

GEOCHEMICAL, GEOPHYSICAL, GEOLOGICAL

and

TRENCHING REPORT

on the

SUMMIT CAMP PROPERTY

Similkameen Mining Division
British Columbia

North Lat. 49°25' West Long. 121°45'
NTS 92H/6

LOG NO: 1214	RD.
ACTION:	
FILE NO:	

FILMED

Prepared for

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GEOLOGICAL BRANCH
ASSESSMENT REPORT

November 2, 1988

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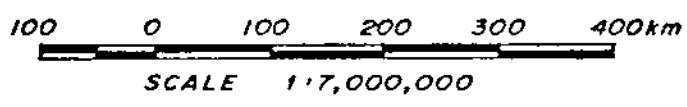
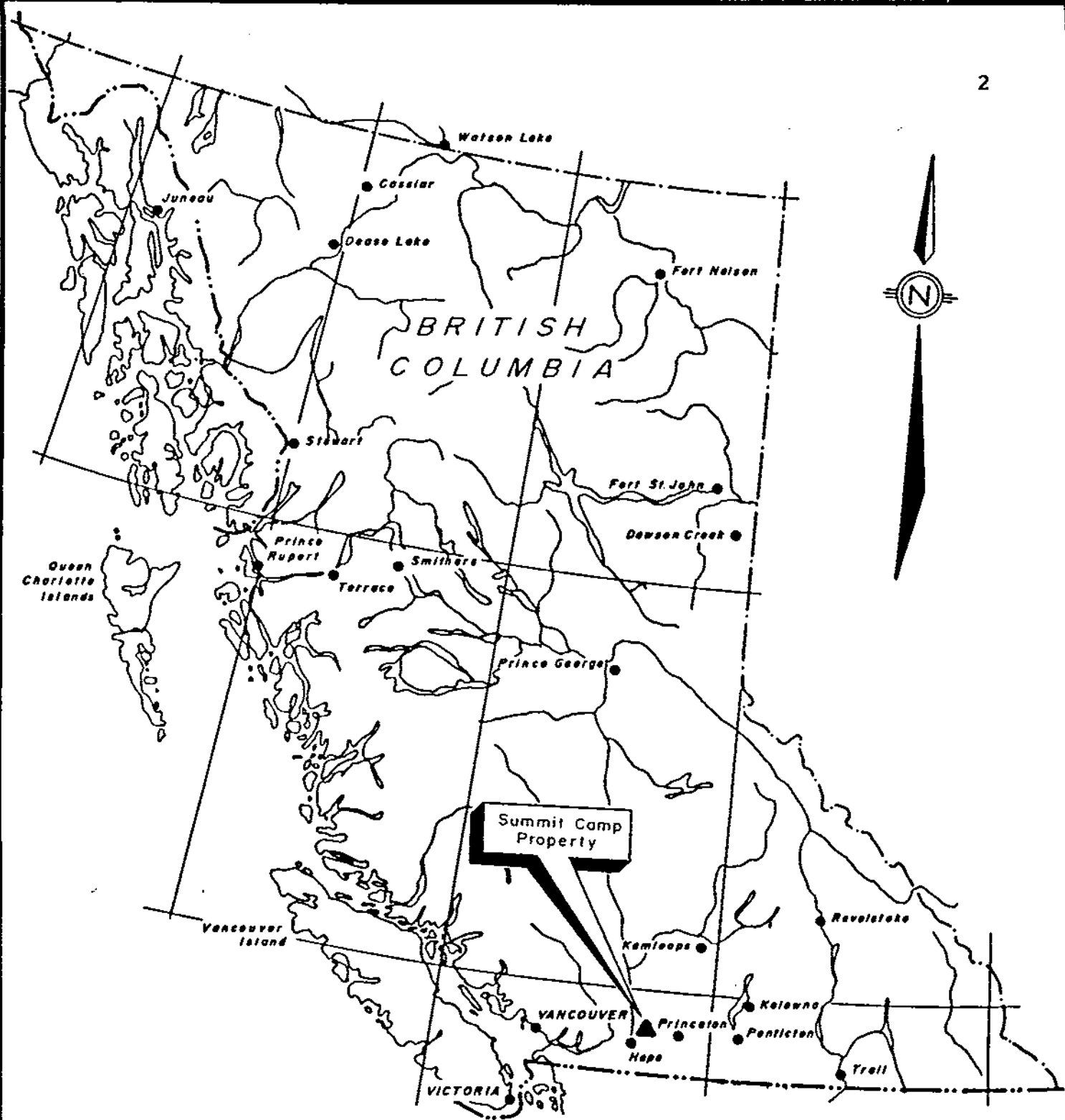
INTRODUCTION

Harrisburg-Dayton Corp. and Schellex Gold Corp. both of Vancouver, British Columbia hold an option to purchase the Southern No. 8 fraction, the Sutter, Skyline, Vigo, Lulu, Sky, Spike and Amberty claims (the "Summit Camp Property"), which are located in the Similkameen Mining Division. This report, prepared at the request of the directors of Harrisburg-Dayton Resource Corp., describes the Phase I and II exploration programs conducted on the claims. These programs consisted of grid establishment, VLF-EM survey, prospecting, road building, trenching, soil and rock geochemistry surveys and was conducted between June 13th and September 13th, 1988.

SUMMARY

The Summit Camp Property consists of an irregularly shaped fractional claim, four reverted crown grants, and three M.G.S. claims. Together, the claims total 29 units and are located some 27 kilometers east/northeast of Hope, in the Similkameen Mining Division, British Columbia. It is readily accessible by well maintained logging roads, departing from the Coquihalla Highway 52 kilometers north of Hope. These roads are kept open during winter if logging is in progress.

The subject property is underlain by tuffaceous and pelitic sediments of the Upper Jurassic Dewdney Creek Group. Mineralization is generally consistent in character throughout the area. It consists of silver-bearing sulfides in quartz carbonate veins localized along locally prominent, steeply dipping fault structures, subsidiary faults and tension fractures. The veins varies in width and usually consist of a central core of massive sulfides with veinlets and disseminations distributed outward.



Harrisburg - Dayton Resource Corp.

Location Map

SUMMIT CAMP PROPERTY

Similkomeen Mining Division
NTS: 92 H/6

October, 1988 Figure 1

Boa Services Ltd.

Exploration and development in this area commenced in 1894 with the staking of the main claims presently covered by the Sky claim. Sporadic work continued for the next forty years with the development of the Indiana, Queen Bess, Mountain View and the Blue Bell adits and the Summit shaft. Subsequent work was largely focussed on Treasure Mountain, just east of the property. Exploration resumed in 1982 when Unicorn Resources Ltd. conducted a regional soil geochemistry program and detailed underground sampling and mapping on portions of the ground presently controlled by Harrisburg-Dayton. In 1983, MPH consultants, on behalf of Unicorn Resources Ltd., carried out a geological, geophysical, geochemical and diamond drilling program. Their work indicated that certain geochemical and geophysical anomalies as well as two mineralized structures warrant further investigation before more drilling is contemplated.

The 1988 geochemistry survey delineated 8 anomalous zones, 7 of which have coincident EM conductors. The Basil vein, discovered during this year's program, is located within one of these anomalous zones. The size and intensity of the anomaly indicates a larger structure than the Basil Vein or perhaps a series of parallel structures.

The trenching program exposed the Indiana vein for 390 meters and sampling of the trenches have shown that the vein is mineralized, though in varying degrees, throughout the entire exposed strike length.

The Summit Camp property is favourably situated just west of Huldra Silver and has shown the existence of similar mineralized veins. From the results of the exploration program, the potential for discovering more mineralized structures is good. A follow-up program of prospecting, legal survey of the property and diamond drilling is recommended. The estimated cost of this program is \$185,500.00.

PROPERTY AND OWNERSHIP

The property is comprised of an irregularly shaped fractional claim (Southern No.8), four reverted crown grants (Sutter, Skyline, Vigo and Lulu), and three overlapping M.G.S. claims (Sky, Spike, and Amberty) totalling 29 units. The claims are situated in the Similkameen Mining Division and are held under a 50-50 option by Harrisburg-Dayton Resources Corp. and Schellex Gold Corp. The following table summarizes the pertinent claim data:

<u>Claim</u> <u>Name</u>	<u>Lot</u> <u>No.</u>	<u>Record</u> <u>No.</u>	<u>Expiry</u> <u>Date</u>
Southern No.8		461	Oct 12/89
Sutter	93	737	Sept 27/90
Skyline	94	738	Sept 27/90
Vigo	91	1053	June 25/90
Lulu	92	1054	June 25/90
Sky		1128	Aug 18/90
Spike		1215	Oct 27/90
Amberty		1671	July 9/90

LOCATION AND ACCESS

The property lies just west of Treasure Mountain, some 27 kilometers east/northeast of Hope, on NTS Map Sheet 92 H/6. The geographical coordinates of the claims are 49°25' N. Latitude and 121°45' W. Longitude.

Access to the property is by 38 kilometers of well maintained logging roads departing from the Coquihalla Highway 1.5 kilometers north of the toll booth (52 kilometers north of Hope), followed by approximately three kilometers of dirt road.



121°04'

Southern 8 Claim

VENUS SILVER

HOPE

ARGENTUM

49°25'

SKY

Huldra Silver Inc.

L 94

L 130

L 93

L 132

AMBERTY

SPIKE

Amberty Creek

OCTOPUSSY

QUEEN BESS 2

QUEEN BESS 1

Harrisburg - Dayton Properties

Volca Creek

1.0 0 1.0 2.0 km

SCALE 1:50,000

New Westminster Mining Division

Similkameen Mining Division

Harrisburg - Dayton Resource Corp.

Claim Map

SUMMIT CAMP PROPERTY

Similkameen Mining Division

NTS: 92 H/6

October, 1988

Figure 2

Boa Services Ltd.

PHYSIOGRAPHY

The Southern No.8 claim covers the lower point on an east/west - trending ridge, between Sutter and Amberty Creeks, on which Treasure Mountain is the highest point. Both creeks are part of the drainage into the Tulameen River to the east. The claim and eastern half of the optioned ground is generally moderately forested with fir, spruce and some cedar, with elevations ranging from 1402 meters above sea level to 1524 meters. The western portion of the optioned ground straddles a prominent north/south ridge linking Mount Sutter and Tulameen Mountain, with elevations to 1860 meters. Forest cover diminishes rapidly as treeline is approached at about 1830 meters. The western boundary of the property lies at the headwaters of Dewdney Creek which flows norhtwesterly for 13 kilometers to the Coquihalla River.

The area experiences moderate to heavy snowfall precluding surface exploration activity until May or June in the lower areas, July in the higher portions. There is sufficient water supply to meet exploration requirements.

HISTORY

The immediate area, known as the "Treasure Mountain", "Summit Camp" or "Silver Chief-Silver Hill" property, has seen sporadic but at times intensive activity during four periods following its discovery in 1894. Initial work was carried out from shortly after the discovery to about 1913. From 1920 to 1932 some production was realized and then in the 1950's the Treasure Mountain area again produced a minor amount from a 50 ton per day mill. During this decade Huldra Silver Inc. has been actively exploring the claims immediately east of Harrisburg-Dayton's holdings.

In 1894 to 1896, the main claims covered by the present Sky property were staked as surface mineral occurrences. In 1899 the Indiana Company was formed to include the Sutter, Skyline, Lulu and Vigo claims with assays up to 200 oz./ton silver, \$4-\$6 in gold, and copper and lead values. By 1900 inaccessibility to the area had prevented further development.

Sporadic exploration continued to 1913 when a report by G.D. Galloway on the Summit Camp area summarized some of the pertinent properties including claims on Treasure Mountain, the Indiana and Stevenson Groups (Sky property) and Halls showings. Only very small lenses of high grade had been found with clearly defined veins being preferentially hosted in limestones and slates of the Carboniferous formation. The Indiana property is described as three parallel structures, 1" to 6" wide, with some adit development. High grade assays included 0.08 oz/ton gold, 23.8 oz/ton silver and 3.6% lead. The Stevenson Group immediately to the west of the Indiana and including the Summit No. 1 claim was reported as a continuation of the Indiana structure. The Hall property to the south and west was reported to contain pyritic quartzites producing rusty beds that averaged 0.02 oz/ton gold, 0.7 oz/ton silver across four feet.

The most impressive developments were on the Treasure Mountain Mining Company's properties on Treasure Mountain. Two veins striking at N40°E cut limestone, argillite and quartz, sometimes adjacent to a porphyry dike. The galena mineralization varied from inches to four feet in width with payshoots of galena assaying up to 130 oz/ton silver. The Morningstar, Vigo and Lulu had similar but minor showings within their boundaries.

In 1919 the Indiana Company drove 340 feet of cross cuts and tunnels. In the main tunnel 3.5 feet of massive mineralization in highly siliceous argillite was found in a shoot along

20 feet of the structure. Again on the Stevenson an open cut and shaft exposed 3 feet of lead within which 10 inches of massive galena occurred. In 1920 it was reported that the Mountain View claim in the same area hosted 1,500 feet of strike length of favourable structure hosted in andesite, slate and limestone cut by diorite dykes. Assays ran as high as 22% lead and 40 oz/ton silver. However, lack of developed tonnage resulted in sporadic development and the main thrust was concentrated on Treasure Mountain (Silver Chief) property where the vein averaged 4 feet with lenses of massive lead sulfide and zinc sulfide mineralization.

Development continued on the Eureka to the west of the Silver Chief in 1924 and 43 tons of ore was shipped to the smelter.

In 1927, the Bluebell lower adit (now called the "D" adit) was driven including 224 feet of crosscutting and 102 feet of drifting on the vein. This was done 150 feet below the other workings, or "A" adit, but on the same vein.

In 1929 rehabilitation of underground workings were once again commenced on the Silver King Mining Company's Bluebell, Mary E properties and preparation for stoping was undertaken at the Silver Chief. Three carloads of sorted ore were shipped to the smelter. Mining and milling operations continued in 1930 on the Silver King Mining Company properties and approximately 79 tons of lead concentrate were shipped. However, financial trouble caused an early shutdown. Operations on the Silver King continued into 1931. It appears following the brief workings in 1932 that the camp development virtually ceased until the 1950's.

A summary of the metals shipped to the end of 1952 indicates that the Eureka and Silver Chief deposits produced 40,431 ounces of silver, 392,357 pounds of lead and 102,079 pounds of zinc from an estimated 1,300 tons of concentrates. In 1954 a 50 ton concentrator was installed to work the upper levels of the old Silver King or Mary E Mine showings. Descriptions in the 1955 Annual Report describe the activities as being primarily rehabilitation of underground workings preparation for 1956 production and by the end of the year the first zinc concentrate was shipped to the smelter. This activity was short lived and production ceased in 1957.

In 1970 the Copper Range Exploration Company Inc. conducted geochemical soil, rock, stream sediment surveys and reopened the numbers 1, 2, and 3 levels of the old Silver King Mine. No further follow up work is mentioned.

In 1982 Unicorn Resources Ltd. completed a regional soil geochemistry program that indicated some high lead geochemical trends to the north and west of the known workings. Further detailed geological assessment in the same year including detailed underground sampling and mapping. This demonstrated that the vein system being explored had sporadic higher grade mineralization. The survey also indicated an apparent metallogenic zonation from heavy zinc/pyrite mineralization to the east with increasing lead and silver values to the west.

In 1983, MPH Consultants, on behalf of Unicorn Resources Ltd., carried out a geological, geophysical, geochemical and diamond drilling program. They concluded that VLF-EM and silver/lead soil geochemistry were appropriate exploration tools for identifying high-grade silver targets. Their work delineated the Indiana Fault although they suggest that it is not a continuous structure through to the Summit area. The Summit trend is suggested to pass north of the Indiana adit, while the

Bluebell workings form another separate trend to the south. A new showing west/northwest of the Indiana adit was noted.

The Queen Bess Fault, on which is located the Mountain View adit, is also delineated but to a lesser degree and the grid did not extend far enough southwest to encompass the Queen Bess workings. A geochemically anomalous zone 200 to 300 meters southeast of the Mountain View adit, in an area of heavy overburden, has not been evaluated and may be related to the Treasure Mountain Fault.

Drilling in eight holes was concentrated on down-dip areas below the upper Bluebell, Indiana and Mountain View adits, resulting in sub-economic intersections. The best assay, from beneath the Indiana adit, was 21.2 ounces silver per ton, 4.4% lead, and 10.7% zinc over 30 centimeters.

Trenching in the area of the new showing produced encouraging assays, including 16.0 oz/ton silver, 1.7% lead, and 10.6% zinc over 1.22 meters. The fault zone was found to narrow drastically in a short distance and it was concluded that further surface work was required to delineate the zone. A 'new' adit was discovered, designated Adit "E", on a 15 centimeter mineralized fault zone which produced low assays. No work was done to investigate the extent of this zone.

In 1986, some stripping and diamond drilling was done by a private company on the ground immediately west and south of the Southern No.8 claim, but no details or records of this work are available. A narrow zinc rich vein trending eastward beside a creek was exposed near the west claim boundary of the Southern No.8 claim.

In 1987, Harrisburg-Dayton established a grid over the Southern No.8 claim in late August and conducted VLF-EM,

magnetometer and soil geochemistry surveys. The geochemistry survey indicated good potential for mineralization as some strong anomalies were delineated. Trenching was carried out in late October and exposed intermittent vein segments along a 170 meter strike trend that yielded silver values of 88.38 oz/ton and 50.9 oz/ton over 0.5 and 0.9 meters respectively.

GENERAL GEOLOGY

The most recent published regional mapping appears as Map No. 12-1969 which accompanies J.W.H. Monger's GSC Paper 69-47 on the Hope Mapsheet (west half).

Submarine volcanic and marine clastic rocks of the Devonian Hozameen Group, comprising a north/northwest trending, easterly dipping sequence, are bounded by the Fraser River fault system on the west and Hozameen fault to the east. Pelite, chert, limestone and mafic volcanic rocks are mapped.

The north/northwest trending Hozameen fault hosts numerous serpentinite, peridotite, pyroxenite bodies. Numerous gold occurrences (including the Carolin Mine) occur within the fault zone and the ultramafic rocks.

The Lower and Middle Jurassic Ladner Group pelites and volcanoclastic sandstones define a broad north/northwesterly trending syncline.

Tuffaceous and pelitic sediments of the Upper Jurassic Dewdney Group overlie the Ladner Group to the southeast and are in fault contact (Chuwanten Fault) with the Lower Cretaceous Pasayten sandstone, conglomerate and pelitic sediments in the east. The mineral deposits of the Treasure Mountain area are hosted by the Dewdney Creek and Pasayten Group rocks. Deposits are localized along faults apparently related to the Chuwanten fault system.

LEGEND

TERTIARY

MIOCENE AND EARLIER

24 Granodiorite, quartz diorite

EARLY TERTIARY AND/OR LATE CRETACEOUS

20 Foliated granodiorite, quartz diorite

CRETACEOUS

UPPER CRETACEOUS OR (?) OLDER

19 Quartz diorite

LOWER CRETACEOUS KINGSVALE GROUP

18 Basalt, andesite, agglomerate, tuff

PASAYTEN GROUP

17 Sandstone, conglomerate, pelite

JACKASS MOUNTAIN GROUP

16 16 a; sandstone pelite, and conglomerate; 16 b; sandstone, minor conglomerate

JURASSIC AND/OR LOWER CRETACEOUS

13 Foliated granodiorite

JURASSIC

UPPER JURASSIC DEWDNEY CREEK GROUP

12 12a; sandstone, pelite; 12b; tuff, pelite

LOWER AND MIDDLE JURASSIC LADNER GROUP

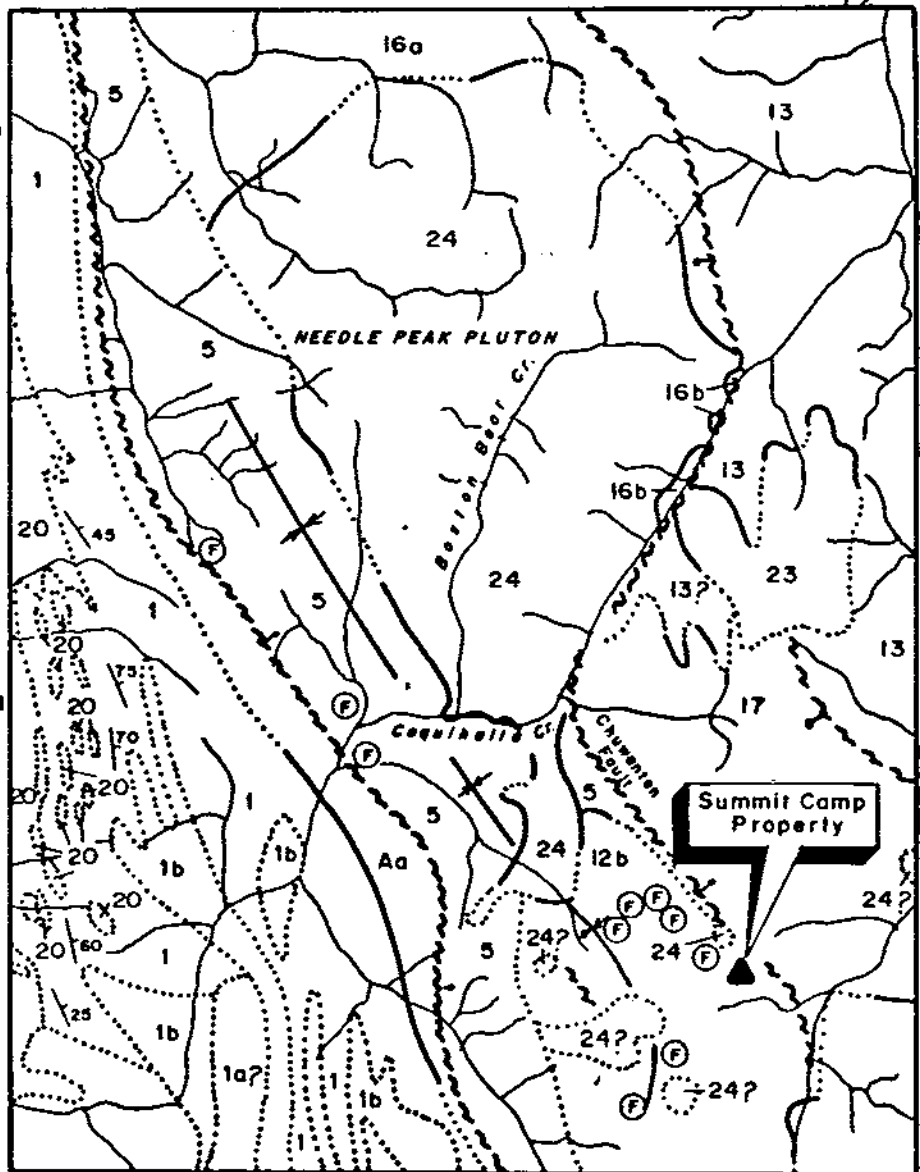
5 Pelite, volcanic sandstone

DEVONIAN (?), CARBONIFEROUS (?), AND PERMIAN (?) HOZAMEEN GROUP

1 1; pelite, chert, basic volcanic rock, minor limestone; 1a; chert, basic volcanic rock; 1b; basic volcanic rock; 1c; chert, pelite; 1d; basic volcanic rock, chert, pelite; 1e; limestone

ULTRAMAFIC ROCK

A Aa; serpentine, serpentized peridotite, includes some Upper Paleozoic volcanic rocks in broad belt northeast of Hope; Ab; pyroxenite; Ac; hornblende



Note: After G.S.C. Map 12, 1969

Harrisburg — Dayton Resource Corp.

General Geology Map

SUMMIT CAMP PROPERTY

Similkameen Mining Division

NTS: 92 H/6

October, 1988

Boa Services Ltd.

Figure 3

Numerous stocks and plugs of late Cretaceous to Miocene granodiorite and quartz diorite intrude most of the rock units in the area, including a small plug with a distinct iron-oxide halo immediately north of the Sky claim.

1988 EXPLORATION PROGRAM

The exploration program was managed by Boa Services Ltd. and conducted by personnel supplied by Harrisburg-Dayton Resource Corp. The program was divided into two separate phases. Phase I consisted of establishment of a survey control grid, soil geochemistry and VLF-EM surveys. The field work was undertaken between June 21 and July 20. Phase II consisted of road building, trenching and rock geochemistry survey. This part of the program was conducted between July 27 and September 13.

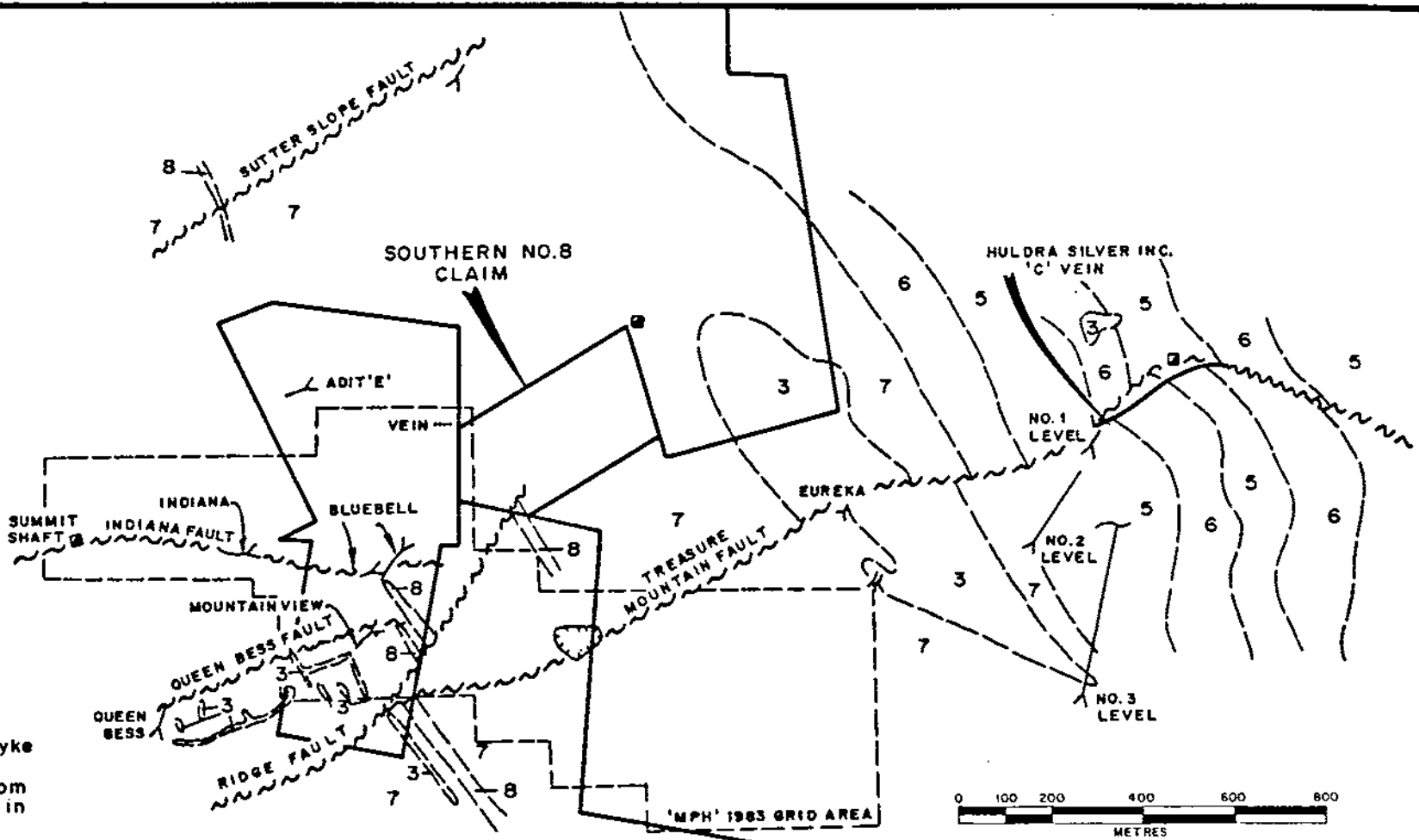
Phase I

Grid Establishment

A survey control grid was established using a compass and both a beltchain and a drag chain. The 100N by 100E origin for the grid was established to allow for a two coordinate orientation.

From the legal corner post of the Spike claim, a westerly baseline (270°) was established using a drag chain. This baseline was flagged, labelled and slope corrected for 1.85 kilometers. Survey lines were established in a north-south direction at 50 meter intervals using belt chains. Sample stations were put in at 25 meter intervals on all lines.

All together, 31.1 line kilometers of control grid was established, including 2 baselines totaling 2.9 kilometers and 28.2 kilometers of survey lines. Figure 8 shows the orientation and location of the grid.



LEGEND

- 1 Granitic intrusive
- 2 Feldspar porphyry dyke
- 3 Intrusives ranging from dioritic to gabbroic in composition, some lamprophyres

PASAYTEN FORMATION

- 4 Conglomerate, minor arkose
- 5 Arkose, minor conglomerate and argillite
- 6 Predominantly argillite

DEWDNEY CREEK FORMATION

- 7 Agglomerate, volcanic breccia, tuff, conglomerate, argillite
- 8 Predominantly argillite, minor tuff

- Defined fault
- Assumed fault
- Adit
- Contact (approximate)

Note: Property and grid location boundaries approximate only

After J.M.Black, B.C.M.M. Ann. Rpt. 1952



Harrisburg-Dayton Resource Corp.

Local Geology

SUMMIT CAMP PROPERTY

Similkameen Mining Division

NTS: 92H/6

October, 1988

Figure 4

Boo Services Ltd.

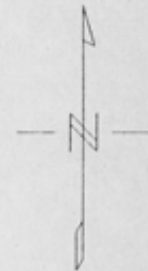
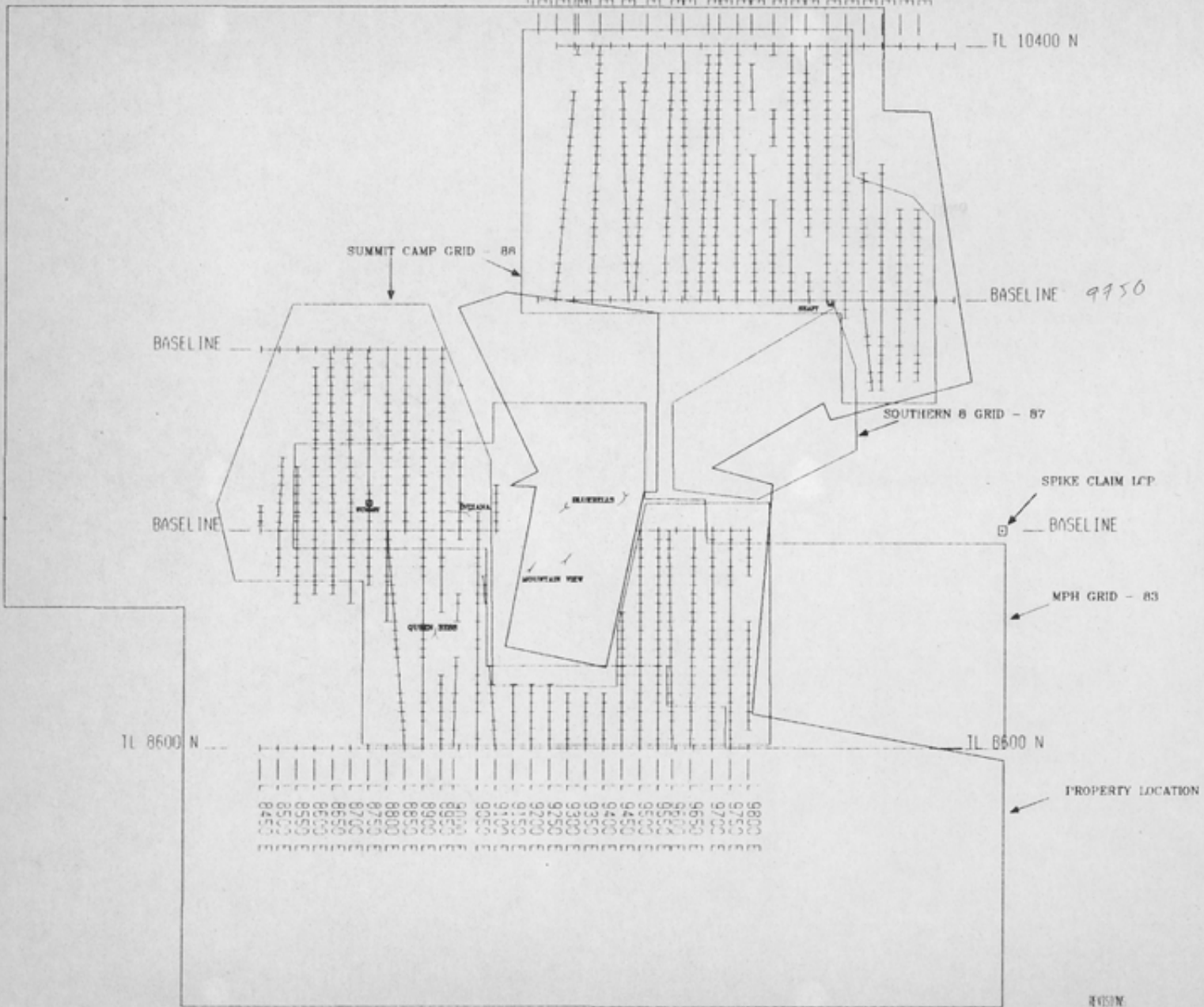
Soil Geochemistry Survey

28 kilometers of geochemical samples of the "B" and "C" soil horizons were collected over the survey control grid. A total of 966 samples were collected on a 50 x 25 meter grid. All soil samples were placed in kraft paper envelopes, field dried and delivered to Acme Analytical Laboratories in Vancouver, B.C. There, the samples were dried at 60°C, sieved to minus 80 mesh and were analyzed for 30 elements by inductively coupled argon plasma (ICP) and gold by atomic absorption (AA). The Certificate of Analysis for the soil samples accompanies this report as Appendix I.

The results of the survey were sent to Tony Clark Consulting where Mr. Clark, a doctor in geology, conducted a statistical analysis of the results and determined anomalous levels for gold, silver, copper, lead, zinc and cadmium. The histograms for these five elements are included in this report as Appendix II and value and symbol plots for gold, silver, copper, lead, zinc and cadmium are show in Figures 9 to 20.

The survey produced some very encouraging results as many samples returned anomalous values. One sample taken at L8750E 9275N produced extremely high results; but, this sample was ignored in the analysis due to its proximity to the Summit Shaft and thus probable contamination. The silver values in general were quite high as a very large proportion of samples was above the normally recognized "threshold" for B.C. of 1 ppm. A number of samples yielded results that were significantly above the anomalous levels for copper, lead, zinc and silver suggesting a possible 2nd population. However, a plot of the sample locations of this possible 2nd population didnt produce any notable trends or patterns. From the results of the survey, eight muti-element anomalous areas were identified. These anomalous zones, numbered 1 to 8 are shown on Figure 25 along with VLF conductor axes.

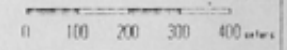
L 10200
 L 10150
 L 10100
 L 10050
 L 10000
 L 9950
 L 9900
 L 9850
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 L 9700
 L 9650
 L 9600
 L 9550
 L 9500
 L 9450
 L 9400
 L 9350
 L 9300
 L 9250
 L 9200
 L 9150



LEGEND

- ADIT
- SHAFT

SEE PROPERTY AND CLAIM MESSAGES APPROPRIATE



HARRISBURG-DAYTON RESOURCE CORP
SUMMIT CAMP

GRID LOCATION

Revised By: BOB SERVICE LTD.

Project No:	Sheet No:	Scale:	DATE:
1000	1000	1:1000	1988
1000	1000	1:1000	1988

BOB SERVICE LTD.

REVISION

No.	Date	Approved By

Anomaly 1 and 2 are parallel and trend northwesterly. The highest results from the survey was returned from these two areas including most of the anomalous cadmium samples. The best results from the two zones were 702 ppm copper, 3540 ppm lead, 3210 ppm zinc, 12.8 ppm silver, 78 ppb gold and 129 ppm cadmium. A new 30cm wide mineralized vein (Basil Vein) was found this season within anomaly 1. However, the size of the Basil Vein cannot totally account for the intensity of the anomaly, suggesting possibly a larger structure in this area. These two anomalies line up reasonably well with the Vigo vein structure on the Southern No.8 fraction and could represent a possible extension of the Vigo structure.

Anomaly 3 is a large broad zone that trends northeasterly paralleling, but mostly keeping upslope of Sutter Creek. It is also the only geochemical anomaly that is not associated with an VLF conductor. Although the values are not consistently as high as zones 1 and 2, it still carries some highly anomalous values reaching up to 304 ppm copper, 716 ppm lead, 1200 ppm zinc, 14.6 ppm silver, 128 ppb gold and 85 ppm cadmium.

Anomalies 4, 5 and 6 are relatively small, 150 to 250 meters long, northeasterly trending zones. In general, they are low in gold, cadmium and zinc values but with decent silver values. The high silver value of 51.6 ppm in anomaly 5 was near a pyritized shear zone. The best results from these three anomalies are 400 ppm copper, 1845 ppm lead, 866 ppm zinc, 63.5 ppm silver, 93 ppb gold and 14 ppm cadmium.

Anomaly 7 trends east-west and is 650 meters in length. It follows the Indiana Fault and covers the Indiana adit, the Summit shaft and a number of lead, zinc, silver showings. Except for the single sample taken by the Summit shaft, the values in general are of modest intensity. The highest values

obtained in this zone, excluding the sample by the Summit shaft, are 47 ppm copper, 1238 ppm lead, 373 zinc, 28.2 ppm silver, 28 ppb gold and 5 ppm cadmium.

Anomaly 8 is a small anomaly around the Queen Bess workings.

VLF-EM SURVEY

A total of 28.2 line kilometers of very low frequency electro-magnetic (VLF-EM) survey was completed on the property with a Geonics EM-16 receiver. Vertical in-phase (dip angle %) and quadrature (out-of-phase dip angle %) component readings were taken at 25 meter station intervals along north-south lines spaced every 50 meters. Two VLF transmitter stations were used for the survey. Cutler, Maine (24.0 KHz), as it most favourably couples with the east-west striking veins structures on the property; and Jim Creek (Seattle) Washington (24.8 KHz) to delineate possible transverse faults or mineralized structures. Chris Basil, an experienced geophysical technician, conducted the survey and interpreted the data. The operator faced north when using Cutler, and faced west when using Seattle.

Previous use of the VLF-EM on this property by MPH consultants in 1983 produced strong correlations with known vein structures and existing workings and was therefore used as the primary geophysical tool in this year's expanded exploration program. Results from this survey confirmed the usefulness of this method.

VLF-EM Results

The survey data, presented in raw data profile format and contoured Fraser filtered format can be seen in Figures 21-24, and the conductor axes are plotted on Figure 25.

Numerous conductive anomalies and cross overs were delineated by the survey. Nine anomalies, labelled "A" through "I", with peak to peak displacements of greater than 25% were judged to be of substantial interest. With few exceptions, the results from the Seattle and Cutler transmitters were nearly identical in character and extent, though the response intensity was greater with Cutler. For this reason, as well as its more favourable alignment, all interpretation, unless otherwise mentioned, is based on the Cutler data.

Conductor A extends from line 8500E to 9100E and exhibits the most intense in-phase response of over 90% peak to peak displacement. The weak to nearly zero out-of-phase response indicates a very good conductor. Spanning over 600 meters and open to the east and west, this anomaly links the Summit shaft, the open cuts to west and east of it, with the Indiana adit. The symmetrical signature, or character, of the in-phase profiles points to a near vertically dipping "sheet-type" conductor.

Conductor B extends from line 8600E to line 9000E and subparallels conductor A. Spanning 400 meters in length and open to the east and west, this structure exhibits a comparatively moderate in-phase response (42% peak to peak), though a similar quadrature signature of little to no response, suggests a good conductor. As with conductor A, the symmetrical in-phase character points to a near vertical dipping body, while the broader peak to peak width may indicate greater overburden depth. No substantial slope changes were observed on this portion of the grid, eliminating possible topographic effects, though it was noted that a sharp creek gulley/gorge parallels this anomaly 50 to 175 meters to the south.

Conductor C spans 300 meters along strike and is open to the west. It sub-parallel conductor A and most likely represents the Queen Bess workings and fault. Extreme slope conditions

(70% to 100%) weakens the interpretability of the profiles insofar as dip and conductor quality are concerned. Looking at data from a previous VLF survey, it appears likely that the Queen Bess conductor extends another 700 meters to the east and through, or closely parallel to the Mountain View workings.

Conductor D exhibits a maximum 39% peak to peak in-phase deflection and strikes ENE-WSW along 100 meter strike length. The quadrature signature, up to 50% of the in-phase response and of the same polarity, indicates a weak conductor. Conductive fluids in shear zones of faults can response in this manner, as well as poorly conductive and/or discontinuous mineralization. This conductor is on strike with a conductor delineated by the 1987 Southern No.8 geophysical program and also with the newly discovered "Basil vein" 50 meters to the northeast.

Conductor E exhibits a sharp 50% peak to peak deflection of the in-phase while the quadrature response is quite low in comparison. It strikes northeasterly for 300 meters from line 9900E to line 10200E and is open to the northeast. The ground is swampy in this region which may be the cause of this conductor, however, a stronger quadrature is usually expected from groundwater conductors.

Conductor F is a localized anomaly striking northeasterly for over 150 meters from line 9800E to 10000E. The sharp in-phase crossover and near zero quadrature response suggests a narrow conductor of small dimensions. Data obtained using the Seattle transmitter station agrees with the narrow model, but delineates a body striking NNE-SSW over 450 meters in length. As a conductor of this strike orientation should couple with Seattle very well, it is considered a more accurate view of this anomaly.

Conductor G spans 400 meters in length, strikes northeast and exhibits a sharp narrow character similar to conductor F. This anomaly may represent the Sutter Ridge Fault.

Conductors H and I both exhibit a similar signatures. Both anomalies show strong quadrature responses of the same polarity as the in-phase component indicating weak conductors. Conductor "I" appears to be of small dimension than Conductor "H".

PHASE II

Road Building and Trenching

An extension of the existing road on the property was constructed to provide access to the Indiana adit and the Summit shaft. A total of 1.3 kilometers of 4x4 road was constructed using a Caterpillar D6-D bulldozer and a 225 backhoe excavator. Due to the lack of road building material and the steepness of the hill the road has a rather steep gradient (approximately 28%) just before reaching a relatively flat area near the top of the hill. In all, the road contains 6 switchbacks and consists mostly of pebble to cobble size rocks. Figure 5 shows the orientation of the road along with the location of the two trenches.

Trenching was done in two areas along the Indiana fault employing the D6-D bulldozer and the 225 backhoe. The "Summit trench starts 74 meters west of the Summit shaft and runs generally easterly right over and past the shaft following the fault structure exposing showings discovered in precious programs for a total length of 315 meters. The trench ended in a pod of massive sulfide, but due to the steepness of the terrain, the machinery were unable to continue further along the strike of the fault. The "Indiana trench" starts at the mouth

of the Indiana adit and continues southeastward for 75 meters. Both trenches exposed the Indiana vein and showed that the vein structure is continuous and mineralized throughout the exposed strike length. Mr. J. Laird, an experience prospector directed the road construction and trenching.

The trenches exposed a continuous quartz-carbonate vein that is mineralized with sphalerite, galena, pyrite, arsenopyrite, pyrrhotite, and chalcopyrite in varying amounts, ranging from disseminations to pods of massive sulfide. The width of the vein also varies from a few centimeters to over 3 meters. The orientation of the vein is generally east-west to slightly north of east. The host rock is usually a volcanic conglomerate and volcanic sandstone with some argillite.

Rock Geochemistry Survey

A rock geochemistry survey was conducted over the two trenches. Channel samples of the vein taken at two meter intervals. The samples were collected by the writer, placed in labelled plastic sample bags and sent to Acme laboratories in Vancouver for analysis. There, the samples were crushed and analyzed using minus 100 mesh sample pulps. A 30 element ICP analysis was first used for all the samples to produce a data base and all the samples that returned high results were re-analyzed for copper, lead, zinc, silver and gold using fire assay methods. The Certificate of analysis for the rock samples form part of this report as Appendix III. In all, 200 channel samples were taken, 40 from the Indiana trench and 160 from the Summit trench. The sample locations and analytical data for the Summit and the Indiana trenches are plotted on Figures 7 and 8 respectively.

The channel samples returned some very high results and also indicates that the vein is mineralized, in varying degrees, throughout the entire exposed strike length. The highest assays from the survey for copper, lead, zinc, silver and gold are .95%, 51.58%, 22.99%, 119.80 oz/ton and .095 oz/ton respectively for the Summit trench and .32%, 34.96%, 19.39%, 60.28 oz/ton and .144 oz/ton for the Indiana trench.

Local Geology

The property is underlain by a sequence of northwest trending conglomerate and sandstone, with a high incidence of volcanic fragments, and argillite from the Upper Jurassic Dewdney Creek Group. These units have been intruded by Late Cretaceous to Early Tertiary diorite-basalt-dacite dykes and diorite intrusives.

Cross cutting quartz-carbonate vein systems are mineralized with variable amounts of pyrrhotite, sphalerite, arsenopyrite, chalcopyrite, pyrite, argentiferous galena and ruby silver. They generally have a preferred orientation of 80° within the Indiana fault and 50° in the Queen Bess fault. Thickness of the veins along the faults are variable and are controlled by host rocks and cross faulting; the vein structures demonstrates a preferred thickening within argillites and generally have epidote and sericite in the matrix and as alteration selvages.

During the exploration program, Mr. C. Basil discovered a quartz-carbonate vein with an average width of about 30 cm mineralized mostly with sphalerite with some galena and chalcopyrite. This newly discovered "Basil vein" is situated in the northeastern portion of the grid(10200E, 9725N) within geochemical anomaly 1. The vein has an orientation of 064/78N and has an exposed strike length of about 20 meters at present. The host rock is an altered lithic crystal tuff with epidote and some sericite alteration. The mineralogy is similar to the other showings on the property.

Mineralogy

Six rock specimens were taken from the Summit (S1 to S4) and Indiana (S5 and S6) trenches and were submitted to Mr. C.H.B. Leitch P. Eng, for a petrographic examination. The sample description sheets form part of this report as appendix IV. From the study, the following mineral assemblage was identified:

<u>Opaque</u>		<u>Gangues</u>
Sphalerite	Pyrite	Quartz
Galena	Chalcopyrite	Calcite
Arsenopyrite	Ruby Silver	Sericite
Pyrrhotite	Tennantite	Biotite
Marcarsite	Limonite	

Two silver-bearing minerals were observed: ruby silver, probably proustite, the arsenic end-member of the proustite-pyrargyrite series, and tetrahedrite-tennantite, again probably the arsenic end-member tennantite because of the abundant arsenopyrite present. No gold was observed in the samples, even in the arsenopyrite where it might be expected.

Sphalerite and galena are the most abundant sulfide minerals in all the specimens. They occur as very coarse-grains (about 1-2cm across), and are commonly intergrown. Sphalerite may be twinned and commonly contains minute blebs of chalcopyrite around its margins. Chalcopyrite also forms separate grains up to 1mm across, especially as inclusions within the large masses of pyrrhotite that are common within these rocks. It is with these inclusions of chalcopyrite in or around the pyrrhotite (especially near where there are also grains of galena and sphalerite) that the ruby silver and tennantite are most common. The ruby silver and tennantite are fine-grained (up to 0.2mm across, but are not badly locked with the other mineral, and so might be fairly straightforward to liberate. Minor oxidation has produced limonite (mainly goethite) in fractures cutting the sulfides.

DISCUSSION

The recent successes at Huldra Silver has generated interest in the area for high grade silver bearing veins. The general characteristics of this type of deposit are: (1) quartz-carbonate veins filling in tension fractures or lodes controlled by fault structures. (2) Their mineralogy, which include sphalerite, galena, chalcopyrite, tetrahedrite-tennantite, ruby silver, pyrite and pyrrotite. The Summit Camp property has several mineralized structures of this character, and both the Vigo and the Indiana veins have shown pockets of economic mineralization. The soil geochemical and VLF-EM surveys have delineated a number of coincident anomalous areas. All these zones trend either northeast or east-west which are the preferred orientations of the mineralized veins in this area, and the discovery of the Basil vein within anomaly 1 supports this potential. The intensity of geochemical anomaly 1 and the EM conductor in this zone would suggest a larger structure than the Basil vein, or a series of parallel structures.

CONCLUSIONS

The Summit Camp Property is favourably situated just west of Huldra Silver and investigation thus far has shown similar mineralized structures. The soil geochemistry survey identified 8 multi-element anomalous zones, 7 of which are coincident with VLF-EM conductors.

The results from the trenching program shows that the Indiana vein is mineralized for 390 meters with values ranging up to .95% copper, 51.58% lead, 22.99% zinc, 119.8 oz/ton silver and .144 oz/ton gold.

RECOMMENDATIONS

After analysis of the results, the following program is recommended for further exploration of the property:

- (1) a legal survey should be conducted to establish the boundary of the property.
- (2) prospecting, and if warranted trenching, of the anomalous zones at the northern portion of the grid.
- (3) diamond drilling of the Indiana structure exposed by the Summit trench to test for the continuity of the structure at depth.

COST ESTIMATES

Legal survey of the property	\$8000.00
Prospecting and trenching	20000.00
Assay costs	4000.00
Diamond drilling	
1350m of BQ at \$90/m all inclusive	121500.00
Management Fee	15000.00
Contingency	<u>17000.00</u>
TOTAL	<u>\$185500.00</u>

STATEMENT OF COSTS

Personnel

T. Anderson-cook			
69.5 days at \$115/day		\$7992.50	
M. Antochin-sampler			
30 days at \$115/day		3450.00	
C. Basil-geophysical technician			
54.5 days at \$150/day		8175.00	
J. Bella-labourer			
7 days at \$100/day		700.00	
P. Chung-geologist			
19 days at \$250/day		4750.00	
C. Huey-camp caretaker			
60 days at \$115/day		6900.00	
J. Huey-labourer			
9 days at \$100/day		900.00	
K. Huey-Labourer			
8.5 days at \$100/day		850.00	
J. Laird-pro prospector			
26 days at \$200/day		5200.00	
J. Owen-Labourer			
4 days at \$100/day		400.00	
C. Ridley-sampler			
10 days at \$100/day		1000.00	
D. Ridley-pro prospector			
30 days at \$165/day		4950.00	
G. Schellenberg-camp supervisor			
3 months(June-Sept) at \$1000/month		3000.00	\$48267.50

Vehicle Rental

Toyota 4x4			
4 months at \$1065/month		4260.00	
6185 km at \$.35/km		2164.75	


Blazer		
4 months at \$1448/month	\$5792.00	
4300 km at \$.35/km	1505.00	
Ford 4x4		
9 days at \$40/day	360.00	
1250 km at \$.35/km	437.50	
GMC 4x4		
14 days at \$35/day	490.00	
2952 km at \$.35/km	1033.20	
Honda 4-trax		
3 months at \$1855/month	5565.00	23,221.92
Equipment Rental		
24' trailer		
4 months at \$718.75/month	2875.00	
20' trailer		
4 months at \$568.75/month	2275.00	
Wash trailer		
4 months at \$587.50/month	2350.00	
Tent trailer		
4 months at \$262.50/month	1050.00	
Generator		
4 months at \$1250/month	5000.00	
Heaters	1050.00	
Compressor	924.46	
EM-16	200.00	
Radio		
4 months at \$200/month	800.00	
Firehose	716.54	
Skidder	809.00	
225 Excavater		
147.5 hours at \$100/hour	14750.00	
D6-D Bulldozer		
140 hours at \$79/hour	11060.00	
Mob and demob for excavator and bulldozer		
	682.00	44,542.00

Food	\$4642.03	
Transportation (freight, toll charges)	1131.58	
Consumables (fuel, oil, kerosene, flagging, soil bags, rock sample bags, etc.)	4642.03	
Tent	503.50	
Camp Mobilization	5573.10	
Camp Setup	7240.00	
Administration	327.85	
Assays	15863.3	
Recording Fees	120.00	
Management Fees	7700.00	49,691.94
		<hr/>
Total Exploration Expenditure		\$165,723.36

Report Costs

Petrographic Study	\$400.00	
Statistical Analysis	190.00	
Report Writing	1000.00	
Computer Drafting	2755.00	
Drafting	390.00	
Reproduction and Printing	150.00	
Photocopies	20.00	
Miscellaneous (courier, binding)	30.00	<u>4935.00</u>
 TOTAL COST OF PROGRAM		 <u>\$170,658.36</u>

Submitted by

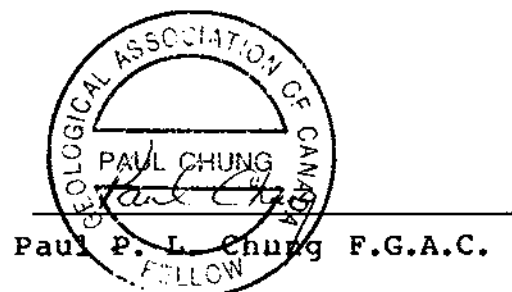


 Paul P.L. Chung, F.G.A.C.

STATEMENT OF QUALIFICATIONS

I, Paul P.L. Chung, of the City of Richmond, Province of British Columbia, DO HEREBY CERTIFY THAT:

- (1) I am a Consulting Geologist with business address office at Suite 2640-650 West Georgia Street, Vancouver, British Columbia, V6B 4N8, and President of Boa Services Ltd.
- (2) I am a graduate in geology with a Bachelor of Science degree from the University of British Columbia, in 1981.
- (3) I have practised my profession continuously since graduation.
- (4) I am a Fellow of the Geological Association of Canada.
- (5) I have conducted various mineral exploration programmes in B.C., Yukon, Manitoba, Ontario, Quebec, Nova Scotia, and Nevada.
- (6) I supervised the exploration program conducted on the Summit Camp between June 13 and September 13, 1988; and prepared this report documenting the data from this program.
- (7) I own 2,000 shares in the capital stock of Harrisburg-Dayton Resources Corp.



Dated at Vancouver, British Columbia, this 2nd day of November, 1988.

STATEMENT OF QUALIFICATIONS

I, CHRISTOPHER BASIL, of 206-960 Jervis St., Vancouver, B.C. do hereby certify that:

I am presently employed by Coast Mountain Geological Ltd. of Vancouver, as a Geophysical Projects Manager as well as a self employed private contractor.

I majored in physics at McGill University, Montreal for 2.5 years.

I have been active, full time, in my profession conducting geophysical surveys and interpreting the results for 10 years, in Canada, U.S. and Australia.

I personally conducted the 1988 geophysical program, and have based the interpretation upon this year's results and from past experience.

I hold 3000 shares of Schellex Gold Corp., which has an option for 50% of the Summit Camp properties and have based my conclusions and recommendations on professional concerns only.

Dated at Vancouver, this 2nd day of November, 1988.



