

EXPLORATION
NTS 82F/1W

100000 1220	RD.

Mr. David Wiklund
Box 1480
Creston, B.C.
VOB 1G0

G E O C H E M I C A L S U R V E Y

Sun Claims

Nelson M.D., B.C.

Work Performed September 1988

Latitude 49° 9' N Longitude 116° 18' W

FILED

Sample Locations

Sun #5, #6, #7

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

Claim Group

Sun #5 9 units Record #3263
Sun #6 4 units Record #3317
Sun #7 3 units Record #3318
Sun #8 4 units Record #3889

18,154

Harry I. Davies

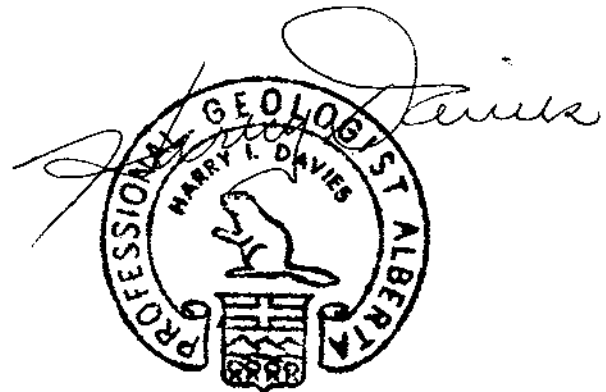


TABLE OF CONTENTS

INTRODUCTION	PAGE 1
LOCATION	1
TOPOGRAPHY	1
PREVIOUS WORK	2
GEOLOGY AND STRUCTURE	3
CURRENT WORK PROGRAM	4
LABORATORY PROCEDURES	4
ASSAY RESULTS	5
INTERPRETATION	5
RECOMMENDATIONS	6
STATEMENT OF QUALIFICATIONS	7
STATEMENT OF EXPENDITURES	8
INDEX MAP	9
CLAIM MAP	10
ASSAYS	11 - 14
DISPLAY MAP	POCKET

INTRODUCTION

The writer Mr. Harry Davies (P. Geologist, Alberta) was retained by Mr. David Wiklund of Creston, B.C. to carry out a Geochemical survey over a portion of his Sun Claims, which are located in the Kitchener area of the East Kootenays B.C. Nelson M.D.

The location of the sample points and the collecting of the soil samples were carried out during September 1988.

A thirty element geochemical analysis was done by Acme Laboratories of Vancouver, B.C.

One of the purposes of the work was to earn work credits as outlined in the Mineral Act regulations of B.C.

LOCATION

The Sun group of claims which total 20 units, located in four claims are contiguous. They are located about 3.5 Km south-east of Kitchener, B.C. The claim area lies between Russell Creek on the West and Birch Creek on the East. This area can be located on Map #82F/1W. Access is by logging road leading south from Kitchener.

TOPOGRAPHY

The claim block is located on a north facing slope of a mountain and lies between elevations of about 700m and 1500 meters. The slope ranges from 10 to 45 degrees, but

flattens out on top in the area of Sun #8. A number of small gullies transect the property running in a general north-south direction. With the exception of a few scattered rock bluffs, a very small percentage of the area exhibits rock outcrop.

Soil cover ranges from less than a meter on the steep slopes to many of meters on the lower slopes. The ridges, which are numerous on the lower slopes are a product of glaciation, being composed of till.

There is little surface drainage and except for Russell Creek there is no flowing water source on the claim block.

The claim area has not been logged as there are only scattered stands of commercial grade timber available.

PREVIOUS WORK

The areas in which these claims are located has evidently been held continually since before the turn of the century. The original claims were evidently staked on a number of east-west trending quartz veins which occupies fractures, and exhibited a few scattered areas of thin massive galena. The individual veins range in thickness from 5 cm to 15 cm, and are contained in an area of about 100 by 200 meters. Numerous barren quartz veins are also located in this area.

An attempt to evaluate these veins were made by drifting two adits below and across the veins. No official data has been forthcoming from this work. This work was done during

the 1930's.

In the late 1970's an effort to evaluate the mineralization was made by stripping by bulldozer with questionable results. The top adit was covered and probably more damage was caused than information obtained.

In 1983 the author and Mr. David Wiklund did a geochemical survey over a portion of the claim and obtained good numbers in Lead. The claims were subsequently optioned to Cominco, who redid and expanded the geochemical survey, together with a UTEM geophysical survey. The Geochem survey indicated an anomalous area 1900 meters in length and varying in width. The anomaly was still open to both the north and south and could be expanded upon. The claim block was returned to Mr. David Wiklund as the option was terminated.

GEOLOGY AND STRUCTURE

The claim block is underlain by the Middle Aldridge of Pre-Cambrian age which consists of interbedded massive dark grey quartzites and very dark grey to black shales which in places are thinly bedded and exhibit a varve appearance. The sequence dips to the east at about 30 degrees and strikes roughly north-south. A number of fractures or shears are evident but appear to be of no consequence. One and perhaps two of the argillaceous quartzite beds appear brecciated

and exhibit a fair amount of pyrrhotite and was anomalous in both lead and zinc. These beds may be the source of the lead zinc anomaly, as the anomaly does not correlate with the mineralized quartz veins.

There are a number of basic intrusives in the area. One fairly large diorite stock is located near the east claim line.

CURRENT WORK PROGRAM

The current program consisted of surveying in a base line and 5 additional geochem lines on the postulated southern extension of the geochem anomaly mentioned in the "Previous Work" paragraph.

The lines were located 100 meters apart in a north-south direction and each sample station was spaced 50 meters apart. A total of 134 samples were collected over 6500 meters of line. Samples were taken from the "B" horizon except where glacial till prohibited reaching the depth required. The depth of the overburden increased rapidly as the valley floor was approached, and ridges of glacial till were evident especially to the east of the base line.

