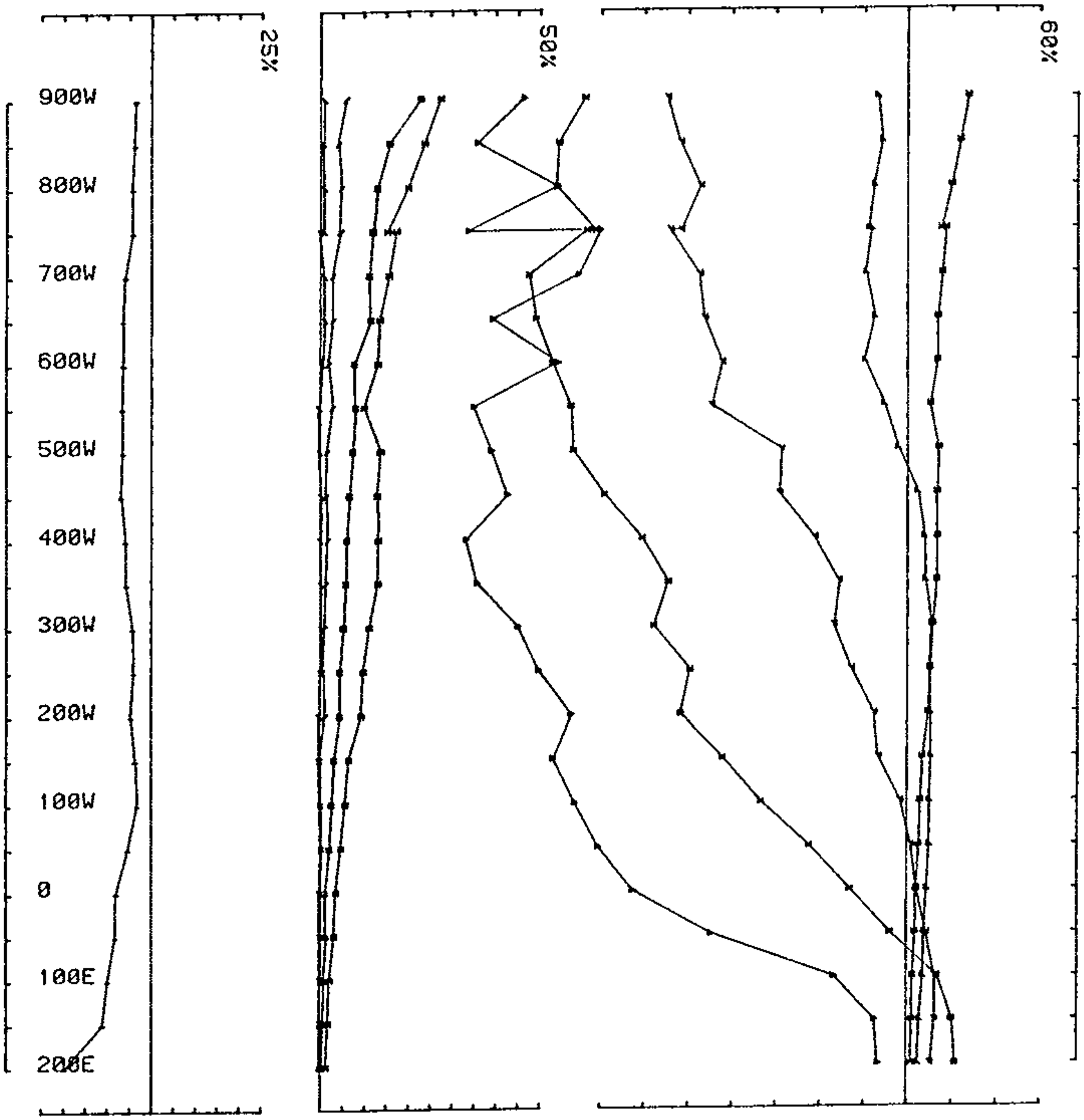

UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
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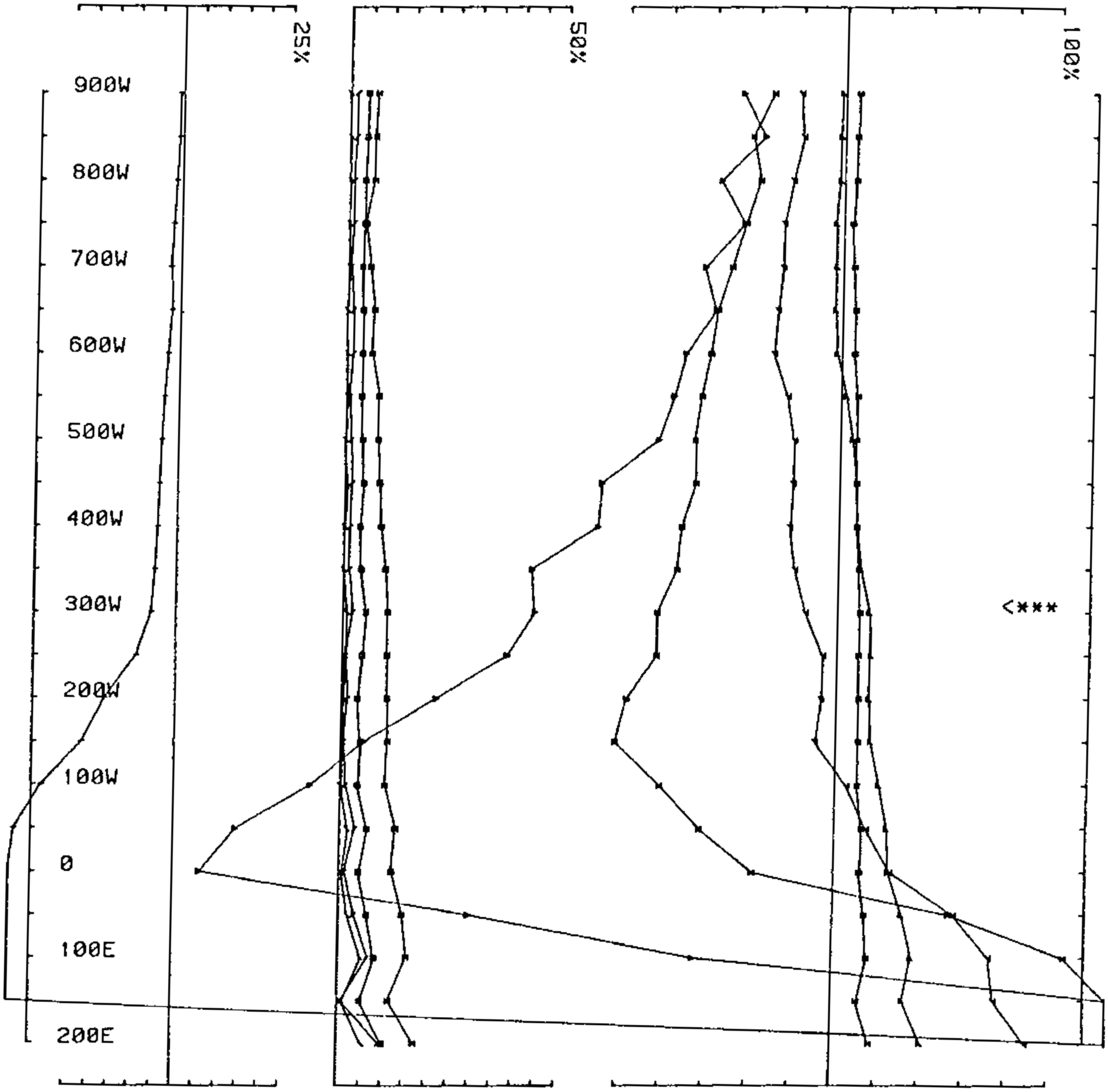

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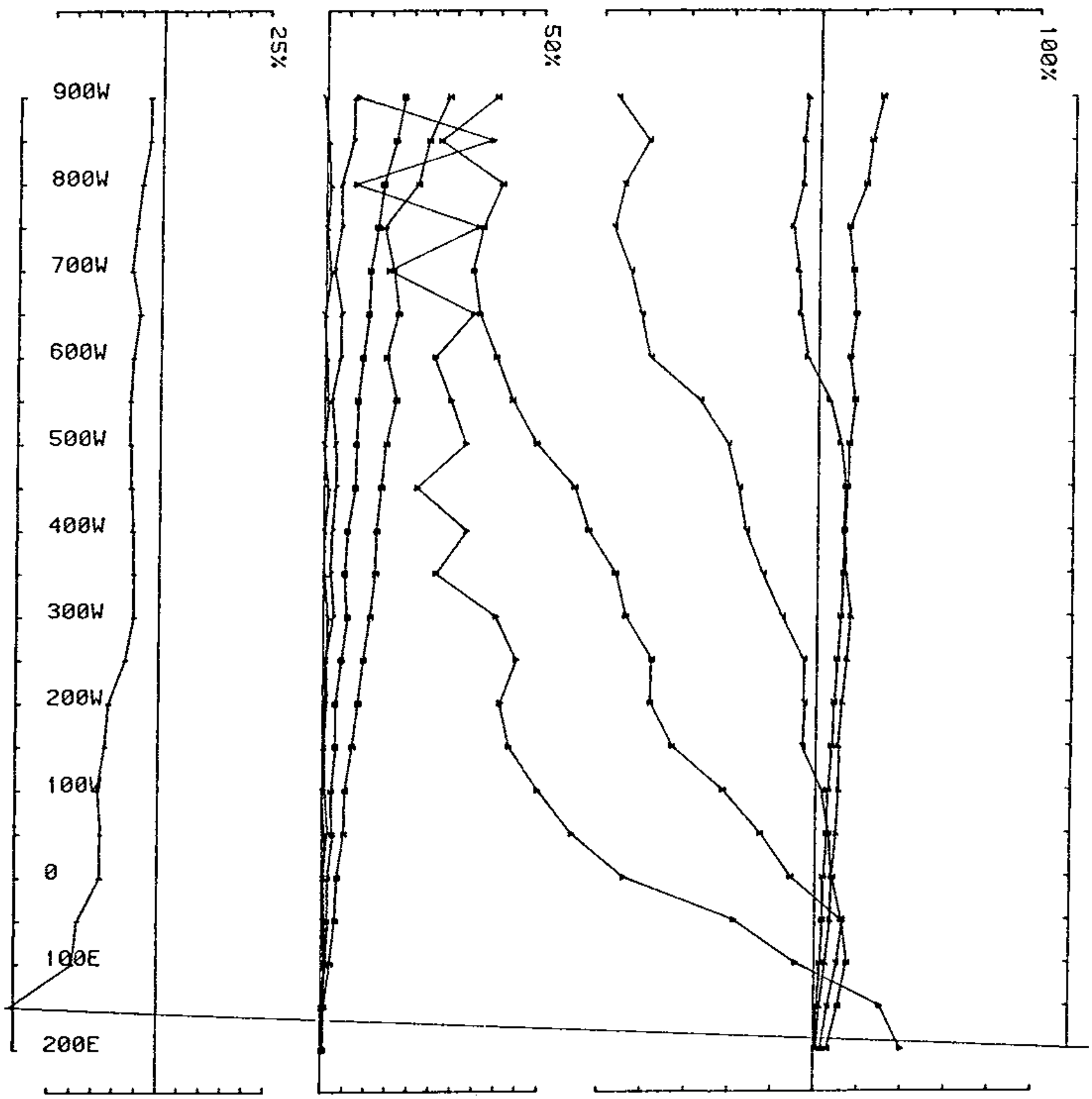

UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
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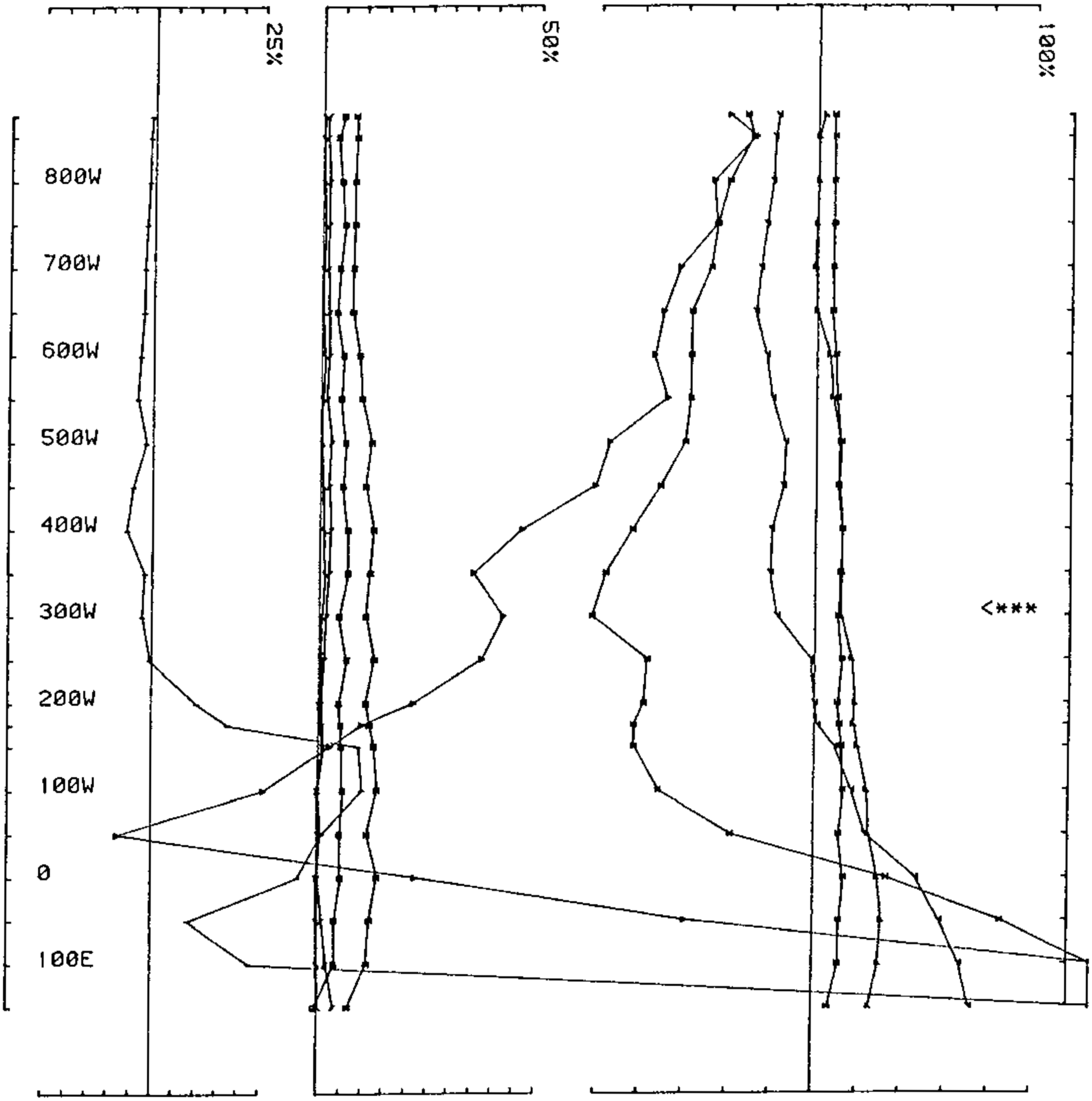

