ARIS SUMMARY SHEET

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SSESSMENT REPORT 18639   MINING DIVISION: Liard

ROPERTY: Kutcho Creek
OCATION: LAT   58 12 00   LONG   128 22 00
               UTM   09 6450941   537227
               NTS   104I01W
LAIM(S):   Josh 2-5,Dangerous,Pink One,Pink Two
PERATOR(S):   Esso Res.
UTHOR(S):   Holbeck, P.
EPORT YEAR: 1989, 60 Pages
OMMODITIES
EARCHED FOR: Copper,Zinc,Silver
EYWORDS: Triassic,Kutcho Formation,Sericite schist,Tuff,Pyroclastics
               Tight folds,Volcanogenic,Massive sulphides
ORK
ONE: Geochemical,Geophysical,Geological
          GEOL   600.0 ha
              Map(s) - 1; Scale(s) - 1:5000
          GRAV   6.2 km
              Map(s) - 3; Scale(s) - 1:2500
          SOIL   551 sample(s) ;ME
              Map(s) - 13; Scale(s) - 1:5000
ELATED
ORTS: 04863,05120,05294,05475,05641,05778,06025,06026,06038,06039,06273
               06343,06373,07433,07437,07537

1988 GEOCHEMICAL AND GEOPHYSICAL REPORT

on the

KUTCHO CLAIM GROUPS: 89A AND 89B

Liard Mining Division
NTS: 104I/1
Latitude: 58 12'N Longitude: 128 22'

Owned and Operated by :

Esso Minerals Canada Limited
1600-409 Granville Street
Vancouver, B.C. V6C 1T2

Report by:

Peter Holbek

March 10, 1989

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SUMMARY

The Kutcho-89A and 89B claim groups are located in the Liard Mining Division, approximately 100km east of Dease Lake. The claim groups lie immediately to the south of, and are contiguous with, claims hosting the Kutcho Creek volcanogenic massive sulphide deposits.

Exploration work in the area of the 89 claim groups was sporadic between 1968 and 1983. Since 1984-85, when geological mapping and a Questor airborne INPUT survey identified EM conductors within areas of favourable geology, exploration has been carried out on an annual basis. This report describes a program of soil geochemical and gravity surveys designed to locate drill targets along previously defined airborne and ground EM conductors.

Gravity surveys were carried out on four conductors. The surveys indicate that near-surface large sulphide lenses are not present in the areas tested. However, in two of the areas surveyed, gravity anomalies were detected in the vicinity of EM conductors. In general, gravity anomalies were low contrast and could indicate lithological changes or narrow (<10m) sulphide lenses at depths greater than 25m.

The soil survey covered an area 1800 by 2200m and yielded a number of weakly-defined multi-element anomalies parallel to an EM conductor trend. Copper, zinc and silver anomalies, although displaced relative to source by glaciation, suggest that the conductor is caused by sulphide mineralization and indicate two zones of metal enrichment along the conductor trend.

Further evaluation of EM conductors with coincident gravity and/or geochemical anomalies will require drill testing.

1.0 INTRODUCTION

1.1 Location and Access

The Kutcho Creek property is located within the Liard Mining Divison, NTS 104I/1, approximately 100 km east of Dease Lake, in northwest British Columbia (Figure 1.1). Geodetic coordinates are 58° 12′ N and 128° 22′ W.

Access to the property is by fixed-wing aircraft from Smithers, Dease Lake or Watson Lake to the 1100m gravel airstrip located beside Kutcho Creek. The property is connected to the airstrip by an 8km long road, however, the large size of the property requires helicopter access to the southern claim groups.

1.2 Climate and Physiography

Located within the Cassiar Mountains, on the divide between Arctic and Pacific watersheds, the area is moderately rugged with elevations ranging from 1400m to 2200m. Most of the area is alpine, with treeline at approximately 1500m. Snow cover can persist for nine months of the year. Structural fabric and two periods of glaciation have produced an intersecting pattern of east-west and north-south ridges. Major valleys are often filled with a deep layer of till.

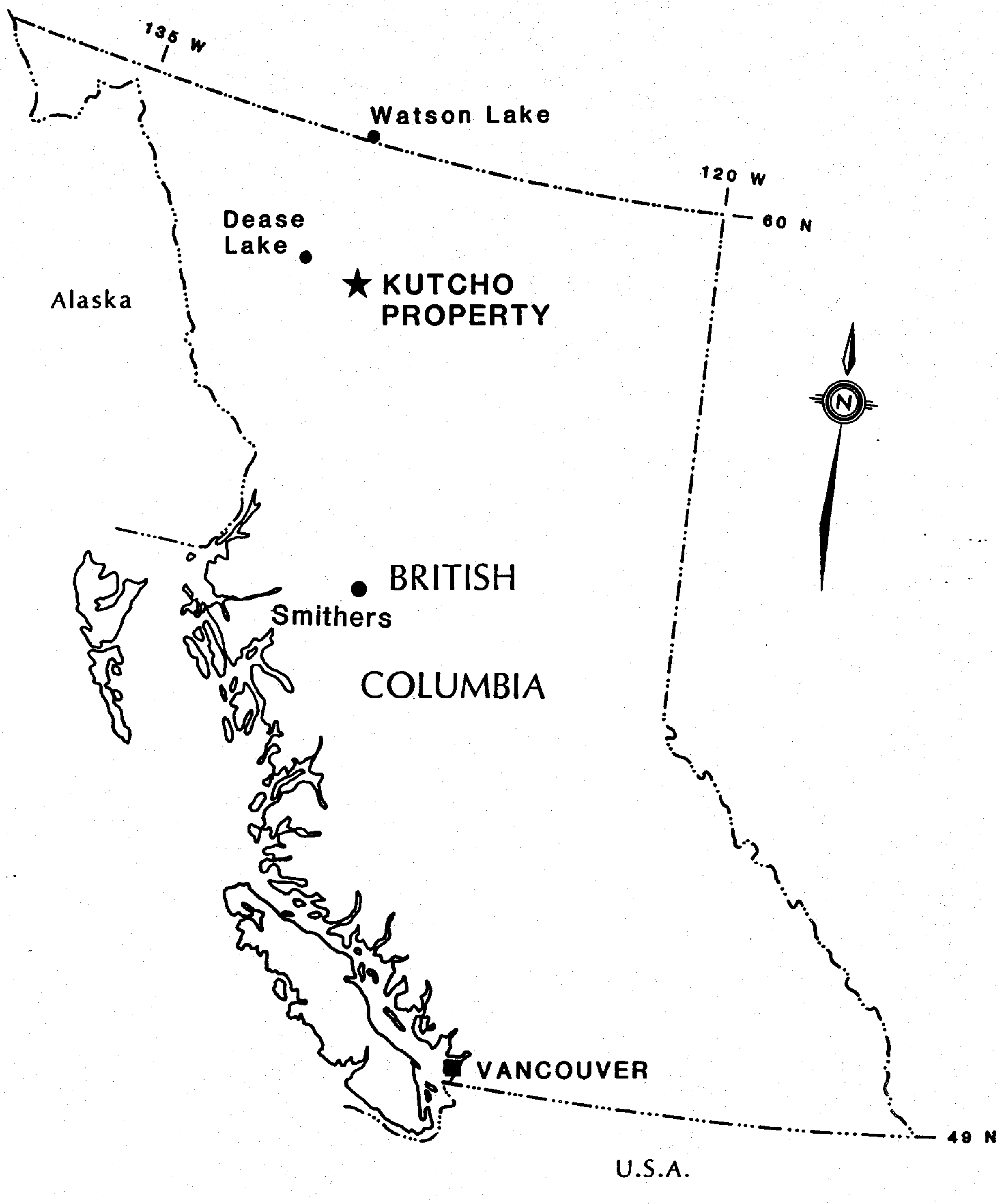

Figure 1.1 Property location map.

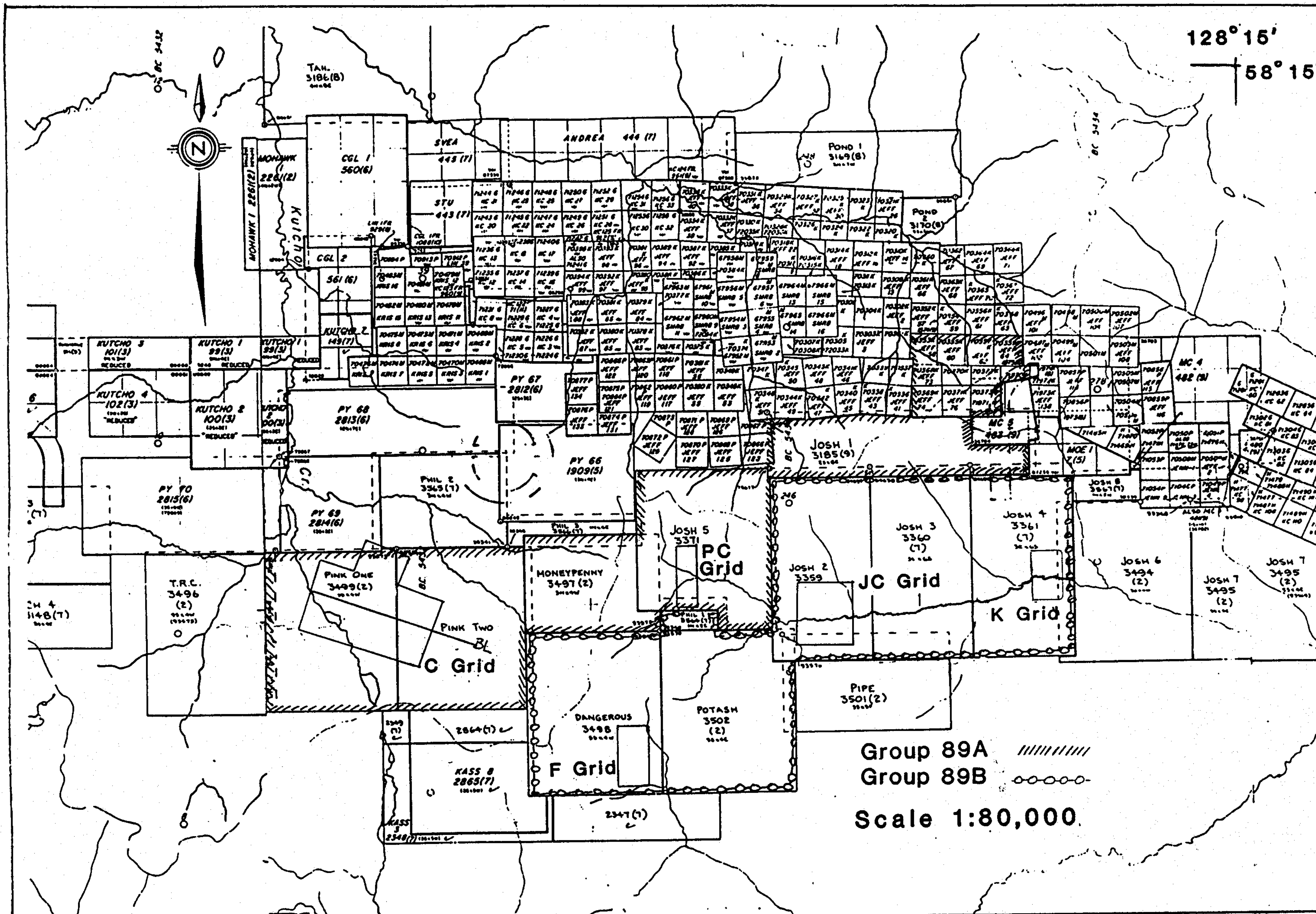

Figure 1.2 Claim map showing Kutcho 89A and 89B claim groups and location of grid areas.

TABLE 1 - CLAIM STATUS

GROUP 89A

CLAIM NAME	UNITS	DATE LOCATED	EXPIRY DATE	RECORD NUMBER
PINK ONE	20	Jan. 26/86	Feb. 7/91	3499
PINK TWO	20	Jan. 25/86	Feb. 7/91	3500
MONEY PENNY	12	Jan. 24/86	Feb. 7/92	3497
JOSH 1	16	Aug. 25/84	Sept. 7/89	3185
JOSH 5	20	July 21/85	Aug. 19/91	3371
JEFF 58	1	Aug. 27/73	Aug. 27/92	70353
JEFF 60	1	Aug. 27/73	Aug. 27/92	70355
JEFF 62	1	Aug. 27/73	Aug. 27/92	70357
JEFF 64	1	Aug. 27/73	Aug. 27/92	70359
JEFF 73	1	Aug. 27/73	Aug. 27/92	70368
JEFF 74	1	Aug. 27/73	Aug. 27/92	70369
JEFF 75	1	Aug. 27/73	Aug. 27/92	70370
JEFF 76	1	Aug. 27/73	Aug. 27/92	70371
JEFF 77	1	Aug. 27/73	Aug. 27/92	70372
JEFF 78	1	Aug. 27/73	Aug. 27/90	70373
JEFF 135	1	Aug. 20/74	Aug. 20/92	71970
JEFF 136	1	Aug. 20/74	Aug. 20/92	71970

CLAIM GROUP 89B

CLAIM NAME	UNITS	DATE LOCATED	EXPIRY DATE	RECORD NUMBER
DANGEROUS	20	Jan. 24/86	Feb. 7/91	3498
POTASH	20	Jan. 24/86	Feb. 7/91	3502
PHIL 1	2	June 27/86	July 7/92	3564
JOSH 2	18	June 21/85	July 17/91	3359
JOSH 3	18	June 21/85	July 17/90	3360
JOSH 4	18	June 21/85	July 17/90	3361

1.3 Property and History

The property lies to the south of, and is contiguous with, claims covering the Kutcho Creek polymetallic volcanogenic massive sulphide deposits. Claim groups are shown on Figure 1.2 and claim status is summarized in Table 1.1.

Various portions of the property have been held and worked by different companies in the past. The most significant exploration was carried out by Imperial Oil Ltd. (Esso Minerals Canada) who, in 1975, drilled three short holes to test conductors indentified by a 1974 Aerodat airborne EM survey. Geological mapping in 1984 and 1985 suggested that altered felsic volcanics on the property were structurally related to rocks hosting the Kutcho deposits. A Questor helicopter-borne MKVI INPUT EM and Magnetic survey flown in November 1985 identified a number of conductors within areas of favourable geology on the property. Since then, evaluation of the airborne conductors, consisting of relogging and lithogeochemical sampling of drill core from the 1975 program, ground geophysics, geology and geochemical surveys, has been carried out on an annual basis.

1.4 Current Work

The 1988 exploration program was carried out between August 23 and 31, and consisted of gravity surveys and a soil geochemical survey over selected target areas (Fig. 1.2). Target areas are primarily airborne EM conductors coincident with favourable geology.

A total of 6.2 line kilometers of gravity survey was completed over four targets (JC, PC, F and K). An 1800m by 2200m soil geochemical survey was completed over a fifth target area (C). The soil grid consisted of 25m sample spacing on lines spaced 200m apart along the trend of the EM conductor. A total of 551 soil samples were collected. A summary of work performed on each target and claim is given in Table 1.2.

The exploration crew was mobilized from Vancouver or Smithers and lodged at the Esso/Sumac camp located on the north side of the Kutcho deposit area. A Hughes 500D helicopter was contracted from Okanogan Helicopters in Smithers to transport the crew from the camp to the grid areas.

TABLE 1.2 - WORK PERFORMED AT EACH TARGET

TARGET	GRAVITY (km)	GEOCHEM (km)	CLAIM
C		16.8	Pink Two
PC	1.2		Josh 5
F	1.0		Dangerous
JC	2.6		Josh 2
K	1.4		Josh 4
TOTAL	6.2	16.8	

2.0 GEOLOGY

2.1 Regional Geology

The Kutcho property lies within the King Salmon Allochthon, a narrow belt of Triassic island arc volcanics and Jurassic sediments sandwiched between two northerly dipping thrust faults. Penetrative foliation and axial planes of the major folds are parallel to these bounding faults. The belt of volcanics is thickest in the area where it hosts volcanogenic massive sulphide deposits; due in part to primary deposition, but also to stratigraphic repetition by folding and thrusting. Major folds are delineated by the Sinwa Limestone and the contact between Kutcho Formation volcanics and Inklin Formation argillites (Fig. 2.1).

Volcanogenic mineralization of the Kutcho deposits occurs at the contact between footwall lapilli tuffs and hanging wall quartz and quartz-feldspar crystal tuffs. The main sulphide bearing horizon is marked by extensive hydrothermal alteration and the presence of thinly bedded ash tuffs, the latter indicating a temporary hiatus in volcanic activity. This sulphide horizon is geochemically, and often visually, recognizable over a strike length of 8 km.

The coarsest grained pyroclastic rocks of the Kutcho Formation occur in the vicinity of the known sulphide deposits and become noticeably finer grained towards the south and east. The major center of volcanism is postulated to be northeast of the Kutcho sulphide lens, although subordinate centers may exist elsewhere on the property.

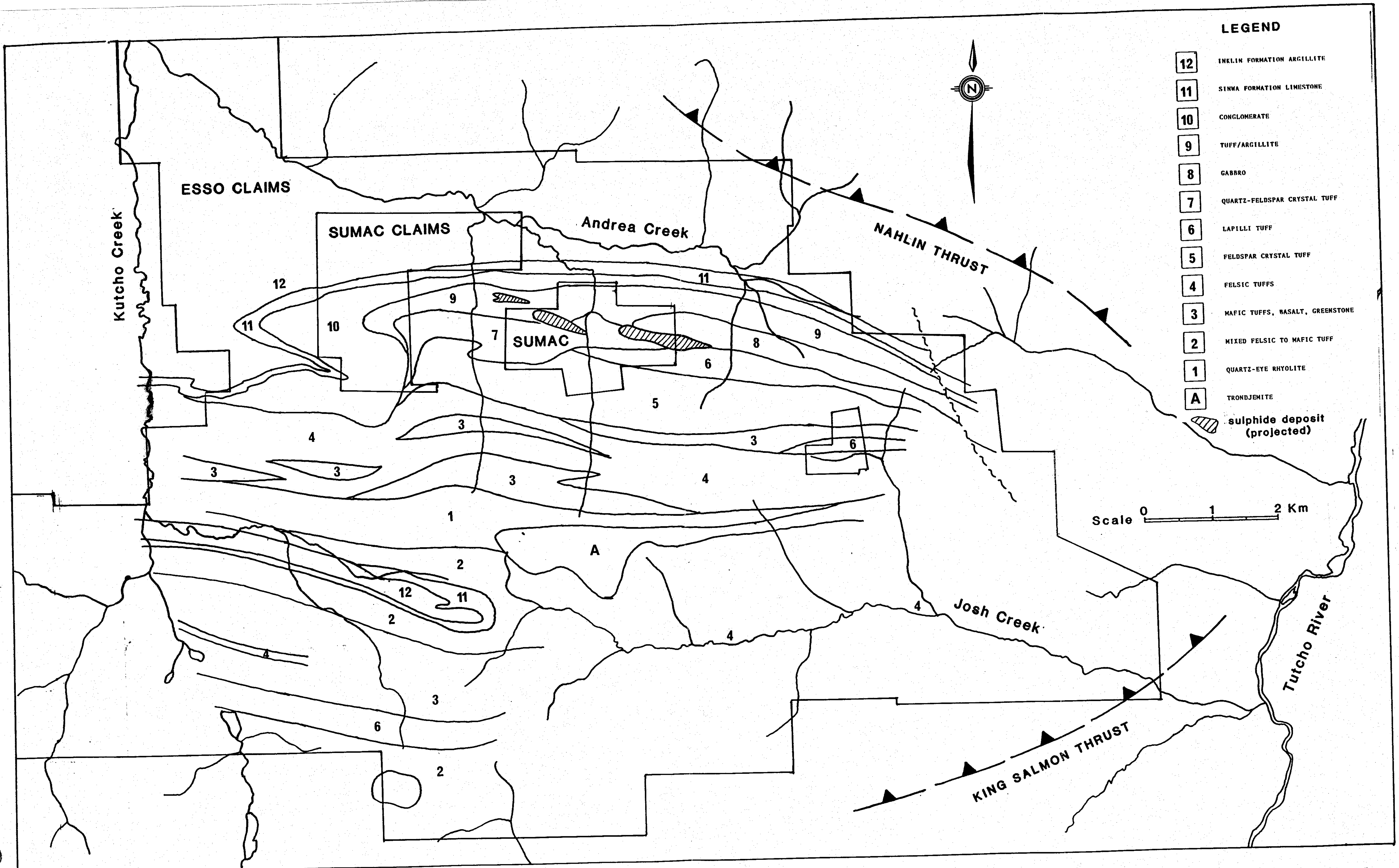

Figure 2.1 Generalized Geology, Kutcho Creek Property.

2.2 Property Geology

Rocks which underlie the Kutcho 89A and B claim groups are part of the Kutcho formation and consist of pyroclastic, flow and minor sedimentary units of mafic and felsic compositions. Lithological units tend to be thinly bedded and are finer grained than their compositional counterparts which host the Kutcho sulphide deposits. All rock units dip steeply to moderately to the north.

Geology of target C is reasonably well known from current and previous mapping (Figure 2.2). The main EM conductor is underlain, at its eastern end, by a thin (10 to 50m) band of sericite schist which hosts weakly mineralized chert or silica exhalite layers and small lenses of semi-massive to massive pyrite (Holbek and Thiersch, 1986). This felsic band is bounded on both sides by chlorite-epidote schists, inferred to be basalt flows. Outcrops are sparse within the geochemical grid area but the few that were observed indicate that the geology on the eastern end likely continues under the rest of the grid area. Sinwa limestone and argillite occur along the northern margin of the grid and support the hypothesis that the stratigraphic positions of the target C conductors and the Kutcho sulphide deposits are correlative.

Geology of the F grid is unknown. Outcrop areas to the north and east suggest that the conductor occurs within thinly interbedded mafic and felsic ash tuffs. The conductor may be part of an east-northeast trending set of conductors; some of which have been drilled and shown to be sulphide-rich argillaceous beds within hydrothermally altered felsic tuffs.

The PC grid overlies altered and mineralized pyroclastic rocks exposed in a northeast trending tributary of Josh Creek. A series of silicified, sericitic and pyritic quartz crystal tuff outcrops occur over an apparent thickness of 70m within the stream bed. Downstream from these outcrops there are numerous rounded boulders of sphalerite and galena bearing, finely banded, cherts or exhalites. No significant ground or airborne EM conductors have been found in this area.

The JC and K grids straddle Josh Creek with the EM conductors located on the north side of the Creek in areas of deep and swampy overburden. Rocks exposed in the stream bed consist of siliceous and sericitic schists derived from felsic ash tuffs. Pyritic layers, up to 30cm wide and traceable over 100m along strike, occur on the cliffs along the stream gully in the JC grid area. Neither the EM conductors nor the gravity anomalies correlate well with the pyritic exposures. On the K grid, the EM conductor occurs along the northern slope of the Josh Creek canyon. Rocks in this area are weakly altered crystal and crystal ash tuffs which are interbedded with minor amounts of mafic ash. The conductor appears to coincide with a narrow band of sericitic and pyritic ash tuff. Small fragments of graphitic argillite float were observed at one locality in this area.

3.0 GEOCHEMISTRY

3.1 Methods

A total of 551 soil samples were collected at 25m stations on grid lines spaced at 200m intervals along the EM conductor axis. Samples were taken from the B horizon where possible, at depths between 10-15cm. Some sample lines were located in moderately swampy areas, particularly near the central part of the grid. Samples were placed in kraft paper bags and air dried before shipment.

Analyses were performed by Acme Analytical Ltd. of Vancouver using Induction Coupled Plasma methods for 30 elements. Samples are sieved to -80 mesh and a 0.5g subsample is digested in 3ml of hot aqua regia for 1 hour and then diluted to 10ml with water prior to analysis.

Of the 30 elements analyzed 14 are deemed insignificant due to a combination of high detection limits, partial digestion and low background values. Analytical results for the remaining elements, which consist of Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, Ca, P, La, Cr, Mg, Ba, and Al, were statistically evaluated using Geomicro Systems' computer program GEOCHEM. 1:5,000 scale proportional symbol plots (Figs. 3.2 to 3.14) were used to define anomalous areas.

3.2 Description of Results

Previous geochemical surveys in the property area establised that copper and zinc, being major components of the sulphide deposits, were the best geochemical indicators. Arsenic and silver, although very minor components of the sulphide lenses, were also found to be useful as they were less influenced by background lithological changes. Similarly, lead and barium, trace components of the sulphide deposits, are useful geochemical indicators due to their different dispersion characteristics in the surficial environment, relative to copper and zinc. Rocks which underlie the grid area consist of interlayered basalt flows and tuffs and felsic ash tuffs. Sulphide deposits are typically hosted by altered felsic rocks. It was thought that the altered felsic rocks would have a detectable difference in soil geochemical signature from the basaltic rocks, particularly for Ni, Co, Cr, Al, Mg and Ca, and therefore element plots would help with geological mapping in overburden areas. However, this does not appear to be the case.

Table 3.1 is a summary of the basic statistics for the 16 elements investigated. Histograms and cumulative probability plots (Sinclair, 1974) were produced for each element and "threshold" values were chosen to separate different sample populations. In many cases, particularly for the major elements, sample populations were normally or log normally distributed and data were plotted as proportional sized symbols between values of mean minus 2 standard deviations and mean plus 2 standard deviations. The elements associated with sulphide deposits were generally bimodal and threshold values were chosen to separate background from anomalous populations. For those metals that did not have two (or more) distinct populations on the cumulative probability plots, thresholds were subjectively chosen between values at the mean plus one standard deviation and the 90th percentile.

To aid in the evaluation of multi-element data, element correlations were investigated. Both expected and unexpected correlations were noted. Elements associated with mafic lithologies (Mg, Cr, Co, and Ni) displayed a high degree of intercorrelation (Fig. 3.1) with the exception of Fe which did not correlate with any other elements. Although Cu and Zn are strongly correlated, the other elements associated with mineralization (Pb, Ag, As, and Ba) correlate poorly. P and La are strongly associated, which is not surprising as they occur in the same mineral, monazite, which is enriched in felsic, relative to mafic, rocks. Ba, Ca and Mn show strong correlations to P and La, suggesting a 'felsic' association. However, Cu correlates equally well with both Ni and La. Indeed, there is a high level of correlation between many of the elements that connot be accounted for by geological association and suggests that at least some element distribution is controlled by sample medium.

TABLE 3.1

ELEMENT	MIN	MAX	MEAN	S.D.	THRESHOLD
Al	0.22	5.04	2.4	0.75	
Ca	0.04	4.86	0.67	0.68	
Cr	3	295	54	25	85
Co	2	47	12	6	20
Fe	0.26	28.46	4.2	1.8	
Mg	0.05	3.16	0.79	0.34	
Mn	48	4176	640	380	1000
La	2	91	15	10	
Ni	8	304	52	30	80
P	0.01	0.23	0.06	0.03	0.10
As	2	66	9	7.5	18
Ba	12	604	150	75	225
Cu	10	514	55	65	100
Ag	0.1	1.3	.14	.1	0.15
Pb	2	59	13.6	5	20
Zn	37	1358	130	115	150

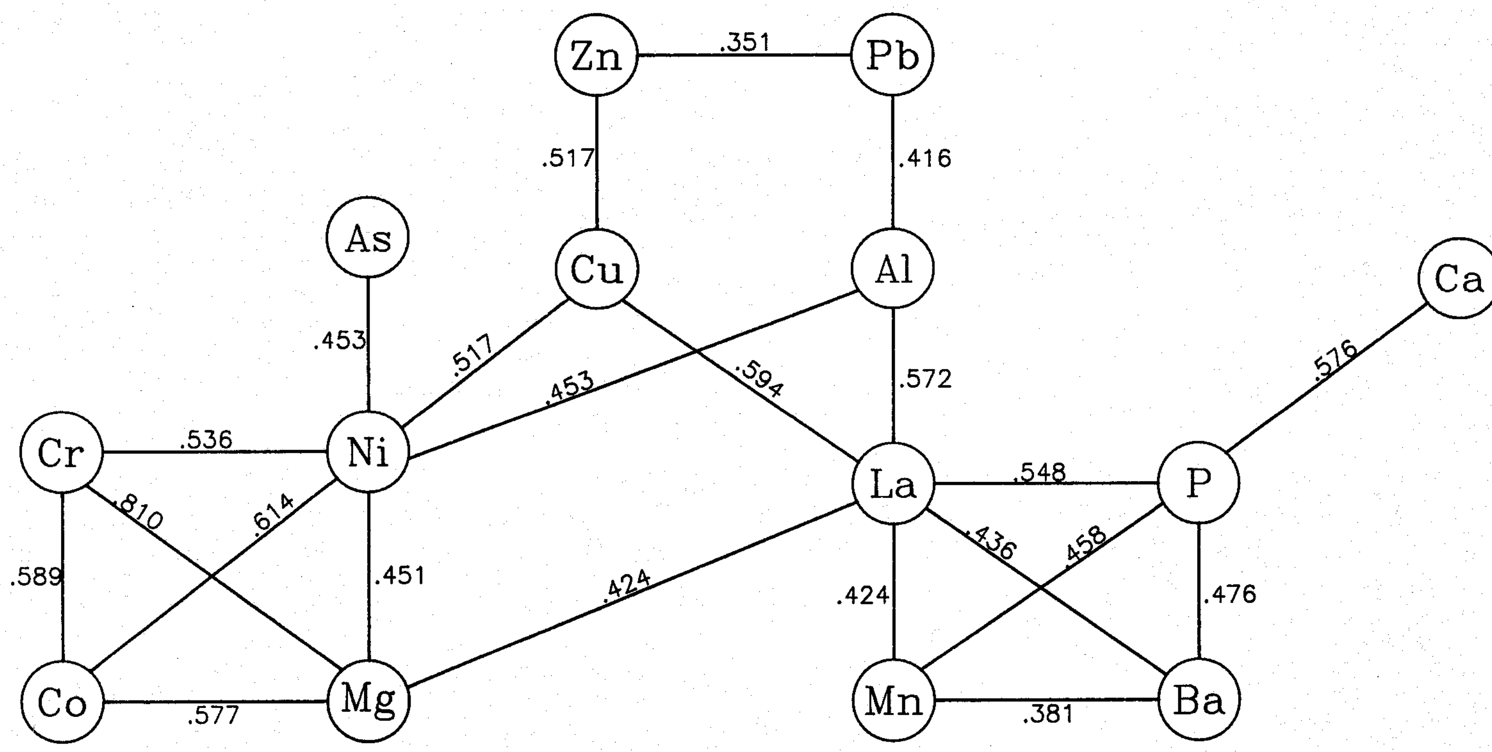

Figure 3.1 Significant correlations (n=551) of soil geochemical results for the Target "C" Grid, Kutcho Creek area.

Silver values were generally low and of low contrast, consequently the anomalies are small and not well clustered. Anomalous values (Fig. 3.2) form a weak trend which follows the trend of the EM conductor, although displaced 50 to 100m to the north in the "down-ice" direction. A single point anomaly occurs in the extreme southwest corner of the grid and may relate to the southernmost conductor, although this anomaly was not duplicated by any other elements.

Copper has a bimodal log normal population which is due to the influence of mineralization. The anomalies are not well clustered (Fig. 3.3) and suggest multiple sources. In a general way, the anomalous values appear to have been smeared in the down ice direction, north-westerly, from the northern two conductor trends. A small anomaly occurs on line 1600W at 950N and is unexplained.

Zinc displays good range and contrast with similar population characteristics to copper. The zinc anomaly is, however, much better clustered forming an egg shaped area, approximately 350m wide and 1400m long, centered near 2000W and 200N (Fig. 3.4). This anomalous area could be caused by down-ice dispersion from the northern-most conductor. The more southern conductors do not have significant zinc expressions. A single point anomaly at 1600W-950N corresponds to the copper anomaly at that location.

Lead has a log-normal population, low contrast, and weak, poorly clustered anomalies (Fig. 3.5). Spatial distribution of lead anomalies is similar to that of copper, but they are closer to the EM conductor trends.