The samples were collected in cloth bags, hung to dry, then shipped to Acme Laboratories in Vancouver for analysis.

LABORATORY PROCEDURES

The samples were first dried at 105 degrees for 12 hours. They were then sieved through an 80 mesh screen with the

minus 80 fraction retained for analysis. A .5 gram sample was put into a test tube along with 1 ml of water plus 3 ml conc HCL and 1 ml HNO₃. The sample was digested in a water bath at 100 degrees centigrade with an occasional shaking to insure complete digestion. Water was then added to bring the volume up to 10 ml, shaken and allowed to settle. The sample was then run through an atomic absorption apparatus with the appropriate standards.

ASSAY RESULTS

Refer to data sheets from Acme Laboratories.

An ICP analysis of 30 elements was requested from Acme Laboratories.

Using a threshold value of 40 PPM for lead and 175 PPM for zinc there were 54 stations anomalous in lead and 53 stations anomalous in zinc. There were also some spotty silver and arsenic stations. One very high copper value was suspect. Further samples were obtained, but results are not available at this time.

INTERPRETATION

It is apparent that the lead-zinc anomalies extend north and east of the previously known anomaly. The decrease in apparent values of lead and zinc reflect the increasing overburden expected towards the north as the valley floor is approached.

Also the presence of ridges of glacial silts and gravels at the lower elevations, leads to some low values.

The correlation between lead and zinc remains consistent, with erratic values in silver and arsenic which generally occurs as a halo around the anomaly.

The eastward shift of the anomaly towards the north reflects the east dipping strata being successively eroded and being exposed.

RECOMMENDATIONS

The anomaly as it now exists is about 2400 meters in length. It is still open to south and could be expanded in that direction.

As a UTEM survey failed to detect an underlying orebody perhaps a survey with an instrument not so effected by the high voltage power lines which, exists on the eastern edge of the claims, would be advisable.

STATEMENT OF QUALIFICATIONS

NAME: Harry I. Davies

ADDRESS: Box 12 Boswell, B.C. V0B 1A0

EDUCATION: BSc (H) Geology University of Manitoba 1950

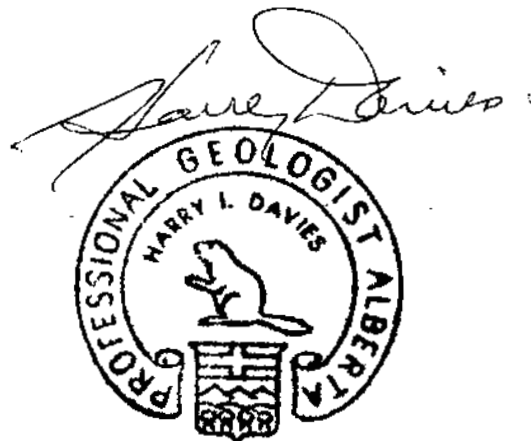
EMPLOYMENT: Manitoba Dept of Mines, three summers field work in Pre-Cambrian area.

Mobil Oil Canada Ltd., 10 years with two years engaged in structural field work.

Consulting Geologist twenty eight years with 25% of time employed in hard rock projects.

ASSOCIATIONS: Professional Engineers of Alberta (Geologist) Membership granted 1960

Harry I. Davies (P.Geol)



STATEMENT OF EXPENDITURES

Costs related to 500 m of base line, soil sampling lines and collecting 134 soil samples on the sun claims, Kitchener area, Nelson Mining Division, British Columbia.

Base line and soil sampling September 1988.

SALARIES:

H. Davies (supervision)	3 days	\$ 900.00
Labor (soil sampling)	5 days	500.00
Base line		200.00

TRANSPORTATION:

4WD (gas & oil incl.)	5 days @ \$60/day	300.00
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ASSAYS:

Acme Laboratories	951.40
Shipping Samples	13.95

SUPPLIES:

Ribbon, thread etc.	25.00
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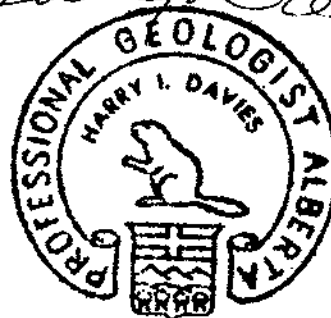
REPORT PREPREATION:

