

ARIS SUMMARY SHEET

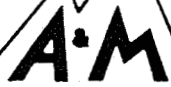
District Geologist, Nelson

Off Confidential: 89.11.16

ASSESSMENT REPORT 18478

MINING DIVISION: Nelson

PROPERTY: June
LOCATION: LAT 49 16 00 LONG 117 23 00
UTM 11 5456952 472111
NTS 082F06W
CLAIM(S): June, Rockford, Ontario, West Minster, St. Louis, Gordon, Monte Carlo
OPERATOR(S): Kootenay King Res.
AUTHOR(S): Allen, D.G.
REPORT YEAR: 1988, 94 Pages
COMMODITIES
SEARCHED FOR: Molybdenum/Molybdenite, Copper, Lead, Zinc, Silver
KEYWORDS: Hall Formation, Rossland Formation, Sediments, Volcanics, Dyke swarm
Fractures, Quartz veins, Pyrite, Pyrrhotite, Chalcopyrite, Galena
Sphalerite, Molybdenite, Scheelite
WORK
DONE: Geochemical, Physical
LINE 3.6 km
SOIL 351 sample(s) ;ME
MINFILE: 082FSW213, 082FSW226, 082FSW300, 082FSW301



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FILE NO:	

SUMMARY REPORT

on the

ERIE CREEK PROPERTY

Nelson Mining Division - British Columbia

Lat. 49° 16' N.

Long. 117° 23' W.

N.T.S. 82 F/6W

FILMED

for

KOOTENAY KING RESOURCES INC.

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

SUB-RECORDER RECEIVED FEB 20 1989 M.R. # \$ VANCOUVER, B.C.

18,478

by

Donald G. Allen, P. Eng. (B.C.)

August 9, 1988

Vancouver, B.C.

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SUMMARY

Kootenay King Resources Inc. holds 107 claim units which cover a molybdenum-copper-tungsten-lead-zinc-silver + gold prospect in the Erie Creek area of southeastern British Columbia. In 1987, the company conducted an exploration program comprising line cutting, prospecting and geochemical surveys on the property. Results of this work are summarized in this report.

The property is situated 11 kilometres northwest of Salmo and is accessible by good logging road. Nine of the 25 largest gold producers in British Columbia, in terms of past production, lie within 25 kilometres of the property.

The Erie Creek prospect is centered on a complex swarm of porphyritic acid to basic dikes of Eocene age which intrude sedimentary and volcanic rocks of the Hall and Rossland Formations, both of Jurassic age. The dike complex extends northward and southward for a total distance of 17 kilometres and is six kilometres wide. Mineralization on the property occurs in four concentric zones:

- 1) an inner zone of molybdenite + scheelite (tungsten) mineralization which occurs in fracture and quartz vein stockworks;
- 2) a surrounding zone of chalcopyrite + scheelite in fracture zones and shear veins;
- 3) an outer zone of galena-sphalerite-chalcopyrite + gold shear veins; and
- 4) a widespread zone of disseminated and fracture controlled pyrite and pyrrhotite.

The property has had a long history dating back to the late 1890's. The numerous mineralized shear zones have been explored by prospect pits, shafts and adits. The molybdenum-copper potential has been investigated in recent years by McIntyre Porcupine Mines and AMAX Exploration Ltd. (now Canamax Resources Inc.). Their work to date has included geological, geochemical and geophysical surveys and 2778 metres of diamond drilling in 15 holes. However, surveys to date have not fully delineated or tested the lead-zinc-silver zone. Silver values of

fully delineated or tested the lead-zinc-silver zone. Silver values of up to 7.8 ounces per ton have been reported from shear veins and values of 1.2 ounces per ton have been reported in one of McIntyre Porcupine's drill holes.

Exploration work conducted by Kootenay King has identified gold values of up to 0.045 ounces per ton in some shear veins. Also identified is a prominent silver-lead-zinc anomaly with scattered gold, copper and arsenic anomalies in soils of the northwestern part of the claim group. A follow-up exploration program is proposed to evaluate these anomalies.

CONCLUSION

The Erie Creek prospect is a zoned porphyry-type deposit with a central quartz vein stockwork zone containing molybdenum-copper-tungsten mineralization, and a peripheral zone with veins containing copper, lead, zinc and silver mineralization.

Soil geochemical surveys to date have partly defined the peripheral zone, particularly in the northwestern part of the claim group where widespread silver, lead, zinc anomalies, weaker copper and arsenic anomalies and scattered gold anomalies have been obtained.

A modest follow-up exploration program is warranted to identify the source of the anomalies. The survey area is underlain by volcanic and sedimentary rocks which are potentially favourable hosts for stratabound base metal mineralization. Also underlying part of the area is a lobe of the Nelson batholith, the contact area of which might be a favourable locus for epigenetic mineralization.

In addition, other lower priority targets remain as suggested by Canamax. Should molybdenum tungsten and copper prices improve, then a possible target would be a buried high grade ($\pm 0.4\%$ MoS_2 equivalent) at depths greater than 200 metres below the Erie Creek valley floor. Other targets are low-grade tungsten in calc-silicate hornfels on the west side of Erie Creek and silver-bearing hydrothermal breccias beneath Erie Creek.

RECOMMENDATION

A two phase exploration program is recommended to further evaluate the Erie Creek property. Phase I will comprise prospecting, mapping, trenching, and rock sampling (1) to evaluate the multi-element geochemical anomalies obtained in the northwest part of the claim group and (2) to conduct additional sampling and geochemical surveys to fully define the area of interest on the Ben Hassen showing. A few more widely spaced geochemical survey lines should be established in order to fully outline the silver-lead-zinc zone. Should results be favourable, then a Phase II program of trenching and diamond drilling will be warranted.

ESTIMATED COSTS OF RECOMMENDATIONPHASE I Prospecting, mapping, trenching and rock sampling.

Salaries

Geologist	15 man-days @ \$200/day	\$ 3,000
2 Assistant samplers	30 man-days @ \$150/day	4,500
Room and Board	45 man-days @ \$40/day	1,800
Geochemical analyses	250 samples @ \$15 each	3,750
Vehicle rental, transportation		1,000
Bulldozer trenching	50 hrs. @ \$80 all inclusive	4,000
Report		<u>2,000</u>

Subtotal \$20,050

Contingencies 1,950**TOTAL PHASE I \$22,000**PHASE II Diamond drilling.

Drilling	2,000 feet @ \$35/foot all inclusive	\$70,000
Bulldozer	Trenching, road construction, drillsite preparation, land reclamation 100 hours @ \$100/hour	10,000
Engineering, supervision, consulting		7,000
Assays		<u>5,000</u>

Subtotal \$92,000

Contingencies 10,000**TOTAL PHASE II \$102,000****GRAND TOTAL \$124,000**

INTRODUCTION

Kootenay King Resources Inc. holds, by staking and by option from Canamax Resources Inc., 107 claim units in the Erie Creek area near Salmo, in southwestern British Columbia. The claims cover a concentrically zoned molybdenum-tungsten-copper-lead-zinc-silver stockwork and vein system centered on a swarm of acid to basic dikes. The property was acquired by the company for its precious and base metal potential.

The Erie Creek property is one of a large number of important mineral deposits comprising a variety of commodity types in the Nelson-Salmo-Ymir area. Nine of the twenty-five largest gold mines in B.C. (in terms of past production), lie within 25 kilometres of the property. These include the deposits of the Sheep Creek and Ymir gold camps, and the Granite-Poorman, Second Relief and Arlington Mines. Exploration activity in the area has been intense, with companies such as Lectus Development/U.S. Borax having announced new discoveries.

This report, prepared at the request of Mr. Larry Sostad, summarizes results of exploration work carried out by the company during the period 1985 to 1987. Also summarized are results of work carried out prior to 1980 by AMAX Exploration Inc. (now Canamax Resources Inc.) who investigated the property for its potential as a large tonnage low-grade molybdenum-copper-tungsten deposit.

LOCATION AND ACCESS

The Erie Creek property is situated 11 kilometres northwest of Salmo and 25 kilometres southwest of Nelson (see Figures 1 and 2). The claims lie on both sides of Erie Creek near its confluence with Grassy and Craigtown Creeks.

The area is in the Bonnington Range of the Selkirk Mountains. Topography in the claim area is moderately steep but not rugged. Elevations range from 900 to 1,700 metres (3,000 to 5,500 feet). Slopes are covered with a light growth of cedar, balsam fir, Douglas fir,

ERIE CREEK PROPERTY LOCATION MAP

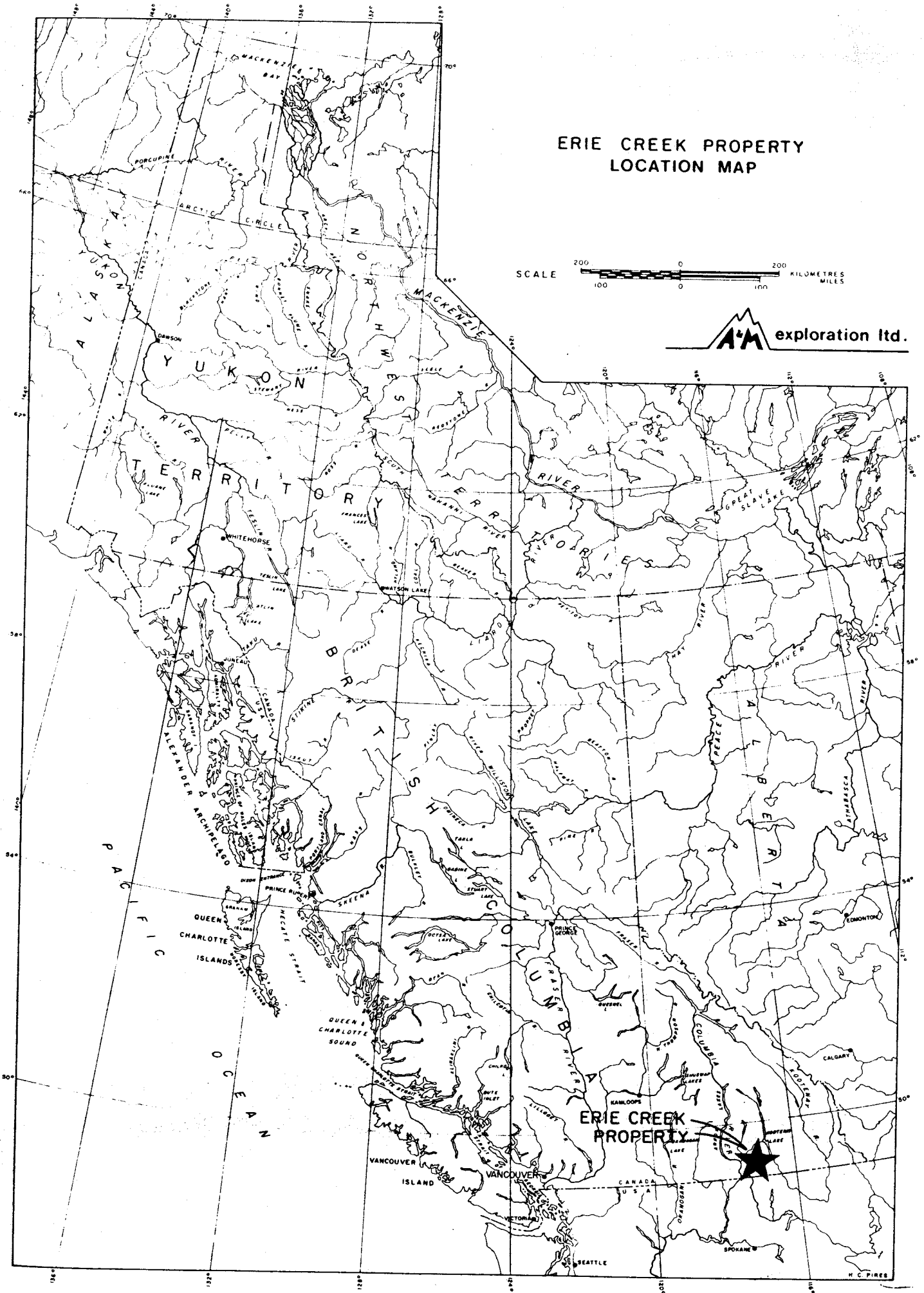
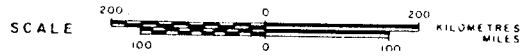


FIGURE - 1

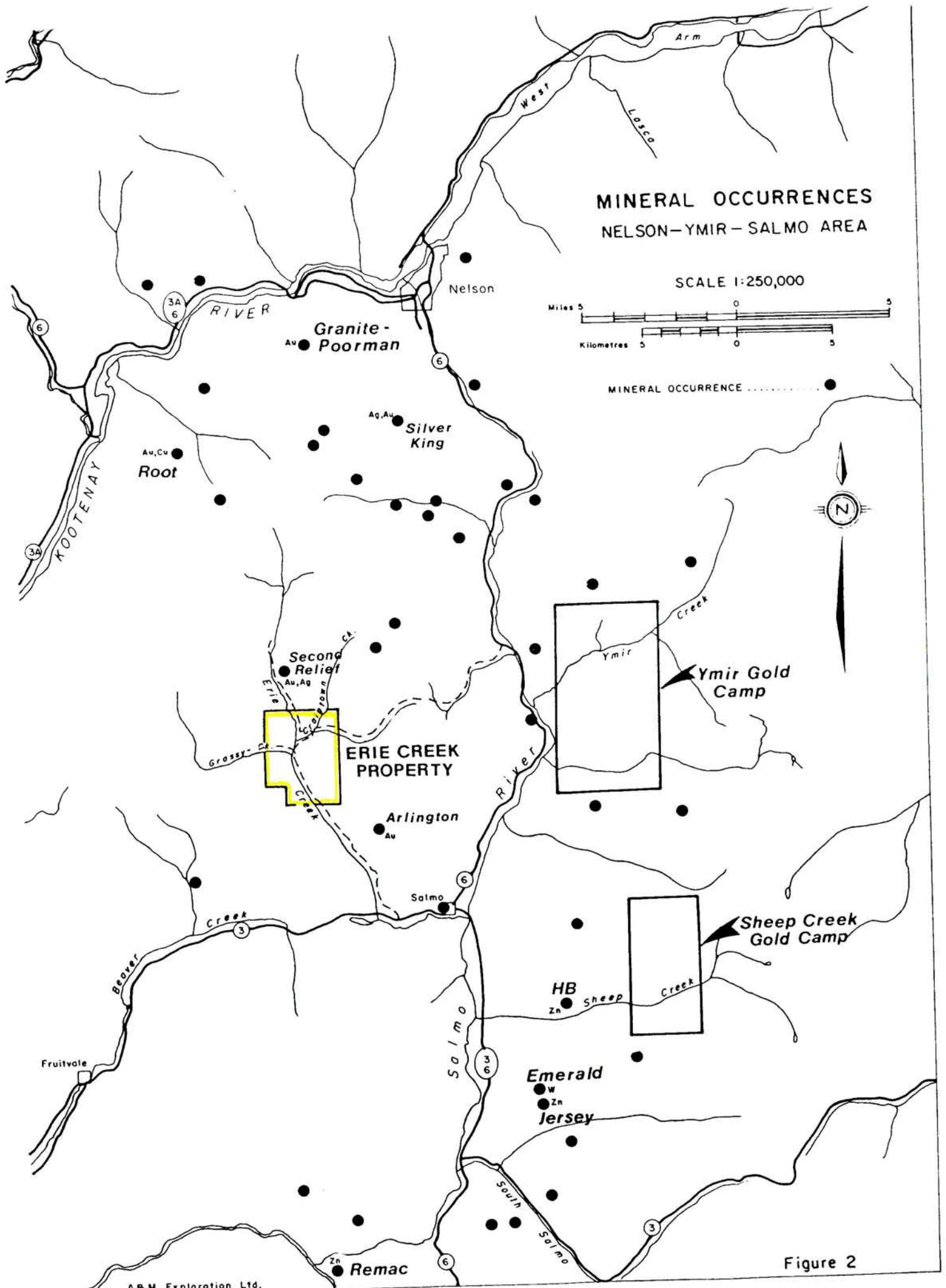


Figure 2

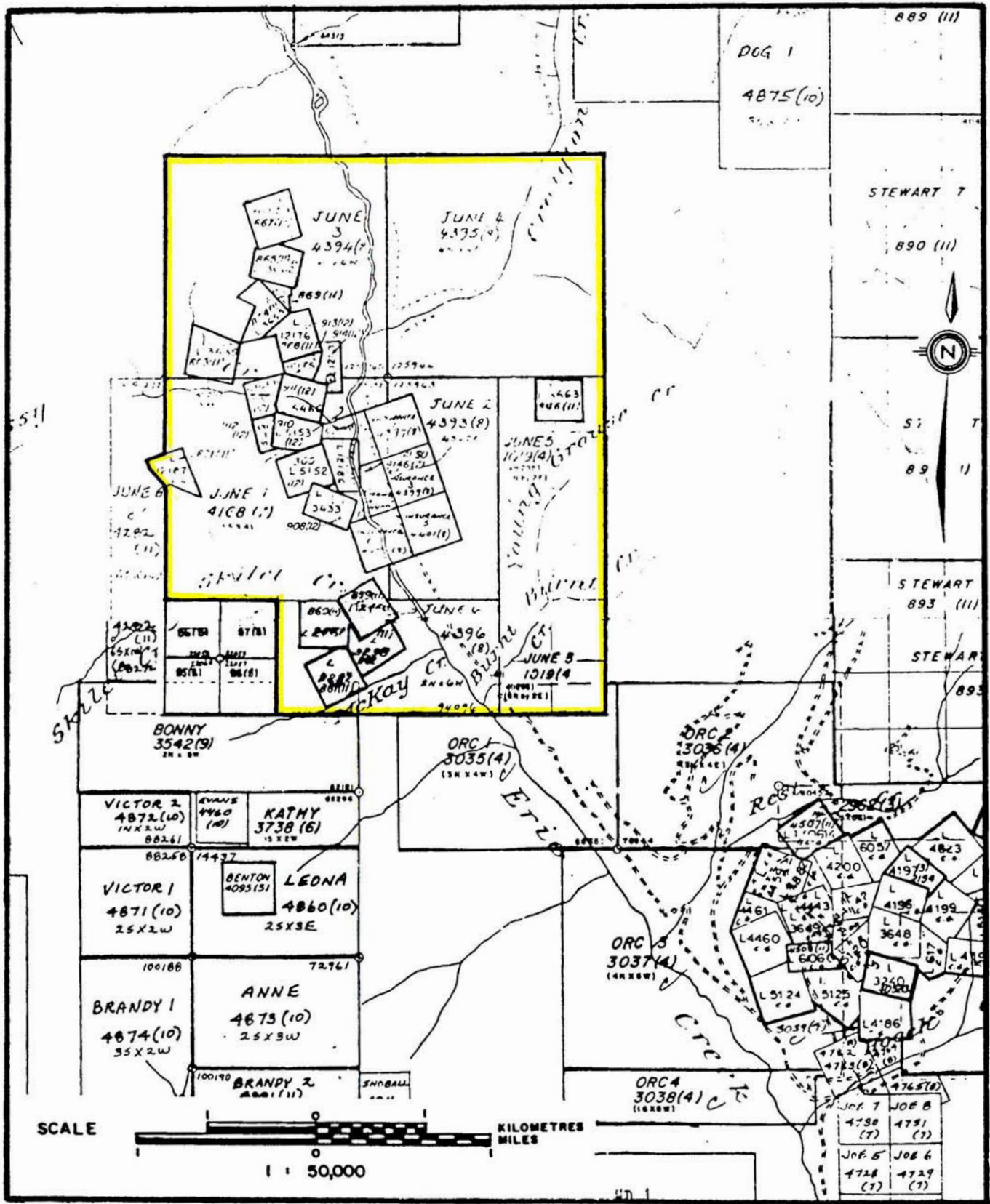
larch, hemlock, poplar and birch with an undergrowth of alder, willow, huckleberry and false azalea.

Access is by a well maintained logging road from Highway 3, about 15 minutes' drive from Salmo.

CLAIM DATA

The Erie Creek property comprises 107 claim units (Figure 3) and are registered in the name of Kootenay King Resources Inc. Claim data are as follows:

<u>CLAIM NAME</u>	<u>RECORD NO.</u>	<u>TYPE</u>	<u>LOT NO.</u>	<u>NO. OF UNITS</u>	<u>EXPIRY DATE</u>
Arnold	867	Rev. Crown Grant	4079	1	Nov. 23, 1988
Belle	860	" "	2461	1	Nov. 23, 1988
Ben Hassan	866	" "	3663	1	Nov. 23, 1988
Bully Boy	862	" "	3238	1	Nov. 23, 1988
Rosa	859	" "	2460	1	Nov. 23, 1988
Copper King	910	" "	5153	1	Dec. 15, 1988
Dora	909	" "	5152	1	Dec. 15, 1988
Drum Lummon	912	" "	5481	1	Dec. 15, 1988
Eddie	870	" "	12186	1	Nov. 23, 1988
Florence	861	" "	3227	1	Nov. 23, 1988
Good Enough	911	" "	5466	1	Dec. 15, 1988
Gordon	913	" "	12175	1	Dec. 15, 1988
Homestake	908	" "	3662	1	Dec. 15, 1988
Louise	871	" "	12187	1	Nov. 23, 1988
Maude S	865	" "	3662	1	Nov. 23, 1988
Monte Carlo	907	" "	1066	1	Dec. 15, 1988
Nelson	914	" "	12177	1	Dec. 15, 1988
Ontario	864	" "	3659	1	Nov. 23, 1988
Rockford	863	" "	3435	1	Nov. 23, 1988
St. Louis	868	" "	13176	1	Nov. 23, 1988
Westminster Fraction	869	" "	12184	1	Nov. 23, 1988
June 1	4168	Mod. Grid.	-	16	July 2, 1989
June 2	4393	" "	-	8	Aug. 11, 1989
June 3	4394	" "	-	16	Aug. 11, 1989
June 4	4395	" "	-	16	Aug. 11, 1989
June 5	1019	" "	-	12	Apr. 18, 1989
June 6	4396	" "	-	12	Aug. 11, 1989
Insurance 1-6	4397-4402	2-post	-	6	Aug. 11, 1989



KOOTENAY KING RESOURCES INC. N.T.S. 82 F/3 W, 6 W

CLAIM MAP

ERIE CREEK PROPERTY

Nelson Mining Division - British Columbia



HISTORY

Mineralization on the property was first explored in the 1890's. Little information is available on the work carried out at that time. In the 1896 B.C. Minister of Mines Annual Report (Carlyle, 1896) brief mention is made of discoveries on the Ben Hassan and Arnold (reverted crown grant) claims.

In 1926 to 1928 Consolidated Mining and Smelting Ltd. conducted diamond drilling on "copper-gold" deposits (O'Grady, 1928) on the Arnold, St. Louis and Drum Lummon claims.

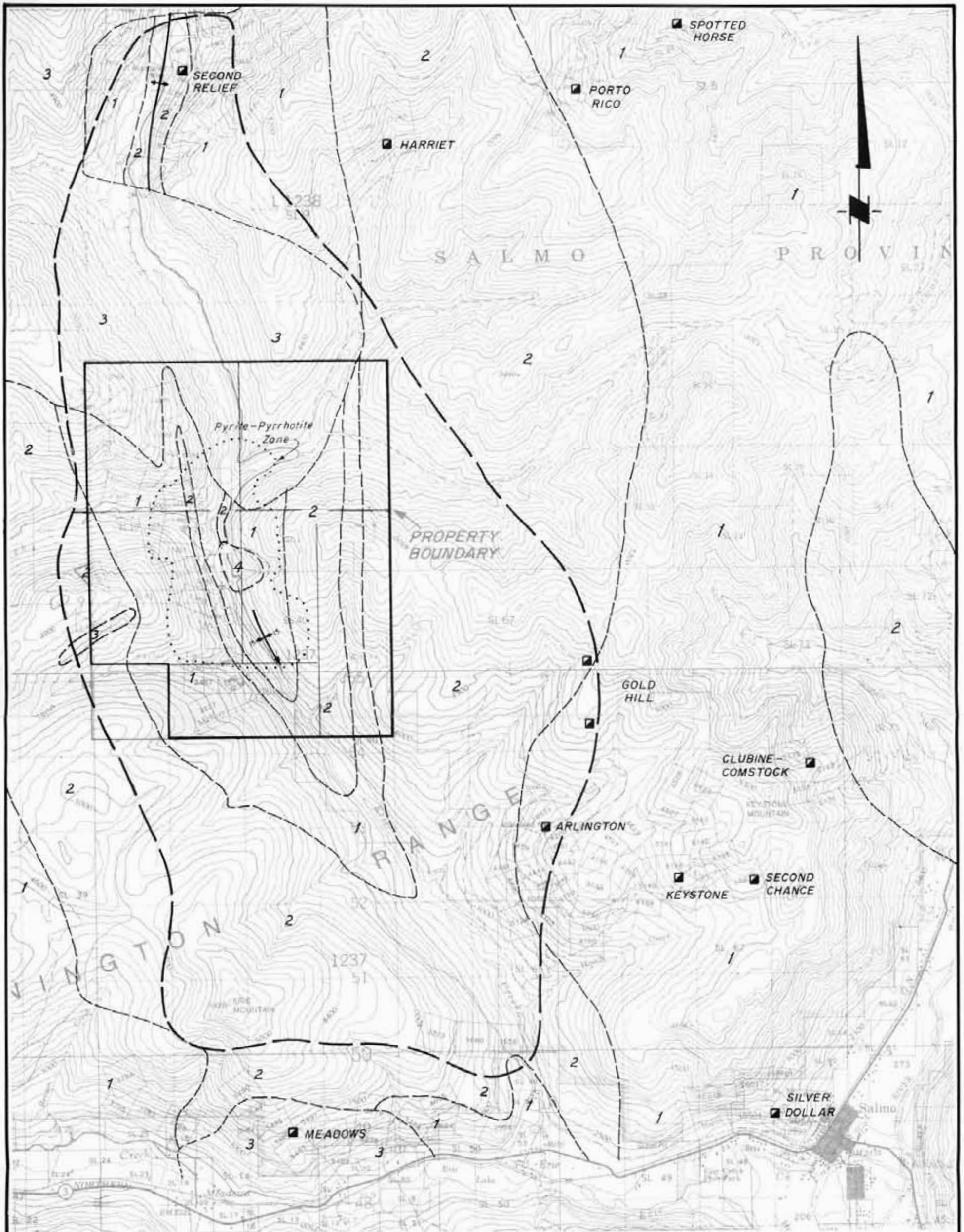
In 1968, the property was held by Canzac Mines Ltd. and optioned to McIntyre Porcupine Mines Ltd. who in 1969 and 1970 conducted 1712 metres of drilling in 12 holes. The best mineralization encountered was 85 metres grading 0.115% MoS_2 and 0.05% copper including a 30 metre section grading 1.2 oz/ton silver. The property was acquired by AMAX who, in 1976 to 1979, conducted detailed geological mapping, geochemical sampling, geophysical surveys and diamond drilling totalling 1066 metres in four holes mainly in the central stockwork zone. Best grades encountered were 17 metres grading 0.06% WO_3 in drill hole 80-4, and 36 metres grading 0.07% MoS_2 in drill hole 79-1.

REGIONAL GEOLOGY

The Erie Creek property is in the Nelson Map-Area of Little (1960) and the Bonnington Map-Area of Walker (1934). Geology of the immediate claim area is summarized on Figure 4.

The property lies near one of the lobes of the 160 m.y. old Nelson batholith. In this area, it is composed of coarse grained porphyritic granodiorite-granite containing numerous white orthoclase phenocrysts in a groundmass of orthoclase, plagioclase and quartz with minor amounts of hornblende and biotite. The granite has intruded sedimentary rocks of the "Sinemurian beds" (Little, 1960) and volcanic rocks of the Rossland Formation, both of Lower Jurassic age.

A complex array of dikes and sills of porphyritic rhyolite, quartz



LEGEND

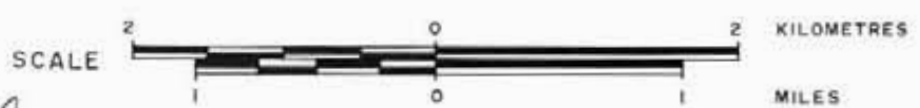
- 4 ERIE CREEK STOCK
- 3 NELSON BATHOLITH - *Porphyritic granodiorite*
- 2 ROSSLAND FORMATION - *Augite porphyritic basalt, volcanic breccia.*
- 1 HALL FORMATION - *Argillite, phyllite.*

SYMBOLS

- Limit of Erie Creek Dyke Complex.
- Approximate geological contact.
- Mine or prospect
- Major fold axis (anticline).

ERIE CREEK PROPERTY
NELSON M. D. - B. C.

REGIONAL GEOLOGY



D.S. Allen

Vancouver -

S.P. & G.T.

latite, dacite, and basalt (Erie Creek dike swarm) occurs in the Erie Creek basin for a distance of at least 17 kilometres, between the Arlington and Second Relief Mines. The swarm is about one kilometre wide. An age determination of 47 million years has been reported by Hodgson et al (1979). Dikes trend north-south and parallel Erie Creek. Abundance of dikes ranges from about three per 100 metres to as many as thirty per 100 metres in the centre of the property where one or more of the dikes assume stock-like dimensions.

A number of former producers of base and precious metals occur in the immediate vicinity of Erie Creek, notably the Second Relief Mine (past production - 99,000 ounces of gold from 228,000 tons of ore) to the north and the Arlington (past production - 56,000 ounces of gold and 100,000 ounces of silver from 85,000 tons of ore). Both deposits and a number of other prospects are associated with the Erie Creek dike swarm although a direct genetic relation has not been established.

PROPERTY GEOLOGY

The property geology has been described by the writer (Allen, 1977) and Hodgson, Parry and Lebel (1980). The following is a brief summary. For details, see assessment reports on file with the B.C. Ministry of Energy, Mines and Petroleum Resources.

The main geological features of the property are a quartz monzonite stock containing a well developed quartz vein stockwork about 400 metres in diameter, and swarms of quartz-feldspar porphyry dikes. Host rocks are hornfelsic siltstone of the "Sinemurian Beds" and/or Hall Formation, and augite basalt and volcanic breccia of the Rosslund Formation.

Erie Creek Stock

The Erie Creek stock is a light grey quartz monzonite with an aplitic texture. Four sub-types with complex cross-cutting relationships between types and molybdenum mineralization have been noted.

Dikes

Dikes of quartz-feldspar porphyry of various textures are abundant

on the property, much more so than indicated on the accompanying maps. They range in width from several centimetres to about 20 metres. In general, they trend north-south ($+30^{\circ}$) and have steep dips. Numerous phases have been recognized. Age relationships with each other and with mineralization are complex. Most dikes appear to be intramineral and postmineral in age.

The most prevalent dike type is a biotite quartz-feldspar porphyry which in itself has variable proportions of phenocrysts of biotite, quartz and feldspar. Other common readily identifiable dike phases include white quartz porphyry and black basalt dikes.

Alteration

Three main alteration types have been mapped.

- 1) Biotite hornfels is apparently a contact metamorphic effect related to both the Nelson batholith and the Erie Creek dike swarm. It is developed mainly in argillite and siltstone.
- 2) Weak quartz-sericite-pyrite alteration occurs in envelopes along and adjacent to fractures and molybdenite-quartz veins.
- 3) Chlorite occurs mainly on fractures and in shear veins in augite andesite and hornfels.

Mineralization

Mineralization on the Erie Creek property occurs roughly in four concentric zones.

- 1) An inner quartz-molybdenite + scheelite zone is approximately 600 metres in diameter and is centered on the east side of Erie Creek. Host rocks are quartz monzonite dikes and stock, and white rhyolite. Grades in the zone range from 96 to 590 parts per million molybdenum, 166 to 1960 parts per million copper and 50 to 1400 parts per million tungsten. Best results reported by McIntyre Porcupine Mines were 85 metres of 0.115% MoS_2 and 0.05% Cu (including 30 metres of 1.2 ounces per ton silver).
- 2) Chalcopyrite occurs over an area of 1.5 to 2 kilometres, both in and around the molybdenite zone. Chalcopyrite occurs in quartz and sulphide veinlets, as fracture coatings, and in shear veins with pyrite, pyrrhotite and minor amounts of scheelite. Best copper

values were obtained up to 1.3% from vein and dump samples mainly on the west side of Erie Creek.

- 3) Pyrite and pyrrhotite occur finely disseminated and as fracture coatings in and around the molybdenite-chalcopyrite zone, over an area of about 1.5 by 2.5 kilometres.
- 4) Sphalerite and galena along with some gold occur in shear veins beyond the molybdenite zone. They are found on the Arnold, St. Louis, Ben Hassen and Rosa reverted crown grant claims.

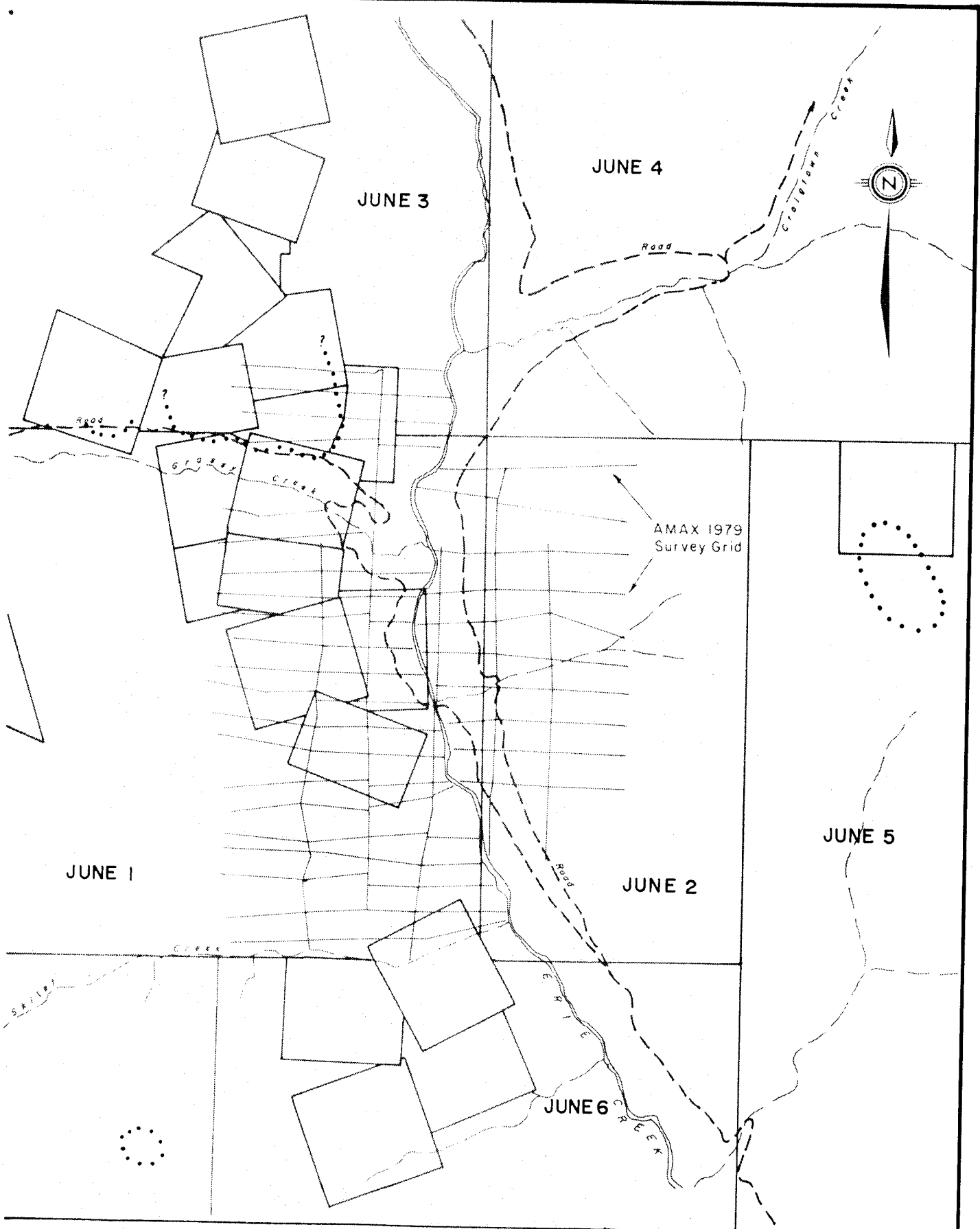
The distribution of gold and silver appears to be erratic. McIntyre Porcupine Mines reported a 30 metre composite in drill hole 69-5 that assays 1.2 ounces per ton silver. Elsewhere, silver values up to 90 parts per million (2.6 ounces per ton) are reported by AMAX from the shear veins mentioned above. Gold values of up to 620 parts per billion (0.017 ounces per ton) are also reported.

GEOCHEMISTRY

Previous Work

Results of soil and rock geochemical sampling by AMAX are summarized on Figures 5a to 5f. The following data reinforces the zoning pattern already described above:

- 1) A molybdenum soil anomaly 700 metres in diameter centered east of Erie Creek.
- 2) A tungsten anomaly about 1.2 kilometres in diameter which overlaps the molybdenum anomaly.
- 3) A copper soil anomaly which is two kilometres in diameter.
- 4) Lead and zinc soil anomaly patterns occur beyond the copper anomalies.
- 5) Silver values are anomalous (0.8-2.4 ppm) mainly in the extreme northwest part of the sampled area. Elsewhere, reconnaissance sampling has revealed several clusters of silver anomalies in soil (0.8 to 2.8 ppm with one anomalous value of 10.6 ppm obtained in the southwestern corner of the claim group) that warrant follow-up.