Christopher Basil

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APPENDIX I

Certificate of Analysis - Soils

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 1ML 1-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR NY FE SN CA P LA CR NG BA TI B V AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JULY 11 1988

DATE REPORT MAILED: July 16/88

ASSAYER: C. Leong D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

HARRISBURG DAYTON PROJECT-SUMMIT CAMP

File # 88-2576

Page 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Mn	Co	Ni	Fe	As	J	Au	Th	St	Cd	Sb	Bi	V	Cr	P	La	Cr	Ng	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
L93E 101-00N	1	36	62	104	.6	8	4	726	4.36	142	5	ND	1	21	1	2	2	51	.50	.060	3	13	.19	44	.06	2	1.31	.01	.05	1	26
L93E 102-75N	2	44	89	72	1.3	7	6	298	4.42	143	5	ND	1	14	1	2	6	43	.15	.072	4	15	.19	24	.06	4	2.81	.01	.03	1	4
L93E 102-75N	3	27	240	157	.9	12	7	538	4.30	282	5	ND	1	10	1	4	4	64	.11	.044	3	28	.39	26	.08	2	2.85	.01	.04	1	93
L93E 102+50N	5	38	222	210	3.0	16	9	482	4.62	259	5	ND	1	9	1	2	2	55	.09	.062	7	26	.35	19	.09	2	4.79	.01	.05	1	2
L93E 102+60N	3	33	124	148	2.1	13	15	973	5.18	113	5	ND	1	13	1	2	2	54	.17	.066	4	18	.24	31	.08	2	4.32	.01	.04	1	1
L93E 101+50N	2	24	56	97	2.1	10	5	324	5.35	80	5	ND	1	10	1	2	2	59	.09	.052	4	19	.20	24	.08	5	2.77	.01	.03	1	1
L93E 101+25N	5	40	71	103	3.3	8	10	1307	7.32	163	5	ND	2	11	1	3	2	52	.13	.077	6	23	.20	24	.08	3	4.45	.01	.04	1	36
L93E 101+00N	1	33	92	321	.4	15	16	2323	4.53	118	5	ND	1	29	4	2	2	53	.74	.100	5	26	.36	44	.05	5	1.74	.01	.05	1	1
L93E 100+75N	3	21	50	177	1.0	14	9	756	4.46	19	5	ND	1	16	1	2	3	76	.24	.036	5	34	.27	29	.07	4	1.64	.01	.04	1	5
L93E 100+50N	1	16	29	73	.2	19	8	210	5.63	12	5	ND	1	13	1	2	2	100	.11	.023	4	60	.28	29	.10	2	1.95	.01	.03	1	1
L93E 100+25N	1	20	80	91	.5	20	7	272	6.09	13	5	ND	2	11	1	2	2	101	.11	.048	4	77	.33	19	.09	2	2.73	.01	.03	1	1
L93E 99+75N	2	50	210	561	1.4	41	13	607	5.14	36	5	ND	1	14	1	3	2	76	.19	.027	6	60	.77	52	.07	2	3.80	.01	.04	1	3
L93E 99+50N	6	32	527	464	3.5	14	16	4382	4.49	29	5	ND	1	10	1	2	5	73	.12	.073	5	23	.27	45	.04	6	2.56	.01	.05	1	1
L93E 99+25N	5	32	235	311	1.9	12	6	515	5.57	30	5	ND	2	11	1	2	2	72	.14	.045	4	37	.28	25	.06	9	3.65	.01	.04	1	1
L93E 99+00N	2	23	176	321	.8	23	7	503	4.27	55	5	ND	1	20	1	2	2	73	.35	.040	5	51	.56	35	.04	3	2.01	.01	.03	1	1
L93E 98+25N	2	14	43	101	.2	8	6	261	4.88	15	5	ND	1	13	1	2	6	105	.26	.026	4	36	.11	38	.07	3	1.21	.01	.03	1	1
L93E 98+00N	2	12	48	102	.3	8	5	335	5.37	16	5	ND	1	13	1	2	2	104	.25	.023	4	37	.13	30	.07	3	1.37	.01	.03	1	1
L93E 97+75N	2	16	74	151	.4	10	9	1056	4.19	23	5	ND	1	10	1	2	4	81	.14	.036	5	32	.15	26	.09	6	1.22	.01	.03	1	2
L93E 97+50N	2	37	225	352	.6	15	9	1861	2.26	65	5	ND	1	13	5	3	2	35	.27	.092	11	27	.29	41	.02	13	1.94	.01	.05	1	1
L93E 97+25N	1	19	43	61	.2	10	5	160	5.23	13	5	ND	1	11	1	2	3	76	.10	.041	4	50	.26	20	.06	7	2.55	.01	.02	1	1
L93E 97+00N	2	22	100	300	.5	12	11	5935	3.55	37	5	ND	1	21	3	2	2	56	.37	.083	8	26	.24	74	.04	4	2.25	.01	.04	2	1
L94E 103+00N	9	44	139	138	3.6	16	32	1265	3.53	93	5	ND	1	14	1	4	2	57	.17	.089	6	13	.17	43	.05	3	2.87	.01	.04	1	2
L94E 102+75N	3	222	1845	131	63.4	9	15	503	2.15	47	5	ND	1	9	3	3	2	20	.16	.145	8	9	.06	11	.03	4	4.58	.01	.02	1	4
L94E 102+25N	2	23	119	260	1.8	14	9	1639	3.67	42	5	ND	1	21	2	1	3	65	.37	.065	4	24	.33	49	.07	6	1.38	.01	.07	1	1
L94E 102+50N	2	33	164	321	1.7	18	16	1224	4.57	81	5	ND	1	20	3	2	2	63	.31	.080	6	33	.47	46	.05	2	2.53	.01	.04	1	1
L94E 101+75N	3	27	86	126	.5	21	7	311	4.50	33	5	ND	1	20	1	3	2	77	.25	.047	5	60	.41	28	.07	6	2.12	.01	.03	1	1
L94E 101+50N	2	29	83	205	1.7	25	9	434	5.20	28	5	ND	1	14	1	2	2	90	.16	.040	4	59	.49	32	.06	4	2.43	.01	.03	1	8
L94E 101+25N	3	44	130	183	1.4	14	9	928	4.51	112	5	ND	1	15	2	4	5	68	.20	.069	3	30	.37	41	.04	6	1.73	.01	.03	2	2
L94E 101+00N	4	59	122	737	2.0	34	12	1545	3.91	429	5	ND	1	26	13	3	5	53	.61	.098	13	39	.50	37	.03	4	2.87	.01	.05	1	1
L94E 100+75N	4	43	120	350	1.3	24	10	584	4.90	85	5	ND	1	18	1	3	2	74	.24	.037	5	50	.59	50	.06	4	2.45	.01	.04	1	1
L94E 103+25N	2	36	190	267	1.2	17	12	2987	4.20	24	5	ND	1	16	2	2	6	66	.28	.080	5	34	.34	65	.05	2	1.93	.01	.06	1	1
L94E 100+00N	2	35	90	302	1.2	20	11	1625	4.49	42	5	ND	1	17	2	2	5	73	.29	.064	7	45	.49	50	.05	5	2.47	.01	.05	1	1
L94E 99+50N	2	25	48	203	.7	16	11	672	4.45	23	5	ND	1	18	1	2	2	78	.29	.042	6	44	.41	39	.04	6	2.00	.01	.03	1	2
L94E 99+25N	2	28	103	203	1.1	12	10	1684	3.95	20	5	ND	1	16	1	2	2	50	.28	.061	5	30	.35	51	.03	9	1.65	.01	.05	1	1
L94E 99+00N	3	25	58	264	1.3	23	8	837	2.39	22	5	ND	1	19	1	2	3	56	.28	.049	5	40	.50	59	.04	6	1.86	.01	.05	1	1
L94E 98+75N	3	41	34	427	1.8	21	14	2839	2.38	40	5	ND	1	22	10	2	2	44	.53	.127	17	36	.40	50	.03	10	2.50	.01	.08	1	3
STD C130-9	17	57	39	152	7.1	67	28	1099	4.39	38	17	8	26	45	17	16	20	55	.46	.086	24	55	.91	171	.06	34	1.95	.06	.14	12	51

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Pb	Sn	Cd	Sb	Bi	V	Cr	P	Ca	Cl	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	PPM	%	PPM	%	%	%	PPM	PPM
L94E 98+50N	2	23	46	187	.4	23	13	1224	4.54	21	5	ND	1	17	1	2	3	80	.24	.048	6	52	.41	60	.07	4	1.74	.01	.03	1	1
L94E 98+25N	1	10	10	60	.4	8	6	251	3.55	13	5	ND	1	13	1	2	2	101	.17	.023	5	38	.14	36	.06	2	.98	.01	.02	1	2
L94E 98+00N	3	28	77	418	.8	18	12	879	5.34	32	5	ND	1	22	5	2	2	56	.56	.046	9	37	.38	49	.04	5	1.69	.01	.03	1	1
L94E 97+75N	5	15	135	372	1.5	16	12	875	4.29	46	5	ND	1	17	3	3	2	69	.27	.059	8	42	.42	43	.06	4	2.53	.01	.02	1	1
L94E 97+50N	2	34	81	120	8.0	13	11	2286	1.89	13	5	ND	1	12	3	2	2	30	.14	.125	6	23	.32	36	.01	3	1.76	.01	.03	1	2
L94E 97+00N	1	10	36	84	.9	7	11	1237	2.63	12	5	ND	1	13	1	2	4	48	.14	.046	6	26	.21	36	.04	2	1.56	.01	.02	1	1
L94+50E 104+00N	3	56	65	148	.4	17	9	239	5.00	104	5	ND	1	8	1	2	2	48	.10	.054	8	26	.23	24	.08	5	4.52	.01	.03	1	56
L94+50E 103+25N	2	31	33	81	.3	10	8	196	5.22	188	5	ND	1	15	1	2	2	46	.14	.057	2	15	.18	24	.09	5	3.08	.01	.03	1	8
L94+50E 103+00N	2	59	78	228	1.0	19	55	1040	2.19	291	5	ND	1	20	3	2	2	26	.50	.107	13	25	.22	18	.03	8	4.17	.01	.03	2	1
L94+50E 102+75N	7	23	163	596	1.2	6	5	380	4.61	87	5	ND	1	6	1	11	2	101	.06	.037	6	10	.08	20	.02	2	1.69	.01	.03	1	2
L94+50E 102+50N	5	36	731	223	5.5	9	6	334	4.04	129	5	ND	1	10	1	2	2	56	.11	.082	5	15	.18	33	.03	7	2.63	.01	.03	1	1
L94+50E 102+00N	2	27	112	385	2.0	12	11	1184	2.41	50	5	ND	1	25	10	2	2	38	.44	.072	7	20	.24	33	.02	7	1.76	.01	.05	1	1
L94+50E 101+75N	4	44	91	760	8.5	19	19	3756	3.48	110	5	ND	1	18	14	2	2	56	.35	.126	8	38	.43	36	.03	8	2.98	.01	.05	1	14
L94+50E 101+50N	1	23	72	183	2.5	9	8	2010	3.14	43	5	ND	1	11	3	2	4	48	.15	.077	6	23	.31	35	.03	7	2.12	.01	.03	1	1
L94+50E 101+25N	6	25	61	122	.5	9	7	732	3.71	19	5	ND	1	14	1	2	2	78	.25	.071	3	15	.13	55	.05	5	1.34	.01	.05	1	1
L94+50E 101+00N	4	34	133	314	2.0	18	10	772	4.13	63	5	ND	1	14	2	2	2	73	.23	.130	4	60	.32	53	.03	9	1.97	.01	.05	1	2
L94+50E 100+72N	3	47	100	444	2.4	31	19	1676	4.46	76	5	ND	1	20	2	2	2	68	.31	.075	7	44	.67	49	.04	5	2.60	.01	.04	1	1
L94+50E 100+50N	1	28	89	201	2.6	10	8	867	2.69	18	5	ND	1	18	2	2	2	49	.33	.072	3	19	.26	67	.03	5	1.16	.01	.07	1	1
L94+50E 100+25N	3	51	156	813	1.6	22	14	2812	2.55	240	5	ND	1	38	20	3	2	35	1.34	.207	17	31	.36	49	.02	9	2.46	.01	.05	1	1
L94+50E 100+00N	2	19	47	113	.2	15	9	355	4.87	26	5	ND	1	12	1	2	2	93	.13	.053	4	58	.33	33	.08	2	1.69	.01	.02	1	2
L94+50E 99+75N	2	17	41	108	.3	14	9	470	5.28	27	5	ND	1	14	1	2	2	113	.15	.052	4	55	.30	28	.10	3	1.53	.01	.04	1	1
L94+50E 99+50N	3	36	204	348	2.4	21	13	1583	3.40	70	5	ND	1	22	4	4	2	50	.46	.084	8	30	.42	42	.03	11	2.25	.01	.03	1	2
L94+50E 99+25N	2	40	78	467	1.2	21	11	2872	2.51	50	5	ND	1	32	12	3	2	35	.98	.120	15	28	.29	53	.02	10	2.02	.01	.04	1	1
L94+50E 99+00N	2	32	62	312	.5	14	12	1847	3.54	50	5	ND	1	26	5	2	4	53	.62	.096	7	37	.40	63	.03	14	1.62	.01	.04	1	1
L94+50E 98+75N	2	25	61	277	.5	17	15	2518	3.84	29	5	ND	1	25	3	3	2	62	.54	.089	6	43	.44	62	.03	3	1.77	.01	.03	1	2
L94+50E 98+50N	6	39	95	318	1.1	18	15	1641	4.57	43	5	ND	1	17	2	3	2	71	.26	.090	9	45	.47	69	.05	5	2.21	.01	.04	1	4
L94+50E 98+00N	5	25	99	316	1.2	13	12	1070	3.02	36	5	ND	1	17	3	2	3	49	.36	.057	7	31	.34	48	.04	7	1.67	.01	.02	1	1
L94+50E 97+75N	2	24	84	419	1.4	17	8	487	2.71	18	5	ND	1	15	1	2	2	51	.18	.058	5	40	.61	43	.03	8	1.52	.01	.04	1	1
L94+50E 97+25N	1	18	53	106	1.0	8	7	263	3.62	25	5	ND	1	11	1	2	6	47	.11	.053	5	35	.28	29	.05	6	2.48	.01	.04	1	2
L94+50E 97+00N	1	6	18	28	.4	2	4	160	.83	6	5	ND	1	12	1	2	5	26	.10	.016	5	15	.14	44	.05	6	.85	.01	.02	1	1
L94+50E 89+75N	1	27	42	120	.9	10	11	3586	3.24	44	5	ND	1	12	1	2	2	57	.14	.058	4	20	.20	50	.05	7	1.03	.01	.04	1	2
L94+50E 89+50N	7	27	51	419	1.4	9	9	4215	2.08	289	5	ND	1	21	7	2	2	43	.83	.073	8	20	.14	47	.03	5	1.57	.01	.03	1	4
L94+50E 89+25N	3	19	61	290	1.1	7	20	1662	4.14	74	5	ND	1	17	1	3	2	64	.25	.058	7	20	.23	60	.05	7	1.85	.01	.04	1	1
L94+50E 89+00N	8	27	40	204	1.4	10	14	1722	2.76	127	5	ND	1	20	3	2	2	39	.58	.112	11	22	.30	39	.02	11	2.45	.01	.03	1	1
L94+50E 88+75N	3	41	53	304	.8	20	13	1171	2.99	82	5	ND	1	13	4	4	2	42	.23	.079	15	30	.40	65	.03	11	2.73	.01	.07	1	2
L94+50E 88+50N	1	2	7	20	.3	2	5	119	1.77	23	5	ND	2	6	1	3	2	73	.09	.024	2	9	.36	9	.16	11	.45	.01	.02	1	1
STD C/AU-S	18	57	42	132	6.9	67	31	1044	4.11	40	14	7	37	47	17	16	19	56	.46	.089	38	55	.91	173	.06	31	1.93	.06	.14	12	52

HARRISBURG DAYTON PROJECT-SUMMIT CAMP FILE # 88-2576

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	D	Au	Tl	Sr	Cd	Sb	Bi	V	Ca	P	La	Ce	Hg	Ba	Tl	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
L94+50E 88+25N	1	37	27	74	.5	23	9	340	6.26	28	5	ND	2	11	1	2	2	103	.11	.083	5	38	.40	30	.12	5	2.22	.01	.02	1	1
L94+50E 89+00N	1	8	12	25	.5	6	1	203	1.30	5	5	ND	1	9	1	2	2	47	.08	.025	4	15	.35	26	.06	2	.69	.01	.02	2	1
L94+50E 87+75N	2	23	24	40	.7	7	5	274	6.15	18	5	ND	2	6	1	2	2	39	.06	.093	4	21	.14	15	.19	4	2.46	.01	.02	1	1
L94+50E 87+25N	1	2	6	25	.1	2	1	72	1.75	5	5	ND	1	3	1	2	2	55	.03	.009	2	8	.04	5	.11	7	.34	.01	.01	1	1
L94+50E 87+00N	1	19	22	38	.6	5	3	311	4.36	11	5	ND	1	10	1	2	2	77	.10	.061	3	16	.11	16	.11	6	1.89	.01	.02	1	1
L94+50E 85+75N	1	85	22	35	1.0	8	3	223	2.70	10	5	ND	1	6	1	3	4	30	.05	.141	4	14	.19	28	.04	5	4.47	.01	.04	1	3
L94+50E 85+50N	1	30	23	37	.6	6	4	751	5.53	15	5	ND	2	7	1	2	2	64	.08	.148	3	13	.14	16	.08	7	2.53	.01	.03	1	1
L94+50E 86+00N	3	50	180	142	1.3	8	8	1079	7.50	35	6	ND	1	14	1	2	2	86	.11	.077	3	20	.34	41	.04	5	2.66	.01	.04	1	4
L95E 102+25N	4	46	27	88	.4	13	8	271	5.27	65	5	ND	1	9	1	2	5	68	.09	.035	7	29	.32	27	.13	5	3.37	.01	.04	2	10
L95E 103+00N	3	35	26	89	.7	18	9	359	4.62	27	5	ND	2	10	1	2	5	75	.10	.035	5	35	.35	29	.11	4	2.07	.01	.03	1	1
L95E 102+50N	2	42	37	78	.5	12	5	466	3.87	52	5	ND	1	14	1	2	2	54	.13	.060	6	23	.23	39	.07	7	2.82	.01	.03	1	4
L95E 102+25N	3	50	566	886	1.6	21	8	930	5.67	109	5	ND	1	12	1	6	4	68	.12	.087	6	41	.53	41	.03	4	3.31	.01	.05	2	5
L95E 101+75N	2	21	51	77	1.0	8	3	130	4.78	42	6	ND	1	9	1	4	3	61	.07	.036	4	26	.15	24	.04	2	2.09	.01	.03	1	1
L95E 101+50N	1	38	45	158	.6	18	6	388	4.32	94	6	ND	1	15	1	2	2	68	.16	.036	5	39	.48	54	.03	3	2.43	.01	.02	1	3
L95E 102+25N	3	30	57	557	1.4	18	9	1267	2.91	57	6	ND	1	20	8	3	4	45	.32	.059	8	29	.46	47	.04	4	2.34	.01	.04	1	4
L95E 101+00N	1	28	51	137	.5	19	8	410	5.95	32	7	ND	1	13	1	2	2	86	.14	.060	5	60	.44	37	.07	3	2.76	.01	.03	1	1
L95E 100+75N	1	24	48	120	1.0	11	4	313	6.00	38	5	ND	1	13	1	2	5	96	.15	.067	4	45	.25	24	.06	3	1.83	.01	.02	1	1
L95E 100+50N	2	48	87	344	1.2	19	8	699	4.79	53	5	ND	2	17	1	2	2	68	.25	.067	5	39	.54	46	.05	7	2.84	.01	.05	1	8
L95E 100+25N	2	24	55	222	.3	11	6	548	4.75	34	6	ND	1	14	2	2	2	88	.19	.039	4	33	.24	41	.07	5	1.55	.01	.03	1	1
L95E 100+00N	1	58	95	250	.6	21	7	542	4.63	38	5	ND	1	13	1	5	2	69	.16	.048	5	43	.55	48	.04	2	1.68	.01	.03	2	7
L95E 99+75N	1	12	18	74	.2	8	4	347	3.03	7	5	ND	1	9	1	2	2	82	.09	.019	4	24	.09	19	.10	4	.88	.01	.02	1	1
L95E 99+25N	1	18	27	106	.4	9	5	596	3.62	32	5	ND	2	13	1	3	2	74	.18	.043	5	29	.23	28	.06	3	1.19	.01	.03	1	1
L95E 99+00N	3	42	98	244	1.2	17	8	951	4.62	41	5	ND	1	15	1	2	2	72	.28	.078	5	41	.35	37	.05	6	2.51	.01	.03	1	8
L95E 98+75N	4	39	89	194	1.1	14	10	1023	4.85	80	5	ND	1	18	1	2	2	83	.36	.073	6	44	.29	38	.06	4	1.97	.01	.03	1	1
L95E 98+50N	3	36	73	230	.7	25	10	558	4.28	48	5	ND	1	15	1	2	2	72	.24	.061	6	56	.54	41	.05	2	2.02	.01	.03	1	1
L95E 98+00N	14	59	716	315	4.5	15	22	7661	2.06	45	5	ND	1	26	16	8	4	31	.70	.126	15	24	.23	61	.02	6	2.37	.01	.05	1	1
L95E 97+75N	6	33	96	270	1.5	14	18	3087	5.06	63	5	ND	1	26	7	2	2	50	.80	.074	8	32	.32	56	.02	3	1.64	.01	.03	2	1
L95E 97+50N	1	27	66	183	.9	17	11	3109	3.87	31	5	ND	1	21	2	2	3	50	.38	.110	6	26	.57	76	.03	3	1.88	.01	.05	1	1
L95E 97+25N	1	22	35	91	.9	10	6	345	2.56	14	5	ND	1	11	1	2	2	42	.11	.070	7	29	.35	42	.03	5	2.06	.01	.02	1	1
L95E 97+00N	1	8	21	41	.1	6	3	151	2.08	9	5	ND	1	12	1	2	2	49	.09	.024	6	18	.25	34	.02	2	1.33	.01	.02	2	255
L95E 92+00N	9	49	82	459	.8	21	10	4349	4.02	226	5	ND	1	18	5	3	2	55	.42	.062	7	37	.83	64	.03	5	2.57	.02	.05	1	5
L95E 91+75N	35	30	37	184	2.1	13	19	11475	2.33	380	5	ND	1	46	12	2	4	34	2.20	.221	11	15	.16	100	.02	10	2.42	.01	.03	2	1
L95E 91+50N	1	15	35	112	.1	14	7	699	4.62	26	5	ND	1	12	1	2	5	71	.18	.051	5	33	.69	36	.05	2	2.04	.01	.04	1	1
L95E 91+25N	1	11	16	66	.5	8	5	477	3.48	18	5	ND	1	13	1	3	5	67	.21	.035	2	14	.36	19	.08	3	1.59	.03	.03	2	1
L95E 91+00N	2	21	49	136	.1	5	8	890	7.62	24	5	ND	2	17	1	2	4	65	.15	.039	5	19	.58	41	.11	7	2.36	.02	.06	1	1
L95E 90+75N	1	24	38	145	.3	16	8	585	4.15	23	5	ND	1	13	1	3	4	51	.18	.036	5	33	.63	43	.04	5	2.30	.02	.07	3	1
STD C.102-E	17	56	43	132	7.2	68	27	1084	4.05	39	16	3	36	47	17	17	19	56	.46	.084	38	56	.91	171	.06	33	1.92	.06	.14	13	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Hg PPM	Co PPM	Mn PPM	Fe %	As PPM	D PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	Ga PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	V PPM	Au* PPM
L95E 90+50N	2	16	42	290	.2	10	14	1771	4.40	64	5	ND	1	15	1	6	2	54	.26	.053	8	25	.36	59	.03	3	2.65	.01	.05	1	1
L95E 90+25N	2	25	63	157	.7	11	10	520	4.29	137	5	ND	1	26	1	6	2	66	1.00	.044	9	32	.36	47	.04	2	2.60	.01	.06	1	1
L95E 90+00N	5	11	29	59	.6	3	8	612	4.82	102	5	ND	1	17	1	8	2	59	.47	.042	8	11	.47	45	.02	3	3.39	.01	.02	2	1
L95E 89+75N	2	8	16	61	.1	4	7	227	5.59	36	5	ND	1	9	1	7	2	105	.11	.031	2	12	.19	15	.11	2	1.35	.01	.03	1	1
L95E 89+50N	2	17	78	189	.5	10	9	492	6.74	55	5	ND	3	9	1	6	2	71	.13	.039	3	41	.39	35	.06	5	4.71	.01	.04	1	1
L95E 88+25N	3	19	35	202	.5	8	8	349	4.87	217	5	ND	1	15	1	6	7	62	.35	.044	7	27	.27	48	.03	3	2.44	.01	.05	1	1
L95E 89+00N	2	37	35	318	1.2	23	11	2846	1.94	63	5	ND	1	32	9	3	2	27	1.06	.111	12	33	.35	62	.01	3	2.17	.01	.05	1	1
L95E 89+75N	1	17	20	87	.1	9	9	204	8.80	25	5	ND	1	10	1	5	2	169	.09	.053	4	43	.32	31	.14	3	2.67	.01	.04	1	2
L95E 88+50N	3	10	22	52	.1	5	7	229	5.88	26	5	ND	1	10	1	4	2	93	.10	.063	5	28	.19	22	.14	2	2.19	.01	.04	1	1
L95E 88+25N	3	43	17	238	.8	31	38	3026	5.13	27	5	ND	1	19	3	5	2	60	.60	.063	15	35	.36	49	.07	3	3.11	.01	.05	1	1
L95E 88+00N	1	17	29	83	.3	4	7	405	4.94	19	5	ND	1	7	1	4	2	88	.12	.045	2	12	.29	10	.08	7	1.94	.01	.03	1	1
L95E 87+75N	1	33	30	173	.4	12	37	4146	3.26	10	5	ND	1	9	1	3	2	56	.10	.066	13	23	.26	70	.09	4	2.28	.01	.03	1	1
L95E 87+50N	1	3	18	23	.6	2	5	145	1.58	2	5	ND	1	5	1	4	2	56	.07	.016	3	6	.06	9	.16	3	.43	.01	.02	1	1
L95E 87+25N	1	24	229	124	1.8	4	10	521	3.85	36	5	ND	1	8	1	6	2	61	.08	.068	2	19	.21	18	.15	3	3.90	.01	.03	2	1
L95E 87+00N	1	26	52	143	.6	10	19	1737	5.93	46	5	ND	1	12	1	6	3	91	.12	.054	4	42	.46	28	.07	7	2.81	.01	.04	1	1
L95E 86+75N	1	25	20	78	.3	11	11	966	5.38	12	5	ND	1	9	1	2	5	63	.07	.050	5	31	.46	46	.03	3	2.40	.01	.06	1	1
L95E 86+50N	1	21	27	118	.3	20	9	502	6.34	15	5	ND	1	10	1	5	2	85	.10	.058	5	61	.45	39	.07	2	4.39	.01	.04	1	1
L95E 86+25N	1	3	4	19	.1	4	4	95	1.47	2	5	ND	1	6	1	4	2	44	.05	.007	4	18	.04	6	.05	5	.40	.01	.02	1	1
L95E 86+00N	1	3	3	17	.1	3	3	54	.96	2	5	ND	1	6	1	2	2	30	.07	.006	5	13	.03	8	.03	2	.39	.01	.02	1	1
L95+50E 104+00N	2	18	28	74	.1	11	8	209	6.09	24	5	ND	1	16	1	3	4	105	.21	.061	4	43	.27	25	.13	3	1.65	.01	.03	1	1
L95+50E 103+25N	2	19	68	65	1.1	6	5	117	3.28	42	5	ND	1	8	1	5	4	51	.12	.027	3	17	.14	33	.08	5	3.37	.01	.03	1	1
L95+50E 103+00N	1	13	26	46	.3	8	6	170	3.26	9	5	ND	1	11	1	2	5	89	.12	.021	5	32	.10	25	.08	4	1.08	.01	.04	2	5
L95+50E 102+75N	1	36	31	121	.3	19	9	250	4.45	33	5	ND	1	14	1	2	2	76	.11	.034	6	39	.45	67	.06	2	3.19	.01	.04	1	4
L95+50E 102+50N	2	55	60	259	1.1	29	11	551	4.82	96	5	ND	1	18	1	4	2	69	.18	.066	6	39	.67	91	.04	2	3.42	.01	.06	1	1
L95+50E 102+25N	3	42	183	135	2.5	13	11	775	3.59	255	5	ND	1	17	2	4	6	46	.14	.079	7	20	.15	52	.04	7	2.89	.01	.05	1	1
L95+50E 102+00N	1	20	34	94	1.7	8	6	286	4.15	40	5	ND	1	8	1	3	2	82	.07	.029	6	25	.12	30	.05	5	1.59	.01	.04	1	1
L95+50E 101+75N	1	36	58	172	.8	20	10	644	5.12	66	5	ND	1	16	1	2	3	71	.15	.083	5	44	.43	44	.05	4	3.31	.01	.05	1	13
L95+50E 101+50N	7	56	418	644	10.4	17	22	1766	5.24	194	5	ND	1	17	5	12	5	66	.26	.102	10	32	.39	42	.05	4	4.79	.01	.06	1	14
L95+50E 101+25N	2	38	67	184	1.0	18	13	722	4.49	52	5	ND	1	14	1	5	2	70	.18	.053	7	39	.46	47	.04	3	2.81	.01	.04	1	1
L95+50E 101+00N	1	39	62	157	.4	18	9	670	4.28	36	5	ND	1	10	1	2	3	65	.11	.049	5	46	.42	32	.06	2	4.07	.01	.03	1	3
L95+50E 100+75N	1	55	91	386	2.6	12	9	580	5.85	40	5	ND	1	11	1	7	2	80	.11	.038	5	41	.28	28	.04	3	2.33	.01	.02	1	4
L95+50E 100+50N	3	30	71	172	.7	12	8	514	5.39	45	5	ND	1	10	1	2	2	81	.11	.048	6	35	.23	28	.07	3	2.17	.01	.03	1	2
L95+50E 100+25N	2	29	67	178	.4	9	8	707	5.07	32	5	ND	1	9	1	5	4	67	.10	.055	5	41	.25	25	.08	6	3.25	.01	.02	1	1
L95+50E 100+00N	1	31	71	301	.5	15	10	369	6.91	23	5	ND	1	13	1	2	2	102	.13	.046	6	48	.42	37	.08	3	2.80	.01	.03	1	1
L95+50E 99+50N	2	32	44	195	.6	13	8	442	5.45	25	5	ND	2	10	1	2	2	66	.12	.082	4	45	.37	36	.07	2	4.42	.01	.05	1	1
L95+50E 99+25N	2	24	76	164	.5	11	8	266	5.02	33	5	ND	1	13	1	2	2	88	.15	.042	6	34	.32	37	.05	4	2.05	.01	.03	1	1
STD C:AC-S	17	59	36	152	7.1	67	27	1041	4.09	38	18	8	37	47	18	16	19	57	.46	.089	39	58	.91	173	.06	33	1.96	.06	.13	13	51

SAMPLE	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	U PPM	Ko PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Cr %	P %	Ca PPM	Cr PPM	Ng %	Ba PPM	Ti %	B PPM	Al %	Wa %	K %	V PPM	Am ⁺ PPM
L95+50E 39+00N	4	29	55	345	1.0	11	8	958	4.50	37	5	ND	1	18	2	4	2	86	.28	.037	7	35	.29	53	.07	6	2.09	.01	.05	1	1
L95+50E 38+75N	3	29	77	314	.5	12	9	1688	4.39	25	5	ND	1	21	3	2	2	76	.39	.046	9	37	.35	79	.06	5	1.73	.01	.05	1	2
L95+50E 38+50N	8	57	165	471	1.8	13	12	1366	3.34	32	5	ND	1	20	4	3	4	67	.38	.072	26	45	.35	50	.05	8	2.38	.01	.04	1	1
L95+50E 38+25N	4	37	47	227	.6	14	10	949	3.12	40	5	ND	1	19	4	2	2	56	.42	.065	8	47	.95	33	.03	13	1.34	.01	.03	1	16
L95+50E 37+75W	7	32	109	219	1.6	10	9	709	2.58	79	5	ND	1	33	4	4	2	46	.90	.063	9	29	.32	66	.03	8	1.50	.01	.03	1	2
L95+50E 37+50W	2	43	90	294	1.4	17	23	5030	4.57	98	5	ND	1	18	2	2	2	66	.20	.105	10	49	.53	73	.04	3	2.17	.01	.04	1	1
L95+50E 37+25N	1	26	34	97	.7	12	14	6665	3.54	13	5	ND	1	18	1	2	2	46	.14	.111	6	35	.37	73	.02	5	2.05	.01	.05	1	1
L95+50E 37+00N	1	13	12	46	.4	6	4	170	3.04	11	5	ND	1	11	1	2	2	54	.07	.036	5	20	.17	40	.02	2	1.28	.01	.03	1	1
L95+50E 32+00N	6	12	48	174	1.1	11	5	275	2.80	226	5	ND	1	29	1	3	2	38	1.07	.052	9	27	.45	48	.03	7	2.48	.01	.04	3	3
L95+50E 31+75N	4	43	23	151	.6	4	9	339	9.24	21	5	ND	1	6	1	4	2	55	.09	.053	6	14	.49	15	.03	6	2.41	.01	.03	1	4
L95+50E 31+50N	1	14	14	54	.5	4	6	133	2.85	7	5	ND	1	6	1	2	2	54	.08	.033	5	10	.07	28	.03	2	1.67	.01	.03	1	3
L95+50E 31+25N	1	12	18	72	.2	7	6	542	5.02	18	5	ND	1	7	1	2	2	119	.11	.039	5	28	.30	27	.07	2	1.80	.01	.03	1	2
L95+50E 31+00N	4	23	59	176	1.6	14	23	1386	4.19	190	5	ND	1	18	1	2	2	54	.42	.057	14	32	.36	50	.03	7	3.53	.01	.04	1	2
L95+50E 30+75W	5	19	48	186	.4	10	8	276	8.01	270	5	ND	1	14	1	2	3	90	.26	.044	9	33	.42	54	.05	4	3.18	.01	.04	1	1
L95+50E 30+50N	3	8	21	84	.2	3	6	212	5.49	74	5	ND	1	15	1	3	4	66	.52	.027	7	16	.18	36	.01	2	2.07	.01	.03	1	1
L95+50E 30+25N	2	21	102	212	2.1	6	12	1125	6.74	698	6	ND	1	7	1	6	2	54	.10	.058	4	15	.41	41	.02	5	3.42	.01	.05	1	1
L95+50E 30+00N	2	21	77	292	.6	16	12	757	5.28	113	5	ND	3	25	1	3	5	72	.18	.054	5	26	.61	90	.11	4	3.37	.01	.05	1	1
L95+50E 39+75N	2	18	42	107	.5	9	7	390	9.23	43	5	ND	1	10	1	3	2	89	.09	.045	5	41	.27	32	.07	4	2.95	.01	.03	1	2
L95+50E 39+50W	3	39	52	309	1.2	18	13	2732	3.47	223	5	ND	1	27	4	2	2	46	.77	.104	15	34	.42	65	.02	5	2.83	.01	.04	1	1
L95+50E 39+25N	1	9	9	54	.1	3	4	225	2.23	20	5	ND	1	6	1	2	2	47	.12	.026	3	11	.17	22	.05	5	.91	.01	.02	1	1
L95+50E 39+00N	2	17	19	78	.3	9	7	501	6.23	33	5	ND	2	10	1	2	2	73	.09	.087	4	27	.29	24	.11	4	3.67	.01	.04	1	1
L95+50E 38+75N	2	9	21	100	.3	3	6	241	5.38	13	5	ND	1	8	1	2	2	82	.11	.042	4	23	.15	24	.10	3	1.89	.01	.03	1	1
L95+50E 38+50N	3	15	62	101	.5	6	9	469	6.82	26	5	ND	1	7	1	2	2	78	.07	.076	4	26	.14	17	.08	12	1.91	.01	.02	1	1
L95+50E 38+25N	2	12	16	88	.5	8	5	235	4.50	12	5	ND	1	12	1	2	3	86	.16	.045	4	23	.15	23	.06	2	1.53	.01	.02	1	2
L95+50E 38+00N	2	34	29	156	.2	19	10	453	4.61	27	5	ND	1	10	1	5	2	67	.12	.045	7	41	.57	53	.04	5	2.67	.01	.04	1	1
L95+50E 37+75N	1	41	46	160	.9	14	38	2085	4.60	17	5	ND	1	12	1	2	2	60	.14	.105	6	35	.54	54	.02	5	2.38	.01	.05	1	1
L95+50E 37+50N	1	20	34	175	.7	13	8	463	6.81	34	5	ND	1	10	1	5	2	106	.09	.074	4	40	.41	24	.08	4	2.02	.01	.04	1	1
L95+50E 37+25N	1	20	28	142	.7	11	7	436	5.76	15	5	ND	2	8	1	2	2	78	.08	.079	4	46	.27	28	.06	4	3.87	.01	.04	1	2
L95+50E 37+00N	1	24	26	103	2.0	13	12	6951	3.29	16	5	ND	1	15	1	2	3	59	.27	.049	7	28	.33	93	.03	2	2.08	.01	.05	1	2
L95+50E 36+52N	1	13	14	40	.3	5	6	367	4.88	10	5	ND	2	7	1	2	2	114	.07	.067	5	21	.24	27	.08	3	1.24	.01	.04	2	1
L95+50E 36+25N	1	30	31	96	.2	18	12	366	5.19	18	5	ND	2	9	1	2	2	67	.10	.088	4	40	.58	33	.06	3	4.67	.01	.03	1	1
L95+50E 36+00N	1	46	43	115	.4	19	11	522	6.17	32	5	ND	2	10	1	3	2	76	.11	.130	5	45	.72	40	.04	2	3.34	.01	.04	1	1
L96E 103+75N	1	52	38	78	1.3	7	17	176	2.95	24	5	ND	1	8	1	4	2	37	.07	.065	6	17	.13	19	.08	2	4.49	.01	.03	1	2
L96E 103+75AN	2	20	38	78	.4	7	7	250	3.67	16	5	ND	1	12	1	3	2	66	.15	.038	3	17	.19	31	.09	2	2.09	.01	.03	1	1
L96E 103+50N	2	38	37	92	.4	11	11	203	6.29	59	5	ND	2	10	1	3	2	81	.08	.046	6	32	.27	18	.14	6	5.76	.01	.03	1	2
L96E 102+25N	2	27	22	64	.6	5	5	114	3.14	10	5	ND	1	10	1	3	4	48	.12	.038	6	16	.12	17	.07	2	2.49	.01	.03	1	1
STD C/AU-8	18	57	40	102	7.1	67	28	1943	4.09	41	16	7	36	47	17	16	19	56	.46	.088	38	57	.92	171	.06	34	1.93	.06	.14	12	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mi PPM	Co PPM	Mn PPM	Fe %	As PPM	V PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Si %	K %	W PPM	Au* PPB
L96E 103+00M	2	70	28	71	1.4	10	6	120	2.79	17	6	ND	1	11	2	3	2	31	.14	.077	6	14	.11	15	.03	13	3.11	.01	.02	1	3
L96E 102+75N	1	30	43	167	.6	19	9	397	6.36	37	5	ND	2	18	1	5	2	94	.20	.038	6	57	.39	36	.08	2	2.57	.01	.04	1	16
L96E 102+50N	4	30	72	126	1.6	10	48	2563	3.98	26	5	ND	1	13	3	2	2	51	.15	.059	12	36	.15	28	.06	2	3.76	.01	.03	1	1
L96E 102+25N	2	88	1743	157	51.6	5	8	285	18.30	691	7	ND	1	24	1	373	53	51	.02	.105	2	3	.19	23	.12	2	.80	.02	.17	15	13
L96E 102+00W	1	46	49	122	1.3	20	9	531	5.93	45	5	ND	1	16	1	9	2	91	.17	.351	4	52	.45	27	.08	2	1.83	.01	.04	1	2
L96E 101+75N	1	64	238	319	4.4	15	10	541	5.74	175	6	ND	1	13	1	16	2	73	.16	.073	5	33	.37	43	.04	2	4.40	.01	.04	1	5
L96E 102+50N	1	34	113	166	3.3	14	8	357	5.55	62	5	ND	1	12	1	10	4	106	.11	.034	5	40	.27	27	.05	2	3.11	.01	.03	2	10
L96E 101+25N	2	59	100	208	1.5	15	10	500	8.12	91	5	ND	1	21	1	8	4	86	.28	.050	5	33	.30	36	.06	2	2.62	.01	.04	1	1
L96E 101+00N	1	166	71	734	1.4	43	19	775	3.47	68	5	ND	1	31	1	6	2	60	.34	.039	7	28	.89	169	.17	6	4.90	.01	.11	1	4
L96E 100+75N	1	41	71	131	2.7	14	6	259	4.46	42	5	ND	1	14	1	3	2	66	.16	.044	5	33	.31	35	.05	3	3.06	.01	.03	1	1
L96E 100+50N	1	42	55	179	1.1	17	7	325	4.59	56	5	ND	1	12	1	2	2	65	.12	.074	6	31	.42	40	.06	2	4.82	.01	.04	1	1
L96E 100+25N	1	65	81	211	1.7	23	11	740	4.69	39	5	ND	1	16	1	3	3	69	.20	.084	5	42	.56	38	.05	2	3.32	.01	.06	1	1
L96E 100+00N	2	47	58	183	2.2	19	11	848	4.24	61	5	ND	1	14	1	3	2	54	.17	.090	7	33	.48	42	.06	2	4.08	.01	.05	1	2
L96E 99+75N	1	43	77	232	.8	17	8	360	4.14	43	5	ND	1	11	1	3	2	55	.13	.052	4	39	.43	38	.06	2	4.19	.01	.03	1	4
L96E 99+50N	1	23	86	187	.9	17	7	320	6.24	38	8	ND	2	15	1	5	2	110	.14	.035	6	47	.33	32	.07	2	2.51	.01	.05	1	1
L96E 99+25N	1	14	20	66	.2	7	4	255	2.81	22	5	ND	1	10	1	2	2	86	.15	.022	4	14	.07	23	.09	3	.91	.01	.02	1	1
L96E 99+00N	22	90	235	555	5.1	18	14	8107	3.62	70	5	ND	1	20	20	4	2	58	.33	.097	17	38	.34	85	.06	3	3.12	.01	.05	2	2
L96E 98+75N	3	24	43	160	.5	11	6	363	4.49	55	5	ND	1	16	1	2	2	105	.15	.032	8	31	.19	53	.11	2	1.84	.01	.04	1	1
L96E 95+50N	10	168	590	853	5.0	18	12	6049	1.87	43	5	ND	1	39	36	4	2	29	1.11	.171	53	40	.28	96	.02	3	3.09	.01	.05	1	1
L96E 98+25N	4	37	105	474	.6	15	10	625	4.39	65	5	ND	2	31	3	9	5	79	.53	.029	13	39	.49	90	.06	3	2.06	.01	.05	1	3
L96E 98+00N	13	29	212	256	3.1	13	29	2001	4.43	89	5	ND	1	30	4	13	2	63	.74	.085	8	22	.41	50	.02	2	1.82	.01	.07	1	1
L96E 97+75N	8	36	111	374	2.9	16	9	349	2.51	56	5	ND	1	24	3	6	3	49	.55	.096	9	37	.48	52	.03	2	2.45	.01	.04	1	1
L96E 97+50N	1	46	42	201	.6	23	12	765	4.55	29	5	ND	1	15	1	3	2	59	.10	.065	7	36	.72	104	.02	2	3.34	.01	.10	1	1
L96E 97+25N	1	33	50	160	.4	20	9	1027	4.50	25	7	ND	2	16	1	2	2	58	.13	.053	6	15	.61	65	.04	2	2.14	.01	.07	1	2
L96E 97+00N	1	90	44	210	.9	27	15	926	4.47	20	5	ND	1	16	1	5	2	55	.16	.076	11	46	.70	84	.03	4	3.15	.01	.06	1	1
L96E 92+00R	2	19	52	80	1.1	7	8	321	3.58	69	5	ND	1	14	1	2	2	52	.44	.047	6	13	.11	23	.04	2	1.38	.01	.03	2	1
L96E 91+75N	3	62	36	374	.7	29	16	3326	3.90	60	5	ND	1	24	4	6	2	56	.63	.163	14	53	.60	62	.03	3	2.98	.01	.04	1	1
L96E 91+50N	1	15	28	92	.5	10	11	1309	5.52	10	5	ND	1	15	1	2	2	71	.34	.045	6	26	.20	51	.13	2	2.09	.01	.04	1	1
L96E 91+25N	1	11	7	51	.2	2	6	127	2.89	3	5	ND	1	5	1	2	2	64	.04	.023	4	12	.08	20	.05	2	1.07	.01	.02	3	1
L96E 91+25NA	5	23	7	119	.1	9	7	370	3.91	14	5	ND	1	6	1	2	2	148	.09	.032	5	25	.18	21	.03	2	1.41	.01	.02	1	2
L96E 91+00N	4	14	38	159	.1	9	9	1773	7.10	49	5	ND	1	12	1	2	2	80	.22	.066	8	22	.25	67	.08	3	2.19	.01	.04	1	2
L96E 90+75N	3	24	38	155	.4	17	12	380	5.87	47	5	ND	1	22	1	2	2	69	.17	.054	7	27	.62	90	.09	2	5.00	.01	.02	1	1
L96E 90+50N	5	24	61	257	.5	17	26	2361	4.92	143	5	ND	1	24	1	3	2	55	.63	.080	9	32	.57	76	.02	2	2.95	.01	.05	1	1
L96E 90+25N	5	26	27	164	.6	10	6	2593	1.37	109	5	ND	1	60	4	2	2	21	3.09	.113	10	17	.21	50	.01	10	1.79	.01	.03	1	1
L96E 90+00N	4	28	46	197	.9	13	12	575	4.08	541	5	ND	1	21	1	5	2	59	.61	.053	11	32	.31	41	.05	6	3.19	.01	.03	1	1
L96E 89+75N	1	16	33	126	.2	9	9	272	7.94	24	5	ND	2	10	1	2	2	94	.10	.058	4	39	.30	29	.05	2	2.37	.01	.04	1	2
L96E 89+50N	2	28	38	263	.4	23	18	2945	5.25	47	5	ND	1	22	2	2	2	76	.35	.050	3	44	.72	104	.06	2	2.66	.01	.06	1	3
STD C/AU+S	17	57	42	132	6.7	67	27	1052	4.11	40	14	8	37	47	17	16	20	56	.47	.086	38	56	.93	172	.06	32	1.94	.06	.13	14	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	U PPM	Au PPM	Tl PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Tl %	B PPM	Al %	Na %	K %	W PPM	Au# PPM
L96E 59+25N	2	20	30	253	.4	11	8	749	5.92	143	5	ND	1	18	1	2	2	93	.44	.046	7	30	.36	67	.07	2	2.98	.01	.02	1	1
L96E 59+00N	1	22	35	101	.4	19	7	266	5.46	28	5	ND	1	10	1	2	2	80	.12	.043	4	51	.37	31	.07	3	3.31	.01	.04	2	1
L96E 88+75N	1	15	12	55	.1	13	6	970	4.25	14	5	ND	1	8	1	2	2	84	.07	.061	4	36	.21	16	.08	2	1.23	.01	.02	1	1
L96E 98+50N	1	11	17	69	.3	9	5	399	4.94	10	5	ND	1	9	1	2	2	91	.10	.044	4	32	.20	18	.08	2	1.36	.01	.04	1	2
L96E 58+25N	1	23	20	101	.1	16	10	397	5.56	33	5	ND	1	14	1	2	2	84	.17	.045	5	38	.41	57	.10	2	1.91	.01	.04	1	1
L96E 38+00N	2	52	29	260	.9	28	20	4879	4.50	31	5	ND	1	28	3	2	2	43	.74	.139	21	31	.53	101	.03	5	3.46	.01	.05	1	1
L96E 87+75N	1	17	22	82	.8	9	5	192	4.78	15	5	ND	1	13	1	2	2	64	.15	.037	6	26	.20	43	.07	2	2.03	.01	.02	1	4
L96E 37+50N	3	63	31	181	.8	10	14	3172	2.72	33	5	ND	1	25	3	2	2	44	.53	.077	16	29	.20	37	.04	8	2.59	.01	.03	1	1
L96E 37+25N	1	12	79	151	1.4	3	5	539	3.73	14	5	ND	1	8	1	2	4	36	.14	.035	4	17	.11	21	.03	2	1.38	.01	.03	1	1
L96E 87+00N	1	39	36	83	.5	15	7	390	5.51	17	5	ND	2	7	1	2	4	49	.06	.078	5	55	.28	32	.03	2	6.05	.01	.03	1	2
L96E 95+75N	2	60	36	67	.3	21	11	439	6.71	71	5	ND	1	6	1	3	2	60	.09	.103	3	64	.36	21	.07	2	5.35	.01	.02	1	1
L96E 86+50N	1	14	25	38	.4	5	2	151	3.94	11	5	ND	1	4	1	2	2	73	.05	.038	3	15	.19	10	.15	2	1.77	.01	.02	1	1
L96E 36+25N	1	15	25	73	.1	7	4	230	3.68	12	5	ND	1	7	1	2	2	58	.06	.055	4	31	.26	29	.04	2	2.98	.01	.02	1	3
L96E 86+00N	1	21	37	105	.4	8	6	330	5.69	57	5	ND	2	6	1	4	2	80	.08	.067	4	40	.31	29	.10	2	4.01	.01	.03	1	1
L96+50E 124+00N	1	17	18	55	.4	7	4	1030	2.22	9	5	ND	1	11	1	2	2	50	.16	.055	4	17	.09	38	.07	6	1.10	.01	.04	1	1
L96+50E 193+75N	1	20	23	102	.3	11	11	604	3.39	35	5	ND	1	23	1	2	2	57	.14	.040	3	21	.31	50	.10	3	1.68	.01	.02	1	1
L96+50E 103+50N	1	22	24	99	.5	11	8	288	4.95	26	5	ND	1	12	1	2	2	80	.15	.031	5	27	.18	21	.08	2	2.65	.01	.02	1	1
L96+50E 133+25N	1	21	54	170	.3	13	6	261	5.24	39	5	ND	1	10	1	2	2	88	.11	.033	4	36	.28	22	.12	2	1.96	.01	.03	1	1
L96+50E 103+00N	1	15	27	84	.3	8	4	280	3.06	28	5	ND	1	10	1	2	2	105	.10	.041	6	25	.14	32	.16	4	1.16	.01	.04	1	1
L96+50E 162+75N	1	48	189	277	2.5	8	7	463	10.56	185	5	ND	2	8	1	1	3	75	.10	.083	4	29	.35	20	.09	2	2.83	.01	.03	1	1
L96+50E 102+50N	1	28	134	194	1.1	7	38	1209	4.63	128	5	ND	1	13	1	2	3	72	.15	.054	4	21	.22	65	.08	2	1.67	.01	.02	1	2
L96+50E 182+25N	1	18	14	54	1.7	4	3	172	3.97	11	7	ND	1	8	1	3	2	55	.11	.041	2	11	.07	16	.07	2	1.35	.01	.03	2	1
L96+50E 102+00N	1	75	72	300	2.1	20	61	4014	3.73	85	5	ND	1	17	5	2	7	49	.23	.074	10	28	.33	48	.04	6	3.19	.01	.03	1	1
L96+50E 101+75N	1	41	110	181	2.2	15	8	538	5.31	46	5	ND	1	9	2	3	4	69	.10	.043	4	47	.28	24	.07	3	4.27	.01	.03	1	1
L96+50E 101+50N	1	38	78	191	1.4	16	8	444	5.29	36	5	ND	1	10	1	4	7	65	.11	.090	4	40	.36	38	.07	5	4.62	.01	.03	1	1
L96+50E 101+00N	4	152	172	135	4.0	13	7	618	6.84	105	5	ND	1	9	2	4	2	88	.13	.073	8	45	.21	27	.07	2	5.50	.01	.03	1	1
L96+50E 100+75N	1	37	52	113	1.2	14	5	349	4.27	42	5	ND	1	10	1	2	3	59	.11	.071	4	33	.28	29	.05	4	3.08	.01	.03	1	2
L96+50E 100+50N	1	46	60	214	1.5	21	11	833	4.09	44	5	ND	1	14	1	2	4	62	.17	.067	7	46	.60	49	.05	5	2.94	.01	.03	1	1
L96+50E 190+25N	2	27	68	136	.9	14	6	374	6.39	48	5	ND	1	10	1	2	2	84	.10	.034	4	41	.35	28	.05	2	2.23	.01	.03	1	1
L96+50E 160+00N	1	29	55	137	.3	12	5	337	5.18	57	5	ND	2	7	1	2	8	54	.09	.072	4	37	.33	32	.06	2	5.86	.01	.03	1	1
L96+50E 99+50N	4	38	49	265	2.8	23	8	293	5.04	41	5	ND	1	17	2	2	2	63	.25	.059	5	45	.66	47	.06	2	3.27	.01	.04	1	1
L96+50E 99+25N	5	29	62	286	.3	12	6	293	6.37	66	5	ND	2	12	1	2	2	74	.11	.031	5	32	.33	44	.11	8	2.82	.01	.04	1	1
L96+50E 99+00N	4	41	90	324	1.5	12	8	1264	3.90	59	5	ND	1	18	2	3	4	58	.25	.044	9	29	.35	49	.05	2	1.78	.01	.04	1	2
L96+50E 98+75N	5	88	246	754	2.3	19	16	1349	5.35	172	5	ND	1	25	7	8	6	66	.43	.068	17	41	.60	76	.05	2	2.85	.01	.04	1	2
L96+50E 98+50N	8	89	361	772	6.3	11	22	6265	2.57	74	5	ND	1	32	20	3	4	36	.88	.101	20	33	.23	71	.02	2	3.25	.01	.03	2	1
L96+50E 98+25N	13	37	147	406	1.9	13	15	2174	4.09	109	5	ND	1	20	4	15	5	60	.38	.073	9	33	.39	71	.03	4	2.45	.01	.04	2	1
STD D78D-S	17	59	40	132	7.2	67	28	1045	4.39	38	15	7	36	46	17	16	19	56	.46	.086	39	55	.91	172	.06	32	1.96	.06	.13	12	50

SAMPLE#	NO	CU	PD	CD	AG	NI	CO	KC	FE	AS	V	AU	TH	SR	CD	SB	BI	Z	CA	P	LA	CR	KG	BA	TI	S	AL	HA	K	W	AU*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
L96+50E 93+00N	1	31	30	62	1.0	7	5	623	1.59	7	5	ND	1	9	1	2	3	27	.07	.052	7	17	.15	34	.01	4	1.63	.01	.03	1	1
L96+50E 93+75N	1	40	57	147	.3	12	19	2239	4.23	24	5	ND	1	13	1	2	4	54	.09	.075	9	40	.41	78	.02	5	3.12	.01	.06	2	1
L96+50E 97+50N	1	33	19	102	1.1	17	6	422	3.12	11	7	ND	1	14	1	2	2	51	.11	.049	8	30	.45	47	.03	3	2.80	.01	.04	1	1
L96+50E 97+25N	1	21	28	123	.9	16	8	524	4.11	13	6	ND	1	14	1	2	2	60	.12	.049	8	37	.55	50	.04	6	3.22	.01	.02	1	2
L96+50E 97+00N	2	37	28	137	1.1	19	9	645	3.34	16	5	ND	1	15	1	2	5	53	.13	.055	8	37	.62	53	.05	2	3.25	.01	.05	1	1
L96+50E 90+00N	2	26	24	93	.6	14	3	312	7.41	26	5	ND	2	16	1	2	2	108	.22	.047	7	48	.36	36	.13	11	2.17	.01	.03	1	1
L96+50E 91+50N	1	22	33	143	.5	11	8	354	8.25	23	6	ND	1	10	1	2	2	95	.09	.046	5	42	.28	47	.06	2	2.28	.01	.02	2	1
L96+50E 91+25N	1	18	17	132	.2	9	7	665	3.62	57	5	ND	1	12	1	2	2	73	.26	.035	5	17	.16	14	.04	3	1.45	.01	.03	1	1
L96+50E 91+00N	2	23	23	142	.5	17	8	527	7.25	34	6	ND	2	9	1	2	2	117	.15	.077	5	54	.39	22	.04	2	1.99	.01	.04	1	2
L96+50E 92+75N	4	70	57	966	.5	41	11	1532	4.23	172	5	ND	2	21	7	5	2	53	.32	.061	30	43	.45	96	.04	3	3.23	.01	.06	2	3
L96+50E 90+50N	28	72	46	629	1.6	46	15	16773	3.33	405	5	ND	1	43	44	3	2	49	1.33	.249	27	30	.36	219	.02	13	3.07	.01	.04	1	3
L96+50E 90+25N	3	17	29	90	.1	6	5	308	3.37	123	5	ND	2	8	1	3	5	62	.14	.022	5	24	.16	25	.02	2	1.69	.01	.02	1	1
L96+50E 90+00N	4	17	40	224	.7	10	7	233	4.92	254	5	ND	1	20	1	2	2	63	.47	.024	7	29	.38	54	.03	4	2.27	.01	.03	1	1
L96+50E 89+75N	4	26	34	191	.7	12	7	235	7.27	706	5	ND	2	25	1	2	2	93	.76	.026	7	36	.31	52	.05	2	2.08	.01	.04	1	1
L96+50E 89+50N	34	34	74	228	2.2	10	35	12465	5.52	846	5	ND	1	11	8	2	2	75	.21	.147	27	36	.11	103	.04	3	5.26	.01	.04	15	1
L96+50E 89+25N	1	25	30	150	.7	16	13	741	4.09	57	5	ND	1	18	1	2	2	67	.31	.049	9	34	.36	74	.03	3	2.08	.01	.04	1	1
L96+50E 89+00N	6	42	53	300	1.2	16	16	3440	3.32	214	5	ND	1	36	9	2	2	39	1.22	.110	17	29	.23	60	.02	3	2.88	.01	.03	2	1
L96+50E 88+75N	1	11	6	30	.7	5	4	98	1.57	3	5	ND	1	4	1	2	2	44	.04	.015	5	12	.04	15	.05	8	.46	.02	.02	1	1
L96+50E 88+50N	1	20	23	107	.9	18	8	699	4.59	31	5	ND	1	18	1	2	2	74	.30	.055	8	39	.58	64	.04	5	2.24	.01	.05	1	1
L96+50E 88+25N	1	22	19	113	.4	13	8	263	4.72	17	5	ND	1	20	1	2	2	72	.32	.052	7	36	.48	70	.03	2	2.19	.01	.05	1	2
L96+50E 88+00N	3	25	71	50	1.9	5	36	6893	3.41	16	5	ND	1	13	1	3	3	51	.25	.137	8	37	.17	30	.03	9	2.91	.02	.02	1	1
L96+50E 87+75N	1	11	19	58	.5	4	5	255	3.54	7	5	ND	1	7	1	3	2	55	.06	.039	4	20	.13	30	.02	4	1.56	.01	.02	1	2
L96+50E 87+50N	1	18	33	68	1.9	5	6	453	1.33	5	5	ND	1	39	1	2	3	18	1.93	.106	9	14	.18	70	.01	5	1.44	.01	.03	1	1
L96+50E 87+25N	1	37	22	72	1.2	10	8	255	1.21	8	5	ND	1	16	1	2	2	18	.25	.157	14	20	.22	35	.01	17	3.26	.01	.04	1	1
L96+50E 87+00N	1	23	18	101	.3	14	14	2770	3.98	13	5	ND	1	20	1	2	3	72	.36	.031	7	37	.43	67	.06	3	1.96	.01	.05	1	1
L96+50E 85+75N	1	24	25	84	1.0	7	7	439	5.77	16	5	ND	1	7	1	2	2	57	.09	.058	5	32	.24	24	.08	2	5.42	.01	.02	1	3
L96+50E 86+50N	1	17	23	96	.4	9	6	365	7.66	11	5	ND	2	10	1	2	4	131	.08	.052	5	39	.31	26	.09	2	2.52	.01	.03	1	2
L96+50E 86+25N	1	39	28	176	.4	26	11	466	4.50	16	5	ND	1	13	1	1	2	77	.18	.047	6	46	.62	47	.06	6	2.89	.01	.04	1	6
L96+50E 86+00N	1	22	21	118	.6	11	7	448	5.53	18	5	ND	2	10	1	2	2	70	.12	.037	5	38	.35	33	.06	12	3.96	.01	.03	1	1
L97E 104+00N	1	21	19	58	.1	4	7	822	5.24	30	5	ND	1	12	1	2	5	93	.12	.050	3	25	.25	44	.08	2	1.95	.01	.04	1	7
L97E 103+75N	1	24	26	137	.5	21	9	287	5.17	62	5	ND	2	11	1	2	2	81	.11	.036	4	69	.27	35	.07	3	4.35	.01	.03	1	1
L97E 103+50N	1	22	23	135	.4	22	8	312	5.20	58	5	ND	1	11	1	2	2	90	.12	.036	4	70	.37	33	.07	6	4.52	.01	.03	1	1
L97E 103+25N	1	46	30	117	1.3	5	5	356	6.46	797	5	ND	1	9	1	9	5	87	.12	.052	5	22	.16	37	.12	2	1.37	.01	.03	1	2
L97E 102+00N	1	21	48	132	3.0	9	6	573	6.38	21	5	ND	2	14	1	2	4	100	.14	.143	6	34	.23	36	.12	2	2.06	.01	.06	1	2
L97E 102+75N	1	15	44	144	.4	7	7	230	7.83	16	5	ND	2	9	1	3	2	101	.09	.047	6	36	.24	26	.14	2	2.41	.01	.03	1	1
L97E 102+50N	1	17	18	110	.3	8	4	250	5.55	19	5	ND	1	9	1	2	2	107	.11	.063	4	31	.21	20	.11	2	2.42	.01	.02	1	1
STD C-140-3	17	57	48	132	6.3	68	29	1039	4.27	37	18	7	37	47	17	16	18	56	.46	.089	39	56	.91	172	.06	23	1.94	.06	.13	12	49

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Bi	Co	Ni	Pb	As	U	Au	Tb	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	B	Al	Na	K	W	Au*	PPS
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPS	
197E 100+25N	1	20	22	78	2.4	12	14	1841	4.46	15	5	ND	1	10	1	4	5	64	.11	.066	3	20	.28	33	.14	7	2.24	.01	.04	1	69	
197E 101+25N	1	15	43	107	.4	11	7	290	4.73	16	5	ND	1	8	1	5	3	84	.09	.041	3	34	.18	24	.09	2	2.28	.01	.03	1	5	
197E 101+50N	1	10	42	64	.5	6	6	265	6.07	28	5	ND	1	10	1	4	2	107	.13	.062	2	24	.18	20	.13	2	1.94	.01	.01	1	1	
197E 101+25N	1	10	32	89	.3	13	7	230	6.56	16	5	ND	1	12	1	4	2	89	.12	.040	3	47	.21	19	.09	2	1.88	.01	.03	1	1	
197E 101+00N	1	52	70	333	.3	32	11	342	6.48	161	5	ND	1	14	1	8	2	81	.16	.041	3	85	.68	38	.07	3	3.58	.01	.04	1	3	
197E 100+75N	1	10	36	187	.5	19	9	182	5.99	25	5	ND	1	12	1	4	2	99	.14	.039	3	67	.29	32	.09	8	2.30	.01	.03	1	1	
197E 100+50N	3	34	162	146	7.5	12	17	400	5.04	68	5	ND	1	9	1	6	4	79	.10	.035	6	28	.21	25	.07	4	2.35	.01	.03	1	1	
197E 100+25N	2	109	126	371	3.6	17	18	1708	3.52	139	5	ND	1	20	5	6	2	52	.29	.068	7	29	.43	45	.04	10	2.57	.01	.03	1	1	
197E 100+00N	2	45	99	241	2.7	11	8	921	3.19	58	5	ND	1	16	2	7	2	61	.21	.063	5	30	.36	39	.05	4	2.48	.01	.04	1	11	
197E 99+75N	3	35	151	193	2.0	9	16	2837	6.77	339	5	ND	1	28	5	4	2	70	.39	.152	7	20	.18	48	.01	8	1.64	.01	.03	1	1	
197E 99+50N	1	24	62	190	1.0	12	7	333	4.78	49	5	ND	1	13	1	4	3	70	.15	.076	4	29	.38	44	.07	3	3.14	.01	.04	1	1	
197E 99+25N	2	28	94	296	.9	14	8	743	2.26	26	5	ND	1	18	1	4	3	40	.24	.064	6	32	.55	48	.03	3	2.67	.01	.04	1	32	
197E 99+00N	4	43	410	148	2.0	5	18	5117	3.68	35	5	ND	1	16	3	2	3	50	.27	.103	8	23	.16	35	.04	6	2.68	.01	.03	1	1	
197E 98+75N	5	55	570	200	14.6	7	14	3164	2.95	82	5	ND	1	12	2	3	6	37	.25	.111	8	30	.21	24	.03	9	3.83	.01	.02	1	1	
197E 98+50N	1	19	35	74	.6	12	7	197	6.80	20	5	ND	1	14	1	4	2	91	.11	.042	5	37	.33	35	.08	8	1.79	.01	.03	1	1	
197E 98+25N	1	28	64	153	.4	10	6	187	5.17	24	5	ND	1	9	1	4	2	72	.09	.045	4	39	.22	32	.06	16	1.85	.01	.03	1	1	
197E 98+00N	4	30	103	268	1.1	15	8	1437	2.10	34	5	ND	1	23	8	5	2	31	.51	.075	8	27	.32	53	.02	6	1.52	.01	.03	1	1	
197E 97+75N	1	33	46	117	1.0	13	12	1014	4.60	19	5	ND	1	10	1	2	6	48	.12	.112	8	30	.44	34	.03	5	3.01	.01	.04	1	1	
197E 97+50N	1	24	35	134	.5	11	7	566	3.40	17	5	ND	1	10	1	4	3	43	.08	.061	7	25	.45	63	.02	4	2.61	.01	.05	1	1	
197E 97+25N	1	10	17	50	.6	3	4	222	2.20	5	5	ND	1	6	1	3	2	38	.04	.030	5	12	.09	33	.01	2	1.24	.01	.02	2	2	
197E 97+00N	1	32	44	131	.3	15	8	418	5.99	25	5	ND	2	9	1	2	2	55	.09	.059	4	33	.47	40	.03	4	2.33	.01	.04	2	1	
197E 92+00N	1	7	13	33	.3	13	6	156	2.83	2	5	ND	1	11	1	2	3	90	.10	.017	2	53	.20	19	.08	4	.85	.01	.02	1	1	
197E 91+75N	1	19	21	88	.5	15	6	210	6.44	62	5	ND	1	9	1	3	2	105	.07	.037	3	65	.39	19	.05	10	1.94	.01	.03	1	1	
197E 91+25N	2	16	27	47	.1	7	7	131	7.96	9	5	ND	2	7	1	3	2	130	.06	.016	4	44	.16	21	.14	2	2.06	.01	.02	1	1	
197E 91+00N	1	12	27	43	1.6	6	3	126	1.77	7	5	ND	1	6	1	2	2	42	.10	.034	5	13	.08	24	.01	3	1.16	.01	.01	1	1	
197E 90+75N	1	9	26	67	.2	10	5	230	3.73	4	5	ND	1	5	1	2	2	70	.05	.025	5	27	.14	18	.05	6	1.53	.01	.02	1	2	
197E 90+25N	3	15	29	139	.2	10	7	605	5.85	50	5	ND	1	15	1	3	2	78	.25	.053	4	34	.25	39	.10	5	1.59	.01	.03	1	1	
197E 90+00N	1	21	26	97	.7	10	6	423	6.09	26	5	ND	1	9	1	8	2	82	.10	.080	4	29	.25	25	.04	3	1.52	.01	.03	1	1	
197E 89+75N	1	11	17	59	.3	4	3	114	2.47	8	5	ND	1	10	1	2	2	42	.19	.023	3	13	.14	22	.03	3	.89	.01	.03	1	1	
197E 89+50N	4	44	39	374	.8	20	10	4279	1.56	67	5	ND	1	29	8	2	2	45	.88	.088	11	31	.38	74	.02	7	2.12	.01	.03	1	2	
197E 89+25N	4	41	38	339	.3	20	5	2435	2.84	255	5	ND	1	43	4	4	2	30	1.66	.070	9	17	.52	57	.01	10	1.53	.01	.06	1	1	
197E 89+00N	12	89	10	440	.7	39	2	2316	.24	32	5	ND	1	92	7	6	2	7	4.33	.093	9	14	.07	40	.01	16	.70	.01	.04	2	2	
197E 89+75N	8	21	23	140	1.6	9	8	1074	1.53	111	5	ND	1	38	2	2	2	20	1.50	.080	13	21	.17	56	.02	4	1.73	.01	.05	4	1	
197E 89+50N	8	30	31	199	.3	14	26	4768	9.01	96	5	ND	1	15	2	2	2	65	.26	.083	12	42	.44	78	.02	2	2.83	.01	.03	1	1	
197E 88+25N	2	17	46	93	1.4	11	11	10127	2.66	9	5	ND	1	22	2	2	2	36	.53	.083	11	21	.28	136	.02	5	2.92	.02	.06	1	1	
197E 88+00N	1	14	30	58	2.6	9	16	408	1.97	5	5	ND	1	11	1	2	2	33	.12	.038	6	12	.19	48	.03	2	1.31	.02	.05	1	1	
STD C.AZ-S	17	58	38	132	7.1	68	28	1057	4.08	40	17	7	36	45	17	16	18	55	.46	.085	38	56	.91	171	.06	34	1.93	.06	.13	12	51	

