# GEOLOGICAL , GEOCHEMICAL & GEOPHYSICAL REPORT



on the



## HOP MINERAL CLAIMS

Dease Lake - Thibert Creek Area
Liard Mining Division, B.C.

Latitude 58 degrees 50 minutes N.
Longitude 130 degrees 30 minutes W.

on behalf of



BIG I DEVELOPMENTS LTD.

by

James W. McLeod, B.Sc.



Vancouver, British Columbia
January 12, 1989

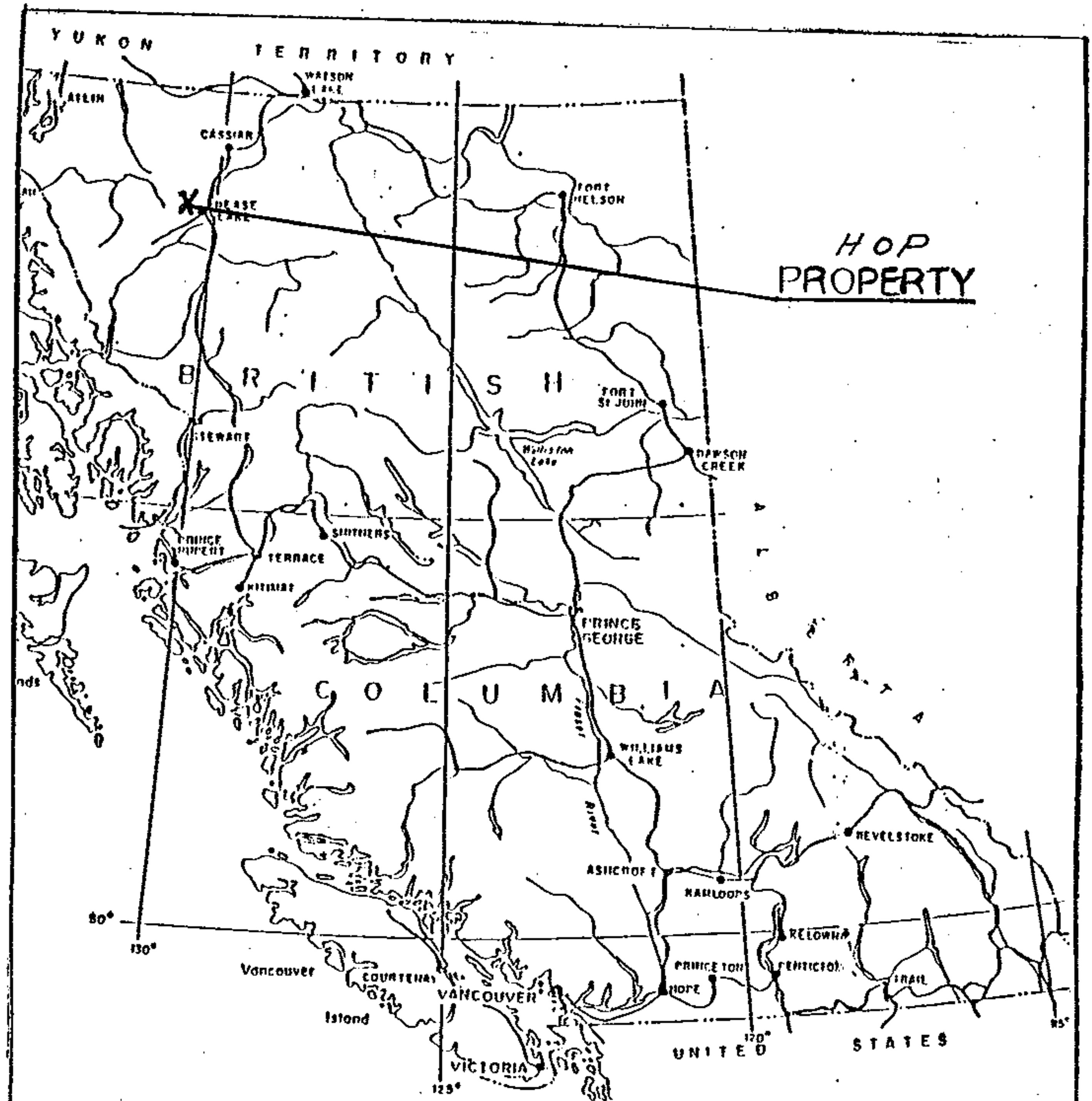
# TABLE OF CONTENTS



## APPENDICES



## FIGURES




HOP MINERAL CLAIM GROUP

LOCATION PLAN
LIARD MINING DIVISION

0 200 400 KILOMETERS

| Figure: | NTS | Drawn by: | Date: |
| --- | --- | --- | --- |
| 1 | 104 J | J.W.M. | 01/89 |

GEOLOGICAL ASSOCIATION OF CANADA · FELLOW · J. W. McLEOD

## INTRODUCTION

During the period September 21 through October 5, 1988 the writer supervised an exploration program on the Hop mineral claims. The fieldwork performed was of a grid-controlled nature and included geological outcrop mapping, rock, silt and soil sampling, prospecting and VLF-EM and magnetometer surveys. The grid was established by installing a baseline and grid survey lines normal to the baseline (see Figure 5). Also, a photogeophysical survey was conducted on the claim area by J.C. Explorations Ltd. of Vancouver, B.C. and is included in this report as Figure 1.

The work program was helicopter supported from the Village of Dease Lake, British Columbia.

A tent camp was established near the headwaters of Rose creek.

This report is being prepared at the request of the Board of Directors of Big I Developments Ltd. of Vancouver, B.C.

## LOCATION AND ACCESS

The Hop mineral claims are located 50 kilometers northwest of the Village of Dease Lake, B.C. on the northside of Thibert Creek and on the south-facing slope of Vowel Mountain. The claims occur at approximately 58 degrees 50 minutes N. latitude and 130 degrees 30 minutes W. longitude and may be located on NTS map reference 104 J.

Access to the property is by helicopter from Dease Lake, B.C., but a summer road from the north-end of Dease Lake (Porter Landing) up Thibert Creek presently comes within 3 kilometres of the property. The writer feels that summer road access to the property could be accomplished with a minimum of time and expense if future exploration results warrant it.

## PROPERTY AND OWNERSHIP

The Hop claim group consists of six adjoining 4x4 claim blocks for a total of 96 contiguous units which are listed as follows:

| Claim Name | Number of Units | Record Number | Anniversary Date |
|---|---|---|---|
| Hop 54 | 16 | 3683 | October 20 |
| Hop 55 | 16 | 3684 | October 20 |
| Hop 56 | 16 | 3685 | October 20 |
| Hop 57 | 16 | 3686 | October 20 |

| | | | |
|---|---|---|---|
| Hop 58 | 16 | 3687 | October 20 |
| Hop 59 | 16 | 3688 | October 20 |
| TOTAL | 96 units | | |

The Hop mineral claim group is owned by Mr. Douglas Hopper of 828 West Hastings Street, Vancouver, British Columbia and are held under an Option to Purchase Agreement by Big I Developments Ltd. of 304 - 626 West Pender Street, Vancouver, British Columbia, V6B 1V9.

## TOPOGRAPHICAL AND PHYSICAL ENVIRONMENT

The Hop mineral claims are situated on the northside of Thibert Creek on the south-facing slope of Vowel Mountain. The claim area ranges in elevation from 1036 metres (3400') to 1585 metres (5200') M.S.L. in rounded mountainous terrain. The property lies in the Sub-Alpine Forest biotic zone and timberline occurs at approximately 1200 metres (4000'). Below timberline spruce, pine, aspen and mountain alder predominate while above timberline dwarf juniper occurs in some areas while "buckbrush" is extensive over large areas. Glacial debris does not appear to be extensive or widespread with the exception of possibly the fill in the Thibert Creek valley. It should be noted that soil development is very juvenile with rare occurrences of good A-B horizons and most often a dark brown soil with sub-angular to angular rock fragments occurs.

The area experiences warm northern summers and cold winters. The area receives low to moderate precipitation of between 40 - 125 cm. (15 - 50 inches). A moderate amount of the precipitation occurs as snow.

The surface mineral exploration season generally extends for 6 to 7 months from April to November partly because of the south-facing location of most of the claim group.

## HISTORY

To the best of the writers knowledge the particular area covered by the Hop mineral claims has not been previouly staked nor is there a history of previous mineral exploration work with the exception of sparse stream sediment (silt) sampling with subsequent analyses for gold and cursory follow-up prospecting performed in 1972.

On the other hand the placer exploration and production history of the Thibert Creek area is long and colourful. Placer gold was first discovered on Thibert Creek which flows easterly into the north-end of Dease Lake in 1873. Official production during the period 1874 through 1895 was $1,279,000. From its' discovery to the present day intermittant placer mining activity has taken place on Thibert Creek with the production of an undetermined amount of placer gold and platinum group elements (PGE) comprised mainly of platinum and osmiridium (4:1).

During 1986 as the mineral claims were being staked, the writer conducted a reconnaissance geological mapping and geochemical soil, silt and rock sampling program. Results of this work were filed as assessment work.

## REGIONAL GEOLOGY

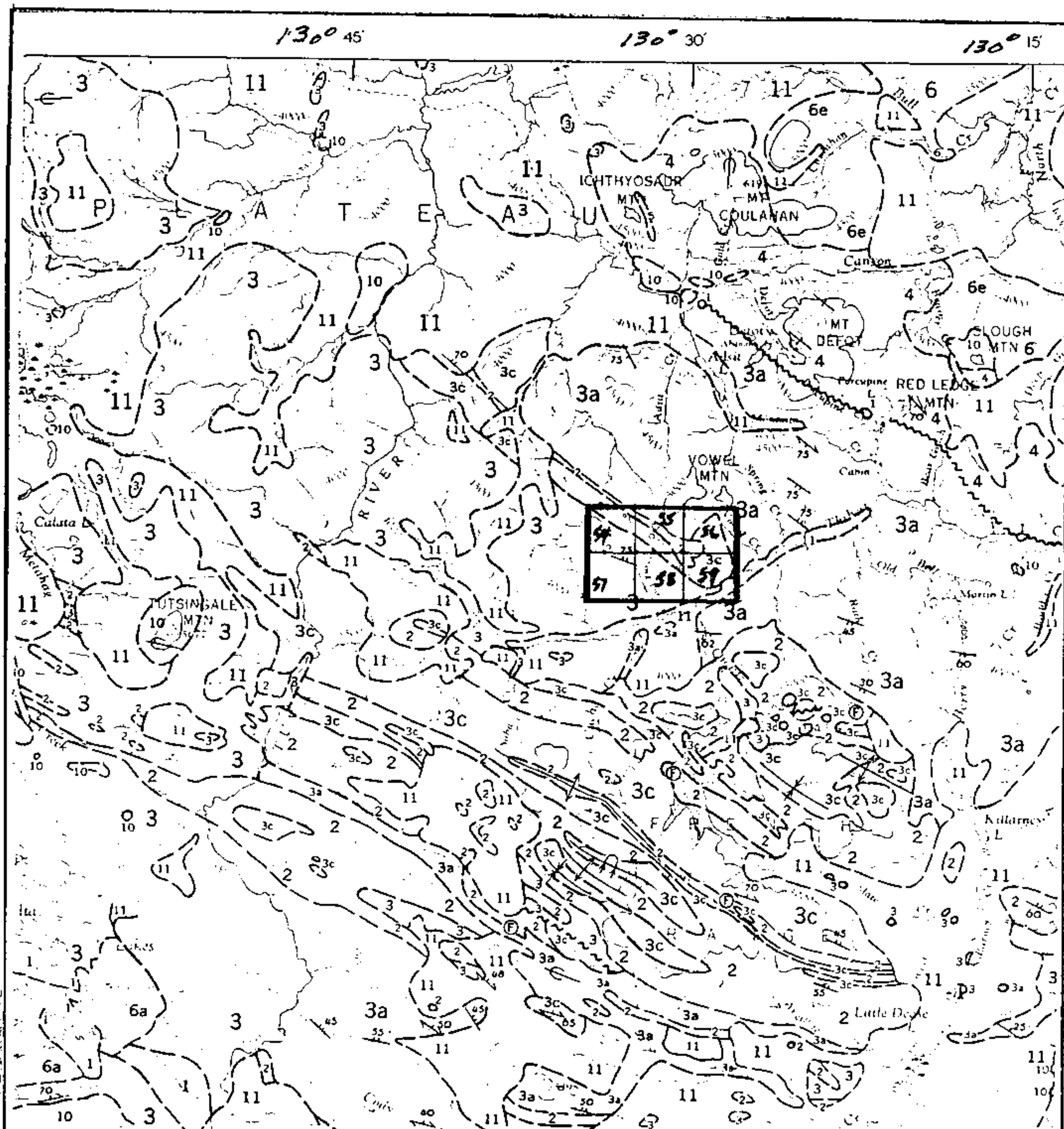
The general area has been described by Members of the Geological Survey of Canada on Dease Lake Map 21-1962. The map covers the area defined by NTS sheet 104 J and describes the work performed during "Operation Stikine", 1956 and from work undertaken during the period 1956-61.

The general area about the Hop claim group is underlain by a northwest-southeast trending elongate belt of Permian to pre-Upper Triassic age rocks. The older Permian rocks are mainly as limestones and limey sediments while the younger pre-Upper Triassic rocks occur mainly as intercalated volcano-sediments which are comprised of mainly greenstone and phyllite, jasper, chert, greywacke, slate, limestone, fine grained clastic rocks and conglomerate.

The older limey sediments which occur as elongate NW-SE zones in the apparently younger intercalated volcano-sediments appear to have attained this style from isoclinal folding toward the southwest. Many of the folds observed are overturned and along the extreme northeast corner of the map area southwesterly trending thrust faulting is recorded. The trusting has brought Upper Triassic andesitic-basaltic volcanics and minor sediments against the older rocks.

## LOCAL GEOLOGY

The Hop claim group is underlain by intercalated? sediments and volcanics. The volcanic rocks observed were generally fine grained greenish crystalline andesite to layered or banded, fine grained, crystal, lithic andesitic? tuff. The sedimentary rocks observed were as fine to coarse grained grey coloured limestone; grey to brown coloured, aphanitic chert with a stong conchoidal fracture; grey to black coloured mudstone (argillaceous); grey to buff coloured phyllite and a very fine grained, black coloured (carbonaceous) shale and schist. The rocks observed do not appear to have undergone metamorphism but structural preparation and alteration in places appears quite intense.




# HOP MINERAL CLAIM GROUP

## GEOLOGY & CLAIM MAP
## LIARD MINING DIVISION

0 5 10 KILOMETERS

GEOLOGICAL ASSOCIATION OF CANADA
J. W. McLEOD
FELLOW

| Figure: | NTS | Drawn by | Date: |
|---|---|---|---|
| 2 | 104J | J.W.M. | 12/87 |

# LEGEND

## CENOZOIC

QUATERNARY

PLEISTOCENE AND RECENT

**11** Fluviatile gravel, sand, and silt; glacial outwash; till and alpine moraine

TERTIARY AND QUATERNARY

LATE TERTIARY AND PLEISTOCENE

**10** Basalt, olivine basalt; minor trachyte and rhyolite; in part younger than 11

TERTIARY

PALEOCENE AND (?) LATER

**9** Lacustrine sandstone, siltstone, conglomerate, and tuff; contains coalified wood and thin coal seams

## MESOZOIC

JURASSIC

LOWER JURASSIC

**8** Granite-boulder conglomerate, chert-pebble conglomerate. greywacke, quartzose sandstone, siltstone and shale; 8a, metamorphosed equivalents of 8 and including abundant sills and dykes of quartz-feldspar porphyry

**7** Well bedded greywacke, graded siltstone and silty sandstone, slate; minor volcanic sandstone and pebbly mudstone; 7a, metamorphosed equivalents of 7 and including abundant sills and dykes of quartz-feldspar porphyry

TRIASSIC AND LATER

**6** Undifferentiated granitic rocks, mainly granodiorite; 6a, granite and granodiorite; 6b, quartz monzonite; 6c, diorite and monzonite; 6d, syenite; 6e, diorite and gabbro

TRIASSIC

UPPER TRIASSIC

**5** Limestone; minor sandstone, argillite, and chert

**4** Andesite, basalt, tuff, breccia, volcanic sandstone and conglomerate; minor greywacke, argillite, and shale; many small stocks, dykes, and sills of porphyritic andesite and basalt; 4a, andesite and basalt porphyry

TRIASSIC AND EARLIER

PRE UPPER TRIASSIC

**3** Undivided, fine-grained clastic sediments and intercalated volcanic rocks, largely altered to greenstone and phyllite; chert, jasper, greywacke, and limestone; 3a, chert, slate, argillite, greywacke, greenstone, and limestone; mainly pre-Permian but probably includes younger rocks; 3b, mainly greenstone; age uncertain; 3c, greenstone, jasper, slate, chert, greywacke, fine-grained clastic rocks, conglomerate; mainly post-Permian, in part older than 2

## PALAEOZOIC

PERMIAN

**2** Chiefly limestone and dolomitic limestone; minor chert, argillite, and sandy limestone; may locally include limestone older than 2

PERMIAN (?)

**1** Peridotite, serpentinite, and small irregular bodies of meta-diorite and meta-gabbro; age uncertain, may be pre-Permian or Triassic

## METAMORPHIC ROCKS

**A** Diorite-gneiss, amphibolite, migmatite

**B** Biotite-muscovite-quartz gneiss and schist; minor crystalline limestone, greenstone, and quartzite; probably Devono-Mississippian and (?) Pennsylvanian

The rocks generally appear to have been deposited in a pelagic marine environment and some of the andesitic volcanics may exhibit a "pillow" structure indicating sub-marine deposition.

Considerable folding and fracturing is observed throughout the relatively small area covered by the exploration efforts to date. Evidence of northeast-southwest folding with a northwesterly fold axis is observed in a number of places and what has been thought of as intercalations of volcanics within the sedimentary section observed may in fact be major post-depositional contacts. The writer feels that the tuffaceous volcanics are possibly intercalations within the section while the andesites may have been deposited later.

Alteration minerals observed on the property in order of increasing abundance were mainly as chlorite, calcite and quartz. The chlorite alteration is mainly evident in the andesites as is the calcite which was found mainly near the contact. The calcite is found to occur as a white coloured secondary film or coating on steep cliff-faces of highly fractured andesitic rock or as fracture filling and veinlets in coarser crystalline form in the andesite often accompanying quartz. Silicification is pervasive and widespread in certain argillaceous or shaley rock units.

The only sulphide mineralization observed by the writer were very localized occurrences of pyrite and in one location as pyrite and chalcopyrite. In places a moderate amount of manganese staining was found to be present. The gold values encountered seem to occur with quartz veining or silicified zones, but there seems to be a marked absence of sulphides.

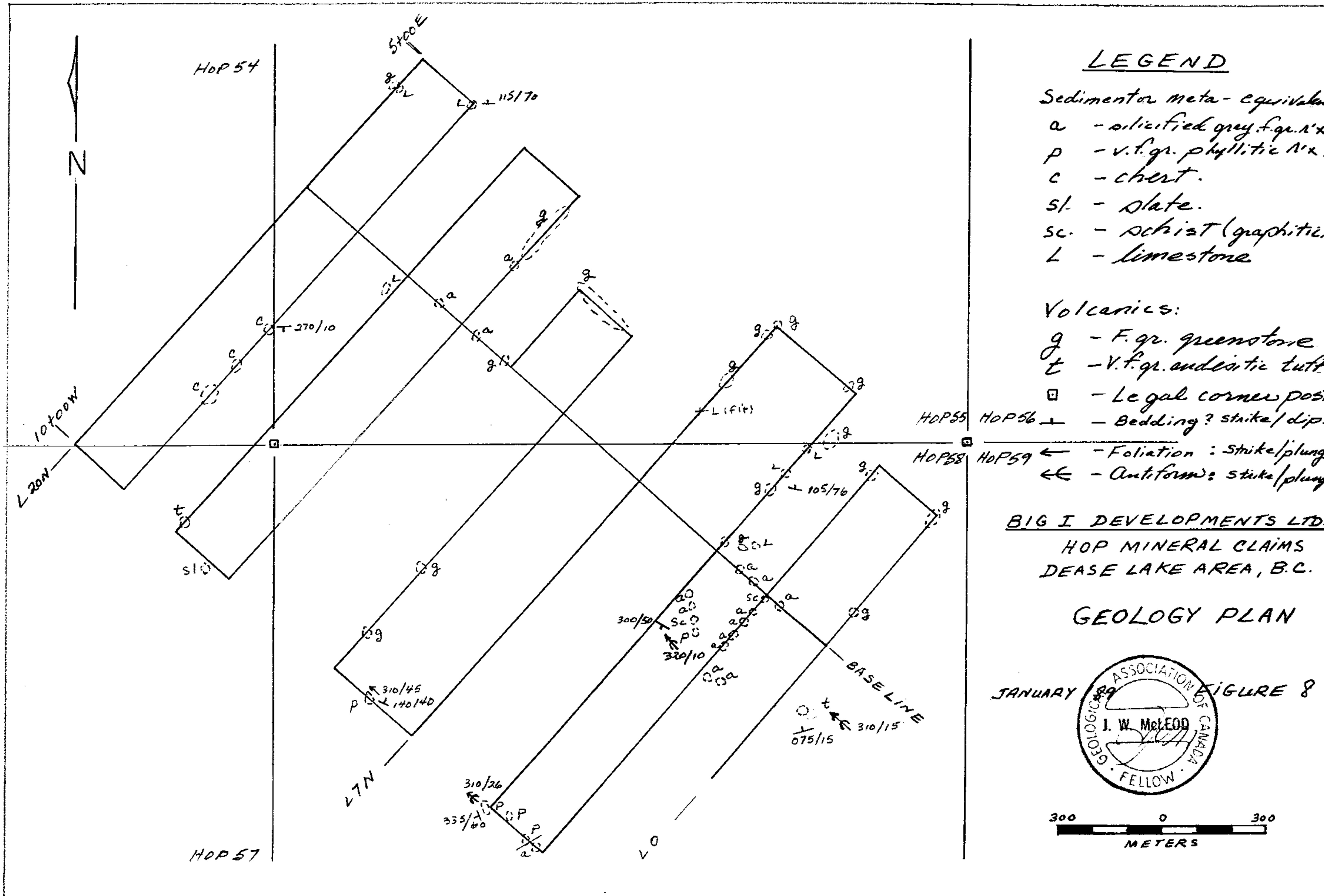
## PRESENT WORK PROGRAM

The present work program involved reconnaissance geological mapping and prospecting mainly along the 2 kilometers of baseline and 15.3 kilometers of grid lines which were installed.

A soil sampling program was undertaken along the lines at 50 meter intervals. A total of 350 soils, 15 silts and 61 rock samples were taken.

The soil samples were taken from the "B" soil horizon where possible, but a majority of the samples were taken from a brown soil with many angular to sub-angular rock fragments. The soil is thought to be very juvenile because of climatic, precipitation and drainage conditions experienced in this area, in the relatively short period of time since the area was scoured by glaciation.

The samples were placed in Kraft sample bags and subsequently shipped to Vancouver, B.C. The samples were analysed by Acme Analytical Laboratories of 852 East Hastings Street, Vancouver, B.C. The samples were analysed for 30 elements by the induction coupled plasma (ICP) method and for gold by agua regia digestion and subsequent detection


LEGEND
Sedimentary meta-equivalent.
a - silicified grey f.gr. r'x.
p - v.f.gr. phyllitic r'x.
c - chert.
sl - slate.
sc. - schist (graphitic)
L - limestone
Volcanics:
g - F.gr. greenstone
t - V.f.gr. andesitic tuff
- Legal corner post.
- Bedding? strike/dip.
- Foliation: strike/plunge
- Antiform: strike/plunge
BIG I DEVELOPMENTS LTD.
HOP MINERAL CLAIMS
DEASE LAKE AREA, B.C.
GEOLOGY PLAN
JANUARY 89
FIGURE 8
ASSOCIATION OF CANADA
GEOLOGICAL
J. W. McLEOD
FELLOW
300
0
300
METERS
N
HOP 54
HOP 55
HOP 56
HOP 57
HOP 58
HOP 59
5+00E
10+00W
L 20N
L 7N
L 0
BASELINE
115/70
270/10
105/76
300/50
320/10
310/45
140/40
310/26
335/60
310/15
075/15
L (fit)

by atomic absorption (AA).

A filter analyses of the high level aeromagnetic data for the area was made to determine the vector distortion of the data (see Figure 3) which may indicate sub-surface structure and geological contacts. This data was used to determine the lay-out of the grid and subsequent ground magnetometer and VLF-EM surveys over the grid appear to confirm this interpretation (see Figures 6&7).

The magnetometer and VLF-EM used in the survey were a G-826 Proton-type, serial no. 223 measuring total magnetic field and a Geotronics G28, serial no. V 102, measuring the dip angle of the very low frequency submarine communications signal transmitted from Seattle, Washington, USA at a frequency of 24.8 kilohertz (Khz).

## CONCLUSIONS

The initial reconnaissance work performed by the writer on the Hop claim group during 1986 revealed a number of positive features which encouraged Big I Developments Ltd. to undertake the present work program on the property.

A number of anomalous indications are revealed by the exploration methods used to date and which are listed as follows: 1) Filtering the available high level aeromagnetic data; 2) Geochemistry; 3) Ground magnetometer survey; 4) Ground VLF-EM survey and 5) Geology and prospecting. The results of each method will be listed as follows:

1) **Vector distortion of the aeromagnetic data** - An examination of Figure 3 reveals two linear zones which are thought to be major geological contacts trending northwest-southeast ie. those with distinctly different remnant magnetism or lateral susceptibilities, as well as, one sub-parallel linear fault? zone cutting through two and possibly three vector distortion lows which are situated on the southwest side of the grid. Two discontinuous sub-parallel east-west fracture or fault zones may cut the southern corner of the grid. Not all of the above mentioned features occur in the area presently covered by the grid.

2) **Geochemical soil, silt and rock data** - A review of the geochemical data suggested that zinc and barium offered the best opportunity for contourability. An examination of the resulting plots, Figures 4 and 5 reveals very localized zones of anomalous zinc and a northwest-southeast trend of the barium contours. Further contouring of other elements may be undertaken, but from plotting of individual anomalous values of gold, silver, arsenic, copper and molybdenum the best bet seems to be arsenic although some grouping of other elements is indicated. A apparent lack of correlation between gold sample values obtained during the 1986 sampling program and the present one suggests that re-analysing a number of select samples should be undertaken. The re-analyses will be done on a few samples using fire

assaying.

3) **Ground magnetometer results** - The magnetometer data appears to delineate the contact across the northeastern side of the grid and reinforces the vector distortion low in the northwestern quadrant of the present grid. The magnetic high on the southwestern end of Line 10, as well as, the northeastern linear high ie. contact, conform well with the mapped occurrences of greenstone or andesitic volcanics (see Figure 6).

