GEOCHEMICAL AND GEOPHYSICAL SURVEYING

TRENCHING AND DRILLING REPORT

- on the -

RHUB 1 - 13 and BARB 1 CLAIMS

Omineca Mining Division
British Columbia

N.T.S. 93F/11W and 12E

Lat. 53 37'N, Long. 125 30'W

- for -

MINGOLD RESOURCES INC.
709 - 837 West Hastings Street
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- by -

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Part 1 of 2

December, 1988

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INTRODUCTION

This report describes the exploration program carried out by Mingold Resources Inc., on the RHUB 1-13 and BARB 1 claims. This included 27.5 kilometers of VLF-EM, 1500 soil samples, 21.7 kilometers of control grid, 365 meters of backhoe trenching, 16 reverse-circulation drill holes totalling 1214.9 meters, and 6 diamond drill holes totalling 1036.9 meters. This work was done from November 1-22, 1987 and May 6 to August 9, 1988.

LOCATION AND ACCESS

The RHUB and BARB claims are located 70 km south of Burns Lake on the north shore of Intata Reach within the Nechako Reservoir watershed. The property spans the boundary between the 93F/11W and 93F/12E mapsheets and is centered at latitude 53 37'N and longitude 125 30'W.

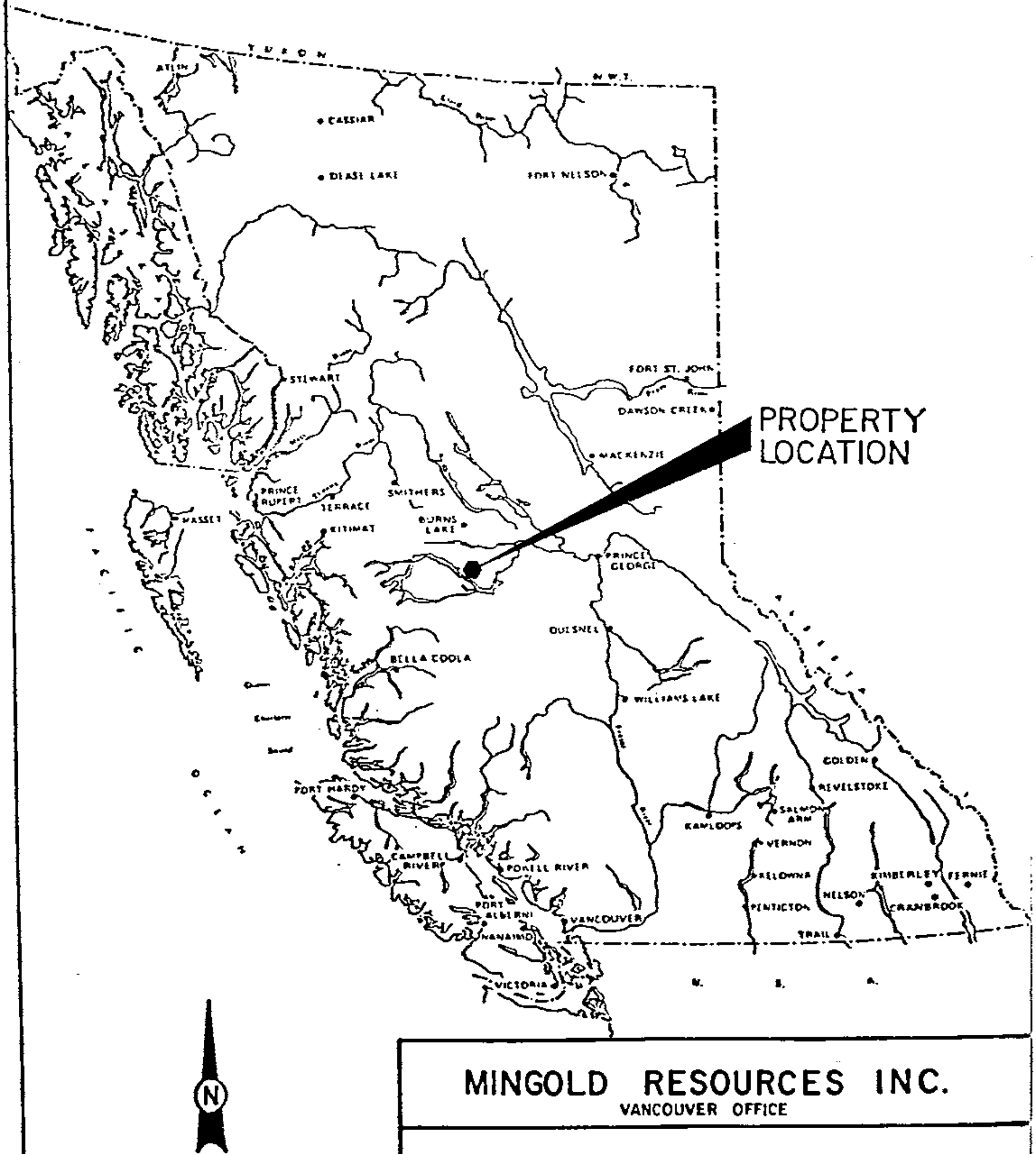
Access to and within the property is excellent with a network of logging roads traversing most of the claims. These roads are connected to two major haulage routes - one to Burns Lake via the Francois Lake Ferry and the other to Vanderhoof. Much of the logging in this area is done in the winter so the haulage roads are maintained year round.

Topography in general is quite subdued. Elevations vary from 900 meters (2950 feet) to 1370 meters (4500 feet) although much of the area varies by less than 100 meters (325 feet). Glaciation has strongly influenced the area resulting in a distinct ENE trend to most topographic features and a heavy mantling of the area in till.

Much of the claim block has been clear-cut logged in recent years and is now in various stages of regrowth. Where untouched, the forest cover consists of mature stands of spruce, fir and pine interspersed with aspen and small alder. Valley bottoms are often occupied by swamps and/or lakes surrounded by dense intergrowths of buckbrush and willow.

CLAIMS

The RHUB-BARB property consists of a contiguous block of 15 mineral claims totalling 283 units. The claims occur in the Omineca Mining Division and are wholly owned by Mingold Resources Inc. In September of 1988, all the claims, except for RHUB 14, were grouped into three blocks for assessment purposes. A summary of the claim information is included in Table 1 below:

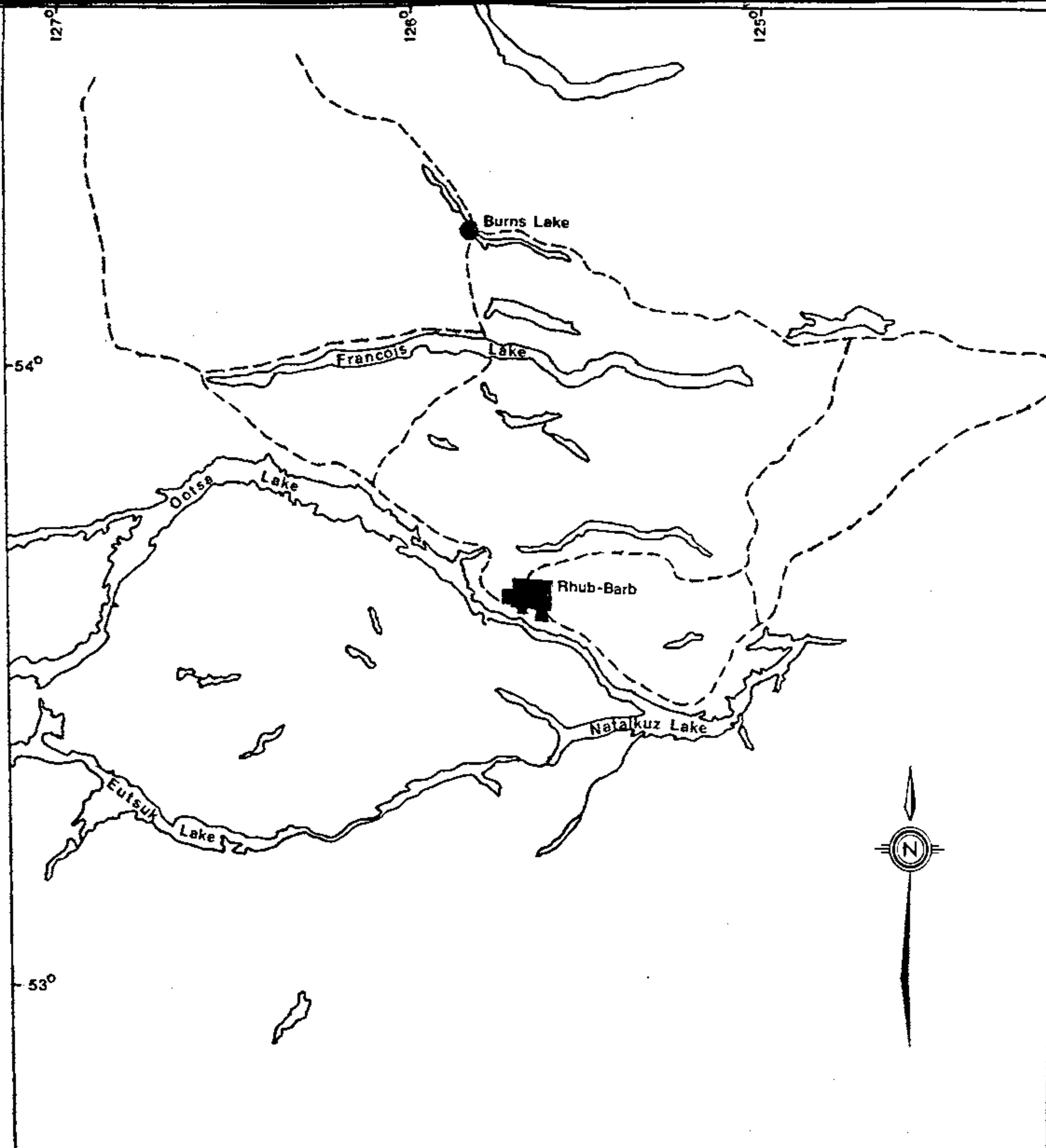


MINGOLD RESOURCES INC.

VANCOUVER OFFICE

LOCATION MAP

DRAWN BY:	DATE: Dec. '88	APPROVED BY
BRITISH COLUMBIA	0 100 200 300 KM.	1



MINGOLD RESOURCES INC.

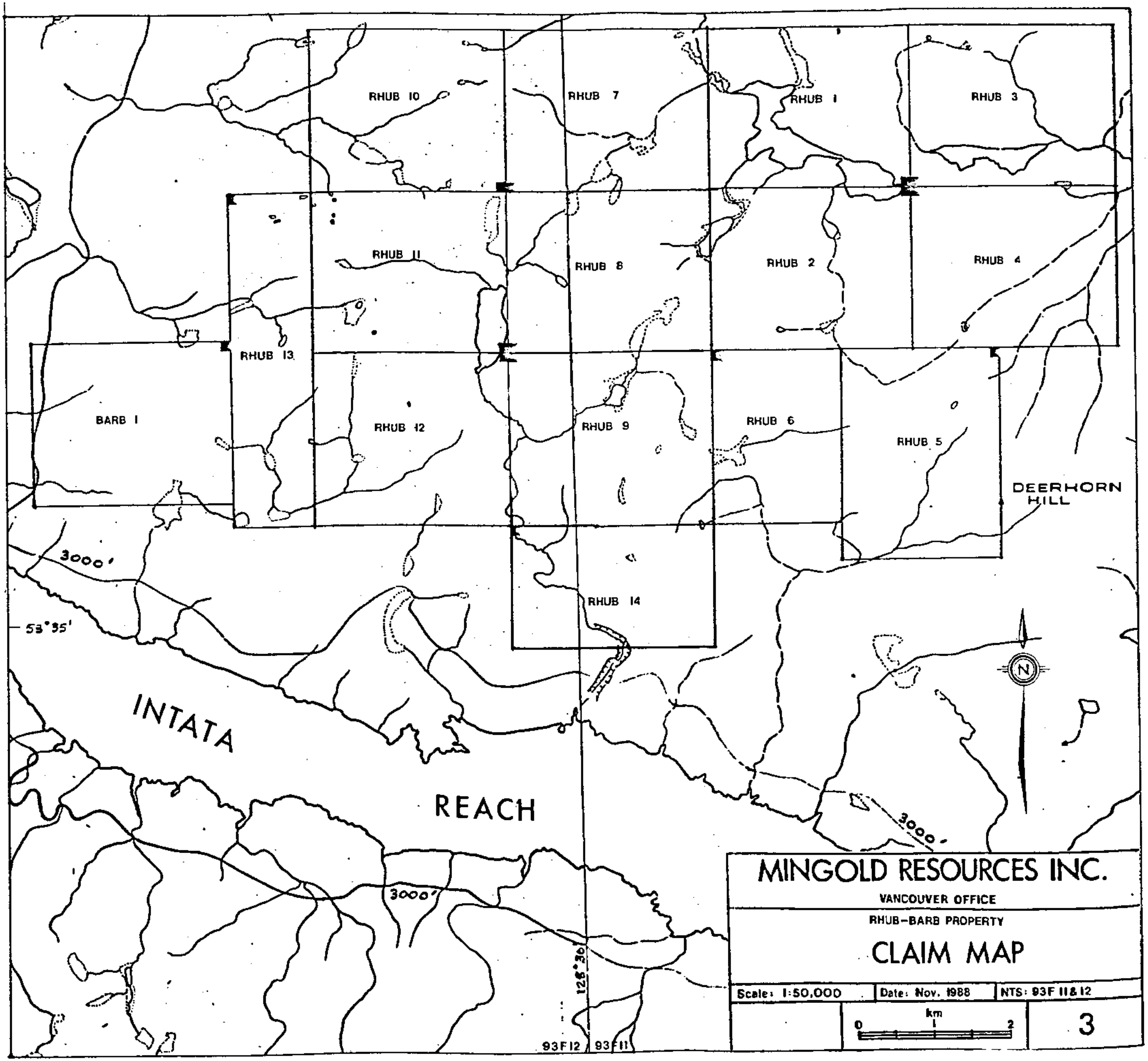
VANCOUVER OFFICE

OOTSA LAKE PROJECT

Scale: 1:1,000,000 | Date: Nov. 1988 | NTS: 93E&F

km 0 10 20 30 40

Figure No. 2


RHUB 10
RHUB 7
RHUB 1
RHUB 3
RHUB 11
RHUB 8
RHUB 2
RHUB 4
RHUB 13
BARB 1
RHUB 12
RHUB 9
RHUB 6
RHUB 5
DEERHORN HILL
RHUB 14
3000'
53°35'
INTATA
REACH
3000'
3000'
128°30'
93F12
93F11
MINGOLD RESOURCES INC.
VANCOUVER OFFICE
RHUB-BARB PROPERTY
CLAIM MAP
Scale: 1:50,000
Date: Nov. 1988
NTS: 93F 11&12
km
0
1
2
3

	CLAIM NAME	RECORD NO.	NO. OF UNITS	EXPIRY DATE
	Barb 1	7930	20	Sept. 22, 1993
Group I	Rhub 10	8046	20	Oct. 23, 1993
(96 units)	Rhub 11	8047	20	Oct. 23, 1993
	Rhub 12	8048	20	Oct. 23, 1993
	Rhub 13	8049	16	Oct. 23, 1993
	Rhub 1	7933	20	Sept. 24, 1994
Group II	Rhub 3	7935	20	Sept. 24, 1994
(100 units)	Rhub 7	8043	20	Oct. 23, 1998
	Rhub 8	8044	20	Oct. 23, 1998
	Rhub 9	8045	20	Oct. 23, 1998
	Rhub 2	7934	20	Sept. 24, 1990
Group III	Rhub 4	7936	20	Sept. 24, 1990
(72 units)	Rhub 5	8041	20	Oct. 23, 1990
	Rhub 6	8042	12	Oct. 23, 1990
	Rhub 14	9540	15	July 12, 1989

*NOTE - Expiry dates include assessment credits presently being applied.

PROPERTY HISTORY

The first known work in the area was by H.W. Tipper of the Geological Survey of Canada in 1949. At that time, he carried out the initial government mapping of the area which was later published in G.S.C. Memoir 324. Since that time, no record of assessment for the claim area is known until 1980. During this period, it is believed that the area received sporadic exploration for porphyry type deposits and possibly for perlite. Due to the extensive overburden and poor geochemical response in the areas, nothing of economic interest was located., In recent years, with the increase in gold prices and the success of the Nevada type epithermal gold deposits, several major mining companies tested this area for its epithermal potential. It appears that most encountered the same problems that hampered earlier exploration due to their strong reliance on geochemistry. In 1980, Guichon Explorco Ltd. staked the MAR claims covering much of the area of the present RHUB claims. They recognized the epithermal nature of the mineralization and also the lack of geochemical response in soils and silt samples. Rock-chip sampling outlined two zones of epithermal alteration with elevated levels in arsenic, mercury and to a lesser extent gold. Although more detailed rock-chip sampling was recommended, (Ireland, 1981) it appears that this work was not carried out.

In the summer of 1985, two Hudson Bay Exploration (later became Mingold Resources) personnel examined the MAR claims area as part of an initial study of the Ootsa Lake Volcanics package. Although this study was only of cursory nature to assess the epithermal potential of the volcanics for a program the next year, several float samples of chalcedonic quartz were found in the area of the old MAR 11 claim. One sample assayed 70 ppb gold which spurred our interest in the area and the Ootsa Lake Volcanics package in general. In 1986, the RHUB and BARB claims were staked to cover the Guichon Explorco mineralized area and an outcrop with moderately anomalous gold values on the Barb 1 claim discovered by Mingold personnel.

In the summer of 1987, the source of chalcedonic quartz on the the old Mar II claim was located. Subsequent prospecting and trenching outlined an area of epithermal silver and gold mineralization in altered Ootsa Lake Volcanics. This prospect is referred to as the "Silver Zone" and has been the main focus of attention thus far. Silver values are as high as 17.86 oz/ton and gold values are as high as 0.209 oz/ton.

The showing on the Barb 1 claims was further exposed by trenching and although epithermal veins up to one meter wide were found, silver and gold values were less than 0.5 oz/t and 0.03 oz/t respectively. This showing is referred to as the "Barb Zone."

A reverse circulation drill program was carried out on the "Silver Zone" and "Barb Zone" in the fall of 1987. Results of this program are described later in this report.

In 1988, detailed grid surveys were conducted over VLF-EM targets obtained in 1987. In addition, trenching and diamond drilling was done on the "Silver Zone". A new zone referred to as the "Quarry Zone" was located southwest of Davidson Lake. The occurrence consists of an area of epithermal quartz veining and breccia with weakly anomalous gold values. No drilling of this zone has been done to test for better grade mineralization at depth.

GEOLOGY

The RHUB-BARB claims occur in the south-central part of the Intermontane Geological Belt of the Northern Cordillera.

Lithologies range in age from late Triassic through Miocene with intermediate to felsic volcanics being the dominant rock types.

The oldest rocks in the area are the U. Triassic Takla Group Volcanics which consist of an island arc sequence of intermediate to basic volcanics. These were superceded by the Hazelton Group Volcanics in early to mid-Jurassic time. Although this package of dominantly calc-alkaline basaltic to rhyolitic volcanics is prevalent elsewhere in the region, it is relatively scarce immediate to the claim area.

The lower Mesozoic rocks are overlain unconformably by an extensive volcanic sequence known as the Ootsa Lake Volcanics. These are the dominant rocks in the area and consist of U. Cretaceous to Eocene subaerial flows and pyroclastics mainly of felsic to intermediate composition. These rocks are widespread, occupying depressions in the eroded pre-Tertiary surface.

These rocks are in turn overlain unconformably by andesitic to basaltic flows of the Oligocene to Miocene Endako Group. They are relatively flat lying and believed to have resulted from "plateau-type" extrusion into the area. Due to erosion and glacial scouring, exposures typically occur on the tops of the higher ridges.

The region is structurally complex. The strong northwesterly trending fault system typical of the Cordillera has been very active in this area. Strong northeasterly trending and northerly trending faults have also developed and may be associated with a collapsed cauldera system in the area.

CONTROL GRID

In 1987, six separate detailed grids were located over areas of significant float or bedrock gold or silver geochem anomalies. Soil and VLF-EM and limited magnetometer and resistivity (EM-16R) surveys were carried over these areas. A reconnaissance scale (300 meter spacing) grid was then established using a single base line (20N) located along the southern portion of the claims block. All lines, including the baseline, were located by hip-chain and marked by flagging. Significant discrepancies in the location of the various lines resulted.

In 1988, a series of baselines and tie lines were established by nylon chain and picketed every 25 meters. The old 20N baseline was re-established using the old 0+00 station as a starting point. All old lines were tied into the new control grid wherever possible. Baselines were established at 20N, 30N and 40N as shown on Plate No. 1 (pocket). Tielines were located at 0+00, 33E and 60E. In total 17.7 kilometers of baseline and 4.0 kilometers of tieline was established. No linecutting was done as the presence of large clearcut areas and generally light timber made this unnecessary. A chainage error on the 0+00 tieline resulted in the 30N baseline actually being at 30+25N on the west side of Sam Hardy Lake.

A series of seven detailed grids designated Grid "A" through Grid "G" were establised using the new control grid. These grids were located over areas of extremely high (Fraser-filtered values greater than 40) or intersecting EM conductors assumed to be associated with major fault structures.

SOIL GEOCHEMISTRY

A total of 1500 soil samples were collected on the RHUB-BARB claims in 1988. Of these, 432 samples were from the Group I claims, 492 samples were from the Group II claims and 576 were from the Group III claims.

Soil sampling was carried out over seven different detailed grids designated "A" through "G" and also on the Quarry Zone and the eastern part of the Silver Discovery Grid (4417 Grid)-see Plate No. 2 to 10. For a breakdown of the sampling on each grid see Table 2 below:

TABLE 2 - Soil Geochemistry Breakdown

GRID NAME	NO. OF SAMPLES	CLAIM GROUP NO.
A	240	I
B	96	I
C	96	I
D	183	II (91), III (92)
E	173	III
F	176	II
G	84	II
QUARRY	29	III
4417 GRID	48	II
	1125	

In addition, another 375 soils were taken on the old reconnaisance lines 51E, 54E, 57E, 60E, 63E, 66E, 69E and 72E. 93 samples were taken on Group II claims and 282 samples were taken on Group III claims (see Plate No. II).

SAMPLING PROCEDURE

Soil samples were collected on chain and compass grid lines which were spaced 100 meters apart with a 25 meter sample spacing. Reconnaisance samples were taken on lines 300 meters apart with a 25 meter sample spacing. Where Reconnaisance lines overlapped with old detailed grids no samples were taken.

Samples were collected from a depth of 15 to 25cm in the gray brown "B" horizon and placed in gussetted Kraft bags. Due to the heavy glacial overburden over much of the area, the "B" horizon sampled may not be a true "B" horizon. Some oxidation of this layer has occurred but till layers probably are not permitting the normal circulation of ground waters to occur.

Samples were air-dried and then shipped to Acme Analytical Laboratories in Vancouver for analysis.

ANALYTICAL PROCEDURE

All samples sent to the lab are dried and then sieved to -80 mesh. A 0.5 gram sample of this material is then digested with 3 ml. of 3-1-2- HCl-HNO3-H2O at 95 C. for one hour. This solution is then diluted to 10ml with water and analysed for a 30 element package by an ICP unit. Gold detection limit by ICP is only 3 ppm, so separate analyses were done for gold by standard AA. This method uses a 10 gram sample which is ignited at 600 C, digested with hot aqua regia and extracted by MIBK. This is then analyzed using a graphite furnace AA unit. Mercury analyses were done using the solutions extracted during the ICP digestion. The aliquouts of the extract are added to a stannous chloride - hydrochloric acid solution. The reduced mercury is swept out of solution and passed into the mercury cell of a cold vapor AA using a F & J scientific mercury assembly.

DISCUSSION OF RESULTS

Soil geochemistry is apparently severely hindered by the generally thick (1-5+ meters) overburden comprised of glacial gravel and dense compact till. Apart from scattered single station anomalies in gold and silver, most values vary only slightly from background levels. Gold or silver anomalies are only considered valid if they have coincident trace element backup. On this basis, the only gold-silver anomalies of significance were on the 4417 Grid. Subsequent trenching of these anomalies indicated that glacially transported float boulders from the Silver Zone were incorporated into the upper till layer causing the anomalies.

It appears that the glacial till is affecting geochemical response in the areas surveyed and soil sampling is probably not an effective tool for locating buried mineralized zones. As the results of the 4417 sampling indicate however, the soil response from transported mineralized float could aid in tracing the float back to its source.

VLF-EM SURVEYS

VLF-EM surveys were carried out over all the detailed grids ("A" to "G") using a Geonics EM-16 unit. The operation of this unit is well documented in the literature and will not be reiterated in this report. As survey lines were run north-south, the transmitter station at Cutler, Maine (NAA-17.8 kHZ) was used. In all cases, the operator was facing south when readings were taken.

Results were terrain corrected using a calculator program based on a paper by D. Eberle (1981) which is included in this report as Appendix III. For input the program requires the slope in percent, the azimuth of the baseline (090) and the azimuth of the local terrain or ridge trends (070). The formula used to derive the correction value is:

$$\text{Terrain correction} = 1/2 \arctan \left(\frac{\sqrt{2}}{\tan S} - \cot S \right)$$

Where S = measured terrain slope along survey line.

In areas of moderate slope, the terrain correction makes little difference but in steeper areas it can dramatically change the results.

The results were smoothed using the standard Fraser filtering technique. All the positive values were then plotted and contoured as shown on Plate No. 12 to 18. Readings were taken every 25 meters on lines 100 meters apart at the same stations as the geochem samples. The raw data included at the end of this report as Appendix II.

INTERPRETATION OF RESULTS

As expected the detailed VLF-EM surveys confirmed the presence of significant anomalies detected in the 1987 reconnaissance survey.

Anomalous trends are fairly consistent from grid to grid in two main directions. The most prominent is at 050 - 070 while the second is less distinct at 090 - 110 . These coincide with the two known ice directions suggesting that subsurface topography may be playing a significant part. At least some of the anomalies are due to significant faults which have been located in ground follow-up. The major anomaly (92) on line 3W on "A" grid, for instance, coincides with a major fault contact between Endako basalts and Ootsa Lake rhyolites. Many of these faults would be traceable on airphotos except that the strong glacial grooving in the 060 - 070 direction masks them. From our work on the Silver Zone and elsewhere we know that north-south faults are also present but our north-south survey lines do not detect them. There is some suggestion on the VLF-EM maps that these faults are shifting anomalies but to properly interpret them would require resurveying the area in an east-west direction.

Attempts at verifying the nature of some of the EM anomalies were unsuccessful due to the depth of overburden. Drilling will be required to determine their true significance.

A total of 27.5 kilometers of VLF-EM was completed. A breakdown of the kilometers surveyed for each grid is shown in Table 3 below. The number of anomalies greater than +40 units (Fraser - filtered) is also listed. Note that a series of anomalies on one line associated with a single conductor are counted as only one anomaly.

TABLE 3 - VLF-EM Statistics

GRID NAME	Km. SURVEY	NO. OF ANOMALIES	GROUP NO.
"A"	6.0	10	I
"B"	2.4	4	I
"C"	2.4	0	I
"D"	5.4	1	II, III
"E"	4.5	2	III
"F"	4.7	2	II
"G"	2.1	2	II
TOTAL	27.5		

The total on Group I claims was 10.8 kilometers, on Group II claims 9.5 kilometers and on Group III claims 7.2 kilometers.

TRENCHING

Trenching was done using a track mounted JCB 805B backhoe with a one cubic yard bucket from R.F. Klein & Sons Ltd. in Prince George. The machine with operator rented for $78.00/hour. Total hours of trenching in 1988 came to 67 hours with a total mob-demob charge of $918.00.

"A" GRID

A total of four trenches were done on this grid in 18 hours. The location of these trenches is shown on the soil geochem map (Plate No. 2). Only trench AT-2 reached bedrock which was fresh Ootsa Lake porphyritic dacite. The dimensions of the trenches were as follows:

AT-1	20m. long	x	1.5m	wide	x	4.6m. deep
AT-2	25m. long	x	1.5m	wide	x	4.0m. deep
AT-3	20m. long	x	1.5m	wide	x	4.6m. deep
AT-2	5m. long	x	1.5m	wide	x	4.6m. deep

No sampling was done on any of the trenches.

QUARRY ZONE

A single trench (QT-1) 44 meters long was done on this zone in 4 hours. The location of the trench is shown on the reconnaissance soil geochem map (Plate No. 11). The entire trench exposed bedrock which was highly kaolinized Ootsa Lake rhyolite which was brecciated and healed by light to medium gray amorphous silica. The Quarry zone area was first chip sampled in which the broken suboutcrop rock chips were collected continuously over 5 meter intervals. Then the area was trenched and channel sampled every

2 meters along the length of the trench. These results are shown on Plate No. 19. Gold and silver values were locally above background but not significant for rock samples. Molybdenum values were weakly anomalous suggesting a possible link to a deeper porphyry system. The weak precious metal values could be significant if the Quarry Zone breccia is part of the sinter cap of a deeper epithermal system.

SILVER ZONE

A total of six trenches were done on the Silver Zone in 25 hours. The location of the trenches is shown on Plate No. 21. Trenches MBHT-6, 7 and 8 exposed bedrock while overburden was deeper than the limits of the backhoe in MBHT-9, 10 and 11. The dimensions of the trenches were as follows:

MBHT-6	24m. long	x	1.5m. wide	x	1m. deep
MBHT-7	25m. long	x	1.5m. wide	x	3.7m. deep
MBHT-8	117m. long	x	1.5m. wide	x	0.2-2.0m. deep
MBHT-9	20m. long	x	1.5m. wide	x	4.6m. deep
MBHT-10	5m. long	x	1.5m. wide	x	4.6m. deep
MBHT-11	5m. long	x	1.5m. wide	x	4.0m. deep

Trenches MBHT-6, 7 and 8 were channel sampled as shown on Plate No. 21. MBHT-6 averaged 4.71 oz/t silver and 0.017 oz/t gold over 7.0 meters. This includes 3.2 meters running 6.55 oz/t silver and 0.026 oz/t gold. This mineralization appeared to be associated with a northerly trending fault zone however MBHT-7 and 8 returned only weakly anomalous values.

4417 GRID

A total of four trenches were done in 20 hours on the 4417 Grid. This area returned anomalous values in silver and gold in soils in earlier work. Prospecting of the area located numerous float boulders some of which appeared to be suboutcrop. Trenching of this area failed to reach bedrock in any of the trenches and showed the float to be glacially transported material probably from the Silver Zone. The location of these trenches is shown on Plate No. 10. The trenches had the following dimensions:

4417 T-1	20m. long	x	1.5m. wide	x	4.6m. deep
4417 T-2A	25m. long	x	1.5m. wide	x	4.6m. deep
4417 T-2B	5m. long	x	1.5m. wide	x	4.6m. deep
4417 T-3	5m. long	x	1.5m. wide	x	4.0m. deep

REVERSE CIRCULATION DRILLING

In November of 1987, a total of 16 reverse-circulation drill holes were done on the Rhub-Barb claims for a total of 1159.5 meters. 8 of the holes were done on the Barb Zone (610.2 meters), 6 on the Silver Zone (579.1 meters) and 2 on the 4417 Grid (25.60 meters). The logs with assays are included as a separate booklet included with this report.

All drilling was done by Specialized Drilling Services (S.D.S.) with a Schramm track mounted CSR Drill and a separate track mounted service truck. Pipe diameter was 3 1/2 inches.

BARB ZONE

A total of 8 holes were drilled on the Barb Zone (see Plate No.22) for a total of 610.2 meters. Seven of these were drilled on the main Barb vein system running 140 and one hole (BRH-7) was drilled on the possible strike extension of a secondary set of veins running 045 . Only holes BRH-1, 2 and 8 intersected significant mineralization (>.025 oz/t gold). Other holes had appreciable silica breccia but only minor precious metal values with the exception of BRH-4 and 7 which carried only background values.

The best intersection was in BRH-1 which ran 2150 ppb (0.063 oz/t) gold over 5 feet (1.52 m).

SILVER ZONE

A total of 6 holes were drilled on the Silver Zone for a total of 579.1 meters (see Plate No. 20, 21). Holes SRH-1, 2 and 3 were drilled below the mineralized zone while SRH-4, 5 and 6 intersected zone material. SRH-5 and 6 tested an east-west trending vein system. Both holes intersected several sections of low grade silver (less than 1 oz/t) and significant silica breccia and pyrite but no economic grades of mineralization. Hole SRH-4 tested for north-south trending mineralization and interesected two separate zones of silver and gold mineralization. The upper zone ran 1.09 oz/t silver and 0.010 oz/t gold over 3.05 meters while the lower zone ran 1.05 oz/t silver and 0.068 oz/t gold over 4.57 meters. It is believed that the lower zone is north-south trending and ties in with the mineralization intersected in trench MBHT-6. It is possible, however, the hole intersected the same east-west trending zone hit in holes SRH-5 and 6. If this is the case, it would be drilled partially down dip and along strike.

4417 GRID

A total of 2 holes were done on the 4417 Grid for a total of 25.60 meter. Due to a broken Odex casing hammer and severe winter conditions both holes were stopped in overburden. The location of the holes is shown on Plate No. 10.

For a description of the geology and assays for all the drill holes refer to the logs included as a separate booklet with this report. A summary of the drill holes is shown in Table 4 below:

TABLE 4 - Summary of R.C. Drilling

HOLE NO.	ANGLE	DIRECTION	DEPTH	SIGNIFICANT INTERSECTIONS
BRH-1	-60	220	36.58	19.81-21.34m of 0.18 oz/t Ag, 0.063 oz/t Au
BRH-2	-50	220	85.34	70.10-71.62m of 0.08 oz/t Ag, 0.026 oz/t Au
BRH-3	-50	225	85.34	--
BRH-4	-60	225	70.10	--
BRH-5	-50	225	95.10	--
BRH-6	-50	225	67.06	--
BRH-7	-50	135	91.44	--
BRH-8	-60	225	79.25	32.00-33.53m of 0.08 oz/t Ag, 0.022 oz/t Au
SRH-1	-50	300	91.44	--
SRH-2	-50	340	91.44	--
SRH-3	-50	340	143.26	--
SRH-4	-50	070	70.10	6.10- 7.62m of 1.23 oz/t Ag, 0.009 oz/t Au
				7.62- 9.14m of 0.94 oz/t Ag, 0.011 oz/t Au
				36.58-38.10m of 0.74 oz/t Ag, 0.123 oz/t Au
				38.10-39.62m of 1.36 oz/t Ag, 0.061 oz/t Au
				39.62-41.15m of 1.04 oz/t Ag, 0.019 oz/t Au
SRH-5	-50	160	91.44	--
SRH-6	-50	160	91.44	25.91-27.43m of 0.87 oz/t Ag, 0.008 oz/t Au
4417 RH-1	-50	160	18.90	--
4417 RH-2	-60	340	6.71	--

Reject chip samples are stored on each drill site.

DIAMOND DRILLING

In July of 1988, a total of 6 NQ diamond drill holes were done on the Silver Zone (Rhub 8) for a total of 1036.9 meters. The location of these holes is shown on Plate No. 21. Holes SDH-7, 9, 10, 11 and 12 were located to test a north-south trending fault zone which ran 4.71 oz/t silver and 0.17 oz/t gold over 7 meters in trench MBHT-6. Only SDH-9 and 11 intersected significant mineralization. SDH-9 ran 0.81 oz/t silver and 0.209 oz/t gold over 1.52 meters with an adjacent sample running 0.17 oz/t silver and 0.039 oz/t gold over 1.22 meters. SDH-11 ran 1.33 oz/t silver and 0.012 oz/t gold over 1.52 meters.

Hole SDH-8 was drilled to intersect an east-west trending vein system hit in holes SRH-5 and 6 in 1987. Five separate mineralized sections were intersected as shown in Table 5 below. Grades vary from 1.23 oz/t silver and 0.002 oz/t gold to 5.92

oz/t silver and 0.001 oz/t gold over 1.52 meters.

Due to complex geology and structure in the Silver Zone area, correlation of rock types and mineralization from hole to hole is extremely difficult. Varying intensities and types of alteration can result in considerably different colours and textures within the same rock unit. As well, the presence of faulting and associated lahars and/or tectomic breccias result in dramatic thickness and rock type changes over short intervals in the core. The mineralization is associated with pyrite-marcasite and possibly native gold and silver within argillically altered (kaolinized) and silicified Ootsa Lake rhyolite flows and tuffs. Zones either consist of brecciated rhyolite healed by gray to black amorphous silica or as a series of stockwork veins and veinlets of amorphous silica with varying amounts of pyrite and marcasite. All mineralization is microscopic in nature and appears to show little correlation with the amount of sulphides or silica present. Although mineralization shows a preference for the rhyolite flows and tuffs, it is actually crosscutting the lithologies. Main controls for the mineralization appear to be fracture intensity and porosity of the hostrock. The precious metals are obviously associated with a low-temperature (epithermal) system similar to the volcanic hosted gold-silver deposits found in the southern U.S. and elsewhere in B.C. The hostrocks are Tertiary in age and appear to be part of a collapsed couldera type environment.

TABLE 5 - Summary of R.C. Drilling

HOLE NO.	ANGLE	DIRECTION	DEPTH	SIGNIFICANT INTERSECTIONS
SDH-7	-62	072	114.60	40.53-41.88m of 1.17oz/t Ag, 0.013oz/t Au
SDH-8	-65	160	123.75	59.74-61.26m of 1.45oz/t Ag, 0.001oz/t Au
				73.45-74.98m of 1.23oz/t Ag, 0.002oz/t Au
				79.55-81.07m of 5.92oz/t Ag, 0.001oz/t Au
				85.65-87.17m of 3.10oz/t Ag, 0.002oz/t Au
				96.31-97.84m of 4.61oz/t Ag, 0.001oz/t Au
SDH-9	-60	070	154.23	63.09-64.62m of 0.81oz/t Ag, 0.209oz/t Au
				64.62-65.84m of 0.17oz/t Ag, 0.039oz/t Au
SDH-10	-50	260	186.54	
SDH-11	-50	260	215.19	166.42-65.84m of 1.33oz/t Ag, 0.012oz/t Au
SDH-12	-50	260	242.62	

All core is stored on the Silver Zone near the intersection of the M-17 and M-19 roads.

CONCLUSION

Our work on the Rhub-Barb claims indicates that epithermal precions metal-bearing solutions have been active in the area. The Tertiary Ootsa Lake Volcanics are the hostrocks with mineralization associated with lineal fault zones possibly related to a collapsed cauldera environment. Most mineralization located thus far has been subeconomic in grade and of limited extent.

The soil geochemical surveys have been hampered by the thick mantle of glacial debris prevalent over most of the area. Where the glacial cover thins, such as on the Silver Zone, soils yield anomalous results in both trace elements and precious metals. Also where mineralized float has been incorporated into the upper till layer, soils can be used to outline the dispersion train.

The VLF-EM has been effective at delineating fault zones but gives no indication whether mineralization will be present. The sulphide mineralization is generally too disseminated to be detected by electromagnetic instruments. IP is being considered for the future. However as grades and sulphide content are apparently not directly correlated it remains to be seen how effective it will be at locating precious metal mineralization.

Trenching has been one of the best exploration tools thus far. In combination with prospecting it has successfully delineated the mineralized zones where overburden depths are less than 4.5 meters.

Reverse circulation drilling is useful where lithology and structure are well known but can be confusing otherwise. Hole SRH-4 is a good example. This hole intersected some of the best grades of silver and gold mineralization but it is uncertain whether it crosscuts or subparallels the vein/breccia system. Also sequences like lahars and agglomerates are difficult to recognize in chips resulting in correlation problems between drill holes.

The diamond drilling added significantly to our understanding of the subsurface geology. Even with drill core however, the plethora of faults, shears and multidirectional veins complicates geologic and structural interpretations. The diamond drilling has confirmed some of the earlier suspicions about the mineralization. The two major ones are that the grades of precious metal mineralization are not directly proportional to the amount or type of silica or to the amount of sulphides present.

In summary, there appears to be significant potential for Nevada-type epithermal occurrences in this area however it will be a difficult process in locating them in heavily glaciated terrain. It seems to that word "capricious" was coined with epithermal occurrences in mind and they are living up to their reputation.

K. J. Taylor,
Senior Project Geologist

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STATEMENT OF QUALIFICATIONS

I, Kenneth J. Taylor of 15732 - 92B Avenue, Surrey, British Columbia do hereby certify that:

1. I am a geologist with a B.Sc. in Geology from the University of British Columbia, 1973.

2. I have practised my profession continuously since 1973.

3. I have participated in or supervised the work on the Rhub 1-13 and Barb 1 claims since their inception.

4. I have had experience exploring for epithermal gold and silver deposits throughout British Columbia for the past three years.

5. I have inspected the work done on the Rhub-Barb claims and found it to conform to accepted standards within the mining industry.

K. J. Taylor
Senior Project Geologist
Mingold Resources Inc.
December 16, 1988

STATEMENT OF COSTS

Personnel

K. Taylor	-	Project Supervisor	$175/day
J. Nicholson	-	Geologist	$125/day
R. Diment	-	Geologist	$125/day
J. Lainsbury	-	Geologist	$125/day
J. Thomlinson	-	Fieldman	$100/day
W. Kowal	-	Geological Technician	$ 95/day
D. Cosgrove	-	Contract Fieldman	$100/day
K. Galambos	-	Geologist	$120/day
R. Wood	-	Sampler	$100/day
S. Conlin	-	Sampler	$100/day

Breakdown of Costs & Dates

GROUP I - 96 Units

(Barb I, Rhub 10-13)

VLF-EM (Grids A,B,C) June 1-4/88 (3.5 mandays)	
- 3.5 mandays @ $95/manday	$ 332.50
Soils (Grids A,B,C) May 19, 21-23/88 (10.5 mandays)	
- 3.5 mandays @ $100/manday	350.00
- 3 mandays @ $ 95/manday	285.00
- 4 mandays @ $125/manday	500.00
- Assays - 432 @ $11.25 each	4860.00
- Sample prep. - 432 @ 0.85 each	367.20
Control Grid May 6, 7, 12, 13/88 (7 mandays)	
- 3.5 mandays @ $100/manday	350.00
- 3.5 mandays @ $ 95/manday	332.50
Trenching (Grid A) - June 27, 29	
- 18 hrs backhoe @ $78.00/hr.	1404.00
- Mob-demob 1/3 of $918.00	306.00
- Supervision - 2 mandays @ $175/manday	350.00

<u>Reverse-circulation Drilling</u> Nov. 1, 4-11/87	
- 1990 ft. CSR drilling @ 12.00/ft. incl. fuel	$ 23880.00
- 12 ft. CSR drilling (over 300 ft depth) @ 13.50/ft	162.00
- Mob-demob- ½ of $8000	4000.00
- Logging chips - 8 mandays @ $175/manday	1400.00
- Sampling - 18 mandays @$100/manday	1800.00
- Assays - 366 @ 6.50/sample	2379.00
- Sample prep - 366 @ 3.00/sample	1098.00
- Sample shipping - ½ of $702.00	351.00
<u>Room/Board</u>	
- 49 mandays for field crew @ $25/manday	1225.00
- 2 mandays for backhoe operator @ $25/manday	50.00
- 9 days for 2 drillers @ $25/manday	450.00
<u>Transportation</u>	
- Truck rental - 23 days @ $50/day incl. fuel	1150.00
<u>Supplies</u>	
- Flagging, thread, soil bags	150.00
- Plastic sample bags for CSR drilling	100.00
	$ 47632.20

STATEMENT OF COSTS

GROUP II - 100 Units

(Rhub 1, 3, 7, 8, 9)

<u>VLF-EM</u> (Grids F. G, D) June 11-13/88 (3 mandays)	
- 2.5 mandays @ $ 95/manday	237.50
- 0.5 manday @ $100/manday	50.00
<u>Soils</u> (Grids F, G, D) May 28, 29, 30/88 (7 mandays)	
- 3 mandays @ $100/manday	300.00
- 3 mandays @ $ 95/manday	285.00
- 1 manday @ $125/manday	125.00
- Assays - 351 samples @ $11.25/sample	3948.75
- Prep. 351 @ 0.85	298.35
<u>Reconn. Soils</u> June 17, 18 (2 mandays)	
- 2 mandays @ $95/manday	190.00
- Assays - 93 samples @ 11.25/sample	1046.25
- - Sample prep 93 @ 0.85	79.05
<u>4417 Grid Soils</u> June 20, 21/88 (2 mandays)	
- 2 mandays @ $95/manday	190.00
- Assays - 48 samples @ $11.25/sample	540.00
- Sample prep. 48 @ 0.85	40.80
<u>Control Grid</u> May 17-20 (8 mandays)	
- 4 mandays @ $100/manday	400.00
- 4 mandays @ $ 95/manday	380.00
<u>Trenching</u> (4417, Silver) May 21-26/88	
- 45 hrs. backhoe @ $78/hr.	3510.00
- Mob-demob - 1/3 of $918	306.00
- 6 days supervision @ $175/manday	1050.00
<u>Rock Sampling</u> June 5 - 10 (12 mandays)	
- 4 mandays cleaning debris @ $125/manday	500.00
- 3 mandays cleaning debris @ $ 95/manday	285.00
- 2 mandays sampling @ $125/day	250.00
- 3 mandays sampling @ $ 95/manday	285.00
- Assays - 79 samples @ $11.25/sample	888.75
- - 79 samples @ $ 3.00 ea.	237.00
<u>Diamond Drilling</u> (Silver) July 5-15, Aug. 9/88	
- 3402 ft. of drilling (NQ) @ $16/ft.	54432.00
- Mob-demob	1000.00
- Splitting core - 13 mandays @ $ 95/manday	1235.00
- - 15 mandays @ $125/manday	1875.00
- Logging core - 27.5 mandays @ $175/manday	4812.50
- Assays - 599 samples @ $13.00/sample	7774.00
- Sample prep. 599 @ 3.00	1797.00
- Sample shipping	427.00

Reverse-circulation Drilling Nov. 12 - 22/87 (Silver, 4417)	
- 1814 ft. of CSR drilling @ $12.00/ft. incl. fuel	$ 21768.00
- 170 ft. of CSR drilling (over 300 ft. depth) @ $13.50/ft.	2295.00
- Mob-demob - ½ of $8000	4000.00
- Logging chips - 11 mandays @ $175/manday	1925.00
- Sampling - 22 mandays @ $100/manday	2200.00
- Assays - 347 samples @ $6.50/sample	2255.50
- Sample prep. 347 @ 3.00	1041.00
- Sample shipping - ½ of $702.00	351.00
Room/Board	
- 134.5 mandays for crew @ $25/manday	3362.50
- 12 days for 4 diamond drillers @ $25/manday	1200.00
- 13 days for 2 CSR drillers @ $25.manday	650.00
Transportation	
- Truck rental - 48 days @ $50/day incl. fuel	2400.00
Supplies	
- Flagging,thread, soil bags	150.00
- Plastic sample bags for CSR & Diamond Drilling	230.00
	$132602.95

Apply:	2 yrs on Rhub 1, 3 @ 100/yr (1990)	$ 8,000
	3 yrs on Rhub 3 @ 200/yr (1993)	12,000
	4 yrs on Rhub 1 @ 200/yr (1994)	16,000
	8 yrs on Rhub 7, 8, 9 @ 200/yr (1998)	96,000
		$ 132,000

STATEMENT OF COSTS

GROUP III - 72 Units

(Rhub 2, 4, 5, 6,)

VLF-EM (Grid O, E) June 4, 9, 10 (2.5 mandays)	
- 2.5 mandays @ $100/manday	$ 250.00
Soils (Grid E, E + Quarry Zone) May 2, 24, 26, 27 (9.5 mandays)	
- 4 mandays @ $125/manday	500.00
- 2.5 mandays @ $100/manday	250.00
- 3 mandays @ $95/manday	285.00
- Assays - 294 samples @ 11.25/sample	3307.50
- Sample prep. 294 @ 0.85	249.90
Reconn. Soils (All except L51E, 54E) June 17, 18, 19 (5 mandays)	
- 1 manday @ $125/manday	125.00
- 3 mandays @ $100/day	300.00
- 1 manday @ $95/day	95.00
- Assays - 282 samples @ $11.25/sample	3172.50
- Sample prep. 282 @ 0.85 ea.	239.70
Trenching (Quarry Zone) May 21	
- 4 hrs backhoe @ $78/hr	312.00
- Mob-demob - 1/3 of $918	306.00
- Supervision - 0.5 mandays @ $175/manday	87.50
Rock Sampling (Quarry Zone) May 21, June 2 & 3/88 (5 mandays)	
- 1 manday @ $175/manday	175.00
- 2 mandays cleaning debris @ $125/day	250.00
- 2 mandays sampling @ $95/manday	190.00
- Assays - 22 samples @ $11.25 ea.	247.50
- Sample prep - 22 @ 3.00	66.00
- Assays - 13 samples @ $11.25 ea.	146.25
- Sample prep - 13 @ 3.00	39.00
Control Grid - May 13, 14, 15, 16 (7 mandays)	
- 3.5 mandays @ $100/day	350.00
- 3.5 mandays @ $ 95/day	332.50
Room/Board	
- 30 mandays @ $25/manday	750.00
- 1 manday for backhoe operator @ $25/manday	25.00
Transportation	
- 18 days truck rental @ $50/day incl. fuel	900.00
Supplies - Flagging, thread, bags	200.00
	$ 13151.35

I ASSAY CERTIFICATES

-SOIL GEOCHEMISTRY-

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUN 03 1988 DATE REPORT MAILED: June 10/88 ASSAYER. C. Leong D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT-620 File # 88-1752 Page 1

A' Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L4W 24+00N	1	17	13	121	.1	15	10	672	3.82	8	5	ND	3	19	1	2	2	61	.18	.136	18	28	.47	156	.10	2	4.04	.01	.08	1	5	50
L4W 23+75N	1	6	10	34	.2	9	5	170	2.07	4	5	ND	3	24	1	2	2	40	.21	.033	13	15	.17	94	.08	2	1.06	.01	.05	1	3	30
L4W 23+50N	1	6	5	58	.2	11	4	509	2.26	3	5	ND	3	19	1	2	4	43	.19	.023	13	17	.22	104	.08	2	1.86	.01	.03	1	1	20
L4W 23+25N	1	5	7	69	.1	9	5	614	2.02	2	5	ND	2	21	1	3	3	37	.21	.037	13	16	.24	125	.08	6	1.52	.01	.05	1	3	10
L4W 23+00N	1	5	6	79	.1	8	4	268	1.72	2	5	ND	2	21	1	2	3	29	.21	.072	12	13	.16	121	.07	4	1.20	.01	.06	1	1	5
L4W 22+75N	1	9	4	64	.3	13	5	209	2.37	4	5	ND	3	20	1	3	2	37	.20	.142	14	16	.21	137	.06	2	1.60	.01	.06	1	1	5
L4W 22+50N	1	8	7	39	.1	8	3	213	1.96	3	5	ND	2	26	1	2	2	36	.28	.041	16	15	.26	77	.09	3	.92	.02	.04	1	1	5
L4W 22+25N	1	7	5	115	.1	8	6	305	1.84	2	5	ND	2	20	1	2	2	29	.17	.057	12	14	.19	105	.06	2	1.60	.01	.05	1	1	80
L4W 22+00N	1	7	9	69	.1	9	5	422	2.14	2	5	ND	1	22	1	2	2	34	.17	.109	11	16	.38	122	.05	4	1.48	.01	.02	1	1	20
L4W 21+75N	1	8	5	56	.1	9	4	200	1.84	2	5	ND	2	24	1	2	4	34	.19	.021	14	14	.22	88	.09	3	1.13	.01	.03	1	2	5
L4W 22+50N	1	9	10	72	.1	14	6	357	2.25	4	5	ND	2	22	1	2	2	39	.19	.037	13	22	.26	106	.10	2	1.83	.01	.04	1	5	10
L4W 21+25N	1	8	10	45	.1	5	4	237	1.68	2	5	ND	1	21	1	2	2	29	.19	.022	13	14	.20	77	.08	2	1.04	.01	.04	1	1	5
L4W 21+00N	1	11	6	75	.1	16	6	208	2.18	2	5	ND	2	22	1	2	2	32	.21	.052	11	16	.28	121	.07	2	1.81	.01	.04	1	1	10
L4W 20+75N	1	5	5	78	.2	9	4	288	1.64	2	5	ND	2	17	1	2	2	28	.16	.026	12	13	.18	97	.06	2	1.40	.01	.04	1	1	5
L4W 20+50N	1	4	5	72	.2	5	3	326	1.48	2	5	ND	2	17	1	2	2	26	.19	.027	12	11	.15	89	.06	3	1.38	.01	.06	1	2	5
L4W 20+25N	1	6	10	48	.2	7	3	460	1.64	3	5	ND	2	18	1	2	2	30	.17	.022	13	12	.16	82	.06	3	1.28	.01	.08	1	2	10
L4W 20+00N	1	5	3	64	.1	4	4	384	1.53	2	5	ND	2	27	1	3	6	26	.19	.020	13	10	.19	99	.06	2	1.41	.01	.05	1	1	5
L4W 19+75N	1	8	5	47	.3	7	4	272	1.69	2	5	ND	3	22	1	2	6	31	.19	.022	14	14	.18	101	.06	2	1.13	.01	.05	1	1	5
L4W 19+50N	1	8	5	68	.1	7	5	697	1.78	2	5	ND	1	26	1	2	3	32	.25	.021	16	14	.19	150	.07	2	1.56	.01	.07	1	2	10
L4W 19+25N	1	8	5	84	.1	4	3	589	1.63	2	5	ND	2	37	1	2	3	28	.31	.038	17	12	.18	135	.07	2	1.19	.01	.06	1	1	20
L4W 19+00N	1	7	5	95	.4	8	3	363	1.68	2	5	ND	2	30	1	2	3	29	.32	.049	14	13	.17	111	.07	10	.89	.01	.12	1	1	5
L4W 18+75N	1	6	2	54	.1	7	4	175	1.86	2	5	ND	2	17	1	2	4	34	.20	.027	21	15	.18	64	.08	3	.85	.01	.09	1	1	5
L4W 18+50N	1	3	7	45	.1	4	3	240	1.34	2	5	ND	2	17	1	3	2	25	.21	.016	12	10	.14	63	.07	4	.73	.01	.07	1	68	5
L4W 18+00N	1	5	7	41	.3	6	4	261	1.26	2	5	ND	3	20	1	2	2	21	.26	.017	11	11	.16	62	.06	2	.73	.01	.09	1	1	5
L4W 17+75N	2	4	11	28	.2	7	4	284	1.50	2	5	ND	2	23	1	2	3	26	.27	.029	12	12	.23	68	.06	2	.89	.01	.08	1	2	20
L4W 17+50N	1	4	6	37	.1	6	3	189	1.47	2	5	ND	1	24	1	2	2	23	.26	.014	10	12	.18	57	.06	4	.87	.02	.05	1	1	10
L3W 24+00N	2	25	16	178	.2	35	20	2101	4.81	9	5	ND	4	29	1	2	5	75	.34	.126	30	35	1.01	147	.11	2	3.88	.01	.07	1	1	40
L3W 23+75N	1	14	12	56	.1	12	4	233	2.24	2	5	ND	3	21	1	2	2	42	.24	.042	14	20	.35	77	.12	2	1.70	.01	.03	1	1	10
L3W 23+50N	1	5	6	74	.2	9	4	187	1.58	2	6	ND	2	20	1	4	2	29	.18	.032	11	14	.17	82	.09	2	1.07	.01	.05	1	2	5
L3W 23+25N	1	5	13	46	.1	5	2	206	1.51	2	5	ND	4	19	1	2	2	24	.25	.018	17	12	.22	60	.09	5	1.09	.01	.08	1	1	10
L3W 23+00N	1	6	2	43	.1	6	2	188	1.25	2	5	ND	3	17	1	2	2	22	.22	.011	12	11	.17	54	.09	2	.89	.01	.07	1	1	5
L3W 22+75N	1	8	4	40	.1	8	4	157	1.58	2	5	ND	2	19	1	2	2	30	.18	.016	12	13	.18	75	.09	2	.87	.01	.04	1	1	5
L3W 22+50N	1	9	8	45	.1	9	3	239	2.41	4	5	ND	3	19	1	2	4	43	.16	.029	13	18	.24	108	.07	2	1.70	.01	.05	1	2	20
L3W 22+25N	1	10	8	42	.2	11	5	211	2.25	5	5	ND	3	23	1	2	3	41	.19	.048	13	16	.21	133	.08	2	1.41	.01	.06	1	1	30
L3W 22+00N	1	11	10	86	.1	15	6	795	2.49	3	5	ND	2	23	1	3	2	43	.22	.056	13	21	.27	138	.09	2	2.02	.01	.06	1	1	20
L3W 21+75N	1	7	6	43	.1	7	3	171	1.74	2	5	ND	2	20	1	2	6	32	.19	.022	11	14	.22	70	.10	2	1.01	.01	.05	1	1	50
STD C/AU-S	18	62	38	132	6.7	67	30	1071	4.11	40	20	8	38	48	18	17	20	59	.48	.083	41	60	.95	183	.07	34	1.96	.07	.13	12	50	1400

"A" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L3W 21+50N	1	13	8	52	.1	14	7	243	2.81	2	5	ND	1	24	1	2	2	54	.22	.043	10	27	.38	90	.17	2	1.40	.01	.03	1	1	20
L3W 21+25N	1	14	5	65	.3	24	8	277	3.09	3	5	ND	2	28	1	2	2	54	.26	.067	10	29	.41	110	.14	8	2.07	.01	.03	1	2	10
L3W 21+00N	2	8	11	97	.1	7	4	424	2.53	3	5	ND	4	93	1	2	2	34	.26	.060	19	12	.28	187	.07	2	2.11	.01	.09	1	1	60
L3W 20+75N	1	9	8	51	.1	7	4	223	1.99	2	5	ND	2	20	1	2	2	33	.16	.042	14	15	.21	111	.06	2	1.59	.01	.02	1	1	10
L3W 20+50N	1	9	8	55	.3	9	4	223	1.66	2	5	ND	2	23	1	2	2	28	.21	.033	13	12	.21	97	.07	4	1.13	.01	.06	1	1	10
L3W 20+25N	1	6	9	37	.2	8	4	175	1.09	2	5	ND	2	19	1	4	2	33	.20	.041	11	14	.21	91	.07	3	1.09	.01	.06	1	1	5
L3W 20+00N	1	9	4	36	.3	8	3	146	1.63	2	5	ND	2	21	1	2	2	30	.18	.021	12	12	.18	70	.08	10	.87	.01	.05	2	1	60
L3W 19+75N	1	6	5	45	.2	5	3	309	1.51	2	5	ND	3	32	1	5	2	25	.20	.019	13	10	.18	98	.07	4	1.07	.01	.07	2	2	5
L3W 19+50N	1	7	3	91	.1	7	3	1212	1.38	2	5	ND	1	42	1	2	2	19	.36	.062	15	9	.17	206	.05	4	1.09	.01	.12	1	1	10
L3W 19+25N	1	9	2	33	.2	9	4	272	1.72	2	5	ND	3	20	1	2	2	32	.20	.023	14	14	.15	78	.08	2	.66	.01	.08	1	1	5
L3W 19+00N	1	6	2	62	.1	7	3	284	1.50	2	5	ND	1	18	1	2	2	25	.23	.045	12	12	.13	96	.07	5	.78	.01	.08	1	1	5
L3W 18+75N	1	10	3	40	.4	6	3	206	1.79	4	5	ND	3	23	1	2	5	31	.28	.041	15	14	.19	68	.08	4	.77	.01	.08	1	2	20
L3W 18+50N	1	6	5	47	.1	6	3	281	1.56	2	5	ND	1	22	1	2	2	27	.23	.025	15	11	.16	79	.07	10	.77	.01	.07	1	1	10
L3W 18+25N	1	15	8	43	.1	10	4	340	2.34	8	5	ND	2	36	1	2	2	39	.34	.046	19	17	.29	94	.08	4	1.01	.02	.07	1	1	30
L3W 18+00N	1	6	5	46	.2	6	3	183	1.44	2	5	ND	1	22	1	4	2	24	.20	.023	11	11	.17	70	.06	3	.87	.01	.07	1	1	10
L3W 17+75N	1	6	6	28	.1	7	2	151	1.34	2	5	ND	2	22	1	2	5	23	.22	.028	13	11	.18	60	.08	7	.68	.01	.07	1	1	5
L3W 17+50N	1	7	7	40	.1	9	4	154	1.83	2	5	ND	1	17	1	2	2	31	.15	.046	11	14	.15	93	.06	3	1.18	.01	.05	1	2	5
L2W 24+00N	1	6	8	51	.2	5	3	272	1.39	2	5	ND	3	21	1	2	2	24	.18	.033	10	12	.16	74	.08	3	.89	.01	.05	1	32	5
L2W 23+75N	1	8	12	67	.2	10	5	199	2.55	3	5	ND	5	13	1	2	2	39	.12	.072	16	19	.25	90	.07	3	2.52	.01	.06	1	2	20
L2W 23+50N	1	4	5	62	.1	6	4	284	1.64	2	5	ND	1	19	1	2	2	28	.17	.036	12	12	.16	94	.07	2	1.32	.01	.05	1	1	5
L2W 23+25N	2	8	16	125	.2	13	7	374	2.51	3	5	ND	2	27	1	2	2	39	.26	.112	10	20	.28	121	.11	2	1.86	.01	.08	1	1	10
L2W 23+00N	1	7	12	50	.3	10	3	328	1.64	2	5	ND	2	24	1	2	2	27	.23	.031	15	13	.24	77	.08	4	1.03	.01	.04	1	1	5
L2W 22+75N	1	5	15	64	.2	7	5	214	1.75	2	5	ND	3	22	1	3	2	34	.23	.027	11	17	.25	63	.14	5	.89	.01	.06	1	1	5
L2W 22+50N	1	8	19	65	.1	9	6	260	2.31	2	5	ND	1	25	1	2	2	43	.26	.025	10	23	.36	66	.19	4	1.14	.01	.03	1	3	5
L2W 22+25N	1	7	8	50	.3	9	4	190	1.88	2	5	ND	3	23	1	2	2	34	.22	.023	10	16	.27	58	.12	2	.97	.01	.05	1	1	10
L2W 22+00N	1	9	10	75	.2	12	6	446	2.24	2	5	ND	2	27	1	3	2	39	.27	.026	12	20	.31	74	.11	3	1.18	.01	.06	1	1	10
L2W 21+75N	1	8	9	57	.1	10	5	240	1.85	2	5	ND	2	25	1	3	2	33	.24	.028	11	16	.20	63	.09	5	.89	.01	.11	1	38	5
L2W 21+50N	1	8	12	64	.1	7	3	235	1.70	2	5	ND	1	23	1	2	2	28	.22	.023	15	15	.25	62	.09	2	.90	.01	.09	1	1	10
L2W 21+25N	1	9	14	42	.1	8	3	273	1.51	3	5	ND	3	26	1	4	2	26	.26	.040	20	14	.23	72	.09	7	.86	.01	.07	2	1	20
L2W 21+00N	1	4	11	63	.2	7	3	204	1.68	2	5	ND	2	21	1	2	2	28	.21	.032	12	12	.19	56	.07	2	.80	.01	.07	1	1	5
L2W 20+75N	1	9	5	37	.2	5	6	214	2.04	5	5	ND	3	30	1	4	2	37	.25	.047	13	15	.19	81	.08	3	.73	.01	.10	1	1	10
L2W 20+50N	1	5	9	81	.1	8	4	647	1.81	3	5	ND	1	36	1	2	4	29	.33	.120	11	13	.15	108	.05	2	1.02	.01	.09	1	1	5
L2W 20+25N	1	9	9	40	.2	9	4	181	2.09	5	5	ND	2	29	1	6	2	37	.30	.051	12	15	.20	59	.08	3	.81	.01	.12	2	1	10
L2W 20+00N	1	6	12	55	.1	9	2	304	1.51	2	5	ND	2	18	1	2	2	26	.19	.058	10	11	.12	94	.06	3	.90	.01	.08	1	1	5
L2W 19+75N	1	6	9	30	.3	5	3	166	1.61	3	5	ND	3	20	1	3	2	30	.19	.021	10	12	.13	71	.08	2	.65	.01	.12	1	2	5
L2W 19+50N	1	7	8	58	.2	9	3	419	1.69	2	5	ND	2	22	1	2	2	28	.21	.068	10	12	.14	120	.06	5	.91	.01	.08	1	1	5
STD C/AU-S	21	61	42	132	8.0	73	31	1074	4.13	44	17	8	40	53	19	16	21	59	.48	.096	40	59	.96	183	.08	37	1.99	.07	.16	15	48	1300

	SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
	L2W 19+25N	1	8	9	45	.1	8	4	240	1.76	2	5	ND	1	22	1	2	5	31	.23	.033	13	13	.16	88	.07	2	.77	.01	.11	1	11	5
	L2W 19+00N	1	7	8	42	.2	7	4	405	1.75	2	5	ND	3	21	1	2	2	31	.21	.039	12	12	.15	85	.07	2	.75	.01	.09	2	4	5
"A" Grid	L2W 18+75N	1	8	8	60	.2	6	4	183	1.80	2	5	ND	2	21	1	2	4	28	.22	.045	15	12	.18	85	.06	2	.95	.01	.10	1	6	5
	L2W 18+50N	1	8	5	46	.1	7	4	179	1.31	2	5	ND	1	23	1	2	2	22	.23	.014	21	9	.15	72	.06	2	.77	.01	.08	1	9	5
	L2W 18+25N	1	7	3	47	.1	8	4	135	1.40	2	5	ND	1	18	1	2	2	25	.18	.015	12	10	.16	71	.07	2	.84	.01	.05	1	5	5
	L2W 18+00N	1	6	8	79	.2	10	5	251	1.77	2	5	ND	3	21	1	2	2	29	.20	.053	15	11	.19	113	.07	2	1.31	.01	.18	1	15	5
	L2W 17+75N	1	8	8	57	.1	8	4	632	1.34	3	5	ND	2	24	1	2	2	25	.26	.041	15	11	.15	87	.06	6	.88	.01	.07	1	2	30
	L2W 17+50N	1	4	7	80	.1	6	3	637	1.09	2	5	ND	1	33	1	2	3	21	.27	.051	11	9	.10	104	.06	2	.69	.01	.10	1	1	10
	L1W 30+75N	1	10	9	107	.3	9	6	270	2.42	2	5	ND	3	43	1	4	2	38	.36	.152	15	16	.26	172	.07	2	1.35	.01	.08	1	2	5
	L1W 30+50N	1	15	12	147	.3	10	9	311	2.56	2	5	ND	2	43	1	2	3	37	.29	.251	14	16	.25	194	.06	2	1.52	.01	.10	1	5	20
	L1W 30+25N	1	17	12	37	.1	9	6	905	2.91	3	5	ND	2	45	1	2	2	47	.41	.056	20	17	.32	128	.06	3	1.59	.01	.09	1	3	10
	L1W 30+00N	1	10	6	40	.3	9	5	237	2.28	3	5	ND	3	28	1	3	2	41	.23	.045	13	16	.21	98	.08	8	1.05	.01	.11	1	6	5
	L1W 29+75N	1	12	7	47	.2	8	5	190	2.22	2	5	ND	4	26	1	2	2	34	.23	.081	13	14	.21	100	.07	2	1.44	.01	.07	1	5	5
	L1W 29+50N	1	13	18	100	.2	15	6	203	3.40	7	5	ND	3	45	1	2	8	48	.35	.286	15	19	.25	158	.06	7	2.68	.01	.07	1	7	20
"B" Grid	L1W 29+25N	1	9	9	43	.2	11	4	156	2.08	3	5	ND	2	26	1	2	2	37	.23	.066	12	14	.18	93	.08	3	1.43	.01	.06	2	4	10
	L1W 29+00N	1	16	14	62	.1	12	8	1264	2.46	2	5	ND	1	43	1	2	2	37	.35	.043	31	16	.31	149	.05	3	1.73	.01	.08	1	2	20
	L1W 28+75N	1	10	11	35	.1	3	4	174	1.34	2	5	ND	3	24	1	2	2	28	.19	.019	13	11	.20	79	.08	2	.78	.01	.04	1	3	5
	L1W 28+50N	1	9	10	36	.1	6	3	182	1.54	2	5	ND	2	25	1	2	3	25	.20	.024	13	12	.22	86	.07	3	.98	.01	.05	1	3	5
	L1W 28+25N	1	9	11	41	.2	7	4	244	2.03	5	5	ND	2	24	1	2	2	33	.19	.032	14	13	.23	83	.06	2	1.41	.01	.06	1	7	5
	L1W 28+00N	1	9	9	53	.3	6	5	449	1.71	2	6	ND	2	24	1	2	2	30	.21	.035	13	11	.18	71	.07	6	.98	.01	.05	1	1	5
	L1W 27+75N	1	8	10	51	.1	7	5	515	1.76	2	5	ND	2	25	1	2	3	30	.20	.040	15	13	.20	99	.07	8	1.21	.01	.03	1	4	10
	L1W 27+50N	1	11	9	45	.1	8	4	202	1.96	3	5	ND	3	26	1	2	3	33	.19	.023	15	13	.27	113	.08	2	1.40	.01	.06	1	1	5
	L1W 27+25N	2	12	11	66	.1	8	3	242	2.49	2	5	ND	3	14	1	2	2	48	.12	.056	15	16	.19	77	.07	2	1.63	.01	.05	1	1	30
	L1W 27+00N	1	10	8	57	.1	8	5	582	2.19	3	5	ND	3	16	1	2	3	39	.13	.042	17	15	.18	108	.07	2	1.79	.01	.04	1	1	20
	L1W 26+75N	1	12	5	51	.1	5	4	250	1.73	2	5	ND	2	23	1	2	4	28	.18	.035	13	11	.20	100	.07	4	1.29	.01	.05	1	6	10
	L1W 24+00N	1	11	14	31	.6	5	3	137	1.68	2	5	ND	4	28	1	2	2	27	.36	.048	21	15	.22	67	.06	3	1.18	.02	.08	1	1	110
	L1W 23+75N	1	7	7	44	.1	7	4	286	1.73	2	5	ND	1	23	1	2	2	30	.18	.030	13	12	.15	91	.07	3	.91	.01	.07	1	1	10
	L1W 23+50N	1	9	6	44	.5	7	5	179	1.67	3	5	ND	3	21	1	3	2	28	.18	.027	13	13	.16	85	.05	3	.89	.01	.07	1	6	20
	L1W 23+25N	1	12	12	64	.2	10	5	217	2.01	2	5	ND	3	26	1	3	4	32	.25	.066	13	16	.20	87	.07	4	1.08	.01	.08	1	3	5
"A" Grid	L1W 23+00N	1	8	7	75	.1	10	6	385	2.14	2	5	ND	2	27	1	2	2	38	.23	.044	12	19	.21	123	.10	2	1.11	.01	.03	1	3	5
	L1W 22+75N	1	10	9	79	.1	10	6	219	2.26	2	5	ND	2	34	1	2	2	38	.33	.083	11	18	.24	89	.10	2	1.12	.01	.06	1	2	5
	L1W 22+50N	1	11	6	59	.1	10	6	201	1.86	2	5	ND	2	26	1	2	4	32	.26	.030	14	16	.23	65	.10	2	.88	.01	.08	1	1	5
	L1W 22+25N	1	12	13	87	.2	11	7	347	2.33	2	5	ND	3	30	1	2	3	40	.28	.065	13	20	.29	82	.12	5	1.19	.01	.06	1	1	5
	L1W 22+00N	1	12	8	81	.1	10	7	424	2.38	2	5	ND	1	33	1	2	2	40	.36	.064	17	21	.26	88	.11	2	1.24	.01	.05	1	1	5
	L1W 21+75N	1	12	4	39	.4	9	4	202	1.98	2	6	ND	4	21	1	3	6	39	.20	.019	13	17	.20	50	.12	2	.64	.01	.10	1	1	40
	L1W 21+50N	1	12	7	47	.3	4	5	612	1.97	4	5	ND	3	26	1	2	2	36	.23	.030	16	14	.17	117	.09	3	.75	.01	.19	1	3	5
	STD C/AU-S	20	64	42	132	8.0	69	31	1088	4.28	44	25	9	41	53	19	16	23	59	.48	.091	40	60	.96	186	.08	38	1.81	.07	.16	14	49	1300

Grid	SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
	L1W 21+25N	1	4	4	60	.2	9	5	435	1.95	3	5	ND	1	29	1	2	2	33	.28	.086	13	17	.18	102	.08	2	1.01	.01	.16	1	3	5
	L1W 20+50N	1	5	4	33	.1	6	3	136	1.54	3	5	ND	1	30	1	2	2	25	.25	.022	12	14	.22	88	.07	3	1.04	.02	.05	1	1	5
	L1W 20+25N	1	5	8	78	.2	10	5	463	2.19	2	5	ND	1	31	1	2	2	38	.30	.079	13	17	.20	106	.07	2	1.14	.01	.09	1	1	5
	L1W 20+00N	1	4	2	80	.2	9	4	455	1.86	2	5	ND	1	30	1	2	2	31	.31	.053	13	15	.18	113	.05	3	1.15	.01	.13	1	2	5
	L1W 19+75N	1	2	8	55	.2	8	4	394	1.78	3	5	ND	1	21	1	2	2	33	.18	.047	12	15	.14	85	.08	3	.96	.01	.08	1	1	5
"A" Grid	L1W 19+50N	1	3	2	60	.1	5	4	335	1.47	2	5	ND	1	19	1	3	2	28	.18	.048	11	14	.11	91	.06	2	.75	.01	.07	1	2	5
	L1W 19+25N	1	6	4	49	.3	12	5	249	2.30	3	5	ND	2	25	1	2	2	40	.26	.044	14	18	.23	77	.07	3	1.02	.01	.08	1	1	5
	L1W 19+00N	1	3	5	49	.1	6	3	196	1.68	2	5	ND	1	22	1	2	3	29	.24	.025	16	15	.17	55	.07	2	.81	.01	.07	1	92	5
	L1W 18+75N	1	6	7	53	.1	8	5	253	1.81	2	5	ND	1	26	1	3	2	31	.21	.039	14	16	.21	87	.08	2	1.11	.01	.05	1	7	5
	L1W 18+50N	1	6	4	44	.2	9	4	207	1.88	5	5	ND	1	25	1	2	2	34	.26	.028	14	16	.19	68	.10	2	.84	.01	.08	1	1	5
	L1W 18+00N	1	5	9	52	.2	10	3	163	1.91	2	5	ND	1	23	1	2	2	34	.22	.057	12	18	.16	82	.08	2	1.09	.01	.05	1	1	5
	L1W 17+75N	1	6	6	72	.3	11	4	461	1.90	2	5	ND	1	25	1	2	2	31	.25	.079	12	17	.15	107	.07	2	1.16	.01	.09	1	2	10
	L1W 17+50N	1	5	9	82	.5	11	5	359	1.83	2	5	ND	1	23	1	2	2	29	.23	.081	13	16	.16	99	.06	3	1.28	.01	.10	1	1	20
	LOW 30+75N	1	6	6	36	.2	7	3	180	1.27	3	5	ND	1	33	1	2	2	24	.23	.030	13	11	.19	103	.09	4	.92	.02	.08	1	1	5
	LOW 30+50N	1	5	5	92	.1	9	3	606	2.23	2	5	ND	1	34	1	3	2	39	.27	.089	13	18	.20	133	.08	2	1.12	.01	.14	1	1	5
	LOW 30+25N	1	4	12	41	.2	7	4	229	1.96	6	5	ND	2	41	1	5	2	34	.30	.066	14	16	.21	113	.08	2	1.10	.01	.08	1	1	20
	LOW 30+00N	1	8	8	46	.5	12	4	187	2.23	7	6	ND	2	26	1	2	2	40	.22	.074	12	16	.19	101	.08	3	1.39	.01	.10	1	9	30
	LOW 29+75N	1	7	7	72	.3	14	6	234	2.56	4	5	ND	1	25	1	2	2	45	.22	.064	13	18	.22	129	.08	3	1.89	.01	.10	1	2	20
	LOW 29+50N	1	3	9	32	.2	7	3	169	1.82	4	5	ND	1	27	1	3	2	33	.24	.036	13	14	.22	92	.10	4	1.13	.01	.05	2	3	10
	LOW 29+25N	1	6	2	50	.2	9	4	226	1.70	4	5	ND	1	28	1	2	2	31	.23	.029	13	16	.23	86	.09	4	1.05	.02	.07	1	1	5
"B" Grid	LOW 29+00N	1	1	5	38	.1	5	4	166	1.24	2	5	ND	1	27	1	2	2	24	.26	.035	13	12	.22	77	.10	2	.83	.02	.04	1	1	5
	LOW 28+75N	1	7	8	45	.1	8	4	255	1.93	6	5	ND	1	34	1	2	3	39	.34	.052	14	15	.25	78	.10	4	.93	.01	.08	1	27	5
	LOW 28+50N	1	3	5	36	.1	5	2	152	1.19	2	5	ND	1	23	1	2	2	22	.21	.023	12	12	.21	67	.10	2	.89	.01	.07	1	1	5
	LOW 28+25N	1	5	10	46	.4	6	4	256	1.67	3	5	ND	1	24	1	2	2	30	.20	.023	14	12	.20	72	.07	3	1.07	.01	.09	2	1	5
	LOW 28+00N	1	6	6	54	.3	10	4	249	1.79	3	5	ND	1	27	1	2	3	31	.23	.035	16	13	.21	90	.08	2	1.17	.01	.07	1	2	10
	LOW 27+75N	1	4	7	55	.2	7	3	317	1.69	3	5	ND	1	21	1	2	3	31	.17	.025	14	13	.18	75	.08	2	1.17	.01	.05	1	1	5
	LOW 27+50N	1	4	7	51	.3	7	4	293	1.83	2	5	ND	1	30	1	2	2	33	.28	.042	11	13	.17	77	.07	3	1.28	.01	.06	1	1	5
	LOW 27+25N	1	4	7	96	.3	14	6	218	2.11	4	5	ND	1	22	1	2	2	33	.17	.073	12	17	.17	108	.06	7	2.06	.01	.08	1	1	5
	LOW 27+00N	1	4	10	73	.2	11	4	397	1.89	2	5	ND	1	26	1	3	3	32	.22	.054	13	14	.17	112	.07	5	1.64	.01	.03	1	2	10
	LOW 26+75N	1	3	6	35	.2	5	3	156	1.23	2	5	ND	1	24	1	4	2	23	.21	.023	12	11	.19	80	.10	2	.95	.01	.08	1	1	5
	L1E 30+75N	1	2	8	30	.3	7	3	165	1.14	2	5	ND	1	28	1	2	2	22	.24	.033	13	11	.18	88	.09	5	.92	.02	.06	1	1	5
	L1E 30+50N	1	15	8	80	.2	14	8	887	2.55	5	5	ND	1	48	1	2	2	42	.37	.083	18	19	.30	143	.07	2	1.43	.02	.21	1	4	30
	L1E 30+25N	1	5	8	82	.4	11	6	354	2.44	5	5	ND	1	26	1	2	2	41	.23	.163	13	17	.20	103	.08	4	1.71	.01	.06	1	12	40
	L1E 30+00N	1	3	4	97	.2	9	4	428	1.98	2	5	ND	1	27	1	3	2	31	.21	.151	12	35	.12	110	.06	4	1.80	.01	.08	1	1	20
	L1E 29+75N	1	4	6	47	.1	7	5	240	2.02	4	5	ND	1	34	1	3	2	38	.29	.048	12	16	.22	105	.09	4	1.19	.01	.05	1	1	10
	L1E 29+50N	1	4	8	42	.1	6	3	193	1.60	2	5	ND	1	25	1	2	2	33	.19	.017	12	13	.19	85	.09	2	1.05	.01	.04	1	1	10
	STD C/AU-S	21	61	42	137	8.2	74	31	1081	4.13	37	20	8	40	56	19	18	21	60	.48	.093	41	62	.96	189	.08	36	1.97	.08	.17	14	47	1300

	SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
	L1E 29+25N	1	8	10	69	.2	11	6	333	2.13	3	5	ND	2	21	1	2	5	33	.18	.053	13	13	.26	126	.06	5	1.98	.01	.06	1	1	10
	L1E 29+00N	1	10	16	103	.5	16	6	191	2.42	4	5	ND	3	26	1	2	4	35	.19	.072	12	15	.23	114	.05	3	2.54	.02	.09	1	5	20
	L1E 28+75N	2	11	12	72	.1	10	6	591	2.86	2	5	ND	1	37	1	2	2	51	.29	.069	17	18	.33	144	.07	8	2.39	.01	.09	2	1	10
B" Grid	L1E 28+50N	1	7	8	47	.1	7	5	245	1.86	5	5	ND	2	35	1	3	2	34	.32	.077	14	11	.24	92	.08	10	.99	.02	.08	1	1	5
	L1E 28+25N	1	10	11	97	.1	8	6	830	1.89	3	5	ND	1	26	1	2	2	30	.25	.085	13	13	.21	97	.06	4	1.26	.01	.07	1	1	5
	L1E 28+00N	1	10	11	62	.1	12	6	156	2.16	2	5	ND	2	20	1	2	4	31	.14	.116	11	14	.19	99	.05	2	2.20	.01	.06	1	1	5
	L1E 27+75N	1	5	7	38	.1	9	5	150	1.75	2	5	ND	1	18	1	2	2	30	.15	.044	9	11	.17	87	.07	2	1.23	.01	.06	2	1	5
	L1E 24+00N	3	14	14	75	.5	23	8	317	3.30	2	5	ND	4	56	1	3	7	60	.29	.086	15	33	.63	107	.11	2	2.77	.01	.12	1	1	20
	L1E 23+75N	1	9	14	88	.3	14	6	260	2.14	2	5	ND	3	24	1	2	2	35	.20	.068	11	14	.20	109	.07	4	1.64	.01	.07	1	1	5
	L1E 23+50N	2	14	19	141	.3	24	10	731	4.07	2	5	ND	2	41	1	4	5	76	.29	.190	17	36	.74	121	.12	3	2.95	.01	.11	1	2	30
	L1E 23+25N	2	19	28	97	.1	38	20	1857	4.35	2	5	ND	2	151	1	2	2	89	.98	.128	40	48	1.37	202	.08	4	3.73	.01	.17	1	1	40
"A" Grid	L1E 23+00N	2	13	18	131	.1	37	9	698	3.94	2	5	ND	4	82	1	2	2	83	.49	.114	17	51	.89	175	.19	5	3.38	.01	.24	1	1	5
	L1E 22+75N	1	8	6	68	.3	18	6	373	2.08	2	5	ND	3	39	1	2	3	38	.28	.045	13	21	.28	116	.09	5	1.52	.01	.10	1	1	5
	L1E 22+50N	1	14	12	74	.2	23	10	1160	2.93	2	5	2	4	62	1	2	2	48	.47	.074	21	26	.75	156	.11	2	1.97	.02	.11	1	1	10
	L1E 22+25N	1	5	13	48	.1	9	5	487	1.63	4	5	ND	2	40	1	2	4	25	.32	.059	16	12	.22	131	.07	5	1.26	.02	.13	1	2	20
	L1E 22+00N	1	6	10	41	.1	7	5	480	1.75	2	5	ND	1	24	1	2	4	32	.22	.018	12	12	.16	81	.08	8	.77	.01	.10	1	1	5
	L1E 21+75N	1	8	6	52	.1	9	4	559	1.85	2	5	ND	2	24	1	2	5	32	.23	.030	15	14	.20	84	.07	2	1.02	.01	.09	1	1	10
	L1E 21+50N	1	7	8	40	.1	6	4	359	1.76	2	5	ND	2	24	1	2	2	31	.22	.030	13	13	.22	76	.07	6	.92	.01	.08	1	21	5
	L1E 21+25N	1	7	7	39	.2	7	4	336	1.60	2	5	ND	3	21	1	2	2	30	.19	.020	13	12	.18	67	.08	11	.75	.02	.07	1	1	5
	L2E 30+50N	1	9	9	45	.1	9	4	393	1.75	2	5	ND	1	26	1	3	2	29	.22	.030	13	11	.21	82	.07	3	1.05	.01	.07	2	1	10
	L2E 30+25N	1	6	6	47	.1	7	4	283	1.86	3	5	ND	2	21	1	2	2	30	.18	.059	12	12	.20	85	.07	2	1.16	.01	.06	1	1	20
	L2E 30+00N	1	6	9	54	.1	9	3	183	1.88	2	5	ND	1	24	1	2	2	29	.19	.057	11	11	.20	90	.06	3	1.52	.01	.05	1	2	10
	L2E 29+75N	1	7	11	58	.1	11	6	492	2.22	3	5	ND	2	17	1	2	3	34	.17	.103	12	14	.19	93	.06	6	1.74	.01	.09	1	1	30
	L2E 29+50N	1	9	10	35	.1	5	2	178	1.85	2	5	ND	1	20	1	2	2	34	.20	.036	12	13	.18	74	.08	2	.99	.01	.05	1	1	5
	L2E 29+25N	1	6	10	32	.1	5	3	151	1.52	2	5	ND	1	16	1	2	2	28	.16	.016	12	10	.17	70	.08	2	.90	.01	.06	1	1	5
8" Grid	L2E 29+00N	1	6	8	32	.1	5	3	143	1.51	2	5	ND	2	17	1	2	2	28	.14	.017	10	10	.15	82	.06	2	.99	.01	.05	1	1	10
	L2E 28+75N	2	9	15	52	.1	10	4	187	2.51	4	5	ND	4	10	1	2	2	39	.09	.048	13	16	.22	69	.07	2	2.64	.01	.04	1	1	20
	L2E 28+50N	1	6	15	51	.1	8	4	357	2.23	2	5	ND	2	11	1	2	2	38	.11	.040	12	14	.18	67	.08	3	1.89	.01	.05	2	2	10
	L2E 28+25N	1	6	12	58	.1	6	4	671	2.06	2	5	ND	2	11	1	2	2	34	.14	.043	11	11	.15	68	.05	2	2.04	.01	.06	1	1	30
	L2E 28+00N	1	8	15	45	.1	4	3	225	1.54	2	5	ND	6	20	1	2	2	20	.19	.035	17	7	.15	123	.05	3	2.81	.01	.16	1	1	20
	L2E 27+75N	1	8	7	63	.1	9	5	464	1.82	2	5	ND	2	16	1	2	2	29	.17	.054	14	10	.20	88	.08	2	1.61	.01	.09	1	1	10
	L2E 27+50N	1	6	6	35	.2	8	3	154	1.39	2	5	ND	1	21	1	2	4	24	.22	.018	9	8	.18	51	.06	4	.79	.01	.08	1	2	5
	L2E 27+25N	1	7	7	41	.1	8	5	266	1.68	2	5	ND	1	19	1	2	2	31	.14	.023	11	11	.19	63	.07	3	.93	.01	.03	1	1	5
	L2E 27+00N	1	5	8	39	.1	6	3	191	1.52	2	5	ND	1	18	1	2	2	29	.15	.014	10	11	.17	58	.07	2	.86	.01	.07	2	1	5
	L2E 26+75N	1	4	3	34	.3	8	4	258	1.64	2	5	ND	2	21	1	3	2	29	.17	.026	11	10	.18	67	.07	2	.90	.01	.06	1	1	10
"A" Grid	L2E 24+00N	1	6	12	61	.1	9	5	239	1.96	4	5	ND	1	18	1	2	2	32	.15	.044	11	13	.17	89	.07	2	1.46	.01	.06	1	1	5
	STD C/AU-S	21	62	41	132	7.6	72	31	1083	4.15	42	17	8	39	53	20	17	24	58.	.48	.088	40	59	.96	183	.08	36	1.99	.07	.15	11	53	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L2E 23+75N	1	4	7	35	.1	3	2	135	.95	2	5	ND	3	28	1	3	3	20	.27	.026	15	10	.19	91	.09	2	.74	.02	.05	1	2	10
L2E 23+50N	2	10	10	81	.1	12	6	349	2.86	4	5	ND	3	14	1	2	2	51	.11	.060	15	20	.26	117	.08	2	2.83	.01	.06	1	1	20
L2E 23+25N	1	18	11	133	.1	22	12	1386	3.63	2	5	ND	2	53	1	2	2	54	.45	.076	21	25	.74	192	.09	4	3.08	.01	.08	1	1	20
L2E 23+00N	1	8	9	102	.1	14	7	648	2.19	2	5	ND	1	31	1	2	2	34	.32	.072	15	15	.34	134	.08	2	1.61	.01	.09	1	1	10
L2E 22+75N	1	5	9	43	.1	7	4	225	1.58	2	5	ND	2	23	1	2	2	30	.23	.027	13	12	.19	79	.09	2	.80	.01	.06	1	1	5
L2E 22+50N	1	6	5	58	.1	7	3	275	1.68	2	5	ND	1	22	1	2	2	30	.24	.043	14	13	.18	75	.08	3	.91	.01	.07	1	1	5
L2E 22+25N	1	10	6	69	.1	8	3	293	1.90	2	5	ND	1	24	1	2	3	34	.25	.038	13	14	.20	79	.08	2	.87	.01	.11	1	2	5
L2E 22+00N	1	9	7	72	.1	9	4	441	1.67	2	5	ND	1	26	1	2	2	29	.30	.034	16	14	.19	89	.08	6	.92	.01	.11	1	23	5
L2E 21+75N	1	9	4	47	.1	9	4	291	1.76	2	5	ND	2	27	1	2	2	30	.27	.025	17	13	.23	75	.07	2	.93	.02	.12	1	1	10
L2E 21+50N	1	7	6	53	.1	9	3	202	1.57	2	5	ND	1	22	1	2	2	27	.23	.016	13	12	.22	65	.08	9	.87	.02	.06	1	1	5
L2E 21+25N	1	8	8	53	.1	8	3	245	1.85	2	5	ND	1	23	1	3	2	33	.26	.026	15	15	.22	74	.08	4	.89	.01	.09	1	2	5
L2E 21+00N	1	7	10	51	.1	8	4	272	1.70	2	5	ND	1	24	1	2	2	30	.27	.030	15	12	.18	67	.08	7	.85	.02	.10	1	1	5
L2E 20+75N	1	9	9	109	.1	10	6	257	2.10	2	5	ND	2	33	1	2	2	34	.41	.089	14	17	.23	99	.07	2	1.39	.01	.07	1	1	5
L2E 20+50N	1	8	3	70	.1	14	5	191	2.12	3	5	ND	2	20	1	2	2	35	.24	.081	13	16	.20	94	.07	10	1.51	.01	.08	1	1	5
L2E 20+25N	1	9	9	44	.2	10	5	217	1.88	4	5	ND	2	21	1	2	2	33	.22	.040	14	15	.24	107	.07	5	1.66	.01	.04	2	1	5
L2E 20+00N	1	13	5	50	.1	15	8	252	2.77	2	5	ND	3	29	1	2	2	53	.31	.043	18	31	.63	114	.08	2	1.95	.02	.04	1	1	20
L2E 19+75N	2	28	7	95	.1	24	14	933	3.95	2	5	ND	1	58	1	2	3	65	.80	.119	31	32	1.03	149	.08	9	2.32	.03	.08	1	2	20
L2E 19+50N	1	8	3	54	.1	8	5	238	2.01	4	5	ND	2	21	1	3	2	35	.23	.104	13	15	.17	80	.07	2	1.02	.01	.11	1	1	5
L2E 19+25N	1	12	5	35	.1	8	4	311	1.75	2	5	ND	1	29	1	2	2	34	.38	.052	18	14	.24	87	.07	4	.93	.03	.06	1	1	30
L2E 19+00N	1	10	8	41	.2	11	4	381	1.96	2	5	ND	3	31	1	2	2	36	.30	.038	19	14	.25	83	.08	5	.94	.02	.12	1	1	20
L2E 18+75N	1	8	8	35	.3	7	4	172	1.71	2	5	ND	2	23	1	2	2	33	.22	.022	13	14	.19	66	.09	5	.83	.01	.08	1	2	5
L2E 18+50N	1	6	5	30	.2	5	3	155	1.41	2	5	ND	3	24	1	3	2	28	.23	.027	14	12	.18	64	.09	14	.68	.02	.08	2	1	5
L2E 18+25N	1	23	7	83	.1	15	11	701	3.47	6	5	ND	2	60	1	2	2	51	.54	.080	22	23	.75	166	.07	2	1.93	.03	.13	1	1	60
L2E 18+00N	1	26	5	89	.1	17	12	761	3.64	3	5	ND	3	61	1	2	2	53	.56	.088	22	24	.84	147	.07	4	2.04	.03	.13	1	1	80
L3E 30+75N	1	8	5	33	.2	6	4	318	1.46	2	5	ND	1	29	1	2	2	25	.28	.025	14	11	.23	81	.07	6	.96	.02	.09	2	1	10
L3E 30+50N	1	9	6	33	.2	4	3	199	1.15	2	5	ND	1	28	1	2	2	21	.31	.019	13	10	.20	77	.07	2	.88	.02	.10	1	1	20
L3E 30+25N	1	8	9	35	.1	5	4	232	1.24	2	5	ND	1	24	1	2	2	21	.40	.027	15	10	.21	66	.06	2	.96	.02	.09	1	1	20
L3E 29+75N	1	9	3	35	.2	7	3	207	1.92	2	6	ND	2	23	1	3	2	37	.24	.047	13	15	.20	84	.08	3	.98	.02	.08	1	2	10
L3E 29+50N	1	6	8	47	.2	8	4	181	1.62	2	9	ND	2	16	1	2	2	30	.16	.025	12	11	.19	74	.07	4	1.08	.01	.05	2	1	5
L3E 29+25N	1	6	4	45	.2	7	4	244	1.82	3	5	ND	1	23	1	2	2	33	.23	.032	14	13	.22	99	.08	6	1.11	.01	.06	2	1	5
L3E 29+00N	1	9	6	42	.1	8	5	237	2.11	5	5	ND	1	22	1	3	4	38	.24	.045	15	16	.25	82	.08	6	1.19	.01	.08	1	1	5
L3E 28+75N	1	4	10	83	.1	8	3	134	1.47	2	5	ND	2	17	1	3	2	25	.17	.039	14	12	.18	121	.07	2	2.15	.01	.07	1	1	5
L3E 28+50N	1	10	7	47	.4	11	5	213	2.32	3	5	ND	3	19	1	2	2	43	.31	.038	15	16	.22	100	.07	3	1.92	.01	.11	2	1	10
L3E 28+25N	1	6	2	88	.1	8	4	526	1.79	2	5	ND	7	42	1	2	2	25	.34	.051	25	11	.23	192	.05	2	2.30	.01	.20	1	1	5
L3E 28+00N	1	6	2	40	.1	8	4	193	1.59	2	5	ND	1	22	1	2	2	28	.21	.025	13	10	.23	68	.07	3	1.02	.01	.06	1	2	5
L3E 27+75N	1	7	6	34	.4	6	4	247	1.70	4	6	ND	1	17	1	2	2	32	.15	.028	11	12	.19	74	.07	4	.87	.01	.06	1	1	5
STD C/AU-S	19	63	38	132	6.9	73	30	1069	4.21	42	18	8	38	49	19	17	20	59	.48	.085	41	61	.95	183	.07	32	1.96	.07	.17	13	53	1300

"A" Grid

"B" Grid

	SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
	L3E 27+50W	1	10	9	55	.1	12	4	232	2.13	2	5	ND	3	22	1	2	2	35	.19	.030	16	14	.26	90	.06	2	1.94	.01	.06	1	1	20
"B" Grid	L3E 27+25W	1	10	9	54	.1	6	6	411	2.61	2	5	ND	1	30	1	2	2	60	.37	.069	19	12	.45	113	.11	2	1.71	.01	.13	1	1	10
	L3E 27+00W	1	9	7	100	.1	10	5	334	2.51	4	5	ND	3	19	1	2	2	41	.17	.061	14	16	.21	101	.07	2	2.54	.01	.05	1	1	30
	L3E 26+75W	1	7	9	79	.1	12	5	847	2.07	2	5	ND	2	17	1	2	2	36	.17	.083	13	14	.16	114	.07	2	1.98	.01	.06	1	1	10
	L3E 24+00W	2	9	5	121	.1	14	6	1056	2.43	2	5	ND	3	19	1	2	2	41	.15	.058	14	20	.27	110	.09	2	2.70	.01	.07	1	2	20
	L3E 23+75W	3	13	14	108	.1	24	7	500	3.55	5	5	ND	5	23	1	2	2	61	.14	.134	15	28	.36	120	.11	2	3.80	.01	.06	1	1	20
	L3E 23+50W	2	14	12	113	.1	27	9	1106	3.34	6	5	ND	3	52	1	2	2	52	.42	.092	18	27	.52	205	.11	2	4.10	.01	.10	1	3	10
	L3E 23+25W	1	15	15	98	.1	26	10	1262	3.62	3	5	ND	6	65	1	2	2	73	.59	.072	26	34	.74	220	.15	2	2.80	.02	.11	1	1	20
	L3E 23+00W	2	17	14	158	.1	28	18	2442	4.17	3	5	ND	8	106	1	2	2	86	.88	.104	35	40	.90	327	.29	2	3.47	.01	.26	1	1	30
	L3E 22+75W	1	9	8	67	.1	7	3	302	1.84	2	5	ND	2	23	1	2	2	32	.24	.080	12	15	.19	88	.09	4	1.10	.01	.09	1	1	20
	L3E 22+50W	1	8	6	70	.1	8	3	307	1.73	5	5	ND	1	22	1	2	2	27	.24	.090	12	13	.17	148	.06	2	1.29	.01	.10	1	2	10
	L3E 22+25W	1	7	6	44	.1	6	3	182	1.42	2	5	ND	3	19	1	2	2	27	.21	.017	12	12	.16	69	.08	2	.85	.01	.07	1	1	5
	L3E 22+00W	1	7	9	48	.1	5	2	161	1.45	2	5	ND	3	17	1	2	2	28	.19	.020	13	11	.16	80	.08	5	.88	.01	.05	1	1	5
	L3E 21+75W	1	7	5	34	.1	4	3	142	1.33	2	5	ND	3	20	1	2	2	26	.19	.017	13	11	.15	71	.09	2	.79	.01	.06	1	2	5
"A" Grid	L3E 21+50W	1	9	8	39	.1	7	4	166	1.59	2	5	ND	3	20	1	2	2	30	.21	.024	13	12	.18	70	.09	2	.89	.01	.06	2	1	10
	L3E 21+25W	1	9	3	47	.1	8	4	195	1.96	2	5	ND	3	21	1	2	2	39	.21	.022	14	16	.18	66	.10	5	.82	.02	.07	1	1	5
	L3E 21+00W	1	9	8	57	.1	8	3	332	1.90	2	5	ND	2	25	1	2	2	36	.29	.033	13	18	.30	63	.13	2	1.04	.02	.08	1	1	5
	L3E 20+75W	1	9	7	59	.1	9	4	202	1.91	2	5	ND	3	23	1	5	2	33	.25	.047	14	16	.24	99	.08	3	1.24	.02	.07	1	1	5
	L3E 20+50W	1	8	5	34	.1	8	3	184	1.98	2	5	ND	3	22	1	2	2	43	.23	.014	13	18	.17	73	.11	2	.73	.01	.09	1	1	5
	L3E 20+25W	1	8	6	41	.1	5	4	329	1.88	2	5	ND	3	21	1	2	2	38	.24	.029	12	16	.16	87	.09	2	.73	.01	.13	1	2	5
	L3E 19+75W	1	30	11	89	.2	20	7	684	3.43	5	5	ND	3	60	1	2	2	46	.75	.067	47	26	.48	147	.04	2	3.09	.02	.18	1	1	40
	L3E 19+50W	1	10	10	47	.1	6	4	450	1.93	4	5	ND	3	27	1	2	5	35	.25	.045	19	15	.22	88	.07	8	1.11	.02	.07	1	2	20
	L3E 19+25W	1	9	7	46	.2	4	3	298	1.45	4	5	ND	3	18	1	2	3	27	.17	.026	13	12	.16	61	.07	3	.97	.01	.07	1	1	5
	L3E 19+00W	1	7	4	45	.2	5	3	193	1.67	2	5	ND	3	21	1	2	2	32	.21	.031	12	13	.18	69	.08	2	.95	.01	.06	1	1	5
	L3E 18+75W	1	7	6	37	.2	4	2	217	1.42	2	5	ND	4	18	1	4	2	28	.19	.016	13	13	.15	61	.09	2	.83	.01	.06	1	1	5
	L3E 18+50W	1	9	6	26	.1	3	2	133	1.16	2	5	ND	3	20	1	3	2	23	.19	.010	11	10	.17	52	.09	2	.69	.01	.05	1	2	5
	L3E 18+25W	1	7	9	30	.3	4	2	174	1.56	2	5	ND	4	26	1	2	2	31	.25	.034	15	13	.19	68	.10	2	.70	.02	.07	1	1	20
	L3E 18+00W	1	22	12	61	.1	12	7	473	2.95	11	5	ND	6	59	1	3	2	46	.49	.056	23	20	.46	140	.07	2	1.57	.03	.12	1	1	50
	L3E 17+75W	1	22	11	59	.1	14	7	679	2.77	7	5	ND	5	58	1	4	2	47	.52	.061	21	18	.45	133	.07	3	1.26	.03	.12	1	2	30
	L3E 17+50W	1	25	15	91	.1	15	10	2229	3.29	2	5	ND	2	57	1	2	2	43	.53	.076	32	21	.40	193	.03	6	3.22	.02	.10	1	1	20
	L4E 30+75W	1	11	8	44	.2	5	4	371	1.61	3	5	ND	3	24	1	2	2	29	.21	.020	14	12	.21	77	.07	2	1.03	.01	.07	1	2	10
	L4E 30+50W	1	13	8	49	.1	6	4	517	1.82	2	5	ND	2	27	1	2	2	28	.25	.030	15	14	.23	97	.06	3	1.53	.01	.09	1	1	10
	L4E 30+25W	1	9	8	38	.2	6	4	235	1.49	3	5	ND	4	23	1	4	2	27	.21	.018	13	11	.22	77	.08	2	1.05	.01	.08	1	1	5
"B" Grid	L4E 30+00W	1	13	8	52	.1	7	5	453	1.98	4	5	ND	2	25	1	2	3	34	.24	.040	15	15	.22	102	.07	2	1.47	.01	.07	1	2	20
	L4E 29+75W	1	14	5	79	.2	11	6	229	2.69	2	5	ND	3	28	1	2	2	42	.31	.085	11	17	.28	94	.05	3	2.03	.01	.07	1	4	10
	L4E 29+50W	1	8	5	40	.1	7	3	372	1.68	2	5	ND	4	18	1	4	2	33	.19	.026	12	13	.14	64	.07	2	.92	.01	.07	1	1	5
	STD C/AU-S	19	62	36	132	6.9	69	31	1057	4.08	44	15	8	39	48	19	17	17	59	.47	.090	40	59	.94	182	.07	33	1.93	.07	.13	13	52	1300

MINGOLD RESOURCES PROJECT-620 FILE # 88-1752

	SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
	L4E 29+25N	1	10	6	49	.1	6	4	378	1.92	4	5	ND	1	25	1	2	5	31	.22	.040	13	11	.25	90	.06	9	1.30	.01	.07	1	9	10
	L4E 29+00N	1	8	9	38	.2	3	2	310	1.61	2	5	ND	1	25	1	2	2	29	.22	.034	11	10	.15	74	.05	3	1.02	.01	.07	1	7	5
	L4E 28+75N	1	8	6	70	.1	7	5	508	1.99	2	5	ND	1	23	1	3	5	31	.18	.167	11	13	.14	169	.05	4	1.43	.01	.06	1	1	5
	L4E 28+50N	1	10	10	48	.1	7	5	264	2.12	6	5	ND	2	29	1	2	2	37	.24	.046	12	14	.23	94	.07	5	1.22	.01	.07	1	1	5
	L4E 28+25N	1	34	6	77	.1	11	6	1676	1.95	2	5	ND	2	27	1	2	2	31	.28	.052	16	13	.19	123	.05	4	1.43	.01	.07	1	1	10
"B" Grid	L4E 28+00N	1	12	3	42	.1	7	5	996	1.81	2	5	ND	1	29	1	2	4	31	.27	.028	10	13	.25	106	.05	4	1.53	.01	.05	1	1	10
	L4E 27+75N	1	7	5	34	.2	3	2	153	1.26	3	5	ND	3	21	1	2	2	22	.19	.015	12	10	.18	69	.07	5	.91	.01	.06	1	8	5
	L4E 27+50N	1	8	10	49	.2	8	3	197	1.63	2	6	ND	3	23	1	3	5	29	.23	.066	11	11	.14	73	.06	6	1.16	.01	.08	1	1	5
	L4E 27+25N	1	7	7	21	.1	1	2	156	.96	6	5	ND	2	21	1	2	2	20	.19	.007	11	9	.18	61	.08	5	.88	.02	.04	1	4	5
	L4E 27+00N	1	7	9	42	.3	5	4	165	1.73	2	5	ND	3	16	1	2	4	29	.13	.030	13	12	.18	93	.07	4	1.61	.01	.05	1	2	10
	L4E 26+75N	1	9	9	62	.2	10	4	360	2.31	3	5	ND	3	14	1	3	2	37	.13	.079	13	16	.23	93	.07	8	2.16	.01	.05	1	1	5
	L4E 24+00N	1	9	7	41	.2	6	4	225	1.79	5	5	ND	4	20	1	2	2	33	.20	.032	12	14	.20	83	.08	8	1.11	.01	.05	1	1	5
	L4E 23+75N	1	8	7	98	.1	11	6	725	2.09	2	5	ND	2	25	1	3	2	32	.26	.086	12	14	.17	126	.06	5	1.90	.01	.07	1	8	5
	L4E 23+50N	1	9	5	36	.1	8	3	232	1.75	4	5	ND	4	19	1	2	2	35	.19	.020	13	14	.16	73	.09	2	.80	.01	.06	2	1	5
	L4E 23+25N	1	9	7	113	.2	7	3	632	1.77	2	5	ND	5	23	1	2	2	29	.33	.043	15	12	.21	181	.09	2	1.11	.01	.14	1	2	5
	L4E 23+00N	1	7	5	53	.1	5	2	186	1.26	3	5	ND	3	15	1	2	2	22	.18	.015	13	8	.12	73	.08	3	.92	.01	.08	1	1	5
	L4E 22+75N	1	8	6	43	.4	9	3	159	1.62	4	7	ND	3	15	1	3	3	27	.18	.051	12	12	.14	81	.07	3	1.11	.01	.07	2	4	5
	L4E 22+50N	1	7	3	44	.2	5	3	171	1.40	2	5	ND	3	16	1	2	2	26	.18	.021	11	21	.15	70	.07	2	.95	.01	.06	1	1	5
	L4E 22+25N	1	7	6	37	.2	8	2	343	1.37	2	5	ND	2	20	1	2	3	25	.20	.010	14	11	.16	71	.09	2	.80	.01	.06	1	1	5
	L4E 22+00N	1	8	5	47	.2	7	3	204	1.53	2	5	ND	3	20	1	2	2	27	.21	.033	13	11	.16	74	.07	7	.90	.01	.06	1	3	5
	L4E 21+75N	1	10	7	44	.3	9	3	174	1.87	3	5	ND	4	22	1	2	5	32	.24	.043	13	14	.20	96	.07	2	1.14	.01	.07	2	1	5
"A" Grid	L4E 21+50N	1	9	4	60	.1	7	3	190	1.75	3	5	ND	3	23	1	2	2	31	.27	.039	13	14	.16	90	.07	2	1.05	.01	.07	1	3	5
	L4E 21+25N	1	11	6	46	.1	7	3	363	1.43	7	5	ND	4	25	1	3	2	27	.31	.021	24	14	.21	69	.08	11	.99	.02	.08	2	1	5
	L4E 21+00N	2	13	10	67	.4	10	4	883	1.49	5	8	ND	3	32	1	2	2	25	.46	.032	20	12	.21	96	.05	10	1.01	.02	.08	1	1	30
	L4E 20+75N	1	12	3	45	.3	10	4	442	1.93	5	5	ND	3	27	1	2	5	34	.31	.032	13	15	.20	92	.08	2	.88	.01	.14	1	1	10
	L4E 20+50N	1	10	9	80	.1	9	4	312	2.03	2	5	ND	2	26	1	2	2	33	.27	.088	12	17	.18	102	.07	2	1.06	.01	.15	1	4	5
	L4E 20+25N	1	7	8	45	.2	4	2	220	1.50	2	5	ND	3	23	1	4	2	25	.25	.038	13	13	.22	78	.07	2	.96	.01	.08	2	22	5
	L4E 20+00N	1	9	6	38	.2	3	2	217	1.49	5	5	ND	4	24	1	4	5	26	.23	.021	15	13	.18	67	.07	3	.86	.01	.07	1	1	10
	L4E 19+75N	1	8	3	32	.1	3	2	261	1.34	5	5	ND	3	25	1	3	2	26	.23	.026	14	10	.18	80	.08	2	.74	.02	.08	1	1	5
	L4E 19+50N	1	7	6	36	.1	6	4	341	1.49	3	5	ND	4	22	1	2	2	27	.23	.018	14	11	.18	78	.07	2	.91	.01	.07	2	3	5
	L4E 19+25N	1	9	6	100	.1	13	4	312	2.13	3	5	ND	2	17	1	2	2	30	.19	.119	13	15	.19	121	.05	2	2.09	.01	.06	1	1	10
	L4E 19+00N	1	11	7	40	.3	7	3	194	1.59	4	5	ND	3	19	1	3	5	28	.21	.029	12	12	.19	63	.07	2	.99	.01	.07	2	1	5
	L4E 18+75N	1	8	6	31	.2	2	2	148	1.37	2	5	ND	3	19	1	2	2	26	.18	.015	12	11	.16	61	.08	4	.88	.01	.06	2	1	5
	L4E 18+50N	1	7	7	29	.2	7	2	149	1.36	3	5	ND	3	19	1	2	2	24	.20	.016	13	11	.17	59	.08	3	.89	.01	.05	1	1	5
	L4E 18+25N	1	10	7	54	.3	9	4	430	1.85	5	5	ND	3	24	1	2	2	31	.25	.045	17	15	.20	110	.06	3	1.61	.01	.07	1	1	10
	L4E 18+00N	2	27	10	165	.3	27	11	1417	4.13	2	5	ND	6	56	1	2	2	55	.58	.172	32	33	.83	228	.06	2	4.74	.01	.11	1	2	30
	STD C/AU-S	18	62	37	132	6.5	68	29	1072	4.14	44	16	8	37	48	18	16	24	58	.48	.082	40	58	.94	181	.07	30	1.96	.07	.15	12	49	1400

MINGOLD RESOURCES PROJECT-620 FILE # 88-1752

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
"A" Grid { L4E 17+75W	2	14	9	143	.2	17	12	1265	3.19	2	5	ND	4	48	1	3	2	48	.38	.117	21	22	.52	217	.07	2	3.49	.01	.12	1	1	30
L4E 17+50W	2	20	10	123	.1	23	12	547	4.54	2	5	ND	4	36	1	3	2	71	.34	.166	19	37	.96	148	.10	12	3.46	.02	.08	1	1	40
L14E 33+50W	1	5	3	33	.1	4	6	169	1.99	3	5	ND	2	34	1	2	3	36	.24	.040	12	14	.20	107	.09	3	1.03	.02	.08	1	1	5
L14E 33+25W	1	5	7	71	.2	9	6	212	2.17	4	5	ND	3	25	1	2	3	33	.22	.090	11	13	.20	91	.07	2	1.95	.01	.06	1	1	10
L14E 33+00W	1	5	10	41	.1	7	5	163	1.59	2	5	ND	2	22	1	2	2	28	.21	.032	10	12	.22	72	.11	2	.98	.01	.07	1	2	5
L14E 32+75W	1	7	9	51	.1	8	7	229	2.33	5	5	ND	3	25	1	2	2	43	.24	.028	11	19	.36	68	.16	2	1.21	.01	.06	1	1	5
L14E 32+50W	1	9	9	82	.1	10	6	301	2.56	2	3	ND	2	26	1	2	2	43	.24	.042	11	20	.35	88	.13	10	1.53	.01	.07	1	4	5
L14E 32+25W	1	7	8	57	.1	11	6	192	2.35	2	5	ND	2	27	1	5	6	38	.25	.108	11	16	.24	101	.08	12	1.61	.01	.07	1	1	5
L14E 32+00W	1	5	3	88	.3	14	6	206	2.10	2	3	ND	4	19	1	4	2	35	.21	.052	12	16	.23	95	.10	2	1.62	.01	.11	1	1	5
L14E 31+75W	1	6	14	72	.1	15	8	243	2.53	2	5	ND	2	25	1	3	2	41	.23	.104	12	18	.28	110	.10	3	1.88	.01	.05	1	3	10
L14E 31+50W	1	18	12	69	.3	15	6	279	2.44	3	5	ND	5	25	1	2	3	40	.25	.065	12	22	.34	86	.11	2	1.84	.02	.10	1	1	5
L14E 31+25W	1	13	9	108	.3	23	11	271	3.86	2	5	ND	3	30	1	2	2	60	.30	.095	10	30	.42	151	.12	3	3.19	.01	.08	1	1	20
L14E 31+00W	1	8	6	131	.1	22	11	609	3.19	2	5	ND	3	35	1	2	2	48	.32	.152	10	23	.35	126	.11	2	2.66	.01	.07	1	1	5
L14E 30+75W	1	6	8	46	.1	9	7	201	2.33	3	5	ND	3	21	1	3	2	40	.15	.051	13	16	.24	119	.09	7	1.74	.01	.05	1	2	5
L14E 30+50W	1	11	8	61	.2	13	7	199	2.24	2	5	ND	3	23	1	3	2	39	.19	.039	13	19	.27	95	.11	2	1.79	.01	.07	1	2	5
L14E 30+25W	1	7	8	67	.1	17	9	332	2.86	2	5	ND	3	24	1	2	2	50	.22	.067	10	24	.33	124	.14	7	1.91	.01	.04	1	1	5
L14E 30+00W	1	11	8	58	.2	12	7	218	2.57	2	5	ND	4	27	1	2	2	43	.24	.091	12	20	.32	104	.11	2	1.71	.02	.10	1	1	5
L14E 29+75W	1	12	9	59	.3	12	7	305	2.52	4	5	ND	4	29	1	3	2	42	.30	.077	16	19	.33	99	.10	3	1.68	.02	.10	1	1	5
"C" Grid L14E 29+50W	1	12	11	168	.1	16	11	271	3.57	3	5	ND	2	29	1	2	2	57	.26	.155	11	29	.39	109	.14	3	2.16	.01	.08	1	1	5
L14E 29+25W	1	10	5	103	.1	13	9	298	2.86	3	5	ND	3	23	1	2	2	48	.23	.087	12	24	.38	92	.12	2	1.76	.01	.08	1	1	5
L14E 29+00W	1	9	9	69	.1	14	8	270	2.81	2	5	ND	3	22	1	2	2	47	.20	.073	12	23	.37	102	.13	2	1.89	.01	.06	1	2	5
L14E 28+75W	1	12	11	120	.2	17	11	503	3.06	2	5	ND	3	21	1	2	5	49	.21	.120	10	27	.38	101	.14	2	2.25	.01	.09	1	2	10
L15E 33+50W	1	5	8	42	.1	3	3	146	1.50	2	5	ND	3	14	1	2	2	25	.11	.063	11	11	.13	70	.07	5	1.15	.01	.07	1	1	5
L15E 33+25W	1	7	8	53	.3	6	4	193	1.83	3	5	ND	1	26	1	2	4	28	.26	.038	12	14	.24	90	.06	2	1.37	.01	.10	1	1	5
L15E 33+00W	1	8	8	43	.3	5	4	186	1.83	2	5	ND	3	17	1	2	2	33	.13	.017	11	12	.13	71	.06	2	1.25	.01	.09	1	1	5
L15E 32+75W	1	5	10	51	.1	7	6	272	1.97	2	5	ND	2	25	1	2	2	35	.25	.035	12	14	.24	92	.08	9	1.20	.01	.08	1	1	5
L15E 32+50W	1	7	6	61	.1	7	5	318	1.72	3	5	ND	2	22	1	2	4	31	.22	.046	10	12	.16	72	.07	6	1.19	.01	.08	1	2	5
L15E 32+25W	1	5	5	33	.3	6	4	189	1.46	3	6	ND	3	26	1	2	2	27	.25	.041	13	11	.21	69	.08	2	.86	.01	.11	2	2	5
L15E 32+00W	1	8	12	68	.1	8	6	219	2.16	2	5	ND	2	26	1	2	2	41	.27	.032	11	21	.31	68	.16	2	1.11	.01	.05	1	4	5
L15E 31+75W	1	9	9	51	.1	9	5	215	2.07	3	5	ND	1	23	1	2	2	36	.22	.025	11	18	.31	70	.11	2	1.24	.01	.06	1	1	5
L15E 31+50W	1	5	6	35	.2	6	5	174	1.84	2	5	ND	2	24	1	2	2	35	.23	.034	11	14	.23	81	.10	2	.96	.01	.08	1	1	5
L15E 31+25W	1	6	12	60	.1	6	6	267	2.28	2	5	ND	2	23	1	2	2	40	.21	.066	10	17	.21	72	.10	2	1.28	.01	.08	1	1	5
L15E 31+00W	1	3	8	27	.1	4	3	127	1.23	2	5	ND	2	30	1	2	2	22	.24	.037	12	11	.19	82	.09	4	.90	.02	.08	1	1	5
L15E 30+75W	1	7	9	58	.1	10	7	347	2.38	5	5	ND	1	22	1	2	5	44	.20	.034	11	18	.26	80	.12	4	1.30	.01	.08	1	1	5
L15E 30+50W	1	8	11	51	.3	8	5	298	2.15	2	5	ND	4	17	1	2	2	36	.14	.067	13	14	.20	85	.08	3	1.67	.01	.13	2	3	10
L15E 30+25W	1	10	4	80	.1	16	9	271	3.25	3	5	ND	2	15	1	2	2	56	.12	.047	10	25	.34	107	.13	3	2.69	.01	.06	1	4	20
STD C/AU-S	21	61	40	132	7.7	70	31	1074	4.14	42	17	8	40	53	20	16	20	59	.48	.095	40	60	.96	183	.08	33	1.98	.08	.17	13	51	1400

MINGOLD RESOURCES PROJECT-620 FILE # 88-1752

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L15E 30+00N	1	7	9	84	.1	15	6	353	2.67	2	5	ND	6	22	1	2	2	44	.25	.078	13	21	.31	136	.09	2	2.29	.01	.07	1	1	20
L15E 29+75N	1	7	9	73	.1	15	6	266	2.75	2	5	ND	4	26	1	2	3	41	.24	.121	15	19	.33	148	.07	2	2.58	.01	.07	1	1	10
L15E 29+50N	1	11	5	99	.1	21	7	224	2.75	2	5	ND	3	22	1	2	2	41	.20	.067	12	20	.32	155	.06	2	2.89	.01	.06	1	1	10
L15E 29+25N	1	8	6	61	.3	14	6	206	2.79	2	5	ND	4	26	1	2	2	45	.21	.063	16	20	.29	132	.07	2	2.59	.01	.07	1	1	20
L15E 29+00N	1	8	8	102	.1	5	4	216	2.05	2	5	ND	6	18	1	2	2	31	.11	.052	16	13	.19	147	.08	2	2.31	.01	.06	1	1	20
L15E 28+75N	1	2	7	88	.1	12	5	298	2.13	2	5	ND	3	16	1	2	2	34	.17	.077	11	17	.22	62	.09	2	1.92	.01	.08	1	1	10
L16E 33+50N	1	4	6	43	.3	6	4	166	1.80	6	5	ND	3	19	1	2	2	32	.17	.023	12	11	.21	81	.07	3	1.13	.01	.05	1	2	5
L16E 33+25N	1	5	7	38	.2	8	3	167	1.80	2	5	ND	3	22	1	2	2	34	.23	.030	14	12	.21	78	.07	2	.98	.01	.05	1	1	5
L16E 33+00N	1	4	10	81	.1	13	7	367	2.69	4	5	ND	4	16	1	2	2	43	.16	.096	11	18	.21	96	.06	2	2.46	.01	.06	1	1	10
L16E 32+75N	1	5	5	48	.1	7	3	185	1.95	3	5	ND	3	18	1	2	2	35	.17	.030	12	18	.20	81	.07	2	1.18	.01	.07	1	1	5
L16E 32+50N	1	7	7	40	.2	6	3	184	1.67	3	5	ND	3	16	1	2	4	32	.21	.027	12	14	.32	56	.11	2	1.03	.01	.05	2	1	5
L16E 32+25N	1	5	6	47	.1	7	4	201	1.65	2	5	ND	2	21	1	2	2	29	.22	.024	13	15	.28	73	.09	2	1.28	.01	.06	1	16	5
L16E 32+00N	1	6	5	43	.1	7	4	178	1.70	2	5	ND	3	21	1	2	2	30	.23	.026	11	13	.28	74	.08	2	1.08	.01	.04	1	1	5
L16E 31+75N	1	5	5	60	.1	7	5	208	2.13	2	5	ND	3	22	1	3	2	37	.22	.034	13	16	.30	84	.09	5	1.28	.01	.06	1	1	5
L16E 31+50N	1	3	3	36	.1	4	3	143	1.26	2	5	ND	2	18	1	2	2	24	.16	.017	12	9	.14	65	.07	2	.76	.01	.05	1	1	5
L16E 31+25N	1	4	5	20	.1	6	3	144	1.26	5	5	ND	3	20	1	2	4	22	.18	.013	11	10	.23	61	.08	2	.80	.01	.08	1	1	10
L16E 31+00N	1	4	9	23	.2	5	2	106	1.18	4	5	ND	4	32	1	2	2	20	.24	.033	12	8	.16	109	.07	4	.88	.02	.09	1	1	5
L16E 30+75N	1	2	7	36	.1	6	3	182	1.78	2	5	ND	3	22	1	3	2	33	.20	.034	13	12	.20	73	.07	2	1.02	.01	.07	1	14	5
L16E 30+50N	1	3	6	35	.2	7	2	171	1.54	3	5	ND	4	28	1	2	4	25	.28	.046	15	10	.20	89	.07	2	1.03	.01	.09	1	1	5
L16E 30+25N	1	3	8	40	.1	10	5	184	2.35	2	5	ND	1	23	1	3	2	40	.26	.056	12	15	.23	115	.07	2	1.55	.01	.07	1	1	5
L16E 30+00N	1	4	8	45	.2	8	3	170	1.58	3	5	ND	4	22	1	3	3	27	.25	.027	12	15	.33	68	.10	2	1.05	.02	.07	1	1	5
L16E 29+75N	1	7	6	106	.1	8	6	235	2.27	3	5	ND	4	19	1	2	4	34	.25	.168	13	14	.19	102	.06	2	1.77	.01	.08	1	3	5
L16E 29+50N	2	10	11	156	.4	9	4	523	2.93	2	5	ND	5	46	1	2	2	41	.18	.108	16	17	.24	246	.09	2	3.03	.01	.14	1	1	20
L16E 29+00N	2	13	9	84	.1	15	7	262	3.70	2	5	ND	4	19	1	2	2	58	.12	.082	16	21	.27	130	.04	2	4.10	.01	.06	1	1	10
L16E 28+75N	1	6	6	38	.2	7	4	160	2.18	5	5	ND	3	16	1	2	2	40	.14	.043	12	16	.18	102	.07	2	1.46	.01	.05	1	1	5
L17E 33+50N	1	4	11	45	.1	9	4	330	1.79	6	5	ND	2	17	1	2	2	32	.18	.036	11	12	.19	63	.07	2	1.09	.01	.06	1	1	5
L17E 33+25N	1	4	7	44	.1	9	3	359	1.93	3	5	ND	2	19	1	2	2	35	.18	.035	11	14	.20	81	.07	2	1.23	.01	.07	1	1	10
L17E 33+00N	1	6	12	47	.1	9	5	180	2.25	3	5	ND	3	24	1	3	2	38	.24	.062	11	15	.18	87	.06	2	1.69	.01	.08	1	1	5
L17E 32+75N	1	4	5	33	.2	6	3	174	1.55	2	5	ND	3	22	1	2	3	26	.22	.035	13	10	.20	73	.07	2	1.00	.01	.07	1	1	5
L17E 32+50N	1	11	12	59	.1	12	5	538	2.48	2	5	ND	3	29	1	4	2	38	.28	.041	16	17	.32	110	.06	2	2.07	.01	.09	1	1	5
L17E 32+25N	1	4	4	35	.1	10	3	172	1.60	5	5	ND	2	22	1	3	2	28	.22	.033	12	11	.22	74	.07	2	1.02	.01	.05	1	1	10
L17E 32+00N	1	9	4	82	.1	11	7	199	2.48	4	5	ND	3	19	1	2	2	37	.19	.091	12	17	.20	111	.05	2	2.10	.01	.07	1	6	20
L17E 31+75N	1	8	7	44	.1	7	4	376	1.82	5	5	ND	2	27	1	2	2	31	.22	.026	14	12	.22	91	.06	2	1.25	.01	.07	2	1	5
L17E 31+50N	1	6	11	51	.1	9	5	300	2.23	6	5	ND	1	20	1	2	2	39	.18	.086	12	13	.17	85	.06	6	1.25	.01	.09	1	1	10
L17E 31+25N	1	15	8	59	.2	11	5	673	2.32	4	5	ND	2	43	1	2	2	32	.38	.043	25	14	.27	151	.04	2	1.98	.02	.14	1	1	20
L17E 31+00N	1	1	3	27	.1	4	1	129	1.34	6	5	ND	2	17	1	5	4	26	.15	.020	10	9	.13	61	.07	3	.75	.01	.07	1	2	5
STD C/AU-S	18	59	44	132	7.0	72	31	1082	4.18	44	14	8	38	49	18	18	18	59	.48	.086	41	59	.96	178	.07	33	1.99	.07	.15	13	18	1400

2" Grid

MINGOLD RESOURCES PROJECT-620 FILE # 88-1752

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L17E 30+75N	1	5	9	33	.2	6	3	120	1.24	3	5	ND	3	17	1	6	2	23	.18	.023	11	7	.15	70	.08	2	.81	.01	.08	2	2	20
L17E 30+50N	1	8	6	43	.2	6	2	133	1.55	2	5	ND	2	25	1	2	3	26	.23	.028	13	10	.20	81	.08	3	1.00	.02	.07	1	1	10
L17E 30+25N	1	15	14	81	.1	12	6	863	2.39	3	5	ND	1	38	1	2	3	40	.46	.031	37	16	.40	115	.06	2	1.65	.02	.07	1	1	10
L17E 30+00N	1	12	11	110	.2	13	5	311	2.43	2	5	ND	2	26	1	2	3	36	.22	.124	14	15	.25	94	.06	3	2.08	.01	.07	1	1	5
L17E 29+75N	1	8	11	86	.2	12	4	405	2.38	2	5	ND	2	31	1	3	4	36	.26	.122	13	14	.24	125	.06	2	1.87	.01	.10	1	1	10
L17E 29+50N	1	5	8	49	.1	6	3	343	1.83	2	5	ND	2	22	1	2	4	34	.23	.046	13	12	.18	86	.07	2	1.02	.01	.08	1	1	5
L17E 29+25N	1	6	8	44	.1	5	3	261	1.82	3	5	ND	1	22	1	2	2	34	.21	.046	12	12	.19	88	.07	4	1.12	.02	.06	1	1	5
L17E 29+00N	1	7	7	46	.1	7	3	173	1.73	2	5	ND	2	20	1	2	3	31	.18	.027	12	12	.20	83	.08	4	1.05	.01	.06	1	3	5
L17E 28+75N	1	7	7	50	.1	12	4	223	2.07	2	5	ND	2	19	1	2	2	37	.16	.034	11	15	.20	89	.07	2	1.68	.01	.05	2	1	5
L18E 33+50N	1	10	9	87	.1	12	7	407	3.09	3	5	ND	2	21	1	2	5	50	.23	.162	9	20	.25	91	.08	4	1.77	.01	.08	1	1	10
L18E 33+25N	1	9	6	62	.2	9	5	538	1.98	2	5	ND	1	21	1	2	3	31	.20	.100	12	12	.14	106	.06	2	1.10	.01	.10	1	1	20
L18E 33+00N	1	7	5	28	.3	5	3	142	1.32	2	5	ND	2	30	1	2	2	23	.26	.036	12	9	.19	92	.08	13	.86	.02	.07	1	1	5
L18E 32+50N	1	9	10	55	.1	8	4	242	2.18	2	5	ND	2	22	1	3	2	37	.20	.049	11	15	.26	88	.09	2	1.54	.01	.07	1	1	10
L18E 32+25N	1	8	8	65	.1	9	4	334	2.07	2	5	ND	1	21	1	2	4	34	.19	.067	11	14	.22	104	.07	3	1.48	.01	.06	1	2	20
L18E 32+00N	1	6	6	41	.1	4	2	176	1.47	2	5	ND	1	18	1	2	2	27	.17	.033	11	9	.12	67	.07	3	.92	.01	.05	1	2	10
L18E 31+50N	1	14	12	67	.3	9	8	1371	2.36	5	5	ND	3	46	1	4	2	43	.46	.064	18	14	.27	142	.07	15	1.30	.02	.11	1	1	50
L18E 31+25N	1	10	9	38	.1	7	5	485	2.03	2	5	ND	2	37	1	2	2	36	.31	.039	16	13	.26	116	.08	7	1.17	.02	.06	1	1	20
L18E 31+00N	1	15	9	43	.1	8	5	458	2.07	2	5	ND	4	42	1	2	2	34	.36	.044	18	13	.27	124	.07	5	1.20	.03	.07	1	2	30
L18E 30+75N	1	12	10	45	.1	6	4	289	2.04	2	5	ND	4	40	1	4	2	34	.34	.044	18	13	.29	119	.07	8	1.30	.03	.10	1	1	10
L18E 30+25N	1	8	11	56	.1	9	4	566	1.93	2	5	ND	1	25	1	2	2	32	.22	.039	14	11	.19	85	.07	5	1.27	.01	.06	1	1	5
L18E 30+00N	1	12	8	77	.1	8	5	1072	2.16	2	5	ND	1	32	1	2	2	34	.26	.063	28	14	.25	112	.06	9	1.67	.02	.07	1	1	5
L18E 29+75N	1	11	8	66	.2	8	3	351	1.93	2	5	ND	1	26	1	3	2	29	.22	.048	13	14	.21	86	.06	2	1.50	.01	.06	1	1	10
L18E 29+50N	1	9	4	36	.4	5	3	370	1.73	2	5	ND	3	25	1	3	2	30	.21	.036	13	11	.19	84	.07	7	1.18	.01	.07	1	1	5
L18E 29+25N	1	11	8	50	.1	10	4	297	2.02	2	5	ND	1	33	1	2	2	36	.26	.037	15	14	.21	103	.07	6	1.25	.02	.06	2	1	5
L18E 29+00N	1	7	8	41	.2	6	4	213	1.70	2	5	ND	2	21	1	4	4	30	.17	.026	12	12	.17	86	.08	4	1.21	.01	.04	1	1	5
L18E 28+75N	1	7	11	43	.1	10	3	171	2.14	4	5	ND	1	34	1	3	2	36	.24	.058	11	14	.18	131	.08	7	1.62	.01	.06	1	1	10
L36E 31+25N	1	7	11	60	.1	5	3	207	1.88	3	5	ND	2	20	1	3	3	32	.17	.032	10	11	.16	83	.07	2	1.11	.01	.07	1	2	5
L36E 31+00N	1	7	11	63	.1	7	4	161	2.05	5	5	ND	1	20	1	2	2	30	.20	.081	11	11	.16	88	.05	6	1.53	.01	.05	1	2	20
L36E 30+75N	1	6	13	82	.1	6	4	263	2.01	2	5	ND	2	15	1	2	2	32	.12	.061	11	11	.16	87	.06	5	1.41	.01	.07	1	1	20
L36E 30+50N	1	5	12	78	.2	5	4	134	1.48	2	5	ND	2	17	1	3	2	23	.14	.038	12	9	.16	80	.06	5	1.24	.01	.07	1	1	10
L36E 30+25N	1	8	15	66	.1	3	3	172	1.43	2	5	ND	1	30	1	3	2	20	.25	.022	31	11	.22	84	.05	4	1.33	.02	.06	1	1	30
L36E 30+00N	1	9	15	66	.2	6	4	408	2.01	2	5	ND	1	28	1	2	2	32	.30	.014	60	13	.19	69	.05	2	1.33	.01	.07	1	1	20
L36E 29+75N	1	7	9	99	.4	7	4	322	1.86	2	5	ND	3	26	1	4	2	35	.31	.044	13	12	.13	88	.07	2	.98	.01	.16	1	2	5
L36E 29+50N	1	6	11	92	.3	7	4	188	2.14	6	5	ND	2	15	1	6	3	33	.13	.037	11	12	.18	61	.05	7	1.33	.01	.08	1	1	10
L36E 29+25N	1	10	16	51	.3	7	4	198	2.08	2	5	ND	3	20	1	4	3	36	.23	.041	13	13	.21	76	.08	8	1.13	.01	.09	1	1	20
L36E 29+00N	1	7	7	64	.1	4	4	176	1.72	2	5	ND	1	23	1	2	2	29	.22	.012	13	11	.21	71	.07	2	1.00	.01	.06	1	1	10
STD C/AU-S	18	60	43	132	6.6	69	29	1045	4.07	39	14	7	37	47	18	16	25	57	.47	.083	39	58	.93	176	.07	34	1.95	.07	.13	13	49	1300

2" Grid

Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L36E 28+75N	1	5	10	85	.1	8	4	216	2.43	4	5	ND	2	25	1	2	2	39	.26	.028	11	14	.24	85	.07	2	1.36	.01	.10	1	42	10
L36E 28+50N	1	13	9	61	.2	10	6	219	2.68	2	5	ND	3	25	1	2	2	43	.30	.031	11	14	.28	80	.06	2	1.86	.01	.09	1	1	20
L36E 28+25N	1	6	9	89	.1	8	4	238	2.36	2	5	ND	1	18	1	2	2	35	.20	.096	13	12	.21	69	.05	5	1.46	.01	.09	2	3	20
L36E 28+00N	1	7	10	77	.2	7	4	396	2.40	3	5	ND	2	22	1	2	2	38	.22	.079	14	14	.22	110	.05	6	1.66	.01	.06	1	4	30
L36E 27+75N	1	7	11	113	.1	7	3	359	2.13	2	5	ND	1	19	1	2	2	31	.20	.064	13	13	.19	79	.05	2	1.58	.01	.06	1	1	5
L36E 27+50N	1	6	12	51	.1	7	3	177	1.70	4	5	ND	2	17	1	2	3	28	.21	.024	14	9	.21	80	.07	2	1.16	.01	.05	1	1	5
L36E 27+25N	1	9	16	91	.2	8	4	228	2.31	4	5	ND	3	18	1	2	2	33	.20	.035	13	12	.24	83	.06	2	2.16	.01	.08	1	1	20
L37E 31+25N	1	6	9	88	.1	7	3	156	2.33	2	5	ND	1	14	1	2	2	35	.10	.066	11	11	.16	73	.06	3	1.56	.01	.07	1	2	5
L37E 31+00N	1	5	11	46	.1	5	2	144	1.24	2	5	ND	1	27	1	2	2	22	.21	.010	15	9	.19	55	.08	5	.86	.02	.05	2	1	5
L37E 30+75N	1	10	4	51	.1	11	3	225	2.26	2	5	ND	2	45	1	2	3	36	.37	.055	18	15	.22	133	.07	4	1.71	.01	.07	1	1	5
L37E 30+50N	1	3	11	57	.2	5	3	139	1.45	2	5	ND	2	22	1	3	3	27	.15	.014	11	10	.12	57	.06	2	.76	.01	.07	3	1	5
L37E 30+25N	1	7	10	67	.2	6	3	169	1.76	2	5	ND	2	22	1	3	2	31	.16	.027	12	12	.16	71	.07	3	.90	.01	.08	2	2	5
L37E 30+00N	1	5	14	84	.3	5	4	336	2.04	2	6	ND	3	22	1	3	2	34	.18	.022	12	14	.20	53	.07	8	1.07	.01	.07	1	1	5
L37E 29+75N	1	10	13	71	.1	7	5	349	2.23	2	5	ND	1	20	1	2	2	39	.20	.022	12	17	.14	61	.07	3	1.13	.01	.05	1	1	5
L37E 29+50N	1	6	12	66	.3	7	4	446	2.06	4	5	ND	2	16	1	2	2	33	.23	.027	12	12	.21	65	.06	5	1.30	.01	.07	1	1	5
L37E 29+25N	1	7	15	66	.1	11	4	202	2.33	4	5	ND	1	16	1	2	2	37	.17	.049	12	19	.22	84	.06	5	1.76	.01	.05	1	1	5
L37E 29+00N	1	8	8	46	.1	8	4	202	2.32	4	5	ND	3	41	1	2	2	41	.17	.026	12	17	.22	118	.09	2	1.37	.01	.09	1	1	5
L37E 28+75N	1	8	8	93	.1	7	4	209	2.52	2	5	ND	2	22	1	2	2	38	.28	.085	13	15	.25	103	.05	2	1.98	.01	.07	1	1	5
L37E 28+50N	1	5	11	93	.1	6	5	597	2.16	2	5	ND	2	18	1	2	4	34	.26	.055	13	12	.19	112	.04	4	1.39	.01	.07	1	2	5
L37E 28+25N	1	4	12	85	.1	10	5	400	2.50	3	5	ND	3	21	1	2	2	38	.29	.028	14	13	.23	89	.06	2	2.23	.01	.08	1	1	5
L37E 28+00N	1	6	13	55	.1	7	4	156	1.90	2	5	ND	3	17	1	3	2	30	.13	.036	14	12	.18	96	.05	4	1.74	.01	.04	1	1	5
L37E 27+75N	1	5	9	57	.1	6	4	228	1.71	2	5	ND	3	16	1	2	2	28	.20	.031	13	10	.18	82	.05	5	1.51	.01	.06	2	1	5
L37E 27+50N	1	6	12	66	.1	7	3	325	2.23	5	5	ND	2	14	1	2	2	35	.16	.085	13	13	.18	90	.05	2	1.68	.01	.06	1	1	20
L37E 27+25N	1	7	10	100	.1	9	5	255	2.00	3	5	ND	2	13	1	4	2	29	.15	.061	12	13	.16	88	.04	3	2.16	.01	.06	1	1	10
L38E 31+25N	1	3	8	61	.1	4	2	224	1.49	3	5	ND	2	13	1	3	2	27	.10	.054	11	12	.07	65	.05	3	.78	.01	.05	1	2	10
L38E 30+75N	3	33	18	107	.2	13	7	1274	3.33	9	5	ND	3	104	1	2	3	41	.76	.041	85	17	.32	140	.03	2	2.73	.01	.09	1	1	30
L38E 30+50N	1	12	8	89	.3	7	4	1669	1.54	2	5	ND	1	28	1	2	2	26	.26	.026	15	12	.06	89	.05	2	.70	.01	.06	1	1	10
L38E 30+25N	1	7	9	80	.2	6	3	203	1.86	2	5	ND	2	17	1	2	2	31	.15	.057	12	16	.13	75	.06	2	1.04	.01	.05	1	1	5
L38E 30+00N	1	14	14	94	.2	6	3	396	2.20	2	5	ND	1	17	1	2	2	36	.23	.075	11	18	.16	61	.05	4	1.22	.01	.08	1	2	10
L38E 29+75N	1	5	12	52	.2	3	3	270	1.62	2	6	ND	2	19	1	2	3	27	.19	.040	13	11	.18	69	.06	7	1.04	.01	.06	1	1	5
L38E 29+50N	1	5	12	72	.2	5	4	244	1.58	2	5	ND	1	13	1	2	2	26	.13	.061	12	11	.14	58	.05	2	1.02	.01	.05	1	1	5
L38E 29+25N	1	8	12	62	.1	7	5	275	2.39	4	5	ND	2	25	1	2	3	35	.27	.057	14	13	.29	91	.05	2	1.54	.01	.09	1	1	5
L38E 29+00N	1	7	13	89	.4	3	3	322	1.64	2	5	ND	3	14	1	2	2	28	.17	.040	11	12	.31	72	.04	2	1.14	.01	.07	1	1	20
L38E 28+75N	1	9	13	107	.5	5	3	823	1.82	3	5	ND	3	18	1	2	5	27	.27	.136	11	12	.12	99	.04	3	1.24	.01	.09	1	1	30
L38E 28+50N	1	8	14	61	.2	6	3	444	2.06	2	5	ND	2	20	1	2	2	34	.23	.062	12	14	.19	77	.06	4	1.22	.01	.06	1	2	10
L38E 28+25N	1	4	13	79	.2	8	4	421	2.16	3	5	ND	2	24	1	2	2	31	.28	.086	13	13	.18	105	.04	3	1.43	.01	.09	1	1	20
STD C/AU-S	19	62	42	132	6.9	68	30	1099	4.25	40	18	8	38	49	19	16	20	59	.49	.091	41	60	.96	179	.07	34	2.00	.08	.14	13	47	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L38E 28+00W	1	7	5	62	.1	3	3	163	1.89	2	5	ND	1	17	1	2	2	30	.16	.060	12	11	.16	65	.05	5	1.13	.01	.05	1	12	20
L38E 27+75W	1	9	2	37	.2	5	3	161	1.81	2	5	ND	2	20	1	2	2	30	.17	.041	12	12	.17	71	.06	3	.93	.01	.05	2	7	10
L38E 27+50W	1	6	5	31	.1	1	2	129	1.58	2	5	ND	2	18	1	2	2	27	.18	.036	13	10	.16	53	.05	2	.94	.01	.03	1	4	5
L38E 27+25W	1	7	9	57	.1	2	3	289	1.50	2	5	ND	1	22	1	2	2	23	.21	.028	18	10	.18	70	.05	4	1.16	.01	.05	1	3	10
L39E 31+25W	1	5	12	63	.1	9	5	169	2.40	2	5	ND	3	17	1	3	2	35	.21	.068	10	15	.20	93	.05	2	1.85	.01	.06	1	5	20
L39E 31+00W	1	6	9	33	.1	1	2	100	1.09	2	5	ND	1	20	1	2	2	19	.14	.016	13	8	.14	57	.06	2	.72	.01	.05	2	4	10
L39E 30+75W	1	7	11	84	.1	6	3	210	2.23	2	5	ND	1	27	1	2	2	34	.24	.075	13	14	.23	63	.06	4	1.31	.01	.06	1	2	20
L39E 30+50W	1	8	11	92	.1	4	6	692	2.03	2	5	ND	1	25	1	2	5	31	.19	.077	15	11	.15	74	.05	2	1.31	.01	.05	1	1	10
L39E 30+25W	1	8	6	83	.2	11	7	608	2.11	2	5	ND	2	17	1	2	2	32	.14	.051	11	17	.22	71	.06	3	1.24	.01	.05	1	1	5
L39E 30+00W	1	4	7	57	.1	5	2	639	1.54	2	5	ND	2	15	1	2	2	27	.15	.038	12	10	.17	68	.07	2	.83	.01	.06	1	1	5
L39E 29+75W	1	8	14	83	.1	6	5	283	2.46	2	5	ND	3	16	1	3	2	38	.14	.165	12	14	.17	76	.04	5	1.54	.02	.05	1	3	20
L39E 29+50W	1	7	6	69	.3	5	4	259	1.78	2	6	ND	3	17	1	2	2	29	.17	.058	13	12	.18	74	.05	2	1.05	.01	.06	1	3	10
L39E 29+25W	1	5	9	98	.1	7	4	204	2.08	2	5	ND	3	17	1	2	2	31	.15	.092	11	32	.15	73	.05	3	1.31	.01	.05	1	2	10
L39E 29+00W	1	7	9	57	.2	5	4	364	2.03	3	5	ND	2	27	1	2	2	34	.17	.046	12	13	.17	86	.05	3	1.01	.01	.07	1	1	20
L39E 28+75W	1	7	9	106	.1	7	3	248	2.28	2	5	ND	2	31	1	2	2	38	.33	.120	10	18	.18	84	.06	3	1.38	.01	.06	1	3	5
L39E 28+50W	1	5	8	50	.1	10	4	228	1.76	2	5	ND	2	21	1	3	2	30	.29	.045	11	12	.14	57	.05	5	1.16	.01	.06	1	2	5
L39E 28+25W	1	6	11	63	.1	8	5	596	2.27	4	5	ND	3	30	1	2	2	37	.32	.067	18	15	.24	103	.07	2	1.16	.01	.09	1	1	5
L39E 28+00W	1	5	9	65	.1	9	5	417	2.21	2	5	ND	2	25	1	2	2	36	.28	.069	16	15	.22	93	.06	8	1.21	.01	.09	1	1	10
L39E 27+75W	1	5	8	43	.3	5	4	206	1.50	2	5	ND	3	21	1	3	2	21	.19	.022	21	9	.20	62	.04	4	1.11	.01	.07	1	1	5
L39E 27+50W	1	11	11	58	.1	8	5	469	2.14	4	5	ND	3	48	1	2	2	33	.40	.058	27	13	.26	104	.07	2	1.05	.02	.07	1	1	10
L39E 27+~~35~~25W	1	3	39	55	.1	7	4	232	2.28	2	5	ND	1	18	1	3	2	40	.18	.055	12	13	.19	68	.06	3	1.30	.01	.05	1	1	10
L40E 31+25W	1	4	13	73	.1	7	5	193	2.39	5	5	ND	2	19	1	3	2	38	.16	.074	12	15	.23	82	.07	2	1.31	.01	.06	1	1	5
L40E 31+00W	1	7	7	70	.3	9	4	349	1.88	2	5	ND	4	15	1	2	2	33	.10	.040	11	12	.11	55	.06	3	.93	.01	.07	1	1	5
L40E 30+75W	1	6	9	89	.3	8	5	249	2.25	2	5	ND	3	27	1	2	2	36	.31	.092	11	14	.19	71	.05	2	1.15	.01	.08	1	3	5
L40E 30+50W	1	5	13	102	.1	6	4	225	2.44	3	5	ND	4	26	1	2	2	36	.24	.102	14	14	.20	88	.06	6	1.67	.01	.07	1	1	5
L40E 30+25W	1	7	14	103	.2	11	5	390	2.56	3	5	ND	3	21	1	2	2	39	.18	.107	13	16	.24	95	.06	3	1.65	.01	.07	1	3	5
L40E 30+00W	1	9	11	102	.2	6	5	1430	2.04	2	5	ND	2	43	1	2	2	31	.34	.155	13	13	.09	138	.05	4	1.07	.01	.07	1	1	5
L40E 29+75W	1	6	8	156	.1	8	5	327	2.32	2	5	ND	4	36	1	2	2	36	.35	.164	12	14	.16	108	.05	6	1.41	.01	.07	1	2	5
L40E 29+50W	1	2	8	87	.1	5	3	180	1.62	2	5	ND	2	22	1	2	2	24	.19	.123	10	11	.13	83	.05	2	1.12	.01	.06	1	1	5
L40E 29+25W	1	7	11	47	.1	6	4	240	1.81	2	5	ND	2	27	1	2	2	32	.26	.039	12	12	.14	81	.05	2	.95	.01	.07	1	1	10
L40E 29+00W	1	5	7	74	.1	6	3	611	1.35	2	3	ND	1	16	1	3	2	26	.18	.041	11	13	.08	65	.05	2	.53	.01	.07	1	1	5
L40E 28+75W	1	5	11	51	.1	8	5	258	2.23	4	5	ND	3	21	1	2	2	39	.20	.037	13	16	.19	58	.07	2	1.08	.01	.08	1	1	5
L40E 28+50W	1	7	6	52	.1	9	4	209	1.99	2	3	ND	3	20	1	2	2	34	.17	.049	12	16	.16	71	.06	5	1.07	.01	.06	1	2	5
L40E 28+25W	1	7	9	61	.2	11	5	178	2.41	4	5	ND	3	16	1	2	3	39	.13	.069	11	15	.18	84	.06	5	1.36	.01	.06	1	2	10
L40E 28+00W	1	5	7	39	.1	3	3	154	1.21	2	7	ND	2	18	1	2	2	20	.17	.013	15	10	.15	52	.06	10	.82	.01	.06	1	1	5
L40E 27+75W	1	5	8	61	.1	8	4	445	1.68	2	5	ND	2	34	1	2	2	22	.32	.038	28	12	.24	97	.04	4	1.47	.01	.09	1	1	20
STD C/AU-S	18	61	41	132	6.9	71	30	1071	4.12	42	24	8	38	48	18	16	17	59	.48	.089	41	60	.95	178	.07	30	1.96	.07	.14	13	49	1300

"G" Grid

MINGOLD RESOURCES PROJECT-620 FILE # 88-1752

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L40E 27+50N	1	1	5	82	.1	5	4	586	1.86	2	5	ND	1	18	1	2	2	30	.23	.082	11	11	.13	65	.04	2	1.16	.02	.08	1	3	20
L40E 27+25N	1	2	9	69	.1	5	4	215	1.45	2	5	ND	1	24	1	2	2	26	.22	.031	12	10	.12	66	.05	2	.99	.01	.05	1	1	10
L67+50E 31+00N	1	6	8	121	.1	12	7	260	2.77	2	5	ND	2	18	1	2	2	45	.17	.060	12	16	.25	100	.08	7	1.90	.01	.05	1	1	40
L67+50E 30+75N	1	1	15	89	.1	5	4	204	1.91	2	5	ND	1	13	1	2	4	34	.14	.032	12	12	.19	72	.06	2	1.16	.01	.06	1	4	10
L67+50E 30+50N	1	2	6	124	.2	6	5	170	2.02	3	5	ND	2	13	1	2	3	32	.14	.052	12	13	.18	66	.06	2	1.44	.01	.06	1	1	30
L67+50E 30+25N	1	1	10	86	.2	5	4	304	1.70	2	5	ND	1	13	1	2	6	32	.15	.046	11	11	.13	55	.06	5	1.18	.01	.06	1	1	20
L67+50E 30+00N	1	1	9	103	.1	8	6	360	2.10	2	5	ND	2	13	1	2	2	35	.15	.041	12	14	.21	79	.07	2	1.71	.01	.06	1	1	30
L67+50E 29+75N	1	3	8	48	.1	10	6	232	2.46	4	5	ND	2	16	1	2	6	43	.16	.028	14	16	.26	92	.08	3	1.41	.01	.09	2	2	20
L67+50E 29+50N	1	6	11	90	.2	9	5	202	1.88	2	6	ND	3	12	1	2	2	31	.14	.023	12	11	.19	68	.07	2	1.38	.01	.05	1	1	30
L67+50E 29+25N	1	3	14	52	.1	6	4	227	1.68	2	5	ND	2	16	1	2	2	30	.16	.017	14	11	.25	67	.07	2	1.13	.01	.05	1	1	20
L67+50E 29+00N	3	5	46	70	.1	6	4	426	2.11	42	5	ND	3	22	1	6	2	22	.18	.041	28	8	.18	68	.04	2	1.01	.01	.08	1	1	120
L67+50E 28+75N	3	7	23	64	.1	5	5	566	2.07	13	5	ND	3	14	1	2	4	25	.17	.024	23	9	.20	56	.05	2	.89	.01	.08	1	2	20
L67+50E 28+50N	1	6	20	75	.2	6	5	408	2.15	5	5	ND	3	20	1	2	2	34	.21	.034	20	14	.24	87	.06	9	1.33	.01	.07	1	1	30
L68+50E 31+00N	1	1	11	59	.1	8	5	225	2.47	4	5	ND	1	17	1	2	2	45	.20	.026	12	17	.30	67	.10	2	1.39	.01	.08	1	1	20
L68+50E 30+75N	1	1	6	112	.1	7	5	179	2.07	5	5	ND	1	14	1	3	2	36	.14	.028	12	16	.21	58	.08	2	1.22	.01	.06	1	1	30
L68+50E 30+50N	1	2	13	77	.2	7	4	352	2.23	6	5	ND	3	10	1	2	2	35	.12	.065	14	15	.20	59	.06	6	1.67	.01	.06	1	1	20
L68+50E 30+25N	1	2	13	173	.1	7	6	413	2.21	2	5	ND	1	13	1	2	3	33	.12	.090	12	14	.22	85	.05	2	1.73	.01	.06	1	1	60
L68+50E 30+00N	1	4	16	93	.3	6	4	214	2.18	5	5	ND	2	10	1	2	2	33	.11	.070	15	14	.19	74	.05	2	1.50	.01	.05	1	1	30
L68+50E 29+75N	3	1	10	85	.6	3	4	368	1.44	2	5	ND	1	14	1	2	2	26	.15	.030	11	11	.12	68	.05	2	1.06	.01	.06	1	1	40
L68+50E 29+50N	39	3	28	26	.7	4	3	121	1.91	34	5	ND	6	25	1	3	2	21	.09	.025	33	7	.11	76	.04	5	.55	.01	.14	1	2	10
L68+50E 29+25N	4	7	15	46	.1	6	5	351	2.22	11	6	ND	4	25	1	3	2	35	.23	.034	27	14	.22	62	.08	2	.94	.02	.08	2	3	30
L68+50E 29+00N	2	6	15	43	.1	6	4	233	2.15	13	5	ND	3	20	1	2	2	35	.19	.033	16	14	.20	62	.09	3	.94	.01	.06	2	2	20
L68+50E 28+75N	2	1	13	71	.2	5	5	497	2.05	5	5	ND	1	21	1	2	2	35	.20	.056	13	14	.20	94	.06	2	1.31	.01	.06	1	1	30
L69+50E 31+00N	2	5	10	92	.1	10	6	221	2.93	13	5	ND	1	16	1	2	2	43	.17	.092	16	16	.28	82	.05	2	1.96	.01	.08	1	5	20
L69+50E 30+75N	1	1	12	52	.1	2	3	221	1.57	4	5	ND	3	15	1	2	2	28	.16	.034	14	11	.18	59	.07	2	.93	.01	.06	1	4	20
L69+50E 30+50N	1	2	12	49	.3	2	4	226	1.36	2	5	ND	1	19	1	2	2	25	.19	.031	13	9	.13	56	.06	2	.88	.01	.07	2	1	10
L69+50E 30+25N	1	3	12	48	.2	5	3	178	1.82	7	5	ND	2	16	1	2	2	31	.18	.057	13	12	.19	65	.07	4	1.17	.01	.06	1	1	20
L69+50E 30+00N	2	4	13	44	.1	7	5	344	1.81	4	5	ND	2	23	1	2	2	32	.27	.048	18	12	.21	80	.07	2	.95	.01	.07	2	1	30
L69+50E 29+75N	3	4	13	40	.2	3	3	239	1.34	2	6	ND	3	14	1	2	2	21	.16	.035	18	8	.13	59	.04	2	.89	.01	.07	1	1	20
L69+50E 29+50N	3	2	14	41	.1	3	3	249	1.74	6	5	ND	2	19	1	2	3	30	.20	.040	17	11	.18	65	.07	6	.65	.01	.08	1	1	30
L69+50E 29+25N	1	3	13	38	.1	5	4	283	2.01	7	5	ND	4	24	1	2	2	34	.24	.037	24	14	.21	61	.08	7	.81	.01	.06	1	1	10
STD C/AU-S	19	62	38	132	7.1	70	30	1099	4.23	44	21	9	40	50	19	16	23	61	.49	.091	40	60	.96	180	.07	33	1.97	.08	.15	15	50	1300

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: MAY 30 1988 DATE REPORT MAILED: *June 7/88* ASSAYER [illegible] D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT-620 File # 88-1652 Page 1

"A" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
0+00E 25+00N	1	4	11	112	.1	9	7	2206	1.95	2	5	ND	2	23	1	3	2	34	.23	.136	12	14	.13	179	.07	2	1.56	.01	.07	1	1	50
0+00E 24+75N	1	3	5	137	.1	7	5	1046	1.61	2	5	ND	2	46	1	5	2	25	.32	.137	16	10	.17	149	.07	4	1.73	.01	.07	1	1	30
0+00E 24+50N	1	6	7	87	.2	9	4	1111	1.61	2	5	ND	2	22	1	2	2	28	.18	.040	14	11	.16	144	.07	2	1.63	.01	.05	2	1	20
0+00E 24+25N	1	4	2	70	.1	7	4	887	1.48	2	5	ND	2	23	1	2	2	26	.19	.030	13	13	.15	149	.07	5	1.28	.01	.08	1	1	10
0+00E 24+00N	1	2	5	99	.1	9	5	1010	1.51	2	5	ND	2	20	1	4	2	26	.19	.045	13	11	.15	155	.07	2	1.32	.01	.06	1	1	5
0+00E 23+75N	1	5	6	161	.1	9	5	1746	1.99	2	5	ND	2	26	1	2	2	33	.22	.057	14	13	.19	173	.07	4	2.02	.01	.06	1	2	20
0+00E 23+50N	1	9	7	122	.1	11	5	1785	2.10	2	5	ND	2	32	1	2	2	38	.26	.052	15	15	.19	198	.07	2	1.90	.01	.06	1	1	20
0+00E 23+25N	1	6	2	105	.1	11	5	1012	1.70	2	5	ND	2	26	1	3	2	29	.20	.039	12	14	.18	132	.06	2	1.45	.01	.06	1	1	10
0+00E 23+00N	1	4	12	96	.1	13	6	1010	1.95	2	5	ND	2	22	1	2	2	34	.18	.053	13	16	.18	153	.07	2	1.43	.01	.07	1	1	5
0+00E 22+75N	1	4	4	80	.1	11	6	948	1.70	2	5	ND	2	22	1	2	2	32	.21	.051	11	17	.16	128	.08	4	1.15	.01	.07	1	2	10
0+00E 22+50N	1	8	6	68	.1	12	6	699	2.16	2	5	ND	2	25	1	3	3	42	.23	.025	13	21	.22	113	.10	2	1.53	.01	.06	1	1	20
0+00E 22+25N	1	5	8	134	.1	13	7	1335	2.14	2	5	ND	2	32	1	2	2	37	.36	.128	10	19	.21	179	.10	2	1.28	.01	.07	1	1	20
0+00E 22+00N	1	10	2	64	.1	14	6	466	2.34	2	5	ND	3	28	1	3	2	44	.23	.047	13	22	.25	110	.11	7	1.36	.01	.07	1	1	10
0+00E 21+75N	1	5	7	72	.1	13	6	923	1.95	2	5	ND	2	28	1	2	4	38	.25	.029	13	16	.19	139	.10	4	1.13	.01	.08	1	1	5
0+00E 21+50N	1	9	2	49	.1	12	7	493	2.22	2	5	ND	4	32	1	2	2	42	.29	.023	18	17	.21	113	.09	6	1.00	.01	.16	1	8	10
0+00E 21+25N	1	11	7	67	.1	9	6	1196	2.19	2	5	ND	1	57	1	2	2	33	.65	.150	18	37	.19	197	.06	4	1.14	.01	.22	1	1	10
0+00E 21+00N	1	7	9	63	.2	7	3	493	1.60	2	5	ND	1	27	1	2	3	26	.32	.098	12	13	.14	124	.07	2	.87	.01	.19	1	1	5
0+00E 20+75N	1	5	5	105	.2	11	5	686	1.89	2	5	ND	3	23	1	3	2	32	.27	.091	12	15	.17	137	.06	7	1.09	.01	.07	1	1	10
0+00E 20+50N	1	4	6	97	.1	10	6	572	1.98	2	5	ND	2	18	1	2	2	35	.20	.066	12	15	.16	107	.06	2	1.27	.01	.04	1	1	5
0+00E 20+25N	1	6	4	83	.1	11	5	591	2.01	3	5	ND	3	13	1	3	2	34	.15	.042	12	15	.19	88	.07	5	1.82	.01	.06	1	1	5
0+00E 20+00N	1	6	10	74	.1	9	4	334	1.74	2	5	ND	2	18	1	2	2	28	.16	.076	11	13	.14	96	.06	2	1.33	.01	.06	1	2	5
0+00E 19+75N	1	3	6	59	.2	11	4	714	1.50	2	5	ND	3	15	1	2	2	27	.14	.049	12	13	.12	104	.06	2	1.02	.01	.04	1	1	5
0+00E 19+50N	1	5	9	75	.1	7	4	379	1.43	2	5	ND	1	18	1	2	2	26	.17	.020	11	12	.13	105	.06	2	1.20	.01	.04	1	1	5
0+00E 19+25N	1	2	6	80	.1	5	4	1290	1.39	2	5	ND	2	19	1	2	2	26	.19	.049	13	12	.13	151	.07	7	.97	.01	.07	1	1	5
0+00E 19+00N	1	4	7	69	.1	10	4	673	1.54	2	5	ND	1	18	1	2	2	29	.19	.036	12	15	.15	119	.08	7	1.08	.01	.06	1	1	5
0+00E 18+75N	1	4	6	48	.2	10	4	388	1.58	2	5	ND	2	17	1	2	4	29	.18	.051	12	13	.13	99	.08	4	1.03	.01	.06	2	1	5
0+00E 18+50N	1	7	6	39	.1	6	3	289	1.41	2	5	ND	2	23	1	2	3	26	.19	.027	13	12	.13	71	.08	2	.86	.01	.07	1	1	5
0+00E 18+25N	1	9	6	38	.1	9	6	181	2.11	2	5	ND	1	17	1	2	2	40	.16	.036	11	18	.17	97	.08	2	1.21	.01	.04	1	2	5
0+00E 18+00N	1	3	5	62	.1	10	3	353	1.66	2	5	ND	1	14	1	2	3	29	.17	.070	11	15	.14	96	.07	2	1.20	.01	.06	1	1	5
0+00E 17+75N	1	3	6	68	.1	8	4	939	1.65	2	5	ND	1	19	1	2	2	29	.20	.094	11	12	.11	127	.06	3	1.00	.01	.08	1	1	20
0+00E 17+50N	1	4	4	69	.1	10	5	456	1.75	2	5	ND	2	26	1	2	2	29	.25	.111	12	15	.18	126	.06	2	1.19	.01	.08	1	1	10
1+00E 21+00N	2	55	19	94	.3	34	8	2095	3.39	10	5	ND	1	76	1	2	2	43	.80	.066	85	26	.53	269	.03	2	3.39	.02	.17	1	1	40
1+00E 20+75N	1	26	12	260	.1	15	8	1512	2.62	2	5	ND	1	82	1	2	2	32	.93	.175	32	19	.29	292	.03	2	2.21	.01	.17	1	2	30
1+00E 20+50N	1	5	7	120	.2	4	4	686	1.72	2	5	ND	1	23	1	2	2	29	.22	.097	13	14	.13	133	.06	2	.93	.01	.08	1	1	5
1+00E 20+25N	1	4	10	75	.1	8	4	439	1.63	2	5	ND	1	22	1	3	2	28	.21	.055	17	12	.17	89	.06	2	.97	.01	.06	1	1	10
1+00E 20+00N	3	28	10	76	.1	19	7	968	3.08	14	12	ND	1	64	1	2	3	43	.72	.078	58	24	.38	165	.03	6	2.62	.01	.17	1	1	60
STD C/AU-S	19	62	40	132	7.3	68	30	1073	4.10	42	18	8	39	51	19	17	23	60	.47	.091	41	61	.97	180	.07	31	1.97	.07	.14	13	50	1300