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	B PPM	Au PPM	Tl PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPM
L97E 27-75N	1	8	14	41	.7	8	4	99	2.08	3	5	ND	1	12	1	2	2	39	.15	.050	4	17	.16	54	.03	2	1.07	.01	.05	1	1
L97E 37-50N	1	8	1	16	.2	8	5	80	2.66	2	5	ND	1	6	1	2	3	68	.04	.014	5	19	.08	16	.02	2	.87	.01	.02	1	1
L97E 87-25W	1	31	36	116	2.0	10	165	8118	2.17	8	5	ND	1	22	4	2	2	19	.45	.155	14	15	.78	46	.01	2	2.67	.01	.06	1	1
L97E 37-00W	1	1	9	23	.3	9	5	156	1.35	2	5	ND	1	7	1	2	2	44	.08	.015	3	21	.05	15	.03	2	.41	.01	.02	1	1
L97E 36-75N	1	2	2	17	.2	3	3	49	1.04	3	5	ND	1	6	1	2	2	33	.04	.011	4	12	.05	15	.01	2	.57	.01	.02	1	1
L97E 36-50N	1	1	4	19	.1	2	2	41	.73	2	5	ND	1	2	1	2	2	26	.02	.010	3	5	.03	7	.05	2	.35	.01	.01	1	1
L97E 36-25N	7	24	68	172	1.0	17	52	2452	5.95	36	5	ND	1	13	2	2	2	73	.26	.043	4	25	.50	52	.06	2	2.61	.01	.04	1	1
L97E 36-00N	1	18	39	84	.4	12	7	310	7.30	17	5	ND	1	7	1	2	2	104	.09	.030	3	34	.42	28	.06	2	2.27	.01	.04	1	1
L97-50E 91-00N	1	21	43	113	.3	13	8	562	5.39	27	5	ND	1	9	1	3	2	76	.10	.045	4	35	.48	38	.02	2	2.07	.01	.04	1	1
L97-50E 91-75N	1	26	49	165	.4	17	9	391	6.83	28	5	ND	1	9	1	4	2	65	.10	.079	3	43	.55	38	.03	2	3.58	.01	.04	1	1
L97-50E 91-50N	1	13	36	136	.4	7	7	171	7.42	13	5	ND	1	11	1	2	2	114	.18	.066	5	29	.19	43	.04	2	2.03	.01	.03	1	1
L97-50E 91-00N	1	16	24	132	.3	10	7	160	5.42	10	5	ND	1	12	1	2	2	69	.16	.035	4	38	.23	28	.03	2	2.32	.01	.02	1	1
L97-50E 90-75W	1	10	26	105	.5	10	8	221	6.19	15	5	ND	1	8	1	2	2	84	.08	.047	4	30	.24	27	.05	2	2.25	.01	.03	1	2
L97-50E 90-50N	1	28	78	241	.6	8	3	289	.73	10	5	ND	1	73	5	2	2	10	3.01	.104	6	10	.10	32	.01	7	.67	.01	.05	1	1
L97-50E 89-50N	1	14	25	153	.4	16	9	695	2.10	44	5	ND	1	17	2	2	2	28	.44	.074	7	20	.47	41	.02	3	1.51	.01	.03	1	1
L97-50E 89-25N	1	6	2	58	.3	5	3	29	.20	2	5	ND	1	35	1	2	2	5	.37	.074	4	1	.03	128	.01	2	.60	.01	.02	1	1
L97-50E 89-00N	1	35	34	125	.2	28	14	642	3.52	17	5	ND	1	14	1	4	2	54	.19	.058	7	42	.83	53	.03	2	2.81	.01	.04	1	5
L97-50E 88-75N	1	16	22	49	.2	6	7	158	5.55	8	5	ND	1	6	1	2	2	95	.04	.053	4	25	.17	16	.06	2	1.76	.01	.03	1	1
L97-50E 88-50N	1	1	4	29	.3	3	3	54	1.49	3	5	ND	1	4	1	2	2	36	.03	.015	4	9	.04	9	.03	2	.50	.01	.02	1	1
L97-50E 88-25N	1	1	2	27	.1	3	2	36	.76	2	5	ND	1	4	1	2	2	24	.03	.008	5	5	.02	8	.03	3	.32	.01	.02	1	3
L97-50E 38-00N	1	5	7	40	.3	5	3	83	1.42	2	5	ND	1	10	1	2	2	44	.05	.026	5	16	.08	35	.05	2	.69	.02	.04	1	2
L97-50E 87-75N	1	5	5	23	.1	6	3	72	1.37	2	5	ND	1	5	1	2	2	46	.03	.017	4	10	.05	14	.04	5	.49	.01	.02	1	1
L97-50E 87-50N	1	34	31	89	.5	18	9	241	4.39	10	5	ND	2	9	1	3	2	46	.07	.057	4	40	.58	50	.01	2	2.92	.01	.06	1	12
L97-50E 87-25N	1	3	3	19	.1	3	3	51	1.08	2	5	ND	1	4	1	2	2	31	.02	.009	6	11	.03	16	.03	2	.41	.01	.02	1	2
L97-50E 87-00N	1	4	20	35	.2	4	3	79	.97	4	5	ND	1	8	1	2	3	32	.06	.013	5	13	.15	29	.05	2	1.22	.01	.03	1	1
L97-50E 86-75N	1	2	2	21	.1	3	3	48	.99	2	5	ND	1	3	1	2	2	27	.02	.006	3	6	.02	6	.04	2	.21	.01	.02	1	3
L97-50E 86-50N	3	34	18	101	3.0	11	27	10970	2.00	2	5	ND	1	28	4	2	2	22	.60	.174	23	28	.10	87	.02	4	2.28	.01	.06	1	2
L97-50E 86-25N	3	17	38	90	.4	5	8	168	6.21	15	5	ND	1	8	1	4	2	99	.15	.018	4	23	.15	20	.10	2	2.70	.01	.04	1	2
L97-50E 86-00N	1	25	24	101	.4	16	9	247	5.71	18	5	ND	1	11	1	2	2	76	.11	.032	6	42	.53	47	.06	2	2.28	.01	.04	1	1
L98E 104-00N	3	200	68	310	1.1	16	62	3804	7.07	19	5	ND	1	17	6	6	5	64	.36	.143	11	29	.22	86	.04	4	3.72	.01	.06	2	1
L98E 103-75N	4	455	54	324	1.1	19	44	2187	10.27	23	5	ND	1	29	6	2	10	62	.53	.143	5	26	.29	93	.05	4	2.36	.01	.08	1	13
L98E 102-25N	1	62	59	85	1.9	8	9	1013	1.80	5	5	ND	1	19	1	2	4	40	.48	.078	2	9	.44	35	.02	3	1.58	.01	.07	1	1
L98E 102-00N	1	85	70	223	1.8	11	12	4489	2.48	6	5	ND	1	31	1	2	2	45	.70	.226	3	15	.54	292	.02	6	2.47	.01	.04	1	9
L98E 101-50N	1	15	41	121	.6	9	8	293	5.39	21	5	ND	2	10	1	6	4	94	.17	.047	3	33	.16	24	.06	3	1.90	.01	.03	1	3
L98E 101-25N	1	48	125	324	1.0	13	9	258	5.76	123	5	ND	1	12	1	4	3	80	.19	.049	4	39	.29	28	.08	5	2.28	.01	.04	1	36
L98E 99-75N	8	54	147	274	1.9	11	11	473	4.27	107	5	ND	1	10	1	8	4	57	.14	.072	6	37	.37	34	.04	6	3.29	.01	.04	1	3
STD C1AU-5	17	61	36	132	7.2	68	30	1053	4.12	38	14	7	36	45	17	17	23	55	.47	.086	38	55	.92	175	.06	33	1.93	.06	.13	13	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Hg PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sc PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	V PPM	Au# PPB
1988 95+25N	3	60	188	291	4.3	12	16	3262	3.51	95	5	ND	1	26	4	3	4	49	.41	.118	8	24	.39	57	.02	4	2.41	.01	.06	1	1
1988 99+00N	7	52	82	163	2.9	8	39	7839	2.25	25	5	ND	1	21	11	4	5	26	.45	.164	10	15	.20	65	.01	6	2.23	.01	.10	1	1
1988 98+75W	4	31	90	126	3.6	8	6	1837	1.88	22	5	ND	1	22	2	5	2	38	.33	.109	9	25	.31	46	.02	4	2.16	.01	.05	1	1
1988 98+25N	5	43	95	100	2.8	4	43	3204	5.19	22	5	ND	1	20	4	2	2	49	.34	.259	9	14	.07	41	.01	5	2.32	.02	.09	1	2
1985 98+00W	2	16	77	130	.5	8	3	317	1.32	22	5	ND	1	18	1	2	2	27	.27	.072	6	26	.31	28	.02	10	1.43	.01	.05	1	1
1988 97+75N	1	7	13	37	.2	3	7	690	1.30	4	5	ND	1	17	1	2	2	27	.13	.034	8	10	.14	87	.01	2	.99	.01	.05	1	1
1988 97+50W	1	20	28	65	.1	7	8	666	5.38	13	5	ND	1	11	1	2	6	61	.07	.132	5	26	.29	36	.03	5	2.08	.01	.04	1	1
1988 97+25N	1	16	16	54	.1	8	6	301	3.56	14	5	ND	1	11	1	2	2	60	.06	.061	5	26	.35	37	.01	1	1.76	.01	.05	1	1
1988 97+00W	1	23	20	77	.4	9	9	306	3.77	13	5	ND	1	11	1	2	2	52	.08	.081	5	28	.40	42	.02	6	2.60	.01	.05	1	2
1988 92+00N	1	20	32	111	.2	9	7	402	5.11	16	5	ND	1	10	1	3	2	68	.11	.053	5	27	.41	38	.03	2	2.40	.01	.04	1	3
1988 91+75N	1	28	26	146	.3	19	9	485	5.77	17	5	ND	1	19	1	2	2	74	.31	.034	5	39	.73	73	.05	2	2.60	.01	.06	1	1
1988 91+50N	1	24	29	155	1.1	15	10	349	4.57	22	5	ND	1	15	1	2	2	66	.32	.034	7	35	.43	53	.04	2	2.55	.01	.03	1	2
1988 91+25N	2	16	28	146	.5	15	7	529	4.62	20	5	ND	1	16	1	2	4	56	.35	.034	7	26	.77	77	.03	3	2.26	.01	.04	1	1
1988 91+00N	2	17	27	287	.7	11	7	200	6.15	17	5	ND	1	17	1	2	3	82	.35	.039	5	31	.27	58	.04	5	2.43	.01	.03	1	1
1988 90+75N	1	39	10	123	3.0	5	3	293	.20	4	5	ND	1	78	4	4	2	3	2.89	.076	25	25	.04	52	.01	7	1.36	.01	.03	1	1
1988 89+50N	1	2	6	20	.2	2	4	52	1.50	3	10	ND	2	6	1	2	3	38	.04	.008	5	10	.03	10	.05	4	.91	.01	.02	1	1
1988 89+25N	1	22	26	124	.6	13	8	363	8.37	17	5	ND	2	10	1	2	2	77	.06	.083	5	36	.43	36	.04	2	2.38	.01	.06	1	1
1988 89+00N	1	19	26	79	.7	10	6	191	2.36	15	5	ND	1	13	1	2	2	57	.10	.045	6	26	.43	49	.02	2	2.44	.01	.03	1	1
1988 88+75N	1	23	33	62	1.8	7	6	171	3.35	9	6	ND	2	10	1	2	2	47	.08	.062	8	24	.28	50	.02	2	3.33	.01	.04	1	1
1988 88+50N	1	19	37	82	1.9	8	7	192	3.63	13	5	ND	1	10	1	3	2	56	.07	.044	8	23	.25	56	.03	2	2.92	.01	.05	1	2
1988 88+25N	5	43	53	128	1.4	21	14	10709	4.03	9	5	ND	1	13	1	2	2	60	.07	.087	9	35	.43	164	.02	2	4.03	.01	.10	1	1
1988 88+00N	1	15	19	72	.4	8	6	326	3.00	7	5	ND	2	8	1	2	2	40	.06	.029	5	21	.28	36	.02	4	2.18	.01	.05	1	1
1988 87+75N	1	16	20	71	.4	12	7	244	4.22	8	5	ND	1	10	1	2	2	71	.07	.048	5	26	.29	35	.03	3	1.75	.01	.05	1	1
1988 87+50N	1	28	24	106	.6	14	9	229	8.11	8	5	ND	2	11	1	2	2	87	.08	.082	7	34	.38	55	.04	2	3.52	.01	.04	1	2
1988 87+25N	1	20	17	59	.2	8	8	156	5.19	7	5	ND	2	12	1	2	2	107	.06	.047	6	27	.28	27	.05	2	2.24	.01	.05	1	1
1988 87+00N	1	13	16	62	.3	8	7	187	4.52	7	5	ND	2	12	1	2	2	129	.08	.028	8	32	.18	54	.09	2	1.70	.01	.04	1	1
1988 86+75N	1	30	19	93	.7	19	9	368	3.95	11	5	ND	1	11	1	2	2	50	.12	.060	8	31	.66	36	.02	3	2.79	.01	.06	1	2
1988 86+50N	1	36	41	115	.3	23	10	268	4.24	15	5	ND	3	11	1	2	2	51	.09	.042	5	46	.65	49	.02	3	4.36	.01	.04	1	1
198+50E 104+00N	1	21	24	39	.1	5	7	250	4.45	6	5	ND	1	10	1	2	7	145	.18	.045	3	20	.19	26	.22	4	1.20	.02	.06	2	1
198+50E 102+75N	1	14	24	34	.1	9	7	118	3.75	32	5	ND	1	15	1	2	8	118	.19	.015	4	40	.10	24	.13	3	.80	.01	.03	2	1
198+50E 103+25N	1	74	390	217	.8	18	43	2246	4.57	88	5	ND	1	32	2	3	2	81	.82	.077	6	36	.61	55	.04	2	2.65	.01	.04	1	1
198+50E 103+00N	1	41	87	206	.6	13	13	12008	2.60	5	5	ND	1	19	2	2	2	55	.32	.072	5	17	.24	96	.05	2	1.66	.01	.05	1	1
198+50E 102+75N	1	29	87	89	2.1	9	14	4465	3.05	7	5	ND	1	22	1	2	2	79	.33	.096	4	19	.48	70	.10	3	1.60	.01	.06	1	1
198+50E 102+50N	2	118	75	378	.8	18	12	434	8.00	72	5	ND	2	17	1	44	4	114	.22	.053	4	50	.54	53	.11	5	2.60	.01	.06	6	2
198+50E 102+25N	1	73	87	191	10.3	7	21	559	4.20	7	5	ND	2	8	1	2	2	66	.17	.063	4	13	.08	17	.15	5	2.86	.01	.01	1	1
198+50E 102+00N	1	9	9	50	.3	7	8	469	2.40	3	5	ND	1	3	1	2	2	64	.09	.010	2	12	.21	8	.14	4	.45	.02	.03	2	2
STD CRAD-3	17	59	41	132	6.6	67	31	1061	4.13	42	17	7	37	47	18	17	19	57	.47	.083	38	56	.93	171	.06	34	2.01	.06	.13	13	53

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	V	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
L98+S0E 101+75N	1	23	26	84	.1	16	7	208	6.08	9	5	ND	1	13	1	7	2	120	.14	.039	4	68	.33	21	.10	4	2.20	.01	.03	1	1
L98+S0E 101+50N	1	28	59	205	1.1	15	7	302	4.83	18	5	ND	2	14	1	4	2	88	.17	.045	5	49	.29	32	.10	5	1.98	.01	.03	1	1
L98+S0E 101+25N	4	100	612	442	4.4	14	26	14097	2.79	72	5	ND	1	15	11	3	2	49	.23	.096	11	33	.21	51	.04	2	3.42	.02	.02	1	1
L98+S0E 101+00N	1	15	20	96	.1	10	5	279	5.22	36	5	ND	1	27	1	5	2	148	.39	.063	4	56	.18	95	.14	5	1.02	.01	.01	1	1
L98+S0E 100+75N	3	26	107	165	1.1	6	6	371	8.10	103	5	ND	1	20	3	13	2	134	.31	.044	4	66	.14	34	.11	8	1.45	.01	.03	1	3
L98+S0E 100+50N	3	62	44	349	.3	14	7	259	7.04	83	5	ND	3	22	1	5	7	155	.21	.073	5	58	.31	120	.12	6	1.53	.01	.03	1	1
L98+S0E 100+25N	2	23	37	124	.4	7	4	180	4.54	29	5	ND	2	16	1	4	7	117	.14	.043	6	34	.24	41	.11	2	1.60	.01	.04	1	2
L98+S0E 100+00N	2	28	54	119	.5	15	5	165	5.27	84	5	ND	1	22	1	4	2	68	.26	.044	4	43	.42	38	.06	7	2.57	.01	.03	1	1
L98+S0E 99+75N	2	304	176	542	7.8	20	17	1319	3.89	193	5	ND	1	29	5	6	3	57	.40	.084	9	37	.54	74	.04	6	3.14	.01	.05	1	1
L98+S0E 99+50N	1	53	135	160	3.2	7	5	416	1.10	19	5	ND	1	15	3	4	2	25	.19	.103	9	24	.24	37	.01	4	1.92	.01	.04	1	1
L98+S0E 99+25N	1	44	58	286	1.6	7	4	421	.70	16	5	ND	1	41	17	2	4	12	.89	.137	6	7	.06	38	.01	12	.69	.01	.05	2	1
L98+S0E 98+50N	4	24	152	232	.5	11	15	1818	4.19	56	5	ND	1	15	3	2	2	52	.20	.059	9	43	.40	56	.04	7	2.58	.01	.03	1	2
L98+S0E 98+25N	1	13	51	86	.5	7	5	518	1.65	10	5	ND	1	21	1	2	2	26	.25	.095	5	28	.32	90	.01	4	1.18	.01	.06	1	1
L98+S0E 97+75N	1	23	18	59	1.2	7	6	562	4.38	7	5	ND	1	16	1	3	2	70	.12	.057	9	27	.24	63	.05	4	1.84	.01	.05	1	2
L98+S0E 97+50N	1	37	22	111	.2	14	7	1235	3.93	7	5	ND	1	12	1	2	2	49	.11	.081	5	34	.47	39	.03	4	2.91	.01	.04	1	1
L98+S0E 97+25N	1	14	18	54	.1	8	6	691	4.20	6	5	ND	1	11	1	2	2	66	.07	.061	5	26	.34	36	.02	3	2.11	.01	.04	1	1
L98+S0E 97+00N	1	22	17	62	.1	8	7	752	5.08	5	5	ND	2	11	1	4	2	65	.07	.060	6	33	.39	38	.02	2	2.46	.01	.05	1	1
L99E 104+00N	1	50	45	86	.9	12	8	443	5.83	91	5	ND	2	12	1	4	2	79	.15	.069	4	39	.41	25	.08	12	2.19	.01	.04	1	2
L99E 102+25N	1	152	1026	285	1.0	4	16	4669	4.14	4	5	ND	1	18	1	2	3	102	.33	.049	2	17	.26	57	.03	2	2.77	.01	.04	1	1
L99E 103+00N	1	54	105	663	1.9	15	12	1380	3.69	59	5	ND	1	27	3	2	2	55	.54	.059	11	32	.40	53	.05	6	2.88	.01	.03	1	1
L99E 102+75N	1	400	63	171	17.9	11	109	10468	6.05	39	5	ND	1	10	3	5	2	64	.20	.208	5	29	.31	72	.04	8	4.62	.01	.04	1	1
L99E 102+50N	2	97	68	229	2.1	12	22	1832	4.70	16	5	ND	1	9	1	5	2	60	.11	.108	6	32	.24	33	.10	12	3.41	.01	.02	1	1
L99E 102+25N	1	21	30	62	.9	6	4	1273	1.76	2	5	ND	1	17	1	2	5	46	.29	.049	4	20	.31	28	.11	2	1.23	.01	.03	1	1
L99E 102+00N	1	227	72	319	2.4	14	6	21129	1.34	2	5	ND	1	13	14	3	3	32	.30	.140	10	13	.06	161	.05	10	3.55	.02	.01	1	1
L99E 101+75N	1	26	30	113	.6	8	5	675	3.41	8	5	ND	1	12	1	2	2	69	.13	.060	4	32	.21	30	.05	5	1.60	.01	.03	2	1
L99E 101+50N	1	22	58	268	.6	15	23	1003	3.17	19	5	ND	1	17	3	3	2	60	.20	.045	5	41	.33	64	.04	5	1.52	.01	.03	1	1
L99E 101+25N	1	29	79	396	.9	17	13	519	4.41	26	5	ND	2	20	3	3	2	67	.25	.048	4	50	.40	57	.08	5	1.69	.01	.03	2	1
L99E 101+00N	1	24	58	193	.5	20	13	1310	3.46	19	5	ND	1	13	2	4	2	62	.17	.037	4	53	.51	31	.05	2	1.12	.01	.02	2	1
L99E 100+75N	2	39	478	95	5.2	7	26	1946	2.93	13	5	ND	1	11	1	2	2	35	.17	.084	5	27	.12	15	.04	7	3.35	.02	.01	1	1
L99E 100+50N	2	49	241	233	2.4	11	36	2462	3.81	23	5	ND	1	21	4	3	2	57	.35	.065	9	30	.29	49	.06	19	2.11	.01	.04	1	2
L99E 100+25N	1	31	231	274	.6	6	6	218	3.06	36	5	ND	1	16	2	2	2	53	.23	.027	7	23	.16	40	.14	7	1.38	.01	.02	1	2
L99E 100+00N	2	56	45	151	2.7	8	7	1322	1.96	37	5	ND	1	12	2	2	2	36	.16	.036	7	20	.14	25	.05	19	1.79	.02	.02	1	1
L99E 99+75N	2	42	93	243	1.2	12	13	681	4.65	102	5	ND	1	23	2	2	2	66	.36	.043	5	37	.34	40	.06	3	2.12	.01	.03	1	1
L99E 99+50N	2	23	45	113	.9	12	8	388	5.54	89	5	ND	1	13	1	4	2	93	.13	.047	5	34	.41	33	.08	7	1.75	.01	.04	1	1
L99E 99+25N	5	20	153	373	2.5	13	8	303	3.08	64	5	ND	1	15	1	4	2	67	.19	.037	7	25	.49	41	.04	6	2.58	.01	.03	2	1
L99E 99+00N	2	20	101	91	1.7	7	3	118	1.42	11	5	ND	1	16	1	2	3	38	.17	.024	7	25	.22	31	.10	2	1.92	.01	.02	1	2
STD C:AD+S	17	61	42	132	6.6	68	28	1056	4.11	38	17	7	36	47	17	16	19	56	.47	.091	38	55	.93	171	.06	34	2.00	.06	.14	14	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ml PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	SD PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	B PPM	Al %	Na %	I %	W PPM	Au* PPM
L99K 99+75N	1	21	66	103	.6	7	3	134	1.10	15	5	ND	1	15	1	2	2	22	.21	.061	5	24	.35	40	.01	3	1.39	.01	.04	1	1
L99K 97+75N	1	29	71	168	.2	21	12	653	3.78	33	5	ND	1	16	1	2	2	53	.24	.059	5	37	.74	55	.02	4	1.75	.01	.05	1	1
L99E 97+50M	1	46	150	570	1.5	26	15	1007	4.05	36	5	ND	1	18	2	3	2	64	.27	.068	7	44	.78	74	.03	7	1.89	.01	.05	1	2
L99K 97+25N	1	41	32	153	.4	22	11	500	5.03	18	5	ND	3	14	1	2	2	62	.12	.050	6	49	.80	62	.02	2	3.76	.01	.07	1	1
L99E 97+00K	1	38	24	152	.3	24	12	741	4.31	12	5	ND	1	16	1	2	2	64	.15	.089	6	47	.75	99	.03	4	2.92	.01	.08	1	1
L99+50E 104+00M	1	150	81	145	1.4	9	26	3533	1.32	40	5	ND	1	33	2	2	2	26	.83	.128	11	14	.22	62	.02	5	2.43	.01	.05	2	1
L99+50E 103+75N	1	18	12	39	.3	8	6	269	3.21	29	5	ND	1	14	1	2	2	70	.17	.050	4	20	.10	30	.06	4	1.12	.01	.04	1	2
L99+50E 102+50M	1	20	19	50	.4	9	5	133	4.92	76	5	ND	1	11	1	2	2	111	.10	.020	6	35	.11	21	.07	5	1.17	.01	.02	1	1
L99+50E 103+00N	1	30	44	132	1.1	3	4	214	5.62	33	5	ND	1	7	1	52	5	89	.14	.046	3	7	.04	14	.02	8	.64	.01	.04	1	16
L99+50E 102+75N	1	63	139	259	2.7	10	15	4102	2.60	37	5	ND	1	30	5	3	2	42	.78	.093	11	22	.17	58	.03	7	2.10	.01	.05	1	1
L99+50E 102+50N	1	64	37	270	1.5	15	10	3505	3.63	51	7	ND	1	21	2	3	7	64	.33	.068	6	29	.42	85	.07	3	1.60	.01	.07	1	1
L99+50E 102+25M	1	4	2	21	.2	1	3	83	1.27	2	5	ND	1	5	1	2	2	33	.08	.010	3	9	.01	15	.05	2	.16	.01	.03	1	3
L99+50E 102+00N	1	6	4	22	.1	3	1	61	.77	2	5	ND	1	8	1	2	2	27	.07	.007	5	10	.03	15	.03	4	.39	.01	.02	1	1
L99+50E 101+75N	1	80	21	84	3.9	7	6	4244	1.56	4	5	ND	1	30	3	2	2	34	.81	.092	10	23	.17	42	.02	4	2.05	.01	.04	1	1
L99+50E 101+50N	1	73	38	247	.8	28	11	534	3.54	16	5	ND	1	17	2	2	2	67	.23	.042	6	52	.69	50	.06	5	2.04	.01	.03	1	1
L99+50E 101+25N	1	9	14	80	.8	6	1	172	.77	3	5	ND	1	13	1	2	4	18	.20	.042	2	8	.09	67	.03	5	.27	.01	.04	1	1
L99+50E 101+00N	2	37	134	347	1.5	17	11	878	2.74	58	5	ND	1	24	5	2	2	41	.56	.079	7	31	.52	56	.02	5	2.04	.01	.02	1	3
L99+50E 100+75N	1	23	55	203	1.1	14	8	774	1.96	16	5	ND	1	38	5	2	2	25	1.02	.089	5	19	.34	88	.01	7	1.09	.01	.04	1	1
L99+50E 100+50N	2	32	129	288	1.1	18	6	377	3.14	78	5	ND	1	27	5	2	2	45	.61	.095	8	34	.59	55	.02	6	2.04	.01	.04	1	2
L99+50E 100+25N	3	36	135	334	1.5	19	17	2320	4.23	79	5	ND	1	29	6	2	3	46	.64	.095	8	33	.59	70	.02	4	2.10	.01	.06	1	1
L99+50E 100+00N	1	21	67	250	.8	19	12	1867	2.79	31	5	ND	1	25	4	2	4	37	.62	.068	5	23	.61	66	.02	5	1.44	.01	.08	1	1
L99+50E 99+75N	1	39	95	262	1.0	24	11	1110	2.53	26	5	ND	1	40	7	3	6	40	.93	.086	7	29	.63	140	.02	6	1.43	.01	.07	1	1
L99+50E 99+50N	1	29	181	258	.9	16	14	2518	2.08	24	3	ND	1	29	7	2	5	30	.67	.099	6	23	.38	86	.01	5	1.32	.01	.06	1	1
L99+50E 99+25N	1	15	20	65	.5	5	6	198	3.53	13	5	ND	1	12	1	2	2	61	.10	.029	4	25	.26	21	.06	4	1.78	.01	.01	1	1
L99+50E 99+00N	1	26	22	102	.6	13	8	244	3.36	14	5	ND	1	11	1	3	4	60	.11	.035	5	43	.40	37	.05	4	2.85	.01	.02	1	1
L99+50E 98+25N	1	14	157	161	.6	4	5	305	.74	12	5	ND	1	26	4	3	2	10	.86	.056	2	7	.14	30	.01	5	.42	.01	.06	1	1
L99+50E 98+00N	1	19	18	580	.7	7	1	47	.17	4	5	ND	1	62	9	2	2	5	2.54	.063	2	1	.04	30	.01	9	.18	.01	.04	2	1
L99+50E 97+75N	1	325	259	3344	5.4	22	12	5494	1.73	23	5	ND	1	56	57	7	2	23	2.16	.146	18	21	.29	62	.02	9	2.34	.01	.06	6	1
L99+50E 97+50N	2	75	135	1201	2.2	18	17	1369	4.10	38	5	ND	1	25	8	5	3	54	.64	.076	7	39	.60	44	.02	4	2.48	.01	.03	2	8
L99+50E 97+25N	2	169	294	1822	8.0	33	17	2085	3.81	44	5	ND	1	26	15	4	6	56	.65	.084	10	46	.78	54	.03	5	2.39	.01	.05	2	78
L99+50E 97+00N	1	35	116	698	.7	40	18	520	4.67	30	5	ND	1	16	2	3	9	69	.21	.045	8	56	.77	79	.04	2	3.56	.01	.03	2	1
L100E 104+00M	3	85	188	112	3.8	11	126	10804	1.56	55	5	ND	1	21	1	2	7	19	.53	.164	11	18	.11	59	.02	9	3.36	.01	.04	3	1
L100E 103+75N	2	62	100	95	3.3	9	58	4783	1.50	48	5	ND	1	21	4	2	2	22	.50	.124	8	16	.14	49	.01	5	2.44	.01	.04	1	3
L100E 103+50M	1	15	18	43	.2	10	7	191	4.16	19	5	ND	1	9	1	2	4	94	.10	.021	4	35	.11	17	.06	3	1.17	.01	.01	1	2
L100E 103+25N	1	2	8	24	.1	6	3	75	1.65	2	5	ND	1	6	1	2	2	49	.04	.008	4	21	.03	12	.04	2	.41	.01	.01	1	1
L100E 102+00N	1	5	9	43	.1	6	4	1444	.67	3	5	ND	1	10	1	2	2	18	.10	.010	3	7	.03	77	.03	2	.28	.01	.02	2	1
STD C/AU-5	18	58	42	132	6.7	67	27	1060	4.17	39	16	8	36	48	18	16	23	57	.47	.087	39	57	.93	176	.06	34	1.96	.06	.13	12	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Hg PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Yt %	B PPM	Al %	Na %	K %	W PPM	As* PPM
L100E 100+75N	1	60	83	226	1.6	17	12	1930	2.71	37	5	ND	1	20	3	2	4	44	.46	.080	9	36	.45	44	.03	4	2.36	.01	.04	1	10
L100E 102+50N	1	25	58	81	2.9	3	2	59	.42	5	5	ND	1	20	3	1	2	11	.45	.084	7	15	.10	47	.01	2	.94	.01	.04	1	1
L100E 102+25N	1	36	68	238	2.3	8	7	2460	.93	10	5	ND	1	43	6	4	2	15	1.29	.094	8	13	.16	90	.01	3	1.11	.01	.07	1	1
L100E 102+00N	1	3	10	36	.1	3	2	107	1.17	3	5	ND	1	9	1	2	2	32	.11	.015	4	16	.07	20	.02	4	.31	.01	.05	1	1
L100E 101+75N	1	32	28	131	.1	24	10	566	5.47	15	5	ND	1	14	1	2	7	63	.21	.054	6	45	.61	41	.04	7	1.74	.01	.04	1	2
L100E 101+50N	1	13	19	54	.7	8	6	156	5.10	10	5	ND	1	12	1	3	3	114	.12	.030	4	50	.58	32	.10	5	2.04	.01	.05	1	1
L100E 101+25N	1	26	17	113	.4	27	8	299	3.92	9	5	ND	1	15	1	2	5	62	.16	.029	5	61	.89	37	.06	2	2.84	.01	.05	1	1
L100E 101+00N	1	15	63	144	1.0	9	3	245	1.59	20	5	ND	1	24	2	2	2	27	.51	.058	4	24	.39	43	.01	3	1.21	.01	.04	1	2
L100E 100+75N	1	25	107	178	1.5	12	5	1235	2.30	35	6	ND	1	26	4	2	8	42	.51	.117	8	28	.47	89	.01	3	1.70	.01	.06	1	1
L100E 100+25N	2	15	86	179	.8	12	8	372	3.00	26	5	ND	1	16	1	2	3	50	.31	.063	5	28	.65	57	.01	2	1.96	.01	.05	1	1
L100E 100+00N	1	28	70	208	.7	17	11	968	3.14	30	5	ND	1	18	1	2	2	46	.33	.067	6	35	.61	61	.02	2	1.74	.01	.06	1	1
L100E 99+75N	1	18	43	391	.5	9	3	512	.74	7	5	ND	1	61	5	4	2	8	2.47	.077	3	5	.10	80	.01	5	.40	.01	.04	1	1
L100E 99+50N	1	22	48	206	1.0	12	8	188	6.30	24	5	ND	2	11	1	4	7	97	.12	.055	5	44	.37	25	.10	3	3.27	.01	.03	1	1
L100E 99+25N	2	16	34	187	.6	13	6	317	2.84	26	5	ND	1	17	1	4	2	57	.23	.039	6	39	.55	48	.05	3	1.74	.01	.05	1	1
L100E 99+00N	1	3	16	56	.6	1	2	111	.79	7	5	ND	2	10	1	3	2	17	.12	.050	4	10	.10	26	.01	2	.71	.01	.06	1	1
L100E 98+75N	1	4	7	83	12.6	1	1	40	.20	3	5	ND	1	16	1	2	2	5	.48	.037	2	4	.05	18	.01	6	.14	.01	.04	1	1
L100E 98+50N	2	54	85	562	2.6	11	21	2583	3.66	51	5	ND	1	42	12	2	3	34	1.37	.129	9	19	.25	62	.01	2	1.53	.01	.05	1	1
L100E 98+25N	1	42	69	769	1.1	8	12	1714	2.76	24	5	ND	1	49	15	2	2	23	1.96	.115	6	14	.19	48	.01	8	1.29	.02	.09	1	1
L100E 98+00N	1	9	20	79	.6	2	2	113	.65	4	5	ND	1	15	2	2	2	14	.26	.034	3	9	.03	39	.04	2	.48	.02	.04	1	1
L100E 97+75N	2	81	86	480	1.3	6	4	2507	.37	2	5	ND	1	53	8	5	2	5	2.08	.120	14	6	.07	51	.01	6	2.64	.01	.03	1	1
L100E 97+50N	1	7	30	192	.9	1	1	603	.24	3	5	ND	1	26	3	4	2	4	.81	.079	2	2	.06	73	.01	3	.21	.01	.07	1	1
L100E 97+25N	3	79	256	904	4.2	11	18	8453	1.55	12	5	ND	1	41	23	2	2	15	1.59	.266	14	14	.09	56	.02	4	4.59	.01	.05	1	1
L100E 97+00N	1	9	40	146	.5	4	4	244	2.36	6	5	ND	1	11	1	2	2	65	.18	.022	4	20	.07	20	.08	2	.80	.01	.03	1	3
L100E 97+00AN	1	14	30	238	.5	7	6	1405	3.43	4	5	ND	1	19	4	3	2	53	.47	.029	4	16	.26	68	.05	2	1.31	.01	.05	1	1
L100E 96+75N	1	30	263	793	.7	13	19	3779	4.66	45	5	ND	1	27	5	2	3	53	.72	.085	6	22	.29	67	.05	5	2.30	.01	.06	1	12
L100E 96+50N	12	74	160	1605	1.8	38	19	16128	2.84	20	5	ND	1	30	40	2	3	41	.89	.094	11	32	.47	116	.03	4	2.88	.01	.04	2	3
L100E 94+25N	1	4	22	60	.3	1	3	285	1.72	7	6	ND	1	5	1	4	2	51	.05	.023	5	9	.07	12	.06	2	.69	.01	.04	1	1
L100+50E 100+50N	2	19	79	191	.6	16	9	1186	3.21	40	5	ND	1	14	1	2	2	45	.19	.054	7	30	.62	48	.02	5	1.88	.01	.05	1	23
L100+50E 100+25N	1	20	87	259	.5	14	10	1519	1.65	14	5	ND	1	38	6	2	2	18	1.31	.098	3	17	.33	67	.01	6	.66	.01	.09	1	1
L100+50E 99+50N	3	37	114	445	1.0	8	40	3442	3.66	98	5	ND	1	28	10	2	2	45	.93	.057	9	22	.32	73	.02	8	1.84	.01	.05	1	1
L100+50E 99+25N	1	75	145	1071	5.8	15	11	1886	2.92	50	5	ND	1	24	9	2	2	45	.89	.062	9	28	.38	53	.04	3	2.38	.01	.04	1	1
L100+50E 99+00N	1	67	124	1062	2.1	15	13	1452	3.27	42	5	ND	1	19	5	2	2	52	.44	.053	7	33	.49	60	.04	4	2.19	.01	.04	1	3
L100+50E 98+75N	1	159	244	1995	3.1	20	18	2924	3.21	52	5	ND	1	20	8	2	9	46	.54	.035	10	41	.57	52	.06	2	2.98	.01	.04	2	3
L100+50E 98+50N	1	61	104	852	.5	16	9	221	4.17	30	5	ND	3	12	1	2	4	68	.14	.019	6	42	.44	46	.12	5	2.39	.01	.04	2	1
L100+50E 98+25N	1	88	109	1067	1.4	30	12	323	5.31	28	5	ND	1	17	3	4	3	75	.22	.031	8	48	.70	85	.07	2	2.88	.01	.05	1	1
L100+50E 96+00N	1	524	182	1028	7.7	13	12	5476	2.06	32	5	ND	1	46	36	2	2	27	1.74	.129	28	49	.24	74	.03	4	3.11	.01	.04	2	12
STD C/AU-5	17	58	38	132	6.5	67	29	1051	4.10	40	17	7	36	47	16	16	20	55	.46	.089	38	56	.92	173	.06	34	1.96	.05	.13	11	52

SAMPLE#	Hg	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	V	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	%	PPM	PPM
L100+50E 97+75N	1	15	45	212	.4	3	2	255	1.8	2	5	ND	1	28	2	2	4	.91	.070	2	2	.06	49	.01	8	.19	.01	.08	1	1	
L100+50E 97+25N	1	21	47	348	.9	4	3	204	2.42	12	5	ND	1	19	1	2	31	.48	.057	2	10	.11	63	.06	4	1.04	.01	.04	1	1	
L100+50E 97+00N	1	84	110	1382	1.3	13	8	2916	1.70	27	5	ND	1	70	19	4	2	18	3.35	.127	10	14	.18	54	.02	7	1.69	.01	.04	1	1
L101E 100+75N	1	26	33	134	.6	14	6	495	2.49	10	5	ND	1	11	1	2	3	50	.17	.045	4	26	.36	37	.04	7	1.54	.01	.03	1	2
L101E 100+50N	1	24	26	82	.3	14	8	259	5.97	9	5	ND	1	11	1	2	2	91	.10	.030	6	51	.53	32	.09	2	3.02	.01	.03	1	1
L101E 100+00N	1	15	27	105	.3	9	6	252	4.20	14	5	ND	1	9	1	2	2	58	.09	.041	5	37	.26	43	.06	3	4.43	.01	.02	1	1
L101E 99+25N	1	32	51	605	1.3	7	7	814	2.92	19	5	ND	1	11	2	4	4	55	.19	.028	6	21	.27	29	.06	6	1.40	.01	.02	1	1
L101E 99+00N	1	50	219	436	.7	13	8	250	4.96	67	5	ND	1	12	1	7	2	72	.14	.029	4	43	.40	29	.04	2	2.71	.01	.02	1	1
L101E 98+75N	1	88	16	618	2.7	4	1	178	.36	4	5	ND	1	71	10	2	2	6	5.48	.044	3	5	.05	32	.01	6	.41	.01	.01	1	1
L101E 98+50N	1	15	29	84	.7	6	5	94	3.21	21	5	ND	1	9	1	2	4	71	.12	.019	3	22	.13	26	.03	4	.97	.01	.01	1	2
L101E 98+25N	1	593	339	3218	3.3	13	15	14907	1.66	38	5	ND	1	31	129	2	4	24	1.46	.221	36	23	.15	155	.02	10	3.94	.01	.03	5	1
L101E 98+00N	1	57	91	398	2.3	11	8	463	5.47	49	5	ND	1	8	1	2	2	58	.11	.051	4	30	.48	36	.07	3	3.61	.01	.03	1	1
L101E 97+75N	1	2	8	30	.1	1	3	148	.85	2	5	ND	1	3	1	3	2	27	.03	.006	2	4	.02	8	.06	3	.27	.01	.01	1	1
L101E 97+50N	3	702	408	3186	7.4	16	19	12665	1.37	22	5	ND	1	64	85	3	2	24	2.90	.136	26	37	.16	147	.02	7	2.34	.01	.07	6	1
L101E 97+25N	3	76	64	1045	1.1	12	9	393	5.96	71	5	ND	1	28	4	4	2	71	.77	.041	5	27	.27	55	.09	2	1.91	.01	.94	1	5
L101E 97+00N	4	105	112	1673	6.7	14	4	6131	1.04	79	5	ND	1	81	49	5	2	13	3.31	.109	9	34	.10	149	.01	7	1.39	.01	.03	2	1
L101E 97-00AN	6	90	92	1005	4.9	10	3	2508	.74	67	5	ND	1	125	20	6	2	11	4.47	.154	7	38	.13	68	.01	13	1.28	.02	.03	1	1
L101E 96+00N	2	19	26	80	.2	6	7	409	5.60	5	5	ND	2	5	1	2	2	75	.07	.074	1	22	.20	21	.15	3	3.25	.01	.03	1	1
L101E 95+75N	1	12	29	104	1.0	3	4	547	2.92	4	5	ND	1	8	1	2	2	55	.16	.029	4	15	.08	28	.06	4	1.30	.01	.04	1	1
L101E 95+50N	7	34	84	560	2.3	19	5	7818	2.12	30	5	ND	1	29	14	2	2	33	1.10	.164	13	31	.18	85	.04	8	3.00	.02	.02	1	1
L101E 95+25N	1	13	28	59	.6	4	4	287	3.51	26	5	ND	1	6	1	3	2	57	.05	.040	5	15	.12	24	.03	2	1.10	.01	.02	1	15
L101E 95+00N	1	2	2	14	.1	1	1	38	.32	2	5	ND	1	1	1	2	3	9	.02	.010	2	2	.02	5	.02	10	.13	.02	.02	1	1
L101E 94+75N	1	25	86	206	.6	8	9	1086	4.21	29	5	ND	1	9	1	2	4	54	.11	.061	4	19	.44	43	.02	5	2.15	.01	.04	1	1
L101E 94+50N	1	12	21	64	.1	6	4	631	3.39	7	5	ND	1	7	1	3	2	69	.08	.041	3	14	.13	30	.05	5	1.14	.01	.02	1	1
L101+50E 99+50N	1	293	1065	3076	4.5	14	12	6659	2.20	79	5	ND	1	48	51	2	2	32	2.14	.137	14	38	.27	66	.03	6	2.91	.01	.03	5	1
L101+50E 99+25N	1	270	1620	2444	4.2	12	12	8339	2.10	82	5	ND	1	54	38	2	2	28	2.54	.228	21	48	.27	70	.03	8	3.89	.01	.04	2	1
L101+50E 99+00N	1	311	1983	1540	6.4	12	12	9901	2.18	67	5	ND	1	25	55	2	3	39	.88	.190	22	37	.22	48	.04	10	4.60	.02	.03	2	33
L101+50E 98+75N	1	128	275	1904	2.6	21	12	4568	3.70	62	5	ND	1	26	20	2	2	49	1.13	.069	10	39	.83	57	.05	6	3.03	.01	.03	1	1
L101+50E 98+50N	1	21	52	267	1.1	6	7	1453	3.11	18	5	ND	1	12	3	2	2	54	.19	.041	5	19	.29	61	.05	3	1.61	.01	.03	1	1
L101+50E 98+25N	1	25	50	282	.9	5	5	669	3.26	27	5	ND	1	11	2	3	2	61	.15	.035	4	21	.33	45	.05	4	1.54	.01	.03	1	3
L101+50E 98+00N	1	34	114	396	1.0	7	6	367	3.47	19	5	ND	1	9	1	3	2	60	.11	.034	4	28	.32	29	.03	6	3.06	.01	.02	1	75
L101+50E 97+75N	1	10	43	145	.3	4	8	437	2.90	9	5	ND	1	9	1	2	2	96	.22	.021	4	16	.15	28	.09	2	1.16	.01	.02	1	3
L101+50E 97+50N	1	25	50	222	.9	7	8	208	8.64	22	5	ND	2	11	1	2	2	126	.13	.026	4	36	.25	20	.11	2	2.15	.01	.03	1	1
L101+50E 97+25N	1	159	247	2081	6.3	14	8	2602	3.22	63	5	ND	1	32	19	2	2	51	1.22	.054	18	54	.33	44	.05	4	2.24	.01	.03	3	1
L101+50E 96+75N	2	10	72	281	1.4	4	11	542	4.37	6	5	ND	1	11	1	2	3	84	.25	.040	5	22	.09	31	.13	5	1.50	.01	.03	1	1
L101+50E 96+50N	1	9	64	133	.3	10	6	474	4.66	13	5	ND	1	12	1	3	2	95	.14	.050	4	39	.41	22	.05	4	2.12	.01	.02	1	1
STD. C. 150-1	17	57	35	132	6.5	64	27	1048	4.10	39	17	8	36	47	17	16	20	55	.46	.087	38	55	.92	176	.06	34	1.96	.06	.14	11	52

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	NI PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CR %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	VA %	K %	W PPM	AU* PPM
L101+50E 95+75N	1	3	64	58	.2	4	4	486	2.17	9	5	ND	1	7	1	2	2	45	.06	.039	4	16	.13	19	.02	2	1.12	.01	.01	1	2
L101+50E 95+50N	1	14	26	147	.3	4	8	922	4.08	13	5	ND	1	12	1	2	2	31	.11	.059	5	13	.30	35	.01	4	1.43	.01	.02	1	1
L101+50E 95+25N	1	5	4	20	.1	1	1	114	.36	2	5	ND	1	7	1	2	2	11	.08	.015	5	7	.03	22	.02	7	.27	.01	.02	1	37
L101+50E 95+00N	1	12	19	55	.1	5	6	496	3.04	7	5	ND	1	14	1	2	2	67	.17	.035	4	26	.22	48	.03	2	1.33	.01	.01	1	1
L101+50E 94+75N	1	13	17	68	.1	18	8	347	4.17	6	5	ND	1	15	1	2	6	88	.15	.038	3	52	.30	42	.05	3	1.51	.01	.02	1	1
L102E 99+90N	1	13	36	250	.2	7	5	141	2.80	2	5	ND	1	15	1	3	2	120	.29	.011	7	22	.13	51	.08	2	1.41	.01	.02	1	4
L102E 99+25N	1	77	100	705	2.4	20	11	433	6.63	21	5	ND	1	17	1	2	6	104	.17	.048	5	53	.84	43	.07	5	2.87	.01	.02	1	3
L102E 99+20N	1	315	3540	2127	7.1	14	14	11910	2.27	96	5	ND	1	30	48	2	2	37	1.03	.142	24	56	.24	56	.04	8	3.31	.02	.01	1	1
L102E 98+75N	1	265	53	2430	2.6	13	5	6914	.67	20	5	ND	1	69	63	3	2	10	3.78	.129	9	21	.15	109	.01	7	1.32	.01	.03	3	1
L102E 98+50N	1	18	31	156	1.0	8	6	403	3.58	22	5	ND	1	10	1	2	2	110	.20	.033	5	20	.19	18	.07	2	1.35	.01	.01	1	6
L102E 98+25N	1	97	414	1255	2.1	15	12	3499	3.65	58	5	ND	1	24	14	2	6	55	.83	.064	11	38	.43	50	.05	5	3.04	.01	.01	1	7
L102E 98+00N	1	45	119	901	1.3	18	10	1336	3.41	43	5	ND	1	21	7	2	2	55	.76	.042	7	40	.49	39	.05	5	2.15	.01	.02	1	3
L102E 97+75N	1	308	1009	2599	5.6	29	9	12557	1.58	41	5	ND	1	50	68	2	2	21	3.07	.118	37	49	.43	135	.01	4	1.91	.01	.04	2	1
L102E 97+50N	1	33	80	271	.9	14	9	399	3.60	15	5	ND	1	10	1	2	2	63	.11	.033	6	16	.36	48	.07	3	3.77	.01	.02	1	3
L102E 97+25N	1	26	97	532	.3	13	16	1197	4.82	37	5	ND	1	10	3	4	2	68	.15	.046	5	34	.34	51	.06	3	2.46	.01	.02	1	2
L102E 97+00N	1	20	44	125	.5	15	8	472	5.20	16	5	ND	2	11	1	3	2	84	.13	.043	4	44	.40	22	.07	2	1.97	.01	.03	1	21
L102E 97+00AN	1	24	56	134	.1	15	9	308	5.49	19	5	ND	1	15	1	3	2	143	.16	.023	4	48	.46	20	.06	2	2.00	.01	.01	1	1
L102E 96+75N	1	18	153	282	.7	10	5	310	4.23	12	5	ND	1	10	1	2	2	53	.17	.056	3	39	.29	21	.05	3	3.44	.01	.02	2	1
L102E 96+50N	1	9	40	55	.1	4	5	175	2.56	8	5	ND	1	4	1	2	2	68	.04	.019	4	23	.10	13	.05	4	1.08	.01	.01	1	1
L102E 96+50N	1	16	38	67	.2	12	7	464	4.84	14	5	ND	1	10	1	2	2	87	.12	.056	4	42	.26	31	.05	2	1.74	.01	.01	1	1
L102E 95+25N	1	21	38	100	.1	18	8	545	4.99	15	5	ND	1	12	1	2	2	85	.14	.049	4	46	.46	42	.04	3	2.07	.01	.03	1	1
L102E 95+00N	1	17	24	84	.1	9	9	3631	3.46	4	5	ND	1	16	1	2	2	62	.31	.080	4	19	.40	65	.03	5	1.61	.01	.05	1	1
L102E 94+75N	1	16	20	71	.1	17	7	540	4.00	5	5	ND	1	16	1	2	2	70	.24	.048	3	35	.35	54	.05	3	1.96	.01	.04	1	4
L10+75E 96+75N	6	45	419	439	8.4	17	15	12644	1.10	12	5	ND	1	14	13	2	2	12	.54	.163	17	12	.07	55	.01	2	3.70	.01	.03	1	1
L10+75E 96+00N	1	16	16	72	.2	7	7	442	5.25	7	5	ND	1	8	1	2	2	77	.09	.048	4	25	.15	13	.08	5	1.17	.01	.02	1	1
L10+75E 95+75N	1	40	94	296	1.3	13	8	456	4.46	27	5	ND	1	9	1	3	2	57	.11	.057	5	36	.41	35	.05	2	4.12	.01	.02	1	2
L10+75E 95+00N	1	11	43	86	.3	6	7	268	5.62	24	5	ND	1	8	1	2	2	74	.09	.062	5	27	.27	25	.03	2	1.76	.01	.02	1	1
L10+75E 94+75N	1	8	11	37	.1	4	4	393	1.63	2	5	ND	1	9	1	2	2	41	.10	.019	4	21	.07	30	.03	4	.49	.01	.02	1	1
L10+75E-94+50N	1	27	55	222	.2	16	12	531	5.29	39	5	ND	1	16	1	3	2	64	.22	.048	5	35	.64	61	.02	5	2.90	.01	.04	1	6
STD C/AD-S	18	57	40	132	6.8	67	28	1044	4.10	38	18	7	37	47	17	16	19	56	.46	.087	38	58	.91	173	.06	32	1.96	.06	.14	13	50

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 1-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR NH FE SR CA P LA CR NG BA YI B W AND LIMITED FOR NA K AND AL. NO DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: P1-5 SOIL P6 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 16 GR SAMPLE.

DATE RECEIVED: JUL 19 1988 DATE REPORT MAILED: July 27/88 ASSAYER: C. Leong, D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

HARRISBURG-DAYTON RES. PROJECT B8804 File # 88-2804 Page 1

SAMPLE#	No	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	V	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	%	PPM	PPM
L88+50E 91+75N	1	10	21	25	.1	1	1	69	1.63	2	5	ND	1	4	1	2	2	33	.04	.083	3	7	.07	16	.03	2	1.20	.01	.01	2	2
L88+50E 91+25N	3	15	36	80	.4	7	4	191	2.79	5	5	ND	1	8	1	2	3	39	.06	.070	6	22	.37	25	.03	2	2.17	.01	.02	1	1
L88+50E 91+00N	1	4	11	16	.1	1	1	37	.69	2	5	ND	1	3	1	3	4	19	.03	.014	3	4	.03	17	.04	2	.55	.01	.01	1	1
L88+50E 90+75N	1	1	6	17	.1	1	1	13	.32	2	5	ND	1	5	1	2	2	7	.04	.036	2	3	.02	15	.02	2	.47	.01	.01	2	1
L88+50E 90+50N	1	12	47	87	.1	6	4	162	4.82	19	5	ND	1	7	1	2	3	76	.06	.036	4	25	.26	22	.12	2	2.78	.01	.03	1	1
L88+50E 90+25N	2	21	32	143	.4	8	8	1038	4.64	21	5	ND	1	16	1	2	2	71	.08	.081	4	13	.39	74	.11	4	3.25	.01	.04	1	1
L88+50E 90+00N	2	27	50	229	.7	6	10	909	4.57	174	5	ND	1	11	1	4	2	67	.10	.071	3	10	.38	52	.11	3	2.63	.01	.06	1	1
L88+50E 89+50N	2	47	157	354	1.1	16	12	600	4.58	115	5	ND	1	19	1	2	4	65	.16	.048	4	28	.57	40	.09	6	3.17	.01	.01	1	1
L88+50E 89+25N	1	105	560	982	4.0	23	59	3476	5.59	171	5	ND	1	31	8	7	2	60	.34	.124	3	17	.66	85	.05	4	4.44	.01	.04	1	2
L88+50E 89+00N	1	46	211	364	5.5	6	7	393	3.74	76	5	ND	1	8	1	2	2	48	.13	.053	3	13	.36	20	.08	2	3.87	.01	.01	1	1
L88+50E 88+75N	1	47	180	247	1.5	14	14	586	4.55	32	5	ND	1	15	1	4	4	62	.09	.058	4	22	.55	58	.08	2	4.11	.01	.03	1	3
L88+50E 88+50N	1	30	83	143	.7	4	7	451	6.15	9	5	ND	1	15	1	2	2	87	.11	.083	2	14	.62	87	.13	2	3.75	.01	.05	1	1
L88+50E 88+00N	1	22	44	85	.2	2	5	250	4.59	9	5	ND	1	6	1	3	2	73	.09	.072	2	11	.29	33	.12	2	3.73	.01	.02	1	1
L88+50E 87+50N	3	36	55	133	.7	8	5	407	4.40	8	5	ND	1	9	1	2	3	62	.08	.064	3	22	.42	57	.08	2	4.32	.01	.05	1	5
L88+50E 87+25N	2	32	54	156	.8	10	7	334	4.77	19	5	ND	1	9	1	2	2	64	.10	.081	3	28	.58	44	.08	3	5.69	.01	.02	1	7
L88+50E 87+00N	3	34	58	116	1.0	6	6	471	4.29	10	5	ND	1	6	1	2	2	50	.09	.082	3	18	.31	27	.07	6	4.43	.01	.04	1	1
L88+50E 86+75N	2	34	76	73	1.3	7	5	238	5.17	11	5	ND	1	10	2	2	4	83	.18	.046	4	14	.24	26	.18	5	1.87	.01	.04	1	2
L88+50E 86+50N	5	22	36	91	.8	4	6	328	3.81	2	5	ND	1	6	2	2	2	69	.09	.053	4	14	.36	23	.14	3	5.09	.01	.01	1	1
L88+50E 86+00N	2	31	41	116	.2	10	3	229	2.55	8	5	ND	1	10	1	4	2	51	.13	.062	4	25	.61	26	.05	4	2.33	.01	.02	2	1
L89+50E 91+25N	1	3	13	28	.1	1	2	75	1.16	2	5	ND	1	4	1	3	2	34	.03	.023	2	10	.08	15	.07	2	.55	.01	.01	1	1
L89+50E 91+00N	1	12	10	25	.1	3	2	33	1.50	3	6	ND	1	3	1	2	2	19	.02	.055	4	7	.03	12	.02	2	1.61	.01	.02	2	1
L89+50E 90+25N	3	25	27	78	.3	6	4	260	4.05	53	5	ND	1	7	1	5	4	61	.08	.045	4	13	.26	18	.10	4	4.22	.01	.05	1	1
L89+50E 89+75N	2	52	184	218	1.7	11	10	1040	3.94	174	5	ND	1	11	2	4	3	57	.10	.083	4	13	.31	44	.07	3	2.80	.01	.03	1	12
L89+50E 89+00N	1	33	35	75	.5	4	5	235	5.86	9	5	ND	1	7	1	2	2	80	.06	.072	2	13	.34	27	.12	3	4.01	.01	.02	1	2
L89+50E 87+75N	1	25	35	67	.4	4	4	196	6.00	9	5	ND	1	12	1	2	5	90	.12	.069	2	13	.28	38	.13	2	4.42	.01	.03	1	1
L89+50E 87+50N	1	7	23	42	.1	2	3	114	3.09	2	5	ND	1	8	1	4	2	101	.12	.026	2	8	.15	29	.12	3	.62	.01	.03	2	1
L89+50E 87+25N	1	16	24	56	.3	9	4	147	5.41	3	7	ND	1	7	1	2	2	112	.21	.046	2	34	.46	30	.12	2	2.18	.01	.04	1	1
L89+50E 87+00N	1	86	11	25	.6	1	2	22	.16	2	5	ND	1	5	1	2	2	2	.07	.110	9	2	.01	3	.01	2	3.49	.01	.01	1	1
L89+50E 86+75N	13	15	32	93	.7	2	5	362	5.08	8	5	ND	3	27	1	2	2	97	.09	.044	5	10	1.07	76	.18	3	2.47	.02	.14	1	2
L89+50E 86+50N	2	27	37	104	.9	7	5	224	1.44	25	5	ND	1	7	1	2	3	45	.08	.054	3	18	.25	28	.10	2	5.50	.01	.03	1	8
L89+50E 86+25N	1	9	14	29	.5	2	2	56	1.42	4	5	ND	1	3	1	2	2	27	.04	.025	2	9	.07	9	.04	2	.86	.01	.02	1	1
L89+50E 86+00N	1	19	32	61	2.8	4	3	71	2.32	10	5	ND	1	13	1	2	2	14	.12	.132	7	13	.10	46	.01	4	2.28	.01	.10	1	1
L90E 90+25N	3	25	26	64	.2	8	4	159	3.04	35	5	ND	2	7	1	3	2	40	.08	.059	5	16	.22	21	.08	3	5.66	.01	.01	1	1
L90E 90+00N	1	12	20	47	.1	5	3	160	1.68	15	5	ND	1	15	1	5	2	46	.21	.024	3	8	.08	53	.07	2	.55	.01	.04	2	1
L90E 89+50N	2	23	71	215	.9	8	5	747	3.48	125	5	ND	1	19	3	3	3	82	.23	.055	4	15	.24	70	.11	4	1.68	.01	.05	1	1
L90E 88+50N	2	28	43	134	1.4	7	6	254	3.79	20	5	ND	3	8	1	2	2	50	.08	.054	3	19	.28	35	.12	5	5.29	.02	.03	1	10
STD C/AU-S	17	57	36	132	7.1	67	27	1073	3.98	38	17	6	36	47	17	17	21	56	.45	.087	39	56	.89	172	.06	33	1.91	.06	.13	12	52