4) **Ground VLF-EM results** - An examination of Figure 7 reveals that raw data anomalies occur on the periphery of magnetic highs ie. greenstone contacts for example along the northestern boundary of the grid and near the western-end of L10. Not so easily explained are the anomalies on the northwestern edge of the grid or in the central portion of the grid and trending northwest-southeast although a rough correlation appears to exist between this trend and apparent occurrence of the altered (silicified) mudstone or argillaceous unit.

5) **Geological interpretation of the present grid area** - The area covered by the present grid is underlain mainly by a section of northwest-southeast to east-west trending sediments and possibly intercalated tuffaceous volcanics which appear to have been intruded by andesitic volcanics (greenstone?). The sediments have undergone very low grade metamorphism, but more likely diagenetic changes, some tilting, northeast-southwest folding, in places considerable fracturing and attendant siliceous (quartz) and/or calcite alteration and possible precious metal mineralization.

## RECOMMENDATIONS

The writer recommends the following two phase exploration program for the Hop claim group.

Initiation of Phase II is conditional on the results obtained from the Phase I program.

### Phase I

Geological mapping and prospecting of the entire claim group, a suggested scale for mapping could be 1:5000. Line installation over the claim group at 200 metre line spacing with 50 metre station intervals for a total of 120 line kilometres (of which approximately 14% is completed). On the above described grid the following surveys could be undertaken: geochemical soil, silt and rock sampling; magnetometer and VLF-EM surveys.

Close-spaced grids and the subsequent surveys could be undertaken over anomalous or mineralized areas revealed by the Phase I program.

Hand trenching anomalous or mineralized zones which are encountered should be considered before a bulldozer and/or drill are brought in.

Phase II

Bulldozer work including road construction, trenching mineralized or anomalous zones and for drill site preparation.

Diamond core drilling of the priority anomalous zones.

COST ESTIMATE

Phase I

| | |
|---|---|
| Geological mapping and supervision for 1 month | $ 9,000 |
| A prospector for 1 month | 6,000 |
| Line installer for 1 month | 6,000 |
| Geochemical soil and silt sampling surveys including close-spaced grids | 7,000 |
| Geochemical sample preparation and analyses of approximately 2,500 samples | 15,000 |
| Magnetometer surveys including base recorder and interpretation | 6,000 |
| VLF-EM surveys including interpretation | 6,000 |
| Hand trenching including explosives, etc. | 2,000 |
| Transportation including mobilization and de-mobilization of the camp | 8,000 |
| Camp and board for 180 mandays @ $40/day plus the cook | 10,000 |
| Equipment and supplies | 3,000 |
| Reports, maps, licenses and fees | 2,000 |
| Insurance, Workers compensation, etc. | 5,000 |
| Contingency | 7,000 |
| **Sub-total(carried forward)** | **$ 92,000** |

Phase II

| | |
|---|---|
| Geological mapping, sampling and supervision for 1 month | $ 9,000 |
| Bulldozer contract for access road, trenching and drill site preparation for 150 hours @ $120/hour | 18,000 |
| 850 metres diamond core drilling @ $80/metre, all inclusive | 68,000 |
| Transportation | 5,000 |
| Camp and board | 5,000 |
| Sample preparation, boxing core and core storage facility | 1,000 |
| Sample analyses - 500 samples @ $10 ea. | 5,000 |
| Contingency | 11,000 |
| Sub-total | $122,000 |
| TOTAL | $214,000 |

Respectfully submitted,

GEOLOGICAL ASSOCIATION OF CANADA
J. W. McLEOD
FELLOW

James W. McLeod, Geologist

# STATEMENT OF COSTS

| | | |
|---|---|---|
| Transportation: | | |
| | Helicopter | 786.45 |
| | Truck rental | 600.00 |
| | Mileage @ $0.30/km. | 1200.00 |
| | Fuel and repairs | 258.45 |
| Wages: Geologist and two assistants | | 7,500.00 |
| Photogeophysical interpretation | | 2,500.00 |
| Room | | 370.27 |
| Food | | 968.27 |
| Analyses | | 4,961.95 |
| Licenses, fees, etc. | | 500.00 |
| Telephone | | 50.67 |
| Report | | 1000.00 |
| Magnetometer and VLF-EM rental | | 800.00 |
| Equipment and supplies | | 593.37 |
| | TOTAL | $22,089.43 |

# REFERENCES

B.C. Minister of Mines Annual Report: 1902, p.44 ; 1929, p.112; 1937, B45.

B.C. Department of Mines, Bulletin No. 1 (1932): Lode-Gold Deposits of British Columbia, compiled by John D. Galloway.

McLeod, J.W. (1987): Geological and Geochemical Reconnaissance Report on the Hop Mineral Claims, Assessment Report, B.C. Ministry of Energy, Mines and Petroleum Resources.

O'Neill, J.J. and Gunning, H.C. (1934): Geological Survey of Canada, Economic Geology Series No. 13, Platinum and Allied Metal Deposits of Canada.

B.C. Ministry of Energy, Mines and Petroleum Resources, Open File 1986-7 (1986): Occurrence and Distribution of Platinum-Group Elements in British Columbia, compiled by V.J. Rublee.

# CERTIFICATE

I, JAMES W. McLEOD, of the Village of Ladner, Province of British Columbia, hereby certify as follows:

1) I am a Consulting Geologist with an office at 5303 River Road, Delta, B.C., V4K 1S8.

2) I am a Fellow of the Geological Association of Canada.

3) I graduated with a degree of Bachelor of Science, Major Geology, from the University of British Columbia in 1969.

4) I have practised my profession since 1969.

5) I do have an interest in the Hop mineral claim group which I received for financing previous fieldwork.

6) The above report is based on personal field experience gained on the property during 1986 and 1988 as well as from government reports and from personal communications with other parties familiar with the general area.

DATED at Ladner, Province of Britsh Columbia, this 12th day of January, 1989.

GEOLOGICAL ASSOCIATION OF CANADA
J. W. McLEOD
FELLOW

James W. McLeod, B.Sc.

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

# GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P10 SOIL P11 SILT P12-P13 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: OCT 6 1988 DATE REPORT MAILED: Oct 14/88 ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

BIG I DEVELOPMENTS File # 88-5051 Page 1

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L20N 10+00W | 7 | 58 | 15 | 94 | .1 | 28 | 10 | 498 | 3.12 | 7 | 5 | ND | 1 | 21 | 1 | 2 | 3 | 31 | .19 | .033 | 14 | 18 | .53 | 171 | .04 | 3 | 1.38 | .01 | .10 | 1 | 2 |
| L20N 9+50W | 5 | 66 | 26 | 148 | .3 | 46 | 11 | 515 | 4.47 | 7 | 5 | ND | 1 | 29 | 2 | 2 | 5 | 56 | .15 | .069 | 16 | 41 | .56 | 724 | .08 | 3 | 2.42 | .01 | .09 | 1 | 1 |
| L20N 9+00W | 5 | 32 | 15 | 69 | .3 | 17 | 5 | 200 | 2.09 | 4 | 5 | ND | 1 | 45 | 3 | 2 | 3 | 40 | .29 | .081 | 13 | 23 | .22 | 887 | .03 | 3 | 1.81 | .01 | .06 | 1 | 1 |
| L20N 8+50W | 6 | 47 | 13 | 100 | .2 | 35 | 10 | 413 | 3.54 | 8 | 6 | ND | 1 | 42 | 3 | 2 | 3 | 47 | .17 | .042 | 13 | 32 | .56 | 589 | .08 | 3 | 1.75 | .01 | .07 | 1 | 1 |
| L20N 8+00W | 7 | 58 | 21 | 128 | .5 | 36 | 16 | 1414 | 3.66 | 8 | 5 | ND | 1 | 247 | 2 | 2 | 3 | 50 | 1.75 | .155 | 13 | 36 | .47 | 899 | .04 | 2 | 2.32 | .01 | .09 | 1 | 2 |
| L20N 7+50W | 6 | 46 | 15 | 129 | .3 | 26 | 16 | 1423 | 4.02 | 6 | 6 | ND | 1 | 27 | 1 | 2 | 2 | 62 | .19 | .083 | 12 | 36 | .38 | 463 | .06 | 2 | 1.89 | .01 | .11 | 1 | 1 |
| L20N 7+00W | 4 | 31 | 12 | 102 | .2 | 26 | 8 | 421 | 5.76 | 6 | 5 | ND | 3 | 14 | 2 | 3 | 2 | 75 | .21 | .105 | 12 | 40 | .49 | 175 | .16 | 2 | 2.08 | .01 | .06 | 1 | 1 |
| L20N 6+50W | 3 | 21 | 19 | 137 | .3 | 24 | 9 | 763 | 6.11 | 7 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 86 | .11 | .075 | 12 | 40 | .37 | 215 | .28 | 2 | 2.47 | .01 | .09 | 1 | 1 |
| L20N 6+00W | 3 | 33 | 26 | 147 | .5 | 20 | 12 | 1419 | 4.87 | 6 | 5 | ND | 1 | 32 | 4 | 2 | 2 | 59 | .30 | .101 | 13 | 29 | .34 | 661 | .07 | 5 | 1.93 | .01 | .11 | 1 | 1 |
| L20N 5+50W | 4 | 29 | 19 | 95 | .1 | 25 | 9 | 544 | 4.78 | 7 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 68 | .09 | .065 | 13 | 37 | .38 | 204 | .20 | 2 | 2.49 | .01 | .05 | 1 | 1 |
| L20N 5+00W | 3 | 36 | 16 | 104 | .1 | 29 | 9 | 596 | 3.63 | 6 | 5 | ND | 1 | 35 | 1 | 2 | 2 | 53 | .30 | .094 | 11 | 37 | .39 | 580 | .04 | 2 | 2.07 | .01 | .07 | 1 | 1 |
| L20N 4+50W | 4 | 36 | 21 | 95 | .4 | 25 | 7 | 315 | 3.98 | 5 | 5 | ND | 1 | 16 | 2 | 2 | 4 | 66 | .11 | .089 | 14 | 41 | .39 | 265 | .11 | 2 | 2.97 | .01 | .07 | 1 | 1 |
| L20N 4+00W | 3 | 22 | 23 | 79 | .2 | 17 | 6 | 425 | 5.21 | 5 | 6 | ND | 2 | 15 | 1 | 2 | 2 | 88 | .11 | .142 | 13 | 35 | .31 | 111 | .29 | 2 | 1.94 | .01 | .06 | 1 | 2 |
| L20N 3+50W | 3 | 19 | 19 | 111 | .1 | 23 | 11 | 971 | 6.59 | 7 | 6 | ND | 3 | 12 | 1 | 2 | 3 | 80 | .11 | .175 | 14 | 40 | .41 | 144 | .34 | 2 | 2.01 | .01 | .07 | 1 | 1 |
| L20N 3+00W | 3 | 27 | 22 | 101 | .3 | 21 | 7 | 432 | 4.43 | 6 | 5 | ND | 1 | 13 | 2 | 2 | 2 | 69 | .10 | .068 | 15 | 37 | .38 | 164 | .18 | 3 | 2.43 | .01 | .06 | 1 | 2 |
| L20N 2+50W | 9 | 31 | 15 | 70 | .2 | 25 | 9 | 394 | 3.70 | 12 | 5 | ND | 3 | 23 | 1 | 4 | 2 | 45 | .09 | .062 | 17 | 28 | .43 | 231 | .09 | 2 | 1.77 | .01 | .09 | 2 | 10 |
| L20N 2+00W | 4 | 28 | 16 | 120 | .1 | 20 | 9 | 629 | 5.34 | 4 | 5 | ND | 1 | 13 | 2 | 2 | 2 | 73 | .10 | .085 | 16 | 36 | .34 | 186 | .21 | 2 | 1.98 | .01 | .05 | 1 | 1 |
| L20N 1+50W | 3 | 21 | 15 | 87 | .1 | 22 | 8 | 483 | 4.77 | 6 | 5 | ND | 1 | 14 | 1 | 2 | 2 | 64 | .17 | .062 | 13 | 37 | .38 | 153 | .18 | 2 | 2.35 | .01 | .05 | 2 | 2 |
| L20N 1+00W | 4 | 29 | 13 | 114 | .3 | 25 | 8 | 636 | 4.80 | 2 | 6 | ND | 1 | 15 | 2 | 2 | 2 | 67 | .19 | .084 | 16 | 39 | .38 | 417 | .17 | 3 | 2.94 | .01 | .05 | 1 | 3 |
| L20N 0+50W | 4 | 23 | 14 | 114 | .1 | 24 | 8 | 595 | 5.25 | 3 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 59 | .19 | .081 | 15 | 37 | .36 | 449 | .18 | 2 | 3.09 | .01 | .04 | 1 | 2 |
| L20N 0+50E | 2 | 30 | 17 | 94 | .1 | 37 | 12 | 711 | 3.85 | 7 | 5 | ND | 1 | 12 | 1 | 2 | 4 | 51 | .15 | .052 | 13 | 38 | .61 | 195 | .10 | 2 | 2.22 | .01 | .07 | 1 | 1 |
| L20N 1+00E | 2 | 46 | 17 | 119 | .1 | 47 | 12 | 664 | 4.78 | 4 | 5 | ND | 2 | 39 | 2 | 4 | 2 | 55 | .36 | .081 | 26 | 48 | .73 | 1054 | .22 | 2 | 2.84 | .02 | .08 | 1 | 3 |
| L20N 1+50E | 3 | 25 | 14 | 97 | .1 | 27 | 10 | 643 | 4.18 | 4 | 5 | ND | 1 | 12 | 1 | 2 | 2 | 61 | .17 | .077 | 12 | 41 | .50 | 246 | .10 | 2 | 2.20 | .01 | .06 | 1 | 1 |
| L20N 2+00E | 2 | 65 | 14 | 99 | .1 | 56 | 13 | 593 | 4.68 | 6 | 5 | ND | 1 | 22 | 2 | 3 | 2 | 66 | .29 | .076 | 20 | 52 | .79 | 766 | .09 | 3 | 3.34 | .01 | .10 | 1 | 2 |
| L20N 2+50E | 3 | 66 | 16 | 110 | .1 | 50 | 12 | 515 | 4.64 | 7 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 64 | .21 | .072 | 16 | 52 | .82 | 465 | .09 | 3 | 3.08 | .01 | .10 | 1 | 4 |
| L20N 3+00E | 1 | 38 | 15 | 115 | .1 | 45 | 15 | 1134 | 4.67 | 6 | 6 | ND | 1 | 27 | 1 | 2 | 2 | 61 | .77 | .178 | 26 | 50 | .70 | 807 | .08 | 2 | 2.51 | .01 | .09 | 1 | 1 |
| L20N 3+50E | 1 | 27 | 19 | 106 | .2 | 53 | 14 | 734 | 5.75 | 6 | 5 | ND | 1 | 7 | 2 | 4 | 2 | 66 | .14 | .116 | 15 | 55 | .57 | 116 | .10 | 6 | 2.07 | .01 | .09 | 2 | 1 |
| L20N 4+00E | 2 | 18 | 17 | 102 | .1 | 25 | 10 | 654 | 6.44 | 5 | 5 | ND | 2 | 9 | 1 | 2 | 2 | 77 | .12 | .077 | 17 | 38 | .37 | 184 | .39 | 2 | 2.74 | .01 | .06 | 2 | 1 |
| L20N 4+50E | 2 | 17 | 10 | 107 | .1 | 25 | 9 | 806 | 5.23 | 3 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 71 | .07 | .100 | 15 | 42 | .36 | 156 | .14 | 2 | 2.45 | .01 | .06 | 1 | 3 |
| L20N 5+00E | 3 | 26 | 17 | 117 | .1 | 26 | 9 | 705 | 4.91 | 3 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 59 | .09 | .125 | 14 | 37 | .33 | 436 | .05 | 2 | 1.69 | .01 | .07 | 1 | 7 |
| L18N 10+00W | 4 | 44 | 13 | 88 | .4 | 17 | 6 | 416 | 4.62 | 4 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 85 | .15 | .053 | 18 | 35 | .24 | 355 | .33 | 2 | 2.01 | .01 | .06 | 1 | 1 |
| L18N 9+50W | 4 | 57 | 13 | 75 | .1 | 25 | 6 | 411 | 3.53 | 2 | 5 | ND | 1 | 78 | 1 | 2 | 2 | 68 | .60 | .055 | 19 | 30 | .29 | 708 | .23 | 2 | 1.64 | .01 | .06 | 1 | 4 |
| L18N 9+00W | 3 | 25 | 17 | 82 | .1 | 15 | 5 | 293 | 3.31 | 4 | 5 | ND | 1 | 51 | 1 | 2 | 2 | 75 | .19 | .044 | 12 | 25 | .23 | 314 | .08 | 2 | 1.81 | .01 | .05 | 2 | 2 |
| L18N 8+50W | 4 | 94 | 13 | 134 | .5 | 56 | 13 | 561 | 3.18 | 9 | 5 | ND | 1 | 119 | 1 | 2 | 2 | 40 | 1.04 | .107 | 24 | 42 | .55 | 839 | .03 | 2 | 2.29 | .01 | .10 | 1 | 1 |
| L18N 8+00W | 3 | 41 | 15 | 124 | .2 | 40 | 10 | 441 | 2.92 | 5 | 5 | ND | 1 | 79 | 1 | 2 | 2 | 42 | .97 | .130 | 16 | 46 | .61 | 1784 | .04 | 3 | 2.34 | .01 | .09 | 1 | 4 |
| L18N 7+50W | 4 | 35 | 20 | 87 | .2 | 21 | 8 | 495 | 3.49 | 6 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 66 | .27 | .070 | 12 | 30 | .28 | 580 | .08 | 2 | 1.41 | .01 | .09 | 1 | 1 |
| STD C/AU-S | 17 | 57 | 39 | 132 | 6.7 | 68 | 30 | 1015 | 4.00 | 40 | 22 | 8 | 37 | 48 | 20 | 16 | 21 | 58 | .48 | .097 | 39 | 55 | .90 | 174 | .06 | 34 | 1.95 | .06 | .15 | 11 | 51 |