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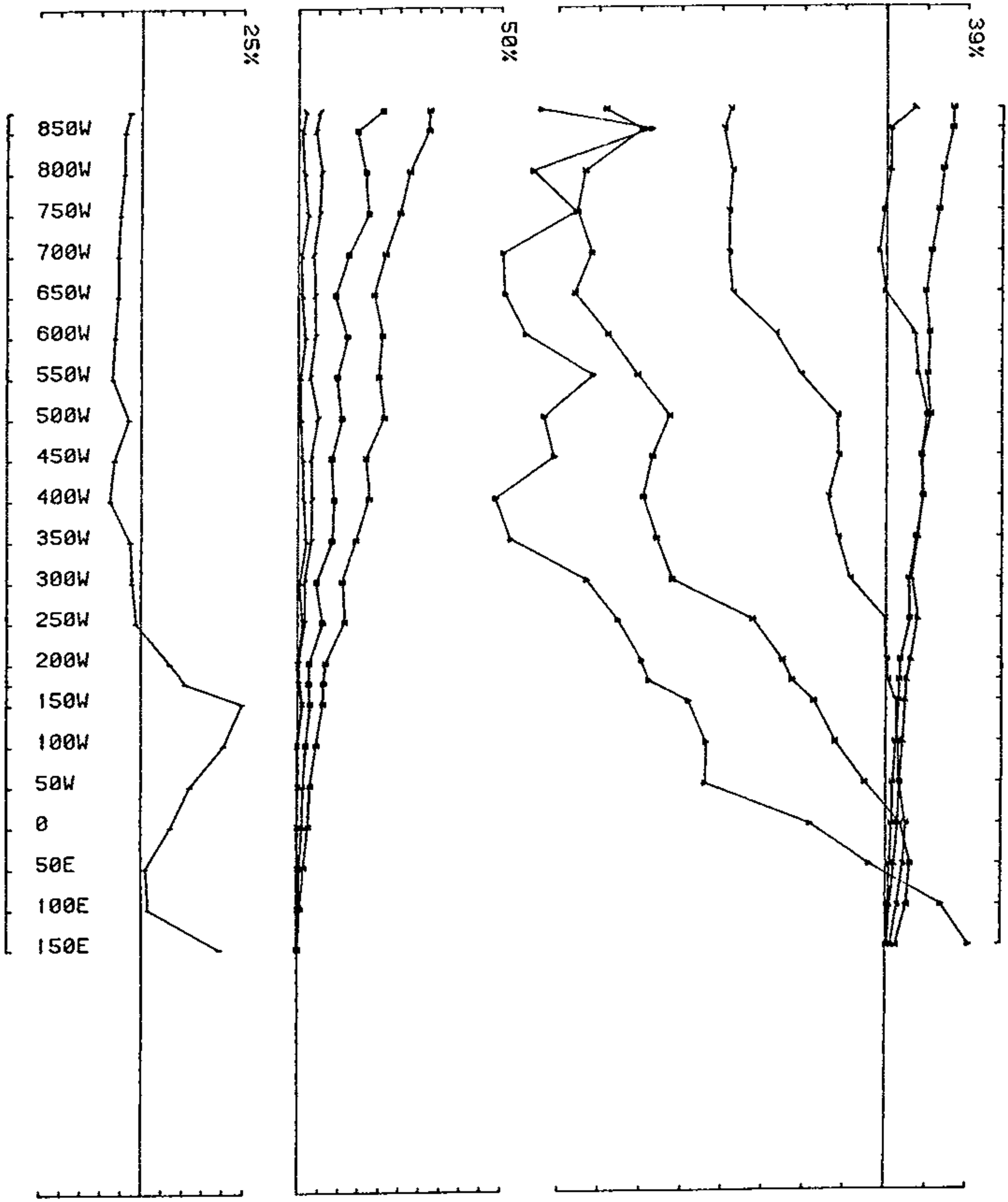
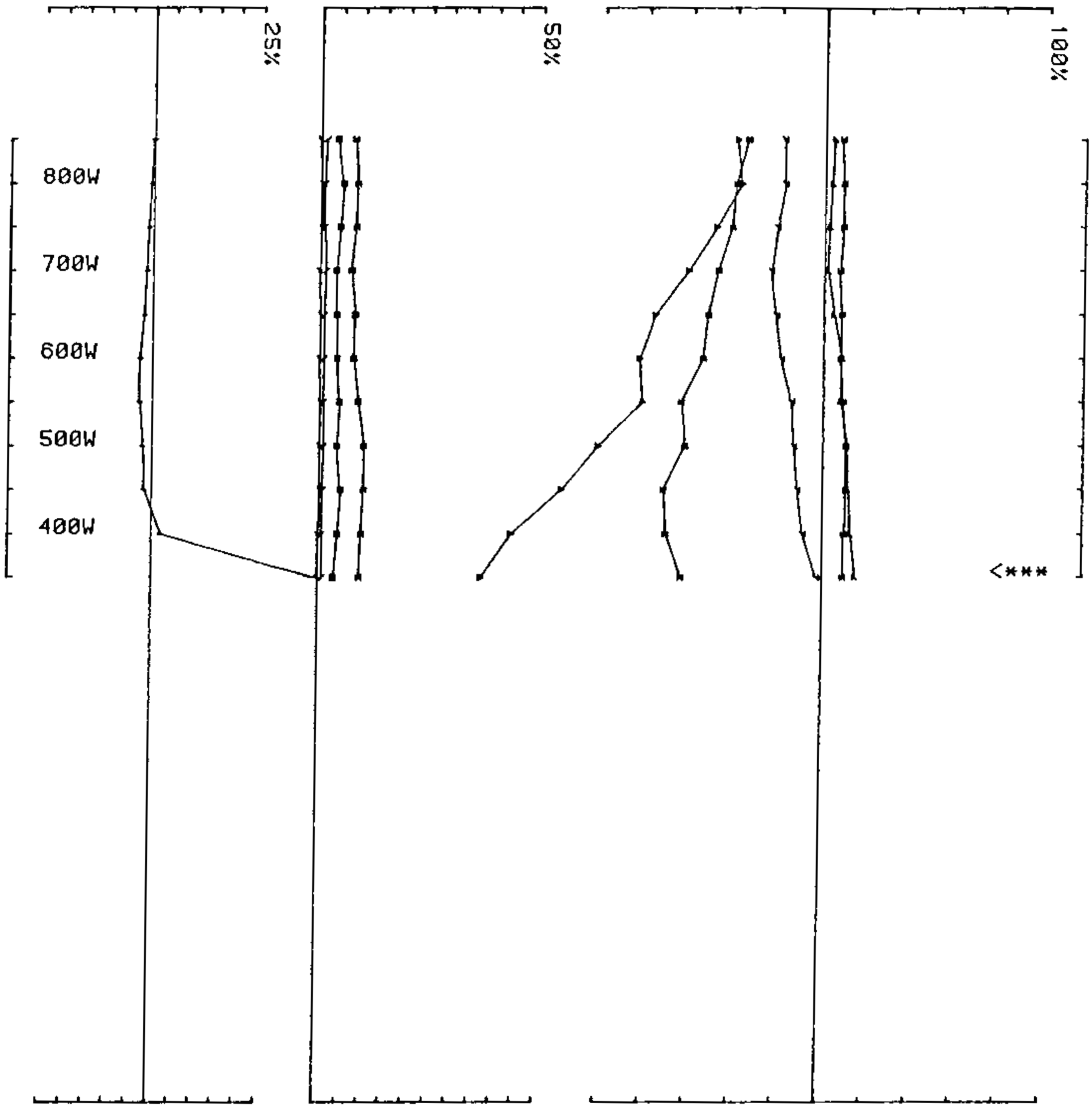


UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.

conducted by S.J.V. CONSULTANTS LTD. Job 8805 base freq (hz) 30.974 Y

loop no 2 line 700N component Hz secondary field Ch I contin. norm.



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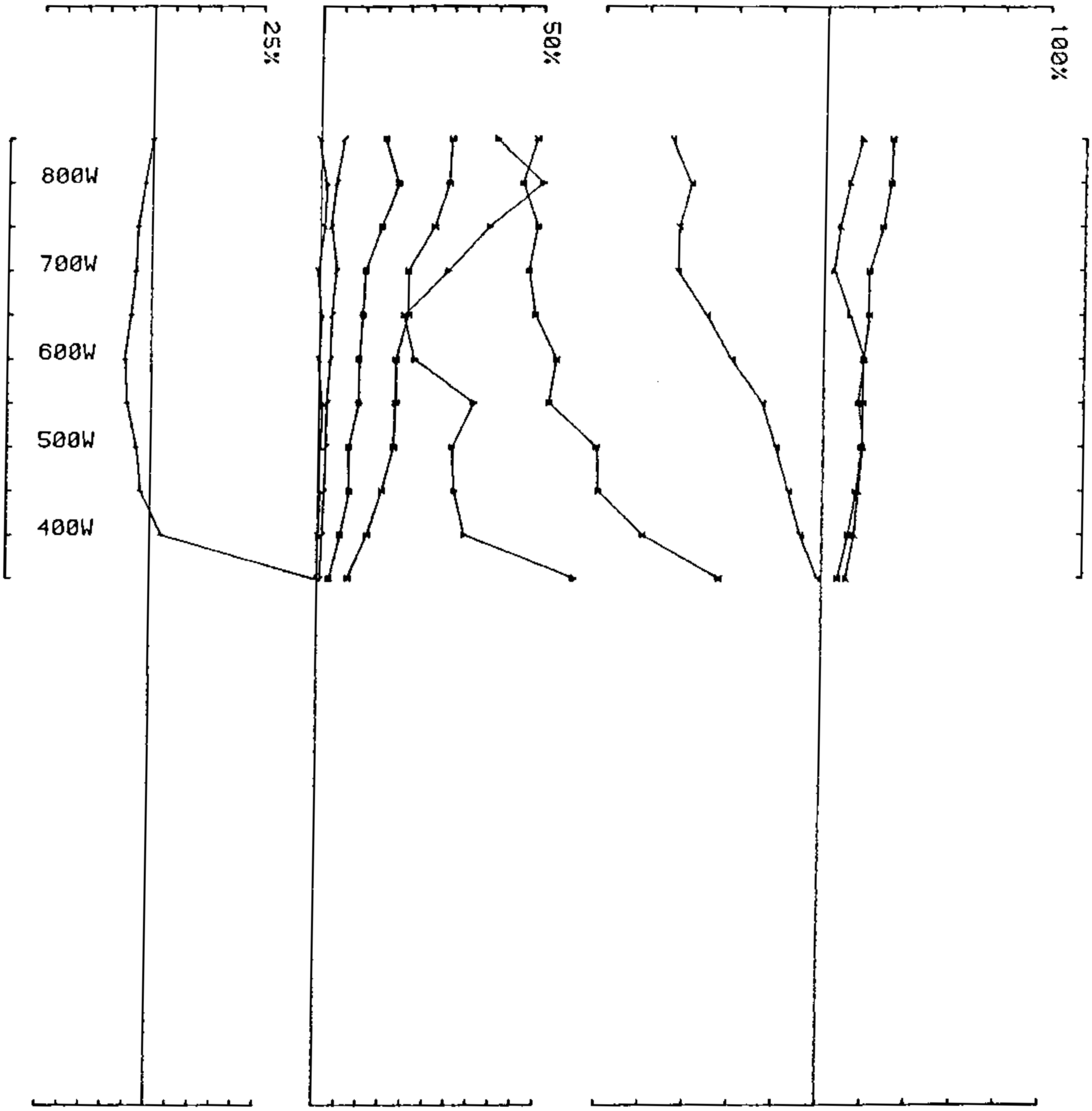

UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
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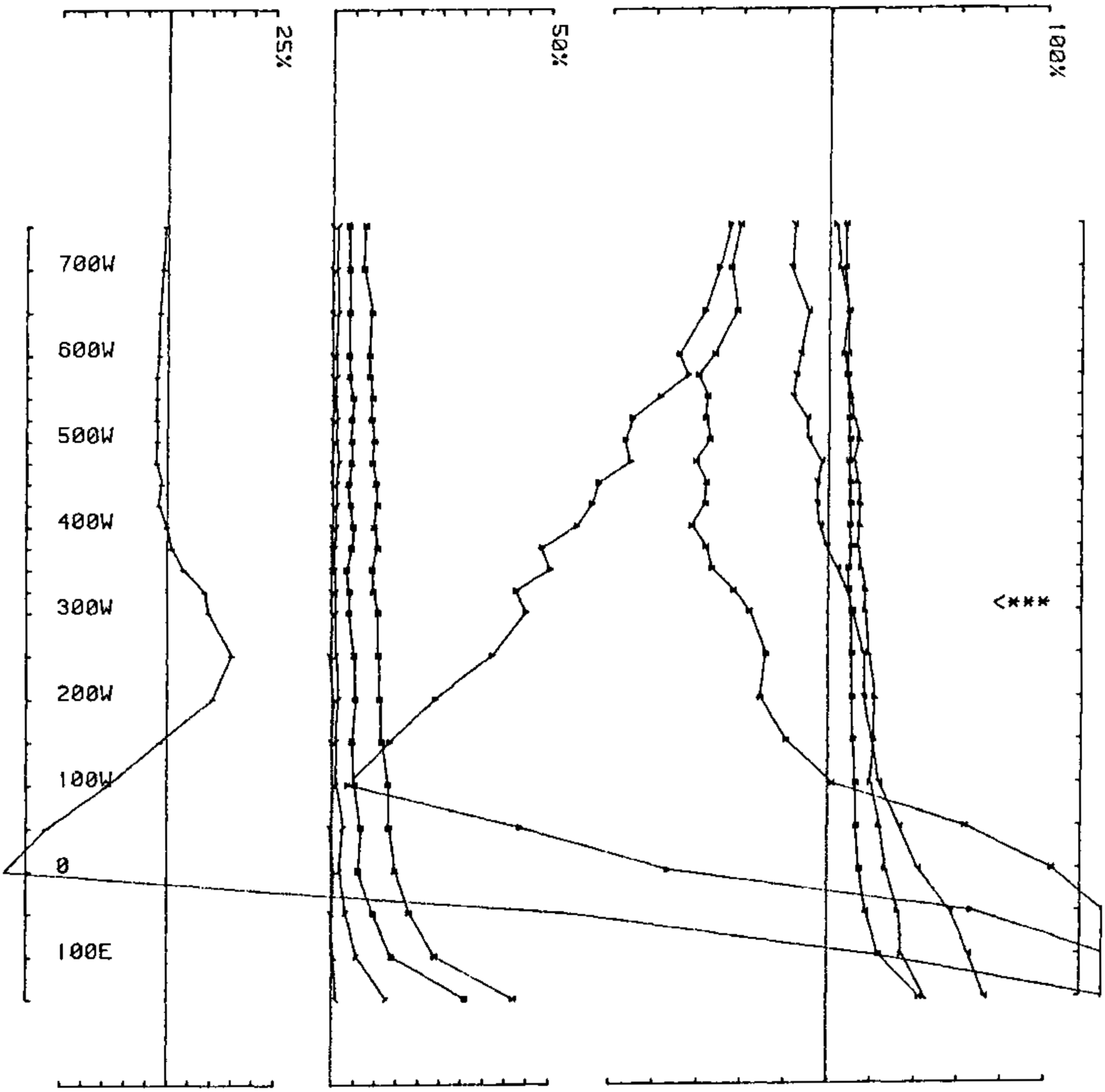

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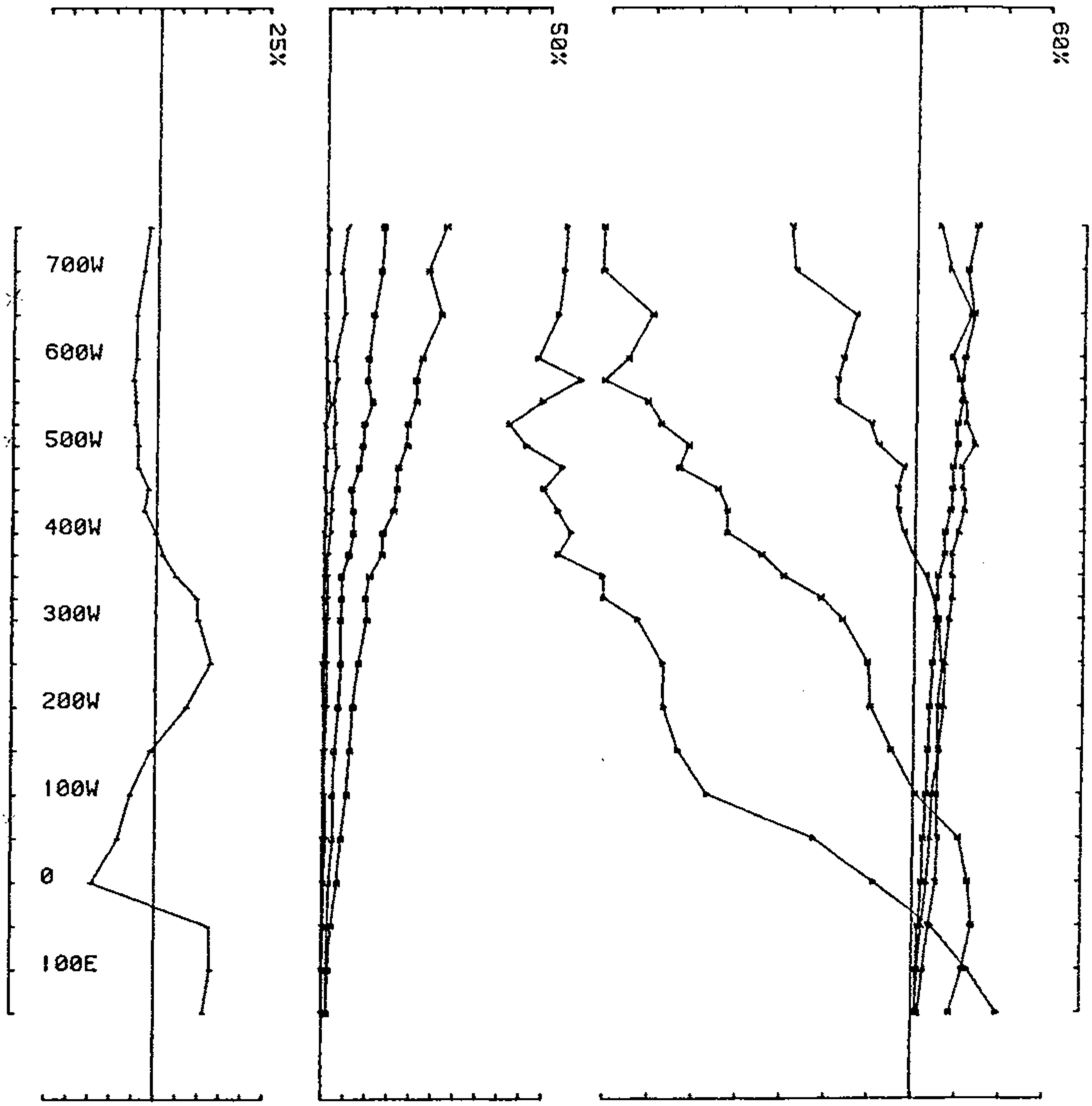

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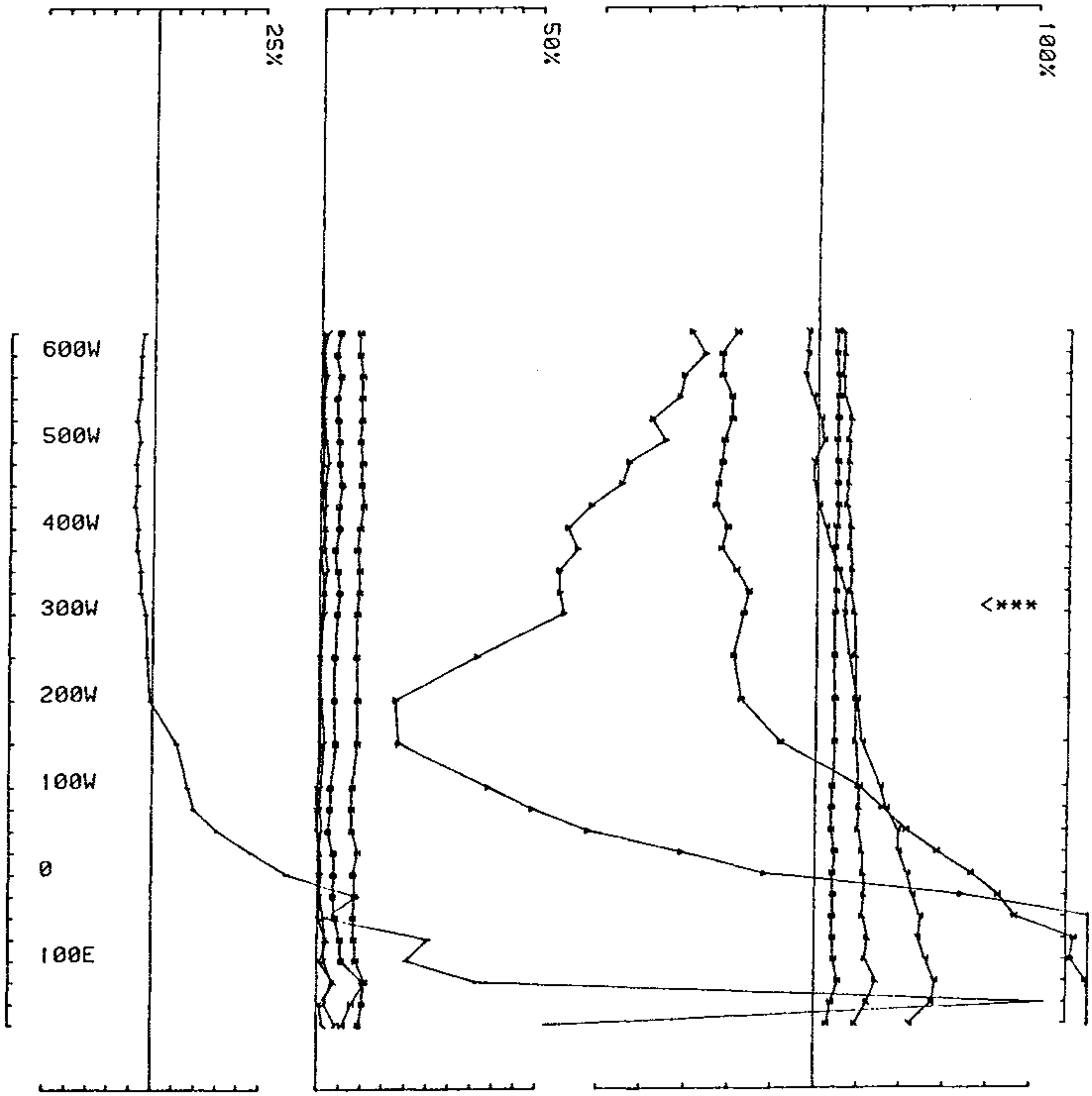