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	V	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Tl	B	Al	Wa	K	V	As*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
L90E 88+25N	2	36	44	198	.6	30	11	422	4.46	22	5	ND	1	11	1	2	2	63	.11	.049	2	59	.68	49	.09	4	4.51	.01	.05	1	1
L90E 87+50N	23	30	26	121	.4	28	8	634	6.24	3	5	ND	2	13	1	2	2	143	.20	.066	2	170	1.56	87	.20	6	5.52	.02	.12	1	1
L90E 87+25N	1	26	28	73	.5	7	5	421	5.27	4	5	ND	1	7	1	2	2	120	.13	.047	2	23	.57	36	.17	6	3.24	.01	.05	1	1
L90E 87+00N	1	12	18	44	.1	5	4	205	5.92	4	5	ND	1	5	1	2	3	113	.08	.035	2	11	.34	26	.20	3	1.80	.01	.04	1	1
L90E 86+50N	3	17	34	73	.5	7	4	581	3.78	15	5	ND	1	14	1	2	2	69	.17	.054	3	13	.22	37	.08	3	1.46	.01	.05	1	2
L90+50E 91+00N	1	13	18	35	.1	5	3	92	2.60	8	5	ND	1	4	1	3	2	48	.02	.025	4	16	.07	13	.07	2	1.31	.01	.02	1	1
L90+50E 90+50N	4	17	36	79	.5	7	4	566	4.03	16	5	ND	1	15	1	2	2	73	.18	.058	2	13	.24	40	.09	2	1.61	.01	.06	1	1
L90+50E 90+25N	2	41	29	83	.6	12	26	1000	2.18	12	5	ND	1	12	1	2	2	40	.09	.101	5	10	.19	19	.03	2	2.61	.01	.04	1	1
L90+50E 90+00N	3	41	31	316	.4	22	10	508	4.90	96	5	ND	2	12	1	2	4	73	.10	.035	5	29	.62	36	.09	2	2.80	.01	.06	1	2
L90+50E 89+50N	1	35	54	179	.2	12	30	1262	3.47	122	5	ND	1	57	2	4	2	48	.63	.097	3	15	.40	140	.04	4	2.04	.01	.08	1	1
L90+50E 89+00N	2	43	49	155	.4	26	9	344	5.02	63	5	ND	2	13	1	3	2	67	.14	.048	3	50	.54	47	.08	2	3.94	.01	.03	1	1
L90+50E 88+75N	5	54	115	184	1.6	21	13	616	7.12	40	6	ND	1	19	1	2	2	73	.09	.111	3	29	.61	59	.09	2	3.49	.01	.07	1	8
L90+50E 88+00N	3	16	23	41	.3	6	3	146	3.03	7	5	ND	1	6	1	2	2	72	.06	.028	3	10	.13	19	.09	2	1.15	.01	.02	1	1
L90+50E 87+75N	2	19	43	67	.7	7	5	285	3.21	15	5	ND	1	9	1	2	2	67	.08	.045	2	13	.19	23	.08	2	1.38	.01	.04	1	1
L90+50E 87+50N	2	18	26	54	.3	5	3	193	3.74	11	5	ND	1	4	1	2	2	62	.04	.046	2	12	.21	14	.09	2	3.28	.01	.02	1	1
L90+50E 87+25N	3	97	23	62	3.4	5	9	1028	2.03	11	5	ND	1	11	2	2	2	35	.10	.193	9	8	.08	26	.06	4	4.99	.01	.04	1	1
L90+50E 87+00N	1	21	63	203	.7	10	5	731	3.23	117	5	ND	1	19	3	3	2	76	.23	.051	4	12	.22	69	.11	2	1.63	.01	.05	1	4
L90+50E 86+25N	1	13	10	31	.4	5	3	78	1.73	7	5	ND	1	5	1	2	2	44	.04	.029	5	11	.08	12	.02	2	.93	.01	.05	2	1
L90+50E 86+00N	1	27	19	51	1.3	7	5	32	.88	2	5	ND	1	8	1	2	3	5	.08	.136	7	4	.03	10	.01	6	2.27	.01	.09	1	1
L91E 93+25N	2	13	26	48	1.0	7	7	224	2.50	3	5	ND	1	9	1	2	2	43	.10	.067	4	12	.24	20	.03	2	2.25	.01	.05	1	1
L91E 93+00N	2	19	28	133	.2	11	5	250	3.00	31	5	ND	1	9	1	3	2	47	.08	.031	4	19	.32	26	.03	4	1.69	.01	.05	1	1
L91E 92+75N	1	15	14	43	.5	8	4	155	1.52	5	5	ND	1	6	1	2	2	24	.04	.049	3	9	.18	17	.02	3	1.07	.01	.05	1	1
L91E 92+50N	1	25	19	55	.4	6	5	294	3.13	21	5	ND	1	8	1	2	5	43	.09	.052	3	12	.18	20	.08	4	2.87	.01	.02	1	2
L91E 92+25N	1	14	90	46	.3	4	3	82	1.60	8	5	ND	1	19	1	2	2	28	.08	.055	2	7	.12	40	.05	2	.98	.01	.04	1	1
L91E 92+00N	1	10	5	34	.3	4	4	61	1.77	9	6	ND	2	4	1	2	2	54	.04	.019	2	6	.04	16	.11	2	.39	.01	.03	1	1
L91E 90+75N	1	19	23	59	.2	7	5	161	1.80	15	5	ND	1	6	1	2	2	63	.05	.042	4	17	.19	19	.09	2	2.09	.01	.03	1	1
L91E 90+50N	1	26	22	63	.4	7	7	402	3.46	23	5	ND	1	11	1	2	4	43	.13	.057	3	12	.21	24	.09	7	3.53	.01	.04	1	1
L91E 90+25N	1	16	29	75	.4	5	5	292	3.44	28	5	ND	1	7	1	2	2	72	.10	.033	3	12	.21	35	.12	2	1.57	.01	.06	1	1
L91E 90+00N	2	30	58	143	.4	7	6	423	3.87	37	5	ND	1	9	1	6	2	68	.08	.055	4	14	.27	38	.08	2	2.61	.01	.04	1	25
L91E 88+25N	2	25	33	75	.8	11	5	675	4.43	15	5	ND	1	14	1	2	2	71	.20	.081	2	26	.31	42	.09	2	1.98	.01	.05	1	1
L91E 87+75N	2	13	20	46	.4	7	4	231	4.61	4	5	ND	2	8	1	2	2	86	.10	.038	2	17	.45	23	.10	4	3.24	.01	.02	1	1
L91E 87+50N	2	15	16	31	.6	5	4	143	3.49	8	5	ND	1	4	1	2	2	71	.05	.026	8	14	.14	16	.04	2	1.87	.01	.02	1	40
L91E 87+25N	1	31	16	29	.4	3	6	146	3.19	7	5	ND	1	4	1	3	2	98	.03	.024	7	10	.18	8	.07	3	1.71	.01	.04	1	9
L91E 86+75N	1	9	13	28	.4	4	3	107	2.53	6	6	ND	1	7	1	3	2	50	.08	.035	5	10	.15	15	.03	2	1.59	.01	.04	1	9
L91E 86+50N	1	45	40	39	1.6	17	4	63	.38	3	5	ND	1	7	1	3	2	4	.08	.189	6	15	.09	11	.01	5	2.01	.01	.10	1	1
L91E 86+25N	1	8	6	38	.3	6	4	123	2.44	7	5	ND	1	6	1	2	2	65	.04	.013	5	16	.12	15	.05	3	.82	.01	.02	1	1
STD C/AD-S	17	57	38	132	6.9	68	29	1075	3.99	38	17	8	37	48	17	16	20	57	.45	.083	39	57	.89	175	.06	33	1.92	.06	.13	12	53

SAMPLE	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Tl	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	B	Al	Na	K	Mg	Zn*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
L91K 86	1	12	15	52	.1	5	8	108	.55	2	5	ND	1	15	2	2	2	4	.15	.078	5	3	.05	39	.01	6	1.26	.01	.07	2	1
L91+50K 87+75N	1	10	27	46	.1	8	5	343	5.06	16	5	ND	1	9	1	3	2	91	.11	.037	4	35	.33	28	.11	3	3.04	.01	.02	1	3
L91+50K 87+50N	2	21	20	36	.4	3	5	189	4.85	11	5	ND	1	5	1	2	2	78	.04	.048	6	20	.16	15	.07	4	3.28	.01	.01	1	1
L91+50K 87+00N	1	16	35	60	.9	8	6	200	6.86	29	5	ND	1	8	1	3	2	84	.05	.027	5	28	.32	28	.04	2	2.24	.01	.04	1	1
L91+50K 86+75N	1	5	36	51	.3	3	5	181	2.13	6	5	ND	1	9	1	3	2	54	.07	.017	5	16	.10	26	.07	2	.77	.01	.03	1	1
L91+50K 86+50N	1	25	31	80	.4	11	6	274	6.16	23	5	ND	2	11	1	2	2	73	.08	.030	6	32	.44	60	.02	2	2.83	.01	.04	1	1
L91+50K 86+25N	1	10	18	44	.3	4	8	138	4.34	10	5	ND	1	10	1	3	4	95	.08	.020	4	25	.18	32	.07	6	1.20	.01	.03	1	1
L91+50K 86+00N	1	8	19	52	.3	4	5	255	4.88	12	5	ND	1	9	1	3	2	124	.06	.027	5	23	.23	28	.09	3	1.54	.01	.04	1	1
L92K 87+75N	1	10	38	41	.5	7	5	181	3.41	10	5	ND	2	7	1	2	2	68	.07	.037	5	16	.16	22	.14	3	1.26	.01	.02	1	2
L92K 87+50N	1	18	15	42	.9	2	3	12	.08	2	5	ND	1	6	1	4	2	3	.08	.109	18	2	.01	7	.01	9	2.81	.01	.04	2	1
L92K 87+25N	1	11	12	49	.2	4	4	15	.17	4	5	ND	1	10	1	3	2	2	.18	.134	7	3	.02	11	.01	4	2.06	.01	.04	1	1
L92K 87+00N	2	12	30	78	.2	11	6	207	3.39	18	5	ND	1	13	1	5	2	65	.11	.020	6	30	.51	32	.07	7	1.90	.01	.05	1	1
L92K 86+75N	2	24	27	59	.2	1	11	215	13.21	21	5	ND	1	6	1	2	2	44	.07	.073	6	10	.08	15	.02	2	2.31	.01	.06	1	1
L92K 86+54N	2	20	25	85	.1	11	7	241	6.62	26	5	ND	1	11	1	2	2	93	.10	.026	5	44	.39	41	.04	3	2.83	.01	.03	1	1
L92K 86+25N	1	13	14	33	.7	2	3	62	2.18	2	5	ND	1	5	1	2	2	38	.02	.029	6	17	.03	20	.03	4	2.09	.01	.02	1	1
L92K 86+00N	1	14	25	82	.4	4	5	190	5.71	18	5	ND	1	8	1	2	2	82	.04	.034	5	25	.29	47	.03	3	2.39	.01	.04	1	5
L92+50K 87+75N	1	37	25	47	.9	5	5	96	2.85	10	5	ND	1	6	1	2	2	31	.06	.052	7	23	.11	19	.05	6	3.54	.01	.03	1	18
L92+50K 87+50N	1	23	24	50	2.6	5	3	62	.61	3	7	ND	1	19	1	4	2	4	.19	.144	6	5	.04	65	.01	5	1.89	.01	.08	1	1
L92+50K 87+25N	1	18	25	80	.3	13	7	318	4.95	18	6	ND	1	10	1	2	2	102	.08	.035	5	34	.31	34	.12	7	1.98	.01	.05	1	1
L92+50K 87+00N	2	31	33	170	.3	23	10	458	5.27	23	5	ND	1	12	1	2	2	82	.09	.031	6	42	.73	60	.07	4	2.75	.01	.04	1	1
L92+50K 86+75N	2	19	32	89	.4	11	7	244	6.68	17	5	ND	2	10	1	2	2	102	.08	.030	5	40	.41	32	.11	6	3.50	.01	.05	1	2
L92+50K 86+50N	1	3	7	23	.9	1	2	42	1.40	2	5	ND	1	5	1	2	5	27	.03	.020	3	7	.04	14	.05	4	.96	.02	.03	1	1
L92+50K 86+25N	1	3	6	26	.4	1	3	53	1.10	4	7	ND	1	7	1	3	2	29	.05	.013	4	7	.04	27	.03	5	.47	.01	.04	1	1
L92+50K 86+00N	2	16	23	67	.3	7	4	235	5.33	15	5	ND	1	6	1	2	4	86	.05	.057	5	22	.25	34	.06	2	1.98	.01	.05	1	2
L93K 87+50N	1	26	138	163	2.5	13	8	365	6.02	21	5	ND	3	9	1	2	2	71	.09	.056	5	48	.44	35	.09	8	6.07	.01	.05	1	2
L93K 87+25N	1	15	21	48	.4	5	5	162	2.50	7	5	ND	1	7	1	2	2	61	.05	.033	4	19	.14	25	.09	9	1.35	.01	.03	1	1
L93K 87+00N	1	11	20	50	.3	6	5	162	3.10	10	5	ND	1	6	1	2	5	60	.05	.027	5	16	.14	29	.06	3	1.32	.01	.03	1	1
L93K 86+75N	1	13	12	33	.4	5	3	32	1.54	2	5	ND	1	7	1	2	2	13	.07	.072	2	8	.05	13	.01	10	1.91	.02	.01	1	1
L93K 86+50N	1	5	12	34	.2	8	6	159	2.95	5	6	ND	2	5	1	4	2	95	.03	.011	6	31	.07	23	.08	4	.81	.01	.03	1	1
L93K 86+25N	2	18	28	84	.4	12	8	250	8.25	23	5	ND	3	7	1	2	2	106	.05	.031	6	38	.43	43	.10	2	2.66	.01	.05	1	2
L93K 86+00N	1	14	33	86	1.0	6	6	199	5.49	19	5	ND	3	6	1	2	2	79	.05	.037	6	32	.28	39	.05	5	2.83	.01	.07	1	1
L93+50K 104+00N	11	53	107	231	1.4	17	19	778	6.07	246	5	ND	1	19	3	2	2	77	.26	.090	5	13	.19	94	.04	2	2.11	.01	.07	1	5
L93+50K 103+75N	9	75	159	198	3.3	14	26	985	8.27	438	5	ND	1	12	1	2	2	53	.08	.108	5	23	.48	32	.06	4	5.31	.01	.06	1	29
L93+50K 103+50N	2	35	75	67	.4	6	5	220	4.57	220	5	ND	2	6	1	2	2	33	.06	.066	5	19	.18	25	.07	4	7.12	.01	.01	1	26
L93+50K 103+25N	1	35	114	143	1.1	10	8	1162	4.46	104	5	ND	1	17	1	3	2	52	.20	.098	4	16	.28	62	.04	4	1.81	.01	.04	1	50
L93+50K 103+00N	2	46	266	185	4.6	9	33	1524	4.97	128	5	ND	2	11	1	3	2	48	.07	.129	4	19	.29	29	.03	6	2.66	.01	.03	1	3
STD C/AD-S	17	58	36	131	7.2	68	28	1064	3.91	39	18	7	36	47	18	16	20	56	.44	.085	38	57	.87	175	.06	33	1.90	.06	.13	12	50

SAMPLE	No PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Cr %	P %	La PPM	Ce PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Ca %	K %	W PPM	Au*
L93+50E 102+75N	2	53	290	241	2.2	13	20	689	5.74	302	5	ND	1	9	1	5	13	37	.09	.107	7	19	.39	23	.06	5	3.92	.01	.03	1	28
L93+50E 102+50N	1	37	229	325	2.2	12	25	1651	2.65	89	5	ND	1	27	5	3	6	34	.48	.076	6	13	.22	70	.04	4	1.91	.01	.02	1	5
L93+50E 102+25W	2	37	105	572	1.0	13	26	4472	4.24	149	5	ND	1	27	5	2	2	52	.58	.117	4	19	.41	85	.03	4	1.93	.01	.05	1	1
L93+50E 102+00N	3	38	185	254	1.6	18	26	3710	3.79	161	5	ND	1	15	1	3	5	46	.25	.127	4	25	.41	73	.02	8	2.34	.01	.04	1	2
L93+50E 101+75W	3	56	113	410	3.6	23	5	419	2.58	387	5	ND	1	19	5	2	2	39	.52	.121	20	42	.59	23	.01	7	2.60	.02	.05	1	67
L93+50E 101+50N	7	39	179	367	2.4	16	26	2865	3.65	380	5	ND	1	16	4	4	3	46	.40	.144	12	27	.40	29	.02	4	3.14	.02	.04	1	3
L93+50E 101+25W	5	35	103	229	1.0	14	15	2677	3.60	140	5	ND	1	19	4	4	2	46	.39	.099	6	21	.27	65	.03	3	1.50	.01	.05	1	10
L93+50E 101+00N	3	41	132	236	1.6	18	17	3101	4.43	143	5	ND	1	15	4	2	2	43	.28	.164	11	22	.35	48	.02	3	2.60	.01	.06	1	1
L93+50E 100+75W	4	38	56	413	.9	17	19	3551	4.09	71	5	ND	1	25	8	5	2	47	.73	.120	11	32	.43	43	.02	4	2.17	.01	.06	1	1
L93+50E 100+50N	1	33	30	80	2.3	8	5	316	4.61	22	5	ND	2	8	1	2	3	65	.13	.075	4	25	.20	18	.05	2	1.94	.01	.04	1	1
L93+50E 100+00W	2	25	43	107	.2	14	8	346	7.14	17	5	ND	3	11	1	3	3	99	.32	.051	4	39	.43	32	.12	4	2.14	.01	.02	1	4
L93+50E 99+75N	1	24	71	134	.6	13	8	388	5.82	17	5	ND	2	8	1	2	2	78	.09	.051	4	42	.30	31	.12	4	3.68	.01	.02	1	14
L93+50E 99+50N	1	18	76	109	.5	7	6	360	4.31	14	5	ND	1	9	1	3	2	76	.13	.032	3	22	.27	21	.14	5	1.78	.01	.02	1	1
L93+50E 99+25N	2	47	114	186	.3	14	20	1171	6.99	34	5	ND	3	8	1	3	2	54	.10	.090	4	27	.27	39	.05	2	3.44	.01	.05	1	1
L93+50E 99+00W	1	6	18	36	.3	2	2	83	1.93	2	5	ND	2	4	1	3	2	31	.04	.024	2	6	.03	18	.03	4	.86	.01	.02	2	1
L93+50E 98+75N	5	37	370	335	3.9	11	13	3055	1.57	32	5	ND	1	17	3	2	5	49	.40	.072	6	21	.24	73	.04	7	2.82	.01	.05	1	1
L93+50E 98+25N	3	69	223	931	1.5	24	12	2525	2.68	82	5	ND	1	32	16	6	2	33	1.35	.137	17	27	.33	41	.01	10	2.16	.01	.06	1	1
L93+50E 97+75N	2	34	170	281	1.2	15	15	3401	2.74	79	5	ND	1	11	4	3	2	39	.26	.106	15	37	.42	30	.01	8	2.58	.01	.05	1	1
L93+50E 97+50W	1	25	36	61	1.6	11	7	556	5.27	16	5	ND	1	10	1	3	2	65	.13	.049	5	37	.20	33	.04	5	1.74	.01	.03	1	2
L93+50E 97+25W	1	18	23	68	.5	12	7	266	4.12	10	5	ND	2	10	1	2	2	71	.10	.037	4	48	.35	78	.05	5	1.40	.01	.05	1	1
L93+50E 97+00N	2	27	35	142	1.1	10	10	4989	2.46	13	5	ND	1	12	2	2	2	38	.21	.143	6	34	.25	43	.01	6	2.73	.01	.04	1	1
L93+50E 87+50N	1	24	22	36	.3	6	4	121	3.58	8	6	ND	2	6	1	2	2	61	.05	.037	4	20	.14	25	.08	7	2.74	.01	.04	1	1
L93+50E 87+25W	1	42	49	48	1.5	8	10	1298	6.83	44	5	ND	2	9	1	4	2	57	.07	.197	3	8	.28	64	.03	3	2.08	.01	.04	1	6
L93+50E 87+00N	1	27	18	38	.7	12	4	155	2.95	3	5	ND	1	6	1	2	2	31	.06	.050	4	35	.44	14	.04	7	2.35	.01	.02	1	4
L93+50E 86+75W	1	26	27	41	.6	8	5	105	5.61	4	5	ND	2	9	1	3	2	51	.07	.067	4	15	.16	37	.07	4	2.34	.01	.04	1	3
L93+50E 86+50N	1	29	25	47	.2	5	4	242	5.68	4	5	ND	1	7	1	2	2	100	.07	.047	3	18	.37	33	.14	4	3.49	.01	.03	1	1
L93+50E 86+25N	2	41	20	69	.5	13	5	223	4.90	11	5	ND	2	16	1	2	5	60	.11	.062	3	27	.58	53	.07	3	5.02	.01	.06	1	8
L93+50E 86+00N	3	50	16	50	.5	11	6	211	5.27	9	5	ND	3	9	1	2	2	70	.07	.074	5	26	.40	40	.11	3	7.45	.01	.04	1	6
L94E 87+50W	1	82	43	60	1.8	5	27	1016	6.79	25	5	ND	2	7	1	3	2	61	.05	.133	3	17	.15	15	.05	3	4.24	.01	.05	1	3
L94E 87+25W	1	9	20	29	.2	3	4	292	1.97	5	5	ND	1	5	1	2	2	70	.07	.020	2	9	.13	14	.12	3	.56	.01	.03	1	13
L94E 87+00N	1	36	20	43	.5	5	4	193	2.64	3	5	ND	1	6	1	2	2	42	.06	.079	4	16	.28	18	.02	3	2.86	.01	.04	1	1
L94E 86+50N	1	23	20	28	.3	7	4	155	3.48	6	5	ND	1	7	1	2	2	44	.06	.059	4	18	.15	23	.04	7	2.60	.01	.03	1	1
L94E 86+25W	1	20	18	33	.2	5	4	832	5.43	8	5	ND	1	10	1	2	4	72	.07	.055	3	13	.19	33	.09	3	2.02	.01	.03	1	5
L94E 86+00N	2	15	25	34	.2	5	5	497	4.47	4	5	ND	1	8	1	2	2	103	.09	.048	3	13	.20	24	.09	5	1.16	.01	.03	1	2
L97+50E 103+50W	1	27	56	221	1.1	13	9	583	4.76	124	5	ND	2	12	1	2	2	62	.16	.035	6	28	.30	50	.05	5	1.97	.01	.08	1	1
L97+50E 102+75W	1	24	28	110	.4	14	11	713	4.72	22	5	ND	2	12	1	2	4	58	.13	.057	3	26	.34	35	.08	4	3.46	.01	.06	1	3
STD C/AO-S	18	58	38	127	7.1	67	28	1028	3.96	37	17	7	36	46	16	17	19	55	.46	.085	38	55	.90	175	.06	34	1.93	.06	.13	11	52

HARRISBURG-DAYTON RES. PROJECT B8804 FILE # 88-2804

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L97+50E 102+25N	1	17	53	91	.5	10	6	957	3.42	71	5	ND	1	16	1	2	2	71	.19	.038	4	27	.27	40	.05	3	1.35	.01	.10	1	3
L97+50E 101+00W	2	207	327	1200	3.1	24	12	32531	1.58	14	5	ND	1	26	85	2	2	38	.34	.149	21	19	.13	222	.02	5	4.12	.01	.05	1	1
L97+50E 100+50W	1	5	7	39	.4	4	3	319	1.64	2	5	ND	1	5	1	2	2	43	.06	.009	4	11	.04	8	.04	4	.38	.01	.02	1	1
L97+50E 100+25W	2	100	132	352	4.2	18	40	2339	3.48	154	5	ND	2	16	4	2	2	46	.20	.067	9	25	.45	70	.03	7	2.89	.01	.04	1	10
L97+50E 100+00W	2	47	356	319	6.5	12	13	2063	3.49	70	5	ND	1	30	4	4	2	48	.49	.084	7	23	.31	54	.03	4	2.31	.01	.05	1	3
L97+50E 99+75W	1	23	69	131	.7	6	5	1298	1.78	32	5	ND	1	20	3	2	2	35	.31	.041	7	12	.14	43	.03	4	1.04	.01	.03	1	1
L97+50E 99+50W	4	13	32	172	.8	7	4	2872	.58	135	5	ND	1	49	4	4	2	8	1.35	.101	3	4	.07	80	.01	11	.80	.01	.07	1	128
L97+50E 99+25W	7	36	119	78	2.3	4	15	3946	1.91	22	5	ND	1	14	2	2	2	33	.22	.121	10	19	.13	34	.01	5	2.23	.01	.04	1	1
L97+50E 99+00W	2	2	33	51	.5	3	1	69	.46	17	5	ND	1	16	1	2	2	17	.23	.030	3	7	.05	43	.02	3	.43	.01	.04	1	1
L97+50E 98+50E	2	27	87	350	.8	16	9	2429	2.27	42	5	ND	1	26	3	2	2	30	.74	.074	7	26	.35	52	.02	7	1.44	.01	.04	1	2
L97+50E 98+25N	1	13	25	45	.3	9	5	511	4.25	12	5	ND	1	8	1	2	2	67	.03	.078	5	16	.12	38	.04	5	1.04	.01	.03	1	1
L97+50E 98+00E	1	5	10	27	.3	3	1	77	1.17	5	5	ND	1	7	1	2	2	31	.01	.029	5	10	.10	24	.01	2	1.06	.01	.01	1	1
L97+50E 97+75W	1	10	10	33	.2	4	2	120	1.30	8	5	ND	1	9	1	2	2	29	.04	.042	5	13	.15	34	.01	6	.95	.01	.03	1	2
L97+50E 97+50W	1	14	21	51	.5	6	5	1910	2.16	7	5	ND	1	9	1	2	2	34	.08	.049	8	14	.15	83	.01	5	1.24	.01	.04	1	1
L97+50E 97+25W	1	7	11	37	.2	4	3	199	1.58	4	5	ND	1	6	1	2	2	40	.03	.024	4	11	.07	29	.02	3	.59	.01	.02	1	1
L97+50E 97+00W	1	13	17	47	.8	7	4	264	2.34	11	5	ND	2	6	1	2	2	39	.04	.038	5	15	.21	38	.01	3	1.19	.01	.03	1	1
STD C/AU-5	18	58	43	132	6.6	70	29	1096	4.07	39	17	8	36	47	17	21	22	58	.46	.081	39	58	.92	174	.06	34	1.98	.06	.13	11	49

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Tl	B	Al	Na	K	U	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
88-DR-1 L104X 98+75M	1	298	384	1572	7.2	2	5	6861	4.97	2	5	ND	1	2	10	6	3	2	.03	.013	7	1	.15	46	.01	23	.97	.01	.15	1	11
88-DR-2 L89+50X 104M	1	212	47	77	.9	11	19	973	6.94	3	5	ND	1	12	1	2	6	302	.52	.030	2	23	2.21	5	.30	2	2.95	.03	.20	2	58
88-DR-3 L92+30X 100+75M	1	580	30	46	5.7	6	57	711	20.65	148	5	ND	1	62	1	2	2	29	.84	.022	2	2	.36	7	.04	26	1.93	.10	.04	1	27
88-DR-4	1	5223	20096	87373	184.8	19	27	2693	6.18	1356	5	ND	1	1	2170	2765	45	2	.01	.004	2	1	.01	1	.01	32	.08	.01	.02	3	2110
88-DR-5	1	478	20198	25467	196.0	7	18	432	5.72	14061	5	ND	1	4	252	812	2	9	.01	.018	2	3	.03	17	.01	12	.34	.01	.13	1	1192
88-DR-6	1	112	20052	4816	203.6	3	2	451	1.21	747	5	ND	1	3	71	950	3	7	.02	.022	2	4	.08	16	.01	5	.12	.01	.09	2	783
88-DR-7	1	228	1147	8709	35.7	1	31	57233	14.17	13309	7	ND	4	40	60	352	2	11	7.62	.002	10	3	.90	10	.01	2	.39	.01	.08	1	112
88-DR-8	1	35	901	59752	4.9	4	23	7713	7.41	13781	5	ND	1	23	607	17	2	19	5.04	.005	1	1	.82	15	.01	8	1.52	.01	.06	3	70
88-DR-9	1	5387	20738	52630	366.6	18	22	4482	10.28	86	5	ND	2	3	566	101	700	46	.06	.017	2	55	.75	19	.01	6	3.28	.01	.13	3	543
88-DR-10	2	1031	1978	11101	43.0	13	13	3293	14.02	45	5	ND	1	1	109	20	33	58	.04	.015	2	42	.98	13	.01	5	1.94	.01	.12	1	13
88-DR-11	1	1788	1640	16323	35.3	4	16	4934	9.25	29	5	ND	1	2	173	10	5	60	.10	.062	3	13	.95	29	.01	7	3.40	.01	.12	1	37
88-DR-12	1	792	50	28054	1.9	15	40	160	30.12	345	5	ND	1	38	257	2	8	18	1.31	.186	2	3	.05	4	.05	5	1.64	.12	.03	2	106
STD C/AU-8	18	59	39	131	6.6	69	29	1038	4.08	38	23	8	37	47	17	17	20	58	.46	.086	41	56	.92	175	.06	34	1.96	.06	.13	13	470

- ASSAY REQUIRED FOR CORRECT RESULT for Pb Zn As > 10,000 ppm
 Ag > 35 ppm
 Sb > 1000 ppm

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR NH FK SR CA P LA CR NG BA TI B W AND LIMITED FOR NA K AND AL. AD DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-P7 SOIL P8 ROCK AD* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JUL 22 1988 DATE REPORT MAILED: July 29/88 ASSAYER: C. Leong D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

HARRISBURG DAYTON RES. CORP. PROJECT B8804 File # 88-2917 Page 1

Table with columns: SAMPLE#, No PPM, Cu PPM, Pb PPM, Zn PPM, Ag PPM, Ni PPM, Co PPM, Mn PPM, Fe PPM, As PPM, U PPM, Au PPM, Tl PPM, Sr PPM, Cd PPM, Sb PPM, Bi PPM, V PPM, Ca PPM, P PPM, La PPM, Cr PPM, Mg PPM, Ba PPM, Ti PPM, B PPM, Al PPM, Na PPM, K PPM, W PPM, Au* PPM.

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	U PPM	Au PPM	Tl PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Yt %	B PPM	Al %	Na %	K %	W PPM	Au ^c PPM
L85+92E 9457Y	1	20	51	98	1.0	10	3	214	1.72	14	5	ND	1	6	1	2	2	33	.06	.116	4	19	.32	15	.01	2	1.56	.01	.06	1	1
L86+00E 96+50N	1	8	5	58	.2	2	2	51	.77	4	5	ND	1	4	1	2	3	27	.06	.017	3	5	.05	21	.03	6	.51	.01	.02	1	1
L86+00E 96+25N	1	11	12	66	.3	13	3	295	2.64	7	5	ND	1	7	1	2	2	44	.07	.035	5	18	.40	25	.06	8	1.38	.01	.06	1	1
L86+00E 96+00N	1	14	12	41	.3	8	3	169	1.74	3	5	ND	3	6	2	2	2	50	.05	.054	5	29	.22	19	.08	6	2.01	.01	.04	1	28
L86+00E 95+75N	1	17	18	58	.2	5	2	203	2.86	5	5	ND	1	5	3	2	2	38	.05	.049	6	11	.16	20	.06	7	2.25	.01	.03	1	1
L86+00E 95+50N	1	9	22	64	.2	6	3	241	1.48	7	5	ND	1	4	1	2	2	30	.04	.058	4	15	.21	13	.03	5	.82	.01	.05	1	1
L86+00E 95+25N	1	13	22	56	.1	6	3	232	2.21	6	5	ND	1	6	1	2	2	34	.06	.055	5	16	.25	27	.04	2	3.20	.01	.03	1	1
L86+00E 95+00N	1	15	17	43	.1	5	3	134	2.06	3	5	ND	2	6	1	2	2	41	.07	.082	5	18	.27	18	.06	6	1.44	.01	.05	1	4
L86+00E 94+75N	3	17	12	47	.1	7	3	267	4.04	7	5	ND	2	4	1	2	2	43	.03	.045	4	27	.16	15	.12	2	2.48	.01	.02	2	1
L86+00E 94+50N	1	6	33	61	.2	3	1	37	.81	3	5	ND	1	3	1	3	2	20	.02	.035	4	7	.05	12	.10	4	1.23	.01	.02	1	1
L86+00E 94+25N	1	5	12	31	.1	3	1	33	.43	5	5	ND	1	4	1	2	2	13	.03	.040	2	3	.04	14	.03	6	.53	.01	.02	1	1
L86+00E 94+00N	1	8	7	27	.3	1	1	32	.84	2	5	ND	1	3	1	2	2	20	.02	.033	7	5	.03	13	.05	9	1.37	.01	.02	1	1
L86+00E 93+75N	1	11	5	42	.1	3	2	74	1.84	6	5	ND	1	4	1	2	2	29	.02	.035	4	7	.06	17	.05	4	.95	.01	.02	1	1
L86+00E 93+50N	1	19	11	65	.1	5	2	131	1.55	4	5	WC	1	4	1	2	2	31	.04	.073	6	13	.22	14	.02	2	2.23	.01	.01	1	1
L86+00E 93+25N	1	15	16	72	.4	8	4	330	3.19	6	5	ND	3	5	1	2	2	47	.05	.053	5	20	.37	16	.06	4	2.31	.01	.04	1	1
L86+00E 93+00N	1	13	15	52	.7	5	2	100	1.74	3	5	ND	3	3	3	2	2	23	.03	.075	6	10	.12	10	.01	10	2.06	.01	.03	1	1
L86+00E 92+75N	1	17	23	91	.4	8	5	465	2.78	9	5	ND	1	5	1	4	2	53	.07	.082	4	19	.46	17	.03	2	2.08	.01	.05	2	1
L86+00E 92+50N	1	17	144	110	1.0	6	5	399	2.63	20	5	ND	2	5	1	2	2	35	.05	.109	5	17	.26	14	.02	3	1.73	.01	.05	1	1
L86+00E 92+25N	1	22	23	87	.1	6	27	7145	3.90	16	5	ND	1	6	1	2	2	70	.07	.169	4	14	.42	21	.04	2	2.75	.01	.06	1	1
L86+00E 92+00N	1	11	18	88	.2	8	13	1601	4.42	25	5	ND	4	11	1	2	2	111	.28	.042	3	19	1.09	15	.33	8	1.84	.01	.05	1	1
L86+00E 91+75N	1	4	10	24	.2	3	2	59	.55	4	7	ND	2	4	1	2	2	16	.03	.025	3	5	.06	12	.04	8	.57	.01	.03	1	1
L86+00E 91+50N	1	11	18	40	.4	4	2	58	1.41	6	5	ND	2	4	1	2	2	23	.03	.073	5	12	.10	11	.04	8	1.62	.01	.04	1	1
L86+00E 91+25N	1	22	18	86	.1	13	6	356	3.34	8	5	ND	2	9	1	2	2	55	.07	.038	6	28	.45	28	.05	2	1.98	.01	.06	1	1
L86+00E 90+75N	1	9	15	36	.7	2	2	40	1.65	2	8	ND	3	4	1	2	3	20	.03	.039	5	11	.06	11	.04	13	1.77	.01	.02	1	1
L86+00E 90+50N	1	7	21	40	.3	3	2	72	1.16	2	5	ND	2	4	1	2	2	27	.02	.037	2	7	.07	15	.06	5	.85	.01	.03	1	1
L86+00E 90+25N	1	7	9	18	.3	1	1	18	.56	2	5	ND	3	3	1	2	2	19	.02	.041	5	6	.02	8	.06	9	1.53	.01	.02	2	1
L86+50E 96+75N	1	5	5	14	.1	2	1	36	.50	2	5	ND	1	2	1	2	2	22	.03	.008	2	5	.08	12	.06	5	.29	.01	.02	1	1
L86+50E 96+50N	1	11	9	23	.1	4	2	36	1.09	2	5	ND	1	3	1	3	2	38	.03	.010	2	4	.02	16	.07	9	.21	.01	.01	1	1
L86+50E 96+25N	1	10	5	30	.3	3	3	128	1.52	4	5	ND	2	5	1	2	2	36	.08	.052	4	9	.12	17	.06	7	.90	.01	.03	1	3
L86+50E 96+00N	1	27	26	74	.3	8	10	896	5.44	13	5	ND	1	9	1	2	2	93	.09	.056	2	17	.46	34	.14	2	1.76	.01	.05	1	1
L86+50E 95+75N	1	15	8	61	.6	5	5	851	4.25	13	5	ND	3	5	1	2	2	37	.06	.043	3	8	.14	30	.09	3	1.45	.01	.04	1	1
L86+50E 95+50N	1	12	18	44	.3	6	3	146	2.54	5	5	ND	3	6	1	2	2	38	.05	.035	7	20	.24	18	.08	4	2.21	.01	.04	1	1
L86+50E 95+25N	1	10	17	32	.6	5	2	89	1.81	3	7	ND	1	5	1	2	2	39	.05	.059	4	17	.15	15	.04	3	1.53	.01	.04	1	1
L86+50E 95+00N	1	14	10	25	.3	4	2	50	1.06	2	5	ND	2	5	1	2	2	23	.04	.058	7	15	.13	16	.03	10	1.96	.01	.04	1	2
L86+50E 94+75N	1	14	8	29	.3	7	2	64	1.42	2	5	ND	1	4	1	2	4	21	.04	.073	4	15	.17	13	.03	4	1.66	.01	.04	1	1
L86+50E 94+50N	1	13	9	55	.1	7	3	147	2.60	7	5	ND	3	7	1	2	3	45	.06	.040	4	24	.22	18	.06	9	1.73	.01	.04	1	1
L86+50E 94+25N	1	10	8	22	.2	2	1	70	1.25	2	5	ND	3	4	1	2	2	30	.03	.025	4	8	.08	11	.07	10	1.01	.01	.03	2	1
STD C/AG-5	17	59	35	132	7.2	60	29	1068	4.10	37	17	7	37	47	16	17	19	58	.47	.087	38	58	.91	173	.08	34	1.97	.06	.17	12	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	V PPM	Au PPM	Tl PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Tl %	B PPM	Al %	Mg %	K %	W PPM	Au* PPM
L86+50E 34+00H	1	5	4	21	.1	3	1	35	.54	2	5	ND	1	2	1	2	2	17	.02	.017	2	5	.03	8	.03	2	.38	.01	.01	1	2
L86+50E 33+75N	1	12	10	33	.1	3	3	53	2.41	4	5	ND	1	2	1	2	2	16	.02	.045	3	8	.06	15	.05	7	1.08	.01	.02	1	1
L86+50E 32+50N	1	11	14	39	.1	7	3	108	2.11	3	5	ND	1	7	1	3	3	41	.05	.037	6	17	.21	19	.05	6	1.72	.01	.03	1	1
L86+50E 33+25N	1	10	16	21	.1	3	2	78	1.21	3	5	ND	1	5	1	2	2	30	.03	.037	4	10	.06	17	.04	2	1.00	.01	.02	1	1
L86+50E 33+00N	1	27	14	37	.2	6	3	118	1.95	5	5	ND	1	4	1	2	5	38	.04	.035	4	17	.16	14	.08	4	2.27	.01	.03	1	1
L86+50E 32+75N	1	14	133	113	.2	6	20	2406	3.52	15	5	ND	1	6	1	2	2	55	.07	.062	3	12	.36	24	.04	8	1.39	.01	.11	1	5
L86+50E 32+50N	1	20	919	135	28.2	6	4	305	1.93	19	5	ND	1	5	1	2	4	34	.09	.108	4	14	.25	10	.02	3	1.50	.01	.05	1	1
L86+50E 32+25N	1	23	37	82	.4	8	11	1133	2.48	8	5	ND	1	5	1	2	4	38	.05	.074	6	16	.31	18	.04	2	2.65	.01	.04	1	1
L86+50E 31+50N	1	16	19	81	.1	10	4	245	2.71	8	5	ND	1	6	1	2	2	39	.06	.061	5	19	.43	17	.03	4	2.01	.01	.07	1	1
L86+50E 31+25N	1	14	12	29	.3	3	2	51	1.47	2	5	ND	1	4	1	2	3	30	.03	.086	5	12	.12	9	.02	3	1.81	.01	.03	1	1
L86+50E 31+00N	2	20	24	77	.3	8	12	921	3.39	6	5	ND	1	6	1	2	2	53	.06	.121	5	14	.31	16	.06	1	2.10	.01	.06	1	1
L86+50E 30+75N	1	3	17	46	.1	2	2	161	1.68	4	5	ND	1	4	1	2	2	28	.05	.078	3	8	.15	16	.04	5	1.34	.01	.05	1	1
L86+50E 30+50N	1	19	21	52	.3	5	2	112	2.97	4	5	ND	1	5	1	2	3	28	.04	.066	7	14	.17	15	.03	5	3.05	.01	.04	2	1
L86+50E 30+25N	2	23	37	109	.1	12	7	540	4.54	13	5	ND	1	13	1	2	2	64	.07	.049	5	22	.44	55	.10	3	2.63	.01	.05	1	1
L87+00E 36+75N	1	11	11	23	.4	2	1	26	.82	2	8	ND	1	3	1	2	2	18	.04	.034	3	5	.03	11	.02	8	.93	.01	.02	1	1
L87+00E 36+50N	1	13	18	58	.1	4	3	196	1.32	2	5	ND	1	5	1	2	2	35	.11	.077	2	12	.23	16	.06	8	1.29	.01	.05	1	1
L87+00E 36+25N	1	32	18	38	.1	7	2	133	2.51	2	5	ND	1	6	1	2	3	62	.11	.049	3	11	.11	38	.05	2	1.29	.01	.02	2	1
L87+00E 36+00N	1	9	14	35	.1	6	3	113	1.61	3	5	ND	1	9	1	2	2	44	.05	.020	7	11	.10	26	.02	6	.84	.01	.03	1	1
L87+00E 35+75N	1	18	6	35	.1	6	2	64	1.34	2	5	ND	1	4	1	2	2	28	.04	.080	4	13	.09	14	.01	6	1.96	.01	.03	1	1
L87+00E 35+50N	1	18	24	95	.1	18	7	408	4.33	13	5	ND	1	8	1	2	2	62	.09	.039	9	32	.52	25	.06	6	2.38	.01	.04	1	20
L87+00E 35+25N	1	14	16	70	.1	16	5	312	2.83	6	5	ND	1	6	1	2	2	49	.07	.063	3	29	.52	18	.04	3	1.44	.01	.05	1	26
L87+00E 35+00N	1	13	16	57	.2	9	4	155	1.71	5	7	ND	1	11	1	2	4	27	.09	.042	5	23	.38	19	.03	6	1.84	.01	.05	1	1
L87+00E 34+75N	1	14	17	39	.2	10	4	154	1.93	6	5	ND	1	9	1	2	2	43	.07	.039	5	24	.22	27	.04	3	1.20	.01	.04	3	1
L87+00E 34+50N	1	12	10	22	.2	4	2	37	1.08	2	6	ND	2	4	1	2	2	20	.03	.040	4	12	.06	12	.02	7	1.68	.01	.02	1	1
L87+00E 34+00N	2	14	16	46	.8	5	4	347	1.37	14	5	ND	1	5	1	2	3	33	.05	.115	5	10	.20	17	.02	7	1.37	.01	.07	1	2
L87+00E 33+75N	1	13	16	40	.3	6	3	118	2.18	3	5	ND	2	5	1	2	4	38	.04	.036	6	13	.15	17	.07	6	1.81	.01	.03	2	1
L87+00E 33+50N	1	14	18	51	.1	9	7	634	3.70	10	5	ND	2	9	2	2	5	90	.19	.023	4	21	.58	32	.20	4	1.48	.01	.06	3	1
L87+00E 33+25N	2	17	34	61	.1	10	5	405	3.59	10	5	ND	1	7	2	3	2	57	.05	.035	6	23	.22	23	.08	4	2.05	.01	.03	1	1
L87+00E 33+00N	2	17	17	49	.9	6	3	73	1.74	7	6	ND	1	6	3	2	2	20	.03	.078	4	12	.08	26	.01	9	1.80	.01	.05	3	1
L87+00E 32+75N	1	3	12	16	.3	1	1	35	.80	2	5	ND	2	4	1	2	2	22	.06	.025	4	4	.06	5	.09	9	.74	.01	.02	1	1
L87+00E 32+50N	1	33	620	373	4.1	12	11	1121	4.75	187	6	ND	2	8	1	9	8	67	.09	.037	6	29	.41	21	.06	5	2.06	.01	.05	1	13
L87+00E 32+25N	1	8	28	52	.4	3	4	411	2.46	11	5	ND	2	24	1	3	2	58	.42	.041	2	7	.28	29	.25	7	.77	.01	.06	2	1
L87+00E 31+75N	2	16	28	81	.6	5	4	193	2.40	5	5	ND	1	5	1	2	2	36	.05	.041	5	20	.19	15	.05	6	2.25	.01	.04	1	1
L87+00E 31+50N	1	13	23	39	.6	3	2	85	1.21	2	5	ND	2	4	2	2	2	23	.03	.049	6	13	.14	9	.04	9	2.12	.01	.03	2	1
L87+00E 31+25N	1	15	29	66	.4	4	3	117	2.75	5	7	ND	2	5	2	2	2	32	.04	.042	5	17	.20	16	.04	6	2.32	.01	.04	1	1
L87+00E 31+00N	1	9	19	30	.1	4	1	52	.84	2	5	ND	1	5	1	3	2	22	.08	.056	5	18	.12	8	.04	6	1.57	.01	.02	3	2
L87+00E 30+00N	1	11	26	42	.4	3	2	70	2.66	11	7	ND	3	5	1	4	2	39	.03	.027	7	13	.06	18	.08	9	3.26	.01	.03	3	3
STD C/AU-3	18	57	42	133	7.1	69	30	1075	4.17	40	21	7	38	47	18	17	18	59	.47	.091	39	57	.92	173	.08	35	2.02	.06	.17	13	53

SAMPLE	Mo	Cu	Pb	Zn	Ag	Mn	Co	Ni	Fe	As	U	Au	Hg	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Ng	Ba	Ti	B	Al	Na	K	V	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
L87+50E 97+00W	1	14	21	62	.1	11	7	411	3.77	13	5	ND	1	9	1	2	2	79	.08	.045	3	32	.28	27	.11	2	1.34	.01	.05	1	1
L87+50E 96+75W	2	16	18	61	.1	8	6	624	3.74	8	5	ND	1	6	1	2	4	66	.06	.059	4	17	.29	30	.09	9	1.82	.01	.05	1	1
L87+50E 96+50E	1	16	17	39	.1	6	3	96	2.76	6	5	ND	1	7	1	2	2	52	.04	.037	4	17	.07	20	.09	3	1.02	.01	.03	1	2
L87+50E 96+25W	1	9	38	52	.7	6	4	288	2.34	5	5	ND	1	9	2	2	2	49	.06	.055	3	18	.16	25	.06	6	1.23	.01	.04	1	1
L87+50E 96+00W	1	19	21	42	.1	6	10	897	3.87	5	5	ND	1	6	1	2	2	76	.10	.068	2	15	.22	19	.09	6	1.65	.01	.04	1	1
L87+50E 95+75W	1	19	24	32	.3	4	3	89	2.15	6	5	ND	1	6	1	2	2	44	.04	.023	4	16	.10	15	.10	4	1.76	.01	.02	2	1
L87+50E 95+00W	1	21	36	90	.3	11	18	2755	3.02	17	5	ND	1	8	1	2	2	46	.09	.119	5	20	.34	31	.03	9	1.75	.01	.07	1	1
L87+50E 94+75W	1	16	20	46	1.0	4	4	204	2.97	7	5	ND	1	5	1	3	3	40	.06	.056	4	11	.12	14	.06	7	2.27	.01	.02	2	1
L87+50E 94+50W	1	15	18	40	.2	4	3	145	1.56	15	5	ND	1	5	1	2	2	25	.04	.057	5	9	.07	12	.04	6	1.75	.01	.03	1	1
L87+50E 94+25W	2	21	31	112	.7	8	9	396	3.45	22	5	ND	1	10	1	4	2	51	.15	.052	14	20	.27	27	.08	9	2.76	.02	.05	1	1
L87+50E 93+75W	2	23	22	66	.2	6	4	322	2.49	8	5	ND	1	7	1	2	3	41	.08	.122	4	11	.26	16	.04	8	2.12	.01	.05	1	2
L87+50E 93+25W	1	7	64	26	.6	3	2	64	1.00	5	5	ND	1	7	1	2	2	30	.04	.038	6	11	.09	17	.05	8	1.19	.01	.04	1	1
L87+50E 93+00W	2	14	192	48	1.0	7	3	161	2.51	7	5	ND	2	8	2	2	2	55	.07	.038	7	19	.25	18	.10	9	2.84	.01	.04	1	1
L87+50E 93+00NA	1	12	29	35	.4	4	3	90	1.60	3	5	ND	1	5	1	2	2	27	.04	.034	6	15	.10	14	.08	8	2.38	.01	.02	1	1
L87+50E 92+75W	1	446	27491	1857	288.5	18	12	3236	8.41	1790	5	ND	1	11	5	691	2	56	.14	.094	6	32	.51	21	.04	6	2.07	.01	.09	3	775
L87+50E 92+25W	1	12	223	46	2.0	3	1	42	.58	19	5	ND	1	4	1	10	2	9	.03	.059	3	6	.03	9	.02	7	1.24	.01	.02	2	4
L87+50E 91+75W	1	13	32	63	.4	6	4	226	2.64	12	5	ND	2	9	3	2	2	68	.06	.020	7	19	.16	22	.12	8	2.15	.01	.03	1	1
L87+50E 91+50W	2	12	226	90	.2	5	7	3877	2.73	12	5	ND	2	12	1	3	2	69	.25	.039	3	6	.07	61	.16	6	1.23	.01	.03	1	1
L87+50E 91+25W	3	11	33	44	.5	2	2	137	2.46	5	5	ND	1	6	1	3	2	35	.06	.070	4	11	.10	17	.06	5	1.86	.01	.03	2	1
L87+50E 91+00W	3	9	22	67	.3	6	2	88	1.48	12	5	ND	3	9	1	3	2	84	.12	.027	4	11	.10	27	.07	9	.80	.01	.04	1	1
L87+50E 90+75W	3	10	28	62	.2	5	3	103	2.49	7	5	ND	1	10	2	2	2	44	.06	.028	4	13	.13	19	.06	9	1.04	.01	.04	2	1
L87+50E 90+50W	1	14	52	50	.6	5	3	94	2.85	11	5	ND	2	9	1	2	4	56	.07	.025	7	19	.17	21	.07	5	2.19	.01	.05	1	2
L88+00E 97+00W	2	27	117	149	.5	12	23	4379	4.59	19	5	ND	1	9	2	3	2	69	.12	.100	3	28	.35	75	.09	8	1.81	.01	.08	2	1
L88+00E 96+25W	1	9	19	55	.2	5	3	150	2.51	9	5	ND	1	6	1	2	2	45	.05	.027	4	11	.11	18	.07	7	1.10	.01	.04	1	1
L88+00E 95+75W	1	18	77	86	.8	5	5	483	4.19	18	5	ND	3	7	2	4	2	84	.06	.046	3	11	.17	38	.08	10	1.59	.01	.05	1	1
L88+00E 95+50W	3	22	43	86	.1	8	13	3015	3.22	10	5	ND	2	7	1	2	2	54	.08	.139	5	20	.32	35	.04	7	2.20	.01	.07	1	1
L88+00E 95+25W	2	15	37	104	.2	11	11	1164	2.39	15	5	ND	1	6	2	4	2	35	.06	.114	6	18	.23	23	.02	8	2.14	.01	.06	1	1
L88+00E 95+00W	1	34	660	604	8.3	13	15	4222	2.22	43	6	ND	3	26	11	10	2	31	.83	.230	11	18	.28	29	.01	13	2.54	.01	.11	1	1
L88+00E 94+75W	2	22	24	86	.4	10	20	1524	2.90	16	5	ND	1	9	2	2	2	51	.11	.113	5	18	.41	25	.04	11	1.84	.01	.08	1	6
L88+00E 94+25W	1	14	9	21	.6	1	1	28	.96	2	5	ND	1	3	2	2	2	8	.02	.058	3	6	.02	9	.01	13	1.30	.01	.03	1	1
L88+00E 94+00W	1	6	22	21	.1	2	2	51	.56	3	5	ND	1	6	1	2	2	16	.04	.041	2	8	.05	12	.02	6	.53	.01	.03	1	1
L88+00E 93+75W	1	7	14	24	.1	2	2	46	1.49	5	5	ND	1	8	1	2	2	44	.05	.022	5	9	.08	22	.06	4	1.10	.01	.03	1	1
L88+00E 93+50W	1	16	18	31	.3	4	2	77	1.73	5	5	ND	1	5	1	2	2	33	.03	.074	3	8	.07	19	.05	8	1.16	.01	.03	1	1
L88+00E 93+25W	1	13	29	62	.3	4	3	115	3.06	8	5	ND	2	8	1	2	2	62	.05	.021	4	14	.12	21	.12	7	1.23	.01	.03	1	1
L88+00E 93+00W	1	4	154	35	11.1	2	1	29	.67	67	5	ND	1	6	1	14	2	26	.03	.012	3	9	.05	14	.11	4	.65	.01	.02	2	28
L88+00E 92+75W	1	18	306	227	1.7	12	5	329	2.25	12	5	ND	1	11	2	2	2	36	.16	.075	9	26	.42	20	.04	3	2.81	.01	.06	1	1
STD C7XU-S	18	59	42	132	7.1	69	30	1086	4.14	41	19	8	37	47	17	17	22	59	.47	.086	40	60	.90	176	.07	35	2.01	.05	.17	13	51

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	V	Cr	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
L88-00E 32-50N	1	25	337	190	2.2	4	1	62	1.47	12	5	ND	1	4	3	3	2	25	.03	.040	5	12	.07	22	.07	2	2.33	.01	.01	1	3
L88-00E 32-25N	1	10	11	21	.4	3	1	38	1.47	2	5	ND	1	3	1	2	2	30	.02	.022	4	9	.03	10	.06	3	1.63	.01	.01	1	1
L88-00E 32-00N	1	6	16	24	.7	2	1	25	1.02	2	5	ND	1	3	1	2	2	18	.02	.031	4	6	.02	9	.06	6	1.21	.01	.01	2	2
L88-00E 31-75N	2	22	23	59	.6	9	4	606	5.10	21	5	ND	2	6	1	2	2	83	.08	.050	3	24	.36	25	.19	4	3.73	.01	.02	1	1
L88-00E 31-50N	1	8	17	37	.3	1	1	31	.63	3	5	ND	1	5	1	2	2	18	.04	.051	4	8	.06	14	.03	3	1.53	.01	.01	2	1
L88-00E 31-25N	2	12	26	50	.2	3	1	72	1.43	6	5	ND	1	7	1	2	2	27	.04	.116	7	15	.16	28	.01	2	2.55	.01	.03	4	1
L88-00E 30-75N	8	15	32	36	.6	8	3	276	4.09	24	5	ND	1	11	1	2	2	63	.08	.076	3	20	.21	28	.04	3	1.47	.01	.05	1	1
L88-00E 30-60N	1	12	26	37	.5	2	1	47	.83	4	5	ND	1	5	1	2	2	25	.04	.037	4	11	.05	16	.03	2	1.49	.01	.02	2	1
L88-00E 30-25N	2	14	30	100	.1	10	4	452	6.10	18	5	ND	1	9	1	2	2	80	.10	.027	5	29	.55	27	.11	3	2.32	.01	.03	1	1
L88-00E 30-00N	2	12	32	55	.2	6	2	119	1.97	4	5	ND	1	6	1	2	2	46	.05	.030	7	18	.21	24	.14	3	3.58	.01	.02	2	1
L88-00E 39-50N	2	34	358	379	.6	11	30	4638	4.76	104	5	ND	1	15	1	3	2	61	.16	.126	3	18	.62	106	.05	3	2.64	.01	.09	1	1
L88-00E 37-00N	1	29	26	423	.2	11	11	2912	1.51	79	5	ND	1	63	6	2	2	22	1.96	.261	10	14	.25	46	.01	7	2.13	.01	.06	1	1
L88-00E 36-75N	1	30	24	126	.2	29	11	995	2.81	14	5	ND	1	30	2	2	2	42	.68	.090	6	35	.60	58	.01	4	1.76	.01	.05	1	1
L88-00E 36-50N	2	14	20	60	.3	4	5	481	2.95	3	5	ND	1	6	2	2	4	46	.07	.055	2	11	.15	32	.07	4	1.22	.01	.03	1	2
L88-00E 36-25N	3	21	40	134	.1	10	14	3287	3.00	11	5	WC	1	11	2	2	2	45	.22	.125	5	16	.26	43	.03	5	2.01	.01	.04	1	1
L88-00E 36-00N	2	14	34	74	.2	8	6	725	1.26	8	5	ND	1	8	1	2	2	47	.07	.057	3	20	.23	25	.04	2	1.29	.01	.03	1	1
L88-00E 35-75N	2	22	25	63	.8	7	4	348	1.34	4	5	ND	1	5	1	2	2	23	.06	.115	8	11	.15	12	.01	3	2.07	.01	.02	1	1
L88-00E 35-50N	1	9	17	40	.6	7	2	127	1.57	4	5	ND	1	9	1	2	2	37	.08	.053	5	21	.22	22	.02	3	1.33	.01	.03	1	2
L88-00E 35-25N	2	15	22	58	.8	8	8	425	2.51	6	5	ND	1	7	3	2	2	37	.06	.076	7	18	.18	25	.02	5	1.93	.01	.03	1	1
L88-00E 35-00N	1	17	22	84	.3	10	12	1570	4.00	8	5	ND	1	9	1	2	2	52	.09	.059	4	26	.35	39	.04	2	1.68	.01	.04	1	1
L88-00E 34-75N	1	9	18	54	.1	7	3	199	1.51	3	5	ND	1	7	1	2	2	33	.07	.052	4	17	.25	19	.04	2	1.25	.01	.04	1	1
L88-00E 34-50N	1	11	11	29	.1	3	2	59	2.33	2	5	ND	1	6	1	2	3	39	.04	.028	3	8	.04	29	.08	2	1.13	.01	.01	2	1
L88-00E 34-25N	2	14	15	51	.1	9	5	445	3.11	6	5	ND	1	8	1	2	2	59	.05	.036	4	25	.24	33	.04	2	1.57	.01	.04	2	1
L88-00E 34-00N	2	14	23	59	.4	7	6	301	1.75	7	5	ND	1	7	1	2	2	38	.06	.075	5	18	.25	17	.03	6	1.61	.01	.04	1	1
L88-00E 34-00N	1	13	15	38	.2	7	3	184	2.14	6	5	ND	1	6	1	2	5	37	.04	.032	5	18	.22	17	.03	6	1.54	.01	.03	1	1
L88-00E 33-75N	1	20	5	32	.2	5	1	119	1.27	11	5	ND	1	6	1	2	2	29	.05	.062	3	8	.09	20	.02	4	1.20	.01	.02	1	1
L88-00E 33-50N	1	9	13	29	.1	4	2	75	1.67	6	5	ND	1	6	1	2	2	56	.04	.013	5	11	.07	16	.08	2	1.11	.01	.01	1	1
L88-00E 33-25N	1	23	37	93	.3	15	6	291	4.14	20	5	ND	1	10	2	2	2	59	.08	.028	6	32	.53	23	.05	4	2.11	.01	.03	1	1
L88-00E 33-00N	1	7	122	51	3.6	2	1	18	.33	40	5	ND	1	7	1	2	2	10	.06	.034	4	8	.04	18	.01	3	.90	.01	.02	1	3
L88-00E 32-50N	1	8	15	30	.2	4	2	57	.74	2	5	ND	1	5	1	2	2	13	.04	.062	6	10	.13	19	.01	2	1.35	.01	.02	1	1
L88-00E 32-25N	1	4	17	21	.1	2	2	39	.92	2	5	ND	1	4	1	2	2	28	.04	.028	4	8	.05	7	.07	3	1.10	.01	.01	1	1
L88-00E 32-00N	2	19	24	165	.5	11	8	1332	2.45	41	5	ND	1	25	2	2	2	37	.56	.131	8	28	.36	37	.01	2	2.04	.01	.04	1	1
L88-00E 36-75N	1	25	33	194	2.2	17	8	549	2.76	30	5	ND	1	20	3	2	2	40	.37	.108	8	40	.52	54	.01	4	2.33	.01	.05	1	1
L88-00E 35-50N	2	16	55	108	.6	8	17	1619	2.65	29	5	ND	1	9	3	2	4	45	.11	.078	5	20	.22	28	.03	3	1.63	.01	.05	1	1
L88-00E 36-00N	1	19	35	114	.5	12	9	1018	2.74	11	5	ND	1	12	2	2	2	40	.17	.102	6	22	.33	48	.01	2	1.80	.01	.06	1	2
L88-00E 35-75N	1	77	1439	268	.7	10	16	3468	2.82	43	5	ND	1	15	3	3	2	36	.32	.135	17	15	.27	26	.02	3	1.86	.01	.04	1	1
S ² D C/AG-S	17	57	41	132	7.1	68	28	1031	4.99	40	17	7	37	47	18	17	20	56	.47	.092	38	55	.93	171	.06	32	2.00	.06	.14	12	50