APPENDIX I

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L18N 7+00W | 5 | 31 | 23 | 104 | .1 | 24 | 9 | 663 | 5.62 | 3 | 5 | ND | 2 | 14 | 1 | 2 | 3 | 81 | .10 | .058 | 17 | 40 | .40 | 277 | .35 | 2 | 1.92 | .01 | .07 | 1 | 2 |
| L18N 6+50W | 2 | 47 | 16 | 86 | .1 | 32 | 9 | 466 | 4.71 | 6 | 5 | ND | 1 | 14 | 1 | 2 | 2 | 63 | .13 | .050 | 16 | 45 | .68 | 160 | .11 | 2 | 2.29 | .01 | .09 | 1 | 12 |
| L18N 6+00W | 5 | 53 | 22 | 98 | .1 | 39 | 12 | 509 | 4.37 | 7 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 58 | .16 | .047 | 16 | 47 | .69 | 278 | .08 | 3 | 2.59 | .01 | .10 | 1 | 1 |
| L18N 5+50W | 6 | 35 | 23 | 172 | .6 | 22 | 11 | 933 | 7.59 | 4 | 5 | ND | 3 | 21 | 1 | 2 | 2 | 84 | .14 | .103 | 16 | 47 | .37 | 382 | .32 | 3 | 2.89 | .01 | .10 | 1 | 1 |
| L18N 5+00W | 7 | 87 | 21 | 150 | .1 | 44 | 16 | 1166 | 4.18 | 10 | 5 | ND | 1 | 58 | 1 | 2 | 2 | 40 | .52 | .103 | 16 | 39 | .69 | 913 | .04 | 5 | 2.11 | .01 | .18 | 1 | 1 |
| L18N 4+50W | 2 | 25 | 27 | 243 | .2 | 27 | 11 | 949 | 9.81 | 2 | 6 | ND | 4 | 10 | 1 | 2 | 2 | 98 | .10 | .270 | 13 | 52 | .47 | 275 | .38 | 2 | 2.31 | .01 | .08 | 1 | 1 |
| L18N 4+00W | 9 | 105 | 18 | 206 | .3 | 49 | 12 | 1498 | 4.45 | 11 | 5 | ND | 1 | 57 | 1 | 2 | 2 | 31 | .66 | .087 | 16 | 33 | .64 | 1055 | .02 | 6 | 2.06 | .01 | .18 | 1 | 3 |
| L18N 3+50W | 3 | 44 | 13 | 105 | .1 | 50 | 15 | 735 | 3.93 | 10 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 57 | .30 | .071 | 17 | 54 | .81 | 449 | .10 | 4 | 2.22 | .01 | .11 | 1 | 2 |
| L18N 3+00W | 2 | 41 | 11 | 120 | .5 | 29 | 9 | 695 | 4.49 | 2 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 72 | .21 | .090 | 15 | 51 | .50 | 697 | .08 | 3 | 2.53 | .01 | .11 | 1 | 1 |
| L18N 2+50W | 4 | 36 | 8 | 64 | .2 | 26 | 10 | 922 | 2.24 | 2 | 5 | ND | 1 | 109 | 1 | 2 | 2 | 38 | 2.27 | .149 | 9 | 33 | .49 | 710 | .02 | 5 | 1.87 | .01 | .08 | 1 | 1 |
| L18N 2+00W | 3 | 32 | 16 | 114 | .1 | 31 | 10 | 609 | 3.96 | 3 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 58 | .27 | .061 | 15 | 46 | .64 | 272 | .10 | 3 | 1.97 | .01 | .09 | 1 | 1 |
| L18N 1+50W | 3 | 29 | 19 | 172 | .1 | 24 | 10 | 721 | 3.61 | 4 | 5 | ND | 1 | 25 | 2 | 2 | 2 | 57 | .44 | .092 | 16 | 40 | .53 | 554 | .09 | 5 | 1.58 | .01 | .11 | 1 | 1 |
| L18N 1+00W | 3 | 18 | 13 | 177 | .2 | 23 | 8 | 568 | 4.02 | 2 | 5 | ND | 1 | 25 | 2 | 2 | 2 | 60 | .48 | .110 | 16 | 42 | .42 | 790 | .15 | 3 | 2.66 | .01 | .08 | 1 | 1 |
| L18N 0+50W | 4 | 84 | 23 | 111 | .1 | 54 | 11 | 1029 | 3.89 | 9 | 5 | ND | 1 | 44 | 1 | 2 | 3 | 51 | 1.16 | .182 | 40 | 57 | .74 | 1386 | .06 | 2 | 3.44 | .01 | .13 | 1 | 2 |
| L18N 0+50E | 3 | 27 | 10 | 154 | .2 | 17 | 11 | 1158 | 9.30 | 2 | 5 | ND | 3 | 9 | 1 | 2 | 2 | 117 | .19 | .156 | 16 | 61 | .36 | 206 | .42 | 2 | 1.94 | .01 | .08 | 1 | 1 |
| L18N 1+00E | 1 | 53 | 12 | 156 | .1 | 49 | 16 | 1050 | 5.80 | 15 | 5 | ND | 1 | 41 | 1 | 2 | 2 | 71 | 1.45 | .144 | 27 | 75 | .80 | 887 | .16 | 2 | 3.86 | .02 | .11 | 1 | 1 |
| L18N 1+50E | 2 | 67 | 15 | 107 | .1 | 56 | 14 | 1512 | 4.70 | 8 | 5 | ND | 1 | 32 | 2 | 2 | 2 | 70 | 1.23 | .094 | 15 | 73 | 1.13 | 930 | .09 | 5 | 3.40 | .01 | .14 | 1 | 1 |
| L18N 2+00E | 6 | 90 | 19 | 117 | .1 | 57 | 15 | 706 | 5.28 | 9 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 70 | 1.00 | .069 | 25 | 65 | 1.13 | 1050 | .11 | 4 | 2.98 | .01 | .13 | 1 | 1 |
| L18N 2+50E | 2 | 124 | 11 | 131 | .1 | 74 | 18 | 502 | 4.98 | 2 | 5 | ND | 4 | 37 | 3 | 3 | 2 | 73 | .91 | .095 | 36 | 77 | 1.16 | 708 | .25 | 5 | 4.24 | .02 | .14 | 1 | 6 |
| L18N 3+00E | 1 | 54 | 6 | 88 | .2 | 44 | 12 | 617 | 4.29 | 4 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 71 | .38 | .108 | 14 | 61 | .88 | 276 | .11 | 4 | 3.05 | .01 | .10 | 1 | 1 |
| L18N 3+50E | 1 | 24 | 12 | 97 | .1 | 32 | 12 | 1053 | 6.69 | 6 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 90 | .13 | .129 | 14 | 67 | .54 | 125 | .14 | 2 | 2.64 | .01 | .12 | 1 | 1 |
| L18N 4+00E | 1 | 17 | 10 | 104 | .1 | 24 | 11 | 1063 | 6.27 | 3 | 7 | ND | 1 | 13 | 2 | 2 | 2 | 72 | .33 | .122 | 18 | 47 | .40 | 186 | .21 | 2 | 3.07 | .01 | .07 | 1 | 1 |
| L18N 4+50E | 1 | 27 | 13 | 138 | .1 | 39 | 12 | 1008 | 5.80 | 4 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 69 | .70 | .172 | 24 | 53 | .47 | 364 | .12 | 3 | 3.16 | .01 | .09 | 1 | 2 |
| L18N 5+00E | 1 | 22 | 16 | 106 | .1 | 35 | 12 | 1373 | 5.62 | 2 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 81 | .31 | .137 | 20 | 60 | .36 | 219 | .10 | 2 | 2.37 | .01 | .09 | 1 | 3 |
| L16N 10+00W | 3 | 17 | 15 | 119 | .4 | 15 | 7 | 618 | 6.18 | 2 | 5 | ND | 3 | 19 | 1 | 2 | 2 | 94 | .11 | .158 | 15 | 42 | .29 | 139 | .34 | 5 | 1.94 | .01 | .07 | 1 | 1 |
| L16N 9+50W | 3 | 51 | 15 | 127 | .3 | 34 | 15 | 1132 | 4.88 | 3 | 5 | ND | 1 | 117 | 1 | 2 | 2 | 72 | .75 | .086 | 19 | 46 | .54 | 608 | .11 | 2 | 2.77 | .01 | .13 | 1 | 1 |
| L16N 9+00W | 3 | 49 | 15 | 117 | .6 | 38 | 14 | 788 | 4.64 | 5 | 5 | ND | 2 | 36 | 3 | 2 | 2 | 65 | .27 | .107 | 21 | 51 | .72 | 528 | .09 | 5 | 2.99 | .01 | .14 | 1 | 17 |
| L16N 8+50W | 3 | 47 | 15 | 138 | .4 | 31 | 9 | 581 | 3.70 | 4 | 5 | ND | 1 | 30 | 1 | 2 | 3 | 56 | .25 | .114 | 13 | 46 | .44 | 551 | .03 | 2 | 2.19 | .01 | .16 | 2 | 1 |
| L16N 8+00W | 2 | 54 | 15 | 123 | .1 | 29 | 18 | 2407 | 3.57 | 6 | 5 | ND | 1 | 22 | 1 | 2 | 2 | 51 | .34 | .087 | 14 | 37 | .41 | 414 | .05 | 2 | 1.29 | .01 | .13 | 1 | 3 |
| L16N 7+50W | 2 | 35 | 18 | 113 | .5 | 24 | 8 | 536 | 3.97 | 3 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 75 | .12 | .102 | 15 | 42 | .42 | 356 | .17 | 2 | 2.33 | .01 | .09 | 1 | 1 |
| L16N 7+00W | 2 | 34 | 14 | 105 | .3 | 28 | 9 | 409 | 4.50 | 5 | 5 | ND | 4 | 18 | 1 | 2 | 2 | 74 | .16 | .073 | 15 | 48 | .57 | 181 | .18 | 2 | 2.59 | .01 | .10 | 1 | 1 |
| L16N 6+50W | 3 | 75 | 19 | 158 | .3 | 62 | 17 | 1174 | 5.58 | 5 | 5 | ND | 2 | 63 | 3 | 2 | 2 | 67 | 1.15 | .111 | 24 | 57 | .80 | 1354 | .15 | 5 | 3.68 | .01 | .14 | 1 | 2 |
| L16N 6+00W | 2 | 88 | 9 | 59 | 1.1 | 36 | 11 | 576 | 3.17 | 2 | 5 | ND | 1 | 96 | 4 | 2 | 2 | 52 | 2.65 | .172 | 15 | 38 | .65 | 607 | .07 | 6 | 2.24 | .01 | .09 | 1 | 1 |
| L16N 5+50W | 3 | 130 | 24 | 132 | .9 | 66 | 15 | 1269 | 4.56 | 10 | 6 | ND | 2 | 97 | 3 | 3 | 2 | 57 | 1.78 | .115 | 24 | 54 | .75 | 1442 | .06 | 5 | 3.17 | .01 | .18 | 1 | 8 |
| L16N 5+00W | 1 | 49 | 12 | 120 | .5 | 51 | 17 | 767 | 4.45 | 7 | 5 | ND | 4 | 22 | 5 | 3 | 2 | 67 | .36 | .065 | 15 | 61 | .91 | 248 | .15 | 5 | 3.18 | .01 | .11 | 2 | 1 |
| L16N 4+50W | 4 | 59 | 12 | 147 | .5 | 39 | 15 | 1810 | 5.22 | 4 | 5 | ND | 1 | 19 | 2 | 2 | 2 | 78 | .19 | .054 | 16 | 51 | .70 | 608 | .17 | 2 | 2.37 | .01 | .13 | 2 | 3 |
| STD C/AU-S | 18 | 57 | 42 | 132 | 7.1 | 68 | 28 | 1014 | 3.90 | 38 | 23 | 7 | 36 | 44 | 18 | 19 | 23 | 55 | .48 | .094 | 37 | 56 | .86 | 175 | .06 | 32 | 1.96 | .06 | .14 | 11 | 48 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L16N 4+00W | 3 | 40 | 18 | 96 | .5 | 25 | 8 | 477 | 4.18 | 3 | 5 | ND | 1 | 12 | 1 | 2 | 7 | 68 | .15 | .063 | 15 | 40 | .49 | 316 | .19 | 2 | 1.68 | .01 | .07 | 1 | 2 |
| L16N 3+50W | 11 | 128 | 16 | 170 | .5 | 52 | 11 | 574 | 5.03 | 6 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 50 | .21 | .112 | 19 | 48 | .74 | 1236 | .02 | 2 | 3.14 | .01 | .17 | 1 | 1 |
| L16N 3+00W | 7 | 82 | 18 | 122 | .4 | 47 | 14 | 809 | 4.49 | 6 | 6 | ND | 1 | 27 | 1 | 3 | 2 | 57 | .25 | .091 | 15 | 47 | .77 | 750 | .06 | 3 | 2.62 | .01 | .11 | 1 | 1 |
| L16N 2+50W | 9 | 52 | 23 | 133 | .2 | 33 | 11 | 767 | 4.70 | 3 | 5 | ND | 1 | 32 | 1 | 2 | 5 | 58 | .29 | .082 | 12 | 39 | .55 | 735 | .08 | 2 | 2.18 | .01 | .15 | 1 | 1 |
| L16N 2+00W | 10 | 77 | 19 | 136 | .4 | 33 | 10 | 610 | 5.02 | 6 | 5 | ND | 1 | 25 | 1 | 3 | 2 | 62 | .16 | .100 | 15 | 40 | .51 | 976 | .05 | 2 | 3.08 | .01 | .12 | 1 | 1 |
| L16N 1+50W | 9 | 45 | 15 | 147 | .8 | 26 | 9 | 717 | 6.28 | 3 | 5 | ND | 1 | 20 | 2 | 2 | 4 | 74 | .26 | .142 | 17 | 46 | .35 | 841 | .13 | 3 | 3.06 | .01 | .08 | 2 | 2 |
| L16N 1+00W | 4 | 53 | 19 | 100 | .1 | 50 | 13 | 1036 | 3.55 | 6 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 37 | .56 | .060 | 23 | 37 | .79 | 1018 | .07 | 2 | 1.98 | .01 | .09 | 1 | 1 |
| L16N 0+50W | 2 | 68 | 16 | 103 | .1 | 24 | 10 | 856 | 5.16 | 2 | 5 | ND | 1 | 10 | 1 | 2 | 4 | 64 | .14 | .096 | 29 | 37 | .30 | 550 | .20 | 2 | 3.24 | .01 | .05 | 2 | 1 |
| L16N 0+50E | 5 | 67 | 16 | 97 | .2 | 31 | 19 | 1556 | 2.69 | 2 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 36 | .11 | .093 | 20 | 33 | .42 | 760 | .05 | 2 | 1.83 | .01 | .08 | 2 | 2 |
| L16N 1+00E | 5 | 38 | 15 | 123 | .1 | 34 | 10 | 648 | 4.06 | 3 | 5 | ND | 1 | 41 | 1 | 3 | 4 | 55 | .53 | .108 | 16 | 45 | .65 | 680 | .10 | 4 | 1.88 | .01 | .08 | 1 | 1 |
| L16N 1+50E | 4 | 34 | 13 | 128 | .3 | 50 | 27 | 2862 | 5.75 | 2 | 6 | ND | 1 | 22 | 1 | 2 | 2 | 112 | .88 | .096 | 12 | 131 | 1.72 | 336 | .43 | 3 | 2.21 | .01 | .10 | 1 | 2 |
| L16N 2+00E | 4 | 53 | 9 | 101 | .1 | 39 | 16 | 1037 | 4.78 | 2 | 5 | ND | 1 | 35 | 1 | 2 | 2 | 72 | .72 | .117 | 17 | 54 | .91 | 351 | .14 | 2 | 2.81 | .01 | .05 | 1 | 1 |
| L16N 2+50E | 1 | 62 | 10 | 86 | .1 | 62 | 20 | 744 | 4.66 | 5 | 5 | ND | 2 | 18 | 1 | 3 | 4 | 84 | .59 | .064 | 11 | 67 | 1.57 | 174 | .25 | 4 | 2.50 | .01 | .07 | 1 | 1 |
| L16N 3+00E | 2 | 35 | 12 | 119 | .1 | 24 | 13 | 1116 | 6.27 | 2 | 5 | ND | 1 | 22 | 2 | 2 | 4 | 92 | .68 | .133 | 15 | 55 | .68 | 119 | .23 | 3 | 2.42 | .01 | .06 | 1 | 1 |
| L16N 3+50E | 1 | 38 | 16 | 102 | .1 | 32 | 18 | 999 | 6.64 | 2 | 6 | ND | 1 | 13 | 1 | 4 | 2 | 108 | .48 | .061 | 10 | 62 | .97 | 104 | .37 | 3 | 2.85 | .01 | .05 | 1 | 1 |
| L16N 4+00E | 1 | 33 | 15 | 114 | .1 | 57 | 16 | 893 | 5.71 | 10 | 5 | ND | 1 | 15 | 3 | 2 | 4 | 76 | .49 | .096 | 14 | 57 | .68 | 147 | .15 | 5 | 2.02 | .01 | .12 | 1 | 1 |
| L16N 4+50E | 2 | 15 | 12 | 118 | .2 | 21 | 10 | 1215 | 5.67 | 2 | 5 | ND | 1 | 8 | 1 | 3 | 2 | 74 | .13 | .100 | 17 | 39 | .22 | 139 | .16 | 3 | 2.44 | .01 | .06 | 2 | 1 |
| L16N 5+00E | 1 | 28 | 14 | 121 | .3 | 61 | 16 | 1055 | 6.09 | 2 | 5 | ND | 1 | 14 | 2 | 3 | 2 | 66 | .36 | .079 | 16 | 58 | .51 | 377 | .09 | 5 | 2.17 | .01 | .13 | 1 | 2 |
| L14N 10+00W | 4 | 40 | 16 | 112 | .4 | 34 | 11 | 666 | 3.74 | 2 | 6 | ND | 2 | 37 | 1 | 2 | 5 | 59 | .24 | .052 | 16 | 42 | .58 | 433 | .11 | 3 | 2.59 | .01 | .08 | 1 | 1 |
| L14N 9+50W | 3 | 31 | 15 | 86 | .1 | 28 | 9 | 450 | 3.66 | 3 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 54 | .16 | .060 | 14 | 39 | .47 | 257 | .12 | 2 | 2.19 | .01 | .09 | 2 | 1 |
| L14N 9+00W | 3 | 27 | 19 | 118 | .6 | 30 | 11 | 506 | 5.34 | 3 | 5 | ND | 4 | 18 | 2 | 5 | 2 | 70 | .11 | .171 | 14 | 46 | .47 | 287 | .24 | 6 | 2.89 | .01 | .10 | 3 | 2 |
| L14N 8+50W | 4 | 163 | 25 | 188 | .8 | 71 | 16 | 910 | 5.00 | 6 | 6 | ND | 2 | 97 | 1 | 2 | 2 | 54 | 1.42 | .095 | 25 | 63 | 1.07 | 1901 | .04 | 4 | 3.40 | .01 | .26 | 1 | 1 |
| L14N 8+00W | 3 | 104 | 21 | 145 | .3 | 59 | 15 | 860 | 4.30 | 5 | 5 | ND | 2 | 68 | 1 | 2 | 2 | 54 | 1.02 | .075 | 19 | 56 | .87 | 1194 | .10 | 4 | 2.49 | .01 | .12 | 1 | 1 |
| L14N 7+50W | 2 | 48 | 5 | 108 | .2 | 24 | 7 | 638 | 1.18 | 2 | 5 | ND | 1 | 190 | 1 | 2 | 2 | 15 | 3.27 | .128 | 6 | 27 | .34 | 1166 | .01 | 8 | .83 | .02 | .07 | 1 | 1 |
| L14N 7+00W | 3 | 39 | 12 | 129 | .2 | 26 | 13 | 1128 | 3.31 | 2 | 5 | ND | 1 | 69 | 1 | 2 | 2 | 50 | 1.22 | .100 | 12 | 36 | .63 | 841 | .03 | 4 | 1.41 | .01 | .13 | 1 | 1 |
| L14N 6+50W | 4 | 146 | 10 | 224 | .3 | 59 | 16 | 1107 | 4.58 | 6 | 6 | ND | 1 | 95 | 2 | 4 | 4 | 60 | 1.92 | .152 | 24 | 65 | 1.00 | 1179 | .06 | 6 | 3.03 | .01 | .12 | 1 | 4 |
| L14N 6+00W | 2 | 59 | 20 | 122 | .3 | 56 | 17 | 1011 | 5.02 | 5 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 68 | .49 | .071 | 17 | 69 | 1.06 | 809 | .10 | 6 | 2.92 | .01 | .11 | 1 | 1 |
| L14N 5+50W | 7 | 120 | 13 | 135 | .3 | 72 | 31 | 4993 | 4.29 | 5 | 5 | ND | 1 | 104 | 1 | 2 | 2 | 50 | 2.12 | .149 | 29 | 104 | .81 | 1153 | .04 | 3 | 3.33 | .01 | .09 | 1 | 2 |
| L14N 5+00W | 2 | 20 | 16 | 60 | .1 | 14 | 4 | 240 | 2.84 | 2 | 5 | ND | 1 | 11 | 1 | 2 | 2 | 76 | .15 | .046 | 12 | 36 | .27 | 147 | .15 | 2 | 1.59 | .01 | .06 | 2 | 1 |
| L14N 4+50W | 3 | 27 | 19 | 122 | .4 | 28 | 9 | 590 | 6.08 | 4 | 5 | ND | 2 | 10 | 1 | 3 | 5 | 79 | .15 | .144 | 15 | 49 | .46 | 156 | .23 | 3 | 2.67 | .01 | .07 | 2 | 2 |
| L14N 4+00W | 4 | 30 | 17 | 81 | .3 | 18 | 9 | 992 | 2.62 | 2 | 5 | ND | 2 | 47 | 1 | 2 | 2 | 38 | 1.35 | .094 | 14 | 24 | .55 | 1680 | .06 | 5 | 2.13 | .01 | .11 | 1 | 1 |
| L14N 3+50W | 3 | 51 | 6 | 173 | .3 | 27 | 8 | 1542 | 1.89 | 2 | 5 | ND | 1 | 109 | 1 | 2 | 2 | 22 | 3.15 | .176 | 12 | 23 | .42 | 1577 | .03 | 5 | 1.49 | .01 | .05 | 1 | 1 |
| L14N 3+00W | 4 | 53 | 7 | 142 | .3 | 28 | 4 | 260 | 1.14 | 2 | 5 | ND | 1 | 158 | 2 | 2 | 2 | 15 | 3.76 | .159 | 9 | 20 | .32 | 1551 | .02 | 10 | 1.19 | .02 | .04 | 1 | 2 |
| L14N 2+50W | 2 | 33 | 3 | 91 | .4 | 19 | 3 | 385 | .49 | 2 | 5 | ND | 1 | 131 | 3 | 2 | 2 | 5 | 3.47 | .134 | 5 | 9 | .25 | 1510 | .01 | 6 | .62 | .01 | .06 | 1 | 1 |
| L14N 2+00W | 4 | 112 | 14 | 133 | 1.0 | 48 | 11 | 1147 | 3.11 | 4 | 7 | ND | 1 | 131 | 1 | 4 | 2 | 34 | 2.78 | .199 | 16 | 41 | .59 | 3814 | .01 | 7 | 2.61 | .01 | .13 | 1 | 1 |
| L14N 1+50W | 2 | 47 | 17 | 137 | .4 | 27 | 9 | 1322 | 4.18 | 2 | 10 | ND | 2 | 23 | 2 | 3 | 2 | 64 | .38 | .092 | 24 | 34 | .31 | 1855 | .12 | 6 | 1.80 | .01 | .07 | 1 | 2 |
| STD C/AU-S | 18 | 57 | 40 | 132 | 6.7 | 67 | 28 | 1035 | 3.94 | 38 | 23 | 8 | 36 | 47 | 19 | 16 | 23 | 57 | .48 | .093 | 38 | 57 | .90 | 175 | .06 | 34 | 1.97 | .06 | .15 | 13 | 53 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L14N 1+00W | 3 | 27 | 13 | 203 | .1 | 18 | 13 | 7372 | 3.01 | 2 | 5 | ND | 1 | 47 | 2 | 2 | 2 | 48 | 1.05 | .129 | 10 | 24 | .25 | 1733 | .08 | 2 | .86 | .01 | .09 | 1 | 1 |
| L14N 0+50W | 1 | 21 | 9 | 54 | .1 | 14 | 5 | 324 | 3.18 | 3 | 5 | ND | 1 | 10 | 1 | 2 | 2 | 77 | .17 | .079 | 10 | 34 | .24 | 387 | .15 | 2 | 1.16 | .01 | .06 | 1 | 1 |
| L14N 0+50E | 2 | 42 | 20 | 89 | .2 | 15 | 7 | 489 | 3.94 | 3 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 51 | .07 | .175 | 14 | 30 | .19 | 613 | .06 | 2 | 1.85 | .01 | .06 | 1 | 1 |
| L14N 1+00E | 4 | 34 | 14 | 62 | .1 | 26 | 7 | 303 | 3.33 | 9 | 5 | ND | 1 | 12 | 3 | 2 | 2 | 39 | .11 | .056 | 18 | 32 | .45 | 221 | .06 | 3 | 1.60 | .01 | .09 | 2 | 1 |
| L14N 1+50E | 2 | 35 | 5 | 84 | .1 | 17 | 11 | 1064 | 3.23 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 47 | .44 | .122 | 12 | 29 | .28 | 269 | .07 | 2 | 1.73 | .01 | .04 | 1 | 1 |
| L14N 2+00E | 3 | 40 | 8 | 99 | .1 | 16 | 12 | 1581 | 3.55 | 2 | 5 | ND | 1 | 94 | 1 | 2 | 2 | 55 | 2.15 | .244 | 12 | 39 | .32 | 491 | .07 | 2 | 1.46 | .01 | .03 | 1 | 1 |
| L14N 2+50E | 1 | 47 | 11 | 106 | .2 | 32 | 19 | 952 | 5.95 | 2 | 5 | ND | 1 | 12 | 3 | 2 | 2 | 157 | 1.44 | .084 | 3 | 63 | 1.68 | 105 | .42 | 6 | 2.90 | .01 | .08 | 1 | 1 |
| L14N 3+00E | 1 | 68 | 6 | 102 | .1 | 45 | 24 | 1285 | 5.42 | 3 | 5 | ND | 1 | 19 | 2 | 2 | 2 | 97 | .82 | .091 | 6 | 63 | 1.39 | 142 | .18 | 3 | 2.60 | .01 | .07 | 1 | 7 |
| L14N 3+50E | 1 | 38 | 13 | 95 | .1 | 41 | 21 | 641 | 5.68 | 2 | 5 | ND | 1 | 12 | 2 | 3 | 2 | 104 | 1.58 | .075 | 3 | 71 | 2.21 | 70 | .42 | 5 | 3.10 | .01 | .11 | 1 | 1 |
| L14N 4+50E | 1 | 58 | 3 | 79 | .1 | 48 | 13 | 548 | 3.90 | 3 | 5 | ND | 2 | 18 | 1 | 2 | 2 | 68 | .50 | .077 | 11 | 55 | .96 | 138 | .15 | 2 | 1.96 | .01 | .05 | 1 | 8 |
| L14N 5+00E | 1 | 23 | 9 | 95 | .1 | 30 | 27 | 10501 | 3.80 | 2 | 5 | ND | 1 | 19 | 2 | 2 | 2 | 55 | 1.03 | .278 | 9 | 41 | .50 | 503 | .02 | 2 | 2.13 | .01 | .05 | 1 | 1 |
| L12N 0+50E | 2 | 29 | 3 | 122 | .1 | 25 | 12 | 1416 | 3.89 | 2 | 5 | ND | 2 | 21 | 3 | 2 | 7 | 70 | .64 | .095 | 8 | 50 | .61 | 252 | .11 | 4 | 1.86 | .01 | .06 | 1 | 1 |
| L12N 1+00E | 1 | 127 | 12 | 101 | .1 | 26 | 11 | 928 | 3.96 | 2 | 5 | ND | 1 | 42 | 2 | 2 | 2 | 66 | .98 | .263 | 23 | 47 | .57 | 400 | .05 | 3 | 3.32 | .01 | .06 | 1 | 1 |
| L12N 1+50E | 1 | 106 | 8 | 74 | .1 | 22 | 8 | 661 | 2.83 | 2 | 5 | ND | 1 | 66 | 1 | 2 | 2 | 68 | 1.78 | .380 | 34 | 40 | .46 | 240 | .03 | 2 | 3.06 | .01 | .03 | 1 | 1 |
| L12N 2+00E | 1 | 47 | 9 | 91 | .1 | 49 | 14 | 763 | 3.88 | 2 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 63 | .37 | .068 | 12 | 54 | .92 | 135 | .14 | 5 | 2.40 | .01 | .08 | 1 | 1 |
| L12N 2+50E | 1 | 42 | 18 | 133 | .1 | 29 | 11 | 1010 | 5.01 | 2 | 5 | ND | 1 | 15 | 1 | 2 | 3 | 92 | .49 | .082 | 8 | 55 | .56 | 143 | .12 | 2 | 2.13 | .01 | .06 | 1 | 1 |
| L12N 3+00E | 1 | 102 | 8 | 120 | .1 | 43 | 18 | 865 | 4.42 | 4 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 81 | 1.44 | .080 | 9 | 60 | 1.35 | 172 | .18 | 2 | 2.28 | .01 | .08 | 1 | 1 |
| L10N 10+00W | 1 | 44 | 15 | 152 | .1 | 33 | 11 | 617 | 4.01 | 4 | 5 | ND | 1 | 14 | 1 | 2 | 2 | 60 | .23 | .045 | 10 | 43 | .62 | 234 | .10 | 2 | 1.77 | .01 | .12 | 1 | 2 |
| L10N 9+50W | 2 | 41 | 13 | 95 | .1 | 34 | 10 | 559 | 3.68 | 4 | 5 | ND | 2 | 16 | 1 | 2 | 2 | 52 | .26 | .049 | 13 | 40 | .70 | 183 | .10 | 2 | 1.86 | .01 | .10 | 1 | 1 |
| L10N 9+50W A | 2 | 39 | 5 | 148 | .2 | 21 | 8 | 524 | 3.58 | 2 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 60 | .29 | .069 | 14 | 37 | .37 | 342 | .09 | 2 | 1.86 | .01 | .08 | 1 | 1 |
| L10N 9+00W | 4 | 44 | 5 | 111 | .1 | 29 | 9 | 1110 | 3.00 | 2 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 41 | .17 | .042 | 14 | 33 | .65 | 206 | .07 | 2 | 1.60 | .01 | .10 | 1 | 1 |
| L10N 8+50W | 2 | 37 | 22 | 169 | .5 | 39 | 12 | 568 | 5.53 | 6 | 5 | ND | 4 | 13 | 2 | 2 | 2 | 71 | .12 | .060 | 13 | 47 | .64 | 184 | .25 | 2 | 3.25 | .01 | .10 | 2 | 1 |
| L10N 8+00W | 2 | 35 | 12 | 98 | .1 | 32 | 11 | 977 | 3.99 | 3 | 5 | ND | 2 | 14 | 1 | 2 | 2 | 64 | .24 | .078 | 11 | 43 | .67 | 160 | .12 | 2 | 1.96 | .01 | .08 | 1 | 12 |
| L10N 7+50W | 3 | 84 | 11 | 125 | .1 | 47 | 20 | 2651 | 4.69 | 4 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 75 | .15 | .113 | 34 | 62 | .74 | 1486 | .06 | 2 | 3.73 | .01 | .11 | 2 | 1 |
| L10N 7+00W | 1 | 28 | 9 | 87 | .1 | 25 | 9 | 607 | 3.38 | 3 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 59 | .33 | .065 | 10 | 40 | .48 | 181 | .09 | 2 | 1.35 | .01 | .08 | 1 | 1 |
| L10N 6+50W | 1 | 93 | 7 | 83 | .2 | 38 | 12 | 1155 | 3.15 | 2 | 5 | ND | 1 | 93 | 2 | 2 | 2 | 38 | 1.86 | .200 | 18 | 44 | .52 | 1376 | .04 | 2 | 2.18 | .01 | .07 | 1 | 1 |
| L10N 6+00W | 1 | 25 | 11 | 157 | .1 | 41 | 13 | 630 | 6.20 | 5 | 5 | ND | 3 | 11 | 1 | 2 | 2 | 78 | .20 | .147 | 12 | 59 | .68 | 215 | .28 | 2 | 3.15 | .01 | .11 | 2 | 1 |
| L10N 5+50W | 2 | 29 | 13 | 145 | .1 | 32 | 10 | 614 | 4.66 | 3 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 75 | .36 | .073 | 16 | 50 | .59 | 461 | .24 | 2 | 2.30 | .01 | .08 | 1 | 1 |
| L10N 5+00W | 2 | 37 | 12 | 99 | .1 | 52 | 13 | 587 | 4.95 | 4 | 5 | ND | 2 | 21 | 1 | 2 | 2 | 81 | .41 | .041 | 9 | 71 | 1.14 | 290 | .23 | 2 | 2.56 | .01 | .11 | 1 | 1 |
| L10N 4+50W | 2 | 29 | 7 | 134 | .1 | 33 | 10 | 566 | 5.43 | 4 | 5 | ND | 3 | 17 | 2 | 3 | 2 | 80 | .27 | .043 | 12 | 56 | .77 | 272 | .27 | 2 | 2.21 | .01 | .12 | 1 | 1 |
| L10N 4+00W | 6 | 50 | 14 | 143 | .2 | 47 | 14 | 599 | 5.16 | 5 | 5 | ND | 1 | 55 | 1 | 2 | 2 | 67 | .77 | .102 | 18 | 56 | .75 | 834 | .12 | 2 | 3.07 | .01 | .10 | 1 | 2 |
| L10N 3+50W | 2 | 42 | 5 | 112 | .5 | 22 | 8 | 545 | 2.60 | 2 | 5 | ND | 1 | 149 | 2 | 2 | 2 | 32 | 2.55 | .183 | 10 | 30 | .38 | 1050 | .05 | 2 | 1.60 | .01 | .06 | 1 | 2 |
| L10N 3+00W | 2 | 50 | 14 | 137 | .1 | 42 | 12 | 770 | 4.70 | 4 | 5 | ND | 1 | 39 | 1 | 2 | 2 | 64 | .65 | .138 | 20 | 58 | .68 | 740 | .12 | 2 | 2.89 | .01 | .09 | 1 | 1 |
| L10N 2+50W | 1 | 38 | 17 | 118 | .1 | 37 | 13 | 814 | 5.40 | 3 | 5 | ND | 1 | 32 | 1 | 2 | 2 | 68 | .62 | .110 | 23 | 56 | .58 | 588 | .17 | 2 | 3.52 | .01 | .06 | 1 | 1 |
| L10N 2+00W | 1 | 33 | 8 | 109 | .1 | 39 | 12 | 669 | 5.46 | 2 | 5 | ND | 1 | 14 | 1 | 2 | 2 | 83 | .25 | .064 | 10 | 70 | .79 | 132 | .21 | 2 | 2.32 | .01 | .08 | 1 | 1 |
| L10N 1+50W | 2 | 37 | 10 | 112 | .3 | 39 | 13 | 687 | 6.35 | 2 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 101 | .44 | .060 | 10 | 81 | .94 | 139 | .28 | 2 | 2.31 | .01 | .06 | 1 | 1 |
| STD C/AU-S | 18 | 57 | 38 | 132 | 7.1 | 68 | 28 | 1018 | 3.90 | 37 | 20 | 7 | 37 | 45 | 17 | 17 | 20 | 56 | .47 | .090 | 37 | 57 | .85 | 175 | .06 | 32 | 1.92 | .06 | .14 | 12 | 49 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L10N 0+50E | 3 | 43 | 11 | 131 | .1 | 45 | 23 | 1633 | 6.17 | 2 | 5 | ND | 1 | 34 | 1 | 2 | 2 | 128 | .86 | .115 | 11 | 102 | 1.09 | 331 | .22 | 4 | 2.27 | .01 | .10 | 1 | 1 |
| L10N 1+00E | 2 | 51 | 6 | 119 | .1 | 48 | 18 | 1062 | 4.87 | 3 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 87 | .76 | .091 | 14 | 69 | 1.18 | 236 | .24 | 2 | 2.59 | .01 | .07 | 1 | 2 |
| L10N 1+50E | 2 | 35 | 12 | 144 | .1 | 21 | 11 | 1340 | 7.13 | 5 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 129 | .39 | .067 | 12 | 58 | .37 | 136 | .33 | 2 | 1.81 | .01 | .09 | 1 | 1 |
| L10N 2+00E | 2 | 50 | 9 | 140 | .2 | 22 | 16 | 1965 | 5.60 | 4 | 5 | ND | 1 | 25 | 1 | 2 | 3 | 93 | .76 | .149 | 11 | 46 | .49 | 184 | .09 | 2 | 1.92 | .01 | .07 | 1 | 2 |
| L10N 2+50E | 2 | 71 | 17 | 186 | .1 | 21 | 16 | 1331 | 7.97 | 2 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 101 | .25 | .070 | 18 | 45 | .35 | 120 | .46 | 2 | 2.25 | .01 | .06 | 1 | 1 |
| L10N 3+00E | 1 | 53 | 11 | 102 | .1 | 37 | 13 | 910 | 5.38 | 5 | 5 | ND | 1 | 16 | 1 | 3 | 2 | 88 | .44 | .075 | 14 | 52 | .79 | 116 | .23 | 3 | 3.03 | .01 | .05 | 1 | 1 |
| L7N 10+00W | 3 | 56 | 16 | 110 | .2 | 34 | 11 | 675 | 3.77 | 5 | 5 | ND | 1 | 20 | 1 | 3 | 2 | 57 | .28 | .027 | 13 | 38 | .68 | 525 | .12 | 2 | 2.03 | .01 | .13 | 1 | 1 |
| L7N 9+50W | 5 | 100 | 17 | 147 | .2 | 44 | 13 | 685 | 4.40 | 3 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 58 | .29 | .052 | 13 | 41 | .75 | 694 | .06 | 2 | 2.58 | .01 | .18 | 1 | 2 |
| L7N 9+00W | 7 | 109 | 26 | 232 | .2 | 47 | 14 | 1209 | 5.08 | 7 | 5 | ND | 1 | 52 | 1 | 2 | 2 | 66 | .48 | .115 | 17 | 48 | .68 | 1215 | .05 | 2 | 3.04 | .01 | .18 | 1 | 2 |
| L7N 8+50W | 11 | 186 | 32 | 461 | .8 | 61 | 18 | 1226 | 5.44 | 11 | 5 | ND | 1 | 139 | 1 | 2 | 2 | 60 | 1.40 | .162 | 15 | 50 | .78 | 1173 | .03 | 3 | 3.59 | .01 | .28 | 1 | 1 |
| L7N 8+00W | 2 | 48 | 5 | 176 | .3 | 49 | 14 | 708 | 5.81 | 6 | 5 | ND | 2 | 15 | 1 | 2 | 4 | 74 | .25 | .097 | 13 | 50 | .91 | 354 | .14 | 4 | 2.98 | .01 | .13 | 1 | 1 |
| L7N 7+50W | 4 | 44 | 14 | 120 | .1 | 38 | 10 | 415 | 4.26 | 8 | 5 | ND | 3 | 11 | 1 | 3 | 2 | 53 | .15 | .054 | 15 | 36 | .73 | 136 | .11 | 4 | 2.50 | .01 | .08 | 4 | 2 |
| L7N 7+00W | 4 | 26 | 4 | 108 | .1 | 38 | 13 | 557 | 6.28 | 6 | 5 | ND | 4 | 11 | 1 | 2 | 2 | 75 | .18 | .169 | 14 | 45 | .66 | 184 | .33 | 2 | 3.74 | .01 | .08 | 2 | 1 |
| L7N 6+50W | 3 | 27 | 13 | 154 | .7 | 20 | 9 | 670 | 6.98 | 3 | 5 | ND | 4 | 8 | 1 | 3 | 2 | 87 | .10 | .109 | 20 | 44 | .27 | 152 | .48 | 3 | 4.09 | .01 | .05 | 2 | 1 |
| L7N 6+00W | 3 | 51 | 4 | 151 | .7 | 34 | 11 | 620 | 6.49 | 3 | 5 | ND | 3 | 9 | 1 | 2 | 2 | 93 | .15 | .061 | 20 | 57 | .57 | 204 | .37 | 4 | 4.20 | .01 | .09 | 1 | 1 |
| L7N 5+50W | 3 | 17 | 18 | 78 | .3 | 13 | 5 | 332 | 4.29 | 6 | 5 | ND | 3 | 10 | 1 | 2 | 2 | 92 | .17 | .103 | 14 | 34 | .21 | 175 | .42 | 3 | 1.50 | .01 | .07 | 1 | 3 |
| L7N 5+00W | 3 | 45 | 7 | 114 | .4 | 28 | 10 | 610 | 5.86 | 5 | 5 | ND | 2 | 10 | 2 | 3 | 3 | 73 | .16 | .098 | 31 | 42 | .35 | 208 | .27 | 5 | 4.83 | .01 | .06 | 2 | 1 |
| L7N 4+50W | 3 | 22 | 2 | 106 | .5 | 20 | 8 | 545 | 7.11 | 4 | 5 | ND | 4 | 6 | 1 | 2 | 2 | 81 | .15 | .099 | 18 | 39 | .36 | 126 | .45 | 4 | 3.95 | .01 | .05 | 3 | 3 |
| L7N 4+00W | 2 | 37 | 12 | 102 | .3 | 42 | 13 | 536 | 4.31 | 7 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 69 | .24 | .046 | 12 | 52 | .81 | 177 | .14 | 3 | 2.78 | .01 | .07 | 1 | 1 |
| L7N 3+50W | 2 | 85 | 8 | 126 | .4 | 77 | 15 | 683 | 4.56 | 10 | 5 | ND | 2 | 45 | 1 | 3 | 3 | 66 | .99 | .057 | 21 | 62 | .92 | 687 | .15 | 4 | 2.80 | .01 | .13 | 1 | 2 |
| L7N 3+00W | 3 | 23 | 8 | 86 | .1 | 21 | 8 | 4931 | 6.68 | 3 | 5 | ND | 1 | 165 | 2 | 2 | 2 | 4 | 3.96 | .146 | 2 | 6 | .13 | 1025 | .01 | 11 | .21 | .01 | .04 | 1 | 1 |
| L7N 2+50W | 1 | 30 | 2 | 192 | .3 | 20 | 7 | 998 | 2.48 | 4 | 5 | ND | 1 | 168 | 2 | 2 | 2 | 13 | 4.36 | .155 | 3 | 7 | .17 | 1104 | .01 | 8 | .24 | .01 | .08 | 1 | 1 |
| L7N 2+00W | 2 | 38 | 7 | 106 | .1 | 43 | 11 | 559 | 4.73 | 3 | 5 | ND | 1 | 31 | 1 | 3 | 3 | 95 | .77 | .050 | 13 | 67 | .99 | 480 | .32 | 2 | 2.35 | .01 | .08 | 1 | 1 |
| L7N 1+50W | 4 | 74 | 9 | 177 | .4 | 40 | 12 | 1473 | 3.33 | 5 | 5 | ND | 1 | 124 | 1 | 2 | 2 | 44 | 3.58 | .308 | 29 | 50 | .50 | 427 | .03 | 2 | 2.90 | .01 | .07 | 1 | 1 |
| L7N 1+00W | 3 | 59 | 7 | 113 | .5 | 32 | 11 | 770 | 4.27 | 4 | 5 | ND | 1 | 66 | 1 | 2 | 2 | 69 | 1.68 | .290 | 21 | 62 | .50 | 798 | .05 | 3 | 2.85 | .01 | .06 | 1 | 1 |
| L7N 0+50W | 3 | 81 | 12 | 160 | .2 | 62 | 18 | 858 | 6.34 | 6 | 5 | ND | 1 | 75 | 1 | 2 | 2 | 96 | 2.03 | .136 | 21 | 93 | 1.07 | 994 | .16 | 5 | 3.88 | .01 | .12 | 1 | 16 |
| L7N 0+50E | 2 | 57 | 9 | 78 | .1 | 26 | 17 | 2480 | 2.23 | 6 | 5 | ND | 1 | 108 | 1 | 2 | 2 | 34 | 3.29 | .241 | 16 | 32 | .32 | 460 | .03 | 4 | 1.66 | .01 | .05 | 1 | 2 |
| L7N 1+00E | 2 | 64 | 3 | 115 | .1 | 26 | 11 | 1429 | 5.04 | 3 | 7 | ND | 1 | 16 | 1 | 2 | 2 | 89 | .44 | .153 | 38 | 47 | .36 | 221 | .10 | 2 | 3.74 | .01 | .05 | 1 | 1 |
| L7N 1+50E | 1 | 33 | 5 | 174 | .2 | 24 | 12 | 1502 | 6.18 | 3 | 5 | ND | 1 | 14 | 1 | 3 | 2 | 113 | .32 | .088 | 11 | 59 | .44 | 259 | .21 | 2 | 2.36 | .01 | .06 | 1 | 1 |
| L7N 2+00E | 1 | 36 | 10 | 181 | .2 | 16 | 10 | 1117 | 6.17 | 2 | 5 | ND | 1 | 20 | 1 | 3 | 3 | 81 | .84 | .095 | 19 | 35 | .21 | 170 | .28 | 2 | 1.97 | .01 | .05 | 1 | 1 |
| L7N 2+50E | 1 | 36 | 9 | 191 | .2 | 18 | 16 | 3104 | 6.11 | 2 | 5 | ND | 1 | 21 | 1 | 2 | 3 | 87 | 2.05 | .100 | 12 | 40 | .31 | 170 | .26 | 5 | 1.85 | .01 | .06 | 1 | 2 |
| L7N 3+00E | 2 | 68 | 14 | 107 | .1 | 50 | 19 | 1252 | 4.92 | 5 | 5 | ND | 1 | 31 | 1 | 2 | 2 | 82 | .89 | .155 | 20 | 58 | 1.10 | 306 | .12 | 3 | 3.70 | .01 | .08 | 1 | 1 |
| L7N 3+50E | 2 | 32 | 3 | 102 | .2 | 16 | 8 | 874 | 6.11 | 4 | 5 | ND | 1 | 11 | 1 | 3 | 2 | 125 | .28 | .071 | 16 | 47 | .29 | 106 | .32 | 4 | 1.85 | .01 | .06 | 2 | 1 |
| L7N 4+00E | 1 | 80 | 2 | 106 | .1 | 52 | 28 | 882 | 7.11 | 6 | 5 | ND | 1 | 13 | 1 | 2 | 3 | 168 | 2.22 | .049 | 3 | 69 | 2.79 | 73 | .48 | 13 | 3.75 | .01 | .10 | 1 | 2 |
| L4+25N 10+15W | 1 | 44 | 13 | 74 | .1 | 17 | 6 | 338 | 3.77 | 4 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 63 | .17 | .053 | 15 | 28 | .42 | 343 | .09 | 3 | 2.63 | .01 | .05 | 2 | 1 |
| L4N 10+00W | 4 | 29 | 15 | 114 | .8 | 23 | 7 | 503 | 5.76 | 5 | 5 | ND | 3 | 10 | 1 | 3 | 2 | 92 | .08 | .073 | 17 | 43 | .36 | 266 | .32 | 3 | 2.50 | .01 | .08 | 2 | 1 |
| STD C/AU-S | 17 | 58 | 42 | 132 | 7.0 | 68 | 30 | 1019 | 3.97 | 44 | 23 | 8 | 37 | 47 | 20 | 16 | 17 | 59 | .49 | .092 | 39 | 55 | .90 | 172 | .07 | 31 | 2.00 | .06 | .14 | 13 | 51 |