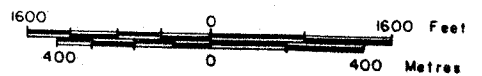
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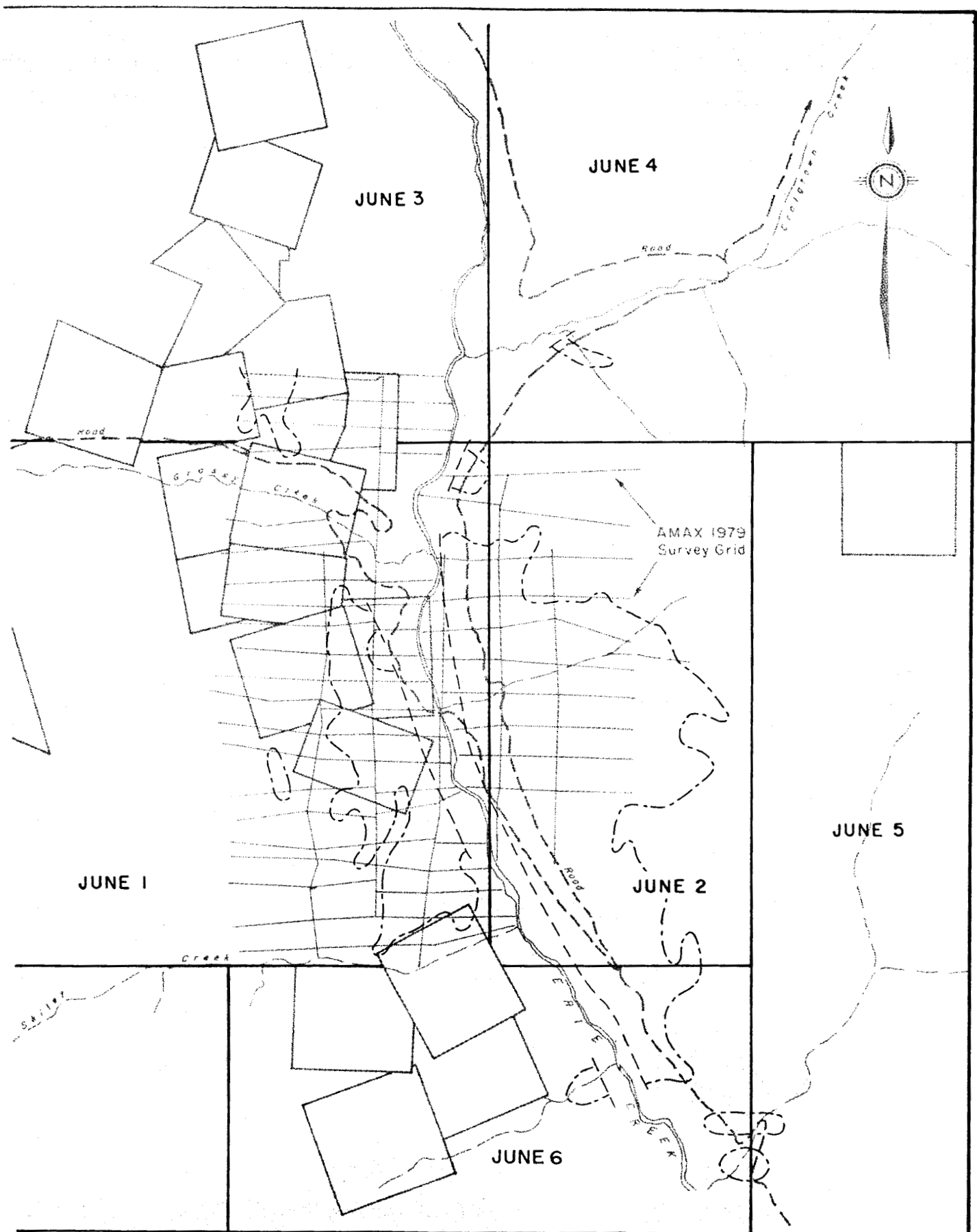


p.p.m. Ag DISTRIBUTION MAP

ERIE CREEK PROPERTY
NELSON MINING DIVISION



D. G. ...
After Hodgson, Parry, LeBel (Amax), 1980



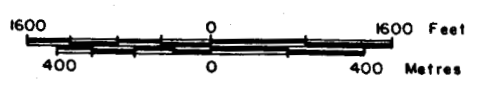
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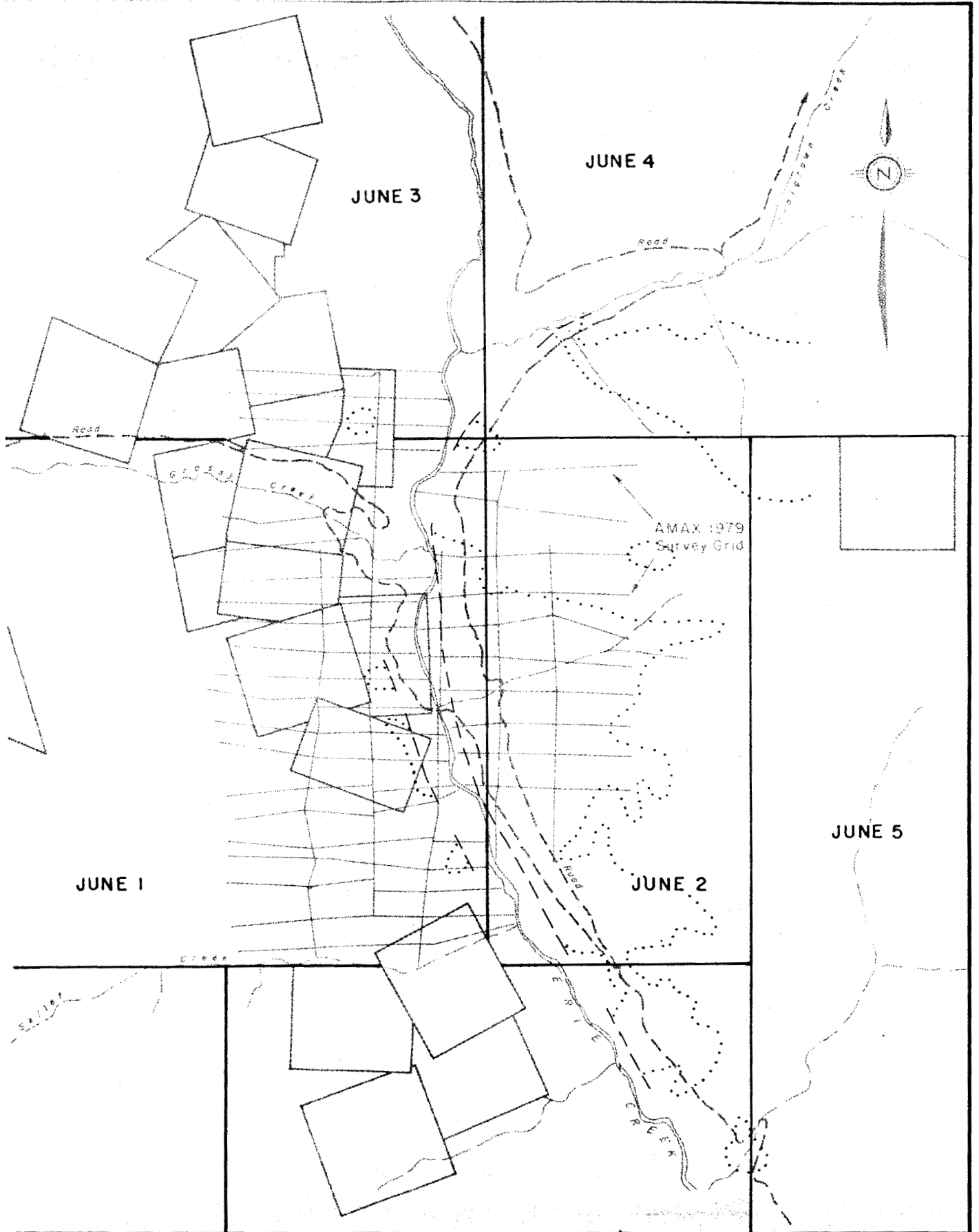
p.p.m. W \geq 15

D. G. Allen

After Hodgson, Parry, LeBel (Amax), 1980.

**p.p.m. W DISTRIBUTION MAP
ERIE CREEK PROPERTY
NELSON MINING DIVISION**





LEGEND

p.p.m. Mo \geq 4

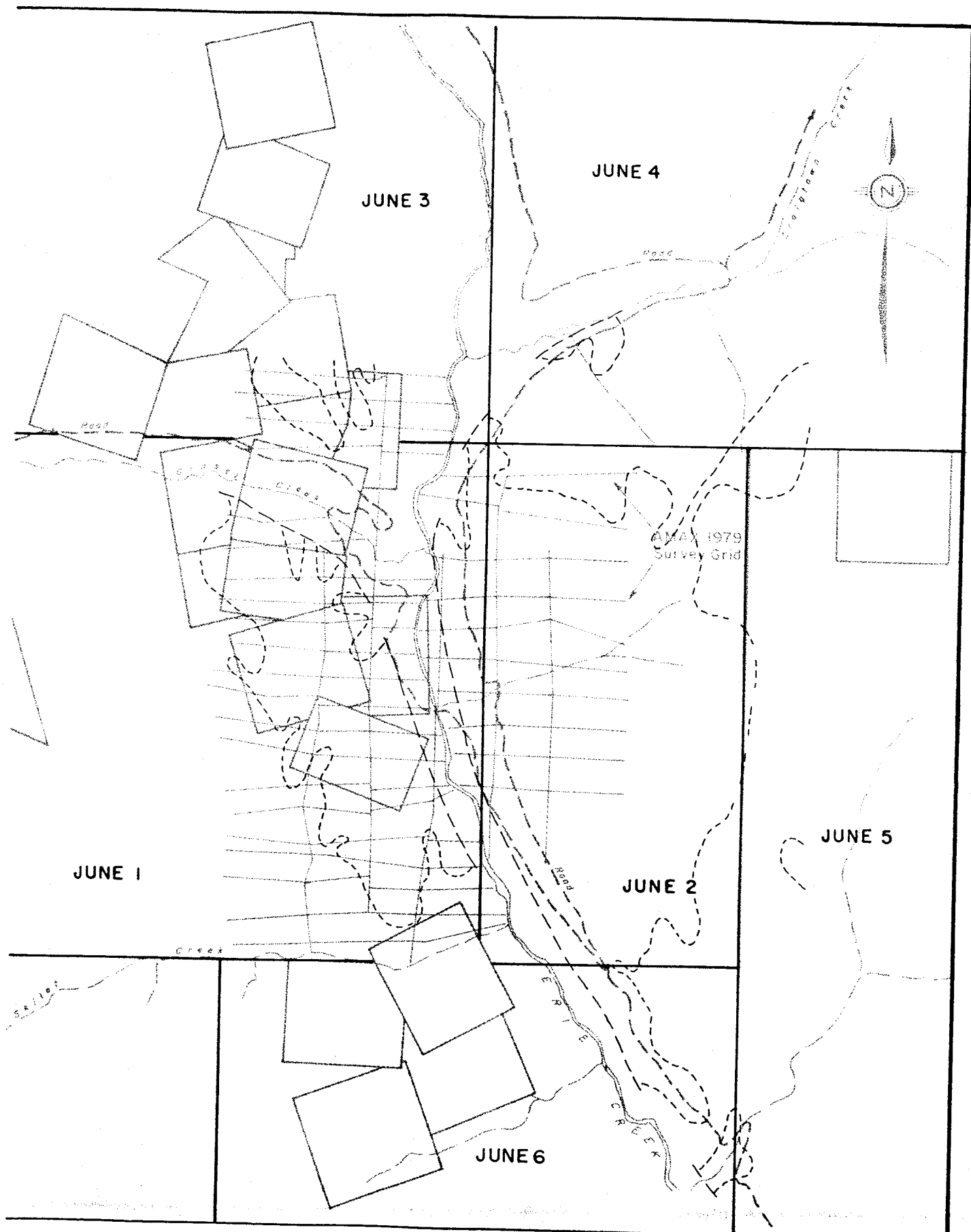


D. Gall

After Hodgson, Parry, LeBel (Amax), 1980.

**p.p.m. Mo DISTRIBUTION MAP
ERIE CREEK PROPERTY
NELSON MINING DIVISION**





LEGEND

p.p.m. Cu \geq 100

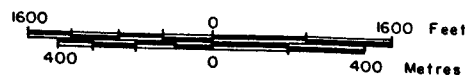


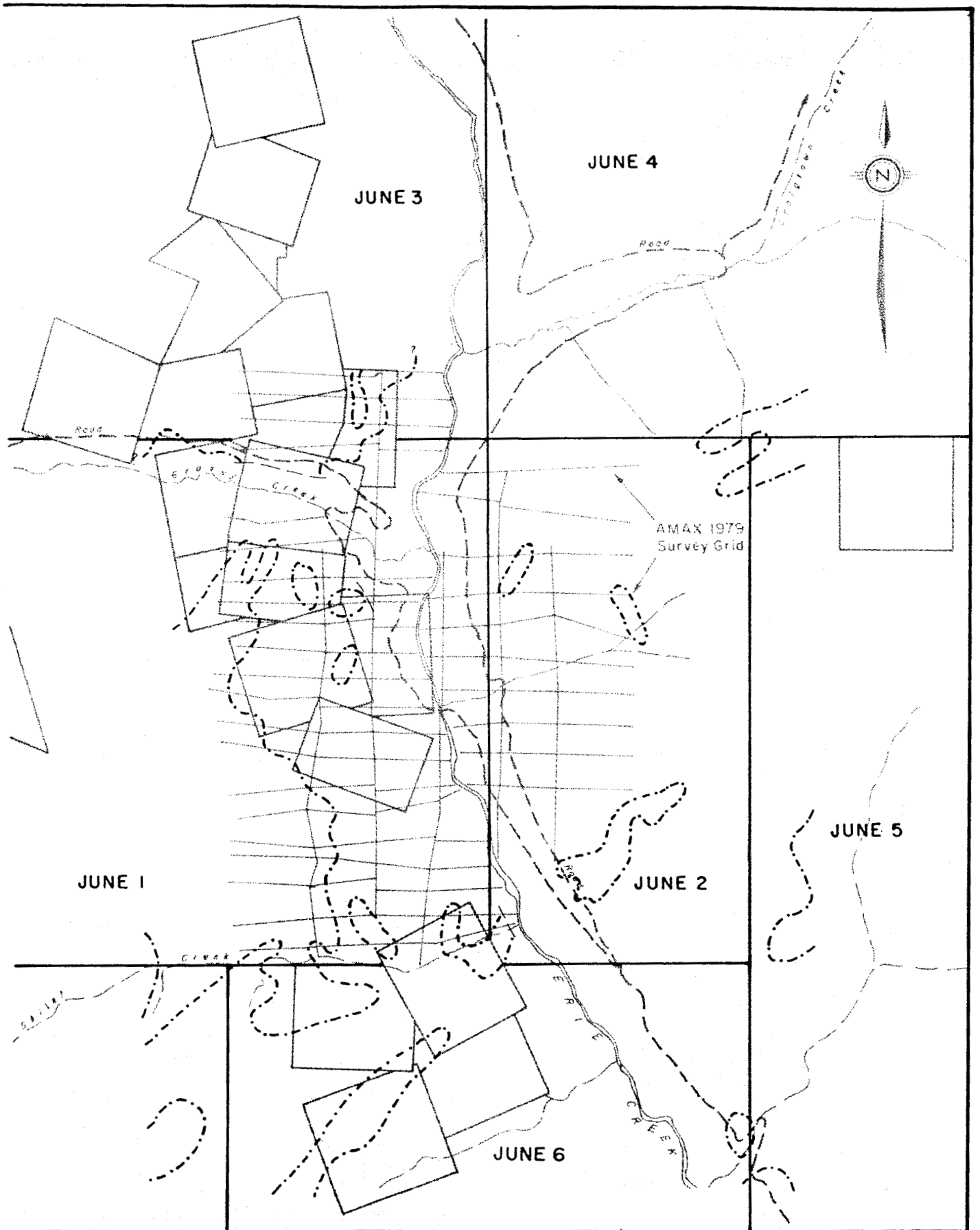
D. G. Allen

After Hodgson, Parry, LeBel (Amax), 1980.

p.p.m. Cu DISTRIBUTION MAP

**ERIE CREEK PROPERTY
NELSON MINING DIVISION**





LEGEND

p.p.m. Pb \cong 50

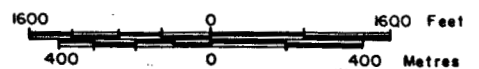


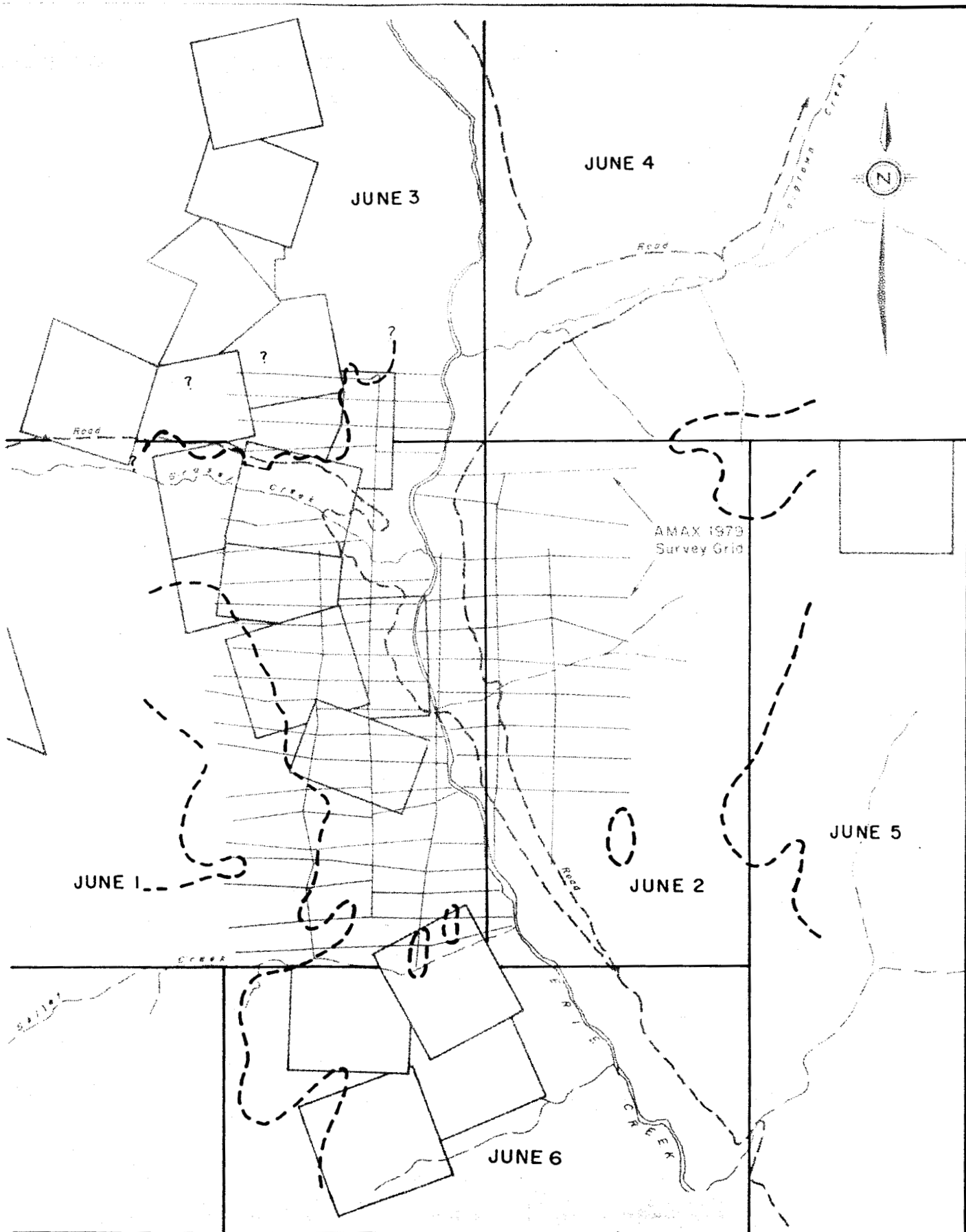
D.G. all

After Hodgson, Parry, LeBel (Amax), 1980.


p.p.m. Pb DISTRIBUTION MAP

**ERIE CREEK PROPERTY
NELSON MINING DIVISION**



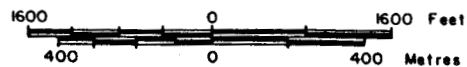


LEGEND

p.p.m. Zn \approx 200 

D. S. Allen

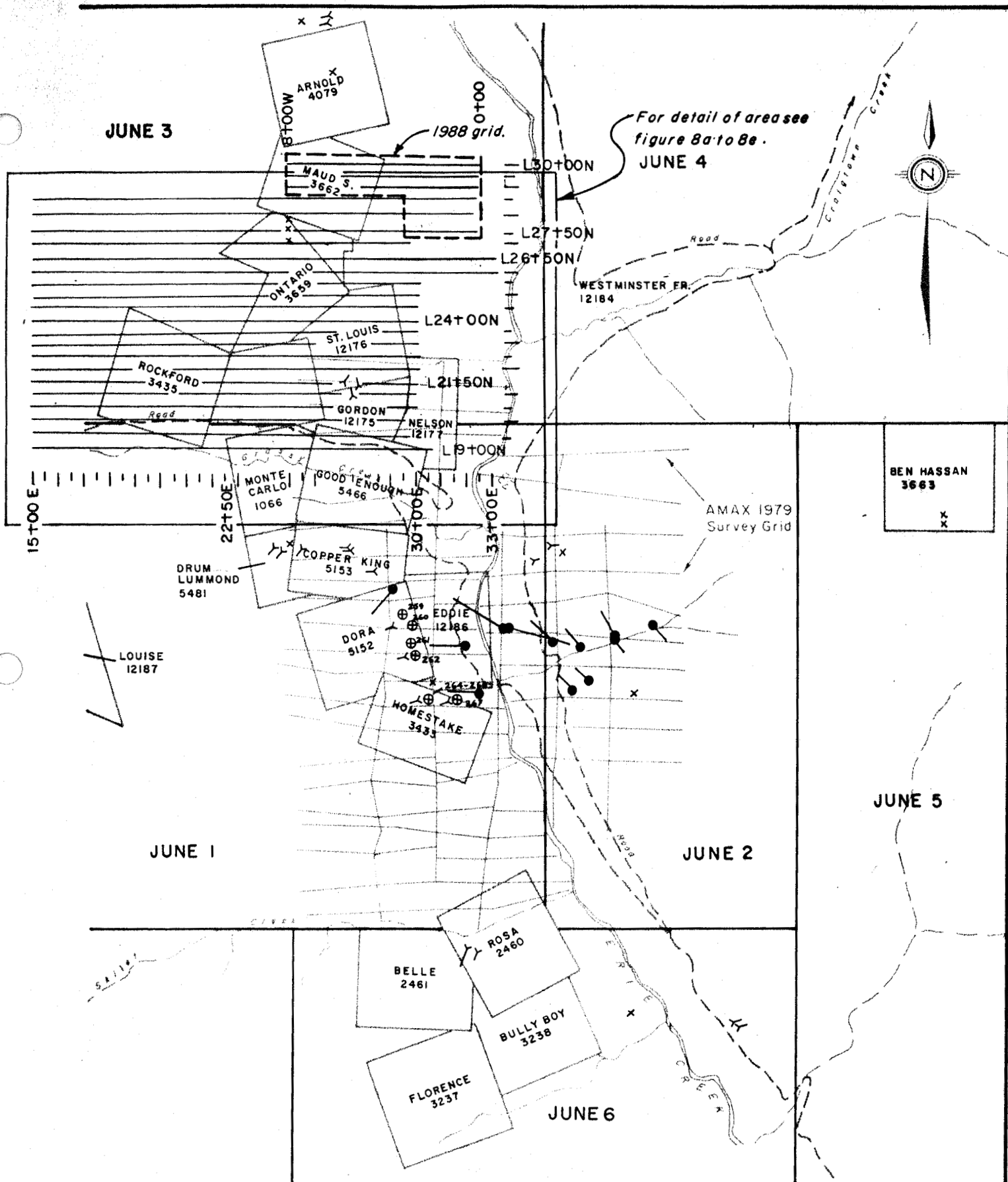
**p.p.m. Zn DISTRIBUTION MAP
ERIE CREEK PROPERTY
NELSON MINING DIVISION**



After Hodgson, Parry, LeBel (Amax), 1980.

JUNE 3

For detail of area see figure 8a to 8e.
JUNE 4



BEN HASSAN
3663
x
x

JUNE 1

JUNE 2

JUNE 5

JUNE 6

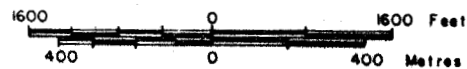
LEGEND

- Adit Y
- Shaft, Pit x x
- Drill hole ●
- Rock sample, sample no. ⊕ 267

Claims, Drill Holes, Adits, Sample Sites

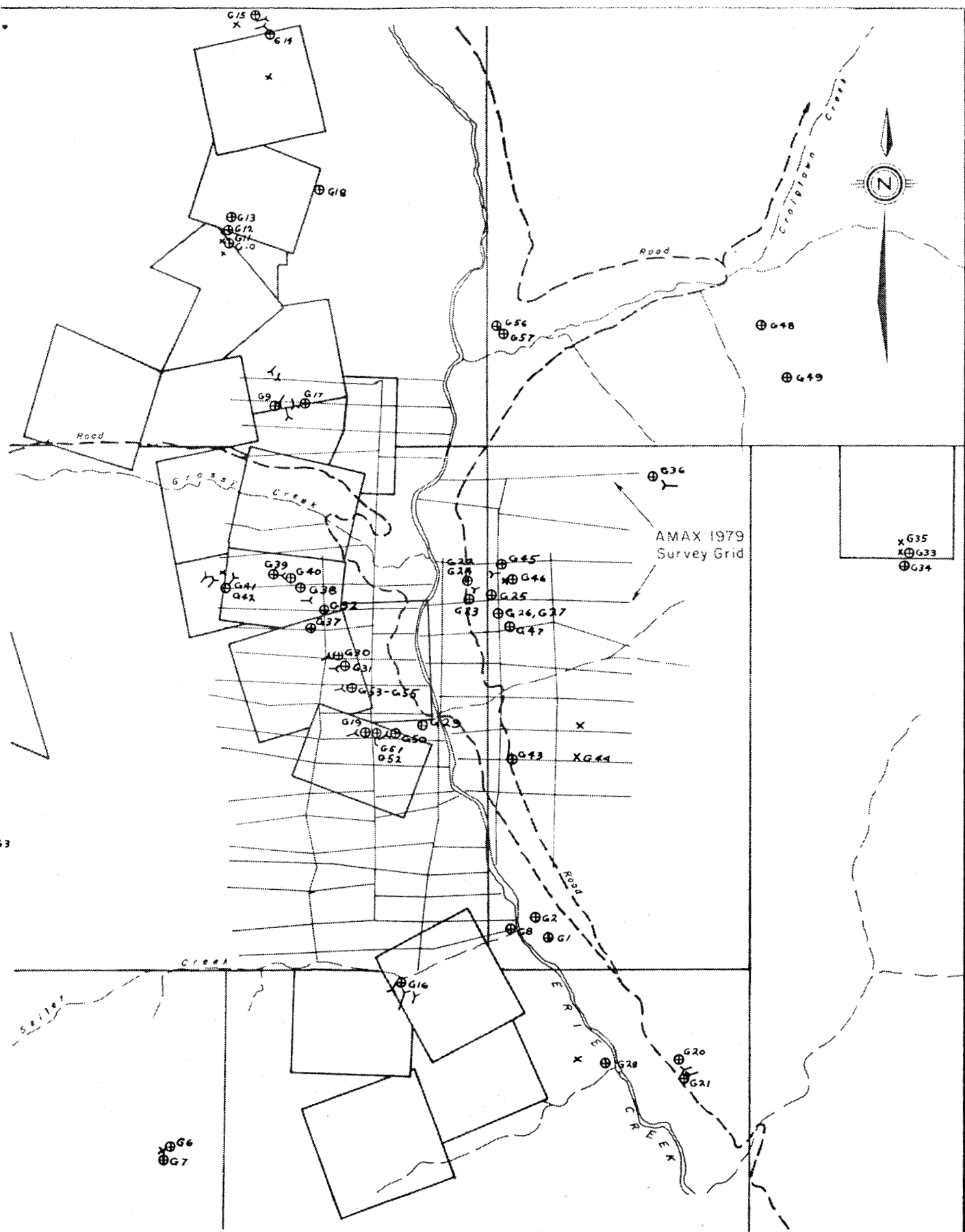
ERIE CREEK PROPERTY
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After Hodgson, Parry, LeBel (Amax), 1980.

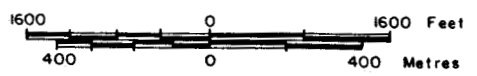
Figure 6



LEGEND

- Adit J
- Shaft, Pit X X
- Rock sample, sample no. ⊕ G₁₇

**1986 sample sites
ERIE CREEK PROPERTY
NELSON MINING DIVISION**



After Hodgson, Parry, LeBel (Amax), 1980.

D. J. Allen

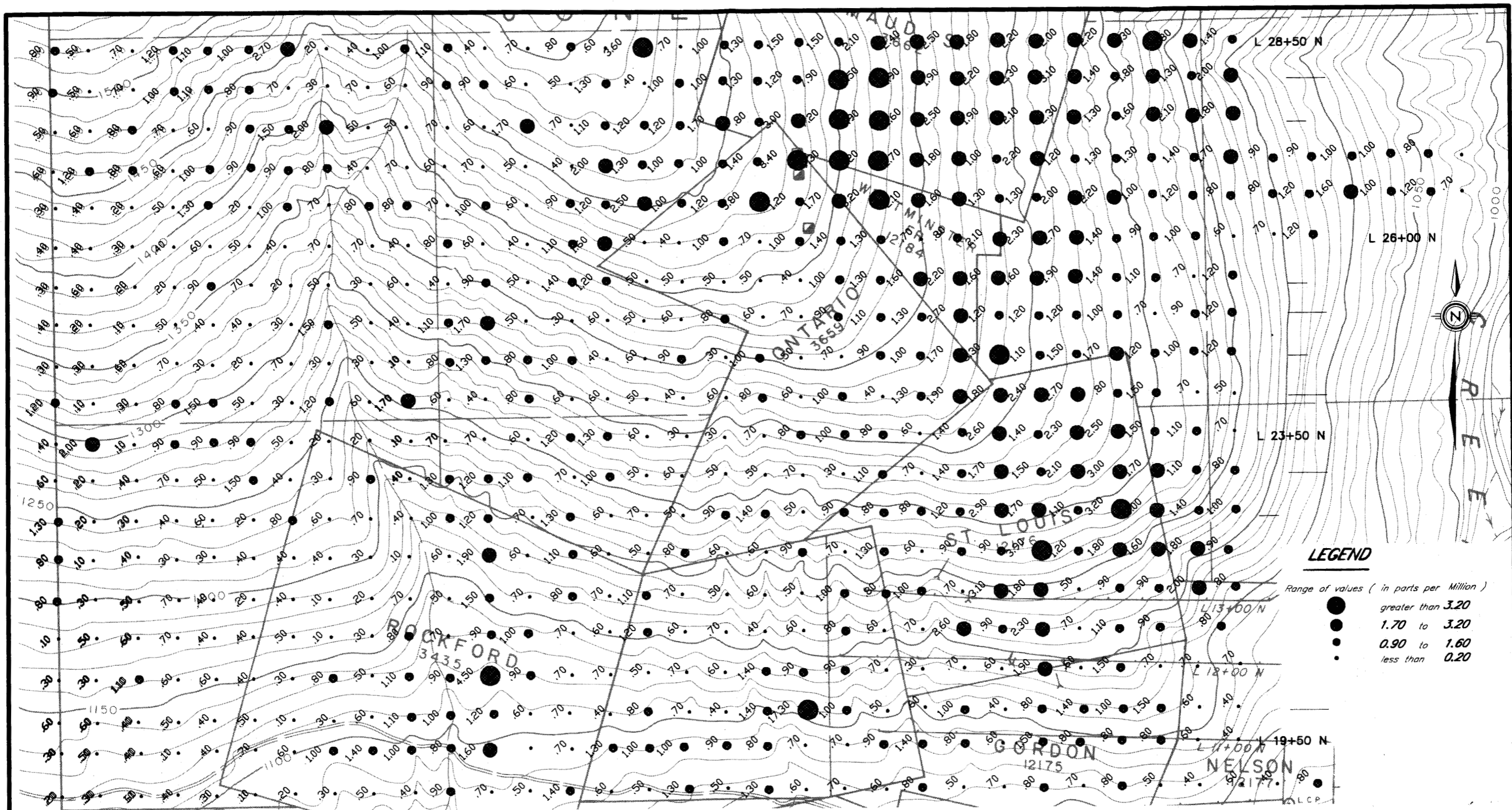
Recent Work

Since acquiring the property in 1985, Kootenay King Resources Inc. has undertaken prospecting and geochemical sampling with the view of determining its precious metal potential. Results of this work are summarized below.

In 1985, most of the available drill core pulps on storage at Rossbacher Laboratory Ltd. were selected and analyzed for gold. Samples were analyzed to investigate whether or not gold values are present in the molybdenum-tungsten zone. Except for a few scattered anomalous values of 20 to 30 parts per billion, only two significant values of 180 and 350 parts per billion (0.005 and 0.01 ounces per ton) were obtained from the interval 162 to 170 feet (2.4 metres). In this interval Parry (1980) reports the presence of chlorite-actinolite veins up to 15 centimetres wide containing up to 10% pyrrhotite and locally 1% chalcopyrite. Several samples taken by the writer (Figure 6) from the copper-tungsten zone were analyzed for gold and found to be slightly anomalous (up to 70 parts per billion).

In 1986, a prospecting program was carried out on the Erie Creek property. An attempt was made to locate and sample as many of the old prospect pits, trenches and adits as possible. A total of 58 rock samples were collected. Most were a series of grab samples or rock chip samples collected from float, dumps and outcrop. Samples were shipped to Acme Analytical Laboratories and analyzed for gold and silver by standard atomic absorption techniques. Selected samples were fire assayed for gold and silver. Sample sites are plotted on Figure 7 and analytical results presented in Appendix II. Results of sampling reveal a low but significant range of gold and silver values. Approximately one third of the samples contain anomalous gold (greater than 10 parts per billion) and silver (greater than 1.5 parts per million). Of particular interest are gold values of 0.01 to 0.045 ounces obtained from quartz veins on the Ben Hassan claim in the eastern part of the claim group, and silver values of up to 7.8 ounces per ton.

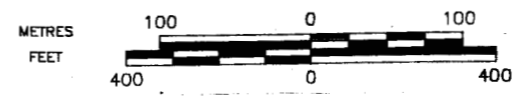
In 1987 a flagged grid was established in the northwestern part of the property (June 3 claim) to cover some of the known copper bearing



LEGEND

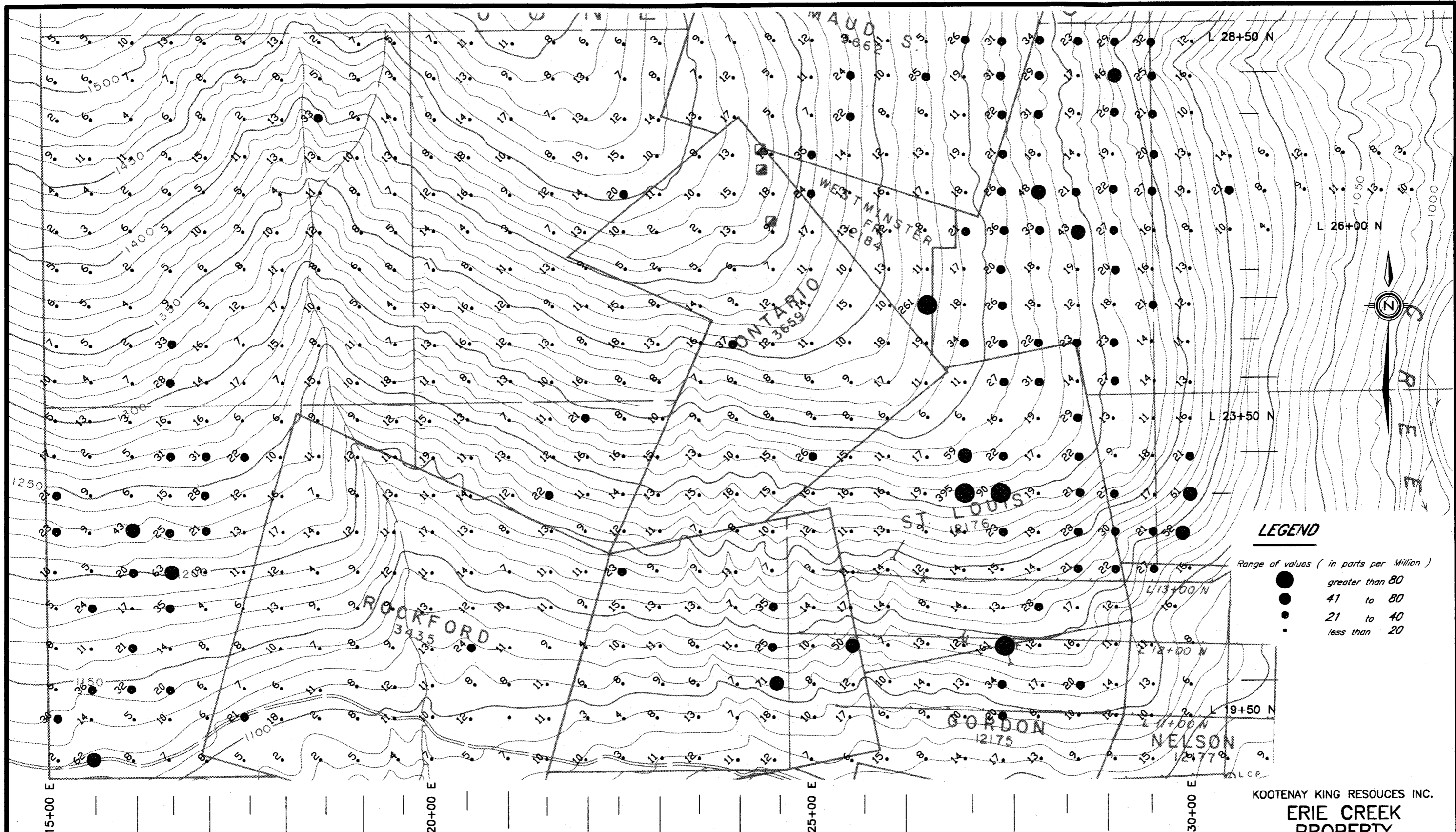
Range of values (in parts per Million)

- greater than 3.20
- 1.70 to 3.20
- 0.90 to 1.60
- less than 0.20



W. J. Allen
A.M. exploration ltd.

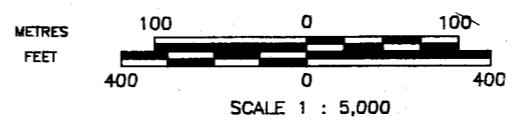
KOOTENAY KING RESOURCES INC.
ERIE CREEK PROPERTY
 NELSON MINING DIVISION - BRITISH COLUMBIA
GEOCHEMICAL MAP
SILVER ppm



LEGEND

- Range of values (in parts per Million)
- greater than 80
 - 41 to 80
 - 21 to 40
 - less than 20

D.S. all
A.M. exploration ltd.