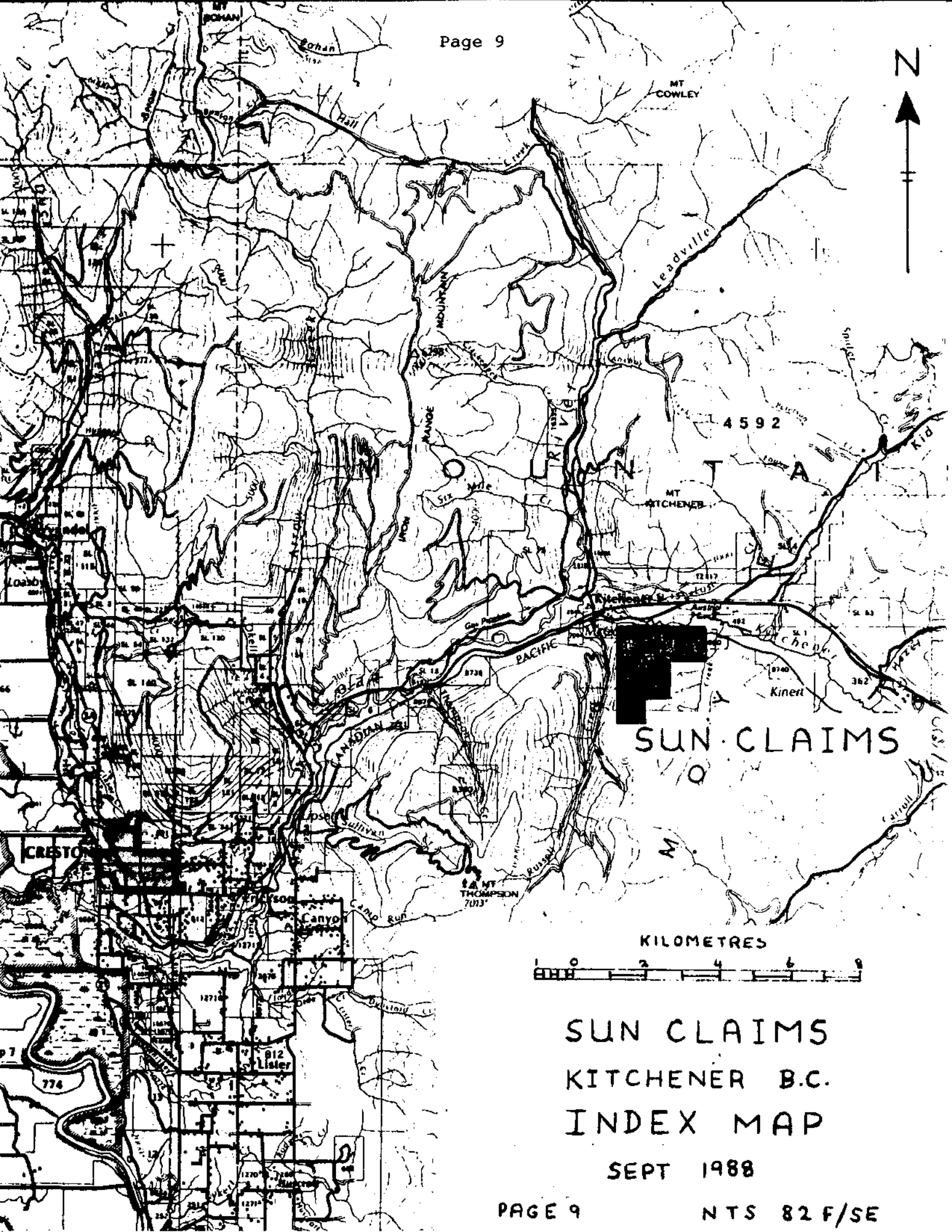
Map construction, writing report	500.00
Drafting, typing, photocopying, etc.	<u>200.00</u>

TOTAL EXPENDITURES

\$3590.35

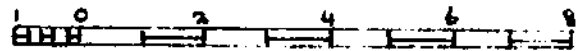
Submitted by H. I. Davies (P.Geol)





SUN CLAIMS

KILOMETRES



SUN CLAIMS
KITCHENER B.C.
INDEX MAP

SEPT 1988

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH HCL 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR Hg Pb Sr Ca P Li Cr Mg Ba Ti B W AND LIMITED FOR Na K AND AL. AN DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: SOIL -80 MESH

