ASSESSMENT REPORT
ON
GEOLOGICAL, GEOCHEMICAL & GEOPHYSICAL WORK
ON THE FOLLOWING CLAIMS

TR 5 ..... 4961(9)

[PART OF THE NORTH GROUP]

AND

TR 8 ..... 4964(9)

[PART OF THE SOUTH GROUP]

located

80 KM NORTH-NORTHWEST OF
STEWART, BRITISH COLUMBIA
SKEENA MINING DIVISION

56 degrees 35 minutes latitude
130 degrees 09 minutes longitude

N.T.S. 104B/9E

PROJECT PERIOD: June 11 - Sept. 27, 1987

ON BEHALF OF
TEUTON RESOURCES CORP.
VANCOUVER, B.C.

REPORT BY

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Date: Dec. 28, 1988

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1. INTRODUCTION

A. Property, Location, Access and Physiography

The TR property is located about 80 km north-northwest of Stewart, British Columbia. Nearest road is the Cassiar-Stewart Highway about 17 km to the east. Access is presently dependent upon helicopter services based at Stewart (Vancouver Island Helicopters) or alternatively at Bob Quinn Lake (Northern Mountain Helicopters). During the 1988 program, personnel and supplies were shuttled in from the air strip at Tide Lake Flats, situated at the terminus of the Granduc mining road about 20 km south of the property.

The claims cover an area of rugged, mountainous terrain at the head of the Treaty Creek Glacier. Elevations vary from approximately 1500 m to 2175 m. Vegetation in the area is limited to low-lying shrubs, mountain grasses and heather.

A nunatak exposed at high elevation along the eastern flank of the Treaty Glacier, covered variously by the TR 5, 8, 9 and 10 claims, constitutes the area of predominant interest on the TR property. Approximately 3,000 m long and averaging about 500 m wide, the nunatak features moderate to steep slopes with contours paralleling its northeast axis. Topography and orthophoto relative to claim lines are reproduced in this report as Figure 4. Ablation occurring prior to the date of the airphoto on which Fig. 4 is based has extended the real boundaries of the nunatak. For this reason, some of the geochemical lines put in during the 1988 work program appear to be overlying ice -- they are not.

Maximum rock exposure occurs where retreat of permanent snow and icefields has has been most pronounced. These exposures are interspersed with areas covered by glacial debris, talus and moraine. Although slopes are steep, most of the exposed areas can be accessed by foot without the help of mountaineering equipment.

Climate is severe, particularly at higher elevations. Heavy snowfalls in winter and rain in the short summer working season are typical of the Stewart area. Inclement weather conditions and reliance on helicopter transport make this a high cost area to explore for minerals.

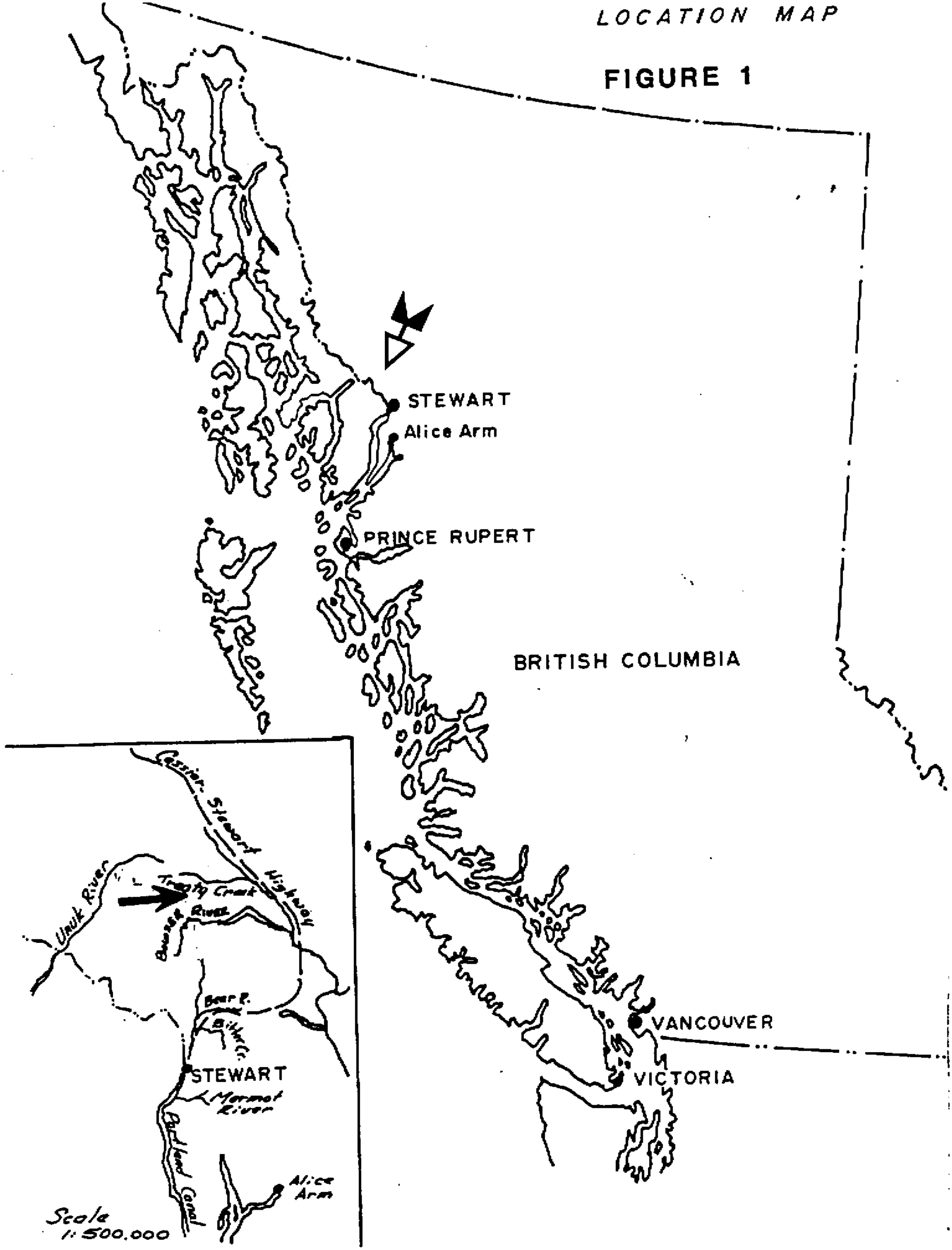
B. Status of Property

Relevant claim information is summarized below:

Name	Record No.	No. of Units	Anniversary Date
TR 5	4961(9)	20	Sept. 30, 1987
TR 8	4964(9)	8	Sept. 30, 1987

LOCATION MAP

FIGURE 1



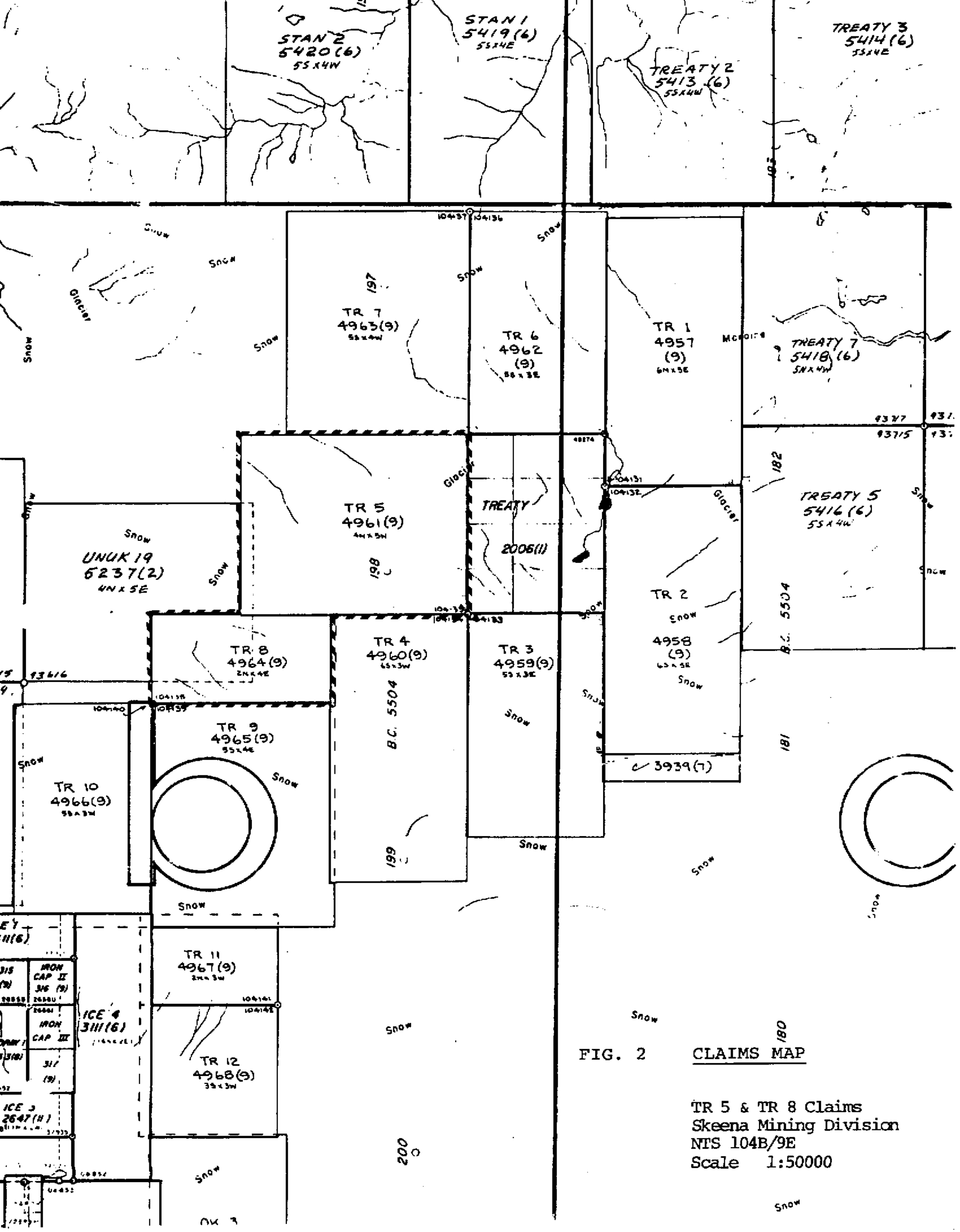


FIG. 2 CLAIMS MAP

TR 5 & TR 8 Claims
Skeena Mining Division
NTS 104B/9E
Scale 1:50000

Claim locations are shown on Fig. 2 after government N.T.S. map 104B/9E. The TR 5 claim belongs to the North Group, the TR 8 claim to the South Group. The claims are owned by Teuton Resources Corp. of Vancouver, British Columbia.

C. History

Two, brief isolated accounts in the B.C. Department of Mines Annual Reports mention that the Consolidated Mining and Smelting Company of Canada Ltd. (now Cominco) explored a large mineralized zone, parts of which are now covered by the TR 5 claim, during 1929 and 1930. Although Consolidated located 57 surveyed Crown-grant mineral claims in the area, exploration ended abruptly in 1931 and the claims were abandoned. Results of their exploration efforts were not published.

It is also reported that several prospecting syndicates explored the general Treaty Creek area during the 1950's (Ref. 1). In 1953, prospectors Charles Knipple and Tim Williams reported a small silver sulfide vein south of the Treaty Claim. Large boulders of tetrahedrite were also reported on the ice surface (source remains unlocated). Further work in 1967 ostensibly located a significant magnetic anomaly at the junction of Treaty Creek and South Treaty Glaciers. This, and further work in the area was concentrated on the highly visible alteration zones to the north and east of the TR 5 & 8 claims (these zones are covered by other claims in the TR series).

Prior to 1987, very little work, if any, had been carried out on the relatively isolated nunatak controlled by the TR 5 and 8 claims. Then, a small prospecting effort mounted late during the season led to the an unexpected discovery--native gold associated with skarn-like rocks just up from the ice edge on the eastern edge of the nunatak. This zone was dubbed the "Konkin" after its discoverer. At the instance of the exploration contractor a diamond drill was moved in to test the zone. Results of this work are contained in an assessment report filed with the B.C. Ministry of Mines and Energy Resources (Ref. 10).

The 1988 program was designed as a larger scale follow-up to the results obtained in 1987.

D. References

1. GROVE, E.W., P.ENG., PH.D. (1983): Private Report for Teuton Resources Corp. on the Treaty Claim.

2. GROVE, E.W. (1982): Unuk River, Salmon River, Anyox Map Areas. Ministry of Energy, Mines and Petroleum Resources, B.C.

3. GROVE, E.W. (1971): Bulletin 58, Geology and Mineral Deposits of the Stewart Area. B.C.M.E.M.P.R.

4. ANNUAL REPORTS, MINISTER OF MINES, B.C.:
1929 -- p. C102; 1930 -- p. A110.

5. BRITISH COLUMBIA MINER (1928): "Portland Canal Notes" by W.R. Hull, p. 36, December 1, 1928.

6. KRUCHKOWSKI, E.R. (1981): Geological Report Treaty Claim -- Bowser-Unuk Project, NTS 104B/9E, for E & B Explorations Ltd.

7. CREMONESE, P.ENG. (1984): Assessment Report on Prospecting Work on the Electrum 1 and Electrum 6 Claims, NTS 104B/9E, On File with the B.C.M.E.M.P.R.

8. CREMONESE, P.ENG. (1985): Assessment Report on Geological and Geochemical Work on the Treaty Claim, NTS 104B/9E, On File with the B.C.M.E.M.P.R.

9. CREMONESE, P.ENG. (Feb., 1987): Assessment Report on Geochemical Work on the Treaty & TR 2 claims, NTS 104B/9E, On File with the B.C.M.E.M.P.R.

10. CREMONESE, P.ENG. (Dec., 1988): Assessment Report on Diamond Drilling, Geological and Geochemical Work on the TR 4, 5 & TR 8 claims, NTS 104B/9E, On File with the B.C.M.E.M.P.R.

11. OSTENSOE, ERIK A. (Feb., 1984): Report on the Gold Wedge Property, Sulphurets Creek Area. Private report for Catear Resources Ltd.

12. TRIBE, N.L., P.ENG. (Apr., 1986): Progress Report 1985 Field Season, Sulphurets Property. Report in Statement of Material Facts filed on behalf of Newhawk Gold Mines Ltd.

13. WALUS, A. (Oct., 1988): Field Report and Maps on 1988 Treaty Creek Project for Teuton Resources Corp.

14. FIELDNOTES/FIELDMAPS (June-Sept. 1988): Sundry material collected by field personnel during 1988 Treaty Creek Project for Teuton Resources Corp.

15. SAYER, C., P. GEOL. (Sept., 1988): Drill Recommendations - TR 5 and TR 8 Claims; Private Report for Teuton Resources.

16. STANLEY, CLIFFORD R. (1987): PROBPLOT--An Interactive Computer Program to Fit Mixtures of Normal (or Log Normal) Distributions with Maximum Likelihood Optimization Procedures; Instruction Manual -- Association of Exploration

Geochemists, Special Volume 14.

E. Summary of Work Done.

On June 11, 1988 the author flew into the TR property by helicopter to assess snow conditions, select potential campsites and, if feasible, chart a route up the Treaty Glacier for a Bombardier or similar piece of equipment. During this visit it was noted that the main showings discovered on the TR 5 and 8 claims the previous year were largely free of snow.

Merl Cloutier, blaster, and an assistant left Vancouver for the property in late June with instructions to set up a camp near the "Konkin" showing and begin a trenching program. Thereafter two additional workers, both well-experienced with blasting and trenching, were flown in. One of these, Tom Kennedy, was put in charge of field operations. Subsequently, Alex Walus, geologist, and Eric MacKenzie (field hand experienced in operation of geophysical equipment) joined the crew. Two additional assistants were later added to the work force. During this time, the author made several visits to the property to supervise activities. Geologists Chris Sayer and Paul MacGuigan also made visits during the 1988 program.

The primary thrust of the 1988 program was directed at blasting, trenching and sampling of mineralized zones exposed in the northeastern portion of the nunatak on the TR 5 and 8 claims. Twenty-six trenches were excavated totalling 275.5 meters in length. Of this 258.4 meters were sampled, generating 282 samples. Average trench width was about 0.6 meters, depth varying from 0.6 m to 1.2 m depending upon degree of surface weathering. In several places, especially the upper portions of the Konkin Zone, overburden made trenching to bedrock a tedious and time-consuming process.

The "Main Grid" was constructed covering most of the area in the northeastern end of the nunatak. Baseline spanned 600 meters with cross-lines every 50 meters [additional cross-lines were used in the magnetometer survey]. Several reconnaissance rock and soil geochem lines were also put in to the test areas northeast, east, and southwest of the main grid. A detail grid was emplaced in the northeastern portion of the main grid in order to follow-up some high gold geochemical values. Altogether 439 soil and 487 rock samples were taken. A further 11 reconaissance rock geochemical samples were taken.

An Omni "Tie-Line" Magnetomer System was used to take readings along 5,570 m of grid at 579 stations.

Geological mapping at a scale of 1:2000 was undertaken to cover most of the exposed area of the nunatak. The Main Grid area in the northeastern portion of the nunatak was done with as much accuracy as surface conditions allowed (extensive talus and overburden, some steep, inaccessible places). This area, shown in Fig. 5, encompassed roughly 280,000 sq. meters (800m by 350m, on average). The longer, southwestern portion of the nunatak was also mapped at 1:2000, but work here was of a preliminary nature as there was not enough time to establish a control grid. This latter area is roughly 200m wide by 1800m long, or about 360,000 sq. meters (see Fig. 6). Detailed mapping of the Konkin Gold Zone at 1:200 was also completed, covering an area estimated at 7,500 square meters. Similar detailed mapping of trenches outside the Konkin Zone was not initiated as planned due to time constraints.

It was originally anticipated that a diamond drilling program would close out the 1988 field program. A full drill camp, complete with cookshack, showers, and other requisites, was operational by the first week of September. The labour crew had also blasted out and levelled three large drill pads, dimensions 6 m by 6 m minimum. Sites for these drill pads, #s 1-3, are shown on Fig. 7 (#1 and #2) and Fig. 5 (#3).

Delays in finding a suitable drill contractor ultimately led to a decision to close down the project in mid-September. Another factor was the proximity of the end of the field season (large costs overruns were incurred due to adverse weather conditions in a small drill program carried out near the end of the previous year's field season). Crew and equipment were flown out of the property on Sept. 22, just prior to the onset of a severe storm. During the hasty demobilization, some of the field notes for the 1988 project were lost (or unwittingly left on site). These included geochemical sample descriptions for some of the samples taken on the TR 5 and 8 claims, as well as notes describing sample locations for minor work carried out on the adjacent TR 1, 2, 3, and Treaty claims. Estimated prorated costs for this latter work have been deducted from the total 1988 program costs.

For simplicity, work on the North and South Groups of the TR claims has been presented in the format of a single assessment report. Since the main work area overlapped the boundary of the two groups, costs have been prorated as shown at the end of the Work Cost Statement (Appendix I).

2. TECHNICAL DATA AND INTERPRETATION

A. Regional Geology

The property lies along the eastern edge of a broad, NNW trending belt of Triassic and Jurassic age volcanic and sedimentary rocks termed by Grove (1971) as the "Stewart Complex" [see Fig. 3]. This belt is bounded to the west by the Coast Crystalline Belt (mainly granodiorites) and to the east by a thick series of sedimentary rocks known as the Bowser assemblage (Middle Jurassic to Upper Jurassic age).

In the Sulphurets-Treaty Creek area, the lowermost formation consists of clastic rocks comprised of medium grained lapilli tuffs of andesite composition (Unuk River Formation). It is believed to be as much as 3,000 meters thick. Significantly most of the economic gold-silver deposits within the Stewart area are contained within rocks of the Unuk River Formation.

Lying unconformably above is the Betty Creek Formation, consisting of red and green volcanic sandstone, pillow lavas, conglomerate, and tuffs. The Betty Creek varies in thickness and may pinch out altogether.

Above the Betty Creek is the Salmon River Formation of marine siltstones, greywackes, conglomerates, minor limestone, and minor volcanic components.

This volcanic-sedimentary sequence is cut in several places by a variety of intrusive rocks varying from diorite to granite to syenite. The plutons are marked generally by distinct zones of pervasive pyrite-sericite alteration. Argillic assemblages containing alunite and native sulfur are also associated with certain prominent gossans in the Treaty Creek area.

Up to the present date the area has undergone exploration for porphyry copper-molybdenum deposits (Sulphurets property, Kerr property) and epithermal vein-type gold-silver deposits (Sulphurets property, Gold Wedge property). A recent discovery at Eskay Creek, just west of the area but in the same lithologies, has indicated a third potential target: massive sulfide deposits carrying significant values in precious metals. These are thought to occur near the base of the Salmon River Formation.

B. Property Geology/Mineralogy

a. Introduction

Geological mapping was carried out by A. Walus, holder of a Master's Degree in geology, specializing in petrography. Geology of the nunatak was mapped at a scale of 1:2000. In order to

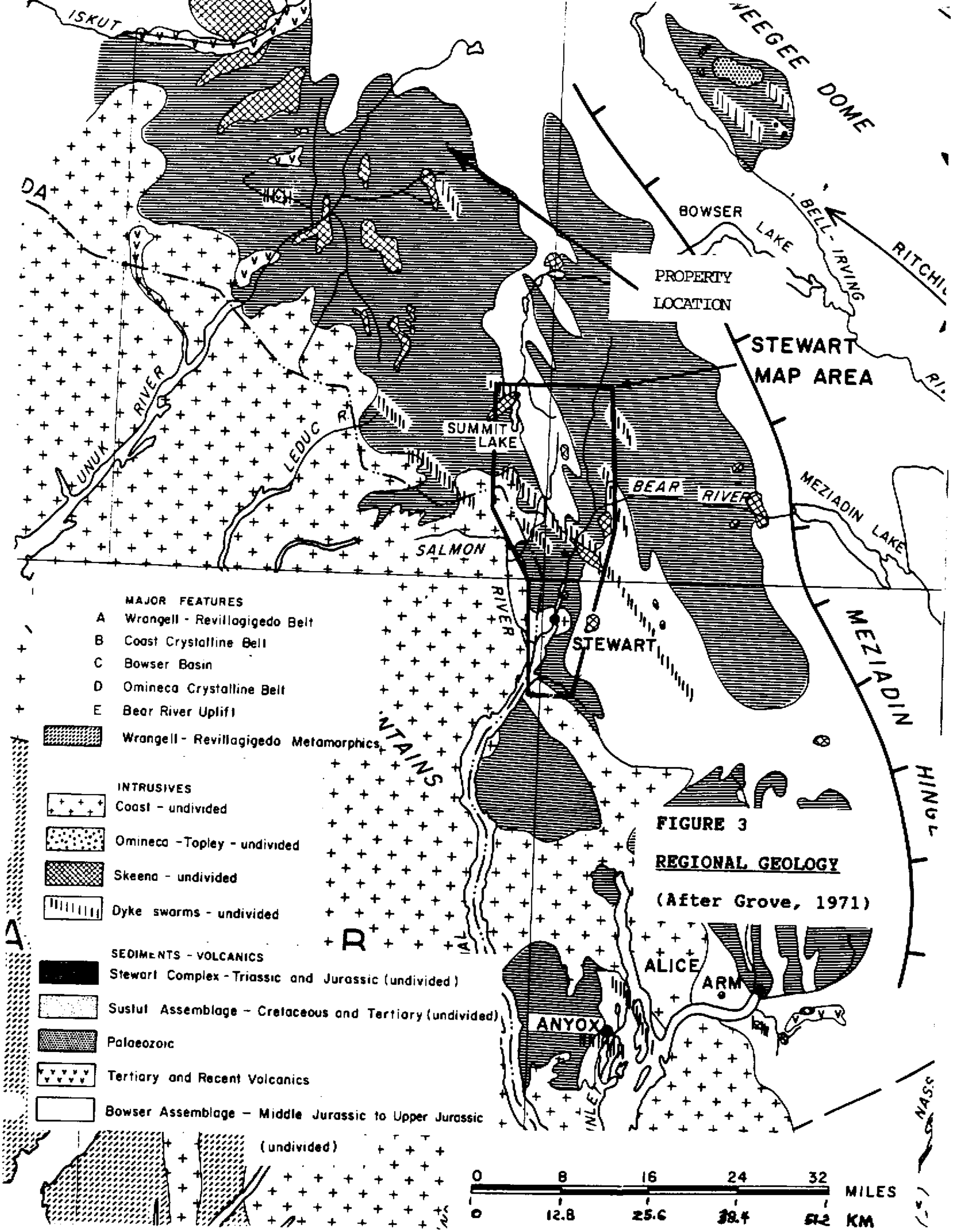


FIGURE 3

REGIONAL GEOLOGY

(After Grove, 1971)

facilitate representation, the nunatak was mapped in two parts. The northeastern portion is found in Fig. 5, entitled "Geological Map of the Nunatak (East)"; the southwestern portion is found in Fig. 6, entitled "Geological Map of the Nunatak (West)". The two maps overlap to a certain extent. Because a control grid was established over a large part of the Fig. 5 geology (East), work thereon can be considered much more accurate than its Fig. 6 (West) counterpart. During mapping, extensive overburden and talus cover necessitated approximation of geological contacts between rock outcrops in both sections of the nunatak.

A detailed map of the "Konkin" area has been drawn at a scale of 1:200: see Fig. 7, "Geological Map Konkin Gold Zone". It was originally planned to map in detail all of the areas trenched on the property. Unfortunately time constraints postponed this work to the following field season.

b. Geology/Mineralogy of Nunatak (East)--Fig. 5

Two distinct horizons are present: at the bottom, a sedimentary sequence consisting of alternating beds of limestone, massive, greenish siltstone trending occasionally into more pelitic rock (possibly a mudstone) and conglomerate (a small occurrence of fine-grained conglomerate was spotted at 350N 90W on the Main Grid, all substantially silicified with disseminated pyrite; above, a volcanic unit consisting of andesite lapilli tuff which in a few places passes into volcanic breccia and sometimes into flow breccia. The former is cut by dykes of diorite (lesser granite, hornblende-augite porphyry and minor rhyolite), the latter by dykes of aphanitic andesite. Due to strong cleavage the lapilli tuff is in many places transformed to semi-schists. It is believed that the units are overturned, the sedimentary sequence being the younger of the two.

Both sedimentary and volcanic units have been intruded by a variety of plutons. In the northeast corner of the nunatak, a heavily silicified diorite contains disseminated pyrite mineralization (3 to 5%) accompanied by low grade gold values. Because of the intensity of silicification, classification as a diorite is not certain--however, in places, the fabric of the plutonic rock has been preserved). Just north of the "Konkin" zone, a diorite intrusive is exposed in several small outcrops (its extent is probably larger than shown on Fig. 5: cf. Magnetometer Survey, Fig. 21). Two "skarn-like" bands are exposed naturally and by trenching in the Konkin zone, and are believed related to the diorite.

A long northeast trending zone of alteration straddles the volcanic-sedimentary contact in the "Goat Trail" area. It features strong sericite, silica, pyrite, limonite, clay, calcite, chlorite alterations with the proportions of constituents changing in broad range. It may or may not be related to a similiar, narrower zone in andesite lapilli tuffs about 200 m southwest. Linear, northerly trending zones of alteration are also present in the Konkin zone area.

The Goat Trail alteration zone exhibits a distinct form of gold mineralization as outlined by geochemical sampling. Gold values are accompanied by elevated levels of lead, zinc, silver, antimony, arsenic, and in the area proximate to the silicified diorite, copper. The lead-zinc-silver values are believed to be associated with minor galena and sphalerite, the antimony and arsenic values possibly with tetrahedrite. Gold values obtained in the alteration zone 200 m southwest, however, appear to be associated with arsenic only.

c. Geology/Mineralogy of the Nunatak (West) Fig. 6

This portion exhibits the same volcanic-sedimentary package as in the eastern portion of the nunatak. Lying above it is another volcanic-sedimentary sequence consisting of andesite crystal tuff, andesite, lapilli tuff, volcanic sandstone and, in large part, dark banded siltstone which may be built at least partly with volcanic material. In some places, the bands of siltstone are intercalated with thin layers of volcanic sandstone or even with andesite crystal tuff (with distinct laths of feldspar). The volcanic sandstone appears to be reworked andesite crystal tuff, since full gradation between the latter and andesite crystal tuff is present.

Rocks in this area have been cut by abundant steep faults running approximately NE-SW to N-S.

A linear alteration zone extending northeast from the southwestern edge of the nunatak has been traced for approximately 450 meters. Predominant alteration is quartz-sericite-pyrite. The alteration is not homogenous but is intermingled with rocks untouched by alteration. Large portions of the altered rocks are almost devoid of pyrite while some portions have pyrite concentrations up to 20-30%. Pyrite occurs as very fine to medium sized grains or in semi-massive form; it is either evenly distributed throughout the rock or comprises thin veins, lenses, or patches up to 10 cm in diameter. Throughout this zone there are numerous thin veins of quartz-calcite. Strong gold-arsenic geochemistry in this area, both from soil and rock samples, suggests a situation similar to that occurring at Catear's Goldwedge property approximately 8 km to the south.

Two other types of mineralization were noted in the area. Auriferous sphalerite and galena occur in gossanous outcrops in the central portion of geochemical Line MC (cf. samples TK004 and 005--Figs. 19-20). Float boulders containing galena in a quartz gangue were also discovered close to Station BC 6+25S on Line BC (cf. sample ENM Float #1--Figs. 19-20).

Two forms of intrusive are evident in the northeastern portion of the Fig. 6 area (in the area of overlap with Fig. 5). One is a diorite, the other, believed to be an altered granite. Dykes of diorite, and to a lesser extent, granite, were also observed. Some dykes of augite porphyry were noted as well as two dykes of rhyolite. [The dykes have not been mapped because of the preliminary nature of the work in this area].

d. Geology/Mineralogy Konkin Gold Zone - Fig. 7 (Indexed Fig. 5)

The Konkin Zone is generally an andesitic package of rocks bounded to the north by a dioritic intrusion. Two parallel skarn zones ranging from 12 to 20 m wide run approximately east-west. To the west they are covered by overburden and they extend about 30 m east where they are cut off by north trending faults. Within the andesite are also north trending zones of sericitic, limonitic, clay alteration which occur east of the skarns. These zones may be 3-8 m wide and run up to 50 m in length. Pyrite is also common in this type of alteration.

The skarn zones are mainly characterized by epidote alteration with local magnetite and calcite replacement. Sulfide mineralization is often up to 60% consisting of pyrite with auxiliary chalcopyrite. Other minerals observed in the skarn assemblage include chlorite, diopside, specular hematite, malachite, azurite, and limonite.

In one location known as the "Gold Pit" a local concentration of native gold occurs which can be seen with the unaided eye. The "Gold Pit" features quartz calcite veinlets in an extremely vuggy zone about 1.2 m by 3 m in area. Local structural features are complex--mechanism for the gold enrichment has not yet been ascertained.

Drilling done in 1987 tested the southernmost skarn band which hosts the Gold Pit. One of three holes intersected 5.5 ft grading 0.8 oz/ton near hole bottom. According to present understanding of structural relations, these holes were inadequately sited and probably only grazed the outer fringe of the southern skarn.

C. Trenching & Sampling

a. Introduction

Altogether 26 separate trenches were excavated during the 1988 program, totalling 275.5 linear meters from which 282 samples (plus one grab) were taken. Most of the samples taken were 1.0 m in length or a little less. The trenching program was confined to the northeastern end of the nunatak--trench and sample locations are shown on Fig. 8--with the greatest density of trenching taking place in the "Konkin" area. In general trenches were approximately 0.6 meters in width and from 0.6 to 1.2 meters deep, depending upon degree of weathering in the rock. Certain trenches, such as #'s 31 and 32, required extensive surface clearing of overburden.

Although the trenches run from #'s 1 to 33, there are no trenches for #'s 23 to 29 inclusive. These were sited but were not begun due to other work taking precedence.

Gold values in oz./ton are recorded on Fig. 9. In the Konkin area, it was observed that there was some correlation between copper values and gold values, hence it was decided to plot the former on Fig. 11. Likewise, in the Goat Trail area and vicinity, arsenic values appeared to be somewhat associated with gold--arsenic values in trench samples can be found in Fig. 10.

Individual trenched areas (Diags. 1 to 6, Figs. 9-11) are discussed below.

b. Diagram 1 - "Konkin"

The impetus for work in this area came from the discovery of the "Gold Pit" in 1987. It yielded grades up to 28.0 oz/ton Au over 1.2 meters as well as several bonanza specimens containing coarse gold. Two 1987 chip samples from an outcrop 30 meters north of the Gold Pit returned values better than 1.0 oz/ton each over an interval of 1.2 meters. Although much of the area was masked by glacial overburden, it was assumed from the sample results that the locus for the gold mineralization was a northerly trending structure.

Trenching through outcrop and overburden in 1988 has shown that the initial interpretation was in error. The Gold Pit mineralization is now thought to represent a locally intense concentration of gold values within a broad, easterly trending band of skarn-like rocks. A parallel band of similar rocks, also easterly striking, contains the second set of high gold values discovered in 1987.

The northern band was tested by Trenches 1, 4 and 32 (Trench 4 crossed only a partial width of the band). The following gold-bearing intervals (weighted averages) were uncovered by sampling:

Trench #	Interval Sample #s	Length m	Gold oz/ton
TR-1	5-19	15.0	0.220
TR-4	3-8	3.8	0.401
TR-32	2-18	17.0	0.061

Signficant copper values were also obtained in the northern band as follows:

Trench #	Interval Sample #s	Length m	Copper %
TR-1	6-8	3	0.18
TR-32	7-16	10	0.36

Continuity of the northern skarn band along strike is obscured in both directions by overburden. Present trenching defines a strike length of about 20 meters.

The southern band returned gold-bearing intervals in four trenches (#'s 9, 30, 31 and 33). Only the uppermost Trench, #31, can be said with certainty to have cut across the full width of the auriferous portion of the skarn; the others all have at least one end still in gold mineralization. Based on gold grades and geology of Trench #3, the southern skarn band does not extend much beyond the exposures in Trenches 9 and 33, however, continuity along strike to the southwest remains unresolved because of talus cover. Trench intervals for gold are as follows:

Trench #	Interval Sample #s	Length m	Gold oz/ton
TR-9	Ext.#2-9	10.1	0.098
TR-30	1-5	5.0	0.102
TR-31	7-8	2.0	0.145
TR-33	1-5	5.0	0.193

For copper:

Trench #	Interval Sample #s	Length m	Copper %
TR-30	4-7	4.0	1.01
TR-31	7-8	2.0	0.29

Although copper values are found within both bands, the correlation with gold values is only partial. The same might be said of tungsten: analysis of the ICP assay certificates shows that anomalous tungsten levels are associated with some, but not all of the better gold values.

c. Diagram 2

Trenches #'s 5, 6 & 7 explore a sericite-pyrite alteration zone in lapilli tuffs between the western ends of Lines 150N and 200N on the Main Grid. A chip sample returned 0.6 oz/ton over 2.0 m in this area in 1987.

Although values cannot be considered high-grade, the three trenches returned consistently anomalous levels in gold. The best interval occured at the northern end of Trench 7: 0.072 over 1.8 meters. Signficantly, all three trenches registered anomalous arsenic content: cf. Fig. 10.

Further trenching was planned at this site but was put off for safety reasons (dangerous loose rock directly above zone).

d. Diagram 3 - "Upper Goat Trail"

Four trenches were put in here to test the center of a very intense, northeasterly trending, broad band of pyrite-sericite alteration. The trenches, #'s 19-22 inclusive, expose highly altered lapilli tuffs close to the sedimentary contact.

Gold values obtained from sampling the trenches appear to define a roughly northerly trending structure (visual identification of structure was rendered difficult if not impossible by the pervasiveness of alteration, particularly in Trench 22). Best value was obtained in Trench 19, 0.56 oz/ton gold over 0.9 meters contained within a larger interval having a weighted average of 0.312 oz/ton gold over 1.9 m. This was accompanied by elevated values in arsenic, lead and antimony. Not surprisingly, these three elements are also present in anomalous levels in the multi-element soil geochemical anomaly defined by the Main Grid geochem survey (cf. Figs. 17, 15 and 18, respectively). An interval in Trench 20 (Sample #s 5-9, incl.) returned a weighted average of 0.076 oz/ton gold over 4.5 meters.

Lack of mineral content in Trench 21 suggests that this was put in a little off structure. Although gold values in Trench 22 are appreciably weaker than in Trenches 19 and 20, this may be due to leaching (workers reported they were unable to reach non-weathered material).

e. Diagram 4 - "Lower Goat Trail"

Trenches 10, 11 and 12 explore a sedimentary sequence of alternating beds of limestone, mudstone and conglomerate containing disseminated pyrite. Gold values range from background levels to sub-ore grade (i.e., 0.124 oz/ton over 0.9 meters, Trench 12) were obtained, with no definite association to rock structure. It is probable that the gold values represent leakage from a primary structure not too far distant. Associated arsenic values were not present, suggesting different mineralogy to that in the Upper Goat Trail area.

f. Diagram 5

This is an interesting site spanning the contact area between the northeasterly-trending alteration zone described previously in the "Upper Gold Trail" section and a large outcrop of heavily silicified diorite. Trench 18 is in the altered lapilli tuffs and registered gold values between 0.016 and 0.081 oz/ton from five samples; Trench 13 is in the silicified diorite (also containing disseminated pyrite) and returned values ranging from a low of 0.013 oz/ton gold to a high of 0.076 oz/ton gold.

The Diagram 5 area is statistically significant because of the ubiquitous nature of the anomalous gold values--note that trenching was done in two different directions. The main metal association is iron (pyrite), although several of the sample sites also contain weak to moderately anomalous levels of arsenic.

g. Diagram 6

Located in relatively unaltered lapilli tuffs near the eastern end of Line 600N, this area features four trenches put in somewhat at random to test pyritic outcrops. All trenches contained intervals with anomalous gold content, however Trench 15 had the best values: a 3.6 m interval returned a weighted average of 0.052 oz/ton gold. Whether this interval is related to any of the gold values reported in the other trenches is not known.

D. Geochemistry--Soils

a. Introduction

Geochemical soil samples were collected from the Main Grid (and follow-up "Detail Grid") areas, results from which are presented in Figs. 12 to 18. Two reconnaissance geochemical lines were also put in, results from which are presented in Figs. 19 to 20.

Samples from the Main Grid were collected at 20 m intervals along lines separated by 50 m. A follow-up detail grid was also emplaced from which samples were collected every 5 m along lines separated by 12.5 m. The detail grid is located in the north-eastern portion of the Main Grid. Sampling was precluded at certain sites by steepness, snow cover or rock outcrop.

Samples from reconnaissance lines "BC" and "MC" test the area southwest of the Main Grid and were taken every 25m.

b. Treatment of Data

Soil samples collected during the 1988 program were tested for gold content by atomic absorption methods; an additional 29 elements were analysed for using ICP. Results were recorded both in Assay Certificates (see Appendices) and on floppy disk.

Analytic results for elements gold, silver, copper, lead, zinc, arsenic and antimony were selected for statistical treatment based on distribution patterns. [Gold was the primary target of the exploration program; silver, copper, lead, zinc, arsenic and antimony were considered to be of importance primarily as pathfinders for gold.]

The data was run through the "Probplot" computer program (Ref. 16), an interactive computer program designed to fit mixtures of normal (or log-normal) distributions with maximum likelihood optimization procedures. Summary statistics and a histogram have been plotted for each of the seven elements noted above: see Appendix III. In general, these reveal log-normal distributions, typical of geochemical data. Probability plots have also been included in Appendix III.

Inflection points on most, if not all, of the probability plots indicate the presence of several populations. Attempts to break these out into separate populations using the complex software available on the Probplot program were not successful. It was not clear whether two, three or even four populations were represented by the data, and the separated populations often showed a considerable degree of overlap. In the end it was decided that, for the grid samples, simply contouring the data was the best method for analysing results. As for the reconnaissance soil lines, samples registering values in excess of mean + one standard deviation were emphasized by placing a small diamond beside the numerical value on Figs. 19-20; those in excess of the mean + two standard deviations were emphasized by a large diamond.

[Note: Classification of the sample population into conventional background, threshold and anomalous categories was rendered difficult by two factors. First, the population was skewed because a large proportion of the samples were "anomalous" anyway--for instance, soil samples registering in excess of 200 ppb gold generally have been considered worthy of follow-up in the Stewart area, yet the mean for the project soil samples was 303 ppb gold. This was a direct result of the concentration of the geochemical samples in the Main Grid area, close to known occurrences of gold mineralization. Second, it is now obvious from the combined results of the 1988 program that several different types of gold mineralization exist on the property. These different types are in all probability represented by different populations, further complicating matters].

c. Discussion of Results

c.1 -- Gold

Gold values for the Main Grid area are shown in Fig. 12; for the reconnaissance soil lines "BC" and "MC" in Fig. 19.

The Main Grid area has been contoured at the 700, 1100, 1500 and 2,000 ppb gold levels. A distinct anomaly is evident in the southeastern corner of the Main Grid, interepreted as being related to the "Konkin" area. Extension of the anomaly to the north-northeast is interpreted as either signalling an extension of the known Konkin mineralization or representing down-glacier contamination from the Konkin zone.

A unique feature of the "Konkin" soil gold anomaly is that it is associated with a distinct copper anomaly (and to a lesser extent a silver anomaly), however lead, zinc, arsenic and antimony appear only at background or slightly elevated levels.

The pronounced gold anomaly evident between Lines 350N and 600N, northeastern portion of the Main Grid, appears to be associated with a broad zone of pyrite-sericite alteration roughly coinciding with the volcanic-sedimentary contact. Unfortunately sampling density in the northeasternmost portion was limited due to steepness and extensive rock outcrop. The anomaly is about 100 m wide and has an inferred length of 250 m. It is open to the northeast and southeast.

