GEOPHYSICAL REPORT

on the

GENESIS CLAIM GROUP

Kamloops Mining Division

NTS 92-I/11 and 92-I/14
Latitude 50°49'24" N - Longitude 121°24'30" W
Property Centre

Owner/Operator
TROVE RESOURCES LTD.
505 - 850 Burrard Street
Vancouver, B.C.
V6Z 2J1

Report Prepared By
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May 1989

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INTRODUCTION

The Genesis property is located approximately 200 km northeast of Vancouver near the town of Cache Creek in south-central British Columbia.

The property covers rocks belonging to the Nicola Group. These rocks have the potential to host massive sulphide deposits of volcanogenic origin.

The exploration program carried out on the property in 1988 was conducted in two phases. In May 1988, a soil geochemical survey was carried out over the conductive zone delineated as a result of the Genie-EM survey done in the spring of 1987. The grid was subsequently extended to the south and northwest, and magnetometer, VLF-EM and moving source Genie EM surveys were conducted in order to extend the aforementioned Genie-EM trend.

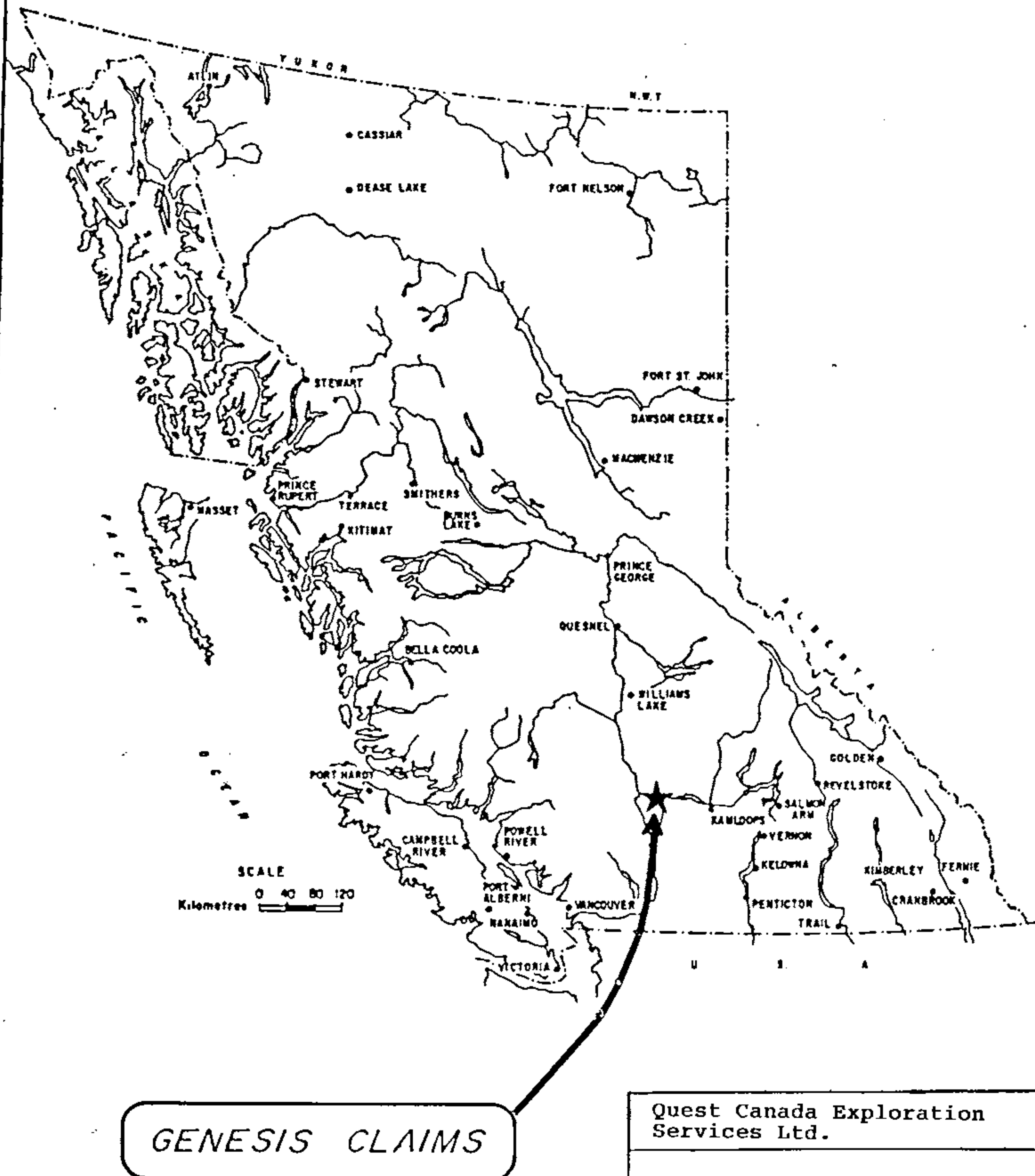
SUMMARY

The Genesis Group is comprised of six claim blocks totalling 73 units.

The property is centered 6 km west-northwest of the town of Cache Creek and extends 3 km north and 3 km south.

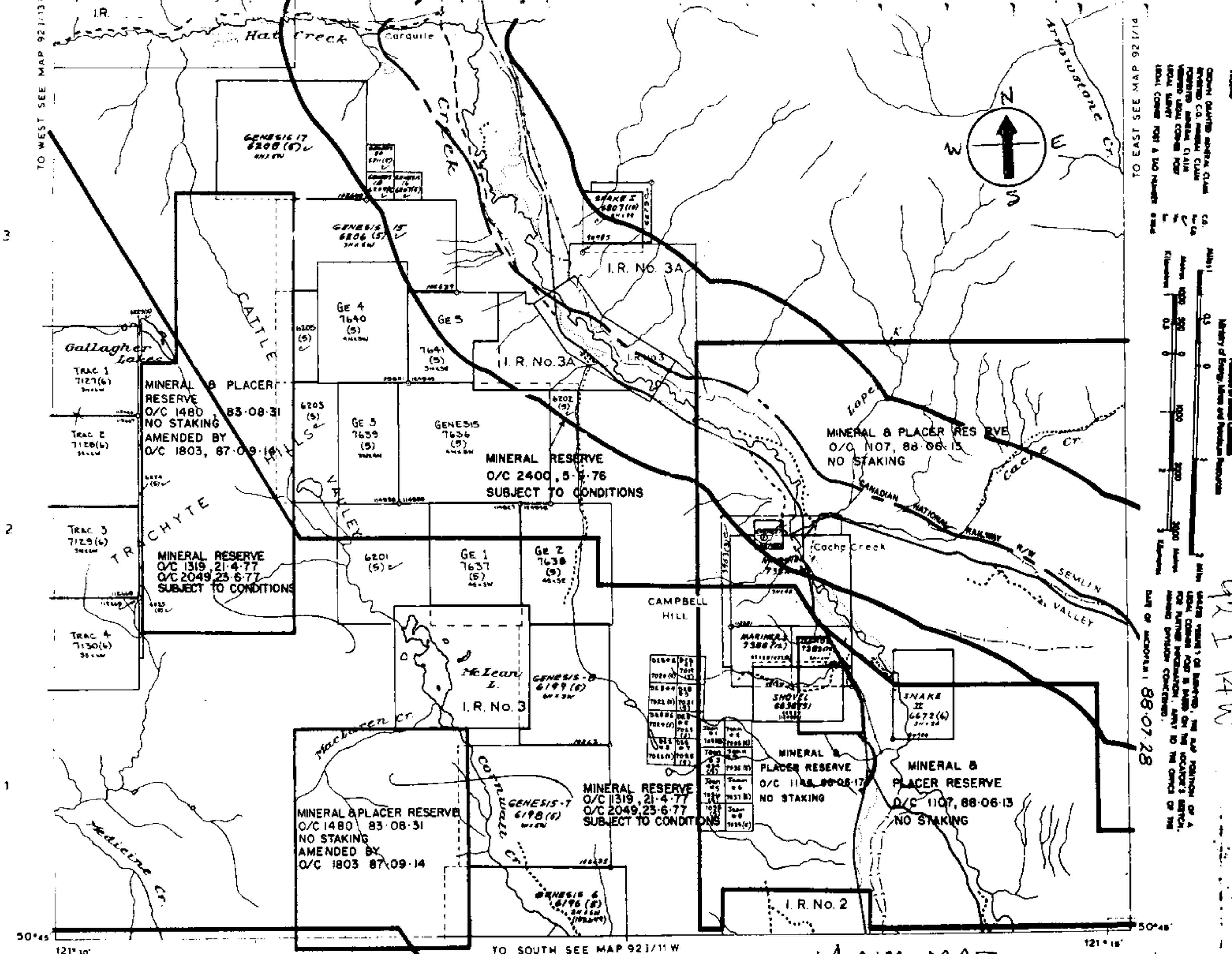
Access to the claims is via a 2 wheel drive road off Highway 97 approximately 5 km north of Cache Creek.

The Genesis property is underlain by a long, relatively narrow, north-northwesterly trending belt of submarine volcanics and



Quest Canada Exploration Services Ltd.
GENESIS CLAIMS
LOCATION MAP
KILOMETERS 0 100 200 300
TROVE RESOURCES LTD.
SCALE: 1:8,000,000 DATE: May 85

Figure 1



CLAIM MAP

DEPARTMENT OF MINES AND PETROLEUM RESOURCES sediments belonging to the Nicola Group. Rock types include basic to acidic volcaniclastics and flows with intercalated argillic sediments.

The geophysical exploration program described in this report was primarily conducted to extend the known Genie-EM trend that runs diagonally across the length of the grid in the Genesis claim block. A soil geochemical survey was also conducted over this trend. Geophysical plans were prepared at a scale of 1:10,000 for the various surveys.

PROPERTY AND OWNERSHIP

The Genesis property consists of 6 contiguous mineral claims containing 73 units. Claim data is as follows:

Claim Name	Record #	Units	Recording Date
Genesis	7636	20	May 12, 1988
GE 1	7637	12	May 12, 1988
GE 2	7638	12	May 12, 1988
GE 3	7639	8	May 12, 1988
GE 4	7640	12	May 12, 1988
GE 5	7641	9	May 12, 1988

The claims are owned and operated by Trove Resources Ltd. of 505 - 850 Burrard Street, Vancouver, B.C.

LOCATION AND ACCESS

The property centre lies approximately 6 km west-northwest of Cache Creek at 50°49' north latitude and 121°24' west longitude. The southern boundary is just east of the northern end of McLean Lake, with the property extending for about 6 km in a north-northwesterly direction.

Access to the property is by way of a gravel 2 wheel drive range road leaving Highway 97 approximately 5 km north of Cache Creek at the Bonaparte Indian Reserve.

PHYSIOGRAPHY AND VEGETATION

Relief is gentle to moderate with elevations ranging from 1500 to 4500 feet above sea level.

The climate is semi-arid with annual rainfall ranging from 28 to 36 centimeters. Temperatures vary from up to 40°C in summer to as low as -35°C in winter.

The vegetation consists of grasslands, sage brush and cactus at lower elevations, with increasing amounts of pine and fir at higher elevations.

Rock outcrop is limited to slopes and valleys.

REGIONAL GEOLOGY

The Genesis claims lie within a north-northwest trending belt of Triassic volcanic and sedimentary rocks belonging to the Nicola Group. Rock types include basic to acidic volcaniclastics and flows with intercalated argillic sediments and their metamorphic equivalents. The belt is bounded on the east unconformably by sediments of the Ashcroft Formation, which consists of argillite, siltstone, sandstone and conglomerate. A fault contact with the Permian Cache Creek Complex and with unnamed Cretaceous sediments forms the western boundary of the belt. The Cretaceous sediments consist of conglomerate, sandstone and minor shale with coal horizons. The Cache Creek Complex consists of basalt, pillow basalt, diabase and gabbro intrusions, massive carbonate with argillite and tuffaceous interbeds (the Marble Canyon Formation), and local basalt and chert sequences with small bodies of ultramafic rock.

REGIONAL EXPLORATION HISTORY

The first major survey of the Ashcroft area was made by S. Duffell and K.C. McTaggart as shown in the G.S.C. Memoir No. 262 (1952).

Several studies, (Ladd 1977, 1979 and Travers 1978) were conducted in the late seventies. The second major publication was compiled by J.W.H. Monger, G.S.C. 1980-82, and W.S. McMillan, B.C.M.M.P.R. 1969-75 and 1977-80. The results of this work are presented in the G.S.C. Open File 980.

The area was subject to exploration activity in the 1960's and early 1970's by major mining companies and Vancouver juniors. Exploration targets were porphyry copper deposits.

Most of the recent work has been south of Cache Creek near Red Hill. Noranda Exploration Co., Bethlehem Copper Corp. and Guichon Explorco Limited are some of the companies who have worked on the gossan zones at Red Hill. Recent studies by D. Gamble (1980-81) have recognized the potential for volcanogenic stratabound sulphide deposits within the Nicola Group near Red Hill. The Selco Division of B.P. Canada Limited is now actively exploring this area.

Geochemical and geophysical work has been conducted on the ground west of Cache Creek by Vancouver juniors in the early seventies. Results reported included gold, copper, zinc and lead anomalies (Assessment Reports 3153, 4068 and 9177).

PROPERTY EXPLORATION HISTORY

The area covered by the Genesis property received very little exploration prior to 1986. There are two government assessment reports documenting exploration programs conducted in the early seventies.

Report No. 3153 written by C.A. Lannle, P.Eng. in 1971 describes a soil geochemical survey for Cu, Pb and Zn, and a magnetometer survey conducted on the McLean claim group. Results of this program show a strong zinc anomaly with weak lead association stretching for over 600 m. The cause of this anomaly was never adequately explained.

Report No. 4068 prepared by G.B. Phelps, P.Eng. in 1972 describes a Cu soil geochemical survey conducted on the Ham and Eggs claim group. Results show a moderate copper geochemical anomaly trending north-northeast for approximately 1 km. However, the location map from the assessment report does not provide enough information to adequately correlate this anomaly to known topography in the area. It appears that the anomaly lies in the northern portion of the Genesis Group, within the GE 4 and GE 5 claims.

The Genesis property is the subject of a Prospecting Report prepared by Quest Canada Exploration Services Inc. in July 1986. This report by Ralph Shearing, P.Geol., states that the property is largely underlain by rocks which have the potential of hosting volcanogenic exhalative massive sulphide deposits.

PROPERTY GEOLOGY

Lithology

The claim block appears to be underlain by a bimodal suite of felsic to mafic volcanic flows and pyroclastic deposits. The general lithologic form of the rocks appears to be consistent with other members of the Nicola group. Clastic units form a relatively small proportion, approximately 5-10%, of the total stratigraphic column. In detail:

Andesitic Flows

Medium to dark green fine grained andesitic flows are the dominant mafic volcanic unit. This unit tends to be massive, poorly foliated, and rarely weakly hematitic. Pillow structures were not observed, but a sub-aqueous depositional environment is suspected. Interbedded pyroclastic sequences are infrequently noted.

Quartz Feldspar Porphyritic Flows

Light apple green, weakly sericitized felsic flows are identified throughout the property. Quartz eyes may exceed 0.5 cm and typically occupy 5-10% rock volume. Reliable strike indicators may be obtained from the flow bands frequently noted within this unit. Compositionally the unit ranges from dacitic to rhyodacitic.

Quartz Feldspar Porphyritic Fragmentals

Well defined felsic fragmentals are commonly identified in the north central grid area. Elongate 1.0 x 4.0 cm pale weathering oval fragments are strained at an apparent ratio of 2:1. Feldspars within this unit are generally pale cream and lightly sericitized.

Limestone

Grey to buff, medium grained limestone units are present as narrow, 10-15 m wide, intervolcanic sediments.

Intrusive Lithologies

Granodiorite

A large intrusive stock was found in the south of the claim block. This unit is typically massive, homogeneous, medium grained and unfoliated. Compositionally this rock is placed in a granodiorite field.

Mafic Dykes:

Small mafic dykes, discordant to all lithologies, are noted throughout the map area. Typically these units are less than 3.0 metres in width.

Structure

Bedding in the Genesis Group trends 125 degrees and dips south-westerly at 50 degrees. Bedding attitudes are coplanar with much of the foliation data. Cleavage bedding relations typically suggest the section is upright.

Small scale faults are frequently encountered within the claim area. The strength of shearing within the Nicola volcanics in this region is perhaps their most outstanding feature. Crenulated foliations, intrafolial folds and small scale nappe structures may be localized to some of these structures.

Large scale antiforms or synforms were not identified on the property.

GEOCHEMICAL SURVEY

The soil geochemical survey was conducted between May 13 and 20, 1988. A 50 metre line separation and 25 metre station interval flagged line grid was established over anomaly A on the Genesis claim. This grid covered the area from 9200 E to 8900 E on Line 10400 N to 8400 E to 7900 E on Line 11500 N of the grid established in the spring of 1987. In all, a total of about 12 km of grid was established and approximately 500 "B" horizon soil samples were collected. All soil samples were placed in kraft paper envelopes, field dried and delivered to Acme Analytical Laboratories in Vancouver, British Columbia. There, the samples were dried at 60°C, sieved to minus 80 mesh and were analyzed for 30 elements by inductively coupled argon plasma (ICP) and for gold by atomic absorption (AA). The certificate of analysis for the soil samples accompanies this report as Appendix I.

GEOPHYSICAL SURVEYS

The geophysical surveys were carried out in November and December 1988. A total of 43.85 km of grid was established and 38.35 km of magnetometer/2 station VLF-EM surveying and 39.20 km of moving source Genie-EM surveying were conducted during the program.

The VLF stations used for the survey were Cutler, Maine, U.S.A., 24.0 KHz located at 44°38'50" N, 67°16'54" W, and Seattle, Washington, U.S.A., 24.8 KHz located at 48°12'15" N, 121°55'00" W. The field procedures and specifications for the Omni-Plus VLF/Magnetometer system and the Genie portable EM system can be found in Appendices IV and V respectively.

Moving Source Genie Survey

The moving source Genie survey was carried out using a Genie SE-88 transmitter and an IGS-EM4 receiver. This system is a variant on the horizontal loop electromagnetic system in which the receiver and transmitter are separated by a fixed distance (100 m) and are moved in tandem along survey lines.

The transmitter is designed to simultaneously transmit signals at two well-separated frequencies. One of these is referred to as the reference frequency (112.5 Hz.) and the other is the signal frequency, which can be 337.5, 1012.5 or 3037.5 Hz. The receiver is a digital acquisition system capable of signal stacking and averaging the transmitted signals of the reference and one of the signal frequencies, and storing the amplitudes of these signals, as well as calculating the amplitude ratios of the various signals ie. 3037.5/112.5, 1012.5/112.5 and 337.5/112.5.

In the present survey, the percentage variations for the three amplitude ratios are plotted for each survey line. In a non-conductive environment the results are zero, while in the presence of a conductor, the measured values will show a negative value similar in shape to conventional HLEM results. If the 3037.5 frequency ratio dominates the response compared to the other two measured ratios, it indicates a weak conductor, whereas if the response at all three frequency ratios is similar, it indicates a strong conductor.

The moving source Genie data for the three frequency ratios has been plotted in profile at a scale of 1:10,000 (Map 1).

Magnetometer and VLF-EM Surveys

Magnetic and VLF-EM data were obtained using an EDA Omni-Plus digital acquisition system.

Diurnal variations of the earth's magnetic field were recorded with a second base station unit. Field and base station data was merged at the end of each survey day to remove the effects of these variations. The measuring accuracy of this procedure is ± 2 nT.

The magnetic field data has been corrected for diurnal variations and the ambient value of 57,000 nT has been removed from the measured values (Map 2). The residual data has been contoured at a scale of 1:10,000 and is presented on Map 3.

The VLF-EM data was measured at the same time as the magnetic data. The system is capable of sequentially measuring the in-phase, quadrature and horizontal field strength components of signals broadcast by up to three VLF transmitters operating in the 15 to 30 kHz. range. In the current survey, the variations in signals put out by the transmitters in Cutler, Maine and Seattle, Washington were measured.

The in-phase and quadrature results for both the Cutler and Seattle signals is presented in profile at a scale of 1:10,000 on Maps 4 and 6 respectively. The in-phase data has also been Fraser-filtered and contoured on Maps 5 and 7.

RESULTS

Geochemical Survey

No significant results were obtained from the soil geochemical survey.

Geophysical Surveys

The moving source Genie data (Map 1) has outlined a series of conductive trends in the northernmost part of the grid bearing S55E. Most are short strike length anomalies, generally less than 400 m in length. The exception is anomaly A which extends from line 12300 N to 11300 N. Responses are very strong - in some cases exceeding -50% at the 3037.5/112.5 frequency ratio - and are caused by very near surface vertical conductors. However, the results at the other two frequency ratios are significantly weaker, indicating that these are weak to fair conductors only. Of these, anomaly A is the strongest because it is the widest, consisting of a broad conductive zone, or alternatively, a series of closely spaced zones.

Conductors B and C, located between lines 11100 N and 10200 N in the central part of the grid, may be the en echelon or a faulted continuation of anomaly A. The responses are weak as discussed above, however on lines 10900 N and 10700 N, the strong positive shoulder on the west side suggests a dip in that direction. The strongest responses are between 10700 N and 10400 N, though again these responses indicate only weak conductors.

In the southern part of the grid there are no conductive anomalies. There is, however, a series of positive Genie anomalies again dominated by the 3037.5/112.5 frequency response, eg. line 9700 N between 9400E and 9600 E. These results were obtained along the steep sloping part of the grid.

The residual magnetic results presented on Map 3 are shown for only the northern and southern portions of the grid. In the northern part, the magnetic relief is very minor and no trends have been developed. This suggests that the rock underlying the grid is relatively homogeneous and non-magnetic. In the southern part, results show a more active magnetic environment, though one that appears to be erratic. There is a weak trend that extends from 9000 N to at least 10000 N between 9200 E and 9450 E. This anomaly is near the change of topography on the grid and is immediately above the positive Genie anomalies mentioned earlier.

