GEOCHEMICAL, GEOLOGICAL, GEOPHYSICAL AND DIAMOND DRILLING ASSESSMENT REPORT ON THE IRON MOUNTAIN PROPERTY

NICOLA MINING DIVISION,
MERRITT AREA, BRITISH COLUMBIA

LOCATION:
N.T.S.: 92 I - 2
LATITUDE: 50° 03'N.
LONGITUDE: 122° 45'W.

CLAIMS:

TWO (480), BY (481), FOUR (482), TWO BY FOUR (484),
SHORT STUD (667), FIR STUD (1216), FIERRO #3 (997)

REPORT FOR:

GOLDEN DYNASTY RESOURCES LTD.
WORLD TRADE CENTRE
SUITE 404-999 CANADA PLACE
VANCOUVER, BRITISH COLUMBIA V6C 3E2

OWNER

K. WAYNE LIVINGSTONE
6775 WEST BOULEVARD
VANCOUVER, BRITISH COLUMBIA

PREPARED BY:

PETER A. CHRISTOPHER, PHD., P.ENG.
PETER CHRISTOPHER & ASSOCIATES INC.
3707 WEST 34TH AVENUE
VANCOUVER, B.C. V6N 2K9

JULY 1989

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SUMMARY

The Iron Mountain Property, consisting of 7 metric mineral claims totaling 32 units covers about 8 square kilometers in the Nicola Mining Division about 7 kilometer south-southwest of Merritt, B.C. Good road access exists to a number of old workings on the property which include Leadville shaft from which 36 tons shipped to Trail in 1947 produced 67 ounces of silver, 11,819 pounds of lead, and 484 pounds of zinc.

The property has a long history of exploration and development with hematite-chalcopyrite occurrences located on the south side of Iron Mountain in 1897. The property has named surface workings called the Charmer, Leadville, Comstock, Lucky Todd and LD with the Comstock baritic lead-zinc-silver showing developed by the Leadville shaft and the Charmer gold-copper-hematite zone developed by three short shafts. The property is reported to have been worked by lessees in 1947, and some ore was shipped.

Iron Mountain is underlain by basic to acidic volcanic rocks and associated sedimentary rocks of the Triassic Nicola Group. The area has previous been explored by Quintana Minerals Corporation, Chevron Standard Limited, Kidd Creek Mines Ltd. and others because of a similar geological setting to deposits in the Highland Valley, the presence of a favourable volcanic setting for massive sulphide deposits, and the presence of high grade baritic lead-zinc silver mineralization. Recent interest has been stimulated by the discovery of strong gold values with hematite-chalcopyrite mineralization on the surrounding Diane Property of Abermin Corporation and in the number 3 shaft on the Charmer Zone. The Iron Mountain Property contains hematite-chalcopyrite zones which had not been adequately tested for gold content.

The 1989 work program conducted for Golden Dynasty Resources Ltd. tested the Comstock zone with 3 diamond drill holes (IM-89-1 to 3) and tested auriferous quartz veins in the Shaft 3 with one hole (IM89-4). The grid constructed by Chevron Minerals on the LD zone was relocated and extended with soil samples (498), VLF-EM and magnetics completed over about 12.5 km. Mineralization developed by the Leadville shaft is either of limited extent or offset by faults. A five foot intersection below the number 3 shaft in the Charmer Zone contained 4700 ppm copper, 23.2 ppm silver and 760 ppb gold. Soil samples from the LD zone contained up to 366 ppm copper, 835 ppm lead, 2772 ppm zinc, 2.7 ppm silver and 2204 ppm barium with modestly anomalous gold values up to 39 ppb.

Field checking is recommended for the anomalous zone of barium, lead, and zinc to the east of the LD zone but further targets must be developed before undertaking the Stage 2 drill program recommended by Crooker (1987).

INTRODUCTION

The Iron Mountain Property, consisting of 7 metric mineral claims totaling 32 metric units covers about 800 hectares in the Nicola Mining Division near Merritt, British Columbia. The property was acquired by Golden Dynasty Resources Ltd. in July 1987 to explore gold bearing quartz-specularite veins on the Fierro # 3 claim and to investigate the possibility of stratabound, precious metal enhanced base metal deposits along strike and dip from the Lucky Todd (Leadville) Shaft and other old workings. Based on a 1987 exploration program conducted for Golden Dynasty, Mr. Grant F. Crooker FGAC (1987) recommended a Stage I diamond drill program and systematic grid coverage for the LD zone.

Peter Christopher & Associates Inc. was retained by the management of Golden Dynasty to conduct the exploration program recommended by Crooker (1987). An initial property inspection was conducted by the writer on May 2nd and 3rd, 1989 with a notice of work and reclamation filed in Kamloops on May 2nd, 1989.

The Stage I exploration program on the Iron Mountain Property was conducted between May 11, 1989 and June 30, 1989. This report summarizes the results of the Stage I Program.

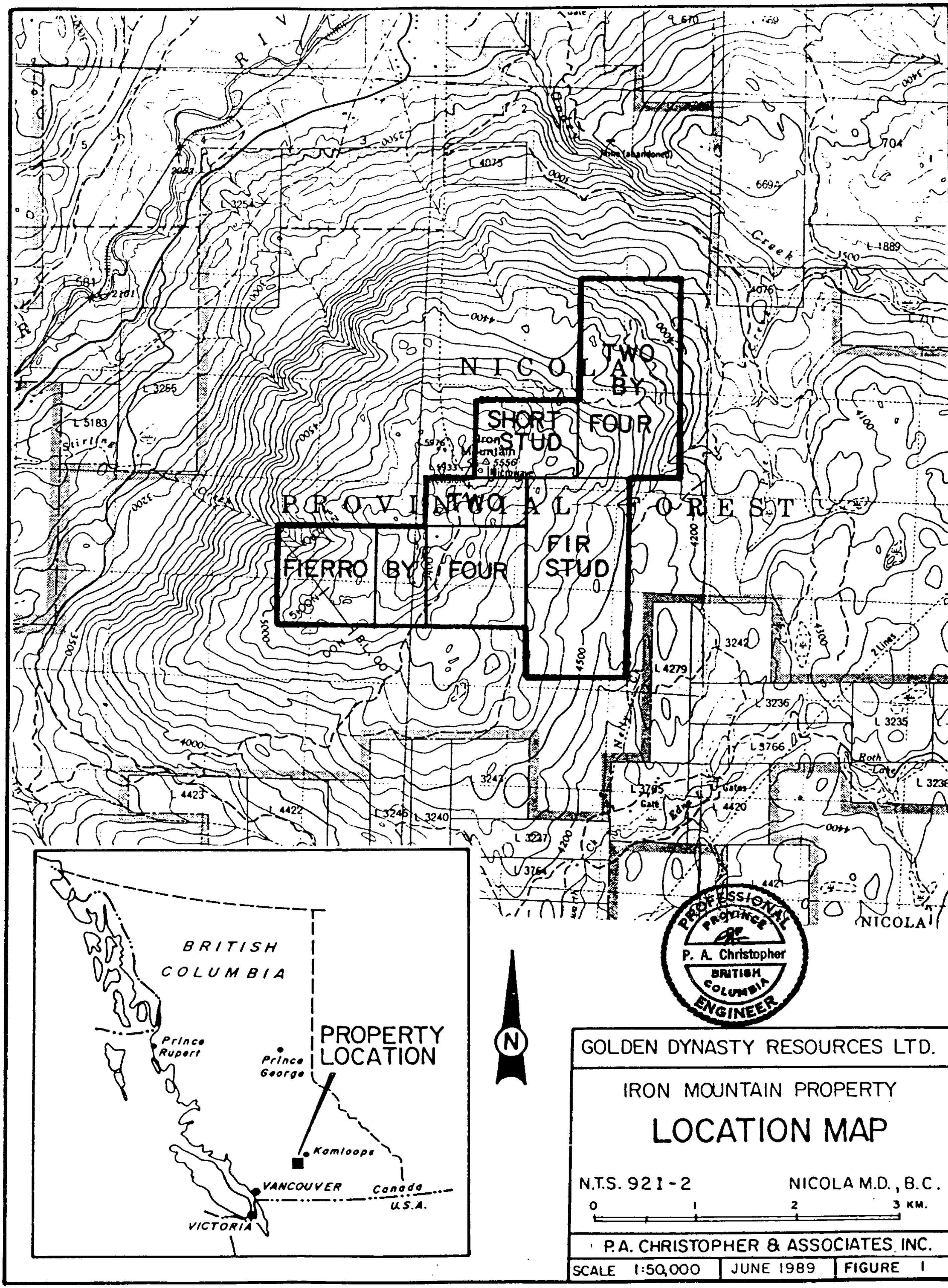
LOCATION AND ACCESS (FIGURES 1 & 2)

The Iron Mountain Property is located on the northeast, east and south flanks of Iron Mountain approximately 7 km south of Merritt, British Columbia in the Nicola Mining Division. The property is centered at geographic coordinates 50^{o} 03'N. latitude and 122^{o} 45'W in N.T.S. map sheet 92-I-2.

Access to the property is via a well maintained road used for servicing a microwave installation at about 1694 meters on Iron Mountain. The access road is reached via the Veale road which branch off the Coldwater Road approximately 5 km southwest of the Coldwater Road junction with Highway 5. Access to the Two By Four and Fir Stud claims is via the Fox Farm road which branches off Highway 5 approximately 2 km east of Merritt or via the Godey Creek Road which branches from the Coldwater Road about 2 km south of highway 5. The Coquihalla Highway cuts across the western flank of Iron Mountain within 2 km of the western boundary of Fierro #3. The Coquihalla Highway allows same day, drive in access to the property from Vancouver and one hour drive in access from Kamloops, British Columbia.

PHYSIOGRAPHY AND VEGETATION

The property is situated within the Interior Plateau of south central British Columbia with the topography of Iron Mountain typical of the high rolling uplands of the region. Elevations on the property range from 3700 feet (1128 meters) in the northeast corner of the Two By Four claim to 5556 feet (1694 meters) at the summit of Iron Mountain with most of the property above 4700 feet (1433 meters).



GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

LOCATION MAP

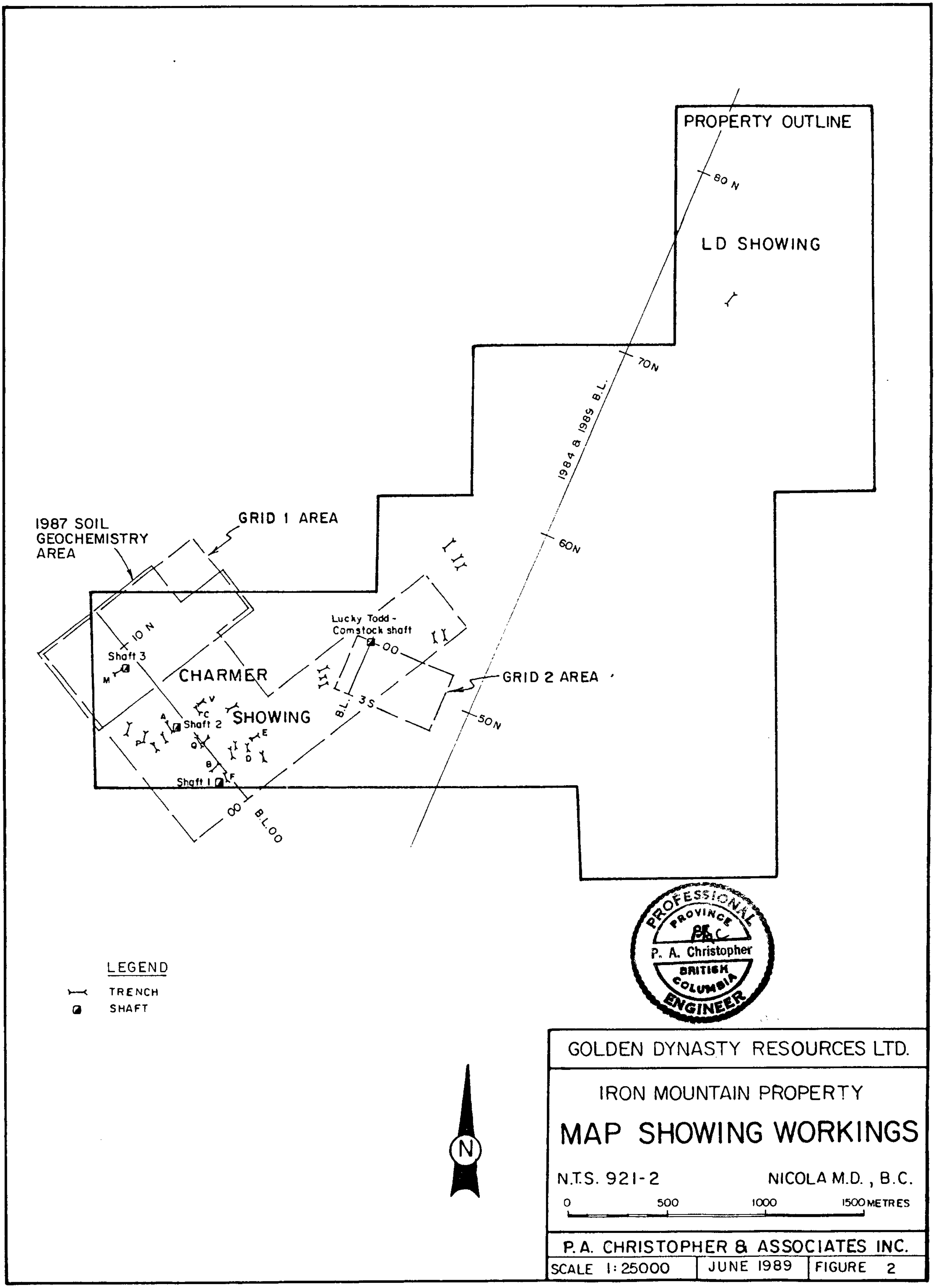
N.T.S. 92 I - 2 NICOLA M.D., B.C.

0 1 2 3 KM.

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE 1:50,000	JUNE 1989	FIGURE 1

CHONG


PROPERTY OUTLINE
80 N
LD SHOWING
70N
1984 & 1989 B.L.
60N
1987 SOIL GEOCHEMISTRY AREA
GRID 1 AREA
10 N
Shaft 3
CHARMER
SHOWING
Shaft 2
Shaft 1
Lucky Todd - Comstock shaft
00
B.L. 3S
GRID 2 AREA
50N
00
B.L.00
LEGEND
TRENCH
SHAFT
PROFESSIONAL ENGINEER
PROVINCE OF B.C.
P. A. Christopher
BRITISH COLUMBIA
N
GOLDEN DYNASTY RESOURCES LTD.
IRON MOUNTAIN PROPERTY
MAP SHOWING WORKINGS
N.T.S. 921-2
NICOLA M.D., B.C.
0
500
1000
1500 METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE 1:25000
JUNE 1989
FIGURE 2

CHONG

The property is moderately forested with fir, spruce and pine with commercial stands generally restricted to lower elevations. Open timbered and grassy slopes occur on the plateau top which along with broad valleys are used for rangeland. Till and soil cover ranges from one to several meters and is generally thicker on the lower slopes.

PROPERTY DEFINITION

The Iron Mountain Property, comprised of seven metric claims totaling 32 units covers about 800 hectares in the Nicola Mining Division, British Columbia. Claim records, examined in the recording office in Merritt, British Columbia indicate that the claims comprising the Iron Mountain Property were acquired between July 7, 1978 and December 11, 1981 by K.W. Livingstone or his agent. Pertinent claim data is summarized in Table 1 and claim locations are shown on Figure 2.

Table 1. Pertinent Claim Data for Iron Mountain Property.

Name	Record #	Units/Shape	Recorded	Work Due*	Staker
TWO	480(7)	2/1Nx2E	July 7/78	1998	K.W.Livingstone
BY	481(7)	2/2Sx1W	"	1998	"
FOUR	482(7)	4/2Sx2E	"	1998	"
TWO BY FOUR	484(7)	8/4Nx2E	"	1998	"
SHORT STUD	667(7)	4/2Sx2W	July 26/79	1998	W.A. Howell
FIERRO #3	997(2)	4/2Nx2E	Feb. 5/81	1998	"
FIR STUD	1216(12)	8/4Sx2W	Dec. 11/81	1994	"

* Prior to Recording 1989 Work Program

HISTORY

The earliest exploration reported in the Iron Mountain area was in the area of the Fierro 3 claim. The work apparently focused on base metal mineralization occurring as stringers and blebs in andesitic flows and pyroclastics and culminated in the sinking of three shafts, the Charmer (Shaft 1), the Islander (Shaft 2) and the Victoria (Shaft 3) in 1896 (Nelles and Marshall Smith, 1987).

The initial discovery of the 'Leadville' barite-galena showing was made by Emmett Todd in 1927 with development including sinking of a 70 foot shaft in 1927 and 1928. In 1929, Comstock B.C. Ltd held 1000 acres of claimed land but failed to expedite the planed exploration programs.

In 1947 George Hunter and partners acquired the Leadville and renamed the shaft 'Lucky Todd'. The shaft was rehabilitated with a 36 ton shipment to Trail yielding 67 ounces of silver, 11,819 pounds of lead and 484 pounds of zinc.

In 1951 Granby Mining Corporation dewatered and sampled the 'Lucky Todd Shaft'. In 1958, New Jersey Zinc is reported to have conducted diamond drilling north of the Leadville Shaft area.

From 1968 to 1974 Acoplomo Mining and Development Co. Ltd., under the direction of Sherwin F. Kelly conducted magnetometer, E.M., soil sampling and diamond drilled 586 feet. Location and results of diamond drilling are unknown.

In 1977 Quintana Minerals Corporation mapped the property and in 1978 Dr. W.J. McMillan of the British Columbia Ministry of Mines conducted regional mapping of Iron Mountain (McMillan, 1979).

From 1979 to 1981 Chevron Canada Ltd. held the property under option from Gordon Richards of JMT. Chevron conducted geological mapping, soil sampling and geophysical surveys. In 1983 Billiton Canada Ltd. conducted a Pulse E.M. test over the Lucky Todd area of the property and in 1984 Kidd Creek Mines Ltd. conducted soil and rock geochemical surveys and 13.5 line kilometers of magnetometer, induced polarization survey and resistivity surveys.

In 1983, Aberford Resources Ltd. located the Diane 1-5 claims, west of the Iron Mountain property, based on anomalous results from a regional geochemical program. Prospecting, geological mapping and geochemistry was successful in locating several areas of mineralization. In 1984, Kidd Creek Mines Ltd. conducted ground geophysical surveys and rock and soil geochemistry along four kilometers of cut line.

The 1984 induced polarization survey by Kid Creek Mines Ltd. covered the trench A through E area of the Fierro 3 claim. The chargeability pattern is consistent with sulphide content of 1 to 3 percent but the abundant magnetite and hematite exposed in trenches responds poorly to the induced polarization method (Boronowski and Hendrickson, 1984).

In 1986, Internstional Maple Leaf Resources Corp. optioned the Diane claims from Abermin Resources Ltd. and conducted rock and soil geochemistry, geological mapping, prospecting and trenching. A airborne geophysical survey was conducted by Aerodat Ltd. of Mississauga, Ontario.

In May 1987, Merlin Resources Ltd. acquired an option to earn a 50% interest in the Diane Claims. In 1988 Merlin drilled 570 meters in 9 holes on the Diane 1 claim with the best intersection of 1.38 meters of 15.56g (0.454 oz/t Au) and 16.43g/t (0.479 oz/t Ag) at 59 meters in drill hole STR-88-1.

In July 1987 Golden Dynasty Resources Ltd. obtained an option to purchase the Iron Mountain Property from R.O.R. Enterprises Ltd. and retained Peter Christopher and Associates Inc. to conduct a geochemical sampling, VLF-EM and magnetic survey with the construction of 25 line kilometers of grid and the collection of 360 soil and 18 rock samples (Crooker, 1987).

This report covers a geochemical, geophysical and drilling program conducted by Peter Christopher & Associates Inc. for Golden Dynasty Resources Ltd. in May 1989.

WORK PROGRAM

The 1989 field program was conducted between May 1, 1987 and May 26, 1989 with Peter A. Christopher P.Eng., PhD. of Peter Christopher & Associates Inc. to supervise the field program and prepare an assessment reports on the property. Mr. Gerry Hayne B.Sc collected data for the magnetic and VLF-EM surveys and F.L. Chong of Chong Drafting was retained to plot magnetic data and plot profiles for the VLF-EM surveys. Geochemical values were plotted and contoured by Chong Drafting.

The 1989 work program consisting of geochemical sampling, VLF-EM and magnetic surveys and 1495 feet of NQ diamond drilling in four holes. Geochemical and geophysical surveys were conducted over the LD showing area. Diamond drilling was conducted in the Grid #1 area on the Fierro 3 claim and Grid #2 area covering the Lucky Todd-Comstock Shaft area on the By and Four claims. Drill holes were logged and sampled by the writer with a total of 82 samples of split core were collected. Drill logs are presented in Appendix C with drill holes summarized on Figures 11a through 11d. Drilling was contracted by Iron Mountain Drilling Ltd. of Merritt, B.C.

A total of about 22 line kilometers of grid was chained and flagged in the Grid #1 and LD areas. Stations were chained, flagged and some picketed at 25 meter intervals. A soil and rock geochemical program was conducted over the LD Grid area with a total of 498 soils collected from the B horizon at a depth of about 25 centimeters, placed in kraft soil bags and shipped to Acme Analytical Laboratories Ltd. in Vancouver for 30 element ICP and gold geochemical analyses. Contoured geochemical maps for gold/silver, copper/barium, and lead/zinc are presented as Figures 5 through 7. A total of 5 rock samples were collected mainly from old workings in the LD and Grid # 1 area with sample locations and significant gold results plotted on Figures 2 and 5. Analytical values are presented in Appendix A.

VLF-EM readings were generally taken using Seattle for station 1 except as noted on plots (Hawaii used on May 24 for part of Line 75N and 77N) and Cutler as station 2 (Annapolis used on May 15 for lines 75N through 78N). Base station readings indicated diurnal magnetic variations of less than 100 gammas during the survey and considering the strong magnetic relief in the grid area, no correction for diurnal variation was made. Copies of field notes for magnetic and VLF-Em data are presented as Appendix B. Profiles for VLF-EM data are presented as Figures 8 and 9 with contoured magnetic data presented as Figure 10. Copies of field notes for geophysical surveys are presented in Appendix B. A total of 12 km of magnetic and VLF-Em survey was completed.

A cost statement for the 1989 work program is presented as Appendix D to this report.

REGIONAL GEOLOGY

The Iron Mountain Property lies within the Intermontane Belt of the Canadian Cordillera and is underlain by marine and continental volcanic and sedimentary rocks of the Upper Triassic, Nicola

Group. The Iron Mountain Property is underlain by rocks classified by Preto (1979) as part of the Western Belt of the Nicola Group which is situated west of the Allison Fault zone. Cretaceous Kingsvale Group volcanic and sedimentary rocks outcrop to the north and east of the property. The area is segmented by northeasterly, northwesterly and northerly trending faults.

The regional geology has been mapped by Cockfield (1939-1944, 1948), Schau (1968), Preto (1979) and McMillan (1977, 1978).

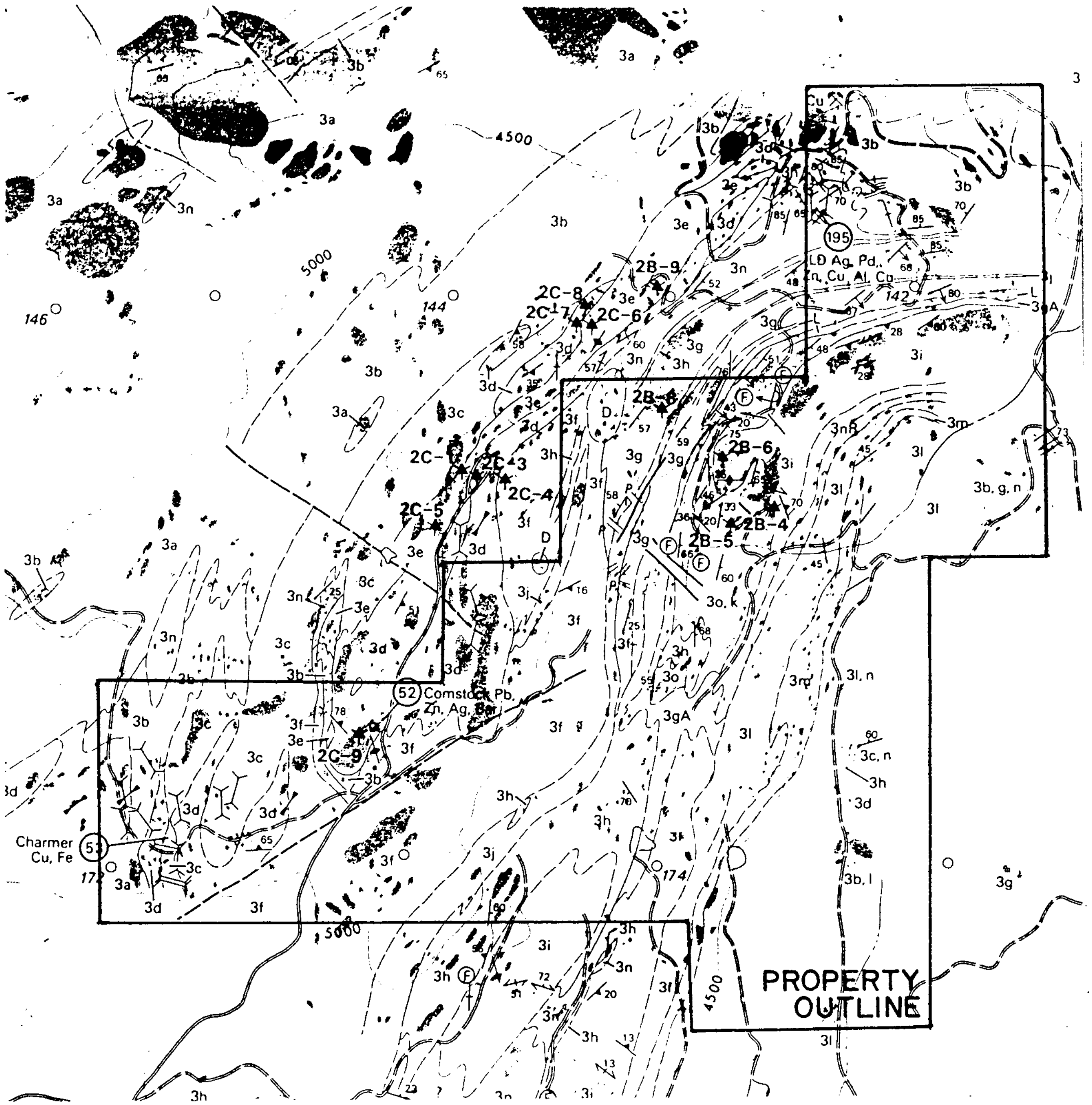
PROPERTY GEOLOGY (Figure 3)

The description of the local geology of the Iron Mountain Property was summarized by Crooker (1987) as follows: "The geology of Iron Mountain was mapped in detail by W.J. McMillan (Paper 79-1 p.34; reproduced as Figure 3) in 1978. A 5,000 meter thick section of Nicola Group is exposed on Iron Mountain. At the base of the section is a microdiorite of unknown thickness. The microdiorite is overlain by an approximately 1500 meter thick sequence of basaltic and andesitic flows. Flow breccia and andesitic volcanic breccia occur within the flows. Near the top of the flow unit, rhyolitic breccias and potassium-rich rhyolitic lavas become common with lesser chloritic fragment acid to andesitic breccias.

The acid lava and breccia zone is overlain southward by basaltic to andesitic flows with contained argillaceous limestones indicating periods of quiescence and felsic tuffs indicating periods of explosive volcanic activity. To the northeast, the basic flows pinch out and sandy to pebbly volcano-sedimentary rocks overlie the rhyolitic zone. Limestone breccia overlies the volcano-sedimentary rocks with a thin bed of impure limestone overlying the limestone breccia. Further northeast, the rhyolitic zone and overlying sedimentary rocks abut against a large, irregularly lensoid body of andesitic lapilli to bomb breccia. The thin impure limestone unit also overlies the andesitic lapilli to bomb breccia and volcanic breccias with mainly acidic clasts overlie the limestone.

An 8 kilometer long marker unit is composed of feldspathic, often quartz bearing, red lapilli tuff. To the south it is overlain by limestone bodies and overlies basic volcanic rocks. Northerly, it is overlain by andesitic to acidic volcano-sedimentary rocks and breccias. Fossiliferous limestone layers are found within the volcano-sedimentary rocks. A distinctive golden brown weathering argillite to sandstone succession ranging up to 10 meters in thickness forms the top of the sedimentary unit in the northeast.

Lensy bodies of siliceous volcanic rocks overlie the sedimentary unit to the northeast, and occur within the limestones to the south. Dark green, massive to bedded fragmental plagioclase-bearing crystal lithic tuffs and flows interfinger with the dacite to the east of Iron Mountain peak. The feldspathic volcanics appear to be largely of pyroclastic origin and the variations in rock types resemble those of subaerial cinder cones.



GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

GEOLOGY

N.T.S. 92I-2 NICOLA M.D., B.C.

0 500 1000 METRES

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE 1:25,000	JUNE 1989	FIGURE 3a

PROFESSIONAL ENGINEER — PROVINCE OF BRITISH COLUMBIA — P. A. Christopher

CHONG

LEGEND

LATE TRIASSIC
WESTERN BELT (KARNIAN TO NORIAN)

3p	GREEN·QUARTZ PLAGIOCLASE DACITE PORPHYRY FLOWS AND BRECCIA, CHERTY AND CHYSTAL TUFFS
3o	MONOMICTIC (FLOW) BRECCIA, CLASTS ARE PLAGIOCLASE PORPHYRITIC
3n	VOLCANIC SANDSTONE TO SILTSTONE AND TUFF, RED VERSION (R)
3m	RED REEFOID LIMESTONE
3l	RED TO PURPLE ANDESITIC BRECCIA AND TUFF
3k	GREEN TO GREY-GREEN PLAGIOCLASE CRYSTAL-LITHIC ASH TO LAPILLI TUFF AND BRECCIA
3j	RED ACCRETIONARY LAPILLI TUFF, LITHIC CLASTS, QUARTZ, AND FELDSPAR CRYSTAL FRAGMENTS
3i	GENERALLY GREEN MASSIVE TO FLOW LAYERED POTASSIC FELDSPAR-POOR DACITE FLOWS AND BRECCIA; LOCAL DACITE TUFF
3h	MASSIVE TO POORLY BEDDED LIMESTONE, LOCALLY FOSSILIFEROUS AND REEFOID, ASSOCIATED LIMY SEDIMENTARY ROCKS
3g	POLYMICTIC ACIDIC FRAGMENTAL VOLCANIC ROCKS WITH LOCAL *PYRITIC CLASTS AND BEDS*; PARTS OF THE SECTION HAVE INTERLAYERED ARGILLITE (A), LIMESTONE (L), AND VOLCANIC SANDSTONE
3f	AMYGDALOIDAL DARK GREEN PLAGIOCLASE ANDESITE FLOWS, AGGLOMERATE OR FLOW BRECCIA
3e	ASH FLOW TUFF, PROBABLY SUBMARINE; LAPILLI TO ASH-SIZED CLASTS
3d	BROWN TO PINKISH POTASSIC FELDSPAR-RICH DACITE TO RHYOLITE FLOWS AND FLOW BRECCIAS; WHITE TO PALE GREEN RHYOLITE
3c	MIXED ANDESITE-TO DACITE-CLAST VOLCANIC BRECCIA
3b	GREEN TO GREY ANDESITIC VOLCANIC BRECCIAS
3a	DARK GREY TO GREEN MASSIVE TO PLAGIOCLASE PORPHYRITIC ANDESITE TO BASALT FLOWS; AUGITE-RICH VARIETIES (A) SIMILAR TO UNIT 1a; RED TO BROWN VARIETIES (R); CHLORITE SCHIST (S) OR GNEISS (Gn) DERIVED FROM THE VOLCANIC ROCKS

Geology by W. J. McMillanetal
Preliminary Map 47, 1981

CUTTING WESTERN BELT ROCKS

DIORITE (D), MICRODIORITE (MD), PORPHYRY DYKES P

SYMBOLS

AREA OF OUTCROP

GEOLOGICAL BOUNDARY DEFINED, APPROXIMATE

FAULT APPROXIMATE, ASSUMED

ATTITUDE OF BEDDING:

TOPS UNKNOWN, VERTICAL, DIP UNKNOWN 45

TOPS KNOWN, OVERTURNED

ATTITUDE OF SCHISTOSITY

PRIMARY IGNEOUS FLOW STRUCTURES:

INCLINED, VERTICAL, DIP UNKNOWN

FOSSIL LOCALITY Ⓕ

DYKE P

TRENCH

ADIT OR TUNNEL

SHAFT

INCLINED SHAFT

PROSPECT PIT

MINERAL SHOWING, WITH NAME, MINERAL INVENTORY NUMBER (i.e., 92I/SE-55) AND COMMODITY ⚒ or (51) SOO Cu

COMMODITIES

COPPER	Cu	GOLD	Au
IRON	Fe	SILVER	Ag
MOLYBDENUM	Mo	BARITE	Bar
LEAD	Pb	COAL	Coal
ZINC	Zn		

CHEMICAL ANALYSIS SAMPLE LOCATION

To accompany report by G.F. Crooker

GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

LEGEND FOR GEOLOGY

N.T.S. 92I-2 NICOLA M.D., B.C.

P. A. CHRISTOPHER & ASSOCIATES INC.

SCALE —	JUNE 1989	FIGURE 3b

CHONG

Overlying the dacitic to feldspathic volcanics are red sandstones which are in turn overlain by red to purple volcanic breccias. A calcareous reefoid unit, in which calcareous organic remains occur in a dark hematitic red matrix, overlies the volcanic breccias. The reefoid unit has a strike length of approximately 4 kilometers and is of variable thickness. A mixed assemblage of acidic breccias, and andesitic breccias, flows and tuffs form the top of the section.

Rock units strike northerly to northeasterly and have steep easterly dips. Limited evidence appear to indicate tops to the east. The area is disected by northwest trending structures which control the location of Godey Creek and Kwinshatin Creek valleys. The northwest structure contains auriferous quartz veins on the Fierro #3 claim. The northwest structures are cut and slightly offset in a right lateral direction by northerly to northeasterly structure that lie east of Iron Mountain."

