ARIS SUMMARY SHEET

District Geologist, Kamloops — Off Confidential: 90.03.23

ASSESSMENT REPORT 18604 — MINING DIVISION: Kamloops

PROPERTY: Mow
LOCATION: LAT 51 02 00 LONG 120 53 00
UTM 10 5655445 648417
NTS 092P02W
CLAIM(S): Mow
OPERATOR(S): Iron River Res.
AUTHOR(S): Hendrickson, G.A.
REPORT YEAR: 1989, 31 Pages
COMMODITIES
SEARCHED FOR: Copper,Silver,Gold
KEYWORDS: Triassic,Nicola Group,Deadman River Formation,Basalt
WORK
DONE: Geophysical,Physical
IPOL 1.0 km
Map(s) - 1; Scale(s) - 1:2000
ROAD 2.0 km
RELATED
REPORTS: 08342,08430,09136
MINFILE: 092P 156

REPORT

ON THE

INDUCED POLARIZATION SURVEY

MOW #1 MINERAL CLAIM

ARROWSTONE PROJECT

DEADMAN RIVER VALLEY, BRITISH COLUMBIA

KAMLOOPS MINING DIVISION

LAT. 51 02'N, LONG. 120 53'W.

N.T.S. 92P/2W

OWNER: MICHAEL DICKENS
SAVONA, B.C.

OPERATOR: IRON RIVER RESOURCES LIMITED
VANCOUVER, B.C.

BY

GRANT A. HENDRICKSON, P.GEOPH.

TABLE OF CONTENTS

APPENDICES

1. Cost Statement.
2. Qualifications and Certifications.
3. Induced Polarization Data.

MAPS (IN POCKET)

Figure #6: Gradient Array Profiles 1:2000.

INTRODUCTION

This report describes an Induced Polarization survey conducted November 10, 11 and 12, 1988, on 940 meters of line on the MOW 1 claim. The survey was done over a strong VLF electromagnetic anomaly, in combination with a magnetic low found in an earlier survey (see references), in an effort to determine if the anomaly was caused by the presence of sulphides.

The property consists of 72 units in 4 claims located approximately 60 kms northwest of Kamloops, B.C., in the Deadman River Valley. The property is held under option by Iron River Resources Limited of Vancouver from the owner Michael Dickens of Savona, B.C.

Copper mineralization was found in two areas on the property by M. Dickens in 1980, with subsequent exploration being done in 1983 and 1984 by Canamax Resources and Northair Mines Ltd. The recent geophysical surveys were over an area containing angular clasts of chalcocite with good gold and silver values located in the overburden. The work in 1988 has been done in an effort to find the source of the chalcocite mineralization.

LOCATION AND ACCESS

The property is located approximately 60 kms northwest of Kamloops, B.C., in the Mowich Lake area of the Deadman River Valley. Access is by 29 kms of paved and gravel road from the Trans-Canada Highway at a point 5 kms west of the village of Savona.

TOPOGRAPHY AND CLIMATE

The Deadman River Valley is relatively narrow with moderately steep sides. Topography on the claims is moderate to rugged with elevations ranging from 650m to 1200m.

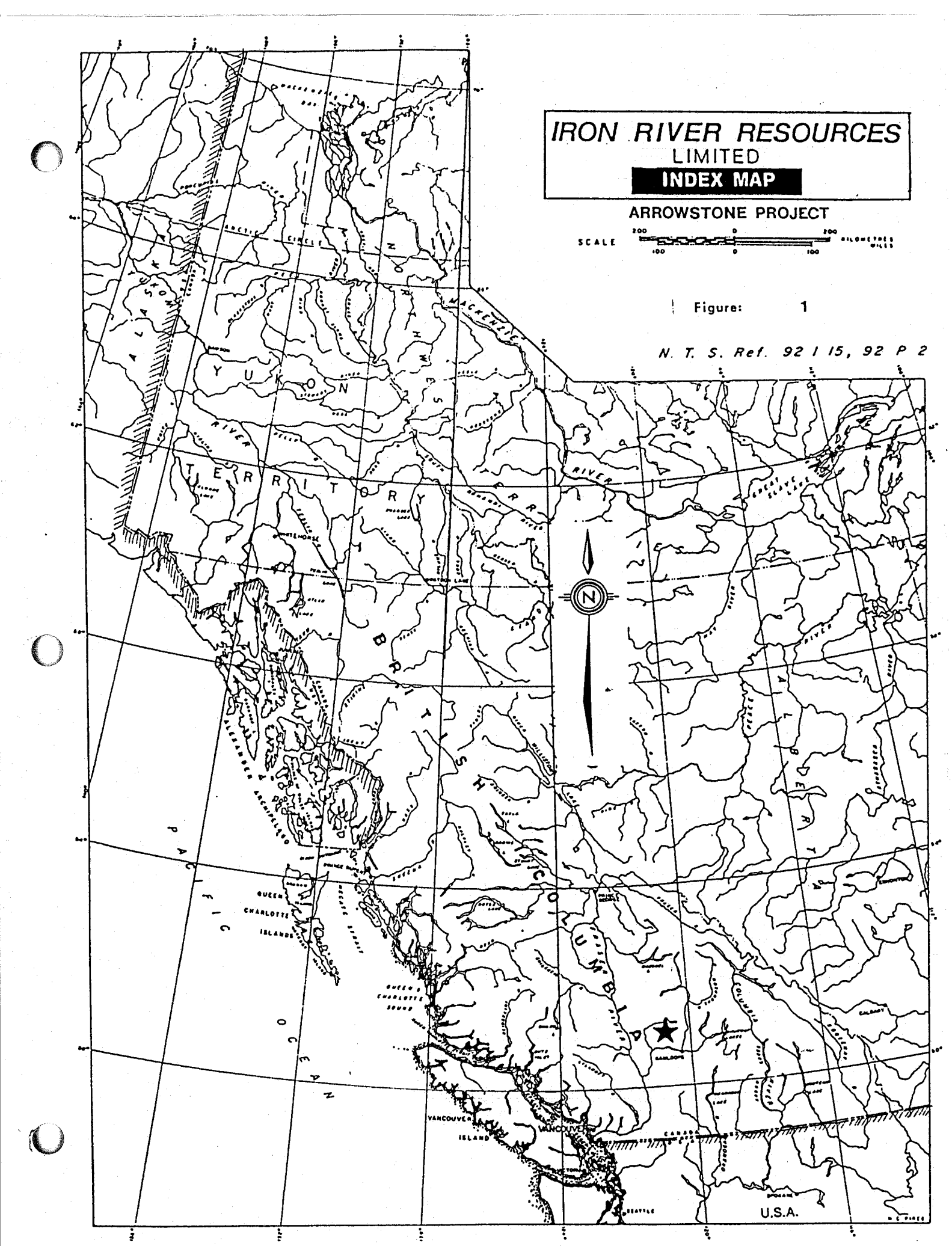
Outcrop is best along cliffs, creeks and road cuts and relatively poor elsewhere. There are very few exposures in the area of the present program.

