R.L. WRIGHT & ASSOCIATES

GEOLOGICAL CONSULTANTS

ASSESSMENT REPORT

on

GEOLOGICAL MAPPING
LINECUTTING
GEOCHEMICAL SURVEYS
VLF-EM SURVEYS
INDUCED POLARIZATION SURVEYS

of the

DOVE PROPERTY
Courtenay, B.C.

Claims: Ideal 1-22
Harmony 1-16

Nanaimo Mining Division

Owner: Joseph L. Paquet
1425 N. Island Highway
Campbell River, B.C. V9Z 2E4

NTS: 92F/11 & 92F/14
Latitude: 49° 45' N
Longitude: 125° 13' W

Operators: Visible Gold Inc.
P.O. Box 49078
1763 - 595 Burrard St.
Vancouver, B.C. V7X 1G4

Westmin Resources Ltd.
P.O. Box 49066, Bentall Centre
1055 Dunsmuir St.
Vancouver, B.C. V7X 1C4

September 15, 1989

R.L. Wright, MSc., FGAC

INTRODUCTION

The attached Year End Report on the Dove Property covers work done from May 15, 1988 to August 1989, the majority of which was filed for assessment on June 16, 1989. Because this Year End Report is the sixth report written on the project and because it was not written as an assessment report, a number of deficiencies relating to background information and financial aspects are apparent. The following covering report is intended to address these deficiencies and to upgrade an internal progress report to assessment report standard as indicated in the Mineral Act Regulations.

The field program in 1988 involved **geological mapping** of the entire property at a scale of 1:10,000 with more detailed followup mapping of specific areas of interest on grids at 1:2500 scale. **Linecutting** was done to clear existing grids of new growth and to establish new grids, namely the NS and McKay grids. **Geochemical soil sampling** was done on several roads to complete coverage from previous years and along grid lines on the Paquet, NS, McKay and Regan grids to augment existing data based on previous work. An **Induced Polarization** survey was run on the NS and Main grids as well as a number of test lines in new areas to determine the feasibility of more extensive work at a later date. A **VLF-EM** ground survey was run on the NS, Paquet, Main (North), McKay and Regan grids, to followup results of an earlier airborne EM survey (Wright, 1988b).

COST STATEMENTS

Each of these activities involved different personnel and covered different areas. To simplify the apportioning of costs per claim, each activity is treated separately and the cost of each activity per claim is determined, then these are combined to give a total expenditure per claim. The costs claimed on the Statement of Work filed on June 16, 1989 represent only about 75% of the total project costs, the balance being logistical and support costs not claimed for assessment purposes or costs incurred outside the June 16, 1988 to June 15, 1989 period (eg. startup costs from May 15, 1988 to June 15, 1988).

a) GEOLOGICAL MAPPING

Geological mapping was undertaken to provide uniform coverage of the entire property and hence the cost of work per claim is calculated as the total cost of geological mapping, divided by 374, the number of claim units on the property, and prorated according to the number of units per claim.

Statement of Expenditures
Geological Mapping

Supplies: bags, flagging, etc.		$ 2910.78
Airphotos:		872.78
Transportation:		
Truck rentals - June 15-Dec.15, 1988		9486.17
Gas - 1/2 of total		1808.97
Repairs - 1/2 of total		566.71
Accommodation:		
A. Weston and R. Wright June 15-Dec.15		3651.33
Wages:		
Geologist, A. Weston, June 15-Nov. 7, 128 days @ $170.00	21,760.00	
Helper, A. Donaghy, July 1-Oct. 31, 552 hrs @ $11.15	6154.80	
Helper, R. Garlock, July 1-Aug. 31, 47 hrs @ $11.15	524.05	
Helper, E. Radcliffe, June 15-Oct. 31, 161.5 hrs @ $13.24 to $14.64	2189.03	

Supervision:	
R. Wright, incl. salary, accomm., office rental, equipment rentals, 30 days @ $340.00	10,200.00
Compilation, report writing: 20 days @ $250.00	5000.00
Total Cost	$65,124.62
Cost per unit (÷374) = $174.13	

b) Linecutting

Linecutting was done primarily on the McKay, NS, Paquet and Main grids, with some effort involved in clearing old overgrown roads and cut lines, to gain access to the new areas. A total of 45.125 line kilometres were cut - the total cost has been calculated on a per km basis and assigned to each claim according to the number of line kilometres on each.

