# GEOCHEMICAL & GEOPHYSICAL REPORT

on the

# ZUMAR PROPERTY

VERNON MINING DIVISION
BRITISH COLUMBIA

LATITUDE 50° 1' NORTH
LONGITUDE 119° 38' WEST

NTS MAPSHEET 82L/4E

for

SKYWORLD RESOURCES & DEVELOPMENT LTD.
#2460-555 WEST HASTINGS STREET
VANCOUVER, BRITISH COLUMBIA

by

**Douglas H. Wood, B.Sc., FGAC**
**Consulting Geologist**

**February 6, 1989**

18713

# ARIS SUMMARY SHEET

District Geologist, Kamloops — Off Confidential: 90.05.02

ASSESSMENT REPORT 18713 — MINING DIVISION: Vernon

PROPERTY: Zumar
LOCATION: LAT 50 01 00 LONG 119 38 00
UTM 11 5543587 311347
NTS 082L04E
CLAIM(S): Zumar 2,Zumar 4
OPERATOR(S): Skyworld Res. & Dev. Whitewater Res.
AUTHOR(S): Wood, D.H.
REPORT YEAR: 1989, 53 Pages
COMMODITIES SEARCHED FOR: Copper
KEYWORDS: Paleozoic,Andesites,Tuffs,Quartzites,Quartz veins,Pyrite Chalcopyrite
WORK DONE: Geochemical,Geophysical,Physical
EMGR 15.8 km;VLF
Map(s) - 1; Scale(s) - 1:2500
LINE 17.0 km
MAGG 15.8 km
Map(s) - 1; Scale(s) - 1:2500
SOIL 411 sample(s) ;ME
Map(s) - 6; Scale(s) - 1:2500
RELATED REPORTS: 15400,16416
MINFILE: 082LSW111

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## 1.0 SUMMARY

A mineral exploration program conducted over the Zumar 2 and 4 Claims during late November and early December 1988 has resulted in a reinterpretation of an area of anomalous copper in soils and determined that the overall chemistry and structural features (derived from a VLF-EM interpretation) are consistent with a north-northeasterly striking zone of copper mineralization.

Anomalously high values for copper in soils were noted in two distinct clusters consistent with previous property soil surveys - the Zumar vein on the Zumar 4 claim and a copper-silver anomaly located in the southwest portion of the Zumar 4 claim (Wilmot, 1987; Morrison, 1986).

Gold and silver geochemistry were found to be of limited value in outlining either the Zumar vein or the Zumar 4 target area.

By examining several other trace elements including Calcium, Phosphorus, Potassium and Vanadium, the anomalous clusters of copper in soils are shown to be similar while existing in separate lithological and structural environments. The Zumar vein is located in what appears to be a roughly east-west quartz fracture filling system with an associated VLF-EM conductor and a local magnetic high. The anomalous zone for copper within the Zumar 4 is associated with a strong north-northeasterly trending VLF-EM conductor and also with a local magnetic high.

The similarity in chemistry between the known mineralization at the Zumar vein and in the southern portion of the Zumar 4 claim is interpreted to be the result of a syngenetic source for mineralization.

A two phase continued exploration program is recommended to further test the economic potential of the Zumar 4 target area

and other portions of the Zumar claims not as yet explored. Phases II should be success contingent upon the results of the first phase programs.

The first phase should include a detailed geological, geochemical, geophysical survey of the Zumar 4 target area in conjunction with further reconnaissance surveys elsewhere on the Zumar claims. The second phase consisting of surface bulldozer trenching and stripping is recommended to test detailed survey targets. Upon the completion of the second phase, should results warrant further exploration, a program of upto 1000 meters of diamond drilling is suggested. A separate budget would be required for any drilling programs.

The estimated cost of the first phase is $79,700 and for the second phase is $19,200 for a total of $98,900. These further expenditures on the Zumar claims are well warranted by the encouraging results of the recent program.

Respectfully submitted,

Douglas H. Wood

Douglas H. Wood, B.Sc., FGAC
Consulting Geologist

GEOLOGICAL ASSOCIATION OF CANADA
DOUGLAS H. WOOD
FELLOW

## 2.0 INTRODUCTION

### 2.1 Terms of Reference

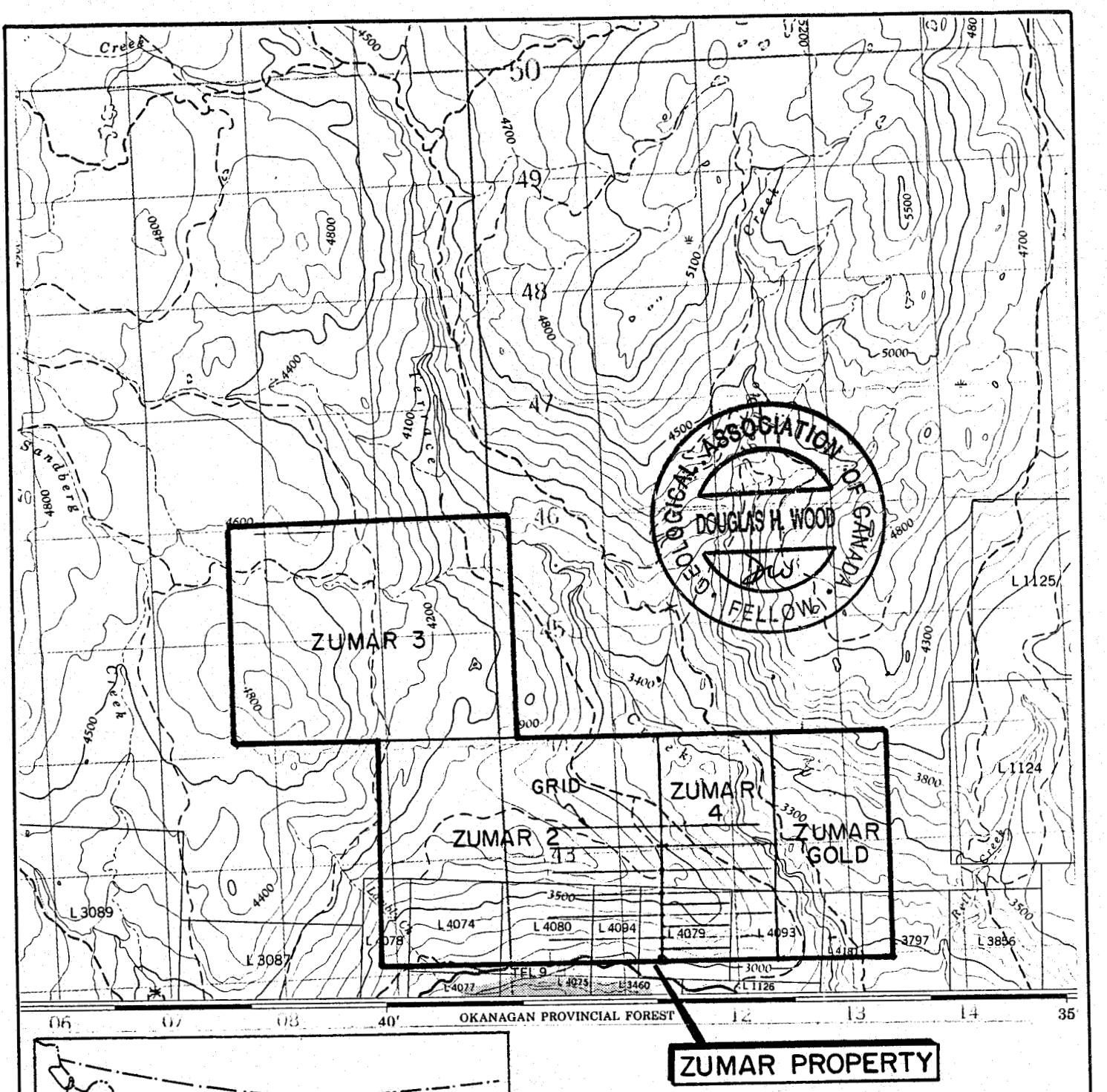
Pursuant to a request from the directors of Skyworld Resources and Development Ltd., the present report summarizes the results of prior exploration programs conducted over the Zumar property and details the results of the most recent field work completed between November 28 and December 12, 1988.

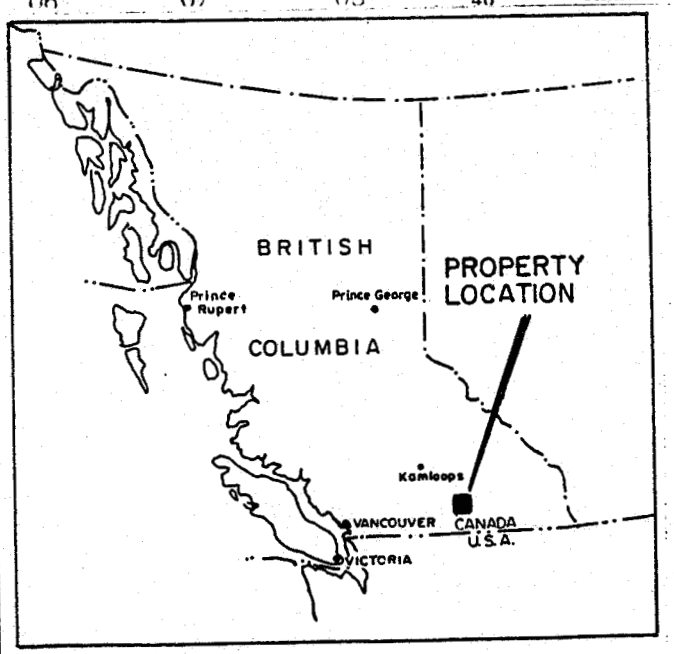
The recent field program included reconnaissance scale soil sampling on east-west grid lines in conjunction with magnetometer and VLF-EM surveys. This work was conducted by crews and contractors employed by Laroth Engineering Ltd. of Vancouver, B.C. under the supervision of Mr. E.N. Larabie, P.Eng. Mr. D.H. Wood, Consulting Geologist, assisted with this program and visited the property during May 1988 and on November 26, 1988 prior to the commencement of exploration work.

The purpose of these surveys was to determine the probability of north-south trending gold mineralization similar to that reported to be present on the Brett Claims located approximately 20 km north of the Zumar property.

### 2.2 Location and Access

The Zumar property is located on the north side of Lambly Creek between Terrace and Sandberg Creek and is situated approximately 30 km by road northwest of the city of Kelowna, B.C. The property is accessed via Westside road from Kelowna, north to the Bear Creek (Lambly Creek) logging road and then for 16 km west. The L.C.P. (legal corner post) for the Zumar 2 and 4 claims is situated some 200 meters due north of the 16 km post on the north side of the logging road.




SKYWORLD RESOURCE & DEVELOPMENT LTD.

ZUMAR PROPERTY

# LOCATION MAP

N.T.S. 82L-4E

VERNON M.D., B.C.

0 1 2 KM.

| | |
|---|---|
| SCALE : 1:50,000 | DATE : JAN. 1989 |
| DRAWN BY: D.W. | FIGURE Nº. 1 |

CHONG

The property is located on the eastern half of NTS mapsheet 82L/4 and is centered at Latitude 50° 01' North, Longitude 119° 38' West.

## 2.3 Topography, Climate and Vegetation

The property lies within the Okanogan Plateau area of the British Columbia Interior Region. Elevations on the property range from 915 meters (3000 feet) at the southern boundary of the claims to over 1280 meters (4200 feet) at the northeast corner of the Zumar 2 claim. Slopes are gentle and ridge tops are rounded.

The property area lies within the rainshadow of the Coast Mountains with precipitation being sparse and occurring mainly as snow during the winter months. Snow accumulation is generally less than 1 meter over the winter, allowing year round access to the property. Water for mining and milling purposes is available from local drainages.

Vegetation on the property is open pine and fir in most areas. Much of the property area has been logged over the past 20 to 30 years. Gully areas and north facing slopes tend to have thick growths of underbrush and deciduous trees. Abundant timber is available for mining purposes.

## 2.4 Property Status

The Zumar property comprises four metric grid mining claims totalling 56 units and covering some 1400 hectares. The claims are in good standing and are owned by Skyworld Resources and Development Ltd.

The particulars of the Zumar claims are as follows:

| Claim Name | Rec. # | No. Units | Expiry Date |
|---|---|---|---|
| Zumar Gold | 2157 | 8 | Oct. 3, 1992 |
| Zumar 2 | 711 | 20 | Oct. 19, 1990 |
| Zumar 3 | 2090 | 20 | May 2, 1989 |
| Zumar 4 | 2026 | 8 | Nov. 1, 1991 |

During the course of the recent field program several of the key claim posts were examined and found to be well and legally located.

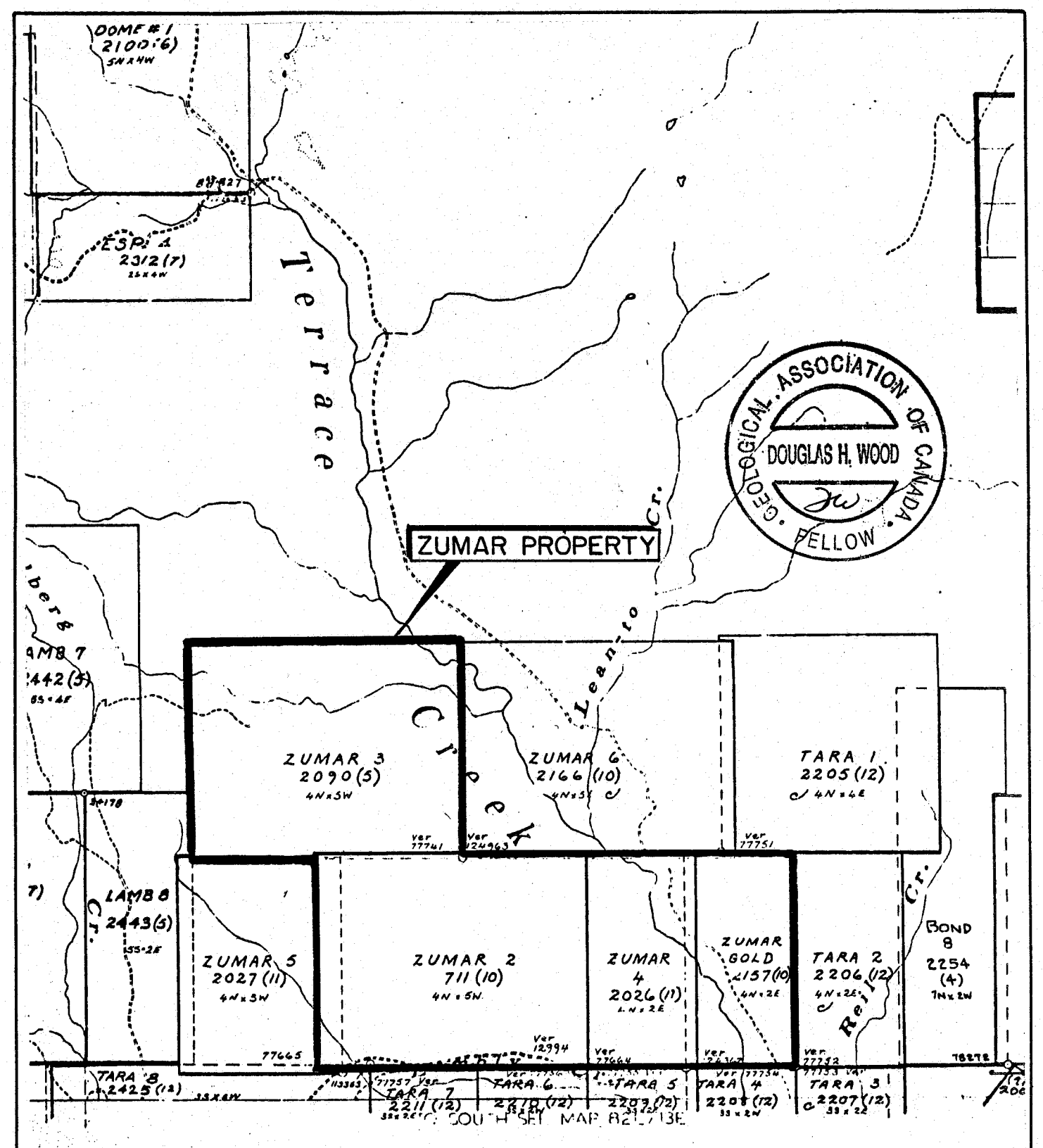
The writer has not verified title to any of these claims as this was beyond the scope of the present report and should be covered by an opinion provided by the company's counsel.

## 2.5 Survey Procedures

Grid emplacement was accomplished by chain and compass survey with stations on all east-west lines marked by two colour survey flagging every 25 meters. A cut and picket baseline was established with stations marked at 50 meter intervals north from the L.C.P. for the Zumar 2 and 4 claims. Stations on all east-west grid lines were numbered east or west of the baseline. Slope corrections were made between stations on all lines.

The east-west grid lines were spaced at 200 meter intervals for 1000 meters to either side of the baseline. Within the southeast portion of the grid, an additional three fill-in grid lines were placed for 600 meters east of the baseline in an area where previous surveys indicated a north-south trend in silver geochemistry.

Soils were collected at 25 meter intervals for the 600 meters east of the baseline on the 100 meter spaced lines from 0+00N to




| SKYWORLD RESOURCE & DEVELOPMENT LTD. | |
|---|---|
| ZUMAR PROPERTY | |
| CLAIM MAP | |
| N.T.S. 82L-4E | VERNON M.D., B.C. |
| 0 1 2 KM. | |
| SCALE : 1:50,000 | DATE : JAN. 1989 |
| DRAWN BY: D.W. | FIGURE Nº. 2 |

CHONG

6+00N and at 50 meter intervals elsewhere. Soil samples were placed in kraft paper bags and subsequently sent to Acme Analytical Laboratories in Vancouver, B.C. for analysis.

A magnetometer survey was conducted over the grid area using a Barringer Research Model GM-122 proton magnetometer. Readings were taken in gammas at 25 meter station and all lines were looped at the baseline to allow for correction of diurnal variations.

A VLF-EM survey was conducted using a Sabre Model 27 receiver tuned to the Jim Creek (Seattle), Washington station (24.8 KHz). Readings were taken for dip angle and field strength at 25 meter stations.

## 3.0 PROPERTY HISTORY

The first modern references to mineralization on the Zumar claims dates to the late 1970's when the Zumar 2 claim was staked. In late 1979 an east-west trending narrow quartz vein discovered near the north edge of the Zumar 2 claim (Zumar vein) was explored by diamond drilling along a strike length of 50 meters and to a depth of 30 meters.

A bulk tonnage sample of selected quartz material from the Zumar vein totalling 60.8 tons was shipped from this vein to the Trail smelter in 1980 with a reported recovery grade of 0.139 oz/t gold and 1.23 oz/t silver.

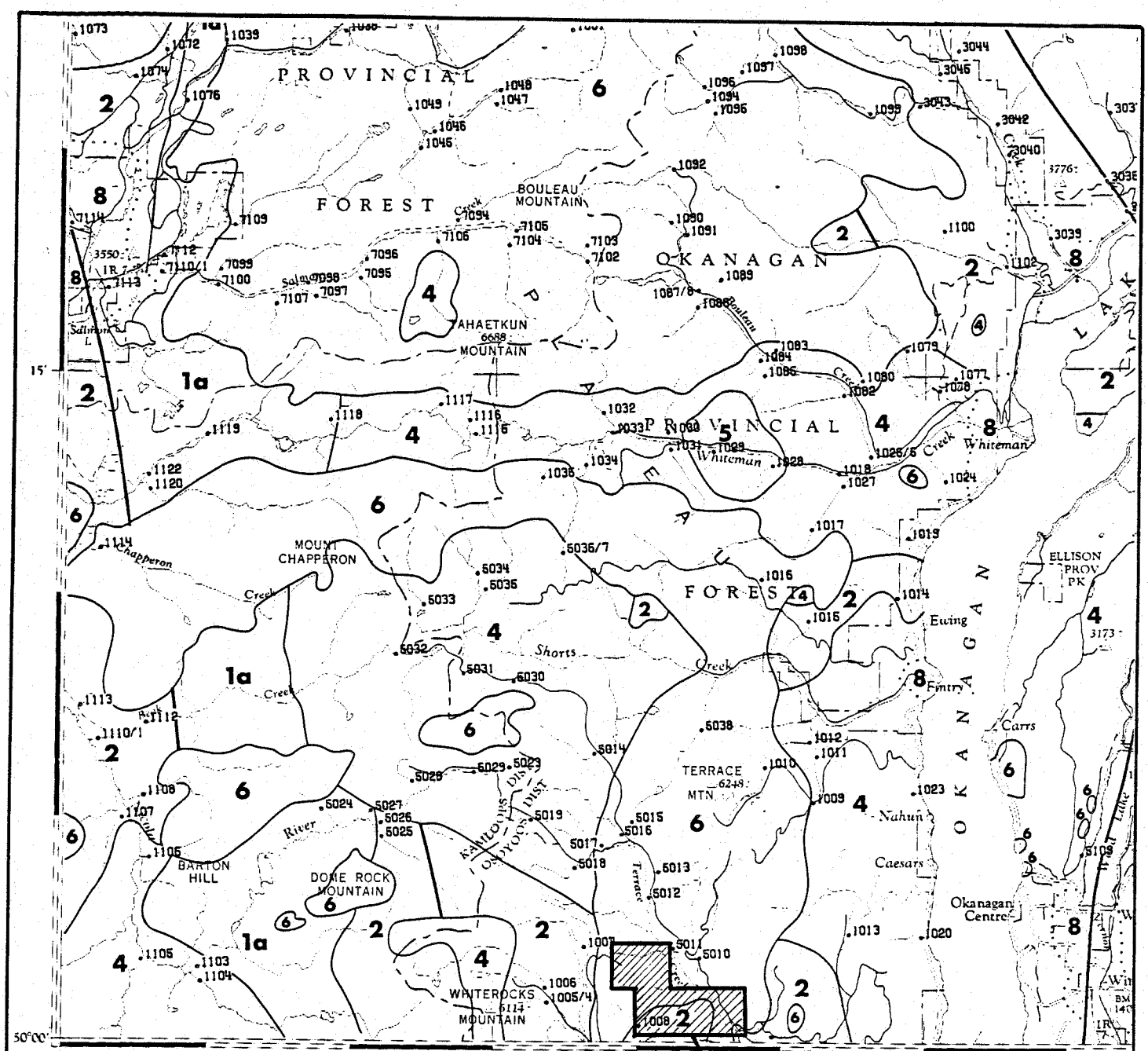
In 1986 and 1987, after the property was acquired by Skyworld Resources and Development Ltd., exploration programs consisting of geochemical, geophysical, geological, trenching and diamond drilling extended the known length of the Zumar vein and examined anomalous areas elsewhere on the property.

Based upon the results of these programs it was decided that the grade and down dip extent of the Zumar vein was not sufficient to warrant further development on the vein (Wilmot, 1987). It was also found that geochemical targets within other areas of the property were possibly related to a mineralized source (Wilmot, 1987; Morrison, 1986) and warranted further exploration.

Recently, north trending gold bearing structures have been reported at the Brett Claims located approximately 15 km north of and along the same geological trend as the Zumar property.

## 4.0 GEOLOGY

The Zumar property is underlain by a mixed assemblage of volcanic and sedimentary rocks ranging from Permian to Tertiary age.




ZUMAR PROPERTY

**LEGEND**

Note: This legend is common to National Geochemical Reconnaissance Map 4-1976, Open File 409; Map 5-1976, Open File 410 and Map 6-1976, Open File 411

QUATERNARY

[0] Glacial, lacustrine, and fluviatile gravel, sand, silt and clay

TERTIARY

[7] Plateau basalts, olivine basalts

[6] Volcanic flow rocks with interbedded sedimentary rocks; 6a, conglomerate, sandstone, shale and tuff

[5] CORYELL: alkalic plutonic rocks; porphyritic granite and rhyolite

JURASSIC - CRETACEOUS

[4] NELSON and VALHALLA: granitic plutonic rocks

JURASSIC

[3] Maffic and ultramafic intrusive rocks, pyroxinite, hornblendite serpentinite

PALEOZOIC (including UPPER PROTEROZOIC and TRIASSIC)

[2] Basaltic and andesitic lavas, greenstone, tuff, quartzite, limestone and argillite; 2a, quartzite, argillite, limestone, slate, schist, phyllite, sandstone and conglomerate

PROTEROZOIC (SHUSWAP TERRANE)

[1] Gneiss, minor schist, limestone, marble, dolomite, slate, phyllite; 1a, schist, quartzite, limestone, slate, argillite

Geological contact.....
Fault.....
Dyke.....
Mineral occurence.....

Legend modified and geology compiled for the geochemical map by T.E. Kaiming from maps 1059A, by H.M.A. Rice 1945, 1946, and A.G. Jones 1947, 1951

Geological cartography by the Geological Survey of Canada

SKYWORLD RESOURCE & DEVELOPMENT LTD.

ZUMAR PROPERTY

# REGIONAL GEOLOGY

N.T.S. 82L-4E VERNON M.D., B.C.

0 5 10 KM.

| | |
|---|---|
| SCALE : 1:250,000 | DATE : JAN. 1989 |
| DRAWN BY: D.W. | FIGURE Nº. 3 |

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Mineralization, as exposed at the Zumar vein occurs within narrow east-west trending quartz veins containing up to 5% pyrite with minor chalcopyrite. The host rock has been chloritized and is typically limonitic adjacent to the veins.

A north trending possibly fault related feature extends north-northwesterly from the southwest corner of the Zumar 4 claim and separates Permian metavolcanics on the west from Tertiary sediments and volcanics on the east side of the structure.

Numerous Late Mesozoic to Tertiary intrusive rocks occur over the property area. These include granodiorite of the Nelson Intrusives and hypabyssal volcanics of probable Eocene or later age.

## 5.0 GEOCHEMISTRY

### 5.1 Introduction

Soils results for 415 samples were analyzed and thresholds for anomalous values derived for plotting and interpretive purposes using the method of Sinclair (1976). Symbolic maps were prepared by Mr. J. Harrop of Cyber Quest Exploration Systems Ltd. using the PC-Xplor software package on an IBM-AT compatible computer.

Data interpretation is based upon the authors' experience and upon suggestions made by Mr. Harrop. Values in excess of the derived high background population thresholds for the elements presented are considered anomalous.

## 5.2 Results and Interpretation

### 5.21 Gold (ppb)

| Population | Mean | Thresholds |
|---|---|---|
| 1 | not determined | 12.0 ppb |
| 2 | not determined | 20.0 ppb |

Three populations were inferred for gold soil values. The low values ( < 12 ppb) are considered background. Higher values were empirically divided into two separate populations, those between 12 ppb and 19 ppb and those ≥ 20 ppb. Experience has shown that gold values in soils greater than 20 ppb are indicative of nearby sources of mineralization and should be considered anomalous.

Gold results for the grid area are spotty with a slight coincidence of anomalous values flanking the location of the Zumar vein (Figure 4). The source of anomalous gold values to the south of copper anomalies in the southern portion of the Zumar 4 claim is not clear, however the presence of these and coincident high background (12 to 19 ppb) gold in soils in this area suggest close proximity to source.

### 5.22 Copper (ppm)

| Population | Mean | Thresholds | |
|---|---|---|---|
| 1 | 23.195 | n/a | 46.533 |
| 2 | 64.810 | 51.762 | 77.857 |
| 3 | 155.000 | 75.000 | 235.000 |

Three populations were derived for copper in soils. The low background population is considered to be indicative of unmineralized source rocks. Samples above the lower threshold of the middle population and particularly above the lower threshold of the high background population show very good correlation to

the known mineralization at the Zumar vein showing and within the southern portion of the Zumar 4 claim (figure 5). Symbol plots for copper were drafted to show both these populations with small symbols for the middle population (2) and larger ones for the high background population (3). Soil values within population 3 are considered anomalous and those within population 2 appear to indicate proximity to mineralization.

### 5.23 Vanadium (ppm)

| Population | Mean | Thresholds | |
|---|---|---|---|
| 1 | 36.285 | 23.769 | 55.393 |
| 2 | 58.050 | 30.656 | 109.920 |

Two populations were derived for Vanadium. The two appear to be related to the two dominant lithologies underlying the property, with very high values - above the high background population upper threshold - associated with copper anomalies (figure 6). Anomalous vanadium is most likely due the presence of magnetite in the vicinity of the Zumar vein and where coincident with copper anomalies in the southern portion of the Zumar 4 claim. Local magnetic highs in these two areas supports this hypothesis.

### 5.24 Potassium (%)

| Population | Mean | Thresholds | |
|---|---|---|---|
| 1 | 0.120 | 0.081 | 0.179 |
| 2 | 0.254 | 0.149 | 0.431 |
| 3 | 0.612 | 0.279 | 1.341 |

The high background population for potassium in soils produces a pattern when plotted which indicates a potassium alteration zone extending southeastward from the Zumar vein area (figure 7). This coincides with plotted population 2 copper results and

pyritic quartz mapped through this area during previous survey work (Morrison, 1986). During any subsequent property examinations this area should be thoroughly prospected.

### 5.25 Calcium (%)

| Population | Mean | Thresholds | |
|---|---|---|---|
| 1 | 0.206 | 0.153 | 0.279 |
| 2 | 0.310 | 0.245 | 0.392 |
| 3 | 0.442 | 0.325 | 0.600 |
| 4 | 0.697 | 0.381 | 1.276 |

The four populations overlap which makes interpretation of the lower background populations difficult. However the coincidence of the values greater than 0.60% Ca with anomalous copper soil results in the southern portion of the Zumar 4 claim suggests the possibility that copper anomalies there are related to a zone of calcium alteration, which often accompanies disseminated copper mineralization (figure 8). The lack of well defined calcium enrichment in the vicinity of the Zumar vein is consistent with fissure filling mineralization known to occur there.

### 5.26 Phosphorous (%)

| Population | Mean | Thresholds | |
|---|---|---|---|
| 1 | 0.043 | 0.017 | 0.111 |
| 2 | 0.134 | 0.072 | 0.250 |

Phosphorous geochemistry on the zumar soil grid highlights the two dominant underlying lithologies with Tertiary aged volcanic and hypabbysal rocks being richer in phosphorous (figure 9). The contact between Permian and Tertiary lithologies can be inferred as a southeast trending break extending from the northwest corner of the grid area toward the east end of Line 6+00N. The overlapping populations between 0.072 % and 0.111 %

were plotted as small circles and values greater than 0.111 % plotted as large circles. The coincidence of high background phosphorous in the vicinity of anomalous copper the southern portion of the Zumar 4 claim appears to related to localized lithological or mineralogical conditions. The lack of a similar coincidence at the Zumar vein is interpreted to be due to differing lithology or mode of mineralization.

Copper, calcium, vanadium and phosphorous soil anomalies are coincident in the southern portion of the Zumar 4 claim centered on Line 3+00N between stations 4+00E and 4+75E. A southerly trend from this area can be inferred extending to Line 1+00N at 4+00E in the case of copper and to lesser degree for calcium and vanadium. This trend may be influenced by topography and further geochemical studies in this area centered on Line 3+00N.