DATE RECEIVED: SEP 11 1988

DATE REPORT MAILED: Sept 15/88

ASSAYER: C. Leong D. TOYE OR C. LEONG, CERTIFIED B.C. ASSAYERS

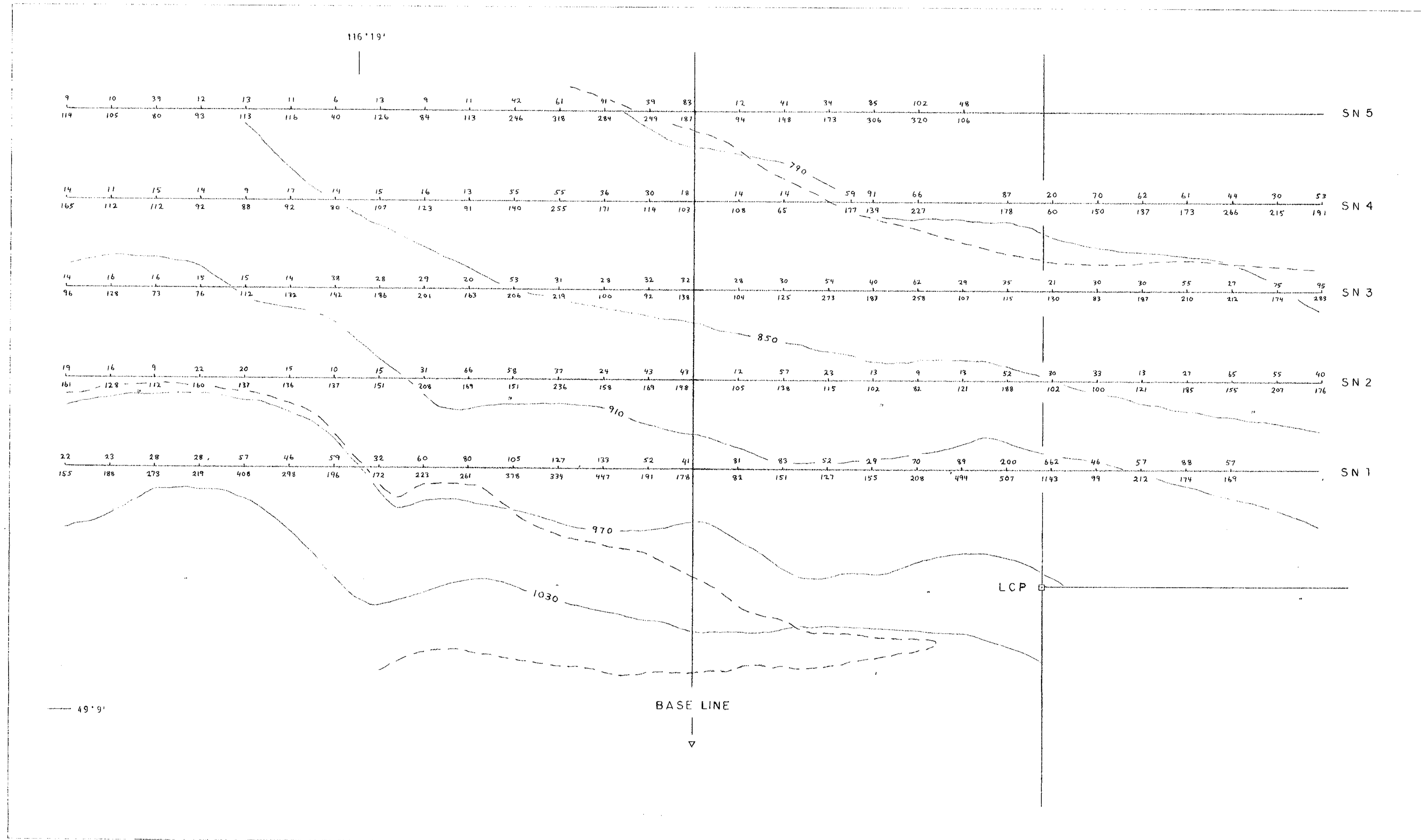
DAVID WIKLUND File # 88-4398 Page 1

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Bi	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	B1	V	Ce	P	La	Cr	Hg	Se	Ti	B	Al	Na	K	W
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM
SW-5 700W	1	12	9	114	.2	19	8	748	1.81	7	6	ND	4	22	1	2	2	24	.15	.167	11	11	.20	223	.06	4	2.76	.02	.11	1
SW-5 650W	1	17	10	105	.1	19	9	517	2.06	6	5	ND	5	22	1	2	2	27	.14	.124	11	12	.26	178	.09	3	3.19	.02	.13	1
SW-5 600W	1	14	39	80	.2	17	9	214	2.04	6	5	ND	6	17	1	2	2	28	.11	.084	12	10	.20	151	.08	2	2.60	.01	.11	1
SW-5 550W	1	12	12	93	.1	15	7	685	1.80	7	5	ND	5	27	1	2	2	25	.17	.119	12	11	.21	201	.08	3	2.41	.01	.12	1
SW-5 500W	1	19	13	113	.2	18	9	277	2.17	6	5	ND	7	22	2	2	2	29	.15	.127	12	12	.26	221	.10	3	3.22	.01	.12	1
SW-5 450W	1	13	11	116	.1	15	7	592	1.93	8	5	ND	4	34	1	2	3	24	.21	.183	9	10	.19	196	.11	2	3.25	.02	.12	1
SW-5 400W	1	8	6	40	.1	8	5	279	1.44	3	5	ND	5	17	1	2	3	17	.14	.076	17	12	.23	112	.03	4	.94	.01	.10	1
SW-5 350W	1	10	13	126	.1	15	6	1007	1.53	5	6	ND	4	32	1	4	2	22	.20	.173	8	8	.13	179	.10	6	3.13	.02	.09	1
SW-5 300W	1	11	9	84	.1	15	7	309	1.50	7	6	ND	4	19	1	2	2	25	.13	.157	10	14	.17	182	.08	2	2.66	.01	.09	1
SW-5 250W	1	19	11	113	.1	18	8	553	1.91	9	6	ND	6	33	1	2	2	24	.18	.394	10	12	.23	227	.08	2	3.15	.01	.14	1
SW-5 200W	1	15	42	246	.4	27	8	816	1.98	9	6	ND	6	27	2	4	2	26	.17	.206	8	9	.17	159	.13	5	4.13	.02	.09	1
SW-5 150W	1	13	61	314	.2	27	9	482	1.80	9	6	ND	6	27	2	2	2	21	.15	.076	17	9	.16	197	.06	4	2.49	.01	.13	1
SW-5 100W	1	13	42	284	.2	24	7	443	1.82	9	5	ND	6	30	2	2	2	22	.18	.123	13	9	.15	212	.10	3	3.29	.02	.09	1
SW-5 050W	1	15	39	249	.3	28	8	1370	2.04	11	9	ND	6	33	2	6	2	27	.21	.163	10	10	.17	231	.10	4	3.77	.06	.23	1
SW-5 000	1	21	83	187	.5	21	9	411	2.04	9	5	ND	6	18	1	2	2	23	.13	.080	21	10	.19	219	.09	2	3.09	.02	.12	1
SW-5 050E	1	19	12	94	.3	20	9	154	2.19	6	5	ND	5	19	1	2	2	28	.14	.262	12	12	.24	128	.09	3	3.39	.02	.13	1
SW-5 100E	1	54	41	148	.4	35	11	1017	3.81	8	9	ND	8	55	1	2	2	31	.76	.069	57	29	.53	234	.07	3	4.16	.01	.31	1