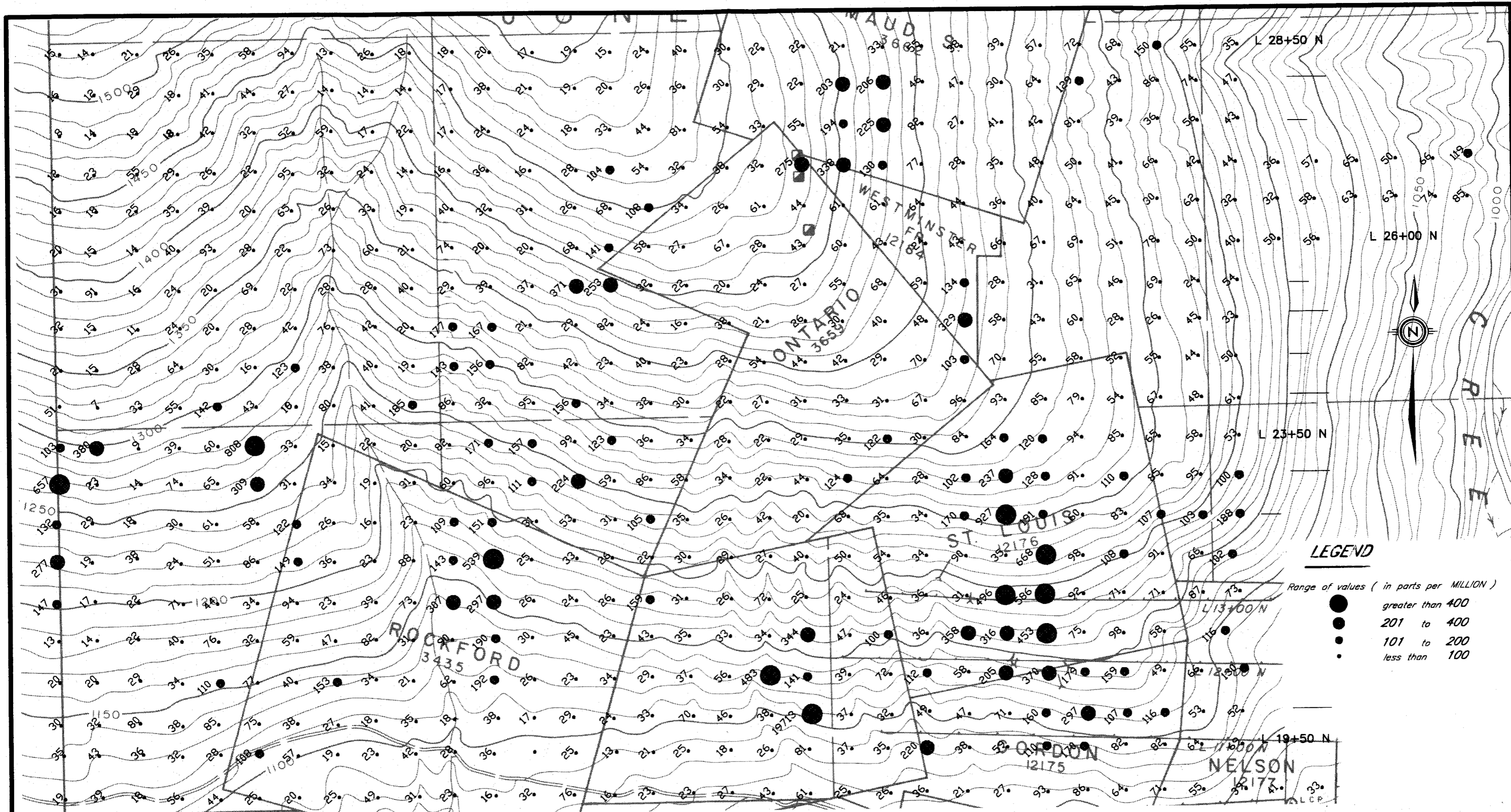


KOOTENAY KING RESOURCES INC.
ERIE CREEK PROPERTY
 NELSON MINING DIVISION - BRITISH COLUMBIA
GEOCHEMICAL MAP
ARSENIC ppm

AUGUST , 1988

N.T.S. B2 F/ 3 & 6

FIGURE 8b

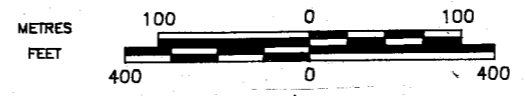


LEGEND

Range of values (in parts per MILLION)

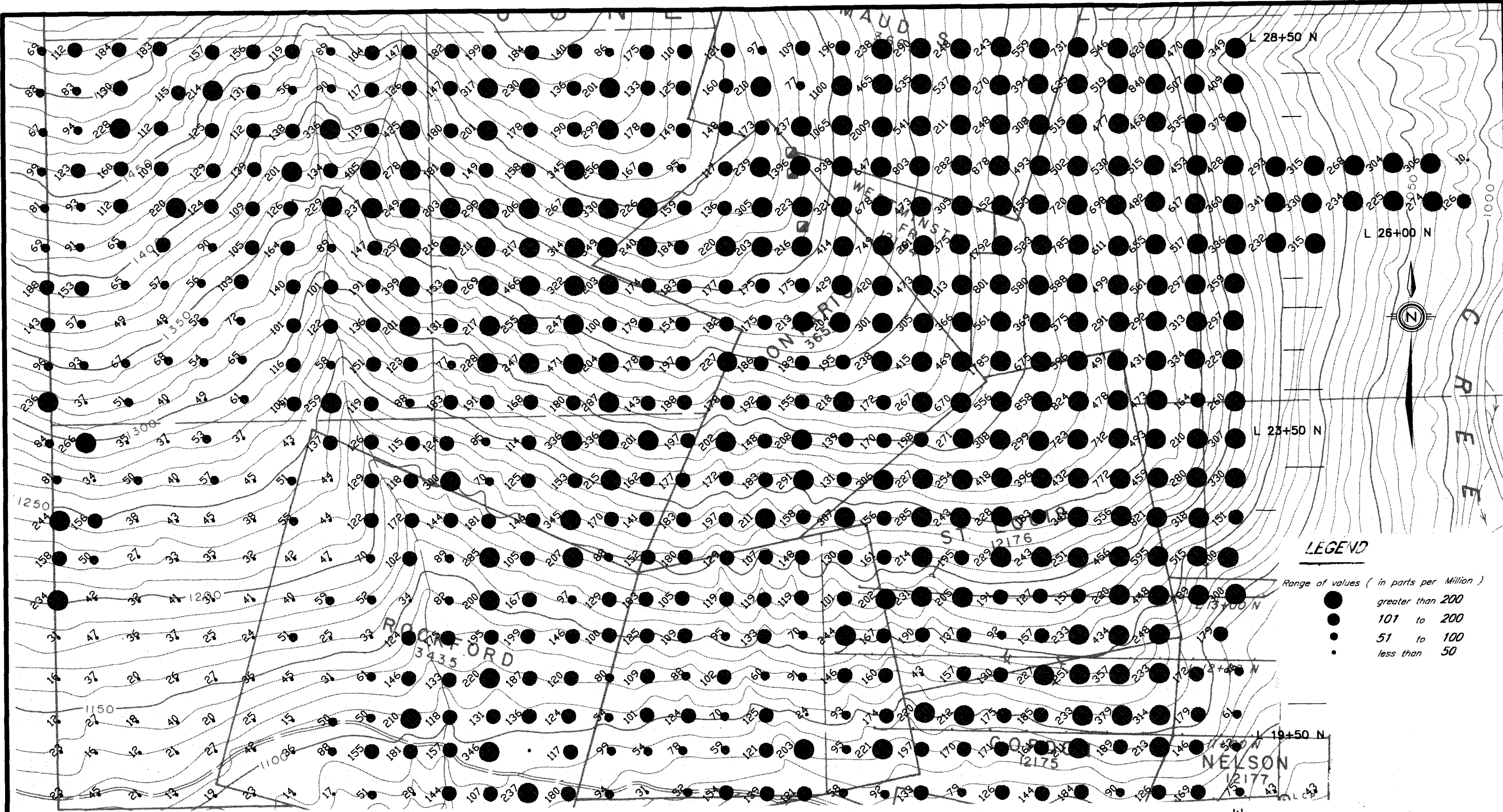
- greater than 400
- 201 to 400
- 101 to 200
- less than 100

D.G. Allen
A.M. exploration Ltd.



KOOTENAY KING RESOURCES INC.
ERIE CREEK PROPERTY
 NELSON MINING DIVISION - BRITISH COLUMBIA
GEOCHEMICAL MAP
COPPER ppm

AUGUST, 1988 N.T.S. 82 F/ 3 & 6 **FIGURE 8c**



LEGEND

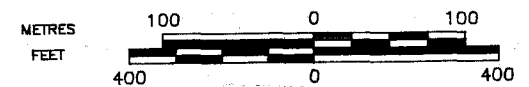
Range of values (in parts per Million)

- greater than 200
- 101 to 200
- 51 to 100
- less than 50

KOOTENAY KING RESOURCES INC.
ERIE CREEK PROPERTY
 NELSON MINING DIVISION - BRITISH COLUMBIA

GEOCHEMICAL MAP
LEAD ppm

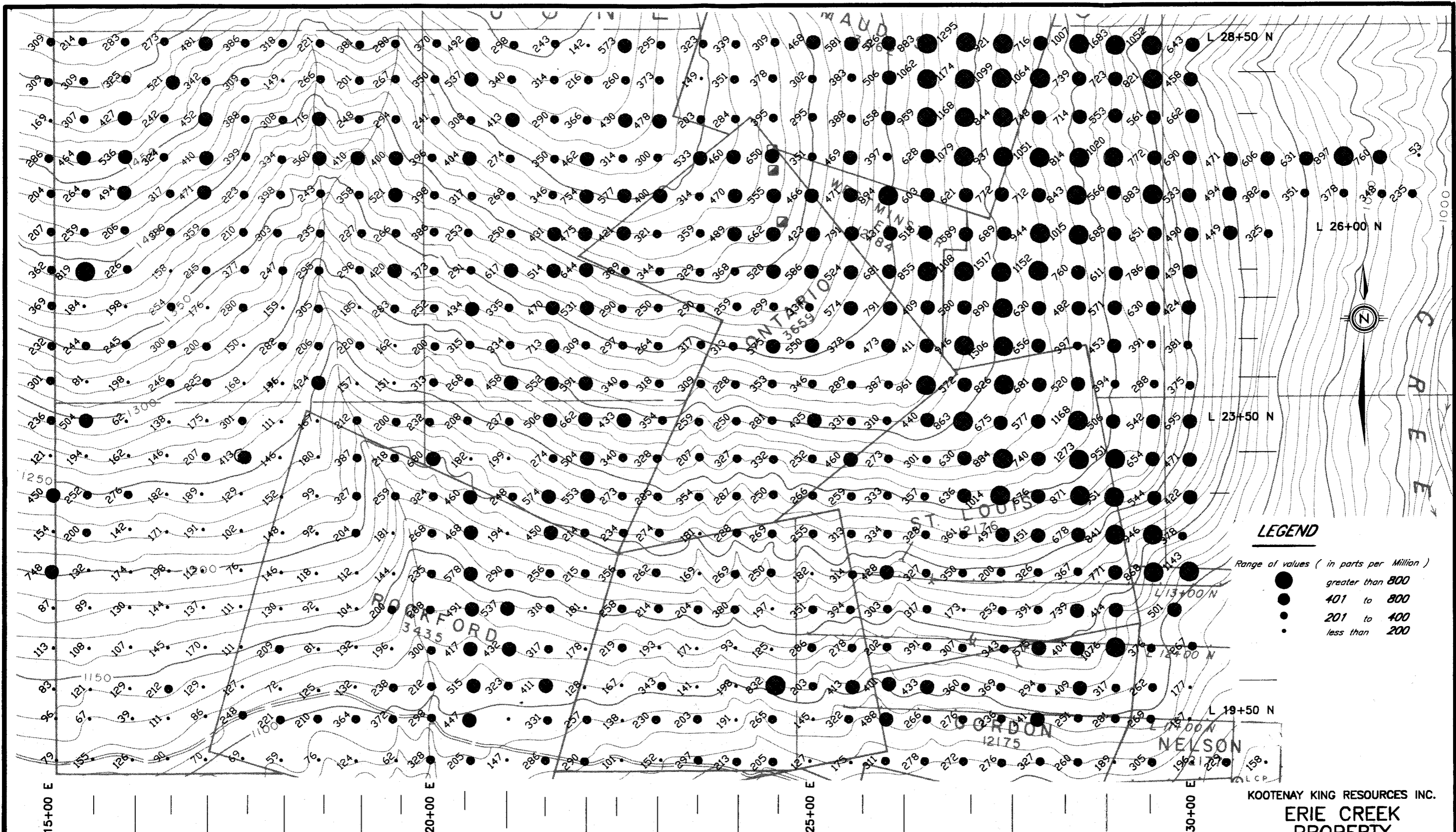
D.G. Allen
A.M. exploration Ltd.



AUGUST, 1988

N.T.S. B2 F/ 3 & 6

FIGURE 8d

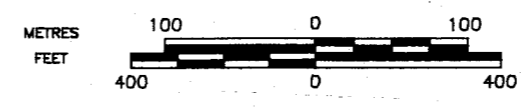


LEGEND

Range of values (in parts per Million)

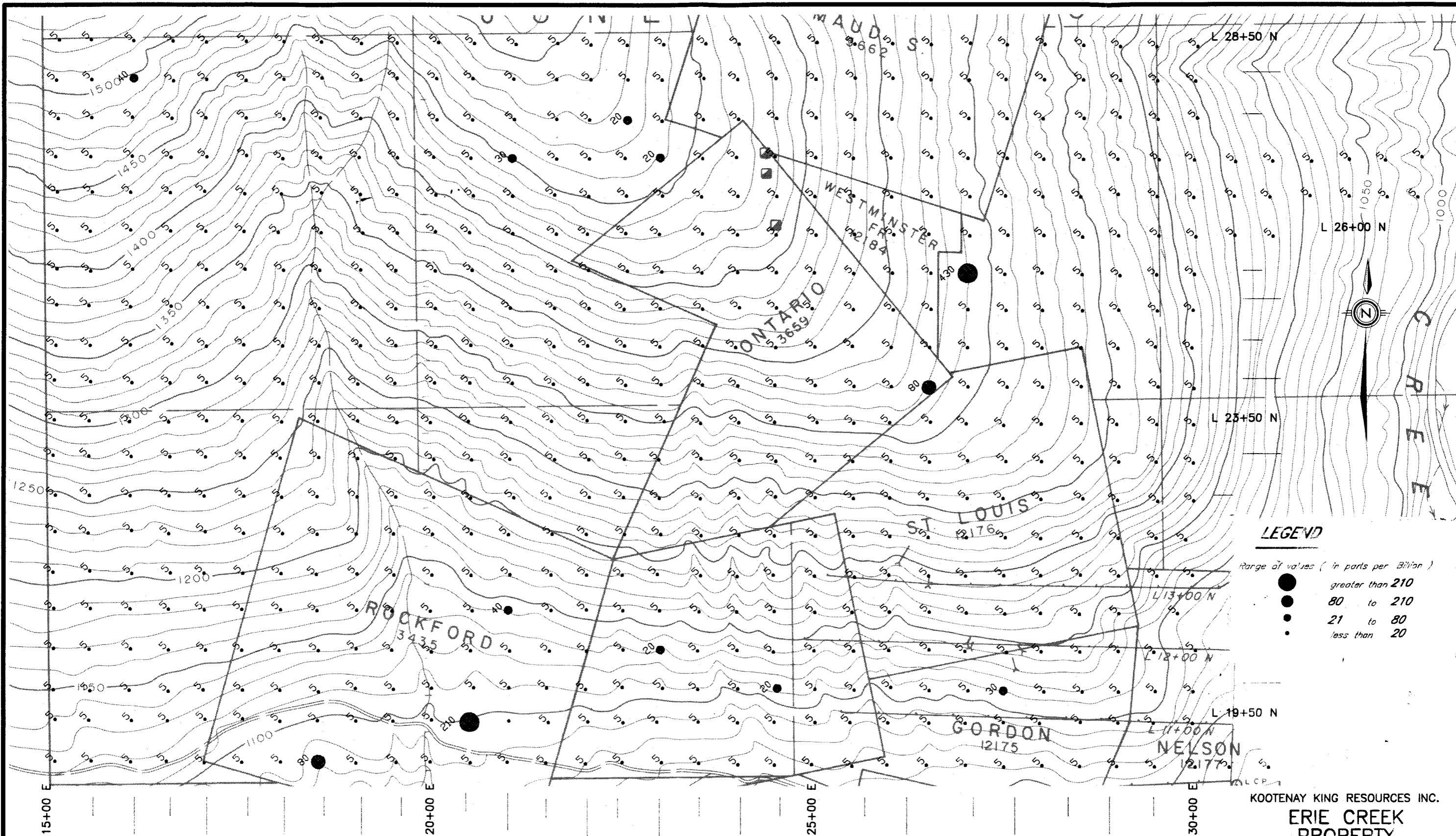
- greater than 800
- 401 to 800
- 201 to 400
- less than 200

A.M. *Donald J. de*
exploration Ltd.



KOOTENAY KING RESOURCES INC.
ERIE CREEK PROPERTY
NELSON MINING DIVISION - BRITISH COLUMBIA
GEOCHEMICAL MAP
ZINC ppm

AUGUST, 1988 N.T.S. 82 F/ 3 & 6 **FIGURE 8e**



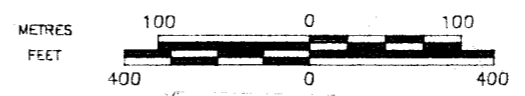
LEGEND

Range of values (in parts per Billion)

- greater than 210
- 80 to 210
- 21 to 80
- less than 20

KOOTENAY KING RESOURCES INC.
ERIE CREEK PROPERTY
 NELSON MINING DIVISION - BRITISH COLUMBIA
GEOCHEMICAL MAP
 GOLD ppb

Donald F. Allen
A.M. exploration Ltd.



shear veins. Lines were run with compass and hip chain and B horizon soil samples were collected at 50 metre intervals along the lines. Samples were placed in Kraft paper bags and shipped to Rossbacher Laboratory Ltd. Gold determinations were made by standard atomic absorption techniques. Samples were then shipped to Acme Analytical Laboratories Ltd. for 30 element determinations by inductively coupled plasma (I.C.P.) spectrometry.

Results of soil sampling conducted in 1987 are presented in Appendix II and a statistical summary of selected elements are presented in Appendix III. Sample sites and silver, arsenic, copper, lead, zinc, and gold values are plotted on Figures 6a to 6f.

Inspection of the statistical summaries and plots shows very high background values of silver, lead and zinc in soils, particularly in the northeastern part of the grid area. The anomalous areas, in part, appear to be spatially related to some of the known shafts and adits, although they extend well beyond.

Gold values are generally uniformly low although a number of scattered isolated gold values ranging from 20 to 410 parts per billion occur throughout the grid area.

Of potential interest as gold targets are two areas of moderately anomalous arsenic values (greater than 20 parts per million with peaks ranging from 35 to 395 parts per million). One is a north trending belt through the silver-lead-zinc anomalous area and the other a northeast trending belt in the southwest part of the survey grid.

Scattered clusters of anomalous copper values (100 to 907 parts per million) occur throughout the grid. One highly anomalous value of 19713 parts per million (1.97%) presumably is related to a nearby copper-bearing pyritic shear zone.

DISCUSSION OF RESULTS

Although gold values obtained to date on the Erie Creek property are generally low, two gold targets requiring further evaluation have been identified:

- (1) on the Ben Hassan claim, gold values in the range of 0.01 to 0.045 ounces per ton have been obtained on quartz veins, and
 - (2) in the 1987 grid area, a number of scattered isolated gold anomalies in and around two irregular belts of arsenic anomalies.
- A possible favourable feature of the latter is that one of the arsenic anomalies parallels the sedimentary-volcanic stratigraphic trend.

Also of interest are the widespread silver, lead and zinc anomalies which have not been fully delineated. They occur in an area underlain by volcanic and sedimentary rocks which are intruded by a lobe of the Nelson batholith and by dikes of the Erie Creek dike swarm, all of which are favorable hosts for a variety of base and precious metal deposits. Follow-up prospecting, mapping and rock geochemical sampling are warranted to identify their source.

Donald G. Allen

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CERTIFICATE

I, Donald G. Allen, certify that;

1. I am a Consulting Geological Engineer, of A & M Exploration Ltd., with offices at #704 - 850 West Hastings Street, Vancouver, British Columbia.
2. I am a graduate of the University of British Columbia with degrees in Geological Engineering (B.A.Sc., 1964; M.A.Sc., 1966).
3. I have practised my profession of exploration geologist since 1964 in British Columbia, the Yukon, Alaska and various parts of the Western United States.
4. I am a member in good standing of the Association of Professional Engineers of British Columbia.
5. This report is based on the fieldwork carried out personally by the writer from September 28 to October 2, 1976 (for AMAX), on property visits on October 12, 1985 and October 3, 1987; on information supplied by Canamax Resources Inc. (see References); and on field work carried out by George King, Larry Sostad, and Bill Markinson in 1987.
6. I hold no interest, nor do I expect to receive any, in the Erie Creek property, or in Kootenay King Resources Inc.
7. I consent to the use of my name and this report in a Statement of Material Facts or in a Prospectus in connection with raising of funds for the project covered by this report.

August 9, 1988
Vancouver, B.C.



Donald G. Allen
P. Eng. (B.C.)

APPENDIX I

SAMPLE DESCRIPTIONS

APPENDIX I

Description of samples collected by G. King (Newcastle Explorations Ltd.)

- G 1. Roadbed sample.
2. Rusty sulphide bearing felsic intermediate rock.
3. Mineralized float (chalcopyrite, molybdenite).
4. Sample from site of old shaft @ 4,900' elevation.
5. As above.
6. As above.
7. "Wallrock".
8. Angular float - quartz-feldspar porphyry.
9. Quartz-feldspar porphyry containing minor pyrite and galena.
10. Quartz vein containing pyrite.
11. Quartz vein containing chalcopyrite and pyrrhotite from shaft at 4,650' elevation.
12. As above.
13. From small pit at 600' elevation.
14. From adit at 4,300' elevation.
15. Quartz vein from adit immediately to the west of sample 14.
16. Adit dump sample at Skillet Creek.
17. Sample from near adit @ 3,750' elevation.
18. Sample from near adit @ 4,100' elevation.
19. Mineralized wall rock from trench at 3,400' elevation.
20. Float sample.
21. Sample from trench.
22. 50 metres west of upper road.
23. As above.
24. At adit 75 metres east of upper road.
25. From trench 75 metres east of upper road.
26. 100 metres east of upper road.
27. As above.
28. Hornfels volcanic rock with pyrite and pyrrhotite on fractures.
29. 20 metres above trench.
30. Stockwork mineralization in white rhyolite from adit.
31. Hornfels with chalcopyrite on fractures.
32. Float sample 20 metres north of drill site 69-1.
33. Quartz vein material with galena, pyrite and chalcopyrite from south shaft on Ben Hassan claim.
34. Mineralized wallrock, mainly dump material.
35. Quartz vein 2 cm wide from north shaft.
36. Adit dump material - minor mineralization in volcanic rock.
37. Hornfels with chalcopyrite.
38. Hornfels with chalcopyrite and pyrite.
39. Mineralized hornfels.
40. Quartz feldspar porphyry containing chalcopyrite and pyrite.
41. Adit at 3,000' elevation.
42. Trench at 3,850' elevation.

43. Float with chalcopyrite and pyrite.
44. Quartz vein up to 1' wide containing abundant pyrite and minor chalcopyrite.
45. Hornfels containing quartz vein stockwork - dump material.
46. Hornfels from trench at 3,650' elevation.
47. No description.
48. Calc-silicate hornfels containing galena-quartz veinlets.
49. Oxidized felsite.
50. Adit at 3,300' elevation.
51. North part of Homestake claim.
52. Adit in Homestake claim.
53. Adit in Dora claim.
54. Adit and trench at 3,400' elevation.
55. Adit in southeast part of Dora claim.
56. Silicified intermediate dike rock containing chalcopyrite and pyrrhotite.
57. As above.
58. Felsic dike.

APPENDIX II

ANALYTICAL RESULTS

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOLUTION

DATE RECEIVED: NOV 30 1987

DATE REPORT MAILED: Dec 3/87

ASSAYER: *D. Toye* DEAN TOYE, CERTIFIED B.C. ASSAYER

ROSSBACHER LABORATORY PROJECT-CERT #87830

File # 87-5954

Page 1

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	MI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
S 19+00N 15+00E	1	19	23	79	.2	16	8	391	3.04	2	5	ND	6	18	1	2	2	46	.16	.073	13	27	.33	97	.12	2	2.99	.02	.07	1
S 19+00N 15+50E	4	39	45	155	.3	20	10	1952	3.33	62	5	ND	9	49	1	2	2	58	.33	.060	20	34	.43	132	.13	2	2.28	.03	.07	1
S 19+00N 16+00E	1	18	21	126	.6	16	7	634	3.58	8	5	2	5	20	1	2	2	60	.20	.223	8	37	.36	162	.12	2	1.98	.02	.07	1
S 19+00N 16+50E	2	56	13	90	.4	21	11	431	3.97	7	5	ND	5	30	1	2	2	83	.31	.053	13	50	.59	114	.12	2	1.70	.03	.09	1
S 19+00N 17+00E	1	44	19	70	.3	21	8	371	3.36	8	5	ND	7	20	1	2	2	69	.26	.090	13	44	.53	108	.10	2	1.87	.03	.08	1
S 19+00N 17+50E	1	25	23	69	.1	20	8	492	3.73	5	5	ND	11	27	1	2	2	75	.27	.112	8	43	.43	108	.13	2	2.27	.03	.07	1
S 19+00N 18+00E	1	20	14	59	.2	16	8	307	3.36	2	5	ND	9	19	1	2	2	67	.22	.091	9	42	.37	78	.09	2	1.66	.02	.07	1
S 19+00N 18+50E	1	25	17	76	.3	13	8	472	3.18	2	5	ND	5	23	1	2	2	63	.24	.097	9	42	.29	59	.06	2	1.15	.02	.06	1
S 19+00N 19+00E	1	49	51	124	.5	23	10	465	4.06	5	7	ND	5	46	1	2	2	76	.34	.102	20	67	.69	177	.10	2	2.24	.03	.15	1
S 19+00N 19+50E	1	31	20	62	.4	16	7	226	2.98	4	5	ND	6	22	1	2	2	63	.28	.096	11	41	.37	72	.05	2	.90	.02	.07	1
S 19+00N 20+00E	1	23	144	328	.9	10	7	3180	2.90	7	5	ND	6	30	3	2	2	39	.17	.116	12	15	.19	197	.11	2	2.38	.02	.07	1
S 19+00N 20+50E	2	16	107	205	.7	9	6	886	2.94	5	5	ND	4	17	1	2	2	36	.15	.067	9	14	.18	85	.12	2	3.36	.02	.05	1
S 19+00N 21+00E	1	32	237	147	.5	8	3	961	1.45	7	5	ND	1	80	3	2	2	23	.55	.050	8	12	.13	146	.05	4	.71	.03	.07	1
S 19+00N 21+50E	2	76	180	286	1.4	14	8	1175	3.07	10	11	ND	8	83	2	2	2	47	.43	.055	37	36	.53	170	.09	2	2.76	.03	.11	1
S 19+00N 22+00E	1	16	94	290	.6	10	6	1246	2.82	10	5	ND	5	45	2	2	2	40	.29	.155	12	19	.29	126	.09	2	2.40	.03	.07	1
S 19+00N 22+50E	1	23	31	101	.5	14	8	856	3.36	3	5	ND	4	16	1	2	2	60	.16	.100	9	31	.33	110	.12	2	3.07	.02	.07	1
S 19+00N 23+00E	1	23	52	152	1.3	11	9	961	3.58	11	5	ND	4	21	1	2	2	52	.14	.108	9	25	.26	126	.12	2	3.15	.02	.06	1
S 19+00N 23+50E	5	27	154	297	.5	11	8	6225	2.53	12	5	ND	3	63	3	2	2	39	.45	.122	12	15	.21	459	.11	2	1.36	.03	.12	1
S 19+00N 24+00E	1	43	139	213	1.3	12	7	1175	3.07	11	7	ND	7	48	1	2	2	44	.26	.119	21	21	.43	179	.09	2	2.67	.03	.10	1
S 19+00N 24+50E	1	61	121	205	.6	17	8	778	3.61	12	5	ND	8	34	1	2	2	60	.25	.109	22	32	.56	192	.10	2	2.25	.03	.15	1
S 19+00N 25+00E	1	25	58	127	.7	14	8	1171	3.16	7	5	ND	5	24	1	2	2	55	.20	.098	13	31	.33	155	.11	2	2.31	.03	.08	1
S 19+00N 25+50E	1	26	92	175	.6	14	8	1051	3.54	6	5	ND	5	51	1	2	2	64	.37	.078	11	31	.34	259	.10	2	2.10	.03	.07	1
S 19+00N 26+00E	2	36	133	311	.8	14	9	2209	3.08	15	5	ND	4	68	3	2	2	41	.39	.148	14	22	.31	227	.10	2	2.83	.03	.09	1
S 19+00N 26+50E	1	21	79	278	.5	74	17	1930	3.99	8	5	ND	6	56	2	2	2	65	.49	.137	16	58	1.51	341	.29	4	2.64	.04	.23	1
S 19+00N 27+00E	1	27	126	272	.7	15	8	1911	3.27	14	5	ND	5	50	1	2	2	46	.31	.281	9	21	.29	274	.12	2	2.49	.03	.09	1
S 19+00N 27+50E	1	93	144	276	.8	18	11	560	4.01	17	5	ND	7	40	2	2	2	68	.28	.073	15	29	.58	158	.15	2	3.38	.03	.13	1
S 19+00N 28+00E	1	86	184	327	.7	15	11	1347	3.78	13	5	ND	5	56	3	2	3	56	.35	.097	13	24	.52	264	.14	2	2.63	.03	.12	1
S 19+00N 28+50E	2	64	90	260	.8	17	14	1949	3.17	9	5	ND	7	97	3	2	2	42	.54	.146	21	19	.40	280	.12	3	3.23	.04	.12	1
S 19+00N 29+00E	1	71	126	189	.5	18	11	999	3.46	9	5	ND	6	50	1	2	2	56	.35	.121	15	27	.31	166	.11	2	2.67	.03	.10	1
S 19+00N 29+50E	2	55	169	305	.4	18	11	1439	3.48	15	5	ND	5	77	4	2	2	56	.54	.107	11	23	.54	263	.12	3	2.61	.03	.12	1
S 19+00N 30+00E	1	39	75	196	.6	17	11	1212	3.22	6	5	ND	5	56	2	2	3	52	.42	.069	12	22	.46	216	.13	2	2.60	.03	.10	1
S 19+00N 30+50E	2	41	43	229	.4	18	16	2011	3.82	8	5	ND	4	96	2	2	2	58	.69	.173	9	20	.49	446	.16	4	3.22	.05	.14	1
S 19+00N 31+00E	2	33	43	158	.8	18	10	840	3.36	9	5	ND	6	30	1	2	2	52	.25	.170	9	23	.46	169	.13	2	4.15	.03	.08	1
S 19+50N 15+00E	1	35	23	96	.3	20	9	576	3.46	30	5	ND	7	35	1	2	2	66	.34	.096	16	37	.53	124	.11	2	2.07	.03	.13	1
S 19+50N 15+50E	1	43	16	67	.5	24	8	348	3.20	14	5	ND	9	33	1	2	2	61	.33	.119	18	44	.58	133	.11	2	2.15	.03	.13	1
S 19+50N 16+00E	1	36	12	39	.4	18	7	269	2.93	5	6	ND	8	33	1	2	2	59	.44	.113	21	41	.48	97	.09	2	1.16	.03	.11	2
S 19+50N 16+50E	1	32	21	111	.1	21	9	345	3.63	10	5	ND	6	25	1	2	2	67	.24	.141	10	40	.47	85	.13	2	2.68	.03	.09	1
S 19+50N 17+00E	1	28	27	86	.4	19	8	980	3.39	6	5	ND	6	24	1	2	2	66	.28	.129	12	42	.45	153	.11	2	2.24	.03	.07	1
S 19+50N 17+50E	3	108	42	248	.7	19	14	2763	3.63	21	5	ND	6	50	3	2	2	59	.37	.114	23	27	.41	175	.13	2	3.05	.03	.09	1
STD C	18	57	38	132	7.1	67	27	1018	4.01	43	26	7	37	49	17	18	20	55	.47	.085	37	57	.85	175	.07	32	1.88	.08	.14	13

SAMPLE#	MO PPH	CU PPH	PB PPH	ZN PPH	AG PPH	NI PPH	CO PPH	MN PPH	FE %	AS PPH	U PPH	AU PPH	TH PPH	SR PPH	CU PPH	SB PPH	BI PPH	V PPH	CA %	P %	LA PPH	CR PPH	MG %	BA PPH	TI %	B PPH	AL %	NA %	K %	M PPH
S 19+50N 18+00E	2	57	36	221	.6	17	11	1672	3.42	18	5	ND	6	15	1	2	2	53	.14	.205	10	25	.37	176	.13	2	3.65	.03	.06	1
S 19+50N 18+50E	1	19	88	210	1.0	12	8	1395	3.28	2	5	ND	4	19	1	2	2	45	.17	.120	9	21	.27	199	.13	2	3.00	.03	.05	1
S 19+50N 19+00E	1	23	155	364	1.4	13	8	787	3.36	8	5	ND	8	18	1	2	2	47	.14	.097	16	20	.35	125	.12	2	4.13	.03	.06	3
S 19+50N 19+50E	1	42	181	372	1.0	14	6	548	3.50	11	5	ND	7	39	1	2	2	49	.33	.146	18	24	.47	269	.05	2	2.62	.03	.07	2
S 19+50N 20+00E	1	28	157	298	.8	10	5	457	3.44	10	5	ND	8	37	1	2	2	49	.31	.076	18	17	.39	125	.06	2	2.11	.02	.07	2
S 19+50N 20+50E	2	36	346	447	1.6	12	7	7114	3.15	12	5	ND	5	73	7	2	2	48	.56	.175	12	19	.23	444	.09	3	1.64	.04	.13	1
S 19+50N 21+50E	1	25	117	331	.7	12	8	1140	3.36	11	5	ND	7	63	2	2	2	42	.45	.203	15	21	.43	284	.11	2	3.35	.04	.08	1
S 19+50N 22+00E	1	13	99	257	1.3	8	6	1618	2.78	3	5	ND	6	25	2	2	2	38	.20	.171	11	14	.18	209	.10	2	2.01	.03	.06	1
S 19+50N 22+50E	1	21	54	138	1.0	14	7	872	3.14	4	5	ND	6	20	1	2	2	50	.18	.153	11	25	.31	127	.11	2	2.90	.03	.06	1
S 19+50N 23+00E	1	25	78	230	1.0	12	7	1091	2.82	8	5	ND	6	36	2	2	2	36	.32	.181	17	17	.27	227	.14	2	4.35	.04	.05	1
S 19+50N 23+50E	1	18	59	203	.9	10	6	1598	2.77	13	5	ND	5	62	2	2	2	33	.36	.289	8	15	.15	270	.14	2	2.73	.03	.06	1
S 19+50N 24+00E	1	26	121	191	.8	13	8	1208	3.63	7	5	ND	7	35	1	2	2	58	.26	.088	15	30	.40	164	.10	2	1.81	.03	.08	1
S 19+50N 24+50E	1	81	203	265	.7	19	9	841	4.06	18	5	ND	10	91	1	2	2	61	.59	.131	24	30	.68	158	.09	2	2.33	.04	.14	1
S 19+50N 25+00E	1	37	95	145	.7	16	9	1464	3.51	10	5	ND	4	61	1	2	2	62	.36	.073	11	34	.41	234	.10	3	1.65	.03	.10	1
S 19+50N 25+50E	1	35	221	322	.9	14	10	2107	3.53	17	5	ND	4	59	1	2	2	53	.40	.096	13	27	.42	199	.10	2	1.78	.03	.08	1
S 19+50N 26+00E	1	220	197	488	1.4	20	21	1755	3.96	6	5	ND	12	160	5	2	4	50	.85	.189	47	29	.60	256	.11	3	3.57	.05	.13	1
S 19+50N 26+50E	1	38	170	266	.8	14	9	1144	3.79	9	5	ND	5	50	2	2	2	58	.37	.094	16	25	.46	183	.11	2	1.70	.03	.08	2
S 19+50N 27+00E	1	59	171	276	.6	16	9	1363	3.87	10	5	ND	5	83	2	2	2	64	.57	.102	12	28	.54	273	.12	2	2.18	.04	.09	1
S 19+50N 27+50E	1	110	161	236	1.5	18	10	902	3.91	20	5	ND	5	63	1	2	2	63	.44	.099	15	31	.56	224	.12	2	3.32	.03	.11	1
S 19+50N 28+00E	1	170	211	441	.8	20	16	1271	4.61	8	5	ND	9	68	6	2	3	69	.45	.138	23	32	.86	250	.17	2	3.25	.04	.18	3
S 19+50N 28+50E	1	82	189	251	.8	15	10	874	3.80	10	5	ND	7	60	2	2	2	56	.36	.096	18	24	.49	186	.11	2	2.31	.03	.09	1
S 19+50N 29+00E	1	82	213	281	.8	16	17	1715	3.95	12	5	ND	7	91	2	2	2	56	.61	.171	21	25	.53	299	.10	2	2.54	.04	.12	1
S 19+50N 29+50E	1	64	146	269	.6	17	10	781	3.65	10	5	ND	5	53	3	2	2	57	.41	.098	15	25	.54	179	.12	2	2.25	.04	.09	1
S 19+50N 30+00E	2	69	52	167	.4	21	15	901	4.16	2	5	ND	6	39	1	2	2	67	.30	.147	13	27	.59	151	.16	2	3.06	.04	.12	1
S 20+00N 20+50E	1	38	131	515	1.2	11	8	3204	3.13	8	5	ND	6	18	4	2	2	38	.15	.249	12	16	.26	147	.14	2	4.65	.04	.08	1
S 20+00N 21+00E	1	17	136	323	.6	10	7	1019	3.38	8	5	ND	6	61	2	2	2	48	.48	.127	14	20	.31	204	.09	2	1.90	.03	.09	1
S 20+00N 21+50E	1	29	124	411	.7	14	8	1749	3.47	11	5	ND	10	34	3	2	2	44	.23	.293	20	22	.41	332	.13	2	3.97	.04	.11	1
S 20+00N 22+00E	1	24	54	128	.4	15	8	895	3.62	6	5	ND	6	25	1	2	2	66	.23	.144	13	37	.34	142	.10	2	2.04	.03	.06	1
S 20+00N 22+50E	1	33	101	167	.8	13	8	1155	3.19	8	5	ND	5	25	1	2	2	50	.20	.107	14	23	.34	142	.11	2	2.74	.03	.05	1
S 20+00N 23+00E	2	70	124	343	.7	20	11	2729	3.51	9	5	ND	6	63	2	2	2	48	.35	.141	22	30	.44	209	.15	2	3.07	.04	.09	3
S 20+00N 23+50E	1	46	70	141	.4	17	10	886	4.30	6	5	ND	5	43	1	2	2	85	.37	.072	13	39	.60	179	.13	2	2.48	.04	.11	1
S 20+00N 24+00E	1	38	125	198	1.4	14	8	856	3.41	7	5	ND	7	29	1	2	2	50	.19	.094	18	25	.40	140	.11	2	3.53	.03	.08	1
T 20+00N 24+50E	3	19713	24	832	17.3	9	49	953	3.28	71	5	ND	9	279	12	3	10	37	2.61	.029	14	145	.44	28	.01	2	1.41	.06	.17	1
S 20+00N 25+00E	1	37	93	203	1.0	15	8	1258	3.69	8	5	ND	6	26	1	2	2	60	.22	.101	19	29	.37	166	.12	2	3.05	.03	.06	1
S 20+00N 25+50E	1	32	174	413	.5	15	10	1823	3.23	12	5	ND	4	48	3	2	2	46	.38	.199	13	26	.32	248	.10	2	2.31	.04	.07	1
S 20+00N 26+00E	2	49	220	401	.6	17	13	3340	4.29	10	5	ND	4	93	3	2	2	73	.58	.109	18	36	.54	369	.11	2	2.29	.04	.10	1
S 20+00N 26+50E	1	47	212	433	1.0	15	11	2749	3.38	14	5	ND	4	152	4	2	2	53	.95	.098	14	25	.48	508	.10	2	1.69	.04	.11	1
S 20+00N 27+00E	1	71	175	360	.4	17	11	1594	3.60	13	5	ND	4	94	5	2	2	58	.51	.130	13	28	.55	331	.13	2	2.56	.04	.10	1
S 20+00N 27+50E	1	160	185	369	.8	19	13	1647	4.17	34	5	ND	4	81	3	2	4	66	.56	.108	14	29	.61	286	.15	2	2.62	.04	.14	1
STD C	18	58	40	132	7.4	68	27	1025	4.12	39	24	7	38	49	18	16	19	56	.49	.086	37	58	.86	177	.08	33	1.93	.08	.13	11