"A" Grid

F" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
1+00E 19+75W	1	39	9	93	.2	33	8	929	3.59	11	16	ND	2	75	1	2	2	43	1.06	.093	65	30	.53	209	.03	2	3.37	.02	.28	1	1	50
1+00E 19+50W	1	7	10	63	.1	8	5	451	1.82	2	5	ND	2	25	1	3	2	32	.27	.064	14	17	.19	92	.08	8	.86	.01	.07	1	1	5
1+00E 19+25W	1	4	13	76	.1	8	5	529	1.85	2	5	ND	2	18	1	2	4	34	.19	.089	12	17	.35	107	.06	2	.93	.01	.06	1	1	5
1+00E 19+00W	1	4	9	90	.2	9	6	703	1.65	2	5	ND	2	19	1	2	2	29	.18	.107	12	14	.10	128	.06	2	1.15	.01	.06	1	2	5
1+00E 18+75W	1	12	10	42	.1	12	6	289	2.32	3	5	ND	4	35	1	2	2	45	.32	.046	20	25	.22	91	.10	2	.93	.02	.07	1	1	30
1+00E 18+50W	1	5	7	46	.1	7	5	334	1.89	3	5	ND	3	19	1	2	3	34	.20	.061	13	16	.16	74	.07	3	1.14	.01	.07	2	1	20
1+00E 18+25W	1	6	8	82	.2	5	3	212	1.41	2	5	ND	5	16	1	2	4	24	.21	.076	21	12	.12	51	.06	2	1.09	.01	.09	1	3	20
1+00E 18+00W	1	5	9	61	.1	7	3	299	1.64	2	5	ND	3	20	1	2	3	31	.20	.037	14	13	.17	63	.08	2	1.14	.01	.07	1	1	20
1+00E 17+75W	1	5	8	80	.1	8	5	761	1.81	2	5	ND	1	25	1	2	4	30	.23	.082	13	17	.16	105	.06	2	1.40	.01	.09	1	1	10
1+00E 17+50W	1	12	16	75	.2	16	7	506	2.70	2	5	ND	3	44	1	2	2	42	.40	.043	22	20	.36	117	.06	2	2.12	.01	.13	1	1	30
L40E 43+00W	1	3	4	39	.1	8	3	164	1.54	5	5	ND	2	24	1	3	2	28	.20	.027	16	5	.21	81	.07	2	1.01	.01	.06	2	1	20
L40E 42+75W	1	6	7	47	.2	8	5	228	1.07	6	5	ND	3	25	1	2	2	33	.22	.026	16	13	.26	72	.08	2	1.06	.01	.07	2	2	20
L40E 42+50W	1	10	7	92	.2	12	7	370	2.27	8	5	ND	3	27	1	2	2	36	.24	.060	18	15	.25	95	.07	2	1.50	.01	.07	1	1	30
L40E 42+25W	1	8	14	112	.3	8	7	471	2.47	5	5	ND	2	22	1	2	6	44	.15	.063	14	21	.20	98	.10	2	1.19	.01	.06	1	5	10
L40E 42+00W	1	6	9	97	.1	13	5	426	2.30	4	5	ND	1	26	1	2	2	38	.27	.065	18	21	.26	93	.07	2	1.30	.01	.07	1	1	40
L40E 41+75W	1	11	11	96	.1	15	9	917	2.20	6	5	ND	2	29	1	2	2	36	.24	.038	21	20	.21	98	.08	2	1.23	.01	.07	1	1	10
L40E 41+50W	1	4	7	91	.1	8	5	284	1.93	3	5	ND	3	26	1	2	6	36	.24	.030	17	13	.21	92	.08	2	1.22	.01	.06	1	2	20
L40E 41+25W	2	9	16	96	.1	7	10	1385	2.50	6	5	ND	2	24	1	2	2	42	.27	.040	22	16	.15	147	.06	3	1.65	.01	.06	1	3	10
L40E 41+00W	2	8	14	108	.2	8	6	885	2.64	30	5	ND	1	21	1	2	2	47	.29	.033	13	15	.20	78	.05	6	1.26	.01	.07	1	1	10
L40E 40+25W	2	11	13	83	.1	6	8	933	2.75	24	5	ND	1	20	1	2	2	37	.35	.057	15	10	.23	138	.01	2	1.77	.01	.15	1	1	20
L40E 40+00W	1	6	13	85	.3	15	7	560	2.35	4	5	ND	3	15	1	2	2	40	.37	.048	12	23	.19	91	.09	2	1.68	.01	.06	1	1	10
L40E 39+75W	1	5	6	87	.1	13	6	419	2.43	4	5	ND	3	22	1	2	6	41	.31	.043	14	20	.24	117	.08	2	1.84	.01	.07	1	1	5
L40E 39+50W	1	9	12	93	.2	9	6	540	2.22	4	5	ND	2	24	1	2	5	36	.26	.079	13	15	.22	99	.07	9	1.41	.01	.08	1	1	5
L40E 39+25W	1	5	9	88	.2	8	4	209	1.79	2	5	ND	2	19	1	2	2	31	.20	.048	11	12	.15	59	.06	2	1.25	.01	.07	1	1	10
L40E 39+00W	1	6	9	70	.3	10	5	578	1.87	3	5	ND	3	26	1	4	4	31	.27	.042	15	13	.22	130	.06	5	1.37	.01	.10	1	1	10
L41E 43+00W	1	6	7	74	.1	10	7	315	2.58	6	5	ND	3	24	1	2	3	50	.24	.041	15	23	.28	79	.12	2	1.11	.01	.05	1	1	5
L41E 42+75W	1	14	8	65	.1	8	6	447	2.15	9	5	ND	1	31	1	2	2	33	.27	.034	24	15	.27	98	.05	2	1.53	.02	.06	1	1	10
L41E 42+50W	1	9	4	47	.1	8	5	206	1.85	5	5	ND	2	25	1	2	5	32	.23	.039	18	15	.24	86	.07	10	1.08	.02	.08	1	1	20
L41E 42+25W	1	11	5	58	.1	11	6	311	1.99	5	5	ND	1	25	1	2	4	29	.19	.054	28	17	.20	94	.05	2	1.38	.01	.05	1	1	30
L41E 42+00W	1	12	9	90	.3	10	6	419	2.31	9	5	ND	1	34	1	2	4	33	.34	.063	22	15	.23	99	.04	2	1.70	.01	.10	1	1	20
L41E 41+75W	1	8	10	58	.1	5	3	210	1.73	3	5	ND	2	21	1	2	2	32	.16	.028	13	12	.15	66	.07	2	.93	.01	.05	1	1	10
L41E 41+50W	1	7	9	80	.1	7	5	271	2.16	10	5	ND	2	15	1	2	2	35	.14	.036	13	14	.21	62	.06	2	1.22	.01	.05	1	1	10
L41E 41+25W	1	9	13	78	.1	11	6	251	2.48	18	5	ND	2	23	1	2	2	38	.18	.046	16	15	.29	85	.06	5	1.53	.01	.07	1	1	30
L41E 41+00W	1	8	7	65	.1	6	5	200	2.16	13	5	ND	3	24	1	2	2	39	.21	.043	12	14	.18	84	.06	8	1.18	.01	.05	1	1	10
L41E 40+75W	1	6	6	100	.1	5	4	315	1.48	2	5	ND	1	19	1	2	2	28	.20	.025	12	14	.12	63	.07	2	.79	.01	.08	1	1	5
L41E 40+50W	1	9	10	81	.2	10	6	369	2.22	12	5	ND	1	28	1	2	5	38	.28	.063	16	16	.24	91	.06	6	1.22	.01	.08	1	1	10
STD C/AU-S	19	63	45	132	7.2	71	29	1068	4.06	41	20	8	40	51	20	16	23	60	.47	.091	41	61	.97	180	.07	33	1.94	.07	.14	12	53	1300

MINGOLD RESOURCES PROJECT-620 FILE # 88-1652

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L41E 40+25W	1	9	9	141	.1	25	10	356	3.57	13	5	ND	4	44	1	2	2	55	.48	.132	12	26	.34	169	.10	5	2.61	.01	.15	1	1	20
L41E 40+00W	1	7	12	122	.1	14	9	306	2.94	2	5	ND	2	30	1	2	2	46	.26	.138	13	23	.23	94	.10	2	1.69	.01	.08	1	1	10
L41E 39+75W	1	3	14	170	.1	1	5	379	2.28	2	5	ND	1	15	1	2	2	33	.14	.103	13	16	.11	76	.06	9	1.89	.01	.07	1	1	20
L41E 39+50W	1	6	11	58	.1	10	6	204	2.19	3	5	ND	1	19	1	2	2	39	.18	.036	13	14	.21	88	.08	2	1.41	.01	.03	1	9	10
L41E 39+25W	2	8	6	99	.1	15	8	327	3.23	8	5	ND	1	22	1	2	2	48	.23	.131	12	18	.26	125	.05	5	2.55	.01	.08	1	1	10
L41E 39+00W	1	4	4	53	.1	8	4	290	1.77	2	5	ND	2	20	1	2	2	31	.16	.031	13	12	.13	62	.07	6	1.20	.01	.07	1	1	5
L42E 43+00W	1	7	12	54	.1	4	6	423	1.95	7	5	ND	1	28	1	2	2	34	.24	.034	16	14	.20	80	.07	5	1.10	.01	.07	1	1	10
L42E 42+75W	1	1	5	44	.1	3	2	150	1.51	2	5	ND	1	16	1	3	6	31	.14	.018	13	11	.08	48	.07	2	.57	.01	.06	1	1	5
L42E 42+50W	1	7	7	57	.1	5	4	351	1.69	4	5	ND	1	17	1	2	2	32	.11	.026	15	14	.10	61	.07	3	.78	.01	.06	1	1	5
L42E 42+25W	1	3	8	52	.1	4	3	276	1.43	2	5	ND	1	20	1	2	5	26	.15	.016	16	12	.12	65	.07	2	.80	.01	.08	1	1	5
L42E 42+00W	1	4	8	50	.1	6	3	196	1.74	2	5	ND	1	19	1	3	3	33	.17	.032	11	16	.14	62	.09	2	.72	.01	.07	1	1	5
L42E 41+75W	1	8	11	76	.1	11	4	213	2.19	8	5	ND	2	17	1	2	2	36	.15	.055	14	18	.19	78	.07	6	1.28	.01	.07	1	1	5
L42E 41+50W	1	8	10	62	.1	8	4	262	2.06	9	5	ND	1	17	1	2	3	37	.14	.034	13	13	.15	58	.07	5	1.13	.01	.06	1	1	5
L42E 41+25W	1	6	12	88	.1	9	7	926	2.12	2	5	ND	2	27	1	2	3	37	.24	.071	13	14	.14	97	.07	5	1.01	.01	.06	1	1	10
L42E 41+00W	1	6	13	120	.2	9	6	321	2.40	2	5	ND	1	39	1	2	2	38	.40	.127	13	16	.18	118	.07	2	1.32	.01	.09	1	48	10
L42E 40+75W	1	9	12	49	.1	8	4	219	2.16	23	5	ND	3	28	1	2	2	36	.27	.045	17	15	.22	89	.08	8	1.19	.01	.10	1	3	20
L42E 40+50W	1	5	10	61	.1	10	5	320	2.02	3	5	ND	1	24	1	2	2	35	.21	.025	13	14	.21	99	.08	3	1.19	.01	.08	1	1	10
L42E 40+25W	1	8	3	51	.1	10	4	223	1.99	2	5	ND	1	27	1	2	2	36	.24	.031	18	16	.22	85	.08	10	1.16	.01	.06	1	1	20
L42E 40+00W	1	4	5	51	.1	8	4	282	1.70	2	5	ND	1	25	1	2	2	29	.22	.022	18	13	.21	74	.07	8	1.12	.02	.07	1	2	10
L42E 39+75W	1	7	7	53	.1	9	4	198	2.00	3	5	ND	3	30	1	2	2	33	.31	.062	18	16	.22	97	.08	2	1.25	.02	.08	1	1	20
L42E 39+50W	1	3	9	46	.1	8	3	210	1.78	2	5	ND	3	23	1	4	2	32	.20	.026	15	12	.18	72	.09	12	1.16	.02	.07	2	1	10
L42E 39+25W	1	8	7	42	.1	7	3	198	1.72	4	5	ND	3	25	1	2	6	29	.22	.030	15	11	.18	75	.08	8	1.14	.02	.07	1	1	20
L42E 39+00W	1	5	9	42	.1	8	4	187	1.68	4	5	ND	3	23	1	2	2	31	.21	.028	14	12	.18	78	.09	10	1.02	.02	.06	2	1	5
L43E 43+00W	1	6	11	113	.1	10	5	430	2.23	6	5	ND	3	16	1	2	2	35	.13	.155	12	13	.14	74	.06	8	1.61	.01	.08	1	1	10
L43E 42+75W	1	7	9	91	.1	7	5	415	2.07	3	5	ND	3	14	1	2	2	35	.12	.071	13	14	.11	71	.06	2	1.18	.01	.07	1	1	5
L43E 42+50W	1	8	13	99	.2	6	5	1202	2.77	7	5	ND	3	21	1	2	6	42	.18	.265	13	17	.16	124	.07	6	1.61	.01	.07	1	6	5
L43E 42+25W	1	7	10	79	.2	5	3	222	2.20	7	5	ND	2	18	1	2	2	38	.16	.107	12	14	.12	78	.05	2	1.19	.01	.08	1	15	20
L43E 42+00W	1	5	8	135	.1	7	5	250	2.46	7	5	ND	3	21	1	2	2	38	.16	.143	12	18	.17	91	.07	4	1.17	.01	.06	2	1	10
L43E 41+75W	1	5	7	121	.1	4	5	606	1.97	2	5	ND	2	13	1	2	2	36	.14	.051	12	21	.12	69	.09	2	.79	.01	.08	1	1	10
L43E 41+50W	1	10	7	63	.1	9	6	473	2.07	6	5	ND	2	31	1	2	3	33	.27	.057	31	12	.19	93	.06	2	1.36	.01	.08	1	1	20
L43E 41+25W	1	9	8	72	.1	8	4	229	1.88	2	5	ND	1	22	1	2	2	30	.18	.030	20	12	.21	72	.09	2	1.02	.01	.10	1	1	5
L43E 41+00W	1	6	2	81	.1	9	6	292	2.55	14	5	ND	3	22	1	3	2	42	.20	.038	14	17	.18	72	.07	2	1.50	.01	.08	1	1	20
L43E 40+75W	1	5	5	95	.1	8	5	251	2.23	3	5	ND	2	25	1	2	2	39	.20	.117	13	16	.14	99	.07	2	1.46	.01	.10	1	1	10
L43E 40+50W	1	9	12	58	.1	7	4	264	2.07	5	5	ND	2	28	1	2	2	32	.24	.026	22	16	.25	82	.08	2	1.43	.01	.09	2	1	10
L43E 40+25W	1	7	5	66	.1	5	3	230	1.81	2	5	ND	2	22	1	2	2	32	.21	.029	15	13	.17	68	.08	7	1.10	.01	.09	1	1	5
L43E 40+00W	1	13	6	73	.1	10	5	505	2.36	4	5	ND	2	30	1	2	2	37	.25	.045	28	16	.25	98	.05	3	2.03	.01	.09	1	1	20
STD C/AU-S	20	63	40	132	7.4	73	31	1085	4.18	40	23	8	39	52	20	17	20	61	.48	.094	42	61	.90	181	.07	34	2.08	.08	.16	13	47	1300

MINGOLD RESOURCES PROJECT-620 FILE # 88-1652

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L43E 39+75N	1	9	7	81	.2	8	6	282	2.35	4	5	ND	3	24	1	2	2	38	.18	.074	14	15	.22	93	.09	4	1.95	.01	.10	1	1	10
L43E 39+50N	1	6	11	33	.1	4	4	151	1.43	3	5	ND	2	23	1	2	5	24	.18	.018	14	12	.19	69	.06	2	1.01	.02	.07	1	1	20
L43E 39+25N	1	4	8	38	.1	1	3	159	1.36	2	5	ND	2	21	1	2	3	25	.17	.010	13	12	.17	65	.08	2	.89	.01	.05	2	4	5
L43E 39+00N	1	7	8	46	.2	6	4	226	1.51	4	5	ND	2	18	1	2	2	27	.15	.038	13	13	.15	68	.07	2	1.01	.01	.07	1	1	10
L43E 38+75N	1	10	5	59	.1	8	5	549	2.08	3	5	ND	1	32	1	2	3	33	.26	.033	20	16	.20	103	.06	2	1.55	.01	.07	1	1	5
L43E 38+50N	1	7	3	45	.2	9	5	185	2.11	3	5	ND	1	20	1	2	2	37	.18	.044	13	18	.17	84	.09	26	1.41	.02	.06	2	1	5
L43E 38+25N	1	7	7	50	.2	6	5	214	1.82	2	5	ND	2	23	1	2	2	32	.20	.026	13	15	.17	77	.08	2	1.18	.01	.05	1	1	5
L43E 38+00N	1	7	10	41	.1	6	5	234	1.77	2	5	ND	1	26	1	2	2	32	.22	.031	17	18	.19	86	.09	2	1.09	.01	.07	1	1	5
L43E 37+75N	1	8	10	66	.1	7	6	341	2.20	2	5	ND	2	27	1	3	2	41	.25	.030	15	22	.25	87	.14	7	1.32	.02	.08	1	1	5
L43E 37+50N	1	8	6	43	.1	8	5	221	1.65	2	5	ND	2	25	1	2	3	30	.22	.026	16	13	.18	70	.09	2	1.00	.01	.06	2	1	5
L43E 37+25N	1	9	9	98	.1	11	10	1306	2.42	5	5	ND	1	33	1	2	2	40	.29	.058	21	17	.25	110	.07	2	1.93	.01	.07	1	1	10
L43E 37+00N	2	11	11	147	.5	13	6	316	2.96	13	5	ND	3	18	1	2	2	48	.19	.075	18	20	.28	53	.09	2	1.06	.01	.08	1	1	18
L44E 41+75N	1	7	9	61	.1	3	3	197	2.16	9	5	ND	2	16	1	3	2	36	.16	.069	12	14	.15	87	.07	2	1.13	.01	.09	1	1	5
L44E 41+50N	1	8	9	62	.2	8	6	316	1.73	3	5	ND	2	20	1	2	2	29	.19	.044	15	12	.18	78	.07	2	1.02	.01	.07	1	1	5
L44E 41+25N	1	7	3	82	.1	3	2	375	1.89	3	5	ND	2	15	1	2	2	34	.13	.072	12	16	.09	89	.08	2	1.01	.01	.07	1	1	10
L44E 41+00N	1	15	7	83	.3	8	6	617	2.14	9	5	ND	1	55	1	2	5	29	.53	.062	75	13	.22	141	.05	2	1.58	.01	.11	1	1	20
L44E 40+75N	1	9	9	47	.2	8	6	235	2.34	17	5	ND	3	24	1	2	2	40	.23	.079	15	16	.22	86	.08	2	1.17	.02	.09	2	2	5
L44E 40+50N	1	19	3	83	.3	11	8	1080	2.41	11	5	ND	1	50	1	2	2	32	.41	.070	39	15	.29	137	.03	2	2.01	.01	.10	1	1	50
L44E 40+25N	1	7	12	54	.3	9	3	410	1.98	9	5	ND	2	26	1	2	2	34	.25	.063	12	13	.18	79	.07	2	1.08	.01	.06	1	1	5
L44E 40+00N	1	4	9	50	.1	2	5	332	1.59	5	5	ND	2	20	1	2	2	29	.16	.033	14	12	.14	69	.07	2	.91	.01	.06	1	1	5
L44E 39+75N	1	6	2	30	.1	1	2	144	1.10	2	5	ND	2	16	1	2	2	23	.15	.019	11	10	.06	47	.07	2	.50	.01	.07	1	2	5
L44E 39+50N	1	4	3	36	.1	1	2	313	1.48	2	5	ND	1	17	1	3	2	27	.16	.041	12	13	.13	69	.08	2	.84	.01	.07	2	1	5
L44E 39+25N	1	7	8	45	.2	8	4	229	1.58	3	5	ND	1	29	1	2	2	25	.23	.025	15	11	.20	83	.08	5	1.15	.02	.07	2	1	5
L44E 39+00N	1	7	8	43	.1	2	2	246	1.60	2	5	ND	2	17	1	2	2	29	.12	.069	12	13	.09	64	.07	6	.86	.01	.06	1	1	5
L44E 38+75N	1	10	6	48	.1	7	6	256	2.23	5	5	ND	2	25	1	2	2	41	.21	.059	11	19	.21	118	.10	5	1.32	.01	.05	1	1	10
L44E 38+50N	1	6	8	45	.1	4	3	329	1.80	2	5	ND	2	17	1	3	2	33	.17	.043	11	14	.13	68	.09	2	.97	.01	.06	1	1	5
L44E 38+25N	1	7	6	32	.2	11	4	189	1.86	4	5	ND	2	28	1	2	2	33	.25	.033	12	16	.21	82	.10	2	1.12	.01	.07	2	1	5
L44E 38+00N	1	5	6	35	.1	3	5	245	1.32	4	5	ND	2	19	1	2	3	24	.19	.021	14	10	.12	60	.08	2	.81	.01	.05	1	1	5
L44E 37+75N	1	7	10	54	.1	5	5	412	1.66	2	5	ND	2	18	1	2	2	31	.17	.030	13	15	.15	63	.10	2	.96	.01	.05	1	1	5
L44E 37+50N	1	6	17	57	.1	5	6	478	1.98	2	5	ND	1	25	1	2	2	34	.23	.032	17	15	.21	89	.06	2	1.23	.01	.06	1	1	10
L44E 37+00N	2	7	16	156	.3	8	6	290	2.64	12	5	ND	3	12	1	2	2	41	.11	.099	11	17	.16	91	.07	2	2.14	.01	.04	1	3	20
L45E 43+00N	1	6	5	45	.1	7	4	340	1.76	6	5	ND	2	23	1	2	6	30	.20	.023	17	11	.22	89	.07	2	1.15	.01	.07	1	2	10
L45E 42+75N	1	6	12	62	.1	12	6	218	2.22	8	5	ND	3	23	1	4	2	35	.19	.031	12	16	.31	92	.09	2	1.48	.01	.07	1	1	20
L45E 42+50N	1	8	10	62	.1	10	4	622	1.99	6	5	ND	2	26	1	2	2	33	.23	.021	15	14	.24	90	.08	2	1.27	.01	.07	2	1	10
L45E 42+25N	1	8	8	38	.1	8	5	310	2.05	8	5	ND	2	25	1	2	2	33	.20	.038	14	17	.25	94	.09	2	1.33	.01	.06	1	1	10
L45E 42+00N	1	11	10	59	.2	11	5	315	2.16	14	5	ND	2	29	1	2	2	34	.26	.033	20	16	.32	98	.08	2	1.30	.02	.08	1	1	30
STD C/AU-S	19	63	39	132	8.0	68	29	1103	4.09	42	20	8	37	48	19	18	19	59	.48	.098	39	63	.96	183	.07	34	2.01	.07	.13	15	53	1300

MINGOLD RESOURCES PROJECT-620 FILE # 88-1652

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L45E 41+75W	1	5	8	60	.1	10	4	282	2.13	6	5	ND	2	23	1	4	2	35	.22	.053	14	18	.26	86	.08	2	1.19	.01	.09	1	1	10
L45E 39+75W	1	6	9	74	.4	8	3	348	1.93	3	5	ND	2	37	1	2	2	32	.31	.059	17	16	.21	118	.06	3	1.10	.02	.07	1	2	20
L45E 39+50W	1	7	4	52	.3	10	4	322	1.94	7	5	ND	3	28	1	2	3	34	.23	.058	13	13	.19	90	.07	2	.93	.01	.10	2	1	20
L45E 39+25W	1	5	13	70	.1	9	3	222	1.96	3	5	ND	2	23	1	2	2	31	.20	.114	12	16	.19	118	.07	2	1.39	.01	.07	1	2	10
L45E 39+00W	1	6	11	81	.2	10	5	516	1.97	2	5	ND	2	18	1	2	2	32	.15	.085	11	12	.17	100	.07	2	1.30	.01	.06	1	1	5
L45E 38+75W	1	12	15	73	.1	20	7	318	2.94	4	5	ND	1	24	1	2	2	51	.22	.068	10	25	.31	109	.12	4	2.08	.01	.07	1	1	10
L45E 38+50W	1	7	16	63	.2	11	5	267	2.04	4	5	ND	1	25	1	2	2	38	.23	.024	11	17	.23	77	.12	2	1.03	.01	.07	1	4	5
L45E 38+25W	1	6	9	47	.2	8	3	146	1.46	2	5	ND	2	21	1	2	2	28	.19	.020	12	10	.16	63	.09	2	.88	.01	.05	2	1	5
L45E 38+00W	1	4	8	52	.2	7	4	163	1.79	2	5	ND	2	22	1	2	2	30	.20	.045	13	16	.20	90	.08	2	1.15	.01	.05	1	1	5
L45E 37+75W	1	4	17	39	.1	10	3	183	1.19	2	5	ND	2	28	1	2	2	20	.25	.021	17	14	.25	87	.09	4	1.05	.02	.06	1	1	5
L45E 37+50W	1	5	9	50	.1	6	2	156	1.16	2	5	ND	2	16	1	2	2	21	.15	.018	11	8	.19	66	.08	2	.89	.01	.05	1	1	5
L45E 37+25W	1	7	11	54	.1	10	4	190	1.35	2	5	ND	2	18	1	3	2	33	.15	.046	10	13	.17	84	.07	10	1.22	.01	.12	1	2	10
L45E 37+00W	1	9	15	58	.2	10	6	190	2.57	6	5	ND	2	18	1	2	2	45	.10	.041	9	18	.24	111	.09	2	1.80	.01	.06	1	1	20
L46E 44+00W	1	3	9	44	.1	8	3	275	1.58	4	5	ND	1	26	1	2	3	28	.23	.023	12	12	.19	73	.07	2	.81	.01	.07	1	1	10
L46E 43+75W	1	7	7	36	.2	8	2	183	1.65	9	5	ND	2	21	1	2	2	31	.18	.018	12	11	.20	71	.07	2	.77	.01	.05	2	2	10
L46E 43+50W	1	5	8	34	.1	6	2	183	1.53	7	5	ND	2	21	1	2	3	30	.18	.014	13	11	.19	69	.07	3	.68	.01	.06	2	1	5
L46E 43+25W	1	5	13	63	.2	8	4	372	1.63	4	5	ND	1	19	1	2	3	27	.19	.022	12	10	.14	71	.05	2	1.08	.01	.06	1	1	20
L46E 43+00W	1	5	11	59	.1	7	5	309	1.88	5	5	ND	2	20	1	2	2	31	.18	.020	14	14	.23	71	.07	2	1.14	.01	.05	1	2	10
L46E 42+75W	1	5	7	51	.2	10	2	233	1.77	6	5	ND	2	21	1	2	2	30	.18	.014	13	12	.24	70	.09	2	1.05	.01	.04	1	1	5
L46E 42+50W	1	9	8	62	.1	13	5	356	2.16	3	5	ND	1	25	1	2	3	35	.23	.040	12	19	.21	73	.08	2	1.09	.01	.06	1	1	10
L46E 42+25W	1	5	7	65	.2	11	4	291	2.07	6	5	ND	1	20	1	2	2	37	.16	.026	12	14	.21	80	.09	13	1.20	.01	.05	1	2	5
L46E 42+00W	1	7	6	52	.3	10	4	325	1.97	4	5	ND	2	21	1	2	2	37	.19	.022	11	14	.17	73	.08	3	.94	.01	.05	1	1	10
L46E 41+75W	1	5	7	74	.2	7	4	322	1.93	17	5	ND	1	23	1	2	3	30	.17	.037	12	13	.18	82	.08	3	1.26	.01	.06	1	1	10
L46E 41+50W	1	5	2	48	.1	7	4	212	1.75	2	5	ND	2	21	1	3	2	32	.16	.033	10	12	.17	62	.06	2	.92	.01	.05	2	1	5
L46E 41+25W	1	3	10	111	.4	9	5	797	1.77	5	5	ND	2	28	1	2	2	30	.17	.026	13	13	.18	116	.06	2	1.12	.01	.07	1	2	20
L46E 41+00W	1	6	7	86	.1	11	5	708	1.70	3	5	ND	2	20	1	2	2	32	.21	.043	12	10	.13	80	.07	3	1.11	.01	.08	1	1	10
L46E 40+75W	1	4	9	61	.1	7	3	320	1.77	3	5	ND	3	18	1	2	2	29	.17	.044	12	13	.17	90	.07	2	1.07	.01	.06	1	1	5
L46E 40+50W	1	2	10	73	.1	6	3	332	1.62	2	5	ND	1	19	1	2	3	27	.17	.041	12	10	.14	96	.07	2	1.14	.01	.06	1	1	5
L46E 40+25W	1	5	9	62	.2	9	4	209	1.94	9	5	ND	2	17	1	2	2	32	.16	.053	10	11	.18	93	.06	3	1.42	.01	.05	1	1	20
L46E 40+00W	3	11	15	63	.5	11	5	384	2.11	68	5	ND	1	47	1	2	3	31	.37	.026	51	13	.30	98	.03	2	1.70	.01	.09	1	1	120
L46E 39+50W	1	8	2	87	.1	8	6	262	2.27	3	5	ND	2	13	1	2	2	36	.12	.094	12	16	.17	93	.07	4	1.84	.01	.05	1	1	20
L46E 39+25W	1	8	20	79	.1	11	5	378	1.85	2	5	ND	2	13	1	2	2	30	.12	.077	11	12	.14	83	.06	2	1.52	.01	.04	1	2	20
L46E 39+00W	1	5	2	44	.1	6	5	242	1.88	4	5	ND	2	24	1	2	6	32	.21	.050	13	12	.21	104	.07	2	1.12	.01	.05	2	1	38
L46E 38+75W	1	8	9	173	.3	12	7	514	2.91	2	5	ND	3	13	1	2	2	41	.12	.190	13	18	.22	121	.05	4	2.68	.01	.07	1	1	30
L46E 38+50W	1	5	8	102	.1	6	5	376	2.14	3	5	ND	2	32	1	2	2	32	.12	.090	10	14	.18	98	.06	2	1.81	.01	.04	1	2	28
L46E 38+25W	1	7	10	46	.2	4	3	195	1.32	2	5	ND	1	36	1	2	2	22	.29	.031	15	12	.18	104	.06	3	.95	.02	.05	3	1	18
STD C/AU-S	19	63	41	133	7.9	71	27	1122	4.18	44	18	8	37	48	20	18	24	59	.49	.095	38	61	.97	179	.07	32	2.03	.06	.14	14	47	1400

"F" Grid

MINGOLD RESOURCES PROJECT-620 FILE # 88-1652

F" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L46E 38+00W	1	6	33	40	.1	6	3	134	1.28	2	5	ND	1	20	1	2	2	22	.17	.020	13	14	.16	86	.07	2	1.03	.02	.04	1	1	5
L46E 37+75W	1	5	10	42	.1	4	2	140	1.29	2	5	ND	2	13	1	2	2	25	.12	.029	11	9	.15	49	.08	2	1.08	.01	.03	1	2	10
L46E 37+50W	1	6	14	34	.1	7	3	137	1.47	2	5	ND	1	29	1	2	2	23	.22	.023	15	12	.21	107	.06	4	1.25	.02	.04	1	1	10
L46E 37+25W	1	11	5	49	.1	11	6	224	1.62	2	5	ND	1	36	1	2	2	30	.43	.028	17	23	.29	98	.06	3	1.33	.01	.06	1	2	20
L46E 37+00W	1	7	3	42	.1	7	1	115	.97	2	5	ND	1	20	1	2	2	17	.16	.014	12	11	.16	77	.05	2	1.04	.01	.04	1	2	5
L47E 43+75W	1	4	12	58	.1	10	4	357	1.91	2	5	ND	2	20	1	3	3	33	.20	.045	13	14	.18	87	.07	2	1.46	.01	.09	1	4	5
L47E 43+50W	1	5	7	52	.1	9	4	450	1.40	2	5	ND	1	23	1	2	3	30	.24	.049	11	16	.18	96	.07	2	1.05	.01	.06	1	1	5
L47E 43+25W	1	6	2	31	.1	10	3	197	1.80	6	5	ND	2	20	1	2	3	32	.19	.058	11	13	.17	87	.06	8	1.16	.01	.05	1	6	5
L47E 43+00W	1	7	6	32	.1	8	3	184	1.31	5	5	ND	3	21	1	2	2	29	.20	.016	12	13	.18	75	.08	2	.76	.01	.06	1	1	5
L47E 42+75W	1	5	6	49	.1	7	3	219	1.58	2	5	ND	1	22	1	2	2	30	.23	.014	13	13	.20	72	.10	2	.93	.01	.05	1	1	5
L47E 42+50W	1	8	2	62	.1	11	5	386	2.40	2	5	ND	1	21	1	2	2	46	.23	.036	11	23	.19	80	.11	2	1.19	.01	.04	1	2	10
L47E 42+25W	1	9	3	67	.1	8	6	322	2.43	4	5	ND	2	19	1	2	5	46	.17	.032	10	21	.23	86	.10	2	1.28	.01	.05	1	2	5
L47E 42+00W	1	8	8	61	.1	8	4	252	1.74	6	5	ND	2	16	1	2	2	30	.16	.034	12	15	.18	70	.07	2	1.02	.01	.05	1	1	10
L47E 41+75W	1	4	6	52	.1	8	2	193	1.63	7	5	ND	2	17	1	2	2	29	.17	.029	11	12	.15	64	.06	2	.95	.01	.06	1	1	5
L47E 41+50W	1	5	2	31	.1	11	3	265	1.46	3	5	ND	2	15	1	2	2	26	.16	.041	22	9	.14	75	.05	2	.92	.01	.07	1	2	10
L47E 41+25W	1	7	7	38	.2	7	4	234	1.46	3	5	ND	2	23	1	2	2	24	.23	.021	19	11	.18	79	.06	2	1.05	.01	.07	1	1	5
L47E 41+00W	2	34	23	98	.1	31	13	1963	4.34	30	5	ND	4	63	1	5	2	50	.69	.048	46	32	.59	290	.02	2	4.90	.02	.20	2	2	50
L47E 40+75W	1	12	12	62	.1	13	6	532	2.68	14	5	ND	1	37	1	2	2	38	.33	.044	23	18	.39	125	.04	2	2.22	.01	.09	1	1	50
L47E 40+50W	1	11	8	74	.1	12	6	1119	2.87	12	5	ND	1	38	1	2	2	43	.32	.050	21	18	.36	123	.04	2	2.28	.01	.09	1	1	30
L47E 40+25W	1	5	3	64	.1	5	5	503	2.11	5	5	ND	2	11	1	2	2	38	.12	.038	10	14	.17	82	.07	2	1.40	.01	.04	1	2	5
L47E 40+00W	1	7	9	58	.1	10	2	204	1.51	4	5	ND	2	16	1	2	2	28	.14	.021	12	11	.14	79	.07	3	1.19	.01	.04	1	2	5
L47E 39+50W	1	7	9	50	.1	8	4	213	1.92	5	5	ND	3	14	1	2	2	32	.13	.070	13	11	.16	79	.06	2	1.40	.01	.05	1	1	10
L47E 39+25W	1	8	9	87	.1	10	5	225	2.38	3	5	ND	2	9	1	2	2	36	.10	.150	10	12	.15	81	.05	3	1.85	.01	.05	1	2	30
L47E 39+00W	1	7	9	40	.1	6	3	212	1.62	2	5	ND	3	26	1	2	2	24	.24	.039	14	13	.27	83	.06	2	1.14	.01	.05	2	1	20
L48E 44+00W	1	7	2	59	.2	6	3	235	1.43	2	5	ND	2	18	1	2	3	26	.17	.036	13	8	.16	76	.07	3	1.01	.01	.04	1	1	20
L48E 43+75W	2	15	17	151	.3	16	8	258	3.32	7	5	ND	3	20	1	2	2	46	.31	.218	12	22	.34	156	.06	2	3.28	.01	.07	1	1	30
L48E 43+50W	1	6	5	62	.1	7	4	827	1.67	2	5	ND	1	18	1	2	2	27	.21	.099	13	17	.16	108	.06	2	1.09	.01	.06	1	3	30
L48E 43+25W	1	24	5	115	.2	25	11	867	3.27	11	5	ND	2	39	1	2	2	65	.71	.149	17	40	.63	97	.21	4	2.59	.02	.09	1	2	20
L48E 43+00W	2	11	10	77	.1	16	6	693	2.80	5	5	ND	2	18	1	2	2	51	.22	.065	11	22	.23	113	.11	6	2.26	.01	.04	1	8	30
L48E 42+75W	1	11	10	42	.1	11	3	200	2.01	8	5	ND	3	17	1	2	2	34	.18	.042	13	17	.22	79	.07	2	1.31	.01	.05	2	1	10
L48E 42+50W	1	8	10	73	.1	12	5	448	2.12	6	5	ND	3	17	1	2	2	35	.18	.078	22	14	.19	84	.06	2	1.85	.01	.04	1	1	20
L48E 42+25W	1	6	10	85	.1	7	4	346	1.84	2	5	ND	2	14	1	2	2	30	.20	.101	11	13	.14	72	.05	2	1.47	.01	.04	1	1	10
L48E 42+00W	1	7	4	43	.1	11	5	187	2.10	13	5	ND	2	20	1	2	5	39	.23	.042	13	13	.22	100	.07	2	1.39	.01	.04	2	1	30
L48E 41+75W	1	8	2	51	.1	12	4	147	1.76	3	5	ND	2	16	1	2	2	34	.21	.074	13	17	.20	66	.08	2	1.35	.01	.07	1	1	20
L48E 41+50W	1	5	4	82	.1	8	4	512	1.38	2	5	ND	2	16	1	2	2	24	.17	.038	14	12	.15	81	.05	4	1.22	.01	.06	1	2	10
L48E 41+25W	1	6	5	57	.1	10	3	157	1.62	3	5	ND	3	16	1	2	3	27	.16	.062	12	12	.14	76	.05	2	1.09	.01	.05	1	1	20
STD C/AU-S	18	63	38	129	7.7	71	27	1005	4.04	41	20	8	36	47	20	16	23	59	.47	.094	38	61	.95	179	.07	32	1.98	.06	.14	14	48	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L48E 41+00N	1	7	10	80	.1	8	4	222	1.75	3	5	ND	2	17	1	2	2	29	.20	.075	13	13	.17	80	.06	3	1.28	.01	.05	1	5	10
L48E 40+75N	1	7	13	35	.2	4	3	155	1.45	6	5	ND	3	22	1	2	2	28	.24	.016	18	11	.17	62	.07	2	.84	.01	.06	1	2	5
L48E 40+50N	1	6	8	36	.1	4	5	237	1.38	4	5	ND	2	20	1	2	2	27	.22	.015	18	12	.16	62	.08	7	.88	.01	.04	2	1	5
L48E 40+25N	5	8	6	66	.1	6	7	229	2.09	2	5	ND	3	27	1	2	2	40	.20	.031	16	15	.21	100	.06	3	1.71	.01	.04	1	1	5
L48E 40+00N	4	13	7	76	.3	8	9	884	2.38	3	5	ND	1	51	1	2	2	42	.35	.105	14	17	.30	76	.09	3	1.42	.01	.10	1	1	5
L48E 39+75N	7	8	4	64	.1	6	5	535	1.78	3	5	ND	2	58	1	2	2	33	.38	.019	14	14	.22	72	.07	2	1.21	.01	.03	1	3	5
L48E 39+50N	13	8	6	59	.1	7	6	202	2.30	2	5	ND	2	15	1	3	2	46	.13	.022	13	16	.22	60	.08	2	1.39	.01	.05	1	1	5
L50E 30+00N	1	10	16	65	.1	7	4	191	2.06	8	5	ND	2	20	1	2	2	33	.19	.049	16	13	.25	88	.07	2	1.64	.01	.05	1	1	5
L50E 29+75N	1	6	14	90	.1	10	6	268	2.14	2	5	ND	3	16	1	2	2	33	.17	.070	12	14	.21	103	.07	2	1.89	.01	.05	1	2	10
L50E 29+50N	1	12	4	53	.1	10	7	222	2.41	4	5	ND	3	20	1	2	2	42	.23	.091	17	16	.24	87	.07	4	1.42	.01	.07	1	1	5
L50E 29+00N	1	9	7	66	.1	5	5	270	1.80	3	5	ND	2	17	1	2	2	31	.17	.050	15	13	.21	82	.06	6	1.28	.01	.05	1	15	5
L50E 28+75N	1	4	9	47	.2	4	4	173	1.57	2	5	ND	1	17	1	3	5	31	.17	.022	13	12	.19	68	.11	7	1.10	.01	.05	1	1	5
L50E 28+50N	1	7	7	69	.1	7	5	173	2.06	3	5	ND	2	17	1	2	2	32	.16	.057	14	15	.24	98	.06	2	1.87	.01	.06	1	3	5
L50E 28+25N	1	8	3	82	.2	10	5	170	1.98	2	5	ND	3	11	1	2	2	30	.10	.083	12	12	.17	95	.06	3	1.90	.01	.05	1	1	10
L50E 28+00N	1	7	15	50	.1	7	4	154	1.64	2	5	ND	2	16	1	2	2	28	.16	.035	15	15	.21	93	.07	2	1.74	.01	.06	1	1	5
L50E 27+75N	1	8	12	71	.1	15	7	250	2.41	7	5	ND	3	19	1	2	3	37	.20	.123	14	16	.24	135	.07	2	2.17	.01	.06	1	1	20
L50E 27+50N	1	6	12	106	.1	11	6	283	2.57	2	5	ND	1	18	1	2	2	40	.17	.108	12	20	.24	124	.10	2	2.54	.01	.06	1	2	30
L50E 27+25N	1	9	5	56	.1	10	5	195	2.20	2	5	ND	3	15	1	2	2	37	.14	.058	13	14	.17	91	.07	2	1.73	.01	.05	1	2	5
L50E 27+00N	1	4	11	34	.1	7	4	152	1.25	2	5	ND	2	20	1	3	2	23	.19	.029	13	10	.21	72	.08	7	1.06	.01	.05	1	1	5
L50E 26+75N	1	3	8	42	.1	4	3	124	1.19	2	5	ND	1	16	1	2	2	25	.14	.018	12	10	.13	62	.09	2	.86	.01	.03	1	1	5
L50E 26+50N	1	5	3	42	.1	4	3	164	1.39	2	5	ND	2	24	1	3	2	26	.23	.029	15	12	.22	80	.09	7	1.04	.01	.05	1	1	5
L50E 26+25N	1	10	10	68	.1	10	5	432	2.16	3	5	ND	1	29	1	2	4	35	.22	.040	19	18	.28	111	.06	6	1.37	.02	.06	1	1	20
L50E 26+00N	1	5	12	48	.1	7	4	160	1.59	2	5	ND	3	17	1	4	3	30	.16	.021	13	13	.19	61	.11	2	1.02	.01	.08	1	2	5
L50E 25+75N	1	9	8	74	.2	9	4	176	1.75	2	5	ND	1	23	1	2	2	31	.20	.033	17	18	.23	83	.07	4	1.31	.01	.06	1	1	5
L50E 25+50N	1	13	18	107	.4	12	9	228	2.96	5	5	ND	2	29	1	3	2	46	.33	.159	15	19	.26	139	.08	6	2.05	.01	.06	1	1	10
L50E 25+25N	1	8	7	85	.1	10	6	320	2.25	4	5	ND	2	10	1	2	2	28	.09	.045	8	12	.13	119	.01	4	2.12	.01	.08	1	2	5
L50E 24+50N	1	24	25	86	.1	22	11	350	3.71	5	5	ND	2	26	1	2	3	67	.24	.106	12	36	.54	120	.18	11	2.92	.01	.04	1	1	10
L50E 24+25N	1	10	10	96	.1	14	6	483	2.55	7	5	ND	2	20	1	2	2	39	.17	.103	14	18	.27	132	.06	3	2.34	.01	.07	1	1	20
L50E 24+00N	1	8	13	59	.1	10	7	220	2.43	6	5	ND	3	16	1	2	3	39	.14	.069	14	25	.25	118	.06	2	1.88	.01	.06	1	1	10
L51E 30+00N	1	9	18	76	.2	12	6	310	2.36	5	5	ND	4	15	1	2	3	36	.14	.079	13	15	.22	109	.07	3	2.00	.01	.06	1	3	20
L51E 29+75N	1	4	5	56	.1	8	3	147	1.47	2	5	ND	3	15	1	2	6	27	.14	.031	14	12	.17	80	.08	2	1.17	.01	.04	1	1	10
L51E 29+00N	1	7	9	115	.1	10	5	425	2.36	4	5	ND	1	18	1	2	3	34	.16	.131	13	35	.17	159	.03	2	2.04	.01	.07	1	2	30
L51E 28+75N	1	8	10	54	.1	5	3	165	1.72	3	5	ND	3	21	1	2	2	31	.21	.020	15	13	.19	94	.07	2	1.16	.01	.07	1	1	5
L51E 28+50N	1	9	7	52	.2	11	6	216	2.30	3	5	ND	4	16	1	2	2	39	.14	.066	14	17	.21	126	.08	6	1.78	.01	.06	1	2	10
L51E 28+00N	1	7	14	62	.2	9	5	182	2.02	2	5	ND	3	21	1	2	2	31	.18	.073	13	15	.20	136	.06	5	2.18	.01	.04	1	1	30
L51E 27+75N	1	6	17	97	.1	10	5	263	2.12	2	5	ND	3	15	1	2	2	33	.14	.087	13	16	.17	103	.07	2	2.30	.01	.06	1	1	20
STD C/AU-S	20	63	42	131	7.6	73	29	1098	4.28	42	17	8	40	53	20	16	23	63	.48	.097	40	63	.93	182	.08	39	2.00	.08	.16	14	48	1400

D" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L51E 27+50N	1	4	18	95	.1	12	5	262	2.21	2	5	ND	3	11	1	3	2	31	.12	.096	11	14	.13	82	.06	4	2.11	.01	.04	1	1	20
L51E 27+25N	1	8	10	51	.1	6	6	326	1.39	2	5	ND	1	22	1	2	3	25	.25	.020	13	13	.19	83	.05	11	1.28	.01	.05	1	1	10
L51E 27+00N	1	4	14	85	.1	7	5	207	2.18	2	5	ND	2	19	1	2	3	33	.25	.072	11	12	.14	94	.06	7	1.47	.01	.05	1	1	5
L51E 26+75N	1	5	21	66	.1	9	5	140	2.32	2	5	ND	1	13	1	2	2	35	.13	.070	12	16	.14	96	.04	2	1.85	.01	.03	1	1	5
L51E 26+50N	1	6	10	43	.1	5	3	148	1.47	2	5	ND	1	16	1	2	4	24	.18	.024	12	14	.16	88	.07	6	1.06	.01	.04	2	1	5
L51E 26+00N	1	7	15	113	.1	12	7	226	2.98	2	5	ND	3	14	1	2	2	42	.18	.182	12	20	.19	105	.06	2	2.49	.01	.05	1	1	10
L51E 25+75N	1	8	11	43	.1	9	5	196	1.85	2	5	ND	2	18	1	2	2	29	.25	.039	13	15	.23	85	.08	2	1.15	.01	.04	2	1	10
L51E 25+50N	1	8	15	44	.1	10	7	303	2.18	6	5	ND	3	17	1	2	3	37	.21	.052	13	19	.19	77	.07	3	1.33	.01	.04	1	1	5
L51E 25+25N	1	6	12	36	.1	9	4	194	1.80	2	5	ND	2	17	1	3	4	32	.20	.033	12	19	.16	72	.08	7	.92	.01	.03	2	3	5
L51E 24+75N	1	10	18	48	.1	12	6	237	2.44	2	5	ND	3	16	1	2	2	42	.19	.069	13	19	.21	102	.08	4	1.46	.02	.05	1	1	10
L51E 24+50N	1	12	9	71	.1	12	9	581	2.47	2	5	ND	1	30	1	3	2	41	.33	.053	17	21	.33	131	.07	2	1.75	.01	.05	1	1	20
L51E 24+25N	1	9	10	58	.1	16	7	309	2.47	2	5	ND	3	17	1	2	4	38	.20	.080	12	22	.24	136	.07	4	1.90	.01	.06	1	1	10
L51E 24+00N	1	5	18	71	.1	9	5	253	2.30	2	5	ND	2	20	1	2	2	38	.23	.045	9	20	.26	89	.10	7	1.64	.01	.03	1	1	5
L52E 30+00N	1	8	9	49	.1	5	4	202	2.11	4	5	ND	2	16	1	2	3	32	.20	.048	14	14	.20	105	.07	5	1.46	.01	.03	2	1	5
L52E 29+00N	1	8	12	95	.1	9	4	213	2.14	4	5	ND	1	10	1	2	3	29	.11	.075	10	14	.16	79	.05	2	1.70	.01	.04	1	1	5
L52E 28+75N	1	5	15	43	.1	8	3	131	1.48	3	5	ND	1	22	1	2	5	22	.23	.022	15	15	.17	110	.06	2	1.20	.01	.03	3	2	10
L52E 27+75N	1	6	13	38	.1	7	5	187	1.69	2	5	ND	1	20	1	2	3	27	.22	.023	12	12	.19	103	.06	2	1.16	.01	.05	1	1	5
L52E 27+50N	1	6	9	61	.1	8	6	131	1.61	2	5	ND	1	19	1	2	3	25	.18	.030	10	18	.13	90	.04	5	1.30	.01	.04	1	1	20
L52E 27+00N	1	6	18	40	.1	11	4	179	1.82	2	5	ND	1	50	1	3	5	24	.71	.032	22	16	.23	125	.05	2	1.41	.02	.04	1	1	20
L52E 26+75N	1	7	13	57	.1	7	4	263	2.02	2	5	ND	1	32	1	4	2	31	.35	.048	19	16	.20	128	.05	4	1.32	.01	.04	2	1	10
L52E 26+50N	1	7	16	45	.1	8	4	131	1.64	2	5	ND	2	12	1	3	4	24	.14	.057	11	17	.17	72	.04	7	2.09	.01	.04	1	1	10
L52E 26+25N	2	22	18	112	.1	19	13	921	4.19	11	5	ND	1	38	1	2	2	66	.43	.087	19	30	.47	189	.04	2	3.70	.01	.09	1	4	30
L52E 26+00N	1	9	15	99	.1	11	8	316	2.52	4	5	ND	3	15	1	2	2	36	.18	.090	11	15	.21	116	.05	2	2.15	.01	.06	1	1	20
L52E 25+75N	1	7	13	61	.1	11	4	176	1.77	7	5	ND	2	14	1	2	2	27	.14	.043	11	12	.15	102	.06	2	1.58	.01	.04	1	1	10
L52E 25+50N	1	7	12	47	.1	8	5	259	1.82	3	5	ND	2	15	1	2	4	30	.18	.040	12	12	.17	79	.07	7	1.07	.01	.04	2	1	5
L52E 24+75N	1	9	10	86	.2	13	7	220	2.61	4	5	ND	1	13	1	2	5	38	.14	.130	11	18	.23	102	.07	3	2.25	.01	.04	1	1	20
L52E 24+50N	1	12	9	70	.2	12	5	418	2.36	4	5	ND	1	31	1	2	2	36	.36	.047	24	20	.34	112	.07	2	1.76	.01	.05	1	1	30
L52E 24+25N	1	6	12	45	.1	7	4	237	1.74	3	5	ND	1	19	1	2	2	28	.23	.033	14	14	.22	70	.07	2	.94	.01	.05	2	1	5
L52E 24+00N	2	29	20	145	.1	21	19	3921	4.33	13	5	ND	2	47	1	2	2	52	.49	.106	37	30	.59	235	.01	2	4.48	.01	.13	1	1	40
L53E 29+25N	1	7	5	61	.1	7	7	225	2.32	5	5	ND	1	11	1	2	2	34	.11	.068	12	14	.16	88	.05	2	1.83	.01	.04	1	1	5
L53E 28+75N	1	6	12	50	.2	6	2	138	1.40	2	5	ND	1	19	1	2	4	23	.20	.021	12	10	.15	81	.04	2	1.11	.01	.04	1	2	5
L53E 28+50N	1	10	16	65	.1	10	7	215	2.40	6	5	ND	2	25	1	2	2	36	.22	.077	14	16	.19	134	.05	2	2.07	.01	.04	1	1	10
L53E 28+25N	1	4	10	51	.1	1	1	218	1.57	2	5	ND	1	20	1	2	2	26	.09	.059	9	10	.08	60	.04	5	1.31	.01	.05	1	1	5
L53E 27+25N	1	10	14	65	.1	10	6	668	2.31	2	5	ND	3	20	1	2	2	35	.23	.078	14	15	.24	101	.06	3	1.50	.01	.06	1	1	5
L53E 27+00N	1	6	9	39	.1	3	3	129	1.33	2	5	ND	2	15	1	2	2	23	.14	.023	12	8	.13	63	.06	2	1.03	.01	.05	2	1	5
L53E 26+75N	1	7	11	41	.1	7	4	186	1.35	4	5	ND	2	20	1	2	2	24	.19	.023	12	14	.19	79	.08	2	1.12	.01	.06	2	1	10
STD C/AU-S	19	64	43	132	7.9	71	28	1116	4.12	41	18	8	37	48	19	17	18	59	.49	.088	39	60	.87	183	.07	34	2.06	.07	.14	13	51	1300

"D" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L53E 26+50N	1	6	11	44	.1	5	3	271	1.21	2	5	ND	2	21	1	2	2	25	.24	.021	14	10	.15	77	.10	2	.98	.01	.06	2	1	5
L53E 26+25N	1	3	18	73	.1	10	4	251	1.88	5	5	ND	2	11	1	2	2	29	.10	.066	11	12	.16	102	.05	2	1.86	.01	.03	1	1	10
L53E 26+00N	1	3	12	39	.1	5	1	115	1.10	2	5	ND	2	14	1	2	6	22	.13	.013	11	11	.12	55	.07	6	.85	.01	.03	2	2	5
L53E 25+75N	1	4	11	40	.2	8	3	171	1.24	3	5	ND	1	16	1	3	3	26	.14	.017	12	11	.12	69	.07	3	.70	.01	.05	2	1	5
L53E 25+50N	1	7	12	76	.1	10	5	221	2.11	7	5	ND	3	24	1	2	4	36	.25	.055	15	17	.25	85	.08	4	1.18	.01	.06	1	1	5
L53E 25+25N	1	5	9	51	.1	6	4	189	1.85	3	5	ND	2	20	1	2	2	33	.21	.048	16	13	.22	85	.07	5	1.10	.01	.05	1	1	5
L53E 25+00N	1	10	14	71	.2	11	6	877	2.28	5	5	ND	2	34	1	2	2	35	.31	.039	26	18	.34	125	.05	4	1.86	.01	.07	1	1	10
L53E 24+75N	1	4	18	39	.2	5	2	164	1.38	2	5	ND	2	18	1	2	2	26	.17	.012	15	11	.19	55	.07	3	.82	.01	.04	1	1	5
L53E 24+50N	1	5	12	41	.1	6	3	187	1.57	2	5	ND	1	22	1	2	2	27	.21	.028	16	12	.22	73	.06	3	1.02	.01	.05	1	2	5
L53E 24+25N	1	6	6	59	.1	8	6	785	2.15	6	5	ND	1	22	1	2	2	35	.20	.040	16	15	.25	83	.05	3	1.44	.01	.06	1	4	20
L53E 24+00N	1	8	12	48	.3	7	2	310	1.63	3	5	ND	1	25	1	2	2	27	.24	.033	18	12	.24	78	.06	6	1.21	.01	.07	1	1	10
L54E 30+00N	1	5	8	55	.1	9	4	297	1.98	7	5	ND	1	27	1	2	2	32	.29	.050	21	15	.26	120	.06	2	1.32	.01	.06	1	1	10
L54E 29+75N	1	4	14	71	.3	8	3	159	1.69	3	5	ND	2	18	1	3	2	29	.16	.024	13	13	.18	98	.06	2	1.30	.01	.06	1	1	5
L54E 29+50N	1	7	13	61	.1	11	5	168	2.10	6	5	ND	3	13	1	2	2	32	.10	.072	11	14	.20	107	.06	2	1.07	.01	.05	1	1	30
L54E 29+25N	1	4	11	40	.2	6	2	120	1.13	2	5	ND	3	12	1	2	2	23	.11	.020	11	9	.09	63	.07	4	.99	.01	.05	1	1	5
L54E 29+00N <	1	4	9	44	.1	6	4	154	1.66	3	5	ND	2	15	1	2	5	30	.14	.027	12	12	.18	84	.07	2	1.42	.01	.03	2	1	5
L54E 28+00N	1	3	11	42	.1	6	3	197	1.55	5	5	ND	2	19	1	2	2	28	.19	.027	13	12	.22	67	.07	2	.97	.01	.05	2	1	5
L54E 27+75N	1	4	11	57	.1	8	3	273	1.59	2	5	ND	1	17	1	2	7	28	.16	.023	12	12	.22	68	.07	2	1.12	.01	.05	1	1	10
L54E 27+50N	1	5	16	62	.1	7	3	169	1.53	2	5	ND	3	16	1	2	2	25	.14	.034	13	12	.19	72	.06	2	1.31	.01	.04	1	1	5
L54E 27+25N <	1	7	11	57	.2	8	3	220	1.69	2	5	ND	1	21	1	2	2	27	.19	.036	15	13	.25	84	.05	4	1.56	.01	.07	1	2	20
L54E 26+75N	1	6	10	57	.2	11	3	157	2.18	3	5	ND	3	13	1	2	2	34	.13	.066	12	13	.18	76	.07	3	1.60	.01	.06	1	1	20
L54E 26+50N	1	3	7	50	.1	5	3	144	1.48	2	5	ND	2	17	1	2	2	26	.16	.026	12	12	.18	72	.08	2	1.18	.01	.06	1	1	10
L54E 26+25N	1	2	10	47	.2	6	2	170	1.32	2	5	ND	3	15	1	2	2	25	.14	.024	12	10	.15	63	.07	6	1.01	.01	.05	2	1	5
L54E 26+00N	1	7	7	88	.3	11	5	255	2.30	2	5	ND	2	26	1	2	5	39	.22	.056	12	19	.29	89	.09	3	1.40	.01	.04	1	1	5
L54E 25+75N <	1	4	11	47	.1	7	4	209	1.67	2	5	ND	2	25	1	2	2	29	.25	.026	14	16	.28	70	.09	10	1.11	.01	.04	2	1	5
L54E 25+25N	1	27	18	128	.1	19	10	1432	3.57	6	5	ND	1	56	1	2	2	47	.48	.090	40	26	.47	217	.01	2	3.88	.01	.14	1	1	40
L54E 25+00N	1	2	6	44	.1	5	2	222	1.43	2	5	ND	2	20	1	2	2	25	.19	.020	14	11	.22	65	.07	2	.92	.01	.04	1	1	5
L54E 24+75N	1	5	11	50	.1	7	3	185	1.51	2	5	ND	2	20	1	2	7	27	.19	.022	14	15	.21	62	.07	2	1.02	.01	.05	1	2	10
L54E 24+50N	1	7	6	44	.2	9	3	259	1.61	4	5	ND	3	18	1	4	2	28	.18	.021	14	13	.23	63	.07	2	.97	.01	.05	2	1	5
L54E 24+25N	1	6	14	49	.1	8	5	238	1.92	2	5	ND	2	22	1	2	4	34	.21	.020	13	18	.27	65	.09	2	1.19	.01	.06	1	1	5
L54E 24+00N	1	5	6	35	.1	8	3	159	1.41	2	5	ND	2	21	1	2	2	24	.18	.021	14	11	.22	68	.07	3	.95	.01	.06	2	3	5
L55E 30+00N	1	6	9	58	.1	6	4	405	1.61	2	5	ND	1	30	1	2	2	27	.29	.027	23	12	.18	94	.04	2	1.11	.01	.05	1	2	5
L55E 29+75N <	1	5	8	67	.1	8	3	137	1.05	2	5	ND	1	33	1	2	2	30	.34	.043	13	12	.16	108	.05	2	1.37	.01	.04	1	1	10
L55E 28+75N	1	7	14	64	.2	9	4	275	1.80	3	5	ND	3	22	1	2	4	30	.23	.034	14	13	.25	81	.06	2	1.33	.01	.06	1	1	5
L55E 28+50N	1	5	10	53	.1	8	2	219	1.56	2	5	ND	2	19	1	2	2	28	.18	.022	15	11	.21	71	.07	7	1.11	.01	.06	1	2	5
L55E 28+25N	1	5	6	40	.2	8	2	153	1.43	2	5	ND	2	16	1	2	2	26	.17	.029	13	11	.19	66	.07	7	.98	.01	.04	3	1	5
STD C/AU-S	19	62	44	132	7.5	70	29	1074	4.11	43	15	8	39	51	19	16	18	61	.47	.091	41	61	.97	180	.07	33	1.97	.07	.15	13	50	1300

"D" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L55E 28+00N	1	5	13	48	.1	5	4	133	1.75	2	5	ND	2	12	1	2	4	31	.11	.052	11	12	.13	69	.07	4	1.34	.01	.03	1	2	20
L55E 27+75N	1	6	13	62	.1	8	5	216	1.87	2	5	ND	3	22	1	2	2	29	.19	.037	15	15	.28	102	.06	4	1.98	.01	.06	1	1	10
L55E 27+50N	1	5	8	46	.1	4	4	194	1.57	2	5	ND	1	18	1	2	2	28	.15	.028	12	11	.20	70	.06	2	1.15	.01	.05	1	1	5
L55E 27+25N	1	4	10	54	.2	8	4	183	1.75	2	5	ND	1	22	1	2	2	33	.21	.032	14	14	.25	76	.07	2	1.30	.01	.06	1	1	20
L55E 27+00N	1	4	9	44	.1	6	3	131	1.31	2	5	ND	2	16	1	4	2	24	.16	.026	12	12	.16	68	.08	2	1.02	.01	.04	1	1	10
L55E 26+75N	1	8	16	73	.2	9	5	145	1.94	3	5	ND	3	20	1	2	2	30	.19	.066	11	12	.16	92	.05	2	1.77	.01	.07	1	2	5
L55E 26+00N	1	9	14	75	.2	9	5	217	1.99	2	5	ND	2	18	1	2	2	36	.19	.045	13	20	.21	68	.10	4	2.03	.01	.05	1	1	5
L55E 25+75N	1	8	8	53	.1	8	9	311	2.29	2	5	ND	2	23	1	2	2	41	.20	.043	12	20	.30	90	.09	2	1.47	.01	.05	1	1	5
L55E 25+50N	1	16	14	89	.1	12	9	457	2.88	3	5	ND	1	34	1	2	2	49	.28	.065	19	23	.35	126	.07	4	2.21	.01	.08	1	1	20
L55E 25+25N	1	15	18	98	.1	15	8	594	2.89	7	5	ND	1	34	1	2	2	45	.33	.054	18	22	.40	131	.04	4	2.31	.01	.08	2	1	10
L55E 25+00N	1	7	9	45	.1	9	4	194	1.84	2	5	ND	2	21	1	2	2	34	.23	.039	15	15	.24	75	.08	7	.99	.01	.06	1	1	5
L55E 24+50N	1	23	17	94	.2	16	12	1030	2.98	3	5	ND	1	44	1	4	3	38	.35	.052	30	21	.38	217	.01	2	3.40	.01	.16	1	1	40
L55E 24+25N	1	10	7	67	.1	11	7	469	2.23	4	5	ND	1	29	1	2	2	35	.27	.052	17	16	.31	104	.04	3	1.55	.01	.09	1	2	20
L55E 24+00N	1	7	6	46	.1	8	4	179	1.51	3	5	ND	1	19	1	2	2	27	.18	.020	13	14	.22	62	.08	3	1.06	.01	.04	1	1	5
L56E 30+00N	1	6	10	53	.2	7	4	197	1.54	2	5	ND	2	18	1	2	2	27	.18	.021	13	13	.21	66	.07	2	.97	.01	.05	1	1	5
L56E 29+75N	1	5	9	45	.1	6	3	178	1.31	2	5	ND	2	23	1	2	2	22	.22	.019	15	13	.24	77	.08	2	1.00	.01	.06	1	2	10
L56E 29+50N	1	4	10	40	.1	8	4	201	1.26	2	5	ND	3	24	1	2	2	23	.26	.032	16	12	.25	77	.10	12	.92	.02	.07	1	1	5
L56E 29+25N	1	2	14	33	.1	6	3	162	1.12	2	5	ND	3	24	1	2	5	21	.27	.044	16	14	.22	71	.10	8	.82	.02	.07	1	1	10
L56E 29+00N	1	7	12	44	.3	9	5	193	1.52	2	5	ND	3	22	1	2	2	27	.23	.035	16	12	.24	77	.09	4	1.00	.02	.07	1	4	10
L56E 28+75N	1	8	13	46	.1	7	5	239	2.03	2	5	ND	3	24	1	2	3	37	.26	.051	17	16	.26	102	.09	11	1.20	.02	.06	1	1	20
L56E 28+50N	1	7	15	42	.1	6	5	206	1.93	3	5	ND	4	21	1	2	2	34	.23	.048	16	13	.24	95	.08	11	1.22	.01	.05	2	1	20
L56E 28+25N	1	5	11	44	.1	8	6	235	1.70	4	5	ND	2	22	1	2	2	31	.22	.042	16	13	.24	91	.08	2	1.19	.01	.06	1	1	10
L56E 28+00N	1	4	12	39	.1	5	3	147	1.22	2	5	ND	3	19	1	2	2	22	.19	.033	13	10	.22	87	.08	10	1.17	.01	.05	1	2	5
L56E 27+75N	1	9	16	49	.2	6	5	175	1.72	2	5	ND	3	20	1	2	2	30	.19	.033	14	12	.20	98	.08	3	1.28	.01	.05	1	1	5
L56E 27+50N	1	8	15	57	.1	9	6	190	1.94	3	5	ND	3	20	1	2	2	32	.17	.031	14	14	.22	116	.07	5	1.44	.01	.06	1	1	5
L56E 27+25N	1	7	6	36	.1	9	4	195	1.79	4	5	ND	3	26	1	2	2	33	.25	.041	16	17	.22	93	.09	4	1.05	.02	.06	1	1	5
L56E 26+50N	1	14	15	65	.2	17	10	358	3.13	7	5	ND	2	22	1	2	2	54	.20	.038	14	25	.44	98	.09	6	2.02	.01	.06	1	1	5
L56E 26+25N	1	11	11	42	.1	9	6	256	2.14	9	5	ND	2	28	1	2	2	39	.30	.038	19	18	.28	71	.09	3	1.08	.02	.08	1	2	5
L56E 26+00N	1	7	11	48	.1	9	6	216	2.30	3	5	ND	2	21	1	2	5	46	.19	.032	12	21	.27	86	.11	2	1.40	.01	.06	1	1	5
L56E 25+75N	1	10	9	41	.1	8	6	244	2.34	4	5	ND	2	25	1	2	2	46	.22	.030	13	21	.29	98	.12	8	1.11	.02	.07	1	1	5
L56E 25+50N	1	6	9	32	.1	11	4	182	1.64	2	5	ND	2	25	1	2	2	30	.26	.051	16	13	.22	94	.09	6	1.01	.02	.04	1	1	5
L56E 25+25N	1	4	10	34	.1	8	3	190	1.46	2	5	ND	2	25	1	2	2	28	.28	.046	17	13	.24	71	.09	2	.87	.02	.07	1	2	10
L56E 24+75N	1	6	9	35	.1	6	3	171	1.33	2	5	ND	3	21	1	2	2	22	.23	.033	14	13	.24	67	.08	4	.96	.01	.05	1	1	10
L56E 24+50N	1	4	9	37	.1	7	3	155	1.28	2	5	ND	2	21	1	2	2	22	.21	.027	14	11	.24	68	.08	5	.94	.01	.06	1	1	5
L56E 24+25N	1	8	17	52	.1	8	3	227	1.60	2	5	ND	2	27	1	2	2	26	.23	.019	16	16	.31	90	.07	2	1.39	.01	.09	1	12	20
L56E 24+00N	1	9	8	53	.1	9	5	249	2.21	4	5	ND	3	31	1	2	2	33	.28	.045	17	20	.33	101	.07	2	1.56	.02	.09	1	2	30
STD C/AU-S	19	60	40	130	7.1	70	30	1049	3.98	42	17	7	38	50	18	16	18	59	.46	.086	40	59	.95	178	.07	32	1.94	.07	.15	12	50	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L57E 30+00N	1	4	18	35	.1	14	4	180	1.35	2	5	ND	3	23	1	2	2	23	.28	.050	18	25	.22	72	.09	2	1.00	.01	.08	1	1	5
L57E 29+75N	1	4	13	39	.1	10	4	177	1.48	2	5	ND	3	24	1	4	3	26	.25	.032	16	16	.21	81	.05	11	.96	.02	.06	1	7	5
L57E 29+50N	1	9	11	34	.1	8	4	251	1.74	2	5	ND	3	27	1	2	2	31	.28	.049	17	15	.24	85	.10	2	1.06	.02	.07	1	3	5
L57E 29+25N	1	9	11	45	.1	10	6	240	1.90	3	5	ND	3	36	1	2	2	29	.37	.048	18	14	.31	106	.07	5	1.32	.02	.08	1	2	20
L57E 29+00N	1	6	13	42	.1	10	3	189	1.50	2	5	ND	2	23	1	2	3	27	.22	.022	15	17	.23	68	.10	2	.98	.01	.07	1	2	10
L57E 28+75N	1	8	13	33	.1	12	4	195	1.71	2	5	ND	3	25	1	2	2	31	.28	.051	16	18	.23	95	.08	8	1.15	.02	.07	1	3	20
L57E 28+50N	1	5	9	50	.1	8	4	170	1.71	2	5	ND	1	18	1	2	2	29	.16	.033	12	12	.18	82	.07	2	1.23	.01	.05	1	7	5
L57E 28+25N	1	6	10	37	.1	8	4	160	1.42	3	5	ND	3	19	1	2	2	23	.19	.033	13	15	.20	80	.08	2	1.11	.01	.06	1	1	20
L57E 28+00N	1	13	9	92	.1	15	6	200	2.27	6	5	ND	2	25	1	2	3	33	.22	.061	14	17	.24	134	.07	3	2.04	.01	.10	1	1	38
L57E 27+75N	1	12	6	125	.4	11	7	340	2.34	2	5	ND	2	22	1	2	6	37	.22	.099	14	16	.22	108	.07	5	1.66	.01	.09	1	5	20
L57E 27+50N	1	13	14	72	.1	12	8	347	2.52	8	5	ND	3	31	1	2	2	39	.31	.064	19	19	.29	111	.06	2	1.57	.01	.10	1	4	28
L57E 27+25N	1	14	12	64	.2	14	6	248	2.08	2	5	ND	1	28	1	2	3	37	.30	.024	24	17	.26	79	.08	2	1.25	.01	.08	1	1	18
L57E 27+00N	1	10	12	94	.1	16	8	237	2.75	8	5	ND	1	18	1	2	2	50	.24	.088	15	23	.32	72	.08	2	1.55	.01	.05	1	1	5
L57E 26+75N	1	9	14	58	.1	12	5	267	2.43	3	5	ND	1	21	1	2	3	45	.21	.035	14	21	.32	69	.13	2	1.28	.01	.06	1	1	5
L57E 26+50N	1	9	10	49	.1	10	7	320	2.21	3	5	ND	1	25	1	2	2	41	.21	.026	14	20	.28	86	.11	2	1.38	.01	.05	1	1	5
L57E 26+25N	1	7	9	38	.1	9	5	191	1.82	6	5	ND	2	21	1	2	2	33	.22	.041	15	15	.21	81	.08	2	1.03	.01	.07	1	1	5
L57E 26+00N	1	7	10	40	.2	10	6	201	2.05	4	5	ND	2	21	1	2	2	39	.20	.030	15	16	.25	96	.10	2	1.08	.01	.05	1	2	5
L57E 25+75N	1	5	12	31	.1	7	5	143	1.56	2	5	ND	2	21	1	2	2	32	.20	.036	14	18	.17	80	.08	7	.77	.02	.05	1	1	5
L57E 25+50N	1	8	9	48	.1	7	4	154	1.40	2	5	ND	1	24	1	2	3	25	.23	.016	16	15	.19	83	.04	3	1.13	.01	.07	2	1	5
L57E 25+25N	1	4	10	38	.1	6	3	205	1.74	2	5	ND	2	21	1	2	2	31	.22	.038	16	13	.22	67	.08	2	.92	.01	.07	1	1	5
L57E 25+00N	1	5	12	38	.1	7	4	159	1.51	2	5	ND	2	18	1	2	6	28	.16	.021	12	11	.18	61	.08	3	.88	.01	.05	1	1	5
L57E 24+75N	1	10	11	43	.1	8	5	254	2.21	5	5	ND	3	26	1	2	4	36	.27	.043	17	17	.20	96	.08	5	1.42	.02	.07	2	1	5
L57E 24+50N	1	5	17	45	.1	7	5	199	1.81	2	5	ND	2	25	1	2	2	31	.26	.041	16	16	.28	83	.10	4	1.26	.01	.05	1	2	5
L57E 24+25N	1	6	9	52	.1	12	4	194	1.46	2	5	ND	1	24	1	2	3	22	.21	.016	15	22	.27	79	.06	4	1.27	.01	.08	1	1	10
L57E 24+00N	1	7	10	40	.1	10	4	228	1.89	3	5	ND	3	24	1	2	3	33	.27	.054	18	17	.24	92	.08	15	1.29	.02	.07	1	1	5
L58E 30+00N	1	7	12	34	.1	6	4	185	1.69	2	5	ND	2	22	1	2	2	31	.22	.037	14	12	.20	81	.09	2	.97	.01	.06	1	1	10
L58E 29+75N	1	4	12	37	.1	7	3	264	1.60	2	5	ND	2	18	1	2	2	30	.17	.022	13	14	.18	65	.08	2	.93	.01	.04	1	1	5
L58E 29+50N	1	20	14	70	.1	13	8	545	3.04	8	5	ND	6	60	1	2	2	44	.48	.055	30	21	.40	170	.07	7	1.75	.03	.12	1	1	68
L58E 29+25N	1	20	14	75	.1	13	9	639	3.14	13	5	ND	5	61	1	2	2	47	.51	.060	31	21	.43	177	.07	3	1.80	.02	.12	1	2	78
L58E 29+00N	1	21	16	71	.1	16	8	624	3.11	9	5	ND	6	65	1	3	2	45	.54	.061	35	21	.42	175	.06	2	1.75	.02	.14	1	1	60
L58E 28+75N	1	7	11	41	.1	8	5	208	2.15	4	5	ND	2	26	1	2	3	40	.27	.052	17	20	.22	95	.09	4	1.14	.01	.06	1	1	20
L58E 28+25N	1	12	13	50	.1	11	4	366	1.83	4	5	ND	2	34	1	2	6	31	.33	.030	32	17	.26	83	.07	20	1.04	.02	.08	1	1	30
L58E 28+00N	1	8	14	52	.1	10	6	314	2.12	6	5	ND	3	26	1	2	2	38	.27	.055	18	16	.23	85	.08	6	1.09	.01	.08	1	1	10
L58E 27+75N	1	7	10	48	.1	9	6	369	2.19	4	5	ND	1	31	1	2	3	41	.32	.043	17	19	.32	84	.10	4	1.12	.02	.08	1	1	20
L58E 27+50N	1	14	26	183	.3	14	10	603	3.00	7	5	ND	1	54	1	2	2	48	.61	.078	18	26	.31	169	.06	3	1.84	.01	.09	1	2	20
L58E 27+00N	1	6	9	42	.2	11	6	214	2.07	6	5	ND	3	25	1	2	3	38	.24	.042	16	22	.24	84	.09	3	1.10	.01	.05	1	1	10
STD C/AU-S	19	63	40	132	7.4	71	31	1069	4.09	40	18	8	39	52	20	15	19	61	.47	.090	42	61	.88	181	.07	32	1.98	.07	.13	12	52	1300

	SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
	L58E 26+75N	1	8	2	42	.1	6	3	252	2.04	3	5	ND	2	22	1	2	2	33	.27	.054	15	16	.28	92	.08	2	1.24	.01	.05	1	1	10
	L58E 26+50N	1	9	7	57	.1	9	6	277	2.22	4	5	ND	2	19	1	2	2	36	.20	.039	14	14	.24	88	.07	2	1.43	.01	.06	1	1	20
	L58E 26+25N	1	10	2	44	.1	8	5	239	2.24	2	5	ND	3	22	1	2	2	40	.20	.046	15	21	.22	108	.09	4	1.25	.01	.05	1	1	10
"D" Grid	L58E 25+75N	1	11	4	50	.2	11	5	240	2.16	4	5	ND	2	20	1	2	2	35	.24	.040	15	15	.29	83	.08	3	1.22	.01	.06	1	2	5
	L58E 25+50N	1	9	8	47	.3	8	5	238	2.43	3	5	ND	3	20	1	2	2	40	.25	.051	16	17	.28	86	.08	2	1.31	.01	.07	1	3	10
	L58E 25+25N	1	7	12	35	.1	8	3	209	1.79	3	5	ND	2	21	1	2	3	30	.22	.030	13	14	.27	68	.10	2	.99	.01	.05	1	1	5
	L58E 25+00N	1	9	3	39	.1	6	4	193	1.94	2	5	ND	3	19	1	2	4	32	.20	.032	13	15	.24	76	.08	2	1.14	.01	.05	1	1	10
	L58E 24+50N	1	5	2	29	.1	4	1	145	.95	2	5	ND	2	18	1	3	2	17	.20	.024	13	10	.22	62	.08	5	.83	.01	.05	1	3	20
	L58E 24+25N	1	9	12	32	.1	5	4	174	1.51	2	5	ND	3	18	1	2	2	26	.20	.029	13	12	.24	67	.08	3	.97	.01	.05	1	1	5
	L58E 24+00N	1	8	8	34	.1	7	3	193	1.72	3	5	ND	3	19	1	2	4	28	.22	.042	16	13	.24	75	.08	2	1.07	.01	.06	1	1	10
	L74E 37+00N	1	9	10	55	.4	11	5	183	2.27	6	5	ND	4	15	1	2	2	35	.15	.084	12	17	.18	79	.07	5	1.48	.01	.04	1	1	20
	L74E 36+75N	1	4	7	30	.1	4	3	164	1.09	2	5	ND	2	14	1	3	2	23	.14	.014	12	12	.09	55	.08	2	.60	.01	.04	1	1	5
	L74E 36+50N	1	7	8	36	.2	8	4	157	1.25	2	5	ND	1	18	1	2	2	20	.16	.026	13	10	.15	73	.06	2	.97	.01	.05	1	3	20
	L74E 36+25N	1	6	7	44	.1	5	2	119	1.45	5	5	ND	3	11	1	2	2	26	.12	.072	11	11	.12	59	.06	2	1.44	.01	.05	1	1	10
	L74E 36+00N	1	8	2	46	.2	9	6	243	2.13	4	5	ND	3	28	1	2	2	37	.21	.050	13	16	.21	97	.09	2	1.12	.01	.05	1	1	20
	L74E 35+75N	1	3	9	55	.1	4	4	225	1.23	2	5	ND	2	9	1	2	2	22	.11	.029	11	8	.09	43	.07	2	.85	.01	.04	1	3	5
	L74E 35+50N	1	5	13	109	.2	7	4	205	2.02	4	5	ND	3	12	1	2	2	31	.14	.120	12	16	.12	61	.07	2	1.51	.01	.05	1	1	20
	L74E 35+25N	1	8	9	73	.1	6	4	218	2.07	2	5	ND	2	13	1	2	2	36	.13	.076	11	14	.12	67	.07	2	1.21	.01	.05	1	1	10
	L74E 35+00N	1	9	10	111	.2	11	7	177	2.45	3	5	ND	3	12	1	2	3	40	.13	.141	11	22	.14	88	.08	7	1.95	.01	.04	1	3	10
	L74E 34+75N	1	6	23	127	.1	9	6	243	2.57	4	5	ND	3	13	1	2	4	38	.15	.216	12	17	.17	79	.06	2	1.85	.01	.04	2	1	20
	L74E 34+50N	1	4	8	66	.2	8	5	159	1.47	2	5	ND	2	23	1	2	2	25	.28	.034	14	14	.16	62	.07	3	.91	.01	.05	1	1	5
	L74E 34+25N	1	15	5	63	.3	12	7	531	2.48	5	5	ND	1	32	1	2	2	35	.44	.030	22	19	.32	104	.06	6	2.02	.01	.08	1	1	10
"E" Grid	L74E 33+75N	2	32	9	115	.3	23	13	1079	3.87	11	5	ND	1	48	1	2	2	54	.47	.052	95	29	.53	171	.05	2	3.10	.01	.10	1	1	30
	L74E 33+50N	1	12	12	134	.3	13	9	657	3.03	2	5	ND	2	30	1	2	2	56	.32	.059	23	27	.34	78	.17	2	1.32	.01	.05	1	3	10
	L74E 33+25N	1	6	11	48	.1	5	3	150	1.10	2	5	ND	2	18	1	2	2	22	.10	.014	13	8	.11	53	.08	2	.62	.01	.05	1	1	5
	L74E 33+00N	1	7	6	68	.1	5	4	270	2.12	2	5	ND	1	13	1	2	2	37	.09	.095	11	17	.10	56	.07	2	1.10	.01	.04	1	1	5
	L74E 32+75N	1	9	15	71	.5	9	6	265	2.47	7	5	ND	3	13	1	2	2	40	.15	.085	13	17	.19	70	.07	4	1.34	.01	.09	1	1	30
	L74E 32+25N	1	5	5	39	.1	7	2	147	1.28	2	5	ND	1	19	1	2	2	22	.17	.024	14	10	.14	61	.06	5	.87	.01	.05	1	1	30
	L74E 32+00N	1	3	13	38	.1	3	2	151	1.11	2	5	ND	2	12	1	2	2	23	.12	.018	12	8	.09	50	.08	5	.61	.01	.05	1	1	5
	L75E 37+00N	1	6	5	44	.1	7	4	192	1.53	3	5	ND	2	17	1	2	2	29	.15	.036	11	11	.12	84	.07	7	.85	.01	.04	1	1	20
	L75E 36+75N	1	9	6	65	.1	14	7	285	2.51	6	5	ND	2	15	1	2	4	42	.17	.103	11	16	.19	115	.07	2	1.40	.01	.06	1	1	10
	L75E 36+50N	1	7	5	70	.3	8	6	164	2.66	10	5	ND	2	20	1	2	2	44	.16	.092	12	17	.16	93	.07	2	1.76	.01	.04	1	1	20
	L75E 36+25N	1	11	10	64	.3	11	6	184	2.12	7	5	ND	2	16	1	2	2	36	.32	.056	12	15	.15	67	.07	3	1.38	.01	.05	1	1	20
	L75E 36+00N	1	7	4	52	.1	7	2	265	1.80	3	5	ND	1	19	1	2	2	23	.16	.033	11	15	.11	61	.05	2	1.03	.01	.04	1	1	10
	L75E 35+75N	1	5	8	62	.2	6	3	152	1.50	4	5	ND	1	16	1	3	2	26	.12	.052	11	9	.07	50	.05	3	.83	.01	.06	1	1	5
	L75E 35+50N	1	5	16	64	.1	7	5	232	1.97	9	5	ND	2	11	1	2	2	33	.30	.069	11	12	.11	47	.05	2	1.06	.01	.06	1	1	5
	STD C/AU-S	18	64	36	132	7.9	68	30	1111	4.07	41	17	8	36	48	20	16	22	56	.48	.098	38	58	.96	181	.07	34	2.03	.07	.14	12	50	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L75E 35+25N	1	6	22	88	.1	5	3	186	1.87	2	5	ND	2	12	1	2	2	30	.10	.083	11	12	.21	58	.06	2	1.22	.02	.06	1	1	20
L75E 35+00N	1	6	22	88	.2	7	6	234	2.47	3	5	ND	4	10	1	2	2	36	.09	.118	13	15	.17	69	.06	2	2.15	.01	.06	1	1	30
L75E 34+75N	1	8	17	104	.1	11	8	229	2.71	3	5	ND	3	17	1	2	2	40	.13	.132	13	17	.20	85	.07	4	2.45	.01	.07	1	3	40
L75E 34+50N	1	5	19	78	.1	10	6	270	2.41	4	5	ND	2	20	1	2	2	42	.19	.089	11	17	.17	75	.08	2	1.31	.01	.05	1	1	10
L75E 34+25N	1	3	14	61	.1	4	3	134	1.22	2	5	ND	1	18	1	2	4	25	.19	.026	12	10	.10	63	.08	2	.53	.01	.06	1	2	5
L75E 33+75N	1	3	15	37	.1	4	3	125	1.22	2	5	ND	1	17	1	2	4	25	.16	.023	12	11	.13	48	.09	3	.81	.01	.07	2	1	5
L75E 33+50N	1	6	27	51	.1	8	5	185	1.67	3	5	ND	1	15	1	2	2	34	.16	.025	12	16	.17	55	.15	2	.91	.01	.06	1	1	5
L75E 33+25N	1	4	10	32	.1	3	2	94	.87	2	5	ND	1	11	1	2	2	20	.10	.011	12	9	.08	41	.07	2	.47	.01	.05	1	1	5
L75E 32+75N	1	5	17	37	.1	4	3	137	1.22	2	5	ND	1	19	1	2	2	31	.14	.018	11	13	.11	39	.17	3	.55	.01	.06	1	1	5
L75E 32+50N	1	3	15	39	.1	5	3	134	1.32	2	5	ND	1	13	1	2	2	26	.14	.027	12	9	.12	54	.07	2	.84	.01	.05	1	2	5
L75E 32+25N	1	7	11	47	.1	9	5	206	1.79	4	5	ND	2	13	1	2	2	34	.16	.032	11	17	.32	48	.10	2	.99	.01	.11	1	2	10
L75E 32+00N	1	6	12	46	.1	8	5	239	2.01	3	5	ND	2	14	1	2	5	34	.16	.052	13	13	.21	67	.07	2	1.18	.01	.06	1	2	20
L76E 37+00N	1	4	10	28	.1	5	4	101	1.04	2	5	ND	1	18	1	2	2	22	.12	.016	12	9	.09	66	.07	2	.83	.01	.05	1	1	10
L76E 36+75N	1	8	18	101	.1	10	6	256	3.02	8	5	ND	3	30	1	2	4	44	.24	.181	12	17	.26	86	.06	11	2.12	.01	.08	1	1	20
L76E 36+50N	2	10	18	81	.1	13	7	191	3.05	15	5	ND	3	25	1	3	5	47	.18	.110	11	19	.21	113	.06	2	2.90	.01	.05	1	1	40
L76E 36+25N	1	7	21	80	.2	10	6	251	2.14	2	5	ND	1	21	1	2	5	31	.17	.116	13	14	.18	67	.06	4	1.48	.01	.08	1	1	20
L76E 36+00N	5	22	38	125	.5	14	11	1490	3.69	9	5	ND	2	45	1	2	6	48	.37	.057	56	22	.45	145	.03	2	2.91	.01	.14	1	1	20
L76E 35+75N	1	4	9	64	.1	7	4	162	2.07	2	5	ND	1	13	1	2	2	42	.10	.045	11	18	.12	53	.10	2	.99	.01	.03	1	2	10
L76E 35+50N	1	6	23	100	.1	6	4	266	2.17	3	5	ND	3	18	1	2	2	31	.15	.177	12	15	.10	59	.08	3	1.69	.01	.05	1	1	10
L76E 35+25N	1	3	9	70	.1	3	2	354	1.30	2	5	ND	1	9	1	2	2	25	.08	.041	13	12	.06	45	.08	2	.91	.01	.05	1	1	20
L76E 35+00N	1	9	14	66	.2	13	7	193	2.55	4	5	ND	2	13	1	2	4	41	.11	.076	12	18	.20	67	.07	2	2.06	.01	.04	1	2	20
L76E 34+75N	1	6	14	64	.1	11	7	184	2.65	6	5	ND	2	14	1	2	3	42	.12	.098	12	19	.22	75	.08	2	1.96	.01	.05	1	1	30
L76E 34+50N	1	9	13	79	.1	11	7	360	2.52	2	5	ND	1	14	1	2	2	44	.12	.140	10	21	.16	74	.09	2	1.53	.01	.05	1	[illegible]	10
L76E 34+25N	1	3	10	43	.1	3	1	84	1.15	2	6	ND	1	14	1	2	2	25	.11	.029	10	12	.05	43	.10	2	.54	.01	.03	1	13	5
L76E 33+75N	2	23	24	100	.2	23	8	624	2.63	5	5	ND	1	119	1	3	2	30	1.41	.091	94	19	.43	148	.02	2	2.83	.01	.13	1	1	90
L76E 33+50N	2	25	18	89	.3	15	6	368	2.63	6	5	ND	1	73	1	2	3	31	.76	.050	73	20	.40	137	.02	2	2.45	.01	.14	1	[illegible]	100
L76E 33+00N	1	6	13	40	.1	4	3	100	1.05	3	5	ND	1	17	1	2	2	20	.16	.019	15	9	.08	61	.06	2	.66	.01	.07	1	1	10
L76E 32+75N	1	3	11	34	.1	7	4	181	1.23	2	5	ND	2	26	1	2	2	22	.26	.025	16	10	.22	57	.08	2	.79	.02	.05	1	1	5
L76E 32+50N	1	6	11	36	.2	7	4	209	1.42	3	5	ND	3	27	1	2	2	25	.28	.011	18	12	.22	54	.08	2	.91	.02	.08	1	1	5
L76E 32+00N	1	7	10	54	.1	8	6	268	1.60	2	5	ND	1	28	1	2	2	26	.28	.027	24	12	.19	64	.05	2	1.25	.01	.07	1	2	10
L77E 37+00N	1	5	7	34	.1	4	2	112	1.46	2	5	ND	1	11	1	3	3	36	.07	.013	11	19	.04	52	.10	3	.53	.01	.05	1	2	10
L77E 36+75N	1	5	10	71	.1	7	4	206	2.13	2	5	ND	2	10	1	2	2	38	.15	.121	11	15	.11	85	.08	2	1.24	.01	.06	1	1	5
L77E 36+25N	1	4	7	44	.1	4	3	140	1.78	4	5	ND	2	12	1	3	2	36	.12	.039	10	15	.11	48	.08	2	.83	.01	.06	2	1	10
L77E 36+00N	1	6	9	36	.1	4	2	103	1.10	2	5	ND	2	19	1	2	2	21	.15	.019	15	9	.10	54	.06	2	.84	.01	.06	1	1	5
L77E 35+75N	1	4	5	32	.1	2	1	95	.95	2	5	ND	1	12	1	2	2	22	.10	.014	11	7	.04	33	.07	2	.45	.01	.05	1	1	5
L77E 35+50N	1	4	5	34	.2	6	3	122	1.14	2	5	ND	1	13	1	2	2	24	.12	.019	12	10	.12	39	.08	2	.55	.01	.04	1	1	5
STD C/AU-S	19	62	41	132	7.1	71	31	1076	4.07	43	18	8	39	51	19	20	23	60	.48	.090	41	61	.97	180	.07	35	1.97	.07	.14	12	48	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L77E 35+25N	2	5	29	81	.1	6	5	215	2.26	10	5	ND	1	15	1	2	4	34	.13	.121	13	13	.13	66	.05	2	1.24	.01	.04	1	1	20
L77E 35+00N	1	5	18	45	.1	8	4	139	1.59	2	5	ND	1	14	1	2	3	31	.13	.032	10	13	.13	55	.10	2	.89	.01	.03	3	1	10
L77E 34+00N	1	5	12	41	.1	8	2	181	1.34	5	5	ND	1	21	1	2	2	23	.20	.019	18	10	.16	62	.06	4	.80	.01	.06	1	1	5
L77E 33+75N	1	5	18	38	.1	7	3	203	1.56	3	5	ND	1	22	1	2	4	27	.24	.031	15	12	.22	62	.07	8	.91	.01	.05	2	1	5
L77E 33+50N	1	6	18	46	.1	9	4	151	1.90	2	5	ND	1	14	1	2	4	33	.15	.044	12	10	.15	52	.05	2	1.04	.01	.06	1	1	5
L77E 33+25N	1	5	14	34	.1	8	2	130	1.26	2	5	ND	1	21	1	2	5	21	.16	.020	16	9	.16	55	.05	2	.93	.01	.05	1	1	10
L77E 33+00N	1	10	18	76	.1	18	10	575	2.34	3	5	ND	1	22	1	2	2	35	.23	.060	19	15	.24	98	.06	2	1.57	.01	.07	1	1	20
L77E 32+75N	1	5	10	34	.1	5	3	195	1.26	2	5	ND	1	20	1	2	2	21	.20	.017	15	10	.19	57	.06	7	.82	.01	.05	2	1	5
L77E 32+50N	1	14	25	53	.3	19	6	737	2.24	10	5	ND	1	40	1	2	5	32	.40	.037	32	15	.33	88	.04	2	1.78	.01	.09	2	12	20
L77E 32+25N	1	4	11	43	.1	7	2	131	1.51	3	5	ND	1	12	1	2	3	24	.10	.069	13	13	.10	60	.05	2	.92	.01	.04	2	2	5
L77E 32+00N	1	6	21	49	.2	7	4	281	1.68	2	5	ND	2	19	1	2	7	29	.17	.017	21	13	.21	61	.08	2	1.00	.01	.03	1	41	5
L78E 36+50N	1	29	26	85	.5	21	7	874	3.07	8	5	ND	1	66	1	2	2	35	.61	.066	65	20	.46	231	.02	2	3.29	.01	.10	1	1	50
L78E 36+25N	1	7	16	40	.1	7	3	293	1.66	3	5	ND	1	27	1	2	2	27	.26	.036	22	12	.23	88	.06	2	1.05	.01	.06	2	1	10
L78E 36+00N	1	7	11	35	.1	7	2	258	1.37	5	5	ND	1	25	1	2	2	22	.24	.014	20	11	.21	69	.05	2	1.02	.01	.05	1	1	5
L78E 35+75N	1	5	12	31	.1	5	2	118	.97	3	5	ND	1	19	1	2	3	17	.18	.015	13	6	.11	35	.05	2	.69	.01	.04	1	1	10
L78E 35+50N	2	32	24	115	.6	23	9	609	3.66	13	5	ND	1	104	1	3	2	38	1.14	.087	95	23	.56	226	.01	2	4.33	.01	.11	1	1	110
L78E 35+00N	1	6	8	45	.1	9	7	462	1.70	2	5	ND	2	25	1	2	2	28	.28	.041	17	11	.23	76	.07	2	.95	.01	.07	1	1	10
L78E 34+75N	1	4	10	41	.1	4	3	127	1.20	3	5	ND	1	15	1	2	2	22	.14	.016	15	9	.14	50	.07	2	.65	.01	.04	1	1	5
STD C/AU-S	20	59	40	131	7.1	70	30	1110	4.10	43	18	8	37	47	20	22	19	59	.48	.089	38	62	.96	169	.07	33	2.03	.06	.13	11	50	1400
L78E 34+50N	1	9	12	90	.1	9	4	381	2.25	4	5	ND	1	17	1	2	3	37	.18	.046	15	16	.23	75	.08	2	1.25	.01	.05	1	1	5
L78E 34+25N	1	4	5	62	.1	8	1	177	1.56	2	5	ND	1	14	1	2	2	26	.13	.031	14	10	.14	55	.05	2	.85	.01	.04	1	1	5
L78E 34+00N	1	7	5	59	.1	8	4	319	1.90	2	5	ND	2	18	1	2	2	31	.15	.054	18	14	.20	69	.05	2	1.23	.01	.04	1	1	5
L78E 33+75N	1	5	7	44	.1	4	2	196	1.36	2	5	ND	2	11	1	2	2	27	.13	.029	11	11	.10	47	.06	2	.66	.01	.05	1	1	5
L78E 33+50N	1	7	13	77	.2	10	4	307	1.97	2	5	ND	2	19	1	2	4	30	.17	.046	13	12	.21	79	.06	2	1.39	.01	.05	1	1	5
L78E 33+25N	1	4	14	54	.1	9	4	182	1.61	2	5	ND	1	15	1	2	2	28	.14	.022	12	12	.18	48	.07	2	.95	.01	.03	2	1	5
L78E 33+00N	1	4	17	60	.1	7	5	452	1.34	2	5	ND	2	20	1	2	2	23	.21	.031	14	8	.16	66	.06	2	.83	.01	.06	1	3	5
L78E 32+75N	1	8	12	51	.2	8	3	180	1.59	2	5	ND	1	18	1	2	2	25	.17	.025	14	12	.28	66	.05	2	1.09	.01	.07	1	1	10
L78E 32+50N	1	12	14	51	.2	13	6	521	2.03	5	5	ND	1	34	1	4	2	28	.35	.021	43	14	.28	93	.04	2	1.67	.01	.09	2	1	30
L78E 32+25N	1	6	12	53	.1	8	3	185	2.10	2	5	ND	3	16	1	2	4	36	.17	.053	13	12	.19	66	.07	4	1.08	.01	.04	1	1	10
L78E 32+00N	1	6	9	40	.2	6	2	157	1.47	2	5	ND	2	11	1	2	2	27	.13	.019	11	12	.18	40	.09	2	.69	.01	.04	1	1	5
L79E 37+00N	1	5	15	68	.1	8	4	222	1.86	2	5	ND	1	17	1	2	2	31	.19	.049	12	12	.20	77	.07	2	.91	.01	.06	1	1	5
L79E 36+75N	1	9	16	68	.2	9	5	331	1.91	2	5	ND	2	25	1	2	2	30	.27	.032	36	12	.29	73	.11	2	1.09	.02	.05	1	1	5
L79E 36+50N	1	6	11	56	.1	7	3	201	1.56	2	5	ND	2	20	1	2	5	27	.27	.019	38	12	.20	62	.07	2	1.03	.01	.05	1	1	5
L79E 36+25N	1	6	10	65	.1	6	6	245	1.86	2	5	ND	1	19	1	2	3	30	.23	.025	16	13	.22	73	.06	2	1.30	.01	.04	1	1	5
L79E 36+00N	1	11	15	80	.2	15	5	368	2.57	8	5	ND	1	20	1	2	2	38	.21	.049	17	16	.31	80	.05	2	1.86	.01	.06	1	1	10
L79E 35+75N	1	8	12	54	.2	9	3	179	1.63	2	5	ND	2	18	1	2	2	26	.18	.037	13	12	.20	62	.07	2	1.02	.01	.05	1	1	10
L79E 35+50N	1	9	15	45	.1	7	3	222	1.78	2	5	ND	1	26	1	2	2	29	.30	.048	23	13	.21	65	.06	2	1.00	.01	.05	1	1	5

"E" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L79E 35+25N	1	9	11	70	.3	9	4	267	2.14	2	5	ND	1	18	1	2	2	29	.22	.037	22	16	.23	77	.05	2	1.45	.01	.08	1	1	20
L79E 35+00N	1	9	15	83	.1	7	4	440	2.07	4	5	ND	1	20	1	2	2	29	.20	.023	19	13	.27	68	.05	3	1.31	.01	.06	1	1	10
L79E 34+75N	1	10	14	69	.2	9	4	322	2.06	2	5	ND	1	28	1	2	2	27	.36	.031	22	15	.33	94	.05	6	1.43	.01	.07	2	2	10
L79E 34+50N	1	6	12	50	.1	7	4	213	1.95	4	5	ND	2	22	1	2	2	27	.28	.018	17	14	.27	75	.06	4	1.28	.01	.05	1	1	5
L79E 34+25N	1	9	9	44	.1	10	3	257	2.04	3	5	ND	2	19	1	2	2	29	.24	.017	19	13	.25	66	.07	5	1.15	.01	.05	2	1	5
L79E 34+00N	1	6	10	56	.1	8	4	207	1.96	2	5	ND	2	19	1	2	2	26	.28	.015	13	13	.24	53	.07	4	1.16	.01	.05	1	1	5
L79E 33+75N	1	8	17	69	.1	10	4	267	2.38	2	5	ND	2	21	1	2	2	38	.26	.030	16	17	.30	68	.10	6	1.46	.01	.05	1	1	5
L79E 33+50N	1	6	15	39	.1	9	3	194	2.00	2	5	ND	2	18	1	2	2	31	.25	.024	15	17	.24	50	.08	2	1.09	.01	.05	1	1	5
L79E 33+25N	1	8	19	48	.1	8	4	212	2.27	2	5	ND	1	22	1	2	2	35	.28	.024	15	19	.30	75	.09	2	1.47	.01	.03	2	1	5
L79E 33+00N	1	8	14	49	.1	16	6	216	2.68	6	5	ND	2	25	1	2	6	45	.26	.033	13	27	.35	78	.12	2	1.56	.01	.04	1	2	10
L79E 32+75N	1	8	12	54	.1	18	4	207	2.35	3	5	ND	2	10	1	2	2	37	.25	.030	12	16	.31	60	.09	2	1.30	.01	.04	1	1	10
L79E 32+50N	1	9	16	94	.1	17	5	354	3.04	6	5	ND	2	14	1	2	2	43	.18	.063	15	22	.32	85	.07	2	2.14	.01	.06	1	2	20
L79E 32+25N	1	7	7	71	.1	8	4	235	2.35	4	5	ND	3	17	1	2	2	34	.21	.038	13	17	.31	76	.07	2	1.07	.01	.07	1	1	5
L79E 32+00N	1	5	12	70	.2	10	4	322	2.19	5	5	ND	2	17	1	2	2	32	.21	.046	14	15	.22	66	.08	4	1.48	.01	.06	1	1	5
L80E 37+00N	1	5	12	58	.1	4	1	137	1.82	2	5	ND	2	16	1	2	2	28	.26	.035	12	15	.11	42	.09	9	.68	.01	.07	1	1	5
L80E 36+75N	1	5	13	40	.1	5	3	176	1.97	3	5	ND	2	18	1	3	2	32	.26	.031	15	13	.22	53	.09	7	1.09	.01	.04	1	2	5
L80E 36+50N	1	4	11	42	.1	5	3	171	1.75	2	5	ND	2	10	1	2	2	26	.30	.012	14	13	.23	54	.09	7	1.08	.01	.05	3	1	5
L80E 36+25N	1	5	9	52	.1	7	3	167	1.70	2	5	ND	2	14	1	2	2	26	.20	.014	13	11	.21	51	.07	3	1.07	.01	.05	1	1	50
L80E 36+00N	1	6	10	44	.2	7	3	158	1.72	2	5	ND	3	14	1	2	5	26	.21	.017	14	12	.18	49	.08	3	.97	.01	.05	2	1	10
L80E 35+75N	1	3	12	47	.1	3	3	193	1.51	2	5	ND	2	14	1	2	2	24	.20	.016	14	10	.13	46	.07	3	.87	.01	.06	2	1	5
L80E 35+50N	1	4	6	46	.1	3	3	181	1.51	2	5	ND	1	16	1	2	2	22	.21	.017	14	10	.17	53	.06	5	.97	.01	.06	2	1	5
L80E 35+25N	1	7	8	46	.2	6	2	162	1.87	5	5	ND	2	20	1	2	5	28	.23	.024	14	11	.20	57	.08	2	.98	.01	.07	2	1	10
L80E 35+00N	1	8	10	53	.2	5	3	198	2.23	3	5	ND	1	32	1	2	2	31	.36	.059	17	14	.21	75	.06	5	1.22	.01	.09	1	1	20
L80E 34+75N	1	9	12	54	.3	6	3	232	2.31	9	5	ND	3	25	1	2	2	36	.31	.043	17	15	.27	72	.07	2	1.21	.01	.07	1	[illegible]	10
L80E 34+50N	1	9	11	88	.2	7	5	306	2.35	3	5	ND	2	17	1	2	3	32	.19	.051	17	15	.23	65	.05	3	1.42	.01	.06	1	2	5
L80E 34+25N	1	5	10	49	.2	5	4	195	1.82	2	5	ND	2	14	1	2	3	26	.17	.012	14	13	.24	53	.07	2	1.05	.01	.06	1	2	5
L80E 34+00N	1	7	6	46	.1	5	2	166	1.78	2	5	ND	2	16	1	2	2	25	.21	.022	13	16	.22	45	.07	3	1.09	.01	.08	2	2	10
L80E 33+75N	1	9	17	62	.1	12	5	244	2.48	4	5	ND	3	21	1	2	7	40	.28	.035	14	23	.40	65	.11	4	1.54	.01	.05	1	4	10
L80E 33+50N	1	9	15	69	.1	10	6	674	2.58	5	5	ND	1	21	1	2	2	38	.25	.038	17	16	.32	82	.05	4	1.75	.01	.06	1	1	10
L80E 33+25N	1	8	14	53	.2	8	4	241	2.31	6	5	ND	2	21	1	2	2	35	.30	.029	19	17	.32	73	.08	2	1.59	.01	.06	1	1	20
L80E 33+00N	1	5	12	47	.1	7	3	227	2.12	2	5	ND	2	18	1	3	2	33	.25	.029	13	14	.26	63	.09	2	1.28	.01	.05	2	1	5
L80E 32+75N	1	5	13	50	.1	5	3	156	1.94	2	5	ND	2	19	1	4	2	34	.24	.019	15	16	.16	55	.10	4	1.13	.01	.08	1	1	5
L80E 32+50N	1	6	11	47	.1	5	2	246	1.78	2	5	ND	2	17	1	2	3	23	.24	.019	15	13	.24	60	.07	2	1.22	.01	.05	1	1	5
L80E 32+25N	1	6	25	71	.1	10	3	239	2.39	2	5	ND	3	15	1	2	2	44	.10	.025	12	20	.27	60	.17	2	1.50	.01	.05	1	2	10
L80E 32+00N	1	6	12	41	.1	10	3	179	1.84	2	5	ND	3	17	1	2	2	28	.20	.015	11	16	.26	52	.11	2	1.21	.01	.08	1	1	60
L81E 37+00N	1	4	13	46	.3	5	3	148	1.95	2	5	ND	3	11	1	2	2	32	.15	.026	11	14	.15	55	.08	2	1.06	.01	.05	1	1	10
STD C/AU-S	19	61	42	129	7.4	67	28	1066	4.01	37	17	8	40	50	18	20	19	59	.53	.088	41	61	.95	178	.07	33	1.92	.07	.15	12	47	1300

"E" Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L01E 36+75N	1	2	10	36	.2	3	3	155	1.47	2	5	ND	1	15	1	3	3	29	.19	.018	13	14	.17	44	.09	2	.79	.01	.04	1	5	5
L01E 36+50N	1	4	10	43	.3	10	5	332	1.49	2	5	ND	1	19	1	2	3	27	.24	.018	20	11	.14	56	.06	2	1.05	.01	.07	1	1	10
L01E 36+25N	1	6	12	47	.2	7	6	227	1.80	2	5	ND	2	20	1	2	2	31	.23	.048	11	13	.15	67	.07	2	1.21	.01	.06	1	1	5
L01E 35+50N	1	2	10	35	.2	7	4	123	1.20	2	5	ND	2	13	1	2	2	23	.13	.017	13	10	.13	46	.07	2	.64	.01	.05	1	3	10
L01E 35+25N	1	4	7	39	.2	5	5	167	1.56	2	5	ND	1	19	1	2	2	27	.18	.030	14	12	.21	58	.08	2	.93	.01	.05	1	2	5
L01E 35+00N	1	5	7	37	.3	8	4	240	1.47	4	5	ND	2	25	1	2	2	25	.24	.031	17	12	.19	69	.07	2	.81	.01	.06	2	1	5
L01E 34+75N	1	4	13	43	.3	5	4	140	1.53	2	5	ND	1	21	1	4	2	27	.21	.025	14	13	.14	51	.06	3	.86	.01	.05	1	[illegible]	5
L01E 34+50N	1	6	7	53	.4	7	5	198	1.64	3	5	ND	1	21	1	2	4	27	.21	.035	17	14	.18	60	.05	2	.98	.01	.06	1	3	5
L01E 34+25N	1	4	13	44	.3	6	5	203	1.64	2	5	ND	1	20	1	3	4	27	.18	.041	18	14	.21	74	.07	2	1.03	.01	.06	1	4	10
L01E 34+00N	1	6	5	53	.2	16	5	292	1.76	3	5	ND	1	32	1	2	4	28	.26	.022	25	29	.25	86	.04	5	1.31	.01	.05	1	1	20
L01E 33+75N	1	2	8	42	.1	7	5	160	1.53	2	5	ND	1	17	1	2	2	26	.15	.023	14	11	.26	53	.06	7	.99	.01	.04	1	2	20
L01E 33+50N	1	8	15	57	.3	8	5	157	2.17	2	5	ND	1	12	1	2	2	40	.10	.034	11	15	.18	58	.07	2	1.23	.01	.05	1	1	10
L01E 33+25N	1	10	18	74	.3	12	8	290	2.62	2	5	ND	1	23	1	2	2	45	.25	.046	15	21	.38	69	.10	2	1.67	.01	.06	1	4	20
L01E 33+00N	1	4	9	39	.2	8	4	153	1.34	2	5	ND	2	16	1	2	3	24	.18	.018	15	12	.20	47	.07	3	.92	.01	.05	2	1	5
L01E 32+75N	1	5	12	58	.4	9	4	190	1.65	2	5	ND	2	10	1	2	3	27	.14	.053	13	17	.16	50	.05	3	1.31	.01	.05	1	3	5
L01E 32+50N	1	8	13	67	.2	13	6	277	2.78	2	5	ND	2	20	1	2	2	56	.17	.032	13	25	.51	69	.13	6	1.60	.01	.05	1	1	5
L01E 32+25N	1	6	9	58	.2	38	7	552	2.34	2	5	ND	2	17	1	3	5	37	.16	.037	12	28	.23	59	.10	3	1.43	.01	.03	1	1	5
L01E 32+00N	1	6	7	56	.1	26	7	310	2.48	3	5	ND	2	19	1	2	2	42	.17	.037	11	22	.27	78	.11	2	1.86	.01	.04	1	1	10
L02E 37+00N	1	10	9	76	.1	14	6	202	2.51	2	5	ND	1	15	1	2	2	36	.28	.082	11	30	.37	52	.05	2	1.03	.01	.07	1	1	20
L02E 36+75N	1	4	8	46	.1	4	3	121	1.36	3	5	ND	1	9	1	2	4	23	.09	.033	11	12	.15	40	.03	4	1.11	.01	.06	1	1	5
L02E 36+50N	2	8	9	174	.1	8	7	532	2.58	2	5	ND	1	13	1	2	5	40	.17	.052	12	22	.28	85	.05	4	2.08	.01	.08	1	1	40
L02E 36+25N	1	4	3	58	.1	7	4	162	2.16	6	5	ND	2	16	1	2	2	35	.18	.062	14	14	.17	65	.06	10	1.42	.01	.06	1	1	10
L02E 36+00N	1	4	7	64	.3	6	4	185	1.60	2	5	ND	1	13	1	2	3	26	.14	.018	15	13	.21	60	.05	9	1.20	.01	.05	1	[illegible]	10
L02E 35+75N	1	4	6	55	.3	5	3	157	1.46	2	5	ND	2	12	1	2	3	29	.11	.025	13	11	.12	53	.06	2	.91	.01	.06	1	1	5
L02E 35+50N	1	5	5	47	.2	5	3	161	1.68	2	5	ND	2	15	1	2	2	28	.14	.038	13	12	.20	72	.07	3	1.16	.01	.04	1	1	20
L02E 35+25N	1	4	9	65	.2	5	5	283	1.91	2	5	ND	2	19	1	2	3	32	.20	.064	14	15	.14	60	.06	2	1.24	.01	.04	1	1	5
L02E 35+00N	1	2	10	48	.2	4	3	143	1.60	2	5	ND	2	12	1	2	2	29	.14	.038	12	14	.16	42	.07	2	1.06	.01	.04	1	1	10
L02E 34+75N	1	6	9	39	.1	6	1	164	1.55	3	5	ND	2	14	1	2	2	28	.15	.022	13	13	.19	50	.08	6	.91	.01	.04	1	1	5
L02E 34+50N	1	8	13	99	.1	19	11	663	2.97	5	5	ND	2	23	1	2	2	47	.21	.092	15	20	.37	108	.12	3	2.23	.01	.08	1	2	20
L02E 34+25N	1	7	16	78	.2	17	9	325	2.83	6	5	ND	3	18	1	3	2	44	.16	.055	16	17	.29	95	.10	2	2.28	.01	.04	1	1	30
L02E 34+00N	1	8	21	114	.2	15	8	468	2.51	2	5	ND	1	14	1	3	2	51	.20	.051	11	20	.37	80	.13	2	2.14	.01	.06	1	1	20
L02E 33+75N	1	7	11	51	.2	13	6	186	2.25	6	5	ND	3	11	1	2	2	38	.12	.036	14	16	.23	52	.09	2	1.59	.01	.04	1	1	10
L02E 33+50N	1	5	8	46	.2	11	6	191	2.23	5	5	ND	3	16	1	2	2	37	.14	.041	13	16	.20	79	.07	2	1.67	.01	.04	1	1	30
L02E 33+25N	1	7	11	72	.3	8	5	236	2.03	4	5	ND	2	16	1	2	2	35	.16	.041	18	16	.22	61	.06	3	1.65	.01	.07	1	1	10
L02E 33+00N	1	7	13	73	.4	13	6	441	2.40	5	5	ND	1	18	1	2	2	43	.19	.064	20	16	.23	84	.10	3	1.35	.01	.04	1	1	20
L02E 32+75N	1	9	11	84	.2	11	6	380	2.21	6	5	ND	1	23	1	2	2	34	.20	.055	22	17	.26	85	.05	2	1.67	.01	.06	1	1	30
STD C/AU-S	19	61	36	132	7.3	67	30	1063	4.01	45	18	8	38	50	18	16	25	58	.47	.091	40	60	.96	179	.07	31	1.94	.07	.14	11	50	1400

E' Grid

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
L82E 32+50N	1	7	15	72	.1	9	5	241	2.31	6	5	ND	2	15	1	2	4	35	.14	.076	14	17	.22	62	.03	2	1.81	.01	.09	1	1	30
L82E 32+25N	2	8	12	82	.4	12	6	200	2.54	11	5	ND	3	10	1	2	2	41	.08	.079	15	21	.17	68	.06	2	2.17	.01	.05	1	3	50
L82E 32+00N	10	6	17	55	.3	5	1	180	1.48	13	5	ND	1	11	1	2	3	25	.05	.039	25	15	.07	45	.02	2	1.30	.01	.06	1	5	30

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUN 23 1988 DATE REPORT MAILED: July 1/88 ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT-620 File # 88-2196 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L35+50E 44+00N	1	10	13	37	.1	8	5	190	1.91	6	5	ND	1	22	1	2	2	37	.21	.032	13	16	.27	73	.10	2	1.06	.01	.07	2	1	20
OLD L35+50E 43+75N	1	25	24	94	.1	16	16	2786	4.10	23	12	ND	4	64	1	2	2	62	.56	.097	35	25	.49	227	.02	2	3.63	.02	.12	1	1	40
OLD L35+50E 43+50N	1	10	12	42	.1	5	3	189	1.58	6	5	ND	2	22	1	2	2	31	.21	.027	13	11	.21	80	.08	7	.92	.02	.04	1	1	10
OLD L35+50E 43+25N	1	14	6	43	.1	4	5	229	2.20	11	5	ND	3	25	1	2	3	42	.27	.063	15	15	.25	86	.06	4	1.14	.01	.08	1	1	20
OLD L35+50E 43+00N	1	13	12	52	.2	7	5	217	2.16	11	14	ND	3	16	1	2	4	40	.15	.054	14	15	.20	88	.06	2	1.42	.01	.06	1	2	20
OLD L35+50E 42+75N	1	9	13	48	.2	3	3	165	1.69	4	13	ND	4	21	1	2	6	33	.21	.028	15	14	.24	78	.05	12	.97	.02	.04	2	25	10
OLD L35+50E 42+50N	1	11	13	46	.1	9	7	213	2.36	12	5	ND	3	18	1	2	2	43	.16	.067	13	18	.29	128	.08	5	1.97	.01	.08	1	1	20
OLD L35+50E 42+25N	1	7	11	42	.1	5	4	153	1.64	19	5	ND	1	17	1	2	2	31	.17	.031	12	11	.21	74	.07	5	1.04	.01	.02	1	1	10
OLD L35+50E 42+00N	1	8	16	51	.9	5	3	136	1.59	64	5	ND	3	17	1	2	2	28	.15	.038	14	12	.18	79	.06	10	1.01	.01	.05	1	1	40
OLD L35+50E 41+75N	2	36	25	156	.8	17	6	438	3.30	34	12	ND	1	129	1	2	2	29	2.07	.074	207	18	.44	211	.01	2	3.59	.02	.16	1	1	150
OLD L35+50E 41+50N	1	5	13	95	.1	6	4	180	1.99	17	5	ND	1	16	1	2	2	33	.14	.049	15	12	.22	99	.05	5	1.53	.01	.05	1	1	5
OLD L35+50E 41+25N	1	12	14	72	.1	6	4	200	2.16	14	5	ND	4	27	1	2	2	36	.24	.061	16	13	.24	99	.05	6	1.46	.02	.08	1	1	10
OLD L35+50E 41+00N	1	7	12	76	.1	6	4	256	1.78	9	5	ND	1	19	1	2	2	30	.16	.036	15	12	.20	85	.04	8	1.16	.01	.05	1	3	20
OLD L36+50E 44+00N	1	6	10	41	.1	4	3	155	1.58	6	5	ND	1	21	1	2	2	26	.16	.031	13	10	.18	88	.05	13	1.11	.01	.03	1	1	10
OLD L36+50E 43+75N	1	6	9	52	.1	4	3	200	1.66	7	5	ND	2	22	1	2	2	29	.18	.052	13	12	.19	90	.05	6	1.12	.01	.05	1	1	20
OLD L36+50E 43+50N	1	17	11	59	.2	7	6	2067	1.84	15	13	ND	2	130	1	2	3	26	1.75	.060	22	10	.27	154	.01	2	1.16	.01	.10	1	1	70
OLD L36+50E 43+25N	1	8	17	54	.1	9	4	177	1.92	19	5	ND	5	17	1	2	4	30	.14	.067	13	13	.21	109	.05	2	1.73	.01	.06	1	1	30
OLD L36+50E 43+00N	1	9	11	40	.1	6	5	165	2.00	22	5	ND	1	18	1	2	2	33	.14	.064	13	11	.21	96	.05	7	1.59	.01	.06	1	1	30
OLD L36+50E 42+75N	1	14	9	47	.1	5	4	355	2.10	45	5	ND	5	57	1	5	2	36	.40	.055	22	15	.24	123	.07	2	.90	.03	.10	2	2	90
OLD L36+50E 42+50N	3	9	13	57	1.6	5	2	152	1.84	122	5	ND	3	20	1	4	9	29	.17	.060	15	11	.17	113	.03	9	1.39	.01	.05	1	1	60
OLD L36+50E 42+25N	1	10	11	72	.6	9	4	374	2.14	40	5	ND	2	40	1	2	2	29	.51	.045	35	13	.31	119	.03	2	1.64	.02	.10	1	1	50
OLD L36+50E 42+00N	1	10	16	66	.1	10	5	398	2.04	23	5	ND	1	38	1	2	2	34	.36	.032	54	13	.28	114	.04	9	1.29	.02	.08	1	1	70
OLD L36+50E 41+75N	1	10	11	60	.1	7	4	314	1.85	9	5	ND	1	28	1	2	3	33	.27	.015	34	13	.26	77	.06	9	1.01	.02	.05	1	3	20
OLD L36+50E 41+50N	1	9	14	53	.1	5	5	316	1.89	12	5	ND	3	31	1	2	2	32	.29	.012	128	13	.26	86	.06	9	1.05	.02	.06	1	2	30
OLD L36+50E 41+25N	1	7	12	95	.1	2	5	269	1.66	8	5	ND	1	14	1	2	4	28	.11	.064	14	11	.12	74	.03	2	1.09	.01	.05	1	1	30
OLD L36+50E 41+00N	1	4	19	115	.1	4	3	998	1.72	5	5	ND	3	10	1	2	4	27	.09	.085	14	11	.14	79	.04	2	1.28	.01	.06	1	1	20
OLD L37+50E 42+75N	5	32	34	129	.8	20	6	214	3.72	33	11	ND	4	129	1	2	2	38	2.00	.068	426	22	.39	249	.01	2	4.23	.01	.15	1	6	280
OLD L37+50E 42+50N	2	20	26	106	.1	15	7	478	2.63	37	5	ND	5	47	1	2	3	34	.59	.020	269	17	.38	109	.03	2	2.18	.02	.12	1	2	90
OLD L37+50E 42+25N	1	8	9	82	.1	12	4	490	2.25	19	5	ND	2	34	1	5	2	32	.36	.028	36	15	.34	117	.03	2	1.63	.01	.09	1	11	50
OLD L37+50E 42+00N	1	6	7	52	.2	8	6	193	2.20	22	7	ND	1	22	1	3	3	37	.20	.055	15	14	.22	95	.05	2	1.34	.01	.09	1	4	40
OLD L37+50E 41+75N	1	6	10	64	.1	10	6	188	2.30	11	5	ND	3	15	1	2	6	40	.13	.058	10	15	.21	101	.05	2	1.47	.01	.04	1	6	20
OLD L37+50E 41+50N	1	3	13	128	.3	6	4	278	1.78	5	5	ND	4	16	1	2	2	30	.16	.065	12	11	.15	96	.03	2	1.10	.01	.12	1	1	20
OLD L37+50E 41+25N	1	5	9	110	.1	5	3	422	1.66	4	5	ND	2	15	1	2	2	30	.12	.050	11	13	.14	83	.05	5	.96	.01	.04	1	1	10
OLD L37+50E 41+00N	1	5	13	130	.1	6	5	194	2.12	7	5	ND	3	17	1	2	2	39	.12	.030	11	13	.19	66	.07	6	1.09	.01	.07	1	3	20
OLD L38+00E 41+75N	6	3	18	142	.1	7	4	402	3.13	33	5	ND	1	10	1	4	2	26	.13	.058	9	8	.31	67	.01	4	1.60	.01	.05	1	1	20
OLD L38+00E 41+50N	1	7	10	72	.1	6	3	332	2.09	7	5	ND	2	25	1	3	4	36	.22	.017	15	13	.17	63	.05	6	1.16	.01	.06	1	1	10
STD C/AU-S	18	57	42	131	7.0	70	30	1077	4.01	42	19	6	36	48	18	17	18	59	.46	.084	40	59	.91	180	.07	34	1.33	.07	.14	13	49	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L38+00E 41+25N	1	7	6	57	.1	7	5	224	2.12	5	5	ND	2	29	1	2	2	39	.30	.011	30	15	.24	71	.07	16	1.24	.02	.05	1	1	20
OLD L38+00E 41+00N	4	22	42	197	.2	23	9	1351	3.98	32	5	ND	1	66	1	2	4	47	.85	.035	222	26	.53	195	.01	2	4.80	.01	.14	1	3	100
OLD L38+00E 40+75N	1	6	14	110	.1	4	5	311	1.94	9	5	ND	1	20	1	2	2	34	.20	.021	22	11	.17	74	.05	4	1.29	.01	.04	1	1	20
OLD L38+00E 40+50N	1	4	16	172	.1	4	3	1063	1.86	11	5	ND	1	14	1	2	2	37	.14	.021	14	14	.15	99	.05	3	1.06	.01	.05	1	1	10
OLD L38+50E 42+75N	1	29	30	138	.1	15	9	1211	3.88	20	5	ND	1	93	1	2	3	45	1.26	.034	99	22	.49	208	.01	2	3.90	.02	.16	1	1	50
OLD L38+50E 42+50N	1	7	11	50	.1	5	5	292	1.89	10	5	ND	1	30	1	3	2	34	.27	.023	15	14	.23	78	.06	16	.99	.02	.04	1	1	20
OLD L38+50E 42+25N	1	5	10	43	.1	8	3	176	1.47	3	5	ND	2	27	1	2	3	29	.24	.018	21	10	.20	77	.07	13	.91	.02	.04	1	43	10
OLD L38+50E 42+00N	1	8	9	45	.1	4	4	201	1.70	5	5	ND	3	12	1	2	2	39	.10	.014	11	13	.13	46	.07	9	.80	.01	.06	1	1	5
OLD L38+50E 41+75N	1	9	24	75	.2	10	5	406	2.61	21	5	ND	2	44	1	2	6	37	.54	.022	50	17	.29	104	.04	12	2.32	.02	.06	1	1	30
OLD L38+50E 41+50N	1	11	22	73	.1	6	5	556	2.54	16	5	ND	2	55	1	2	2	37	.67	.015	105	15	.26	108	.04	5	1.96	.02	.05	1	1	40
OLD L38+50E 41+25N	1	9	14	80	.1	7	4	247	1.82	6	5	ND	1	27	1	3	2	33	.30	.012	26	13	.24	78	.06	15	1.24	.02	.05	1	1	10
OLD L38+50E 41+00N	1	8	10	49	.1	6	4	592	1.93	8	5	ND	3	28	1	2	2	34	.29	.011	22	13	.23	73	.07	9	1.10	.02	.07	1	1	20
OLD L51+00E 39+75N	1	5	7	34	.1	5	3	156	1.37	[illegible]	5	ND	3	21	1	2	2	27	.22	.025	13	10	.18	69	.07	2	.93	.01	.06	1	[illegible]	10
OLD L51+00E 39+50N	1	6	5	45	.1	5	3	230	1.37	3	5	ND	1	15	1	2	3	28	.21	.035	14	10	.18	64	.07	13	1.06	.01	.04	1	[illegible]	20
OLD L51+00E 39+25N	1	9	10	99	.1	8	6	1296	1.81	2	5	ND	1	26	1	2	2	31	.35	.112	15	14	.27	165	.05	11	1.30	.01	.08	1	[illegible]	30
OLD L51+00E 39+00N	1	7	6	40	.1	6	4	200	1.63	6	5	ND	3	18	1	2	2	33	.20	.025	13	11	.16	65	.06	10	.87	.01	.06	1	[illegible]	20
OLD L51+00E 38+75N	1	8	8	31	.1	7	3	212	1.41	10	5	ND	2	22	1	2	3	27	.29	.041	18	11	.22	63	.07	20	.77	.02	.07	1	[illegible]	20
OLD L51+00E 38+50N	1	10	17	52	.1	10	5	599	1.92	5	5	ND	1	30	1	2	2	31	.34	.033	32	15	.28	90	.04	8	1.38	.01	.05	1	[illegible]	30
OLD L51+00E 38+25N	1	6	10	32	.1	6	4	197	1.59	6	5	ND	2	18	1	3	2	29	.22	.036	14	10	.20	71	.08	8	.95	.01	.04	1	[illegible]	30
OLD L51+00E 38+00N	1	9	9	43	.1	5	5	358	1.64	6	5	ND	1	24	1	2	2	29	.25	.033	19	14	.24	85	.06	11	1.27	.02	.05	1	[illegible]	20
OLD L51+00E 37+75N	11	20	12	117	.3	37	20	3866	4.57	18	5	ND	1	189	1	2	2	48	2.06	.153	63	19	.33	272	.01	4	3.13	.01	.11	1	2	260
OLD L51+00E 37+50N	1	17	13	131	.1	14	6	404	1.70	3	5	ND	1	180	1	2	2	18	2.32	.074	48	14	.30	172	.01	2	2.02	.01	.07	1	1	90
OLD L51+00E 37+25N	1	9	18	62	.1	9	6	595	2.19	4	5	ND	1	26	1	2	2	42	.20	.035	13	21	.25	80	.12	2	1.34	.01	.03	1	1	20
OLD L51+00E 37+00N	1	9	11	69	.2	10	4	326	2.28	7	5	ND	2	12	1	2	3	35	.11	.133	11	16	.16	94	.05	12	1.71	.01	.07	1	1	10
OLD L51+00E 36+75N	1	8	11	81	.1	8	6	555	2.21	2	5	ND	1	16	1	3	2	39	.13	.111	10	17	.14	95	.08	6	1.43	.01	.04	1	3	20
OLD L51+00E 36+50N	1	7	14	61	.2	8	3	205	1.68	2	5	ND	4	13	1	2	2	30	.10	.073	11	12	.12	78	.06	7	1.59	.01	.08	1	2	30
OLD L51+00E 36+25N	1	7	8	56	.1	8	5	571	1.77	3	5	ND	1	24	1	2	2	35	.21	.029	15	14	.23	79	.08	10	1.29	.01	.05	1	1	10
OLD L51+00E 36+00N	1	9	10	138	.1	12	6	199	2.42	6	5	ND	2	13	1	3	2	37	.11	.129	11	17	.16	92	.05	7	2.01	.01	.06	2	2	30
OLD L51+00E 35+75N	1	4	7	41	.1	8	4	290	1.52	2	5	ND	3	32	1	2	2	30	.28	.044	18	12	.25	98	.10	13	.98	.02	.06	1	18	10
OLD L51+00E 35+50N	1	4	10	39	.1	6	4	202	1.38	3	5	ND	2	20	1	3	2	28	.17	.028	12	11	.16	76	.07	10	.81	.01	.07	2	1	30
OLD L51+00E 35+25N	1	3	18	32	.1	5	3	134	1.19	2	5	ND	1	21	1	2	3	24	.19	.035	12	10	.18	72	.07	2	.76	.01	.07	2	2	10
OLD L51+00E 35+00N	1	4	9	34	.1	5	4	109	1.59	3	5	ND	1	15	1	2	2	29	.12	.070	11	12	.13	83	.05	7	1.28	.01	.06	2	1	20
OLD L51+00E 34+75N	1	8	7	35	.5	6	3	119	1.34	4	5	ND	2	24	1	2	2	27	.19	.031	14	12	.16	79	.07	17	.90	.02	.06	2	2	10
OLD L51+00E 34+50N	1	6	10	81	.1	12	5	190	2.30	5	5	ND	4	13	1	2	2	37	.11	.128	10	16	.16	97	.06	6	1.74	.01	.06	1	1	20
OLD L51+00E 34+25N	1	13	17	85	.1	12	7	645	2.30	4	5	ND	1	49	1	2	2	41	.43	.043	41	20	.27	122	.09	8	1.55	.02	.07	1	1	30
OLD L51+00E 34+00N	1	6	11	90	.2	8	5	400	2.08	2	5	ND	1	12	1	3	5	36	.12	.077	10	15	.15	73	.08	5	1.50	.01	.06	1	2	20
STD C/AU-S	18	58	44	131	6.8	67	29	1064	3.99	44	21	8	36	47	17	17	19	58	.45	.086	39	58	.90	176	.06	33	1.92	.07	.15	13	50	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L51+00E 33+75N	1	8	13	84	.2	11	5	673	1.63	2	5	ND	4	15	1	3	4	29	.15	.044	12	22	.16	67	.07	3	1.19	.01	.05	1	1	20
OLD L51+00E 33+50N	1	4	12	74	.3	8	4	307	1.69	3	5	ND	5	15	1	3	3	32	.15	.036	11	33	.14	72	.08	18	1.07	.01	.05	1	1	10
OLD L51+00E 33+25N	1	10	18	62	.1	6	3	391	1.87	7	5	ND	2	23	1	3	2	32	.23	.051	16	17	.18	80	.05	8	.87	.01	.07	1	1	30
OLD L51+00E 33+00N	1	12	20	56	.1	9	4	443	1.90	6	5	ND	1	51	1	2	2	29	.60	.050	73	16	.24	113	.04	10	1.79	.02	.05	1	2	40
OLD L51+00E 32+75N	1	7	14	60	.2	8	3	377	1.44	2	5	ND	3	17	1	2	7	25	.16	.020	12	12	.19	63	.07	12	1.09	.01	.02	1	1	20
OLD L51+00E 32+50N	1	9	16	66	.1	9	3	467	1.55	2	5	ND	3	18	1	2	2	30	.19	.024	12	15	.18	61	.08	4	.99	.01	.05	1	1	5
OLD L51+00E 32+25N	1	9	14	56	.3	7	5	740	1.65	3	5	ND	4	25	1	2	2	30	.23	.036	14	16	.19	89	.06	9	1.09	.01	.05	1	2	20
OLD L51+00E 32+00N	1	9	16	58	.1	10	5	214	2.00	3	5	ND	4	17	1	2	2	31	.16	.074	12	15	.21	100	.07	9	1.67	.01	.05	1	1	10
OLD L51+00E 29+50N	1	10	13	67	.1	6	4	256	1.83	6	5	ND	2	39	1	2	2	29	.42	.053	18	13	.27	99	.05	15	1.30	.02	.05	1	1	30
OLD L51+00E 29+25N	1	6	20	65	.1	7	3	178	1.58	2	5	ND	2	16	1	2	2	28	.17	.035	13	13	.20	66	.06	12	1.27	.01	.03	1	1	20
OLD L51+00E 29+00N	1	10	14	67	.1	11	4	397	1.99	5	5	ND	2	21	1	2	2	35	.21	.037	12	18	.27	72	.09	2	1.47	.01	.05	1	1	10
OLD L51+00E 23+00N	1	9	7	67	.1	7	4	341	2.06	2	5	ND	4	17	1	2	2	35	.18	.057	12	15	.20	114	.06	7	1.54	.01	.05	1	1	20
OLD L51+00E 22+75N	1	7	16	59	.4	6	5	904	1.60	2	5	ND	2	33	1	2	2	30	.24	.028	15	12	.18	122	.05	9	1.14	.01	.05	1	1	30
OLD L51+00E 22+50N	1	10	17	67	.2	12	4	243	2.02	2	5	ND	2	20	1	2	2	36	.20	.040	14	20	.33	87	.07	9	1.67	.01	.04	1	1	30
OLD L51+00E 22+25N	1	10	18	74	.4	12	6	299	2.18	9	5	ND	4	14	1	4	2	35	.14	.074	11	17	.25	97	.06	16	1.89	.01	.05	1	2	20
OLD L51+00E 20+00N	1	6	11	44	.3	5	4	194	1.68	4	9	ND	2	20	1	3	2	30	.18	.030	12	14	.23	76	.07	10	1.17	.01	.05	1	1	10
OLD L51+00E 19+75N	1	8	9	50	.1	8	4	502	1.74	3	5	ND	1	21	1	2	2	31	.18	.040	11	14	.22	77	.06	9	1.30	.01	.03	1	1	20
OLD L51+00E 19+50N	1	5	8	47	.1	6	2	188	1.44	6	5	ND	1	19	1	2	2	26	.17	.023	11	11	.18	65	.06	2	1.01	.01	.06	1	1	10
OLD L51+00E 19+25N	1	5	10	44	.1	9	3	203	1.71	2	5	ND	1	18	1	2	3	32	.17	.033	12	14	.23	74	.08	16	1.14	.02	.04	1	2	10
OLD L54+00E 38+50N	1	7	11	63	.1	15	7	263	2.77	8	5	ND	2	16	1	3	2	50	.16	.063	9	22	.28	113	.09	2	2.00	.01	.03	1	1	20
OLD L54+00E 38+25N	1	8	16	129	.2	10	6	402	2.83	10	5	ND	4	15	1	2	3	41	.14	.145	10	37	.20	122	.07	4	2.88	.01	.06	1	1	40
OLD L54+00E 38+00N	1	8	9	77	.1	6	5	269	2.03	6	5	ND	3	15	1	2	2	32	.17	.065	11	14	.19	79	.05	10	1.59	.01	.05	1	1	20
OLD L54+00E 37+75N	1	9	13	69	.1	12	5	203	2.23	8	5	ND	2	15	1	3	2	35	.15	.069	11	14	.19	100	.05	2	1.77	.01	.04	1	1	20
OLD L54+00E 37+50N	1	8	6	27	.1	7	3	144	1.30	3	5	ND	5	24	1	2	5	25	.24	.035	14	12	.19	80	.07	2	.81	.02	.07	1	1	20
OLD L54+00E 37+00N	1	9	10	64	.5	8	4	184	1.77	11	7	ND	5	17	1	3	2	30	.13	.061	11	15	.18	97	.05	3	1.54	.01	.07	1	2	30
OLD L54+00E 36+75N	1	10	8	37	.1	5	4	229	1.85	9	5	ND	4	14	1	2	2	35	.13	.033	12	14	.16	73	.07	2	1.08	.01	.04	1	1	20
OLD L54+00E 36+50N	1	8	15	125	.1	8	4	254	2.10	5	5	ND	2	10	1	2	2	31	.10	.082	12	14	.37	78	.06	2	1.98	.01	.05	1	1	10
OLD L54+00E 36+25N	1	7	12	59	.1	6	4	630	1.70	2	5	ND	4	10	1	2	2	29	.09	.053	11	11	.12	72	.05	2	1.20	.01	.04	1	1	20
OLD L54+00E 36+00N	1	8	10	43	.1	6	3	162	1.44	3	5	ND	2	21	1	3	2	27	.19	.032	12	12	.20	90	.07	2	1.11	.01	.04	1	1	10
OLD L54+00E 35+75N	1	12	18	78	.1	10	5	448	2.13	10	5	ND	1	36	1	2	2	35	.39	.038	26	19	.21	127	.04	2	1.66	.01	.05	1	1	30
OLD L54+00E 35+50N	1	9	9	78	.1	7	3	263	1.72	8	5	ND	2	11	1	2	2	28	.10	.068	11	14	.10	63	.05	2	1.41	.01	.03	1	1	20
OLD L54+00E 35+25N	1	5	6	34	.3	9	1	124	.97	7	10	ND	3	18	1	2	2	17	.18	.023	11	15	.18	70	.05	2	.93	.01	.06	2	1	30
OLD L54+00E 35+00N	1	7	11	38	.1	6	2	143	1.15	3	5	ND	1	19	1	2	2	20	.19	.026	13	11	.19	68	.06	2	.95	.01	.05	1	1	20
OLD L54+00E 34+75N	1	5	7	38	.2	6	2	137	1.32	3	5	ND	3	15	1	2	2	26	.16	.023	12	14	.17	62	.07	2	.87	.01	.05	1	1	10
OLD L54+00E 34+50N	1	5	10	36	.1	7	2	145	1.33	2	5	ND	1	16	1	2	2	24	.17	.031	13	16	.18	67	.07	2	.98	.01	.03	1	1	20
OLD L54+00E 34+25N	1	8	15	127	.1	9	5	313	2.64	10	9	ND	5	16	1	2	2	35	.14	.191	14	15	.20	136	.04	2	1.98	.01	.08	1	2	30
STD C/AU-S	17	62	42	132	6.6	69	31	1085	4.08	44	19	8	38	47	18	16	20	59	.46	.080	41	61	.92	180	.07	33	1.96	.07	.14	12	52	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L54+00E 34+00N	1	2	13	60	.1	4	3	168	1.86	5	5	ND	3	12	1	2	7	28	.11	.067	10	11	.14	70	.05	2	1.44	.01	.02	1	1	20
OLD L54+00E 33+75N	1	3	15	36	.1	4	2	89	.80	2	5	ND	1	10	1	2	2	14	.10	.013	11	8	.16	54	.04	2	1.05	.01	.01	1	5	10
OLD L54+00E 33+50N	1	4	16	94	.1	10	4	174	1.87	10	5	ND	1	10	1	2	2	27	.09	.065	11	13	.21	107	.04	2	2.13	.01	.03	1	1	30
OLD L54+00E 33+25N	1	6	18	81	.4	16	5	161	2.35	4	5	ND	4	11	1	2	5	32	.10	.046	19	21	.42	90	.04	2	2.10	.01	.07	1	1	20
OLD L54+00E 33+00N	1	8	14	60	.1	7	3	151	1.90	4	5	ND	2	13	1	2	2	29	.11	.050	11	12	.20	107	.05	2	1.79	.01	.04	1	1	30
OLD L54+00E 32+75N	1	2	10	44	.1	6	4	151	1.58	3	5	ND	1	15	1	2	2	28	.14	.029	11	11	.19	74	.06	2	1.12	.01	.02	3	1	10
OLD L54+00E 32+50N	1	3	15	51	.5	4	3	180	1.34	6	5	ND	2	21	1	2	7	23	.20	.031	15	10	.21	77	.05	4	1.02	.01	.07	2	1	20
OLD L54+00E 32+25N	1	7	21	90	.1	7	3	137	1.91	6	5	ND	1	15	1	2	2	26	.12	.056	12	12	.19	93	.04	2	1.93	.01	.03	1	1	30
OLD L54+00E 32+00N	1	6	18	57	.3	6	2	124	1.42	6	5	ND	3	14	1	2	11	24	.13	.029	12	10	.15	73	.05	6	1.05	.01	.04	1	1	20
OLD L54+00E 31+75N	1	6	10	45	.1	7	2	160	1.26	2	5	ND	1	15	1	2	2	22	.14	.016	12	11	.19	64	.05	4	.82	.01	.01	1	1	10
OLD L54+00E 31+50N	1	8	20	87	.3	14	8	948	2.93	6	5	ND	1	45	1	2	3	39	.51	.032	26	22	.72	131	.05	2	2.39	.02	.11	1	1	30
OLD L54+00E 31+25N	1	5	12	44	.2	4	3	140	1.37	3	5	ND	1	18	1	2	2	24	.20	.031	13	10	.20	73	.05	7	.98	.01	.03	2	1	10
OLD L54+00E 31+00N	1	22	31	159	.1	16	9	1819	3.76	7	5	ND	1	50	1	2	2	45	.60	.065	39	23	.59	204	.02	2	3.83	.02	.17	1	1	30
OLD L54+00E 30+75N	1	6	11	45	.2	4	2	114	1.25	3	5	ND	1	13	1	2	3	21	.11	.029	11	10	.14	71	.03	3	1.15	.01	.05	2	2	20
OLD L54+00E 30+50N	1	1	10	74	.3	5	2	132	1.49	2	5	ND	2	19	1	2	2	24	.19	.050	12	11	.18	94	.04	2	1.23	.01	.08	1	1	20
OLD L54+00E 30+25N	1	8	12	58	.1	6	3	136	1.49	3	5	ND	1	12	1	2	3	24	.15	.036	11	11	.16	70	.04	4	1.29	.01	.03	1	1	10
OLD L54+00E 30+00N	1	8	21	80	.1	10	5	184	2.38	8	5	ND	3	15	1	2	3	32	.13	.082	14	14	.25	133	.04	2	2.62	.01	.05	1	1	30
OLD L54+00E 29+75N	1	5	17	91	.1	4	4	342	1.55	2	5	ND	1	95	1	3	2	24	.50	.036	20	11	.24	123	.03	6	1.33	.01	.07	1	1	20
OLD L54+00E 29+50N	1	8	16	54	.1	8	4	189	1.96	7	5	ND	2	10	1	2	2	31	.09	.062	12	14	.20	94	.05	2	1.52	.01	.05	1	1	20
OLD L54+00E 29+25N	1	2	10	46	.1	4	3	112	1.14	2	5	ND	1	12	1	2	2	20	.13	.027	11	8	.15	59	.05	5	.92	.01	.04	1	1	10
OLD L54+00E 29+00N	1	6	11	70	.2	7	4	149	1.77	5	5	ND	1	15	1	2	2	28	.15	.066	14	13	.21	99	.05	2	1.53	.01	.04	1	1	20
OLD L54+00E 22+75N	1	2	13	39	.1	6	4	185	1.49	4	5	ND	3	18	1	2	2	27	.22	.035	16	12	.25	66	.06	2	.97	.01	.06	1	16	10
OLD L54+00E 22+50N	1	4	9	39	.1	7	3	148	1.24	2	5	ND	1	16	1	2	2	21	.16	.020	13	10	.22	60	.05	2	.90	.01	.05	1	6	40
OLD L54+00E 22+25N	1	5	13	46	.4	6	4	146	1.42	2	5	ND	1	17	1	2	2	27	.18	.023	12	12	.25	61	.08	2	.93	.01	.05	1	1	10
OLD L54+00E 22+00N	1	6	14	64	.1	10	4	281	2.19	6	5	ND	1	21	1	2	2	40	.22	.036	13	19	.37	73	.09	2	1.43	.01	.05	1	1	20
OLD L54+00E 21+75N	1	3	15	40	.1	5	4	164	1.49	4	5	ND	2	17	1	2	2	28	.19	.026	13	11	.23	59	.07	12	.96	.01	.03	1	1	10
OLD L54+00E 21+50N	1	8	11	39	.4	6	3	159	1.51	4	5	ND	1	15	1	2	12	27	.17	.030	13	12	.23	69	.06	2	1.04	.01	.05	1	1	20
OLD L54+00E 21+25N	1	2	10	43	.1	6	3	141	1.51	3	5	ND	1	15	1	2	2	28	.15	.020	12	15	.22	66	.06	3	1.00	.01	.03	1	3	10
OLD L54+00E 21+00N	1	5	8	38	.1	4	3	144	1.55	2	5	ND	1	15	1	2	2	28	.16	.027	14	10	.21	63	.06	11	.95	.01	.04	1	1	20
OLD L54+00E 20+75N	1	7	11	43	.1	5	3	134	1.48	6	5	ND	1	14	1	2	2	27	.14	.021	12	12	.21	62	.06	2	1.00	.01	.05	1	1	20
OLD L54+00E 20+50N	1	20	21	133	.1	22	12	1349	3.85	8	5	ND	2	49	1	2	2	56	.40	.063	31	33	.55	210	.01	2	4.09	.01	.19	1	1	40
OLD L54+00E 20+25N	1	10	12	42	.1	9	4	219	2.05	4	5	ND	2	22	1	2	2	40	.23	.037	17	17	.26	84	.08	2	1.03	.01	.06	1	1	10
OLD L54+00E 20+00N	1	4	10	36	.1	4	3	184	1.36	3	5	ND	1	18	1	2	2	26	.20	.026	13	13	.24	62	.07	13	.85	.01	.05	1	1	20
OLD L57+00E 37+50N	1	6	11	48	.1	5	4	291	1.40	4	5	ND	1	19	1	3	3	25	.21	.036	14	10	.24	68	.05	11	.97	.01	.06	1	2	20
OLD L57+00E 37+25N	1	5	13	53	.2	5	4	266	1.39	2	5	ND	1	15	1	2	5	24	.16	.031	13	8	.20	60	.04	6	1.01	.01	.05	1	1	10
OLD L57+00E 37+00N	1	8	10	49	.1	5	3	188	1.63	5	5	ND	1	17	1	2	2	27	.21	.042	15	11	.23	65	.04	11	1.12	.01	.06	1	1	20
STD C/AU-S	18	63	42	132	7.2	72	31	1042	4.12	44	21	8	36	48	18	17	21	61	.47	.082	41	59	.93	179	.07	32	1.97	.07	.16	12	50	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L57+00E 36+75N	1	2	16	47	.1	2	2	245	1.38	3	5	ND	2	16	1	3	2	26	.16	.026	16	11	.16	73	.06	8	.94	.01	.02	1	1	20
OLD L57+00E 36+50N	1	3	9	52	.1	1	2	169	1.31	2	5	ND	1	15	1	2	3	23	.15	.034	13	9	.14	64	.05	2	.89	.01	.04	1	1	40
OLD L57+00E 36+25N	1	13	17	91	.1	11	6	496	2.24	10	5	ND	1	39	1	2	3	34	.35	.060	30	20	.29	136	.03	2	2.30	.01	.08	1	1	40
OLD L57+00E 36+00N	1	19	33	122	.1	12	9	923	3.04	9	5	ND	1	46	1	4	2	43	.44	.058	28	19	.43	200	.02	2	3.09	.02	.16	1	2	30
OLD L57+00E 35+75N	2	15	27	131	.1	13	10	1188	3.40	9	5	ND	1	50	1	3	2	43	.51	.067	31	18	.58	175	.03	7	3.16	.02	.12	1	1	40
OLD L57+00E 35+50N	1	10	17	77	.4	6	7	1163	2.12	9	7	ND	1	38	1	4	2	28	.35	.052	33	10	.26	125	.03	5	1.42	.02	.12	1	1	30
OLD L57+00E 35+25N	1	8	18	81	.3	6	3	268	1.55	3	5	ND	1	33	1	3	3	24	.26	.044	20	15	.17	115	.03	2	1.25	.01	.08	1	1	30
OLD L57+00E 35+00N	1	7	12	55	.1	5	2	185	1.26	5	5	ND	1	18	1	2	2	24	.21	.025	12	9	.17	59	.06	7	.68	.01	.07	1	2	10
OLD L57+00E 34+75N	1	5	17	58	.2	5	4	558	1.60	3	5	ND	1	36	1	3	2	27	.39	.031	26	13	.23	98	.04	5	1.18	.01	.07	1	1	30
OLD L57+00E 34+50N	1	6	17	63	.1	6	6	881	1.70	2	5	ND	1	38	1	5	2	28	.37	.040	20	14	.23	118	.04	3	1.24	.01	.07	1	1	20
OLD L57+00E 34+25N	1	9	11	57	.3	6	5	385	1.55	2	5	ND	2	31	1	2	2	27	.32	.027	19	12	.25	82	.05	2	.95	.01	.06	1	2	20
OLD L57+00E 34+00N	1	15	23	93	.1	14	9	1821	2.83	13	5	ND	1	40	1	7	2	39	.37	.079	34	18	.35	166	.03	3	2.33	.01	.09	1	1	60
OLD L57+00E 33+75N	1	5	12	39	.1	6	3	206	1.55	6	5	ND	1	19	1	2	4	28	.20	.028	14	11	.26	69	.07	2	.99	.01	.04	1	1	20
OLD L57+00E 33+50N	1	8	13	52	.1	7	5	342	1.68	7	5	ND	1	20	1	2	7	30	.19	.021	16	12	.24	72	.06	4	1.10	.01	.04	1	2	20
OLD L57+00E 33+25N	1	8	13	54	.1	6	4	205	1.84	3	5	ND	1	16	1	2	2	33	.14	.023	13	14	.23	74	.07	11	1.20	.01	.04	1	1	10
OLD L57+00E 33+00N	1	6	15	49	.1	5	4	148	1.49	3	5	ND	1	15	1	2	2	30	.15	.018	11	10	.17	59	.06	15	.88	.01	.02	1	2	10
OLD L57+00E 32+75N	1	7	13	46	.1	5	3	129	1.38	4	5	ND	1	14	1	3	2	26	.14	.015	12	10	.14	56	.05	5	.89	.01	.05	2	1	10
OLD L57+00E 32+50N	1	17	26	91	.1	12	10	972	3.15	15	5	ND	1	33	1	6	2	46	.29	.043	28	17	.36	153	.03	3	2.37	.01	.12	1	1	30
OLD L57+00E 32+25N	1	6	15	41	.1	2	2	131	1.06	2	6	ND	1	13	1	2	2	19	.12	.020	15	9	.10	57	.04	12	.72	.01	.05	2	1	10
OLD L57+00E 32+00N	1	9	16	51	.1	7	3	144	1.51	2	5	ND	1	22	1	2	2	25	.20	.026	16	16	.18	77	.04	2	1.14	.01	.05	2	2	30
OLD L57+00E 31+75NA	1	3	11	43	.1	4	3	131	1.32	2	5	ND	1	14	1	2	2	25	.14	.029	12	10	.14	64	.06	2	.91	.01	.03	2	1	20
OLD L57+00E 31+75NB	1	8	22	72	.1	14	5	997	1.95	4	5	ND	1	34	1	3	2	31	.34	.042	28	16	.26	110	.04	11	1.60	.01	.07	1	1	10
OLD L57+00E 31+50N	1	9	19	72	.1	7	4	630	1.87	5	5	ND	1	29	1	2	2	30	.29	.032	24	14	.25	96	.05	16	1.49	.01	.07	1	1	20
OLD L57+00E 31+25N	1	4	17	44	.1	3	3	170	1.19	2	5	ND	1	17	1	2	4	23	.19	.015	13	9	.17	53	.06	18	.74	.01	.05	2	2	10
OLD L57+00E 31+00N	1	8	14	73	.1	9	5	528	1.81	3	5	ND	1	26	1	2	2	30	.25	.033	18	13	.24	88	.04	9	1.56	.01	.07	1	1	30
OLD L57+00E 30+75N	1	18	38	127	.1	14	15	2060	4.08	12	5	ND	1	50	1	3	2	59	.48	.109	36	20	.44	209	.02	2	3.70	.01	.15	1	2	30
OLD L57+00E 30+50N	1	5	18	51	.1	3	4	372	1.26	2	5	ND	1	15	1	3	2	23	.13	.025	15	10	.13	66	.04	13	.83	.01	.04	2	1	20
OLD L57+00E 30+25N	1	5	10	52	.1	5	3	154	1.31	4	5	ND	1	22	1	2	2	20	.21	.034	22	10	.18	75	.03	10	1.23	.01	.05	2	1	30
OLD L57+00E 30+00N	1	8	9	47	.4	7	3	166	1.19	2	5	ND	3	17	1	2	2	20	.18	.021	15	9	.20	62	.06	15	.93	.01	.08	2	1	20
OLD L57+00E 29+75N	1	12	22	90	.1	13	5	495	2.01	8	5	ND	1	38	1	2	2	26	.32	.055	45	16	.28	136	.02	9	2.25	.01	.10	1	1	40
OLD L57+00E 29+50N	1	7	16	46	.1	5	3	145	1.28	2	5	ND	1	39	1	2	5	22	.20	.027	15	9	.18	67	.05	12	.96	.01	.04	1	1	20
OLD L57+00E 29+25N	1	5	11	48	.2	8	3	150	1.12	3	6	ND	1	20	1	2	2	20	.21	.019	14	10	.21	68	.07	13	.90	.01	.04	2	1	20
OLD L57+00E 29+00N	1	8	15	48	.3	7	4	158	1.53	3	5	ND	1	19	1	2	2	27	.20	.031	13	12	.21	65	.06	6	1.14	.01	.07	3	2	20
→ OLD L57+00E 28+75N	1	7	10	46	.1	6	2	191	1.62	4	5	ND	1	19	1	2	3	28	.22	.040	14	12	.23	70	.05	13	1.13	.01	.04	2	1	20
OLD L60+00E 39+75N	1	9	15	78	.1	8	4	808	1.81	8	5	ND	1	17	1	2	2	30	.17	.042	16	11	.20	75	.04	5	1.20	.01	.05	1	1	20
OLD L60+00E 39+50N	1	9	15	66	.1	7	3	225	1.58	3	5	ND	1	18	1	2	2	28	.17	.029	15	13	.22	66	.05	8	1.15	.01	.03	1	2	10
STD C/AU-S	18	60	44	131	6.7	70	29	1067	3.99	43	20	8	36	47	18	16	18	59	.45	.081	40	38	.91	180	.07	32	1.91	.07	.16	13	51	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L60+00E 39+25N	1	9	8	49	.2	10	3	207	1.51	6	11	ND	3	17	1	2	6	28	.19	.031	14	13	.22	60	.06	4	1.05	.01	.05	1	1	10
OLD L60+00E 39+00N	1	10	9	48	.3	5	3	175	1.48	4	5	ND	1	17	1	2	2	27	.18	.020	12	11	.21	53	.06	4	.99	.01	.05	1	1	20
OLD L60+00E 38+75N	1	5	8	40	.3	6	3	191	1.44	3	5	ND	1	18	1	2	3	27	.20	.032	13	10	.24	57	.06	2	.96	.01	.07	1	1	20
OLD L60+00E 38+50N	1	9	4	69	.3	7	5	399	1.94	8	10	ND	2	20	1	2	2	30	.19	.035	16	11	.29	79	.04	2	1.68	.01	.10	1	2	30
OLD L60+00E 38+25N	1	6	12	43	.2	5	3	175	1.34	4	9	ND	1	16	1	2	2	24	.15	.021	13	8	.21	56	.06	2	.96	.01	.07	2	1	10
OLD L60+00E 38+00N	1	7	12	55	.1	5	5	369	1.58	6	5	ND	1	16	1	2	6	26	.16	.028	15	9	.19	63	.04	2	1.16	.01	.05	1	2	20
OLD L60+00E 37+75N	1	7	7	50	.1	16	4	239	1.69	4	5	ND	1	13	1	2	4	29	.15	.022	12	21	.69	52	.07	2	1.19	.01	.07	1	1	5
OLD L60+00E 37+50N	1	6	6	47	.1	4	1	165	1.32	2	5	ND	1	14	1	3	2	24	.13	.020	12	10	.18	51	.05	3	.98	.01	.05	1	1	10
OLD L60+00E 37+25N	1	5	6	37	.2	3	3	136	1.27	3	10	ND	5	13	1	2	5	22	.13	.016	13	9	.17	52	.05	6	.89	.01	.06	1	1	10
OLD L60+00E 37+00N	1	7	13	67	.2	7	6	642	1.77	5	5	ND	3	23	1	2	2	29	.19	.042	19	12	.19	84	.04	4	1.21	.01	.07	1	1	30
OLD L60+00E 36+75N	1	6	6	36	.1	3	2	127	1.05	2	5	ND	2	13	1	2	6	20	.13	.016	12	8	.13	45	.05	2	.74	.01	.07	1	1	10
OLD L60+00E 36+50N	1	6	12	47	.1	5	3	136	1.32	3	5	ND	1	14	1	2	2	22	.14	.021	13	9	.18	64	.05	3	1.08	.01	.05	1	2	20
OLD L60+00E 36+25N	1	5	8	40	.1	5	2	134	1.17	3	5	ND	2	17	1	2	2	21	.18	.030	14	8	.17	60	.06	4	.93	.01	.04	1	1	10
OLD L60+00E 36+00N	1	13	27	121	.2	11	11	1254	3.20	8	5	ND	3	41	1	2	2	54	.40	.070	20	17	.36	154	.03	2	2.87	.02	.09	1	1	30
OLD L60+00E 35+75N	1	4	13	53	.1	4	2	136	1.24	2	5	ND	2	15	1	2	2	23	.15	.016	12	9	.17	56	.07	3	.94	.01	.03	1	1	10
OLD L60+00E 35+50N	1	4	9	42	.1	7	3	130	.97	3	5	ND	2	18	1	2	2	18	.19	.024	12	12	.19	63	.06	6	.87	.01	.04	1	1	20
OLD L60+00E 35+25N	1	13	6	76	.5	7	5	461	1.61	3	5	ND	2	49	1	2	2	25	.60	.033	31	13	.29	110	.02	3	1.63	.01	.08	1	1	40
OLD L60+00E 35+00N	2	32	18	151	.2	22	10	891	4.23	5	5	ND	4	63	1	2	2	46	.63	.066	56	29	.56	269	.01	5	4.99	.02	.19	1	1	90
OLD L60+00E 34+75N	1	3	10	43	.2	4	3	152	1.26	2	8	ND	4	18	1	5	3	22	.21	.031	14	10	.24	60	.06	12	1.00	.01	.07	1	1	30
OLD L60+00E 34+50N	1	11	13	75	.4	9	5	295	2.19	5	5	ND	1	19	1	4	2	39	.19	.027	14	16	.30	69	.07	3	1.36	.01	.07	1	1	20
OLD L60+00E 34+25N	1	8	12	55	.3	8	4	190	1.76	2	5	ND	2	19	1	2	2	29	.19	.029	15	12	.26	69	.05	14	1.33	.01	.07	1	1	30
OLD L60+00E 34+00N	1	7	9	48	.1	6	5	216	1.60	5	5	ND	1	18	1	2	2	30	.19	.025	14	13	.24	63	.08	2	.99	.01	.03	1	1	10
OLD L60+00E 33+75N	1	7	13	45	.2	7	3	144	1.29	5	9	ND	3	16	1	2	2	21	.18	.026	14	10	.22	55	.06	17	1.08	.01	.08	2	3	20
OLD L60+00E 33+50N	1	14	23	73	.1	8	7	267	2.62	5	5	ND	2	18	1	2	2	51	.17	.031	13	21	.31	70	.11	5	1.55	.01	.05	1	1	30
OLD L60+00E 33+25N	1	11	17	66	.1	12	4	194	2.12	7	5	ND	1	18	1	2	2	35	.16	.026	14	14	.28	94	.05	2	2.09	.01	.08	1	1	20
OLD L60+00E 33+00N	1	3	10	43	.1	5	3	137	1.15	2	5	ND	1	15	1	3	2	21	.16	.016	13	9	.18	52	.07	6	.95	.01	.06	2	1	10
OLD L60+00E 32+75N	1	9	14	50	.1	5	3	156	1.31	2	5	ND	1	15	1	2	2	23	.15	.016	13	9	.22	59	.06	13	1.09	.01	.06	2	1	10
OLD L60+00E 32+50N	1	7	13	42	.1	6	3	162	1.38	2	5	ND	1	18	1	2	2	22	.19	.027	13	11	.23	64	.05	12	1.21	.01	.05	1	2	30
OLD L60+00E 32+25N	1	6	13	49	.1	6	4	167	1.46	2	5	ND	1	15	1	2	5	23	.13	.025	12	10	.24	58	.05	2	1.29	.01	.05	1	1	30
OLD L60+00E 32+00N	1	4	11	40	.3	4	3	146	1.31	3	6	ND	2	15	1	2	2	23	.16	.018	12	11	.20	48	.07	4	.93	.01	.08	1	1	10
OLD L60+00E 31+75N	1	3	8	44	.1	4	4	143	1.45	4	5	ND	1	12	1	3	2	25	.13	.018	12	11	.20	45	.05	13	1.03	.01	.06	1	1	10
OLD L60+00E 31+50N	1	8	13	44	.1	4	4	130	1.32	2	10	ND	1	19	1	3	2	22	.17	.022	15	10	.15	64	.04	11	1.00	.01	.09	2	1	20
OLD L60+00E 31+25N	1	7	13	46	.1	5	4	172	1.71	5	5	ND	1	14	1	2	2	29	.17	.034	14	11	.23	53	.06	10	1.19	.01	.04	2	1	10
OLD L60+00E 31+00N	1	9	6	41	.1	5	3	152	1.33	3	5	ND	1	16	1	2	2	23	.17	.027	14	10	.19	60	.06	2	.87	.01	.05	1	1	20
OLD L60+00E 30+75N	1	10	12	78	.1	9	5	227	1.90	3	8	ND	2	22	1	4	4	29	.21	.031	18	15	.30	93	.04	13	1.82	.01	.12	1	2	30
OLD L60+00E 30+50N	1	5	8	41	.1	4	3	143	1.24	2	5	ND	1	16	1	3	2	21	.17	.021	12	10	.20	53	.06	18	.85	.01	.05	1	1	10
STD C/AU-S	18	62	40	132	7.1	70	30	1046	4.13	42	19	8	37	48	18	17	18	59	.46	.084	40	59	.93	182	.07	31	1.98	.07	.14	12	53	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L60+00E 30+25N	1	9	12	58	.1	8	4	218	1.69	2	5	ND	1	19	1	2	3	27	.18	.023	16	12	.27	71	.05	2	1.28	.01	.03	1	1	30
OLD L60+00E 30+00N	1	6	10	40	.2	4	3	129	1.16	2	5	ND	1	14	1	2	3	22	.15	.016	12	9	.14	50	.05	2	.77	.01	.02	2	1	10
OLD L60+00E 29+75N	1	12	12	62	.4	11	6	426	2.02	6	5	ND	1	22	1	2	2	36	.20	.026	18	14	.25	85	.05	2	1.47	.01	.06	2	1	20
OLD L60+00E 29+50N	1	3	10	46	.1	8	4	206	1.68	2	5	ND	1	19	1	2	2	32	.19	.028	15	12	.24	67	.07	2	1.04	.01	.04	3	1	10
OLD L60+00E 29+25N	1	2	13	54	.1	8	4	198	1.54	2	5	ND	1	17	1	2	3	29	.17	.016	13	10	.22	64	.08	6	1.01	.01	.02	1	1	5
OLD L60+00E 29+00N	1	9	8	48	.2	9	4	198	2.00	5	5	ND	1	22	1	2	2	37	.23	.040	14	13	.24	82	.08	2	1.21	.01	.04	2	1	5
OLD L60+00E 28+75N	1	6	16	42	.1	6	4	199	1.59	4	5	ND	1	16	1	2	3	30	.17	.026	13	10	.21	59	.08	2	.97	.01	.03	2	1	10
OLD L60+00E 28+50N	1	5	9	46	.1	6	4	216	1.63	2	5	ND	1	20	1	2	2	30	.21	.027	14	12	.25	69	.07	2	1.02	.01	.02	2	1	20
OLD L60+00E 28+25N	1	4	12	37	.1	4	4	160	1.26	2	5	ND	1	21	1	2	3	23	.22	.031	15	9	.23	68	.07	2	.85	.01	.04	2	1	10
OLD L60+00E 28+00N	1	8	15	56	.1	8	5	291	1.89	2	5	ND	1	25	1	2	2	32	.27	.036	17	16	.33	85	.07	2	1.38	.01	.05	1	1	20
OLD L60+00E 27+75N	1	4	10	40	.1	4	3	165	1.28	2	5	ND	1	21	1	2	5	23	.21	.027	13	10	.24	67	.08	6	.95	.01	.04	1	12	20
OLD L60+00E 27+50N	1	8	13	56	.1	11	6	312	1.87	5	5	ND	1	25	1	2	2	35	.26	.044	16	14	.30	85	.08	3	1.22	.01	.02	1	1	30
OLD L60+00E 27+25N	1	7	11	43	.1	6	3	197	1.65	3	5	ND	1	19	1	2	2	31	.21	.030	14	12	.25	68	.08	3	1.04	.01	.02	2	2	20
OLD L60+00E 27+00N	1	6	9	45	.1	6	3	185	1.57	2	5	ND	1	20	1	2	2	27	.20	.029	14	11	.23	67	.05	4	1.16	.01	.03	1	1	30
OLD L60+00E 26+75N	1	8	15	59	.1	8	5	311	2.08	2	5	ND	1	19	1	2	2	39	.20	.024	13	18	.33	60	.11	2	1.28	.01	.04	1	1	10
OLD L60+00E 26+50N	1	7	11	70	.1	11	5	252	2.12	2	5	ND	1	23	1	3	2	43	.28	.050	12	16	.32	62	.10	7	1.14	.01	.04	1	1	5
OLD L60+00E 26+25N	1	6	13	69	.1	8	5	310	1.87	3	5	ND	1	25	1	2	2	33	.28	.057	16	13	.27	88	.06	2	1.21	.01	.05	1	1	20
OLD L60+00E 26+00N	1	4	6	51	.1	5	4	202	1.78	2	5	ND	1	19	1	2	2	34	.19	.030	13	13	.22	73	.08	14	1.00	.01	.03	2	1	5
OLD L60+00E 25+75N	1	2	11	44	.1	5	3	164	1.63	3	5	ND	1	14	1	2	3	30	.14	.019	12	11	.20	55	.07	15	1.06	.01	.02	2	1	5
OLD L60+00E 25+50N	1	1	9	27	.1	2	2	111	.80	2	5	ND	1	10	1	2	2	18	.11	.013	11	6	.06	38	.05	3	.55	.01	.04	1	1	5
OLD L60+00E 25+25N	1	13	17	89	.3	17	8	802	2.59	6	5	ND	1	41	1	2	2	41	.46	.038	29	21	.39	147	.03	6	2.46	.01	.11	1	1	30
OLD L60+00E 25+00N	1	3	15	36	.4	7	4	190	1.59	2	5	ND	1	19	1	2	2	30	.22	.040	15	10	.24	72	.07	11	1.01	.01	.05	2	1	10
OLD L60+00E 24+75N	1	4	11	60	.1	10	7	269	2.67	2	5	ND	1	22	1	2	2	55	.22	.029	11	24	.29	81	.12	13	1.57	.01	.03	1	3	20
OLD L60+00E 24+50N	1	8	10	47	.1	3	3	161	1.48	2	5	ND	1	15	1	2	8	27	.15	.019	13	12	.19	59	.05	2	.99	.01	.04	1	1	10
OLD L60+00E 24+25N	1	7	11	64	.2	8	5	269	1.89	2	5	ND	1	22	1	2	2	33	.21	.038	15	13	.26	86	.05	3	1.24	.01	.05	1	1	20
OLD L63+00E 39+75N	1	4	7	51	.1	2	3	219	1.07	2	5	ND	1	13	1	3	2	19	.15	.025	11	7	.14	52	.04	12	.61	.01	.04	1	1	40
OLD L63+00E 39+50N	1	2	7	31	.1	5	2	117	.95	2	5	ND	1	16	1	2	2	20	.15	.013	11	7	.12	47	.06	8	.67	.01	.03	1	1	30
OLD L63+00E 39+25N	1	1	10	31	.1	2	2	139	.99	2	5	ND	1	13	1	2	2	19	.13	.022	10	7	.15	61	.06	4	.87	.01	.01	2	1	20
OLD L63+00E 39+00N	1	1	9	54	.1	5	3	154	1.36	2	5	ND	1	13	1	2	2	29	.14	.037	9	9	.11	60	.06	3	.65	.01	.04	1	1	30
OLD L63+00E 38+75N	1	4	4	59	.1	10	4	348	1.84	2	5	ND	1	13	1	2	2	25	.12	.027	12	19	.36	71	.04	11	.82	.02	.09	1	1	10
OLD L63+00E 38+50N	1	5	10	24	.2	2	1	66	.61	2	5	ND	1	13	1	3	3	13	.11	.020	12	5	.06	46	.04	9	.61	.01	.05	1	1	10
OLD L63+00E 38+25N	1	7	13	59	.5	9	5	255	2.08	9	5	ND	2	17	1	2	2	36	.18	.032	17	17	.33	64	.07	8	1.19	.01	.07	1	1	30
OLD L63+00E 38+00N	1	2	5	35	.1	2	3	112	1.20	3	5	ND	1	15	1	2	2	22	.14	.018	11	8	.14	60	.05	12	.80	.01	.05	1	1	10
OLD L63+00E 37+75N	1	1	12	52	.2	1	2	281	1.38	8	5	ND	1	10	1	1	2	24	.13	.046	11	8	.14	52	.04	7	.99	.01	.04	2	1	20
OLD L63+00E 37+50N	1	3	8	50	.1	2	4	172	1.13	2	5	ND	1	14	1	2	3	18	.11	.022	13	7	.11	54	.04	6	.93	.01	.06	1	33	30
OLD L63+00E 37+25N	1	2	11	40	.2	2	2	126	1.08	2	5	ND	1	14	1	3	2	20	.12	.016	12	8	.14	51	.06	4	.99	.01	.03	1	1	10
STD C/AU-S	18	58	43	132	6.6	71	30	1079	4.04	41	16	7	35	47	18	17	19	59	.46	.086	39	58	.92	178	.07	31	1.92	.07	.15	13	49	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L63+00E 37+00N	1	7	14	47	.2	3	2	113	1.10	2	5	ND	2	15	1	2	2	18	.13	.024	19	10	.13	66	.04	2	.80	.02	.09	1	1	30
OLD L63+00E 36+75N	1	4	13	83	.1	3	1	272	.85	2	5	ND	1	13	1	2	4	18	.13	.017	12	8	.09	77	.06	13	.57	.01	.04	1	1	20
OLD L63+00E 36+50N	1	2	13	38	.1	3	2	135	1.03	2	5	ND	1	14	1	2	4	20	.13	.014	10	9	.14	54	.06	2	.92	.01	.04	1	1	10
OLD L63+00E 36+25N	1	6	11	45	.1	4	2	162	1.19	2	5	ND	2	13	1	2	2	21	.13	.024	12	9	.11	50	.03	2	.94	.01	.07	1	1	20
OLD L63+00E 36+00N	1	12	7	73	.2	9	4	297	2.48	2	5	ND	3	15	1	2	5	64	.25	.077	17	22	.36	60	.08	10	.76	.02	.06	1	2	30
OLD L63+00E 35+75N	1	24	24	115	.1	11	24	1608	3.42	8	5	ND	1	37	1	2	5	48	.35	.072	23	21	.39	162	.01	2	3.31	.02	.11	1	1	40
OLD L63+00E 35+50N	1	11	27	84	.1	12	15	707	3.61	30	5	ND	4	23	1	3	2	55	.21	.050	19	18	.32	137	.02	2	2.45	.02	.17	1	1	10
OLD L63+00E 35+25N	1	6	13	36	.6	5	2	153	1.28	2	5	ND	4	15	1	2	2	25	.14	.012	12	11	.18	56	.07	2	.78	.01	.06	1	1	10
OLD L63+00E 35+00N	1	4	7	28	.1	1	2	106	1.00	2	5	ND	1	13	1	2	3	24	.12	.013	10	8	.08	46	.06	11	.53	.01	.06	1	2	5
OLD L63+00E 34+75N	1	8	16	50	.1	4	3	150	1.39	2	5	ND	1	17	1	2	2	26	.15	.018	15	10	.16	68	.04	2	1.06	.01	.05	1	1	10
OLD L63+00E 34+50N	1	31	30	159	.2	17	14	559	4.14	9	5	ND	2	62	1	2	2	47	.52	.120	35	24	.48	271	.01	2	4.83	.01	.18	1	1	30
OLD L63+00E 34+25N	1	5	10	47	.2	2	2	144	1.27	3	5	ND	1	18	1	2	4	23	.17	.015	12	8	.17	65	.05	2	.92	.01	.08	1	1	5
OLD L63+00E 34+00N	1	6	11	50	.1	8	3	170	1.50	2	5	ND	1	16	1	2	2	23	.17	.023	12	16	.24	66	.04	2	1.36	.01	.04	1	2	20
OLD L63+00E 33+75N	1	3	13	31	.1	2	2	106	1.20	2	5	ND	1	17	1	2	6	22	.16	.017	12	8	.13	57	.04	5	.96	.01	.05	1	1	10
OLD L63+00E 33+50N	1	1	7	39	.1	2	2	197	1.10	2	5	ND	1	11	1	2	2	20	.10	.037	12	9	.09	48	.04	11	.88	.01	.06	1	1	20
OLD L63+00E 33+25N	1	7	13	68	.1	8	5	980	1.92	2	5	ND	1	29	1	2	2	30	.38	.028	28	17	.28	100	.03	2	1.90	.01	.09	1	1	30
OLD L63+00E 33+00N	1	7	18	78	.1	6	4	332	1.86	4	5	ND	1	25	1	2	3	30	.25	.032	19	13	.25	89	.04	2	1.68	.01	.08	1	1	30
OLD L63+00E 32+75N	1	3	9	41	.1	3	2	126	1.07	2	5	ND	1	18	1	2	2	19	.15	.026	17	7	.11	63	.03	2	.93	.01	.05	1	2	20
OLD L63+00E 32+50N	1	7	7	45	.1	4	2	314	1.31	2	5	ND	1	19	1	2	6	24	.20	.028	14	9	.15	62	.05	2	.76	.01	.04	1	1	20
OLD L63+00E 32+25N	1	4	11	68	.1	3	4	497	1.47	4	5	ND	1	27	1	2	2	23	.36	.033	15	10	.15	69	.03	15	.76	.02	.10	1	1	30
OLD L63+00E 32+00N	1	4	13	43	.2	4	2	321	1.26	4	5	ND	1	17	1	3	2	22	.16	.018	23	9	.13	60	.04	7	.84	.01	.07	1	1	10
OLD L63+00E 31+75N	1	7	16	52	.6	9	5	464	1.44	5	5	ND	2	17	1	3	2	24	.17	.042	20	9	.16	67	.04	9	1.29	.01	.07	2	1	40
OLD L63+00E 31+50N	1	4	17	53	.3	3	3	238	1.43	2	5	ND	1	20	1	5	2	23	.22	.050	21	10	.18	77	.03	2	1.28	.01	.10	1	1	30
OLD L63+00E 31+25N	1	4	12	43	.4	2	2	148	1.16	6	5	ND	1	18	1	2	6	19	.15	.029	18	9	.13	56	.04	6	.96	.01	.08	1	2	30
OLD L63+00E 31+00N	1	1	12	37	.1	3	2	139	1.01	4	5	ND	1	21	1	2	2	20	.20	.018	12	7	.10	49	.05	10	.59	.01	.05	1	1	10
OLD L63+00E 30+75N	1	1	13	32	.1	3	2	140	1.13	5	5	ND	1	14	1	2	3	21	.14	.015	12	9	.17	53	.07	8	.73	.01	.05	2	1	20
OLD L63+00E 30+50N	1	5	16	68	.6	6	5	431	1.99	4	5	ND	1	24	1	2	2	36	.21	.030	20	12	.25	81	.05	2	1.42	.01	.09	1	2	20
OLD L63+00E 30+25N	1	8	15	65	.4	10	5	236	2.36	10	5	ND	2	20	1	2	2	40	.17	.034	14	19	.28	103	.07	2	1.59	.01	.07	1	1	40
OLD L63+00E 30+00N	1	6	10	84	.6	6	5	621	2.17	6	5	ND	1	19	1	3	5	35	.23	.067	13	14	.25	98	.05	2	1.69	.01	.06	1	1	50
OLD L63+00E 29+75N	1	3	11	65	.7	5	3	341	1.63	5	5	ND	1	12	1	3	2	31	.12	.041	11	12	.13	61	.06	4	1.12	.01	.06	1	2	40
OLD L63+00E 29+50N	2	16	16	126	.1	16	10	979	3.76	9	5	ND	1	37	1	2	2	50	.33	.069	24	24	.50	165	.02	3	3.96	.01	.14	1	2	30
OLD L63+00E 29+25N	1	9	12	64	.3	7	6	470	2.23	6	5	ND	2	30	1	2	2	35	.30	.049	20	16	.29	113	.06	7	1.59	.01	.10	1	1	40
OLD L63+00E 29+00N	1	3	13	64	.1	7	4	358	1.72	5	5	ND	1	28	1	3	2	32	.21	.033	14	15	.23	79	.06	2	1.13	.01	.05	1	1	20
OLD L63+00E 28+75N	1	5	13	40	.2	7	3	199	1.67	6	5	ND	1	21	1	2	3	31	.22	.036	15	13	.25	70	.07	8	1.06	.02	.06	1	2	10
OLD L63+00E 28+50N	1	4	9	51	.3	5	3	289	1.52	3	5	ND	1	20	1	2	2	29	.20	.024	15	13	.22	70	.07	6	.96	.01	.05	1	1	30
OLD L63+00E 28+25N	1	10	20	110	.1	14	9	822	3.57	11	5	ND	1	26	1	2	2	51	.25	.066	19	21	.44	139	.02	2	1.12	.01	.11	1	1	30
STD C/AU-S	18	58	43	132	6.8	70	30	1127	4.21	43	21	8	36	48	18	17	19	60	.47	.081	40	60	.95	179	.07	33	2.05	.07	.14	13	47	1400

