GEOCHEMICAL REPORT FOR
ASSESSMENT WORK
LONE SILVER 1, 2, 3 CLAIMS
LONE SILVER PROPERTY
NELSON, M.D.

82 F/3
49° 03'N 117° 16'E

A Report Prepared by
R. W. Klassen

for

CORONA CORPORATION
1440-800 West Pender Street
Vancouver, B.C.
V6C 2V6

January, 1989

REPORTS-50:rep3

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SUMMARY

The Lone Silver 1, Lone Silver 2 and Lone Silver 3 mineral claims, located 14km south of Salmo, B.C.. at Rosebud Lake, were optioned by Corona Corp. (Lacana Mining) in 1988. The claims, originally worked from 1909-1915 and 1936-1941 producing 192 high graded tons of 0.448 oz/ton Au and 116.2 oz/ton Ag., are cut by the Black Bluff overthrust fault which is considered a potential host for large scale economic Au-Ag mineralization.

The 1988 work programme, which coincided with work on Corona's Cat and Zip claims to the west, included 147 soil samples along 4km of grid line over the trace of the fault, as well as geological mapping, rock and silt sampling.

The soil grid failed to define a geochemical signature over the fault zone leaving no targets for further work. However excavation around and rehabilitation in the adits may still produce favorable results.

CORONA CORPORATION

LONE SILVER PROPERTY

PROPERTY LOCATION

DATE:	SCALE:	DRAWING No.
Jan 1989	No Scale	1

Location and Access

Corona's Lone Silver claims are located off Highway #3, 14km south of Salmo, B.C. at Rosebud Lake, south of the Junction of the Salmo and South Salmo Rivers in the Nelson M.D. Access to the claims is by all weather gravel road (Fig 1).

Physiography

The claims are situated in an area of moderate relief around Rosebud Lake and are covered by extensive pine, spruce, larch and balsam forest. A few creeks and swamps are present in the area.

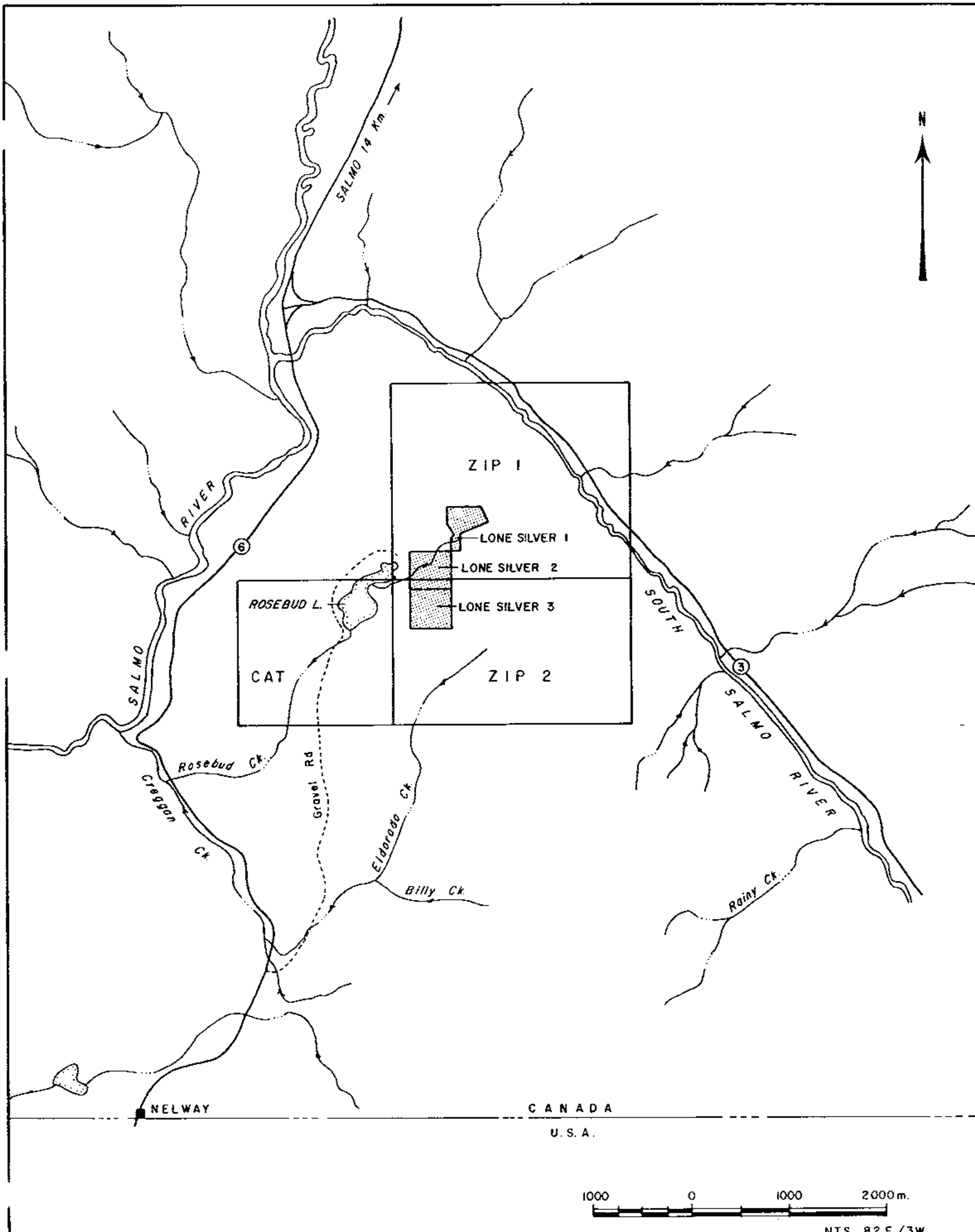
Claims

The Lone Silver Claims were optioned by Corona (Lacana Mining Corp) from O.G.G. Resources of Penticton B.C. in March, 1988 (Fig 2).

Name	Record #	# Units	Expiry Date
Lone Silver 1	55	1	09/06/91
Lone Silver 2	1331	1	07/11/91
Lone Silver 3	1332	1	07/11/91

Regional Geology

The geology of the Salmo area, described in BCDM Bulletin No. 41, 1959, and GSC openfile 1195 contains an early Paleozoic Pend d'Oreille sedimentary sequence of dolomite, limestone, phyllite, argillite and slate that is highly deformed and in some places greatly changed by thermal metamorphism. Within this sequence, the grey dolomite and limestone of the Middle Cambrian Nelway formation is unconformably overlain by the black argillite, slate and argillaceous limestone of the Middle Ordovician Active Formation.



CORONA CORPORATION

LONE SILVER 1,2,3 CLAIMS

CLAIM MAP

DATE: JAN. 1989	SCALE: 1 : 50,000	DRAWING No. 2

The sediments have been intruded by granite, granodiorite and syenite of the Jurassic Nelson intrusions and quartz monzonite of the Teritiary Coryell intrusions. Minor sills and dykes of felsite, apilite and lamprophyre are also present.

The complex deformation of the area includes primary overturned and isoclinal folds which have undergone secondary deformation to open or isoclinal folds. Bedding and thrust faults are common.

Property Geology

The Black Bluff fault, striking 066° and dipping to the SE, cuts the property on the South side of Rosebud Lake. The fault brings dolomite of the middle member of the Nelway formation to the south into contact with argillite of the Active formation to the north.

At the Lone Silver workings, the Black Bluff fault is represented by a zone of faults with a wide variety of attitudes. The fault is marked by brecciated zones in the dolomite and by graphitic schist in the argillite.

The Styx Creek Fault striking 350° slightly offsets the Black Bluff fault.