Coincident anomalous copper and vanadium which occur at the Zumar vein as well as in the southern portion of the Zumar 4 claim indicate a common source of mineralization. Vanadium usually accompanies stratabound copper deposits but is also known to occur as an impurity in iron rich minerals such as magnetite- local magnetic highs over both areas of anomalous vanadium are the probable source of magnetite. Differences in potassium, calcium and phosphorous geochemistry between the Zumar vein and Zumar 4 copper anomaly appear to reflect different lithological and mineralization types.

In addition to the above documented elements, barium, manganese and nickel geochemistry were examined. Nickel was not found to reflect the known mineralization at the Zumar vein or the copper anomalies on the Zumar 4 claim. Manganese showed good correlation with both areas, but also proved to heavily affected by Tertiary lithologies. Barium was found to coincident with known mineralization at the Zumar vein but was significantly shifted east and north in the area of the ZUmar 4 copper

anomalies. Barium, manganese and nickel were not chosen for plotting.

## 6.0 GEOPHYSICS

### 6.1 Introduction

Magnetometer and VLF-EM surveys were conducted over the survey area in order to test for north trending structures in the vicinity of copper - silver anomalies noted from previous property surveys (Wilmot, 1987). Field data was plotted and a rough interpretation provided by Mr. John Ashenhurst of S.J.V. Consultants using the Geo-pack software package.

### 6.2 Results and Interpretation

Several dominant features are apparent from the plotted VLF-EM and Magnetometer results. Three strongly magnetic features, one located in the immediate area of the Zumar vein, a second coincident with copper soil anomalies in the southern portion of the Zumar 4 claim and a third associated with an inferred fault in the northeast corner of the grid area (figure 10). Local magnetic highs located at the Zumar vein and in the area of Zumar 4 copper anomalies are probably due to the presence of magnetite within mineralized systems. The coincident presence of vanadium anomalies at these two local magnetic highs also suggests the presence of magnetite or another iron mineral.

A large broad magnetic high in the northwestern portion of the grid area is probably due to the presence of mafic volcanics (G.S.C. Open file 410) rather than contact metamorphism of andesite (Morrison, 1986).

A north-south trending linear magnetic high from Line 0+00N at station 3+00E to Line 12+00N station 3+50E has the appearance of

a dike and coincides with copper soil anomalies on Line 3+00N at the local magnetic high at station 4+00E.

Numerous VLF-EM cross-overs were encountered over the grid area, many of which are probably a result of the angle of the station to the survey lines (figure 11). Strong VLF-EM conductors are situated to the north of the Zumar vein, trending southeasterly, and to the west of the copper anomalies in the southern portion of the Zumar 4 claim trending north-south with a probable fault related break between lines 2+00N and 3+00N.

## 7.0 CONCLUSIONS

Geochemical and geophysical data gathered during the recent survey on the Zumar claims indicates the presence of copper mineralization associated with Tertiary aged structures in the south-central portion of the Zumar 4 claim.

Similarities in the chemical and magnetic signatures of this anomalous area and the Zumar vein showing area are indicative of a common source of mineralization.

North-south trending VLF-EM derived structural elements in the area of the Zumar 4 target area suggest a similar type of mineralization environment to that reportedly present on the Brett claims property located some 20 km north of the Zumar claims.

A zone of copper and potassium enrichment and trending southeastward from the the area of the zumar vein showing follows a series of outcrops whith reported quartz veins containing minor sulfide mineralization.

## 8.0 RECOMMENDATIONS

Further exploration work, particularly in the area of copper anomalies in the southern portion of the Zumar 4 claim, is recommended. Detailed surveys in this area should include systematic geological mapping and prospecting in conjunction with Horizontal Loop EM (HLEM) and soil sampling.

Other areas of the Zumar claims to the north and west of the most recent survey work, should be covered by reconnaissance scale geological and geochemical surveys. A zone of copper and potassium enrichment extending southeasterly form the Zumar vein showing should also be thoroughly prospected.

Target areas outlined and detailed by the above surveys should be bulldozer trenched to determine the extent and grade of mineralization.

This two phase success contingent program is estimated to cost $98,900 with the first phase consisting of ground survey at $79,700 and the second of limited trenching at $19,200.

Should results warrant, a third phase of exploration consisting of follow-up trenching and diamond drilling is suggested. A separate budget would be submitted for this phase of exploration.

## 8.1 Projected Cost Breakdown - Zumar Project

### Phase I

**Detailed Scale Follow-up Surveys**

| | |
|---|---|
| Mapping and Prospecting | $ 4,000 |
| Grid Emplacement - 15 km of Cut Line | 8,000 |
| Soil Sampling - 650 samples incl. assays | 13,000 |
| Rock Sampling - 50 samples incl. assays | 1,000 |
| HLEM Survey - 8 days @ $650/day | 5,200 |

**Reconnaissance Scale Surveys**

| | |
|---|---|
| Mapping and Prospecting | $ 2,500 |
| Grid Emplacement - 20 km of Chained Line | 5,000 |
| Soil Sampling - 450 samples incl. assays | 9,000 |
| Rock sampling - 25 samples incl. assays | 600 |
| Magnetometer Survey | 2,500 |
| VLF-EM Survey | 2,500 |

**Logistics**

| | |
|---|---|
| Food and Accommodation - 45 man-days @ $100/day | 4,500 |
| Transportation - 2 vehicles for 20 days | 2,400 |
| Supervision and Geological Support | 5,000 |
| Report Preparation | 6,000 |
| Contingencies - approx. 12% | 8,500 |

**Total Phase I** **$ 79,700**

### Phase II - Contingent on Phase I Results

**Trenching of Detailed Survey Targets**

| | |
|---|---|
| Mob/Demob | $ 1,200 |
| Access - 2 days @ $750/day | 1,500 |
| Trenching - 8 days @ $750/day | 6,000 |
| Geological Support and Supervision | 2,500 |
| Assays - 50 rocks @ $20 | 1,000 |
| Logistics - 20 man-days @ $100/man-day | 2,000 |
| Report Preparation | 2,500 |
| Contingencies - approx. 15% | 2,500 |

**Total Phase II** **$ 19,200**

## APPENDIX A - CERTIFICATE OF QUALIFICATIONS

### Certificate - Douglas H. Wood

I Douglas H. Wood of the city of Vancouver in the Province of British Columbia do hereby certify as follows:

1. I am an independent consulting geologist based in Vancouver, B.C. and have active in mineral exploration since 1977.

2. I graduated from the University of British Columbia in 1981 with a Bachelor of Science degree in Geological Sciences and spent a further year at the post-graduate level at the University of B.C.

3. I am a fellow in good standing of the Geological Association of Canada (F4594).

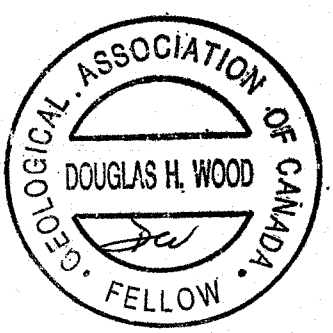
4. I visited the Zumar property on July 1, 1988 and again on November 26, 1988 and provided supervision to the field crews during the period between November 28 and December 12, 1988 when work was performed.

5. I have no interest, contingent or otherwise in the Zumar property nor in the securities of Skyworld Resources and Development Ltd.

6. I consent to and authorize the use of the attached report and my name in the Company's Prospectus, Statement of Material Facts or other public documents.

Dated at Vancouver, Province of British Columbia, this 6th day of February, 1989.

Douglas H. Wood, B.Sc., FGAC
Consulting Geologist



## APPENDIX B - REFERENCES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Rose, Hawkes and Webb (1979)
Geochemistry in Mineral Exploration; Academic Press.

Sinclair, A.J. (1976)
Probability Graphs; Association of Exploration Geochemists Special Vol. #4.

Wilmot, A.D. (1987)
Progress Report on the Zumar Mineral Claims, Vernon Mining Division for Skyworld Resources and Development Ltd.

# APPENDIX C - ASSAYERS' CERTIFICATES

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

# GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Soil -80 Mesh AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: DEC 15 1988 DATE REPORT MAILED: Dec. 20, 1988 SIGNED BY. Bernard Chan D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