A distinctive feature is a more or less overlapping, antimony anomaly. Throughout the rest of the main grid area antimony values are at background levels only. Coincident arsenic and lead-zinc-silver anomalies are also present. Copper is anomalous only in the northernmost portion.

Another gold anomaly occurs between Lines 50N and 150N at the western edge of the Main Grid. It is probably an expression of the structure hosting the gold mineralization trench sampled in Diag. 2, Fig. 9 (sericite schists). This anomaly shows a good correlation with an arsenic anomaly at the same site (cf. Fig.-17). Based on the arsenic/gold association, the gold anomaly between Stations 50W and 150W on Lines 0N and 50N is probably due to the same source.

The spot gold high of 1,435 ppb at Line 250N, Station 100W, is tentatively interepreted as having been caused by a glacial erratic.

Soil reconnaissance lines put in to test the southwestern portion of the nunatak disclosed broad areas of elevated gold values, particularly the southwestern portion of line "MC". While only those values in excess of 1390 ppb (mean + 1 standard deviation) have been specially marked on Fig. 19, it should be stated that the typical "rule-of-thumb" in the Stewart area has been to re-examine all soil values in excess of 200 ppb gold. Based on trials contouring the Main Grid area, a "cut-off" of 700 ppb is probably more appropriate for this part of the project area. [This higher value may be due to the fact the soils are more in the nature of talus fines than true soils. Since the southwestern portion of the nunatak will need follow-up grid geochemical sampling, it would be premature at this stage to rigidly define anomalous levels anyway.]

Twenty-seven of the samples collected along Lines BC and MC registered values in excess of 700 ppb gold. The best values occurred between Stations 9+50S and 10+25S on Line MC. These returned soil geochem values ranging between 1470 ppb and 2410 ppb in gold. The reading of 1705 ppb at Station 16+50S on line BC may represent a downhill continuation. Another high on Line MC occurs at 4+25S; it returned 1720 ppb gold, flanked by values of 1330 and 850 ppb on either side.

c.2 -- Silver

Silver values for the main grid are shown on Fig. 13. Contour levels are at 3, 4, 5 and 7 ppm.

As discussed in the preceding section on gold, overlapping silver anomalies mark both the Konkin and Goat Trail gold anomalies . The anomaly over the Konkin zone is less pronounced, reflecting the relatively low silver-gold ratios as defined in mineral samples taken from that area (many of the higher grade Konkin mineral samples have a higher gold content than silver content). The silver values in the Goat Trail area appear to be associated with lead-zinc values.

Another silver anomaly is evident between the Konkin and the Goat Trail anomaly. It's source is unknown but may be a downhill expression of the broader silver anomaly located due west. This latter anomaly appears to be related to an extensive, somewhat diffuse copper anomaly whose origin is speculated as being close to the ridge crest.

Other, smaller silver anomalies present on Fig. 13 are interpreted as associated with gold anomalies discussed in the section on gold.

c.3 -- Copper

Copper values for the main grid are shown on Fig. 14. Contour intervals are at 250, 325, 400 and 500 ppm.

The Konkin and Goat Trail copper anomalies have been discussed in section C.1 (Gold). Of most interest, is a broad, diffuse copper anomaly occupying much of the central portion of the Main Grid area. Values taper downhill to the east. Because the strongest values are at the top of the hill, at the western edge of the grid lines, the source for this anomaly is speculated as being outside the sampled area. Abundant copper-stained float (in volcanics) was found in talus scattered throughout the central portion of the anomaly.

c.4 -- Lead

Lead values for the Main Grid are shown on Fig. 15. Contour intervals are at 200, 300, 400 and 500 ppm.

A large lead anomaly overlaps the gold anomaly located in the Goat Trail area in the northeastern portion of the Main Grid. Values range to 807 ppm. Lead also shows a strong silver, zinc, antimony, and arsenic association.

Spot highs located in the southwestern portion of the Main Grid are not directly associated with other anomalies or known mineralization.

c.5 -- Zinc

Zinc values for the Main Grid are shown on Fig. 16. Contour intervals are at 300, 450, 600 and 800 ppm.

The same comments with respect to lead (section c.4) also apply to zinc.

c.6 -- Arsenic

Arsenic values for the Main Grid area are shown on Fig. 17; for the reconnaissance soil lines "BC" and "MC" on Fig. 20. [Arsenic was the only metal other than gold plotted on figures for the geochemical reconnaissance lines on the southwest portion of the nunatak; this was because it was the only metal exhibiting a strong gold correlation in this part of the project area].

Contour intervals for the Main Grid samples are at 500, 800, 1100 and 1500 ppm. The two arsenic anomalies evident on Fig. 17, one in the Goat Trail area, the other in the southwestern corner of the grid, have already been discussed in the section on gold.

Reconnaissance geochem lines "BC" and "MC" contain several sections showing highly elevated levels of arsenic. The most anomalous area occurs at the southwestern end of Line MC, with three sample sites registering values in excess of 2160 ppm (equal to mean + 2 standard deviations: marked by a large diamond). Highest value obtained was 5,389 ppm arsenic at MC 9+75S. Another "large diamond" occurs downhill on Line BC at 16+50S--3,103 ppm.

Values between 1230 and 2159 ppm have been marked on Fig. 17 as small diamonds. There are 27 of these samples--one prominent cluster occurs on Line MC between 3+25S and 4+25S inclusive. As stated in the previous section on gold, setting threshold values has been difficult because of the high background values inherent in the survey results. The same applies to the arsenic soil values obtained on the reconnaissance lines, particularly Line

MC. A closely spaced grid survey should be undertaken in this area in order to properly define anomalies.

c.7 -- Antimony

Antimony values for the Main Grid area are shown on Fig. 18. Contour intervals are at 6, 14, 25 and 40 ppm.

The only antimony anomaly occurs in the "Goat Trail" area and coincides with gold, silver, lead, zinc and arsenic anomalies occurring there as well.

E. Geochemistry - Rock

a. Introduction

Geochemical rock samples were collected from reconnaissance lines north and east of the Main Grid ("WC", "GTC" and "BC" Lines:) and also southwest of the Main Grid ("UC" Line). Gold values are shown on Fig. 19, arsenic values on Fig. 20.

Samples were collected every 10 m along the lines. Lines "WC", "GTC" and the northern portion of "BC" are straight lines; the southern portion of Line "BC" and all of "UC" are irregular lines following rock outcrop.

Eleven spot rock geochemical samples were taken in the southwestern corner of the nunatak. These are termed NG-1 to NG-7, TK-004 to TK-006, and ENM Float #1.

Unfortunately rock geochemical sample descriptions were either inadvertently left at camp or lost during demobilization. Where possible brief descriptions are given from memory or by reference to geological mapping.

b. Treatment of Data

Rock samples collected during the 1988 program were tested for gold content by atomic absorption methods; an additional 29 elements were analysed for using ICP. Results were recorded both in Assay Certificates (see Appendices) and on floppy disk.

Analytic results for elements gold and arsenic were selected for statistical treatment based on distribution patterns. Data was run through the "Probplot" computer program (Ref. 16), an interactive computer program designed to fit mixtures of normal (or log-normal) distributions with maximum likelihood optimization procedures. Summary statistics and a histogram have been plotted for each of the seven elements noted above: see Appendix III. Both gold and silver show approximate log-normal distributions. Probability plots featuring several inflection points for both gold and arsenic (suggestive of several different populations) have also been included in Appendix III.

Difficulty in separating populations has precluded simple classification of anomalous or non-anomalous levels. The same reasons as stated in the section on soil geochemistry apply here as well. Since contouring was not available as an alternative method (non-grid samples), it was decided merely to emphasize those samples lying greater than one standard deviation from the mean (represented on the Figures as a small diamond), as well as those samples greater than two standard deviations from the mean (represented on the Figures as a large diamond).

Gold values are to be found on Fig. 19; values for the most important pathfinder element, arsenic, on Fig. 20.

c. Discussion of Results

c.1 -- Gold

The mean value for gold content in rock geochemical samples taken during the 1988 survey was 76 ppb. Mean plus 1 standard deviation equalled 730 ppb (rounded), and mean plus 2 standard deviations 1380 ppb.

Most anomalous rock geochem line was the southern portion of Line BC (Diag. 3; Fig. 19). From 23 samples taken along 220 m, values ranged between a low of 141 ppb to a high of 6465 ppb. Arithmetic average was 800 ppb (0.023 oz/ton), very anomalous considering the length of the interval. As located, this line would be within the unit termed "heavily silicified diorite" on Fig. 5 (Geological Map of the Nunatak {East}). Gold values obtained correspond in general with values from Trench 13, also in the same unit but some 80 m to the west.

The northern portion of Line BC (Diag. 2; Fig. 19) is also in the heavily silicified diorite but gold values are not as strong. Apart from the 1660 ppb sample at 2+70N, values are below the arithmetic mean for the southern part of Line BC. Similarily Line WGC, uphill to the northwest (also Diag. 2; Fig. 19) and situated in andesite lapilli tuffs, recorded some anomalous gold values but background gold values are not particularly high. Values of 3575 and 1635 ppb gold registered at GTC 0+30N and GTC 0+40N, respectively, should be investigated; ditto for the highs at GTC 1+90N and 2+10N. Uphill again to Line WC, in andesite lapilli tuff, gold values attenuate sharply. Best value was 790 ppb at WC 1+10N.

Turning to the southwestern portion of the nunatak, Line UC showed a cluster of anomalous gold samples at UC 4+70S (985 ppb), 4+80S (1025 ppb) and UC 5+00S (2215 ppb). According to Fig. 6 (Geological Map of the Nunatak {West}), these samples were taken from a sedimentary sequence of alternating beds of limestone, siltstone, mudstone and conglomerate. Two other isolated highs occur: at UC 1+60S (6255 ppb) in dioritic rock; and at UC 8+70S (1480 ppb) in the sedimentary sequence.

Perhaps the most interesting of the rock geochemical samples are those in the "NG" series, taken at random from the strong linear alteration zone in lapilli tuffs at the extreme southwest corner of the nunatak. A distinctive feature of the alteration zone is the abundance of quartz-calcite veining or stockworks. Seven samples ranged from 211 to 1725 ppb in gold, with an arithmetic mean of 1100 ppb.

TK 004 returned 5177 ppb in gold and was a sample of gossanous outcrop in volcanic rocks containing pyrite and a mineral believed to be sphalerite. TK 005 returned 6891 ppb in gold from a similar gossanous outcrop and featured pyrite, sphalerite and minor copper stain. TK006 was a pyritized float sample of andesite lapilli tuff which returned a value of 857 ppb in gold. Sample ENM Float #1 was selected from an area of abundant float boulders containing galena and sphalerite in a quartz gangue. Source remains unknown. This sample returned a value of 925 ppb gold and 158.4 ppm silver.

c.2--Arsenic

The mean value for gold content in rock geochemical samples taken during the 1988 survey was 88 ppb. Mean plus 1 standard deviation equalled 450 ppb (rounded), and mean plus 2 standard deviations 780 ppb.

The lack of high arsenic values in both the southern and northern portions of Line BC (Diags. 2 & 3, Fig. 20) indicates that gold values in the silicified diorite probably are not associated with arsenic. By contrast, elevated arsenic values occur in Lines GTC in approximate spatial correlation to the high gold values. This suggests that the form of gold mineralization occurring in the lapilli tuffs is arsenic related (as borne out by trenching in lapilli tuffs in the southwestern portion of the Main Grid area (Trenches 5, 6 & 7). The slightly elevated arsenic values registered at the beginning of Line UC are probably a continuation of this last mentioned area. At UC 8+70S, an arsenic value of 1,641 ppm corresponds well with a gold high of 1,480 ppb.

In the southwestern corner of the nunatak, arsenic values show a very strong correlation with gold in the "NG" series. The seven NG samples range from 417 to 1360 ppm arsenic with an arithmetic mean of 868 ppm. The NG samples are in an alteration zone in lapilli tuffs.

Arsenic highs were also obtained in samples TK005 and 006: 1344 and 854 ppm, respectively. Lesser values of 524 and

482 ppm were obtained from samples TKO-06 and ENM Float #1.

F. Geochemistry--Field Procedure and Laboratory Technique

Soil samples were taken from 20 to 30 cm below surface by digging with a prospectors pick. Soil development in this alpine-type area can be characterized as very immature--the sampled horizon, accordingly, does not fit readily into conventional classifications. The more proper classification, perhaps, would be to term the samples "talus fines". In any event, care was taken to ensure that all of the samples were taken from the same horizon/material to ensure a proper statistical distribution. The range of values exhibited in the data, and the good correlation of geochemical anomalies with known surface mineral showings, indicates that the material sampled was a good medium for geochemical study.

After sampling, soils were placed into a standard kraft bag, labelled, and allowed to dry before being shipped from the property. Rock geochemical samples were taken by chipping with a prospector's pick. These were also placed in a standard kraft bag, labelled, and allowed to dry before being shipped from the property.

Gold analyses were carried out either by standard fire-assay techniques (one-half assay ton), or by Atomic Absorption, by Acme Analytical Laboratories of Vancouver. In the latter case, 10 gm sub-samples were subjected to standard fire assay preconcentration techniques to produce silver beads which were then dissolved in reagent prior to determination of gold content by AA.

All samples were also tested using the 30-element Inductively Coupled Argon Plasma analysis. Preparation consisted of digesting representative 0.5 gm sub-samples with 3 ml of 3-1-2 HCl-HNO3-H2O at 95 deg. C. for one hour, followed by dilution to 10 ml with water.

G. Geophysics

It was originally anticipated that the auriferous "skarn" mineralization in the Konkin area could be traced under glacial debris and talus by utilizing a magnetometer survey. This supposition arose from the observation that magnetite was also included in the skarn minerals. Although it turned out that the mag survey was useful in delineating the intrusive proximate to the skarn, it did not pick up the skarn mineralization per se.

A magnetomer system was rented from Ashworth Explorations Limited. It was comprised of two magnetometers, both model Omni IV "Tie-Line", one with total field capability and the other with total field and base station capabilities. Each had 48K Ram Memory, a Remote Total Field Sensor, a pole assembly (four, 0.6 meter sections) and a rechargeable battery cartridge with battery charger.

Readings were taken in the field by Eric MacKenzie, an operator with lengthy experience in exploration, in general, and geopohysical surveys, in particular. Readings were recorded electronically and stored on a disk. Data was thereafter fed into a computer and plotted. Base mag was 56,000 gammas.

Results of the mag survey over the Main Grid area have been contoured on Fig. 21 (Magnetometer Survey) at 100 gamma intervals. Where possible, line spacing was reduced to 25 m, with stations taken every 10 m along lines (as compared to the geochemical survey which saw 50 m line spacings, and 20 m sample intervals).

The contouring defines a magnetic anomaly trending roughly southwest and corresponding to the diorite intrusive mapped just north of the Konkin zone. The anomaly is open to the southwest and northeast. Extension of the anomaly to Line 50S suggests that the "Konkin" diorite is probably larger than mapped (Fig. 5) and may even join with the diorite outcropping near the beginning of Rock Geochem Line "UC" (see Fig. 5). Heavy talus cover between these two points makes confirmation of this supposition difficult.

H. Conclusions

Results from the combined geochemical and trench sampling programs have defined a number of forms of gold mineralization on the TR 5 and 8 claims. Each of these zones appears to have a unique character according to its host.

In the andesite lapilli tuffs, gold values are accompanied universally by arsenic mineralization with the exception of the Konkin Gold Zone area. The arsenic-gold association is most prevalent at the southwestern end of the nunatak, a site as yet only lightly explored but which holds particular promise because of the observed presence of abundant quartz-calcite veining or stockworks in a linear pyrite-sericite alteration zone. The situation here appears quite similar to the high-level epithermal Au-As mineralization presently being exploited at the Gold Wedge property by Catear Resources Inc. to the south. Within the southwestern portion of the Main Grid, Au-As mineralization was also discovered by trenching in altered sericite schists. Preliminary indications are that the gold mineralization is not as strong as at the southwestern end of the nunatak, possibly due to lack of stockwork veining. The "Goat Trail" area also shows an arsenic-gold association, but the suspicion is that the situation here is different from the two areas just discussed. The gold anomaly in the Goat Trail area is also overlapped by coincident antimony-lead-zinc-silver anomalies, suggesting a different mineral assemblage. Intensity and width of the gold anomaly in the Goat Trail area suggest that this is a prime exploration target. During the 1988 program, Drill Pad #3 was erected on a small knoll uphill from Upper Goat Trail trenches: upon completion of further rock sampling, this pad should prove an ideal spot to test down-dip extensions of auriferous mineralization in the area. Such further sampling should be carried out systematically along the steep gossanous slopes by experienced mountaineering geologists.

Gold mineralization in the Konkin Gold area has a different flavor. Although within an andesite package, the gold occurs in skarn-like rocks (whether or not it is a true skarn is still a matter for academic controversy). Mineral associations are not definite: massive pyrite bands, epidote, chalcopyrite, calcite veining and an unknown tungsten mineral are known to accompany some of the higher gold values but none of the above can be correlated completely with all of the strong gold values. Further work in this area is probably now confined to diamond drilling because of the depth of overburden southwest along putative strike of the skarn bands. Two drill pads have already been located to probe depth extensions of the present skarn exposures.

Preliminary trenching and rock geochemical sampling of rocks within the silicified diorite outcropping in the northeastern portion of the nunatak has identified widespread low-grade gold values. Further work should be undertaken to determine whether these represent a halo around a higher-grade structure of potential economic importance.

It is recommended that a control grid be established to cover the area southwest of the Main Grid to the southwestern edge of the nunatak. Rock and soil geochemical sampling, geological mapping and follow-up trenching should be carried out in this area. Favourable sites such as the linear alteration zone at the southwestern tip of the nunatak, the TK004 and TK005 areas, etc. should be carefully prospected. Float boulders, such as from the ENM Float #1 Sample area, should be carefully followed to source.

Respectfully submitted,

D. Cremonese

D. Cremonese, P.Eng.
December 28, 1988

APPENDIX I -- WORK COST STATEMENT

FIELD PERSONNEL (June to Sept., 1988):

Merl Cloutier, Blaster --June 25-July 28; --Aug. 15-Sept. 3; 53 days @ $267/day	$ 14,150
Tom Kennedy, Foreman -- July 7 - Aug. 31; 56 days @ $185/day	10,360
Ken Gourley, Assistant -- July 7 - Aug. 31; -- Sept. 15 -27; 69 days @ $150/day	10,350
Alex Walus, Geologist -- Aug. 8 - Sept. 16; 40 days @ $150/day	6,000
Eric MacKenzie, Assistant -- Aug. 8 - Sept. 16; 40 days @ $150/day	6,000
Mike Harris, Assistant -- Aug. 15 - Sept. 4; 21 days @ $125/day	2,625
Ken Hopkins, Assistant -- Aug. 27 - Sept. 22; 27 days @ $110/day	2,970
Chris Sayer, Geologist -- Aug. 25 - Sept. 2; 7.5 days @ $285/day	2,138

SUPERVISION/ENGINEERING

D. Cremonese, P.Eng. 22 days @ $300/day	6,600
Paul MacGuigan, Senior Geologist 2 days @ $400/day	800

HELICOPTER [Vancouver Island Helicopters]

Base cost for machine:	40.5 hrs @ $520/hr.	21,060
Fuel (Stewart base):	22.2 hrs @ $78.50/hr.	1,743
Fuel (Tide Lake strip):	15.3 hrs @ $87/hr.	1,331
Fuel (Bob Quinn):	3.0 hrs @ $114.50/hr.	343

FOOD -- Bob's Mercantile, Stewart, B.C. 6,564

SUPPLIES & EQUIPMENT

Plywood and 2 by 4s for tent frames, camp	3,137
General supplies: including powder, fuses, B-line, first aid, camp equipment, water line, diesel,	

kerosene, sample bags, tools, etc.	7,920
Rental of full field camp (five tents), generator, radio, water heaters, diesel heaters, etc.	
90 days @ $75/day	6,750
Rental of pluggers, drill sharpener, trenching tools	
90 days @ $40/day	3,600
Rental of "Omni" Tie-Line Magnetomer (Ashworth Ex.)	
9 days @ $185/day	1,665
Orthophotos and digitized topos: Eagle Maps	8,040

ASSAYS -- Acme Analytical

Fire assay for gold, 1/2 assay ton	
189 @ $8.50/sample	1,607
Geochem for gold (AA)	
748 @ $4.50/sample	3,366
30 element ICP	
937 @ $6.25/sample	5,856
Rock sample preparation	
498 @ $3.00/sample	1,494
Soil sample preparation	
439 @ $0.85/sample	373

TRANSPORTATION/ACCOMMODATION/SUPPORT COSTS

Personnel travel costs: Vancouver-Stewart-Van.	8,402
Transport equipment and supplies	340
Accommodation - Stewart (four months)	1,200
Expediting: Limar Industries & H. Foerster	2,498
Field Radio -- B.C. Tel charges	687

REPORT COSTS

Report and map preparation, compilation and research	
D. Cremonese, P.Eng., 6 days @ $300/day	1,800
Computer Draughting -- RPM	2,400
Word Processor - 8 hrs. @ $25/hr.	200
Map prints and material	160
Report copies, jackets, etc.	25

GRAND TOTAL.......... <u>$154,555</u>

Allocation:	TR 5 claim [North Group] 75 % =	$115,916
	Work filed [North Group-TR 5 Claim]	($ 75,000)
	Surplus	40,916
	TR 8 claim [South Group] 20 % =	$ 30,911
	Work filed [South Group-TR 8 Claim]	($ 12,700)
	Surplus	18,211

Allocation (Continued from Previous Page)

Work on neighbouring TR claims* 5% = $ 7,728
Work was not filed .....

*This work was of a minor nature, consisting of one reconnaissance geochemical soil line and some reconnaissance rock samples. Work would have been included in report but sample location notes were either lost or inadvertently left on site.

APPENDIX II - CERTIFICATE

I, Dino M. Cremonese, do hereby certify that:

1. I am a mineral property consultant with an office at Suite 200-675 W. Hastings, Vancouver, B.C.

2. I am a graduate of the University of British Columbia (B.A.Sc. in metallurgical engineering, 1972, and L.L.B., 1979).

3. I am a Professional Engineer registered with the Association of Professional Engineers of the Province of British Columbia as a resident member, #13876.

4. I have practiced my profession since 1979.

5. This report is based upon work carried out on the TR 5 and 8 mineral claims, Skeena Mining Division from June to September of 1988. I am satisfied that trench, rock and soil geochemical samples were taken properly and with care, and that geophysical readings were taken properly and with care, all by qualified personnel. Reference to field notes and maps made by geologist Alex Walus is acknowledged.

6. I am a principal of Teuton Resources Corp., owner of the TR 5 and 8 claims: this report was prepared solely for satisfying assessment work requirements in accordance with government regulations.

Dated at Vancouver, B.C. this 28th day of December, 1988.

D. Cremonese, P.Eng.

APPENDIX III

"PROBPLOT" SUMMARY STATISTICS

AND

PROBABILITY PLOTS

1988 GEOCHEMICAL DATA

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = AU Unit = PPM N = 443

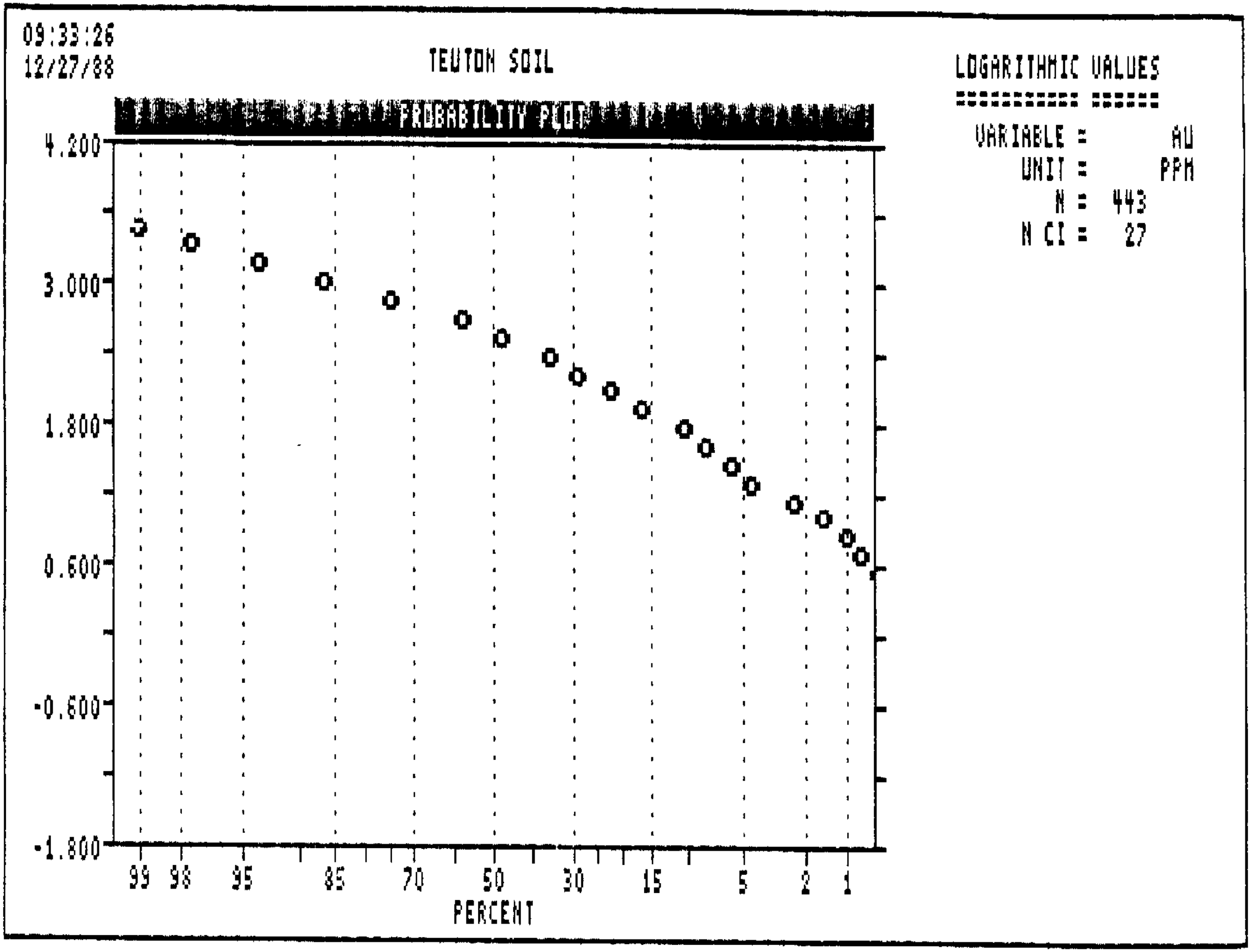
Mean =	2.4824	Min =	0.0000	1st Quartile =	2.1621
Std. Dev. =	0.5525	Max =	4.0152	Median =	2.5855
CV % =	22.2561	Skewness =	-0.9118	3rd Quartile =	2.8588

Anti-Log Mean = 303.688 Anti-Log Std. Dev. : (-) 85.101
(+) 1083.726

%	cum %	antilog	cls int	(# of bins = 27 - bin size = 0.1544)
0.00	0.11	0.837	-0.0772	
0.23	0.34	1.195	0.0772	
0.00	0.34	1.705	0.2316	
0.00	0.34	2.433	0.3861	
0.23	0.56	3.471	0.5405	
0.23	0.79	4.954	0.6949	
0.23	1.01	7.069	0.8494	
0.45	1.46	10.088	1.0038	*
0.90	2.36	14.395	1.1582	**
2.03	4.39	20.542	1.3126	****
1.35	5.74	29.314	1.4671	***
2.26	8.00	41.831	1.6215	****
2.26	10.25	59.694	1.7759	****
6.09	16.33	85.185	1.9304	************
5.42	21.73	121.560	2.0848	***********
6.77	28.49	173.468	2.2392	*************
6.77	35.25	247.541	2.3936	*************
12.19	47.41	353.245	2.5481	************************
10.38	57.77	504.086	2.7025	*********************
17.16	74.89	719.339	2.8569	**********************************
11.96	86.82	1026.509	3.0114	************************
7.00	93.81	1464.844	3.1658	**************
3.84	97.64	2090.356	3.3202	********
1.35	98.99	2982.972	3.4746	***
0.68	99.66	4256.748	3.6291	*
0.00	99.66	6074.448	3.7835	
0.00	99.66	8668.335	3.9379	
0.23	99.89	12369.853	4.0924	
				0 1 2 3 4

Each "*" represents approximately 2.2 observations.

##


09:33:26
12/27/88
TEUTON SOIL
PROBABILITY PLOT
LOGARITHMIC VALUES
VARIABLE = AU
UNIT = PPM
N = 443
N CI = 27
4.200
3.000
1.800
0.600
-0.600
-1.800
99 98 95 85 70 50 30 15 5 2 1
PERCENT

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = AG Unit = PPM N = 443

Mean =	0.2679	Min =	-1.0000	1st Quartile =	0.0414
Std. Dev. =	0.3511	Max =	1.3729	Median =	0.3010
CV % =	131.0478	Skewness =	-0.5673	3rd Quartile =	0.5051

Anti-Log Mean = 1.853 Anti-Log Std. Dev. : (-) 0.826
(+) 4.159

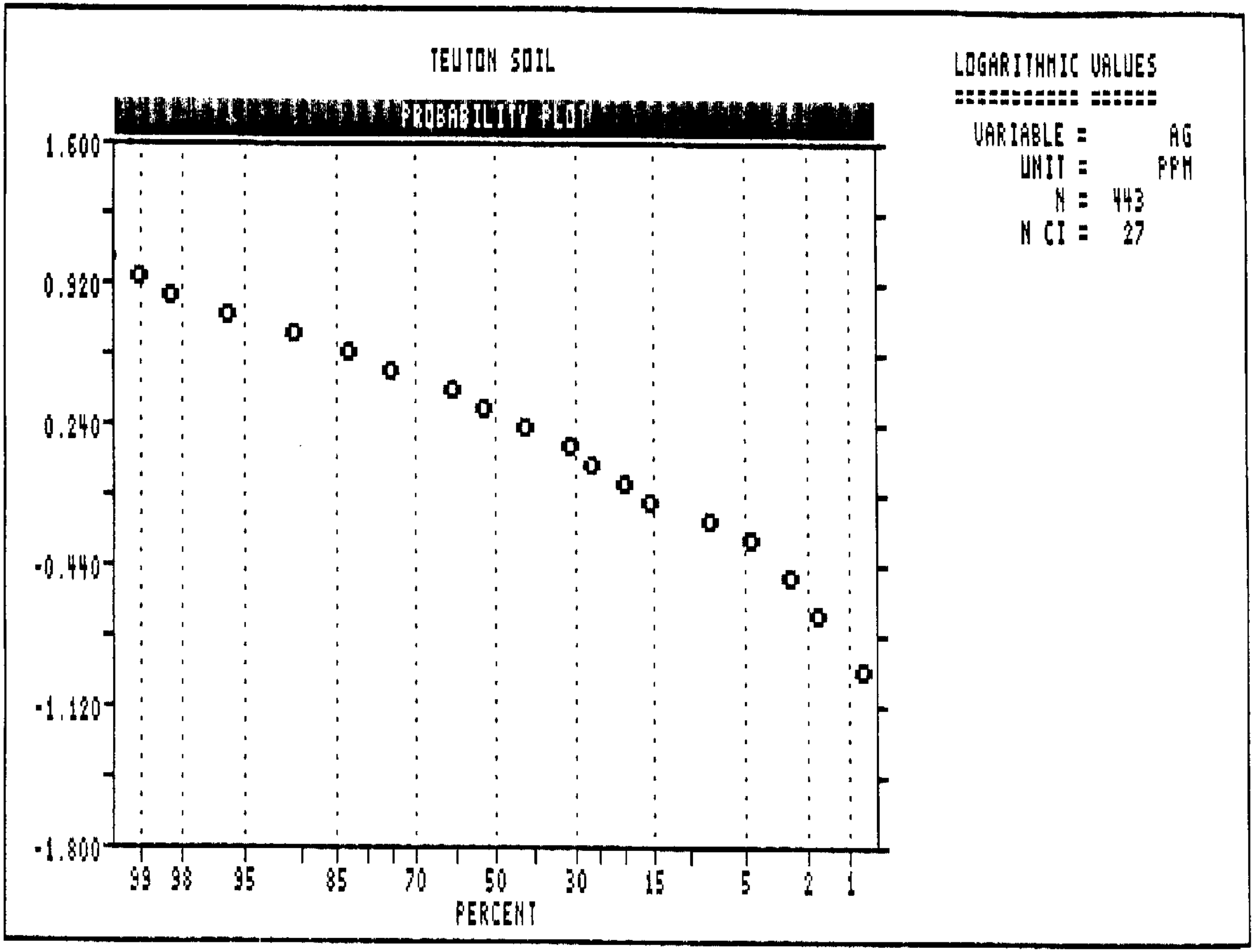
==

%	cum %	antilog	cls int	(# of bins = 27 - bin size = 0.0913)
0.00	0.11	0.090	-1.0456	
0.68	0.79	0.111	-0.9544	*
0.00	0.79	0.137	-0.8631	
0.00	0.79	0.169	-0.7718	
0.90	1.69	0.209	-0.6806	**
0.00	1.69	0.257	-0.5893	
0.90	2.59	0.318	-0.4980	**
0.00	2.59	0.392	-0.4068	
2.03	4.62	0.484	-0.3155	****
3.16	7.77	0.597	-0.2242	******
7.45	15.20	0.736	-0.1330	***************
4.29	19.48	0.908	-0.0417	********
6.77	26.24	1.121	0.0496	*************
4.51	30.74	1.383	0.1408	*********
11.29	42.00	1.706	0.2321	**********************
10.61	52.59	2.105	0.3234	*********************
8.13	60.70	2.598	0.4146	****************
14.45	75.11	3.205	0.5059	*****************************
7.90	83.00	3.955	0.5972	****************
7.67	90.65	4.880	0.6884	***************
5.42	96.06	6.021	0.7797	***********
2.26	98.31	7.429	0.8709	****
0.68	98.99	9.167	0.9622	*
0.45	99.44	11.310	1.0535	*
0.23	99.66	13.956	1.1447	
0.00	99.66	17.219	1.2360	
0.00	99.66	21.246	1.3273	
0.23	99.89	26.215	1.4185	

0 1 2 3 4

Each "*" represents approximately 2.2 observations.

##



TEUTON SOIL
PROBABILITY PLOT
1.600
0.920
0.240
-0.440
-1.120
-1.800
99
98
95
85
70
50
30
15
5
2
1
PERCENT
LOGARITHMIC VALUES
VARIABLE = AG
UNIT = PPM
N = 443
N CI = 27

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable =	CU	Unit =	PPM	N =	443
Mean =	2.1732	Min =	0.6021	1st Quartile =	2.0107
Std. Dev. =	0.3449	Max =	3.1319	Median =	2.2368
CV % =	15.8708	Skewness =	-1.2137	3rd Quartile =	2.3834

Anti-Log Mean = 149.014 Anti-Log Std. Dev. : (-) 67.347
(+) 329.712

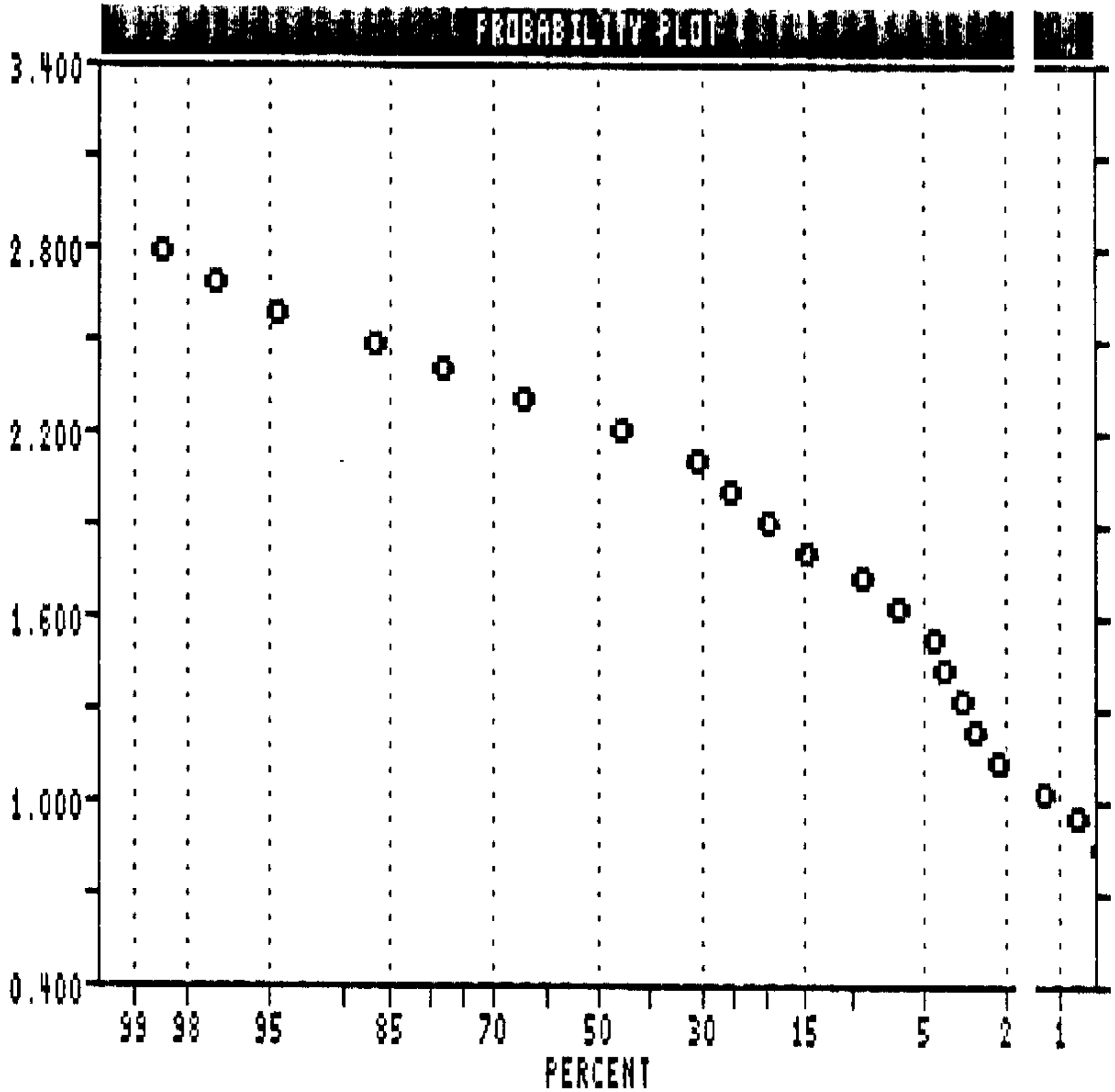
%	cum %	antilog	cls int	(# of bins = 27 - bin size = 0.0973)
0.00	0.11	3.576	0.5534	
0.23	0.34	4.474	0.6507	
0.00	0.34	5.598	0.7480	
0.23	0.56	7.004	0.8453	
0.23	0.79	8.762	0.9426	
0.45	1.24	10.963	1.0399	*
0.90	2.14	13.716	1.1372	**
0.68	2.82	17.160	1.2345	*
0.45	3.27	21.470	1.3318	*
0.68	3.94	26.862	1.4291	*
0.45	4.39	33.608	1.5264	*
2.03	6.42	42.048	1.6237	****
2.48	8.90	52.607	1.7210	*****
5.42	14.30	65.819	1.8183	***********
4.97	19.26	82.348	1.9157	**********
5.64	24.89	103.028	2.0130	***********
5.64	30.52	128.901	2.1103	***********
14.22	44.71	161.273	2.2076	*****************************
19.41	64.08	201.773	2.3049	***************************************
13.77	77.82	252.445	2.4022	****************************
9.03	86.82	315.842	2.4995	******************
7.67	94.48	395.160	2.5968	***************
2.71	97.18	494.397	2.6941	*****
1.35	98.54	618.555	2.7914	***
1.13	99.66	773.894	2.8887	**
0.00	99.66	968.244	2.9860	
0.00	99.66	1211.401	3.0833	
0.23	99.89	1515.622	3.1806	

0 1 2 3 4

Each "*" represents approximately 2.2 observations.