SW-5 150E	1	21	34	173	1.0	27	9	304	2.33	7	5	ND	6	21	2	4	2	28	.18	.136	13	14	.20	161	.11	2	4.54	.02	.13	1
SW-5 200E	1	20	85	306	.5	27	10	364	2.35	8	5	ND	6	27	2	2	2	25	.22	.095	18	15	.26	256	.05	3	3.20	.01	.21	1
SW-5 250E	1	29	102	320	.7	34	11	357	3.33	18	5	ND	8	17	1	2	2	33	.14	.041	14	21	.29	146	.10	5	3.56	.02	.28	1
SW-5 300E	1	16	48	106	.4	19	8	273	2.14	7	7	ND	9	15	2	2	2	21	.16	.011	27	18	.52	107	.05	4	1.95	.01	.18	1
SW-4 700W	1	12	14	165	.4	22	7	1288	1.75	10	5	ND	5	32	2	2	6	23	.21	.241	8	10	.20	178	.09	4	2.82	.02	.13	1
SW-4 650W	1	10	11	112	.3	13	6	542	1.65	4	6	ND	4	17	1	2	2	22	.11	.098	10	9	.16	200	.08	2	2.30	.01	.09	1
SW-4 600W	1	12	15	112	.2	19	7	703	1.64	4	5	ND	4	19	2	2	2	22	.12	.153	10	11	.19	212	.08	2	2.53	.01	.11	1
SW-4 550W	1	9	14	92	.2	18	7	1012	1.70	2	5	ND	5	14	2	2	2	23	.10	.035	12	11	.19	189	.07	3	1.97	.01	.12	1
SW-4 500W	1	15	9	88	.1	20	7	293	1.76	2	5	ND	5	20	2	2	2	25	.12	.188	12	10	.20	179	.09	4	3.03	.02	.10	1
SW-4 450W	1	16	17	92	.1	23	8	344	1.92	5	5	ND	5	20	1	2	2	26	.13	.266	10	13	.22	169	.10	3	2.90	.01	.14	1
SW-4 400W	1	18	14	80	.1	17	7	197	1.87	3	5	ND	6	21	2	2	2	24	.19	.071	13	10	.20	149	.10	4	3.25	.02	.12	1
SW-4 350W	1	14	15	107	.3	21	7	204	2.24	2	6	ND	6	19	2	4	2	29	.15	.081	10	10	.21	180	.12	9	3.95	.02	.12	1
SW-4 300W	1	9	16	123	.2	17	8	629	1.65	4	5	ND	3	16	1	2	2	22	.15	.123	11	11	.18	126	.07	3	1.87	.01	.11	1
SW-4 250W	1	13	13	91	.3	20	8	218	2.11	2	5	ND	5	21	2	2	2	28	.19	.067	9	9	.17	149	.11	4	3.70	.02	.10	1
SW-4 200W	1	32	55	140	.5	23	8	345	2.13	8	6	ND	7	23	2	4	2	28	.14	.139	19	9	.17	191	.13	5	6.68	.03	.11	1
SW-4 150W	1	19	55	255	.4	32	7	343	2.02	7	8	ND	7	25	3	2	2	28	.15	.133	18	12	.19	198	.10	6	3.88	.02	.10	1
SW-4 100W	1	16	36	171	.4	23	8	258	1.79	6	9	ND	6	21	1	4	2	22	.13	.138	13	10	.19	222	.09	2	3.05	.02	.10	1
SW-4 050W	1	11	30	114	.1	17	6	377	1.79	4	5	ND	3	22	1	2	2	24	.16	.178	8	7	.13	166	.10	2	3.50	.02	.08	1
SW-4 000	1	14	18	103	.1	20	8	348	1.82	4	5	ND	4	20	1	4	2	23	.14	.076	14	13	.24	209	.08	2	2.94	.02	.14	1
STD C	17	58	39	132	6.9	67	38	962	4.18	82	22	7	38	47	19	17	18	59	.84	.092	39	35	.88	177	.07	32	1.87	.06	.15	13