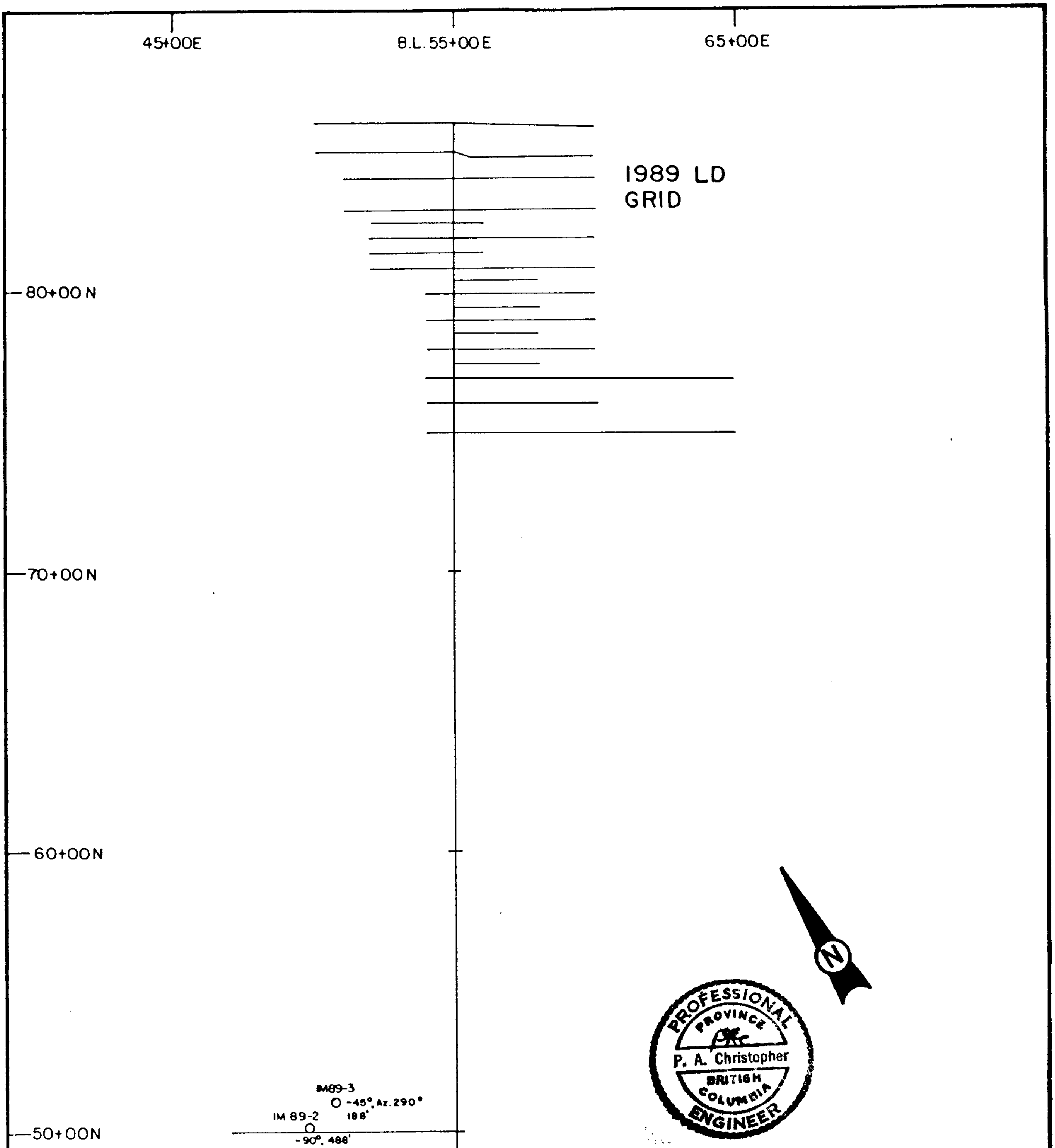
MINERALIZATION

Two main types of mineral showings are presently known to occur on the Iron Mountain Property. The first type, lead-zinc-silver-barite (gold ?) is volcanogenic massive sulphide or replacement type minerlaization that occurs at the Lucky Todd-Comstock Shaft and at the LD Showing (Figures 2 and 3). At the Lucky Todd showing, barite rich lead-zinc-silver mineralization has been explored by a >100 foot inclined shaft. The shaft is inaccessible at the present time but Cockfield (1948) describes the zone as striking N25^{o}E and dipping 80^{o}NW with heavy impregnation of barite accompanied by galena, sphalerite and pyrite. Dump material indicates at least two types of mineralization: banded veins and possibly bedded mineralization in a flow banded, K-rich rhyolite lava and rotated blocks of bedded, impure barite that carry small amounts of sphalerite, galena and grey copper. A shipment in 1947 of 36 tons of ore to the Trail smelter gave net contents of 67 oz silver (1.86 oz/ton), 11,819 lbs. lead (16.04%) and 484 lbs zinc (0.67%).

At the LD showing silver-lead-zinc-copper-barite-gold has been exposed in several old pits. Samples of float and outcrop by Kid Creek Mines personnel (Boronowski and Hendrickson, 1984) gave copper values ranging from 10 to 3240 ppm, silver values ranging from 0.4 to 59.4 ppm an gold values ranging from 1 to 2960 ppb. The writer collected three samples from mineral occurrences in the LD grid area with values ranging up to 11623 ppm copper, 8989 ppm lead, 13514 ppm zinc, 27.9 ppm silver and 129 ppb gold (see Figure 5).

Crooker (1987) described a number of geological conditions on Iron Mountain that fit into the volcanogenic massive sulphide conceptual model. These features include the presence of dacitic to rhyolitic flows and flow breccias, discontinuous pods and thin jasper beds, sulphide fragments, bedded gypsum, and galena-sphalerite-barite mineralization. Howell (1987 misc. notes) suggested possible volcanic centers near Iron Mountain Peak, the Lucky Todd shaft, Charmer zone and LD occurrence.

The second type of mineral showing present on the Iron Mountain property is structurally controlled auriferous quartz-specularite-



GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

1989 GRID & DRILL HOLE LOCATION

N.T.S. 92I-2 NICOLA M.D., B.C.

0 500 1000 METRES

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE 1:20,000	JUNE 1989	FIGURE 4

CHONG

chalcopyrite veins in the Charmer Zone. A number of trenches and 3 shafts have exposed quartz-specularite veins over a discontinuous strike length of 800 meters. At shaft 3 the vein strikes 160^{o}-340^{o} and dips at 50-55^{o} to the west. At Shaft 3 (Figure 2) three quartz veins varying from 5 to 25 cm in width occur within a 2 meter wide zone in basaltic andesite. The veins are mineralized with chalcopyrite, malachite and grey sulphides. Specular hematite occurs in patches up to 15%. One meter chip samples IM-22 and IM-24 taken by Crooker (1987) returned 0.295 and 0.286 oz Au/ton respectively. Drill hole IM-89-4 tested below shaft 3 and intersected a zone between 130 and 195 feet which contained an average of 1030 ppm copper which included five feet from 190 to 195 feet which contained 4700 ppm copper, 23.2 ppm silver and 760 ppb gold.

GEOPHYSICAL SURVEYS

A total of 12 line kilometers of VLF-EM and magnetics was completed during the 1989 field season. The VLF-EM and magnetic surveys were completed over about 12 kilometers of the LD grid area (Figures 4, 8a, 8b, & 9). A Geonics EM-16 unit was employed for the VLF-EM survey with Cutler, Maine (Figure 8a) and Seattle (Figure 8b) the preferred stations and Hawaii and Annapolis used when either Cutler or Seattle were not transmitting. A Scintrex MP-2 proton procession magnetometer with a pole mounted sensor was used for collecting magnetic field readings. VLF-EM data profiles were plotted and magnetic data was contoured (Figure 9) by Chong Drafting. Diurnal variations in the magnetic field were evaluated by looping to established base stations. The diurnal variations were found to be low in comparison to total magnetic relief and machine readings were employed without correction for diurnal variation.

VLF-EM Results

LD Grid was surveyed to test for conductors along strike from the LD showings. A number of strong NE trending conductors are associated with what may be NE trending, structurally controlled drainage. West of the baseline, a strong NE trending conductor follows a creek valley. At the west end of line 81N, the conductor coincides with a strong magnetic low. The magnetic low and VLF-EM conductor extend northeasterly along a creek to the baseline at 86N. On both Seattle and Cutler stations, a conductor extends from line 75N 54+75E to line 80N 55+75E and parallels a valley situated just west of the LD showing. A northeasterly trending conductive zone revealed by the Seattle channel is associated with a copper occurrence at 54+50E on Line 82N.

Magnetic Results

Magnetic intensity was measured at 25 meter intervals in the LD Grid area with values ranging from a low of 55782 gammas at 52+25E on line 81N to 57421 gammas at 53+75E on line 81N. Values from the 1989 survey were contoured with a 200 gamma contour interval on Figure 9. The main magnetic feature is a strong magnetic low which coincides with a two station VLF-Em anomaly and extends from 52+25E on line 81N to 55+25E on line 86N. A strong magnetic high occurs just east of the southerly end of the anomaly. The strong low follows a creek that may be along an altered fault structure.

GEOCHEMICAL SURVEY

Soil geochemical sampling was conducted to complete coverage of the LD showing area. Four hundred and ninety eight samples were taken in the LD Grid area and analyzed at Acme Analytical Laboratories Ltd. for 30 element ICP and for gold by Atomic Absorption. The results for gold/silver, copper/barium and zinc/lead are shown on Figures 5 to 7 respectively.

Five rock geochemical samples were collected from trenches in the LD and Grid 1 area. LD area rock sample results are shown on Figure 5. A total of 82 core samples were obtained by splitting of NQ core with sample intervals summarized on core logs in Appendix C. Rock samples were analyzed by 30 element ICP and for gold by Atomic Absorption.

Results

Gold values in soils range from 1 to 39 ppb with values of 5 and above considered of interest and values over 20 ppb considered anomalous. Values of 10 ppb are contoured on Figure 5 but only seven isolated samples of 10 or more were found and only one above 20 ppb. Rock sample C14936 at L82N 54+80E contained 129 ppb and was associated with an isolated high soil of 14 ppb.

Silver values in soils ranged from 0.1 ppm to 2.7 ppm with 6 values over 0.9 considered weakly anomalous and contoured on Figure 5. The six anomalous silver values are all in the area of the LD showings and within a zone of anomalous barium. A 27.9 ppm rock sample was obtained from the LD showing at L77+80N 56+15E.

Copper values in soils ranged from 9 to 366 ppm with 37 values above 50 ppm considered of interest and contoured at the 50 ppm and 100 ppm levels. The anomalous copper values occur in a NE trending belt in the center of the grid area. Rock sample C14936 contained 11623 ppm copper for a six foot chip across a shear zone mineralized with chalcopyrite, bornite, malachite and azurite.

Barium values in soils range from 59 to 2204 ppm with values over 300 ppm considered to be of interest and 20 samples over 600 ppm considered strongly anomalous and contoured on Figure 6. A NE trending zone of anomalous barium values coincides with anomalous copper values and known showings. In the area of the LD showing, strong lead and zinc values are associated with strong barium.

Lead values ranged from 2 to 835 ppm with eighteen values of 30 ppm and above considered of interest and contoured on Figure 7. The strongest lead response (second highest zinc 2683 ppm) occurs east of the main LD showing at L78N 58+50E. The sample warrants follow-up prospecting.

Zinc values range from 28 to 2772 ppm with 52 values of 200 ppm or greater considered anomalous and contoured on Figure 7 at 200 and 500 ppm. Anomalous zinc values are concentrated in the area of LD showing and in a band extending southeasterly from the LD showing.

1989 DRILLING

The 1989 drill program consisted of four NQ diamond drill holes (Figures 4, 10, 11a-11d) totaling 1495 feet (455.7 meters). Iron Mountain Drilling Ltd. of Merritt, B.C. (Ph. 378-4843) was the drill contractor and provided a D6 Cat for drill setups. Drilling started on May 11, 1989 and was completed on May 25, 1989. Drill core is stored near the Leadville Shaft on the Iron Mountain property. Typical specimens from drill holes were collected and are stored by Peter Christopher & Assoc. Inc. in Vancouver. Core selected for sampling was split and logged by the writer with 82 core samples selected for analysis. Drill logs with a summary of sampling and results is provided in Appendix C. A summary of dill holes is provided in Table 2.

Table 2. Drill Hole Summary.

Hole	Grid Location	Bearing	Angle	Length Ft/M.	Colar El. M.
IM-89-1	L45+80N 50+20E	293°	-45°	425'/129.5	1588
IM-89-2	L50+15N 49+85E	Vertical	-90°	488'/148.7	1653
IM-89-3	L51+00N 50+10E	290°	-45°	188'/ 57.3	1642
IM-89-4	L 8+40N 0+65W	042°	-45°	394'/120.1	1565

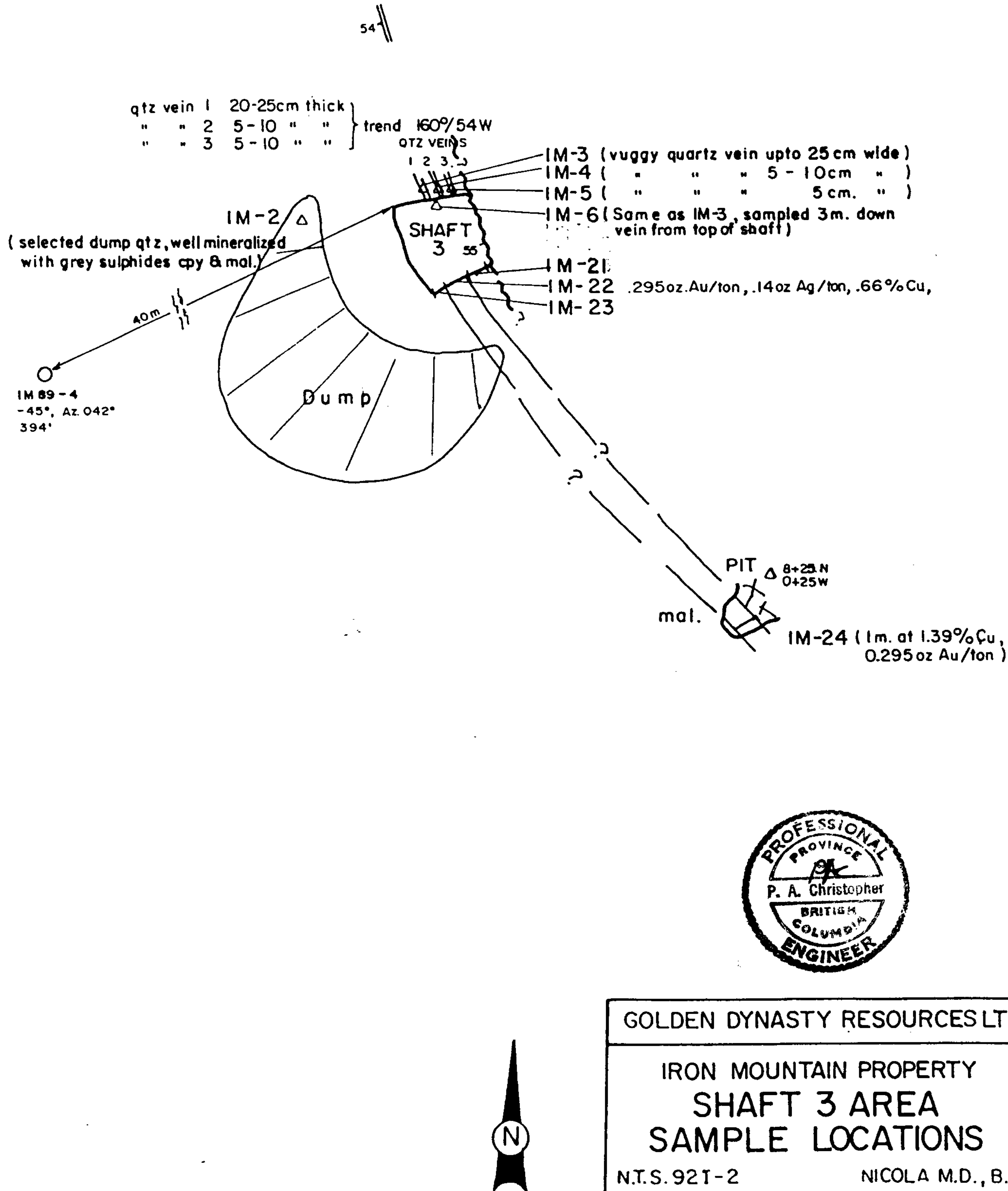
Drill hole IM-89-1 was drilled to test moderately anomalous base metal values associated with a jasperoid horizon along strike from the Leadville (Lucky Todd) shaft. From 340 to 390 feet, the hole contained a hemititic stockwork in rhyodacitic and rhyolitic breccia. Mineralization consisted of disseminated pyrite, veinlets of hemitite and minor chalcopyrite, and quartz/specular hematite veinlets. The interval 340-390 feet averaged 585 ppm copper with the interval 350-360 feet containing 117 ppb gold and the interval 370-380 containing 8.6 ppm silver.

Drill holes IM-89-2 and IM-89-3 were drilled to test for strike and dip extensions of mineralization exploited by the Leadville (Lucky Todd) Shaft. The holes did not intersect mineralization similar to what present in outcrop and in the shaft dump. Mineralization is either very restricted or displaced by faulting.

Drill hole IM-89-4 (Figure 10) tested below Shaft 3 in the Charmer Zone. The hole intersected 65 feet (130 to 195 feet) grading 1031 ppm copper which included 5 feet (190-195 feet) grading 23.2 ppm silver, 760 ppb gold and 4700 ppm copper. The shear zone exposed in shaft 3 appears to decrease in grade at depth.

DISCUSSION OF IRON MOUNTAIN PROPERTY

The Iron Mountain Property is an established mineral property with three documented mineral occurrences (B.C. Government Mineral Inventory 92I/SE-52 Lucky Todd-Comstock; 53 Charmer; 195 LD) with reported copper-iron-gold and silver-lead-zinc-copper-gold mineralization. Each of the know mineral zones has potential for vein type precious metals and volcanic hosted massive sulphide deposits.



PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher

GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

SHAFT 3 AREA SAMPLE LOCATIONS

N.T.S. 92I-2 NICOLA M.D., B.C.

0 5 10 METRES

P. A. CHRISTOPHER & ASSOCIATES INC.

SCALE 1:200	JUNE 1989	FIGURE 10

CHONG

Exploration during the 1989 field season concentrated on extending previous geochemical and geophysical coverage in the area of the LD Zone. Geochemical results shows a barium, copper, zinc and lead anomaly associated with the LD showing area, but surface values must improve at depth for the showing to be of economic interest. Surface geochemical sampling failed to enhance the previously suggested precious metal association.

The 1987 exploration program (Crooker, 1987) was successful in locating a meter wide zone at shaft #3 (Figure 10) with two chip samples averaged 0.291 oz Au/ton over one meter. IM-89-4 tested below the mineralized shear and intersected 65 feet averaging 1031 ppm copper with a best interval from 190-195' of 4700 ppm copper, 23.2 ppm silver and 760 ppb gold. Unfortunately the mineralization at Shaft 3 appears to diminish at depth.

The Lucky Todd-Comstock was tested along strike by IM-89-1 with the hole directed at a jasperoid horrizon and moderately anomalous base metal soil geochemical anomaly. Hole 1 contained only moderately anomalous copper and zinc values.

The Lucky Todd-Comstock shaft are was tested by holes IM-89-2 and IM-89-3. The holes failed to intersect the mineralized zone which must be a lens or dislocated by faulting.

CONCLUSIONS AND RECOMMENDATIONS

The Stage 1 exploration program conducted by Golden Dynasty Resources Ltd. on the Iron Mountain Property has outlined a base metal soil geochemical anomaly in the LD showing area. The presence of barium with copper, lead and zinc values suggests a possible massive sulphide environment. Values in the area must improve at depth for the zone to have economic significance.

Drilling of the Lucky Todd-Comstock Zone has not located significant intersections, and testing below Shaft 3 in the Charmer zone located a broad zone with low grade copper (1031 ppm over 65 feet) and reduced gold values (760 ppb over 5 feet).

Since Stage 1 drilling has not defined significant intersection, continuation with the Stage 2 drilling program recommended by Crooker (1987) is not recommended.

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CERTIFICATE

I, Peter A. Christopher, PhD, P.Eng., of 3707 West 34th Avenue, Vancouver, British Columbia V6N 2K9, do hereby certify that:

1) I am a consulting geological engineer and have maintained an independent practice since 1981.

2) I am a Fellow of the Geological Association of Canada, a member of the Canadian Institute of Mining and Metallurgy, a member of the Society of Economic Geologists and a registered member of the Association of Professional Engineers of B.C. since 1976.

3) I hold a PhD. (1973) with a major in Geology from the University of British Columbia.

4) I have been practising my profession as a Geologist for over 22 years.

5) I am a director of Golden Dynasty Resources Ltd. and hold 20,000 shares of the issued securities of Golden Dynasty Resources Ltd.

6) I have based this report on previous exploration experience in the area of the Iron Mountiain Property, a review of government and company reports listed in the bibliography, and on a Stage I program conducted under my supervision between May 2, 1989 and May 26, 1989.

7) I consent to the use of this report by for any Filing Statement, Statement of Material Facts, or addessment work filed by Golden Dynasty Resources Ltd.

Peter A. Christopher, PhD., P.Eng.
July 4, 1989

Peter Christopher & Associates Inc.
GEOLOGICAL & EXPLORATION SERVICES
3707 West 34th Ave., Vancouver, B.C. V6N 2K9

Office/Res: 263-6152

July 4, 1989

Golden Dynasty Resources Ltd.
World Trade Centre
Suite 404-999 Canada Place
Vancouver, British Columbia V6C 3E2

Dear Sirs:

I, Peter A. Christopher PhD., P.Eng. hereby consent to the use of my report dated July 4, 1989 on the Iron Mountain Property, Nicola Mining Division, British Columbia, in any Filing Statement, Statement of Material Facts, or for assessment work.

Dated at Vancouver, British Columbia, this 4th day of July, 1989.

Peter A. Christopher PhD., P.Eng.

PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. CHRISTOPHER

APPENDIX A

CERTIFICATES OF ANALYSIS

DESCRIPTIONS OF ROCK SAMPLES

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P14 SOIL P15-P17 CORE AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JUN 8 1989 DATE REPORT MAILED: June 13/89. SIGNED BY.........D.TOYE. C.LEONG. J.WANG; CERTIFIED B.C. ASSAYERS