Mineralization occurs in dolomite, either in quartz lenses or along fractures in the dolomite breccia. Quartz veins containing fine grained galena, pyrite, tetrahedrite, azurite and malachite pinch and swell irregularly with a maximum width of 10cm.

History

The property, originally known as the Hope, shipped Ag-Au ore from 1909 to 1915. The claims lapsed and the property lay idle until 1935 when it was staked by John and Robert Sapples of Salmo. Ore shipments were made from 1936 to 1941. The claims again lapsed and were restaked in 1965 by L.C. DeKock of Nelson. All interests were transferred to O.G.G. Resources in a 1979 B/S agreement. O.G.G. have kept the claims in good standing.

Ore Shipments

Year	Tons	Au (oz/ton)	Ag (oz/ton)
1909-15	86	0.256	156.5
1936-41	106	0.603	83.5
	192	0.448	116.2

1988 Work

The 1988 work coincided with work on Corona's Cat claim and Zip claims, which border the Lone Silver. Work on the Lone Silver 1, 2 and 3 consisted of 147 soil samples along 4km of grid lines, 28 rock samples and one heavy mineral creek sample.

The work was carried out in May 1988 and anomalous results were followed up in October 1988.

All samples from the project were sent to Acme Analytical of Vancouver for analysis by 30 element ICP plus Au by Atomic Absorption.

Soil Programme

A soil grid was put in over the trace of the Black Bluff fault to try and locate anomalous Au-Ag zones along the fault not exposed in outcrop. Grid lines were put in perpendicular to a 400m cut baseline that runs along strike (066°) of the fault. A 100m line spacing was used with lines running N and S of the baseline to cover all three claims, sample station interval was 25m. A total of 147 "B" horizon soil samples were collected along 4km of grid line.

Results from the soil survey were disappointing and no geochemical signature was defined over the fault area. The large depth of overburden in the area may limit the effectiveness of soil samples. Sample locations are given in Figure 3 and analytical results are given in Appendix I.

Geological Mapping

Geological mapping and rock sampling was limited by lack of outcrop on the claims. The old adits and trenches were located and sampled, however no attempts were made to sample inside the adits due to unsafe structural conditions. Samples were also taken from outcrop along a ridge in the SW corner of Lone Silver 3.

Anomalous results occurred from samples around the old adits and the waste dump. Sample #1113 of a quartz vein hosted in brecciated dolomite produced values of 290 ppb Au and 542.6 ppm Ag. Sample #7089, quartz float taken from the waste dump produced values of 250 ppb Au and 27.0 ppm Ag. Sample locations are given in Figure 3, Figure 4 and assay results are given in Appendix II.

Pan Concentrate

One heavy mineral sample was panned from a creek just below the workings. No elevated Au, Ag values were present. Sample location is given in Figure 3 and assay result is given in Appendix III.

Conclusions and Recommendations

Because of the lack of geochemical response over the soil grid, no targets can be defined for further work. Excavation around and rehabilitation in the adits may still produce favourable results.

REFERENCES

Fyles, James T. and Hewlett, C.G.; Stratigraphy and Structure of the Salmo Lead-Zinc Area, Bulletin No. 41; BCDM, 1959.

Little, H.W.; Preliminary Geologic Notes and Map of Nelson (N.T.S. 82F West Half) Map Area, B.C. Geological Survey of Canada, O.F. 1195.

Minister of Mines, B.C. Annual Report, 1938, pp. E17 - E21.

Weymark, William J.; Preliminary Report on the Lone Silver Mining Property, Nelson Mining Division, British Columbia; March 28, 1969.

STATEMENT OF COSTS

Salaries	
6.5 man days x $125.00/day	$ 812.00
Assays	
28 Rock Samples x $20/sample	$ 560.00
147 Soil Samples x $20/sample	2,940.00
1 Pan Concentrate x $20/sample	20.00
Accommodation and Food	
6.5 man days x $50/day	$ 325.00
Transportation	
3 days x $40/day	$ 120.00
Report Preparation	
2 man days x $125/day	$ 250.00
	$5,027.00