09:39:44
12/27/88

TEUTON SOIL



LOGARITHMIC VALUES
========== ======

VARIABLE = CU
UNIT = PPM
N = 443
N CI = 27

##

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = PB   Unit = PPM   N = 443

Mean =	2.0722	Min =	1.2304	1st Quartile =	1.8062
Std. Dev. =	0.3375	Max =	3.1212	Median =	2.0700
CV % =	16.2895	Skewness =	0.1094	3rd Quartile =	2.3112

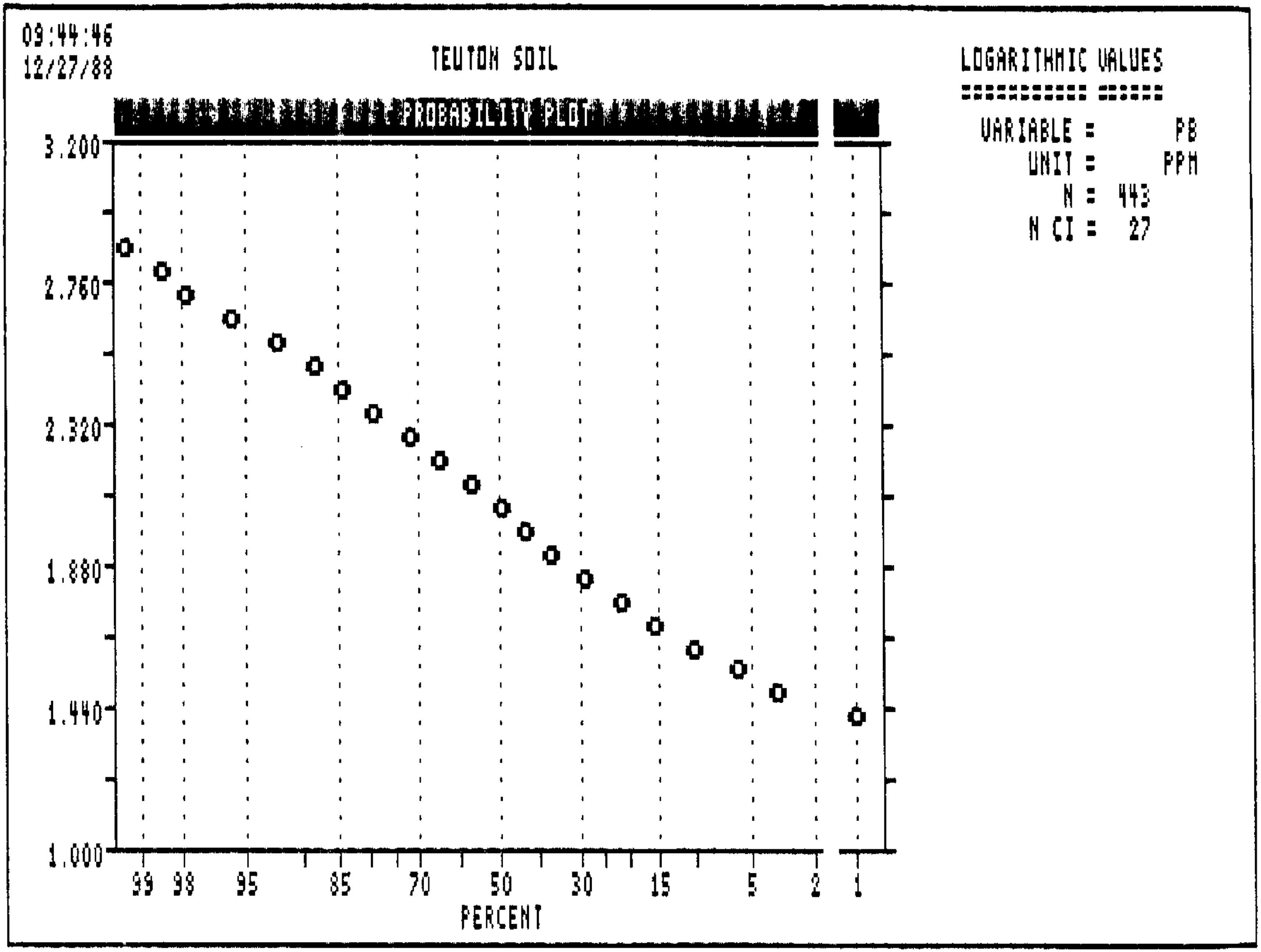
Anti-Log Mean = 118.077   Anti-Log Std. Dev. : (-) 54.277
(+) 256.868

%	cum %	antilog	cls int	(# of bins = 27 - bin size = 0.0727)
0.00	0.11	15.635	1.1941	
0.23	0.34	18.485	1.2668	
0.00	0.34	21.854	1.3395	
0.68	1.01	25.838	1.4123	*
2.48	3.49	30.548	1.4850	*****
2.48	5.97	36.116	1.5577	*****
4.06	10.02	42.699	1.6304	********
5.42	15.43	50.483	1.7031	***********
5.64	21.06	59.685	1.7759	***********
7.45	28.49	70.565	1.8486	***************
7.90	36.37	83.428	1.9213	****************
6.55	42.91	98.636	1.9940	*************
6.32	49.21	116.616	2.0668	*************
7.22	56.42	137.873	2.1395	**************
8.13	64.53	163.005	2.2122	****************
7.00	71.51	192.719	2.2849	**************
7.45	78.94	227.849	2.3576	***************
5.42	84.35	269.382	2.4304	***********
3.84	88.18	318.486	2.5031	********
4.29	92.45	376.542	2.5758	********
3.39	95.83	445.180	2.6485	*******
2.03	97.86	526.330	2.7213	****
0.68	98.54	622.273	2.7940	*
0.68	99.21	735.704	2.8667	*
0.45	99.66	869.812	2.9394	*
0.00	99.66	1028.366	3.0121	
0.00	99.66	1215.823	3.0849	
0.23	99.89	1437.450	3.1576	

0 1 2 3 4

Each "*" represents approximately 2.2 observations.

##



09:44:46
12/27/88
TEUTON SOIL
PROBABILITY PLOT
LOGARITHMIC VALUES
VARIABLE = PB
UNIT = PPM
N = 443
N CI = 27
3.200
2.760
2.320
1.880
1.440
1.000
99 98 95 85 70 50 30 15 5 2 1
PERCENT

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = ZN Unit = PPM N = 443

Mean =	2.3582	Min =	1.3010	1st Quartile =	2.2075
Std. Dev. =	0.2758	Max =	3.3306	Median =	2.3243
CV % =	11.6967	Skewness =	-0.1391	3rd Quartile =	2.5403

Anti-Log Mean = 228.124 Anti-Log Std. Dev. : (-) 120.877
(+) 430.526

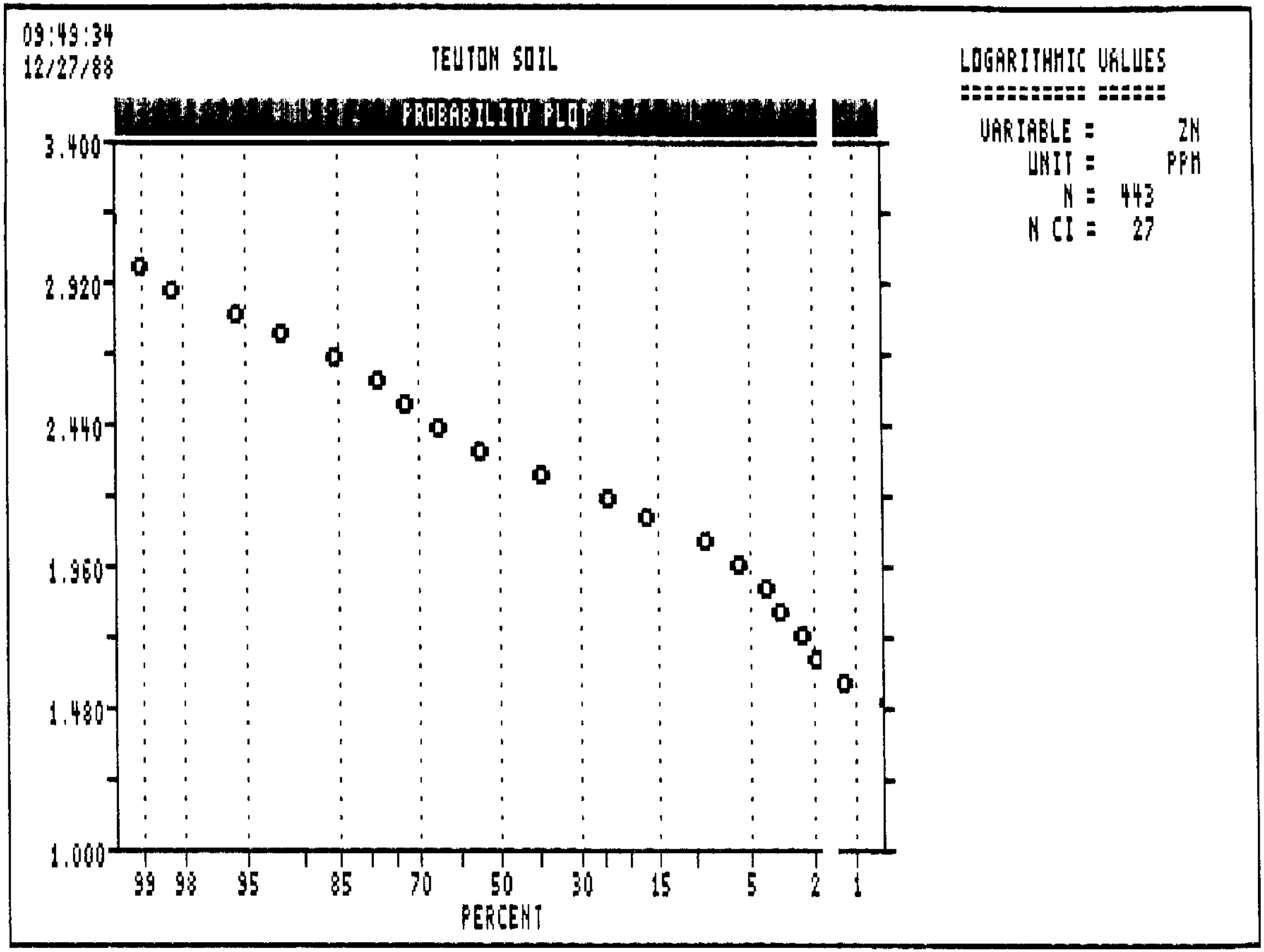
==

%	cum %	antilog	cls int	(# of bins = 27 - bin size = 0.0781)
0.00	0.11	18.281	1.2620	
0.23	0.34	21.881	1.3401	
0.00	0.34	26.189	1.4181	
0.23	0.56	31.346	1.4962	
0.68	1.24	37.518	1.5742	*
0.68	1.91	44.906	1.6523	*
0.45	2.36	53.748	1.7304	*
0.90	3.27	64.332	1.8084	**
0.68	3.94	76.999	1.8865	*
1.81	5.74	92.161	1.9645	****
2.93	8.67	110.309	2.0426	******
7.90	16.55	132.029	2.1207	****************
7.22	23.76	158.027	2.1987	**************
15.12	38.85	189.144	2.2768	******************************
15.80	54.62	226.388	2.3549	*******************************
10.16	64.75	270.966	2.4329	********************
7.67	72.41	324.322	2.5110	***************
5.87	78.27	388.183	2.5890	************
7.22	85.47	464.620	2.6671	**************
6.55	92.00	556.108	2.7452	*************
3.61	95.61	665.610	2.8232	*******
2.71	98.31	796.675	2.9013	*****
0.68	98.99	953.547	2.9793	*
0.00	98.99	1141.309	3.0574	
0.45	99.44	1366.042	3.1355	*
0.00	99.44	1635.028	3.2135	
0.23	99.66	1956.979	3.2916	
0.23	99.89	2342.325	3.3696	

0 1 2 3 4

Each "*" represents approximately 2.2 observations.

##


09:49:34
12/27/88
TEUTON SOIL
PROBABILITY PLOT
LOGARITHMIC VALUES
VARIABLE = ZN
UNIT = PPM
N = 443
N CI = 27
3.400
2.920
2.440
1.960
1.480
1.000
99
98
95
85
70
50
30
15
5
2
1
PERCENT

##

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = AS   Unit = PPM   N = 443

Mean =	2.4637	Min =	1.1461	1st Quartile =	2.0908
Std. Dev. =	0.5076	Max =	3.7315	Median =	2.5922
CV % =	20.6041	Skewness =	-0.5676	3rd Quartile =	2.8325

Anti-Log Mean = 290.888   Anti-Log Std. Dev. : (-) 90.385
(+) 936.173

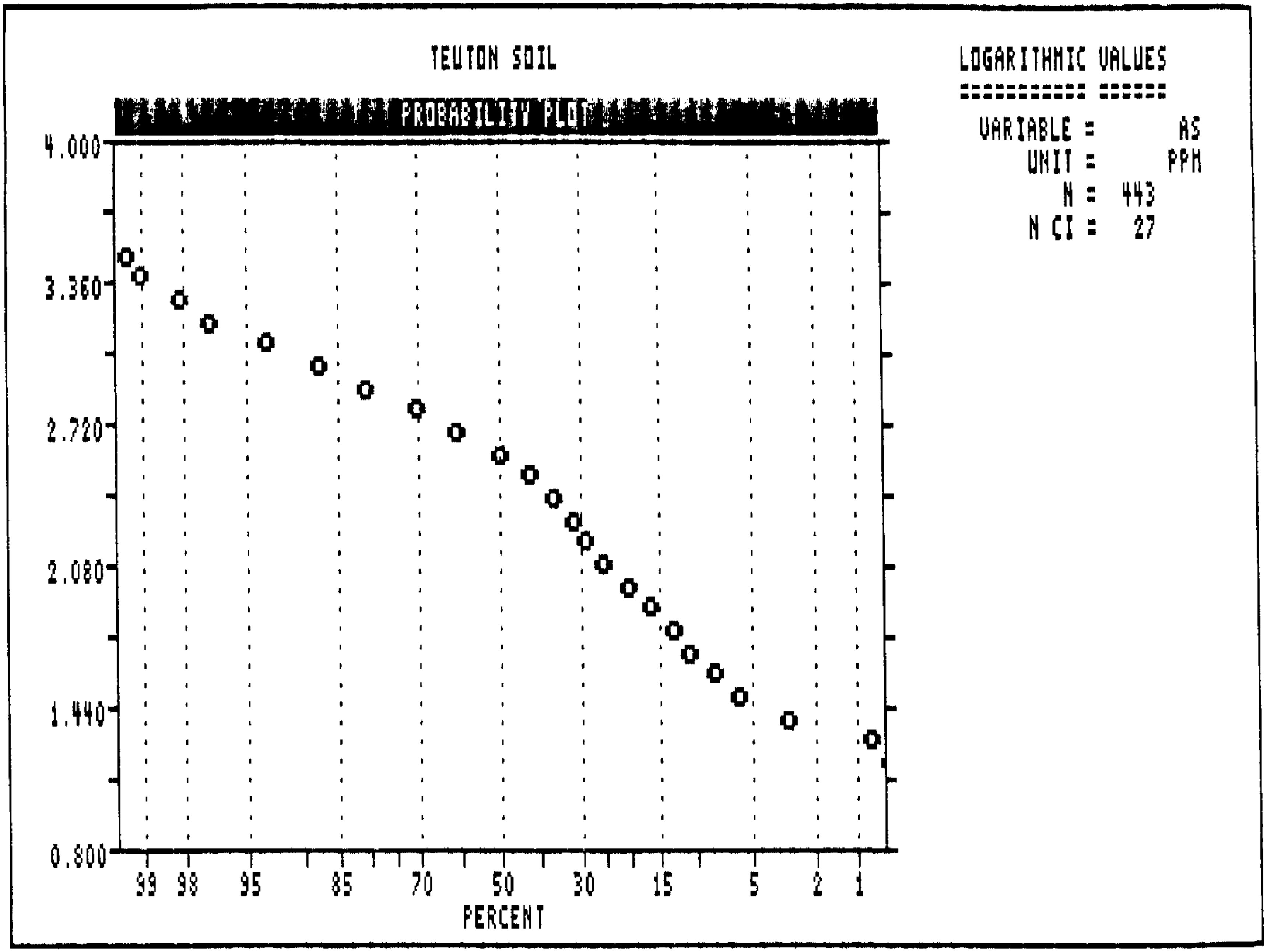
==

%	cum %	antilog	cls int	(# of bins = 27 - bin size = 0.0994)
0.00	0.11	12.406	1.0964	
0.45	0.56	15.698	1.1958	*
0.23	0.79	19.737	1.2953	
2.26	3.04	24.815	1.3947	****
2.93	5.97	31.200	1.4942	******
2.03	8.00	39.228	1.5936	****
2.71	10.70	49.321	1.6930	*****
2.03	12.73	62.012	1.7925	****
3.61	16.33	77.967	1.8919	*******
3.61	19.93	98.028	1.9913	*******
4.97	24.89	123.250	2.0908	**********
3.61	28.49	154.962	2.1902	*******
2.93	31.42	194.833	2.2897	******
4.74	36.15	244.962	2.3891	*********
5.87	42.00	307.990	2.4885	************
7.45	49.44	387.235	2.5880	***************
11.06	60.47	486.869	2.6874	**********************
9.71	70.16	612.139	2.7869	*******************
10.38	80.52	769.640	2.8863	*********************
7.22	87.73	967.666	2.9857	**************
5.64	93.36	1216.643	3.0852	***********
3.61	96.96	1529.681	3.1846	*******
1.13	98.09	1923.262	3.2840	**
0.90	98.99	2418.111	3.3835	**
0.23	99.21	3040.282	3.4829	
0.45	99.66	3822.536	3.5824	*
0.00	99.66	4806.062	3.6818	
0.23	99.89	6042.644	3.7812	

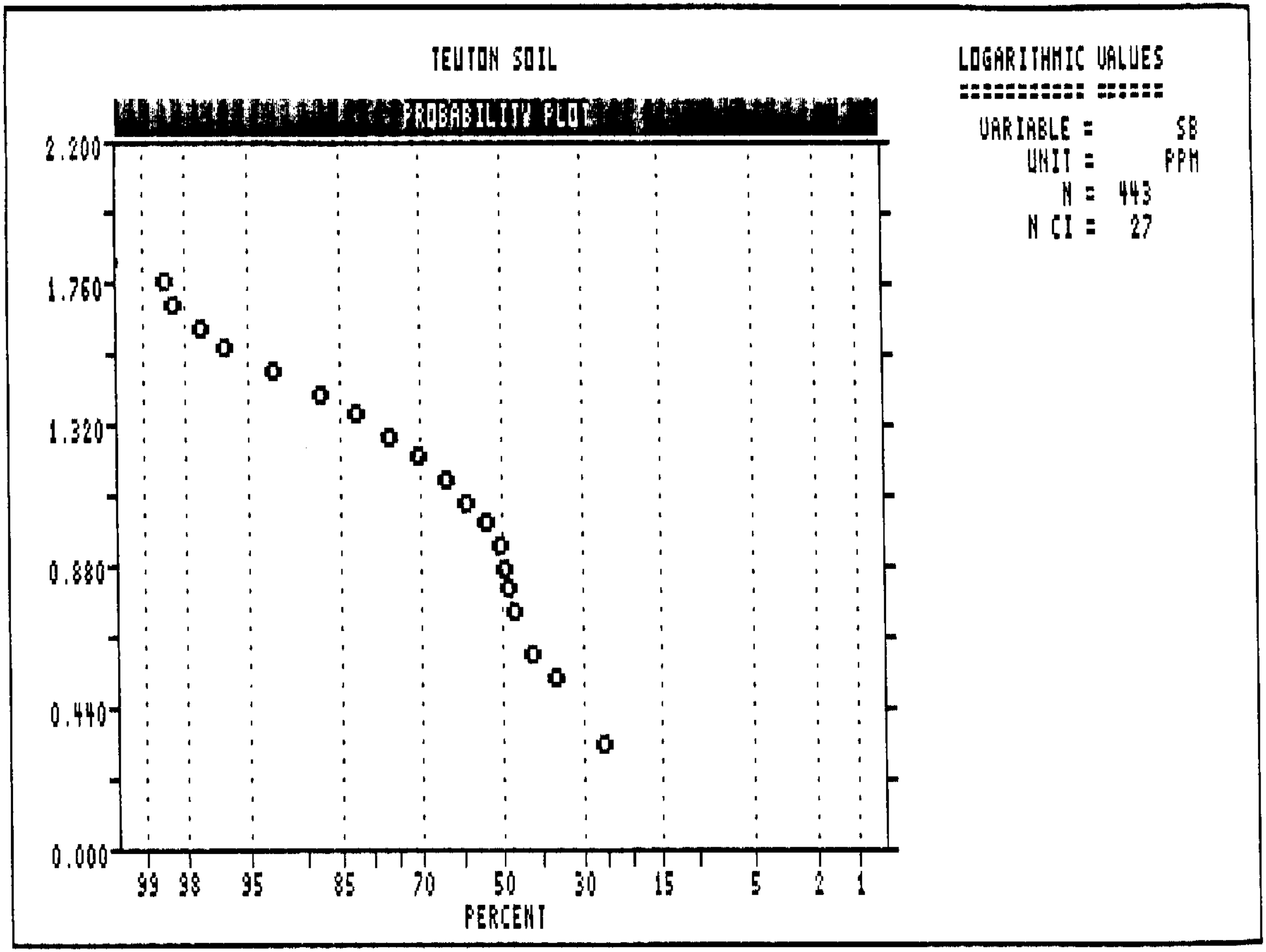
0   1   2   3   4

Each "*" represents approximately 2.2 observations.

##


TEUTON SOIL
PROBABILITY PLOT
LOGARITHMIC VALUES
VARIABLE = AS
UNIT = PPM
N = 443
N CI = 27
4.000
3.360
2.720
2.080
1.440
0.800
99 98 95 85 70 50 30 15 5 2 1
PERCENT

```
################################################################################
SUMMARY STATISTICS and HISTOGRAM                                LOGARITHMIC VALUES

 Variable =        SB         Unit =        PPM                  N =     443

      Mean =     0.8689         Min =      0.3010   1st Quartile =     0.3010
Std. Dev. =     0.4602         Max =      2.0682         Median =     0.9287
     CV % =    52.9615    Skewness =      0.0988   3rd Quartile =     1.2788

        Anti-Log Mean =      7.394      Anti-Log Std. Dev. : (-)      2.563
                                                           (+)     21.334

================================================================================
  %    cum %    antilog   cls int   (# of bins = 27  -  bin size =   0.0680)
 -----  -----   -------   -------   ----------------------------------------------
 0.00   0.11     1.849    0.2670
25.28  25.34     2.163    0.3350   ******************************* -->    50
 0.00  25.34     2.529    0.4030
 0.00  25.34     2.958    0.4709
10.84  36.15     3.459    0.5389   *********************
 5.64  41.78     4.045    0.6069   ***********
 0.00  41.78     4.730    0.6749
 4.51  46.28     5.531    0.7428   *********
 1.81  48.09     6.468    0.8108   ****
 0.90  48.99     7.564    0.8788   **
 0.90  49.89     8.845    0.9467   **
 3.84  53.72    10.344    1.0147   ********
 4.74  58.45    12.096    1.0827   *********
 4.97  63.40    14.146    1.1506   **********
 6.77  70.16    16.542    1.2186   *************
 6.32  76.46    19.345    1.2866   *************
 5.87  82.32    22.622    1.3545   ************
 5.42  87.73    26.454    1.4225   ***********
 5.19  92.91    30.936    1.4905   **********
 3.39  96.28    36.177    1.5584   *******
 1.13  97.41    42.306    1.6264   **
 0.90  98.31    49.473    1.6944   **
 0.23  98.54    57.854    1.7623
 0.90  99.44    67.655    1.8303   **
 0.23  99.66    79.116    1.8983
 0.00  99.66    92.520    1.9662
 0.00  99.66   108.194    2.0342
 0.23  99.89   126.523    2.1022
--------------------------------------------------------------------------------
                                   0         1         2         3         4

                        Each "*" represents approximately 2.2 observations.

################################################################################
```


TEUTON SOIL
PROBABILITY PLOT
2.200
1.760
1.320
0.880
0.440
0.000
99
98
95
85
70
50
30
15
5
2
1
PERCENT
LOGARITHMIC VALUES
VARIABLE = SB
UNIT = PPM
N = 443
N CI = 27

##

SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

Variable = AU Unit = PPB N = 264

Mean =	1.9170	Min =	0.0000	1st Quartile =	1.4150
Std. Dev. =	0.8947	Max =	3.8106	Median =	1.9823
CV % =	46.6746	Skewness =	-0.3567	3rd Quartile =	2.5055

Anti-Log Mean = 82.603 Anti-Log Std. Dev. : (-) 10.526
(+) 648.252

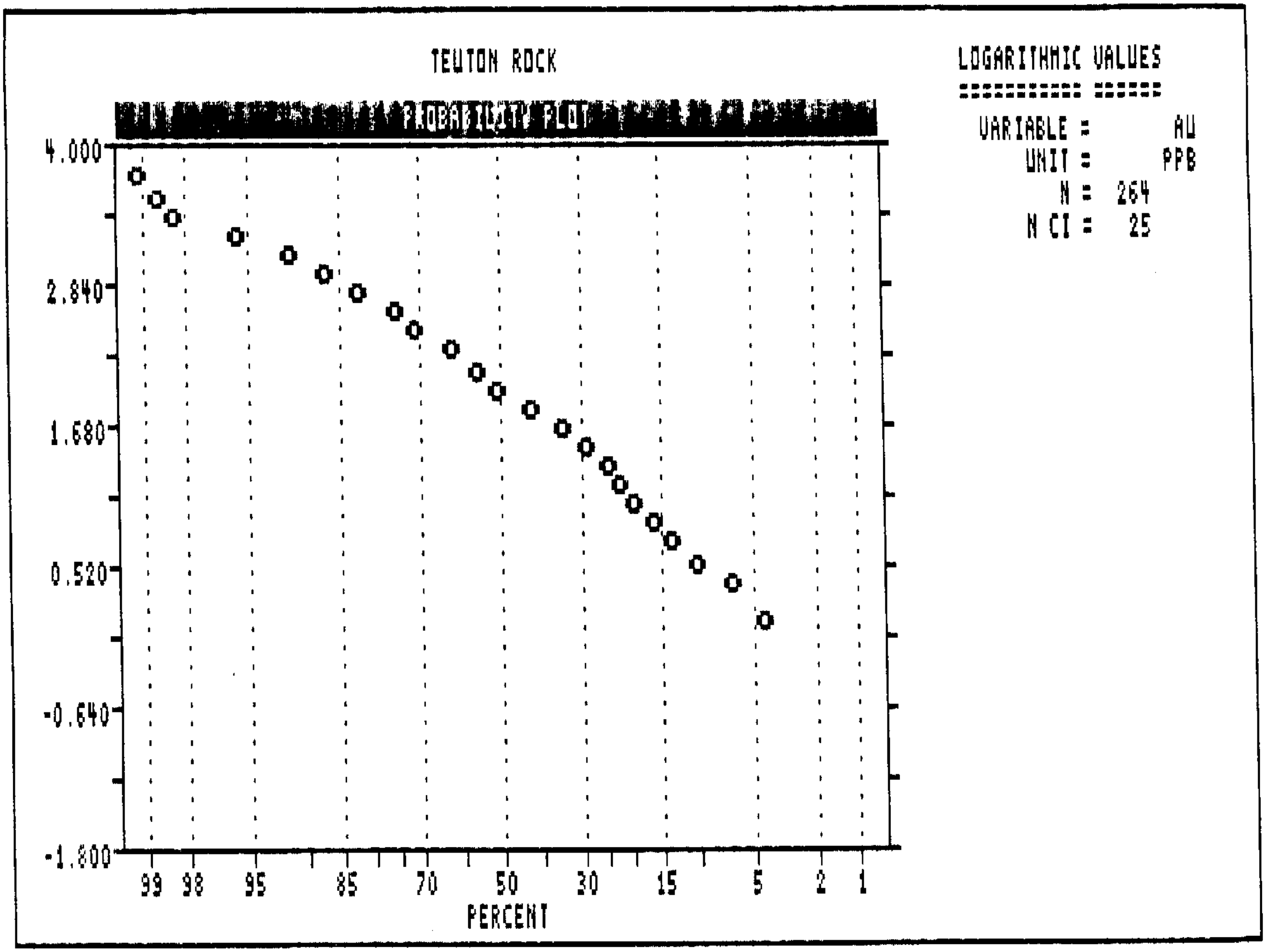
==

%	cum %	antilog	cls int	(# of bins = 25 - bin size = 0.1588)
0.00	0.19	0.833	-0.0794	
4.17	4.34	1.201	0.0794	******
0.00	4.34	1.730	0.2382	
2.27	6.60	2.494	0.3969	***
3.41	10.00	3.595	0.5557	*****
3.41	13.40	5.182	0.7145	*****
2.65	16.04	7.469	0.8733	****
3.03	19.06	10.765	1.0320	*****
2.65	21.70	15.517	1.1908	****
2.27	23.96	22.365	1.3496	***
4.55	28.49	32.237	1.5084	*******
5.68	34.15	46.465	1.6671	*********
7.95	42.08	66.973	1.8259	************
8.33	50.38	96.532	1.9847	*************
5.30	55.66	139.138	2.1434	********
6.44	62.08	200.548	2.3022	**********
8.71	70.75	289.063	2.4610	*************
4.55	75.28	416.645	2.6198	*******
6.82	82.08	600.537	2.7785	**********
5.30	87.36	865.592	2.9373	********
4.17	91.51	1247.633	3.0961	******
4.17	95.66	1798.294	3.2549	******
2.65	98.30	2591.996	3.4136	****
0.38	98.68	3736.010	3.5724	*
0.38	99.06	5384.950	3.7312	*
0.76	99.81	7761.674	3.8900	*

0 1 2 3 4

Each "*" represents approximately 1.7 observations.

##


TEUTON ROCK
PROBABILITY PLOT
LOGARITHMIC VALUES
VARIABLE = AU
UNIT = PPB
N = 264
N CI = 25
4.000
2.840
1.680
0.520
-0.640
-1.800
99 98 95 85 70 50 30 15 5 2 1
PERCENT

##

SUMMARY STATISTICS and HISTOGRAM — LOGARITHMIC VALUES

Variable = AS   Unit = PPM   N = 264

Mean =	1.9447	Min =	0.3010	1st Quartile =	1.5185
Std. Dev. =	0.6128	Max =	3.2151	Median =	2.0043
CV % =	31.5109	Skewness =	-0.4414	3rd Quartile =	2.4232

Anti-Log Mean = 88.043   Anti-Log Std. Dev. : (-) 21.474
(+) 360.983

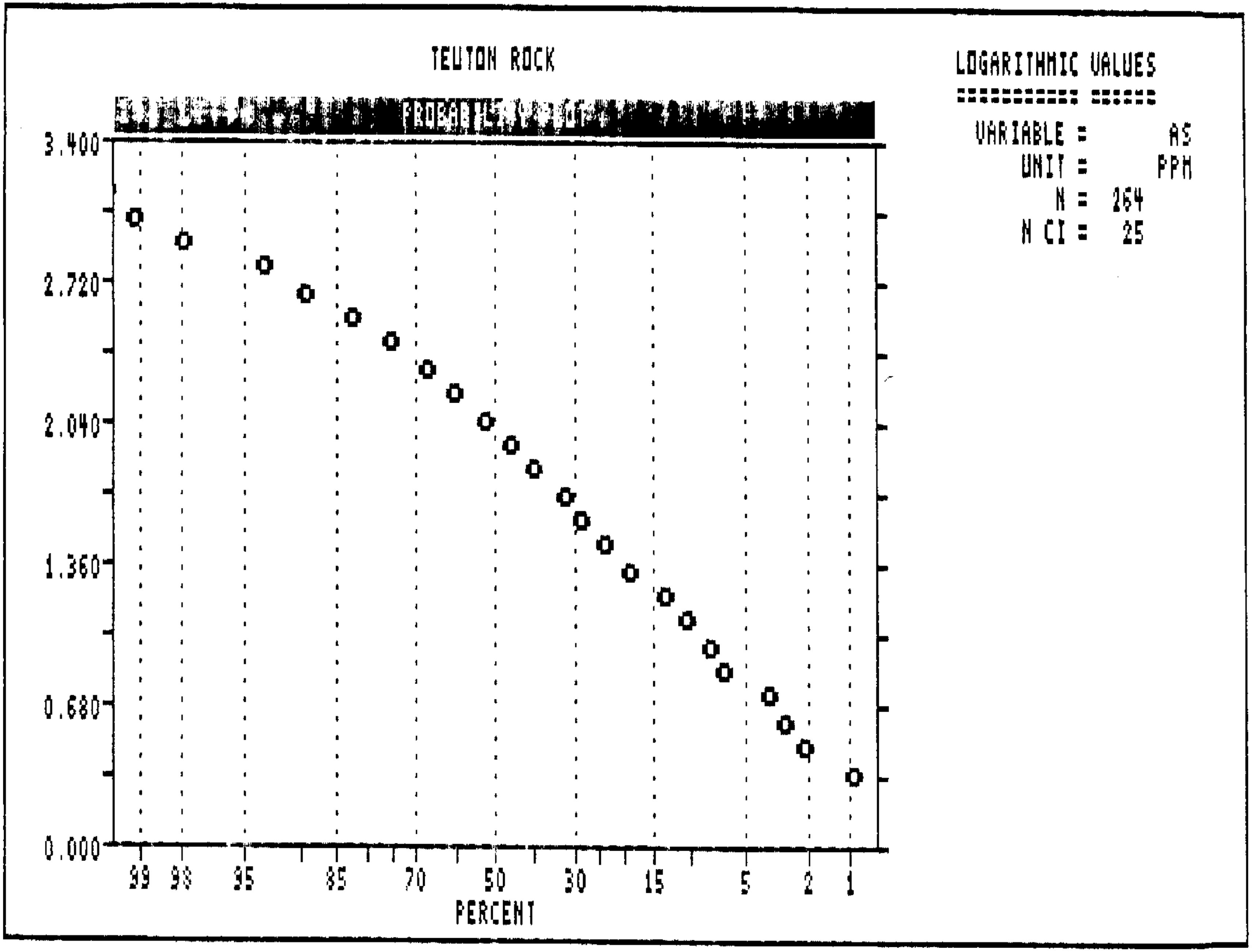
==

%	cum %	antilog	cls int	(# of bins = 25 - bin size = 0.1214)
0.00	0.19	1.739	0.2403	
0.76	0.94	2.300	0.3617	*
1.14	2.08	3.042	0.4832	**
0.76	2.83	4.023	0.6046	*
0.76	3.58	5.321	0.7260	*
3.03	6.60	7.038	0.8474	*****
1.14	7.74	9.308	0.9688	**
2.65	10.38	12.310	1.0903	****
2.65	13.02	16.281	1.2117	****
5.68	18.68	21.533	1.3331	*********
4.55	23.21	28.479	1.4545	*******
4.92	28.11	37.665	1.5759	********
3.79	31.89	49.815	1.6974	******
7.58	39.43	65.884	1.8188	************
6.06	45.47	87.136	1.9402	*********
6.82	52.26	115.244	2.0616	***********
7.95	60.19	152.419	2.1830	************
6.44	66.60	201.585	2.3045	**********
8.71	75.28	266.612	2.4259	**************
7.20	82.45	352.613	2.5473	***********
6.82	89.25	466.357	2.6687	***********
4.17	93.40	616.792	2.7901	******
4.55	97.92	815.753	2.9116	*******
1.14	99.06	1078.894	3.0330	**
0.38	99.43	1426.917	3.1544	*
0.38	99.81	1887.203	3.2758	*

Scale: 0 1 2 3 4

Each "*" represents approximately 1.7 observations.

##


TEUTON ROCK
LOGARITHMIC VALUES
VARIABLE = AS
UNIT = PPM
N = 264
N CI = 25
3.400
2.720
2.040
1.360
0.680
0.000
99
98
95
85
70
50
30
15
5
2
1
PERCENT

APPENDIX IV

ASSAY CERTIFICATES

F

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: JUL 19 1988
DATE REPORT MAILED: July 25/88.

ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: .... D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES FILE # 88-2787 Page 1

SAMPLE#	AU** oz/t
TR1 88-1	.006
TR1 88-2	.008
TR1 88-3	.006
TR1 88-4	.014
TR1 88-5	.056
TR1 88-6	.122
TR1 88-7	1.374
TR1 88-8	.102
TR1 88-9	.086
TR1 88-10	.034
TR1 88-11	.044
TR1 88-12	.042
TR1 88-13	.162
TR1 88-14	.308
TR1 88-15	.372
TR1 88-16	.198
TR1 88-17	.152
TR1 88-18	.086
TR1 88-19	.172
TR2 88-1	.008
TR2 88-2	.010
TR2 88-3	.004
TR2 88-4	.032
TR2 88-5	.018
TR2 88-6	.026
TR2 88-7	.010
TR2 88-8	.068
TR2 88-9	.008
TR2 88-10	.004
TR2 88-11	.002
TR2 88-12	.008
TR2 88-13	.002
TR2 88-14	.004
TR2 88-15	.004
TR2 88-16	.004
TR2 88-17	.002

SAMPLE#	AU** oz/t
TR2 88-18	.002
TR3 88-1	.003
TR3 88-2	.014
TR3 88-3	.008
TR3 88-4	.004
TR3 88-5	.002
TR3 88-6	.005
TR3 88-7	.009
TR3 88-8	.026
TR3 88-9	.009
TR3 88-10	.015
TR3 88-11	.002
TR3 88-12	.005
TR3 88-13	.002
TR3 88-14	.005
TR3 88-15	.006
TR3 88-16	.004
TR3 88-17	.001
TR3 88-18	.006
TR3 88-19	.009
TR3 88-20	.018
TR3 88-21	.017
TR3 88-22	.018
TR3 88-23	.009
TR3 88-24	.006
TR3 88-25	.005
TR3 88-26	.010
TR3 88-27	.016
TR3 88-28	.008
TR3 88-29	.006
TR4 88-1	.007
TR4 88-2	.012
TR4 88-3	1.206
TR4 88-4	.744
TR4 88-5	.158
TR4 88-6	.053

SAMPLE#	AU** oz/t
TR4 88-7	.064
TR4 88-8	.036
TR4 GRAB	.194
~~TK-001 GRAB~~	~~.062~~
~~TK-002 FLOAT~~	~~.229~~
~~LIMO~~	~~3.892~~

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: JUL 28 1988
DATE REPORT MAILED: Aug. 6/88

ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: C. Leong. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES FILE # 88-3097 Page 1

SAMPLE#	AU** oz/t
~~TK-003~~	~~.001~~
TK-004	.151
TK-005	.201
TR5 88-1	.010
TR5 88-2	.017
TR5 88-3	.004
TR5 88-4	.009
TR5 88-5	.011
TR5 88-6	.025
TR5 88-7	.032
TR5 88-8	.014
TR6 88-1	.029
TR6 88-2	.039
TR6 88-3	.021
TR6 88-4	.011
TR6 88-5	.007
TR6 88-6	.011
TR6 88-7	.009
TR6 88-8	.004
TR7 88-1	.109
TR7 88-2	.058
TR7 88-3	.027
TR8 88-1	.002
TR8 88-2	.006
TR8 88-3	.002
TR8 88-4	.001
TR8 88-5	.002
TR8 88-6	.004
TR8 88-7	.001
TR8 88-8	.007
TR8 88-9	.002
TR8 88-10	.001
TR8 88-11	.003
TR8 88-12	.002
TR8 88-13	.004
TR8 88-14	.007

SAMPLE#	AU** oz/t
TR8 88-15	.003
TR10 88-1	.017
TR10 88-2	.018
TR10 88-3	.002
TR10 88-4	.003
TR10 88-5	.002
TR11 88-1	.054
TR11 88-2	.010
TR11 88-3	.052
TR11 88-4	.014
TR11 88-5	.013
TR11 88-6	.006
TR11 88-7	.008
TR11 88-8	.039
TR11 88-9	.002
TR11 88-10	.005
TR12 88-1	.007
TR12 88-2	.124
TR12 88-3	.028
TR12 88-4	.011
TR12 88-5	.083
TR12 88-6	.022
TR13 88-1	.017
TR13 88-2	.076
TR13 88-3	.057
TR13 88-4	.072
TR13 88-5	.055
TR13 88-6	.019
TR13 88-7	.044
TR13 88-8	.024
TR13 88-9	.041
TR13 88-10	.035
TR13 88-11	.036
TR14 88-1	.014
TR14 88-2	.062
TR14 88-3	.014

SAMPLE#	AU** oz/t
TR15 88-1	.002
TR15 88-2	.025
TR15 88-3	.095
TR15 88-4	.018
TR15 88-5	.123
TR15 88-6	.046

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: AUG 11 1988
DATE REPORT MAILED: Aug 16/88

ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: D.Toye D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES FILE # 88-3501 Page 1

SAMPLE#	AU** oz/t
L125S 0W	.002
L150S 40W	.003
L150S 35W	.002
L150S 30W	.001
L150S 25W	.006
L150S 20W	.004
L150S 15W	.041
L150S 10W	.004
L150S 5W	.001
L150S 0W	.002
L175S 80W	.001
L175S 75W	.001
L175S 70W	.013
L175S 65W	.001
L175S 60W	.002
L175S 55W	.001
L175S 50W	.013
L175S 45W	.004
L175S 40W	.001
L175S 35W	.002
TK 006	.025
TR13 88-12	.026
TR13 88-13	.014
TR13 88-14	.052
TR13 88-15	.017
TR13 88-16	.021
TR13 88-17	.013
TR16 88-1	.012
TR16 88-2	.021
TR16 88-3	.027
TR16 88-4	.008
TR16 88-5	.007
TR16 88-6	.005
TR17 88-1	.007
TR17 88-2	.012
TR17 88-3	.057

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: AUG 11 1988
DATE REPORT MAILED: Aug. 19/88.

ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK AU** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: .... D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES FILE # 88-3501A

"GOAT TRAIL" SAMPLES

SAMPLE#	AU** oz/t
TR18 88-1	.032
TR18 88-2	.106
TR18 88-3	.028
TR18 88-4	.081
TR18 88-5	.022
TR19 88-1	.013
TR19 88-2	.560
TR19 88-3	.093
TR19 88-4	.042
TR19 88-5	.005
TR19 88-6	.013
TR20 88-1	.004
TR20 88-2	.008
TR20 88-3	.003
TR20 88-4	.004
TR20 88-5	.056
TR20 88-6	.114
TR20 88-7	.043
TR20 88-8	.099
TR20 88-9	.081
TR20 88-10	.019

ACME ANAL..ICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUV.. B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1..