PETER A. CHRISTOPHER PROJECT GOLDEN DYNASTY File # 89-1394 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L86N 50+00E	1	16	4	73	.1	8	5	460	2.07	2	5	ND	1	30	1	2	2	49	.42	.062	5	19	.32	141	.10	2	1.17	.01	.11	1	1
L86N 50+25E	1	45	3	78	.1	14	10	452	3.14	4	5	ND	1	36	1	2	2	72	.49	.058	9	27	.50	168	.12	3	1.86	.01	.13	1	2
L86N 50+50E	1	32	7	121	.1	11	10	1275	2.27	5	5	ND	1	27	1	2	2	46	.36	.251	7	18	.29	277	.09	2	2.60	.01	.08	1	2
L86N 50+75E	1	27	5	57	.1	10	8	676	2.24	3	5	ND	1	34	1	2	2	55	.63	.040	7	21	.31	143	.10	3	1.19	.01	.11	1	2
L86N 51+00E	1	24	2	47	.1	9	8	427	2.44	2	5	ND	1	34	1	2	2	62	.50	.022	7	21	.35	88	.11	3	1.00	.01	.11	1	1
L86N 51+25E	1	25	10	90	.1	11	9	1306	2.51	3	5	ND	1	35	1	2	2	54	.52	.052	7	21	.36	203	.10	2	2.06	.01	.10	1	1
L86N 51+50E	1	19	3	38	.1	8	6	521	2.07	4	5	ND	1	27	1	2	2	56	.40	.025	5	20	.27	115	.09	5	.98	.01	.11	1	2
L86N 51+75E	1	22	6	35	.1	8	6	559	1.97	3	5	ND	1	51	1	2	3	54	.78	.023	5	19	.27	110	.09	4	.93	.01	.10	2	16
L86N 52+00E	1	31	5	32	.1	10	7	344	2.36	3	5	ND	1	34	1	2	2	61	.59	.011	7	22	.28	74	.10	3	1.00	.01	.08	1	3
L86N 52+25E	1	39	6	44	.1	10	8	494	2.34	2	5	ND	1	36	1	2	3	55	.65	.080	7	21	.32	109	.08	5	1.14	.01	.10	2	1
L86N 52+50E	1	42	9	59	.1	11	8	728	2.38	3	5	ND	1	37	1	2	2	55	.55	.110	7	22	.32	177	.09	7	1.33	.01	.13	1	1
L86N 52+75E	1	29	5	54	.1	11	8	797	2.15	4	5	ND	1	37	1	2	2	53	.69	.048	5	19	.28	145	.08	3	1.35	.01	.08	1	3
L86N 53+00E	1	34	7	51	.1	10	8	486	2.25	4	5	ND	1	37	1	2	2	60	.80	.041	6	21	.31	100	.09	6	1.09	.01	.11	1	1
L86N 53+25E	1	27	4	57	.1	9	7	605	2.12	4	5	ND	1	47	1	2	2	53	1.12	.053	5	19	.31	135	.08	8	1.09	.01	.12	1	2
L86N 53+50E	1	19	10	87	.1	6	6	1337	1.70	2	5	ND	1	28	1	2	2	39	.45	.108	3	14	.20	176	.05	2	1.04	.01	.09	1	1
L86N 53+75E	1	10	5	43	.1	6	5	328	1.85	2	5	ND	1	24	1	2	4	50	.31	.033	3	18	.21	101	.10	2	.94	.01	.05	1	1
L86N 54+00E	1	11	6	63	.1	5	5	504	1.76	2	5	ND	1	22	1	2	2	48	.32	.027	3	17	.19	120	.09	3	.85	.01	.09	1	6
L86N 54+25E	1	14	4	42	.1	7	5	342	2.01	2	5	ND	1	25	1	2	4	57	.35	.015	4	20	.23	91	.10	2	.85	.01	.08	1	1
L86N 54+50E	1	18	4	75	.1	8	6	566	2.12	3	5	ND	1	32	1	2	2	55	.43	.056	5	20	.26	137	.09	5	1.06	.01	.09	1	1
L86N 54+75E	1	26	4	61	.1	9	8	486	2.54	7	5	ND	1	35	1	2	2	65	.53	.044	6	24	.37	97	.11	7	1.00	.01	.14	1	1
L86N 55+00E	1	23	5	85	.2	10	9	585	2.64	5	5	ND	1	36	1	2	2	57	.55	.079	6	22	.35	144	.09	2	1.35	.01	.13	1	2
L86N 55+25E	1	9	6	69	.1	7	4	201	1.56	4	5	ND	1	21	1	2	3	36	.38	.043	3	13	.21	81	.09	2	1.04	.01	.07	1	2
L86N 55+50E	1	21	7	65	.1	8	6	576	2.16	2	5	ND	1	34	1	2	2	52	.55	.051	4	20	.28	175	.10	8	.95	.01	.13	1	2
L86N 55+75E	1	14	5	41	.1	6	5	257	1.83	2	5	ND	1	24	1	2	2	46	.40	.021	4	16	.22	93	.09	3	.91	.01	.06	2	1
L86N 56+00E	1	15	3	72	.2	6	6	609	1.82	2	5	ND	1	23	1	2	4	44	.41	.039	4	17	.22	141	.08	8	1.02	.01	.11	1	2
L86N 56+25E	1	19	9	79	.1	9	6	521	1.97	5	5	ND	1	22	1	2	2	44	.37	.053	5	17	.27	244	.08	2	1.54	.01	.07	1	1
L86N 56+50E	1	37	9	44	.2	13	9	194	3.09	3	5	ND	2	28	1	2	2	80	.47	.070	7	29	.43	109	.10	4	1.37	.01	.07	1	3
L86N 56+75E	1	15	14	219	.1	10	6	1907	1.92	6	5	ND	1	22	1	2	2	39	.32	.178	4	14	.20	484	.07	7	1.70	.01	.06	1	2
L86N 57+00E	1	14	5	61	.1	6	5	374	2.00	2	5	ND	1	24	1	2	4	53	.37	.039	3	19	.23	137	.09	3	1.03	.01	.05	1	1
L86N 57+25E	1	17	5	94	.1	9	6	726	2.15	4	5	ND	1	27	1	2	2	57	.40	.033	4	21	.27	161	.10	9	1.01	.01	.09	1	1
L86N 57+50E	1	21	8	84	.1	8	8	322	2.45	5	5	ND	1	33	1	2	2	57	.48	.014	6	21	.28	209	.08	7	.97	.01	.08	1	2
L86N 57+75E	1	47	8	82	.1	9	9	509	2.45	3	5	ND	1	50	1	2	2	50	.86	.023	9	20	.34	277	.08	4	1.65	.01	.09	1	2
L86N 58+00E	1	21	9	130	.1	8	6	693	2.11	3	5	ND	1	25	1	2	4	52	.38	.038	5	18	.26	247	.08	4	1.20	.01	.08	1	2
L86N 58+25E	1	26	8	41	.1	9	8	403	2.43	5	5	ND	1	33	1	2	2	64	.47	.018	8	22	.33	143	.10	2	1.05	.01	.08	1	8
L86N 58+50E	1	20	7	64	.1	8	7	586	1.99	5	5	ND	1	36	1	2	2	51	.53	.034	4	18	.27	147	.09	3	1.10	.01	.08	1	2
L86N 58+75E	1	14	5	103	.1	7	5	627	1.93	4	5	ND	1	24	1	2	2	46	.34	.052	3	18	.23	165	.09	2	1.27	.01	.09	1	2
STD C/AU-S	19	63	38	132	7.1	73	30	957	3.87	38	17	6	36	51	18	16	21	58	.50	.088	38	56	.87	176	.07	32	1.82	.06	.13	12	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L86N 59+00E	1	59	2	50	.1	14	10	399	2.09	3	5	ND	2	78	1	2	2	71	2.19	.020	12	25	.54	173	.12	9	1.74	.03	.10	1	3
L86N 59+25E	1	17	8	215	.1	5	7	973	2.10	4	5	ND	1	50	1	2	2	37	.70	.099	5	10	.24	280	.07	7	1.47	.02	.12	1	1
L86N 59+50E	1	16	5	75	.1	6	6	722	1.89	4	5	ND	1	38	1	2	2	46	.48	.035	4	15	.25	135	.10	5	1.08	.01	.13	1	1
L86N 59+75E	1	18	2	63	.1	9	7	494	2.65	2	5	ND	1	32	1	2	2	68	.41	.021	5	22	.30	146	.13	3	1.65	.01	.08	1	2
L86N 60+00E	1	19	5	53	.1	7	7	306	2.49	4	5	ND	1	35	1	2	2	65	.44	.017	5	21	.30	155	.13	2	1.47	.01	.06	1	1
L85N 50+00E	1	37	4	76	.1	10	11	1180	2.62	8	5	ND	1	43	1	2	3	54	.64	.057	7	18	.39	171	.09	4	2.04	.01	.07	1	1
L85N 50+25E	1	29	7	60	.1	9	9	933	2.21	3	5	ND	1	40	1	2	2	50	.70	.023	6	16	.30	146	.09	3	1.69	.01	.12	1	2
L85N 50+50E	1	29	6	90	.2	9	10	2040	2.04	6	5	ND	1	46	1	2	3	42	.83	.056	5	13	.27	222	.07	2	1.69	.01	.10	1	1
L85N 50+75E	1	26	6	70	.1	9	9	1221	2.19	3	5	ND	1	36	1	2	2	49	.52	.054	5	17	.30	180	.08	3	1.69	.01	.08	1	1
L85N 51+00E	1	25	3	83	.2	11	8	742	2.34	4	5	ND	1	38	1	2	2	51	.51	.050	6	17	.30	161	.09	3	1.72	.01	.08	1	1
L85N 51+25E	1	28	2	95	.1	12	11	891	2.38	3	5	ND	1	47	1	2	2	48	.77	.148	5	17	.31	191	.08	6	1.49	.01	.10	1	3
L85N 51+50E	1	32	6	62	.2	11	9	702	2.46	5	5	ND	1	52	1	2	2	55	1.01	.061	7	19	.33	164	.10	9	1.54	.02	.13	1	4
L85N 51+75E	1	27	3	103	.1	10	10	1257	2.32	5	5	ND	1	50	1	2	2	49	.89	.161	7	17	.32	253	.08	9	1.65	.01	.14	1	3
L85N 52+00E	1	24	3	57	.1	9	7	592	2.16	4	5	ND	1	39	1	2	2	54	.79	.044	5	18	.32	119	.10	5	1.21	.01	.15	1	3
L85N 52+25E	1	28	4	52	.1	10	8	341	2.39	6	5	ND	1	34	1	2	2	57	.51	.038	6	19	.35	119	.10	3	1.56	.01	.07	1	2
L85N 52+50E	1	24	5	102	.1	10	8	789	2.34	5	5	ND	2	25	1	2	2	49	.33	.106	6	17	.33	224	.09	6	2.27	.01	.06	1	1
L85N 52+75E	1	18	8	85	.2	9	7	767	2.04	3	5	ND	1	34	1	2	2	49	.47	.045	5	17	.26	146	.09	2	1.27	.01	.11	1	15
L85N 53+00E	1	20	5	87	.2	10	7	653	2.51	5	5	ND	2	25	1	2	3	55	.37	.043	6	20	.31	217	.11	8	2.33	.01	.09	1	3
L85N 53+25E	1	17	8	59	.1	8	6	448	2.19	3	5	ND	1	30	1	2	2	57	.39	.020	5	18	.28	137	.12	2	1.10	.01	.06	1	3
L85N 53+50E	1	13	3	96	.2	7	5	613	1.97	7	5	ND	1	27	1	2	4	54	.38	.056	4	17	.21	135	.10	11	.98	.01	.09	1	3
L85N 53+75E	1	20	2	76	.1	10	8	638	2.25	4	5	ND	1	39	1	2	2	56	.54	.044	6	18	.30	142	.11	11	1.07	.02	.14	1	2
L85N 54+00E	1	25	3	63	.1	12	9	541	2.48	4	5	ND	1	39	1	2	2	56	.61	.075	7	20	.35	152	.11	9	1.59	.02	.10	1	5
L85N 54+25E	1	28	7	50	.2	11	8	601	2.61	5	5	ND	2	41	1	2	2	62	.67	.053	7	21	.36	138	.12	5	1.41	.02	.12	1	3
L85N 54+50E	1	21	5	66	.2	12	7	375	2.34	5	5	ND	2	28	1	2	2	55	.42	.068	6	18	.30	196	.11	5	1.46	.02	.09	1	3
L85N 54+75E	1	20	6	64	.1	11	7	391	2.28	4	5	ND	1	31	1	2	2	55	.50	.068	5	18	.30	198	.10	5	1.33	.02	.09	1	2
L85N 55+00E	1	30	2	102	.2	10	6	1068	1.89	3	5	ND	1	52	1	2	2	45	.98	.110	4	15	.19	471	.08	6	1.13	.01	.09	1	1
L85N 55+25E	1	15	6	61	.1	7	5	466	1.71	2	5	ND	1	22	1	2	2	40	.34	.036	4	14	.22	235	.09	4	1.08	.01	.06	1	3
L85N 55+50E	1	22	3	51	.1	8	7	220	2.37	4	5	ND	1	25	1	2	2	62	.34	.023	5	20	.29	111	.11	2	1.44	.01	.04	1	2
L85N 55+75E	1	24	5	75	.2	9	7	846	2.27	4	5	ND	2	27	1	2	2	52	.64	.064	5	18	.28	362	.10	7	1.78	.01	.11	1	2
L85N 56+00E	1	22	3	60	.1	11	7	583	2.57	2	5	ND	1	27	1	2	2	63	.51	.029	6	22	.31	259	.12	4	1.53	.01	.10	1	1
L85N 56+25E	1	23	5	54	.1	10	7	531	2.26	2	5	ND	1	26	1	2	2	53	.49	.054	6	17	.28	242	.10	4	1.50	.01	.10	1	2
L85N 56+50E	1	49	5	51	.1	13	9	678	2.45	2	5	ND	1	37	1	2	2	50	.78	.017	10	19	.34	314	.10	5	2.07	.02	.06	1	2
L85N 56+75E	1	25	6	90	.1	10	8	933	2.45	5	5	ND	2	32	1	2	2	57	.59	.048	6	19	.33	240	.10	6	1.65	.01	.12	1	1
L85N 57+00E	1	23	6	67	.1	10	7	564	2.24	3	5	ND	1	40	1	2	2	57	.52	.038	6	19	.31	179	.10	3	1.19	.01	.09	1	2
L85N 57+25E	1	24	3	50	.1	11	7	408	2.47	3	5	ND	1	33	1	2	2	64	.46	.033	5	20	.32	119	.11	5	1.26	.01	.07	1	1
L85N 57+50E	1	22	4	130	.2	11	8	1006	2.54	5	5	ND	2	30	1	2	2	58	.45	.133	6	20	.31	248	.10	2	1.95	.01	.08	1	1
STD C/AU-S	18	62	36	132	7.0	72	30	967	3.90	40	20	7	36	49	18	17	20	56	.47	.084	37	55	.86	175	.07	32	1.81	.06	.13	12	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L85N 57+75E	1	24	6	67	.1	10	7	506	2.59	4	5	ND	1	33	1	2	2	69	.46	.055	5	23	.31	161	.12	8	1.16	.01	.11	1	1
L85N 58+00E	1	30	6	74	.1	11	9	427	2.68	5	5	ND	1	33	1	2	2	71	.44	.066	6	23	.33	134	.11	4	1.29	.01	.10	1	7
L85N 58+25E	1	21	8	71	.1	8	6	403	2.19	5	5	ND	1	25	1	2	3	57	.34	.066	4	19	.26	139	.10	6	1.27	.01	.06	1	1
L85N 58+50E	1	17	7	43	.1	9	5	249	2.23	2	5	ND	2	28	1	2	2	66	.37	.033	4	21	.23	78	.12	5	.84	.01	.06	1	1
L85N 58+75E	1	13	4	56	.1	8	6	391	2.08	2	5	ND	1	29	1	2	4	59	.41	.019	4	18	.24	75	.12	3	.81	.02	.11	1	1
L85N 59+00E	1	24	7	57	.1	9	8	458	2.33	2	5	ND	1	43	1	2	2	60	.53	.033	6	20	.28	147	.11	7	1.03	.02	.13	1	1
L85N 59+25E	1	38	6	53	.2	11	8	479	2.68	4	5	ND	1	63	1	2	4	66	.78	.042	9	22	.38	152	.11	6	1.28	.02	.16	1	1
L85N 59+50E	1	17	14	109	.2	8	6	327	1.65	2	5	ND	1	29	1	2	4	36	.33	.182	4	11	.19	178	.08	2	1.30	.01	.08	1	1
L85N 59+75E	1	18	11	134	.1	8	6	1391	1.99	3	5	ND	1	37	1	2	2	50	.67	.067	4	17	.24	228	.09	4	1.03	.01	.11	1	1
L85N 60+00E	1	31	11	43	.3	8	7	287	2.26	6	5	ND	2	45	1	5	2	57	.96	.017	7	18	.28	124	.10	5	1.12	.02	.09	2	1
L84N 51+00E	1	21	10	97	.1	12	6	603	2.13	2	5	ND	1	29	1	2	2	51	.38	.057	5	18	.27	202	.11	3	1.59	.01	.08	1	1
L84N 51+25E	1	21	11	70	.2	13	6	773	2.20	4	5	ND	2	29	1	2	2	54	.42	.058	5	19	.27	191	.11	8	1.35	.02	.09	1	1
L84N 51+50E	1	42	10	56	.1	11	8	698	2.33	3	5	ND	1	41	1	2	2	49	.89	.027	9	16	.29	176	.10	9	1.69	.02	.10	1	1
L84N 51+75E	1	28	7	95	.3	12	9	1081	2.46	5	5	ND	1	37	1	2	2	53	.74	.165	6	20	.34	254	.09	5	1.95	.01	.18	1	1
L84N 52+00E	1	23	6	56	.1	9	7	734	2.20	3	5	ND	1	37	1	2	2	54	.81	.036	5	18	.29	155	.09	4	1.26	.01	.14	1	1
L84N 52+25E	1	16	6	49	.1	9	6	411	2.18	5	5	ND	1	32	1	2	2	59	.38	.038	5	20	.29	109	.13	3	1.06	.02	.09	1	1
L84N 52+50E	1	19	8	50	.1	9	7	433	2.28	2	5	ND	1	44	1	2	2	63	.52	.033	5	21	.31	95	.13	4	.90	.02	.13	1	1
L84N 52+75E	1	25	9	49	.2	9	7	683	2.05	4	5	ND	1	54	1	2	3	56	1.07	.034	5	19	.25	142	.10	6	.87	.01	.09	1	1
L84N 53+00E	1	20	5	41	.1	9	7	399	2.23	2	5	ND	1	39	1	2	2	61	.57	.036	5	21	.27	98	.12	6	.90	.02	.12	1	1
L84N 53+25E	1	39	9	41	.2	12	8	340	2.54	2	5	ND	2	40	1	2	4	63	.81	.021	9	23	.33	124	.12	5	1.21	.02	.10	1	1
L84N 53+50E	1	35	8	58	.2	12	9	451	2.68	3	5	ND	2	40	1	2	2	63	.73	.045	8	22	.33	208	.12	5	1.56	.02	.09	1	1
L84N 53+75E	1	21	8	52	.1	11	7	388	2.21	2	5	ND	1	31	1	2	3	56	.50	.048	5	19	.26	149	.11	4	1.25	.02	.13	1	1
L84N 54+00E	1	23	7	57	.1	9	7	489	2.49	2	5	ND	1	32	1	2	2	64	.49	.046	6	21	.31	128	.12	4	1.10	.02	.11	1	3
L84N 54+25E	1	20	6	90	.1	10	7	771	2.34	2	5	ND	1	28	1	2	2	58	.46	.047	5	20	.31	136	.11	3	1.29	.02	.13	1	1
L84N 54+50E	1	19	6	68	.3	10	7	423	2.31	2	5	ND	1	25	1	2	3	61	.40	.031	5	22	.29	113	.12	3	1.05	.02	.17	1	1
L84N 54+75E	1	26	10	105	.3	10	7	552	2.01	5	5	ND	1	26	1	2	2	44	.62	.211	6	14	.24	365	.09	5	2.08	.01	.11	1	1
L84N 55+00E	1	147	13	126	.1	10	8	1543	2.31	7	5	ND	1	30	1	2	2	47	.67	.146	9	15	.25	624	.09	5	1.96	.02	.07	1	1
L84N 55+25E	1	48	8	62	.2	13	10	714	2.70	3	5	ND	2	38	1	2	2	66	.76	.048	9	21	.40	410	.11	4	1.58	.02	.12	1	1
L84N 55+50E	1	29	10	90	.1	12	9	844	2.54	4	5	ND	1	31	1	2	2	60	.43	.073	6	21	.34	252	.11	2	1.56	.02	.08	1	1
L84N 55+75E	1	35	7	79	.1	13	10	433	3.01	4	5	ND	2	36	1	2	2	71	.48	.070	8	25	.40	218	.12	6	1.90	.02	.09	1	2
L84N 56+00E	1	23	5	104	.1	12	8	730	2.03	2	5	ND	1	27	1	2	2	43	.53	.044	5	14	.27	268	.08	2	1.42	.02	.12	1	1
L84N 56+25E	1	59	10	92	.2	14	9	616	2.48	2	5	ND	1	42	1	2	2	54	1.02	.028	10	22	.28	356	.10	4	1.62	.02	.08	1	1
L84N 56+50E	1	38	5	90	.1	11	8	584	2.54	4	5	ND	2	38	1	2	2	63	.76	.023	9	20	.28	276	.11	3	1.47	.02	.09	1	2
L84N 56+75E	1	37	3	62	.2	10	8	912	2.21	2	5	ND	2	47	1	2	2	58	.62	.015	8	19	.32	229	.11	3	1.22	.02	.14	1	3
L84N 57+00E	1	21	8	112	.1	11	7	433	2.26	4	5	ND	2	29	1	2	2	57	.36	.069	5	19	.31	160	.11	3	1.34	.01	.08	1	2
L84N 57+25E	1	23	15	62	.2	11	7	292	2.49	4	5	ND	2	30	1	2	2	61	.37	.044	5	20	.32	194	.12	3	1.55	.01	.09	1	1
STD C/AU-S	18	63	42	132	7.1	73	30	958	3.81	43	18	6	37	51	18	15	24	58	.47	.089	38	55	.86	176	.07	32	1.80	.06	.13	12	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L84N 57+50E	1	19	8	59	.1	9	6	387	2.10	2	5	ND	1	31	1	2	2	55	.43	.029	5	17	.29	139	.12	2	1.08	.01	.10	1	7
L84N 57+75E	1	33	7	62	.1	12	8	436	2.54	2	5	ND	1	37	1	2	3	64	.50	.030	8	20	.37	157	.12	3	1.49	.02	.15	1	3
L84N 58+00E	1	23	6	47	.1	9	7	561	1.99	2	5	ND	1	41	1	2	2	56	.65	.022	6	16	.31	165	.10	8	1.30	.01	.13	1	1
L84N 58+25E	1	13	5	79	.1	7	5	316	1.82	2	5	ND	1	25	1	2	2	46	.36	.037	3	15	.22	113	.10	5	1.07	.01	.07	1	2
L84N 58+50E	1	32	10	69	.1	11	9	295	2.69	2	5	ND	1	32	1	2	2	65	.41	.057	6	21	.39	149	.12	5	1.84	.02	.08	1	1
L84N 58+75E	1	15	8	58	.1	8	5	305	2.06	5	5	ND	1	26	1	2	2	56	.37	.033	4	17	.24	99	.11	3	.98	.01	.08	1	1
L84N 59+00E	1	20	6	46	.1	9	6	614	2.27	2	5	ND	1	47	1	2	2	59	.60	.033	6	18	.31	110	.10	3	1.00	.01	.11	1	1
L84N 59+25E	1	25	9	52	.1	9	8	419	2.39	2	5	ND	1	39	1	2	2	58	.70	.031	6	18	.31	133	.10	4	1.26	.02	.07	1	7
L84N 59+50E	1	37	11	36	.2	12	8	222	2.67	2	5	ND	2	64	1	2	2	68	1.02	.023	8	22	.35	120	.11	7	1.12	.06	.09	1	1
L84N 59+75E	1	39	8	35	.1	13	9	206	3.05	2	5	ND	2	74	1	2	2	78	1.14	.024	10	25	.40	127	.13	8	1.32	.06	.11	1	1
L84N 60+00E	1	17	5	33	.1	9	7	177	2.53	4	5	ND	1	38	1	2	2	73	.47	.018	5	22	.28	59	.13	9	.98	.02	.09	1	2
L83N 51+00E	1	15	7	42	.1	9	7	846	2.14	3	5	ND	1	38	1	3	2	56	.56	.024	4	17	.27	151	.10	3	1.03	.02	.08	1	1
L83N 51+25E	1	38	9	42	.1	12	9	548	2.70	2	5	ND	1	58	1	2	2	69	.88	.039	7	23	.40	111	.11	9	1.14	.02	.15	1	1
L83N 51+50E	1	28	8	35	.1	10	8	424	2.61	2	5	ND	1	38	1	2	2	70	.71	.022	7	22	.32	101	.12	6	1.15	.02	.08	1	1
L83N 51+75E	1	29	12	42	.1	14	8	465	2.53	3	5	ND	2	38	1	2	2	67	.76	.025	6	25	.32	112	.12	6	1.17	.02	.08	1	4
L83N 52+00E	1	26	10	34	.1	12	8	433	2.41	2	5	ND	1	38	1	2	2	63	.85	.041	6	21	.34	100	.12	6	1.21	.02	.13	1	1
L83N 52+25E	1	19	5	31	.2	10	8	451	2.17	3	5	ND	2	34	1	2	2	59	.55	.031	5	19	.30	87	.11	4	1.03	.01	.10	1	1
L83N 52+50E	1	27	8	32	.1	11	8	321	2.41	2	5	ND	1	37	1	2	3	66	.55	.024	6	22	.34	91	.12	3	1.03	.02	.06	1	1
L83N 52+75E	1	45	10	37	.1	15	11	431	2.82	2	5	ND	2	43	1	2	2	70	.84	.041	10	25	.44	113	.12	5	1.38	.02	.12	1	1
L83N 53+00E	1	33	10	46	.2	14	10	515	2.74	4	5	ND	2	37	1	2	3	67	.77	.014	8	21	.36	192	.13	4	1.91	.02	.08	1	1
L83N 53+25E	1	47	9	50	.1	11	8	453	2.94	4	5	ND	1	37	1	2	2	69	.87	.017	7	21	.36	222	.11	9	1.73	.02	.09	1	1
L83N 53+50E	1	28	8	97	.1	7	7	828	2.13	2	5	ND	1	16	1	2	2	46	.24	.055	4	11	.23	151	.10	3	2.20	.02	.06	1	1
L83N 53+75E	1	18	7	71	.1	8	7	418	2.12	2	5	ND	1	22	1	2	2	53	.38	.034	3	15	.26	142	.10	3	1.62	.01	.07	1	3
L83N 54+00E	1	25	7	88	.1	10	6	660	2.05	2	5	ND	3	21	1	2	2	47	.39	.032	3	15	.29	237	.10	3	1.88	.01	.05	1	1
L83N 54+25E	1	22	13	107	.1	8	6	992	1.92	2	5	ND	1	25	1	2	3	38	.47	.164	4	9	.16	456	.08	3	1.98	.02	.04	1	1
L83N 54+50E	1	16	5	61	.2	8	7	262	2.09	3	5	ND	1	22	1	2	3	50	.42	.027	4	15	.23	223	.09	5	1.29	.01	.09	1	1
L83N 54+75E	1	25	11	101	.2	10	7	279	2.64	7	5	ND	2	14	1	2	2	54	.22	.289	5	16	.28	169	.12	2	3.43	.01	.04	1	1
L83N 55+00E	1	50	12	98	.1	12	10	972	2.72	5	5	ND	2	33	1	2	2	56	.70	.060	24	19	.32	484	.11	2	3.19	.02	.11	1	1
L83N 55+25E	1	22	5	51	.1	10	9	455	2.31	2	5	ND	1	27	1	2	2	60	.50	.011	6	19	.26	215	.11	5	1.28	.01	.07	1	1
L83N 55+50E	1	89	11	75	.3	12	8	844	2.15	2	5	ND	1	53	1	2	3	44	1.59	.048	14	15	.30	551	.08	6	1.99	.02	.06	1	1
L83N 55+75E	1	45	9	95	.1	12	10	776	2.76	5	5	ND	1	27	1	2	3	61	.49	.116	7	20	.37	306	.09	2	2.21	.01	.08	1	1
L83N 56+00E	1	21	9	43	.1	11	7	394	2.17	2	5	ND	2	26	1	2	2	55	.50	.020	6	18	.29	164	.11	6	1.36	.01	.09	2	1
L83N 56+25E	1	28	7	67	.1	11	7	539	2.34	3	5	ND	1	33	1	2	2	55	.53	.042	6	20	.33	269	.11	6	1.65	.01	.09	1	1
L83N 56+50E	1	26	10	84	.1	8	7	234	2.10	2	5	ND	1	13	1	2	2	46	.19	.173	5	14	.25	150	.11	2	2.53	.01	.03	1	1
L83N 56+75E	1	15	10	99	.2	8	7	338	2.17	4	5	ND	2	31	1	2	2	43	.43	.057	6	15	.24	201	.10	5	2.02	.02	.11	1	1
L83N 57+00E	1	131	11	85	.1	11	8	900	2.41	5	5	ND	1	29	1	2	2	56	.47	.079	5	19	.38	292	.09	2	1.95	.01	.06	1	1
STD C/AU-S	17	62	42	132	7.1	73	31	943	3.84	40	19	6	36	50	17	17	17	57	.47	.089	37	55	.86	174	.07	31	1.83	.06	.13	12	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L83N 57+25E	1	22	9	80	.2	7	7	605	2.47	3	5	ND	1	34	1	2	2	60	.53	.030	6	20	.28	263	.11	2	1.69	.01	.11	1	1
L83N 57+50E	1	17	5	97	.3	6	7	648	2.26	5	5	ND	1	28	1	2	2	54	.38	.029	5	17	.25	204	.10	6	1.30	.01	.08	1	1
L83N 57+75E	1	19	9	66	.2	7	8	744	2.26	3	5	ND	1	35	1	2	2	56	.48	.023	6	17	.28	194	.10	5	1.36	.01	.09	1	1
L83N 58+00E	1	18	2	91	.1	7	7	735	2.06	2	5	ND	1	36	1	2	2	51	.47	.034	4	16	.25	166	.10	3	1.21	.01	.11	1	1
L83N 58+25E	1	28	8	110	.1	9	9	945	2.39	2	5	ND	1	49	1	2	2	53	.79	.040	7	18	.33	199	.09	5	1.52	.01	.17	1	1
L83N 58+50E	1	35	8	58	.1	9	9	531	2.51	2	5	ND	1	48	1	2	2	60	.82	.018	7	20	.38	131	.11	2	1.39	.02	.13	1	1
L83N 58+75E	1	22	4	70	.1	7	9	404	2.53	3	5	ND	1	34	1	2	2	63	.55	.043	5	19	.30	117	.11	7	1.05	.01	.10	1	1
L83N 59+00E	1	13	9	52	.1	6	6	452	2.01	4	5	ND	1	34	1	2	2	55	.42	.033	4	17	.23	105	.10	2	.99	.01	.12	1	1
L83N 59+25E	1	26	9	44	.1	8	8	517	2.35	2	5	ND	1	64	1	2	2	62	.86	.020	6	19	.35	181	.11	4	1.00	.01	.11	1	1
L83N 59+50E	1	20	6	56	.2	8	7	465	2.29	3	5	ND	1	41	1	2	2	62	.45	.069	5	20	.24	117	.10	6	1.08	.01	.07	1	2
L83N 59+75E	1	37	9	64	.2	8	10	660	2.75	2	5	ND	1	88	1	2	2	57	.97	.018	9	18	.37	191	.10	4	1.64	.02	.08	1	1
L83N 60+00E	1	22	7	59	.1	8	7	335	2.46	4	5	ND	1	41	1	2	2	64	.48	.029	6	19	.32	104	.12	3	1.09	.02	.11	1	4
L82-50E 52+00E	1	27	7	40	.2	11	8	430	2.62	2	5	ND	1	37	1	2	2	71	.79	.023	6	25	.30	163	.12	6	1.33	.02	.07	1	1
L82+50E 52+25E	1	18	3	42	.2	8	7	392	2.38	2	5	ND	1	29	1	2	2	65	.42	.057	5	21	.26	100	.12	3	1.13	.01	.07	2	10
L82+50E 52+50E	1	61	10	48	.4	10	8	519	2.64	2	5	ND	2	38	1	2	2	53	1.12	.016	13	20	.32	226	.11	4	2.16	.02	.06	1	2
L82+50E 52+75E	1	20	7	45	.1	9	7	508	2.31	2	5	ND	1	29	1	2	2	57	.56	.027	6	19	.31	142	.11	3	1.54	.02	.07	2	1
L82+50E 53+00E	1	15	9	71	.1	7	7	387	1.99	2	5	ND	1	20	1	2	2	45	.38	.046	4	14	.28	145	.09	5	1.43	.02	.07	1	1
L82+50E 53+25E	1	13	5	53	.1	5	4	322	1.27	2	5	ND	1	15	1	2	2	26	.21	.041	2	8	.13	124	.07	2	1.35	.01	.03	1	4
L82-50E 53+50E	1	19	6	74	.3	16	6	166	1.58	6	5	ND	2	15	1	2	2	34	.21	.043	3	11	.19	130	.10	5	1.89	.02	.05	1	1
L82+50E 53+75E	1	35	12	103	.3	9	7	665	2.18	2	5	ND	1	19	1	2	2	39	.31	.073	4	11	.26	359	.07	2	2.52	.01	.06	1	1
L82+50E 54+00E	1	50	6	54	.2	13	10	379	3.09	5	5	ND	3	37	1	2	2	81	.53	.046	9	25	.49	147	.13	2	1.61	.01	.09	1	2
L82+50E 54+25E	1	22	7	46	.1	8	7	361	2.55	3	5	ND	1	24	1	2	2	68	.39	.040	4	19	.29	110	.11	2	1.52	.01	.07	1	3
L82+50E 54+50E	1	30	11	88	.1	11	9	1081	2.80	3	5	ND	1	27	1	2	2	69	.47	.074	5	20	.34	230	.10	2	2.26	.01	.07	1	1
L82+50E 54+75E	1	60	7	76	.1	12	11	901	3.49	6	5	ND	1	36	1	2	2	71	.66	.060	10	21	.48	317	.10	2	1.93	.01	.10	1	1
L82+50E 55+00E	1	25	10	76	.2	8	7	623	2.08	2	5	ND	5	27	1	2	2	47	.52	.046	6	16	.25	265	.08	5	1.54	.01	.08	1	1
L82+50E 55+25E	1	88	8	91	.2	8	9	972	2.40	2	5	ND	1	38	1	2	5	50	.87	.054	8	16	.33	325	.08	4	1.78	.01	.14	1	1
L82+50E 55+50E	1	172	6	55	.2	12	10	520	2.91	6	5	ND	1	40	1	2	2	70	.73	.057	9	22	.46	272	.11	5	1.66	.02	.08	1	1
L82+50E 55+75E	1	22	12	104	.3	10	8	810	2.48	2	5	ND	1	22	1	2	2	54	.33	.132	5	17	.31	239	.09	3	2.36	.01	.05	1	1
L82+50E 56+00E	1	56	8	55	.1	13	10	388	2.95	2	5	ND	1	42	1	2	2	76	.60	.058	9	25	.46	142	.12	2	1.71	.01	.12	1	2
L82N 52+00E	1	29	11	31	.1	10	9	498	2.67	4	5	ND	1	41	1	2	2	56	.87	.020	7	18	.32	276	.10	6	2.28	.03	.04	1	1
L82N 52+25E	1	25	9	36	.1	10	9	378	2.44	2	5	ND	1	41	1	2	2	55	1.17	.019	8	18	.26	304	.11	9	2.17	.02	.10	1	1
L82N 52+50E	1	40	6	36	.1	11	9	408	2.74	2	5	ND	2	37	1	2	2	67	.69	.040	9	24	.39	145	.13	3	1.43	.02	.14	1	2
L82N 52+75E	1	24	7	66	.3	10	8	457	2.35	4	5	ND	2	22	1	2	4	58	.42	.079	7	17	.29	144	.11	4	2.39	.02	.12	1	1
L82N 53+00E	1	23	6	54	.1	10	7	557	2.38	2	5	ND	1	31	1	2	3	65	.41	.051	5	20	.32	122	.11	2	1.32	.01	.05	1	1
L82N 53+25E	1	18	7	93	.1	10	7	739	2.36	2	5	ND	1	20	1	2	2	50	.31	.122	5	15	.26	147	.11	2	2.52	.01	.04	1	1
L82N 53+50E	1	46	9	44	.1	15	10	285	3.12	2	5	ND	2	37	1	2	2	84	.56	.040	8	29	.57	178	.14	2	1.90	.01	.06	1	1
STD C/AU-S	17	62	40	132	7.1	69	30	956	3.83	40	18	7	36	51	18	19	20	58	.47	.089	38	55	.87	178	.07	33	1.83	.06	.13	12	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L82N 53+75E	1	24	12	95	.1	8	5	547	1.82	2	5	ND	1	21	1	2	2	35	.39	.114	7	11	.22	223	.08	2	2.56	.01	.06	1	1
L82N 54+00E	1	15	9	67	.1	9	7	601	2.52	4	7	ND	1	15	1	2	2	52	.21	.090	5	15	.26	157	.12	4	2.70	.01	.05	1	1
L82N 54+25E	1	29	8	60	.1	12	8	541	2.84	5	5	ND	2	31	1	2	2	69	.37	.037	8	23	.41	229	.12	3	2.94	.01	.06	1	1
L82N 54+50E	1	19	9	60	.1	10	8	571	2.57	4	5	ND	2	31	1	2	2	64	.43	.020	5	20	.33	195	.12	2	1.87	.01	.09	1	14
L82N 54+75E	1	105	10	61	.1	12	9	539	2.86	3	5	ND	2	39	1	2	2	70	.59	.047	9	23	.42	232	.12	5	1.97	.01	.11	1	2
L82N 55+00E	1	366	10	75	.3	10	8	1005	2.42	2	5	ND	1	34	1	2	3	50	.65	.043	7	15	.34	234	.08	4	1.51	.01	.13	1	1
L82N 55+25E	1	88	5	70	.1	15	13	725	3.37	8	5	ND	1	61	1	2	2	74	2.05	.075	9	21	.82	126	.10	9	1.73	.02	.11	1	3
L82N 55+50E	1	41	6	49	.1	13	8	309	2.71	2	5	ND	2	28	1	2	2	65	.67	.050	9	23	.48	299	.12	2	1.35	.02	.07	1	1
L82N 55+75E	1	21	4	73	.1	9	7	739	2.53	2	7	ND	1	32	1	2	2	62	.47	.048	5	19	.34	278	.10	3	2.35	.01	.05	1	1
L82N 56+00E	1	29	10	59	.1	10	9	537	2.82	2	5	ND	1	31	1	2	2	65	.46	.014	8	18	.39	173	.10	3	1.39	.01	.08	1	1
L82N 56+25E	1	25	7	87	.1	7	7	743	2.20	2	5	ND	1	33	1	2	2	54	.48	.027	5	16	.30	167	.09	7	1.10	.01	.10	1	1
L82N 56+50E	1	17	5	72	.1	8	6	821	1.97	2	5	ND	1	38	1	2	3	50	.55	.033	4	16	.25	169	.09	7	1.09	.01	.12	1	1
L82N 56+75E	1	17	5	53	.1	8	6	331	2.08	2	5	ND	1	34	1	2	3	54	.44	.028	5	17	.26	98	.12	5	1.10	.01	.11	1	1
L82N 57+00E	1	16	4	58	.1	8	6	580	1.95	2	5	ND	1	37	1	2	2	54	.49	.023	4	17	.27	118	.11	2	.91	.01	.11	1	1
L82N 57+25E	1	15	6	67	.2	7	6	462	2.09	2	5	ND	1	25	1	2	2	54	.33	.037	3	17	.25	110	.11	3	1.20	.01	.09	1	2
L82N 57+50E	1	30	6	51	.1	11	9	240	2.93	4	5	ND	2	35	1	2	2	77	.46	.058	6	24	.40	100	.12	4	1.39	.01	.09	1	2
L82N 57+75E	1	21	6	70	.1	10	7	574	2.25	3	5	ND	1	42	1	2	2	55	.74	.122	5	18	.31	172	.09	2	1.48	.01	.11	1	1
L82N 58+00E	1	16	7	53	.1	9	7	549	1.99	3	5	ND	1	32	1	2	2	50	.46	.071	4	17	.27	128	.09	2	1.19	.01	.08	1	1
L82N 58+25E	1	21	6	59	.1	8	8	537	2.28	3	5	ND	1	36	1	2	5	59	.71	.037	5	19	.30	135	.10	5	1.35	.01	.09	1	2
L82N 58+50E	1	23	2	68	.2	10	7	675	2.00	2	5	ND	1	52	1	2	4	52	.83	.051	4	17	.26	133	.09	4	1.04	.01	.09	1	1
L82N 58+75E	1	17	7	59	.1	9	7	520	1.98	2	5	ND	1	46	1	2	2	49	.50	.048	4	15	.25	135	.09	2	1.31	.01	.10	1	1
L82N 59+00E	1	23	7	39	.1	10	7	256	2.50	2	5	ND	1	44	1	2	2	69	.46	.049	5	22	.30	113	.12	5	1.10	.01	.06	1	2
L82N 59+25E	1	32	5	45	.1	13	8	253	3.04	4	5	ND	1	43	1	2	2	83	.52	.052	5	26	.43	94	.13	5	1.39	.01	.08	2	2
L82N 59+50E	1	27	6	41	.2	11	8	389	2.44	3	5	ND	1	48	1	2	3	66	.56	.017	6	21	.33	133	.12	2	1.31	.02	.08	1	1
L82N 59+75E	1	48	7	42	.1	14	9	270	3.29	5	5	ND	1	43	1	2	2	94	.57	.056	9	28	.46	63	.12	2	1.09	.02	.07	1	5
L82N 60+00E	1	21	10	100	.3	11	7	259	2.34	3	6	ND	2	32	1	2	3	57	.40	.057	4	20	.34	148	.11	4	1.88	.01	.08	1	1
L81+50N 52+00E	1	53	4	58	.2	14	11	551	2.99	5	5	ND	1	43	1	2	2	72	.75	.056	8	23	.52	122	.11	2	1.56	.02	.10	1	2
L81+50N 52+25E	1	46	5	86	.1	13	10	621	2.85	7	5	ND	1	39	1	2	2	66	.65	.093	7	20	.50	159	.11	3	1.57	.02	.14	1	2
L81+50N 52+50E	1	50	7	73	.2	13	10	606	2.95	2	5	ND	1	38	1	2	2	71	.67	.073	9	23	.52	169	.11	2	1.69	.01	.10	1	2
L81+50N 52+75E	1	30	10	75	.1	12	8	294	2.67	3	5	ND	1	30	1	2	2	65	.42	.047	5	22	.40	165	.12	4	1.86	.01	.08	1	1
L81+50N 53+00E	1	25	15	116	.1	8	15	3026	4.80	8	5	ND	1	16	1	2	2	55	.57	.047	11	9	.56	279	.03	3	1.76	.01	.13	1	1
L81+50N 53+25E	1	24	8	70	.1	12	7	346	2.27	4	5	ND	1	28	1	2	2	51	.32	.057	5	18	.31	116	.11	3	2.86	.01	.07	1	1
L81+50N 53+50E	1	19	4	58	.2	11	7	535	2.17	4	5	ND	1	25	1	2	3	49	.33	.073	4	18	.28	220	.11	2	2.09	.01	.07	1	1
L81+50N 53+75E	1	24	10	77	.1	13	8	572	2.25	3	5	ND	1	26	1	2	4	50	.41	.130	5	18	.33	207	.10	2	2.18	.01	.05	1	2
L81+50N 54+00E	1	18	13	100	.1	12	6	468	2.53	4	5	ND	1	15	1	2	2	54	.21	.159	5	17	.30	208	.12	3	2.89	.01	.04	1	2
L81+50N 54+25E	1	14	9	49	.1	7	5	747	1.76	2	5	ND	1	21	1	2	5	39	.37	.043	3	13	.22	278	.09	2	1.68	.01	.09	2	1
STD C/AU-S	17	61	43	132	7.1	73	30	941	3.75	38	19	6	36	49	18	19	19	56	.47	.087	37	55	.86	175	.07	32	1.84	.06	.13	11	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L81+50N 54+50E	1	25	7	40	.1	10	7	749	2.23	2	5	ND	2	31	1	2	2	54	.57	.018	6	18	.30	218	.10	2	1.65	.01	.12	2	2
L81+50N 54+75E	1	33	7	33	.2	12	9	739	2.47	2	5	ND	1	29	1	3	2	59	.45	.164	7	21	.33	398	.10	4	1.94	.01	.07	1	2
L81+50N 55+00E	1	13	9	53	.2	7	5	568	1.44	2	5	ND	1	21	1	3	2	34	.38	.055	3	11	.18	324	.07	7	.99	.01	.06	1	1
L81+50N 55+25E	1	21	15	80	.1	11	8	522	2.86	2	5	ND	1	19	1	2	2	66	.29	.071	5	19	.35	263	.12	2	2.98	.01	.05	1	1
L81+50N 55+50E	1	35	6	78	.1	13	9	547	2.88	6	5	ND	1	24	1	2	2	72	.40	.147	6	22	.43	302	.11	6	2.34	.01	.07	1	1
L81+50N 55+75E	1	25	9	97	.1	9	7	1186	2.26	2	5	ND	1	30	1	2	2	57	.53	.048	6	19	.28	500	.09	3	1.65	.01	.12	1	3
L81+50N 56+00E	1	58	8	54	.2	16	10	402	2.99	3	5	ND	2	44	1	2	2	77	.73	.055	10	25	.52	166	.12	2	1.59	.02	.10	1	4
L81N 52+00E	1	37	8	35	.1	15	8	208	2.99	4	5	ND	2	40	1	3	2	88	.49	.054	7	27	.43	77	.12	4	1.10	.01	.05	1	2
L81N 52+25E	1	16	11	31	.1	4	4	119	1.88	2	5	ND	2	11	1	2	2	43	.13	.121	3	11	.14	75	.09	3	1.66	.01	.02	1	1
L81N 52+50E	1	25	9	74	.1	12	8	593	2.78	3	5	ND	1	22	1	2	2	63	.29	.103	5	18	.33	113	.13	3	2.97	.01	.06	1	1
L81N 52+75E	1	18	9	73	.2	7	7	1065	2.22	2	5	ND	1	21	1	2	2	47	.27	.144	6	11	.22	166	.11	3	2.89	.01	.05	1	1
L81N 53+00E	1	11	9	88	.1	7	5	676	1.53	4	5	ND	1	19	1	2	2	35	.22	.060	3	11	.19	226	.08	4	1.43	.01	.04	1	1
L81N 53+25E	1	24	9	78	.1	11	6	516	2.14	2	5	ND	1	36	1	2	2	54	.47	.099	5	17	.30	290	.09	4	1.37	.01	.08	1	5
L81N 53+50E	1	75	12	51	.2	9	5	1026	1.41	2	5	ND	1	60	1	3	2	31	2.77	.052	11	10	.22	299	.05	7	1.29	.01	.06	1	2
L81N 53+75E	1	22	7	28	.1	8	8	386	2.20	2	5	ND	1	26	1	2	2	58	.55	.012	5	17	.25	95	.10	2	1.21	.02	.05	2	3
L81N 54+00E	1	30	9	31	.1	7	7	368	2.00	4	5	ND	1	34	1	2	2	49	.93	.017	6	15	.24	153	.09	4	1.30	.01	.13	2	1
L81N 54+25E	1	20	8	36	.1	10	6	195	2.15	2	5	ND	1	22	1	3	2	52	.36	.016	6	18	.29	139	.11	3	1.97	.01	.10	1	1
L81N 54+50E	1	18	5	36	.1	7	7	504	2.00	2	5	ND	1	28	1	2	2	53	.50	.016	5	17	.24	201	.10	2	1.15	.01	.09	1	1
L81N 54+75E	1	24	10	94	.1	14	9	1225	2.83	4	5	ND	1	27	1	2	2	62	.53	.080	7	20	.36	434	.11	4	2.99	.01	.10	1	1
L81N 55+00E	1	16	12	177	.1	10	8	2333	2.37	3	5	ND	1	19	1	2	2	50	.36	.226	4	17	.24	447	.09	2	1.91	.01	.07	1	1
L81N 55+25E	1	28	11	84	.1	14	9	677	2.94	2	5	ND	2	24	1	2	2	69	.36	.120	6	23	.42	393	.12	4	3.22	.01	.06	1	1
L81N 55+50E	1	31	21	99	.1	11	8	1212	2.54	2	5	ND	1	28	1	2	2	60	.51	.060	5	19	.36	598	.11	5	2.41	.01	.11	1	1
L81N 55+75E	1	28	13	102	.1	12	10	796	2.89	3	5	ND	1	28	1	2	2	65	.41	.031	7	21	.35	340	.12	5	2.18	.01	.12	1	1
L81N 56+00E	1	33	36	141	.1	11	11	1790	2.75	5	5	ND	1	31	1	2	2	55	.51	.111	9	16	.32	1191	.09	2	2.82	.01	.11	1	1
L81N 56+25E	1	54	7	85	.1	14	10	511	2.84	4	5	ND	1	59	1	2	2	72	1.93	.064	10	23	.52	262	.11	5	1.50	.02	.09	1	1
L81N 56+50E	1	28	9	53	.1	11	8	538	2.56	2	5	ND	1	34	1	2	2	65	.55	.027	7	21	.34	254	.12	2	1.42	.02	.13	1	1
L81N 56+75E	1	21	6	50	.1	8	7	495	2.15	2	5	ND	1	37	1	2	2	55	.63	.054	5	17	.27	150	.10	6	1.03	.01	.14	1	1
L81N 57+00E	1	25	11	98	.1	10	9	467	2.62	3	5	ND	1	34	1	2	2	61	.50	.041	4	19	.39	122	.11	6	1.63	.01	.13	1	1
L81N 57+25E	1	34	6	105	.1	10	10	455	2.68	3	5	ND	1	41	1	2	2	67	.81	.047	7	20	.37	125	.10	4	1.26	.02	.14	1	1
L81N 57+50E	1	29	10	71	.1	9	8	237	2.53	2	5	ND	2	33	1	3	2	69	.62	.018	6	21	.29	74	.10	5	.99	.02	.06	1	1
L81N 57+75E	1	30	9	117	.1	12	8	592	2.18	3	5	ND	1	45	1	2	2	52	.80	.085	7	18	.32	242	.09	6	1.33	.02	.08	1	2
L81N 59+00E	1	19	10	62	.1	10	7	509	2.20	2	5	ND	1	34	1	2	2	55	.49	.112	5	19	.27	205	.10	6	1.32	.02	.09	1	1
L81N 58+25E	1	14	8	41	.1	7	5	297	1.86	2	5	ND	1	30	1	2	2	54	.39	.031	3	17	.22	76	.11	5	.83	.01	.06	2	2
L81N 58+50E	1	19	8	37	.1	9	8	325	2.44	2	5	ND	1	45	1	2	2	68	.42	.033	5	22	.34	73	.12	3	.96	.01	.09	1	1
L81N 58+75E	1	21	7	42	.1	10	8	396	2.39	2	5	ND	1	47	1	2	2	66	.56	.032	5	21	.35	130	.12	3	1.04	.01	.07	1	1
L81N 59+00E	1	22	9	72	.1	9	7	612	2.07	2	5	ND	1	29	1	2	2	51	.48	.029	6	17	.28	143	.10	5	1.56	.02	.05	1	2
STD C/AU-S	18	62	39	132	7.1	72	31	956	3.83	37	18	6	37	50	17	14	22	58	.47	.090	37	55	.86	175	.07	32	1.78	.06	.13	11	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L81N 59+25E	1	20	7	71	.2	10	6	535	2.12	2	5	ND	2	25	1	2	2	50	.37	.082	4	17	.31	140	.09	2	1.46	.01	.08	1	3
L81N 59+50E	1	15	15	36	.1	8	5	585	1.89	2	5	ND	2	32	1	2	2	51	.44	.025	4	18	.25	107	.11	4	.83	.01	.08	1	3
L81N 59+75E	1	28	9	51	.1	10	7	550	2.15	2	5	ND	1	42	1	2	2	54	.89	.038	6	19	.33	155	.10	4	1.11	.02	.08	1	2
L81N 60+00E	1	15	6	72	.5	9	6	807	1.85	2	5	ND	2	30	1	2	2	45	.43	.059	4	15	.22	155	.08	4	1.12	.01	.08	1	1
L80+50N 55+00E	1	21	8	42	.1	10	7	212	2.79	2	5	ND	2	26	1	2	2	66	.37	.035	5	21	.35	206	.10	2	1.58	.01	.07	1	1
L80+50N 55+25E	1	26	21	86	.2	12	10	1405	2.74	5	5	ND	1	35	1	2	2	60	.60	.085	9	23	.32	1239	.08	4	1.91	.01	.13	1	1
L80+50N 55+50E	1	26	23	135	.2	8	7	1598	1.98	3	5	ND	1	34	1	2	2	46	.87	.056	6	18	.26	592	.07	5	1.23	.01	.21	1	1
L80+50N 55+75E	1	52	16	128	.3	9	11	1545	2.63	2	5	ND	1	35	1	2	2	49	.67	.065	10	15	.37	753	.07	5	2.04	.01	.19	1	1
L80+50N 56+00E	1	38	13	83	.2	11	10	1093	2.79	7	5	ND	1	35	1	2	2	61	.61	.032	9	21	.41	400	.09	2	1.62	.01	.18	1	1
L80+50N 56+25E	1	57	14	96	.3	15	10	500	2.75	2	5	ND	1	55	1	2	2	68	1.85	.080	9	23	.53	196	.10	3	1.36	.02	.13	1	1
L80+50N 56+50E	1	32	8	64	.2	10	8	557	2.34	2	5	ND	2	38	1	2	2	60	.92	.032	7	21	.35	227	.10	8	1.10	.02	.13	1	1
L80+50N 56+75E	1	41	7	144	.1	11	8	477	2.54	2	5	ND	1	36	1	2	2	61	.93	.044	7	22	.32	196	.10	8	1.26	.02	.13	1	1
L80+50N 57+00E	1	34	9	249	.2	13	9	493	2.58	2	5	ND	1	37	2	2	2	59	.71	.049	8	21	.36	192	.10	4	1.53	.02	.08	1	1
L80+50N 57+25E	1	49	19	155	1.1	13	9	459	2.88	4	5	ND	1	42	2	2	2	70	.68	.040	8	24	.46	262	.12	3	1.49	.02	.10	1	2
L80+50N 57+50E	1	36	11	76	.4	11	9	712	2.59	2	5	ND	1	51	1	2	2	56	1.24	.041	9	22	.44	393	.10	9	1.69	.02	.10	1	1
L80+50N 57+75E	1	40	9	46	.5	15	10	444	3.09	2	5	ND	2	45	1	2	2	77	.64	.032	10	26	.51	210	.13	2	1.68	.02	.08	2	1
L80+50N 58+00E	1	25	6	43	.2	11	7	467	2.41	2	5	ND	2	40	1	2	2	64	.60	.035	6	25	.34	141	.12	8	1.08	.02	.12	2	1
L80N 54+00E	1	28	11	55	.4	11	8	961	2.36	4	5	ND	1	29	1	2	2	48	.81	.053	8	18	.27	220	.08	6	2.03	.02	.11	1	1
L80N 54+25E	1	35	9	47	.1	10	8	500	2.40	3	5	ND	1	28	1	2	2	56	.67	.024	7	18	.31	118	.09	2	1.47	.01	.10	2	1
L80N 54+50E	1	18	4	79	.1	7	7	1159	1.87	2	5	ND	1	26	1	2	2	43	.54	.059	4	16	.24	195	.08	4	1.31	.01	.07	1	3
L80N 54+75E	1	17	6	73	.1	9	7	418	2.25	2	5	ND	1	24	1	2	3	53	.35	.045	4	16	.31	136	.10	2	1.97	.01	.06	1	1
L80N 55+00E	1	14	10	44	.1	8	6	213	2.28	2	5	ND	1	25	1	2	2	55	.37	.025	4	17	.26	193	.10	6	1.53	.01	.06	2	3
L80N 55+25E	1	17	13	119	.1	9	7	1556	2.32	3	5	ND	1	29	1	2	2	53	.49	.028	5	16	.26	398	.10	3	1.78	.01	.12	1	1
L80N 55+50E	1	18	16	164	.1	6	5	1565	1.76	2	5	ND	1	33	1	2	2	31	.46	.038	5	10	.16	838	.07	3	1.44	.01	.11	1	1
L80N 55+75E	1	29	7	66	.2	12	8	364	2.50	3	5	ND	2	36	1	2	2	65	.63	.033	7	21	.36	136	.11	3	1.18	.01	.12	1	2
L80N 56+00E	1	36	9	207	.1	12	9	646	2.45	2	5	ND	1	34	2	2	3	56	.96	.053	6	21	.36	203	.09	6	1.38	.02	.17	1	1
L80N 56+25E	1	39	32	226	.7	13	8	701	2.38	5	5	ND	1	43	3	2	2	60	.94	.058	8	22	.41	255	.09	11	1.37	.02	.12	1	1
L80N 56+50E	1	27	13	221	.1	11	7	384	2.37	2	5	ND	1	31	4	2	2	61	.43	.050	7	20	.33	142	.11	2	1.14	.02	.08	1	5
L80N 56+75E	2	58	121	1037	1.4	12	8	855	2.42	3	5	ND	1	35	12	2	2	57	.64	.070	8	20	.40	292	.09	11	1.57	.01	.09	1	1
L80N 57+00E	1	41	32	839	.4	11	8	451	2.39	2	5	ND	1	32	6	2	2	61	.52	.034	6	20	.39	178	.09	2	1.26	.01	.07	1	1
L80N 57+25E	1	23	8	124	.2	12	8	548	2.50	2	5	ND	1	25	1	2	2	54	.38	.076	6	18	.37	241	.09	4	2.35	.01	.08	1	1
L80N 57+50E	1	13	11	125	.1	8	6	1169	1.86	2	5	ND	1	22	1	2	2	40	.49	.088	4	13	.22	324	.08	2	1.52	.01	.06	1	4
L80N 57+75E	1	23	6	49	.1	10	7	467	2.42	2	5	ND	1	39	1	2	2	65	.67	.022	6	21	.35	198	.12	4	1.09	.02	.10	1	1
L80N 58+00E	1	17	6	61	.1	11	8	544	2.27	2	5	ND	1	38	1	2	2	58	.60	.018	5	19	.33	229	.11	5	1.26	.02	.10	1	1
L80N 58+25E	1	19	6	110	.1	12	8	695	2.27	2	5	ND	1	35	1	2	2	54	.57	.093	4	18	.33	363	.10	7	1.35	.02	.08	1	1
L80N 58+50E	1	20	12	98	.1	10	7	521	2.42	2	5	ND	1	24	1	2	2	49	.40	.083	4	14	.30	281	.07	2	1.84	.02	.06	1	1
STD C/AU-S	17	62	41	131	7.0	72	30	940	3.86	39	16	7	36	49	17	18	21	56	.47	.088	36	55	.87	175	.07	31	1.82	.06	.13	11	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L80N 58+75E	1	16	7	119	.1	8	7	305	2.01	2	5	ND	1	18	1	2	10	41	.37	.066	4	12	.21	239	.08	3	1.98	.02	.08	1	5
L80N 59+00E	1	21	8	67	.1	8	7	340	2.21	2	5	ND	1	22	1	2	2	49	.31	.083	3	16	.26	155	.09	2	1.19	.01	.04	1	2
L80N 59+25E	1	12	2	57	.1	5	5	417	1.89	2	5	ND	1	23	1	2	2	46	.33	.028	3	13	.23	133	.09	3	1.02	.01	.06	1	2
L80N 59+50E	1	32	2	60	.1	12	9	272	2.92	2	5	ND	1	34	1	2	2	68	.44	.065	5	22	.44	153	.11	3	1.73	.01	.09	1	39
L80N 59+75E	1	21	5	88	.1	9	7	400	2.40	2	5	ND	1	30	1	2	2	59	.52	.038	4	19	.32	167	.11	5	1.37	.01	.05	1	2
L80N 60+00E	1	16	6	62	.1	7	6	254	2.41	2	5	ND	1	26	1	2	2	56	.37	.042	4	19	.28	142	.11	6	1.54	.01	.07	1	1
L79+50N 55+00E	1	38	2	184	.1	10	9	543	2.51	2	5	ND	1	34	1	2	2	57	.82	.031	7	19	.34	159	.10	4	1.55	.01	.10	1	4
L79+50N 55+25E	1	47	9	73	.2	13	10	381	3.22	4	5	ND	2	37	1	2	2	64	.84	.029	12	25	.52	157	.11	5	2.29	.02	.10	1	1
L79+50N 55+50E	1	38	5	133	.1	12	9	784	2.72	5	5	ND	1	42	2	4	2	63	1.03	.107	8	22	.39	185	.11	11	1.34	.02	.12	1	1
L79+50N 55+75E	1	34	5	131	.1	11	9	706	2.44	3	5	ND	1	37	2	2	2	56	.94	.093	7	20	.35	171	.09	6	1.14	.01	.10	1	1
L79+50N 56+00E	4	51	215	517	.5	12	8	848	2.54	4	5	ND	1	34	12	2	2	54	.69	.127	7	18	.34	373	.09	4	1.39	.01	.09	1	1
L79+50N 56+25E	5	49	56	565	1.0	10	9	1235	3.11	8	5	ND	1	34	8	3	2	68	.59	.047	6	20	.36	292	.10	5	1.24	.01	.09	1	2
L79+50N 56+50E	1	29	13	179	.8	9	8	571	2.44	3	5	ND	1	33	2	2	2	55	.59	.060	7	19	.30	548	.09	5	1.51	.01	.09	1	1
L79+50N 56+75E	1	22	6	130	.1	10	8	725	2.51	4	5	ND	1	25	1	2	2	57	.41	.103	4	19	.32	299	.09	3	1.54	.01	.09	1	1
L79+50N 57+00E	1	20	10	184	.2	9	7	635	2.28	2	5	ND	1	24	1	2	2	53	.37	.069	4	17	.28	450	.09	3	1.49	.01	.08	1	1
L79+50N 57+25E	1	18	9	259	.3	8	6	612	2.00	2	5	ND	1	22	2	4	2	44	.38	.053	3	14	.24	406	.08	3	1.23	.01	.08	1	1
L79+50N 57+50E	1	29	12	252	.5	10	9	579	2.77	2	5	ND	1	28	1	2	2	56	.41	.083	7	18	.36	769	.10	2	2.57	.01	.06	1	1
L79+50N 57+75E	1	24	21	260	.2	10	7	1169	2.44	3	5	ND	1	43	1	2	2	49	.90	.080	6	17	.33	937	.08	4	1.68	.01	.09	1	1
L79+50N 58+00E	1	24	9	136	.2	9	8	947	2.37	5	5	ND	1	37	1	2	2	51	.56	.092	5	17	.32	821	.09	5	1.66	.01	.11	1	1
L79N 54+00E	1	22	10	212	.1	10	8	1411	2.59	7	5	ND	1	24	2	2	2	48	.41	.219	7	17	.32	600	.08	3	2.17	.01	.06	1	1
L79N 54+25E	1	23	8	95	.1	9	7	274	2.70	2	5	ND	1	29	1	2	2	55	.40	.102	5	20	.33	249	.09	4	2.15	.01	.07	1	2
L79N 54+50E	1	24	8	237	.1	8	6	756	2.36	7	5	ND	1	25	1	2	2	50	.41	.085	5	17	.27	363	.09	2	1.71	.01	.10	1	1
L79N 54+75E	1	40	6	126	.1	9	7	610	2.44	2	5	ND	1	30	1	2	2	57	.51	.028	5	18	.30	246	.10	2	1.55	.01	.10	1	1
L79N 55+00E	1	27	5	110	.1	9	8	566	2.60	6	5	ND	1	31	1	2	2	62	.84	.038	6	21	.33	154	.10	7	1.41	.01	.12	1	1
L79N 55+25E	1	27	6	94	.1	10	9	412	2.51	3	5	ND	1	32	1	2	2	60	.98	.016	7	19	.31	143	.10	5	1.25	.01	.09	1	3
L79N 55+50E	1	27	8	92	.1	8	9	421	2.50	3	5	ND	1	33	1	2	2	60	1.06	.017	6	19	.31	145	.10	8	1.24	.02	.09	1	3
L79N 55+75E	1	41	25	247	.7	7	7	1088	2.03	7	5	ND	1	42	2	4	2	40	.72	.043	5	11	.22	575	.06	3	1.03	.01	.07	1	4
L79N 56+00E	1	28	4	106	.3	9	9	707	2.50	4	5	ND	1	34	1	2	2	59	.43	.030	6	20	.35	240	.10	2	1.50	.01	.05	1	1
L79N 56+25E	1	42	8	64	.1	14	10	297	3.18	4	5	ND	1	39	1	2	2	81	.52	.036	7	26	.51	174	.12	2	1.57	.01	.08	1	2
L79N 56+50E	1	46	2	68	.3	14	11	235	3.45	6	5	ND	1	35	1	2	2	87	.49	.051	7	28	.57	278	.12	3	1.76	.01	.05	1	2
L79N 56+75E	1	22	16	256	.2	9	10	908	2.77	6	5	ND	1	26	1	2	2	54	.39	.092	5	17	.36	573	.08	2	2.59	.01	.06	1	1
L79N 57+00E	1	42	31	287	.2	8	10	1444	3.32	4	5	ND	1	28	1	2	2	60	.39	.031	5	16	.34	591	.09	2	2.67	.01	.06	1	1
L79N 57+25E	1	36	25	277	.1	10	10	1216	2.97	2	5	ND	1	40	2	2	2	59	.65	.039	8	19	.36	902	.09	5	2.27	.01	.11	1	1
L79N 57+50E	1	27	18	149	.1	9	10	731	2.91	7	5	ND	1	37	1	2	2	64	.50	.031	6	21	.39	627	.11	3	1.75	.01	.16	1	2
L79N 57+75E	1	41	24	162	.2	10	10	1122	3.17	6	5	ND	1	46	1	2	2	64	.75	.045	9	21	.43	809	.10	5	1.78	.01	.19	1	1
L79N 58+00E	1	21	37	222	.1	9	10	1032	2.70	6	5	ND	1	36	1	2	2	50	.38	.055	7	15	.33	1680	.08	4	2.30	.01	.07	1	4
STD C/AU-S	17	63	36	132	7.1	70	31	986	3.95	42	17	6	36	50	18	14	18	57	.47	.088	37	55	.87	172	.07	31	1.85	.06	.13	11	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L79N 58+25E	1	32	26	242	.2	10	10	606	2.96	5	5	ND	1	42	2	2	2	66	.51	.029	8	22	.43	1165	.12	4	2.53	.01	.09	1	1
L79N 58+50E	1	22	75	531	1.0	4	8	1581	1.81	2	5	ND	1	58	3	2	2	36	1.08	.108	8	9	.18	2204	.04	9	1.34	.01	.11	1	1
L79N 58+75E	1	22	26	262	.1	7	7	536	2.40	2	5	ND	1	31	2	2	2	57	.40	.025	6	17	.29	854	.10	2	1.72	.02	.08	1	1
L79N 59+00E	1	27	7	98	.1	9	8	307	2.60	2	5	ND	1	33	1	2	2	65	.42	.064	4	20	.43	190	.11	6	1.60	.01	.08	1	1
L79N 59+25E	1	21	6	93	.1	7	7	290	2.46	2	5	ND	1	34	1	2	2	67	.44	.023	5	21	.33	179	.12	6	1.17	.02	.11	1	1
L79N 59+50E	1	38	36	635	.1	8	7	1601	2.02	5	5	ND	1	51	4	2	2	54	1.47	.042	6	17	.33	335	.08	8	1.12	.02	.08	1	1
L79N 59+75E	1	55	8	117	.1	12	9	422	2.80	7	5	ND	2	72	1	2	2	76	1.71	.067	10	23	.53	243	.13	5	1.44	.03	.07	1	1
L79N 60+00E	1	19	14	274	.1	9	7	329	2.45	4	5	ND	1	30	2	2	2	62	.42	.044	5	22	.34	175	.12	2	1.80	.01	.08	1	1
L78+50N 55+00E	1	37	15	94	.2	9	9	646	2.63	5	5	ND	1	38	1	2	2	58	1.06	.024	9	21	.39	183	.11	2	1.80	.02	.08	1	1
L78+50N 55+25E	1	27	13	85	.1	8	8	511	2.29	5	5	ND	1	34	1	2	2	59	.99	.028	7	19	.31	164	.11	3	1.32	.02	.09	1	2
L78+50N 55+50E	2	32	18	150	.2	10	7	722	2.20	6	5	ND	1	35	1	2	2	56	1.22	.039	7	18	.40	186	.09	5	1.38	.02	.09	1	1
L78+50N 55+75E	1	29	17	225	.2	8	7	833	1.88	2	5	ND	1	43	2	2	2	45	2.02	.035	5	14	.30	261	.07	10	1.21	.01	.07	1	1
L78+50N 56+00E	1	24	16	274	.5	10	9	557	2.54	3	5	ND	1	36	3	2	2	63	.49	.049	6	20	.34	307	.12	11	1.83	.02	.08	1	1
L78+50N 56+25E	1	19	16	425	.5	8	7	1290	2.35	5	5	ND	1	39	4	2	2	53	.51	.033	4	16	.27	763	.09	5	1.88	.01	.10	1	1
L78+50N 56+50E	1	24	17	202	.1	9	8	905	2.29	2	5	ND	1	26	2	2	2	54	.36	.076	5	18	.31	272	.10	6	1.80	.01	.09	1	2
L78+50N 56+75E	1	15	10	126	.2	5	5	1027	1.63	2	5	ND	1	33	2	2	2	42	.45	.052	3	14	.22	235	.08	7	.94	.01	.29	1	1
L78+50N 57+00E	1	43	20	148	.1	12	11	1255	2.92	4	5	ND	1	46	1	2	2	68	.64	.040	9	24	.44	442	.12	4	2.08	.01	.13	1	1
L78+50N 57+25E	1	42	13	154	.1	11	11	1164	2.77	2	5	ND	1	54	2	2	2	67	.79	.053	7	23	.47	332	.10	8	1.65	.01	.23	1	3
L78+50N 57+50E	1	25	8	102	.2	8	8	541	2.65	2	5	ND	1	36	1	2	3	68	.47	.031	6	21	.35	218	.13	3	1.45	.02	.12	1	1
L78+50N 57+75E	1	20	6	98	.1	8	7	517	2.32	2	5	ND	1	33	1	2	2	61	.42	.044	5	19	.28	201	.12	8	1.26	.02	.11	1	1
L78+50N 58+00E	1	16	5	92	.1	8	6	352	2.12	2	5	ND	1	28	1	2	2	59	.38	.033	4	18	.24	154	.12	5	1.07	.02	.09	1	1
L78N 54+00E	1	28	12	61	.1	9	9	883	2.70	2	5	ND	1	37	1	2	2	68	.48	.024	8	21	.37	190	.12	7	1.43	.02	.15	1	2
L78N 54+25E	1	63	10	63	.1	16	12	538	3.51	6	5	ND	1	51	1	2	2	81	.68	.028	12	27	.67	169	.13	5	2.29	.02	.14	1	3
L78N 54+50E	1	29	9	61	.1	9	9	861	2.40	2	5	ND	1	49	1	2	2	58	.78	.034	6	18	.38	165	.10	10	1.27	.01	.23	1	1
L78N 54+75E	1	24	16	370	.2	11	7	773	2.21	3	5	ND	1	27	3	2	2	55	.48	.113	5	19	.28	248	.10	7	1.56	.01	.11	1	1
L78N 55+00E	1	37	14	175	.1	10	8	662	2.38	2	5	ND	1	41	2	2	2	62	1.29	.056	8	21	.37	146	.11	10	1.39	.02	.09	1	2
L78N 55+25E	1	28	8	104	.1	9	7	515	2.27	2	5	ND	1	38	1	2	2	64	.75	.055	6	20	.33	132	.11	3	1.17	.01	.08	1	1
L78N 55+50E	1	31	13	144	.3	9	8	639	2.47	5	5	ND	1	32	1	2	2	65	.60	.045	7	20	.40	208	.11	6	1.56	.02	.10	1	4
L78N 55+75E	1	22	8	114	.1	8	8	322	2.60	2	5	ND	1	32	1	2	2	71	.41	.040	5	22	.34	158	.13	2	1.30	.01	.06	1	1
L78N 56+00E	1	17	11	163	.1	6	6	409	2.11	2	5	ND	1	27	1	2	2	58	.37	.037	4	18	.26	157	.11	8	1.08	.01	.10	1	2
L78N 56+25E	1	50	22	171	.4	14	10	388	3.00	10	5	ND	1	44	2	2	2	79	.56	.047	9	25	.50	232	.12	4	2.04	.01	.08	1	2
L78N 56+50E	1	24	29	317	.3	8	9	973	2.40	3	5	ND	1	35	3	2	2	61	.51	.045	6	19	.32	363	.11	2	1.52	.01	.13	1	6
L78N 56+75E	1	20	66	171	.4	6	7	590	2.20	3	5	ND	1	33	2	2	2	59	.43	.040	6	19	.29	300	.11	5	1.14	.01	.16	1	2
L78N 57+00E	1	38	17	68	.2	12	8	450	2.43	5	5	ND	1	49	1	2	2	67	.85	.031	9	22	.39	178	.11	3	1.19	.02	.12	1	1
L78N 57+25E	1	29	19	151	.1	8	8	934	2.07	2	5	ND	1	55	2	2	2	52	1.46	.035	6	17	.33	365	.09	6	1.23	.02	.13	1	1
L78N 57+50E	1	20	13	68	.1	8	7	532	1.91	2	5	ND	1	42	1	2	2	51	.98	.025	5	16	.28	155	.09	7	1.05	.02	.12	1	1
STD C/AU-S	17	63	41	132	7.1	69	31	960	3.78	40	18	7	36	50	18	14	21	58	.46	.089	37	55	.85	176	.07	34	1.34	.06	.13	11	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L78N 57+75E	1	13	12	83	.1	7	6	496	1.94	2	5	ND	1	29	1	2	2	51	.59	.068	3	15	.23	142	.08	3	.88	.01	.11	1	1
L78N 58+00E	1	34	5	38	.1	10	9	243	2.91	2	5	ND	1	31	1	2	2	76	.46	.045	6	20	.42	79	.08	2	.39	.01	.07	1	1
L78N 58+25E	1	77	5	78	.2	10	9	350	2.50	2	5	ND	1	34	1	2	2	60	.61	.014	8	22	.37	158	.09	2	1.22	.02	.06	1	3
L78N 58+50E	2	67	835	2683	2.7	7	5	4683	2.90	39	5	ND	1	57	21	2	2	43	1.45	.113	9	12	.28	1544	.04	6	1.43	.02	.07	1	1
L78N 58+75E	1	22	25	448	.2	10	6	934	2.14	8	5	ND	1	33	4	2	3	54	.62	.063	6	18	.31	339	.09	2	1.00	.01	.07	1	1
L78N 59+00E	2	15	15	227	.2	8	5	731	1.99	9	5	ND	1	26	1	2	2	53	.42	.042	4	16	.26	217	.08	2	.97	.01	.05	1	1
L78N 59+25E	6	24	21	223	.1	10	6	1597	2.27	19	5	ND	1	29	1	2	2	55	.60	.031	5	17	.25	210	.08	2	1.07	.01	.11	1	1
L78N 59+50E	2	44	12	87	.1	10	8	430	2.62	3	5	ND	2	39	1	2	2	67	.51	.026	9	23	.44	291	.10	2	1.16	.01	.06	1	1
L78N 59+75E	1	20	10	311	.1	7	6	906	1.95	4	5	ND	1	31	5	2	2	49	.66	.057	3	15	.25	340	.07	2	.90	.01	.08	1	1
L78N 60+00E	1	13	7	82	.1	9	6	320	2.22	2	5	ND	1	27	1	2	2	62	.43	.035	3	19	.29	192	.10	5	.91	.01	.07	1	1
L77+50N 55+00E	1	15	21	220	.1	5	5	483	2.03	2	5	ND	1	25	2	2	3	55	.48	.025	4	17	.27	100	.10	2	.90	.01	.09	1	2
L77+50N 55+25E	1	21	27	170	.1	8	5	500	1.86	2	5	ND	1	37	2	2	2	51	.86	.025	5	15	.27	199	.08	5	.83	.01	.08	1	1
L77+50N 55+50E	1	11	4	161	.1	7	4	609	1.71	2	5	ND	1	17	1	2	2	45	.30	.034	3	14	.20	141	.08	2	.93	.01	.05	1	2
L77+50N 55+75E	1	11	8	94	.1	6	5	402	1.83	2	5	ND	1	20	1	2	3	49	.30	.034	3	15	.21	129	.09	2	.99	.01	.05	1	1
L77+50N 56+00E	7	29	407	2772	1.4	7	5	5192	2.20	12	5	ND	1	48	8	2	3	39	5.60	.069	8	9	.20	1344	.05	8	1.80	.01	.13	1	4
L77+50N 56+25E	1	17	44	366	.2	7	6	1376	1.90	2	5	ND	1	23	3	2	2	45	.63	.038	3	15	.22	410	.07	4	.94	.01	.10	1	2
L77+50N 56+50E	1	15	47	327	.1	6	5	787	1.64	2	5	ND	1	37	5	2	2	44	.88	.033	3	13	.23	351	.07	4	.79	.01	.09	1	1
L77+50N 56+75E	3	26	92	978	.5	5	4	2947	2.97	10	5	ND	1	34	4	2	2	42	6.11	.141	6	7	.59	616	.04	7	2.03	.01	.13	1	1
L77+50N 57+00E	1	20	6	130	.1	10	8	491	2.36	3	5	ND	1	32	1	2	2	60	.73	.082	4	18	.29	144	.07	2	1.13	.01	.08	1	3
L77+50N 57+25E	1	20	18	135	.1	9	6	516	2.04	2	5	ND	1	38	1	2	2	53	.69	.059	4	17	.27	167	.08	2	.98	.01	.09	1	1
L77+50N 57+50E	1	29	9	132	.1	10	8	491	2.45	2	5	ND	1	38	1	2	2	52	.79	.064	6	19	.37	163	.08	4	1.19	.01	.11	1	1
L77+50N 57+75E	1	27	7	140	.1	12	7	390	2.29	2	5	ND	1	33	1	2	2	60	.34	.092	5	19	.32	166	.08	4	1.11	.01	.06	1	2
L77+50N 58+00E	1	74	17	591	.1	13	9	815	2.46	5	5	ND	1	39	3	2	2	50	1.09	.032	10	21	.39	277	.08	2	1.92	.02	.04	1	1
L77N 54+00E	1	19	5	69	.1	10	5	435	1.93	2	5	ND	1	25	1	2	2	49	.34	.031	4	16	.27	146	.08	2	1.19	.01	.05	1	1
L77N 54+25E	1	20	4	92	.1	10	6	629	2.00	2	5	ND	1	24	1	2	2	53	.31	.037	4	17	.26	177	.10	2	1.34	.01	.05	1	3
L77N 54+50E	1	20	4	175	.1	6	5	857	1.65	2	5	ND	1	15	1	2	3	37	.21	.098	3	11	.19	385	.07	2	1.31	.01	.05	1	1
L77N 54+75E	1	17	7	244	.1	8	5	415	1.75	2	5	ND	1	19	1	2	2	43	.29	.043	3	14	.22	205	.08	3	1.05	.01	.06	1	1
L77N 55+00E	1	13	6	184	.1	8	5	365	1.89	2	5	ND	1	21	1	2	2	52	.34	.021	3	16	.23	178	.09	2	.91	.01	.07	1	1
L77N 55+25E	1	41	11	118	.1	10	7	680	2.40	2	5	ND	1	35	1	2	2	65	2.42	.048	7	19	.45	129	.09	2	1.10	.01	.07	1	2
L77N 55+50E	1	20	5	95	.1	7	6	549	1.96	3	5	ND	1	24	1	2	2	54	1.03	.031	4	16	.28	128	.09	2	.95	.01	.07	1	1
L77N 55+75E	1	9	4	66	.1	7	5	432	1.74	3	5	ND	1	21	1	2	2	46	.35	.030	3	15	.19	102	.09	2	.89	.01	.07	1	1
L77N 56+00E	1	20	8	91	.6	9	6	575	1.91	2	5	ND	1	27	1	2	2	50	.70	.039	4	16	.23	125	.08	2	.95	.01	.09	1	1
L77N 56+25E	1	19	8	76	.1	7	5	520	1.86	2	5	ND	1	27	1	2	2	49	.70	.040	4	15	.22	111	.07	2	.90	.01	.09	1	2
L77N 56+50E	1	21	17	135	.2	7	6	629	1.71	2	5	ND	1	35	1	2	2	45	1.46	.032	4	14	.23	155	.06	5	.78	.01	.08	1	2
L77N 56+75E	1	22	25	165	.1	7	6	715	1.75	3	5	ND	1	36	1	2	2	45	1.77	.032	4	13	.24	169	.06	4	.78	.01	.07	1	2
L77N 57+00E	1	110	19	190	.2	11	3	441	1.14	5	5	ND	1	81	2	2	2	31	2.76	.078	8	12	.25	224	.02	3	.94	.01	.03	1	1
STD C/AU-S	18	61	36	132	7.1	73	29	984	3.76	36	17	7	36	49	17	16	21	56	.46	.086	36	55	.85	174	.07	32	1.81	.06	.13	11	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L77N 57+25E	1	30	9	189	.1	9	8	627	2.07	4	5	ND	1	44	1	2	2	52	1.03	.143	4	17	.29	195	.07	3	1.19	.02	.07	1	1
L77N 57+50E	3	15	11	269	.4	7	4	1093	1.16	2	5	ND	1	58	2	2	2	30	1.51	.093	2	9	.18	295	.05	8	.60	.01	.10	1	1
L77N 57+75E	1	29	39	762	.5	9	6	994	2.46	16	5	ND	1	28	2	2	2	70	.47	.028	6	18	.51	139	.09	2	1.49	.02	.04	1	3
L77N 58+00E	1	16	10	87	.1	8	7	409	2.27	5	5	ND	1	24	1	2	2	61	.37	.044	4	19	.30	111	.09	2	1.19	.02	.06	1	1
L77N 58+25E	1	28	10	86	.3	10	9	484	2.42	6	5	ND	1	34	1	2	2	58	.76	.019	7	18	.31	199	.09	4	1.49	.02	.05	1	1
L77N 58+50E	1	19	15	87	.1	8	6	1032	1.86	3	5	ND	1	32	1	2	2	50	.75	.040	4	15	.25	254	.07	2	.97	.01	.06	1	1
L77N 58+75E	1	22	7	74	.1	9	7	491	2.20	2	5	ND	1	24	1	2	2	54	.50	.050	7	16	.27	242	.09	2	1.56	.01	.08	1	4
L77N 59+00E	1	19	10	47	.2	8	6	472	2.00	2	5	ND	1	26	1	2	2	51	.60	.021	5	16	.25	302	.09	2	1.35	.01	.05	1	1
L77N 59+25E	1	23	12	67	.1	12	7	561	2.31	5	5	ND	1	26	1	2	2	56	.50	.035	5	18	.29	284	.10	4	1.57	.01	.08	1	4
L77N 59+50E	1	31	11	79	.1	11	7	310	2.64	4	5	ND	1	25	1	2	2	60	.37	.051	5	18	.33	299	.10	2	2.16	.01	.07	1	1
L77N 59+75E	1	20	7	104	.1	11	9	977	2.60	4	5	ND	1	29	1	2	2	58	.41	.048	4	18	.33	372	.09	2	2.48	.01	.06	1	1
L77N 60+00E	1	18	7	103	.1	10	9	618	2.53	5	5	ND	1	24	1	2	2	59	.37	.074	4	18	.29	261	.10	2	2.35	.01	.07	1	1
L77N 60+25E	1	18	8	75	.1	9	7	596	2.49	5	5	ND	1	24	1	2	2	64	.36	.032	4	19	.30	210	.11	2	1.59	.01	.07	1	1
L77N 60+50E	1	12	6	76	.1	7	6	1371	1.87	2	5	ND	1	23	1	2	2	47	.36	.037	3	14	.21	240	.08	2	1.18	.01	.07	1	1
L77N 60+75E	1	15	5	45	.1	8	6	223	2.20	2	5	ND	1	19	1	2	2	55	.28	.024	3	17	.26	142	.09	2	1.35	.01	.08	1	1
L77N 61+00E	1	17	10	108	.1	7	6	655	2.05	2	5	ND	1	24	1	2	2	50	.42	.043	4	15	.26	248	.08	2	1.05	.01	.11	1	1
L77N 61+25E	1	28	10	79	.1	9	8	622	2.20	2	5	ND	1	36	1	2	2	55	.60	.038	7	17	.28	259	.10	2	1.17	.01	.11	1	1
L77N 61+50E	1	41	11	51	.1	10	9	485	2.47	2	5	ND	1	37	1	2	2	61	.67	.011	10	20	.35	235	.11	2	1.36	.02	.12	1	2
L77N 61+75E	1	55	13	69	.1	11	8	745	2.49	2	5	ND	1	38	1	2	2	51	.87	.026	11	17	.33	355	.10	4	2.26	.02	.08	1	1
L77N 62+00E	1	31	13	55	.1	11	8	516	2.34	5	5	ND	1	35	1	2	2	57	.80	.028	7	18	.32	205	.09	4	1.52	.02	.07	1	1
L77N 62+25E	1	41	6	50	.1	14	8	297	2.75	3	5	ND	1	40	1	2	2	70	.90	.021	16	23	.41	132	.12	3	1.88	.02	.09	1	2
L77N 62+50E	1	36	11	58	.1	12	11	402	3.30	3	5	ND	1	34	1	2	2	78	.65	.021	9	23	.52	146	.12	3	2.06	.02	.12	1	1
L77N 62+75E	1	52	9	56	.1	12	9	727	2.66	4	5	ND	1	32	1	2	2	55	.85	.021	10	19	.36	153	.09	5	1.77	.02	.16	1	1
L77N 63+00E	1	31	5	62	.1	9	8	784	2.08	2	5	ND	1	37	1	2	2	48	.93	.045	6	16	.28	185	.08	3	1.21	.01	.12	1	1
L77N 63+25E	1	36	10	134	.1	11	9	1354	2.47	8	5	ND	1	41	1	2	2	55	.72	.103	6	20	.35	392	.08	3	1.66	.01	.11	1	1
L77N 63+50E	1	25	10	93	.1	9	8	1145	2.31	3	5	ND	1	35	1	2	2	54	.65	.060	6	19	.35	276	.08	4	1.48	.01	.13	1	1
L77N 63+75E	1	51	13	60	.2	15	11	452	3.25	7	5	ND	3	42	1	2	2	80	.64	.026	13	28	.48	150	.13	4	1.96	.02	.13	1	1
L77N 64+00E	1	31	9	61	.1	11	9	345	2.69	4	5	ND	1	40	1	2	3	69	.72	.042	7	23	.37	124	.12	2	1.32	.02	.10	1	1
L77N 64+25E	1	29	10	60	.1	13	9	498	2.53	4	5	ND	1	33	1	2	2	64	.65	.023	8	22	.31	139	.12	2	1.50	.02	.06	1	2
L77N 64+50E	1	29	10	88	.2	12	9	871	2.94	5	5	ND	1	31	1	2	2	58	.64	.105	11	19	.45	293	.08	3	2.93	.01	.10	1	1
L77N 64+75E	1	26	14	71	.1	12	9	696	2.70	3	5	ND	1	32	1	2	2	63	.55	.059	8	22	.36	180	.10	3	2.04	.01	.11	1	1
L77N 65+00E	1	25	8	50	.1	9	8	452	2.44	4	5	ND	1	34	1	2	2	63	.51	.014	6	19	.32	133	.10	2	1.24	.01	.10	1	1
L76N 54+00E	1	12	5	57	.1	6	5	557	1.78	2	5	ND	1	24	1	2	2	51	.30	.024	3	16	.20	102	.09	2	.88	.01	.05	1	1
L76N 54+25E	1	11	9	98	.1	6	5	602	1.77	2	5	ND	1	27	1	2	2	48	.35	.024	3	16	.22	236	.10	2	.88	.01	.10	1	1
L76N 54+50E	1	17	13	213	.1	7	6	591	1.82	2	5	ND	1	25	4	2	2	47	.37	.022	4	15	.23	237	.09	3	.86	.01	.09	1	1
L76N 54+75E	1	20	18	223	.4	6	6	711	2.22	2	5	ND	1	22	1	2	2	57	.38	.019	5	13	.50	149	.07	2	1.01	.01	.09	1	2
STD C/AU-S	18	63	42	132	7.1	70	30	958	3.90	42	18	7	37	50	19	14	23	58	.46	.089	37	55	.85	175	.07	31	1.81	.06	.13	12	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L76N 55+00E	1	18	13	157	.2	7	6	407	2.45	2	5	ND	1	26	1	2	2	65	.41	.024	4	19	.36	121	.11	3	.97	.01	.08	1	7
L76N 55+25E	1	14	3	104	.1	6	6	703	2.05	2	5	ND	1	24	1	2	2	53	.43	.042	3	15	.23	122	.09	6	.98	.01	.09	1	1
L76N 55+50E	1	26	8	118	.2	10	7	535	2.20	2	5	ND	1	33	1	2	2	60	.91	.050	5	19	.32	133	.09	11	1.02	.02	.10	1	1
L76N 55+75E	1	30	18	186	.2	10	8	825	2.30	5	5	ND	1	33	2	2	3	57	.90	.030	7	21	.36	286	.10	4	1.38	.02	.14	1	1
L76N 56+00E	1	45	8	430	.3	10	9	681	2.23	4	5	ND	1	40	3	2	2	49	1.53	.032	9	19	.37	369	.09	6	1.76	.02	.05	1	1
L76N 56+25E	1	72	11	796	.4	10	7	496	1.99	4	5	ND	1	44	5	2	2	44	1.60	.043	9	18	.35	199	.07	4	1.72	.02	.05	1	1
L76N 56+50E	1	36	9	155	.4	12	9	655	2.50	4	5	ND	1	40	1	2	3	63	.66	.103	7	21	.39	152	.10	5	1.33	.02	.09	1	1
L76N 56+75E	1	23	16	546	.3	8	7	817	2.37	5	5	ND	1	34	5	2	2	62	.56	.050	6	20	.30	267	.10	7	1.30	.02	.05	1	1
L76N 57+00E	1	25	6	156	.2	10	7	313	2.81	4	5	ND	2	35	1	2	2	84	.49	.030	5	25	.35	109	.13	6	.98	.02	.08	1	2
L76N 57+25E	1	13	5	80	.1	8	8	880	2.10	2	5	ND	1	28	1	2	3	50	.47	.075	3	14	.30	151	.08	5	1.29	.01	.10	1	1
L76N 57+50E	1	27	3	56	.1	9	8	366	2.74	3	5	ND	1	27	1	2	2	72	.41	.071	4	21	.37	88	.09	8	1.13	.01	.07	1	1
L76N 57+75E	1	15	5	106	.1	9	7	733	2.41	2	5	ND	1	21	1	2	2	57	.33	.032	4	16	.29	282	.09	6	1.85	.01	.05	1	1
L76N 58+00E	1	11	2	106	.1	5	5	740	1.99	2	5	ND	1	22	1	2	2	51	.33	.037	3	15	.23	195	.09	5	1.18	.01	.05	1	1
L76N 58+25E	1	27	7	30	.1	11	6	664	2.23	2	5	ND	1	25	1	2	2	54	.48	.026	9	19	.27	293	.10	6	1.83	.02	.06	1	1
L76N 58+50E	1	16	2	62	.1	7	6	324	2.06	2	5	ND	1	22	1	2	2	51	.34	.045	4	16	.24	175	.10	4	1.43	.01	.05	1	1
L76N 58+75E	1	19	9	66	.1	9	6	281	2.26	2	5	ND	1	20	1	2	2	56	.33	.037	4	17	.30	223	.10	4	1.57	.01	.05	1	12
L76N 59+00E	1	9	3	50	.1	4	5	380	1.39	4	5	ND	1	17	1	2	2	36	.29	.037	2	10	.13	126	.08	3	.79	.01	.04	1	1
L76N 59+25E	1	19	11	123	.2	9	7	1007	2.67	2	5	ND	1	23	1	2	2	64	.38	.068	5	19	.31	260	.11	4	2.08	.01	.06	1	1
L76N 59+50E	1	19	8	174	.1	9	8	2143	2.66	4	5	ND	1	25	1	2	2	56	.48	.064	5	16	.29	435	.10	9	2.33	.01	.17	1	1
L76N 59+75E	1	21	7	85	.1	8	7	879	2.35	2	5	ND	1	29	1	2	2	59	.48	.045	4	18	.30	228	.11	3	1.39	.01	.13	1	1
L76N 60+00E	1	18	5	70	.2	7	7	640	2.16	4	5	ND	1	33	1	2	2	57	.57	.031	4	18	.28	187	.11	9	1.03	.01	.11	1	1
L75N 54+00E	1	12	2	148	.1	7	7	967	2.28	2	5	ND	1	27	1	2	2	61	.35	.022	4	18	.26	144	.11	4	1.07	.01	.07	1	1
L75N 54+25E	1	9	9	167	.2	5	4	612	1.70	2	5	ND	1	21	1	2	2	45	.34	.029	3	13	.20	122	.09	6	.85	.01	.07	1	1
L75N 54+50E	1	13	11	112	.1	6	6	721	1.86	2	5	ND	1	26	1	2	2	48	.38	.072	3	14	.21	113	.08	2	.98	.01	.07	1	1
L75N 54+75E	1	21	5	87	.4	10	8	365	2.21	6	5	ND	1	27	1	2	3	54	.38	.089	4	17	.34	133	.10	6	1.48	.01	.07	1	1
L75N 55+00E	1	34	10	102	.1	11	9	545	2.51	2	5	ND	1	34	1	2	2	67	.58	.065	6	22	.39	124	.10	7	1.21	.01	.11	1	1
L75N 55+25E	1	29	8	155	.6	10	7	490	2.19	2	5	ND	1	30	1	2	2	58	.58	.056	6	18	.33	135	.08	6	1.09	.01	.10	1	1
L75N 55+50E	1	26	2	48	.1	10	10	215	2.91	5	5	ND	2	35	1	2	2	94	.48	.024	5	25	.41	76	.14	9	1.14	.02	.06	1	2
L75N 55+75E	1	30	3	64	.2	11	10	295	3.09	5	5	ND	1	34	1	2	2	94	.46	.054	5	26	.44	88	.12	8	1.45	.02	.05	1	2
L75N 56+00E	1	30	2	69	.2	19	10	255	2.73	6	5	ND	1	31	1	2	2	65	.41	.068	4	20	.39	127	.12	6	2.24	.02	.06	1	1
L75N 56+25E	1	12	2	71	.1	10	6	344	1.83	2	5	ND	1	20	1	2	2	45	.26	.100	3	14	.21	100	.09	3	1.32	.01	.05	1	1
L75N 56+50E	1	31	2	97	.1	12	8	335	2.53	4	5	ND	1	32	1	2	2	60	.62	.052	5	20	.33	126	.09	7	1.90	.02	.06	1	1
L75N 56+75E	1	27	2	39	.1	10	8	189	2.67	4	5	ND	1	41	1	2	2	81	.49	.029	5	25	.36	73	.14	9	1.03	.02	.05	1	1
L75N 57+00E	1	20	3	73	.1	10	7	272	2.36	2	5	ND	1	23	1	2	2	60	.33	.097	4	19	.28	147	.11	4	1.69	.01	.05	1	1
L75N 57+25E	1	19	10	101	.1	9	8	421	2.52	4	5	ND	1	20	1	2	2	59	.31	.073	4	17	.28	150	.10	4	2.24	.01	.06	1	1
L75N 57+50E	1	17	5	77	.1	9	8	446	2.35	2	5	ND	1	25	1	2	2	60	.40	.048	4	18	.27	135	.11	3	1.58	.01	.06	1	1
STD C/AU-S	17	52	38	132	7.1	71	30	943	3.71	36	17	7	37	49	18	14	22	57	.47	.087	37	55	.86	176	.07	34	1.77	.06	.13	11	52