A composite variable, combining Cu, Pb, Zn and Ag (Fig. 3.6) gives a slightly more informative plot than any of the single metals. Anomalies display down-slope and/or down-ice dispersion from the northern two conductor trends. The strongest geochemical response is associated with the northernmost conductor between lines 1800 and 2200W.

Arsenic has a log-normal distribution and low contrast anomalies. Anomalous values form single line clusters with an overall weak easterly trend that, unlike the other elements, occurs south of the north conductor trend (Fig. 3.7). This separation of arsenic from Cu, Zn and Ag anomalies has been noted in previous surveys on the property and may reflect preferential arsenic enrichment in the footwall relative to the hanging-wall.

Barium has a skewed normal distribution with three peaks on the histogram, possibly reflecting three overlapping populations. Spatial distribution of barium values (Fig. 3.8) appears to be unrelated to the location of EM conductors, with the higher values concentrating along the north and south edges of the grid area. This spatial distribution is possibly lithologically controlled and may reflect proximity to limestone as Ba which occurs as a substitute for Ca in carbonates is readily digestable by aqua regia whereas barite is not. However, distribution of calcium (Fig. 3.9), although similar to barium, is much more erratic and does not appear to indicate control by carbonate rocks.

Manganese (Fig. 3.10) and lanthanum (Fig. 3.11) have low contrast single populations and, like calcium, symbol plots are not particularly informative. There is a weak northwesterly trend defined by alternating areas of high and low values which is approximately parallel to topography. This suggests that surficial geology and ground water have more influence on Ca, Mn, La and P distribution than bedrock geology.

Iron has a skewed normal distribution and two extreme highs. A proportional symbol plot (Fig. 3.12) which emphasizes the high (>6.0%) iron values shows poorly clustered anomalies that could reflect dispersion from areas along the conductive trends or, alternatively, indicate areas of shallow overburden.

Nickel has a normal distribution and produces a symbol plot (Fig. 3.13) similar to that of iron. A symbol plot for a composite variable calculated from Cr, Co, Ni and Mg values (Fig. 3.14) may outline areas underlain by mafic rocks. However, comparisons of the anomalous areas with air photographs suggests that anomalies correspond to areas proximal to outcrop.

3.3 Discussion of Results

The northernmost of three EM conductors at target C is over 4 km long and is hosted, on its eastern end, by hydrothermally altered felsic volcanic rocks which contain bands of massive sulphide and weakly mineralized silica exhalites. Previous surveys demonstrated that poorly defined, low contrast soil geochemical anomalies coincide with this area. The soil geochemical grid was extended 1800m to the west of the previous grid to test the geochemical response of a western portion of the conductor and to determine whether geochemistry could help define lithological contacts in overburden covered areas. Factors anticipated to affect the soil geochemical response included: variations in depth of glacial till and till content, variations in development of soil profile, drainage (or lack of), permafrost and frost boils. These factors, together with only partial digestion for certain elements, rendered major and trace element chemistry ineffective for defining underlying lithologies. Trends for composite values of closely correlated element groups were better defined than for the individual elements but, in the case of Cr, Co, Ni and Mg, appeared to be more related to topography (proximity to outcrop) and drainage than to bedrock geology. Elements associated with volcanogenic mineralization, particularly copper, zinc and silver, displayed anomalies that appear to correlate with EM conductors.

Significant soil response of copper, zinc and possibly iron, suggest that the northern two EM conductors are caused by sulphide mineralization. The strongest base metal anomalies are associated with the northern conductor between 1800 and 2200W.

4.0 GEOPHYSICS

4.1 Methods and Equipment

Gravity surveys were performed over EM conductors in an attempt to discriminate between massive sulphide and argillaceous conductors. Over six line kilometers of surveying was completed over four targets. At least two lines were surveyed on each grid, either 150 or 200m apart. Survey stations were located at 25m intervals along the grid lines.

Any geological condition that results in a horizontal variation in density, such as the presence of massive sulphides or a change in lithological density or porosity, will cause a gravity anomaly. The gravimeter is an extremely sensitive weighing device that records the relative variation in gravity, using an astatic system to measure minute changes in the length of a weighted spring. The unit of measurement is the milligal; one gal being equal to 1cm/sec/sec. Bouguer gravity is the result of corrections for various factors including: instrument drift; height of instrument; latitude and tidal effects; and changes in elevation between survey stations. The LaCoste-Romberg Model G gravimeter, with an accuracy of +/- 0.02 mgals, was used in this survey.

Station elevations were measured using a GDD Model C hydrostatic elevation meter. This instrument consists of a transducer and a fluid filled plastic tube 29m long that is stretched between survey stations. The instrument calculates the elevation difference based on relative fluid pressure and is accurate to +/- 0.005m.

4.2 Description of Results

The results are presented as profiles at a scale of 1:2,500 (Figures 4.1 to 4.8). The scales for the elevation and gravity profiles are 1cm = 50m and 0.5mgals respectively. The approximate location of the grids can be found on Figure 1.2.

JC GRID

Both fixed-source GENIE and airborne INPUT surveys have outlined a series of weak EM conductor trends over the grid area. Four lines near the center of the conductor trends were surveyed with gravity and elevation meters (Fig. 4.1 and 4.2) in order to determine the nature of the conductors. Lines 1450E and 1600E were extended to the south, over Josh Creek, where altered felsic volcanic rocks contain disseminated pyrite.

The survey outlined two areas of interest. The first is a gravity low centered at 350N on lines 1450E and 1600E. This anomaly correlates with highly altered felsic volcanics found in Josh Creek. A fixed-source GENIE conductor correlates with the north side of this gravity low and may indicate the contact between the altered volcanic rocks and denser rocks to the north. The second area is located between 500N and 600N and consists of two separate high density zones. The gravity profiles of these zones have a maximum relief of 0.5mgals and their shape suggests that the source is within 30m of the surface. There are no EM conductors directly coincident with either of these gravity trends. A weak conductor at 700N may be caused by the contact between these high density units and lighter rocks to the north.

PC GRID

Altered felsic volcanic rocks which contain disseminated to semi-massive pyrite are exposed in creek gullies that cross the grid area. This area was surveyed with fixed-source GENIE in 1986 but failed to locate any conductors coincident with the altered volcanic rocks. The gravity survey (Figs. 4.3 and 4.4) detected a low density anomaly between 325N and 375N on both lines which may be caused by a zone of altered and/or leached rocks.

K GRID

This grid covers an airborne INPUT EM conductor located on the north side of Josh creek. No significant density anomalies were detected along either of the two lines surveyed with the gravity meter (Figs. 4.5 and 4.6).

F GRID

The target on this grid is an airborne INPUT EM conductor. The EM anomaly has a low amplitude and may be caused by a deep conductor just north of a steeply incised creek valley. The gravity survey (Fig. 4.7 and 4.8) detected a weak gravity anomaly between 0 and 100N which is coincident with the interpreted trend of the INPUT conductor. The density anomaly has a maximum amplitude of 0.25 mgals and is not well defined.

4.3 Discussion of Results

Gravity highs were detected on grids JC and F. The two anomalous features on grid JC do not correlate directly with the EM conductors outlined in this area and could be caused by density contrasts between rock units. The weak EM anomaly at 700N could then be interpreted as the contact between high density rocks on the south and low density rocks to the north.

The airborne EM anomaly on grid F is interpreted to be caused by a deep conductor. A weak gravity high coincident with this conductor suggests a sulphide source.

Surface indications of mineralization on the PC grid do not have any associated EM or gravity anomalies and therefore a sulphide deposit at shallow to moderate depths is improbable. Surface features may mark potentially productive stratigraphy. The lack of a gravity high associated with the conductor on grid K indicates that if the conductor is caused by sulphides, then the sulphide horizon is thin.

5.0 CONCLUSIONS AND RECOMMENDATIONS

The 1988 exploration program on the Kutcho claim groups was designed to further evaluate areas of favourable geology and/or geophysics and to identify areas for drill testing. Four areas were investigated with Bouguer gravity surveys (JC, PC, K & F) and one area with soil geochemistry (C).

Targets JC, PC and K appear to occur within approximately the same stratigraphic sequence which has a strike length in excess of 6 km. This sequence displays both favourable geology for volcanogenic deposits and evidence of hydrothermal alteration and mineralization. However, EM conductors do not correlate with the best surface indications of mineralization and both EM and gravity surveys indicate that there is little likelihood of any near-surface sulphide deposit. Potential for deep sulphide deposits cannot be ruled out and further evaluation of this package of stratigraphy will require drill testing.

Target F contains a deep EM anomaly with a coincident weak high-density anomaly. The EM conductor has a relatively short strike length (700 m) and the geology is unknown. The target area should be gridded and the conductor located with a deep-penetrating ground EM survey. Soil geochemistry may offer some encouragement but as the target is deep results are likely to be ambiguous. If the ground EM survey is successful the target should be drill tested.

Target C consists of multiple, parallel EM conductors. The northern-most conductor, which has a strike length in excess of 4 km, is associated with exposed sulphide mineralization at its eastern end. Significant base metal soil anomalies associated with the central part of the conductor supports a sulphide source. This area should be surveyed with a ground EM system to accurately locate the conductor, which should then be drill tested.

APPENDIX I

STATEMENT OF COSTS

STATEMENT OF COSTS

LABOUR - August 23-31

Z. Doborzynski - 9 days @ 333/day	$ 2,997	
P. Holbek - 5 days @ 253/day	1,265	
H. Marsden - 7 days @ 165/day	1,155	
B. Dupuis - 9 days @ 110/day	990	
A. McEntesh - 9 days @ 110/day	990	
D. Rawlek - 5 days @ 110/day	550	
G. Grant - 5 days @ 80/day	400	
B. McDonald - 5 days @ 80/day	400	
P. Wood - 4 days @ 80/day	320	
		$ 9,067

FOOD AND ACCOMMODATION

76 man days @ $50/day	$ 3,800	$ 3,800

EQUIPMENT RENTAL

Gravimeter $200/day	$ 1,800	
Software	260	
		$ 2,060

GEOCHEMICAL ANALYSIS

551 soil samples @ 7.10 (incl. prep.)	$ 3,912	
Air Freight	102	
		$ 4,014

TRANSPORTATION

Canadian Airlines	$ 1,460	
Central Mtn. Air - Twin Otter	3,640	
Flywest Airservices	720	
Okanagan Helicopters - Hughes 500D		
9 hours @ $665 (incl. fuel & oil)	5,985	
Freight	840	
		$12,645

Report Preparation	$ 3,000	$ 3,000
TOTAL		$34,586

APPENDIX II

STATEMENT OF QUALIFICATIONS

STATEMENT OF QUALIFICATIONS

I, Peter Holbek, DO HEREBY CERTIFY THAT:

1) I am a project geologist presently employed by Esso Minerals Canada, a division of Esso Resources Canada Limited, located at 1600 - 409 Granville Street, Vancouver, B.C. V6C 1T2.

2) I graduated from the University of British Columbia with a B.Sc.(Hons.) in geology in 1980 and an M.Sc. in geology in 1988.

3) I have actively practiced my profession in North America since 1975.

4) The work described herein was done by me or under my direct supervision.

DATED THIS 29th DAY OF NOVEMBER, 1988 AT VANCOUVER, B.C.

Peter Holbek

APPENDIX III

GEOCHEMICAL DATA, GRID PLOTS

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

SEP 30 1988

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL P -40 mesh, Pulverized.

DATE RECEIVED: SEP 21 1988 DATE REPORT MAILED: Sept 29/88 ASSAYER......D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

88.9.30

ESSO MINERALS CANADA LTD. PROJECT 122-KUTCHO File # 88-4699 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
24+00W 7+00N	3	34	14	158	.1	46	11	605	5.49	7	5	ND	1	21	1	2	2	56	.35	.042	9	56	.81	151	.10	2	1.74	.01	.04	1
24+00W 6+75N	3	20	15	106	.1	23	8	489	6.22	2	5	ND	2	7	1	2	2	52	.08	.062	12	42	.56	59	.18	2	3.00	.01	.04	1
24+00W 6+50N	3	47	21	161	.3	44	14	759	5.80	2	5	ND	3	16	1	2	2	44	.24	.050	29	37	.74	109	.21	2	3.92	.02	.05	1
24+00W 6+25N	5	49	18	110	.2	29	9	400	5.67	9	5	ND	2	9	1	2	3	49	.09	.037	20	47	.85	58	.07	2	2.97	.01	.03	1
24+00W 6+00N	1	18	11	113	.1	22	8	457	5.13	2	5	ND	1	6	1	2	2	65	.08	.031	4	53	1.28	42	.12	2	2.34	.01	.02	1
24+00W 5+75N	3	20	19	77	.2	20	9	845	5.22	4	5	ND	1	9	1	2	2	72	.08	.064	9	47	.65	68	.13	2	1.71	.01	.04	1
24+00W 5+50N	1	71	13	127	.1	38	15	768	5.07	8	5	ND	1	24	1	2	2	57	.40	.036	55	56	1.09	128	.07	2	1.97	.01	.04	1
24+00W 5+25N	1	80	10	158	.1	36	17	819	3.76	2	5	ND	1	29	1	2	2	48	.48	.054	15	46	.98	122	.07	2	1.60	.01	.03	1
24+00W 4+75N	1	40	17	134	.1	31	8	369	3.85	4	5	ND	1	26	1	2	2	45	.47	.043	21	34	.59	181	.08	2	2.59	.01	.05	1
24+00W 4+50N	1	14	13	127	.1	21	5	281	2.64	2	5	ND	1	27	1	2	2	41	.38	.024	11	30	.56	130	.07	2	1.64	.01	.04	1
24+00W 4+25N	2	57	19	326	.1	38	14	1443	5.35	3	5	ND	1	24	2	2	2	58	.48	.073	16	49	.69	147	.16	2	3.00	.01	.04	1
24+00W 4+00N	2	32	12	109	.1	46	14	598	6.27	8	5	ND	3	11	1	2	2	69	.19	.087	10	60	.98	93	.20	2	2.63	.01	.05	1
STD C	18	58	40	128	7.0	66	26	923	3.80	39	17	6	34	47	16	18	17	55	.46	.087	36	56	.83	167	.06	38	1.81	.06	.14	13
24+00W 3+75N	1	21	13	74	.1	28	7	347	3.37	2	5	ND	2	16	1	2	2	49	.14	.051	8	40	.67	110	.06	2	1.81	.01	.04	1
24+00W 3+50N	2	35	13	277	.5	24	6	350	3.68	5	5	ND	1	16	1	2	2	52	.12	.044	13	44	.55	104	.06	2	2.46	.01	.04	1
24+00W 3+25N	1	19	11	81	.1	29	7	308	2.87	6	5	ND	1	26	1	2	2	41	.25	.045	10	38	.61	119	.05	2	2.00	.01	.05	1
24+00W 3+00N	1	16	8	109	.1	26	7	294	2.61	8	5	ND	1	26	1	2	3	41	.24	.041	11	32	.59	135	.05	2	1.50	.01	.05	1
24+00W 2+75N	1	50	14	224	.2	31	8	552	3.41	10	5	ND	1	26	1	2	2	46	.56	.067	15	44	.67	131	.07	2	2.22	.01	.04	1
24+00W 2+50N	1	22	14	61	.2	29	8	410	2.70	5	5	ND	1	32	1	2	2	40	.44	.039	13	34	.59	163	.04	2	1.79	.01	.04	1
24+00W 2+25N	1	19	13	84	.3	31	8	342	3.28	7	5	ND	1	22	1	2	2	45	.36	.036	10	39	.64	142	.05	2	2.27	.01	.04	1
24+00W 2+00N	1	20	12	77	.2	37	8	343	4.06	3	5	ND	1	19	1	2	2	55	.20	.033	10	54	.86	121	.06	2	2.41	.01	.07	1
24+00W 1+75N	1	77	12	153	.2	33	9	577	3.04	5	5	ND	1	30	1	2	2	37	1.01	.057	14	42	.67	111	.06	2	1.82	.01	.03	1
24+00W 1+50N	1	22	10	46	.1	30	7	252	2.46	8	5	ND	2	32	1	2	2	42	.31	.048	11	35	.62	115	.07	2	1.33	.01	.04	2
24+00W 1+25N	1	17	14	81	.1	28	10	410	3.29	7	5	ND	1	19	1	2	2	63	.31	.030	8	61	.95	113	.10	2	1.90	.01	.05	1
24+00W 1+00N	1	29	10	84	.3	26	7	334	2.68	10	5	ND	1	29	1	2	2	47	.36	.042	11	39	.63	121	.07	2	1.66	.01	.04	1
24+00W 0+75N	1	36	11	97	.1	34	8	350	3.23	8	5	ND	1	19	1	2	3	54	.19	.035	8	49	.89	89	.08	2	1.72	.01	.04	1
24+00W 0+50N	1	13	9	47	.2	19	5	198	2.78	6	5	ND	2	18	1	2	2	47	.21	.024	9	31	.49	86	.06	2	1.34	.01	.05	2
24+00W 0+25N	1	49	11	114	.2	56	18	678	5.96	2	5	ND	1	20	1	2	2	76	.36	.055	8	53	1.03	119	.03	2	2.28	.01	.05	1
RE 24+00W 1+25N	1	18	13	82	.2	30	10	417	3.34	10	5	ND	1	19	1	2	2	64	.32	.030	9	61	.97	114	.10	2	1.91	.01	.06	1
24+00W 0+00N	1	47	14	274	.2	55	12	610	3.43	14	5	ND	1	40	2	2	2	49	.98	.070	13	55	.85	147	.05	2	1.97	.01	.05	1
24+00W 0+25S	1	92	9	340	.1	57	12	667	2.93	8	5	ND	1	34	3	2	2	32	1.17	.053	19	34	.50	126	.05	3	1.52	.01	.04	1
24+00W 0+50S	1	68	8	122	.1	41	10	566	2.44	5	5	ND	1	40	1	2	2	35	1.27	.057	10	39	.56	125	.04	2	1.27	.01	.04	1
24+00W 0+75S	1	31	7	49	.1	34	9	442	2.29	4	5	ND	1	37	1	2	2	35	1.16	.044	8	42	.59	107	.05	2	1.11	.01	.05	2
24+00W 1+00S	1	31	11	66	.1	45	13	489	3.26	4	5	ND	1	31	1	2	2	47	.39	.051	11	64	.82	155	.05	2	1.76	.01	.05	1
24+00W 1+25S	1	41	11	62	.1	46	10	367	3.14	8	5	ND	1	29	1	2	2	50	.40	.047	8	63	.86	124	.09	2	1.72	.01	.04	1
24+00W 1+50S	1	22	11	65	.1	42	13	523	4.55	8	5	ND	1	15	1	2	2	66	.31	.052	5	67	.92	72	.13	2	1.80	.01	.04	1
24+00W 1+75S	1	366	11	189	.1	84	28	629	5.25	15	5	ND	1	22	1	2	2	75	.74	.039	8	136	1.72	84	.15	2	2.20	.01	.04	1
24+00W 2+00S	1	157	11	96	.1	64	17	686	3.83	6	5	ND	1	33	1	2	2	42	1.25	.047	15	53	.68	122	.09	2	1.30	.02	.04	1

ESSO MINERALS CANADA LTD. PROJECT 122-KUTCHO FILE # 88-4699

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
24+00W 2+25S	1	75	7	78	.1	49	17	520	4.69	8	5	ND	1	17	1	2	3	57	.86	.047	5	71	.88	76	.15	2	1.71	.01	.03	2
24+00W 2+50S	1	37	10	61	.1	71	23	491	4.17	2	5	ND	1	11	1	2	2	63	.38	.036	4	102	1.23	41	.22	3	2.21	.01	.03	1
24+00W 2+75S	2	47	13	113	.2	70	27	721	5.73	19	5	ND	1	14	1	2	2	42	.71	.048	12	72	.80	63	.15	2	2.60	.01	.05	2
24+00W 3+00S	1	47	12	108	.1	56	18	958	3.31	6	5	ND	1	23	1	2	2	52	.86	.063	12	66	.80	99	.09	2	1.86	.01	.05	1
24+00W 3+25S	1	22	14	90	.1	49	17	755	3.88	2	5	ND	1	17	1	2	2	56	.41	.048	9	57	.82	79	.13	2	2.04	.01	.04	2
24+00W 3+50S	1	17	10	59	.1	41	12	534	3.00	5	5	ND	1	18	1	2	2	49	.28	.034	10	50	.92	74	.12	2	2.11	.01	.05	1
24+00W 3+75S	1	55	25	218	.1	69	17	1435	4.79	2	5	ND	1	13	2	2	2	30	.18	.105	27	68	.39	161	.05	2	3.87	.02	.06	1
24+00W 4+00S	1	22	13	76	.1	47	16	613	3.05	4	5	ND	1	16	1	2	2	54	.29	.045	7	59	.97	81	.13	2	1.97	.01	.05	2
24+00W 4+25S	1	91	37	110	.1	255	47	1440	5.00	14	5	ND	1	27	1	2	2	49	1.24	.144	24	295	3.16	147	.03	3	2.44	.01	.06	1
RE 24+00W 6+25S	1	21	19	64	.1	67	13	689	3.83	63	5	ND	1	17	1	2	2	56	.23	.053	7	83	1.12	95	.10	2	2.08	.01	.04	2
24+00W 5+00S	1	84	13	271	.1	50	13	745	4.13	11	5	ND	1	33	1	2	2	52	.88	.070	24	52	.95	201	.07	2	2.53	.01	.05	1
24+00W 5+50S P	1	34	19	74	.1	84	17	1084	3.60	9	5	ND	1	41	1	2	3	56	.89	.092	11	87	1.08	245	.04	4	2.13	.02	.11	2
24+00W 5+75S P	1	40	19	66	.1	148	16	700	3.47	7	5	ND	1	28	1	3	2	58	.40	.044	8	102	1.64	134	.09	5	1.90	.02	.10	1
24+00W 6+00S	1	36	27	96	.2	96	41	2208	4.78	12	5	ND	1	23	1	2	2	60	.35	.080	9	91	1.18	127	.09	2	2.31	.01	.06	1
24+00W 6+25S	1	20	21	64	.1	65	13	681	3.75	63	5	ND	1	17	1	3	2	55	.22	.050	6	82	1.07	91	.10	5	2.02	.01	.04	3
24+00W 6+50S	1	13	15	63	.1	32	6	296	3.57	5	5	ND	1	17	1	2	2	56	.14	.033	9	47	.56	125	.06	3	2.11	.01	.04	1
24+00W 6+75S	1	28	15	79	.1	61	8	477	2.80	4	5	ND	1	39	1	2	2	48	.75	.037	15	68	.72	247	.08	2	1.72	.01	.06	2
24+00W 7+00S	1	21	11	64	.1	60	11	483	3.19	6	5	ND	1	25	1	2	2	52	.33	.039	8	68	1.22	103	.11	3	1.61	.01	.06	1
STD C	18	57	45	132	7.1	69	29	1026	4.04	35	18	7	37	46	18	17	19	58	.49	.088	37	58	.92	163	.07	31	2.02	.06	.13	13
24+00W 7+25S	1	31	11	63	.2	64	12	509	3.18	8	5	ND	1	32	1	2	2	48	.44	.064	11	65	1.15	155	.08	3	1.90	.01	.06	1
24+00W 7+50S P	1	21	15	70	.1	47	19	1286	4.00	9	5	ND	1	24	1	2	2	76	.35	.040	9	86	.92	110	.14	3	1.59	.02	.09	1
24+00W 7+75S P	1	23	12	87	.1	57	16	802	3.69	8	5	ND	1	27	1	2	2	53	.45	.042	10	68	1.15	124	.12	3	1.89	.02	.08	2
24+00W 8+00S	1	22	13	59	.2	47	11	507	3.01	5	5	ND	1	29	1	2	2	50	.37	.059	9	61	.93	168	.08	2	1.77	.01	.05	2
24+00W 8+25S	1	35	16	84	.1	72	13	967	3.75	11	5	ND	1	31	1	2	2	56	.34	.062	9	65	1.08	154	.09	3	2.42	.01	.04	2
24+00W 8+50S	1	38	14	85	.1	67	15	586	4.14	2	5	ND	3	26	1	2	2	54	.36	.052	16	59	1.17	141	.19	4	2.50	.02	.05	2
24+00W 8+75S	3	23	21	83	.3	23	7	371	5.43	2	5	ND	3	9	1	2	2	54	.16	.055	18	43	.45	62	.25	2	2.80	.02	.06	1
24+00W 9+00S	1	18	14	76	.1	46	10	422	3.94	9	5	ND	1	17	1	2	2	56	.28	.041	6	64	1.15	78	.14	3	2.40	.01	.04	1
24+00W 9+25S	1	27	10	66	.1	47	11	470	3.70	9	5	ND	1	16	1	2	2	51	.36	.057	6	62	1.14	61	.14	2	2.14	.01	.03	2
24+00W 9+50S	1	17	11	70	1.0	42	11	537	4.20	6	5	6	1	14	1	2	2	55	.30	.049	5	61	1.09	57	.15	2	2.33	.01	.03	1
24+00W 9+75S	1	12	10	49	.1	30	8	405	4.59	12	5	ND	1	15	1	3	2	71	.27	.227	4	63	.87	61	.10	2	1.84	.01	.03	3
24+00W 10+00S	1	18	9	62	.1	24	7	376	4.16	6	5	ND	1	9	1	2	2	44	.21	.036	3	43	.72	32	.16	2	1.55	.01	.03	1
22+00W 7+00N	2	86	14	155	.5	62	13	717	5.01	2	5	ND	1	37	1	2	2	47	.58	.058	40	50	.86	296	.06	2	3.41	.01	.09	1
22+00W 6+75N P	4	215	22	271	.6	65	19	1398	6.74	7	5	ND	1	38	1	2	2	64	.66	.073	91	62	1.02	296	.09	2	3.73	.02	.13	1
22+00W 6+50N	1	78	17	157	.1	48	12	633	4.27	2	5	ND	1	31	1	2	2	50	.43	.045	38	44	.77	182	.11	2	2.44	.01	.06	1
22+00W 6+25N	1	61	19	179	.1	44	14	891	4.18	2	5	ND	1	32	1	3	2	66	.49	.041	24	71	1.32	193	.05	2	2.15	.01	.06	1
22+00W 6+00N	1	36	7	103	.1	35	9	455	2.87	7	5	ND	1	28	1	3	2	53	.43	.044	13	52	1.05	97	.11	2	1.38	.01	.03	1
22+00W 5+75N	1	87	21	217	.1	58	12	720	4.36	2	5	ND	1	39	1	2	2	59	.80	.091	35	59	1.06	252	.05	2	3.10	.01	.07	1
22+00W 5+50N	2	103	15	375	.1	79	21	1227	6.58	7	5	ND	2	40	2	2	2	62	.93	.066	27	53	1.04	219	.21	2	3.20	.03	.07	1
STD C	17	58	43	132	6.8	68	29	1056	4.02	36	16	7	37	47	18	16	20	58	.49	.092	37	56	.91	175	.06	32	2.00	.06	.13	12

ESSO MINERALS CANADA LTD. PROJECT 122-KUTCHO FILE # 88-4699

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM
22+00W 5+25N	1	78	18	259	.2	51	24	1487	4.58	4	5	ND	1	39	2	3	2	63	.50	.081	19	63	1.28	198	.07	3	2.41	.02	.09	1
22+00W 5+00N	1	59	15	182	.1	37	14	687	3.84	2	5	ND	1	25	1	2	2	59	.35	.065	14	54	1.06	137	.06	2	1.37	.01	.06	1
22+00W 4+75N	2	161	22	302	.1	41	14	940	4.92	2	5	ND	1	34	4	2	2	51	1.08	.093	33	39	.65	154	.10	2	2.51	.02	.05	1
22+00W 4+50N	2	24	20	185	.2	19	6	336	4.59	2	5	ND	3	10	1	2	2	51	.12	.042	23	39	.53	94	.16	2	2.42	.02	.08	2
22+00W 4+25N	1	28	9	173	.1	15	10	1309	3.86	2	5	ND	1	8	1	2	2	50	.14	.047	3	29	.58	61	.04	2	1.26	.01	.04	1
22+00W 4+00N	1	38	12	216	.1	53	13	562	4.05	5	5	ND	1	16	1	2	2	79	.38	.026	5	99	2.06	89	.09	2	2.53	.02	.05	1
22+00W 3+75N	3	124	20	360	.5	33	12	571	4.99	10	5	ND	1	15	2	2	2	44	.25	.046	27	40	.47	113	.10	2	2.99	.01	.06	1
STD C	18	56	43	129	6.8	65	28	998	3.97	37	18	7	38	47	17	19	19	58	.47	.088	38	55	.89	170	.07	32	2.02	.06	.15	13
22+00W 3+50N	8	199	17	1042	.3	52	21	908	6.00	2	5	ND	1	15	3	3	2	75	.32	.051	6	96	1.34	78	.10	2	2.57	.01	.04	1
22+00W 3+25N	2	150	19	422	.1	26	17	1698	5.02	2	5	ND	1	32	2	2	2	42	1.58	.082	26	34	.51	133	.07	2	2.55	.01	.05	1
22+00W 3+00N	3	47	19	150	.2	40	19	732	8.61	10	5	ND	2	14	1	3	2	121	.36	.047	10	72	1.22	54	.25	2	2.67	.01	.06	1
RE 22+00W 1+75N	1	63	16	181	.6	44	12	530	4.23	5	5	ND	1	30	1	2	2	58	1.24	.041	11	69	1.31	88	.07	2	2.43	.01	.05	1
22+00W 2+75N	1	27	14	187	.1	44	19	795	5.52	2	5	ND	1	15	1	2	2	97	.36	.044	9	87	1.52	94	.12	2	2.59	.01	.04	1
22+00W 2+50N	1	68	5	160	.1	15	10	641	4.13	2	5	ND	1	19	1	2	2	46	.99	.066	5	20	.34	40	.01	2	.89	.01	.02	1
22+00W 2+25N	1	81	14	224	.4	36	15	983	3.48	2	5	ND	1	40	1	2	2	46	1.45	.089	15	51	.88	123	.04	2	2.13	.01	.03	1
22+00W 2+00N	1	127	12	279	.1	57	19	842	4.38	3	5	ND	1	27	1	2	2	62	.96	.054	15	74	1.50	89	.10	2	2.47	.02	.04	1
22+00W 1+75N	1	61	14	172	.4	42	12	506	4.07	2	5	ND	1	29	1	2	2	55	1.22	.041	12	67	1.25	87	.07	2	2.32	.01	.04	1
22+00W 1+50N	1	307	13	238	.1	45	30	1261	3.03	2	5	ND	1	35	2	2	2	29	2.01	.105	29	34	.50	126	.04	2	2.25	.01	.03	1
22+00W 1+25N	2	16	12	96	.1	20	6	217	3.03	3	5	ND	1	20	1	2	2	73	.41	.017	7	44	.65	101	.21	2	1.36	.01	.05	1
22+00W 1+00N	1	219	17	318	.2	81	17	724	4.57	6	5	ND	1	30	1	2	2	67	.55	.068	18	86	1.47	184	.07	2	3.03	.01	.07	1
22+00W 0+75N	1	124	13	495	.2	74	18	811	4.36	3	5	ND	1	27	2	2	2	58	.63	.054	18	66	-1.13	142	.08	2	2.40	.01	.06	1
22+00W 0+50N	2	35	15	140	.2	36	13	467	4.23	4	5	ND	1	15	2	2	2	69	.28	.038	14	61	.77	108	.21	2	1.74	.01	.05	1
22+00W 0+25N	1	264	13	196	.1	97	29	1046	4.69	2	5	ND	1	31	1	2	2	56	1.22	.061	25	68	.98	136	.10	2	2.54	.01	.05	1
22+00W 0+00N	1	35	13	92	.1	94	33	867	4.88	7	5	ND	1	22	1	2	2	63	1.03	.045	13	189	1.32	82	.13	2	2.31	.01	.03	1
22+00W 0+50S	1	26	8	50	.1	42	10	359	2.77	9	5	ND	1	32	1	2	2	50	.34	.052	11	49	.84	117	.10	2	1.42	.02	.04	1
22+00W 0+75S	1	60	8	68	.1	48	10	601	2.86	8	5	ND	1	26	1	3	2	40	1.07	.045	13	35	.55	107	.05	2	1.60	.01	.05	1
22+00W 1+00S	1	104	9	61	.1	47	13	625	3.22	6	5	ND	1	26	1	2	2	53	.59	.035	14	55	.86	102	.08	2	1.75	.01	.02	1
22+00W 1+25S	1	60	10	65	.1	66	16	704	3.72	3	5	ND	1	29	1	2	2	56	.68	.041	14	68	.95	126	.09	2	1.92	.02	.04	1
22+00W 1+50S	1	36	11	91	.2	63	18	479	4.36	2	5	ND	1	21	1	3	2	61	.70	.042	12	74	.92	110	.09	2	2.09	.01	.05	1
22+00W 1+75S	1	50	11	72	.1	67	15	514	3.72	6	5	ND	1	29	1	2	2	60	.64	.053	13	77	1.01	116	.08	2	1.88	.01	.05	1
22+00W 2+25S	1	58	9	70	.1	82	23	715	4.53	6	5	ND	1	23	1	2	2	59	.49	.050	13	110	1.35	106	.12	3	2.02	.01	.03	1
22+00W 2+50S	1	48	10	61	.1	55	21	459	6.70	11	5	ND	1	12	1	2	2	74	.39	.040	5	87	1.51	54	.15	2	2.52	.01	.01	1
22+00W 2+75S	1	73	2	83	.1	75	22	1257	3.61	2	5	ND	1	26	1	2	2	38	1.64	.072	14	36	.60	103	.09	2	1.96	.02	.01	1
22+00W 3+00S	2	50	14	102	.1	52	24	593	5.01	13	5	ND	1	18	1	2	2	69	.73	.052	9	53	.95	71	.11	2	1.96	.01	.02	1
22+00W 3+25S	1	58	12	100	.1	50	21	1228	5.26	4	5	ND	1	19	1	2	2	58	.73	.056	15	48	.76	124	.13	2	2.31	.01	.04	1
22+00W 3+50S	1	29	13	101	.1	36	15	810	4.49	8	5	ND	1	17	1	2	2	53	.41	.046	15	40	.65	108	.15	2	2.26	.01	.03	1
22+00W 3+75S	1	20	9	73	.1	33	13	405	4.34	16	5	ND	1	11	1	2	2	102	.23	.031	4	62	.91	65	.32	2	1.72	.01	.01	1
22+00W 4+00S	1	23	11	87	.1	44	19	609	4.82	11	5	ND	1	13	1	2	2	81	.39	.019	8	77	1.34	61	.27	2	2.38	.01	.04	1
STD C	18	58	41	132	7.1	68	30	1030	4.17	42	20	6	39	49	18	16	20	60	.50	.093	40	52	.94	182	.07	33	1.95	.06	.15	12