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	HG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
S 20+00N 28+00E	2	297	233	294	1.4	17	17	1351	4.74	17	5	ND	7	94	5	2	7	71	.60	.169	23	27	.86	422	.14	3	2.79	.04	.32	1
S 20+00N 28+50E	1	107	379	409	1.0	16	10	1228	4.06	20	5	ND	6	74	3	2	6	55	.44	.086	16	25	.53	282	.13	2	2.34	.04	.14	1
S 20+00N 29+00E	1	116	314	317	1.5	17	13	417	4.48	14	6	ND	9	42	1	2	3	60	.24	.095	21	27	.58	126	.13	2	3.28	.03	.14	1
S 20+00N 29+50E	1	53	179	262	.6	16	10	794	3.76	13	5	ND	6	55	2	2	2	53	.43	.071	14	23	.47	197	.14	2	2.83	.04	.11	1
S 20+00N 30+00E	1	52	61	177	.4	20	11	767	3.64	6	5	ND	5	64	1	2	2	58	.47	.138	12	26	.55	159	.15	3	2.81	.04	.10	1
S 20+50N 20+50E	2	192	220	417	4.5	14	9	2655	3.49	24	9	ND	7	67	5	2	2	43	.39	.124	45	24	.30	229	.15	2	4.33	.04	.13	2
S 20+50N 21+00E	1	26	187	432	.9	13	8	2353	3.04	11	5	ND	6	40	3	2	2	41	.27	.149	16	22	.35	231	.09	2	2.48	.03	.09	1
S 20+50N 21+50E	1	23	120	317	.7	12	8	2140	3.25	9	5	ND	6	33	4	2	2	39	.22	.269	16	20	.36	256	.11	3	3.37	.03	.11	1
S 20+50N 22+00E	1	34	80	178	.7	16	9	1303	3.16	4	5	ND	5	39	1	2	2	53	.31	.097	15	26	.41	189	.12	2	3.14	.03	.11	1
S 20+50N 22+50E	1	29	109	219	.5	14	10	1641	3.60	10	5	ND	5	35	2	2	2	58	.24	.090	14	25	.39	215	.12	2	2.34	.03	.09	2
S 20+50N 23+00E	1	37	88	193	.7	18	9	1151	3.83	11	5	ND	4	56	1	2	2	68	.43	.107	11	36	.51	263	.10	2	1.94	.03	.11	1
S 20+50N 23+50E	1	56	102	171	.6	14	10	794	3.67	8	5	ND	7	42	1	2	2	60	.27	.086	14	27	.45	147	.11	2	2.33	.03	.09	1
S 20+50N 24+00E	2	483	60	93	1.4	11	12	526	3.11	11	5	ND	7	30	1	2	2	40	.25	.107	20	20	.44	105	.06	2	2.20	.03	.10	3
S 20+50N 24+50E	2	141	91	125	.9	20	8	540	3.54	25	5	ND	10	42	1	2	2	58	.34	.098	21	37	.83	141	.11	2	2.67	.03	.15	7
S 20+50N 25+00E	1	39	146	286	.9	19	9	1524	3.38	10	5	ND	4	70	3	2	2	53	.48	.081	15	29	.41	218	.10	2	2.41	.03	.10	1
S 20+50N 25+50E	2	72	160	278	.7	22	12	1633	3.80	50	5	ND	4	112	2	2	2	65	.63	.146	14	37	.69	228	.09	2	2.59	.03	.21	3
S 20+50N 26+00E	2	112	43	202	.3	21	25	1658	4.47	7	5	ND	5	78	2	2	2	90	.44	.141	10	35	1.10	406	.19	2	3.19	.03	.51	1
S 20+50N 26+50E	1	58	157	391	.7	17	12	1849	3.67	13	5	ND	7	113	5	2	2	51	.71	.170	16	25	.43	359	.10	2	2.64	.04	.10	1
S 20+50N 27+00E	1	205	130	307	.6	22	24	1648	4.48	12	5	ND	5	90	3	2	2	75	.48	.099	16	37	.88	318	.15	2	3.26	.04	.23	1
S 20+50N 27+50E	1	370	227	343	1.9	25	22	1452	4.73	161	5	ND	6	79	4	2	7	66	.43	.106	19	30	.75	249	.13	2	3.33	.04	.21	2
S 20+50N 28+00E	1	179	251	575	.6	27	15	1145	4.40	12	5	ND	6	42	7	2	3	62	.26	.069	16	29	.64	187	.15	2	2.87	.03	.15	1
S 20+50N 28+50E	1	159	357	404	1.5	17	13	1075	4.63	16	5	ND	9	83	3	2	5	54	.51	.155	20	28	.61	300	.13	3	2.21	.04	.22	1
S 20+50N 29+00E	1	49	233	1076	.7	19	18	1414	3.68	11	5	ND	4	117	15	2	3	44	.91	.144	14	20	.38	308	.10	3	2.26	.04	.11	1
S 20+50N 29+50E	1	66	172	376	.7	18	13	1097	3.59	11	5	ND	5	53	4	2	3	48	.42	.103	12	20	.43	177	.13	2	2.83	.04	.08	1
S 20+50N 30+00E	1	130	96	267	.7	16	26	1713	4.42	8	5	ND	4	44	1	2	3	61	.33	.152	16	25	.61	150	.14	2	2.89	.04	.14	1
S 21+00N 20+50E	1	190	195	491	.9	18	10	3132	3.51	12	5	ND	7	53	4	2	3	43	.34	.228	20	24	.38	259	.11	2	3.81	.04	.11	1
S 21+00N 21+00E	1	30	199	537	1.0	15	8	1765	3.27	10	5	ND	8	41	4	2	2	42	.32	.166	21	20	.38	233	.12	2	3.81	.04	.10	1
S 21+00N 21+50E	1	45	146	310	.7	15	9	1569	3.32	11	5	ND	8	91	2	2	2	44	.51	.101	19	22	.46	269	.10	2	3.12	.03	.14	1
S 21+00N 22+00E	1	23	100	181	.6	12	7	970	3.18	9	5	ND	5	32	1	2	2	46	.25	.076	14	18	.32	139	.11	2	2.73	.03	.09	1
S 21+00N 22+50E	1	43	125	258	1.2	12	8	1544	3.24	15	5	ND	8	49	2	2	2	45	.33	.189	18	18	.33	218	.10	2	3.29	.03	.10	1
S 21+00N 23+00E	1	35	109	214	.6	14	9	1360	3.34	13	5	ND	5	60	2	2	2	55	.42	.130	14	23	.42	216	.09	2	2.36	.03	.12	1
S 21+00N 23+50E	1	33	95	204	.7	13	8	636	3.42	13	5	ND	5	38	1	2	2	55	.25	.131	12	22	.45	161	.08	2	1.92	.03	.09	1
S 21+00N 24+00E	1	34	133	380	.4	14	12	2236	3.45	7	5	ND	5	76	3	2	2	48	.44	.165	15	24	.47	287	.09	2	2.36	.03	.12	1
S 21+00N 24+50E	5	344	70	197	.6	30	17	1216	7.79	35	5	ND	12	85	1	4	2	115	.79	.216	26	148	2.39	221	.23	2	4.30	.04	1.86	7
S 21+00N 25+00E	1	47	244	351	.8	18	10	1497	3.59	14	5	ND	6	67	2	2	2	53	.44	.074	18	30	.48	234	.11	2	2.62	.03	.08	1
S 21+00N 25+50E	1	100	167	394	.6	29	16	3209	3.76	17	5	ND	6	81	5	2	2	51	.48	.134	17	51	.72	489	.12	2	2.85	.04	.24	1
S 21+00N 26+00E	1	36	190	303	.7	14	8	1495	3.07	14	5	ND	6	99	3	2	2	45	.55	.113	21	20	.43	226	.08	2	2.64	.03	.10	1
S 21+00N 26+50E	1	358	137	317	2.6	23	22	2015	4.26	8	5	ND	13	96	3	2	11	52	.46	.188	37	30	.78	341	.09	2	4.55	.03	.26	1
S 21+00N 27+00E	2	316	92	173	.9	20	14	1328	5.11	14	5	ND	6	72	1	2	4	76	.39	.107	14	27	.67	278	.15	2	3.62	.04	.23	1
STD C	18	58	41	132	7.1	67	27	1019	4.06	41	25	7	37	49	18	17	18	55	.48	.085	37	58	.85	175	.08	32	1.90	.08	.15	11

SAMPLE#	MO PPH	CU PPH	PB PPH	ZN PPH	AG PPH	NI PPH	CO PPH	MN PPH	FE %	AS PPH	U PPH	AU PPH	TH PPH	SR PPH	CD PPH	SB PPH	BI PPH	V PPH	CA %	P %	LA PPH	CR PPH	MG %	BA PPH	TI %	B PPH	AL %	NA %	K %	M PPH
S 21+00N 27+50E	2	453	157	253	2.3	21	18	846	5.07	13	5	ND	5	48	2	2	4	69	.16	.094	19	52	.79	165	.11	2	3.10	.03	.21	2
S 21+00N 28+00E	1	75	233	391	.7	16	12	901	3.92	28	5	ND	6	56	6	2	2	60	.42	.062	15	23	.56	181	.13	2	2.99	.03	.11	1
S 21+00N 28+50E	1	98	434	739	1.1	19	12	864	4.35	17	5	ND	8	64	8	2	3	58	.47	.084	23	25	.56	200	.14	2	3.22	.04	.11	1
S 21+00N 29+00E	1	58	248	414	.9	16	10	1325	3.72	12	5	ND	5	60	4	2	2	50	.45	.118	13	22	.45	311	.13	2	3.18	.04	.11	1
S 21+00N 29+50E	1	116	179	501	.8	19	33	1455	4.00	16	5	ND	3	115	5	2	4	52	.63	.130	13	20	.42	204	.10	3	1.75	.04	.11	2
S 21+00N 29+75E	2	147	234	748	.8	29	28	1478	5.24	10	5	ND	7	56	4	2	4	76	.42	.088	17	31	.73	221	.18	2	3.40	.04	.15	1
S 21+50N 20+50E	2	26	167	290	.7	13	8	1066	3.18	7	5	ND	10	27	2	2	2	47	.20	.103	15	17	.33	150	.14	3	3.89	.03	.07	1
S 21+50N 21+00E	1	24	97	256	.8	14	9	1039	3.26	11	5	ND	7	32	2	2	2	46	.24	.334	13	20	.32	225	.11	2	3.43	.03	.10	1
S 21+50N 21+50E	1	26	129	215	.7	11	7	1063	3.24	11	5	ND	6	39	1	2	2	52	.27	.083	17	19	.34	145	.09	2	2.40	.03	.07	2
S 21+50N 22+00E	1	159	183	356	1.1	22	10	2279	3.71	23	10	ND	7	108	2	2	2	52	.48	.111	68	30	.48	176	.10	2	3.39	.04	.15	1
S 21+50N 22+50E	1	31	105	262	.7	12	9	2982	2.86	9	5	ND	4	45	3	2	2	39	.31	.145	14	17	.28	238	.10	2	2.87	.03	.06	1
S 21+50N 23+00E	1	26	119	169	.5	10	6	1176	2.67	9	5	ND	5	63	1	2	2	41	.36	.060	13	15	.31	134	.08	2	2.01	.03	.05	4
S 21+50N 23+50E	3	72	119	269	.6	25	18	2570	3.97	11	5	ND	9	57	2	2	2	55	.35	.191	25	45	.66	287	.12	2	2.96	.03	.13	1
S 21+50N 24+00E	1	25	119	250	.5	13	7	1405	3.40	7	5	ND	5	63	1	2	2	54	.36	.077	19	21	.40	190	.08	2	1.92	.03	.08	1
S 21+50N 24+50E	1	24	101	182	1.0	10	6	529	3.67	9	5	ND	8	36	1	2	2	61	.29	.057	21	19	.39	112	.09	2	1.51	.03	.07	3
S 21+50N 25+00E	1	46	202	314	.8	15	10	1661	3.38	11	5	ND	5	94	2	2	2	55	.53	.091	19	26	.46	228	.11	3	2.74	.04	.10	1
S 21+50N 25+50E	1	36	231	428	1.0	15	10	1509	3.46	14	5	ND	7	93	5	4	2	51	.54	.141	21	23	.45	280	.12	3	3.32	.04	.12	1
S 21+50N 26+00E	1	31	205	327	.7	14	8	1758	3.38	12	5	ND	7	76	3	2	2	52	.41	.081	21	23	.46	261	.08	2	2.23	.03	.13	1
S 21+50N 26+50E	2	496	191	350	3.1	20	31	2604	4.24	14	5	ND	11	72	2	2	19	51	.38	.143	33	41	.71	287	.08	2	3.89	.03	.21	1
S 21+50N 27+00E	3	586	127	200	1.8	23	25	1155	5.63	15	5	ND	7	40	1	2	6	82	.24	.114	19	30	.83	208	.16	2	4.28	.03	.22	1
S 21+50N 27+50E	1	92	151	326	.5	16	17	855	4.28	14	5	ND	4	80	4	2	2	66	.44	.073	16	24	.57	197	.13	2	3.12	.03	.13	2
S 21+50N 28+00E	1	71	220	367	.9	15	11	597	3.97	21	5	ND	7	40	3	2	2	61	.27	.054	14	24	.54	150	.14	2	3.10	.03	.12	1
S 21+50N 28+50E	1	71	448	771	.9	17	12	1055	4.56	22	5	ND	6	54	7	2	6	59	.38	.078	15	25	.55	206	.13	2	2.33	.03	.12	1
S 21+50N 29+00E	1	87	789	868	2.0	24	12	984	4.70	27	5	ND	9	73	8	2	7	55	.47	.122	28	34	.61	216	.13	2	3.39	.04	.16	1
S 21+50N 29+50E	1	73	300	1143	.8	25	22	1703	4.12	16	5	ND	5	76	15	2	3	58	.58	.069	16	24	.53	293	.18	3	2.80	.05	.11	1
S 21+50N 30+00E	5	277	158	154	.8	18	36	1344	5.54	23	5	ND	5	39	3	2	6	62	.18	.204	16	20	.47	109	.08	2	2.03	.03	.15	1
S 22+00N 20+50E	1	25	105	194	.6	13	7	496	3.62	8	5	ND	8	35	1	2	2	59	.27	.058	16	22	.37	112	.11	2	2.29	.03	.09	1
S 22+00N 21+00E	1	33	207	450	1.1	15	9	1631	3.17	13	5	ND	9	67	3	2	2	41	.41	.252	21	20	.38	197	.10	2	3.47	.04	.13	1
S 22+00N 21+50E	1	26	88	214	.6	15	8	1145	3.21	9	5	ND	7	60	1	2	2	52	.41	.126	14	23	.40	185	.10	2	2.44	.03	.12	1
S 22+00N 22+00E	1	22	152	234	.5	11	7	1680	3.04	12	5	ND	5	94	2	2	2	45	.56	.073	16	16	.35	211	.10	3	2.26	.03	.10	1
S 22+00N 22+50E	1	30	180	274	.8	13	7	1735	2.99	11	5	ND	5	78	2	2	2	44	.46	.108	19	16	.35	208	.08	2	2.38	.03	.10	3
S 22+00N 23+00E	1	29	129	181	.6	12	7	1137	3.08	7	5	ND	5	53	1	2	2	48	.35	.070	16	19	.39	168	.08	2	2.14	.03	.07	1
S 22+00N 23+50E	1	27	107	228	.6	13	8	1031	3.18	8	5	ND	6	31	1	2	2	49	.23	.141	14	21	.39	162	.08	2	2.52	.03	.09	1
S 22+00N 24+00E	1	40	148	269	.9	16	9	1103	3.49	10	5	ND	8	52	1	2	2	54	.28	.063	20	27	.53	190	.10	2	2.56	.03	.11	2
S 22+00N 24+50E	1	50	130	255	.7	19	13	1598	3.93	12	5	ND	6	73	2	2	2	66	.43	.078	16	32	.60	229	.13	2	2.72	.03	.13	1
S 22+00N 25+00E	1	54	161	313	1.3	19	12	1212	3.83	11	5	ND	5	53	2	2	2	69	.36	.107	15	37	.52	173	.10	2	2.19	.03	.11	1
S 22+00N 25+50E	1	34	214	334	.6	14	9	1770	3.44	13	5	ND	7	67	3	2	2	53	.39	.104	21	23	.48	232	.10	2	2.78	.03	.11	1
S 22+00N 26+00E	1	90	195	328	.9	18	13	1783	3.58	9	5	ND	9	56	2	2	2	54	.35	.112	31	26	.53	178	.10	2	3.15	.03	.12	1
S 22+00N 26+50E	1	35	229	361	.9	16	9	1773	3.46	14	5	ND	14	83	3	2	3	51	.51	.113	22	27	.56	313	.07	2	2.86	.03	.14	1
STD C	18	58	41	132	7.2	67	28	1031	4.04	40	22	7	37	49	18	17	19	58	.47	.085	36	57	.85	174	.07	32	1.89	.08	.13	12

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	M PPM
S 22+00N 27+00E	2	668	243	497	3.9	32	24	1262	6.09	23	5	ND	9	60	3	2	14	73	.37	.158	21	43	.85	237	.15	2	4.44	.05	.21	1
S 22+00N 27+50E	1	98	251	451	1.2	16	33	1357	4.31	18	5	ND	6	62	4	2	2	62	.38	.119	31	25	.57	162	.09	2	3.19	.04	.16	1
S 22+00N 28+00E	2	108	456	678	1.8	18	14	815	4.65	28	7	ND	7	65	4	2	6	58	.48	.078	19	25	.57	209	.14	2	3.46	.04	.16	1
S 22+00N 28+50E	1	91	595	841	1.6	19	12	1504	4.62	30	5	ND	8	92	11	2	5	54	.70	.109	22	26	.63	317	.13	3	3.05	.04	.19	1
S 22+00N 29+00E	1	66	515	946	1.8	21	14	769	4.72	21	5	ND	10	64	5	2	2	57	.48	.077	26	29	.67	211	.17	2	3.83	.05	.15	1
S 22+00N 29+50E	1	102	200	378	.9	38	17	1402	4.66	52	5	ND	6	82	3	2	2	60	.68	.084	14	35	.75	329	.16	2	4.11	.05	.18	1
S 22+00N 29+85E	2	132	244	450	1.3	30	27	904	5.05	21	6	ND	7	55	1	2	3	63	.36	.130	20	30	.72	182	.12	2	3.84	.04	.17	1
S 22+50N 20+50E	1	31	146	248	.7	11	7	1039	3.54	12	5	ND	7	40	1	2	2	54	.26	.104	16	19	.35	149	.10	2	2.82	.03	.09	1
S 22+50N 21+00E	1	53	345	574	1.3	19	9	1215	3.47	22	5	ND	15	84	3	2	2	45	.43	.179	34	27	.61	268	.11	2	3.40	.04	.20	1
S 22+50N 21+50E	1	31	170	553	.6	15	10	1886	3.29	11	5	ND	9	71	6	2	2	41	.38	.293	21	23	.39	249	.10	2	3.08	.04	.14	1
S 22+50N 22+00E	1	105	141	273	.7	15	11	1501	3.61	14	5	ND	10	61	2	2	2	50	.35	.130	23	25	.51	201	.10	2	3.07	.03	.19	2
S 22+50N 22+50E	1	35	183	285	.5	11	8	1979	3.08	13	5	ND	6	96	2	2	2	45	.63	.108	17	18	.42	286	.08	2	2.14	.03	.13	1
S 22+50N 23+00E	1	26	197	354	.9	14	9	1851	3.08	15	6	ND	9	72	3	2	2	41	.45	.154	21	21	.44	273	.12	3	3.26	.04	.15	2
S 22+50N 23+50E	1	42	211	287	1.4	14	8	1624	3.26	18	5	ND	11	70	2	2	2	46	.38	.110	26	22	.49	234	.11	2	3.56	.04	.14	1
S 22+50N 24+00E	1	20	158	250	.5	15	7	1713	3.16	15	5	ND	6	74	1	2	2	43	.44	.124	24	23	.53	284	.05	2	2.79	.03	.15	1
S 22+50N 24+50E	1	68	307	266	.9	16	8	744	4.28	16	5	ND	14	54	1	2	2	61	.33	.082	33	33	.74	185	.10	2	2.13	.03	.19	1
S 22+50N 25+00E	1	35	156	259	.8	19	9	1095	3.47	16	5	ND	8	100	2	2	2	52	.50	.147	25	30	.69	283	.09	2	2.68	.04	.20	1
S 22+50N 25+50E	1	34	285	333	.8	15	9	2278	3.83	16	5	ND	7	78	3	2	2	54	.44	.116	21	26	.52	343	.07	2	2.93	.03	.13	1
S 22+50N 26+00E	1	170	243	357	1.2	22	19	1809	4.66	19	5	ND	9	74	2	2	4	60	.42	.122	28	42	.77	261	.10	2	3.68	.03	.20	1
S 22+50N 26+50E	3	927	228	636	2.9	25	22	1808	5.89	395	6	ND	13	103	6	2	15	62	.57	.179	23	35	.74	403	.14	2	3.94	.05	.20	1
S 22+50N 27+00E	2	191	183	1014	1.7	23	26	1114	5.72	90	5	ND	6	52	4	2	3	60	.28	.108	20	38	.69	192	.12	2	4.12	.04	.17	1
S 22+50N 27+50E	1	60	344	676	1.1	17	15	1255	3.97	19	5	ND	7	43	4	2	4	49	.32	.054	18	23	.46	202	.13	2	2.97	.03	.11	2
S 22+50N 28+00E	1	83	556	871	3.2	24	12	551	4.52	21	5	ND	8	79	3	2	4	58	.64	.086	19	25	.71	243	.17	2	4.04	.05	.16	1
S 22+50N 28+50E	2	107	821	951	3.0	19	17	1147	4.58	27	5	ND	6	66	5	2	9	51	.51	.119	29	27	.62	208	.11	2	2.94	.04	.18	2
S 22+50N 29+00E	1	103	318	544	1.4	26	19	1115	5.05	17	5	ND	8	104	3	2	4	58	.64	.144	24	26	.82	237	.14	2	3.69	.05	.23	1
S 22+50N 29+50E	2	188	151	422	1.0	36	31	1122	6.02	61	5	ND	5	121	4	2	2	64	1.00	.136	15	26	.72	207	.13	4	3.61	.05	.25	1
S 22+50N 30+00E	5	657	81	121	.6	15	37	567	10.03	17	6	ND	7	49	1	2	2	112	.24	.179	15	31	.65	100	.17	2	4.86	.05	.31	1
S 23+00N 20+50E	1	111	125	199	1.1	11	8	918	3.06	13	7	ND	7	40	1	2	2	45	.24	.082	17	16	.37	117	.08	2	2.78	.03	.12	1
S 23+00N 21+00E	1	224	153	274	.7	20	12	2304	3.46	12	5	ND	11	67	2	2	2	50	.37	.089	23	30	.59	258	.11	2	3.30	.03	.18	1
S 23+00N 21+50E	1	59	215	504	1.0	19	10	1761	3.02	16	5	ND	8	89	6	2	2	38	.60	.226	21	25	.51	264	.11	2	3.03	.04	.14	1
S 23+00N 22+00E	1	86	162	340	.5	22	12	1973	3.80	16	5	ND	9	90	3	2	2	54	.43	.145	20	35	.75	290	.11	2	3.40	.03	.24	1
S 23+00N 22+50E	1	58	177	328	.6	20	11	1768	3.80	15	5	ND	11	81	3	2	2	53	.43	.115	24	33	.73	309	.11	2	3.69	.03	.22	1
S 23+00N 23+00E	1	34	172	207	.5	13	9	1905	3.56	13	5	ND	9	78	2	2	2	50	.40	.080	21	21	.44	294	.10	2	2.51	.03	.13	1
S 23+00N 23+50E	1	22	183	327	.5	11	8	2492	2.88	10	5	ND	8	77	5	2	2	40	.39	.079	25	17	.41	322	.07	2	2.72	.03	.11	2
S 23+00N 24+00E	1	44	291	332	.7	15	9	1776	3.57	15	5	ND	7	99	2	2	2	49	.45	.101	24	27	.55	303	.07	2	2.75	.03	.15	2
S 23+00N 24+50E	1	124	131	252	.3	18	16	1060	4.57	26	5	ND	10	75	1	2	2	73	.37	.092	30	27	.75	254	.09	2	3.92	.03	.27	2
S 23+00N 25+00E	1	64	306	460	1.1	27	13	4393	3.24	15	5	ND	7	119	3	2	2	42	.72	.117	25	41	.54	335	.08	2	2.13	.04	.16	1
S 23+00N 25+50E	1	28	227	273	.7	15	9	2224	3.51	11	5	ND	7	63	2	2	2	49	.35	.079	21	24	.48	279	.08	2	2.74	.03	.10	1
S 23+00N 26+00E	1	102	254	301	1.4	19	12	1542	3.91	17	5	ND	9	56	2	2	2	52	.35	.135	24	33	.67	272	.07	2	3.14	.03	.17	1
STD C	18	58	39	132	7.2	68	27	1031	4.06	44	25	7	38	49	18	18	19	56	.48	.086	37	58	.85	177	.08	32	1.89	.08	.15	11

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MM	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	M
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM
S 23+00N 26+50E	3	237	418	630	1.7	18	15	1303	7.53	59	5	ND	6	124	4	2	8	75	.61	.118	15	36	.90	325	.16	3	3.74	.05	.22	1
S 23+00N 27+00E	1	128	396	884	1.5	22	19	1461	5.07	22	5	ND	5	67	5	2	5	48	.49	.120	15	24	.49	207	.11	2	3.05	.03	.11	1
S 23+00N 27+50E	1	91	432	740	2.1	23	18	1078	4.62	17	5	ND	7	42	3	2	8	52	.32	.095	22	28	.58	159	.14	2	3.29	.03	.10	1
S 23+00N 28+00E	1	110	772	1273	3.0	26	14	666	5.00	22	5	ND	8	51	4	2	8	53	.33	.078	22	33	.68	136	.14	2	3.53	.04	.12	1
S 23+00N 28+50E	1	85	459	931	1.7	25	14	987	4.83	9	5	ND	9	45	5	2	4	59	.34	.109	22	27	.67	262	.17	2	3.57	.04	.15	1
S 23+00N 29+00E	1	95	280	654	1.1	34	30	1918	4.95	18	5	ND	4	84	5	2	2	64	.59	.256	23	53	1.28	355	.12	2	3.69	.05	.28	1
S 23+00N 29+50E	1	100	330	471	.8	31	20	1444	4.92	21	5	ND	6	53	5	2	2	59	.31	.174	19	40	.92	261	.13	2	3.62	.04	.17	1
S 23+00N 30+00E	1	103	84	236	.4	19	26	1146	5.94	5	5	ND	7	49	1	2	2	94	.38	.088	18	20	1.11	221	.26	2	3.03	.04	.30	1
S 23+50N 20+50E	1	157	114	237	.6	15	11	1589	3.31	7	5	ND	9	34	2	2	2	43	.18	.092	23	20	.44	225	.10	2	3.80	.03	.09	1
S 23+50N 21+00E	1	99	336	506	1.2	18	9	1455	3.37	11	5	ND	8	70	2	2	2	45	.37	.073	20	28	.59	228	.08	2	2.97	.03	.12	1
S 23+50N 21+50E	1	123	336	662	1.3	32	14	1689	3.90	21	5	ND	13	82	2	2	2	52	.43	.154	28	44	.87	312	.12	2	3.75	.03	.18	1
S 23+50N 22+00E	1	36	201	433	.6	16	9	2560	3.32	8	5	ND	8	72	3	2	2	43	.38	.188	18	24	.55	321	.10	2	3.22	.03	.18	1
S 23+50N 22+50E	1	34	197	354	.3	17	9	1653	3.27	10	5	ND	10	66	2	2	2	44	.41	.127	23	26	.62	245	.10	2	3.01	.03	.16	1
S 23+50N 23+00E	1	28	202	259	.3	11	8	1950	2.82	9	5	ND	5	115	4	2	2	40	.60	.117	20	16	.34	280	.06	2	1.93	.03	.11	1
S 23+50N 23+50E	1	22	148	250	.7	12	7	1807	3.10	8	5	ND	7	78	2	2	2	43	.39	.093	21	19	.42	223	.07	2	2.54	.03	.08	1
S 23+50N 24+00E	1	29	208	281	.8	12	7	1839	3.21	8	5	ND	6	81	2	2	2	43	.40	.088	20	20	.43	276	.08	2	2.50	.03	.09	1
S 23+50N 24+50E	1	35	139	435	1.0	16	10	937	3.38	9	5	ND	12	61	3	2	2	41	.40	.267	28	20	.47	314	.10	2	3.66	.04	.13	1
S 23+50N 25+00E	1	122	170	331	.8	38	20	1539	4.55	8	5	ND	16	72	1	2	2	56	.35	.159	32	55	1.14	335	.13	2	4.27	.04	.29	1
S 23+50N 25+50E	1	30	198	310	.6	16	8	1496	3.33	6	5	ND	8	52	2	2	2	46	.24	.080	23	27	.58	245	.08	2	2.68	.02	.10	1
S 23+50N 26+00E	1	84	271	440	1.4	23	19	2396	3.47	6	5	ND	7	59	3	2	2	43	.35	.106	28	27	.53	205	.07	2	2.78	.03	.08	1
S 23+50N 26+50E	2	164	308	863	2.6	20	33	1191	4.84	6	5	ND	9	61	4	2	12	53	.30	.105	40	28	.60	147	.13	2	3.30	.04	.11	1
S 23+50N 27+00E	2	120	299	675	1.4	21	18	1406	5.51	16	5	ND	5	41	3	2	2	62	.22	.145	14	29	.64	195	.14	2	3.75	.03	.16	1
S 23+50N 27+50E	1	94	723	577	2.3	18	11	992	5.04	19	5	ND	6	35	2	2	6	48	.20	.115	16	25	.51	142	.12	2	3.55	.03	.10	1
S 23+50N 28+00E	1	85	712	1168	2.5	16	12	738	4.46	29	5	ND	8	41	4	2	8	46	.24	.080	17	26	.51	140	.12	2	2.91	.04	.11	1
S 23+50N 28+50E	1	65	493	506	1.5	17	9	1025	3.94	13	5	ND	6	58	3	2	3	47	.39	.116	19	22	.63	253	.13	2	3.15	.05	.13	1
S 23+50N 29+00E	1	58	210	542	1.1	20	12	1158	3.76	11	7	ND	7	71	4	2	2	44	.43	.104	21	23	.56	276	.15	2	3.68	.05	.10	1
S 23+50N 29+50E	2	53	307	695	.7	17	21	2363	3.78	16	5	ND	3	77	7	2	2	51	.62	.138	17	21	.51	265	.09	2	2.57	.04	.12	2
S 23+50N 30+00E	1	51	236	301	1.2	16	15	598	3.30	10	5	ND	5	20	1	2	2	39	.15	.093	13	19	.36	112	.13	2	2.99	.03	.07	1
S 24+00N 20+50E	1	32	191	268	.4	13	8	3434	2.75	8	5	ND	6	92	3	2	2	37	.49	.071	17	19	.46	318	.08	2	2.45	.03	.10	1
S 24+00N 21+00E	1	95	168	458	.8	22	10	1036	3.16	13	5	ND	8	60	3	2	2	40	.36	.151	11	23	.46	186	.10	2	3.12	.03	.11	1
S 24+00N 21+50E	1	156	180	552	.6	21	13	2116	3.68	10	5	ND	10	68	7	2	2	42	.30	.246	20	29	.54	302	.12	2	3.44	.03	.15	1
S 24+00N 22+00E	2	34	287	591	.6	14	8	11232	2.62	16	5	ND	3	133	9	2	2	34	.59	.084	15	21	.42	638	.07	2	2.16	.03	.14	1
S 24+00N 22+50E	1	32	143	340	.5	14	9	1628	3.10	8	5	ND	8	99	4	2	2	40	.56	.137	24	20	.46	258	.09	2	2.83	.03	.15	1
S 24+00N 23+00E	1	30	188	318	.4	12	7	2791	2.88	8	5	ND	6	80	4	2	2	38	.47	.155	19	18	.35	339	.07	5	2.24	.03	.09	1
S 24+00N 23+50E	1	22	178	309	.6	13	6	2509	2.57	7	5	ND	5	144	3	2	2	34	.78	.153	18	19	.44	455	.05	2	2.16	.03	.11	1
S 24+00N 24+00E	1	27	192	228	.8	10	6	1254	3.19	6	5	ND	5	54	1	2	3	44	.28	.081	18	18	.39	167	.06	2	2.06	.02	.09	1
S 24+00N 24+50E	1	31	155	353	.6	12	9	1646	3.04	8	5	ND	6	82	3	2	2	40	.45	.132	18	18	.38	282	.09	2	2.55	.03	.10	1
S 24+00N 25+00E A	1	33	218	346	1.0	16	8	2814	3.32	6	5	ND	8	94	3	2	2	45	.43	.115	22	24	.54	330	.07	2	2.73	.03	.11	1
S 24+00N 25+00E B	1	36	229	430	.7	12	12	2583	2.90	11	5	ND	6	75	6	2	2	35	.40	.197	22	17	.34	249	.06	2	1.90	.03	.09	1
STD C	18	58	38	131	7.0	67	27	1021	4.07	39	21	7	38	49	18	16	18	56	.48	.085	36	58	.85	175	.08	31	1.91	.08	.13	12

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	HG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
S 24+00N 25+50E	1	31	172	289	.4	16	8	1606	3.47	9	5	ND	7	76	2	2	2	48	.49	.148	20	28	.63	337	.06	2	2.66	.03	.17	2
S 24+00N 26+00E	1	67	267	387	1.3	22	13	1844	3.75	17	5	ND	5	70	3	2	5	46	.42	.098	17	28	.54	255	.10	2	2.59	.03	.12	1
S 24+00N 26+50E	1	96	670	961	1.9	19	14	1029	5.20	11	5	ND	6	81	8	2	8	63	.43	.109	15	32	.74	254	.15	3	3.52	.04	.14	2
S 24+00N 27+00E	1	93	556	572	1.8	17	10	1003	5.50	11	5	ND	5	45	1	2	4	48	.26	.119	12	24	.56	136	.13	3	3.83	.03	.10	1
S 24+00N 27+50E	1	85	858	826	2.4	18	12	1109	4.58	27	5	ND	5	33	2	2	3	47	.22	.080	16	29	.62	154	.11	2	3.00	.03	.12	1
S 24+00N 28+00E	1	79	824	681	2.7	14	8	1068	4.32	31	5	ND	3	49	4	2	7	43	.30	.102	15	24	.50	181	.08	2	2.34	.03	.12	3
S 24+00N 28+50E	1	54	478	520	.8	17	11	1162	4.08	14	5	ND	5	38	2	2	2	50	.24	.122	16	23	.63	181	.12	2	2.83	.04	.10	1
S 24+00N 29+00E	1	67	473	394	1.5	17	9	1076	4.32	27	5	ND	5	39	2	2	2	54	.24	.142	17	27	.67	232	.12	2	2.94	.03	.11	1
S 24+00N 29+50E	2	48	164	288	.7	18	14	1264	4.09	14	5	ND	3	41	2	2	2	66	.38	.114	8	22	.59	179	.11	2	3.66	.03	.12	2
S 24+00N 30+00E	1	61	260	375	.5	16	12	1505	4.28	13	5	ND	3	67	3	2	2	46	.47	.151	8	30	.58	235	.10	2	2.16	.03	.10	2
S 24+50N 20+50E	1	156	228	315	1.3	17	12	2084	3.58	16	5	ND	10	74	2	2	2	46	.49	.119	22	24	.57	261	.10	2	3.80	.03	.16	1
S 24+50N 21+00E	1	82	247	334	.8	15	11	2206	3.26	12	5	ND	7	98	4	2	2	42	.49	.150	21	24	.57	305	.08	2	2.97	.03	.16	1
S 24+50N 21+50E	1	42	471	713	1.0	14	9	3117	3.03	13	5	ND	7	89	8	2	2	35	.51	.131	24	21	.52	362	.07	2	2.37	.03	.15	1
S 24+50N 22+00E	1	23	204	309	.4	14	9	1830	3.21	8	5	ND	10	53	3	2	2	44	.32	.121	21	23	.53	274	.11	2	2.73	.03	.15	1
S 24+50N 22+50E	1	40	178	297	.6	16	10	1824	3.46	18	5	ND	8	69	2	2	2	47	.39	.126	24	25	.62	247	.09	2	3.11	.03	.15	3
S 24+50N 23+00E	1	23	197	264	.9	12	7	2697	3.07	13	5	ND	6	61	3	2	2	44	.30	.084	22	18	.43	321	.07	2	2.61	.02	.10	2
S 24+50N 23+50E	1	28	227	317	.3	12	7	1913	2.93	16	5	ND	4	121	2	2	2	39	.57	.163	17	19	.47	376	.04	2	2.11	.03	.12	2
S 24+50N 24+00E	1	54	186	313	1.0	11	11	2383	3.14	37	5	ND	5	83	6	2	2	38	.40	.165	17	18	.37	382	.04	2	2.09	.02	.14	2
S 24+50N 24+50E	1	44	189	575	.5	13	14	2932	2.98	12	5	ND	5	97	11	2	2	36	.58	.158	18	18	.35	337	.07	4	2.23	.03	.10	1
S 24+50N 25+00E A	1	42	195	550	.7	12	14	2776	2.91	11	5	ND	5	100	11	2	2	35	.60	.145	16	17	.35	319	.07	2	2.10	.03	.10	1
S 24+50N 25+00E B	1	36	196	304	.7	13	11	2043	3.19	11	5	ND	6	66	3	2	2	45	.54	.082	24	19	.44	180	.07	2	2.06	.03	.11	1
S 24+50N 25+50E	1	29	238	378	.9	13	8	1060	3.21	10	5	ND	5	51	2	2	2	44	.33	.049	14	20	.44	174	.09	2	2.19	.03	.10	1
S 24+50N 26+00E	1	70	415	473	1.0	17	9	1326	3.92	18	5	ND	5	108	3	2	6	50	.56	.100	16	27	.64	339	.09	2	2.02	.03	.14	2
S 24+50N 26+50E	1	103	469	411	1.7	13	10	1279	4.75	19	5	ND	3	57	4	2	4	44	.31	.183	15	21	.45	191	.07	2	2.47	.03	.10	1
S 24+50N 27+00E	2	70	1785	946	3.3	17	17	3343	4.61	34	5	ND	4	63	5	2	4	48	.50	.137	16	24	.48	217	.09	2	2.17	.03	.11	1
S 24+50N 27+50E	1	55	675	1506	1.1	38	11	1055	3.85	22	5	ND	5	32	4	2	4	42	.26	.110	14	30	.59	143	.12	2	3.31	.03	.08	1
S 24+50N 28+00E	1	58	596	656	1.5	17	10	1297	4.49	22	5	ND	4	61	3	2	2	55	.42	.174	17	25	.75	314	.12	2	2.45	.04	.14	1
S 24+50N 28+50E	1	52	497	397	1.7	20	8	916	4.09	23	6	ND	5	21	1	2	3	47	.14	.116	13	24	.51	147	.11	2	3.07	.03	.09	1
S 24+50N 29+00E	1	55	431	453	1.2	17	9	1306	3.99	23	5	ND	4	68	2	2	2	49	.45	.081	14	22	.59	309	.11	2	2.63	.03	.10	1
S 24+50N 29+50E	1	44	334	391	1.0	14	9	1315	3.63	14	5	ND	5	43	1	2	2	47	.38	.140	8	18	.45	232	.10	5	2.63	.03	.10	1
S 24+50N 30+00E	1	50	229	381	1.2	24	10	689	4.39	11	6	ND	6	36	1	2	5	54	.29	.078	11	34	.74	181	.16	2	3.32	.03	.10	1
S 25+00N 20+50E	1	167	217	434	1.7	15	8	3303	2.87	16	5	ND	6	89	3	2	2	38	.48	.104	22	19	.45	368	.08	2	2.78	.03	.12	1
S 25+00N 21+00E	1	21	255	335	.5	10	6	2514	2.66	12	5	ND	6	61	3	2	2	34	.36	.094	17	15	.43	282	.06	2	2.32	.02	.13	1
S 25+00N 21+50E	1	29	247	470	.3	14	8	1864	3.10	9	5	ND	8	63	3	2	2	39	.40	.167	16	20	.49	326	.09	2	2.54	.03	.13	1
S 25+00N 22+00E	1	82	100	531	.6	14	13	3021	3.68	11	5	ND	7	107	8	2	2	38	.45	.141	17	19	.56	639	.12	2	2.30	.03	.19	1
S 25+00N 22+50E	1	24	179	290	.5	13	7	1708	2.85	15	5	ND	6	71	2	2	2	38	.41	.155	18	21	.50	303	.06	2	2.17	.03	.16	3
S 25+00N 23+00E	1	16	154	250	.6	10	6	2297	2.74	8	5	ND	5	57	2	2	2	39	.30	.088	16	15	.35	311	.06	2	2.22	.03	.10	1
S 25+00N 23+50E	1	38	182	290	.8	13	7	1569	2.94	14	5	ND	5	82	3	2	2	40	.41	.141	16	19	.45	263	.05	2	2.41	.02	.12	1
S 25+00N 24+00E	1	21	175	259	.6	11	7	1969	2.89	9	5	ND	4	79	2	2	2	39	.39	.078	15	18	.38	184	.05	2	1.82	.02	.11	1
STD C	18	59	39	130	7.0	67	27	1026	4.03	41	20	7	37	48	18	16	19	55	.47	.085	36	58	.88	174	.07	31	1.87	.08	.13	11