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
L75N 57+75E	1	12	12	114	.1	10	6	1381	2.06	2	5	ND	1	17	1	2	2	44	.29	.052	4	11	.18	245	.09	4	1.83	.02	.05	1	1
L75N 58+00E	1	11	11	127	.1	8	6	999	1.89	4	5	ND	1	18	1	2	2	46	.25	.047	3	13	.20	230	.10	3	1.60	.02	.04	1	1
L75N 58+25E	1	22	14	56	.1	11	7	272	2.57	2	5	ND	1	34	1	2	2	68	.44	.015	5	21	.33	190	.14	6	1.49	.01	.05	1	6
L75N 58+50E	1	17	9	64	.1	8	6	327	2.13	2	5	ND	1	23	1	2	3	57	.36	.029	4	18	.26	143	.11	3	1.06	.01	.05	1	2
L75N 58+75E	1	13	9	56	.1	7	5	401	2.00	2	5	ND	1	25	1	2	3	54	.36	.022	4	17	.24	149	.11	2	.99	.01	.07	1	1
L75N 59+00E	1	16	7	57	.1	7	6	296	2.18	2	5	ND	1	28	1	2	2	59	.41	.029	4	18	.26	133	.11	6	.96	.01	.07	1	1
L75N 59+25E	1	15	10	97	.1	8	6	391	2.23	3	5	ND	1	21	1	2	2	59	.32	.064	3	17	.25	137	.09	8	.95	.01	.05	1	1
L75N 59+50E	1	13	10	55	.1	5	5	210	1.89	2	5	ND	1	22	1	2	2	47	.30	.039	3	14	.20	100	.10	2	1.03	.01	.06	1	1
L75N 59+75E	1	18	7	54	.2	8	6	529	2.29	3	5	ND	1	29	1	2	2	61	.38	.022	4	17	.28	107	.10	3	.95	.01	.06	1	1
L75N 60+00E	1	31	13	135	.1	10	8	850	2.43	6	5	ND	1	34	2	2	2	54	1.49	.063	7	17	.31	149	.08	10	1.51	.01	.08	1	2
L75N 60+25E	1	25	10	85	.1	9	9	552	2.49	2	5	ND	1	32	1	2	2	59	.61	.034	4	17	.35	121	.09	3	1.60	.01	.07	1	1
L75N 60+50E	1	26	8	137	.1	9	9	888	2.48	6	5	ND	1	39	2	2	2	56	.89	.072	5	16	.32	154	.08	10	1.53	.01	.11	1	2
L75N 60+75E	1	57	17	336	.2	15	9	772	2.71	17	5	ND	1	43	2	2	2	51	1.08	.021	10	19	.39	119	.10	5	2.05	.02	.05	1	1
L75N 61+00E	1	19	16	207	.1	10	7	508	2.37	3	5	ND	1	25	1	2	2	50	.57	.032	5	16	.29	135	.08	2	1.69	.01	.08	1	1
L75N 61+25E	1	17	15	107	.1	9	7	1027	1.88	4	5	ND	1	29	1	2	2	45	.65	.044	4	14	.28	201	.08	6	1.12	.01	.08	1	1
L75N 61+50E	1	14	9	82	.1	8	6	326	2.02	2	5	ND	1	21	1	2	2	51	.32	.022	3	15	.25	147	.10	2	1.26	.01	.05	1	2
L75N 61+75E	1	17	12	131	.1	8	8	1188	2.10	8	5	ND	1	21	1	2	2	43	.35	.106	4	12	.26	254	.08	3	2.09	.01	.06	1	1
L75N 62+00E	1	17	10	76	.1	9	7	500	2.42	2	5	ND	1	31	1	2	2	64	.44	.028	4	19	.32	151	.13	2	1.34	.01	.07	1	17
L75N 62+25E	1	19	9	47	.1	10	8	213	2.70	4	5	ND	1	30	1	2	4	73	.39	.013	4	22	.33	97	.14	2	1.20	.01	.08	1	1
L75N 62+50E	1	20	15	110	.2	9	7	821	2.79	7	5	ND	1	27	1	2	4	59	.33	.186	4	16	.27	169	.10	6	2.05	.01	.05	1	2
L75N 62+75E	1	14	5	53	.1	7	5	553	1.86	2	5	ND	1	25	1	2	2	43	.36	.040	4	14	.23	157	.09	2	1.21	.01	.11	1	1
L75N 63+00E	1	21	11	82	.1	6	11	1046	3.51	3	5	ND	1	27	1	2	2	67	.48	.038	7	12	.55	259	.09	6	1.53	.01	.17	1	2
L75N 63+25E	1	41	15	107	.1	9	13	1054	3.78	4	5	ND	1	29	1	2	2	68	.56	.041	10	15	.57	315	.09	4	1.92	.01	.24	1	1
L75N 63+50E	1	55	10	127	.2	10	15	1582	4.59	16	5	ND	1	27	2	2	2	76	.68	.096	11	17	1.21	280	.10	3	2.61	.01	.17	1	1
L75N 63+75E	1	28	10	111	.3	8	9	506	3.35	8	5	ND	1	27	1	2	2	60	.45	.029	8	15	.48	232	.11	4	1.80	.01	.17	1	1
L75N 64+00E	1	21	12	162	.1	7	8	999	2.44	6	5	ND	1	25	1	2	2	44	.43	.046	7	13	.30	275	.08	5	1.57	.01	.15	1	1
L75N 64+25E	1	27	14	172	.1	9	10	1103	2.92	8	5	ND	1	31	1	2	2	57	.58	.046	9	18	.38	265	.09	4	1.73	.01	.19	1	1
L75N 64+50E	1	25	12	116	.1	8	9	595	2.99	7	5	ND	1	31	1	2	2	60	.67	.013	10	19	.35	172	.12	9	1.91	.02	.18	1	1
L75N 64+75E	1	39	10	131	.2	10	9	824	2.70	6	5	ND	1	38	1	2	2	57	1.54	.041	10	17	.37	218	.08	13	1.54	.02	.18	1	1
L75N 65+00E	1	37	12	91	.2	11	9	671	2.70	6	5	ND	1	39	1	2	5	59	1.21	.044	11	18	.41	190	.09	6	1.50	.02	.13	1	2
STD C/AU-S	17	62	40	132	7.1	72	31	948	3.86	38	16	7	36	50	18	14	20	57	.48	.090	38	55	.88	174	.07	34	1.71	.06	.13	11	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
C 14851	2	60	10	122	.2	9	10	946	3.50	2	5	ND	2	5	1	2	2	34	.21	.051	9	9	.10	324	.04	2	.29	.01	.16	1	1
C 14852	1	14	9	73	.1	6	9	946	2.50	2	5	ND	2	14	1	2	4	27	.17	.056	11	23	.02	1214	.02	2	.20	.01	.17	1	3
C 14853	2	22	13	87	.1	7	9	1162	2.98	2	5	ND	2	10	1	2	2	33	.18	.052	9	9	.02	1414	.02	2	.21	.01	.16	2	1
C 14854	1	7	16	82	.1	5	6	1368	2.99	5	5	ND	2	6	1	2	2	28	.18	.059	13	20	.01	714	.02	2	.20	.01	.17	1	2
C 14855	2	28	7	94	.1	5	8	884	3.18	2	5	ND	2	9	1	2	2	33	.16	.056	12	6	.01	1068	.02	2	.17	.01	.16	3	2
C 14856	1	34	13	103	.1	5	6	268	3.42	9	5	ND	2	4	1	2	2	39	.16	.059	13	18	.02	105	.02	2	.20	.01	.16	2	1
C 14857	2	146	14	98	.1	6	9	980	3.55	4	5	ND	2	5	1	3	2	37	.15	.053	13	7	.01	405	.02	2	.19	.01	.17	2	1
C 14858	1	43	15	134	.1	3	9	612	3.50	8	5	ND	2	5	1	2	2	36	.20	.062	16	15	.10	468	.02	2	.34	.01	.18	1	1
C 14859	1	11	12	199	.1	4	8	1503	2.60	3	5	ND	2	6	1	2	2	27	.20	.059	16	5	.04	575	.01	2	.26	.01	.18	1	1
C 14860	1	115	39	462	.1	5	11	1207	3.72	4	5	ND	2	4	1	2	2	35	.21	.065	18	9	.04	396	.01	2	.28	.01	.18	1	1
C 14861	1	399	20	491	.1	6	12	1598	3.97	3	5	ND	1	6	1	2	3	24	.28	.055	17	5	.12	624	.01	2	.32	.01	.18	1	1
C 14862	1	16	14	275	.1	5	11	1165	3.58	6	5	ND	2	4	1	2	2	29	.23	.068	21	10	.05	312	.01	7	.33	.01	.20	1	1
C 14863	2	28	12	325	.1	3	16	2305	4.57	4	5	ND	1	6	1	2	2	27	.21	.069	21	3	.05	928	.01	2	.33	.01	.20	1	1
C 14864	1	8	20	393	.1	5	10	1039	3.36	2	5	ND	1	7	1	2	2	44	.21	.063	17	12	.12	601	.01	8	.41	.01	.19	1	1
C 14865	1	14	21	351	.1	4	10	792	4.31	5	5	ND	2	9	1	2	2	36	.17	.061	14	5	.02	977	.01	2	.25	.01	.16	1	1
C 14866	1	172	20	561	.1	4	11	1130	4.61	3	5	ND	1	5	1	2	2	28	.20	.062	18	8	.05	288	.01	3	.31	.01	.18	1	1
C 14867	1	6	17	398	.1	3	10	2268	2.96	2	5	ND	1	6	1	2	2	21	.48	.060	18	3	.05	465	.01	4	.31	.01	.18	1	1
C 14868	1	7	17	491	.1	6	11	1223	3.60	2	5	ND	2	5	1	2	2	35	.27	.060	15	13	.25	206	.02	2	.49	.01	.17	1	1
C 14869	3	6	20	411	.2	5	17	5216	4.34	7	5	ND	2	7	1	3	2	27	.18	.060	9	4	.03	1083	.01	4	.27	.01	.18	1	2
C 14870	1	6	17	572	.2	6	14	1385	3.87	2	9	ND	2	6	1	2	2	34	.64	.056	14	10	.27	313	.01	3	.49	.01	.17	1	1
C 14871	1	5	15	324	.1	5	10	1303	2.83	2	5	ND	1	8	1	2	2	30	.48	.055	11	5	.09	634	.01	6	.28	.01	.17	1	1
C 14872	1	7	15	218	.1	5	9	1254	3.37	2	5	ND	1	8	1	2	2	44	.44	.055	12	12	.11	662	.02	6	.24	.01	.18	1	3
C 14873	2	14	16	205	.1	6	12	1979	3.57	2	5	ND	2	15	1	2	3	38	.17	.051	7	4	.02	1719	.01	10	.23	.01	.17	1	1
C 14874	1	12	14	159	.1	5	11	481	4.06	2	5	ND	1	5	1	2	3	54	.16	.054	12	15	.05	396	.02	2	.26	.01	.17	1	1
C 14875	2	33	25	99	.1	7	9	136	7.76	16	5	ND	2	7	1	5	3	135	.16	.053	10	4	.02	440'	.02	2	.25	.01	.17	4	2
C 14876	2	46	30	245	.1	8	13	640	10.27	12	5	ND	2	10	1	7	2	153	.17	.054	6	18	.04	755	.01	5	.27	.01	.17	7	4
C 14877	4	22	20	192	.1	9	9	605	9.20	11	5	ND	1	12	1	3	2	103	.15	.049	7	4	.06	772	.01	5	.21	.01	.14	6	1
C 14878	3	16	18	52	.2	6	7	262	5.96	6	6	ND	2	16	1	3	2	100	.07	.028	4	36	.01	1413	.01	5	.13	.01	.12	5	1
C 14879	4	21	34	68	.4	3	5	193	2.30	5	5	ND	1	26	1	4	2	17	.17	.060	2	4	.01	1196	.01	5	.18	.01	.14	1	2
C 14880	10	98	95	93	2.1	7	18	308	3.19	33	5	ND	1	18	1	9	2	21	.11	.037	2	21	.02	96	.01	4	.18	.01	.13	1	8
C 14881	2	28	14	101	.2	2	9	985	2.40	3	5	ND	1	14	1	6	2	4	.21	.056	4	2	.03	1270	.01	9	.24	.01	.20	1	1
C 14882	2	54	11	45	.2	4	7	747	2.11	3	5	ND	1	17	1	4	2	7	.18	.052	2	19	.05	1180	.01	7	.21	.01	.18	1	1
C 14883	2	11	11	45	.1	6	10	719	3.18	4	5	ND	1	4	1	2	2	12	.14	.049	4	4	.05	427	.01	4	.20	.01	.16	1	1
C 14884	2	8	7	28	.1	2	7	898	2.55	2	5	ND	2	6	1	2	2	7	.18	.052	8	15	.03	741	.01	2	.16	.01	.16	2	1
C 14885	2	161	12	108	.2	4	11	980	4.87	2	5	ND	1	21	1	7	2	7	.14	.044	5	2	.12	1529	.01	8	.26	.01	.18	1	18
C 14886	3	734	7	147	.3	2	12	1100	6.15	6	5	ND	1	11	1	12	5	12	.12	.038	2	8	.15	911	.01	5	.51	.01	.15	1	117
STD C/AU-R	18	64	37	132	7.1	73	31	1044	3.83	39	18	7	36	51	17	14	18	58	.51	.088	38	55	.86	178	.07	32	1.85	.06	.13	12	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM
C 14887	3	132	33	119	.4	3	7	496	3.63	10	5	ND	1	7	1	12	2
C 14888	61	1534	300	365	8.6	6	11	463	1.49	410	5	ND	1	69	12	228	2
C 14889	34	314	103	371	2.8	4	25	945	4.94	95	5	ND	1	15	4	49	2
C 14890	1	11	16	230	.1	1	9	1334	3.74	2	5	ND	1	38	1	2	2
C 14891	1	9	8	145	.1	2	7	1063	3.65	2	5	ND	1	28	1	2	2
C 14892	1	20	15	209	.1	1	6	645	2.61	2	5	ND	1	16	1	2	2
C 14893	4	128	36	880	.4	9	15	953	5.51	16	5	ND	1	9	5	2	2
C 14894	2	14	10	396	.1	2	6	2229	2.96	2	5	ND	1	8	1	2	2
C 14895	4	9	10	131	.1	7	5	1929	2.64	2	5	ND	1	25	1	2	2
C 14896	1	4	7	183	.1	1	5	1531	2.03	2	5	ND	2	14	1	2	2
C 14897	4	23	159	529	.2	4	6	1136	2.83	2	5	ND	1	202	3	2	2
C 14898	5	16	19	42	.6	4	9	1109	2.53	3	5	ND	1	15	1	2	2
C 14899	1	8	18	79	.2	3	6	1911	3.29	5	5	ND	1	17	1	2	2
C 14900	4	40	6	46	.5	4	5	1485	2.08	2	5	ND	1	6	1	2	2
C 14901	2	19	10	34	.2	1	4	993	1.34	2	5	ND	1	12	1	2	2
C 14902	6	24	32	51	1.6	3	4	1108	2.20	2	5	ND	1	16	1	2	2
C 14903	6	11	24	27	.7	2	5	257	1.13	4	5	ND	1	11	1	2	2
C 14904	4	15	15	63	.1	4	5	870	2.25	2	5	ND	1	11	1	2	2
C 14905	2	6	8	67	.1	3	4	888	2.25	2	5	ND	1	10	1	2	2
C 14906	3	10	17	288	.1	3	4	184	2.25	2	5	ND	1	6	1	2	2
C 14907	11	19	33	4383	.9	3	6	841	3.21	13	5	ND	1	45	23	2	2
C 14908	4	18	81	698	.2	7	5	826	2.74	4	5	ND	1	8	5	2	2
C 14909	2	23	7	312	.1	5	13	1705	4.71	4	5	ND	1	16	2	2	2
C 14910	2	37	6	244	.1	12	17	1913	4.82	2	5	ND	1	15	1	2	2
C 14911	1	56	8	164	.1	9	13	1521	4.07	2	5	ND	1	13	1	2	2
C 14912	1	79	8	329	.1	14	27	3485	7.31	2	5	ND	1	10	1	2	2
C 14913	1	76	9	152	.1	5	17	1579	7.00	2	5	ND	1	9	1	2	2
C 14914	1	182	7	122	.1	2	13	1545	4.92	2	5	ND	1	9	1	2	2
C 14915	1	75	3	172	.2	15	20	3575	5.94	6	5	ND	1	10	1	2	2
C 14916	3	71	5	59	.1	6	29	989	8.00	4	5	ND	1	8	1	2	2
C 14917	2	692	9	82	.2	4	27	828	8.01	7	5	ND	1	4	1	2	2
C 14918	2	1969	4	114	.9	5	24	639	10.84	6	5	ND	1	11	1	2	17
C 14919	2	513	3	121	.3	8	13	1175	8.88	5	5	ND	1	7	1	2	2
C 14920	1	568	6	150	.6	9	19	2323	7.54	10	5	ND	1	7	1	2	2
C 14921	1	277	8	96	.5	4	14	1427	7.07	12	5	ND	1	8	1	2	2
C 14922	1	236	5	88	.1	2	14	1118	9.26	7	5	ND	1	5	1	2	2
STD C/AU-R	17	62	43	132	7.2	72	31	951	3.84	41	20	7	37	51	18	15	23