1988 Soil Sample Assays

APPENDIX I

LACANA MINING PROJECT-6101 FILE # 88-1686

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L2+00W 1+25S	1	27	42	161	.5	43	10	279	2.71	5	5	ND	7	17	1	2	4	44	.30	.032	20	37	.69	212	.09	6	2.70	.01	.18	1	2
L2+00W 1+50S	2	16	34	303	.1	46	12	685	2.70	4	5	ND	5	27	1	2	3	42	.80	.125	18	27	.71	285	.09	2	2.03	.02	.19	1	1
L2+00W 1+75S	1	15	13	234	.2	36	9	531	2.41	8	5	ND	6	34	1	2	5	33	.32	.335	14	25	.36	291	.11	5	2.53	.02	.16	1	1
L2+50W 2+00S	5	35	42	111	.1	36	13	903	3.70	9	5	ND	6	25	1	2	2	55	.67	.088	16	20	2.03	192	.14	11	2.51	.01	.39	1	2
L2+50W 2+25S	1	18	35	139	.1	41	15	1174	4.32	5	5	ND	7	32	1	2	4	36	.31	.147	19	21	1.10	292	.11	7	2.52	.01	.28	1	1
L2+50W 2+50S	1	19	31	118	.1	59	16	634	4.33	3	5	ND	8	38	1	2	5	29	.34	.062	31	22	.83	185	.09	6	3.25	.02	.12	1	2
L2+50W 2+75S	1	22	250	208	.5	42	14	882	4.18	11	5	ND	11	35	1	7	2	30	.54	.101	36	19	.62	158	.09	4	2.39	.01	.13	2	175
L2+50W 3+00S	1	24	36	91	.1	47	15	638	4.06	5	5	ND	15	45	1	2	2	24	.60	.059	49	19	.68	129	.08	7	2.74	.02	.10	1	19
L2+50W 3+25S	1	15	30	144	.2	45	13	1259	3.40	7	5	ND	8	35	1	3	2	32	.31	.085	20	21	.48	211	.10	8	2.98	.02	.16	1	5
L2+50W 3+50S	1	22	29	122	.3	59	14	1049	4.02	7	5	ND	8	39	1	2	2	30	.39	.060	28	27	.60	193	.10	9	3.46	.02	.19	1	1
L2+50W 3+75S	1	18	25	110	.1	38	13	1155	3.40	11	5	ND	8	34	1	2	4	27	.27	.072	21	24	.53	214	.11	7	3.63	.03	.12	1	1
L2+50W 4+00S	2	24	42	134	.2	56	15	913	3.98	8	5	ND	7	37	1	2	2	24	.41	.093	36	18	.43	175	.06	9	2.55	.01	.11	1	2
L1+00W 0+25N	2	20	27	217	.2	32	10	494	3.06	3	5	ND	7	18	1	4	2	37	.27	.145	19	31	.64	263	.11	10	2.77	.02	.16	1	1
L1+00W 0+00	1	24	49	206	.2	30	9	1297	2.54	4	5	ND	2	26	2	2	2	41	1.35	.118	22	24	.98	253	.06	4	1.72	.01	.18	1	1
L1+00W 0+00A	1	29	26	168	.5	35	8	186	2.71	3	5	ND	7	22	1	2	2	44	.29	.149	18	27	.42	231	.12	5	3.02	.02	.14	1	1
L1+00W 0+25S	1	21	14	176	.1	29	9	336	2.27	5	5	ND	7	22	1	5	2	37	.34	.127	23	31	.46	221	.08	2	1.52	.02	.15	3	1
L1+00W 0+50S	2	32	30	280	.1	41	10	447	2.70	5	5	ND	7	23	1	2	2	49	.48	.129	27	43	.76	205	.08	5	1.55	.02	.22	2	3
L1+00W 0+75S	1	29	29	198	.1	41	10	517	2.71	5	5	ND	6	25	1	2	2	44	.43	.141	22	40	.56	252	.09	4	2.07	.02	.23	1	1
L1+00W 1+00S	1	24	75	562	.2	33	7	1054	2.80	2	5	ND	3	28	2	5	2	69	1.45	.329	18	32	.89	328	.08	3	2.43	.03	.18	1	1
L1+00W 1+25S	1	22	49	223	.1	34	10	397	2.91	2	5	ND	6	19	1	2	2	51	.29	.112	21	28	.49	290	.10	2	2.55	.02	.17	1	1
L1+00W 1+50S	2	28	48	193	.1	40	11	268	3.18	6	5	ND	8	24	1	2	2	50	.32	.089	24	37	.55	264	.13	5	3.22	.03	.21	2	1
L1+00W 1+75S	1	22	13	236	.8	31	8	211	2.32	4	5	ND	6	28	1	2	2	32	.31	.207	21	26	.32	176	.12	6	2.60	.03	.12	1	2
L1+00W 2+00S	1	21	15	198	.4	30	9	254	2.65	8	5	ND	6	24	1	4	2	36	.25	.185	19	27	.42	234	.10	2	2.08	.02	.15	1	1
L1+00W 2+25S	1	18	19	227	.2	41	9	331	2.63	8	5	ND	6	33	1	3	2	38	.34	.270	16	30	.39	380	.12	10	2.82	.02	.17	1	5
L1+00W 2+50S	1	18	17	231	.2	34	8	366	2.40	5	5	ND	6	28	1	2	2	33	.28	.296	14	28	.37	269	.11	4	2.52	.02	.16	1	1
L1+00W 2+75S	1	21	23	213	.2	41	11	440	3.08	6	5	ND	5	26	1	2	2	46	.30	.219	14	34	.61	251	.14	4	2.71	.02	.20	1	1
STD C/AU-S	19	61	42	133	7.1	72	32	1108	4.18	39	15	8	40	53	19	17	24	61	.49	.095	39	60	.90	184	.08	34	1.70	.08	.17	13	51
L1+00W 3+00S	1	18	24	242	.1	51	12	1925	3.28	2	5	ND	4	30	1	2	2	37	.25	.203	14	34	.71	464	.16	5	2.64	.02	.20	1	3
L1+00W 3+25S	1	32	31	132	.1	47	11	512	3.97	8	5	ND	9	31	1	2	2	37	.30	.120	26	26	.61	212	.15	24	4.32	.03	.16	1	2
L1+00W 3+50S	1	27	37	105	.1	46	14	709	4.39	7	5	ND	14	33	1	2	2	27	.34	.058	43	23	.57	177	.10	5	3.20	.02	.09	1	1
L1+00W 3+75S	1	36	24	113	.2	50	16	573	4.07	5	5	ND	11	33	1	2	2	33	.27	.077	40	28	.56	146	.11	4	3.47	.02	.13	1	1
L1+00W 4+00S	1	30	30	167	.1	60	16	956	4.00	5	5	ND	6	40	1	2	2	30	.50	.054	44	34	.49	193	.07	2	2.32	.01	.12	1	1
L1+00W 4+25S	1	28	28	134	.1	65	17	612	4.44	2	5	ND	8	30	1	2	2	28	.34	.062	36	29	.43	132	.08	2	2.96	.02	.11	1	1
0+00 2+75N	1	33	28	234	.6	37	12	253	3.22	7	5	ND	5	28	1	2	2	51	.52	.102	22	41	.56	210	.12	5	3.71	.02	.19	1	1
0+00 2+50N	1	15	23	272	.5	35	7	457	2.31	2	5	ND	5	19	1	2	2	40	.20	.259	15	27	.34	259	.10	2	2.82	.02	.11	1	2
STD C/AU-S	20	60	42	130	7.6	72	33	1094	4.17	43	18	8	39	52	20	17	21	62	.48	.092	40	61	.89	181	.08	36	1.92	.08	.15	12	52