LAROTH ENGINEERING LTD. PROJECT ZUMAR File # 88-6289 Page 1

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L12+00N 9+50W | 1 | 19 | 11 | 84 | .3 | 17 | 6 | 408 | 2.32 | 3 | 5 | ND | 3 | 28 | 1 | 2 | 2 | 37 | .32 | .178 | 12 | 18 | .29 | 156 | .10 | 8 | 2.69 | .02 | .13 | 1 | 1 |
| L12+00N 9+00W | 1 | 12 | 11 | 54 | .1 | 13 | 6 | 491 | 2.28 | 2 | 5 | ND | 1 | 27 | 1 | 2 | 2 | 40 | .41 | .087 | 7 | 16 | .30 | 123 | .10 | 8 | 2.16 | .02 | .15 | 1 | 1 |
| L12+00N 8+50W | 1 | 14 | 6 | 42 | .1 | 7 | 6 | 231 | 2.62 | 2 | 5 | ND | 4 | 24 | 1 | 2 | 2 | 53 | .30 | .041 | 13 | 19 | .33 | 53 | .11 | 10 | 1.04 | .02 | .16 | 1 | 1 |
| L12+00N 8+00W | 1 | 28 | 5 | 65 | .4 | 18 | 9 | 451 | 3.61 | 5 | 5 | ND | 9 | 35 | 1 | 2 | 2 | 77 | .44 | .085 | 34 | 30 | .75 | 123 | .14 | 8 | 1.93 | .02 | .40 | 2 | 3 |
| L12+00N 7+50W | 1 | 18 | 13 | 106 | .3 | 18 | 6 | 500 | 2.24 | 2 | 5 | ND | 3 | 44 | 1 | 2 | 2 | 39 | .57 | .218 | 9 | 16 | .32 | 123 | .10 | 4 | 2.38 | .02 | .14 | 1 | 1 |
| L12+00N 7+00W | 1 | 9 | 7 | 84 | .1 | 10 | 5 | 691 | 1.87 | 2 | 5 | ND | 1 | 27 | 1 | 2 | 2 | 34 | .27 | .097 | 7 | 16 | .21 | 139 | .08 | 6 | 1.11 | .01 | .10 | 1 | 2 |
| L12+00N 6+50W | 1 | 17 | 7 | 84 | .2 | 16 | 6 | 327 | 2.19 | 2 | 5 | ND | 3 | 32 | 1 | 2 | 2 | 35 | .27 | .095 | 13 | 18 | .31 | 133 | .10 | 7 | 2.51 | .02 | .13 | 1 | 1 |
| L12+00N 6+00W | 1 | 12 | 8 | 33 | .2 | 15 | 6 | 297 | 2.05 | 2 | 5 | ND | 3 | 22 | 1 | 2 | 2 | 30 | .22 | .214 | 8 | 17 | .23 | 179 | .09 | 8 | 2.38 | .02 | .11 | 1 | 2 |
| L12+00N 5+50W | 1 | 12 | 8 | 58 | .1 | 18 | 5 | 570 | 1.72 | 2 | 5 | ND | 1 | 38 | 1 | 2 | 2 | 27 | .36 | .227 | 7 | 16 | .22 | 220 | .08 | 8 | 1.89 | .02 | .10 | 1 | 1 |
| L12+00N 5+00W | 1 | 7 | 2 | 43 | .2 | 11 | 6 | 287 | 2.27 | 4 | 5 | ND | 4 | 23 | 1 | 2 | 2 | 43 | .27 | .061 | 13 | 23 | .33 | 94 | .09 | 7 | 1.07 | .02 | .15 | 2 | 4 |
| L12+00N 4+50W | 1 | 13 | 5 | 74 | .2 | 19 | 6 | 444 | 2.21 | 2 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 35 | .32 | .175 | 8 | 20 | .27 | 133 | .09 | 2 | 2.14 | .02 | .12 | 1 | 1 |
| L12+00N 4+00W | 1 | 30 | 6 | 57 | .2 | 24 | 6 | 343 | 2.19 | 2 | 5 | ND | 3 | 32 | 1 | 2 | 2 | 38 | .32 | .079 | 16 | 21 | .30 | 114 | .10 | 3 | 2.49 | .02 | .14 | 1 | 1 |
| L12+00N 3+50W | 1 | 13 | 6 | 79 | .1 | 15 | 5 | 1009 | 1.96 | 2 | 5 | ND | 2 | 28 | 1 | 2 | 2 | 34 | .26 | .188 | 7 | 19 | .23 | 179 | .09 | 5 | 1.70 | .02 | .12 | 1 | 2 |
| L12+00N 3+00W | 1 | 11 | 8 | 57 | .1 | 16 | 5 | 280 | 2.22 | 2 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 42 | .23 | .057 | 10 | 25 | .30 | 120 | .10 | 6 | 1.48 | .02 | .12 | 1 | 2 |
| L12+00N 2+50W | 1 | 13 | 5 | 48 | .2 | 16 | 5 | 312 | 1.77 | 4 | 5 | ND | 3 | 27 | 1 | 2 | 2 | 29 | .23 | .199 | 7 | 14 | .21 | 118 | .09 | 3 | 2.01 | .02 | .11 | 3 | 1 |
| L12+00N 2+00W | 1 | 10 | 6 | 51 | .2 | 22 | 6 | 206 | 1.91 | 4 | 5 | ND | 3 | 29 | 1 | 2 | 2 | 32 | .22 | .163 | 7 | 24 | .26 | 183 | .09 | 5 | 1.81 | .02 | .09 | 1 | 1 |
| L12+00N 1+50W | 1 | 16 | 7 | 46 | .1 | 15 | 7 | 337 | 2.66 | 4 | 5 | ND | 7 | 46 | 1 | 2 | 2 | 58 | .47 | .098 | 25 | 28 | .39 | 72 | .10 | 2 | 1.02 | .02 | .14 | 2 | 12 |
| L12+00N 1+00W | 1 | 12 | 9 | 34 | .2 | 11 | 5 | 209 | 1.95 | 2 | 5 | ND | 4 | 32 | 1 | 2 | 2 | 29 | .29 | .015 | 9 | 19 | .23 | 68 | .08 | 6 | 1.58 | .02 | .09 | 1 | 2 |
| L12+00N 0+50W | 1 | 9 | 6 | 34 | .1 | 11 | 5 | 303 | 1.84 | 2 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 30 | .20 | .027 | 8 | 21 | .23 | 94 | .08 | 7 | 1.42 | .01 | .13 | 1 | 1 |
| L12+00N 0+00W | 1 | 9 | 3 | 55 | .1 | 14 | 4 | 264 | 1.87 | 5 | 5 | ND | 3 | 39 | 1 | 2 | 2 | 34 | .32 | .055 | 11 | 20 | .20 | 104 | .08 | 2 | 1.40 | .02 | .10 | 1 | 1 |
| L12+00N 0+50E | 1 | 9 | 7 | 65 | .2 | 13 | 5 | 211 | 2.07 | 3 | 5 | ND | 3 | 41 | 1 | 2 | 2 | 39 | .32 | .047 | 9 | 23 | .29 | 91 | .10 | 4 | 1.51 | .02 | .17 | 1 | 1 |
| L12+00N 1+00E | 1 | 11 | 8 | 48 | .2 | 11 | 6 | 391 | 1.95 | 2 | 6 | ND | 2 | 40 | 1 | 2 | 2 | 34 | .33 | .023 | 7 | 24 | .27 | 77 | .09 | 8 | 1.47 | .02 | .13 | 1 | 1 |
| L12+00N 1+50E | 1 | 17 | 9 | 81 | .1 | 37 | 11 | 425 | 3.19 | 2 | 5 | ND | 9 | 100 | 1 | 2 | 2 | 67 | .78 | .095 | 36 | 46 | .97 | 115 | .12 | 6 | 1.92 | .03 | .17 | 1 | 2 |
| L12+00N 2+00E | 1 | 13 | 2 | 73 | .1 | 20 | 5 | 180 | 1.73 | 3 | 5 | ND | 3 | 42 | 1 | 2 | 2 | 31 | .23 | .126 | 10 | 17 | .24 | 136 | .08 | 3 | 1.65 | .02 | .10 | 1 | 3 |
| L12+00N 2+50E | 1 | 12 | 5 | 48 | .2 | 14 | 5 | 167 | 1.96 | 2 | 5 | ND | 4 | 52 | 1 | 2 | 2 | 30 | .40 | .017 | 11 | 18 | .29 | 63 | .09 | 5 | 1.84 | .02 | .10 | 2 | 2 |
| L12+00N 3+00E | 1 | 12 | 9 | 53 | .3 | 19 | 5 | 179 | 1.94 | 2 | 5 | ND | 3 | 54 | 1 | 2 | 2 | 32 | .36 | .089 | 7 | 23 | .27 | 102 | .08 | 6 | 1.76 | .02 | .08 | 1 | 1 |
| L12+00N 3+50E | 1 | 18 | 8 | 100 | .1 | 19 | 6 | 315 | 2.08 | 2 | 5 | ND | 5 | 20 | 1 | 2 | 2 | 33 | .16 | .163 | 12 | 18 | .32 | 172 | .10 | 6 | 2.72 | .02 | .11 | 1 | 3 |
| L12+00N 4+00E | 1 | 11 | 4 | 70 | .2 | 18 | 6 | 513 | 1.94 | 2 | 5 | ND | 4 | 25 | 1 | 2 | 2 | 31 | .19 | .137 | 8 | 15 | .24 | 165 | .08 | 5 | 1.92 | .01 | .10 | 1 | 4 |
| L12+00N 4+50E | 1 | 10 | 6 | 71 | .3 | 21 | 5 | 263 | 1.79 | 5 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 27 | .20 | .179 | 8 | 14 | .20 | 172 | .08 | 7 | 1.71 | .01 | .09 | 1 | 2 |
| L12+00N 5+00E | 1 | 12 | 6 | 86 | .4 | 16 | 6 | 527 | 2.24 | 3 | 5 | ND | 5 | 23 | 1 | 2 | 2 | 38 | .21 | .128 | 9 | 15 | .22 | 135 | .09 | 5 | 1.97 | .02 | .09 | 1 | 1 |
| L12+00N 5+50E | 1 | 11 | 7 | 82 | .2 | 18 | 6 | 363 | 2.07 | 2 | 5 | ND | 5 | 18 | 1 | 2 | 2 | 33 | .15 | .113 | 8 | 17 | .22 | 148 | .08 | 8 | 1.84 | .01 | .09 | 1 | 1 |
| L12+00N 6+00E | 1 | 11 | 4 | 35 | .1 | 12 | 6 | 195 | 2.52 | 5 | 5 | ND | 8 | 31 | 1 | 2 | 2 | 49 | .31 | .077 | 20 | 26 | .30 | 53 | .08 | 9 | .89 | .01 | .11 | 1 | 1 |
| L12+00N 7+00E | 1 | 17 | 2 | 62 | .1 | 15 | 7 | 244 | 3.21 | 4 | 5 | ND | 8 | 46 | 1 | 2 | 2 | 56 | .38 | .073 | 22 | 24 | .37 | 54 | .08 | 6 | .87 | .02 | .17 | 1 | 5 |
| L12+00N 7+50E | 1 | 8 | 6 | 94 | .1 | 12 | 5 | 345 | 1.57 | 4 | 5 | ND | 3 | 19 | 1 | 3 | 2 | 25 | .13 | .166 | 6 | 10 | .18 | 169 | .07 | 3 | 1.73 | .02 | .08 | 1 | 2 |
| L12+00N 8+00E | 1 | 13 | 11 | 99 | .3 | 16 | 6 | 384 | 1.89 | 3 | 5 | ND | 5 | 27 | 1 | 2 | 2 | 27 | .19 | .096 | 8 | 13 | .24 | 195 | .09 | 6 | 2.29 | .02 | .11 | 1 | 2 |
| L12+00N 8+50E | 1 | 13 | 6 | 74 | .3 | 16 | 5 | 255 | 1.90 | 2 | 5 | ND | 4 | 34 | 1 | 2 | 2 | 29 | .24 | .134 | 11 | 13 | .21 | 153 | .07 | 4 | 1.53 | .01 | .10 | 1 | 1 |
| STD C/AU-S | 18 | 57 | 38 | 132 | 6.9 | 67 | 31 | 1022 | 3.92 | 40 | 22 | 7 | 39 | 48 | 18 | 20 | 23 | 60 | .47 | .089 | 40 | 53 | .91 | 177 | .06 | 39 | 1.94 | .06 | .13 | 12 | 48 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L12+00N 9+00E | 1 | 7 | 2 | 42 | .1 | 5 | 4 | 252 | 2.08 | 2 | 5 | ND | 6 | 17 | 1 | 2 | 2 | 32 | .16 | .034 | 8 | 16 | .18 | 78 | .07 | 2 | .99 | .01 | .09 | 1 | 1 |
| L12+00N 9+50E | 1 | 10 | 2 | 54 | .1 | 8 | 4 | 217 | 1.99 | 2 | 5 | ND | 4 | 22 | 1 | 2 | 2 | 29 | .18 | .039 | 9 | 15 | .22 | 103 | .08 | 2 | 1.38 | .01 | .10 | 1 | 1 |
| L10+00N 10+00W | 1 | 27 | 8 | 184 | .2 | 15 | 10 | 767 | 2.79 | 2 | 5 | ND | 2 | 18 | 1 | 2 | 2 | 61 | .22 | .089 | 5 | 17 | .57 | 235 | .12 | 4 | 2.22 | .02 | .32 | 1 | 1 |
| L10+00N 9+50W | 1 | 49 | 11 | 140 | .1 | 14 | 12 | 635 | 3.86 | 5 | 5 | ND | 3 | 15 | 1 | 2 | 2 | 90 | .19 | .090 | 7 | 16 | .82 | 187 | .15 | 2 | 2.83 | .01 | .38 | 1 | 10 |
| L10+00N 9+00W | 1 | 19 | 6 | 157 | .1 | 21 | 7 | 551 | 2.18 | 2 | 5 | ND | 3 | 18 | 1 | 2 | 2 | 36 | .19 | .111 | 8 | 16 | .29 | 205 | .09 | 3 | 2.00 | .02 | .11 | 1 | 1 |
| L10+00N 8+50W | 1 | 19 | 4 | 125 | .1 | 14 | 7 | 587 | 2.57 | 2 | 5 | ND | 4 | 19 | 1 | 2 | 2 | 41 | .19 | .141 | 9 | 18 | .35 | 189 | .10 | 4 | 2.41 | .02 | .16 | 1 | 1 |
| L10+00N 8+00W | 1 | 25 | 5 | 133 | .1 | 13 | 9 | 596 | 2.84 | 2 | 5 | ND | 2 | 19 | 1 | 2 | 2 | 56 | .24 | .080 | 6 | 13 | .46 | 169 | .11 | 5 | 2.20 | .01 | .24 | 1 | 1 |
| L10+00N 7+50W | 1 | 24 | 5 | 96 | .1 | 19 | 8 | 353 | 2.84 | 2 | 5 | ND | 5 | 28 | 1 | 2 | 2 | 54 | .26 | .096 | 11 | 23 | .44 | 157 | .10 | 3 | 1.70 | .02 | .21 | 1 | 2 |
| L10+00N 7+00W | 1 | 16 | 11 | 113 | .1 | 14 | 7 | 432 | 2.26 | 2 | 5 | ND | 3 | 20 | 1 | 2 | 2 | 35 | .21 | .149 | 7 | 17 | .28 | 157 | .08 | 2 | 1.97 | .01 | .12 | 1 | 3 |
| L10+00N 6+50W | 1 | 17 | 6 | 122 | .1 | 27 | 7 | 428 | 2.35 | 4 | 5 | ND | 4 | 28 | 1 | 2 | 2 | 35 | .26 | .148 | 11 | 22 | .33 | 222 | .09 | 2 | 2.26 | .02 | .13 | 1 | 1 |
| L10+00N 6+00W | 1 | 13 | 9 | 173 | .2 | 14 | 6 | 1358 | 2.06 | 2 | 5 | ND | 2 | 42 | 1 | 2 | 2 | 33 | .46 | .149 | 7 | 16 | .26 | 235 | .08 | 7 | 1.51 | .02 | .14 | 1 | 1 |
| L10+00N 5+50W | 1 | 18 | 3 | 103 | .2 | 16 | 7 | 458 | 2.38 | 2 | 5 | ND | 4 | 30 | 1 | 2 | 2 | 44 | .32 | .121 | 9 | 20 | .35 | 133 | .09 | 2 | 1.51 | .02 | .17 | 1 | 2 |
| L10+00N 5+00W | 1 | 32 | 7 | 107 | .2 | 16 | 10 | 327 | 3.47 | 2 | 5 | ND | 5 | 26 | 1 | 2 | 2 | 66 | .24 | .050 | 10 | 23 | .58 | 110 | .13 | 7 | 2.23 | .01 | .27 | 1 | 1 |
| L10+00N 4+50W | 1 | 16 | 4 | 67 | .2 | 15 | 7 | 297 | 2.23 | 2 | 5 | ND | 4 | 24 | 1 | 2 | 2 | 41 | .22 | .048 | 12 | 21 | .30 | 100 | .10 | 6 | 1.39 | .02 | .14 | 1 | 1 |
| L10+00N 4+00W | 1 | 74 | 5 | 80 | .1 | 7 | 15 | 1165 | 5.13 | 2 | 5 | ND | 5 | 69 | 1 | 2 | 2 | 120 | 1.15 | .162 | 21 | 8 | .78 | 59 | .09 | 2 | 1.39 | .03 | .32 | 6 | 13 |
| L10+00N 3+50W | 1 | 19 | 7 | 84 | .1 | 9 | 7 | 535 | 2.52 | 4 | 5 | ND | 3 | 38 | 1 | 2 | 2 | 46 | .43 | .083 | 6 | 15 | .28 | 124 | .08 | 3 | 1.67 | .01 | .14 | 1 | 1 |
| L10+00N 3+00W | 1 | 15 | 7 | 75 | .1 | 17 | 6 | 335 | 2.15 | 2 | 5 | ND | 4 | 25 | 1 | 2 | 2 | 34 | .20 | .099 | 9 | 16 | .28 | 159 | .09 | 2 | 1.87 | .01 | .14 | 1 | 1 |
| L10+00N 2+50W | 1 | 13 | 5 | 75 | .2 | 13 | 6 | 397 | 1.81 | 2 | 5 | ND | 3 | 20 | 1 | 2 | 2 | 29 | .18 | .120 | 8 | 14 | .17 | 109 | .08 | 2 | 1.51 | .02 | .10 | 1 | 4 |
| L10+00N 2+00W | 1 | 21 | 5 | 61 | .1 | 29 | 7 | 323 | 2.25 | 2 | 5 | ND | 4 | 35 | 1 | 2 | 5 | 34 | .23 | .127 | 10 | 29 | .35 | 186 | .11 | 5 | 2.83 | .02 | .12 | 1 | 1 |
| L10+00N 1+50W | 1 | 10 | 9 | 100 | .1 | 17 | 5 | 660 | 1.79 | 2 | 5 | ND | 3 | 40 | 1 | 2 | 2 | 27 | .35 | .299 | 6 | 17 | .20 | 270 | .08 | 7 | 1.65 | .02 | .12 | 1 | 1 |
| L10+00N 1+00W | 1 | 15 | 7 | 91 | .1 | 21 | 7 | 391 | 2.23 | 2 | 5 | ND | 5 | 38 | 1 | 2 | 2 | 36 | .33 | .144 | 8 | 22 | .31 | 143 | .09 | 4 | 2.06 | .02 | .14 | 1 | 1 |
| L10+00N 0+50W | 1 | 14 | 7 | 101 | .2 | 19 | 6 | 559 | 2.00 | 2 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 32 | .29 | .161 | 8 | 19 | .24 | 174 | .09 | 5 | 1.87 | .02 | .11 | 1 | 1 |
| L10+00N 0+00W | 1 | 17 | 3 | 54 | .1 | 15 | 6 | 374 | 2.55 | 2 | 5 | ND | 6 | 39 | 1 | 2 | 2 | 53 | .36 | .094 | 18 | 26 | .34 | 95 | .10 | 2 | 1.29 | .02 | .15 | 1 | 1 |
| L10+00N 0+50E | 1 | 15 | 6 | 46 | .1 | 20 | 6 | 264 | 2.31 | 2 | 5 | ND | 5 | 33 | 1 | 2 | 2 | 43 | .28 | .037 | 16 | 27 | .31 | 100 | .10 | 2 | 1.61 | .02 | .11 | 1 | 1 |
| L10+00N 1+00E | 1 | 11 | 5 | 31 | .1 | 16 | 5 | 191 | 1.89 | 3 | 5 | ND | 4 | 31 | 1 | 2 | 2 | 33 | .27 | .071 | 10 | 17 | .19 | 82 | .09 | 2 | 1.50 | .02 | .09 | 1 | 1 |
| L10+00N 1+50E | 1 | 12 | 2 | 33 | .1 | 9 | 4 | 160 | 2.34 | 2 | 5 | ND | 7 | 32 | 1 | 2 | 12 | 54 | .26 | .038 | 20 | 23 | .20 | 46 | .10 | 2 | .65 | .02 | .09 | 1 | 1 |
| L10+00N 2+00E | 1 | 13 | 5 | 54 | .1 | 10 | 4 | 393 | 1.58 | 2 | 5 | ND | 4 | 27 | 1 | 2 | 2 | 27 | .18 | .131 | 7 | 12 | .16 | 165 | .07 | 5 | 1.39 | .02 | .08 | 1 | 2 |
| L10+00N 2+50E | 1 | 21 | 10 | 85 | .3 | 13 | 8 | 567 | 2.51 | 3 | 5 | ND | 5 | 33 | 1 | 2 | 2 | 43 | .37 | .125 | 9 | 16 | .34 | 122 | .10 | 5 | 1.98 | .02 | .14 | 1 | 1 |
| L10+00N 3+00E | 1 | 18 | 8 | 67 | .2 | 10 | 6 | 256 | 2.52 | 4 | 5 | ND | 5 | 28 | 1 | 2 | 2 | 47 | .28 | .053 | 7 | 19 | .33 | 90 | .11 | 3 | 1.57 | .02 | .14 | 1 | 1 |
| L10+00N 3+50E | 1 | 20 | 10 | 111 | .4 | 14 | 6 | 324 | 1.90 | 2 | 5 | ND | 4 | 24 | 1 | 2 | 2 | 29 | .21 | .170 | 7 | 13 | .25 | 157 | .09 | 2 | 2.00 | .02 | .08 | 1 | 1 |
| L10+00N 4+00E | 1 | 62 | 9 | 71 | .2 | 14 | 12 | 784 | 4.53 | 5 | 5 | ND | 9 | 55 | 1 | 2 | 2 | 103 | .92 | .123 | 29 | 23 | .89 | 67 | .12 | 6 | 1.71 | .03 | .20 | 1 | 14 |
| L10+00N 4+50E | 1 | 21 | 10 | 56 | .2 | 11 | 6 | 295 | 2.58 | 2 | 5 | ND | 5 | 36 | 1 | 2 | 2 | 49 | .35 | .059 | 14 | 20 | .35 | 100 | .10 | 5 | 1.44 | .02 | .15 | 1 | 1 |
| L10+00N 5+00E | 1 | 17 | 11 | 99 | .4 | 16 | 6 | 402 | 2.12 | 2 | 5 | ND | 4 | 21 | 1 | 2 | 2 | 32 | .21 | .099 | 6 | 14 | .28 | 181 | .10 | 4 | 2.35 | .01 | .12 | 1 | 2 |
| L10+00N 5+50E | 1 | 13 | 6 | 41 | .1 | 12 | 6 | 179 | 2.65 | 2 | 5 | ND | 9 | 42 | 1 | 2 | 2 | 57 | .30 | .060 | 19 | 27 | .36 | 83 | .11 | 8 | 1.02 | .02 | .11 | 1 | 17 |
| L10+00N 6+00E | 1 | 15 | 11 | 46 | .1 | 13 | 7 | 184 | 2.86 | 2 | 5 | ND | 7 | 29 | 1 | 2 | 2 | 51 | .22 | .049 | 13 | 24 | .35 | 98 | .11 | 3 | 1.63 | .01 | .11 | 1 | 1 |
| L10+00N 6+50E | 1 | 18 | 13 | 83 | .2 | 17 | 7 | 299 | 3.06 | 2 | 5 | ND | 8 | 19 | 1 | 2 | 2 | 51 | .16 | .117 | 13 | 21 | .32 | 152 | .10 | 3 | 2.22 | .01 | .08 | 1 | 1 |
| STD C/AU-S | 18 | 59 | 42 | 132 | 6.5 | 67 | 31 | 1006 | 4.00 | 39 | 23 | 7 | 39 | 47 | 18 | 16 | 24 | 58 | .46 | .085 | 38 | 56 | .89 | 172 | .06 | 34 | 1.85 | .06 | .14 | 12 | 51 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L10+00N 7+00E | 1 | 11 | 6 | 66 | .1 | 18 | 8 | 340 | 5.02 | 2 | 5 | ND | 19 | 26 | 1 | 2 | 2 | 86 | .23 | .073 | 13 | 31 | .39 | 92 | .10 | 2 | 1.73 | .01 | .09 | 1 | 1 |
| L10+00N 7+50E | 1 | 9 | 2 | 30 | .1 | 11 | 5 | 201 | 2.77 | 2 | 5 | ND | 7 | 33 | 1 | 2 | 2 | 50 | .35 | .083 | 21 | 27 | .30 | 41 | .08 | 7 | .72 | .01 | .09 | 2 | 2 |
| L10+00N 8+00E | 1 | 8 | 4 | 45 | .1 | 13 | 5 | 153 | 2.47 | 2 | 5 | ND | 5 | 25 | 1 | 2 | 2 | 37 | .17 | .029 | 10 | 20 | .25 | 78 | .09 | 4 | 1.68 | .01 | .09 | 1 | 1 |
| L10+00N 8+50E | 1 | 5 | 4 | 57 | .1 | 12 | 4 | 356 | 2.14 | 2 | 5 | ND | 3 | 29 | 1 | 2 | 2 | 34 | .24 | .089 | 7 | 14 | .23 | 106 | .08 | 7 | 1.46 | .02 | .11 | 1 | 1 |
| L10+00N 9+00E | 1 | 7 | 5 | 42 | .1 | 15 | 5 | 137 | 2.09 | 6 | 5 | ND | 4 | 38 | 1 | 2 | 2 | 26 | .25 | .100 | 8 | 16 | .20 | 97 | .08 | 2 | 1.88 | .02 | .11 | 1 | 2 |
| L10+00N 9+50E | 1 | 277 | 10 | 147 | .8 | 12 | 18 | 2107 | 4.14 | 2 | 5 | ND | 3 | 235 | 2 | 2 | 2 | 88 | 2.32 | .307 | 20 | 18 | .82 | 205 | .09 | 6 | 2.19 | .02 | .25 | 1 | 8 |
| L8+00N 10+00W | 1 | 73 | 11 | 115 | .1 | 21 | 12 | 454 | 4.25 | 3 | 5 | ND | 5 | 34 | 1 | 2 | 3 | 87 | .35 | .053 | 14 | 30 | .79 | 167 | .14 | 9 | 3.09 | .01 | .40 | 1 | 1 |
| L8+00N 9+50W | 1 | 24 | 6 | 83 | .2 | 14 | 8 | 378 | 2.90 | 2 | 5 | ND | 3 | 22 | 1 | 3 | 2 | 50 | .25 | .032 | 6 | 25 | .49 | 107 | .11 | 5 | 2.12 | .02 | .27 | 1 | 3 |
| L8+00N 9+00W | 1 | 32 | 4 | 155 | .1 | 16 | 9 | 1100 | 2.96 | 2 | 5 | ND | 4 | 28 | 1 | 2 | 2 | 53 | .30 | .089 | 9 | 19 | .45 | 197 | .09 | 4 | 2.27 | .01 | .19 | 1 | 1 |
| L8+00N 8+50W | 1 | 27 | 8 | 100 | .1 | 18 | 8 | 758 | 2.62 | 3 | 5 | ND | 5 | 26 | 1 | 2 | 2 | 45 | .25 | .068 | 12 | 19 | .41 | 190 | .09 | 4 | 1.98 | .01 | .23 | 1 | 4 |
| L8+00N 8+00W | 1 | 36 | 9 | 127 | .2 | 15 | 8 | 665 | 2.91 | 3 | 5 | ND | 3 | 23 | 1 | 2 | 2 | 53 | .22 | .056 | 8 | 16 | .48 | 197 | .09 | 9 | 2.26 | .01 | .24 | 1 | 1 |
| L8+00N 7+50W | 1 | 32 | 8 | 122 | .2 | 16 | 9 | 973 | 3.16 | 5 | 5 | ND | 4 | 29 | 1 | 2 | 2 | 59 | .30 | .035 | 12 | 18 | .49 | 179 | .10 | 7 | 2.13 | .01 | .32 | 1 | 2 |
| L8+00N 7+00W | 1 | 26 | 6 | 139 | .1 | 17 | 9 | 1092 | 3.12 | 2 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 54 | .36 | .051 | 11 | 22 | .48 | 225 | .10 | 2 | 2.43 | .01 | .27 | 1 | 1 |
| L8+00N 6+50W | 1 | 53 | 9 | 220 | .2 | 17 | 14 | 2222 | 3.61 | 2 | 5 | ND | 3 | 40 | 1 | 2 | 2 | 67 | .44 | .078 | 10 | 17 | .54 | 278 | .09 | 6 | 2.43 | .01 | .27 | 1 | 3 |
| L8+00N 6+00W | 1 | 18 | 4 | 77 | .2 | 13 | 7 | 403 | 3.17 | 2 | 5 | ND | 5 | 28 | 1 | 2 | 2 | 59 | .29 | .034 | 12 | 21 | .43 | 106 | .10 | 2 | 1.51 | .01 | .27 | 1 | 1 |
| L8+00N 5+50W | 1 | 18 | 8 | 99 | .1 | 18 | 7 | 269 | 2.86 | 2 | 5 | ND | 5 | 28 | 1 | 2 | 2 | 45 | .24 | .076 | 10 | 20 | .36 | 174 | .10 | 5 | 2.56 | .02 | .20 | 1 | 1 |
| L8+00N 5+00W | 1 | 188 | 8 | 134 | .7 | 16 | 22 | 1053 | 6.74 | 5 | 5 | ND | 3 | 25 | 1 | 4 | 2 | 181 | .47 | .083 | 10 | 17 | 1.69 | 160 | .22 | 5 | 2.98 | .01 | 1.05 | 3 | 116 |
| L8+00N 4+50W | 1 | 108 | 14 | 233 | .4 | 17 | 18 | 2104 | 5.11 | 4 | 5 | ND | 2 | 27 | 1 | 2 | 2 | 115 | .35 | .075 | 7 | 12 | 1.10 | 339 | .16 | 6 | 3.04 | .01 | .54 | 1 | 18 |
| L8+00N 4+00W | 1 | 61 | 6 | 173 | .4 | 13 | 14 | 1314 | 4.32 | 5 | 5 | ND | 4 | 29 | 1 | 4 | 2 | 96 | .37 | .057 | 11 | 17 | .90 | 266 | .15 | 8 | 3.15 | .01 | .54 | 1 | 2 |
| L8+00N 3+50W | 1 | 252 | 6 | 132 | .5 | 11 | 29 | 1083 | 8.42 | 3 | 5 | ND | 2 | 21 | 1 | 5 | 2 | 261 | .50 | .093 | 6 | 14 | 2.29 | 284 | .30 | 2 | 3.41 | .01 | 1.37 | 7 | 4 |
| L8+00N 3+00W | 1 | 57 | 11 | 159 | .4 | 17 | 12 | 1016 | 3.77 | 4 | 5 | ND | 4 | 48 | 1 | 2 | 2 | 79 | .34 | .118 | 9 | 20 | .58 | 227 | .10 | 7 | 2.33 | .02 | .29 | 3 | 2 |
| L8+00N 2+50W | 1 | 17 | 12 | 150 | .3 | 24 | 8 | 447 | 2.58 | 3 | 6 | ND | 4 | 39 | 1 | 2 | 2 | 37 | .27 | .201 | 7 | 21 | .37 | 230 | .09 | 9 | 2.57 | .02 | .17 | 1 | 5 |
| L8+00N 2+00W | 1 | 11 | 5 | 113 | .2 | 13 | 7 | 571 | 2.31 | 2 | 5 | ND | 4 | 46 | 1 | 2 | 2 | 35 | .32 | .155 | 7 | 16 | .29 | 209 | .08 | 7 | 1.96 | .01 | .16 | 1 | 1 |
| L8+00N 1+50W | 1 | 20 | 10 | 109 | .3 | 16 | 6 | 242 | 2.66 | 2 | 5 | ND | 5 | 29 | 1 | 2 | 2 | 41 | .19 | .181 | 9 | 17 | .34 | 134 | .09 | 3 | 2.71 | .02 | .12 | 1 | 22 |
| L8+00N 1+00W | 1 | 32 | 6 | 72 | .1 | 16 | 9 | 495 | 3.58 | 8 | 5 | ND | 8 | 46 | 1 | 2 | 2 | 67 | .52 | .121 | 28 | 27 | .65 | 111 | .11 | 3 | 1.57 | .02 | .33 | 2 | 1 |
| L8+00N 0+50W | 1 | 15 | 9 | 117 | .3 | 15 | 6 | 282 | 2.64 | 2 | 5 | ND | 4 | 31 | 1 | 2 | 2 | 42 | .27 | .105 | 8 | 21 | .33 | 148 | .09 | 5 | 2.10 | .01 | .19 | 1 | 1 |
| L8+00N 0+00W | 1 | 22 | 11 | 160 | .4 | 17 | 7 | 382 | 2.42 | 5 | 6 | ND | 5 | 38 | 1 | 2 | 3 | 36 | .29 | .192 | 9 | 20 | .34 | 252 | .09 | 8 | 2.39 | .01 | .13 | 2 | 3 |
| L8+00N 0+50E | 1 | 49 | 15 | 90 | .1 | 18 | 11 | 667 | 4.04 | 4 | 5 | ND | 10 | 55 | 1 | 2 | 2 | 81 | .61 | .129 | 29 | 33 | .72 | 100 | .11 | 6 | 1.80 | .02 | .24 | 2 | 1 |
| L8+00N 1+00E | 1 | 18 | 13 | 130 | .2 | 30 | 8 | 358 | 2.67 | 2 | 5 | ND | 5 | 47 | 1 | 3 | 2 | 37 | .34 | .179 | 12 | 32 | .40 | 265 | .10 | 6 | 3.08 | .02 | .14 | 1 | 1 |
| L8+00N 1+50E | 1 | 10 | 8 | 173 | .3 | 24 | 7 | 429 | 2.19 | 2 | 9 | ND | 4 | 33 | 1 | 2 | 2 | 33 | .20 | .132 | 5 | 23 | .31 | 202 | .09 | 6 | 2.45 | .02 | .10 | 1 | 1 |
| L8+00N 2+00E | 1 | 25 | 14 | 175 | .1 | 26 | 14 | 861 | 4.56 | 5 | 5 | ND | 10 | 83 | 1 | 5 | 5 | 80 | .54 | .108 | 44 | 61 | .95 | 223 | .17 | 5 | 3.75 | .02 | .12 | 1 | 2 |
| L8+00N 2+50E | 1 | 20 | 12 | 200 | .1 | 23 | 13 | 1004 | 4.43 | 3 | 5 | ND | 8 | 94 | 1 | 3 | 2 | 88 | .69 | .125 | 32 | 65 | .80 | 180 | .20 | 5 | 3.06 | .02 | .15 | 1 | 1 |
| L8+00N 3+00E | 1 | 12 | 10 | 146 | .1 | 15 | 7 | 563 | 2.83 | 3 | 5 | ND | 4 | 48 | 1 | 3 | 3 | 53 | .34 | .051 | 9 | 41 | .45 | 107 | .15 | 8 | 2.17 | .02 | .17 | 1 | 1 |
| L8+00N 3+50E | 1 | 13 | 13 | 163 | .3 | 20 | 9 | 473 | 2.86 | 2 | 6 | ND | 5 | 53 | 1 | 2 | 3 | 53 | .34 | .207 | 11 | 39 | .47 | 180 | .14 | 10 | 2.41 | .01 | .10 | 1 | 3 |
| L8+00N 4+00E | 1 | 11 | 8 | 111 | .2 | 22 | 7 | 516 | 2.67 | 2 | 5 | ND | 5 | 41 | 1 | 2 | 2 | 47 | .30 | .053 | 12 | 37 | .40 | 120 | .11 | 6 | 1.77 | .02 | .13 | 1 | 2 |
| L8+00N 4+50E | 1 | 32 | 7 | 95 | .2 | 20 | 12 | 403 | 3.98 | 5 | 5 | ND | 9 | 86 | 1 | 2 | 2 | 93 | .63 | .096 | 24 | 50 | .82 | 74 | .15 | 11 | 1.64 | .02 | .20 | 1 | 1 |
| STD C/AU-S | 18 | 59 | 40 | 132 | 7.0 | 67 | 30 | 1002 | 4.04 | 36 | 19 | 7 | 36 | 48 | 17 | 17 | 18 | 55 | .48 | .092 | 36 | 53 | .94 | 174 | .06 | 35 | 1.96 | .06 | .14 | 12 | 47 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L8+00N 5+00E | 1 | 13 | 7 | 104 | .1 | 7 | 5 | 316 | 2.04 | 2 | 5 | ND | 3 | 51 | 1 | 2 | 2 | 36 | .33 | .063 | 8 | 16 | .27 | 103 | .10 | 5 | 1.39 | .02 | .16 | 1 | 6 |
| L8+00N 5+50E | 1 | 17 | 10 | 129 | .4 | 15 | 6 | 360 | 2.09 | 2 | 5 | ND | 3 | 29 | 1 | 2 | 2 | 32 | .21 | .068 | 6 | 14 | .29 | 151 | .09 | 6 | 2.07 | .02 | .09 | 1 | 6 |
| L8+00N 6+00E | 1 | 17 | 7 | 146 | .1 | 10 | 7 | 430 | 2.32 | 2 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 37 | .24 | .049 | 5 | 13 | .34 | 128 | .10 | 3 | 2.20 | .02 | .13 | 1 | 2 |
| L8+00N 6+25E | 1 | 12 | 6 | 124 | .1 | 10 | 5 | 438 | 2.07 | 2 | 5 | ND | 1 | 21 | 1 | 2 | 2 | 34 | .22 | .041 | 5 | 14 | .29 | 101 | .09 | 4 | 1.79 | .02 | .10 | 1 | 3 |
| L8+00N 7+00E | 1 | 14 | 6 | 78 | .3 | 11 | 7 | 314 | 2.53 | 2 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 45 | .23 | .052 | 9 | 21 | .35 | 92 | .10 | 3 | 1.56 | .01 | .12 | 1 | 1 |
| L8+00N 7+50E | 1 | 15 | 13 | 99 | .3 | 11 | 7 | 413 | 2.23 | 2 | 5 | ND | 3 | 24 | 1 | 2 | 3 | 36 | .20 | .088 | 8 | 17 | .26 | 132 | .09 | 4 | 1.84 | .01 | .10 | 1 | 1 |
| L8+00N 8+00E | 1 | 17 | 14 | 91 | .1 | 17 | 6 | 308 | 2.55 | 3 | 5 | ND | 4 | 22 | 1 | 2 | 2 | 40 | .20 | .143 | 14 | 19 | .30 | 163 | .10 | 5 | 2.39 | .02 | .08 | 1 | 1 |
| L8+00N 8+50E | 1 | 11 | 11 | 74 | .1 | 15 | 5 | 279 | 2.06 | 2 | 5 | ND | 4 | 24 | 1 | 2 | 3 | 27 | .18 | .085 | 7 | 16 | .24 | 164 | .09 | 2 | 2.02 | .01 | .08 | 1 | 1 |
| L8+00N 9+00E | 1 | 15 | 16 | 78 | .1 | 17 | 7 | 185 | 2.56 | 5 | 5 | ND | 6 | 24 | 1 | 2 | 2 | 38 | .19 | .180 | 13 | 19 | .35 | 170 | .11 | 3 | 2.55 | .02 | .11 | 1 | 4 |
| L8+00N 9+50E | 1 | 19 | 6 | 71 | .2 | 19 | 6 | 225 | 2.71 | 2 | 5 | ND | 7 | 19 | 1 | 2 | 2 | 42 | .18 | .122 | 12 | 21 | .32 | 167 | .10 | 2 | 2.28 | .02 | .10 | 2 | 1 |
| L6+00N 10+00W | 1 | 13 | 8 | 53 | .1 | 12 | 6 | 547 | 2.17 | 3 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 36 | .18 | .037 | 8 | 15 | .26 | 98 | .08 | 4 | 1.37 | .01 | .14 | 2 | 2 |
| L6+00N 9+50W | 1 | 29 | 6 | 82 | .1 | 13 | 7 | 338 | 3.07 | 3 | 5 | ND | 3 | 23 | 1 | 2 | 2 | 58 | .27 | .039 | 9 | 20 | .47 | 106 | .10 | 5 | 1.66 | .01 | .24 | 1 | 3 |
| L6+00N 9+00W | 1 | 20 | 8 | 50 | .2 | 11 | 6 | 354 | 2.51 | 2 | 5 | ND | 3 | 23 | 1 | 2 | 2 | 42 | .31 | .022 | 12 | 17 | .32 | 99 | .10 | 4 | 1.77 | .01 | .20 | 1 | 71 |
| L6+00N 8+50W | 1 | 22 | 7 | 67 | .2 | 11 | 7 | 288 | 2.50 | 2 | 5 | ND | 4 | 28 | 1 | 2 | 3 | 40 | .33 | .037 | 10 | 15 | .34 | 104 | .10 | 4 | 1.93 | .01 | .22 | 1 | 4 |
| L6+00N 8+00W | 1 | 15 | 5 | 67 | .1 | 11 | 7 | 322 | 2.51 | 3 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 43 | .23 | .031 | 10 | 16 | .35 | 110 | .10 | 5 | 1.48 | .01 | .25 | 2 | 1 |
| L6+00N 7+50W | 1 | 17 | 8 | 62 | .1 | 10 | 7 | 331 | 2.63 | 3 | 5 | ND | 4 | 21 | 1 | 2 | 2 | 47 | .25 | .027 | 14 | 20 | .38 | 119 | .11 | 2 | 1.52 | .01 | .26 | 1 | 1 |
| L6+00N 7+00W | 1 | 21 | 10 | 62 | .2 | 11 | 7 | 568 | 2.30 | 4 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 38 | .36 | .061 | 12 | 16 | .31 | 137 | .09 | 2 | 1.55 | .01 | .23 | 1 | 1 |
| L6+00N 6+50W | 1 | 19 | 7 | 69 | .1 | 12 | 6 | 426 | 2.39 | 2 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 42 | .25 | .026 | 10 | 17 | .37 | 107 | .10 | 6 | 1.47 | .01 | .26 | 1 | 1 |
| L6+00N 6+00W | 1 | 22 | 5 | 66 | .2 | 14 | 8 | 381 | 2.51 | 5 | 5 | ND | 4 | 21 | 1 | 2 | 2 | 43 | .26 | .037 | 11 | 19 | .42 | 100 | .11 | 2 | 1.89 | .02 | .31 | 1 | 1 |
| L6+00N 5+50W | 1 | 38 | 9 | 120 | .2 | 21 | 10 | 608 | 3.27 | 4 | 5 | ND | 4 | 28 | 1 | 2 | 2 | 59 | .33 | .049 | 17 | 26 | .57 | 169 | .13 | 5 | 2.69 | .01 | .38 | 1 | 3 |
| L6+00N 5+00W | 1 | 31 | 5 | 103 | .2 | 19 | 9 | 570 | 3.02 | 3 | 5 | ND | 5 | 29 | 1 | 2 | 2 | 51 | .30 | .039 | 14 | 29 | .48 | 160 | .12 | 3 | 2.13 | .01 | .35 | 1 | 1 |
| L6+00N 4+50W | 1 | 34 | 15 | 87 | .2 | 19 | 10 | 374 | 3.28 | 3 | 5 | ND | 5 | 32 | 1 | 2 | 2 | 62 | .33 | .041 | 15 | 24 | .53 | 167 | .14 | 8 | 2.50 | .02 | .38 | 1 | 2 |
| L6+00N 4+00W | 1 | 59 | 10 | 129 | .1 | 17 | 14 | 976 | 3.96 | 5 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 84 | .33 | .061 | 13 | 17 | .73 | 232 | .14 | 4 | 3.06 | .01 | .46 | 2 | 1 |
| L6+00N 3+50W | 1 | 37 | 11 | 104 | .1 | 17 | 10 | 486 | 3.45 | 2 | 5 | ND | 4 | 28 | 1 | 2 | 2 | 65 | .29 | .042 | 16 | 21 | .61 | 191 | .14 | 7 | 2.74 | .02 | .38 | 1 | 1 |
| L6+00N 3+00W | 1 | 42 | 6 | 104 | .2 | 13 | 11 | 560 | 3.56 | 2 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 77 | .33 | .040 | 11 | 15 | .64 | 144 | .12 | 2 | 2.08 | .01 | .46 | 2 | 2 |
| L6+00N 2+50W | 1 | 38 | 9 | 103 | .3 | 17 | 11 | 734 | 3.36 | 2 | 5 | ND | 4 | 35 | 1 | 2 | 2 | 70 | .30 | .050 | 12 | 18 | .56 | 164 | .12 | 4 | 2.27 | .01 | .40 | 2 | 1 |
| L6+00N 2+00W | 1 | 47 | 10 | 75 | .3 | 15 | 10 | 406 | 3.52 | 4 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 75 | .32 | .041 | 13 | 21 | .57 | 129 | .12 | 7 | 1.96 | .01 | .35 | 2 | 2 |
| L6+00N 1+50W | 1 | 31 | 11 | 93 | .1 | 14 | 10 | 977 | 3.04 | 2 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 60 | .34 | .035 | 13 | 21 | .46 | 161 | .11 | 3 | 1.77 | .01 | .32 | 3 | 2 |
| L6+00N 1+00W | 1 | 39 | 11 | 86 | .5 | 11 | 9 | 489 | 3.32 | 2 | 5 | ND | 2 | 54 | 1 | 2 | 2 | 74 | .37 | .031 | 9 | 17 | .49 | 107 | .11 | 7 | 1.81 | .01 | .38 | 5 | 3 |
| L6+00N 0+50W | 1 | 33 | 10 | 83 | .4 | 9 | 8 | 766 | 2.64 | 3 | 5 | ND | 3 | 38 | 1 | 2 | 2 | 49 | .31 | .037 | 11 | 15 | .35 | 145 | .10 | 6 | 1.81 | .01 | .24 | 4 | 5 |
| L6+00N 0+00W | 1 | 25 | 6 | 72 | .1 | 12 | 7 | 339 | 2.83 | 6 | 5 | ND | 4 | 37 | 1 | 2 | 2 | 52 | .34 | .051 | 12 | 18 | .39 | 116 | .11 | 7 | 1.83 | .01 | .23 | 3 | 3 |
| L6+00N 0+25E | 1 | 15 | 9 | 103 | .2 | 10 | 5 | 325 | 2.31 | 4 | 5 | ND | 3 | 23 | 1 | 2 | 2 | 39 | .20 | .038 | 8 | 16 | .30 | 108 | .10 | 8 | 1.62 | .01 | .22 | 1 | 2 |
| L6+00N 0+50E | 1 | 11 | 6 | 47 | .2 | 7 | 5 | 317 | 2.13 | 2 | 5 | ND | 3 | 20 | 1 | 2 | 2 | 38 | .18 | .024 | 8 | 14 | .25 | 85 | .08 | 5 | 1.04 | .01 | .16 | 5 | 1 |
| L6+00N 0+75E | 1 | 17 | 12 | 88 | .1 | 15 | 6 | 326 | 2.38 | 2 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 38 | .28 | .092 | 12 | 17 | .31 | 167 | .09 | 3 | 2.01 | .01 | .16 | 2 | 3 |
| L6+00N 1+00E | 1 | 14 | 9 | 77 | .2 | 9 | 7 | 302 | 2.38 | 3 | 5 | ND | 5 | 24 | 1 | 2 | 2 | 40 | .22 | .042 | 7 | 15 | .32 | 109 | .10 | 4 | 1.80 | .01 | .17 | 1 | 2 |
| L6+00N 1+25E | 1 | 185 | 13 | 194 | .1 | 18 | 9 | 1611 | 3.02 | 2 | 5 | ND | 1 | 49 | 1 | 2 | 2 | 54 | .49 | .055 | 10 | 22 | .54 | 240 | .10 | 2 | 1.93 | .01 | .23 | 1 | 13 |
| STD C/AU-S | 19 | 62 | 40 | 132 | 7.0 | 71 | 31 | 1047 | 4.10 | 42 | 17 | 6 | 39 | 51 | 19 | 20 | 22 | 57 | .49 | .095 | 42 | 56 | .95 | 179 | .07 | 41 | 2.01 | .06 | .14 | 11 | 53 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L6+00N 1+50E | 1 | 16 | 5 | 90 | .1 | 21 | 5 | 861 | 2.35 | 2 | 5 | ND | 3 | 42 | 1 | 2 | 2 | 42 | .40 | .058 | 8 | 28 | .38 | 196 | .10 | 3 | 2.24 | .01 | .15 | 1 | 1 |
| L6+00N 1+75E | 1 | 22 | 10 | 106 | .1 | 27 | 7 | 558 | 2.89 | 5 | 5 | ND | 3 | 28 | 1 | 2 | 2 | 55 | .29 | .036 | 10 | 36 | .54 | 165 | .14 | 8 | 2.47 | .01 | .27 | 2 | 1 |
| L6+00N 2+00E | 1 | 13 | 8 | 86 | .1 | 11 | 4 | 775 | 1.87 | 2 | 5 | ND | 2 | 44 | 1 | 2 | 2 | 38 | .30 | .023 | 5 | 16 | .26 | 134 | .10 | 10 | 1.33 | .02 | .15 | 1 | 1 |
| L6+00N 2+25E | 1 | 17 | 6 | 193 | .1 | 26 | 4 | 660 | 1.63 | 2 | 5 | ND | 2 | 56 | 1 | 2 | 2 | 26 | .29 | .096 | 7 | 25 | .27 | 229 | .08 | 9 | 1.59 | .02 | .14 | 1 | 1 |
| L6+00N 2+50E | 1 | 10 | 9 | 156 | .2 | 32 | 6 | 524 | 1.93 | 4 | 5 | ND | 4 | 37 | 1 | 2 | 2 | 31 | .20 | .090 | 5 | 34 | .32 | 158 | .10 | 4 | 1.84 | .02 | .13 | 1 | 1 |
| L6+00N 2+75E | 1 | 7 | 10 | 137 | .1 | 19 | 5 | 694 | 1.55 | 3 | 5 | ND | 1 | 70 | 1 | 2 | 2 | 27 | .37 | .043 | 6 | 22 | .26 | 149 | .07 | 4 | 1.24 | .02 | .12 | 1 | 1 |
| L6+00N 3+00E | 1 | 14 | 7 | 71 | .1 | 25 | 4 | 186 | 2.08 | 2 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 36 | .19 | .040 | 6 | 32 | .35 | 110 | .11 | 6 | 1.89 | .02 | .12 | 1 | 12 |
| L6+00N 3+25E | 1 | 9 | 6 | 97 | .1 | 19 | 4 | 267 | 1.58 | 4 | 5 | ND | 2 | 28 | 1 | 2 | 3 | 25 | .17 | .096 | 5 | 21 | .24 | 174 | .08 | 8 | 1.57 | .01 | .12 | 1 | 1 |
| L6+00N 3+50E | 1 | 9 | 3 | 57 | .1 | 16 | 4 | 236 | 1.77 | 2 | 5 | ND | 3 | 28 | 1 | 2 | 2 | 31 | .19 | .084 | 7 | 17 | .22 | 124 | .09 | 8 | 1.44 | .02 | .11 | 1 | 1 |
| L6+00N 3+75E | 1 | 7 | 7 | 59 | .1 | 10 | 4 | 253 | 1.74 | 2 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 32 | .18 | .064 | 6 | 16 | .21 | 114 | .09 | 3 | 1.39 | .02 | .11 | 1 | 2 |
| L6+00N 4+00E | 1 | 10 | 9 | 40 | .1 | 10 | 4 | 162 | 2.05 | 2 | 5 | ND | 4 | 32 | 1 | 2 | 2 | 45 | .21 | .040 | 11 | 23 | .26 | 92 | .12 | 5 | 1.04 | .02 | .12 | 2 | 1 |
| L6+00N 4+25E | 1 | 8 | 7 | 63 | .1 | 7 | 4 | 293 | 2.01 | 2 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 46 | .21 | .033 | 14 | 23 | .25 | 80 | .10 | 2 | .89 | .01 | .12 | 1 | 1 |
| L6+00N 4+50E | 1 | 14 | 5 | 64 | .1 | 10 | 4 | 198 | 1.94 | 2 | 5 | ND | 4 | 28 | 1 | 2 | 3 | 36 | .19 | .034 | 8 | 19 | .26 | 136 | .11 | 2 | 1.56 | .02 | .13 | 1 | 1 |
| L6+00N 4+75E | 1 | 16 | 11 | 117 | .2 | 18 | 5 | 343 | 1.95 | 5 | 5 | ND | 3 | 33 | 1 | 2 | 3 | 34 | .21 | .104 | 8 | 21 | .28 | 194 | .10 | 6 | 2.11 | .02 | .11 | 1 | 1 |
| L6+00N 5+00E | 1 | 10 | 6 | 92 | .1 | 10 | 4 | 301 | 1.75 | 2 | 5 | ND | 3 | 25 | 1 | 2 | 2 | 36 | .18 | .043 | 7 | 19 | .20 | 116 | .10 | 5 | 1.31 | .02 | .10 | 1 | 1 |
| L6+00N 5+25E | 1 | 16 | 9 | 112 | .1 | 17 | 4 | 310 | 1.99 | 5 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 36 | .21 | .100 | 8 | 20 | .28 | 177 | .10 | 2 | 2.04 | .02 | .10 | 2 | 1 |
| L6+00N 5+50E | 1 | 19 | 5 | 90 | .3 | 16 | 6 | 214 | 2.27 | 4 | 5 | ND | 4 | 26 | 1 | 2 | 2 | 42 | .23 | .081 | 7 | 19 | .32 | 132 | .11 | 7 | 1.96 | .02 | .13 | 1 | 1 |
| L6+00N 6+00E | 1 | 49 | 6 | 85 | .1 | 16 | 9 | 526 | 3.22 | 4 | 5 | ND | 5 | 52 | 1 | 2 | 2 | 77 | .48 | .084 | 19 | 27 | .62 | 91 | .12 | 4 | 1.79 | .02 | .21 | 1 | 1 |