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MM PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
S 25+00N 24+50E	1	26	213	299	.7	13	8	1858	2.92	12	5	ND	5	86	3	2	2	41	.43	.074	16	21	.47	290	.06	2	2.21	.03	.12	1
S 25+00N 25+00E	1	30	204	334	.9	11	9	1023	3.01	14	5	ND	5	37	2	2	2	43	.31	.071	19	20	.39	121	.09	2	2.35	.03	.08	2
S 25+00N 25+50E	1	40	301	574	1.1	13	11	2075	3.37	15	5	ND	5	77	9	2	2	44	.46	.079	17	21	.43	248	.12	2	2.58	.04	.10	1
S 25+00N 26+00E	1	48	305	791	1.3	30	11	1688	3.75	10	5	ND	6	49	9	2	6	45	.36	.166	14	26	.45	291	.14	3	3.72	.04	.11	1
S 25+00N 26+50E	2	329	366	409	2.7	14	17	1873	6.33	261	5	ND	4	46	3	2	8	52	.23	.203	18	24	.56	204	.07	3	2.72	.03	.13	2
S 25+00N 27+00E	2	58	561	580	1.2	14	14	1884	3.58	18	5	ND	4	43	4	2	3	46	.31	.113	21	23	.50	153	.07	3	2.63	.03	.10	1
S 25+00N 27+50E	1	43	369	890	1.2	19	11	1937	3.47	26	5	ND	5	43	6	2	5	41	.34	.149	15	26	.49	181	.11	2	2.70	.04	.09	1
S 25+00N 28+00E	1	60	575	630	1.2	16	10	1004	4.12	18	5	ND	5	54	2	2	6	53	.37	.175	18	23	.78	277	.13	2	2.85	.05	.14	2
S 25+00N 28+50E	2	28	291	482	1.0	23	11	1639	3.96	12	5	ND	9	47	2	2	2	56	.34	.149	23	30	.93	309	.15	2	2.73	.04	.13	2
S 25+00N 29+00E	2	26	292	571	.7	20	10	994	3.69	18	5	ND	4	38	2	2	5	55	.33	.063	11	24	.45	173	.14	2	2.80	.04	.08	1
S 25+00N 29+50E	1	45	313	630	.9	20	15	817	4.34	21	5	ND	7	30	2	2	4	57	.26	.141	14	24	.68	160	.15	2	3.36	.03	.11	1
S 25+00N 30+00E	1	33	297	424	1.2	12	7	872	3.78	12	5	ND	5	52	3	2	7	48	.44	.073	10	19	.38	248	.13	2	2.47	.04	.09	2
S 25+50N 25+00E	1	55	429	586	1.0	14	9	1566	3.43	11	5	ND	5	78	5	2	6	41	.72	.074	17	19	.44	237	.09	3	1.97	.03	.11	1
S 25+50N 25+50E	2	68	420	524	1.3	11	10	1781	5.11	10	5	ND	5	68	3	2	16	45	.43	.095	14	17	.35	205	.11	3	2.05	.03	.10	1
S 25+50N 26+00E	1	59	473	681	1.6	17	11	1017	4.35	13	5	ND	7	41	3	2	6	55	.26	.093	19	28	.61	176	.14	2	2.96	.03	.11	1
S 25+50N 26+50E	3	134	1113	855	2.2	18	18	2472	5.03	11	5	ND	5	57	7	2	6	51	.31	.150	24	23	.57	192	.09	3	2.62	.03	.15	1
S 25+50N 27+00E	1	28	801	1108	1.6	18	11	1857	3.59	17	5	ND	5	29	6	2	3	45	.27	.078	17	22	.41	161	.13	3	3.16	.04	.07	1
S 25+50N 27+50E	1	31	580	1517	1.6	20	11	2117	3.44	20	5	ND	4	27	8	2	6	40	.26	.089	14	21	.38	257	.12	2	2.95	.03	.09	1
S 25+50N 28+00E	2	65	588	1152	1.9	20	13	1229	4.40	18	5	ND	6	49	4	2	4	57	.40	.122	15	29	.76	241	.13	2	3.46	.04	.13	1
S 25+50N 28+50E	1	46	499	760	1.4	18	9	877	4.13	19	5	ND	7	21	2	2	5	51	.15	.120	14	27	.57	178	.13	2	3.14	.03	.10	1
S 25+50N 29+00E	2	69	561	611	1.1	18	9	755	4.99	20	5	ND	10	37	2	2	6	44	.30	.125	14	21	.51	118	.09	2	3.35	.03	.10	1
S 25+50N 29+50E	2	24	297	786	.7	16	13	706	4.08	16	5	ND	6	27	3	2	6	52	.20	.058	10	23	.45	132	.16	2	2.55	.03	.08	1
S 25+50N 30+00E	1	54	359	439	1.2	11	8	724	4.27	13	5	ND	7	29	2	2	10	49	.21	.079	14	20	.43	173	.11	2	2.28	.03	.09	1
S 26+00N 25+00E	2	60	414	423	1.4	12	9	1130	3.63	17	5	ND	5	49	3	2	5	47	.32	.151	19	21	.46	166	.08	3	2.55	.03	.11	1
S 26+00N 25+50E	2	43	749	791	1.3	14	13	2063	3.45	13	5	ND	7	38	8	2	6	41	.29	.085	16	20	.37	135	.11	3	2.76	.03	.09	1
S 26+00N 26+00E	1	24	261	431	.7	11	7	1617	2.72	12	5	ND	3	61	3	2	2	39	.46	.088	12	18	.35	187	.09	3	1.88	.03	.11	1
S 26+00N 26+50E	2	43	375	518	.8	20	9	1407	3.62	8	5	ND	5	45	3	2	2	47	.29	.130	17	31	.62	265	.12	2	3.09	.04	.11	1
S 26+00N 27+00E	1	66	1792	589	2.1	18	13	2358	3.78	21	5	ND	2	41	3	2	2	44	.31	.149	14	25	.46	181	.06	2	2.21	.03	.09	1
S 26+00N 27+50E	1	67	523	689	2.3	16	9	1615	3.96	36	5	ND	6	42	5	2	9	45	.25	.124	16	26	.45	333	.10	2	2.42	.03	.11	1
S 26+00N 28+00E	1	69	785	944	2.7	18	9	1236	4.29	33	5	ND	6	53	5	2	8	48	.38	.127	14	26	.50	267	.10	2	2.31	.03	.15	1
S 26+00N 28+50E	1	51	611	1015	1.4	15	10	1391	4.02	43	5	ND	6	49	5	2	3	45	.37	.147	16	23	.52	211	.12	2	2.26	.03	.12	1
S 26+00N 29+00E	1	78	655	685	.9	11	7	736	4.41	27	5	ND	5	60	4	2	14	48	.37	.119	12	21	.42	192	.08	2	1.83	.03	.13	1
S 26+00N 29+50E	1	50	517	651	1.0	11	7	575	4.14	16	5	ND	7	41	4	2	9	42	.23	.083	17	20	.41	188	.10	2	2.21	.03	.11	2
S 26+00N 30+00E	1	40	336	490	.6	10	16	699	4.01	8	5	ND	6	38	4	2	8	46	.21	.048	15	19	.40	117	.12	2	1.86	.03	.08	1
S 26+00N 30+50E	1	50	232	449	.7	11	9	714	3.91	10	5	ND	6	39	3	2	7	43	.39	.099	13	19	.42	134	.10	9	2.31	.03	.09	3
S 26+00N 31+00E	1	56	315	325	1.2	11	6	613	4.41	4	5	ND	6	49	3	2	12	43	.25	.179	13	23	.39	165	.09	2	1.95	.03	.08	1
S 26+50N 20+50E	1	32	299	317	1.0	12	8	1330	3.06	16	5	ND	6	81	2	2	2	43	.42	.072	21	19	.43	167	.08	2	2.61	.03	.14	2
S 26+50N 21+00E	1	31	206	268	.6	13	9	2057	2.93	9	5	ND	4	96	3	2	2	41	.43	.119	26	20	.46	222	.06	3	2.71	.03	.14	1
S 26+50N 21+50E	1	26	267	346	.9	12	7	2390	2.73	12	5	ND	5	112	6	2	2	38	.54	.132	19	17	.38	330	.06	3	2.37	.03	.12	2
STD C	18	58	39	133	7.3	66	27	1031	4.03	43	20	7	38	50	17	18	19	56	.47	.087	37	58	.89	178	.08	33	1.88	.08	.13	12

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM
S 26+50M 22+00E	1	68	330	754	1.2	17	10	1309	3.54	14	5	ND	10	112	10	2	6	42	.52	.119	21	25	.44	298	.10	7	3.27	.04	.12	2
S 26+50M 22+50E	1	108	226	577	2.5	16	11	1853	3.64	20	5	ND	8	94	6	2	7	43	.49	.139	23	21	.50	298	.10	2	2.78	.03	.12	1
S 26+50M 23+00E	1	34	159	400	1.0	13	8	2023	2.93	11	5	ND	9	96	13	2	2	41	.39	.085	28	24	.46	295	.09	2	2.45	.03	.13	1
S 26+50M 23+50E	1	26	136	314	1.2	11	8	1438	3.19	10	5	ND	6	60	4	2	2	46	.34	.093	17	18	.35	234	.10	2	2.39	.03	.10	1
S 26+50M 24+00E	1	61	305	470	5.8	16	11	1467	3.10	15	5	ND	6	79	7	2	4	39	.37	.126	19	21	.39	168	.10	2	2.08	.03	.11	2
S 26+50M 24+50E	1	44	223	555	1.2	14	12	3142	3.46	18	5	ND	6	56	5	2	3	55	.35	.122	12	21	.39	260	.12	2	2.06	.03	.12	1
S 26+50M 25+00E	2	61	321	466	1.7	14	10	879	3.20	24	5	ND	6	34	3	2	3	44	.24	.106	16	23	.45	103	.10	2	2.66	.03	.08	1
S 26+50M 25+50E	1	61	678	471	3.2	15	12	1632	3.43	13	5	ND	4	40	3	2	3	43	.29	.145	20	22	.44	150	.07	2	2.37	.03	.07	1
S 26+50M 26+00E	1	64	473	894	2.1	22	12	5427	3.29	16	5	ND	5	58	6	2	2	38	.35	.255	13	23	.39	300	.10	3	2.38	.03	.10	1
S 26+50M 26+50E	1	44	305	603	1.6	18	11	1522	3.67	17	7	ND	8	27	3	2	2	47	.17	.130	16	27	.44	213	.14	2	3.24	.06	.14	10
S 26+50M 27+00E	1	36	452	621	1.3	17	9	1993	3.84	18	5	ND	5	28	5	2	2	49	.22	.164	15	27	.45	179	.13	2	3.02	.03	.09	1
S 26+50M 27+50E	1	40	455	772	1.3	17	13	2035	4.20	26	5	ND	5	26	3	2	3	52	.21	.079	12	24	.41	158	.13	2	2.65	.03	.08	1
S 26+50M 28+00E	1	64	720	712	2.0	15	8	2026	4.04	48	5	ND	5	49	6	2	5	45	.32	.092	15	26	.43	191	.10	2	1.95	.03	.10	1
S 26+50M 28+50E	1	45	698	843	2.2	14	8	969	4.02	21	5	ND	7	43	4	2	4	46	.28	.134	13	28	.50	166	.11	2	2.41	.03	.13	1
S 26+50M 29+00E	1	30	482	566	1.0	9	5	599	3.66	22	5	ND	6	30	3	2	5	40	.21	.106	12	19	.30	119	.08	2	1.92	.03	.10	2
S 26+50M 29+50E	1	62	617	883	1.2	13	6	473	4.06	27	5	ND	9	37	4	2	5	43	.24	.112	14	21	.39	164	.09	2	2.74	.03	.11	1
S 26+50M 30+00E	1	32	360	533	.8	9	9	1211	3.71	19	5	ND	5	31	5	2	4	42	.22	.090	13	18	.33	100	.09	2	1.67	.03	.07	1
S 26+50M 30+50E	1	32	341	494	.8	9	7	631	3.67	21	5	ND	5	36	4	2	6	43	.25	.122	11	17	.31	97	.09	2	1.52	.03	.07	1
S 26+50M 31+00E	1	58	330	382	1.2	9	6	543	4.30	8	5	ND	5	37	4	2	12	39	.24	.063	10	21	.36	122	.08	2	1.51	.03	.06	1
S 26+50M 31+50E	1	63	234	351	1.6	11	9	573	4.79	9	5	ND	7	50	4	2	13	38	.26	.130	14	28	.43	135	.09	2	2.42	.03	.06	3
S 26+50M 32+00E	1	63	225	378	1.0	17	10	731	4.53	11	5	ND	9	37	3	2	13	48	.27	.152	12	31	.49	172	.14	2	2.32	.03	.08	1
S 26+50M 32+50E	1	74	274	348	1.2	16	14	1266	4.30	13	5	ND	6	73	3	2	9	46	.47	.146	17	33	.56	200	.10	2	1.91	.04	.10	1
S 26+50M 33+00E	1	85	126	235	.7	24	13	1410	4.35	10	5	ND	10	71	2	2	3	50	.42	.144	18	33	.80	254	.16	2	3.41	.04	.15	1
S 27+00M 15+00E	1	12	99	286	.6	11	6	2399	2.83	9	5	ND	4	72	3	2	2	42	.49	.132	16	19	.34	279	.07	2	2.41	.03	.10	2
S 27+00M 15+50E	1	23	123	464	1.2	13	6	2171	2.81	11	5	ND	6	98	7	2	2	38	.59	.251	23	19	.39	376	.07	2	2.96	.03	.15	3
S 27+00M 16+00E	1	55	160	536	.8	15	10	3356	3.64	11	5	ND	9	84	6	2	2	43	.47	.227	22	24	.41	506	.07	2	3.53	.03	.15	3
S 27+00M 16+50E	1	29	109	324	.6	12	6	2205	2.75	9	5	ND	5	49	4	2	2	37	.40	.167	17	17	.32	220	.07	2	2.40	.03	.09	1
S 27+00M 17+00E	2	26	129	410	1.0	12	7	3221	2.73	15	5	ND	3	82	5	2	2	36	.48	.142	14	18	.32	335	.07	2	2.26	.03	.07	3
S 27+00M 17+50E	1	22	139	399	.9	12	6	2613	2.43	11	5	ND	3	90	6	2	2	31	.49	.160	11	18	.33	294	.05	2	2.03	.03	.09	3
S 27+00M 18+00E	3	95	201	334	.9	9	12	4962	3.38	13	5	ND	5	95	6	2	2	35	.59	.172	16	15	.32	501	.03	2	2.02	.03	.11	14
S 27+00M 18+50E	1	32	134	560	.8	14	8	1676	2.93	13	5	ND	8	50	7	2	2	35	.29	.221	19	19	.35	267	.09	2	3.18	.03	.08	3
S 27+00M 19+00E	1	24	405	410	.4	12	6	1565	2.88	10	5	ND	5	59	2	2	2	42	.36	.086	14	21	.43	188	.05	2	2.20	.03	.11	5
S 27+00M 19+50E	1	14	278	400	.7	8	5	1748	2.47	13	5	ND	3	55	3	2	2	36	.33	.079	11	13	.29	190	.06	2	1.79	.03	.07	2
S 27+00M 20+00E	1	16	181	396	.6	10	6	3812	2.42	8	5	ND	4	110	6	2	3	32	.59	.173	18	16	.33	494	.06	2	2.32	.03	.13	2
S 27+00M 20+50E	1	36	149	404	.7	16	9	1576	3.14	18	5	ND	7	91	4	2	2	43	.51	.091	19	24	.47	201	.09	2	3.01	.03	.14	1
S 27+00M 21+00E	1	16	158	274	.5	9	6	1924	2.44	10	5	ND	6	82	3	2	2	33	.42	.118	17	14	.33	269	.06	2	2.42	.03	.09	1
S 27+00M 21+50E	1	28	345	350	.4	11	7	1628	2.91	8	5	ND	8	35	3	2	2	39	.22	.191	19	18	.35	163	.07	2	2.49	.02	.10	1
S 27+00M 22+00E	1	104	256	462	2.0	11	11	3160	3.55	19	5	ND	5	131	8	2	60	34	.58	.133	19	16	.32	353	.05	2	1.75	.03	.10	1
S 27+00M 22+50E	1	54	167	314	1.3	12	8	1684	3.00	15	5	ND	4	79	3	2	2	39	.34	.105	14	17	.37	255	.07	2	2.06	.03	.11	1
STD C	19	57	36	132	7.2	67	27	1029	4.07	42	22	7	38	49	18	16	19	56	.47	.086	36	58	.85	177	.08	32	1.88	.08	.14	12

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
S 27+00N 23+00E	1	32	95	300	1.0	11	8	1301	3.15	10	6	ND	4	23	2	2	2	41	.15	.092	8	16	.30	163	.10	2	1.70	.02	.07	2
S 27+00N 23+50E	1	38	117	533	1.0	22	10	1436	3.18	8	5	ND	6	63	4	2	2	40	.32	.207	15	35	.65	445	.15	2	2.22	.03	.18	1
S 27+00N 24+00E	1	32	239	460	1.4	17	9	2737	3.32	13	5	ND	4	51	8	2	2	45	.31	.127	13	37	.58	343	.09	2	1.70	.03	.18	1
S 27+00N 24+50E	4	275	1396	650	8.4	18	34	3245	7.62	13	5	ND	5	72	3	2	10	73	.38	.210	12	30	.75	170	.12	2	3.51	.04	.16	1
S 27+00N 25+00E	3	339	938	351	9.3	15	10	590	5.85	35	5	ND	6	27	1	2	16	56	.10	.162	19	25	.50	92	.11	2	3.08	.03	.10	1
S 27+00N 25+50E	1	130	647	469	3.2	16	13	1165	4.26	14	13	ND	9	26	2	2	4	49	.17	.240	20	24	.40	117	.12	2	3.19	.03	.11	1
S 27+00N 26+00E	1	77	803	397	2.7	13	8	1661	4.10	12	5	ND	5	34	2	2	5	46	.19	.173	14	22	.36	184	.09	2	2.21	.02	.08	1
S 27+00N 26+50E	1	28	282	628	1.8	15	12	1714	3.36	13	5	ND	5	39	3	2	2	40	.24	.251	13	25	.44	259	.09	2	2.07	.03	.08	1
S 27+00N 27+00E	1	35	878	1079	1.0	16	10	1262	3.61	19	5	ND	8	53	6	2	2	40	.40	.289	13	26	.47	262	.09	2	2.22	.03	.09	1
S 27+00N 27+50E	1	48	493	937	2.2	16	10	1258	3.97	21	5	ND	5	42	3	2	6	44	.26	.123	14	27	.51	159	.09	2	2.40	.03	.10	1
S 27+00N 28+00E	1	50	502	1051	1.2	16	11	954	3.94	18	5	ND	6	51	6	2	4	43	.26	.072	18	27	.50	162	.10	2	2.30	.03	.08	1
S 27+00N 28+50E	1	41	530	814	1.3	11	9	847	3.63	14	5	ND	5	35	5	2	4	41	.20	.092	13	20	.35	123	.09	2	2.05	.03	.07	2
S 27+00N 29+00E	1	66	515	1020	1.3	13	11	1656	4.13	19	5	ND	6	36	10	2	6	42	.20	.082	20	23	.41	154	.10	2	2.17	.03	.08	1
S 27+00N 29+50E	1	42	453	772	1.4	12	7	658	4.13	20	5	ND	7	32	6	2	7	44	.17	.145	13	18	.32	167	.11	2	2.34	.03	.09	1
S 27+00N 30+00E	1	44	428	690	1.7	10	8	637	3.98	13	5	ND	6	43	4	2	6	42	.27	.098	12	18	.36	133	.10	2	2.41	.03	.08	1
S 27+00N 30+50E	1	36	293	471	.9	9	7	1934	3.43	14	5	ND	4	38	3	2	2	44	.26	.098	12	15	.28	118	.08	2	1.76	.03	.08	1
S 27+00N 31+00E	1	57	315	606	.9	12	8	1224	4.67	6	5	ND	7	53	5	2	14	49	.31	.159	13	23	.42	197	.10	2	1.81	.03	.10	1
S 27+00N 31+50E	1	65	268	631	1.0	13	11	2332	3.10	12	5	ND	4	69	16	2	3	30	.41	.058	18	24	.21	190	.05	2	1.07	.02	.04	1
S 27+00N 32+00E	1	50	304	897	1.0	14	11	640	4.23	6	5	ND	6	37	6	2	8	43	.26	.079	14	25	.45	142	.10	2	2.00	.03	.07	1
S 27+00N 32+50E	1	66	306	760	.8	15	11	1299	4.09	8	5	ND	6	49	9	2	6	46	.35	.099	20	25	.44	157	.10	2	1.90	.03	.08	1
I 27+00N 33+00E	1	119	10	53	.2	2	2	167	2.67	3	5	ND	8	67	1	2	2	38	.17	.052	11	90	.39	48	.08	2	.78	.06	.09	1
S 27+50N 15+00E	1	8	67	169	.5	10	5	1637	2.65	2	5	ND	5	55	1	2	2	41	.39	.094	16	18	.33	221	.05	2	1.93	.03	.09	1
S 27+50N 15+50E	1	14	94	307	.6	12	6	2261	3.09	6	5	ND	6	57	5	2	2	45	.35	.167	15	18	.34	315	.06	2	2.38	.02	.10	2
S 27+50N 16+00E	1	18	228	427	.8	10	6	2258	2.80	4	5	ND	7	67	4	2	2	37	.38	.150	19	15	.33	272	.05	2	2.24	.03	.12	5
S 27+50N 16+50E	1	18	112	242	.7	12	6	1694	2.96	6	5	ND	5	55	3	2	2	44	.39	.105	16	17	.34	192	.07	2	2.11	.03	.10	8
S 27+50N 17+00E	1	42	125	452	.6	12	10	3567	3.09	8	5	ND	3	61	5	2	2	36	.41	.188	15	18	.35	318	.05	2	2.13	.03	.12	2
S 27+50N 17+50E	1	32	112	388	.9	12	8	2830	2.92	2	5	ND	3	67	6	2	2	39	.49	.102	15	16	.29	312	.08	3	2.66	.03	.08	1
S 27+50N 18+00E	1	52	138	308	1.5	11	6	1399	2.96	13	5	ND	4	65	3	2	2	42	.54	.078	23	21	.36	194	.05	2	2.18	.03	.10	18
S 27+50N 18+50E	1	59	336	716	2.0	10	8	1056	3.06	33	5	ND	4	70	7	2	3	36	.43	.062	22	20	.32	210	.05	2	1.95	.03	.06	9
S 27+50N 19+00E	1	17	119	248	.5	12	6	1589	2.80	2	5	ND	6	41	2	2	2	38	.29	.124	17	17	.34	163	.10	2	3.30	.03	.09	1
S 27+50N 19+50E	1	22	425	294	.5	8	6	2379	2.65	14	5	ND	4	76	2	2	2	36	.40	.088	15	12	.35	290	.05	2	2.21	.02	.14	4
S 27+50N 20+00E	1	17	180	241	.7	10	6	2024	2.62	9	5	ND	4	81	2	2	2	35	.49	.143	20	17	.43	273	.04	2	2.18	.03	.18	1
S 27+50N 20+50E	1	24	201	308	.6	11	7	1527	2.93	14	5	ND	4	110	3	2	2	42	.59	.103	18	18	.40	191	.05	2	2.45	.03	.14	1
S 27+50N 21+00E	1	24	178	413	1.7	12	8	1360	2.97	17	5	ND	9	80	3	2	2	42	.40	.069	28	20	.42	162	.08	2	2.91	.03	.12	1
S 27+50N 21+50E	1	18	190	290	.7	10	6	917	2.80	7	5	ND	10	54	1	2	2	40	.31	.110	24	17	.38	157	.07	2	2.56	.03	.11	1
S 27+50N 22+00E	1	33	299	366	1.1	13	8	2918	3.00	13	5	ND	6	82	4	2	2	41	.38	.097	20	19	.37	282	.08	2	2.29	.03	.12	1
S 27+50N 22+50E	1	44	178	430	1.2	17	10	1805	3.53	12	5	ND	6	64	3	2	2	48	.35	.097	19	22	.50	266	.11	2	2.64	.03	.10	1
S 27+50N 23+00E	1	81	149	478	1.2	15	9	1830	3.53	14	5	ND	4	72	4	2	3	50	.36	.130	17	18	.40	221	.09	2	2.13	.03	.10	1
S 27+50N 23+50E	1	54	148	203	1.7	12	12	2155	3.67	13	5	ND	2	27	3	2	4	42	.13	.239	13	18	.37	116	.05	2	2.50	.02	.09	1
STD C	18	58	37	131	7.4	68	27	1040	4.07	40	22	7	38	50	18	17	18	56	.48	.087	37	58	.85	179	.08	33	1.90	.08	.13	11

SAMPLE#	MO PPH	CU PPH	PB PPH	ZN PPH	AG PPH	NI PPH	CO PPH	MN PPH	FE %	AS PPH	U PPH	AU PPH	TH PPH	SR PPH	CD PPH	SB PPH	BI PPH	V PPH	CA %	P %	LA PPH	CR PPH	MG %	BA PPH	TI %	B PPH	AL %	NA %	K %	M PPH
S 27+50N 24+00E	3	33	173	284	.8	16	10	2890	3.12	17	5	ND	4	62	3	2	2	40	.40	.145	10	23	.47	271	.08	2	2.06	.03	.10	1
S 27+50N 24+50E	2	55	237	395	3.0	14	11	919	4.08	5	5	ND	6	23	2	2	5	48	.11	.114	14	27	.45	120	.12	2	2.73	.02	.07	1
S 27+50N 25+00E	3	194	1065	295	7.2	15	9	1168	7.18	7	5	ND	6	25	2	2	25	54	.13	.177	13	33	.48	119	.10	2	2.23	.02	.10	1
S 27+50N 25+50E	3	225	2009	388	8.9	12	13	1270	5.07	22	5	ND	4	18	2	2	13	48	.14	.204	19	20	.36	103	.07	2	2.64	.02	.07	1
S 27+50N 26+00E	1	82	541	658	2.6	14	16	1738	3.43	8	5	ND	7	32	3	2	2	45	.26	.161	18	20	.42	187	.10	2	3.38	.03	.08	1
S 27+50N 26+50E	1	27	211	959	2.5	16	9	1298	3.15	6	5	ND	8	42	5	2	2	46	.33	.125	20	26	.52	187	.10	2	2.51	.03	.10	1
S 27+50N 27+00E	1	41	248	1168	1.9	18	9	1243	3.50	11	5	ND	7	43	6	2	2	47	.31	.156	21	31	.61	217	.09	2	2.82	.03	.09	1
S 27+50N 27+50E	1	42	308	844	2.1	16	8	1148	3.78	22	5	ND	4	60	4	2	4	47	.34	.115	14	31	.58	201	.08	2	2.24	.03	.11	1
S 27+50N 28+00E	1	81	515	748	2.3	16	7	577	4.10	31	5	ND	7	37	4	2	7	46	.18	.104	16	29	.53	174	.08	2	2.55	.03	.10	1
S 27+50N 28+50E	1	39	477	714	1.3	13	7	819	3.80	19	5	ND	6	30	4	2	5	47	.19	.098	13	20	.39	155	.10	2	2.39	.03	.09	1
S 27+50N 29+00E	1	36	468	553	1.6	10	8	764	4.24	26	5	ND	5	29	3	2	7	49	.18	.123	12	19	.38	142	.10	2	2.16	.02	.06	1
S 27+50N 29+50E	1	56	535	561	2.1	10	10	506	4.17	21	5	ND	6	28	3	2	7	50	.17	.153	13	18	.33	128	.08	2	2.29	.02	.07	1
S 27+50N 30+00E	1	43	378	662	1.8	10	9	657	3.87	10	5	ND	7	27	4	2	5	50	.21	.092	15	17	.38	148	.08	2	2.35	.03	.07	1
S 28+00N 15+00E	1	16	82	309	.9	12	6	2067	2.94	6	5	ND	6	45	4	2	2	42	.35	.224	16	18	.35	247	.06	2	2.48	.03	.09	1
S 28+00N 15+50E	1	12	83	309	.5	11	6	2379	2.83	6	5	ND	4	61	3	2	2	43	.39	.162	15	15	.30	267	.06	2	2.39	.03	.08	1
S 28+00N 16+00E	1	29	130	325	.7	11	7	2346	3.27	7	5	ND	3	40	3	2	2	48	.27	.138	19	17	.36	203	.04	2	2.36	.02	.08	1
S 28+00N 16+50E	1	18	115	521	1.0	14	8	2652	3.03	7	5	ND	6	55	7	2	2	40	.37	.129	17	19	.37	284	.09	2	3.01	.03	.08	1
S 28+00N 17+00E	1	41	214	342	1.1	12	7	1545	2.94	8	5	ND	5	50	3	2	2	44	.29	.114	19	19	.45	195	.05	2	2.54	.02	.11	3
S 28+00N 17+50E	1	44	131	309	.8	13	8	2030	3.00	5	5	ND	4	73	4	2	2	39	.55	.122	17	21	.41	301	.06	3	2.86	.03	.09	1
S 28+00N 18+00E	1	27	56	149	.7	9	6	1066	2.53	8	5	ND	4	56	1	2	2	35	.25	.080	11	15	.30	189	.03	2	1.97	.02	.11	1
S 28+00N 18+50E	1	14	90	266	.3	12	6	1613	2.71	5	5	ND	3	56	3	2	2	36	.42	.231	12	18	.42	335	.06	2	2.71	.03	.10	1
S 28+00N 19+00E	1	14	117	201	.7	10	6	1314	2.89	3	5	ND	5	64	1	2	2	41	.34	.092	13	14	.36	202	.08	2	3.01	.03	.08	1
S 28+00N 19+50E	1	14	126	267	.6	11	6	2215	2.94	3	5	ND	5	37	3	2	2	44	.27	.098	17	15	.34	247	.06	2	2.48	.03	.10	1
S 28+00N 20+00E	1	17	147	350	.9	12	7	1944	2.98	6	5	ND	6	98	5	2	2	43	.51	.171	20	16	.39	286	.07	2	2.99	.03	.13	1
S 28+00N 20+50E	1	38	317	537	.9	10	7	2802	2.68	13	5	ND	6	114	8	2	2	38	.69	.245	19	18	.43	480	.05	3	1.60	.03	.17	1
S 28+00N 21+00E	7	21	230	340	.6	10	6	1625	2.52	9	5	ND	3	67	7	2	2	35	.37	.148	18	15	.33	135	.04	2	2.09	.02	.08	1
S 28+00N 21+50E	1	19	136	314	.5	11	7	2101	2.84	8	5	ND	5	70	4	2	2	39	.36	.207	15	15	.44	359	.07	2	2.38	.03	.10	1
S 28+00N 22+00E	1	20	201	216	1.3	9	6	1981	2.27	13	5	ND	4	107	5	2	2	35	.50	.085	12	14	.28	207	.06	2	1.42	.02	.07	1
S 28+00N 22+50E	1	26	133	260	.4	10	7	1498	3.12	7	5	ND	3	58	2	2	2	45	.35	.082	11	17	.37	244	.07	2	1.21	.02	.07	1
S 28+00N 23+00E	2	36	125	373	1.0	15	9	2594	2.99	8	5	ND	3	68	4	2	2	39	.36	.091	12	16	.35	298	.09	2	1.86	.03	.09	1
S 28+00N 23+50E	1	30	160	149	1.0	10	4	1188	4.17	7	5	ND	4	25	1	2	8	50	.12	.098	10	17	.22	148	.08	2	1.41	.02	.05	1
S 28+00N 24+00E	1	29	210	351	1.3	16	9	2365	3.21	12	5	ND	6	46	3	2	2	44	.28	.182	17	20	.55	299	.11	2	2.78	.03	.13	1
S 28+00N 24+50E	1	22	77	378	1.2	26	10	3002	3.37	5	5	ND	10	99	4	2	2	43	.57	.404	33	32	.60	786	.08	2	3.80	.04	.13	1
S 28+00N 25+00E	3	203	1100	302	7.9	15	9	1167	7.21	11	5	ND	6	30	1	2	27	53	.15	.175	14	35	.50	133	.11	2	2.45	.03	.11	1
S 28+00N 25+50E	2	206	465	383	6.5	17	13	1305	5.19	24	5	ND	6	32	3	2	19	48	.20	.117	15	24	.44	172	.10	2	2.46	.03	.07	1
S 28+00N 26+00E	1	46	635	506	1.9	15	11	1925	3.75	10	5	ND	4	61	2	2	4	45	.42	.149	14	24	.49	268	.09	2	2.24	.03	.08	1
S 28+00N 26+50E	1	47	537	1062	1.9	19	11	1181	4.01	25	5	ND	10	49	4	2	2	48	.27	.167	23	33	.75	290	.10	2	3.12	.03	.11	1
S 28+00N 27+00E	1	30	270	1174	2.2	18	10	1472	3.25	19	5	ND	7	40	6	2	2	42	.28	.198	17	30	.57	208	.09	2	2.56	.03	.09	1
S 28+00N 27+50E	1	64	394	1099	2.3	19	10	1366	3.80	31	5	ND	7	62	11	2	5	46	.40	.186	19	31	.57	250	.09	2	2.91	.03	.11	1
STD C	18	59	39	131	7.6	67	27	1022	4.00	37	19	7	37	47	18	18	18	58	.47	.084	36	56	.88	179	.07	31	1.85	.08	.13	13