The Cutler data (Map 5) shows very little response, indicating that the signal is poorly coupled with the conductors on these grids. The Seattle data (Map 7) is more diagnostic. It has delineated two anomalous trends; one is roughly north-south and the other correlates with the Genie data in the area between lines 10400 N and 10100 N at about 9000E (Genie anomaly B). The north-south anomalies located between lines 12200N and 10900 N at 7600 E and 9400 N to 8300 N roughly at 9000 E do not correlate with any Genie anomalies. These responses are generally weak and may be caused by topographic changes.

CONCLUSIONS

The Genie survey has outlined a series of shallow vertical to steeply west-dipping conductors in the northern part of the grid. Most are about 400 m in strike length. The exception is anomaly A which continues further to the southeast as two distinctive anomalies which end at about line 10300 N. There is no direct magnetic correlation with the EM anomalies on these grids. The magnetic data in the southern part of the grid is significantly different from the rest of the grid as to suggest that this area is underlain by a different geologic unit.

Selective geochemical sampling in the area has not produced significant base metal anomalies which would have been expected considering the shallowness of the conductors outlined in this survey. Consequently the source of the geophysical anomalies covered by the soil sampling can be either graphitic or barren sulphides.

RECOMMENDATIONS

It is recommended that a widely spaced geochemical soil survey be conducted over the unsampled existing grid. Line spacing of 200 metres with sample density of 50 metres should be adequate. Additional work would be contingent upon obtaining favourable results from the soil sampling.

BIBLIOGRAPHY

Duffell, S. and McTaggart, K.C. (1952): Ashcroft map area, British Columbia; Geological Survey of Canada, Memoir 262.

Monger, J.W.H. and McMillan, W.J. (1983): Bedrock geology of Ashcroft (92 I) map area; Geological Survey of Canada, Open File 980.

Shearing, R.E. (1986): Prospecting report on the Genesis North, Genesis Central, Genesis South claim groups; unpublished Assessment Report.

Kamloops Mining Division, Assessment Reports:

#8892 - Guichon Explorco Limited
#9415 - Explorco Limited
#3153 - Adera Mining Limited
#4068 - Milestone Mines Ltd. (N.P.L.)
#9177 - Cominco Ltd.

APPENDIX I

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY AA FROM 10 GRAM SAMPLE.

DATE RECEIVED: MAY 25 1988 DATE REPORT MAILED: May 31/88 ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