SAMPLE#	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
C 14887	5	.19	.050	2	2	.05	429	.01	6	.35	.01	.24	1	5
C 14888	3	.62	.044	3	2	.19	164	.01	10	.32	.01	.24	15	4
C 14889	4	.94	.043	3	3	.37	256	.01	8	.26	.01	.23	1	5
C 14890	4	1.00	.053	8	1	.40	1527	.01	10	.29	.01	.23	1	1
C 14891	3	.66	.050	10	1	.39	1003	.01	11	.31	.01	.24	1	2
C 14892	3	.40	.056	8	1	.16	792	.01	13	.33	.01	.24	1	1
C 14893	24	.16	.065	6	13	.35	53	.01	2	.81	.01	.20	1	1
C 14894	9	.45	.057	16	3	.62	313	.01	6	.69	.01	.15	1	1
C 14895	3	1.52	.053	12	7	.59	628	.01	3	.29	.01	.21	1	1
C 14896	3	.52	.057	14	1	.24	349	.01	3	.73	.01	.17	1	1
C 14897	3	1.12	.051	7	3	.62	54	.01	4	.43	.02	.17	1	1
C 14898	2	.31	.065	10	3	.10	69	.01	5	.38	.01	.26	2	3
C 14899	4	1.21	.061	8	5	.60	81	.01	4	.62	.02	.25	1	2
C 14900	3	.30	.057	14	3	.15	92	.01	3	.52	.01	.24	2	1
C 14901	2	.60	.065	15	2	.18	213	.01	2	.60	.01	.21	2	1
C 14902	2	1.14	.061	7	2	.20	65	.01	7	.61	.01	.19	1	1
C 14903	1	.57	.072	9	1	.08	87	.01	3	.46	.01	.27	2	1
C 14904	4	.82	.051	7	4	.24	96	.01	2	.48	.02	.15	1	1
C 14905	5	.43	.055	11	2	.32	321	.01	3	.74	.02	.15	1	1
C 14906	8	.18	.052	15	3	.36	136	.01	4	.85	.01	.13	1	1
C 14907	10	.20	.053	10	3	.41	48	.01	2	.63	.02	.15	1	1
C 14908	17	.39	.058	13	6	.59	201	.01	4	.72	.03	.08	1	3
C 14909	69	.91	.103	11	9	1.54	170	.18	3	1.52	.05	.08	1	3
C 14910	75	.50	.091	8	13	1.31	269	.09	2	1.60	.04	.10	1	1
C 14911	23	.32	.105	5	7	.11	378	.01	10	.52	.01	.26	1	3
C 14912	51	.38	.106	9	11	.37	595	.01	15	1.04	.01	.25	1	1
C 14913	28	.38	.130	11	3	.20	405	.01	4	.84	.02	.26	1	2
C 14914	14	.29	.101	7	2	.14	432	.01	9	.57	.01	.28	1	1
C 14915	86	2.50	.078	11	35	1.46	720	.03	3	1.56	.01	.23	1	2
C 14916	55	.19	.062	7	5	1.48	511	.01	2	2.65	.01	.17	1	5
C 14917	23	.15	.057	13	2	.46	336	.01	9	1.00	.01	.21	3	13
C 14918	28	.19	.075	11	3	.87	211	.01	2	2.46	.01	.18	2	65
C 14919	38	.48	.080	12	10	.54	385	.01	2	1.28	.01	.28	1	23
C 14920	66	.32	.099	10	15	.48	507	.01	7	1.27	.01	.26	1	2
C 14921	28	.26	.103	10	3	.15	392	.01	6	.60	.01	.28	2	2
C 14922	63	.28	.104	9	2	.62	236	.05	8	1.32	.01	.18	1	1
STD C/AU-R	58	.48	.090	38	55	.88	176	.07	32	1.72	.06	.13	11	490

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
C 14923	2	787	7	94	.3	2	11	1026	8.02	9	5	ND	1	7	1	2	2	20	.26	.106	6	1	.05	237	.01	6	.45	.01	.28	3	5
C 14924	18	4700	17	441	23.2	6	17	790	12.76	168	5	ND	1	4	19	935	3	25	.14	.066	2	5	.05	192	.01	4	.48	.01	.29	1	760
C 14925	1	132	4	194	.6	12	24	2495	10.57	3	5	ND	1	14	1	2	2	54	.94	.064	6	23	.45	865	.01	4	.85	.01	.28	1	8
C 14926	2	139	6	128	.7	5	18	1429	9.19	8	5	ND	1	8	1	12	2	30	1.08	.079	10	6	.27	670	.01	6	.85	.01	.26	1	4
C 14927	3	182	7	135	.2	5	19	2014	8.55	9	5	ND	1	7	1	3	2	59	.44	.064	11	7	.69	738	.01	4	1.70	.02	.21	1	6
C 14928	3	77	2	124	.1	4	19	1806	7.60	7	5	ND	1	6	1	2	2	39	.47	.065	13	7	.97	247	.01	9	1.36	.02	.16	1	2
C 14929	1	41	2	116	.1	5	14	2037	5.81	5	5	ND	1	12	1	2	2	39	.70	.066	11	7	1.14	402	.01	3	1.01	.03	.22	1	1
C 14930	1	13	6	99	.1	2	11	1556	4.66	2	5	ND	1	25	1	2	2	12	.92	.066	9	1	.70	447	.01	6	.45	.01	.26	1	1
C 14931	1	192	5	137	.4	2	12	1994	5.25	3	5	ND	1	21	1	2	2	13	1.15	.068	6	1	1.04	439	.01	8	.44	.01	.23	1	4
C 14932	2	15	4	110	.1	5	9	1861	3.55	2	5	ND	1	19	1	2	2	24	2.07	.059	9	6	.97	211	.01	2	.66	.03	.15	1	1
C 14933	2	97	2	27	.1	1	18	79	19.14	4	5	ND	2	2	1	2	2	10	.01	.018	2	2	.01	148	.01	5	.16	.01	.10	2	1
C 14934	2	80	3	34	.1	3	18	147	16.16	2	5	ND	1	3	1	2	2	8	.02	.028	3	2	.01	522	.01	2	.19	.01	.12	3	1
C 14935	57	590	8989	13514✓	27.9	4	1	404	.66	30	5	ND	1	331	160	106	3	11	.51	.047	2	4	.03	104	.01	5	.15	.01	.09	1	1
C 14936	4	11623✓	48	175	4.2	3	14	718	7.71	5	5	ND	1	7	2	6	4	10	.20	.051	3	1	.07	388	.01	2	.71	.01	.24	9	129
C 14937	3	725	159	201	13.7	7	2	187	.55	81	5	ND	1	23	3	122	3	6	.06	.009	2	7	.07	1381	.01	2	.22	.01	.10	1	18
STD C/AU-R	18	63	38	132	7.1	72	31	1003	3.94	41	18	6	36	50	18	16	24	58	.47	.088	37	54	.88	174	.07	31	1.89	.06	.13	12	510

✓ - ASSAY REQUIRED FOR CORRECT RESULT -

Summary of Rock Samples

Tag #	Sample #	Type	Width	Location	Comments
14933	IM89512-2	Select	-	L0+25N 4+15E	>50% specular hematite
14934	IM89512-1	Chip	1m.	"	10-15% Hem. Dacitic Tuff
14935		Select	-	L77+80N 56+15E	LD showing ga., sph., mal.
14936		Chip	1.8m.	L82+05N 54+80E	mal., az., cpy., py., bornite in shear z.
14937		Chip	0.3m.	L79+10N 56+35E	mal., az, pos. gn. in quartz-carb. vein.