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
22+00W 4+25S P	1	285	12	108	.1	48	15	1285	2.54	17	5	ND	1	46	1	2	3	37	3.04	.160	25	52	.55	122	.03	7	2.14	.04	.04	1
22+00W 4+50S	1	268	35	120	.1	73	15	1038	4.67	12	5	ND	1	31	1	2	2	46	1.56	.079	34	38	.60	156	.18	4	3.33	.03	.04	1
22+00W 4+75S	2	19	19	83	.1	36	11	423	5.45	3	5	ND	3	14	1	2	2	47	.30	.052	13	40	.65	85	.22	2	3.95	.02	.04	1
22+00W 5+00S	2	53	20	114	.1	57	15	957	5.50	6	5	ND	2	29	1	2	2	63	1.11	.081	22	43	.52	166	.27	2	3.59	.02	.04	1
22+00W 5+25S	1	26	13	75	.1	51	15	638	3.94	3	5	ND	1	21	1	2	2	57	.59	.037	8	56	1.20	95	.15	2	2.27	.01	.04	1
22+00W 5+50S	1	37	18	118	.1	46	16	914	5.47	2	5	ND	2	27	1	2	2	57	1.35	.081	22	34	1.00	125	.33	2	3.94	.03	.03	1
STD C	18	56	41	128	6.6	65	27	1001	3.90	42	19	6	38	45	17	17	20	54	.46	.085	36	55	.87	161	.06	32	1.97	.06	.14	12
22+00W 5+75S	2	25	19	104	.1	22	8	557	5.38	4	5	ND	1	7	1	2	2	51	.12	.045	16	41	.40	63	.19	2	2.31	.01	.03	1
22+00W 6+00S P	1	25	18	93	.1	128	21	795	4.51	7	5	ND	1	17	1	2	3	64	.24	.057	9	152	1.71	88	.08	3	2.65	.02	.07	1
22+00W 6+50S	1	33	16	76	.1	73	13	455	3.55	3	5	ND	1	29	1	2	2	49	.49	.068	9	64	1.11	148	.05	2	2.19	.01	.06	1
22+00W 6+75S	1	38	13	84	.1	78	11	584	3.19	5	5	ND	1	30	1	3	2	50	.49	.069	14	59	1.02	119	.06	3	1.93	.01	.06	1
22+00W 7+00S	1	37	11	66	.1	65	11	495	2.95	10	5	ND	1	51	1	2	2	46	.80	.060	10	54	.97	189	.07	4	1.65	.01	.06	1
22+00W 7+25S P	1	43	15	81	.1	71	14	690	3.35	13	5	ND	2	52	1	3	2	52	.82	.060	12	62	1.10	184	.09	5	1.86	.02	.09	1
22+00W 7+50S	1	59	15	81	.1	86	13	561	2.98	11	5	ND	1	54	1	2	2	41	1.30	.064	12	66	.93	232	.05	4	1.94	.01	.07	1
22+00W 7+75S	1	42	13	71	.1	67	12	547	3.11	11	5	ND	1	49	1	2	2	43	1.08	.069	11	56	.95	190	.05	2	1.86	.01	.05	1
22+00W 8+00S	1	40	11	94	.1	75	12	696	3.25	8	5	ND	1	39	1	2	2	45	.84	.066	10	67	1.09	149	.06	3	1.76	.01	.06	1
22+00W 8+25S	1	47	12	80	.1	65	13	1022	3.08	4	5	ND	1	39	1	2	3	40	1.08	.078	12	58	.92	162	.04	5	1.82	.01	.05	1
22+00W 8+50S	1	33	11	69	.1	61	11	528	2.88	3	5	ND	1	36	1	3	2	43	.67	.052	10	59	1.00	138	.07	3	1.59	.01	.05	1
RE 20+00W 6+75N	1	25	15	89	.2	31	7	288	2.84	5	5	ND	1	34	1	2	3	46	.41	.049	14	39	.69	212	.04	2	2.11	.01	.06	1
22+00W 8+75S	1	40	14	81	.1	82	14	455	3.13	5	5	ND	1	40	1	2	3	47	.59	.056	11	61	1.12	153	.09	3	1.76	.01	.06	1
22+00W 9+00S	1	49	12	68	.1	92	24	928	3.73	13	5	ND	2	32	1	3	2	57	.35	.059	10	81	1.25	130	.11	4	1.77	.01	.06	1
20+00W 7+00N	1	20	13	83	.1	31	7	371	2.47	2	5	ND	1	36	1	2	2	43	.47	.031	10	36	.74	151	.07	3	1.36	.01	.05	1
20+00W 6+75N	1	27	15	96	.2	32	8	294	2.94	4	5	ND	1	36	1	2	2	48	.44	.051	15	40	.72	225	.04	2	2.21	.01	.06	1
20+00W 6+25N P	1	47	16	161	.3	42	8	383	3.26	10	5	ND	1	38	1	2	2	42	.97	.079	18	37	.67	248	.03	2	2.44	.01	.08	1
20+00W 6+00N P	1	47	18	211	.1	49	17	995	4.40	4	5	ND	1	37	1	2	2	59	.88	.071	15	55	1.17	214	.04	2	2.64	.01	.09	1
20+00W 5+75N P	1	58	15	205	.3	35	6	265	2.29	3	5	ND	1	62	1	2	2	31	1.92	.101	21	32	.57	299	.02	2	2.09	.01	.07	1
20+00W 5+50N P	1	35	13	190	.1	36	8	453	2.98	6	5	ND	1	33	1	2	3	46	.83	.045	9	44	.88	152	.05	2	1.74	.02	.07	1
20+00W 5+25N P	1	71	17	138	.2	53	10	632	3.49	10	5	ND	1	39	1	2	2	44	1.14	.066	26	46	.83	253	.04	2	2.27	.02	.09	1
20+00W 5+00N	1	44	15	216	.2	39	11	718	3.27	6	5	ND	1	33	1	2	2	49	.60	.078	10	47	.84	206	.04	2	2.16	.01	.06	1
20+00W 4+75N	1	25	14	85	.1	35	7	314	2.81	2	5	ND	1	25	1	2	2	48	.26	.048	9	47	.88	102	.09	2	1.75	.01	.04	1
20+00W 4+50N	2	66	18	279	.1	56	13	539	5.12	3	5	ND	2	21	1	2	2	61	.30	.055	18	48	.88	195	.18	2	2.96	.02	.05	1
20+00W 4+25N	2	88	21	304	.1	40	22	1023	6.70	7	5	ND	1	14	1	3	2	59	.16	.071	12	55	.94	92	.07	2	2.18	.01	.05	1
20+00W 4+00N	1	79	17	478	.1	43	20	682	4.25	4	5	ND	2	20	1	2	2	58	.26	.033	9	59	1.07	119	.06	2	2.31	.01	.05	1
20+00W 3+75N	1	80	14	326	.2	36	14	855	3.62	8	5	ND	1	29	2	2	2	44	1.01	.056	13	42	.76	126	.08	2	2.01	.01	.04	1
20+00W 3+50N	1	176	16	317	.3	88	29	1061	6.04	10	5	ND	2	35	1	2	2	62	1.04	.045	15	58	1.45	170	.18	2	2.53	.02	.06	1
20+00W 3+25N	1	128	15	143	.1	38	17	1551	4.68	4	5	ND	1	28	1	2	3	39	1.41	.077	21	28	.53	120	.13	2	2.48	.02	.04	1
20+00W 3+00N	1	122	18	277	.1	66	27	1829	6.09	2	5	ND	3	24	2	2	2	64	.81	.045	19	45	.86	87	.30	2	3.51	.02	.05	1
20+00W 2+50N	1	86	15	559	.1	51	21	1394	5.22	3	5	ND	1	22	1	2	3	67	.72	.035	12	65	1.15	92	.08	2	2.30	.01	.04	1
STD C	18	57	43	132	6.6	67	29	1032	4.02	37	20	6	36	47	17	16	21	57	.50	.089	37	55	.92	175	.06	32	2.02	.06	.13	11

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM
20+00W 2+25N	1	301	14	303	.1	105	21	937	5.66	3	5	ND	2	30	1	2	2
20+00W 2+00N	2	62	16	222	.2	20	10	1073	4.44	2	5	ND	1	26	1	2	2
20+00W 1+75N	1	66	9	233	.1	70	14	685	4.96	9	5	ND	1	11	1	3	2
20+00W 1+50N	3	258	11	455	.1	59	20	810	4.54	7	5	ND	1	16	1	2	2
20+00W 1+25N	2	97	14	174	.4	30	8	332	2.90	5	5	ND	1	18	1	3	2
20+00W 1+00N	1	447	44	1358	.3	56	31	1500	4.41	4	5	ND	1	32	5	2	2
20+00W 0+75N	1	72	18	128	.1	71	10	595	3.97	9	5	ND	1	35	1	2	2
20+00W 0+50N	1	59	14	602	.1	40	7	501	3.51	5	5	ND	1	27	1	2	2
20+00W 0+25N	1	326	12	353	.1	105	25	900	3.61	24	5	ND	1	37	1	2	2
RE 18+00W 7+00N	1	34	13	101	.1	43	7	402	2.51	5	5	ND	1	52	1	3	2
20+00W 0+00N	2	149	13	181	.1	111	16	864	4.50	12	5	ND	1	37	1	2	2
20+00W 8+25S	1	25	11	98	.1	32	16	837	3.06	2	5	ND	1	23	1	2	3
20+00W 8+50S	1	40	8	90	.2	45	12	554	3.26	7	5	ND	1	29	1	3	3
20+00W 9+00S	1	57	5	80	.1	49	16	622	3.36	10	5	ND	1	32	1	3	2
18+00W 7+00N	1	32	13	96	.1	41	8	423	2.63	3	5	ND	1	57	1	2	2
18+00W 6+75N	2	44	16	112	.1	45	13	881	4.01	9	5	ND	1	32	1	2	2
STD C	18	55	40	132	6.7	69	30	1001	3.97	38	19	8	36	48	18	17	20
18+00W 6+50N	2	48	17	137	.2	56	13	730	4.53	4	5	ND	2	44	1	2	2
18+00W 6+25N	1	22	11	73	.1	35	7	368	2.66	6	5	ND	1	43	1	2	3
18+00W 6+00N P	1	29	15	143	.1	53	13	726	4.08	8	5	ND	2	57	1	2	2
18+00W 5+75N	1	24	10	94	.1	39	10	475	3.18	2	5	ND	1	35	1	2	2
18+00W 5+50N	1	49	15	104	.1	49	10	747	4.05	8	5	ND	1	43	1	2	2
18+00W 5+00N	1	14	15	89	.3	21	5	221	2.55	4	5	ND	1	26	1	2	2
18+00W 4+50N P	1	39	14	289	.1	44	15	762	3.84	10	5	ND	1	25	1	2	2
18+00W 4+25N	1	37	10	325	.1	43	8	431	2.91	9	5	ND	1	39	1	2	2
18+00W 4+00N P	1	302	12	663	.1	84	13	992	3.93	10	5	ND	1	41	4	2	2
18+00W 3+75N	1	17	12	120	.1	25	6	320	2.42	4	5	ND	1	30	1	2	2
18+00W 3+50N	1	26	11	162	.1	19	7	613	2.59	4	5	ND	1	20	2	2	2
18+00W 3+25N	2	27	20	291	.1	27	12	1370	4.79	5	5	ND	1	34	1	2	2
18+00W 3+00N	2	10	19	63	.1	14	3	279	2.37	4	5	ND	1	8	1	2	3
18+00W 2+75N	1	97	18	256	.1	50	17	1546	5.41	5	5	ND	1	39	1	2	2
18+00W 2+50N	2	26	19	149	.1	29	8	398	5.57	2	5	ND	2	11	1	2	2
18+00W 2+25N	11	197	59	463	.1	52	23	1799	10.44	33	5	ND	1	17	3	3	2
18+00W 2+00N	5	30	10	96	.1	13	6	330	6.24	2	5	ND	1	5	1	2	2
18+00W 1+75N	3	58	14	276	.4	32	8	383	5.82	7	5	ND	1	11	1	2	2
18+00W 1+50N	2	53	18	373	.1	63	10	522	5.62	6	5	ND	1	9	1	2	2
18+00W 1+25N	1	24	14	395	.1	55	12	451	4.49	7	5	ND	2	18	1	2	3
18+00W 1+00N	4	13	15	83	.1	22	3	274	7.80	18	5	ND	2	6	1	3	3
STD C	17	58	41	132	6.8	68	29	1014	3.95	38	16	8	36	45	18	16	21

SAMPLE#	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
20+00W 2+25N	64	1.12	.046	21	66	1.45	160	.24	2	3.12	.02	.06	1
20+00W 2+00N	34	1.61	.072	16	23	.36	92	.07	2	1.37	.01	.03	1
20+00W 1+75N	83	.18	.028	5	127	2.32	66	.05	2	2.98	.01	.03	1
20+00W 1+50N	74	.44	.032	6	90	1.62	118	.08	2	2.62	.01	.04	1
20+00W 1+25N	59	.26	.039	10	50	.66	130	.06	2	1.95	.01	.05	1
20+00W 1+00N	38	1.55	.092	30	43	.55	155	.04	2	3.00	.01	.05	1
20+00W 0+75N	39	.96	.053	29	39	.70	171	.08	2	2.32	.02	.06	1
20+00W 0+50N	41	.80	.035	30	36	.60	149	.08	2	2.19	.01	.05	1
20+00W 0+25N	40	1.49	.067	39	40	.69	160	.05	2	2.14	.01	.06	1
RE 18+00W 7+00N	39	.96	.080	18	35	.61	274	.03	2	2.08	.01	.07	2
20+00W 0+00N	50	1.76	.095	28	47	.54	196	.12	3	3.24	.02	.06	1
20+00W 8+25S	55	.41	.100	7	54	.88	110	.05	2	1.79	.01	.05	1
20+00W 8+50S	49	.48	.095	11	56	.78	163	.04	2	1.87	.01	.05	1
20+00W 9+00S	51	.49	.059	10	55	1.00	105	.13	3	1.52	.01	.06	1
18+00W 7+00N	40	.98	.084	18	34	.64	281	.03	2	2.14	.01	.07	2
18+00W 6+75N	61	.32	.109	22	44	.69	370	.03	2	3.35	.01	.09	2
STD C	59	.49	.093	37	53	.87	171	.07	32	1.94	.06	.14	11
18+00W 6+50N	67	.67	.072	17	48	.35	335	.02	2	3.83	.01	.14	1
18+00W 6+25N	46	.51	.050	15	33	.64	208	.05	2	1.77	.01	.07	2
18+00W 6+00N P	62	.95	.075	18	51	.83	332	.03	2	3.15	.01	.11	1
18+00W 5+75N	51	.53	.045	15	33	.65	221	.05	3	2.27	.01	.08	1
18+00W 5+50N	59	1.36	.163	27	40	.66	349	.02	2	3.47	.01	.09	1
18+00W 5+00N	56	.45	.032	11	26	.44	154	.04	2	1.80	.01	.07	2
18+00W 4+50N P	64	.66	.049	10	53	1.18	148	.05	4	2.18	.01	.08	1
18+00W 4+25N	51	.60	.030	14	35	.68	185	.07	3	1.95	.01	.07	1
18+00W 4+00N P	47	1.66	.146	28	48	.70	326	.02	3	3.70	.01	.09	1
18+00W 3+75N	51	.63	.040	10	33	.53	177	.05	2	1.60	.01	.05	1
18+00W 3+50N	50	.26	.064	12	31	.34	210	.06	3	1.39	.01	.05	1
18+00W 3+25N	74	.87	.121	13	34	.49	179	.08	2	1.90	.01	.06	1
18+00W 3+00N	74	.08	.033	11	42	.69	78	.17	2	1.32	.01	.03	1
18+00W 2+75N	36	1.58	.089	29	30	.54	163	.11	2	3.27	.02	.05	1
18+00W 2+50N	82	.16	.032	15	40	.67	60	.20	2	2.23	.01	.05	1
18+00W 2+25N	46	.53	.093	19	33	.61	78	.06	2	2.90	.01	.04	1
18+00W 2+00N	61	.06	.028	9	30	.60	41	.08	2	1.73	.01	.03	1
18+00W 1+75N	77	.11	.039	8	56	.84	87	.09	2	2.87	.01	.04	1
18+00W 1+50N	48	.09	.067	37	43	.58	153	.04	2	4.44	.01	.06	1
18+00W 1+25N	59	.33	.020	10	56	.99	116	.08	2	2.77	.01	.06	1
18+00W 1+00N	87	.07	.056	8	61	.63	51	.19	3	2.16	.01	.04	1
STD C	58	.47	.094	37	56	.86	176	.06	33	1.97	.06	.14	11

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
18+00W 0+75N	2	46	19	114	.1	101	36	592	6.28	26	5	ND	3	11	1	2	2	82	.16	.047	17	72	.95	117	.16	3	4.79	.01	.04	1
18+00W 0+50N	2	9	16	64	.1	18	5	193	2.94	6	5	ND	2	23	1	2	2	73	.66	.013	10	43	.49	140	.10	2	1.58	.01	.05	2
18+00W 0+25N	1	40	11	94	.1	74	11	504	3.30	11	5	ND	1	27	1	2	2	58	.49	.030	9	52	.84	209	.06	3	2.78	.01	.06	1
18+00W 0+00N	1	22	12	67	.1	40	10	505	3.33	6	5	ND	1	28	1	2	3	56	.37	.037	11	44	.78	159	.06	2	2.08	.01	.07	1
18+00W 0+00S	1	26	13	66	.1	46	11	495	3.38	8	5	ND	1	34	1	2	2	56	.45	.049	12	47	.84	141	.06	3	2.14	.01	.06	2
18+00W 0+25S	2	102	13	170	.1	102	14	487	4.26	16	5	ND	2	29	1	2	2	40	1.45	.085	23	35	.52	167	.08	3	2.93	.01	.05	1
18+00W 0+50S	1	115	9	81	.1	43	8	1380	2.83	9	5	ND	1	35	1	2	2	24	2.95	.139	19	18	.20	135	.03	2	1.78	.01	.03	2
18+00W 0+75S	3	27	20	161	.4	43	16	1148	6.39	7	5	ND	1	14	1	2	2	57	.63	.058	18	34	.52	125	.09	2	3.61	.01	.06	1
18+00W 1+00S	1	14	12	73	.1	27	7	303	4.18	9	5	ND	1	25	1	2	2	68	.36	.021	8	37	.60	143	.07	2	2.30	.01	.04	1
STD C	18	59	42	136	6.9	68	30	1020	4.25	45	19	7	37	46	19	17	21	60	.53	.098	38	53	.93	169	.06	32	1.95	.06	.14	13
18+00W 1+50S	1	42	8	78	.2	47	21	440	9.97	12	5	ND	2	6	1	2	2	90	.30	.034	2	128	1.66	12	.63	2	2.49	.01	.01	1
18+00W 1+75S	1	30	13	67	.1	52	12	379	3.80	10	5	ND	2	28	1	2	2	71	.31	.016	9	55	.92	161	.09	2	2.85	.01	.05	1
18+00W 2+00S	1	38	2	67	.1	13	2	131	.26	2	5	ND	1	57	1	2	2	4	4.51	.051	2	3	.05	77	.01	3	.22	.01	.02	2
18+00W 2+50S	2	32	7	86	.1	66	25	511	6.40	21	5	ND	1	7	1	2	2	112	.36	.031	2	104	1.19	40	.51	2	2.04	.01	.01	1
18+00W 2+75S	1	147	15	80	.1	70	11	541	4.13	41	5	ND	2	30	1	2	2	51	1.08	.036	21	38	.74	101	.11	2	2.78	.02	.06	1
18+00W 3+00S	1	47	20	108	.1	52	14	867	5.05	39	5	ND	4	18	1	2	2	66	.70	.029	17	44	.66	134	.16	2	3.10	.01	.06	1
18+00W 3+50S	1	67	12	92	.1	44	11	513	3.51	10	5	ND	1	31	1	2	2	53	.97	.044	13	47	.72	117	.07	2	2.33	.01	.04	1
18+00W 3+75S	1	13	8	49	.1	29	8	441	2.62	5	5	ND	1	20	1	2	2	52	.43	.019	8	44	.72	120	.08	2	1.85	.01	.03	2
18+00W 4+00S	1	11	11	50	.1	24	7	241	2.61	4	5	ND	1	21	1	2	2	52	.31	.019	8	40	.57	135	.09	2	1.60	.01	.03	2
18+00W 4+25S	1	93	10	117	.1	26	8	958	3.10	6	5	ND	1	31	1	2	2	41	1.96	.092	13	34	.52	126	.03	2	1.66	.01	.03	1
18+00W 4+50S	1	34	11	158	.1	38	10	706	3.84	7	5	ND	1	24	1	2	2	49	.87	.070	13	46	.75	121	.09	2	2.24	.01	.08	1
18+00W 4+75S	1	32	12	110	.1	38	16	883	3.77	9	5	ND	1	25	1	2	2	51	.72	.060	11	58	.87	112	.09	2	2.04	.01	.04	1
18+00W 5+00S	1	19	8	53	.1	43	11	430	2.85	8	5	ND	1	22	1	2	2	51	.35	.026	7	50	.78	66	.08	2	1.44	.01	.03	1
RE 18+00W 4+25S	1	93	10	117	.1	28	9	1010	3.12	7	5	ND	2	30	1	2	2	40	2.00	.095	13	35	.51	127	.03	2	1.66	.01	.02	1
18+00W 5+75S	1	41	4	73	.1	19	6	545	1.36	2	5	ND	1	72	1	2	2	17	4.86	.081	7	22	.36	127	.01	5	.85	.01	.02	1
18+00W 6+25S	1	14	13	75	.1	18	7	384	3.26	9	5	ND	1	15	1	2	2	73	.29	.054	9	38	.43	120	.13	2	1.26	.01	.05	1
18+00W 6+50S	1	21	15	110	.1	49	11	523	4.80	12	5	ND	1	17	1	2	2	77	.22	.063	6	71	.87	114	.09	2	1.89	.01	.05	2
18+00W 6+75S	1	27	11	177	.1	79	14	639	4.72	7	5	ND	1	26	1	2	2	59	.41	.096	9	119	1.18	167	.04	3	2.32	.01	.07	1
18+00W 7+00S	1	25	19	189	.1	63	13	542	5.50	12	5	ND	1	20	1	2	2	83	.36	.074	6	108	1.03	153	.11	2	1.91	.01	.06	1
18+00W 7+25S	1	24	17	124	.1	102	17	913	6.10	13	5	ND	1	19	1	2	2	72	.32	.070	9	148	.87	194	.07	2	2.26	.01	.06	1
18+00W 7+50S	1	67	2	91	.1	32	4	381	.64	2	5	ND	1	53	1	2	2	9	3.05	.094	4	16	.17	113	.01	5	.40	.01	.02	2
18+00W 7+75S	1	15	5	78	.1	54	26	690	5.83	22	5	ND	1	10	1	2	2	89	.44	.041	2	103	.91	19	.64	2	2.21	.01	.01	1
18+00W 8+00S	2	19	17	63	.1	36	11	352	4.73	12	5	ND	1	20	1	2	2	67	.73	.038	8	59	.63	85	.16	2	2.48	.01	.03	2
16+00W 11+75N	1	69	7	92	.2	39	6	516	1.85	2	5	ND	1	71	1	2	2	17	2.52	.157	14	21	.50	257	.01	4	1.32	.01	.03	2
16+00W 11+50N	1	91	9	136	.1	52	9	643	2.48	6	5	ND	1	53	1	2	2	30	1.58	.114	27	38	.63	284	.01	3	1.83	.01	.03	1
16+00W 11+25N	1	157	4	59	.1	49	5	346	1.51	2	5	ND	1	66	1	2	2	15	1.99	.147	34	23	.30	250	.01	3	1.47	.01	.02	1
16+00W 10+75N	1	22	10	62	.1	51	10	379	3.55	9	5	ND	1	16	1	2	2	59	.31	.048	8	65	1.07	80	.12	3	2.40	.01	.02	1
16+00W 10+50N	2	14	15	81	.2	35	9	360	4.96	6	5	ND	2	10	1	2	2	76	.16	.039	8	62	.97	59	.15	2	2.42	.01	.04	2
STD C	17	58	42	132	6.6	68	29	1021	4.12	44	17	7	37	47	18	17	19	58	.51	.094	37	56	.90	171	.06	33	2.03	.06	.14	12

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
16+00W 9+75N	3	13	22	103	.2	18	4	342	4.77	6	5	ND	3	9	1	2	3	82	.09	.044	21	40	.31	65	.24	2	1.90	.01	.06	1
16+00W 9+50N	1	26	9	96	.1	30	11	519	3.49	4	5	ND	1	21	1	2	2	63	.52	.048	6	52	1.23	79	.16	2	1.80	.01	.05	1
16+00W 9+25N	2	96	18	298	.1	44	12	731	5.30	2	5	ND	2	34	2	2	2	67	.68	.089	18	50	.72	180	.25	2	2.35	.02	.05	1
16+00W 9+00N	2	355	19	1020	.1	82	22	835	5.62	12	5	ND	1	27	2	2	2	66	.48	.170	20	90	1.29	250	.02	2	4.44	.01	.07	1
RE 16+00W 7+50N	1	28	12	73	.1	37	7	210	2.54	3	5	ND	1	54	1	3	2	38	1.25	.087	19	45	.66	246	.04	2	1.78	.01	.05	1
16+00W 8+75N	2	90	21	749	.1	61	29	1264	6.99	11	5	ND	1	10	1	2	2	85	.19	.046	5	123	2.62	58	.11	2	3.16	.01	.03	1
16+00W 8+25N	1	29	13	143	.1	57	15	573	4.62	7	5	ND	1	21	1	3	2	62	.42	.039	8	74	1.02	112	.08	2	1.83	.01	.04	1
16+00W 8+00N	1	34	6	91	.1	51	9	469	2.29	2	5	ND	1	72	1	2	2	29	2.30	.107	15	47	.70	313	.02	5	1.78	.01	.05	1
16+00W 7+75N	1	24	8	56	.3	36	12	846	2.26	4	5	ND	1	75	1	2	2	34	2.50	.122	10	40	.56	286	.02	2	1.63	.01	.04	1
16+00W 7+50N	1	26	12	65	.1	37	7	209	2.51	3	5	ND	1	56	1	3	2	37	1.24	.086	19	44	.65	251	.04	2	1.80	.01	.05	1
16+00W 7+25N	2	7	14	43	.1	11	3	122	1.67	2	5	ND	1	16	1	2	2	61	.13	.026	10	30	.23	64	.23	2	.94	.01	.04	2
16+00W 6+25N	1	36	12	55	.1	63	13	518	3.09	6	5	ND	1	23	1	2	2	53	.30	.041	10	60	1.02	130	.10	2	1.93	.01	.05	1
16+00W 6+00N	1	14	13	57	.1	23	6	305	3.12	4	5	ND	2	15	1	2	2	53	.08	.031	11	27	.42	114	.06	2	1.98	.01	.05	1
16+00W 5+75N	1	23	15	78	.1	35	9	359	3.53	5	5	ND	2	18	1	2	2	54	.13	.037	11	38	.62	139	.05	2	2.97	.01	.07	1
16+00W 5+50N	2	21	19	76	.1	25	6	374	4.25	9	5	ND	2	12	1	2	2	76	.07	.052	12	36	.49	111	.04	2	3.08	.01	.09	1
16+00W 5+25N	1	26	14	72	.1	41	12	507	3.07	9	5	ND	2	21	1	3	2	48	.14	.031	12	35	.67	144	.05	2	2.61	.01	.07	1
16+00W 5+00N	1	19	12	49	.1	26	5	217	2.29	8	5	ND	1	25	1	2	2	46	.16	.037	10	35	.48	160	.04	2	2.09	.01	.06	1
16+00W 4+75N	1	19	11	51	.1	33	8	447	2.50	4	5	ND	2	38	1	2	2	48	.36	.047	13	43	.72	147	.09	2	1.43	.01	.05	1
16+00W 4+50N	1	49	17	105	.3	58	9	319	4.12	5	5	ND	1	30	1	2	2	62	.23	.112	11	60	.82	313	.01	2	4.69	.01	.10	1
16+00W 4+25N	1	22	14	85	.1	33	8	324	3.52	6	5	ND	1	20	1	2	2	55	.15	.030	10	37	.59	148	.03	2	2.47	.01	.07	1
16+00W 4+00N	1	36	12	83	.1	47	8	414	3.09	6	5	ND	1	25	1	2	2	45	.56	.077	16	37	.59	200	.03	2	2.59	.01	.06	1
16+00W 3+75N	1	19	12	58	.1	36	7	413	2.51	4	5	ND	2	27	1	2	2	38	.53	.023	13	27	.51	152	.07	2	1.78	.01	.06	1
16+00W 3+50N	1	21	13	70	.1	51	11	547	2.96	4	5	ND	2	34	1	2	2	45	.65	.030	14	43	.86	182	.05	2	1.72	.01	.06	1
16+00W 3+25N	1	19	12	63	.1	38	7	353	2.64	9	5	ND	1	29	1	2	2	44	.45	.034	15	32	.65	183	.04	2	2.16	.01	.06	1
16+00W 3+00N	1	16	12	75	.2	30	7	280	3.14	2	5	ND	1	20	1	2	2	52	.20	.031	9	32	.57	161	.03	2	2.07	.01	.06	1
16+00W 2+75N	1	24	18	100	.1	34	8	435	4.75	5	5	ND	1	12	1	2	2	70	.08	.042	10	40	.63	107	.03	2	3.11	.01	.09	1
16+00W 2+50N	1	20	11	77	.1	34	8	406	3.33	2	5	ND	1	19	1	2	2	60	.14	.043	9	42	.65	124	.05	2	1.92	.01	.08	1
16+00W 2+25N	1	24	17	90	.1	38	9	425	4.30	9	5	ND	2	17	1	3	2	62	.11	.040	12	40	.70	126	.06	2	2.88	.01	.07	1
16+00W 2+00N	1	12	14	37	.2	9	3	103	2.02	2	5	ND	1	13	1	2	2	39	.06	.049	12	24	.19	89	.03	2	2.00	.01	.05	2
16+00W 1+75N	1	40	17	121	.1	42	10	494	4.31	6	5	ND	1	15	1	3	2	67	.11	.048	16	42	.62	187	.02	2	3.74	.01	.09	1
16+00W 1+50N	1	17	9	128	.1	38	13	689	4.06	5	5	ND	2	14	1	2	2	62	.48	.031	9	90	1.33	96	.13	3	2.28	.01	.05	1
16+00W 1+25N	1	10	13	48	.1	13	3	142	1.97	2	5	ND	1	17	1	3	2	61	.16	.013	8	23	.27	123	.04	2	1.51	.01	.06	2
16+00W 1+00N	3	41	13	89	.1	51	9	741	3.70	5	5	ND	1	32	1	2	2	44	1.33	.081	19	36	.60	224	.04	3	2.53	.01	.07	1
16+00W 0+75N	2	169	13	104	.1	138	14	563	3.93	52	5	ND	1	34	1	2	2	50	1.08	.067	19	47	.74	218	.04	2	3.05	.01	.07	1
STD C	18	57	40	128	6.7	66	29	981	4.03	37	18	8	37	45	18	18	17	57	.49	.092	38	53	.90	165	.06	32	1.96	.06	.14	13
16+00W 0+50N	5	28	14	133	.1	34	8	400	3.44	11	5	ND	1	22	1	2	2	49	.78	.045	15	37	.57	139	.07	7	2.11	.01	.05	1
16+00W 0+25N	7	21	13	121	.2	28	15	661	6.17	4	5	ND	2	16	1	3	2	84	.63	.032	6	40	1.28	114	.15	2	2.37	.01	.05	1
16+00W 0+00N	3	49	19	141	.1	58	12	707	5.14	14	5	ND	1	23	1	3	2	49	.81	.076	29	33	.57	191	.11	2	3.95	.01	.06	1
STD C	17	58	41	132	7.0	66	30	1027	4.13	41	18	7	36	47	18	17	19	59	.50	.095	38	52	.93	171	.07	33	2.02	.06	.13	12