SAMPLE#	MD	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	M
	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	PPH	%	%	PPH	PPH	%	PPH	%	PPH	%	%	%	PPH
S 28+00N 28+00E	2	129	635	1064	3.1	18	9	1498	4.28	29	5	ND	6	67	10	2	9	41	.27	.093	21	32	.56	198	.10	2	2.76	.03	.12	2
S 28+00N 28+50E	1	43	519	739	1.4	11	7	580	3.75	17	5	ND	6	30	4	2	6	44	.19	.144	12	20	.32	114	.10	2	2.25	.03	.09	1
S 28+00N 29+00E	1	86	840	723	1.8	10	7	516	4.42	46	5	ND	10	46	3	2	10	41	.21	.149	14	17	.36	150	.08	2	2.20	.03	.11	1
S 28+00N 29+50E	1	74	507	821	1.3	11	9	594	4.23	25	5	ND	8	43	6	2	7	47	.25	.098	16	20	.37	118	.11	2	2.39	.03	.09	2
S 28+00N 30+00E	1	47	409	458	2.0	8	6	604	4.20	16	5	ND	6	25	2	2	6	50	.19	.139	13	18	.37	118	.09	2	1.81	.03	.07	3
S 28+50N 15+00E	1	15	69	309	.8	10	6	1732	3.09	5	5	ND	7	37	3	2	2	45	.28	.182	18	17	.31	167	.08	2	2.67	.03	.09	2
S 28+50N 15+50E	1	14	112	214	.5	11	6	2214	3.46	5	5	ND	5	53	2	2	2	54	.34	.091	21	18	.32	191	.06	2	2.09	.03	.09	3
S 28+50N 16+00E	1	21	184	283	.7	12	6	2385	2.91	10	5	ND	5	55	3	2	2	40	.36	.112	18	18	.39	283	.04	2	2.28	.02	.14	6
S 28+50N 16+50E	1	26	183	273	1.2	12	7	3173	2.92	13	5	ND	4	51	4	2	2	42	.30	.128	17	17	.34	279	.06	2	2.19	.02	.09	5
S 28+50N 17+00E	1	35	157	481	1.1	12	7	1832	3.02	9	5	ND	5	75	7	2	2	43	.59	.063	17	19	.36	347	.07	2	2.41	.03	.08	3
S 28+50N 17+50E	1	58	156	386	1.0	16	8	1502	3.33	9	5	ND	6	77	4	2	2	48	.57	.106	21	27	.49	264	.07	2	2.80	.03	.13	3
S 28+50N 18+00E	2	94	119	318	2.7	19	10	2252	3.30	13	5	ND	6	49	3	2	2	45	.27	.061	18	28	.50	272	.06	2	3.00	.03	.12	2
S 28+50N 18+50E	1	13	89	221	.2	10	6	1850	2.89	2	5	ND	5	63	1	2	2	42	.35	.087	15	16	.40	208	.06	2	2.64	.03	.13	1
S 28+50N 19+00E	1	26	104	381	.4	11	7	1965	2.98	7	5	ND	5	63	5	2	2	42	.40	.196	14	16	.34	343	.09	2	2.90	.03	.11	1
S 28+50N 19+50E	1	18	147	280	1.0	11	6	1780	2.90	5	5	ND	7	38	3	2	2	42	.28	.114	20	16	.38	199	.07	2	3.06	.03	.12	1
S 28+50N 20+00E	1	18	182	370	1.1	11	6	2390	2.76	7	5	ND	6	59	4	2	2	39	.38	.120	20	16	.37	228	.08	2	2.74	.03	.13	1
S 28+50N 20+50E	1	20	199	492	.4	10	6	2324	2.50	11	5	ND	5	82	6	2	2	32	.47	.271	14	16	.35	295	.06	2	2.18	.03	.11	2
S 28+50N 21+00E	1	17	184	298	.7	10	6	1433	2.57	11	5	ND	4	80	4	2	2	37	.41	.086	25	19	.37	128	.05	2	2.47	.03	.07	3
S 28+50N 21+50E	1	19	140	243	.8	9	6	1534	2.73	8	5	ND	6	70	3	2	2	39	.36	.070	15	14	.30	219	.07	2	2.49	.03	.07	1
S 28+50N 22+00E	1	15	86	142	.6	7	5	1414	2.86	6	5	ND	3	45	2	2	2	44	.24	.098	11	13	.22	140	.08	2	1.86	.02	.06	1
S 28+50N 22+50E	1	24	175	573	3.6	14	8	2228	3.12	6	5	ND	5	71	3	2	2	40	.30	.080	12	19	.42	204	.10	2	2.40	.03	.09	1
S 28+50N 23+00E	1	40	110	295	.7	14	7	1735	3.07	3	5	ND	5	26	2	2	3	41	.18	.165	13	18	.40	199	.10	2	2.66	.03	.09	1
S 28+50N 23+50E	1	30	121	323	1.0	19	7	1260	3.07	9	5	ND	8	37	1	2	2	43	.24	.108	13	27	.44	194	.13	2	3.28	.03	.10	1
S 28+50N 24+00E	1	22	97	339	1.3	24	10	2599	3.63	7	5	ND	8	47	2	2	2	46	.30	.281	19	36	.74	398	.17	2	3.35	.04	.17	1
S 28+50N 24+50E	1	22	109	309	1.5	16	8	1819	3.39	8	5	ND	9	65	2	2	2	44	.32	.133	27	22	.52	273	.10	2	3.26	.03	.09	1
S 28+50N 25+00E	1	21	196	468	1.5	13	9	3304	3.33	12	5	ND	7	65	4	2	2	46	.42	.135	18	18	.47	388	.10	2	2.68	.04	.14	1
S 28+50N 25+50E	1	33	238	581	2.1	15	11	2215	3.28	3	5	ND	7	40	3	2	3	43	.27	.130	21	22	.48	220	.09	2	2.64	.03	.10	1
S 28+50N 26+00E	1	55	290	526	2.4	18	9	1231	3.44	11	5	ND	12	75	3	2	8	47	.54	.158	32	30	.77	289	.10	2	2.73	.04	.19	1
S 28+50N 26+50E	1	38	248	883	2.5	19	9	1352	3.46	5	5	ND	9	58	5	2	2	47	.42	.138	22	32	.68	247	.11	2	2.91	.04	.10	1
S 28+50N 27+00E	1	39	243	1295	1.8	18	9	912	3.78	26	5	ND	9	37	9	2	2	49	.31	.235	19	29	.58	223	.10	2	2.77	.03	.12	3
S 28+50N 27+50E	1	57	559	921	2.2	13	8	1030	4.07	31	5	ND	6	44	9	2	8	41	.27	.231	15	25	.46	225	.08	2	2.35	.03	.11	2
S 28+50N 28+00E	1	72	731	716	2.0	12	9	817	4.40	34	5	ND	8	36	4	2	7	48	.19	.131	17	23	.42	145	.11	2	2.70	.03	.12	1
S 28+50N 28+50E	2	68	546	1007	2.2	13	9	802	4.10	23	5	ND	7	62	9	2	5	49	.33	.060	21	23	.43	147	.11	2	2.07	.03	.12	2
S 28+50N 29+00E	1	150	620	1683	4.3	20	10	1332	4.09	29	6	ND	10	93	17	2	7	44	.48	.074	34	27	.51	180	.10	2	3.08	.04	.14	1
S 28+50N 29+50E	1	55	470	1052	1.8	14	8	733	3.99	32	5	ND	8	42	7	2	4	48	.26	.098	17	20	.39	180	.12	2	2.89	.03	.12	1
S 28+50N 30+00E	1	35	349	643	1.4	11	8	627	3.75	12	6	ND	8	38	3	2	4	44	.25	.060	16	17	.36	141	.12	2	2.99	.03	.08	3
STD C	18	59	39	133	7.2	67	27	1027	4.04	41	22	7	38	49	17	17	18	56	.47	.085	37	58	.88	176	.08	32	1.87	.08	.13	12

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO₃-H₂O AT 95 DEC. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOLUTION

DATE RECEIVED: OCT 30 1987

DATE REPORT MAILED: *Nov 3/87*ASSAYER: *D. J. J.* DEAN TOYE, CERTIFIED B.C. ASSAYER

ROSSBACHER LABORATORY PROJECT-CERT # 87741

File # 87-5296

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SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	W
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM
S L20+00N 15+00E	1	30	12	83	.6	17	10	246	3.08	6	5	ND	7	22	1	2	2	56	.16	.101	11	29	.50	114	.17	2	3.56	.04	.08	1
S L20+00N 15+50E	1	32	27	121	.6	14	9	587	3.41	36	5	ND	5	21	1	2	2	59	.19	.125	9	25	.43	120	.11	4	1.98	.01	.08	1
S L20+00N 16+00E	2	80	18	129	.4	25	11	398	3.81	32	5	ND	7	32	1	2	2	94	.21	.073	14	50	.64	252	.14	3	1.92	.01	.16	3
S L20+00N 16+50E	1	38	40	212	.5	18	14	1272	4.28	20	5	ND	5	34	1	2	2	74	.28	.254	8	32	.61	259	.19	2	2.43	.01	.10	1
S L20+00N 17+00E	1	85	20	129	.4	19	12	598	3.87	6	5	ND	6	28	1	2	2	79	.27	.093	10	32	.68	132	.17	4	2.85	.01	.13	1
S L20+00N 17+50E	1	75	25	127	.5	16	12	1467	4.68	7	5	ND	6	22	1	2	2	92	.19	.116	9	30	.47	119	.13	6	1.91	.01	.10	1
S L20+00N 18+00E	1	38	15	72	.1	17	9	765	3.16	6	5	ND	3	20	1	2	2	65	.22	.139	10	37	.43	106	.10	2	1.73	.01	.06	1
S L20+00N 18+50E	1	27	50	125	.3	15	10	2324	3.19	11	5	ND	5	20	1	2	2	53	.16	.202	10	28	.41	173	.11	4	2.08	.01	.06	1
S L20+00N 19+00E	1	18	50	132	.6	14	8	865	2.90	8	5	ND	5	29	1	2	2	53	.25	.127	9	25	.33	141	.11	4	2.44	.01	.06	1
S L20+00N 19+50E	1	35	210	238	1.1	10	6	720	2.93	12	5	ND	10	21	1	2	2	48	.20	.100	17	18	.41	112	.06	4	2.02	.01	.07	3
S L20+00N 20+00E	2	18	118	212	1.0	8	6	1504	2.71	11	5	ND	5	36	1	2	2	39	.22	.091	6	13	.21	143	.09	2	2.31	.01	.04	2
S L20+50N 15+00E	1	20	16	113	.3	21	13	1197	3.11	8	5	ND	3	21	1	2	2	53	.16	.126	9	33	.50	163	.13	3	2.37	.01	.08	1
S L20+50N 15+50E	1	20	37	108	.3	14	9	854	3.13	11	5	ND	5	39	1	2	2	56	.29	.128	10	23	.37	190	.12	3	2.46	.01	.08	1
S L20+50N 16+00E	1	29	20	107	1.1	19	10	574	3.20	21	5	ND	6	36	1	2	2	53	.28	.165	12	26	.44	155	.18	2	3.50	.02	.08	1
S L20+50N 16+50E	1	34	26	145	.6	15	9	722	3.28	14	5	ND	6	37	2	2	2	55	.29	.212	10	22	.44	160	.12	2	2.76	.01	.08	1
S L20+50N 17+00E	2	110	27	170	.6	16	15	2239	4.17	8	5	ND	5	54	1	2	2	81	.39	.161	8	28	.76	315	.18	4	2.27	.01	.21	1
S L20+50N 17+50E	1	77	36	111	.4	15	15	1380	3.86	8	5	ND	3	52	1	2	2	72	.37	.123	11	30	.57	185	.10	2	1.86	.01	.10	1
S L20+50N 18+00E	1	40	45	299	.3	18	15	2226	3.34	10	5	ND	5	82	5	2	2	57	.46	.170	14	27	.54	404	.13	4	2.23	.01	.12	1
S L20+50N 18+50E	1	153	31	81	.8	16	10	316	3.24	7	5	ND	10	18	1	2	2	62	.15	.100	21	34	.52	64	.12	2	2.70	.01	.09	1
S L20+50N 19+00E	1	34	61	132	.5	21	9	1141	3.14	8	5	ND	4	29	1	3	2	54	.19	.090	10	21	.32	177	.12	2	2.31	.01	.06	1
S L20+50N 19+50E	1	21	146	196	1.1	9	7	1571	2.78	9	5	ND	5	27	2	2	2	42	.18	.131	10	14	.23	180	.11	3	2.94	.01	.05	2
S L20+50N 20+00E	1	62	133	300	.9	10	8	1820	2.90	13	5	ND	4	97	4	2	2	36	.53	.145	11	15	.28	196	.10	2	2.82	.01	.09	1
S L21+00N 15+00E	1	13	31	87	.1	16	9	533	3.54	5	5	ND	5	19	1	2	2	57	.13	.187	6	25	.39	149	.15	2	3.08	.01	.05	1
S L21+00N 15+50E	2	14	47	89	.5	13	7	722	3.49	24	5	ND	4	31	1	2	2	57	.22	.085	7	24	.35	100	.13	3	1.75	.01	.06	1
S L21+00N 16+00E	1	22	36	130	.6	13	8	1212	3.06	17	5	ND	5	44	1	2	2	49	.34	.171	10	18	.29	178	.13	2	3.11	.02	.07	1
S L21+00N 16+50E	3	40	37	144	.7	13	13	1766	3.88	35	5	ND	5	66	2	2	2	68	.38	.201	9	25	.41	245	.12	3	1.78	.01	.10	1
S L21+00N 17+00E	3	76	25	137	.4	16	12	1465	3.72	4	6	ND	4	37	1	3	2	69	.29	.073	11	26	.52	231	.14	3	2.55	.01	.10	1
S L21+00N 17+50E	1	32	24	111	.4	15	11	1259	3.46	6	5	ND	5	25	1	2	2	60	.18	.081	11	22	.38	173	.16	2	3.21	.01	.08	1
S L21+00N 18+00E	2	59	51	130	.5	17	16	1058	3.69	13	5	ND	7	48	1	2	2	69	.31	.128	26	29	.59	197	.13	2	2.46	.01	.11	1
S L21+00N 18+50E	1	47	25	92	.1	20	12	506	3.81	9	5	ND	4	36	1	2	2	73	.20	.087	9	35	.57	156	.16	2	2.04	.01	.10	1
S L21+00N 19+00E	1	82	33	104	.3	19	12	501	3.42	9	5	ND	6	28	1	2	2	62	.18	.144	8	29	.51	163	.10	2	2.26	.01	.07	1
S L21+00N 19+50E	1	31	124	200	.8	11	8	1922	2.89	9	5	ND	5	33	2	3	2	46	.26	.139	13	17	.30	186	.11	3	2.99	.01	.06	1
S L21+00N 20+00E	1	90	175	288	.7	11	9	1774	3.00	13	5	ND	6	60	4	3	2	41	.33	.111	15	18	.30	209	.09	2	2.47	.01	.07	1
S L21+50N 15+00E	1	17	42	132	.3	13	7	2676	3.31	5	6	ND	6	64	1	3	2	54	.43	.181	12	22	.32	293	.12	4	2.11	.01	.07	1
S L21+50N 15+50E	1	22	32	174	.5	16	8	1731	3.60	20	5	ND	6	38	2	2	2	60	.29	.249	11	24	.34	297	.13	3	2.60	.01	.09	1
S L21+50N 16+00E	2	71	41	198	.7	17	11	1082	3.61	63	5	ND	5	39	1	2	2	60	.25	.202	11	25	.45	171	.13	2	2.88	.01	.10	1
S L21+50N 16+50E	2	44	31	113	.4	15	8	777	3.27	19	5	ND	7	26	1	2	2	58	.18	.103	17	25	.47	119	.11	2	3.09	.01	.10	1
S L21+50N 17+00E	1	34	41	76	.2	14	9	1746	3.20	11	5	ND	3	44	2	2	2	60	.30	.062	13	22	.38	213	.09	2	1.67	.01	.07	1
S L21+50N 17+50E	2	94	40	146	.4	16	13	1706	3.52	12	5	ND	4	46	1	2	2	62	.27	.076	15	24	.51	190	.15	2	2.57	.01	.12	1
STD C	20	58	37	132	7.3	69	28	1057	3.98	41	24	7	40	51	19	16	18	59	.46	.089	38	58	.91	181	.08	34	1.79	.06	.13	12

SAMPLE#	MO	CU	PB	ZN	AG	NI	CO	MN	FE	AS	U	AU	TH	SR	CD	SB	BI	V	CA	P	LA	CR	MG	BA	TI	B	AL	NA	K	M
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	I	I	PPM	PPM	I	PPM	I	PPM	I	I	I	PPM
\$ L21+50N 18+00E	1	23	59	118	.1	16	10	2089	3.31	4	5	ND	5	69	1	2	2	57	.41	.075	14	24	.37	270	.16	4	2.96	.02	.09	1
\$ L21+50N 18+50E	1	39	52	112	.2	17	9	808	3.53	9	5	ND	8	40	1	2	2	63	.29	.111	15	29	.50	148	.14	4	3.00	.01	.10	1
\$ L21+50N 19+00E	1	73	34	144	.7	13	11	615	4.51	12	5	ND	5	48	1	2	2	79	.33	.097	11	31	.41	176	.13	2	1.80	.01	.08	2
\$ L21+50N 19+50E	1	307	82	235	.5	22	13	1156	3.97	11	5	ND	11	74	1	2	2	69	.55	.154	20	37	.59	213	.12	4	2.88	.01	.14	1
\$ L21+50N 20+00E	1	297	200	578	1.5	20	10	2056	3.30	14	7	ND	9	88	8	2	2	42	.60	.298	28	23	.34	299	.10	8	3.84	.02	.13	2
\$ L22+00N 15+00E	1	19	50	200	.1	16	9	2217	3.54	9	5	ND	7	52	1	2	2	56	.31	.154	13	22	.34	269	.13	5	2.55	.02	.09	1
\$ L22+00N 15+50E	1	38	27	142	.4	16	10	1139	3.70	43	5	ND	8	45	1	2	2	64	.36	.107	16	23	.49	290	.15	5	3.22	.01	.15	1
\$ L22+00N 16+00E	1	24	33	171	.3	15	9	1244	3.22	25	5	ND	7	40	1	2	2	48	.34	.280	13	21	.38	237	.13	4	3.64	.03	.11	1
\$ L22+00N 16+50E	1	51	35	191	.3	17	10	1099	3.44	21	5	ND	7	37	1	2	2	55	.26	.120	17	24	.43	178	.14	2	3.13	.02	.13	1
\$ L22+00N 17+00E	2	86	32	102	.4	19	13	481	3.75	13	5	ND	11	28	1	2	2	70	.22	.114	24	32	.71	133	.15	3	3.03	.03	.22	1
\$ L22+00N 17+50E	3	149	42	148	.4	15	13	981	3.53	17	5	ND	9	49	1	2	2	60	.34	.092	28	25	.49	165	.16	3	3.79	.02	.13	1
\$ L22+00N 18+00E	2	36	47	92	.4	15	11	1520	3.48	14	5	ND	5	51	1	2	2	61	.35	.068	14	25	.41	173	.14	4	2.99	.01	.10	1
\$ L22+00N 18+50E	1	23	70	204	.3	13	12	2960	3.00	12	5	ND	3	67	1	2	2	48	.46	.087	14	21	.28	305	.12	4	2.09	.02	.10	1
\$ L22+00N 19+00E	1	88	102	181	.1	14	8	898	3.70	11	5	ND	7	42	1	2	2	68	.31	.063	18	26	.39	155	.10	2	1.90	.01	.08	1
\$ L22+00N 19+50E	1	143	89	268	.6	19	33	2224	4.69	17	5	ND	6	40	2	2	2	74	.28	.138	13	29	.36	261	.14	4	1.88	.01	.10	2
\$ L22+00N 20+00E	1	539	285	468	1.9	21	12	2543	3.66	13	8	ND	8	62	4	2	2	48	.29	.181	30	28	.41	226	.09	5	2.64	.01	.12	1
\$ L22+50N 15+00E	1	29	156	252	.2	14	11	3428	2.73	9	5	ND	5	79	3	2	2	43	.41	.189	16	16	.22	432	.11	2	1.92	.02	.09	1
\$ L22+50N 15+50E	1	18	38	276	.3	15	8	2745	2.81	6	5	ND	5	38	5	2	2	43	.24	.175	13	19	.29	310	.11	3	2.69	.03	.07	1
\$ L22+50N 16+00E	1	30	43	182	.4	14	9	889	3.01	15	5	ND	7	32	2	2	2	46	.24	.153	17	19	.34	210	.13	2	3.43	.04	.09	1
\$ L22+50N 16+50E	2	61	45	189	.6	15	10	1828	3.31	28	5	ND	5	35	1	2	2	55	.24	.177	15	26	.39	198	.09	2	2.35	.01	.10	1
\$ L22+50N 17+00E	2	58	38	129	.2	17	10	1238	3.42	12	5	ND	8	34	1	2	2	60	.22	.076	16	24	.44	167	.12	2	2.46	.01	.09	1
\$ L22+50N 17+50E	3	122	55	152	.8	18	13	1387	3.96	16	5	ND	6	29	1	2	2	63	.22	.151	25	27	.48	130	.10	3	2.86	.01	.11	1
\$ L22+50N 18+00E	1	26	44	99	.6	13	9	1266	3.35	7	5	ND	5	35	1	2	2	55	.23	.058	15	18	.30	209	.15	3	2.65	.02	.07	1
\$ L22+50N 18+50E	1	16	122	327	.7	13	8	1062	2.94	8	5	ND	8	29	2	2	2	43	.21	.105	15	16	.25	206	.14	5	3.72	.02	.07	1
\$ L22+50N 19+00E	1	23	172	259	.4	13	7	1948	3.53	13	5	ND	6	79	1	2	2	63	.55	.093	20	21	.34	203	.13	3	2.28	.02	.11	4
\$ L22+50N 19+50E	1	109	144	324	1.0	14	17	2259	4.59	11	5	ND	5	80	1	2	2	74	.47	.113	27	26	.70	236	.11	2	3.15	.01	.19	7
\$ L22+50N 20+00E	1	151	181	460	1.2	19	8	880	3.04	14	5	ND	9	97	2	2	2	42	.56	.182	18	21	.37	225	.13	5	3.66	.02	.10	1
\$ L23+00N 15+00E	2	23	34	194	.2	14	8	2094	3.23	2	5	ND	6	75	1	3	2	52	.46	.248	17	22	.33	310	.11	3	2.87	.01	.09	1
\$ L23+00N 15+50E	1	14	50	162	.4	12	7	2315	2.87	5	5	ND	7	79	1	2	2	43	.42	.155	22	17	.31	265	.09	3	2.91	.01	.07	1
\$ L23+00N 16+00E	1	74	40	146	.7	17	10	1158	3.84	31	5	ND	8	50	2	2	2	69	.39	.149	15	28	.51	224	.13	4	2.88	.03	.19	1
\$ L23+00N 16+50E	1	65	57	207	.5	17	9	1959	3.04	31	5	ND	6	52	1	2	2	49	.35	.113	13	25	.38	192	.09	3	2.24	.01	.10	1
\$ L23+00N 17+00E	3	309	45	413	1.5	19	11	1216	3.41	22	5	ND	8	34	2	2	2	54	.20	.081	20	25	.39	176	.11	5	2.73	.01	.07	1
\$ L23+00N 17+50E	2	31	51	146	.4	16	10	1579	3.29	10	5	ND	7	51	1	2	2	54	.39	.096	14	24	.34	170	.11	5	2.37	.01	.07	1
\$ L23+00N 18+00E	2	34	44	180	.3	19	10	860	3.45	11	5	ND	7	44	1	2	2	57	.25	.163	18	28	.45	230	.15	2	3.86	.01	.11	1
\$ L23+00N 18+50E	1	19	129	387	.9	13	7	2116	3.07	12	5	ND	8	23	3	2	2	47	.15	.135	16	15	.24	225	.14	4	3.75	.02	.05	1
\$ L23+00N 19+00E	2	31	118	218	.4	13	7	680	3.71	11	5	ND	8	26	1	2	2	64	.22	.117	15	21	.34	112	.08	3	2.26	.01	.07	2
\$ L23+00N 19+50E	2	60	300	680	1.3	14	8	1744	3.26	19	5	ND	7	161	9	3	2	44	.97	.197	25	19	.39	349	.06	3	2.34	.01	.13	2
\$ L23+00N 20+00E	1	96	70	182	1.2	10	7	1863	2.83	11	5	ND	10	49	1	2	2	41	.23	.136	15	15	.31	272	.05	2	2.62	.01	.11	1
\$ L23+50N 15+00E	1	380	266	504	2.0	24	12	3176	3.50	13	10	ND	14	91	8	3	2	49	.38	.198	54	28	.43	279	.10	2	3.14	.02	.16	1
STD C	18	58	39	127	7.4	69	28	1054	4.04	42	18	8	39	51	19	18	21	59	.47	.088	38	59	.84	180	.08	36	1.83	.05	.13	13

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE I	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA I	P I	LA PPM	CR PPM	H6 I	BA PPM	TI I	B PPM	AL I	NA I	K I	M PPM
\$ L23+50N 15+50E	1	9	35	62	.1	7	5	1454	2.50	3	5	ND	4	33	1	2	2	38	.24	.086	11	12	.22	167	.04	2	1.65	.01	.03	1
\$ L23+50N 16+00E	1	39	37	138	.9	12	9	1496	3.09	16	5	ND	5	32	1	2	2	48	.22	.133	11	17	.29	196	.10	2	2.38	.01	.07	1
\$ L23+50N 16+50E	2	60	53	175	.9	15	8	1999	2.70	16	5	ND	7	56	2	2	2	39	.40	.154	10	20	.33	286	.08	2	1.89	.01	.08	1
\$ L23+50N 17+00E	3	808	37	301	.9	50	10	905	4.10	6	5	ND	11	34	1	2	2	54	.28	.136	20	80	1.24	141	.15	2	2.94	.01	.15	1
\$ L23+50N 17+50E	1	33	43	111	.5	14	8	1947	3.01	6	5	ND	5	27	1	2	2	46	.16	.088	11	21	.30	283	.12	3	2.61	.01	.06	1
\$ L23+50N 18+00E	2	15	137	167	.2	12	7	1224	3.39	9	5	ND	4	30	1	2	2	55	.19	.102	9	18	.23	148	.08	2	1.62	.01	.05	1
\$ L23+50N 18+50E	1	22	126	212	.2	8	5	310	2.93	9	5	ND	5	17	1	2	2	45	.19	.100	11	14	.27	96	.04	2	1.51	.01	.04	2
\$ L23+50N 19+00E	1	20	115	200	.1	10	8	2171	3.48	12	5	ND	4	36	1	2	2	53	.23	.187	8	24	.25	179	.07	2	1.52	.01	.06	2
\$ L23+50N 19+50E	1	82	124	232	.7	12	11	3078	2.86	15	5	ND	4	89	5	2	2	36	.43	.150	9	17	.33	341	.07	4	2.03	.01	.09	1
\$ L23+50N 20+00E	2	171	85	208	.7	17	11	1358	3.46	13	5	ND	7	34	1	2	3	46	.21	.132	13	44	.51	175	.08	2	2.61	.01	.12	1
\$ L24+00N 15+00E	1	7	37	81	.1	7	5	1306	2.60	4	5	ND	4	40	1	2	2	40	.27	.143	12	14	.25	252	.03	2	1.58	.01	.06	1
\$ L24+00N 15+50E	1	33	51	198	.3	11	7	2848	3.19	7	5	ND	4	65	2	2	2	47	.31	.249	13	19	.28	423	.07	3	1.87	.01	.07	1
\$ L24+00N 16+00E	2	55	40	246	.8	11	9	1954	3.85	28	5	ND	5	35	2	2	2	64	.25	.070	16	22	.28	176	.14	2	1.51	.01	.06	1
\$ L24+00N 16+50E	2	142	49	225	1.5	13	9	1986	3.47	14	5	ND	3	42	1	2	2	56	.33	.110	13	26	.35	180	.13	2	1.89	.01	.06	1
\$ L24+00N 17+00E	2	43	61	168	.5	15	8	1667	3.45	17	5	ND	5	47	1	2	2	54	.28	.157	14	25	.35	199	.10	2	2.47	.01	.07	1
\$ L24+00N 17+50E	2	16	101	191	.3	12	7	1145	3.97	7	5	ND	6	33	1	2	2	62	.23	.092	10	21	.30	169	.13	3	2.63	.01	.06	1
\$ L24+00N 18+00E	2	19	91	146	.3	11	6	591	3.13	7	5	ND	5	22	1	3	2	51	.17	.139	9	22	.30	102	.07	2	1.78	.01	.05	1
\$ L24+00N 18+50E	1	80	259	424	1.2	11	8	1742	3.09	15	5	ND	7	102	7	2	2	44	.68	.132	29	17	.34	215	.07	3	1.94	.01	.10	15
\$ L24+00N 19+00E	1	41	119	157	.6	10	9	1686	2.89	10	5	ND	3	36	2	2	2	41	.23	.165	12	16	.32	144	.06	3	2.31	.01	.07	1
\$ L24+00N 19+50E	2	185	88	151	1.7	12	10	1838	2.87	18	5	ND	6	38	1	2	2	41	.19	.069	12	20	.38	162	.05	2	2.30	.01	.09	3
\$ L24+00N 20+00E	1	86	183	313	.6	13	9	1786	3.23	11	5	ND	5	55	4	2	2	45	.32	.108	16	20	.29	214	.11	3	2.61	.01	.08	1
\$ L24+50N 15+00E	1	21	96	232	.3	13	8	1817	3.05	7	5	ND	4	61	1	3	2	47	.35	.084	20	20	.37	200	.08	3	1.93	.01	.08	1
\$ L24+50N 15+50E	1	15	93	244	.3	10	6	1722	2.99	5	5	ND	5	62	2	2	2	48	.39	.121	18	18	.33	249	.08	3	2.27	.01	.08	1
\$ L24+50N 16+00E	1	28	67	245	.6	14	8	1689	3.25	2	5	ND	7	60	3	2	2	48	.34	.144	25	20	.35	250	.11	3	3.03	.01	.09	1
\$ L24+50N 16+50E	3	64	68	300	.7	14	9	3020	3.29	33	5	ND	2	40	2	2	2	48	.28	.188	13	20	.29	311	.10	2	1.97	.01	.08	1
\$ L24+50N 17+00E	2	30	54	200	.3	14	8	1493	3.49	16	5	ND	4	41	1	2	2	53	.27	.113	13	20	.33	187	.08	2	1.81	.01	.08	1
\$ L24+50N 17+50E	2	16	65	150	.2	12	8	3050	3.50	7	5	ND	5	72	1	2	2	52	.37	.094	13	16	.27	410	.15	2	2.38	.01	.09	1
\$ L24+50N 18+00E	3	123	116	282	.7	20	10	2115	3.82	15	7	ND	8	82	4	2	2	52	.42	.093	49	32	.52	247	.08	2	3.26	.01	.12	1
\$ L24+50N 18+50E	1	38	58	206	.3	15	10	1472	3.46	8	5	ND	5	87	1	2	3	46	.60	.243	14	26	.67	264	.11	2	2.67	.01	.13	1
\$ L24+50N 19+00E	1	40	151	220	.3	9	9	2523	2.60	11	5	ND	4	86	1	2	2	38	.46	.137	13	15	.30	237	.05	2	1.92	.01	.06	1
\$ L24+50N 19+50E	1	19	123	162	.1	10	6	1865	2.81	7	5	ND	4	71	2	2	2	46	.35	.098	12	15	.31	216	.05	2	1.72	.01	.08	1
\$ L24+50N 20+00E	2	143	77	200	.8	22	12	992	3.68	13	5	ND	9	57	2	2	2	63	.27	.066	14	37	.67	208	.12	2	3.04	.01	.15	2
\$ L25+00N 15+00E	1	32	143	369	.4	15	8	2479	3.16	6	5	ND	7	84	5	2	2	45	.46	.167	21	22	.39	304	.07	2	2.60	.01	.11	1
\$ L25+00N 15+50E	1	15	57	184	.2	12	6	2895	2.73	5	5	ND	5	56	2	2	2	41	.38	.180	14	17	.31	372	.05	4	1.98	.01	.08	1
\$ L25+00N 16+00E	1	11	49	198	.1	11	6	2477	2.79	4	5	ND	5	68	1	2	2	41	.37	.132	15	16	.29	283	.06	2	2.18	.01	.08	1
\$ L25+00N 16+50E	1	24	48	254	.5	12	10	2614	2.82	9	5	ND	6	108	1	3	2	39	.62	.301	18	17	.26	356	.11	2	3.02	.01	.07	1
\$ L25+00N 17+00E	2	20	52	176	.4	13	8	2348	3.04	5	5	ND	4	33	1	2	2	44	.18	.101	15	16	.27	220	.11	3	2.88	.01	.06	1
\$ L25+00N 17+50E	1	28	72	280	.4	14	7	1448	2.80	12	5	ND	7	26	2	2	2	40	.15	.220	14	17	.29	181	.10	4	3.22	.01	.11	1
\$ L25+00N 18+00E	2	42	101	159	.3	14	8	1491	3.27	17	5	ND	5	37	1	2	2	48	.22	.124	13	24	.43	156	.05	2	1.93	.01	.10	1
STD C	19	59	35	131	7.3	69	29	1052	4.12	42	22	7	40	52	17	17	21	60	.47	.088	39	59	.85	178	.08	34	1.84	.06	.14	11

SAMPLE#	MO PPM	CU PPM	PB PPM	ZN PPM	AG PPM	NI PPM	CO PPM	MN PPM	FE %	AS PPM	U PPM	AU PPM	TH PPM	SR PPM	CD PPM	SB PPM	BI PPM	V PPM	CA %	P %	LA PPM	CR PPM	MG %	BA PPM	TI %	B PPM	AL %	NA %	K %	W PPM
\$ L25+00N 18+50E	3	76	122	305	1.5	18	9	1517	4.27	10	5	ND	9	76	1	2	2	63	.42	.121	39	28	.48	240	.09	5	3.44	.01	.13	1
\$ L25+00N 19+00E	2	42	136	185	.5	11	7	822	3.20	5	5	ND	8	33	1	2	2	48	.19	.103	18	19	.39	94	.07	5	2.81	.01	.08	3
\$ L25+00N 19+50E	1	20	201	283	.4	11	7	1831	2.93	4	5	ND	5	50	1	2	2	42	.26	.072	18	18	.40	214	.08	2	2.65	.01	.09	1
\$ L25+00N 20+00E	2	177	131	252	1.1	18	11	1652	3.66	10	5	ND	6	56	1	2	2	54	.30	.106	19	28	.58	225	.10	3	3.52	.01	.15	1
\$ L25+50N 15+00E	2	31	188	362	.3	15	7	2031	3.11	5	5	ND	7	57	3	2	2	42	.38	.115	17	22	.40	292	.07	3	2.36	.01	.13	2
\$ L25+50N 15+50E	2	91	153	819	.6	15	10	2830	3.29	6	5	ND	5	129	11	2	2	40	.83	.121	19	22	.39	383	.10	6	2.76	.01	.12	1
\$ L25+50N 16+00E	1	16	65	226	.2	12	7	2322	3.24	2	5	ND	7	107	1	2	2	45	.47	.236	18	19	.33	358	.07	2	2.72	.01	.08	1
\$ L25+50N 16+50E	1	24	57	158	.2	12	8	1744	3.16	5	5	ND	6	73	1	2	2	44	.32	.124	15	17	.27	305	.15	7	2.52	.01	.08	1
\$ L25+50N 17+00E	2	20	56	215	.9	12	7	1410	2.78	6	5	ND	3	74	1	2	2	36	.47	.209	17	17	.29	284	.10	3	3.34	.01	.09	2
\$ L25+50N 17+50E	2	69	103	377	.7	17	8	551	3.42	8	5	ND	6	50	1	2	2	46	.30	.096	18	23	.38	235	.09	4	3.06	.01	.12	2
\$ L25+50N 18+00E	2	22	140	247	.2	12	7	1515	3.92	11	5	ND	6	44	1	2	2	61	.29	.076	17	22	.39	164	.08	6	1.78	.01	.07	2
\$ L25+50N 18+50E	2	28	101	295	.5	13	8	1962	3.36	8	5	ND	6	51	1	2	2	47	.29	.168	15	22	.38	295	.08	4	2.58	.01	.09	2
\$ L25+50N 19+00E	1	28	191	298	.3	15	8	1695	3.41	6	5	ND	8	56	1	2	2	49	.32	.134	18	24	.47	183	.10	5	3.17	.01	.11	1
\$ L25+50N 19+50E	1	40	399	420	.6	14	8	1965	3.51	8	5	ND	7	80	2	2	2	52	.45	.107	25	24	.49	269	.08	4	2.77	.01	.14	1
\$ L25+50N 20+00E	1	29	153	373	.4	15	8	2453	3.10	7	5	ND	5	136	2	2	2	41	.72	.156	17	23	.50	328	.09	5	2.87	.01	.17	1
\$ L25+50N 20+50E	3	39	269	291	.9	14	8	1670	3.13	8	5	ND	6	97	1	2	2	46	.52	.099	19	22	.47	269	.09	5	2.83	.01	.14	1
\$ L25+50N 21+00E	1	37	466	617	.5	12	8	2837	3.24	11	5	ND	5	123	3	2	2	44	.66	.117	20	21	.48	438	.08	3	2.43	.01	.18	1
\$ L25+50N 21+50E	2	371	322	514	1.4	15	15	1896	4.21	13	5	ND	9	79	1	2	13	53	.34	.094	38	24	.45	284	.10	3	2.62	.01	.11	1
\$ L25+50N 22+00E	3	253	203	644	1.2	17	22	1961	3.85	9	5	ND	7	82	3	2	10	45	.28	.120	36	24	.47	191	.11	2	2.47	.01	.11	1
\$ L25+50N 22+50E	1	32	174	389	.5	14	9	1922	3.45	5	5	ND	8	110	5	2	2	48	.43	.139	27	25	.52	350	.09	3	2.83	.01	.16	1
\$ L25+50N 23+00E	1	22	183	344	.5	12	7	1424	3.31	2	5	ND	8	95	1	2	2	45	.50	.160	23	21	.43	311	.08	2	2.82	.01	.15	1
\$ L25+50N 23+50E	1	20	177	329	.5	11	7	1425	3.20	5	5	ND	7	91	1	2	2	44	.49	.157	21	20	.40	313	.07	3	2.54	.01	.13	1
\$ L25+50N 24+00E	1	24	175	368	.5	13	8	1932	3.14	6	5	ND	5	107	1	2	2	45	.57	.065	22	21	.40	236	.10	2	2.24	.01	.09	1
\$ L25+50N 24+50E	1	27	175	520	.4	12	12	1258	3.37	7	5	ND	6	43	2	2	2	48	.30	.110	17	20	.35	141	.12	5	2.58	.01	.08	1
\$ L26+00N 15+00E	2	20	69	207	.4	15	8	1611	3.29	2	5	ND	4	59	1	2	2	50	.40	.086	19	22	.41	165	.11	2	2.91	.01	.09	1
\$ L26+00N 15+50E	1	15	91	259	.4	12	7	1821	3.00	3	5	ND	7	67	1	2	2	45	.43	.111	26	22	.40	237	.09	4	2.77	.01	.10	1
\$ L26+00N 16+00E	1	14	65	206	.3	12	7	2272	3.11	6	5	ND	5	94	1	2	2	45	.47	.100	19	21	.36	258	.08	4	2.52	.01	.09	1
\$ L26+00N 16+50E	2	40	107	386	.4	17	9	1751	3.79	5	5	ND	9	88	1	2	2	52	.63	.103	37	26	.42	352	.11	2	3.06	.01	.16	1
\$ L26+00N 17+00E	2	93	90	359	.6	20	10	2437	3.69	10	5	ND	6	78	5	2	2	52	.50	.204	17	35	.53	328	.09	3	2.54	.01	.13	1
\$ L26+00N 17+50E	2	28	105	210	.5	12	7	1499	3.36	3	5	ND	6	36	1	2	2	52	.26	.068	20	21	.34	172	.10	2	2.48	.01	.06	1
\$ L26+00N 18+00E	2	22	164	303	.4	12	8	2460	3.34	10	5	ND	5	74	1	2	2	50	.40	.153	18	21	.35	283	.09	2	2.35	.01	.08	2
\$ L26+00N 18+50E	2	73	89	235	.7	14	12	1176	3.49	12	5	ND	9	49	1	2	3	43	.26	.303	14	17	.38	184	.13	2	4.31	.01	.10	1
\$ L26+00N 19+00E	2	60	147	227	.7	19	11	1335	3.81	8	5	ND	9	36	1	2	7	53	.20	.112	20	27	.57	184	.11	3	3.66	.01	.12	1
\$ L26+00N 19+50E	1	21	257	266	.4	11	7	1834	2.97	5	5	ND	7	75	2	2	2	45	.46	.080	21	19	.41	230	.10	2	2.56	.01	.13	1
\$ L26+00N 20+00E	1	74	216	386	.8	13	9	1815	3.21	14	5	ND	5	115	1	2	2	44	.64	.095	37	23	.47	219	.09	2	3.00	.01	.14	1
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\$ L26+00N 21+50E	2	68	314	431	1.1	16	11	1947	3.82	7	5	ND	11	102	4	2	4	55	.47	.112	27	24	.40	179	.09	5	2.05	.01	.11	1
\$ L26+00N 22+00E	2	141	349	475	1.6	14	10	2103	3.79	13	5	ND	6	103	3	2	13	42	.39	.175	22	25	.44	365	.09	5	2.44	.01	.12	1
STD C	19	57	40	132	7.0	68	27	1035	4.12	39	26	8	39	50	17	17	20	57	.47	.085	38	57	.84	179	.08	33	1.82	.05	.13	11