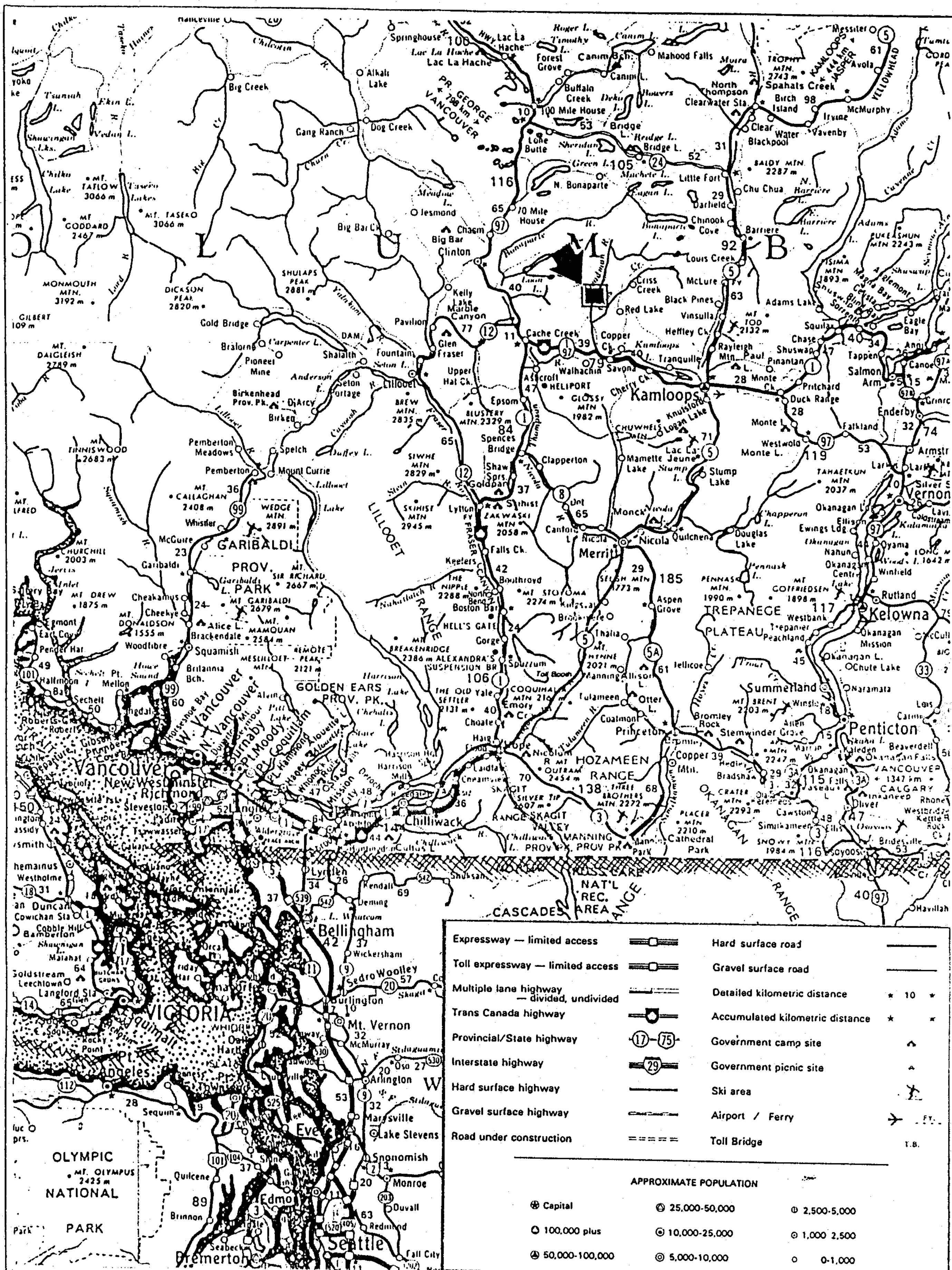
The claims are forested mainly by Lodgepole Pine, with generally light underbrush.

The climate is typical of the interior plateau, with warm summers and cold winters. Snow free conditions usually exist from April to mid-November.

HISTORY

The area has seen sporadic activity since the late 1870's, with the earliest reference in the Index to Annual Reports of the Minister of Mines being 1879. The only major producer in the immediate area was the Vidette Mine located 14 kms north of Mowich Lake. During the 1930's, 54190 tons grading 0.55oz/ton gold, 0.86oz/ton silver and 0.09% copper were produced from narrow quartz veins.


IRON RIVER RESOURCES
LIMITED
INDEX MAP
ARROWSTONE PROJECT
SCALE
200 0 200 KILOMETRES
100 0 100 MILES
Figure: 1
N. T. S. Ref. 92 I 15, 92 P 2
ALASKA
YUKON TERRITORY
NORTHWEST TERRITORIES
ARCTIC CIRCLE
MACKENZIE RIVER
PEACE RIVER
ALBERTA
BRITISH COLUMBIA
PACIFIC OCEAN
QUEEN CHARLOTTE ISLANDS
VANCOUVER ISLAND
VANCOUVER
U.S.A.



Drawn By:	D.P.B.	
Checked By:	J.F.B.	
Date:	Ap / 198	

IRON RIVER RESOURCES
LIMITED
LOCATION MAP

0 50 100
kilometres

Figure: 2

James F. Bristow P. Eng.

Recent history of the property is as follows:

1980 - Prospecting and soil sampling by M. Dickens.

1983 - Preliminary evaluation report by N.L. Tribe.

1983 - Prospecting, soil sampling, magnetometer and I.P. surveys by Canamax Resources.