APPENDIX B

GEOPHYSICAL SURVEY NOTES

① Ft. 55E Stake 58N

May 14 Mag 0 57 0 Sensitive stumps ab road at BL

Mag	Seattle		Cutter		Mag
May 14 RL 80N	-7°/-8		-28/+10		56992
80N 55+25E	-4/-10		-18/0		57208
55+50E	-8/-8		-22/+7		57297
55+75E	-4/-12		-20/+10		57289
creek NE 56+00E	-4/-12		-22/+5		57153
56+25E	-6/-6		-18/+5		56969
56+50E	-16/-12		-7/+5		56939
56+75E	-15/-10		-8/+4		56911
57+00E	-10/-6		-6/-4		56880
57+25E	-11/-1		-6/-4		56875
50E	-4/0		-9/-7		56874
75	+5/+2		-13/-10		56878
5800	+1/-1		-7/0		56925
25	+5/+2		-16/-7		56840
edge of cliff 50	-8/-5		+3/-6		56790
75	0/+5		-12/-10		56969
5900	-4/0		-12/-3		57123
25	-4/+3		-10/-8		57035
50	-8/-1		0/-6		57224
75	-6/+1		-5/-4		57140
6000	-9/-3		0/+3		56849

May 14 Dixon Mt ②

Line 79N	Seattle	Quad	Cutter	Quad	Mag
6000E	-5	-2	-12	-3	56887
Cross NE 59+75	-8	-2	-12	0	57120
Creek 50	-12	-4	-10	0	57258
25	-14	-3	-8	+3	57164
59+00	-11	-4	-4	+2	57090
75	-10	-4	-8	+2	56988
50	-10	-4	-4	-2	56819
25	-7	-2	-7	-2	56976
5800	-8	-3	-5	+5	56830
75	-3	-3	-14	-3	56895
50	0	-1	-15	-8	56873
25	-4	-1	-13	-4	56553
5700	-6	0	-12	-6	56909
75	-9	-1	-7	-2	56890
50	-10	-1	-6	-2	56920
25	-11	-1	-7	-2	56961
5600	-11	-2	-4	+4	56885
75	-11	-3	-4	+1	57016
50	-5	0	-17	-3	56864
25	0	-4	-14	+2	56904
Road 5500	0	-8	-12	+12	56979

③ May 14

Line 79	Seattle	Quad	Cutler	Quad	Mag
54+75E	0	-10	-10	+12	57009
50	+2	-10	-12	+10	57117
25	+2	-11	-12	+5	57015
5400	+3	-11	-14	+12	57069
Line 80/5400	-3	-8	-12	+12	57063
54+25	-1	-7	-16	+5	57003
50	0	-8	-22	+3	56996
75	0	-6	-22	+7	57093
~~					
B.L.					

Check mag at Base Δ 57033 @ 4 PM

④ May 15 — Mag at start — 56765

Line 78 N	Seattle	Quad	Annap. ~~Cutler~~	Quad	Mag.
BL 5500E	+4	-3	-13	+5	57045
25	-7	-6	-8	+3	57030
50	-11	-1	-5	+2	56977
75	-14	+1	-5	+2	57014
5600	-14	+2	-6	+2	56988
25	-16	-1	-11	+4	56997
50	-10	0	-9	+5	56971
75	-9	+4	-10	+2	56888
5700	-19	-1	-10	+8	56905
25	-14	-3	-16	+2	56780
50	-15	0	-14	+5	56893
75	-14	-3	-10	+6	56901
Road EW 5800	-20	-2	-4	+5	56940
Stream SE 25	-28	-7	-4	+5	56931
Cross stream 50	-19	-2	-9	+2	56592
75	-9	+4	-16	0	56904
5900	-9	-4	-17	-3	56914
25	-6	-1	-22	-3	56913
50	0	0	-29	-6	56904
75	-4	+3	-20	-3	56860
6000	-9	0	-17	-3	56892

⑤ May 15 – IRON MT.

Line 77N	Seattle	Q	Annap	Q	Mag
6000	-11	0	-6	-4	56917
5975	-12	+1	-11	+1	56889
50	-14	+4	-5	-3	56909
25	-16	+1	-2	+2	56917
5900	-8	+8	-6	-6	56780
75	-12	+5	-3	-2	56838
50	-9	+5	-3	+2	56810
25	-6	+6	-12	-2	56756
5800	-10	+6	-10	-1	56745
75	-12	+6	-4	0	56789
50	-15	+5	-2	+1	56889
25	-9	+4	-8	0	56909
Marsh 5700	-9	+2	-9	+2	56896
75	-5	0	-10	+2	56957
50	-4	0	-11	+4	56788
25	-5	+2	-7	+7	56708
5600	-12	-2	-5	+5	56945
75	-11	-3	-6	+7	56933
50	-10	-3	-6	+3	56892
Road 25	-7	-2	-5	+5	56820
5500	-6	-5	-5	+4	56982

Check Mag at Base 56785 12[30] PM

May 15 ⑥

Mag at base 56771

Line 76N	Seattle	Q	Annap	Q	Mag
5500E	-21	-7	-3	+10	56862
ROAD N 25	-15	-8	-3	+8	56829
50	-10	-5	-5	+5	56860
75	-5	-2	-8	+3	56885
5600	0	0	-12	+8	56940
Marsh 25	+2	+1	-13	+1	56907
50	-5	+2	-7	+2	56921
Creek N 75	-12	+3	-3	0	56836
5700	-9	+6	-7	-3	56863
25	-6	+9	-8	-6	56703
50	-7	+6	-10	-2	56924
75	-6	+8	-11	-6	56816
5800	-6	+8	-10	-10	56832
25	-7	+7	-7	+5	56840
50	-11	+4	-6	-3	56950
75	-12	+4	-4	-3	56994
5900	-14	+3	-5	-2	56913
25	-11	+4	-6	-6	56805
50	-12	+3	-6	+1	56890
75	-10	+3	-6	-4	56896
6000	-9	+3	-8	+3	56962

May 15 (7)

	Seattle	Q	Annap	Q	Mag
Line 75					
60 00 Road NE	-6	-2	-12	0	56815
75	-3	0	-15	0	56776
50	-7	0	-11	+1	56993
25	-9	-2	-12	+2	56768
59 00	-8	+1	-12	-2	56924
75	-10	-2	-11	+2	56783
50	-7	+3	-12	+6	56938
25	-7	+5	-11	-2	56927
5800	-9	+2	-9	-1	56865
75	-6	+5	-12	-5	56797
50	-5	+6	-12	-4	56828
25	-7	+4	-13	-8	56802
5700	-10	+4	-9	+2	56852
75	-9	+2	-13	-3	56830
Creek N 50	-10	+2	-11	-6	56755
25	-5	0	-10	-1	56841
5600	-1	+3	-9	-3	56822
75	-7	+1	-6	-2	56744
50	-7	-2	-8	+3	57069
ROAD NW 25	-3	-4	-16	+9	56876
BL 5500	-8	-6	-16	+9	56882

Mag at Base check pt 56765

May 16 Mag at B3 — 57119 (8)

L82N	Seattle	Quad	Gutter ~~Annap~~	Quad	Mag
Road 55+50E	-17	-12	-10	+3	56985
55+75	-7	-10	-18	+6	56950
56+00	-4	-7	-21	+6	56954
25	+2	-6	-22	+3	57051
Road NW 50	+5	-9	-26	+4	56905
75	+5	-11	-25	+8	56956
57 00	+4	-12	-22	+6	56755
25	-2	-12	-15	+1	56759
50	-2	-10	-15	+10	56950
75	-3	-5	-15	+8	56833
5800	-11	-9	-9	+7	56858
25	+2	-1	-16	-2	56821
50	+2	+1	-16	-2	" 856
75	-2	0	-8	-4	" 985
Creek NE 5900	-6	+3	-8	-7	919
25	-7	+5	-8	-6	57054
50	-6	+4	-8	-9	56878
Road (W) 75	-9	+3	-6	-5	952
60 00	-12	-1	-1	-2	693

May 16 (9)

Line 81N	Seattle	Q	Gutter	Q	Mag
60+00E	-7	+3	-5	-6	56890
59+75E	-8	+2	-10	-5	869
50	-2	+6	-14	-5	972
25	-6	+6	-3	-6	871
5900	-5	+5	-5	-6	802
75	-12	0	-2	-5	857
50	-2	+1	-11	-3	909
25	-8	0	-6	-4	893
5800	-11	+2	+2	-2	993
75	-18	-3	+10	+5	887
50	-11	-7	-1	+6	835
25	-4	-10	-6	+10	996
5700	+4	-10	-19	+13	57155
75	+8	-13	-23	+13	56908
50	0	-12	-24	+12	872
Road NNE 25	-5	-9	-19	+11	57078
5600	-3	-10	-13	+6	125
75	-8	-9	-15	+9	115
50	-5	-5	-15	+5	56945
25	-6	-7	-13	+3	57064
BL 5500	-8	-6	-13	+9	047

May 16 – Brown Mt. (10)

	Seattle	Q	Gutter	Q	Mag
L81N (cont)	-3	-2	-16	+4	56974
5475E	-6	-4	-11	+4	958
50	-4	-1	-13	+2	57130
25	-3	+2	-14	+2	138
(5400E)	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
L 82N					
5400E	-2	+6	-14	-6	57190
25	+2	+6	-17	-6	56953
50	-2	+1	-14	+1	940
Showing* 75	-2	0	-17	+1	800
BL 5500	-3	-2	-15	-2	457
+25	-7	-4	-14	+6	937

Mag at B3 – 57103

May 16 - Iron Mt (11)

Line 75N	Seattle	Q	Cutler	Q	Mag
BL				check	56920
5475E	0	-8	-12	+14	810
50E	+10	-12	-18	+15	859
25E	+12	-9	-21	+9	814
5400E	+9	-7	-20	+8	687

Line 76N					
5400E	+5	-3	-13	+4	56903
25	+7	-3	-15	+5	957
50	+5	-3	-15	+4	895
75	-14	-10	+3	+13	971

Line 77N					
5475E	0	-4	-11	+5	992
50E	+3	-5	-10	+4	923
25E	-1	-5	-7	+5	764
5400E	-4	-3	0	+5	57007

Line 78N					
54E	-4	-4	-6	+8	57017
5425	-8	-11	-3	+11	054
50	-8	-15	+3	+15	031
75	+4	-7	-3	+12	042
5500 BL	check →				038

May 17 IRON MT. (12)

Check Mag at B3 — 57107

LINE 84N	Seattle	Q	Cutler	Q	Mag
BL 5500E	check →				56859
25	-6	+6	-8	-8	865
50	-2	+4	-15	-10	57106
75	+2	+4	-20	-7	56994
5600	+8	+3	-25	-9	914
25	+12	+2	-26	-4	828
50	+15	+5	-29	-3	870
75	+13	+18	-33	-28	823
5700	-8	-11	+1	+9	752
25	-12	-12	-1	+11	840
50	-8	-9	-6	+6	856
75	-5	-7	-8	+4	964
5800	+1	-2	-14	+3	798
25	-1	-6	-12	+5	808
50	+2	-8	-16	+10	728
75	+7	-6	-17	+7	772
5900	+4	-7	-15	+8	666
Road N 25	-1	-6	-8	+5	684
50	-5	-2	-7	0	734
75	-11	+2	-5	-1	759
6000	-15	+2	+1	-1	829

(13) May 17 — Mag at B3 — 57107

Line 84N	Seattle	Q	Cutler	Q	Mag
5500 BL	-8	+9	-5	-12	56863
5475	-11	+9	0	-10	963
50	-15	+8	+3	-10	898
25	-15	+6	+3	-7	552
5400	-10	0	0	-2	510
75	+6	-2	~~-5~~ 18	~~-2~~ -5	585
50	+6	-5	-21	-2	542
25	+5	-6	-15	+5	708
5300	+10	-6	-25	+5	808
75	+7	-6	-27	+2	725
50	+10	-7	-25	+5	706
25	+11	-5	-28	+3	734
5200	+11	-5	-25	+4	778
75	+12	-4	-27	+4	695
50	+11	-6	-26	+5	745
OC 25	+9	-8	-23	+3	777
5100E	+10	-8	-25	+6	734

(14) May 17

L83N	Seattle	Q	Cutler	Q	Mag
51+00E	+10	-8	-26	+2	57895
25	+2	-8	-15	+6	811
50	-1	-9	-14	+5	608
75	-1	-4	-15	+2	848
5200	-2	-2	-9	0	705
25	-3	-2	-16	-1	617
50	-3	-3	-18	-5	676
75	+4	+1	-25	-5	790
5300	-1	+2	-13	-5	435
25	-10	+2	-1	-5	711
OC 50	-13	+3	+1	-7	795
75	-11	+5	+1	-9	657
5400	-8	+8	+2	-9	798
25	-3	+8	-10	-9	58074
50	-5	+7	-12	-9	205
75	-6	+3	-10	-6	098
BL 5500	-8	0	-8	-4	58871

(15) May 17   Mag at B3 — 57102

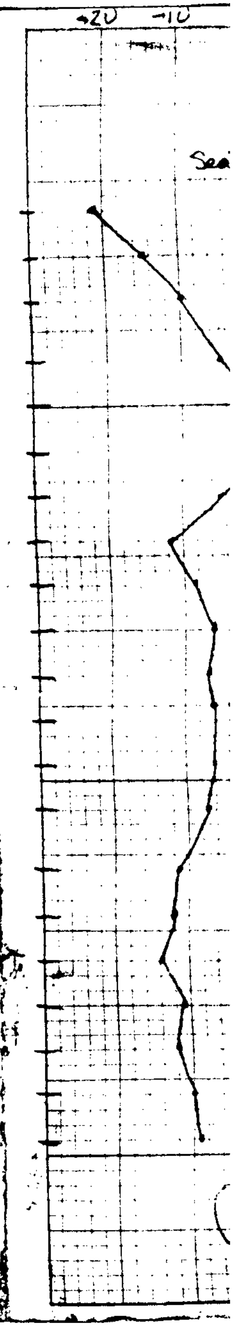
LINE 83N	Seattle	Q	Cutter	Q	MAG
55+25E	-10	-2	-11	-4	56918
50	-5	-2	-12	+4	967
75	-1	0	-12	0	906
5600	-4	-7	-6	+8	876
25	-1	-10	-7	+7	56900
50	+11	-4	-17	+4	57178
75	+18	0	-24	+3	56810
5700	0	-9	-10	+7	846
25	+1	-8	-15	+8	867
50	+4	-5	-14	+5	893
75	+3	-7	-21	+2	796
5800	-1	-8	-13	+5	816
25	-8	-11	-6	+7	728
50	-7	-9	-10	+9	880
75	+3	-3	-17	0	866
5900	+3	-3	-16	-3	836
stream 25	-7	-6	-2	+7	758
50	-2	0	-10	-3	834
75	-2	+3	-6	-4	875
6000	-6	+3	-5	-4	56877

(16) May 17

	Seattle	Q	Cutter	Q	Mag
L82N54E	→				57220
Cliff QC 5375	-10	+4	-6	-8	57182
5350E	-10	+5	-7	-10	56926
25	-14	+5	-4	-6	348
5300	-18	+4	+4	-5	892
75	-20	0	+5	-5	222
50	-18	-2	+5	-1	55994
25	+2	+5	-14	-6	56058
5200	+10	0	-25	-5	56153

L81N

	Seattle	Q	Cutter	Q	Mag
52E	-4	+2	-8	-10	56512
+25	-8	+2	-5	-6	55782
+50	-4	0	-9	-5	57035
75	-4	+3	-5	-5	56847
5300	-3	+4	-5	-8	56933
25	0	+5	-9	-8	915
50	-12	0	-11	-7	990
75	-1	+5	-21	-8	57421

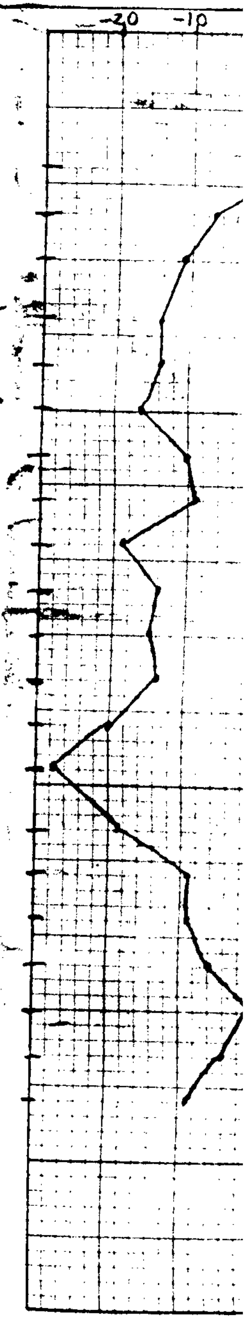


(17) May 19 IRON MT. Mag at E3 57110

LINE 86N	Seattle	Q	Cutter	Q	Mag.
BL 86N 5500E	-3	+3	-9	-7	56564
5475	-9	-9	0	+5	576
50	0	-7	-8	+7	667
25	+6	-8	-12	+5	710
5400E	+3	-9	-13	+13	750
75	-8	-11	-1	+16	755
50	-2	-8	-5	+12	815
25	+1	-5	-7	+11	762
5300	+5	-5	-14	+10	811
75	+3	-4	-15	+8	837
50	-1	-4	-10	+8	835
25	+1	-5	-7	+8	960
5200	+9	-4	-13	+7	57014
75	+20	0	-26	0	57170
50	+16	-1	-25	0	276
25	+9	-4	-21	0	478
5100	+4	-4	-18	-1	56772
75	+7	+2	-25	-2	721
50	+8	-2	-18	+2	57102
25	+10	-4	-15	+3	57114
5000	+11	-5	-15	+3	56771

(18) May 19

Line 85N	Seattle	Q	Cutter	Q	Mag
5000E	+15	-4	-28	+4	56754
+25	+21	-2	-31	0	762
+50	+23	-3	-28	-1	745
+75	+6	-5	-23	+3	750
5100	+7	-3	-20	-2	879
+25	+9	-2	-20	0	714
+50	+2	-4	-13	+4	880
+75	+7	-9	-14	+6	707
5200	+5	-6	-21	+3	789
+25	+9	-6	-24	+6	722
+50	+10	-5	-27	+4	757
+75	+8	-10	-22	+10	821
5300	+10	-10	-25	+9	684
+25	+11	-8	-25	+3	748
+50	+7	-10	-26	+11	777
+75	+2	-10	-18	+7	666
Creek 5400	+14	-3	-20	0	512
+25	+1	+5	-17	-5	577
+50	-13	+7	0	-10	575
+75	-30	+4	+15	-1	612
BL 5500	-29	+4	+14	-8	57102

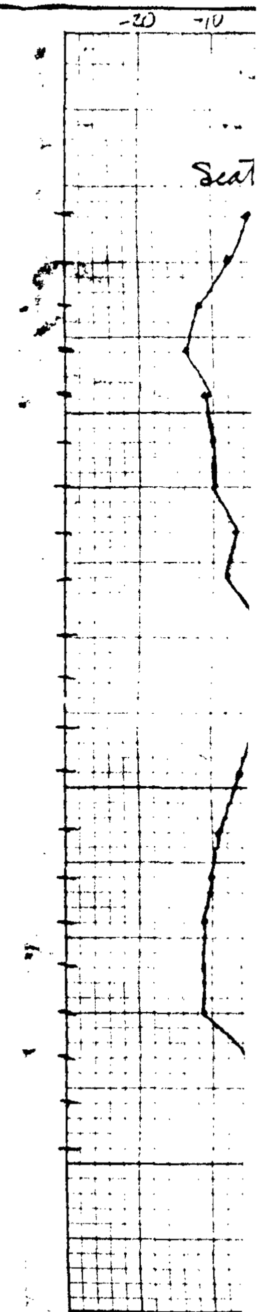


(19) May 19

LINE 86N	Seattle	Q	Cutler	Q	Mag
BL 55E	→			→	56551
+25E	-5	+5	-5	-12	451
+50	-22	+3	+10	-7	383
+75	-19	+5	+7	-7	513
56+00	-17	+2	+5	-5	980
+25	-8	+5	0	-4	905
+50	-9	-1	-5	-6	918
+75	-1	+2	-16	-4	874
57+00	+10	+2	-22	-2	868
+25	+16	+4	-27	-3	834
+50	+17	0	-29	0	777
+75	+3	-6	-15	+2	735
58+00	-1	-6	-8	+4	825
+25	-6	-6	-4	+7	735
+50	-7	-4	-5	+7	658
+75	-5	-2	-8	+3	639
Stream N 59+00	+1	+4	-18	-2	687
+25	-6	+4	-16	-1	672
+50	-5	+6	-15	-2	907
+75	-3	+7	-15	-5	57124
60+00	-9	0	-5	+2	57100

(20) May 19

LINE 85N	Seattle	Q	Cutler	Q	Mag
Road E 60+00 E	-16	0	0	+3	57047
59+75	-15	-1	-5	+4	56874
+50	-17	-2	-2	+3	57260
Stream N +25	-1	-1	-12	0	56623
59+00	0	-5	-12	+7	616
58+75	+1	-7	-15	+4	802
+50	+4	-3	-17	+2	807
+25	-5	-13	-7	+14	678
58+00	-7	-7	-6	+2	771
57+75	-3	-2	-8	+2	774
+50	-8	-6	-7	+5	780
+25	-5	-6	-9	+7	700
57+00	+14	-1	-28	0	772
56+75	+19	+2	-37	-8	844
+50	+10	0	-33	-12	836
+25	+9	+3	-25	-10	849
56+00	+4	+6	-18	-8	904
55+75	-4	+5	-13	-12	868
+50	-10	+5	-5	-12	992
+25	-18	+4	+5	-11	898
55+00				check	57079



(21) May 20

L 77+50N	Seattle	Q	Cutter	Q	Mag
BL 55E	0	-5	-10	+9	56974
55+25E	-13	-5	+2	+5	974
+50	-13	-2	+2	+4	57098
+75	-12	0	0	+5	044
56+00	-11	+1	-3	+3	56892
+25	-11	-1	-4	0	56907
+50	-5	+3	-7	-2	858
+75	-5	+2	-5	+7	932
5700	-15	-2	+2	+9	936
+25	-18	0	+3	+8	912
+50	-13	+3	-3	+2	836
Creek bottom +75	-12	+4	-5	-2	977
" 5800	-19	+1	-5	+2	902

Showing - galena - barite 77+90N 5625E

(22) May 20

Line 78+50N	Seattle	Q	Cutter	Q	Mag
5800E	-15	-6	-10	+4	56808
5775	-6	-2	-16	-2	~~56775~~ 940
50	-6	0	-17	-3	876
25	-10	0	-12	-2	907
5700	-11	0	-10	-2	952
75	-13	0	-6	-2	978
50	-15	0	-3	+3	903
25	-13	+1	-4	+1	910
5600	-14	0	0	+2	948
Creek bottom 75	-11	+3	0	+3	57000
" 50	-7	0	-4	+4	164
25	-3	-4	-12	+1	015
BL 5500	+5	-5	-18	+6	56950

Showing at L79N 5635E — barite, azurite.

Small showing 5675E / L 80N

(23) May 23 - 1989 | B3 Mag 57071

L8250N	Seattle	Q	Cutter	Q	Mag
5500BL	-15	-5	-11	-1	57018
5475E	-8	+2	-18	-6	56950
50	-2	+5	-15	-6	914
25	-4	+5	-11	-8	57011
5400E	-5	+7	-12	-11	57280
75	-11	+5	-4	-11	56775
50	-14	+6	-2	-10	56800
25	-15	+6	0	-8	56355
5300E	-14	+2	0	-3	56134
75E	-5	+2	-14	-4	395
50E	0	0	-19	-4	56556
25E	+4	0	-25	-6	582
5200E	+3	-1	-20	-2	603

L8250N					
5525E	-15	-4	-7	+1	56988
50	-8	-2	-15	+2	57038
75	-7	-4	-15	+3	56884
5600E	-5	-6	-15	+2	900

(24)

L8150N	Seattle	Q	Cutter	Q	Mag
5200E	-8	+3	-6	-5	56820
+25	-3	+7	-12	-9	56572
50	-12	+5	-6	-7	494
75	-19	+6	0	-7	698
5300E	-31	+1	+8	-6	541
+25	-18	+5	-5	-6	57015
+50	-8	+8	-13	-13	57397
+75	-5	+9	-18	-9	56909
5400E	-2	+8	-18	-6	57144
+25E	-1	+5	-20	-7	57097
+50	-4	0	-15	+3	084
+75	-3	-2	-15	+2	076
BL 5500E	-12	-4	-11	+5	56900

L8150N 56E	-9	-10	-11	+11	57016
55+75	-6	-6	-12	+4	56667
+50	-7	-7	-14	+1	924
+25	-7	-5	-10	+7	968

(25)

L 80+50N	Seattle	Q	Cutter	Q	Mag
BL55E	-7	-4	-21	+8	57190
+25	-7	-8	-22	+8	56948
+50	-9	-11	-21	+11	57296
+75	-8	-11	-18	+9	57022
56E	-11	-15	-16	+14	025
(Cross Rd at jctn) +25	-6	-14	-18	+11	054
+50	-9	-11	-22	+10	072
+75	-5	-14	-20	+14	004
57E	-7	-8	-10	+5	050
25	-18	-5	+3	+5	56924
50	-19	-1	+2	-1	956
75	-15	0	+3	-6	846
58E	-5	+3	-8	-7	948

To Hawaii 190° grid
To Cutter 55° grid
To Seattle 160° grid.

(26)

L7950N	Seat	Q	Cut	Q	Mag
58E	+2	+1	-22	-9	56809
5775	-2	0	-22	-8	852
50	-8	0	-10	-12	894
25	-12	-2	-7	-6	922
57E	-17	-4	-6	-4	910
56 75	-21	-4	-5	-1	893
50	-15	-2	-12	-3	931
25	-15	-4	-7	+4	916
56E	-18	-5	-5	+3	968
Stream 5575	-14	-6	-8	+4	57023
50	-5	-6	-25	+4	070
25	-1	-9	-30	+8	295
BL 55E	0	-7	-32	+3	152

L75N (27)

	Hawaii	Q	Cutter	Q	Mag.
60E	+1	-2	-11	+3	56770
60+25E	+1	0	-12	-1	808
+50	+5	+4	-15	-3	824
+75	+5	+5	-13	-1	785
61+00	-5	+4	-15	-4	817
+25	-5	+2	-9	+2	830
+50	-26	-4	+16	+7	740
+75	-30	-5	+20	+8	605
62+00	-28	-3	+19	+8	928
+25	-29	-5	+17	+2	57182
+50	-27	-2	+16	0	57536
+75	-23	0	+12	+2	57120
6300	-17	+4	+5	-2	57338
+25	-18	-2	+5	+1	57084
+50	-24	-8	+10	+5	56949
+75	-25	-7	+10	+7	974
6400	-22	-7	+9	+7	978
+25	-24	-6	+11	+7	853
+50	-27	-10	+11	+5	760
+75	-30	-8	+14	+8	764
65+00E	-30	-10	+13	+8	710

L77N (28)

	Hawaii	Q	Cutter	Q	Mag
65+00E	-32	-8	+18	+6	56882
64+75	-25	-7	+13	+5	704
+50	-24	-6	+10	+6	625
+25	-4	0	-12	-3	668
Creek[N] 64+00	-5	-2	-13	-5	656
63+75	0	+2	-15	-4	748
+50	-2	0	-9	-2	786
+25	-5	-4	-5	+2	819
63+00	-4	-3	-7	+2	934
62+75	-2	-3	-12	0	57048
+50	-3	0	-9	0	56996
+25	-6	-4	-5	+2	57142
Road 62+00	-2	0	-6	-5	56831
61+75	-5	0	-7	+4	790
+50	-7	-4	-2	+4	868
+25	-10	-3	-1	+2	865
61+00	-3	+3	-6	-2	890
60+75	-6	+1	-4	0	902
+50	-8	+2	-2	-3	57036
+25	-7	+4	-2	-7	56932
60+00	-8	+4	N/A		56914

APPENDIX C

DRILL HOLE LOGS

DRILL HOLE SECTIONS FIGURES 11a, 11b, 11c, 11d

— STRONG d
— — MOD
. . . . weak
d = diss or flooded
v = veinlet or vein

DRILL HOLE EVALUATION SUMMARY

Company GOLDEN DYNASTY RES LTD. Property Iron Mtn Section No. 1 Hole No. IM 89-1

Started May 12/89	Bearing 293	Lat.	Collar El. 1588 m.	Logged by W.A. Howell / PAC
Completed May 15/89	Angle -45°	Dep.	Bottom El.	Remarks
Driller Iron Mtn.	Length 425' (129.5m)	Location L4518ON5042OE	Level	

INTERVAL From	Fr To m		CORE RECOVERED Wt.	Ft.	%	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	Au PPB	Cu PPM	
0	6	1.83		0		CASING 0-6' IN BROKEN RUBBLE.						
	7	2.13		1	100	6 – Dark Red to Purple lapilli tuff/breccia	14851	6-10'	.2	1	60	
	10.5	3.20		2.8	80	fragments and matrix often show a	14852	10-20'	.1	3	14	
	15	4.57		4.5	100	xtl tuff component core is oxidized,						
	20	6.10		4.7	94	fractures are commonly limonitic (after hematite?)	14853	20-30'	.1	1	22	
	25	7.52		5.0	100	and are 20° to 60° to C.A						
	30	9.15		4.6	92	29-30.3 locally stronger clay/ser alt - core is	14854	30-40'	.1	2	7	
	35	10.67		4.3	86	green/grey coloured.						
	40	12.20		4.8	96		14855	40-50'	.1	2	28	
	45	13.72		5.0	100	43.5-45 qtz stringers 10° to CA with						
	50	15.24		4.9	98	vuggy/corroded & limonite filled cores.	14856	50-60'	.1	1	34	
	54	16.46		↓		core is hard but not obviously silicified.						
	59	17.99		9.4	94	open limonite coated fractures are common.						
	60	18.29		↓		open fractures are commonly sub ∥ to C.A.	14857	60-70'	.1	1	146	
	65	19.82		5.0	100	occasional Pyrolusite coating fractures						
	70	21.34		4.2	84		14858	70-80'	.1	1	43	
	75	22.87	Box 3	4.5	90							
	78	23.78		2.9	97							
	82	25.00		3.9	97		14859	80-90'	.1	1	11	

si — cb — hem — clay ser.