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK

DATE RECEIVED: AUG 9 1988 DATE REPORT MAILED: Aug 15/88 ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES File # 88-2787R Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
TR1 88-1	3	284	22	118	.9	6	13	3017	7.36	40	5	ND	2	115	1	3	2	83	1.59	.119	4	9	2.18	57	.08	3	3.19	.01	.02	9
TR1 88-2	3	382	27	90	1.4	5	13	2204	8.35	76	5	ND	2	95	1	2	2	71	1.20	.110	4	9	1.74	60	.08	2	2.62	.01	.05	4
TR1 88-3	2	716	23	91	1.2	4	9	2335	6.98	104	5	ND	2	119	1	2	2	75	1.93	.112	4	8	1.80	29	.09	2	2.57	.01	.05	2
TR1 88-4	1	316	13	44	1.0	4	8	1462	8.06	88	5	ND	2	126	1	4	2	36	1.98	.082	3	4	1.01	31	.09	3	1.50	.01	.02	6
TR1 88-5	5	221	22	43	1.9	4	13	2149	14.91	231	5	ND	2	102	1	9	2	51	1.35	.069	3	9	.70	16	.10	4	.95	.01	.03	24
TR1 88-6	2	2995	20	68	14.0	3	30	1993	27.71	295	5	ND	4	38	1	8	2	36	1.22	.043	3	11	.46	6	.05	13	.88	.01	.02	65
TR1 88-7	13	795	37	26	20.4	1	3	209	30.38	844	5	30	4	49	1	23	30	58	.18	.038	2	10	.03	68	.08	13	.27	.01	.06	108
TR1 88-8	2	1480	30	57	10.3	4	35	774	33.29	301	7	ND	6	27	1	12	5	48	.26	.046	3	14	.48	6	.04	9	1.12	.01	.04	98
TR1 88-9	6	606	36	76	4.8	6	65	2470	29.76	303	6	ND	4	27	1	6	3	87	.25	.067	6	10	1.38	4	.01	10	2.99	.01	.10	5
TR1 88-10	4	510	17	30	5.0	3	29	329	22.59	257	5	ND	4	127	1	5	2	82	.67	.086	3	7	.39	10	.08	4	1.04	.01	.06	5
TR1 88-11	7	74	20	58	2.4	4	39	1725	13.19	118	5	ND	2	195	1	3	2	70	2.36	.085	5	8	1.47	10	.06	2	2.38	.01	.03	9
TR1 88-12	3	35	19	59	1.3	4	17	3519	10.08	54	5	ND	2	152	1	2	2	93	4.02	.105	5	10	1.59	20	.10	5	2.53	.01	.02	6
TR1 88-13	6	259	23	43	2.3	4	17	2508	15.13	218	5	3	2	114	1	6	2	52	6.10	.052	3	10	.64	18	.04	3	.93	.01	.06	34
TR1 88-14	2	349	30	38	4.5	3	16	977	30.29	353	6	7	5	47	1	10	2	48	2.04	.038	3	10	.34	15	.03	12	.63	.01	.05	171
TR1 88-15	9	235	37	30	4.7	3	14	429	30.91	322	6	6	4	48	1	8	3	45	.77	.038	2	14	.12	10	.06	10	.38	.01	.03	153
TR1 88-16	5	167	26	30	2.9	5	17	1014	15.46	149	5	6	3	83	1	4	2	57	.90	.069	3	15	.43	21	.08	2	1.00	.01	.04	16
TR1 88-17	8	158	31	34	2.2	6	19	469	21.98	183	5	2	4	48	1	4	2	35	.43	.052	3	16	.43	9	.05	5	.78	.01	.02	20
TR1 88-18	4	110	29	64	2.2	6	23	1477	23.35	173	5	ND	3	52	1	4	3	42	1.63	.047	4	17	1.17	8	.03	6	1.58	.01	.05	9
TR1 88-19	2	41	22	40	2.1	7	8	1545	13.13	138	5	5	3	134	1	5	2	55	2.59	.087	5	14	.63	59	.10	2	1.42	.01	.02	20
TR2 88-1	1	56	16	110	.8	15	20	2004	9.57	38	5	ND	2	32	1	2	2	181	1.81	.168	13	19	2.24	98	.15	2	2.95	.01	.05	2
TR2 88-2	1	66	21	77	.8	9	9	2208	10.51	41	5	ND	4	27	1	2	2	124	.70	.066	7	38	1.61	31	.03	2	2.74	.01	.06	3
TR2 88-3	4	40	28	56	.6	10	7	1106	8.26	41	5	ND	3	15	1	2	2	103	.46	.067	6	39	.95	27	.05	2	1.75	.01	.11	1
TR2 88-4	14	111	43	78	1.2	6	12	1194	18.01	56	5	ND	4	6	1	2	2	123	.14	.063	4	47	1.23	12	.01	3	3.26	.01	.05	1
TR2 88-5	6	198	85	141	1.4	9	12	1474	18.44	105	5	ND	4	4	1	8	2	159	.13	.054	4	41	2.00	11	.01	3	3.91	.01	.07	1
TR2 88-6	6	98	68	89	1.6	4	7	741	17.89	413	5	ND	4	5	1	7	2	122	.06	.057	3	34	1.00	13	.01	2	2.73	.01	.10	1
TR2 88-7	6	71	88	151	1.6	11	9	1431	11.10	154	5	ND	4	6	1	2	2	107	.19	.106	6	32	1.76	29	.01	2	2.94	.01	.09	1
TR2 88-8	8	20	24	61	4.0	8	11	818	12.06	62	5	2	3	19	1	2	2	75	.19	.062	8	35	.96	14	.02	3	2.00	.01	.09	2
TR2 88-9	3	37	71	97	1.3	10	7	1152	6.58	51	5	ND	2	42	1	2	2	80	.04	.062	7	38	.75	30	.07	5	1.25	.02	.08	3
TR2 88-10	2	21	48	60	.4	9	7	1000	5.75	51	5	ND	2	18	1	2	2	81	.27	.067	4	37	.97	64	.05	2	1.42	.02	.11	2
TR2 88-11	1	13	37	57	.5	20	11	648	3.07	29	5	ND	4	11	1	2	2	60	.17	.068	5	32	.70	220	.02	2	.93	.01	.11	1
TR2 88-12	2	22	53	76	.6	33	19	1010	4.20	44	5	ND	2	10	1	2	3	79	.33	.076	14	33	.89	80	.02	2	1.08	.02	.10	1
TR2 88-13	1	22	59	68	.4	17	7	703	3.33	28	5	ND	4	17	1	2	2	68	.24	.069	5	26	.96	113	.04	2	1.18	.01	.11	1
TR2 88-14	1	78	64	119	.8	37	19	1361	6.11	46	5	ND	3	17	1	2	2	96	.56	.173	18	53	1.43	145	.04	2	1.87	.01	.12	1
TR2 88-15	1	86	139	275	1.2	18	25	1518	6.76	64	5	ND	3	19	2	2	2	97	.31	.078	14	31	1.78	154	.03	2	2.62	.01	.09	2
TR2 88-16	1	48	22	64	.5	19	10	812	3.90	23	5	ND	4	19	1	2	2	83	.41	.095	7	29	1.26	142	.06	3	1.61	.01	.12	2
TR2 88-17	1	85	35	191	.9	27	41	1661	12.65	49	5	ND	2	20	1	2	2	395	.74	.092	10	18	1.99	195	.26	11	3.24	.01	.07	1
STD C	18	58	40	132	6.8	67	29	1056	4.12	42	17	6	37	48	18	18	19	57	.50	.090	39	56	.92	175	.06	36	1.99	.06	.14	12

TEUTON RESOURCES FIL # 88-2787R

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
TR2 88-18	1	66	30	117	1.0	14	27	1310	8.50	156	5	ND	1	25	1	3	2	283	.77	.101	7	7	1.66	119	.18	2	2.26	.01	.16	1
TR3 88-1	2	508	35	86	2.5	6	17	1151	4.98	42	5	ND	1	98	1	4	2	125	1.22	.161	4	10	1.64	63	.10	2	2.32	.01	.09	2
TR3 88-2	1	51	12	72	.9	8	10	1455	4.18	20	5	ND	1	46	1	2	2	147	.93	.163	5	12	1.75	70	.07	2	2.25	.02	.09	3
TR3 88-3	1	264	9	70	.5	8	10	1432	4.63	18	5	ND	1	52	1	3	2	157	.89	.166	5	10	1.73	62	.03	4	2.31	.02	.10	2
TR3 88-4	2	241	10	75	.9	7	10	1340	4.09	26	5	ND	1	37	1	2	2	141	.76	.167	8	9	1.61	77	.02	2	1.97	.02	.09	1
TR3 88-5	1	44	6	55	.3	7	9	1010	3.52	12	5	ND	1	61	1	2	2	119	1.00	.155	5	10	1.53	46	.07	2	1.89	.02	.08	4
TR3 88-6	2	336	14	58	.7	6	26	1285	5.68	46	5	ND	2	42	1	3	2	119	.70	.152	5	9	1.43	85	.06	2	1.94	.01	.07	8
TR3 88-7	2	104	14	54	.8	5	15	1134	6.86	45	5	ND	1	48	1	2	2	146	.73	.153	4	8	1.41	64	.07	2	1.99	.01	.09	11
TR3 88-8	2	182	16	31	1.7	2	12	856	11.02	75	5	ND	2	28	1	2	2	135	.26	.160	4	8	.77	86	.01	2	1.30	.01	.12	3
TR3 88-9	1	90	13	43	1.1	3	12	822	6.32	58	5	ND	2	25	1	2	2	104	.18	.196	4	7	1.05	453	.01	5	1.88	.01	.23	3
TR3 88-10	1	233	14	61	2.7	6	11	927	6.74	37	5	ND	2	28	1	3	2	146	.41	.169	6	8	1.87	332	.01	11	2.21	.01	.13	1
TR3 88-11	1	177	7	76	.5	7	13	1094	4.21	11	5	ND	1	47	1	2	2	115	.78	.153	6	7	2.40	94	.01	4	2.65	.01	.10	1
TR3 88-12	4	362	16	79	.9	6	24	1480	7.63	42	5	ND	1	17	1	2	2	166	.42	.168	7	7	1.81	186	.01	2	2.39	.01	.09	1
TR3 88-13	1	46	10	83	.2	6	12	1192	4.35	24	5	ND	1	20	1	2	2	143	.60	.184	6	4	2.31	215	.01	2	2.49	.01	.13	1
TR3 88-14	1	88	8	68	.6	5	11	1028	4.17	34	5	ND	1	26	1	2	2	117	.55	.180	5	5	1.79	222	.01	2	2.04	.01	.15	1
TR3 88-15	2	105	14	57	.9	5	10	869	5.95	39	5	ND	1	42	1	2	2	124	.56	.185	4	10	1.69	102	.01	2	1.96	.01	.10	1
TR3 88-16	1	106	8	74	.3	5	19	1395	4.61	31	5	ND	1	28	1	2	2	130	.55	.179	5	5	2.28	131	.01	3	2.59	.01	.13	1
TR3 88-17	1	39	6	66	.2	5	7	922	3.47	10	5	ND	1	15	1	2	2	116	.51	.179	5	5	2.16	341	.01	2	2.15	.01	.16	2
TR3 88-18	1	88	8	71	.3	5	16	1285	4.94	34	5	ND	1	10	1	2	2	136	.34	.158	5	5	1.63	344	.01	3	1.78	.01	.13	2
TR3 88-19	3	58	34	95	1.3	4	8	815	7.21	135	5	ND	2	36	1	2	2	41	.19	.143	5	2	.22	81	.01	5	.66	.01	.44	1
TR3 88-20	5	41	27	92	1.9	13	13	844	7.90	158	5	ND	1	42	1	2	3	38	.44	.094	5	8	.30	17	.01	18	.63	.01	.27	1
TR3 88-21	10	19	30	35	2.2	2	5	161	6.95	116	5	ND	1	18	1	2	2	38	.06	.051	4	2	.09	40	.01	10	.37	.01	.52	2
TR3 88-22	9	11	21	15	2.5	1	3	105	5.07	171	5	ND	1	21	1	2	2	29	.05	.058	5	2	.06	37	.01	5	.31	.01	.54	1
TR3 88-23	4	11	23	13	1.3	1	3	120	6.03	158	5	ND	2	13	1	2	4	54	.05	.077	5	2	.27	27	.01	3	.51	.01	.44	2
TR3 88-24	2	14	14	39	.8	6	8	487	6.32	108	5	ND	1	16	1	2	3	98	.31	.125	5	9	.91	21	.01	4	1.01	.01	.31	2
TR3 88-25	6	21	10	51	1.6	4	16	737	7.16	172	5	ND	1	13	1	2	2	108	.89	.232	7	4	1.50	16	.01	3	1.52	.01	.18	2
TR3 88-26	7	18	13	25	1.3	4	14	312	6.86	321	5	ND	1	9	1	2	2	66	.23	.129	3	3	.59	13	.01	6	.80	.01	.25	2
TR3 88-27	4	27	10	17	1.1	2	8	306	6.78	110	5	ND	2	57	1	2	2	50	.42	.127	4	2	.39	12	.01	2	.81	.01	.27	5
TR3 88-28	7	15	7	44	.6	2	8	583	6.12	239	5	ND	2	9	1	2	3	94	.33	.172	3	2	1.23	34	.01	3	1.35	.01	.19	1
TR3 88-29	5	19	6	46	.8	2	9	608	7.20	231	5	ND	2	7	1	2	2	104	.26	.160	3	2	1.18	18	.01	3	1.33	.01	.16	3
TR4 88-1	3	20	14	95	.7	10	4	2318	8.01	39	5	ND	1	91	1	5	2	79	3.18	.149	5	7	1.75	50	.09	4	3.09	.01	.08	5
TR4 88-2	3	55	22	70	1.3	18	11	2966	9.30	92	5	ND	2	226	1	6	3	70	4.00	.085	9	17	1.03	113	.11	4	2.31	.01	.01	27
TR4 88-3	2	121	34	26	7.0	5	14	310	28.27	342	5	25	3	71	1	7	8	46	.47	.054	2	8	.07	5	.11	2	.47	.01	.03	76
TR4 88-4	2	84	20	23	5.7	2	5	266	16.99	166	5	26	2	70	1	3	6	48	.33	.044	3	10	.13	28	.04	2	.55	.01	.09	121
TR4 88-5	2	40	18	23	1.6	1	4	349	21.51	252	5	5	3	68	1	12	2	68	.56	.060	3	15	.09	32	.09	2	.63	.01	.02	20
TR4 88-6	21	26	23	14	2.5	1	2	404	12.75	167	5	ND	1	206	1	12	4	84	1.48	.041	3	8	.07	105	.12	2	.90	.01	.01	151
STD C	17	58	39	132	7.2	68	28	1045	3.98	40	21	6	36	47	17	18	19	55	.48	.087	38	55	.89	174	.06	36	1.95	.06	.14	12

TEUTON RESOURCES FILE # 88-2787R

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
TR4 88-7	71	36	24	17	4.2	1	2	330	16.29	170	5	ND	6	89	1	20	12	55	.63	.026	2	8	.11	78	.07	2	.40	.01	.01	566
TR4 88-8	45	68	35	39	3.6	1	6	1968	17.21	226	5	ND	5	116	1	29	10	74	.87	.047	3	10	.44	24	.06	2	.78	.01	.01	142
TR4 GRAB	59	50	29	16	3.7	1	4	262	18.17	142	5	5	5	78	1	24	11	58	.45	.019	2	10	.07	28	.06	2	.41	.01	.01	691
~~TK-001 GRAB~~	~~10~~	~~572~~	~~19~~	~~40~~	~~5.3~~	~~3~~	~~34~~	~~1614~~	~~21.52~~	~~167~~	~~5~~	~~2~~	~~5~~	~~71~~	~~1~~	~~7~~	~~5~~	~~58~~	~~4.03~~	~~.047~~	~~2~~	~~8~~	~~.05~~	~~9~~	~~.03~~	~~2~~	~~1.12~~	~~.01~~	~~.01~~	~~110~~
~~TK-002 FLOAT~~	~~8~~	~~120~~	~~15~~	~~15~~	~~2.1~~	~~5~~	~~15~~	~~193~~	~~13.38~~	~~112~~	~~5~~	~~7~~	~~3~~	~~35~~	~~1~~	~~3~~	~~2~~	~~21~~	~~.22~~	~~.041~~	~~2~~	~~13~~	~~.12~~	~~15~~	~~.04~~	~~3~~	~~.37~~	~~.01~~	~~.03~~	~~18~~
~~LIMO~~	~~10~~	~~2461~~	~~55~~	~~43~~	~~52.4~~	~~1~~	~~8~~	~~495~~	~~40.00~~	~~838~~	~~5~~	~~117~~	~~4~~	~~15~~	~~1~~	~~8~~	~~40~~	~~52~~	~~.12~~	~~.086~~	~~3~~	~~11~~	~~.05~~	~~70~~	~~.02~~	~~3~~	~~.46~~	~~.01~~	~~.09~~	~~11~~
STD C	17	57	37	132	7.1	66	28	1046	4.00	40	19	6	37	47	17	19	22	55	.48	.088	37	55	.90	173	.06	36	1.95	.06	.13	12

ACME ANAL[YTI]CAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOU[VER] B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1[716]

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK

DATE RECEIVED: AUG 9 1988 DATE REPORT MAILED: Aug 15/88 ASSAYER. ... D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES File # 88-3097R Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
~~TK-003~~	~~3~~	~~65~~	~~17~~	~~51~~	~~.8~~	~~24~~	~~13~~	~~813~~	~~5.09~~	~~213~~	~~5~~	~~ND~~	~~1~~	~~123~~	~~1~~	~~12~~	~~2~~	~~126~~	~~3.01~~	~~.257~~	~~9~~	~~62~~	~~1.92~~	~~59~~	~~.01~~	~~6~~	~~2.19~~	~~.01~~	~~.09~~	~~1~~
TK-004	9	694	125	4074	60.7	2	2	17408	3.23	1344	5	3	1	139	18	417	2	58	8.15	.005	9	5	2.26	69	.01	2	.07	.01	.01	1
TK-005	14	1459	69	23621	101.3	13	51	989	24.16	854	5	3	4	6	92	11	2	42	.03	.025	3	26	.63	4	.01	2	1.34	.01	.04	1
TR5 88-1	1	125	19	166	2.7	4	19	2994	6.37	661	5	ND	1	50	1	17	2	43	3.35	.124	10	3	.68	11	.01	7	.38	.01	.15	1
TR5 88-2	2	167	24	1376	7.8	3	17	1311	7.24	692	5	ND	1	20	6	14	2	36	.22	.138	7	4	.12	16	.01	4	.46	.01	.16	1
TR5 88-3	1	189	17	183	2.4	3	12	4714	5.28	408	5	ND	2	85	1	26	2	55	5.78	.039	9	4	1.49	33	.01	3	.35	.01	.15	1
TR5 88-4	1	517	21	180	5.6	3	14	1468	5.72	839	5	ND	2	27	1	50	2	33	1.69	.157	8	2	.35	28	.01	4	.42	.01	.19	1
TR5 88-5	1	707	19	142	6.3	4	16	2134	4.96	897	5	ND	1	27	1	46	2	49	1.66	.152	10	4	.65	29	.01	2	.79	.01	.19	1
TR5 88-6	6	314	29	185	6.5	2	12	3479	4.38	709	5	ND	2	92	1	26	2	39	6.70	.040	15	3	.84	27	.01	2	.81	.01	.09	1
TR5 88-7	9	399	44	155	9.8	3	16	1642	5.35	951	5	ND	1	64	1	43	2	38	2.14	.354	4	3	1.12	20	.01	2	.43	.01	.09	1
TR5 88-8	1	34	12	199	.9	6	18	2894	6.90	1352	5	ND	2	28	1	12	2	108	1.50	.152	9	12	2.11	22	.01	3	1.96	.01	.13	1
TR6 88-1	1	14	14	191	2.5	3	11	3359	4.69	526	5	ND	2	96	1	6	2	50	4.78	.115	7	2	1.28	41	.01	11	.52	.01	.18	1
TR6 88-2	1	93	21	31	3.7	3	18	525	5.98	661	5	2	1	20	1	21	2	15	.30	.111	5	2	.06	9	.01	3	.27	.01	.20	2
TR6 88-3	19	296	36	302	7.0	5	30	1530	7.14	1262	5	ND	1	25	1	79	2	29	1.16	.105	7	2	.24	14	.01	3	.32	.01	.18	1
TR6 88-4	2	505	321	177	5.9	2	24	2596	6.15	870	5	ND	1	14	1	47	3	35	.39	.150	10	3	.18	29	.01	9	.46	.01	.19	1
TR6 88-5	1	476	60	91	8.1	1	18	2597	6.19	1945	5	ND	3	17	1	92	2	26	.12	.168	8	2	.02	52	.01	5	.30	.01	.24	2
TR6 88-6	3	307	26	167	2.9	3	19	2714	6.65	1692	5	ND	1	31	1	31	2	32	1.41	.131	7	3	.34	42	.01	2	.45	.01	.15	1
TR6 88-7	1	31	9	219	.8	4	17	4277	5.86	1829	5	ND	2	59	1	13	2	59	4.77	.132	10	2	.70	32	.01	2	.49	.01	.15	1
TR6 88-8	1	27	9	303	.7	5	18	4742	5.52	726	5	ND	2	31	1	3	2	104	2.37	.141	15	6	1.89	113	.01	5	2.18	.01	.16	1
TR7 88-1	3	12	14	82	2.8	2	11	1522	6.24	1432	5	3	1	44	1	9	2	38	1.21	.165	6	3	.39	20	.01	7	.59	.01	.27	1
TR7 88-2	5	11	15	82	2.7	1	9	841	7.51	1169	5	2	2	42	1	16	2	31	.15	.165	4	2	.23	23	.01	3	.43	.01	.37	2
TR7 88-3	1	21	11	192	1.5	4	14	4631	6.25	659	5	ND	3	107	1	9	2	58	4.04	.142	11	2	1.28	36	.01	2	.52	.01	.20	1
TR8 88-1	6	20	8	51	.5	4	17	626	8.08	64	5	ND	1	11	1	2	2	134	.37	.197	6	4	1.19	35	.01	2	1.38	.02	.11	1
TR8 88-2	10	12	12	12	1.5	2	11	111	6.75	60	5	ND	2	11	1	2	5	48	.08	.064	3	2	.12	26	.01	2	.31	.03	.17	2
TR8 88-3	1	20	7	59	.8	5	20	1153	5.21	72	5	ND	1	13	1	2	2	123	.53	.193	9	5	1.48	173	.01	3	1.81	.02	.14	1
TR8 88-4	3	13	7	63	.3	3	12	938	6.19	34	5	ND	1	23	1	2	2	107	.45	.177	5	3	1.75	106	.01	2	1.88	.02	.09	1
TR8 88-5	10	18	7	49	.6	2	13	699	7.69	58	5	ND	1	10	1	2	2	107	.35	.200	4	3	1.30	29	.01	2	1.42	.02	.10	3
TR8 88-6	1	57	8	69	.7	4	19	1282	4.52	55	5	ND	1	15	1	2	2	108	.41	.168	6	3	1.93	228	.01	4	2.12	.02	.10	1
TR8 88-7	2	67	9	61	.5	3	15	1012	4.98	75	5	ND	1	12	1	2	2	116	.34	.154	4	3	1.70	94	.01	2	1.84	.02	.10	2
TR8 88-8	2	27	20	69	.7	2	12	576	6.95	70	5	ND	1	16	1	2	2	99	.38	.166	5	2	1.44	73	.01	5	1.60	.01	.12	2
TR8 88-9	1	76	6	56	.5	6	13	776	4.54	37	5	ND	1	13	1	2	3	124	.54	.158	7	5	1.78	93	.01	2	1.68	.02	.09	1
TR8 88-10	1	116	8	79	.7	71	30	1479	6.20	23	5	ND	1	40	1	3	2	138	1.18	.073	9	90	3.21	82	.07	2	3.09	.02	.08	1
TR8 88-11	1	185	7	71	.8	18	18	1154	5.07	34	5	ND	1	13	1	2	2	133	.42	.160	6	27	2.11	45	.01	3	2.19	.02	.06	1
TR8 88-12	1	193	9	98	.5	40	24	1331	5.72	31	5	ND	1	13	1	4	2	152	.34	.121	7	60	2.92	88	.01	2	2.90	.02	.06	1
TR8 88-13	1	166	7	48	.6	3	11	974	5.00	32	5	ND	1	31	1	2	2	121	.46	.188	6	3	1.60	238	.01	2	1.60	.02	.08	3
TR8 88-14	3	66	13	45	1.7	3	7	576	8.91	88	5	ND	1	13	1	2	2	124	.25	.159	4	3	1.25	52	.01	2	1.25	.03	.13	2
STD C	17	57	36	132	7.2	67	28	1049	4.00	42	17	6	36	47	17	17	20	55	.48	.099	38	55	.90	174	.06	37	1.94	.06	.14	11

- ASSAY REQUIRED FOR CORRECT RESUL[T] for Cu Zn >10,000 ppm

TEUTON RESOURCES FILE # 88-3097R

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
TR8 88-15	2	54	6	45	.6	2	7	611	6.44	54	5	ND	3	15	1	2	2	110	.43	.180	4	3	1.21	98	.01	2	1.25	.02	.12	2
TR10 88-1	38	101	38	52	7.2	10	8	1181	4.30	187	5	ND	3	56	1	15	2	9	2.50	.057	6	3	.09	20	.01	2	.28	.01	.21	3
TR10 88-2	2	28	10	67	2.6	12	6	1904	6.49	87	5	ND	4	79	1	3	2	29	3.44	.126	8	9	.81	12	.01	2	.91	.01	.19	2
TR10 88-3	1	62	14	153	.8	28	18	2290	8.24	27	5	ND	3	76	1	2	2	103	3.30	.167	15	18	2.10	30	.01	2	2.95	.01	.18	1
TR10 88-4	1	35	12	121	.7	23	14	2177	7.12	71	5	ND	3	66	1	2	2	74	2.77	.137	15	20	1.71	32	.01	2	2.40	.01	.18	1
TR10 88-5	1	7	8	127	.3	14	5	2179	5.88	36	5	ND	4	32	1	2	2	51	1.02	.106	10	22	1.76	40	.01	3	2.22	.01	.14	1
TR11 88-1	14	73	45	35	17.6	12	46	1043	15.00	167	5	ND	4	37	1	6	2	37	1.89	.036	6	3	.14	6	.01	2	.27	.01	.18	3
TR11 88-2	1	14	7	61	2.6	11	15	1784	5.30	68	5	ND	3	67	1	2	2	23	3.08	.038	5	12	.62	7	.01	5	.76	.01	.15	2
TR11 88-3	44	717	63	225	85.6	9	24	1069	9.70	237	5	ND	3	45	2	182	2	170	2.21	.024	3	4	.05	7	.01	2	.18	.01	.15	3
TR11 88-4	2	10	15	29	1.2	10	31	871	5.29	154	5	ND	3	26	1	2	2	10	1.33	.031	7	4	.15	11	.01	4	.40	.01	.20	3
TR11 88-5	5	11	24	13	1.6	16	29	878	7.14	116	5	ND	4	45	1	2	3	5	2.22	.059	6	4	.04	7	.01	3	.20	.01	.15	2
TR11 88-6	3	8	23	80	1.1	16	23	1662	9.12	44	5	ND	4	50	1	2	2	34	2.55	.087	8	12	1.00	9	.01	2	1.11	.01	.13	2
TR11 88-7	6	11	58	69	2.5	15	42	1172	15.86	93	5	ND	5	33	1	2	3	26	1.42	.068	6	11	.76	4	.01	2	1.00	.01	.14	2
TR11 88-8	4	35	67	153	4.5	7	24	2575	15.51	264	5	ND	6	49	1	2	4	51	1.71	.066	35	6	1.79	11	.01	2	2.53	.01	.14	1
TR11 88-9	1	24	4	97	.2	15	8	2184	3.34	9	5	ND	2	100	1	2	2	31	4.96	.089	13	14	1.40	50	.01	3	1.85	.01	.15	1
TR11 88-10	1	17	8	89	.8	17	9	2660	3.30	39	5	ND	2	158	1	2	2	42	6.94	.096	13	13	1.44	222	.01	6	1.54	.01	.16	2
TR12 88-1	1	6	11	133	.9	21	7	2220	9.06	20	5	ND	5	49	1	2	2	52	1.91	.135	8	20	2.09	9	.01	3	2.36	.01	.14	1
TR12 88-2	30	104	121	120	14.4	8	17	1443	15.73	376	5	4	4	44	1	9	16	53	1.95	.043	4	5	.45	5	.01	4	.56	.01	.13	2
TR12 88-3	5	17	26	61	3.4	13	9	674	5.20	139	5	ND	1	9	1	2	2	138	.15	.051	4	11	.51	13	.01	2	.65	.01	.13	2
TR12 88-4	2	7	9	31	1.7	15	19	1106	6.09	63	5	ND	3	59	1	2	2	13	2.34	.052	5	9	.33	17	.01	3	.41	.01	.13	3
TR12 88-5	42	61	122	42	9.5	8	22	1374	15.16	229	5	2	4	57	1	4	12	75	2.47	.025	4	4	.10	4	.01	2	.18	.01	.12	4
TR12 88-6	3	25	10	41	3.2	10	5	699	3.86	58	5	ND	2	24	1	2	2	27	.88	.027	3	8	.25	21	.01	2	.37	.01	.12	4
TR13 88-1	1	8	7	70	.6	25	10	1720	5.84	30	5	ND	4	72	1	2	2	19	2.93	.071	4	12	.99	19	.01	5	1.20	.01	.16	13
TR13 88-2	1	10	11	51	.8	20	15	1799	8.19	46	5	2	4	82	1	2	2	19	3.21	.101	5	8	.73	12	.01	2	.89	.01	.23	24
TR13 88-3	2	120	15	39	1.3	15	16	865	8.87	141	5	ND	3	35	1	2	2	12	1.56	.061	3	7	.21	6	.01	2	.35	.01	.17	6
TR13 88-4	1	8	12	34	.8	12	11	1313	5.73	154	5	2	3	47	1	2	2	16	2.34	.046	4	8	.24	10	.01	2	.19	.01	.13	5
TR13 88-5	1	56	15	55	1.5	14	11	1786	8.12	150	5	ND	4	53	1	2	2	14	2.46	.040	4	6	.68	9	.01	4	.64	.01	.20	3
TR13 88-6	1	22	12	23	.5	15	14	782	5.38	84	5	ND	3	32	1	2	2	8	1.39	.049	3	8	.25	9	.01	2	.34	.02	.13	4
TR13 88-7	1	55	15	68	1.1	30	25	1893	6.41	194	5	ND	2	76	1	2	2	9	3.83	.055	4	6	.19	15	.01	2	.34	.01	.17	3
TR13 88-8	2	77	15	64	1.4	38	31	1516	7.19	246	5	ND	4	49	1	3	2	14	2.68	.069	4	7	.37	15	.01	2	.57	.01	.20	3
TR13 88-9	7	166	25	52	1.8	38	18	1416	6.29	394	5	ND	3	50	1	7	2	8	2.70	.051	4	5	.04	14	.01	7	.20	.01	.16	4
TR13 88-10	14	198	18	88	1.5	13	8	1534	4.72	369	5	ND	2	70	1	7	2	16	3.29	.044	3	7	.13	18	.01	2	.21	.02	.12	4
TR13 88-11	42	162	22	257	1.8	11	9	1689	3.76	288	5	ND	2	77	1	7	2	11	3.23	.046	2	6	.13	23	.01	3	.23	.01	.13	4
TR14 88-1	8	128	26	192	3.7	3	5	702	5.36	60	5	ND	2	61	1	2	2	21	.38	.095	6	3	.24	13	.01	4	.46	.01	.15	4
TR14 88-2	20	10905	94	62	58.6	1	21	42	17.55	305	5	ND	3	4	1	39	21	4	.11	.026	3	2	.01	3	.01	2	.09	.01	.10	4
TR14 88-3	1	103	9	254	1.8	4	11	2620	4.48	35	5	ND	3	16	2	2	2	69	.44	.125	9	11	1.12	68	.01	5	1.56	.01	.16	3
STD C	17	58	36	132	7.2	67	28	1050	4.02	39	18	7	37	48	17	19	20	56	.48	.089	39	56	.89	174	.06	37	1.96	.06	.13	12

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
TR15 88-1	1	6	13	47	.3	12	17	1414	6.08	20	5	ND	1	53	1	2	2	7	2.06	.048	3	2	1.05	7	.01	6	.29	.01	.18	1
TR15 88-2	30	23	62	35	3.6	4	20	474	15.31	97	5	ND	1	9	1	2	9	3	.44	.014	2	1	.16	2	.01	4	.14	.01	.09	1
TR15 88-3	6	4066	61	56	12.7	5	30	1047	16.34	479	5	ND	1	15	1	6	13	8	.84	.010	2	2	.43	2	.01	5	.25	.01	.10	1
TR15 88-4	5	3576	28	39	1.1	17	10	1416	5.67	172	5	ND	1	58	1	6	11	6	1.89	.042	2	4	.57	8	.01	3	.22	.01	.13	2
TR15 88-5	1	50	80	54	6.5	14	10	629	11.88	161	5	3	1	12	1	2	18	15	.59	.029	2	4	.32	4	.01	5	.22	.01	.12	1
TR15 88-6	4	39	29	57	1.6	28	20	1228	10.39	217	5	ND	2	22	1	3	5	20	.84	.037	2	7	.57	6	.01	2	.58	.01	.13	1
STD C	17	57	38	128	7.2	67	29	1074	4.04	39	19	7	36	47	17	17	20	56	.49	.089	38	55	.90	179	.06	36	1.98	.06	.14	12

ACME ANAL[illegible]CAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUV[illegible] B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-17[illegible]

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: AUG 17 1988 DATE REPORT MAILED: Aug 25/88 ASSAYER. C. Leong ...D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES File # 88-3689

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM
TR9 88-1	4	91	23	22	5.0	1	3	458	21.96	233	5	8	4	67	1	26
TR9 88-2	4	58	24	39	3.2	3	6	1068	18.51	161	5	2	4	90	1	16
TR9 88-3	4	130	34	29	4.5	1	3	227	32.31	244	5	5	6	10	1	9
TR9 88-4	3	122	37	30	5.7	1	5	352	30.47	267	5	ND	6	4	1	2
TR9 88-5	2	120	11	67	5.8	17	9	1007	4.00	44	5	ND	4	14	1	13
TR9 88-6	4	125	28	80	1.7	6	7	1653	12.35	100	5	ND	4	14	1	5
TR9 88-7	3	74	13	62	3.1	7	15	2827	15.42	79	5	2	4	106	1	5
TR9 88-8	9	90	11	33	2.8	3	12	1577	18.13	179	5	2	3	120	1	6
TR9 88-9	7	240	19	35	2.2	2	6	494	20.47	356	5	4	5	14	1	4
TR9 88-10	8	16	16	41	.9	3	9	572	6.08	109	5	ND	2	14	1	2
TR9 88-11	2	16	12	52	1.2	3	10	557	7.53	107	5	ND	2	9	1	2
TR9 88-12	9	18	14	33	7.8	2	8	521	5.53	147	5	ND	1	8	1	2
TR9 88-13	5	27	8	41	1.3	3	14	518	7.89	192	5	ND	2	8	1	2
TR9 88-14	1	14	6	59	.6	2	5	768	5.28	23	5	ND	2	9	2	2
TR9 88-15	1	16	32	83	.7	3	9	732	5.96	76	5	ND	2	10	1	2
TR9 88-16	1	17	5	54	.7	2	9	432	5.06	117	5	ND	2	11	2	2
TR9 88-17	4	9	12	57	.6	4	12	658	5.78	104	5	ND	2	18	2	2
TR9 88-18	1	25	6	58	.3	4	13	758	4.72	89	5	ND	1	14	1	2
TR9 88-19	1	50	11	58	.3	12	31	891	6.61	51	5	ND	2	44	1	2
STD C/AU-R	18	57	37	131	7.1	67	28	963	4.12	40	17	8	36	47	16	17

SAMPLE#	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
TR9 88-1	13	79	.62	.043	3	3	.08	61	.09	16	.54	.01	.03	197	8890
TR9 88-2	5	56	.74	.046	2	18	.71	39	.07	10	.97	.01	.01	63	1275
TR9 88-3	12	54	.07	.055	2	7	.06	79	.02	19	.33	.01	.06	146	4840
TR9 88-4	4	47	.04	.063	3	10	.14	50	.01	8	.47	.01	.13	42	1890
TR9 88-5	2	44	.20	.101	7	22	.87	299	.01	9	1.46	.01	.19	1	365
TR9 88-6	2	51	.40	.114	20	25	1.49	165	.01	4	2.90	.01	.67	2	875
TR9 88-7	4	39	4.68	.065	6	16	1.39	14	.02	4	1.77	.01	.11	141	2240
TR9 88-8	7	26	3.45	.049	6	12	.59	16	.03	6	.73	.01	.07	223	2240
TR9 88-9	13	35	.09	.089	3	10	.05	417	.01	13	.46	.01	.17	4	4250
TR9 88-10	2	76	.28	.187	4	15	.99	105	.01	4	1.23	.01	.55	3	225
TR9 88-11	2	94	.32	.207	4	11	1.04	17	.01	3	1.20	.01	.17	1	230
TR9 88-12	2	235	.36	.212	3	12	1.10	56	.01	20	1.23	.01	.33	1	790
TR9 88-13	3	90	.30	.179	5	11	1.12	16	.01	5	1.27	.02	.18	1	545
TR9 88-14	3	105	.37	.228	4	10	1.71	102	.01	12	1.73	.02	.16	1	60
TR9 88-15	2	96	.40	.239	6	8	1.47	44	.01	7	1.67	.02	.19	1	225
TR9 88-16	2	82	.40	.196	6	8	.59	86	.01	5	1.29	.02	.19	1	176
TR9 88-17	3	109	.92	.230	7	12	1.46	59	.01	4	1.63	.02	.13	1	82
TR9 88-18	3	115	.51	.233	5	13	1.63	90	.01	6	1.80	.03	.13	1	99
TR9 88-19	2	133	.88	.186	7	22	2.09	70	.01	2	2.22	.02	.10	1	65
STD C/AU-R	17	56	.47	.095	39	60	.90	173	.06	33	1.94	.06	.15	11	520

ACME ANALY AL LABORATORIES LTD.   852 E. HASTINGS ST. VANCOUVE B.C.   V6A 1R6   PHONE(604)253-3158   FAX(604)253-171

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK

DATE RECEIVED: AUG 11 1988   DATE REPORT MAILED: Aug 27/88   ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES   File # 88-3501R   Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
L125S 0W	1	5	24	107	.1	4	14	1429	6.08	545	5	ND	2	17	1	2	3	129	.49	.146	8	5	1.62	20	.15	2	1.53	.02	.17	1
L150S 40W	1	7	18	88	.1	4	8	1235	2.73	58	5	ND	2	29	1	2	2	35	1.32	.112	10	6	.71	336	.05	8	1.39	.01	.34	1
L150S 35W	1	20	34	123	.1	8	9	1797	4.30	156	5	ND	1	30	1	2	5	46	.40	.111	16	6	1.02	58	.06	3	1.73	.01	.30	1
L150S 30W	6	13	14	46	.2	3	10	445	4.02	348	5	ND	3	29	1	2	2	39	.13	.150	5	6	.39	278	.10	2	.89	.01	.31	2
L150S 25W	2	16	23	41	.2	5	7	458	4.05	386	5	ND	3	31	1	3	5	25	.11	.110	4	7	.25	457	.11	3	.65	.01	.29	2
L150S 20W	1	7	38	94	.2	5	8	1464	3.54	239	5	ND	2	45	1	3	2	48	.40	.104	7	8	.82	205	.07	2	1.58	.01	.29	1
L150S 15W	1	29	41	160	.3	8	17	2286	4.62	55	5	ND	2	86	1	2	4	81	.58	.128	9	13	1.31	1285	.10	2	2.23	.01	.30	3
L150S 10W	1	6	20	80	.1	5	10	1053	5.50	484	5	ND	2	14	1	2	2	53	.22	.132	5	10	.81	14	.07	8	1.10	.01	.30	2
L150S 5W	1	7	12	131	.1	6	16	2243	3.23	45	5	ND	2	39	1	2	2	59	.46	.104	7	7	1.11	511	.09	2	2.01	.01	.30	2
L150S 0W	1	17	17	96	.1	1	14	1175	5.76	205	5	ND	2	13	1	3	3	69	.29	.166	7	9	1.02	49	.16	2	1.36	.01	.28	3
L175S 80W	2	29	64	81	.7	6	3	213	1.61	170	5	ND	3	7	1	3	2	5	.04	.033	6	9	.05	248	.01	2	.41	.01	.18	1
L175S 75W	1	13	36	136	.4	11	4	589	1.23	74	5	ND	3	8	1	2	2	14	.10	.030	6	21	.32	147	.01	5	.52	.03	.12	1
L175S 70W	4	32	30	97	2.6	5	12	1940	5.29	336	6	2	5	20	1	4	2	13	.13	.128	8	3	.06	663	.02	2	.46	.01	.22	1
L175S 65W	2	12	56	111	.6	3	5	414	4.23	210	5	ND	2	40	1	2	2	23	.13	.099	6	10	.45	23	.01	2	.92	.01	.22	1
L175S 60W	1	11	17	80	.1	3	9	1572	3.89	55	5	ND	1	62	1	2	3	48	2.73	.105	17	4	1.20	212	.01	2	1.74	.02	.15	1
L175S 55W	1	6	6	116	.1	1	6	2242	4.68	21	5	ND	1	110	1	2	4	43	11.19	.065	6	2	1.38	787	.01	4	.37	.01	.11	1
L175S 50W	2	15	16	28	1.1	1	9	953	5.15	170	5	ND	1	8	1	2	2	30	.24	.131	8	3	.29	75	.01	4	.87	.01	.27	1
L175S 45W	3	76	14	77	.5	3	20	1822	5.68	133	5	ND	5	32	1	2	2	30	.22	.135	7	5	.41	728	.01	2	1.06	.01	.23	1
L175S 40W	1	17	9	80	.1	1	8	1839	3.42	120	5	ND	1	44	1	2	5	34	1.41	.121	11	1	.94	103	.01	4	1.57	.01	.23	1
L175S 35W	1	34	8	89	.1	3	8	2244	3.10	152	5	ND	1	21	1	2	2	32	.39	.120	16	3	.84	518	.01	7	1.44	.01	.24	1
TK 006	14	55	726	205	3.2	1	10	213	27.40	524	5	2	4	10	1	8	5	21	.02	.268	10	1	.04	116	.01	2	.42	.01	.21	1
TR13 88-12	2	28	19	34	.4	17	27	1971	11.30	112	5	ND	1	59	1	2	6	14	2.99	.056	4	4	.40	4	.01	2	.53	.01	.24	3
TR13 88-13	1	36	20	79	.3	21	26	1319	8.63	86	5	ND	1	51	1	2	2	20	1.83	.088	4	8	.78	4	.01	2	.87	.01	.18	1
TR13 88-14	1	118	107	348	2.5	24	46	733	10.41	174	5	2	2	18	3	3	2	7	.74	.094	3	4	.19	4	.01	2	.52	.01	.25	1
TR13 88-15	8	107	345	539	1.5	12	11	769	4.46	204	5	ND	3	11	5	6	2	11	.34	.033	4	5	.26	14	.01	3	.46	.01	.17	1
TR13 88-16	5	215	38	86	2.9	25	23	2107	5.83	250	5	ND	1	39	1	4	2	16	1.71	.106	6	5	.54	17	.01	2	.90	.01	.29	1
TR13 88-17	6	124	30	59	2.0	15	15	2428	4.12	211	5	ND	1	47	1	3	2	13	2.73	.061	6	4	.58	14	.01	5	.55	.01	.22	1
TR16 88-1	43	111	152	128	18.1	2	8	129	9.69	194	5	ND	1	7	1	10	2	10	.02	.043	6	1	.02	16	.01	2	.27	.01	.19	3
TR16 88-2	6	75	138	62	10.2	2	6	161	7.51	109	5	ND	1	36	1	2	2	16	.01	.040	3	2	.04	18	.01	2	.24	.01	.19	2
TR16 88-3	2	87	74	36	8.4	1	14	365	8.46	98	5	ND	3	25	1	2	6	43	.37	.101	4	3	.10	33	.01	2	.36	.01	.29	4
TR16 88-4	2	127	26	32	2.1	3	18	563	6.98	107	5	ND	1	45	1	2	2	43	.97	.122	7	3	.16	19	.01	2	.43	.01	.36	2
TR16 88-5	1	118	46	60	2.5	1	13	556	11.37	127	5	ND	3	8	1	2	4	62	.13	.110	3	3	.39	7	.01	2	.80	.01	.22	2
TR16 88-6	1	182	36	83	1.2	1	10	871	11.22	64	5	ND	4	10	1	2	3	77	.15	.136	5	4	.62	13	.01	2	1.04	.01	.20	2
TR17 88-1	1	93	24	57	2.9	5	18	928	6.12	81	5	ND	1	50	1	2	2	51	1.40	.130	9	5	.44	8	.01	11	.81	.01	.25	1
TR17 88-2	9	849	77	140	6.2	4	11	300	6.72	155	5	ND	2	30	1	7	4	29	.38	.097	5	2	.18	4	.01	2	.42	.01	.18	2
TR17 88-3	10	4776	201	1378	44.3	2	12	56	14.30	344	5	ND	2	24	10	37	5	12	.10	.029	2	6	.01	3	.01	2	.15	.01	.12	5
STD C	18	58	37	132	7.2	67	28	1070	4.05	37	21	8	37	48	18	17	19	58	.45	.088	39	54	.89	178	.06	36	1.93	.06	.13	12