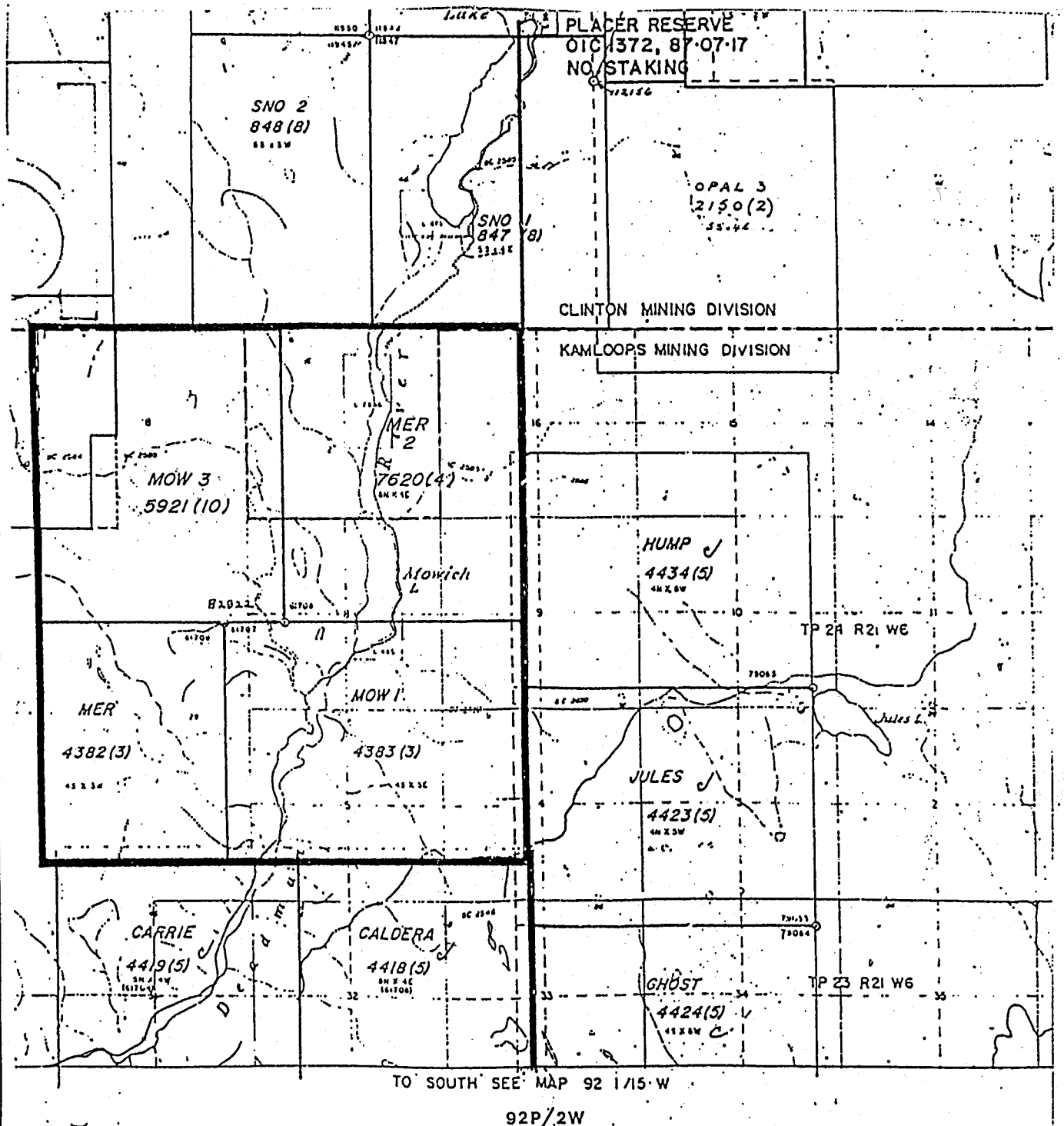
1984 - Road building and trenching by Northair Mines Ltd.

1988 - Property optioned to Iron River Resources Limited. Electromagnetic and Magnetometer Surveys.

CLAIMS (See Figure #3)

The property consists of four contiguous metric claims totalling 72 units.

Claim Name	Units	Record Date	Record No.	Expiry Date
MOW 1	20	23/3/83	4383	23/3/89
MOW 3	20	25/10/84	5921	25/10/89
MER	12	23/3/83	4382	23/3/89
MER 2	20	27/4/88	7620	27/4/89



DEPARTMENT OF MINES AND PETROLEUM RESOURCES

VICTORIA B.C.

SCALE 1/2 MILE = 1 INCH

Miles 1 .5 0 1 2 Miles

Metres 1000 500 0 1000 2000 3000 Metres

Kilometres .5 0 1 2 3 Kilometres

Drawn By: D.P.B.	IRON RIVER RESOURCES LIMITED	Scale:	1:50,000
Checked By: J.F.B.		Figure:	3
Date: JUNE 1988	CLAIM MAP	James F. Bristow P. Eng.	

GEOLOGY

REGIONAL GEOLOGY (Figure #4)

The Mowich Lake property is located in the southern segment of the geological zone known as the Quesnel Trough; a northerly trending belt, up to 45 kms wide, of Upper Triassic age Nicola Group volcanic and sedimentary rocks.

The Quesnel Trough units lie between Permian and older volcanics and sediments to the east, and Permian Cache Creek limestones to the west. The Nicola Group has been intruded by Triassic/Jurassic age intrusives of the Thuya and Takomkane batholiths and younger Cretaceous alkaline to calc-alkaline stocks.

The region is covered by a thin layer of Miocene siliceous ashes and tuffs (Deadman River Formation) and by Eocene plateau basalt.

LOCAL GEOLOGY

The Nicola rocks underlying the Mowich property have been partially exposed by erosion of the plateau basalt and Deadman River Formation along the Deadman River Valley. This recent erosional window traverses the centre of the property in a North-South direction exposing a section of Nicola Group rocks between the younger formations along the properties East and West margins.