Grid	Claim	Kilometres	Total
McKay	Ideal 1	3.20	17.90
	Ideal 5	13.70	
	Ideal 6	1.00	
Main	Ideal 3	0.20	6.30
	Ideal 4	5.70	
	Ideal 12	0.40	
NS	Ideal 2	0.90	16.70
	Ideal 8	14.70	
	Ideal 13	0.50	
	Ideal 14	0.60	
Paquet	Ideal 2	3.15	4.225
	Ideal 12	1.075	
Total			45.125 km

Statement of Expenditures
Linecutting

P. Endersby, contract		$11,454.70
Wages:		
E. Radcliffe, Aug, Sept. 84.5 hrs @ $13.24 to $14.64	1173.38	
R. Garlock, Aug.-Oct., 138 hrs @ $11.15	1538.70	
D. Dixon, Sept., 20 hrs @ $11.15	223.00	
R. Scott, Sept., Oct., 52 hrs @ $11.15	579.80	
F. Hughes, Aug., 69 hrs @ $11.00	759.00	
P. Endersby, Aug, Sept., 100 hrs @ $11.00	1100.00	
B. Scott, Sept., 33 hrs @ $11.00	363.00	
P. Morro, Sept., 15 hrs @ $11.00	165.00	
N. Blondel, Sept, 89 1/2 hrs @ $11.00	984.50	
		6886.38
Transportation, supplies included under geochem, VLF,, etc.		-
Total cost		$18,341.08
Cost per kilometre (÷45.125) = $406.45		

c) Geochemistry

Soil samples were collected from the various grids as well as along roads and test lines in several other areas. Total costs of sampling and analyses are divided by the total number of samples, 1677, and costs are assigned to each claim on a number of samples per claim basis.

Area/Grid	Claim	Samples	Total
Wolf Lake Area	Ideal 22	96	96
H Grid Test	Harmony 1	20	50
	Harmony 2	30	

Anomaly E	Harmony 2	34	63
	Harmony 4	2	
	Harmony 16	27	
NS Grid	Ideal 2	31	524
	Ideal 8	460	
	Ideal 13	21	
	Ideal 14	12	
McKay Grid	Ideal 1	114	589
	Ideal 5	437	
	Ideal 6	38	
Paquet Grid	Ideal 2	51	219
	Ideal 12	168	
Regan Grid	Harmony 7	136	136

Statement of Expenditures
Geochemistry

Supplies:		$1476.41
Shipping Samples:		135.85
Geochemical analyses: 30 element ICP + Au (AA)		
Acme Labs 1677 samples @ $10.41		17,457.03
Transportation:		
Truck rental		3263.27
Gas, oil: 1/4 of total		904.49
Repairs: 1/4 of total		283.35
Wages:		
R. Scott, July-Oct., 94 hrs @ $11.15	1048.10	
R. Garlock, June 15-Oct.,		
180.5 hrs @ $11.15	2012.58	

E. Radcliffe, July-Sept., 136 hrs @ $13.24 to $14.64	1851.09	
A. Donaghy, July, 22.5 hrs @ $11.15	250.88	
D. Dixon, Sept., Oct., 51.5 hrs @ $11.15	574.23	
B. Scott, Sept., 23.5 hrs @ $11.15	262.03	
P. Morro, Sept., 23.5 hrs @ $11.15	262.03	
		6260.94
Supervision: R. Wright. incl. salary, accomm., office rental, equipment rentals, 10 days @ $340.00		3400.00
Total cost		$33,181.34

Cost per sample (÷1677) = $19.77

d) Induced Polarization Survey

Total IP survey costs were prorated on a per km basis and assigned to the claims on a km per claim basis, as follows:

Area	Claim	Kilometres	Total
Regan Grid	Harmony 7	2.40	2.40
NS Grid	Ideal 2	0.85	14.50
	Ideal 8	12.80	
	Ideal 13	0.50	
	Ideal 14	0.35	
Murex Grid	Ideal 1	1.70	2.70
	Ideal 9	1.00	
Main Grid	Ideal 3	0.20	6.30
	Ideal 4	5.70	
	Ideal 12	0.40	
Total			25.90 km

Statement of Expenditures
IP Survey

Contract: Scott Geophysics, Sept.20-Oct. 22		$30,665.86
Wages:		
R. Garlock, 107.5 hrs @ $11.15	1198.63	
E. Radcliffe, 183 hrs @ $14.64	2679.11	
		3877.74
Accommodation: IP crew		1848.31
Supervision: R. Wright, incl. salary, transportation, office, equipment, 21 days @ $340.00		7140.00
Total cost		$43,531.91