LACANA MINING PROJECT-6101 FILE # 88-1686

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
0+00 2+25N	1	7	11	225	.2	21	7	548	2.06	7	5	ND	2	15	1	4	3	31	.19	.296	13	19	.27	231	.09	2	2.29	.01	.09	3	1
0+00 2+00N	1	13	17	201	.2	24	8	339	2.16	5	5	ND	4	16	1	2	2	32	.14	.311	12	21	.29	160	.10	2	2.66	.02	.11	1	1
0+00 1+75N	1	15	22	178	.3	28	8	194	2.56	10	5	ND	4	15	1	2	2	38	.16	.144	14	25	.36	213	.12	3	2.99	.02	.10	1	1
0+00 1+50N	1	14	19	151	.2	25	8	471	2.47	4	5	ND	4	25	1	2	2	37	.37	.269	14	22	.34	273	.11	2	2.57	.02	.13	1	1
0+00 1+25N	1	13	20	172	.1	26	8	196	2.54	8	5	ND	4	22	1	2	3	41	.31	.232	14	23	.34	229	.12	2	2.96	.02	.12	2	1
0+00 1+00N	1	10	22	223	.1	18	7	950	2.15	5	5	ND	3	20	1	2	2	35	.25	.345	12	20	.25	381	.10	3	2.01	.02	.10	1	1
0+00 0+75N	2	14	21	288	.7	30	7	329	2.29	5	5	ND	5	22	1	2	5	37	.24	.223	17	21	.35	251	.10	2	2.34	.02	.14	1	3
0+00 0+50N	1	20	43	291	.1	28	9	968	2.42	12	5	ND	5	21	1	4	2	40	.22	.318	15	22	.38	409	.10	2	2.32	.02	.16	1	4
0+00 0+25N	1	27	86	324	2.8	24	7	2492	2.31	8	5	ND	2	33	2	7	3	37	.50	.265	13	20	.34	404	.10	2	2.00	.02	.14	1	7
0+00 0+00	2	25	29	110	.1	31	8	251	2.50	7	5	ND	9	20	1	4	3	45	.20	.030	29	29	.50	95	.09	15	1.15	.01	.18	2	1
0+00 0+25S	2	35	95	418	.2	37	9	901	2.85	17	5	ND	4	28	1	2	2	47	1.09	.258	18	23	.65	236	.11	2	2.64	.02	.16	1	4
0+00 0+50S	2	28	26	178	.1	41	13	501	3.59	9	5	ND	8	28	1	2	2	53	.66	.083	31	25	.79	224	.10	2	2.72	.02	.17	1	1
0+00 0+75S	1	23	29	97	.1	47	16	528	4.43	8	5	ND	12	38	1	3	2	28	.60	.052	37	23	.80	149	.06	2	2.41	.02	.13	1	13
0+00 1+00S	1	25	31	85	.1	41	18	388	4.47	9	5	ND	16	42	1	3	2	22	.39	.043	41	19	.57	129	.06	2	2.42	.02	.08	1	10
0+00 1+25S	1	30	14	112	.1	39	14	592	4.11	5	5	ND	9	33	1	2	2	37	.32	.079	33	22	.53	224	.11	13	3.44	.02	.11	1	1
0+00 1+50S	1	25	24	141	.1	35	12	548	3.36	9	5	ND	7	23	1	2	2	39	.21	.157	20	22	.45	290	.13	10	3.50	.02	.13	2	2
0+00 1+75S	1	17	19	192	.3	41	9	296	2.77	9	5	ND	6	29	1	2	2	39	.36	.160	17	27	.39	232	.13	2	3.04	.02	.16	2	1
0+00 2+00S	1	20	26	186	.2	40	9	1088	2.82	10	5	ND	5	34	1	2	3	41	.33	.188	18	29	.41	378	.13	15	2.96	.02	.21	2	1
0+00 2+25S	1	17	16	199	.2	37	8	628	2.51	7	5	ND	3	33	1	2	3	36	.38	.208	15	27	.35	357	.10	10	2.25	.02	.17	1	1
0+00 2+50S	1	25	14	135	.2	38	11	352	2.76	11	5	ND	6	26	1	3	2	43	.29	.108	22	32	.44	243	.11	2	2.43	.02	.24	1	1
0+00 2+75S	1	18	13	152	.4	35	9	245	2.59	11	5	ND	6	22	1	2	2	39	.24	.131	20	26	.39	231	.12	2	2.43	.02	.17	2	9
0+00 3+00S	1	22	20	150	.3	42	10	248	2.86	9	5	ND	7	21	1	2	3	43	.25	.112	21	32	.46	226	.12	2	2.88	.02	.20	1	1
0+00 3+25S	1	13	17	219	.1	36	9	761	2.56	10	5	ND	4	23	1	2	2	37	.26	.182	18	30	.41	300	.10	9	2.00	.01	.18	1	2
0+00 3+50S	1	22	17	168	.2	44	10	295	2.90	10	5	ND	6	24	1	2	2	44	.30	.163	19	31	.48	213	.12	11	2.73	.02	.21	1	1
0+00 3+75S	1	30	21	178	.3	38	10	340	2.91	11	5	ND	7	27	1	2	2	45	.34	.129	22	31	.48	228	.12	15	2.70	.02	.20	1	2
0+00 4+00S	1	25	24	156	.3	33	10	319	2.94	20	5	ND	7	23	1	2	2	43	.26	.198	19	30	.45	243	.13	2	3.06	.02	.19	1	1
0+00 4+25S	1	25	18	187	.1	34	9	395	2.75	10	5	ND	6	25	1	2	2	41	.27	.182	20	28	.44	299	.13	2	2.45	.02	.16	1	1
0+00 4+50S	1	20	15	191	.1	24	9	499	2.60	13	5	ND	4	25	1	2	2	36	.29	.313	16	23	.36	221	.11	12	2.68	.02	.14	1	1
0+00 4+75S	1	21	19	160	.3	31	9	377	2.74	13	5	ND	6	22	1	2	2	41	.28	.202	18	29	.45	235	.11	3	2.49	.02	.16	2	1
L1+00E 3+50N	1	27	24	158	.5	29	8	293	2.67	11	5	ND	5	21	1	5	2	37	.38	.293	13	22	.42	219	.13	2	3.90	.02	.10	1	1
L1+00E 3+25N	1	13	20	251	.2	27	7	339	2.45	9	5	ND	4	30	1	4	2	34	.50	.198	13	26	.43	177	.10	2	2.88	.02	.11	1	5
L1+00E 3+00N	1	16	15	238	.3	26	7	781	2.57	9	5	ND	4	37	1	2	2	40	.56	.055	16	28	.50	196	.11	2	2.76	.02	.20	1	2
L1+00E 2+75N	1	30	17	216	.8	37	9	720	2.96	11	5	ND	4	41	1	2	2	43	.64	.040	22	36	.61	257	.13	2	3.39	.03	.21	1	1
L1+00E 2+50N	1	18	13	178	.6	25	8	248	2.42	8	5	ND	5	17	1	3	2	36	.26	.322	12	25	.32	162	.11	2	3.39	.02	.14	1	1
L1+00E 2+25N	1	14	12	153	.4	26	7	311	2.26	3	5	ND	4	16	1	2	2	33	.20	.187	15	23	.35	153	.11	2	2.82	.02	.10	1	3
L1+00E 2+00N	1	16	14	192	.5	26	8	206	2.40	4	5	ND	3	19	1	2	2	35	.26	.210	13	24	.36	211	.11	2	3.00	.02	.12	1	2
L1+00E 1+75N	1	11	12	129	.2	15	6	582	2.07	5	5	ND	2	15	1	2	2	31	.19	.247	12	21	.26	189	.09	2	1.76	.01	.10	1	3
L1+00E 1+50N	1	17	11	148	.5	29	7	282	2.23	10	5	ND	4	19	1	2	2	34	.25	.124	16	25	.39	207	.09	2	2.09	.01	.11	1	2
L1+00E 1+25N	1	13	10	208	.3	28	7	601	2.19	7	5	ND	2	18	1	2	2	30	.18	.287	12	21	.30	299	.10	2	2.35	.02	.12	1	1
L1+00E 1+00N	1	12	12	191	.2	26	7	531	2.27	9	5	ND	4	21	1	3	2	31	.21	.266	12	23	.32	257	.11	2	2.65	.02	.12	1	1
L1+00E 0+75N	1	19	8	162	.5	30	7	242	2.34	8	5	ND	4	20	1	3	2	32	.23	.204	15	24	.36	262	.12	2	2.87	.02	.13	1	3
L1+00E 0+50N	2	21	16	85	.1	31	8	252	2.31	8	5	ND	6	19	1	4	2	39	.30	.064	26	39	.60	156	.10	8	1.31	.02	.19	1	29
L1+00E 0+25N	1	18	11	215	.4	26	6	430	2.17	5	5	ND	4	32	1	3	2	29	.38	.276	14	23	.32	279	.11	2	2.61	.03	.15	1	1
L1+00E BLO	2	13	19	132	.2	20	5	212	1.85	2	5	ND	5	21	1	2	3	34	.28	.098	20	21	.36	194	.06	8	1.17	.01	.14	1	1