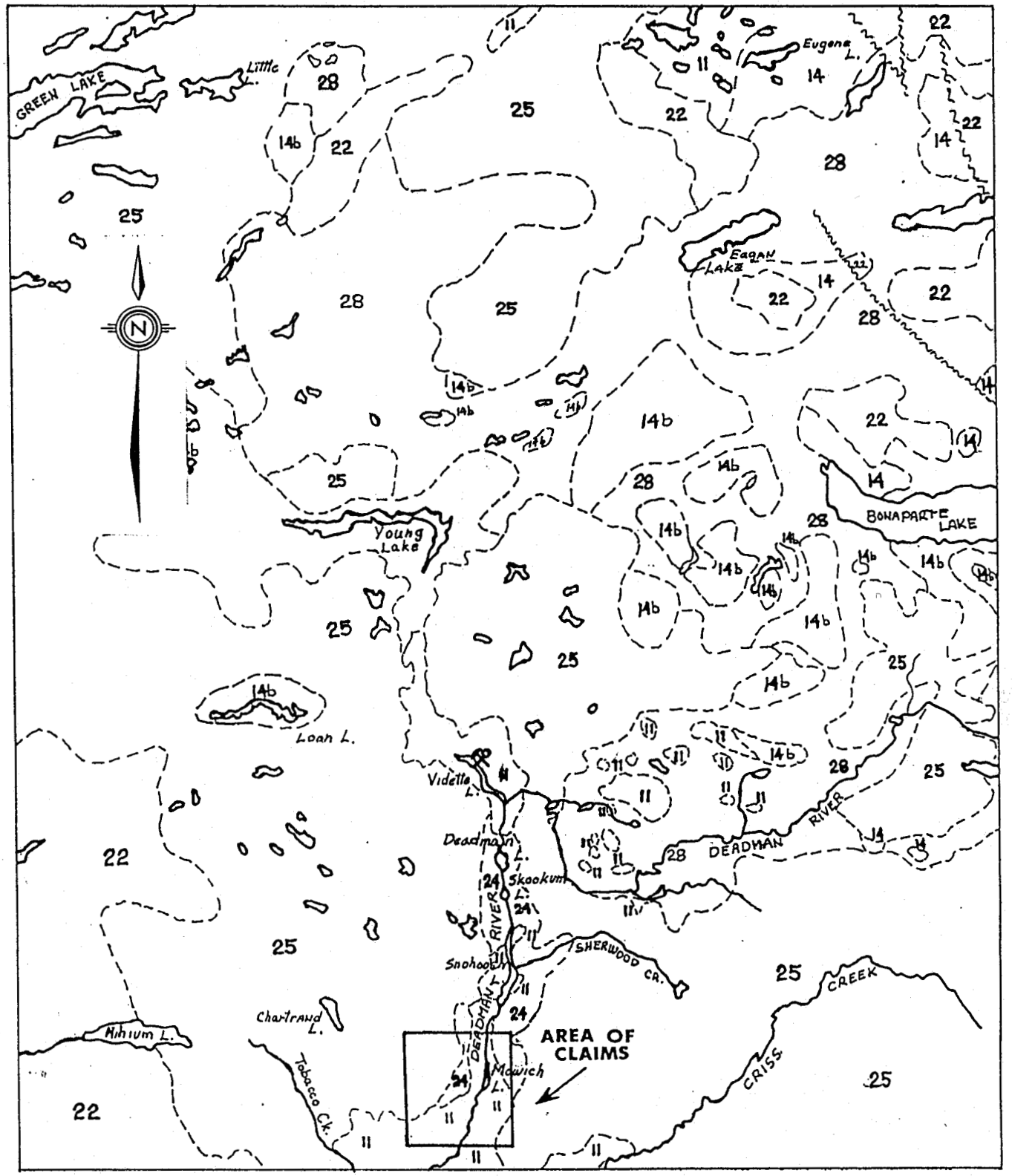
A brief description of the rock types (after Canamax Resources 1984) exposed in the immediate area of the claims is as follows:

NICOLA GROUP SEDIMENTS

(a) Argillite - generally massive to poorly bedded with occasional thin bedded siltstones.

(b) Greywacke - interbedded with argillites and composed of subangular grains less than 1mm and black to grey in colour depending on the quartz and feldspar content.

(c) Limestone, Chert, Quartzite and Conglomerate - occur in minor amounts with argillite and greywacke.



AFTER GSC MAP 1278 A

Drawn By: D.P.B.	IRON RIVER RESOURCES LIMITED	Scale: 1:250 000
Checked By: J.F.B.	GEOLOGY	Figure: 4
Date: June / 1988	James F. Bristow P. Eng.	

NICOLA GROUP VOLCANICS

(a) Polymictic Breccia - a distinctive maroon to green colour, composed of Fragments to 0.5 metres of sediments, syenodiorites, volcanic andesites and augite porphyry in an andesite groundmass. Hematite and epidote alteration is common.

(b) Andesite Breccia - occurs only along the east side of Mowich Lake and consists of rounded to angular clasts to 20cm of fine grained, light green andesite and augite porphyry with minor limestone. The groundmass is tuffaceous andesite and carbonate.

(c) Augite Porphyry - appears to be a flow rock forming the top of the Nicola Formation. It is massive, dark grey green, aphanitic groundmass with up to 8% phenocrysts of augite crystals to 5mm. It can contain up to 10% amygdaloidal material in brecciated areas.

INTRUSIVE ROCKS

The intrusive outcrops mapped by Canamax Resources all occur to the west of the Deadman River. They are reportedly diorite and syenite in composition with a maximum indicated surface exposure size of 300 metres.

TERTIARY ROCKS

(a) Deadman River Formation - this formation unconformably overlies the Nicola Group Rocks. It is composed of Miocene age non-marine tuffs, ashes and arkoses with minor conglomerates and agglomerates. The arkose unit is poorly consolidated and believed to be quite thin. The tuff is white to yellow in colour, fine grained and in at least one area 30 metres thick.

(b) Plateau Basalt - probably of Eocene age, dark grey to brown in colour and often vesicular.

STRUCTURES

The Nicola Group rocks strike northerly with moderate to steep dips to the east and west. Mapping to date suggests there is no repetition due to folding. The Deadman River Valley is believed to be underlain by a major fault with possible left lateral movement in the order of 600 metres. Several apparent northwest-southeast faults have been recognized with some suggestion of accompanying block faulting.

Quartz-carbonate veining in the Nicola and Deadman River formations indicate a hydrothermal system was operating in the post-Tertiary period. Serpentinite, ankerite and mariposite alteration found on the property are further evidence of the presence of a deep seated "plumbing" system.

MINERALIZATION

Mineralization is known at two areas on the property, but for the purposes of this report the area of interest is located 350 meters southeast of the south end of Mowich Lake and 85 meters southeast of the bridge over the Deadman River. A pit in the overburden near the top of the west bank of the Deadman River has exposed angular to subangular fragments of malachite coated chalcocite to 6 cms in diameter. Some of the chalcocite clasts are associated with serpentine and most of the rock fragments composing the overburden are sheared and serpentinized volcanic; possibly augite porphyry. Smaller fragments of similar mineralization were found in the road cut approximately 20 meters to the northwest.

Five samples of selected mineralized fragments averaged 58% copper, 8.47 oz/t. silver and 0.25 oz/t. gold.

EXPLORATION PROGRAM

This limited Induced Polarization survey was conducted to test the previously discovered VLF-EM and magnetic anomaly for sulphide content. The survey consisted of four short lines covering the locations at which the anomalous condition was detected. The total line distance surveyed was 940 meters.