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*	Hg
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB	PPB
OLD L63+00E 28+00N	1	6	11	49	.1	4	3	119	1.19	2	5	ND	1	16	1	2	3	23	.14	.011	11	9	.15	37	.05	8	1.07	.01	.05	1	1	20
OLD L63+00E 27+75N	1	6	7	51	.1	5	3	202	1.39	2	5	ND	1	18	1	2	2	27	.18	.021	13	11	.20	62	.06	9	.97	.01	.07	1	2	10
OLD L63+00E 27+50N	1	15	11	93	.4	14	9	980	2.83	7	5	ND	3	35	1	2	11	39	.30	.057	31	18	.37	150	.02	2	2.66	.01	.12	1	1	40
OLD L63+00E 27+25N	1	9	9	61	.1	8	4	633	1.85	5	5	ND	1	30	1	2	2	30	.30	.041	24	14	.25	107	.04	6	1.60	.01	.09	1	1	30
OLD L63+00E 27+00N	1	14	15	122	.1	19	12	2702	3.56	8	5	ND	2	35	1	2	4	50	.36	.078	30	21	.50	171	.03	6	2.97	.02	.16	1	1	40
OLD L63+00E 26+75N	8	38	25	121	.2	35	22	4754	5.95	8	5	ND	2	95	1	2	13	60	1.29	.101	97	33	.48	299	.01	2	5.67	.02	.21	1	1	100
OLD L63+00E 26+50N	2	31	9	141	.1	18	6	1174	1.84	2	5	ND	1	185	1	2	2	19	3.15	.106	49	13	.25	156	.01	6	2.09	.01	.09	1	1	120
OLD L63+00E 26+25N	3	6	11	65	.1	5	5	127	1.82	2	5	ND	5	12	1	2	3	31	.13	.045	12	12	.14	77	.05	7	1.65	.01	.07	1	1	20
OLD L63+00E 26+00N	1	6	11	62	.1	6	4	164	1.84	5	5	ND	3	15	1	2	3	30	.17	.041	15	13	.26	90	.05	3	1.83	.01	.07	1	1	10
OLD L63+00E 25+75N	1	14	4	133	.8	9	7	547	1.77	3	7	ND	1	125	1	2	8	15	1.71	.085	49	9	.23	154	.01	4	1.91	.01	.09	2	1	160
OLD L66+00E 34+00N	1	3	6	29	.1	2	3	99	.98	2	5	ND	2	18	1	2	10	19	.18	.018	12	7	.12	58	.06	12	.75	.01	.05	1	1	20
OLD L66+00E 33+75N	1	4	9	41	.1	3	3	110	1.34	6	5	ND	3	15	1	2	5	25	.15	.035	10	9	.15	54	.06	6	.96	.01	.08	1	1	10
OLD L66+00E 33+50N	1	3	12	51	.2	2	2	118	1.17	2	5	ND	2	13	1	2	5	22	.13	.024	11	8	.12	51	.05	9	1.02	.01	.07	2	2	20
OLD L66+00E 33+25N	1	6	11	52	.3	5	3	93	1.52	6	10	ND	3	14	1	3	2	29	.14	.039	11	10	.09	53	.04	7	1.03	.01	.09	3	2	10
OLD L66+00E 33+00N	1	3	8	27	.1	3	2	77	.92	2	5	ND	2	13	1	2	6	20	.12	.010	11	7	.09	42	.06	9	.59	.01	.04	1	1	5
OLD L66+00E 32+75N	1	5	10	88	.1	10	6	155	2.85	9	5	ND	2	15	1	2	5	41	.15	.112	13	15	.18	91	.04	8	2.63	.01	.05	1	1	40
OLD L66+00E 32+50N	1	7	12	57	.2	6	4	538	1.34	2	6	ND	2	27	1	2	5	22	.23	.042	30	9	.12	86	.03	4	1.14	.01	.10	1	1	20
OLD L66+00E 32+25N	1	8	20	81	.3	7	7	677	2.18	12	8	ND	2	30	1	5	4	33	.24	.041	36	14	.30	98	.02	4	1.89	.01	.12	1	1	30
OLD L66+00E 32+00N	1	9	11	40	.1	5	3	119	2.19	2	5	ND	1	19	1	2	6	21	.16	.013	27	9	.16	60	.05	2	.82	.01	.07	2	3	10
OLD L66+00E 31+75N	1	12	15	80	.3	11	4	337	2.06	7	5	ND	3	38	1	2	2	30	.22	.027	40	15	.30	156	.04	2	1.73	.01	.11	1	1	20
OLD L66+00E 31+50N	1	4	15	111	.4	7	4	202	2.09	4	5	ND	4	25	1	2	2	32	.12	.108	12	13	.16	64	.05	2	1.71	.01	.08	2	2	30
OLD L66+00E 31+25N	1	3	9	96	.3	7	3	258	1.83	4	5	ND	1	27	1	2	4	30	.22	.096	12	13	.13	75	.05	10	1.12	.01	.09	1	1	20
OLD L66+00E 31+00N	1	9	9	91	.1	16	5	246	2.44	2	5	ND	1	28	1	2	2	46	.28	.058	11	20	.32	78	.11	5	1.43	.01	.06	1	2	10
OLD L66+00E 30+75N	1	11	14	95	.4	12	5	183	2.15	2	5	ND	2	16	1	2	5	32	.15	.042	12	14	.26	94	.04	7	2.09	.01	.11	1	2	30
OLD L66+00E 30+50N	1	5	11	92	.4	8	5	172	2.11	6	5	ND	1	13	1	2	4	35	.13	.095	12	15	.20	71	.06	8	1.70	.01	.05	1	2	40
OLD L66+00E 30+25N	1	3	10	69	.1	4	2	172	1.42	2	5	ND	1	20	1	2	2	33	.13	.019	11	10	.07	73	.06	9	.55	.01	.05	1	1	10
OLD L66+00E 30+00N	1	4	13	106	.1	6	4	257	1.73	2	5	ND	1	19	1	2	2	36	.18	.036	10	14	.16	53	.09	4	.80	.01	.05	1	1	20
OLD L66+00E 29+75N	1	3	15	75	.5	6	4	163	2.02	2	6	ND	2	14	1	2	2	35	.12	.036	11	14	.21	72	.06	3	1.51	.01	.05	1	31	30
OLD L66+00E 29+50N	1	7	9	94	.1	9	4	192	2.11	2	5	ND	1	15	1	2	2	42	.14	.031	10	17	.13	60	.08	7	1.08	.01	.07	1	1	10
OLD L66+00E 29+25N	1	9	14	74	.3	9	5	247	2.23	4	5	ND	3	23	1	5	2	37	.21	.035	16	17	.27	85	.05	2	1.71	.01	.09	1	1	30
OLD L66+00E 29+00N	1	1	11	56	.1	6	3	168	1.56	5	5	ND	1	16	1	3	3	31	.16	.018	11	12	.16	71	.06	9	1.02	.01	.05	1	1	10
OLD L66+00E 28+75N	1	7	13	109	.1	16	7	309	2.91	8	5	ND	1	23	1	2	2	48	.23	.063	11	21	.32	101	.07	13	2.16	.01	.06	1	1	30
OLD L66+00E 28+50N	1	1	12	115	.2	4	4	380	1.70	3	5	ND	1	14	1	3	5	34	.15	.041	12	13	.14	66	.07	4	1.07	.01	.05	1	2	20
OLD L66+00E 28+25N	1	1	8	106	.2	7	4	210	2.05	4	5	ND	1	18	1	2	2	34	.16	.060	11	15	.20	73	.05	3	1.51	.01	.06	1	1	30
OLD L66+00E 28+00N	1	2	17	109	.1	6	3	294	1.43	2	5	ND	1	15	1	2	8	28	.16	.054	10	12	.14	73	.07	8	1.10	.01	.05	1	1	10
OLD L66+00E 27+75N	1	6	14	148	.3	15	10	361	3.03	3	5	ND	3	21	1	3	3	55	.20	.079	9	28	.30	85	.13	2	1.65	.01	.07	1	1	20
STD C/AU-S	18	58	40	132	7.1	68	29	1072	4.05	38	19	8	36	48	18	17	19	59	.46	.087	40	61	.93	181	.07	31	2.00	.07	.14	11	51	1400

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L66+00E 27+50N	1	3	5	70	.1	8	4	325	1.92	2	5	ND	1	14	1	2	2	33	.18	.045	9	14	.22	61	.06	2	1.16	.01	.09	2	1	30
OLD L66+00E 27+25N	1	6	7	144	.2	8	6	661	1.88	3	5	ND	1	13	1	2	2	30	.15	.116	11	12	.15	95	.05	5	1.27	.01	.09	1	2	30
OLD L66+00E 27+00N	1	3	6	55	.1	8	5	172	1.58	2	5	ND	2	17	1	2	2	30	.18	.020	11	12	.17	66	.07	12	.96	.01	.04	1	1	10
OLD L66+00E 26+75N	1	6	7	61	.2	8	3	157	1.60	5	5	ND	1	18	1	2	2	29	.19	.040	12	12	.17	52	.05	6	1.04	.01	.09	1	1	10
OLD L66+00E 26+50N	1	2	7	44	.1	3	2	102	1.22	2	5	ND	1	14	1	2	2	26	.14	.017	10	9	.08	62	.06	3	.62	.01	.05	2	1	20
OLD L69+00E 34+00N	1	5	6	41	.2	7	3	293	1.52	4	8	ND	3	21	1	2	2	27	.23	.016	15	11	.24	62	.06	10	.90	.02	.06	1	1	10
OLD L69+00E 33+75N	1	8	7	54	.1	8	3	167	2.05	7	5	ND	1	18	1	2	3	35	.18	.027	14	13	.20	80	.06	6	1.26	.01	.08	1	1	10
OLD L69+00E 33+50N	1	5	7	64	.2	6	4	149	2.13	7	5	ND	3	11	1	2	2	30	.11	.063	11	13	.13	57	.04	5	1.50	.01	.07	1	2	20
OLD L69+00E 33+25N	1	8	4	42	.1	9	4	163	1.87	5	5	ND	1	20	1	2	2	34	.20	.030	11	13	.17	83	.07	12	1.00	.01	.07	2	1	20
OLD L69+00E 33+00N	1	11	14	81	.3	9	6	684	2.66	10	5	ND	1	32	1	2	6	43	.28	.048	30	16	.25	112	.04	7	2.11	.02	.09	1	2	30
OLD L69+00E 32+75N	1	5	7	42	.5	4	3	161	1.14	2	5	ND	2	22	1	2	2	21	.22	.019	17	10	.17	68	.07	12	.84	.02	.07	2	1	10
OLD L69+00E 32+50N	1	8	6	57	.1	7	3	224	1.66	3	5	ND	1	22	1	2	7	27	.21	.022	15	13	.23	69	.06	2	1.16	.01	.07	1	1	20
OLD L69+00E 32+25N	1	6	8	44	.1	5	3	197	1.26	2	5	ND	1	27	1	2	2	21	.24	.023	18	11	.20	60	.06	7	1.03	.01	.06	1	1	10
OLD L69+00E 32+00N	1	6	5	47	.1	5	3	232	1.36	2	5	ND	1	21	1	2	2	25	.19	.018	17	12	.18	68	.07	9	.76	.01	.08	2	1	20
OLD L69+00E 31+75N	1	7	11	49	.1	9	4	183	1.89	2	5	ND	2	24	1	2	5	35	.20	.022	14	17	.28	67	.10	2	1.19	.01	.04	2	1	20
OLD L69+00E 31+50N	1	9	10	60	.1	12	5	249	1.94	3	5	ND	1	24	1	2	3	32	.22	.036	14	14	.32	74	.07	8	1.24	.01	.07	1	1	10
OLD L69+00E 31+25N	1	9	15	131	.1	14	5	191	3.17	7	5	ND	1	27	1	2	2	45	.25	.162	11	20	.20	96	.06	4	2.43	.01	.07	1	1	30
OLD L69+00E 31+00N	1	14	21	88	.1	11	7	1494	2.41	9	5	ND	1	40	1	2	2	32	.46	.039	129	14	.34	119	.03	2	1.89	.02	.10	1	1	40
OLD L69+00E 30+75N	1	6	12	57	.2	6	3	180	1.68	3	5	ND	2	24	1	2	2	30	.26	.027	26	12	.22	68	.07	4	.95	.01	.08	1	1	20
OLD L69+00E 30+50N	1	5	12	94	.1	6	3	146	1.95	4	5	ND	1	16	1	2	2	30	.18	.082	11	13	.17	60	.05	2	1.38	.01	.06	1	1	30
OLD L69+00E 30+25N	1	8	10	70	.2	10	6	186	2.19	11	5	ND	1	19	1	2	2	36	.17	.073	12	13	.23	108	.05	5	1.56	.01	.09	1	2	30
OLD L69+00E 30+00N	2	9	21	102	.6	12	6	290	2.98	13	5	ND	2	14	1	2	2	42	.14	.100	12	17	.27	99	.04	2	2.29	.01	.07	1	1	40
OLD L69+00E 29+75N	1	5	6	45	.1	9	4	178	1.87	2	5	ND	1	15	1	2	2	31	.16	.039	12	12	.22	60	.06	2	1.08	.01	.05	1	1	20
OLD L69+00E 29+50N	1	11	10	99	.1	22	9	317	3.16	4	5	ND	1	19	1	2	3	56	.20	.054	9	26	.38	87	.12	3	2.01	.01	.07	1	1	30
OLD L69+00E 29+25N	1	8	10	99	.7	12	6	390	2.21	6	5	ND	1	23	1	2	2	34	.27	.065	13	16	.27	99	.06	2	1.52	.01	.08	1	2	20
OLD L69+00E 29+00N	1	5	11	70	.1	10	5	318	2.07	4	5	ND	1	15	1	2	2	35	.15	.047	11	16	.24	86	.06	2	1.32	.01	.05	1	1	30
OLD L69+00E 28+75N	1	5	11	70	.2	7	4	182	1.78	2	5	ND	2	11	1	2	2	30	.11	.029	13	12	.20	68	.06	8	1.43	.01	.04	1	2	20
OLD L72+00E 34+00N	1	5	5	47	.1	10	5	144	1.85	5	5	ND	2	13	1	2	4	31	.13	.043	12	14	.19	100	.06	5	1.42	.01	.05	2	1	10
OLD L72+00E 33+75N	1	8	14	152	.3	9	7	220	2.33	7	5	ND	2	16	1	2	2	32	.18	.096	12	15	.23	131	.05	7	2.05	.01	.06	1	2	20
OLD L72+00E 33+50N	1	6	9	85	.1	10	6	247	2.16	5	5	ND	1	23	1	2	2	35	.23	.073	12	15	.22	118	.05	2	1.34	.01	.05	1	1	10
OLD L72+00E 33+25N	1	7	10	50	.1	10	6	409	2.12	3	5	ND	1	37	1	2	3	39	.40	.046	15	21	.33	92	.10	2	1.09	.01	.05	1	1	30
OLD L72+00E 33+00N	1	12	13	49	.1	12	6	336	2.32	2	5	ND	1	34	1	2	2	43	.35	.045	17	19	.36	88	.12	4	1.18	.02	.07	1	1	10
OLD L72+00E 32+75N	1	14	11	52	.1	16	7	491	2.97	5	5	ND	2	46	1	3	2	53	.41	.059	19	26	.43	122	.12	2	1.41	.02	.05	2	1	10
OLD L72+00E 32+50N	1	11	13	53	.1	17	8	423	3.21	5	5	ND	1	51	1	2	2	53	.49	.064	20	28	.53	118	.13	2	1.64	.02	.06	1	1	5
OLD L72+00E 32+25N	1	10	16	58	.2	15	7	436	2.70	7	5	ND	1	42	1	2	2	44	.43	.045	24	22	.45	112	.10	2	1.76	.02	.07	1	2	30
OLD L72+00E 32+00N	1	4	12	31	.2	8	3	149	1.48	5	5	ND	1	20	1	2	4	27	.19	.025	10	11	.24	62	.07	2	.95	.01	.03	1	1	10
STD C/AU-S	18	57	41	132	6.6	68	29	1042	4.11	40	19	8	37	47	17	16	20	58	.46	.081	39	59	.93	178	.07	32	1.98	.06	.15	13	48	1300

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
OLD L72+00E 31+75N	1	7	12	88	.1	15	7	373	3.84	11	5	ND	2	14	1	2	2	56	.14	.135	12	21	.33	77	.10	4	2.21	.01	.06	1	1	60
OLD L72+00E 31+50N	1	8	7	54	.1	13	6	303	2.97	10	5	ND	2	23	1	2	2	48	.16	.045	15	19	.33	89	.09	5	1.42	.01	.07	1	1	20
OLD L72+00E 31+25N	1	6	8	48	.1	7	3	298	1.60	2	5	ND	1	22	1	3	2	27	.24	.014	24	11	.21	57	.07	2	.96	.01	.06	2	2	10
OLD L72+00E 31+00N	1	5	14	64	.3	9	4	223	1.96	6	5	ND	2	15	1	2	2	29	.15	.052	11	11	.21	62	.04	4	1.34	.01	.08	1	1	20
OLD L72+00E 30+75N	1	9	13	64	.2	15	6	211	2.52	4	5	ND	3	22	1	2	2	42	.19	.056	11	18	.29	115	.10	2	1.75	.01	.06	1	1	30
OLD L72+00E 30+50N	1	7	11	82	.1	10	5	220	2.27	3	5	ND	2	16	1	2	2	33	.15	.099	12	14	.23	121	.06	3	1.72	.01	.05	1	2	40
OLD L72+00E 30+25N	1	6	10	53	.1	9	4	192	1.99	5	5	ND	1	22	1	2	2	32	.25	.054	16	13	.24	94	.07	4	1.20	.01	.05	2	1	20
OLD L72+00E 30+00N	1	6	9	61	.1	8	3	199	1.80	3	5	ND	2	19	1	2	2	30	.20	.044	17	11	.19	84	.06	5	1.24	.01	.05	1	1	10
OLD L72+00E 29+75N	1	4	9	83	.1	7	3	198	1.73	2	5	ND	1	18	1	2	2	28	.19	.041	13	11	.24	67	.06	7	1.29	.01	.05	1	1	20
OLD L72+00E 29+50N	3	43	20	145	.6	28	12	3293	4.86	15	5	ND	4	79	1	2	2	56	.81	.140	86	29	.45	267	.02	4	5.13	.02	.19	1	1	90
OLD L72+00E 29+25N	2	16	20	145	.2	13	6	2010	2.89	14	5	ND	1	29	1	2	2	36	.28	.077	17	16	.34	190	.03	2	2.07	.01	.12	1	1	30
OLD L72+00E 29+00N	1	8	12	131	.1	8	5	251	2.39	7	5	ND	2	19	1	2	2	36	.22	.106	18	16	.26	102	.05	3	1.77	.01	.06	1	1	30
OLD L72+00E 28+75N	1	9	14	178	.1	10	4	249	2.61	8	5	ND	1	16	1	2	3	34	.20	.129	17	17	.31	104	.04	5	2.50	.01	.08	1	1	40
OLD L72+00E 28+50N	1	6	15	90	.1	7	3	212	1.85	2	5	ND	2	20	1	2	2	29	.21	.046	14	11	.22	90	.05	3	1.10	.01	.05	1	1	20
OLD L72+00E 28+25N	1	4	20	80	.1	6	2	179	1.58	2	5	ND	2	13	1	2	3	22	.19	.060	16	10	.20	73	.04	4	1.29	.01	.05	1	1	20
STD C/AU-S	17	58	41	132	7.1	68	28	1062	4.11	44	17	7	36	47	17	16	22	57	.47	.080	39	57	.94	177	.06	33	1.92	.06	.13	12	53	1400

II VLF-EM

-RAW DATA-

VLF-EM Data Sheet

Grid : Anomaly "A"

Line : L 4W (New)

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	-5	-5	+2	-3					
75	-5	-8	+3	-2		-15			
18+00N	-15	-15	+6	-9		-2			
25	-20	-21	+9	-11		+28			
50	-10	-20	+8	-2		+53 *			
75	0	-25	+10	+10		+43			
19+00	+13	-40	+17	+30		-11			
25	0	-48	+21	+21		-43			
50	-7	-35	+15	+8		-25			
75	-6	-15	+6	0		-5			
20+00	-4	-20	+8	+4		-8			
25	-7	-15	+6	-1		-7			
50	-7	-10	+4	-3		0			
75	-5	-10	+4	-1		-7			
21+00	-5	-5	+2	-3		-2			
25	-6	+6	-2	-8		+14 *			
50	+1	-3	+1	+2		+2			
75	+1	0	0	+1		-25			
22+00	-4	+2	-1	-5		-45			
25	-15	+5	-2	-17		-31			
50	-30	-5	-2	-32		+11			
75	-25	-10	+4	-21		+63			
23+00	-23	-14	+6	-17		+98 *			
25	+10	-40	+17	+27		+40			
50	+12	-27	+11	+33		-32			
75	+13	-10	+4	+17		-36			
24+00	+9	-5	+2	+11					
25	+3	0	0	+3					

VLF-EM Data Sheet Line : 12W (New) Tx. : Maine

Grid : ANOMALY "A" Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	-10	-25	+10	0					
75	-20	-15	+6	-14		-4			
18+00N	-22	-18	+7	-15		+16 +			
25	-11	-20	+8	-3		-19			
50	-20	-25	+10	-10		-43			
75	-35	-20	+8	-27		+22			
19+00N	-41	-30	+12	-29		+92*			
25	-5	-45	+19	+14		+54			
50	+5	-40	+17	+22		-18			
75	-5	-50	+22	+17		-39			
20+00	-8	-23	+9	+1		-21			
25	-5	-10	+4	-1		-2			
50	0	+5	-2	-2		-9			
75	+2	+5	-2	0		-25			
21+00	-7	+13	-5	-12		-17			
25	-9	+15	-6	-15		+12			
50	-10	+10	-4	-14		+35*			
75	+5	+15	-6	-1		+24			
22+00	+7	0	0	+7		-6			
25	0	-5	+2	+2		-23			
50	-5	-8	+3	-2		-44			
75	-15	-8	+3	-12		-47			
23+00	-34	-5	+2	-32		-2			
25	-33	-10	+4	-29		+67			
50	-25	-20	+8	-17		+93*			
75	+8	-35	+15	+23		+34			
24+00	+9	-35	+15	+24		-27			
25	+10	-15	+6	+16					
50	+3	-2	+1	+4					

VLF-EM Data Sheet

Line : L2W (New)

Tx. : Maine

Grid : ANOMALY "A"

Facing : South

Δ	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	-7	-30	+12	+5					
75	-15	-15	+6	-9					
18+00N	-20	-10	+4	-16		-36			
25	-30	-15	+6	-24		-31			
50	-38	-14	+6	-32		-16			
75	-33	-23	+9	-24		+19			
19+00	-23	-25	+10	-13		+30 *			
25	-25	-30	+12	-13		+11			
50	-25	-30	+12	-13		+4			
75	-25	-38	+16	-9		+17			
20+00	-15	-35	+15	0		+26 *			
25	0	-9	+4	+4		+14			
50	+5	+10	-4	+1		+4			
75	+14	+18	-7	+7		+8			
21+00	+13	+18	-7	+6		-14			
25	-7	+12	-5	-12		-42			
50	-19	-5	+2	-17		-25			
75	-25	-27	+11	-14		+10			
22+00	-15	-25	+10	-5		+27 *			
25	-4	-13	+5	+1		+25			
50	+1	-11	+4	+5		+15			
75	+3	-8	+3	+6		-2			
23+00	-6	-9	+4	-2		-20			
25	-10	-8	+3	-7		-23			
50	-17	-12	+5	-12		-24			
75	-25	-10	+4	-21		-15			
24+00	-21	-20	+8	-13		+40 *			
25	+5	-36	+15	+20					

VLF-EM Data Sheet

Grid : ANOMALY "A"

Line : L 1 W. (New)

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	-9	-25	+10	+1					
75	-11	-20	+8	-3		-3			
18+00	-10	-20	+8	-2		-4			
25	-10	-18	+7	-3		-2			
50	-10	-11	+4	-6		-2			
75	-6	-12	+5	-1		-12			
19+00	-14	-10	+4	-10		-15			
25	-19	-25	+10	-9		-19			
50	-25	-20	+8	-17		-10			
75	-33	-30	+12	-21		+18			
20+00	-25	-25	+10	-15		+22*			
25	-9	-10	+4	-5		+10			
50	-5	+10	-4	-9		+15			
75	0	+3	-1	-1		-12			
21+00	+3	+3	-1	+2		-41			
25	-30	-15	+6	-24		-2			
50	-40	-55	+24	-16		+30			
75	-25	-40	+17	-8		+27			
22+00	-10	-20	+8	-2		+20			
25	+2	-8	+3	+5		+6			
50	+2	-8	+3	+5		0			
75	0	-10	+4	+4		-15			
23+00	0	-14	+6	+6		-46			
25	-15	-7	+3	-12		-37			
50	-30	-15	+6	-24		+20			
75	-25	-15	+6	-19		+55*			
24+00	-5	-20	+8	+3		↓			
25	-1	-25	+10	+9					

VLF-EM Data Sheet — Line : L 0 (Old/New) — Tx. : Maine

Grid : ANOMALY "A" — Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	-29	-15	+6	-23		1			
75	-12	-10	+4	-8		+34*			
18+00	-4	-15	+6	+2		0			
25	-5	-15	+6	+1		-19			
50	-12	-12	+5	-7		-12			
75	-16	-16	+7	-9		+1			
19+00	-16	-16	+7	-9		+4			
25	-10	-10	+4	-6		-1			
50	-13	-13	+5	-8		-6			
75	-14	-14	+6	-8		-10			
20+00	-21	-21	+9	-12		-12			
25	-23	-23	+9	-14		-11			
50	-31	-31	+13	-18		-7			
75	-33	-33	+14	-19		+10			
21+00	-34	-34	+14	-20		+26*			
25	-11	-11	+4	-7		+12			
50	-10	-10	+4	-6		-4			
75	-16	-16	+7	-9		+2			
22+00	-14	-14	+6	-8		+7			
25	-9	-9	+4	-5		+4			
50	-8	-8	+3	-5		+2			
75	-6	-6	+2	-4		+2			
23+00	-7	-7	+3	-4		+1			
25	-5	-5	+2	-3		-2			
50	-7	-7	+3	-4		-4			
75	-8	-8	+3	-5		-2			
24+00	-10	-10	+4	-6		+2			
25	-9	-9	+4	-5					
50	-7	-7	+3	-4					

VLF-EM Data Sheet

Grid: ANOMALY "A"

Line: L.I.E. (New)

Tx.: Maine

Facing: South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	+9	0	0	+9		↑			
75	+9	0	0	+9		+5			
17+00	+13	+5	-2	+11		-7			
25	+14	+5	-2	+12		-35			
50	+1	0	0	+1		-34			
75	-13	0	0	-13		-11			
18+00	-8	0	0	-8		+1			
25	-17	-5	+2	-15		+16*			
50	-9	-10	+4	-5		+5			
75	-2	0	0	-2		-19			
19+00	-16	-8	+3	-13		-21			
25	-15	-5	+2	-13		-28			
50	-25	-5	+2	-23		-19			
75	-35	-10	+4	-31		+18			
20+00	-26	-5	+2	-24		+36*			
25	-16	-10	+4	-12		+17			
50	-11	-10	+4	-7		-8			
75	-12	0	0	-12		-16			
21+00	-15	0	0	-15		-15			
25	-24	-10	+4	-20		-10			
50	-32	-25	+10	-22		+6			
75	-35	-30	+12	-23		+27			
22+00	-28	-35	+15	-13		+46*			
25	-5	0	0	-5		+35			
50	-2	-40	+17	+15		-1			
75	-4	-15	+6	+2		-5			
23+00	-8	-35	+15	+7		-11			
25	-7	-30	+12	+5		-37			
50	-7	0	0	-7		-26			
75	-3	+35	-15	-18		+6			
24+00	-4	+15	-6	-10		+14*			
25	-9	0	0	-9		↓			
50	-5	0	0	-5					

VLF-EM Data Sheet

Grid: ANOMALY "A"

Line: L2E (New)

Tx.: Maine

Facing: South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	-2	0	0	-2					
75	+2	+10	-4	-2		+5			
18+00N	0	-5	+2	+2		+5			
25	-3	-5	+2	-1		+12 *			
50	+6	0	0	+6		+1			
75	+13	+15	-6	+7		-25			
19+00	-1	0	0	-1		-19			
25	-11	0	0	-11		+10			
50	-8	-15	+6	-2		0			
75	-15	-35	+15	0		-27			
20+00	-13	0	0	-13		-20			
25	-16	0	0	-16		-16			
50	-17	0	0	-17		-10			
75	-22	+15	-6	-28		+22 *			
21+00	-21	-15	+6	-15		+21			
25	-16	-20	+8	-8		-13			
50	-22	-20	+8	-14		-20			
75	-29	-18	+7	-22		+4			
22+00	-27	-18	+7	-20		+29			
25	-21	-22	+9	-12		+47 *			
50	-7	-15	+6	-1		+10			
75	+1	-35	+15	+16		-51			
23+00	0	-45	-19	-19		-18			
25	-5	-30	-12	-17		+29 *			
50	-4	0	0	-4		+21			
75	-3	0	0	-3		+13			
24+00	+3	0	0	+3		+7			
25	+3	0	0	+3					
50	+4	0	0	+4					

VLF-EM Data Sheet

Grid : ANOMALY "A"

Line : L3E (Old/New)

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
17+00N	+1	0	0	+1					
25	-5	-10	+4	-1					
50	-4	-5	+2	-2		-5			
75	-7	-10	+4	-3		+3			
18+00	+3	0	0	+3		+16			
25	+8	0	0	+8		+19			
50	+11	0	0	+11		+9			
75	+9	0	0	+9		-11			
19+00	+2	+7	-3	-1		-31			
25	0	+25	-10	-10		-31			
50	-3	+25	-10	-13		-37			
75	-35	0	0	-35		-12			
(Offset) 20+00	-50 / -16	0 / -35	0 / +15	-50 / -1		+57			
25	-30 / -12	-35 / -50	+15 / +22	/ +10					
50	-15	-45	+19	+4		+58			
75	-8	+7	-3	-11		-21			
21+00	-17	+10	-4	-21		-21			
25	-15	-20	+8	-7		+25*			
50	-6	-15	+6	0		+24			
75	-8	-10	+4	-4		-18			
22+00	-26	-12	+5	-21		-44			
25	-33	-15	+6	-27		-22			
50	-28	-20	+8	-20		+13			
75	-21	-15	+6	-15		+48			
23+00	-6	-50	+22	+16		+70*			
25	-3	-50	+22	+19		+17			
50	-1	0	0	-1		-35			
75	+1	0	0	+1		-16			
24+00	+1	0	0	+1		+4			
25	+3	0	0	+3		+3			
50	+4	+5	-2	+2					

VLF-EM Data Sheet

Grid : ANOMALY "A"

Line : L4E (New)

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
50	-2	+5	-2	-4					
75	-1	+15	-6	-7		-6			
18+00N	-2	+10	-4	-6		-8			
25	-5	+15	-6	-11		+11			
50	-6	+10	-4	-10		+39 *			
75	+6	+5	-2	+4		+27			
19+00	+17	+7	-3	+14		-20			
25	+9	+5	-2	+7		-36			
50	-5	+10	-4	-9		-1			
75	-3	+7	-3	-6		+20 *			
20+00	+7	+10	-4	+3		-11			
25	+2	0	0	+2		-27			
50	-20	-10	+4	-16		+1			
75	-21	-35	+15	-6		+1			
21+00	-11	-10	+4	-7		-3			
25	-14	0	0	-14		+14 *			
50	-10	-20	+8	-2		-4			
75	-13	-20	+8	-5		-31			
22+00	-21	-15	+6	-15		-24			
25	-30	-16	+7	-23		-19			
50	-28	-18	+7	-21		-16			
75	-42	-15	+6	-36		+18			
23+00	-34	-25	+10	-24		+58 *			
25	-27	-30	+12	-15		+56			
50	-4	-40	+17	+13		+13			
75	+4	0	0	+4		+2			
24+00	+7	0	0	+7		+12 *			
25	+12	0	0	+12					
50	+11	0	0	+11		↓			

/

VLF-EM Data Sheet Line : 1W Tx. : MAINE

Grid : ANOMALY "B" Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
26+00									
+25									
+50		—							
+75	+5	0	0	+5	+9				+2
27+00	+2	-6	+2	+4	+4	-16			+1
+25	+2	+5	-2	0	-7	-26			+4
+50	-2	+13	-5	-7	-22	-20			+5
+75	-9	+15	-6	-15	-27	-4			+3
28+00	-3	+22	-9	-12	-26	+6			+11
+25	-12	+6	-2	-14	-21	+24			+7
+50	-5	+5	-2	-7	-2	+38			+8
+75	+11	+15	-6	+5	+17	+13			+8
29+00	+25	+32	-13	+12	+11	-20			+12
+25	+5	+15	-6	-1	-3	-10			+7
+50	+2	+10	-4	-2	+1	+8			+4
+75	+9	+15	-6	+3	+5	+5			+11
30+00	+12	+25	-10	+2	+6	+13			+11
+25	+12	+20	-8	+4	+18	+17			+10
+50	+6	-20	+8	+14	+23				+4
+75	+9	0	0	+9					+7
31+00									

VLF-EM Data Sheet

Line : 0

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
25+00	-4	+27	-11	-15	-47				+8
+25	-13	+45	-19	-32	-57	+21			0
+50	-18	+16	-7	-25	-26	+57			-8
+75	-1	0	0	-1	0	+34			-2
26+00	+6	+13	-5	+1	+8	+18			0
+25	+9	+6	-2	+7	+18	+10			-1
+50	+11	0	0	+11	+18	-11			-2
+75	+7	0	0	+7	+7	-23			-3
27+00	0	0	0	0	-5	-9			-5
+25	-5	0	0	-5	-2	+4			-5
+50	+3	0	0	+3	-1	-13			+4
+75	0	+10	-4	-4	-15	-15			+5
28+00	-5	+15	-6	-11	-16	+7			+5
+25	-1	+10	-4	-5	-8	+20			+6
+50	-1	+5	-2	-3	+4	+30			+2
+75	+7	0	0	+7	+22	+32			0
29+00	+17	+5	-2	+15	+36	+11			+1
+25	+30	+23	-9	+21	+33	-14			+8
+50	+20	+20	-8	+12	+22	-36			+7
+75	+17	+17	-7	+10	-3	-44			+10
30+00	-1	+30	-12	-13	-22	-22			+8
+25	-1	+20	-8	-9	-25	-1			+10
+50	-16	0	0	-16	-23				+8
+75	-7	0	0	-7					+9
31+00									

VLF-EM Data Sheet

Line : 1 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
	-8	-9	+4	-4					-3
24+75	-6	-9	+4	-2	-6				-2
25+00	+13	+19	-8	+5	+3	+26			+9
+25	+22	+16	-7	+15	+20	+22			+14
+50	+18	+20	-8	+10	+25	-21			+20
+75	-3	+20	-8	-11	-1	-71			+11
26+00	-20	+35	-15	-35	-46	-58			+3
+25	-24	0	0	-24	-59	-2			+7
+50	-24	0	0	-24	-48	+26			+6
+75	-9	0	0	-9	-33	+34			+5
27+00	-5	0	0	-5	-14	+24			+4
+25	-4	0	0	-4	-9	+15			+1
+50	+5	0	0	+5	+1	+22			-6
+75	+6	-5	+2	+8	+13	+17			-8
28+00	+10	0	0	+10	+18	+11			-10
+25	+14	0	0	+14	+24	+9			-9
+50	+13	0	0	+13	+27	+4			-11
+75	+15	0	0	+15	+28	+2			-8
29+00	+14	0	0	+14	+29	-7			-2
+25	+11	+10	-4	+7	+21	-10			-2
+50	+18	+15	-6	+12	+19	-5			+6
+75	+13	+22	-9	+4	+16	-14			+6
30+00	+9	+20	-8	+1	+5	-28			+9
+25	-5	+20	-8	-13	-12	-46			+11
+50	-28	0	0	-28	-41	-41			+10
+75	-25	0	0	-25	-53	+7			+13
31+00	-9	0	0	-9	-34	+42			+8
+25	-2	0	0	-2	-11	+30			+4
+50	-2	0	0	-2	-4	+8			+1
+75	-1	0	0	-1	-3	+5			0
32+00	+2	0	0	+2	+1				0

VLF-EM Data Sheet

Line : 2E

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
+75	+3	0	0	+3					+6
26+00	-2	0	0	-2	+1				+5
+25	-15	0	0	-15	-17	-47			0
+50	-27	+10	-4	-31	-46	-28			-1
+75	-14	0	0	-14	-45	+28			+12
27+00	+2	+15	-6	-4	-18	+47			+12
+25	+12	+15	-6	+6	+2	+36			+11
+50	+14	+5	-2	+12	+18	+32			+11
+75	+22	0	0	+22	+34	+21			+11
28+00	+17	0	0	+17	+39	-4			+3
+25	+13	0	0	+13	+30	-14			-3
+50	+12	0	0	+12	+25	-7			-9
+75	+11	0	0	+11	+23	-5			-11
29+00	+11	+5	-2	+9	+20	-6			-10
+25	+13	+12	-5	+8	+17	-5			-4
+50	+12	+12	-5	+7	+15	-16			0
+75	-1	+13	-5	-6	+1	-21			-4
30+00	+7	+17	-7	0	-6	-20			+8
+25	-12	+18	-7	-19	-19	-32			+5
+50	-9	+25	-10	-19	-38	-15			+15
+75	-13	+5	-2	-15	-34				+12

VLF-EM Data Sheet

Line : 3E

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
26+00									
+25	-4	0	0	-4	-12				-3
+50	-8	0	0	-8	-15	-16			+1
+75	-7	0	0	-7	-28	-41			+9
27+00	-17	+11	-4	-21	-56	-30			+8
+25	-30	+13	-5	-35	-58	+23			+4
+50	-20	+8	-3	-23	-33	+47			+12
+75	-3	+17	-7	-10	-11	+39			+13
28+00	+5	+15	-6	-1	+6	+33			+9
+25	+10	+8	-3	+7	+22	+22			+7
+50	+15	0	0	+15	+28	+8			+3
+75	+17	+10	-4	+13	+30	-5			-1
29+00	+17	0	0	+17	+23	-25			-1
+25	+13	+18	-7	+6	+5	-29			-2
+50	+4	+12	-5	-1	-6	-18			-4
+75	+1	+15	-6	-5	-13	-5			+1
30+00	-3	+13	-5	-8	-11	+15			+4
+25	+4	+18	-7	-3	+2	+18			+9
+50	+12	+14	-7	+5	+7				+10
+75	+10	+20	-8	+2					+6
31+00									

VLF-EM Data Sheet

Line : 4E

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
26+00									
+25		—							
+50									
+75	-2	0	0	-2	-9				-1
27+00	-7	0	0	-7	-19	-9			-4
+25	-12	0	0	-12	-18	+7			-3
+50	-6	0	0	-6	-12	-4			+6
+75	-6	0	0	-6	-22	-3			+8
28+00	-9	+16	-7	-16	-15	+32			+10
+25	+8	+16	-7	+1	+10	+24			+10
+50	+20	+27	-11	+9	+9	-9			+9
+75	+4	+10	-4	0	+1	-5			-1
29+00	+6	+12	-5	+1	+4	+3			+4
+25	+7	+10	-4	+3	+4	-2			+5
+50	+5	+10	-4	+1	+2	-1			+5
+75	+3	+5	-2	+1	+3	+3			+5
30+00	+4	+5	-2	+2	+5	+5			+5
+25	+6	+7	-3	+3	+8	+6			+4
+50	+10	+12	-5	+5	+11				+2
+75	+12	+15	-6	+6					-2
31+00									

VLF-EM Data Sheet

Grid : ANOMALY "C"

Line : LINE 14 EAST

Tx. : MAINE

Facing : SOUTH

Δ	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
28+00									
+25									
+50									
+75	-7	+10	-4	-11	+17				-2
29+00	-6	0	0	-6	-6	+20			-1
+25	+3	+7	-3	0	+3	+17			+5
+50	+8	+13	-5	+3	+11	+14			+6
+75	+8	0	0	+8	+17	+18			+2
30+00	+9	0	0	+9	+29	+17			0
+25	+16	-10	+4	+20	+34	-9			+4
+50	+14	0	0	+14	+20	-23			+5
+75	+6	0	0	+6	+11	-16			0
31+00	+5	0	0	+5	+4	-10			+4
+25	+3	+11	-4	-1	+1	-10			+3
+50	+2	0	0	+2	-6	-12			+6
+75	-8	0	0	-8	-11	+7			-1
32+00	-5	-5	+2	-3	+1	+20			-3
+75	+4	0	0	+4	+9	+8			-1
+50	+14	+22	-9	+5	+9	+5			0
+75	+9	+12	-5	+4	+14	+5			-6
33+00	+10	0	0	+10	+14	+3			-3
+25	+4	0	0	+4	+17				-9
+50	+13	0	0	+13					0
+75									
34+00									

VLF-EM Data Sheet

Grid : ....

Line : 15 EAST

Tx. : MAINE

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
28+00		—							
+25									
+50									
+75	+5	0	0	+5	+2				+4
29+00	-3	0	0	-3	-10	-13			+2
+25	-7	0	0	-7	-11	+5			+3
+50	-4	0	0	-4	-5	+12			+8
+75	-1	0	0	-1	+1	+4			+9
30+00	0	-5	+2	+2	-1	-22			+9
+25	-3	0	0	-3	-21	-34			+10
+50	-12	+15	-6	-18	-35	-21			+3
+75	-15	+5	-2	-17	-42	+4			+4
31+00	-19	+15	-6	-25	-31	+36			+2
+25	-4	+5	-2	-6	-6	+31			+6
+50	+5	+12	-5	0	0	+10			+8
+75	+4	+10	-4	0	+4	-3			+6
32+00	+4	0	0	+4	-3	-14			+9
+25	-7	0	0	-7	-10	-1			+3
+50	-5	-5	+2	-3	-4	+21			+4
+75	+5	+14	-6	-1	+11	+29			+3
33+00	+15	+7	-3	+12	+25	+7			+3
+25	+17	+11	-4	+13	+18				+4
+50	+5	0	0	+5					0

VLF-EM Data Sheet

Line : 16 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
28+00									
+25									
+50									
+75	0	0	0	0	-7				+3
29+00	-3	+10	-4	-7	-27	-50			+7
+25	-8	+30	-12	-20	-57	-34			+9
+50	-15	+50	-22	-37	-61	+14			+9
+75	-14	+25	-10	-24	-43	+29			+10
30+00	-17	+5	-2	-19	-32	+24			+7
+25	-15	-5	+2	-13	-19	+26			+5
+50	-6	0	0	-6	-6	+18			+8
+75	+4	+10	-4	0	-1	+15			+10
31+00	+3	+10	-4	-1	+9	+18			+6
+25	+14	+10	-4	+10	+17	+9			+6
+50	+9	+6	-2	+7	+18	-5			+1
+75	+13	+5	-2	+11	+12	-13			+5
32+00	+3	+5	-2	+1	+5	-7			+3
+25	+4	0	0	+4	+5	-13			+2
+50	+1	0	0	+1	-8	-21			+1
+75	-9	0	0	-9	-16	-1			0
33+00	-7	0	0	-7	-9	+19			+4
+25	+4	+15	-6	-2	+3				+7
+50	+11	+15	-6	+5					+6

VLF-EM Data Sheet

Grid :

Line : LINE 17 EAST

Tx. : MAINE

Facing : SOUTH

Δ	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
28+00									
+25									
+50									
+75	-2	+8	-3	-5	-18				+1
29+00	-7	+15	-6	-13	-34	-6			+1
+25	-15	+15	-6	-21	-24	+31			+2
+50	+4	+17	-7	-3	-3	+21			+13
+75	+17	+40	-17	0	-3	-16			+22
30+00	+11	+33	-14	-3	-19	-27			+20
+25	-6	+24	-10	-16	-30	+2			+10
+50	-14	0	0	-14	-17	+35			+5
+75	-3	0	0	-3	+5	+33			+4
31+00	+8	0	0	+8	+16	+2			+4
+25	+11	+8	-3	+8	+7	-20			+5
+50	+7	+20	-8	-1	-4	-4			+7
+75	-3	0	0	-3	+3	+21			0
32+00	+8	+5	-2	+6	+17	+12			0
+25	+15	+10	-4	+11	+15	-22			+1
+50	+4	0	0	+4	-5	-33			0
+75	-9	0	0	-9	-18	-1			-2
33+00	-11	-5	+2	-9	-6	+30			+2
+25	+3	0	0	+3	+12				+4
+50	+14	+13	-5	+9					+5

VLF-EM Data Sheet

Line : 18EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter	Quad.
28+00							
+25							
+50							
+75	+11	0	0	+11	+11		+3
29+00	+5	+12	-5	0	-12	-32	+5
+25	-1	+26	-11	-12	-21	+2	+7
+50	-2	+18	-7	-9	-10	+25	+8
+75	+5	+15	-6	-1	+4	+20	+7
30+00	+21	+37	-16	+5	+10	+4	+11
+25	+17	+28	-12	+5	+8	-3	+6
+50	+8	+13	-5	+3	+7	+1	+2
+75	+2	-5	+2	+4	+9	+6	-4
31+00	+5	0	0	+5	+13	0	-3
+25	+8	0	0	+8	+9	-10	-2
+50	+3	+5	-2	+1	+3	0	0
+75	+6	+10	-4	+2	+9	+13	+3
32+00	+7	0	0	+7	+16	-2	-1
+25	+9	0	0	+9	+7	-22	+3
+50	+2	+10	-4	-2	-6	-13	+3
+75	-2	+5	-2	-4	-6	+3	+2
33+00	-2	0	0	-2	-3	+9	0
+25	-3	-5	+2	-1	+3		-2
+50	+4	0	0	+4			+1

VLF-EM Data Sheet

Grid : ANOMALY "D"

Line : 50 EAST

Tx. : MAINE

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
21+00	+14	+14	-6	+8					-3
+25	+20	+10	-4	+16	+24				-5
+50	+16	+12	-5	+11	+27	-7			-6
+75	+6	0	0	+6	+17	-14			-9
22+00	+7	0	0	+7	+13	+1			-7
+25	+11	0	0	+11	+18	+19			-5
+50	+21	0	0	+21	+32	+19			+2
+75	+16	0	0	+16	+37	-2			+1
23+00	+11	-8	+3	+14	+30	-16			+1
+25	+9	+5	-2	+7	+21	-26			+3
+50	-3	0	0	-3	+4	-27			-1
+75	-3	0	0	-3	-6	-15			-1
24+00	-11	-8	+3	-8	-11	-1			-3
+25	+5	+9	-4	+1	-7	0			+8
+50	-7	+12	-5	-12	-11	-27			+4
+75	-22	0	0	-22	-34	-20			-1
25+00	-9	0	0	-9	-31	+18			+5
+25	-7	0	0	-7	-16	+14			+6
+50	-10	0	0	-10	-17	-19			+6
+75	-25	0	0	-25	-35	-32			+1
26+00	-29	-12	+5	-24	-49	+2			+1
+25	-11	-5	+2	-9	-33	+39			+3
+50	-1	0	0	-1	-10	+35			+1
+75	+3	0	0	+3	+2	+21			0
27+00	+8	0	0	+8	+11	-9			+1
+25	-9	+15	-6	-15	-7	-38			-4
+50	-7	+13	-5	-12	-27	-14			0
+75	-7	+6	-2	-9	-21	+11			-1
28+00	-7	0	0	-7	-16	+17			-1
+25	+3	0	0	+3	-4	+24			+1
+50	+10	+12	-5	+5	+8	+11			+3
+75	+6	+9	-4	+2	+7	-6			0
29+00	+5	+12	-5	0	+2	-15			+2
+25	-4	+10	-4	-8	-8	-19			0
+50	-12	-8	+3	-9	-17	+1			-2
+75	0	-6	+2	+2	-7	+20			+4
30+00	+4	+8	-3	+1	+3				+3

VLF-EM Data Sheet

Line : 51 EAST

Tx. : MAINE

Grid : ....

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+1	0	0	+1	+2				-3
+25	-3	-9	+4	+1	+5	0			-3
150	+4	0	0	+4	+2	-16			+4
175	-4	-5	+2	-2	-11	-16			+1
25+00	-7	+5	-2	-9	-14	+3			+2
+25	-15	-25	+10	-5	-8	+7			0
150	-5	-5	+2	-3	-7	+6			+3
175	0	+10	-4	-4	-2	+16			+3
26+00	+2	0	0	+2	+9	+23			0
+25	+7	0	0	+7	+21	+12			-4
150	+12	-5	+2	+14	+21	-8			-4
175	+7	0	0	+7	+13	-15			-6
27+00	+6	0	0	+6	+6	-18			-5
+25	0	0	0	0	-5	-15			-5
150	-5	0	0	-5	-9	+2			-5
175	-4	0	0	-4	-3	+16			-3
28+00	+1	0	0	+1	+7	+18			-2
+25	+6	0	0	+6	+15	+14			-3
150	+9	0	0	+9	+21	+4			-2
175	+17	+12	-5	+12	+19	-8			+1
29+00	+10	+7	-3	+7	+13	-16			-2
+25	+6	0	0	+6	+3	-9			-2
+50	-3	0	0	-3	+4	+16			-5
175	+4	-8	+3	+7	+19				-3
30+00	+10	-6	+2	+12					-2

VLF-EM Data Sheet

Line : 52 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+10	+6	-2	+8	+13				-3
+25	+9	+9	-4	+5	0	-14			0
+50	+2	+18	-7	-5	-1	0			0
+75	+1	-7	+3	+4	0	-10			+1
25+00	-4	0	0	-4	-11	-11			+1
+25	-7	0	0	-7	-11	+4			+2
+50	-14	-25	+10	-4	-7	+6			-3
+75	-7	-9	+4	-3	-5	+8			-1
26+00	+3	+12	-5	-2	+1	+13			+1
+25	+3	0	0	+3	+8	+6			-3
+50	+5	0	0	+5	+7	-7			-2
+75	+4	+6	-2	+2	+1	-11			0
27+00	-1	0	0	-1	-4	-7			-3
+25	-3	0	0	-3	-6	-5			-2
+50	-3	0	0	-3	-9	-3			-2
+75	-2	+11	-4	-6	-9	+2			-1
28+00	-3	0	0	-3	-7	+3			-2
+25	-4	0	0	-4	-6	+3			-1
+50	-2	0	0	-2	-4	+4			-1
+75	-2	0	0	-2	-2	+19			-2
29+00	+5	+13	-5	0	+15	+24			-6
+25	+15	0	0	+15	+22	-3			-10
+50	+7	0	0	+7	+12	-11			-11
+75	+5	0	0	+5	+11				-9
30+00	+6	0	0	+6					-3

VLF-EM Data Sheet

Line : 53 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+4	0	0	+4	+9				0
+25	+5	0	0	+5	+13	+3			-1
+50	+8	0	0	+8	+12	-8			-2
+75	+8	+10	-4	+4	+5	-7			+1
25+00	+3	+5	-2	+1	+5	0			-3
+25	+4	0	0	+4	+5	-10			-1
+50	+1	0	0	+1	-5	-12			-4
+75	-6	0	0	-6	-7	+6			-5
26+00	-5	-9	+4	-1	+1	+10			-3
+25	-1	-7	+3	+2	+3	-2			0
+50	+1	0	0	+1	-1	-1			+1
+75	-2	0	0	-2	+2	+6			+1
27+00	+4	0	0	+4	+5	+3			+2
+25	+10	+22	-9	+1	+5	+3			+3
+50	+4	0	0	+4	+8	-1			-1
+75	+4	0	0	+4	+4	-9			-1
28+00	0	0	0	0	-1	-5			-1
+25	-1	0	0	-1	-1	-2			-1
+50	0	0	0	0	-3	-3			-2
+75	+3	+14	-6	-3	-4	-3			-2
29+00	-1	0	0	-1	-6	+1			-2
+25	+1	+15	-6	-5	-3	+12			-1
+50	+2	0	0	+2	+6	+11			-3
+75	+4	0	0	+4	+8				-3
30+00	+4	0	0	+4					-3

VLF-EM Data Sheet

Grid : ....

Line : 54 EAST

Tx. : MAINE

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+4	+9	-4	0	+1				-1
+25	+3	+5	-2	+1	+4	+6			+1
+50	+3	0	0	+3	+7	+3			0
+75	+4	0	0	+4	+7	-3			+2
25+00	+6	+8	-3	+3	+4	-3			+3
+25	+4	+7	-3	+1	+4	0			+2
+50	+3	0	0	+3	+4	-5			+2
+75	+1	0	0	+1	-1	-8			+3
26+00	+1	+8	-3	-2	-4	-2			+3
+25	-4	-5	+2	-2	-3	+4			+1
+50	-3	-5	+2	-1	0	+5			0
+75	+1	0	0	+1	+2	+3			+1
27+00	+1	0	0	+1	+3	+4			+1
+25	+2	0	0	+2	+6	+6			-1
+50	+4	0	0	+4	+9	+2			-1
+75	+7	+6	-2	+5	+8	-6			-2
28+00	+9	+15	-6	+3	+3	-6			-1
+25	+8	+19	-8	0	+2	-1			-1
+50	+2	0	0	+2	+2	-1			-2
+75	0	0	0	0	+1	0			-3
29+00	+1	0	0	+1	+2	0			-4
+25	+1	0	0	+1	+1	+5			-3
+50	0	0	0	0	+7	+14			-3
+75	+7	0	0	+7	+15				-4
30+00	+8	0	0	+8					-5

VLF-EM Data Sheet

Line : 55 EAST

Grid :

Tx. : MAINE

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+2	0	0	+2	+5				-5
+25	+3	0	0	+3	+5	0			-5
+50	+2	0	0	+2	+5	+1			-5
+75	+3	0	0	+3	+6	-5			-4
25+00	+3	0	0	+3	0	-7			-3
+25	+1	+11	-4	-3	-1	+4			-3
+50	+2	0	0	+2	+4	+7			0
+75	+4	+5	-2	+2	+6	0			+2
26+00	+8	+10	-4	+4	+4	-8			+4
+25	0	0	0	0	-2	-6			+3
+50	-2	0	0	-2	-2	+5			+4
+75	0	0	0	0	+3	+7			+4
27+00	+3	0	0	+3	+5	+3			+4
+25	+2	0	0	+2	+6	+4			+3
+50	+4	0	0	+4	+9	+1			+4
+75	+5	0	0	+5	+7	-2			+3
28+00	+5	+8	-3	+2	+7	+5			0
+25	+7	+6	-2	+5	+12	+8			-2
+50	+9	+5	-2	+7	+15	-3			-4
+75	+10	+5	-2	+8	+9	-13			-4
29+00	+4	+8	-3	+1	+2	-9			-3
+25	+1	0	0	+1	0	-4			-3
+50	-1	0	0	-1	-2	-7			0
+75	-1	0	0	-1	-7				0
30+00	-2	+10	-4	-6					0

VLF-EM Data Sheet

Line : 56 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+3	0	0	+3	+9				-7
+25	+6	0	0	+6	+16	+15			-9
+50	+10	0	0	+10	+24	+11			-9
+75	+14	0	0	+14	+27	+5			-9
25+00	+13	0	0	+13	+29	+1			-8
+25	+16	0	0	+16	+28	-7			-5
+50	+12	0	0	+12	+22	-8			-4
+75	+8	-5	+2	+10	+20	-7			-3
26+00	+13	+8	-3	+10	+15	-23			+1
+25	+10	+12	-5	+5	-3	-47			+5
+50	-2	+15	-6	-8	-32	-34			-1
+75	-18	+14	-6	-24	-37	-1			-6
27+00	-13	0	0	-13	-33	0			+3
+25	-20	0	0	-20	-37	+10			+4
+50	-17	0	0	-17	-23	+35			+8
+75	-6	0	0	-6	-2	+34			+7
28+00	+4	0	0	+4	+11	+13			+2
+25	+7	0	0	+7	+11	-3			0
+50	+6	+6	-2	+4	+8	-2			-1
+75	+6	+5	-2	+4	+9	+1			0
29+00	+8	+7	-3	+5	+9	-4			0
+25	+4	0	0	+4	+5	-8			0
+50	+1	0	0	+1	+1	-8			0
+75	0	0	0	0	-3				+1
30+00	-3	0	0	-3					+2

VLF-EM Data Sheet

Grid : ....