| L6+00N 6+50E | 1 | 20 | 11 | 107 | .1 | 11 | 6 | 383 | 2.46 | 3 | 5 | ND | 5 | 29 | 1 | 2 | 2 | 51 | .28 | .034 | 6 | 18 | .35 | 105 | .11 | 7 | 1.57 | .02 | .21 | 1 | 1 |
| L6+00N 7+00E | 1 | 15 | 2 | 114 | .1 | 17 | 5 | 488 | 2.16 | 2 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 41 | .25 | .032 | 5 | 20 | .33 | 114 | .11 | 3 | 1.57 | .01 | .12 | 1 | 1 |
| L6+00N 7+50E | 1 | 23 | 9 | 96 | .1 | 17 | 6 | 211 | 2.38 | 2 | 5 | ND | 8 | 22 | 1 | 2 | 2 | 46 | .21 | .037 | 6 | 19 | .35 | 108 | .11 | 3 | 1.88 | .02 | .10 | 1 | 1 |
| L6+00N 8+00E | 1 | 34 | 6 | 88 | .2 | 14 | 7 | 436 | 2.48 | 2 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 52 | .32 | .071 | 7 | 16 | .36 | 110 | .09 | 7 | 1.59 | .02 | .13 | 1 | 1 |
| L6+00N 8+50E | 1 | 17 | 6 | 82 | .2 | 11 | 5 | 317 | 1.85 | 2 | 5 | ND | 2 | 23 | 1 | 2 | 2 | 32 | .24 | .034 | 5 | 13 | .26 | 93 | .08 | 6 | 1.43 | .01 | .13 | 1 | 1 |
| L6+00N 9+00E | 1 | 25 | 7 | 98 | .1 | 15 | 7 | 247 | 2.26 | 3 | 5 | ND | 3 | 23 | 1 | 2 | 3 | 35 | .22 | .123 | 6 | 17 | .31 | 162 | .10 | 3 | 2.40 | .02 | .12 | 1 | 1 |
| L6+00N 9+50E | 1 | 32 | 5 | 85 | .1 | 15 | 9 | 220 | 2.79 | 2 | 5 | ND | 3 | 29 | 1 | 2 | 2 | 56 | .23 | .064 | 6 | 14 | .40 | 122 | .11 | 2 | 1.88 | .01 | .12 | 3 | 2 |
| L5+00N 0+00E | 1 | 28 | 6 | 69 | .2 | 11 | 7 | 517 | 2.61 | 2 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 57 | .29 | .047 | 8 | 15 | .36 | 117 | .09 | 4 | 1.47 | .01 | .21 | 2 | 1 |
| L5+00N 0+25E | 1 | 28 | 7 | 76 | .1 | 13 | 7 | 637 | 2.80 | 5 | 5 | ND | 4 | 31 | 1 | 2 | 2 | 61 | .28 | .030 | 9 | 16 | .36 | 116 | .10 | 5 | 1.46 | .01 | .21 | 2 | 1 |
| L5+00N 0+50E | 1 | 31 | 5 | 74 | .1 | 8 | 7 | 383 | 2.93 | 5 | 5 | ND | 4 | 30 | 1 | 2 | 2 | 66 | .30 | .042 | 9 | 17 | .44 | 95 | .11 | 3 | 1.42 | .01 | .22 | 3 | 3 |
| L5+00N 0+75E | 1 | 32 | 6 | 85 | .1 | 21 | 9 | 500 | 3.19 | 2 | 5 | ND | 4 | 35 | 1 | 2 | 2 | 64 | .34 | .036 | 15 | 33 | .50 | 127 | .13 | 7 | 1.99 | .01 | .26 | 3 | 1 |
| L5+00N 1+00E | 1 | 36 | 11 | 69 | .1 | 23 | 9 | 390 | 3.28 | 2 | 5 | ND | 4 | 34 | 1 | 2 | 2 | 71 | .35 | .048 | 14 | 31 | .50 | 104 | .12 | 7 | 1.76 | .01 | .22 | 2 | 1 |
| L5+00N 1+25E | 1 | 28 | 9 | 55 | .1 | 24 | 9 | 334 | 2.92 | 3 | 5 | ND | 4 | 36 | 1 | 2 | 2 | 66 | .33 | .052 | 11 | 35 | .49 | 87 | .11 | 3 | 1.22 | .01 | .18 | 2 | 1 |
| L5+00N 1+50E | 1 | 34 | 8 | 67 | .1 | 15 | 8 | 292 | 3.22 | 2 | 5 | ND | 4 | 28 | 1 | 2 | 2 | 78 | .30 | .046 | 11 | 19 | .48 | 68 | .12 | 4 | 1.50 | .01 | .21 | 2 | 8 |
| L5+00N 1+75E | 1 | 23 | 8 | 56 | .1 | 8 | 7 | 322 | 2.82 | 2 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 65 | .28 | .037 | 7 | 18 | .34 | 84 | .10 | 4 | 1.26 | .01 | .17 | 1 | 2 |
| L5+00N 2+00E | 1 | 21 | 9 | 66 | .1 | 16 | 5 | 354 | 2.23 | 3 | 5 | ND | 3 | 40 | 1 | 2 | 2 | 43 | .29 | .034 | 11 | 23 | .32 | 117 | .10 | 8 | 1.82 | .01 | .15 | 1 | 1 |
| L5+00N 2+25E | 1 | 23 | 8 | 74 | .2 | 14 | 7 | 397 | 2.94 | 2 | 5 | ND | 4 | 34 | 1 | 2 | 2 | 69 | .33 | .054 | 11 | 20 | .33 | 116 | .10 | 8 | 1.35 | .01 | .18 | 2 | 1 |
| L5+00N 2+50E | 1 | 18 | 12 | 73 | .1 | 12 | 5 | 267 | 2.30 | 5 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 46 | .20 | .040 | 7 | 16 | .26 | 140 | .10 | 4 | 1.62 | .01 | .12 | 1 | 1 |
| STD C/AU-S | 21 | 62 | 39 | 132 | 7.1 | 72 | 31 | 1054 | 4.11 | 40 | 21 | 7 | 39 | 47 | 18 | 17 | 24 | 60 | .49 | .095 | 39 | 57 | .96 | 182 | .07 | 38 | 1.91 | .06 | .14 | 11 | 52 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L5+00N 2+75E | 1 | 7 | 3 | 94 | .1 | 8 | 4 | 327 | 1.66 | 2 | 5 | ND | 2 | 21 | 1 | 2 | 2 | 35 | .20 | .062 | 6 | 12 | .19 | 188 | .08 | 2 | 1.65 | .01 | .11 | 1 | 3 |
| L5+00N 3+00E | 1 | 10 | 6 | 60 | .1 | 9 | 4 | 212 | 1.94 | 2 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 43 | .22 | .050 | 9 | 17 | .22 | 118 | .09 | 2 | 1.44 | .01 | .13 | 1 | 1 |
| L5+00N 3+25E | 1 | 7 | 2 | 51 | .1 | 6 | 3 | 287 | 1.20 | 2 | 5 | ND | 1 | 19 | 1 | 2 | 2 | 24 | .16 | .018 | 5 | 12 | .15 | 90 | .07 | 2 | 1.07 | .01 | .10 | 1 | 1 |
| L5+00N 3+50E | 1 | 15 | 8 | 83 | .1 | 22 | 5 | 291 | 1.75 | 2 | 5 | ND | 2 | 40 | 1 | 2 | 3 | 30 | .27 | .027 | 12 | 34 | .41 | 141 | .09 | 2 | 1.81 | .01 | .17 | 1 | 1 |
| L5+00N 3+75E | 1 | 6 | 2 | 48 | .1 | 7 | 2 | 207 | .77 | 2 | 5 | ND | 1 | 28 | 1 | 2 | 2 | 13 | .16 | .039 | 4 | 11 | .14 | 127 | .04 | 2 | .85 | .01 | .08 | 1 | 1 |
| L5+00N 4+00E | 1 | 7 | 9 | 46 | .3 | 8 | 4 | 179 | 1.54 | 4 | 5 | ND | 2 | 29 | 1 | 2 | 2 | 29 | .17 | .018 | 6 | 18 | .22 | 104 | .09 | 3 | 1.41 | .01 | .14 | 2 | 2 |
| L5+00N 4+25E | 1 | 15 | 3 | 76 | .1 | 11 | 5 | 307 | 2.08 | 2 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 44 | .28 | .021 | 12 | 23 | .31 | 118 | .11 | 2 | 1.71 | .01 | .22 | 1 | 1 |
| L5+00N 4+50E | 1 | 15 | 12 | 80 | .1 | 17 | 6 | 238 | 2.83 | 3 | 5 | ND | 4 | 65 | 1 | 2 | 2 | 57 | .29 | .061 | 13 | 33 | .46 | 185 | .14 | 2 | 3.01 | .01 | .15 | 1 | 1 |
| L5+00N 4+75E | 1 | 12 | 4 | 67 | .1 | 11 | 5 | 164 | 2.01 | 2 | 5 | ND | 1 | 50 | 1 | 2 | 2 | 42 | .23 | .038 | 8 | 19 | .31 | 161 | .11 | 2 | 1.83 | .01 | .12 | 1 | 1 |
| L5+00N 5+00E | 1 | 14 | 9 | 79 | .3 | 12 | 5 | 297 | 1.78 | 2 | 5 | ND | 2 | 40 | 1 | 2 | 2 | 32 | .27 | .068 | 9 | 15 | .23 | 186 | .09 | 5 | 2.15 | .02 | .13 | 1 | 1 |
| L5+00N 5+25E | 1 | 12 | 11 | 70 | .1 | 9 | 5 | 491 | 1.87 | 2 | 5 | ND | 1 | 37 | 1 | 2 | 2 | 39 | .27 | .030 | 9 | 19 | .25 | 157 | .09 | 2 | 1.43 | .01 | .17 | 1 | 2 |
| L5+00N 5+50E | 1 | 16 | 6 | 74 | .2 | 11 | 5 | 551 | 2.07 | 3 | 5 | ND | 2 | 43 | 1 | 2 | 2 | 41 | .33 | .035 | 9 | 18 | .28 | 162 | .10 | 3 | 2.03 | .01 | .15 | 1 | 1 |
| L5+00N 5+75E | 1 | 17 | 5 | 85 | .3 | 11 | 5 | 271 | 2.14 | 2 | 5 | ND | 2 | 37 | 1 | 2 | 2 | 45 | .28 | .029 | 8 | 17 | .30 | 114 | .10 | 2 | 1.82 | .01 | .18 | 1 | 1 |
| L5+00N 6+00E | 1 | 63 | 11 | 84 | .3 | 15 | 8 | 378 | 3.54 | 2 | 5 | ND | 3 | 49 | 1 | 2 | 2 | 83 | .50 | .069 | 16 | 24 | .59 | 84 | .12 | 2 | 1.98 | .01 | .26 | 1 | 6 |
| L4+00N 10+00W | 1 | 10 | 5 | 48 | .2 | 11 | 4 | 274 | 1.77 | 3 | 5 | ND | 2 | 21 | 1 | 2 | 2 | 33 | .21 | .042 | 8 | 15 | .21 | 114 | .08 | 2 | 1.53 | .01 | .16 | 1 | 1 |
| L4+00N 9+50W | 1 | 18 | 6 | 40 | .1 | 9 | 5 | 471 | 1.79 | 2 | 5 | ND | 1 | 26 | 1 | 2 | 2 | 31 | .32 | .019 | 11 | 14 | .25 | 91 | .07 | 2 | 1.34 | .01 | .20 | 1 | 2 |
| L4+00N 9+00W | 1 | 12 | 9 | 55 | .1 | 9 | 5 | 591 | 2.08 | 5 | 5 | ND | 1 | 18 | 1 | 2 | 2 | 41 | .19 | .026 | 9 | 14 | .23 | 116 | .07 | 2 | 1.32 | .01 | .15 | 1 | 1 |
| L4+00N 8+50W | 1 | 16 | 8 | 37 | .1 | 6 | 5 | 676 | 1.76 | 2 | 5 | ND | 1 | 24 | 1 | 2 | 2 | 34 | .22 | .014 | 11 | 12 | .19 | 122 | .07 | 2 | 1.12 | .01 | .17 | 1 | 2 |
| L4+00N 8+00W | 1 | 12 | 12 | 43 | .2 | 8 | 5 | 510 | 1.90 | 2 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 36 | .27 | .025 | 9 | 13 | .22 | 121 | .08 | 3 | 1.58 | .01 | .19 | 1 | 1 |
| L4+00N 7+50W | 1 | 14 | 7 | 62 | .1 | 6 | 5 | 1322 | 1.91 | 2 | 5 | ND | 1 | 20 | 1 | 2 | 2 | 44 | .21 | .031 | 7 | 12 | .23 | 134 | .07 | 2 | 1.04 | .01 | .15 | 1 | 1 |
| L4+00N 7+00W | 1 | 19 | 4 | 100 | .2 | 11 | 6 | 1024 | 2.02 | 4 | 5 | ND | 1 | 30 | 1 | 2 | 2 | 39 | .30 | .062 | 9 | 15 | .25 | 230 | .08 | 2 | 1.71 | .01 | .22 | 2 | 1 |
| L4+00N 6+50W | 1 | 19 | 11 | 37 | .5 | 8 | 5 | 521 | 1.83 | 4 | 6 | ND | 3 | 27 | 1 | 3 | 2 | 36 | .34 | .023 | 10 | 13 | .22 | 114 | .08 | 7 | 1.53 | .01 | .17 | 2 | 1 |
| L4+00N 6+00W | 1 | 23 | 3 | 75 | .3 | 10 | 6 | 810 | 2.01 | 2 | 5 | ND | 1 | 44 | 1 | 2 | 2 | 40 | .54 | .069 | 10 | 15 | .25 | 201 | .08 | 6 | 1.53 | .01 | .24 | 1 | 2 |
| L4+00N 5+50W | 1 | 14 | 6 | 52 | .1 | 9 | 5 | 380 | 1.95 | 2 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 38 | .20 | .022 | 9 | 15 | .24 | 135 | .09 | 2 | 1.48 | .01 | .20 | 2 | 1 |
| L4+00N 5+00W | 1 | 9 | 10 | 49 | .2 | 8 | 4 | 481 | 1.68 | 3 | 5 | ND | 1 | 26 | 1 | 2 | 2 | 34 | .27 | .027 | 6 | 13 | .21 | 143 | .07 | 4 | 1.12 | .01 | .19 | 2 | 1 |
| L4+00N 4+50W | 1 | 19 | 6 | 41 | .3 | 11 | 6 | 218 | 2.31 | 3 | 5 | ND | 2 | 19 | 1 | 3 | 3 | 53 | .21 | .022 | 12 | 19 | .32 | 82 | .08 | 2 | .98 | .01 | .24 | 1 | 3 |
| L4+00N 4+00W | 1 | 12 | 6 | 48 | .1 | 14 | 6 | 432 | 1.90 | 2 | 5 | ND | 2 | 18 | 1 | 2 | 2 | 38 | .18 | .016 | 7 | 18 | .27 | 103 | .08 | 2 | 1.25 | .01 | .22 | 2 | 1 |
| L4+00N 3+50W | 1 | 30 | 10 | 77 | .1 | 13 | 7 | 905 | 1.96 | 3 | 5 | ND | 1 | 55 | 1 | 2 | 2 | 38 | .49 | .029 | 8 | 14 | .35 | 146 | .08 | 2 | 1.82 | .02 | .24 | 1 | 1 |
| L4+00N 3+00W | 1 | 39 | 11 | 99 | .2 | 20 | 10 | 648 | 2.84 | 4 | 5 | ND | 2 | 34 | 1 | 3 | 2 | 60 | .34 | .062 | 10 | 26 | .53 | 218 | .11 | 5 | 2.55 | .01 | .39 | 1 | 1 |
| L4+00N 2+50W | 1 | 67 | 16 | 103 | .3 | 17 | 12 | 598 | 4.09 | 4 | 5 | ND | 2 | 23 | 1 | 2 | 2 | 97 | .29 | .047 | 12 | 25 | .84 | 149 | .14 | 6 | 2.64 | .01 | .53 | 1 | 10 |
| L4+00N 2+00W | 1 | 34 | 11 | 99 | .3 | 14 | 9 | 799 | 2.72 | 3 | 5 | ND | 2 | 31 | 1 | 3 | 2 | 63 | .32 | .049 | 10 | 19 | .52 | 171 | .10 | 6 | 2.02 | .01 | .39 | 1 | 1 |
| L4+00N 1+50W | 1 | 39 | 3 | 96 | .1 | 16 | 11 | 971 | 3.17 | 3 | 5 | ND | 2 | 36 | 1 | 2 | 2 | 74 | .35 | .046 | 10 | 21 | .59 | 173 | .11 | 3 | 2.15 | .01 | .49 | 1 | 1 |
| L4+00N 1+00W | 1 | 42 | 9 | 73 | .1 | 11 | 7 | 701 | 2.33 | 3 | 5 | ND | 1 | 74 | 1 | 2 | 2 | 51 | .40 | .024 | 11 | 15 | .43 | 115 | .09 | 2 | 1.89 | .01 | .30 | 1 | 1 |
| L4+00N 0+50W | 1 | 19 | 8 | 61 | .1 | 9 | 6 | 828 | 2.11 | 3 | 5 | ND | 1 | 33 | 1 | 2 | 3 | 45 | .27 | .022 | 8 | 12 | .32 | 139 | .07 | 2 | 1.33 | .01 | .28 | 2 | 1 |
| L4+00N 0+00W | 1 | 32 | 7 | 47 | .1 | 14 | 7 | 590 | 2.38 | 2 | 5 | ND | 2 | 39 | 1 | 2 | 3 | 55 | .33 | .023 | 10 | 15 | .35 | 99 | .07 | 4 | 1.09 | .01 | .28 | 4 | 5 |
| L4+00N 0125E | 1 | 23 | 4 | 59 | .1 | 12 | 7 | 609 | 2.34 | 2 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 51 | .27 | .026 | 9 | 14 | .33 | 127 | .08 | 2 | 1.45 | .01 | .27 | 1 | 1 |
| STD C/AU-S | 17 | 58 | 43 | 132 | 7.2 | 67 | 29 | 985 | 3.91 | 43 | 18 | 7 | 37 | 47 | 18 | 19 | 19 | 57 | .46 | .096 | 38 | 56 | .85 | 176 | .06 | 32 | 1.86 | .06 | .13 | 12 | 48 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L4+00N 0+50E | 1 | 26 | 5 | 57 | .3 | 13 | 7 | 579 | 2.38 | 2 | 6 | ND | 2 | 35 | 1 | 2 | 2 | 51 | .30 | .028 | 9 | 14 | .35 | 135 | .08 | 3 | 1.61 | .01 | .27 | 1 | 3 |
| L4+00N 0+75E | 1 | 25 | 8 | 51 | .2 | 19 | 7 | 470 | 2.59 | 2 | 5 | ND | 2 | 34 | 1 | 2 | 2 | 58 | .28 | .025 | 9 | 15 | .33 | 113 | .09 | 2 | 1.67 | .01 | .23 | 2 | 7 |
| L4+00N 1+00E | 1 | 20 | 7 | 65 | .2 | 12 | 6 | 495 | 2.38 | 4 | 5 | ND | 3 | 36 | 1 | 2 | 2 | 52 | .28 | .025 | 8 | 15 | .32 | 109 | .09 | 4 | 1.44 | .01 | .25 | 1 | 2 |
| L4+00N 1+25E | 1 | 22 | 7 | 88 | .1 | 23 | 7 | 420 | 2.71 | 2 | 5 | ND | 3 | 32 | 1 | 2 | 2 | 53 | .30 | .034 | 11 | 22 | .34 | 130 | .10 | 2 | 2.17 | .02 | .24 | 1 | 1 |
| L4+00N 1+50E | 1 | 22 | 6 | 67 | .1 | 21 | 7 | 479 | 3.06 | 2 | 5 | ND | 2 | 32 | 1 | 2 | 2 | 68 | .32 | .053 | 10 | 28 | .36 | 121 | .08 | 2 | 1.37 | .01 | .19 | 1 | 1 |
| L4+00N 1+75E | 1 | 21 | 12 | 72 | .6 | 18 | 7 | 365 | 2.60 | 4 | 5 | ND | 5 | 26 | 1 | 4 | 2 | 54 | .29 | .031 | 10 | 24 | .33 | 107 | .10 | 8 | 1.91 | .01 | .19 | 1 | 4 |
| L4+00N 2+00E | 1 | 17 | 7 | 47 | .2 | 13 | 6 | 412 | 2.40 | 2 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 57 | .32 | .021 | 11 | 19 | .30 | 83 | .09 | 2 | 1.29 | .01 | .21 | 2 | 1 |
| L4+00N 2+25E | 1 | 20 | 6 | 47 | .2 | 12 | 7 | 460 | 2.67 | 2 | 6 | ND | 3 | 31 | 1 | 2 | 2 | 63 | .28 | .020 | 12 | 18 | .31 | 79 | .09 | 3 | 1.22 | .01 | .22 | 2 | 1 |
| L4+00N 2+50E | 1 | 18 | 8 | 45 | .1 | 11 | 6 | 323 | 2.65 | 4 | 5 | ND | 3 | 24 | 1 | 2 | 3 | 65 | .27 | .020 | 11 | 16 | .30 | 55 | .10 | 2 | 1.08 | .01 | .21 | 3 | 1 |
| L4+00N 2+75E | 1 | 15 | 6 | 56 | .1 | 12 | 5 | 280 | 2.29 | 2 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 48 | .28 | .063 | 11 | 16 | .25 | 99 | .09 | 2 | 1.63 | .01 | .16 | 1 | 1 |
| L4+00N 3+00E | 1 | 11 | 3 | 67 | .2 | 10 | 4 | 270 | 1.89 | 2 | 5 | ND | 2 | 29 | 1 | 2 | 2 | 40 | .27 | .055 | 8 | 14 | .22 | 115 | .08 | 2 | 1.59 | .01 | .10 | 1 | 2 |
| L4+00N 3+25E | 1 | 17 | 8 | 62 | .1 | 13 | 6 | 276 | 2.26 | 2 | 5 | ND | 3 | 29 | 1 | 2 | 2 | 49 | .31 | .072 | 16 | 18 | .29 | 119 | .09 | 2 | 1.49 | .02 | .18 | 1 | 2 |
| L4+00N 3+50E | 1 | 13 | 11 | 87 | .2 | 20 | 6 | 390 | 1.92 | 2 | 5 | ND | 3 | 37 | 1 | 2 | 2 | 36 | .26 | .168 | 9 | 21 | .27 | 201 | .09 | 5 | 2.11 | .01 | .13 | 1 | 1 |
| L4+00N 3+75E | 1 | 9 | 8 | 43 | .1 | 12 | 4 | 184 | 1.48 | 2 | 5 | ND | 2 | 27 | 1 | 2 | 2 | 27 | .22 | .028 | 5 | 14 | .22 | 96 | .08 | 2 | 1.58 | .01 | .11 | 1 | 3 |
| L4+00N 4+00E | 1 | 13 | 8 | 114 | .1 | 17 | 5 | 748 | 1.84 | 2 | 5 | ND | 2 | 35 | 1 | 2 | 2 | 30 | .24 | .128 | 9 | 18 | .26 | 303 | .09 | 2 | 2.48 | .01 | .14 | 1 | 2 |
| L4+00N 4+25E | 1 | 19 | 8 | 73 | .1 | 20 | 7 | 317 | 2.81 | 2 | 5 | ND | 5 | 60 | 1 | 2 | 2 | 60 | .30 | .044 | 18 | 29 | .48 | 140 | .13 | 2 | 2.42 | .01 | .22 | 1 | 1 |
| L4+00N 4+50E | 1 | 18 | 7 | 97 | .1 | 18 | 7 | 426 | 2.84 | 2 | 5 | ND | 4 | 64 | 1 | 2 | 2 | 58 | .34 | .067 | 14 | 28 | .47 | 289 | .14 | 2 | 2.97 | .01 | .22 | 1 | 2 |
| L4+00N 4+75E | 1 | 26 | 10 | 99 | .1 | 20 | 8 | 713 | 2.90 | 4 | 5 | ND | 4 | 44 | 1 | 2 | 2 | 64 | .34 | .065 | 11 | 31 | .49 | 170 | .13 | 2 | 1.88 | .01 | .26 | 1 | 3 |
| L4+00N 5+00E | 1 | 19 | 7 | 94 | .2 | 14 | 6 | 381 | 2.23 | 2 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 44 | .28 | .031 | 7 | 21 | .36 | 167 | .11 | 2 | 2.14 | .01 | .19 | 1 | 1 |
| L4+00N 5+25E | 1 | 23 | 10 | 76 | .5 | 15 | 7 | 379 | 2.40 | 4 | 5 | ND | 4 | 79 | 1 | 3 | 2 | 51 | .34 | .030 | 12 | 25 | .39 | 298 | .12 | 2 | 2.05 | .01 | .22 | 2 | 5 |
| L4+00N 5+50E | 1 | 51 | 8 | 107 | .5 | 20 | 9 | 596 | 3.30 | 2 | 5 | ND | 4 | 75 | 1 | 2 | 2 | 66 | .60 | .070 | 16 | 25 | .52 | 159 | .12 | 3 | 2.96 | .01 | .23 | 1 | 2 |
| L4+00N 5+75E | 1 | 27 | 8 | 160 | .2 | 16 | 6 | 822 | 2.25 | 2 | 5 | ND | 2 | 60 | 1 | 2 | 2 | 45 | .55 | .099 | 9 | 17 | .32 | 162 | .09 | 7 | 2.09 | .01 | .21 | 1 | 1 |
| L4+00N 6+00E | 1 | 34 | 12 | 150 | .4 | 20 | 8 | 525 | 2.97 | 2 | 5 | ND | 4 | 48 | 1 | 2 | 2 | 61 | .38 | .074 | 11 | 22 | .43 | 162 | .11 | 4 | 2.70 | .01 | .15 | 1 | 2 |
| L4+00N 6+50E | 1 | 15 | 6 | 94 | .1 | 8 | 5 | 536 | 1.75 | 2 | 5 | ND | 1 | 34 | 1 | 2 | 2 | 36 | .36 | .044 | 5 | 12 | .24 | 99 | .08 | 6 | 1.47 | .01 | .17 | 1 | 1 |
| L4+00N 7+00E | 1 | 58 | 5 | 163 | .3 | 23 | 12 | 648 | 4.61 | 2 | 5 | ND | 2 | 87 | 1 | 2 | 2 | 94 | .95 | .136 | 11 | 26 | .86 | 200 | .08 | 2 | 2.87 | .02 | .25 | 1 | 1 |
| L4+00N 7+50E | 1 | 18 | 4 | 87 | .1 | 12 | 6 | 254 | 2.29 | 2 | 5 | ND | 3 | 29 | 1 | 2 | 2 | 46 | .29 | .034 | 7 | 18 | .31 | 97 | .10 | 3 | 1.79 | .01 | .19 | 1 | 10 |
| L4+00N 8+00E | 1 | 19 | 3 | 73 | .2 | 17 | 6 | 270 | 2.20 | 3 | 5 | ND | 3 | 27 | 1 | 2 | 2 | 45 | .26 | .037 | 7 | 20 | .30 | 116 | .10 | 4 | 1.95 | .02 | .15 | 1 | 1 |
| L4+00N 8+50E | 1 | 15 | 4 | 94 | .2 | 13 | 5 | 235 | 1.96 | 2 | 5 | ND | 2 | 27 | 1 | 2 | 2 | 42 | .22 | .039 | 6 | 15 | .25 | 88 | .09 | 2 | 1.63 | .01 | .13 | 1 | 1 |
| L4+00N 9+00E | 1 | 13 | 5 | 118 | .1 | 14 | 5 | 329 | 1.64 | 3 | 5 | ND | 2 | 34 | 1 | 2 | 2 | 33 | .29 | .115 | 5 | 13 | .21 | 152 | .07 | 2 | 1.66 | .02 | .12 | 2 | 1 |
| L4+00N 9+50E | 1 | 23 | 4 | 152 | .1 | 14 | 6 | 560 | 2.29 | 2 | 5 | ND | 2 | 36 | 1 | 2 | 2 | 45 | .29 | .066 | 8 | 17 | .27 | 191 | .09 | 2 | 1.94 | .02 | .14 | 1 | 1 |
| L3+00N 0+00E | 1 | 35 | 7 | 89 | .2 | 16 | 8 | 559 | 2.93 | 2 | 5 | ND | 2 | 40 | 1 | 2 | 2 | 61 | .32 | .038 | 12 | 21 | .49 | 161 | .11 | 4 | 2.09 | .01 | .39 | 1 | 1 |
| L3+00N 0+25E | 1 | 26 | 8 | 78 | .3 | 20 | 8 | 548 | 2.76 | 3 | 5 | ND | 3 | 38 | 1 | 3 | 2 | 56 | .28 | .036 | 10 | 24 | .46 | 154 | .11 | 3 | 2.03 | .01 | .32 | 1 | 2 |
| L3+00N 0+50E | 1 | 32 | 6 | 67 | .1 | 13 | 8 | 491 | 2.80 | 2 | 5 | ND | 2 | 39 | 1 | 2 | 2 | 59 | .28 | .025 | 10 | 18 | .42 | 112 | .10 | 2 | 1.82 | .01 | .26 | 1 | 1 |
| L3+00N 0+75E | 1 | 32 | 10 | 85 | .2 | 12 | 8 | 743 | 3.01 | 2 | 5 | ND | 3 | 43 | 1 | 2 | 2 | 69 | .32 | .020 | 12 | 17 | .41 | 129 | .11 | 2 | 1.47 | .01 | .27 | 2 | 1 |
| L3+00N 1+00E | 1 | 28 | 10 | 90 | .1 | 13 | 8 | 703 | 3.08 | 2 | 5 | ND | 2 | 40 | 1 | 2 | 2 | 65 | .32 | .030 | 12 | 20 | .41 | 149 | .11 | 2 | 1.81 | .01 | .31 | 1 | 1 |
| L3+00N 1+25E | 1 | 21 | 11 | 98 | .2 | 18 | 7 | 586 | 2.35 | 2 | 5 | ND | 3 | 31 | 1 | 3 | 2 | 43 | .25 | .046 | 11 | 21 | .33 | 159 | .10 | 4 | 2.11 | .01 | .22 | 1 | 2 |
| STD C/AU-S | 18 | 60 | 40 | 132 | 6.7 | 68 | 30 | 1006 | 3.98 | 42 | 22 | 7 | 36 | 47 | 18 | 18 | 21 | 57 | .47 | .095 | 38 | 53 | .87 | 176 | .06 | 36 | 1.91 | .06 | .13 | 11 | 51 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L3+00N 1+50E | 1 | 21 | 5 | 59 | .2 | 23 | 7 | 288 | 2.68 | 2 | 5 | ND | 4 | 31 | 1 | 2 | 3 | 57 | .27 | .034 | 13 | 32 | .41 | 99 | .10 | 4 | 1.58 | .01 | .26 | 1 | 2 |
| L3+00N 1+75E | 1 | 29 | 10 | 73 | .2 | 14 | 7 | 537 | 2.86 | 5 | 5 | ND | 3 | 37 | 1 | 2 | 3 | 59 | .34 | .050 | 15 | 21 | .36 | 144 | .10 | 6 | 2.05 | .01 | .24 | 2 | 3 |
| L3+00N 2+00E | 1 | 25 | 9 | 63 | .2 | 10 | 6 | 528 | 2.88 | 5 | 5 | ND | 3 | 38 | 1 | 2 | 2 | 65 | .34 | .042 | 12 | 14 | .30 | 105 | .09 | 4 | 1.47 | .01 | .19 | 2 | 1 |
| L3+00N 2+25E | 1 | 24 | 13 | 52 | .1 | 7 | 6 | 363 | 2.94 | 2 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 67 | .30 | .021 | 11 | 13 | .32 | 80 | .10 | 3 | 1.47 | .02 | .20 | 4 | 2 |
| L3+00N 2+50E | 1 | 42 | 8 | 56 | .1 | 9 | 7 | 297 | 3.38 | 3 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 77 | .33 | .024 | 15 | 16 | .39 | 67 | .11 | 2 | 1.68 | .01 | .25 | 2 | 1 |
| L3+00N 2+75E | 1 | 31 | 8 | 62 | .1 | 8 | 6 | 251 | 2.79 | 2 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 59 | .34 | .018 | 12 | 15 | .36 | 64 | .11 | 4 | 1.74 | .01 | .25 | 1 | 5 |
| L3+00N 3+00E | 1 | 24 | 6 | 65 | .1 | 7 | 6 | 661 | 2.55 | 2 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 62 | .31 | .023 | 12 | 13 | .31 | 69 | .09 | 2 | 1.26 | .01 | .22 | 1 | 1 |
| L3+00N 3+25E | 1 | 16 | 8 | 82 | .1 | 9 | 5 | 442 | 2.25 | 2 | 5 | ND | 2 | 31 | 1 | 2 | 2 | 45 | .33 | .018 | 13 | 17 | .28 | 140 | .10 | 2 | 2.20 | .02 | .16 | 1 | 1 |
| L3+00N 3+50E | 1 | 20 | 7 | 47 | .1 | 10 | 6 | 243 | 2.55 | 2 | 5 | ND | 4 | 35 | 1 | 2 | 2 | 64 | .37 | .046 | 15 | 23 | .31 | 77 | .11 | 2 | 1.14 | .01 | .17 | 2 | 2 |
| L3+00N 4+00E | 1 | 17 | 17 | 110 | .1 | 18 | 11 | 1043 | 3.82 | 2 | 5 | ND | 6 | 147 | 1 | 2 | 2 | 92 | .70 | .095 | 26 | 28 | .89 | 241 | .25 | 10 | 3.62 | .05 | .26 | 1 | 1 |
| L3+00N 4+25E | 1 | 74 | 13 | 87 | .2 | 11 | 12 | 951 | 4.56 | 9 | 5 | ND | 4 | 95 | 1 | 2 | 2 | 107 | .96 | .161 | 20 | 21 | 1.04 | 98 | .09 | 2 | 2.79 | .02 | .26 | 1 | 4 |
| L3+00N 4+50E | 1 | 158 | 10 | 121 | .1 | 11 | 15 | 1204 | 5.69 | 10 | 5 | ND | 2 | 90 | 1 | 2 | 2 | 133 | .84 | .136 | 16 | 21 | 1.17 | 106 | .10 | 3 | 2.58 | .02 | .41 | 2 | 3 |
| L3+00N 4+75E | 1 | 147 | 11 | 111 | .4 | 12 | 12 | 554 | 4.48 | 4 | 5 | ND | 4 | 80 | 1 | 2 | 2 | 103 | .67 | .080 | 15 | 18 | .72 | 101 | .14 | 8 | 2.42 | .02 | .38 | 1 | 4 |
| L3+00N 5+00E | 1 | 63 | 13 | 97 | .1 | 15 | 9 | 480 | 3.66 | 6 | 5 | ND | 4 | 49 | 1 | 2 | 2 | 84 | .45 | .045 | 19 | 25 | .56 | 151 | .14 | 2 | 2.32 | .01 | .34 | 1 | 7 |
| L3+00N 5+25E | 1 | 54 | 12 | 90 | .1 | 14 | 9 | 577 | 3.30 | 2 | 5 | ND | 2 | 53 | 1 | 2 | 2 | 71 | .49 | .039 | 12 | 21 | .52 | 111 | .13 | 2 | 2.20 | .01 | .35 | 1 | 2 |
| L3+00N 5+50E | 1 | 44 | 11 | 112 | .1 | 20 | 9 | 587 | 3.26 | 3 | 5 | ND | 3 | 60 | 1 | 2 | 2 | 64 | .45 | .021 | 14 | 28 | .50 | 159 | .13 | 2 | 2.26 | .01 | .35 | 1 | 1 |
| L3+00N 5+75E | 1 | 44 | 11 | 100 | .1 | 15 | 9 | 673 | 2.96 | 3 | 5 | ND | 3 | 128 | 1 | 2 | 2 | 63 | .48 | .022 | 16 | 24 | .47 | 173 | .12 | 4 | 2.07 | .01 | .30 | 1 | 1 |
| L3+00N 6+00E | 1 | 30 | 11 | 100 | .2 | 13 | 7 | 435 | 2.69 | 2 | 5 | ND | 3 | 44 | 1 | 2 | 2 | 55 | .36 | .024 | 9 | 20 | .39 | 105 | .11 | 7 | 2.07 | .01 | .25 | 1 | 1 |
| L2+00N 10+00W | 1 | 8 | 8 | 57 | .1 | 11 | 5 | 448 | 1.97 | 2 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 41 | .16 | .025 | 9 | 19 | .22 | 113 | .09 | 2 | 1.46 | .01 | .11 | 2 | 1 |
| L2+00N 9+50W | 1 | 18 | 7 | 58 | .1 | 10 | 5 | 491 | 2.05 | 2 | 5 | ND | 2 | 32 | 1 | 2 | 2 | 40 | .41 | .019 | 13 | 15 | .26 | 90 | .08 | 2 | 1.75 | .02 | .16 | 1 | 2 |
| L2+00N 9+00W | 1 | 18 | 8 | 102 | .1 | 13 | 6 | 589 | 2.02 | 3 | 5 | ND | 2 | 34 | 1 | 2 | 3 | 38 | .29 | .137 | 11 | 16 | .24 | 206 | .08 | 2 | 1.88 | .02 | .13 | 1 | 1 |
| L2+00N 8+50W | 1 | 12 | 11 | 72 | .2 | 9 | 6 | 760 | 2.17 | 2 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 44 | .27 | .054 | 9 | 17 | .25 | 147 | .09 | 4 | 1.68 | .01 | .15 | 1 | 1 |
| L2+00N 8+00W | 1 | 13 | 5 | 59 | .1 | 9 | 5 | 636 | 1.89 | 2 | 5 | ND | 2 | 31 | 1 | 2 | 2 | 37 | .28 | .050 | 9 | 13 | .21 | 141 | .08 | 5 | 1.63 | .01 | .16 | 1 | 1 |
| L2+00N 7+50W | 1 | 16 | 8 | 75 | .1 | 13 | 6 | 445 | 2.27 | 2 | 5 | ND | 3 | 36 | 1 | 2 | 2 | 46 | .39 | .053 | 12 | 20 | .27 | 119 | .10 | 4 | 1.69 | .01 | .20 | 1 | 1 |
| L2+00N 7+00W | 1 | 20 | 8 | 48 | .1 | 8 | 6 | 640 | 2.13 | 3 | 5 | ND | 2 | 34 | 1 | 2 | 2 | 48 | .36 | .017 | 10 | 14 | .28 | 89 | .09 | 2 | 1.65 | .02 | .18 | 1 | 1 |
| L2+00N 6+50W | 1 | 16 | 6 | 58 | .1 | 11 | 6 | 327 | 2.86 | 2 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 73 | .30 | .039 | 15 | 29 | .31 | 96 | .13 | 2 | 1.32 | .02 | .17 | 1 | 1 |
| L2+00N 6+00W | 1 | 11 | 13 | 89 | .2 | 10 | 5 | 371 | 2.12 | 2 | 5 | ND | 2 | 23 | 1 | 2 | 2 | 47 | .23 | .041 | 8 | 15 | .23 | 128 | .09 | 4 | 1.60 | .01 | .15 | 1 | 1 |
| L2+00N 5+50W | 1 | 22 | 12 | 82 | .1 | 15 | 7 | 371 | 2.48 | 2 | 5 | ND | 1 | 29 | 1 | 2 | 2 | 51 | .30 | .049 | 8 | 20 | .33 | 148 | .11 | 2 | 2.17 | .01 | .20 | 1 | 1 |
| L2+00N 5+00W | 1 | 20 | 11 | 76 | .2 | 14 | 7 | 306 | 2.29 | 4 | 5 | ND | 2 | 29 | 1 | 2 | 2 | 46 | .28 | .078 | 8 | 16 | .29 | 146 | .09 | 5 | 2.05 | .02 | .15 | 1 | 1 |
| L2+00N 4+50W | 1 | 31 | 9 | 89 | .2 | 15 | 8 | 369 | 2.95 | 6 | 5 | ND | 3 | 25 | 1 | 2 | 2 | 60 | .25 | .048 | 10 | 18 | .43 | 130 | .11 | 3 | 2.19 | .01 | .24 | 1 | 7 |
| L2+00N 4+00W | 1 | 27 | 8 | 61 | .1 | 15 | 7 | 297 | 2.47 | 2 | 5 | ND | 1 | 34 | 1 | 2 | 2 | 49 | .28 | .026 | 10 | 17 | .35 | 117 | .10 | 2 | 2.11 | .02 | .19 | 1 | 1 |
| L2+00N 3+50W | 1 | 31 | 12 | 72 | .3 | 16 | 8 | 393 | 2.59 | 6 | 6 | ND | 3 | 36 | 1 | 2 | 2 | 52 | .27 | .065 | 11 | 17 | .38 | 150 | .10 | 5 | 2.64 | .02 | .21 | 1 | 4 |
| L2+00N 3+00W | 1 | 37 | 9 | 94 | .1 | 13 | 9 | 660 | 2.74 | 3 | 5 | ND | 1 | 34 | 1 | 2 | 2 | 58 | .29 | .048 | 8 | 16 | .45 | 163 | .10 | 3 | 2.15 | .01 | .29 | 1 | 3 |
| L2+00N 2+50W | 1 | 39 | 14 | 94 | .1 | 16 | 9 | 612 | 2.67 | 3 | 5 | ND | 2 | 39 | 1 | 2 | 2 | 56 | .35 | .069 | 12 | 18 | .44 | 181 | .10 | 2 | 2.67 | .02 | .23 | 1 | 1 |
| L2+00N 2+00W | 1 | 36 | 11 | 77 | .1 | 12 | 8 | 681 | 2.48 | 3 | 5 | ND | 2 | 48 | 1 | 2 | 2 | 51 | .38 | .048 | 10 | 16 | .42 | 148 | .09 | 3 | 2.05 | .01 | .31 | 1 | 1 |
| L2+00N 1+50W | 1 | 36 | 11 | 69 | .1 | 17 | 9 | 406 | 2.85 | 7 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 61 | .29 | .042 | 12 | 26 | .49 | 158 | .11 | 2 | 2.25 | .02 | .31 | 1 | 3 |
| STD C/AU-S | 18 | 58 | 37 | 132 | 6.6 | 68 | 30 | 1007 | 4.04 | 43 | 18 | 7 | 36 | 47 | 18 | 18 | 19 | 58 | .48 | .093 | 39 | 53 | .88 | 176 | .06 | 34 | 1.94 | .06 | .13 | 11 | 50 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L2+00N 1+00W | 1 | 44 | 9 | 77 | .5 | 12 | 9 | 701 | 2.69 | 2 | 5 | ND | 3 | 46 | 1 | 2 | 2 | 59 | .30 | .029 | 11 | 19 | .43 | 169 | .11 | 11 | 1.91 | .01 | .42 | 1 | 1 |
| L2+00N 0+50W | 1 | 55 | 5 | 109 | .5 | 16 | 10 | 668 | 3.23 | 2 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 72 | .30 | .073 | 12 | 22 | .50 | 170 | .11 | 6 | 1.99 | .01 | .29 | 1 | 1 |
| L2+00N 0+00W | 1 | 35 | 11 | 84 | .3 | 16 | 9 | 569 | 3.27 | 3 | 5 | ND | 4 | 43 | 1 | 2 | 2 | 69 | .31 | .054 | 23 | 27 | .50 | 143 | .12 | 5 | 1.63 | .01 | .36 | 1 | 1 |
| L2+00N 0+25E | 1 | 32 | 13 | 86 | .6 | 17 | 9 | 479 | 3.11 | 5 | 5 | ND | 4 | 41 | 1 | 3 | 2 | 64 | .29 | .043 | 13 | 24 | .48 | 139 | .12 | 8 | 2.36 | .01 | .38 | 1 | 1 |
| L2+00N 0+50E | 1 | 30 | 9 | 82 | .2 | 15 | 9 | 776 | 3.00 | 2 | 5 | ND | 2 | 45 | 1 | 2 | 2 | 63 | .31 | .027 | 11 | 19 | .47 | 147 | .11 | 3 | 2.10 | .01 | .38 | 1 | 1 |
| L2+00N 0+75E | 1 | 37 | 6 | 79 | .3 | 12 | 9 | 456 | 3.16 | 2 | 5 | ND | 2 | 35 | 1 | 2 | 3 | 71 | .27 | .027 | 9 | 18 | .48 | 117 | .12 | 3 | 2.02 | .01 | .35 | 1 | 1 |
| L2+00N 1+00E | 1 | 35 | 10 | 91 | .4 | 16 | 10 | 633 | 3.23 | 4 | 5 | ND | 3 | 36 | 1 | 2 | 2 | 72 | .25 | .025 | 10 | 20 | .49 | 138 | .12 | 4 | 2.08 | .01 | .34 | 1 | 1 |
| L2+00N 1+25E | 1 | 27 | 9 | 128 | .3 | 16 | 8 | 1068 | 2.75 | 2 | 5 | ND | 2 | 43 | 1 | 2 | 2 | 59 | .32 | .061 | 12 | 19 | .36 | 179 | .09 | 7 | 1.84 | .01 | .26 | 1 | 3 |
| L2+00N 1+50E | 1 | 27 | 10 | 79 | .1 | 15 | 8 | 565 | 2.88 | 3 | 5 | ND | 2 | 27 | 1 | 2 | 2 | 64 | .21 | .063 | 10 | 17 | .39 | 127 | .10 | 3 | 1.92 | .01 | .27 | 1 | 8 |
| L2+00N 1+75E | 1 | 32 | 10 | 80 | .4 | 13 | 8 | 531 | 3.12 | 3 | 5 | ND | 3 | 43 | 1 | 2 | 2 | 67 | .34 | .029 | 12 | 17 | .41 | 98 | .11 | 4 | 2.11 | .02 | .25 | 1 | 1 |
| L2+00N 2+00E | 1 | 32 | 5 | 142 | .4 | 13 | 7 | 522 | 2.67 | 2 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 58 | .35 | .060 | 9 | 13 | .40 | 124 | .10 | 8 | 2.33 | .01 | .25 | 1 | 1 |
| L2+00N 2+25E | 1 | 50 | 7 | 93 | .5 | 20 | 11 | 347 | 4.25 | 4 | 5 | ND | 4 | 32 | 1 | 2 | 2 | 98 | .27 | .044 | 17 | 25 | .57 | 124 | .13 | 6 | 2.33 | .01 | .34 | 1 | 2 |
| L2+00N 2+50E | 1 | 97 | 9 | 80 | .6 | 15 | 9 | 290 | 4.46 | 2 | 5 | ND | 4 | 53 | 1 | 2 | 2 | 104 | .38 | .060 | 15 | 24 | .56 | 86 | .13 | 8 | 2.01 | .01 | .40 | 1 | 1 |
| L2+00N 2+75E | 1 | 47 | 9 | 67 | .3 | 13 | 9 | 309 | 4.00 | 4 | 5 | ND | 4 | 41 | 1 | 2 | 2 | 95 | .33 | .035 | 16 | 20 | .50 | 99 | .12 | 5 | 1.74 | .01 | .38 | 2 | 3 |
| L2+00N 3+00E | 1 | 37 | 9 | 94 | .2 | 16 | 9 | 347 | 3.33 | 4 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 75 | .33 | .024 | 13 | 19 | .45 | 97 | .12 | 5 | 1.92 | .01 | .30 | 1 | 2 |
| L2+00N 3+25E | 1 | 52 | 16 | 120 | .3 | 19 | 10 | 464 | 4.14 | 5 | 5 | ND | 7 | 77 | 1 | 2 | 2 | 96 | .55 | .065 | 27 | 31 | .53 | 117 | .16 | 6 | 2.69 | .02 | .25 | 1 | 1 |
| L2+00N 3+50E | 1 | 38 | 10 | 95 | .1 | 22 | 10 | 459 | 4.20 | 4 | 5 | ND | 4 | 89 | 1 | 2 | 2 | 104 | .46 | .104 | 28 | 35 | .69 | 154 | .23 | 2 | 2.47 | .02 | .25 | 2 | 1 |
| L2+00N 3+75E | 1 | 35 | 11 | 112 | .4 | 19 | 9 | 418 | 3.75 | 2 | 5 | ND | 3 | 58 | 1 | 2 | 2 | 83 | .39 | .057 | 13 | 24 | .54 | 121 | .13 | 6 | 2.21 | .01 | .29 | 1 | 1 |
| L2+00N 4+00E | 1 | 145 | 15 | 123 | .8 | 17 | 14 | 1097 | 5.32 | 3 | 5 | ND | 5 | 82 | 1 | 2 | 2 | 112 | .72 | .064 | 18 | 25 | .79 | 102 | .12 | 4 | 2.87 | .02 | .27 | 2 | 14 |
| L2+00N 4+25E | 1 | 51 | 14 | 101 | .3 | 17 | 10 | 540 | 3.86 | 3 | 5 | ND | 4 | 56 | 1 | 2 | 2 | 90 | .38 | .026 | 16 | 24 | .60 | 83 | .13 | 5 | 1.95 | .01 | .37 | 2 | 6 |
| L2+00N 4+50E | 1 | 55 | 11 | 125 | .2 | 15 | 10 | 446 | 3.67 | 3 | 5 | ND | 3 | 55 | 1 | 2 | 2 | 76 | .45 | .051 | 14 | 17 | .48 | 120 | .13 | 4 | 2.73 | .02 | .27 | 1 | 1 |
| L2+00N 4+75E | 1 | 25 | 10 | 126 | .4 | 12 | 8 | 524 | 3.14 | 5 | 5 | ND | 6 | 52 | 1 | 2 | 2 | 80 | .43 | .047 | 19 | 21 | .54 | 176 | .14 | 5 | 1.58 | .01 | .29 | 1 | 2 |
| L2+00N 5+00E | 1 | 66 | 9 | 169 | .2 | 16 | 11 | 951 | 3.96 | 4 | 5 | ND | 3 | 91 | 1 | 2 | 2 | 83 | .57 | .053 | 17 | 19 | .49 | 135 | .11 | 7 | 2.76 | .02 | .32 | 1 | 1 |
| L2+00N 5+25E | 1 | 46 | 12 | 146 | .3 | 16 | 9 | 919 | 3.69 | 4 | 5 | ND | 3 | 81 | 1 | 2 | 2 | 82 | .50 | .040 | 13 | 20 | .45 | 133 | .11 | 5 | 2.12 | .01 | .31 | 1 | 3 |
| L2+00N 5+50E | 1 | 54 | 9 | 94 | .2 | 29 | 10 | 433 | 3.81 | 6 | 5 | ND | 5 | 70 | 1 | 2 | 2 | 82 | .47 | .040 | 22 | 37 | .55 | 118 | .13 | 4 | 2.30 | .01 | .33 | 1 | 1 |
| L2+00N 5+75E | 1 | 41 | 9 | 129 | .1 | 23 | 9 | 714 | 3.21 | 4 | 5 | ND | 3 | 64 | 1 | 2 | 2 | 67 | .51 | .057 | 14 | 26 | .41 | 149 | .11 | 4 | 2.35 | .01 | .28 | 1 | 2 |
| L2+00N 6+00E | 1 | 28 | 9 | 76 | .2 | 23 | 9 | 497 | 2.76 | 2 | 5 | ND | 3 | 43 | 1 | 2 | 2 | 56 | .38 | .021 | 13 | 28 | .42 | 113 | .11 | 2 | 2.14 | .01 | .22 | 1 | 1 |
| L2+00N 6+50E | 1 | 54 | 11 | 112 | .3 | 21 | 12 | 850 | 4.01 | 3 | 5 | ND | 4 | 57 | 1 | 2 | 2 | 93 | .40 | .028 | 15 | 32 | .63 | 125 | .14 | 6 | 2.33 | .01 | .32 | 2 | 9 |
| L2+00N 7+00E | 1 | 69 | 11 | 112 | .4 | 16 | 11 | 580 | 4.27 | 5 | 5 | ND | 4 | 51 | 1 | 5 | 3 | 93 | .43 | .051 | 16 | 25 | .64 | 112 | .13 | 6 | 2.51 | .02 | .39 | 3 | 1 |
| L2+00N 7+50E | 1 | 36 | 11 | 123 | .1 | 27 | 9 | 520 | 3.07 | 2 | 5 | ND | 2 | 48 | 1 | 2 | 2 | 60 | .43 | .041 | 13 | 38 | .55 | 149 | .12 | 2 | 2.41 | .02 | .34 | 1 | 5 |
| L2+00N 8+25E | 1 | 86 | 12 | 136 | .1 | 26 | 14 | 730 | 4.07 | 6 | 5 | ND | 3 | 51 | 1 | 2 | 2 | 89 | .54 | .064 | 19 | 33 | .59 | 120 | .11 | 2 | 2.46 | .01 | .33 | 1 | 4 |
| L2+00N 8+50E | 1 | 41 | 16 | 108 | .1 | 30 | 10 | 450 | 3.31 | 8 | 5 | ND | 4 | 45 | 1 | 3 | 2 | 59 | .41 | .061 | 19 | 36 | .48 | 154 | .13 | 2 | 3.03 | .01 | .34 | 3 | 1 |
| L2+00N 9+00E | 1 | 33 | 7 | 93 | .1 | 16 | 8 | 473 | 3.14 | 6 | 5 | ND | 3 | 42 | 1 | 2 | 2 | 67 | .36 | .022 | 17 | 25 | .42 | 106 | .12 | 2 | 1.85 | .01 | .32 | 1 | 87 |
| L2+00N 9+50E | 1 | 29 | 8 | 102 | .3 | 16 | 9 | 598 | 3.00 | 3 | 5 | ND | 4 | 44 | 1 | 2 | 2 | 67 | .35 | .055 | 15 | 25 | .45 | 112 | .11 | 7 | 1.54 | .01 | .27 | 2 | 1 |
| L1+00N 0+00E | 1 | 28 | 7 | 70 | .3 | 13 | 8 | 540 | 2.54 | 2 | 5 | ND | 2 | 47 | 1 | 2 | 2 | 52 | .30 | .029 | 10 | 20 | .43 | 167 | .10 | 5 | 2.06 | .01 | .37 | 1 | 1 |
| L1+00N 0+25E | 1 | 29 | 12 | 82 | .1 | 12 | 9 | 504 | 2.93 | 4 | 5 | ND | 1 | 51 | 1 | 2 | 2 | 63 | .31 | .027 | 9 | 18 | .52 | 142 | .11 | 2 | 2.27 | .01 | .42 | 3 | 1 |
| STD C/AU-S | 18 | 58 | 40 | 132 | 6.8 | 69 | 30 | 1020 | 4.01 | 44 | 18 | 7 | 37 | 48 | 18 | 19 | 20 | 60 | .47 | .094 | 40 | 56 | .87 | 178 | .06 | 35 | 1.94 | .06 | .13 | 12 | 52 |