SAMPLE#	MO PPM	CU PPH	PB PPH	ZN PPH	AG PPH	NI PPH	CO PPH	MN PPH	FE I	AS PPH	U PPH	AU PPH	TH PPH	SR PPH	CD PPH	SB PPH	BI PPH	V PPH	CA I	P I	LA PPM	CR PPH	MG I	BA PPH	TI I	B PPH	AL I	NA I	K I	M PPM
\$ L26+00N 22+50E	1	58	240	421	.5	16	13	2317	3.74	10	5	ND	6	85	7	2	2	53	.33	.113	27	30	.56	368	.12	2	2.33	.01	.14	1
\$ L26+00N 23+00E	1	27	184	321	.4	13	8	1670	3.18	2	5	ND	8	98	3	2	2	46	.45	.182	24	25	.48	387	.09	3	2.80	.01	.15	1
\$ L26+00N 23+50E	1	67	220	359	1.0	13	24	2719	3.17	2	8	ND	6	57	3	2	2	50	.25	.123	57	25	.40	164	.09	5	2.59	.01	.09	1
\$ L26+00N 24+00E	1	28	203	489	.7	15	10	2013	3.25	13	5	ND	5	85	4	2	2	49	.41	.077	19	25	.43	228	.09	2	2.18	.01	.11	1
\$ L26+00N 24+50E	1	43	216	662	1.0	13	14	1742	3.43	9	5	ND	6	50	5	2	2	51	.34	.133	22	23	.41	143	.11	4	2.63	.01	.09	1
\$ L26+50N 15+00E	1	16	81	204	.3	11	7	1741	2.84	4	5	ND	4	68	2	2	2	46	.44	.126	17	19	.35	265	.08	3	2.44	.01	.10	2
\$ L26+50N 15+50E	1	18	93	264	.4	14	8	2136	3.04	4	5	ND	7	74	2	2	2	47	.45	.202	23	26	.46	366	.07	2	2.83	.01	.12	1
\$ L26+50N 16+00E	1	25	112	494	.2	13	8	3509	2.98	2	5	ND	5	93	4	2	2	42	.60	.206	21	22	.36	563	.07	2	2.61	.01	.13	1
\$ L26+50N 16+50E	1	35	220	317	.5	14	9	2455	3.53	6	5	ND	5	92	2	2	2	52	.51	.119	35	23	.40	228	.05	2	3.09	.01	.14	1
\$ L26+50N 17+00E	1	39	124	471	1.3	14	8	2570	3.23	5	5	ND	7	65	6	2	2	46	.39	.255	18	23	.33	433	.08	4	2.76	.01	.09	1
\$ L26+50N 17+50E	1	20	109	223	.2	14	7	2094	2.91	5	5	ND	7	40	3	2	2	43	.22	.109	14	20	.31	202	.12	2	3.05	.01	.06	1
\$ L26+50N 18+00E	1	65	126	398	1.0	19	11	953	3.56	4	5	ND	8	60	3	2	2	45	.42	.157	17	31	.51	346	.13	3	4.30	.02	.11	2
\$ L26+50N 18+50E	1	26	229	243	.7	10	8	3034	2.73	11	5	ND	5	62	4	2	2	42	.34	.099	15	16	.28	267	.06	2	1.64	.01	.08	2
\$ L26+50N 19+00E	1	33	237	358	.8	15	8	2699	3.32	8	5	ND	8	60	4	2	2	51	.30	.159	29	26	.47	290	.10	3	2.99	.01	.15	1
\$ L26+50N 19+50E	1	19	249	521	.8	11	7	2386	2.59	7	5	ND	6	70	4	2	2	36	.40	.154	19	18	.33	362	.09	2	2.56	.01	.09	2
\$ L26+50N 20+00E	1	40	203	398	.7	14	9	1485	2.96	12	5	ND	5	107	4	2	2	46	.60	.154	20	26	.47	290	.08	2	2.52	.01	.16	1
706521	5	181	2839	6129	7.1	9	9	476	4.40	49	5	ND	3	3	82	2	2	33	.06	.038	3	55	.46	21	.01	2	.97	.01	.22	1
706522	3	2051	24160	42048	71.5	10	37	524	5.15	3641	5	ND	1	2	314	30	11	20	.06	.026	2	61	.33	8	.01	2	.60	.01	.13	1
STD C	18	59	40	129	7.1	67	28	1042	4.03	38	21	8	40	50	18	18	19	58	.47	.087	38	61	.84	180	.08	37	1.82	.06	.13	13

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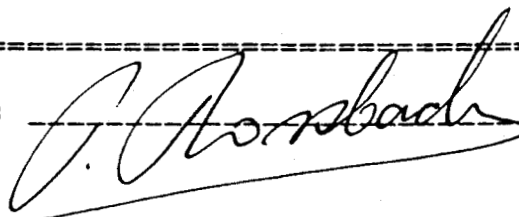
CERTIFICATE OF ANALYSIS

TO : KOOTENAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER B.C.
 PROJECT: 410
 TYPE OF ANALYSIS: GEOCHEMICAL

CERTIFICATE#: 87741
 INVOICE#: 80138
 DATE ENTERED: 87-10-30
 FILE NAME: KKR87741
 PAGE # : 1

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S	1600E	S
S	1650E	S
S	1700E	S
S	1750E	S
S	1800E	S
S	1850E	S
S	1900E	S
S	1950E	S
S	L2000N 2000E	S
S	L2050N 1500E	S
S	1550E	S
S	1600E	S
S	1650E	S
S	1700E	S
S	1750E	S
S	1800E	S
S	1850E	S
S	1900E	S
S	1950E	S
S	L2050N 2000E	S
S	L2100N 1500E	S
S	1550E	S
S	1600E	S
S	1650E	S
S	1700E	S
S	1750E	S
S	1800E	S
S	1850E	S
S	1900E	S
S	1950E	S
S	L2100N 2000E	S
S	L2150N 1500E	S
S	1550E	S
S	1600E	S
S	1650E	S
S	1700E	S
S	1750E	S
S	L2150N 1800E	S

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CERTIFICATE OF ANALYSIS

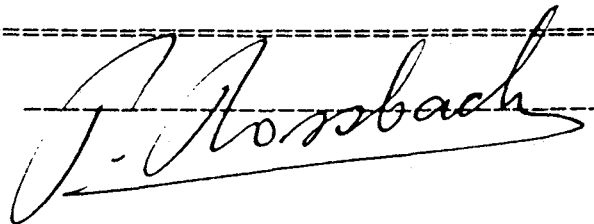
TO : KOOTENAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER B.C.

CERTIFICATE#: 87741
 INVOICE#: 80138
 DATE ENTERED: 87-10-30
 FILE NAME: KKR87741
 PAGE # : 2

PROJECT: 410
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
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S	1900E	5
S	1950E	5
S	L2150N 2000E	5
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S	1600E	5
S	1650E	5
S	1700E	5
S	1750E	5
S	1800E	5
S	1850E	5
S	1900E	5
S	1950E	5
S	L2200N 2000E	5
S	L2250N 1500E	5
S	1550E	5
S	1600E	5
S	1650E	5
S	1700E	5
S	1750E	5
S	1800E	5
S	1850E	5
S	1900E	5
S	1950E	5
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S	1550E	5
S	1600E	5
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S	1800E	5
S	1850E	5
S	1900E	5
S	1950E	5
S	L2300N 2000E	5
S	L2350N 1500E	5
S	1550E	5
S	L2350N 1600E	5

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APPENDIX III

STATISTICAL ANALYSIS OF 1987 SOIL GEOCHEMICAL DATA

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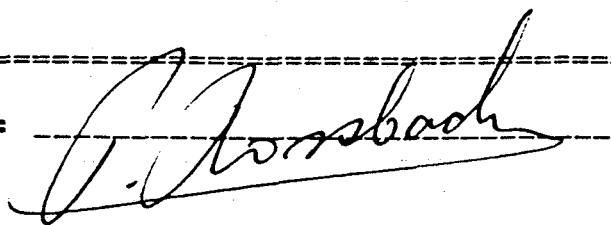
CERTIFICATE OF ANALYSIS

TO : KOOTENAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER B.C.
 PROJECT: 410
 TYPE OF ANALYSIS: GEOCHEMICAL

CERTIFICATE#: 87741
 INVOICE#: 80138
 DATE ENTERED: 87-10-30
 FILE NAME: KKR87741
 PAGE # : 3

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S	1700E	S
S	1750E	S
S	1800E	S
S	1850E	S
S	1900E	S
S	1950E	S
S	L2350N 2000E	S
S	L2400N 1500E	S
S	1550E	S
S	1600E	S
S	1650E	S
S	1700E	S
S	1750E	S
S	1800E	S
S	1850E	S
S	1900E	S
S	1950E	S
S	L2400N 2000E	S
S	L2450N 1500E	S
S	1550E	S
S	1600E	S
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S	1700E	S
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S	1850E	S
S	1900E	S
S	1950E	S
S	L2450N 2000E	S
S	L2500N 1500E	S
S	1550E	S
S	1600E	S
S	1650E	S
S	1700E	S
S	1750E	S
S	1800E	S
S	1850E	S
S	1900E	S
S	L2450N 1950E	S

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2225 S. SPRINGER AVENUE
 BURNABY, B.C. V5B 3N1
 TEL : (604) 299 - 6910

CERTIFICATE OF ANALYSIS

CLIENT : KOOTENAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER B.C.
 PROJECT: 410
 TYPE OF ANALYSIS: GEOCHEMICAL

CERTIFICATE#: 97741
 INVOICE#: 90138
 DATE ENTERED: 87-10-30
 FILE NAME: KKR87741
 PAGE # : 4

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3	1550E	5
3	1600E	5
3	1650E	5
3	1700E	5
3	1750E	5
3	1800E	5
3	1850E	5
3	L2550N 1900E	5
3	1950E	5
3	2000E	5
3	2050E	5
3	2100E	5
3	2150E	5
3	2200E	5
3	2250E	5
3	2300E	5
3	2350E	5
3	2400E	5
3	L2550N 2450E	5
3	L2600N 1500E	5
3	1550E	5
3	1600E	5
3	1650E	5
3	1700E	5
3	1750E	5
3	1800E	5
3	1850E	5
3	L2600N 1900E	5
3	1950E	5
3	2000E	5
3	2050E	5
3	2100E	5
3	2150E	5
3	2200E	5
3	2250E	5
3	2300E	5
3	2350E	5
3	L2600N 2400E	5

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ROSSBACHER LABORATORY LTD.

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BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

CERTIFICATE OF ANALYSIS

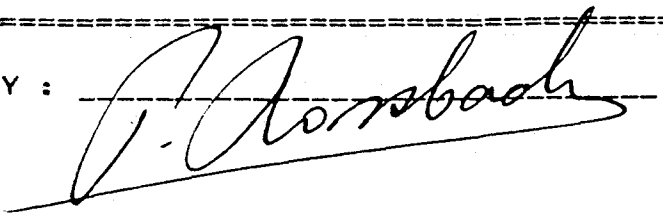
TO : KOOTENAY KING RESOURCES INC.,
619-744 W HASTINGS ST.,
VANCOUVER B.C.

CERTIFICATE#: 87741
INVOICE#: 80138
DATE ENTERED: 87-10-30
FILE NAME: KKR87741
PAGE # : 5

PROJECT: 410
TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
S	L2600N 2450E	5
S	L2650N 1500E	5
S	1550E	5
S	1600E	5
S	1650E	5
S	1700E	5
S	1750E	5
S	1800E	5
S	1850E	5
S	1900E	5
S	1950E	5
S	L2650N 2000E	5

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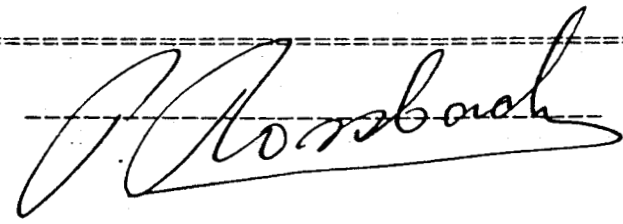
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 BURNABY, B.C. V5B 3N1
 TEL : (604) 299 - 6910

TO : KOOTNAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER, B.C.

CERTIFICATE#: 87830
 INVOICE#: 80255
 DATE ENTERED: 87-12-03
 FILE NAME: KKR87830
 PAGE # : 1

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
S	1900N 1500E	5
S	1550E	5
S	1600E	5
S	1650E	5
S	1700E	5
S	1750E	5
S	1800E	5
S	1850E	80
S	1900E	5
S	1900N 1950E	5
S	2000E	5
S	2050E	5
S	2100E	5
S	2150E	5
S	2200E	5
S	2250E	5
S	2300E	5
S	2350E	5
S	2400E	5
S	1900N 2450E	5
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2750E	5
S	2800E	5
S	2850E	5
S	2900E	5
S	1900N 2950E	5
S	3000E	5
S	3050E	5
S	1900N 3100E	5
S	1950N 1500E	5
S	1550E	5
S	1600E	5
S	1650E	5
S	1700E	5
S	1750E	5
S	1950N 1800E	5

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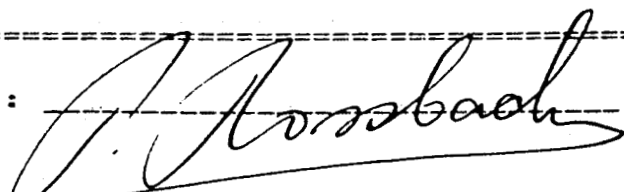
CLIENT: KOOTNAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER, B.C.

CERTIFICATE#: 87830
 INVOICE#: 80255
 DATE ENTERED: 87-12-03
 FILE NAME: KKR87830
 PAGE # : 2

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

INDEX	SAMPLE NAME	PPB Au
S	1950N 1850E	5
S	1900E	5
S	1950E	5
S	2000E	5
S	2050E	210
S	2150E	5
S	2200E	5
S	2250E	5
S	2300E	5
S	1950N 2350E	5
S	2400E	5
S	2450E	5
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2750E	5
S	2800E	5
S	1950N 2850E	5
S	2900E	5
S	2950E	5
S	1950N 3000E	5
S	2000N 2050E	5
S	2100E	5
S	2150E	5
S	2200E	5
S	2250E	5
S	2300E	5
S	2000N 2350E	5
S	2400E	5
S	2450E	20
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2750E	30
S	2800E	5
S	2000N 2850E	5

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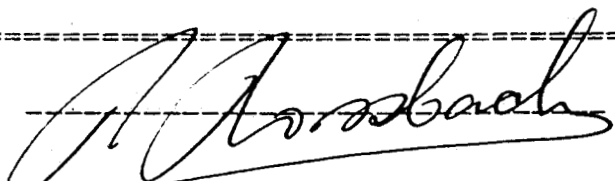
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BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

TO : KOOTNAY KING RESOURCES INC.,
619-744 W HASTINGS ST.,
VANCOUVER, B.C.

CERTIFICATE#: 87830
INVOICE#: 80255
DATE ENTERED: 87-12-03
FILE NAME: KPR87830
PAGE # : 3

PROJECT:
TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
S	2000N 2900E	5
S	2950E	5
S	2000N 3000E	5
S	2050N 2050E	5
S	2100E	5
S	2150E	5
S	2200E	5
S	2250E	5
S	2300E	20
S	2050N 2350E	5
S	2400E	5
S	2450E	5
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2750E	5
S	2800E	5
S	2050N 2850E	5
S	2900E	5
S	2950E	5
S	2050N 3000E	5
S	2100N 2050E	5
S	2100E	40
S	2150E	5
S	2200E	5
S	2250E	5
S	2300E	5
S	2100N 2350E	5
S	2400E	5
S	2450E	5
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2750E	5
S	2800E	5
S	2100N 2850E	5

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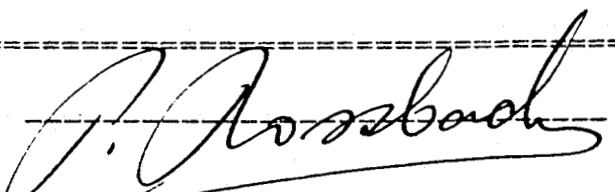
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 619-744 W HASTINGS ST.,
 VANCOUVER, B.C.

CERTIFICATE#: 87930
 INVOICE#: 00255
 DATE ENTERED: 87-12-03
 FILE NAME: MKRS7830
 PAGE # : 4

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
S	2100N 2900E	S
S	2950E	S
S	2100N 3000E	S
S	2150N 2050E	S
S	2100E	S
S	2150E	S
S	2200E	S
S	2250E	S
S	2300E	S
S	2150N 2350E	S
S	2400E	S
S	2450E	S
S	2500E	S
S	2550E	S
S	2600E	S
S	2650E	S
S	2700E	S
S	2750E	S
S	2800E	S
S	2150N 2850E	S
S	2900E	S
S	2950E	S
S	2150N 3000E	S
S	2200N 2050E	S
S	2100E	S
S	2150E	S
S	2200E	S
S	2250E	S
S	2300E	S
S	2200N 2350E	S
S	2400E	S
S	2450E	S
S	2500E	S
S	2550E	S
S	2600E	S
S	2650E	S
S	2700E	S
S	2750E	S
S	2800E	S
S	2200N 2850E	S

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 VANCOUVER, B.C.

CERTIFICATE#: 07830
 INVOICE#: 80255
 DATE ENTERED: 87-12-03
 FILE NAME: KKR87830
 PAGE # : 5

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
0	2200N 2900E	0
0	2950E	0
0	2200N 2985E	0
0	2250N 2050E	0
0	2100E	0
0	2150E	0
0	2200E	0
0	2250E	0
0	2300E	0
0	2250N 2350E	0
0	2400E	0
0	2450E	0
0	2500E	0
0	2550E	0
0	2600E	0
0	2650E	0
0	2700E	0
0	2750E	0
0	2800E	0
0	2250N 2850E	0
0	2900E	0
0	2950E	0
0	2250N 3000E	0
0	2300N 2050E	0
0	2100E	0
0	2150E	0
0	2200E	0
0	2250E	0
0	2300E	0
0	2300N 2350E	0
0	2400E	0
0	2450E	0
0	2500E	0
0	2550E	0
0	2600E	0
0	2650E	0
0	2700E	0
0	2750E	0
0	2800E	0
0	2300N 2850E	0

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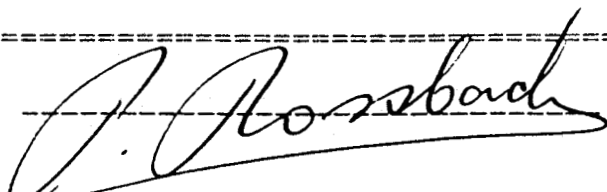
TO : KOOTNAY KING RESOURCES INC.,
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 VANCOUVER, B.C.

CERTIFICATE#: 97030
 INVOICE#: 90255
 DATE ENTERED: 87-12-03
 FILE NAME: KKR97030
 PAGE # : 6

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
5	2300N 2900E	5
5	2950E	5
5	2300N 3000E	5
5	2350N 2050E	5
5	2100E	5
5	2150E	5
5	2200E	5
5	2250E	5
5	2300E	5
5	2350N 2350E	5
5	2400E	5
5	2450E	5
5	2500E	5
5	2550E	5
5	2600E	5
5	2650E	5
5	2700E	5
5	2750E	5
5	2800E	5
5	2350N 2850E	5
5	2900E	5
5	2950E	5
5	2350N 3000E	5
5	2400N 2050E	5
5	2100E	5
5	2150E	5
5	2200E	5
5	2250E	5
5	2300E	5
5	2400N 2350E	5
5	2400E	5
5	2450E	5
5	2500AE	5
5	2500BE	5
5	2550E	5
5	2600E	5
5	2650E	80
5	2700E	5
5	2750E	5
5	2400N 2800E	5

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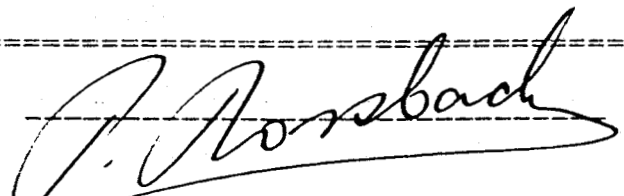
TO : KOOTNAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER, B.C.

CERTIFICATE#: 87830
 INVOICE#: 80255
 DATE ENTERED: 97-12-03
 FILE NAME: MKR87830
 PAGE # : 7

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
S	2400N 2850E	5
S	2900E	5
S	2950E	5
S	2400N 3000E	5
S	2450N 2050E	5
S	2100E	5
S	2150E	5
S	2200E	5
S	2250E	5
S	2450N 2300E	5
S	2350E	5
S	2400E	5
S	2450E	5
S	2500AE	5
S	2500BE	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2450N 2750E	5
S	2800E	5
S	2850E	5
S	2900E	5
S	2950E	5
S	2450N 3000E	5
S	2500N 2050E	5
S	2100E	5
S	2150E	5
S	2200E	5
S	2500N 2250E	5
S	2300E	5
S	2350E	5
S	2400E	5
S	2450E	5
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2500N 2750E	5

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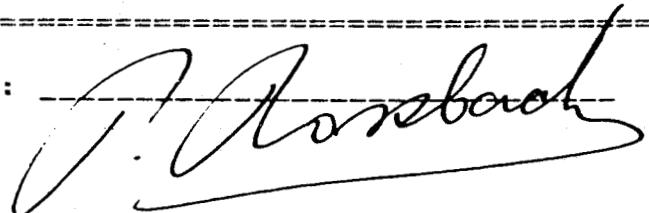
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 VANCOUVER, B.C.

CERTIFICATE#: 87830
 INVOICE#: 80255
 DATE ENTERED: 87-12-03
 FILE NAME: KKR87830
 PAGE # : 6

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	FPB Au
S	2500N 2800E	S
S	2850E	S
S	2900E	S
S	2950E	S
S	2500N 3000E	S
S	2550N 2500E	S
S	2550E	S
S	2600E	S
S	2650E	S
S	2550N 2700E	430
S	2750E	S
S	2800E	S
S	2850E	S
S	2900E	S
S	2950E	S
S	2550N 3000E	S
S	2600N 2500E	S
S	2550E	S
S	2600E	S
S	2600N 2650E	S
S	2700E	S
S	2750E	S
S	2800E	S
S	2850E	S
S	2900E	S
S	2950E	S
S	3000E	S
S	3050E	S
S	2600N 3100E	S
S	2650N 2050E	S
S	2100E	S
S	2150E	S
S	2200E	S
S	2250E	S
S	2300E	S
S	2350E	S
S	2400E	S
S	2450E	S
S	2500E	S
S	2650N 2550E	S

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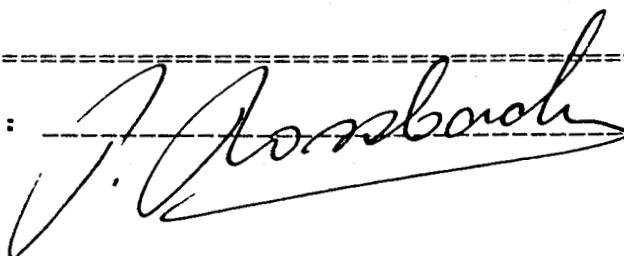
TO : KOOTNAY KING RESOURCES INC.,
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CERTIFICATE#: 87830
 INVOICE#: 80255
 DATE ENTERED: 87-12-03
 FILE NAME: KKR87830
 PAGE # : 10

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

PRE FIX	SAMPLE NAME	PPB Au
S	2700N 2750E	5
S	2800E	5
S	2850E	5
S	2900E	5
S	2950E	5
S	3000E	5
S	3050E	5
S	3100E	5
S	3150E	5
S	2700N 3200E	5
S	3250E	5
T	2700N 3300E	5
S	2750N 1500E	5
S	1550E	5
S	1600E	5
S	1650E	5
S	1700E	5
S	1750E	5
S	1800E	5
S	2750N 1850E	5
S	1900E	5
S	1950E	5
S	2000E	5
S	2050E	5
S	2100E	5
S	2150E	5
S	2200E	5
S	2250E	20
S	2300E	5
S	2750N 2350E	5
S	2400E	5
S	2450E	5
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2750E	5
S	2800E	5
S	2750N 2850E	5

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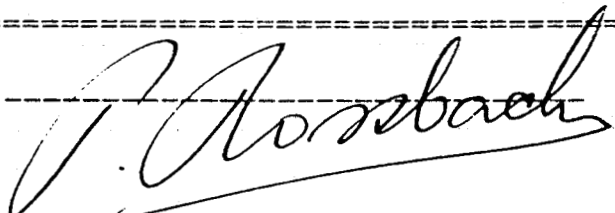
CLIENT: KOOTNAY KING RESOURCES INC.,
 619-744 W HASTINGS ST.,
 VANCOUVER, B.C.

CERTIFICATE#: 87830
 INVOICE#: 80255
 DATE ENTERED: 87-12-03
 FILE NAME: KRR87830
 PAGE # : 11

PROJECT:
 TYPE OF ANALYSIS: GEOCHEMICAL

INDEX	SAMPLE NAME	PPB Au
S	2750N 2900E	5
S	2950E	5
S	2750N 3000E	5
S	2800N 1500E	5
S	1550E	5
S	1600E	40
S	1650E	5
S	1700E	5
S	1750E	5
S	2800N 1800E	5
S	1850E	5
S	1900E	5
S	1950E	5
S	2000E	5
S	2050E	5
S	2100E	5
S	2150E	5
S	2200E	5
S	2250E	5
S	2800N 2300E	5
S	2350E	5
S	2400E	5
S	2450E	5
S	2500E	5
S	2550E	5
S	2600E	5
S	2650E	5
S	2700E	5
S	2750E	5
S	2800N 2800E	5
S	2850E	5
S	2900E	5
S	2950E	5
S	2800N 3000E	5
S	2850N 1500E	5
S	1550E	5
S	1600E	5
S	1650E	5
S	1700E	5
S	2850N 1750E	5

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CERTIFICATE OF ANALYSIS

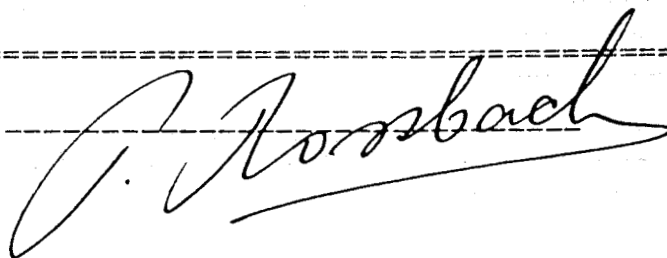
CLIENT: KOOTNAY KING RESOURCES INC.,
619-744 W HASTINGS ST.,
VANCOUVER, B.C.

CERTIFICATE#: 87830
INVOICE#: 80255
DATE ENTERED: 87-12-03
FILE NAME: KKR87830
PAGE # : 12

PROJECT:
TYPE OF ANALYSIS: GEOCHEMICAL

INDEX	SAMPLE NAME	FPB Au
5	2850N 1800E	5
5	1850E	5
5	1900E	5
5	1950E	5
5	2000E	5
5	2050E	5
5	2100E	5
5	2150E	5
5	2200E	5
5	2850N 2250E	5
5	2300E	5
5	2350E	5
5	2400E	5
5	2450E	5
5	2500E	5
5	2550E	5
5	2600E	5
5	2650E	5
5	2700E	5
5	2850N 2750E	5
5	2800E	5
5	2850E	5
5	2900E	5
5	2950E	5
5	2850N 3000E	5

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STATISTICAL REPORT

2225 S. SPRINGER AVENUE
 BURNABY, B.C. V5B 3N1
 TEL : (604) 299 - 6910

Client: A&M EXPLORATION LTD.
 850 W. HASTINGS ST.
 VANCOUVER, B.C.

Project: ERIE CREEK
 Date: 88-08-04

Element: CU

Sample Type: Soil

CLASS INTERVAL	CLASS FREQUENCY	RELATIVE FREQUENCY%	CUMULATIVE FREQUENCY%	CLASS MEAN
0 - 39	295	49.41	49.41	26.24
40 - 78	163	27.30	76.71	55.96
79 - 117	69	11.56	88.27	93.99
118 - 156	23	3.85	92.12	137.17
157 - 195	17	2.85	94.97	174.88
196 - 234	6	1.01	95.98	213.83
235 - 273	2	0.34	96.32	245.00
274 - 312	6	1.01	97.33	293.67
313 - 351	3	0.50	97.83	332.67
352 - 390	4	0.67	98.50	369.75
391 - 429	0	0.00	98.50	0.00
430 - 468	1	0.17	98.67	453.00
469 - 507	2	0.34	99.01	489.50
508 - 546	1	0.17	99.18	539.00
547 - 585	0	0.00	99.18	0.00
586 - 624	1	0.17	99.35	586.00
625 - 663	1	0.17	99.52	657.00
664 - 702	1	0.17	99.69	668.00
703 - 741	0	0.00	99.69	0.00
742 - 780	0	0.00	99.69	0.00
781 - 819	1	0.17	99.86	808.00
820 - 858	0	0.00	99.86	0.00
859 - 897	0	0.00	99.86	0.00
898 - 936	1	0.17	100.00	927.00

For Statistics

For All Data

Number of Samples:	597	597
Arithmetic Mean :	68.85	N.A.
Standard Deviation :	91.57	N.A.
Minimum Value :	7	.1
Maximum Value :	927	927
Range :	0 -- 10000 PPM	.1 -- 927 PPM

File(s) used for Statistics:

1 F2 F3 F4

ROSSBACHER LABORATORY LTD.

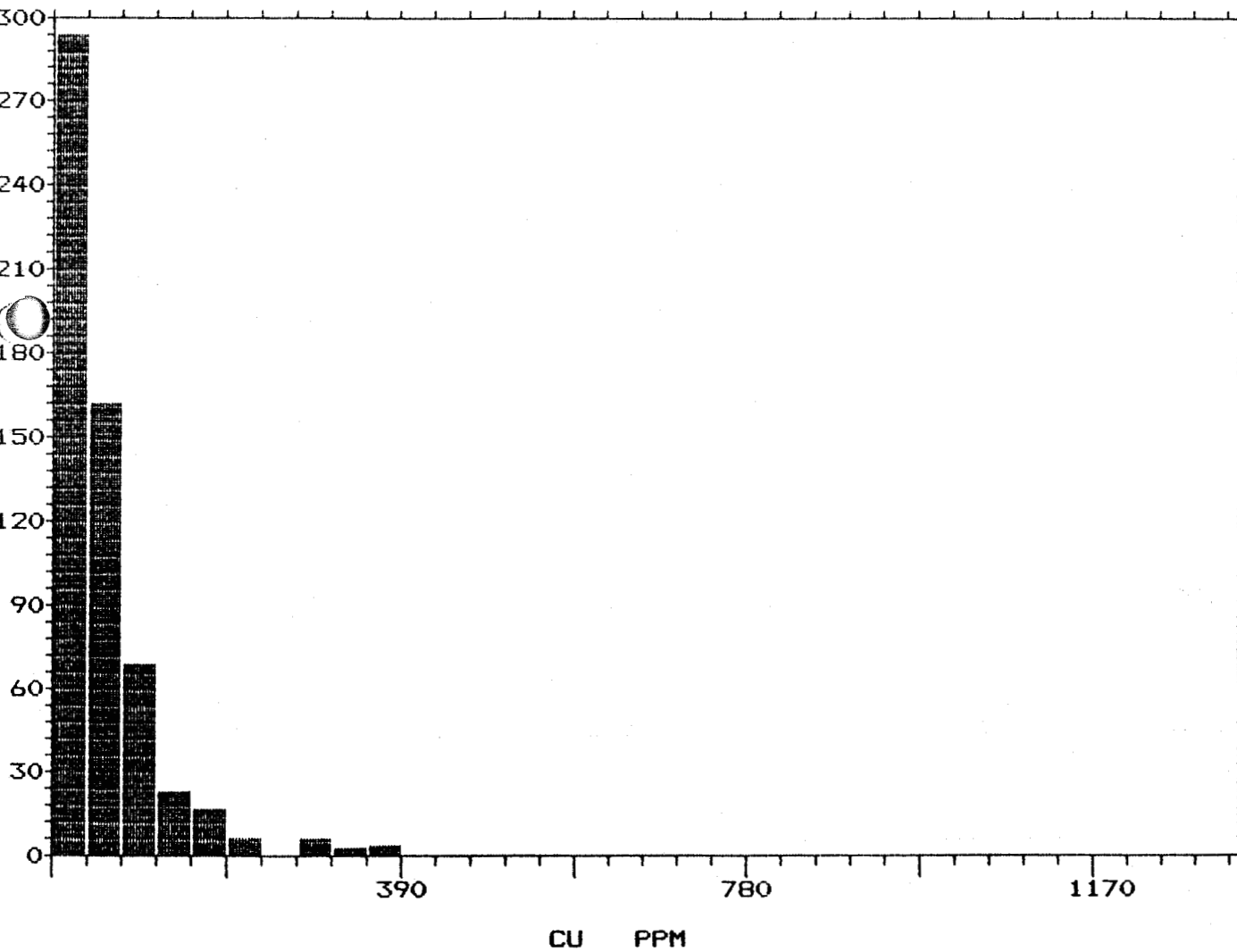
2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.
Element: CU

Project: ERIE CREEK
Date: 88-08-04
Sample Type: Soil

Frequency Histogram

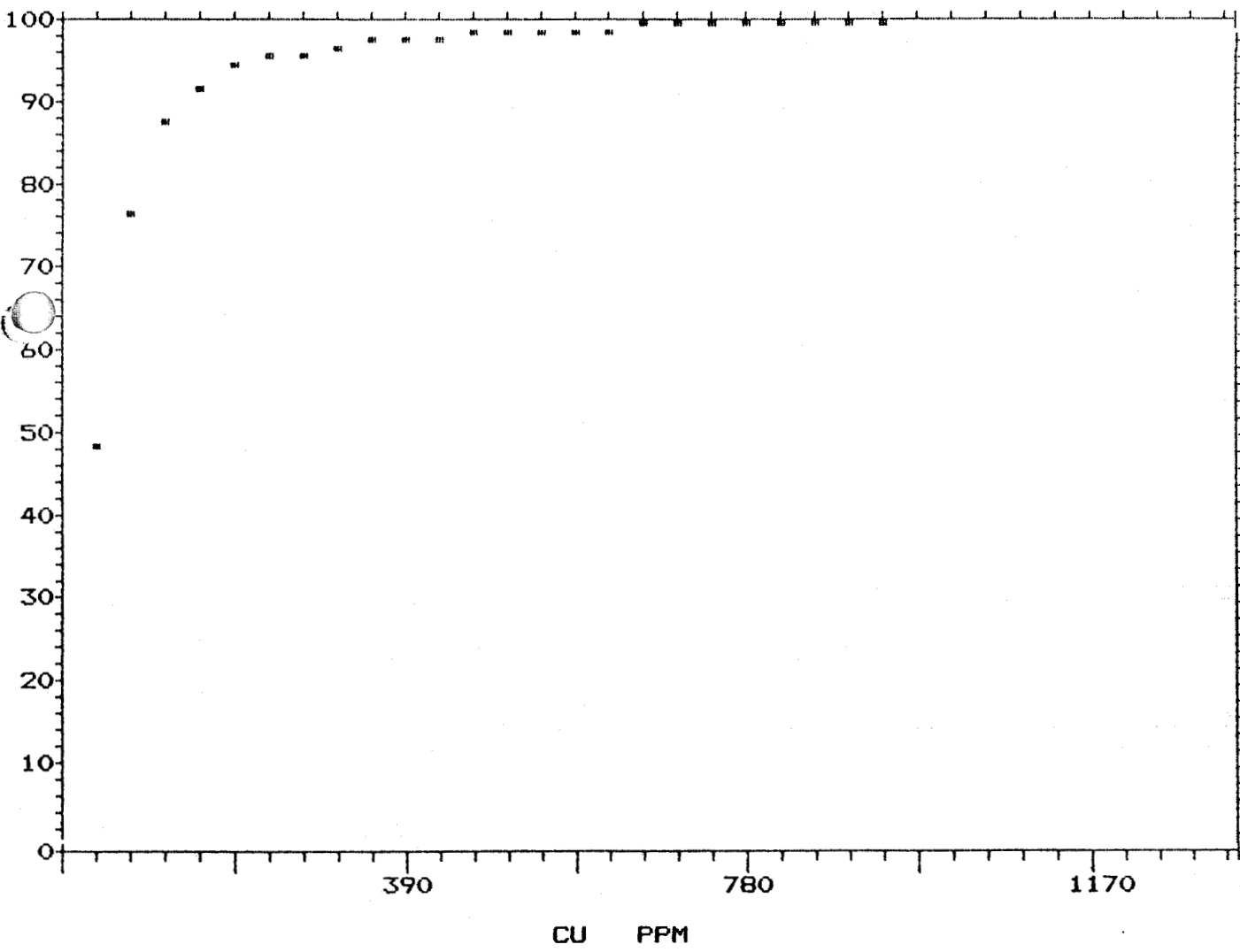


STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.
Element: CU

Project: ERIE CREEK
Date: 88-08-04
Sample Type: Soil

Cumulative Frequency Histogram



OSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
 BURNABY, B.C. V5B 3N1
 TEL : (604) 299 - 6910

STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
 850 W. HASTINGS ST.
 VANCOUVER, B.C.

Project: ERIE CREEK
 Date: 88-08-04

Element: AG Sample Type: Soil

CLASS INTERVAL	CLASS FREQUENCY	RELATIVE FREQUENCY%	CUMULATIVE FREQUENCY%	CLASS MEAN
0.0 - 0.4	117	19.60	19.60	0.31
0.5 - 0.8	229	38.36	57.96	0.65
0.9 - 1.2	114	19.10	77.06	1.03
1.3 - 1.6	57	9.55	86.61	1.41
1.7 - 1.9	26	4.36	90.97	1.78
2.0 - 2.3	21	3.52	94.49	2.13
2.4 - 2.7	12	2.01	96.50	2.56
2.8 - 3.1	6	1.01	97.51	3.02
3.2 - 3.5	4	0.67	98.18	3.22
3.6 - 3.9	2	0.34	98.52	3.75
4.0 - 4.3	1	0.17	98.69	4.30
4.4 - 4.7	1	0.17	98.86	4.50
4.8 - 5.0	0	0.00	98.86	0.00
5.1 - 5.4	0	0.00	98.86	0.00
5.5 - 5.8	1	0.17	99.03	5.80
5.9 - 6.2	0	0.00	99.03	0.00
6.3 - 6.6	1	0.17	99.20	6.50
6.7 - 7.0	0	0.00	99.20	0.00
7.1 - 7.4	1	0.17	99.37	7.20
7.5 - 7.8	0	0.00	99.37	0.00
7.9 - 8.1	1	0.17	99.54	7.90
8.2 - 8.5	1	0.17	99.71	8.40
8.6 - 8.9	1	0.17	99.88	8.90
9.0 - 9.3	1	0.17	100.00	9.30

For Statistics

For All Data

Number of Samples:	597	597
Arithmetic Mean :	1.01	N.A.
Standard Deviation :	.99	N.A.
Minimum Value :	.1	.1
Maximum Value :	9.3	9.3
Range :	0 -- 10000 PPM	.1 -- 9.3 PPM

File(s) used for Statistics:

F2 F3 F4

SSBACHER LABORATORY LTD.