The gradient array Induced Polarization technique was utilized for this survey. Current electrode separation was 500 meters. Potential electrode separation was 20 meters. Measurements were taken every 10 meters along the survey lines.

The gradient array technique is a cost effective method for examining large blocks of ground with excellent horizontal resolution.

With the spacings used on this survey, the depth of investigation is confined to the first 100 meters, with the array focused at the 50 meter depth.

The pulse duration of the I.P. transmitter was 2 seconds. The I.P. receiver analysed the decay curve through four windows of 120, 220, 420 and 820 millseconds width respectively. The delay time prior to the start of an I.P. measurement was 160 millseconds. The 3rd window (width 420 ms) is the data displayed in the accompanying map. Data is displayed in stacked profile form to facilitate viewing the relative differences in response along the lines. The raw I.P. data (computer listing) is appended to the back of this report.

GEOPHYSICAL EQUIPMENT

1 - BRGM I.P-2 Induced Polarization Receiver (time domain).
1 - Huntec 2.5kva I.P. Transmitter and Motor Generator.
3 - King VHF Portable Radios.
1 - Toshiba 3100 Field Computer.
1 - Hewlett Packard Quietjet Printer.

PERSONNEL (DELTA GEOSCIENCE LTD)

Grant Hendrickson - Supervisor/Senior Geophysicist
Rick Ofner - Junior Geophysicist/Crew Chief
Greg Martin - Technician.
Michael Dickens - Helper - Savona, B.C.

SURVEY RESULTS

A perusal of the data suggests that the VLF response is most likely due to a geological contact between rock types that have a good resistivity contrast. This contact zone trends E-W, with the rocks to the north being much more resistive (higher resistivity).

Typical resistivities for various rock types are:

Intrusives	- greater than 2000 ohm-m.
Volcanic flows	- greater than 3000 ohm-m.
Tuffs	- approx. 1000 ohm-m.
Greywacke	- approx. 400 ohm-m.
Sandstones	- approx. 200 ohm-m.
Shales	- less than 100 ohm-m.
Overburden (Sandy Clay)	- approx. 50 ohm-m.

In conjunction with the noted resistivity contrast, the rocks to the north have a higher chargeability (sulphide?) background, perhaps 2 to 3% more sulphide.

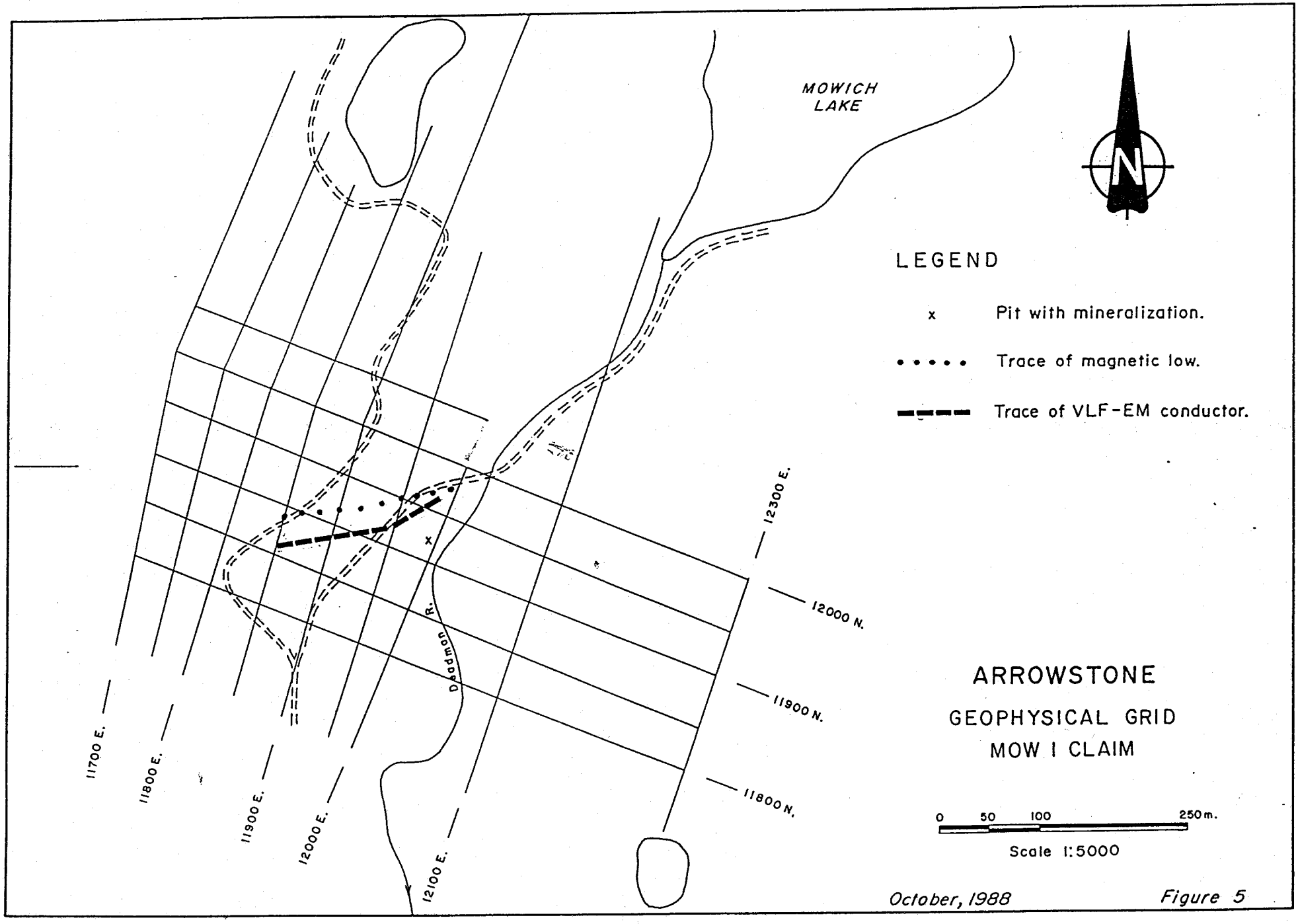
The uniform or gradual increase in chargeability and resistivity as you move north along the lines, is consistent with a buried geological contact. To the northeast corner of the I.P. grid, the changes in resistivity and chargeability are much more abrupt, which is interesting. These abrupt changes may be due to there being much less overburden and/or thin sulphide rich zones with accompanying silicification. Graphite can cause higher chargeability readings, however these are normally accompanied by much lower resistivity values.

In any event, the sulphide content of the bedrock is likely higher in the northeast corner of the grid. thus this area could be the source of the sulphide float. More I.P. work would be required to fully evaluate this area, however this recommendation should be preceded by detailed surface prospecting of the area in question.