Cost per kilometre (÷25.90) = $1680.77

e) VLF-EM Survey

A total of 97.25 km of lines were run on Hawaii and/or Seattle transmitters, as follows:

Grid	Claim	Kilometres	Total
McKay	Ideal 1	6.40	34.20
	Ideal 5	25.80	
	Ideal 6	2.00	
Main	Ideal 4	20.05	27.60
	Ideal 7	7.55	
Paquet	Ideal 2	3.70	13.85
	Ideal 12	10.15	

NS	Ideal 2	0.85	14.50
	Ideal 8	12.80	
	Ideal 13	0.50	
	Ideal 14	0.35	
Total			97.25 km

Statement of Expenditures
VLF-EM Survey

Supplies:		$1476.41
Transportation:		
Truck Rental:		3263.27
Gas for trucks, 1/4 of total		904.49
Repairs, 1/4 of total		283.35
Instrument Rental, @ $10.00/day		1176.60
Wages:		
E. Radcliffe, July-Oct., 222.5 hrs @ $14.00	3116.05	
R. Garlock, July-Oct., 174 hrs @ $11.15	1940.00	
A. Donaghy, Aug., 22.5 hrs @ $11.15	250.88	
R. Scott, Aug.-Oct., 207 hrs @ $11.15	2308.05	
D. Dixon, Aug.-Oct., 345 hrs @ $11.15	3846.76	
		11,461.85
Supervision: R. Wright, incl. accomm., office, equipment rental, 20 days @ $340.00		6800.00
Compilation, Report writing: 15 days @ $250.00		3750.00
Total cost		$29,115.97

Cost per kilometre (÷97.25) = $299.93

Statement of Expenditures

Claim	Units	Geology	Linecut	Geochem	I P	VLF	TOTAL
Ideal 1	16	2786.08	1300.64	2255.62	2857.31	1916.12	11,115.77
Ideal 2	20	3482.60	1646.12	1622.46	1428.65	1362.24	9,542.07
Ideal 3	20	3482.60	81.29	-	336.15	-	3,900.04
Ideal 4	20	3482.60	2316.77	-	9580.38	6002.83	21,382.58
Ideal 5	9	1567.17	5568.37	8646.54	-	7724.34	23,506.42
Ideal 6	9	1567.17	406.45	751.87	-	598.79	3,324.28
Ideal 7	6	1044.78	-	-	-	2260.42	3,305.20
Ideal 8	20	3482.60	5974.82	9101.62	21513.84	3832.23	43,905.11
Ideal 9	12	2089.56	-	-	1680.77	-	3,770.33
Ideal 10	20	3482.60	-	-	-	-	3,482.60
Ideal 11	20	3482.60	-	-	-	-	3,482.60
Ideal 12	20	3482.60	599.51	3324.07	672.31	3038.84	11,117.33
Ideal 13	1	174.13	203.23	415.51	840.38	149.70	1,782.95
Ideal 14	1	174.13	243.88	237.43	588.27	104.79	1,348.50
Ideal 15	1	174.13	-	-	-	-	174.13
Ideal 16	1	174.13	-	-	-	-	174.13
Ideal 17	1	174.13	-	-	-	-	174.13
Ideal 18*	1	174.13	-	-	-	-	(174.13)
Ideal 19*	1	174.13	-	-	-	-	(174.13)
Ideal 20	2	348.26	-	-	-	-	348.26
Ideal 21	4	696.52	-	-	-	-	696.52
Ideal 22	12	2089.56	-	1899.47	-	-	3,989.03
Harmony 1	20	3482.60	-	395.72	-	-	3,878.32
Harmony 2	20	3482.60	-	1266.31	-	-	4,748.91
Harmony 3	10	1741.30	-	-	-	-	1,741.30
Harmony 4	10	1741.30	-	39.57	-	-	1,780.87
Harmony 5	20	3482.60	-	-	-	-	3,482.60
Harmony 6	20	3482.60	-	-	-	-	3,482.60
Harmony 7	18	3134.34	-	2690.91	4033.84	2125.69	11,984.78
Harmony 8	1	174.13	-	-	-	-	174.13

Harmony 9	12	2089.56	-	-	-	-	2,089.56
Harmony 10	8	1393.04	-	-	-	-	1,393.04
Harmony 11	1	174.13	-	-	-	-	174.13
Harmony 12	1	174.13	-	-	-	-	174.13
Harmony 13*	1	174.13	-	-	-	-	(174.13)
Harmony 14*	1	174.13	-	-	-	-	(174.13)
Harmony 15	9	1567.17	-	-	-	-	1,567.17
Harmony 16	5	870.65	-	534.23	-	-	1,404.88
		65124.62	18341.08	33181.34	43531.91	29115.97	189,294.92