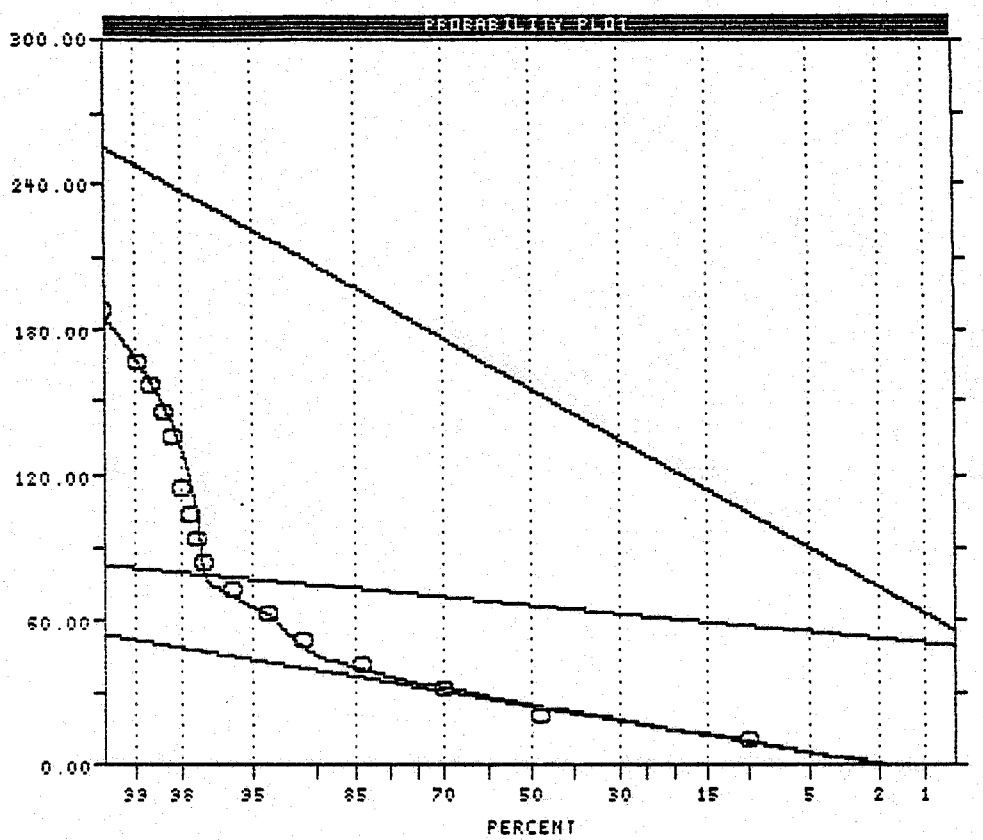
| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L1+00N 0+50E | 1 | 21 | 6 | 81 | .2 | 10 | 6 | 353 | 2.07 | 2 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 43 | .18 | .020 | 7 | 14 | .35 | 84 | .08 | 2 | 1.66 | .01 | .27 | 1 | 1 |
| L1+00N 0+75E | 1 | 27 | 11 | 108 | .5 | 17 | 7 | 541 | 2.74 | 2 | 5 | ND | 5 | 29 | 1 | 2 | 2 | 56 | .24 | .031 | 11 | 24 | .42 | 122 | .10 | 7 | 1.97 | .01 | .33 | 1 | 1 |
| L1+00N 1+00E | 1 | 24 | 8 | 105 | .3 | 10 | 6 | 550 | 2.61 | 2 | 5 | ND | 2 | 31 | 1 | 3 | 2 | 56 | .31 | .028 | 10 | 17 | .34 | 126 | .08 | 4 | 1.63 | .01 | .27 | 2 | 167 |
| L1+00N 1+25E | 1 | 33 | 8 | 121 | .3 | 14 | 7 | 482 | 2.80 | 2 | 5 | ND | 3 | 28 | 1 | 3 | 2 | 61 | .29 | .047 | 8 | 20 | .39 | 102 | .09 | 4 | 1.92 | .01 | .24 | 1 | 1 |
| L1+00N 1+50E | 1 | 27 | 10 | 90 | .4 | 13 | 7 | 529 | 2.60 | 3 | 5 | ND | 3 | 31 | 1 | 2 | 2 | 62 | .28 | .052 | 9 | 18 | .37 | 115 | .08 | 7 | 1.76 | .01 | .23 | 1 | 1 |
| L1+00N 1+75E | 1 | 31 | 8 | 74 | .2 | 12 | 7 | 323 | 2.99 | 2 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 66 | .24 | .030 | 11 | 17 | .36 | 100 | .09 | 2 | 1.74 | .01 | .23 | 1 | 7 |
| L1+00N 2+00E | 1 | 37 | 2 | 71 | .2 | 10 | 7 | 383 | 2.87 | 2 | 5 | ND | 4 | 24 | 1 | 2 | 3 | 69 | .23 | .049 | 11 | 15 | .43 | 74 | .08 | 3 | 1.33 | .01 | .28 | 1 | 1 |
| L1+00N 2+25E | 1 | 31 | 4 | 73 | .1 | 12 | 7 | 486 | 2.43 | 2 | 5 | ND | 3 | 30 | 1 | 2 | 2 | 53 | .22 | .023 | 10 | 15 | .35 | 109 | .08 | 2 | 1.50 | .01 | .25 | 1 | 6 |
| L1+00N 2+50E | 1 | 20 | 4 | 84 | .1 | 8 | 5 | 457 | 2.04 | 2 | 5 | ND | 2 | 29 | 1 | 2 | 2 | 45 | .22 | .020 | 9 | 11 | .29 | 92 | .08 | 2 | 1.43 | .01 | .23 | 1 | 1 |
| L1+00N 2+75E | 1 | 40 | 11 | 101 | .3 | 17 | 9 | 483 | 3.13 | 2 | 5 | ND | 3 | 44 | 1 | 2 | 2 | 66 | .31 | .040 | 15 | 20 | .49 | 145 | .11 | 2 | 2.20 | .01 | .34 | 1 | 1 |
| L1+00N 3+00E | 1 | 39 | 12 | 83 | .6 | 12 | 9 | 310 | 3.57 | 2 | 5 | ND | 4 | 38 | 1 | 3 | 2 | 82 | .28 | .030 | 12 | 18 | .55 | 105 | .12 | 5 | 2.02 | .01 | .36 | 1 | 6 |
| L1+00N 3+25E | 1 | 39 | 13 | 70 | .2 | 13 | 8 | 270 | 3.61 | 2 | 5 | ND | 5 | 50 | 1 | 2 | 2 | 83 | .31 | .040 | 19 | 20 | .59 | 100 | .13 | 5 | 2.02 | .01 | .39 | 1 | 1 |
| L1+00N 3+50E | 1 | 44 | 16 | 94 | .3 | 17 | 12 | 782 | 3.83 | 2 | 5 | ND | 5 | 66 | 1 | 2 | 2 | 89 | .42 | .081 | 23 | 27 | .64 | 149 | .15 | 5 | 2.54 | .01 | .36 | 1 | 15 |
| L1+00N 3+75E | 1 | 49 | 7 | 62 | .2 | 12 | 8 | 281 | 3.39 | 3 | 5 | ND | 4 | 41 | 1 | 2 | 2 | 83 | .28 | .031 | 14 | 19 | .54 | 86 | .12 | 3 | 1.64 | .01 | .32 | 1 | 2 |
| L1+00N 4+00E | 1 | 129 | 8 | 115 | .6 | 12 | 13 | 643 | 4.85 | 2 | 5 | ND | 3 | 75 | 1 | 2 | 2 | 111 | .52 | .057 | 13 | 20 | .68 | 83 | .13 | 3 | 2.22 | .01 | .37 | 3 | 9 |
| L1+00N 4+25E | 1 | 77 | 7 | 97 | .2 | 12 | 10 | 321 | 3.97 | 2 | 5 | ND | 3 | 49 | 1 | 2 | 2 | 90 | .41 | .031 | 10 | 16 | .53 | 71 | .12 | 4 | 2.00 | .01 | .36 | 1 | 3 |
| L1+00N 4+50E | 1 | 49 | 12 | 104 | .3 | 12 | 8 | 506 | 3.14 | 2 | 5 | ND | 2 | 43 | 1 | 2 | 2 | 68 | .35 | .035 | 11 | 14 | .39 | 104 | .10 | 3 | 2.08 | .01 | .25 | 2 | 2 |
| L1+00N 4+75E | 1 | 19 | 7 | 146 | .2 | 9 | 4 | 328 | 1.64 | 2 | 5 | ND | 2 | 39 | 1 | 2 | 2 | 33 | .30 | .054 | 6 | 9 | .22 | 104 | .07 | 4 | 1.65 | .01 | .14 | 1 | 1 |
| L1+00N 5+00E | 1 | 67 | 7 | 79 | .4 | 14 | 10 | 336 | 3.60 | 6 | 5 | ND | 4 | 54 | 1 | 2 | 2 | 85 | .39 | .056 | 12 | 19 | .54 | 113 | .13 | 4 | 2.06 | .01 | .31 | 1 | 2 |
| L1+00N 5+25E | 1 | 38 | 11 | 97 | .5 | 11 | 8 | 290 | 3.23 | 7 | 6 | ND | 6 | 55 | 1 | 2 | 2 | 81 | .46 | .062 | 22 | 19 | .57 | 193 | .13 | 4 | 1.67 | .01 | .28 | 1 | 1 |
| L1+00N 5+50E | 1 | 35 | 7 | 85 | .4 | 13 | 8 | 273 | 3.11 | 4 | 5 | ND | 6 | 49 | 1 | 2 | 2 | 74 | .34 | .044 | 15 | 21 | .53 | 164 | .12 | 4 | 1.69 | .01 | .30 | 1 | 1 |
| L1+00N 5+75E | 1 | 31 | 9 | 127 | .4 | 17 | 6 | 518 | 2.25 | 4 | 5 | ND | 3 | 45 | 1 | 2 | 2 | 46 | .38 | .066 | 11 | 18 | .31 | 180 | .09 | 6 | 2.16 | .01 | .21 | 1 | 1 |
| L1+00N 6+00E | 1 | 34 | 10 | 99 | .2 | 21 | 8 | 730 | 2.50 | 2 | 5 | ND | 2 | 58 | 1 | 2 | 2 | 49 | .59 | .042 | 13 | 26 | .41 | 160 | .09 | 2 | 2.08 | .01 | .21 | 1 | 1 |
| L0+00 10+00W | 1 | 22 | 8 | 48 | .4 | 15 | 7 | 365 | 2.32 | 2 | 5 | ND | 5 | 39 | 1 | 2 | 2 | 47 | .51 | .063 | 17 | 23 | .46 | 86 | .08 | 5 | 1.27 | .01 | .21 | 1 | 2 |
| L0+00 9+50W | 1 | 10 | 9 | 37 | .1 | 12 | 5 | 190 | 1.92 | 2 | 5 | ND | 4 | 25 | 1 | 2 | 2 | 41 | .23 | .070 | 10 | 20 | .27 | 95 | .08 | 3 | 1.19 | .01 | .15 | 1 | 1 |
| L0+00 9+00W | 1 | 21 | 7 | 36 | .3 | 17 | 7 | 311 | 2.37 | 2 | 5 | ND | 6 | 37 | 1 | 2 | 2 | 47 | .38 | .055 | 21 | 26 | .43 | 63 | .07 | 4 | 1.09 | .01 | .17 | 1 | 1 |
| L0+00 8+50W | 1 | 11 | 9 | 53 | .2 | 12 | 5 | 403 | 1.84 | 2 | 5 | ND | 3 | 23 | 1 | 2 | 2 | 38 | .22 | .065 | 9 | 18 | .23 | 123 | .07 | 3 | 1.32 | .01 | .15 | 1 | 1 |
| L0+00 8+00W | 1 | 7 | 11 | 50 | .3 | 9 | 4 | 636 | 1.47 | 2 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 29 | .18 | .034 | 5 | 14 | .21 | 126 | .07 | 5 | 1.31 | .01 | .13 | 1 | 1 |
| L0+00 7+50W | 1 | 13 | 12 | 81 | .5 | 15 | 5 | 538 | 1.77 | 3 | 6 | ND | 3 | 29 | 1 | 2 | 4 | 31 | .26 | .136 | 8 | 16 | .26 | 199 | .08 | 4 | 2.10 | .01 | .16 | 1 | 3 |
| L0+00 7+00W | 1 | 10 | 9 | 43 | .2 | 8 | 5 | 367 | 1.74 | 2 | 5 | ND | 3 | 24 | 1 | 2 | 2 | 37 | .19 | .021 | 9 | 14 | .26 | 84 | .08 | 6 | 1.13 | .01 | .15 | 1 | 1 |
| L0+00 6+50W | 1 | 14 | 9 | 71 | .4 | 10 | 5 | 467 | 1.64 | 2 | 5 | ND | 2 | 24 | 1 | 2 | 2 | 32 | .23 | .082 | 7 | 11 | .24 | 134 | .07 | 4 | 1.72 | .01 | .15 | 1 | 1 |
| L0+00 6+00W | 1 | 9 | 10 | 71 | .1 | 9 | 4 | 739 | 1.55 | 2 | 5 | ND | 1 | 17 | 1 | 2 | 2 | 32 | .18 | .076 | 4 | 12 | .19 | 140 | .06 | 2 | 1.34 | .01 | .13 | 1 | 1 |
| L0+00 5+50W | 1 | 21 | 4 | 36 | .2 | 7 | 6 | 330 | 1.96 | 3 | 5 | ND | 5 | 42 | 1 | 2 | 2 | 51 | 1.10 | .116 | 18 | 15 | .34 | 53 | .07 | 3 | .70 | .02 | .11 | 1 | 10 |
| L0+00 5+00W | 1 | 12 | 9 | 46 | .3 | 7 | 5 | 546 | 1.67 | 2 | 5 | ND | 2 | 22 | 1 | 2 | 2 | 36 | .22 | .026 | 8 | 13 | .18 | 127 | .06 | 4 | 1.07 | .01 | .13 | 1 | 1 |
| L0+00 4+50W | 1 | 10 | 8 | 48 | .1 | 7 | 4 | 430 | 1.61 | 3 | 5 | ND | 2 | 20 | 1 | 2 | 2 | 34 | .20 | .018 | 7 | 13 | .19 | 108 | .07 | 2 | 1.19 | .01 | .15 | 1 | 1 |
| L0+00 4+00W | 1 | 19 | 10 | 83 | .3 | 10 | 5 | 450 | 1.64 | 3 | 5 | ND | 2 | 33 | 1 | 2 | 2 | 36 | .44 | .130 | 10 | 14 | .24 | 125 | .06 | 5 | 1.15 | .01 | .13 | 1 | 1 |
| STD C/AU-S | 18 | 58 | 42 | 132 | 6.5 | 68 | 30 | 1020 | 4.05 | 42 | 18 | 7 | 36 | 47 | 18 | 18 | 21 | 58 | .47 | .095 | 38 | 55 | .87 | 171 | .06 | 33 | 1.92 | .06 | .13 | 11 | 51 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L0+00 3+50W | 1 | 32 | 12 | 75 | .1 | 16 | 8 | 520 | 2.78 | 4 | 5 | ND | 4 | 38 | 1 | 2 | 2 | 60 | .46 | .070 | 15 | 22 | .54 | 125 | .10 | 2 | 2.01 | .02 | .25 | 1 | 7 |
| L0+00 3+00W | 1 | 23 | 3 | 90 | .1 | 13 | 7 | 733 | 1.90 | 3 | 5 | ND | 2 | 37 | 1 | 2 | 2 | 39 | .35 | .155 | 7 | 12 | .35 | 160 | .08 | 5 | 1.92 | .01 | .19 | 1 | 1 |
| L0+00 2+50W | 1 | 14 | 2 | 62 | .2 | 9 | 6 | 373 | 1.86 | 2 | 5 | ND | 2 | 41 | 1 | 2 | 2 | 37 | .38 | .019 | 4 | 12 | .33 | 80 | .08 | 6 | 1.89 | .01 | .17 | 1 | 1 |
| L0+00 2+00W | 1 | 31 | 6 | 165 | .2 | 12 | 7 | 1010 | 2.74 | 6 | 5 | ND | 1 | 33 | 1 | 2 | 5 | 53 | .31 | .051 | 8 | 14 | .39 | 156 | .08 | 5 | 2.67 | .01 | .25 | 2 | 2 |
| L0+00 1+50W | 1 | 30 | 4 | 132 | .2 | 13 | 9 | 1072 | 2.86 | 4 | 5 | ND | 3 | 34 | 1 | 2 | 2 | 63 | .43 | .030 | 8 | 21 | .54 | 148 | .10 | 5 | 2.43 | .01 | .25 | 1 | 3 |
| L0+00 1+00W | 1 | 24 | 5 | 94 | .1 | 11 | 7 | 790 | 2.42 | 4 | 5 | ND | 2 | 37 | 1 | 2 | 2 | 47 | .35 | .026 | 10 | 14 | .38 | 153 | .10 | 4 | 2.54 | .01 | .22 | 1 | 1 |
| L0+00 0+50W | 1 | 34 | 9 | 103 | .1 | 11 | 8 | 737 | 2.79 | 8 | 5 | ND | 4 | 45 | 1 | 2 | 2 | 54 | .37 | .032 | 17 | 14 | .40 | 112 | .09 | 3 | 2.25 | .01 | .27 | 1 | 3 |
| L0+00 0+00W | 1 | 24 | 10 | 76 | .1 | 11 | 7 | 489 | 2.51 | 3 | 5 | ND | 1 | 33 | 1 | 2 | 2 | 53 | .27 | .021 | 8 | 16 | .45 | 89 | .09 | 2 | 2.16 | .01 | .29 | 1 | 1 |
| L0+00 0+25E | 1 | 64 | 5 | 125 | .1 | 16 | 12 | 1086 | 3.91 | 7 | 5 | ND | 2 | 53 | 1 | 2 | 2 | 71 | .48 | .044 | 14 | 17 | .55 | 136 | .09 | 6 | 2.85 | .01 | .38 | 1 | 18 |
| L0+00 0+50E | 1 | 40 | 15 | 117 | .3 | 15 | 10 | 1091 | 3.24 | 10 | 6 | ND | 3 | 40 | 1 | 2 | 2 | 63 | .42 | .030 | 13 | 18 | .49 | 158 | .10 | 7 | 2.78 | .01 | .34 | 2 | 1 |
| L0+00 0+75E | 1 | 66 | 14 | 114 | .2 | 15 | 11 | 678 | 3.83 | 8 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 84 | .32 | .035 | 10 | 17 | .62 | 130 | .11 | 5 | 3.10 | .01 | .34 | 2 | 2 |
| L0+00 1+00E | 1 | 75 | 10 | 93 | .2 | 18 | 11 | 474 | 3.91 | 7 | 5 | ND | 4 | 28 | 1 | 2 | 2 | 92 | .34 | .050 | 17 | 21 | .72 | 119 | .12 | 6 | 2.81 | .01 | .39 | 1 | 1 |
| L0+00 1+25E | 1 | 51 | 9 | 108 | .1 | 15 | 10 | 437 | 3.61 | 5 | 5 | ND | 3 | 28 | 1 | 2 | 2 | 80 | .35 | .059 | 15 | 24 | .65 | 99 | .11 | 2 | 2.58 | .01 | .33 | 2 | 19 |
| L0+00 1+50E | 1 | 25 | 14 | 143 | .3 | 15 | 7 | 609 | 2.43 | 7 | 5 | ND | 3 | 27 | 1 | 2 | 2 | 50 | .28 | .072 | 8 | 16 | .38 | 157 | .09 | 7 | 2.51 | .01 | .23 | 1 | 1 |
| L0+00 1+75E | 1 | 36 | 13 | 96 | .3 | 11 | 8 | 467 | 3.37 | 3 | 5 | ND | 4 | 38 | 1 | 2 | 2 | 77 | .41 | .057 | 11 | 15 | .44 | 111 | .11 | 6 | 2.25 | .01 | .23 | 3 | 1 |
| L0+00 2+00E | 1 | 15 | 16 | 90 | .2 | 9 | 7 | 687 | 2.04 | 4 | 5 | ND | 2 | 48 | 1 | 2 | 2 | 45 | .30 | .021 | 8 | 11 | .31 | 109 | .08 | 3 | 1.52 | .01 | .20 | 2 | 4 |
| L0+00 2+25E | 1 | 45 | 9 | 119 | .4 | 12 | 10 | 552 | 3.50 | 6 | 5 | ND | 4 | 77 | 1 | 2 | 2 | 75 | .48 | .032 | 12 | 16 | .52 | 113 | .09 | 8 | 2.14 | .01 | .33 | 1 | 1 |
| L0+00 2+50E | 1 | 22 | 11 | 67 | .1 | 10 | 7 | 354 | 2.73 | 3 | 5 | ND | 2 | 45 | 1 | 2 | 2 | 60 | .31 | .027 | 7 | 14 | .37 | 101 | .09 | 3 | 2.00 | .01 | .20 | 1 | 1 |
| L0+00 2+75E | 2 | 19 | 5 | 81 | .1 | 12 | 6 | 415 | 2.43 | 2 | 5 | ND | 1 | 46 | 1 | 2 | 2 | 52 | .32 | .035 | 7 | 14 | .33 | 109 | .08 | 2 | 1.99 | .01 | .15 | 1 | 1 |
| L0+00 3+00E | 1 | 18 | 5 | 109 | .1 | 10 | 6 | 590 | 2.63 | 2 | 5 | ND | 4 | 39 | 1 | 2 | 2 | 56 | .31 | .029 | 9 | 14 | .35 | 127 | .10 | 2 | 1.85 | .01 | .24 | 1 | 1 |
| L0+00 3+25E | 1 | 19 | 4 | 93 | .1 | 15 | 6 | 544 | 2.45 | 2 | 5 | ND | 3 | 55 | 1 | 2 | 2 | 50 | .42 | .026 | 11 | 22 | .37 | 153 | .11 | 4 | 1.88 | .01 | .22 | 1 | 1 |
| L0+00 3+50E | 1 | 21 | 12 | 86 | .2 | 12 | 6 | 336 | 2.68 | 2 | 5 | ND | 4 | 39 | 1 | 2 | 6 | 56 | .31 | .032 | 9 | 16 | .37 | 154 | .12 | 7 | 2.45 | .02 | .19 | 1 | 1 |
| L0+00 3+75E | 1 | 24 | 14 | 82 | .4 | 16 | 7 | 439 | 2.89 | 5 | 5 | ND | 4 | 44 | 1 | 2 | 2 | 61 | .38 | .023 | 10 | 20 | .39 | 120 | .12 | 9 | 2.13 | .01 | .26 | 1 | 2 |
| L0+00 4+00E | 1 | 38 | 11 | 101 | .3 | 14 | 8 | 406 | 3.52 | 4 | 5 | ND | 4 | 37 | 1 | 2 | 2 | 78 | .27 | .031 | 12 | 19 | .48 | 141 | .13 | 6 | 2.32 | .01 | .31 | 1 | 1 |
| L0+00 4+25E | 1 | 27 | 13 | 152 | .3 | 13 | 8 | 839 | 2.58 | 2 | 5 | ND | 3 | 58 | 1 | 2 | 2 | 54 | .60 | .039 | 11 | 16 | .37 | 165 | .10 | 6 | 2.14 | .01 | .22 | 2 | 1 |
| L0+00 4+50E | 1 | 46 | 12 | 113 | .2 | 14 | 8 | 764 | 2.91 | 5 | 5 | ND | 3 | 56 | 1 | 2 | 2 | 61 | .43 | .035 | 10 | 17 | .36 | 186 | .11 | 8 | 2.39 | .01 | .28 | 1 | 1 |
| L0+00 4+75E | 1 | 74 | 10 | 111 | .4 | 20 | 9 | 367 | 3.57 | 5 | 5 | ND | 4 | 54 | 1 | 2 | 2 | 74 | .43 | .058 | 13 | 27 | .51 | 113 | .13 | 8 | 2.40 | .02 | .32 | 1 | 1 |
| L0+00 5+00E | 1 | 40 | 11 | 88 | .1 | 13 | 8 | 281 | 3.43 | 6 | 5 | ND | 5 | 49 | 1 | 2 | 2 | 75 | .35 | .032 | 12 | 20 | .55 | 162 | .14 | 2 | 2.09 | .02 | .32 | 1 | 93 |
| L0+00 5+25E | 1 | 22 | 5 | 106 | .2 | 9 | 7 | 510 | 2.38 | 3 | 5 | ND | 4 | 35 | 1 | 2 | 2 | 53 | .28 | .025 | 8 | 14 | .38 | 153 | .11 | 6 | 1.63 | .01 | .23 | 1 | 1 |
| L0+00 5+50E | 1 | 23 | 9 | 91 | .1 | 13 | 6 | 628 | 2.01 | 3 | 5 | ND | 2 | 39 | 1 | 2 | 2 | 41 | .35 | .024 | 8 | 19 | .32 | 157 | .09 | 3 | 1.69 | .01 | .22 | 1 | 1 |
| L0+00 5+75E | 1 | 27 | 15 | 113 | .5 | 24 | 8 | 884 | 2.59 | 4 | 5 | ND | 5 | 57 | 1 | 2 | 2 | 50 | .45 | .070 | 10 | 35 | .44 | 217 | .11 | 9 | 1.85 | .01 | .25 | 1 | 1 |
| L0+00 6+00E | 1 | 34 | 13 | 101 | .1 | 18 | 7 | 462 | 2.69 | 7 | 5 | ND | 3 | 39 | 1 | 2 | 2 | 51 | .32 | .063 | 9 | 20 | .37 | 146 | .10 | 6 | 2.35 | .01 | .26 | 2 | 1 |
| L0+00 6+50E | 1 | 24 | 5 | 71 | .1 | 14 | 6 | 563 | 1.94 | 6 | 5 | ND | 3 | 36 | 1 | 2 | 2 | 34 | .29 | .029 | 9 | 15 | .28 | 147 | .09 | 6 | 2.28 | .02 | .13 | 1 | 2 |
| L0+00 7+00E | 1 | 49 | 9 | 90 | .2 | 20 | 10 | 638 | 3.45 | 3 | 5 | ND | 4 | 38 | 1 | 2 | 2 | 73 | .34 | .048 | 12 | 28 | .58 | 143 | .11 | 6 | 2.02 | .01 | .36 | 1 | 1 |
| L0+00 7+50E | 1 | 44 | 12 | 67 | .1 | 20 | 10 | 494 | 3.12 | 7 | 5 | ND | 3 | 38 | 1 | 2 | 2 | 62 | .36 | .023 | 14 | 28 | .54 | 133 | .11 | 3 | 2.27 | .01 | .31 | 1 | 2 |
| L0+00 8+00E | 1 | 42 | 7 | 87 | .4 | 15 | 9 | 642 | 2.78 | 2 | 5 | ND | 4 | 42 | 1 | 2 | 2 | 57 | .39 | .057 | 12 | 20 | .42 | 140 | .09 | 6 | 1.80 | .01 | .26 | 1 | 12 |
| STD C/AU-S | 17 | 58 | 42 | 131 | 6.6 | 67 | 29 | 996 | 3.95 | 42 | 20 | 8 | 36 | 47 | 18 | 17 | 19 | 57 | .47 | .088 | 38 | 53 | .85 | 175 | .06 | 37 | 1.86 | .06 | .13 | 12 | 53 |