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Mn	Co	Ni	Fe	As	U	Au	Th	Sr	Ca	Sb	Bi	V	Cr	P	La	Ce	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
L89+00E 55+50N	1	17	17	52	.2	7	6	271	3.51	4	5	ND	1	6	2	2	49	.05	.057	6	14	.19	22	.06	2	2.28	.01	.03	2	1	
L89+00E 55+00N	2	61	23	87	.4	11	5	222	3.75	6	5	ND	1	8	2	3	70	.06	.054	5	16	.13	49	.08	3	1.63	.01	.03	2	1	
L89+00E 94+75W	1	18	17	111	.6	17	12	473	2.47	8	5	ND	1	10	1	2	34	.13	.099	9	30	.39	25	.02	4	3.32	.01	.04	2	1	
L89+00E 54+50W	1	15	21	55	.1	10	4	220	2.51	8	5	ND	1	9	1	2	38	.08	.055	6	24	.31	20	.04	2	1.78	.01	.05	1	2	
L89+00E 54+25W	1	25	14	47	1.1	5	3	160	1.72	7	5	ND	1	6	2	2	28	.05	.094	7	17	.19	13	.02	2	2.88	.01	.03	3	1	
L89+00E 54+00N	1	24	12	39	.3	3	5	321	3.35	6	5	ND	1	6	1	2	3	53	.06	.074	4	9	.07	17	.07	3	1.56	.01	.02	2	1
L89+00E 97+75W	1	15	11	43	.7	5	4	150	1.43	8	5	ND	1	7	2	2	28	.05	.077	7	10	.12	15	.02	5	1.89	.01	.04	2	1	
L89+00E 92+50W	1	23	20	52	.3	7	12	855	2.85	17	5	ND	1	9	2	2	3	57	.10	.084	5	18	.29	21	.07	4	1.69	.01	.04	3	1
L89+00E 92+25W	1	14	19	41	.1	7	4	143	3.58	19	5	ND	1	10	1	2	2	87	.09	.029	5	24	.15	23	.09	2	1.44	.01	.03	2	1
L89+00E 92+00W	1	14	18	37	.4	4	3	193	3.39	7	5	ND	1	7	1	2	2	48	.06	.035	5	13	.09	18	.05	2	1.52	.01	.03	1	2
L89+00E 92+75W	1	5	23	27	.6	3	1	59	.72	7	5	ND	1	7	1	2	2	22	.05	.027	5	10	.08	17	.05	2	.84	.01	.04	1	1
L89+00E 92+50W	1	16	27	50	.2	7	11	706	3.57	15	6	ND	1	7	2	2	3	66	.07	.045	4	20	.24	18	.13	5	1.65	.01	.05	2	1
L89+00E 92+25W	1	7	27	33	.1	5	2	91	1.39	6	5	ND	1	10	1	2	2	37	.08	.030	7	15	.19	17	.05	2	1.30	.01	.04	1	2
L89+00E 91+00W	1	7	14	28	.2	4	1	42	.54	3	5	ND	1	9	1	2	2	16	.07	.079	4	11	.10	16	.04	5	1.03	.01	.04	1	1
L89+00E 91+75W	1	15	14	35	.5	6	2	67	1.16	3	6	ND	1	7	1	2	2	30	.06	.091	5	17	.20	14	.03	3	1.90	.01	.04	3	1
L89+00E 91+25W	1	12	27	29	.2	3	1	73	2.31	13	5	ND	1	6	1	2	2	52	.06	.048	5	15	.09	16	.06	2	1.97	.01	.02	2	1
L89+00E 91+00W	1	6	16	34	.1	4	2	71	1.57	3	5	ND	1	6	1	2	2	43	.04	.024	3	8	.05	13	.09	2	.66	.01	.02	1	1
L89+00E 90+75W	3	23	36	128	.2	12	5	287	1.90	20	5	ND	2	3	1	2	2	67	.08	.046	6	25	.33	23	.13	2	2.88	.01	.04	2	1
L89+00E 90+25W	3	32	50	250	.5	11	33	2532	3.78	36	5	ND	1	43	3	3	2	58	.35	.128	10	13	.41	89	.08	5	3.51	.01	.09	1	1
L89+00E 90+25NA	1	22	37	55	.3	5	7	755	1.45	4	5	ND	1	12	1	2	2	30	.19	.061	7	13	.14	27	.02	6	1.57	.01	.04	1	1
L89+00E 90+00N	1	25	112	191	.8	10	11	758	3.36	79	5	ND	1	23	2	2	3	58	.23	.076	6	15	.28	53	.09	2	2.26	.01	.05	1	1
L89+00E 95+25W	3	29	292	220	1.3	13	23	4011	5.38	41	5	ND	1	13	1	2	2	91	.13	.098	4	28	.44	62	.13	2	2.10	.01	.07	1	2
L89+00E 99+00W	1	24	158	236	1.4	9	6	943	3.58	51	5	ND	1	30	2	2	2	66	.44	.079	4	14	.40	63	.14	4	2.49	.01	.10	1	1
L89+00E 93+75W	4	29	127	350	1.2	10	11	703	4.48	33	5	ND	1	16	1	2	2	64	.17	.078	4	18	.46	43	.13	2	4.41	.01	.06	1	1
L89+00E 98+50W	2	23	133	291	.7	8	9	866	2.96	50	5	ND	1	21	2	2	2	65	.26	.082	3	15	.37	57	.12	2	2.99	.01	.06	1	1
L89+00E 87+50W	1	21	55	72	.7	6	2	247	1.39	21	5	ND	1	9	1	2	2	49	.17	.051	4	12	.20	22	.15	2	2.00	.01	.04	1	1
L89+00E 87+25W	1	18	56	75	.5	7	3	263	4.52	18	5	ND	2	7	1	2	3	99	.09	.039	4	18	.27	23	.22	4	2.44	.01	.04	1	1
L89+00E 87+00W	1	15	57	115	.2	9	6	631	5.99	17	5	ND	1	8	1	2	2	79	.10	.049	4	26	.37	30	.12	4	2.32	.01	.06	2	1
L89+00E 86+75W	2	39	54	161	1.2	10	59	1030	3.42	11	5	ND	1	18	3	2	2	56	.29	.068	11	22	.28	22	.09	5	2.22	.01	.04	1	1
L89+00E 86+25W	13	19	13	225	.3	18	101	22027	3.64	6	6	ND	1	90	19	2	2	14	2.16	.106	7	9	.04	94	.01	14	1.29	.01	.03	7	1
L89+00E 86+00W	1	15	21	66	.6	4	3	299	.30	3	5	ND	1	81	1	2	2	4	1.90	.082	3	3	.04	29	.01	7	.43	.01	.07	1	1
L89+00E 97+00W	1	16	28	77	.4	8	5	406	3.17	10	5	ND	1	12	1	2	2	61	.12	.038	6	25	.25	28	.03	2	1.85	.01	.04	1	2
L89+00E 96+75W	1	24	100	150	1.2	10	12	1873	2.51	25	5	ND	1	11	2	2	2	40	.14	.108	6	23	.34	25	.01	2	2.08	.01	.06	1	2
L89+00E 96+50W	2	26	35	140	1.0	14	12	681	4.04	13	5	ND	1	14	3	2	3	64	.16	.051	6	32	.47	29	.05	2	1.94	.01	.04	1	1
L89+00E 95+75W	1	17	22	57	.2	5	8	1595	4.00	3	5	ND	1	6	1	2	2	60	.23	.074	3	15	.44	38	.07	2	2.10	.01	.07	1	1
STD C/AU-S	17	58	29	132	7.1	67	26	1059	4.07	40	22	7	36	45	17	18	20	55	.47	.388	39	55	.92	164	.07	31	1.98	.06	.13	11	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	D PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	S PPM	Al %	Na %	K %	W PPM	As ² PPM
L89+50E 95+50N	1	25	26	73	.5	12	5	254	3.70	13	5	ND	1	10	1	2	2	60	.07	.043	5	29	.35	42	.01	2	1.65	.01	.04	1	1
L89+50E 95+25N	1	26	21	108	.1	16	7	583	3.58	14	5	ND	1	24	1	2	2	53	.41	.060	4	34	.58	76	.01	2	1.54	.01	.07	1	1
L89+50E 95+00N	2	20	19	144	.1	7	17	4314	4.10	20	5	ND	1	13	1	2	2	59	.22	.102	4	12	.27	51	.06	2	2.15	.01	.05	1	1
L89+50E 94+50N	2	12	16	47	.1	5	3	184	5.36	8	5	ND	2	5	1	2	2	141	.03	.028	3	19	.12	19	.18	2	1.36	.01	.03	1	3
L89+50E 94+00N	1	14	16	45	.1	16	6	321	3.28	10	5	ND	1	8	1	2	3	58	.06	.029	3	29	.37	19	.07	2	1.01	.01	.04	1	1
L89+50E 93+75N	1	12	16	34	.1	12	4	160	2.39	12	5	ND	1	11	1	2	3	63	.13	.031	4	42	.31	13	.08	2	.89	.01	.03	1	1
L89+50E 93+50N	1	13	8	24	.5	3	1	42	.42	3	5	ND	1	3	1	2	2	7	.03	.104	4	6	.06	7	.01	3	1.83	.01	.03	1	1
L89+50E 93+00N	2	12	166	43	2.0	3	3	162	1.86	17	5	ND	1	4	1	2	2	26	.06	.082	4	12	.12	10	.02	3	2.53	.01	.03	1	1
L89+50E 92+75N	1	26	47	72	.9	7	4	141	4.70	39	6	ND	2	6	1	2	3	63	.05	.047	3	22	.24	18	.10	2	4.90	.01	.02	1	1
L89+50E 92+50N	1	14	16	28	1.0	3	2	86	1.25	5	5	ND	1	6	1	2	2	25	.05	.035	4	7	.10	17	.01	2	1.48	.01	.03	1	1
L89+50E 92+25N	1	13	34	46	.3	6	3	124	1.91	10	5	ND	1	7	1	2	2	38	.05	.029	5	17	.15	15	.06	2	1.61	.01	.02	1	1
L89+50E 92+00N	1	20	14	31	1.7	3	2	19	.69	2	5	ND	1	7	1	2	2	8	.03	.101	3	5	.03	17	.01	3	1.47	.01	.03	1	1
L89+50E 91+75N	1	5	18	22	.3	3	1	63	.79	3	5	ND	1	6	1	2	3	24	.05	.040	3	8	.07	14	.05	3	.82	.01	.03	1	1
L90+00E 94+00N	1	24	109	282	.2	11	11	3302	2.24	31	5	ND	1	27	5	2	2	35	.58	.106	10	20	.29	51	.01	2	1.97	.01	.04	1	2
L90+00E 94+75N	1	19	24	56	.4	8	17	2189	3.63	42	6	ND	1	12	2	2	2	44	.19	.060	7	18	.22	30	.02	5	1.80	.01	.04	1	1
L90+00E 94+25N	1	18	18	43	.2	5	4	247	4.09	3	7	ND	1	7	1	2	2	61	.12	.055	3	13	.18	34	.05	2	1.52	.01	.03	1	1
L90+00E 94+00N	1	19	14	45	.7	5	3	85	1.81	5	5	ND	1	8	1	2	2	18	.06	.106	4	9	.07	20	.01	3	1.98	.01	.03	1	1
L90+00E 93+75N	1	42	23	35	1.0	10	5	158	1.31	4	5	ND	1	8	1	2	2	29	.06	.056	6	11	.10	33	.02	2	1.42	.01	.03	1	1
L90+00E 93+50N	2	28	35	42	1.5	6	2	109	1.88	35	5	ND	1	8	1	2	2	14	.08	.173	4	11	.10	22	.01	3	1.80	.01	.05	1	1
L90+00E 93+00N	1	14	30	40	1.0	3	2	183	1.75	19	5	ND	1	10	1	3	2	47	.07	.038	2	5	.09	17	.04	2	.75	.01	.03	1	1
L90+00E 92+75N	2	23	1003	77	5.2	4	2	123	1.85	17	5	ND	1	6	3	3	2	36	.07	.076	5	7	.12	13	.02	3	1.70	.01	.03	1	2
L90+00E 92+50N	1	19	46	54	2.8	6	4	200	1.81	13	5	ND	1	5	2	2	2	23	.04	.091	4	11	.16	12	.01	4	1.70	.01	.04	1	2
L90+00E 92+25N	1	21	21	46	.7	5	16	365	.94	4	5	ND	1	7	1	2	2	14	.09	.083	6	7	.11	13	.01	7	1.68	.01	.05	1	1
L90+00E 91+75N	1	22	12	38	.6	4	2	138	1.13	6	5	ND	1	11	1	2	2	28	.07	.108	4	8	.12	29	.03	5	1.45	.01	.03	1	1
L90+00E 91+00N	1	7	17	20	.4	3	1	33	.56	2	5	ND	1	4	1	2	2	15	.04	.038	3	6	.05	12	.03	2	.88	.01	.02	1	2
L90+50E 93+50N	1	47	1238	361	7.3	9	7	1245	9.72	590	9	ND	1	7	1	19	2	85	.11	.068	4	48	.62	18	.03	2	2.89	.01	.03	2	1
L90+50E 92+25N	2	19	25	33	.4	8	5	133	2.22	18	5	ND	1	12	1	2	2	37	.07	.058	5	8	.18	29	.03	2	1.65	.01	.03	2	2
L90+50E 92+00N	1	18	32	51	.8	7	3	115	2.35	16	5	ND	1	8	1	2	3	31	.07	.063	3	16	.17	17	.01	2	1.30	.01	.04	1	2
L90+50E 91+75N	2	22	23	44	1.1	5	4	116	1.16	6	5	ND	1	7	2	2	2	18	.07	.110	7	9	.13	12	.01	4	2.15	.01	.04	1	1
L90+50E 91+25N	1	20	15	34	.5	4	3	64	1.44	3	5	ND	1	5	1	2	4	42	.04	.030	4	7	.04	16	.05	10	.89	.01	.03	1	1
L86+50E 8197N	1	15	16	34	.5	5	2	83	2.30	5	5	ND	1	6	1	2	2	35	.06	.059	7	21	.19	18	.04	4	3.16	.01	.03	2	1
L86+50E 8163N	1	25	27	114	.2	14	7	561	4.23	19	5	ND	1	8	1	2	2	59	.10	.074	7	28	.60	22	.06	2	3.07	.01	.04	1	2
L87+01E 8157N	2	10	17	36	.5	5	2	76	2.69	4	5	ND	1	7	1	2	2	40	.06	.055	5	20	.11	18	.06	3	1.53	.01	.03	1	1
L87+00E 8192N	1	12	20	37	.5	4	2	117	1.58	3	5	ND	1	7	1	2	3	33	.06	.060	6	13	.19	13	.04	11	1.87	.01	.02	2	1
STD C/AG-5	18	58	42	132	7.1	67	28	1059	4.06	41	21	6	37	45	18	16	19	55	.48	.085	38	53	.94	164	.06	33	1.98	.06	.12	11	51

HARRISBURG DAYTON RES. CORP. PROJECT B8804 FILE # 88-2917

SAMPLE#	No	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Hg	Ba	Ti	B	Al	Na	I	W	Am*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
88-DR-13	5	33	542	311	4.1	7	20	26775	11.79	187	5	ND	2	4	1	2	2	49	.12	.055	3	4	.79	24	.01	2	1.98	.01	.20	1	29
88-DR-14	1	45	63	229	.6	2	2	298	16.07	220	5	ND	1	3	1	11	2	33	.09	.018	2	4	.06	7	.04	2	.43	.03	.07	6	30
88-DR-15	1	25	21	68	.2	3	2	950	14.34	15	5	ND	3	41	1	2	2	57	.69	.042	2	6	.41	5	.18	2	1.40	.01	.03	2	1

APPENDIX II

Histograms for Gold, Silver, Copper
Lead, zinc and Cadmium

Histogram for Cu_ppm

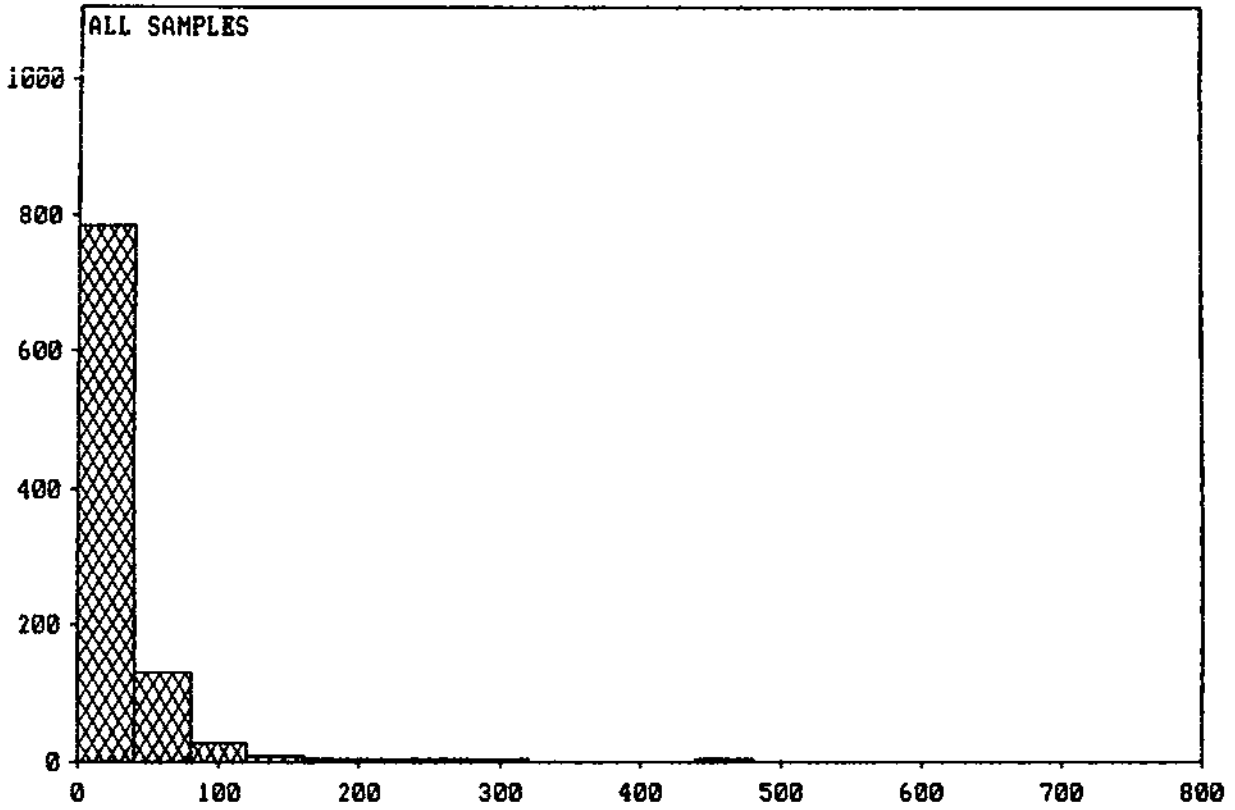
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	40	783	81	783	81	Mean
40	80	130	13	913	95	
80	120	26	3	939	97	
120	160	6	1	945	98	
160	200	3	0	948	98	
200	240	4	0	952	99	
240	280	2	0	954	99	
280	320	5	1	959	99	
320	360	1	0	960	99	
360	400	0	0	960	99	
400	440	1	0	961	99	
440	480	2	0	963	100	
480	520	0	0	963	100	
520	560	1	0	964	100	
560	600	1	0	965	100	
600	640	0	0	965	100	
640	680	0	0	965	100	
680	720	1	0	966	100	
720	760	0	0	966	100	
760	800	0	0	966	100	

Data elements inside histogram 966
 Data elements outside histogram 0

Descriptive Statistics

Mean 33.27226
 Variance 2788.352
 Standard Deviation 52.80484
 Skewness 6.924889

Histogram for Cu_ppm



Mean = 33.272 Variance = 2788
Standard Deviation = 52.8 Skewness = 6.925

Histogram for Cu_ppm *** DATA OUTSIDE RANGE ***

Lower limit	Upper limit	Frequency	%	Cumulative	%
0	10	113	12	113	12
10	20	304	31	417	43
20	30	241	25	658	68
30	40	125	13	783	81
40	50	66	7	849	88
50	60	33	3	882	91
60	70	16	2	898	93
70	80	15	2	913	95
80	90	14	1	927	96
90	100	6	1	933	97
100	110	5	1	938	97
110	120	1	0	939	97
120	130	1	0	940	97
130	140	0	0	940	97
140	150	0	0	940	97
150	160	5	1	945	98
160	170	3	0	948	98
170	180	0	0	948	98
180	190	0	0	948	98
190	200	1	0	949	98

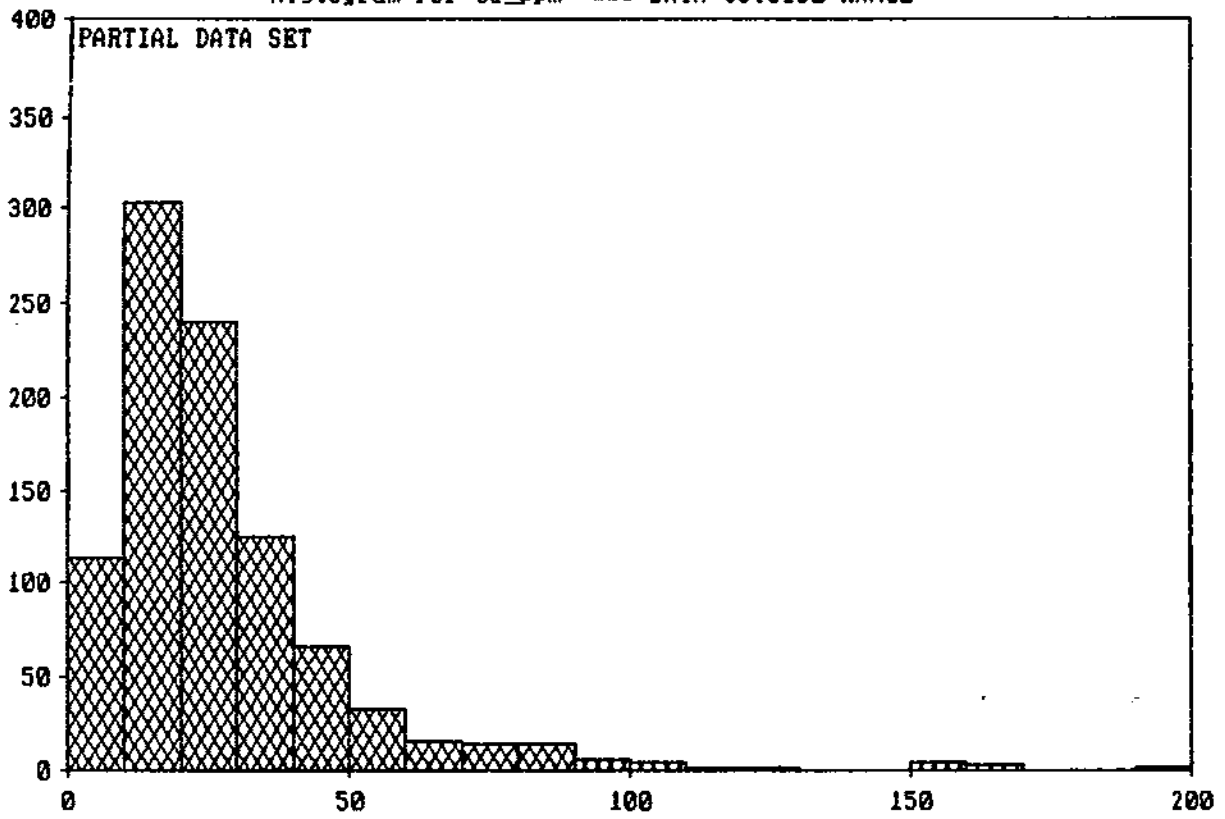
Mean

Data elements inside histogram 949
 Data elements outside histogram 17

Descriptive Statistics

Mean 33.27226
 Variance 2788.352
 Standard Deviation 52.80484
 Skewness 6.924889

Histogram for Cu_ppm *** DATA OUTSIDE RANGE ***



Mean = 33.272 Variance = 2788
Standard Deviation = 52.8 Skewness = 6.925

Histogram for Pb_ppm

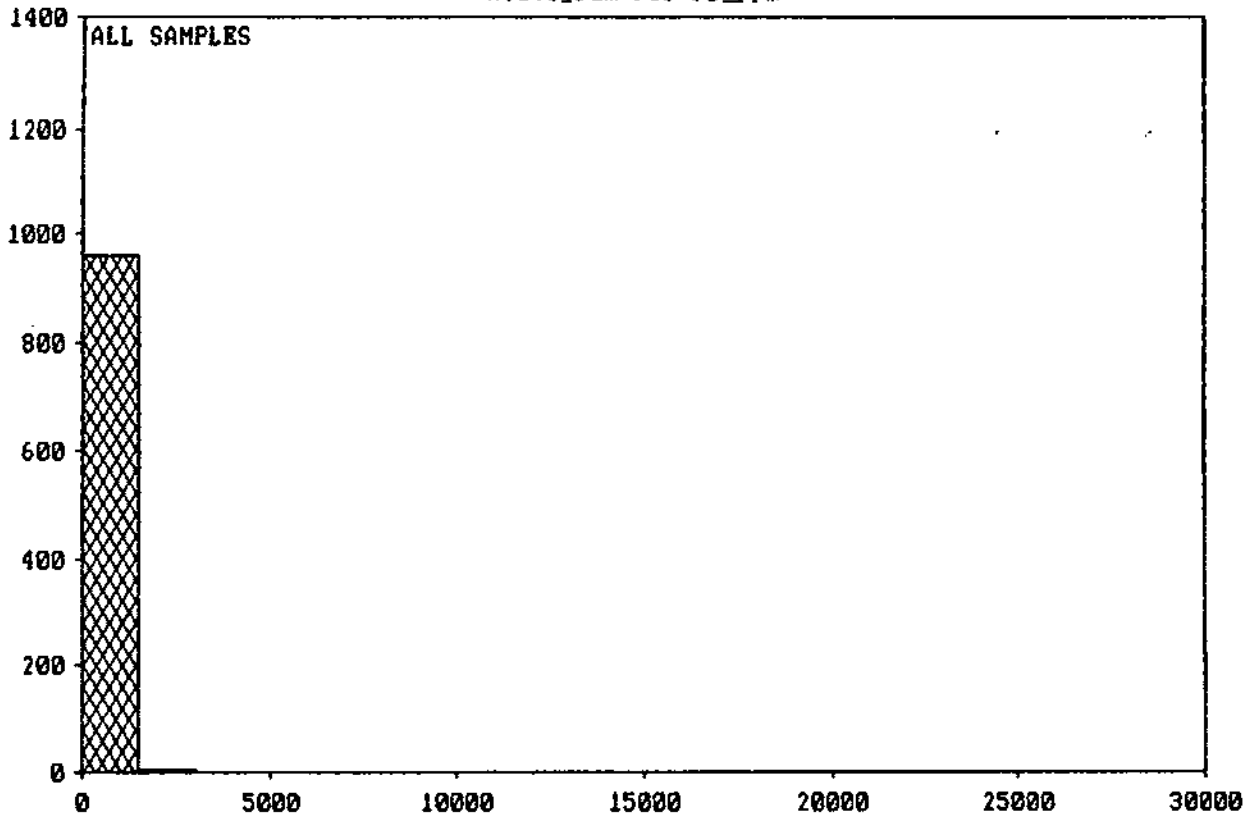
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	1500	960	99	960	99	Mean
1500	3000	4	0	964	100	
3000	4500	1	0	965	100	
4500	6000	0	0	965	100	
6000	7500	0	0	965	100	
7500	9000	0	0	965	100	
9000	10500	0	0	965	100	
10500	12000	0	0	965	100	
12000	13500	0	0	965	100	
13500	15000	0	0	965	100	
15000	16500	0	0	965	100	
16500	18000	0	0	965	100	
18000	19500	0	0	965	100	
19500	21000	0	0	965	100	
21000	22500	0	0	965	100	
22500	24000	0	0	965	100	
24000	25500	0	0	965	100	
25500	27000	0	0	965	100	
27000	28500	1	0	966	100	
28500	30000	0	0	966	100	

Data elements inside histogram 966
 Data elements outside histogram 0

Descriptive Statistics

Mean 109.2039
 Variance 817682.8
 Standard Deviation 904.2581
 Skewness 28.88395

Histogram for Pb_ppm



Mean = 109.2 Variance = 817700
Standard Deviation = 904.3 Skewness = 28.88

Histogram for Pb_ppm *** DATA OUTSIDE RANGE ***

Lower limit	Upper limit	Frequency	%	Cumulative	%
0	20	238	25	238	25
20	40	306	32	544	56
40	60	131	14	675	70
60	80	74	8	749	78
80	100	50	5	799	83
100	120	39	4	838	87
120	140	24	2	862	89
140	160	15	2	877	91
160	180	11	1	888	92
180	200	12	1	900	93
200	220	5	1	905	94
220	240	11	1	916	95
240	260	7	1	923	96
260	280	3	0	926	96
280	300	3	0	929	96
300	320	1	0	930	96
320	340	3	0	933	97
340	360	2	0	935	97
360	380	2	0	937	97
380	400	1	0	938	97

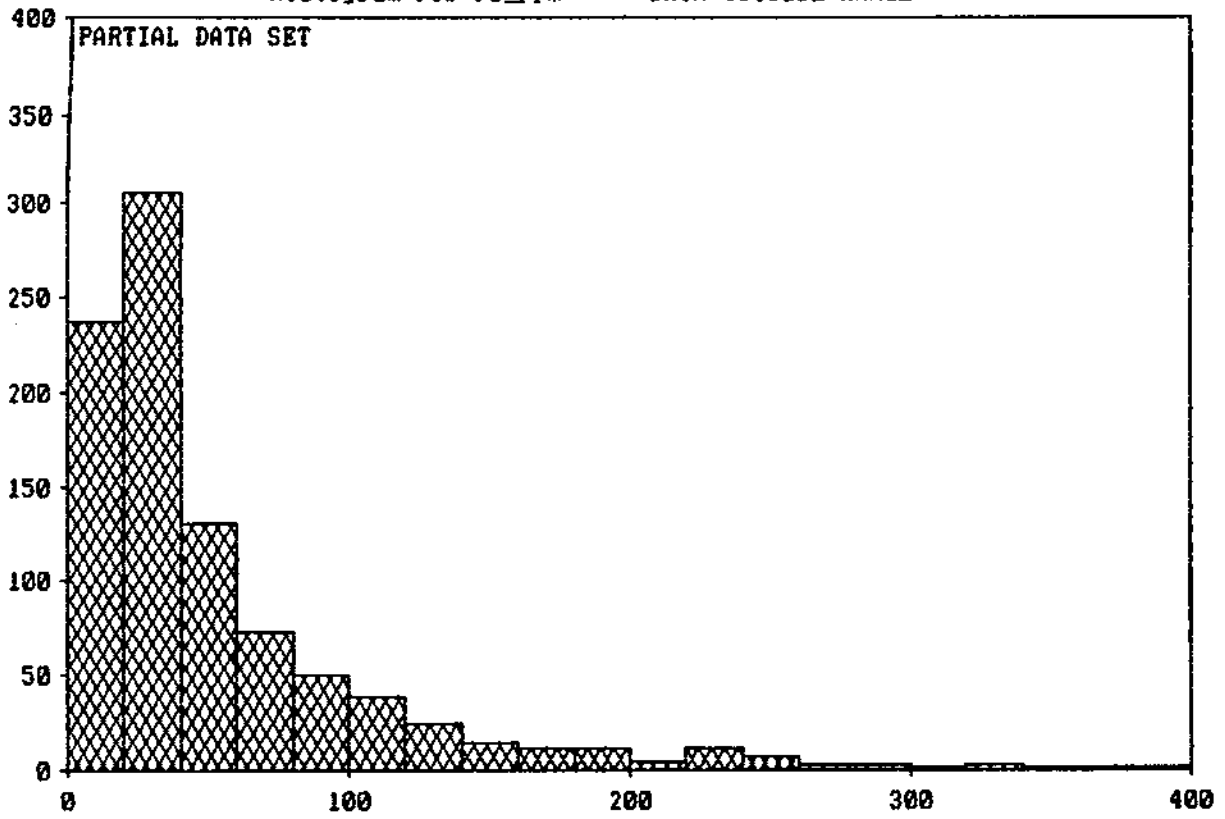
Mean

Data elements inside histogram 938
 Data elements outside histogram 28

Descriptive Statistics

Mean 109.2039
 Variance 817682.8
 Standard Deviation 904.2581
 Skewness 28.88395

Histogram for Pb_ppm *** DATA OUTSIDE RANGE ***



Mean = 109.2 Variance = 817700
Standard Deviation = 904.3 Skewness = 28.88

Histogram for Zn_ppm

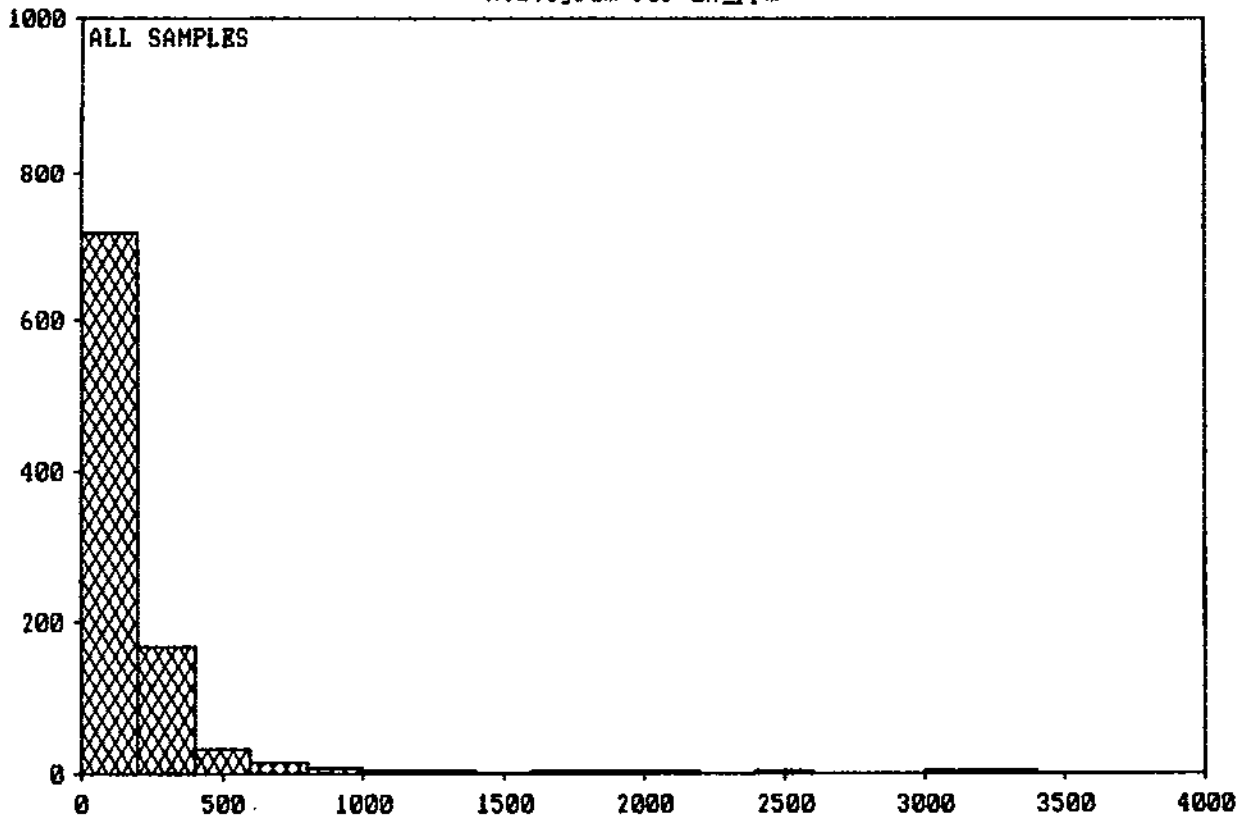
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	200	716	74	716	74	Mean
200	400	170	18	886	92	
400	600	31	3	917	95	
600	800	15	2	932	96	
800	1000	8	1	940	97	
1000	1200	5	1	945	98	
1200	1400	4	0	949	98	
1400	1600	1	0	950	98	
1600	1800	2	0	952	99	
1800	2000	4	0	956	99	
2000	2200	3	0	959	99	
2200	2400	0	0	959	99	
2400	2600	3	0	962	100	
2600	2800	0	0	962	100	
2800	3000	0	0	962	100	
3000	3200	2	0	964	100	
3200	3400	2	0	966	100	
3400	3600	0	0	966	100	
3600	3800	0	0	966	100	
3800	4000	0	0	966	100	

Data elements inside histogram 966
 Data elements outside histogram 0

Descriptive Statistics

Mean 195.7143
 Variance 114945.7
 Standard Deviation 339.0364
 Skewness 5.466342

Histogram for Zn_ppm



Mean = 195.71 Variance = 114900
Standard Deviation = 339 Skewness = 5.466

Histogram for Zn_ppm *** DATA OUTSIDE RANGE ***

Lower limit	Upper limit	Frequency	%	Cumulative	%
0	50	216	22	216	22
50	100	258	27	474	49
100	150	155	16	629	65
150	200	87	9	716	74
200	250	61	6	777	80
250	300	47	5	824	85
300	350	37	4	861	89
350	400	25	3	886	92
400	450	14	1	900	93
450	500	6	1	906	94
500	550	2	0	908	94
550	600	9	1	917	95
600	650	5	1	922	95
650	700	2	0	924	96
700	750	3	0	927	96
750	800	5	1	932	96
800	850	1	0	933	97
850	900	3	0	936	97
900	950	3	0	939	97
950	1000	1	0	940	97

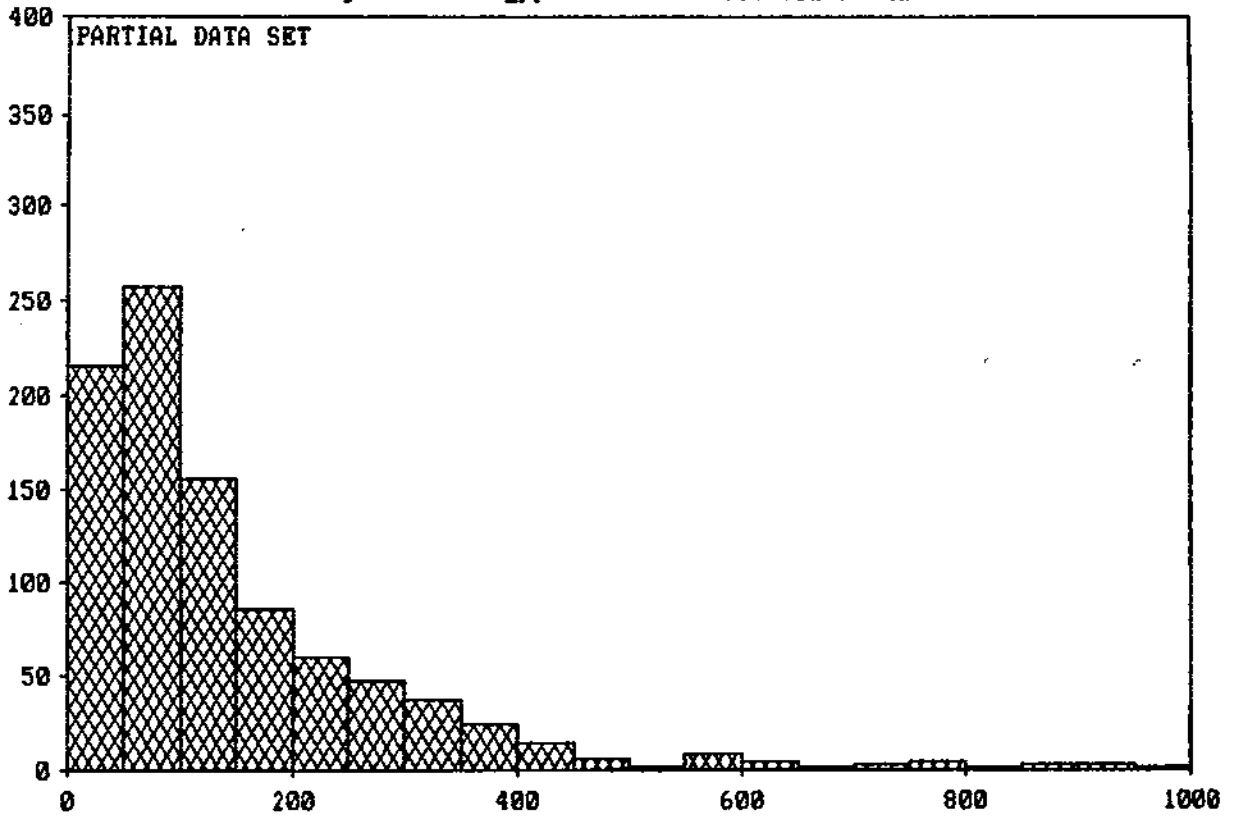
Mean

Data elements inside histogram 940
 Data elements outside histogram 26

Descriptive Statistics

Mean 195.7143
 Variance 114945.7
 Standard Deviation 339.0364
 Skewness 5.466342

Histogram for Zn_ppm *** DATA OUTSIDE RANGE ***



Mean = 195.71 Variance = 114900
Standard Deviation = 339 Skewness = 5.466

Histogram for Ag_ppm

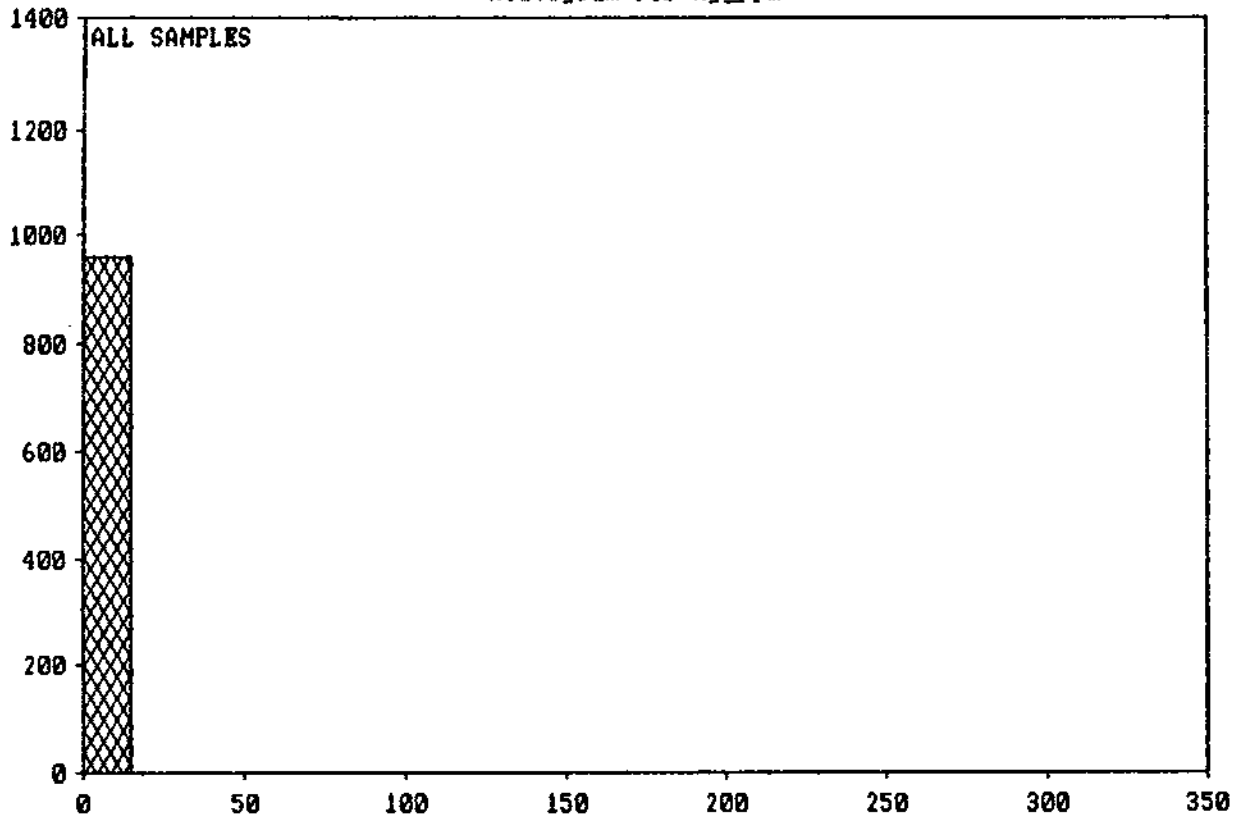
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	15	961	99	961	99	Mean
15	30	2	0	963	100	
30	45	0	0	963	100	
45	60	1	0	964	100	
60	75	1	0	965	100	
75	90	0	0	965	100	
90	105	0	0	965	100	
105	120	0	0	965	100	
120	135	0	0	965	100	
135	150	0	0	965	100	
150	165	0	0	965	100	
165	180	0	0	965	100	
180	195	0	0	965	100	
195	210	0	0	965	100	
210	225	0	0	965	100	
225	240	0	0	965	100	
240	255	0	0	965	100	
255	270	0	0	965	100	
270	285	0	0	965	100	
285	300	1	0	966	100	

Data elements inside histogram 966
 Data elements outside histogram 0

Descriptive Statistics

Mean 1.496167
 Variance 95.36863
 Standard Deviation 9.765686
 Skewness 26.75869

Histogram for Ag_ppm



Mean = 1.4962 Variance = 95.37
Standard Deviation = 9.766 Skewness = 26.76

Histogram for Ag_ppm *** DATA OUTSIDE RANGE ***

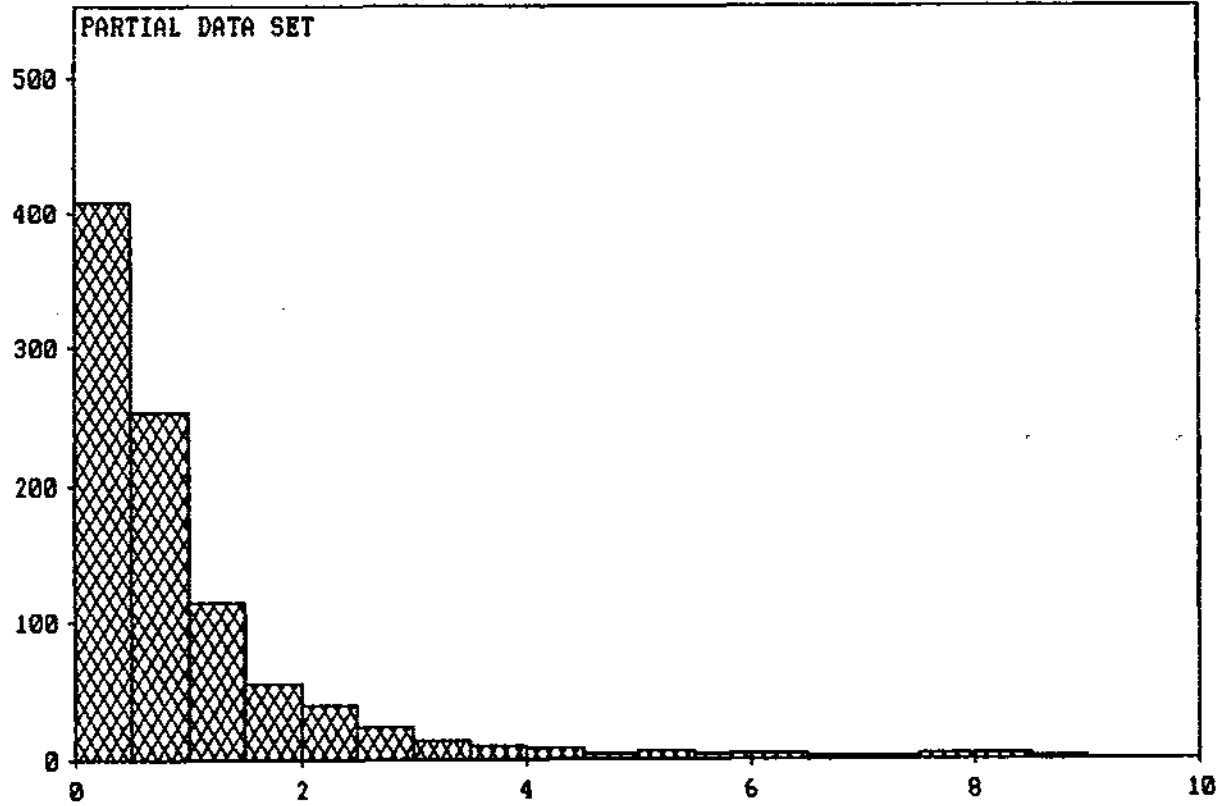
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	0.5	408	42	408	42	
0.5	1	254	26	662	69	
1	1.5	115	12	777	80	Mean
1.5	2	56	6	833	86	
2	2.5	39	4	872	90	
2.5	3	24	2	896	93	
3	3.5	14	1	910	94	
3.5	4	9	1	919	95	
4	4.5	8	1	927	96	
4.5	5	4	0	931	96	
5	5.5	5	1	936	97	
5.5	6	4	0	940	97	
6	6.5	3	0	943	98	
6.5	7	2	0	945	98	
7	7.5	2	0	947	98	
7.5	8	4	0	951	98	
8	8.5	4	0	955	99	
8.5	9	1	0	956	99	
9	9.5	0	0	956	99	
9.5	10	0	0	956	99	

Data elements inside histogram 956
 Data elements outside histogram 10

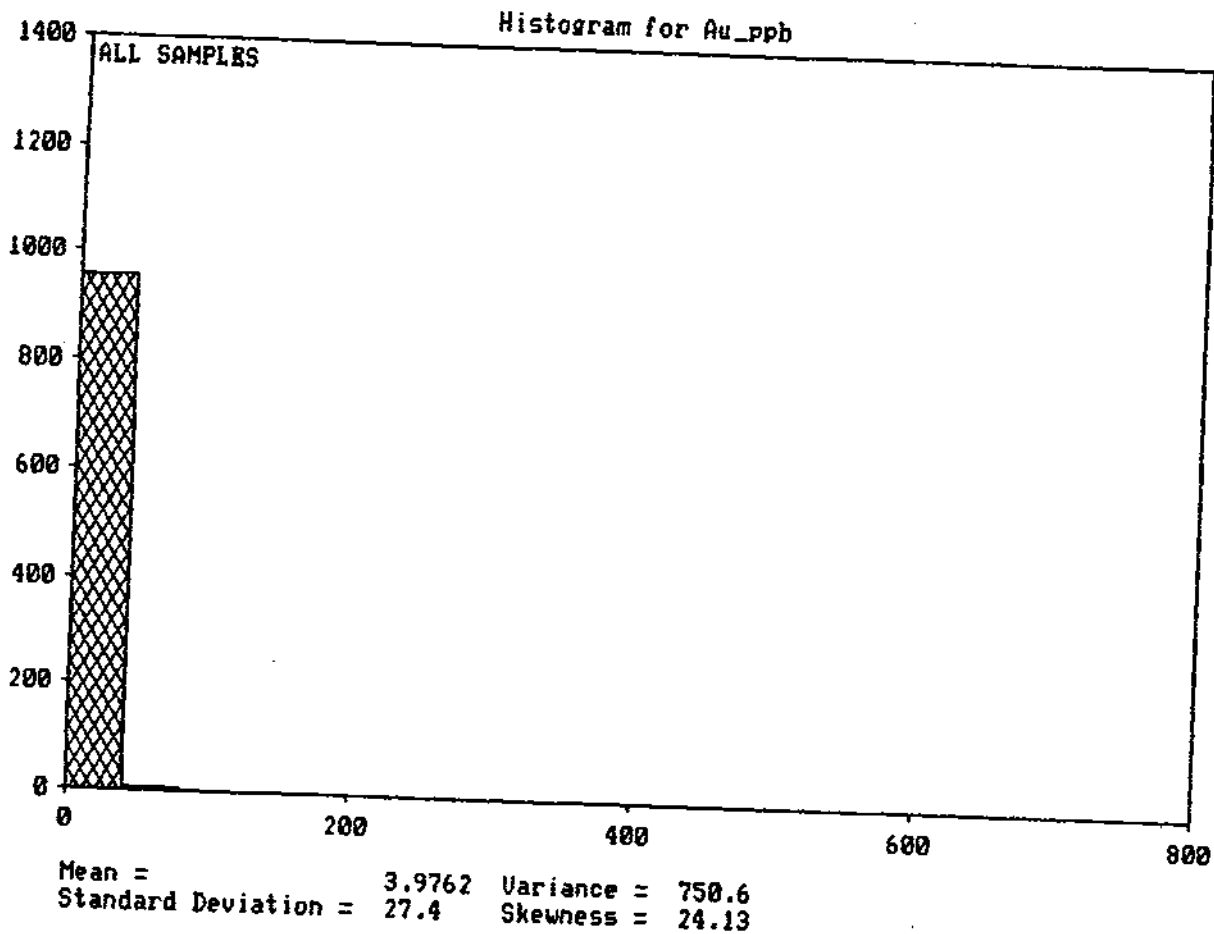
Descriptive Statistics

Mean 1.496167
 Variance 95.36863
 Standard Deviation 9.765686
 Skewness 26.75869

Histogram for Ag_ppm *** DATA OUTSIDE RANGE ***



Mean = 1.4962 Variance = 95.37
Standard Deviation = 9.766 Skewness = 26.76



Routine: FREHIST File: D:HAALL.TXT Date: 09-27-1988
 Comment: ALL SAMPLES

Histogram for Au_ppb

Lower limit	Upper limit	Frequency	%	Cumulative	%	Mean
0	40	955	99	955	99	
40	80	7	1	962	100	
80	120	1	0	963	100	
120	160	1	0	964	100	
160	200	0	0	964	100	
200	240	0	0	964	100	
240	280	1	0	965	100	
280	320	0	0	965	100	
320	360	0	0	965	100	
360	400	0	0	965	100	
400	440	0	0	965	100	
440	480	0	0	965	100	
480	520	0	0	965	100	
520	560	0	0	965	100	
560	600	0	0	965	100	
600	640	0	0	965	100	
640	680	0	0	965	100	
680	720	0	0	965	100	
720	760	1	0	966	100	

Histogram for Au_ppb *** DATA OUTSIDE RANGE ***

Lower limit	Upper limit	Frequency	%	Cumulative	%
0	1	0	0	0	0
1	2	679	70	679	70
2	3	129	13	808	84
3	4	49	5	857	89
4	5	23	2	880	91
5	6	15	2	895	93
6	7	6	1	901	93
7	8	4	0	905	94
8	9	8	1	913	95
9	10	3	0	916	95
10	11	6	1	922	95
11	12	1	0	923	96
12	13	3	0	926	96
13	14	5	1	931	96
14	15	3	0	934	97
15	16	1	0	935	97
16	17	3	0	938	97
17	18	0	0	938	97
18	19	1	0	939	97
19	20	1	0	940	97

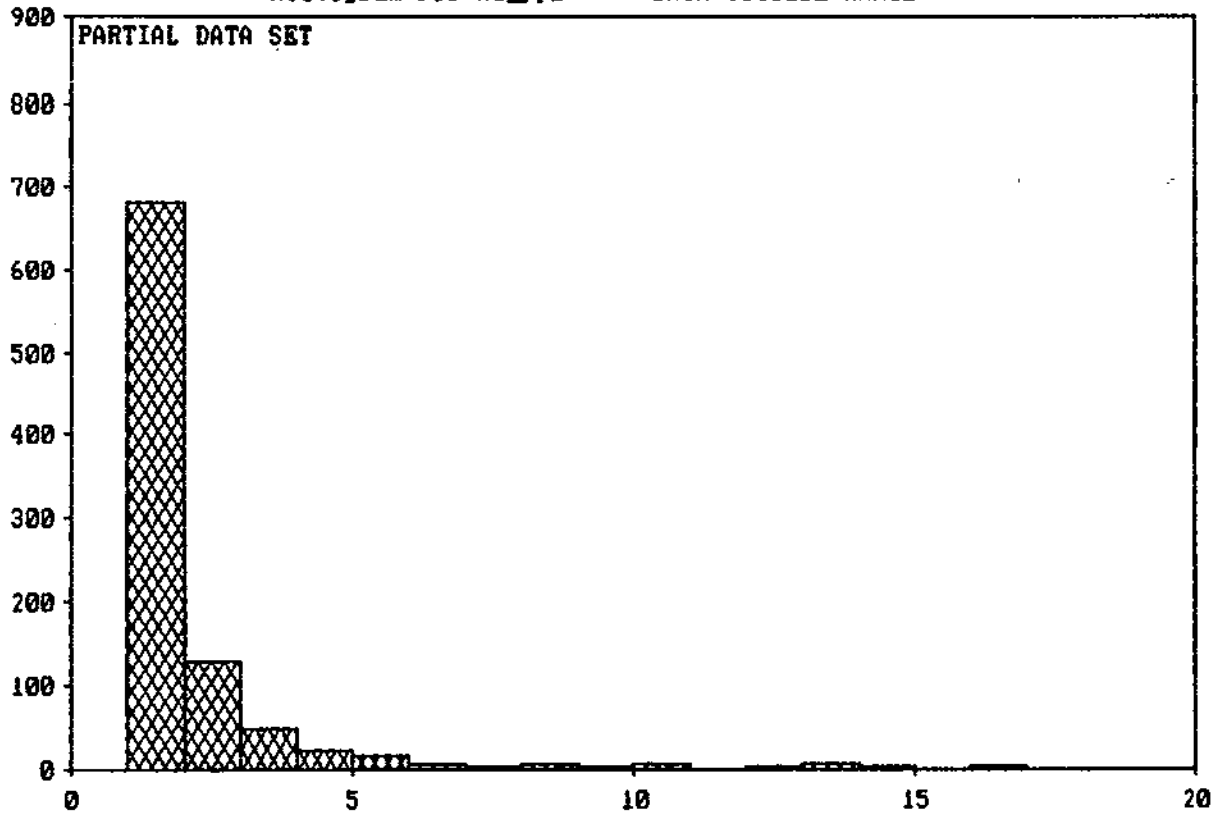
Mean

Data elements inside histogram 940
 Data elements outside histogram 26

Descriptive Statistics

Mean 3.976191
 Variance 750.6161
 Standard Deviation 27.39737
 Skewness 24.13042

Histogram for Au_ppb *** DATA OUTSIDE RANGE ***



Mean = 3.9762 Variance = 750.6
Standard Deviation = 27.4 Skewness = 24.13

Histogram for Sb_ppm

Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	40	962	100	962	100	Mean
40	80	2	0	964	100	
80	120	0	0	964	100	
120	160	0	0	964	100	
160	200	0	0	964	100	
200	240	0	0	964	100	
240	280	0	0	964	100	
280	320	0	0	964	100	
320	360	0	0	964	100	
360	400	1	0	965	100	
400	440	0	0	965	100	
440	480	0	0	965	100	
480	520	0	0	965	100	
520	560	0	0	965	100	
560	600	0	0	965	100	
600	640	0	0	965	100	
640	680	0	0	965	100	
680	720	1	0	966	100	
720	760	0	0	966	100	
760	800	0	0	966	100	

Data elements inside histogram 966
 Data elements outside histogram 0

Descriptive Statistics

Mean 3.917184
 Variance 638.5258
 Standard Deviation 25.26907
 Skewness 24.08541

Histogram for Sb_ppm *** DATA OUTSIDE RANGE ***

Lower limit	Upper limit	Frequency	%	Cumulative	%
0	1	0	0	0	0
1	2	0	0	0	0
2	3	659	68	659	68
3	4	145	15	804	83
4	5	80	8	884	92
5	6	30	3	914	95
6	7	17	2	931	96
7	8	7	1	938	97
8	9	10	1	948	98
9	10	3	0	951	98
10	11	3	0	954	99
11	12	1	0	955	99
12	13	1	0	956	99
13	14	2	0	958	99
14	15	1	0	959	99
15	16	1	0	960	99
16	17	1	0	961	99
17	18	0	0	961	99
18	19	0	0	961	99
19	20	1	0	962	100

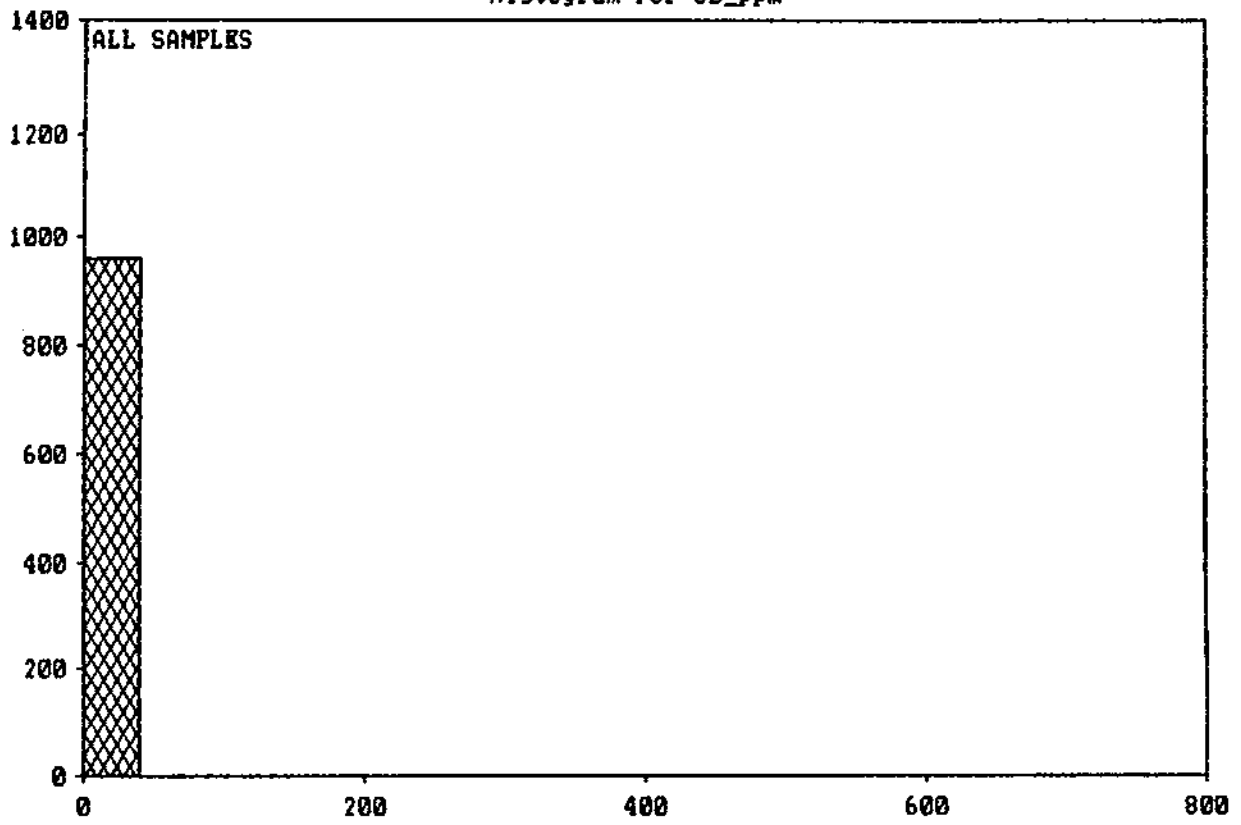
Mean

Data elements inside histogram 962
 Data elements outside histogram 4

Descriptive Statistics

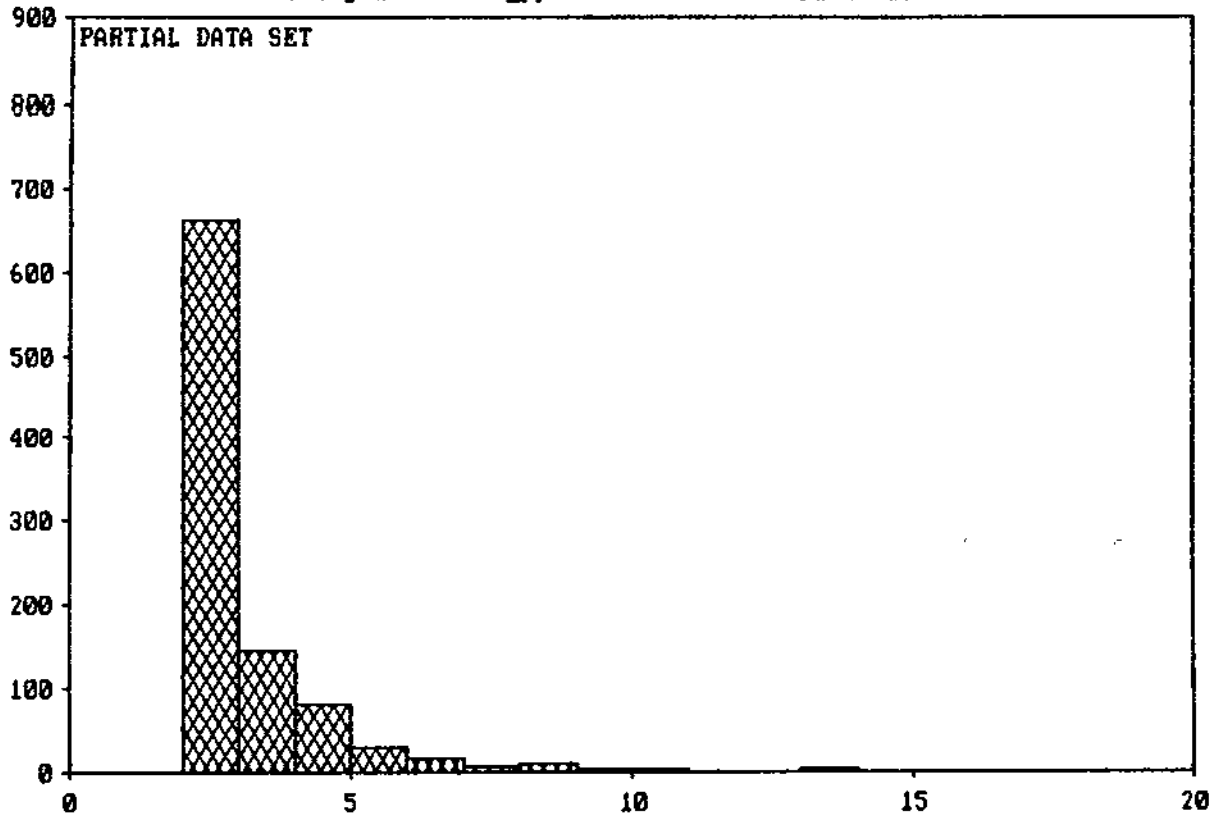
Mean 3.917184
 Variance 638.5258
 Standard Deviation 25.26907
 Skewness 24.08541