TROVE RESOURCES PROJECT-E 88 05 File # 88-1577 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L15N 84+00W	2	33	4	218	.3	37	11	1633	3.17	5	5	ND	3	80	1	2	2	48	1.03	.071	10	46	.75	267	.12	2	1.82	.04	.47	1	1
L15N 83+75W	1	42	6	70	.5	23	4	487	1.01	10	5	ND	1	269	1	2	2	14	18.03	.058	4	17	.38	114	.03	4	.53	.03	.13	1	1
L15N 83+50W	1	41	2	45	.6	19	4	394	1.18	5	5	ND	1	498	1	3	2	15	15.09	.040	3	15	.57	124	.04	9	.78	.04	.21	1	1
L15N 83+25W	2	51	4	92	.5	43	9	509	2.30	12	5	ND	2	466	1	2	2	36	12.06	.055	6	36	.94	111	.06	9	1.26	.03	.20	1	1
L15N 83+00W	2	27	6	141	.3	39	11	642	3.25	8	6	ND	4	65	1	2	2	54	.94	.025	8	46	.76	104	.14	2	2.05	.03	.37	1	1
L15N 82+75W	1	38	3	86	.4	29	6	597	1.60	7	5	ND	2	283	1	3	2	23	12.35	.064	5	24	.54	136	.04	10	.90	.02	.21	1	1
L15N 82+50W	2	82	8	380	.3	54	11	1531	2.98	11	5	ND	3	115	2	3	2	42	3.62	.114	11	41	.66	255	.08	18	1.74	.03	.37	1	1
L15N 82+25W	2	47	9	223	.4	47	11	971	3.17	10	5	ND	4	84	1	2	2	49	2.36	.035	10	45	.70	179	.12	6	2.09	.02	.35	1	1
L15N 82+00W	1	37	4	66	.2	25	5	622	1.39	9	5	ND	1	297	1	2	2	19	16.84	.063	4	19	.52	138	.03	11	.72	.02	.13	1	1
L15N 81+75W	3	64	7	230	.3	77	16	879	4.45	14	5	ND	5	74	1	2	2	68	1.94	.050	14	80	1.19	144	.12	13	2.72	.04	.68	1	1
L15N 81+50W	3	39	6	136	.3	62	14	1264	3.82	2	5	ND	4	65	1	2	2	60	.95	.047	12	74	1.08	190	.11	2	2.22	.02	.41	1	3
L15N 81+25W	3	51	7	228	.4	59	13	1562	3.91	10	5	ND	3	69	1	2	2	58	.91	.059	13	66	.90	303	.11	2	2.45	.02	.38	1	1
L15N 81+00W	3	52	7	177	.2	68	14	1329	3.94	9	5	ND	3	57	1	2	2	58	.90	.057	13	72	1.01	228	.11	2	2.26	.04	.34	1	1
L15N 80+75W	5	83	8	167	.1	119	20	985	5.08	14	5	ND	4	48	1	2	2	82	.77	.056	18	109	1.74	179	.12	8	3.19	.02	.28	1	2
L15N 80+50W	3	33	4	146	.2	49	14	494	3.98	11	5	ND	4	45	1	2	2	67	.55	.042	12	67	1.00	153	.15	2	2.60	.01	.35	1	1
L15N 80+25W	3	30	10	177	.4	44	12	1305	3.36	6	5	ND	4	51	1	2	2	54	.73	.053	10	52	.84	188	.11	2	2.10	.01	.31	1	1
L15N 80+00W	2	24	4	153	.1	39	10	654	3.35	3	5	ND	3	37	1	2	2	55	.43	.036	7	48	.82	164	.14	2	2.13	.02	.37	1	1
L15N 79+75W	3	22	5	179	.2	36	11	595	3.25	4	5	ND	3	34	1	2	2	53	.40	.036	8	46	.80	149	.13	7	2.17	.03	.24	1	1
L15N 79+50W	3	39	5	208	.4	50	14	701	4.03	11	7	ND	4	55	1	2	2	66	.86	.061	10	55	1.08	136	.13	5	2.43	.01	.30	1	1
L15N 79+25W	5	45	5	241	.1	55	14	668	4.26	11	5	ND	4	50	1	2	2	71	.65	.028	11	57	1.22	106	.13	2	2.48	.03	.24	1	1
L15N 79+00W	4	75	6	220	.3	71	14	934	4.12	11	5	ND	4	56	1	2	2	63	1.74	.024	19	51	.98	136	.11	2	2.28	.01	.30	1	1
L114+50N 79+50E	5	73	6	238	.3	102	17	655	5.26	14	5	ND	5	43	1	2	2	83	.60	.069	17	97	1.57	125	.11	4	3.28	.01	.44	2	1
L114+50N 79+75E	2	59	8	133	.3	36	6	667	1.58	12	5	ND	2	272	2	3	2	24	11.51	.104	5	25	.71	179	.04	18	.92	.04	.17	1	1
L114+50N 80+00E	4	41	9	193	.1	50	13	842	4.14	8	5	ND	4	56	1	2	2	63	.74	.087	11	56	.98	193	.12	2	2.32	.01	.26	1	1
L114+50N 80+25E	3	52	6	137	.3	82	16	784	4.17	9	5	ND	4	64	1	3	2	69	.85	.095	15	100	1.23	154	.15	7	2.43	.01	.32	1	1
L114+50N 80+50E	4	42	5	195	.2	50	13	874	4.13	10	5	ND	3	56	1	3	3	62	.72	.089	11	56	.97	198	.11	2	2.30	.02	.25	1	1
L114+50N 80+75E	3	36	6	209	.2	44	11	1127	3.29	6	5	ND	3	53	1	2	2	51	.61	.046	9	49	.75	203	.12	2	2.03	.03	.26	1	1
L114+50N 81+00E	4	65	5	208	.4	75	15	992	4.25	13	5	ND	4	59	1	2	2	62	.91	.090	14	74	1.21	188	.10	2	2.43	.01	.41	2	1
L114+50N 81+25E	2	28	6	171	.2	39	10	841	3.06	2	5	ND	2	54	1	2	2	48	.52	.049	8	50	.75	211	.13	6	2.11	.03	.29	1	1
L114+50N 81+50E	3	33	6	220	.1	49	12	1263	3.38	7	5	ND	3	58	1	2	3	52	.63	.069	11	53	.77	282	.13	2	2.44	.03	.29	1	1
L114+50N 81+75E	2	39	4	168	.1	55	12	720	3.77	6	5	ND	3	46	1	2	2	58	.52	.041	14	62	.96	201	.14	2	2.64	.01	.28	1	1
L114+50N 82+00E	3	26	7	148	.1	42	12	530	3.45	3	5	ND	2	35	1	2	2	58	.36	.037	8	54	.85	157	.14	2	2.18	.03	.20	2	1
L114+50N 82+25E	2	30	3	178	.1	48	13	910	3.52	5	5	ND	3	40	1	2	2	52	.46	.042	12	58	.87	197	.13	2	2.37	.02	.29	2	1
L114+50N 82+50E	2	28	6	159	.1	43	12	723	3.38	7	5	ND	3	52	1	2	2	53	.56	.070	9	50	.79	167	.13	2	2.21	.02	.30	1	3
L114+50N 82+75E	2	35	6	212	.3	43	11	724	3.21	2	5	ND	3	54	1	2	2	50	.50	.052	10	46	.70	182	.13	2	2.28	.03	.29	1	1
L114+50N 83+00E	3	36	5	154	.1	48	11	428	3.99	9	5	ND	4	50	1	2	2	60	.62	.056	13	54	.96	109	.13	4	2.20	.03	.32	1	1
STD C/AU-S	20	63	39	132	7.4	73	31	1091	4.05	42	16	8	40	55	20	15	20	61	.49	.094	40	60	.95	181	.08	31	1.89	.06	.17	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L114+50N 83+25E	1	32	8	135	.3	39	10	949	2.89	2	5	ND	1	50	1	2	5	48	.74	.043	8	39	.66	146	.11	9	1.81	.01	.23	2	2
L114+50N 83+50E	1	32	4	135	.2	32	9	424	2.40	2	5	ND	2	232	1	2	4	36	5.02	.025	6	27	.72	85	.08	10	1.53	.03	.24	1	1
L114+50N 83+75E	1	69	4	170	.5	41	8	810	2.22	4	5	ND	1	211	2	2	4	32	11.00	.113	6	32	.67	126	.05	16	1.33	.02	.17	1	1
L114+50N 84+00E	1	67	5	173	.5	41	8	810	2.29	4	5	ND	2	203	2	2	5	33	10.22	.108	6	33	.68	124	.05	15	1.39	.05	.18	1	1
L114+50N 84+00EA	1	52	4	100	.4	35	6	577	1.62	8	5	ND	1	272	1	3	3	24	17.24	.070	4	23	.63	113	.03	14	.89	.02	.10	1	1
L114N 79+75E	2	28	6	166	.3	48	11	442	3.38	4	5	ND	3	35	1	2	2	55	.55	.025	8	52	.98	124	.12	2	2.10	.02	.22	1	1
L114N 80+00E	2	36	8	170	.1	60	13	548	3.52	3	5	ND	3	47	1	2	4	58	.53	.061	12	59	.96	160	.12	2	2.50	.01	.25	1	3
L114N 80+25E	3	36	8	218	.2	49	12	1181	2.95	7	5	ND	2	48	1	2	4	45	.58	.054	9	51	.78	159	.07	4	1.48	.02	.19	1	1
L114N 80+50E	3	32	5	158	.1	45	12	753	3.41	6	5	ND	2	40	1	2	2	60	.43	.031	9	50	.87	134	.11	4	2.10	.03	.22	1	1
L114N 80+75E	2	38	9	157	.1	55	14	450	3.94	4	5	ND	2	36	1	3	2	68	.37	.036	12	57	1.03	151	.12	3	2.64	.02	.20	3	1
L114N 81+00E	2	31	5	180	.1	38	11	1191	2.99	2	5	ND	2	52	1	2	2	48	.54	.062	7	40	.72	213	.11	4	2.03	.02	.21	1	1
L114N 81+25E	1	28	6	216	.4	35	8	1058	2.64	9	5	ND	3	52	1	3	4	42	.48	.069	6	38	.62	211	.10	3	1.77	.01	.24	2	1
L114N 81+50E	1	27	6	177	.2	40	10	1082	2.98	2	5	ND	3	48	1	2	2	48	.45	.050	8	43	.71	224	.12	3	2.12	.03	.25	1	1
L114N 81+75E	1	24	6	138	.1	41	10	1180	2.90	2	5	ND	2	45	1	2	3	47	.43	.076	8	44	.71	197	.11	3	1.90	.01	.22	1	1
L114N 82+00E	1	23	5	173	.2	38	10	928	2.78	2	5	ND	2	50	1	2	4	45	.54	.050	8	40	.66	182	.11	5	1.84	.03	.23	1	1
L114N 82+25E	2	28	6	136	.3	39	9	631	2.96	2	5	ND	2	38	1	2	2	51	.43	.029	9	44	.65	136	.12	4	1.69	.03	.22	2	2
L114N 82+50E	2	29	8	209	.1	43	10	700	3.13	5	5	ND	2	36	1	2	3	51	.40	.042	9	52	.78	141	.11	5	1.88	.01	.26	1	1
L114N 82+75E	1	25	4	120	.1	32	8	1088	2.56	2	5	ND	2	49	1	2	2	41	.59	.050	5	39	.61	163	.09	5	1.54	.04	.32	1	1
L114N 83+00E	2	33	7	146	.1	42	10	1130	2.76	2	5	ND	2	58	1	2	2	48	1.26	.049	7	41	.75	163	.09	7	1.54	.01	.21	1	1
L114N 83+25E	2	23	9	115	.2	33	10	840	3.03	6	5	ND	2	33	1	2	3	54	.43	.026	7	43	.72	149	.13	6	1.78	.01	.18	2	1
L114N 83+50E	1	28	7	211	.1	34	9	1211	2.82	6	5	ND	1	44	1	2	2	48	.52	.034	7	37	.57	174	.11	8	1.75	.01	.28	3	3
L114N 83+75E	2	31	7	127	.1	39	12	1034	3.22	2	5	ND	1	45	1	2	2	56	.42	.020	9	43	.78	135	.13	2	1.76	.01	.18	1	1
L114N 84+00E	1	40	7	166	.1	41	12	1227	3.16	11	5	ND	1	65	1	2	2	48	.75	.094	10	42	.75	201	.09	4	2.15	.02	.20	1	1
L114N 84+25E	3	127	6	124	.1	48	13	682	3.50	18	5	ND	1	93	1	2	2	57	2.54	.058	9	46	1.04	83	.08	3	1.75	.03	.12	4	1
L114N 84+50E	1	29	4	126	.1	28	9	1497	2.39	2	5	ND	1	69	1	2	2	36	.71	.025	6	31	.47	151	.09	7	1.50	.02	.36	1	1
L114N 84+75E	1	29	5	169	.1	33	10	1058	2.66	2	5	ND	1	55	1	2	3	42	.58	.023	6	37	.55	129	.11	5	1.63	.02	.30	1	1
L113+50N 80+25E	2	26	7	146	.1	41	11	853	3.10	4	5	ND	1	36	1	2	5	51	.38	.061	8	42	.74	158	.10	3	2.01	.04	.17	1	1
L113+50N 80+50E	2	38	4	264	.1	35	9	1810	2.60	3	5	ND	1	41	1	2	2	41	.42	.060	6	39	.60	302	.08	6	1.62	.02	.21	1	1
L113+50N 80+75E	1	36	4	239	.1	38	9	1352	2.84	4	5	ND	1	52	1	2	2	46	.51	.059	7	40	.63	327	.10	7	1.76	.02	.24	1	1
L113+50N 81+00E	2	27	4	143	.1	38	10	774	3.07	3	5	ND	1	39	1	2	2	51	.39	.048	7	42	.76	155	.10	3	2.00	.02	.25	1	1
L113+50N 81+25E	3	40	6	142	.1	46	12	1027	3.48	5	5	ND	2	44	1	2	2	58	.57	.032	10	49	.95	147	.09	3	2.00	.04	.17	1	2
L113+50N 81+50E	2	31	4	158	.1	42	10	886	3.39	2	5	ND	1	44	1	2	2	55	.53	.056	9	48	.77	175	.11	5	1.78	.01	.26	1	1
L113+50N 81+75E	2	26	5	130	.1	43	11	707	3.17	5	5	ND	2	47	1	2	2	53	.54	.037	9	46	.69	233	.13	2	2.38	.01	.21	1	1
L113+50N 82+00E	1	26	8	171	.1	42	10	941	3.01	7	5	ND	2	48	1	2	2	47	.52	.065	9	42	.65	249	.11	5	1.98	.03	.26	1	1
L113+50N 82+25E	2	21	6	147	.1	31	9	1090	2.54	6	5	ND	1	39	1	2	2	43	.42	.048	6	37	.58	183	.10	4	1.49	.01	.15	1	1
L113+50N 82+50E	2	24	3	189	.1	34	8	649	2.74	2	5	ND	1	43	1	2	2	44	.55	.042	6	39	.63	161	.10	4	1.78	.03	.25	1	1
STD C/AU-S	19	62	39	132	7.1	70	30	1061	4.00	44	18	8	40	53	19	15	17	60	.49	.089	41	61	.94	179	.07	34	1.80	.07	.15	14	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L113+50N 82+75E	3	51	9	121	.2	59	12	718	3.30	15	5	ND	3	71	1	2	2	68	2.12	.059	10	55	.93	129	.10	2	1.85	.01	.15	1	1
L113+50N 83+00E	2	34	9	235	.1	49	11	1042	3.26	4	5	ND	3	48	1	2	2	57	.46	.039	11	53	.73	219	.13	9	2.17	.01	.32	1	1
L113+50N 83+25E	2	35	8	157	.2	54	12	836	3.20	9	5	ND	4	40	1	2	2	60	.40	.032	11	54	.78	185	.13	2	2.25	.01	.23	1	1
L113+50N 83+50E	2	35	7	154	.1	42	11	1579	2.77	5	5	ND	2	47	1	2	2	46	.51	.081	9	44	.64	253	.09	2	1.78	.02	.27	1	1
L113+50N 83+75E	2	35	9	161	.1	44	12	1176	3.15	8	5	ND	3	55	1	2	2	55	.47	.113	11	48	.69	233	.12	6	2.26	.03	.28	2	2
L113+50N 84+00E	2	39	7	145	.1	48	12	1009	3.21	6	5	ND	3	52	1	2	2	53	.52	.059	12	44	.75	245	.13	5	2.43	.01	.24	1	1
L113+50N 84+25E	2	37	9	151	.1	44	13	1469	3.34	9	5	ND	3	52	1	2	2	56	.58	.045	12	46	.81	286	.12	6	2.44	.02	.21	1	1
L113+50N 84+50E	1	32	8	104	.1	36	11	897	3.00	6	5	ND	2	41	1	2	2	51	.51	.021	8	40	.64	125	.12	9	1.96	.02	.37	1	1
L113+50N 84+75E	3	60	9	119	.1	46	12	833	3.38	19	5	ND	3	64	1	2	2	59	1.94	.074	11	40	.87	134	.10	2	1.77	.01	.15	1	1
L113+50N 85+00E	2	24	12	146	.1	40	10	1101	3.04	6	5	ND	3	51	1	2	2	53	.44	.054	9	43	.67	219	.14	5	2.29	.02	.26	2	1
L113+50N 85+25E	2	39	8	263	.1	41	12	1807	2.84	3	5	ND	3	61	2	2	2	45	.57	.069	9	40	.64	229	.10	14	1.97	.03	.30	1	1
L113N 80+50E	1	74	11	287	.1	60	10	1772	2.58	5	5	ND	3	70	2	2	2	47	.73	.073	10	42	.68	276	.10	7	1.89	.03	.21	1	1
L113N 80+75E	2	25	8	154	.1	38	9	1341	2.64	4	5	ND	2	40	1	2	2	48	.37	.045	7	45	.62	222	.11	10	1.75	.01	.20	1	1
L113N 81+00E	3	26	8	204	.1	40	11	1512	2.88	8	5	ND	3	43	1	2	2	48	.42	.055	8	45	.63	249	.10	2	1.93	.03	.24	1	2
L113N 81+25E	2	32	5	176	.1	39	10	1169	3.13	7	5	ND	4	47	1	2	2	50	.45	.051	10	41	.71	272	.10	11	2.09	.01	.26	1	1
L113N 81+50E	2	28	7	134	.1	35	10	822	2.92	4	5	ND	3	47	1	2	2	50	.45	.027	9	41	.69	185	.11	10	1.85	.04	.20	1	1
L113N 81+75E	2	25	7	136	.1	29	8	1051	2.47	3	5	ND	3	74	1	2	3	45	.77	.035	6	33	.59	191	.09	10	1.41	.04	.23	2	1
L113N 82+00E	2	22	7	135	.2	30	9	1296	2.32	2	5	ND	2	40	1	2	3	42	.39	.040	6	31	.50	173	.09	2	1.44	.01	.18	1	1
L113N 82+25E	3	30	6	139	.1	40	11	1179	2.73	5	5	ND	2	41	1	2	2	47	.38	.048	10	46	.63	229	.11	2	1.88	.03	.21	1	1
L113N 82+50E	2	25	7	153	.1	35	9	1117	2.54	2	5	ND	3	40	1	2	3	45	.39	.040	7	40	.57	217	.11	6	1.68	.06	.19	2	1
L113N 82+75E	2	26	8	143	.1	40	11	714	3.12	7	5	ND	3	34	1	2	2	58	.36	.028	9	51	.79	153	.13	4	1.86	.04	.20	1	2
L113N 83+00E	3	36	9	134	.1	58	15	530	3.63	3	5	ND	3	43	1	2	3	69	.38	.062	12	64	.96	226	.13	5	2.66	.02	.21	2	1
L113N 83+25E	2	29	6	156	.1	31	9	1388	2.36	2	5	ND	2	44	1	2	2	44	.39	.045	5	35	.55	213	.10	9	1.33	.02	.21	1	1
L113N 83+50E	3	44	9	122	.1	59	13	517	3.56	10	5	ND	3	49	1	2	3	66	.60	.059	14	61	.90	192	.13	2	2.38	.03	.27	1	1
L113N 83+75E	2	32	5	181	.1	41	10	1570	2.78	3	5	ND	3	52	1	2	2	47	.50	.067	9	42	.63	301	.11	3	2.00	.06	.24	1	1
L113N 84+00E	3	51	7	136	.1	73	16	790	3.77	9	5	ND	4	44	1	2	2	67	.50	.076	13	63	1.19	143	.11	3	1.89	.03	.18	1	1
L113N 84+25E	2	34	8	152	.1	45	11	1267	3.07	6	5	ND	3	41	1	2	2	52	.48	.042	10	46	.74	196	.09	2	1.82	.02	.19	1	1
L113N 84+50E	2	22	8	263	.1	28	8	1547	2.01	5	5	ND	2	43	1	2	2	34	.46	.098	5	27	.38	150	.08	6	1.32	.02	.20	1	1
L113N 84+75E	4	39	9	219	.1	41	11	1329	3.01	13	5	ND	3	49	1	2	2	45	.52	.047	11	32	.57	230	.08	11	1.72	.03	.20	1	1
L113N 85+00E	2	25	8	195	.1	33	9	1076	2.56	6	5	ND	3	45	1	2	2	42	.44	.067	7	35	.51	230	.11	3	1.80	.02	.25	1	2
L113N 85+25E	2	32	8	221	.1	40	10	1222	2.70	2	5	ND	3	45	1	2	3	44	.43	.044	10	36	.56	295	.11	3	1.86	.03	.21	1	1
L113N 85+50E	1	43	9	246	.1	32	9	2232	2.36	5	5	ND	3	92	1	2	2	40	.88	.110	6	32	.46	330	.09	11	1.54	.03	.33	1	1
L112+50N 81+00E	2	24	6	160	.1	41	11	632	2.71	2	5	ND	1	40	1	2	2	45	.37	.105	6	41	.65	193	.09	2	2.17	.01	.17	1	1
L112+50N 81+25E	2	33	9	142	.1	41	12	949	2.78	4	5	ND	2	45	1	2	3	49	.52	.047	8	45	.68	221	.09	3	1.75	.02	.15	1	1
L112+50N 81+50E	2	38	9	214	.1	46	12	1191	2.81	6	5	ND	3	52	1	2	2	47	.50	.096	9	43	.67	329	.09	6	2.04	.03	.20	1	1
L112+50N 81+75E	2	32	7	144	.1	35	10	1143	2.70	4	5	ND	4	41	1	2	2	45	.40	.046	10	37	.59	192	.09	3	1.55	.03	.19	1	2
STD C/AU-S	19	63	40	129	6.8	70	31	1169	3.68	41	19	8	41	53	17	20	20	60	.45	.088	41	61	.86	190	.07	34	1.71	.09	.13	13	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L112+50N 82+00E	1	18	5	192	.2	25	8	906	2.14	2	5	ND	3	47	1	2	3	32	.52	.052	5	30	.45	178	.08	3	1.49	.03	.19	1	1
L112+50N 82+25E	2	26	6	277	.3	38	11	1217	2.83	8	5	ND	3	40	1	2	2	42	.59	.050	7	46	.70	233	.09	4	1.79	.02	.30	1	1
L112+50N 82+50E	3	36	11	147	.2	51	13	934	3.37	7	5	ND	4	55	1	2	2	53	.68	.058	10	56	.90	158	.10	3	1.98	.05	.26	1	1
L112+50N 82+75E	3	40	6	170	.3	52	13	821	3.25	9	5	ND	3	45	1	2	2	52	.86	.047	9	55	.93	136	.09	3	1.99	.02	.24	1	2
L112+50N 83+00E	3	27	8	188	.2	41	11	660	3.47	8	5	ND	3	33	1	2	2	55	.48	.038	9	58	.87	131	.12	2	2.03	.01	.33	1	1
L112+50N 83+25E	2	18	5	183	.1	26	10	518	2.88	9	5	ND	2	33	1	2	2	49	.37	.028	6	39	.67	90	.13	2	1.58	.01	.24	2	1
L112+50N 83+50E	1	25	5	226	.2	29	10	1490	2.88	5	5	ND	2	45	1	2	2	47	.51	.050	6	39	.72	172	.13	2	1.83	.02	.32	1	1
L112+50N 83+75E	2	24	5	148	.2	40	13	1176	3.18	7	5	ND	3	40	1	2	3	52	.52	.030	8	54	.78	157	.13	3	2.22	.01	.35	1	1
L112+50N 84+00E	2	22	7	162	.4	31	10	1136	2.83	2	5	ND	3	34	1	2	3	45	.45	.053	7	44	.67	162	.11	3	1.78	.02	.33	2	1
L112+50N 84+25E	3	43	3	134	.1	74	16	737	3.98	12	5	ND	3	38	1	2	2	66	.59	.059	12	79	1.22	134	.13	2	2.37	.01	.26	1	1
L112+50N 84+50E	2	22	6	134	.3	43	12	868	3.01	6	5	ND	3	31	1	2	4	51	.43	.028	7	54	.74	167	.14	2	2.15	.01	.27	1	1
L112+50N 84+75E	2	25	6	153	.1	40	12	1377	3.06	8	5	ND	3	39	1	2	3	49	.53	.031	7	49	.73	203	.13	3	2.15	.05	.22	1	1
L112+50N 85+00E	1	42	6	177	.1	57	14	1146	3.20	10	5	ND	3	64	1	2	2	48	.87	.105	11	69	.75	296	.13	6	2.16	.04	.33	1	1
L112+50N 85+25E	2	25	7	168	.2	40	12	1463	3.19	12	5	ND	3	38	1	2	2	48	.57	.044	9	48	.73	261	.13	3	2.42	.05	.32	1	1
L112+50N 85+50E	2	41	6	158	.2	66	17	1187	3.74	6	5	ND	4	60	1	2	2	60	.91	.063	12	76	.94	288	.15	4	2.75	.05	.37	1	1
L112+50N 85+75E	2	39	8	149	.2	60	18	837	4.01	11	5	ND	4	50	1	2	2	67	.77	.087	13	71	1.12	200	.15	2	3.10	.01	.27	1	1
L112+50N 86+00E	3	32	6	128	.2	43	12	852	3.37	6	5	ND	3	35	1	2	2	57	.30	.023	9	55	.82	139	.14	2	2.19	.04	.28	1	1
L112N 81+00E	3	37	9	160	.2	51	14	737	3.74	12	6	ND	4	43	1	3	2	62	.51	.064	12	61	1.03	161	.14	4	2.29	.04	.25	1	1
L112N 81+25E	3	33	6	158	.2	48	13	592	3.62	7	5	ND	4	34	1	2	2	57	.43	.046	10	60	1.05	130	.12	3	2.21	.02	.25	1	1
L112N 81+50E	2	31	8	159	.4	39	11	817	3.20	6	5	ND	3	42	1	3	2	52	.49	.054	9	49	.78	169	.12	5	1.81	.03	.31	1	4
L112N 81+75E	2	27	7	141	.1	41	12	548	3.30	3	5	ND	4	40	1	2	2	53	.47	.021	11	50	.80	159	.13	2	2.19	.01	.25	1	1
L112N 82+00E	3	27	8	189	.2	39	13	559	3.42	6	5	ND	4	31	1	2	3	54	.31	.058	9	49	.76	142	.13	4	2.34	.02	.31	1	1
L112N 82+25E	3	31	5	187	.2	44	13	780	3.50	5	5	ND	3	41	1	2	2	54	.44	.055	10	54	.90	160	.13	2	2.44	.02	.30	1	1
L112N 82+50E	2	34	4	205	.1	48	15	712	3.77	6	5	ND	3	36	1	2	2	61	.41	.071	10	60	.98	176	.13	2	2.51	.01	.27	1	3
L112N 82+75E	2	31	6	280	.2	39	12	1006	3.36	6	5	ND	3	43	1	2	2	52	.50	.070	9	50	.83	264	.12	4	2.20	.02	.34	1	1
L112N 83+00E	3	45	10	263	.1	60	14	881	4.01	10	5	ND	3	53	1	2	2	60	1.05	.082	11	74	1.08	191	.13	14	2.80	.04	.58	1	3
L112N 83+25E	5	47	8	273	.2	57	14	743	3.97	12	5	ND	3	50	1	3	3	59	.57	.039	13	52	.82	151	.09	5	2.33	.04	.44	1	1
L112N 83+50E	1	24	6	208	.2	30	9	1470	2.64	4	5	ND	2	46	1	2	2	42	.56	.069	6	38	.58	211	.11	3	1.92	.02	.30	1	1
L112N 83+75E	1	23	6	134	.1	33	10	1006	2.91	3	5	ND	3	33	1	2	2	49	.42	.024	7	44	.64	176	.13	3	1.91	.03	.36	1	1
L112N 84+00E	3	48	9	158	.2	76	19	655	4.59	11	5	ND	4	35	1	2	2	79	.51	.061	13	84	1.48	104	.15	5	2.96	.02	.35	1	3
L112N 84+25E	2	36	5	200	.2	71	16	907	3.76	5	5	ND	3	43	1	3	2	59	.57	.054	11	83	1.00	278	.17	5	2.71	.05	.35	1	1
L112N 84+50E	2	32	5	197	.3	46	14	1307	3.17	7	5	ND	4	52	1	2	2	49	.64	.081	10	54	.75	277	.13	5	2.45	.03	.41	1	1
L112N 84+75E	2	32	8	186	.2	50	14	1093	3.62	8	5	ND	3	44	1	2	2	58	.54	.064	11	62	.91	250	.15	4	2.70	.04	.38	1	1
L112N 85+00E	2	30	7	224	.2	40	12	1635	2.96	3	5	ND	3	42	1	2	2	45	.54	.086	8	48	.67	319	.12	3	2.18	.01	.41	1	1
L112N 85+25E	2	33	8	171	.2	51	13	1445	3.39	7	5	ND	3	49	1	2	2	50	.80	.077	10	54	.82	285	.13	8	2.59	.03	.37	1	1
L112N 85+50E	2	28	6	154	.2	41	13	1225	3.35	7	5	ND	3	39	1	2	3	53	.52	.048	9	50	.78	267	.14	2	2.57	.02	.31	1	1
STD C/AU-S	21	61	42	138	8.0	70	31	1144	4.08	40	19	9	41	52	19	18	22	64	.50	.097	41	61	.97	184	.08	32	1.97	.08	.16	14	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L112N 85+75E	2	30	5	129	.1	44	11	1035	3.58	2	5	ND	3	42	1	2	3	53	.52	.020	5	54	.83	244	.13	3	2.59	.01	.27	1	6
L112N 86+00E	1	37	8	117	.3	35	11	1367	2.87	4	5	ND	4	57	1	2	2	43	.60	.064	9	39	.59	189	.10	3	2.20	.01	.23	2	3
L112N 86+27E	2	48	8	120	.2	54	14	1335	3.53	4	5	ND	3	58	1	2	2	52	.76	.071	12	54	.88	242	.11	4	2.29	.01	.26	1	1
L111+50N 81+50E	4	76	6	151	.3	90	15	577	4.17	13	5	ND	4	46	1	2	2	65	.80	.073	17	73	1.29	141	.09	8	2.43	.01	.34	1	4
L111+50N 81+75E	2	38	3	138	.3	45	10	686	3.03	7	5	ND	3	58	1	2	2	46	1.41	.081	10	45	.82	131	.09	7	1.62	.01	.20	1	1
L111+50N 82+00E	4	49	10	142	.1	62	13	442	4.15	9	5	ND	4	43	1	2	3	60	.60	.041	16	62	1.02	128	.11	3	2.45	.01	.24	1	1
L111+50N 82+25E	1	35	4	267	.3	28	5	503	1.75	2	5	ND	1	209	3	2	2	23	5.98	.121	4	25	.51	150	.05	19	1.20	.01	.24	1	1
L111+50N 82+50E	2	25	3	170	.3	32	8	946	2.50	2	5	ND	3	49	1	2	2	36	.48	.065	6	37	.53	198	.08	6	1.53	.01	.23	1	1
L111+50N 82+75E	1	22	5	446	.1	41	8	374	2.85	2	5	ND	3	39	1	2	2	42	.41	.061	5	43	.64	144	.11	9	2.02	.01	.27	1	1
L111+50N 83+00E	2	20	4	146	.1	26	7	788	2.67	2	5	ND	3	33	1	2	2	42	.41	.028	5	34	.65	115	.10	5	1.71	.01	.24	1	1
L111+50N 83+25E	2	39	3	315	.3	44	11	1288	2.97	2	5	ND	3	108	4	2	2	41	.82	.183	8	46	.69	283	.09	10	2.15	.01	.33	1	2
L111+50N 83+50E	2	39	6	203	.1	52	10	1014	3.52	4	5	ND	3	48	1	2	2	50	.51	.062	9	58	.90	231	.11	12	2.27	.03	.42	1	1
L111+50N 83+75E	3	37	6	162	.1	54	12	718	3.65	8	5	ND	4	44	1	2	2	54	.46	.064	11	55	.92	206	.13	5	2.96	.01	.39	1	1
L111+50N 84+00E	3	36	6	119	.1	54	12	599	4.01	5	5	ND	3	41	1	2	2	64	.47	.032	11	64	1.07	137	.15	9	2.66	.01	.35	1	2
L111+50N 84+25E	2	19	3	137	.2	30	8	977	2.55	2	5	ND	3	32	1	3	3	38	.40	.036	6	36	.61	142	.09	3	1.68	.01	.26	2	4
L111+50N 84+50E	3	42	5	157	.1	55	13	899	3.77	8	5	ND	3	42	1	2	2	59	.45	.051	10	62	.97	171	.13	10	2.44	.01	.31	1	5
L111+50N 84+75E	2	34	2	135	.1	42	11	1030	3.25	10	5	ND	3	45	1	2	6	49	.47	.049	9	45	.76	209	.11	6	2.15	.01	.36	1	2
L111+50N 85+00E	3	49	6	131	.1	67	15	1061	4.07	8	5	ND	4	52	1	2	2	58	.71	.052	14	63	1.05	230	.12	5	2.58	.02	.36	1	1
L111+50N 85+50E	2	44	4	142	.1	74	15	1535	3.58	5	5	ND	4	63	1	2	2	48	.83	.058	13	79	.94	343	.14	8	2.41	.01	.44	1	1
L111+50N 85+75E	2	33	6	170	.1	47	11	1350	3.22	4	5	ND	4	48	1	2	2	44	.62	.060	9	50	.72	278	.12	6	2.23	.02	.40	1	1
L111+50N 86+00E	3	30	6	138	.1	48	13	1437	3.33	5	5	ND	3	46	1	2	2	48	.59	.048	9	53	.74	234	.13	4	2.22	.02	.29	1	6
L111+50N 86+25E	2	42	7	155	.1	47	12	1522	3.25	5	5	ND	2	63	1	2	2	46	.68	.090	10	49	.74	283	.11	11	2.18	.02	.41	1	5
L111+50N 86+50E	2	40	8	126	.1	54	14	1595	3.42	5	5	ND	3	50	1	2	3	49	.63	.085	12	55	.83	280	.12	6	2.58	.01	.41	1	1
L111N 82+25E	2	22	5	185	.2	31	7	705	2.72	6	5	ND	3	35	1	2	2	41	.46	.045	7	38	.60	178	.10	3	1.65	.01	.24	1	1
L111N 82+50E	2	22	6	156	.1	33	8	994	2.51	2	5	ND	2	40	1	2	2	35	.49	.033	7	35	.58	189	.09	4	1.81	.02	.22	1	6
L111N 82+75E	2	16	5	110	.1	26	8	678	2.50	2	5	ND	2	26	1	2	2	41	.38	.024	4	32	.59	104	.09	3	1.40	.01	.29	1	2
L111N 83+00E	2	27	7	330	.1	41	10	1224	3.21	3	5	ND	3	40	1	2	2	43	.51	.079	8	43	.76	207	.09	6	2.10	.01	.39	1	1
L111N 83+25E	2	24	5	121	.1	36	10	532	3.10	3	5	ND	2	31	1	2	2	50	.42	.027	7	43	.79	129	.11	2	2.02	.01	.18	1	1
L111N 83+50E	2	28	5	150	.1	44	11	972	3.26	11	5	ND	2	39	1	2	2	49	.51	.053	9	53	.86	179	.11	4	1.95	.03	.29	1	3
L111N 83+75E	2	23	5	305	.1	37	8	1516	2.47	2	5	ND	2	40	2	2	2	35	.42	.104	7	36	.51	274	.08	7	1.74	.01	.30	1	1
L111N 84+00E	3	20	7	117	.1	32	9	791	3.09	2	5	ND	2	25	1	2	2	50	.41	.023	6	39	.82	112	.12	2	1.79	.01	.16	1	1
L111N 84+25E	3	25	10	136	.1	34	10	1184	2.90	4	5	ND	2	38	1	2	2	45	.48	.029	7	38	.74	196	.10	7	1.86	.01	.23	2	1
L111N 84+50E	1	34	6	165	.4	26	6	987	1.39	5	5	ND	1	521	2	2	2	21	10.98	.188	3	21	.42	69	.04	12	.86	.02	.20	1	2
L111N 84+75E	3	37	6	200	.1	43	12	1298	3.22	5	5	ND	3	51	1	2	3	45	.59	.038	9	43	.72	221	.10	3	2.17	.02	.24	1	3
L111N 85+00E	3	39	7	194	.1	44	11	1078	2.97	6	5	ND	2	52	1	2	2	40	.54	.079	10	38	.65	236	.09	7	2.22	.02	.26	1	1
L111N 85+25E	3	39	6	153	.1	62	13	981	3.46	2	5	ND	4	47	1	2	3	51	.59	.041	11	57	.91	193	.11	3	2.19	.01	.27	1	1
STD C/AU-S	20	63	41	131	7.5	72	30	1070	4.03	39	25	8	40	53	19	17	22	59	.49	.091	42	61	.95	180	.07	31	1.90	.05	.16	14	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L111N 85+50E	3	64	11	142	.3	79	16	730	4.49	17	5	ND	4	53	1	2	2	76	1.01	.047	13	67	1.41	122	.13	4	2.52	.03	.25	2	2
L111N 85+75E	3	51	6	154	.3	55	13	1228	3.51	14	5	ND	3	58	1	2	2	56	1.28	.063	9	53	1.00	180	.09	8	2.09	.01	.26	1	1
L111N 86+00E	1	26	5	132	.2	37	12	1142	3.43	5	5	ND	3	46	1	2	2	57	.59	.043	9	46	.77	201	.12	5	2.23	.03	.35	2	1
L111N 86+25E	1	38	9	158	.1	35	11	1335	3.48	8	5	ND	2	43	1	3	2	52	.59	.059	8	37	.75	207	.11	9	2.17	.02	.32	1	1
L111N 86+50E	2	28	7	111	.1	35	10	1378	3.09	3	5	ND	2	43	1	2	3	50	.50	.027	7	37	.72	203	.11	7	2.16	.02	.23	1	2
L111N 86+75E	1	32	6	140	.2	38	11	1652	3.13	3	5	ND	3	49	1	2	2	48	.66	.043	9	39	.78	269	.11	6	2.13	.04	.30	1	1
L111N 87+00E	2	26	8	125	.3	37	12	1581	3.05	7	5	ND	3	42	1	2	2	50	.56	.048	8	39	.69	234	.11	4	1.97	.04	.23	1	2
L110+50N 82+25E	2	16	6	155	.2	21	7	749	2.26	2	5	ND	2	30	1	2	2	38	.39	.040	4	30	.48	134	.09	7	1.32	.01	.19	1	1
L110+50N 82+50E	1	21	5	182	.1	32	8	981	2.52	4	5	ND	2	36	1	3	3	39	.41	.041	6	34	.54	219	.09	7	1.78	.02	.22	2	1
L110+50N 82+75E	1	21	6	208	.3	32	8	1139	2.51	2	5	ND	3	38	1	2	2	39	.41	.041	6	33	.49	256	.10	9	1.86	.02	.26	1	1
L110+50N 83+00E	2	28	6	233	.1	38	10	1115	3.27	3	5	ND	2	41	1	2	3	52	.63	.048	8	43	.74	215	.11	8	2.09	.01	.24	1	3
L110+50N 83+25E	2	31	6	169	.2	44	10	761	3.44	8	5	ND	3	40	1	2	2	55	.50	.041	9	53	.92	175	.10	5	2.02	.01	.27	1	6
L110+50N 83+50E	2	23	8	175	.2	31	9	814	3.05	5	5	ND	2	32	1	2	2	52	.41	.029	6	40	.78	143	.10	5	1.73	.02	.21	1	3
L110+50N 83+75E	2	34	5	147	.3	53	12	642	3.45	11	5	ND	3	46	1	2	3	56	.55	.052	11	56	.91	163	.12	4	2.25	.02	.25	1	5
L110+50N 84+00E	2	27	6	187	.1	33	9	1170	2.80	3	5	ND	3	45	1	2	2	44	.51	.043	8	38	.60	211	.10	5	1.85	.01	.25	1	4
L110+50N 84+25E	2	26	6	191	.1	31	9	1184	2.76	3	5	ND	2	40	1	2	4	44	.63	.044	7	37	.58	216	.11	7	1.83	.02	.26	1	1
L110+50N 84+50E	2	26	9	183	.1	35	9	1106	2.94	6	5	ND	2	45	1	2	2	47	.50	.041	8	39	.62	206	.11	7	2.00	.01	.25	1	1
L110+50N 84+75E	2	26	4	183	.1	39	10	1092	2.94	5	5	ND	2	40	1	2	2	46	.42	.046	8	40	.64	198	.11	10	2.08	.01	.25	1	2
L110+50N 85+00E	2	33	5	250	.1	37	9	1070	2.84	6	5	ND	2	46	1	2	2	45	.45	.062	7	39	.66	223	.10	5	1.75	.01	.23	1	1
L110+50N 85+25E	2	27	8	165	.1	40	11	1180	3.13	6	5	ND	2	43	1	2	3	52	.49	.041	7	46	.76	186	.10	5	2.05	.01	.18	1	1
L110+50N 85+50E	2	36	6	199	.2	48	12	946	3.66	8	5	ND	3	52	1	2	3	56	.48	.060	10	52	.86	232	.12	8	2.43	.02	.33	1	2
L110+50N 85+75E	3	31	7	132	.1	51	12	605	3.95	12	5	ND	3	45	1	2	2	64	.52	.026	9	60	.96	186	.12	7	2.42	.01	.24	1	3
L110+50N 86+00E	1	8	2	17	.2	4	1	40	.20	4	5	ND	1	1302	1	2	5	2	16.72	.060	2	2	.26	16	.01	8	.09	.01	.02	1	1
L110+50N 86+25E	1	23	7	198	.1	32	10	850	2.67	3	5	ND	2	84	1	2	2	43	.86	.033	5	34	.65	122	.10	5	1.78	.01	.27	1	1
L110+50N 86+50E	1	26	5	178	.1	38	12	1145	3.08	5	5	ND	3	50	1	2	2	46	.50	.092	8	38	.70	225	.10	5	2.12	.01	.26	1	1
L110+50N 86+75E	1	17	4	121	.1	27	8	658	2.35	6	5	ND	2	26	1	2	2	39	.33	.022	5	30	.51	128	.09	2	1.76	.01	.13	1	1
L110+50N 87+00E	2	28	5	112	.1	40	11	649	3.27	11	5	ND	3	40	1	2	2	54	.56	.042	8	43	.78	126	.11	4	2.06	.01	.39	1	2
L110+50N 87+25E	2	39	5	153	.3	40	12	1074	3.53	9	5	ND	3	56	1	2	2	56	.68	.038	8	42	.82	166	.11	10	2.11	.03	.26	1	2
L110N 82+75E	2	25	9	138	.3	34	9	940	2.82	8	5	ND	3	45	1	2	2	46	.65	.025	7	39	.68	159	.09	4	1.56	.01	.20	1	1
L110N 83+00E	2	26	9	197	.2	32	9	1272	2.53	4	5	ND	2	63	1	2	2	40	.77	.055	6	35	.56	193	.08	7	1.73	.01	.21	2	1
L110N 83+25E	2	25	7	168	.1	30	8	1082	2.42	5	5	ND	1	254	1	2	2	37	3.53	.061	4	33	.58	61	.08	6	1.69	.03	.20	1	1
L110N 83+50E	2	25	4	172	.1	39	11	745	3.22	5	5	ND	2	41	1	2	2	55	.50	.033	8	47	.74	158	.12	5	2.04	.02	.21	1	1
L110N 83+75E	2	29	6	160	.1	42	10	933	3.05	8	5	ND	2	57	1	2	2	50	.73	.046	8	50	.76	172	.10	9	1.92	.01	.24	1	1
L110N 84+00E	2	37	9	143	.1	56	11	544	3.78	8	5	ND	2	35	1	2	2	60	.47	.047	11	59	.97	167	.11	3	2.52	.01	.26	1	1
L110N 84+25E	2	19	5	181	.1	24	7	1177	2.32	2	5	ND	2	36	1	2	2	39	.46	.039	5	29	.50	177	.09	8	1.43	.01	.22	1	1
L110N 84+50E	2	29	6	172	.1	44	11	907	3.41	13	5	ND	3	45	1	2	4	53	.56	.056	9	51	.84	213	.12	7	2.26	.02	.33	1	1