DRILL HOLE EVALUATION SUMMARY

Company: GOLDEN DYNASTY   Property: IRON MTN   Section No. 2   Hole No. I.M. 89-1

Started	Bearing	Lat.	Collar El.	Logged by W.A. HOWELL // ARC
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL From	To		CORE RECOVERED Wt.	Ft.	%	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	Au PPB	Cu PPM	
82	87			4.9	98+							
	90	Box 6		2.9	97		14860	90-100'	.1	1	115	
	95			5.0	100	86 - 99 Rhy Bx Silica & limonitic frags,						
	100			5.0	100	minor jasper on contacts 25-30° to C.A. (upper / lower)	14861	100-110'	.1	1	399	
	105			5.0	100	101 - 103 Rhy Bx similar to above, 100' 1mm qtz 45°c						
	110	Box 7		5.0	100	109-109.7 Red lapilli tuff with local? K-spar	14862	110-120	.1	1	16	
	115			4.9	98	flooding. 115 core is more clay alt, frags						
	120			4.5	90	are distinctive Gouge 113.2, broken clay alt	14863	120-130'	.1	1	28	
	125			4.9	98	to 116, gouge @ 115						
	130	Box 8		4.9	98	120.5: 1-2mm QTZ V.	14864	130-140'	.1	1	8	
	134			3.85	96	129' 2" gouge SEC SOFT CLAY RICH RUSTY						
	139			4.9	98	~~Lithic Tuff~~ AGGLOMERATE, minor 1mm QTZ VEINS 30°/c						
	144			5.0	100	140-155 1-2mm QTZ+Hem V @ 45°/c	14865	140-150	.1	1	14	
	145	Box 9		.67	67%	155-156 Fault zone with gouge						
	149			3.8	95%	156-163 Weakly Oxidized						
	153			2.5	62	164- 6" gouge	14866	150-160'	.1	1	172	
	154	Sort Core		0	0	160' - 1" QTZ V. 45°/c						
	159			4	80							
	164			4.9	98		14867	160-170'	.1	1	6	

Box 10

DRILL HOLE EVALUATION SUMMARY

Company .... Property IRON MTN. .... Section No. 3 Hole No. IM 89-1

Started		Bearing		Lat.		Collar El.		Logged by	PKC
Completed		Angle		Dep.		Bottom El.		Remarks	
Driller		Length		Location		Level			

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM	
	170		5.9	98+	Rusty alt. agg. or lapilli tuff	14868	170-180'	.1	1	7	
	175		4.9	98	178-178.5 Gouge Zone						
	179		4.0	100	187': 1" QTZ VEIN.						
	184		5.0	100	190-210's Med-XTAL-LITHIC tuff	14869	180-190'	.2	2	6	
	189	BOX 11	4.9	98							
	190		1.0	100		14870	190-200'	.2	1	6	
	196		5.0	100							
	200	BOX 12 204'	5.0	100		14871	200-210'	.1	1	5	
	205		4.9+	99							
	210		4.9+	99	210': 6" Fng tuffaceous mudstone @45°/c	14872	210-220'	.1	3	7	
	215		4.9	98	209': 1mm Qtz VEIN. w.HEM.						
	219		3.9+	98	220': 2mm ✓ ✓ w.HEM	14873	220-230'	.1	1	14	
	224	Box 13	4.9	98	224'-230': QTZ HEM VEINING & STOCKWORK						
	229		4.9	98	FR + VEINING @ ≈45°/c	14874	230'-240'	.1	1	12	
	234		4.9	98	230-240': Reduced Veining						
	239	Box 14	5.0	100	240-245.5': Healed Bx	14875	240-250'	.1	2	33	
	240		1.0	100	245.5-247: JASPER						
	245		4.9	98	249': 4" gouge						
	250		4.9	9.8	247-251': CATACLASTIC BX, HEALED.	14876	250-260'	.1	4	46	

DRILL HOLE EVALUATION SUMMARY

Company .... Property .... Section No. 4 Hole No. IM 89-1

Started	Bearing	Lat.	Collar El.	Logged by PAC
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM	
		253	2.7	88	251-255: JASPER 255-256: Hem. Bx.						
	257' Box 15	258	4.9	98	256-256.5: Frg. mudstone						
		260	1.7	85	256.5-258: Green Tuff 258.5 & 260: 2" gouge	14877	260-270'	.1	1	22	
		265	4.9	98	258-261: Br Weathered (Rusty) contacts @ 30-45°/c						
		267	1.9	98	263-264: Red Bx Tuff 264-278 JASPER						
		268	1.[illegible]	85	266-266.5: 6" Green Bx Tuff.						
		269	0.8	40%	278-280. Rusty Brecciated Jasper	14878	270-280	.2	1	16	
	274 Box 16	273	2.5	63	280-282.5: Jasper 289: 1/4" Qtz. V. Rusty						
		277	3.9	97	282.5 — 292 Breccia [illegible]						
		280	2.9	97	angular frag. → 3" some Jasper	14879	280-290	.4	2	21	
		285	4.9	98	frag. 293-298: 1% Py frag.						
	Box 17	290	4.8	96	292.5-293.0" Contact zone talc in fault? @ 45°/c	14880	290-300'	2.1	8	88	
		295	5.0	100							
		300	4.9	98	293.0-298: Rhy & Jasper frag → 6" in dacitic matrix	14881	300-310'	.2	1	28	
		305	4.8	96	298-300 Fault Zone @ 45°/c						
	308 Box 18	310	4.5	90	300-306 Rhy [illegible]	14882	310-320'	.2	1	54	
		315	4.8	96	306-316.5 Dacitic matrix Agglomerate 20°/c 316.5						
		320	4.5	90	312-315 mainly gouge. 319 TR Cpy 3% min Py	14883	320-330'	.1	1	11	
		325	4.8	96	325-335 Clay altered dacite or Rhy Tuff.						

327- Box 19

335 - 339 Mixed Rhy & dacite Tuff Bx.

DRILL HOLE EVALUATION SUMMARY

Company .... Property .... Section No. .... Hole No. IM 89-1

Started	Bearing	Lat.	Collar El.	Logged by PAC
Completed May 18/89	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY		
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM
	330		4.8	96	330-330.5; 335-340; 343-344; 345-345.5 Rhy	14884#	330-340'	.1	1	8
	335		4.9	98	345.5-348.5; Green Clay + Ser Alt Rhy Bx					
	340	344 Box 22	4.9+	98+	344-345; 348-365; Intense Hem (Limonite) Stockworks	14885#	340-350'	.2	18	161
	345		4.9	98	in mixed dacite + Rhyolitic Breccia 350-351: CPY + minor mol. <1%					
	350		4.9+	99		14886#	350-360'	.3	117	734
	355 / 360	361 Box 23	4.97 / 4.9+	98 / 98		14887#	360-370'	.4	5	132
	365		4.9+	98	360' 1cm gouge 10-15°/c					
	370	1' washed	2.5	50%	366-370' Broken + Gouge w. 1' washed	14888#	370'-380'	8.6	4	1584
	374		1.5	32%	370-375 Broken					
	378		3.6	90%	378-379 Broken - sand Recovered 50% rec	14889#	380-390'	2.8	5	314
	383	Box 22 382	5.0	100%	379'-382' Dis. Py. Cubes ≈1mm Hem + Cpy Blebs					
	388		5.0	100%	381' 1/4" Hem @45°/c w minor Cpy	14890#	390-400'	.1	1	14
	393		5.0	100%	Clear glassy Qtz + Milky Qtz.					
	396		3.0	100%	383-384': Cpy + Hem 20-30°/c ends @ Shear					
	400		1.8	44%	386.5-387: 40% Qtz + Spec. Hem Veinlets.	14891#	400-410'	.1	2	9
	405	Box 23	5	100%	379-425: Rhy & Rhy Bx (End)					
	410		4	80%	400' 1/4" Qtz Hem V. 15°/c	14892#	410-425'	.1	1	20
	415		3.5	75%	394'-395' 1/4-1/2" Qtz + Hem @ 10°/c					
	420		6"	5%	409-425 Broken Rusty.					
	425 END		1	20%						

DRILL HOLE EVALUATION SUMMARY

Company GOLDEN DYNASTY Property IRON MTN Section No. 1 Hole No. IM 89-2

Started MAY 19/89	Bearing VERTICAL	Lat.	Collar El. 1653m.	Logged by P.A.C.
Completed	Angle -90°	Dep.	Bottom El.	Remarks
Driller IRON MTN.	Length 488' (148.7m)	Location L50+15N 49+85E	Level	

INTERVAL From	To	CORE RECOVERED Wt.	Ft.	%	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	Au PPB	Cu PPM	
	14	Box 1	3	21	Casing to 15 ft.						
	15		6"	50%	Andesitic to Dacitic lapilli tuff 15-17' several FR @ 15-35°/c						
	17		2.0	100	Calcite stringers, [illegible] veinlets 2-3% ex.						
	20		2.9	96	27' contact @ 25°/c.						
	23		2.7	90	30-31' 1% dis Py						
	28	Box 2	5	100							
	30		1.9	38							
	35		5	100							
	40	Box 3	5	100	42': 1" gouge @ 45°/c 46': 1" gouge @ 45°/c						
	45		5	100	51': 6" gouge @ 30°/c						
	50		4.25	85	52-54' gouge and fault Bx	14893	50-60'	.4	1	128	
	55		3.5	70	41' → 1% Py						
	60	Box 4	4	80	53 — Rhyolitic lithic tuff						
	69		4	100	59-60: Clay altered fault Bx						
	74.5		5	95	73-74: Dacitic lapilli Tuff						
	79.5	Box 5	5	100	70.5-71: Clay alted Rhy						
	84.5		4.9	98	79.5 - 3" Broken Rusty.						
	90		5.4	98	82: 2mm Py @ 45°/c						
	95	Box	5	100	80-95: FR @ 20-45/c weak						

DRILL HOLE EVALUATION SUMMARY

Company .... Property .... Section No. 2 Hole No. IH89-2

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM	
	100		4.8	96	106-107; 100-102: Dacitic Lapilli Tuff.						
	105		4.9	98	109-110: Rusty FR @ 80°/c.						
	110	Box 7	4.7	94							
	115		5	100							
	120		4.8	98%	120': QTZ-CARB 2mm @ 45°/c	#14894	120-130'	.1	1	14	
	125		4.9	98%							
	128	Box 8	2.5	83%	126-128': Broken & Rusty						
	130		1.8	90%	132-137: Dacitic lapilli Tuff. frag CONTACTS.						
	135		4.9	98%	140-142 Broken minor gouge; SHEAR @ 20°/c 142'						
	139		3.9	98%	145-151': Softer Rhy. (dacitic?) lithic tuff.						
	144		4.8	96%	6" Broken with minor gouge @ 151'						
	149	Box 9	4.9	98%							
	154		4.7	94%							
	159		4.9	98%	158: ½" qtz lined vugs						
	164	Box 10	3.5	70%	159: Serp. on shear @ 20°/c						
	168		4.0	100%	159-163 Broken & sheared w minor gouge						
	170		2.0	100%	164-175: 5-7% qtz & carbonate veinlets.						
	175		4.9	98%	170-175: Layered Rhy. bed @ 20-30°/c						
	180	Box 11	4.8	96%		14895	170-180'	.1	1	9	

DRILL HOLE EVALUATION SUMMARY

Company .... Property .... Section No. 3 Hole No. IM89-2

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%							
	183	Box 11	2.9	96	Rhy + Rhy lithic Tuff cont.						
	183.6		.25	50	2-3% qtz-carb veining						
	186		2.9	96%							
	188		1.8	90%	188: 1/4" qtz.-calc. 187-188: Broken						
	193		4.9	98%							
	198	Box 12	5	100%							
	203		5	100%	201-202: 5-7% qtz-carb veinlets @ 45°/c						
	204		.95	95%							
	208		3.9	97%	208 - 2" SHEARING @ 45°/c clay alt						
	212		3.5	73.5%	213.5-218.5: Broken Core minor gouge.						
	215	Box 13	1	33.3%	Rhy. Reddish → white matrix @ 240'						
	218		2	66.6%	Layered from 240 ave 30°/c						
	222		3.5	82%							
	227		4.6	92%							
	230		3	100%							
	233	Box 14	2.6	87%							
	236		3+	100%							
	240		4	100%							
	244		3.9	97%							

DRILL HOLE EVALUATION SUMMARY

Company .... Property .... Section No. 4 Hole No. IM 89-2

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM	
	Box 15/248' 248.5		4.4	97%							
	253		4.5	100%							
	258		4.8	96%	257-258.5: Broken with mod. gouge 30% carb						
	263		4	80%	fm 259-259.6. 259.6-261: Gouge, Broken fault.						
	267	Box 16, 265.5'	3.9	75%	263-266; Broken, moderate gouge 267-274; ✓ ✓ ✓						
	270		2.5	82%	275.5-276.5; ✓ ✓ ✓ 278.5-295; ✓ heavy ✓						
	271		.3	30%	276-281: 5% Carb + QTZ carb veinlets @ 80-90°/c.a.						
	272		.5	50%							
	274		1.6	80%							
	276		4.6	92%							
	280	Box 17	4.8	96		#14896	280-295	.1	1	4	
	294		3	2							
	297		2.1	70%							
	302		4.8	96%	300-312: 5-7% carb + qtz + carb veinlets clay altered (dacite?)						
	307	Box 18	5	100%	304-305: Hem alter of matrix	#14897	300-310'	.2	1	23	
	312		4.7	94%	308-309: 6" broken + gouge						
	317		5	100%	320-322; 324-328: Strong Fault.						
	322		3.0	60%	minor Py.	#14898	320-330'	.6	3	16	
	325.5		2.0	58%							

DRILL HOLE EVALUATION SUMMARY

Company .... Property .... Section No. 5 Hole No. IM 89-2

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM	
	330'	Box 19	2	44%	330'-370', 2(-7)% Py FR + Vein + matrix frags						
	335		5	100%	370'-389', 1-3% Py mainly FR + Vein						
	340		4.9	98%	346.5-351 Broken w moderate gouge.	#14899	340-350'	.2	2	8	
	345	Box 20	5	100%	353.5-354.5. Broken w minor gouge.						
	350		3.8	76%	348': 2mm spec. hem qtz veinlet 70°/c						
	352.5		2	80%							
	354.5		1.5	75%							
	359.5	Box 21	4.8	96%							
	364.5		4.9	98	366-368: Broken w. moderate clay						
	367		2.0	80	shear @ 45°/c						
	370		[illegible]	83	374': 2 x 1/4" Qtz veins @ 45°/c.	#14900	370-380'	.5	1	40	
	372		1.5	75%	388': 2" gouge.						
	377	Box 22	4.8	96%	382': layering @ 55°/c						
	380		2.1	70%	390': ✓ @ 20°/c						
	382.5		2.2	88%							
	386		3.0	89%							
	389		2.8	92%							
	394	Box 23	4.5	90%							
	397		2	66%	395.5-397: Broken strong gouge; 394 broken						

DRILL HOLE EVALUATION SUMMARY

Company | Property | Section No. 6 | Hole No. IM 89-2

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM	
	400		2.8	93%	400-426! Strongly broken & gouge.	#14901	400'-410'	.2	1	19	
	403		1	33							
	406.5		1.0	40%							
	409		1	40							
	411		1.5	75%		#14902	410-420'	1.6	1	24	
	413	BOX 24	1.9	95%							
	415.6		2.0	80%							
	417		.8	55%							
	419		1	50%							
	421.5		1.25	50%		#14903	420-430.5	.7	1	11	
	426		3.5	77%							
	430		3.1	78%							
	435	BOX 25	4.8	96%	432 - 1" QTZ-CARB @ 30°/c						
	440		4.6	92%	Variable layering of Rhy.						
	445		5	100%	449' - 6" broken w. mod. clay gouge.						
	450	BOX 2[illegible]	4	80%	438-440 FR. Py 3-5%	#14904	450-461	.1	1	15	
	454		2	50%	450-453.6 Broken with [illegible] gouge.						
	456.5		2.1	96%							
	461.		4.4	91%							

DRILL HOLE EVALUATION SUMMARY

Company .... Property .... Section No. 7 Hole No. IM89-2

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu PPM	
	465.6		.8	18%	MIS. LATCH						
471.5	470.0	BOX 27	2.2	48%	465.5-469 Broken and Gouge						
	472.0		1.8	90%	470- END (488') Broken moderate gouge						
	473.0		.6	60%							
	475.0		1.8	90%		#14905	475-488'	.1	1	6	
	478.5		2.2	63%							
	481.0		1.5	60%							
	482.6		.8	54%							
	486.6		1	25%							
	488		.5	33%							

DRILL HOLE EVALUATION SUMMARY

Company Golden Dynasty Res. Ltd. Property Iron Mtn. Section No. 1 Hole No. IM 89-3

Started May 21/89	Bearing 290°	Lat. L51N Δ 5010E	Collar El. 1642m	Logged by PAC	
Completed May 22/89	Angle -45°	Dep.	Bottom El.	Remarks	
Driller Iron Mtn. Drilling	Length 188 Ft. (57.3m)	Location GRID 2 (main)	Level		

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu PPM	
	10		2	20	19 Ft Casing FIRST SOLID CORE @31'	#14906	10-30'	0.1	1	10	
	15		2.5	50	Rhyodacite lithic tuff dark grey & hard						
	20		2.5	50	generally fing matrix same rhyolite sections						
	22/6		1	40	39-43': Rusty fracture surfaces						
	24		.7	48	39-41': Broken with minor gouge						
34½	35	Box 2	6	58	Fragments generally fing.						
	39		3.8	95%							
	40		.8	80%							
	44		3.9	97%							
	48/6	Box 3	4.4	98%							
	52		3.4	97%							
	57		4.6	92%	54-66': Broken minor gouge						
	60		2.2	73%							
	61		0.6	60%							
	63		1	50%							
	66		2	66%							
	70		3.9	97%	71': layering 30°/c						
	73		2.9	96%	76-85': broken 82-85 Rusty 2-3% Py						
	76		2.8	93%							

DRILL HOLE EVALUATION SUMMARY

Company *Golden Dynasty Res. Ltd.* Property *Iron Mtn.* Section No. *2* Hole No. *IM89-3*

Started	Bearing	Lat.	Collar El.	Logged by *PAC*
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu PPM	
	80	BOX 5	2.5	62	77': 1" QTZ-PY breccia vein 90°/c	#14907	80-90'	0.8	1	19	
	84		3	75							
	88		3.5	87	86': 1" QTZ-CARB-PY.						
	89		.5	50							
	91		1	50							
	94		2.5	83							
	98	BOX 6	39	96							
	101		2.8	93	100-101: Broken 101/6-102 broken and gouge						
	105/6		3.8	84%	104-105: Broken						
	108/6		2.8	93	102: minor gouge 8" broken						
	110		1	66	111: 1" QTZ-CARB @ 20°/c	#14908	110-120'	0.2	3	18	
	113		2.6	86%	111-146: Broken						
	114	BOX 7	.88	88							
	116		1.7	85%							
	120		3.5	87%							
	122		.7	35%							
	125/6		2.5	71%							
	127'		1.3	83%							
	128'		.7	70%							

DRILL HOLE EVALUATION SUMMARY

Company | Property | Section No. 3 | Hole No. IM89-3

Started	Bearing	Lat.	Collar El.	Logged by RAC
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%							
	130	Box 8	1.1	55	126-135: Broken minor gouge. Rusty.						
	131/6		1.4	94%	139-146½: ✓ ✓ ✓ .						
	133		1.0	66							
	135		1.2	60%	143: Start of main Rhyolite						
	137/6		1.5	60%							
	140		2.1	84%	145-146/6: Rusty Broken minor gouge.						
	141		.8	80%	148-150/6: Gouge and broken (Fault)						
	142		.5	50	150-153: Broken.						
	143	Box 9	.5	50%	157-163: Strongly Broken with mod. gouge						
	146/6		3.3	95%	164-179: White Rhy						
	150		2	58%	3mm QTZ-CARB-PY veinlet 10° @ 171'						
	154		3.9	97%	165-170: Broken mod. gouge						
	157/6		3.4	97%							
	160		.3	13%							
	163	Box 10	2	66%	173/6-175/6: Broken w. gouge (mod						
	167		2.5	63%							
	170		2.0	66%							
	175		4.9	98%	SPEC @ 177'						
	180	Box 11	4.9	98%							

DRILL HOLE EVALUATION SUMMARY

Company *Golden Dynasty Res. Ltd.* Property *Iron Mtn.* Section No. *4* Hole No. *IM89-3*

Started	Bearing	Lat.	Collar El.	Logged by *PAC*
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%							
	183		3	100%	179-188 END QTZ-CARB VEINLETS @ 60-70°/c						
	188		46	92%	SPEC @ 181						
	END										

DRILL HOLE EVALUATION SUMMARY

Company Golden Dynasty Res. Ltd. Property Iron Mtn. (Charmer Zone) Section No. 1 Hole No. IM 89-4

Started May 22/89	Bearing 42°	Lat.	Collar El. 1565 m.	Logged by PAC
Completed May 24/89	Angle -45°	Dep.	Bottom El.	Remarks
Driller IRON MTN.	Length 394'	Location L8+40N 0+65W	Level	

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu PPM	
	6		.8	13	to 24.5 AND or Dacite: black fragmental	#14909	0-17.5'	.1	3	23	
	7		.8	80	strongly magnetic (10%), Vesicular 19-22						
	10		2.5	83	24.5-25.0: Vesicular And? Rusty						
	11		.6	60	25- weakly mag agglomerate/lapilli tuff.						
	12		.5	50	31-31/6: several 1mm qtz-limonite						
	13		.3	30	veinlets @ 45%c						
	15.5		1	40	36/6-38: Rubble + Broken						
	16		.33	33	41: gouge.						
	16.5		.5	50		#14910	17.5-24.5	.1	1	37	
	17.5		.5	50							
	19.	BOX2	1.4	93							
	23		2.5	68							
	24.5		.5	33		#14911	24.5-40'	.1	3	56	
	29.5		3.7	75%							
	30.5		.9	90							
	35		3.5	78%							
	36.5	BOX3	.7	47%							
	40		2.4	69%		#14912	40-50'	.1	1	79	
	45		4.8	96%							

DRILL HOLE EVALUATION SUMMARY

Company *Golden Dynasty Res. Ltd.* Property *Iron Mtn.* Section No. *2* Hole No. *IM89-4*

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu PPM	
	50'		4.8	96		#14913	50-60'	.1	2	76	
	55'	BOX 4			50-52: Broken mod. gouge						
	60'		3.2	64	50-68: Rusty with stockworks (limonitic)	#14914	60-70'	.1	1	182	
	65'		3.5	70	55-56: Broken & Gouge						
	70'		4.7	94	59-62: ✓ ✓	#14915	70-80'	.2	2	75	
~~75'~~	71'	Box 5	.95	95	3"@71': ✓ ✓						
	76'		4.9	98							
	80'		3.5	88	84-88: Course lithic tuff breccia w						
	82		1.8	90	Chl alt fragments. also 71-72; 75-75/6						
	87		4.8	96	73': 1/4" QTZ-CARB-LIMONITE @45°/c						
	90		2.9	96	79': ✓ ✓ – –						
~~91'~~	95	Box 6	4.9	98	76-80': several 1mm veinlets @ 45-80°/c						
	100		4.9	98	89/6-90: 2 1mm qtz v. 80-90°/c	#14916	94-108'	.1	5	71	
104/6	105	Box 7	4.8	96	90/6-94: Rhy(?) [Spec 93']						
	110'		4.7	94	95-101: Angular cherty breccia	#14917	108-120'	.2	13	692	
	115'		4.9	98	101-109: Chl frag Bx (soft.)						
	120'		5.0	100	109: 3/4" hem veinlet with mal. stain						
~~125'~~	125'	BOX 8	4.8	96	30°/c						
	130'		4.9	98	109-110/6: Rusty Broken. 111-118: frag Arg. fr. with hem	#14918	130-140'	.9	65	1969	

110: PY-CPY QTZ Veinlet @80°/c 2mm

SPEC 130'

DRILL HOLE EVALUATION SUMMARY

Company: Golden Dynasty Res. Ltd. Property: IRON MTN. Section No. 3 Hole No. IM89-4

Started	Bearing	Lat.	Collar El.	Logged by PAC
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu PPM	
	135'		4.8	96	SPEC 134/6 - 134-135/6 20% spec hem @45°						
	139'		3.2	80%	138-140+: Broken with mod gouge.						
	144		4	80%	134-138; 140-144/6: Breccia chl. frag.	#14919	140-150'	.3	23	513	
	149		4.6	92%	Broken & Gouge 147/6-149						
	153		3	75%	147-147/6: 50% qtz vein.	#14920	150-160'	.6	2	568	
159	157/6	BOX10	3.5	78%	147-160: Broken moderate gouge.						
	160		1.5	60%	156-188: Lithic Tuff Breccia	#14921	160-170'	.5	2	277	
	163		2.5	83%	162-163: Broken with mod gouge						
	166/6		2.2	63%	164-165: ✓ ✓ ✓ ✓						
	170		3.0	86%	FAULT 169-172/6: Strong Broken & gouge (Very strong @170)	#14922	170-180'	.1	1	236	
	172/6		.8	32%	175-176/6: Broken.						
177'	176	BOX11	2.9	83%							
	180		3.3	83%		#14923	180-190'	.3	5	787	
	183		.8	27%							
	186		2	66%	190-194: Mal, cpy, hem assoc with qtz veinlets						
194'	190	BOX12	3	75%	194-195 Gouge & Broken. SPEC 190/6-192	#14924	190-195'	23.2	760	4700	
	195		4.6	92%		#14925	195-205'	.6	8	132	
	200		4.7	94%							
	205		5.0	100%		#14926	205-215'	.7	4	139	

DRILL HOLE EVALUATION SUMMARY

Company Golden Dynasty Res. Ltd. Property Iron Mtn. Section No. 4 Hole No. IM 89-4

Started	Bearing	Lat.	Collar El.	Logged by PAC
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu PPM	
	210		4.8	96	strong carb. alt. from 190'-227'						
212'	212	Box 13	1	50	210-212 + 213-215 Broken minor clay also @ 218; 219; 226-227						
	215		1.5	50	207': ½" qtz-carb-limonite 30%c	#14927	215-225	.2	6	182	
	219		3.5	89	215': 2" qtz-carbonate-limonite 45°/c						
	223		3.5	89	226-227: Broken mod-strong gouge						
	227		3.5	89	227-232: Fng Basaltic or And. dyke (?)						
230/6	230	Box 14	2.3	76%	Coarse lithic tuff						
	234		3.8	95%	Carb. alt. 239-246 → carb-qtz veinlets						
	236		.5	25%							
	239		2.9	97%		#14928	239-254'	.1	2	77	
	244		4.9	98%	245': ¾" qtz-carb.v. @ 45°/c centred in (py-cpy-bn minor)						
248/6	249	Box 15	4.8	96%	6" bleached zone. 248': 2×¼" + ⅛" qtz-carb v @						
	254		4.9	98%	45°/c. 244-249: 1-2% Py, lim-	#14929	254'-267'	.1	1	41	
	257/6		3.0	86%	243: minor mal, mag, 257/6-258/6 mag weak altered						
	262/6	Box 16	5.0	100%	259-262: Carb altered several ⅛-¼" qtz carb						
	267		3.4	98%	@ 45°/c. 261': ¼" qtz-carb @ 45°/c. 265': 1" qtz carb/60°/c.						
	272				263-267: several Qtz-carb veinlets to 1¼" (@ 265)						
	277		3.9	97	@ ≈ 45°/c. some stockwork veining 254-255; 259-267: carb-qtz veining ≈ @ 45°/c.						
282/6	282	Box 17	4.9	98%	382: ¼-½" Qtz-carb @ 15°/c						
					269-271: weakly carb. altered + 281/6-283						

DRILL HOLE EVALUATION SUMMARY

Company *Golden Dynasty Res. Ltd.* Property Section No. 5 Hole No. IM 89-4

Started	Bearing	Lat.	Collar El.	Logged by
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

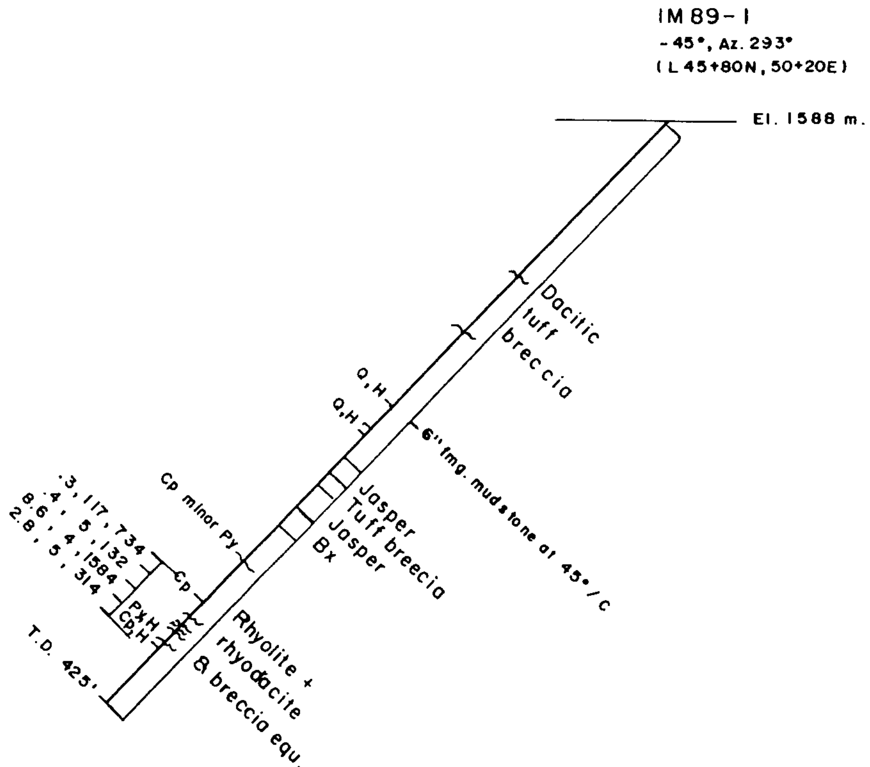
INTERVAL		CORE RECOVERED			DESCRIPTION	Sample No.	Interval	ASSAY			
From	To	Wt.	Ft.	%				Ag PPM	Au PPB	Cu PPM	
	287		4.7	94							
	292		4.8	96	293: Jasper Layers & Frag. appear.						
	296		3.8	95	296-297: Diorite Dyke. 297-299: Layering						
	300	Box 18	3.7	93	folded 300: minor py						
	305		5	100%	317 — 395 Rhyolitic lithic Tuff.						
	310		5	100%	320-341 Carbonate altered & veined						
317/6	315	Box 19	4.8	98%	333' 1" qtz: carb @ 20°/c						
	320		4.8	96%	336'-338': 15% qtz carb veinlets to 1".	#14930	320-330'	.1	1	13	
	324		4.5	90%	330-338: strong carb alt & 340-341':						
333	329	Box 20	4.8	96%	331-332: strong broken & gouge						
	334		4.7	94%	336- Broken & gouge.	#14931	330-341'	.4	4	192	
	339		4.9	98%	343-345: Qtz & 3-5% min.						
	344		4.9	98%	355-358/6 strong fault with talc & sip						
	349/6	Box 21	5	91%	362-363 mod gouge & broken						
	353'		3.3								
	357		3.1								
	358		.8	80%							
366'	363	Box 22	4.8	96%							
	368'		4.9	98%							

DRILL HOLE EVALUATION SUMMARY

Company *Golden Dynasty Res Ltd.* Property *IRON MTN.* Section No. *6* Hole No. *IM 87-4*

Started	Bearing	Lat.	Collar El.	Logged by *PAC*
Completed	Angle	Dep.	Bottom El.	Remarks
Driller	Length	Location	Level	

INTERVAL From	INTERVAL To	CORE RECOVERED Wt.	CORE RECOVERED Ft.	CORE RECOVERED %	DESCRIPTION	Sample No.	Interval	ASSAY Ag PPM	ASSAY Au PPB	ASSAY Cu. PPM	
	373'		4.9	98%	377': 6" gouge						
	378'		4.9	98%	385': 3/4" qtz vein. 45°/c						
383'	383'	Box 23	5	100%							
	388'		4.8	96%	389': 1" qtz v. @ 45°/c.						
	393'		4.7	94%							
	394'		1	100%	1-2% Py. 390-394':	#14932	388-394'	.1	1	15	
	END'										



LEGEND

~~	Fault or shear
Q	Quartz vein
H	Hematite
Cp	Chalcopyrite
Py	Pyrite
M	Malachite
Cb	Carbonate
Bx	Breccia
Ch	Chlorite
.3, 23, 513	Ag ppm, Au ppb, Cu ppm.

GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

DRILL HOLE SECTION IM 89 - 1

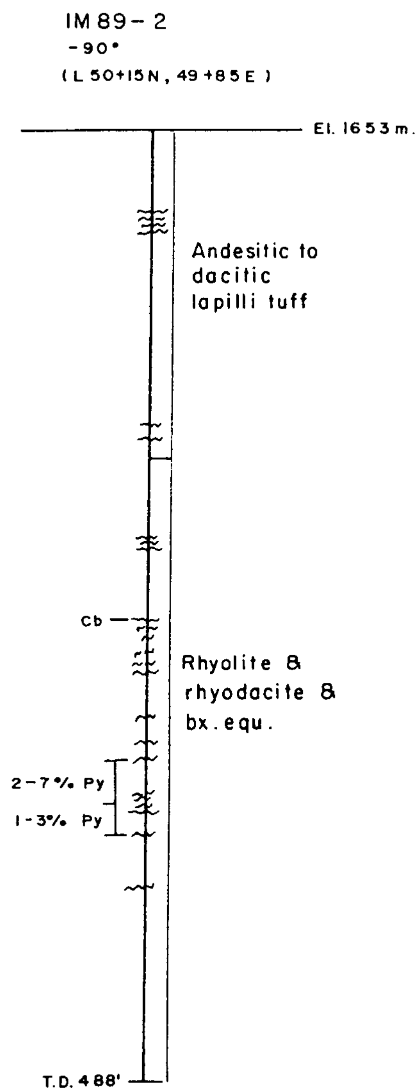
N.T.S. 92I-2 NICOLA M.D., B.C.