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM
SN-4 050K	1	11	14	208	.2	15	8	429	1.80	3	5	ND	3	21	2	2	23	.13	.277	6	8	.16	139	.10	3	3.18	.01	.09	1	
SN-4 100K	1	6	14	65	.1	13	5	465	1.32	2	5	ND	3	12	2	2	17	.11	.078	10	8	.14	164	.05	3	1.94	.01	.08	2	
SN-4 175E	1	13	59	177	.6	23	9	685	2.05	6	5	ND	5	24	1	2	3	.23	.137	10	10	.19	157	.09	3	3.42	.01	.12	1	
SN-4 200K	1	22	91	139	.2	18	8	137	2.39	12	6	ND	7	9	1	2	2	19	.07	.029	26	14	.31	101	.02	2	1.30	.01	.11	2
SN-4 250E	1	13	66	227	.7	24	8	1152	2.00	6	5	ND	5	20	3	2	2	23	.13	.224	13	12	.20	203	.07	3	3.32	.01	.09	1
SN-4 350E	1	29	97	178	.3	29	12	638	3.40	8	7	ND	11	31	1	2	2	31	.44	.030	28	24	.40	202	.08	2	3.52	.02	.25	1
SN-4 400E	1	21	20	60	.1	20	9	340	2.82	8	9	ND	12	8	2	2	2	20	.10	.016	40	17	.71	48	.03	2	1.37	.01	.23	2
SN-4 450E	1	27	70	150	.3	19	8	244	2.53	8	8	ND	8	13	2	2	2	27	.11	.012	22	19	.31	102	.05	2	2.51	.01	.12	1
SN-4 500E	1	14	62	137	.1	13	7	322	1.90	8	5	ND	4	16	2	2	2	19	.18	.032	21	9	.20	79	.02	2	1.37	.01	.12	2
SN-4 550E	1	18	61	173	.2	21	6	423	1.83	4	8	ND	6	18	2	2	2	22	.15	.015	20	13	.29	92	.04	4	1.75	.01	.12	2
SN-4 600E	1	12	44	266	.3	18	8	503	2.01	3	9	ND	6	13	3	2	3	23	.09	.063	13	11	.18	209	.06	4	3.28	.01	.13	1
SN-4 650E	1	14	30	215	.6	16	6	835	1.83	6	5	ND	4	23	2	2	2	24	.17	.239	8	9	.13	136	.10	2	3.47	.01	.09	1
SN-4 700E	1	14	53	191	.4	27	10	572	2.89	11	7	ND	9	24	2	7	2	31	.14	.091	15	13	.21	227	.12	4	5.40	.02	.13	1
SN-3 700W	1	20	14	96	.2	27	7	151	2.07	6	7	ND	9	23	1	2	2	28	.17	.117	16	13	.22	128	.13	2	4.05	.02	.10	1
SN-3 650W	1	16	16	128	.2	26	8	352	2.12	6	6	ND	7	21	2	2	2	27	.15	.116	14	12	.23	155	.11	3	3.53	.02	.11	1
SN-3 600W	1	21	16	73	.4	22	7	180	1.73	6	5	ND	5	23	2	2	2	23	.16	.098	14	9	.18	138	.11	2	3.57	.03	.08	1
SN-3 550W	1	20	15	76	.1	21	8	206	2.12	4	7	ND	7	20	1	2	2	27	.14	.058	15	12	.25	237	.09	2	2.85	.01	.13	1
SN-3 500W	1	12	15	112	.1	20	7	340	1.85	12	5	ND	3	26	1	7	2	25	.18	.356	7	8	.11	168	.13	2	4.41	.02	.06	2
SN-3 450W	1	16	14	132	.2	20	7	353	1.66	6	6	ND	5	24	2	2	4	22	.17	.128	16	8	.12	127	.13	2	3.55	.02	.08	1
SN-3 400W	1	13	38	142	.1	18	8	258	1.97	7	5	ND	6	25	1	2	2	19	.14	.250	12	10	.22	196	.06	2	2.20	.01	.11	2
SN-3 350W	1	13	28	186	.3	19	7	614	1.80	12	5	ND	5	26	2	2	2	21	.20	.236	10	10	.17	196	.10	2	2.73	.02	.10	1
SN-3 300W	1	12	29	201	.3	20	6	807	1.69	7	5	ND	5	26	2	2	2	22	.17	.236	7	9	.13	202	.10	5	3.07	.02	.08	2
SN-3 250W	1	14	20	163	.4	28	6	173	1.70	8	5	ND	4	30	2	2	2	24	.20	.183	10	7	.14	121	.13	3	4.00	.02	.08	1
SN-3 200W	1	16	53	206	.1	27	7	694	1.79	15	5	ND	6	26	3	2	3	19	.16	.254	12	8	.14	172	.08	2	3.14	.02	.10	1
SN-3 150W	1	18	31	219	.3	28	7	397	1.84	7	5	ND	5	26	2	2	2	25	.20	.136	12	10	.18	197	.12	2	3.52	.02	.09	1
SN-3 100W	1	19	28	100	.6	21	8	198	2.01	5	6	ND	7	19	2	2	2	25	.16	.053	19	12	.27	159	.09	6	2.77	.01	.12	1
SN-3 050W	1	16	32	92	.2	21	7	258	1.93	9	7	ND	5	19	2	2	2	23	.22	.014	22	14	.32	85	.06	3	1.92	.01	.15	1
SN-3 000	1	24	32	138	.7	25	8	295	2.68	11	5	ND	8	30	3	4	4	28	.23	.054	16	15	.24	172	.13	2	4.64	.02	.16	1
SN-3 050E	1	16	28	104	.4	19	7	160	2.05	5	7	ND	6	19	3	3	2	26	.14	.066	11	9	.18	115	.12	4	3.98	.02	.10	1
SN-3 100E	1	18	30	125	.5	21	8	301	1.86	5	6	ND	6	19	2	2	2	24	.18	.068	16	10	.21	156	.10	3	3.40	.02	.10	1
SN-3 150E	1	13	54	273	.8	24	7	968	1.47	4	5	ND	4	18	3	2	2	20	.13	.165	9	9	.15	190	.09	5	2.51	.02	.08	1
SN-3 200E	1	15	40	183	.9	23	7	663	1.74	4	5	ND	5	21	3	2	2	21	.15	.306	8	7	.13	167	.12	4	3.64	.02	.07	1
SN-3 250E	1	15	62	258	1.0	32	9	367	2.13	7	8	ND	6	22	3	2	2	25	.15	.099	15	12	.24	169	.10	5	3.64	.02	.11	1
SN-3 300E	1	19	29	107	.5	21	7	395	2.08	7	5	ND	6	20	1	2	3	27	.18	.078	13	11	.19	131	.11	3	3.87	.02	.10	1
SN-3 350E	1	15	35	115	.4	20	8	212	2.27	9	5	ND	5	21	1	2	4	25	.29	.053	14	14	.25	99	.09	2	3.64	.02	.10	1
SN-3 400E	1	12	21	130	.2	16	7	432	1.91	6	5	ND	4	16	1	2	3	22	.15	.168	10	13	.21	134	.08	2	2.82	.01	.12	1
STD C	18	56	39	132	6.7	67	30	1034	4.34	40	21	8	37	47	19	16	19	59	.45	.892	39	55	.91	176	.87	32	1.93	.06	.15	12