TEUTON RESOURCES FILE # 88-3501R

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
TR18 88-1	5	6	11	9	1.4	8	5	61	4.62	88	5	ND	2	17	1	6	8	16	.02	.029	9	5	.03	25	.01	2	.19	.01	.29	3
TR18 88-2	127	77	273	18	14.8	2	9	55	29.60	1261	5	4	1	6	1	18	100	15	.01	.045	2	1	.01	15	.01	2	.16	.02	11.04	1
TR18 88-3	2	36	17	27	1.5	8	2	179	4.01	60	6	ND	2	6	1	2	2	33	.02	.040	4	11	.29	48	.01	3	.42	.02	.12	3
TR18 88-4	2	48	26	88	1.3	16	7	910	4.73	41	5	4	3	52	1	2	2	74	.50	.290	10	19	1.15	157	.01	4	1.41	.01	.21	2
TR18 88-5	1	58	4	109	.3	22	5	1573	3.30	18	5	ND	2	28	1	3	2	112	.50	.149	11	25	1.43	62	.01	4	1.90	.01	.17	1
TR19 88-1	3	12	168	7	4.3	1	2	24	3.74	42	7	ND	2	6	1	9	4	10	.01	.005	7	3	.02	181	.01	4	.24	.01	.28	2
TR19 88-2	28	103	1380	45	37.3	1	8	402	24.69	381	5	27	2	4	1	103	40	23	.01	.049	3	2	.01	96	.01	2	.34	.01	.27	3
TR19 88-3	21	83	157	15	11.8	1	5	39	10.47	189	5	ND	2	6	1	20	2	31	.01	.024	3	4	.01	257	.01	6	.22	.01	.13	2
TR19 88-4	24	165	73	18	13.9	1	8	25	16.19	75	5	ND	2	11	1	28	3	17	.01	.028	35	13	.01	93	.01	6	.20	.01	.15	3
TR19 88-5	1	40	12	12	2.0	2	4	486	5.61	43	5	ND	2	12	1	5	3	6	.01	.050	9	4	.02	513	.01	8	.27	.01	.21	1
TR19 88-6	2	41	53	15	4.4	3	3	74	4.39	51	5	ND	2	14	1	4	4	8	.01	.048	22	5	.03	522	.01	3	.31	.01	.21	4
TR20 88-1	5	192	70	280	1.0	38	54	4001	9.65	455	5	ND	4	19	1	17	2	69	.09	.078	13	41	.39	839	.01	8	1.74	.01	.28	1
TR20 88-2	1	74	27	132	.7	30	23	2507	8.64	175	5	ND	2	31	1	11	2	49	2.04	.095	11	28	.55	86	.01	6	1.07	.01	.26	1
TR20 88-3	7	42	23	31	.5	2	5	317	5.69	110	5	ND	1	14	1	12	2	5	.01	.034	6	4	.02	401	.01	4	.30	.01	.20	2
TR29 88-4	9	41	16	24	.7	4	4	201	4.00	84	5	ND	1	11	1	11	2	6	.01	.037	7	5	.01	505	.01	2	.24	.01	.15	2
TR29 88-5	83	93	867	21	22.8	4	6	102	14.46	157	5	2	1	8	1	55	7	5	.01	.011	16	4	.01	54	.01	9	.26	.01	.59	1
TR29 88-6	40	82	27	18	25.2	3	12	18	18.08	178	5	3	2	4	1	12	9	4	.01	.002	8	2	.01	55	.01	2	.24	.01	.16	4
TR29 88-7	16	22	53	10	26.0	1	3	29	6.69	71	5	2	1	66	1	14	8	6	.01	.009	10	4	.01	49	.01	11	.16	.01	.44	1
TR29 88-8	36	280	45	22	9.9	1	10	29	19.71	358	5	4	3	10	1	80	23	9	.01	.052	9	2	.01	134	.01	2	.28	.01	.22	2
TR29 88-9	33	98	88	11	11.9	1	5	27	13.83	274	5	5	1	27	1	46	12	20	.01	.043	9	1	.01	53	.01	2	.15	.01	.52	1
TR29 88-10	1	29	4	17	2.9	1	3	71	4.19	116	7	ND	2	18	1	2	2	6	.01	.042	4	3	.02	353	.01	6	.26	.01	.25	2
STD C	18	61	38	132	6.7	73	29	1069	4.13	42	16	8	36	49	18	17	20	59	.47	.092	40	56	.93	181	.07	36	2.05	.06	.15	12

TR20 not 29

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: AUG 30 1988 DATE REPORT MAILED: Sept 6/88 ASSAYER..C. Leong..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES File # 88-4036

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
KG-001	8	5757	68	505	2.0	6	13	1922	3.77	118	5	ND	1	77	3	4	2	65	.91	.093	12	4	.95	246	.17	14	1.89	.03	.11	2	590
KG-003	4	12251	157	56	23.2	2	4	186	2.10	352	5	ND	1	212	1	33	2	5	.35	.034	5	1	.05	61	.01	4	.26	.01	.13	2	78
TR-31-88-13	1	299	5	60	.8	7	17	1365	4.89	13	5	ND	1	84	1	4	2	154	3.14	.143	8	8	1.42	147	.02	9	2.43	.01	.25	1	137
TR-31-88-14	1	287	6	76	.5	8	7	1456	4.64	14	5	ND	1	24	1	3	2	118	1.02	.169	8	10	1.95	247	.01	3	2.52	.02	.13	1	93
TR-31-88-15	1	251	8	68	.7	8	10	1403	4.55	3	5	ND	1	21	1	4	2	105	1.00	.156	9	8	1.93	216	.01	4	2.55	.01	.19	1	120
TR-31-88-16	1	41	8	60	.4	7	9	1351	4.46	18	5	ND	1	24	1	3	2	93	.94	.149	8	6	1.91	213	.01	7	2.55	.01	.19	1	25
TR-31-88-17	1	176	10	65	.7	7	11	1279	4.86	37	5	ND	1	13	1	5	2	105	.52	.163	7	7	2.12	344	.01	3	2.77	.01	.19	1	129
TR-31-88-18	1	29	8	69	.4	6	11	1212	4.97	11	5	ND	1	17	1	3	2	103	.68	.158	7	6	2.17	438	.01	4	2.91	.01	.18	1	56
TR-32-88-1	4	205	85	146	1.7	10	31	2213	9.89	63	8	ND	1	30	1	4	2	464	.86	.165	5	18	2.77	46	.13	2	4.45	.01	.07	2	118
TR-32-88-2	1	266	25	81	1.2	8	17	1303	5.04	17	5	ND	1	62	1	4	2	172	1.46	.144	4	11	1.67	39	.08	4	2.44	.02	.05	1	330
TR-32-88-3	3	269	38	123	1.8	11	23	1776	7.89	56	5	ND	1	78	1	2	2	377	1.13	.158	5	18	2.58	23	.15	3	3.84	.01	.03	3	89
TR-32-88-4	2	73	12	72	1.0	5	10	1816	5.43	25	5	ND	1	154	1	7	2	68	4.78	.096	4	7	1.72	20	.06	10	2.58	.01	.07	3	116
TR-32-88-5	2	49	19	95	.7	4	2	2012	4.66	18	5	ND	1	215	1	5	2	71	7.95	.089	4	7	1.67	6	.07	2	2.65	.01	.04	3	62
TR-32-88-6	1	292	42	132	3.3	3	2	2588	7.85	61	5	ND	1	168	1	7	2	95	6.08	.108	7	11	1.98	52	.05	8	3.32	.01	.08	4	565
TR-32-88-7	2	879	46	117	7.3	5	5	2593	11.13	99	5	2	1	145	1	6	2	79	8.34	.067	5	12	1.43	33	.03	2	2.40	.01	.05	44	3740
TR-32-88-8	3	2072	31	138	11.5	4	20	2384	15.50	171	5	2	1	48	1	5	2	44	5.48	.032	3	12	1.33	12	.01	2	1.84	.01	.02	58	2430
TR-32-88-9	2	2181	25	125	11.8	6	11	2867	11.02	151	5	2	1	85	2	8	3	40	4.82	.037	7	14	1.31	30	.02	2	1.87	.01	.03	43	2215
TR-32-88-10	1	5840	17	146	22.0	3	11	3202	10.54	251	5	5	1	86	3	6	2	36	8.12	.029	3	11	1.31	20	.02	3	1.56	.01	.01	20	6280
TR-32-88-11	2	9693	27	183	51.1	7	13	2547	12.50	238	5	5	2	88	3	2	3	43	5.81	.059	8	16	1.48	19	.04	3	2.13	.01	.03	63	6820
TR-32-88-12	1	3028	43	511	21.8	5	7	3510	13.83	180	5	3	3	73	8	7	2	54	5.87	.062	9	18	2.08	30	.05	2	3.16	.01	.02	42	4615
TR-32-88-13	2	5564	29	247	22.6	9	5	4515	11.32	88	5	ND	1	99	2	7	2	85	2.88	.080	10	19	3.27	100	.06	2	4.61	.01	.04	8	280
TR-32-88-14	1	1311	20	119	7.7	10	3	2410	6.28	43	5	ND	1	189	1	8	2	49	7.88	.086	6	13	1.50	31	.05	2	2.51	.01	.06	9	275
TR-32-88-15	5	3735	32	151	28.9	10	8	4284	15.56	122	8	4	1	98	2	2	5	83	1.53	.074	19	20	1.95	140	.05	2	3.44	.01	.06	24	7390
TR-32-88-16	3	1447	14	91	4.7	12	4	2555	6.45	49	5	ND	1	173	1	5	2	63	3.22	.094	7	13	1.74	149	.08	2	2.92	.01	.06	12	151
TR-32-88-17	1	68	6	43	1.4	25	2	994	2.72	9	5	ND	1	58	1	2	2	52	.82	.097	9	24	.84	145	.08	3	1.29	.01	.11	1	340
TR-32-88-18	2	64	6	57	2.0	26	4	1127	3.15	8	5	ND	1	30	1	2	2	74	.44	.096	10	29	1.13	398	.03	2	1.52	.01	.11	1	565
TR-32-88-19	1	37	9	59	1.1	21	3	1381	3.98	16	5	ND	1	65	1	3	2	70	.93	.107	10	25	1.13	238	.03	2	1.85	.01	.10	1	230
TR-32-88-20	1	18	9	57	1.3	23	4	1329	3.04	11	5	ND	1	12	1	2	2	62	.30	.097	10	28	.97	212	.01	3	1.43	.01	.14	1	470
TR-32-88-21	3	489	31	48	5.8	6	18	847	25.88	210	6	3	1	40	1	2	8	52	.37	.063	5	15	.51	10	.01	2	1.61	.01	.11	9	6810
TR-32-88-22	2	273	25	83	2.4	5	16	3073	13.62	81	5	ND	1	79	1	5	3	75	2.41	.082	9	15	1.95	16	.04	2	3.25	.01	.04	13	1825
TR-32-88-23	2	143	25	50	2.7	7	11	1963	12.03	134	5	2	1	167	1	8	5	64	1.81	.063	8	15	.93	22	.07	2	1.97	.01	.05	8	1810
TR-32-88-24	4	76	20	69	1.2	11	3	2110	7.03	45	5	ND	1	86	1	6	2	83	2.96	.111	8	18	1.45	43	.10	3	2.66	.01	.10	4	230
TR-33-88-1	7	246	16	56	3.1	5	25	2098	10.35	91	5	ND	1	129	1	5	2	70	3.94	.078	5	8	1.37	13	.06	2	1.98	.01	.04	8	1125
TR-33-88-2	23	182	17	16	17.9	1	6	258	17.77	178	9	10	1	69	1	4	30	177	.55	.064	2	4	.17	29	.16	2	.61	.01	.05	50	18120
TR-33-88-3	16	201	12	20	5.9	1	6	399	10.86	97	8	ND	1	76	1	5	10	95	.63	.050	2	4	.32	31	.11	2	.88	.01	.10	108	6440
TR-33-88-4	15	204	21	40	5.8	7	12	554	16.35	164	8	ND	1	24	1	2	10	85	.24	.054	4	11	.50	14	.04	2	.94	.01	.08	32	5630
TR-33-88-5	9	327	16	31	3.6	2	5	476	14.38	96	8	ND	2	34	1	2	5	73	.27	.079	7	10	.32	69	.03	2	.95	.01	.16	28	1725
STD C/AU-R	19	52	42	132	7.4	73	30	1123	4.03	43	24	8	36	53	19	18	21	64	.51	.087	40	61	.33	180	.07	41	2.03	.06	.14	13	475

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

TR 21 22 30 31 9 EXT 1, EXT 2 P. 6-7

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P5 SOIL P6-P8 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: AUG 31 1988 DATE REPORT MAILED: Sept 9/88 ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES File # 88-4109 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
GT 1+40N	7	134	172	153	5.0	7	11	1365	8.53	614	5	ND	2	13	2	6	2	38	.02	.139	15	8	.40	236	.01	4	.91	.01	.15	1	1465
GT 1+20N	7	143	137	159	3.6	9	15	1769	9.53	689	5	ND	2	13	2	5	2	39	.02	.142	17	3	.44	275	.01	10	1.02	.01	.17	1	1055
GT 1+00N	5	143	92	259	2.9	16	21	2322	7.34	439	5	ND	3	15	3	4	2	41	.08	.114	19	11	.58	407	.01	7	1.31	.02	.15	1	775
GT 0+80N	8	224	199	193	3.7	12	36	3754	5.37	1860	5	ND	2	14	3	28	2	48	.06	.154	21	6	.52	313	.01	7	1.39	.01	.16	1	1385
GT 0+60N	14	409	100	309	7.0	47	34	5624	10.05	2261	5	ND	4	24	4	41	2	58	.31	.125	54	18	.58	388	.01	3	1.22	.01	.12	1	1435
GT 0+40N	23	63	257	130	6.4	4	11	1448	7.33	340	5	2	1	15	2	18	2	30	.04	.074	27	6	.24	273	.01	8	.81	.01	.16	1	4175
GT 0+20N	5	97	215	175	2.9	5	26	3641	8.70	1162	5	ND	3	18	2	12	2	33	.03	.156	24	5	.36	370	.01	4	1.16	.01	.16	1	2015
6+00N 0+60E	4	258	126	209	2.5	7	20	2742	7.13	490	5	ND	1	18	3	3	2	35	.20	.154	20	3	.51	514	.01	7	1.00	.01	.10	2	635
6+00N 0+80E	3	248	218	225	2.8	8	28	3885	8.25	625	5	ND	1	15	3	4	2	40	.24	.186	25	3	.58	709	.01	4	1.24	.01	.12	1	655
6+00N 1+00E	5	332	907	366	9.0	4	27	3902	11.03	705	5	2	2	15	4	54	2	41	.09	.199	17	3	.47	355	.01	4	1.04	.01	.13	1	2175
6+00N 1+20E	4	318	349	326	4.2	6	30	3612	9.13	648	5	ND	1	22	4	16	2	57	.32	.167	22	5	.90	545	.03	17	1.51	.03	.12	1	855
6+00N 1+40E	4	1355	319	2141	6.0	11	32	6274	10.03	455	5	ND	2	20	21	8	2	38	.22	.177	35	5	.50	401	.01	9	1.72	.01	.15	1	1455
6+00N 1+60E	16	500	213	242	22.6	3	20	2706	14.99	296	5	3	4	19	3	29	12	38	.06	.165	16	3	.23	53	.01	7	.66	.01	.26	3	2795
6+00N 1+80E	4	258	145	465	2.6	15	21	2570	8.13	302	5	ND	3	11	4	3	2	42	.09	.137	15	10	.60	240	.01	4	1.40	.01	.12	1	735
6+00N 2+00E	5	261	160	466	3.0	14	21	2160	8.33	315	5	ND	2	12	3	4	3	40	.13	.143	14	9	.57	236	.01	3	1.21	.01	.10	1	725
5+50N 0+20W	2	102	48	162	.9	10	17	1729	5.88	100	5	ND	1	24	2	3	2	73	.34	.108	16	7	.72	315	.05	3	1.55	.05	.09	1	131
5+50N 0+00E	2	139	44	153	1.5	9	16	1716	5.89	102	6	ND	2	44	1	4	3	82	.49	.129	20	7	.90	1579	.03	5	2.12	.05	.11	1	142
5+50N 0+20E	6	158	106	193	1.3	10	19	1503	7.37	446	5	ND	1	15	2	4	2	65	.15	.149	25	11	.73	431	.02	4	2.61	.03	.09	1	335
5+50N 0+40E	6	91	95	111	1.5	6	6	427	5.80	286	5	ND	3	8	1	3	2	64	.07	.098	21	12	.45	225	.01	6	2.71	.01	.09	1	285
5+50N 0+60E	12	76	210	170	7.0	3	15	2210	14.02	435	5	5	2	10	2	9	4	38	.03	.173	26	6	.10	230	.01	6	1.84	.01	.13	1	10355
5+00N 0+60W	3	73	157	292	1.4	7	14	5190	5.46	310	5	ND	1	18	3	2	2	57	.18	.186	8	8	.10	386	.01	3	.70	.01	.12	1	225
5+00N 0+40W	5	93	118	155	1.5	8	15	2974	7.27	647	5	ND	2	13	2	2	2	97	.05	.144	12	9	.10	263	.01	2	1.16	.01	.13	1	104
5+00N 0+20W	7	68	75	108	1.6	8	8	801	6.23	389	7	ND	2	10	1	4	2	76	.05	.124	14	11	.28	156	.01	4	1.97	.01	.11	1	215
5+00N 0+00W	3	66	47	97	1.1	4	11	1112	5.05	162	5	ND	1	5	1	4	2	47	.02	.148	14	6	.34	180	.01	2	1.79	.01	.08	1	255
5+00N 0+20E	3	55	44	121	1.0	6	9	1312	4.64	156	5	ND	1	12	1	3	2	65	.10	.160	8	7	.31	286	.01	2	1.68	.01	.09	1	68
5+00N 0+40E	3	40	50	74	1.1	5	8	1309	3.89	141	5	ND	1	12	1	3	2	59	.08	.139	10	6	.18	113	.03	3	1.11	.01	.09	1	99
4+50N 1+80W	2	76	38	77	.6	4	7	415	4.03	68	6	ND	1	5	1	2	2	56	.05	.110	12	8	.35	165	.01	5	2.30	.01	.07	1	72
4+50N 1+60W	2	69	41	124	.7	6	10	1221	4.66	111	5	ND	1	11	1	2	2	57	.10	.120	10	6	.32	436	.01	4	1.64	.01	.09	2	62
4+50N 1+40W	2	85	39	122	.9	7	14	2169	5.03	101	5	ND	1	13	1	2	2	64	.23	.133	18	6	.59	775	.01	8	2.21	.01	.09	1	73
4+50N 1+20W	2	56	36	93	2.6	5	8	912	3.82	91	5	ND	1	8	1	4	2	60	.08	.147	13	8	.42	286	.01	12	2.35	.01	.09	1	102
4+50N 1+00W	2	34	36	71	1.0	4	6	747	3.12	99	5	ND	1	12	1	3	2	53	.14	.123	10	6	.21	363	.01	3	1.22	.01	.10	1	83
4+50N 0+80W	4	73	73	127	.8	7	12	1731	5.76	220	5	ND	1	12	1	2	2	75	.07	.148	13	9	.30	667	.01	3	2.39	.01	.10	1	86
4+50N 0+60W	3	59	70	134	2.7	6	12	1772	5.69	325	5	ND	1	11	2	2	2	54	.08	.164	10	7	.35	277	.01	3	1.86	.01	.09	1	245
4+50N 0+40W	4	57	78	110	1.0	6	13	3194	6.14	280	5	ND	2	13	2	2	2	55	.09	.132	12	8	.21	302	.01	3	1.54	.01	.10	1	235
4+50N 0+20W	5	56	100	95	2.2	4	19	2355	8.24	395	5	ND	1	20	2	2	2	51	.08	.419	14	5	.30	613	.01	6	1.38	.01	.10	1	565
4+50N 0+00W	8	44	66	111	1.3	6	9	1102	5.35	249	5	ND	1	21	2	2	2	52	.19	.151	15	8	.37	333	.01	4	1.78	.01	.09	2	295
STD C/AU-S	20	62	42	132	7.1	73	31	1054	4.13	39	18	8	36	52	20	17	21	61	.49	.084	40	61	.94	179	.07	39	1.98	.06	.13	12	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
4+50N 0+20E	2	63	100	172	.9	5	10	1278	7.28	528	5	ND	1	22	1	2	2	52	.17	.213	6	5	.08	423	.01	3	.66	.01	.14	1	134
4+50N 0+40E	4	4	662	92	2.6	1	1	45	3.48	232	5	ND	1	73	1	2	3	11	.03	.067	12	1	.02	111	.01	6	.27	.01	.39	2	450
4+00N 2+20W	1	99	29	106	.2	7	15	1533	4.78	64	5	ND	1	19	1	2	2	60	.35	.123	17	5	.45	1022	.01	4	1.49	.01	.12	1	41
4+00N 2+00W	1	74	30	102	.1	4	10	871	4.41	66	5	ND	1	12	1	2	2	78	.18	.158	12	5	.32	903	.01	3	1.99	.01	.11	1	39
4+00N 1+80W	1	95	25	113	.3	5	8	944	3.62	69	5	ND	1	10	1	2	4	59	.10	.132	8	5	.36	488	.01	3	1.68	.01	.13	1	43
4+00N 1+60W	1	62	48	117	.6	4	12	1903	4.15	102	5	ND	2	17	1	3	2	67	.09	.140	9	5	.34	311	.01	3	1.61	.01	.15	1	67
4+00N 1+40W	1	80	47	118	.4	6	10	1399	4.59	118	5	ND	1	13	1	3	2	60	.10	.180	7	6	.38	473	.01	3	2.00	.01	.12	1	85
4+00N 1+20W	1	118	80	161	.6	8	15	2175	5.42	212	5	ND	1	22	1	2	3	64	.27	.187	14	9	.56	1075	.01	7	2.29	.01	.11	1	151
4+00N 1+00W	1	88	67	200	.1	8	18	2970	4.87	132	5	ND	1	58	1	3	2	66	.75	.263	10	6	.61	1541	.01	4	1.87	.01	.15	1	87
4+00N 0+80W	1	64	60	78	.9	3	10	1641	3.72	124	5	ND	1	7	1	2	2	60	.04	.142	11	7	.31	182	.01	2	1.80	.01	.11	1	189
4+00N 0+60W	1	75	45	129	1.4	6	11	1796	4.47	115	5	ND	1	12	1	3	2	60	.11	.165	10	6	.54	383	.01	3	2.17	.01	.12	1	97
4+00N 0+40W	7	112	165	189	1.8	7	28	3411	7.90	333	5	ND	2	27	1	2	2	54	.15	.172	19	5	.58	761	.02	3	1.90	.03	.11	1	520
4+00N 0+20W	3	78	89	171	2.0	10	25	2739	6.36	228	5	ND	1	43	1	3	2	63	.42	.160	20	6	.79	802	.03	2	2.10	.07	.14	1	345
4+00N 0+00W	6	189	268	353	6.9	13	31	2821	7.60	349	5	ND	1	28	3	2	3	50	.17	.143	26	11	.48	910	.01	2	3.02	.02	.10	1	545
4+00N 0+20E	8	73	259	283	1.6	3	8	1022	12.19	677	5	2	3	17	1	19	2	13	.04	.082	40	3	.06	366	.01	3	.77	.01	.12	1	2450
4+00N 0+40E	4	152	527	303	3.7	8	25	3085	7.99	413	5	2	2	29	2	13	2	48	.09	.169	19	8	.42	620	.01	4	1.67	.01	.15	1	1070
4+00N 0+60E	3	197	421	478	3.8	10	24	3685	8.68	448	5	2	1	34	3	14	2	41	.22	.155	20	6	.44	571	.01	4	1.26	.01	.16	1	1810
4+00N 0+80E	4	115	372	241	3.3	6	26	5360	9.29	603	5	2	5	29	1	5	2	41	.10	.189	21	8	.34	431	.01	4	1.56	.01	.19	1	1550
4+00N 1+00E	6	53	286	126	2.9	4	22	4207	8.90	957	5	2	4	19	1	8	2	36	.02	.210	20	6	.30	382	.01	4	1.43	.01	.21	2	1815
4+00N 1+20E	3	99	274	238	2.9	7	20	2658	7.43	465	5	ND	4	20	1	5	2	42	.05	.134	16	8	.48	476	.01	3	1.34	.01	.19	2	1250
4+00N 1+40E	5	102	217	205	2.8	10	26	3774	8.42	1510	5	ND	5	21	1	11	2	32	.05	.144	23	6	.35	472	.01	8	1.22	.01	.20	1	1245
4+00N 1+60E	4	101	194	210	2.7	9	23	3098	7.66	812	5	ND	4	21	1	5	3	36	.15	.127	20	7	.42	489	.01	2	1.16	.01	.18	1	915
3+50N 1+60W	1	195	97	138	2.0	7	18	2037	4.96	98	5	ND	1	38	1	2	2	72	.57	.158	23	7	.67	1930	.01	4	1.81	.01	.17	1	166
3+50N 1+40W	1	253	81	166	.9	9	19	3216	5.32	133	5	ND	1	33	1	4	3	81	.39	.182	20	8	.80	1009	.01	3	2.20	.01	.17	1	102
3+50N 1+20W	1	201	95	165	1.0	8	19	2322	5.79	240	5	ND	3	17	1	5	2	72	.18	.157	16	8	.75	346	.01	4	2.19	.01	.16	1	315
3+50N 0+60W	1	179	77	163	1.2	8	20	1813	5.87	138	5	ND	2	26	1	5	3	82	.36	.151	18	7	.80	699	.02	5	1.63	.01	.14	1	165
3+50N 0+40W	1	165	63	155	1.2	9	19	1383	5.92	109	5	ND	3	31	1	2	2	88	.33	.092	18	8	.86	571	.04	6	1.61	.04	.13	1	178
3+50N 0+20W	1	170	66	163	1.3	8	18	1347	5.44	112	5	ND	2	24	1	3	2	78	.35	.131	18	8	.78	539	.01	4	1.54	.01	.12	1	171
3+50N 0+00W	2	127	72	152	.6	6	17	1910	5.41	142	5	ND	2	63	1	3	2	72	.36	.113	17	7	.70	534	.01	3	2.14	.01	.13	1	172
3+50N 0+20E	2	162	111	178	5.4	46	19	11385	7.94	452	5	2	2	75	1	2	2	54	.36	.102	54	7	.44	1084	.01	4	1.64	.01	.12	2	1690
3+50N 0+40E	3	148	179	281	3.2	15	24	3687	7.14	355	5	ND	3	44	2	2	2	54	.39	.113	24	7	.69	600	.04	5	1.48	.03	.14	1	895
3+50N 0+60E	3	157	437	430	3.9	12	24	4054	7.43	691	5	ND	5	46	4	4	2	50	.28	.131	25	8	.58	621	.02	11	1.42	.01	.15	1	1350
3+50N 0+80E	2	158	190	1646	3.0	16	18	2511	6.08	235	5	ND	3	42	12	3	2	57	.37	.126	26	8	.81	601	.01	10	1.94	.01	.14	1	680
3+50N 1+00E	1	237	79	518	1.9	16	20	2587	6.23	136	5	ND	2	64	6	3	3	73	.61	.125	23	11	1.05	676	.08	4	1.59	.06	.14	1	430
3+50N 1+20E	2	115	43	388	1.7	32	22	3846	3.94	158	5	ND	6	48	2	3	6	15	.56	.126	32	6	.15	336	.01	6	.87	.01	.36	1	255
3+00N 2+00W	1	481	126	265	3.1	8	28	3681	6.71	123	5	ND	2	32	1	3	3	84	.54	.153	27	7	.84	1144	.02	6	1.85	.01	.17	2	139
STD C/AU-S	19	62	43	132	6.9	73	31	1057	4.15	41	22	8	38	53	19	17	23	61	.49	.084	39	61	.95	183	.07	38	2.01	.06	.14	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
3+00N 1+80W	1	325	113	299	2.6	6	23	3322	5.03	108	5	ND	1	34	1	2	4	72	.60	.157	17	6	.69	1155	.02	4	1.43	.01	.13	1	79
3+00N 1+60W	1	280	81	196	2.0	6	21	2777	5.46	85	5	ND	3	32	1	3	2	78	.58	.178	20	6	.72	1009	.03	3	1.40	.01	.10	1	152
3+00N 1+40W	1	308	89	177	1.9	6	22	5191	5.33	99	5	ND	1	36	1	2	2	70	.52	.134	23	5	.65	1883	.02	3	1.46	.01	.11	2	245
3+00N 1+20W	1	236	65	174	2.0	6	17	1586	5.12	81	5	ND	1	32	1	3	2	73	.50	.159	23	6	.64	1147	.01	4	1.51	.01	.10	2	235
3+00N 1+00W	1	197	51	168	1.8	7	15	1077	5.05	77	5	ND	1	30	1	2	2	76	.50	.168	20	7	.70	951	.02	6	1.55	.02	.11	2	196
3+00N 0+80W	1	198	56	187	1.4	6	15	1310	5.06	86	5	ND	1	29	1	3	3	78	.50	.191	18	7	.62	1101	.01	4	1.62	.01	.11	2	174
3+00N 0+60W	1	199	79	191	2.1	8	16	1127	5.21	85	5	ND	1	29	1	2	2	77	.53	.172	17	10	.67	762	.01	5	1.46	.01	.09	2	225
3+00N 0+40W	1	190	58	178	1.3	7	18	1375	5.30	70	5	ND	1	29	1	2	2	80	.56	.175	18	8	.70	795	.01	4	1.38	.01	.10	2	255
3+00N 0+20W	1	160	56	157	.9	9	18	1760	5.04	91	5	ND	1	24	1	2	2	73	.46	.150	17	10	.62	734	.01	10	1.15	.01	.09	2	138
3+00N 0+00W	1	240	65	181	1.5	7	18	1521	5.11	71	5	ND	1	29	1	2	2	77	.57	.170	18	7	.68	882	.02	5	1.31	.01	.10	1	117
3+00N 0+20E	1	219	60	176	1.4	7	19	1863	5.29	73	5	ND	2	29	1	2	2	83	.59	.186	17	6	.72	800	.02	5	1.32	.01	.10	1	79
3+00N 0+40E	1	213	60	175	1.3	8	19	1966	5.29	78	5	ND	2	29	1	2	2	81	.57	.179	17	7	.71	711	.03	6	1.22	.01	.10	1	95
3+00N 0+60E	1	210	53	170	1.2	7	19	1813	5.38	67	5	ND	2	36	1	3	2	86	.72	.195	17	7	.84	872	.02	4	1.38	.01	.10	1	165
3+00N 0+80E	1	184	55	169	1.7	9	19	2026	5.76	123	5	ND	2	47	1	2	2	88	1.27	.170	16	8	1.04	570	.02	5	1.68	.01	.15	1	166
2+50N 2+00W	4	506	177	246	3.5	9	28	3765	6.99	147	5	ND	2	59	2	2	2	73	.62	.214	25	6	.73	516	.03	5	1.46	.02	.13	1	235
2+50N 1+80W	4	386	110	212	3.1	9	26	3087	6.45	136	5	ND	3	49	1	2	2	77	.68	.213	21	6	.83	550	.04	6	1.47	.03	.11	1	152
2+50N 1+60W	2	328	96	202	3.2	11	24	2501	6.15	123	5	ND	2	44	1	3	3	74	.70	.205	18	7	.78	673	.06	5	1.30	.04	.10	1	139
2+50N 1+40W	1	365	74	199	2.5	12	23	2873	6.07	98	5	ND	1	39	1	3	2	77	.70	.193	19	10	.82	867	.06	5	1.38	.03	.09	1	132
2+50N 1+20W	1	373	80	203	4.2	10	22	2849	6.02	82	5	ND	2	34	1	2	2	82	.70	.202	21	7	.71	819	.03	4	1.17	.02	.11	1	92
2+50N 1+00W	1	282	68	204	2.6	11	22	2695	6.03	109	5	ND	2	36	1	2	2	81	.69	.191	22	8	.77	754	.05	8	1.20	.03	.09	1	245
2+50N 0+80W	1	321	70	211	1.9	9	21	2427	5.61	53	5	ND	2	40	1	2	2	89	.88	.218	20	7	.66	933	.03	7	1.10	.01	.11	1	1435
2+50N 0+60W	1	163	47	204	1.2	9	25	2340	6.23	59	5	ND	3	37	1	3	2	96	.99	.222	18	6	1.08	691	.02	18	1.55	.01	.11	1	74
2+50N 0+40W	1	327	74	203	2.0	10	22	2610	5.82	60	5	ND	4	32	1	3	2	90	.74	.220	22	8	.65	857	.03	6	1.13	.01	.13	2	78
2+50N 0+20W	1	334	84	216	2.3	11	22	2593	6.05	76	5	ND	3	30	1	2	2	94	.69	.230	22	8	.62	810	.02	13	1.07	.01	.11	1	90
2+50N 0+00W	1	325	74	222	2.6	9	21	2323	5.68	71	5	ND	2	30	1	2	2	87	.69	.224	20	7	.72	760	.01	7	1.17	.01	.12	1	73
2+50N 0+20E	1	294	76	210	2.0	11	20	2388	5.88	124	5	ND	3	28	1	2	2	84	.61	.191	20	8	.68	644	.02	8	1.18	.01	.10	1	143
2+50N 0+40E	1	194	69	176	1.6	17	22	1763	5.91	129	5	ND	3	52	1	2	2	80	.77	.160	16	13	1.02	574	.14	3	1.33	.10	.10	1	157
2+50N 0+60E	2	345	139	252	3.8	15	28	2938	6.58	207	5	ND	3	44	2	2	2	72	.65	.205	20	11	.89	976	.07	3	1.45	.04	.10	1	325
2+50N 0+80E	1	189	63	169	2.4	10	18	1919	5.85	148	5	ND	2	37	1	3	2	81	.84	.195	17	8	.86	449	.03	5	1.42	.01	.14	2	355
2+50N 1+00E	3	248	83	185	2.9	17	26	2281	7.34	224	5	ND	3	40	1	2	2	76	.60	.161	17	9	.95	551	.07	5	1.53	.05	.12	4	625
2+00N 1+80W	1	262	83	180	2.0	10	21	2482	5.90	61	5	ND	3	38	1	2	2	85	.80	.223	20	8	.74	764	.05	7	1.10	.03	.11	1	68
2+00N 1+40W	1	299	134	242	3.6	12	23	2946	6.20	92	5	ND	3	35	1	3	2	80	.76	.205	22	8	.73	764	.05	5	1.17	.03	.10	1	102
2+00N 1+20W	1	302	141	269	3.8	13	24	2755	6.32	111	5	ND	3	38	2	2	2	80	.76	.206	21	8	.75	795	.07	4	1.20	.04	.11	1	139
2+00N 1+00W	1	270	99	201	2.5	11	22	2709	5.88	65	5	ND	3	39	1	3	2	81	.77	.198	20	8	.76	864	.07	4	1.16	.04	.11	1	57
2+00N 0+80W	1	265	101	202	2.6	12	22	2733	5.90	75	5	ND	3	40	1	3	2	80	.81	.210	21	9	.73	790	.07	3	1.13	.04	.10	1	107
2+00N 0+60W	1	253	80	166	1.5	10	20	2488	5.55	62	5	ND	2	29	1	2	2	82	.68	.210	19	8	.62	831	.01	5	1.03	.01	.11	1	68
STD C/AU-S	19	62	41	132	7.2	72	31	1061	4.15	42	18	8	37	53	19	18	22	63	.49	.091	39	61	.95	179	.07	38	2.00	.06	.13	11	49