* These claims lapsed after work done but prior to filing assessment, hence:

Total cost of work:	$189,294.92
Less: work on abandoned claims:	697.08
Total cost of work claimed:	$188,597.84

R.L. Wright, MSc., FGAC
R.L. Wright & Associates

Statement of Qualifications

I, Robert L. Wright, geologist, residing at 105 Sunset Drive, in the village of Lions Bay, province of British Columbia, hereby certify that:

1. I received a B.Sc. degree in Honours Geology from McMaster University, Hamilton, Ontario in 1971 and a M.Sc. degree in Geology from the University of British Columbia, Vancouver, B.C. in 1974.

2. I have been practising my profession as an exploration geologist since 1975.

3. I am a Fellow of the Geological Association of Canada.

4. I am the proprietor of the exploration consulting firm, R.L. Wright & Associates.

5. The work described in this report was undertaken under my direct supervision, on a consulting basis, on behalf of Westmin Resources Ltd., 1055 Dunsmuir Street, Vancouver, B.C.

12 day of Sept., 1989
Vancouver, British Columbia

RLWright.
R.L. Wright, M.Sc., FGAC
R.L. Wright & Associates

R.L. WRIGHT & ASSOCIATES

GEOLOGICAL CONSULTANTS

1988 YEAR END REPORT

on the

DOVE PROJECT

Courtenay, B.C.
Nanaimo Mining Division
NTS: 92F/11 & 92F/14
Lat: 49° 45'N
Long: 125° 13'W

for

WESTMIN RESOURCES LTD.
P.O. Box 49066 Bentall Centre
904-1055 Dunsmuir St.
Vancouver, B. C. V7X 1C4

and

VISIBLE GOLD INC.
P.O. Box 49078
1763-595 Burrard St.
Vancouver, B.C. V7X 1G4

July 15, 1989

R. L. Wright, MSc, FGAC

R.L. (Bob) Wright M.Sc., F.G.A.C., Box 266 Lions Bay B.C. VON 2E0 • (604) 921-9370

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SUMMARY

The Dove property, consisting of 370 claim units in the Ideal and Harmony claim groups, is located 15 km northwest of Courtenay, Vancouver Island, B. C., on the east flank of Mount Washington.

The property is being explored by a joint venture between Westmin Resources Ltd. and Visible Gold Inc. under an option agreement with the owner, Joseph L. Paquet, who retains a 7.5% carried net profits interest.

The Dove project involves exploration for high-grade lode gold deposits of epithermal-type in an area previously, partially explored for porphyry copper deposits. The property covers a portion of a large Tertiary magmatic hydrothermal system which intruded and mineralized basalts of the Triassic Karmutsen Formation and unconformably overlying epiclastic sediments of the Cretaceous Nanaimo Group. Epithermal-type gold/silver mineralization is also hosted by the Tertiary intrusions and diatreme breccias, and appears to favour a position close to the sub-Cretaceous unconformity, a substantial portion of which is covered by the Dove property.