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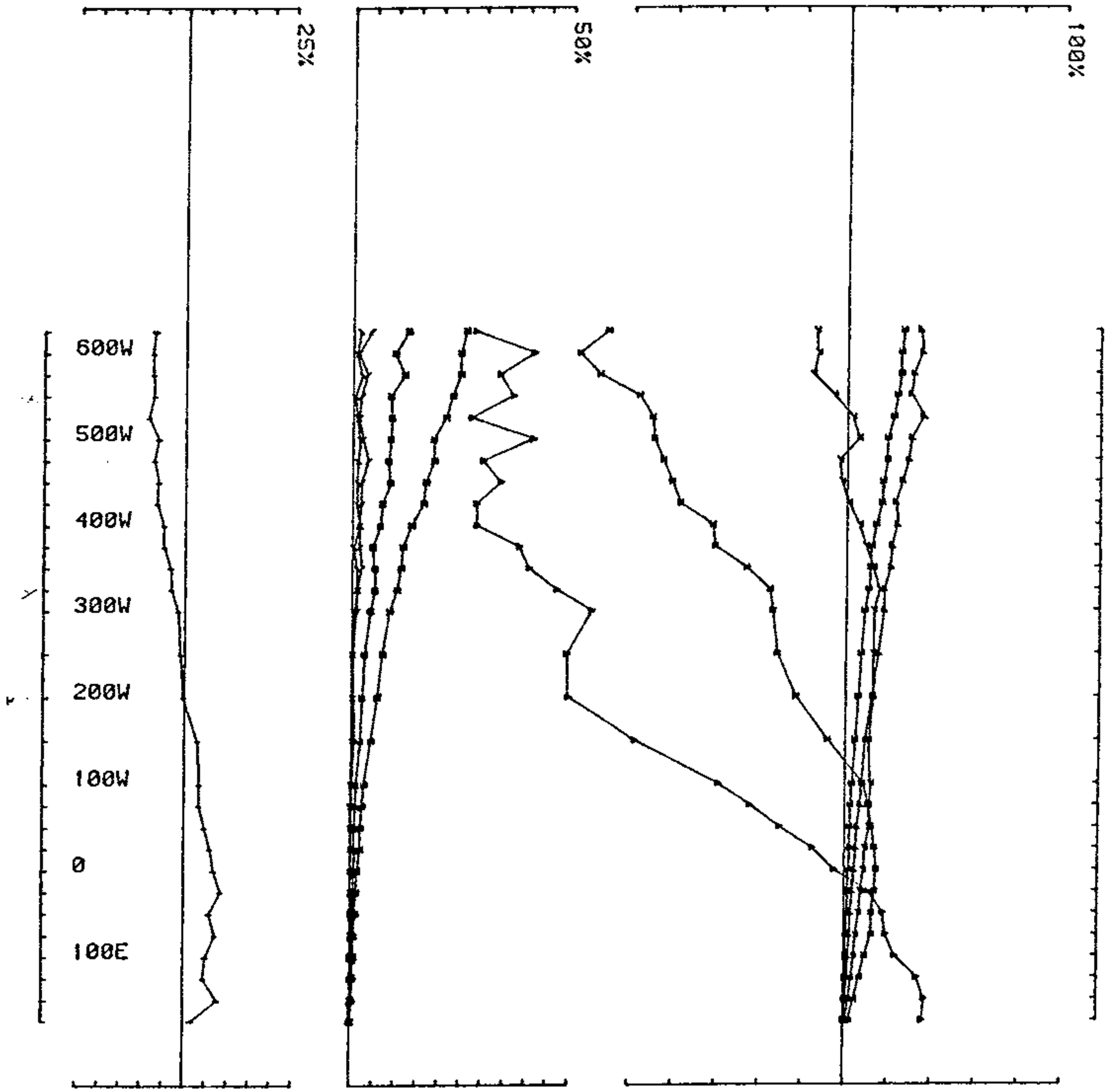

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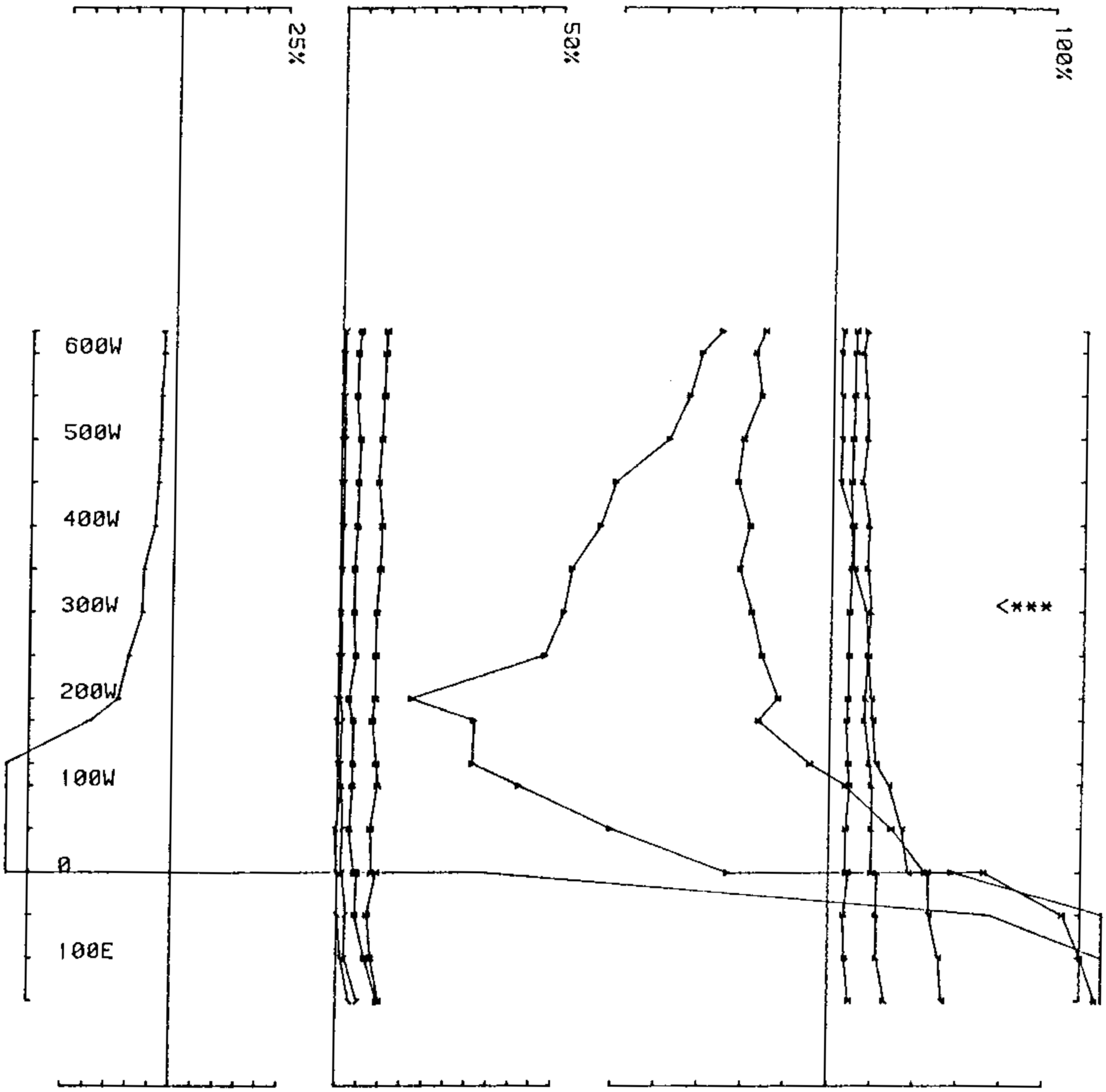

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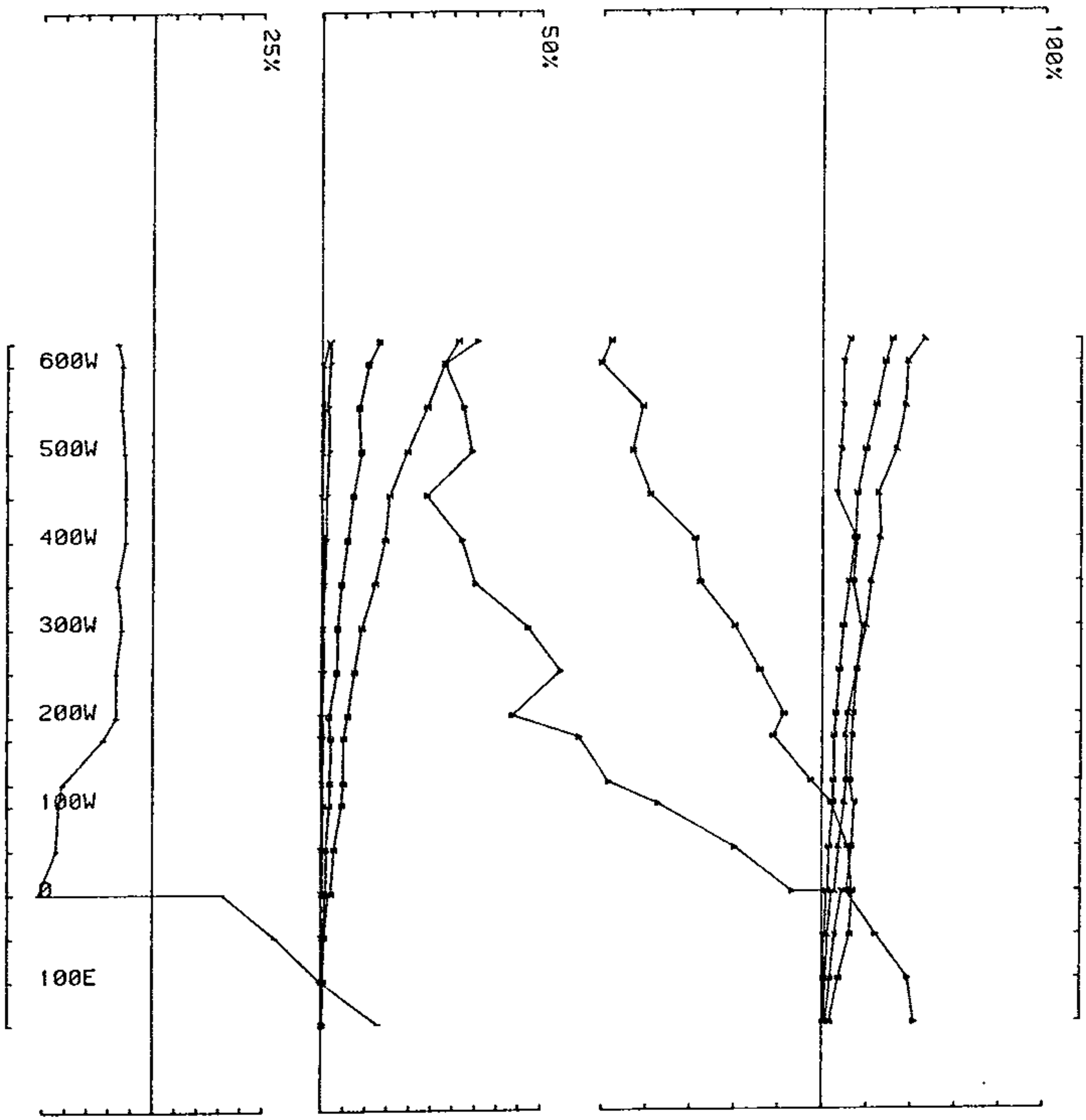

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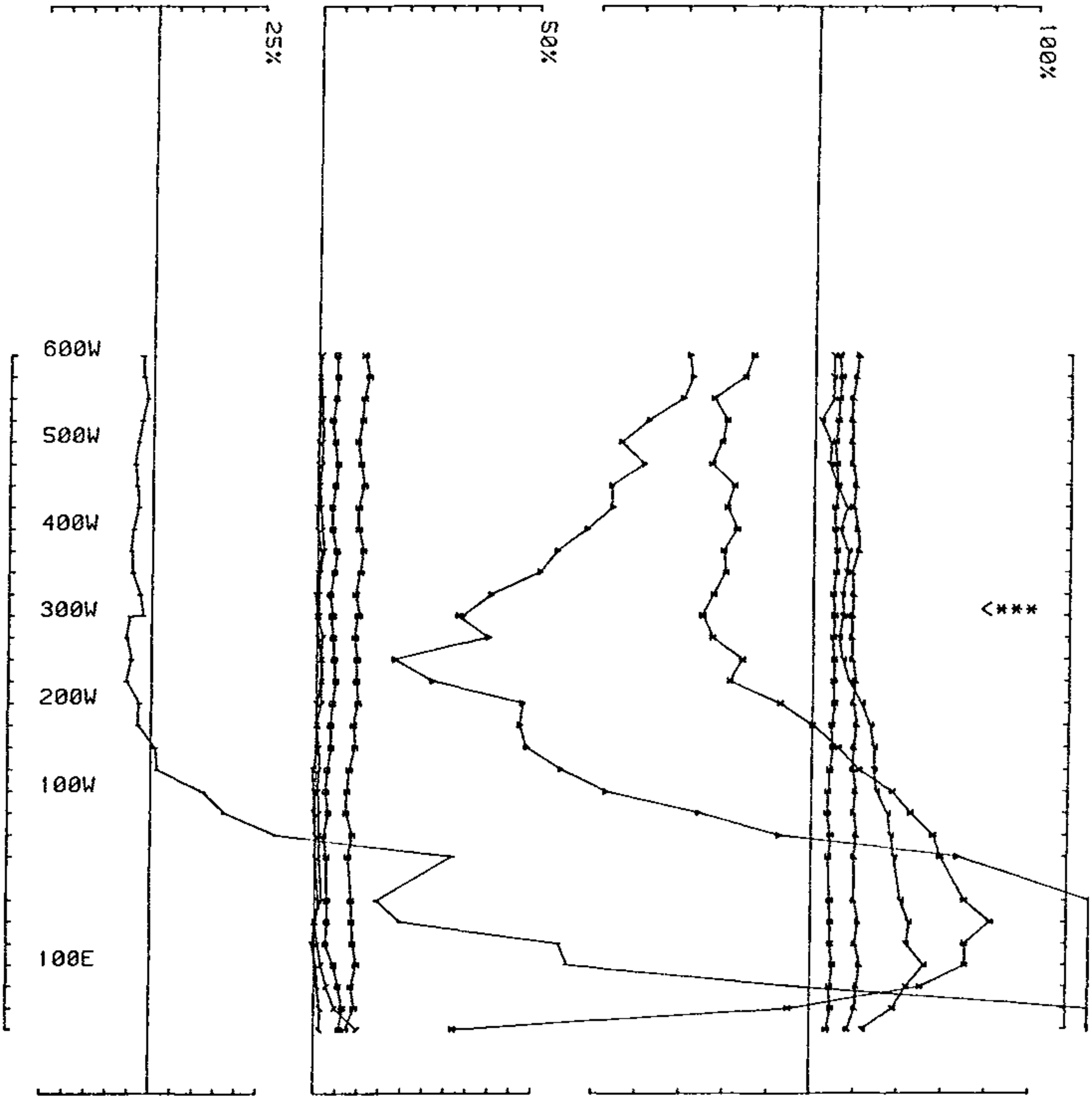