TEUTON RESOURCES FILE # 88-4109

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
2+00N 0+40W	2	263	111	194	1.3	9	21	2939	6.17	86	5	ND	2	30	1	2	2	84	.53	.213	22	7	.66	794	.03	4	1.09	.01	.13	1	69
2+00N 0+20W	1	339	110	205	2.3	9	20	2292	5.81	92	5	ND	2	30	1	2	2	77	.66	.203	19	7	.53	781	.02	4	1.02	.01	.11	1	64
2+00N 0+00W	2	279	133	244	4.2	10	21	2289	6.17	104	5	ND	2	28	1	2	2	82	.74	.249	20	8	.59	557	.01	4	1.02	.01	.14	1	55
2+00N 0+20E	2	299	147	261	4.6	9	20	2283	5.80	109	5	ND	2	29	1	3	2	74	.66	.201	18	7	.73	710	.01	6	1.30	.01	.14	1	109
2+00N 0+60E	4	200	50	135	2.5	14	22	1687	7.52	206	5	ND	2	27	1	3	2	90	.49	.152	14	11	1.04	212	.01	5	1.78	.01	.19	2	520
2+00N 1+00E	3	105	45	127	1.0	14	22	1458	7.84	152	5	ND	2	39	1	2	2	115	1.06	.153	12	10	1.22	110	.03	6	2.01	.01	.19	1	332
1+50N 2+20W	7	395	366	495	3.6	17	46	4402	8.75	504	5	ND	2	41	6	3	2	73	.47	.192	25	12	1.03	489	.06	3	1.97	.02	.14	1	750
1+50N 2+00W	9	293	191	277	1.8	13	52	3497	11.71	531	5	ND	4	36	1	3	2	97	.25	.285	16	12	1.09	246	.03	3	2.13	.01	.16	1	1263
1+50N 1+80W	4	352	131	282	2.2	25	46	3685	3.30	375	5	ND	2	44	2	2	2	80	.65	.195	23	18	1.02	566	.06	9	1.94	.04	.15	1	532
1+50N 1+60W	3	402	80	212	1.9	12	27	2369	6.83	172	5	ND	2	34	1	2	2	77	.62	.203	22	9	1.01	853	.04	6	1.71	.02	.14	1	322
1+50N 1+40W	2	336	79	210	1.9	11	26	2875	5.84	175	5	ND	1	33	1	2	2	78	.63	.204	20	9	1.12	842	.04	4	1.83	.01	.13	1	413
1+50N 1+00W	3	422	206	305	5.1	12	30	3590	7.33	227	5	ND	3	29	2	2	2	79	.53	.205	22	9	.88	360	.03	6	1.59	.01	.14	1	262
1+50N 0+20E	2	163	51	144	1.4	11	21	2104	6.45	173	5	ND	2	48	1	2	2	77	.57	.163	18	9	1.11	501	.09	3	1.68	.06	.15	1	251
1+50N 0+40E	2	179	105	222	1.3	11	25	2678	7.31	296	5	ND	2	31	1	2	2	89	.54	.162	19	8	1.13	699	.02	3	2.12	.01	.18	1	492
1+50N 0+60E	3	436	55	143	3.5	9	21	2545	9.53	296	5	ND	1	44	1	3	2	80	.74	.156	14	9	.99	235	.03	9	1.75	.01	.13	10	1810
1+50N 0+80E	4	152	54	142	1.4	15	24	1693	8.29	163	5	ND	1	25	1	2	2	118	.47	.159	13	10	1.24	149	.02	5	1.36	.01	.15	1	472
1+50N 1+00E	2	135	45	117	1.1	12	23	1469	7.81	166	5	ND	3	29	1	2	2	108	.58	.164	11	10	1.12	121	.03	4	1.72	.01	.13	1	491
1+00N 2+00W	7	430	93	203	4.5	9	33	5763	3.65	562	5	ND	3	24	2	2	2	58	.42	.195	28	4	.72	303	.04	14	1.43	.02	.11	1	1170
1+00N 1+80W	8	247	94	205	2.2	9	37	4668	8.52	267	5	ND	3	35	2	2	2	94	.56	.157	24	5	1.09	191	.07	3	1.80	.03	.11	1	692
1+00N 1+60W	4	236	113	131	2.5	9	33	4192	7.76	198	5	ND	3	40	1	3	2	88	.65	.202	28	5	.86	290	.06	3	1.53	.03	.13	1	272
1+00N 1+40W	3	221	79	154	1.5	9	24	2886	6.47	169	5	ND	2	36	1	2	2	71	.64	.192	27	6	.77	207	.05	7	1.36	.02	.11	1	272
1+00N 1+20W	3	231	76	166	1.6	10	24	2973	6.94	175	5	ND	1	38	1	2	2	73	.75	.197	29	7	.87	220	.05	23	1.48	.03	.14	2	282
1+00N 1+00W	3	226	75	158	1.3	13	25	2708	7.03	154	5	ND	2	42	1	2	3	74	.78	.193	26	9	.90	272	.09	4	1.49	.05	.14	1	231
1+00N 0+80W	1	117	26	117	.3	12	14	1684	4.55	41	5	ND	1	59	1	2	2	57	2.11	.142	18	14	.83	260	.02	7	1.43	.01	.13	1	38
1+00N 0+60W	1	155	31	120	.4	14	16	1697	4.79	35	5	ND	1	67	1	2	2	71	2.44	.143	14	16	1.00	457	.02	3	1.58	.01	.15	1	46
1+00N 0+40W	1	263	47	159	.7	13	24	2812	6.53	89	5	ND	1	48	1	2	2	81	1.21	.152	22	15	1.02	435	.07	6	1.61	.05	.13	1	67
1+00N 0+20W	2	194	58	160	.9	13	21	2506	6.17	109	5	ND	1	29	1	2	2	71	.67	.183	24	12	.92	423	.02	6	1.59	.01	.16	2	124
1+00N 0+00W	3	178	52	148	2.1	7	20	2554	6.53	287	5	ND	2	26	1	2	3	66	.50	.169	18	6	.88	470	.03	13	1.49	.01	.16	1	422
1+00N 0+40E	4	476	41	120	2.5	6	22	2521	9.91	228	5	ND	1	51	1	2	2	102	.72	.134	11	9	1.25	110	.03	9	2.25	.01	.18	14	1392
1+00N 0+60E	5	188	42	117	3.2	14	24	1792	8.25	213	5	ND	2	21	1	2	2	88	.36	.169	13	9	.96	241	.01	4	1.67	.01	.18	2	781
1+00N 1+00E	3	133	52	167	1.0	19	24	1600	7.21	220	5	ND	1	42	1	2	3	100	1.34	.147	13	14	1.25	80	.03	7	1.98	.01	.18	1	350
0+50N 1+80W	2	183	54	198	1.0	14	51	5761	11.69	1120	5	ND	3	44	1	5	2	82	.41	.210	26	6	.85	184	.06	8	1.66	.05	.18	3	851
0+50N 1+60W	4	95	64	157	1.1	8	40	3957	11.65	1088	5	ND	5	15	1	2	2	65	.07	.270	16	6	.69	259	.01	4	1.46	.01	.16	2	783
0+50N 1+40W	4	104	58	156	1.3	10	41	4018	10.01	783	5	ND	4	28	1	2	2	65	.22	.205	16	7	.90	236	.05	6	1.61	.05	.15	1	562
0+50N 1+20W	7	290	79	175	3.2	3	33	4433	8.33	528	5	ND	3	26	1	3	2	58	.34	.187	23	5	.67	529	.03	9	1.31	.01	.13	1	544
0+50N 1+00W	5	325	70	175	2.9	13	34	3878	8.60	472	5	ND	2	52	1	2	2	72	.68	.181	24	8	1.04	482	.16	5	1.67	.12	.12	2	753
STD C/AU-S	18	61	41	132	6.5	72	30	1042	4.16	42	21	6	36	53	18	16	21	60	.48	.092	41	61	.34	181	.07	41	1.97	.06	.14	13	53

TEUTON RESOURCES FILE # 88-4109

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM
0+50N 0+80W	9	312	105	206	3.1	8	28	4643	8.31	413	5	ND	1	29	2
0+50N 0+60W	5	225	71	150	3.0	6	23	3699	7.76	480	5	ND	1	19	1
0+50N 0+40W	4	233	66	164	2.5	6	24	3179	6.98	370	5	ND	1	22	1
0+50N 0+20W	3	172	52	163	2.3	5	22	3029	5.95	391	5	ND	2	27	1
0+50N 0+00W	2	178	63	164	2.2	6	22	2914	6.63	359	5	ND	2	26	1
0+50N 0+20E	3	437	44	132	2.5	7	30	2549	10.46	282	5	ND	1	36	1
0+50N 0+40E	4	429	41	121	3.5	12	25	2577	10.27	207	5	ND	1	39	1
0+50N 0+60E	4	370	49	122	2.9	11	21	1761	10.50	225	5	ND	1	31	1
0+00N 2+60W	6	390	96	251	2.5	17	37	5212	8.38	362	5	ND	4	34	3
0+00N 2+40W	3	210	62	180	2.3	11	36	4752	8.55	392	5	ND	2	30	1
0+00N 2+20W	2	202	63	181	2.3	11	35	4532	8.87	427	5	ND	2	33	1
0+00N 2+00W	3	173	58	170	2.1	10	34	4226	8.69	409	5	ND	1	33	1
0+00N 1+80W	4	163	66	176	2.9	10	39	4819	9.47	500	5	ND	2	34	1
0+00N 1+60W	3	140	76	208	2.2	16	38	5186	9.69	462	5	ND	3	54	1
0+00N 1+40W	3	154	96	221	2.4	15	40	5092	9.80	575	5	ND	2	32	1
0+00N 1+20W	1	90	64	204	1.5	10	31	3810	8.93	567	5	ND	2	28	1
0+00N 1+00W	1	71	47	196	1.6	7	25	3123	8.16	481	5	ND	3	22	1
0+00N 0+80W	2	125	86	235	1.9	15	40	4623	11.39	923	5	ND	3	33	1
0+00N 0+60W	5	221	71	193	4.1	7	29	3549	8.54	618	5	ND	3	18	1
0+00N 0+40W	2	117	54	159	1.9	16	32	2900	8.97	411	5	ND	2	80	1
0+00N 0+20W	5	235	77	199	2.5	9	31	3908	8.46	524	5	ND	2	24	1
0+00N 0+00W	2	204	69	174	1.7	10	24	3059	7.08	419	5	ND	2	25	1
0+00N 0+20E	3	243	59	155	3.7	14	30	2476	8.48	299	5	ND	1	33	1
0+00N 0+40E	5	259	86	277	2.3	28	28	2209	6.70	364	5	ND	1	28	2
STD C/AU-S	19	63	42	132	7.1	72	31	1067	4.24	43	19	8	37	52	19

SAMPLE#	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
0+50N 0+80W	3	3	80	.40	.177	24	5	.69	500	.04	4	1.55	.01	.12	1	960
0+50N 0+60W	4	2	58	.35	.161	21	4	.79	449	.02	2	1.47	.01	.14	1	945
0+50N 0+40W	3	2	59	.43	.153	18	4	.76	467	.02	6	1.39	.01	.16	1	750
0+50N 0+20W	2	2	59	.44	.152	18	4	.94	407	.02	4	1.65	.01	.18	1	445
0+50N 0+00W	2	2	64	.40	.142	19	5	.86	542	.02	3	1.58	.01	.16	1	580
0+50N 0+20E	2	5	110	.44	.144	12	9	1.29	346	.03	5	2.26	.01	.15	14	1115
0+50N 0+40E	5	4	106	.58	.139	14	11	1.30	215	.02	5	2.29	.01	.17	9	1690
0+50N 0+60E	3	4	94	.35	.134	11	10	1.11	264	.02	6	1.93	.01	.15	12	1255
0+00N 2+60W	2	2	64	.43	.145	35	8	.84	337	.01	3	1.81	.02	.12	1	460
0+00N 2+40W	2	2	74	.55	.149	32	6	1.02	252	.02	6	1.39	.01	.13	1	445
0+00N 2+20W	2	3	75	.48	.152	31	6	1.03	281	.03	5	1.88	.02	.14	1	520
0+00N 2+00W	4	2	77	.46	.151	29	5	1.07	262	.03	2	1.89	.02	.13	1	575
0+00N 1+80W	2	2	83	.42	.171	30	6	1.04	267	.02	10	1.96	.02	.16	1	510
0+00N 1+60W	5	2	95	.69	.155	35	7	1.20	281	.14	5	2.00	.11	.14	1	585
0+00N 1+40W	2	2	83	.43	.166	32	7	.91	217	.03	6	1.72	.02	.13	1	850
0+00N 1+20W	4	2	86	.41	.170	24	6	1.02	386	.02	3	1.72	.01	.14	1	775
0+00N 1+00W	5	2	98	.42	.164	21	6	1.10	350	.01	2	1.73	.01	.17	1	660
0+00N 0+80W	4	2	76	.34	.135	30	9	.75	163	.01	3	1.47	.01	.15	1	925
0+00N 0+60W	2	3	62	.30	.158	22	4	.77	352	.02	4	1.40	.01	.12	1	940
0+00N 0+40W	4	2	92	.98	.125	23	7	1.50	289	.23	4	2.07	.21	.18	1	625
0+00N 0+20W	2	2	63	.40	.173	25	9	.77	454	.02	8	1.53	.01	.15	1	780
0+00N 0+00W	4	2	73	.43	.142	20	6	.98	466	.01	5	1.75	.01	.20	1	705
0+00N 0+20E	2	2	78	.45	.142	17	8	.98	290	.06	6	1.57	.05	.16	1	735
0+00N 0+40E	2	2	64	.49	.105	18	10	.62	401	.01	6	1.37	.01	.12	1	620
STD C/AU-S	17	21	63	.49	.085	42	61	.96	179	.07	37	2.01	.06	.14	13	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	
TR-21-88 1	2	13	59	21	1.2	6	2	79	3.36	79	5	ND	1	13	1	2	2	5	.02	.032	8	9	.02	493	.01	3	.31	.01	.16	1	112	.003
TR-21-88 2	3	56	43	19	11.2	4	2	143	4.07	40	5	ND	2	6	1	4	2	5	.02	.035	5	15	.02	91	.01	4	.24	.01	.13	1	82	.002
TR-21-88 3	4	95	58	21	37.5	5	4	467	5.01	75	5	ND	3	18	1	5	2	5	.01	.041	6	4	.03	607	.01	3	.29	.01	.15	1	197	.006
TR-22-88 1	1	57	12	99	1.4	6	9	2134	3.57	1859	5	ND	3	35	1	5	2	49	.22	.076	26	17	.99	714	.01	2	1.49	.01	.14	1	210	.006
TR-22-88 2	1	102	14	117	1.2	7	10	1953	3.59	853	5	ND	3	65	1	2	2	64	.22	.073	23	14	1.48	1472	.01	7	1.63	.01	.12	1	175	.005
TR-22-88 3	2	282	16	93	1.2	49	22	2116	4.69	993	5	ND	1	41	1	4	2	86	1.64	.065	19	69	1.74	352	.01	2	2.13	.01	.16	1	73	.002
TR-22-88 4	5	206	23	152	9.3	12	11	2274	4.04	259	5	ND	1	34	1	5	2	64	.79	.078	37	11	.76	398	.01	4	1.08	.01	.12	1	440	.018
TR-22-88 5	2	137	15	135	1.7	7	9	2392	3.76	508	5	ND	1	21	1	2	2	74	.72	.079	29	15	1.23	199	.01	5	1.76	.01	.13	2	210	.006
TR-22-88 6	5	93	29	147	4.9	3	7	1553	3.82	257	5	ND	1	24	1	3	2	31	.33	.055	15	9	.29	405	.01	3	.76	.01	.23	1	590	.017
TR-22-88 7	6	139	12	62	9.1	14	4	2564	2.87	46	5	ND	2	12	1	13	2	33	.06	.035	6	14	.03	314	.01	6	.24	.01	.11	1	470	.014
TR-22-88 8	10	215	50	50	94.1	8	2	1452	3.20	115	5	ND	3	27	1	72	2	50	.02	.026	7	6	.03	181	.01	9	.26	.01	.14	2	1140	.033
TR-22-88 9	8	193	14	66	10.7	8	3	1613	4.56	64	5	ND	2	9	1	24	2	56	.02	.036	9	13	.03	154	.01	4	.34	.01	.15	1	470	.014
TR-22-88 10	2	42	7	24	1.9	8	5	1085	3.71	32	5	ND	5	5	1	2	2	7	.02	.040	6	7	.03	146	.01	4	.28	.01	.17	1	210	.006
TR-22-88 11	2	55	12	31	2.8	5	4	1221	5.09	99	5	ND	4	6	1	2	2	6	.02	.043	8	13	.03	145	.01	4	.31	.01	.16	2	310	.009
TR-22-88 12	2	25	7	17	1.8	6	4	589	4.45	57	5	ND	3	5	1	2	2	9	.02	.039	8	5	.03	76	.01	9	.27	.01	.17	2	390	.011
TR-22-88 13	2	96	9	17	1.4	4	2	238	6.30	64	5	ND	5	5	1	2	2	9	.01	.064	5	14	.03	42	.01	5	.29	.01	.14	1	305	.009
TR-22-88 14	3	23	14	19	5.2	10	2	54	6.13	102	5	ND	4	4	1	2	2	11	.02	.040	8	11	.03	12	.01	4	.25	.01	.17	2	660	.019
TR-22-88 15	2	20	6	21	1.8	19	7	76	4.82	100	5	ND	4	4	1	3	2	12	.03	.027	6	14	.04	11	.01	3	.29	.01	.18	2	480	.014
TR-22-88 16	13	37	8	52	.7	16	6	122	4.32	46	5	ND	1	5	1	2	2	7	.27	.045	7	10	.03	17	.01	5	.37	.01	.16	1	114	.003
TR-22-88 17	7	39	32	54	2.3	21	21	199	3.47	190	5	ND	1	8	2	2	6	11	.20	.046	7	14	.11	6	.01	5	.48	.01	.17	1	920	.027
TR-22-88 18	6	38	71	250	3.0	17	13	1111	11.59	167	5	ND	1	22	5	2	2	21	.95	.035	5	8	.30	4	.01	7	.52	.01	.21	1	690	.020
TR-22-88 19	4	42	14	51	.9	7	8	1382	2.98	84	5	ND	3	12	1	3	2	24	.06	.042	6	14	.06	145	.01	7	.38	.01	.17	1	250	.007
TR-30-88 1	1	68	12	74	.5	8	20	1267	5.18	10	5	ND	2	40	1	2	2	140	.72	.151	8	11	2.47	203	.02	2	3.08	.01	.07	1	27	.001
TR-30-88 2	1	171	10	75	.5	8	16	1247	5.07	10	5	ND	2	27	1	2	2	128	.65	.161	11	9	2.36	308	.02	5	2.92	.01	.11	1	63	.002
TR-30-88 3	1	276	16	81	5.0	7	16	1445	6.37	29	5	6	3	16	2	2	2	130	.53	.146	18	8	2.32	240	.01	6	3.08	.01	.17	1	8820	.257
TR-30-88 4	3	21843	32	191	36.4	10	9	2747	9.17	114	5	ND	9	88	7	436	2	48	5.13	.038	10	21	1.45	35	.01	2	2.05	.01	.08	17	2970	.087
TR-30-88 5	2	9083	17	134	14.2	8	10	2981	9.75	93	5	3	7	115	4	2	3	42	7.57	.030	6	13	1.69	26	.01	6	2.09	.01	.01	26	1730	.050
TR-30-88 6	2	7388	21	167	9.2	8	7	2960	10.67	105	5	3	7	116	4	4	3	42	7.49	.024	5	17	1.65	21	.01	5	2.25	.01	.01	42	1560	.046
TR-30-88 7	2	2087	22	90	4.4	10	17	2234	19.41	241	5	3	4	61	3	2	5	34	4.60	.021	4	17	1.13	8	.01	4	1.77	.01	.01	23	2350	.069
TR-31-88 1	1	147	18	67	.3	10	10	1088	4.18	18	5	ND	1	23	1	4	2	107	.78	.199	6	14	1.62	294	.01	8	2.14	.02	.07	4	68	.002
TR-31-88 2	1	99	15	75	.3	10	12	1169	5.00	22	5	ND	1	14	1	2	2	104	.57	.171	6	11	1.88	141	.01	6	2.43	.02	.11	4	82	.002
TR-31-88 3	1	60	18	76	.7	13	14	1178	5.26	11	5	ND	3	12	1	2	2	116	.48	.142	11	17	2.22	173	.01	7	2.89	.01	.16	1	34	.001
TR-31-88 4	2	97	15	96	.9	8	23	1197	5.48	19	5	ND	3	14	2	2	2	122	.45	.140	11	10	1.94	244	.01	9	2.51	.01	.14	1	101	.003
TR-31-88 5	1	47	23	113	1.3	6	6	2070	6.92	20	5	ND	1	75	2	4	2	96	4.95	.088	9	11	1.76	80	.01	2	2.95	.01	.19	1	148	.004
TR-31-88 6	2	91	11	42	2.8	3	3	1786	2.11	23	5	ND	2	244	1	2	2	21	25.93	.025	6	8	.47	161	.01	2	.77	.01	.06	5	510	.015
TR-31-88 7	3	2411	20	114	4.8	6	3	2535	5.95	47	5	2	2	140	2	4	2	69	8.33	.058	9	20	1.19	25	.01	5	2.08	.01	.09	7	4920	.114
STD C/AU-R	20	62	41	132	7.2	72	31	1058	4.13	42	19	7	36	53	20	19	23	61	.49	.085	40	61	.91	183	.07	40	1.99	.06	.14	13	500	

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM
TR-31-88 8	4	3557	13	89	5.8	5	2	2418	6.51	52	5	4	1	171	2
TR-31-88 9	2	498	15	97	1.1	8	2	2580	6.38	25	5	ND	1	170	1
TR-31-88 10	3	159	7	61	.6	6	8	2428	6.36	16	5	ND	1	193	1
TR-31-88 11	2	80	20	72	1.3	7	15	1561	6.88	32	5	ND	1	35	1
TR-31-88 12	3	395	15	75	1.8	9	27	1651	7.14	31	5	ND	1	29	1
TR 9 EXT 88-1	2	43	11	73	.7	4	10	3281	15.29	182	5	ND	2	97	3
TR 9 EXT 88-2	3	60	12	84	3.5	7	20	3425	16.80	178	5	10	1	36	2
~~[illegible]~~	~~4~~	~~43~~	~~13~~	~~7~~	~~1.4~~	~~8~~	~~16~~	~~150~~	~~3.37~~	~~22~~	~~5~~	~~ND~~	~~1~~	~~4~~	~~1~~
STD C/AU-R	19	62	43	132	7.2	73	31	1051	4.11	44	19	8	37	52	19

SAMPLE#	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	
TR-31-88 8	2	3	75	9.49	.062	6	9	1.36	35	.04	8	2.12	.01	.10	3	5050	.147
TR-31-88 9	5	3	81	5.13	.091	7	13	1.62	146	.07	4	3.05	.01	.13	3	124	.004
TR-31-88 10	4	2	97	7.56	.092	5	6	1.39	75	.08	3	2.61	.01	.14	6	350	.010
TR-31-88 11	2	2	90	1.57	.123	9	9	1.44	61	.01	2	2.77	.01	.37	1	182	.057
TR-31-88 12	2	2	135	.70	.130	9	7	1.70	60	.01	10	2.81	.01	.35	1	430	.013
TR 9 EXT 88-1	4	2	57	4.44	.041	7	20	1.56	29	.05	2	2.08	.01	.05	38	950	.028
TR 9 EXT 88-2	2	5	43	1.69	.029	7	15	1.72	9	.02	2	2.10	.01	.04	3	7680	.224
~~[illegible]~~	~~7~~	~~2~~	~~3~~	~~.09~~	~~.001~~	~~2~~	~~54~~	~~.04~~	~~21~~	~~.01~~	~~3~~	~~.10~~	~~.01~~	~~.04~~	~~1~~	~~410~~	.012
STD C/AU-R	17	18	61	.50	.081	41	60	.95	181	.07	33	2.01	.06	.15	11	505	

ROCKS

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
BC 2+20N	1	24	35	120	1.6	25	10	1640	6.32	363	5	ND	3	25	2	3	2	16	1.17	.059	5	11	.60	11	.01	2	1.16	.01	.30	1	980
BC 2+10N	1	50	8	82	3.3	17	9	1850	4.24	71	5	ND	2	57	1	2	4	15	3.16	.038	4	13	.82	19	.01	3	1.28	.01	.26	1	225
BC 2+00N	1	9	21	68	.6	9	4	1193	2.69	91	5	ND	2	13	1	2	4	5	.48	.024	5	2	.05	25	.01	3	.40	.01	.20	1	505
BC 1+90N	1	17	16	130	.4	17	4	3739	6.56	124	5	ND	3	44	1	2	3	22	2.98	.071	6	14	2.05	39	.01	9	1.84	.01	.28	1	153
BC 1+80N	7	118	12	112	.6	28	9	3574	3.82	181	5	ND	2	64	1	6	3	12	3.88	.037	5	11	1.08	34	.01	2	.90	.01	.21	1	555
BC 1+70N	1	10	8	52	.4	21	19	2144	5.85	167	5	ND	3	47	1	2	2	12	2.78	.051	5	17	1.08	18	.01	6	1.11	.01	.31	1	325
BC 1+60N	1	11	6	136	.3	25	8	4676	5.19	75	5	ND	3	36	1	2	2	27	2.15	.051	6	24	2.86	30	.01	3	2.39	.01	.28	1	275
BC 1+50N	1	16	317	753	.8	16	9	6131	2.45	58	5	ND	2	118	1	7	2	4	3.93	.032	6	7	.42	16	.01	2	.43	.01	.20	1	1455
BC 1+40N	2	13	76	202	.7	16	9	231	3.94	140	5	ND	3	14	1	6	2	5	.25	.044	7	3	.07	19	.01	3	.53	.01	.25	1	275
BC 1+30N	2	64	48	157	2.3	25	32	7190	13.63	253	5	ND	3	32	1	4	2	4	2.10	.066	2	7	.42	4	.01	3	.39	.01	.24	1	655
BC 1+20N	2	52	817	2591	2.4	17	13	421	7.54	400	5	4	2	11	17	8	2	9	.33	.035	3	3	.06	8	.01	2	.34	.01	.21	1	6465
BC 1+10N	4	10	6	60	.2	15	10	1075	2.84	51	5	ND	3	32	1	2	2	18	1.78	.034	6	12	.64	39	.01	3	.84	.02	.19	1	335
BC 1+00N	1	4	5	98	.3	14	7	2010	3.87	50	5	ND	2	34	1	2	2	18	2.61	.056	7	17	1.87	79	.01	5	1.78	.01	.25	1	141
BC 0+90N	2	14	23	58	1.7	19	27	902	6.66	65	5	ND	3	20	1	2	2	18	1.43	.037	16	16	.67	16	.01	3	1.03	.01	.19	1	1145
BC 0+80N	1	13	18	83	.7	15	6	1059	3.68	26	5	ND	2	55	1	2	2	14	1.88	.042	8	14	.58	17	.01	3	1.02	.01	.23	1	235
BC 0+70N	3	35	6	58	.6	15	5	1732	2.39	120	5	ND	2	59	1	2	2	16	3.49	.044	7	13	.69	56	.01	2	.86	.01	.17	1	745
BC 0+60N	3	12	36	95	.3	15	4	997	2.33	20	5	ND	2	32	1	2	2	11	1.92	.028	8	13	.33	42	.01	6	.53	.02	.20	1	126
BC 0+50N	45	19	58	23	3.9	31	21	3867	14.51	106	5	ND	2	105	1	2	7	7	8.21	.039	10	3	.06	9	.01	2	.29	.01	.25	1	585
BC 0+40N	1	7	6	82	.2	23	14	1316	3.07	63	5	ND	2	32	1	2	2	46	1.60	.051	14	34	1.47	97	.01	5	1.68	.02	.22	1	315
BC 0+30N	1	5	25	34	.6	5	4	724	1.59	95	5	ND	2	24	1	2	2	8	1.79	.019	8	10	.21	96	.01	5	.53	.01	.22	1	265
BC 0+20N	1	11	2	4	.5	3	4	391	1.33	40	5	ND	1	145	1	2	2	2	.73	.012	4	1	.03	29	.01	2	.32	.01	.23	1	255
BC 0+10N	5	3755	64	39	28.3	16	128	995	15.41	75	5	ND	2	32	1	2	5	8	1.92	.063	4	14	.28	4	.01	2	.45	.01	.13	1	2115
BC 0+00N	1	35	21	125	1.9	25	17	2349	8.38	164	5	ND	3	27	1	3	4	29	1.67	.070	7	28	2.04	16	.01	3	2.45	.01	.27	1	255
~~BC 3+50N 1+40E~~	1	9	2	71	.4	26	10	1107	3.10	4	5	ND	4	33	1	2	2	40	1.04	.067	15	30	1.42	140	.01	7	1.66	.02	.14	1	975
~~BC 1+00N 0+20E~~	1	19	11	170	.1	1	14	1075	8.16	21	5	ND	3	29	1	2	2	31	1.01	.151	15	7	1.35	250	.17	5	2.40	.02	.05	2	19
~~BC 1+00N 0+80E~~	1	61	5	51	.4	5	8	655	3.06	21	5	ND	2	21	1	2	2	80	.80	.163	7	9	1.25	131	.01	2	1.49	.02	.13	1	42
STD C/AU-R	18	59	40	132	6.5	68	29	963	4.14	40	21	8	36	47	18	17	18	58	.53	.081	38	61	.92	172	.06	31	2.01	.06	.15	13	490

ACME / YTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VAN /ER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)25

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P5 SOIL P6-P13 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: SEP 27 1988 DATE REPORT MAILED: Oct 3/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TEUTON RESOURCES File # 88-4826 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L6+25N 0+00E	1	108	139	257	.7	6	24	2730	7.13	400	5	ND	3	34	1	11	2	66	1.00	.239	16	10	.64	729	.01	3	1.35	.02	.22	1	250
L6+25N 0+05E	1	242	361	335	2.0	7	36	4170	10.01	927	5	ND	4	29	1	13	2	73	.50	.288	23	16	.93	801	.01	6	1.85	.01	.23	1	530
L6+25N 0+20E	1	358	487	510	4.6	5	32	5386	10.69	713	5	ND	3	20	2	35	2	65	.31	.251	20	14	.78	552	.01	2	1.49	.01	.24	1	905
L6+25N 0+25E	3	350	478	458	5.1	6	29	4465	10.44	715	5	ND	3	17	1	34	2	54	.18	.239	19	13	.63	543	.01	2	1.34	.01	.25	1	890
L6+25N 0+30E	2	442	398	527	4.5	6	30	5439	10.27	614	5	ND	3	17	2	31	2	52	.21	.244	20	14	.63	624	.01	3	1.40	.02	.22	1	905
L6+25N 0+35E	1	416	286	565	4.0	8	23	5104	9.53	352	5	ND	3	16	2	16	2	47	.16	.221	16	13	.57	433	.01	2	1.46	.01	.27	1	970
L6+25N 0+80E	1	119	88	196	1.0	5	19	2593	6.63	361	5	ND	3	24	1	11	2	50	.53	.197	15	9	.54	581	.01	3	1.17	.01	.21	2	310
L6+25N 0+35E	1	131	87	189	1.0	5	18	2661	6.07	327	5	ND	3	24	1	10	2	46	.53	.178	15	7	.51	663	.01	2	1.16	.01	.21	1	370
L6+25N 0+90E	2	194	367	255	1.0	8	54	6093	10.84	1024	5	ND	3	27	1	20	2	92	.58	.430	31	18	.95	1363	.01	2	1.81	.01	.20	2	255
L6+25N 0+95E	1	119	94	191	.7	6	22	2851	6.90	355	5	ND	2	23	1	12	2	62	.55	.232	16	10	.59	796	.01	2	1.23	.01	.18	1	305
L6+12N 0+00E	1	185	156	244	1.7	6	44	5392	13.97	1085	5	ND	4	24	1	8	2	76	.32	.528	37	13	.91	783	.01	2	1.82	.01	.22	1	550
L6+12N 0+20E	3	342	450	339	4.2	5	28	4264	10.48	722	5	ND	4	14	1	43	2	53	.12	.263	19	13	.65	515	.01	2	1.38	.01	.25	1	1370
L6+12N 0+35E	3	498	364	566	5.8	5	21	3797	12.99	394	5	ND	4	11	1	18	4	49	.05	.302	16	12	.51	326	.01	2	1.22	.01	.26	1	830
L6+12N 0+80E	1	156	141	251	1.3	7	21	3144	7.62	471	5	ND	2	23	1	15	2	48	.38	.212	19	10	.47	632	.01	2	1.03	.01	.18	1	570
L6+12N 0+85E	1	180	128	244	1.5	6	21	3629	7.04	480	5	ND	3	22	1	14	2	38	.39	.190	19	9	.48	702	.01	2	1.13	.01	.22	1	710
L6+12N 0+90E	1	173	145	224	1.4	5	21	3913	7.02	523	5	ND	3	21	1	13	2	33	.33	.207	23	8	.47	672	.01-	2	1.13	.01	.25	1	780
L6+12N 0+95E	1	176	163	225	1.4	5	22	3178	7.26	451	5	ND	4	24	2	11	2	41	.35	.209	20	8	.51	898	.01	4	1.06	.01	.18	3	540
L6+12N 1+00E	1	334	441	543	2.8	8	43	5130	12.40	1731	5	ND	3	14	1	27	2	66	.31	.330	29	16	.78	545	.01	2	1.57	.01	.19	1	850
L6+12N 1+25E	2	338	437	350	4.4	5	29	4241	10.11	642	5	ND	2	13	1	45	2	53	.14	.264	18	15	.74	500	.01	2	1.39	.01	.23	1	1220
L6+12N 1+30E	4	272	456	300	6.9	5	19	2745	9.60	602	5	ND	3	18	1	34	2	40	.07	.215	15	12	.37	303	.01	6	1.00	.01	.28	1	1430
L6+00N 0+75E	2	179	156	255	1.8	8	21	3392	7.37	457	5	ND	3	19	1	15	2	45	.22	.183	19	10	.51	732	.01	2	1.09	.01	.17	2	1920
L6+00N 0+80E	2	152	139	277	1.7	7	21	2910	7.27	357	5	ND	2	21	1	16	2	50	.25	.172	16	11	.50	797	.01	3	1.06	.01	.14	3	660
L6+00N 0+85E	1	213	186	222	1.6	6	20	3730	7.26	571	5	ND	3	14	1	20	2	32	.20	.196	23	8	.42	687	.01	2	1.06	.01	.20	3	770
L6+00N 0+90E	1	249	151	230	1.9	5	29	4237	9.08	728	5	ND	2	14	1	16	2	58	.27	.249	25	13	.81	700	.01	2	1.60	.01	.22	1	690
L6+00N 0+95E	1	392	335	242	3.4	8	53	7213	12.92	1084	5	ND	4	12	1	21	2	82	.25	.414	25	18	1.05	688	.01	2	2.12	.01	.19	3	810
L6+00N 1+00E	1	498	117	239	1.9	13	32	5434	7.59	527	5	ND	2	20	1	9	2	41	.34	.187	27	18	.86	849	.01	2	1.56	.01	.22	1	440
L6+00N 1+10E	2	394	802	433	10.0	5	26	4352	10.60	605	5	2	2	18	1	117	3	40	.23	.217	17	13	.50	416	.01	2	1.06	.01	.26	1	1840
L6+00N 1+15E	1	288	420	318	3.9	5	26	4124	9.37	603	5	ND	3	20	1	32	2	40	.26	.226	19	12	.59	606	.01	2	1.21	.01	.25	1	1150
L6+00N 1+20E	4	265	368	280	5.2	6	22	3050	9.72	720	5	ND	4	13	1	39	2	42	.08	.215	17	15	.53	428	.01	2	1.20	.01	.24	1	1420
L6+00N 1+25E	1	258	291	380	3.4	5	25	4329	9.29	648	5	ND	3	18	1	31	2	40	.29	.216	20	11	.63	513	.01	2	1.18	.02	.21	1	1550
L6+00N 1+30E	3	745	424	601	5.1	8	29	8029	10.20	535	5	ND	3	13	3	25	2	39	.09	.218	15	15	.38	336	.01	2	1.63	.01	.25	2	1205
L6+00N 1+35E	1	620	450	769	3.8	10	24	6325	9.17	360	5	ND	3	15	4	22	2	42	.22	.236	19	15	.50	399	.01	2	1.63	.01	.27	1	760
L5+87N 0+70E	1	221	330	213	2.5	5	24	4892	8.70	977	5	ND	4	13	1	24	2	19	.18	.273	27	8	.30	912	.01	3	.86	.01	.21	2	840
L5+87N 0+75E	1	248	371	176	2.4	6	26	5475	8.66	900	5	ND	3	12	1	23	2	24	.16	.276	28	8	.37	724	.01	2	.96	.01	.20	4	620
L5+87N 0+90E	1	241	241	192	2.2	6	25	4303	8.19	713	5	ND	3	16	1	16	2	36	.29	.246	27	11	.61	914	.01	2	1.35	.01	.22	2	490
L5+87N 0+35E	1	248	165	219	1.7	6	25	4286	7.82	635	5	ND	2	17	1	13	2	43	.37	.237	26	11	.74	995	.01	2	1.52	.01	.25	1	610
L5+75N 0+20E	2	156	153	336	1.9	12	24	2952	8.17	333	5	ND	3	37	1	17	2	60	.41	.180	15	15	.71	748	.08	3	1.32	.07	.16	3	570
STD C/AU-S	17	53	40	132	7.1	67	30	1013	3.95	37	17	7	38	47	17	19	20	59	.46	.094	39	55	.86	173	.07	33	1.85	.06	.15	12	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+75N 0+25E	2	159	145	309	1.8	10	23	2886	8.32	383	5	ND	3	21	1	14	2	55	.24	.184	16	12	.56	744	.02	2	1.21	.02	.15	1	555
L5+75N 0+30E	1	194	134	314	1.5	8	23	2700	7.98	316	5	ND	3	20	1	17	2	60	.25	.176	15	12	.56	649	.03	2	1.28	.02	.15	1	635
L5+75N 0+35E	1	124	164	307	1.9	10	27	4143	8.42	686	5	ND	3	20	1	15	2	45	.19	.195	24	12	.43	796	.01	4	1.16	.02	.16	8	1305
L5+75N 0+40E	1	148	135	249	1.4	10	25	3102	7.96	612	5	ND	3	17	1	15	2	52	.18	.196	22	13	.66	680	.02	3	1.49	.02	.16	3	505
L5+75N 0+45E	1	156	156	262	1.4	10	22	2616	7.67	391	5	ND	3	18	1	16	2	60	.20	.176	19	13	.62	493	.03	2	1.50	.03	.14	1	520
L5+75N 0+50E	2	98	138	282	1.5	6	19	3796	10.53	1057	5	ND	5	9	1	16	2	27	.12	.274	46	10	.31	407	.01	2	1.20	.01	.16	1	1030
L5+75N 0+55E	1	191	172	389	1.8	12	28	5808	8.78	562	5	ND	3	17	2	14	2	43	.14	.225	22	14	.60	474	.02	2	1.58	.03	.18	4	1010
L5+75N 0+60E	1	313	614	160	2.9	6	36	7443	10.19	1137	5	ND	3	11	1	18	2	33	.15	.265	30	11	.68	843	.01	3	1.37	.01	.20	1	172
L5+75N 0+65E	1	265	269	197	1.6	6	27	5257	8.21	796	5	ND	3	11	1	17	2	29	.19	.239	27	10	.64	870	.01	2	1.32	.01	.20	2	395
L5+75N 0+70E	1	231	111	261	1.8	5	26	5612	8.70	955	5	2	3	14	1	22	2	21	.20	.240	25	10	.49	974	.01	2	1.14	.01	.21	1	1485
L5+75N 0+75E	1	206	112	259	2.3	6	23	5130	7.95	887	5	ND	2	12	1	15	3	20	.21	.227	25	8	.52	771	.01	2	1.15	.01	.21	1	805
L5+75N 0+80E	1	192	137	206	1.7	6	22	4656	7.55	748	5	ND	3	18	1	11	2	27	.26	.207	26	9	.64	1118	.01	8	1.33	.01	.22	1	450
L5+62N 0+10E	1	149	78	210	.9	9	22	1666	7.08	152	5	ND	3	35	1	11	3	77	.50	.121	14	13	.71	530	.10	3	1.31	.08	.14	1	121
L5+62N 0+15E	2	223	218	456	2.1	9	27	3433	8.99	412	5	ND	3	16	1	21	2	51	.19	.182	18	12	.45	607	.01	3	1.16	.01	.16	1	1040
L5+62N 0+20E	1	133	172	330	2.1	10	20	2406	7.79	263	5	ND	3	18	1	12	2	56	.24	.179	23	11	.48	452	.02	2	1.27	.02	.13	2	560
L5+62N 0+25E	1	137	182	365	1.5	10	18	1483	7.71	298	5	ND	2	23	1	18	2	60	.25	.162	16	13	.57	374	.04	2	1.35	.04	.15	3	625
L5+62N 0+30E	1	108	103	281	1.0	12	22	3190	7.44	530	5	ND	3	29	1	9	2	54	.36	.169	22	15	.81	605	.06	2	1.50	.06	.16	1	375
L5+62N 0+35E	1	133	120	250	1.2	9	20	2032	6.96	246	5	ND	4	26	1	12	2	66	.30	.144	16	11	.65	427	.06	3	1.35	.06	.13	1	295
L5+62N 0+40E	1	143	133	250	1.1	10	21	2400	6.96	311	5	ND	2	17	1	12	2	63	.20	.150	17	13	.57	470	.03	4	1.39	.02	.13	1	335
L5+62N 0+45E	1	138	118	243	1.1	10	22	2236	7.26	306	5	ND	3	29	1	12	2	68	.35	.154	18	14	.73	467	.06	2	1.49	.06	.14	1	275
L5+62N 0+50E	1	150	129	240	1.1	9	22	2473	7.58	373	5	ND	3	17	1	13	2	63	.18	.165	18	11	.61	407	.03	2	1.47	.03	.13	1	435
L5+62N 0+55E	1	139	151	249	1.5	11	27	3900	8.73	538	5	ND	4	28	1	11	2	59	.30	.221	19	14	.87	241	.08	2	1.70	.08	.17	1	510
L5+62N 0+60E	2	146	95	227	.9	8	29	4753	9.92	786	5	ND	3	14	1	13	3	45	.14	.288	24	14	.62	454	.02	2	1.49	.03	.16	3	385
L5+62N 0+65E	1	153	125	187	1.5	2	33	5621	11.00	1083	5	ND	4	7	1	16	3	18	.03	.383	22	7	.22	410	.01	2	.70	.01	.16	2	1150
L5+62N 0+70E	1	287	211	321	1.7	9	26	5013	7.91	523	5	ND	3	16	1	12	2	36	.22	.203	27	10	.56	790	.01	2	1.34	.01	.18	1	435
L5+62N 0+75E	1	210	147	243	2.1	9	25	3654	8.37	605	5	ND	3	13	1	13	2	33	.17	.215	22	10	.46	628	.01	6	1.09	.01	.18	1	585
L5+62N 0+80E	1	85	189	247	1.0	6	23	3647	6.49	358	5	ND	2	20	1	10	2	38	.50	.187	19	12	.73	326	.01	3	1.49	.01	.28	1	275
L5+50N 0+20E	2	187	202	227	1.2	9	25	4798	7.77	292	5	ND	2	19	1	14	2	56	.11	.187	21	13	.44	938	.03	2	1.23	.01	.13	1	375
L5+50N 0+25E	1	116	147	202	1.2	8	24	3739	9.93	564	5	ND	3	31	1	16	2	56	.27	.266	17	15	.51	647	.06	2	1.21	.06	.14	2	645
L5+50N 0+30E	6	154	100	204	2.0	9	16	2725	8.68	305	5	ND	10	10	1	15	3	35	.10	.159	25	11	.33	358	.05	2	2.14	.07	.14	4	705
L5+50N 0+35E	3	171	262	226	1.5	9	19	1985	10.09	719	5	ND	4	14	1	16	2	50	.08	.270	21	14	.44	509	.01	2	1.45	.01	.19	4	1130
L5+50N 0+40E	1	123	79	204	.8	11	22	2216	7.07	278	5	ND	3	27	1	10	2	69	.31	.166	16	12	.71	475	.06	2	1.59	.06	.14	1	295
L5+50N 0+45E	1	183	156	222	.9	7	27	2823	8.67	314	5	ND	3	10	1	15	2	56	.11	.228	17	11	.46	422	.01	2	1.47	.01	.15	2	560
L5+50N 0+50E	1	269	136	257	1.1	10	30	4548	9.15	572	5	ND	2	14	1	12	2	58	.19	.246	23	14	.73	426	.01	2	1.93	.02	.17	2	635
L5+50N 0+55E	1	361	277	250	4.4	7	34	3017	11.68	2199	5	4	4	6	1	39	2	25	.05	.200	36	9	.25	283	.01	2	.81	.01	.13	1	4070
L5+50N 0+60E	1	416	361	338	4.0	6	38	1899	13.01	1195	5	3	2	8	1	61	3	22	.06	.242	21	8	.14	439	.01	2	.65	.01	.13	1	1870
STD C/AU-S	18	59	42	132	6.5	68	30	1025	4.01	42	16	8	38	49	17	19	19	60	.47	.096	40	57	.88	183	.07	33	1.93	.06	.15	11	53