Line : 57 EAST

Tx. : MAINE

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+2	0	0	+2	0				-3
+25	-2	0	0	-2	-6	-4			-2
+50	-4	0	0	-4	-4	+9			+1
+75	0	0	0	0	+3	+10			+1
25+00	+5	+5	-2	+3	+6	+8			0
+25	+5	+6	-2	+3	+11	+8			-3
+50	+8	0	0	+8	+14	+5			-5
+75	+6	0	0	+6	+16	+15			-9
26+00	+10	0	0	+10	+29	+23			-8
+25	+23	+11	-4	+19	+39	+7			-1
+50	+23	+8	-3	+20	+36	-18			+1
+75	+21	+12	-5	+16	+21	-31			+6
27+00	+10	+13	-5	+5	+5	-32			+4
+25	0	0	0	0	-11	-53			+3
+50	-11	0	0	-11	-48	-54			+3
+75	-29	+20	-8	-37	-65	+8			-1
28+00	-28	0	0	-28	-40	+50			+5
+25	-12	0	0	-12	-15	+38			+9
+50	-3	0	0	-3	-2	+18			+8
+75	+1	0	0	+1	+3	+5			+4
29+00	+2	0	0	+2	+3	-4			+3
+25	+1	0	0	+1	-1	-6			0
+50	-2	0	0	-2	-3	-1			-1
+75	-1	0	0	-1	-2				-2
30+00	-1	0	0	-1					-2

VLF-EM Data Sheet

Line : 58EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
24+00	+4	0	0	+4					-2
+25	-1	0	0	-1	+3				-2
+50	0	0	0	0	-1	-2			-1
+75	+1	0	0	+1	+1	+2			+1
25+00	0	0	0	0	+1	-1			+3
+25	+2	+5	-2	0	0	+1			+5
+50	+4	+5	-2	+2	+2	-1			+7
+75	+4	+18	-7	-3	-1	-8			+7
26+00	-3	0	0	-3	-6	-6			+4
+25	-6	-5	+2	-4	-7	+1			+2
+50	+1	+5	-2	-1	-5	+15			+2
+75	+13	+9	-4	+9	+8	+26			0
27+00	+17	+12	-5	+12	+21	+11			0
+25	+12	+12	-5	+7	+19	-13			-2
+50	+3	+5	-2	+1	+8	-17			-3
+75	-1	-5	+2	+1	+2	-8			-1
28+00	+2	+7	-3	-1	0	-5			+4
+25	0	+5	-2	-2	-3	-4			+3
+50	-2	0	0	-2	-4	-1			+2
+75	-4	-5	+2	-2	-4	-2			+2
29+00	-4	0	0	-4	-6	-3			+3
+25	-3	0	0	-3	-7	+1			+1
+50	-2	0	0	-2	-5	+4			0
+75	-1	0	0	-1	-3	+1			-1
30+00	-3	0	0	-3	-4				-2

VLF-EM Data Sheet

Grid : ANOMALY "E"

Line : L74E (New)

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
30+00N	+5	-10	+4	+9					
25	+10	+8	-3	+7		-7			
50	+9	+3	-1	+8		-13			
75	+2	+2	-1	+1		-3			
31+00	+3	+5	-2	+1		+7			
25	+6	+2	-1	+5		+9			
50	+5	+3	-1	+4		+11 *			
75	+13	+5	-2	+11		+2			
32+00	+15	+15	-6	+9		-2			
25	+14	+15	-6	+8		+4			
50	+14	+10	-4	+10		-3			
75	+15	+10	-4	+11		-19			
33+00	+10	+15	-6	+4		-16			
25	+7	+10	-4	-2		-9			
50	+8	+16	-7	+1		-2			
75	+1	+23	-9	-8		+25			
34+00	+5	0	0	+5		+29 *			
25	+15	+5	-2	+13		+7			
50	+15	+6	-2	+13		-2			
75	+14	+4	-2	+12		-6			
35+00	+11	-3	+1	+12		-12			
25	+5	-5	+2	+7		-14			
50	+4	-3	+1	+5		-17			
75	0	0	0	0		-12			
36+00	-4	+3	-1	-5		+2			
25	0	+5	-2	-2		+14			
50	+1	+5	-2	-1		+19 *			
75	+10	+5	-2	+8		0			
37+00	+10	+5	-2	+8					
25	+2	+8	-3	-1					

VLF-EM Data Sheet

Line : L 7.5 E (New)

Tx. : Maine

Grid : Anomaly "E"

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
30+00 N	+15	+3	-1	+14					
25	+15	+1	0	+15		-8			
50	+16	+3	-1	+15		-18			
75	+8	+4	-2	+6		-12			
31+00	+6	0	0	+6		-12			
25	+5	+6	-2	+3		-20			
50	0	+8	-3	-3		-15			
75	-6	+5	-2	-8		+8			
32+00	-5	+5	-2	-7		+26 *			
25	+8	+10	-4	+4		+16			
50	+10	+8	-3	+7		-1			
75	+9	+8	-3	+6		+3			
33+00	+8	+10	-4	+4		+14 *			
25	+18	+15	-6	+12		+11			
50	+19	+18	-7	+12		+7			
75	+21	+15	-6	+15		+8			
34+00	+20	+10	-4	+16		+7			
25	+19	0	0	+19		-8			
50	+15	-10	+4	+19		-26			
75	+10	+5	-2	+8		-22			
35+00	+7	+7	-3	+4		-11			
25	+2	+3	-1	+1		-12			
50	0	0	0	0		-15			
75	-5	+5	-2	-7		-11			
36+00	-5	+6	-2	-7		-19			
25	-9	+5	-2	-11		-20			
50	-20	+6	-2	-22		+22 *			
75	-13	+8	-3	-16					
37+00	+6	+3	-1	+5					

VLF-EM Data Sheet

Grid : ANOMALY "E"

Line : L 76 E (New)

Tx. : Maine

Facing : South

Station	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
30+00N	+5	+2	-1	+4					
25	+6	+7	-3	+3		+7			
50	+8	+12	-5	+3		+23			
75	+13	+5	-2	+11		+27 *			
31+00	+20	+5	-2	+18		+13			
25	+25	+4	-2	+23		-8			
50	+21	+5	-2	+19		-23			
75	+18	+10	-4	+14		-23			
32+00	+7	+5	-2	+5		-5			
25	+7	+5	-2	+5		+10			
50	+12	+8	-3	+9		+5			
75	+14	+8	-3	+11		-6			
33+00	+12	+10	-4	+8		+1			
25	+10	+10	-4	+6		+18			
50	+21	+17	-7	+14		+17			
75	+22	+10	-4	+18		+2			
34+00	+23	+10	-4	+19		-4			
25	+17	+5	-2	+15		-3			
50	+15	-8	+3	+18		-11			
75	+12	-3	+1	+13		-14			
35+00	+8	-3	+1	+9		-13			
25	+9	+3	-1	+8		-19			
50	+5	+11	-4	+1		-28			
75	+1	+10	-4	-3		-24			
36+00	-10	+15	-6	-16		+3			
25	-10	0	0	-10		+17 *			
50	-4	+5	-2	-6		+4			
75	+1	+10	-4	-3		-11			
37+00	-5	+10	-4	-9		0			
25	-7	+10	-4	-11					
50	0	+3	-1	-1					

VLF-EM Data Sheet Line : L77E (New) Tx. : Maine

Grid : ANOMALY "E" Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
25	+13	+5	-2	+11					
50	+17	+8	-3	+14		+3			
75	+18	+3	-1	+17		-24			
30+00N	+15	+10	-4	+11		-41			
25	+1	+13	-5	-4		-17			
50	-3	+15	-6	-9		+10			
75	+7	+20	-8	-1		+14			
31+00	+5	+17	-7	-2		+15 *			
25	+10	+10	-4	+6		+9			
50	+13	+17	-7	+6		+3			
75	+15	+20	-8	+7		+1			
32+00	+13	+12	-5	+8		-3			
25	+7	+3	-1	+6		0			
50	+10	+10	-4	+6		+7			
75	+12	+10	-4	+8		+5			
33+00	+13	+5	-2	+11		+2			
25	+12	+10	-4	+8		+6			
50	+17	+10	-4	+13		+8			
75	+22	+25	-10	+12		+4			
34+00	+25	+20	-8	+17		-6			
25	+15	+8	-3	+12		-12			
50	+13	+5	-2	+11		-12			
75	+8	+5	-2	+6		0			
35+00	+6	+2	-1	+5		+10 *			
25	+10	-5	+2	+12		-4			
50	+11	+5	-2	+9		-14			
75	+8	+10	-4	+4		-9			
36+00	+5	+5	-2	+3		-3			
25	+4	+7	-3	+1		+8			
50	+5	+4	-2	+3		+14 *			
75	+9	0	0	+9		-7			
37+00	0	+10	-4	-4					

VLF-EM Data Sheet

Grid : ANOMALY "E"

Line : L 78 E (New)

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
30+00N	+19	-5	+2	+21					
25	+13	-5	+2	+15		-23			
50	+10	+10	-4	+6		-3			
75	+12	+13	-5	+7		+3			
31+00	+17	+15	-6	+11		-16			
25	+13	+20	-8	+5		-39			
50	+3	+14	-6	-3		-35			
75	-14	+15	-6	-20		-1			
32+00	-8	+13	-5	-13		+29			
25	-9	+5	-2	-11		+41 *			
50	+7	0	0	+7		+22			
75	+12	+5	-2	+10		-4			
33+00	+10	+5	-2	+8		-7			
25	+12	+18	-7	+5		+6			
50	+12	+15	-6	+6		+16 *			
75	+17	+10	-4	+13		+3			
34+00	+22	+20	-8	+14		-9			
25	+16	+20	-8	+8		-1			
50	+20	+25	-10	+10		-1			
75	+15	+10	-4	+11		-12			
35+00	+10	+10	-4	+6		-11			
25	+6	+7	-3	+3		-1			
50	+5	+5	-2	+3		+8			
75	+7	+5	-2	+5		+10 *			
36+00	+13	+10	-4	+9		+1			
25	+13	+10	-4	+9		-6			
50	+10	+10	-4	+6		-2			
75	+10	+10	-4	+6					
37+00	+11	+10	-4	+7					

VLF-EM Data Sheet

Grid : ANOMALY "E"

Line : L79E

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
30+00N	+16	+20	-8	+8					
25	+10	+10	-4	+6		+12			
50	+15	0	0	+15		+1			
75	+15	+10	-4	+11		-9			
31+00	+17	+15	-6	+11		-12			
25	+14	+20	-8	+6		+7			
50	+8	+10	-4	+4		+17 *			
75	+18	-4	+2	+20		-12			
32+00	+7	-1	0	+7		-26			
25	+7	+5	-2	+5		-17			
50	0	+10	-4	-4		+4			
75	+3	+10	-4	-1		+15 *			
33+00	+9	+8	-3	+6		+8			
25	+8	+10	-4	+4		+10			
50	+15	+15	-6	+9		+11			
75	+20	+23	-9	+11		+8			
34+00	+25	+28	-12	+13		+1			
25	+29	+33	-14	+15		-12			
50	+20	+25	-10	+10		-16			
75	+16	+25	-10	+6		-13			
35+00	+15	+28	-12	+3		-11			
25	+10	+25	-10	0		+6			
50	+5	+17	-7	-2		+19 *			
75	+13	+5	-2	+11		+3			
36+00	+11	+12	-5	+6		-3			
25	+8	+4	-2	+6		+4			
50	+10	+4	-2	+8		+2			
75	+12	+9	-4	+8					
37+00	+10	+6	-2	+8					

VLF-EM Data Sheet

Line : L 80E (New)

Tx. : Maine

Grid : ANOMALY "E"

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
30+00 N	+9	+10	-4	+5					
25	+6	+15	-6	0		-2			
50	+7	+21	-9	-2		+10			
75	+10	+13	-5	+5		+1			
31+00	+7	+10	-4	+3		-6			
25	+5	+10	-4	+1		-2			
50	0	-2	+1	+1		-6			
75	-3	-10	+4	+1		-11			
32+00	-7	-5	+2	-5		+2			
25	0	+10	-4	-4		+14			
50	+5	+8	-3	+2		+15 *			
75	+5	+5	-2	+3		+11			
33+00	+15	+13	-5	+10		+9			
25	+13	+16	-7	+6		+21 *			
50	+22	+14	-6	+16		+16			
75	+26	+12	-5	+21		-13			
34+00	+27	+25	-10	+17		-31			
25	+17	+25	-10	+7		-31			
50	+15	+35	-15	0		-22			
75	+10	+40	-17	-7		-2			
35+00	+5	+32	-13	-8		+20			
25	-3	-5	+2	-1		+27 *			
50	+10	+10	-4	+6		+16			
75	+15	+8	-3	+12		-3			
36+00	+13	+10	-4	+9		-9			
25	+12	+15	-6	+6		-6			
50	+8	+5	-2	+6		-8			
75	+7	+10	-4	+3					
37+00	+6	+12	-5	+1					

VLF-EM Data Sheet

Grid: Anomaly "L"

Line: L81E (New)

Tx.: Maine

Facing: South

Δ	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
30+00N	+12	+5	-2	+10					
25	+20	+12	-5	+15		-4			
50	+22	+18	-7	+15		-7			
75	+10	+10	-4	+6		+4			
31+00	+19	+5	-2	+17		-9			
25	+10	+6	-2	+8		-13			
50	+10	+10	-4	+6		-5			
75	+5	-2	+1	+6		-16			
32+00	+3	0	0	+3		-20			
25	-5	+5	-2	-7		+4			
50	+2	+15	-6	-4		+21 *			
75	+10	+15	-6	+4		+15			
33+00	+13	+17	-7	+6		+7			
25	+15	+15	-6	+9		-1			
50	+15	+16	-7	+8		-11			
75	+15	+23	-9	+6		+15			
34+00	+10	+25	-10	0		+45 *			
25	+48	+45	-19	+29		-7			
50	+30	+20	-8	+22		-47			
75	+5	+12	-5	0		-17			
35+00	+8	+10	-4	+4		+7			
25	+1	0	0	+1		+22*			
50	+12	+5	-2	+10		+20			
75	+21	+10	-4	+17		-4			
36+00	+19	+12	-5	+14		-16			
25	+12	+8	-3	+9		-12			
50	+10	+10	-4	+6		-13			
75	+9	+10	-4	+5					
37+00	+3	+14	-6	-3					

VLF-EM Data Sheet

Grid : ANOMALY "E"

Line : L82E (New)

Tx. : Maine

Facing : South

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter	Non-terrain corrected F.F.		Quad.
50	+15	+10	-4	+11					
75	+17	+10	-4	+13		-7			
30+00	+20	+16	-7	+13		-20			
25	+10	+15	-6	+4		-19			
50	+7	+13	-5	+2		-9			
75	0	+10	-4	-4		-2			
31+00	-5	-15	+6	+1		+7			
25	-9	-10	+4	-5		+26			
50	+5	-10	+4	+9		+29			
75	+11	-5	+2	+13		+6			
32+00	+18	-5	+2	+20		-26			
25	+15	+18	-7	+8		-34			
50	+11	+30	-12	-1		-11			
75	+5	+25	-10	-5		+17			
33+00	+9	+20	-8	+1		+22 *			
25	+16	+15	-6	+10		+8			
50	+10	+6	-2	+8		+5			
75	+15	+10	-4	+11		+1			
34+00	+20	+20	-8	+12		-9			
[illegible]	+12	+10	-4	+8		-3			
[illegible]	+12	+15	-6	+6		+11			
75	+16	+13	-5	+11		+12 *			
35+00	+20	+14	-6	+14		+4			
[illegible]	+20	+13	-5	+15		+3			
[illegible]	+20	+15	-6	+14		-1			
[illegible]	+20	+6	-2	+18		-17			
36+00	+16	+15	-6	+10		-20			
25	+10	+13	-5	+5		-7			
50	+10	+17	-7	+3		-5			
75	+10	+12	-5	+5					
37+00	-7	+23	-9	-2					

/

VLF-EM Data Sheet

Line : 41E

Tx. : MAINE

Grid : ANOMALY "E"

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st. Diff.	F. Filter			Quad.
39+00	-4	0	0	-4	+4				-4
+25	+6	-5	+2	+8	+13	-3			+1
+50	+5	0	0	+5	+1	-36			+1
+75	-4	0	0	-4	-23	-44			-2
40+00	-21	-5	+2	-19	-43	-13			-11
+25	-29	-12	+5	-24	-36	+31			-8
+50	-16	-10	+4	-12	-12	+44			0
+75	0	0	0	0	+8	+33			+1
41+00	+12	+9	-4	+8	+21	+21			+1
+25	+22	+21	-9	+13	+29	+6			+2
+50	+25	+21	-9	+16	+27	-9			+4
+75	+21	+25	-10	+11	+20	-6			+5
42+00	+18	+22	-9	+9	+21	+4			+5
+25	+21	+23	-9	+12	+24	+4			+7
+50	+24	+28	-12	+12	+25	0			+6
+75	+24	+26	-11	+13	+24				+5
43+00	+21	+24	-10	+11					+5

VLF-EM Data Sheet

Line : 42E

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
39+00	-18	-7	+3	-15					0
+25	-11	0	0	-11	-26				0
+50	+1	0	0	+1	-10	+26			-1
+75	-1	0	0	-1	0	+3			-1
40+00	-6	0	0	-6	-7	-17			+1
+25	-11	0	0	-11	-17	-8			+1
+50	-10	-14	+6	-4	-15	+15			+2
+75	-2	-9	+4	+2	-2	+20			+3
41+00	+3	0	0	+3	+5	+8			+1
+25	+9	+14	-6	+3	+6	-1			+3
+50	+10	+22	-9	+1	+4	0			+3
+75	+15	+24	-10	+5	+6	+9			+3
42+00	+17	+23	-9	+8	+13	+10			+2
+25	+15	+16	-7	+8	+16	+1			-1
+50	+17	+27	-11	+6	+14	0			+1
+75	+18	+19	-8	+10	+16	+6			+1
43+00	+19	+23	-9	+10	+20				0

VLF-EM Data Sheet

Grid : ....

Line : 43 E

Tx. : MAINE

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
+50	+14	0	0	+14	+19				+2
+75	+2	-8	+3	+5	-1	-49			-1
37+00	-10	-11	+4	-6	-30	-44			-2
+25	-26	-6	+2	-24	-45	-14			-6
+50	-25	-10	+4	-21	-44	+4			0
+75	-28	-12	+5	-23	-41	+16			+3
38+00	-22	-11	+4	-18	-28	+24			+3
+25	-14	-9	+4	-10	-17	+14			+3
+50	-10	-7	+3	-7	-14	+5			+4
+75	-7	0	0	-7	-12	+8			+3
39+00	-5	0	0	-5	-6	+8			0
+25	-1	0	0	-1	-4	+1			-1
+50	-3	0	0	-3	-5	0			-1
+75	-2	0	0	-2	-4	+1			-3
40+00	0	+5	-2	-2	-4	0			-2
+25	-2	0	0	-2	-4	0			-1
+50	0	+5	-2	-2	-4	-5			+1
+75	-2	0	0	-2	-9	-6			0
41+00	0	+18	-7	-7	-10	+12			+3
+25	+3	+14	-6	-3	+3	+21			+3
+50	+6	0	0	+6	+11	+7			-1
+75	+8	+7	-3	+5	+10	-4			-1
42+00	+9	+10	-4	+5	+7	-6			-2
+25	+10	+19	-8	+2	+4	-2			0
+50	+9	+18	-7	+2	+5	0			-1
+75	+9	+15	-6	+3	+4	-2			+2
43+00	+11	+24	-10	+1	+3				-1
+25	+11	+23	-9	+2					-1

VLF-EM Data Sheet

Line : 44 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
37+00	+5	0	0	+5	-2				-3
+25	-7	0	0	-7	-28	-39			-3
+50	-21	0	0	-21	-41	-11			-4
+75	-24	-11	+4	-20	-39	+11			-1
38+00	-23	-10	+4	-19	-30	+23			+3
+25	-15	-10	+4	-11	-16	+25			+6
+50	-8	-8	+3	-5	-5	+18			+3
+75	-3	-7	+3	0	+2	+6			+2
39+00	+2	0	0	+2	+1	-3			+3
+25	+1	+5	-2	-1	-1	-1			-1
+50	0	0	0	0	0	+5			0
+75	+2	+5	-2	0	+4	+7			0
40+00	+6	+6	-2	+4	+7	-6			-1
+25	+10	+16	-7	+3	-2	-16			0
+50	+7	+30	-12	-5	-9	-15			-1
+75	+3	+17	-7	-4	-17	-17			-1
41+00	-6	+18	-7	-13	-26	-2			-1
+25	-10	+7	-3	-13	-19	+21			-2
+50	-2	+10	-4	-6	-5	+20			-1
+75	+3	+6	-2	+1	+1	+8			-2
42+00	+6	+14	-6	0	+3	+5			-2
+25	+3	0	0	+3	+6	+1			-3
+50	+3	0	0	+3	+4	-2			-4
+75	+1	0	0	+1	+4				-5
43+00	+3	0	0	+3					-5

VLF-EM Data Sheet

Line : 45 EAST

Grid :

Tx. : MAINE

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
37+00	0	0	0	0	-10				-4
+25	-10	0	0	-10	-19	-9			-7
+50	-9	0	0	-9	-19	-4			-1
+75	-10	0	0	-10	-23	0			+2
38+00	-13	0	0	-13	-19	+13			+1
+25	-8	-5	+2	-6	-10	+15			0
+50	-4	0	0	-4	-4	+16			+1
+75	0	0	0	0	+6	+17			+1
39+00	+6	0	0	+6	+13	0			+1
+25	+12	+12	-5	+7	+6	-22			+5
+50	+11	+30	-12	-1	-9	-19			+7
+75	-1	+18	-7	-8	-13	+3			+2
40+00	-5	0	0	-5	-6	+12			+2
+25	-1	0	0	-1	-1	+5			+1
+50	0	0	0	0	-1	0			+1
+75	-1	0	0	-1	-1	-1			-1
41+00	0	0	0	0	-2	-2			-1
+25	-2	0	0	-2	-3	+2			-2
+50	-1	0	0	-1	0	+4			0
+75	+1	0	0	+1	+1	-5			+1
42+00	0	0	0	0	-5	-9			+2
+25	-5	0	0	-5	-8	+3			+2
+50	-3	0	0	-3	-2	+11			-4
+75	-3	-11	+4	+1	+3				-1
43+00	0	-5	+2	+2					-4

VLF-EM Data Sheet

Line : 46 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

Δ	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter	Quad.
37+00	-8	0	0	-8	-27		-9
+25	-19	0	0	-19	-31	+16	-5
+50	-12	0	0	-12	-11	+37	-1
+75	+1	0	0	+1	+6	+22	0
38+00	+5	0	0	+5	+11	+9	0
+25	+6	0	0	+6	+15	+5	-1
+50	+9	0	0	+9	+16	-7	+1
+75	+10	+8	-3	+7	+8	-12	+1
39+00	+6	+12	-5	+1	+4	-15	+1
+25	+3	0	0	+3	-7	-31	+1
+50	-3	+16	-7	-10	-27	-22	+2
+75	-13	+9	-4	-17	-29	+5	-5
40+00	-12	0	0	-12	-22	+15	-2
+25	-16	-14	+6	-10	-14	+16	-5
+50	-15	-27	+11	-4	-6	+10	-5
+75	-11	-21	+9	-2	-4	+2	-1
41+00	-10	-20	+8	-2	-4	-2	-3
+25	-8	-14	+6	-2	-6	-6	0
+50	-7	-7	+3	-4	-10	-6	-1
+75	-8	-5	+2	-6	-12	-8	+1
42+00	-6	0	0	-6	-18	-14	+3
+25	-10	+6	-2	-12	-26	-12	+2
+50	-14	0	0	-14	-30	+3	+2
+75	-16	0	0	-16	-23	+23	+2
43+00	-10	-8	+3	-7	-7	+29	+2
+25	0	0	0	0	+6	+22	+4
+50	+6	0	0	+6	+15	+11	+4
+75	+9	0	0	+9	+17		+5
44+00	+11	+7	-3	+8			+5

VLF-EM Data Sheet

Line : 47 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
39+00	+2	0	0	+2	+4				-3
+25	+2	0	0	+2	+9	+11			-2
+50	+10	+8	-3	+7	+15	+4			+3
+75	+8	0	0	+8	+13	-21			+3
40+00	-1	-15	+6	+5	-6	-58			0
+25	-17	-15	+6	-11	-45	-46			-5
+50	-36	-5	+2	-34	-52	+18			-9
+75	-25	-16	+7	-18	-27	+35			0
41+00	-15	-15	+6	-9	-17	+13			+3
+25	-15	-16	+7	-8	-14	+14			0
+50	-11	-12	+5	-6	-3	+27			-2
+75	-2	-12	+5	+3	+13	+18			-4
42+00	+6	-11	+4	+10	+15	-13			0
+25	+1	-10	+4	+5	0	-35			-1
+50	0	+13	-5	-5	-20	-18			+3
+75	-15	0	0	-15	-18	+28			-4
43+00	-9	-15	+6	-3	+8	+46			-3
+25	+5	-14	+6	+11	+28	+23			+1
+50	+11	-15	+6	+17	+31	-3			+4
+75	+11	-7	+3	+14	+25				+3
44+00	+11	0	0	+11					+4

VLF-EM Data Sheet

Line : 48 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
39+00	0	0	0	0	+5				-5
+25	+5	0	0	+5	+9	-6			-2
+50	-2	-15	+6	+4	-1	-17			-5
+75	-7	-5	+2	-5	-8	+9			-6
40+00	-12	-21	+9	-3	+8	+6			-6
+25	-13	-55	+24	+11	-2	-29			-7
+50	-19	-15	+6	-13	-21	-12			-8
+75	-14	-14	+6	-8	-14	+11			-4
41+00	-12	-14	+6	-6	-10	+3			-1
+25	-11	-17	+7	-4	-11	-3			+1
+50	-14	-18	+7	-7	-13	-8			-1
+75	-15	-21	+9	-6	-19	-10			-2
42+00	-10	+8	-3	-13	-23	+4			+5
+25	-8	+5	-2	-10	-15	+9			+7
+50	-9	-10	+4	-5	-14	-7			+6
+75	-12	-7	+3	-9	-22	-16			+4
43+00	-15	-6	+2	-13	-30	0			+1
+25	-17	0	0	-17	-22	+24			-2
+50	-5	0	0	-5	-6	+25			0
+75	-4	-8	+3	-1	+3	+19			-5
44+00	+4	0	0	+4	+13	+15			-1
+25	+9	0	0	+9	+18				+1
+50	+12	+7	-3	+9					+2

VLF-EM Data Sheet

Line : 36 EAST

Tx. : MAINE

Grid : ANOMALY G

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
27+00									
+25	+15	+25	-10	+5	+12				+1
+50	+14	+16	-7	+7	+9	-10			+2
+75	+12	+25	-10	+2	+2	-9			+3
28+00	+11	+26	-11	0	0	-2			+3
+25	+9	+21	-9	0	0	+5			0
+50	+6	+15	-6	0	+5	+12			-2
+75	+9	+11	-4	+5	+12	+16			-1
29+00	+11	+11	-4	+7	+21	+16			0
+25	+16	+5	-2	+14	+28	-3			+1
+50	+17	+7	-3	+14	+18	-25			+4
+75	+13	+23	-9	+4	+3	-29			+3
30+00	+6	+18	-7	-1	-11	-15			+1
+25	-5	+12	-5	-10	-12	+13			-4
+50	-2	0	0	-2	+2	+14			-3
+75	+4	0	0	+4	+2	+1			+1
31+00	+2	+10	-4	-2	+3				+1
+25	+9	+11	-4	+5					+4

VLF-EM Data Sheet

Line : 37 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
27+00									
+25	+16	0	0	+16					-5
+50	+17	0	0	+17	+33				-4
+75	+12	-8	+3	+15	+32	-11			-4
28+00	+11	+10	-4	+7	+22	-41			-2
+25	+9	+57	-25	-16	-9	-48			-1
+50	+14	+54	-24	-10	-26	-1			+4
+75	+10	+25	-10	0	-10	+33			+1
29+00	+11	+10	-4	+7	+7	+23			0
+25	+9	+7	-3	+6	+13	0			+1
+50	+5	+10	-4	+1	+7	-19			0
+75	+5	+30	-12	-7	-6	-13			+2
30+00	+13	+28	-12	+1	-6	+9			+4
+25	+12	+25	-10	+2	+3	+15			+2
+50	+14	+16	-7	+7	+9	+12			+2
+75	+11	+7	-3	+8	+15	+15			-3
31+00	+16	0	0	+16	+24	+17			0
+25	+18	+5	-2	+16	+32				+3

VLF-EM Data Sheet

Grid:

Line: 38 EAST

Tx.: MAINE

Facing: SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
27+00									
+25	+7	0	0	+7	+5				-9
+50	-2	0	0	-2	-11	-21			-12
+75	-11	-5	+2	-9	-16	+12			-15
28+00	-14	-16	+7	-7	+1	+45			-14
+25	+4	-10	+4	+8	+29	+49			-9
+50	+36	+35	-15	+21	+50	+12			+5
+75	+35	+14	-6	+29	+41	-36			+9
29+00	+18	+15	-6	+12	+14	-48			+3
+25	+11	+21	-9	+2	-7	-25			+2
+50	0	+21	-9	-9	-11	+15			-2
+75	+5	+18	-7	-2	+8	+40			+1
30+00	+21	+27	-11	+10	+29	+38			+3
+25	+30	+26	-11	+19	+46	+21			+1
+50	+40	+32	-13	+27	+50	-3			+3
+25	+33	+24	-10	+23	+43	-8			+1
31+00	+20	0	0	+20	+42				-3
+25	+20	-5	+2	+22					0

VLF-EM Data Sheet

Line : 39 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st. Diff.	F. Filter			Quad.
27+00N									
+25	+5	0	0	+5	+3				-3
+50	+2	+9	-4	-2	-13	-31			-4
+75	-11	0	0	-11	-28	-17			-4
28+00	-19	-5	+2	-17	-30	+14			-3
+25	-18	-12	+5	-13	-14	+34			-4
+50	-6	-12	+5	-1	+4	+17			-3
+75	+9	+10	-4	+5	+3	-4			+1
29+00	+10	+28	-12	-2	0	+3			-2
+25	+5	+7	-3	+2	+6	+15			-3
+50	+10	+15	-6	+4	+15	+23			-2
+75	+20	+23	-9	+11	+29	+31			-1
30+00	+25	+18	-7	+18	+46	+34			-5
+25	+37	+21	-9	+28	+63	+17			-4
+50	+44	+21	-9	+35	+63	-8			-1
+75	+36	+20	-8	+28	+55	-11			-3
31+00	+33	+14	-6	+27	+52				-1
+25	+23	-5	+2	+25					-2

VLF-EM Data Sheet

Line : 40 EAST

Tx. : MAINE

Grid :

Facing : SOUTH

△	Dip Angle	Slope %	Correction Factor	Reading	1st Diff.	F. Filter			Quad.
27+00									
+25	-6	0	0	-6					-2
+50	-2	0	0	-2	-8				-1
+75	0	+12	-5	-5	-7	-1			+1
28+00	-4	0	0	-4	-9	-6			-1
+25	-11	-5	+2	-9	-13	-4			-3
+50	-10	-15	+6	-4	-13	+6			-4
+75	+1	+10	-4	-3	-7	+4			0
29+00	+3	+22	-9	-6	-9	+11			-1
+25	-1	-26	+11	+10	+4	+24			-5
+50	+1	-10	+4	+5	+15	+2			-5
+75	+7	+15	-6	+1	+6	-12			-4
30+00	+12	+25	-10	+2	+3	+2			-3
+25	+15	+22	-9	+6	+8	+16			-6
+50	+21	+19	-8	+13	+19	+26			-5
+75	+32	+27	-11	+21	+34	+22			-3
31+00	+30	+24	-10	+20	+41	-8			-1
+25	+13	+17	-7	+6	+26				-7

III A METHOD OF REDUCING TERRAIN RELIEF EFFECTS

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A METHOD OF REDUCING TERRAIN RELIEF EFFECTS FROM VLF-EM DATA

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ABSTRACT

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In VLF-observations uneven terrain relief causes distinct anomalies that originate from elliptic field polarization. This slope rotation field is produced by the interference of the radiated horizontal magnetic field with a component reflected by the earth's inclined surface. A diagram has been developed to provide the tilt and eccentricity (ratio of half axes) of the slope rotation ellipse, if the dip of the slope along the direction of the radiated magnetic field is known. It turns out to be possible to separate the influence of relief from that of local conductive bodies. The application is demonstrated on field data gathered in areas of hilly terrain.

INTRODUCTION

Electromagnetic induction by artificial very long waves has been employed in mineral research for a decade and a half. Commercially available, easily operated, light, one-man units make use of powerful naval radio stations in the VLF (very low frequency) range (15—25 kHz). The transmitter radiates both electric, and magnetic components. At sufficiently large distances from the transmitting antenna the radiated field can be considered plane and homogeneous within the area to be investigated. The primary magnetic field is linearly polarized and lies in a horizontal plane at right angles to the line that connects the selected station and the observation point.

Because of the finite conductivity of the earth there is always a secondary magnetic field present, the vector of which is parallel to the surface, provided that the ground is electrically uniform. However, with a conductive geologic body being embedded in the homogeneous half space and roughly orientated parallel to the path of propagation, a secondary magnetic field will be induced. This field interferes with the horizontal primary magnetic field. The interference of alternating fields of equal frequency; but different amplitude, phase, and direction yields an elliptically polarized field. At the point of observation the resultant field vector rotates in a plane and traces out an ellipse (Grant

0016-7142/81/0000—0000/$02.50

and West, 1965). In flat lying areas, elliptic field polarization therefore distinguishes a zone of electric heterogeneity, which may be related to geologic contacts, faults, mineralized bodies, or conductive overburden.

The general practice in VLF-prospecting is to determine the tilt angle ϕ and eccentricity q of the magnetic polarization ellipse. The tilt ϕ is the inclination of the major axis with respect to the horizontal, and the ellipticity q is the ratio of the minor to the major half axis.

The tilt ϕ is given by:

$$\tan 2\phi = \frac{2\frac{Z}{Y}\cos\delta}{1-\left(\frac{Z}{Y}\right)^2} \tag{1}$$

and the ellipticity by:

$$q = \frac{Y\,Z\sin\delta}{a^2}\,, \tag{2a}$$

$$q^2 = \frac{\left(\frac{Z}{Y}\right)^2 - \frac{(Z\cos\delta)^2}{1-\left(\frac{Z}{Y}\right)^2}}{1-\frac{(Z\cos\delta)^2}{1-\left(\frac{Z}{Y}\right)^2}} \tag{2b}$$

(Heiland, 1963; Smith and Ward, 1974) where Y = the total horizontal magnetic field; Z = the vertical component of induced magnetic field; δ = the phase-difference between the rectangular field components Y and Z; and the major half axis $a = |Z\exp(i\delta)\sin\phi + Z\cos\phi|$. The method is widely considered a quick, cheap, and easy means of reconnaissance in geophysical prospecting. It has been applied to: (a) assistance in geologic mapping (Telford et al., 1977); (b) ground follow-up of airborne EM surveys so as to exactly determine the position of electrically disturhing bodies (Jinno et al., 1975); (c) detection of shallow conductive, possibly mineralized, bodies (Eberle, 1977).

A remarkably disturbing influence on measured tilt and eccentricity data is produced by topographic relief in hilly areas. Uneven terrain relief makes significant anomalies appear which must be distinguished from conductor anomalies. Whittles (1969) first described these effects on tilt angle data. Karous (1979) and Baker and Myers (1980) have very recently dealt with the reduction of terrain relief influence from measured VLF data. Whereas Karous sug[illegible]s an analytical calculation for an approximately two-dimensional relief, which still involves a lot of computation, Baker and Myers offer a much simpler way of reduction based on model studies, but for tilt angle

This paper represents a method of correction for both tilt and eccentricity. Presuming a two-dimensional relief, the amount of terrain-produced tilt and eccentricity can be provided by use of a graph, the incoming magnetic field being at any angle with respect to the strike of morphology.

DESCRIPTION OF THE PHENOMENON

The influence of terrain relief is demonstrated hy Fig.1 which shows a section of a survey carried out in part of the Harz Mountains in central Germany. The primary magnetic field radiated by the French transmitter FUO oscillates parallel to the NW—SE orientated profile lines, whereas the strike of the Grotenberg is nearly perpendicular to the magnetic field direction.

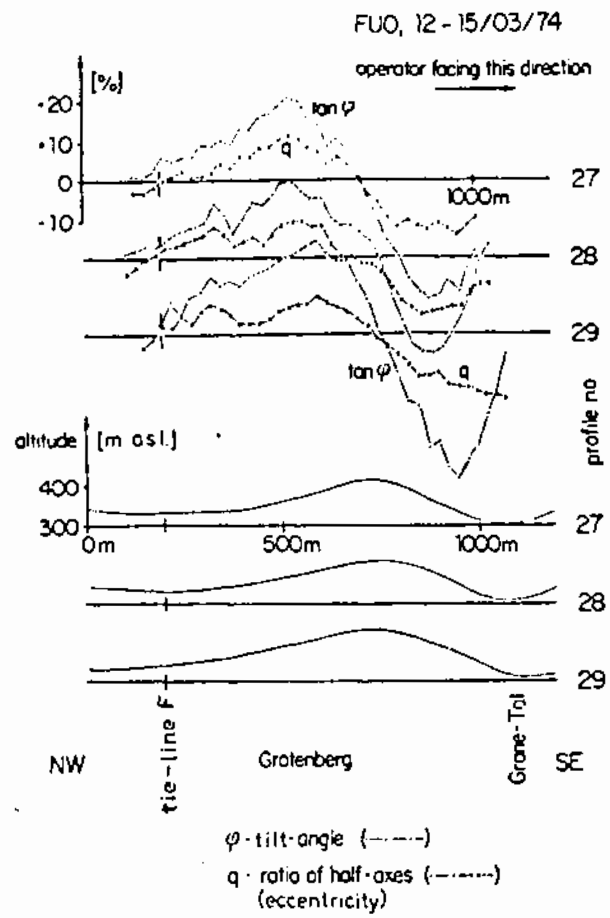

Fig.1. Very-long-wave induction anomaly produced by hilly relief; me[illegible]ed in the Harz Mountains/central Germany. In the absence of near-surface electric inhomogeneities the observed curves of tilt ($\tan\phi$) and eccentricity q have the same sign along the survey line.

The anomaly produced by terrain relief (shown in the upper part of Fig. 1) is characterized by a wide range of about 400 m between its extreme values. The measured tilt and eccentricity obviously have the same sign following the wavy terrain shape between Grotenberg and Grane valley. With the direction of observation pointing southeast, both the measured data are positive along the line section which climbs up from the northwest to the southeast; the summit gives rise to a cross-over, whereby the measured data become negative on the slope that leads down to the Grane valley. Across the valley floor there occurs another cross-over of tilt and eccentricity. A deeply buried conductive body could not produce any anomaly of this appearance because of the skin effect which makes the induced electric current density concentrate in a superficial layer and follows the shape of the terrain.

CALCULATION OF THE SLOPE ROTATION FIELD

The subsoil is supposed to be electrically homogeneous. Its surface is inclined at an angle $(90° - \tau)$ with respect to the horizontal. The incoming magnetic field from the very distant artificial source with amplitude H_{pe} is described by $H_{ye} = H_{pe} \exp(-ik_0 z_e)$ and $H_{ze} = 0$. (The terms in $\exp(-i\omega t)$ depending upon time t are neglected in this discussion.) At the sloping surface the magnetic field with amplitude $H_{pr} = R_s H_{pe}$ will be reflected. Its components are:

$$H_{yr} = H_{pr} \cos 2\tau \exp(-ik_0 z_r)$$
$$H_{zr} = -H_{pr} \sin 2\tau \exp(-ik_0 z_r)$$

(see Fig. 2). $\tau\,(>45°)$ = the angle of incidence; $k_0 = 2\pi/\lambda$, the wave number in free space; $z_e = z$, the path of the incoming magnetic field component; $z_r = y \sin 2\tau - z \cos 2\tau$, the path of the reflected magnetic field component; $R_s = R \exp(i\phi)$ = the complex reflection coefficient (the index s indicates that the horizontal electric field component E_x is directed at right angles to the plane of wave incidence).

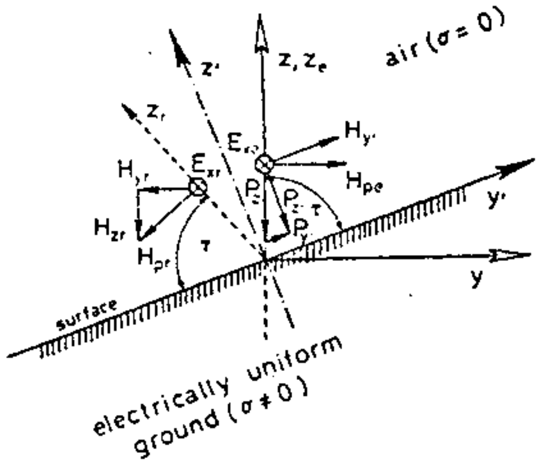

Fig. 2. Reflection of plane waves at a sloping surface of a non-layered conductive earth. The angle of wave-incidence is τ. The linear incoming magnetic field with amplitude H_{pe} and the reflected with amplitude H_{pr} oscillate parallel; the induced electric field E_x is at right angles to the y—z plane of incidence.

Considering the low height $z \approx 1.5$ m of the observation point above the surface as well as the large wavelength $\lambda \approx 15{,}000$ m the exponents of the e-functions become very small, which leads to $\exp(-ik_0 z_e) \approx \exp(-ik_0 z_r)$. The vertical component Z_r and horizontal component Y_r of the composite field vector then become:

$$Z_r = H_{zr} = -R_s H_{pe} \sin 2\tau$$
$$Y_r = H_{ye} + H_{yr} = H_{pe} + R_s H_{pe} \cos 2\tau$$

As the reflected components differ in amplitude, phase and orientation from the incoming field, an elliptically polarized interference field will result near the sloping surface, the relative magnitude of which is:

$$\frac{Z_r}{Y_r} = \hat{A} = -\frac{R_s \sin 2\tau}{1 + R_s \cos 2\tau} \qquad (3)$$

The real and imaginary parts of the complex ratio in eq. 3 can be separated:

$$Re(\hat{A}) = -\frac{R \sin 2\tau\,(R \cos 2\tau + \cos\phi)}{(1 + R \cos 2\tau \cos\phi)^2 + (R \cos 2\tau \sin\phi)^2} \qquad (4)$$

$$Im(\hat{A}) = -\frac{R \sin 2\tau \sin\phi}{(1 + R \cos 2\tau \cos\phi)^2 + (R \cos 2\tau \sin\phi)^2} \qquad (5)$$

With regard to the range of ground conductivity and relative dielectric constants as well as to the low frequencies applied, the amount R and phase ϕ of the reflection coefficient R_s are approximately given by $R \approx 1$ and $\phi \approx 180°$: very long waves are almost perfectly reflected by the earth's surface. Introducing these approximate values of R and ϕ into eqs. 4 and 5 yields:

$$Re(\hat{A}) = \cot\tau$$
$$Im(\hat{A}) = -\frac{\sin\phi}{2\sin^2\tau}\cot\tau \qquad (\tau > 45°)$$

The total amount of the relative magnitude is:

$$T = |\hat{A}| = \cot\tau \left(1 + \frac{\sin^2\phi}{4\sin^4\tau}\right)^{1/2} \approx \cot\tau\,; \qquad 1 \gg \frac{\sin^2\phi}{4\sin^4\tau}$$

It is now possible to calculate both the characteristic quantities — tilt ($\tan\phi_{top}$) and eccentricity q_{top} — of the elliptic slope-rotation field. By u eq. 1 the tilt angle ϕ_{top} can be easily determined:

$$\tan 2\phi_{top} = \frac{2\cos\delta}{\frac{1}{T} - T} = \frac{2\cos\delta}{\tan\tau - \cot\tau}$$

The phase δ between the rectangular components Z_r and Y_r will be known considering the fact that for a non-layered, well conductive earth the angle of surface impedance for very low frequencies is approximately equal to 45° (Watt, 1967, p. 185). Thus the phase δ can be set:

$$\delta = 45° + \arctan\left(\frac{Im(\hat{A})}{Re(\hat{A})}\right) = 45° - \arctan\left(\frac{\sin\phi}{2\sin^2\tau}\right) \approx 45°$$

The fact that the additional phase lag is extremely small for very long waves is due to the electric properties of the reflecting slope. The tilt angle ϕ_{top} therefore results in:

$$\phi_{top} = \tfrac{1}{2}\arctan\left(\frac{(2)^{1/2}}{\tan\tau - \cot\tau}\right) \qquad (8)$$

Analogous to eq. 2 the eccentricity of the slope-rotation field is defined by $q_{top} = Im[\hat{A}\,\exp(i\delta)]$ which leads to a suitable approximation:

$$q_{top} \approx -\tfrac{1}{2}\cot\tau\,\sin(\phi + \delta)$$

With regard to the phase lag $\phi \approx \pi$ of reflection and the phase $\delta \approx \pi/4$ between the rectangular field components Z_r and Y_r, the eccentricity becomes:

$$q_{top} \approx \frac{\sqrt{2}}{4}\cot\tau \qquad (9)$$

The slope-rotation field of tilt (eq. 8) and eccentricity (eq. 9) is generated 'up hill and down dale'. This near-surface composite field of a wave with grazing incidence is like that of the so-called Zenneck surface wave (Grosskopf, 1970, pp. 364—365). It is a guided wave, the amplitude of which decays in the transverse y direction as well as in the z direction. Its path of propagation is orientated at right angles to that of the radiated primary field as well as to the general strike of morphology. The vector of propagation (Poynting vector) that belongs to the incoming field of a distant source therefore deviates from the true path of propagation near the hillside and is slightly inclined towards the ridge. This corresponds to the well-known fact that reception of radio signals is frequently better on top of a hill than in a valley.

REDUCTION FROM MEASUREMENT

Ma field observations have shown that the influence of terrain reli n VLF data essentially depends upon the orientation of the primary ma field H_{y0} with respect to the general strike of the morphologic structures the project area. No effect exists if the primary field H_{y0} oscillates para the general strike, but maximum coupling for terrain relief effect occurs H_{y0} oscillates at right angles to the latter direction. In this position the p of the radiated primary wave is parallel to the general strike of morpholo structures, which points to the transmitter. There are two special cases o angle ξ_1 between the direction of the incoming magnetic field and strike morphology ($\xi_1 = 0°$ and 90°, resp.).

For any other value $0° < \xi_1 < 90°$ the component $H'_{y0} = H_{y0}\sin\xi_1$ onl gives rise to the slope-rotation field. In this frequently occurring case, th true angle τ of incidence is given by:

$$\tan\tau = \tan\tau'\,\frac{\sin\xi_2}{\sin\xi_1} \qquad (\xi_2 \neq 0)$$

where τ' = the apparent angle of incidence along the profile line that is d minable from precise topographic maps or from inclination measuremen ξ_1 = the angle between the direction of the incoming magnetic field and strike of morphology; ξ_2 = the angle between the survey line and strike morphology. Applying eq. 10 to eqs. 8 and 9 it is possible to determine slope-rotation field with the incoming magnetic field at any orientation respect to the general strike of morphology.

The quantities given by eqs. 8 and 9 for the elliptically polarized field the sloping surface of a non-layered earth are plotted in the graph of Fi a function of the true angle τ of incidence. If the inclination $(90° - \tau)$ o

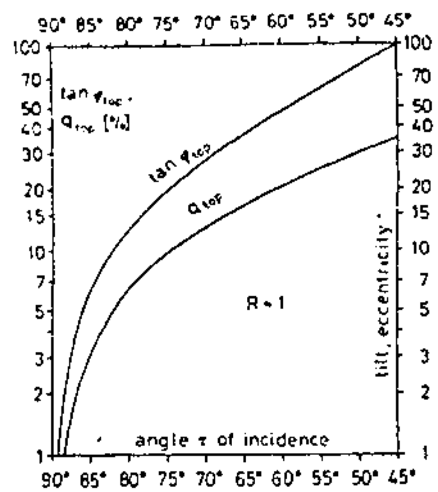

Fig. 3. Tangent of tilt angle ($\tan\phi_{top}$) and eccentricity q_{top} of the elliptic magnetic ference field as a function of the true angle τ of incidence. The amount R of the re coefficient is supposed to be 1.

lope along the direction of the incoming magnetic field H_{y0} is known by ither *inclination measurements* or precise topographic maps, the tilt and ccentricity of the slope rotation field can easily be taken from this graph.

By comparison of the measured and calculated curves it is possible to at ast qualitatively separate the influence of terrain relief from conductor nomalies. Differences between the measured values and the diagram values re produced by any type of local conductive bodies, some of which are the im of geophysical prospecting.

PPLICATION TO SURVEY DATA

Along survey line 29 of the Grotenberg—Granetal area, where the influence f terrain relief was first represented (cf. Fig. 1), tilt ($\tan \phi_{top}$) and eccentricity $_{top}$ of the slope rotation field were determined by the graph of Fig. 3, the nclination ($90° - \tau$) of terrain being taken from the topographic map 1 : 25 000) sheet no. 4128, Clausthal—Zellerfeld (Fig. 4). On this line, angles

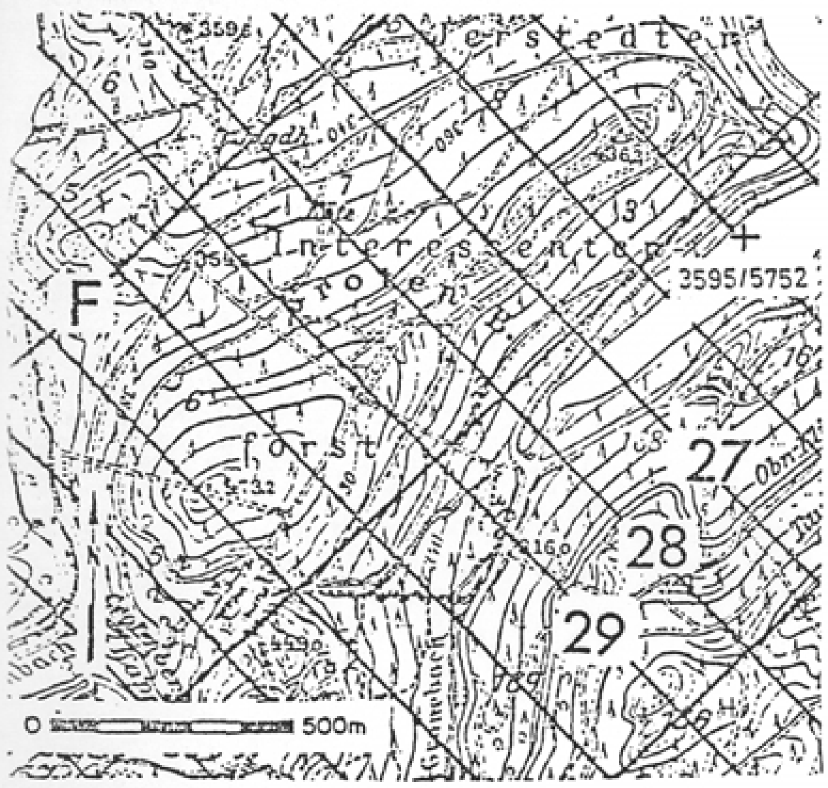

Fig. 4. Section of the topographic map (1 : 25 000) sheet no. 4128 Clausthal—Zellerfeld, which was used for the determination of the true angle τ of wave incidence in the Grotenberg—Granetal area.

of $60° < \xi_1 < 80°$, and $70° < \xi_2 < 90°$ were encountered. The diagram values of tilt ($\tan \phi_{top}$) and eccentricity q_{top} evidently fit the observed data ($\tan \phi, q$) pretty well (cf. Fig. 5), i.e., the large anomaly registered between the tie line F

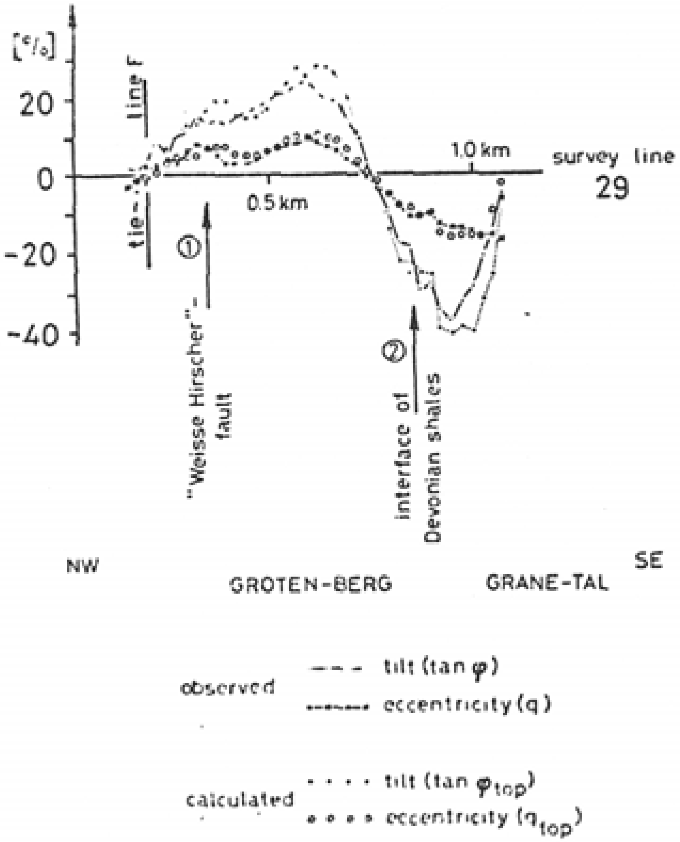

Fig. 5. Calculated terrain relief produced tilt ($\tan \phi_{top}$) and eccentricity q_{top} of the magnetic polarization ellipse in comparison with the observed tilt ($\tan \phi$) and eccentricity q on survey line 29 in the Grotenberg—Grane-Tal area.

and Grane-Tal is produced by elliptic polarization that results from the sloping surface of the region. This anomaly is without any interest for geophysical prospecting. However, the slight differences perceptible in each pair of tilt- and eccentricity-curves can be significant. The anomaly 200 m east of the control line F (see arrow 1) is produced by the regional Weisse Hirscher fault; the anomaly near Grane-Tal (see arrow 2) indicates an interface between different Devonian shales.

The biggest sulfidic mineralization of the Harz Mountains is the Rammelsberg zinc—lead deposit near the town of Goslar. A few survey lines were arranged for measurements in the surroundings of the mine. In spite of

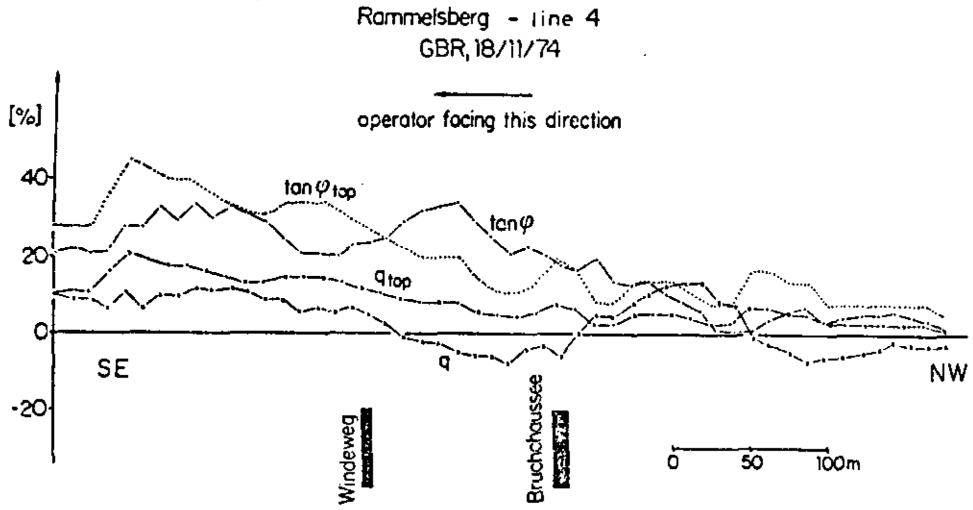

Fig. 6. Tilt (tan φ) and eccentricity (q) observations on survey line 4 of the Rammelsberg area near the town of Goslar/Harz. A trained interpretor will already recognize the anomaly of tilt values in the vicinity of Windeweg in spite of the strong influence from accentuated terrain relief. Tilt ($\tan\phi_{top}$) and eccentricity (q_{top}) of the slope rotation field are calculated.

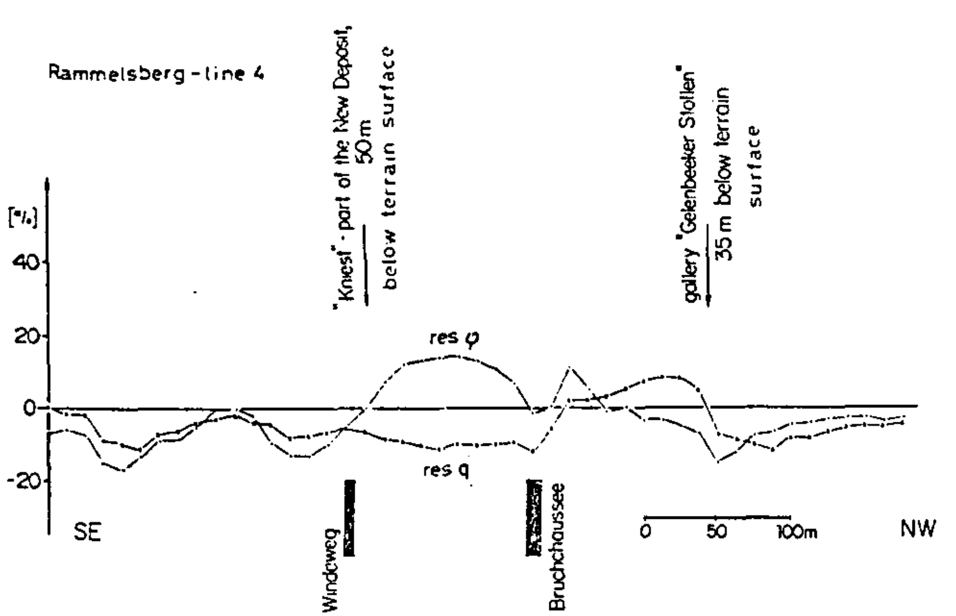

Fig. 7. Residual tilt (res φ) and eccentricity (res q) on survey line 4 of the Rammelsberg area. The res φ anomaly near Windeweg appears much more clearly than the corresponding tilt (tan φ). It is produced by the shallow Kniest part of the Rammelsberg zinc—lead sulfide deposit.

strongly accentuated terrain relief, which rather distorts the observed d... the shallow Kniest part of the deposit could be detected by VLF-observatio... A simple model calculation yielded an approximate depth of 50 m for the to... of this mineralized body. Fig. 6 shows the observed values of tilt (tan φ) and eccentricity q as well as the calculated ($\tan\phi_{top}$, q_{top}) due to the slope-rotation field along line 4.

In Fig. 7 the residual tilt (resϕ) and eccentricity (res$q$) are represented. The... are the difference of measured and calculated tilt and eccentricity at each observation point. This way of representing terrain-corrected conductor anomalies might be justified if linear superposition of the field components produced by sloping terrain relief and buried conductive bodies, occurs. However, anomalies that are due to inhomogeneities of underground conductivity are often emphasized by this crude manner of reducing relief effects.

CONCLUSIONS

The calculated tilt values ($\tan\phi_{top}$[%]) of Fig. 3 are in good agreement with the experimental real component data dR [%] of Baker and Myers (1980) up to an angle of slope inclination of 15° and an angle of wave incidence of 75°. Beyond this value, however, a slight difference between calculated and experimental data is observed. It grows with increasing angles of slope inclination, which may be due to both mathematical assumptions and model arrangements in the determination of the relief effect on VLF dat...

Anomalies that are produced by sloping terrain relief will frequently superpose those of the geologic conductors in which the prospector is much more interested. The correction method derived from the model of a non-layered earth with an inclined surface is a simple, practical procedure that allows us to remove the influence of terrain relief from field data and makes geologic signals appear more clearly. It has proved to be helpful in interpretational work.

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IV ASSAY CERTIFICATES

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DATE REPORT MAILED: Dec. 8/87

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CUTTING AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: ..D. Toye.. DEAN TOYE, CERTIFIED B.C. ASSAYER

MINGOLD RESOURCES File # 87-5984 Page 1

SAMPLE#	AG PPM	AU* PPB
SRH-1 20-25	.7	29
SRH-1 25-30	.5	9
SRH-1 30-35	.2	11
SRH-1 35-40	.5	9
SRH-1 40-45	.5	19
SRH-1 45-50	.1	4
SRH-1 50-55	.2	12
SRH-1 55-60	.2	22
SRH-1 60-65	.1	8
SRH-1 65-70	.1	3
SRH-1 75-80	.2	7
SRH-1 80-85	.2	3
SRH-1 85-90	.2	1
SRH-1 90-95	.2	11
SRH-1 95-100	.2	8
SRH-1 100-105	.5	10
SRH-1 105-110	.2	7
SRH-1 110-115	.1	9
SRH-1 115-120	.1	11
SRH-1 120-125	.2	13
SRH-1 125-130	.3	2
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SRH-1 200-205	.1	6
SRH-1 210-215	.1	3
SRH-1 215-220	.3	4
SRH-1 220-225	.1	2
STD C/AU-R	7.3	520

SAMPLE#	AG PPM	AU* PPB
SRH-1 225-230	.1	1
SRH-1 230-235	.1	1
SRH-1 235-240	.1	1
SRH-1 240-245	.5	17
SRH-1 245-250	.1	1
SRH-1 250-255	.1	4
SRH-1 255-260	.1	1
SRH-1 260-265	.4	3
SRH-1 265-270	.2	1
SRH-1 270-275	.3	3
SRH-1 275-280	.7	1
SRH-1 280-285	.5	1
SRH-1 285-290	.6	4
SRH-1 290-295	.4	3
SRH-1 295-300	.3	1
SRH-2 25-30	.4	4
SRH-2 30-35	.2	3
SRH-2 35-40	.1	1
SRH-2 40-45	.1	1
SRH-2 45-50	.1	1
SRH-2 50-55	.2	1
SRH-2 65-70	.2	1
SRH-2 70-75	.2	1
SRH-2 80-85	.1	1
SRH-2 90-95	.1	2
SRH-2 95-100	.1	1
SRH-2 100-105	.2	1
SRH-2 105-110	.1	1
SRH-2 110-115	.1	1
SRH-2 115-120	.2	1
SRH-2 120-125	.2	27
SRH-2 135-140	.2	1
SRH-2 140-145	.2	48
SRH-2 150-155	.2	3
SRH-2 160-165	.1	1
SRH-2 165-170	.4	3
STD C/AU-R	7.6	490

SAMPLE#	AG PPM	AU* PPB
SRH-2 170-175	.3	1
SRH-2 190-195	.1	1
SRH-2 195-200	.4	1
SRH-2 200-205	.3	5
SRH-2 205-210	.5	10
SRH-2 210-215	.1	11
SRH-2 220-225	.4	1
SRH-2 225-230	.3	1
SRH-2 230-235	.1	1
SRH-2 235-240	.1	1
SRH-2 240-245	.2	6
SRH-2 245-250	.1	3
SRH-2 260-265	.6	1
SRH-2 265-270	.1	1
SRH-2 270-275	.1	3
SRH-2 275-280	.1	6
SRH-2 280-285	.1	5
SRH-2 285-290	.1	1
SRH-3 50-55	.9	23
SRH-3 55-60	.3	8
SRH-3 60-65	.2	27
SRH-3 65-70	.3	9
SRH-3 70-75	.5	10
SRH-3 75-80	.1	4
SRH-3 80-85	.1	6
SRH-3 85-90	.4	1
SRH-3 90-95	.1	1
SRH-3 95-100	.2	1
SRH-3 100-105	.1	5
SRH-3 105-110	.7	39
SRH-3 110-115	.6	10
SRH-3 115-120	.5	28
SRH-3 120-125	.1	4
SRH-3 125-130	.1	3
SRH-3 130-135	.1	1
SRH-3 135-140	.1	1
STD C/AU-R	7.5	490

SAMPLE#	AG PPM	AU* PPB
SRH-3140-145	.1	1
SRH-3 145-150	.1	1
SRH-3 150-155	.2	6
SRH-3 155-160	.1	1
SRH-3 160-165	.1	1
SRH-3 165-170	.1	1
SRH-3 170-175	.2	4
SRH-3 175-180	.1	1
SRH-3 180-185	.1	2
SRH-3 190-195	.1	1
SRH-3 195-200	.2	1
SRH-3 200-205	.1	1
SRH-3 205-210	.4	1
SRH-3 210-215	.2	1
SRH-3 215-220	1.0	1
SRH-3 220-225	.3	2
SRH-3 225-230	.5	1
SRH-3 230-235	.1	1
SRH-3 235-240	.3	1
SRH-3 240-245	.2	1
SRH-3 245-250	.1	2
SRH-3 250-255	.1	6
SRH-3 265-270	.1	1
SRH-3 270-275	.2	1
SRH-3 280-285	.2	1
SRH-3 285-290	.1	1
SRH-3 290-295	.2	4
SRH-3 295-300	.1	2
SRH-3 300-305	.3	1
SRH-3 305-310	.1	3
SRH-3 310-315	.4	6
SRH-3 315-320	.5	7
SRH-3 325-330	.2	6
SRH-3 330-335	.6	2
STD C/AU-R	7.5	505
SRH-3 335-340	.7	1
SRH-3 340-345	.9	1

SAMPLE#	AG PPM	AU* PPB
SRH-3 345-350	.1	1
SRH-3 355-360	.1	1
SRH-3 360-365	.1	1
SRH-3 365-370	.1	2
SRH-3 370-375	.1	1
SRH-3 375-380	.1	1
SRH-3 380-385	.1	2
SRH-3 385-390	.1	1
SRH-3 390-395	.1	1
SRH-3 395-400	.1	1
SRH-3 400-405	.1	3
SRH-3 405-410	.1	1
SRH-3 410-415	.2	1
SRH-3 415-420	.1	1
SRH-3 420-425	.1	1
SRH-3 425-430	.1	1
SRH-3 430-435	.2	2
SRH-3 435-440	.2	11
SRH-3 440-445	.5	7
SRH-3 445-450	.4	2
SRH-3 450-455	.1	1
SRH-3 455-460	.1	3
SRH-3 460-465	.2	2
SRH-3 465-470	.2	5
SRH-4 10-15	.1	1
SRH-4 15-20	6.3	120
SRH-4 20-25	41.9	300
SRH-4 25-30	31.9	380
SRH-4 30-35	4.8	89
SRH-4 35-40	.6	12
SRH-4 40-45	.4	21
SRH-4 45-50	.1	1
SRH-4 50-55	.3	2
SRH-4 55-60	.3	5
SRH-4 60-65	.4	7
SRH-4 65-70	1.5	45
STD C/AU-R	7.3	520

SAMPLE#	AG PPM	AU* PPB
SRH-4 70-75	.5	13
SRH-4 75-80	.4	8
SRH-4 80-85	.7	18
SRH-4 85-90	.9	15
SRH-4 90-95	.7	22
SRH-4 95-100	1.1	29
SRH-4 100-105	.4	11
SRH-4 105-110	.5	9
SRH-4 110-115	.6	10
SRH-4 115-120	.4	14
SRH-4 120-125	25.3	4170
SRH-4 125-130	46.2	2090
SRH-4 130-135	35.4	650
SRH-4 135-140	8.0	440
SRH-4 140-145	6.1	187
SRH-4 145-150	3.5	113
SRH-4 150-155	2.3	74
SRH-4 155-160	2.0	31
SRH-4 160-165	3.7	58
SRH-4 165-170	5.2	34
SRH-4 170-175	5.1	86
SRH-4 175-180	3.7	128
SRH-4 180-185	3.6	89
SRH-4 185-190	4.3	38
SRH-4 190-195	4.6	93
SRH-4 195-200	1.9	43
SRH-4 200-205	1.9	46
SRH-4 205-210	1.1	27
SRH-4 210-215	.8	33
SRH-4 215-220	.2	9
SRH-4 220-225	.6	18
SRH-4 225-230	.7	16
SRH-5 20-25	1.0	45
SRH-5 25-30	12.5	219
SRH-5 30-35	1.5	12
SRH-5 35-40	.2	6
STD C/AU-R	7.5	510

SAMPLE#	AG PPM	AU* PPB
SRH-5 40-45	3.9	29
SRH-5 45-50	3.4	48
SRH-5 50-55	2.8	26
SRH-5 55-60	4.7	220
SRH-5 60-65	2.2	95
SRH-5 65-70	1.3	41
SRH-5 70-75	8.6	54
SRH-5 75-80	9.0	121
SRH-5 80-85	12.0	87
SRH-5 85-90	6.7	83
SRH-5 90-95	.9	12
SRH-5 95-100	.4	3
SRH-5 100-105	.3	11
SRH-5 105-110	.2	1
SRH-5 110-115	.1	1
SRH-5 115-120	.1	1
SRH-5 120-125	.2	13
SRH-5 125-130	.1	1
SRH-5 130-135	.1	1
SRH-5 135-140	1.1	33
STD C/AU-R	[illegible]	510
SRH-5 140-145	1.0	49
SRH-5 145-150	.8	20
SRH-5 150-155	1.5	29
SRH-5 155-160	1.4	25
SRH-5 160-165	4.7	148
SRH-5 165-170	7.6	139
SRH-5 170-175	7.2	230
SRH-5 175-180	4.1	159
SRH-5 180-185	19.6	187
SRH-5 185-190	8.5	270
SRH-5 190-195	7.5	136
SRH-5 195-200	4.5	101
SRH-5 200-205	.7	19
SRH-5 205-210	.1	1
SRH-5 210-215	1.3	29
SRH-5 215-220	.1	3

SAMPLE#	AG PPM	AU* PPB
SRH-5 220-225	1.0	19
SRH-5 225-230	.8	33
SRH-5 230-235	1.4	79
SRH-5 235-240	2.3	87
SRH-5 240-245	1.6	54
SRH-5 245-250	1.8	83
SRH-5 250-255	.7	32
SRH-5 255-260	1.9	87
SRH-5 260-265	1.6	33
SRH-5 265-270	1.1	43
SRH-5 270-275	1.5	44
SRH-5 275-280	.8	36
SRH-5 280-285	1.8	47
SRH-5 285-290	1.0	34
SRH-5 290-295	.6	25
SRH-5 295-300	.5	17
SRH-6 35-40	2.5	27
SRH-6 40-45	7.8	101
SRH-6 45-50	5.8	105
SRH-6 50-55	2.7	75
SRH-6 55-60	9.0	102
SRH-6 60-65	3.5	101
SRH-6 65-70	4.1	38
SRH-6 70-75	5.3	43
SRH-6 75-80	9.2	83
SRH-6 80-85	18.1	92
SRH-6 85-90	29.7	280
SRH-6 90-95	5.8	24
SRH-6 95-100	2.3	10
SRH-6 100-105	1.2	6
SRH-6 105-110	.3	3
SRH-6 110-115	.8	29
SRH-6 115-120	.3	15
SRH-6 120-125	.3	7
SRH-6 125-130	.1	6
SRH-6 130-135	.1	2
STD C/AU-R	7.4	510

SAMPLE#	AG PPM	AU* PPB
SRH-6 135-140	.1	1
SRH-6 140-145	.3	1
SRH-6 145-150	.3	1
SRH-6 150-155	.7	1
SRH-6 155-160	.4	3
SRH-6 160-165	1.7	8
SRH-6 165-170	1.0	7
SRH-6 170-175	.9	16
SRH-6 175-180	1.4	17
SRH-6 180-185	1.4	13
SRH-6 185-190	2.1	12
STD C/AU-R	7.3	500
SRH-6 190-195	1.4	15
SRH-6 195-200	2.4	19
SRH-6 200-205	1.5	7
SRH-6 205-210	.6	27
SRH-6 210-215	.8	17
SRH-6 215-220	.5	16
SRH-6 220-225	.5	12
SRH-6 225-230	.1	8
SRH-6 230-235	.5	18
SRH-6 235-240	.2	13
SRH-6 240-245	.8	9
SRH-6 245-250	.3	5
SRH-6 250-255	.7	4
SRH-6 255-260	.3	1
SRH-6 260-265	.6	1
SRH-6 265-270	.2	1
SRH-6 270-275	.8	2
SRH-6 275-280	.3	3
SRH-6 280-285	.5	1
SRH-6 285-290	.3	1
SRH-6 290-295	.3	3
SRH-6 295-300	.2	1

SAMPLE#	AG PPM	AU* PPB
54130	.6	17
54142	.3	20
54144	.1	1
54157	.3	3
54160	.1	6
54182	.4	14
54183	.1	1
54186	1.0	1
54188	.1	1
54195	.2	5
54196	.2	10
54200	.1	1
54202	.2	7
54206	.3	1
54207	.1	7
54208	.5	8
54214	.2	7
54218	.2	1
54222	.1	4
54229	.1	8
54230	.2	35
54258	.1	1
54272	.1	1
54273	.1	1
54277	.1	1
54291	.3	1
STD C/AU-R	7.4	470

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE (604) 253-3158 FAX (604) 253-1716

DATE RECEIVED: DEC 1 1987
DATE REPORT MAILED: Dec. 8/87..

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: CUTTING AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

ASSAYER: ..D. Toye.. DEAN TOYE, CERTIFIED B.C. ASSAYER

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SAMPLE#	AG PPM	AU* PPB
BRH-1 19-25	.1	6
BRH-1 25-30	.1	1
BRH-1 30-35	.1	2
BRH-1 35-40	.1	1
BRH-1 40-45	.1	1
BRH-1 45-50	.1	2
BRH-1 50-55	.1	2
BRH-1 55-60	.2	1
BRH-1 60-65	4.4	910
BRH-1 65-70	6.1	2150
BRH-1 70-75	2.6	320
BRH-1 75-80	3.0	118
BRH-1 80-85	.5	51
BRH-1 85-90	1.3	76
BRH-1 90-95	.3	29
BRH-1 95-100	.8	50
BRH-1 100-105	.4	49
BRH-1 105-110	.4	29
BRH-1 110-115	.4	43
BRH-1 115-120	.4	300
BRH-2 10-15	.1	1
BRH-2 15-20	.1	4
BRH-2 20-25	.1	1
BRH-2 25-30	.2	1
BRH-2 30-35	.1	1
BRH-2 35-40	.1	1
BRH-2 40-45	.1	1
BRH-2 45-50	.1	1
BRH-2 50-55	.1	1
BRH-2 55-60	.1	1
BRH-2 60-65	.1	2
BRH-2 65-70	.1	1
BRH-2. 70-75	.2	1
BRH-2 75-80	.3	1
BRH-2 80-85	.1	3
BRH-2 85-90	.1	2
STD C/AU-R	7.3	485

SAMPLE#	AG PPM	AU* PPB
BRH-2 90-95	.1	1
BRH-2 95-100	.1	3
BRH-2 100-105	.2	1
BRH-2 105-110	.1	1
BRH-2 110-115	.1	1
BRH-2 115-120	.2	1
BRH-2 120-125	.1	1
BRH-2 125-130	.1	2
BRH-2 130-135	.1	1
BRH-2 135-140	.1	2
BRH-2 140-145	.3	1
BRH-2 145-150	.1	1
BRH-2 150-155	.2	4
BRH-2 155-160	.1	1
BRH-2 160-165	.1	3
BRH-2 165-170	.1	1
BRH-2 170-175	.1	2
BRH-2 175-180	.2	3
BRH-2 180-185	.1	1
BRH-2 185-190	.1	1
BRH-2 190-195	.1	1
BRH-2 195-200	.1	2
BRH-2 200-205	.1	1
BRH-2 205-210	.1	3
BRH-2 210-215	.5	120
BRH-2 215-220	.1	48
BRH-2 220-225	1.5	320
BRH-2 225-230	.9	210
BRH-2 230-235	2.8	870
BRH-2 235-240	.7	97
BRH-2 240-245	.6	91
BRH-2 245-250	.4	97
BRH-2 250-255	.2	59
BRH-2 255-260	.3	32
BRH-2 260-265	.2	15
BRH-2 265-270	.4	13
STD C/AU-R	7.5	490

SAMPLE#	AG PPM	AU* PPB
BRH-2 270-275	.2	5
BRH-2 275-280	.1	3
BRH-3 10-15	.3	1
BRH-3 15-20	.1	1
BRH-3 20-25	.2	1
BRH-3 25-30	.3	6
BRH-3 30-35	.1	1
BRH-3 35-40	.1	1
BRH-3 40-45	.1	1
BRH-3 45-50	.2	1
BRH-3 50-55	.1	1
BRH-3 55-60	.2	1
BRH-3 60-65	.1	1
BRH-3 65-70	.1	1
BRH-3 70-75	.1	1
BRH-3 75-80	.1	1
BRH-3 80-85	.4	1
BRH-3 85-90	.1	1
BRH-3 90-95	.1	1
BRH-3 95-100	.1	1
BRH-3 100-105	.1	1
BRH-3 105-110	.1	1
BRH-3 110-115	.3	2
BRH-3 115-120	.2	1
BRH-3 120-125	.1	1
BRH-3 125-130	.2	1
BRH-3 130-135	.1	1
BRH-3 135-140	.1	1
BRH-3 140-145	.1	3
BRH-3 145-150	.2	1
BRH-3 150-155	.3	1
BRH-3 155-160	.2	1
STD C/AU-R	7.4	510
BRH-3 160-165	.1	1
BRH-3 165-170	.2	1
BRH-3 170-175	.3	1
BRH-3 175-180	.1	1

SAMPLE#	AG PPM	AU* PPB
BRH-3 180-185	.1	1
BRH-3 185-190	.1	1
BRH-3 190-195	.1	3
BRH-3 195-200	.1	1
BRH-3 200-205	.1	1
BRH-3 205-210	.1	1
BRH-3 210-215	.1	4
BRH-3 215-220	.1	1
BRH-3 220-225	.1	1
BRH-3 225-230	.1	1
BRH-3 230-235	.1	1
BRH-3 235-240	.1	8
BRH-3 240-245	.7	230
BRH-3 245-250	1.2	350
BRH-3 250-255	1.3	370
BRH-3 255-260	.2	43
BRH-3 260-265	.1	38
BRH-3 265-270	.4	26
BRH-3 270-275	.6	58
BRH-3 275-280	.3	21
BRH-4 15-20	.1	1
BRH-4 20-25	.1	1
BRH-4 25-30	.1	1
BRH-4 30-35	.1	1
BRH-4 35-40	.3	1
BRH-4 40-45	.3	1
BRH-4 45-50	.1	1
BRH-4 50-55	.1	1
BRH-4 55-60	.1	1
BRH-4 60-65	.1	2
BRH-4 65-70	.3	1
BRH-4 70-75	.1	1
BRH-4 75-80	.2	1
BRH-4 80-85	.2	1
BRH-4 85-90	.2	1
BRH-4 90-95	.2	1
STD C/AU-R	7.4	500

SAMPLE#	AG PPM	AU* PPB
BRH-4 95-100	.1	11
BRH-4 100-105	.2	4
BRH-4 105-110	.2	2
BRH-4 110-115	.2	2
BRH-4 115-120	.2	3
BRH-4 120-125	.1	1
BRH-4 125-130	.1	1
BRH-4 130-135	.4	79
BRH-4 135-140	.1	9
BRH-4 140-145	.1	4
BRH-4 145-150	.1	3
BRH-4 150-155	.1	4
BRH-4 155-160	.2	1
BRH-4 160-165	.2	1
BRH-4 165-170	.2	2
BRH-4 170-175	.1	4
BRH-4 175-180	.1	1
BRH-4 180-185	.1	2
BRH-4 185-190	.2	1
BRH-4 190-195	.1	1
BRH-4 195-200	.1	1
BRH-4 200-205	.1	1
BRH-4 205-210	.1	1
BRH-4 210-215	.1	1
BRH-4 215-220	.1	1
BRH-4 220-225	.2	1
BRH-4 225-230	.2	1
20-25→ BRH-5 25-30	.1	1
30-35→ BRH-5 35-40	.2	1
BRH-5 40-45	.1	2
BRH-5 45-50	.1	1
BRH-5 50-55	.1	1
BRH-5 55-60	.1	3
BRH-5 60-65	.1	1
BRH-5 65-70	.1	1
BRH-5 70-75	.1	1
STD C/AU-R	7.6	510

	SAMPLE#	AG PPM	AU* PPB
	BRH-5 75-80	.1	6
	BRH-5 80-85	.2	12
85-90 →	BRH-5 90-95	.1	17
	BRH-5 95-100	.3	10
100-105 →	BRH-5 105-110	.3	12
	BRH-5 110-115	.2	7
	BRH-5 115-120	.2	1
120-125 →	BRH-5 125-130	.2	1
	BRH-5 130-135	.2	2
	BRH-5 135-140	.4	8
140-145 →			
	BRH-5 145-150	.2	1
	BRH-5 150-155	.1	1
	BRH-5 155-160	.3	2
	BRH-5 160-165	.1	1
	BRH-5 165-170	.1	1
	BRH-5 170-175	.1	1
	BRH-5 175-180	.2	1
	BRH-5 180-185	.2	1
	BRH-5 185-190	.3	9
	BRH-5 190-195	.2	3
	BRH-5 195-200	.2	20
	BRH-5 200-205	.1	4
	BRH-5 205-210	.2	3
	BRH-5 210-215	.1	1
	BRH-5 215-220	.1	1
	BRH-5 220-225	.1	3
	BRH-5 225-230	.1	1
	BRH-5 230-235	.1	2
	BRH-5 235-240	.1	1
	BRH-5 240-245	.3	1
	BRH-5 245-250	.2	1
	BRH-5 250-255	.1	1
	BRH-5 255-260	.1	1
	BRH-5 260-265	.2	2
	BRH-5 265-270	.1	1
	BRH-5 270-275	.2	1
	STD C/AU-R	7.3	510

	SAMPLE#	AG PPM	AU* PPB
	BRH-5 275-280	1.1	6
	BRH-5 280-285	.2	5
285 290→	BRH-5 290-295	.2	1
	BRH-5 295-300	.1	3
	BRH-5 300-305	.1	1
	BRH-5 305-310	.1	5
310-312→	BRH-6 50-55	.1	3
	BRH-6 55-60	.3	11
	BRH-6 60-65	.2	40
	BRH-6 65-70	.6	64
	BRH-6 70-75	1.2	60
	BRH-6 75-80	.3	18
	BRH-6 80-85	.3	15
	BRH-6 85-90	.3	11
	BRH-6 90-95	.1	7
	BRH-6 95-100	.3	5
	BRH-6 100-105	.2	8
	BRH-6 105-110	.1	1
	BRH-6 110-115	.2	1
	BRH-6 115-120	.1	1
	BRH-6 120-125	.1	1
	BRH-6 125-130	.1	1
	BRH-6 130-135	.2	6
	BRH-6 135-140	.1	1
	BRH-6 140-145	.1	7
	BRH-6 145-150	.1	12
	BRH-6 150-155	.2	11
	BRH-6 155-160	.3	1
	BRH-6 160-165	.1	13
	BRH-6 165-170	.1	1
	BRH-6 170-175	.1	3
	BRH-6 175-180	.1	1
	BRH-6 180-185	.1	1
	BRH-6 185-190	.1	1
	BRH-6 190-195	.1	1
	BRH-6 195-200	.1	4
	STD C/AU-R	7.3	490

SAMPLE#	AG PPM	AU* PPB
BRH-6 200-205	.2	1
BRH-6 205-210	.3	1
BRH-6 210-215	.4	1
BRH-6 215-220	.5	1
BRH-7 20-25	.4	1
BRH-7 25-30	.2	1
BRH-7 30-35	.2	2
BRH-7 35-40	.1	1
BRH-7 40-45	.1	1
BRH-7 45-50	.1	2
BRH-7 50-55	.2	1
BRH-7 55-60	.1	1
BRH-7 60-65	.1	1
BRH-7 65-70	.2	1
BRH-7 70-75	.3	1
BRH-7 75-80	.2	1
BRH-7 80-85	.1	1
BRH-7 85-90	.1	2
BRH-7 90-95	.1	1
BRH-7 95-100	.2	1
BRH-7 100-105	.1	4
BRH-7 105-110	.1	1
BRH-7 110-115	.2	1
BRH-7 115-120	.1	1
BRH-7 120-125	.3	3
BRH-7 125-130	.2	1
BRH-7 130-135	.2	3
BRH-7 135-140	.1	1
BRH-7 140-145	.1	1
BRH-7 145-150	.2	1
BRH-7 150-155	.1	1
BRH-7 155-160	.1	1
BRH-7 160-165	.2	4
BRH-7 165-170	.3	1
BRH-7 170-175	.2	1
BRH-7 175-180	.1	1
STD C/AU-R	7.5	490

SAMPLE#	AG PPM	AU* PPB
BRH-7 180-185	.1	4
BRH-7 185-190	.1	1
BRH-7 190-195	.1	1
BRH-7 195-200	.2	1
BRH-7 200-205	.1	1
BRH-7 205-210	.1	5
BRH-7 210-215	.4	5
BRH-7 215-220	.2	3
BRH-7 220-225	.1	1
BRH-7 225-230	.1	1
BRH-7 230-235	.1	6
BRH-7 235-240	.1	1
BRH-7 240-245	.1	1
BRH-7 245-250	.1	4
BRH-7 250-255	.2	5
BRH-7 255-260	.1	5
BRH-7 260-265	.1	3
BRH-7 265-270	.4	1
BRH-7 270-275	.9	1
BRH-7 275-280	.4	2
BRH-7 280-285	.1	1
BRH-7 285-290	.2	1
BRH-7 290-295	.1	1
BRH-7 295-300	.1	2
BRH-8 30-35	.1	1
BRH-8 35-40	.1	1
BRH-8 40-45	.1	1
BRH-8 45-50	.1	1
BRH-8 50-55	.1	1
BRH-8 55-60	.3	4
BRH-8 60-65	.1	1
BRH-8 65-70	.1	1
BRH-8 70-75	.1	1
BRH-8 75-80	.2	7
BRH-8 80-85	.2	19
BRH-8 85-90	.1	43
STD C/AU-R	7.4	505

SAMPLE#	AG PPM	AU* PPB
BRH-8 90-95	.8	114
BRH-8 95-100	2.5	155
BRH-8 100-105	.5	61
BRH-8 105-110	2.6	740
BRH-8 110-115	.6	265
BRH-8 115-120	1.0	490
BRH-8 120-125	.3	91
BRH-8 125-130	.4	66
BRH-8 130-135	.2	19
BRH-8 135-140	.1	1
BRH-8 140-145	.1	1
BRH-8 145-150	.1	1
BRH-8 150-155	.1	1
BRH-8 155-160	.1	6
BRH-8 160-165	.1	1
BRH-8 165-170	.1	1
BRH-8 170-175	.1	2
BRH-8 175-180	.1	1
BRH-8 180-185	.3	1
BRH-8 185-190	.1	1
BRH-8 190-195	.2	15
BRH-8 195-200	.2	1
BRH-8 200-205	.3	6
BRH-8 205-210	.1	1
BRH-8 210-215	.1	1
BRH-8 215-220	.1	1
BRH-8 220-225	.1	1
BRH-8 225-230	.1	1
BRH-8 230-235	.1	1
BRH-8 235-240	.2	1
BRH-8 240-245	.1	1
BRH-8 245-250	.1	1
BRH-8 250-255	.1	1
BRH-8 255-260	.2	3
STD C/AU-R	7.6	530

SAMPLE#	AG PPM	AU* PPB
BRH-5 20-25	.2	2
BRH-5 30-35	.2	1
BRH-5 85-90	.4	25
BRH-5 100-105	.4	1
BRH-5 120-125	.1	3
BRH-5 140-145	.3	3
BRH-5 285-290	.2	2
BRH-5 310-315	.1	5
STD C/AU-R	7.6	480

V ASSAY CERTIFICATES

-DIAMOND DRILLING-

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: JUL 18 1988
DATE REPORT MAILED: July 22/88

ASSAY CERTIFICATE

- SAMPLE TYPE: P1-P5 CORE P6-P8 ROCK CHIP

ASSAYER: C. Leong D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT 620 RHUB-BARB FILE # 88-2802 Page 1

	SAMPLE#	Ag OZ/T	Au OZ/T
	C-51301	.02	.001
	C-51302	.01	.001
SDH-7	C-51303	.01	.001
	C-51304	.01	.001
	C-51305	.02	.001
	C-51306	.01	.002
	C-51307	.04	.001
	C-51308	.23	.004
	C-51309	.08	.004
	C-51310	.89	.001
	C-51311	.01	.001
	C-51312	.12	.003
	C-51313	.02	.003
	C-51314	.65	.005
	C-51315	.02	.001
	C-51316	.01	.001
SDH-8	C-51317	.03	.001
	C-51318	.01	.001
	C-51319	.01	.001
	C-51320	.06	.002
	C-51321	.03	.001
	C-51322	.11	.004
	C-51323	.04	.001
	C-51324	.02	.002
	C-51325	.02	.001
	C-51326	.02	.001
	C-51327	.04	.001
	C-51328	.01	.001
	C-51329	.01	.001
	C-51330	.02	.001
	C-51331	1.45	.001
	C-51332	.01	.001
	C-51333	.06	.001
	C-51334	.05	.001
	C-51335	.05	.002
	C-51336	.05	.002

	SAMPLE#	Ag OZ/T	Au OZ/T
	C-51337	.07	.001
	C-51338	1.23	.002
	C-51339	.03	.001
SDH-8	C-51340	.03	.001
	C-51341	.03	.001
	C-51342	5.92	.001
	C-51343	.05	.001
	C-51344	.06	.001
	C-51345	.04	.001
	C-51346	3.10	.002
	C-51347	.06	.001
	C-51348	.07	.001
	C-51349	.02	.001
	C-51350	.50	.001
	C-51351	.03	.001
	C-51352	.05	.001
	C-51353	4.61	.001
	C-51354	.06	.001
	C-51355	.04	.001
	C-51356	.03	.001
	C-51357	.05	.001
	C-51358	.01	.001
	C-51359	.03	.001
	C-51360	.01	.001
	C-51361	.01	.001
	C-51362	.01	.001
	C-51363	.03	.001
	C-51364	.03	.001
SDH-11	C-51365	.01	.001
	C-51366	.01	.001
	C-51367	.02	.001
	C-51368	.01	.001
	C-51369	.01	.001
	C-51370	.01	.001
	C-51371	.02	.001
	C-51372	.02	.001

SAMPLE#	Ag OZ/T	Au OZ/T
C-51373	.01	.001
C-51374	.02	.001
C-51375	.01	.001
C-51376	.01	.001
C-51377	.02	.001
C-51378	.03	.001
C-51379	.01	.001
C-51380	.03	.001
C-51381	.02	.001
C-51382	.01	.001
C-51383	.01	.001
C-51384	.02	.001
C-51385	.01	.001
C-51386	.01	.001
C-51387	.01	.001
C-51388	.01	.001
C-51389	.01	.001
C-51390	.02	.001
C-51391	.01	.001
C-51392	.01	.001
C-51393	.01	.001
C-51394	.01	.001
C-51395	.01	.001
C-51396	.01	.001
E-54951	.10	.003
E-54952	.03	.001
E-54953	.01	.001
E-54954	.14	.002
E-54955	.04	.001
E-54956	.02	.001
E-54957	.03	.001
E-54958	.04	.001
E-54959	.08	.004
E-54960	.06	.003
E-54961	.07	.001
E-54962	1.17	.013

SDH-7

SAMPLE#	Ag OZ/T	Au OZ/T
E-54963	.16	.003
E-54964	.06	.002
E-54965	.27	.007
E-54966	.05	.001
E-54967	.01	.001
E-54968	.01	.001
E-54969	.09	.002
E-54970	.13	.006
E-54971	.02	.001
E-54972	.04	.001
E-54973	.02	.002
E-54974	.03	.002
E-54975	.05	.003
E-54976	.01	.001
E-54977	.02	.001
E-54978	.03	.001
E-54979	.01	.001
SDH-7 E-54980	.01	.001
E-54981	.01	.001
E-54982	.02	.001
E-54983	.04	.001
E-54984	.03	.001
E-54985	.04	.001
E-54986	.01	.001
E-54987	.01	.001
E-54988	.02	.001
E-54989	.03	.001
E-54990	.01	.001
E-54991	.01	.001
E-54992	.01	.001
E-54993	.02	.001
E-54994	.01	.001
E-54995	.01	.001
E-54996	.01	.001
E-54997	.01	.001
E-54998	.02	.001

SAMPLE#	Ag OZ/T	Au OZ/T
E-54999	.03	.001
E-55000	.03	.001

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: JUL 26 1988
DATE REPORT MAILED: July 30/88

ASSAY CERTIFICATE

- SAMPLE TYPE: Core AU - 20 GM REGULAR ASSAY.