Histogram for Sb_ppm



Mean = 3.9172 Variance = 638.5
Standard Deviation = 25.27 Skewness = 24.09

Histogram for Sb_ppm *** DATA OUTSIDE RANGE ***



Mean = 3.9172 Variance = 638.5
Standard Deviation = 25.27 Skewness = 24.09

Histogram for Cd_ppm

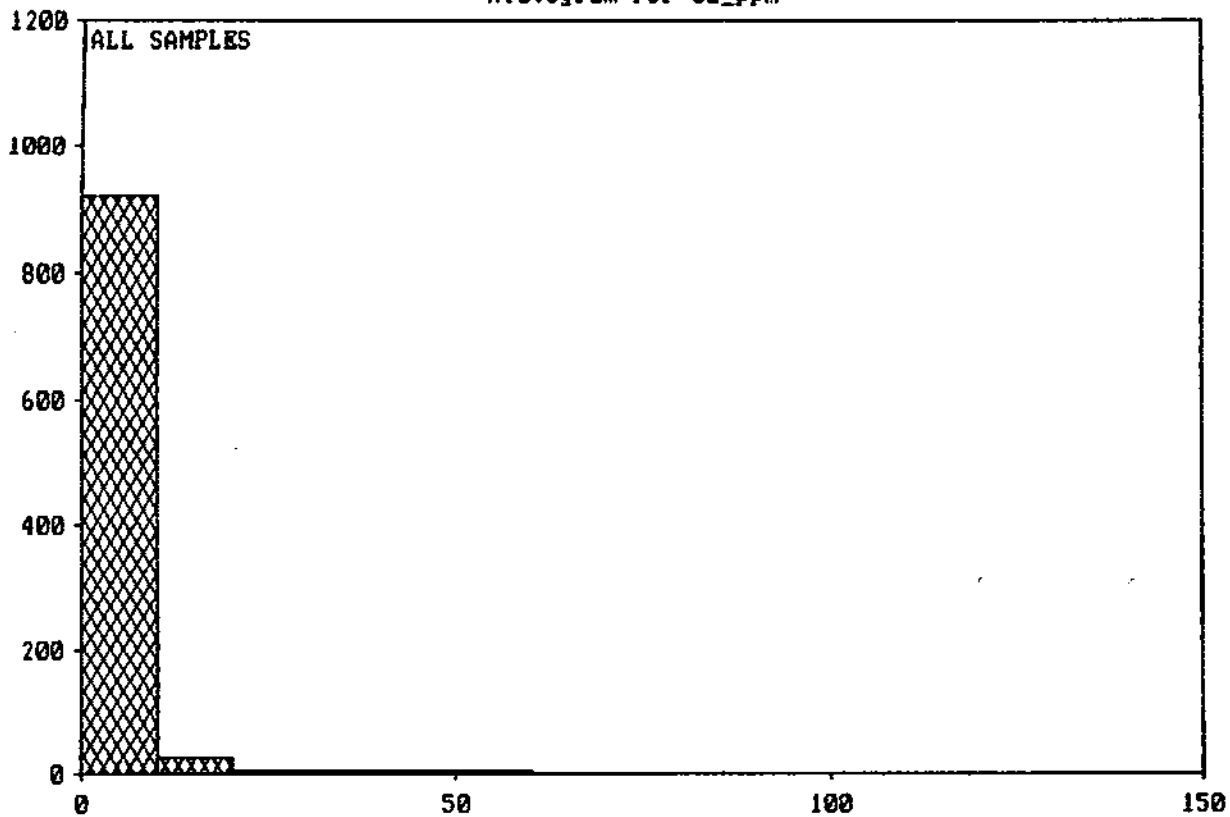
Lower limit	Upper limit	Frequency	%	Cumulative	%	
0	10	921	95	921	95	Mean
10	20	24	2	945	98	
20	30	6	1	951	98	
30	40	3	0	954	99	
40	50	4	0	958	99	
50	60	3	0	961	99	
60	70	2	0	963	100	
70	80	0	0	963	100	
80	90	2	0	965	100	
90	100	0	0	965	100	
100	110	0	0	965	100	
110	120	0	0	965	100	
120	130	1	0	966	100	
130	140	0	0	966	100	
140	150	0	0	966	100	

Data elements inside histogram 966
 Data elements outside histogram 0

Descriptive Statistics

Mean 2.908903
 Variance 66.3046
 Standard Deviation 8.142764
 Skewness 8.656632

Histogram for Cd_ppm



Mean = 2.9089 Variance = 66.3
Standard Deviation = 8.143 Skewness = 8.657

Histogram for Cd_ppm *** DATA OUTSIDE RANGE ***

Lower limit	Upper limit	Frequency	%	Cumulative	%
0	1	0	0	0	0
1	2	697	72	697	72
2	3	92	10	789	82
3	4	51	5	840	87
4	5	31	3	871	90
5	6	22	2	893	92
6	7	6	1	899	93
7	8	8	1	907	94
8	9	10	1	917	95
9	10	4	0	921	95
10	11	4	0	925	96
11	12	3	0	928	96
12	13	3	0	931	96
13	14	2	0	933	97
14	15	4	0	937	97
15	16	2	0	939	97
16	17	2	0	941	97
17	18	1	0	942	98
18	19	0	0	942	98
19	20	8	1	950	98

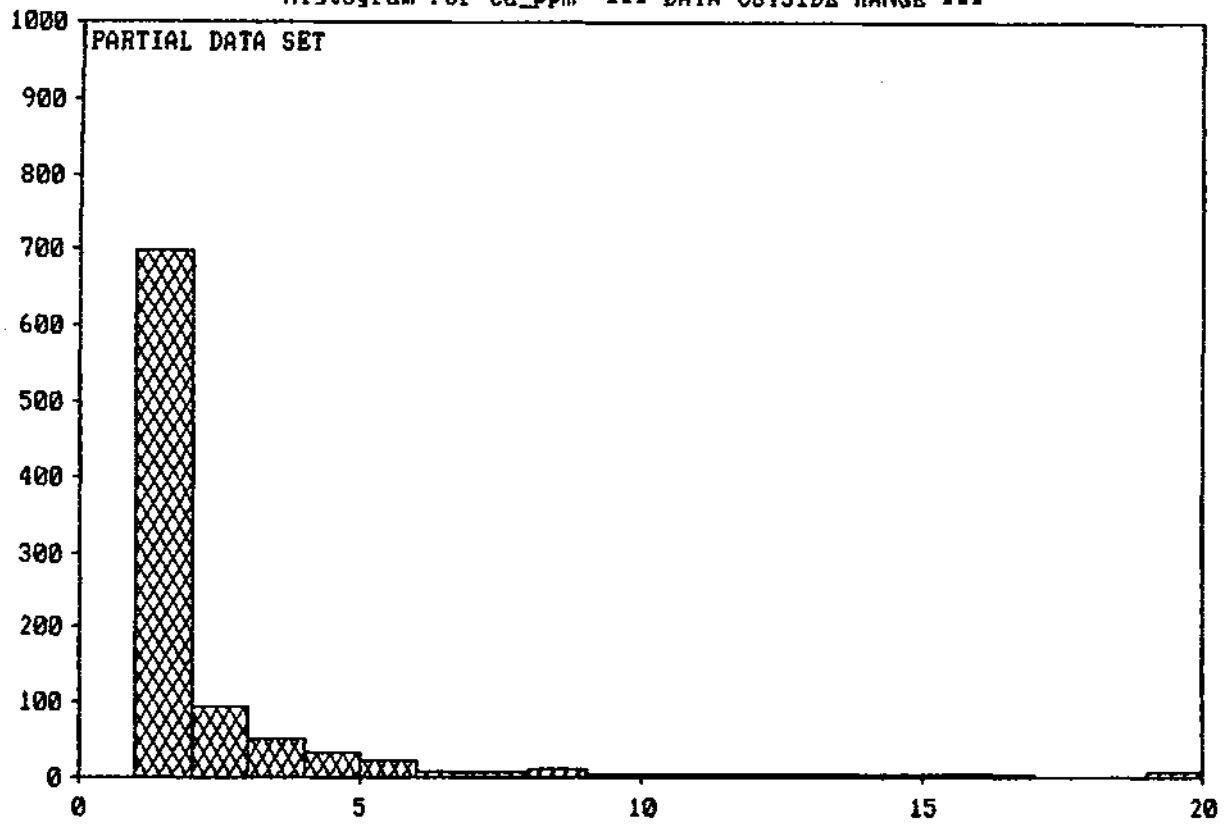
Mean

Data elements inside histogram 950
 Data elements outside histogram 16

Descriptive Statistics

Mean 2.908903
 Variance 66.3046
 Standard Deviation 8.142764
 Skewness 8.656632

Histogram for Cd_ppm *** DATA OUTSIDE RANGE ***



Mean = 2.9089 Variance = 66.3
Standard Deviation = 8.143 Skewness = 8.657

APPENDIX III

Certificate of Analysis - Rocks

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR NG BA YI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: AUG 26 1988 DATE REPORT MAILED: *Sept 6/88* ASSAYER: *C. Leong* D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

HARRISBURG DAYTON RES. CORP. PROJECT SUMMIT CAMP File # 88-3976 Page 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	%	%	%	PPM	PPM	
8804 CHS 1	1	1351	15842	99999	397.5	8	35	3704	13.15	5049	9	2	1	1	1547	908	2	7	.02	.004	2	1	.04	9	.01	2	.24	.01	.11	3	1545
8804 CHS 1A	1	476	15400	10712	114.7	7	31	10352	11.29	20138	11	ND	1	3	208	239	3	25	.34	.021	2	6	.23	29	.01	2	1.07	.01	.13	1	655
8804 CHS 2	1	128	1746	971	22.1	5	15	3115	6.54	450	5	ND	1	2	6	27	4	13	.01	.037	2	7	.05	28	.01	2	.63	.01	.18	1	4
8804 CHS 3	2	496	2430	1915	90.3	7	27	8942	12.35	210	5	ND	2	2	13	50	2	11	.02	.039	2	5	.02	43	.01	2	.81	.01	.18	1	6
8804 CHS 4	1	55	1595	1155	7.5	4	12	6426	3.97	179	10	ND	2	4	14	13	2	13	.09	.021	4	4	.22	56	.01	3	1.14	.01	.17	1	4
8804 CHS 5	2	1694	19111	41444	57.1	15	56	6398	19.68	721	5	ND	1	2	424	29	3	18	.20	.014	2	4	.48	29	.01	2	1.27	.01	.17	10	9
8804 CHS 6	1	41	140	254	1.2	14	14	3881	4.53	79	5	ND	1	10	2	2	3	55	.43	.037	5	15	1.10	52	.01	4	2.01	.03	.14	1	4
8804 CHS 6	1	203	2292	5693	56.6	8	31	78391	8.31	4629	90	ND	7	96	69	92	20	21	.20	.010	13	6	.11	179	.01	2	1.48	.01	.19	1	7
8804 CHS 9	1	83	1157	2284	20.2	19	32	26692	5.85	1623	5	ND	1	12	34	25	2	45	.06	.028	4	11	.86	119	.01	2	2.14	.01	.19	1	6
8804 CHS 10	2	569	20566	22516	116.5	4	16	3197	7.94	1741	5	ND	1	7	513	143	2	18	.10	.013	2	4	.14	15	.01	2	.68	.01	.14	1	415
8804 CHS 11	3	181	9720	3479	62.5	1	7	2054	9.34	900	5	ND	2	1	39	51	2	29	.01	.035	2	6	.14	19	.01	5	.83	.01	.18	1	215
8804 CHS 12	1	161	2218	1250	87.4	2	5	513	7.82	548	5	ND	2	1	5	60	2	9	.01	.019	2	4	.01	12	.01	2	.38	.01	.16	1	1095
8804 CHS 13	2	358	17480	14740	78.3	8	13	2401	9.84	2775	8	ND	1	1	156	117	2	6	.07	.011	2	1	.09	8	.01	2	.42	.01	.11	1	81
8804 CHS 14	1	424	18618	36032	268.7	4	13	1812	12.55	586	5	ND	1	1	350	290	1	4	.04	.005	2	2	.06	3	.01	3	.23	.01	.06	1	675
8804 CHS 15	1	185	6565	2565	70.3	6	11	12432	4.97	1801	5	ND	1	10	39	183	2	10	.14	.021	4	4	.08	38	.01	8	.77	.01	.17	1	28
8804 CHS 16	2	1010	21125	5224	262.1	12	17	19715	8.04	4539	5	ND	1	9	66	1737	2	21	.09	.031	3	5	.14	39	.01	2	.88	.01	.20	1	265
8804 CHS 17	2	2443	15828	99999	228.6	11	70	2206	26.55	7624	5	3	2	1	1455	643	3	5	.01	.005	2	2	.05	2	.01	2	.30	.01	.07	3	1935
8804 CHS 18	1	10131	19247	48987	267.1	7	100	2146	10.83	18153	5	ND	1	2	579	991	2	15	.03	.009	2	5	.12	19	.01	3	.59	.01	.11	1	1715
8804 CHS 19	2	871	19549	46743	173.0	6	17	8941	10.11	4951	5	ND	1	4	461	239	2	26	.11	.031	3	6	.21	28	.01	4	.88	.01	.17	2	925
8804 CHS 20	2	7388	18493	99999	234.9	4	108	2938	17.66	19865	5	2	1	1	1781	1820	2	6	.01	.002	2	1	.12	3	.01	5	.36	.01	.06	4	1125
8804 CHS 21	1	577	20573	17702	212.0	1	11	13157	7.55	3314	6	ND	1	5	234	281	4	20	.09	.023	2	5	.16	21	.01	2	.94	.01	.14	1	1165
8804 CHS 22	2	1089	18196	32702	221.4	11	34	2845	16.34	13394	5	ND	1	1	317	248	2	19	.03	.016	2	6	.17	10	.01	2	.84	.01	.13	1	158
8804 CHS 23	1	2992	20388	57898	252.0	10	12	5040	7.93	933	9	ND	1	5	722	832	2	18	.04	.017	2	4	.15	16	.01	2	.59	.01	.14	2	1935
8804 CHS 24	1	915	19269	85599	295.6	8	12	26145	9.11	2361	8	ND	1	2	972	520	2	25	.36	.024	2	6	.34	18	.01	2	.70	.01	.22	3	1875
8804 CHS 25	1	36	313	227	2.8	15	12	2311	3.31	30	7	ND	2	16	2	2	2	55	.84	.032	6	13	1.25	34	.04	2	2.56	.04	.15	1	3
8804 CHS 26	4	316	6125	2617	85.4	5	9	15242	4.28	1192	5	ND	1	23	30	132	2	22	.29	.042	9	7	.44	76	.01	2	1.25	.01	.19	1	15
8804 CHS 27	4	76	845	901	5.6	12	10	10936	5.51	169	5	ND	1	17	8	38	2	37	.27	.044	6	10	.39	38	.03	11	1.41	.01	.20	1	1
8804 CHS 28	9	88	2764	2029	62.1	6	9	34215	5.02	835	5	ND	1	59	17	326	4	11	.12	.024	4	6	.09	150	.01	2	.65	.01	.16	1	9
8804 CHS 29	6	75	929	1691	9.2	11	9	3926	6.59	201	5	ND	2	11	14	48	2	38	.16	.040	6	8	.52	92	.01	2	2.00	.01	.15	1	2
8804 CHS 30	4	75	1132	1100	28.3	8	9	17708	4.68	797	5	ND	1	44	10	102	2	39	1.44	.030	5	9	.54	40	.03	7	1.69	.01	.13	1	14
8804 CHS 31	5	103	15207	4864	96.5	7	10	26153	5.52	3608	5	ND	1	25	83	107	2	39	.34	.040	9	5	.27	151	.01	4	1.65	.01	.17	1	23
8804 CHS 32	4	54	304	724	2.7	12	12	6289	5.10	120	5	ND	1	15	8	7	2	51	.54	.039	12	12	.96	101	.01	5	2.23	.03	.17	1	3
8804 CHS 33	7	297	18755	5316	95.2	10	12	4313	7.14	163	7	ND	1	6	45	60	2	29	.26	.036	5	7	.20	29	.03	6	.94	.01	.19	1	265
8804 CHS 34	4	585	20189	36507	97.6	12	21	6670	13.85	562	5	ND	1	6	409	94	6	26	.21	.066	4	7	.21	24	.01	11	1.02	.01	.18	2	375
8804 CHS 35	3	2571	19768	39995	265.0	3	10	9131	11.97	2882	5	ND	1	7	1264	1907	5	9	.05	.010	3	2	.04	6	.01	2	.33	.01	.11	3	725
8804 CHS 36	13	408	16410	62085	81.3	3	24	13235	15.35	5635	5	ND	1	2	638	267	2	17	.21	.022	4	3	.21	11	.01	2	.75	.01	.14	4	285
STD C/AC-3	19	59	42	132	6.9	70	30	1064	4.13	43	21	7	39	49	16	20	19	60	.49	.087	42	59	.96	180	.07	34	1.95	.06	.13	12	430

Assay required for high grade samples

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Mn PPM	Co PPM	Ni PPM	Fe %	As PPM	U PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	V PPM	Au* PPB
8804 CHS 35A	2	2799	17575	31465	294.5	11	9	8561	9.13	1777	5	ND	1	5	278	1020	6	8	.16	.009	2	12	.15	12	.01	2	.49	.01	.12	1	2175
8804 CHS 37	1	82	871	800	10.4	17	21	4845	7.04	88	5	ND	1	13	4	25	2	92	.64	.040	4	35	1.22	30	.02	3	2.81	.04	.26	3	4
8804 CHS 38	4	1384	18490	27301	317.4	13	17	24406	8.95	2304	5	ND	1	6	275	1469	2	19	.10	.033	4	15	.14	22	.01	2	.91	.01	.19	1	60
8804 CHS 39	1	1770	17407	72179	267.7	4	10	21208	9.94	2507	5	ND	1	5	725	2595	5	3	.33	.006	2	8	.05	5	.01	2	.13	.01	.07	2	695
8804 CHS 40	2	1015	17846	23927	304.0	8	20	4453	16.42	799	5	ND	1	1	234	263	2	6	.02	.027	2	10	.01	11	.01	2	.48	.01	.14	5	245
8804 CHS 41	1	770	20749	74826	252.6	12	42	3705	13.62	6665	5	ND	1	1	738	288	3	19	.05	.024	2	13	.14	9	.01	2	.54	.01	.16	3	495
8804 CHS 42	19	256	7348	2442	51.1	5	11	12590	12.19	521	5	ND	1	5	19	59	2	43	.10	.107	7	29	.63	25	.01	2	1.92	.01	.21	2	13
8804 CHS 43	1	156	4095	3664	27.0	12	20	47171	12.90	1948	5	ND	1	27	36	83	2	15	.07	.031	11	14	.08	355	.01	10	1.32	.01	.22	2	5
8804 CHS 44	1	171	5334	4560	36.1	8	18	45996	9.31	3397	5	ND	1	25	84	255	2	26	.05	.039	9	12	.18	113	.01	8	1.09	.01	.21	7	39
8804 CHS 45	1	85	619	890	6.1	12	14	8648	8.15	190	5	ND	1	5	3	20	2	41	.14	.052	6	18	1.06	45	.01	2	2.19	.01	.25	3	2
8804 CHS 46	1	96	9937	6590	61.3	10	13	11287	6.05	276	5	ND	1	7	61	52	2	37	.37	.063	5	15	.44	36	.01	3	1.42	.01	.20	3	17
8804 CHS 47	1	87	2973	2907	13.0	8	8	4423	5.35	120	5	ND	1	4	29	20	2	26	.09	.016	5	13	.61	32	.01	2	1.59	.01	.18	3	1
8804 CHS 48	2	28	1209	701	5.2	8	8	6701	3.53	135	5	ND	1	3	5	12	2	25	.11	.038	7	12	.49	41	.01	3	1.70	.01	.17	3	1
8804 CHS 49	1	38	112	215	1.1	10	15	3211	5.07	40	5	ND	1	19	2	12	2	91	.39	.068	8	21	1.08	24	.03	7	2.40	.04	.10	3	3
8804 CHS 50	2	24	125	432	.6	8	8	3204	2.85	33	5	ND	1	20	2	10	2	31	.49	.058	8	12	.53	49	.03	3	1.63	.03	.23	1	6
8804 CHS 51	1	23	98	188	.6	11	11	2000	4.43	32	5	ND	1	13	1	12	2	89	.41	.064	7	30	1.28	22	.12	5	2.14	.03	.09	3	5
8804 CHS 52	1	105	3878	3349	12.2	8	12	3455	6.15	39	5	ND	1	15	29	19	2	48	.36	.063	6	19	.97	33	.03	2	2.17	.03	.20	3	4
8804 CHS 53	1	44	2081	1269	7.9	9	16	4668	4.51	92	5	ND	1	19	5	13	2	35	.64	.071	10	18	.95	17	.07	3	2.50	.03	.19	2	1
8804 CHS 54	3	464	20993	4940	172.6	7	8	1987	5.12	411	5	ND	1	4	62	129	2	5	.07	.026	3	7	.08	14	.01	2	.56	.01	.17	8	88
8804 CHS 55	1	788	20832	14127	251.0	3	10	22300	4.73	10117	5	3	1	8	157	1763	2	4	.05	.011	2	4	.04	20	.01	2	.32	.01	.10	1	1955
8804 CHS 56	1	463	16490	10723	184.3	6	16	46658	8.67	1740	5	ND	1	16	122	547	2	18	.05	.031	3	16	.19	36	.01	6	.91	.01	.17	1	55
8804 CHS 57	1	1386	20262	31945	311.4	4	10	15339	11.84	2319	5	ND	1	5	375	1194	2	4	.01	.035	3	9	.01	14	.01	7	.48	.01	.17	1	625
8804 CHS 58	2	396	19577	36901	108.1	12	25	2911	9.00	233	5	ND	1	3	436	99	2	11	.03	.040	3	13	.07	18	.01	2	.60	.01	.19	1	53
8804 CHS 59	2	363	9773	5928	150.4	13	16	4500	9.56	1297	5	ND	1	4	69	159	2	9	.03	.079	4	9	.04	22	.01	4	.51	.01	.23	7	103
8804 CHS 60	2	464	20381	62272	296.0	12	32	4281	9.40	369	5	ND	1	5	583	240	2	18	.09	.042	2	20	.23	23	.01	2	.96	.01	.18	3	62
8804 CHS 61	2	1127	20446	21899	241.6	6	25	9592	8.76	4383	5	ND	1	5	222	209	3	15	.03	.040	2	15	.06	24	.01	3	.46	.01	.21	3	415
8804 CHS 62	3	522	19270	80155	292.4	14	36	16524	12.90	1978	5	ND	1	11	849	367	2	10	.07	.035	3	12	.10	28	.02	5	.73	.01	.23	4	545
8804 CHS 63	1	477	18908	55156	215.4	18	26	12041	15.19	235	5	ND	1	5	567	135	2	52	.11	.057	4	24	.59	23	.01	3	2.11	.01	.31	3	31
8804 CHS 64	2	481	22486	40350	59.7	29	39	3564	12.28	6320	5	ND	1	5	337	136	2	78	.18	.054	2	23	.96	22	.01	2	2.10	.01	.24	1	835
8804 CHS 65	1	324	4557	20295	50.7	10	17	1165	4.92	12849	5	ND	1	2	251	78	2	11	.05	.033	2	6	.14	18	.01	2	.55	.01	.19	1	140
8804 CHS 66	5	109	5136	16112	38.4	12	34	5577	6.92	26072	5	ND	1	7	150	106	2	7	.06	.019	2	12	.02	31	.01	2	.28	.01	.15	1	515
8804 CHS 67	4	98	2383	2009	14.4	6	12	5198	4.19	4323	5	ND	1	4	37	48	2	11	.04	.048	3	7	.03	36	.01	4	.48	.01	.20	1	81
8804 CHS 68	2	105	2313	1391	16.8	9	10	4794	4.54	731	5	ND	1	3	17	69	2	19	.04	.035	3	8	.11	22	.01	9	.73	.01	.22	1	29
8804 CHS 69	1	296	3690	44103	19.3	14	39	3278	11.90	19612	5	ND	1	1	415	90	2	4	.11	.032	2	10	.01	14	.01	4	.27	.01	.16	1	285
8804 CHS 70	2	407	2480	13961	46.1	9	9	819	4.24	15053	5	ND	1	3	146	95	2	4	.04	.031	2	7	.01	28	.01	2	.22	.01	.18	1	365
8804 CHS 71	1	249	5226	5280	53.8	7	15	496	7.03	40315	5	ND	1	1	88	251	2	4	.03	.029	2	7	.01	12	.01	5	.18	.01	.15	1	1035
STD C/AU-3	19	59	40	131	7.1	71	31	1035	4.26	39	23	8	38	49	18	20	19	60	.49	.094	41	61	.95	179	.07	32	2.00	.05	.16	13	515

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	O	Au	Tb	Sr	Cl	SB	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	V	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	PPM	PPM	
8804 CHS 72	1	271	21229	1642	105.0	4	14	292	8.57	15554	5	ND	1	1	18	179	2	8	.05	.043	2	2	.01	11	.01	17	.26	.01	.19	1	855
8804 CHS 73	5	123	4347	3487	21.9	11	11	2595	6.98	4974	5	ND	1	2	42	28	2	22	.10	.040	2	10	.14	16	.01	9	.68	.01	.20	1	62
8804 CHS 74	2	182	9859	3906	46.4	5	21	1669	7.60	16374	5	ND	1	9	56	142	2	12	.10	.035	2	3	.04	19	.01	15	.43	.01	.20	1	875
8804 CHS 75	4	1001	24920	9499	271.1	6	10	1662	14.98	15741	5	ND	1	2	83	2272	5	6	.02	.036	3	2	.01	13	.01	11	.19	.01	.15	1	935
8804 CHS 76	23	219	9049	1486	74.7	1	9	1722	16.49	4528	5	ND	1	2	2	83	2	12	.01	.041	2	2	.01	26	.01	9	.64	.01	.20	1	105
8804 CHS 76A	3	543	7082	25370	55.0	14	36	5347	15.18	16342	5	ND	1	1	237	249	2	8	.06	.016	2	7	.01	13	.01	10	.25	.01	.16	1	945
8804 CHS 77	9	163	7472	7510	78.0	4	7	9389	5.26	2752	5	ND	1	5	64	251	2	15	.05	.034	4	3	.12	32	.01	6	.80	.01	.22	2	115
8804 CHS 78	5	301	10915	20703	59.5	11	40	2598	11.76	15819	5	ND	1	2	196	67	2	12	.06	.042	2	8	.04	20	.01	12	.60	.01	.21	1	395
8804 CHS 79	1	354	18717	3558	103.9	5	18	3916	16.35	15705	5	ND	2	2	41	154	2	10	.03	.048	2	5	.01	37	.01	13	.70	.01	.19	1	215
8804 CHS 80	3	1008	22260	32031	256.9	6	37	2327	14.28	16265	5	3	1	1	332	472	2	5	.02	.017	2	6	.01	18	.01	10	.31	.01	.14	1	1995
8804 CHS 81	1	605	24946	14126	268.8	3	8	1974	7.08	10792	5	2	1	1	150	1294	2	4	.04	.014	2	3	.01	10	.01	12	.15	.01	.08	1	1055
8804 CHS 82	1	642	24423	8307	231.6	21	22	399	14.19	15790	5	ND	1	2	85	230	2	10	.01	.029	2	9	.02	21	.01	10	.39	.01	.19	1	355
8804 CHS 83	1	1105	20322	31956	282.7	3	27	16132	18.87	15732	5	ND	1	5	287	498	2	7	.07	.013	2	3	.01	14	.01	8	.33	.01	.14	1	995
8804 CHS 84	1	1902	18287	27904	272.4	6	25	4486	30.37	12530	5	ND	2	1	250	311	2	3	.12	.009	2	4	.01	9	.01	14	.16	.01	.11	1	425
8804 CHS 85	1	313	19859	6412	125.8	1	7	1822	3.52	15818	5	ND	1	1	47	122	2	11	.04	.048	2	5	.02	22	.01	7	.48	.01	.22	1	405
8804 CHS 86	1	1910	20265	35251	203.2	16	24	3886	19.81	15739	5	ND	1	1	315	195	11	7	.01	.016	2	6	.01	8	.01	13	.30	.01	.16	1	555
8804 CHS 87	1	876	24716	19286	265.8	8	34	11442	10.56	15714	5	ND	1	3	160	194	2	8	.01	.021	4	6	.01	34	.01	7	.38	.01	.18	1	535
8804 CHS 88	2	614	25474	2886	258.0	5	10	429	5.52	16010	5	ND	2	1	35	1856	3	3	.02	.011	2	6	.01	12	.01	2	.17	.01	.10	1	2575
8804 CHS 88A	1	193	25624	1971	246.5	1	4	321	11.56	2496	5	ND	2	1	2	128	2	7	.01	.036	2	4	.01	14	.01	4	.44	.01	.24	1	66
8804 CHS 89	3	481	24780	2607	254.7	4	6	1786	12.09	15985	5	ND	2	2	10	968	2	6	.01	.027	2	5	.01	19	.01	8	.39	.01	.17	1	445
8804 CHS 90	4	1482	25816	18195	264.0	1	4	280	7.54	9269	5	ND	2	1	170	866	2	2	.01	.021	2	2	.01	24	.01	5	.25	.01	.15	1	815
8804 CHS 91	2	1236	19550	48171	257.2	15	27	1440	23.83	9024	5	ND	2	1	525	716	2	5	.01	.011	2	4	.03	1	.01	11	.23	.01	.11	29	285
8804 CHS 92	1	296	22531	2911	238.7	7	12	1365	8.51	7792	5	ND	2	1	20	262	2	7	.02	.043	2	3	.01	27	.01	5	.36	.01	.19	1	135
8804 CHS 93	2	2477	20746	41476	258.0	12	21	828	24.28	11924	5	ND	3	1	276	1379	2	4	.01	.022	2	3	.01	9	.01	2	.27	.01	.12	1	1195
8804 CHS 94	1	1944	23876	60831	300.5	9	60	2537	9.42	16342	5	3	1	2	877	1256	2	6	.03	.015	2	3	.01	17	.01	11	.29	.01	.15	1	2045
8804 CHS 95	3	810	25173	5806	244.6	5	6	705	12.72	15736	5	2	2	1	48	333	2	11	.01	.031	2	6	.05	22	.01	14	.63	.01	.21	1	1650
8804 CHS 96	1	2782	18500	36801	244.9	13	29	2186	31.82	2430	5	ND	2	1	350	420	2	5	.04	.007	2	3	.05	7	.01	9	.29	.01	.10	3	103
8804 CHS 96A	2	1022	26554	2913	277.3	6	6	696	5.09	11976	5	2	1	1	38	1193	2	4	.01	.017	2	6	.01	23	.01	6	.34	.01	.16	1	1275
8804 CHS 97	1	903	22176	21657	309.1	6	44	4027	12.15	15790	5	ND	1	5	239	431	2	22	.18	.035	2	5	.20	21	.01	16	1.03	.01	.21	1	525
8804 CHS 98	2	641	21918	86979	205.7	10	25	10862	14.28	9475	5	ND	1	3	1057	235	2	12	.17	.016	2	6	.17	14	.01	12	.79	.01	.14	2	395
8804 CHS 99	1	1516	22543	43076	335.7	4	54	4108	15.87	16357	5	2	2	1	391	1144	2	6	.06	.011	2	1	.04	16	.01	12	.32	.01	.15	1	1325
8804 CHS 100	2	1080	9953	90306	143.7	10	28	1745	19.90	15785	5	ND	3	1	1046	1088	2	8	.01	.015	2	4	.04	12	.01	12	.41	.01	.14	2	595
8804 CHS 101	2	1849	21048	42439	308.7	9	24	1620	22.71	16026	5	3	2	1	422	830	2	6	.02	.013	2	4	.01	12	.01	2	.24	.01	.14	1	1735
8804 CHS 102	1	2581	9793	50656	234.7	6	28	2067	31.19	15816	5	2	3	1	494	521	2	3	.01	.005	2	2	.01	1	.01	7	.15	.01	.08	2	1955
8804 CHS 103	1	952	19967	99999	247.3	7	20	5203	19.58	14656	5	ND	2	1	1496	892	2	5	.03	.003	2	2	.10	3	.01	5	.34	.01	.04	2	785
8804 CHS 104	1	898	22195	35470	217.9	13	18	45186	11.52	13060	5	ND	1	6	297	943	2	26	.59	.018	3	10	.26	7	.02	9	.89	.01	.09	1	545
STD C/AU-R	19	62	41	137	7.0	71	30	1049	4.17	44	17	7	38	50	19	16	22	60	.47	.091	39	60	.94	182	.07	34	2.00	.06	.15	11	520

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Mi	Co	Mn	Fe	As	U	Au	Tb	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
8804 CHS 105	2	818	20162	48220	199.5	47	31	5894	13.48	12119	5	2	3	3	419	260	2	43	.11	.028	2	41	.30	16	.01	5	1.12	.01	.17	1	1340
8804 CHS 106	1	227	7069	15351	43.8	13	12	3524	6.58	906	5	ND	1	2	91	20	2	16	.16	.048	2	3	.07	20	.01	6	.40	.01	.18	1	13
8804 CHS 106A	3	1637	21134	9480	107.6	15	20	781	6.78	3457	5	ND	1	3	167	59	2	14	.02	.030	2	5	.03	26	.01	4	.56	.01	.21	1	112
8804 CHS 107	5	93	3465	955	28.8	3	9	1409	4.18	1368	5	ND	1	5	13	41	2	10	.04	.036	4	4	.05	45	.01	10	.60	.01	.27	1	25
8804 CHS 107A	1	512	13327	6506	114.5	15	20	3577	6.24	3463	5	ND	1	5	77	79	2	28	.16	.025	2	6	.27	17	.02	3	1.01	.01	.14	1	220
8804 CHS 108	3	99	10832	4473	42.6	4	9	4549	5.13	924	5	ND	1	2	78	105	2	11	.04	.029	2	4	.02	14	.01	9	.30	.01	.14	2	17
8804 CHS 108A	1	126	5663	522	25.2	2	6	743	7.10	1534	5	ND	1	6	2	35	2	25	.08	.061	3	4	.28	22	.01	9	.84	.01	.25	1	19
8804 CHS 109	5	96	2816	3450	19.3	12	7	3109	4.69	983	5	ND	1	5	30	30	2	21	.06	.027	3	5	.08	30	.01	18	.79	.01	.23	1	3
8804 CHS 109A	4	296	7120	16466	85.6	22	26	8965	8.44	1171	5	ND	2	3	164	112	2	21	.11	.053	4	5	.07	29	.01	12	.91	.01	.23	1	34
8804 CHS 110	1	1188	22270	13567	271.4	3	28	27816	9.73	12041	5	2	8	3	132	2461	2	11	.02	.015	3	3	.01	23	.01	14	.25	.01	.10	1	1760
8804 CHS 110A	6	705	24726	714	150.0	2	4	358	3.51	10681	5	ND	1	3	5	89	3	6	.02	.029	2	2	.01	35	.01	4	.37	.01	.21	14	290
8804 CHS 111	8	242	3878	2513	92.4	15	10	12644	4.63	1021	5	ND	2	6	21	250	2	21	.05	.024	4	9	.11	30	.01	4	.62	.01	.17	1	23
8804 CHS 111A	5	374	14000	2168	20.0	15	13	3013	4.41	411	5	ND	1	4	18	28	2	21	.10	.052	5	5	.06	34	.01	14	.61	.01	.22	1	2
8804 CHS 112	4	1219	24443	1431	200.3	3	8	620	4.02	9677	5	ND	1	4	47	1542	2	8	.05	.024	2	3	.03	16	.01	5	.34	.01	.12	11	340
8804 CHS 113	4	906	24340	13404	215.2	13	7	1964	4.83	232	5	ND	1	2	161	435	2	17	.08	.034	3	4	.07	24	.01	6	.49	.01	.23	1	260
8804 CHS 113A	4	1311	21905	46672	231.1	11	19	2045	6.20	3553	5	ND	2	4	567	414	3	15	.09	.025	2	5	.12	18	.02	6	.64	.01	.17	1	510
8804 CHS 114	5	475	24451	4321	185.8	4	11	4539	11.28	6694	5	ND	2	1	27	620	2	12	.03	.032	4	4	.01	7	.01	12	.71	.01	.20	10	36
8804 CHS 114A	2	179	25176	769	298.3	3	2	514	2.48	3987	5	ND	1	4	24	1373	2	8	.02	.006	2	4	.02	17	.01	3	.23	.01	.11	5	310
8804 CHS 114B	4	660	10619	1026	247.5	4	5	285	4.00	2134	5	ND	1	2	38	137	4	10	.03	.025	2	4	.03	24	.01	6	.35	.01	.21	3	136
8804 CHS 115	1	404	24797	1719	208.3	2	4	1070	5.03	722	5	ND	2	2	15	878	49	4	.02	.017	2	2	.01	11	.01	4	.26	.01	.10	1	56
8804 CHS 115A	3	503	14625	34986	68.8	17	13	1697	7.69	1038	5	ND	1	2	291	41	2	14	.07	.028	4	4	.08	19	.01	4	.57	.01	.19	1	16
8804 CHS 116	4	185	5737	880	63.3	4	5	778	7.30	555	5	ND	1	4	3	61	2	26	.02	.046	2	10	.11	19	.01	9	.85	.01	.19	1	3
8804 CHS 116A	4	375	7152	1626	196.7	7	5	591	4.30	683	5	ND	1	2	35	71	2	15	.03	.023	2	5	.05	27	.01	9	.46	.01	.19	1	82
8804 CHS 117	2	2402	23049	33022	220.0	4	7	1440	4.79	3143	5	ND	2	2	334	2384	2	9	.02	.023	2	3	.05	13	.01	6	.38	.01	.14	1	570
8804 CHS 118	1	712	16899	5037	96.6	3	21	471	10.09	12138	5	2	1	1	75	361	2	3	.04	.004	2	4	.01	7	.01	8	.12	.01	.06	19	1030
8804 CHS 119	2	241	6276	1510	68.8	2	5	389	4.75	1854	5	ND	1	3	20	79	2	12	.04	.056	4	3	.03	22	.01	13	.57	.01	.18	1	450
8804 CHS 120	1	3105	22388	14664	215.7	2	5	1289	7.50	756	5	ND	2	6	161	4070	2	10	.01	.009	2	16	.01	5	.01	7	.32	.01	.09	1	690
8804 CHS 121	2	238	13437	2888	83.7	11	8	1919	4.80	1297	5	ND	1	5	84	56	2	22	.05	.032	5	7	.18	29	.01	6	.93	.01	.20	1	28
8804 CHS 122	1	377	13245	671	68.7	3	7	211	7.51	12198	5	ND	1	3	7	138	2	7	.01	.017	3	4	.02	54	.01	9	.41	.01	.20	11	1190
8804 CHS 123	1	125	5778	5719	42.7	2	8	1464	5.72	5956	5	ND	1	2	94	67	2	9	.04	.006	2	3	.03	8	.01	4	.38	.01	.04	9	127
8804 CHS 123A	2	911	18950	40799	241.9	22	26	3584	11.96	2631	5	ND	2	5	399	202	2	37	.18	.024	2	9	.33	6	.04	7	1.24	.01	.11	1	101
8804 CHS 124	4	565	21608	3952	141.2	6	11	1155	19.22	11953	5	2	2	2	25	1904	2	10	.02	.021	4	10	.02	17	.01	10	.51	.01	.12	16	1300
8804 CHS 125	2	233	24181	819	184.1	3	5	709	7.54	11752	5	ND	1	2	2	249	2	10	.03	.010	2	5	.03	10	.01	10	.41	.01	.08	17	650
8804 CHS 126	1	1482	17696	46735	223.4	23	33	1610	16.83	11594	5	ND	2	3	503	439	2	9	.07	.006	2	4	.04	2	.01	4	.29	.01	.11	1	440
8804 CHS 127	1	148	5233	3211	30.3	5	53	950	16.43	12302	5	3	2	4	81	439	2	11	.05	.011	2	3	.03	13	.01	14	.52	.01	.13	1	2580
8804 CHS 128	1	823	18707	99999	231.6	9	19	4139	16.61	6270	5	2	2	1	2575	769	3	7	.06	.010	2	3	.05	4	.01	4	.22	.01	.06	1	1320
STD C/AU-2	18	60	38	133	7.1	67	29	1095	4.00	41	20	7	37	49	20	17	21	59	.48	.089	41	56	.93	180	.06	34	2.02	.06	.14	12	480

HARRISBURG DAYTON RES. CORP. PROJECT SUMMIT CAMP FILE # 88-3976

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Tb	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPM
8804 CHS 129	1	113	3737	3290	29.0	4	4	16901	3.35	1170	5	ND	1	5	42	45	3	7	.06	.004	7	5	.05	74	.01	2	.52	.01	.02	1	47
8804 CHS 130	1	236	21790	4550	117.6	1	11	52477	3.73	10107	6	ND	1	14	107	2558	10	5	.02	.013	4	3	.01	51	.01	2	.29	.01	.14	1	453
8804 CHS 131	1	70	5727	1071	43.8	1	4	10352	4.71	4734	5	ND	1	2	14	132	2	18	.03	.022	3	4	.33	29	.01	2	.99	.01	.16	1	104
8804 CHS 132	1	256	5520	1299	140.2	1	4	920	11.10	1084	7	ND	1	1	4	199	2	20	.01	.035	2	7	.01	11	.01	4	.42	.01	.21	1	115
8804 CHS 133	1	78	35569	658	251.2	5	32	1379	5.96	14129	5	ND	1	5	23	436	2	10	.03	.016	2	2	.10	13	.01	4	.42	.01	.18	1	840
8804 CHS 134	1	429	35351	18737	247.3	1	7	39706	5.74	5561	5	ND	1	3	241	5777	3	4	.13	.007	2	2	.10	17	.01	2	.30	.01	.13	1	252
8804 CHS 135	1	100	5227	2603	45.0	6	8	2352	19.38	1074	5	ND	1	3	6	115	3	43	.05	.039	4	22	.25	16	.01	3	1.12	.01	.19	1	35
8804 CHS 136	1	351	35912	27205	215.9	10	17	43533	9.57	3415	9	ND	1	11	432	2386	2	15	.14	.029	2	6	.03	14	.01	2	.29	.01	.23	1	95
8804 CHS 137	1	559	35032	11207	291.6	1	21	65869	13.29	13754	6	ND	1	17	184	4498	2	14	.02	.021	6	8	.04	22	.01	2	.54	.01	.21	1	785
8804 CHS 138	1	175	35576	4379	151.3	4	9	20039	4.40	2693	5	ND	1	15	66	5025	2	7	.02	.007	2	5	.05	31	.01	2	.36	.01	.16	1	52
8804 CHS 139	2	222	5751	3765	46.5	4	7	4233	8.65	2007	6	ND	1	4	21	185	5	10	.03	.012	2	3	.16	15	.01	2	.68	.01	.20	1	70
8804 CHS 140	1	205	18157	3568	96.0	14	11	17624	6.90	1300	5	ND	1	10	29	198	2	11	.09	.029	3	7	.04	23	.01	2	.45	.01	.25	1	53
8804 CHS 141	1	283	21419	3919	139.4	4	11	21183	4.26	4320	6	ND	1	3	43	210	2	6	.06	.031	6	4	.01	58	.01	2	.68	.01	.25	1	39
8804 CHS 142	1	858	32457	29948	296.3	3	16	16648	14.79	13812	5	ND	1	2	292	1025	20	5	.01	.015	6	1	.01	22	.01	2	.31	.01	.18	1	1205
8804 CHS 143	4	161	8055	3446	49.4	4	10	9745	7.33	3860	5	ND	1	6	24	66	2	17	.01	.034	4	3	.01	24	.01	8	.59	.01	.24	1	58
8804 CHS 144	1	3149	34846	71274	312.3	47	17	10513	10.52	2566	5	ND	1	19	929	463	2	23	3.88	.050	2	30	.16	3	.01	7	.43	.01	.19	3	119
8804 CHS 145	1	1088	24359	29990	273.0	42	8	37986	12.39	6022	7	ND	1	21	321	219	6	16	3.85	.041	2	46	.36	12	.01	2	.44	.01	.21	6	45
8804 CHS 146	1	2241	26248	48566	240.9	93	14	26873	14.99	2434	7	ND	1	17	595	743	6	16	4.43	.038	1	30	.30	9	.01	4	.39	.01	.20	2	42
8804 CHS 147	1	2643	30435	29973	290.7	71	29	14338	5.92	3167	5	ND	1	11	451	700	6	25	.17	.047	3	45	.23	14	.01	2	.65	.01	.19	1	166
8804 CHS 148	1	659	20701	67068	192.4	32	13	69307	12.20	1989	6	ND	2	13	961	852	19	19	1.16	.012	3	46	.49	17	.01	2	.50	.01	.10	2	35
8804 CHS 149	1	285	14163	3947	42.8	86	26	6212	11.22	285	6	ND	1	8	45	48	2	117	.30	.071	4	308	1.92	22	.08	2	4.37	.01	.45	1	9
8804 CHS 150	1	174	2879	5137	63.7	33	14	22446	4.84	687	6	ND	1	54	49	341	2	59	.60	.060	6	40	1.39	33	.02	2	2.63	.01	.16	1	10
8804 CHS 151	1	83	2139	4161	25.1	71	21	23004	6.32	684	5	ND	1	58	36	71	3	84	.40	.047	7	124	1.63	18	.01	5	3.15	.02	.18	1	1
8804 CHS 152	4	46	2026	3767	17.4	29	14	26445	5.34	711	5	ND	1	88	40	185	3	48	.49	.062	8	24	1.15	54	.01	2	2.41	.01	.17	1	5
8804 CHS 153	6	441	12660	17808	182.1	24	14	45298	6.23	1749	5	ND	1	87	210	804	6	36	.42	.055	6	12	.43	41	.01	2	1.15	.01	.19	1	9
8804 CHS 154	4	340	7450	13937	140.0	25	17	30132	6.85	1634	5	ND	1	51	152	346	2	54	.40	.056	8	38	.76	59	.01	3	2.17	.01	.22	1	27
8804 CHS 155	2	226	8122	19143	67.6	57	23	78806	11.42	5659	7	ND	6	338	201	396	39	45	.70	.024	9	104	.61	25	.01	2	1.22	.01	.19	1	54
8804 CHS 156	1	1252	21859	56773	270.9	83	22	33311	15.24	3424	5	ND	1	39	752	393	2	62	.23	.045	4	125	1.13	8	.01	2	2.26	.01	.17	3	147
8804 CHS 157	1	1312	20599	40425	283.9	145	22	20974	16.13	1443	6	ND	1	27	527	306	2	92	3.86	.032	4	99	2.12	8	.01	2	4.47	.01	.17	2	123
8804 CHS 158	1	1494	20948	44504	292.1	43	14	60435	11.70	14286	6	ND	1	15	476	2124	10	20	.91	.017	2	60	.45	17	.01	2	.50	.01	.15	2	525
8804 CHS 159	1	1666	29225	35476	367.1	78	19	43799	12.96	13696	9	ND	1	26	388	2801	2	26	4.70	.015	3	120	.58	16	.01	2	.73	.01	.13	2	204
8804 CHS 160	1	976	23466	39094	227.1	51	12	13742	11.79	1075	5	ND	1	9	469	452	5	62	1.16	.073	4	53	.90	9	.01	2	2.29	.01	.19	3	199
8804 CHS 161	1	872	20922	75997	243.6	3	4	75842	8.37	9440	9	ND	4	44	935	949	33	6	4.14	.004	7	6	.18	27	.01	2	.19	.01	.07	2	126
8804 CHS 162	1	1908	25766	63667	164.7	31	10	56725	7.10	6287	6	ND	1	13	843	2155	2	18	.77	.017	2	58	.40	1	.01	2	.56	.01	.13	2	93
8804 CHS 162A	1	386	11034	54407	51.5	10	26	11789	11.06	434	6	ND	1	51	650	70	2	35	5.49	.011	4	6	1.55	19	.01	5	3.61	.01	.15	2	6
8804 CHS 163	1	3391	21638	35854	251.0	104	17	26550	14.40	2278	5	ND	1	12	443	450	3	24	2.05	.030	3	55	.47	7	.01	2	.61	.01	.26	2	64
STD C/AU-R	19	63	42	133	7.3	67	31	1097	4.01	41	16	8	38	51	19	17	23	61	.48	.089	42	61	.94	180	.07	33	1.95	.06	.13	12	305

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
8804 CHS 163A	2	2176	21949	57303	305.0	22	14	13025	12.32	87	6	ND	1	45	775	288	6	59	3.44	.019	3	11	1.41	10	.04	2	2.82	.01	.16	3	21
8804 CHS 163B	2	309	26124	18402	62.5	7	13	8436	11.49	325	5	ND	1	32	191	73	2	55	13.12	.020	7	10	.96	23	.01	8	2.31	.01	.17	1	2
8804 CHS 164	1	2050	23441	43736	186.0	73	15	15326	20.83	379	5	ND	1	27	552	117	4	64	2.13	.029	3	121	.96	16	.01	5	2.04	.01	.20	2	640
8804 CHS 164A	3	950	24187	63462	168.9	15	20	7258	15.09	169	6	ND	1	19	897	105	13	53	1.24	.021	3	23	.88	20	.02	2	2.39	.01	.23	4	91
8804 CHS 165	1	163	4941	16686	49.2	6	5	67518	9.00	5982	7	ND	5	35	154	824	18	18	6.68	.035	3	67	.45	43	.01	2	.54	.01	.18	1	33
8804 CHS 165A	4	668	22459	19232	256.5	16	15	12398	14.95	523	7	ND	1	23	212	152	3	88	1.49	.035	4	16	1.64	16	.05	2	3.94	.01	.25	1	48
8804 CHS 166	2	1364	22134	42536	325.1	174	16	6906	20.99	534	5	ND	1	6	580	425	20	12	.82	.015	2	35	.10	8	.01	2	.26	.01	.16	1	2190
8804 CHS 167	1	2387	24736	59272	289.8	178	22	16570	19.91	338	5	ND	1	3	897	698	14	32	.54	.019	2	146	.30	8	.01	2	.78	.01	.17	3	690
8804 CHS 168	1	1767	25298	59999	258.5	51	32	7906	13.78	741	5	ND	1	2	2335	399	2	30	.16	.035	2	109	.38	10	.01	2	.93	.01	.17	4	77
8804 CHS 169	1	1315	31456	46065	269.4	39	14	33773	14.09	1947	5	ND	1	37	714	975	12	22	.13	.030	3	15	.12	39	.01	4	.80	.01	.20	2	37
8804 CHS 170	3	404	21239	18051	75.7	15	14	5550	9.39	1216	5	ND	1	6	207	65	8	20	.22	.094	6	9	.15	36	.01	2	.73	.01	.26	1	19
8804 CHS 171	3	3535	25777	52295	263.3	49	28	6255	12.43	1298	5	ND	1	8	802	541	10	53	.28	.053	7	16	.67	28	.01	2	1.62	.01	.21	2	16
8804 CHS 172	2	1720	28032	50985	150.1	139	191	5904	23.29	17292	6	2	1	3	849	394	7	106	.09	.041	2	353	1.72	10	.01	10	3.29	.01	.13	2	1330
8804 CHS 173	4	281	27790	1773	100.3	72	238	3520	12.13	17370	5	ND	1	11	23	334	13	50	.21	.044	4	78	.75	20	.01	3	1.86	.01	.30	1	790
8804 CHS 174	1	28	667	1159	3.6	8	19	10365	6.76	701	5	ND	1	19	10	16	2	89	.94	.078	6	14	2.33	43	.01	3	3.58	.01	.20	1	2
8804 CHS 175	2	41	1894	3196	14.3	17	18	21992	9.65	642	5	ND	1	29	27	21	10	67	.37	.050	6	22	1.76	33	.01	2	3.68	.01	.15	1	1
8804 CHS 176	2	40	2520	5785	16.6	18	8	40428	6.25	639	5	ND	1	57	51	69	9	29	.62	.078	9	19	.20	38	.01	2	1.04	.01	.20	1	1
8804 CHS 177	4	31	172	556	1.0	17	6	4469	4.22	108	5	ND	1	7	5	9	8	33	.17	.040	10	10	.74	45	.01	6	1.56	.01	.23	1	1
8804 CHS 179	4	15	108	215	.8	42	28	12841	6.24	851	5	ND	1	13	2	4	5	54	.51	.091	26	37	.91	25	.01	2	2.50	.01	.21	1	8
STD C/AU-R	20	64	43	134	7.5	72	31	1158	4.29	44	17	8	40	52	19	17	23	60	.52	.083	40	60	.94	188	.07	34	1.98	.06	.15	12	520

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
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DATE RECEIVED: SEP 7 1988

DATE REPORT MAILED: *Sept. 20/88.*

ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK

ASSAYER: *C. Leong* D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

HARRISBURG DAYTON RES. CORP. PROJECT SUMMIT CAMP FILE # 88-3976R Page 1

SAMPLE#	Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T
8804 CHS 1	.19	11.29	16.71	19.55	.048
8804 CHS 1A	.05	1.79	2.47	3.68	.022
8804 CHS 3	.05	.47	.24	2.83	.001
8804 CHS 5	.20	2.27	4.76	1.79	.001
8804 CHS 8	.02	.31	.74	2.15	.001
8804 CHS 10	.06	2.86	2.39	4.66	.014
8804 CHS 11	.02	1.12	.42	2.61	.010
8804 CHS 12	.02	.27	.14	2.79	.027
8804 CHS 13	.04	1.96	1.64	2.44	.005
8804 CHS 14	.06	8.79	3.89	10.03	.023
8804 CHS 15	.02	.85	.28	2.07	.002
8804 CHS 16	.10	4.27	.70	33.98	.006
8804 CHS 17	.27	14.57	11.54	18.17	.072
8804 CHS 18	.95	18.57	5.29	32.33	.044
8804 CHS 19	.10	2.73	5.26	5.46	.024
8804 CHS 20	.91	15.18	13.68	49.55	.042
8804 CHS 21	.06	3.24	1.99	6.53	.038
8804 CHS 22	.13	4.71	3.67	6.61	.006
8804 CHS 23	.32	19.23	5.82	28.67	.057
8804 CHS 24	.11	3.14	9.50	13.56	.055
8804 CHS 26	.04	.75	.30	2.57	.001
8804 CHS 28	.01	.35	.24	2.00	.001
8804 CHS 31	.01	1.67	.57	2.64	.001
8804 CHS 33	.03	2.01	.61	2.88	.008
8804 CHS 34	.06	2.31	3.77	2.75	.008
8804 CHS 35	.29	16.55	12.66	59.20	.023
8804 CHS 36	.05	1.74	6.81	2.31	.006

SAMPLE#	Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T
8804 CHS 36A	.26	16.62	3.30	27.94	.068
8804 CHS 38	.14	9.36	3.16	25.75	.002
8804 CHS 39	.19	45.32	7.56	64.05	.031
8804 CHS 40	.11	7.23	2.60	9.65	.006
8804 CHS 41	.12	6.09	8.15	7.68	.011
8804 CHS 46	.01	1.36	.86	1.90	.004
8804 CHS 54	.05	3.80	.64	5.34	.004
8804 CHS 55	.07	29.36	1.36	39.49	.068
8804 CHS 56	.04	2.11	1.14	5.24	.004
8804 CHS 57	.12	8.84	3.13	24.07	.026
8804 CHS 58	.04	2.27	3.69	3.04	.003
8804 CHS 59	.04	1.27	.74	4.55	.002
8804 CHS 60	.04	8.65	6.18	8.12	.002
8804 CHS 61	.11	6.89	2.37	7.11	.014
8804 CHS 62	.06	11.40	8.14	11.87	.014
8804 CHS 63	.05	5.17	5.83	5.89	.002
8804 CHS 64	.06	2.46	3.64	1.55	.022
8804 CHS 65	.03	.58	2.26	1.52	.006
8804 CHS 66	.01	.66	1.79	1.15	.013
8804 CHS 69	.03	.48	4.91	.57	.008
8804 CHS 70	.04	.32	1.57	1.39	.010
8804 CHS 71	.02	.65	.68	1.61	.029

SAMPLE#	Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T
8804 CHS 72	.02	1.92	.16	2.93	.024
8804 CHS 74	.02	.89	.39	1.35	.021
8804 CHS 75	.10	13.74	.96	29.37	.029
8804 CHS 76	.02	.94	.16	2.32	.003
8804 CHS 76A	.05	.81	2.55	1.65	.029
8804 CHS 77	.01	.83	.82	2.19	.006
8804 CHS 78	.03	1.05	2.09	1.75	.011
8804 CHS 79	.03	1.86	.41	3.14	.007
8804 CHS 80	.11	4.33	3.20	7.63	.064
8804 CHS 81	.06	26.50	1.40	39.46	.042
8804 CHS 82	.06	3.56	.90	6.91	.013
8804 CHS 83	.11	4.07	3.37	14.40	.035
8804 CHS 84	.20	3.01	2.90	8.30	.018
8804 CHS 85	.03	1.91	.71	3.82	.014
8804 CHS 86	.28	3.28	3.55	6.04	.021
8804 CHS 87	.09	2.95	2.00	7.49	.018
8804 CHS 88	.06	23.94	.34	50.01	.095
8804 CHS 88A	.02	3.09	.21	7.34	.002
8804 CHS 89	.05	9.20	.30	25.28	.018
8804 CHS 90	.15	11.08	1.84	34.38	.024
8804 CHS 91	.13	14.04	4.73	17.43	.009
8804 CHS 92	.03	2.20	.41	6.97	.007
8804 CHS 93	.25	9.44	4.34	28.27	.048
8804 CHS 94	.19	4.51	5.87	11.57	.079
8804 CHS 95	.08	2.47	.70	6.96	.026
8804 CHS 96	.29	6.85	4.28	12.81	.008
8804 CHS 96A	.09	16.86	.31	31.87	.052
8804 CHS 97	.09	7.35	2.27	12.47	.021
8804 CHS 98	.07	2.71	9.27	5.74	.011
8804 CHS 99	.14	7.30	4.25	15.11	.047
8804 CHS 100	.12	1.04	9.84	4.98	.019
8804 CHS 101	.18	4.39	4.57	10.18	.047
8804 CHS 102	.30	8.22	6.08	13.62	.062
8804 CHS 103	.14	19.89	16.22	32.42	.024
8804 CHS 104	.09	3.27	4.29	6.55	.018

SAMPLE#	Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T
8804 CHS 105	.10	3.26	5.64	6.08	.043
8804 CHS 106	.02	.81	1.63	1.22	.001
8804 CHS 106A	.16	2.13	1.19	3.28	.005
8804 CHS 107A	.05	1.40	.89	3.41	.005
8804 CHS 108	.01	1.05	.62	1.25	.001
8804 CHS 109A	.03	.87	1.88	2.49	.001
8804 CHS 110	.12	3.25	1.57	29.21	.057
8804 CHS 110A	.06	2.27	.08	4.13	.010
8804 CHS 111	.02	.41	.32	2.54	.001
8804 CHS 111A	.04	1.29	.27	.51	.001
8804 CHS 112	.12	39.52	.18	45.36	.009
8804 CHS 113	.08	11.05	1.36	23.46	.006
8804 CHS 113A	.14	11.19	4.86	15.31	.011
8804 CHS 114	.05	2.55	.61	5.19	.002
8804 CHS 114A	.02	30.31	.07	43.36	.010
8804 CHS 114B	.06	.98	.13	8.91	.004
8804 CHS 115	.04	25.00	.22	27.57	.002
8804 CHS 115A	.05	1.46	3.37	2.07	.001
8804 CHS 116	.02	.62	.11	1.82	.001
8804 CHS 116A	.03	.71	.18	5.19	.003
8804 CHS 117	.26	38.19	3.10	74.03	.017
8804 CHS 118	.07	1.57	.66	2.61	.032
8804 CHS 119	.02	.60	.16	1.70	.013
8804 CHS 120	.29	51.58	1.45	119.80	.021
8804 CHS 121	.02	1.25	.36	2.36	.001
8804 CHS 122	.04	1.23	.08	1.94	.036
8804 CHS 123	.01	.59	.72	1.17	.004
8804 CHS 123A	.09	6.50	4.23	7.41	.004
8804 CHS 124	.05	3.28	.53	3.86	.045
8804 CHS 125	.02	2.22	.10	4.97	.026
8804 CHS 126	.17	4.53	5.05	10.07	.014
8804 CHS 127	.01	.58	.39	.78	.074
8804 CHS 128	.11	9.78	22.99	22.35	.047