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L5+50N 0+65E	1	743	245	521	3.4	14	36	5100	7.82	627	5	ND	4	18	6	21	2	34	.26	.181	41	10	.70	424	.02	3	1.63	.03	.14	1	475
L5+50N 0+70E	2	531	310	487	3.3	11	39	4271	8.88	525	5	ND	3	17	3	18	2	59	.36	.227	28	13	.84	368	.01	2	1.68	.01	.16	1	520
L5+50N 0+75E	1	214	249	463	2.8	7	29	3806	8.79	583	5	ND	2	18	5	24	2	37	.32	.224	22	11	.54	430	.01	2	1.01	.01	.18	1	825
L5+50N 0+80E	2	197	139	220	2.2	3	27	3708	8.78	570	5	ND	3	12	1	15	2	45	.13	.264	16	9	.54	325	.02	2	1.18	.02	.15	1	575
L5+37N 0+20E	1	115	128	185	1.1	5	18	2152	9.20	605	5	ND	4	11	2	9	2	37	.14	.258	19	8	.34	474	.01	2	1.03	.01	.10	1	595
L5+37N 0+25E	1	104	97	172	1.0	7	15	1417	5.92	238	5	ND	2	11	2	5	2	51	.16	.159	15	9	.47	418	.01	4	1.37	.01	.09	1	305
L5+37N 0+30E	2	383	155	192	6.7	6	36	6329	10.42	919	5	ND	3	20	2	64	2	47	.10	.305	17	12	.48	750	.01	2	1.74	.01	.11	1	685
L5+37N 0+35E	2	231	327	287	1.6	7	22	2012	10.41	849	5	ND	3	9	1	14	2	55	.08	.267	20	12	.50	364	.01	2	1.79	.01	.12	2	1005
L5+37N 0+40E	6	125	139	199	.7	8	42	6287	11.97	1232	5	ND	3	7	1	16	2	45	.07	.253	36	15	.45	261	.02	2	2.66	.02	.09	10	545
L5+37N 0+45E	6	228	167	302	1.1	9	25	3824	9.19	421	5	ND	5	6	4	17	2	38	.03	.155	24	13	.39	178	.01	2	2.57	.02	.11	2	710
L5+37N 0+50E	5	192	241	197	3.2	7	17	1668	9.96	984	5	ND	4	7	2	71	2	46	.07	.243	12	15	.46	166	.01	3	1.84	.01	.10	2	750
L5+37N 0+55E	4	362	265	414	1.3	9	43	23632	9.16	566	5	ND	2	4	5	16	2	45	.02	.197	14	12	.47	361	.01	2	2.87	.01	.11	2	1120
L5+37N 0+60E	3	337	314	186	1.4	2	36	4588	12.82	1429	5	ND	6	5	2	53	2	29	.16	.509	23	9	.58	91	.01	2	1.34	.01	.13	1	285
L5+37N 0+65E	3	216	192	332	2.4	8	16	2025	8.75	381	5	ND	3	9	2	24	2	36	.02	.157	23	10	.37	223	.01	3	1.52	.01	.17	3	775
L5+37N 0+70E	3	101	178	230	1.9	4	23	4188	10.46	489	5	ND	3	7	2	16	2	47	.03	.243	14	10	.28	173	.01	2	1.40	.02	.12	2	715
L5+25N 0+10E	1	124	73	182	.8	8	18	2283	6.36	201	5	ND	3	20	1	9	2	67	.32	.163	18	12	.78	910	.01	2	1.73	.01	.10	1	195
L5+25N 0+15E	1	127	90	211	.9	12	19	2206	7.00	283	5	ND	3	16	1	10	2	64	.27	.187	18	13	.71	720	.02	2	1.61	.01	.09	1	710
L5+25N 0+20E	6	282	122	256	.6	15	24	3753	10.35	697	5	ND	3	7	2	13	2	47	.10	.277	23	16	.54	340	.01	3	2.19	.01	.10	3	520
L5+25N 0+25E	8	185	154	296	1.2	11	32	3291	12.89	891	5	ND	3	8	1	25	2	45	.10	.272	18	15	.54	164	.01	2	1.77	.02	.11	4	875
L5+25N 0+30E	6	187	114	216	.9	10	27	3002	10.12	840	5	ND	4	6	2	20	2	41	.06	.168	19	14	.47	158	.01	2	2.25	.01	.11	1	2510
L5+25N 0+35E	6	100	166	208	.6	5	24	2945	11.32	996	5	ND	3	5	1	15	2	52	.04	.194	17	15	.44	161	.01	2	2.25	.01	.11	3	550
L5+25N 0+40E	5	66	92	113	.2	3	17	4738	7.74	439	5	ND	2	6	1	11	2	56	.03	.211	15	10	.19	177	.01	2	1.96	.02	.10	1	215
L5+25N 0+45E	5	83	119	134	.4	4	16	3825	8.70	551	5	ND	2	7	1	15	2	60	.03	.241	14	11	.21	180	.01	2	2.13	.01	.11	2	320
L5+25N 0+50E	4	94	137	154	1.5	5	8	1430	7.94	418	5	ND	2	8	1	28	2	52	.04	.229	12	8	.20	206	.01	2	1.82	.01	.12	3	520
L5+25N 0+55E	3	156	117	163	3.0	4	18	3468	9.75	694	5	ND	2	10	1	27	2	61	.04	.234	13	11	.22	331	.01	2	2.02	.01	.13	2	225
L5+25N 0+60E	4	101	154	182	3.6	4	7	1125	7.74	406	5	ND	2	10	1	27	3	56	.03	.186	10	7	.11	291	.01	3	1.45	.01	.12	3	465
L5+25N 0+65E	5	96	180	166	3.7	6	9	1660	9.27	448	5	ND	2	11	1	22	2	53	.03	.221	12	11	.11	316	.01	2	1.69	.01	.14	2	520
L5+25N 0+70E	9	86	230	215	5.0	3	40	4994	17.81	478	5	6	3	12	1	26	2	27	.02	.311	17	9	.07	357	.01	2	1.73	.02	.22	4	3495
B.C. 0+25S	2	149	92	213	1.3	25	26	3312	6.38	250	5	ND	4	26	1	6	2	43	.39	.143	22	12	.55	671	.01	2	1.14	.01	.15	1	335
B.C. 0+50S	4	130	101	225	1.8	20	29	2738	7.19	408	5	ND	4	46	2	5	2	59	.62	.129	17	12	.64	424	.09	2	1.11	.10	.15	1	225
B.C. 0+75S	3	141	59	164	1.2	22	17	1418	4.19	203	5	ND	4	26	1	2	2	25	.38	.106	16	8	.27	412	.01	5	.72	.01	.13	1	208
B.C. 1+00S	4	126	139	202	2.0	20	21	1749	5.27	256	5	ND	4	25	1	5	3	26	.29	.127	15	7	.28	382	.01	5	.64	.01	.11	1	250
B.C. 1+25S	7	178	111	198	2.1	17	23	2537	6.00	295	5	ND	4	26	1	4	2	28	.26	.131	16	7	.27	439	.01	3	.69	.01	.12	1	265
B.C. 1+50S	6	173	171	219	2.0	18	25	2859	6.38	325	5	ND	5	27	1	9	2	30	.25	.135	17	7	.29	476	.01	3	.73	.01	.12	1	320
B.C. 1+75S	4	147	81	196	1.5	22	21	2015	5.16	330	5	ND	5	26	1	5	2	33	.34	.122	16	8	.28	481	.01	3	.73	.02	.12	1	225
B.C. 2+00S	3	140	56	199	1.0	26	22	1585	5.55	396	5	ND	3	31	1	5	2	56	.89	.107	15	14	.61	334	.03	2	1.22	.01	.12	1	182
STD C/AU-S	18	60	41	132	7.6	70	30	1027	3.99	41	18	7	39	49	17	17	21	61	.47	.097	40	55	.87	179	.07	33	1.92	.06	.15	11	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
B.C. 2+25S	3	145	66	178	1.6	24	17	1409	4.46	212	5	ND	4	23	2	4	3	28	.35	.113	16	9	.29	402	.01	5	.74	.02	.13	1	325
B.C. 2+50S	5	190	92	245	1.5	28	24	2181	5.73	411	5	ND	4	39	1	9	2	50	1.05	.127	18	15	.60	436	.03	10	1.19	.01	.14	1	325
B.C. 2+75S	4	195	128	336	2.3	29	25	2206	6.15	605	5	ND	4	29	2	11	2	49	.69	.110	17	15	.60	357	.02	5	1.20	.01	.13	1	350
B.C. 3+00S	3	142	126	325	2.9	27	23	1681	6.08	655	5	ND	3	38	1	12	2	55	1.35	.102	13	16	.73	205	.05	8	1.22	.02	.12	1	350
B.C. 3+25S	2	133	127	349	3.2	25	21	1580	5.74	582	5	ND	3	43	2	9	2	52	1.89	.098	11	16	.68	187	.03	16	1.19	.01	.14	1	345
B.C. 3+50S	2	106	103	298	3.5	22	18	1240	5.35	465	5	ND	2	41	1	9	2	49	1.98	.098	9	13	.57	129	.04	16	.93	.01	.09	1	385
B.C. 3+75S	3	170	194	517	5.3	26	24	2166	6.56	617	5	ND	2	36	1	12	3	53	1.27	.108	14	15	.75	213	.03	3	1.26	.01	.15	1	495
B.C. 4+00S	3	153	157	318	2.6	27	24	1830	6.35	600	5	ND	2	26	1	12	2	54	.58	.100	13	17	.66	217	.03	3	1.10	.01	.10	1	530
B.C. 4+25S	4	161	173	404	2.5	28	24	2235	5.89	438	5	ND	4	41	1	13	2	44	.97	.113	15	15	.56	342	.03	6	1.09	.03	.15	1	275
B.C. 4+50S	2	138	165	389	1.6	27	22	2037	5.07	252	5	ND	3	38	1	10	2	28	1.14	.109	13	11	.31	376	.01	2	.85	.01	.17	1	78
B.C. 4+75S	2	130	163	389	1.7	27	21	2059	5.23	269	5	ND	3	29	1	9	2	29	.75	.116	15	10	.29	380	.01	2	.85	.01	.17	1	160
B.C. 5+00S	3	151	185	502	4.9	26	23	2161	5.99	394	5	ND	3	32	3	10	2	34	.95	.118	13	12	.42	308	.01	4	.91	.01	.16	1	345
B.C. 5+25S	3	163	221	608	6.2	26	24	2186	6.75	545	5	ND	2	34	2	14	3	43	1.50	.106	13	16	.65	171	.03	3	1.07	.01	.17	1	615
B.C. 5+50S	4	200	307	760	9.7	26	26	2476	7.25	642	5	ND	3	30	4	19	2	45	.68	.126	16	15	.65	201	.02	4	1.09	.01	.14	1	925
B.C. 5+75S	5	180	196	516	4.4	33	24	2377	5.75	433	5	ND	3	48	3	14	2	39	1.60	.117	12	16	.54	236	.02	8	1.01	.01	.16	1	615
B.C. 6+00S	4	135	134	294	2.7	27	18	1605	4.51	314	5	ND	2	46	2	13	2	30	1.71	.094	9	14	.43	150	.02	13	.69	.01	.09	1	315
B.C. 6+25S	5	169	308	544	5.7	29	23	2527	5.54	507	5	ND	3	38	2	28	2	36	.70	.133	16	11	.41	368	.01	2	.90	.02	.15	3	235
B.C. 6+50S	6	248	312	917	7.5	28	24	2626	6.12	458	5	ND	4	41	5	18	2	45	1.50	.117	16	16	.53	337	.01	6	1.08	.01	.17	1	585
B.C. 6+75S	7	229	164	356	3.4	22	16	1745	4.25	290	5	ND	2	70	2	16	2	28	2.65	.098	9	8	.29	362	.01	7	.68	.01	.18	1	385
B.C. 7+00S	5	252	659	1172	12.3	31	29	3334	7.68	1293	5	ND	4	41	8	40	2	38	.58	.131	17	15	.44	366	.01	4	.99	.01	.16	1	855
B.C. 7+25S	5	178	291	509	4.9	24	19	2064	5.15	469	5	ND	3	64	2	24	2	33	1.87	.125	12	11	.42	298	.01	7	.81	.01	.14	1	225
B.C. 7+50S	5	171	332	674	5.4	26	22	2457	5.09	422	5	ND	2	51	3	25	4	27	1.26	.122	15	12	.39	398	.01	3	.88	.01	.16	2	235
B.C. 7+75S	4	131	255	386	4.2	22	15	1660	4.10	357	5	ND	2	43	1	25	3	23	1.02	.123	12	9	.35	196	.01	4	.64	.01	.11	6	176
B.C. 8+00S	5	159	377	475	4.6	27	19	2343	5.10	448	5	ND	3	30	1	30	2	34	.60	.138	15	10	.41	236	.01	3	.81	.01	.12	1	149
B.C. 8+25S	3	162	284	449	4.6	25	22	2457	6.04	571	5	ND	2	46	1	22	2	55	1.35	.168	12	16	.71	328	.01	6	1.24	.01	.17	1	205
B.C. 8+50S	2	184	212	446	3.3	23	28	2809	7.46	859	5	ND	1	33	1	23	2	67	.82	.230	12	20	.84	361	.03	2	1.36	.03	.15	1	435
B.C. 8+75S	1	140	128	316	2.0	20	21	2166	6.09	515	5	ND	1	51	1	15	2	71	1.46	.201	10	21	1.01	351	.05	2	1.51	.05	.19	1	335
B.C. 9+00S	1	161	183	389	3.2	19	22	2531	6.65	719	5	ND	1	50	1	20	2	77	1.77	.255	11	20	.87	385	.01	2	1.42	.01	.18	1	325
B.C. 9+25S	1	147	159	397	2.8	24	26	2696	7.11	758	5	ND	2	52	1	20	2	71	.87	.210	11	19	1.02	309	.13	10	1.33	.11	.14	1	465
B.C. 9+50S	3	229	198	529	2.8	21	26	3236	7.17	1179	5	ND	1	32	1	22	2	46	.61	.231	13	12	.57	410	.01	2	1.02	.02	.13	1	445
B.C. 9+75S	3	231	158	553	2.9	17	24	3222	6.82	1229	5	ND	2	37	2	28	2	42	.72	.238	11	10	.48	357	.01	6	.91	.01	.15	1	450
B.C. 10+00S	1	187	146	395	2.8	20	25	2745	7.11	799	5	ND	1	30	1	19	2	63	.87	.255	11	18	.82	353	.01	4	1.31	.01	.15	1	505
B.C. 10+25S	1	170	218	457	3.5	23	25	2692	7.12	776	5	ND	1	31	1	20	2	73	.82	.258	12	20	.86	354	.02	2	1.31	.02	.14	1	825
B.C. 10+50S	1	168	110	291	2.2	18	22	2161	6.62	500	5	ND	1	24	1	16	2	63	.77	.291	10	18	.88	232	.01	2	1.32	.01	.13	1	345
B.C. 10+75S	1	185	109	292	2.3	17	24	2300	7.04	522	5	ND	1	22	1	16	2	62	.70	.296	11	17	.83	353	.01	2	1.28	.01	.14	1	365
B.C. 11+00S	1	204	117	332	2.3	18	25	2708	6.93	458	5	ND	2	24	1	16	2	58	.68	.261	10	16	.72	346	.01	2	1.22	.01	.15	1	315
STD C/AU-S	18	58	44	132	6.6	69	29	1020	3.98	39	18	7	38	48	18	16	22	59	.46	.095	39	55	.86	179	.07	33	1.89	.06	.15	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
B.C. 11+25S	1	197	88	268	2.0	16	24	2162	6.84	386	5	ND	3	30	1	13	3	62	.86	.302	10	17	.80	303	.01	8	1.40	.05	.19	1	231
B.C. 11+50S	1	162	194	387	2.8	20	22	2454	6.82	647	5	ND	2	55	1	19	2	83	2.12	.255	11	21	.97	380	.01	4	1.68	.01	.23	1	360
B.C. 11+75S	1	161	169	365	2.6	20	23	2479	6.95	741	5	ND	2	38	1	19	2	75	.95	.250	11	19	.97	343	.04	3	1.54	.04	.18	1	450
B.C. 12+00S	1	172	201	446	3.3	23	24	2943	7.18	826	5	ND	2	37	1	22	2	79	1.05	.241	13	21	.87	388	.01	3	1.49	.02	.18	1	450
B.C. 12+25S	1	156	228	474	4.3	21	21	2562	6.72	647	5	ND	1	63	2	19	2	90	2.43	.214	12	20	.89	531	.01	4	1.65	.01	.25	1	265
B.C. 12+50S	2	201	237	576	4.3	34	31	3970	8.37	1215	5	ND	3	37	2	30	2	84	1.12	.208	15	26	.78	399	.01	7	1.51	.01	.21	1	510
B.C. 12+75S	1	156	202	416	2.8	21	22	2491	6.75	639	5	ND	2	58	1	19	2	87	2.11	.251	12	21	.95	438	.01	3	1.63	.01	.21	1	330
B.C. 13+00S	1	161	228	463	3.0	21	22	2673	6.92	680	5	ND	1	49	1	19	2	87	1.71	.243	13	21	.86	435	.01	4	1.55	.01	.21	1	360
B.C. 13+25S	1	154	188	402	2.8	20	21	2410	6.52	622	5	ND	2	64	1	18	2	85	2.28	.229	11	20	.94	461	.01	7	1.61	.01	.22	1	260
B.C. 13+50S	1	157	165	395	2.8	24	23	2499	6.85	770	5	ND	2	51	1	22	2	79	1.70	.240	12	23	.91	357	.01	3	1.57	.01	.21	1	420
B.C. 13+75S	1	163	176	405	3.2	22	23	2486	6.92	732	5	ND	2	53	1	21	4	80	1.75	.268	13	21	.92	361	.01	8	1.54	.01	.20	1	410
B.C. 14+00S	1	172	212	450	3.0	21	23	2660	6.94	752	5	ND	2	54	1	18	2	85	1.83	.242	12	21	.94	396	.01	3	1.65	.01	.22	1	210
B.C. 14+25S	1	186	242	517	3.5	22	24	2978	7.38	850	5	ND	2	44	2	21	2	84	1.37	.259	14	20	.90	431	.01	2	1.57	.01	.21	1	370
B.C. 14+50S	1	192	273	517	3.6	22	25	3052	7.61	866	5	ND	2	36	1	20	2	89	1.04	.258	14	20	.93	444	.01	8	1.64	.01	.20	1	360
B.C. 14+75S	1	176	204	427	2.9	18	23	2623	6.98	767	5	ND	2	33	1	18	2	81	.87	.284	13	19	.95	380	.01	2	1.53	.01	.17	1	430
B.C. 15+00S	1	171	291	524	4.2	24	25	2567	7.51	754	5	ND	2	59	1	22	2	87	2.20	.247	13	21	.89	443	.01	4	1.52	.01	.20	1	650
B.C. 15+25S	1	211	244	442	3.3	20	25	3205	7.59	962	5	ND	2	34	1	22	2	80	.90	.250	13	18	.89	453	.01	3	1.56	.01	.20	1	560
B.C. 15+50S	2	173	425	634	5.9	29	28	2945	8.39	932	5	ND	2	43	1	29	2	99	1.35	.252	15	25	.86	438	.01	4	1.50	.01	.18	1	340
B.C. 15+75S	1	189	469	711	5.4	29	29	3914	8.07	1058	5	ND	2	49	3	27	4	86	1.60	.239	15	21	.66	601	.01	3	1.30	.01	.19	1	430
B.C. 16+00S	1	175	208	401	3.0	16	22	2768	6.33	788	5	ND	1	32	1	19	2	68	.90	.248	11	16	.80	391	.01	12	1.35	.01	.17	1	560
B.C. 16+25S	1	211	203	294	1.7	16	20	2617	6.06	1010	5	ND	3	47	1	15	4	52	1.07	.222	11	15	.95	354	.01	8	1.48	.02	.17	1	670
B.C. 16+50S	1	503	642	680	4.6	13	31	5411	9.00	3103	5	ND	2	37	2	36	5	48	.59	.228	12	14	.74	466	.01	2	1.42	.01	.21	1	1705
B.C. 16+75S	1	160	98	221	1.4	18	21	2458	5.74	798	5	ND	2	43	1	17	2	50	.93	.211	11	17	.84	349	.01	4	1.30	.01	.14	1	430
B.C. 17+00S	1	127	64	173	1.1	19	17	1599	4.88	475	5	ND	3	81	1	9	2	45	1.81	.168	9	16	.96	315	.01	8	1.60	.01	.21	1	410
B.C. 17+25S	1	230	89	201	1.8	16	27	3556	7.08	1493	5	ND	2	30	1	28	2	63	.68	.254	11	18	.92	427	.01	3	1.43	.01	.18	1	705
B.C. 17+50S	1	235	94	202	1.8	15	27	3545	7.26	1448	5	ND	3	31	1	26	2	64	.73	.256	11	19	.94	421	.01	11	1.47	.01	.18	1	810
M.C. 0+00S	1	90	149	254	1.2	14	7	368	3.27	164	5	ND	2	25	1	7	2	27	.49	.146	17	10	.35	397	.01	4	1.15	.01	.16	1	48
M.C. 0+25S	2	139	204	387	2.3	22	15	1750	4.54	196	5	ND	3	28	1	14	2	30	.55	.179	22	10	.31	329	.01	5	1.00	.01	.16	1	92
M.C. 0+50S	4	151	256	417	4.4	27	19	2442	4.62	290	5	ND	4	29	2	24	2	27	.46	.157	18	10	.29	306	.01	4	.82	.01	.14	3	108
M.C. 0+75S	7	165	279	468	4.4	32	21	2466	4.87	354	5	ND	5	34	2	28	2	28	.52	.155	19	10	.31	363	.01	3	.89	.01	.17	2	125
M.C. 1+00S	6	178	322	453	4.9	31	23	2615	5.26	427	5	ND	4	30	2	27	2	29	.56	.162	20	11	.30	450	.01	11	.92	.01	.19	3	212
M.C. 1+25S	4	151	214	367	3.1	28	24	2471	5.35	451	5	ND	5	32	2	23	2	33	.52	.154	19	10	.36	474	.02	4	.95	.02	.16	4	164
M.C. 1+50S	7	190	467	634	5.6	32	25	2940	6.05	627	5	ND	5	35	4	35	2	34	.64	.161	18	12	.40	354	.01	6	.95	.02	.18	1	340
M.C. 1+75S	7	185	466	608	6.5	31	26	2671	6.47	680	5	ND	4	34	3	36	2	46	.80	.164	18	13	.49	304	.01	12	1.01	.01	.16	1	350
M.C. 2+00S	5	169	211	472	2.6	35	35	3231	8.36	966	5	ND	4	29	2	21	2	91	.65	.147	18	17	.81	286	.05	8	1.62	.02	.13	1	220
M.C. 2+25S	6	193	338	502	4.6	42	42	3280	7.66	750	5	ND	4	27	3	26	2	87	.78	.126	22	22	1.11	303	.04	9	1.88	.01	.14	1	144
STD C/AU-S	17	58	43	132	6.7	69	30	1023	3.98	41	21	7	40	48	19	18	20	60	.46	.094	40	55	.87	181	.07	33	1.93	.06	.15	12	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
M.C. 2+50S	9	244	410	682	4.7	32	29	4832	6.51	865	5	ND	4	32	6	28	2	37	.53	.161	19	10	.39	390	.01	5	.83	.01	.14	1	280
M.C. 2+75S	3	226	179	413	2.7	40	37	3152	8.39	1172	5	ND	4	31	4	20	2	75	.47	.135	17	26	.97	334	.05	3	1.53	.04	.12	1	550
M.C. 3+00S	6	262	262	565	4.1	22	27	4548	7.43	1083	5	ND	4	36	5	28	4	36	.56	.201	15	9	.37	444	.01	3	.78	.01	.16	1	530
M.C. 3+25S	8	272	362	829	5.3	27	33	4955	7.98	1395	5	ND	4	37	6	34	2	40	.54	.187	17	12	.45	478	.01	5	.92	.01	.15	1	710
M.C. 3+50S	6	264	232	574	3.4	21	29	4247	7.38	1235	5	ND	4	38	5	28	2	42	.59	.215	14	10	.49	543	.01	6	.94	.02	.15	1	460
M.C. 3+75S	3	313	164	735	3.6	16	29	4613	8.46	1600	5	ND	4	35	6	36	2	40	.61	.261	13	8	.36	427	.01	7	.83	.01	.17	1	690
M.C. 4+00S	4	297	233	596	4.6	21	32	3772	8.38	1400	5	ND	4	27	4	19	2	64	.47	.148	20	16	.72	500	.01	6	1.49	.02	.15	1	1330
M.C. 4+25S	3	312	232	760	4.3	22	36	4687	8.81	1329	5	ND	4	27	7	24	2	59	.49	.180	16	15	.55	472	.01	4	1.16	.02	.16	1	1720
M.C. 4+50S	2	267	212	505	4.0	19	30	2976	8.51	759	5	ND	2	26	4	24	2	63	.59	.244	16	18	.73	393	.02	3	1.32	.02	.16	2	850
M.C. 4+75S	1	257	176	530	3.6	20	32	3931	7.71	864	5	ND	3	28	5	26	2	53	.61	.241	12	13	.55	364	.01	5	1.08	.01	.15	1	740
M.C. 5+00S	1	248	156	439	2.9	22	33	3488	7.82	780	5	ND	3	29	4	25	2	62	.70	.239	12	16	.67	380	.02	5	1.20	.02	.16	2	550
M.C. 5+25S	1	221	97	262	2.0	19	29	2844	7.31	538	5	ND	3	31	3	17	2	51	.78	.320	11	11	.50	225	.01	7	.93	.01	.17	1	390
M.C. 5+50S	1	230	137	312	2.9	17	29	3061	7.40	747	5	ND	3	26	3	23	2	49	.65	.269	12	12	.64	219	.01	7	1.06	.01	.15	1	840
M.C. 5+75S	1	222	122	305	2.5	21	30	3359	7.70	841	5	ND	2	27	3	23	3	48	.64	.264	12	14	.56	186	.01	9	.99	.01	.15	1	810
M.C. 6+00S	1	195	112	289	2.3	21	27	3012	7.19	677	5	ND	2	26	3	18	3	51	.66	.239	11	15	.62	207	.01	4	1.05	.01	.15	1	570
M.C. 6+25S	1	190	126	370	2.6	21	30	3299	7.55	940	5	ND	3	30	3	19	2	52	.65	.233	12	14	.68	249	.01	3	1.13	.01	.15	1	840
M.C. 6+50S	1	220	230	504	3.1	20	31	3752	7.71	1051	5	ND	2	31	2	21	2	51	.62	.240	12	16	.70	447	.01	5	1.18	.01	.16	1	1150
M.C. 6+75S	1	181	200	401	3.0	21	27	3359	7.14	1181	5	ND	1	28	2	26	2	52	.60	.224	11	16	.73	386	.01	3	1.19	.01	.15	1	810
M.C. 7+00S	2	235	381	559	4.4	25	34	4453	8.65	1679	5	ND	3	29	4	34	2	59	.62	.205	13	17	.71	519	.01	5	1.31	.01	.18	1	950
M.C. 7+25S	2	214	208	442	3.9	31	32	3900	8.25	1210	5	ND	3	31	5	28	2	69	.64	.212	15	21	.72	398	.01	5	1.26	.01	.16	1	680
M.C. 7+50S	2	206	263	655	5.4	22	24	3408	7.84	1430	5	ND	2	26	4	35	2	58	.56	.253	14	14	.42	395	.01	6	.93	.01	.16	1	1100
M.C. 7+75S	2	351	326	573	5.7	17	29	3577	7.32	1389	5	ND	2	28	4	32	2	54	.52	.220	14	10	.52	562	.01	4	1.09	.01	.15	1	920
M.C. 8+00S	2	251	290	631	4.0	22	31	3859	7.33	1218	5	ND	2	32	3	30	2	50	.64	.233	13	11	.47	533	.01	2	.94	.01	.15	1	1180
M.C. 8+25S	2	268	402	693	4.2	21	30	4627	8.13	2029	5	ND	2	31	4	21	2	61	.64	.226	15	14	.59	620	.01	2	1.14	.01	.17	1	670
M.C. 8+50S	3	186	290	662	3.9	27	30	3210	8.09	1162	5	ND	2	32	4	27	2	73	.77	.271	15	18	.74	421	.01	3	1.27	.01	.15	1	490
M.C. 8+75S	2	206	584	867	7.1	30	32	4355	9.20	1381	5	ND	2	28	6	26	2	101	.67	.236	19	23	.76	603	.01	2	1.40	.01	.15	1	340
M.C. 9+00S	2	185	442	688	6.5	32	31	4145	8.14	939	5	ND	2	33	5	25	2	81	.72	.251	15	19	.58	533	.01	2	1.06	.01	.13	1	740
M.C. 9+25S	2	201	388	731	4.7	27	30	4887	7.92	1046	5	ND	2	30	6	29	2	62	.63	.232	14	12	.44	668	.01	4	.88	.01	.14	1	530
M.C. 9+50S	2	392	472	489	4.3	19	31	5317	9.42	1783	5	ND	3	51	4	27	2	70	.79	.222	14	16	.97	439	.12	9	1.53	.08	.17	1	1470
M.C. 9+75S	3	682	1322	1316	8.6	15	39	7244	11.94	5389	5	3	1	53	7	46	2	47	.58	.214	14	13	.70	468	.01	2	1.42	.01	.19	1	2620
M.C. 10+00S	2	367	349	697	5.8	21	33	5451	9.69	2128	5	ND	1	41	4	39	2	61	.66	.228	15	16	.64	352	.01	4	1.18	.01	.16	1	1750
M.C. 10+25S	2	704	200	341	5.2	12	28	5385	11.90	2886	5	ND	2	58	3	32	3	48	.86	.222	12	9	.53	413	.01	5	1.04	.01	.17	1	2410
M.C. 10+50S	1	231	132	266	2.2	20	30	3508	7.67	1187	5	ND	2	28	3	21	2	66	.65	.234	13	18	.82	532	.01	2	1.30	.01	.14	1	760
M.C. 10+75S	1	228	83	190	1.5	16	26	3407	6.93	1292	5	ND	2	27	1	18	2	60	.65	.234	10	16	.86	458	.01	5	1.34	.01	.16	1	540
M.C. 11+00S	2	356	205	381	2.9	25	38	5891	11.11	3723	5	ND	1	39	2	60	2	66	.63	.171	16	23	.75	607	.01	2	1.26	.01	.17	2	1070
STD C/AU-S	18	59	40	132	6.8	69	30	1024	4.03	40	19	7	39	49	18	16	21	60	.47	.093	40	56	.87	182	.07	33	1.96	.06	.16	13	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+75N 0+30E	1	10	111	18	1.2	2	1	28	1.90	262	5	ND	2	24	1	2	4	7	.03	.064	13	1	.03	618	.01	4	.39	.01	.30	1	545
L5+75N 0+35E	1	9	18	78	.5	2	9	1836	3.11	244	5	ND	2	40	1	3	4	21	1.75	.108	11	5	.76	83	.01	4	1.33	.01	.35	1	37
L5+75N 0+50E	1	22	19	94	.7	3	8	1960	3.66	293	5	ND	2	32	1	2	2	31	1.30	.111	11	7	.81	80	.01	3	1.47	.02	.27	1	68
L5+75N 0+53E	1	86	14	240	1.0	4	10	2551	4.58	312	5	ND	2	17	1	3	2	34	.63	.123	14	7	.93	38	.01	2	1.50	.01	.28	1	129
L5+71N 0+47E	1	19	22	132	.3	3	9	1435	3.46	133	5	ND	2	31	1	2	2	34	1.20	.118	13	7	.84	127	.01	2	1.52	.01	.31	1	20
L5+64N 0+56E	1	42	20	144	.7	4	10	1707	3.75	200	5	ND	2	29	1	2	2	37	1.02	.117	14	7	.77	28	.01	2	1.23	.02	.26	1	63
L5+64N 0+58E	1	23	20	123	.6	3	8	1249	3.57	224	5	ND	2	19	1	2	2	31	.62	.122	13	7	.80	56	.01	3	1.37	.01	.30	1	70
L5+63N 0+53E	1	22	24	152	.5	3	9	2157	3.60	244	5	ND	2	46	1	2	2	34	2.21	.114	13	7	.87	48	.01	3	1.38	.01	.28	1	99
L5+62N 0+20E	1	17	114	67	1.1	1	2	87	3.90	115	5	ND	1	8	1	3	2	8	.02	.069	7	1	.02	471	.01	2	.37	.01	.25	1	310
L5+62N 0+25E	1	11	24	557	.3	3	10	3234	4.07	180	5	ND	2	46	2	2	2	29	2.77	.117	11	6	.72	28	.01	2	1.20	.01	.29	1	215
L5+62N 0+30E	10	36	852	51	1.5	3	1	49	2.55	315	5	ND	2	200	1	2	2	10	.02	.060	9	3	.01	606	.01	2	.25	.01	.15	1	1050
L5+62N 0+40E	1	46	32	192	.8	4	18	2274	5.66	407	5	ND	2	35	1	2	2	79	1.54	.169	11	8	1.62	54	.01	3	1.96	.01	.24	1	85
L5+62N 0+50E	1	29	27	189	.4	5	10	2447	3.90	177	5	ND	3	24	1	2	2	38	1.03	.116	13	8	1.04	116	.01	2	1.61	.01	.22	1	33
L5+60N 0+05E	1	39	20	103	.9	2	7	850	4.33	113	5	ND	3	13	1	2	2	24	.37	.143	8	6	.59	40	.01	2	.94	.01	.21	1	152
L5+53N 0+04E	1	193	34	214	.4	7	11	1395	3.60	148	5	ND	1	24	1	2	2	20	1.10	.044	20	7	.80	63	.01	2	1.28	.01	.26	1	59
L5+53N 0+60E	1	180	100	163	1.1	7	7	1792	2.43	127	5	ND	2	34	1	2	3	19	1.58	.099	14	6	.65	163	.01	6	1.15	.01	.26	1	31
L5+52N 0+57E	1	88	102	40	4.6	3	6	138	3.81	578	5	ND	2	14	1	18	4	5	.04	.032	6	1	.02	25	.01	4	.25	.01	.19	3	2475
L5+50N 0+20E	1	26	70	72	2.4	1	2	69	3.29	385	5	ND	1	75	1	3	3	6	.05	.115	15	1	.02	1217	.01	2	.33	.01	.20	1	225
L5+50N 0+25E	1	10	41	54	.7	2	3	448	3.19	235	5	ND	3	78	1	2	2	15	.09	.121	18	4	.30	969	.01	4	.63	.01	.20	1	189
L5+50N 0+30E	1	72	11	122	.6	4	7	1704	2.88	258	5	ND	2	47	1	2	2	22	2.05	.111	15	6	.55	128	.01	3	1.13	.01	.29	1	48
L5+50N 0+32E	1	12	12	122	.3	3	10	2251	3.85	347	5	ND	2	39	1	2	2	41	1.81	.120	17	8	1.07	60	.01	2	1.43	.01	.26	1	82
L5+50N 0+35E	1	13	103	72	1.2	2	2	178	5.77	490	5	ND	2	16	1	2	2	42	.03	.134	11	1	.17	267	.01	3	.48	.01	.26	1	580
L5+50N 0+40E	1	35	19	186	1.1	5	10	1407	5.60	444	5	ND	3	30	1	2	2	80	.42	.209	12	10	1.54	414	.09	3	2.07	.01	.20	2	125
L5+50N 0+42E	1	26	30	183	.8	6	16	1765	5.86	251	5	ND	3	31	1	2	2	101	.52	.120	12	9	1.73	60	.03	2	2.18	.01	.20	1	141
L5+50N 0+45E	1	14	62	72	.7	4	10	903	5.20	117	5	ND	3	13	1	2	4	55	.48	.141	13	8	.80	36	.01	3	1.10	.01	.23	2	32
L5+50N 0+55E	1	152	27	232	.7	10	11	2254	3.68	186	5	ND	3	16	2	2	2	22	.38	.057	28	9	1.31	227	.01	2	1.89	.01	.28	1	43
L5+50N 0+60E	1	99	55	146	1.5	7	12	1513	3.44	189	5	ND	2	34	1	3	3	19	1.31	.059	10	10	1.15	108	.01	2	1.67	.01	.31	1	36
L5+49N 0+00E	1	143	348	557	1.0	6	9	1886	2.90	217	5	ND	2	55	8	2	2	16	2.53	.043	11	8	.84	67	.01	2	1.32	.01	.29	1	67
L5+47N 0+00E	1	85	59	34	6.2	3	6	124	4.29	474	5	ND	3	9	1	34	2	15	.19	.136	10	1	.05	28	.01	4	.43	.01	.25	1	775
L5+47N 0+04E	1	261	28	150	.6	6	10	1634	2.71	136	5	ND	2	32	1	2	3	18	1.30	.084	15	7	.90	108	.01	2	1.32	.01	.24	1	31
L5+47N 0+05E	1	418	38	123	2.2	4	13	1450	3.56	363	5	ND	3	19	1	23	2	27	.62	.132	17	7	.72	40	.01	4	1.15	.01	.25	1	106
L5+46N 0+00E	1	70	49	53	6.7	4	7	73	4.65	282	5	ND	3	10	1	42	2	15	.18	.145	10	2	.04	29	.01	4	.47	.01	.29	2	780
L5+46N 0+02E	1	153	77	245	1.3	5	11	1758	2.65	124	5	ND	2	39	2	2	2	17	1.76	.060	16	8	.97	143	.01	2	1.38	.01	.27	1	117
L5+45N 0+06E	1	118	113	84	4.9	2	3	296	5.35	675	5	ND	3	30	1	33	3	29	.07	.124	13	2	.19	266	.01	3	.55	.01	.28	1	1455
L5+45N 0+60E	1	58	62	35	6.8	5	8	92	4.53	466	5	2	3	11	1	24	3	15	.15	.118	8	2	.03	19	.01	6	.45	.01	.26	2	1760
L5+43N 0+03E	1	44	82	91	2.7	4	8	35	4.33	477	5	2	3	9	2	18	2	12	.13	.058	7	1	.02	14	.01	5	.34	.01	.22	2	1450
L5+42N 0+00E	2	64	106	80	7.2	4	6	37	2.91	303	5	ND	1	15	1	34	2	11	.05	.042	8	2	.02	30	.01	2	.33	.01	.21	2	2135
STD C/AU-R	18	59	42	132	6.9	70	30	1028	4.09	43	17	8	38	49	18	16	19	61	.47	.095	40	57	.89	179	.07	32	1.99	.06	.15	13	485