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
16+00W 0+00S	2	41	15	116	.1	51	11	477	4.71	13	5	ND	3	22	1	2	2	48	.82	.074	24	33	.50	192	.08	2	3.25	.01	.05	1
16+00W 0+25S	1	95	15	132	.1	106	11	594	4.34	17	5	ND	3	23	1	2	2	45	.92	.061	26	36	.60	138	.07	2	2.98	.01	.06	1
16+00W 0+50S	1	73	13	112	.1	61	11	1150	3.74	9	5	ND	2	28	1	3	2	33	1.38	.095	24	33	.47	201	.04	2	2.45	.01	.05	1
16+00W 0+75S	1	197	13	106	.1	251	29	699	5.37	13	5	ND	6	20	1	2	2	44	.37	.055	26	41	.39	191	.09	2	3.52	.01	.07	1
16+00W 1+00S	1	137	11	102	.1	71	15	789	3.60	14	5	ND	2	32	1	2	2	29	2.36	.114	25	34	.50	116	.02	2	2.55	.01	.05	1
16+00W 1+25S	2	169	17	106	.1	57	14	705	4.39	25	5	ND	2	22	1	3	2	41	.81	.107	26	35	.46	133	.02	2	2.75	.01	.06	1
16+00W 1+50S	1	108	16	130	.1	54	10	1037	4.13	19	5	ND	2	24	1	2	2	37	.92	.099	20	31	.46	202	.02	2	2.67	.01	.06	1
16+00W 1+75S	1	17	10	75	.1	30	8	302	2.95	10	5	ND	2	19	1	2	2	63	.30	.012	9	33	.63	127	.06	2	2.19	.01	.05	1
16+00W 2+00S	1	55	18	159	.1	57	11	545	4.84	27	5	ND	1	19	1	2	3	67	.81	.037	16	42	.67	199	.06	2	3.32	.01	.08	1
16+00W 2+25S	1	24	13	43	.1	14	4	98	1.44	2	5	ND	1	13	1	3	2	41	.45	.036	9	25	.22	110	.11	2	.34	.01	.03	2
16+00W 2+50S	2	31	13	131	.1	53	21	673	4.91	21	5	ND	2	15	1	2	2	74	.62	.033	12	57	1.03	110	.15	2	2.74	.01	.05	1
16+00W 2+75S	1	17	9	76	.1	26	11	448	3.45	2	5	ND	1	13	1	2	2	93	.83	.037	6	56	.85	87	.30	2	1.52	.01	.03	1
16+00W 3+25S	1	30	30	111	.1	25	12	566	3.73	5	5	ND	1	15	1	2	2	82	.73	.049	11	47	.62	143	.18	2	1.97	.01	.04	1
16+00W 3+50S	1	24	13	112	.1	28	14	747	3.61	4	5	ND	1	18	1	2	2	71	.64	.045	9	41	.57	125	.09	2	1.86	.01	.07	1
16+00W 3+75S	1	21	11	80	.1	36	8	346	2.96	10	5	ND	1	31	1	2	2	58	.32	.031	9	37	.64	182	.05	3	1.94	.01	.08	1
16+00W 4+00S	1	16	12	63	.1	30	7	290	2.68	8	5	ND	1	31	1	2	2	52	.24	.026	9	32	.57	162	.05	2	1.69	.01	.07	1
16+00W 4+25S P	1	22	13	79	.1	36	9	471	2.78	9	5	ND	1	36	1	2	2	52	.44	.047	10	35	.67	168	.06	3	1.59	.01	.10	1
16+00W 4+50S	1	25	12	80	.1	46	12	515	3.24	15	5	ND	1	35	1	2	2	56	.42	.041	11	47	.85	171	.07	2	2.06	.01	.09	1
16+00W 4+75S	1	41	10	94	.1	49	11	689	3.09	9	5	ND	1	42	1	2	2	50	1.58	.077	12	43	.71	248	.03	3	2.20	.01	.10	1
16+00W 5+00S	1	23	8	92	.1	37	9	550	2.64	7	5	ND	1	32	1	2	2	46	.96	.056	8	47	.67	176	.04	2	1.74	.01	.09	1
16+00W 5+25S	1	48	11	86	.1	44	11	420	3.16	10	5	ND	1	32	1	2	2	55	1.17	.073	14	51	.77	114	.02	4	1.66	.01	.06	1
16+00W 5+50S P	1	16	2	45	.1	8	2	48	.46	2	5	ND	1	73	1	3	2	6	4.73	.063	3	7	.07	103	.01	4	.34	.01	.02	2
RE 16+00W 4+75S	1	40	11	93	.1	48	11	689	3.07	11	5	ND	1	42	1	3	2	50	1.62	.077	12	42	.71	244	.03	3	2.19	.01	.10	1
16+00W 5+75S	1	36	8	95	.1	35	7	438	2.22	9	5	ND	1	59	1	2	2	33	2.92	.083	11	32	.53	216	.01	3	1.60	.01	.05	1
STD C	17	58	41	128	6.7	67	29	983	4.07	41	18	7	36	45	18	17	18	58	.50	.092	36	55	.86	162	.07	32	1.96	.06	.14	13
16+00W 6+00S	1	30	13	90	.1	41	9	878	2.50	5	5	ND	2	51	1	3	2	37	1.60	.062	12	36	.63	220	.02	3	1.56	.01	.06	1
16+00W 6+25S	1	15	13	82	.1	40	9	365	3.86	9	5	ND	1	21	1	2	2	62	.27	.040	9	56	.81	142	.11	6	1.74	.01	.05	1
16+00W 6+75S	1	23	8	59	.1	48	10	381	3.01	6	5	ND	1	26	1	2	2	47	.32	.034	10	54	.81	125	.09	2	1.71	.01	.04	1
16+00W 7+00S	1	10	9	53	.1	18	6	242	2.37	6	5	ND	1	15	1	3	3	54	.19	.024	8	43	.39	116	.12	2	1.19	.01	.04	1
16+00W 7+25S	1	37	7	96	.1	77	40	997	6.38	9	5	ND	1	14	1	2	2	89	.37	.061	3	87	1.09	73	.35	2	1.89	.01	.03	1
16+00W 7+50S	1	24	16	94	.1	55	16	680	4.15	9	5	ND	2	25	1	2	2	66	.52	.041	8	68	1.03	132	.12	3	1.79	.01	.06	1
16+00W 7+75S	1	21	7	69	.1	62	16	692	3.43	7	5	ND	1	23	1	2	2	56	.41	.038	7	76	1.04	79	.10	2	1.40	.01	.06	1
16+00W 8+00S	1	19	14	94	.2	39	20	1468	4.15	10	5	ND	1	19	1	2	2	63	.34	.043	8	65	.86	113	.10	2	1.76	.01	.06	1
16+00W 8+25S	2	81	17	129	.1	78	14	969	5.25	13	5	ND	1	35	1	2	2	62	.88	.106	35	77	.69	217	.10	2	3.11	.01	.06	1
16+00W 8+75S	1	30	15	95	.1	49	12	968	5.43	11	5	ND	2	84	1	3	3	70	.89	.078	26	48	.71	333	.24	3	3.43	.02	.05	1
16+00W 9+00S	1	43	13	104	.1	52	10	650	3.64	10	5	ND	1	50	1	2	2	51	.90	.061	21	43	.79	345	.06	7	2.40	.01	.07	1
16+00W 9+25S	1	43	20	142	.1	83	17	836	4.56	16	5	ND	1	43	1	2	2	57	.80	.096	17	90	1.15	233	.07	3	2.49	.01	.07	1
16+00W 9+75S	1	14	17	181	.1	56	12	372	4.22	12	5	ND	1	17	1	3	2	51	.23	.060	19	46	.60	129	.12	2	3.45	.01	.07	1
STD C	18	60	45	132	6.9	69	30	1026	4.24	44	18	7	37	47	18	16	20	59	.51	.096	38	55	.90	175	.07	33	2.04	.06	.14	11

ESSO MINERALS CANADA LTD. PROJECT 122-KUTCHO FILE # 88-4699

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM
16+00W 10+00S	1	28	8	82	.1	58	12	696	4.06	6	5	ND	1	15	1	2	2	73	.24	.061	12	53	.73	98	.09	2	1.76	.01	.04	1
14+00W 12+00N	1	15	14	79	.1	21	8	388	3.47	6	5	ND	1	10	1	2	2	108	.14	.034	6	45	.45	66	.19	2	.99	.01	.03	1
14+00W 11+75N	2	13	12	70	.1	16	7	337	3.79	9	5	ND	2	10	1	2	2	118	.10	.048	8	40	.46	61	.20	2	1.33	.01	.04	2
14+00W 11+50N	1	14	11	52	.1	28	7	351	3.86	8	5	ND	1	12	1	2	2	72	.19	.051	8	54	.67	71	.15	2	1.75	.01	.02	2
STD C	18	56	38	128	6.7	67	30	1012	4.10	41	17	7	36	48	18	16	21	59	.49	.093	37	57	.91	161	.06	32	1.92	.06	.13	13
14+00W 11+00N	1	19	12	66	.3	37	9	415	3.85	10	5	ND	2	14	1	3	3	66	.23	.043	9	58	.97	87	.09	2	2.31	.01	.03	2
14+00W 10+75N	1	20	13	75	.1	33	8	369	4.00	4	5	ND	2	14	1	2	2	72	.10	.042	9	44	.68	106	.05	2	2.27	.01	.05	1
14+00W 10+50N	1	8	13	39	.1	13	3	131	1.96	2	5	ND	1	12	1	2	2	62	.10	.017	7	40	.31	80	.07	2	1.36	.01	.04	2
14+00W 6+75N	1	24	7	56	.1	59	17	635	3.21	6	5	ND	1	25	1	2	2	57	.36	.046	9	75	1.19	102	.12	2	1.55	.01	.03	1
14+00W 6+50N	1	51	13	85	.1	68	11	424	3.95	7	5	ND	1	32	1	2	2	63	.76	.050	19	73	.97	317	.06	2	2.59	.01	.06	1
14+00W 6+25N	1	18	5	63	.1	54	10	361	3.97	7	5	ND	1	14	1	2	2	64	.22	.034	7	86	1.21	82	.11	4	2.00	.01	.03	1
14+00W 6+00N	5	97	17	148	.1	183	27	4176	5.58	17	5	ND	1	48	2	3	2	67	1.46	.110	34	133	1.35	604	.03	2	4.31	.01	.08	1
14+00W 5+50N	1	50	12	107	.1	89	13	970	3.23	3	5	ND	1	44	1	2	2	49	1.62	.087	12	74	1.04	292	.04	2	2.12	.01	.05	1
14+00W 5+25N	1	65	10	113	.4	139	16	719	5.05	10	5	ND	1	32	1	2	2	68	1.17	.062	14	105	1.57	248	.08	2	3.02	.01	.07	1
14+00W 5+00N	1	37	8	81	.2	96	17	670	3.92	12	5	ND	1	29	1	4	2	60	1.01	.065	8	105	1.80	145	.07	2	2.34	.01	.04	1
14+00W 4+75N	1	73	21	181	.1	101	23	1459	5.14	14	5	ND	1	27	1	2	2	54	1.39	.092	13	95	1.04	236	.07	2	2.83	.01	.06	1
14+00W 4+50N	1	71	9	458	.1	133	25	949	5.23	13	5	ND	1	20	1	2	3	69	.94	.059	16	131	1.87	137	.09	4	2.89	.01	.04	1
14+00W 4+25N	1	27	13	102	.1	105	16	594	5.60	8	5	ND	1	14	1	2	3	86	.23	.048	12	135	2.21	108	.14	2	2.60	.01	.04	1
14+00W 4+00N	1	14	13	54	.1	25	8	299	3.04	8	5	ND	1	16	1	2	2	74	.14	.041	6	56	.73	109	.15	2	1.63	.01	.03	1
14+00W 3+75N	2	20	14	85	.1	26	6	321	4.22	10	5	ND	1	10	1	2	2	43	.10	.063	20	37	.46	105	.10	2	2.09	.01	.04	1
14+00W 3+50N	1	36	6	72	.1	46	17	561	4.56	9	5	ND	1	12	1	2	2	65	.21	.036	8	66	1.21	50	.07	2	2.83	.01	.02	1
14+00W 3+25N	1	151	13	204	.1	103	14	542	4.90	16	5	ND	1	32	1	2	2	63	1.26	.127	21	93	1.15	284	.04	2	3.69	.01	.05	1
14+00W 3+00N	1	148	13	321	.2	102	15	828	4.26	10	5	ND	1	36	2	2	2	53	1.67	.122	20	88	1.11	267	.04	2	3.14	.01	.06	1
14+00W 2+75N	1	55	9	128	.1	57	16	659	5.82	10	5	ND	3	11	1	2	2	65	.35	.070	16	47	1.11	86	.30	2	4.41	.02	.03	1
14+00W 2+50N	2	140	21	245	.6	93	39	621	6.20	15	5	ND	2	21	1	2	3	42	.79	.065	21	51	.57	61	.11	2	3.58	.01	.03	1
14+00W 2+25N	1	17	11	53	.1	15	4	140	2.71	9	5	ND	1	15	1	2	2	62	.42	.030	8	29	.28	88	.04	2	1.60	.01	.02	1
14+00W 2+00N	2	73	17	103	.1	78	21	3920	4.14	15	5	ND	1	35	1	2	2	54	1.74	.117	44	49	.64	368	.02	2	3.60	.01	.06	1
14+00W 1+75N	1	18	12	63	.1	34	8	343	4.22	10	5	ND	1	15	1	2	2	73	.14	.042	8	54	.64	110	.08	2	2.12	.01	.04	1
14+00W 1+50N	1	27	31	70	.1	50	10	399	4.10	12	5	ND	1	14	1	3	2	56	.17	.043	8	60	.78	103	.07	2	2.63	.01	.03	1
RE 14+00W 2+50N	2	140	22	245	.7	97	39	624	6.19	15	5	ND	1	21	1	3	2	43	.79	.065	20	56	.57	59	.10	2	3.60	.01	.03	1
14+00W 1+25N	1	29	16	98	.1	55	11	399	4.86	11	5	ND	1	12	1	2	2	61	.12	.041	10	58	.81	111	.08	2	3.51	.01	.05	1
14+00W 1+00N	1	33	15	80	.1	69	15	445	4.06	11	5	ND	2	16	1	2	2	55	.15	.029	10	54	.79	135	.09	2	3.31	.01	.04	1
14+00W 0+75N	1	19	14	61	.2	30	8	289	4.10	11	5	ND	2	10	1	4	3	65	.09	.035	12	46	.50	85	.15	3	2.38	.01	.03	1
14+00W 0+50N	1	41	10	60	.1	102	13	301	3.27	16	5	ND	1	11	1	2	3	52	.12	.026	6	57	.68	81	.07	2	1.99	.01	.03	1
14+00W 0+25N	1	32	13	96	.2	46	9	428	3.75	11	5	ND	1	33	1	2	2	52	.64	.077	16	41	.56	245	.02	2	2.85	.01	.05	1
14+00W 0+00N	1	17	8	69	.1	32	8	334	3.28	7	5	ND	1	16	1	2	2	59	.14	.023	7	47	.63	81	.06	2	1.81	.01	.03	1
14+00W 0+25S	1	19	15	80	.1	38	9	396	4.88	15	5	ND	2	14	1	2	4	61	.14	.030	10	63	.88	83	.10	2	2.76	.01	.03	1
14+00W 0+50S	1	15	14	52	.2	29	7	250	3.26	10	5	ND	2	13	1	3	2	58	.12	.022	8	52	.59	94	.10	4	2.24	.01	.03	1
STD C	17	59	41	132	7.0	69	30	1028	4.17	43	18	7	36	47	16	16	22	59	.50	.095	38	58	.93	172	.07	33	2.01	.06	.13	13

ESSO MINERALS CANADA LTD. PROJECT 122-KUTCHO FILE # 88-4699

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
14+00W 1+00S	1	23	14	67	.1	47	12	455	3.51	7	5	ND	2	19	1	2	2	62	.19	.019	9	56	.92	119	.08	2	2.98	.01	.04	1
14+00W 1+25S	2	30	15	79	.1	46	11	494	4.37	12	5	ND	2	17	1	3	2	55	.16	.031	18	56	.80	146	.07	4	3.34	.01	.07	1
14+00W 1+50S	1	27	13	67	.1	46	9	296	3.95	6	5	ND	2	15	1	2	2	61	.17	.026	9	57	.96	130	.05	3	3.54	.01	.08	1
14+00W 2+00S	1	15	17	118	.3	31	7	211	3.76	7	5	ND	1	18	1	3	2	78	.50	.035	11	47	.60	124	.08	2	2.74	.01	.04	1
14+00W 2+25S	1	36	12	153	.1	55	9	848	3.98	14	5	ND	1	32	1	2	2	44	1.44	.131	18	43	.73	163	.04	2	2.87	.01	.07	1
14+00W 2+50S	1	35	14	303	.1	55	16	1032	4.63	13	5	ND	1	31	1	2	2	60	1.83	.114	11	76	1.26	209	.02	2	4.05	.01	.08	1
14+00W 3+00S	1	53	10	102	.1	51	21	481	6.98	6	5	ND	1	12	1	2	2	137	.34	.028	13	76	.80	108	.01	2	3.07	.01	.04	1
14+00W 3+50S	1	21	14	75	.1	36	8	330	3.65	9	5	ND	1	21	1	3	3	68	.43	.013	9	48	.70	150	.07	2	2.47	.01	.04	1
14+00W 3+75S	1	65	13	100	.1	50	12	771	3.55	8	5	ND	1	34	1	3	2	52	1.30	.056	20	50	.72	200	.03	2	2.99	.01	.07	1
14+00W 4+00S	1	24	15	107	.1	38	14	717	3.68	7	5	ND	1	22	1	3	2	60	.56	.066	12	51	.61	174	.04	2	2.33	.01	.07	1
14+00W 4+25S	1	14	7	66	.1	26	7	332	2.25	8	5	ND	1	28	1	3	2	46	.43	.026	8	37	.59	121	.06	2	1.38	.01	.04	1
14+00W 4+50S	1	20	12	69	.1	36	9	442	2.70	6	5	ND	1	33	1	2	2	50	.42	.041	9	43	.66	156	.06	2	1.54	.01	.07	1
14+00W 4+75S	1	25	9	107	.1	39	9	398	2.88	3	5	ND	1	40	1	2	2	51	.57	.060	13	42	.67	227	.03	2	1.97	.01	.09	1
14+00W 5+00S	1	25	12	78	.1	40	10	491	2.78	10	5	ND	1	53	1	2	2	50	.54	.049	13	41	.71	212	.05	3	1.64	.01	.08	1
14+00W 6+25S	1	12	9	103	.1	25	8	357	3.03	4	5	ND	1	23	1	2	3	60	.42	.030	8	54	.76	106	.09	2	1.89	.01	.07	1
14+00W 6+50S	1	18	15	122	.1	41	11	539	4.25	10	5	ND	1	15	1	2	2	71	.14	.056	9	46	.70	124	.06	2	2.64	.01	.05	1
14+00W 6+75S	1	10	15	93	.1	18	5	321	3.85	9	5	ND	1	16	1	3	2	61	.09	.056	11	32	.35	140	.06	2	2.12	.01	.05	1
14+00W 7+00S	1	12	11	72	.2	24	5	254	3.76	8	5	ND	1	15	1	2	2	62	.11	.029	11	39	.46	139	.09	2	1.90	.01	.04	1
14+00W 7+25S	1	15	12	64	.1	41	7	269	3.00	12	5	ND	2	23	1	3	2	56	.22	.033	8	47	.77	155	.08	2	1.91	.01	.05	1
14+00W 7+50S	1	7	12	46	.1	11	3	106	1.66	5	5	ND	1	17	1	2	2	41	.11	.023	8	26	.23	119	.05	2	1.19	.01	.03	2
14+00W 7+75S	1	16	14	76	.1	34	8	359	3.08	7	5	ND	1	21	1	2	2	58	.20	.050	10	49	.69	143	.06	2	1.52	.01	.04	1
14+00W 9+25S	1	27	11	98	.1	42	10	914	2.74	6	5	ND	1	44	1	2	2	45	.78	.077	15	43	.63	251	.03	2	1.93	.01	.05	1
14+00W 9+25S	1	31	10	84	.1	55	9	415	2.70	9	5	ND	1	47	1	2	2	45	1.28	.059	12	54	.81	195	.04	4	1.68	.01	.07	1
14+00W 9+50S	1	42	13	108	.1	65	12	611	3.65	10	5	ND	1	36	1	2	2	62	.88	.097	17	74	.97	193	.03	2	2.84	.01	.06	1
14+00W 9+75S	2	19	14	100	.1	29	8	707	4.77	9	5	ND	1	10	1	2	2	63	.14	.062	13	49	.55	95	.10	2	1.74	.01	.05	1
RE 14+00W 7+75S	1	16	12	76	.1	34	8	365	3.12	6	5	ND	1	21	1	3	2	59	.20	.050	10	50	.69	143	.06	3	1.53	.01	.04	1
14+00W 10+00S	2	12	23	99	.1	32	10	646	7.79	10	5	ND	2	13	1	2	2	88	.12	.094	13	61	.59	142	.27	2	1.97	.01	.04	1
12+00W 7+00N	2	70	19	336	.1	88	11	337	3.82	11	5	ND	1	43	1	3	2	47	1.34	.137	34	64	.72	387	.06	2	3.82	.01	.06	1
12+00W 6+75N	2	23	13	127	.2	36	11	533	4.10	10	5	ND	1	29	1	2	2	64	.46	.090	12	75	.76	194	.06	2	1.93	.01	.05	1
STD C	19	56	40	127	6.7	66	29	998	4.06	40	18	7	34	44	17	19	19	58	.48	.093	36	53	.90	160	.06	33	1.96	.06	.14	12
12+00W 6+50N	1	21	13	109	.2	70	20	510	6.31	5	5	ND	1	17	1	2	2	121	.26	.043	7	105	1.46	114	.23	2	2.57	.01	.04	1
12+00W 6+25N	1	26	12	65	.1	54	12	426	3.18	11	5	ND	1	22	1	2	2	54	.26	.040	9	58	.94	120	.08	4	2.30	.01	.04	1
12+00W 6+00N	3	16	18	69	.2	23	4	243	4.42	10	5	ND	2	10	1	3	2	51	.06	.053	15	41	.34	73	.06	2	2.94	.01	.06	1
12+00W 5+75N	1	24	13	70	.1	52	11	380	4.08	16	5	ND	1	13	1	2	2	56	.23	.068	9	66	1.01	94	.09	2	2.99	.01	.04	1
12+00W 5+50N	1	20	10	58	.1	44	10	309	3.39	6	5	ND	1	14	1	2	2	65	.26	.035	6	75	1.09	73	.12	2	2.22	.01	.04	1
12+00W 5+25N	1	22	12	63	.1	43	9	325	3.30	7	5	ND	1	14	1	3	3	59	.17	.050	8	65	.84	85	.08	2	2.22	.01	.05	1
12+00W 5+00N	1	15	11	59	.1	35	8	313	3.44	10	5	ND	1	13	1	3	2	61	.16	.036	7	56	.78	80	.08	3	1.99	.01	.04	1
12+00W 4+75N	1	13	12	61	.6	13	4	130	2.14	6	5	ND	1	11	1	3	2	39	.07	.094	8	36	.25	79	.01	2	1.60	.01	.03	1
STD C	18	59	44	132	7.0	69	30	1030	4.17	44	18	7	37	48	18	17	21	60	.50	.096	38	55	.94	175	.07	33	2.04	.06	.14	12

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
12+00W 4+50N	3	10	13	117	.1	12	3	350	4.52	9	5	ND	1	8	1	2	2	56	.04	.035	8	22	.81	63	.07	2	2.07	.01	.05	1
12+00W 4+25N	2	14	18	81	.1	18	5	365	3.54	3	5	ND	1	9	1	2	2	67	.06	.056	15	33	.34	101	.06	2	2.09	.01	.05	2
12+00W 4+00N	2	17	17	99	.1	32	11	862	7.69	11	5	ND	2	11	1	2	3	79	.09	.081	14	65	.55	99	.14	2	2.88	.02	.06	1
12+00W 3+75N	2	27	16	95	.4	21	6	520	4.37	2	5	ND	1	12	1	2	2	73	.21	.074	15	56	.46	91	.10	2	1.92	.01	.05	1
12-00W 3+50N	1	26	12	91	.2	40	10	356	5.02	6	5	ND	1	17	1	2	2	82	.24	.051	9	66	.76	108	.13	2	2.42	.01	.04	1
12+00W 3+25N	1	250	15	533	.1	109	16	889	4.69	10	5	ND	1	33	1	2	2	55	.91	.151	33	80	.93	358	.04	2	4.40	.01	.08	1
12+00W 3+00N	1	14	12	54	.2	22	6	397	3.19	3	5	ND	1	11	1	2	2	75	.10	.050	8	53	.42	67	.10	2	1.44	.01	.05	2
12+00W 2+75N	2	25	16	79	1.0	35	9	389	8.81	14	5	ND	2	8	1	2	3	98	.08	.081	10	75	.66	63	.19	2	2.83	.01	.04	1
RE 12+00W 1+75N	1	19	14	82	.1	37	8	262	3.91	7	5	ND	1	13	1	2	2	66	.14	.051	8	66	.69	85	.10	5	1.82	.01	.05	1
12+00W 2+50N	1	99	15	86	.1	87	14	580	4.13	8	5	ND	1	28	1	2	2	44	1.29	.067	19	54	.91	145	.05	2	2.71	.01	.06	1
12+00W 2+25N	1	9	17	58	.1	12	4	218	2.03	4	5	ND	1	10	1	2	2	60	.26	.016	11	34	.54	69	.19	2	1.41	.01	.03	1
12+00W 2+00N	1	246	13	108	.1	69	15	1044	4.16	9	5	ND	1	31	1	2	2	58	1.43	.104	35	50	.96	224	.04	2	3.27	.03	.08	1
12+00W 1+75N	1	21	12	83	.1	37	8	263	3.85	5	5	ND	1	13	1	2	2	65	.15	.050	8	66	.69	85	.10	2	1.82	.01	.05	1
STD C	17	57	39	129	7.0	66	29	983	4.02	40	18	7	35	45	17	18	22	57	.47	.091	36	55	.89	160	.06	32	1.94	.06	.14	13
12+00W 1+50N	2	19	10	73	.2	50	11	472	4.73	9	5	ND	1	11	1	2	2	83	.19	.054	6	96	1.01	70	.11	3	1.96	.01	.05	1
12+00W 1+25N	2	56	5	81	.3	144	28	521	6.80	18	5	ND	1	10	1	2	2	101	.10	.036	4	222	1.95	55	.39	2	2.71	.01	.03	1
12+00W 1+00N	2	162	9	142	.4	146	27	1384	6.95	22	5	ND	1	31	1	2	2	76	1.19	.107	35	67	1.30	193	.13	2	3.45	.01	.06	1
12+00W 0+75N	2	10	19	58	.2	14	4	286	4.25	3	5	ND	1	7	1	2	2	84	.07	.034	13	38	.39	59	.23	2	2.06	.01	.04	1
12+00W 0+50N	2	43	13	117	.1	81	12	527	4.89	7	5	ND	1	20	1	2	2	53	.66	.058	21	53	.71	86	.13	2	3.23	.01	.05	1
12+00W 0+25N	1	25	14	89	.1	57	10	468	4.56	7	5	ND	2	15	1	2	2	64	.17	.044	11	60	.92	101	.16	2	2.66	.01	.05	1
12+00W 0+00N	1	200	21	208	.1	126	12	830	4.45	16	5	ND	1	33	1	2	2	36	1.85	.137	33	47	.73	146	.04	5	3.50	.01	.07	1
12+00W 0+25S	2	13	16	77	.1	19	5	370	5.01	4	5	ND	1	8	1	2	2	69	.08	.046	14	45	.32	58	.18	2	1.82	.01	.05	1
12+00W 0+50S	1	25	18	102	.1	49	9	359	4.24	4	5	ND	1	11	1	2	2	71	.08	.034	12	54	.69	123	.06	2	3.21	.01	.06	1
12+00W 0+75S	1	13	13	65	.1	21	5	270	3.60	6	5	ND	1	12	1	2	2	74	.06	.034	11	35	.34	96	.06	2	1.97	.01	.06	1
12+00W 1+00S	3	45	19	146	.1	51	8	352	5.65	15	5	ND	1	8	1	2	2	65	.11	.046	19	48	.51	97	.03	2	4.00	.01	.08	1
12+00W 1+25S	2	43	15	113	.1	62	7	607	4.39	9	5	ND	1	21	1	2	2	36	.64	.080	37	40	.60	131	.05	2	3.38	.01	.05	1
12+00W 1+50S	1	16	10	79	.1	32	12	459	4.81	6	5	ND	1	9	1	2	2	114	.14	.034	4	63	.90	76	.29	2	1.99	.01	.03	1
12+00W 1+75S	3	35	9	78	.1	39	12	395	5.65	16	5	ND	1	5	1	2	2	102	.14	.025	7	68	.86	35	.43	2	2.05	.01	.02	1
12+00W 2+00S	2	104	12	68	.1	26	8	593	3.20	2	5	ND	1	53	1	2	2	50	2.62	.227	24	35	.21	108	.02	2	2.12	.01	.02	1
12+00W 2+25S	1	6	20	76	.1	13	3	155	2.01	2	5	ND	1	12	1	2	2	63	.18	.015	16	32	.25	96	.16	2	1.26	.01	.03	1
12+00W 2+50S	1	27	13	130	.2	47	11	786	3.59	7	5	ND	1	25	1	2	2	56	.57	.091	15	55	.50	278	.02	2	2.90	.01	.06	1
12+00W 3+00S	2	36	16	120	.1	36	6	1157	4.73	10	5	ND	1	21	1	2	2	31	1.35	.114	45	26	.31	175	.03	2	3.72	.01	.06	1
12+00W 3+25S	1	14	10	72	.1	25	6	246	3.33	2	5	ND	1	14	1	2	2	83	.22	.012	7	46	.66	115	.13	2	1.87	.01	.03	1
12+00W 3+50S	1	149	14	146	.1	105	14	1844	5.86	11	5	ND	1	26	1	2	2	60	.84	.058	28	105	1.29	187	.09	2	3.14	.01	.07	1
12+00W 3+75S	1	69	15	163	.1	45	8	849	3.75	3	5	ND	1	28	1	2	2	43	1.83	.142	21	35	.53	147	.03	2	2.94	.01	.07	1
12+00W 4+00S	1	98	13	121	.1	73	12	665	3.65	27	5	ND	1	23	1	2	2	49	1.08	.055	14	42	.73	142	.04	2	2.73	.01	.06	1
12+00W 4+25S	1	50	14	145	.1	48	11	881	3.47	7	5	ND	1	27	1	2	2	48	1.33	.077	12	42	.69	147	.03	3	2.55	.01	.07	1
12+00W 4+50S	1	45	15	101	.1	56	15	757	3.70	7	5	ND	2	32	1	3	2	60	1.02	.035	10	51	.99	165	.05	3	2.45	.01	.09	1
STD C	17	58	42	132	6.8	66	30	1025	4.11	42	18	7	36	47	18	16	21	58	.50	.095	38	53	.92	171	.07	33	1.98	.06	.14	12