LACANA MINING PROJECT-6101 FILE # 88-1686

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L1+00E 0+25S	1	36	69	370	1.1	32	10	685	2.97	8	5	ND	5	24	1	2	2	31	1.29	.088	22	32	1.29	247	.10	2	2.56	.02	.20	1	1
L1+00E 0+50S	1	22	27	194	.8	31	7	456	2.33	5	5	ND	4	25	1	2	2	37	.29	.205	16	28	.52	266	.09	3	2.22	.02	.21	1	1
L1+00E 0+75S	1	22	25	132	.1	37	13	977	3.94	10	5	ND	9	56	1	2	2	34	.76	.122	29	25	.65	215	.09	2	2.86	.02	.23	1	1
L1+00E 1+00S	1	14	22	217	.1	28	10	1750	3.63	11	5	ND	7	50	1	2	2	30	.39	.269	15	23	.35	394	.10	2	2.69	.02	.16	1	1
L1+00E 1+25S	1	17	20	155	.1	39	10	757	2.92	7	5	ND	5	23	1	2	2	38	.23	.123	14	30	.47	261	.12	9	3.11	.02	.18	1	2
L1+00E 1+50S	1	19	21	163	.3	32	7	453	2.67	9	5	ND	5	28	1	2	2	37	.28	.181	16	27	.42	221	.12	4	2.86	.02	.17	1	1
L1+00E 1+75S	1	11	23	145	.2	32	11	754	3.50	4	5	ND	5	22	1	3	2	30	.21	.087	19	21	.51	208	.08	2	2.28	.01	.12	1	1
L1+00E 2+00S	1	21	31	133	.1	44	14	490	4.35	13	5	ND	11	32	1	2	2	28	.33	.121	31	18	.41	207	.10	2	3.00	.02	.11	1	1
L1+00E 2+25S	1	20	21	157	.2	36	11	473	3.28	7	5	ND	6	26	1	2	2	36	.26	.106	19	29	.63	272	.10	6	3.14	.02	.18	1	1
L1+00E 2+50S	1	14	20	173	.4	31	7	557	2.47	8	5	ND	4	27	1	2	3	34	.29	.184	15	25	.42	266	.10	2	2.42	.02	.18	1	1
L1+00E 2+75S	1	21	20	153	.3	30	7	366	2.61	9	5	ND	5	30	1	2	2	34	.28	.184	18	25	.45	283	.12	8	3.01	.03	.21	1	2
L1+00E 3+00S	1	12	19	220	.3	22	8	1065	2.35	8	5	ND	3	27	1	2	2	31	.24	.248	12	22	.30	339	.11	6	2.28	.02	.15	1	6
L1+00E 3+25S	1	15	22	140	.5	31	8	516	2.72	10	5	ND	5	27	1	2	2	35	.26	.254	15	28	.46	290	.11	2	2.92	.02	.17	1	1
L2+00E 3+00N	1	25	34	162	.1	29	9	729	2.63	15	5	ND	6	32	1	4	2	41	.59	.051	22	31	.51	193	.10	5	2.41	.02	.18	2	1
L2+00E 2+75N	1	25	11	173	.1	31	10	868	2.70	14	5	ND	4	42	1	2	3	41	.76	.025	25	34	.57	180	.10	7	2.63	.03	.12	2	2
L2+00E 2+50N	1	25	20	114	.2	31	8	373	2.58	11	5	ND	7	36	1	2	2	40	.55	.051	24	32	.54	152	.08	4	1.87	.03	.14	1	4
L2+00E 2+25N	1	29	27	170	.4	31	9	591	2.80	10	5	ND	5	36	1	2	3	43	.61	.028	21	39	.62	205	.11	5	2.71	.03	.14	1	2
L2+00E 2+00N	2	37	21	251	.5	42	11	576	3.36	14	5	ND	6	28	1	2	2	51	.45	.243	20	42	.55	301	.12	2	4.23	.02	.23	1	1
L2+00E 1+75N	1	18	18	177	.3	29	9	408	2.46	7	5	ND	4	19	1	2	2	36	.29	.193	14	26	.39	257	.12	2	2.88	.02	.11	2	2
L2+00E 1+50N	2	25	18	180	.4	34	9	278	2.59	4	5	ND	5	23	1	4	2	38	.27	.172	17	26	.41	215	.14	2	3.81	.02	.12	2	1
L2+00E 1+25N	1	16	23	175	.3	28	8	217	2.28	7	5	ND	6	24	1	2	2	33	.31	.165	13	22	.37	206	.11	2	2.60	.02	.11	1	1
L2+00E 1+00N	1	19	5	184	.1	32	8	269	2.46	8	5	ND	5	21	1	2	3	37	.25	.200	15	26	.42	223	.11	2	2.77	.02	.10	1	1
L2+00E 0+75N	1	21	14	160	.7	29	9	263	2.47	9	5	ND	7	24	1	2	6	39	.28	.136	26	29	.44	225	.11	2	2.77	.02	.15	1	2
L2+00E 0+50N	1	13	17	187	.1	26	8	660	2.15	4	5	ND	5	24	1	2	3	35	.26	.117	18	27	.41	265	.09	2	1.80	.01	.11	1	2
L2+00E 0+25N	1	25	7	79	.1	24	9	233	2.46	2	5	ND	7	22	1	2	2	44	.25	.045	24	24	.63	116	.10	4	1.36	.01	.15	1	3
L2+00E 0+00	1	17	17	179	.1	31	8	455	2.31	4	5	ND	3	30	1	2	2	34	.30	.284	16	22	.40	310	.10	13	2.64	.02	.16	1	1
L2+00E 0+25S	1	24	25	152	.2	37	13	389	2.63	9	5	ND	7	21	1	2	2	43	.32	.107	24	43	.67	227	.11	8	1.95	.02	.23	5	1
L2+00E 0+50S	1	24	24	117	.1	34	10	231	2.59	7	5	ND	6	19	1	2	2	44	.29	.057	24	39	.66	207	.11	3	1.91	.02	.21	3	2
L2+00E 0+75S	1	29	18	156	.3	41	11	248	2.63	10	5	ND	8	30	1	2	2	43	.34	.163	18	33	.54	250	.10	2	2.41	.02	.17	4	2
L2+00E 1+00S	1	17	19	132	.1	42	12	648	3.41	4	5	ND	6	25	1	2	2	35	.21	.116	20	24	.60	248	.12	4	3.39	.02	.12	1	1
L2+00E 1+25S	1	18	17	120	.1	36	9	672	2.79	5	5	ND	6	28	1	4	2	34	.25	.147	17	26	.50	265	.11	3	2.71	.02	.12	1	2
L2+00E 1+50S	1	22	22	148	.1	41	12	915	3.75	8	5	ND	8	35	1	2	2	32	.32	.100	24	21	.34	269	.08	2	2.68	.02	.12	1	2
L2+00E 1+75S	1	29	19	122	.1	39	11	811	3.48	8	5	ND	8	28	1	2	2	32	.25	.075	26	22	.36	200	.10	7	2.60	.02	.13	1	1
L2+00E 2+00S	2	23	19	130	.1	40	12	554	3.77	10	5	ND	10	25	1	2	2	38	.26	.068	26	28	.52	176	.09	6	2.53	.01	.14	2	4
L3+00E 2+50N	1	19	22	139	.4	27	9	177	2.56	10	5	ND	6	16	1	2	2	33	.18	.171	12	23	.30	196	.11	2	3.53	.02	.08	1	1
L3+00E 2+25N	1	11	15	145	.2	29	8	217	2.57	9	5	ND	5	20	1	2	2	40	.29	.044	14	28	.43	185	.09	2	2.55	.02	.09	1	1
L3+00E 2+00N	1	34	24	182	.5	34	11	314	3.10	10	5	ND	7	20	1	1	2	46	.23	.167	16	29	.49	202	.15	2	4.80	.02	.10	1	1
L3+00E 1+75N	1	22	22	183	.5	32	9	494	2.76	11	5	ND	6	24	1	2	2	37	.32	.135	16	29	.42	226	.11	3	3.26	.02	.13	1	1
L3+00E 1+50N	1	27	17	161	.4	31	10	176	2.67	9	5	ND	6	15	1	2	2	39	.23	.112	14	31	.39	189	.11	2	3.16	.02	.12	1	1
L3+00E 1+25N	1	39	26	245	.6	43	11	581	3.32	13	5	ND	7	27	1	2	2	50	.43	.253	19	42	.49	308	.12	2	4.38	.02	.21	1	1
L3+00E 1+00N	1	15	20	197	.3	27	9	258	2.42	5	5	ND	5	16	1	3	2	33	.21	.265	13	26	.32	221	.10	8	2.84	.02	.10	1	3
L3+00E 0+75N	1	15	16	171	.3	29	7	250	2.35	3	5	ND	5	21	1	2	2	34	.26	.180	15	25	.35	213	.10	2	2.89	.02	.11	1	1
L3+00E 0+50N	1	15	16	152	.2	25	8	437	2.14	3	5	ND	5	22	1	2	2	34	.26	.101	19	27	.38	228	.08	2	1.76	.01	.14	1	1
L3+00E 0+25N	1	24	29	110	.3	25	10	248	2.38	5	5	ND	7	21	1	2	2	39	.24	.080	24	28	.48	158	.09	5	1.96	.02	.14	1	2
L3+00E BL0	1	19	13	160	.4	29	10	399	2.39	8	5	ND	6	23	1	3	2	36	.29	.190	18	33	.47	257	.09	7	2.25	.02	.19	2	1
L3+00E 0+25S	1	23	23	191	.1	31	9	396	2.89	10	5	ND	9	16	1	2	2	39	.17	.243	15	28	.42	256	.12	11	3.47	.02	.15	1	1