| SAMPLE# | Mo PPM | Cu PPM | Pb PPM | Zn PPM | Ag PPM | Ni PPM | Co PPM | Mn PPM | Fe % | As PPM | U PPM | Au PPM | Th PPM | Sr PPM | Cd PPM | Sb PPM | Bi PPM | V PPM | Ca % | P % | La PPM | Cr PPM | Mg % | Ba PPM | Ti % | B PPM | Al % | Na % | K % | W PPM | Au* PPB |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| L0+00 8+50E | 1 | 44 | 10 | 108 | .1 | 22 | 11 | 1339 | 3.10 | 2 | 5 | ND | 4 | 46 | 1 | 2 | 2 | 54 | .46 | .040 | 16 | 30 | .51 | 187 | .12 | 5 | 2.95 | .01 | .27 | 1 | 10 |
| L0+00 9+00E | 1 | 35 | 13 | 94 | .2 | 24 | 10 | 594 | 3.12 | 2 | 5 | ND | 4 | 42 | 1 | 2 | 2 | 58 | .39 | .043 | 13 | 31 | .51 | 139 | .12 | 5 | 2.45 | .02 | .27 | 1 | 1 |
| L0+00 9+50E | 1 | 47 | 9 | 86 | .1 | 27 | 10 | 464 | 3.19 | 2 | 5 | ND | 6 | 56 | 1 | 2 | 2 | 55 | .45 | .067 | 18 | 38 | .57 | 155 | .13 | 7 | 3.04 | .01 | .37 | 1 | 1 |
| L0+00 10+00E | 1 | 43 | 11 | 99 | .1 | 26 | 11 | 694 | 3.25 | 2 | 5 | ND | 5 | 40 | 1 | 2 | 2 | 62 | .37 | .039 | 15 | 36 | .56 | 147 | .13 | 8 | 2.42 | .02 | .28 | 1 | 1 |
| L11+50N 0+00 | 1 | 11 | 6 | 38 | .1 | 8 | 4 | 529 | 1.69 | 2 | 5 | ND | 2 | 49 | 1 | 2 | 2 | 28 | .41 | .222 | 7 | 16 | .19 | 196 | .07 | 6 | 1.43 | .02 | .11 | 1 | 1 |
| L11+00N 0+00 | 1 | 6 | 4 | 33 | .2 | 8 | 5 | 545 | 1.50 | 2 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 22 | .18 | .273 | 4 | 10 | .11 | 158 | .08 | 4 | 1.88 | .02 | .08 | 1 | 1 |
| L10+50N 0+00 | 1 | 8 | 5 | 63 | .2 | 17 | 4 | 575 | 1.56 | 2 | 5 | ND | 2 | 30 | 1 | 2 | 2 | 24 | .24 | .248 | 4 | 16 | .17 | 251 | .07 | 7 | 1.50 | .01 | .07 | 1 | 1 |
| L9+50N 0+00 | 1 | 16 | 12 | 85 | .3 | 19 | 6 | 424 | 2.09 | 2 | 5 | ND | 3 | 33 | 1 | 2 | 3 | 34 | .25 | .121 | 10 | 20 | .26 | 188 | .09 | 6 | 2.04 | .02 | .10 | 1 | 1 |
| L9+00N 0+00 | 1 | 15 | 12 | 156 | .3 | 19 | 6 | 476 | 2.12 | 2 | 5 | ND | 3 | 33 | 1 | 2 | 2 | 34 | .26 | .236 | 8 | 20 | .28 | 232 | .09 | 6 | 2.08 | .02 | .12 | 1 | 1 |
| L8+50N 0+00 | 1 | 19 | 7 | 89 | .3 | 19 | 7 | 250 | 2.55 | 2 | 5 | ND | 4 | 33 | 1 | 3 | 2 | 47 | .28 | .083 | 9 | 29 | .40 | 137 | .11 | 8 | 2.11 | .02 | .17 | 1 | 1 |
| L7+50N 0+00 | 1 | 59 | 11 | 73 | .1 | 16 | 11 | 439 | 4.08 | 3 | 5 | ND | 7 | 44 | 1 | 3 | 2 | 98 | .52 | .102 | 25 | 29 | .69 | 101 | .12 | 9 | 1.98 | .02 | .25 | 2 | 1 |
| L7+00N 0+00 | 1 | 14 | 9 | 159 | .2 | 10 | 6 | 1174 | 2.25 | 2 | 5 | ND | 2 | 26 | 1 | 2 | 2 | 40 | .23 | .071 | 7 | 16 | .29 | 192 | .09 | 6 | 1.75 | .01 | .15 | 1 | 1 |
| L6+50N 0+00 | 1 | 21 | 11 | 80 | .2 | 12 | 8 | 530 | 2.94 | 2 | 5 | ND | 4 | 35 | 1 | 2 | 2 | 61 | .35 | .063 | 11 | 18 | .39 | 133 | .10 | 6 | 1.49 | .01 | .17 | 2 | 31 |
| L5+50N 0+00 | 1 | 23 | 10 | 83 | .2 | 12 | 8 | 670 | 2.71 | 2 | 5 | ND | 3 | 39 | 1 | 2 | 2 | 54 | .35 | .042 | 10 | 19 | .34 | 125 | .10 | 7 | 1.71 | .02 | .19 | 1 | 1 |
| L4+50N 0+00 | 1 | 36 | 10 | 68 | .3 | 10 | 8 | 659 | 2.85 | 2 | 5 | ND | 3 | 35 | 1 | 2 | 2 | 57 | .31 | .046 | 12 | 17 | .39 | 144 | .09 | 8 | 1.82 | .01 | .26 | 1 | 2 |
| L3+50N 0+00 | 1 | 36 | 12 | 97 | .2 | 18 | 9 | 780 | 2.95 | 2 | 5 | ND | 3 | 47 | 1 | 2 | 2 | 58 | .42 | .046 | 14 | 23 | .51 | 178 | .10 | 9 | 2.13 | .01 | .32 | 1 | 1 |
| L2+50N 0+00 | 1 | 33 | 11 | 94 | .2 | 19 | 9 | 506 | 2.90 | 2 | 5 | ND | 4 | 36 | 1 | 2 | 3 | 55 | .30 | .061 | 12 | 21 | .51 | 228 | .12 | 11 | 2.80 | .02 | .32 | 1 | 1 |
| L1+50N 0+00 | 1 | 43 | 15 | 98 | .2 | 11 | 11 | 781 | 3.37 | 2 | 5 | ND | 3 | 46 | 1 | 2 | 2 | 78 | .34 | .032 | 9 | 18 | .71 | 172 | .13 | 11 | 2.41 | .01 | .52 | 1 | 1 |
| L0+50N 0+00 | 1 | 30 | 14 | 93 | .3 | 15 | 10 | 474 | 3.33 | 2 | 5 | ND | 4 | 43 | 1 | 2 | 2 | 70 | .30 | .045 | 12 | 26 | .62 | 160 | .13 | 5 | 2.55 | .01 | .32 | 1 | 1 |
| STD C/AU-S | 17 | 59 | 40 | 132 | 6.7 | 68 | 30 | 1026 | 4.05 | 41 | 22 | 8 | 39 | 48 | 18 | 17 | 18 | 60 | .48 | .094 | 39 | 55 | .93 | 178 | .06 | 38 | 2.03 | .06 | .13 | 11 | 51 |

# APPENDIX D - GEOCHEMISTRY STATISTICS

Zumar Property: Skyworld Resources Development Lt




ARITHMETIC VALUES

VARIABLE = Cu ppm

UNIT =

N = 415

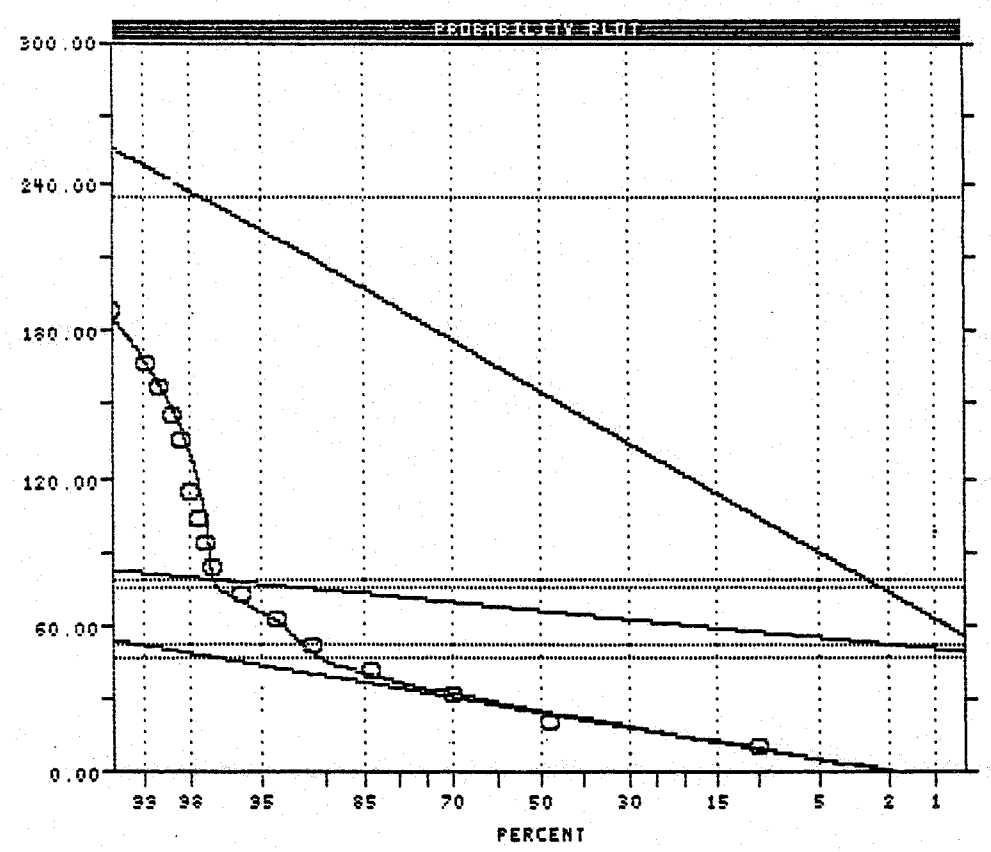
N CI = 27

POPULATIONS

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | 23.195 | 11.669 | 92.5 |
| 2 | 64.810 | 6.524 | 4.7 |
| 3 | 155.000 | 40.000 | 2.8 |