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
12+00W 4+75S	1	31	17	73	.1	39	10	542	3.32	3	5	ND	1	33	1	2	2	56	.57	.090	14	48	.73	236	.02	2	2.47	.01	.08	1
12+00W 5+00S	1	28	15	85	.1	39	10	511	2.81	6	5	ND	1	38	1	2	3	47	.65	.055	12	43	.66	181	.03	3	1.89	.01	.09	1
12+00W 5+25S	1	21	12	88	.1	35	8	353	3.05	5	5	ND	1	22	1	2	3	56	.21	.031	7	50	.71	137	.04	2	1.91	.01	.07	1
12+00W 5+50S	1	19	14	87	.1	36	9	462	2.79	10	5	ND	1	30	1	2	2	51	.33	.025	8	47	.70	163	.05	2	1.64	.01	.07	1
12+00W 5+75S	1	25	17	85	.1	45	10	504	3.07	5	5	ND	1	39	1	2	3	54	.49	.041	11	53	.82	230	.04	2	2.10	.01	.09	1
12+00W 6+00S	1	30	14	85	.1	48	8	402	2.78	6	5	ND	1	55	1	2	2	44	1.11	.067	12	51	.78	230	.03	5	2.02	.01	.08	1
12+00W 6+25S	1	23	15	83	.1	43	10	531	2.74	3	5	ND	1	35	1	2	2	47	.64	.046	10	54	.82	176	.05	2	1.77	.01	.07	1
12+00W 6+75S	1	40	14	95	.1	59	11	564	3.08	5	5	ND	1	49	1	3	2	48	.98	.054	15	63	.98	203	.05	3	1.92	.01	.08	1
12+00W 7+00S	1	76	16	101	.1	79	12	712	3.28	8	5	ND	1	52	1	2	2	48	1.79	.095	28	64	.85	327	.01	2	2.91	.01	.10	1
12+00W 7+25S	1	28	17	78	.1	51	11	540	3.08	8	5	ND	1	36	1	2	2	51	.67	.034	14	55	.80	214	.05	2	2.16	.01	.06	1
12+00W 7+50S	1	20	15	73	.1	37	7	553	2.86	5	5	ND	1	34	1	2	2	52	.58	.040	11	44	.56	222	.03	2	1.93	.01	.07	1
12+00W 7+75S	1	21	12	113	.1	36	9	515	2.68	2	5	ND	1	36	1	2	2	45	.68	.062	8	42	.65	128	.02	2	1.75	.02	.08	1
12+00W 8+00S	1	19	18	86	.1	27	7	397	3.26	5	5	ND	1	19	1	2	2	60	.13	.055	12	47	.44	143	.13	2	1.62	.01	.07	1
12+00W 8+25S	1	50	21	120	.1	72	16	645	5.13	5	5	ND	1	24	1	2	3	67	.20	.063	23	64	.81	263	.13	2	3.82	.02	.07	1
12+00W 8+50S	1	30	22	100	.1	50	11	490	4.01	3	5	ND	1	28	1	2	2	65	.23	.038	16	52	.66	297	.10	2	2.63	.01	.07	2
12+00W 8+75S	1	19	10	54	.1	35	8	410	2.39	4	5	ND	2	36	1	2	2	43	.40	.045	9	46	.70	121	.08	2	1.09	.01	.05	1
RE 12+00W 10+00S	1	21	13	72	.1	36	7	284	2.20	7	5	ND	1	46	1	2	2	41	.43	.042	12	39	.63	191	.04	4	1.23	.02	.05	1
12+00W 9+00S	1	16	9	61	.1	33	8	368	2.24	2	5	ND	1	35	1	3	2	39	.46	.050	9	45	.67	141	.05	2	1.35	.01	.05	2
12+00W 9+25S	1	24	10	66	.1	36	8	408	2.48	7	5	ND	1	39	1	3	3	41	.53	.053	9	45	.78	148	.06	2	1.31	.01	.05	2
STD C	17	58	40	122	7.1	67	27	990	3.77	42	18	6	37	48	17	16	18	54	.45	.086	38	53	.85	160	.06	32	1.87	.06	.14	13
12+00W 9+75S	1	110	25	149	.1	85	13	1019	3.84	2	5	ND	1	59	1	2	2	51	1.57	.108	26	78	.79	378	.05	2	3.03	.02	.06	1
12+00W 10+00S	1	21	14	74	.1	37	7	290	2.25	5	5	ND	1	47	1	2	3	42	.44	.043	12	39	.64	197	.04	3	1.24	.02	.06	1
10+00W 6+75N	1	30	15	62	.1	46	10	386	3.11	5	5	ND	1	16	1	2	2	59	.16	.025	8	61	.84	111	.06	2	2.19	.01	.04	1
10+00W 6+50N	2	15	12	76	.1	21	10	602	3.83	4	5	ND	1	16	1	2	3	52	.30	.063	12	39	.57	102	.07	2	1.39	.01	.08	1
10+00W 6+25N	1	49	11	99	.5	37	7	703	1.88	2	5	ND	1	40	1	2	2	23	1.52	.164	17	38	.34	275	.01	2	1.90	.01	.03	1
10+00W 6+00N	1	16	15	76	.1	29	7	342	3.12	6	5	ND	1	14	1	2	2	68	.22	.034	7	53	.53	112	.07	2	1.48	.01	.04	1
10+00W 5+75N	2	50	15	101	.3	59	11	1228	3.65	4	5	ND	1	41	1	2	2	51	1.66	.114	23	75	.66	331	.08	2	2.83	.02	.05	1
10+00W 5+50N	1	30	10	58	.1	53	12	611	2.88	4	5	ND	2	32	1	2	2	50	.38	.050	12	59	.95	153	.11	2	1.35	.01	.04	1
10+00W 5+25N	1	29	13	73	.1	56	20	713	3.63	10	5	ND	1	17	1	2	2	64	.38	.043	8	82	1.38	90	.17	2	1.94	.01	.01	1
10+00W 5+00N	3	201	20	83	.2	15	3	177	2.80	2	5	ND	1	7	1	2	2	23	.07	.082	36	31	.19	61	.04	2	4.10	.02	.04	2
10+00W 4+75N	1	21	18	88	.2	29	8	366	4.08	5	5	ND	1	9	1	2	2	55	.05	.034	11	35	.56	83	.03	2	2.81	.01	.05	2
10+00W 4+50N	2	28	18	186	.1	28	13	430	4.24	10	5	ND	1	9	1	2	2	75	.16	.047	9	57	.64	53	.20	2	1.83	.01	.02	1
10+00W 4+25N	2	24	16	137	.3	23	7	321	2.94	3	5	ND	1	10	1	2	2	57	.12	.058	10	46	.50	70	.09	2	1.83	.01	.03	1
10+00W 4+00N	2	24	15	113	.1	53	10	591	4.67	3	5	ND	1	11	1	2	2	57	.10	.052	11	71	.68	73	.10	2	2.08	.01	.04	1
10+00W 3+75N	2	21	12	79	.1	33	11	424	4.39	2	5	ND	1	10	1	2	2	68	.12	.045	8	61	.67	63	.11	2	1.66	.01	.03	1
10+00W 3+50N	3	51	22	118	.3	41	9	524	4.76	2	5	ND	1	9	1	2	2	58	.06	.089	17	61	.55	104	.04	2	3.17	.01	.06	2
10+00W 3+25N	1	28	18	212	.2	27	8	758	3.35	2	5	ND	1	18	1	2	2	61	.53	.045	15	57	.51	184	.07	2	1.69	.01	.06	1
10+00W 3+00N	2	55	16	183	1.3	65	11	1812	3.02	2	5	ND	1	34	1	2	2	30	.99	.210	28	56	.47	265	.01	2	2.93	.01	.04	1
STD C	18	57	42	132	6.7	67	29	1069	4.06	36	17	6	37	48	18	19	20	59	.50	.092	39	57	.93	177	.07	33	2.06	.06	.13	13

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
10+00W 2+75N	2	36	24	101	.1	50	13	843	4.15	20	5	ND	1	30	1	2	2	40	.96	.069	29	55	.52	196	.05	3	2.11	.01	.04	1
10+00W 2+50N	1	20	13	73	.2	42	16	860	5.17	20	5	ND	1	17	1	2	2	73	.26	.067	8	68	.58	153	.10	2	1.81	.01	.02	1
10+00W 2+25N	1	54	15	86	.1	56	12	472	3.31	11	5	ND	1	26	1	2	2	44	.62	.042	17	41	.63	219	.02	2	2.81	.01	.05	1
10+00W 2+00N	1	54	12	98	.1	85	15	630	3.76	17	5	ND	1	29	1	2	2	46	.68	.077	23	48	.71	163	.04	2	2.59	.01	.04	1
10+00W 1+75N	2	86	18	103	.1	100	20	1768	5.56	23	5	ND	2	36	1	2	2	65	1.16	.082	49	60	.97	368	.17	2	3.76	.02	.06	1
10+00W 1+50N	1	93	16	142	.1	193	19	1029	5.31	23	5	ND	2	32	1	2	2	54	.88	.079	31	54	.88	257	.15	2	3.47	.01	.05	1
10+00W 1+25N	3	514	11	96	.1	304	20	2238	3.01	66	5	ND	1	64	1	2	2	34	3.29	.220	39	78	.54	296	.02	2	2.84	.01	.04	1
10+00W 1+00N	1	70	12	119	.1	80	12	662	3.01	16	5	ND	1	50	1	2	2	41	2.42	.096	15	56	.78	205	.03	3	2.12	.01	.04	1
10+00W 0-75N	1	68	14	141	.1	100	15	556	4.33	19	5	ND	1	30	1	2	2	57	.67	.095	18	78	1.12	251	.04	2	3.24	.01	.05	1
10+00W 0+50N	1	39	12	90	.2	56	20	794	5.04	18	5	ND	1	12	1	2	2	75	.29	.057	6	83	1.51	73	.11	3	2.78	.01	.03	2
10+00W 0+25N	2	52	22	121	.1	79	16	710	5.60	22	5	ND	2	17	1	2	2	55	.86	.051	22	48	.72	112	.09	3	3.29	.01	.05	1
10+00W 0+00N	1	371	13	139	.1	131	15	1039	3.86	50	5	ND	1	34	1	2	2	26	2.60	.175	77	38	.30	107	.03	3	4.66	.01	.03	1
10+00W 0+25S	1	134	15	186	.1	101	10	644	4.85	40	5	ND	1	30	1	2	2	41	1.34	.110	42	44	.49	104	.09	3	3.94	.02	.04	1
10+00W 0+50S	1	18	16	82	.2	39	9	359	4.91	14	5	ND	2	11	1	2	2	80	.14	.019	8	58	.86	57	.15	2	2.21	.01	.04	1
10+00W 1+00S	2	54	19	115	.1	81	15	346	5.75	13	5	ND	3	14	1	2	2	74	.19	.029	15	52	.72	80	.24	3	2.77	.01	.04	1
10+00W 1+25S	3	391	13	99	.1	74	12	650	4.03	48	5	ND	1	18	1	2	2	25	1.35	.167	90	42	.27	103	.03	7	4.88	.01	.03	1
10+00W 1+50S	1	78	19	156	.1	44	7	804	4.79	34	5	ND	1	37	1	2	2	39	1.83	.124	50	43	.33	118	.04	3	3.53	.01	.04	1
10+00W 2+25S	3	28	24	115	.1	21	3	587	5.44	26	5	ND	3	12	1	2	3	15	.69	.078	33	14	.17	58	.07	3	4.71	.01	.03	1
RE 10+00W 0+50S	1	16	15	83	.1	38	9	357	5.01	15	5	ND	2	11	1	2	2	81	.13	.019	8	58	.87	56	.16	3	2.26	.01	.04	1
10+00W 1+50S	1	16	14	159	.1	44	18	1299	4.98	12	5	ND	1	13	1	2	2	79	.42	.039	11	76	.99	157	.11	2	2.41	.01	.03	1
10+00W 2+75S	2	24	16	116	.1	58	9	528	4.59	17	5	ND	3	16	1	2	2	47	.61	.030	19	61	.67	111	.05	3	2.42	.01	.04	1
10+00W 3+00S	3	71	14	128	.1	79	14	544	4.92	24	5	ND	1	19	1	2	2	38	.92	.069	31	42	.64	69	.06	3	3.12	.01	.04	1
10+00W 3+25S	1	42	10	94	.1	85	15	654	3.72	14	5	ND	1	19	1	2	2	51	.61	.031	10	77	1.33	104	.06	3	2.02	.01	.04	1
10+00W 3+75S	1	13	12	95	.1	32	6	287	3.62	9	5	ND	1	11	1	2	2	54	.16	.046	10	50	.60	93	.05	3	1.76	.01	.04	1
10+00W 4+00S	1	21	6	77	.1	62	15	495	3.36	9	5	ND	1	18	1	2	2	54	.28	.022	7	67	1.12	93	.08	3	1.93	.01	.04	1
STD C	18	58	41	125	6.6	64	29	1003	4.00	43	19	7	37	48	18	16	20	55	.45	.092	37	55	.85	168	.06	32	1.85	.06	.13	13
10+00W 4+25S	1	23	11	77	.2	54	11	444	3.44	13	5	ND	1	23	1	2	2	62	.23	.029	9	65	.89	137	.06	6	1.83	.01	.07	1
10+00W 4+50S	1	22	13	76	.1	50	14	651	3.43	15	5	ND	1	25	1	2	2	58	.28	.031	7	58	.97	118	.09	3	1.67	.01	.05	1
10+00W 4+75S	1	38	12	105	.1	68	11	638	3.60	18	5	ND	1	39	1	2	2	57	.66	.073	15	65	.94	230	.03	3	2.52	.01	.06	1
10+00W 5+00S	1	44	8	90	.1	69	12	530	3.17	12	5	ND	1	42	1	2	2	50	1.35	.068	13	58	.90	181	.03	3	1.36	.01	.06	1
10+00W 5+50S	1	78	12	109	.2	129	16	1041	3.95	16	5	ND	1	59	1	2	2	55	2.08	.084	19	93	1.12	365	.01	4	2.99	.01	.09	1
10+00W 6+00S	1	14	10	59	.1	25	5	195	2.16	9	5	ND	1	29	1	2	2	41	.78	.033	9	27	.45	207	.03	2	1.43	.01	.04	1
10+00W 6+25S	1	16	7	80	.2	38	7	294	2.94	11	5	ND	1	23	1	2	2	59	.34	.018	6	49	.66	111	.07	2	1.34	.01	.05	1
10+00W 6+50S	1	55	11	96	.1	76	14	525	3.80	13	5	ND	1	29	1	2	2	61	.67	.026	27	65	1.06	181	.06	3	2.13	.01	.05	1
10+00W 6+75S	1	34	12	96	.1	46	11	503	3.32	13	5	ND	1	33	1	2	2	48	.91	.060	15	49	.64	211	.04	2	1.98	.01	.05	2
10+00W 7+50S	1	42	9	117	.1	69	9	440	2.88	8	5	ND	1	52	1	2	2	41	1.66	.091	19	53	.69	273	.02	2	2.12	.01	.06	1
10+00W 7+75S	1	36	12	134	.2	63	12	782	3.42	10	5	ND	1	44	1	2	2	45	1.61	.083	12	54	.71	226	.02	2	2.20	.01	.07	1
10+00W 8+25S	1	52	11	119	.2	83	9	457	2.86	15	5	ND	1	58	1	2	2	40	2.17	.094	15	57	.79	231	.02	4	1.96	.01	.06	1
STD C	18	58	42	132	7.1	69	30	1032	4.20	43	19	8	36	47	18	16	19	59	.51	.096	38	53	.89	172	.07	33	2.01	.06	.13	12

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
10+00W 8+75S	1	60	12	98	.1	82	13	704	3.60	10	5	ND	1	44	1	2	2	46	1.19	.082	20	70	.99	235	.03	2	2.27	.01	.07	1
10+00W 9+25S	1	43	12	102	.1	73	11	537	3.35	14	5	ND	1	44	1	2	2	48	.94	.056	12	70	.94	213	.03	3	2.09	.01	.07	1
10+00W 9+75S	1	51	14	100	.1	64	8	505	2.90	10	5	ND	1	54	1	2	2	41	1.16	.065	15	52	.75	283	.02	2	1.93	.01	.05	1
10+00W 10+00S	1	85	18	125	.1	99	13	739	3.89	17	5	ND	1	55	1	2	2	51	1.29	.086	29	77	1.01	348	.02	2	2.76	.01	.07	1
8+00W 6+75N	1	82	14	159	.4	50	8	460	3.30	11	5	ND	2	47	1	2	2	39	1.25	.176	38	37	.54	503	.01	2	3.87	.01	.06	1
8+00W 6+50N	1	24	20	110	.1	37	9	468	4.56	15	5	ND	1	12	1	2	2	56	.09	.053	15	36	.50	129	.09	3	2.89	.01	.05	1
8+00W 6+25N	1	21	13	90	.1	33	8	407	3.51	14	5	ND	1	13	1	2	2	43	.09	.038	11	33	.52	112	.03	4	2.29	.01	.04	1
8+00W 6+00N	1	26	15	98	.1	51	13	577	3.43	11	5	ND	1	15	1	2	2	51	.16	.046	9	50	.85	109	.05	3	2.49	.01	.05	1
8+00W 5+75N	1	17	17	88	.1	35	9	403	3.32	10	5	ND	1	15	1	2	2	46	.18	.052	9	41	.69	120	.05	3	2.64	.01	.04	1
8+00W 5+50N	2	86	16	229	.1	99	19	1473	5.24	21	5	ND	2	34	1	2	2	55	.94	.086	35	92	1.01	342	.07	2	3.12	.01	.08	1
8+00W 5+25N	1	30	8	65	.1	41	13	588	3.03	4	5	ND	1	22	1	2	2	49	.30	.050	10	45	.91	120	.08	3	1.60	.01	.03	1
8+00W 5+00N	1	18	13	76	.1	30	8	350	3.54	11	5	ND	1	10	1	2	2	68	.10	.030	6	46	.69	76	.05	2	1.94	.01	.03	1
8+00W 4+75N	1	21	15	95	.1	28	7	423	3.74	9	5	ND	1	12	1	2	2	57	.05	.052	8	34	.52	117	.01	2	2.54	.01	.05	1
8+00W 4+50N	1	21	17	80	.1	28	7	370	3.34	8	5	ND	1	12	1	2	2	50	.07	.055	9	31	.50	111	.02	3	2.21	.01	.05	1
8+00W 4+25N	1	24	15	94	.1	38	10	450	3.10	11	5	ND	1	20	1	2	2	46	.13	.044	10	33	.62	160	.02	3	2.24	.01	.05	1
8+00W 4+00N	4	24	20	181	.1	15	3	406	5.30	13	5	ND	2	5	1	2	2	25	.05	.073	29	22	.20	82	.08	2	3.36	.02	.05	1
8+00W 3+75N	1	17	17	104	.1	28	12	728	6.06	14	5	ND	2	9	1	2	2	89	.10	.084	8	50	.73	89	.13	3	2.32	.01	.06	2
8+00W 3+50N	1	30	11	95	.1	58	15	579	5.04	13	5	ND	1	10	1	2	2	69	.17	.038	8	80	1.24	70	.12	2	2.45	.01	.03	1
8+00W 3+25N	1	36	14	79	.1	64	15	643	3.68	10	5	ND	1	19	1	2	2	59	.28	.049	10	64	1.05	123	.08	4	2.10	.01	.04	1
8+00W 3+00N	3	37	20	100	.2	28	7	534	5.26	7	5	ND	1	7	1	2	2	60	.05	.074	14	39	.36	80	.02	2	2.55	.01	.06	1
STD C	17	58	40	124	6.5	65	29	999	3.99	42	18	7	34	47	17	17	19	54	.44	.090	34	55	.83	169	.05	31	1.82	.06	.13	13
8+00W 2+75N	2	96	14	149	.1	53	12	864	4.45	13	5	ND	1	16	1	2	2	43	.22	.127	28	45	.49	171	.02	2	3.26	.01	.05	1
8+00W 2+50N	1	147	18	154	.1	68	16	1093	4.30	9	5	ND	1	24	1	2	2	42	.54	.139	44	36	.36	233	.02	2	3.80	.01	.03	1
RE 8+00W 3+25N	1	36	12	76	.1	59	15	608	3.50	11	5	ND	1	18	1	2	2	56	.26	.048	10	62	1.00	119	.08	3	2.01	.01	.04	1
8+00W 2+25N	1	23	15	102	.1	35	11	394	5.65	12	5	ND	1	11	1	2	2	84	.10	.043	8	54	.63	98	.12	2	1.90	.01	.03	1
8+00W 2+00N	1	56	16	178	.2	71	13	820	3.99	11	5	ND	1	33	1	2	2	54	.73	.161	19	64	.88	334	.02	2	3.17	.01	.06	1
8+00W 1+75N	1	17	12	67	.1	31	8	295	3.77	6	5	ND	1	11	1	2	3	73	.14	.036	7	54	.66	85	.06	2	1.89	.01	.03	2
8+00W 1+50N	1	30	17	94	.3	57	14	555	4.38	39	5	ND	1	13	1	2	3	58	.13	.044	7	62	.91	96	.05	3	2.79	.01	.03	1
8+00W 1+25N	1	34	9	86	.1	49	8	509	2.52	6	5	ND	1	42	1	2	2	38	1.85	.083	11	50	.72	206	.03	3	1.93	.01	.03	1
8+00W 1+00N	1	61	10	89	.1	72	25	741	4.65	9	5	ND	2	17	1	2	3	71	.41	.041	8	85	1.59	129	.13	2	2.41	.01	.04	1
8+00W 0+75N	1	36	20	128	.1	49	12	697	4.84	11	5	ND	1	11	1	2	2	67	.10	.043	11	63	.86	115	.05	3	3.00	.01	.05	1
8+00W 0+50N	1	22	12	102	.1	31	8	334	4.44	11	5	ND	1	15	1	2	2	62	.15	.038	12	47	.52	97	.06	2	2.19	.01	.03	1
8+00W 0+25N	1	35	14	107	.1	40	16	407	7.63	15	5	ND	2	6	1	2	2	86	.21	.036	9	72	.76	36	.45	2	2.49	.01	.03	1
8+00W 0+00N	1	156	12	77	.1	110	12	644	3.47	27	5	ND	1	22	1	2	2	33	1.27	.049	19	32	.53	104	.05	3	2.37	.01	.04	1
6+00W 7+00N	2	19	12	100	.1	26	7	429	4.63	5	5	ND	1	10	1	2	2	54	.09	.058	10	37	.49	82	.07	2	2.15	.01	.04	1
6+00W 6+75N	1	43	9	130	.1	52	18	764	4.25	15	5	ND	1	20	1	2	2	55	.20	.060	9	58	.89	118	.05	2	2.23	.01	.04	1
6+00W 6+25N	4	92	9	149	.1	41	13	2155	4.29	7	5	ND	1	51	1	2	2	41	1.44	.128	35	31	.33	325	.06	2	2.13	.01	.03	1
6+00W 6+00N	2	58	13	198	.1	45	9	363	3.61	6	5	ND	2	39	1	2	2	49	1.04	.083	35	37	.34	225	.20	3	3.24	.02	.04	1
6+00W 5+75N	1	32	16	209	.2	44	11	632	4.87	7	5	ND	2	34	1	2	2	49	.83	.068	22	38	.51	190	.17	4	3.02	.01	.04	1
STD C	17	58	43	132	6.6	68	30	1020	4.16	44	18	7	37	47	18	20	21	59	.50	.094	37	56	.89	172	.07	33	2.01	.06	.14	11

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
6+00W 5+50N	2	36	16	169	.2	41	13	604	4.37	8	5	ND	1	36	1	2	2	59	.72	.058	14	41	.71	205	.07	2	2.35	.01	.07	1
6+00W 5+25N	2	41	11	113	.1	37	13	1110	4.24	2	5	ND	1	36	1	2	2	45	.52	.082	18	34	.62	223	.03	2	3.00	.01	.06	1
6+00W 5+00N	2	16	10	90	.1	16	6	394	3.16	9	5	ND	1	17	1	2	2	83	.21	.048	7	32	.42	101	.10	2	1.20	.01	.06	1
STD C	18	58	38	124	7.0	68	28	978	4.10	44	17	7	37	48	17	17	19	53	.46	.092	35	55	.87	157	.05	31	2.04	.06	.14	11
6+00W 4+75N	2	42	18	133	.2	46	11	561	5.74	2	5	ND	1	26	1	2	2	68	.37	.078	26	46	.72	263	.14	2	4.99	.01	.07	1
6+00W 4+50N	2	50	11	187	.1	65	15	1359	5.28	2	5	ND	1	28	1	2	2	64	.28	.080	19	51	.93	333	.07	2	4.73	.01	.09	1
6+00W 4+25N	1	30	18	128	.1	41	11	639	4.42	10	5	ND	1	25	1	2	2	54	.28	.062	12	40	.70	203	.09	2	3.10	.01	.06	1
6+00W 4+00N	1	28	14	101	.1	41	9	641	3.80	5	5	ND	1	27	1	2	2	52	.25	.078	12	44	.74	245	.02	2	3.44	.01	.07	1
6+00W 3+75N	1	25	16	98	.1	37	10	539	3.46	7	5	ND	1	19	1	2	2	47	.14	.051	11	34	.67	130	.04	2	3.00	.01	.07	1
6+00W 3+50N	1	25	18	92	.1	36	10	554	3.44	6	5	ND	1	21	1	2	2	47	.15	.047	11	33	.68	142	.03	2	2.99	.01	.07	1
6+00W 3+25N	2	26	19	129	.1	34	8	547	4.88	10	5	ND	1	12	1	2	2	53	.08	.072	13	40	.64	124	.03	3	3.84	.01	.08	1
6+00W 3+00N	1	27	15	94	.1	42	10	472	3.99	13	5	ND	1	18	1	2	2	55	.15	.048	9	41	.80	128	.04	2	3.26	.01	.07	1
6+00W 2+75N	1	15	13	77	.1	28	6	305	3.57	8	5	ND	3	14	1	2	2	48	.08	.029	11	32	.53	132	.03	2	3.03	.01	.08	1
6+00W 2+50N	1	20	15	99	.1	38	10	507	3.96	5	5	ND	1	15	1	2	2	55	.14	.042	7	47	.85	110	.04	2	3.04	.01	.06	1
6+00W 2+25N	2	18	12	76	.1	19	7	385	3.70	5	5	ND	1	10	1	2	2	65	.07	.045	11	32	.47	72	.07	2	1.99	.01	.05	1
6+00W 2+00N	6	25	14	69	.2	17	5	239	9.50	13	5	ND	1	7	1	2	2	47	.04	.132	11	41	.30	54	.05	2	2.23	.01	.05	1
6+00W 1+75N	1	25	14	73	.6	43	12	528	4.31	5	5	ND	1	14	1	2	2	49	.16	.051	7	52	.90	84	.05	2	2.79	.01	.05	1
6+00W 1+50N	1	20	11	95	.1	39	15	1034	5.20	10	5	ND	1	13	1	2	2	73	.30	.064	7	64	1.18	56	.10	2	2.15	.01	.05	1
6+00W 1+25N	1	34	10	102	.1	41	10	581	4.15	2	5	ND	1	11	1	2	2	46	.11	.064	12	47	.62	83	.05	2	2.63	.01	.05	1
6+00W 1+00N	2	81	11	153	.1	142	14	1210	5.51	9	5	ND	1	17	1	2	2	50	.21	.116	38	58	.72	181	.10	2	5.04	.01	.06	1
6+00W 0+75N	3	22	14	126	.1	30	10	554	6.83	2	5	ND	1	9	1	2	2	79	.17	.064	15	45	.58	63	.31	3	3.96	.01	.05	1
6+00W 0+50N	1	125	5	131	.2	78	15	1864	3.48	5	5	ND	1	40	1	2	2	43	2.16	.162	35	52	.80	200	.02	2	2.98	.01	.07	1
6+00W 0+25N	2	215	6	154	.1	68	12	1362	5.52	2	5	ND	1	18	1	2	2	29	.56	.110	50	34	.46	150	.06	2	4.00	.01	.07	1
6+00W 0+00N	1	179	15	175	.1	69	9	871	4.48	27	5	ND	1	25	1	2	2	37	1.27	.140	48	36	.45	136	.04	4	3.73	.01	.07	1
20+00S 0+00	2	159	11	173	.2	99	15	780	4.89	6	5	ND	1	40	1	2	2	47	1.84	.098	28	42	.58	198	.10	3	3.81	.02	.06	1
20+00S 0+25	1	24	9	82	.1	34	9	415	4.67	7	5	ND	2	12	1	2	2	69	.25	.038	7	51	.74	84	.16	2	2.17	.01	.04	1
20+00S 0+50	1	83	11	118	.1	58	10	440	5.21	7	5	ND	1	11	1	2	2	60	.19	.064	8	60	.90	127	.06	2	3.47	.01	.07	1
20+00S 0+75	1	41	8	55	.1	46	13	688	3.11	8	5	ND	1	22	1	2	2	44	.87	.022	9	50	.83	128	.05	2	2.16	.01	.03	1
20+00S 1+00	3	22	18	84	.1	29	9	372	6.19	13	5	ND	1	11	1	2	2	75	.18	.039	10	56	.60	91	.12	3	2.52	.01	.04	1
20+00S 1+25	1	22	11	72	.1	35	11	513	4.11	4	5	ND	1	15	1	2	2	59	.18	.024	8	48	.79	91	.07	2	2.27	.01	.04	1
RE 20+00S 0+25	1	22	8	84	.1	35	9	388	4.82	4	5	ND	1	13	1	2	2	72	.26	.039	7	52	.76	86	.16	2	2.34	.01	.04	1
20+00S 1+50	1	112	8	141	.3	83	39	3182	2.63	2	5	ND	1	48	2	2	2	20	3.92	.124	19	25	.23	255	.02	4	2.14	.01	.05	1
20+00S 1+75	6	211	7	112	.1	82	18	1076	28.46	35	5	ND	3	12	1	2	2	28	.76	.073	14	40	.15	65	.06	2	2.82	.01	.04	1
20+00S 2+00	1	30	6	84	.2	27	8	278	21.25	4	5	ND	3	9	1	2	2	84	.58	.074	3	58	.73	36	.23	2	1.39	.01	.03	1
20+00S 2+25	1	123	15	142	.1	74	18	873	5.77	8	5	ND	1	25	1	2	2	58	1.19	.057	28	68	.81	143	.14	2	4.05	.01	.04	1
20+00S 2+50	1	15	10	69	.1	29	8	306	4.82	11	5	ND	1	11	1	2	2	67	.16	.040	8	50	.76	75	.13	2	1.98	.01	.04	1
20+00S 2+75	3	10	16	74	.1	18	7	356	4.19	14	5	ND	2	7	1	2	2	117	.12	.041	14	42	.48	72	.37	2	1.21	.01	.04	1
20+00S 3+00	1	257	5	83	.1	116	16	1399	3.57	13	5	ND	1	31	1	2	2	38	1.98	.076	24	31	.62	151	.11	2	2.10	.01	.04	1
STD C	19	59	39	132	6.7	68	29	1045	4.08	43	16	8	36	48	18	19	22	55	.50	.095	36	55	.90	173	.06	33	1.98	.06	.14	12