STD C/AU-S	19	61	38	129	7.0	69	29	1047	4.03	42	19	7	38	52	18	16	17	63	.49	.089	40	59	.94	176	.07	30	1.81	.06	.14	12	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L110N 84+75E	2	24	5	156	.1	36	10	1053	2.76	4	5	ND	2	34	1	3	2	46	.37	.035	7	39	.65	184	.11	2	1.79	.03	.21	2	3
L110N 85+00E	2	21	2	151	.1	29	9	1063	2.44	2	5	ND	2	32	1	2	2	39	.35	.033	5	33	.61	150	.09	2	1.63	.03	.16	1	1
L110N 85+25E	2	41	5	182	.1	47	13	1088	3.24	6	5	ND	2	58	1	2	2	52	.68	.080	8	48	.87	195	.09	5	1.85	.01	.20	1	1
L110N 85+50E	6	57	9	204	.3	51	14	673	4.16	13	5	ND	3	43	1	2	2	55	.45	.034	12	42	1.22	144	.07	4	2.18	.02	.22	1	1
L110N 85+75E	2	33	4	367	.1	31	12	893	2.68	5	5	ND	2	104	1	2	2	41	.44	.039	7	31	.73	118	.08	3	1.41	.02	.12	1	1
L110N 86+00E	2	31	4	143	.1	42	11	1149	2.87	4	5	ND	3	51	1	2	3	49	.45	.033	7	49	.68	210	.13	3	1.80	.01	.20	1	1
L110N 86+25E	3	45	7	137	.2	52	14	721	4.14	8	5	ND	3	39	1	2	2	66	.53	.030	11	54	1.05	119	.11	3	2.29	.02	.23	1	1
L110N 86+50E	2	54	3	181	.2	46	14	1450	3.72	6	5	ND	2	82	1	2	2	54	1.02	.119	9	45	1.09	215	.08	7	2.04	.02	.24	1	1
L110N 86+75E	2	32	5	263	.1	26	9	2526	2.32	2	5	ND	2	70	2	2	3	35	.65	.067	6	25	.45	310	.07	4	1.49	.02	.23	1	1
L110N 87+00E	3	50	3	234	.3	52	15	895	3.90	6	5	ND	3	82	1	2	2	62	.66	.037	13	49	.87	272	.14	2	2.76	.03	.22	1	1
L110N 87+25E	1	27	2	35	.3	13	4	156	.69	4	5	ND	1	519	1	3	2	10	20.51	.032	2	7	.43	62	.01	4	.38	.02	.02	1	1
L110N 87+50E	1	40	2	42	.4	16	6	251	1.31	2	5	ND	1	467	1	2	2	15	17.50	.046	3	4	.56	56	.01	16	.66	.01	.10	1	1
L110N 87+75E	1	36	3	277	.2	26	9	1751	2.31	2	5	ND	1	96	1	2	2	36	1.08	.109	5	27	.45	231	.08	6	1.55	.01	.23	1	1
L109+50N 83+00E	2	28	3	162	.1	42	10	644	3.30	6	5	ND	2	36	1	2	2	60	.47	.028	9	50	.91	136	.12	5	1.80	.02	.22	1	2
L109+50N 83+25E	6	77	9	283	.1	61	12	537	3.97	13	5	ND	2	40	1	4	3	54	.57	.061	17	37	1.06	103	.10	2	1.92	.02	.18	1	1
L109+50N 83+50E	2	31	4	219	.2	39	10	737	3.18	2	5	ND	3	50	1	2	2	57	.69	.050	10	39	.65	240	.14	6	2.26	.03	.19	1	1
L109+50N 83+75E	2	23	4	172	.2	33	8	763	2.83	2	5	ND	3	37	1	2	2	48	.48	.028	7	39	.63	194	.12	2	1.95	.03	.15	1	1
L109+50N 84+00E	2	28	4	210	.1	32	8	816	2.76	3	5	ND	2	37	1	2	3	45	.45	.039	7	40	.59	195	.11	3	1.88	.01	.20	2	1
L109+50N 84+25E	2	30	7	174	.1	40	11	1158	3.16	3	5	ND	3	43	1	2	2	52	.60	.058	8	45	.80	190	.10	8	1.79	.02	.33	1	1
L109+50N 84+50E	2	29	4	186	.1	33	10	999	2.85	5	5	ND	1	31	1	2	2	48	.41	.034	6	37	.68	159	.10	4	1.67	.01	.17	1	1
L109+50N 84+75E	2	25	4	152	.2	29	9	777	2.83	4	5	ND	2	45	1	2	2	48	.39	.044	6	37	.64	171	.12	4	1.73	.02	.22	2	1
L109+50N 85+00E	2	30	4	134	.2	42	11	629	3.53	2	5	ND	2	35	1	2	2	60	.43	.027	4	48	.96	143	.10	4	2.07	.02	.26	1	1
L109+50N 85+25E	2	40	4	154	.1	51	13	676	3.76	5	5	ND	2	40	1	2	2	64	.43	.044	10	54	.98	152	.11	6	2.28	.01	.31	1	1
L109+50N 85+50E	2	32	6	186	.1	32	9	718	3.04	7	5	ND	2	57	1	2	2	49	.52	.050	7	36	.67	115	.11	8	1.70	.01	.27	1	4
L109+50N 85+75E	1	4	2	11	.1	4	1	67	.10	5	5	ND	1	1549	1	2	3	2	22.42	.047	2	2	.33	17	.01	11	.07	.01	.03	1	1
L109+50N 86+00E	2	46	3	137	.1	87	16	499	4.40	12	5	ND	3	83	1	2	2	77	.92	.023	12	85	1.23	93	.16	3	2.53	.03	.34	1	1
L109+50N 86+25E	1	26	3	253	.2	30	8	592	2.64	2	5	ND	1	53	1	2	2	45	.45	.034	6	39	.56	116	.12	6	1.49	.01	.27	1	1
L109+50N 86+50E	2	53	2	140	.1	59	15	569	4.24	10	5	ND	2	38	1	3	2	74	.44	.033	11	62	1.11	98	.13	3	2.32	.01	.23	1	1
L109+50N 87+00E	1	41	6	338	.2	38	11	1297	2.93	7	5	ND	3	62	2	2	2	45	.54	.105	8	39	.69	308	.11	7	1.94	.02	.30	1	1
L109+50N 87+25E	2	27	5	184	.1	32	11	1544	2.83	2	5	ND	1	55	1	2	2	44	.53	.044	8	34	.61	224	.11	6	1.93	.03	.27	1	1
L109+50N 87+50E	2	26	7	111	.2	30	11	1010	2.98	3	5	ND	1	52	1	2	2	55	.47	.020	7	34	.68	118	.12	7	1.78	.01	.24	1	1
L109+50N 87+75E	2	29	7	146	.1	34	11	999	3.40	5	5	ND	2	48	1	2	2	54	.51	.036	9	38	.78	160	.12	7	2.18	.03	.26	1	1
L109+50N 88+00E	1	31	5	163	.1	45	13	1195	3.41	8	5	ND	2	47	1	2	2	56	.61	.060	11	50	.72	269	.13	3	2.62	.02	.25	1	1
L109N 83+50E	2	36	9	145	.1	61	13	665	3.85	6	5	ND	2	45	1	2	4	62	.63	.050	12	67	1.01	189	.14	3	2.49	.02	.33	1	1
L109N 83+75E	2	26	7	165	.1	40	9	588	3.28	7	5	ND	1	38	1	2	2	52	.46	.037	9	46	.76	182	.13	6	2.29	.02	.25	2	1
L109N 84+00E	2	37	5	224	.1	48	11	1145	3.49	5	5	ND	2	53	2	3	2	54	.70	.059	9	51	.85	263	.09	9	2.09	.01	.34	1	2
STD C/AU-S	19	62	36	132	7.2	72	30	1064	4.07	42	19	7	40	53	19	17	21	61	.50	.090	42	61	.96	181	.07	30	1.86	.07	.13	14	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L109N 84+25E	1	15	6	333	.2	24	7	347	2.50	2	6	ND	3	38	3	2	2	42	.43	.024	6	31	.46	100	.12	2	1.73	.05	.21	1	1
L109N 84+50E	1	38	5	170	.2	37	12	563	3.84	2	8	ND	4	42	1	2	2	62	.58	.031	10	42	.94	89	.14	5	2.03	.03	.44	1	1
L109N 84+75E	2	55	4	164	.4	64	16	606	4.61	2	6	ND	3	43	1	2	2	78	.80	.027	15	60	1.20	116	.12	2	2.53	.02	.47	1	1
L109N 85+00E	2	53	9	133	.2	47	14	391	4.70	2	5	ND	4	51	1	3	2	87	.62	.017	14	48	1.03	90	.16	2	2.47	.04	.53	1	1
L109N 85+25E	2	29	3	159	.3	32	9	596	3.22	2	5	ND	3	44	1	3	3	57	.51	.051	8	36	.75	180	.13	6	2.04	.04	.36	2	1
L109N 85+50E	1	32	4	251	.3	37	9	1445	2.73	3	5	ND	3	89	1	2	2	43	.99	.145	8	38	.57	344	.09	12	1.78	.02	.44	1	1
L109N 85+75E	2	81	8	147	.2	55	17	635	4.68	13	5	ND	3	57	1	3	2	90	.86	.073	14	49	1.41	119	.14	2	2.45	.01	.20	2	2
L109N 86+00E	3	53	4	152	.3	73	14	598	4.43	8	8	ND	4	39	1	2	2	75	.53	.052	13	73	1.26	141	.10	2	2.54	.04	.34	1	1
L109N 86+25E	2	35	6	161	.2	49	13	1062	3.56	3	5	ND	3	45	1	2	2	58	.57	.041	31	52	.90	187	.11	2	2.19	.07	.40	1	1
L109N 86+50E	2	41	6	198	.2	50	14	1120	3.52	2	5	ND	2	59	1	2	2	55	.72	.095	13	46	.89	235	.10	2	2.42	.03	.26	1	1
L109N 86+75E	2	35	6	205	.1	44	12	1391	3.13	2	5	ND	2	50	1	2	3	48	.63	.092	9	40	.67	271	.10	5	2.05	.03	.33	1	1
L109N 87+00E	2	47	8	174	.3	63	16	788	3.80	3	6	ND	3	57	1	2	2	61	.64	.068	12	59	.99	238	.13	2	2.55	.03	.27	1	3
L109N 87+25E	2	30	6	134	.1	42	13	778	3.74	2	5	ND	1	49	1	2	2	58	.60	.054	11	49	.86	157	.13	2	2.52	.02	.37	1	1
L109N 87+50E	2	29	4	208	.3	35	11	1106	3.11	2	5	ND	3	57	1	2	4	46	.61	.042	7	38	.67	200	.11	6	2.09	.03	.38	1	1
L109N 87+75E	2	35	7	143	.1	58	15	537	4.06	3	6	ND	3	49	1	2	2	69	.55	.034	12	63	.94	172	.16	2	2.89	.03	.33	1	1
L109N 88+00E	2	30	4	138	.3	37	12	981	3.09	2	5	ND	3	57	1	3	2	48	.60	.025	8	45	.66	192	.12	4	2.14	.05	.45	1	1
L109N 88+25E	2	30	3	131	.1	44	13	795	3.63	2	5	ND	1	49	1	2	3	59	.51	.030	10	54	.78	165	.14	2	2.48	.03	.39	1	1
L109N 88+50E	1	33	6	247	.1	34	10	1950	2.70	2	5	ND	1	50	1	2	3	39	.77	.071	8	34	.58	292	.09	7	1.86	.04	.33	1	1
L108+50N 83+75E	2	27	3	212	.2	33	9	639	3.09	2	6	ND	2	42	1	2	2	47	.54	.042	7	40	.71	160	.08	8	1.75	.01	.28	1	1
L108+50N 84+00E	3	32	9	166	.1	39	12	392	3.83	2	5	ND	3	32	1	3	3	69	.38	.032	9	39	1.01	96	.12	2	2.06	.01	.24	1	1
L108+50N 84+25E	3	39	9	194	.3	43	10	1337	2.87	7	5	ND	1	90	2	3	2	45	2.57	.044	8	38	.81	198	.08	6	1.64	.01	.18	2	1
L108+50N 84+50E	3	59	8	170	.4	67	16	627	4.46	6	5	ND	3	46	1	3	2	76	.82	.052	14	62	1.26	200	.12	2	2.79	.02	.28	1	2
L108+50N 84+75E	4	82	9	184	.3	102	19	853	4.91	10	5	ND	3	40	1	2	2	81	.64	.058	15	86	1.69	136	.09	5	2.78	.03	.21	1	1
L108+50N 85+00E	3	73	8	162	.3	90	17	755	4.29	15	5	ND	2	71	1	2	2	72	2.44	.064	11	77	1.58	131	.08	2	2.41	.04	.20	1	1
L108+50N 85+25E	2	39	6	179	.4	55	14	1490	3.32	2	6	ND	2	64	1	3	3	50	.99	.096	11	51	.77	412	.09	2	2.16	.02	.38	1	1
L108+50N 85+50E	2	33	4	145	.1	55	13	832	3.40	2	5	ND	2	41	1	2	4	54	.53	.042	11	53	.85	231	.12	2	2.56	.01	.31	2	1
L108+50N 85+75E	2	32	8	157	.1	45	12	1126	3.18	3	5	ND	1	40	1	2	3	50	.54	.042	9	51	.77	196	.11	2	2.09	.01	.32	2	1
L108+50N 86+00E	2	44	6	234	.1	45	12	1269	3.14	3	5	ND	1	67	1	2	2	45	.76	.123	8	45	.77	294	.08	2	1.96	.01	.33	1	1
L108+50N 86+25E	2	29	6	165	.1	41	12	1128	3.12	2	5	ND	1	38	1	2	2	49	.58	.048	10	46	.72	187	.11	2	2.00	.04	.39	1	1
L108+50N 86+50E	2	33	4	210	.1	40	12	1452	3.08	5	5	ND	2	44	1	2	2	46	.51	.096	8	45	.68	243	.10	2	2.11	.03	.35	1	1
L108+50N 86+75E	2	32	7	150	.1	51	14	877	3.77	2	5	ND	3	44	1	2	3	56	.55	.050	11	61	.88	207	.13	2	2.48	.05	.39	1	1
L108+50N 87+00E	2	31	5	163	.1	49	12	1022	3.64	3	5	ND	2	42	1	2	2	53	.55	.039	10	61	.80	246	.12	2	2.40	.01	.32	2	1
L108+50N 87+25E	2	28	8	160	.1	40	11	1163	3.02	2	5	ND	1	44	1	2	2	47	.54	.029	8	43	.67	218	.11	4	2.10	.01	.29	1	1
L108+50N 87+50E	1	30	6	149	.1	41	12	1004	3.37	2	5	ND	2	40	1	2	2	52	.51	.058	11	46	.70	226	.12	2	2.61	.03	.33	1	1
L108+50N 87+75E	1	36	7	144	.1	42	14	1315	3.68	4	5	ND	1	52	1	2	2	54	.64	.035	10	46	.89	216	.11	2	2.41	.02	.40	1	2
L108+50N 88+00E	1	33	7	159	.1	50	13	781	3.91	2	5	ND	2	42	1	2	2	56	.59	.062	11	59	.87	196	.12	2	2.97	.03	.37	1	1
STD C/AU-S	19	61	42	131	7.2	71	31	1044	4.00	41	18	7	39	53	18	17	21	64	.49	.089	41	61	.95	179	.07	32	1.85	.08	.13	15	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L108+50N 88+25E	2	37	9	168	.2	43	12	967	3.30	5	5	ND	2	38	1	2	2	49	.54	.031	11	43	.71	190	.11	2	2.43	.01	.27	1	4
L108+50N 88+50E	3	58	9	133	.1	72	15	781	4.39	5	5	ND	2	33	1	3	2	67	.60	.064	10	59	1.16	126	.07	3	2.56	.01	.44	1	7
L108+50N 88+75E	2	58	10	131	.3	60	16	974	4.14	2	8	ND	3	41	1	2	2	62	.68	.063	11	57	1.12	165	.09	3	2.61	.01	.40	1	1
L108N 84+25E	1	39	9	196	.1	47	12	568	3.27	2	5	ND	2	43	1	2	2	53	.49	.069	12	42	.76	249	.12	3	2.53	.01	.28	1	1
L108N 84+50E	2	27	9	150	.1	39	10	683	3.01	4	5	ND	3	40	1	2	2	47	.52	.058	9	36	.67	162	.10	5	1.95	.03	.30	1	2
L108N 84+75E	2	29	7	197	.2	37	9	1314	2.61	2	5	ND	2	48	1	3	2	42	.60	.046	8	33	.61	253	.09	4	1.86	.03	.21	1	9
L108N 85+00E	1	33	6	238	.1	37	11	1486	3.00	3	5	ND	1	47	1	2	2	45	.49	.127	7	38	.68	320	.09	5	2.04	.03	.32	1	1
L108N 85+25E	2	24	9	167	.1	27	7	1170	2.22	2	5	ND	2	33	1	3	2	35	.42	.040	5	29	.49	186	.08	4	1.56	.01	.22	1	1
L108N 85+50E	2	22	7	123	.1	32	9	794	2.61	2	5	ND	1	29	1	2	2	45	.33	.021	5	35	.60	131	.10	2	1.63	.01	.19	1	2
L108N 85+75E	2	26	8	158	.1	35	9	987	2.64	4	5	ND	1	32	1	2	2	42	.37	.043	6	33	.59	180	.10	8	1.83	.01	.25	2	2
L108N 86+00E	1	31	8	154	.1	44	12	1078	3.06	2	5	ND	2	41	1	2	2	48	.48	.064	10	44	.74	202	.10	4	2.07	.02	.30	1	1
L108N 86+25E	1	30	10	218	.1	39	11	922	2.93	5	5	ND	2	43	1	3	2	45	.48	.057	8	40	.65	178	.10	5	2.12	.01	.31	1	1
L108N 86+50E	2	32	7	146	.1	50	12	805	3.56	4	5	ND	2	38	1	2	2	56	.48	.032	9	57	1.00	186	.11	4	2.28	.01	.33	2	1
L108N 86+75E	1	31	7	156	.1	45	12	1076	3.21	2	5	ND	3	43	1	2	2	51	.49	.067	9	44	.74	224	.31	2	2.43	.01	.28	1	1
L108N 87+00E	3	40	6	136	.1	56	14	778	4.09	5	5	ND	2	41	1	2	3	63	.61	.025	11	62	1.08	166	.10	4	2.45	.01	.34	1	1
L108N 87+25E	2	36	8	146	.1	49	12	907	3.59	5	5	ND	2	46	1	2	2	54	.59	.039	11	51	.83	214	.12	3	2.49	.02	.41	1	2
L108N 87+50E	2	55	9	120	.1	65	15	743	3.95	6	5	ND	1	39	1	2	2	68	.52	.028	13	57	1.12	130	.12	2	2.27	.03	.19	1	1
L108N 87+75E	1	37	8	187	.1	41	12	844	3.33	2	5	ND	2	44	1	2	3	51	.54	.032	8	42	.82	156	.11	3	2.20	.03	.31	1	1
L108N 88+00E	1	34	8	138	.1	45	13	970	3.62	3	5	ND	2	43	1	2	3	54	.53	.043	10	51	.86	211	.12	6	2.49	.03	.42	1	4
L108N 88+25E	2	32	9	154	.1	40	11	881	3.47	2	5	ND	1	35	1	2	2	51	.53	.051	9	45	.78	195	.31	3	2.38	.01	.34	1	1
L108N 88+50E	1	24	9	164	.1	29	9	1165	2.29	2	5	ND	1	32	1	2	2	36	.46	.083	7	27	.45	398	.07	2	1.52	.02	.18	1	1
L108N 88+75E	1	28	7	136	.1	32	11	1145	2.91	2	5	ND	1	43	1	2	2	42	.67	.046	8	37	.62	398	.09	5	2.01	.01	.37	1	2
L108N 89+00E	1	48	6	160	.1	47	13	1388	3.57	5	5	ND	1	53	1	2	2	51	.82	.083	8	45	.91	228	.08	11	2.13	.01	.52	1	1
L108N 89+25E	1	32	8	122	.1	33	9	1278	2.44	2	5	ND	1	80	1	2	2	36	.67	.022	6	29	.57	141	.08	8	1.53	.01	.34	1	1
L107+50N 84+50E	3	32	10	194	.1	40	11	1373	3.21	5	5	ND	2	43	1	3	2	51	.59	.049	9	41	.70	246	.10	4	2.15	.01	.28	1	1
L107+50N 84+75E	2	34	8	184	.1	39	10	1059	2.92	2	5	ND	1	47	1	2	2	47	.71	.051	8	38	.69	210	.09	5	1.82	.02	.24	1	1
L107+50N 85+00E	2	29	6	357	.1	35	10	1637	2.65	2	5	ND	1	46	1	2	2	39	.58	.066	8	34	.65	256	.08	4	1.71	.01	.27	1	1
L107+50N 85+25E	1	23	6	213	.1	27	9	835	2.71	2	6	ND	2	29	1	2	3	43	.31	.048	5	30	.68	126	.10	5	1.64	.01	.21	2	1
L107+50N 85+50E	1	45	7	186	.1	53	12	1476	3.00	2	5	ND	1	53	1	2	2	46	.61	.087	8	46	.94	173	.07	7	1.84	.01	.27	1	3
L107+50N 85+75E	2	38	11	170	.1	44	11	1104	3.05	5	5	ND	1	46	1	2	2	48	.58	.064	8	46	.74	192	.09	6	1.99	.01	.28	1	5
L107+50N 86+00E	2	40	7	176	.1	47	13	1142	3.26	6	5	ND	2	42	1	2	2	52	.53	.061	11	47	.81	228	.11	5	2.33	.01	.35	1	1
L107+50N 86+25E	2	40	6	159	.1	50	12	1007	3.48	4	5	ND	1	40	1	2	2	55	.53	.078	9	57	.92	220	.10	5	2.06	.01	.35	1	1
L107+50N 86+50E	2	37	9	160	.1	49	13	1239	3.48	4	5	ND	1	42	1	2	2	56	.59	.040	11	56	.85	237	.12	4	2.28	.01	.30	1	1
L107+50N 86+75E	2	42	6	146	.1	58	14	620	3.81	5	5	ND	2	44	1	2	4	64	.52	.059	13	61	.94	193	.13	2	2.82	.02	.25	1	2
L107+50N 87+00E	2	36	6	219	.1	39	11	1219	3.14	2	5	ND	2	45	1	2	2	47	.57	.055	9	42	.69	266	.11	4	2.13	.02	.35	1	1
L107+50N 87+25E	2	47	7	150	.1	55	15	993	3.72	6	5	ND	2	48	1	2	4	61	.62	.066	12	56	.93	219	.12	5	2.50	.01	.44	1	1
STD C/AU-S	18	60	44	127	6.8	70	29	1038	3.92	40	22	7	38	50	18	17	18	64	.48	.088	40	60	.92	172	.07	34	1.79	.06	.14	14	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L107+50N 87+50E	3	35	6	158	.1	45	13	1030	3.79	2	5	ND	2	42	1	2	2	51	.65	.042	10	53	.90	155	.11	2	2.33	.01	.37	1	1
L107+50N 87+75E	2	36	5	143	.1	45	13	830	3.84	5	5	ND	2	48	1	3	2	53	.65	.043	11	55	.91	181	.12	2	2.73	.01	.35	2	1
L107+50N 88+00E	2	41	6	146	.1	46	14	1024	3.84	2	5	ND	2	62	1	2	2	50	.90	.058	10	51	1.00	213	.11	6	2.56	.02	.46	1	1
L107+50N 88+25E	2	42	4	148	.1	49	14	972	3.93	4	5	ND	1	57	1	2	2	52	.86	.077	10	49	1.01	167	.10	4	2.48	.02	.35	1	1
L107+50N 88+50E	1	39	5	151	.2	46	13	1196	3.58	2	5	ND	1	62	1	2	2	45	.99	.082	11	53	.90	242	.10	6	2.32	.01	.50	1	2
L107+50N 88+75E	2	40	3	142	.1	50	13	1137	3.81	5	5	ND	1	58	1	2	2	50	.86	.069	11	54	.99	218	.11	3	2.51	.01	.43	1	1
L107+50N 89+00E	2	50	3	143	.1	48	14	1182	4.00	4	5	ND	1	65	1	2	2	53	1.04	.088	10	51	1.15	171	.09	8	2.38	.01	.45	1	1
L107+50N 89+25E	1	37	4	127	.2	48	13	1174	3.54	2	5	ND	2	74	1	2	3	47	.91	.071	10	54	.93	210	.11	5	2.34	.01	.48	1	1
L107+50N 89+50E	2	56	4	117	.1	51	14	1032	3.82	3	5	ND	1	112	1	2	2	54	1.35	.057	10	50	1.13	123	.11	9	2.22	.02	.38	1	1
L107N 85+00E	2	27	8	104	.1	38	11	954	3.23	5	5	ND	2	36	1	2	2	46	.42	.052	8	42	.73	208	.12	2	2.24	.01	.21	1	1
L107N 85+25E	2	27	6	150	.3	39	10	829	3.22	2	5	ND	3	38	1	2	2	45	.40	.056	10	43	.78	207	.11	2	2.18	.01	.28	1	1
L107N 85+50E	1	35	4	193	.1	34	8	1336	2.62	2	5	ND	2	53	1	2	3	38	.52	.077	7	36	.58	244	.09	2	1.76	.01	.31	1	1
L107N 85+75E	2	41	5	270	.2	47	14	1035	3.52	7	5	ND	4	62	2	2	2	47	.65	.138	12	42	.89	220	.11	3	2.21	.01	.35	1	2
L107N 86+00E	2	40	6	273	.2	45	12	805	3.47	2	6	ND	2	37	1	2	2	49	.48	.053	11	44	.89	189	.11	4	2.17	.01	.28	1	1
L107N 86+25E	3	51	7	190	.1	55	13	799	3.94	8	5	ND	2	51	1	2	2	54	.77	.088	14	48	1.01	191	.12	2	2.11	.01	.27	2	1
L107N 86+50E	2	44	6	159	.2	50	14	1104	3.73	3	5	ND	2	49	1	2	2	53	.76	.058	12	49	.93	249	.13	2	2.24	.02	.33	1	1
L107N 86+75E	2	50	7	180	.2	60	15	1276	4.02	7	5	ND	2	64	1	2	2	55	.87	.134	12	64	1.04	326	.10	4	2.48	.01	.38	1	1
L107N 87+00E	2	47	6	207	.1	50	13	1536	3.51	3	5	ND	2	55	1	2	2	48	.73	.091	10	53	.89	331	.10	5	2.20	.02	.38	1	1
L107N 87+25E	2	40	5	138	.1	49	13	1122	3.53	2	5	ND	2	39	1	2	2	49	.56	.029	11	56	.89	193	.12	2	2.30	.02	.26	1	1
L107N 87+50E	3	45	9	186	.1	52	14	1108	3.76	6	5	ND	2	56	1	3	2	52	.68	.065	11	61	.93	243	.11	2	2.33	.02	.31	1	1
L107N 87+75E	1	46	6	151	.1	50	13	1251	3.33	2	5	ND	1	62	1	2	2	47	1.01	.070	11	48	.81	226	.10	2	2.13	.04	.34	1	2
L107N 88+00E	2	42	5	182	.1	44	13	1534	3.29	2	5	ND	1	63	1	2	2	45	.95	.075	10	45	.79	242	.09	5	2.16	.01	.37	1	1
L107N 88+25E	2	47	8	159	.1	44	13	1377	3.37	6	5	ND	1	84	1	2	2	45	1.28	.098	10	45	.82	257	.08	8	2.28	.03	.40	1	1
L107N 88+50E	2	51	5	132	.1	55	14	1072	4.00	2	5	ND	1	55	1	2	2	56	.91	.058	11	52	1.18	163	.10	3	2.46	.02	.32	1	1
L107N 88+75E	2	53	5	167	.1	51	13	1097	3.65	2	5	ND	1	103	1	2	2	52	2.30	.083	9	47	1.12	188	.09	5	2.22	.01	.31	1	1
L107N 89+00E	2	29	5	213	.1	28	10	1644	2.46	2	5	ND	2	62	1	2	2	33	.72	.052	6	29	.54	193	.07	2	1.63	.02	.23	1	1
L107N 89+25E	2	22	5	113	.1	29	11	966	2.98	2	5	ND	1	43	1	2	2	46	.55	.019	8	39	.64	101	.12	2	1.89	.03	.27	1	1
L107N 89+50E	1	3	2	4	.1	2	1	29	.09	3	5	ND	1	588	1	2	2	1	21.01	.010	2	2	.08	5	.01	2	.05	.01	.04	1	1
L107N 89+75E	2	50	4	137	.1	45	13	1089	3.63	2	5	ND	2	133	1	2	2	48	1.96	.089	8	44	1.06	135	.09	9	2.30	.02	.43	1	1
L107N 90+00E	2	30	5	141	.1	34	11	1140	2.96	2	5	ND	2	62	1	2	2	37	.71	.037	8	35	.66	102	.08	2	1.94	.01	.31	1	1
L106+50 85+25E	1	32	3	204	.1	31	9	723	2.85	2	5	ND	2	33	1	2	2	38	.42	.041	8	34	.61	210	.11	2	2.10	.03	.26	1	1
L106+50 85+50E	2	28	6	218	.1	39	11	737	3.18	3	5	ND	3	39	1	2	2	45	.49	.042	9	40	.80	158	.12	2	2.37	.03	.25	1	1
L106+50 85+75E	2	32	4	201	.1	42	11	673	2.95	3	5	ND	2	48	1	2	2	40	.54	.105	10	35	.78	183	.10	2	2.18	.01	.24	1	1
L106+50 86+00E	2	38	5	234	.2	35	11	1101	3.39	3	5	ND	3	47	1	2	2	48	.50	.076	9	38	.83	255	.11	2	2.09	.01	.27	1	1
L106+50 86+25E	3	35	4	183	.2	46	12	848	3.51	4	5	ND	2	39	1	2	3	49	.53	.049	10	48	.90	204	.12	2	2.32	.03	.24	1	1
L106+50 86+50E	3	44	7	154	.3	54	13	917	3.57	9	5	ND	3	39	1	2	3	53	.62	.052	12	50	1.00	181	.11	2	1.92	.02	.24	1	1
STD C/AU-S	20	63	38	132	7.3	72	30	1079	4.12	41	20	8	40	53	19	16	21	59	.50	.091	41	61	.96	180	.07	33	1.88	.07	.13	14	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L106+50 86+75E	3	31	3	194	.1	39	10	1002	3.30	2	5	ND	3	32	1	2	2	47	.40	.066	9	43	.78	225	.12	2	2.14	.04	.24	1	1
L106+50 87+00E	2	39	4	186	.1	48	13	1188	3.61	5	5	ND	3	50	1	2	2	51	.66	.060	13	52	.93	262	.12	2	2.55	.03	.33	1	1
L106+50 87+25E	2	42	2	175	.2	51	14	1270	3.78	2	5	ND	2	51	1	2	2	53	.77	.053	11	59	1.02	245	.10	2	2.43	.01	.33	1	1
L106+50 87+50E	3	52	7	145	.1	74	17	1064	4.34	6	5	ND	2	46	1	2	3	62	.74	.067	12	77	1.40	137	.10	2	2.37	.04	.32	1	1
L106+50 87+75E	2	46	7	184	.2	51	15	1003	3.72	7	5	ND	4	71	1	2	2	53	.77	.067	14	52	.97	256	.12	2	2.60	.06	.37	2	1
L106+50 88+00E	2	30	6	258	.1	52	13	717	3.63	2	5	ND	3	45	1	2	2	52	.57	.080	10	52	.92	148	.12	2	2.68	.02	.20	1	1
L106+50 88+25E	2	47	5	289	.1	44	11	1301	2.75	4	5	ND	2	130	3	2	2	39	3.62	.078	7	41	.84	165	.06	18	1.66	.02	.33	1	2
L106+50 88+50E	2	39	5	178	.1	42	13	1391	3.32	5	5	ND	2	80	1	2	3	44	1.15	.063	11	43	.87	242	.09	2	2.18	.05	.38	1	2
L106+50 88+75E	2	46	6	157	.1	61	15	1095	4.04	2	5	ND	2	68	1	2	2	53	.99	.089	12	61	1.19	210	.10	5	2.58	.02	.45	1	2
L106+50 89+00E	1	49	4	176	.3	61	15	1209	4.18	2	5	ND	3	70	1	2	2	55	.91	.082	11	58	1.15	213	.09	4	2.59	.01	.55	1	1
L106+50 89+25E	2	72	3	162	.3	50	15	1174	4.06	6	5	ND	2	91	1	2	2	56	1.45	.102	9	44	1.36	177	.07	8	2.34	.03	.38	1	1
L106+50 89+50E	2	49	3	147	.1	48	15	1045	4.00	6	5	ND	1	70	1	2	2	56	.90	.071	11	47	1.13	158	.10	6	2.58	.03	.44	1	3
L106+50 89+75E	2	38	5	162	.1	40	13	1275	3.64	2	5	ND	2	77	1	2	2	51	.89	.072	11	42	.91	191	.10	2	2.31	.03	.38	1	1
L106+50 90+00E	2	40	3	127	.1	56	15	870	4.23	6	5	ND	4	46	1	2	2	63	.70	.037	12	59	1.34	129	.12	2	2.54	.02	.40	1	5
L106+50 90+25E	1	40	3	154	.2	42	12	1302	3.29	2	5	ND	2	65	1	2	2	44	1.24	.072	9	44	.83	206	.08	2	2.06	.02	.41	1	1
L106 85+75E	2	34	7	171	.2	41	13	831	3.61	2	5	ND	4	55	1	2	2	54	.63	.045	11	46	.88	210	.12	2	2.57	.02	.23	1	1
L106 86+00E	2	38	5	214	.1	41	13	911	3.54	3	7	ND	4	47	1	2	3	51	.47	.086	12	45	.85	231	.12	2	2.37	.01	.25	1	1
L106 86+25E	1	34	5	199	.2	35	11	904	3.40	2	5	ND	4	47	1	2	2	46	.56	.051	10	38	.96	185	.12	2	2.48	.01	.27	1	1
L106 86+50E	2	38	6	139	.1	49	14	965	3.82	3	5	ND	2	39	1	2	2	57	.57	.034	10	53	1.12	194	.10	2	2.36	.01	.35	1	1
L106 86+75E	2	48	4	193	.2	44	12	1273	3.37	2	5	ND	2	84	1	2	2	47	.91	.177	9	48	.86	325	.08	2	2.25	.01	.35	1	1
L106 87+00E	2	39	6	151	.1	54	14	1324	4.06	5	5	ND	2	43	1	2	2	56	.71	.042	10	59	1.11	210	.10	8	2.47	.01	.43	1	1
L106 87+25E	2	37	4	184	.1	34	9	1199	2.63	2	5	ND	3	39	1	2	2	39	.52	.084	8	34	.59	191	.08	2	1.76	.01	.16	2	1
L106 87+50E	3	48	5	136	.1	71	15	680	4.33	6	5	ND	4	42	1	2	2	66	.59	.066	14	70	1.26	141	.12	2	2.57	.01	.33	1	1
L106 87+75E	2	48	9	140	.2	59	15	1256	3.88	12	5	ND	3	65	1	3	2	58	1.14	.099	12	65	1.16	201	.08	2	2.29	.02	.33	1	1
L106 88+00E	2	46	5	155	.1	52	14	1105	3.54	4	5	ND	2	75	1	2	2	53	1.25	.091	11	55	1.01	230	.08	2	2.26	.02	.40	1	1
L106 88+25E	2	40	4	156	.1	48	14	929	3.48	7	5	ND	2	63	1	2	2	52	.97	.068	12	51	.95	224	.10	7	2.46	.02	.42	1	3
L106 88+50E	2	39	8	155	.1	46	14	1051	3.50	2	5	ND	2	59	1	3	2	51	.94	.051	12	49	.87	212	.11	2	2.46	.04	.43	1	1
L106 88+75E	2	47	6	156	.3	51	14	1160	3.71	4	5	ND	2	66	1	2	4	53	1.10	.073	11	53	1.02	189	.09	2	2.39	.01	.42	1	1
L106 89+00E	2	45	6	136	.1	48	14	1075	3.70	8	5	ND	1	77	1	2	2	53	1.14	.079	12	49	1.02	201	.10	6	2.52	.02	.39	1	2
L106 89+25E	2	43	8	132	.2	53	14	938	3.69	6	5	ND	2	60	1	3	2	52	.99	.059	13	50	1.03	163	.11	2	2.39	.02	.40	1	3
L106 89+50E	2	57	7	173	.1	46	13	1206	3.62	6	5	ND	2	90	1	2	2	48	1.18	.080	10	41	1.07	169	.08	7	2.12	.01	.36	1	2
L106 89+75E	2	42	6	160	.1	38	12	1143	3.22	2	5	ND	1	74	1	2	2	47	1.19	.055	9	38	.79	189	.10	2	2.14	.02	.28	1	1
L106 90+00E	2	47	5	197	.1	46	13	1504	3.49	4	5	ND	2	73	1	3	2	46	1.11	.074	10	43	.98	265	.08	3	2.14	.01	.43	1	1
L106 90+25E	2	72	5	157	.4	59	14	1083	3.78	16	5	ND	2	67	1	3	2	56	2.94	.125	9	49	1.25	154	.06	7	2.07	.01	.33	1	12
L106 90+50E	2	31	5	152	.1	36	13	1115	3.45	2	5	ND	2	49	1	2	2	45	.73	.039	9	42	.83	130	.09	2	2.15	.02	.39	1	1
L106 90+75E	1	41	6	141	.1	41	14	1229	3.36	6	5	ND	2	77	1	2	2	49	1.03	.072	12	42	.82	224	.11	2	2.55	.03	.33	1	2
STD C/AU-S	19	61	36	129	7.1	70	30	1057	4.00	38	20	7	39	52	19	17	20	58	.49	.088	41	59	.94	179	.07	31	1.81	.05	.14	11	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L105+50 86+00E	2	31	8	167	.1	39	12	738	3.50	11	5	ND	1	34	1	2	3	55	.44	.033	10	43	.88	170	.11	2	2.03	.04	.24	2	1
L105+50 86+25E	2	30	7	235	.1	30	10	1379	2.89	9	5	ND	1	34	1	2	2	42	.47	.060	7	32	.69	219	.08	2	1.78	.04	.28	1	1
L105+50 86+50E	2	35	8	168	.1	36	11	1169	3.11	10	5	ND	1	40	1	2	2	46	.54	.045	9	38	.76	223	.09	2	2.01	.04	.32	2	2
L105+50 86+75E	1	28	6	171	.1	26	8	1122	2.48	10	5	ND	1	30	1	2	3	37	.30	.047	6	26	.53	220	.08	2	1.62	.03	.21	1	2
L105+50 87+00E	2	41	8	169	.1	42	13	1268	3.34	9	5	ND	1	44	1	2	3	47	.73	.058	9	42	.85	238	.08	5	1.95	.02	.42	1	3
L105+50 87+25E	1	34	9	163	.2	40	12	1055	3.19	13	5	ND	1	47	1	2	3	48	.58	.069	10	43	.82	252	.09	3	2.06	.03	.37	1	2
L105+50 87+50E	1	38	7	178	.1	43	13	1180	3.37	13	5	ND	1	43	1	2	2	48	.60	.087	10	47	.90	223	.09	3	1.97	.02	.34	1	1
L105+50 87+75E	2	38	12	160	.2	36	11	1267	2.94	16	5	ND	1	55	1	2	2	44	.76	.113	9	39	.74	257	.08	6	1.83	.04	.37	1	5
L105+50 88+00E	2	46	10	166	.2	70	14	1249	3.14	16	5	ND	1	69	1	2	3	47	1.24	.102	10	63	.85	198	.06	11	1.73	.02	.42	1	1
L105+50 88+25E	1	47	8	159	.3	49	13	1021	3.28	12	5	ND	1	66	1	2	3	51	1.05	.087	10	47	.96	186	.07	5	2.13	.03	.48	2	3
L105+50 88+50E	2	47	9	135	.2	54	13	814	3.32	17	5	ND	1	66	1	2	2	53	1.04	.076	11	50	1.01	164	.08	9	1.98	.04	.39	1	1
L105+50 88+75E	2	40	11	144	.2	50	14	634	3.59	15	5	ND	1	45	1	2	3	55	.66	.038	11	51	.97	125	.10	3	2.03	.02	.56	1	1
L105+50 89+00E	1	31	9	159	.1	38	11	1064	3.00	9	5	ND	1	62	1	2	4	44	.85	.061	9	40	.76	180	.08	2	1.94	.01	.44	1	1
L105+50 89+25E	2	28	8	354	.2	42	11	1575	2.63	7	5	ND	1	34	1	2	2	37	.43	.053	7	39	.62	137	.07	2	1.76	.01	.23	1	3
L105+50 89+50E	1	7	2	22	.1	7	1	98	.43	3	5	ND	1	730	1	2	2	7	16.14	.026	2	6	.25	20	.01	3	.23	.03	.01	1	1
L105+50 89+75E	2	53	9	152	.1	57	14	975	3.66	11	5	ND	1	74	1	2	2	57	1.07	.039	9	49	1.16	119	.08	3	2.07	.02	.50	1	1
L105+50 90+00E	2	48	8	136	.2	59	14	929	4.11	17	5	ND	1	47	1	2	3	65	.74	.045	11	60	1.04	188	.08	2	2.39	.03	.48	1	1
L105+50 90+25E	2	56	11	142	.4	50	13	1055	3.60	15	5	ND	1	69	1	2	2	53	2.52	.060	10	46	1.03	179	.09	2	2.04	.04	.34	1	1
L105+50 90+50E	1	32	11	174	.2	40	22	1330	3.46	7	5	ND	1	34	1	2	3	50	.56	.042	10	48	.73	191	.11	2	2.37	.03	.35	2	1
L105+50 90+75E	1	41	8	136	.2	49	14	1094	3.62	14	5	ND	1	59	1	2	2	53	.89	.064	10	49	1.07	189	.08	10	2.09	.02	.46	1	2
L105+50 91+00E	1	45	8	136	.2	48	13	1057	3.41	14	5	ND	1	72	1	2	2	53	1.11	.084	9	46	1.01	179	.08	6	1.99	.02	.36	1	1
L105 86+50E	3	73	11	158	.4	68	17	981	4.58	26	5	ND	1	33	1	5	2	78	.64	.053	11	54	1.57	95	.07	2	2.42	.01	.25	1	1
L105 86+75E	2	51	10	160	.2	48	15	931	4.06	17	5	ND	1	50	1	2	2	64	.77	.064	11	52	1.18	167	.07	2	2.39	.02	.33	1	1
L105 87+00E	2	53	10	266	.1	47	14	1364	3.65	16	5	ND	1	51	1	2	2	54	.80	.092	9	48	.98	236	.07	2	2.10	.01	.38	1	2
L105 87+25E	3	51	10	162	.1	61	16	904	4.23	16	5	ND	1	36	1	3	2	69	.63	.042	11	64	1.24	159	.09	2	2.35	.01	.33	2	1
L105 87+50E	2	49	10	170	.2	54	16	1235	3.89	15	5	ND	1	53	1	2	3	60	.83	.062	11	56	1.07	251	.09	7	2.18	.03	.45	2	1
L105 87+75E	1	27	10	147	.1	34	10	1020	2.77	7	5	ND	1	29	1	2	2	48	.40	.052	8	35	.60	201	.09	2	1.76	.01	.23	1	1
L105 88+00E	2	45	10	158	.1	54	15	960	3.88	17	5	ND	1	53	1	2	2	62	.73	.062	11	58	1.10	227	.10	3	2.38	.01	.39	2	1
L105 88+25E	2	41	12	148	.3	49	14	957	3.64	15	5	ND	1	62	1	2	2	58	.90	.067	11	52	1.06	196	.08	3	2.13	.02	.41	1	1
L105 88+50E	2	43	14	145	.2	50	14	884	3.67	15	5	ND	1	56	1	3	2	60	.76	.061	12	52	1.03	203	.10	2	2.40	.01	.41	2	2
L105 88+75E	2	34	9	145	.2	41	13	1000	3.25	12	5	ND	1	60	1	2	3	52	.81	.065	10	44	.85	217	.09	3	2.21	.01	.39	1	1
L105 89+00E	2	42	8	178	.2	43	12	1266	3.01	6	5	ND	1	71	1	2	2	46	1.16	.067	9	42	.81	227	.08	6	1.84	.01	.38	1	1
L105 89+25E	2	41	12	117	.2	48	13	970	3.35	13	5	ND	1	57	1	2	2	53	.88	.065	10	49	.91	182	.09	2	2.17	.01	.38	1	2
L105 89+50E	2	47	9	141	.2	49	14	989	3.52	15	5	ND	1	65	1	2	3	56	1.07	.077	10	48	1.04	192	.08	7	2.08	.02	.51	2	1
L105 89+75E	1	49	8	139	.2	54	14	1009	3.71	10	5	ND	1	54	1	2	2	56	.86	.056	10	50	1.02	186	.09	4	2.29	.01	.46	1	1
L105 90+00E	2	51	7	132	.1	56	15	905	3.76	17	5	ND	1	62	1	2	2	58	.93	.087	10	52	1.21	167	.08	12	2.19	.02	.51	1	1
STD C/AU-S	19	62	38	132	7.4	68	30	1084	4.02	41	24	7	39	53	19	16	20	63	.49	.087	40	60	.96	180	.07	32	1.75	.08	.15	10	48