Respectfully Submitted,

G. Hendrickson

Grant A. Hendrickson, P.Geoph.


MOWICH LAKE
N
LEGEND
x Pit with mineralization.
Trace of magnetic low.
Trace of VLF-EM conductor.
11700 E.
11800 E.
11900 E.
12000 E.
12100 E.
12300 E.
12000 N.
11900 N.
11800 N.
Deadman R.
ARROWSTONE
GEOPHYSICAL GRID
MOW I CLAIM
0 50 100 250 m.
Scale 1:5000
October, 1988
Figure 5

REFERENCES

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(II) 1984, pp. 256 Exploration in British Columbia

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10. Karous, M., and Hjelt, S.E., 1983: Linear Filtering of V.L.F. Dip-Angle Measurements: Geophysical Prospecting.

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12. Coggon, J.H., 1973: A Comparison of I.P. Electrode Arrays: Geophysics, Vol.38, 737-761,

COST STATEMENT

1.	I.P. Survey - Delta Geoscience Ltd.....	$ 2,178.00.
2.	Report Draft.....	$ 1,000.00.
3.	Drafting, Printing etc.....	$ 125.00.
		$ 3,303.00.

DELTA GEOSCIENCE LTD.
Mineral Exploration Geophysics
Consulting and Contracting

642 English Bluff Rd.
Delta, B.C. V4M 2N4
Tel: (604) 943 0983

November 13, 1988.

Inv. C.066.

INVOICE

Iron River Resources Ltd.,
Suite 600,
890 West Pender Street,
Vancouver, B.C.,
V6C 1J9.

Attn: Mr. Dan Berkshire.

Re: Geophysical Survey -
Arrowstone Project, Savona, B.C.

1 day @ $1050.00/day (I.P work).....	$ 1,050.00.
Mob/Demob Charges.....	$ 900.00.
Board: 2 men x $20.00/day each x 3 days..	$ 120.00.
Motel	$ 108.00.
	$ 2,178.00.

NOV 14/88
C.066

STATEMENT OF QUALIFICATION

Grant A. Hendrickson

- B.Science, U.B.C. 1971, Geophysics option.
- For the past 18 years, I have been actively involved in mineral exploration projects throughout Canada and the United States.
- I am a registered Professional Geophysicist with the Association of Professional Engineers, Geologists and Geophysicists of Alberta.
- I am an active member of the S.E.G., E.A.E.G., and B.C.G.S.

Dated at Delta, British Columbia, this 20th day of February, 1989.

G. Hendrickson

Grant A. Hendrickson, P.Geoph.

MOWNOS11.IP

IP - 2 V2.1 PRINTER Utility

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RECALL 19        RECTGL
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RECALL 19 RECTGL
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RECALL 28 RECTGL
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X= 100.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

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RECALL 32 RECTGL
SP=-25 RO= 283.2
M= 14 VP= 77.1 E= 0 I= 2100.0 TIME=2000
M1= 29 M2= 22 M3= 15 M4= 10
X= 70.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 33 RECTGL
SP=-15 RO= 285.0
M= 14 VP= 72.8 E= 0 I= 2100.0 TIME=2000
M1= 28 M2= 21 M3= 15 M4= 9
X= 60.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 34 RECTGL
SP= 4 RO= 252.5
M= 13 VP= 61.1 E= 0 I= 2100.0 TIME=2000
M1= 27 M2= 21 M3= 14 M4= 9
X= 50.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 35 RECTGL
SP=-5 RO= 146.7
M= 11 VP= 34.0 E= 0 I= 2100.0 TIME=2000
M1= 23 M2= 17 M3= 12 M4= 7
X= 40.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 36 RECTGL
SP=-9 RO= 95.8
M= 9 VP= 21.4 E= 0 I= 2100.0 TIME=2000
M1= 20 M2= 15 M3= 10 M4= 6
X= 30.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 37 RECTGL

RECALL 37 RECTGL
SP=-13 RO= 77.6
M= 8 VP= 16.9 E= 0 I= 2100.0 TIME=2000
M1= 17 M2= 13 M3= 9 M4= 5
X= 20.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 38 RECTGL
SP=-4 RO= 60.2
M= 8 VP= 13.0 E= 0 I= 2100.0 TIME=2000
M1= 16 M2= 12 M3= 8 M4= 5
X= 10.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 39 RECTGL
SP=-3 RO= 58.5
M= 6 VP= 12.5 E= 0 I= 2100.0 TIME=2000
M1= 15 M2= 11 M3= 7 M4= 3
X= 0.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 40 RECTGL
SP=-6 RO= 50.6
M= 6 VP= 10.9 E= 0 I= 2100.0 TIME=2000
M1= 13 M2= 10 M3= 7 M4= 4
X=-10.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 41 RECTGL
SP=-11 RO= 53.3
M= 5 VP= 11.7 E= 0 I= 2100.0 TIME=2000
M1= 13 M2= 9 M3= 6 M4= 2
X=-20.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 42 RECTGL
SP=-9 RO= 74.2
M= 6 VP= 16.6 E= 0 I= 2100.0 TIME=2000
M1= 13 M2= 9 M3= 6 M4= 4
X=-30.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 43 RECTGL
SP=-14 RO= 84.0
M= 5 VP= 19.4 E= 0 I= 2100.0 TIME=2000
M1= 12 M2= 9 M3= 6 M4= 3
X=-40.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 44 RECTGL
SP=-18 RO= 83.9
M= 5 VP= 20.3 E= 0 I= 2100.0 TIME=2000
M1= 12 M2= 8 M3= 5 M4= 3
X=-50.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 45 RECTGL
SP=-10 RO= 93.6
M= 5 VP= 23.9 E= 0 I= 2100.0 TIME=2000
M1= 12 M2= 8 M3= 5 M4= 3
X=-60.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 46 RECTGL

RECALL 46 RECTGL
SP=-8 RO= 81.4
M= 5 VP= 22.2 E= 0 I= 2100.0 TIME=2000
M1= 11 M2= 8 M3= 5 M4= 3
X=-70.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 47 RECTGL
SP=-5 RO= 66.8
M= 5 VP= 19.6 E= 0 I= 2100.0 TIME=2000
M1= 12 M2= 9 M3= 6 M4= 3
X=-80.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 48 RECTGL
SP=-5 RO= 60.6
M= 5 VP= 19.4 E= 0 I= 2100.0 TIME=2000
M1= 11 M2= 8 M3= 5 M4= 3
X=-90.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 49 RECTGL
SP=-8 RO= 65.5
M= 3 VP= 23.1 E= 0 I= 2100.0 TIME=2000
M1= 8 M2= 6 M3= 4 M4= 2
X=-100.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 50 RECTGL
SP=-21 RO= 95.5
M= 3 VP= 37.7 E= 0 I= 2100.0 TIME=2000
M1= 7 M2= 5 M3= 3 M4= 2
X=-110.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 51 RECTGL
SP=-14 RO= 96.5
M= 3 VP= 43.1 E= 0 I= 2100.0 TIME=2000
M1= 7 M2= 5 M3= 3 M4= 2
X=-120.0 Y= 0.0 MN/2= 10.0 AB/2= 250.0