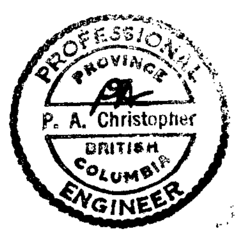
0 20 40 30 METRES

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE 1:1200	JUNE 1989	FIGURE 11a

CHONG





LEGEND

~~	Fault or shear
Q	Quartz vein
H	Hematite
Cp	Chalcopyrite
Py	Pyrite
M	Malachite
Cb	Carbonate
Bx	Breccia
Ch	Chlorite
.3, 23, 513	Ag ppm, Au ppb, Cu ppm.

GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

DRILL HOLE SECTION IM 89 - 2

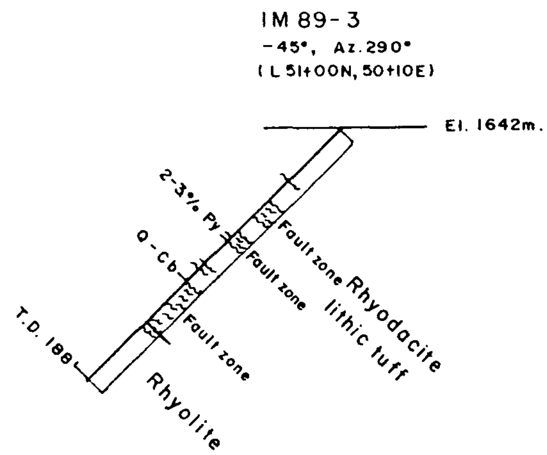
N.T.S. 92I-2 NICOLA M.D., B.C.

0 20 40 30 METRES

P.A CHRISTOPHER & ASSOCIATES INC.

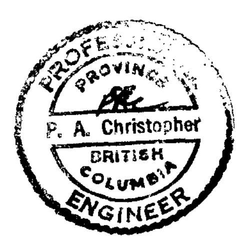
SCALE 1:1200	JUNE 1989	FIGURE 11 b

CHONG



LEGEND

~~	Fault or shear
Q	Quartz vein
H	Hematite
Cp	Chalcopyrite
Py	Pyrite
M	Malachite
Cb	Carbonate
Bx	Breccia
Ch	Chlorite
.3, 23, 513	Ag ppm, Au ppb, Cu ppm.



GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

DRILL HOLE SECTION IM 89 - 3

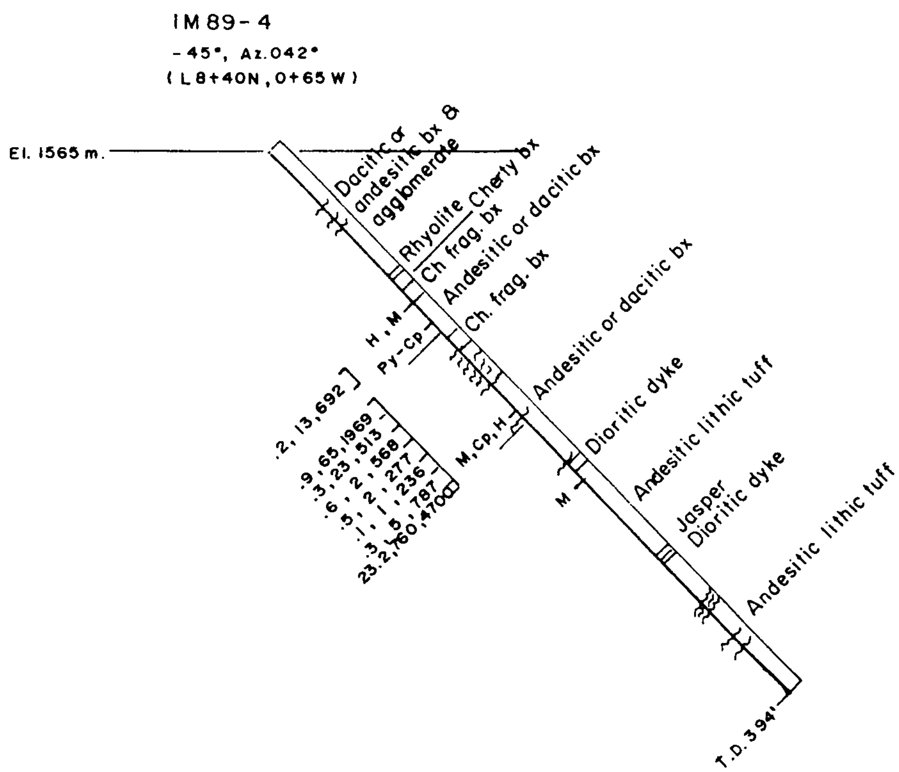
N.T.S. 92I-2 NICOLA M.D., B.C.

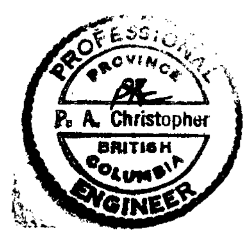
0 20 40 30 METRES

P.A. CHRISTOPHER & ASSOCIATES INC.

SCALE 1:1200	JUNE 1989	FIGURE 11c

CHONG





LEGEND

~~	Fault or shear
Q	Quartz vein
H	Hematite
Cp	Chalcopyrite
Py	Pyrite
M	Malachite
Cb	Carbonate
Bx	Breccia
Ch	Chlorite
.3, 23, 513	Ag ppm, Au ppb, Cu ppm.

GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

DRILL HOLE SECTION IM 89 - 4

N.T.S. 92I-2 NICOLA M.D., B.C.

0 20 40 30 METRES

P.A CHRISTOPHER & ASSOCIATES INC.

SCALE 1:1200	JUNE 1989	FIGURE 11d

CHONG

Appendix D. Cost Statement

Field Personnel			
Peter A. Christopher P.Eng. Consulting Geologist May 2-3;11-12;14-26/89 17 days @ $400ea		$ 6800	
W.A. Howell B.Sc. (Geologist) 5 days @ $350ea August 6, 7/87		1750	
Gerry Hayne B.Sc Geophysical Operator May 11-20;23-26/89 14 days @ $ 175 ea.		2450	
Randy Smallwood Prospector May 11-26/89 16 days @ $ 150 ea.		2400	
Mob.-Demob.		2000	
			$ 15,400.00
Room & Board 52 man days @ $50/day			2,600.00
Transportation			
Vehicle Datsun 4x4s 34 days @ $60/day			2,040.00
Mileage 4550 km @ 0.15ea.			682.50
Fuel			318.44
Coquihalla Tolls			120.00
Ferry			54.00
Rentals			
Magnetometer & VLF-Em 17 days @ $50ea			850.00
Saw Rentals 2 for 16 days ea. @ $25/day			400.00
Core Splitter			50.00
Expendable & Disbursements			
Diamond Drilling			25,415.00
Cat Use 22 hrs. @ $75ea.			1,650.00
Geochemical Analyses Inv 89-1394			6,973.05
Phone			125.05
Maps	$ 9.54		
Pickets	16.94		
HCl	4.76		
Batteries + Hand Lotion	23.76		
Grease	2.50		
Wire	8.88		
Spray paint, nails	8.46		
Hardware For Splitter	29.20		
Film and Developing	34.17		
Topo chain 10 @ $4.00ea.	40.00		
Drafting paper & pad	15.00		
500 soil bags @ .20ea	100.00		
100 rock bags @ .24ea	24.00		
5 boxes flagging 16.50ea	82.50		
1 package tags	13.25		
4 field books @ 3.05ea	12.20		
6 marking pens @ 1.50ea	9.00		
2 maps	9.54		
2 cycle and chain oil	3.00		
			446.70
		sub-total	$57,124.74

Cost Statement Continued:

sub-total Page 1: $57,124.74

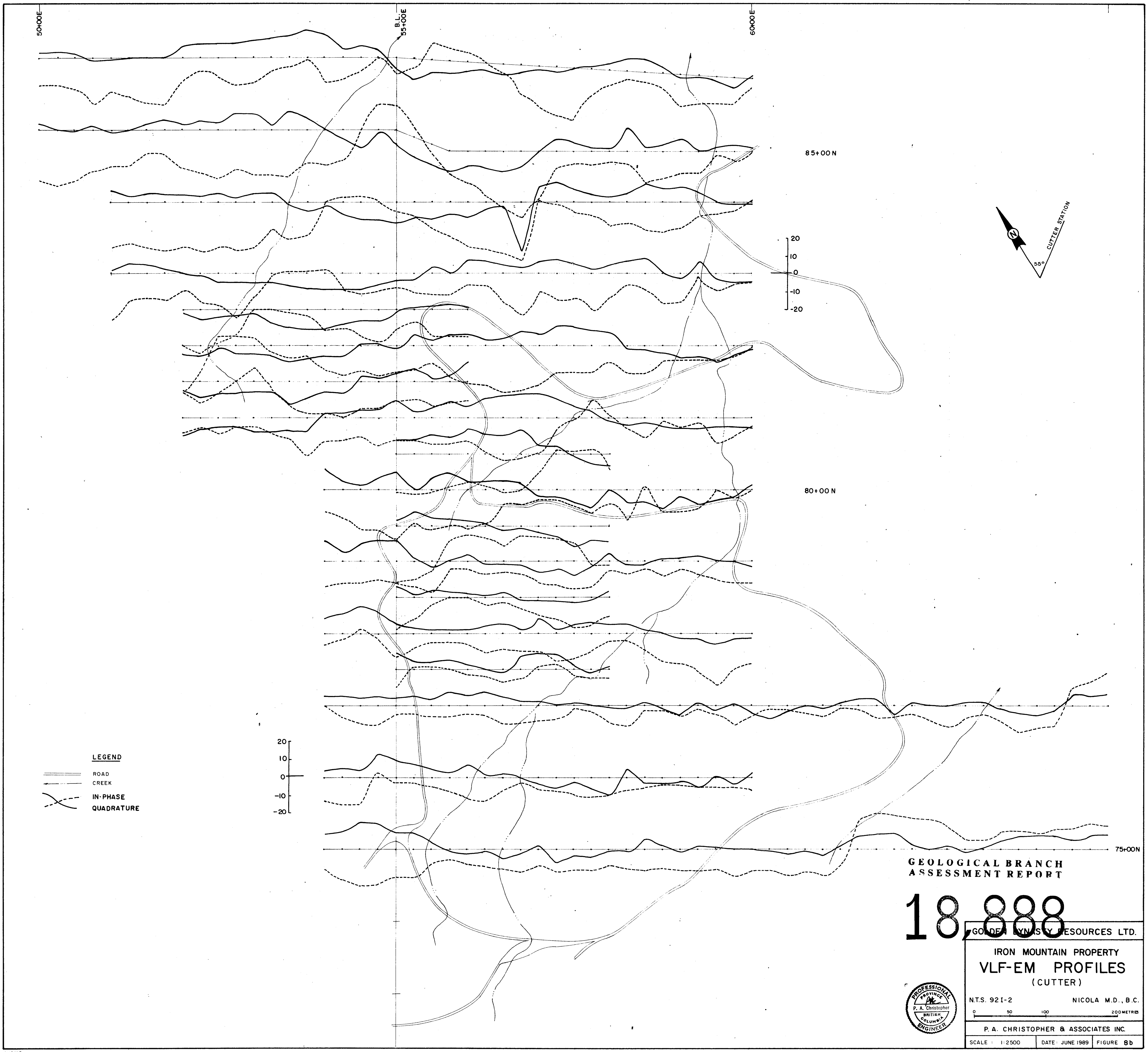
REPORTING COSTS

Drafting 50 hours at $17/hr.	850.00
Word Processing	200.00
Copies, Binding, Office Supplies & Assistance	300.00
Report Preparation and Consulting	4,650.00
Total Cost	$ 63,124.74

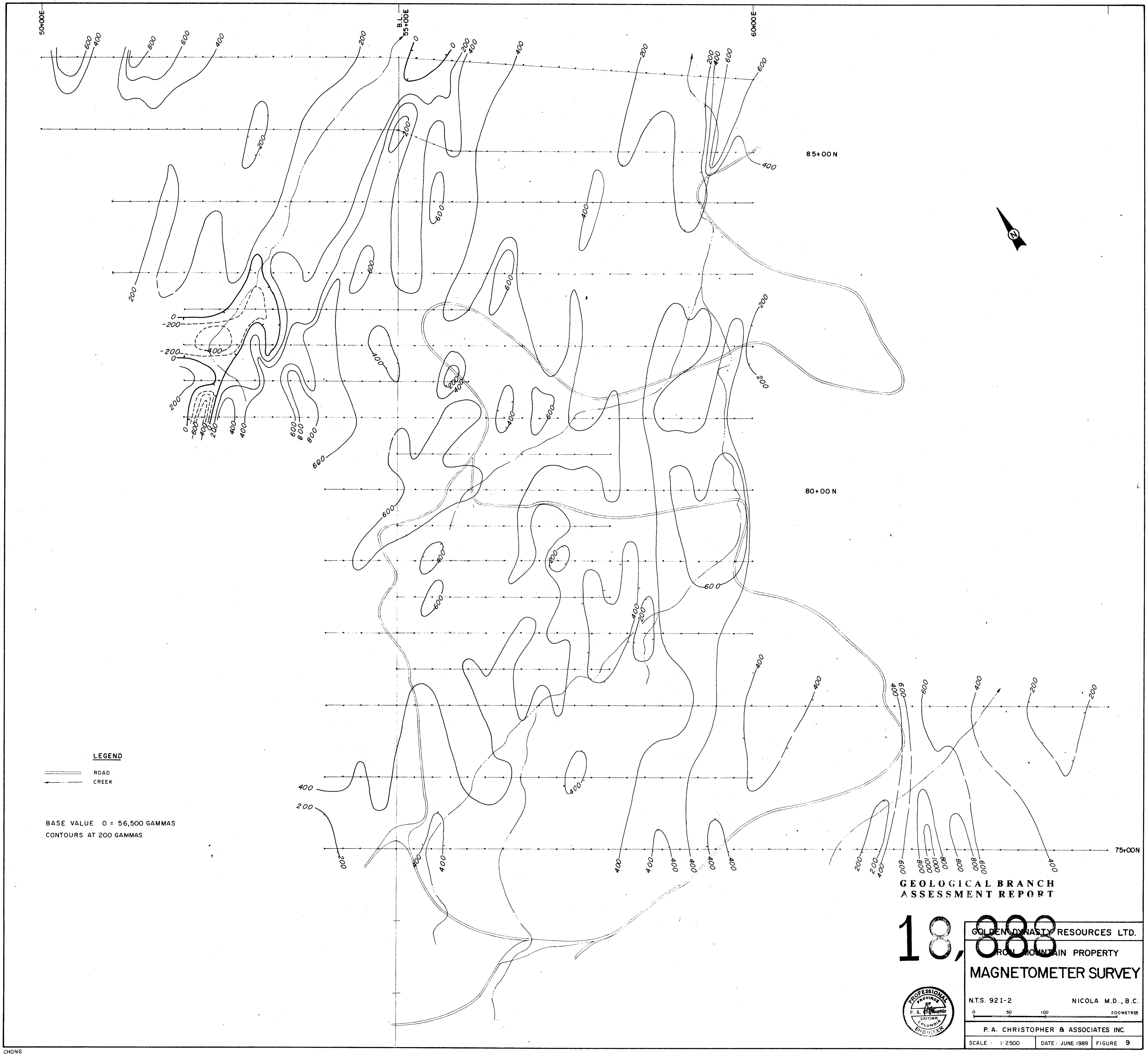
Peter A. Christopher

PROFESSIONAL ENGINEER PROVINCE OF BRITISH COLUMBIA P. A. Christopher

Peter A. Christopher, P. Eng.
July 4, 1989

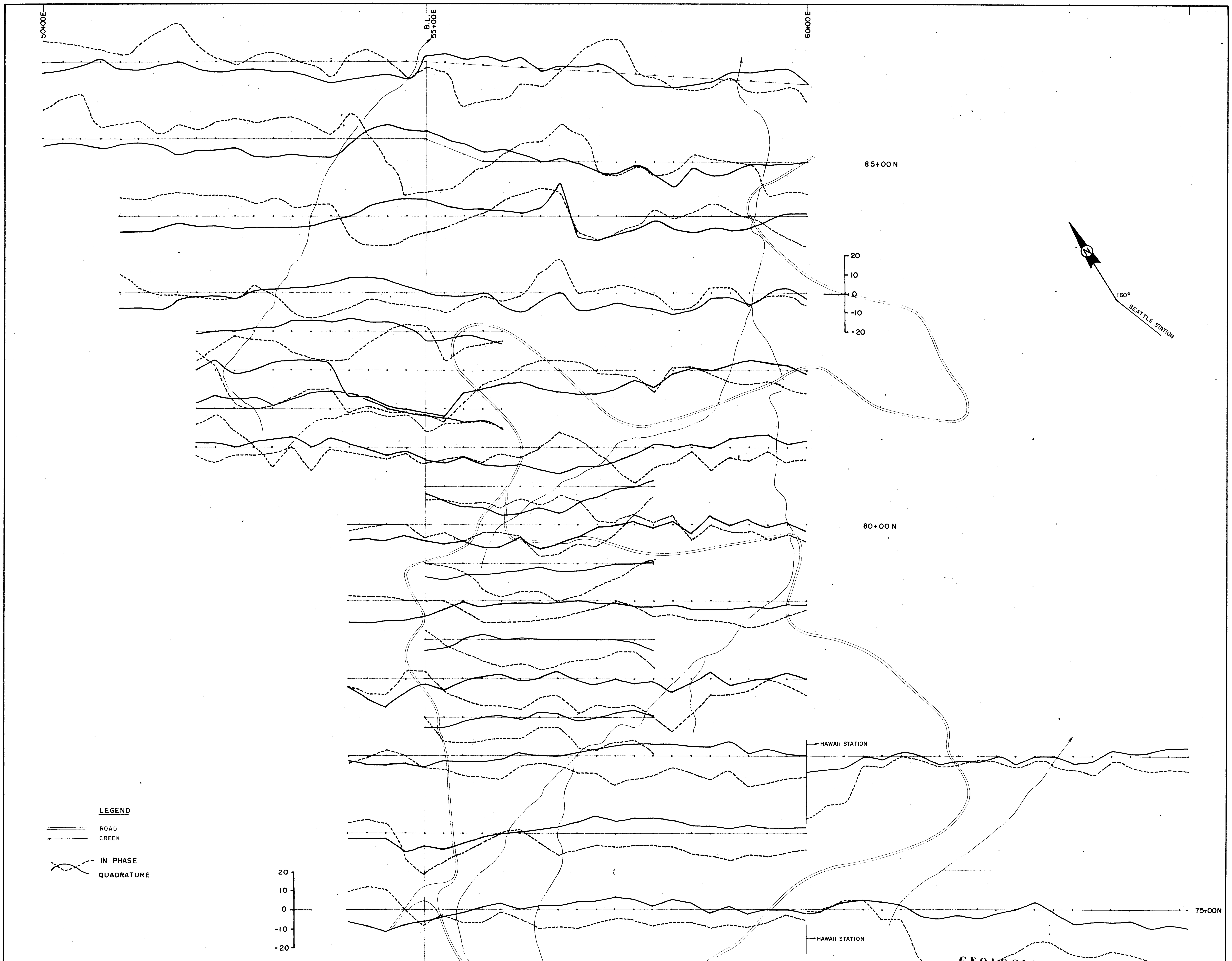


50+00E
B.L. 55+00E
60+00E
85+00 N
80+00 N
75+00N
20
10
0
-10
-20
CUTTER STATION
55°
N
LEGEND
ROAD
CREEK
IN-PHASE
QUADRATURE
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,888
GOLDEN DYNASTY RESOURCES LTD.
IRON MOUNTAIN PROPERTY
VLF-EM PROFILES
(CUTTER)
N.T.S. 92 I-2
NICOLA M.D., B.C.
0
50
100
200 METRES
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher
P. A. CHRISTOPHER & ASSOCIATES INC.
SCALE 1:2500
DATE: JUNE 1989
FIGURE 8b
CHONG



50+00E
B.L. 55+00E
60+00E
85+00N
80+00N
75+00N
LEGEND
ROAD
CREEK
BASE VALUE 0 = 56,500 GAMMAS
CONTOURS AT 200 GAMMAS
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,888
GOLDEN DYNASTY RESOURCES LTD.
PROPERTY
MAGNETOMETER SURVEY
N.T.S. 92I-2
NICOLA M.D., B.C.
0 50 100 200 METRES
P. A. CHRISTOPHER & ASSOCIATES INC.
SCALE : 1:2500
DATE: JUNE 1989
FIGURE 9
PROFESSIONAL
PROVINCE OF
P. A. Christopher
BRITISH COLUMBIA
ENGINEER

CHONG



GEOLOGICAL BRANCH
ASSESSMENT REPORT

18,888

GOLDEN DYNASTY RESOURCES LTD.

IRON MOUNTAIN PROPERTY

VLF-EM PROFILES
(SEATTLE)

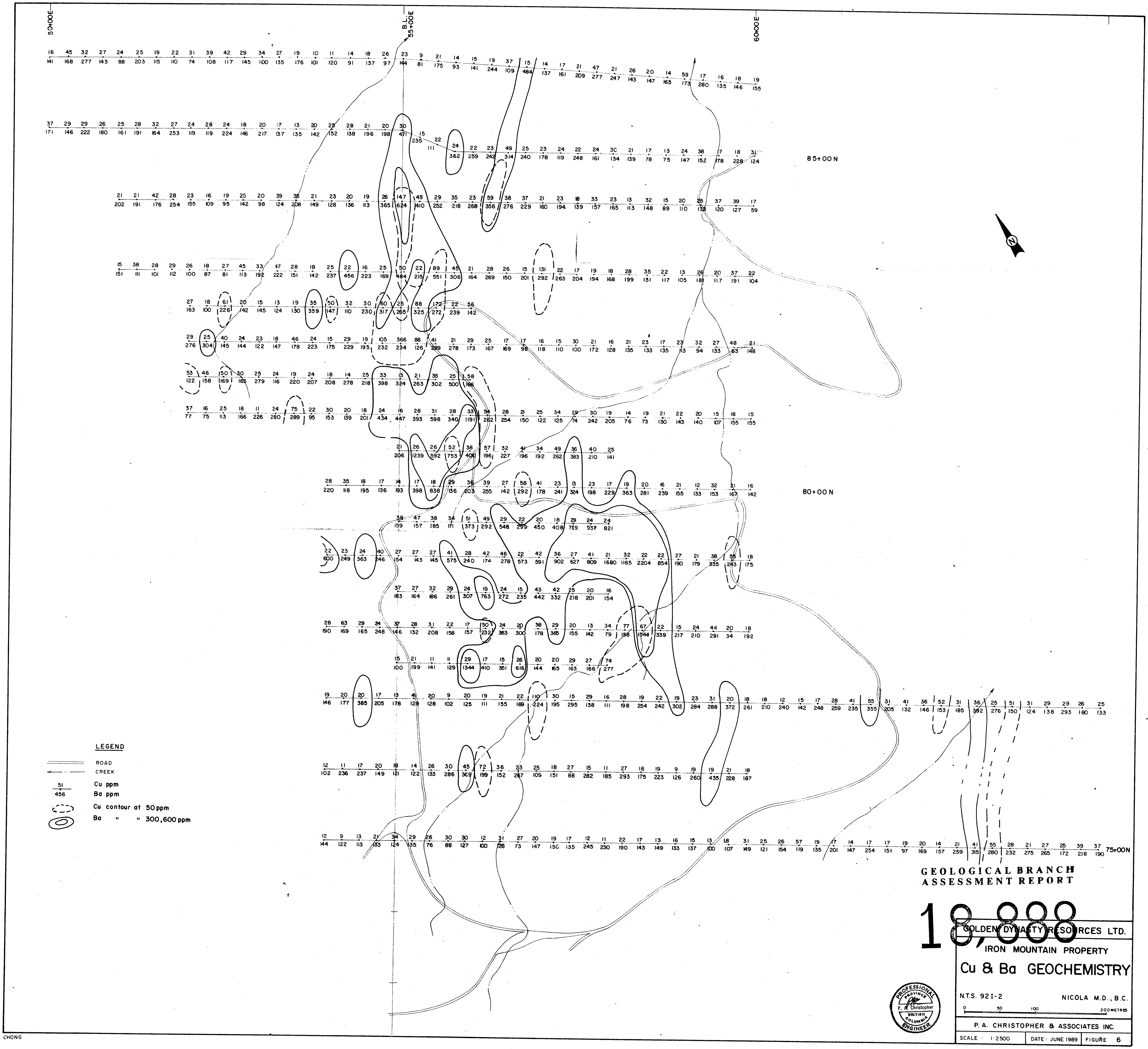
N.T.S. 92I-2 NICOLA M.D., B.C.

0 50 100 200 METRES

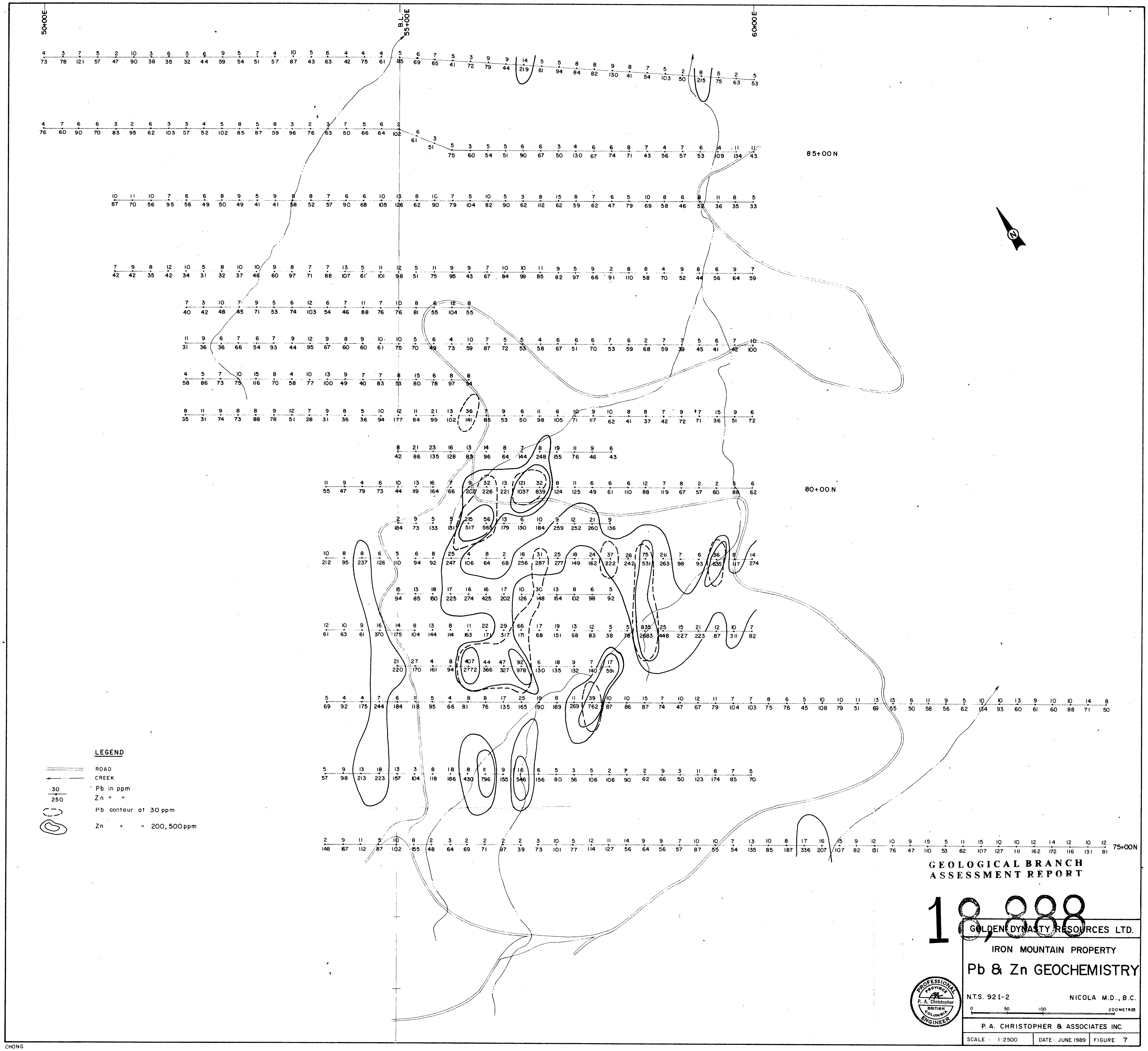
P. A. CHRISTOPHER & ASSOCIATES INC.

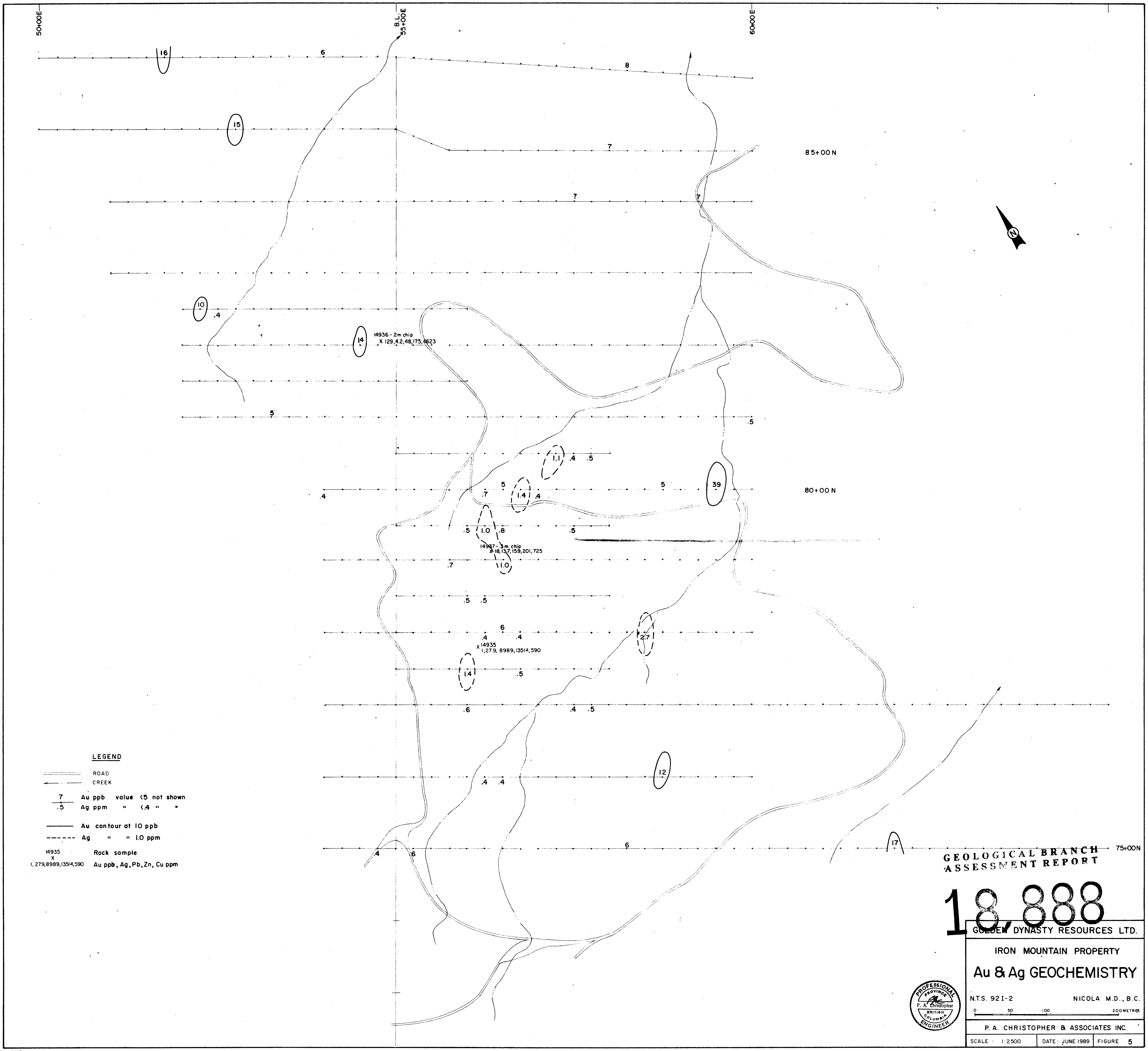
SCALE : 1:2500	DATE: JUNE 1989	FIGURE 8a

CHONG



50+00E
B.L. 55+00E
60+00E
85+00N
80+00N
75+00N
N
LEGEND
ROAD
CREEK
51/456 Cu ppm / Ba ppm
Cu contour at 50 ppm
Ba " " 300,600 ppm
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,888
GOLDEN DYNASTY RESOURCES LTD.
IRON MOUNTAIN PROPERTY
Cu & Ba GEOCHEMISTRY
N.T.S. 92 I-2
NICOLA M.D., B.C.
0 50 100 200 METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE 1:2500
DATE: JUNE 1989
FIGURE 6
PROFESSIONAL ENGINEER PROVINCE OF BRITISH COLUMBIA P. A. Christopher
CHONG


50+00E
B.L.
55+00E
60+00E
85+00N
80+00N
75+00N
N
LEGEND
ROAD
CREEK
30 / 250
Pb in ppm
Zn " "
Pb contour at 30 ppm
Zn " " 200, 500 ppm
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,888
GOLDEN DYNASTY RESOURCES LTD.
IRON MOUNTAIN PROPERTY
Pb & Zn GEOCHEMISTRY
N.T.S. 92I-2
NICOLA M.D., B.C.
0 50 100 200METRES
P.A. CHRISTOPHER & ASSOCIATES INC.
SCALE 1:2500
DATE: JUNE 1989
FIGURE 7
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher
CHONG



50+00E
B.L. 55+00E
60+00E
85+00N
80+00N
75+00N
N
14936 - 2m chip
X 129, 4.2, 48, 175, 1623
14937 - 3m chip
X 18, 13.7, 159, 201, 725
X 14935
1, 27.9, 8989, 13514, 590
LEGEND
ROAD
CREEK
7 Au ppb value <5 not shown
.5 Ag ppm " <.4 " "
Au contour at 10 ppb
Ag " " 1.0 ppm
14935 X 1, 279, 8989, 13514, 590
Rock sample
Au ppb, Ag, Pb, Zn, Cu ppm
GEOLOGICAL BRANCH
ASSESSMENT REPORT
18,888
GOLDEN DYNASTY RESOURCES LTD.
IRON MOUNTAIN PROPERTY
Au & Ag GEOCHEMISTRY
N.T.S. 92 I-2
NICOLA M.D., B.C.
0 50 100 200 METRES
PROFESSIONAL ENGINEER
PROVINCE OF BRITISH COLUMBIA
P. A. Christopher
P. A. CHRISTOPHER & ASSOCIATES INC.
SCALE 1:2500
DATE: JUNE 1989
FIGURE 5

CHONG