20

BIG I DEVELOPMENTS ILE # 88-5051



| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L4N 9+50W | 2 | 29 | 19 | 159 | .2 | 28 | 10 | 653 | 5.42 | 6 | 5 | ND | 2 | 17 | 1 | 2 | 2 | 77 | .19 | .109 | 12 | 42 | .55 | 312 | .24 | 2 | 2.22 | .01 | .10 | 1 | 1 |
| L4N 9+00W | 2 | 30 | 7 | 119 | .2 | 23 | 8 | 396 | 4.72 | 2 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 75 | .29 | .047 | 13 | 37 | .57 | 350 | .19 | 2 | 2.22 | .01 | .09 | 1 | 1 |
| L4N 8+50W | 3 | 30 | 13 | 156 | .6 | 23 | 10 | 766 | 5.75 | 2 | 5 | ND | 2 | 17 | 1 | 2 | 2 | 76 | .16 | .099 | 18 | 42 | .43 | 233 | .28 | 2 | 3.51 | .01 | .07 | 1 | 5 |
| L4N 8+00W | 2 | 26 | 18 | 151 | .2 | 26 | 9 | 516 | 5.60 | 4 | 5 | ND | 3 | 21 | 1 | 2 | 3 | 82 | .21 | .100 | 14 | 41 | .55 | 265 | .27 | 2 | 2.93 | .01 | .10 | 2 | 2 |
| L4N 7+50W | 2 | 99 | 21 | 125 | .1 | 52 | 13 | 529 | 5.63 | 2 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 70 | .33 | .088 | 35 | 52 | .70 | 372 | .21 | 2 | 4.87 | .01 | .13 | 2 | 3 |
| L4N 7+00W | 2 | 38 | 16 | 124 | 1.2 | 28 | 10 | 469 | 6.47 | 2 | 5 | ND | 4 | 8 | 1 | 2 | 2 | 80 | .12 | .093 | 23 | 46 | .41 | 223 | .42 | 2 | 4.52 | .01 | .08 | 1 | 1 |
| L4N 6+50W | 1 | 32 | 8 | 111 | .3 | 26 | 10 | 564 | 6.61 | 2 | 5 | ND | 3 | 8 | 1 | 2 | 2 | 80 | .18 | .116 | 25 | 45 | .44 | 162 | .38 | 2 | 4.92 | .01 | .07 | 2 | 1 |
| L4N 6+00W | 2 | 29 | 16 | 116 | .4 | 19 | 7 | 481 | 5.77 | 4 | 5 | ND | 1 | 11 | 1 | 2 | 3 | 84 | .21 | .078 | 18 | 41 | .36 | 166 | .35 | 2 | 2.81 | .01 | .06 | 1 | 1 |
| L4N 5+50W | 2 | 27 | 7 | 124 | .6 | 21 | 10 | 705 | 6.51 | 3 | 5 | ND | 4 | 7 | 1 | 2 | 2 | 81 | .12 | .130 | 20 | 43 | .32 | 157 | .46 | 2 | 3.99 | .01 | .07 | 2 | 1 |
| L4N 5+00W | 3 | 21 | 18 | 103 | .5 | 19 | 8 | 530 | 5.42 | 2 | 5 | ND | 3 | 9 | 2 | 2 | 3 | 88 | .14 | .076 | 17 | 43 | .33 | 133 | .39 | 2 | 2.83 | .01 | .07 | 2 | 1 |
| L4N 4+50W | 2 | 23 | 16 | 109 | .1 | 20 | 7 | 639 | 5.23 | 3 | 5 | ND | 3 | 8 | 1 | 2 | 2 | 90 | .11 | .085 | 15 | 44 | .37 | 131 | .38 | 2 | 2.24 | .01 | .07 | 2 | 1 |
| L4N 4+00W | 1 | 46 | 11 | 121 | .1 | 41 | 13 | 766 | 4.59 | 5 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 74 | .31 | .057 | 12 | 48 | .91 | 155 | .16 | 2 | 2.21 | .01 | .11 | 1 | 1 |
| L4N 3+50W | 3 | 27 | 11 | 129 | .4 | 23 | 9 | 538 | 4.85 | 4 | 5 | ND | 1 | 12 | 1 | 2 | 2 | 77 | .22 | .080 | 16 | 43 | .49 | 397 | .20 | 2 | 2.58 | .01 | .10 | 1 | 1 |
| L4N 2+50W | 8 | 36 | 15 | 86 | .2 | 21 | 6 | 229 | 3.73 | 5 | 5 | ND | 1 | 17 | 1 | 2 | 2 | 84 | .16 | .038 | 18 | 33 | .37 | 427 | .11 | 2 | 1.89 | .01 | .09 | 1 | 1 |
| L4N 2+00W | 3 | 79 | 15 | 237 | .2 | 52 | 21 | 984 | 5.55 | 3 | 5 | ND | 2 | 47 | 1 | 2 | 2 | 61 | 1.21 | .142 | 21 | 50 | .83 | 971 | .12 | 2 | 3.23 | .01 | .16 | 1 | 1 |
| L4N 1+50W | 3 | 35 | 11 | 141 | .5 | 17 | 7 | 655 | 4.73 | 2 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 73 | .51 | .102 | 17 | 36 | .23 | 872 | .21 | 2 | 1.94 | .01 | .06 | 1 | 1 |
| L4N 1+00W | 1 | 40 | 11 | 110 | .2 | 43 | 12 | 608 | 5.00 | 3 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 84 | .30 | .059 | 11 | 58 | .92 | 176 | .16 | 2 | 2.97 | .01 | .12 | 1 | 1 |
| L4N 0+50W | 1 | 35 | 12 | 142 | .7 | 37 | 11 | 793 | 4.96 | 2 | 5 | ND | 1 | 32 | 1 | 2 | 2 | 92 | 1.15 | .076 | 14 | 72 | .64 | 498 | .17 | 2 | 3.14 | .01 | .07 | 1 | 1 |
| L4N 0+50E | 1 | 49 | 5 | 126 | .3 | 33 | 11 | 753 | 3.61 | 2 | 5 | ND | 1 | 73 | 2 | 2 | 2 | 58 | 2.85 | .182 | 16 | 48 | .59 | 506 | .08 | 3 | 2.70 | .01 | .06 | 1 | 1 |
| L4N 1+00E | 1 | 53 | 4 | 142 | .1 | 24 | 7 | 678 | 2.68 | 2 | 5 | ND | 1 | 42 | 1 | 2 | 2 | 40 | 3.47 | .192 | 13 | 29 | .29 | 253 | .07 | 2 | 1.95 | .01 | .04 | 1 | 1 |
| L4N 1+50E | 2 | 21 | 16 | 161 | .3 | 23 | 9 | 890 | 6.27 | 3 | 5 | ND | 2 | 14 | 1 | 2 | 2 | 102 | .34 | .104 | 13 | 50 | .42 | 222 | .41 | 2 | 1.95 | .01 | .12 | 1 | 1 |
| L4N 2+00E | 1 | 52 | 2 | 174 | .1 | 42 | 14 | 2252 | 5.51 | 2 | 5 | ND | 1 | 31 | 1 | 2 | 2 | 65 | 1.21 | .106 | 16 | 44 | 1.10 | 354 | .16 | 2 | 2.76 | .01 | .10 | 1 | 1 |
| L4N 2+50E | 1 | 40 | 11 | 123 | .1 | 48 | 12 | 1620 | 4.91 | 4 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 72 | 1.00 | .064 | 22 | 53 | .84 | 179 | .15 | 2 | 2.97 | .01 | .13 | 1 | 1 |
| L4N 3+00E | 1 | 70 | 18 | 512 | .1 | 33 | 23 | 6978 | 5.12 | 2 | 5 | ND | 1 | 26 | 6 | 2 | 2 | 62 | 1.34 | .139 | 12 | 40 | .30 | 310 | .17 | 2 | 1.82 | .01 | .05 | 1 | 1 |
| L4N 3+50E | 1 | 66 | 3 | 140 | .1 | 17 | 13 | 5285 | 1.94 | 2 | 5 | ND | 1 | 35 | 1 | 2 | 2 | 35 | 1.93 | .337 | 31 | 23 | .16 | 289 | .02 | 3 | 2.46 | .01 | .05 | 1 | 1 |
| L4N 4+00E | 1 | 15 | 2 | 72 | .1 | 16 | 5 | 1081 | 1.49 | 3 | 5 | ND | 1 | 40 | 1 | 2 | 2 | 18 | 16.08 | .046 | 6 | 15 | .31 | 83 | .04 | 2 | .71 | .01 | .03 | 1 | 1 |
| L4N 4+50E | 1 | 60 | 15 | 143 | .1 | 69 | 17 | 2998 | 5.54 | 8 | 5 | ND | 2 | 24 | 2 | 3 | 2 | 77 | 2.80 | .097 | 33 | 57 | .78 | 238 | .09 | 3 | 2.49 | .01 | .14 | 1 | 1 |
| L4N 5+00E | 2 | 16 | 12 | 116 | .1 | 21 | 11 | 1815 | 5.79 | 4 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 88 | .21 | .082 | 14 | 50 | .29 | 164 | .21 | 2 | 2.08 | .01 | .08 | 2 | 1 |
| L4N 5+50E | 3 | 38 | 16 | 156 | .1 | 39 | 12 | 1580 | 4.45 | 5 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 73 | .20 | .101 | 13 | 52 | .42 | 264 | .07 | 2 | 2.10 | .01 | .12 | 2 | 1 |
| L4N 6+00E | 3 | 20 | 9 | 128 | .1 | 28 | 11 | 1134 | 5.25 | 2 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 78 | .18 | .111 | 14 | 51 | .45 | 342 | .10 | 2 | 2.15 | .01 | .08 | 1 | 1 |
| L2N 10+00W | 4 | 34 | 15 | 154 | .3 | 22 | 11 | 808 | 4.69 | 6 | 5 | ND | 1 | 38 | 1 | 2 | 2 | 56 | .33 | .077 | 15 | 30 | .45 | 519 | .08 | 2 | 1.89 | .01 | .14 | 1 | 1 |
| L2N 9+62W | 3 | 48 | 7 | 180 | .1 | 35 | 16 | 998 | 4.23 | 2 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 56 | .46 | .062 | 16 | 39 | .90 | 342 | .10 | 2 | 2.20 | .01 | .13 | 1 | 1 |
| L2N 9+50W | 5 | 102 | 14 | 152 | .8 | 43 | 10 | 1082 | 3.91 | 3 | 5 | ND | 1 | 194 | 1 | 2 | 2 | 53 | 1.85 | .184 | 15 | 41 | .47 | 1536 | .08 | 2 | 2.39 | .01 | .10 | 1 | 1 |
| L2N 9+00W | 7 | 64 | 20 | 278 | .9 | 35 | 22 | 3006 | 4.92 | 6 | 5 | ND | 1 | 30 | 4 | 2 | 2 | 66 | .31 | .146 | 15 | 38 | .36 | 1211 | .04 | 2 | 2.54 | .01 | .21 | 2 | 1 |
| L2N 8+50W | 5 | 44 | 19 | 184 | .5 | 28 | 13 | 1331 | 5.33 | 5 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 77 | .21 | .107 | 12 | 40 | .42 | 436 | .08 | 2 | 2.43 | .01 | .13 | 2 | 1 |
| L2N 8+00W | 3 | 25 | 25 | 173 | .7 | 22 | 9 | 674 | 5.93 | 6 | 5 | ND | 4 | 13 | 2 | 2 | 2 | 91 | .14 | .111 | 16 | 43 | .43 | 354 | .37 | 2 | 2.08 | .01 | .11 | 2 | 1 |
| STD C/AU-S | 17 | 58 | 35 | 132 | 7.1 | 68 | 28 | 1024 | 3.83 | 38 | 22 | 8 | 37 | 45 | 19 | 18 | 19 | 56 | .47 | .089 | 38 | 55 | .88 | 175 | .06 | 37 | 1.92 | .06 | .15 | 12 | 47 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L2N 7+50W | 4 | 24 | 20 | 125 | .7 | 12 | 7 | 515 | 3.74 | 2 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 99 | .17 | .043 | 17 | 40 | .27 | 410 | .45 | 2 | 1.81 | .01 | .08 | 1 | 1 |
| L2N 7+00W | 2 | 70 | 13 | 135 | 1.4 | 38 | 10 | 429 | 5.71 | 2 | 5 | ND | 1 | 14 | 1 | 2 | 3 | 71 | .17 | .098 | 20 | 54 | .58 | 356 | .15 | 2 | 4.21 | .01 | .14 | 1 | 1 |
| L2N 6+50W | 3 | 18 | 17 | 119 | .5 | 12 | 6 | 474 | 5.89 | 2 | 5 | ND | 3 | 7 | 1 | 2 | 2 | 107 | .06 | .072 | 22 | 44 | .22 | 127 | .63 | 2 | 2.19 | .01 | .06 | 1 | 1 |
| L2N 6+00W | 3 | 20 | 12 | 109 | .1 | 26 | 9 | 477 | 6.30 | 2 | 5 | ND | 4 | 11 | 1 | 3 | 2 | 66 | .26 | .113 | 21 | 42 | .47 | 191 | .38 | 2 | 4.96 | .02 | .07 | 1 | 1 |
| L2N 5+50W | 4 | 21 | 15 | 100 | .3 | 18 | 7 | 607 | 6.66 | 3 | 5 | ND | 3 | 12 | 1 | 2 | 3 | 91 | .14 | .110 | 18 | 45 | .35 | 185 | .41 | 2 | 2.53 | .01 | .08 | 2 | 2 |
| L2N 5+00W | 3 | 32 | 14 | 105 | .1 | 26 | 8 | 568 | 4.23 | 2 | 5 | ND | 3 | 20 | 1 | 2 | 2 | 75 | .20 | .047 | 16 | 41 | .58 | 283 | .20 | 2 | 2.49 | .01 | .12 | 2 | 4 |
| L2N 4+50W | 2 | 40 | 15 | 119 | .1 | 32 | 10 | 700 | 4.17 | 2 | 5 | ND | 1 | 17 | 1 | 2 | 2 | 74 | .23 | .044 | 13 | 44 | .71 | 252 | .15 | 3 | 2.18 | .01 | .14 | 1 | 3 |
| L2N 4+00W | 1 | 51 | 12 | 158 | .2 | 51 | 13 | 892 | 4.29 | 5 | 5 | ND | 2 | 23 | 2 | 2 | 2 | 65 | .41 | .076 | 16 | 54 | 1.00 | 375 | .15 | 3 | 2.62 | .01 | .14 | 1 | 1 |
| L2N 3+50W | 2 | 23 | 17 | 104 | .1 | 26 | 10 | 973 | 5.64 | 7 | 5 | ND | 4 | 12 | 1 | 2 | 2 | 78 | .22 | .103 | 16 | 43 | .49 | 194 | .35 | 2 | 2.29 | .01 | .08 | 1 | 1 |
| L2N 3+00W | 8 | 58 | 20 | 294 | .2 | 36 | 27 | 11450 | 3.30 | 2 | 5 | ND | 1 | 32 | 4 | 2 | 2 | 46 | .56 | .240 | 11 | 38 | .27 | 1428 | .01 | 2 | 1.46 | .01 | .15 | 1 | 1 |
| L2N 2+50W | 2 | 34 | 16 | 127 | .1 | 27 | 16 | 1091 | 4.42 | 5 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 70 | .32 | .088 | 13 | 42 | .57 | 825 | .11 | 2 | 1.61 | .01 | .15 | 1 | 1 |
| L2N 1+00W | 2 | 30 | 25 | 151 | .1 | 20 | 9 | 605 | 6.41 | 5 | 5 | ND | 4 | 5 | 1 | 3 | 2 | 101 | .05 | .135 | 23 | 41 | .33 | 1022 | .43 | 2 | 1.95 | .01 | .08 | 1 | 1 |
| L2N 0+50W | 1 | 41 | 13 | 89 | .1 | 25 | 7 | 258 | 4.21 | 4 | 5 | ND | 2 | 7 | 1 | 3 | 2 | 47 | .10 | .048 | 16 | 34 | .39 | 1896 | .08 | 2 | 1.72 | .01 | .11 | 1 | 1 |
| L2N 0+50E | 1 | 27 | 16 | 281 | .8 | 29 | 14 | 1184 | 5.56 | 2 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 79 | .40 | .083 | 17 | 49 | .47 | 655 | .26 | 2 | 2.61 | .01 | .11 | 1 | 1 |
| L2N 1+00E | 2 | 46 | 12 | 315 | .3 | 25 | 18 | 2015 | 5.51 | 2 | 5 | ND | 2 | 29 | 4 | 3 | 2 | 87 | 1.21 | .088 | 15 | 51 | .41 | 382 | .28 | 2 | 1.98 | .01 | .09 | 1 | 1 |
| L2N 1+50E | 1 | 99 | 11 | 196 | .1 | 42 | 13 | 762 | 4.50 | 4 | 5 | ND | 1 | 55 | 1 | 3 | 2 | 94 | 1.78 | .155 | 22 | 64 | .80 | 479 | .13 | 2 | 3.36 | .01 | .07 | 1 | 2 |
| L2N 2+00E | 1 | 98 | 2 | 110 | .3 | 12 | 4 | 551 | .52 | 2 | 5 | ND | 1 | 114 | 3 | 3 | 2 | 47 | 6.52 | .129 | 3 | 13 | .26 | 207 | .01 | 14 | .58 | .01 | .04 | 1 | 1 |
| L2N 2+50E | 1 | 24 | 23 | 113 | .3 | 17 | 9 | 641 | 3.55 | 4 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 108 | .84 | .070 | 10 | 42 | .49 | 177 | .35 | 3 | 1.34 | .01 | .09 | 1 | 1 |
| L2N 3+00E | 2 | 29 | 20 | 144 | .4 | 18 | 11 | 772 | 6.94 | 4 | 5 | ND | 2 | 19 | 1 | 3 | 2 | 149 | .75 | .082 | 12 | 54 | .37 | 161 | .53 | 2 | 1.44 | .01 | .08 | 1 | 1 |
| L2N 3+50E | 1 | 48 | 14 | 134 | .2 | 39 | 25 | 1177 | 6.31 | 2 | 5 | ND | 2 | 17 | 1 | 2 | 2 | 155 | 2.28 | .083 | 5 | 59 | 1.28 | 100 | .35 | 8 | 2.74 | .01 | .15 | 1 | 1 |
| L2N 4+50E | 1 | 32 | 19 | 144 | .2 | 15 | 11 | 1323 | 5.50 | 2 | 5 | ND | 1 | 17 | 1 | 2 | 3 | 103 | .65 | .100 | 12 | 44 | .26 | 162 | .16 | 3 | 1.49 | .01 | .10 | 1 | 1 |
| L2N 5+00E | 3 | 17 | 18 | 152 | .3 | 20 | 11 | 1889 | 4.77 | 3 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 76 | .88 | .218 | 13 | 47 | .31 | 418 | .07 | 2 | 2.00 | .01 | .07 | 1 | 1 |
| L0 5+00W | 3 | 30 | 21 | 90 | .5 | 18 | 6 | 568 | 5.41 | 4 | 5 | ND | 2 | 10 | 1 | 2 | 2 | 82 | .15 | .080 | 17 | 38 | .27 | 378 | .28 | 2 | 2.06 | .01 | .07 | 1 | 1 |
| L0 4+50W | 3 | 17 | 19 | 95 | .2 | 11 | 5 | 308 | 4.60 | 4 | 5 | ND | 3 | 8 | 1 | 2 | 2 | 93 | .07 | .101 | 21 | 38 | .19 | 187 | .54 | 2 | 1.68 | .01 | .06 | 1 | 1 |
| L0 4+00W | 3 | 29 | 17 | 96 | .3 | 16 | 6 | 360 | 4.22 | 2 | 5 | ND | 1 | 14 | 1 | 2 | 2 | 84 | .13 | .076 | 20 | 40 | .20 | 736 | .32 | 2 | 1.38 | .01 | .06 | 1 | 1 |
| L0 3+50W | 3 | 28 | 17 | 91 | .5 | 15 | 6 | 379 | 4.24 | 2 | 5 | ND | 2 | 10 | 3 | 2 | 2 | 88 | .11 | .051 | 18 | 40 | .27 | 393 | .35 | 3 | 1.57 | .01 | .08 | 1 | 1 |
| L0 3+00W | 2 | 37 | 18 | 118 | .3 | 20 | 7 | 419 | 4.60 | 3 | 5 | ND | 2 | 19 | 1 | 2 | 2 | 85 | .24 | .081 | 24 | 48 | .32 | 658 | .38 | 2 | 2.20 | .01 | .07 | 1 | 1 |
| L0 2+50W | 2 | 36 | 15 | 187 | .2 | 24 | 10 | 1142 | 5.10 | 4 | 5 | ND | 1 | 17 | 1 | 2 | 2 | 81 | .25 | .106 | 23 | 51 | .38 | 567 | .25 | 2 | 2.08 | .01 | .09 | 1 | 1 |
| L0 2+00W | 1 | 25 | 11 | 155 | .1 | 27 | 14 | 920 | 6.26 | 2 | 5 | ND | 1 | 8 | 1 | 2 | 2 | 73 | .15 | .081 | 18 | 47 | .46 | 191 | .29 | 2 | 3.65 | .02 | .07 | 1 | 1 |
| L0 1+50W | 4 | 61 | 18 | 115 | .2 | 49 | 18 | 1366 | 4.09 | 7 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 50 | .36 | .098 | 16 | 62 | .91 | 1328 | .06 | 2 | 1.85 | .01 | .14 | 1 | 1 |
| L0 1+00W | 2 | 66 | 14 | 669 | .1 | 30 | 14 | 1989 | 3.62 | 3 | 5 | ND | 1 | 59 | 5 | 3 | 2 | 47 | 3.12 | .159 | 10 | 36 | .47 | 488 | .09 | 5 | 1.70 | .01 | .09 | 1 | 1 |
| L0 0+50W | 2 | 20 | 16 | 176 | .4 | 21 | 10 | 761 | 7.23 | 3 | 5 | ND | 3 | 24 | 1 | 2 | 2 | 89 | .61 | .074 | 17 | 46 | .32 | 300 | .42 | 2 | 2.43 | .01 | .07 | 1 | 1 |
| L0 0+50E | 1 | 32 | 12 | 196 | .1 | 24 | 16 | 2001 | 4.77 | 2 | 5 | ND | 1 | 46 | 1 | 3 | 2 | 70 | 1.78 | .108 | 12 | 42 | .44 | 439 | .23 | 2 | 1.59 | .01 | .09 | 1 | 1 |
| L0 1+00E | 1 | 96 | 7 | 92 | .1 | 50 | 19 | 1101 | 4.29 | 2 | 5 | ND | 1 | 35 | 1 | 2 | 2 | 81 | 1.85 | .042 | 13 | 64 | 1.16 | 231 | .21 | 2 | 2.41 | .01 | .08 | 1 | 3 |
| L0 1+50E | 2 | 39 | 20 | 221 | .1 | 29 | 20 | 2889 | 6.03 | 8 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 78 | .74 | .112 | 17 | 48 | .50 | 740 | .28 | 2 | 2.22 | .01 | .10 | 1 | 1 |
| L0 2+00E | 1 | 33 | 18 | 174 | .1 | 41 | 16 | 3489 | 6.21 | 2 | 5 | ND | 3 | 22 | 3 | 2 | 2 | 80 | .97 | .098 | 26 | 52 | .64 | 281 | .29 | 4 | 3.83 | .02 | .08 | 1 | 2 |
| STD C/AU-S | 18 | 57 | 43 | 132 | 6.6 | 67 | 29 | 1032 | 3.84 | 38 | 22 | 8 | 37 | 46 | 19 | 16 | 25 | 57 | .47 | .090 | 37 | 57 | .89 | 175 | .06 | 33 | 1.90 | .06 | .15 | 11 | 50 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L0 2+50E | 1 | 113 | 18 | 179 | .1 | 28 | 16 | 3154 | 4.60 | 7 | 8 | ND | 1 | 26 | 1 | 2 | 2 | 75 | .88 | .148 | 56 | 36 | .37 | 166 | .10 | 2 | 3.11 | .01 | .06 | 1 | 1 |
| L0 3+00E | 1 | 51 | 24 | 167 | .3 | 38 | 14 | 2057 | 5.76 | 6 | 6 | ND | 1 | 13 | 3 | 3 | 2 | 79 | .41 | .085 | 19 | 48 | .65 | 168 | .22 | 2 | 3.09 | .01 | .09 | 1 | 5 |
| L0 3+50E | 1 | 105 | 26 | 165 | .1 | 35 | 14 | 1394 | 5.40 | 12 | 6 | ND | 1 | 17 | 1 | 4 | 2 | 106 | .54 | .112 | 24 | 46 | .52 | 141 | .16 | 2 | 3.91 | .01 | .06 | 1 | 2 |
| L0 4+00E | 1 | 61 | 16 | 117 | .2 | 33 | 14 | 861 | 5.62 | 4 | 8 | ND | 1 | 17 | 2 | 4 | 2 | 130 | 1.01 | .070 | 9 | 54 | .99 | 128 | .28 | 5 | 2.77 | .01 | .07 | 1 | 1 |
| L0 4+50E | 1 | 73 | 13 | 104 | .1 | 27 | 20 | 3004 | 4.78 | 5 | 5 | ND | 1 | 58 | 2 | 2 | 2 | 96 | 2.20 | .209 | 8 | 33 | .65 | 201 | .07 | 8 | 2.36 | .01 | .07 | 1 | 1 |