ASSAYER: C. Leong . D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT #620 RHUB-BARB FILE # 88-2967 Page 1

SDH-11

SAMPLE#	Ag OZ/T	Au OZ/T
C 51397	.01	.001
C 51398	.01	.001
C 51399	.01	.001
C 51400	.01	.001
C 51401	.40	.001
C 51402	.99	.001
C 51403	.02	.001
C 51404	.04	.001
C 51405	.46	.001
C 51406	.04	.001
C 51407	.01	.001
C 51408	.01	.001
C 51409	.02	.001
C 51410	.02	.001
C 51411	.03	.001
C 51412	.01	.001
C 51413	.01	.001
C 51414	.01	.001
C 51415	.03	.001
C 51416	.01	.001
C 51417	.01	.001
C 51418	.01	.001
C 51419	.01	.001
C 51420	.03	.001
C 51421	.03	.001
C 51422	.03	.001
C 51423	.01	.001
C 51424	.01	.001
C 51425	.02	.001
C 51426	.01	.001
C 51427	.04	.001
C 51428	.05	.001
C 51429	.03	.001
C 51430	.05	.001
C 51431	.01	.001
C 51432	.03	.001

SAMPLE#	Ag OZ/T	Au OZ/T
C 51433	.01	.001
C 51434	.01	.001
C 51435	.06	.004
C 51436	.01	.001
C 51437	.06	.003
C 51438	.09	.002
C 51439	.05	.002
C 51440	.09	.004
C 51441	.07	.003
C 51442	.02	.001
C 51443	.05	.003
C 51444	.08	.002
C 51445	.21	.004
C 51446	.05	.002
C 51447	.04	.002
C 51448	.02	.001
C 51449	.02	.001
C 51450	.06	.001
C 51451	.05	.003
C 51452	.07	.001
C 51453	.10	.001
C 51454	.07	.001
C 51455	.09	.004
C 51456	.11	.003
C 51457	1.33	.012
C 51458	.09	.003
C 51459	.24	.002
C 51460	.03	.002
C 51461	.18	.002
C 51462	.01	.001
C 51463	.02	.001
C 51464	.03	.001
C 51465	.06	.001
C 51466	.09	.002
C 51467	.02	.002
C 51468	.08	.006

SDH-11

	SAMPLE#	Ag OZ/T	Au OZ/T
	C 51469	.07	.004
	C 51470	.04	.003
	C 51471	.01	.003
	C 51472	.04	.002
	C 51473	.01	.001
	C 51474	.01	.001
	C 51475	.03	.002
	C 51476	.01	.001
	C 51477	.03	.001
	C 51478	.02	.001
	C 51479	.02	.001
	C 51480	.01	.001
	C 51481	.01	.001
	C 51482	.01	.001
	C 51483	.01	.001
	C 51484	.01	.001
	C 51485	.03	.001
	C 51486	.01	.001
	C 51487	.03	.001
	C 51488	.01	.001
	C 51489	.01	.001
SDH-12	C 51490	.02	.001
	C 51491	.01	.001
	C 51492	.01	.001
	C 51493	.01	.001
	C 51494	.01	.001
	C 51495	.01	.001
	C 51496	.01	.001
	C 51497	.01	.001
	C 51498	.01	.001
	C 51499	.01	.001
	C 51500	.02	.001
	E 54551	.02	.001
	E 54552	.01	.001
	E 54553	.02	.001
	E 54554	.01	.001

SAMPLE#	Ag OZ/T	Au OZ/T
E 54555	.03	.001
E 54556	.02	.001
E 54557	.01	.001
E 54558	.01	.001
E 54559	.01	.001
E 54560	.03	.001
E 54561	.01	.001
E 54562	.01	.001
E 54563	.02	.001
E 54564	.02	.001
E 54565	.02	.001
E 54566	.02	.001
E 54567	.03	.001
E 54568	.02	.001
SDH-12 E 54569	.01	.001
E 54570	.01	.001
E 54571	.01	.001
E 54572	.02	.001
E 54573	.03	.001
E 54574	.02	.001
E 54575	.04	.001
E 54576	.01	.001
E 54577	.02	.001
E 54578	.01	.001
E 54579	.01	.001
E 54580	.03	.001
E 54581	.05	.001
E 54582	.06	.001
E 54583	.02	.001
E 54584	.01	.001
E 54585	.04	.001
E 54586	.01	.001
E 54587	.03	.001
E 54588	.01	.001
E 54589	.04	.001
E 54590	.02	.001

MINGOLD RESOURCES PROJECT #620 RHUB-BARB FILE # 88-2967 Page 5

	SAMPLE#	AG oz/t	AU oz/t
	E 54591	.01	.001
	E 54592	.01	.001
SDH-12	E 54593	.01	.001
	E 54594	.02	.001

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: AUG 1 1988
DATE REPORT MAILED: Aug. 8/88.

ASSAY CERTIFICATE

- SAMPLE TYPE: Core AU - 20 GM REGULAR ASSAY.

ASSAYER: C. Leong. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES INC. PROJECT #620 RHUB-BARB FILE # 88-3134 Page 1

SDH-9

SAMPLE#	Ag OZ/T	Au OZ/T
C 51501	.02	.001
C 51502	.01	.001
C 51503	.01	.001
C 51504	.01	.001
C 51505	.01	.001
C 51506	.02	.001
C 51507	.01	.001
C 51508	.02	.001
C 51509	.01	.001
C 51510	.01	.001
C 51511	.01	.001
C 51512	.04	.001
C 51513	.03	.001
C 51514	.03	.001
C 51515	.01	.001
C 51516	.01	.001
C 51517	.01	.001
C 51518	.03	.001
C 51519	.02	.002
C 51520	.13	.001
C 51521	.02	.001
C 51522	.07	.001
C 51523	.10	.002
C 51524	.07	.001
C 51525	.10	.001
C 51526	.10	.003
C 51527	.07	.002
C 51528	.81	.209
C 51529	.17	.039
C 51530	.25	.006
C 51531	.22	.004
C 51532	.11	.002
C 51533	.23	.003
C 51534	.13	.001
C 51535	.93	.007
C 51536	.08	.001

	SAMPLE#	Ag OZ/T	Au OZ/T
	C 51537	.02	.001
	C 51538	.02	.001
	C 51539	.02	.001
	C 51540	.04	.001
	C 51541	.03	.001
SDH-9	C 51542	.01	.001
	C 51543	.02	.001
	C 51544	.01	.001
	C 51545	.02	.001
	C 51546	.02	.001
	C 51547	.01	.001
	C 51548	.01	.001
	C 51549	.01	.001
	E 54595	.05	.001
	E 54596	.02	.001
	E 54597	.04	.002
	E 54598	.02	.001
	E 54599	.05	.002
	E 54600	.02	.001
	E 54601	.03	.001
	E 54602	.03	.001
	E 54603	.03	.002
SDH-12	E 54604	.02	.001
	E 54605	.02	.001
	E 54606	.01	.001
	E 54607	.01	.001
	E 54608	.06	.001
	E 54609	.02	.001
	E 54610	.05	.001
	E 54611	.03	.001
	E 54612	.01	.002
	E 54613	.01	.001
	E 54614	.02	.001
	E 54615	.03	.002
	E 54616	.03	.001
	E 54617	.03	.001

SAMPLE#	Ag OZ/T	Au OZ/T
E 54618	.06	.001
E 54619	.04	.001
E 54620	.04	.001
E 54621	.03	.001
E 54622	.04	.002
E 54623	.04	.001
E 54624	.02	.001
E 54625	.01	.001
E 54626	.01	.001
E 54627	.01	.001
E 54628	.01	.001
E 54629	.01	.001
E 54630	.01	.001
E 54631	.01	.001
E 54632	.01	.001
E 54633	.01	.001
E 54634	.03	.001
E 54635	.02	.001
E 54636	.02	.001
E 54637	.01	.001
E 54638	.02	.007
E 54639	.01	.001
E 54640	.02	.001
E 54641	.02	.001
E 54642	.01	.001
E 54643	.01	.001
E 54644	.01	.001
E 54645	.01	.001
E 54646	.02	.001
E 54647	.01	.001
E 54648	.02	.001
E 54649	.03	.001
E 54650	.01	.001
E 54701	.01	.001
E 54702	.01	.001
E 54703	.01	.001

SDH-12

GOLD RESOURCES INC. PROJECT #620 RHUB-BARB FILE # 88-3134 Page 4

SDH-12

SAMPLE#	Ag OZ/T	Au OZ/T
E 54704	.01	.001
E 54705	.01	.001
E 54706	.01	.001
E 54707	.01	.001
E 54708	.01	.001
E 54709	.01	.001
E 54710	.03	.001
E 54711	.01	.001
E 54712	.01	.001
E 54713	.02	.001

SDH-10

SAMPLE#	Ag OZ/T	Au OZ/T
E 54714	.01	.001
E 54715	.01	.001
E 54716	.01	.001
E 54717	.01	.001
E 54718	.01	.001
E 54719	.01	.001
E 54720	.01	.001
E 54721	.01	.001
E 54722	.01	.001
E 54723	.01	.001
E 54724	.01	.001
E 54725	.01	.001
E 54726	.01	.001
E 54727	.01	.001
E 54728	.01	.001
E 54729	.01	.001
E 54730	.01	.001
E 54731	.01	.001
E 54732	.01	.001
E 54733	.01	.001
E 54734	.01	.001
E 54735	.01	.001
E 54736	.01	.001
E 54737	.01	.001
E 54738	.01	.001
E 54739	.01	.001

SDH-10

SAMPLE#	Ag OZ/T	Au OZ/T
E 54740	.01	.001
E 54741	.01	.001
E 54742	.14	.001
E 54743	.36	.002
E 54744	.02	.001
E 54745	.04	.001
E 54746	.04	.001
E 54747	.02	.001
E 54748	.03	.001
E 54749	.01	.001
E 54750	.01	.001
E 54751	.04	.001
E 54752	.05	.001
E 54753	.10	.001
E 54754	.01	.001
E 54755	.03	.001
E 54756	.03	.001
E 54757	.02	.001
E 54758	.02	.001
E 54759	.01	.001
E 54760	.01	.001
E 54761	.01	.001
E 54762	.02	.001
E 54763	.04	.001
E 54764	.04	.001
E 54765	.03	.001
E 54766	.05	.002
E 54767	.01	.001
E 54768	.01	.001
E 54769	.01	.001
E 54770	.02	.001
E 54771	.02	.001
E 54772	.01	.001
E 54773	.02	.001
E 54774	.01	.001
E 54775	.03	.001

	SAMPLE#	Ag OZ/T	Au OZ/T
	E 54776	.01	.001
	E 54777	.04	.001
	E 54778	.05	.002
	E 54779	.01	.001
SDH-10	E 54780	.01	.001
	E 54781	.01	.001
	E 54782	.01	.001
	E 54783	.01	.001
	E 54784	.06	.001
	E 54785	.02	.001
	E 54786	.01	.001
	E 54787	.02	.001
	E 54788	.01	.001
	E 54789	.01	.001
SDH-9	E 54790	.02	.001
	E 54791	.01	.001
	E 54792	.01	.001
	E 54793	.01	.001
	E 54794	.04	.001
	E 54795	.03	.001
	E 54796	.01	.001
	E 54797	.01	.001
	E 54798	.01	.001
	E 54799	.03	.001
	E 54800	.01	.001

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: AUG 6 1988
DATE REPORT MAILED: Aug. 11/88..

ASSAY CERTIFICATE

- SAMPLE TYPE: Core AU - 20 GM REGULAR ASSAY.

ASSAYER: C. Leong. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES INC. PROJECT #620 FILE # 88-3330A Page 1

SDH-9

SAMPLE#	Ag OZ/T	Au OZ/T
C 51550	.07	.001
C 51551	.01	.001
C 51552	.03	.002
C 51553	.02	.002
C 51554	.01	.001
C 51555	.01	.001
C 51556	.01	.001
C 51557	.02	.001
C 51558	.01	.001
C 51559	.01	.001
C 51560	.01	.001
C 51561	.02	.001
C 51562	.01	.001
C 51563	.01	.002
C 51564	.01	.001
C 51565	.02	.001
C 51566	.01	.001
C 51567	.01	.001
C 51568	.01	.001
C 51569	.01	.001
C 51570	.01	.001
C 51571	.01	.001
C 51572	.02	.001
C 51573	.07	.001
C 51574	.01	.001
C 51575	.03	.001
C 51576	.03	.001
C 51577	.09	.001
C 51578	.02	.001
C 51579	.02	.001
C 51580	.08	.002
C 51581	.04	.001
C 51582	.01	.001
C 51583	.01	.001
C 51584	.01	.001
C 51585	.01	.001

SDH-10

SAMPLE#	Ag OZ/T	Au OZ/T
C 51586	.02	.001
C 51587	.02	.001
C 51588	.01	.001
C 51589	.03	.001
C 51590	.01	.001
C 51591	.01	.001
C 51592	.03	.001
C 51593	.02	.001
C 51594	.01	.001
C 51595	.01	.001
C 51596	.01	.001
C 51597	.02	.001
C 51598	.01	.001
C 51599	.05	.001
C 51600	.01	.001
C 51601	.01	.001
C 51602	.02	.001
C 51603	.03	.001
C 51604	.01	.001
C 51605	.03	.001
C 51606	.02	.001
C 51607	.01	.001
C 51608	.01	.001
C 51609	.01	.001
C 51610	.01	.001
C 51611	.01	.001
C 51612	.04	.001
C 51613	.01	.001
C 51614	.03	.001
C 51615	.14	.001
C 51616	.15	.002
C 51617	.22	.002
C 51618	.04	.001
C 51619	.03	.002
C 51620	.04	.002
C 51621	.78	.002

SAMPLE#	Ag OZ/T	Au OZ/T
C 51622	.03	.002
C 51623	.05	.002
C 51624	.04	.001
C 51625	.03	.001
C 51626	.02	.002
C 51627	.01	.001
C 51628	.04	.001
C 51629	.02	.001
C 51630	.01	.001
C 51631	.01	.001
C 51632	.02	.001
C 51633	.01	.001
C 51634	.02	.001
C 51635	.01	.001
C 51636	.01	.001
C 51637	.01	.001
C 51638	.01	.001
C 51639	.01	.001
C 51640	.01	.001
C 51641	.01	.001
C 51642	.01	.001
C 51643	.01	.001
C 51644	.01	.001
C 51645	.01	.001

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: AUG 17 1988
DATE REPORT MAILED: Aug 30/88

ASSAY CERTIFICATE

- SAMPLE TYPE: Core

ASSAYER: C. Leong D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES INC. PROJECT 602 FILE # 88-3664A

	SAMPLE#	Ag OZ/T	Au OZ/T
SDH-10	C 51646	.01	.001
	C 51647	.01	.001

VI ASSAY CERTIFICATES

-ROCK SAMPLING-

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

20

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P5 CORE P6-P8 ROCK CHIP AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUL 18 1988 DATE REPORT MAILED: July 22/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT 620 RHUB-BARB File # 88-2802 Page 6

	SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
	E-54651 .5-2m	4	14	10	64	.2	3	2	178	3.39	199	5	ND	16	22	1	3	2	13	.22	.041	25	3	.20	104	.02	2	1.14	.03	.12	1	1	350
	E-54652 2-4	5	14	11	53	.4	2	2	171	3.69	317	5	ND	15	26	1	14	3	12	.22	.042	26	3	.19	105	.01	2	1.18	.04	.12	2	1	600
	E-54653 4-6	12	3	13	9	4.5	1	1	82	1.92	3290	5	ND	13	49	1	46	2	4	.27	.118	28	1	.08	122	.01	12	.54	.03	.24	1	105	1500
	E-54654 6-8	7	9	20	32	.2	2	1	190	2.51	308	6	ND	11	49	1	9	2	7	.46	.130	44	2	.17	74	.01	2	1.43	.02	.20	2	1	590
	E-54655 8-10	9	8	18	12	1.6	1	1	171	1.80	1182	5	ND	13	64	1	53	2	6	1.03	.422	38	2	.13	68	.01	12	1.56	.02	.32	1	31	1400
HBHT-7	E-54656 10-12	2	5	10	9	.8	1	1	64	1.29	314	5	ND	14	39	1	24	3	5	.39	.153	28	1	.15	105	.01	9	.95	.03	.21	1	24	2900
	E-54657 12-14	1	5	11	9	.2	1	1	42	1.23	195	6	ND	16	35	1	14	2	5	.19	.033	28	2	.16	137	.01	7	.78	.02	.20	1	1	1300
	E-54658 14-16	1	3	9	7	.1	1	1	120	1.24	152	5	ND	15	47	1	11	2	5	.17	.027	27	1	.12	152	.01	10	.64	.03	.23	1	1	2500
	E-54659 16-18	15	4	13	9	2.3	2	1	126	2.00	483	5	ND	13	93	1	37	2	3	.27	.144	28	3	.08	170	.01	12	.37	.02	.29	1	48	1900
	E-54660 18-20	3	10	12	66	.1	2	2	83	2.72	94	5	ND	17	14	1	2	2	10	.15	.029	21	2	.15	94	.01	17	1.08	.03	.12	1	1	610
	E-54661 20-22	5	8	12	17	.5	1	1	62	1.94	744	5	ND	16	32	1	30	2	9	.26	.090	30	2	.14	107	.01	4	.86	.01	.14	1	1	270
	E-54662 22-24	4	6	14	22	.2	1	1	115	1.18	281	5	ND	15	31	1	7	2	9	.29	.039	26	2	.18	89	.01	13	.91	.02	.11	1	1	340
	E-54663 0-2m	6	5	8	5	9.9	1	1	14	.82	1431	5	ND	14	25	1	40	2	2	.11	.033	24	1	.03	96	.01	4	.45	.04	.18	1	135	1200
	E-54664 2-4	3	4	7	7	2.4	1	1	25	1.07	560	5	ND	15	28	1	15	3	2	.13	.016	19	1	.04	93	.01	9	.48	.01	.22	1	16	1900
	E-54665 4-6	3	2	11	4	.1	1	1	24	.75	24	6	ND	9	22	1	2	3	2	.13	.019	30	1	.08	90	.01	6	.62	.01	.21	1	1	280
	E-54666 6-6.8	6	1	10	4	12.4	2	1	14	1.24	229	5	ND	12	13	1	28	2	2	.04	.010	16	5	.02	126	.01	4	.39	.01	.25	1	10	2200
	E-54667 6.8-7.6	33	13	20	9	239.1	7.03 1	1	6	6.05	3295	5	ND	8	21	1	352	2	3	.05	.041	11	1	.02	36	.01	2	.39	.13	.73	1	1125	9200
	E-54668 7.6-8.7	10	4	6	5	34.8	1.01 1	1	10	1.47	1306	5	ND	7	13	1	68	3	2	.06	.009	13	1	.02	127	.01	2	.51	.05	.23	1	127	12000
HBHT-6	E-54669 9.7-10.6	40	4	20	5	96.4	2.81 1	1	12	3.07	1629	5	ND	8	21	1	59	2	2	.08	.015	14	3	.02	84	.01	2	.52	.07	.45	1	114	9400
	E-54670 10.6-11.6	27	7	19	7	214.2	6.25 1	1	13	2.44	2960	5	ND	9	19	1	159	2	2	.06	.019	12	1	.02	82	.01	5	.43	.02	.37	1	915	3800
	E-54671 11.6-13.6	92	8	15	4	226.4	6.6 1	1	18	1.79	2561	5	ND	7	16	1	135	2	2	.09	.020	13	1	.03	67	.01	13	.40	.01	.27	1	855	3500
	E-54672 15.8-16.2	37	1	15	2	3.6	1	1	14	.97	426	5	ND	25	19	1	47	2	3	.10	.017	29	1	.04	191	.01	8	.54	.03	.23	1	31	760
	E-54673 16.2-17.6	31	4	16	6	6.7	1	1	38	2.92	1186	5	ND	17	44	1	160	2	6	.18	.036	29	2	.07	130	.01	5	.63	.02	.49	1	125	2700
	E-54674 17.6-18.45	13	3	11	4	.7	1	1	23	1.56	663	5	ND	12	33	1	28	2	4	.11	.030	24	3	.04	169	.01	11	.50	.01	.27	1	24	640
	E-54675 18.45-19.2	6	3	9	4	.4	1	1	24	1.05	808	6	ND	14	19	1	7	2	6	.08	.049	29	2	.09	141	.02	6	.67	.02	.23	1	5	360
	E-54676 19.2-21.2	14	4	11	4	.7	1	1	42	1.34	575	5	ND	13	32	1	23	2	6	.10	.033	27	2	.06	142	.01	9	.67	.02	.29	1	12	1050
	E-54677 21.2-21.7	8	3	9	4	.4	1	1	23	.89	398	5	ND	11	30	1	14	2	4	.12	.022	25	2	.06	119	.01	7	.53	.02	.22	1	1	630
	E-54678 21.7-23.6	14	7	12	8	1.2	2	1	78	1.34	582	5	ND	14	46	1	22	2	8	.12	.034	31	4	.08	202	.01	5	.70	.02	.29	1	26	1500
	E-54679 2-4m	3	13	7	40	.3	2	2	185	1.45	21	5	ND	19	22	1	2	2	14	.22	.023	28	2	.21	161	.01	5	1.10	.01	.11	1	3	110
	E-54680 4-6	4	8	6	24	.3	2	1	99	1.15	17	5	ND	18	28	1	2	2	11	.22	.018	27	3	.20	245	.01	14	1.01	.03	.13	1	1	60
	E-54681 8-10	3	9	7	45	.8	3	2	544	1.38	33	5	ND	17	65	1	2	2	12	.27	.020	28	2	.24	555	.01	8	1.07	.02	.11	2	1	140
HBHT-8	E-54682 10-12	2	10	8	67	.2	5	3	729	1.49	16	5	ND	16	32	1	2	2	14	.49	.021	30	3	.28	201	.01	3	1.16	.04	.10	1	1	90
	E-54683 12-14	3	8	7	50	.2	3	2	667	1.38	25	5	ND	17	36	1	2	2	10	.24	.020	30	1	.22	222	.01	6	1.16	.02	.12	2	2	150
	E-54684 14-16	2	9	6	35	.2	1	2	368	1.39	33	5	ND	17	20	1	2	2	9	.20	.022	28	2	.21	156	.01	3	1.07	.03	.12	1	1	70
	E-54685 16-18	2	8	9	34	.1	1	2	246	1.32	23	6	ND	18	31	1	2	2	8	.18	.023	30	2	.18	205	.01	4	.93	.03	.14	1	1	70
	E-54686 18-20	2	6	10	19	.2	1	1	155	1.26	23	5	ND	18	53	1	2	2	6	.14	.020	32	1	.13	286	.01	13	.70	.03	.17	1	1	90
	STD C/AU-R	17	58	38	132	6.8	68	28	1050	4.05	36	24	7	36	47	17	18	19	56	.49	.089	38	55	.93	172	.06	38	1.98	.05	.13	12	485	1400

SAMPLE#		Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
E-54687	20-22	2	11	11	55	.1	2	2	205	1.44	14	9	ND	21	14	1	2	2	12	.13	.029	34	3	.16	101	.01	2	.96	.03	.13	1	1	130
E-54688	-24	2	10	15	38	.1	3	2	161	1.39	17	7	ND	21	12	1	2	3	12	.10	.027	31	5	.16	110	.01	7	1.00	.03	.12	1	2	120
E-54689	-26	2	7	12	28	.1	1	1	183	1.32	17	5	ND	18	19	1	2	2	9	.11	.019	30	2	.16	110	.01	7	.85	.03	.12	1	1	400
E-54690	-28	2	11	14	66	.1	5	3	464	1.75	17	6	ND	17	29	1	3	3	14	.25	.023	32	3	.25	226	.01	4	.98	.02	.11	1	1	100
E-54691	-30	2	11	16	17	.1	1	1	29	1.23	11	8	ND	20	30	1	2	2	3	.08	.022	31	3	.12	119	.01	5	.62	.04	.13	1	1	50
E-54692	-32	1	7	19	13	.1	1	1	28	1.24	9	5	ND	17	58	1	2	2	3	.07	.021	33	1	.10	139	.01	15	.64	.03	.16	1	1	70
E-54693	-34	1	6	14	14	.1	1	1	37	1.59	5	5	ND	16	59	1	2	3	3	.12	.020	32	2	.10	169	.01	2	.64	.03	.22	1	1	60
E-54694	-36	1	6	11	9	.1	1	1	20	1.11	11	5	ND	16	64	1	2	2	2	.15	.017	32	3	.10	136	.01	3	.55	.03	.19	1	1	120
E-54695	-38	1	6	10	9	.1	1	1	32	.98	9	5	ND	16	82	1	2	2	3	.19	.015	32	1	.14	141	.01	5	.73	.03	.19	1	2	140
E-54696	-40	2	8	10	14	.1	1	1	51	1.52	9	7	ND	18	61	1	2	3	5	.17	.021	31	1	.15	277	.01	6	.83	.02	.14	1	1	90
E-54697	-42	2	6	10	9	.1	1	1	42	1.21	13	5	ND	16	92	1	2	2	6	.19	.018	31	3	.16	139	.01	12	.88	.02	.13	1	1	120
E-54698	-44	1	7	10	19	.1	1	1	719	1.46	10	5	ND	14	22	1	2	2	9	.20	.020	28	2	.21	111	.01	2	.93	.02	.11	2	1	90
E-54699	-46	1	10	10	15	.1	1	1	263	1.41	10	5	ND	15	44	1	2	2	6	.20	.019	28	2	.19	124	.01	7	.85	.03	.12	1	1	100
E-54700	46-48	2	18	9	9	.1	1	1	64	1.34	24	5	ND	15	69	1	2	3	5	.12	.020	29	2	.12	167	.01	3	.72	.04	.15	1	1	110
E-54851	50	2	6	9	11	.1	1	1	54	1.10	18	5	ND	15	23	1	2	2	7	.15	.018	29	2	.14	108	.01	2	.79	.02	.11	1	1	130
E-54852	52	2	11	9	37	.1	1	2	693	1.68	14	5	ND	14	25	1	2	2	13	.23	.021	28	2	.31	133	.01	2	1.16	.03	.11	1	1	120
E-54853	54	3	7	9	17	.1	1	1	97	1.53	28	5	ND	14	15	1	3	3	7	.10	.021	29	2	.16	183	.01	2	.89	.02	.17	1	2	220
E-54854	56	3	6	12	28	.1	1	1	202	1.52	21	5	ND	13	17	1	2	2	14	.20	.023	29	2	.27	114	.01	6	1.23	.02	.13	1	1	120
E-54855	58	4	4	14	9	.1	1	1	42	.92	64	5	ND	9	25	1	2	2	2	.16	.015	37	1	.08	86	.01	4	.62	.02	.20	1	3	480
E-54856	60	6	5	13	10	.1	1	1	29	1.46	124	5	ND	16	34	1	5	2	4	.09	.020	34	1	.10	186	.01	7	.60	.03	.19	1	1	320
E-54857	62	4	2	17	5	.1	1	1	24	1.32	118	5	ND	18	33	1	8	2	2	.06	.014	39	2	.05	122	.01	4	.51	.02	.18	1	3	2300
E-54858	64	5	1	15	2	.1	1	1	23	.94	81	5	ND	16	18	1	4	2	1	.08	.008	39	1	.03	99	.01	3	.47	.02	.16	1	1	1100
E-54859	66	5	1	14	3	.1	1	1	15	1.11	72	5	ND	17	29	1	5	2	1	.05	.015	37	2	.03	120	.01	17	.43	.03	.17	1	1	1600
E-54860	68	4	3	14	5	.1	1	1	24	1.14	48	5	ND	14	55	1	4	3	2	.09	.017	37	1	.05	267	.01	2	.49	.03	.20	1	1	700
E-54861	70	2	4	11	5	.1	1	1	35	.91	48	5	ND	9	40	1	5	2	3	.12	.018	29	1	.08	159	.01	2	.55	.04	.16	1	1	2200
E-54862	72	3	3	14	8	.2	1	1	22	1.02	23	5	ND	11	38	1	3	3	4	.14	.020	31	2	.13	324	.01	4	.80	.02	.20	1	1	720
E-54863	74	2	1	10	4	.2	1	1	27	.84	23	5	ND	10	26	1	2	2	3	.10	.016	31	1	.06	118	.01	2	.48	.02	.17	1	1	500
E-54864	76	3	2	15	5	.1	1	1	44	.80	18	6	ND	11	30	1	2	2	3	.15	.019	34	1	.08	116	.01	3	.63	.03	.20	1	1	420
E-54865	78	3	3	7	4	4.8	1	1	4	1.10	661	5	ND	13	17	1	26	2	2	.07	.010	17	1	.02	78	.01	3	.34	.03	.19	1	93	3100
E-54866	80	4	4	13	7	.1	1	1	22	1.52	28	5	ND	10	37	1	3	2	3	.12	.045	31	2	.08	147	.01	2	.57	.02	.20	1	1	430
E-54867	82	3	2	11	5	.2	1	1	10	1.04	14	5	ND	10	26	1	2	2	2	.10	.028	30	2	.07	122	.01	5	.49	.03	.22	1	1	170
E-54868	84	4	6	16	20	.1	1	1	30	1.32	9	5	ND	10	17	1	2	3	2	.09	.022	30	1	.06	89	.01	3	.54	.01	.21	1	1	160
E-54869	86	4	4	16	9	.1	1	1	25	1.70	20	5	ND	10	30	1	3	2	2	.12	.040	34	2	.06	128	.01	2	.51	.02	.24	1	1	180
E-54870	88	3	3	13	4	.1	1	1	13	.77	10	5	ND	9	19	1	2	2	1	.09	.030	35	1	.04	104	.01	2	.46	.01	.21	1	1	140
E-54871	90	3	3	16	5	.1	1	1	24	.82	9	5	ND	10	17	1	2	3	1	.08	.025	37	1	.03	110	.01	2	.39	.02	.21	1	1	130
E-54872	92	4	3	19	5	.1	1	1	18	1.18	9	5	ND	10	36	1	3	2	1	.06	.021	38	2	.03	142	.01	3	.36	.02	.25	1	1	110
STD C/AU-R		18	57	41	132	6.7	67	28	1055	4.15	41	19	7	36	47	18	18	21	56	.49	.089	38	56	.94	176	.06	37	2.00	.06	.13	13	500	1400

(36)

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	I %	W PPM	Aa* PPB	Hg PPB
R-54873 92-94	4	3	20	5	.1	1	1	22	1.11	20	5	ND	8	24	1	2	2	1	.07	.025	36	1	.03	137	.01	2	.38	.01	.24	1	3	130
R-54874 96	4	2	32	4	.1	1	1	18	.69	20	5	ND	11	14	1	2	2	1	.07	.015	42	1	.02	68	.01	2	.37	.01	.20	1	112	100
R-54875 98	4	2	27	4	.1	1	1	15	1.07	7	5	ND	10	22	1	2	2	1	.06	.021	38	1	.02	97	.01	2	.35	.01	.22	1	2	90
R-54876 100	3	3	23	11	.1	1	1	28	.92	16	5	ND	8	29	1	2	2	1	.09	.030	41	1	.03	91	.01	2	.38	.01	.21	1	62	120
R-54877 102	4	5	18	14	.1	2	1	91	1.16	11	5	ND	11	39	1	2	2	2	.12	.040	39	1	.04	226	.01	2	.58	.01	.31	1	3	100
R-54878 104	4	8	22	24	.1	2	1	293	1.45	22	5	ND	12	38	1	3	2	1	.13	.029	40	1	.03	115	.01	2	.39	.01	.22	1	31	90
R-54879 106	3	4	12	16	.1	1	1	145	1.09	9	5	ND	13	55	1	2	2	1	.13	.023	38	1	.03	91	.01	4	.34	.01	.22	1	2	130
STD C/AU-R	17	57	38	132	6.8	68	28	1061	4.04	36	19	6	36	48	17	17	18	57	.49	.089	39	56	.93	172	.06	34	1.99	.06	.14	11	495	1400

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUN 08 1988 DATE REPORT MAILED: June 14/88 ASSAYER. [signature] .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT-620 File # 88-1833

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
60729	24	30	18	28	.1	1	1	47	.73	27	5	ND	6	9	1	2	2	1	.04	.010	11	1	.02	33	.01	2	.28	.01	.16	1	1	50
60730	45	4	25	27	.5	2	1	157	.86	39	5	ND	5	15	1	2	2	2	.10	.011	13	2	.05	43	.01	2	.27	.02	.13	1	37	5
60731	45	16	15	12	.1	1	1	53	.76	26	5	ND	6	12	1	2	2	1	.03	.010	13	1	.02	39	.01	2	.27	.02	.13	1	7	30
60732	57	4	17	9	.1	1	1	110	.82	22	5	ND	7	9	1	2	2	3	.04	.012	17	2	.03	42	.01	2	.34	.03	.13	1	54	5
60733	27	11	22	12	.4	1	1	59	.86	25	8	ND	8	12	1	2	2	1	.04	.012	16	1	.02	37	.01	2	.28	.01	.15	1	5	20
60734	19	4	13	5	.2	1	1	47	.75	31	5	ND	8	11	1	2	2	1	.03	.014	14	1	.02	38	.01	2	.26	.01	.18	1	10	10
60735	32	8	13	6	.1	1	1	24	.84	32	5	ND	5	14	1	2	2	1	.03	.013	14	1	.02	40	.01	2	.25	.03	.16	1	1	20
60736	41	6	15	5	.3	1	1	39	1.27	49	5	ND	6	16	1	2	2	2	.03	.017	14	2	.02	37	.01	2	.23	.02	.16	1	11	10
60737	35	7	13	5	.5	2	1	26	.82	33	5	ND	7	10	1	2	2	1	.02	.010	9	2	.01	31	.01	2	.24	.01	.18	1	2	20
60738	25	4	11	5	.5	1	1	39	.65	29	8	ND	9	14	1	2	2	1	.04	.012	15	1	.03	35	.01	2	.27	.02	.17	1	4	10
60739	28	5	12	4	.1	1	1	25	.54	27	5	ND	6	13	1	2	2	1	.03	.012	8	1	.02	45	.01	4	.25	.03	.13	1	3	40
60740	13	4	13	9	.1	2	1	81	.75	17	5	ND	4	9	1	2	2	4	.06	.011	9	3	.06	47	.01	2	.34	.02	.12	1	3	60
60741	11	5	15	15	.1	1	1	120	.83	17	5	ND	7	6	1	2	2	3	.03	.013	10	1	.03	37	.01	2	.42	.02	.16	1	1	20
STD C/AU-R	18	58	37	132	6.7	69	29	1071	4.05	40	21	6	36	49	17	17	19	58	.49	.083	39	56	.93	178	.07	33	1.76	.07	.13	11	500	1300

ACME ANALYTICAL LABORATORIES LTD.   852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6   PHONE(604)253-3158 FAX(604)253-1716

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THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK   AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMLESS AA.

DATE RECEIVED: AUG 26 1988 DATE REPORT MAILED: Sept 1/88   ASSAYER. . .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

MINGOLD RESOURCES PROJECT 620   File # 88-3936

QUARRY TRENCH #1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
E 24120	2	4	11	33	.1	3	1	221	1.21	10	5	ND	7	3	1	2	2	1	.09	.017	15	7	.07	36	.02	2	.58	.03	.15	1	2	5
E 54880	23	7	15	8	.1	4	1	6	1.39	41	5	ND	9	11	1	2	2	1	.02	.016	19	2	.01	42	.01	2	.28	.01	.18	1	5	40
E 54881	14	4	11	1	.1	4	1	2	.61	25	5	ND	7	8	1	2	2	1	.01	.008	17	18	.01	36	.01	2	.22	.01	.17	1	7	30
E 54882	28	5	12	2	.1	5	1	12	1.00	26	5	ND	7	10	1	2	2	1	.02	.010	16	4	.01	45	.01	2	.28	.01	.22	1	3	50
E 54883	66	5	14	6	.4	3	1	10	1.20	37	6	ND	6	16	1	4	2	1	.01	.018	41	28	.01	50	.01	3	.27	.01	.22	1	2	50
E 54884	22	6	12	3	.5	8	1	57	.92	29	5	ND	6	7	1	2	2	1	.02	.008	11	7	.01	26	.01	2	.23	.01	.16	1	6	70
E 54885	13	4	16	1	.3	1	1	8	.65	29	5	ND	6	5	1	2	2	1	.02	.005	7	30	.01	18	.01	2	.24	.01	.18	1	4	50
E 54886	11	6	11	3	.1	4	1	26	1.12	25	5	ND	7	7	1	2	2	1	.03	.009	9	5	.01	27	.01	2	.30	.01	.18	1	2	50
E 54887	49	2	16	2	.2	3	1	13	1.10	30	5	ND	6	8	1	2	2	1	.02	.012	10	10	.01	32	.01	7	.26	.01	.18	1	5	70
E 54888	90	2	36	1	.2	6	1	34	1.02	29	5	ND	5	13	1	4	2	1	.02	.011	21	4	.01	35	.01	2	.22	.01	.17	1	3	50
E 54889	74	6	19	1	.4	6	1	27	.75	16	5	ND	6	10	1	2	5	1	.03	.008	19	37	.01	28	.01	2	.25	.01	.16	1	2	60
E 54890	109	5	21	2	.5	5	1	35	.88	24	5	ND	6	10	1	3	2	1	.03	.010	22	42	.01	30	.01	2	.29	.01	.17	1	1	60
E 54891	126	6	17	2	.6	9	1	30	1.38	46	5	ND	6	7	1	4	2	1	.02	.016	16	8	.01	35	.01	4	.32	.01	.17	1	2	90
E 54892	93	5	24	3	1.0	4	1	29	1.22	37	5	ND	7	14	1	4	2	2	.03	.011	24	34	.01	46	.01	4	.34	.01	.18	1	2	60
E 54893	75	6	29	9	.6	2	1	35	1.29	32	5	ND	8	15	1	3	2	3	.03	.012	32	5	.01	52	.01	2	.39	.01	.18	1	1	50
E 54894	20	9	7	29	.2	5	1	79	1.47	36	5	ND	6	8	1	3	2	4	.04	.011	33	22	.03	34	.01	2	.56	.01	.14	1	2	60
E 54895	34	11	14	29	.2	4	1	69	1.50	38	9	ND	6	6	1	3	2	3	.04	.020	59	4	.02	28	.01	2	.48	.01	.15	1	1	40
E 54896	9	4	15	29	.1	4	1	93	1.15	21	5	ND	7	6	1	2	2	1	.05	.013	33	14	.03	28	.01	2	.44	.01	.17	1	1	30
E 54897	10	6	18	38	.1	2	1	244	1.57	21	5	ND	7	3	1	2	2	2	.05	.015	12	3	.05	31	.01	3	.57	.01	.14	1	1	20
E 54898	4	3	15	35	.1	3	2	269	1.23	14	5	ND	7	3	1	2	2	2	.05	.015	14	4	.06	37	.01	11	.58	.02	.14	1	1	10
E 54899	7	5	20	38	.1	2	1	275	1.38	20	5	ND	7	5	1	3	2	2	.06	.017	15	3	.06	41	.01	5	.54	.02	.12	1	3	10
E 54900	2	1	18	37	.1	4	1	299	1.33	12	5	ND	8	4	1	3	2	2	.08	.019	16	8	.08	34	.01	2	.59	.02	.14	1	1	5
STD C/AU-R	19	62	40	132	6.9	72	31	1169	4.10	43	18	8	38	49	19	16	18	58	.52	.085	41	60	.91	182	.07	37	2.00	.06	.14	13	495	1300

VII ROCK SAMPLE DESCRIPTIONS

ROCK SAMPLE DESCRIPTIONS (TRENCH #6)

SAMPLE NO.	TYPE	WIDTH (m)	DESCRIPTION
54663	CHANNEL	2	MODERATE TO STRONG ARGILLICALLY ALTERED RHYOLITE FLOW. MINOR STOCKWORK OF BLUE-GREY SILICA VEINS 1mm-1cm WIDE AND ASSOCIATED BRECCIA. Tr-3% PYRITE. FLOW BANDING 028°. FRACTURES 18-20°.
54664	CHANNEL	2	MODERATE TO STRONG ARGILLICALLY ALTERED RHYOLITE FLOW. LIGHT GREY HAIRLINE VEINLETS. NO VISIBLE SULPHIDES. BANDING 028°
54665	CHANNEL	2	SAME DESCRIPTION AS 54664
54666	CHANNEL	.8	INTENSLEY SILICIFIED RHYOLITE BRECCIA. DARK BLUE GREY SILICA MATRIX WITH 3% PYRITE. MINOR BLUE-GREY SILICA VEINS (1-2 cm) TRENDING 020°.
54667	CHANNEL	.8	SAME DESCRIPTION AS 54666
54668	CHANNEL	1.1	SAME DESCRIPTION AS 54666
54669	CHANNEL	1.9	SAME DESCRIPTION AS 54666
54670	CHANNEL	1	SAME DESCRIPTION AS 54666
54671	CHANNEL	2.2	SAME DESCRIPTION AS 54666
54672	CHANNEL	2.4	SHEAR ZONE 110°/VERTICAL LIGHT GREY, BLUE AND BROWN CLAY. NO VISIBLE SULPHIDES
54673	CHANNEL	1.4	SAME DESCRIPTION AS 54672
54674	CHANNEL	.85	MODERATE TO STRONG ARGILLICALLY ALTERED RHYOLITE FLOW [illegible]

ROCK SAMPLE DESCRIPTIONS (TRENCH #6)

SAMPLE No.	TYPE	WIDTH (m)	DESCRIPTION
54675	CHANNEL	.75	SAME DESCRIPTION AS 54674
54676	CHANNEL	2	SAME DESCRIPTION AS 54674
54677	CHANNEL	.5	SAME DESCRIPTION AS 54674
54678	CHANNEL	1.9	SAME DESCRIPTION AS 5467[illegible]

ROCK SAMPLE DESCRIPTIONS (TRENCH # 7)

SAMPLE NO.	TYPE	WIDTH (m)	DESCRIPTION
54651	CHANNEL	1.5	CREAM COLOURED RHYOLITE WITH MODERATE ARGILLIC ALTERATION
54652	CHANNEL	2	CREAM COLOURED RHYOLITE WITH INTENSE ARGILLIC ALTERATION
54653	CHANNEL	2	HONEY TO REDDISH BROWN RHYOLITE WITH INTENSE ARGILLIC ALTERATION. MINOR SILICA HEALED BRECCIA.
54654	CHANNEL	2	HONEY TO REDDISH BROWN RHYOLITE WITH INTENSE ARGILLIC ALTERATION. SILICA HEALED BRECCIA AND STOCK-WORK VEINING.
54655	CHANNEL	2	HONEY TO REDDISH BROWN RHYOLITE WITH INTENSE ARGILLIC ALTERATION CONTAINS MAROON SILICA BRECCIA AND STOCKWORK VEINING.
54656	CHANNEL	2	SAME DESCRIPTION AS 54655
54657	CHANNEL	2	INTENSLEY ARGILLICIZED REDDISH BROWN RHYOLITE WITH LIGHT GREY SILICA HEALED BRECCIA.
54658	CHANNEL	2	SAME DESCRIPTION AS 54657
54659	CHANNEL	2	SAME DESCRIPTION AS 54657
54660	CHANNEL	2	SAME DESCRIPTION AS 54657
54661	CHANNEL	2	SAME DESCRIPTION AS 54657
54662	CHANNEL	2	INTENSLEY ARGILLICIZED CREAM RHYOLITE WITH DARK GREY SILICA BRECCIA AND STOCK WOR VEI

ROCK SAMPLE DESCRIPTIONS (TRENCH - 8)

SAMPLE No	TYPE	WIDTH (m)	DESCRIPTION
54679	CHANNEL	2	BLEACHED RHYODACITE FLOW WEAK ARGILLIC ALTERATION 002/37E
54680	CHANNEL	2	SAME DESCRIPTION AS 54679
54681	CHANNEL	2	SAME DESCRIPTION AS 54679
54682	CHANNEL	2	WEAKLY SILICIFIED GREYISH BROWN RHYODACITE 012/48E
54683	CHANNEL	2	WEAK TO MODERATELY SILICIFIED LIGHT BROWN RHYOLITE WITH MINOR BRECCIATION
54684	CHANNEL	2	WEAK TO MODERATELY SILICIFIED CREAM COLOURED RHYODACITE. MINOR LIGHT GREY SILICA BANDS 015/60 NE
54685	CHANNEL	2	SAME DESCRIPTION AS 54684
54686	CHANNEL	2	SAME DESCRIPTION AS 54684
54687	CHANNEL	2	SAME DESCRIPTION AS 54684
54688	CHANNEL	2	SAME DESCRIPTION AS 54684
54689	CHANNEL	2	WEAKLY SILICIFIED RHYODACITE WITH ORANGE BROWN STAINING ALONG FRACTURES 012/64NE
54690	CHANNEL	2	STRONG ARGILLICALLY ALTERED RHYODACITE, BUFF WHITE TO GREY.
54691	CHANNEL	2 26	MODERATE ARGILLIC ALTERATION OF ORANGE-BROWN RHYO-DACITE MINOR GREY SILICA.
54692	CHANNEL	2	SAME DESCRIPTION [illegible] 54

ROCK SAMPLE DESCRIPTIONS (TRENCH - B) ②

SAMPLE NO.	TYPE	WIDTH(m)	DESCRIPTION
54693	CHANNEL	2	WEAK TO MODERATE ARGILLICALLY ALTERED GREYISH BROWN RHYODACITE. FRACTURES 050°/10(
54694	CHANNEL	2	SAME DESCRIPTION AS 54693
54695	CHANNEL	2	FAULT ZONE. INTENSE ARGILLIC ALTERATION OF RHYODACITE. LIGHT GREY CLAY.
54696	CHANNEL	2	MODERATE ARGILLICALLY ALTERED GREY TO ORANGE BROWN RHYODACITE WITH GREY SILICA BANDS THROUGHOUT.
54697	CHANNEL	2	SAME DESCRIPTION AS 54696
54698	CHANNEL	2 40	SAME DESCRIPTION AS 54696
54699	CHANNEL	2	FAULT ZONE. LIGHT GREY CLAY (INTENSE ARGILLIC ALTERATION)
54700	CHANNEL	2	SAME DESCRIPTION AS 54696
54851	CHANNEL	2	SAME DESCRIPTION AS 54696
54852	CHANNEL	2	SAME DESCRIPTION AS 54699
54853	CHANNEL	2 50	SAME DESCRIPTION AS 54696
54854	CHANNEL	2	SAME DESCRIPTION AS 54699
54855	CHANNEL	2	MODERATE TO STRONG LIMONITIC STAINING OF RHYODACITE GREY SILICA BANDS. IRON SEEPS 010/38 NE
54856	CHANNEL	2	FAULT ZONE. LIGHT GREY TO ORANGE BROWN CLAY

ROCK SAMPLE DESCRIPTIONS (TRENCH - 8)

SAMPLE NO.	TYPE	WIDTH (m)	DESCRIPTION
54857	CHANNEL	2	MODERATELY SILICIFIED LIGHT BROWN RHYODACITE TUFF. 162/68 W
54858	CHANNEL	2	SAME DESCRIPTION AS 54857
54859 - 79	CHANNEL	2	FAULT ZONE. LIGHT GREY TO INTENSE ORANGE BROI· CLAY. IRON SEEPS. VERY INTENSE ARGILLIC ALTERATION

VIII STATEMENT OF COSTS

FOR

PHYSICAL WORK

Group I

STATEMENT OF COSTS

(BARB 1, RHUB 10, 11, 12, 13)

PHYSICAL WORK

Personnel

K. Taylor - Supervisor	$175/day
N. Champion - Backhoe operator	included with backhoe charges
J. Thomlinson - Fieldman	$100/day
W. Kowal - Geological Technician	$ 95/day

Equipment

JCB 805B Backhoe including operator	$ 78/hr.

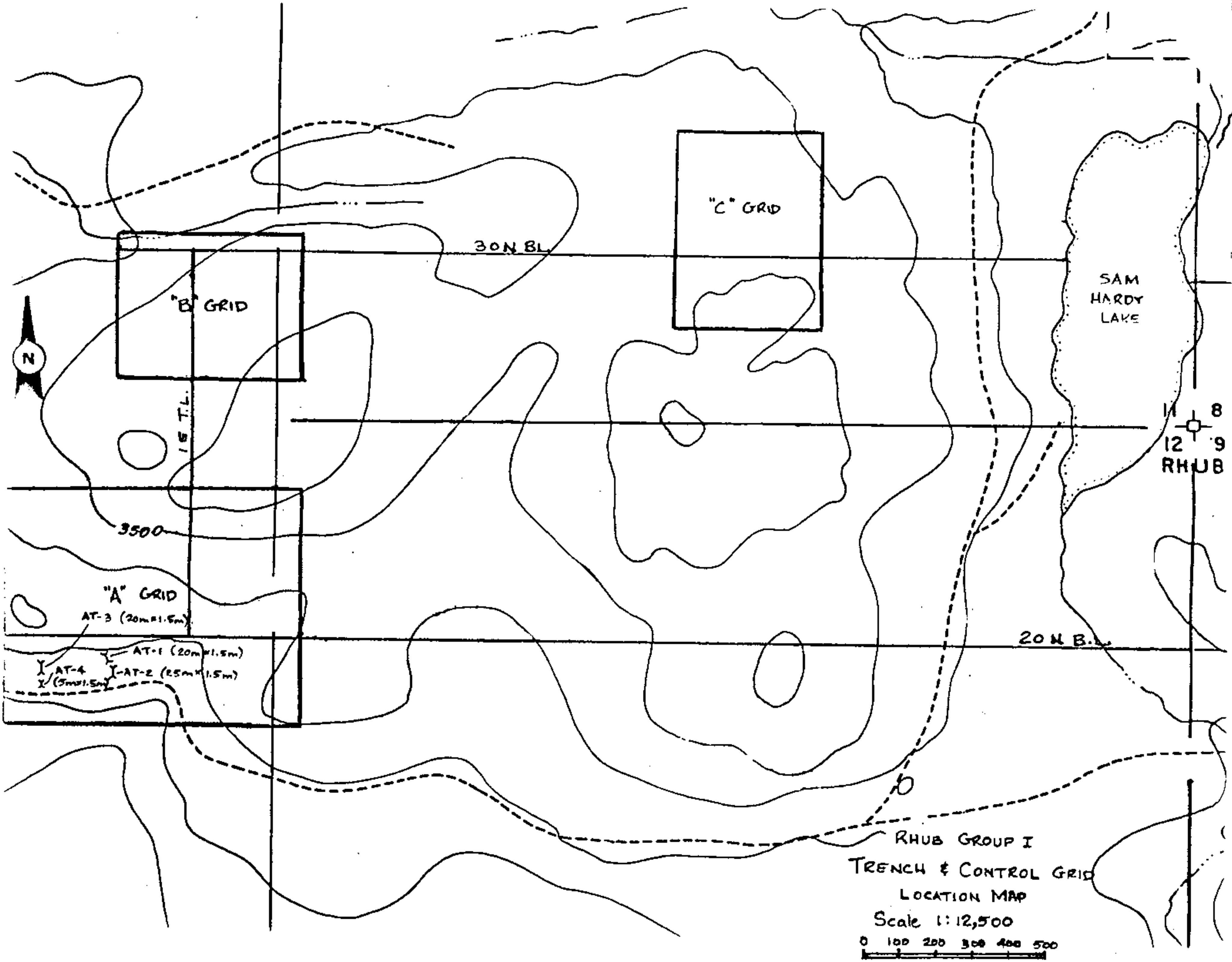
Dates Work Done

May 6, 7, 12, 13, 1988	Control grid by J. Thomlinson, W. Kowal
June 27, 29, 1988	4 trenches on "A" - Grid - AT-1 20m x 1.5m x 4.6m
	- AT-2 25m x 1.5m x 4.0m
	- AT-3 20m x 1.5m x 4.6m
	- AT-4 5m x 1.5m x 4.6m

Cost Breakdown

1) Trenching - 18 hr. backhoe @ $78/hr.	$ 1404.00
- Mob-demob - 1/3 of $918	306.00
- Supervision - 2 days @ $175/day	350.00
- Room/Board - 2 days for 2 men @ $25/man/day	100.00
- Truck Rental - 2 days @ $50/day incl. fuel	100.00
TOTAL	$ 2260.00

2) Control Grid - 5.8 km of baseline, 1 km of tieline	
- 3.5 days @ $100/day	$ 350.00
- 3.5 days @ $ 95/day	332.50
- Room/Board - 3.5 days for 2 men @ $25/man/day	175.00
- Truck rental - 4 days @ $50/day incl. fuel	200.00
TOTAL	$ 1057.50



"C" GRID
30 N BL
"B" GRID
N
SAM
HARDY
LAKE
11
8
12
9
RHUB
1E T.L.
3500
"A" GRID
AT-3 (20m×1.5m)
AT-1 (20m×1.5m)
AT-4
(5m×1.5m)
AT-2 (25m×1.5m)
20 N B.L.
RHUB GROUP I
TRENCH & CONTROL GRID
LOCATION MAP
Scale 1:12,500
0 100 200 300 400 500

Group II

STATEMENT OF COSTS

(RHUB 1, 3, 7, 8, 9)

PHYSICAL WORK

Personnel

K. Taylor - Supervisor	$175/day
N. Champion - Backhoe operator	included with backhoe charges
J. Thomlinson - Fieldman	$100/day
W. Kowal - Geological Technician	$ 95/day

Equipment

JCB 805 B Backhoe incl. operator	$ 78/hr.

Dates Work Done

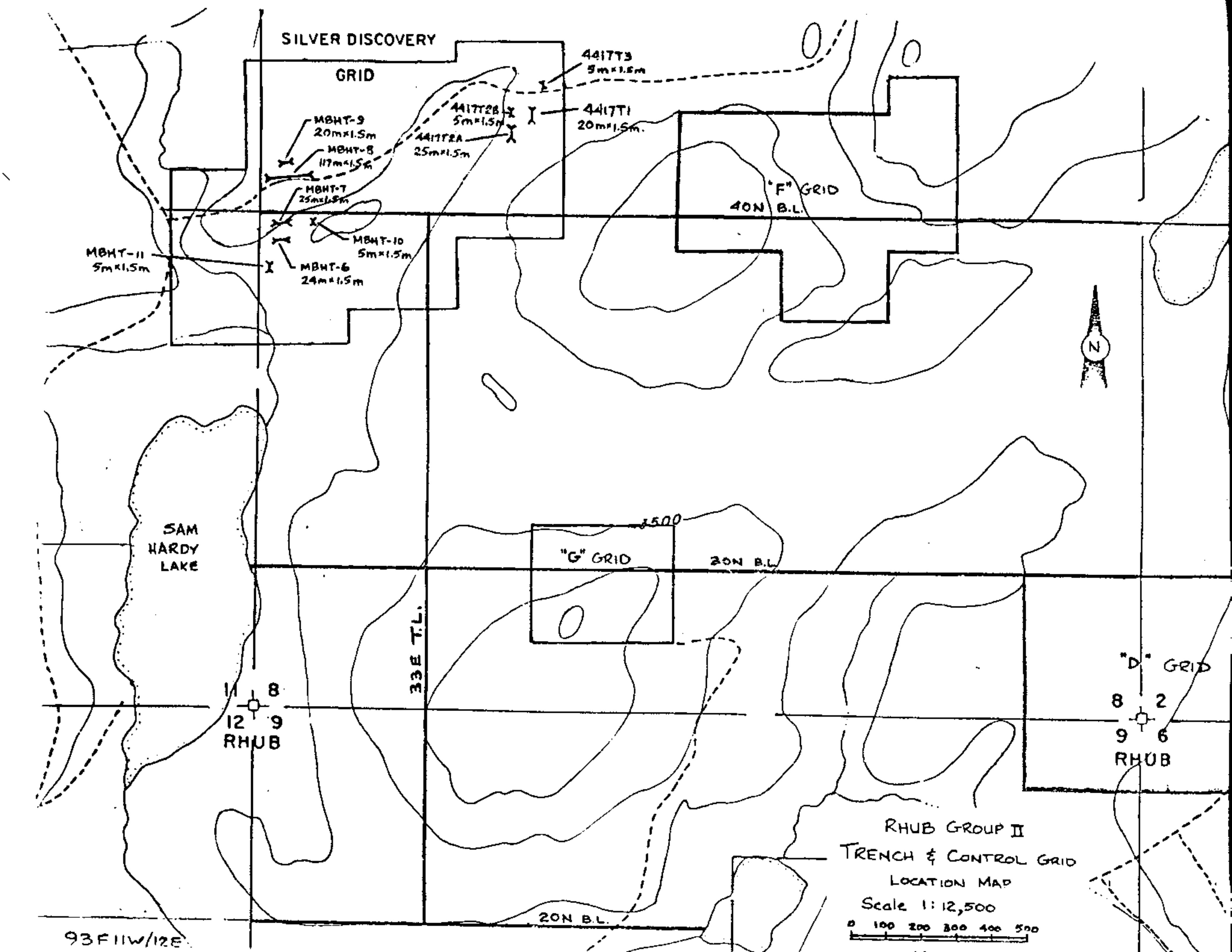
May 17-20, 1988 Control grid by J. Thomlinson, W. Kowal

May 21-24, 1988 4 trenches on 4417 Grid -
- 4417T1 20m x 1.5m x 4.6m
- 4417T2A 25m x 1.5m x 4.6m
- 4417T2B 5m x 1.5m x 4.6m
- 4417T3 5m x 1.5m x 4 m

May 24-26, 1988 6 trenches on Silver Zone -
- MBHT-6 24m x 1.5m x 1 m
- MBHT-7 25m x 1.5m x 3.7m
- MBHT-8 117m x 1.5m
- MBHT-9 20m x 1.5m x 4.6m
- MBHT-10 5m x 1.5m x 4.6m
- MBHT-11 5m x 1.5m x 4 m

Cost Breakdown

1) Trenching	- 45 hr. backhoe @ $78/hr.	$ 3510.00
	- Mob-demob - 1/3 of $918	306.00
	- Supervision - 6 days @ $175/day	1050.00
	- Room/board - 6 days for 2 men @ $25/man/day	300.00
	- Truck Rental - 6 days @ $50/day incl. fuel	300.00
	TOTAL	$ 5466.00
2) Control Grid	- 6.3 km. baseline, 2 km. tieline	
	- 4 days @ $100/day	$ 400.00
	- 4 days @ $ 95/day	380.00
	- Room/board - 4 days for 2 men @ $25/man/day	200.00
	- Truck rental - 4 days @ $50/day incl. fuel	200.00
	TOTAL	$ 1180.00


SILVER DISCOVERY
GRID
4417T3
5m×1.5m
4417T2B
5m×1.5m
4417T1
20m×1.5m
4417T2A
25m×1.5m
MBHT-9
20m×1.5m
MBHT-8
117m×1.5m
MBHT-7
25m×1.5m
MBHT-10
5m×1.5m
MBHT-11
5m×1.5m
MBHT-6
24m×1.5m
"F" GRID
40N B.L.
SAM
HARDY
LAKE
33E T.L.
1500
"G" GRID
20N B.L.
11
8
12
9
RHUB
"D" GRID
8
2
9
6
RHUB
N
RHUB GROUP II
TRENCH & CONTROL GRID
LOCATION MAP
Scale 1:12,500
0 100 200 300 400 500
20N B.L.
93F11W/12E

Group III

STATEMENT OF COSTS

(RHUB 2, 4, 5, 6)

PHYSICAL WORK

Personnel

K. Taylor - Supervisor	$175/day
N. Champion - Backhoe operator	included with backhoe charges
J. Thomlinson - Fieldman	$100/day
W. Kowal - Geological Technician	$ 95/day

Equipment

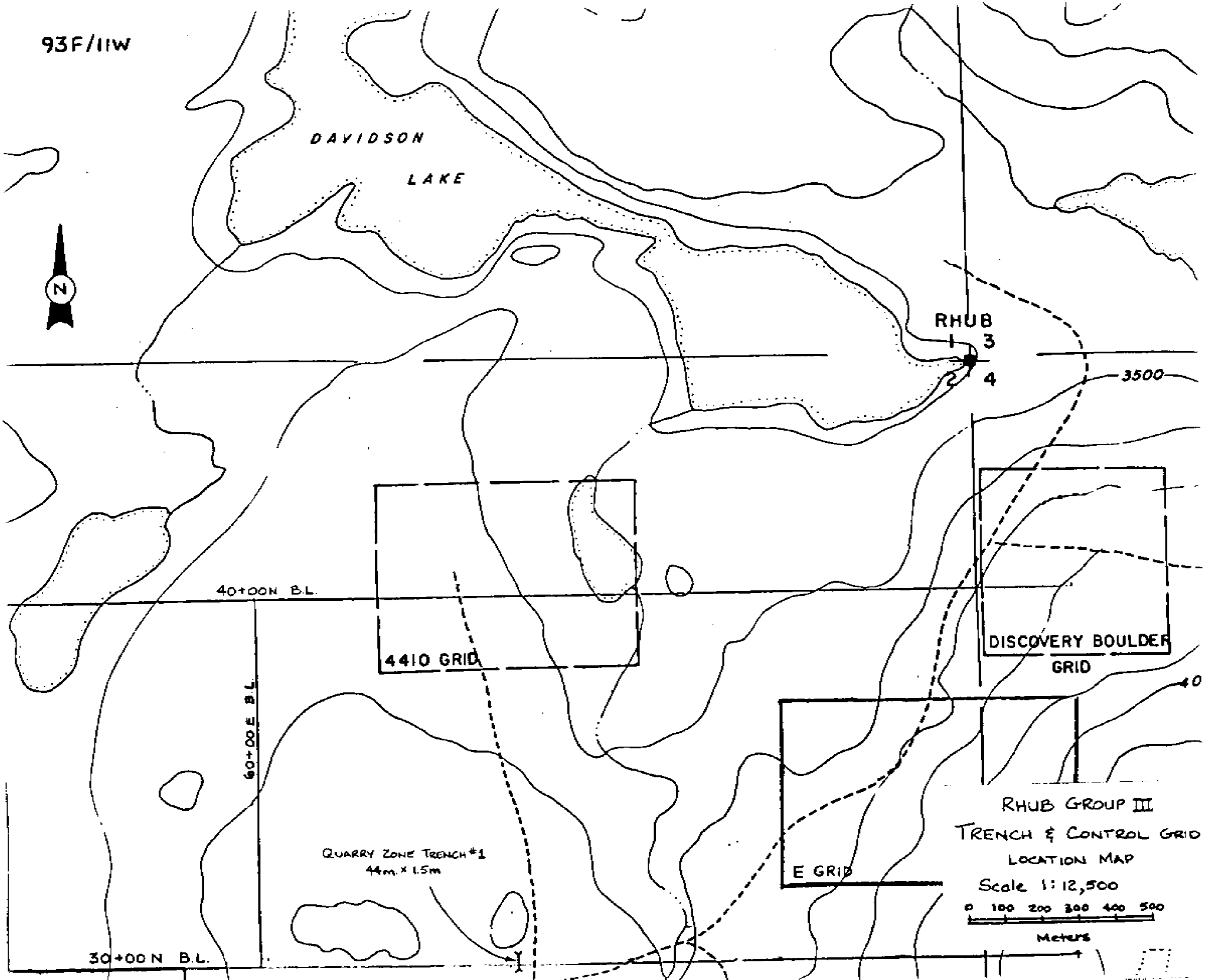
JCB 805 B Backhoe incl. operator	$ 78/hr.

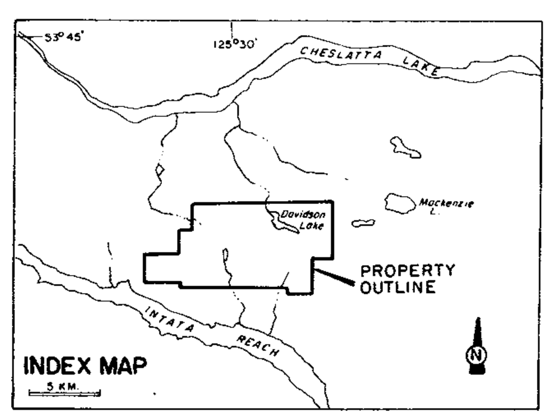
Dates Work Done

May 13 - 16, 1988	Control Grid by J. Thomlinson, W. Kowal
June 2, 1988	Trench (44m. x 1.5m.) on Quarry Zone

Cost Breakdown

1) Trenching	- 4 hr. backhoe @ $78/hr	$ 312.00
	- Mob-demob. - 1/3 of $918	306.00
	- Supervision - 0.5 days @ $175/day	87.50
	- Room/board - 1 day for 2 men @ $25/man/day	50.00
	- Truck rental - 1 day @ $50/day incl. fuel	50.00
	TOTAL	$ 805.50
2) Control Grid	- 5.6 km. of baseline, 1.0 km. of tie-line	
	- 3.5 days @ $100/day	$ 350.00
	- 3.5 days @ $ 95/day	332.50
	- Room/board - 3.5 days for 2 men @ $25/man/day	175.00
	- Truck rental - 4 days @ $50/day incl. fuel	200.00
	TOTAL	$ 1057.50


93F/11W
DAVIDSON
LAKE
N
RHUB
1
3
4
3500
40+00N B.L.
4410 GRID
DISCOVERY BOULDER
GRID
40
60+00E B.L.
E GRID
QUARRY ZONE TRENCH #1
44m. x 1.5m
30+00N B.L.
RHUB GROUP III
TRENCH & CONTROL GRID
LOCATION MAP
Scale 1:12,500
0 100 200 300 400 500
Meters



Part 1 of 2
GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,189

LEGEND

- Legal corner post
- Road
- Creek
- Contour at 100' interval

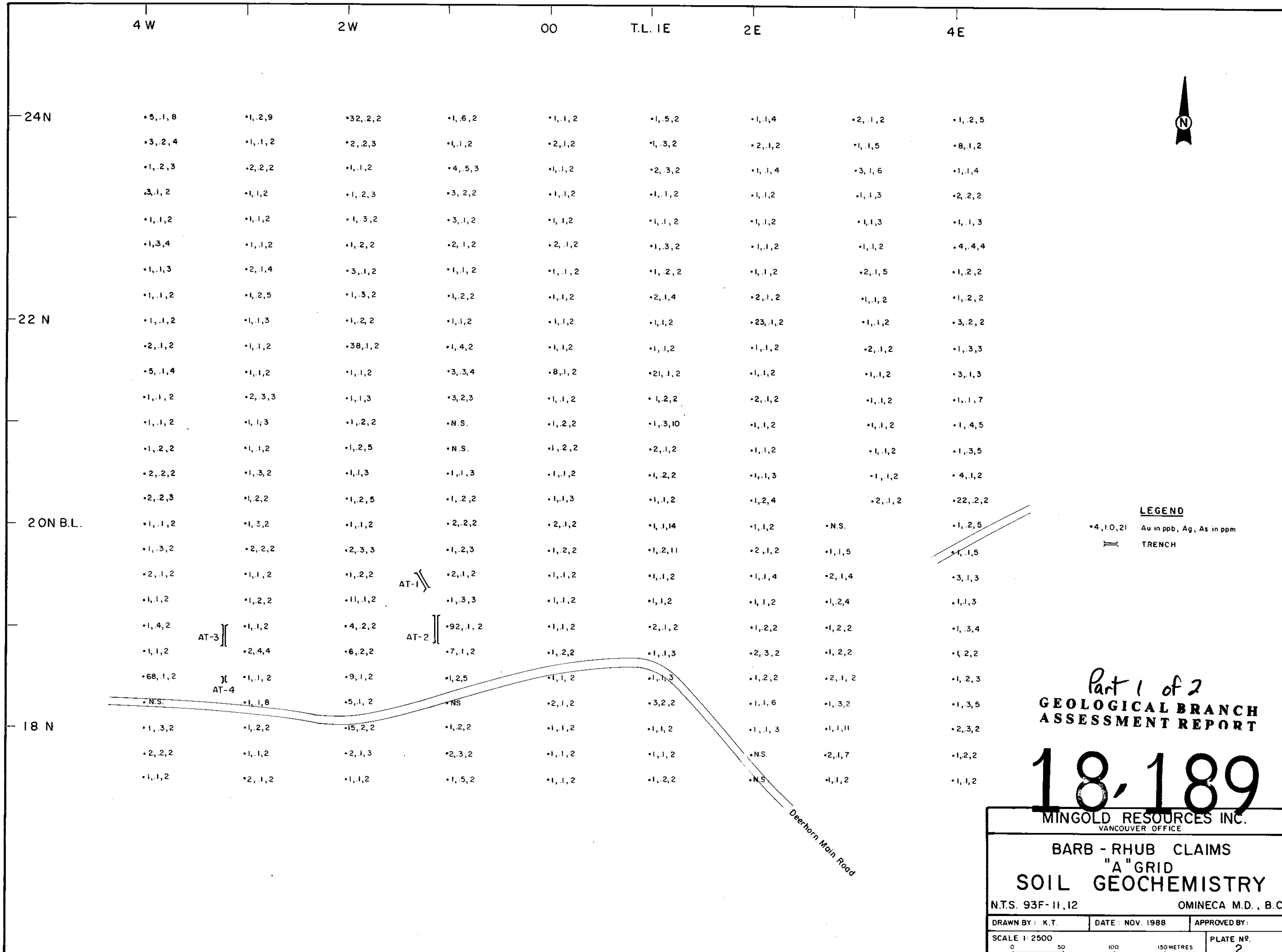
MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS

GRID LOCATION MAP

N.T.S. 93F-11,12		OMINECA M.D., B.C.
DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
	SCALE 1:12,500 0 100 200 600 metres	PLATE No. 1

CHONG



MINGOLD RESOURCES INC.
VANCOUVER OFFICE

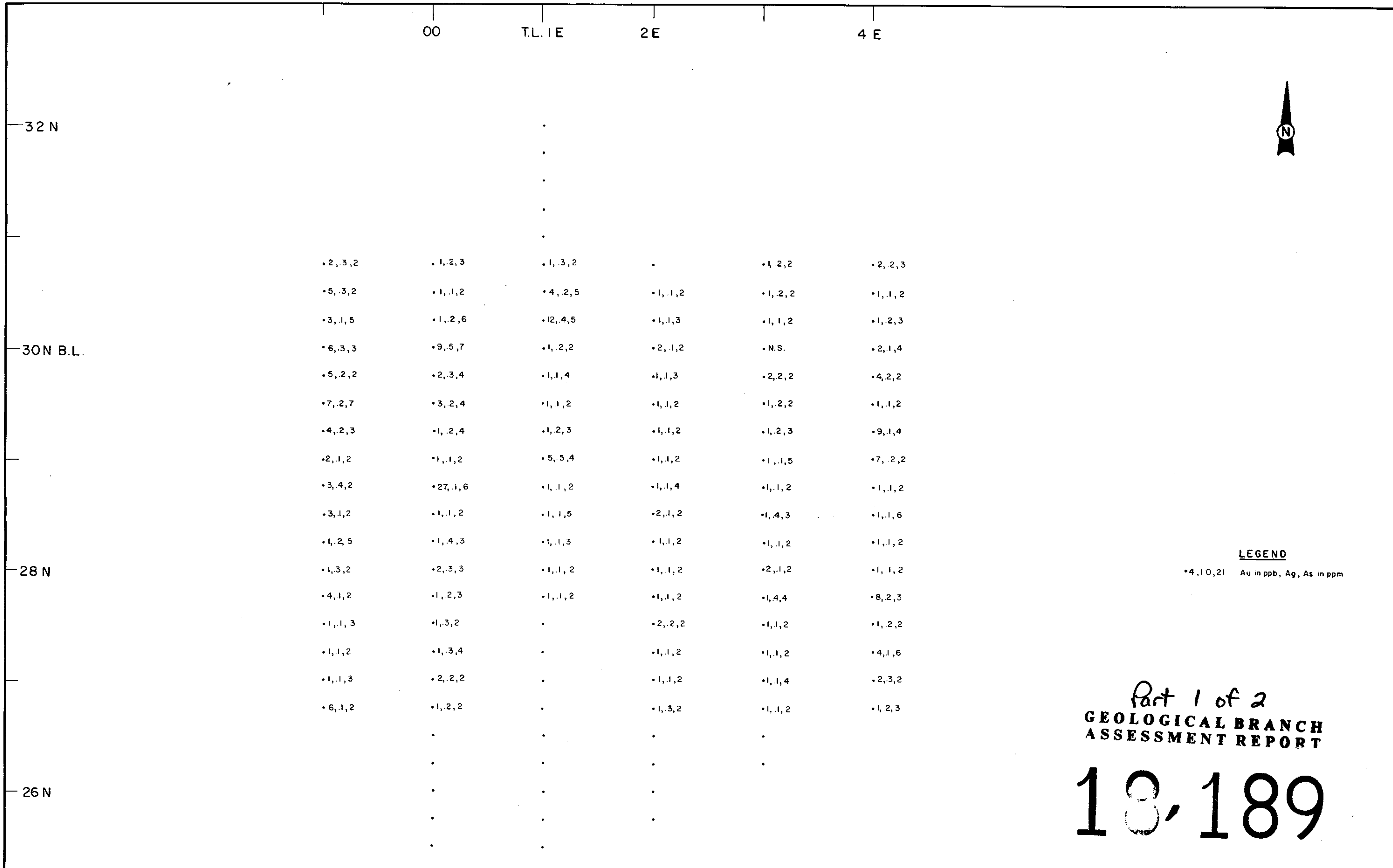
BARB - RHUB CLAIMS
"A" GRID
SOIL GEOCHEMISTRY

N.T.S. 93F-11,12 OMINECA M.D., B.C.