RECALL 52 RECTGL
SP=-7 RO= 75.3
M= 3 VP= 31.3 E= 0 I= 2100.0 TIME=2000
M1= 6 M2= 4 M3= 2 M4= 2
X=-120.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 53 RECTGL
SP=-15 RO= 47.9
M= 3 VP= 17.8 E= 0 I= 2100.0 TIME=2000
M1= 7 M2= 5 M3= 3 M4= 2
X=-110.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 54 RECTGL
SP=-14 RO= 32.2
M= 3 VP= 10.8 E= 0 I= 2100.0 TIME=2000
M1= 8 M2= 5 M3= 3 M4= 2
X=-100.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 55 RECTGL
SP=-17 RO= 54.5

RECALL 55	RECTGL				
SP=-17	RO= 54.5				
M= 3	VP= 16.7	E= 0		I= 2100.0	TIME=2000
M1= 8	M2= 6	M3= 4		M4= 2	
X=-90.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 56	RECTGL				
SP=-10	RO= 76.0				
M= 4	VP= 21.5	E= 0		I= 2100.0	TIME=2000
M1= 10	M2= 7	M3= 4		M4= 3	
X=-80.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 57	RECTGL				
SP=-7	RO= 95.9				
M= 5	VP= 25.2	E= 0		I= 2100.0	TIME=2000
M1= 11	M2= 8	M3= 5		M4= 3	
X=-70.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 58	RECTGL				
SP=-15	RO= 99.3				
M= 5	VP= 24.6	E= 0		I= 2100.0	TIME=2000
M1= 12	M2= 9	M3= 6		M4= 3	
X=-60.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 59	RECTGL				
SP=-15	RO= 95.2				
M= 5	VP= 22.4	E= 0		I= 2100.0	TIME=2000
M1= 11	M2= 8	M3= 5		M4= 3	
X=-50.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 60	RECTGL				
SP=-13	RO= 90.1				
M= 4	VP= 20.3	E= 0		I= 2100.0	TIME=2000
M1= 10	M2= 7	M3= 4		M4= 2	
X=-40.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 61	RECTGL				
SP=-13	RO= 70.8				
M= 4	VP= 15.5	E= 0		I= 2100.0	TIME=2000
M1= 10	M2= 7	M3= 5		M4= 2	
X=-30.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 62	RECTGL				
SP=-9	RO= 76.5				
M= 5	VP= 16.3	E= 0		I= 2100.0	TIME=2000
M1= 12	M2= 9	M3= 6		M4= 3	
X=-20.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	
RECALL 63	RECTGL				
SP=-16	RO= 82.4				
M= 5	VP= 17.4	E= 0		I= 2100.0	TIME=2000
M1= 12	M2= 9	M3= 6		M4= 4	
X=-10.0	Y= 30.0	MN/2= 10.0		AB/2= 250.0	

RECALL 64 RECTGL
SP=-11 RO= 85.5
M= 5 VP= 17.9 E= 0 I= 2100.0 TIME=2000
M1= 12 M2= 9 M3= 6 M4= 3
X= 0.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 65 RECTGL
SP=-9 RO= 69.9
M= 6 VP= 14.7 E= 0 I= 2100.0 TIME=2000
M1= 13 M2= 10 M3= 7 M4= 4
X= 10.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 66 RECTGL
SP=-10 RO= 77.1
M= 6 VP= 16.5 E= 0 I= 2100.0 TIME=2000
M1= 12 M2= 9 M3= 6 M4= 4
X= 20.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 67 RECTGL
SP=-7 RO= 73.5
M= 5 VP= 16.1 E= 0 I= 2100.0 TIME=2000
M1= 10 M2= 8 M3= 5 M4= 3
X= 30.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 68 RECTGL
SP=-12 RO= 105.0
M= 7 VP= 23.7 E= 0 I= 2100.0 TIME=2000
M1= 14 M2= 11 M3= 7 M4= 4
X= 40.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 69 RECTGL
SP=-13 RO= 136.4
M= 10 VP= 32.1 E= 0 I= 2100.0 TIME=2000
M1= 20 M2= 15 M3= 11 M4= 6
X= 50.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 70 RECTGL
SP=-8 RO= 117.0
M= 12 VP= 29.0 E= 0 I= 2100.0 TIME=2000
M1= 25 M2= 19 M3= 13 M4= 8
X= 60.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 71 RECTGL
SP=-8 RO= 99.6
M= 14 VP= 26.2 E= 0 I= 2100.0 TIME=2000
M1= 30 M2= 22 M3= 15 M4= 9
X= 70.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 72 RECTGL
SP=-5 RO= 130.4
M= 13 VP= 36.8 E= 0 I= 2100.0 TIME=2000
M1= 28 M2= 21 M3= 15 M4= 9
X= 80.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 73 RECTGL

RECALL 73 RECTGL
SP=-6 RO= 577.4
M= 17 VP= 176.7 E= 0 I= 2100.0 TIME=2000
M1= 36 M2= 27 M3= 19 M4= 12
X= 90.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 74 RECTGL
SP=-13 RO= 699.1
M= 18 VP= 234.4 E= 0 I= 2100.0 TIME=2000
M1= 36 M2= 27 M3= 19 M4= 12
X= 100.0 Y= 30.0 MN/2= 10.0 AB/2= 250.0