LACANA MINING PROJECT-6101 FILE # 88-1686

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+00E 3+50N	1	24	23	158	.4	31	9	458	3.10	2	5	ND	5	22	1	2	2	42	.30	.070	20	27	.42	152	.10	2	2.78	.02	.09	1	2
L5+00E 3+25N	1	26	19	143	.8	29	9	377	3.07	8	5	ND	6	33	1	2	2	45	.50	.027	21	35	.43	209	.10	12	2.92	.02	.11	1	2
L5+00E 3+00N	1	29	20	140	.6	33	9	313	3.18	12	5	ND	5	23	1	2	2	46	.30	.051	20	34	.41	214	.10	2	3.21	.02	.10	2	1
L5+00E 2+75N	1	24	23	183	.3	37	8	593	2.84	18	5	ND	5	27	1	2	2	43	.42	.087	18	38	.43	175	.11	2	3.19	.02	.12	1	1
L5+00E 2+50N	1	18	23	178	.3	33	8	366	2.82	13	5	ND	5	17	1	2	2	41	.23	.197	16	31	.38	170	.11	2	2.97	.02	.10	2	1
L5+00E 2+25N	1	14	16	177	.2	33	8	606	2.69	15	5	ND	4	17	1	2	2	39	.28	.183	15	29	.37	183	.11	5	2.91	.02	.10	1	1
L5+00E 2+00N	1	16	25	200	.2	33	9	316	2.78	16	5	ND	4	18	1	2	2	40	.24	.257	13	27	.37	179	.11	2	3.16	.02	.12	2	2
L5+00E 1+75N	1	19	19	198	.4	36	8	371	2.76	12	5	ND	6	20	1	2	4	39	.26	.110	16	29	.41	224	.12	2	3.21	.02	.11	1	36
L6+00E 5+00N	1	19	23	295	.1	24	9	1512	2.83	4	5	ND	3	30	2	2	3	37	.43	.202	13	20	.38	298	.10	4	2.99	.02	.12	1	1
L6+00E 4+75N	1	14	19	162	.1	19	9	627	2.92	5	5	ND	3	18	1	2	2	40	.20	.175	11	21	.34	229	.11	2	3.43	.02	.07	1	1
L6+00E 4+50N	1	25	27	139	.1	32	10	445	3.35	6	5	ND	6	28	1	2	2	50	.49	.165	19	28	.57	161	.09	2	2.91	.02	.11	1	1
L6+00E 4+25N	1	18	15	219	.5	25	9	272	3.05	3	5	ND	5	21	1	2	2	37	.28	.171	17	25	.45	197	.11	2	3.91	.02	.08	1	2
L6+00E 4+00N	1	33	21	181	.9	32	10	501	3.01	4	5	ND	5	33	1	4	2	38	.63	.040	27	34	.55	209	.10	2	3.15	.02	.16	1	1
L6+00E 3+75N	1	25	25	200	.9	35	10	1389	2.78	13	5	ND	4	38	2	2	4	45	.78	.050	20	38	.45	235	.11	2	3.11	.03	.14	1	1
L6+00E 3+50N	1	21	21	241	.5	32	9	790	2.72	9	5	ND	4	32	1	2	2	42	.49	.105	17	30	.42	227	.11	3	3.16	.02	.13	1	1
L7+00E 4+50N	1	35	23	122	.1	35	14	446	3.63	5	5	ND	8	15	1	2	3	52	.24	.027	31	39	.95	110	.09	2	2.13	.01	.21	1	1
L7+00E 4+25N	1	15	20	247	.4	24	10	523	2.82	3	5	ND	4	17	1	2	2	34	.23	.195	14	23	.44	210	.10	2	3.38	.01	.17	1	2
L7+00E 4+00N	1	36	22	135	1.1	38	11	997	3.32	6	5	ND	7	34	1	2	3	45	.50	.035	23	34	.61	320	.12	2	4.03	.02	.15	1	1
L7+00E 3+75N	1	16	20	185	.3	24	9	279	2.81	7	5	ND	5	18	1	2	2	36	.26	.241	13	23	.38	194	.11	2	3.62	.02	.09	2	1
L7+00E 3+50N	1	13	23	159	.2	25	9	378	2.80	10	5	ND	5	12	1	2	3	37	.13	.298	14	26	.40	217	.10	2	3.02	.01	.10	1	1
L8+00E 4+50N	1	16	23	223	.3	25	9	444	2.68	5	5	ND	4	20	1	3	2	40	.30	.136	16	26	.41	194	.10	2	2.69	.01	.11	1	1
L8+00E 4+25N	1	23	17	193	.8	32	9	274	2.92	11	5	ND	6	21	1	2	2	41	.36	.083	18	28	.43	190	.12	2	3.64	.01	.12	1	1
L8+00E 4+00N	1	21	16	213	.3	28	10	641	2.69	10	5	ND	5	16	1	2	2	42	.20	.184	17	31	.40	226	.10	2	2.81	.01	.12	1	1
L8+00E 3+75N	1	20	16	195	.2	25	8	280	2.47	8	5	ND	6	16	1	2	2	37	.17	.133	14	24	.37	217	.12	10	2.98	.02	.10	1	1
L8+00E 3+50N	1	18	15	191	.5	25	8	533	2.31	7	5	ND	6	18	1	2	2	32	.22	.227	14	23	.34	222	.12	2	2.93	.01	.11	2	1

1988 Rock Sample Assays

APPENDIX II

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-2 ROCK P3 SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: MAY 09 1988 DATE REPORT MAILED: May 13/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