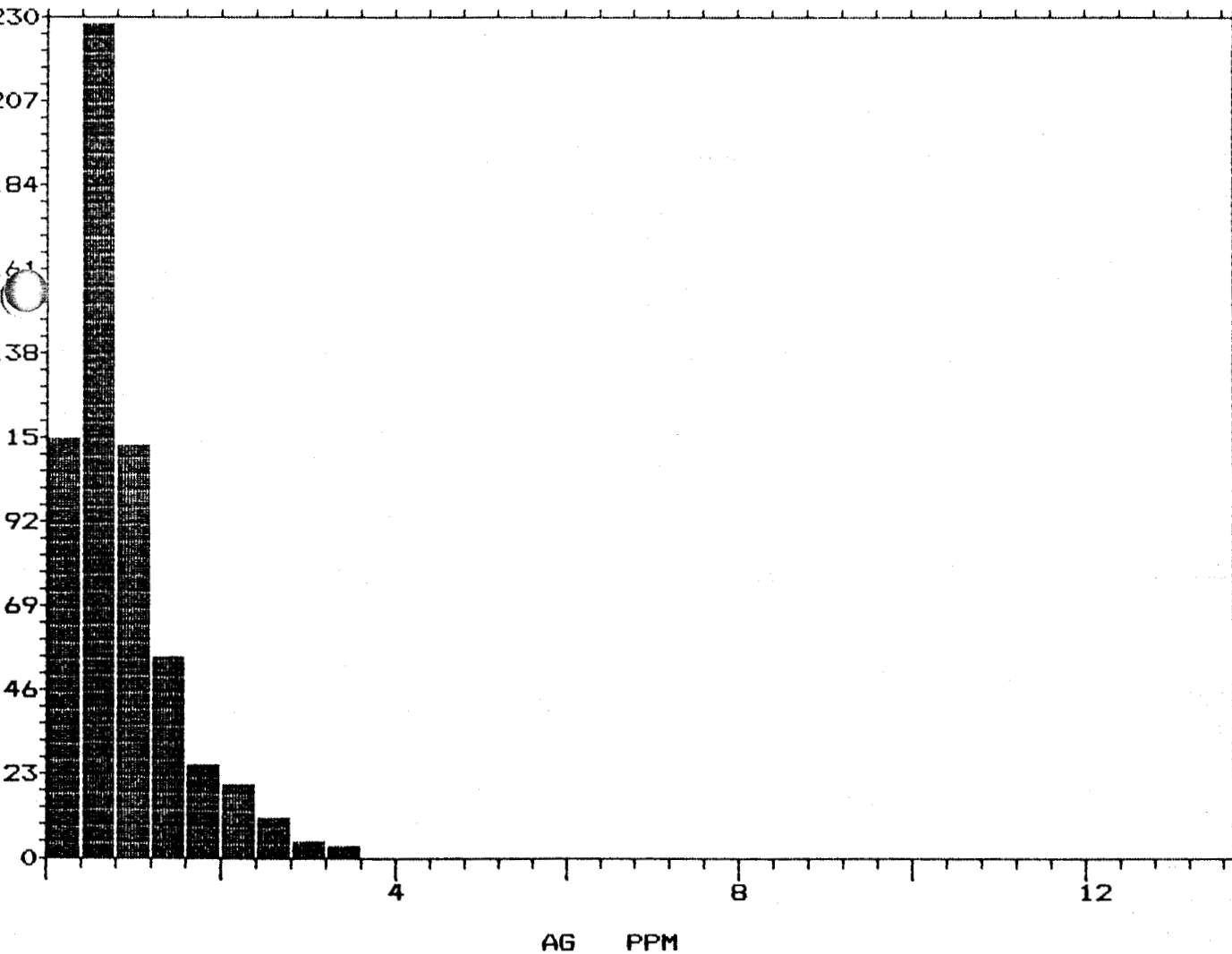
2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.
ement: AG

Project: ERIE CREEK
Date: 88-08-04
Sample Type: Soil

Frequency Histogram



STATISTICAL REPORT

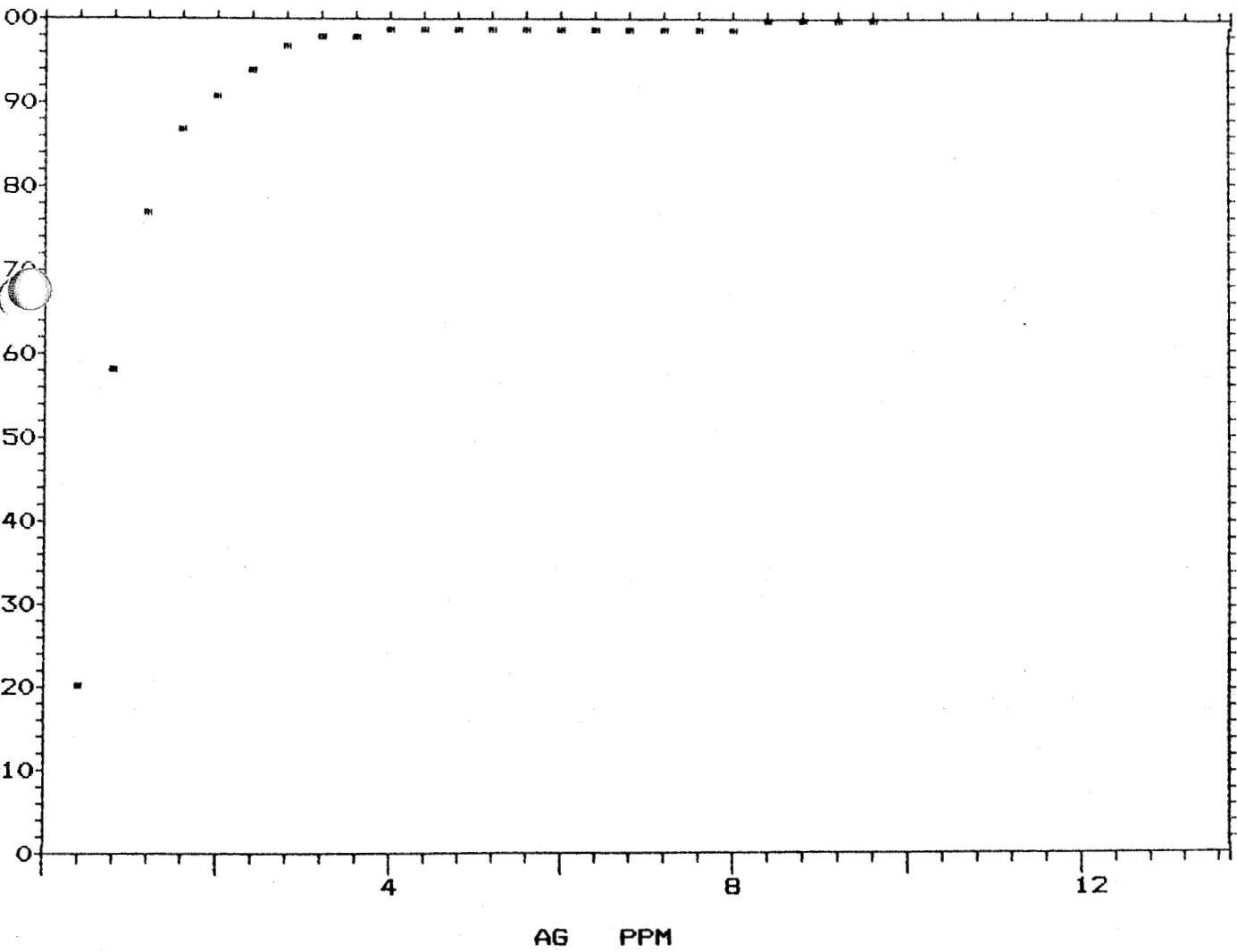
A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.

Project: ERIE CREEK
Date: 88-08-04

ment: AG

Sample Type: Soil

Cumulative Frequency Histogram



ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
 BURNABY, B.C. V5B 3N1
 TEL : (604) 299 - 6910

STATISTICAL REPORT

To: A&M EXPLORATION LTD.
 850 W. HASTINGS ST.
 VANCOUVER, B.C.
 Element: PB

Project: ERIE CREEK
 Date: 88-08-04

Sample Type: Soil

CLASS INTERVAL	CLASS FREQUENCY	RELATIVE FREQUENCY%	CUMULATIVE FREQUENCY%	CLASS MEAN
0 - 84	129	21.61	21.61	45.71
85 - 168	179	29.98	51.59	125.49
169 - 252	154	25.80	77.39	204.35
253 - 336	49	8.21	85.60	296.00
337 - 420	18	3.02	88.62	373.83
421 - 504	26	4.36	92.98	463.46
505 - 588	13	2.18	95.16	533.15
589 - 672	8	1.34	96.50	626.88
673 - 756	7	1.17	97.67	705.29
757 - 840	6	1.01	98.68	808.17
841 - 924	2	0.34	99.02	868.00
925 - 1008	1	0.17	99.19	938.00
1009 - 1092	1	0.17	99.36	1065.00
1093 - 1176	1	0.17	99.53	1100.00
1177 - 1260	0	0.00	99.53	0.00
1261 - 1344	0	0.00	99.53	0.00
1345 - 1428	1	0.17	99.70	1396.00
1429 - 1512	0	0.00	99.70	0.00
1513 - 1596	0	0.00	99.70	0.00
1597 - 1680	0	0.00	99.70	0.00
1681 - 1764	0	0.00	99.70	0.00
1765 - 1848	1	0.17	99.87	1785.00
1849 - 1932	0	0.00	99.87	0.00
1933 - 2016	1	0.17	100.00	2009.00

For Statistics

For All Data

Number of Samples: 597
 Arithmetic Mean : 209.17
 Standard Deviation : 201.62
 Minimum Value : 12
 Maximum Value : 2009
 Range : 0 -- 10000 PPM

597
 N.A.
 N.A.
 .1
 2009
 .1 -- 2009 PPM

File(s) used for Statistics:

1 F2 F3 F4

SSBACHER LABORATORY LTD.

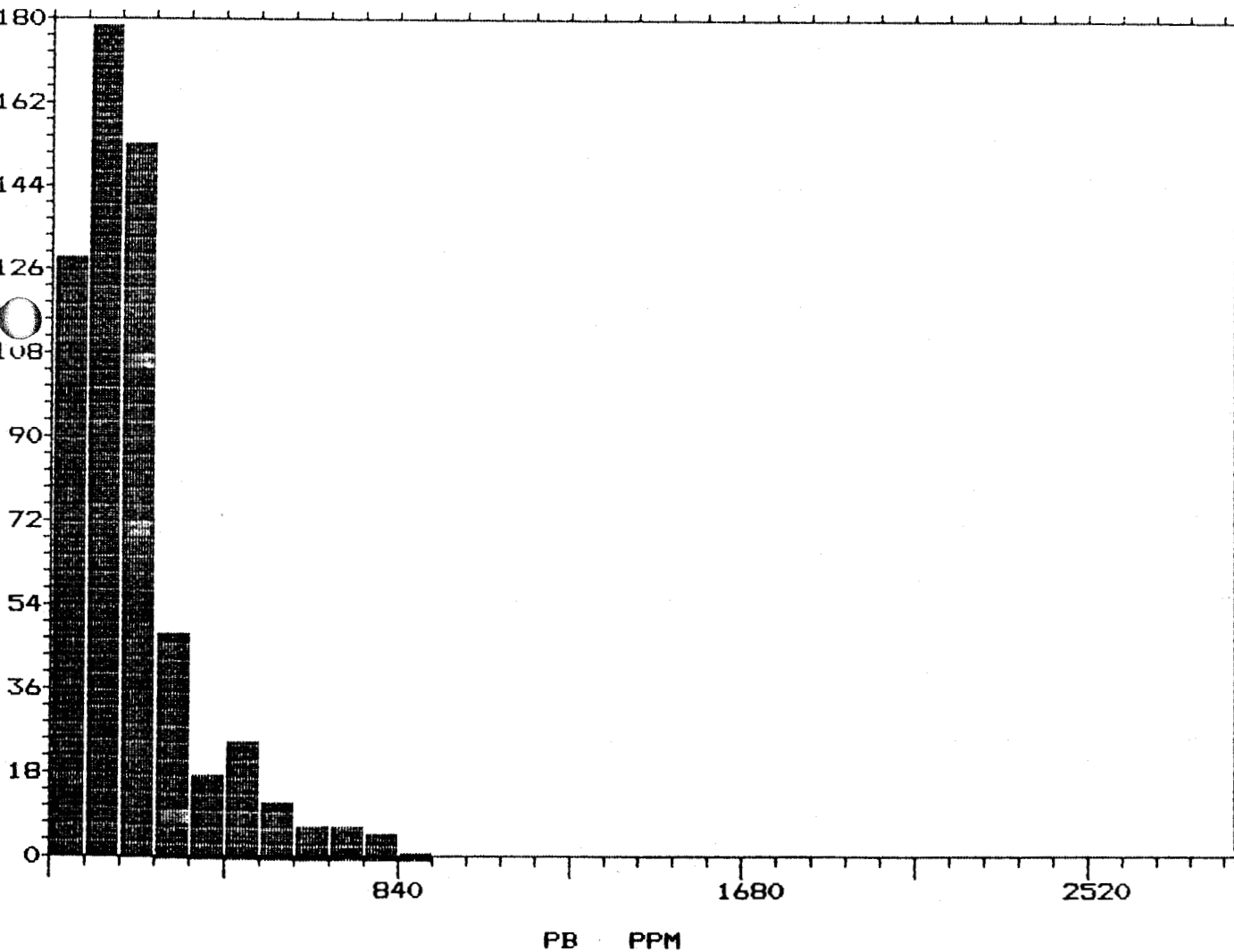
2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.
Element: PB

Project: ERIE CREEK
Date: 88-08-04
Sample Type: Soil

Frequency Histogram



OSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

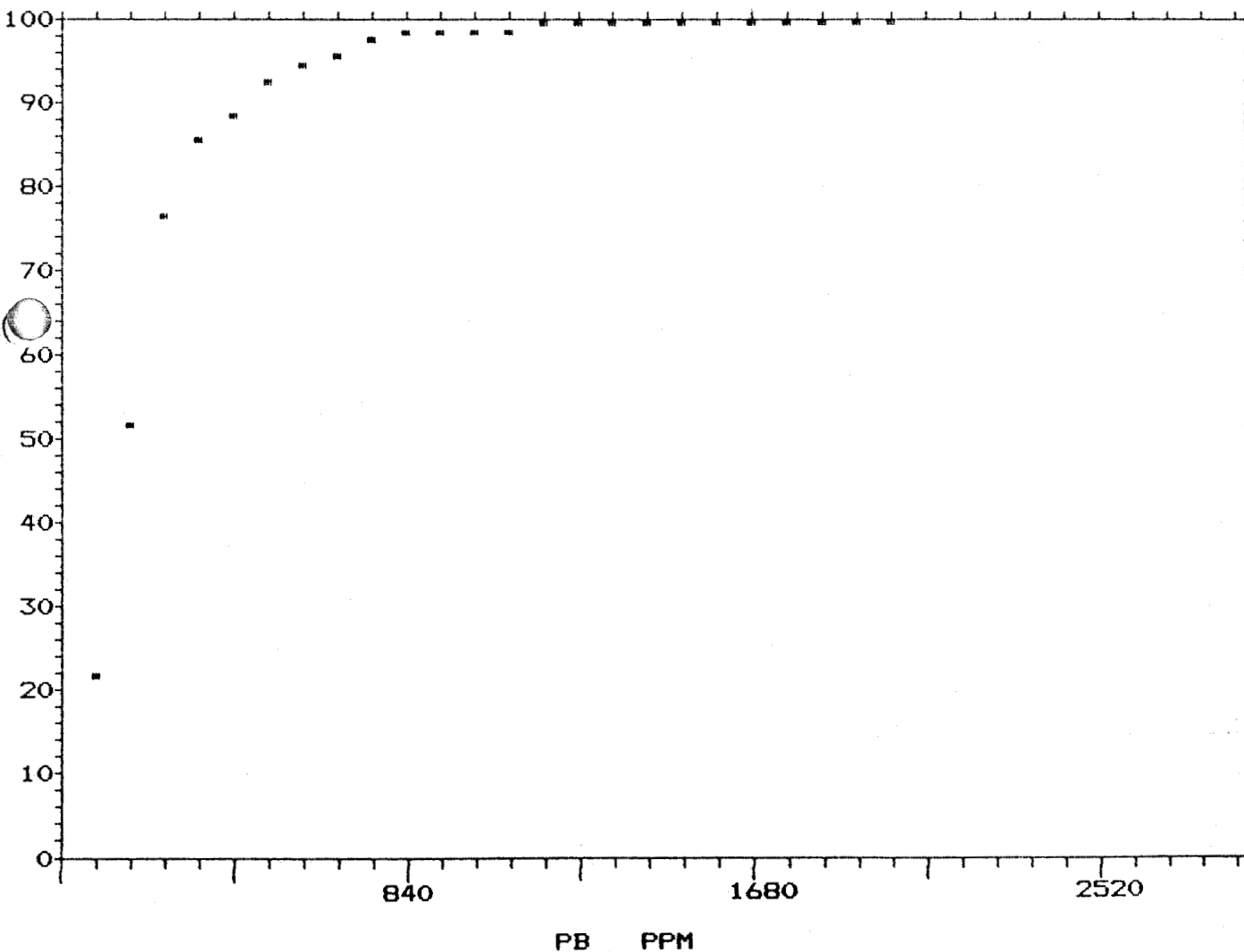
Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.

Project: ERIE CREEK
Date: 88-08-04

Element: FB

Sample Type: Soil

Cumulative Frequency Histogram



ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
 BURNABY, B.C. V5B 3N1
 TEL : (604) 299 - 6910

STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
 850 W. HASTINGS ST.
 VANCOUVER, B.C.

Project: ERIE CREEK
 Date: 88-08-04

Element: ZN

Sample Type: Soil

CLASS INTERVAL	CLASS FREQUENCY	RELATIVE FREQUENCY%	CUMULATIVE FREQUENCY%	CLASS MEAN
0 - 70	7	1.17	1.17	61.14
71 - 140	49	8.21	9.38	109.67
141 - 210	93	15.58	24.96	179.04
211 - 280	97	16.25	41.21	248.14
281 - 350	109	18.26	59.47	312.09
351 - 420	73	12.23	71.70	383.05
421 - 490	44	7.37	79.07	453.75
491 - 560	32	5.36	84.43	523.38
561 - 630	18	3.02	87.45	589.17
631 - 700	18	3.02	90.47	662.94
701 - 770	13	2.18	92.65	732.46
771 - 840	7	1.17	93.82	799.29
841 - 910	11	1.84	95.66	870.09
911 - 980	8	1.34	97.00	946.50
981 - 1050	3	0.50	97.50	1013.67
1051 - 1120	7	1.17	98.67	1069.00
1121 - 1190	4	0.67	99.34	1163.25
1191 - 1260	0	0.00	99.34	0.00
1261 - 1330	2	0.34	99.68	1284.00
1331 - 1400	0	0.00	99.68	0.00
1401 - 1470	0	0.00	99.68	0.00
1471 - 1540	1	0.17	99.85	1506.00
1541 - 1610	0	0.00	99.85	0.00
1611 - 1680	0	0.00	100.00	0.00

For Statistics

For All Data

Number of Samples:	597	597
Arithmetic Mean :	370.1	N.A.
Standard Deviation :	235.91	N.A.
Minimum Value :	39	.1
Maximum Value :	1683	1683
Range :	0 -- 10000 PPM	.1 -- 1683 PPM

File(s) used for Statistics:

1 F2 F3 F4

ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

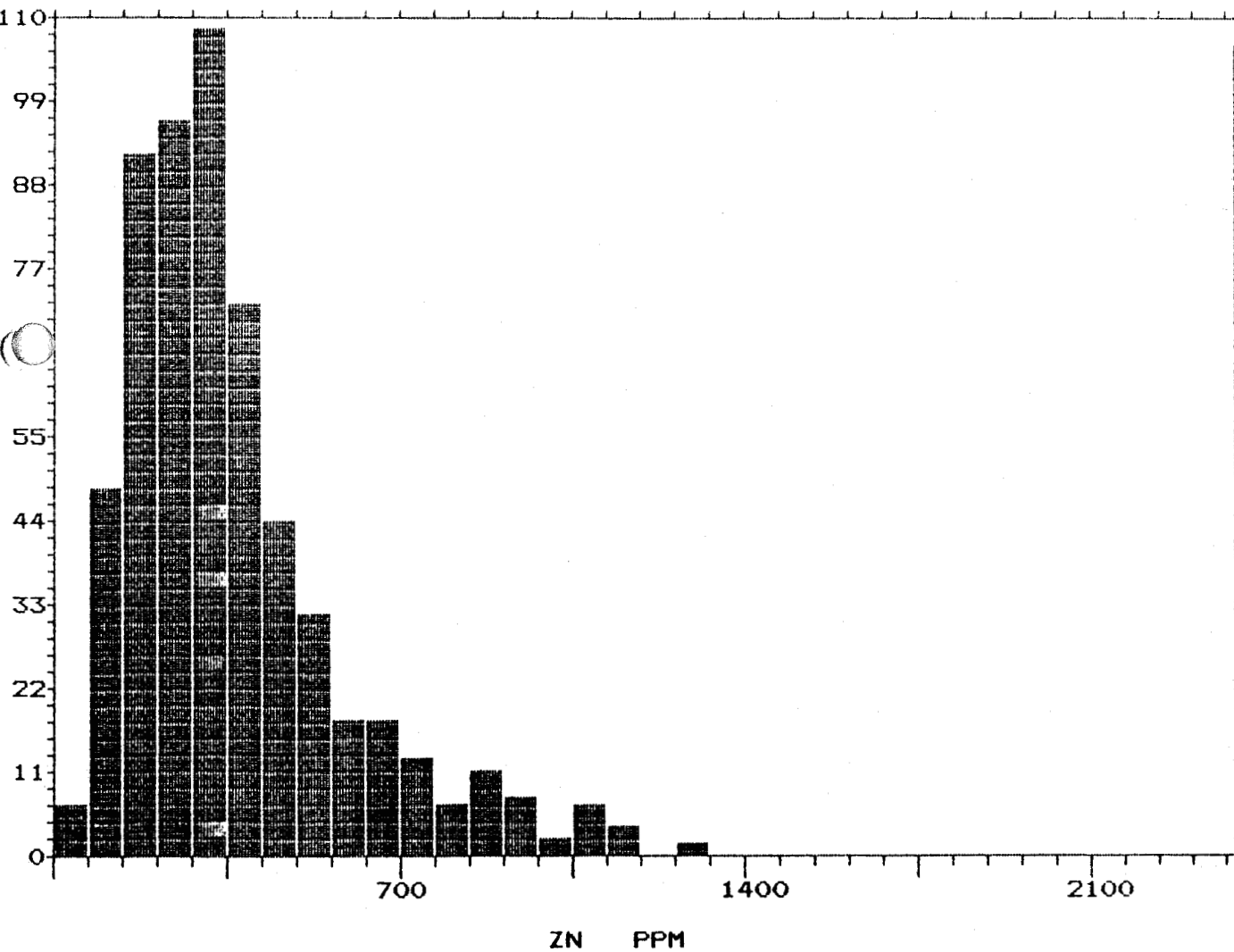
STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.
Element: ZN

Project: ERIE CREEK
Date: 88-08-04
Sample Type: Soil

=====

Frequency Histogram



ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

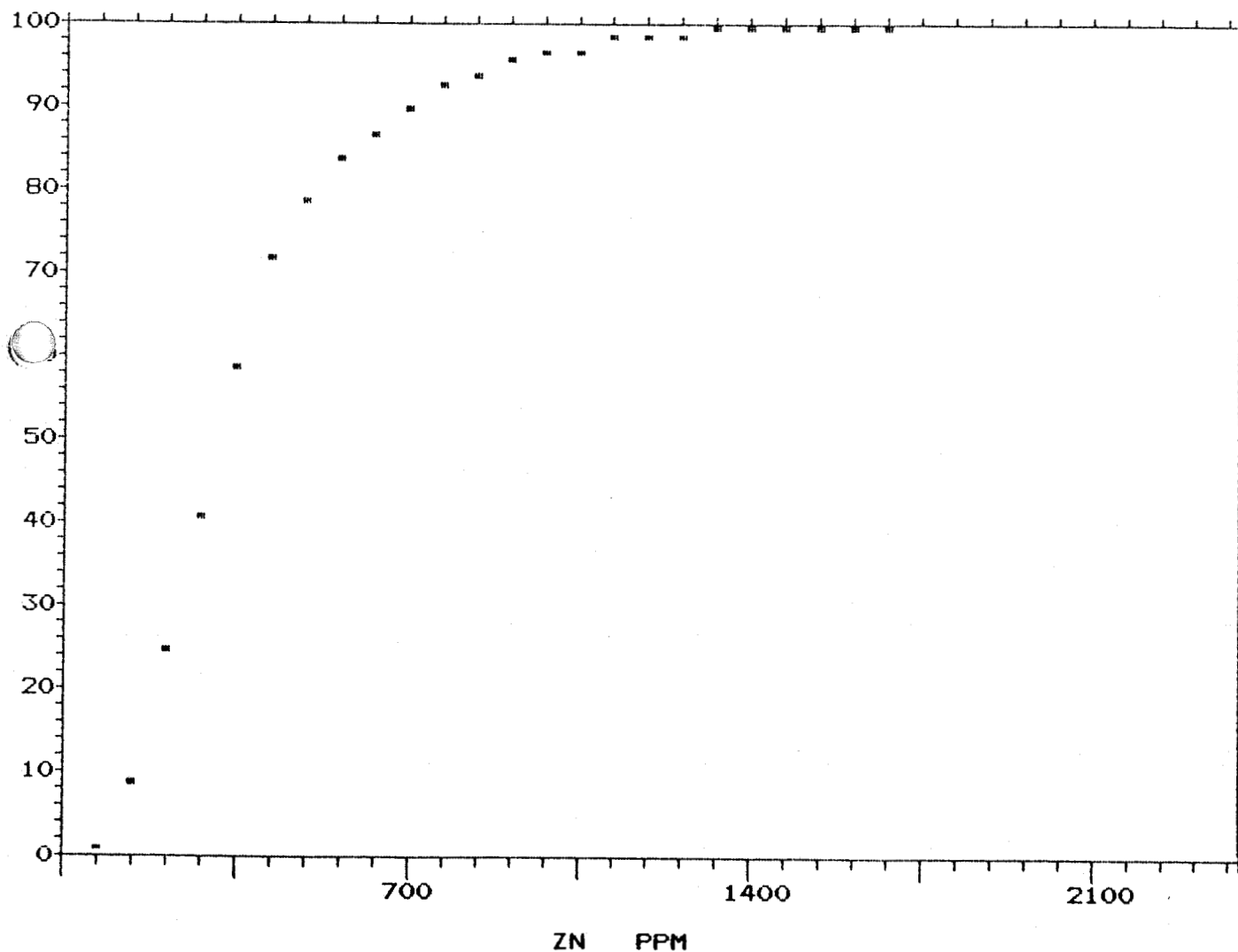
Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.

Project: ERIE CREEK
Date: 88-08-04

Element: ZN

Sample Type: Soil

Cumulative Frequency Histogram



ROSSBACHER LABORATORY LTD.

2225 S. SPRINGER AVENUE
 BURNABY, B.C. V5B 3N1
 TEL : (604) 299 - 6910

STATISTICAL REPORT

To: A&M EXPLORATION LTD.
 850 W. HASTINGS ST.
 VANCOUVER, B.C.

Project: ERIE CREEK
 Date: 88-08-04

Element: AS

Sample Type: Soil

CLASS INTERVAL	CLASS FREQUENCY	RELATIVE FREQUENCY%	CUMULATIVE FREQUENCY%	CLASS MEAN
0 - 16	463	77.55	77.55	9.49
17 - 32	112	18.76	96.31	21.98
33 - 48	13	2.18	98.49	37.15
49 - 64	6	1.01	99.50	57.83
65 - 80	0	0.00	99.50	0.00
81 - 96	1	0.17	99.67	90.00
97 - 112	0	0.00	99.67	0.00
113 - 128	0	0.00	99.67	0.00
129 - 144	0	0.00	99.67	0.00
145 - 160	0	0.00	99.67	0.00
161 - 176	1	0.17	99.84	161.00
177 - 192	0	0.00	99.84	0.00
193 - 208	0	0.00	99.84	0.00
209 - 224	0	0.00	99.84	0.00
225 - 240	0	0.00	99.84	0.00
241 - 256	0	0.00	99.84	0.00
257 - 272	0	0.00	99.84	0.00
273 - 288	0	0.00	99.84	0.00
289 - 304	0	0.00	99.84	0.00
305 - 320	0	0.00	99.84	0.00
321 - 336	0	0.00	99.84	0.00
337 - 352	0	0.00	99.84	0.00
353 - 368	0	0.00	99.84	0.00
369 - 384	0	0.00	100.00	0.00

For Statistics

For All Data

Number of Samples:	597	597
Arithmetic Mean :	13.96	N.A.
Standard Deviation :	19.04	N.A.
Minimum Value :	2	.1
Maximum Value :	395	395
Range :	0 -- 10000 PPM	.1 -- 395 PPM

File(s) used for Statistics:

F1 F2 F3 F4

ROSSBACHER LABORATORY LTD.

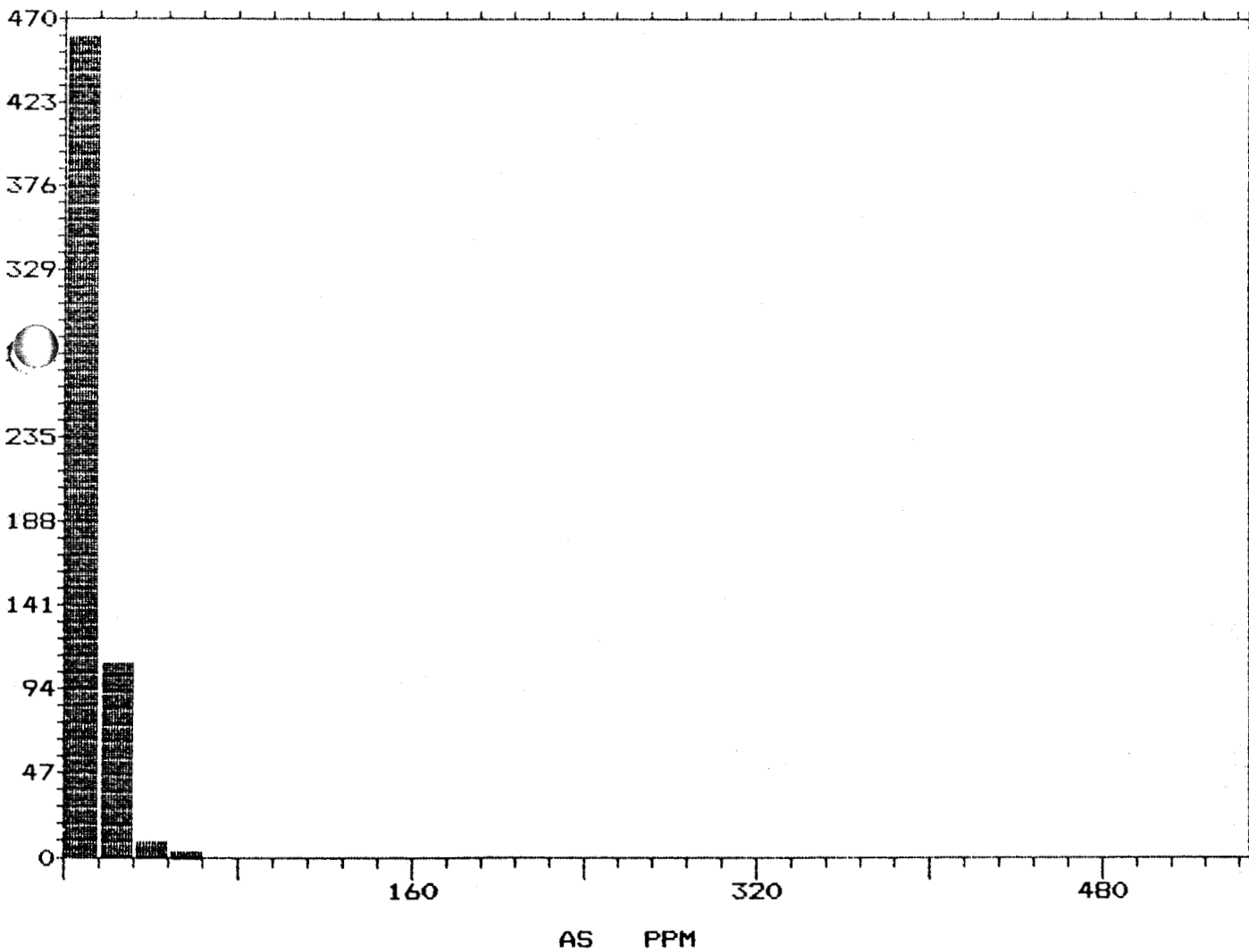
2225 S. SPRINGER AVENUE
BURNABY, B.C. V5B 3N1
TEL : (604) 299 - 6910

STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.
Element: AS

Project: ERIE CREEK
Date: 88-08-04
Sample Type: Soil

Frequency Histogram

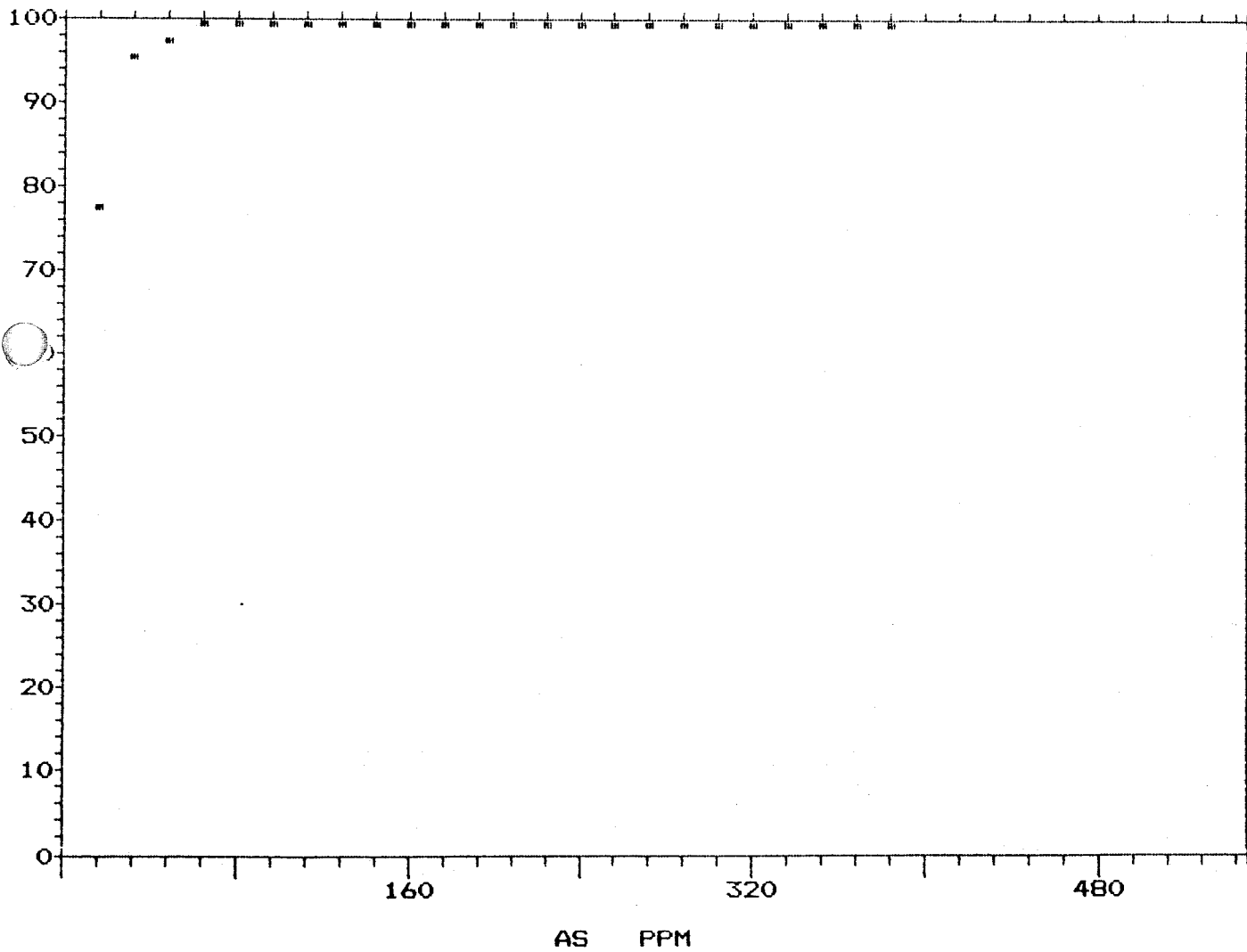


STATISTICAL REPORT

Client: A&M EXPLORATION LTD.
850 W. HASTINGS ST.
VANCOUVER, B.C.
Element: AS

Project: ERIE CREEK
Date: 88-08-04
Sample Type: Soil

Cumulative Frequency Histogram



APPENDIX IV

AFFIDAVIT OF EXPENSES

AFFIDAVIT OF EXPENSES

This will certify that linecutting and geochemical sampling was conducted on the June, Rockford, Ontario, Westminster, St. Louis, Gordon, Goodenough and Monte Carlo claims in the Erie Creek area, Nelson Mining Division, B.C., during the periods of January 15 to August 10, 1988, and September 15 to October 31, 1988. Also included in this work statement are geochemical analyses on samples collected in 1987 and analyzed on December 3, 1987.

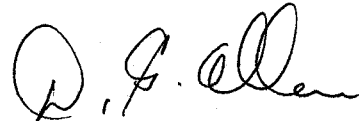
Geochemical analyses and report describing work conducted in 1987.

Salaries	
D. G. Allen	\$ 900.00
Maps, photocopying	155.23
Draughting, computer processing	1,710.00
Typing, compilations	330.00
Geochemical analyses -	
Rossbacher Lab. invoice of December 3, 1987	4,933.80

**Linecutting, collection of approximately 600 soil samples
(not yet analyzed).**

Invoice from Newcastle Exploration	<u>11,495.00</u>
TOTAL	\$19,524.03

Please apply this work as outlined on the November 16, 1988 Statement of Work and place the balance in the PAC account of Kootenay King Resources Ltd.



D. G. Allen,
P. Eng.



Newcastle Explorations Ltd.

619-744 W. HASTINGS STREET, VANCOUVER, B.C. V6C 1A5 CANADA
TELEPHONE: (604) 685-5667

JANUARY 23 1989

TO: KOOTENAY KING RESOURCES INC.

INVOICE #88-28

RE: GEOCHEMICAL & LINECUTTING
SEPT/OCT 1988
ERIE CREEK PROPERTY
SOUTHERN BRITISH COLUMBIA

1. MANPOWER	2 MEN @\$150 da X 22 DAYS	\$6,600.00	
	1 MAN @250 da X 4 DAYS	<u>\$1,000.00</u>	\$7,600.00
2. TRUCK RENTAL	22 DAYS @ \$40 da	\$ 880.00	
	4 DAYS @ \$40 da	\$ 160.00	
	GAS & OIL (RECEIPTS)	<u>\$ 480.00</u>	\$1,520.00
3. FOOD AND ACCOMODATIN	48 MAN DAYS @\$40 da		\$1,920.00
4. EQUIPMENT	TOPO THREAD, FLAGGING, FELT PENS, AXES, POWER SAWS	\$ 455.00	<u>\$ 455.00</u>
	TOTAL		11,495.00
	BALANCE DUE		<u>\$11,495.00</u>