ESSO MINERALS CANADA LTD. PROJECT 122-KUTCHO FILE # 88-4699

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
20+00S 3+25	1	204	15	134	.1	86	13	1293	3.60	12	5	ND	1	36	3	2	2	41	2.20	.133	24	39	.44	148	.06	2	2.27	.02	.06	1
20+00S 3+50	1	34	2	119	.2	36	13	620	4.38	5	5	ND	2	25	2	2	2	72	1.25	.039	11	57	.77	111	.16	3	1.95	.01	.04	1
20+00S 3+75	1	19	7	73	.2	42	13	344	4.27	6	5	ND	2	20	1	2	2	79	.41	.032	6	61	1.06	98	.21	3	2.06	.01	.05	1
20+00S 4+25	1	12	4	75	.2	18	6	237	2.46	6	5	ND	1	23	2	2	2	62	.37	.025	8	33	.46	121	.11	2	1.43	.02	.05	1
20+00S 4+50	1	23	10	61	.2	35	10	379	2.75	5	5	ND	1	27	1	2	2	53	.72	.037	11	45	.81	129	.11	2	1.69	.01	.04	1
20+00S 5+00	2	12	11	108	.1	20	8	364	4.99	6	5	ND	2	15	2	2	2	74	.48	.037	14	41	.45	77	.27	2	1.69	.02	.05	1
20+00S 5+50	1	120	17	124	.1	48	18	1468	5.30	16	5	ND	2	27	4	2	2	68	1.38	.077	20	64	.79	199	.10	2	2.38	.01	.06	1
20+00S 5+75	2	26	6	99	.1	62	24	479	7.77	8	5	ND	2	12	1	3	2	90	.23	.031	8	104	1.55	90	.32	2	2.69	.01	.06	1
20+00S 6+00	1	35	9	89	.1	57	17	597	4.21	8	5	ND	1	25	1	2	2	75	.68	.038	8	65	1.16	190	.08	2	2.65	.01	.10	1
20+00S 6+25	1	114	4	82	.1	47	8	1072	1.41	2	5	ND	1	57	2	2	2	23	4.29	.220	27	41	.34	198	.01	4	1.42	.02	.06	1
STD C	18	60	37	131	7.0	67	30	1026	4.15	40	17	7	38	49	19	17	18	61	.48	.095	40	56	.92	181	.07	32	1.90	.06	.15	11

APPENDIX IV

GEOPHYSICAL DATA

BOUGUER GRAVITY DATA

JOSH CREEK GRID

Line 1150E, Kutcho South

Date=880826 GMT=-7 SC=1.03057 GB1=1987.315 GB2=1987.315 Units=metr BD=2.67 Gf=67 Long=-128.211350 Lat=58.0958 Ydir=0 Cls=0.080 Dft=0.021

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	1300.00	800.00	921.	4762.080	0.32	1507.930	-0.025	*	*
2.00	1150.00	325.00	1133.	4769.690	0.45	1473.850	0.038	1995.31	514.56
3.00	1150.00	350.00	1137.	4768.700	0.39	1479.460	0.040	1994.27	514.61
4.00	1150.00	375.00	1141.	4768.220	0.29	1482.320	0.041	1993.75	514.63
5.00	1150.00	400.00	1146.	4767.720	0.39	1484.860	0.043	1993.27	514.63
6.00	1150.00	425.00	1156.	4767.360	0.29	1487.320	0.046	1992.87	514.70
7.00	1150.00	450.00	1200.	4766.880	0.33	1489.350	0.047	1992.39	514.60
8.00	1150.00	475.00	1205.	4766.110	0.27	1493.500	0.048	1991.58	514.59
9.00	1150.00	500.00	1208.	4765.700	0.34	1495.260	0.049	1991.18	514.52
10.00	1150.00	525.00	1212.	4765.420	0.35	1496.600	0.050	1990.90	514.48
11.00	1150.00	550.00	1216.	4765.290	0.39	1496.940	0.050	1990.78	514.41
12.00	1150.00	575.00	1221.	4765.070	0.37	1498.050	0.051	1990.55	514.38
13.00	1150.00	600.00	1224.	4764.880	0.38	1500.280	0.052	1990.36	514.61
14.00	1150.00	625.00	1230.	4764.760	0.29	1500.370	0.053	1990.21	514.46
15.00	1150.00	650.00	1234.	4764.210	0.41	1502.340	0.053	1989.68	514.30
16.00	1150.00	675.00	1238.	4763.700	0.34	1504.270	0.054	1989.14	514.12
17.00	1150.00	700.00	1242.	4763.340	0.41	1505.380	0.054	1988.79	513.97
18.00	1150.00	725.00	1247.	4762.970	0.17	1506.600	0.055	1988.34	513.74
19.00	1150.00	750.00	1251.	4762.530	0.33	1508.080	0.055	1987.93	513.61
20.00	1150.00	775.00	1255.	4761.600	0.31	1512.360	0.055	1986.97	513.47
21.00	1150.00	800.00	1300.	4760.460	0.37	1517.820	0.056	1985.82	513.37
22.00	1300.00	800.00	1312.	4761.960	0.32	1507.930	0.056	*	*

Line 1300E, Kutcho South

Date=880826 GMT=-7 SC=1.03057 GB1=1987.315 GB2=1987.315 Units=metr BD=2.67 Gf=67 Long=-128.210430
Lat=58.0958 Ydir=0 Cls=0.080 Dft=0.021

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	1300.00	800.00	921.	4762.080	0.32	1407.930	-0.025	*	*
2.00	1300.00	300.00	1112.	4772.070	0.37	1461.440	0.030	1997.72	514.55
3.00	1300.00	325.00	1108.	4771.680	0.37	1463.430	0.029	1997.32	514.52
4.00	1300.00	350.00	1104.	4770.940	0.37	1467.110	0.027	1996.55	514.46
5.00	1300.00	375.00	1100.	4770.290	0.33	1470.320	0.025	1995.86	514.39
6.00	1300.00	400.00	1056.	4769.740	0.36	1473.110	0.024	1995.30	514.36
7.00	1300.00	425.00	1051.	4770.240	0.35	1470.470	0.021	1995.81	514.33
8.00	1300.00	450.00	1043.	4769.880	0.30	1473.220	0.017	1995.42	514.46
9.00	1300.00	475.00	1037.	4768.930	0.24	1478.700	0.015	1994.42	514.51
10.00	1300.00	500.00	1033.	4768.300	0.44	1481.740	0.013	1993.82	514.50
11.00	1300.00	525.00	1028.	4767.950	0.36	1483.580	0.010	1993.44	514.46
12.00	1300.00	550.00	1024.	4767.250	0.33	1486.660	0.008	1992.70	514.31
13.00	1300.00	575.00	1021.	4766.950	0.38	1487.630	0.007	1992.41	514.19
14.00	1300.00	600.00	1017.	4766.930	0.39	1487.520	0.005	1992.38	514.12
15.00	1300.00	625.00	1013.	4766.630	0.33	1488.550	0.002	1992.05	513.98
16.00	1300.00	650.00	1009.	4765.950	0.31	1491.140	0.000	1991.34	513.76
17.00	1300.00	675.00	1004.	4765.310	0.37	1493.700	-0.002	1990.70	513.60
18.00	1300.00	700.00	1000.	4764.580	0.37	1496.790	-0.004	1989.94	513.43
19.00	1300.00	725.00	956.	4763.800	0.37	1500.290	-0.006	1989.13	513.29
20.00	1300.00	750.00	951.	4763.040	0.28	1503.270	-0.009	1988.32	513.05
21.00	1300.00	775.00	946.	4762.540	0.39	1505.470	-0.012	1987.83	512.97
22.00	1300.00	800.00	921.	4762.080	0.32	1507.930	-0.025	1987.31	512.92
23.00	1300.00	800.00	1312.	4761.960	0.32	1507.930	0.056	*	*

Line 1450E, Kutcho South

Date=880825 GMT=-7 SC=1.03057 GB1=2000 GB2=2000 Units=metr BD=2.678 Gf=67 Long=-128.205570 Lat=58.095

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	1600.00	0.00	932.	4774.410	0.35	1457.320	0.022	*	*
2.00	1450.00	0.00	1730.	4774.540	0.30	1455.510	-0.053	2000.12	516.00
3.00	1450.00	25.00	1725.	4774.620	0.28	1454.440	-0.050	2000.20	515.85
4.00	1450.00	50.00	1721.	4774.090	0.41	1455.860	-0.048	1999.69	515.61
5.00	1450.00	75.00	1716.	4774.690	0.28	1452.250	-0.045	2000.28	515.46
6.00	1450.00	100.00	1710.	4775.300	0.30	1448.150	-0.042	2000.91	515.27
7.00	1450.00	125.00	1705.	4776.580	0.27	1441.400	-0.039	2002.22	515.24
8.00	1450.00	150.00	1659.	4777.040	0.30	1438.010	-0.036	2002.71	515.04
9.00	1450.00	175.00	1652.	4776.210	0.37	1441.250	-0.032	2001.88	514.83
10.00	1450.00	200.00	1646.	4777.110	0.37	1435.420	-0.029	2002.81	514.59
11.00	1450.00	225.00	1640.	4777.380	0.36	1433.730	-0.025	2003.08	514.52
12.00	1450.00	250.00	1633.	4778.270	0.27	1427.280	-0.021	2003.98	514.12
13.00	1450.00	275.00	1622.	4776.360	0.36	1436.990	-0.015	2002.04	514.08
14.00	1450.00	300.00	1616.	4775.990	0.37	1439.280	-0.011	2001.67	514.14
15.00	1450.00	325.00	1610.	4775.020	0.34	1444.140	-0.007	2000.66	514.07
16.00	1450.00	350.00	1546.	4773.690	0.29	1451.350	0.007	1999.28	514.09
17.00	1450.00	375.00	1541.	4772.240	0.31	1460.010	0.009	1997.80	514.29
18.00	1450.00	400.00	1536.	4771.380	0.33	1464.870	0.012	1996.92	514.35
19.00	1450.00	425.00	1531.	4770.570	0.40	1468.680	0.015	1996.11	514.27
20.00	1450.00	450.00	1527.	4769.980	0.36	1472.190	0.017	1995.49	514.32
21.00	1450.00	475.00	1522.	4769.840	0.37	1472.970	0.020	1995.35	514.32
22.00	1450.00	500.00	1515.	4770.400	0.38	1469.720	0.024	1995.93	514.24
23.00	1450.00	525.00	1508.	4768.760	0.34	1477.430	0.028	1994.23	514.04
24.00	1450.00	550.00	1503.	4768.340	0.33	1480.150	0.030	1993.80	514.12
25.00	1450.00	575.00	1459.	4768.000	0.36	1482.910	0.032	1993.46	514.31
26.00	1450.00	600.00	1456.	4767.620	0.26	1484.780	0.034	1993.04	514.24
27.00	1450.00	625.00	1453.	4767.210	0.22	1486.250	0.035	1992.60	514.07
28.00	1450.00	650.00	1449.	4766.860	0.26	1487.540	0.037	1992.26	513.96
29.00	1450.00	675.00	1435.	4766.410	0.27	1489.220	0.044	1991.80	513.82
30.00	1450.00	700.00	1427.	4765.920	0.25	1491.010	0.047	1991.29	513.64
31.00	1450.00	725.00	1425.	4765.540	0.22	1492.490	0.048	1990.89	513.51
32.00	1450.00	750.00	1420.	4764.850	0.26	1495.650	0.050	1990.19	513.42
33.00	1450.00	775.00	1416.	4764.120	0.18	1498.860	0.052	1989.42	513.26
34.00	1450.00	800.00	1411.	4763.460	0.32	1501.750	0.054	1988.78	513.17
35.00	1600.00	0.00	1739.	4774.410	0.35	1457.320	-0.057	*	*

Line 1600E, Kutcho South

Date=880825 GMT=-7 SC=1.03057 GB1=2000 GB2=2000 Units=metr BD=2.678 Gf=67 Long=-128.204550 Lat=58.095

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	1600.00	0.00	932.	4774.380	0.35	1457.320	0.022	*	*
2.00	1600.00	0.00	932.	4774.380	0.35	1457.320	0.022	2000.00	516.24
3.00	1600.00	25.00	938.	4774.300	0.41	1456.660	0.025	1999.94	516.03
4.00	1600.00	50.00	943.	4774.730	0.38	1453.530	0.028	2000.37	515.83
5.00	1600.00	75.00	948.	4775.070	0.37	1450.730	0.030	2000.72	515.61
6.00	1600.00	100.00	952.	4775.320	0.38	1448.600	0.032	2000.99	515.44
7.00	1600.00	125.00	958.	4775.630	0.44	1446.330	0.035	2001.33	515.31
8.00	1600.00	150.00	1003.	4776.180	0.41	1443.190	0.038	2001.89	515.24
9.00	1600.00	175.00	1007.	4776.330	0.33	1441.400	0.039	2002.02	515.00
10.00	1600.00	200.00	1012.	4776.470	0.39	1440.050	0.042	2002.19	514.88
11.00	1600.00	225.00	1018.	4777.480	0.30	1434.730	0.044	2003.20	514.83
12.00	1600.00	250.00	1024.	4778.425	0.30	1428.360	0.047	2004.18	514.54
13.00	1600.00	275.00	1030.	4779.230	0.38	1422.390	0.049	2005.04	514.21
14.00	1600.00	300.00	1040.	4779.200	0.35	1420.940	0.053	2005.00	513.87
15.00	1600.00	325.00	1055.	4777.830	0.37	1427.500	0.059	2003.60	513.74
16.00	1600.00	350.00	1108.	4777.910	0.28	1425.550	0.063	2003.66	513.40
17.00	1600.00	375.00	1127.	*	0.40	1443.040	0.068	*	*
18.00	1600.00	400.00	1145.	4773.380	0.40	1454.340	0.071	1999.04	514.40
19.00	1600.00	425.00	1159.	4772.340	0.34	1460.050	0.073	1997.96	514.42
20.00	1600.00	450.00	1204.	4771.710	0.33	1463.770	0.074	1997.30	514.48
21.00	1600.00	475.00	1208.	4771.090	0.39	1467.050	0.074	1996.68	514.49
22.00	1600.00	500.00	1214.	4770.620	0.40	1469.500	0.074	1996.20	514.47
23.00	1600.00	525.00	1218.	4770.040	0.34	1472.200	0.075	1995.59	514.37
24.00	1600.00	550.00	1223.	4769.680	0.31	1474.190	0.075	1995.21	514.36
25.00	1600.00	575.00	1227.	4769.060	0.37	1476.950	0.075	1994.59	514.26
26.00	1600.00	600.00	1233.	4768.550	0.25	1479.550	0.075	1994.03	514.20
27.00	1600.00	625.00	1309.	4767.950	0.33	1482.070	0.071	1993.43	514.08
28.00	1600.00	650.00	1314.	4767.580	0.24	1483.580	0.070	1993.02	513.95
29.00	1600.00	675.00	1318.	4767.070	0.29	1485.760	0.070	1992.51	513.85
30.00	1600.00	700.00	1323.	4766.480	0.37	1488.080	0.069	1991.93	513.70
31.00	1600.00	725.00	1328.	4765.810	0.35	1491.000	0.067	1991.23	513.56
32.00	1600.00	750.00	1333.	4765.400	0.28	1493.150	0.066	1990.79	513.52
33.00	1600.00	775.00	1343.	4764.810	0.28	1495.200	0.063	1990.17	513.29
34.00	1600.00	800.00	1349.	4764.600	0.28	1496.420	0.062	1989.96	513.30
35.00	1600.00	0.00	1739.	4774.410	0.35	1457.320	-0.057	*	*

PC GRID

Line 150E, Kutcho South

Date=880826 GMT=-7 SC=1.03058 GB1=2000 GB2=2000 Units=metr BD=2.67 Gf=67 Long=-128.2343 Lat=58.10

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	150.00	0.00	1356.	4742.420	0.43	1555.000	0.051	*	*
2.00	150.00	0.00	1356.	4742.420	0.43	1555.000	0.051	2000.00	534.51
3.00	150.00	25.00	1359.	4742.980	0.39	1552.190	0.050	2000.56	534.50
4.00	150.00	50.00	1404.	4743.620	0.31	1548.800	0.049	2001.20	534.45
5.00	150.00	75.00	1407.	4744.220	0.33	1545.650	0.049	2001.82	534.43
6.00	150.00	100.00	1410.	4744.740	0.35	1542.590	0.048	2002.36	534.36
7.00	150.00	125.00	1413.	4745.150	0.28	1540.280	0.047	2002.76	534.28
8.00	150.00	150.00	1417.	4745.040	0.31	1540.290	0.046	2002.65	534.16
9.00	150.00	175.00	1420.	4744.670	0.28	1542.330	0.045	2002.26	534.15
10.00	150.00	200.00	1424.	4744.370	0.31	1543.600	0.044	2001.96	534.08
11.00	150.00	225.00	1427.	4744.170	0.40	1544.640	0.043	2001.78	534.08
12.00	150.00	250.00	1430.	4744.090	0.29	1545.150	0.042	2001.66	534.05
13.00	150.00	275.00	1433.	4743.720	0.33	1546.750	0.041	2001.29	533.98
14.00	150.00	300.00	1440.	4743.890	0.39	1545.070	0.039	2001.48	533.82
15.00	150.00	325.00	1445.	4744.050	0.30	1543.820	0.037	2001.61	533.69
16.00	150.00	350.00	1449.	4744.460	0.29	1541.510	0.036	2002.03	533.63
17.00	150.00	375.00	1453.	4744.640	0.33	1540.720	0.034	2002.23	533.65
18.00	150.00	400.00	1456.	4745.010	0.31	1540.590	0.033	2002.60	533.98
19.00	150.00	425.00	1500.	4745.190	0.34	1539.050	0.031	2002.79	533.85
20.00	150.00	450.00	1506.	4744.800	0.41	1540.610	0.029	2002.41	533.76
21.00	150.00	475.00	1511.	4744.210	0.32	1543.720	0.027	2001.77	533.71
22.00	150.00	500.00	1515.	4743.840	0.30	1545.120	0.025	2001.38	533.58
23.00	150.00	525.00	1519.	4743.750	0.36	1545.310	0.023	2001.30	533.52
24.00	150.00	550.00	1523.	4743.640	0.38	1545.260	0.021	2001.19	533.38
25.00	150.00	575.00	1527.	4743.280	0.43	1546.460	0.019	2000.83	533.24
26.00	150.00	600.00	1532.	4743.450	0.31	1545.130	0.017	2000.97	533.10
27.00	150.00	0.00	1749.	4742.540	0.44	1555.000	-0.058	*	*

Line 350E, Kutcho South

Date=880826 GMT=-7 SC=1.03058 GB1=2000 GB2=2000 Units=metr BD=2.67 Gf=67 Long=-128.2332 Lat=58.10

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	150.00	0.00	1356.	4742.420	0.43	1555.000	0.051	*	*
2.00	350.00	0.00	1738.	4743.630	0.38	1549.110	-0.052	2001.08	534.43
3.00	350.00	25.00	1734.	4744.420	0.42	1544.850	-0.050	2001.91	534.40
4.00	350.00	50.00	1730.	4744.850	0.34	1542.710	-0.048	2002.33	534.38
5.00	350.00	75.00	1725.	4745.460	0.36	1539.430	-0.045	2002.97	534.36
6.00	350.00	100.00	1721.	4745.850	0.38	1536.990	-0.043	2003.38	534.27
7.00	350.00	125.00	1717.	4746.150	0.31	1535.440	-0.041	2003.67	534.24
8.00	350.00	150.00	1709.	4746.440	0.30	1533.980	-0.036	2003.97	534.23
9.00	350.00	175.00	1704.	4746.600	0.31	1532.560	-0.033	2004.14	534.11
10.00	350.00	200.00	1700.	4746.850	0.34	1531.420	-0.031	2004.41	534.14
11.00	350.00	225.00	1655.	4747.060	0.32	1529.900	-0.028	2004.63	534.04
12.00	350.00	250.00	1650.	4747.820	0.29	1525.260	-0.025	2005.41	533.88
13.00	350.00	275.00	1646.	4749.415	0.41	1515.800	-0.023	2007.09	533.69
14.00	350.00	300.00	1644.	4748.470	0.40	1520.850	-0.022	2006.11	533.68
15.00	350.00	325.00	1637.	4747.800	0.34	1522.450	-0.018	2005.41	533.28
16.00	350.00	350.00	1632.	4748.150	0.34	1522.450	-0.015	2005.77	533.62
17.00	350.00	375.00	1628.	4748.620	0.32	1519.880	-0.013	2006.26	533.58
18.00	350.00	400.00	1624.	4749.000	0.37	1517.530	-0.011	2006.67	533.51
19.00	350.00	425.00	1619.	4749.240	0.33	1515.990	-0.008	2006.91	533.43
20.00	350.00	450.00	1616.	4748.490	0.35	1519.390	-0.006	2006.14	533.32
21.00	350.00	475.00	1613.	4748.120	0.36	1521.170	-0.005	2005.77	533.27
22.00	350.00	500.00	1609.	4747.790	0.32	1521.900	-0.002	2005.42	533.05
23.00	350.00	525.00	1605.	4747.600	0.31	1522.210	-0.000	2005.22	532.90
24.00	350.00	550.00	1600.	4747.450	0.32	1522.360	0.002	2005.07	532.76
25.00	350.00	575.00	1554.	4747.450	0.38	1520.690	0.006	2005.10	532.44
26.00	350.00	600.00	1550.	4746.040	0.35	1527.680	0.008	2003.64	532.33
27.00	150.00	0.00	1748.	4742.540	0.43	1555.000	-0.057	*	*

K GRID

Line 0, Kutcho South

Date=880827 GMT=-7 SC=1.03056 GB1=2000 GB2=2000 Units=metr BD=2.670 Gf=67 Long=-128.1355 Lat=58.09454

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	0.00	0.00	942.	4832.270	0.36	1234.760	-0.055	*	*
2.00	0.00	0.00	942.	4832.270	0.36	1234.760	-0.055	2000.00	472.76
3.00	0.00	-25.00	949.	4832.650	0.40	1232.590	-0.051	2000.41	472.73
4.00	0.00	-50.00	954.	4832.670	0.40	1232.430	-0.049	2000.43	472.70
5.00	0.00	-75.00	957.	4832.500	0.35	1233.220	-0.047	2000.25	472.66
6.00	0.00	-100.00	1000.	4832.410	0.39	1233.580	-0.046	2000.17	472.63
7.00	0.00	-125.00	1004.	4832.200	0.39	1234.480	-0.044	1999.96	472.57
8.00	0.00	-150.00	1009.	4832.120	0.38	1234.730	-0.041	1999.87	472.52
9.00	0.00	-175.00	1013.	4832.290	0.40	1234.140	-0.039	2000.06	472.57
10.00	0.00	-200.00	1016.	4832.570	0.40	1232.790	-0.038	2000.35	472.58
11.00	0.00	-225.00	1020.	4832.900	0.41	1230.750	-0.036	2000.70	472.51
12.00	0.00	-250.00	1024.	4832.990	0.41	1230.310	-0.034	2000.79	472.50
13.00	0.00	-275.00	1028.	4833.720	0.38	1226.050	-0.032	2001.54	472.39
14.00	0.00	-300.00	1038.	4833.910	0.31	1224.500	-0.027	2001.72	472.25
15.00	0.00	-325.00	1047.	4833.970	0.33	1223.330	-0.023	2001.80	472.08
16.00	0.00	-350.00	1051.	4833.950	0.41	1222.570	-0.021	2001.81	471.92
17.00	0.00	-375.00	1055.	4833.670	0.40	1222.830	-0.019	2001.52	471.66
18.00	0.00	-400.00	1059.	4833.480	0.35	1221.670	-0.017	2001.31	471.21
19.00	0.00	-425.00	1104.	4833.350	0.40	1221.330	-0.014	2001.19	471.01
20.00	0.00	-450.00	1108.	4833.150	0.41	1221.310	-0.013	2001.00	470.79
21.00	0.00	-475.00	1113.	4833.130	0.41	1219.970	-0.010	2000.98	470.49
22.00	0.00	-500.00	1120.	4835.410	0.25	1209.290	-0.007	2003.29	470.68
23.00	0.00	-525.00	1125.	4836.370	0.20	1203.590	-0.005	2004.26	470.51
24.00	0.00	-550.00	1130.	4837.760	0.23	1195.250	-0.003	2005.71	470.30
25.00	0.00	-575.00	1136.	4839.460	0.30	1185.560	-0.000	2007.49	470.16
26.00	0.00	-600.00	1142.	4841.650	0.30	1170.940	0.002	2009.75	469.52
27.00	0.00	-625.00	1150.	4843.340	0.23	1160.300	0.005	2011.47	469.14
28.00	0.00	-650.00	1203.	4844.000	0.32	1155.780	0.010	2012.19	468.95
29.00	0.00	-675.00	1211.	4843.830	0.38	1154.990	0.013	2012.04	468.63
30.00	0.00	0.00	1544.	4832.130	0.37	1234.760	0.003	*	*

Line 250E, Kutcho South

Date=880827 GMT=-7 SC=1.03056 GB1=2000 GB2=2000 Units=metr BD=2.670 Gf=67 Long=-128.1341 Lat=58.09454

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	0.00	0.00	942.	4832.270	0.36	1234.760	-0.055	*	*
2.00	250.00	-200.00	1528.	4833.460	0.37	1226.860	0.009	2001.42	472.48
3.00	250.00	-225.00	1524.	4833.360	0.38	1226.920	0.011	2001.32	472.38
4.00	250.00	-250.00	1518.	4833.290	0.39	1226.930	0.013	2001.25	472.29
5.00	250.00	-275.00	1511.	4833.280	0.41	1226.420	0.015	2001.24	472.17
6.00	250.00	-300.00	1506.	4833.290	0.32	1225.700	0.016	2001.23	471.99
7.00	250.00	-325.00	1501.	4833.120	0.42	1225.800	0.018	2001.08	471.85
8.00	250.00	-350.00	1456.	4832.950	0.38	1225.960	0.019	2000.89	471.67
9.00	250.00	-375.00	1451.	4832.800	0.42	1226.110	0.020	2000.75	471.54
10.00	250.00	-400.00	1447.	4832.630	0.34	1226.270	0.021	2000.55	471.36
11.00	250.00	-425.00	1443.	4832.330	0.42	1226.690	0.022	2000.27	471.14
12.00	250.00	-450.00	1439.	4832.280	0.42	1226.210	0.023	2000.21	470.97
13.00	250.00	-475.00	1433.	4832.400	0.38	1224.680	0.024	2000.32	470.76
14.00	250.00	-500.00	1428.	4832.670	0.39	1222.480	0.025	2000.60	470.59
15.00	250.00	-525.00	1424.	4832.760	0.41	1220.880	0.026	2000.70	470.36
16.00	250.00	-550.00	1418.	4832.380	0.31	1220.370	0.027	2000.28	469.81
17.00	250.00	-575.00	1411.	4834.560	0.38	1207.410	0.027	2002.54	469.51
18.00	250.00	-600.00	1402.	4837.670	0.32	1190.770	0.028	2005.73	469.41
19.00	250.00	-625.00	1353.	4840.410	0.24	1176.880	0.029	2008.53	469.45
20.00	250.00	-650.00	1344.	4843.360	0.28	1158.950	0.029	2011.57	468.96
21.00	250.00	-675.00	1334.	4846.240	0.37	1142.250	0.029	2014.57	468.65
22.00	0.00	0.00	1544.	4832.130	0.36	1234.760	0.003	*	*

F GRID

Line 0, Kutcho South

Date=880828 GMT=-7 SC=1.03059 GB1=2000 GB2=2000 Units=metr BD=2.67 Gf=67 Long=-128.2451 Lat=58.0823

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	0.00	0.00	915.	4729.140	0.21	1742.890	-0.091	*	*
2.00	0.00	0.00	915.	4729.140	0.21	1742.890	-0.091	2000.00	574.55
3.00	0.00	23.68	920.	4728.980	0.19	1744.070	-0.090	1999.83	574.60
4.00	0.00	47.37	924.	4728.570	0.46	1745.720	-0.089	1999.49	574.56
5.00	0.00	71.05	928.	4728.720	0.40	1745.470	-0.087	1999.63	574.64
6.00	0.00	94.74	933.	4727.950	0.34	1748.880	-0.086	1998.82	574.48
7.00	0.00	118.42	935.	4727.450	0.40	1751.070	-0.085	1998.32	574.39
8.00	0.00	142.11	940.	4726.600	0.34	1754.690	-0.084	1997.43	574.20
9.00	0.00	165.79	944.	4726.170	0.36	1756.730	-0.082	1996.99	574.14
10.00	0.00	189.47	947.	4725.830	0.35	1758.190	-0.081	1996.64	574.06
11.00	0.00	213.16	951.	4725.010	0.40	1761.870	-0.080	1995.81	573.94
12.00	0.00	236.84	955.	4724.490	0.40	1764.370	-0.079	1995.28	573.88
13.00	0.00	260.53	958.	4724.100	0.35	1766.390	-0.078	1994.86	573.84
14.00	0.00	284.21	1001.	4723.600	0.32	1768.940	-0.077	1994.34	573.80
15.00	0.00	307.89	1005.	4723.040	0.46	1771.590	-0.075	1993.80	573.77
16.00	0.00	331.58	1008.	4722.360	0.35	1774.850	-0.074	1993.07	573.66
17.00	0.00	355.26	1012.	4721.740	0.34	1778.290	-0.073	1992.43	573.68
18.00	0.00	378.95	1015.	4721.290	0.32	1780.370	-0.071	1991.96	573.60
19.00	0.00	402.63	1020.	4719.940	0.42	1787.530	-0.070	1990.60	573.64
20.00	0.00	426.32	1024.	4719.380	0.36	1791.220	-0.068	1990.01	573.75
21.00	0.00	450.00	1029.	4719.040	0.37	1793.100	-0.066	1989.66	573.76
22.00	0.00	0.00	1218.	4729.100	0.21	1742.890	-0.023	*	*

Line 200E, Kutcho South

Date=880828 GMT=-7 SC=1.03059 GB1=2000 GB2=2000 Units=metr BD=2.67 Gf=67 Long=-128.2432 Lat=58.0823