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L105 90+25E	1	37	9	129	.1	43	13	979	3.37	10	5	ND	1	71	1	2	2	53	1.05	.068	9	44	.94	197	.09	9	2.10	.01	.49	1	1
L105 90+50E	2	46	7	129	.1	49	14	1239	3.56	7	5	ND	1	54	1	2	2	51	1.11	.086	9	45	1.01	169	.07	8	1.95	.01	.40	1	1
L105 90+75E	1	45	3	133	.1	48	14	1134	3.53	8	5	ND	1	75	1	2	2	51	1.04	.089	8	47	1.11	198	.07	15	2.05	.01	.48	1	3
L105 91+00E	1	34	6	123	.1	41	13	888	3.33	4	5	ND	1	60	1	2	2	51	.72	.062	9	47	.89	154	.09	5	2.04	.01	.45	1	1
L105 91+25E	1	36	6	109	.2	50	13	921	3.26	10	5	ND	1	58	1	2	2	51	.92	.073	9	55	.95	148	.09	5	1.98	.01	.44	1	1
L105 91+50E	1	35	7	143	.1	42	12	1067	3.20	5	5	ND	1	45	1	2	2	48	.75	.064	8	52	.76	188	.09	9	1.95	.01	.41	1	2
L104+50 86+75E	1	37	8	147	.1	38	12	846	3.31	6	5	ND	1	53	1	2	2	53	.66	.069	9	44	.86	188	.07	4	2.30	.01	.33	1	1
L104+50 87+00E	2	49	8	149	.2	51	16	1184	3.91	11	5	ND	1	41	1	3	2	64	.61	.055	11	52	1.09	180	.08	3	2.51	.01	.36	1	1
L104+50 87+25E	2	45	6	170	.1	47	14	1102	3.62	12	5	ND	1	57	1	2	2	56	.78	.057	10	49	1.01	238	.08	4	2.29	.02	.35	1	5
L104+50 87+50E	1	39	7	154	.1	42	13	1124	3.38	11	5	ND	1	49	1	3	2	52	.67	.043	9	46	.87	233	.09	7	2.24	.01	.50	1	2
L104+50 87+75E	2	49	4	170	.1	50	14	1117	3.73	12	5	ND	1	55	1	2	2	58	.93	.084	9	53	1.04	215	.08	9	2.28	.01	.52	1	2
L104+50 88+00E	2	51	6	154	.2	54	14	1055	3.51	13	5	ND	1	54	1	2	2	55	.99	.074	9	53	1.10	179	.06	15	1.94	.01	.43	1	1
L104+50 88+25E	1	45	5	106	.1	47	13	965	3.31	11	5	ND	1	74	1	2	2	52	1.07	.081	10	47	.98	219	.08	9	2.13	.01	.42	1	8
L104+50 88+50E	2	48	8	145	.2	51	13	867	3.50	13	5	ND	1	68	1	2	2	55	1.11	.093	10	50	1.03	177	.07	9	2.18	.01	.40	1	2
L104+50 88+75E	1	45	6	164	.1	47	13	984	3.51	10	5	ND	1	56	1	2	2	56	.90	.105	10	52	.93	207	.08	8	2.47	.01	.39	1	1
L104+50 89+00E	1	40	5	137	.1	45	12	935	3.15	8	5	ND	1	75	1	2	2	50	1.06	.071	10	45	.89	223	.08	6	2.02	.01	.41	1	1
L104+50 89+25E	2	47	6	161	.1	51	13	1166	3.36	12	5	ND	1	72	1	2	2	53	1.21	.103	9	52	1.03	203	.06	10	1.97	.01	.42	1	1
L104+50 89+50E	1	38	6	146	.1	46	13	976	3.50	9	5	ND	1	43	1	2	2	51	.76	.070	10	51	.86	184	.09	4	2.18	.01	.50	1	1
L104+50 89+75E	1	40	7	132	.1	45	13	962	3.42	8	5	ND	1	55	1	2	2	53	1.01	.079	9	47	.91	186	.08	10	2.13	.01	.45	1	1
L104+50 90+00E	1	47	7	142	.1	47	14	1054	3.59	11	5	ND	1	57	1	2	2	55	1.06	.078	9	48	1.08	172	.07	10	2.16	.01	.49	1	2
L104+50 90+25E	1	43	4	142	.2	44	13	1100	3.28	8	5	ND	1	55	1	2	2	49	1.04	.076	9	44	.92	200	.07	7	2.01	.01	.48	1	3
L104+50 90+50E	1	39	5	142	.3	41	14	1205	3.36	8	5	ND	1	53	1	2	3	50	.89	.083	10	44	.83	229	.09	4	2.12	.01	.47	2	1
L104+50 90+75E	1	41	5	123	.1	42	15	1005	3.37	8	5	ND	1	47	1	2	2	52	.91	.072	10	42	.83	199	.09	8	2.16	.01	.43	1	1
L104+50 91+00E	1	40	9	115	.1	38	11	1021	2.95	5	5	ND	1	83	1	2	2	46	1.26	.042	8	39	.80	174	.08	14	1.88	.01	.34	1	1
L104+50 91+25E	1	30	4	126	.3	32	10	1188	2.53	3	5	ND	1	55	1	2	3	37	.57	.081	7	34	.64	179	.07	9	1.59	.01	.34	1	1
L104+50 91+50E	1	28	5	121	.2	36	11	789	3.07	3	5	ND	1	46	1	2	2	47	.46	.044	8	49	.77	132	.11	7	1.97	.01	.42	1	1
L104+50 91+75E	1	62	6	106	.4	79	16	753	3.83	11	5	ND	2	57	1	2	2	66	.85	.078	21	68	1.11	161	.11	7	2.10	.01	.40	1	1
L104 87+00E	1	46	8	195	.2	37	12	1186	2.95	6	5	ND	1	63	1	2	2	43	.76	.075	8	37	.92	190	.07	6	2.01	.02	.39	1	2
L104 87+25E	2	46	5	197	.1	40	11	901	3.17	7	5	ND	1	67	1	2	2	45	.87	.082	8	42	1.03	163	.07	5	2.07	.01	.43	2	1
L104 87+50E	1	54	6	130	.4	59	12	475	3.82	9	5	ND	1	43	1	2	2	62	.68	.055	12	57	1.28	126	.09	3	2.50	.01	.39	1	1
L104 87+75E	2	52	8	152	.2	58	14	856	3.72	11	5	ND	1	55	1	2	2	61	.87	.066	10	57	1.21	163	.07	8	2.22	.03	.45	1	2
L104 88+00E	2	44	6	159	.2	49	13	1014	3.39	11	5	ND	1	70	1	2	2	53	1.21	.088	9	50	1.02	201	.07	10	2.14	.01	.45	1	1
L104 88+25E	2	49	5	160	.1	50	13	992	3.40	9	5	ND	1	68	1	2	2	54	1.28	.100	9	53	1.04	175	.06	18	2.04	.01	.44	1	1
L104 88+50E	2	47	6	150	.2	55	14	948	3.49	11	5	ND	1	61	1	3	2	56	1.13	.090	9	63	1.05	163	.07	12	2.31	.01	.49	2	1
L104 88+75E	2	46	7	148	.1	53	13	979	3.29	12	5	ND	1	68	1	2	2	52	1.26	.086	9	58	.97	173	.07	14	1.97	.01	.43	1	4
L104 89+00E	2	45	7	149	.3	53	13	907	3.45	9	5	ND	1	64	1	2	2	55	1.07	.079	10	55	1.03	168	.08	7	2.07	.01	.49	1	2
STD C/AU-S	19	62	37	132	7.3	71	31	1094	4.06	40	21	8	39	53	19	17	19	60	.49	.090	41	61	.96	179	.07	33	1.79	.07	.15	13	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L104 89+25E	1	44	6	153	.1	47	12	956	3.29	8	5	ND	1	61	1	2	2	47	1.06	.083	10	50	.91	164	.07	10	1.92	.01	.41	1	2
L104 89+50E	1	47	8	155	.1	49	13	932	3.33	7	5	ND	1	57	1	2	2	47	1.01	.086	10	52	.94	176	.07	8	1.92	.01	.41	1	2
L104 89+75E	1	38	8	144	.1	40	11	740	2.84	6	5	ND	1	82	1	2	2	40	1.07	.089	9	41	.80	176	.06	6	1.81	.01	.32	1	1
L104 90+00E	1	42	7	147	.1	43	12	927	3.10	7	5	ND	1	63	1	2	2	44	1.02	.074	9	45	.87	189	.07	7	1.82	.01	.37	1	1
L104 90+25E	1	35	9	138	.1	39	12	987	2.99	5	5	ND	1	58	1	2	2	40	.98	.070	9	42	.79	205	.07	5	1.91	.03	.36	1	1
L104 90+50E	1	38	8	132	.1	43	13	991	3.28	7	5	ND	1	46	1	2	3	43	.71	.057	10	44	.84	199	.09	4	2.12	.03	.38	1	2
L104 90+75E	1	38	7	185	.1	36	11	1231	2.89	2	5	ND	1	41	1	2	2	38	.55	.107	8	37	.63	236	.08	2	1.81	.01	.23	1	1
L104 91+00E	1	30	8	129	.1	39	12	767	3.32	6	5	ND	1	39	1	2	2	48	.62	.043	10	45	.76	161	.11	2	2.27	.01	.37	1	2
L104 91+25E	1	36	6	115	.1	44	12	639	3.31	3	5	ND	1	55	1	2	2	46	.50	.038	9	53	.90	129	.11	6	1.84	.01	.28	1	1
L104 91+50E	1	56	9	125	.1	44	16	861	3.75	4	5	ND	1	47	1	2	2	54	.63	.052	11	50	.93	165	.12	2	2.44	.03	.34	1	6
L104 91+75E	1	46	9	152	.1	44	13	1032	3.36	5	5	ND	1	50	1	2	2	44	.76	.088	10	48	.78	244	.09	5	2.05	.01	.41	1	1
L104 92+00E	1	37	7	145	.1	37	11	959	2.99	5	5	ND	1	64	1	2	2	40	1.01	.083	9	43	.74	203	.08	6	1.81	.02	.45	1	1