LACANA MINING PROJECT-6101 File # 88-1333 Page 1

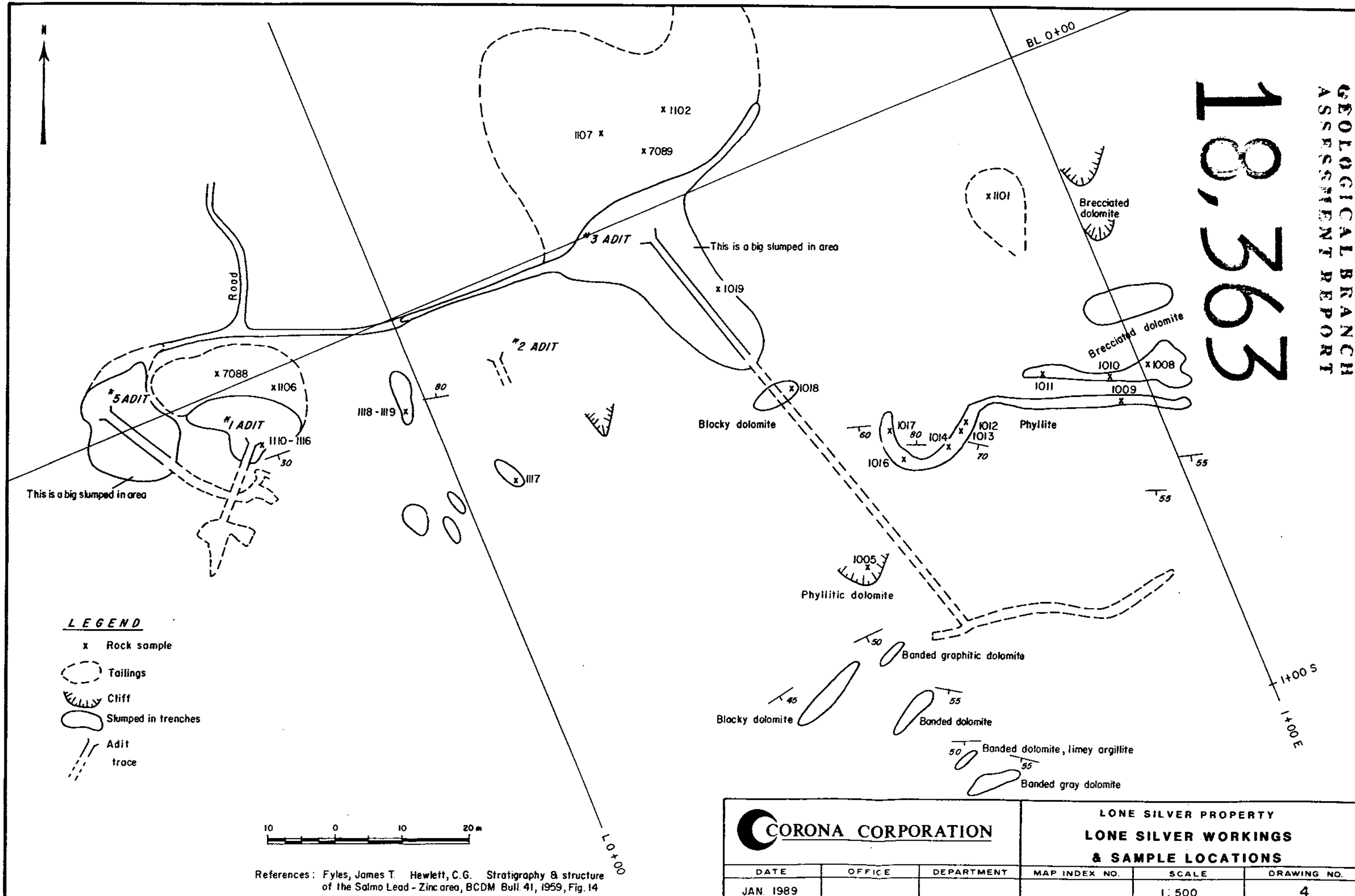
SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
1101	1	7	39	151	6.3	6	1	129	.24	3	5	ND	1	90	1	2	7	21	20.99	.149	5	4	5.96	10	.01	15	.12	.01	.63	1	1
1102	2	116	1733	12120	7.5	3	1	54	.32	6	7	ND	1	2	76	16	2	1	.15	.001	2	2	.06	5	.01	7	.01	.01	.02	2	72
1106	3	2655	133	270	24.7	10	1	205	.80	12	5	ND	1	81	10	42	7	10	16.48	.111	6	2	6.09	16	.01	13	.11	.01	.04	1	151
1107	1	63	18	61	1.1	33	7	430	3.91	10	5	ND	4	78	1	2	2	67	.63	.041	12	196	1.08	96	.28	2	1.26	.08	.71	2	5
1108	4	6	6	11	.3	5	2	4021	1.63	23	5	ND	1	9	1	4	2	2	.06	.008	2	2	.02	37	.01	46	.04	.01	.03	4	1
N 1110	6	174	2373	1773	125.3	3	1	33	.45	17	5	ND	1	9	13	92	2	4	1.26	.015	2	8	.65	4	.01	5	.02	.01	.01	1	56
N 1111	1	14	49	116	1.1	2	1	285	.43	3	5	ND	1	51	1	2	20	13	17.29	.042	2	1	19.50	12	.01	2	.03	.01	.02	1	1
N 1112	1	4	12	11	.8	2	1	221	.48	2	5	ND	1	622	1	2	2	1	15.14	.001	2	4	.19	3	.01	12	.03	.01	.01	1	1
N 1113	251	253	44425	592	542.5	4	3	261	.83	60	5	ND	1	36	7	619	2	18	2.09	.009	2	9	1.24	17	.01	4	.05	.01	.01	1	250
N 1114	3	37	323	264	10.9	3	1	325	.51	5	5	ND	1	54	2	18	18	30	17.38	.054	2	1	19.34	4	.01	2	.05	.01	.01	1	6
N 1115	2	7	252	29	4.3	2	1	254	.44	3	5	ND	1	56	1	2	24	12	17.49	.132	2	1	13.31	12	.01	2	.07	.01	.02	1	1
N 1116	2	3	32	31	.5	5	1	227	.37	2	5	ND	1	80	1	2	22	27	17.43	1.295	5	3	16.91	6	.01	9	.25	.01	.05	2	3
N 1117	1	2	22	22	.2	3	1	235	.22	2	5	ND	1	53	1	2	19	9	19.06	.012	2	1	19.27	5	.01	2	.02	.01	.01	1	1
N 1118	1	4	3	48	.3	2	1	147	.16	2	5	ND	1	42	1	2	26	4	18.14	.007	2	1	20.14	6	.01	4	.03	.01	.01	1	1
N 1119	1	65	16	73	.3	19	17	499	4.45	13	5	ND	5	60	1	10	2	24	2.97	.139	16	21	2.21	107	.02	3	2.09	.01	.25	1	3
STD C/AU-R	20	65	40	133	7.4	73	31	1070	4.13	41	20	8	39	53	19	20	21	54	.49	.094	40	57	.97	183	.08	35	1.67	.07	.14	11	490
N 1005	2	2424	17340	71607	474.5	3	4	173	.52	39	5	ND	1	9	593	515	2	1	.11	.004	2	3	.05	127	.01	2	.01	.01	.01	23	275
N 1006	1	24	377	470	1.0	32	10	331	2.37	87	5	ND	7	759	4	26	2	5	17.14	.019	22	21	.95	23	.01	2	1.04	.01	.34	1	7
N 1007	1	53	730	532	15.3	5	1	347	.54	3	5	ND	1	68	2	17	14	14	13.76	.024	2	1	12.23	26	.01	2	.32	.01	.01	1	1
N 1008	1	5	44	46	.1	5	1	149	.43	8	5	ND	1	10	1	2	2	1	.39	.001	2	9	.07	3	.01	2	.05	.01	.01	4	1
N 1009	1	20	21	53	.6	7	8	553	3.25	6	5	ND	5	44	1	2	2	23	3.23	.105	16	10	.76	106	.01	3	1.31	.03	.23	1	69
N 1010	1	35	61	265	11.9	4	1	277	.52	4	5	ND	1	46	3	15	2	9	18.06	.016	2	6	3.31	11	.01	2	.01	.01	.01	1	1
N 1011	1	1335	3625	3692	215.9	9	3	760	.65	59	5	ND	1	106	97	517	22	21	16.41	.034	3	2	13.10	12	.01	3	.12	.01	.04	1	23
N 1012	1	42	15	93	.5	5	11	587	3.71	2	5	ND	5	55	1	16	2	44	1.75	.112	17	16	1.05	127	.14	2	1.67	.03	1.02	1	1
N 1013	1	54	36	166	1.5	9	10	747	3.33	2	5	ND	3	38	1	5	2	56	.93	.113	13	17	1.27	121	.14	2	2.03	.03	1.12	1	1
N 1014	2	7	14	27	.2	3	2	676	.30	2	5	ND	1	280	1	2	17	31	13.32	.114	6	4	17.24	15	.01	9	.23	.01	.07	1	1
N 1015	1	7	26	91	.8	5	1	1196	1.12	2	5	ND	1	188	1	2	12	23	19.09	.118	6	1	11.59	52	.01	3	.14	.01	.25	1	4
N 1016	3	13	230	59	1.7	2	1	257	.40	2	5	ND	1	161	2	2	6	13	17.61	.075	5	1	8.36	10	.01	10	.06	.01	.03	1	1
N 1017	1	24	72	136	.6	12	2	387	.95	2	5	ND	1	176	1	2	11	26	17.59	.437	11	3	10.80	15	.01	7	.35	.01	.06	1	3
N 1018	1	5	22	38	1.7	3	1	137	.37	2	5	ND	1	74	1	2	20	12	17.92	.035	2	1	20.69	4	.01	2	.03	.01	.02	1	2
N 1019	13	109	77	485	3.4	52	8	402	4.26	24	5	ND	2	151	5	13	4	40	12.74	.690	13	12	.92	141	.01	16	.29	.01	.12	1	1
N 1213	1	1	2	3	.1	1	1	52	.15	2	5	ND	1	226	1	2	2	1	6.20	.001	2	1	.17	1	.01	2	.01	.02	.01	1	1
N 1214	1	3	2	32	.3	20	7	131	1.63	2	5	ND	4	150	1	2	2	3	5.26	.028	14	11	.66	13	.01	2	.75	.01	.11	1	2
N 1215	1	4	2	3	.8	2	1	57	.22	4	5	ND	1	285	1	4	2	1	8.84	.002	4	1	.14	2	.01	2	.03	.02	.10	1	1
S 20816	1	1	2	1	.1	1	1	42	.30	2	5	ND	1	425	1	2	2	1	20.62	.001	7	1	.21	1	.01	2	.01	.01	.01	1	1
N 7088	4	262	118	1700	.9	10	36	375	7.56	5	5	ND	1	51	8	2	2	36	4.55	.040	4	9	1.47	53	.06	8	1.25	.01	.42	1	1
N 7089	2	125	4168	3084	27.0	1	1	126	.30	10	5	ND	1	22	23	20	2	2	1.89	.007	2	4	.93	3	.01	2	.01	.01	.01	1	250
STD C/AU-R	20	63	45	132	7.8	72	31	1111	4.13	42	22	7	39	53	20	17	19	61	.51	.091	39	64	.91	181	.07	34	1.91	.05	.16	13	510