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+42N 0+55E	1	274	19	133	2.0	3	13	692	8.05	804	5	ND	3	9	1	17	2	43	.16	.186	10	13	.27	22	.01	2	.78	.01	.28	1	205
L5+41N 0+55E	1	220	32	151	3.4	4	14	1092	5.51	446	5	ND	3	10	1	13	2	43	.22	.175	11	6	.84	69	.01	2	1.32	.01	.26	1	375
L5+40N 0+02E	1	44	45	71	2.4	2	5	52	2.73	333	5	ND	3	13	1	21	3	16	.21	.114	10	13	.03	40	.01	2	.42	.01	.30	1	535
L5+37N 0+03E	2	15	147	26	3.7	2	1	59	3.05	714	5	ND	3	27	1	22	4	12	.03	.106	9	1	.01	230	.01	5	.28	.01	.28	2	1995
L5+37N 0+25E	1	10	75	122	.3	7	10	1408	2.89	232	5	ND	2	36	1	2	2	15	1.06	.093	12	15	.50	53	.01	2	.96	.01	.30	1	62
L5+37N 0+28E	1	84	13	97	.7	3	7	1270	3.00	379	5	ND	1	32	1	10	2	12	1.31	.117	15	3	.25	46	.01	2	.64	.01	.30	1	76
L5+37N 0+30E	1	12	36	91	.7	2	4	570	5.99	617	5	ND	3	18	1	2	3	74	.19	.210	8	19	.88	227	.01	2	1.13	.01	.30	1	225
L5+37N 0+32E	1	23	12	213	.3	4	12	1186	5.83	295	5	ND	3	15	1	3	2	102	.38	.208	11	8	1.58	41	.01	2	1.86	.01	.21	1	43
L5+37N 0+42E	1	125	20	88	.9	3	7	710	5.63	525	5	ND	2	33	1	3	2	82	.24	.156	8	16	1.02	20	.01	2	1.35	.01	.31	1	39
L5+37N 0+50E	1	16	64	33	1.2	2	3	60	4.12	294	5	ND	3	49	1	18	2	10	.07	.108	14	1	.03	111	.01	2	.31	.01	.24	1	655
L5+37N 0+54E	1	417	20	258	1.2	4	17	3030	5.73	256	5	ND	2	69	1	2	2	74	2.85	.185	12	13	1.56	54	.01	2	2.17	.01	.27	1	111
L5+37N 0+55E	1	17	15	283	.5	6	19	2561	6.23	408	5	ND	3	25	1	5	2	82	.68	.209	13	9	1.59	217	.01	2	2.26	.01	.29	1	47
L5+37N 0+56E	1	12	10	225	.3	3	15	2292	5.90	254	5	ND	2	40	1	3	2	79	1.65	.213	12	16	1.77	80	.01	2	2.35	.01	.31	1	9
L5+37N 0+60E	2	66	72	86	2.5	4	7	383	4.45	668	5	ND	2	9	1	14	2	24	.21	.121	7	2	.28	35	.01	2	.70	.01	.30	1	425
L5+35N 0+03E	1	25	102	64	3.5	3	5	593	3.80	694	5	ND	2	24	1	20	2	13	.04	.145	9	29	.02	459	.01	2	.36	.01	.26	1	965
L5+33N 0+55E	1	100	36	304	.6	3	13	3507	6.14	508	5	ND	2	25	1	8	2	55	.87	.197	15	8	1.19	72	.01	2	1.67	.01	.30	1	295
L5+29N 0+05E	1	74	61	69	2.2	2	2	125	4.64	387	5	ND	3	47	1	27	2	18	.05	.153	11	16	.04	120	.01	2	.52	.01	.50	2	565
L5+25N 0+25E	3	11	74	135	.5	3	10	1155	5.57	438	5	ND	2	30	1	3	2	120	.41	.268	15	10	1.31	754	.01	2	1.98	.01	.34	1	69
UC 0+00S	1	6	11	14	.4	4	6	245	3.27	299	5	ND	3	9	1	2	3	62	.30	.155	6	15	.20	68	.01	2	.53	.02	.25	1	164
UC 0+10S	1	4	11	38	.4	3	11	1074	5.18	531	5	ND	4	12	1	2	2	74	.46	.173	8	8	1.33	45	.05	2	1.40	.01	.22	1	147
UC 0+20S	1	5	14	49	.4	1	3	622	5.49	501	5	ND	4	30	1	3	2	102	.12	.154	8	12	.59	346	.18	2	.75	.03	.22	4	105
UC 0+30S	1	7	22	95	.5	6	15	1844	6.66	670	5	ND	2	25	1	4	2	171	1.57	.180	4	18	1.83	17	.15	2	1.40	.02	.10	1	142
UC 0+40S	1	57	20	19	.7	4	6	244	2.07	259	5	ND	3	13	1	10	2	17	.30	.152	6	13	.05	129	.01	2	.49	.01	.31	1	80
UC 0+50S	1	9	15	59	.5	2	6	1043	4.96	285	5	ND	4	36	1	2	2	66	.36	.149	10	8	.88	83	.06	2	1.13	.02	.17	1	145
UC 0+60S	1	5	13	27	.3	1	4	580	5.27	687	5	ND	4	21	1	2	2	61	.26	.155	9	9	.71	109	.01	2	.87	.02	.23	1	74
UC 0+70S	1	7	11	33	.4	2	4	667	4.94	238	5	ND	4	12	1	2	2	105	.27	.143	6	8	1.12	54	.10	2	1.10	.03	.18	1	60
UC 0+80S	1	9	22	23	.6	1	3	305	4.56	273	5	ND	3	31	1	2	2	32	.04	.098	3	9	.13	203	.09	2	.48	.01	.34	1	94
UC 0+90S	1	6	22	19	.4	4	2	231	2.48	202	5	ND	2	28	1	4	2	51	.28	.121	7	3	.12	78	.11	2	.46	.01	.26	4	475
UC 1+00S	1	14	15	41	.5	2	4	451	5.38	229	5	ND	4	13	1	2	2	69	.13	.163	5	17	.40	181	.19	2	.78	.01	.33	3	126
UC 1+10S	2	12	5	54	.4	2	5	741	5.02	192	5	ND	4	19	1	2	2	77	.25	.156	5	7	.65	99	.13	2	1.00	.02	.26	1	40
UC 1+20S	2	10	16	59	.1	2	5	997	4.54	152	5	ND	2	10	1	2	2	51	.18	.139	6	12	.90	75	.01	2	1.25	.02	.23	1	29
UC 1+30S	1	8	26	147	.7	7	14	5540	5.80	162	5	ND	3	53	1	4	2	114	4.14	.112	11	21	1.65	57	.06	2	2.15	.02	.10	8	122
UC 1+40S	1	8	21	100	.5	7	16	2280	5.44	150	5	ND	5	17	1	2	2	126	1.07	.126	14	21	1.52	68	.01	2	1.84	.02	.19	1	48
UC 1+50S	1	4	8	56	.4	6	10	1854	5.56	133	5	ND	5	24	1	4	2	176	1.08	.134	12	18	1.73	123	.05	2	2.23	.03	.16	1	22
UC 1+60S	4	7	137	25	2.0	4	1	82	.63	92	5	7	1	20	1	3	2	6	.02	.011	2	28	.04	630	.01	2	.32	.01	.21	1	6255
UC 1+70S	1	16	23	437	.2	20	13	1160	2.48	142	5	ND	3	12	5	2	2	15	.28	.043	8	5	.09	152	.01	2	.35	.01	.12	1	385
UC 1+80S	1	32	2	90	.1	12	27	1741	7.80	34	5	ND	1	107	1	2	2	148	3.43	.091	6	16	.93	241	.01	2	.61	.02	.17	1	29
STD C/AU-R	18	60	36	132	7.0	68	31	1031	4.02	42	17	8	40	50	18	16	20	60	.47	.100	41	57	.88	179	.07	32	1.94	.06	.16	11	505

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
UC 1+90S	1	32	8	93	.2	13	24	1349	7.78	19	5	ND	2	25	1	3	3	217	2.62	.105	6	20	1.75	76	.29	4	2.86	.02	.08	1	13
UC 2+00S	1	34	7	127	.1	11	28	1300	9.79	17	5	ND	2	48	1	2	2	201	1.97	.109	10	15	.80	70	.01	7	1.17	.02	.18	1	3
UC 2+10S	1	33	12	134	.1	11	28	1305	9.81	30	5	ND	2	48	1	7	2	192	2.57	.120	10	18	1.83	167	.02	2	2.60	.03	.06	1	6
UC 2+20S	1	85	7	110	.1	12	22	947	7.92	49	5	ND	1	22	1	2	2	186	1.89	.103	7	18	1.32	250	.21	7	2.23	.03	.12	1	65
UC 2+30S	1	41	9	136	.1	15	26	1064	9.23	18	5	ND	2	44	1	2	2	195	2.42	.096	8	22	1.43	242	.05	7	2.39	.02	.10	1	1
UC 2+40S	1	27	8	129	.3	11	24	1295	8.72	79	5	ND	2	44	1	3	2	198	3.39	.103	8	19	1.69	115	.34	2	2.40	.03	.04	1	93
UC 2+50S	3	17	114	36	1.7	5	5	521	1.93	352	5	ND	3	7	1	13	3	49	.36	.142	10	6	.38	132	.01	7	.78	.01	.19	1	75
UC 2+60S	1	22	7	115	.1	2	11	1383	5.44	33	5	ND	4	63	1	3	2	137	3.13	.196	14	7	1.14	147	.15	3	1.97	.05	.14	1	8
UC 2+70S	1	23	15	58	.1	3	12	1156	5.22	228	5	ND	1	17	1	6	2	66	.56	.157	10	2	.07	494	.01	7	.61	.03	.13	1	8
UC 2+80S	1	34	18	129	.5	5	13	1807	4.53	133	5	ND	4	23	1	7	2	143	1.95	.191	15	9	1.59	77	.18	4	1.96	.03	.12	1	63
UC 2+90S	1	42	19	156	.8	32	33	2068	10.41	279	5	ND	2	49	1	9	2	254	2.94	.105	10	50	2.34	28	.01	2	2.77	.03	.05	1	53
UC 3+00S	13	616	25	206	1.5	22	13	1167	4.35	59	5	ND	3	22	1	2	2	72	1.13	.077	16	35	1.17	74	.02	2	1.83	.03	.17	1	505
UC 3+10S	16	814	68	532	2.8	11	9	1099	3.46	34	5	ND	1	21	3	2	2	37	1.69	.024	5	18	.88	70	.03	2	1.42	.02	.07	1	275
UC 3+20S	7	443	30	225	1.5	40	19	1773	4.56	97	5	ND	2	29	1	6	2	61	2.49	.104	16	42	1.89	62	.01	6	2.30	.02	.14	1	96
UC 3+30S	1	39	6	126	.1	15	29	1270	9.45	27	5	ND	2	47	1	2	2	222	3.47	.100	8	23	1.58	163	.01	2	2.42	.03	.07	1	7
UC 3+40S	1	31	11	149	.1	14	29	1487	10.49	248	5	ND	2	29	1	3	2	182	2.31	.124	6	21	1.98	65	.34	2	3.55	.03	.02	1	18
UC 3+50S	1	31	10	110	.1	13	23	968	8.40	41	5	ND	1	24	1	2	2	181	2.05	.113	8	20	1.22	46	.41	3	2.84	.03	.05	1	1
UC 3+60S	1	30	7	145	.1	13	23	1163	8.88	45	5	ND	2	33	1	6	2	206	1.82	.095	6	21	2.00	24	.34	2	2.79	.03	.05	1	1
UC 3+70S	1	30	84	297	.4	7	27	2792	7.67	80	5	ND	1	132	1	11	2	145	4.53	.107	8	12	1.42	23	.30	8	2.40	.02	.07	1	14
UC 3+80S	1	11	2	53	.2	13	7	1029	3.24	40	5	ND	3	7	1	2	2	82	.29	.087	5	39	1.14	56	.01	2	1.61	.03	.06	1	58
UC 3+90S	1	3	2	44	.1	39	7	933	3.04	22	5	ND	4	66	1	2	2	50	.59	.083	11	37	1.50	1488	.07	5	1.94	.03	.23	1	3
UC 4+00S	1	22	5	31	.1	16	7	761	1.98	55	5	ND	3	23	1	2	2	57	1.22	.031	8	39	.53	116	.01	7	.84	.04	.06	1	34
UC 4+10S	2	243	8	40	.5	13	9	611	2.17	170	5	ND	2	12	1	3	2	69	.39	.038	6	34	.43	64	.07	3	.69	.04	.07	1	131
UC 4+20S	1	12	28	66	.4	15	4	551	3.80	139	5	ND	4	8	1	2	2	72	.26	.102	4	62	1.18	157	.21	2	1.14	.03	.14	2	245
UC 4+30S	1	6	8	37	.2	11	5	380	1.61	27	5	ND	3	7	1	2	2	33	.17	.036	6	23	.44	46	.06	14	.60	.04	.09	2	45
UC 4+40S	1	18	13	88	.2	19	7	1030	3.10	33	5	ND	4	13	1	2	2	82	.37	.037	8	51	1.38	32	.09	4	1.45	.04	.06	1	13
UC 4+50S	1	8	2	37	.1	10	3	430	1.23	15	5	ND	2	10	1	2	2	26	.21	.033	4	21	.45	32	.04	2	.68	.04	.07	1	7
UC 4+60S	1	16	10	41	.1	15	4	359	1.34	29	5	ND	2	8	1	2	2	44	.21	.040	5	22	.45	45	.07	4	.64	.04	.08	2	24
UC 4+70S	29	941	9	109	1.3	27	10	586	2.75	150	5	ND	3	40	1	8	2	30	2.66	.037	5	16	.17	138	.01	3	.32	.03	.12	1	985
UC 4+80S	1	64	9	142	.6	5	12	873	4.43	25	5	ND	4	65	1	2	2	115	.89	.103	8	8	1.27	157	.19	2	1.54	.05	.10	1	1025
UC 4+90S	6	151	51	151	1.0	20	9	609	2.96	64	5	ND	6	76	1	2	2	75	.65	.090	11	33	.82	122	.33	2	1.31	.02	.16	1	126
UC 5+00S	4	39	29	44	1.9	12	6	372	3.25	237	5	ND	3	112	1	3	2	53	1.61	.054	7	19	.49	92	.10	11	1.12	.02	.12	1	2215
UC 5+10S	1	115	13	81	.6	13	9	885	2.75	90	5	ND	1	30	1	2	2	80	.77	.074	5	28	1.33	52	.10	3	1.25	.03	.09	1	82
UC 5+20S	1	8	4	187	.1	2	13	1207	8.09	19	5	ND	3	33	1	3	2	24	1.68	.267	16	10	.91	285	.24	2	1.88	.04	.10	1	11
UC 5+30S	1	10	4	155	.1	1	15	1163	9.01	14	5	ND	2	47	1	2	2	36	2.44	.260	16	8	.96	131	.20	2	2.06	.04	.05	1	1
UC 5+40S	1	17	10	149	.1	4	17	1255	8.69	32	5	ND	3	42	1	2	2	50	2.04	.241	19	10	.88	97	.01	2	2.05	.03	.09	1	1
UC 5+50S	6	11	12	34	.1	18	3	605	1.61	309	5	ND	1	58	1	2	2	18	2.38	.060	7	12	.14	84	.01	2	.43	.02	.14	1	1
STD C/AU-R	18	59	36	132	7.1	68	31	1029	4.01	41	23	8	40	49	19	16	19	61	.47	.096	41	56	.88	178	.07	33	1.98	.06	.16	11	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
UC 5+60S	1	14	25	57	.1	6	5	454	1.31	17	5	ND	1	71	1	2	2	5	1.93	.037	7	5	.07	479	.01	4	.30	.01	.17	1	4
UC 5+70S	1	23	12	57	.1	7	5	717	1.88	13	5	ND	2	88	1	2	2	6	2.38	.038	6	2	.04	48	.01	4	.26	.01	.15	1	1
UC 5+80S	1	187	15	79	.1	18	11	1391	2.56	7	5	ND	2	390	1	2	2	21	9.59	.142	11	16	.93	800	.01	2	1.41	.01	.14	1	8
UC 5+90S	1	63	7	140	.1	23	15	1289	3.82	2	5	ND	3	103	1	2	2	21	2.79	.064	14	21	1.58	388	.01	2	2.18	.01	.13	1	5
UC 6+00S	1	25	11	75	.1	16	11	769	2.49	3	5	ND	2	167	1	2	2	18	2.72	.080	11	21	1.09	1812	.01	2	1.53	.01	.16	1	7
UC 6+10S	1	109	20	78	.1	15	11	488	2.72	2	5	ND	3	74	1	2	2	22	1.39	.073	10	20	1.00	586	.01	3	1.49	.01	.13	1	3
UC 6+20S	1	56	11	63	.1	10	7	570	2.00	11	5	ND	3	85	1	2	2	10	1.91	.042	10	8	.30	79	.01	5	.82	.01	.19	1	1
UC 6+30S	1	27	18	44	.1	4	2	1271	1.25	8	5	ND	1	400	1	2	2	5	9.08	.015	5	4	.22	25	.01	3	.21	.01	.05	2	1
UC 6+40S	1	89	11	335	.4	15	12	2548	2.80	4	5	ND	4	139	1	2	2	14	4.41	.097	17	9	.46	99	.01	3	.39	.01	.17	1	4
UC 6+50S	1	78	20	186	.1	18	11	3911	3.57	17	5	ND	3	310	1	3	2	17	8.42	.113	15	10	.45	127	.01	2	.81	.01	.15	1	3
UC 6+60S	1	43	8	108	.1	18	13	1734	2.81	3	5	ND	2	259	1	2	2	18	4.86	.064	9	18	.78	2215	.01	2	1.01	.01	.17	1	5
UC 6+70S	1	114	30	97	.1	18	11	1604	3.01	10	5	ND	3	513	1	2	2	19	11.57	.133	13	18	1.21	136	.01	2	1.72	.01	.13	2	4
UC 6+80S	1	56	13	110	.1	18	11	817	3.67	16	8	ND	3	232	1	2	2	19	5.37	.108	17	10	1.45	162	.01	3	2.39	.01	.14	1	8
UC 6+90S	1	48	22	44	.1	8	7	2803	1.43	3	5	ND	1	867	1	2	2	8	21.20	.073	8	9	.67	2439	.01	2	.33	.01	.10	1	2
UC 7+00S	1	16	51	69	.9	8	5	2243	1.73	50	5	ND	1	129	1	2	2	4	3.93	.031	5	4	.13	165	.01	2	.25	.01	.16	1	11
UC 7+10S	1	84	15	123	.1	55	14	848	3.78	7	5	ND	3	124	1	2	2	26	3.15	.082	14	28	1.43	145	.01	4	1.94	.01	.15	1	2
UC 7+20S	1	53	25	125	.1	22	10	898	4.10	30	5	ND	4	22	1	3	2	82	.69	.083	15	35	1.69	57	.01	3	2.23	.02	.11	1	3
UC 7+30S	1	30	13	134	.1	8	26	1253	9.09	36	5	ND	2	83	1	4	2	156	4.55	.127	8	17	1.27	88	.20	3	3.40	.02	.09	3	1
UC 7+40S	2	99	23	150	.4	39	12	2988	3.79	78	5	ND	2	256	1	2	2	50	15.39	.113	13	31	1.48	34	.01	2	1.98	.01	.13	1	2
UC 7+50S	1	84	76	204	.5	17	9	2307	3.40	78	5	ND	3	50	1	4	2	71	2.80	.067	14	31	1.63	41	.01	2	1.69	.02	.05	1	12
UC 7+60S	1	73	2	91	.4	4	9	1494	3.48	11	5	ND	2	130	1	2	2	48	5.06	.122	7	13	.98	1454	.01	2	1.70	.01	.18	1	19
UC 7+70S	1	5	4	106	.1	4	12	1294	4.31	22	5	ND	2	42	1	2	2	63	2.32	.138	6	11	1.29	117	.01	5	2.04	.01	.20	1	3
UC 7+80S	1	4	6	106	.1	5	11	1181	3.68	86	5	ND	2	89	1	2	2	60	3.64	.142	7	11	1.01	742	.01	4	1.59	.01	.19	1	16
UC 7+90S	1	10	15	164	.1	8	18	1613	7.32	40	5	ND	2	53	1	3	2	117	1.21	.207	7	14	1.59	525	.04	2	2.90	.01	.22	1	49
UC 8+00S	3	25	467	281	3.2	8	8	1827	4.05	386	5	ND	2	21	1	14	2	79	1.17	.061	8	36	1.11	68	.01	3	1.07	.02	.08	1	86
UC 8+10S	2	132	259	776	3.3	41	15	2359	7.35	511	5	ND	4	13	3	14	2	104	.37	.107	8	44	2.10	43	.15	2	2.68	.02	.10	1	46
UC 8+20S	20	47	344	318	1.2	12	6	698	.83	62	5	ND	4	69	2	4	2	24	2.29	.083	9	15	.80	147	.09	5	.90	.02	.04	1	7
UC 8+30S	7	54	684	351	2.5	2	5	991	2.64	130	5	ND	2	22	1	2	3	45	.39	.033	9	11	2.26	109	.20	2	1.80	.01	.08	1	172
UC 8+40S	1	84	27	83	.2	21	14	1033	5.47	68	5	ND	3	13	1	2	2	120	.50	.117	16	36	1.87	71	.01	3	2.36	.02	.06	1	14
UC 8+50S	8	226	25	364	1.4	15	12	1399	5.69	69	5	ND	3	15	1	3	2	93	.24	.082	6	40	1.83	88	.01	2	2.11	.01	.07	1	220
UC 8+60S	7	182	52	367	1.8	13	10	1476	4.40	12	5	ND	2	34	1	2	2	117	1.92	.070	9	40	1.55	144	.04	2	1.52	.02	.07	1	240
UC 8+70S	87	533	376	4492	42.3	1	5	194	44.01	1641	5	ND	10	13	3	7	2	67	.06	.096	4	17	.06	133	.11	2	.83	.01	.08	1	1480
UC 8+80S	4	154	57	309	.9	7	6	1350	2.79	17	5	ND	2	12	2	2	2	48	.68	.053	9	24	.61	69	.01	4	.89	.01	.12	1	165
UC 8+90S	5	62	52	260	3.4	13	10	1179	5.13	217	5	ND	3	7	1	2	3	49	.23	.063	6	21	.73	76	.08	2	1.37	.01	.16	1	188
UC 9+00S	5	197	17	154	.3	22	14	1311	4.14	21	5	ND	4	15	1	2	4	56	.93	.128	14	26	1.52	66	.01	2	1.95	.02	.14	1	68
GTC 2+80N	3	164	177	191	3.5	5	9	233	5.01	317	5	ND	2	16	1	22	2	9	.35	.085	4	3	.02	14	.01	2	.18	.01	.14	1	290
STD C/AU-R	17	57	38	131	7.1	67	29	956	3.70	39	16	7	36	47	17	17	23	58	.44	.089	39	56	.83	175	.07	32	1.85	.06	.15	12	520

TEUTON RESOURCES FILE # 88-4826

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
GTC 2+70N	1	252	3588	7536	10.0	3	13	899	7.68	680	5	ND	3	38	36	21	3	10	.82	.079	5	4	.04	8	.01	6	.27	.01	.19	1	815
GTC 2+60N	1	60	478	1294	4.4	4	11	53	8.33	341	5	ND	4	11	8	13	2	8	.25	.085	4	1	.01	7	.01	5	.20	.01	.15	1	365
GTC 2+50N	1	16	287	191	3.0	1	8	1073	6.60	219	5	ND	1	106	2	6	3	5	1.58	.063	2	1	.01	10	.01	4	.10	.01	.10	1	255
GTC 2+40N	1	73	105	157	2.6	4	18	2200	5.04	513	5	ND	1	83	1	3	2	25	4.38	.148	6	6	.57	27	.01	3	1.14	.01	.17	1	425
GTC 2+30N	1	16	47	256	.1	1	9	3238	3.45	84	5	ND	1	137	1	2	2	19	4.67	.093	7	4	.61	62	.01	2	.99	.01	.25	1	156
GTC 2+20N	1	6	7	115	.1	3	8	3931	3.44	95	5	ND	1	131	1	2	2	15	4.45	.098	6	4	.69	66	.01	3	.75	.01	.28	1	36
GTC 2+10N	1	35	763	3414	8.7	2	7	601	4.36	450	5	ND	1	52	36	18	3	6	1.25	.074	2	1	.04	8	.01	5	.31	.01	.24	1	1285
GTC 2+00N	1	29	12	201	.2	4	10	3014	4.10	28	5	ND	1	109	1	2	2	31	3.04	.081	6	10	1.26	132	.01	2	1.93	.01	.25	1	48
GTC 1+90N	1	75	346	25273	26.7	2	12	235	5.70	547	5	ND	1	31	497	15	3	14	.58	.139	2	2	.08	8	.01	4	.41	.01	.19	1	1825
GTC 1+70N	1	2004	11	225	2.1	3	23	3732	5.33	385	5	ND	1	153	1	30	2	58	5.88	.147	8	6	1.14	22	.01	2	1.52	.01	.20	1	555
GTC 1+60N	1	69	25	554	.5	2	11	3166	3.95	37	5	ND	2	140	8	3	2	77	4.88	.152	11	7	1.30	364	.01	3	1.82	.01	.22	1	51
GTC 1+50N	1	23	70	314	1.8	4	17	2979	5.95	367	5	ND	2	93	3	3	3	80	3.91	.169	9	8	1.57	59	.01	6	2.06	.01	.19	1	645
GTC 1+40N	1	128	24	265	.4	3	15	2562	5.60	51	5	ND	1	90	1	2	2	100	3.90	.172	10	8	1.60	68	.01	2	2.05	.01	.16	1	158
GTC 1+30N	1	12	5	267	.1	3	13	3471	5.29	18	5	ND	1	167	1	2	2	76	5.41	.145	11	7	1.77	326	.01	4	2.45	.01	.24	1	23
GTC 1+20N	1	115	12	212	.3	4	13	2609	4.91	21	5	ND	1	112	1	2	2	63	4.74	.146	8	8	1.47	412	.01	5	2.16	.01	.20	1	26
GTC 1+10N	1	66	15	201	.4	3	12	2610	5.10	100	5	ND	1	76	1	2	2	55	3.73	.152	7	9	1.63	109	.01	4	2.23	.01	.21	1	95
GTC 1+00N	1	14	9	145	.1	3	10	1968	4.19	186	5	ND	1	86	1	2	2	38	3.82	.156	8	8	1.08	103	.01	2	1.69	.01	.31	2	225
GTC 0+90N	1	13	13	151	.1	2	12	2528	3.87	175	5	ND	1	87	1	2	2	20	3.91	.144	5	4	.77	65	.01	2	.38	.01	.26	1	146
GTC 0+80N	1	16	32	300	.3	3	13	2269	5.37	174	5	ND	1	91	1	3	2	52	3.72	.128	7	10	1.27	57	.01	2	1.78	.01	.22	1	46
GTC 0+70N	1	7	5	155	.1	4	10	2395	4.22	21	5	ND	2	94	1	3	4	45	3.65	.115	8	9	1.25	124	.01	5	1.86	.01	.24	1	35
GTC 0+60N	1	43	21	147	.1	11	12	2507	4.09	35	5	ND	1	142	1	3	2	54	5.89	.120	7	15	.99	127	.01	2	1.57	.01	.21	2	53
GTC 0+50N	1	14	16	194	.1	3	16	2651	5.22	52	5	ND	1	130	1	2	2	60	4.74	.171	9	7	1.57	129	.01	2	2.23	.01	.24	1	84
GTC 0+40N	1	142	192	225	1.1	3	12	3816	7.25	131	5	ND	1	45	1	2	2	65	2.46	.119	8	11	1.48	23	.01	2	1.91	.01	.21	1	1635
GTC 0+30N	1	41	165	1219	4.8	3	11	2311	5.33	671	5	3	1	63	12	6	2	30	3.64	.092	8	3	.38	21	.01	7	.63	.01	.18	1	3575
GTC 0+20N	1	15	8	127	.3	3	11	1400	6.70	81	5	ND	1	10	3	2	4	90	.33	.133	6	9	1.64	36	.01	3	1.97	.01	.19	2	33
GTC 0+10N	1	425	13	41	1.7	1	4	114	22.85	346	5	ND	4	6	1	3	4	43	.04	.205	5	4	.09	78	.01	2	.32	.01	.23	4	87
GTC 0+00N	1	75	14	177	.1	4	10	3447	5.79	28	5	ND	2	9	1	2	2	68	.38	.156	14	9	1.41	109	.01	2	2.06	.01	.27	1	68
WC 2+80N	1	84	20	120	.7	13	34	1015	5.50	55	5	ND	1	125	1	5	2	47	5.38	.112	4	12	2.03	39	.01	2	2.60	.01	.11	1	23
WC 2+70N	1	64	7	64	.1	10	15	1163	4.55	10	5	ND	1	104	1	2	2	58	5.28	.099	4	11	1.44	259	.01	2	1.91	.01	.11	1	4
WC 2+60N	1	47	3	71	.1	7	17	1048	4.31	7	5	ND	1	136	1	2	2	59	5.15	.096	5	10	1.60	1436	.01	3	2.02	.01	.11	1	2
WC 2+50N	1	5	2	68	.1	3	16	987	4.61	6	5	ND	1	145	1	2	2	70	4.90	.080	4	8	1.46	1493	.02	3	1.93	.01	.11	1	6
WC 2+30N	1	57	11	99	.2	6	19	1470	5.05	27	5	ND	1	258	1	2	2	57	5.46	.083	5	9	1.73	2036	.01	4	2.80	.01	.12	1	3
WC 2+20N	2	144	56	33	.5	6	23	213	3.67	158	5	ND	1	86	1	6	3	15	.61	.108	2	4	.49	22	.01	3	.96	.01	.14	1	29
WC 2+10N	1	86	6	142	.6	5	17	1573	5.21	27	5	ND	1	196	2	3	2	51	4.45	.104	5	10	1.50	1690	.01	3	2.39	.01	.16	1	2
WC 2+00N	1	9	10	106	.1	6	14	2141	4.87	6	5	ND	1	201	2	2	2	43	6.78	.092	5	8	.96	1129	.01	2	1.73	.01	.15	1	1
WC 1+90N	1	10	5	122	.1	4	16	1273	3.77	5	5	ND	1	265	2	2	2	32	8.50	.081	4	8	1.18	2340	.01	2	2.02	.01	.10	2	2
STD C/AU-R	18	61	39	132	6.8	71	30	1027	4.16	44	19	7	38	49	18	19	19	61	.49	.088	40	57	.91	178	.08	33	2.01	.06	.15	13	475

TEUTON RESOURCES FILE # 88-4826

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
WC 1+80N	1	283	14	113	.3	7	22	1164	5.83	8	5	ND	2	103	1	4	2	66	4.82	.153	7	9	1.82	205	.01	2	2.80	.01	.18	1	3
WC 1+70N	1	111	10	79	.2	6	17	1553	4.26	10	5	ND	1	139	2	2	2	52	9.55	.097	7	7	1.13	497	.01	2	1.59	.01	.12	1	4
WC 1+60N	1	63	13	69	.1	8	19	1266	5.54	16	5	ND	2	116	1	3	2	84	4.56	.123	9	9	1.22	122	.03	2	1.56	.02	.10	1	7
WC 1+50N	1	22	4	94	.3	6	18	1460	4.99	8	5	ND	1	148	2	2	2	66	5.48	.115	7	8	1.56	1235	.01	2	2.14	.01	.11	1	4
WC 1+40N	1	97	5	64	.1	4	14	1440	4.49	7	5	ND	1	126	1	2	2	62	6.16	.101	5	7	1.07	1157	.01	2	1.60	.01	.09	1	5
WC 1+30N	1	174	7	62	.2	2	11	3221	3.34	19	5	ND	1	477	3	2	2	36	16.84	.057	6	7	1.00	1772	.01	2	1.64	.01	.06	1	3
WC 1+20N	1	51	10	131	.2	8	27	1602	5.37	7	5	ND	2	94	2	2	2	65	5.37	.110	5	6	2.86	535	.01	2	3.23	.01	.09	1	9
WC 1+10N	1	9	16	187	.3	3	13	2292	5.16	42	5	ND	2	85	1	2	2	88	3.91	.178	10	7	1.42	69	.01	2	2.07	.01	.17	1	790
WC 1+00N	1	7	7	139	.3	1	10	3715	3.51	27	5	ND	1	342	2	2	2	49	12.43	.107	8	5	1.01	77	.01	2	1.41	.01	.13	1	104
WC 0+80N	1	14	15	186	.3	3	16	2765	4.79	265	5	ND	1	96	1	7	2	50	4.77	.180	9	7	1.32	36	.01	2	1.66	.01	.20	1	460
WC 0+70N	1	74	12	260	.2	4	14	3316	5.27	59	5	ND	1	109	1	2	2	75	3.85	.166	7	9	1.72	277	.01	2	2.41	.01	.20	1	49
WC 0+60N	1	56	24	249	.2	4	15	2076	4.80	66	5	ND	1	67	1	2	2	49	2.56	.168	7	8	1.31	45	.01	2	1.87	.01	.21	1	31
WC 0+50N	1	162	13	305	.6	3	12	2658	4.90	15	5	ND	1	109	1	2	2	61	5.40	.153	10	9	1.47	292	.01	2	2.31	.01	.24	1	27
WC 0+40N	1	32	19	214	1.0	3	14	2530	5.66	168	5	ND	1	112	1	2	2	67	4.49	.171	9	7	1.45	40	.01	2	2.03	.01	.17	1	230
WC 0+30N	1	16	9	178	.3	2	12	2030	4.62	87	5	ND	2	105	1	2	2	62	3.31	.154	8	7	1.22	46	.01	2	1.89	.01	.20	1	112
WC 0+20N	1	62	15	218	.4	4	15	2033	5.17	101	5	ND	2	75	1	2	2	55	3.57	.178	6	6	1.43	34	.01	2	1.86	.01	.22	1	53
WC 0+10N	1	37	55	195	1.0	5	18	2352	5.95	416	5	ND	2	136	1	8	2	80	5.30	.187	7	9	1.13	50	.01	2	2.04	.01	.20	1	56
B.C. 3+70N	1	48	8	87	.1	2	8	2668	3.65	54	5	ND	1	135	1	2	2	70	6.83	.118	7	9	.96	40	.01	2	1.29	.01	.23	1	87
B.C. 3+60N	1	6	11	108	.1	2	12	2193	4.29	27	5	ND	2	54	1	2	2	58	2.22	.117	7	8	1.45	43	.01	2	1.59	.01	.14	1	52
B.C. 3+20N	1	6	6	8	.1	11	7	280	3.01	34	5	ND	2	22	1	2	2	4	.60	.036	4	1	.04	17	.01	3	.15	.01	.10	1	48
B.C. 3+10N	2	8	16	23	.4	9	6	179	2.75	32	5	ND	3	9	2	2	2	4	.24	.034	5	1	.04	15	.01	5	.19	.01	.11	2	147
B.C. 3+00N	1	6	11	10	.2	6	4	48	2.68	74	5	ND	1	6	1	2	2	3	.18	.054	6	1	.03	24	.01	2	.22	.01	.15	1	550
B.C. 2+90N	1	5	7	14	.2	6	4	341	3.58	77	5	ND	2	6	1	2	2	4	.17	.030	3	1	.02	15	.01	3	.18	.01	.14	3	260
B.C. 2+80N	2	11	17	25	.5	8	5	685	2.27	63	5	ND	2	25	1	2	3	21	1.17	.033	4	2	.03	22	.01	2	.16	.01	.15	1	540
B.C. 2+70N	2	27	50	19	8.7	3	15	56	16.26	111	5	ND	2	5	1	3	3	3	.04	.004	2	2	.04	2	.01	2	.12	.01	.06	2	1660
B.C. 2+60N	1	6	5	45	.2	8	7	606	5.38	38	5	ND	2	11	1	2	2	11	.33	.030	2	7	.65	10	.01	2	.76	.01	.10	1	470
B.C. 2+50N	1	11	9	58	.3	12	8	1947	3.54	47	5	ND	3	51	1	2	3	9	3.33	.058	4	9	.72	22	.01	3	.71	.01	.18	1	280
B.C. 2+30N	1	35	8	137	.4	13	7	2723	3.34	92	5	ND	3	26	1	2	2	11	1.36	.032	5	9	.59	15	.01	2	.64	.01	.19	1	350
B.C. 1+25N 20W	4	8	7	77	.1	10	12	1621	3.21	51	5	2	2	40	1	2	2	8	1.76	.027	3	7	.72	20	.01	2	.75	.01	.17	12	1060
B.C. 1+25N 10W	1	6	9	45	.1	13	8	1676	3.77	105	5	ND	2	46	1	2	2	7	1.86	.030	3	4	.35	20	.01	2	.34	.01	.14	1	680
B.C. 1+25N	2	25	1472	5517	3.1	11	13	49	6.49	302	5	4	2	11	67	4	2	4	.18	.046	2	1	.02	6	.01	2	.21	.01	.12	5	3880
B.C. 1+20N 20W	1	4	11	80	.1	6	4	1915	1.87	61	5	ND	1	29	1	2	2	6	2.51	.031	5	5	.79	62	.01	2	.18	.01	.18	1	650
B.C. 1+20N 10W	2	8	18	87	.1	10	5	1102	2.21	123	5	ND	1	25	1	2	2	7	.94	.035	4	4	.31	42	.01	2	.35	.01	.12	1	520
B.C. 1+20N 10E	1	6	6	26	.3	12	9	478	1.98	58	5	ND	3	15	1	2	2	5	.93	.081	8	2	.29	25	.01	4	.25	.01	.17	1	240
B.C. 1+15N 20W	11	14	12	112	.3	15	10	1872	3.64	60	5	ND	1	29	1	2	2	8	1.51	.036	5	4	.19	17	.01	2	.17	.01	.11	1	680
B.C. 1+15N 10W	5	6	8	13	.1	14	12	1562	2.59	89	5	ND	1	80	1	2	2	2	2.86	.043	5	1	.04	30	.01	2	.15	.01	.12	1	290
STD C/AU-R	18	60	39	132	6.7	69	30	1028	3.99	41	16	8	38	49	16	16	20	61	.48	.097	40	57	.88	178	.07	32	1.95	.06	.15	13	530

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	
B.C. 1+15N	8	15	6	25	.1	8	6	2017	2.79	156	5	ND	1	66	1	2	2	3	2.79	.043	7	2	.13	25	.01	2	.20	.01	.16	2	790	
B.C. 1+15N 5E	1	3	5	17	.1	10	8	915	4.11	100	5	ND	2	35	1	2	2	6	1.69	.032	6	2	.07	22	.01	3	.18	.01	.14	1	485	
B.C. 1+15N 10E	1	5	6	24	.1	9	6	1225	4.20	140	5	ND	1	41	1	2	2	4	2.27	.039	5	2	.11	16	.01	2	.18	.01	.15	1	680	
B.C. 1+10N 14W	1	11	14	105	2.9	21	4	3673	5.05	210	5	ND	3	118	1	3	2	16	4.94	.159	9	10	1.00	33	.01	3	.59	.01	.23	1	2095	
B.C. 1+10N 10W	4	6	10	14	.2	8	7	1029	2.47	126	5	ND	1	34	1	2	3	4	1.66	.038	4	5	.21	29	.01	4	.17	.01	.13	2	750	
B.C. 1+10N 5E	1	3	5	12	.1	7	6	1331	3.36	91	5	ND	1	44	1	2	2	14	2.02	.027	9	2	.10	23	.01	2	.17	.01	.15	1	1105	
B.C. 0+20N 10W	1	5	17	131	.1	26	14	1958	5.67	14	5	ND	3	48	1	2	2	47	1.28	.113	22	29	2.22	50	.01	2	2.45	.01	.14	1	74	
B.C. 0+15N	4	41	12	23	.9	13	50	803	4.50	89	5	ND	2	24	1	3	2	5	1.33	.041	11	6	.19	22	.01	2	.26	.01	.23	1	200	
B.C. 0+10N 5W	1	7	17	121	.1	20	4	3294	5.03	7	5	ND	3	98	1	2	2	41	3.93	.115	18	24	2.13	54	.01	2	2.55	.01	.21	1	9	
B.C. 0+5N 5W	1	4	3	63	.4	10	3	1577	2.56	46	5	ND	2	80	1	2	2	26	2.60	.032	10	19	1.05	270	.01	3	1.22	.02	.12	1	202	
B.C. 0+5W	1	3	5	105	.1	16	7	2298	4.25	10	5	ND	3	82	1	2	2	33	2.85	.064	11	30	1.69	68	.01	2	2.04	.01	.15	1	47	
B.C. 0+00N 10W	1	2	2	79	.1	11	5	1806	2.80	5	5	ND	2	66	1	2	2	31	3.03	.050	12	26	1.22	27	.01	2	1.49	.01	.17	1	10	
NG-1	1	162	20	54	1.2	5	11	1796	8.05	1040	5	ND	1	119	1	27	2	13	4.26	.104	3	7	.59	7	.01	4	.22	.01	.17	1	1725	0.050
NG-2	1	173	26	82	.8	6	16	1539	4.29	417	5	ND	1	79	1	29	2	12	3.61	.232	4	3	.41	35	.01	6	.30	.01	.21	1	211	0.006
NG-3	1	232	212	130	1.9	2	6	2132	7.24	656	5	ND	1	106	1	11	2	7	2.56	.038	2	7	.32	21	.01	4	.18	.01	.09	2	970	0.078
NG-4	1	492	49	105	2.2	4	3	10618	7.55	683	5	ND	1	131	1	14	2	13	6.79	.052	4	7	1.04	14	.01	5	.30	.01	.12	1	1525	0.044
NG-5	1	76	236	162	2.2	7	7	4460	11.45	1360	5	ND	1	78	1	2	2	42	2.44	.111	3	11	.73	23	.01	2	.93	.01	.15	1	1190	0.035
NG-6	1	45	44	117	1.2	9	20	1444	7.90	896	5	ND	2	44	2	5	2	22	1.89	.208	3	3	.18	17	.01	3	.48	.01	.22	1	365	0.011
NG-7	6	252	50	238	3.1	3	8	3069	5.48	1026	5	ND	1	63	1	24	2	21	1.72	.070	3	4	.28	13	.01	4	.18	.01	.15	1	1770	0.052
EMN FLOAT #1	1	6251	18108	16892	158.4	4	5	38217	5.88	482	5	ND	1	63	107	2093	2	6	1.94	.032	4	1	.13	16	.01	2	.19	.01	.11	1	925	0.027
~~K.G. 005~~	~~1~~	~~519~~	~~4121~~	~~88011~~	~~63.9~~	~~1~~	~~3~~	~~69~~	~~2.77~~	~~161~~	~~5~~	~~ND~~	~~1~~	~~37~~	~~1260~~	~~85~~	~~3~~	~~5~~	~~.08~~	~~.047~~	~~2~~	~~1~~	~~.01~~	~~5~~	~~.01~~	~~5~~	~~.10~~	~~.01~~	~~.07~~	~~1~~	~~1680~~	~~0.049~~
~~TK 007~~	~~64~~	~~1480~~	~~17708~~	~~1278~~	~~339.7~~	~~1~~	~~3~~	~~1191~~	~~32.98~~	~~1716~~	~~5~~	~~15~~	~~4~~	~~18~~	~~2~~	~~8280~~	~~57~~	~~11~~	~~.05~~	~~.033~~	~~5~~	~~4~~	~~.01~~	~~35~~	~~.01~~	~~2~~	~~.23~~	~~.01~~	~~.18~~	~~1~~	~~12210~~	~~0.?56~~
STD C/AU-R	19	63	40	133	7.1	70	31	1035	4.08	41	21	8	40	51	21	16	19	63	.48	.095	42	58	.89	179	.07	34	1.96	.06	.16	11	515	