SAMPLE#	Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T
8804 CHS 130	.02	2.05	.58	3.45	.011
8804 CHS 132	.02	.59	.14	3.88	.005
8804 CHS 133	.01	6.82	.09	10.75	.018
8804 CHS 134	.04	2.70	1.93	8.29	.008
8804 CHS 136	.03	3.47	2.90	5.33	.002
8804 CHS 137	.05	7.04	1.16	10.38	.019
8804 CHS 138	.01	2.96	.42	3.52	.001
8804 CHS 140	.02	1.12	.34	2.54	.001
8804 CHS 141	.02	1.86	.42	3.56	.001
8804 CHS 142	.08	5.24	3.38	20.75	.031
8804 CHS 143	.02	.67	.34	1.29	.002
8804 CHS 144	.26	12.96	8.93	13.96	.003
8804 CHS 145	.09	5.11	3.51	6.77	.001
8804 CHS 146	.20	8.11	6.85	18.89	.001
8804 CHS 147	.23	28.60	3.30	24.34	.004
8804 CHS 148	.09	3.75	9.58	5.29	.001
8804 CHS 149	.03	1.12	.45	1.21	.001
8804 CHS 150	.02	.29	.61	1.83	.001
8804 CHS 153	.04	1.02	2.01	5.10	.001
8804 CHS 154	.03	.71	1.49	3.76	.001
8804 CHS 155	.02	.93	2.23	1.87	.002
8804 CHS 156	.12	5.35	7.54	10.72	.003
8804 CHS 157	.13	6.71	5.74	7.83	.006
8804 CHS 158	.18	8.19	6.00	36.51	.018
8804 CHS 159	.17	5.89	4.99	13.75	.010
8804 CHS 160	.09	16.72	4.65	19.02	.005
8804 CHS 161	.09	7.55	9.93	18.57	.006
8804 CHS 162	.21	34.96	7.37	60.28	.003
8804 CHS 162A	.04	1.07	8.00	1.47	.001
8804 CHS 163	.31	15.31	4.30	18.33	.003

SAMPLE#		Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T
8804	CHS 163A	.20	15.58	7.48	11.61	.001
8804	CHS 163B	.03	2.39	2.30	1.66	.001
8804	CHS 164	.18	2.22	5.86	4.57	.025
8804	CHS 164A	.09	4.60	8.26	4.23	.003
8804	CHS 165	.02	.58	2.19	1.51	.003
8804	CHS 165A	.06	6.71	2.41	6.60	.002
8804	CHS 166	.12	10.25	5.38	11.74	.144
8804	CHS 167	.21	22.13	7.34	23.53	.026
8804	CHS 168	.19	13.62	19.39	14.02	.006
8804	CHS 169	.11	27.00	5.29	26.70	.001
8804	CHS 170	.03	1.56	1.88	1.82	.001
8804	CHS 171	.32	22.90	5.95	19.17	.001
8804	CHS 172	.16	2.37	6.59	3.52	.033
8804	CHS 173	.02	3.18	.20	2.48	.024

Summit Trench

	Cm	Cu %	WT.AV %	Pb %	WT.AV %	Zn %	WT.AV %	Ag oz/ton	WT.AV oz/ton	Au oz/ton	WT.AV oz/ton
1	51	0.19	0.097	11.29	5.76	16.71	8.52	19.55	9.97	0.048	0.0245
1 A	133	0.05	0.067	1.79	2.38	2.47	3.29	3.68	4.89	0.022	0.0293
3	25	0.05	0.013	0.47	0.12	0.24	0.06	2.83	0.71	0.001	0.0003
5	9	0.20	0.018	2.27	0.20	4.76	0.43	1.79	0.16	0.001	0.0001
8	9	0.02	0.002	0.31	0.03	0.74	0.07	2.15	0.19	0.001	0.0001
10	18	0.06	0.011	2.86	0.51	2.39	0.43	4.66	0.84	0.014	0.0025
11	33	0.02	0.007	1.12	0.37	0.42	0.14	2.61	0.86	0.010	0.0033
12	47	0.02	0.009	0.27	0.13	0.14	0.07	2.79	1.31	0.027	0.0127
13	47	0.04	0.019	1.96	0.92	1.64	0.77	2.44	1.15	0.005	0.0024
14	23	0.06	0.014	8.79	2.02	3.89	0.89	10.03	2.31	0.023	0.0053
15	53	0.02	0.011	0.35	0.45	0.28	0.15	2.07	1.10	0.002	0.0011
16	57	0.10	0.057	4.27	2.43	0.70	0.40	33.98	19.37	0.006	0.0034
17	13	0.27	0.035	14.57	1.89	11.54	1.50	18.17	2.36	0.072	0.0094
18	17	0.95	0.162	18.57	3.16	5.29	0.90	32.33	5.50	0.044	0.0075
19	60	0.10	0.060	2.73	1.64	5.26	3.16	5.46	3.28	0.024	0.0144
20	27	0.91	0.246	15.18	4.10	13.68	3.69	49.55	13.38	0.042	0.0113
21	21	0.06	0.013	3.24	0.68	1.99	0.42	6.53	1.37	0.038	0.0080
22	56	0.13	0.073	4.71	2.64	3.67	2.06	6.61	3.70	0.006	0.0034
23	44	0.32	0.141	19.23	8.46	5.82	2.56	28.67	12.61	0.057	0.0251
24	24	0.11	0.026	3.14	0.75	9.50	2.28	13.56	3.25	0.055	0.0132
26	10	0.04	0.004	0.75	0.08	0.30	0.03	2.57	0.26	0.001	0.0001
28	20	0.01	0.002	0.35	0.07	0.24	0.05	2.00	0.40	0.001	0.0002
31	10	0.01	0.001	1.67	0.17	0.57	0.06	2.64	0.26	0.001	0.0001
33	18	0.03	0.005	2.01	0.36	0.61	0.11	2.88	0.52	0.008	0.0014
34	28	0.06	0.017	2.31	0.65	3.77	1.06	2.75	0.77	0.008	0.0022
35	15	0.29	0.044	16.55	2.48	12.66	1.90	59.20	8.88	0.023	0.0035
36	42	0.05	0.021	1.74	0.73	6.81	2.86	2.31	0.97	0.006	0.0025
36 A	23	0.26	0.060	16.62	3.82	3.30	0.76	27.94	6.43	0.068	0.0156
38	34	0.14	0.048	9.36	3.18	3.16	1.07	25.75	8.76	0.002	0.0007
39	120	0.19	0.228	45.32	54.38	7.56	9.07	64.05	76.86	0.031	0.0372
40	125	0.11	0.138	7.23	9.04	2.60	3.25	9.65	12.06	0.006	0.0075
41	35	0.12	0.042	6.09	2.13	8.15	2.85	7.68	2.69	0.011	0.0039
46	6	0.01	0.001	1.36	0.08	0.86	0.05	1.90	0.11	0.004	0.0002
54	30	0.05	0.015	3.80	1.14	0.64	0.19	5.34	1.60	0.004	0.0012
55	23	0.07	0.016	29.36	6.75	1.36	0.31	39.49	9.08	0.068	0.0156
56	30	0.04	0.012	2.11	0.63	1.14	0.34	5.24	1.57	0.004	0.0012
57	43	0.12	0.052	8.84	3.80	3.13	1.35	24.07	10.35	0.026	0.0112
58	45	0.04	0.018	2.27	1.02	3.69	1.66	3.04	1.37	0.003	0.0014
59	53	0.04	0.021	1.27	0.67	0.74	0.39	4.55	2.41	0.002	0.0011
60	27	0.04	0.011	8.65	2.34	6.18	1.67	8.12	2.19	0.002	0.0005
61	56	0.11	0.062	6.89	3.86	2.37	1.33	7.11	3.98	0.014	0.0078
62	48	0.06	0.029	11.40	5.47	8.14	3.91	11.87	5.70	0.014	0.0067
63	39	0.05	0.020	5.17	2.02	5.83	2.27	5.89	2.30	0.002	0.0008
64	35	0.06	0.021	2.46	0.86	3.64	1.27	1.55	0.54	0.022	0.0077
65	90	0.03	0.027	0.58	0.52	2.26	2.03	1.52	1.37	0.006	0.0054
66	73	0.01	0.007	0.66	0.48	1.79	1.31	1.15	0.84	0.013	0.0095
69	120	0.03	0.036	0.48	0.58	4.91	5.89	0.57	0.68	0.008	0.0096
70	150	0.04	0.060	0.32	0.48	1.57	2.36	1.39	2.09	0.010	0.0150
71	139	0.02	0.028	0.65	0.90	0.68	0.95	1.61	2.24	0.029	0.0403
72	140	0.02	0.028	1.22	2.69	0.16	0.22	2.93	4.10	0.024	0.0336
74	63	0.02	0.013	0.89	0.56	0.39	0.25	1.35	0.85	0.021	0.0132
75	40	0.10	0.040	13.74	5.50	0.96	0.38	29.37	11.75	0.029	0.0116
76	169	0.02	0.034	0.94	1.59	0.16	0.27	2.32	3.42	0.003	0.0051
76 A	71	0.05	0.036	0.81	0.58	2.55	1.81	1.65	1.17	0.029	0.0206
77	114	0.01	0.011	0.83	0.95	0.82	0.93	2.19	2.50	0.006	0.0068

78	114	0.03	0.034	1.05	1.20	2.09	2.38	1.75	2.00	0.011	0.0125
79	200	0.03	0.060	1.86	3.72	0.41	0.82	3.14	6.28	0.007	0.0140
80	134	0.11	0.147	4.33	5.80	3.20	4.29	7.63	10.22	0.064	0.0858
81	95	0.06	0.057	26.50	25.18	1.40	1.33	39.46	37.49	0.042	0.0399
82	102	0.06	0.061	3.56	3.63	0.90	0.92	6.91	7.05	0.013	0.0133
83	120	0.11	0.132	4.07	4.88	3.37	4.04	14.40	17.28	0.035	0.0420
84	162	0.20	0.324	3.01	4.88	2.90	4.70	8.30	13.45	0.018	0.0292
85	260	0.03	0.078	1.91	4.97	0.71	1.85	3.82	9.93	0.014	0.0364
86	263	0.28	0.736	3.28	8.63	3.55	9.34	6.04	15.89	0.021	0.0552
87	430	0.09	0.387	2.95	12.69	2.00	8.60	7.49	32.21	0.018	0.0774
88	55	0.06	0.033	23.94	13.17	0.34	0.19	50.01	27.51	0.095	0.0523
88 A	300	0.02	0.060	3.09	9.27	0.21	0.63	7.34	22.02	0.002	0.0060
89	360	0.05	0.180	9.20	33.12	0.30	1.08	25.28	91.01	0.018	0.0648
90	62	0.15	0.093	11.08	6.87	1.84	1.14	34.38	21.32	0.024	0.0149
91	51	0.13	0.066	14.04	7.16	4.73	2.41	17.43	8.89	0.009	0.0046
92	297	0.03	0.089	2.20	6.53	0.41	1.22	6.97	20.70	0.007	0.0208
93	180	0.25	0.450	9.44	16.99	4.34	7.81	28.27	50.89	0.048	0.0864
94	137	0.19	0.260	4.51	6.18	5.87	8.04	11.57	15.85	0.079	0.1082
95	120	0.08	0.096	2.47	2.96	0.70	0.84	6.96	8.35	0.026	0.0312
96	25	0.29	0.073	6.85	1.71	4.28	1.07	12.81	3.20	0.008	0.0020
96 A	36	0.09	0.032	16.86	6.07	0.31	0.11	31.87	11.47	0.052	0.0187
97	169	0.09	0.152	7.35	12.42	2.27	3.84	12.47	21.07	0.021	0.0355
98	120	0.07	0.084	2.71	3.25	9.27	11.12	5.74	6.89	0.011	0.0132
99	42	0.14	0.059	7.30	3.07	4.25	1.79	15.11	6.35	0.047	0.0197
100	47	0.12	0.056	1.04	0.49	9.84	4.62	4.98	2.34	0.019	0.0089
101	79	0.18	0.142	4.39	3.47	4.57	3.61	10.18	8.04	0.047	0.0371
102	25	0.30	0.075	8.22	2.06	6.08	1.52	13.62	3.41	0.062	0.0155
103	33	0.14	0.046	19.89	6.56	16.22	5.35	32.42	10.70	0.024	0.0079
104	30	0.09	0.027	3.27	0.98	4.29	1.29	6.55	1.97	0.018	0.0054
105	112	0.10	0.112	3.26	3.65	5.64	6.32	6.08	6.81	0.043	0.0482
106	15	0.02	0.003	0.81	0.12	1.63	0.24	1.22	0.18	0.001	0.0002
106 A	24	0.16	0.038	2.13	0.51	1.19	0.29	3.28	0.79	0.005	0.0012
107 A	60	0.05	0.030	1.40	0.84	0.89	0.53	3.41	2.05	0.005	0.0030
108	25	0.01	0.003	1.05	0.26	0.62	0.16	1.25	0.31	0.001	0.0003
109 A	60	0.03	0.018	0.87	0.52	1.88	1.13	2.49	1.49	0.001	0.0006
110	30	0.12	0.036	3.25	0.98	1.57	0.47	29.21	8.76	0.057	0.0171
110 A	32	0.06	0.019	2.27	0.73	0.08	0.03	4.13	1.32	0.010	0.0032
111	36	0.02	0.007	0.41	0.15	0.32	0.12	2.54	0.91	0.001	0.0004
111 A	46	0.04	0.018	1.29	0.59	0.27	0.12	0.51	0.23	0.001	0.0005
112	49	0.12	0.059	39.52	19.36	0.18	0.09	45.36	22.23	0.009	0.0044
113	57	0.08	0.046	11.05	6.30	1.36	0.78	23.46	13.37	0.006	0.0034
113 A	46	0.14	0.064	11.19	5.15	4.86	2.24	15.31	7.04	0.011	0.0051
114	18	0.05	0.009	2.55	0.46	0.61	0.11	5.19	0.93	0.002	0.0004
114 A	13	0.02	0.003	30.31	3.94	0.07	0.01	43.36	5.64	0.010	0.0013
114 B	28	0.06	0.017	0.98	0.27	0.13	0.04	8.91	2.49	0.004	0.0011
115	37	0.04	0.015	25.00	9.25	0.22	0.08	27.57	10.20	0.002	0.0007
115 A	17	0.05	0.009	1.46	0.25	3.37	0.57	2.07	0.35	0.001	0.0002
116	21	0.02	0.004	0.62	0.13	0.11	0.02	1.82	0.38	0.001	0.0002
116 A	17	0.03	0.005	0.71	0.12	0.18	0.03	5.19	0.88	0.003	0.0005
117	178	0.26	0.463	38.19	67.98	3.10	5.52	74.03	131.77	0.017	0.0303
118	30	0.07	0.021	1.57	0.47	0.66	0.20	2.61	0.78	0.032	0.0096
119	15	0.02	0.003	0.60	0.09	0.16	0.02	1.70	0.26	0.013	0.0020
120	40	0.29	0.116	51.58	20.63	1.45	0.58	119.80	47.92	0.021	0.0084
121	16	0.02	0.003	1.25	0.20	0.36	0.06	2.36	0.38	0.001	0.0002
122	18	0.04	0.007	1.23	0.22	0.08	0.01	1.94	0.35	0.036	0.0065
123	6	0.01	0.001	0.59	0.04	0.72	0.04	1.17	0.07	0.004	0.0002
123 A	15	0.09	0.014	6.50	0.98	4.23	0.63	7.41	1.11	0.004	0.0006
124	45	0.05	0.023	3.28	1.48	0.53	0.24	3.86	1.74	0.045	0.0203
125	24	0.02	0.005	2.22	0.53	0.10	0.02	4.97	1.19	0.026	0.0062
126	47	0.17	0.080	4.53	2.13	5.05	2.37	10.07	4.73	0.014	0.0066

127	11	0.01	0.001	0.58	0.06	0.39	0.04	0.78	0.09	0.074	0.0081
128	30	0.11	0.033	9.78	2.93	22.99	6.90	22.35	6.71	0.047	0.0141
130	38	0.02	0.008	2.05	0.78	0.58	0.22	3.45	1.31	0.011	0.0042
132	23	0.02	0.005	0.59	0.14	0.14	0.03	3.88	0.89	0.005	0.0012
133	24	0.01	0.002	6.82	1.64	0.09	0.02	10.75	2.58	0.018	0.0043
134	44	0.04	0.018	2.70	1.19	1.93	0.85	8.29	2.65	0.008	0.0035
136	17	0.03	0.005	3.47	0.59	2.90	0.49	5.33	0.91	0.002	0.0003
137	10	0.05	0.005	7.04	0.70	1.16	0.12	10.38	1.04	0.019	0.0019
138	8	0.01	0.001	2.96	0.24	0.42	0.03	3.52	0.28	0.001	0.0001
140	40	0.02	0.008	1.12	0.45	0.34	0.14	2.54	1.02	0.001	0.0004
141	100	0.02	0.020	1.86	1.86	0.42	0.42	3.56	3.56	0.001	0.0010
142	70	0.08	0.056	5.24	3.67	3.38	2.37	20.75	14.53	0.031	0.0217
143	100	0.02	0.020	0.67	0.67	0.34	0.34	1.29	1.29	0.002	0.0020
			0.061		4.2214		1.6950		8.5012		0.0131
		0.95		51.58		22.99		119.80		0.095	

	Cm	Cu	WT.AV	Pb	WT.AV	Zn	WT.AV	Ag	WT.AV	Au	WT.AV
		%	%	%	%	%	%	oz/ton	oz/ton	oz/ton	oz/ton
144	40	0.26	0.10	12.96	5.18	8.93	3.57	13.96	5.58	0.003	0.0012
145	43	0.09	0.04	5.11	2.20	3.51	1.51	6.77	2.91	0.001	0.0004
146	140	0.20	0.28	8.11	11.35	6.85	9.59	18.89	26.45	0.001	0.0014
147	56	0.23	0.13	28.60	16.02	3.30	1.85	24.34	13.63	0.004	0.0022
148	37	0.09	0.03	3.75	1.39	9.58	3.54	5.29	1.96	0.001	0.0004
149	31	0.03	0.01	1.12	0.35	0.45	0.14	1.21	0.38	0.001	0.0003
150	22	0.02	0.00	0.29	0.06	0.61	0.13	1.83	0.40	0.001	0.0002
153	12	0.04	0.00	1.02	0.12	2.01	0.24	5.10	0.61	0.001	0.0001
154	16	0.03	0.00	0.71	0.11	1.49	0.24	3.76	0.60	0.001	0.0002
155	9	0.02	0.00	0.93	0.08	2.23	0.20	1.87	0.17	0.002	0.0002
156	16	0.12	0.02	5.35	0.86	7.54	1.21	10.72	1.72	0.003	0.0005
157	11	0.13	0.01	6.71	0.74	5.74	0.63	7.83	0.86	0.006	0.0007
158	7	0.18	0.01	8.19	0.57	6.00	0.42	36.51	2.56	0.018	0.0013
159	30	0.17	0.05	5.89	1.77	4.99	1.50	13.75	4.13	0.010	0.0030
160	25	0.09	0.02	16.72	4.18	4.65	1.16	19.02	4.76	0.005	0.0013
161	10	0.09	0.01	7.55	0.76	9.93	0.99	18.57	1.86	0.006	0.0006
162	10	0.21	0.02	34.96	3.50	7.37	0.74	60.28	6.03	0.003	0.0003
162 A	3	0.04	0.00	1.07	0.03	8.00	0.24	1.47	0.04	0.001	0.0000
163	14	0.31	0.04	15.31	2.14	4.30	0.60	18.33	2.57	0.003	0.0004
163 A	10	0.20	0.02	15.58	1.56	7.48	0.75	11.61	1.16	0.001	0.0001
163 B	18	0.03	0.01	2.39	0.43	2.30	0.41	1.66	0.30	0.001	0.0002
164	49	0.18	0.09	2.22	1.09	5.86	2.87	4.57	2.24	0.025	0.0123
164 A	18	0.09	0.02	4.60	0.83	8.26	1.49	4.23	0.76	0.003	0.0005
165	23	0.02	0.00	0.58	0.13	2.19	0.50	1.51	0.35	0.003	0.0007
165 A	22	0.06	0.01	6.71	1.48	2.41	0.53	6.60	1.45	0.002	0.0004
166	20	0.12	0.02	10.25	2.05	5.38	1.08	11.74	2.35	0.144	0.0288
167	57	0.21	0.12	22.13	12.61	7.34	4.18	23.53	13.41	0.026	0.0148
168	46	0.19	0.09	13.62	6.27	19.39	8.92	14.02	6.45	0.006	0.0028
169	58	0.11	0.06	27.00	15.66	5.29	3.07	26.70	15.49	0.001	0.0006
170	57	0.03	0.02	1.56	0.89	1.88	1.07	1.82	1.04	0.001	0.0006
171	10	0.32	0.03	22.90	2.29	5.95	0.60	19.17	1.92	0.001	0.0001
172	23	0.16	0.04	2.37	0.55	6.59	1.52	3.52	0.81	0.033	0.0076
173	17	0.02	0.00	3.18	0.54	0.20	0.03	2.48	0.42	0.024	0.0041
			0.0404		2.9629		1.6825		3.7980		0.0026
		0.32		34.96		19.39		60.28		0.144	

APPENDIX IV

Petrographic Descriptions of 6 Rock
Specimens from Summit Camp

Arsenopyrite forms euhedral crystals up to 2 mm across at the edge of the vein and in the altered wall-rock. It shows typical weak pale purple-brown to bluish anisotropism.

The silicate, or gangue, minerals are mostly quartz, but with a remnant texture that suggest they were partly formed after feldspar: near the sulfides, the quartz is water-clear, with no inclusions, but farther away, it is extremely cloudy, as if it had replaced feldspar. Also, interstitial areas of fine sericite flakes are probably

SAMPLE S-1: VEIN AND HIGHLY SULFIDIZED VEIN MARGIN

Section across a vein margin that includes virtually massive, intergrown, coarse sulfides: pyrrhotite, sphalerite, and galena. Euhedral grains of arsenopyrite are also present. Altered wallrock looks granitic in origin, but now is intensely silicified and sericitized. In polished thin section, the mineral abundances are:

Opagues:

Pyrrhotite (altered)		50%
Includes: Marcasite	20%	
Limonite	5%	
Pyrite	5%	
Galena		10%
Sphalerite		10%
Arsenopyrite		5%
Chalcopyrite		<1%

Ganques:

Quartz		20%
Sericite		5%
Epidote (?)		<1%

Massive pyrrhotite, in coarse anhedral masses up to several centimeters across, but composed of smaller grains several millimeters across, formed the bulk of the vein before incipient alteration (oxidation) to typical "bird's-eye" or lamellar pyrite and marcasite. There is also limonite (probably goethite, to judge by the brown internal reflections) included in the oxidation products of the pyrrhotite. In detail, the pyrrhotite is only left as kernels up to about 1 mm across, which show progressive outward rims of: (1) dark gangue or possibly simply a void; (2) marcasite; (3) limonite; and (4) pyrite. The marcasite is distinguished by strong anisotropism in pale blue to straw-yellow, while the pyrite is pale blue to

SAMPLE S-2: HIGHLY ALTERED VEIN MARGIN IN DIORITIC ROCK

The vein portion of this sample is somewhat like that of S-1: massive sphalerite, as coarse grains up to over a centimeter across. The disseminated euhedral arsenopyrite in the altered wall-rock is also similar, but the alteration is much less intense, so that a dark green altered dioritic rock is visible. The sphalerite is cut by thin veinlets of pyrite, as in S-1, and then both are cut by a 2mm thick white calcite vein. The minerals recognized are:

Opagues:

Sphalerite	10%
Arsenopyrite	10%
Galena	5%
Chalcopyrite	1%
Pyrite	1%
Pyrrhotite	1%
Ruby silver (proustite-pyrargyrite)	tr

Ganques:

Sericite	30%
Quartz	25%
Carbonate (Calcite)	15%

The main mass of sphalerite is anhedral, and about 1-2 cm across. It is formed of grains a few millimeters across, and is strongly fractured. It has been cut by thin pyrite veinlets. The sphalerite is similar to that in S-1, with bright red internal reflections and chalcopyrite disease.

Arsenopyrite grains are euhedral, about 1 mm across, and strongly associated with intensely sericitized areas of the wall rock.

Galena and chalcopyrite seem to be more associated with the quartz (?vein) areas of the slide. They form relatively fine grained anhedral masses up to 1 mm across, with a somewhat interstitial texture. It is with these masses (accompanied by traces of pyrrhotite) that the ruby silver is associated. It forms fine anhedral grains up to 0.2 mm across. It is not sure whether it is proustite (the arsenic end-member) or pyrargyrite (the antimony end-member) but with so much arsenopyrite in the sample, proustite is the more likely, and would then contain about 70% silver.

The altered wall-rock is made up of fairly coarse quartz grains, about 0.5 to 1 mm across, some with the same bladed form as in S-1. There are much more abundant patches of sericite (possibly after plagioclase in an originally ?dioritic rock, although these areas are very dark in hand specimen, suggesting sericitized biotite or perhaps merely iron-stained sericite). Sericite forms small radiating rosettes of flakes, up to 0.2 mm across. The other major gangue mineral, both as pervasive replacements of the wall rock and as veins visible in the hand specimen, is carbonate that reacts freely to cold dilute HCl and must be calcite. It forms grains up to 0.5 mm across in the wall rock, coarser in the vein.

SAMPLE S-3: MASSIVE SPHALERITE VEIN WITH ALTERED WALL ROCK

Very much like the first two samples (S-1 and 2), with a massive sphalerite section (vein) and strongly arsenopyritized margin. The mineral recognizable in polished thin section are:

Opagues:

Sphalerite	20%
Arsenopyrite	10%
Galena	2%
Chalcopyrite	1%
Pyrite	1%

Ganques:

Quartz	35%
Sericite	20%
Carbonate (Calcite)	10%

The sphalerite forms large anhedral grains over a centimeter across, some of which are coarsely twinned (see cut slab). They have the same red internal reflections as in S-1 and 2.

Arsenopyrite, as in the other samples, is found as euhedral crystals about 1 to 2 mm across and almost always surrounded by sericitized areas of wall rock, although they occasionally are included in sphalerite.

Galena is present as rare anhedral masses less than a millimeter across, usually interstitial to the quartz. The galena is marked by curving rows of cleavage pits, indicating late deformation of the galena.

Chalcopyrite is restricted to the minute (20-20 microns) blebs included in sphalerite. This "chalcopyrite disease" is found mainly at the margins of the large sphalerite grains.

No silver-bearing minerals were observed in this sample.

The wall rock is made up of quartz, with the same clear bladed grains, up to 2 mm long, near sulfides and cloudy aggregates of smaller grains elsewhere that may replace former feldspars. Former mafic grains are apparently replaced by sericite and carbonate (calcite), since the dark colouration in the flaky mineral can be seen to be due to partially sericitized biotite in this sample. That is to say, it retains some of its brownish pleochroism in "clots", especially near the sulfides.

SAMPLE S-4: MASSIVE SULFIDE REPLACEMENT OF DIORITIC ROCK

Almost like a sulfide-rich breccia, with areas of intensely wall rock amongst semi-massive sulfides, with white calcite rims to the sulfide areas, rather like reaction rims. Patches of altered pyrrhotite, up to 1-2 cm across, and similar sized areas of sphalerite and galena, with areas of wall rock that look like fragments. Massive replacement by euhedral arsenopyrite in places. In polished thin section, the mineralogy is:

Opaques:

Arsenopyrite	30%
Sphalerite	15%
Galena	15%
Pyrrhotite (altered)	5%
(includes Marcasite 2%)	
Chalcopyrite	2%
limonite	2%
Ruby silver	tr

Ganques:

Quartz	15%
Sericite (including altered biotite)	10%
Carbonate (Calcite)	5%

Coarse, intergrown sphalerite and galena are mixed with areas of euhedral arsenopyrite crystals, and smaller areas of chalcopyrite. Irregular masses of pyrrhotite contain small blebs of chalcopyrite.

The pyrrhotite is altered to the same mixture of lamellar marcasite and pyrite as detailed in S-1. Most of the minor limonite is due to oxidation of this pyrrhotite. These chalcopyrite blebs are of the order of a millimeter across. It is with these (?) that the minor amounts of ruby silver (proustite-pyrrargyrite) are apparently associated.

The ruby silver displays characteristic ruby-red internal reflections, and forms grains up to 0.1 mm across. They appear rounded and would liberate easily.

Arsenopyrite forms euhedral crystal grains to about 3-4 mm across with typical rhomb shapes. No inclusions of precious-metal bearing phases were seen in the arsenopyrite.

The flaky gangue mineral appears to be altered biotite, either sericitized or chloritized. The mineral that closely surrounds the arsenopyrite in this sample is carbonate (calcite, by its reaction to HCl). It is very fine-grained, averaging about 0.02 mm across. Quartz forms much larger, euhedral (hexagonal outlined) crystals up to about 1 mm across.

SAMPLE S-5: MASSIVE SULFIDES (REPLACEMENT)

Basically all sulfides, practically massive galena. No gangues except for traces of quartz and carbonate. All sulfides are cut by limonitic fractures or veins up to almost 1 mm across. The assemblage is the same as in S-4: very coarse anhedral grains of sphalerite and galena up to several centimeters across, with interstitial areas of "bird's-eye" marcasite and pyrite after original pyrrhotite. The mineralogy in polished thin section is as follows:

Opagues:

Galena	50%
Sphalerite	20%
Pyrrhotite (altered)	25%
(now includes Marcasite 15%)	
Pyrite	5%
Limonite	5%
Chalcopyrite	2%
Ruby silver (proustite-pyrargyrite)	tr
Tetrahedrite	tr
Unidentified pinkish mineral	tr

Gaugues:

Quartz	2%
Carbonate	1%

Large masses of pyrrhotite are altered to the typical mixture of marcasite and pyrite. They are up to 2 cm across, with fine (0.5 to 1 mm) inclusions of chalcopyrite. Rare tiny grains of ruby silver are associated with these chalcopyrite, especially where near boundaries with grains of sphalerite and/or galena. In these locations also are even finer (0.05 mm) inclusions of tetrahedrite in the chalcopyrite, and nearby in the galena, a distinctly pinkish, almost isotropic mineral that remains unidentified without study by SEM (scanning electron microscope).

The sphalerite and galena form large rounded anhedral crystals up to 1-2 cm and over 5 cm, respectively. The sphalerite displays brown internal reflections and chalcopyrite disease, while the galena is massive. Both are cut by thin limonitic veinlets, one of which also contains a few small grains (0.05 mm by 0.15 mm) of ruby silver.

Traces of gangue minerals are fine quartz (to 0.1 mm across) and carbonate of 0.03 mm diameter, the latter surrounding the opaque minerals. Carbonate also fills fractures in the opaques, especially galena.

SAMPLE 9-6: SEMI-MASSIVE REPLACEMENT OF ?DIORITIC ROCK

Almost massive arsenopyrite as aggregates to several centimeters across, formed of smaller grains of approximately 1 to 3 mm diameter, in a variably altered ?plutonic igneous host, possibly formerly dioritic in composition. Dark green patches of this former host suggest the presence of biotite or chlorite. Areas of coarse white calcite also are present, that react strongly to cold dilute HCl. There are also occasional small grains of sphalerite and galena, and minor chalcopyrite, visible in the hand specimen. In polished thin section, there are no other minerals observable than those seen in hand specimen:

Opagues:

Arsenopyrite	70%
Sphalerite	5%
Galena	3%
Chalcopyrite	<1%

Ganques:

Carbonate (Calcite)	10%
Quartz	5%
Biotite (partly sericitized)	5%
Sericite	2%

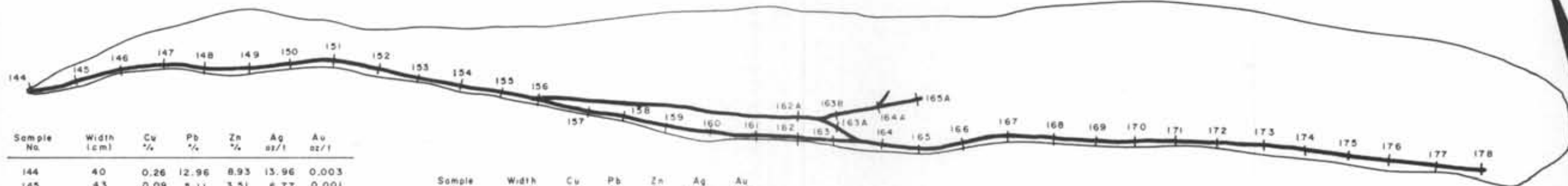
The arsenopyrite forms euhedral crystals, generally of about 1 mm diameter, with typical rhomb-shaped cross-sections. These grains commonly aggregate to masses that are several centimeters across. Coarser (2-3 mm) grains that also polish much better (they contain only rare inclusions of gangue, or holes) tend to be concentrated at the edges of the arsenopyrite masses, especially against the calcite areas. Sphalerite grains in the arsenopyrite are anhedral, up to almost a centimeter across, and show strong red-brown internal reflections. Some smaller grains are also present, in and around the calcite areas. Galena is present as small rounded blebs about 0.5 mm across, that again are present at the contact between the sulfide and calcite areas. Fine grains of chalcopyrite in these areas are only upto 0.2 mm across. They are also anhedral in character. No silver-bearing minerals (proustite-pyrargyrite or tetrahedrite-tennantite) were observed in this sample. No gold was seen in the arsenopyrite.

The white areas interstitial to the massive arsenopyrite areas are composed of fairly coarse-grained intermixed calcite and quartz grains, about 2-3 mm and 1 mm across respectively. Quartz crystals are clear (free of inclusions) and often euhedral, with hexagonal outlines.

The smaller darker patches in these areas are apparently somewhat altered biotite remnants. They display faint, but noticeable, brownish pleochroism, and moderate birefringence. They resemble amphibole except that the extinction is parallel, so a micaceous mineral is indicated. Parts that are lacking in pleochroism are probably more sericitized portions. The dark greenish colouration in hand specimen of these patches suggests derivation from a mafic plutonic igneous rock.

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Sample No.	Width (cm)	Cu %	Pb %	Zn %	Ag oz/t	Au oz/t
144	40	0.26	12.96	8.93	13.96	0.003
145	43	0.09	5.11	3.51	6.77	0.001
146	140	0.20	8.11	6.85	18.89	0.001
147	56	0.23	28.60	3.30	24.34	0.004
148	37	0.09	3.75	9.58	5.29	0.001
149	31	0.03	1.12	0.45	1.21	0.001
150	22	0.02	0.29	0.61	1.83	0.001
153	12	0.04	1.02	2.01	5.10	0.001
154	16	0.03	0.71	1.49	3.76	0.001
155	9	0.02	0.93	2.23	1.87	0.002
156	16	0.12	5.35	7.54	10.72	0.003
157	11	0.13	6.71	5.74	7.83	0.006
158	7	0.18	8.19	6.00	36.51	0.018
159	30	0.17	5.89	4.99	13.75	0.010
160	25	0.09	16.72	4.65	19.02	0.005
161	10	0.09	7.55	9.93	18.57	0.006
162	10	0.21	34.96	7.37	60.28	0.003
162A	3	0.04	1.07	8.00	1.47	0.001
163	14	0.31	15.31	4.30	18.33	0.003
163A	10	0.20	15.58	7.48	11.61	0.001
163B	18	0.03	2.39	2.30	1.66	0.001
164	49	0.18	2.22	5.86	4.57	0.025
164A	18	0.09	4.60	8.26	4.23	0.003

Sample No.	Width (cm)	Cu %	Pb %	Zn %	Ag oz/t	Au oz/t
165	23	0.02	0.58	2.19	1.51	0.003
165A	22	0.06	6.71	2.41	6.60	0.002
166	20	0.12	10.25	5.38	11.74	0.144
167	57	0.21	22.13	7.34	23.53	0.026
168	46	0.19	13.62	19.39	14.02	0.006
169	58	0.11	27.00	5.29	26.70	0.001
170	57	0.03	1.56	1.88	1.82	0.001
171	10	0.32	22.90	19.17	19.17	0.001
172	23	0.16	2.37	3.52	3.52	0.033
173	17	0.02	3.18	0.20	2.48	0.024



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INDIANA TRENCH

SUMMIT CAMP PROPERTY

Similkameen Mining Division

NTS: 92 H/6

October, 1988

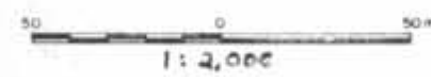
Figure 2

Geo Services Ltd.

Summit Shaft
Summit Trench

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**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

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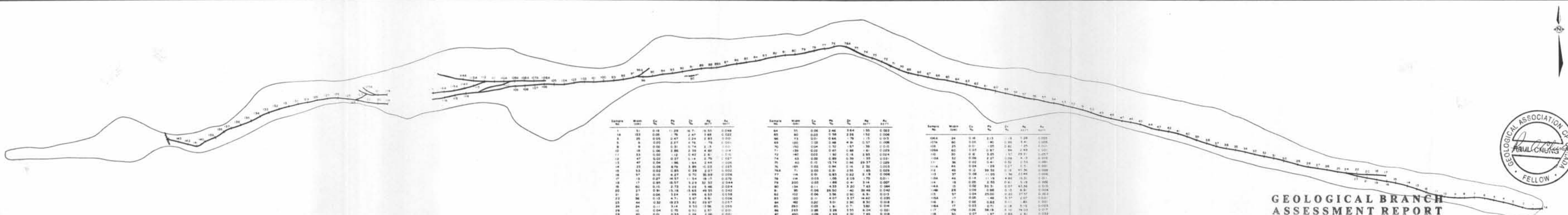
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SUMMIT CAMP PROPERTY

Similkameen Mining Division
NTS 92 H/R

October, 1968 Figure 1

Geo Services Ltd.



Sample No.	Width (cm)	Cu %	Pb %	Zn %	Ag (g/t)	Au (g/t)
1	51	0.18	1.28	16.71	19.55	0.048
18	133	0.05	1.76	2.47	1.88	0.022
2	25	0.05	0.47	2.24	2.81	0.010
5	9	0.00	2.47	4.78	7.8	0.004
8	9	0.00	0.31	0.74	1.15	0.010
10	18	0.06	2.86	2.39	4.66	0.014
17	53	0.02	1.12	0.82	2.81	0.010
19	47	0.02	0.57	0.14	2.79	0.017
15	47	0.04	1.86	1.64	2.44	0.005
14	23	0.06	8.79	3.89	5.23	0.023
10	53	0.02	0.85	0.28	2.07	0.002
18	57	0.10	4.27	0.72	20.88	0.006
17	13	0.27	14.57	11.54	18.17	0.072
18	17	0.39	18.57	12.29	37.37	0.044
16	60	0.10	2.73	1.29	5.46	0.024
20	27	0.31	15.18	11.63	49.51	0.042
21	21	0.06	3.24	1.99	6.33	0.018
22	36	0.12	4.71	2.67	16.51	0.004
44	42	0.32	18.23	13.92	29.97	0.017
24	24	0.17	3.14	0.50	13.96	0.010
28	10	0.04	0.70	0.50	0.57	0.001
29	20	0.01	0.35	0.24	0.90	0.001
31	10	0.01	1.87	0.84	0.87	0.002
33	18	0.03	2.07	0.61	2.88	0.008
34	28	0.06	2.37	3.77	2.70	0.008
35	15	0.29	14.55	12.66	59.80	0.023
36	42	0.00	1.74	0.81	2.51	0.006
38A	23	0.26	16.62	13.20	27.84	0.048
38	34	0.14	6.36	3.16	25.75	0.002
39	110	0.19	45.32	7.56	44.03	0.031
40	125	0.11	7.23	2.43	2.87	0.006
41	35	0.12	6.09	0.15	7.88	0.011
46	6	0.01	1.38	0.84	1.30	0.004
48	45	0.04	2.27	2.84	3.24	0.003
54	67	0.06	9.80	0.44	5.14	0.004
55	23	0.07	29.36	1.34	24.43	0.004
56	30	0.04	2.11	1.14	1.24	0.004
57	45	0.12	8.84	0.17	24.07	0.009
58	45	0.04	2.27	2.84	3.24	0.003
59	53	0.14	1.27	0.74	4.82	0.002
60	27	0.04	4.65	0.14	4.12	0.009
67	36	0.11	4.99	2.17	7.11	0.014
62	36	0.06	11.42	0.14	0.87	0.014
63	36	0.05	6.17	1.43	1.84	0.009

Sample No.	Width (cm)	Cu %	Pb %	Zn %	Ag (g/t)	Au (g/t)
64	55	0.06	2.46	3.64	1.50	0.002
65	80	0.03	0.58	2.28	1.52	0.006
66	73	0.01	0.68	7.9	1.75	0.013
68	190	0.00	0.88	4.84	0.57	0.008
70	150	0.04	0.57	1.57	3.39	0.010
71	139	0.02	0.67	0.88	1.61	0.029
72	140	0.02	1.92	0.18	2.93	0.024
74	63	0.02	0.89	0.59	1.27	0.017
75	40	0.10	13.74	0.46	29.37	0.029
76	189	0.02	0.94	0.18	2.33	0.003
76A	71	0.02	0.81	2.55	0.85	0.028
77	14	0.01	0.83	0.22	2.19	0.006
78	148	0.03	1.06	2.09	1.79	0.011
79	200	0.03	1.88	0.47	3.14	0.007
80	134	0.11	4.33	3.20	7.63	0.044
81	95	0.06	29.50	40	36.48	0.042
82	102	0.06	3.96	0.90	6.91	0.013
83	120	0.17	4.07	3.27	14.40	0.030
84	462	0.20	9.01	2.90	9.30	0.018
85	260	0.03	1.91	0.71	3.82	0.014
86	283	0.08	3.28	1.55	6.04	0.021
87	490	0.28	2.99	2.00	7.49	0.018
88	51	0.01	23.84	0.74	50.01	0.005
88A	300	0.02	3.09	0.21	7.34	0.002
89	820	0.05	9.20	0.30	27.29	0.018
90	42	0.15	11.06	1.84	34.36	0.024
91	61	0.13	18.04	4.73	17.43	0.008
92	297	0.03	2.20	0.47	8.57	0.007
93	180	0.20	9.44	0.94	22.27	0.048
94	137	0.19	4.91	0.87	11.57	0.076
95	130	0.08	2.47	0.70	6.96	0.006
96	25	0.29	6.85	4.28	12.81	0.008
96A	36	0.09	16.88	0.37	31.87	0.030
97	889	0.09	7.26	2.27	47.47	0.021
98	93	0.07	2.71	0.27	7.74	0.011
98	42	0.14	7.30	4.25	15.11	0.047
100	47	0.12	1.04	0.94	4.98	0.019
101	79	0.18	4.39	4.27	10.18	0.047
102	22	0.30	6.22	4.06	3.62	0.062
103	53	0.14	8.89	16.22	12.42	0.024
104	30	0.09	3.27	4.23	8.73	0.018
105	112	0.10	3.24	9.64	6.08	0.043
106	15	0.02	0.8	0.3	1.22	0.001

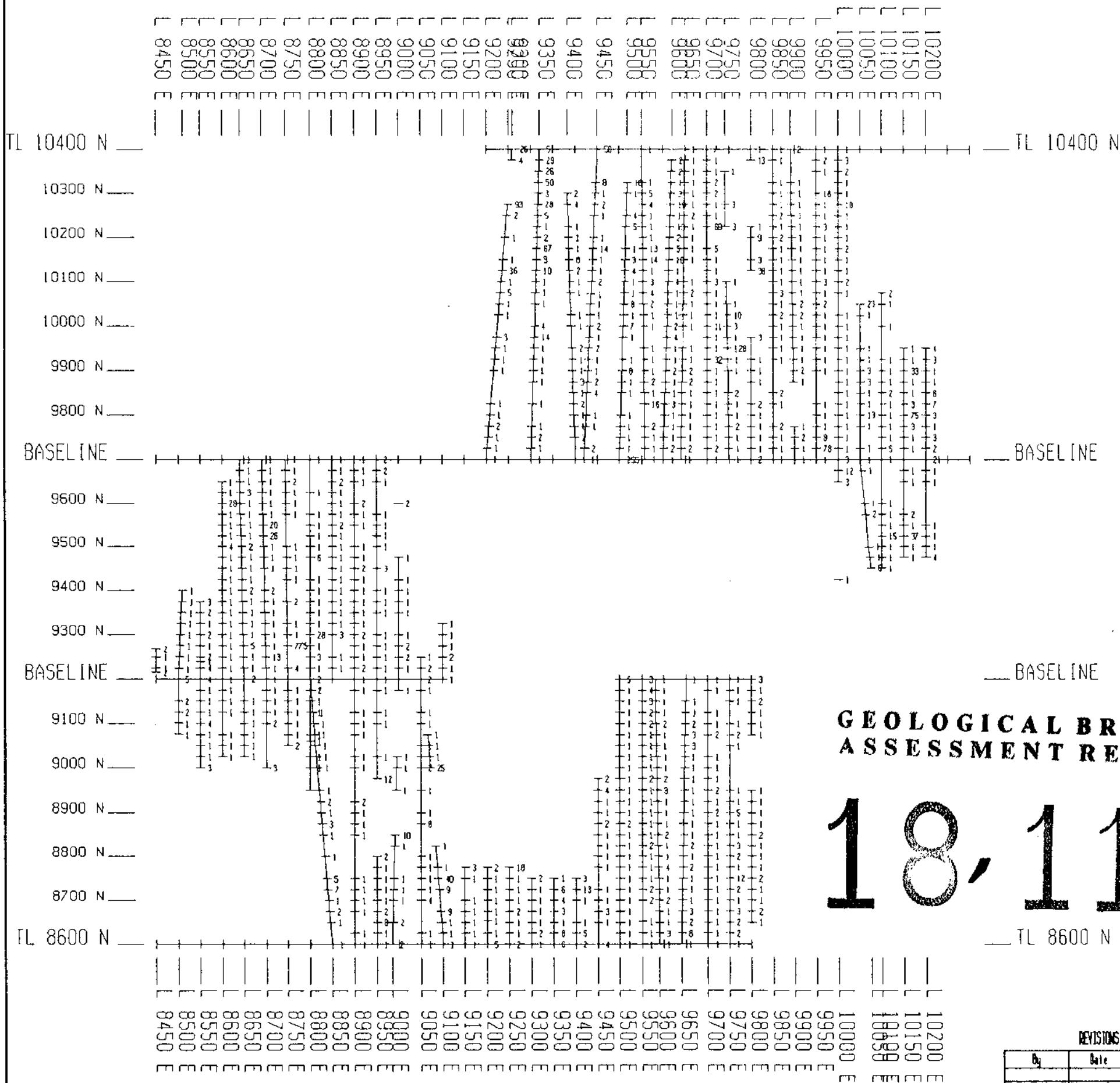
Sample No.	Width (cm)	Cu %	Pb %	Zn %	Ag (g/t)	Au (g/t)
106A	24	0.14	2.13	1.18	1.28	0.001
107A	60	0.05	1.40	0.90	1.41	0.005
108	25	0.07	1.05	0.82	1.25	0.001
108A	60	0.07	0.97	1.84	2.49	0.001
110	30	0.01	3.29	1.57	29.97	0.001
110A	32	0.06	2.27	0.38	4.13	0.010
111	36	0.02	0.41	0.52	0.54	0.001
111A	86	0.04	1.28	0.27	3.51	0.001
112	49	0.13	19.52	0.18	45.56	0.008
113	57	0.08	11.05	3.40	23.48	0.006
113A	44	0.14	11.19	4.86	15.31	0.011
114	18	0.02	2.95	0.61	1.19	0.002
114A	13	0.02	30.31	0.07	43.54	0.010
114B	28	0.08	0.86	0.10	9.97	0.004
115	57	0.04	25.00	0.20	27.57	0.002
115A	27	0.05	1.48	3.57	2.07	0.001
116	81	0.08	0.82	0.11	1.84	0.001
116A	17	0.03	0.71	0.18	5.19	0.003
117	176	0.26	38.18	8.10	74.03	0.017
118	30	0.01	1.57	0.82	0.51	0.002
118	19	0.02	0.60	0.14	1.70	0.013
120	40	0.29	51.98	1.40	19.80	0.021
121	16	0.02	1.25	0.20	1.34	0.001
122	18	0.04	1.23	0.28	1.94	0.006
123	6	0.01	0.29	0.10	0.17	0.004
123A	15	0.09	6.90	4.23	7.41	0.004
124	45	0.05	3.29	3.53	3.86	0.045
125	108	0.08	2.22	0.10	4.37	0.024
126	27	0.17	4.53	1.00	10.07	0.014
127	11	0.01	0.58	0.55	0.79	0.074
128	30	0.11	9.78	22.90	22.35	0.047
130	38	0.08	2.05	0.56	3.45	0.001
132	23	0.02	0.89	0.14	3.89	0.005
133	24	0.01	6.82	0.09	10.75	0.018
134	44	0.04	2.70	1.35	8.23	0.008
136	11	0.03	1.47	0.30	0.33	0.004
137	10	0.02	7.04	1.16	0.39	0.019
138	8	0.01	2.66	0.41	3.32	0.001
140	40	0.20	1.12	0.34	2.54	0.001
141	100	0.08	1.86	0.40	1.36	0.001
142	70	0.20	1.24	7.38	20.75	0.051
143	100	0.20	0.47	0.34	1.29	0.002

**GEOLOGICAL BRANCH
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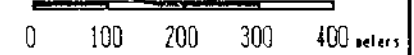


Harrisburg - Dayton Resource Corp.
SUMMIT TRENCH
SUMMIT CAMP PROPERTY
Similkameen Mining Division
NTS 92 N/6
Project 1988
Page 2



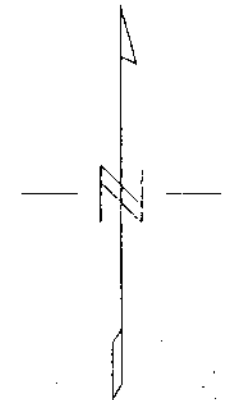
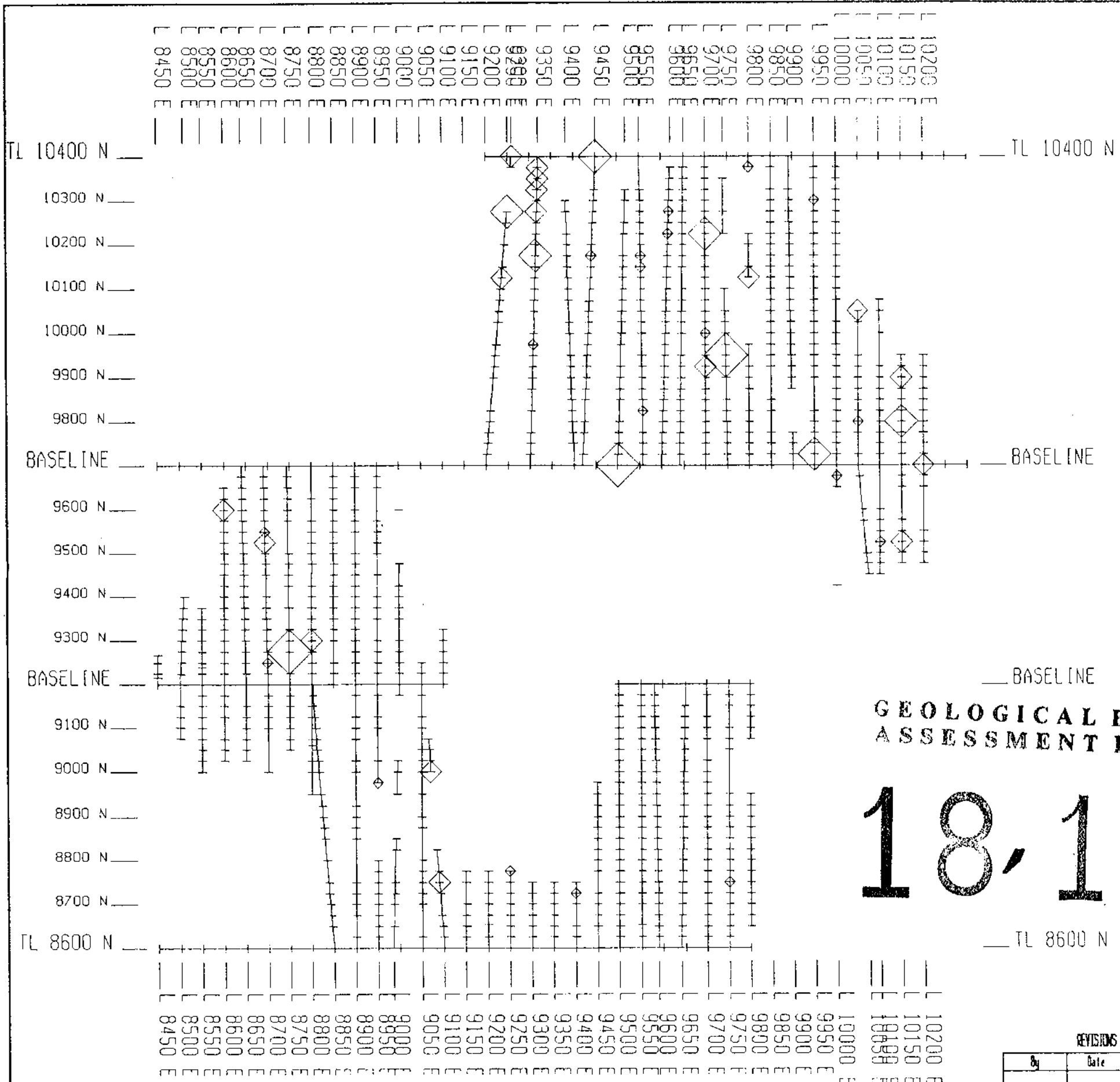
**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111



HARRISBURG-DAYTON RESOURCE CORP			
SUMMIT CAMP			
SOIL GEOCHEMISTRY			
Au (ppb)			
VALUE MAP			
Maps Prepared by: WEST COAST CONSULTING SERVICES INC.			
Project No:	Scale:	Client:	SR/GE
Date:	12/18	Map No:	9
BOA SERVICES LTD.			

REVISONS		
By	Date	Appov. By



- LEGEND**
- + < 10
 - ◆ 10 - 20
 - ◇ 21 - 50
 - ◇ 51 - 100
 - ◇ > 100

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

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By	Date	Appov. By

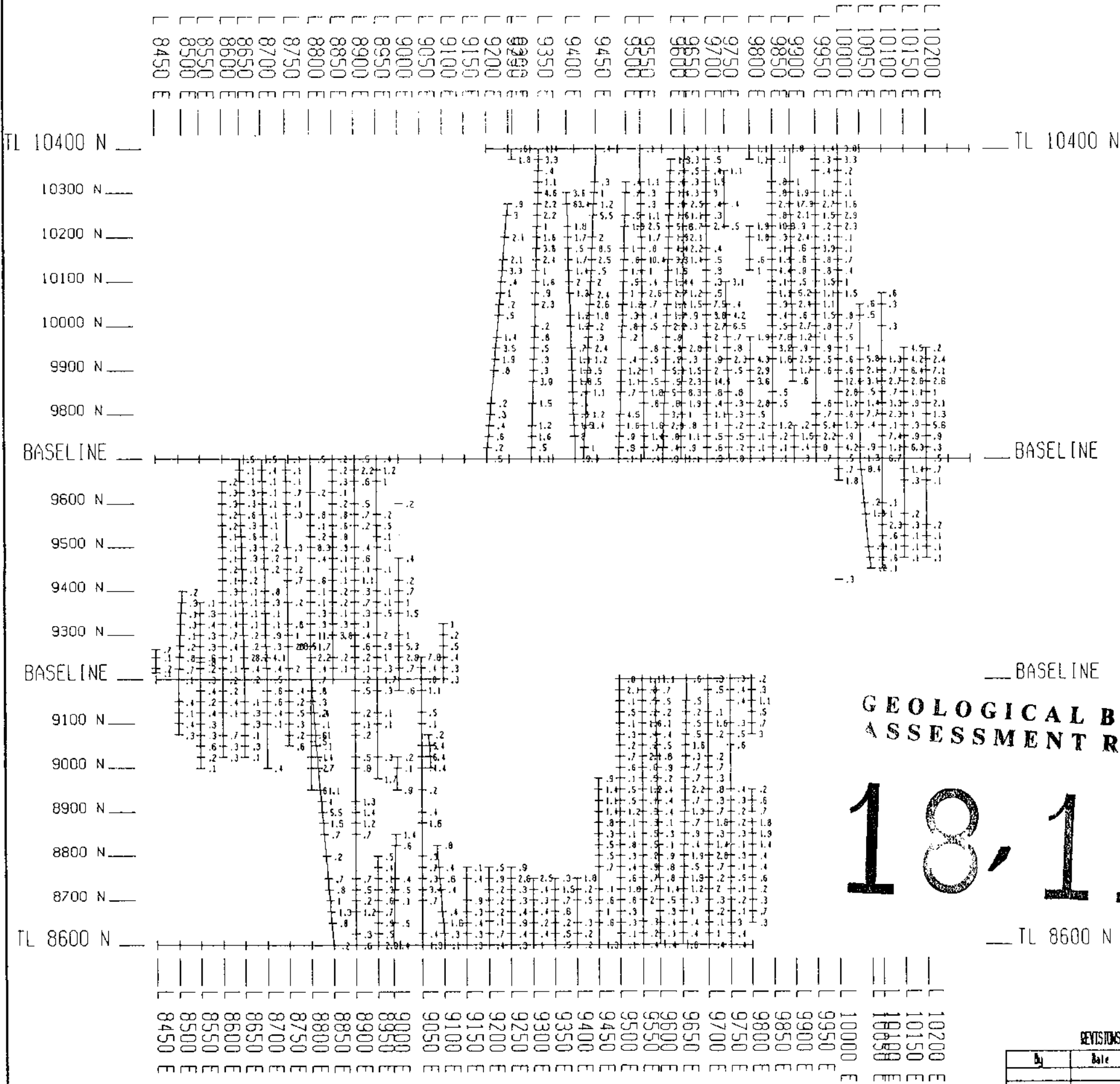
HARRISBURG-DAYTON RESOURCE CORP

SUMMIT CAMP
SOIL GEOCHEMISTRY
Au (ppb)
SYMBOL MAP

Map Prepared by: WEST COAST EXPLOREX SERVICES INC.

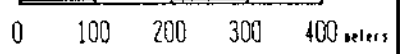
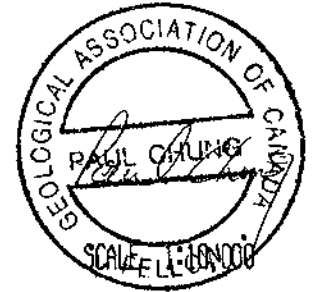
Project No:	Report No:
Client: Seattle	Date: 9/21/92
Date: 8/18	By: 10

BOA SERVICES LTD.



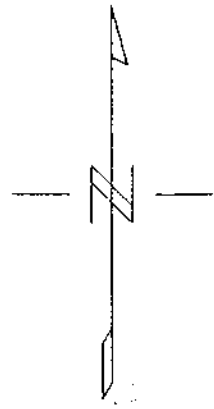
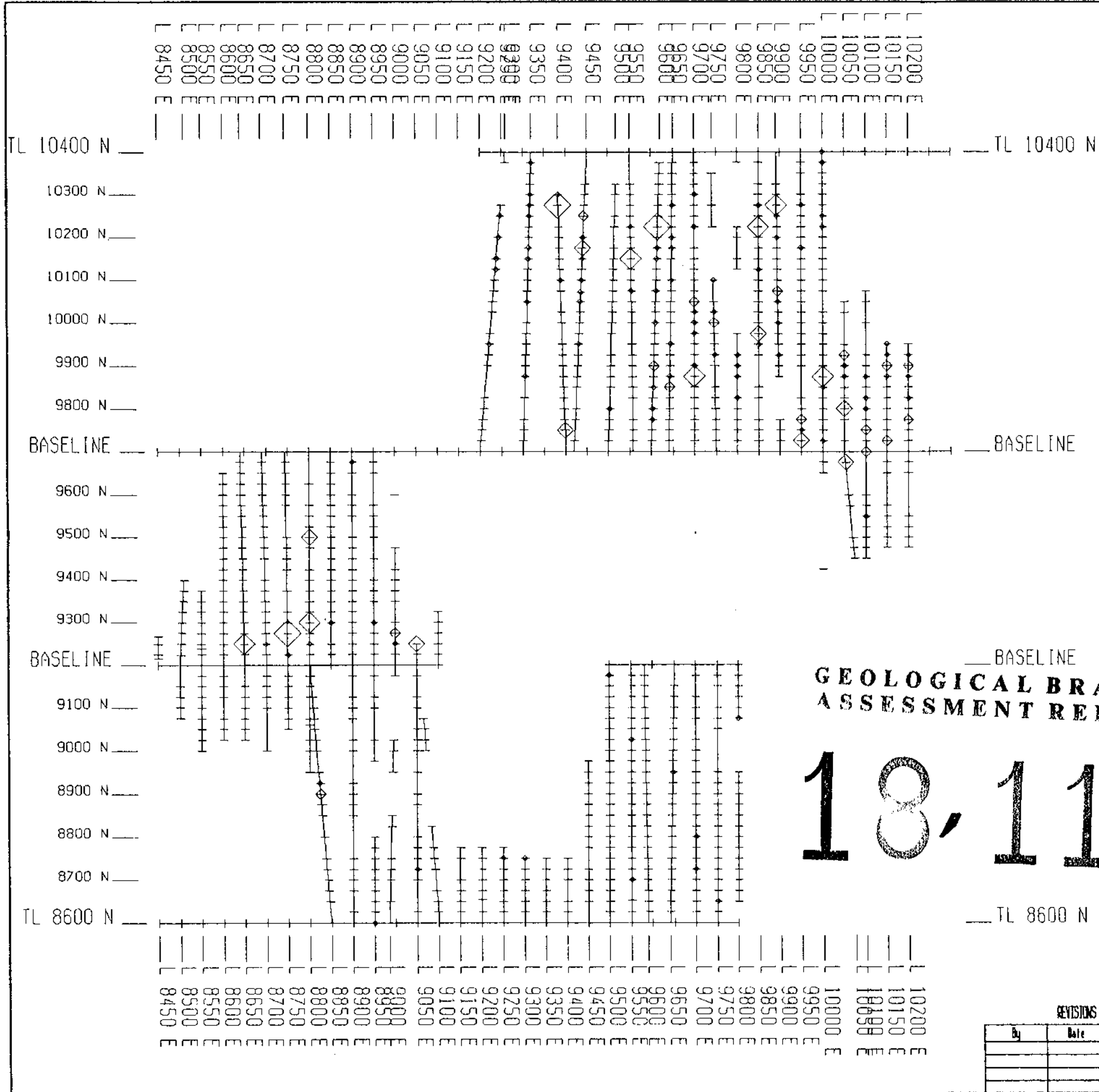
**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111



REVISIONS		
By	Date	Approv. By

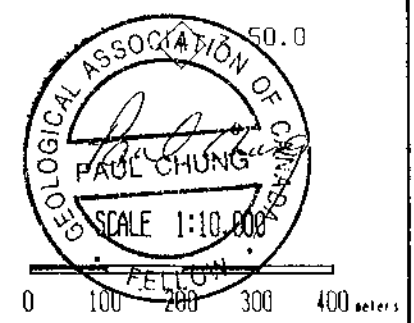
HARRISBURG-DAYTON RESOURCE CORP	
SUMMIT CAMP SOIL GEOCHEMISTRY Ag (ppm) VALUE MAP	
Data Prepared By: STEEL BRIDGE CONSULTING SERVICES INC.	
Project No:	Report No:
Drawing No: 5011k	Date: 9/28/88
Date: 9/28	By: J.L.
BOA SERVICES LTD.	