APPENDIX II

STATEMENT OF COSTS

Soil Sampling

Personnel		
1 geologist - 1 day @ $250.00/day	$ 250.00	
1 supervisor - 7 days @ $200.00/day	1,400.00	
2 assistants - 7 days @ $180.00/man/day	2,520.00	
Accommodation		
6 nights	437.40	
Meals	545.41	
Vehicle Rental	879.55	
Supplies		
flagging	67.50	
soil sample bags	106.00	
hip chain thread	119.00	
soil sample note books	20.00	
Field Equipment and Instrument Rental		
22 personnel days @ $2.00/person/day	44.00	
Management Fee	649.00	
Assay Costs	5,830.00	
Subtotal Soil Sampling		$12,867.86

Grid Establishment

5.5 km brushed line @ $225.00/km	1,237.50	
38.35 km flagged line @ $175.00/km	6,711.25	
Subtotal Grid Establishment		$7,948.75

Geophysical Surveys

Magnetometer and 2 Station VLF 38.35 km @ $180.00/km	6,903.00	
Genie-EM 39.20 km @ $270.00/km	10,584.00	
Subtotal Geophysics		$17,487.00
Assessment Report and Map Compilation		$2,500.00
Total Cost of the 1988 Exploration Program		$40,803.61

Specifications

Frequency Tuning Range	15 to 30 kHz, in 100 Hz increments, with bandwidth of 150 Hz; tuning range accommodates new Puerto Rico station at 28.5 kHz.
Transmitting Stations Measured	Up to 3 stations can be automatically measured at any given grid location within frequency tuning range.
Recorded VLF Magnetic Parameters	Vertical in-phase, vertical quadrature (out-of-phase), total field strength (or optional horizontal amplitude), dip angle.
Standard Memory Capacity	1300 combined VLF magnetic and VLF electric measurements as well as gradiometer and magnetometer readings.
Display	Custom designed, ruggedized liquid crystal display with built-in heater and an operating temperature range from −40°C to +55°C. The display contains six numeric digits, decimal point, battery status monitor, signal strength status monitor and function descriptors.
RS232C Serial I/O Interface	Variable baud rate from 300 to 9600 baud, 8 data bits, 2 stop bits, no parity.
Test Mode	A. Diagnostic Testing (data and programmable memory). B. Self Test (hardware).
Sensor Head	Contains 3 orthogonally mounted coils with automatic tilt compensation.
Operating Environmental Range	−40°C to +55°C; 0 – 100% relative humidity; Weatherproof.
Power Supply	Non-magnetic rechargeable sealed lead-acid 18V DC battery cartridge or belt; 18V DC disposable battery belt; 12V DC external power source for base station operation only.
Weights and Dimensions	
Instrument Console	3.8 kg, 122 x 246 x 210 mm.
Sensor Head	0.9 kg, 140 dia. x 130 mm.
VLF Electronics Module	1.7 kg, 280 x 190 x 60 mm.
Lead Acid Battery Cartridge	1.8 kg, 138 x 95 x 75 mm.
Lead Acid Battery Belt	1.8 kg, 540 x 100 x 40 mm.
Disposable Battery Belt	1.2 kg, 540 x 100 x 40 mm.

APPENDIX III

STATEMENT OF QUALIFICATIONS

I, Ralph Edward Shearing, of 3433 West 12th Avenue, Vancouver, B.C., DO HEREBY CERTIFY THAT:

1. I am President of Quest Canada Exploration Services Inc., a geological consulting and services company, with business office at Suite 840, 650 West Georgia Street, Vancouver, B.C.

2. I am a graduate of the University of British Columbia with a degree of B.Sc., Geology, 1981.

3. I am a Fellow of the Geological Association of Canada.

4. I am a Professional Geologist registered with the Association of Professional Engineers, Geologists and Geophysicists of Alberta. Membership #40288.

5. I have been active in mineral exploration since 1979 as follows:

   a) 1979 - Summer employee with St. Joseph Explorations Limited; Pb, Zn, Au, Ag and U exploration in the Yukon and British Columbia.

   b) 1980 - Summer employee with Sulpetro Minerals Limited; Pb, Zn, Au, Ag and U exploration in the Yukon and northern British Columbia.

   c) 1981 - 1982 - Full-time employee with Sulpetro Minerals Limited; Pb, Zn, Au and Ag exploration in the Yukon and northern British Columbia. Geological and geophysical exploration for Au, Ag, Cu, Pb and Zn in northwestern Quebec and northern Ontario. Geophysical exploration provided significant experience in conducting the following geophysical surveys, as well as in the application of the resultant data: VLF-Electromagnetic, Horizontal Loop Electromagnetic, Proton Magnetometer, Induced Polarization and Gravity.

   d) 1983 - Present - Independent consulting geologist with Quest Canada Exploration Services Inc. Geological and geophysical exploration for Au, Ag, Pb and Zn in central British Columbia.

   e) I supervised the exploration program conducted on the Genesis property during 1988.

Dated this 4th day of May, 1989.

By: [signature]

Ralph E. Shearing, B.Sc., P.Geol.
Consulting Geologist

APPENDIX IV

EDA OMNI-PLUS VLF/MAGNETOMETER SYSTEM

VLF-EM and magnetic field measurements were made using an EDA Omni-Plus geophysical system. The Omni-Plus is a portable, microprocessor-based magnetometer/VLF system which is capable of measuring changes or contrasts detected by two different types of geophysical methods: magnetic and VLF electromagnetic (magnetic and electric).