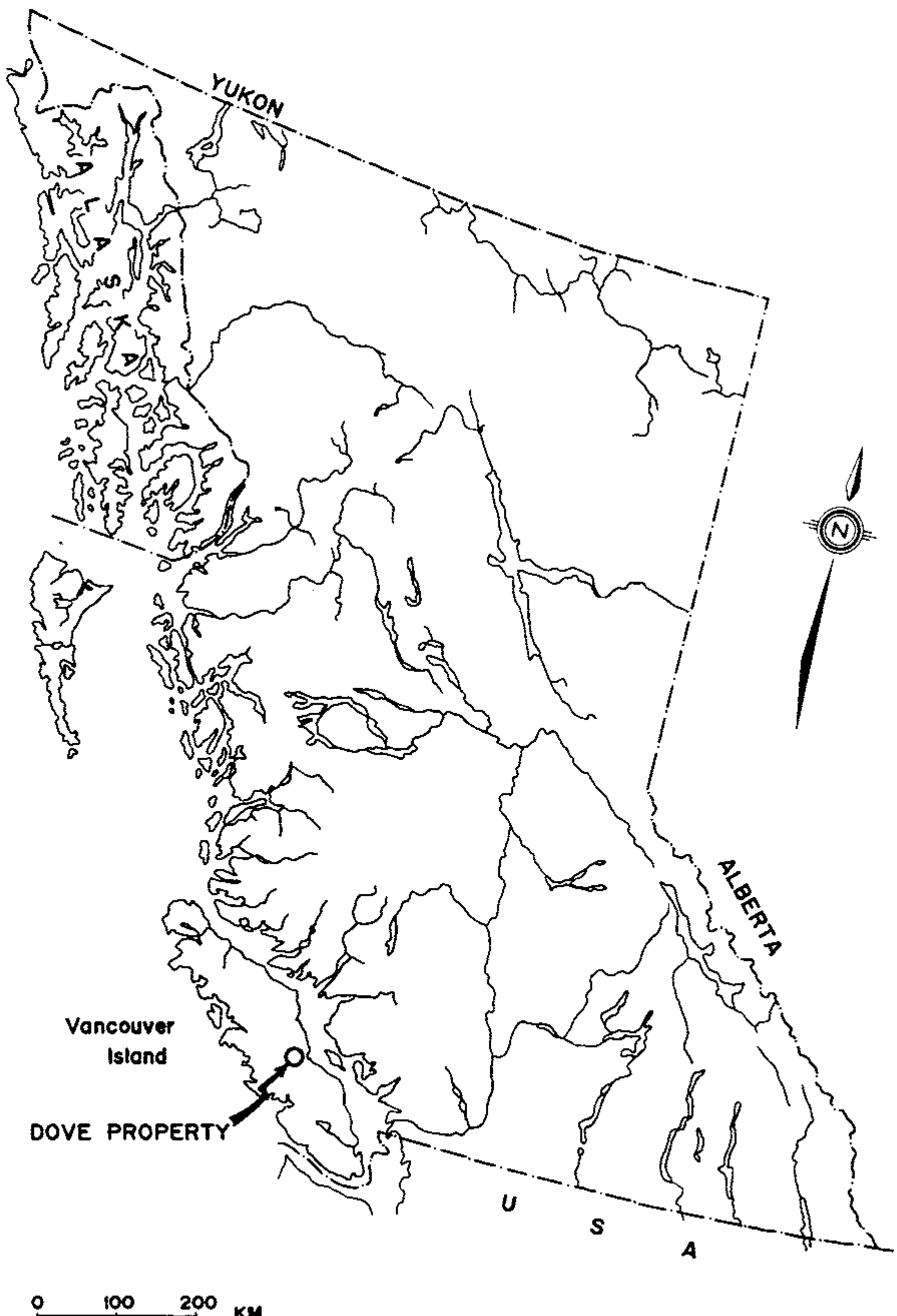
Lode gold deposits described on claims adjoining both the east and west sides of the Dove property contain sample grades of several tenths of an ounce gold over mineable widths with localized values ranging up to several ounces gold per ton.

Exploration on the Dove property in 1986, 1987 and 1988 located several occurrences of epithermal mineralization with anomalous to ore grade gold and/or silver values. The program in 1987 involved soil geochemical and airborne geophysical surveys of the entire property with more detailed induced polarization, VLF-EM and soil geochemistry surveys in most promising areas. This work was followed by a preliminary diamond drill program which demonstrated the presence of significant fault structures, with associated hydrothermal alteration and veining, some

containing anomalous gold values, which are unexposed due to extensive overburden. The 1987 program thus demonstrated the validity of our exploration model, seeking epithermal-type high-grade gold/silver mineralization, associated with base metals, in structures related to Tertiary intrusions. Favourable structures include steep block faults and shallow to flat faults interpreted as either thrusts or detachment faults.

The program in 1988 involved systematic geological mapping of the entire property, with emphasis on areas around known showings, and with more detailed induced polarization, VLF-EM and soil geochemistry surveys on grids cut over the most promising areas. This work outlined several drill targets for further exploration.

It is proposed to follow up these results from 1987 and 1988 with a diamond drill program to evaluate known showings to depth and along strike, as well as to test poorly exposed geological, geochemical and geophysical anomalies. Some additional fill-in grid work will be required to better define drill targets.



Nanaimo M.D.

NTS: 92F/11,14

R L WRIGHT & ASSOC.