USERS VISUAL PARAMETER ESTIMATES

Zumar Property: Skyworld Resources Development Lt




ARITHMETIC VALUES

VARIABLE = Cu ppm

UNIT =

N = 415

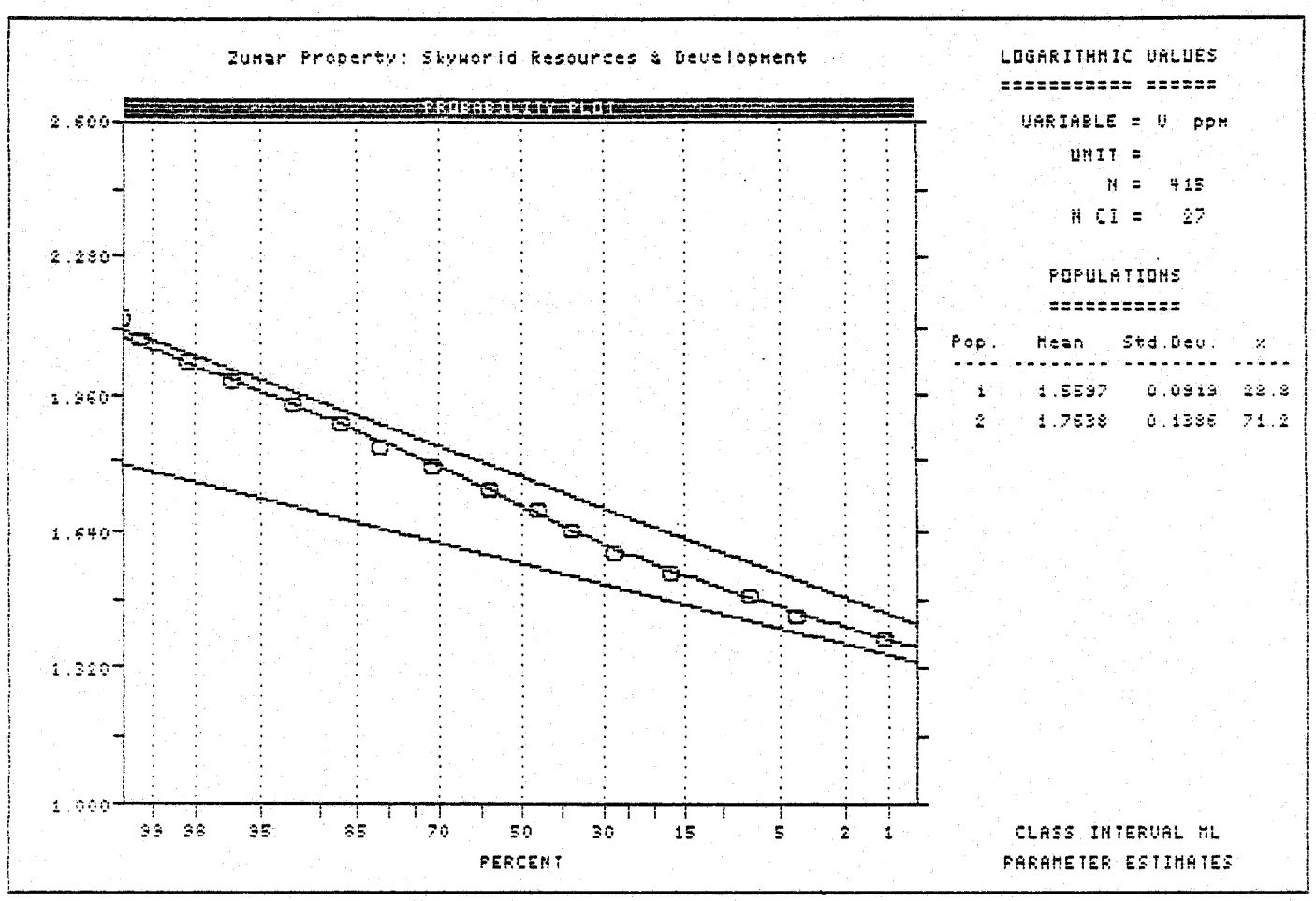
N CI = 27

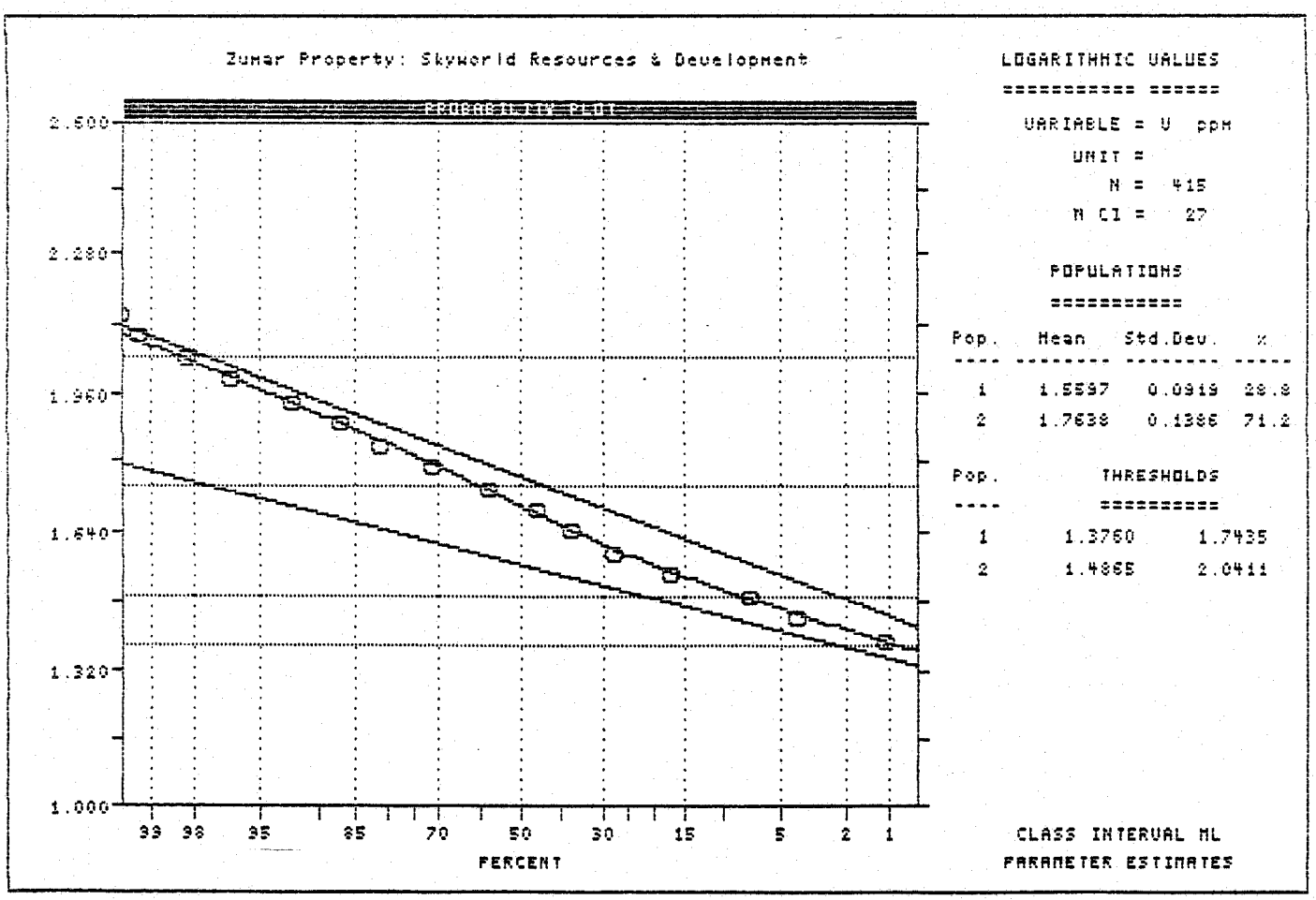
POPULATIONS

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | 23.195 | 11.669 | 92.5 |
| 2 | 64.810 | 6.524 | 4.7 |
| 3 | 155.000 | 40.000 | 2.8 |

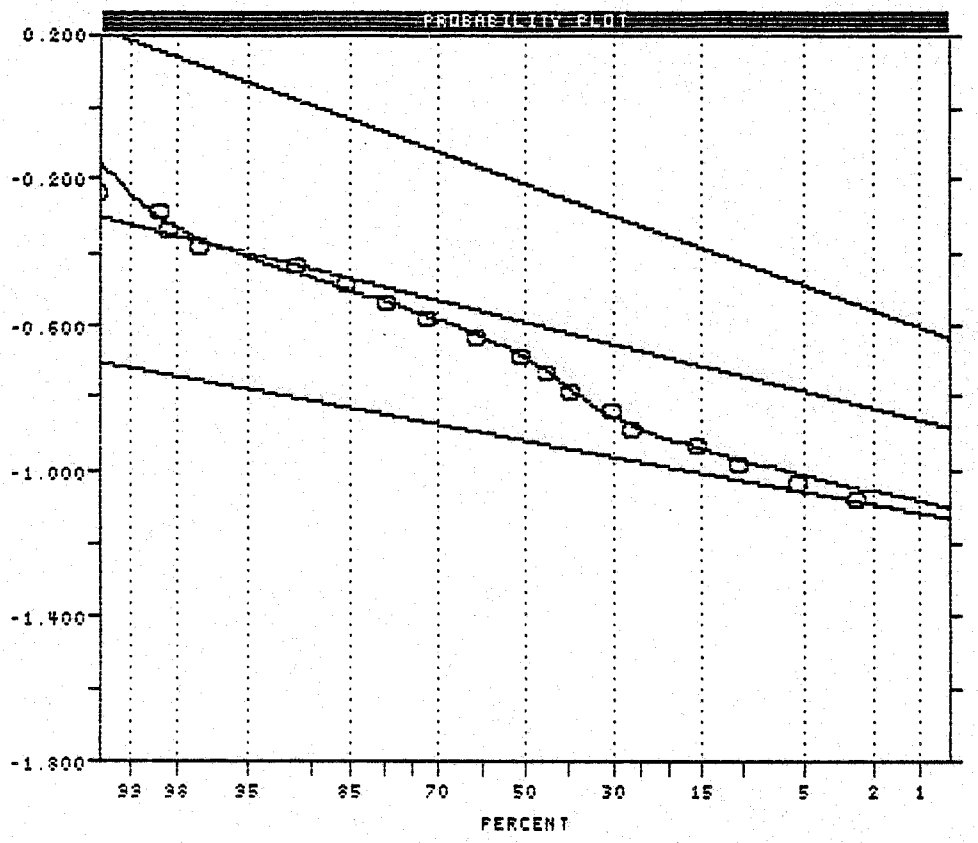
| Pop. | THRESHOLDS | |
|---|---|---|
| 1 | -0.142 | 46.533 |
| 2 | 51.769 | 77.857 |
| 3 | 75.000 | 235.000 |

USERS VISUAL PARAMETER ESTIMATES


Zumar Property: Skyworld Resources & Development
PROBABILITY PLOT
2.600
2.280
1.960
1.640
1.320
1.000
99 98 95 85 70 50 30 15 5 2 1
PERCENT
LOGARITHMIC VALUES
VARIABLE = U ppm
UNIT =
N = 415
N CI = 27
POPULATIONS
Pop. Mean Std.Dev. %
1 1.5597 0.0919 28.8
2 1.7638 0.1386 71.2
CLASS INTERVAL ML
PARAMETER ESTIMATES


Zumar Property: Skyworld Resources & Development
PROBABILITY PLOT
2.600
2.280
1.960
1.640
1.320
1.000
99 98 95 85 70 50 30 15 5 2 1
PERCENT
LOGARITHMIC VALUES
VARIABLE = U ppm
UNIT =
N = 415
N CI = 27
POPULATIONS
Pop. Mean Std.Dev. %
1 1.5597 0.0919 28.8
2 1.7638 0.1386 71.2
Pop. THRESHOLDS
1 1.3760 1.7435
2 1.4865 2.0411
CLASS INTERVAL ML
PARAMETER ESTIMATES

Zumar Property: Skyworld Resources & Development




LOGARITHMIC VALUES

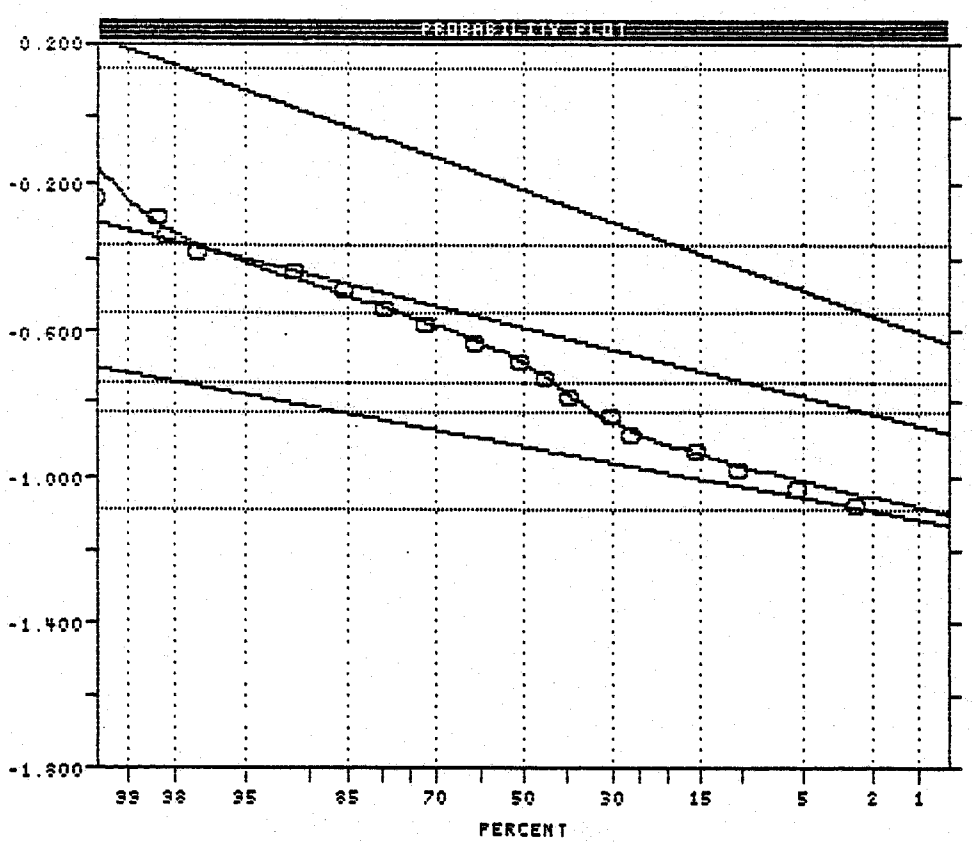
UARIABLE = K %
UNIT =
N = 415
N CI = 27

POPULATIONS

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | -0.9204 | 0.0864 | 37.0 |
| 2 | -0.5959 | 0.1152 | 61.3 |
| 3 | -0.2135 | 0.1704 | 1.7 |

USERS VISUAL
PARAMETER ESTIMATES

Zumar Property: Skyworld Resources & Development




LOGARITHMIC VALUES

UARIABLE = K %
UNIT =
N = 415
N CI = 27

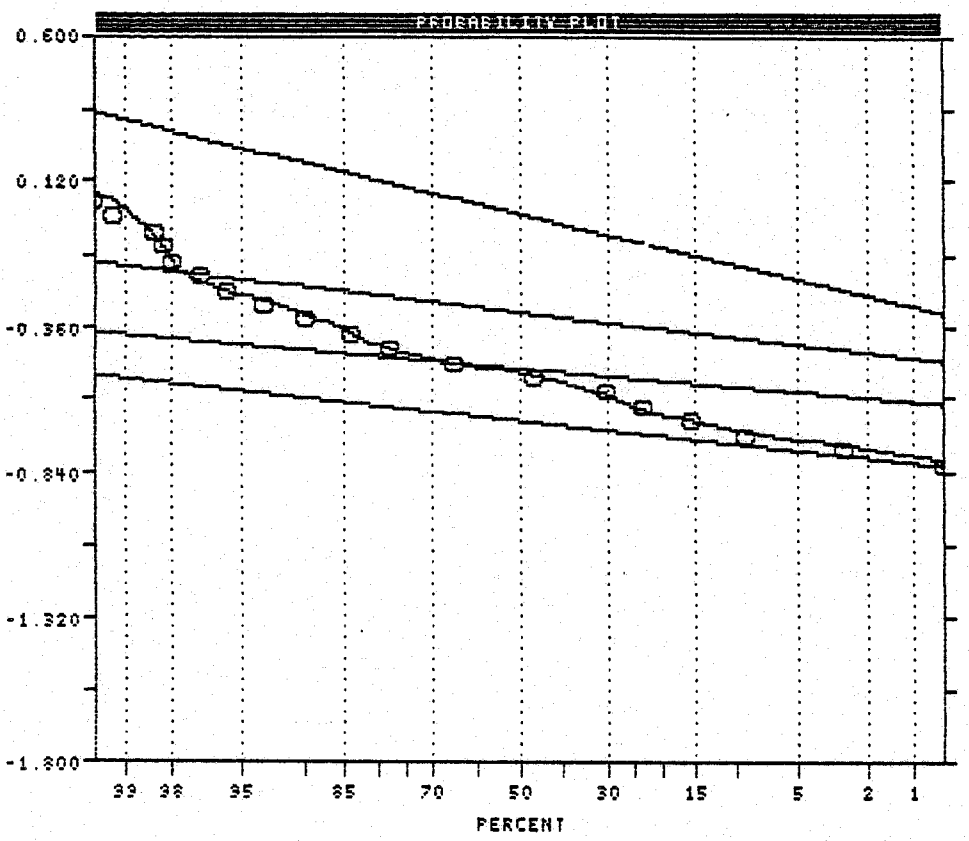
POPULATIONS

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | -0.9204 | 0.0864 | 37.0 |
| 2 | -0.5959 | 0.1152 | 61.3 |
| 3 | -0.2135 | 0.1704 | 1.7 |

| Pop. | THRESHOLDS | |
|---|---|---|
| 1 | -1.0921 | -0.7477 |
| 2 | -0.8269 | -0.3655 |
| 3 | -0.5543 | 0.1273 |

USERS VISUAL
PARAMETER ESTIMATES

Zumar Property: Skyworld Resources & Development




LOGARITHMIC VALUES

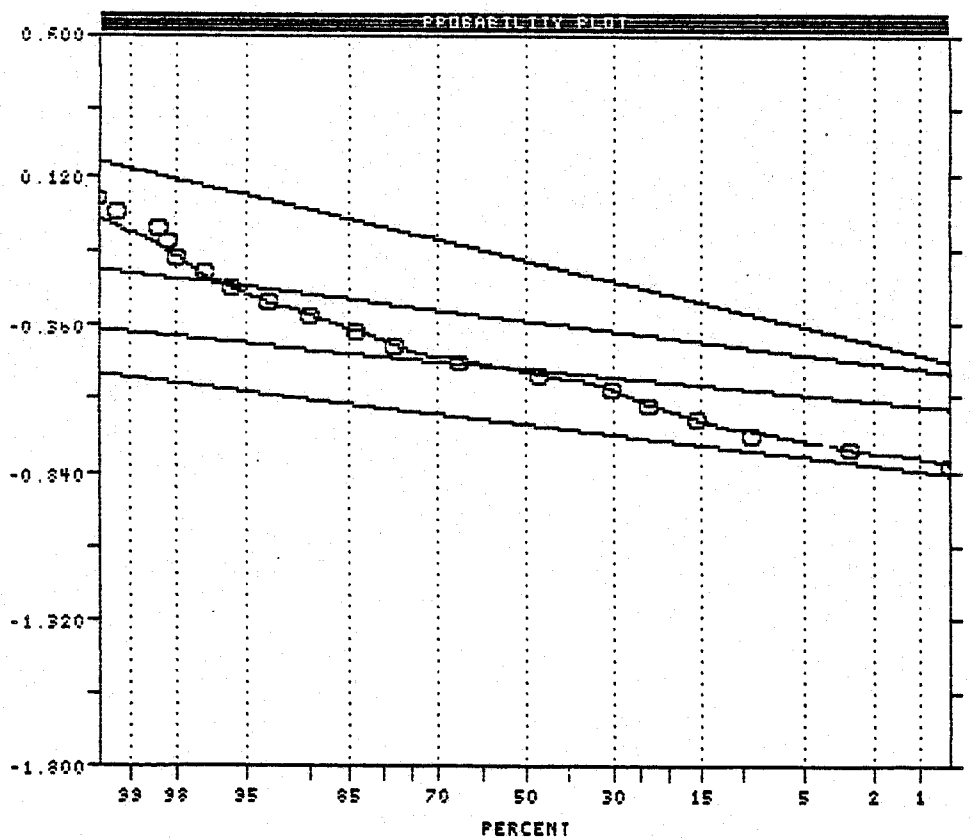
VARIABLE = Ca %
UNIT =
N = 415
N CI = 27

POPULATIONS

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | -0.6769 | 0.0613 | 30.0 |
| 2 | -0.5025 | 0.0495 | 52.0 |
| 3 | -0.3167 | 0.0646 | 15.7 |
| 4 | 0.0090 | 0.1300 | 2.3 |

USERS VISUAL
PARAMETER ESTIMATES

Zumar Property: Skyworld Resources & Development



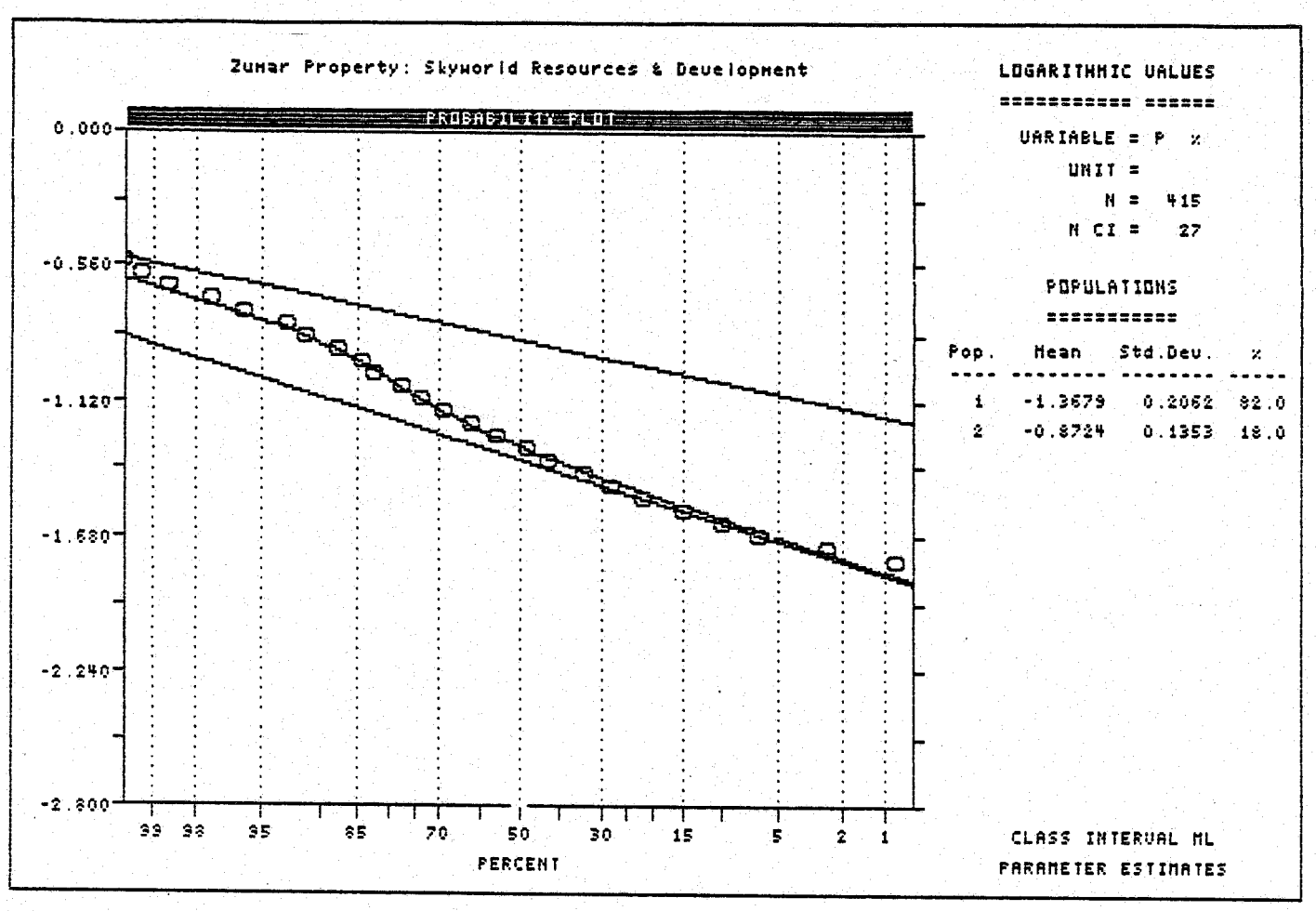

LOGARITHMIC VALUES

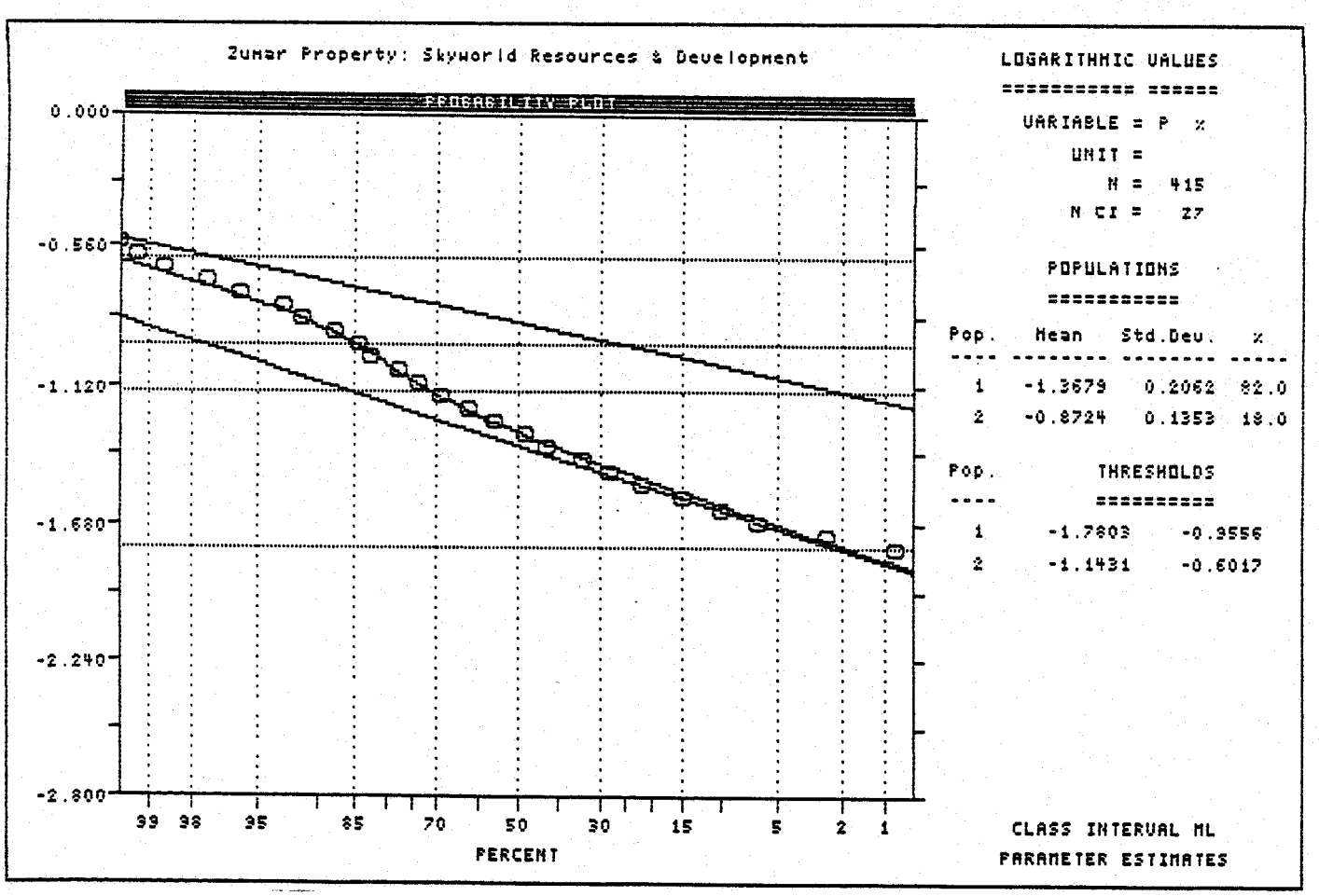
VARIABLE = Ca %
UNIT =
N = 415
N CI = 27