| L0 5+00E | 1 | 82 | 19 | 96 | .2 | 35 | 28 | 1914 | 4.95 | 3 | 5 | ND | 1 | 23 | 1 | 2 | 3 | 121 | 1.46 | .085 | 6 | 37 | 1.10 | 186 | .21 | 4 | 2.06 | .01 | .06 | 1 | 1 |
| BL 20+00N | 3 | 30 | 16 | 97 | .3 | 29 | 13 | 1048 | 4.06 | 7 | 5 | ND | 3 | 16 | 2 | 3 | 2 | 58 | .16 | .062 | 13 | 38 | .59 | 172 | .15 | 7 | 2.00 | .01 | .08 | 1 | 1 |
| BL 19+50N | 2 | 30 | 21 | 109 | .1 | 35 | 11 | 712 | 4.36 | 8 | 5 | ND | 2 | 15 | 1 | 2 | 2 | 61 | .19 | .099 | 14 | 42 | .63 | 205 | .16 | 2 | 2.55 | .01 | .07 | 1 | 2 |
| BL 19+00N | 3 | 36 | 15 | 98 | .3 | 37 | 11 | 571 | 4.01 | 8 | 7 | ND | 1 | 29 | 1 | 2 | 2 | 61 | .55 | .051 | 14 | 46 | .71 | 399 | .09 | 3 | 2.20 | .01 | .08 | 1 | 1 |
| BL 18+50N | 2 | 32 | 20 | 67 | .1 | 23 | 8 | 443 | 7.20 | 7 | 5 | ND | 2 | 12 | 2 | 4 | 5 | 102 | .20 | .073 | 12 | 50 | .53 | 206 | .20 | 2 | 2.61 | .01 | .06 | 2 | 1 |
| BL 18+00N | 2 | 32 | 15 | 101 | .1 | 29 | 11 | 762 | 5.16 | 6 | 5 | ND | 1 | 13 | 2 | 2 | 3 | 68 | .19 | .086 | 15 | 45 | .56 | 161 | .15 | 2 | 2.33 | .01 | .07 | 1 | 1 |
| BL 17+50N | 2 | 19 | 30 | 97 | .4 | 14 | 7 | 622 | 5.76 | 8 | 6 | ND | 3 | 20 | 2 | 2 | 2 | 102 | .24 | .098 | 20 | 36 | .24 | 1210 | .39 | 2 | 1.35 | .01 | .10 | 1 | 1 |
| BL 17+00N | 3 | 31 | 21 | 74 | .1 | 23 | 11 | 1085 | 4.17 | 4 | 5 | ND | 1 | 20 | 3 | 2 | 2 | 56 | .32 | .075 | 19 | 33 | .55 | 444 | .15 | 4 | 1.70 | .01 | .10 | 1 | 2 |
| BL 16+50N | 3 | 76 | 27 | 217 | .5 | 54 | 11 | 851 | 5.04 | 7 | 5 | ND | 1 | 56 | 2 | 2 | 2 | 68 | .59 | .190 | 24 | 54 | .61 | 1737 | .06 | 2 | 3.52 | .01 | .13 | 1 | 1 |
| BL 16+00N | 1 | 29 | 28 | 101 | .1 | 22 | 11 | 1431 | 3.77 | 4 | 5 | ND | 1 | 18 | 2 | 2 | 2 | 63 | .25 | .102 | 20 | 33 | .39 | 728 | .09 | 6 | 1.47 | .01 | .11 | 1 | 1 |
| BL 15+50N | 2 | 30 | 26 | 131 | .3 | 19 | 8 | 990 | 5.67 | 4 | 8 | ND | 1 | 9 | 5 | 2 | 1 | 77 | .09 | .116 | 19 | 36 | .19 | 300 | .21 | 3 | 2.59 | .01 | .05 | 2 | 1 |
| BL 15+00N | 2 | 24 | 22 | 107 | .2 | 25 | 8 | 476 | 5.59 | 9 | 5 | ND | 3 | 10 | 2 | 2 | 3 | 71 | .10 | .080 | 17 | 43 | .44 | 204 | .27 | 2 | 2.65 | .01 | .08 | 3 | 2 |
| BL 14+50N | 2 | 29 | 19 | 75 | .1 | 30 | 9 | 459 | 3.34 | 7 | 9 | ND | 3 | 13 | 1 | 2 | 3 | 46 | .11 | .041 | 18 | 35 | .52 | 194 | .09 | 3 | 1.93 | .01 | .08 | 2 | 1 |
| BL 14+00N | 2 | 41 | 27 | 110 | .6 | 24 | 30 | 5138 | 9.34 | 6 | 5 | ND | 2 | 8 | 3 | 2 | 4 | 123 | .15 | .076 | 17 | 69 | .41 | 334 | .41 | 2 | 2.35 | .01 | .06 | 1 | 1 |
| BL 13+50N | 2 | 47 | 20 | 92 | .3 | 37 | 13 | 656 | 4.39 | 7 | 5 | ND | 1 | 15 | 2 | 2 | 2 | 68 | .24 | .052 | 17 | 51 | .76 | 584 | .16 | 6 | 2.24 | .01 | .09 | 1 | 1 |
| BL 13+00N | 1 | 38 | 22 | 128 | .5 | 20 | 9 | 731 | 6.05 | 6 | 5 | ND | 2 | 7 | 4 | 2 | 2 | 87 | .12 | .089 | 17 | 44 | .35 | 243 | .38 | 3 | 1.93 | .01 | .06 | 1 | 1 |
| BL 12+50N | 2 | 26 | 17 | 80 | .5 | 18 | 6 | 358 | 3.62 | 5 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 66 | .21 | .087 | 13 | 38 | .29 | 298 | .09 | 5 | 1.55 | .01 | .06 | 1 | 2 |
| BL 12+00N | 2 | 34 | 26 | 133 | .3 | 36 | 14 | 886 | 6.46 | 7 | 7 | ND | 1 | 50 | 2 | 2 | 2 | 104 | 1.00 | .081 | 13 | 83 | .88 | 568 | .36 | 3 | 1.83 | .01 | .08 | 1 | 1 |
| BL 11+50N | 1 | 93 | 31 | 118 | .1 | 72 | 23 | 1294 | 5.94 | 9 | 5 | ND | 1 | 47 | 1 | 9 | 2 | 81 | 1.11 | .125 | 25 | 86 | 1.51 | 1140 | .22 | 6 | 3.79 | .01 | .10 | 1 | 3 |
| BL 11+00N | 2 | 66 | 23 | 118 | .3 | 54 | 17 | 988 | 5.68 | 8 | 5 | ND | 1 | 49 | 2 | 3 | 3 | 84 | .91 | .124 | 21 | 80 | 1.17 | 680 | .19 | 8 | 3.14 | .01 | .11 | 1 | 1 |
| BL 10+50N | 4 | 61 | 23 | 89 | .3 | 30 | 26 | 2572 | 5.43 | 7 | 5 | ND | 1 | 56 | 1 | 2 | 2 | 76 | .80 | .229 | 18 | 56 | .47 | 490 | .07 | 2 | 2.65 | .01 | .07 | 1 | 2 |
| BL 10+00N | 2 | 84 | 25 | 109 | .1 | 75 | 22 | 968 | 5.48 | 7 | 5 | ND | 1 | 42 | 2 | 2 | 2 | 89 | 1.34 | .094 | 16 | 89 | 2.09 | 731 | .28 | 5 | 3.15 | .01 | .13 | 1 | 1 |
| BL 9+50N | 3 | 69 | 17 | 90 | .2 | 48 | 13 | 864 | 3.40 | 8 | 8 | ND | 1 | 178 | 1 | 2 | 2 | 48 | 2.17 | .130 | 25 | 56 | .84 | 906 | .07 | 6 | 2.29 | .01 | .09 | 1 | 4 |
| BL 9+00N | 2 | 66 | 21 | 146 | .1 | 42 | 13 | 686 | 5.04 | 8 | 8 | ND | 1 | 37 | 1 | 2 | 2 | 81 | .46 | .112 | 25 | 75 | .67 | 1022 | .21 | 2 | 2.52 | .01 | .10 | 1 | 1 |
| BL 8+50N | 3 | 38 | 17 | 109 | .4 | 41 | 11 | 683 | 4.44 | 7 | 5 | ND | 1 | 31 | 2 | 4 | 2 | 84 | .56 | .087 | 16 | 71 | .88 | 577 | .22 | 6 | 2.00 | .01 | .13 | 1 | 1 |
| BL 8+00N | 2 | 35 | 23 | 117 | .1 | 27 | 9 | 804 | 5.22 | 2 | 8 | ND | 1 | 19 | 1 | 2 | 2 | 91 | .36 | .072 | 18 | 59 | .46 | 352 | .32 | 2 | 2.19 | .01 | .09 | 1 | 4 |
| BL 7+50N | 1 | 43 | 25 | 119 | .2 | 43 | 14 | 1105 | 5.54 | 6 | 7 | ND | 1 | 33 | 1 | 2 | 2 | 79 | .59 | .098 | 20 | 65 | .87 | 554 | .21 | 3 | 2.75 | .01 | .09 | 1 | 1 |
| BL 7+00N | 1 | 45 | 13 | 125 | .1 | 43 | 14 | 1041 | 4.68 | 6 | 8 | ND | 1 | 26 | 1 | 2 | 2 | 69 | .77 | .111 | 19 | 65 | .90 | 354 | .17 | 5 | 2.67 | .01 | .09 | 1 | 3 |
| BL 6+50N | 1 | 32 | 20 | 125 | .1 | 45 | 15 | 1020 | 5.25 | 10 | 5 | ND | 2 | 62 | 2 | 4 | 3 | 65 | 1.25 | .114 | 19 | 57 | .95 | 409 | .28 | 4 | 2.71 | .01 | .09 | 1 | 1 |
| BL 6+00N | 1 | 31 | 15 | 109 | .3 | 31 | 9 | 676 | 4.56 | 6 | 5 | ND | 1 | 12 | 3 | 2 | 2 | 75 | .22 | .082 | 15 | 61 | .59 | 199 | .18 | 5 | 2.18 | .01 | .08 | 2 | 1 |
| BL 5+50N | 4 | 68 | 24 | 141 | .1 | 61 | 18 | 1021 | 5.06 | 9 | 5 | ND | 1 | 27 | 2 | 2 | 2 | 75 | .74 | .058 | 28 | 78 | 1.08 | 692 | .14 | 5 | 2.73 | .01 | .14 | 1 | 2 |
| STD C/AU-S | 18 | 58 | 40 | 132 | 7.1 | 68 | 27 | 1024 | 3.82 | 40 | 20 | 7 | 35 | 44 | 17 | 16 | 22 | 55 | .47 | .091 | 37 | 56 | .87 | 176 | .06 | 32 | 1.84 | .06 | .14 | 12 | 47 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| BL 5+00N | 5 | 44 | 9 | 97 | .1 | 31 | 14 | 2487 | 3.84 | 2 | 5 | ND | 1 | 52 | 1 | 2 | 3 | 60 | 1.29 | .219 | 18 | 54 | .40 | 1359 | .09 | 3 | 2.80 | .01 | .06 | 1 | 1 |
| BL 4+50N | 1 | 41 | 6 | 113 | .1 | 48 | 14 | 716 | 6.40 | 2 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 116 | .37 | .068 | 9 | 93 | 1.15 | 162 | .37 | 3 | 3.05 | .01 | .11 | 1 | 2 |
| BL 4+00N | 1 | 39 | 14 | 105 | .1 | 43 | 13 | 821 | 6.06 | 2 | 5 | ND | 3 | 14 | 1 | 2 | 2 | 84 | .30 | .082 | 17 | 65 | .87 | 219 | .37 | 3 | 3.69 | .01 | .09 | 1 | 2 |
| BL 3+50N | 1 | 30 | 13 | 143 | .1 | 38 | 13 | 865 | 5.67 | 2 | 5 | ND | 3 | 13 | 1 | 2 | 2 | 83 | .24 | .079 | 14 | 58 | .64 | 236 | .27 | 2 | 2.96 | .01 | .09 | 1 | 1 |
| BL 3+00N | 1 | 34 | 2 | 130 | .1 | 46 | 14 | 552 | 5.50 | 2 | 5 | ND | 3 | 15 | 1 | 2 | 2 | 85 | .26 | .056 | 12 | 69 | .84 | 376 | .25 | 3 | 3.29 | .01 | .13 | 1 | 1 |
| BL 2+50N | 1 | 37 | 26 | 51 | .1 | 12 | 3 | 123 | 3.18 | 2 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 16 | .03 | .066 | 23 | 17 | .35 | 325 | .01 | 2 | 1.20 | .01 | .12 | 2 | 3 |
| BL 2+00N | 1 | 104 | 10 | 145 | .1 | 62 | 39 | 1484 | 8.94 | 2 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 205 | .77 | .039 | 5 | 105 | 3.84 | 408 | .46 | 2 | 3.95 | .01 | .05 | 1 | 2 |
| BL 1+50N | 1 | 86 | 8 | 122 | .3 | 51 | 17 | 1031 | 5.53 | 2 | 5 | ND | 3 | 54 | 2 | 3 | 4 | 63 | 1.54 | .094 | 33 | 68 | .98 | 692 | .29 | 3 | 3.26 | .04 | .10 | 1 | 2 |
| BL 1+00N | 1 | 78 | 15 | 198 | .1 | 44 | 16 | 949 | 4.55 | 4 | 5 | ND | 2 | 37 | 2 | 2 | 2 | 80 | 2.17 | .104 | 16 | 66 | .86 | 655 | .13 | 4 | 2.72 | .01 | .08 | 1 | 1 |
| BL 0+50N | 1 | 84 | 17 | 233 | .1 | 31 | 15 | 1672 | 4.32 | 2 | 5 | ND | 1 | 46 | 1 | 2 | 2 | 66 | 2.22 | .151 | 20 | 51 | .53 | 630 | .11 | 2 | 2.27 | .01 | .07 | 1 | 2 |
| BL 0+00N | 1 | 48 | 14 | 78 | .1 | 45 | 15 | 1042 | 3.62 | 2 | 5 | ND | 2 | 28 | 1 | 2 | 2 | 57 | .74 | .047 | 19 | 49 | .91 | 286 | .14 | 2 | 2.00 | .01 | .09 | 1 | 2 |
| L10W 19+50N | 5 | 80 | 15 | 120 | .1 | 37 | 15 | 989 | 3.49 | 2 | 5 | ND | 1 | 39 | 1 | 2 | 3 | 45 | .28 | .072 | 21 | 31 | .56 | 910 | .08 | 2 | 2.21 | .01 | .12 | 1 | 1 |
| L10W 19+00N | 3 | 62 | 13 | 102 | .2 | 31 | 7 | 381 | 2.44 | 2 | 5 | ND | 1 | 46 | 1 | 2 | 3 | 29 | .41 | .081 | 15 | 22 | .47 | 823 | .05 | 2 | 1.50 | .01 | .11 | 1 | 1 |
| L10W 18+50N | 7 | 122 | 14 | 172 | .4 | 57 | 12 | 1263 | 3.42 | 5 | 5 | ND | 1 | 87 | 1 | 3 | 3 | 40 | .80 | .141 | 26 | 35 | .56 | 949 | .04 | 2 | 2.42 | .01 | .12 | 1 | 4 |
| L10W 15+50N | 2 | 23 | 18 | 163 | .4 | 25 | 11 | 684 | 5.73 | 2 | 5 | ND | 3 | 45 | 1 | 2 | 2 | 80 | .26 | .096 | 16 | 42 | .35 | 345 | .33 | 3 | 2.54 | .01 | .11 | 1 | 1 |
| L10W 15+00N | 2 | 35 | 14 | 96 | .1 | 37 | 11 | 642 | 4.16 | 5 | 5 | ND | 1 | 74 | 1 | 2 | 2 | 66 | .29 | .062 | 13 | 48 | .71 | 276 | .12 | 2 | 2.12 | .01 | .11 | 2 | 1 |
| L10W 14+50N | 3 | 54 | 7 | 124 | .1 | 47 | 10 | 668 | 3.23 | 2 | 5 | ND | 1 | 145 | 1 | 2 | 2 | 49 | 1.21 | .095 | 19 | 47 | .66 | 1648 | .05 | 2 | 2.91 | .01 | .11 | 1 | 4 |
| L10W 9+00N | 3 | 29 | 17 | 125 | .1 | 30 | 13 | 1263 | 4.60 | 3 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 67 | .30 | .116 | 16 | 43 | .52 | 528 | .17 | 2 | 2.37 | .01 | .14 | 1 | 2 |
| L10W 8+50N | 2 | 32 | 14 | 99 | .3 | 35 | 10 | 539 | 3.85 | 4 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 63 | .36 | .047 | 15 | 45 | .72 | 353 | .11 | 2 | 2.00 | .01 | .13 | 1 | 2 |
| L10W 8+00N | 1 | 41 | 9 | 119 | .1 | 39 | 13 | 731 | 3.92 | 3 | 5 | ND | 2 | 19 | 1 | 2 | 2 | 59 | .34 | .055 | 14 | 43 | .79 | 328 | .13 | 3 | 2.15 | .01 | .15 | 1 | 9 |
| L10W 7+50N | 2 | 39 | 13 | 113 | .3 | 29 | 9 | 682 | 3.77 | 2 | 5 | ND | 1 | 39 | 1 | 2 | 2 | 60 | .47 | .076 | 11 | 37 | .58 | 459 | .06 | 2 | 1.84 | .01 | .16 | 1 | 1 |
| L10W 3+50N | 4 | 33 | 22 | 143 | .2 | 23 | 8 | 486 | 7.17 | 6 | 5 | ND | 2 | 16 | 1 | 2 | 2 | 86 | .14 | .074 | 17 | 43 | .37 | 180 | .27 | 2 | 2.27 | .01 | .08 | 1 | 2 |
| L10W 3+00N | 3 | 45 | 18 | 151 | .3 | 27 | 12 | 598 | 5.62 | 7 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 57 | .14 | .082 | 17 | 39 | .59 | 133 | .13 | 2 | 2.87 | .01 | .10 | 2 | 1 |
| L10W 2+50N | 5 | 63 | 26 | 62 | .1 | 15 | 4 | 211 | 3.50 | 6 | 5 | ND | 3 | 41 | 1 | 3 | 2 | 21 | .05 | .075 | 24 | 17 | .52 | 120 | .01 | 2 | 1.41 | .01 | .17 | 1 | 2 |
| L3E 11+50N | 1 | 41 | 10 | 120 | .1 | 32 | 17 | 1025 | 6.87 | 2 | 5 | ND | 2 | 10 | 1 | 2 | 2 | 78 | .31 | .076 | 17 | 52 | .68 | 86 | .30 | 2 | 3.98 | .01 | .05 | 1 | 2 |
| L3E 11+00N | 1 | 87 | 6 | 89 | .1 | 55 | 15 | 620 | 4.42 | 4 | 5 | ND | 2 | 23 | 1 | 2 | 3 | 83 | .72 | .064 | 11 | 60 | 1.20 | 165 | .19 | 2 | 2.46 | .01 | .06 | 1 | 3 |
| L3E 10+50N | 1 | 73 | 13 | 80 | .1 | 48 | 15 | 711 | 4.39 | 4 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 79 | .69 | .095 | 11 | 61 | .91 | 228 | .11 | 2 | 2.77 | .01 | .09 | 1 | 2 |
| L5E 19+50N | 1 | 23 | 6 | 12 | .2 | 8 | 3 | 35 | .58 | 2 | 5 | ND | 1 | 38 | 4 | 2 | 2 | 12 | 2.73 | .180 | 6 | 16 | .12 | 376 | .03 | 3 | .84 | .01 | .03 | 1 | 2 |
| L5E 19+00N | 2 | 23 | 16 | 99 | .1 | 35 | 9 | 1115 | 3.74 | 2 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 61 | .20 | .085 | 14 | 50 | .49 | 399 | .04 | 2 | 1.67 | .01 | .10 | 1 | 3 |
| L5E 18+50N | 2 | 18 | 13 | 123 | .1 | 26 | 11 | 991 | 5.54 | 2 | 5 | ND | 1 | 9 | 1 | 2 | 4 | 74 | .17 | .098 | 16 | 51 | .37 | 129 | .17 | 2 | 3.17 | .01 | .08 | 1 | 2 |
| L5E 15+50N | 2 | 20 | 16 | 189 | .1 | 20 | 14 | 2240 | 6.56 | 3 | 5 | ND | 2 | 19 | 1 | 3 | 3 | 90 | .69 | .115 | 15 | 52 | .32 | 498 | .22 | 2 | 1.58 | .01 | .10 | 1 | 1 |
| L5E 15+00N | 1 | 44 | 8 | 118 | .1 | 101 | 23 | 2038 | 5.22 | 2 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 53 | .49 | .193 | 29 | 79 | .77 | 205 | .04 | 3 | 2.83 | .01 | .26 | 1 | 1 |
| L5E 14+50N | 1 | 32 | 9 | 107 | .1 | 47 | 13 | 821 | 4.57 | 2 | 5 | ND | 1 | 12 | 2 | 2 | 2 | 70 | .19 | .084 | 13 | 56 | .64 | 222 | .06 | 2 | 2.53 | .01 | .13 | 1 | 3 |
| L5E 1+50N | 1 | 16 | 16 | 120 | .1 | 20 | 11 | 830 | 5.59 | 2 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 66 | 1.21 | .093 | 20 | 35 | .29 | 146 | .30 | 2 | 3.82 | .02 | .05 | 1 | 1 |
| L5E 1+00N | 1 | 53 | 12 | 105 | .1 | 44 | 22 | 1481 | 6.43 | 3 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 119 | 1.84 | .068 | 8 | 59 | 1.29 | 143 | .29 | 4 | 3.23 | .01 | .08 | 1 | 1 |
| L5E 0+50N | 1 | 52 | 8 | 90 | .2 | 39 | 16 | 860 | 6.31 | 2 | 5 | ND | 3 | 15 | 1 | 2 | 2 | 124 | .72 | .043 | 7 | 63 | 1.05 | 135 | .31 | 2 | 2.77 | .01 | .07 | 1 | 3 |
| STD C/AU-S | 18 | 57 | 41 | 132 | 7.2 | 67 | 29 | 1033 | 3.90 | 38 | 20 | 8 | 36 | 47 | 17 | 16 | 24 | 56 | .48 | .090 | 38 | 58 | .86 | 171 | .06 | 33 | 1.97 | .06 | .15 | 11 | 49 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L6E 5+50N | 1 | 19 | 12 | 139 | .1 | 36 | 11 | 1200 | 5.23 | 2 | 5 | ND | 1 | 12 | 1 | 2 | 2 | 69 | .27 | .154 | 21 | 55 | .54 | 201 | .08 | 2 | 3.27 | .01 | .07 | 1 | 1 |
| L6E 5+00N | 2 | 24 | 17 | 148 | .1 | 25 | 9 | 867 | 4.87 | 5 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 65 | 1.53 | .103 | 13 | 41 | .34 | 544 | .10 | 2 | 2.08 | .01 | .08 | 1 | 1 |
| L6E 4+50N | 4 | 19 | 13 | 142 | .1 | 20 | 11 | 1325 | 4.86 | 3 | 5 | ND | 1 | 21 | 2 | 3 | 5 | 67 | 1.39 | .146 | 12 | 37 | .31 | 578 | .10 | 3 | 1.85 | .01 | .09 | 1 | 1 |
| CW 0+00S | 1 | 23 | 10 | 67 | .1 | 12 | 5 | 414 | 1.47 | 2 | 5 | ND | 1 | 5 | 1 | 2 | 2 | 16 | .10 | .026 | 13 | 8 | .13 | 407 | .01 | 2 | .65 | .01 | .06 | 1 | 1 |
| CW 0+50S | 14 | 44 | 15 | 115 | .1 | 26 | 9 | 437 | 2.57 | 14 | 5 | ND | 1 | 44 | 1 | 2 | 2 | 13 | .05 | .093 | 22 | 5 | .11 | 366 | .01 | 2 | .56 | .01 | .11 | 1 | 1 |
| CW 1+00S | 3 | 49 | 16 | 130 | .1 | 31 | 13 | 1005 | 4.13 | 5 | 5 | ND | 1 | 18 | 1 | 3 | 2 | 50 | .16 | .072 | 15 | 34 | .54 | 447 | .04 | 3 | 1.83 | .01 | .12 | 1 | 2 |
| CW 1+50S | 2 | 60 | 16 | 149 | .1 | 39 | 22 | 1541 | 3.51 | 4 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 50 | .23 | .114 | 17 | 35 | .47 | 1195 | .03 | 2 | 2.06 | .01 | .19 | 1 | 1 |
| CW 2+00S | 3 | 62 | 16 | 125 | .1 | 46 | 17 | 1208 | 3.47 | 6 | 5 | ND | 1 | 25 | 1 | 2 | 2 | 42 | .39 | .048 | 14 | 39 | .70 | 458 | .06 | 4 | 1.78 | .01 | .15 | 1 | 1 |
| CW 2+50S | 2 | 54 | 10 | 141 | .2 | 36 | 15 | 1291 | 3.25 | 4 | 5 | ND | 1 | 25 | 2 | 2 | 2 | 43 | .54 | .085 | 12 | 35 | .66 | 674 | .03 | 4 | 1.62 | .01 | .21 | 1 | 1 |
| CW 3+00S | 2 | 82 | 18 | 115 | .1 | 50 | 16 | 2551 | 3.68 | 6 | 5 | ND | 1 | 32 | 1 | 2 | 2 | 43 | 1.05 | .095 | 24 | 37 | .81 | 804 | .06 | 5 | 2.16 | .01 | .10 | 1 | 1 |
| CW 3+50S | 4 | 45 | 15 | 262 | .4 | 31 | 15 | 1667 | 6.18 | 2 | 5 | ND | 1 | 21 | 2 | 2 | 5 | 82 | .56 | .094 | 12 | 52 | .51 | 772 | .14 | 2 | 2.36 | .01 | .09 | 1 | 2 |
| CW 4+00S | 2 | 34 | 14 | 105 | .1 | 39 | 14 | 938 | 3.89 | 3 | 5 | ND | 1 | 15 | 2 | 3 | 2 | 52 | .47 | .071 | 12 | 33 | .90 | 398 | .12 | 4 | 1.60 | .01 | .10 | 1 | 1 |