DOVE PROJECT
Location Map

Figure 1

A) INTRODUCTION

This report is a summary of the results of the 1988 exploration program on the Dove Property, which was a joint venture between Westmin Resources Ltd. and Visible Gold Inc. Exploration on the Ideal and Harmony claims, which comprise the Dove Property, began on May 15, 1988 when a field office was established in Comox, and systematic geological mapping undertaken. This work was followed by soil grid geochemistry and extensive IP surveys in selected target areas, as preparation for diamond drilling.

The author is the proprietor of the geological consulting firm R.L. Wright & Associates, and has been directly involved in the Dove Project as project manager under contract to Westmin Resources Ltd. since June, 1987. This work was done under the supervision of Richard R. Walker, Exploration Manager, Vancouver Island for Westmin.

B) LOCATION AND ACCESS

The Dove Property is located 15 km northwest of Courtenay, B.C. in NTS map sheets 92F/11E and 92F/14E & W (Figure 1). Access to the property is provided by paved and all-weather gravel roads (logging mains) from Courtenay (20 min.) and Campbell River (30 min.). A network of active logging mains and secondary inactive logging roads owned by Fletcher Challenge southeast of Piggott Creek and by MacMillan Bloedel northwest of Piggott Creek (Harmony 15 claim) crosses the property. Many of the these roads are passable by four-wheel drive vehicle, others could readily be rehabilitated.