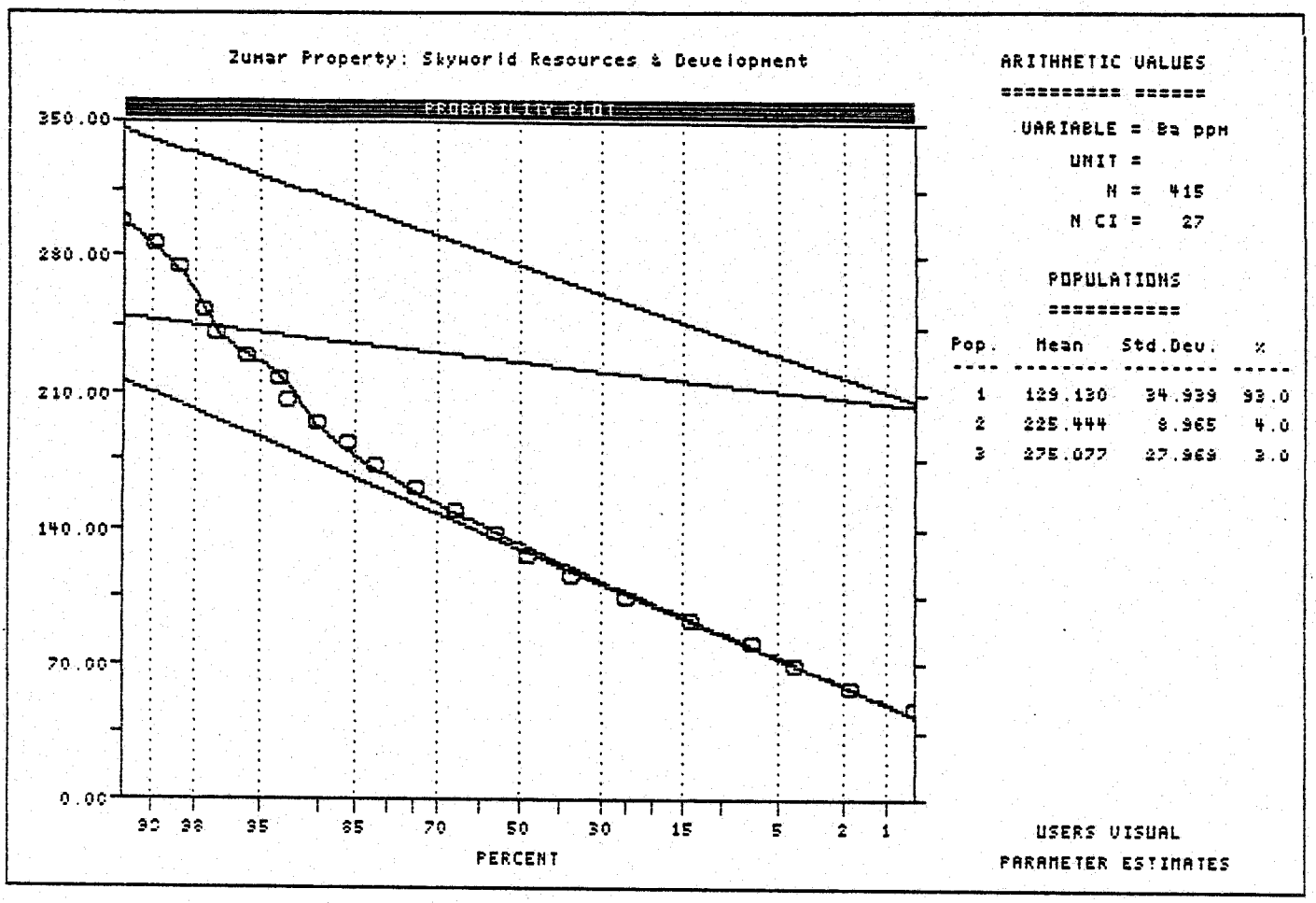
POPULATIONS

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | -0.6856 | 0.0654 | 26.3 |
| 2 | -0.5092 | 0.0510 | 52.1 |
| 3 | -0.3551 | 0.0664 | 17.1 |
| 4 | -0.1569 | 0.1314 | 4.5 |

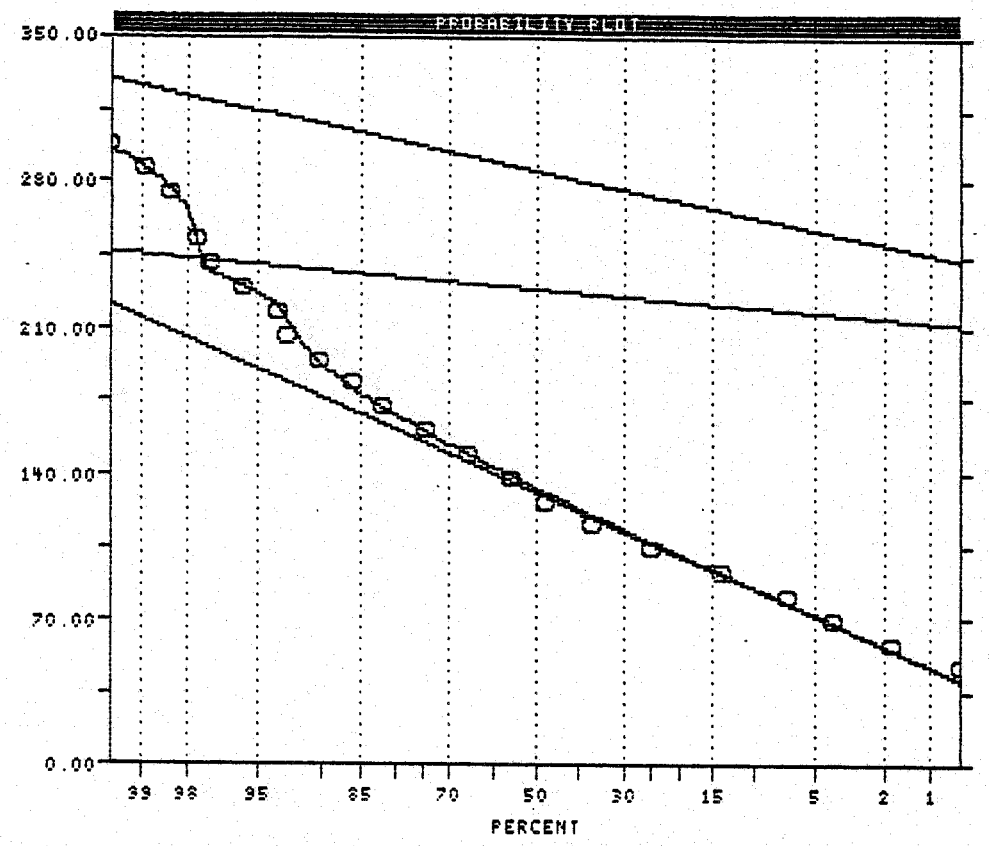
CLASS INTERVAL ML
PARAMETER ESTIMATES


Zumar Property: Skyworld Resources & Development
PROBABILITY PLOT
0.000
-0.560
-1.120
-1.680
-2.240
-2.800
99 98 95 85 70 50 30 15 5 2 1
PERCENT
LOGARITHMIC VALUES
VARIABLE = P %
UNIT =
N = 415
N CI = 27
POPULATIONS
Pop. Mean Std.Dev. %
1 -1.3679 0.2062 82.0
2 -0.8724 0.1353 18.0
CLASS INTERVAL ML
PARAMETER ESTIMATES


Zumar Property: Skyworld Resources & Development
PROBABILITY PLOT
0.000
-0.560
-1.120
-1.680
-2.240
-2.800
99 98 95 85 70 50 30 15 5 2 1
PERCENT
LOGARITHMIC VALUES
VARIABLE = P %
UNIT =
N = 415
N CI = 27
POPULATIONS
Pop. Mean Std.Dev. %
1 -1.3679 0.2062 82.0
2 -0.8724 0.1353 18.0
Pop. THRESHOLDS
1 -1.7803 -0.9556
2 -1.1431 -0.6017
CLASS INTERVAL ML
PARAMETER ESTIMATES


Zumar Property: Skyworld Resources & Deuelopment
PROBABILITY PLOT
350.00
280.00
210.00
140.00
70.00
0.00
90 98 95 85 70 50 30 15 5 2 1
PERCENT
ARITHMETIC VALUES
VARIABLE = Ba ppm
UNIT =
N = 415
N CI = 27
POPULATIONS
Pop. Mean Std.Dev. %
1 129.130 34.939 93.0
2 225.444 8.965 4.0
3 275.077 27.969 3.0
USERS VISUAL
PARAMETER ESTIMATES

Zunar Property: Skyworld Resources & Development




ARITHMETIC VALUES
========== ======

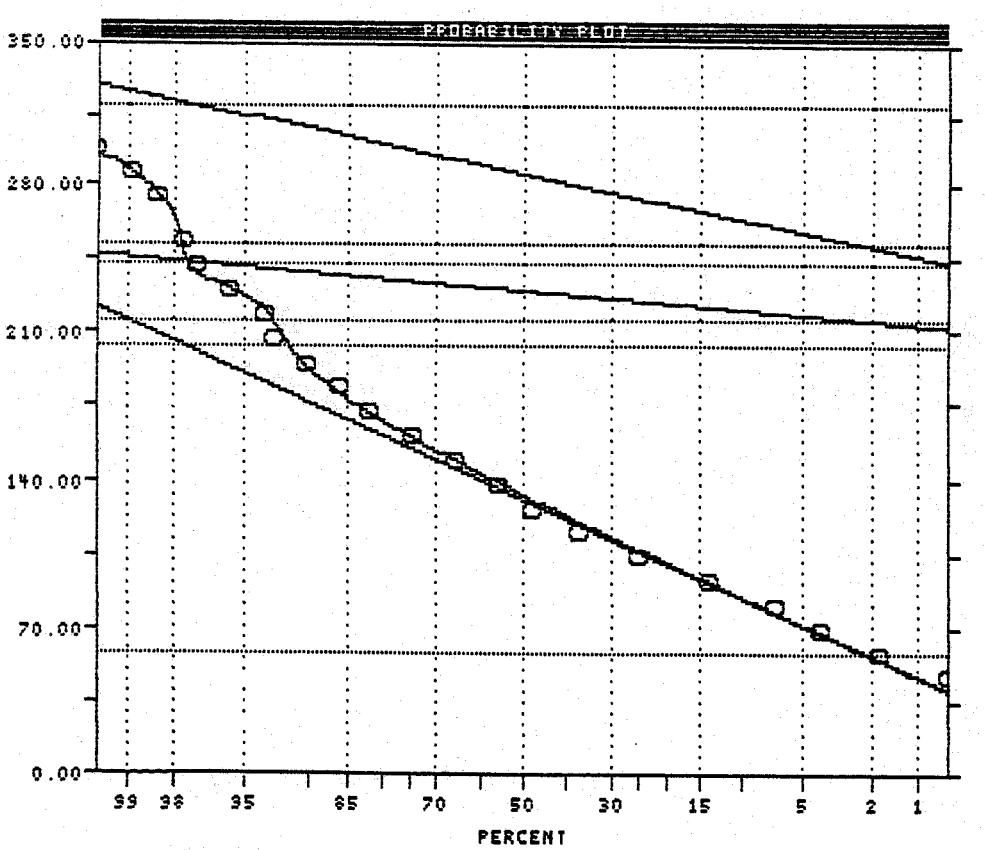
VARIABLE = Ba ppm
UNIT =
N = 415
N CI = 27

POPULATIONS
===========

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | 130.166 | 36.434 | 93.7 |
| 2 | 228.000 | 6.918 | 4.0 |
| 3 | 285.000 | 17.344 | 2.3 |

USERS VISUAL
PARAMETER ESTIMATES

Zunar Property: Skyworld Resources & Development




ARITHMETIC VALUES
========== ======

VARIABLE = Ba ppm
UNIT =
N = 415
N CI = 27

POPULATIONS
===========

| Pop. | Mean | Std.Dev. | % |
|---|---|---|---|
| 1 | 130.124 | 36.476 | 93.7 |
| 2 | 228.000 | 6.920 | 4.0 |
| 3 | 285.000 | 17.340 | 2.3 |

| Pop. | THRESHOLDS | |
|---|---|---|
| | ========== | |
| 1 | 57.171 | 203.077 |
| 2 | 214.160 | 241.840 |
| 3 | 250.320 | 319.680 |

USERS VISUAL
PARAMETER ESTIMATES

Zumar Property: Skyworld Resources Development Lt

##########################################################################

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = Cu ppm  Unit =  N = 415
N CI = 27

Transform = Arithmetic  Number of Populations = 3

# of Missing Observations = 0.

==========

Users Visual Parameter Estimates

| Population | Mean | Std Dev | Percentage |
|---|---|---|---|
| 1 | 23.195 | 11.669 | 92.50 |
| 2 | 64.810 | 6.524 | 4.70 |
| 3 | 155.000 | 40.000 | 2.80 |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | -0.142 | 46.533 |
| 2 | 51.762 | 77.857 |
| 3 | 75.000 | 235.000 |

##########################################################################

Zumar Property: Skyworld Resources & Development

##########################################################################

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = V ppm  Unit =  N = 415
N CI = 27

Transform = Logarithmic  Number of Populations = 2

# of Missing Observations = 0.

==========

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1062.263

Parameterized Degrees of Freedom = 3

| Population | Mean | | Std Dev | Percentage |
|---|---|---|---|---|
| 1 | 36.285 | - | 29.368 | 28.77 |
| | | + | 44.833 | |
| 2 | 58.050 | - | 42.185 | 71.23 |
| | | + | 79.880 | |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | 23.769 | 55.393 |
| 2 | 30.656 | 109.920 |

##########################################################################

Zumar Property: Skyworld Resources & Development

##########################################################################

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = K %  Unit =  N = 415
N CI = 27

Transform = Logarithmic  Number of Populations = 3

# of Missing Observations = 0.

==========

Users Visual Parameter Estimates

| Population | Mean | | Std Dev | Percentage |
|---|---|---|---|---|
| 1 | 0.120 | - | 0.098 | 37.00 |
| | | + | 0.147 | |
| 2 | 0.254 | - | 0.194 | 61.25 |
| | | + | 0.331 | |
| 3 | 0.612 | - | 0.413 | 1.75 |
| | | + | 0.906 | |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | 0.081 | 0.179 |
| 2 | 0.149 | 0.431 |
| 3 | 0.279 | 1.341 |

##########################################################################

Zumar Property: Skyworld Resources & Development

##########################################################################

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = Ca %  Unit =  N = 415
N CI = 27

Transform = Logarithmic  Number of Populations = 4

# of Missing Observations = 0.

==========

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1023.816

Parameterized Degrees of Freedom = 7

| Population | Mean | | Std Dev | Percentage |
|---|---|---|---|---|
| 1 | 0.206 | - | 0.177 | 26.35 |
| | | + | 0.240 | |
| 2 | 0.310 | - | 0.275 | 52.09 |
| | | + | 0.348 | |
| 3 | 0.442 | - | 0.379 | 17.10 |
| | | + | 0.514 | |
| 4 | 0.697 | - | 0.515 | 4.46 |
| | | + | 0.943 | |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | 0.153 | 0.279 |
| 2 | 0.245 | 0.392 |
| 3 | 0.325 | 0.600 |
| 4 | 0.381 | 1.276 |

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Zumar Property: Skyworld Resources & Development

##########################################################################

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = P %  Unit =  N = 415
N CI = 27

Transform = Logarithmic  Number of Populations = 2

# of Missing Observations = 0.

==========

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1263.040

Parameterized Degrees of Freedom = 3

| Population | Mean | | Std Dev | Percentage |
|---|---|---|---|---|
| 1 | 0.043 | - | 0.027 | 82.01 |
| | | + | 0.069 | |
| 2 | 0.134 | - | 0.098 | 17.99 |
| | | + | 0.183 | |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | 0.017 | 0.111 |
| 2 | 0.072 | 0.250 |

##########################################################################

Zumar Property: Skyworld Resources & Development

##########################################################################

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = Ba ppm  Unit =  N = 415
N CI = 27

Transform = Arithmetic  Number of Populations = 3

# of Missing Observations = 0.

==========

Users Visual Parameter Estimates

| Population | Mean | Std Dev | Percentage |
|---|---|---|---|
| 1 | 130.124 | 36.476 | 93.70 |
| 2 | 228.000 | 6.920 | 4.00 |
| 3 | 285.000 | 17.340 | 2.30 |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | 57.171 | 203.077 |
| 2 | 214.160 | 241.840 |
| 3 | 250.320 | 319.680 |

##########################################################################

Zumar Property: Skyworld Resources & Development

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PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = Ni ppm  Unit =  N = 415
N CI = 27

Transform = Arithmetic  Number of Populations = 3

# of Missing Observations = 0.

==========

Incomplete Iteration Parameter Estimates

| Population | Mean | Std Dev | Percentage |
|---|---|---|---|
| 1 | 13.842 | 3.773 | 93.00 |
| 2 | 23.225 | 0.722 | 3.84 |
| 3 | 27.546 | 1.939 | 3.16 |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | 6.295 | 21.389 |
| 2 | 21.781 | 24.670 |
| 3 | 23.667 | 31.424 |

##########################################################################

Zumar Property: Skyworld Resources & Development

##########################################################################

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = LA6289.PPT

Variable = Mn ppm  Unit =  N = 411
N CI = 27

Transform = Arithmetic  Number of Populations = 2

# of Missing Observations = 0.

0 Observations Were Below the Minimum Value of 0.0001
4 Observations Were Above the Maximum Value of 1450.0000

Lower Truncation Correction of 5 percent.

==========

Users Visual Parameter Estimates

| Population | Mean | Std Dev | Percentage |
|---|---|---|---|
| 1 | 430.000 | 176.000 | 93.00 |
| 2 | 1078.233 | 124.550 | 7.00 |

==========

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds | |
|---|---|---|
| 1 | 78.000 | 782.000 |
| 2 | 829.134 | 1327.333 |

##########################################################################

1000 W | 800 W | 600 W | 400 W | 200 W | BASE LINE | 200 E | 400 E | 600 E | 800 E | 1000 E

1200 N

1000 N

800 N

600 N

500 N

400 N

300 N

200 N

100 N

0

1000 W | 800 W | 600 W | 400 W | 200 W | BASE LINE | 200 E | 400 E | 600 E | 800 E | 1000 E

## LEGEND

PROFILES POSITIVE UP & TO LEFT
PROFILE SCALE : 1 CM = 400 NT (GAMMAS)
BASE VALUE : 57500 NT
RANGE - HIGH : 62456 NT
- MEDIAN : 59390 NT
- LOW : 56323 NT
ALL READINGS LOOP CORRECTED

400 NT
0

ROAD - - - - - - - - -
CREEK

INSTRUMENTATION :
BARRINGER RESEARCH LTD.
MODEL GM 122
PROTON PRECESSION MAGNETOMETER

MAGNETIC NORTH

S.J.V. CONSULTANTS LTD.



SKYWORLD RESOURCES & DEVELOPMENTS LTD.

# ZUMAR PROPERTY

VERNON MINING DISTRICT, BRITISH COLUMBIA

N.T.S. : 82 L/4E

## MAGNETICS SURVEY

## PROFILES

SCALE : 1:2500

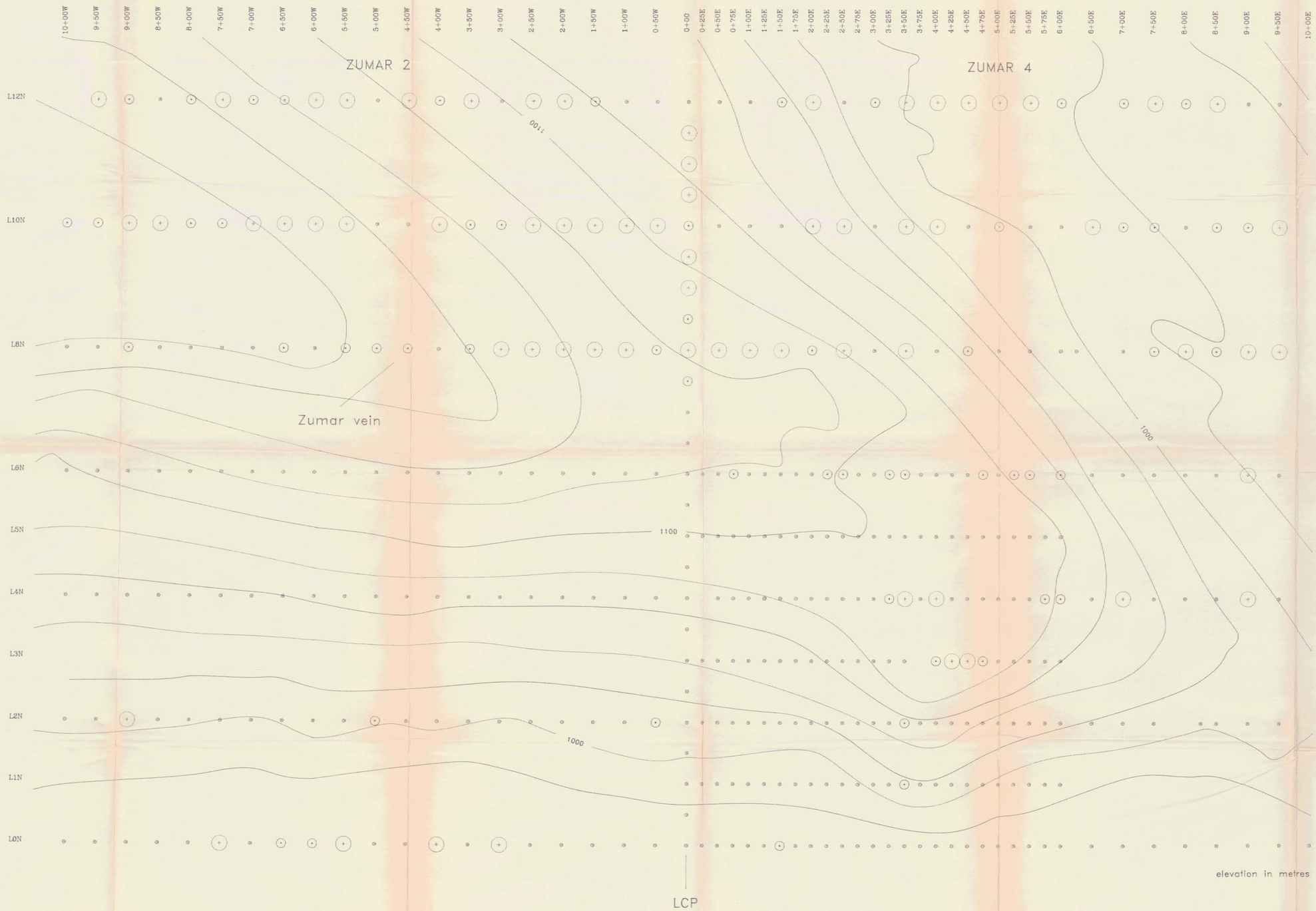
100 0 100 200 300



JANUARY, 1989

PLATE : GM 1

Fig. 10






metres 50 0 50 100 150 200

Skyworld Resources and Development

# Zumar Property

Soil Geochemistry – P
small circles: .072 – .111 % P
large circles: >.111 % P

| | | | |
|---|---|---|---|
| scale 2500 | | NTS | fig No 9 |
| dwn by | | date | |
| chkd by | | project | file No |

Not approved - must show values

10+00W 9+50W 9+00W 8+50W 8+00W 7+50W 7+00W 6+50W 6+00W 5+50W 5+00W 4+50W 4+00W 3+50W 3+00W 2+50W 2+00W 1+50W 1+00W 0+50W 0+00 0+25E 0+50E 0+75E 1+00E 1+25E 1+50E 1+75E 2+00E 2+25E 2+50E 2+75E 3+00E 3+25E 3+50E 3+75E 4+00E 4+25E 4+50E 4+75E 5+00E 5+25E 5+50E 5+75E 6+00E 6+50E 7+00E 7+50E 8+00E 8+50E 9+00E 9+50E 10+00E

ZUMAR 2

ZUMAR 4

L12N

L10N

L8N

L6N

L5N

L4N

L3N

L2N

L1N

L0N

1100

1000

Zumar vein

elevation in metres

LCP

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,713

50 0 50 100 150 200 metres

Skyworld Resources and Development

# Zumar Property

Soil Geochemistry - K
sm: .15 - .28 %K med: .28 - .43 %K
large circles: >.43 %K

| | | | |
|---|---|---|---|
| scale 2500 | NTS | | fig No 7 |
| dwn by | date | | |
| chkd by | project | | file No |

Not approved - would move values

1000 W | 800 W | 600 W | 400 W | 200 W | BASE LINE | 200 E | 400 E | 600 E | 800 E | 1000 E

1200 N
1000 N
800 N
600 N
500 N
400 N
300 N
200 N
100 N
0

1000 W | 800 W | 600 W | 400 W | 200 W | BASE LINE | 200 E | 400 E | 600 E | 800 E | 1000 E

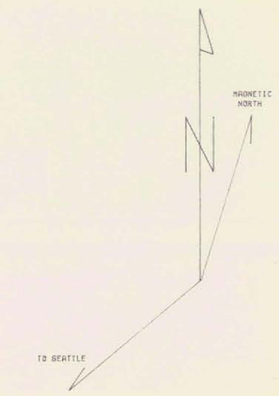
## LEGEND

PROFILES POSITIVE UP
DIP ANGLE - SOLID LINE
  PROFILE SCALE : 1 CM = 5 %
  BASE VALUE : 0 %
FIELD STRENGTH : DASHED LINE
  PROFILE SCALE : 1 CM = 5 %
  BASE VALUE : 40 %
ALL READINGS FACING APPROXIMATELY WSW

ROAD - - - - - - - - -
CREEK

INSTRUMENTATION :
  SABRE ELECTRONICS LTD.
  MODEL 27 VLF RECEIVER
TRANSMITTER :
  JIM CREEK, WASHINGTON (SEATTLE)
  NLK - 24.8 KHZ

S.J.V. CONSULTANTS LTD.






SKYWORLD RESOURCES & DEVELOPMENTS LTD.

ZUMAR PROPERTY

VERNON MINING DISTRICT, BRITISH COLUMBIA

N.T.S. : 82 L/4E

VLF EM SURVEY - NLK

DIP ANGLE / FIELD STRENGTH PROFILES

SCALE : 1:2500

100 0 100 200 300

JANUARY, 1989 PLATE : GV 1



Fig. 11

10+00W 9+50W 9+00W 8+50W 8+00W 7+50W 7+00W 6+50W 6+00W 5+50W 5+00W 4+50W 4+00W 3+50W 3+00W 2+50W 2+00W 1+50W 1+00W 0+50W 0+00 0+25E 0+50E 0+75E 1+00E 1+25E 1+50E 1+75E 2+00E 2+25E 2+50E 2+75E 3+00E 3+25E 3+50E 3+75E 4+00E 4+25E 4+50E 4+75E 5+00E 5+25E 5+50E 5+75E 6+00E 6+50E 7+00E 7+50E 8+00E 8+50E 9+00E 9+50E 10+00E

ZUMAR 2

ZUMAR 4

L12N

L10N

L8N

L6N

L5N

L4N

L3N

L2N

L1N

L0N

1100

1000

Zumar vein

1100

1000

LCP

elevation in metres



N



50 0 50 100 150 200 metres

Skyworld Resources and Development

# Zumar Property

Soil Geochemistry – Ca
sm: .25 – .38 %Ca med: .38 – .60 %Ca
large circles: >.60 %Ca

| | | | |
|---|---|---|---|
| scale 2500 | | NTS | fig No 8 |
| dwn by | | date | |
| chkd by | | project | file No |

Ref. approved annual show volume

10+00W 9+50W 9+00W 8+50W 8+00W 7+50W 7+00W 6+50W 6+00W 5+50W 5+00W 4+50W 4+00W 3+50W 3+00W 2+50W 2+00W 1+50W 1+00W 0+50W 0+00 0+25E 0+50E 0+75E 1+00E 1+25E 1+50E 1+75E 2+00E 2+25E 2+50E 2+75E 3+00E 3+25E 3+50E 3+75E 4+00E 4+25E 4+50E 4+75E 5+00E 5+25E 5+50E 5+75E 6+00E 6+50E 7+00E 7+50E 8+00E 8+50E 9+00E 9+50E 10+00E

ZUMAR 2

ZUMAR 4

L12N

L10N

L8N

L6N

L5N

L4N

L3N

L2N

L1N

L0N

1100

1000

Zumar vein

LCP

elevation in metres

GEOLOGICAL ASSOCIATION OF CANADA · DOUGLAS H. WOOD · FELLOW

N

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,713

50 0 50 100 150 200 metres

Skyworld Resources and Development

# Zumar Property

Soil Geochemistry – V

sm: <55 ppm V med: 55 – 110 ppm V

large circles: >110 ppm V

| | | | |
|---|---|---|---|
| | scale 2500 | NTS | fig No 6 |
| | dwn by | date | |
| | chkd by | project | file No |

Not exposed - would show values

10+00W 9+50W 9+00W 8+50W 8+00W 7+50W 7+00W 6+50W 6+00W 5+50W 5+00W 4+50W 4+00W 3+50W 3+00W 2+50W 2+00W 1+50W 1+00W 0+50W 0+00 0+25E 0+50E 0+75E 1+00E 1+25E 1+50E 1+75E 2+00E 2+25E 2+50E 2+75E 3+00E 3+25E 3+50E 3+75E 4+00E 4+25E 4+50E 4+75E 5+00E 5+25E 5+50E 5+75E 6+00E 6+50E 7+00E 7+50E 8+00E 8+50E 9+00E 9+50E 10+00E

ZUMAR 2

ZUMAR 4

L12N

L10N

L8N

L6N

L5N

L4N

L3N

L2N

L1N

L0N

1100

1000

Zumar vein

elevation in metres

LCP

GEOLOGICAL ASSOCIATION OF CANADA · DOUGLAS H. WOOD · FELLOW

N

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,713

metres
50 0 50 100 150 200

Skyworld Resources and Development

# Zumar Property

Soil Geochemistry – Au
small circles: 12 – 20 ppb Au
large circles: >20 ppb Au

| | | | |
|---|---|---|---|
| | scale 2500 | NTS | fig No 4 |
| | dwn by | date | |
| | chkd by | project | file No |

Not approved - Must show values

T.L.K.

10+00W 9+50W 9+00W 8+50W 8+00W 7+50W 7+00W 6+50W 6+00W 5+50W 5+00W 4+50W 4+00W 3+50W 3+00W 2+50W 2+00W 1+50W 1+00W 0+50W 0+00 0+25E 0+50E 0+75E 1+00E 1+25E 1+50E 1+75E 2+00E 2+25E 2+50E 2+75E 3+00E 3+25E 3+50E 3+75E 4+00E 4+25E 4+50E 4+75E 5+00E 5+25E 5+50E 5+75E 6+00E 6+50E 7+00E 7+50E 8+00E 8+50E 9+00E 9+50E 10+00E

ZUMAR 2

ZUMAR 4

L12N

L10N

L8N

L6N

L5N

L4N

L3N

L2N

L1N

L0N

1100

1000

1100

1000

Zumar vein

LCP

elevation in metres

GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,713

50 0 50 100 150 200 metres

Skyworld Resources and Development

Zumar Property

Soil Geochemistry – Cu
small circles: 50 – 76 ppm Cu
large circles: >76 ppm Cu

| | | |
|---|---|---|
| scale 2500 | NTS | fig No 5 |
| dwn by | date | |
| chkd by | project | file No |

Not approved – amount shows values T.K.