| RC 2 | 2 | 74 | 18 | 232 | .1 | 44 | 20 | 1700 | 5.42 | 4 | 5 | ND | 1 | 31 | 1 | 3 | 2 | 81 | .44 | .085 | 17 | 57 | .71 | 1937 | .07 | 2 | 3.61 | .01 | .12 | 1 | 1 |
| RC 6 | 5 | 56 | 15 | 115 | .1 | 13 | 4 | 150 | 2.65 | 4 | 5 | ND | 1 | 29 | 1 | 2 | 4 | 36 | .25 | .073 | 9 | 19 | .10 | 347 | .01 | 3 | .77 | .01 | .09 | 1 | 1 |
| RC 10 | 4 | 38 | 15 | 118 | .1 | 24 | 9 | 410 | 5.35 | 2 | 5 | ND | 1 | 11 | 1 | 3 | 2 | 54 | .18 | .049 | 11 | 35 | .63 | 391 | .09 | 2 | 1.75 | .01 | .12 | 1 | 1 |
| RC 14 | 1 | 36 | 13 | 143 | .1 | 45 | 14 | 782 | 4.87 | 4 | 5 | ND | 1 | 16 | 1 | 2 | 3 | 76 | .40 | .045 | 10 | 58 | 1.01 | 274 | .12 | 2 | 2.52 | .01 | .11 | 1 | 1 |
| STD C/AU-S | 18 | 57 | 38 | 132 | 7.1 | 68 | 28 | 1023 | 3.90 | 40 | 23 | 7 | 37 | 45 | 19 | 18 | 21 | 56 | .47 | .088 | 37 | 55 | .87 | 175 | .06 | 34 | 1.92 | .06 | .15 | 11 | 53 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L16N 9+00W | 4 | 50 | 11 | 136 | .1 | 51 | 18 | 1508 | 4.09 | 5 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 50 | .54 | .061 | 16 | 43 | 1.15 | 485 | .11 | 4 | 1.68 | .01 | .10 | 1 | 3 |
| L10N 7+00W | 2 | 67 | 14 | 170 | .1 | 50 | 12 | 857 | 3.15 | 4 | 5 | ND | 1 | 67 | 1 | 2 | 2 | 44 | 1.27 | .083 | 13 | 44 | .81 | 513 | .06 | 6 | 1.93 | .01 | .11 | 1 | 1 |
| L4N 3+95W | 4 | 31 | 8 | 215 | .1 | 38 | 19 | 6858 | 3.61 | 2 | 5 | ND | 1 | 36 | 1 | 2 | 4 | 42 | .88 | .065 | 10 | 32 | .87 | 648 | .06 | 4 | 1.51 | .01 | .08 | 1 | 1 |
| L4N 3+00W | 3 | 86 | 12 | 195 | .4 | 43 | 9 | 558 | 2.84 | 2 | 5 | ND | 1 | 69 | 2 | 2 | 2 | 37 | 1.97 | .132 | 21 | 39 | .59 | 472 | .06 | 5 | 2.15 | .01 | .06 | 1 | 1 |
| L2N BL | 2 | 43 | 4 | 106 | .1 | 35 | 16 | 734 | 3.77 | 2 | 5 | ND | 2 | 16 | 1 | 2 | 2 | 75 | .47 | .036 | 7 | 48 | 2.00 | 226 | .18 | 3 | 1.75 | .01 | .06 | 1 | 1 |
| L10W 14+70N | 3 | 34 | 3 | 100 | .1 | 37 | 13 | 1136 | 3.17 | 2 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 40 | .51 | .040 | 12 | 23 | .73 | 467 | .09 | 3 | 1.38 | .01 | .10 | 1 | 1 |
| CW 1 | 4 | 37 | 12 | 184 | .1 | 44 | 16 | 2786 | 3.06 | 4 | 5 | ND | 1 | 27 | 1 | 2 | 4 | 29 | .51 | .058 | 15 | 33 | .69 | 834 | .05 | 2 | 1.21 | .01 | .09 | 1 | 3 |
| RC 3 | 2 | 153 | 6 | 183 | .1 | 36 | 8 | 509 | 2.61 | 2 | 5 | ND | 1 | 63 | 1 | 2 | 2 | 38 | 2.05 | .133 | 13 | 51 | .70 | 434 | .04 | 9 | 1.39 | .01 | .11 | 1 | 1 |
| RC 4 | 1 | 62 | 14 | 143 | .2 | 45 | 20 | 920 | 5.17 | 2 | 5 | ND | 2 | 29 | 1 | 2 | 2 | 103 | 1.97 | .057 | 8 | 65 | 1.54 | 307 | .30 | 8 | 2.46 | .01 | .67 | 1 | 2 |
| RC 5 | 3 | 76 | 12 | 136 | .1 | 38 | 25 | 936 | 5.80 | 6 | 5 | ND | 2 | 16 | 1 | 2 | 2 | 134 | .74 | .037 | 7 | 62 | 3.05 | 271 | .30 | 5 | 2.76 | .01 | .05 | 2 | 1 |
| RC 8 | 2 | 51 | 6 | 116 | .1 | 37 | 21 | 848 | 5.11 | 2 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 107 | .56 | .035 | 7 | 72 | 2.73 | 346 | .24 | 5 | 2.35 | .01 | .06 | 1 | 1 |
| RC 9 | 1 | 50 | 11 | 113 | .1 | 56 | 17 | 884 | 3.98 | 2 | 5 | ND | 2 | 13 | 1 | 2 | 2 | 72 | .58 | .041 | 9 | 94 | 2.30 | 272 | .14 | 2 | 1.94 | .01 | .06 | 1 | 1 |
| RC 11 | 1 | 29 | 4 | 82 | .1 | 14 | 5 | 397 | 1.88 | 2 | 5 | ND | 1 | 13 | 1 | 2 | 2 | 16 | .42 | .032 | 9 | 16 | .50 | 228 | .02 | 5 | .75 | .01 | .08 | 1 | 1 |
| RC 12 | 1 | 42 | 11 | 125 | .1 | 19 | 8 | 584 | 2.29 | 2 | 5 | ND | 1 | 15 | 1 | 2 | 2 | 16 | .50 | .038 | 11 | 20 | .53 | 743 | .02 | 5 | .89 | .01 | .08 | 1 | 1 |
| RC 13 | 1 | 47 | 6 | 106 | .1 | 22 | 7 | 677 | 2.33 | 2 | 5 | ND | 1 | 23 | 1 | 2 | 2 | 19 | .87 | .041 | 12 | 27 | .62 | 383 | .03 | 5 | .97 | .01 | .08 | 1 | 2 |
| STD C/AU-S | 17 | 61 | 45 | 132 | 6.6 | 68 | 30 | 1012 | 4.10 | 41 | 18 | 8 | 38 | 47 | 19 | 19 | 18 | 61 | .47 | .096 | 39 | 58 | .92 | 179 | .07 | 35 | 1.97 | .06 | .14 | 11 | 50 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 6751 | 1 | 4 | 2 | 4 | .1 | 3 | 1 | 40 | .29 | 2 | 5 | ND | 1 | 1 | 1 | 2 | 2 | 2 | .02 | .005 | 2 | 7 | .05 | 25 | .01 | 4 | .08 | .01 | .03 | 5 | 1 |
| 6752 | 1 | 18 | 5 | 9 | .1 | 4 | 1 | 47 | .32 | 2 | 5 | ND | 1 | 3 | 1 | 2 | 5 | 3 | .01 | .004 | 2 | 4 | .04 | 701 | .01 | 2 | .10 | .01 | .03 | 1 | 2 |
| 6753 | 1 | 106 | 6 | 73 | .1 | 77 | 22 | 535 | 5.30 | 2 | 6 | ND | 1 | 25 | 3 | 7 | 3 | 71 | 2.43 | .024 | 2 | 59 | 2.20 | 168 | .27 | 15 | 3.49 | .02 | .05 | 1 | 1 |
| 6754 | 1 | 9 | 2 | 12 | .1 | 7 | 2 | 62 | .58 | 2 | 5 | ND | 1 | 3 | 1 | 2 | 2 | 5 | .06 | .015 | 2 | 4 | .12 | 218 | .01 | 4 | .21 | .01 | .02 | 1 | 1 |
| 6755 | 1 | 14 | 2 | 26 | .1 | 13 | 4 | 105 | .90 | 2 | 5 | ND | 1 | 2 | 1 | 2 | 2 | 3 | .02 | .003 | 9 | 8 | .17 | 785 | .01 | 2 | .40 | .01 | .08 | 4 | 2 |
| 6756 | 1 | 30 | 3 | 39 | .1 | 18 | 7 | 2800 | 1.06 | 2 | 5 | ND | 1 | 12 | 1 | 2 | 2 | 6 | .18 | .008 | 9 | 6 | .32 | 145 | .01 | 2 | .44 | .01 | .05 | 1 | 1 |
| 6757 | 1 | 25 | 3 | 30 | .1 | 17 | 7 | 1031 | .75 | 2 | 5 | ND | 1 | 13 | 2 | 2 | 2 | 3 | .10 | .033 | 4 | 11 | .17 | 338 | .01 | 4 | .31 | .01 | .06 | 8 | 1 |
| 6758 | 1 | 85 | 2 | 26 | .1 | 12 | 10 | 979 | 1.99 | 2 | 5 | ND | 1 | 228 | 3 | 2 | 2 | 33 | 28.02 | .026 | 2 | 15 | .55 | 53 | .04 | 2 | .58 | .01 | .05 | 1 | 1 |
| 6759 | 1 | 39 | 9 | 71 | .1 | 26 | 21 | 537 | 6.75 | 2 | 5 | ND | 1 | 43 | 5 | 2 | 2 | 121 | 2.48 | .064 | 2 | 15 | 1.29 | 31 | .41 | 10 | 2.08 | .03 | .14 | 1 | 1 |
| 6760 | 1 | 15 | 3 | 92 | .2 | 144 | 28 | 553 | 7.90 | 2 | 5 | ND | 2 | 39 | 5 | 4 | 2 | 51 | 2.20 | .380 | 29 | 128 | 2.31 | 33 | .17 | 7 | 1.83 | .01 | .28 | 1 | 2 |
| 6761 | 1 | 17 | 12 | 71 | .1 | 12 | 8 | 470 | 2.68 | 5 | 5 | ND | 3 | 96 | 1 | 2 | 2 | 53 | 1.15 | .061 | 12 | 29 | .96 | 210 | .19 | 5 | 1.41 | .02 | .24 | 1 | 1 |
| 6762 | 1 | 85 | 15 | 97 | .1 | 24 | 12 | 440 | 3.46 | 10 | 5 | ND | 6 | 66 | 1 | 2 | 2 | 52 | 1.08 | .078 | 15 | 29 | 1.04 | 184 | .23 | 8 | 1.98 | .01 | .29 | 1 | 4 |
| 6763 | 1 | 67 | 7 | 76 | .2 | 34 | 23 | 514 | 6.02 | 3 | 5 | ND | 1 | 75 | 8 | 2 | 2 | 126 | 6.38 | .043 | 2 | 30 | 2.10 | 34 | .34 | 11 | 3.59 | .02 | .05 | 1 | 1 |
| 6764 | 1 | 22 | 6 | 23 | .1 | 11 | 5 | 243 | .73 | 3 | 5 | ND | 2 | 3 | 1 | 2 | 2 | 4 | .08 | .006 | 5 | 5 | .15 | 101 | .01 | 2 | .27 | .01 | .06 | 1 | 1 |
| 6765 | 1 | 55 | 7 | 61 | .1 | 42 | 25 | 585 | 6.49 | 4 | 8 | ND | 1 | 17 | 6 | 4 | 2 | 130 | 5.14 | .041 | 2 | 64 | 1.42 | 18 | .24 | 18 | 3.75 | .01 | .02 | 3 | 1 |
| 6766 | 1 | 113 | 9 | 31 | .2 | 28 | 23 | 866 | 7.00 | 2 | 5 | ND | 1 | 20 | 4 | 3 | 2 | 131 | 2.76 | .052 | 2 | 28 | 3.63 | 34 | .43 | 8 | 3.92 | .02 | .02 | 1 | 1 |
| 6767 | 1 | 110 | 10 | 66 | .1 | 59 | 20 | 804 | 5.16 | 3 | 5 | ND | 1 | 16 | 4 | 3 | 2 | 76 | 2.44 | .025 | 3 | 45 | 2.50 | 67 | .27 | 11 | 3.41 | .01 | .03 | 1 | 1 |
| 6768 | 1 | 43 | 8 | 62 | .3 | 30 | 18 | 634 | 6.30 | 7 | 5 | ND | 1 | 294 | 7 | 2 | 2 | 129 | 10.39 | .038 | 2 | 26 | 1.32 | 16 | .31 | 13 | 2.74 | .01 | .02 | 1 | 3 |
| 6769 | 1 | 12 | 6 | 23 | .1 | 13 | 8 | 360 | 2.03 | 2 | 5 | ND | 1 | 1007 | 1 | 2 | 2 | 86 | 18.79 | .010 | 2 | 26 | .65 | 5 | .14 | 3 | 1.37 | .01 | .02 | 2 | 1 |
| 6770 | 1 | 47 | 12 | 91 | .2 | 37 | 28 | 705 | 7.37 | 4 | 5 | ND | 1 | 28 | 6 | 8 | 2 | 168 | 3.97 | .057 | 2 | 28 | 2.08 | 17 | .35 | 21 | 3.90 | .02 | .05 | 1 | 1 |
| 6771 | 4 | 16 | 18 | 29 | .1 | 5 | 2 | 96 | 1.53 | 11 | 5 | ND | 7 | 14 | 1 | 2 | 2 | 13 | .32 | .085 | 5 | 11 | .39 | 216 | .07 | 5 | .65 | .01 | .18 | 1 | 3 |
| 6772 | 1 | 8 | 4 | 14 | .1 | 5 | 3 | 83 | .56 | 2 | 5 | ND | 1 | 6 | 1 | 2 | 4 | 6 | .13 | .008 | 2 | 4 | .12 | 1558 | .01 | 5 | .23 | .01 | .03 | 1 | 1 |
| 6773 | 1 | 5 | 2 | 6 | .1 | 3 | 1 | 53 | .38 | 2 | 5 | ND | 1 | 3 | 1 | 2 | 2 | 3 | .06 | .004 | 3 | 7 | .07 | 135 | .01 | 8 | .13 | .01 | .03 | 5 | 1 |
| 6774 | 1 | 4 | 2 | 8 | .1 | 3 | 1 | 35 | .39 | 2 | 5 | ND | 1 | 2 | 1 | 2 | 3 | 2 | .02 | .006 | 2 | 2 | .07 | 128 | .01 | 2 | .13 | .01 | .03 | 1 | 1 |
| 6775 | 1 | 26 | 13 | 52 | .1 | 24 | 10 | 398 | 2.36 | 2 | 5 | ND | 7 | 12 | 1 | 2 | 2 | 8 | .08 | .030 | 21 | 14 | .69 | 69 | .01 | 5 | 1.32 | .01 | .17 | 1 | 2 |
| 11066 | 1 | 13 | 2 | 12 | .1 | 7 | 2 | 106 | .64 | 2 | 5 | ND | 1 | 5 | 1 | 2 | 3 | 3 | .02 | .009 | 3 | 3 | .13 | 71 | .01 | 2 | .24 | .01 | .05 | 1 | 1 |
| 11067 | 1 | 11 | 2 | 7 | .1 | 8 | 3 | 89 | .50 | 2 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 2 | .02 | .009 | 3 | 9 | .12 | 41 | .01 | 4 | .20 | .01 | .03 | 7 | 2 |
| 11068 | 1 | 12 | 39 | 29 | .1 | 12 | 4 | 1427 | 1.05 | 2 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 5 | .15 | .035 | 3 | 6 | .22 | 312 | .01 | 2 | .34 | .01 | .03 | 1 | 1 |
| 11069 | 1 | 20 | 10 | 41 | .1 | 20 | 7 | 2011 | 1.11 | 2 | 5 | ND | 1 | 10 | 1 | 2 | 4 | 6 | .16 | .006 | 9 | 12 | .33 | 124 | .01 | 3 | .48 | .01 | .07 | 7 | 1 |
| 11070 | 1 | 28 | 4 | 131 | .2 | 15 | 26 | 1001 | 8.37 | 2 | 5 | ND | 2 | 118 | 8 | 3 | 2 | 105 | 4.77 | .186 | 8 | 13 | 1.79 | 492 | .37 | 6 | 2.71 | .02 | .17 | 1 | 1 |
| 11071 | 1 | 14 | 10 | 50 | .1 | 10 | 6 | 539 | 2.57 | 5 | 5 | ND | 2 | 176 | 1 | 2 | 2 | 51 | 2.16 | .056 | 8 | 28 | .88 | 90 | .15 | 5 | 1.94 | .02 | .09 | 1 | 1 |
| 11072 | 1 | 19 | 2 | 35 | .1 | 9 | 3 | 232 | .74 | 2 | 5 | ND | 1 | 51 | 1 | 2 | 2 | 6 | .62 | .020 | 4 | 4 | .20 | 94 | .01 | 4 | .32 | .01 | .05 | 1 | 1 |
| 11073 | 1 | 52 | 11 | 102 | .1 | 76 | 35 | 964 | 7.26 | 2 | 5 | ND | 1 | 55 | 3 | 2 | 2 | 86 | 1.58 | .183 | 13 | 97 | 5.35 | 59 | .15 | 3 | 3.97 | .01 | .12 | 1 | 1 |
| 11074 | 1 | 6 | 2 | 17 | .1 | 8 | 1 | 373 | .48 | 3 | 5 | ND | 1 | 481 | 1 | 2 | 2 | 4 | 25.35 | .005 | 3 | 8 | .43 | 24 | .01 | 2 | .23 | .01 | .01 | 1 | 2 |
| 11075 | 1 | 6 | 3 | 11 | .1 | 7 | 3 | 80 | .49 | 2 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 6 | .31 | .015 | 2 | 11 | .21 | 35 | .01 | 2 | .23 | .01 | .02 | 2 | 1 |
| FALLS | 1 | 3 | 2 | 10 | .1 | 3 | 1 | 79 | .28 | 2 | 5 | ND | 1 | 11 | 1 | 2 | 2 | 1 | .43 | .007 | 2 | 2 | .03 | 65 | .01 | 2 | .07 | .01 | .01 | 1 | 2 |
| STD C/AU-R | 17 | 59 | 41 | 132 | 6.8 | 67 | 29 | 1022 | 4.13 | 42 | 16 | 7 | 37 | 48 | 16 | 20 | 23 | 59 | .48 | .095 | 39 | 53 | .89 | 177 | .07 | 33 | 1.99 | .06 | .15 | 13 | 490 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L10N 6+12W | 1 | 28 | 167 | 104 | .4 | 77 | 28 | 803 | 7.81 | 3 | 5 | ND | 1 | 23 | 2 | 2 | 2 | 95 | .78 | .219 | 16 | 80 | 6.29 | 52 | .06 | 2 | 4.55 | .01 | .09 | 1 | 1 |
| L7N 4+00E | 1 | 49 | 44 | 81 | .1 | 43 | 24 | 633 | 6.83 | 5 | 5 | ND | 1 | 13 | 3 | 4 | 3 | 152 | 2.70 | .055 | 2 | 27 | 1.36 | 41 | .33 | 22 | 2.81 | .02 | .10 | 1 | 2 |
| L7N 5+00E | 2 | 9 | 31 | 52 | .1 | 15 | 9 | 331 | 1.54 | 3 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 12 | .83 | .006 | 2 | 12 | .62 | 14 | .02 | 3 | .62 | .01 | .02 | 1 | 1 |
| L7N 6+00E | 1 | 36 | 37 | 112 | .1 | 23 | 18 | 516 | 4.74 | 3 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 32 | 1.45 | .304 | 25 | 30 | 1.01 | 34 | .30 | 4 | .96 | .02 | .20 | 1 | 1 |
| L4N 3+95W | 1 | 17 | 32 | 42 | .1 | 15 | 4 | 149 | 1.44 | 2 | 5 | ND | 2 | 3 | 1 | 2 | 2 | 6 | .06 | .009 | 8 | 9 | .46 | 177 | .01 | 2 | .68 | .01 | .08 | 1 | 2 |
| L4N 3+85W | 1 | 9 | 13 | 10 | .1 | 5 | 1 | 67 | .29 | 2 | 5 | ND | 1 | 1 | 1 | 2 | 2 | 2 | .04 | .006 | 5 | 5 | .06 | 25 | .01 | 2 | .11 | .01 | .04 | 1 | 1 |
| L4N 2+20E | 1 | 45 | 15 | 63 | .1 | 67 | 20 | 461 | 3.43 | 3 | 5 | ND | 1 | 11 | 1 | 3 | 2 | 51 | 1.24 | .023 | 3 | 65 | 2.47 | 35 | .20 | 5 | 2.20 | .03 | .08 | 1 | 1 |
| L4N 2+35E | 1 | 20 | 9 | 31 | .1 | 39 | 10 | 178 | 1.06 | 2 | 5 | ND | 1 | 95 | 3 | 2 | 3 | 18 | 3.72 | .018 | 2 | 19 | .36 | 30 | .17 | 2 | .47 | .02 | .09 | 1 | 1 |
| L4N 2+95E | 2 | 17 | 16 | 14 | .1 | 9 | 1 | 430 | 1.86 | 2 | 5 | ND | 1 | 9 | 1 | 2 | 2 | 8 | 1.00 | .005 | 3 | 11 | .03 | 35 | .02 | 2 | .07 | .01 | .04 | 1 | 1 |
| L4N 3+00E | 1 | 14 | 67 | 41 | .7 | 20 | 2 | 548 | 1.76 | 2 | 5 | ND | 1 | 23 | 2 | 2 | 2 | 12 | 2.93 | .003 | 5 | 8 | .22 | 185 | .01 | 5 | .35 | .01 | .06 | 1 | 1 |
| L3+75N 4+50E | 1 | 63 | 13 | 52 | .2 | 40 | 21 | 525 | 4.67 | 4 | 8 | ND | 1 | 51 | 7 | 2 | 2 | 102 | 7.64 | .022 | 2 | 52 | .93 | 16 | .18 | 27 | 3.38 | .03 | .01 | 1 | 1 |
| L2N 2+00W | 1 | 21 | 6 | 29 | .1 | 11 | 2 | 84 | .83 | 4 | 5 | ND | 2 | 3 | 2 | 2 | 2 | 13 | .11 | .008 | 9 | 6 | .08 | 161 | .03 | 5 | .30 | .01 | .05 | 1 | 1 |
| L2N 1+50W | 2 | 4 | 10 | 22 | .1 | 8 | 3 | 865 | .58 | 4 | 5 | ND | 1 | 3 | 1 | 2 | 2 | 8 | .29 | .006 | 2 | 8 | .07 | 41 | .01 | 3 | .17 | .01 | .01 | 1 | 1 |
| L2N 0+50W | 3 | 8 | 20 | 9 | .3 | 13 | 2 | 82 | .53 | 2 | 5 | ND | 1 | 1 | 1 | 2 | 3 | 4 | .03 | .005 | 2 | 11 | .07 | 146 | .01 | 5 | .16 | .01 | .02 | 2 | 2 |
| L1+40N 0+25E | 2 | 5 | 4 | 5 | .1 | 6 | 1 | 192 | .28 | 2 | 5 | ND | 1 | 115 | 4 | 2 | 2 | 3 | 2.60 | .003 | 2 | 6 | .06 | 21 | .01 | 4 | .10 | .01 | .01 | 1 | 1 |
| L0 1+12W | 1 | 3 | 5 | 5 | .1 | 5 | 1 | 560 | .22 | 2 | 8 | ND | 1 | 91 | 5 | 2 | 2 | 1 | 6.39 | .004 | 2 | 5 | .04 | 74 | .01 | 2 | .01 | .01 | .01 | 3 | 1 |
| L10W 3+71N "A" | 1 | 48 | 18 | 50 | .1 | 19 | 5 | 241 | 1.71 | 3 | 5 | ND | 1 | 7 | 1 | 2 | 2 | 7 | .11 | .009 | 7 | 10 | .45 | 60 | .01 | 2 | .71 | .01 | .08 | 1 | 10 |
| L10W 8+71N "B" | 1 | 17 | 10 | 17 | .1 | 10 | 2 | 322 | .37 | 5 | 5 | ND | 1 | 8 | 1 | 2 | 2 | 2 | .26 | .003 | 4 | 6 | .07 | 50 | .01 | 4 | .13 | .01 | .05 | 1 | 1 |
| L10W 2+95N | 1 | 20 | 15 | 66 | .1 | 25 | 9 | 367 | 3.95 | 6 | 5 | ND | 6 | 14 | 1 | 2 | 2 | 11 | .03 | .060 | 16 | 17 | .87 | 70 | .01 | 3 | 1.63 | .01 | .12 | 1 | 1 |
| RC 1 | 1 | 7 | 7 | 7 | .1 | 6 | 1 | 84 | .28 | 2 | 5 | ND | 1 | 1 | 1 | 2 | 2 | 1 | .02 | .006 | 2 | 5 | .03 | 35 | .01 | 4 | .06 | .01 | .02 | 1 | 1 |
| RC 7 | 3 | 5 | 3 | 5 | .1 | 8 | 1 | 627 | .26 | 2 | 5 | ND | 1 | 5 | 1 | 2 | 2 | 1 | .15 | .001 | 2 | 6 | .05 | 44 | .01 | 2 | .04 | .01 | .01 | 1 | 1 |
| RC 9 | 2 | 11 | 15 | 10 | .2 | 11 | 2 | 154 | .50 | 2 | 5 | ND | 1 | 8 | 1 | 2 | 2 | 4 | .14 | .006 | 2 | 11 | .12 | 62 | .01 | 2 | .17 | .01 | .01 | 1 | 1 |
| RC 9+50 "W" | 2 | 41 | 13 | 29 | .1 | 9 | 3 | 67 | 1.71 | 4 | 5 | ND | 4 | 8 | 1 | 2 | 2 | 4 | .01 | .014 | 6 | 6 | .17 | 1350 | .01 | 3 | .37 | .01 | .09 | 5 | 1 |
| RC 9+50 "E" | 2 | 6 | 5 | 2 | .1 | 8 | 1 | 262 | .28 | 2 | 5 | ND | 1 | 117 | 2 | 2 | 2 | 1 | 1.87 | .001 | 2 | 8 | .01 | 47 | .01 | 3 | .01 | .01 | .01 | 1 | 10 |
| RC 10 | 2 | 12 | 9 | 22 | .1 | 18 | 3 | 164 | 1.07 | 4 | 5 | ND | 1 | 16 | 1 | 2 | 2 | 7 | .22 | .038 | 4 | 11 | .32 | 195 | .01 | 2 | .45 | .01 | .04 | 1 | 1 |
| STD C/AU-R | 18 | 60 | 37 | 132 | 7.0 | 68 | 31 | 1034 | 4.26 | 42 | 18 | 8 | 39 | 50 | 17 | 17 | 19 | 61 | .49 | .092 | 40 | 55 | .92 | 179 | .07 | 33 | 2.00 | .06 | .15 | 12 | 500 |