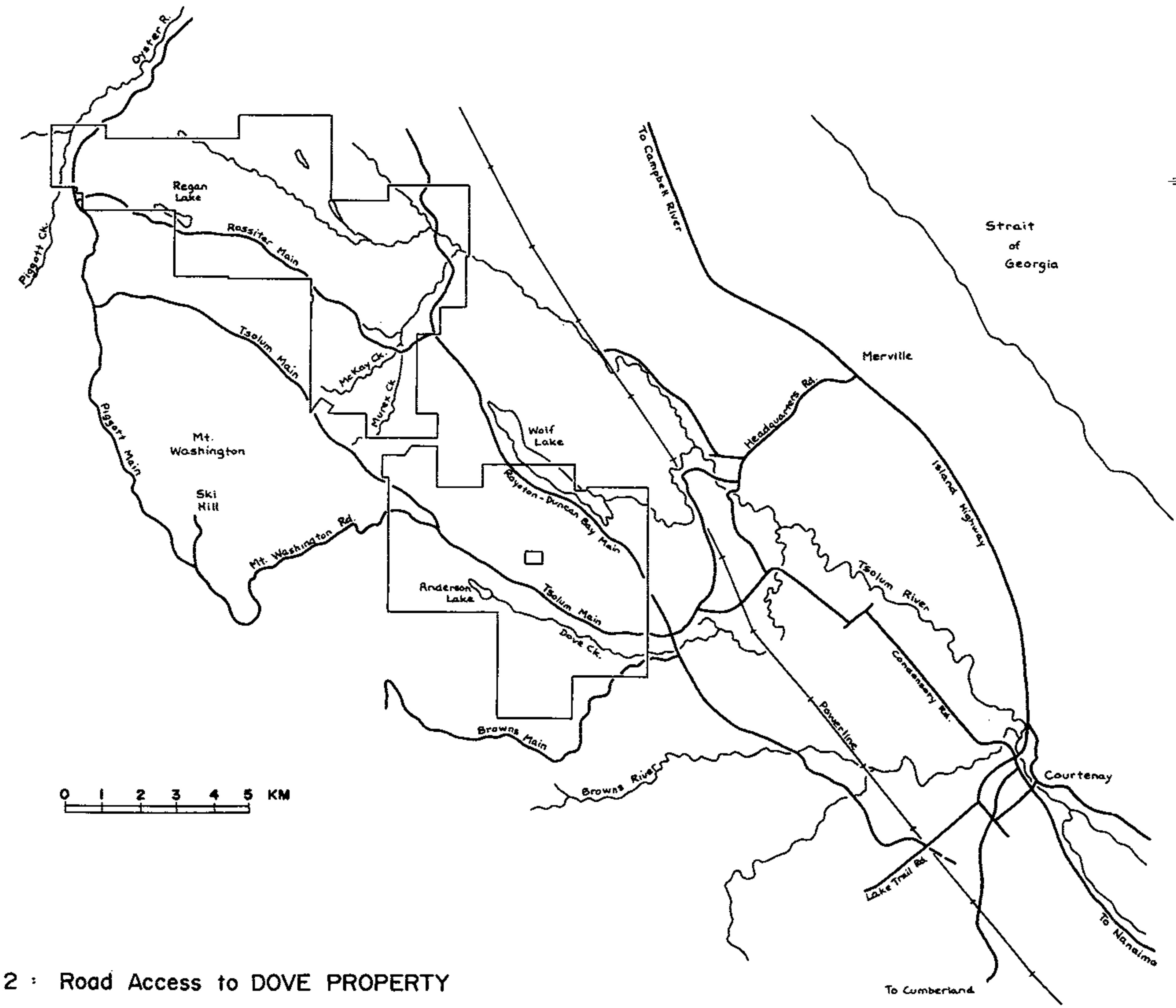


FIGURE 2 : Road Access to DOVE PROPERTY

C) PHYSIOGRAPHY AND VEGETATION

The property lies on the east and north flanks of Mt. Washington, at elevations between 100 m. and 790 m. Topographic slopes are generally low to moderate except along several deeply-incised creeks. The area is covered by a moderately-thick glacial till blanket, up to 20 m. being encountered in diamond drill holes, the average thickness apparently being about 10 m. Good rock exposures are mostly restricted to the creeks in low-lying areas to the east. The western half of the property has numerous ridges of outcrop separated by drift-filled depressions. Overall exposure is about 1 percent.

The entire property has been logged, with second growth fir, hemlock and cedar ranging in age from about 35 years at lower elevations to recent logging slash at higher elevations. Many secondary logging roads are overgrown by alders which can be readily cleared to provide vehicle access to important areas.

Precipitation is moderately high and concentrated in the winter months from November to April. Snow is an impediment to exploration during winter months, particularly above about 500 m. elevation, but would not be a significant problem for a mining operation.

D) PROPERTY DEFINITION

The Dove property currently consists of two groups of claims - the Ideal claims and the Harmony claims which are optioned from J. Paquet. The property is being explored by a joint venture between Westmin Resources Ltd. and Visible Gold Inc.

Under the terms of agreements with J. Paquet, the joint venture may acquire a 100% interest in the claims subject to a 7.5% carried net profits interest retained by Paquet. The joint venture has the option of purchasing a