Station	Line(X)	Stn(Y)	Time	Reading	I.H.	Elev.	TideC.	Obs.Grv.	Bgr.Grv.
1.00	0.00	0.00	915.	4729.140	0.21	1742.890	-0.091	*	*
2.00	200.00	25.00	1158.	4734.880	0.36	1713.150	-0.031	2006.01	574.69
3.00	200.00	50.00	1154.	4734.280	0.29	1717.090	-0.032	2005.37	574.81
4.00	200.00	75.00	1149.	4733.560	0.24	1720.390	-0.034	2004.61	574.68
5.00	200.00	100.00	1145.	4733.130	0.25	1722.470	-0.036	2004.17	574.63
6.00	200.00	125.00	1142.	4732.640	0.31	1724.260	-0.037	2003.68	574.48
7.00	200.00	150.00	1139.	4732.170	0.31	1726.530	-0.038	2003.20	574.42
8.00	200.00	175.00	1135.	4731.650	0.28	1728.770	-0.039	2002.65	574.29
9.00	200.00	200.00	1131.	4731.090	0.31	1731.420	-0.041	2002.08	574.23
10.00	200.00	225.00	1125.	4730.640	0.28	1733.620	-0.043	2001.61	574.17
11.00	200.00	250.00	1121.	4730.200	0.33	1735.490	-0.045	2001.17	574.08
12.00	200.00	275.00	1117.	4729.650	0.38	1738.180	-0.047	2000.61	574.04
13.00	200.00	300.00	1114.	4729.260	0.32	1740.250	-0.048	2000.19	574.00
14.00	200.00	325.00	1110.	4728.480	0.25	1743.960	-0.050	1999.36	573.89
15.00	200.00	350.00	1108.	4727.630	0.37	1748.220	-0.050	1998.52	573.87
16.00	200.00	375.00	1104.	4726.480	0.26	1753.730	-0.052	1997.31	573.71
17.00	200.00	400.00	1100.	4725.410	0.31	1759.500	-0.054	1996.22	573.74
18.00	200.00	425.00	1057.	4724.430	0.35	1764.300	-0.055	1995.22	573.67
19.00	200.00	450.00	1054.	4723.580	0.44	1768.930	-0.056	1994.37	573.71
20.00	200.00	475.00	1050.	4722.560	0.30	1773.870	-0.058	1993.27	573.57
21.00	0.00	0.00	1218.	4729.100	0.21	1742.890	-0.023	*	*

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,639

ESSO MINERALS CANADA

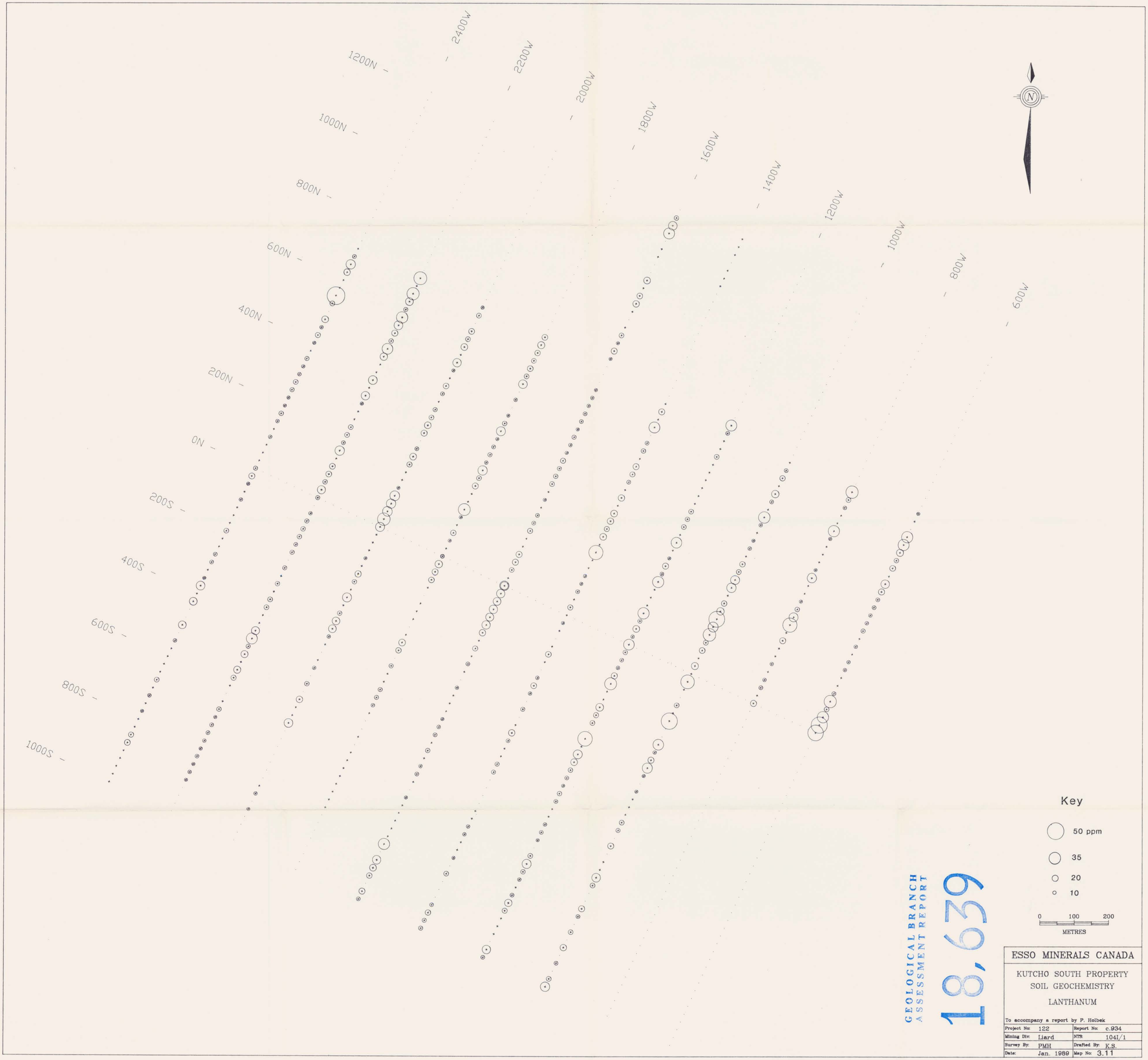
KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY
(Cr+Ni+4Co+20Mg)/4

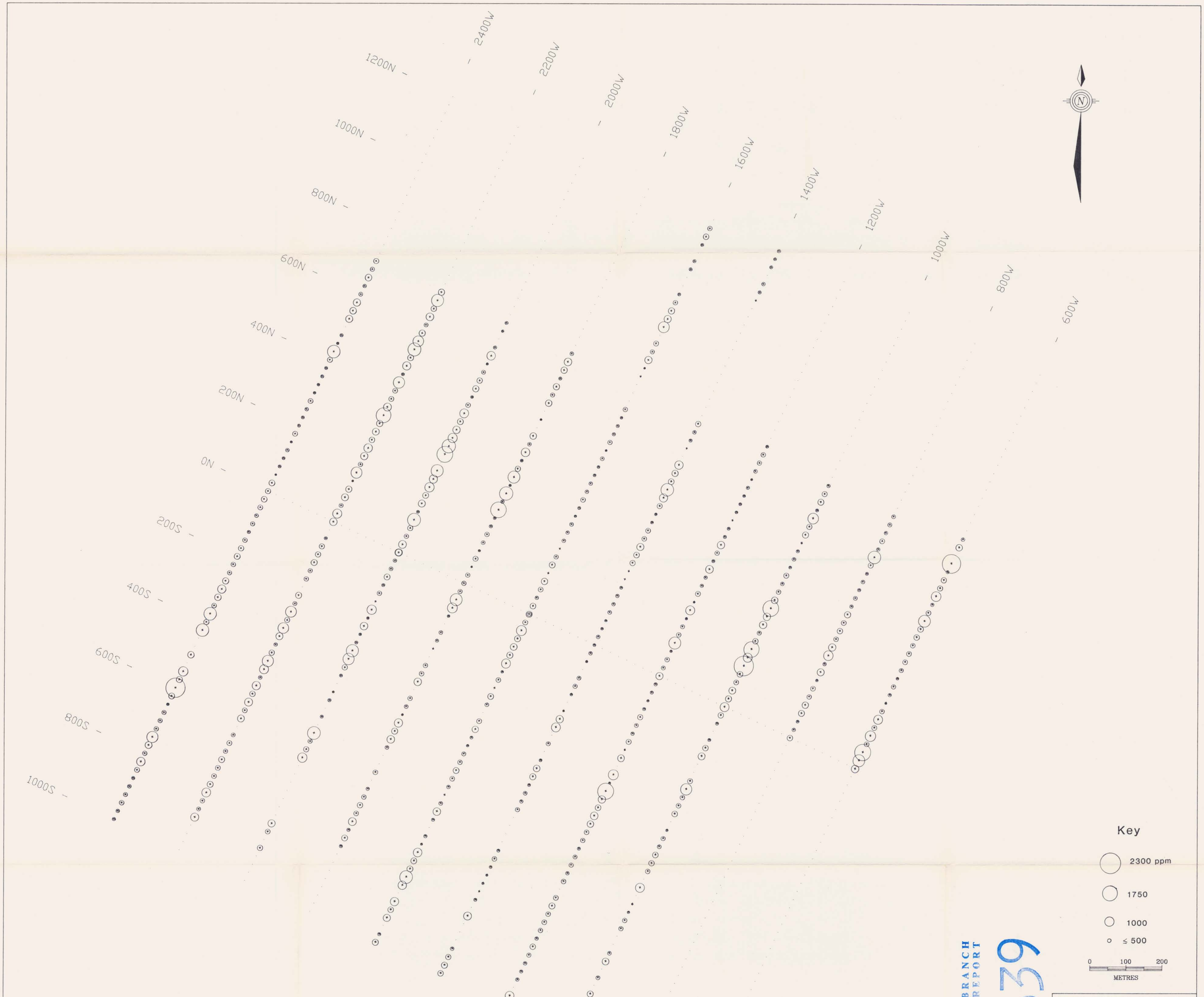
To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.14

2400W
2200W
2000W
1800W
1600W
1400W
1200W
1000W
800W
600W
1200N
1000N
800N
600N
400N
200N
0N
200S
400S
600S
800S
1000S
N
Key
145 ppm
85
45
15 ppm
0 100 200
METRES
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,639
ESSO MINERALS CANADA
KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY
NICKEL
To accompany a report by P. Holbek
Project No: 122
Report No: c.934
Mining Div: Liard
NTS: 104I/1
Survey By: PMH
Drafted By: K.S.
Date: Jan. 1989
Map No: 3.13

1200N
1000N
800N
600N
400N
200N
0N
200S
400S
600S
800S
1000S
2400W
2200W
2000W
1800W
1600W
1400W
1200W
1000W
800W
600W
N
Key
30%
20%
15%
≥ 6%
0
100
200
METRES
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,639
ESSO MINERALS CANADA
KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY
IRON
To accompany a report by P. Holbek
Project No: 122
Report No: c.934
Mining Div: Liard
NTS: 104I/1
Survey By: PMH
Drafted By: K.S.
Date: Jan. 1989
Map No: 3.12


1200N
1000N
800N
600N
400N
200N
0N
200S
400S
600S
800S
1000S
2400W
2200W
2000W
1800W
1600W
1400W
1200W
1000W
800W
600W
N
Key
50 ppm
35
20
10
0
100
200
METRES
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,639
ESSO MINERALS CANADA
KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY
LANTHANUM
To accompany a report by P. Holbek
Project No: 122
Report No: c.934
Mining Div: Liard
NTS: 104I/1
Survey By: PMH
Drafted By: K.S.
Date: Jan. 1989
Map No: 3.11



GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,639

ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

MANGANESE

To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.10

Key

◯	3.0%
○	1.8%
○	1.2%
∘	0.4%

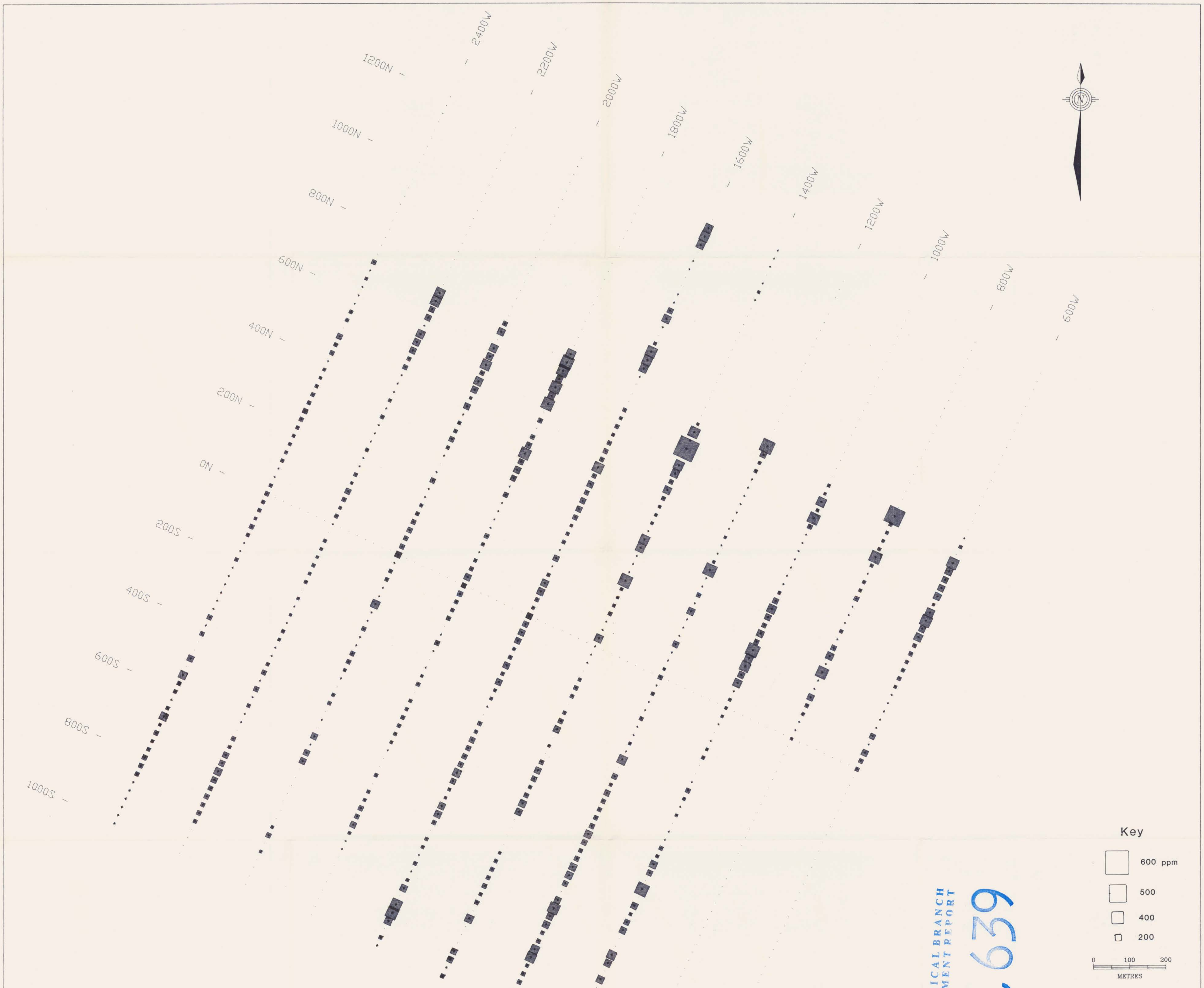
ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

CALCIUM

To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.9



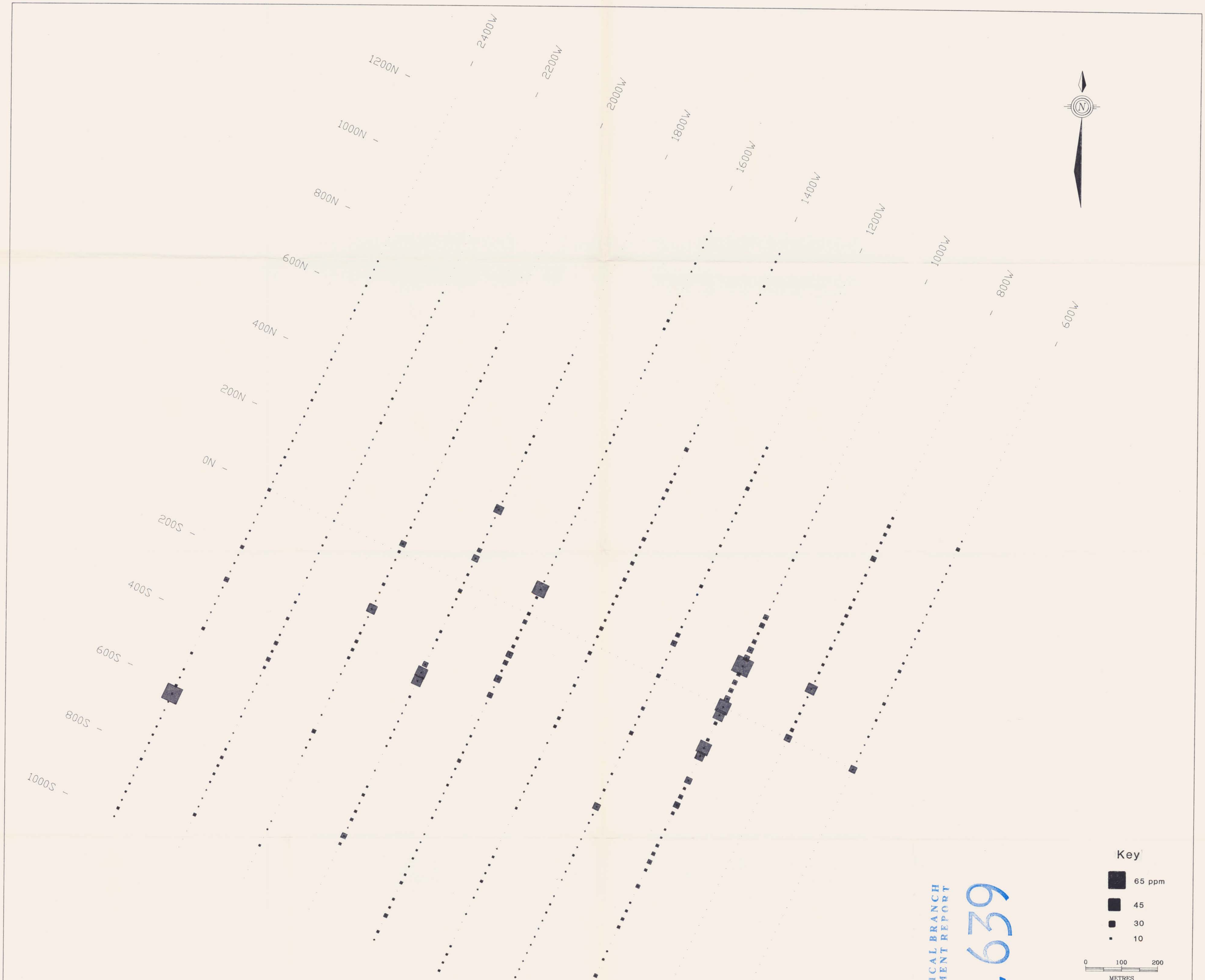
ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

BARIUM

To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.8



ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

ARSENIC

To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.7


1200N
1000N
800N
600N
400N
200N
0N
200S
400S
600S
800S
1000S
2400W
2200W
2000W
1800W
1600W
1400W
1200W
1000W
800W
600W
N
Key
250
175
75
0 100 200
METRES
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,639
ESSO MINERALS CANADA
KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY
(Cu-Zn/2-10Pb-100Ag)/4
To accompany a report by P. Holbek
Project No: 122
Report No: c.934
Mining Div: Liard
NTS: 104I/1
Survey By: PMH
Drafted By: K.S.
Date: Jan. 1989
Map No: 3.6

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,639

ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

LEAD

To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.5

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,639

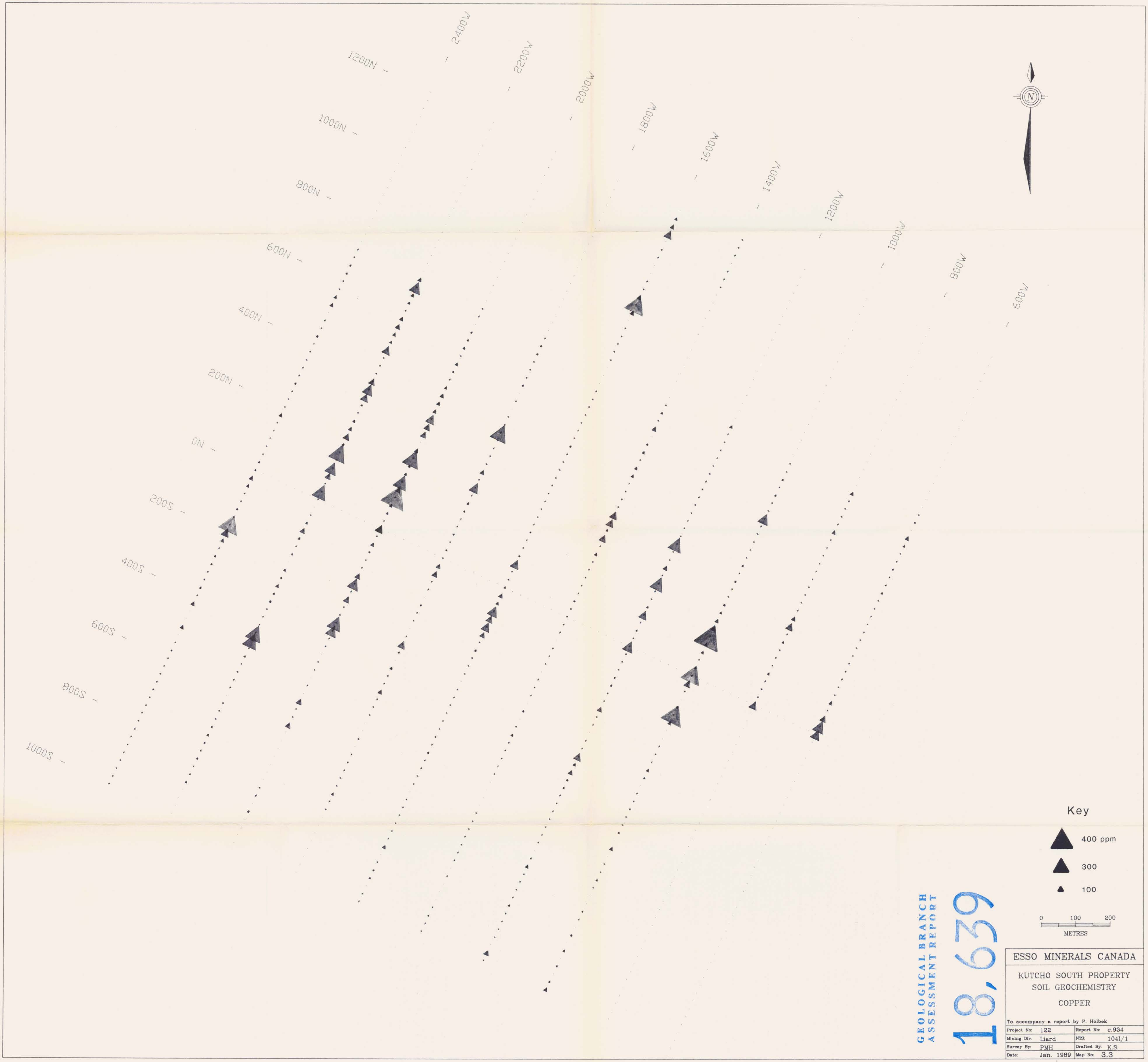
ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

ZINC

To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.4



GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,639

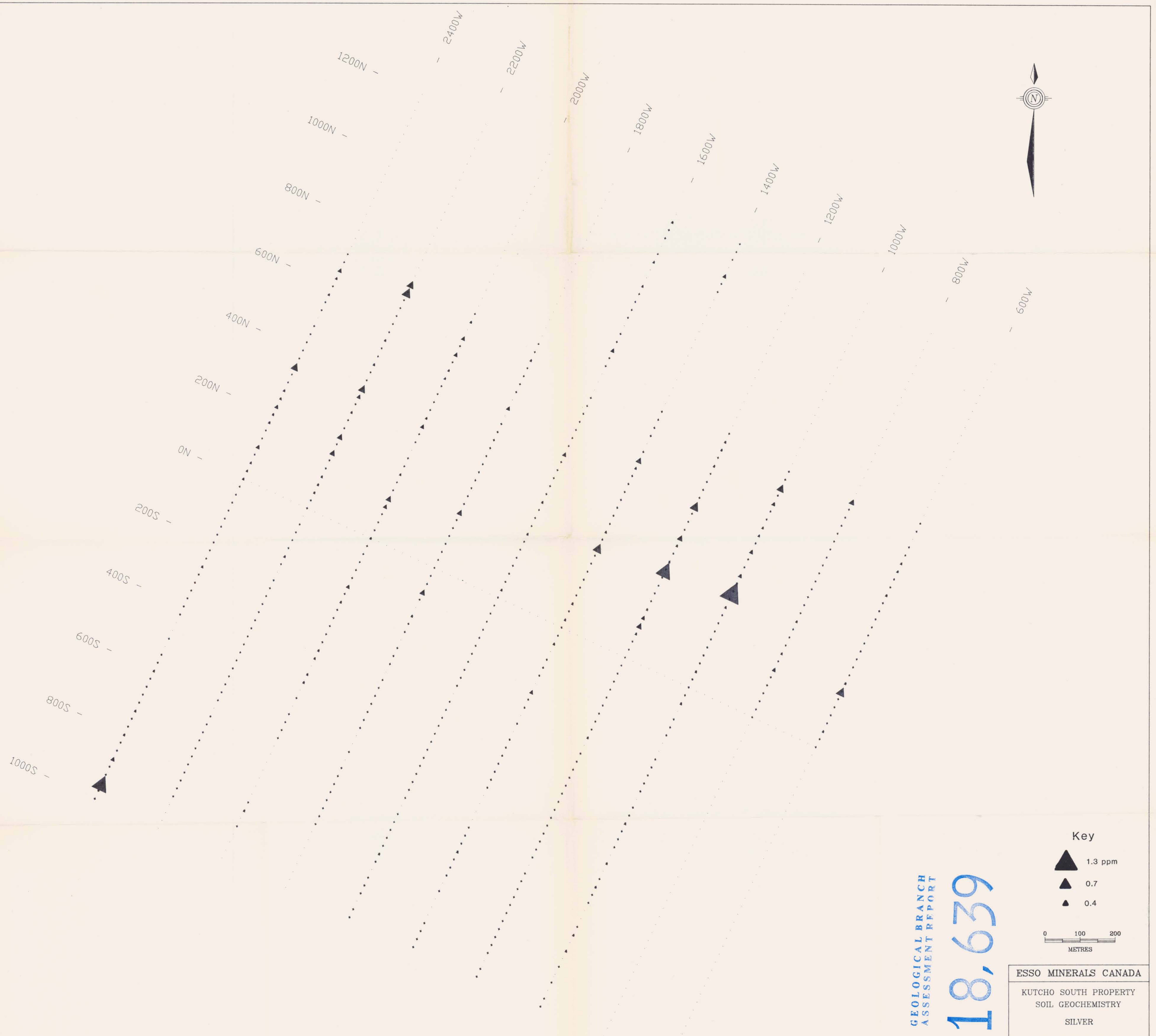
ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

COPPER

To accompany a report by P. Holbek

Project No:	122	Report No:	c.934
Mining Div:	Liard	NTS:	104I/1
Survey By:	PMH	Drafted By:	K.S.
Date:	Jan. 1989	Map No:	3.3



ESSO MINERALS CANADA

KUTCHO SOUTH PROPERTY
SOIL GEOCHEMISTRY

SILVER

To accompany a report by P. Holbek

Project No: 122	Report No: c.934
Mining Div: Liard	NTS: 104I/1
Survey By: PMH	Drafted By: K.S.
Date: Jan. 1989	Map No: 3.2

9	DYKE	FELDSPAR-HORNBLENDE PORPHYRY ANDESITE DIKES
8	DIOR	DIORITE, MICRODIORITE INTRUSIVE
7	LMST	SINWA (?) LIMESTONE; ARGILLACEOUS LIMESTONE
6	CHTF SEXL	TUFFACEOUS CHERTS: MAY BE PARTLY EXHALATIVE IN ORIGIN SILICA EXHALITE: LAMINATED AMORPHOUS QUARTZ AND FINE GRAINED PYRITE
5	QCXT QFXT	QUARTZ CRYSTAL TUFFS QUARTZ-FELDSPAR CRYSTAL TUFFS
4	ASTF	ASH TUFFS: VARIABLE COMPOSITION
3	LATF LXTF	LITHIC ASH TUFFS; LITHIC CRYSTAL TUFFS; FINE GRAINED FELSIC TUFFS; QUARTZ-SERICITE SCHIST
2	MTFW	MAFIC TUFFS AND WACKES: FINE GRAINED CHLORITIC SCHISTS WITH FRAGMENTAL TO EPICLASTIC TEXTURES
1	BSLT	BASALT: FINE TO MEDIUM GRAINED CHLORITIC SCHISTS; COMMONLY WITH COARSE EPIDOTE KNOTS, MAY INCLUDE SOME MTFW

LIMITS OF OUTCROP
GEOLOGICAL CONTACT - DEFINED, INFERRED, APPROXIMATE
FOLIATION, BEDDING
GEOLOGICAL STATION LOCATION
TRENCH
ROCK GEOCHEMICAL SAMPLE LOCATION
TREND OF EM CONDUCTOR DEFINED BY GENIE SURVEY; STRONG, MODERATE
FAULT
SULPHIDE RICH FLOAT

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,639

SCALE 1:5000

0 250 m

REVISIONS

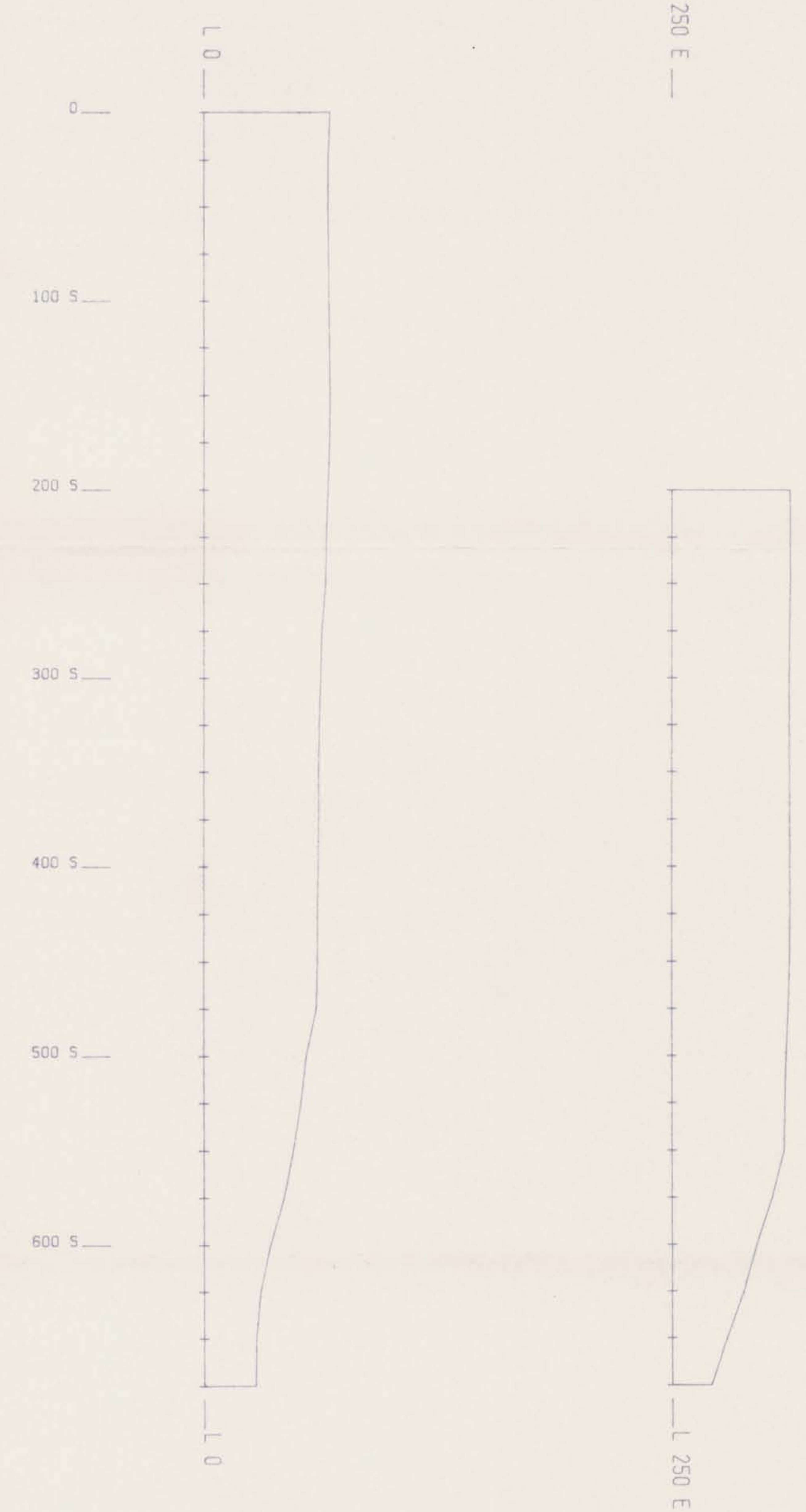
By	Date	Approv. By

ESSO MINERALS CANADA

KUTCHO SOUTH PROJECT
GEOLOGY OF TARGET "C"

To accompany a report by

Project No: 122		Report No:	c.934
Mining Div: Liard		NTS:	104I
Survey By: PH,PT,DH,HM		Drafted By:	PH
Date: March 89		Map No:	2.2



Profile scale : 1cm. = 50m.