# SAMPLE RECORD SHEET



SAMPLER: J. McLEOD

MAP SHEET: 104 J

PROPERTY: HOP

PROJECT: 88-2

AREA: DEASE LAKE, B.C.

COMPANY: BIG I DEVELOPMENTS LTD.

DATE: DEC. /88 – JAN. /89

No. of Sa.: 21

| Sample No. | DESCRIPTION | TYPE of Sa. | WIDTH | Notebook Ref. | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Au ppb |
|---|---|---|---|---|---|---|---|---|---|
| 6751 | BL-1+72N. Blk. argillite c̄ q'tz | Rx | Grab | I back | 4 | 2 | 4 | .1 | 1 |
| 6752 | BL-2+60-90N. Silic. v.f.gr. l.gy. sed. | " | " | " | 18 | 5 | 9 | .1 | 2 |
| 6753 | BL-12+34N. F.gr. greenstone | " | " | " | 106* | 6 | 73* | .1 | 1 |
| 6754 | BL-13+50N Silic gy-blk arg. c̄ q'tz | " | " | II back | 9 | 2 | 12 | .1 | 1 |
| 6755 | BL-14+75-15+00N Silic arg. | " | " | " | 14 | 2 | 26 | .1 | 2 |
| 6756 | | " | " | III | 30 | 8 | 39 | .1 | 1 |
| 6757 | L18N-3+75W. Bd. v.f.gr. chert c̄ q.v. | " | " | III back | 25 | 3 | 30 | .1 | 1 |
| 6758 | L20N-3+67E V.f. gr. andesite c̄ q.v. | " | " | IV " | 85 | 2 | 26 | .1 | 1 |
| 6759 | L20N-3+67E. V.f. gr. grn-red and. | " | " | IV " | 39 | 9 | 71 | .1 | 1 |
| 6760 | L18N-5+00E Grey & red slate? | " | " | IV back | 15 | 3 | 92 | .2 | 2 |
| L16N 8+00W | Jnt. w/ E-Warms Frypan Ck. | Silt | " | VI | 54 | 15* | *123 | .1 | 3* |
| 6761 | L16N-9+60W. Grn f.gr. and. tuff. | Rx | " | VII back | 17 | 12 | 71 | .1 | 1 |
| L10W 14+70N | 50m. S. of Jnt c̄ Frypan ck. | Silt | " | VI " | 34 | 3 | *100 | .1 | 1 |
| 6762 | L10+20W-14+70N Blk. argillite | Rx | " | VI " | 85 | 15* | 97 | .1 | 4* |
| 6763 | L14N-2+50 to 4+50E And.-grnst | Rx | " | VII back | 67 | 7 | 76 | .2 | 1 |
| 6764 | L14N-2+20E Grey argill. c̄ q.v. | Rx | " | VII " | 22 | 6 | 23 | .1 | 1 |
| 6765 | L12N-3+00E Rd-grn and.-L. | " | " | VIII " | 55 | 7 | 61 | .1 | 1 |
| 6766 | L3E-10+25N Andesite (Grnst.) | " | " | " | 113* | 9 | 81 | .2 | 1 |
| 6767 | L0 – 1+22E " | " | " | " | 110* | 10* | 66 | .1 | 1 |
| 6768 | L0 – 4+50E " | " | " | IX back | 43 | 8 | 62 | .3* | 3* |
| 6769 | L0 – 4+79E " | " | " | " | 12 | 6 | 23 | .1 | 1 |

APPENDIX II

# SAMPLE RECORD SHEET

SAMPLER: J. Mc LEOD

MAP SHEET: 104 J

PROPERTY: HOP

PROJECT: 88-2

AREA: DEASE LAKE - B.C.

COMPANY: BID

DATE: DEC./88 - JAN./89

No. of Sa.: 21

| Sample No. | DESCRIPTION | TYPE of Sa. | WIDTH | Notebook Ref. | Cu m | Pb m | Zn m | Ag m | Au b |
|---|---|---|---|---|---|---|---|---|---|
| 6770 | L2N-4+50E Andesite | R.x | Grab | X back | 47 | 12* | 91 | .2 | 1 |
| 6771 | L2N-0+10W Blk. graph. schist | " | " | " | 16 | 18* | 29 | .1 | 3* |
| 6772 | L2N-0+85W. or silic. arg. " | " | " | " | 8 | 4 | 14 | .1 | 1 |
| 6773 | L2N-1+00W " | " | " | " | 5 | 2 | 6 | .1 | 1 |
| 6774 | L1+75N-3+00W " | " | " | XI | 4 | 2 | 8 | .1 | 1 |
| 6775 | L10W-2+40N " or phyllite | " | " | XI back | 26 | 13* | 52 | .1 | 2 |
| 11066 | L4N-10+15W Silic. phyllite | " | " | " | 13 | 2 | 12 | .1 | 1 |
| 11067 | L4+25N-10+15W " | " | " | XII back | 11 | 2 | 7 | .1 | 2 |
| 11068 | L4+25N-10+36W " c̄ q.v. | " | " | " | 12 | 19* | 29 | .1 | 1 |
| 11069 | L4N-0+35E " | " | " | XIII back | 20 | 10* | 41 | .1 | 1 |
| L4N 3+95W | Grey phyllite | " | " | XII back | 17 | 32* | 42 | .1 | 2 |
| L4N 3+85W | Q+z boulder | R'x | Float | " | 9 | 13* | 10 | .1 | 1 |
| L4N 2+20E | And. tuff or grinst. | " | Grab | XIII back | 45 | 16* | 63 | .1 | 1 |
| L4N 2+35E | " | " | " | " | 20 | 9 | 31 | .1 | 1 |
| L4N 2+95E | Jasper-hematite c̄ graded Bd 108°/60N | " | " | XIV | 17 | 16* | 14 | .1 | 1 |
| L4N 3+00E | " " | " | " | " | 14 | 67* | 41 | .7* | 1 |
| 11070 | F.gr. g'n andesite or grinst | " | " | XIV back | 28 | 4 | 131* | .2 | 1 |
| L7N 4+00E | " " " " | " | " | " | 49 | 44* | 81 | .1 | 2 |
| L7N 5+00E | " " " " | " | " | XIII | 9 | 31* | 52 | .1 | 1 |
| L7N 6+00E | " " " " | " | " | " | 36 | 37* | 112* | .1 | 1 |
| L3+75N 4+50E | " " " c̄ jasper | " | " | XIV | 63 | 13 | 52 | .2 | 1 |

# SAMPLE RECORD SHEET



SAMPLER: J. McLEOD

MAP SHEET: 104 J
PROPERTY: HOP

PROJECT: 88-2
AREA: DEASE LAKE, B.C.
COMPANY: BID
DATE: DEC./88 – JAN./89
No. of Sa.: 19

| Sample No. | DESCRIPTION | TYPE of Sa. | WIDTH | Notebook Ref. | Cu m | Pb m | Zn m | Ag m | Au b |
|---|---|---|---|---|---|---|---|---|---|
| L10W 8+71N "A" | Light grey, f.gr. phyllite Bd? N140/48 | R'x | Grab | XV back | 48 | 18* | 50 | .1 | 10* |
| L10W 8+71N "B" | F.gr. dk. grey argillite | " | " | " | 17 | 10* | 17 | .1 | 1 |
| 11071 | F.gr. grn andesite ø qtz vnlts | " | " | XVI back | 14 | 10* | 50 | .1 | 1 |
| L10N 6+12W | Foliated f.gr. X'stal tuff (and.?) | " | " | " | 28 | 167* | 104* | .4* | 1 |
| L2N 2+00W | Siliceous schist | " | " | X back | 21 | 6 | 29 | .1 | 1 |
| L2N 1+50W | " " | " | " | " | 4 | 10* | 22 | .1 | 1 |
| L2N 0+50W | " " | " | " | " | 8 | 20* | 9 | .3* | 2 |
| 11072 | Q'tz in fold hinge of argillite } 1CW | " | " | XVII back | 19 | 2 | 35 | .1 | 1 |
| 11073 | f.gr. grn andesite fract N105/75W | " | " | XIX | 52 | 11* | 102* | .1 | 1 |
| 11074 | f.gr. white-grey X'stal limes't | " | " | " | 6 | 2 | 17 | .1 | 2 |
| 11075 | Q'tz flt?/ 35m. end of camp. | Q'tz R'x | " | " | 6 | 3 | 11 | .1 | 1 |
| Falls | Andesitic tuff c̄ q'tz. | R'x | " | ~~XIX~~ | 3 | 2 | 10 | .1 | 2 |
| L10W 2+25N | Graphitic schist or phyllite | " | " | XI back | 20 | 15* | 66 | .1 | 1 |
| RC1 | R'x from East arm Rose ck. c̄ | R'x silt | " | XVIII | 7 | 7 | 7 | .1 | 1 |
| RC7 | " quartz | " | " | " | 5 | 3 | 5 | .1 | 1 |
| RC9 | " | " | " | " | 11 | 15* | 10 | .2 | 1 |
| RC9+50W | " | " | " | " | 41 | 13* | 29 | .1 | 1 |
| RC9+50E | " | " | " | " | 6 | 5 | 2 | .1 | 10* |
| RC10 | " | " | " | " | 12 | 9 | 22 | .1 | 1 |
| | | | | | | | | | |
| | | | | | | | | | |

# APPENDIX III

Big I
Geophysical Data

| | | | | | MAG |
|---|---|---|---|---|---|
| | | | | VLF-EM | |
| 0 | N | 0 | W | -3 | 5643 |
| 50 | N | 0 | W | 3 | 5632 |
| 100 | N | 0 | W | 5 | 5634 |
| 150 | N | 0 | W | 0 | 5642 |
| 200 | N | 0 | W | 6 | 5632 |
| 250 | N | 0 | W | 5 | 5624 |
| 300 | N | 0 | W | 4 | 5623 |
| 350 | N | 0 | W | 10 | 5623 |
| 400 | N | 0 | W | 5 | 5633 |
| 450 | N | 0 | W | 5 | 5640 |
| 500 | N | 0 | W | 21 | 5632 |
| 550 | N | 0 | W | 21 | 5632 |
| 600 | N | 0 | W | 5 | 5634 |
| 650 | N | 0 | W | -1 | 5642 |
| 700 | N | 0 | W | 0 | 5644 |
| 750 | N | 0 | W | -2 | 5634 |
| 800 | N | 0 | W | -4 | 5640 |
| 850 | N | 0 | W | 6 | 5643 |
| 900 | N | 0 | W | 10 | 5642 |
| 950 | N | 0 | W | 13 | 5641 |
| 1000 | N | 0 | W | 8 | 2641 |
| 1050 | N | 0 | W | 11 | 5640 |
| 1100 | N | 0 | W | 11 | 5644 |
| 1150 | N | 0 | W | 20 | 5653 |
| 1200 | N | 0 | W | 14 | 5641 |
| 1250 | N | 0 | W | 5 | 5644 |
| 1300 | N | 0 | W | 12 | 5631 |
| 1350 | N | 0 | W | 28 | 5641 |
| 1400 | N | 0 | W | 13 | 5640 |
| 1450 | N | 0 | W | 22 | 5641 |
| 1500 | N | 0 | W | 23 | 5643 |
| 1550 | N | 0 | W | 20 | 5642 |
| 1600 | N | 0 | W | 5 | 5644 |
| 1650 | N | 0 | W | 17 | 5640 |
| 1700 | N | 0 | W | 8 | 5652 |
| 1750 | N | 0 | W | 9 | 5651 |
| 1800 | N | 0 | W | 3 | 5641 |
| 1850 | N | 0 | W | 8 | 2633 |
| 1900 | N | 0 | W | 2 | 5633 |
| 1950 | N | 0 | W | 5 | 2643 |
| 2000 | N | 0 | W | 4 | 5624 |
| 1800 | N | 50 | W | 5 | 5650 |
| 1800 | N | 100 | W | 6 | 5631 |
| 1800 | N | 150 | W | 7 | 5633 |
| 1800 | N | 200 | W | 1 | 5633 |
| 1800 | N | 250 | W | 12 | 5640 |
| 1800 | N | 300 | W | 1 | 5642 |
| 1800 | N | 350 | W | -3 | 5633 |
| 1800 | N | 400 | W | 17 | 5641 |
| 1800 | N | 450 | W | 11 | 5640 |
| 1800 | N | 500 | W | 8 | 5634 |
| 1800 | N | 550 | W | 11 | 5650 |
| 1800 | N | 600 | W | 4 | 5634 |
| 1800 | N | 650 | W | 13 | 5644 |

Big I
Geophysical Data

| | | | | VLF-EM | MAG |
|---|---|---|---|---|---|
| 1800 | N | 700 | W | 20 | 5642 |
| 1800 | N | 750 | W | 12 | 5631 |
| 1800 | N | 800 | W | 9 | 5641 |
| 1800 | N | 850 | W | 18 | 5632 |
| 1800 | N | 900 | W | 15 | 5634 |
| 1800 | N | 950 | W | 6 | 5640 |
| 1800 | N | 1000 | W | -4 | 5631 |
| 1850 | N | 1000 | W | -4 | 5644 |
| 1900 | N | 1000 | W | -2 | 5640 |
| 1950 | N | 1000 | W | -2 | 5641 |
| 2000 | N | 1000 | W | 9 | 5632 |
| 2000 | N | 950 | W | -3 | 5642 |
| 2000 | N | 900 | W | -5 | 5634 |
| 2000 | N | 850 | W | -2 | 5632 |
| 2000 | N | 800 | W | 0 | 5640 |
| 2000 | N | 750 | W | -3 | 5640 |
| 2000 | N | 700 | W | 8 | 5641 |
| 2000 | N | 650 | W | 7 | 5642 |
| 2000 | N | 600 | W | 2 | 5642 |
| 2000 | N | 550 | W | 10 | 5651 |
| 2000 | N | 500 | W | 12 | 5632 |
| 2000 | N | 450 | W | 7 | 5642 |
| 2000 | N | 400 | W | 5 | 5644 |
| 2000 | N | 350 | W | 12 | 5641 |
| 2000 | N | 300 | W | 7 | 5632 |
| 2000 | N | 250 | W | 15 | 5644 |
| 2000 | N | 200 | W | 6 | 5634 |
| 2000 | N | 150 | W | 13 | 5632 |
| 2000 | N | 100 | W | 9 | 5634 |
| 2000 | N | 50 | W | 11 | 5644 |
| 2000 | N | 50 | E | 1 | 5641 |
| 2000 | N | 100 | E | 1 | 5650 |
| 2000 | N | 150 | E | 8 | 5644 |
| 2000 | N | 200 | E | 2 | 5634 |
| 2000 | N | 250 | E | 5 | 5623 |
| 2000 | N | 300 | E | 3 | 5623 |
| 2000 | N | 350 | E | 9 | 5632 |
| 2000 | N | 400 | E | -1 | 5660 |
| 2000 | N | 450 | E | 3 | 5630 |
| 2000 | N | 500 | E | 14 | 5641 |
| 1950 | N | 500 | E | 8 | 5650 |
| 1900 | N | 500 | E | 6 | 5642 |
| 1850 | N | 500 | E | -2 | 5633 |
| 1800 | N | 500 | E | 0 | 5633 |
| 1800 | N | 450 | E | 4 | 5640 |
| 1800 | N | 400 | E | -1 | 5641 |
| 1800 | N | 350 | E | 13 | 5633 |
| 1800 | N | 300 | E | 2 | 5634 |
| 1800 | N | 250 | E | -4 | 5631 |
| 1800 | N | 200 | E | 0 | 5650 |
| 1800 | N | 150 | E | 20 | 5634 |
| 1800 | N | 100 | E | 7 | 5640 |
| 1800 | N | 50 | E | 0 | 5631 |
| 1600 | N | 50 | W | 3 | 5634 |