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	V	Au	Tb	St	Cd	Kr	HI	V	Ca	P	La	Cr	Hg	Be	Zi	B	Al	Mg	K	PPM
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM
SN-3 850Z	1	17	30	83	.2	17	7	174	1.88	6	5	ND	7	17	1	3	4	24	.23	.010	10	10	.31	105	.06	3	2.14	.01	.16	1
SN-3 500Z	1	11	30	187	.1	13	6	805	1.75	4	5	ND	4	15	2	2	2	24	.12	.004	11	9	.13	165	.09	2	2.02	.02	.10	1
SN-3 550Z	1	15	55	210	.2	21	7	610	1.85	7	5	ND	7	18	2	2	2	23	.12	.117	15	10	.19	172	.08	2	2.02	.01	.11	1
SN-3 600Z	1	15	27	212	.5	22	7	285	1.86	5	5	ND	6	24	4	5	2	25	.16	.165	9	8	.15	169	.12	6	4.14	.02	.10	1
SN-3 650Z	1	33	75	174	.4	27	12	162	2.33	8	5	ND	13	18	3	4	2	27	.10	.059	14	11	.23	193	.08	4	3.33	.01	.10	1
SN-3 700Z	1	34	95	283	.3	34	10	485	2.59	12	7	ND	10	22	3	5	2	27	.13	.121	17	17	.27	281	.49	2	3.69	.02	.21	1
SN-2 700W	1	11	19	161	.1	28	7	1018	1.62	4	5	ND	4	48	1	2	2	20	.22	.275	10	10	.19	213	.09	2	2.75	.02	.13	1
SN-2 650W	1	11	16	129	.2	18	5	605	1.52	7	5	ND	4	27	1	5	2	21	.19	.282	7	7	.10	152	.12	3	3.84	.02	.08	1
SN-2 600W	1	11	9	112	.1	16	5	477	1.55	9	5	ND	4	34	2	5	2	22	.24	.394	5	7	.10	175	.13	2	3.94	.02	.06	1
SN-2 550W	1	12	22	160	.2	36	8	229	1.75	3	7	ND	5	21	2	2	2	22	.15	.101	15	15	.22	223	.09	4	2.63	.02	.14	1
SN-2 500W	1	13	20	137	.1	24	7	543	1.65	17	5	ND	5	30	1	4	2	23	.20	.179	10	8	.17	163	.11	2	2.85	.02	.12	1
SN-2 450W	1	18	15	136	.3	24	6	269	1.66	5	5	ND	4	25	2	2	2	23	.21	.220	7	8	.15	83	.11	2	3.12	.02	.10	1
SN-2 400W	1	13	10	137	.4	29	6	169	1.85	8	5	ND	6	31	2	5	2	26	.21	.144	7	8	.15	109	.13	4	4.19	.02	.08	1
SN-2 350W	1	14	15	151	.1	27	9	553	1.79	5	5	ND	5	32	2	2	2	23	.19	.163	12	9	.19	162	.10	3	2.47	.01	.12	1
SN-2 300W	1	12	31	208	.1	27	7	906	1.68	7	5	ND	4	28	2	3	2	24	.18	.138	10	8	.15	175	.12	2	3.14	.02	.10	1
SN-2 250W	1	16	66	169	.1	29	8	352	1.80	9	5	ND	8	13	2	2	2	18	.08	.046	19	9	.20	166	.06	2	2.04	.01	.13	1
SN-2 200W	1	17	58	151	.1	22	8	369	1.76	10	5	ND	7	19	2	4	2	19	.14	.801	18	8	.17	139	.07	2	2.08	.01	.11	1
SN-2 150W	1	12	37	236	.2	35	7	521	1.55	3	5	ND	5	29	2	2	2	21	.21	.154	12	9	.18	139	.10	2	2.75	.02	.12	1
SN-2 100W	1	11	24	158	.2	24	6	743	1.62	7	5	ND	4	23	2	2	2	21	.16	.218	10	9	.18	142	.08	3	2.45	.01	.11	1
SN-2 050W	1	10	43	169	.1	18	9	771	2.16	16	5	ND	4	20	1	3	2	26	.19	.183	11	10	.18	111	.08	2	2.23	.01	.12	1
SN-2 800	1	15	43	190	.1	24	8	574	1.83	7	8	ND	6	21	3	2	2	24	.13	.150	11	10	.19	159	.08	3	3.01	.02	.11	1
SN-2 050R	1	14	12	105	.2	19	7	160	1.64	2	6	ND	6	26	1	2	2	22	.15	.046	15	11	.24	102	.08	2	2.32	.02	.11	1
SN-2 100R	1	18	57	138	1.2	18	7	222	1.84	11	5	ND	5	19	1	4	2	25	.13	.201	9	9	.20	121	.12	2	3.48	.02	.11	1
SN-2 150R	1	21	23	115	.3	20	6	217	1.67	9	5	ND	5	27	1	5	2	22	.19	.145	14	8	.14	129	.13	2	4.06	.03	.08	1
SN-2 200Z	1	22	13	102	.5	17	5	136	1.56	5	5	ND	5	24	2	5	2	23	.16	.097	15	8	.14	118	.13	3	3.81	.03	.07	1
SN-2 250Z	1	15	9	82	.1	15	6	370	1.49	4	5	ND	4	19	1	2	2	21	.15	.125	20	10	.16	126	.09	2	2.79	.02	.09	1
SN-2 300Z	1	12	13	121	.1	17	6	323	1.72	3	5	ND	4	24	1	3	2	22	.21	.219	10	9	.16	145	.11	2	3.38	.02	.11	1
SN-2 350Z	1	20	52	188	.5	22	8	246	2.32	12	5	ND	6	16	1	5	2	29	.13	.008	14	14	.26	173	.10	2	3.51	.01	.15	2
SN-2 400Z	1	10	30	102	.3	15	7	230	1.75	11	5	ND	6	22	2	2	4	23	.18	.025	16	18	.27	120	.06	2	2.28	.01	.12	1
SN-2 450Z	1	20	33	100	.3	19	8	209	2.27	13	7	ND	8	41	1	3	2	26	.21	.023	15	15	.26	184	.08	2	3.35	.02	.16	1
SN-2 500Z	1	16	13	121	.1	20	7	176	1.95	7	5	ND	7	19	1	2	2	20	.14	.187	13	11	.23	122	.11	2	3.17	.02	.11	1
SN-2 550Z	1	14	27	185	.3	20	9	173	2.07	9	5	ND	5	17	1	3	2	27	.15	.093	9	9	.14	129	.12	3	4.13	.02	.08	1
SN-2 600Z	1	19	65	155	.1	22	12	163	1.97	6	7	ND	8	15	2	3	2	23	.12	.046	19	15	.25	164	.04	4	1.99	.01	.13	1
SN-2 650Z	1	20	55	207	.4	22	10	346	1.87	6	14	ND	7	17	2	2	2	22	.18	.093	17	10	.21	149	.06	3	2.28	.01	.12	1
SN-2 700Z	1	17	40	176	.1	24	8	298	1.76	7	5	ND	7	18	1	2	2	23	.14	.122	14	14	.24	182	.07	2	2.62	.01	.10	1
SN-1 700W	1	6	22	155	.1	19	9	464	1.55	5	5	ND	2	19	1	3	2	21	.13	.064	7	8	.12	138	.09	2	2.31	.01	.08	2
STD C	18	58	37	132	6.7	67	30	1018	4.15	41	21	7	30	47	18	16	20	39	.44	.096	39	55	.87	177	.87	32	1.83	.06	.15	13