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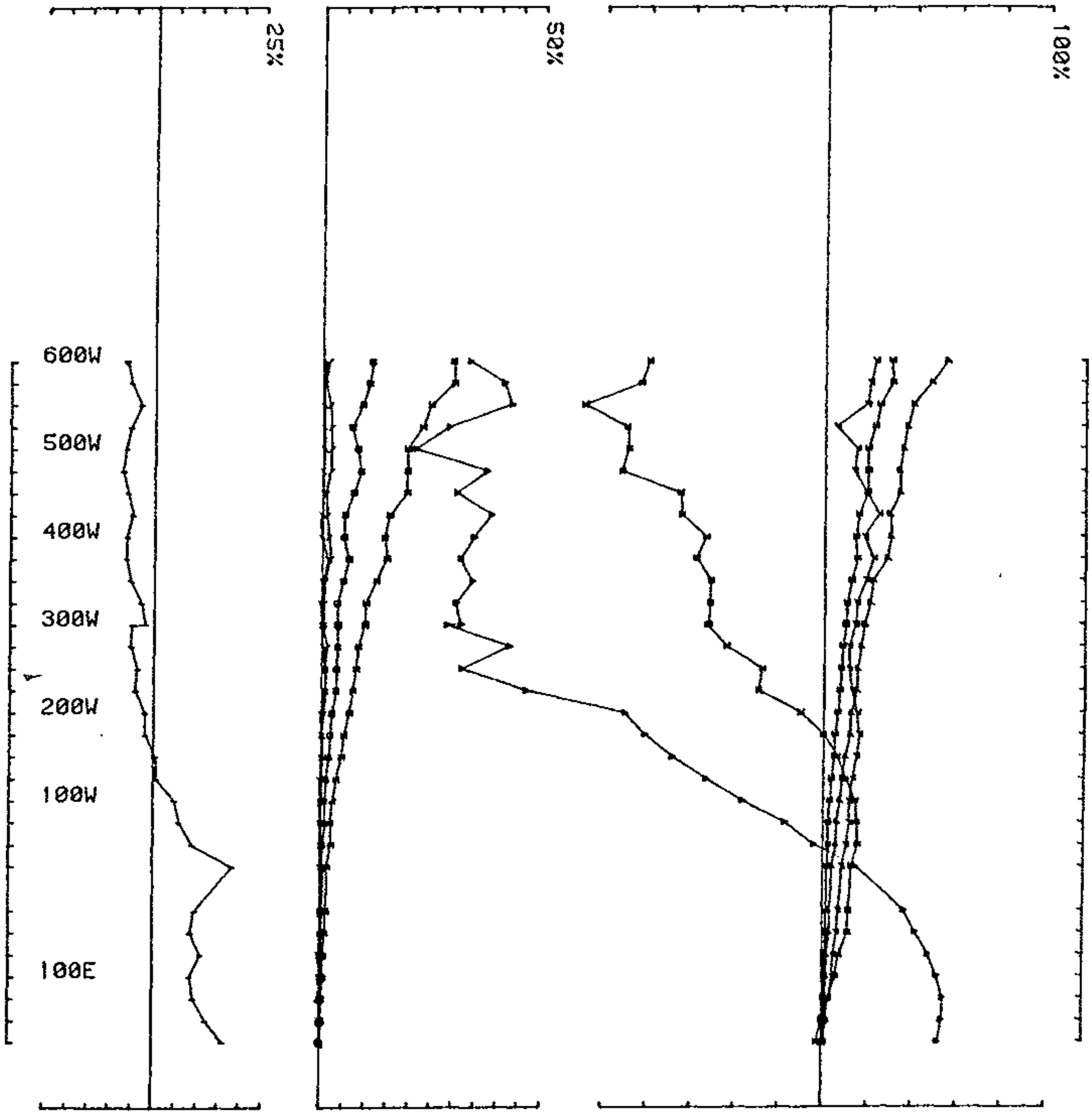

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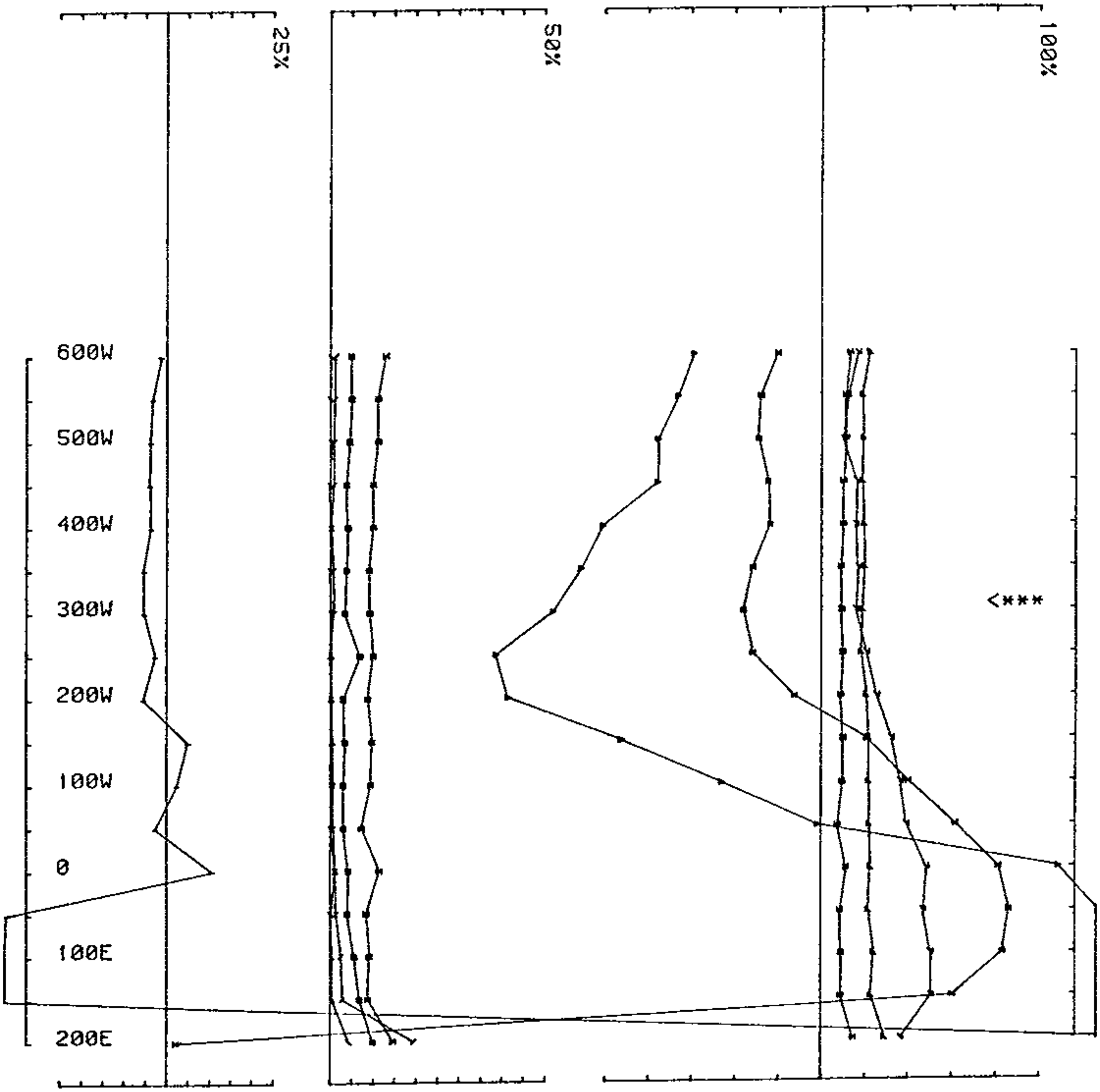

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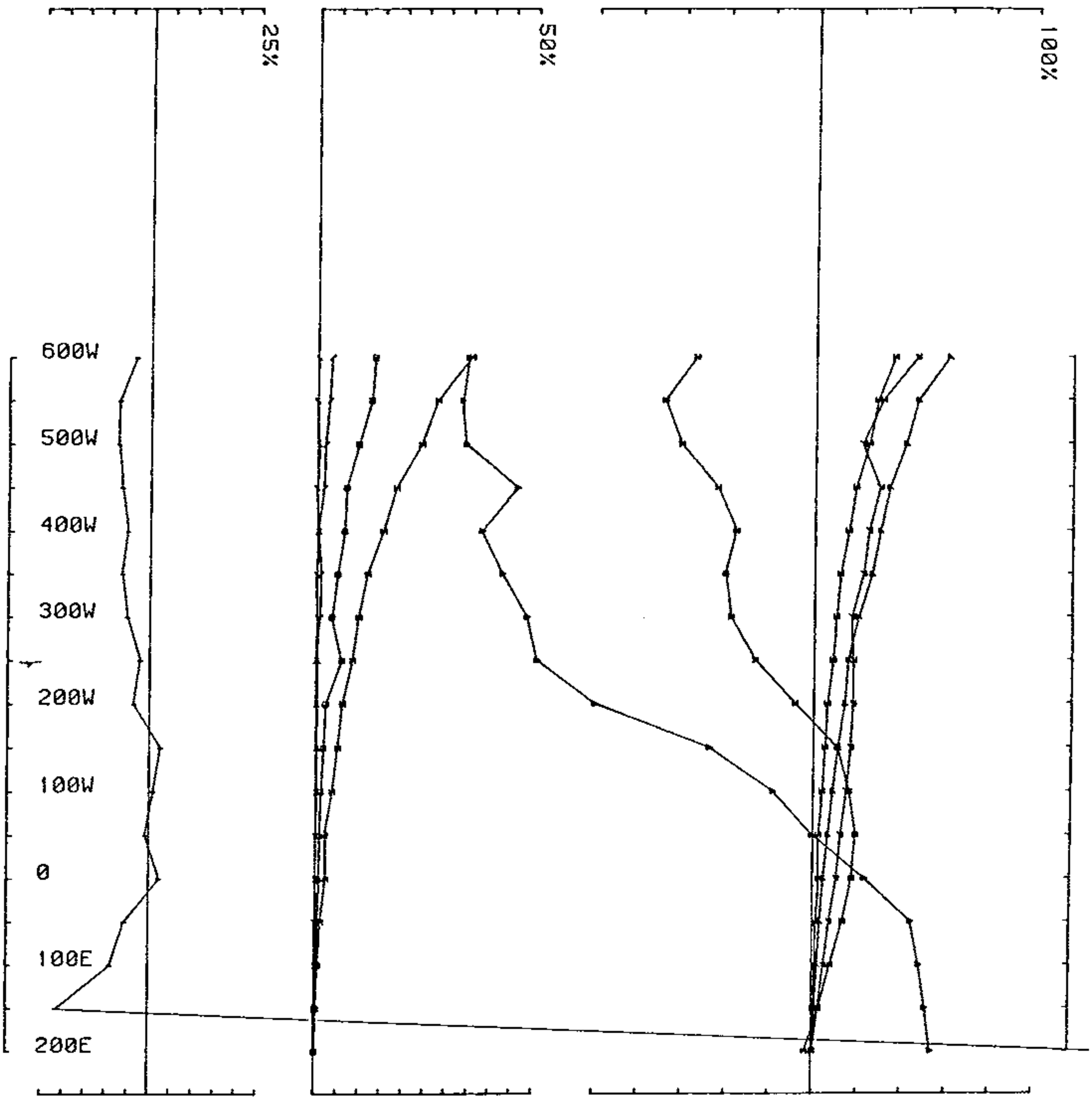

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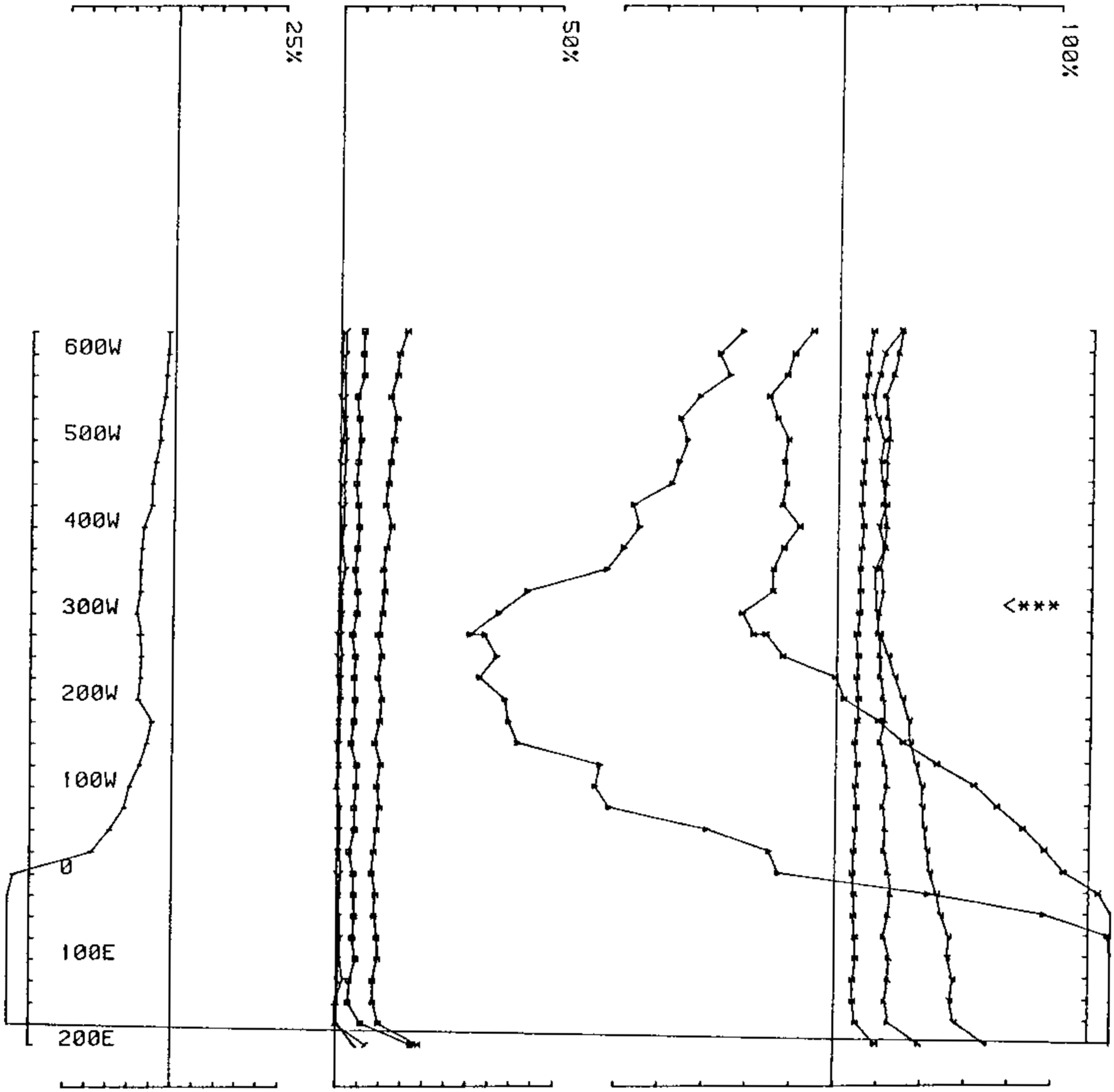

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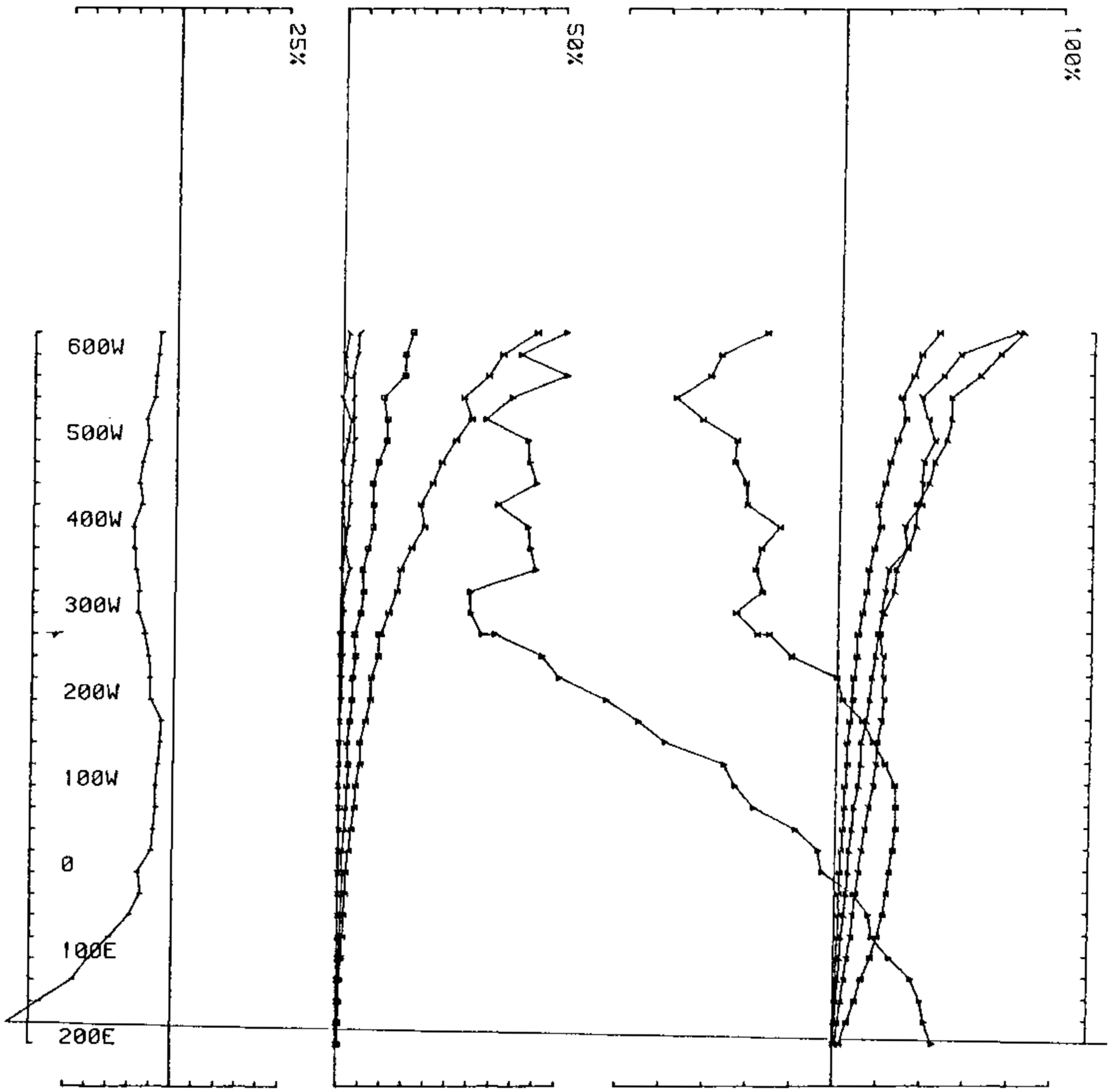