Principle of Operation

Magnetic Field Measurements

If a proton-rich fluid such as kerosene, jet fuel, heptane, etc. is placed into a magnetic field, the protons will align along the magnetic field vector. The magnetic field is induced in the sensor upon depressing the pushbutton. Then this field is suddenly removed. Protons which behave as elementary gyroscopes will start precessing around the remaining magnetic field - that of the earth. The precession frequency is directly proportional to the magnetic field of the earth. The magnetometer counts this frequency, divides it by the appropriate constant to obtain a reading in gammas ($1\gamma = 10^{-5}$ gauss) and displays the reading in the form of a 5 digit number.

Electromagnetic Field Measurements

The VLF (Very Low Frequency) EM method employs an artificial source of EM waves - a VLF antenna, several hundred feet high, which acts essentially as a vertically grounded wire. A worldwide network of high-power VLF stations established for marine and air navigation act as the sources for the VLF-EM exploration method. At present, suitable transmitters for EM prospecting in North America are located at Cutler, Maine, Annapolis, Maryland, and Seattle, Washington. The transmitted frequencies (in the 20 KHz band) are very low frequency (VLF) only by comparison to broadcasting standards, but are in fact very high relative to any other geophysical EM system.

The VLF antenna current is vertical. The main magnetic field component of the primary (transmitted) signal is horizontal and theoretically tangent to circles about the antenna mast. Hence, a transmitting station should be chosen so that its direction is almost parallel to the geological strike in the survey area so as to produce a magnetic field perpendicular to the strike. If a conductor is located in the survey area, eddy currents are established, producing a secondary field in the vicinity of the conductor. The VLF-EM equipment measures the vertical components of this secondary field.

The fact that the source is at infinity means the primary field is essentially uniform over the survey area and hence all conductors are energized uniformly. This enables the detection of a broad variety of conductors, ranging from good conductors - graphite, massive sulphides, to poor conductors - muskeg, clay edges, shear zones, contacts. At times this may be a disadvantage, however, since it may emphasize large-scale, relatively poor conductors at the expense of smaller concentrated bodies. In many environments, the anomalies of interest can be masked by the large amount of geological noise. The penetration of the system is limited by its high frequency in the presence of conductive overburden. However, if the subsurface is resistive, for example, little overburden, the penetration can be quite deep due to the transmitter being so far removed.

The VLF-EM method is also affected by topographic effects, spurious anomalies being picked up on top of conductive hills because the resultant field tends to follow the slope. The distinction between anomaly conductivity and depth is also often difficult. Another major drawback is that it is not always possible to use a transmitting station which gives a primary horizontal field striking at right angles to the geologic strikes in the survey area. In this case, two VLF transmitters, at approximately right angles to each other, should be used to provide better coverage.

Field Procedure

Measurements are obtained by the use of two sensors; a proton precession sensor carried on a pole to measure the magnetometer total field magnitude and a three-component sensor worn on the back to measure the magnetic component of the VLF secondary field. In addition, probes attached through the VLF circuitry housing are used to measure the electric component of the VLF secondary field. An electronics console is worn on the front of the operator that allows the operator to view and store the collected data in internally protected memory. The data stored is protected by a lithium battery which also powers a real-time clock.

Along with the magnetometer and VLF data, the Omni-Plus stores the following information:

- line number
- position number
- date and time
- direction of travel
- statistical error of the magnetometer readings
- signal strength and rate of decay of the magnetometer sensor

- direction, in degrees, of the primary field in relation to the operator
- signal strength and operator quality of the VLF sensor
- natural and cultural features

The Omni-Plus has been designed to simultaneously measure the VLF and magnetometer components. When the READ key is pressed, the previous magnetometer or VLF reading is displayed followed by the new corresponding reading for the particular station. At this point, all measurements have been completed and the data may be stored using one of the RECORD keys. If the operator tries to store the data prior to completion of the VLF measurements, the word "wait" will appear on the display indicating that the VLF measurement process is not completed. Once the VLF measurements are completed, the data may be stored.

The Omni-Plus monitors the VLF frequencies selected for operator quality and signal/noise during each reading. The results are both displayed as descriptor bars and stored in internal memory along with the field results.

Operator quality is a value to help the operator determine whether the measurement was properly taken. Since the in-phase and tilt measurements are dependent on the sensor being within 10 degrees of vertical and motionless, the Omni-Plus monitors the ability of the operator to remain motionless and vertical. As mentioned, the results are outputted on the display using the DECAY descriptor bars. The increased quality of the measurement is indicated by the increased number of bars displayed to a maximum of four. Also, for each measurement, a numeric value is given which ranges from 1 to 9, where 1 is the poorest and 9 is the best. Generally, a value of 5 to 6 should be obtained to ensure an accurate reading.

The signal/noise ratio is an actual measurement of the signal strength to the background noise. The results are outputted visually using the SENSOR descriptor bars when the VLF results are displayed. An increased signal strength is indicated by an increase in the number of bars displayed to a maximum of four. As with the operator quality, a numeric value is given which ranges from 1 to 9, where 1 is the weakest and 9 is the strongest.

The Omni-Plus has been designed whereby, if a weak station is selected, the instrument will automatically increase the measurement period to produce higher quality results. The measurement period for one frequency may range from one to ten seconds.

In standard VLF survey methods, a single or consistent direction is used to maintain comparable signs on all in-phase, quadrature or tilt values relative to each other. Since the Omni-Plus is a no orientation system, a convention was selected that maintained the standard convention that North and East are positive and South and West are negative.

Therefore, the profiles plotted looking east (ie. S to N) and north (ie. W to E) will have the crossover in the correct sense (positive to negative).

APPENDIX V

MOVING SOURCE GENIE ELECTROMAGNETIC INSTRUMENT

Genie Portable EM System - Model SE-88

Field Procedure

The Genie field procedure varies somewhat depending on whether automatic chaining is used (reconnaissance mode) or whether cut and flagged lines are provided.

Automatic Chaining (Reconnaissance)

In this mode, the distance measuring capability of the GENIE is used to keep transmitter and receiver at a desired separation. Accuracy of separation is very good over neutral ground and relatively flat topography. However, steep topography or the presence of large conductors will shorten intercoil separation. In very steep terrain, the reduction in spacing may become appreciable due to transmitter and receiver no longer being maximally coupled. If accurate spacing is required, either lagging or, for small separations, the use of a hip chain by the receiver operator is recommended

The traverse should be started over neutral ground, having selected the desired frequency pair, separation and integration time. Selection of the integration time depends on atmospheric noise and required data accuracy. A measure of atmospheric noise can be obtained by selecting the NOISE MONITOR position with the METER switch while the transmitter is turned off. Quiet atmospheric noise conditions are characterized by a relatively steady signal meter indication. Approaching storm systems or local storms will give large meter fluctuations. Such conditions will require longer integration times to obtain consistent ratio readings.

The receiver operator should now walk along the traverse. As he approaches his station, both transmitter and receiver should be switched on. The METER switch must be in the SIGNAL position. The operator should proceed until the REFERENCE meter reads 1.0 or the pointer is within the short green arc. Meter fluctuations are due to atmospheric noise and movement of the receiving coil in the natural magnetic field.

The SIGNAL meter will also read approximately 1.0 over neutral terrain, but will depart from this reading near a conductor. Values larger or smaller are possible. The SIGNAL meter deflection compared to that of the REFERENCE meter gives thus an immediate visual indication of an anomalous zone.

Transmitter and receiver coils should be vertical and steady during measurement. It is advisable to take more than one ratio reading and use the average, especially at large separations. Once all the measurements at a station are taken, transmitter and receiver should be turned off (receiver to STANDBY in subzero temperatures) to conserve battery power. The receiver operator should mark his station for the transmitter operator and then proceed in the same manner.

This method does not give overlapping coverage of the terrain. If overlap is required, the receiver operator should wear a hip chain. The transmitter operator can then walk along the chain for a distance equal to the desired station spacing before the receiver operator proceeds himself.

Data points are usually plotted at the midpoint between transmitter and receiver.

Observe the following hints to obtain consistent ratio readings:

- In the vicinity and especially directly over conductors, secondary field vectors at two well separated frequencies may show considerably different orientations in space. Repeatability of ratio readings in such locations depends strongly on receiving coil positions and orientation. for the latter reason, the receiver is fitted with a bubble level to facilitate repeatable coil orientation.

- Hold the receiver steady during measurement, especially at large separations, to reduce induction noise.

- Induction noise may also be caused by mechanical coil vibration. Do not tap either coil or receiver during measurement. Actuate the AUTO-HOLD switch gently at large separations when using the single measurement feature.

- Do not wear an electrical analog watch while operating the receiver. The small motor inside the watch creates enough electromagnetic disturbance to impair ratio accuracy.

- The audio alarm should not be used at separations exceeding 100 m. The current in the transducer is large enough to create a disturbing magnetic field. At large separations, this disturbance is comparable in strength to measured signals.

Cut and Flagged Lines

As mentioned in the previous section, flagging or the use of a hip chain are recommended in very steep terrain or when high station accuracy is desired on detail surveys.

Either operator may lead along a flagged traverse. Both operators switch on their equipment when on station. The appropriate separation setting may be preselected on the receiver. The REFERENCE meter must be within the long green arc. SEPARATION and MULTIPLIER controls are used as coarse and fine gain controls respectively to achieve this. To increase the meter reading, increase SEPARATION and/or MULTIPLIER settings and vice versa. When the signal strength condition is met, ratio readings are taken in the same manner as described earlier.

Genie Portable EM System - Model SE-88

Specifications

Transmitter

Transmitting Element	Iron-cored coil for each frequency.
Transmitting Frequency Pairs	Five pairs. 112.5 Hz reference with one of 337.5, 1012.5 or 3037.5 Hz; or 337.5 Hz reference with one of 1012.5 or 3037.5 Hz.
Transmitting Moments	150 Am at 112.5 Hz, 100 Am at 337.5 Hz, 50 Am at 1012.5 Hz, 25 Am at 3037.5 Hz.
Relative Amplitude Stability	Better than 0.1%
Power Supply	Rechargeable Nickel-Cadmium batteries; 2 options available, Normal and Heavy Duty.
Power Supply Endurance	Normal duty pack: 3 hours continuous at 20°C. Heavy duty pack: 5 hours continuous at 20°C.
Operating Temperature Range	-30°C to +50°C
Storage Temperature	-40°C to +50°C
Total Weight with Batteries	Normal duty configuration: 14 kg Heavy duty configuration: 16 kg
Dimensions	Height: 800 mm; Width: 380 mm; Depth: 180 mm

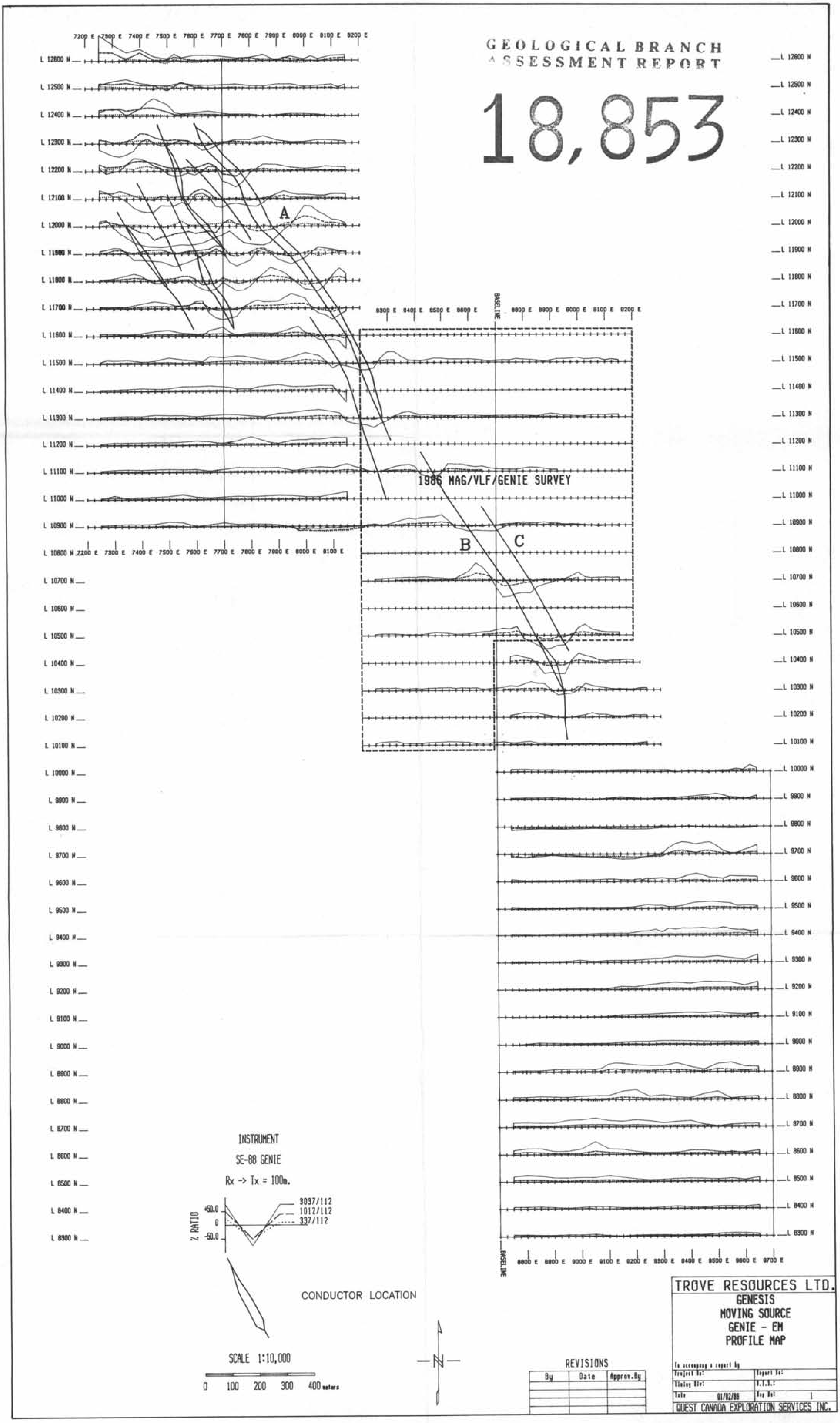
Receiver

Receiving Element	Iron-cored coil
Receiving Frequency Pairs	Same as transmitter
Transmitter-Receiver Separation	Primary selector: 6.26 m, 12.5 m, 25 m, 50 m, 100 m, 200 m plus Multiplier: x 1, x 1.25, x 1.5, x 1.75

Maximum Transmitter-Receiver Separation	200 m under most conditions. Greater separations may be possible, depending on atmospheric and power line noise.
Power Line Filtering	Internally switch selectable at 60 or 50 Hz and 3rd harmonic.
Signal Averaging Time	Switch selectable at 2, 4, 8 or 16 seconds.
Resolution of Ratio Display	0.1%
Power Supply	Rechargeable Nickel-Cadium batteries.
Power Supply Endurance	20 hours continuous at 20°C
Operating Temperature Range	-30°C to +50°C
Total Weight	6 kg
Console Dimensions	Length: 280 mm; Height: 230 mm; Depth: 150 mm
Coil Dimensions	Length: 500 mm; Diameter: 45 mm

Battery Charger

Power Requirements	115 V or 230 V, 50 Hz or 60 Hz, 50 VA
Charging Time	7 hours for completely discharged batteries, subsequent automatic trickle charging. Transmitter and receiver batteries can be charged simultaneously.
Weight	4.5 kg
Dimensions	Length: 290 mm; Height: 150 mm; Depth: 130 mm.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A
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BASELINE
INSTRUMENT
SE-88 GENIE
Rx -> Tx = 100m.
Z RATIO
3037/112
1012/112
337/112
CONDUCTOR LOCATION
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0 100 200 300 400 meters
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Date
Approv.By
TROVE RESOURCES LTD.
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GENIE - EM
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Date 01/02/89
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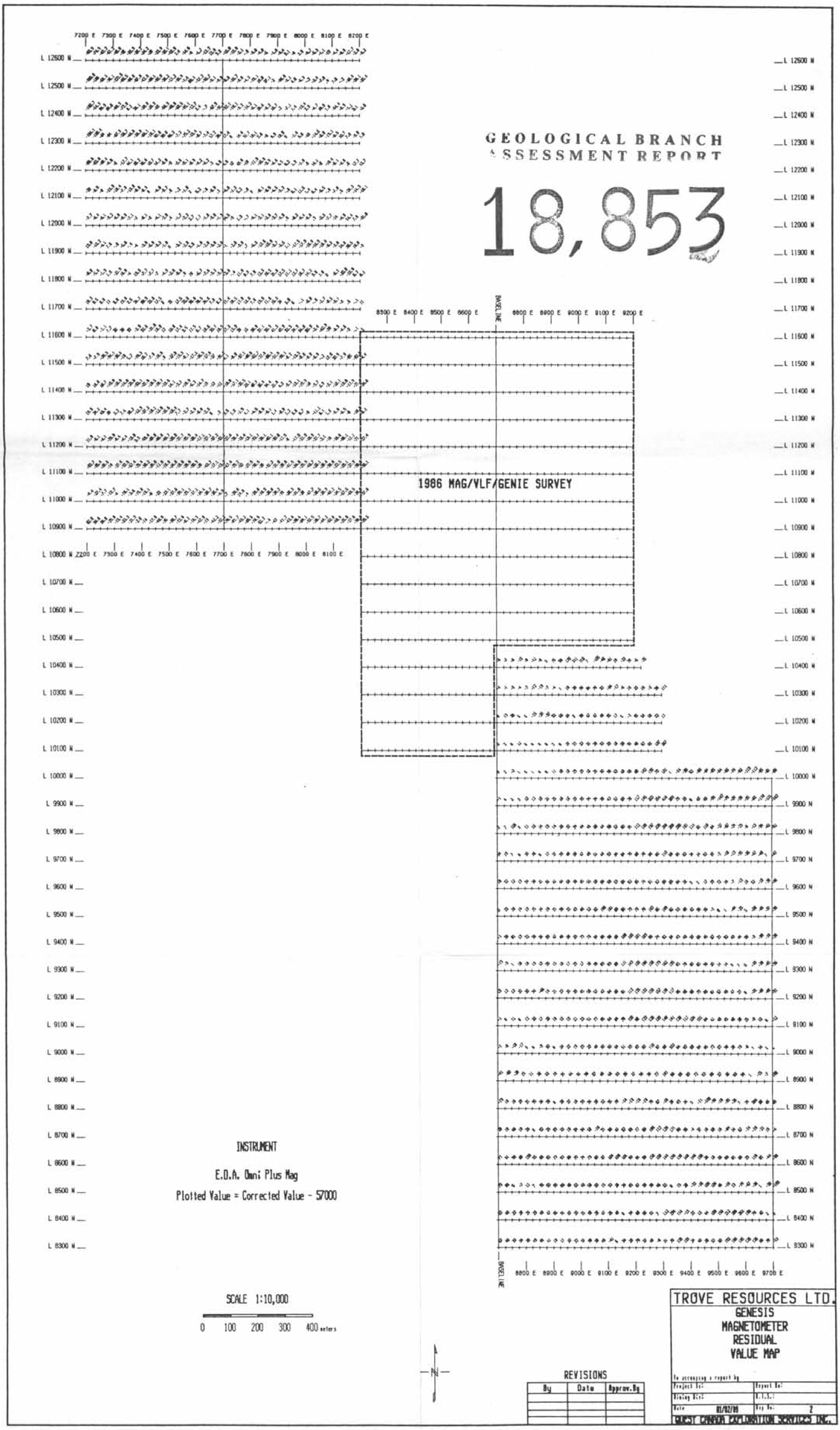
QUEST CANADA EXPLORATION SERVICES INC.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BASELINE
INSTRUMENT
E.D.A. Omni Plus Mag
Plotted Value = Corrected Value - 57000
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REVISIONS
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TROVE RESOURCES LTD.
GENESIS
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GEOLOGICAL BRANCH
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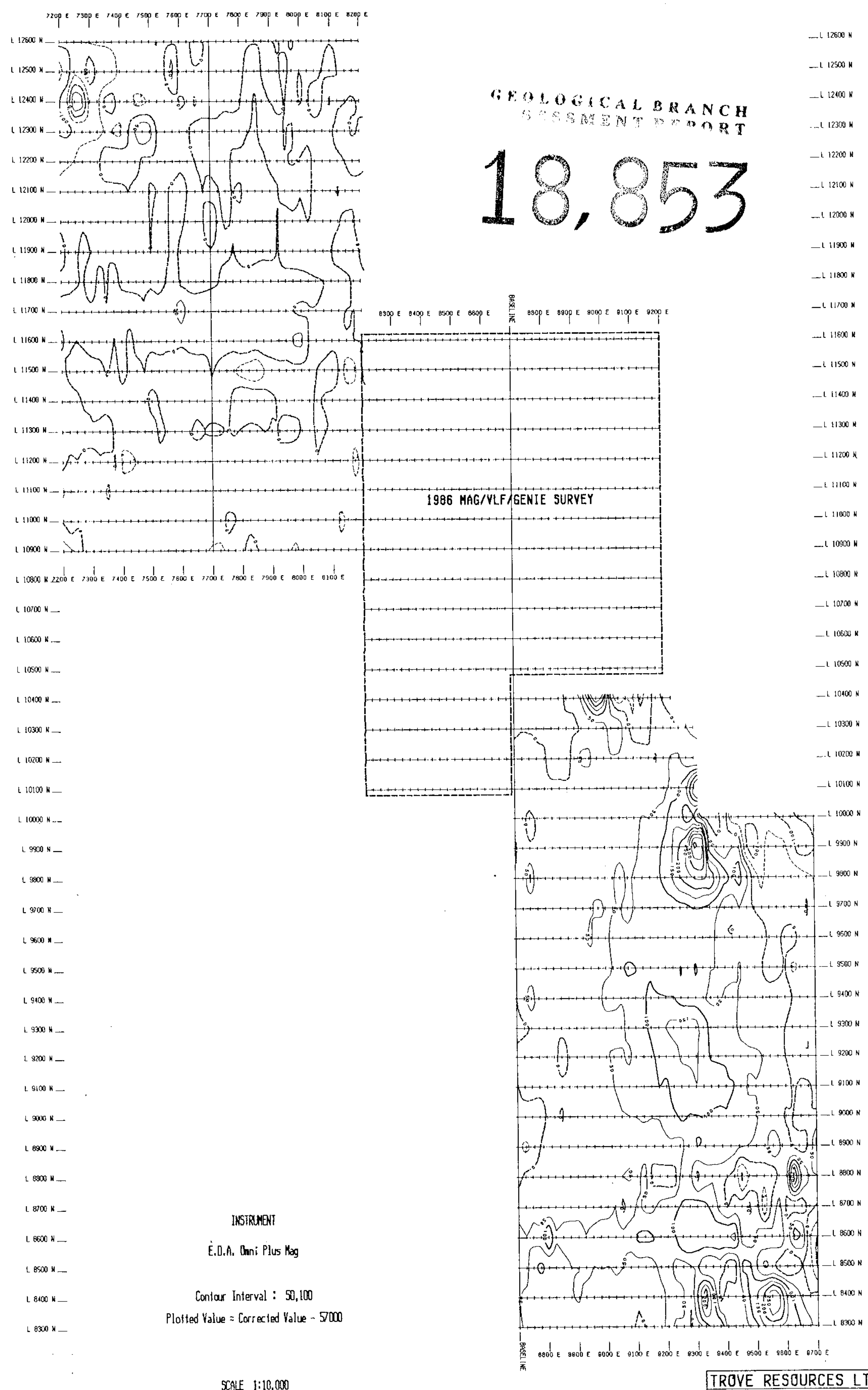
18,853