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Bi PPM	Co PPM	Mn PPM	Fe %	As PPM	V PPM	Au PPM	Tb PPM	Sr PPM	Cd PPM	Sb PPM	Si PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Hg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
SM-1 650W	1	12	23	188	.1	33	7	420	1.98	23	5	ND	5	24	1	2	2	23	.15	.129	9	9	.16	167	.13	2	3.67	.02	.09	1
SM-1 600W	1	10	28	273	.2	33	7	677	1.92	21	5	ND	4	20	1	2	2	22	.20	.130	8	8	.15	174	.13	2	3.38	.02	.09	1
SM-1 550W	1	10	28	219	.1	27	6	510	1.67	16	5	ND	4	26	1	2	2	18	.20	.186	15	10	.22	172	.08	3	2.01	.01	.15	1
SM-1 500W	1	12	57	400	.3	27	7	420	1.96	30	5	ND	5	29	1	2	2	22	.19	.144	11	9	.17	182	.13	4	3.53	.02	.09	2
SM-1 450W	1	13	46	298	.3	29	6	380	1.96	25	5	ND	5	33	1	2	2	23	.23	.154	9	8	.15	137	.15	2	3.93	.02	.08	2
SM-1 400W	1	16	59	196	.2	31	7	261	2.19	29	5	ND	5	32	1	2	2	27	.24	.169	7	11	.18	113	.15	5	4.49	.02	.09	3
SM-1 350W	1	8	32	172	.1	20	6	628	1.53	6	5	ND	4	20	1	2	2	18	.16	.072	13	9	.20	159	.07	2	1.72	.01	.12	1
SM-1 300W	1	12	60	223	.4	32	8	352	2.10	22	5	ND	4	22	1	2	3	25	.17	.195	10	10	.21	155	.11	2	3.32	.02	.11	2
SM-1 250W	1	12	80	261	.2	22	7	439	2.01	19	5	ND	5	24	1	2	3	24	.19	.085	11	14	.24	136	.10	3	2.91	.01	.13	1
SM-1 200W	1	9	105	378	.2	31	7	315	2.13	13	5	ND	5	17	1	2	2	26	.18	.056	12	13	.24	134	.09	3	2.47	.01	.12	1
SM-1 150W	1	10	127	334	.3	25	7	679	1.99	16	5	ND	3	24	1	2	2	23	.21	.061	13	13	.24	166	.07	2	2.15	.01	.13	1
SM-1 100W	1	7	133	447	.1	16	7	1756	1.60	14	5	ND	2	29	4	2	2	19	.25	.174	10	9	.14	209	.08	4	2.00	.02	.12	1
SM-1 050W	1	11	52	191	.1	22	6	455	1.70	10	5	ND	4	21	1	2	2	21	.18	.089	14	11	.21	161	.08	2	2.35	.01	.10	1
SM-1 000	1	8	41	178	.2	18	6	912	1.65	8	5	ND	3	19	1	2	2	20	.14	.102	13	10	.19	195	.07	4	1.98	.01	.11	2
SM-1 050E	1	13	31	82	.1	17	6	278	1.64	9	5	ND	4	20	1	2	2	16	.16	.092	18	9	.24	123	.04	2	1.18	.01	.17	1
SM-1 100E	1	26	83	151	.2	22	11	540	2.82	14	5	ND	8	25	1	2	2	21	.17	.095	29	16	.39	117	.03	2	1.85	.01	.20	1
SM-1 150E	1	21	52	127	.4	29	8	675	2.14	22	5	ND	6	29	1	2	2	24	.22	.088	15	14	.27	179	.09	3	3.42	.02	.13	1
SM-1 200E	1	2011	29	155	1.1	25	7	605	1.84	20	5	ND	4	28	1	2	2	22	.21	.131	10	11	.19	182	.04	2	3.01	.02	.10	1
SM-1 250E	1	20	76	208	.3	20	7	434	1.75	18	5	ND	5	18	1	2	2	19	.14	.047	15	11	.26	155	.06	2	1.81	.01	.16	1
SM-1 300E	1	8	89	494	.5	21	7	1442	1.64	15	5	ND	3	31	6	2	2	19	.30	.084	13	11	.20	195	.07	4	1.95	.02	.15	1
SM-1 350E	1	17	200	507	1.9	20	6	834	1.92	26	5	ND	5	19	3	2	2	22	.14	.142	13	9	.17	112	.13	2	3.55	.02	.09	1
SM-1 400E	1	27	662	1143	2.2	30	7	555	2.43	42	6	ND	5	26	3	3	2	21	.23	.123	11	9	.21	119	.10	3	2.73	.02	.12	1
SM-1 450E	1	15	46	99	.8	18	11	520	2.51	28	5	ND	4	29	1	2	2	20	.35	.109	8	11	.15	125	.14	10	4.35	.02	.13	1
SM-1 500E	1	13	57	212	.2	23	7	346	2.12	21	5	ND	6	22	1	2	2	22	.16	.147	15	11	.23	127	.08	2	2.55	.01	.09	1
SM-1 550E	1	19	80	174	.1	16	9	424	2.35	25	5	ND	8	14	1	2	2	19	.13	.137	22	10	.27	111	.03	2	1.38	.01	.12	1
SM-1 600E	1	17	57	169	.3	20	7	425	2.12	18	5	ND	5	17	1	2	2	21	.16	.087	18	18	.24	124	.06	3	2.12	.01	.10	1
STD C	18	59	43	132	7.1	67	30	1025	4.22	37	22	7	38	46	19	17	23	59	.58	.096	39	56	.93	178	.07	32	2.03	.06	.15	13



790 ELEVATION (M)

ROAD

95 PB
293 ZN SAMPLE STATION

METERS
50 0 50 100
SCALE 1:2500

SUN CLAIMS
KITCHENER B.C. NELSON MINING DIVISION
PB-ZN SOIL SAMPLING
RESULTS IN PPM

FIGURE 1 DATE SEPT. 1988
BY H.I. DAVIES