Big I
Geophysical Data

| | | | | VLF-EM | MAG |
|---|---|---|---|---|---|
| 1600 | N | 100 | W | -6 | 5633 |
| 1600 | N | 150 | W | 3 | 5644 |
| 1600 | N | 200 | W | -2 | 5634 |
| 1600 | N | 250 | W | 0 | 5634 |
| 1600 | N | 300 | W | 8 | 5624 |
| 1600 | N | 350 | W | 5 | 5643 |
| 1600 | N | 400 | W | 3 | 5634 |
| 1600 | N | 450 | W | 4 | 5650 |
| 1600 | N | 500 | W | -3 | 5633 |
| 1600 | N | 550 | W | -2 | 5644 |
| 1600 | N | 600 | W | 1 | 5632 |
| 1600 | N | 650 | W | 11 | 5642 |
| 1600 | N | 700 | W | 2 | 5634 |
| 1600 | N | 750 | W | 6 | 5640 |
| 1600 | N | 800 | W | -4 | 5642 |
| 1600 | N | 850 | W | -5 | 5650 |
| 1600 | N | 900 | W | -5 | 5640 |
| 1600 | N | 950 | W | -7 | 5651 |
| 1600 | N | 1000 | W | 14 | 5644 |
| 1550 | N | 1000 | W | -9 | 5641 |
| 1500 | N | 1000 | W | -9 | 5631 |
| 1450 | N | 1000 | W | 8 | 5630 |
| 1400 | N | 1000 | W | 12 | 5630 |
| 1400 | N | 950 | W | -3 | 5634 |
| 1400 | N | 900 | W | -5 | 5650 |
| 1400 | N | 850 | W | 6 | 5641 |
| 1400 | N | 800 | W | -5 | 5641 |
| 1400 | N | 750 | W | 11 | 5642 |
| 1400 | N | 700 | W | 4 | 5634 |
| 1400 | N | 650 | W | 0 | 5641 |
| 1400 | N | 600 | W | -3 | 5644 |
| 1400 | N | 550 | W | 1 | 5641 |
| 1400 | N | 500 | W | 11 | 5640 |
| 1400 | N | 450 | W | 3 | 5630 |
| 1400 | N | 400 | W | 12 | 5650 |
| 1400 | N | 350 | W | -15 | 5633 |
| 1400 | N | 300 | W | -12 | 5640 |
| 1400 | N | 250 | W | -11 | 5631 |
| 1400 | N | 200 | W | -7 | 5640 |
| 1400 | N | 150 | W | 0 | 5643 |
| 1400 | N | 100 | W | 7 | 5641 |
| 1400 | N | 50 | W | 17 | 5634 |
| 1600 | N | 50 | E | 15 | 5632 |
| 1600 | N | 100 | E | 10 | 5651 |
| 1600 | N | 150 | E | 19 | 5634 |
| 1600 | N | 200 | E | 8 | 5640 |
| 1600 | N | 250 | E | -12 | 5641 |
| 1600 | N | 300 | E | 4 | 5642 |
| 1600 | N | 350 | E | 11 | 5643 |
| 1600 | N | 400 | E | 17 | 5641 |
| 1600 | N | 450 | E | 18 | 5654 |
| 1600 | N | 500 | E | 12 | 5651 |
| 1550 | N | 500 | E | 8 | 5660 |
| 1500 | N | 500 | E | 5 | 5653 |

Big I
Geophysical Data

| | | | | VLF-EM | MAG |
|---|---|---|---|---|---|
| 1450 | N | 500 | E | 7 | 5644 |
| 1400 | N | 500 | E | 6 | 5650 |
| 1400 | N | 450 | E | 18 | 5640 |
| 1400 | N | 400 | E | 10 | 5650 |
| 1400 | N | 350 | E | 8 | 5652 |
| 1400 | N | 300 | E | 6 | 5644 |
| 1400 | N | 250 | E | -4 | 5641 |
| 1400 | N | 200 | E | -4 | 5642 |
| 1400 | N | 150 | E | 21 | 5641 |
| 1400 | N | 100 | E | 14 | 5641 |
| 1400 | N | 50 | E | 15 | 5634 |
| 1200 | N | 50 | E | 14 | 5641 |
| 1200 | N | 100 | E | 9 | 5642 |
| 1200 | N | 150 | E | -4 | 5633 |
| 1200 | N | 200 | E | -4 | 5642 |
| 1200 | N | 250 | E | 5 | 5644 |
| 1200 | N | 300 | E | 7 | 5641 |
| 1150 | N | 300 | E | 6 | 5640 |
| 1100 | N | 300 | E | 5 | 5651 |
| 1050 | N | 300 | E | 9 | 5651 |
| 1000 | N | 300 | E | 9 | 5652 |
| 1000 | N | 250 | E | 8 | 5654 |
| 1000 | N | 200 | E | 7 | 5642 |
| 1000 | N | 150 | E | 0 | 5642 |
| 1000 | N | 100 | E | -4 | 5641 |
| 1000 | N | 50 | E | 3 | 5650 |
| 0 | N | 50 | E | 3 | 5642 |
| 0 | N | 100 | E | 5 | 5640 |
| 0 | N | 150 | E | 8 | 5634 |
| 0 | N | 200 | E | 6 | 5624 |
| 0 | N | 250 | E | 4 | 5633 |
| 0 | N | 300 | E | 7 | 5634 |
| 0 | N | 350 | E | 13 | 5633 |
| 0 | N | 400 | E | 9 | 5654 |
| 0 | N | 450 | E | 9 | 5653 |
| 0 | N | 500 | E | 10 | 5660 |
| 50 | N | 500 | E | 11 | 5660 |
| 100 | N | 500 | E | 9 | 5662 |
| 150 | N | 500 | E | 8 | 5613 |
| 200 | N | 500 | E | 15 | 5623 |
| 200 | N | 450 | E | 11 | 5651 |
| 200 | N | 400 | E | 11 | 5620 |
| 200 | N | 350 | E | 8 | 5630 |
| 200 | N | 300 | E | 6 | 5651 |
| 200 | N | 250 | E | 6 | 5640 |
| 200 | N | 200 | E | 4 | 5624 |
| 200 | N | 150 | E | 4 | 5624 |
| 200 | N | 100 | E | -3 | 5641 |
| 200 | N | 50 | E | 8 | 5640 |
| 200 | N | 50 | W | 11 | 5633 |
| 200 | N | 100 | W | 7 | 5640 |
| 200 | N | 150 | W | 2 | 5634 |
| 200 | N | 200 | W | -2 | 5633 |
| 200 | N | 250 | W | -3 | 5642 |

Big I
Geophysical Data

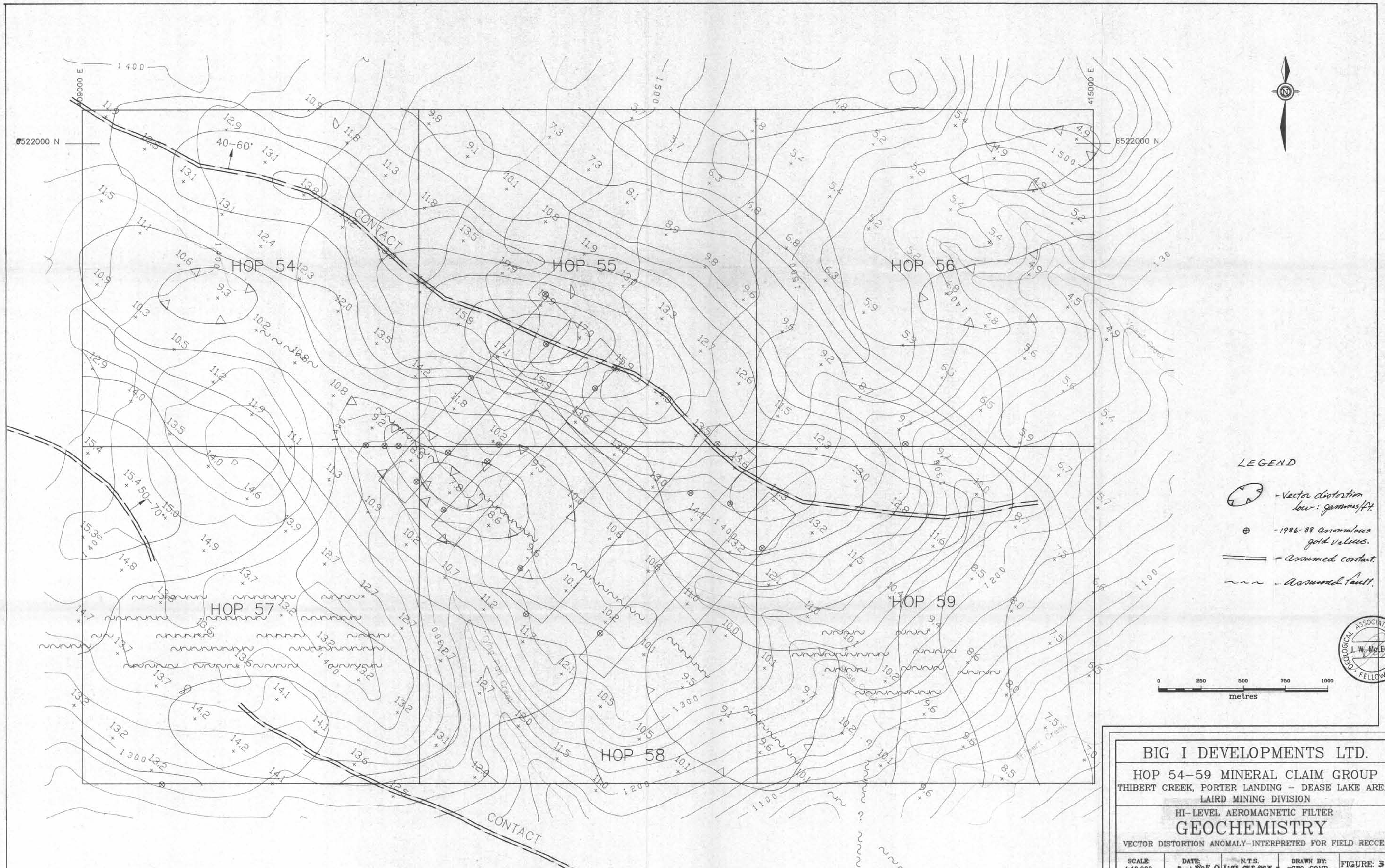
| | | | | VLF-EM | MAG |
|---|---|---|---|---|---|
| 200 | N | 300 | W | 5 | 5641 |
| 200 | N | 350 | W | 2 | 5641 |
| 200 | N | 400 | W | -4 | 5632 |
| 200 | N | 450 | W | 4 | 5632 |
| 200 | N | 500 | W | 2 | 5641 |
| 200 | N | 550 | W | 3 | 5640 |
| 200 | N | 600 | W | 2 | 5630 |
| 200 | N | 650 | W | 12 | 5634 |
| 200 | N | 700 | W | 9 | 5633 |
| 200 | N | 750 | W | 15 | 5640 |
| 200 | N | 800 | W | 4 | 5634 |
| 200 | N | 850 | W | 5 | 5633 |
| 200 | N | 900 | W | 10 | 5641 |
| 200 | N | 950 | W | 4 | 5642 |
| 200 | N | 1000 | W | 5 | 5640 |
| 250 | N | 1000 | W | 4 | 5641 |
| 300 | N | 1000 | W | 6 | 5641 |
| 350 | N | 1000 | W | 13 | 5640 |
| 400 | N | 1000 | W | 17 | 5634 |
| 400 | N | 950 | W | 10 | 5640 |
| 400 | N | 900 | W | 3 | 5640 |
| 400 | N | 850 | W | 8 | 5633 |
| 400 | N | 800 | W | 8 | 5642 |
| 400 | N | 750 | W | 7 | 5650 |
| 400 | N | 700 | W | 7 | 5642 |
| 400 | N | 650 | W | 6 | 5642 |
| 400 | N | 600 | W | 4 | 5634 |
| 400 | N | 550 | W | 2 | 5640 |
| 400 | N | 500 | W | 0 | 5641 |
| 400 | N | 450 | W | -1 | 5634 |
| 400 | N | 400 | W | -5 | 5632 |
| 400 | N | 350 | W | 10 | 5640 |
| 400 | N | 300 | W | 3 | 5634 |
| 400 | N | 250 | W | 13 | 5634 |
| 400 | N | 200 | W | 12 | 5633 |
| 400 | N | 150 | W | 3 | 5642 |
| 400 | N | 100 | W | -6 | 5640 |
| 400 | N | 50 | W | -6 | 5642 |
| 400 | N | 50 | E | 4 | 5642 |
| 400 | N | 100 | E | -2 | 5632 |
| 400 | N | 150 | E | 5 | 5641 |
| 400 | N | 200 | E | 4 | 5641 |
| 400 | N | 250 | E | 8 | 5640 |
| 400 | N | 300 | E | 16 | 5640 |
| 400 | N | 350 | E | 10 | 5643 |
| 400 | N | 400 | E | 0 | 5681 |
| 400 | N | 450 | E | 3 | 5630 |
| 400 | N | 500 | E | 10 | 5630 |
| 400 | N | 550 | E | 6 | 5624 |
| 400 | N | 600 | E | 15 | 5632 |
| 450 | N | 600 | E | 22 | 5630 |
| 500 | N | 600 | E | 12 | 5642 |
| 550 | N | 600 | E | 8 | 5623 |
| 700 | N | 600 | E | 8 | 5642 |

Big I
Geophysical Data

| | | | | | | |
|---|---|---|---|---|---|---|
| | | | | VLF-EM | MAG |
| 700 | N | 550 | E | 8 | 5620 |
| 700 | N | 500 | E | 3 | 5660 |
| 700 | N | 450 | E | 11 | 5691 |
| 700 | N | 400 | E | 9 | 5663 |
| 700 | N | 350 | E | 15 | 5644 |
| 700 | N | 300 | E | 9 | 5653 |
| 700 | N | 250 | E | 4 | 5634 |
| 700 | N | 200 | E | 8 | 5651 |
| 700 | N | 150 | E | 5 | 5642 |
| 700 | N | 100 | E | 8 | 5642 |
| 700 | N | 50 | E | 20 | 5640 |
| 700 | N | 50 | W | 7 | 5642 |
| 700 | N | 100 | W | 6 | 5634 |
| 700 | N | 150 | W | 10 | 5644 |
| 700 | N | 200 | W | 8 | 5640 |
| 700 | N | 250 | W | 10 | 5643 |
| 700 | N | 300 | W | 8 | 5643 |
| 700 | N | 350 | W | 8 | 5644 |
| 700 | N | 400 | W | 6 | 5640 |
| 700 | N | 450 | W | 7 | 5642 |
| 700 | N | 500 | W | 6 | 5641 |
| 700 | N | 550 | W | 8 | 5640 |
| 700 | N | 600 | W | 4 | 5643 |
| 700 | N | 650 | W | 9 | 5643 |
| 700 | N | 700 | W | 11 | 5643 |
| 700 | N | 750 | W | 8 | 5650 |
| 700 | N | 800 | W | 8 | 5644 |
| 700 | N | 850 | W | 12 | 5644 |
| 700 | N | 900 | W | 9 | 5650 |
| 700 | N | 950 | W | 27 | 5644 |
| 700 | N | 1000 | W | 20 | 5650 |
| 750 | N | 1000 | W | 21 | 5651 |
| 800 | N | 1000 | W | 16 | 5644 |
| 850 | N | 1000 | W | 20 | 5652 |
| 900 | N | 1000 | W | 11 | 5653 |
| 950 | N | 1000 | W | 11 | 5650 |
| 1000 | N | 1000 | W | 10 | 5652 |
| 1000 | N | 950 | W | 10 | 5644 |
| 1000 | N | 900 | W | 9 | 5661 |
| 1000 | N | 850 | W | 8 | 5651 |
| 1000 | N | 800 | W | 9 | 5660 |
| 1000 | N | 750 | W | 12 | 5660 |
| 1000 | N | 700 | W | 12 | 5651 |
| 1000 | N | 650 | W | 9 | 5644 |
| 1000 | N | 600 | W | 11 | 5643 |
| 1000 | N | 550 | W | 8 | 5643 |
| 1000 | N | 500 | W | 10 | 5650 |
| 1000 | N | 450 | W | 8 | 5652 |
| 1000 | N | 400 | W | 10 | 5651 |
| 1000 | N | 350 | W | 3 | 5650 |
| 1000 | N | 300 | W | 6 | 5650 |
| 1000 | N | 250 | W | 7 | 5653 |
| 1000 | N | 200 | W | 23 | 5643 |
| 1000 | N | 150 | W | 12 | 5643 |

Big I
Geophysical Data

| | | | | VLF-EM | MAG |
|---|---|---|---|---|---|
| 0 | N | 50 | W | 8 | 5640 |
| 0 | N | 100 | W | 1 | 5642 |
| 0 | N | 150 | W | 11 | 5643 |
| 0 | N | 200 | W | 3 | 5644 |
| 0 | N | 250 | W | -9 | 5643 |
| 0 | N | 300 | W | -9 | 5641 |
| 0 | N | 350 | W | -2 | 5643 |
| 0 | N | 400 | W | -3 | 5640 |
| 0 | N | 450 | W | 0 | 5640 |
| 0 | N | 500 | W | 4 | 5640 |




# BIG I DEVELOPMENTS LTD.

## HOP 54–59 MINERAL CLAIM GROUP

THIBERT CREEK, PORTER LANDING – DEASE LAKE AREA
LAIRD MINING DIVISION

HI–LEVEL AEROMAGNETIC FILTER

## GEOCHEMISTRY

VECTOR DISTORTION ANOMALY–INTERPRETED FOR FIELD RECCE.

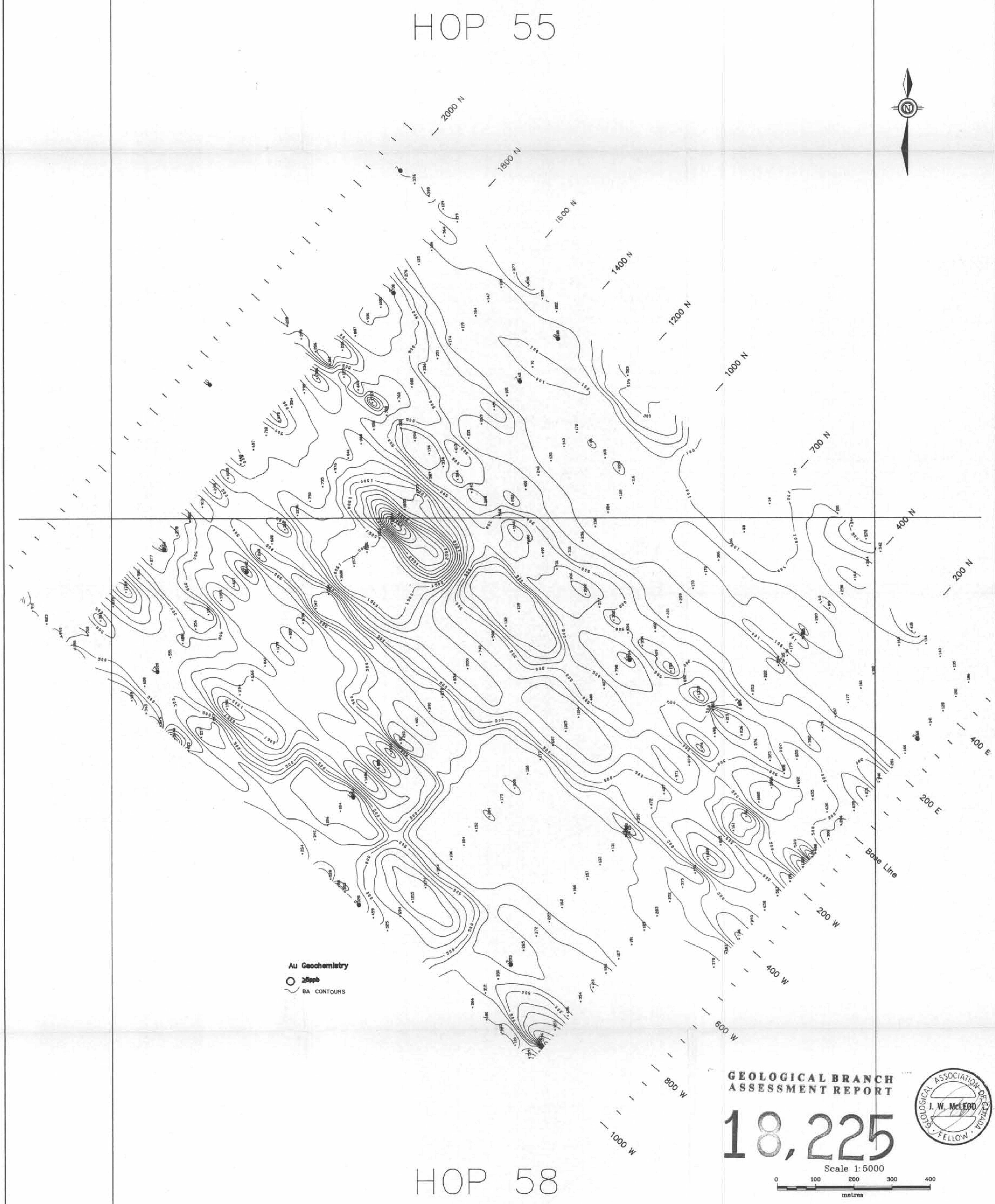
| SCALE: | DATE: | N.T.S. | DRAWN BY: | FIGURE: 3 |
|---|---|---|---|---|
| 1:10,000 | Sept. '88 | 104-I-5/16W | GEO-COMP | |

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,225


GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,225




GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,225

J. W. McLEOD
GEOLOGICAL ASSOCIATION OF CANADA
FELLOW

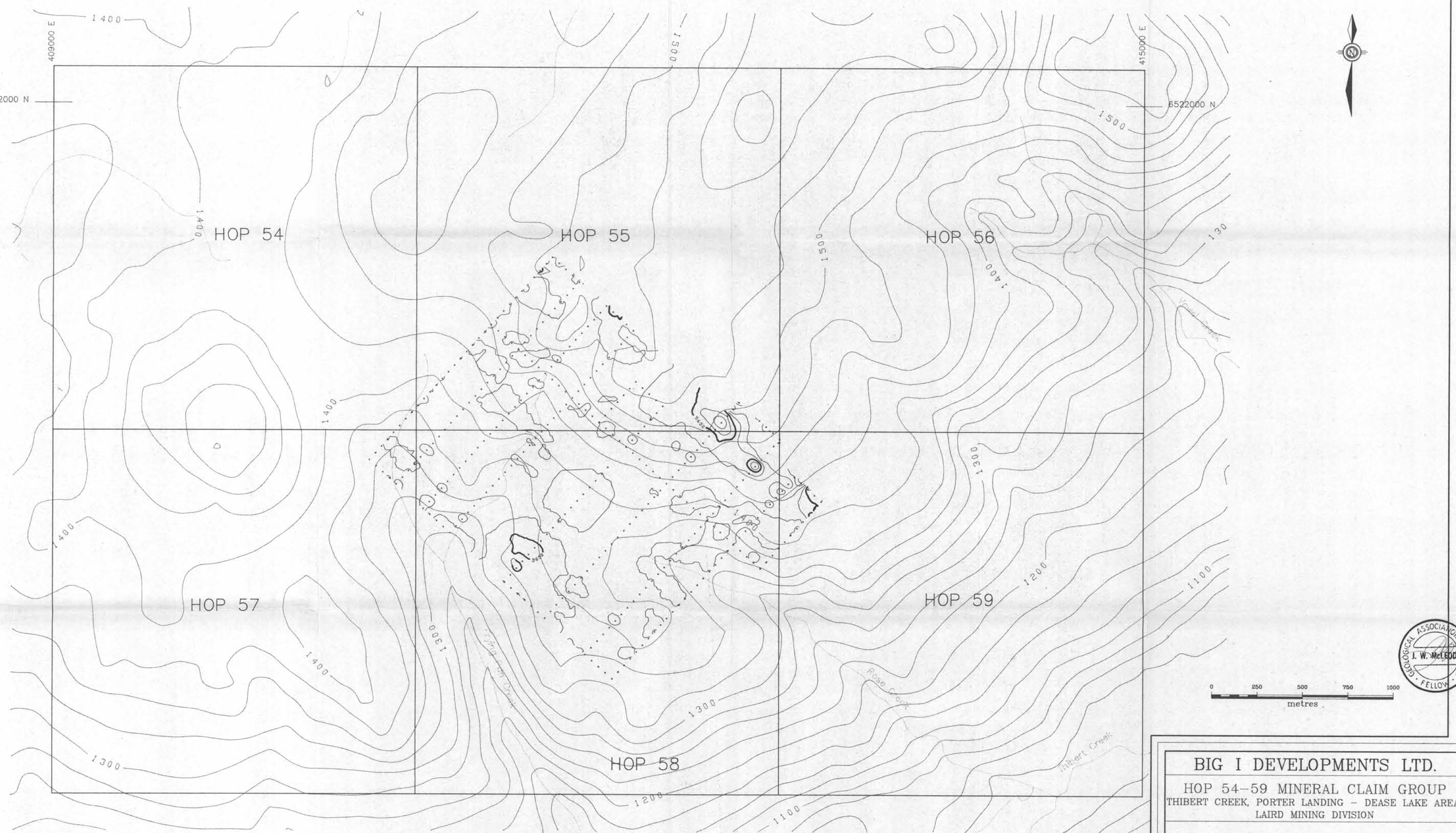
BIG I DEVELOPMENTS LTD.

HOP 54-59 MINERAL CLAIM GROUP
THIBERT CREEK, PORTER LANDING - DEASE LAKE AREA
LAIRD MINING DIVISION

BA GEOCHEMISTRY
SHOWING ANOMALOUS GOLD

| SCALE: | DATE: | N.T.S. | DRAWN BY: | FIGURE: 5 |
|---|---|---|---|---|
| 1:5000 | Dec.'88 | 104-15E/16W | GEO-COMP | |

Geo-Comp Drawing File: BIGI\BA 12-30-88




CONTOUR INTERVAL 100 GAMMAS

# BIG I DEVELOPMENTS LTD.

HOP 54–59 MINERAL CLAIM GROUP

THIBERT CREEK, PORTER LANDING – DEASE LAKE AREA

LAIRD MINING DIVISION

## MAGNETOMETER SURVEY

| SCALE: | DATE: | N.T.S. | DRAWN BY: | FIGURE: |
|---|---|---|---|---|
| 1:10,000 | JAN'89 | 104–15E/16W | GEO-COMP | 6 |

Geo-Comp Drawing File: CAL\MAG 01-05-89

409000 E
415000 E
6522000 N
6522000 N
HOP 54
HOP 55
HOP 56
HOP 57
HOP 58
HOP 59
1400
1500
1300
1200
1100
Rose Creek
Thibert Creek
CONTOUR INTERVAL 5'
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,225
GEOLOGICAL ASSOCIATION OF CANADA
J. W. McLEOD
FELLOW
0 250 500 750 1000
metres
BIG I DEVELOPMENTS LTD.
HOP 54-59 MINERAL CLAIM GROUP
THIBERT CREEK, PORTER LANDING - DEASE LAKE AREA
LAIRD MINING DIVISION
VLF-EM SURVEY
SCALE: 1:10,000
DATE: JAN'89
N.T.S. 104-15E/16W
DRAWN BY: GEO-COMP
FIGURE: 7
Geo-Comp Drawing File: CAL\VLF 01-05-89