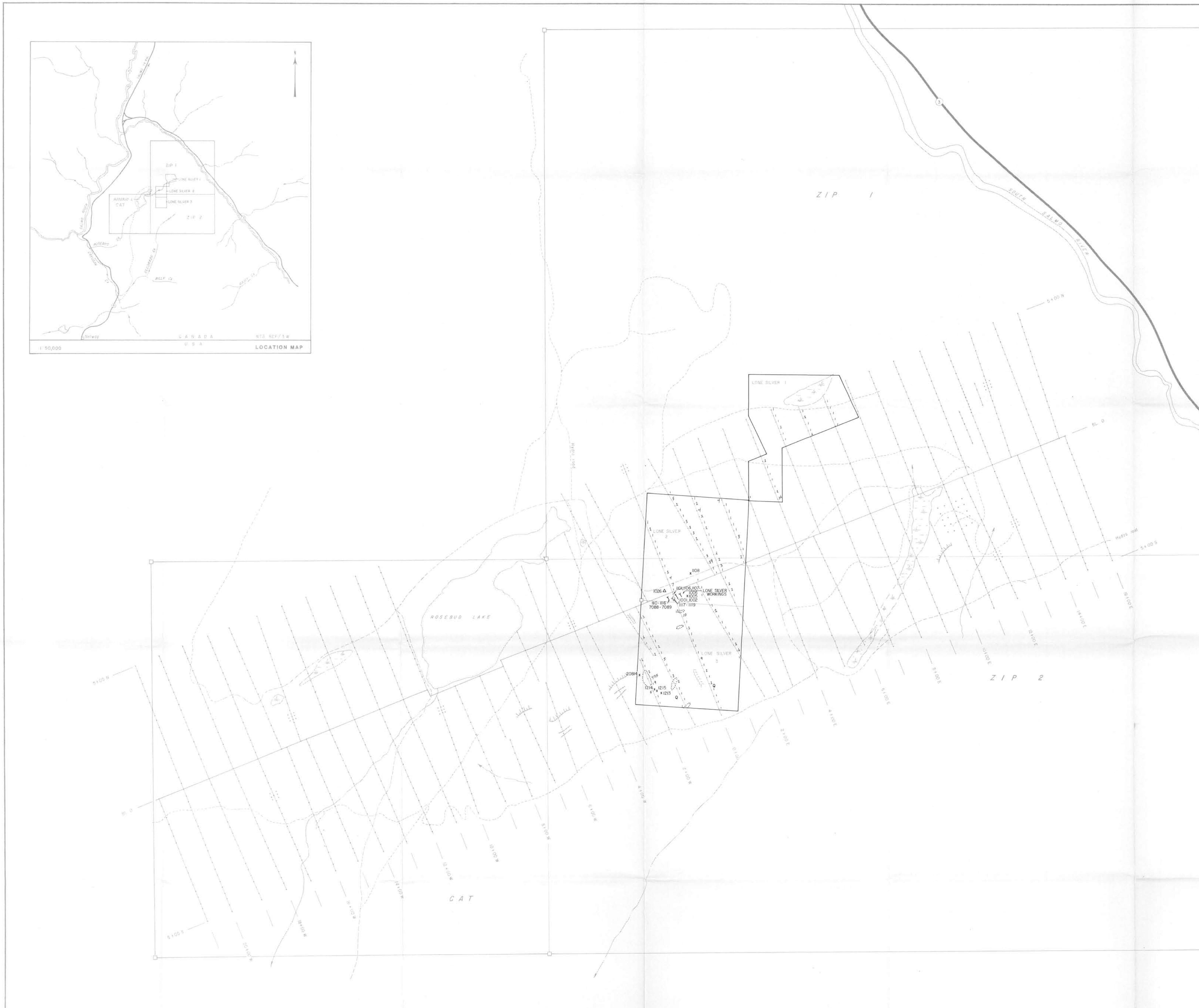
1988 Pan Concentrate Assays

APPENDIX III

LACANA MINING PROJECT-6101 FILE # 88-1686A

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
N 1025	19	121	9526	1129	67.1	16	5	506	1.70	39	5	ND	1	70	9	67	2	35	9.41	.186	10	15	5.24	64	.03	[illegible]	.19	.01	.06	1	1330


N
BL 0+00
L 0+00
1+00 S
1+00 E
Road
#5 ADIT
#1 ADIT
#2 ADIT
#3 ADIT
x 7088
x 1106
1110 - 1116
1118 - 1119
1117
x 1102
1107 x
x 7089
x 1101
x 1019
1018
1005
1010
x 1008
1011
1009
1017
1014
1012
1013
1016
This is a big slumped in area
This is a big slumped in area
Brecciated dolomite
Brecciated dolomite
Blocky dolomite
Phyllite
Phyllitic dolomite
Banded graphitic dolomite
Blocky dolomite
Banded dolomite
Banded dolomite, limey argillite
Banded gray dolomite
30
80
60
80
70
55
55
50
45
55
50
55
LEGEND
x Rock sample
Tailings
Cliff
Slumped in trenches
Adit
trace
10 0 10 20 m
References: Fyles, James T. Hewlett, C.G. Stratigraphy & structure of the Salmo Lead - Zinc area, BCDM Bull. 41, 1959, Fig. 14
CORONA CORPORATION
LONE SILVER PROPERTY
LONE SILVER WORKINGS
& SAMPLE LOCATIONS
DATE
JAN. 1989
OFFICE
DEPARTMENT
MAP INDEX NO.
SCALE
1 : 500
DRAWING NO.
4



GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,363

× ROCK SAMPLE
OUTCROP
▲ SILT SAMPLE
SOIL SAMPLE (Au ppb)

MAP SCALE: 100 0 100 200 300m

NTS 82F/3W

No	Date	MADE BY	DESCRIPTION
1			
2			
3			
4			
5			

DATE	DRAWN BY	CHECKED	APPROVED
JAN 1989	J.V.V		

CORONA CORPORATION

OFFICE	DEPARTMENT

LONE SILVER 1,2,3 CLAIMS

SAMPLE LOCATIONS & SOIL GRID

MAP INDEX NUMBER	SCALE	DRAWING NUMBER
	1:5000	3