INSTRUMENT

E.D.A. Omni Plus Mag

Contour Interval : 50,100

Plotted Value = Corrected Value - 57000

SCALE 1:10,000

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By	Date	Approv.By

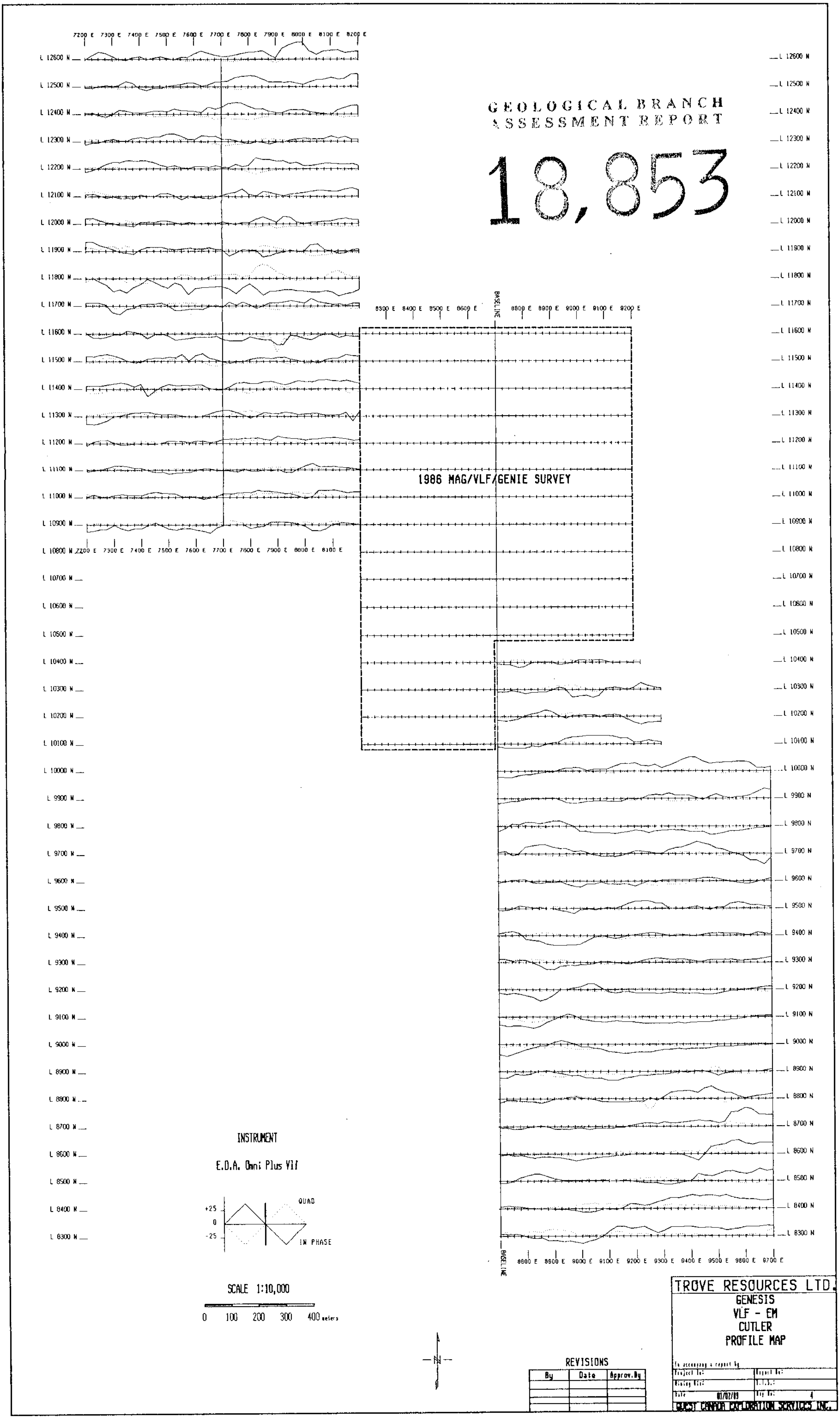
TROVE RESOURCES LTD.

GENESIS
MAGNETOMETER
RESIDUAL
CONTOUR MAP

To accompany a report by

Project No:	Report No:
Mining Div:	N.T.S.:
Date 01/07/89	Map No: 3

QUEST CANADA EXPLORATION SERVICES INC.



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+25
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By
Date
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GENESIS
VLF - EM
CUTLER
PROFILE MAP
Date 01/02/89
4
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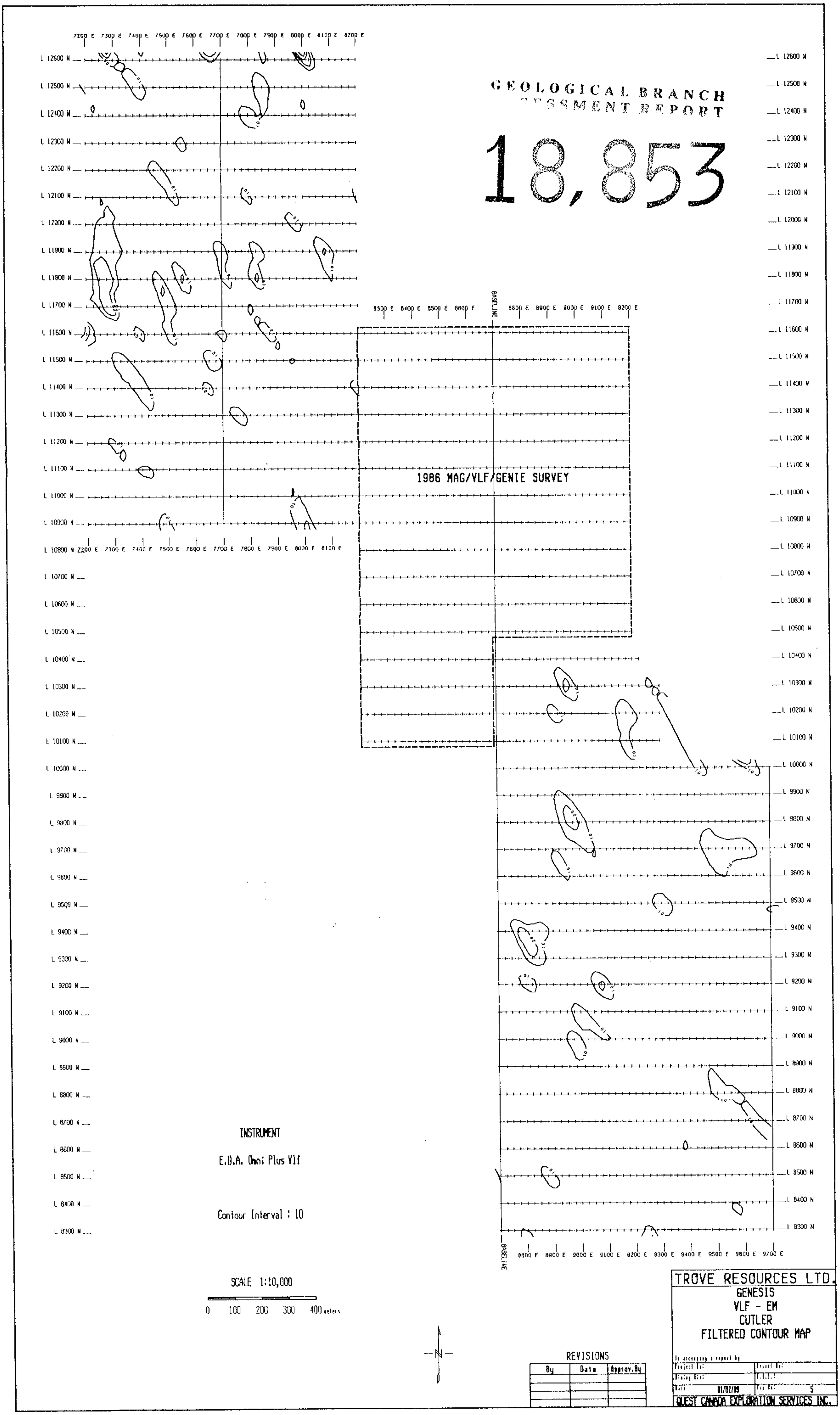
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GENESIS
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QUEST CANADA EXPLORATION SERVICES INC.

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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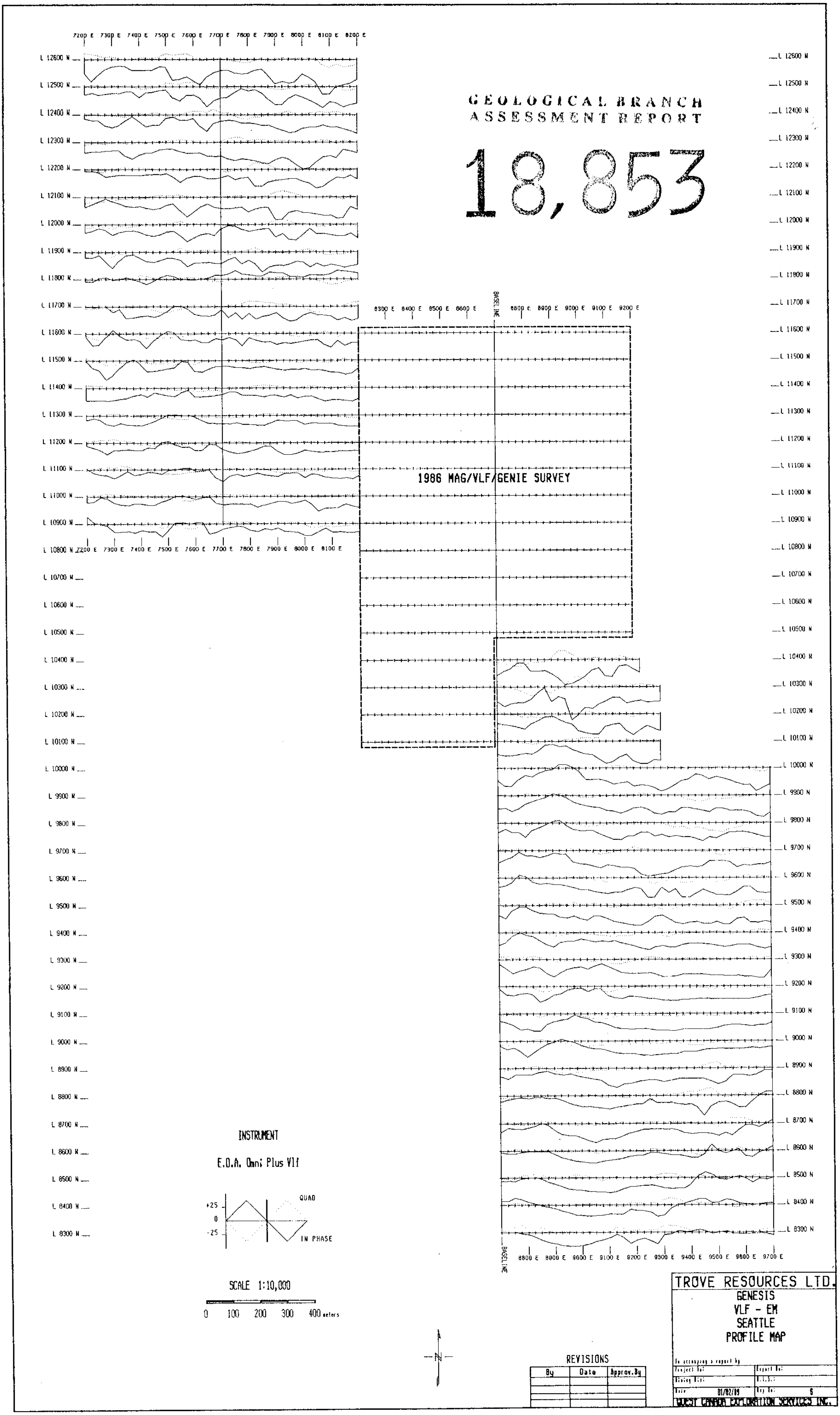

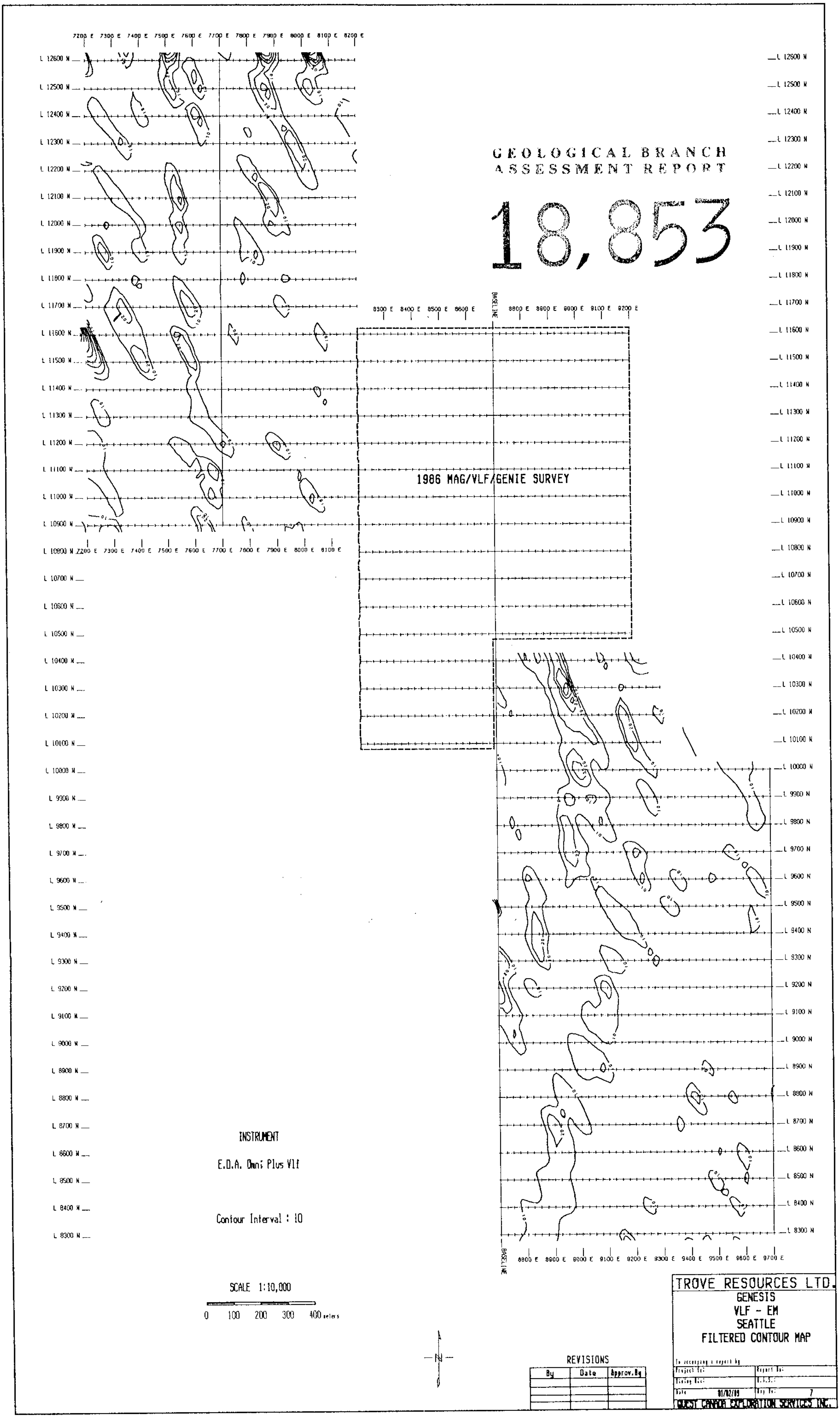
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E.D.A. Omni Plus Vlf
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VLF - EM
SEATTLE
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Date 01/02/89
Map No: 7
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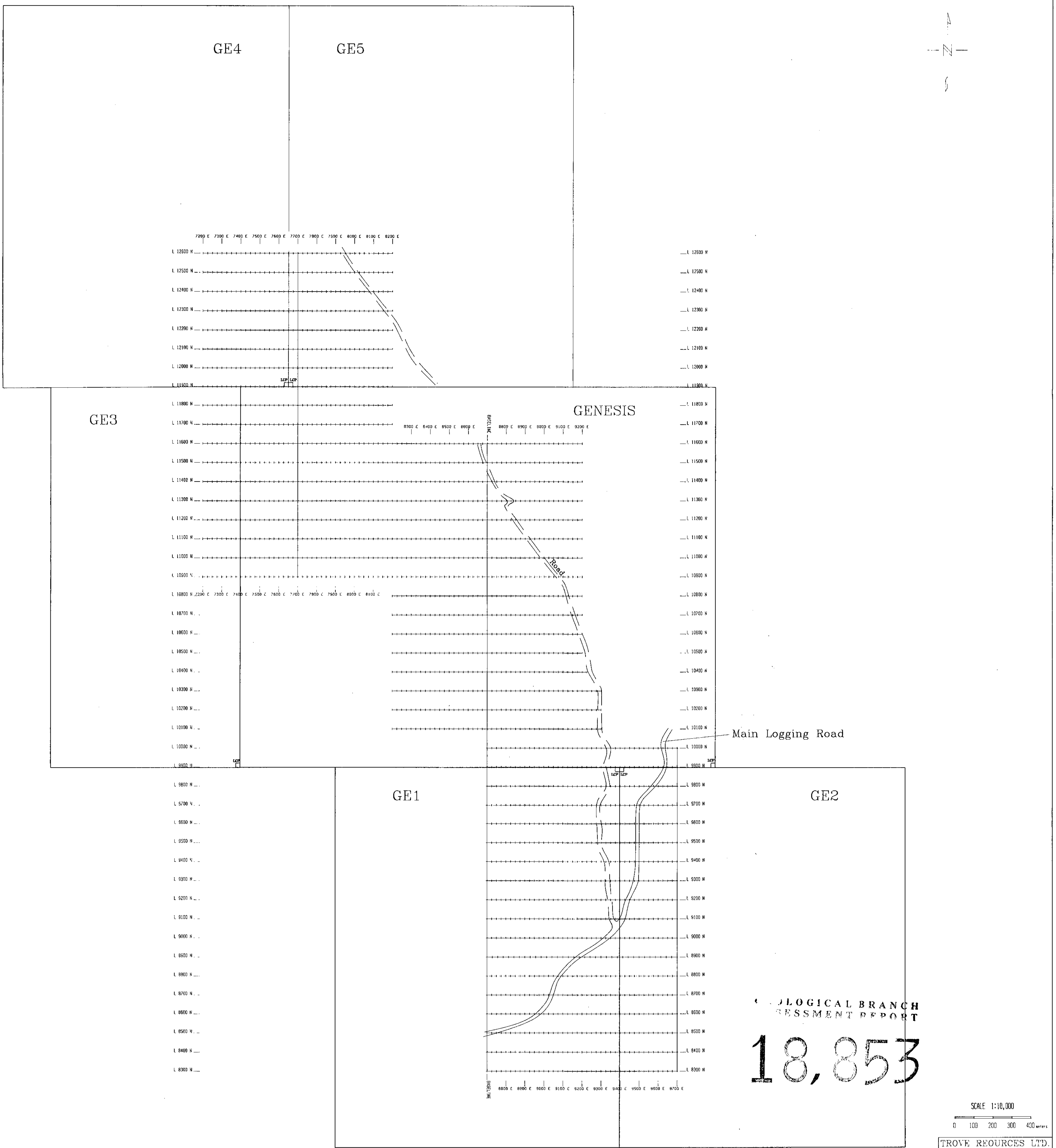

REVISIONS

By	Date	Approv. By

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GENESIS PROPERTY
COMPILATION MAP

To accompany a report by

Project No:	Report No:
Mining Div: Kamloops	NTS: 92I/14
Date: 01/02/89	Map No:

QUEST CANADA EXPLORATION SERVICES INC.