Grid line = base value of 1100m.

SCALE 1:2500

0 25 50 75 100 meters

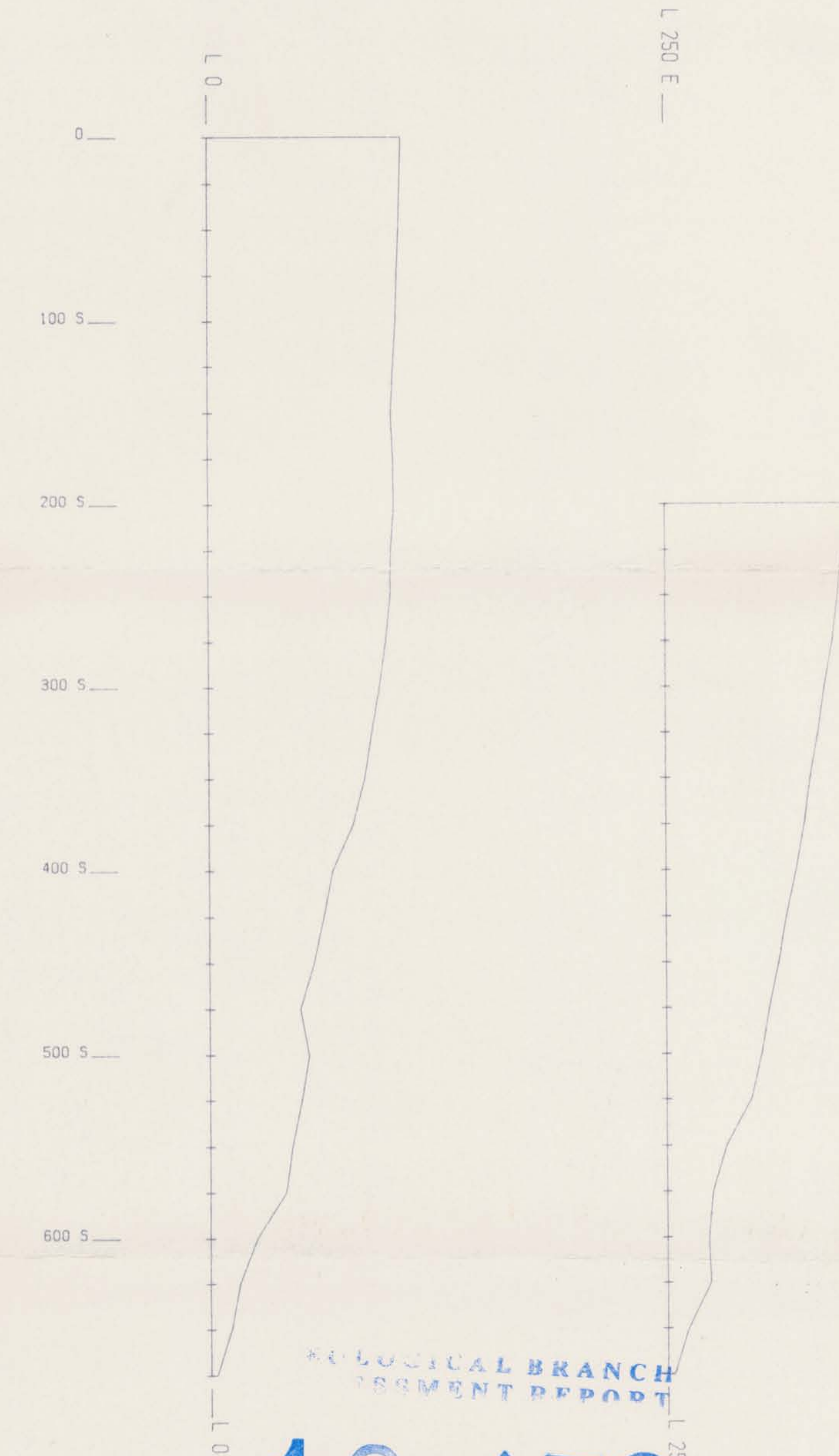
REVISIONS		
By	Date	Approv.By

ESSO MINERALS CANADA

KUTCHO
GRID ''K''
ELEVATION
PROFILE MAP

To accompany a report by P.H. & Z.D.

Project No:		Report No:	
Mining Div:		N.T.S.:	
Survey By:	Z.D.	Drafted By:	S.L.
Date: 01/12/88		Map No:	4.7



Profile scale : 1cm. = 1.0 mgals

Grid line = base value of 425.0

SCALE 1:2500

0 25 50 75 100 meters

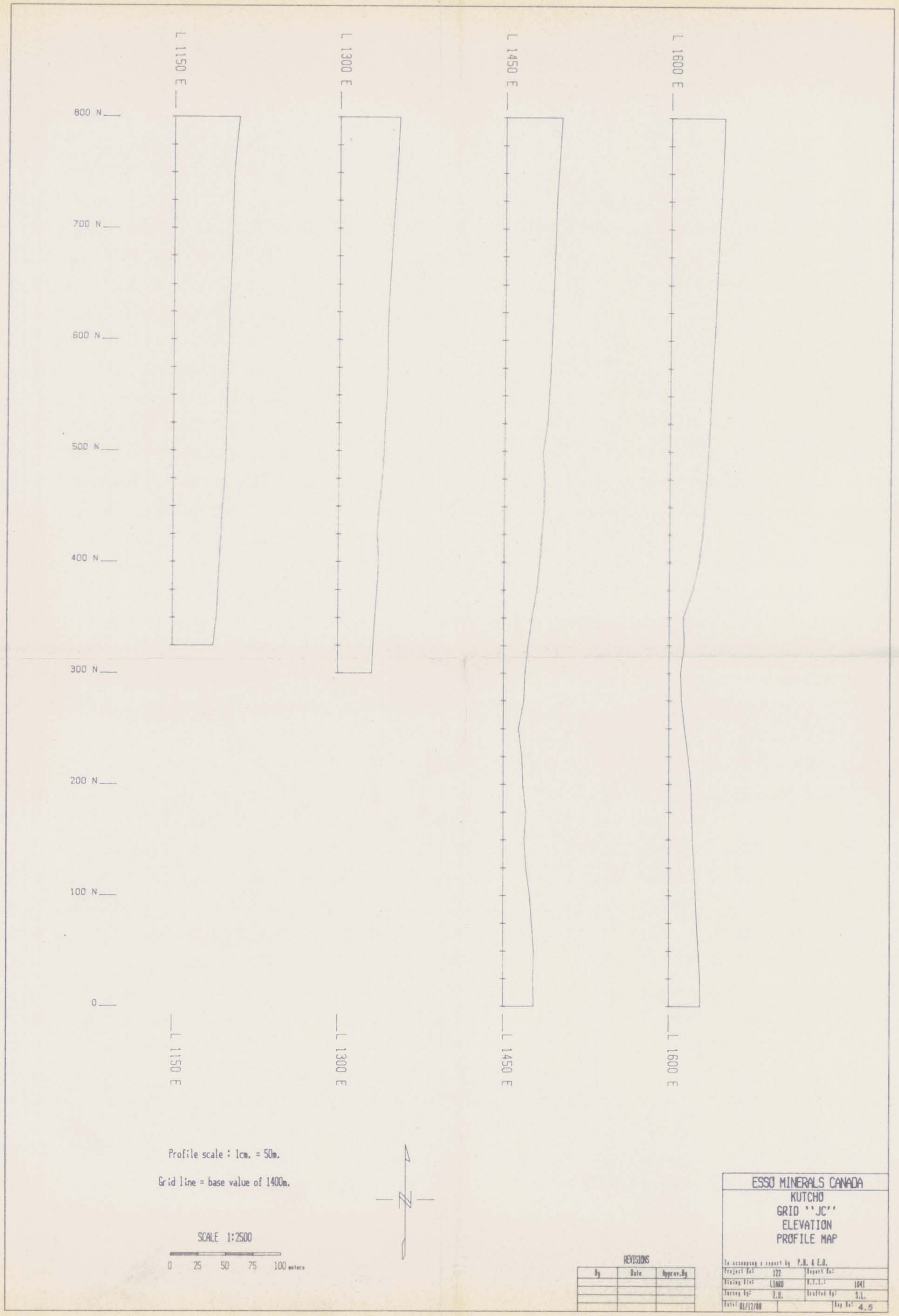
REVISIONS		
By	Date	Approv.By

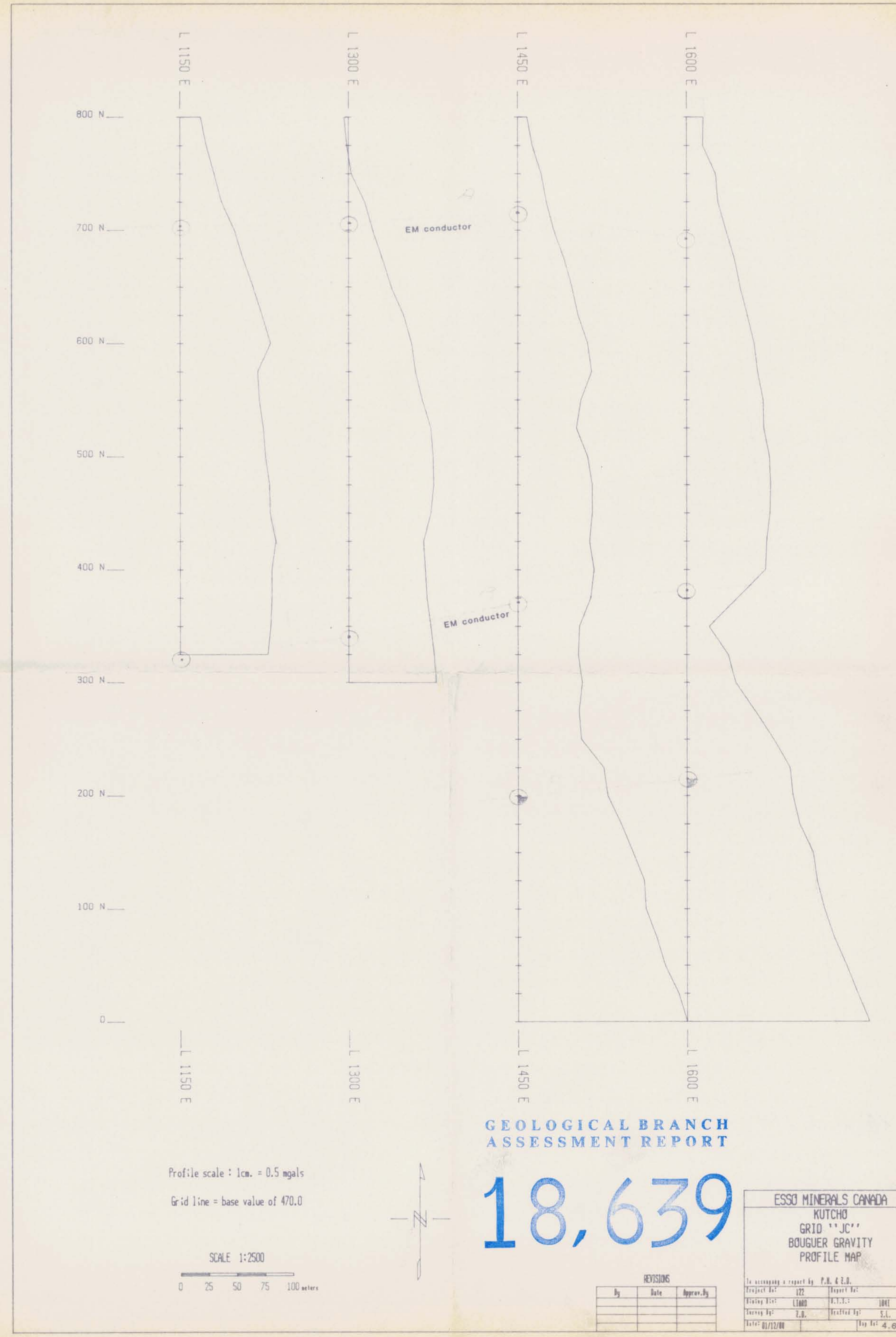
ESSO MINERALS CANADA

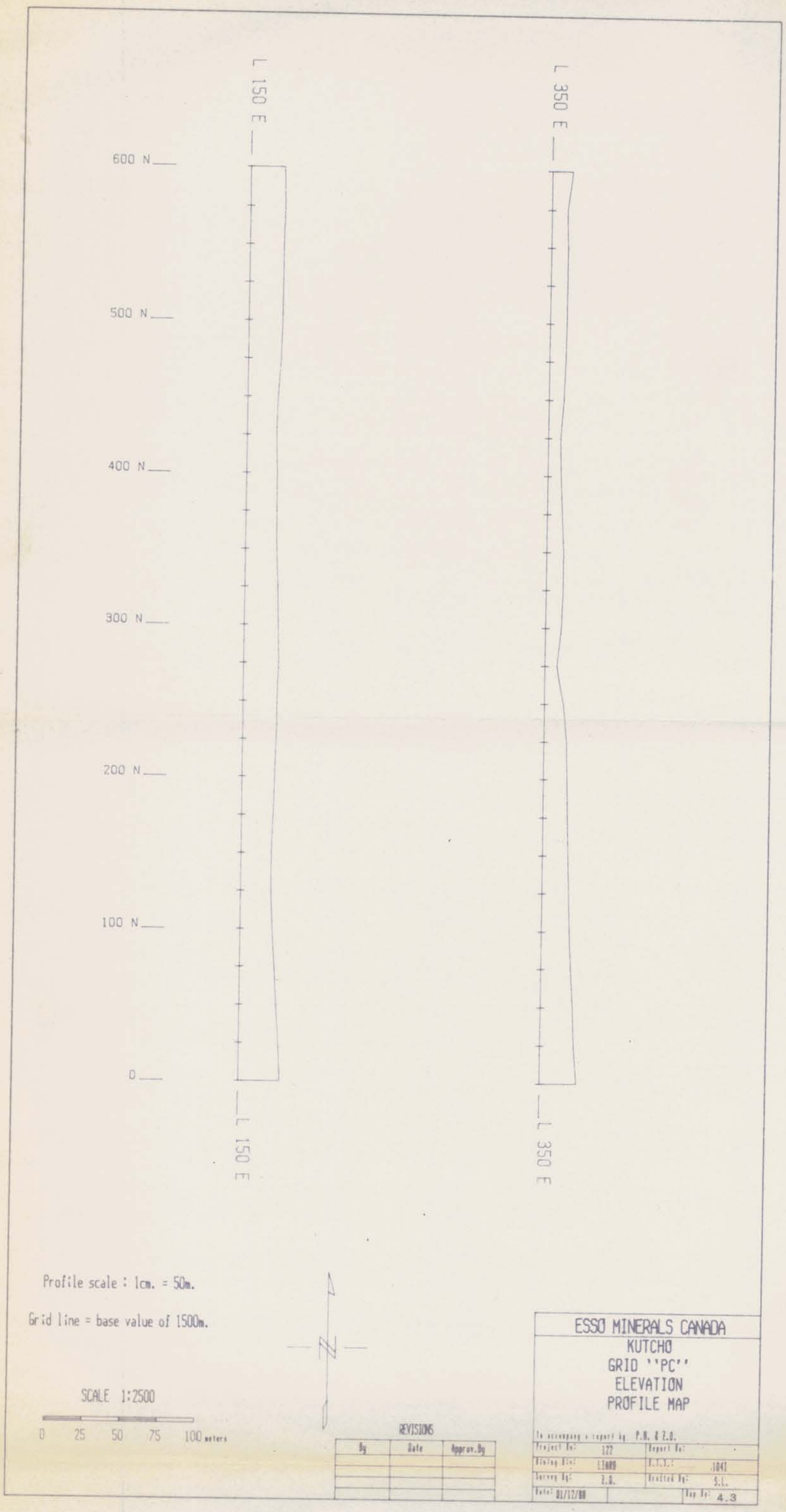
KUTCHO
GRID ''K''
BOUGUER GRAVITY
PROFILE MAP

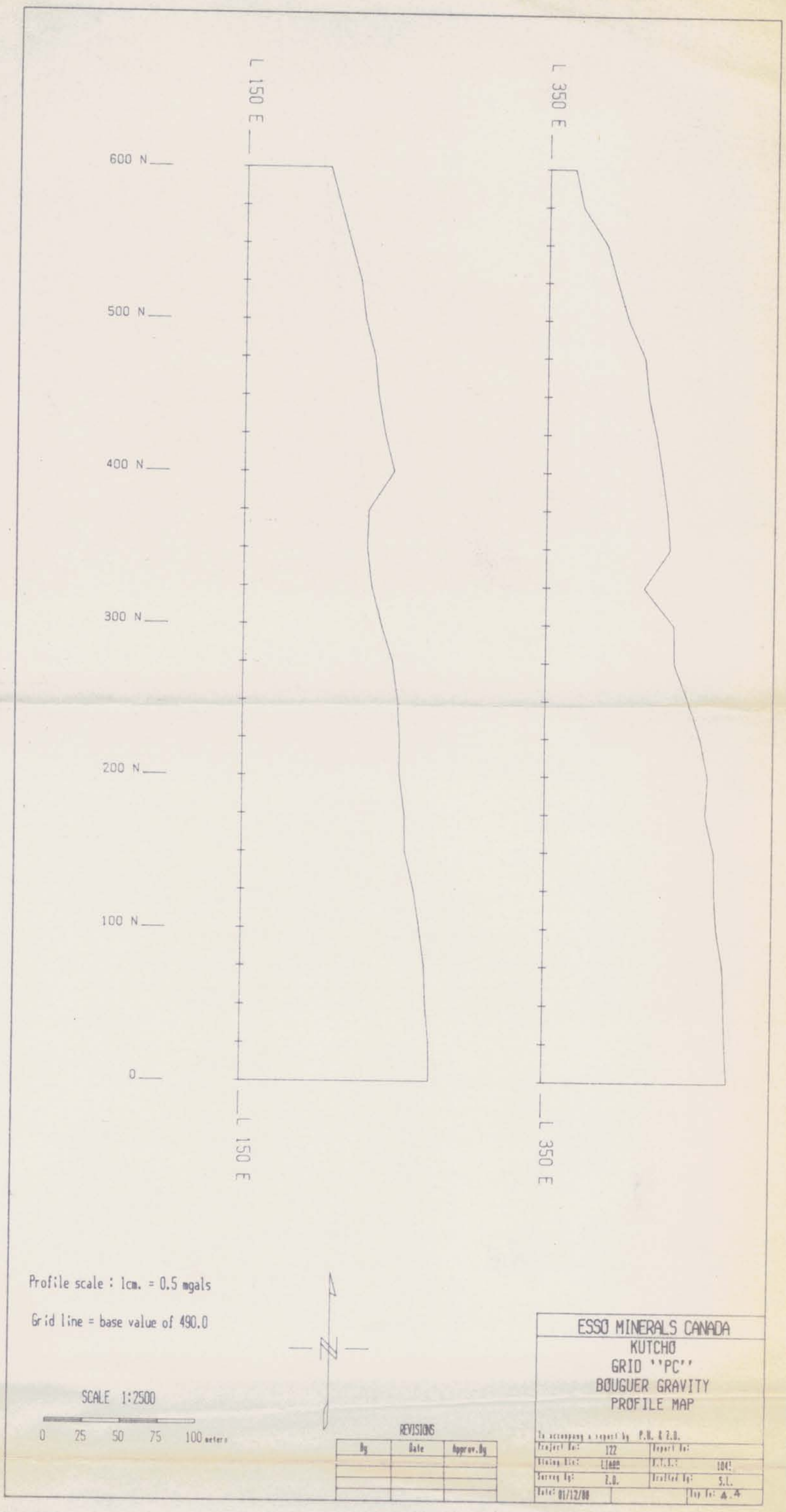
To accompany a report by P.H. & Z.D.

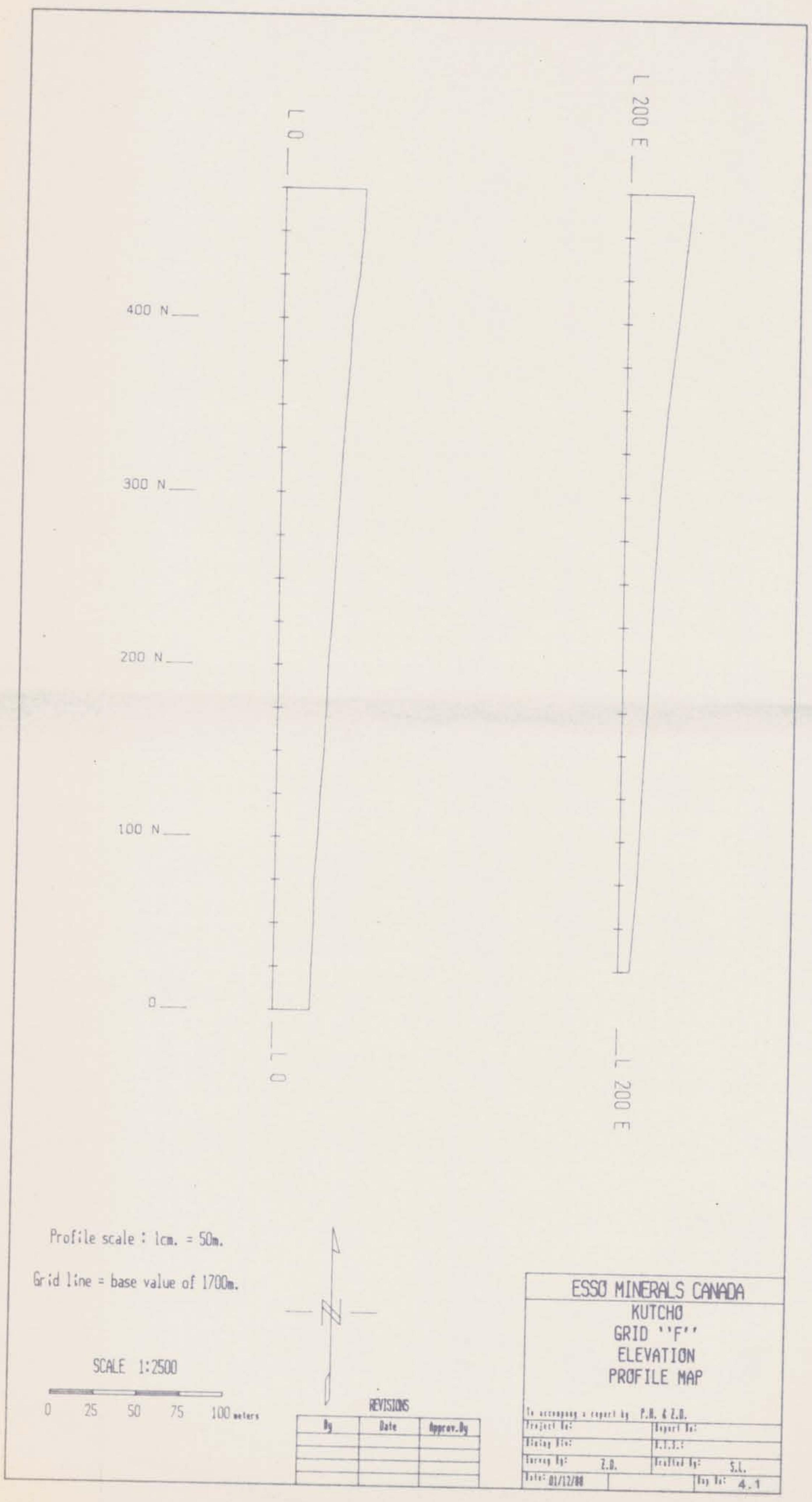
Project No:	122	Report No:	
Mining Div:	LIARD	N.T.S.:	104I
Survey By:	Z.D.	Drafted By:	S.L.
Date: 01/12/88		Map No:	4.8

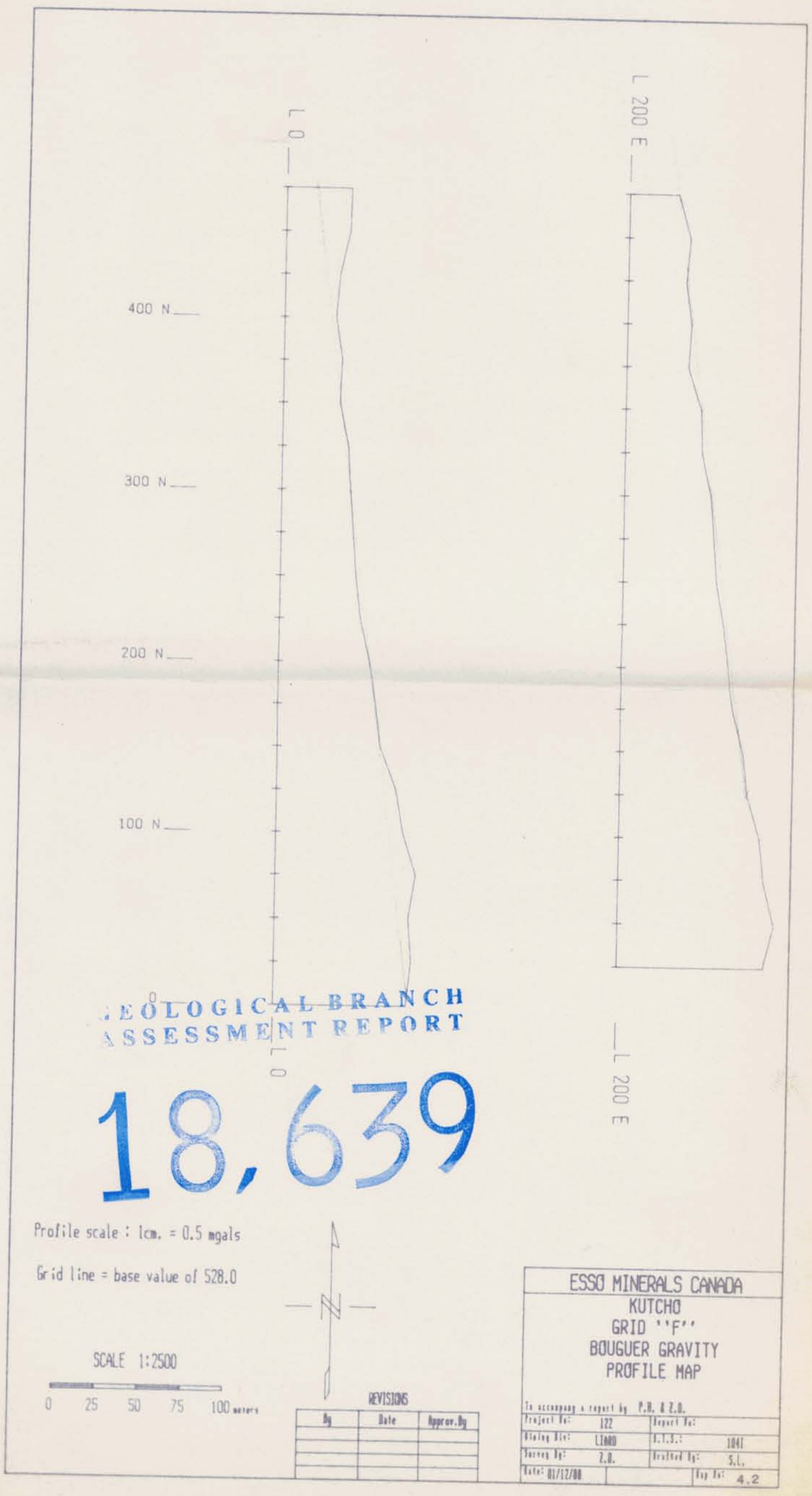

L 1150 E
L 1300 E
L 1450 E
L 1600 E
800 N
700 N
600 N
500 N
400 N
300 N
200 N
100 N
0
Profile scale : 1cm. = 50m.
Grid line = base value of 1400m.
SCALE 1:2500
0 25 50 75 100 meters
REVISIONS
By
Date
Approv.By
ESSO MINERALS CANADA
KUTCHO
GRID ''JC''
ELEVATION
PROFILE MAP
To accompany a report by P.H. & Z.D.
Project No: 122
Mining Div: LIARD
N.T.S.: 104I
Survey By: Z.D.
Drafted By: S.L.
Date: 01/12/88
Map No: 4.5


L 1150 E
L 1300 E
L 1450 E
L 1600 E
800 N
700 N
600 N
500 N
400 N
300 N
200 N
100 N
0
EM conductor
EM conductor
Profile scale : 1cm. = 0.5 mgals
Grid line = base value of 470.0
SCALE 1:2500
0 25 50 75 100 meters
REVISIONS
By
Date
Approv.By
ESSO MINERALS CANADA
KUTCHO
GRID ''JC''
BOUGUER GRAVITY
PROFILE MAP
To accompany a report by P.H. & Z.D.
Project No: 122
Mining Div: LIARD
N.T.S.: 104I
Survey By: Z.D.
Drafted By: S.L.
Date: 01/12/88
Map No: 4.6


L 150 E
L 350 E
600 N
500 N
400 N
300 N
200 N
100 N
0
Profile scale : 1cm. = 50m.
Grid line = base value of 1500m.
SCALE 1:2500
0 25 50 75 100 meters
REVISIONS
By
Date
Approv.By
ESSO MINERALS CANADA
KUTCHO
GRID ''PC''
ELEVATION
PROFILE MAP
P.H. & Z.D.
122
Z.D.
S.L.
01/12/88
4.3


L 150 E
L 350 E
600 N
500 N
400 N
300 N
200 N
100 N
0
Profile scale : 1cm. = 0.5 mgals
Grid line = base value of 490.0
SCALE 1:2500
0 25 50 75 100 meters
REVISIONS
By
Date
Approv.By
ESSO MINERALS CANADA
KUTCHO
GRID ''PC''
BØUGUER GRAVITY
PROFILE MAP
P.H. & Z.D.
122
Z.D.
S.L.
01/12/88
4.4


L 0
L 200 E
400 N
300 N
200 N
100 N
0
Profile scale : 1cm. = 50m.
Grid line = base value of 1700m.
SCALE 1:2500
0 25 50 75 100 meters
REVISIONS
By
Date
Approv.By
ESSO MINERALS CANADA
KUTCHO
GRID ''F''
ELEVATION
PROFILE MAP
P.H. & Z.D.
Z.D.
S.L.
01/12/88
4.1


L 0
L 200 E
400 N
300 N
200 N
100 N
Profile scale : 1cm. = 0.5 mgals
Grid line = base value of 528.0
SCALE 1:2500
0 25 50 75 100 meters
REVISIONS
By
Date
Approv.By
ESSO MINERALS CANADA
KUTCHO
GRID ''F''
BOUGUER GRAVITY
PROFILE MAP
P.H. & Z.D.
122
Z.D.
S.L.
01/12/88
4.2