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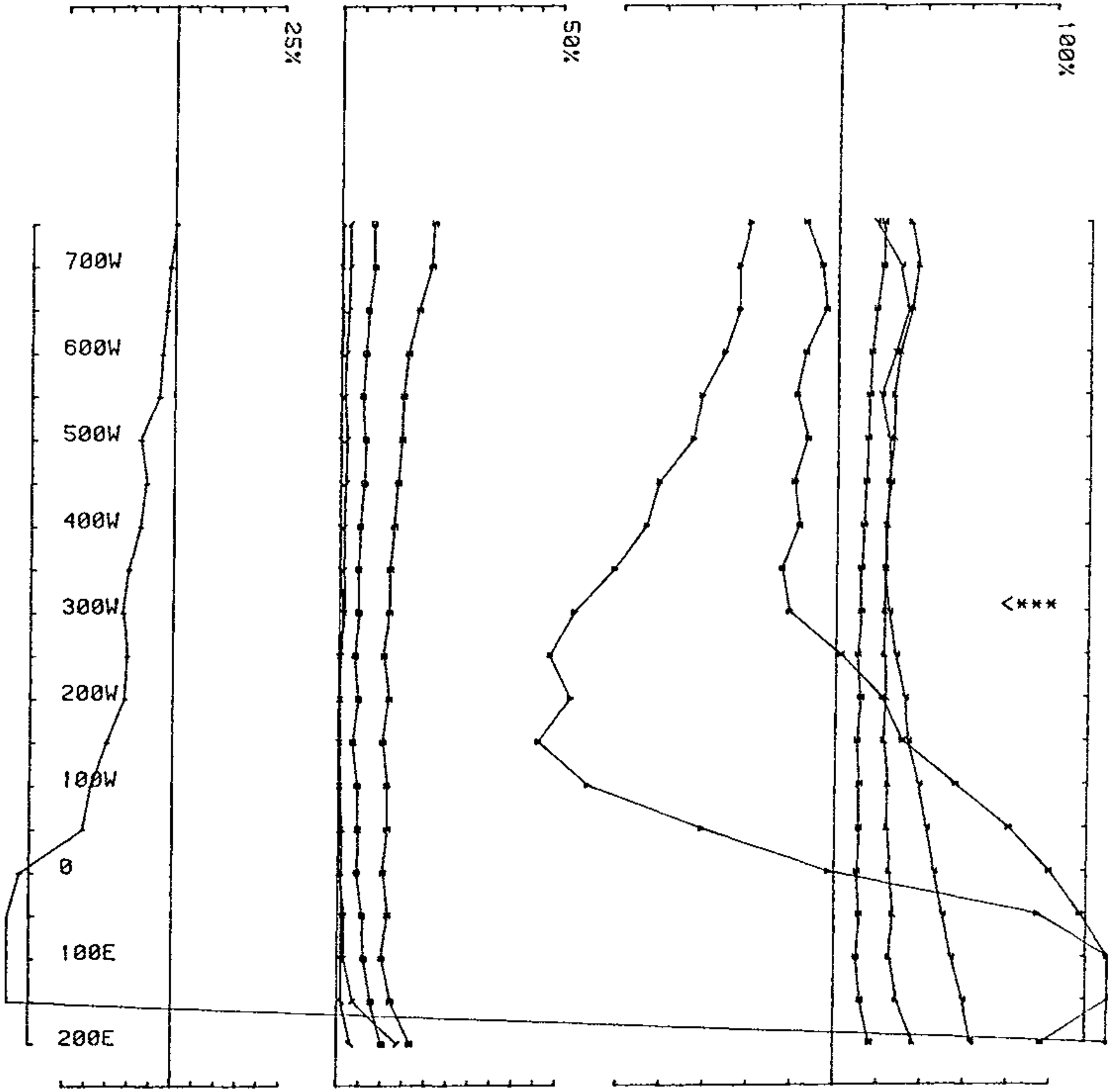

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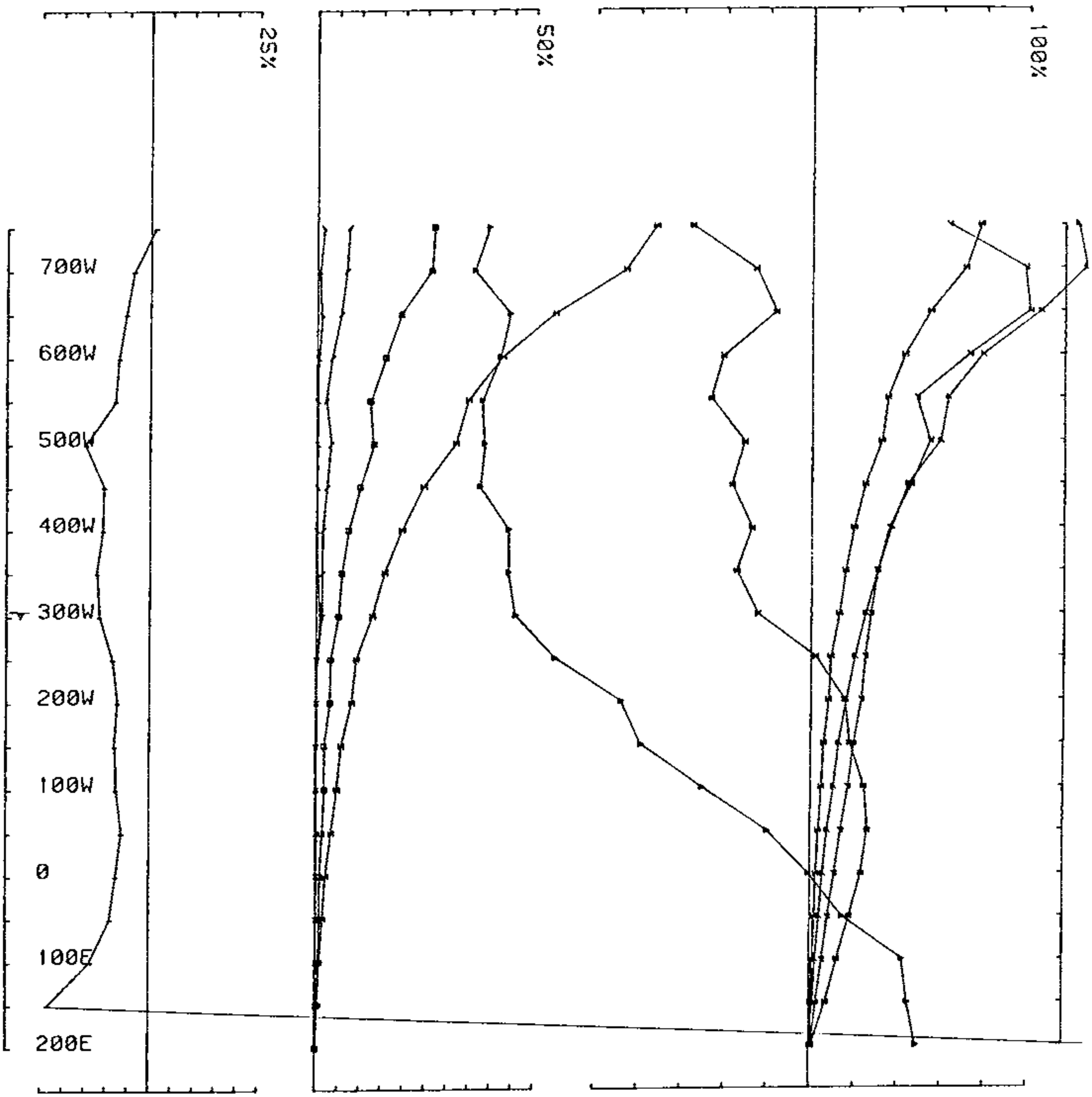

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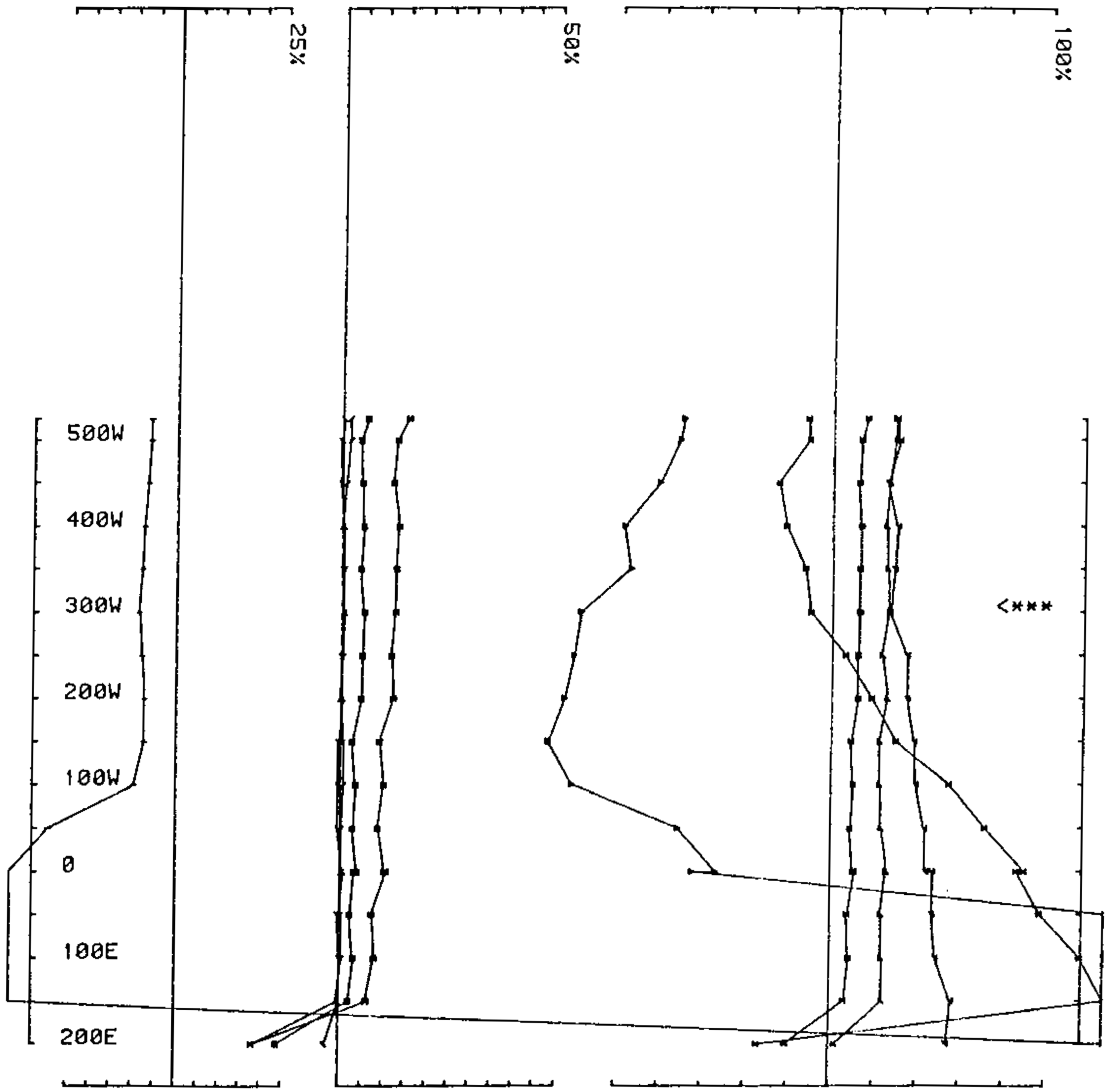

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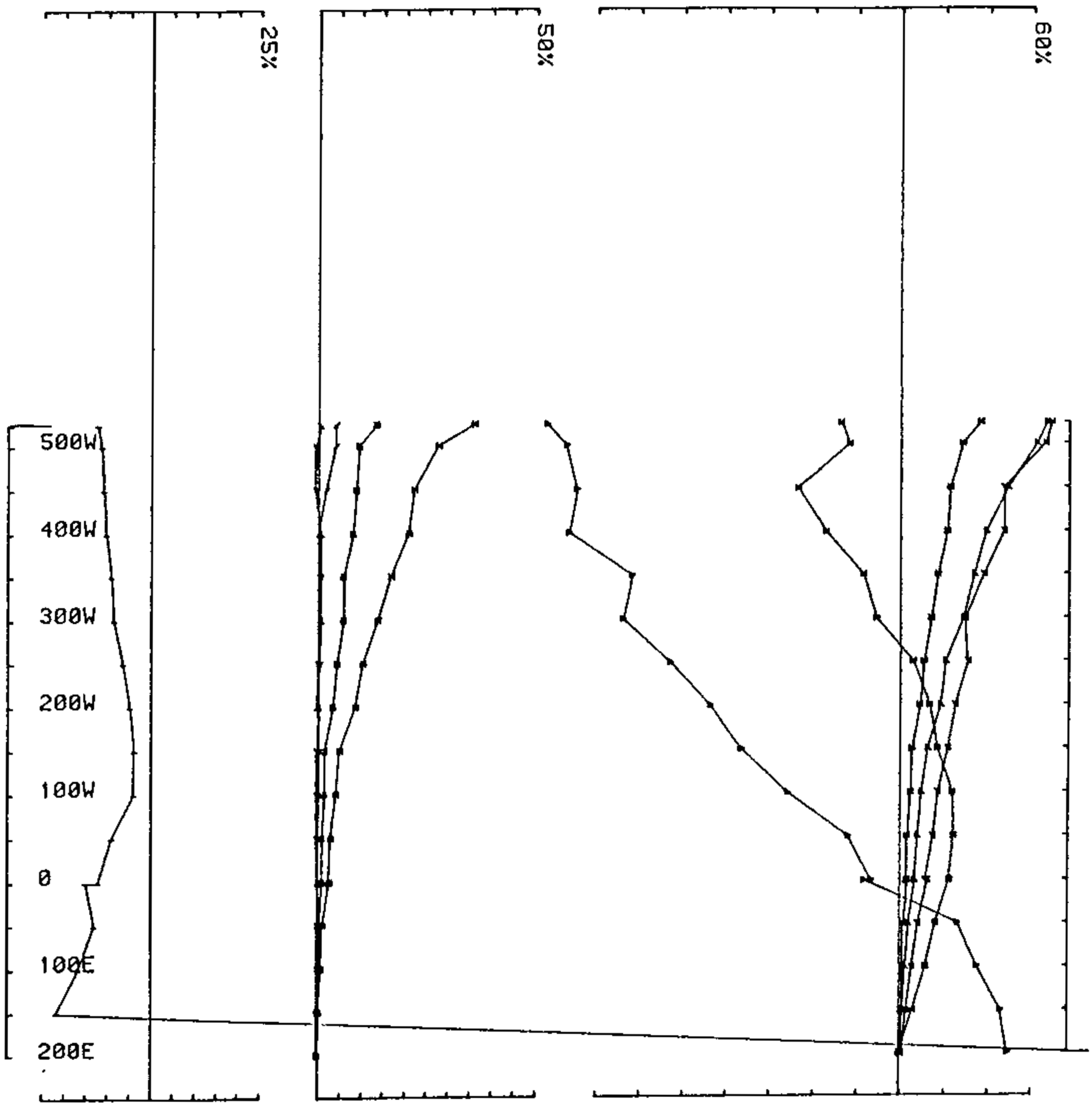

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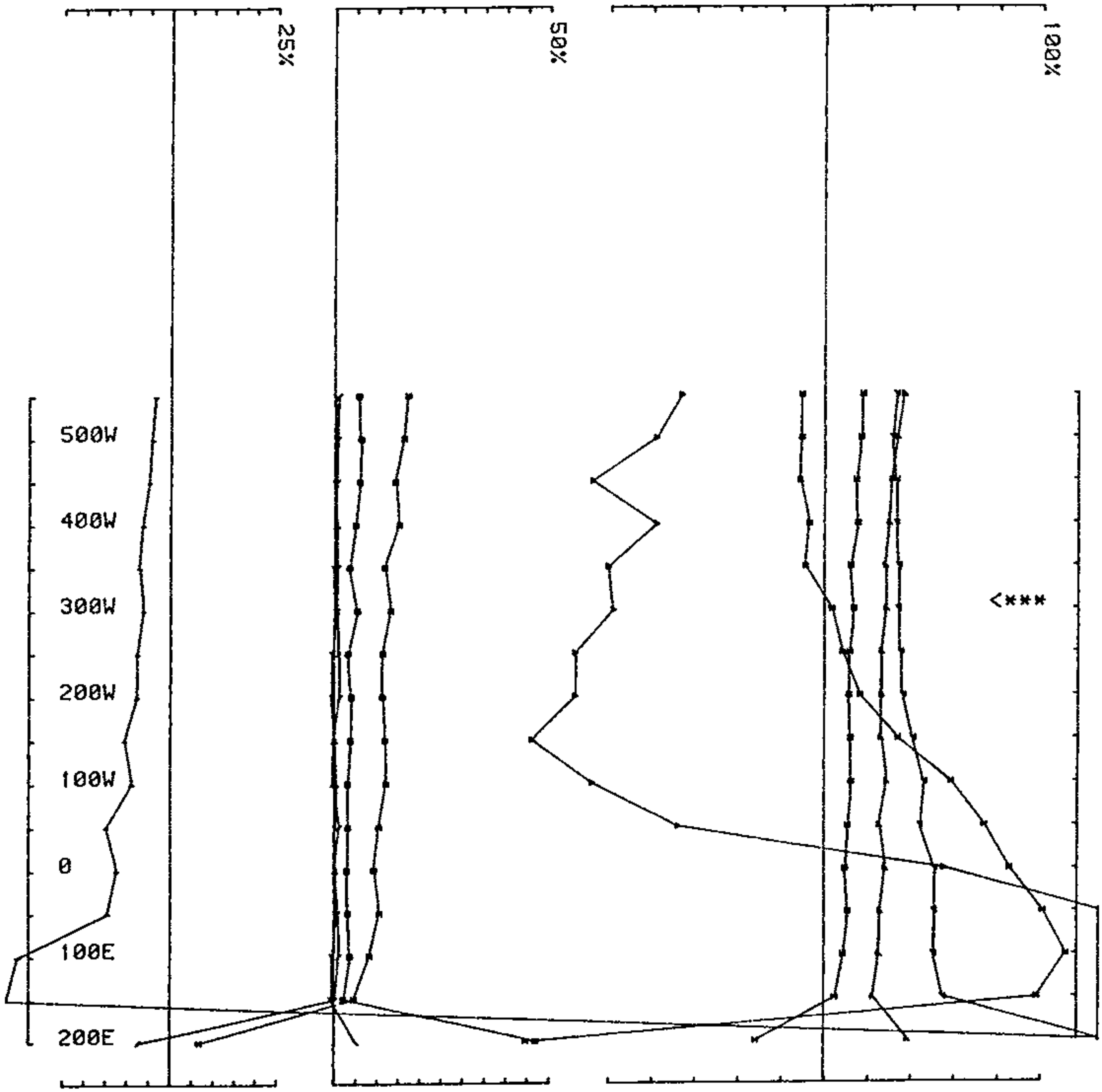