DRAWN BY: K.T. | DATE: NOV. 1988 | APPROVED BY:

SCALE 1:2500 0 50 100 150 METRES | PLATE No. 2

CHONG



MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS
"B" GRID
SOIL GEOCHEMISTRY

N.T.S. 93F-11,12 OMINECA M.D., B.C.

DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:

SCALE 1:2500 (0 50 100 150 METRES) — PLATE Nº. 3

CHONG

	14E		16E		18E
	1,.1,3	1,.1,2	2,.3,6	1,.1,6	1,.1,3
	1,.2,4	1,.3,3	1,.2,2	1,.1,3	1,.2,2
	2,.1,2	1,.3,2	1,.1,4	1,.1,3	1,.3,2
	1,.1,5	1,.1,2	1,.1,3	1,.2,2	N.S.
	4,.1,2	2,.1,3	1,.2,3	1,.1,2	1,.1,2
	1,.1,2	2,.3,3	16,.1,2	1,.1,5	2,.1,2
32N	1,.3,2	4,.1,2	1,.1,2	6,.1,4	2,.1,2
	3,.1,2	1,.1,3	1,.1,2	1,.1,5	N.S.
	1,.3,3	1,.2,2	1,.1,2	1,.1,6	1,.3,5
	1,.3,2	1,.1,2	1,.1,5	1,.2,4	1,.1,2
	1,.1,2	1,.1,5	1,.2,4	2,.1,6	2,.1,2
	2,.1,3	1,.1,5	14,.1,2	2,.2,3	1,.1,2
	2,.2,2	3,.3,2	1,.2,3	1,.2,2	N.S.
	1,.1,2	4,.1,3	1,.1,2	1,.1,3	1,.1,2
30N B.L.	1,.2,2	1,.1,2	1,.2,3	1,.2,2	1,.1,2
	1,.3,4	1,.1,2	3,.1,3	1,.2,2	1,.2,2
	1,.1,3	1,.1,2	1,.4,2	1,.1,2	1,.4,2
	1,.1,3	1,.3,2	N.S.	1,.1,3	1,.1,2
	2,.1,2	1,.1,2	1,.1,2	3,.1,2	1,.2,2
	2,.2,2	1,.1,2	1,.2,5	1,.1,2	1,.1,4

N

LEGEND

•4,1.0,21 Au in ppb, Ag, As in ppm

Part 1 of 2

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,189

MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS
"C" GRID
SOIL GEOCHEMISTRY

N.T.S. 93F-11,12 OMINECA M.D., B.C.

DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 (0 50 100 150 METRES)		PLATE Nº. 4

CHONG

	50E		52E		54E		56E		58E
30N B.L.	1,.1,8	3,.2,5	1,.1,4	N.S	1,.1,7	2,.1,2	1,.2,2	1,.1,2	1,.1,2
	2,.1,2	1,.1,2	N.S.	N.S.	1,.3,3	1,.1,2	2,.1,2	5,.1,2	1,.1,2
	1,.1,4	N.S.	N.S.	N.S.	1,.1,6	N.S.	1,.1,2	3,.1,2	1,.1,8
	N.S.	N.S.	N.S.	1,.1,5	1,.2,2	N.S.	1,.1,2	2,.1,3	2,.1,13
	15,.1,3	2,.1,4	1,.1,4	N.S.	1,.1,3	N.S.	4,.3,2	2,.1,2	1,.1,9
	1,.2,2	1,.1,3	2,.1,3	2,.2,2	N.S.	1,.2,3	1,.1,2	3,.1,2	1,.1,4
	3,.1,3	2,.2,3	N.S.	1,.1,6	N.S.	2,.1,2	1,.1,3	7,.1,2	N.S.
	1,.2,2	N.S.	N.S.	1,.1,2	N.S.	1,.2,2	1,.1,4	1,.1,3	1,.1,4
28N	1,.1,2	1,.2,2	N.S.	N.S.	1,.1,5	2,.1,2	2,.1,2	1,.1,6	1,.1,6
	1,.1,7	1,.1,2	1,.1,2	N.S.	1,.1,2	1,.1,2	1,.2,2	5,.4,2	1,.1,4
	2,.1,2	1,.1,2	1,.1,2	N.S.	1,.1,2	1,.1,2	1,.1,3	4,.1,8	2,.1,7
	2,.1,2	1,.1,2	NS	1,.1,2	2,.2,2	1,.2,2	1,.1,4	1,.2,2	N.S.
	1,.1,2	1,.1,2	1,.1,2	1,.1,2	N.S.	1,.1,2	N.S.	1,.1,8	1,.2,6
	1,.1,2	1,.1,2	1,.1,2	1,.1,4	1,.2,3	2,.2,3	N.S.	1,.1,3	1,.1,3
	1,.1,2	1,.1,2	1,.1,2	1,.1,2	1,.1,2	N.S.	1,.2,7	1,.1,3	1,.1,4
	1,.1,3	N.S.	4,.1,11	1,.1,5	1,.2,2	N.S.	2,.1,9	1,.1,6	1,.1,2
26N	2,.1,2	1,.1,2	1,.1,4	2,.1,2	1,.3,2	1,.2,2	1,.1,3	2,.2,4	N.S.
	1,.2,2	1,.1,2	1,.1,7	1,.2,3	1,.1,2	1,.1,2	1,.1,4	1,.1,2	2,.2,4
	1,.4,5	1,.1,6	1,.1,3	1,.1,7	N.S.	1,.1,3	1,.1,2	1,.1,2	3,.1,3
	2,.1,4	3,.1,2	N.S.	1,.1,3	1,.1,6	1,.1,7	2,.1,2	1,.1,2	1,.1,3
	N.S.	N.S.	N.S.	1,.2,5	1,.1,2	1,.1,2	N.S.	1,.1,2	1,.1,2
	N.S.	1,.1,2	1,.2,4	1,.2,2	2,.1,2	N.S.	1,.1,2	1,.1,5	N.S.
	1,.1,5	1,.1,2	1,.2,4	2,.1,2	1,.2,4	1,.2,3	1,.1,2	2,.1,2	1,.1,2
	1,.1,7	1,.1,2	1,.1,3	4,.1,6	1,.1,2	2,.1,4	12,.1,2	1,.1,2	1,.1,2
24N	1,.1,6	1,.1,2	1,.1,13	1,.3,3	3,.1,2	1,.1,3	2,.1,4	1,.1,3	1,.1,3
22N									

N

LEGEND

•4,.10,21 Au in ppb, Ag, As in ppm

Part 1 of 2

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,189

MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS
"D" GRID
SOIL GEOCHEMISTRY

N.T.S. 93F-11,12 — OMINECA M.D., B.C.

DRAWN BY: K.T. | DATE: NOV. 1988 | APPROVED BY:

SCALE 1: 2500 — 0 50 100 150 METRES | PLATE No. 5

CHONG

	74E		76E		78E		80E		82E
	1,.4,6	1,.1,3	1,.1,2	2,.1,2		1,.1,2	1,.1,2	1,.3,2	1,.1,2
	1,.1,2	1,.1,6	1,.1,8	1,.1,2		1,.2,2	2,.1,3	5,.2,2	1,.1,3
	3,.2,2	1,.1,10	1,.1,15	N.S.	1,.5,8	1,.1,2	1,.1,2	1,.3,2	1,.1,2
	1,.1,5	1,.3,7	1,.2,2	1,.1,4	1,.1,3	1,.1,2	1,.1,2	1,.2,2	1,.1,6
36 N	1,.2,4	1,.1,3	1,.5,9	1,.1,2	1,.1,5	1,.2,8	1,.2,2	N.S.	9,.3,2
	1,.1,2	1,.2,4	2,.1,2	1,.1,2	1,.1,3	1,.2,2	1,.1,2	N.S.	1,.3,2
	1,.2,4	1,.1,9	1,.1,3	1,.2,2	1,.6,13	1,.1,2	1,.1,2	3,.2,2	1,.2,2
	1,.1,2	1,.1,2	1,.1,2	1,.1,10	N.S.	1,.3,2	1,.2,5	2,.2,2	. .2,2
	3,.2,3	6,.2,3	2,.2,4	1,.1,2	1,.1,2	1,.1,4	1,.2,3	1,.3,4	1,.2,2
	1,.1,4	3,.1,3	1,.1,6	N.S.	1,.1,3	2,.2,2	6,.3,9	8,.3,2	1,.1,3
	1,.2,2	1,.1,4	7,.1,2	N.S.	1,.1,4	1,.1,4	2,.2,3	3,.4,3	2,.1,5
	1,.3,5	2,.1,2	13,.1,2	N.S.	1,.1,2	1,.1,3	.2,2,2	4,.3,2	1,.2,6
34 N	N.S.	N.S.	N.S.	1,.1,5	1,.1,2	1,.1,2	2,.1,2	1,.2,3	1,.2,2
	1,.3,11	1,.1,2	1,.2,5	1,.1,3	1,.1,2	1,.1,2	4,.1,4	1,.1,2	1,.2,6
	5,.3,2	1,.1,3	8,.3,6	1,.1,2	1,.2,2	1,.1,2	1,.1,5	1,.3,2	1,.2,5
	1,.1,2	1,.1,2	N.S.	1,.1,2	1,.1,2	1,.1,2	1,.2,6	4,.3,2	1,.3,4
	1,.1,2	N.S.	1,.1,3	1,.1,3	3,.1,2	2,.1,6	1,.1,2	1,.2,2	1,.4,5
	1,.5,7	1,.1,2	1,.1,2	1,.1,2	1,.2,2	1,.1,3	1,.1,2	3,.4,2	1,.2,6
	N.S.	2,.1,2	1,.2,3	12,.3,10	1,.2,5	2,.1,6	1,.1,2	1,.2,2	1,.1,6
	1,.1,2	2,.1,4	N.S.	2,.1,3	1,.1,2	1,.1,4	2,.1,2	1,.2,2	3,.4,11
32 N	1,.1,2	2,.1,3	2,.1,2	41,.2,2	1,.2,2	1,.2,5	1,.1,2	1,.1,3	5,.3,13
30 N B.L.									

LEGEND

•4,1.0,21 Au in ppb, Ag, As in ppm

Part 1 of 2

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,189

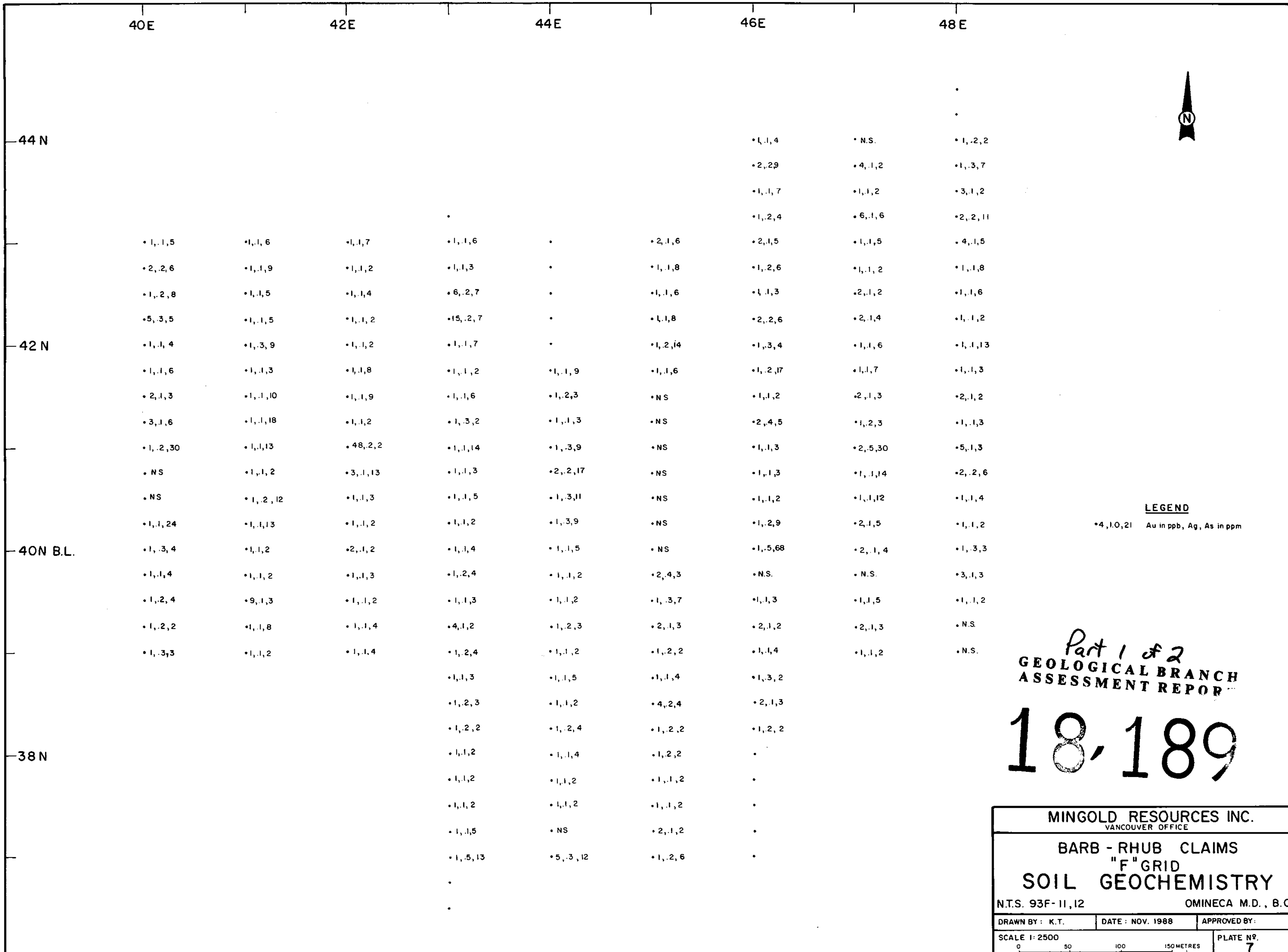
MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS
"E" GRID
SOIL GEOCHEMISTRY

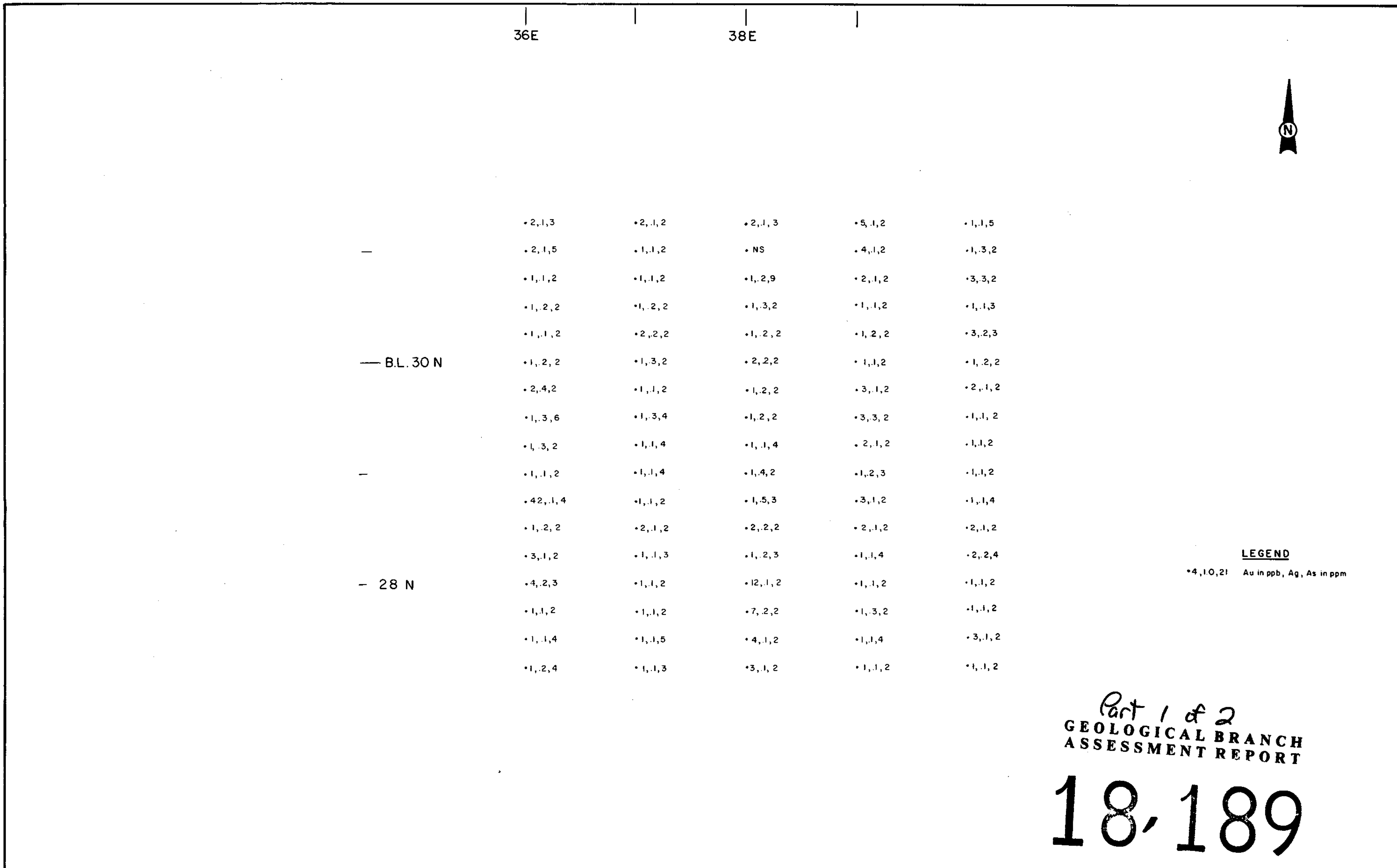
N.T.S. 93F-11,12 OMINECA M.D., B.C.

DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 (0 50 100 150 METRES)		PLATE No. 6

CHONG



40E
42E
44E
46E
48E
44 N
42 N
40N B.L.
38 N
LEGEND
•4,1.0,21 Au in ppb, Ag, As in ppm
Part 1 of 2
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,189
MINGOLD RESOURCES INC.
VANCOUVER OFFICE
BARB - RHUB CLAIMS
"F" GRID
SOIL GEOCHEMISTRY
N.T.S. 93F-11,12
OMINECA M.D., B.C.
DRAWN BY: K.T.
DATE: NOV. 1988
APPROVED BY:
SCALE 1:2500
0 50 100 150 METRES
PLATE No. 7
CHONG

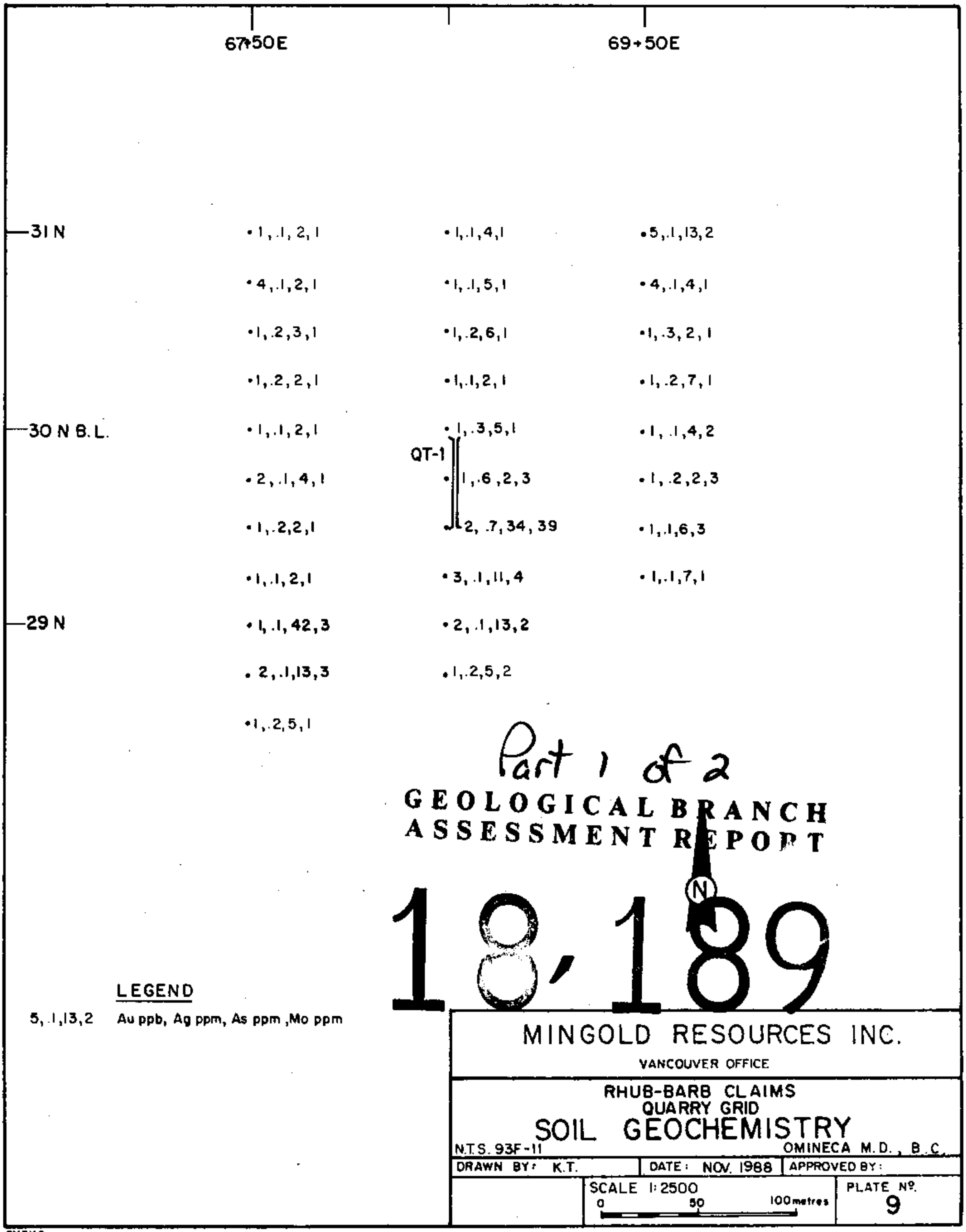


MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS
"G" GRID
SOIL GEOCHEMISTRY

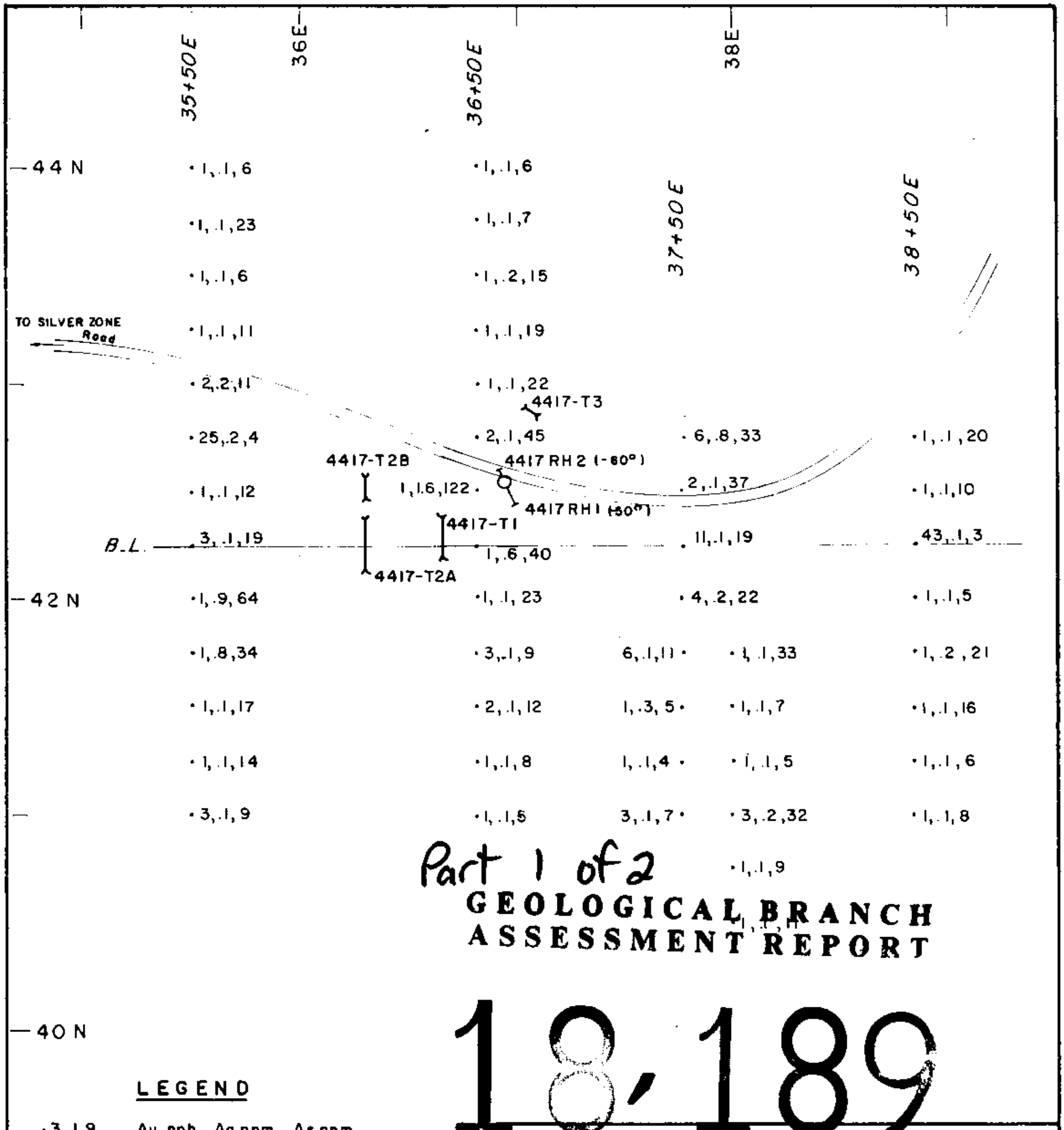
N.T.S. 93F-11,12		OMINECA M.D., B.C.
DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 (0 50 100 150 METRES)		PLATE Nº. 8

CHONG



67+50E
69+50E
31 N
30 N B.L.
29 N
•1,.1,2,1
•4,.1,2,1
•1,.2,3,1
•1,.2,2,1
•1,.1,2,1
•2,.1,4,1
•1,.2,2,1
•1,.1,2,1
•1,.1,42,3
•2,.1,13,3
•1,.2,5,1
•1,.1,4,1
•1,.1,5,1
•1,.2,6,1
•1,.1,2,1
•1,.3,5,1
QT-1
•1,.6,2,3
•2,.7,34,39
•3,.1,11,4
•2,.1,13,2
•1,.2,5,2
•5,.1,13,2
•4,.1,4,1
•1,.3,2,1
•1,.2,7,1
•1,.1,4,2
•1,.2,2,3
•1,.1,6,3
•1,.1,7,1
Part 1 of 2
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,189
N
LEGEND
5,.1,13,2 Au ppb, Ag ppm, As ppm, Mo ppm
MINGOLD RESOURCES INC.
VANCOUVER OFFICE
RHUB-BARB CLAIMS
QUARRY GRID
SOIL GEOCHEMISTRY
N.T.S. 93F-11
OMINECA M.D., B.C.
DRAWN BY: K.T.
DATE: NOV. 1988
APPROVED BY:
SCALE 1:2500
0 50 100 metres
PLATE No. 9

CHONG



MINGOLD RESOURCES INC.

VANCOUVER OFFICE

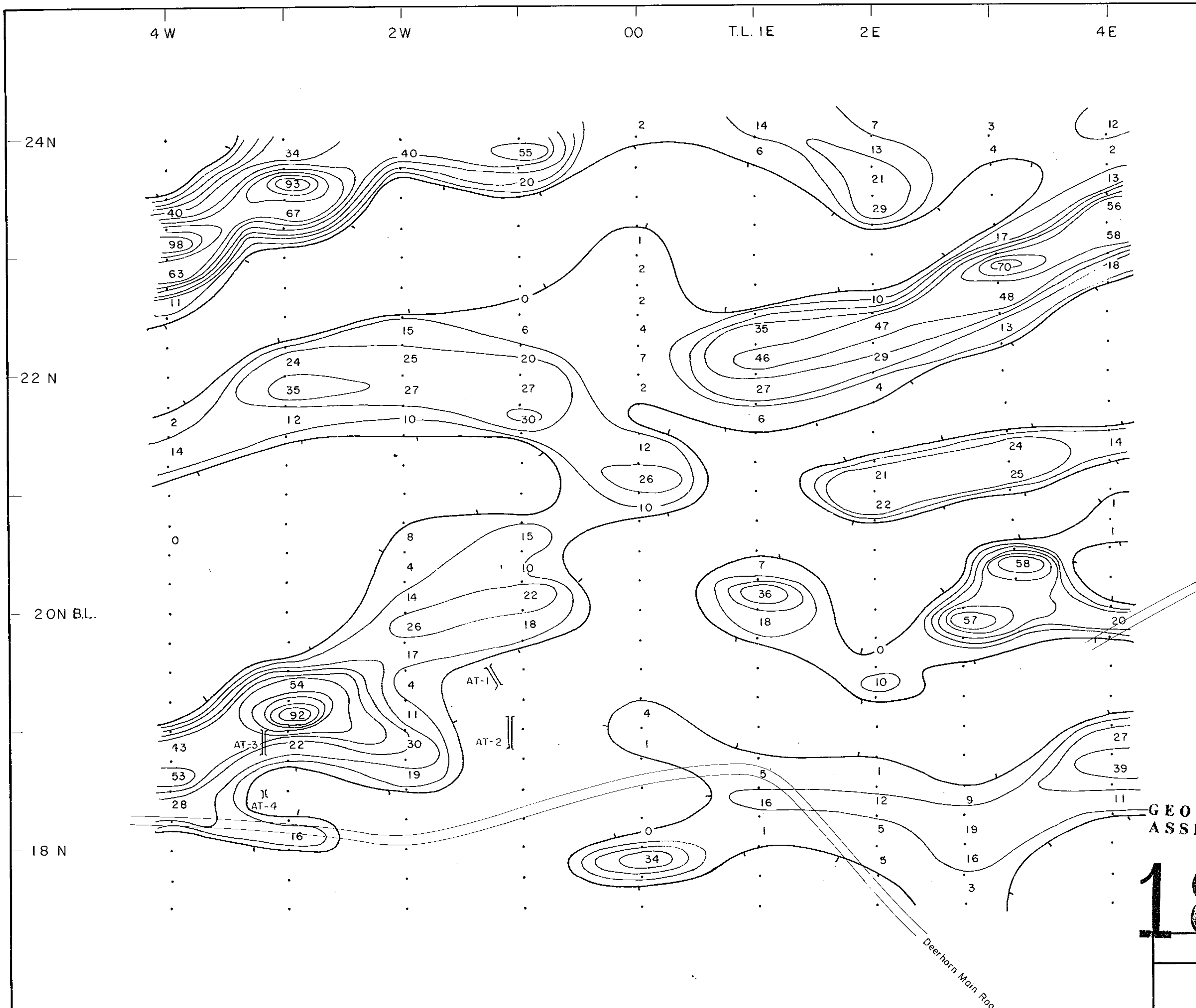
BARB - RHUB CLAIMS
4417 GRID

SOIL GEOCHEMISTRY - Au, Ag, As

DRAWN BY: K.T.	DATE: DEC. 1988	APPROVED BY:
SCALE 1:2500 (0 – 50 – 100 METRES)		PLATE No. 10

CHONG

51+00E
54+00E
57+00E
T.L. 60+00 E
60+00 E
63+00E
66+00E
69+00E
72+00E
40+00 N
BL. 40+00 N
35+00 N
30+00 N
B.L. 30+00N
25+00 N
20+00 N
TRENCH QT-1
LEGEND
·1,.1,8 Au ppb, Ag ppm, As ppm
Co-ordinates in italic are 1987 grid
Part 1 of 2
GEOLOGICAL BRANCH ASSESSMENT REPORT
18,189
MINGOLD RESOURCES INC.
VANCOUVER OFFICE
BARB - RHUB CLAIMS
4410 FILL IN GRID
SOIL GEOCHEMISTRY – Au, Ag, As
N.T.S. 93F-11,12
OMINECA M.D., B.C.
DRAWN BY: K.T.
DATE: DEC. 1988
APPROVED BY:
SCALE 1:2500
0 50 100 200 METRES
PLATE Nº
11
CHONG



LEGEND

21 FRASER FILTERED VALUE

TRENCH

CONTOURS INTERVAL AT 10 DEGREES

Tx MAINE →

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GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,189

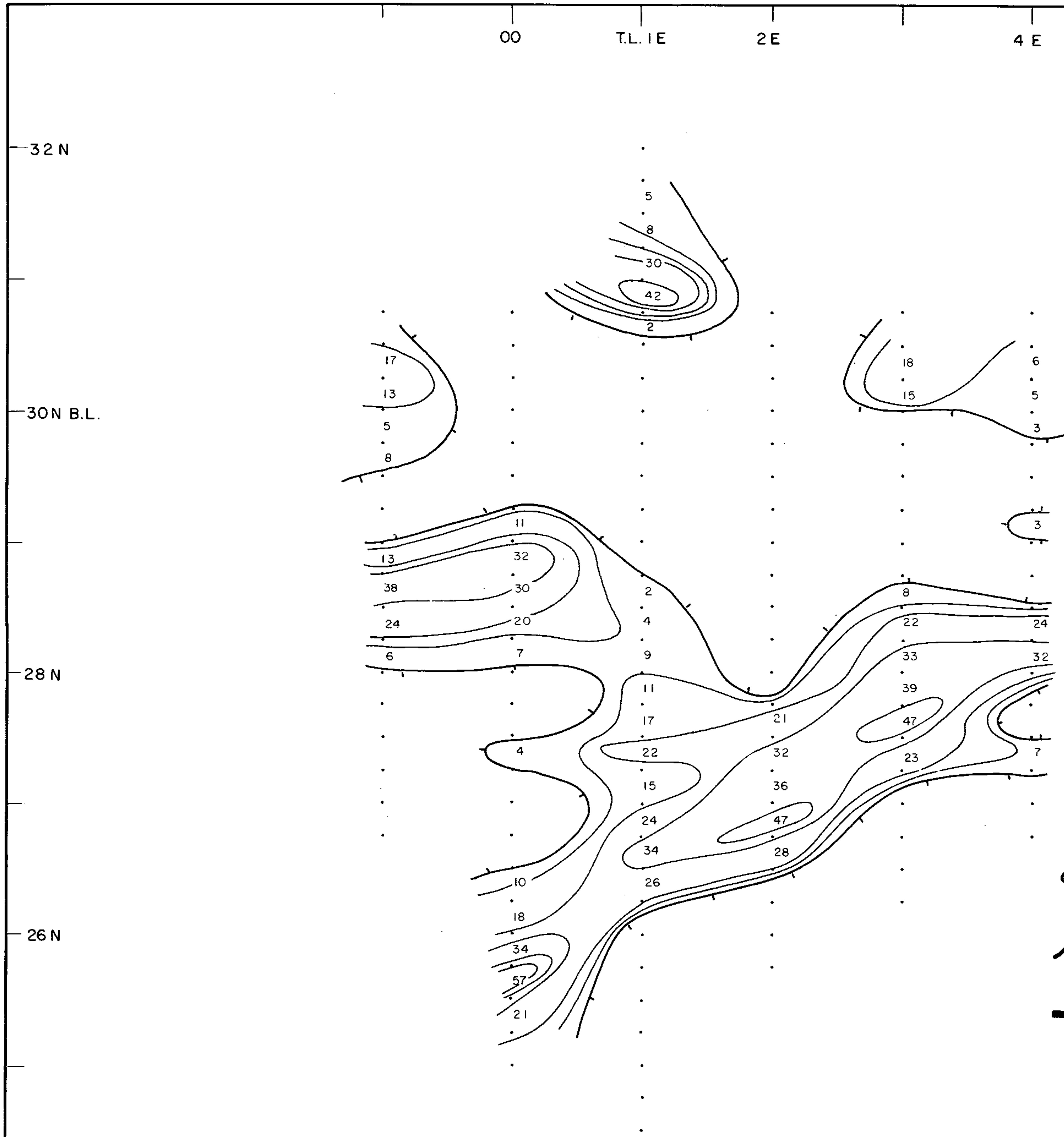
MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS
"A" GRID
VLF-EM SURVEY (Fraser Filtered)

N.T.S. 93F-11,12 — OMINECA M.D., B.C.

DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 (0, 50, 100, 150 METRES)		PLATE Nº. 12

CHONG



Part 1 of 2

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,189

LEGEND

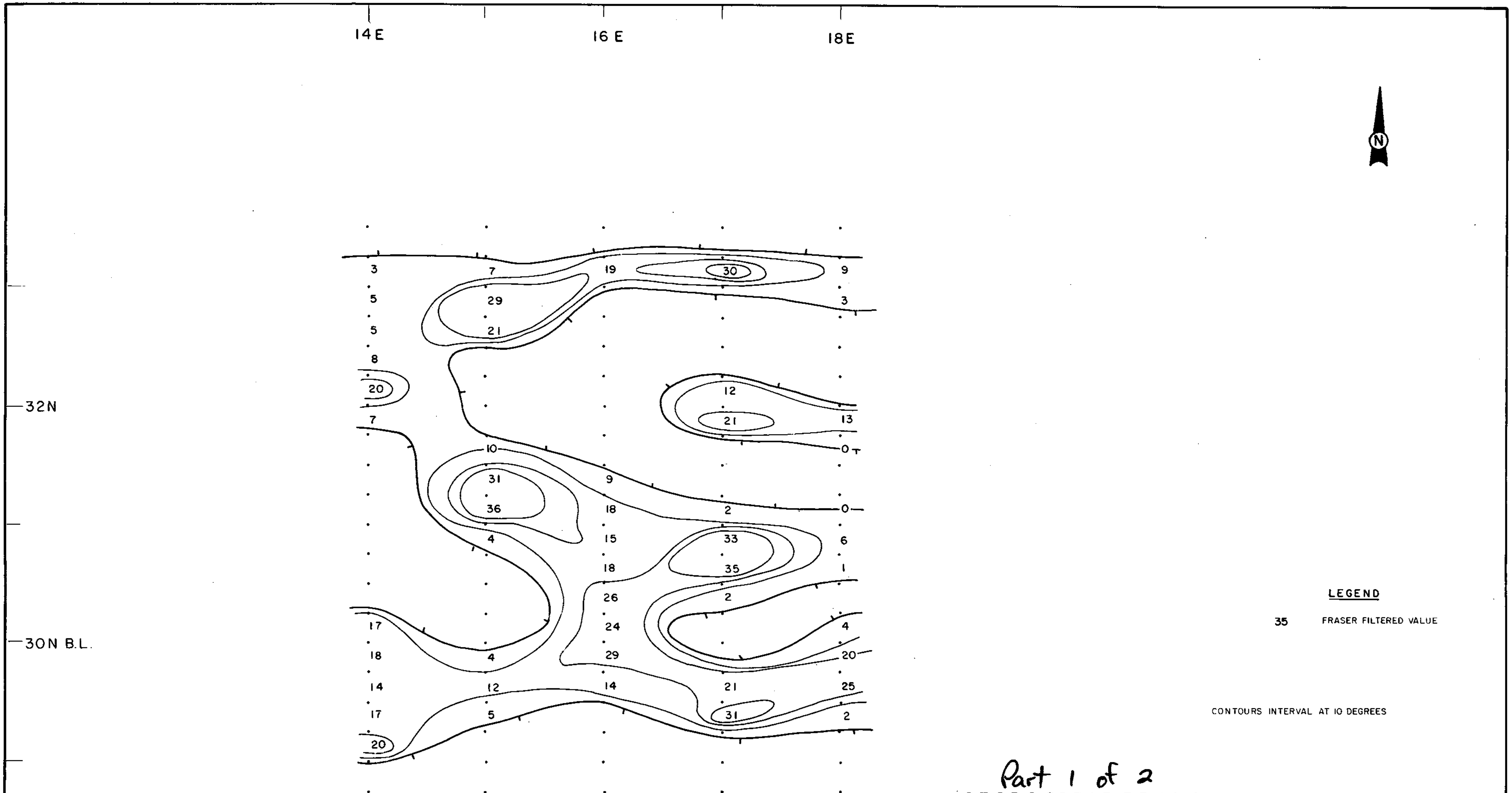
18 FRASER FILTERED VALUE

CONTOURS INTERVAL AT 10 DEGREES

Tx MAINE

MINGOLD RESOURCES INC. VANCOUVER OFFICE		
BARB - RHUB CLAIMS "B" GRID VLF-EM SURVEY (Fraser Filtered)		
N.T.S. 93F-11,12		OMINECA M.D., B.C.
DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 (0 50 100 150 METRES)		PLATE No. 13

CHONG



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GEOLOGICAL BRANCH
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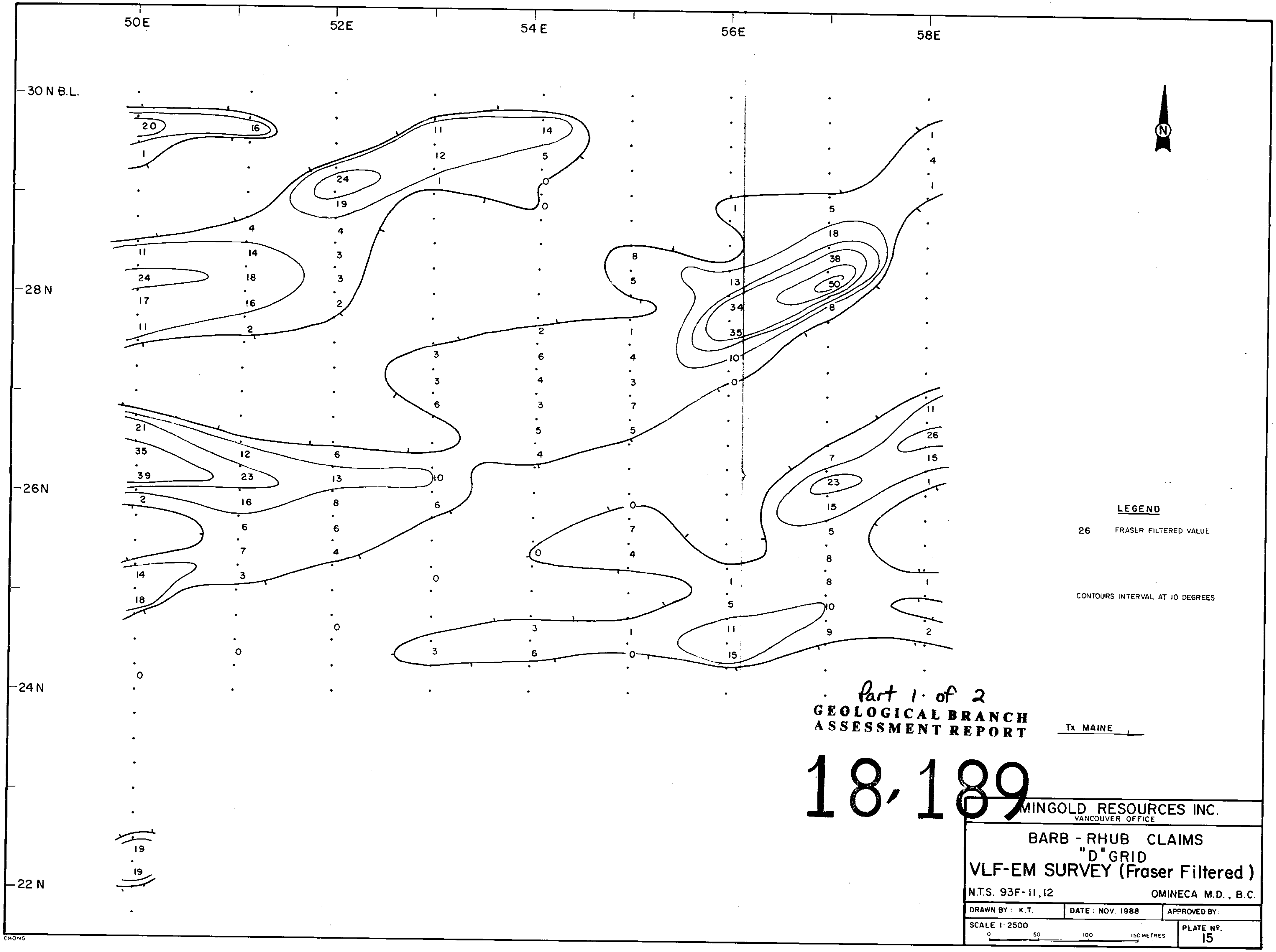
MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB - RHUB CLAIMS
"C" GRID
VLF-EM SURVEY (Fraser Filtered)

N.T.S. 93F-11,12 OMINECA M.D., B.C.

DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 (0 50 100 150 METRES)		PLATE Nº. 14

CHONG


50E
52E
54E
56E
58E
30 N B.L.
28 N
26 N
24 N
22 N
N
LEGEND
26 FRASER FILTERED VALUE
CONTOURS INTERVAL AT 10 DEGREES
Tx MAINE
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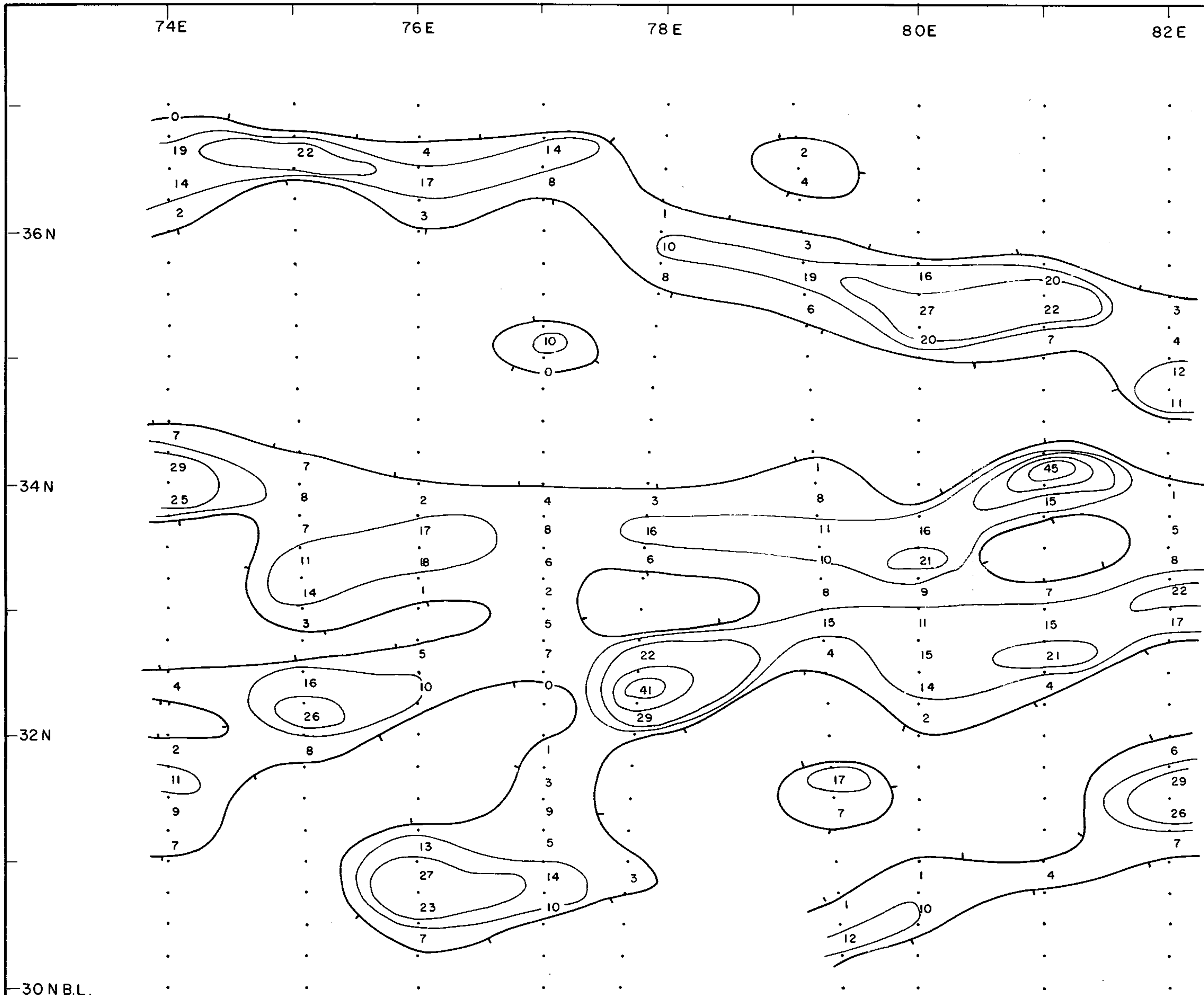
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,189
MINGOLD RESOURCES INC.
VANCOUVER OFFICE
BARB - RHUB CLAIMS
"D" GRID
VLF-EM SURVEY (Fraser Filtered)
N.T.S. 93F-11,12
OMINECA M.D., B.C.
DRAWN BY: K.T.
DATE: NOV. 1988
APPROVED BY:
SCALE 1:2500
0 50 100 150 METRES
PLATE No. 15
CHONG



LEGEND

21 FRASER FILTERED VALUE

CONTOURS INTERVAL AT 10 DEGREES

Tx MAINE

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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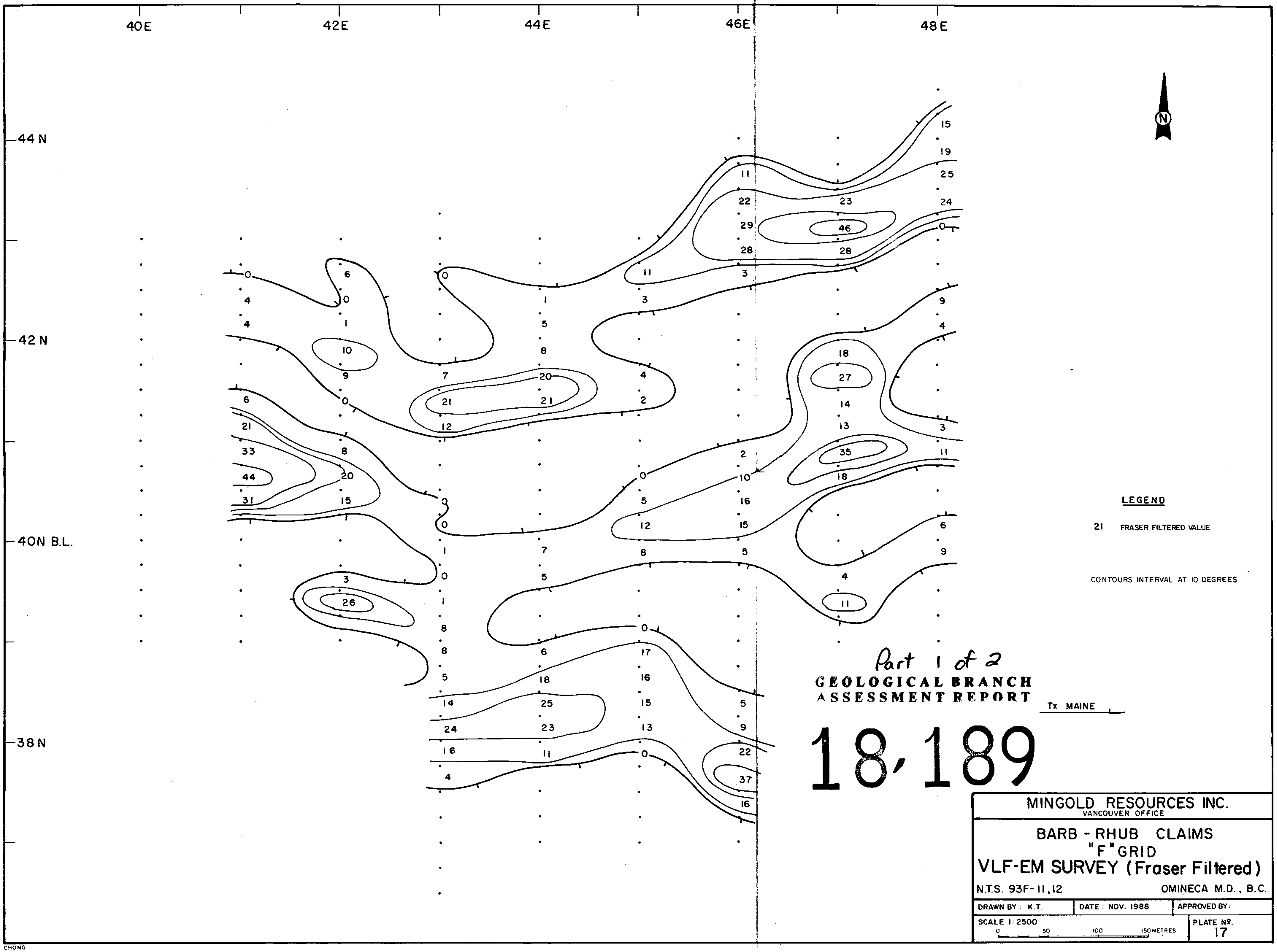
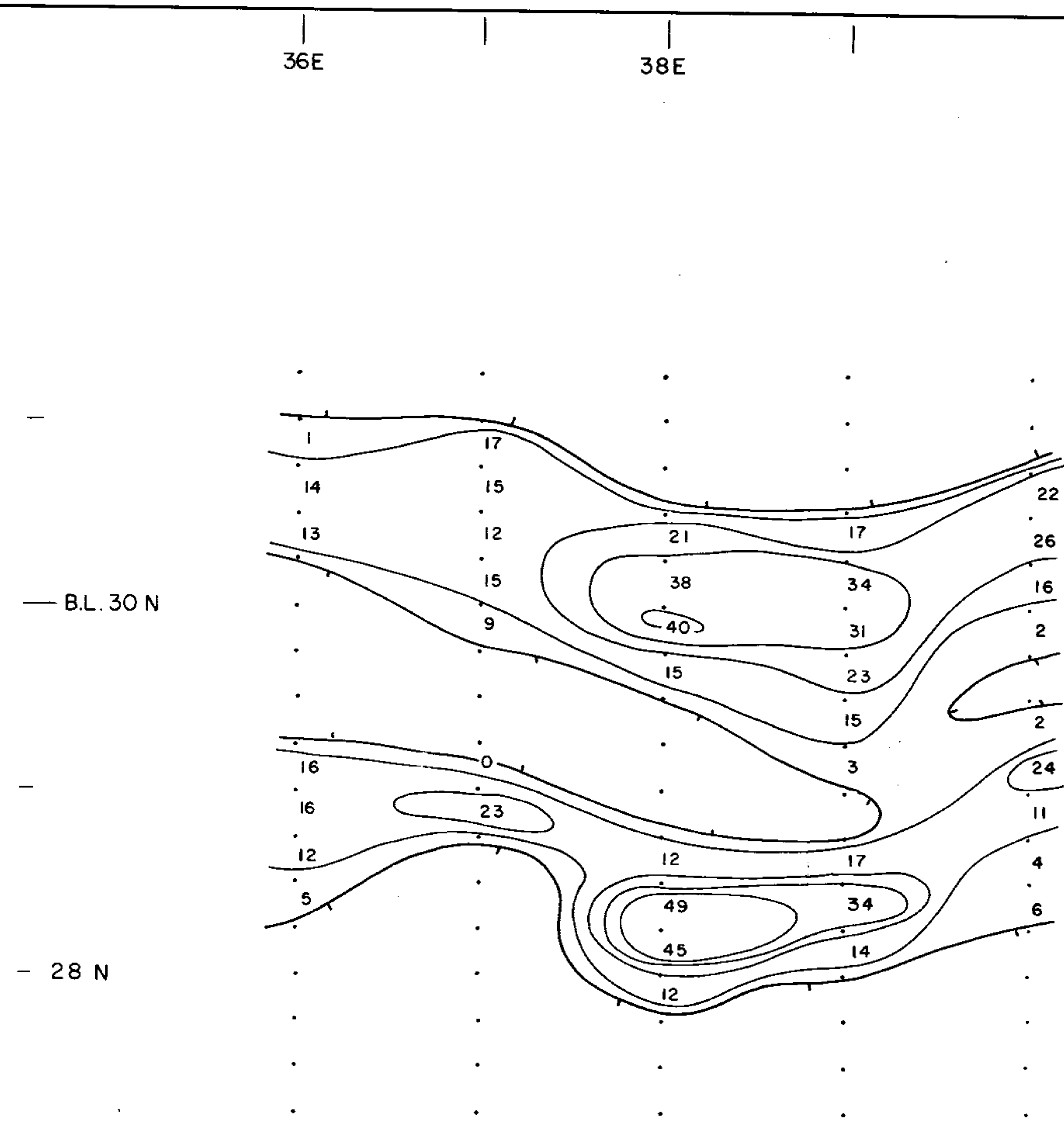
MINGOLD RESOURCES INC. VANCOUVER OFFICE		
BARB - RHUB CLAIMS "E" GRID VLF-EM SURVEY (Fraser Filtered)		
N.T.S. 93F-11,12		OMINECA M.D., B.C.
DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 (0 50 100 150 METRES)		PLATE Nº. 16

CHONG


40E
42E
44E
46E
48E
44 N
42 N
40N B.L.
38 N
N
LEGEND
21 FRASER FILTERED VALUE
CONTOURS INTERVAL AT 10 DEGREES
Part 1 of 2
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,189
Tx MAINE
MINGOLD RESOURCES INC.
VANCOUVER OFFICE
BARB - RHUB CLAIMS
"F" GRID
VLF-EM SURVEY (Fraser Filtered)
N.T.S. 93F-11,12
OMINECA M.D., B.C.
DRAWN BY: K.T.
DATE: NOV. 1988
APPROVED BY:
SCALE 1:2500
0 50 100 150 METRES
PLATE Nº. 17
CHONG



LEGEND

21 FRASER FILTERED VALUE

CONTOURS INTERVAL AT 10 DEGREES

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GEOLOGICAL BRANCH
ASSESSMENT REPORT

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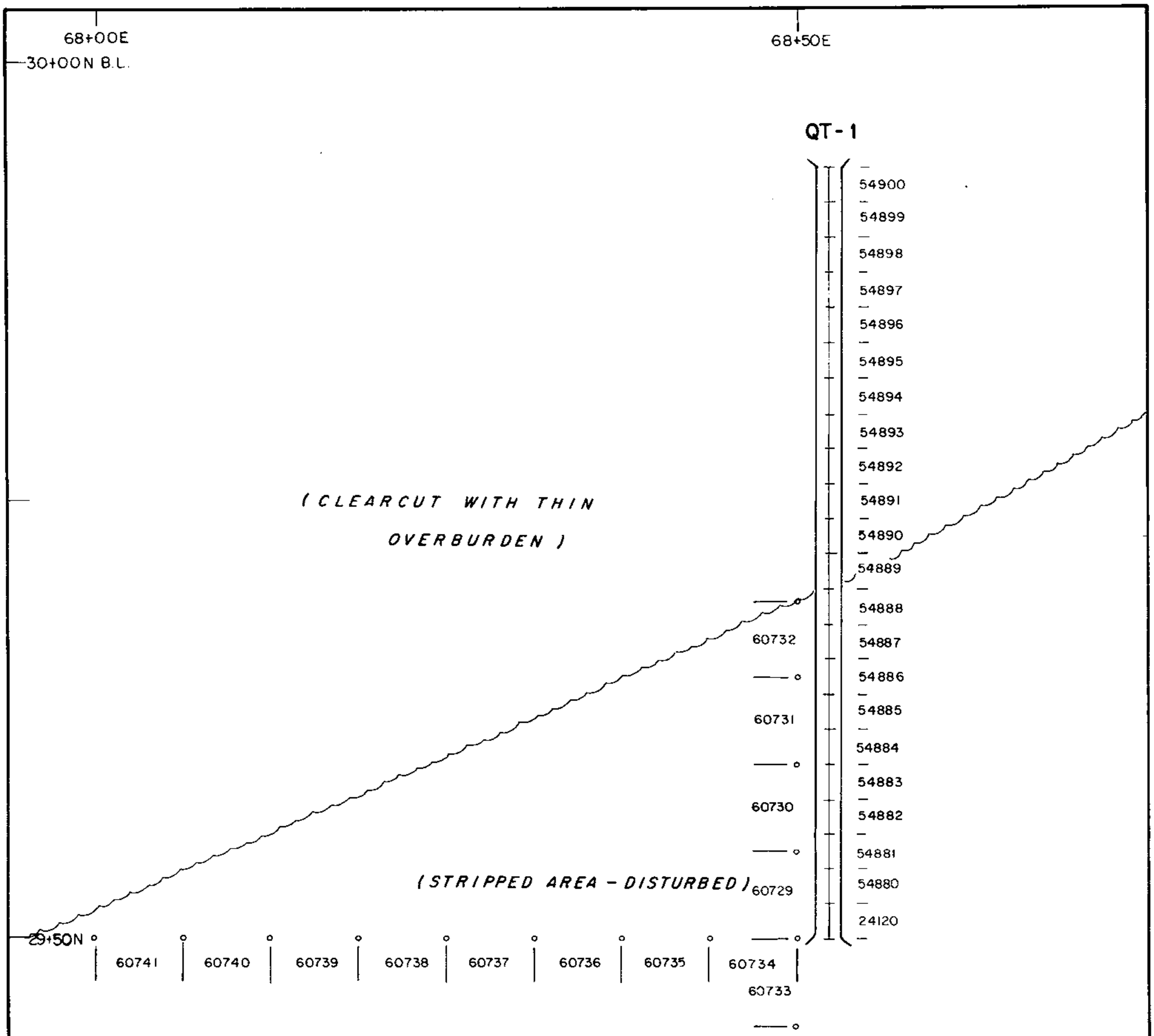
Tx MAINE

MINGOLD RESOURCES INC. VANCOUVER OFFICE		
BARB - RHUB CLAIMS "G" GRID VLF-EM SURVEY (Fraser Filtered)		
N.T.S. 93F-11,12		OMINECA M.D., B.C.
DRAWN BY: K.T.	DATE: NOV. 1988	APPROVED BY:
SCALE 1:2500 0 50 100 150 METRES		PLATE Nº. 18

CHONG



SAMPLE Nº.	TYPE	WIDTH m.	Au ppb	Ag ppm	As ppm	Mo ppm
24120	Channel	2.0	2	.1	10	2
54880	"	"	5	.1	41	23
54881	"	"	7	.1	25	14
54882	"	"	3	.1	26	28
54883	"	"	2	.4	37	66
54884	"	"	6	.5	29	22
54885	"	"	4	.3	29	13
54886	"	"	2	.1	25	11
54887	"	"	5	.2	30	49
54888	"	"	3	.2	29	90
54889	"	"	2	.4	16	74
54890	"	"	1	.5	24	109
54891	"	"	2	.6	46	126
54892	"	"	2	1.0	37	93
54893	"	"	1	.6	32	75
54894	"	"	2	.2	36	20
54895	"	"	1	.2	38	34
54896	"	"	1	.1	21	9
54897	"	"	1	.1	21	10
54898	"	"	1	.1	14	4
54899	"	"	3	.1	20	7
54900	"	"	1	.1	12	2
60729	Cont.chip	5.0	1	.1	27	24
60730	"	"	57	.5	39	45
60731	"	"	7	.1	26	45
60732	"	4.3	54	.1	22	57
60733	"	5.0	5	.4	25	27
60734	"	"	10	.2	31	19
60735	"	"	1	.1	32	32
60736	"	"	11	.3	49	41
60737	"	"	2	.5	33	35
60738	"	"	4	.5	29	25
60739	"	"	3	.1	27	28
60740	"	"	3	.1	17	13
60741	"	"	1	.1	17	11

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GEOLOGICAL BRANCH ASSESSMENT REPORT

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N

MINGOLD RESOURCES INC.

VANCOUVER OFFICE

RHUB - BARB CLAIMS

QUARRY ZONE

TRENCHING & ROCK SAMPLING

N.T.S. 93F-11 OMINECA M.D., B.C.

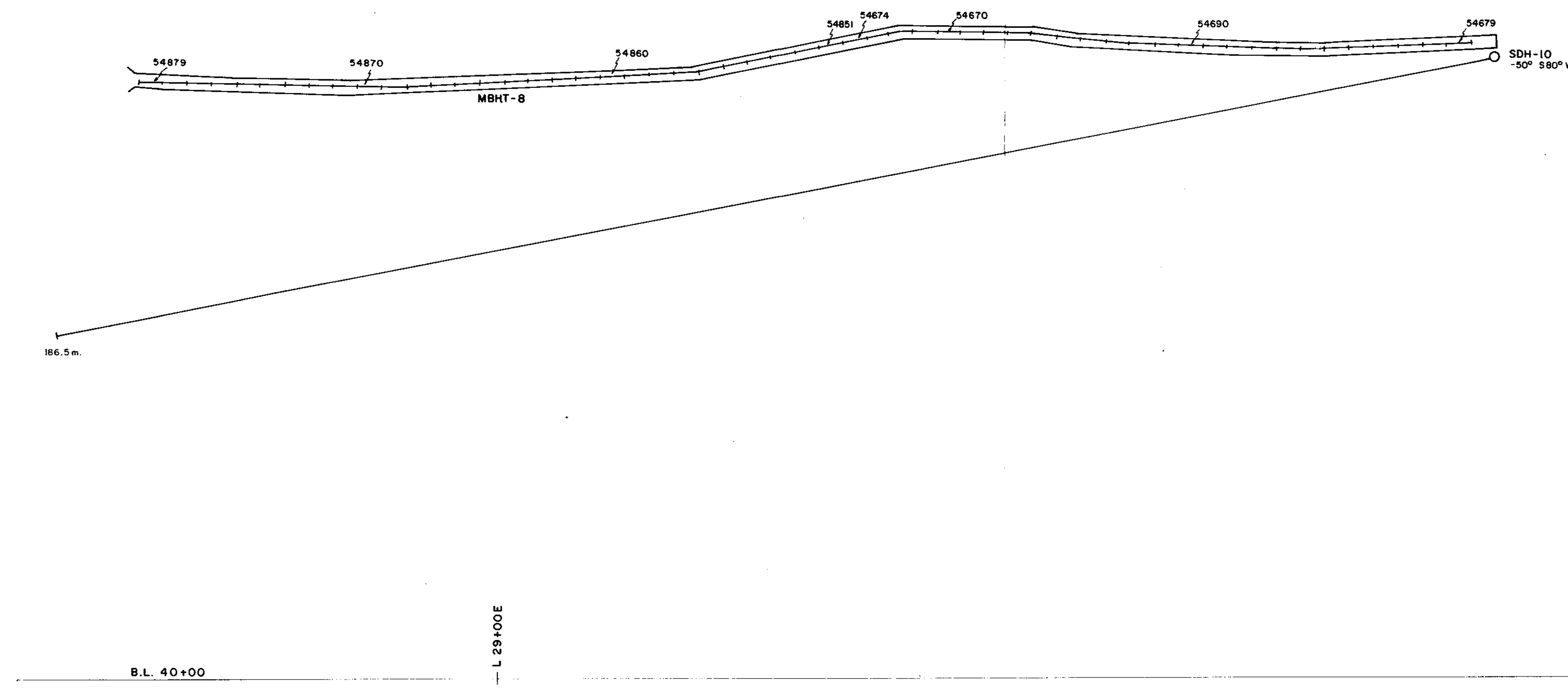
DRAWN BY: K.T. DATE: NOV. 1988 APPROVED BY:

SCALE 1:250 0 5 10metres PLATE Nº. 19

CHONG

TRENCH MBHT - 8

SAMPLE No.	WIDTH (m)	Au (ppb)	Ag (ppm)	As (ppm)
54679	2	3	.3	21
54680	2	1	.3	17
54681	2	1	.8	33
54682	2	1	.2	16
54683	2	2	.2	25
54684	2	1	.2	33
54685	2	1	.1	23
54686	2	1	.2	23
54687	2	1	.1	14
54688	2	2	.1	17
54689	2	1	.1	17
54690	2	1	.1	17
54691	2	1	.1	11
54692	2	1	.1	9
54693	2	1	.1	5
54694	2	1	.1	11
54695	2	2	.1	9
54696	2	1	.1	9
54697	2	1	.1	13
54698	2	1	.1	10
54699	2	1	.1	10
54700	2	1	.1	24
54851	2	1	.1	18
54852	2	1	.1	14
54853	2	2	.1	28
54854	2	1	.1	21
54855	2	3	.1	64
54856	2	1	.1	124
54857	2	3	.1	113
54858	2	1	.1	81
54859	2	1	.1	72
54860	2	1	.1	48
54861	2	1	.1	48
54862	2	1	.2	23
54863	2	1	.2	23
54864	2	1	.1	18
54865	2	93	4.8	661
54866	2	1	.1	28
54867	2	1	.2	14
54868	2	1	.1	9
54869	2	1	.1	20
54870	2	1	.1	10
54871	2	1	.1	9
54872	2	1	.1	9
54873	2	3	.1	20
54874	2	[illegible]	.1	20
54875	2	[illegible]	.1	7
54876	2	62	.1	16
54877	2	3	.1	11
54878	2	31	.1	22
54879	2	2	.1	9



TRENCH MBHT - 7

SAMPLE No.	WIDTH (m)	Au (ppb)	Ag (ppm)	As (ppm)
54651	1.5	1	.2	199
54652	2	1	.4	317
54653	2	105	4.5	1290
54654	2	1	.2	308
54655	2	31	1.6	1182
54656	2	24	.8	314
54657	2	1	.2	195
54658	2	1	.1	152
54659	2	48	2.3	483
54660	2	1	.1	94
54661	2	1	.5	744
54662	2	1	.2	281

TRENCH MBHT - 6

SAMPLE No.	WIDTH (m)	Au (ppb)	Ag (ppm)	As (ppm)
54663	2	135	9.9	1431
54664	2	16	2.4	560
54665	2	1	.1	24
54666	.8	10	12.4	229
54667	.8	1125	239.1	3295
54668	1.1	117	34.8	1306
54669	1.9	114	96.4	1629
54670	1	915	214.4	2960
54671	2.2	855	226.4	2561
54672	2.4	31	3.6	426
54673	1.4	125	6.7	1186
54674	.85	24	.7	663
54675	.75	5	.4	808
54676	2	12	.7	575
54677	.5	1	.4	398
54678	1.9	26	1.2	582

LEGEND

4350	ASSAY Nº.
2.0/3.22/.018	WIDTH, m / Ag / Au (oz / ton)
(trench symbol)	TRENCH
○ SRH	1987 REVERSE CIRCULATION DRILL HOLE
○ SDH	1988 DIAMOND DRILL HOLE

NOTE : ONLY VALUES ≥ 1.0 oz/t Ag OR ≥ 0.03 oz/t Au PLOTTED.

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GEOLOGICAL BRANCH
ASSESSMENT REPORT

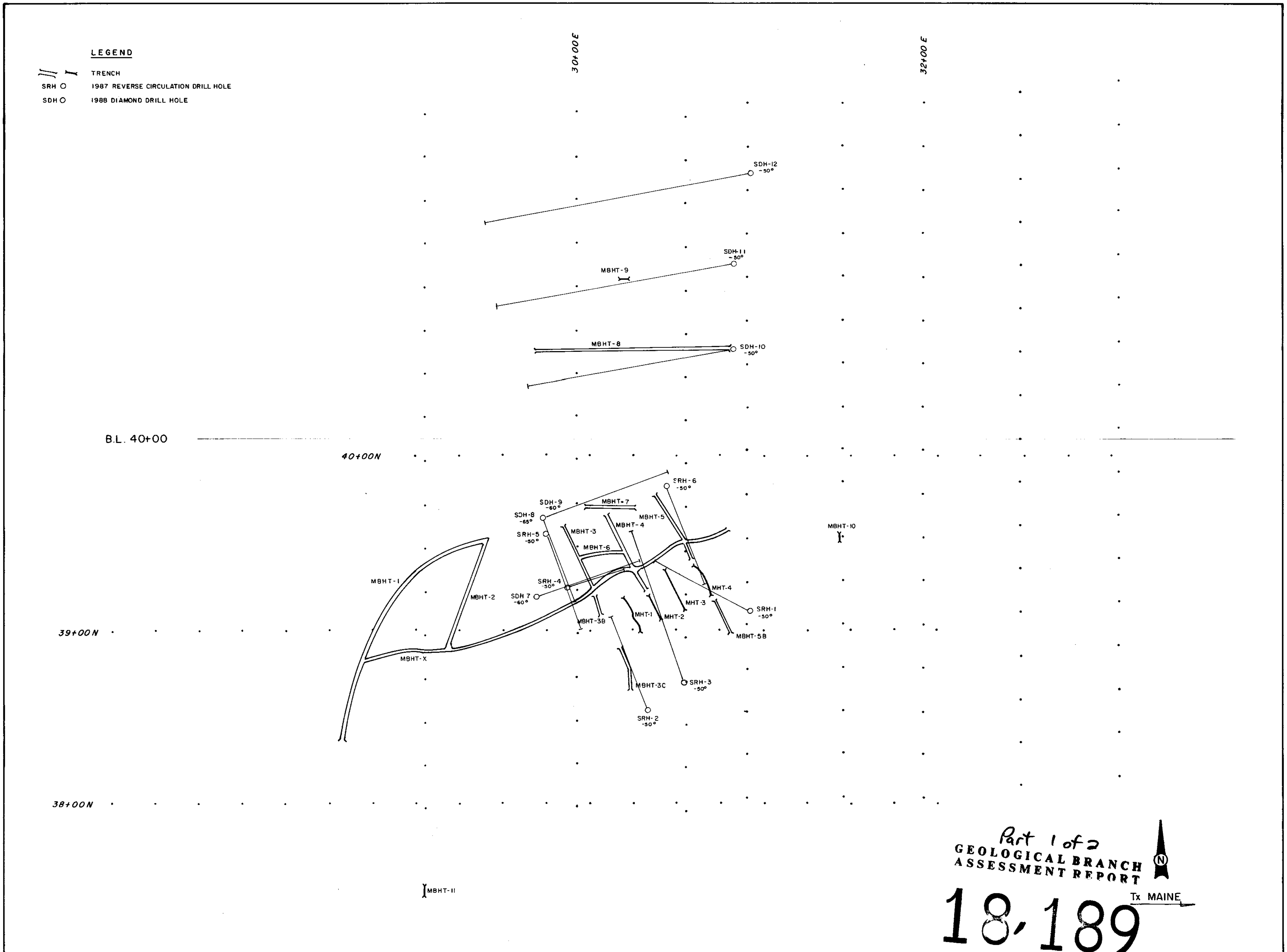
18,189

MINGOLD RESOURCES INC.
VANCOUVER OFFICE

BARB-RHUB CLAIMS
SILVER DISCOVERY
SURFACE DRILLING & TRENCHING

DRAWN BY : K.T. | DATE : NOV. 1988
SCALE 1: 250 (0 5 10 15 metres) | PLATE Nº. : 20

CHONG



Note : *Italic* co-ordinates are 1987 grid whereas straight " " 1988 grid

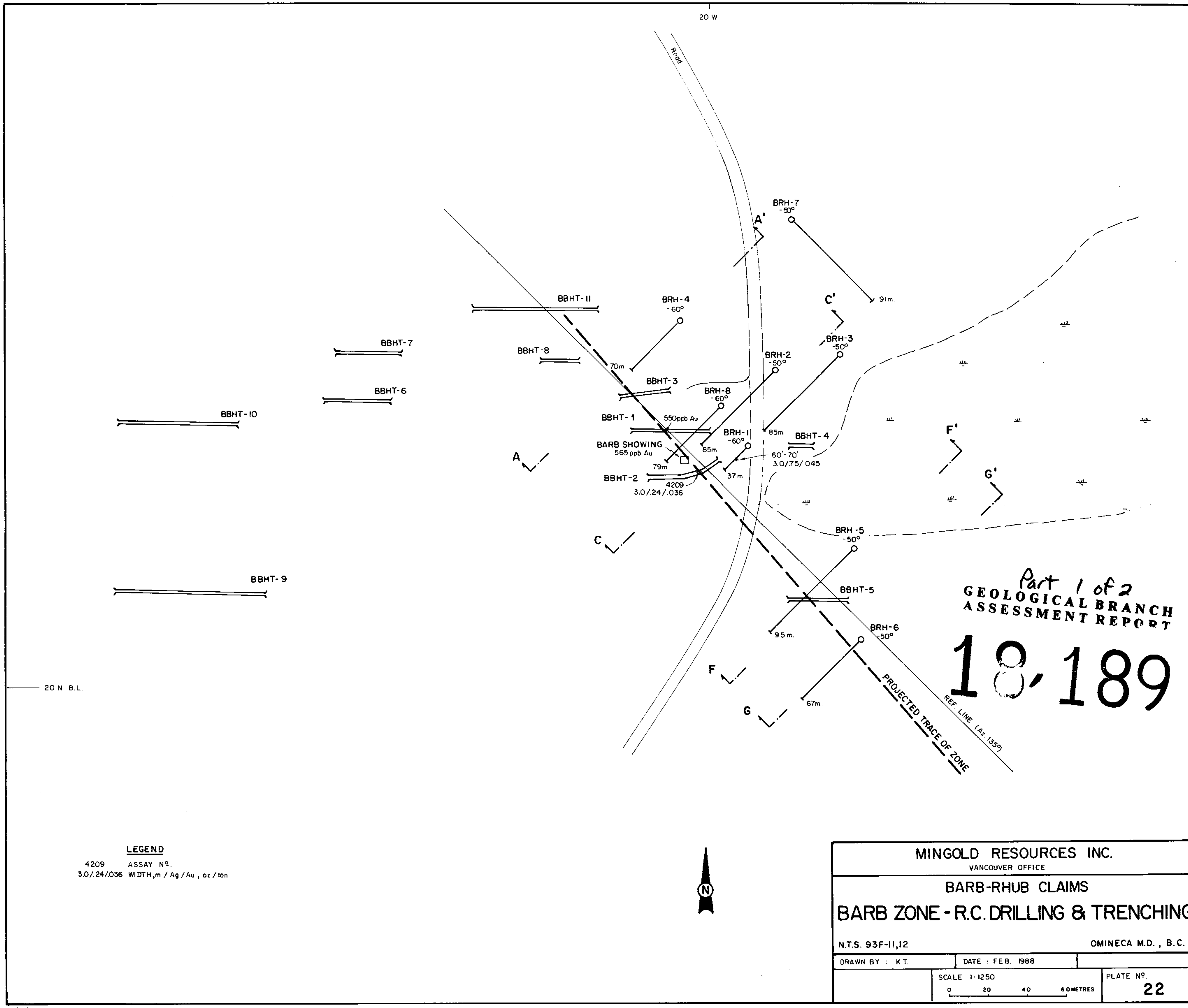
MINGOLD RESOURCES INC.

BARB - RHUB CLAIMS
SILVER ZONE
DRILLING / TRENCHING

N.T.S. 93F-11,12 OMINECA M.D., B.C.

DRAWN BY : K.T.	DATE : NOV. 1988	APPROVED BY :
SCALE 1:1250 (0 20 40 80 METRES)		PLATE No. 21

CHONG



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