RECALL 75 RECTGL
SP=-2 RO= 52.9
M= 5 VP= 12.7 E= 0 I= 2100.0 TIME=2000
M1= 11 M2= 8 M3= 5 M4= 3
X=-120.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 76 RECTGL
SP=-11 RO= 59.4
M= 5 VP= 13.7 E= 0 I= 2100.0 TIME=2000
M1= 11 M2= 8 M3= 5 M4= 3
X=-110.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 77 RECTGL
SP=-4 RO= 62.8
M= 5 VP= 13.8 E= 0 I= 2100.0 TIME=2000
M1= 11 M2= 8 M3= 6 M4= 4
X=-100.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 78 RECTGL
SP=-2 RO= 70.4
M= 7 VP= 14.8 E= 0 I= 2100.0 TIME=2000
M1= 13 M2= 10 M3= 7 M4= 4
X=-90.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 79 RECTGL
SP=-6 RO= 79.2
M= 6 VP= 16.0 E= 0 I= 2100.0 TIME=2000
M1= 14 M2= 10 M3= 7 M4= 4
X=-80.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 80 RECTGL
SP=-13 RO= 93.9
M= 8 VP= 18.3 E= 0 I= 2100.0 TIME=2000
M1= 16 M2= 12 M3= 9 M4= 5
X=-70.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 81 RECTGL
SP=-17 RO= 100.3
M= 8 VP= 18.9 E= 0 I= 2100.0 TIME=2000
M1= 16 M2= 12 M3= 9 M4= 5
X=-60.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 82 RECTGL
SP=-19 RO= 100.3

RECALL 82 RECTGL
SP=-19 RO= 100.3
M= 7 VP= 18.4 E= 0 I= 2100.0 TIME=2000
M1= 15 M2= 11 M3= 8 M4= 5
X=-50.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 83 RECTGL
SP=-7 RO= 87.8
M= 8 VP= 15.7 E= 0 I= 2100.0 TIME=2000
M1= 16 M2= 12 M3= 8 M4= 5
X=-40.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 84 RECTGL
SP=-12 RO= 72.5
M= 8 VP= 12.7 E= 0 I= 2100.0 TIME=2000
M1= 17 M2= 12 M3= 8 M4= 5
X=-30.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 85 RECTGL
SP=-14 RO= 92.5
M= 8 VP= 16.0 E= 0 I= 2100.0 TIME=2000
M1= 17 M2= 13 M3= 9 M4= 6
X=-20.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 86 RECTGL
SP=-17 RO= 123.8
M= 9 VP= 21.3 E= 0 I= 2100.0 TIME=2000
M1= 18 M2= 14 M3= 10 M4= 6
X=-10.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 87 RECTGL
SP=-6 RO= 270.9
M= 11 VP= 46.4 E= 0 I= 2100.0 TIME=2000
M1= 22 M2= 16 M3= 12 M4= 7
X= 0.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 88 RECTGL
SP=-6 RO= 383.4
M= 12 VP= 65.9 E= 0 I= 2100.0 TIME=2000
M1= 23 M2= 18 M3= 12 M4= 8
X= 10.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 89 RECTGL
SP=-7 RO= 307.8
M= 12 VP= 53.3 E= 0 I= 2100.0 TIME=2000
M1= 25 M2= 19 M3= 13 M4= 8
X= 20.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 90 RECTGL
SP= 2 RO= 206.9
M= 12 VP= 36.3 E= 0 I= 2100.0 TIME=2000
M1= 24 M2= 18 M3= 13 M4= 8
X= 30.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 91 RECTGL

RECALL 91 RECTGL
SP=-14 RO= 166.2
M= 13 VP= 29.7 E= 0 I= 2100.0 TIME=2000
M1= 25 M2= 19 M3= 13 M4= 9
X= 40.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 92 RECTGL
SP=-13 RO= 138.1
M= 13 VP= 25.3 E= 0 I= 2100.0 TIME=2000
M1= 26 M2= 19 M3= 14 M4= 8
X= 50.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 93 RECTGL
SP=-0 RO= 139.6
M= 13 VP= 26.3 E= 0 I= 2100.0 TIME=2000
M1= 26 M2= 20 M3= 14 M4= 9
X= 60.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 94 RECTGL
SP=-10 RO= 133.3
M= 13 VP= 26.0 E= 0 I= 2100.0 TIME=2000
M1= 27 M2= 20 M3= 14 M4= 9
X= 70.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 95 RECTGL
SP= 4 RO= 118.6
M= 14 VP= 24.0 E= 0 I= 2100.0 TIME=2000
M1= 27 M2= 21 M3= 15 M4= 9
X= 80.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 96 RECTGL
SP= 12 RO= 121.3
M= 14 VP= 25.5 E= 0 I= 2100.0 TIME=2000
M1= 28 M2= 21 M3= 15 M4= 9
X= 90.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 97 RECTGL
SP=-11 RO= 129.7
M= 14 VP= 28.5 E= 0 I= 2100.0 TIME=2000
M1= 30 M2= 22 M3= 15 M4= 10
X= 100.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

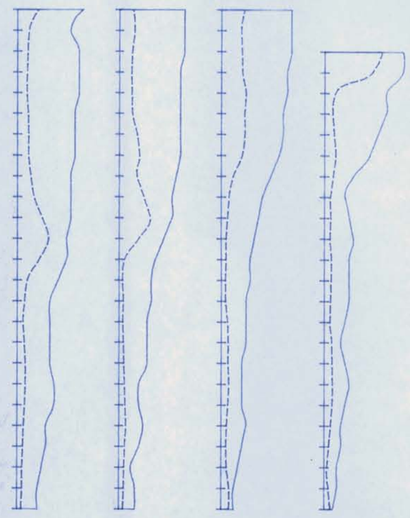
RECALL 98 RECTGL
SP=-7 RO= 144.1
M= 14 VP= 33.1 E= 0 I= 2100.0 TIME=2000
M1= 26 M2= 19 M3= 13 M4= 11
X= 110.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

RECALL 99 RECTGL
SP=-9 RO= 264.8
M= 15 VP= 63.8 E= 0 I= 2100.0 TIME=2000
M1= 31 M2= 23 M3= 16 M4= 10
X= 120.0 Y=-100.0 MN/2= 10.0 AB/2= 250.0

11700 E | 11750 E | 11800 E | 11850 E | 11900 E | 11950 E | 12000 E | 12050 E | 12100 E | 12150 E | 12200 E | 12250 E | 12300 E

12400 N
12350 N
12300 N
12250 N
12200 N
12150 N
12100 N
12050 N
12000 N
11950 N
11900 N
11850 N
11800 N
11750 N
11700 N

Inclination: 72 Deg
Declination: 23 Deg E



GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,604

IRON RIVER RESOURCES LTD

ARROWSTONE PROJECT
MOW N-S GRID, NTS 92P/2W
KAMLOOPS MINING DIVISION
INDUCED POLARIZATION SURVEY
Gradient Array Profiles, AB=500m, MN=20m

Chargeability solid line @ 1 cm = 10ms
Resistivity dashed line @ 1 cm = 500 ohm-m
SCALE 1:2000

DELTA GEOSCIENCE LTD

FIG. 6