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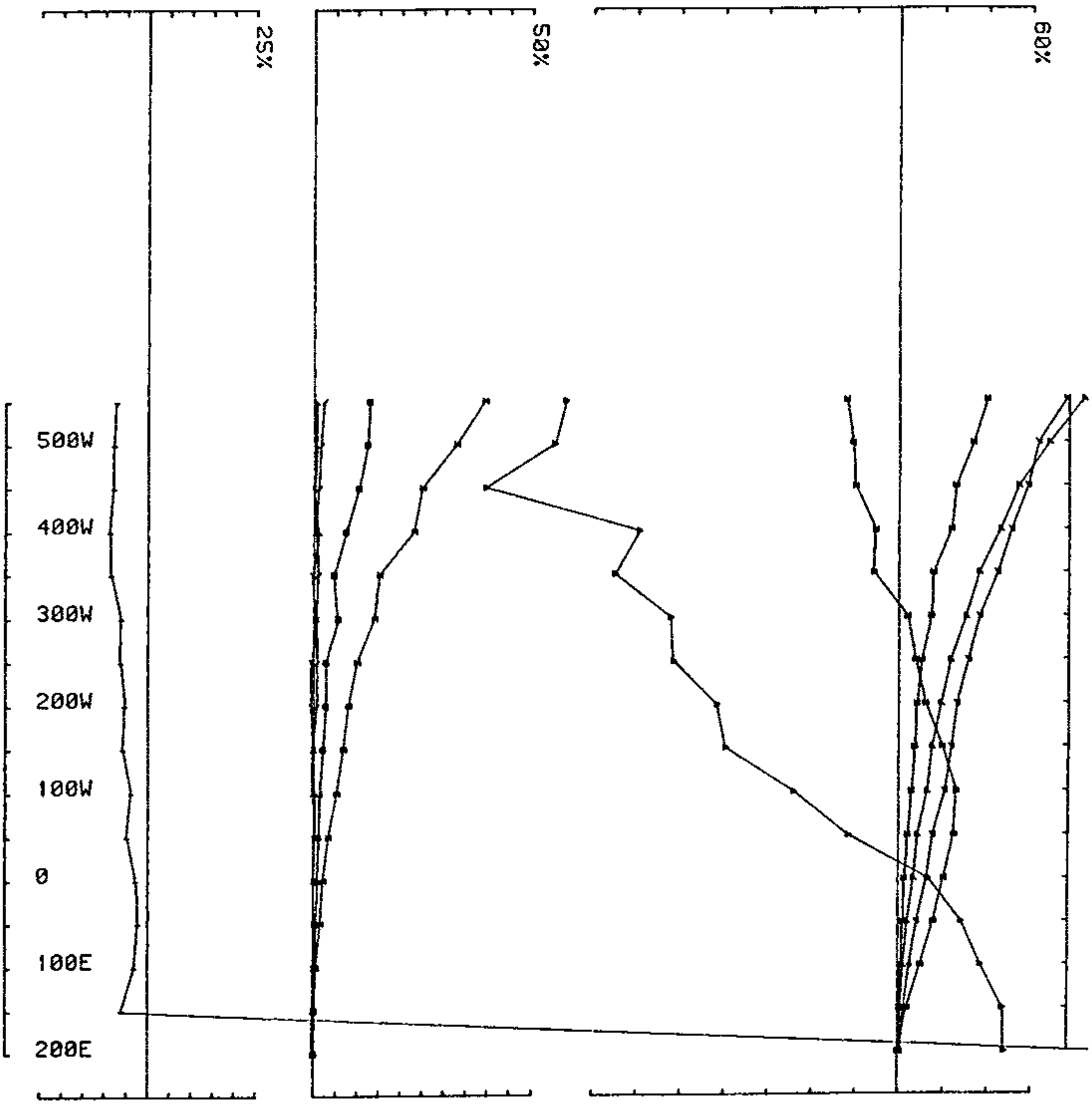
loop no 2 line 300S component Hz secondary field Ch I point norm.



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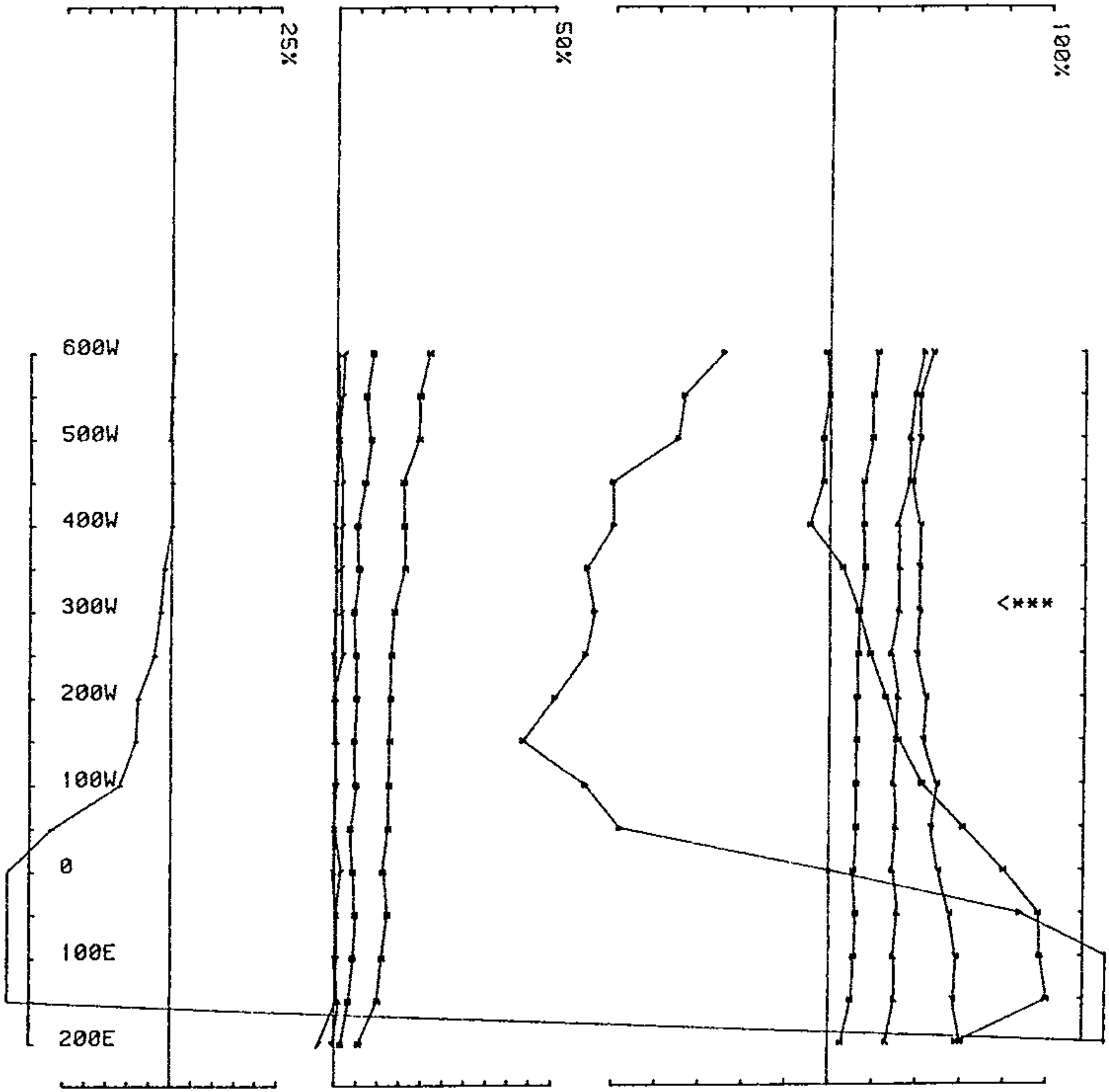

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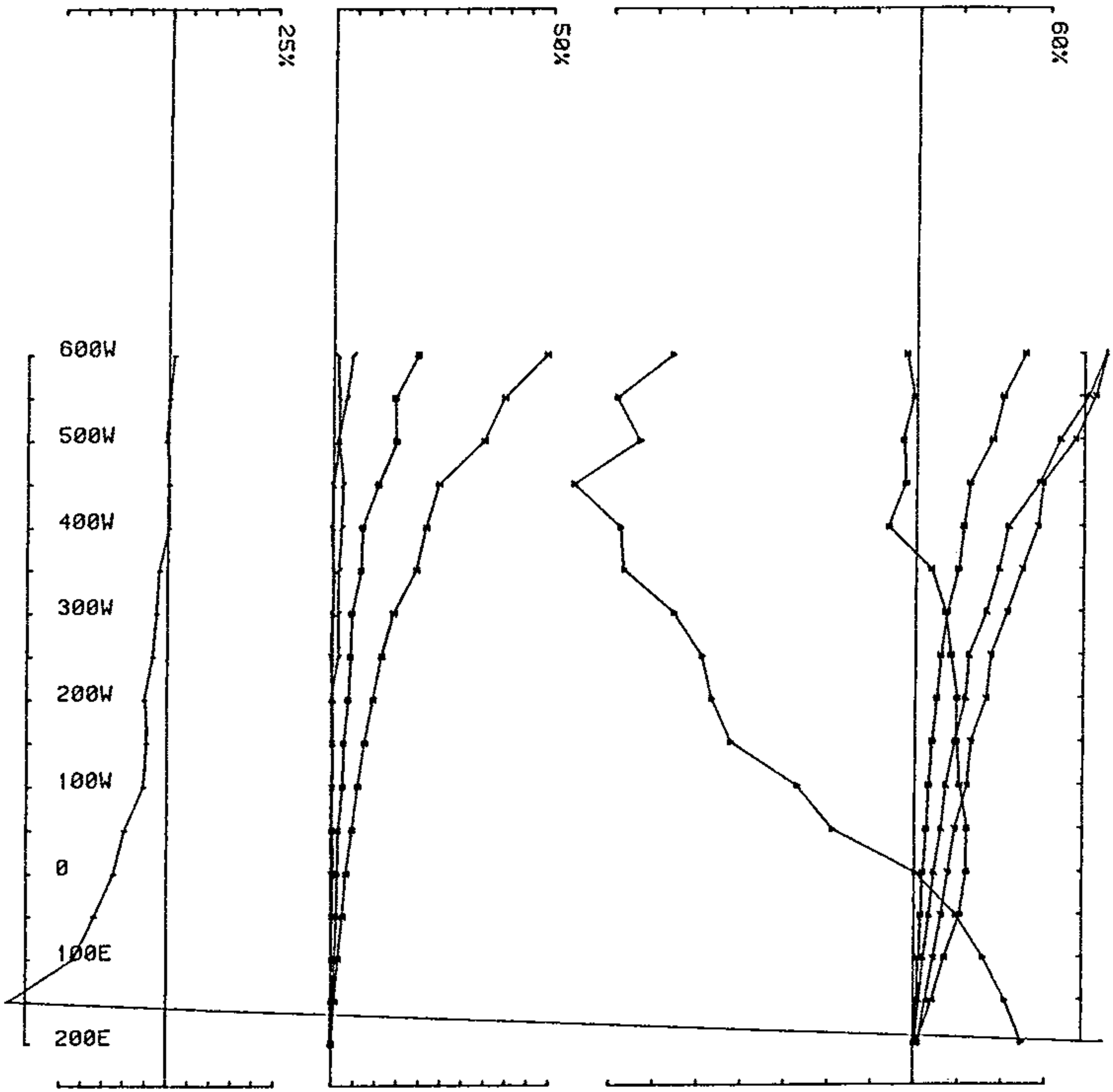

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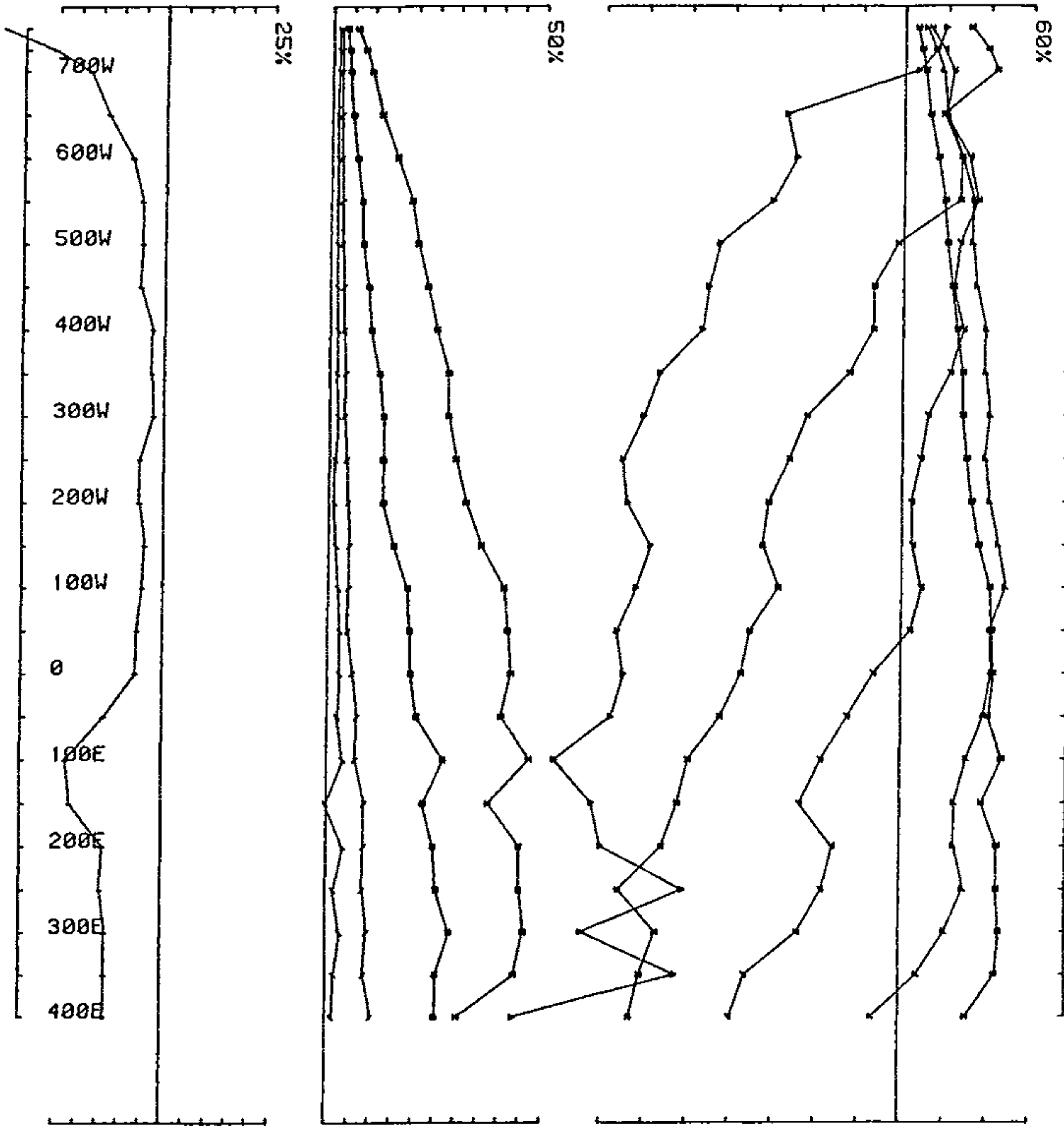

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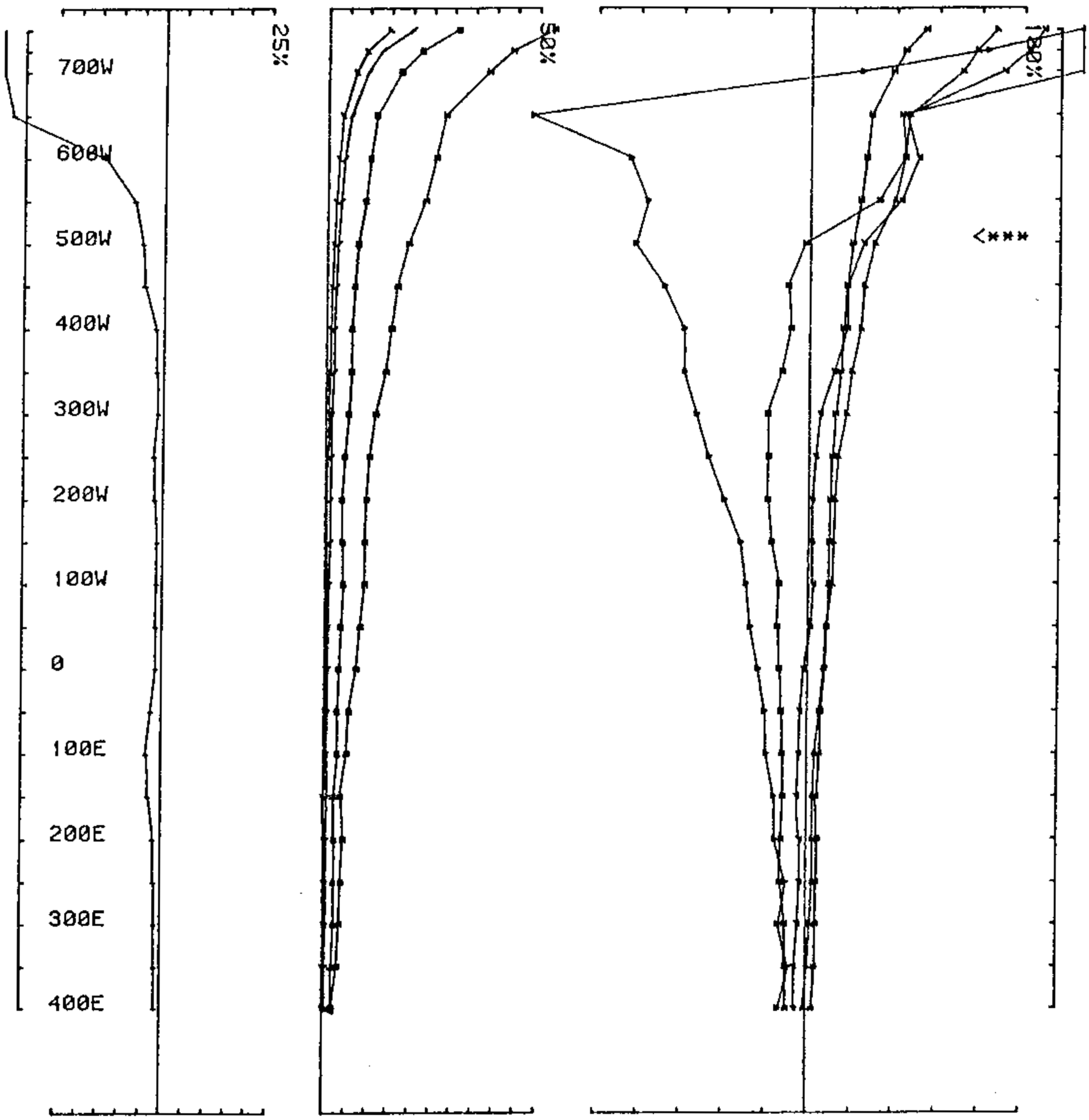

UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
conducted by S.J.V. CONSULTANTS LTD. job 8805 base freq (hz) 30.974
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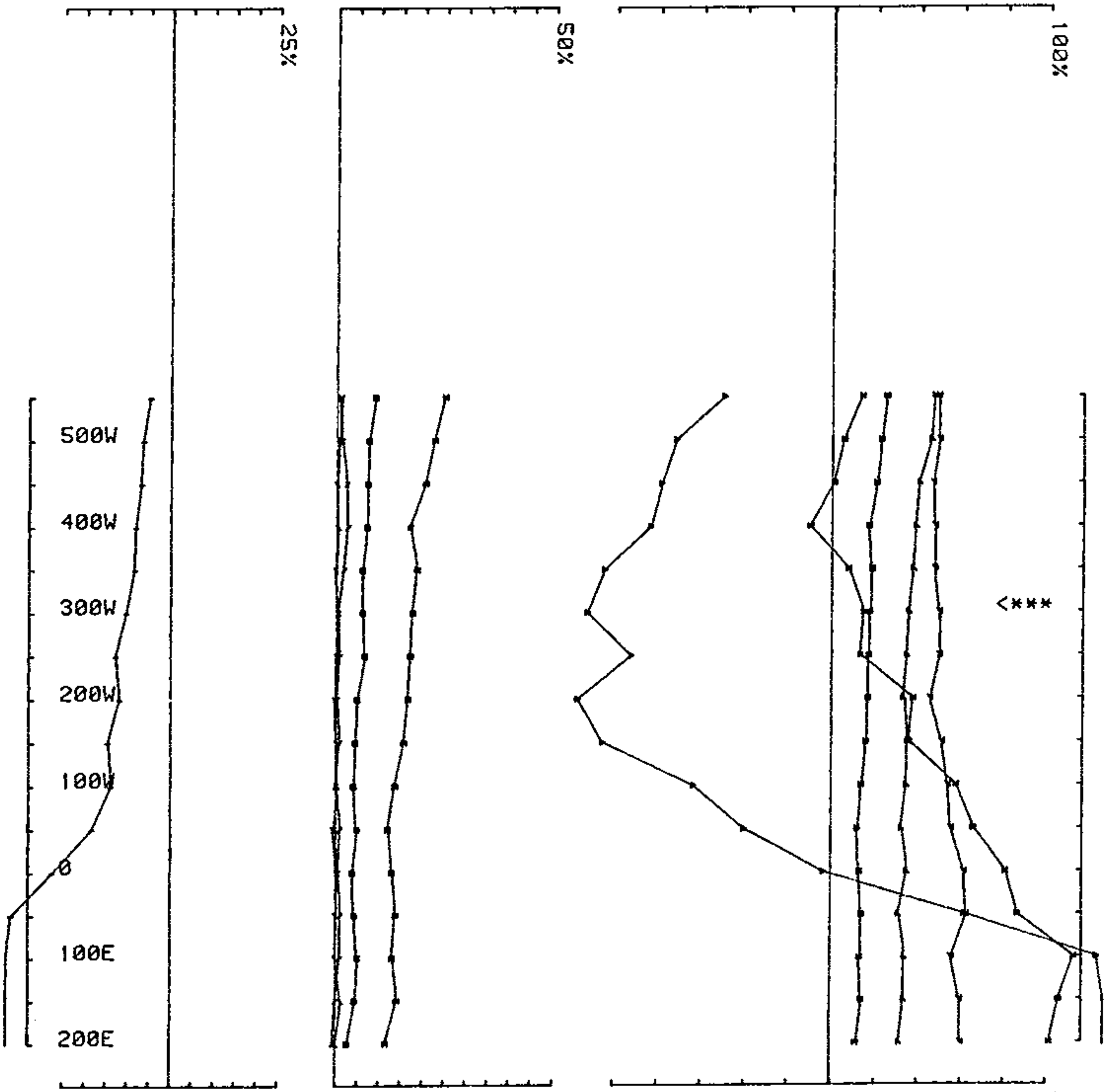
APPENDIX III

STATEMENT OF EXPENDITURES



UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
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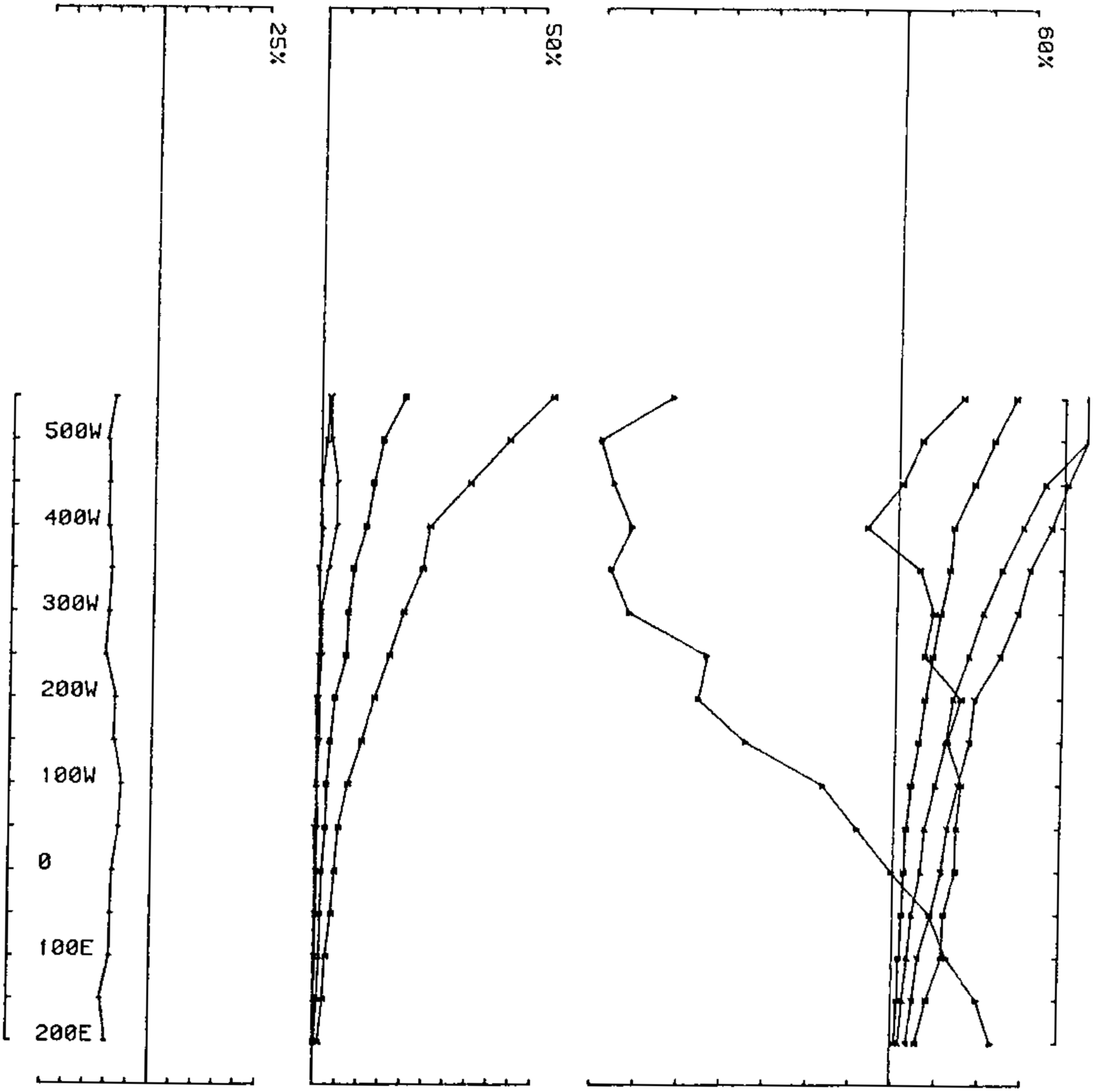
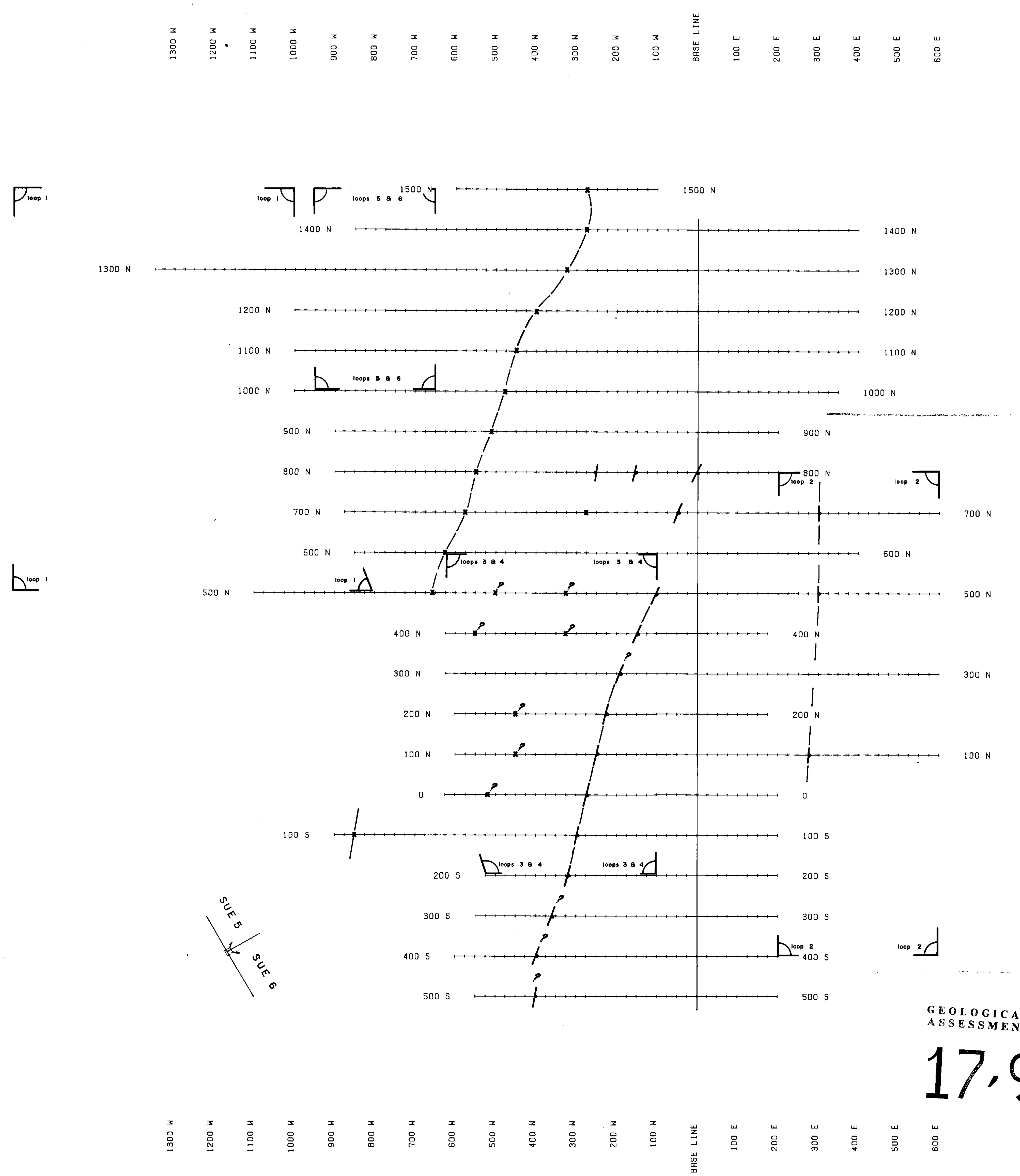
loop no 2 line 500S component Hz secondary field Ch 1 point norm.



UTEM SURVEY at SOO CLAIMS for DECADE INTERNATIONAL DEVELOPMENT LTD.
conducted by S.J.V. CONSULTANTS LTD. job 8805 base freq (hz) 30.974
loop no 2 line 500S component Hz secondary field Ch 1 contin. norm.

STATEMENT OF COSTS
Field Programs, May 1-22 and September 25-29, 1988

Wages:		
J. MacInnis - field assistant - May 3-22, 1988 19½ days @ $170/day	$ 3,315.00	
B. Saunders - field assistant - May 3-22, 1988 19½ days @ $125/day	2,437.50	
R. Ney - field assistant - May 3-16, 1988 14 days @ $135/day	1,890.00	
M. Pearson - instrument operator - Sept 25-29, 1988 5 days @ $185/day	925.00	
H.M. Jones, P.Eng. - geologist - supervisor - Sept 1, 3-10, 12-13, Sept 25-29, 1988 16 days @ $400/day	6,400.00	$14,967.50
Room and Board:		
Accommodation	1,465.65	
Meals, etc.	1,545.64	3,011.29
Field Equipment:		
Hip chains, flagging, sampling tools, etc.		702.51
Vehicle Rentals:		
Cana and Budget truck rentals, including gas and insurance		1,304.54
Assays:		
Acme Analytical Laboratories - 896 soils, 26 rocks		10,598.85
Contractors:		
Eagle Mapping Service - base map preparation	3,625.00	
S.J.V. Consultants Ltd. - UTEM geophysical survey	18,250.98	
Tony Clark Consulting - geochemical consulting and maps	590.00	22,465.98
Instrumental Rental:		
VLF-EM @ $35/day		175.00
Report and Map Preparation:		
Report preparation	2,000.00	
Drafting, map prints	450.00	
Word processing, copies	325.00	2,775.00
Management Fees		
On all costs except professional fees @ 12%		5,712.00
TOTAL EXPENDITURES		$61,711.69



LEGEND

CROSSOVER AXIS (SHALLOW WEAK) — conductive

CONTACT (CHANGE IN BACKGROUND CONDUCTIVITY)

LOOP CORNERS — loop 2

INSTRUMENT USED : UTEM (TIME DOMAIN EM SYSTEM)
LAMONTAGNE GEOPHISICS LTD.

DECADE INTERNATIONAL DEVELOPMENT LTD.

SUE CLAIMS

SOO RIVER, WHISTLER, B.C.

UTEM COMPILATION MAP

VANCOUVER, M.D. N.T.S. 92J/2W

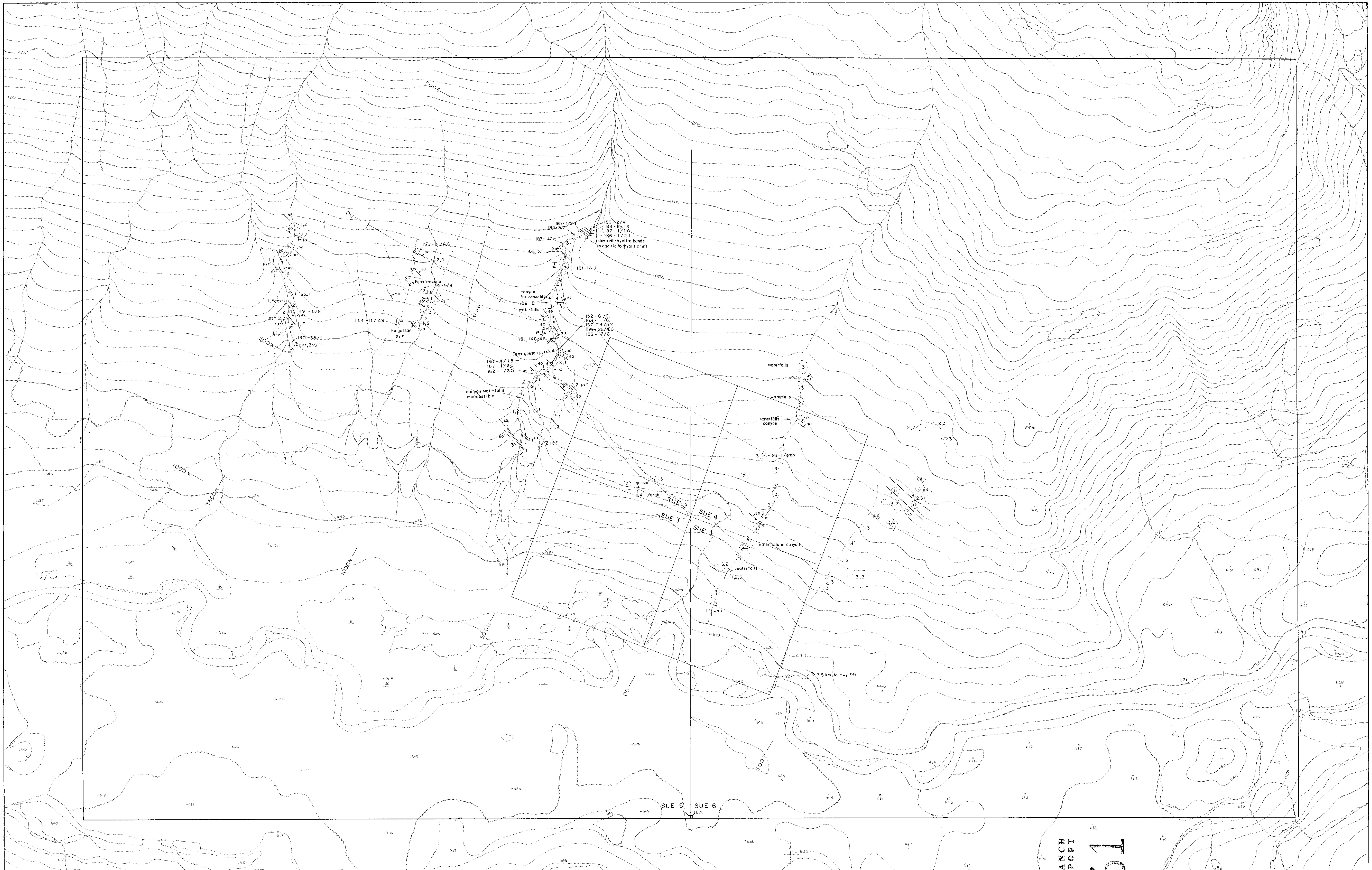
SCALE 1:5000

100 0 100 200 300

MAY, 1988

PLATE 88-1

S.J.V. CONSULTANTS LTD.