- LEGEND**
- + < 2.0
 - * 2.0 - 5.0
 - ◇ 5.1 - 7.5
 - ◇ 7.5 - 10.0
 - ◇ 10.1 - 50.0

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111



REVISIONS

By	Date	Approv. By

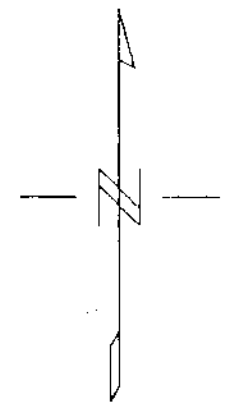
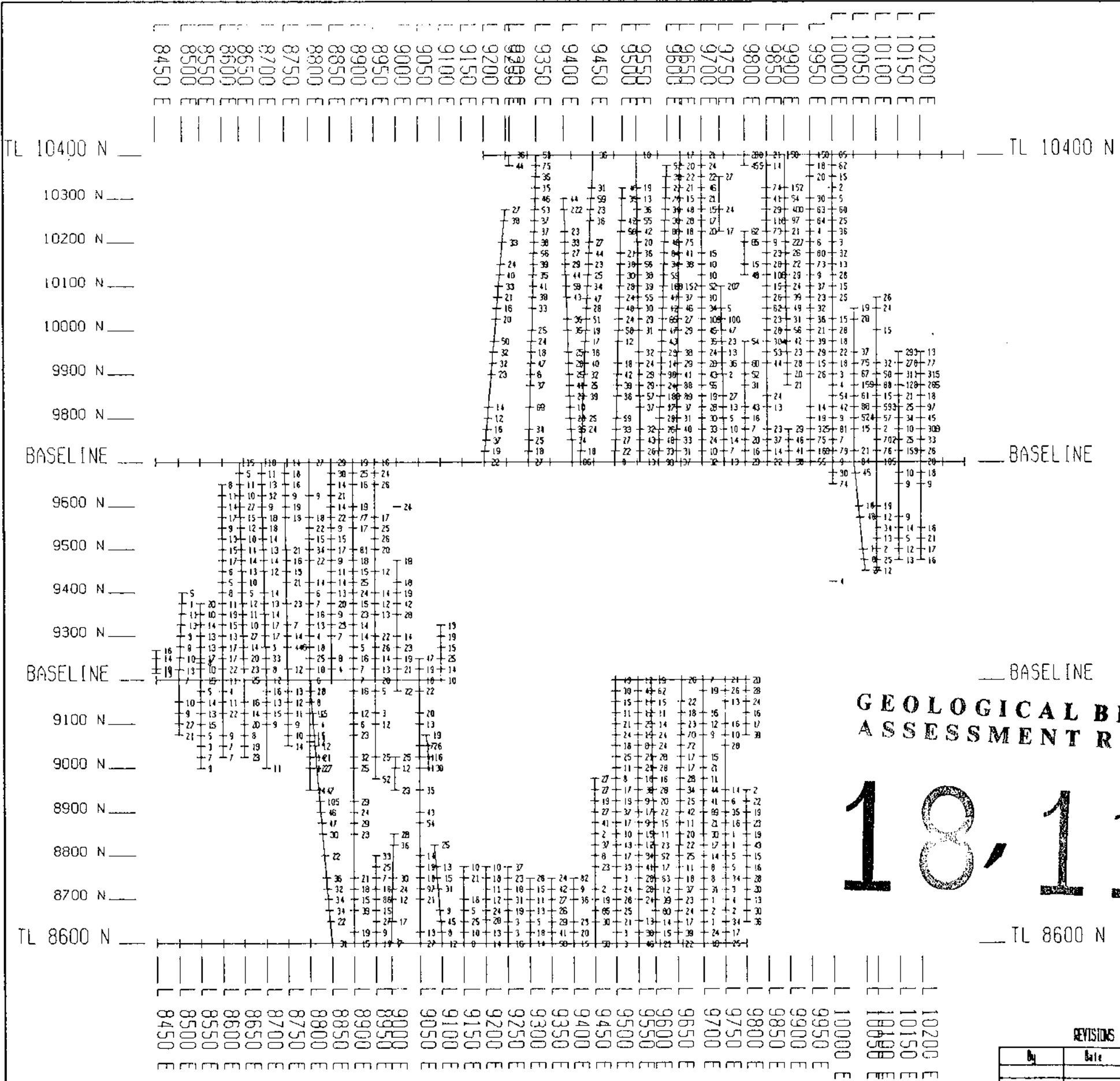
HARRISBURG-DAYTON RESOURCE CORP

**SUMMIT CAMP
SOIL GEOCHEMISTRY
Ag (ppm)
SYMBOL MAP**

Days Prepared By: **ORIEL GIBSON EXPLORATION SERVICES INC.**

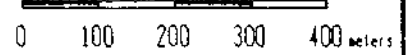
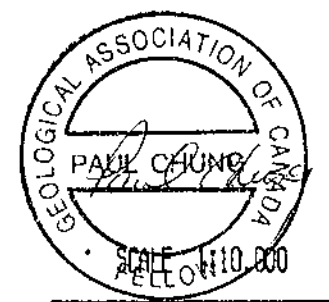
Project No:	Report No:
Drawing Title: Symbol	Scale: 920/9E
Date: 01/88	Page No: 12

BOA SERVICES LTD.



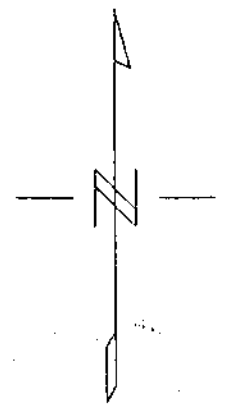
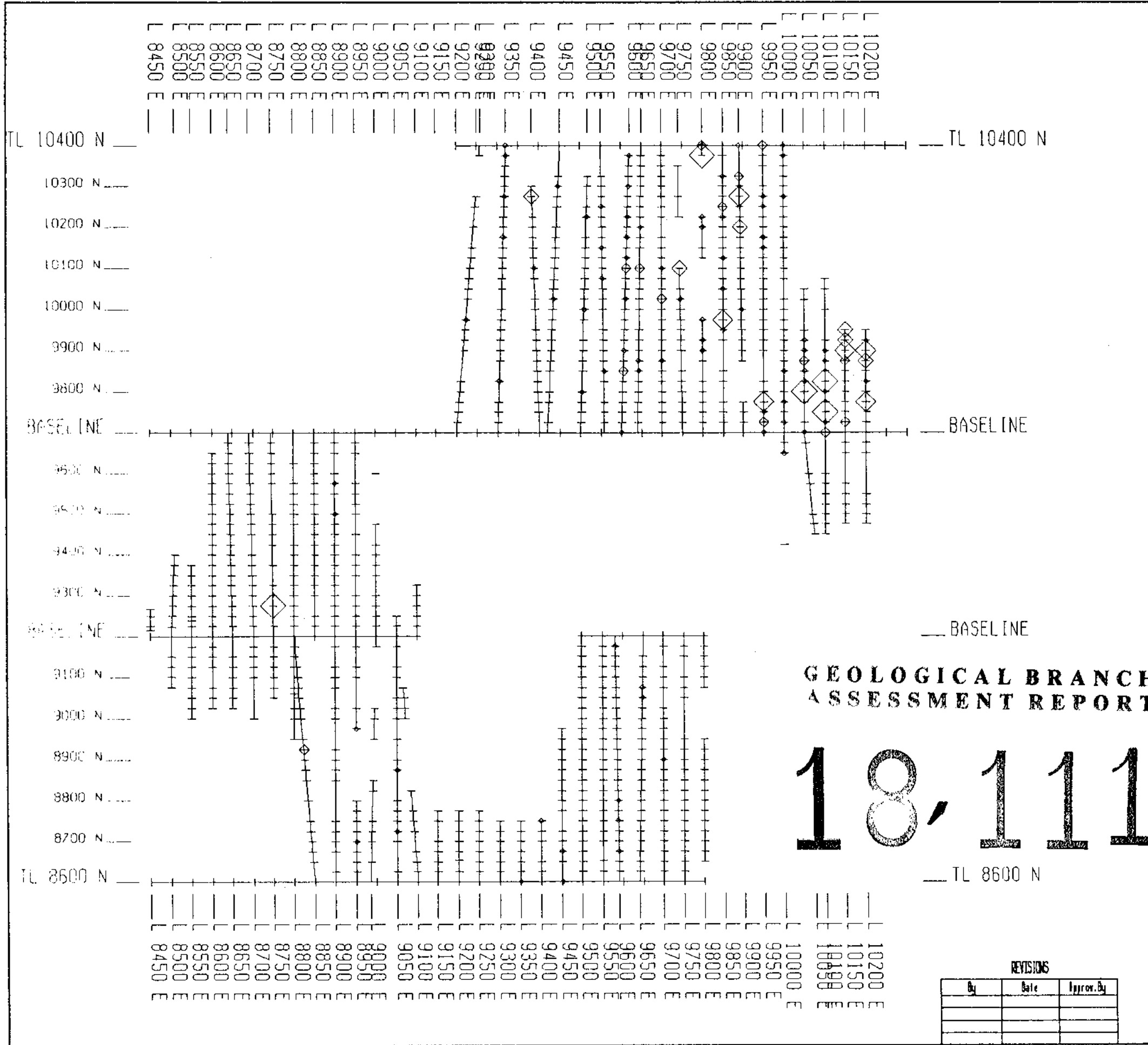
**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111



HARRISBURG-DAYTON RESOURCE CORP	
SUMMIT CAMP SOIL GEOCHEMISTRY Cu (ppm) VALUE MAP	
Map Prepared By: HARRISBURG-DAYTON RESOURCE SERVICES INC.	Project No:
Drawing Title: Soil Geochem. Value Map	Date: 02/10
Scale: 1:10,000	Sheet No: 13
BOA SERVICES LTD.	

REVISIONS		
By	Date	Approved By

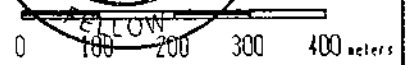
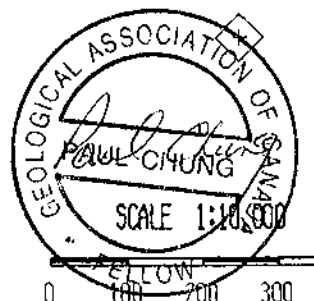


LEGEND

- + < 50
- * 50 - 100
- ◇ 101 - 200
- ◇+ 201 - 300
- ◇+ 301 - 400
- ◇* > 400

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

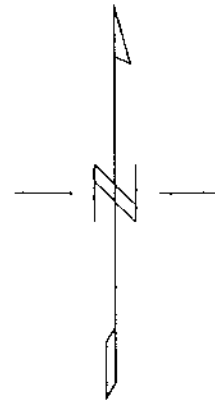
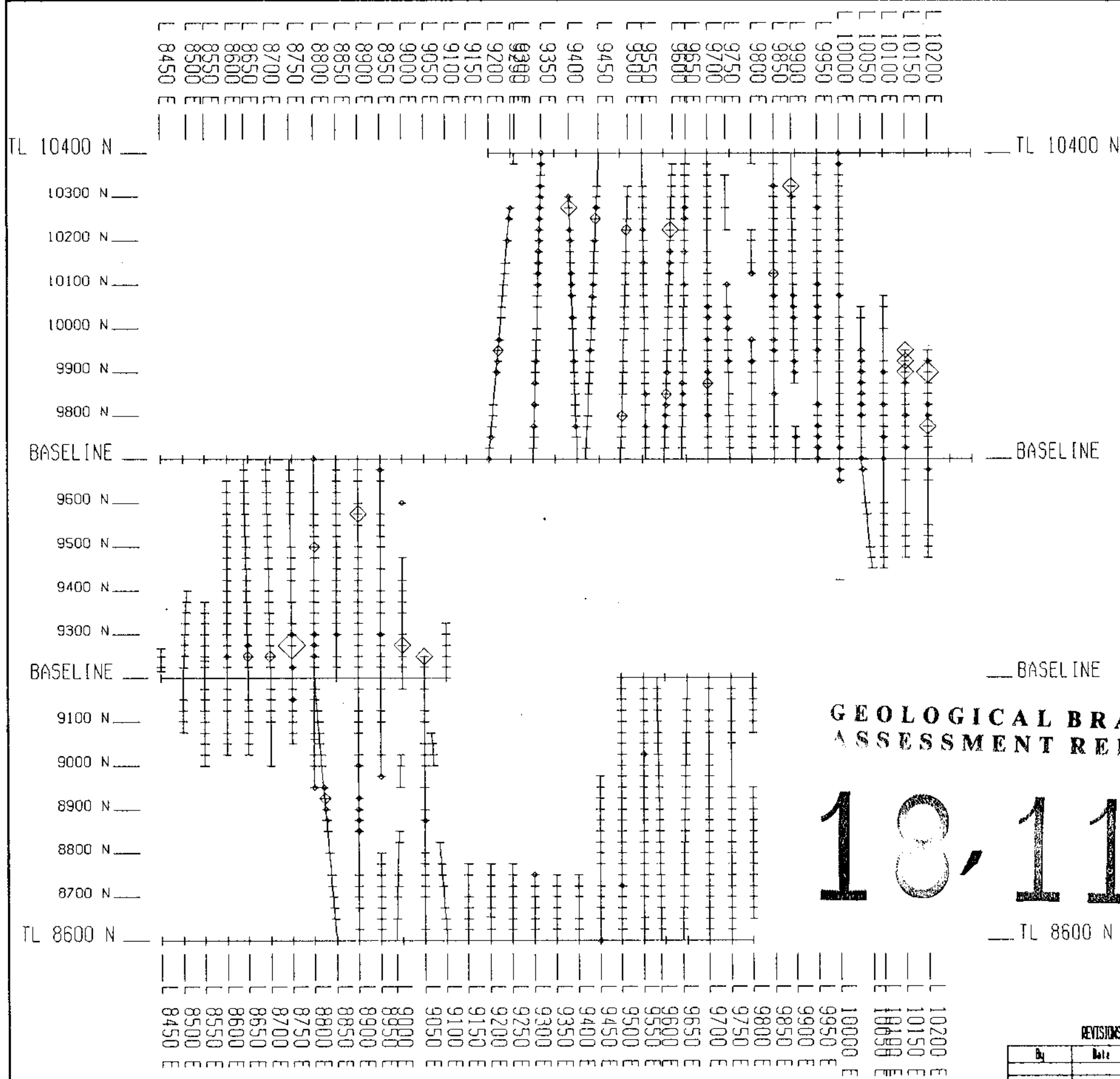
18,111



HARRISBURG-DAYTON RESOURCE CORP	
SUMMIT CAMP	
SOIL GEOCHEMISTRY	
Cu (ppm)	
SYMBOL MAP	
Maps Prepared by: WEST CANADA EXPLORATION SERVICES INC.	
Project No:	Report No:
Drawing No: 5011k	Date: 12/1/88
Date: 05/88	Page No: 14
BOA SERVICES LTD.	

REVISIONS

By	Date	Approv. By



LEGEND

- + < 100
- ♦ 100 - 500
- ◊ 501 - 1000
- ⊕ 1001 - 2000
- ⊕ 2001 - 4000
- ⊕ > 4000

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111

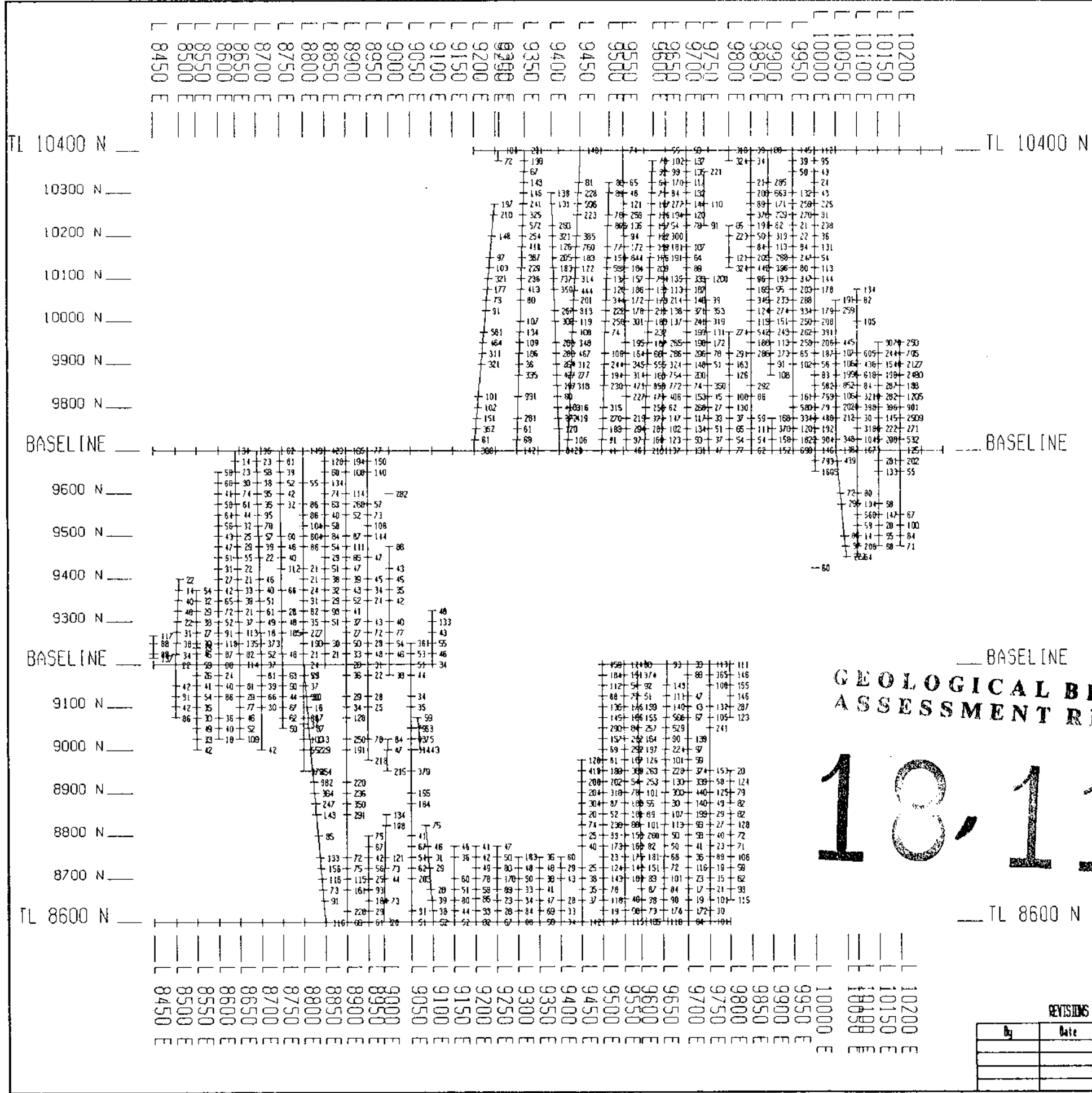


SCALE 1:10,000
0 100 200 300 400 meters

HARRISBURG-DAYTON RESOURCE CORP	
SUMMIT CAMP	
SOIL GEOCHEMISTRY	
Pb (ppm)	
SYMBOL MAP	
Prepared By: HARRISBURG-DAYTON RESOURCE CORP	
Project No:	Report No:
Drawing No: 51416	Date: 02/88
Date: 03/88	Page No: 16
BOA SERVICES LTD.	

REVISIONS

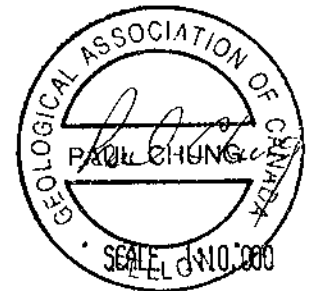
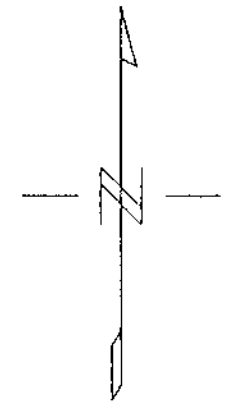
By	Date	Approved By



— BASELINE
**GEOLOGICAL BRANCH
 ASSESSMENT REPORT**

18,111

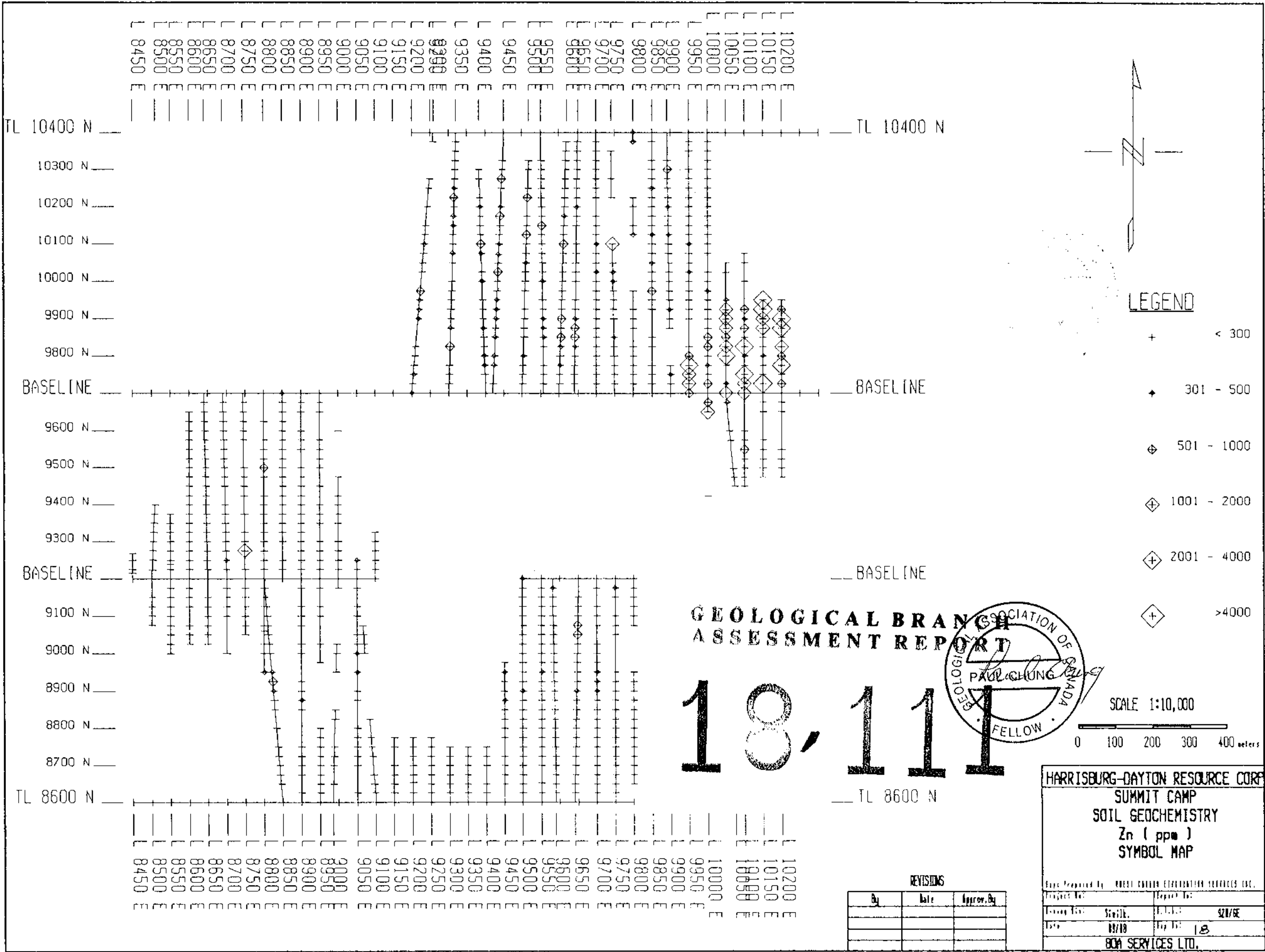
— TL 8600 N



HARRISBURG-DAYTON RESOURCE CORP	
SUMMIT CAMP SOIL GEOCHEMISTRY Zn (ppm) VALUE MAP	
Maps Prepared by: BRISTOL GEOTECHNOLOGICAL SERVICES INC.	
Project No:	Report No:
Drawing Title: Summit	Scale: 1:10,000
Date: 03/18	Fig No: 17
BGA SERVICES LTD.	

REVISIONS

By	Date	Appov. By



TL 10400 N
 10300 N
 10200 N
 10100 N
 10000 N
 9900 N
 9800 N
 BASELINE
 9600 N
 9500 N
 9400 N
 9300 N
 BASELINE
 9100 N
 9000 N
 8900 N
 8800 N
 8700 N
 TL 8600 N

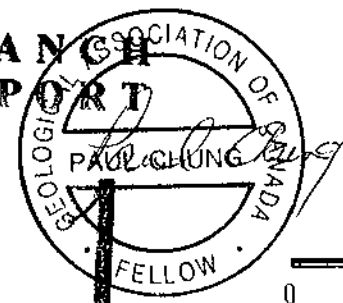
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 10100 E
 10050 E
 10000 E
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 9550 E
 9500 E
 9450 E
 9400 E
 9350 E
 9300 E
 9250 E
 9200 E
 9150 E
 9100 E
 9050 E
 9000 E
 8950 E
 8900 E
 8850 E
 8800 E
 8750 E
 8700 E
 8650 E
 8600 E
 8550 E
 8500 E
 8450 E

TL 10400 N
 BASELINE
 BASELINE
 BASELINE
 TL 8600 N

- LEGEND**
- + < 300
 - ♦ 301 - 500
 - ◊ 501 - 1000
 - ◊ 1001 - 2000
 - ◊ 2001 - 4000
 - ◊ >4000

**GEOLOGICAL BRANCH
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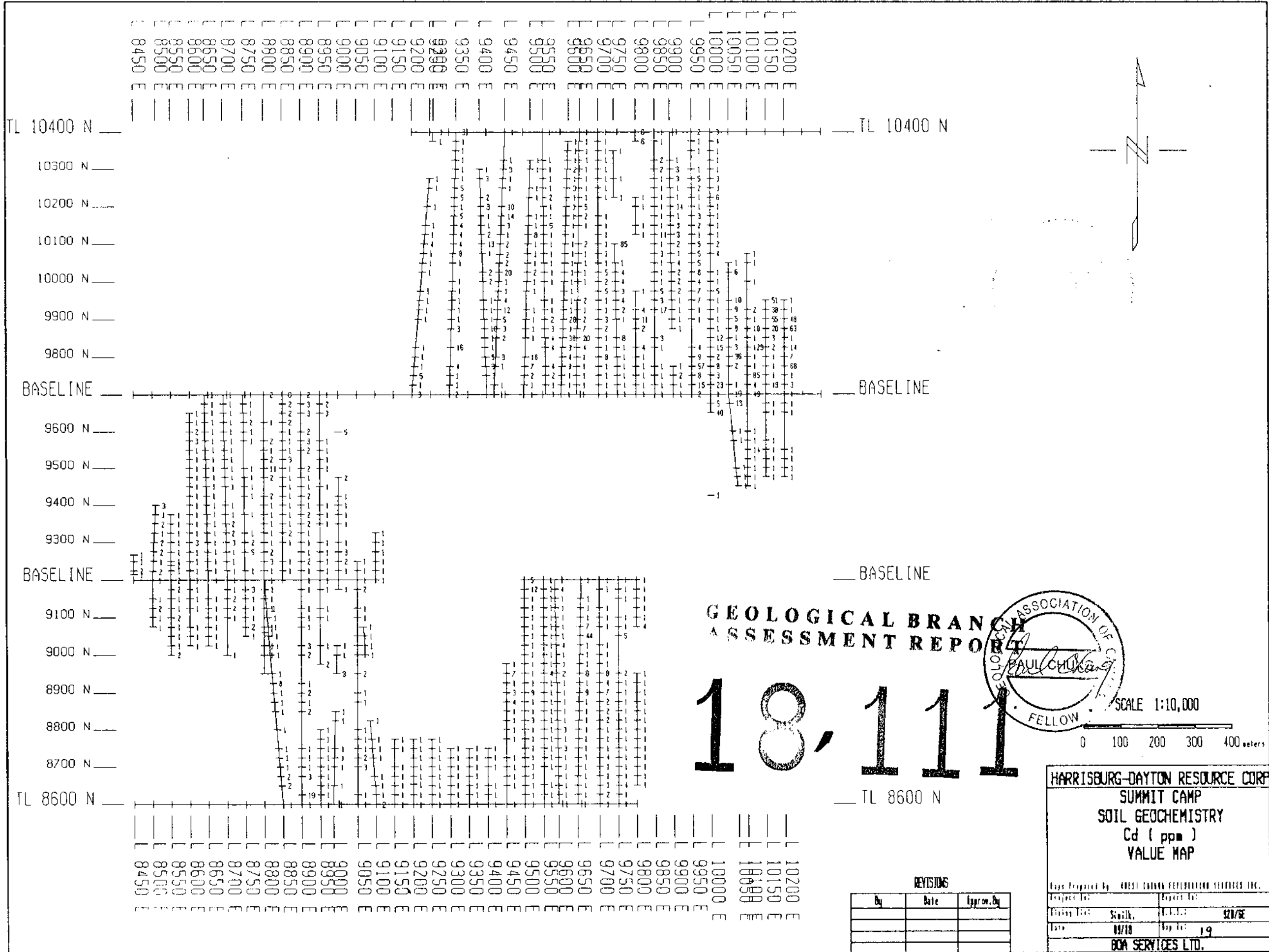


SCALE 1:10,000
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REVISIONS

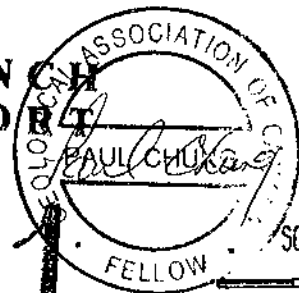
By	Date	Approv. By

HARRISBURG-DAYTON RESOURCE CORP	
SUMMIT CAMP	
SOIL GEOCHEMISTRY	
Zn (ppm)	
SYMBOL MAP	
Data Prepared by: WEST COAST EDUCATION SERVICES INC.	
Project No:	Report No:
Drawing Title: Summit	Scale: 1:10,000
Date: 07/10	Fig No: 18
BOA SERVICES LTD.	

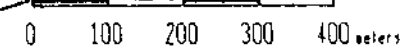


**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111

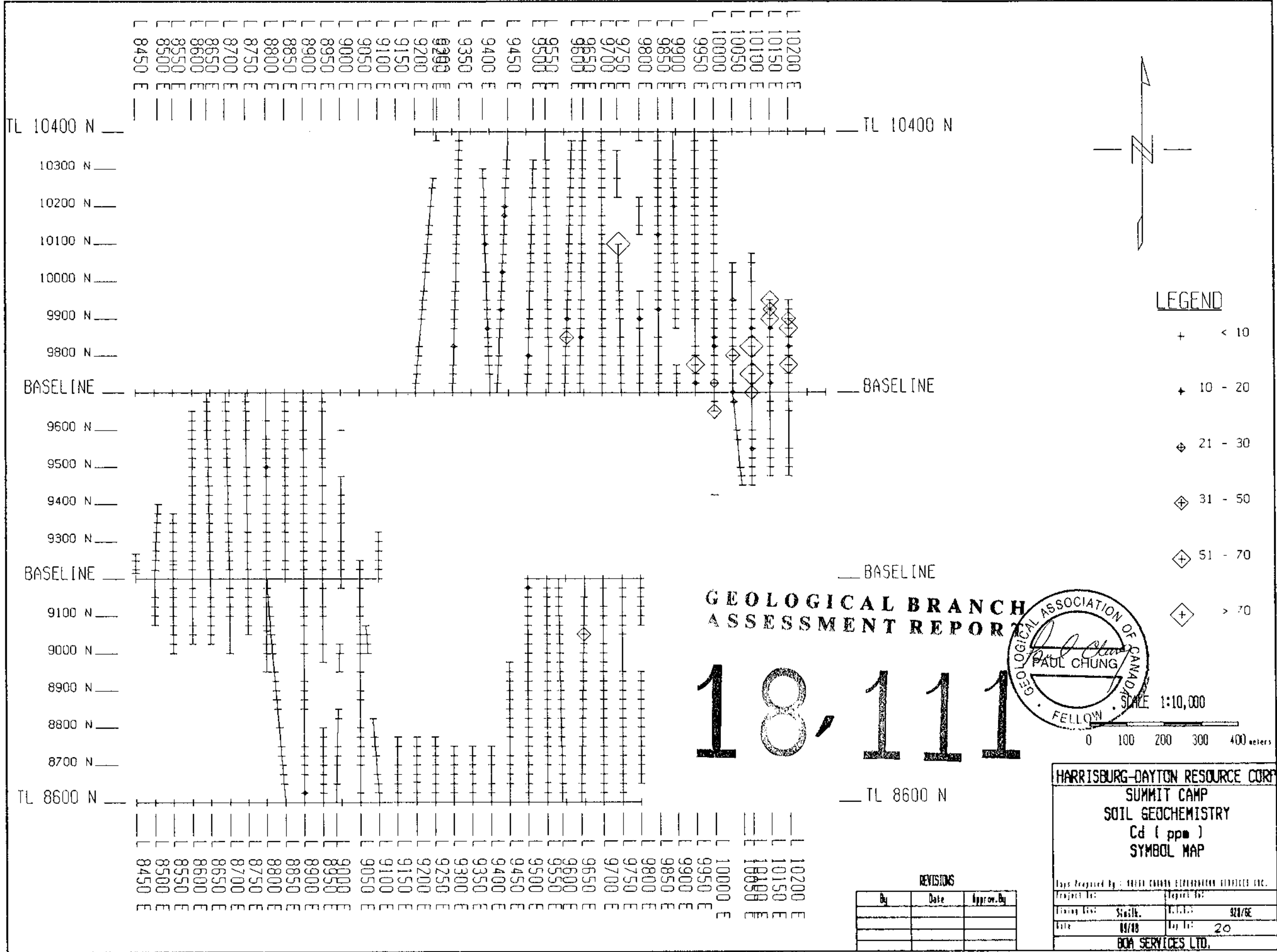


SCALE 1:10,000



REVISIONS		
By	Date	Approv. By

HARRISBURG-DAYTON RESOURCE CORP	
SUMMIT CAMP	
SOIL GEOCHEMISTRY	
Cd (ppm)	
VALUE MAP	
Map Prepared By: GREST CONSULTING ENGINEERING SERVICES INC.	
Project No:	Report No:
Drawing Title: Summit	Sheet No: 521/52
Date: 09/10	Scale: 1:10,000
BOA SERVICES LTD.	

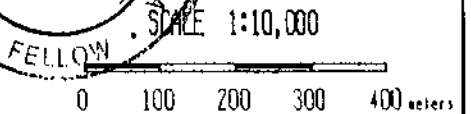
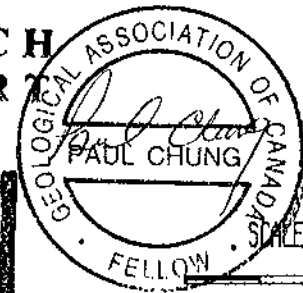


LEGEND

- + < 10
- 10 - 20
- ◊ 21 - 30
- ◊+ 31 - 50
- ◊+ 51 - 70
- + > 70

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

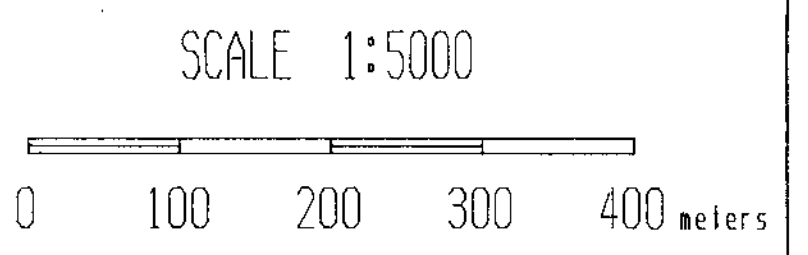
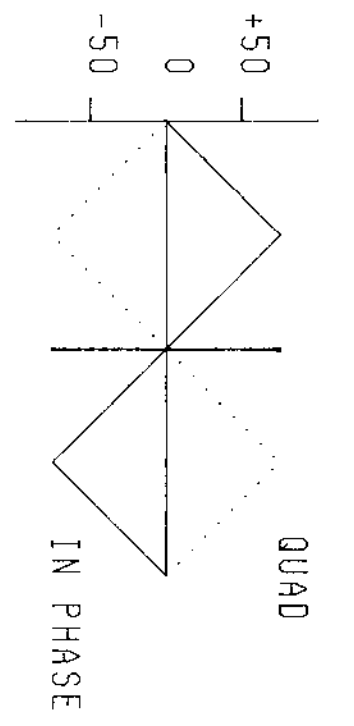
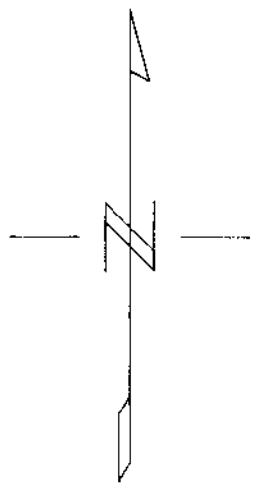
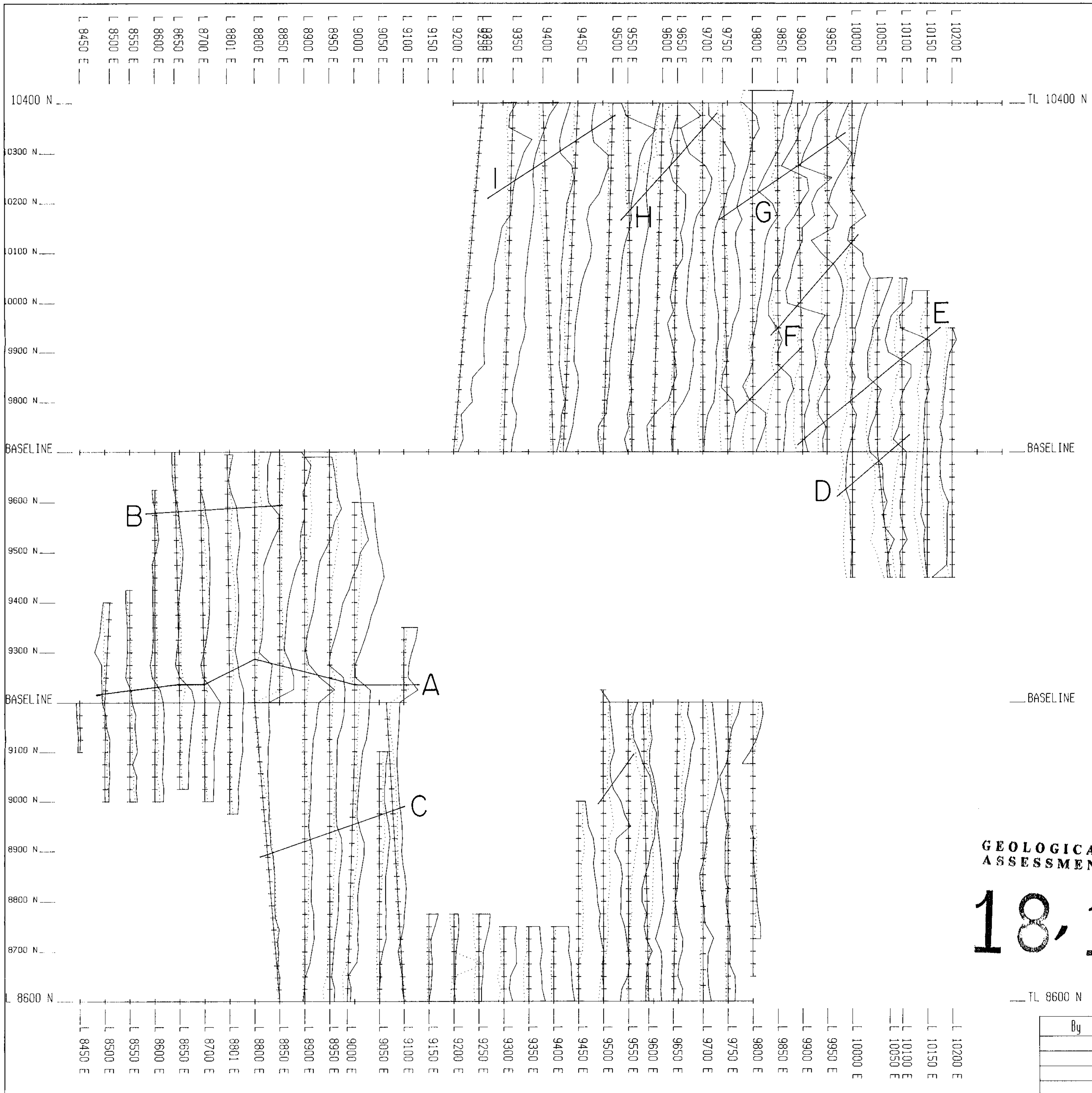
18,111



HARRISBURG-DAYTON RESOURCE CORP.			
SUMMIT CAMP SOIL GEOCHEMISTRY Cd (ppm) SYMBOL MAP			
Days Required By: BOA CONSULTING SERVICES INC.			
Project No:	Site:		Report No: 92/06
Drawing Date:	01/08	By:	20
BOA SERVICES LTD.			

REVISIONS

By	Date	Approved By



**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111

TL 8600 N

REVISIONS

By	Date	Approv. By

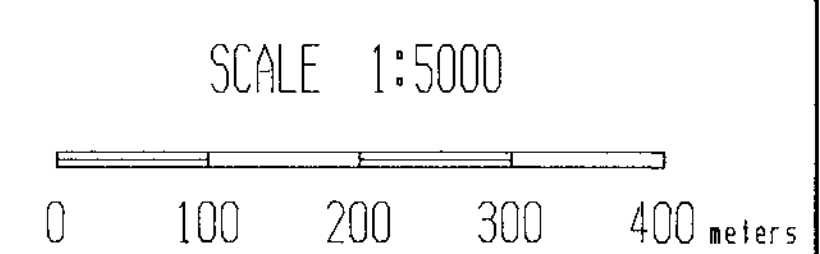
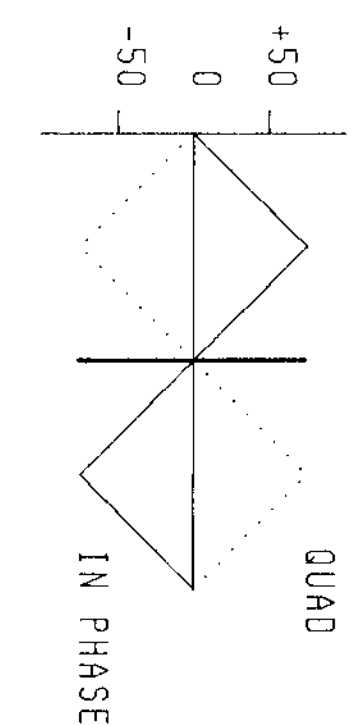
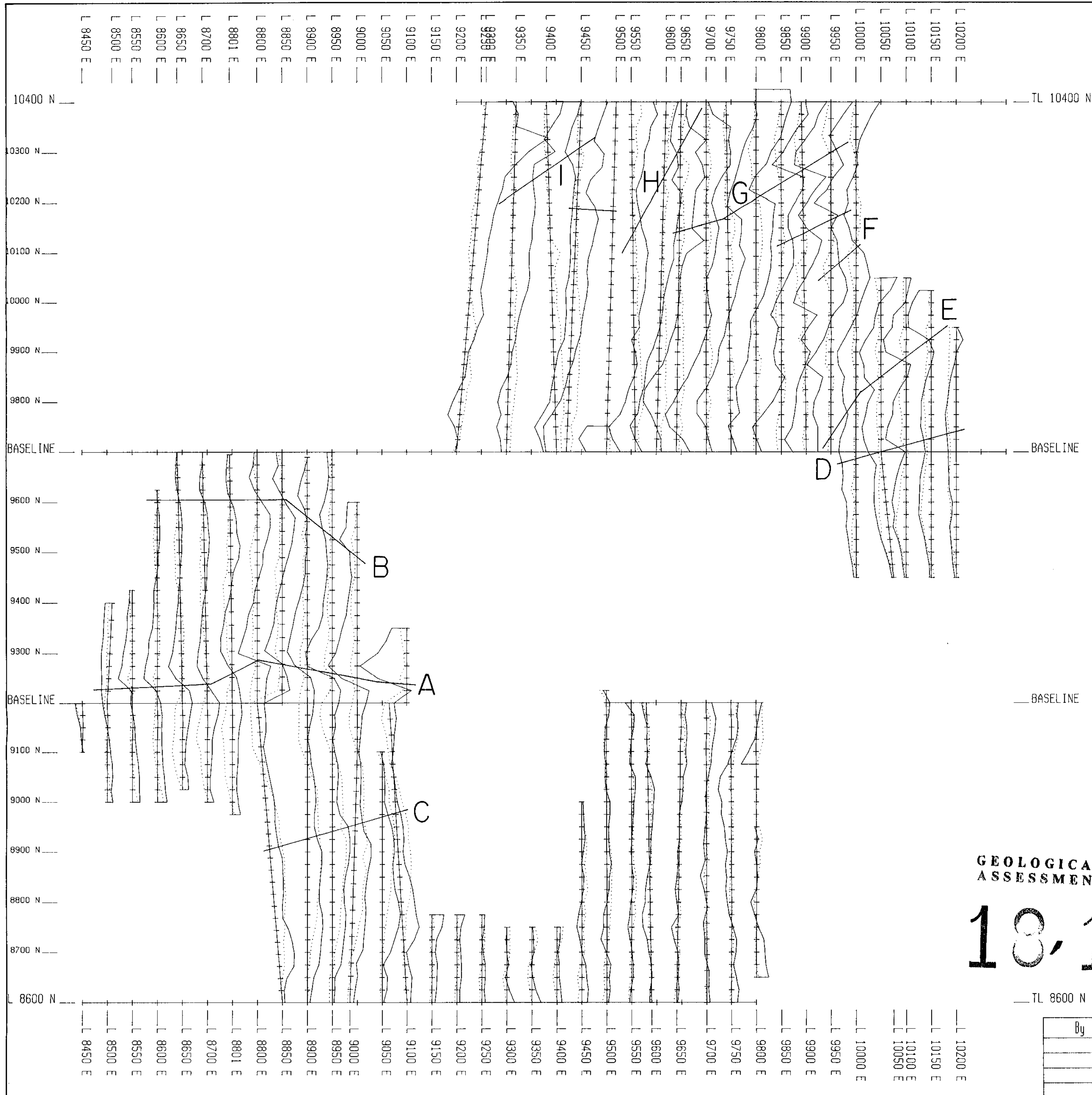
HARRISBURG-DAYTON RESOURCE CORP

SUMMIT CAMP
VLF - EM
SEATTLE
PROFILE MAP

Maps Prepared By: QUEST CANADA EXPLORATION SERVICES INC.

Project No:	Report No:
Mining Div: Similk.	N.T.S.: 92H / 6E
Date: 08/88	Map No: 21

BOA SERVICES LTD.



**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

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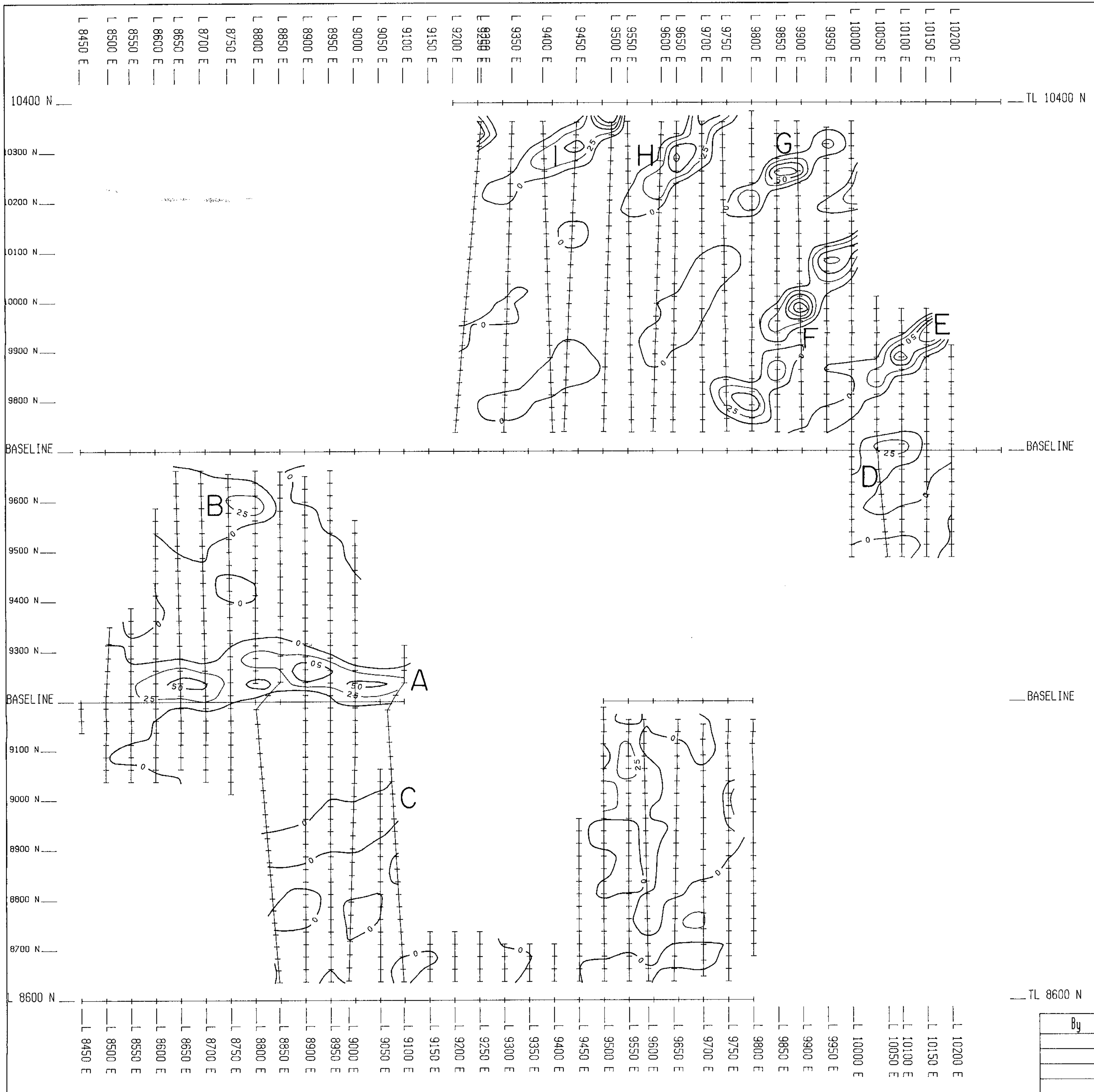
REVISIONS

By	Date	Appov.By

HARRISBURG-DAYTON RESOURCE CORP
SUMMIT CAMP
VLF - EM
CUTLER
PROFILE MAP

Maps Prepared By : QUEST CANADA EXPLORATION SERVICES INC.
 Project No: _____ Report No: _____
 Mining Div: Similk, N.T.S.: 92H / 6E
 Date: 08/88 Map No: 22

BOA SERVICES LTD.

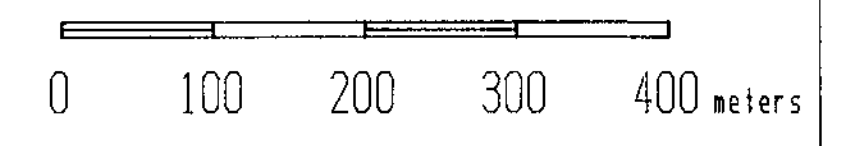


**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

18,111

Contour Interval : 25,50

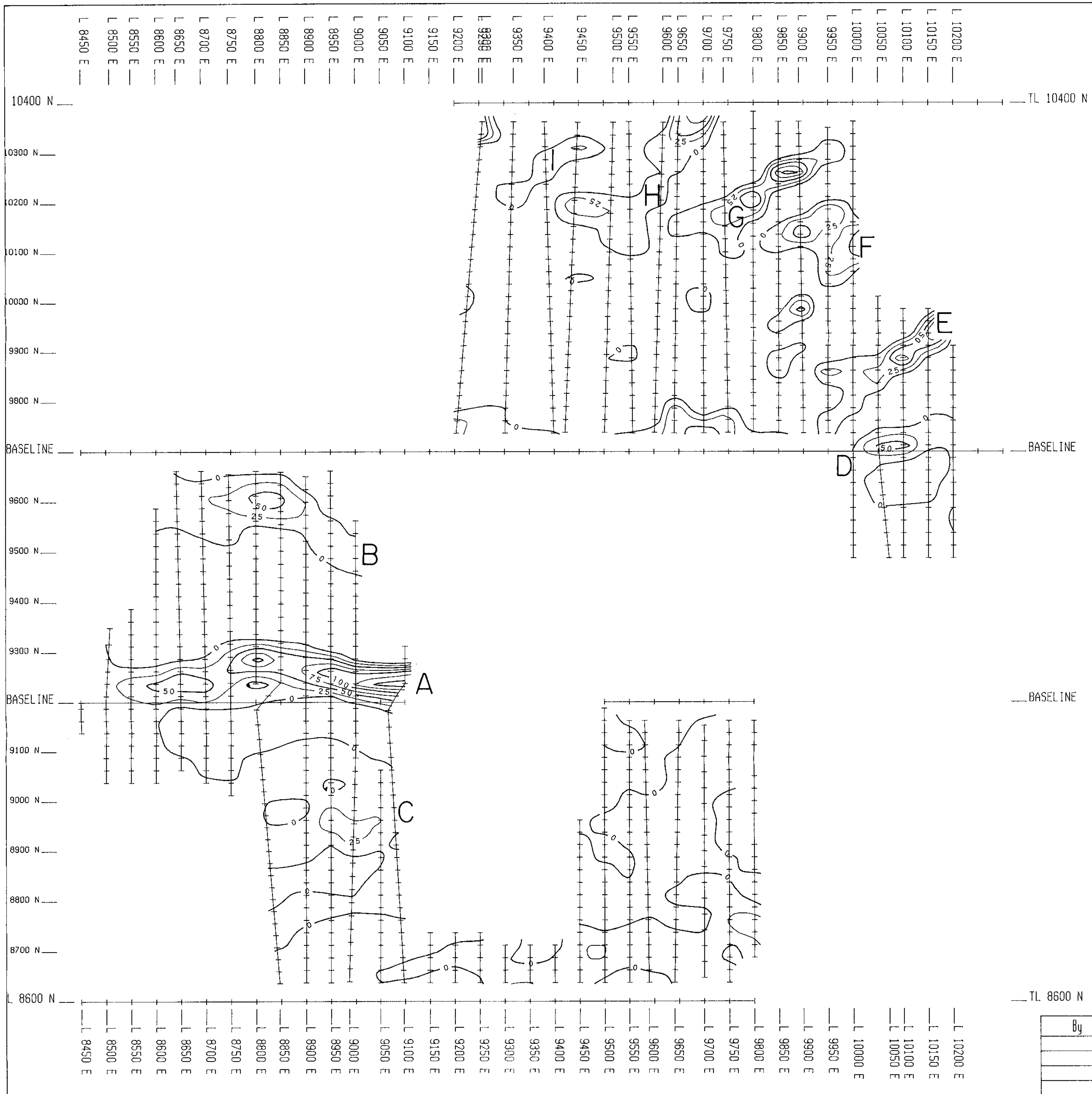
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HARRISBURG-DAYTON RESOURCE CORP			
SUMMIT CAMP SEATTLE VLF-EM FRASER FILTERED CONTOUR MAP			
Maps Prepared By : QUEST CANADA EXPLORATION SERVICES INC.			
Project No:		Report No:	
Mining Div:	Similk.	N.T.S.:	92H / 6E
Date	08/88	Map No:	23
BOA SERVICES LTD.			

REVISIONS

By	Date	Appov.By

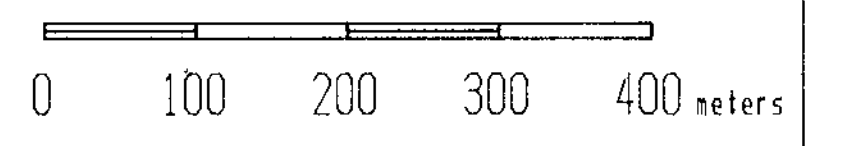


GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,111

Contour Interval : 25,50

SCALE 1:5000



HARRISBURG-DAYTON RESOURCE CORP

SUMMIT CAMP
CUTLER VLF-EM
FRASER FILTERED
CONTOUR MAP

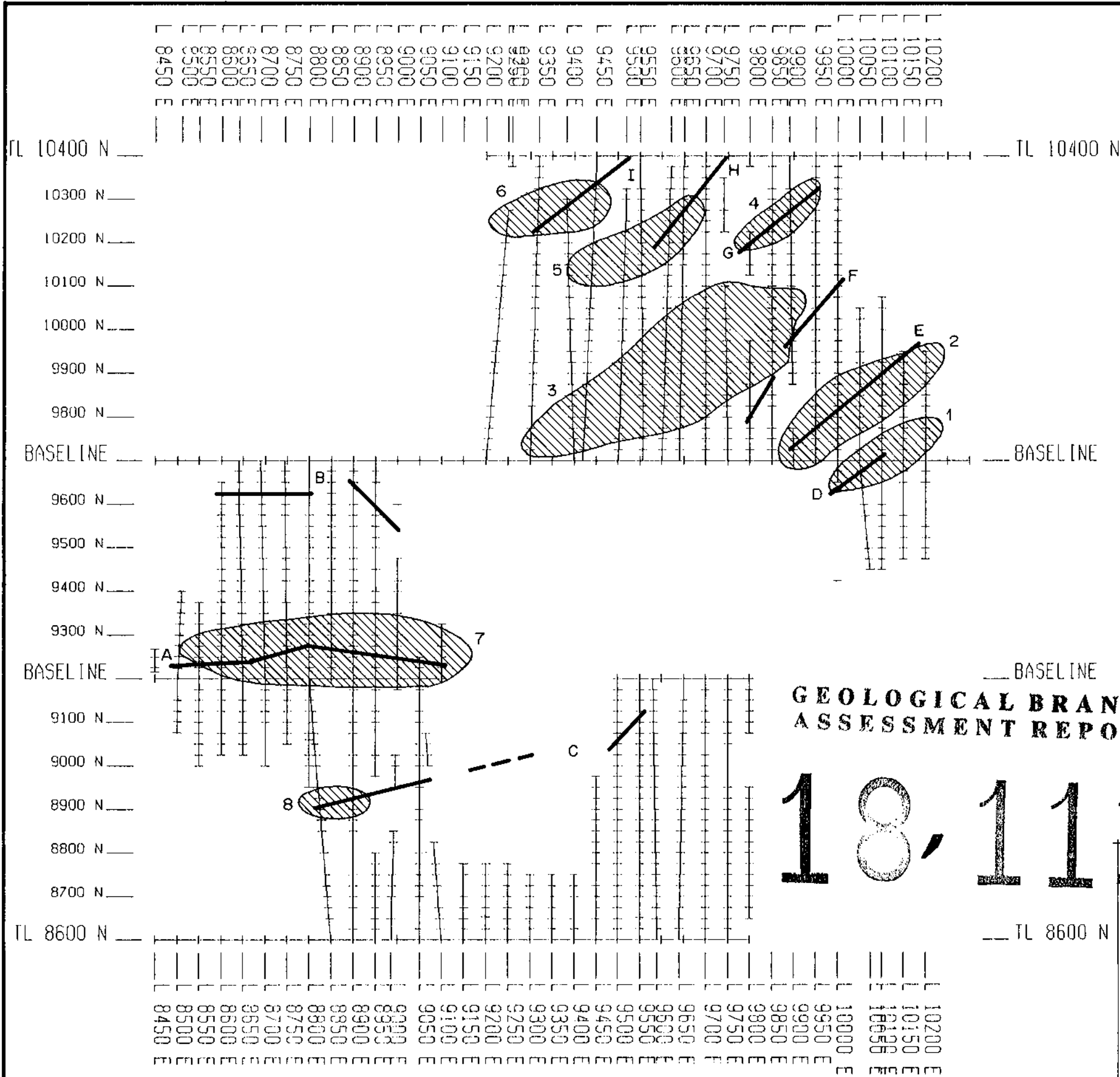
Maps Prepared By : QUEST CANADA EXPLORATION SERVICES INC.

Project No:		Report No:	
Mining Div:	Similk.	N.T.S.:	92H / 6E
Date	08/88	Map No:	24

BOA SERVICES LTD.

REVISIONS

By	Date	Approv. By



LEGEND
 4 Soil anomalies
 C VLF-EM conductor axis



100 0 100 200 300 400 500 m
 SCALE 1:10,000

**GEOLOGICAL BRANCH
 ASSESSMENT REPORT**

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Harrisburg - Dayton Resource Corp.
**Soil Anomalies &
 VLF-EM Conductor Axis**
SUMMIT CAMP PROPERTY
 Similkameen Mining Division
 NTS: 92 H/6

October, 1988 Figure 45

Boa Services Ltd.