LEGEND :—

CRETACEOUS OR EARLIER
- 6 Lamprophyre dyke

COAST RANGE INTRUSIVES
- 5 Diorite and granodiorite

LOWER CRETACEOUS
Gambier Group
- 4 Quartz - sericite schist
- 3 Andesite - mainly tuffs
- 2 Dacite - mainly tuffs
- 1 Rhyolite - tuffs

Limit of outcrop
Fracture
Bedding
Schistosity
py+ >2% pyrite
Creek
Dry gully
Main logging road
Abandoned logging road
154-11/2.9 Sample Nº. — Au in ppb / Width in metres

DECADE INTERNATIONAL DEVELOPMENT LTD.

H.M. JONES & ASSOCIATES INC. VANCOUVER, B.C.

SUE CLAIMS

GEOLOGY

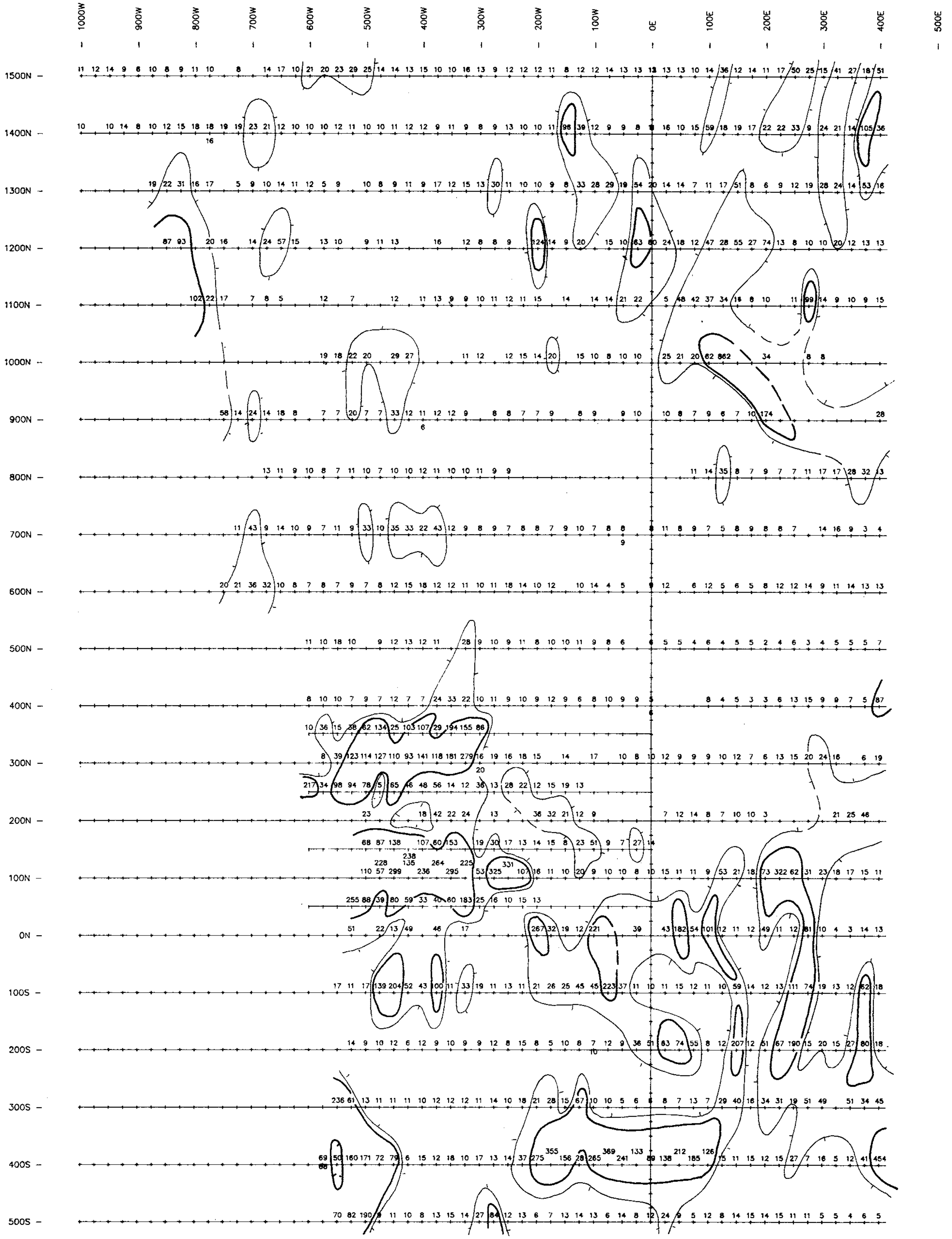
SOO RIVER, WHISTLER AREA

N.T.S. 92J-2W VANCOUVER M.D., B.C.

0 100 200 300 400 500METRES

SCALE 1:5000	MAY 1988 REVISED OCT. 1988	FIG. 3
H. M. JONES		

CHONG



862 COPPM

Co ANOMALOUS ≥20 ppm

" " ≥60 "

GEOLOGICAL BRANCH ASSESSMENT REPORT

17,961

0 200

metres

DECADE INTERNATIONAL DEVELOPMENT LTD.

SUE CLAIMS
Soo River, Whistler Area

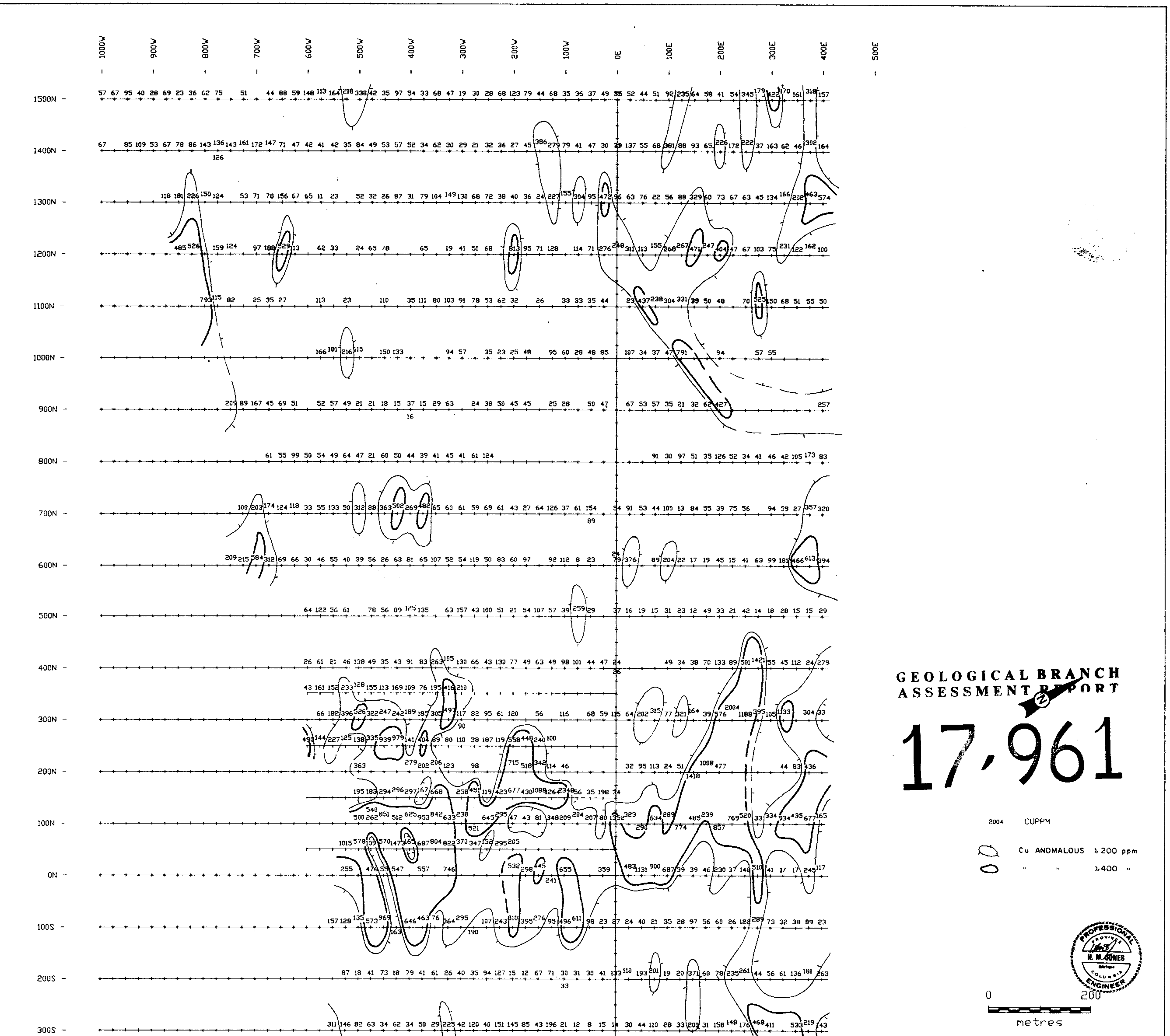
Vancouver M.D. 92J/2W

SOIL GEOCHEMISTRY
COBALT

DATE: 18 Oct 1988 | SCALE: 1 : 5000

Drawn By: TONY CLARK CONSULTING

FIG. 4



DECADE INTERNATIONAL DEVELOPMENT LTD.

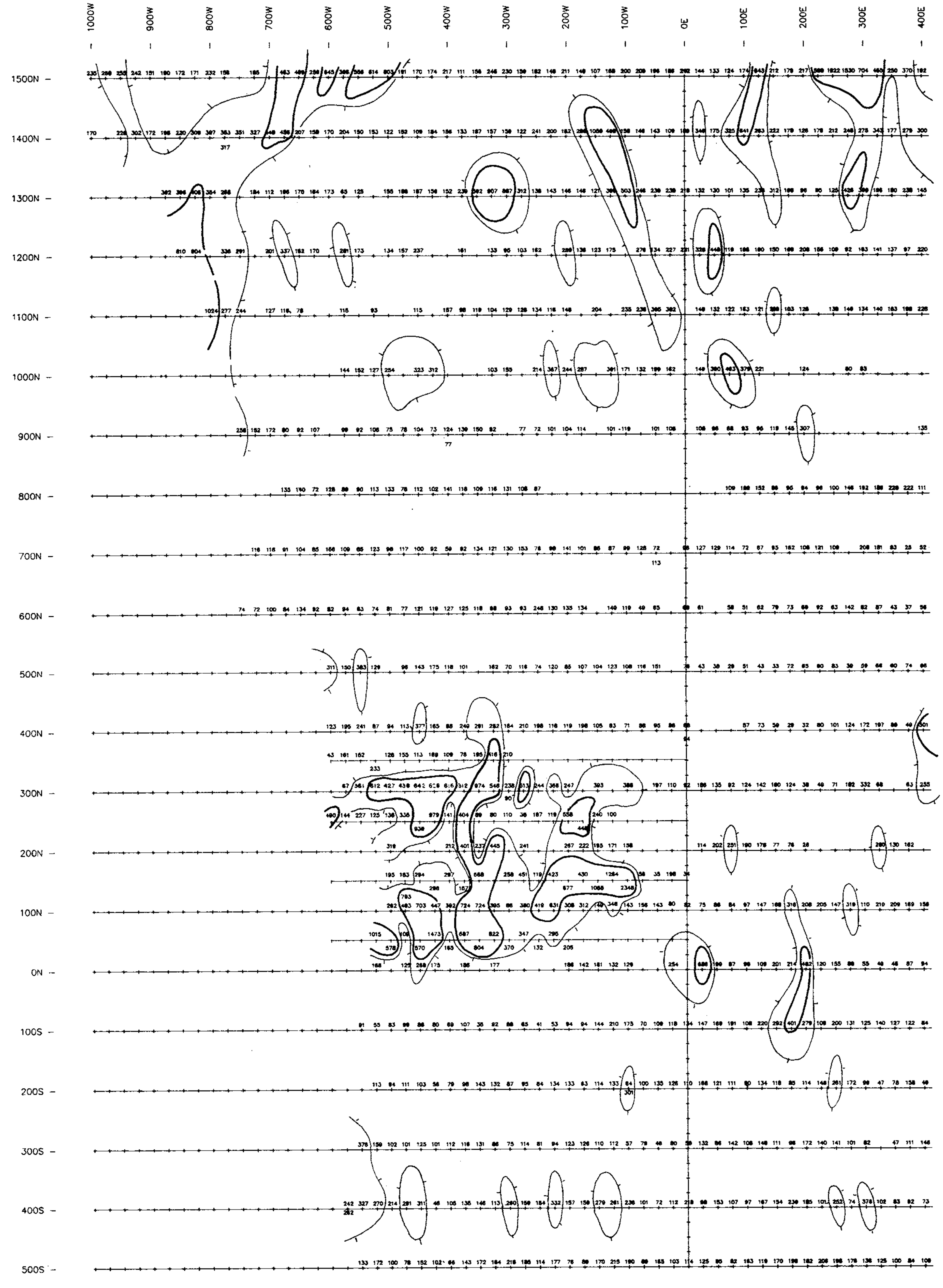
SUE CLAIMS
Soo River, Whistler Area
Vancouver M.D. 92J/2W

SOIL GEOCHEMISTRY
COPPER

DATE: 18 Oct 1988 | SCALE: 1 : 5000

Drawn By: TONY CLARK CONSULTING

FIG. 5



1822 ZNPPM

Zn ANOMALOUS ≥ 250 PPM

" " ≥ 400 "

GEOLOGICAL BRANCH
ASSESSMENT REPORT

17,961

0 200
metres

DECADE INTERNATIONAL DEVELOPMENT LTD.

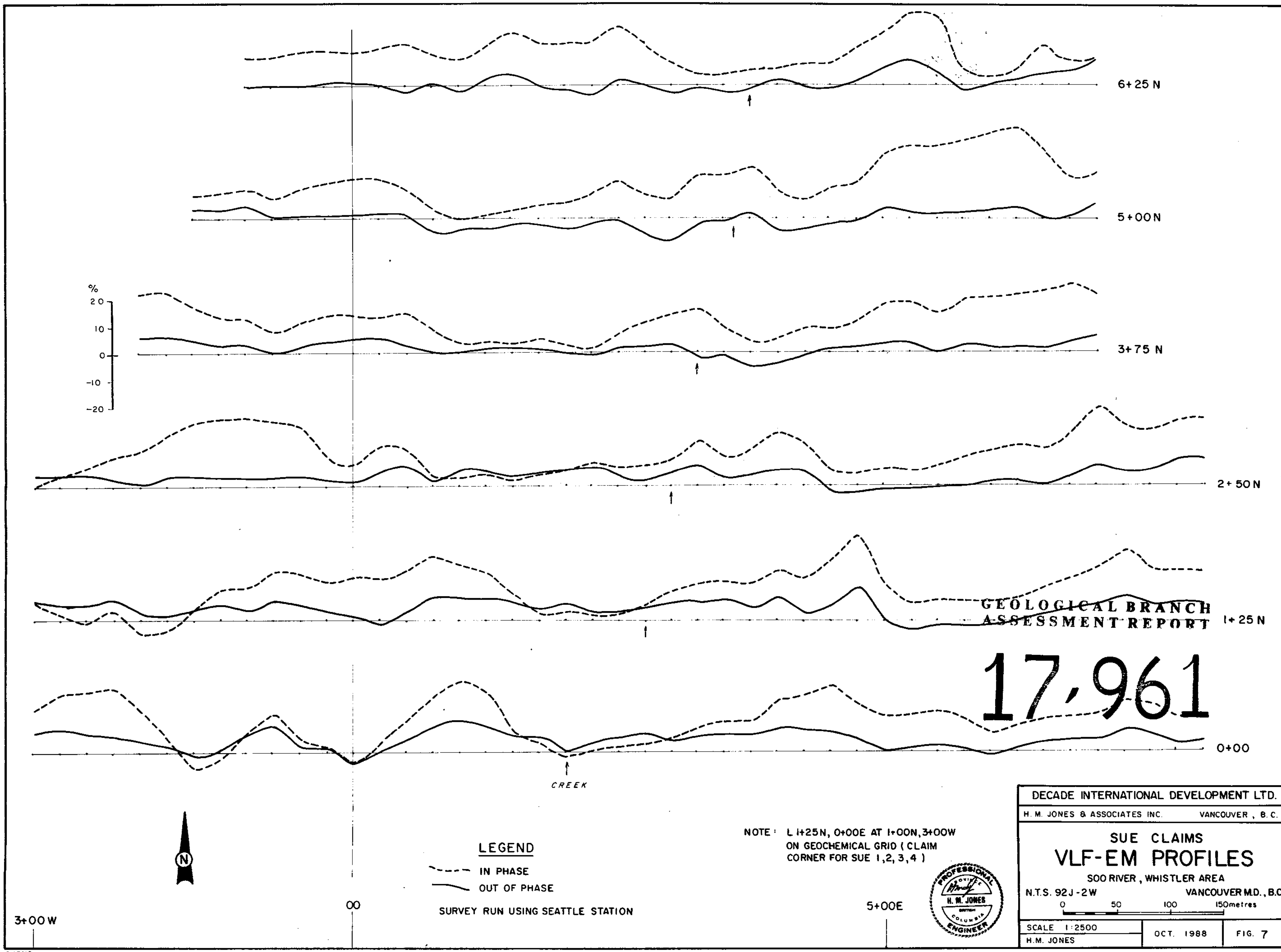
SUE CLAIMS
Soo River, Whistler Area
Vancouver M.D. 92J/2W

SOIL GEOCHEMISTRY
ZINC

DATE: 18 Oct 1988 | SCALE: 1 : 5000

Drawn By: TONY CLARK CONSULTING

FIG. 6


6+25 N
5+00N
3+75 N
2+50N
1+25 N
0+00
%
20
10
0
-10
-20
CREEK
GEOLOGICAL BRANCH
ASSESSMENT REPORT
17,961
N
LEGEND
IN PHASE
OUT OF PHASE
SURVEY RUN USING SEATTLE STATION
NOTE: L 1+25N, 0+00E AT 1+00N, 3+00W ON GEOCHEMICAL GRID (CLAIM CORNER FOR SUE 1,2,3,4)
3+00W
00
5+00E
PROFESSIONAL ENGINEER
H. M. JONES
BRITISH COLUMBIA
DECADE INTERNATIONAL DEVELOPMENT LTD.
H. M. JONES & ASSOCIATES INC.
VANCOUVER, B.C.
SUE CLAIMS
VLF-EM PROFILES
SOO RIVER, WHISTLER AREA
N.T.S. 92J-2W
VANCOUVER M.D., B.C.
0
50
100
150metres
SCALE 1:2500
H.M. JONES
OCT. 1988
FIG. 7
CHONG