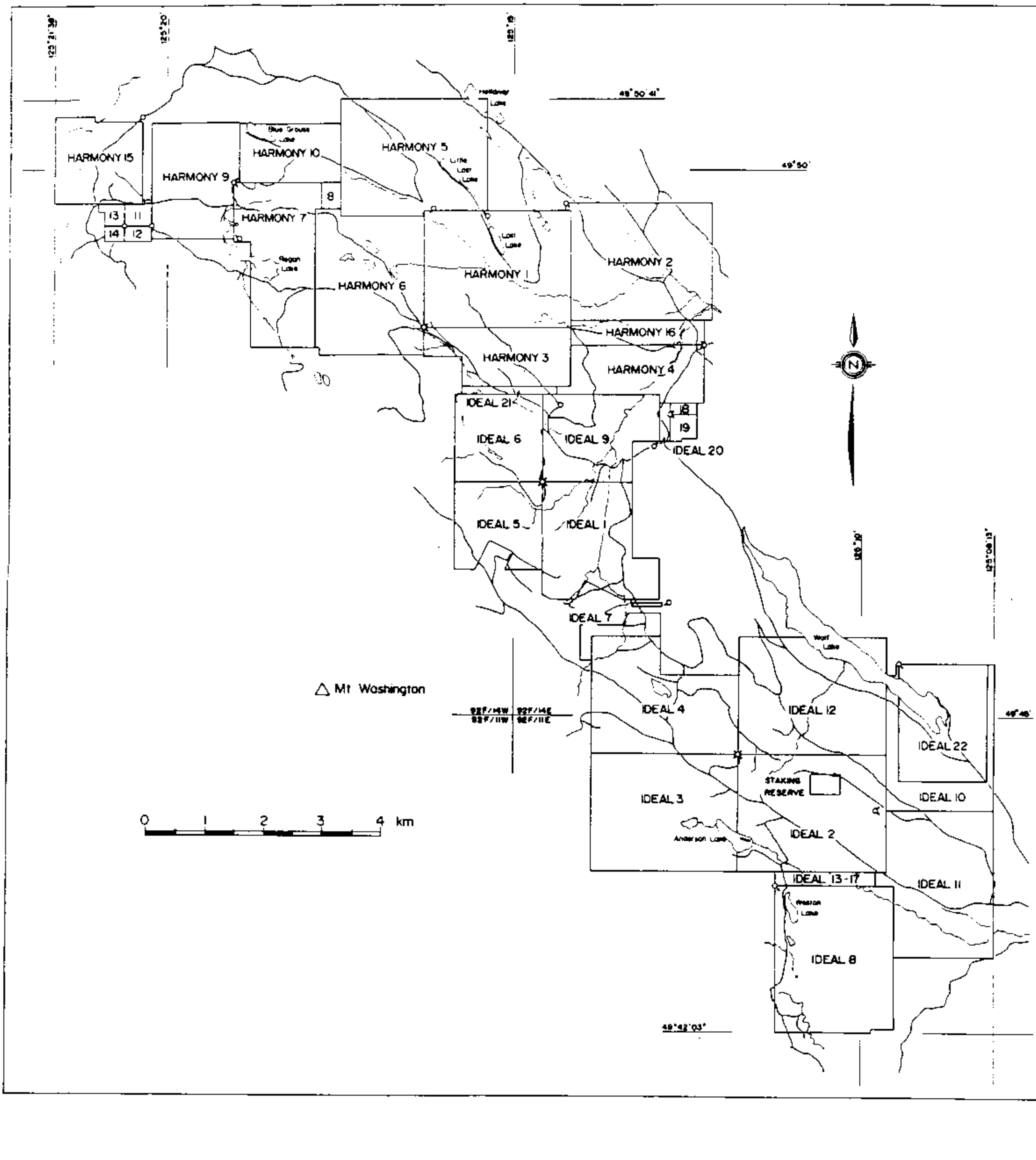


Figure 3. Claim Map: Ideal and Harmony Claims.

further 5% net profits interest from Paquet for $1,000,000 on the Ideal claims and $1,000,000 on the Harmony claims.

TABLE I.

DOVE PROJECT: IDEAL CLAIMS

CLAIM	NO. OF UNITS	RECORD NO.	RECORD DATE	CURRENT EXPIRY DATE*
IDEAL				
1	16	2388	June 2, 1986	1993
2	20	2389	June 3, 1986	1995
3	20	2390	June 3, 1986	1994
4	20	2391	June 3, 1986	1994
5	9	2392	June 3, 1986	1993
6	9	2393	June 4, 1986	1993
7	6	2411	June 13, 1986	1994
8	20	2454	Aug. 6, 1986	1995
9	12	2440	July 29, 1986	1993
10	20	2559	Feb. 20, 1987	1995
11	20	2560	Feb. 13, 1987	1995
12	20	2610	Apr. 7, 1987	1994
13	1	2619	Apr. 16, 1987	1995
14	1	2620	Apr. 16, 1987	1995
15	1	2621	Apr. 16, 1987	1995
16	1	2622	Apr. 16, 1987	1995
17	1	2623	Apr. 16, 1987	1995
20	2	2746	Aug. 4, 1987	1993
21	4	2747	Aug. 4, 1987	1993
22	12	2993	June 17, 1988	1995
	215 units			

*as of July 15, 1989

TABLE II.

DOVE PROJECT: HARMONY CLAIMS

CLAIM	NO. OF UNITS	RECORD NO.	RECORD DATE	CURRENT EXPIRY DATE*
HARMONY				
1	20	2456	Aug. 18, 1986	1990
2	20	2459	Aug. 22, 1986	1990
3	10	2460	Sept. 2, 1986	1994
4	10	2466	Sept. 10, 1986	1994
5	20	2483	Oct. 9, 1986	1990
6	20	2604	Mar. 26, 1987	1994
7	18	2606	Apr. 3, 1987	1996
8	1	2615	Apr. 10, 1987	1991
9	12	2618	Apr. 16, 1987	1996
10	8	2628	Apr. 24, 1987	1991
11	1	2653	May 6, 1987	1991
12	1	2654	May 6, 1987	1991
15	9	2743	July 29, 1987	1990
16	5	2745	Aug. 4, 1987	1994
	155 units			

*as of July 15, 1989

E) HISTORY

The exploration history of the area was summarized by Richard R. Walker in his engineering report dated May 20, 1987, based on available assessment reports, as follows.

The Dove property lies on the east flank of Mt. Washington, marginal to, and in part overlapping, an area which has received extensive exploration beginning in 1940 and continuing to present.

1940: J. M., and R. D. McKay discovered and staked several gold-bearing veins near the top of Mt. Washington 4.5 km west of the Dove property. Here, the Murray vein (Domineer vein) was exposed by trenching by D. F. Kidd.

1944-45: Consolidated Mining and Smelting excavated additional trenches across and drove a short adit into the Murray vein.

1951-59: Noranda Exploration Ltd. explored Mt. Washington with initial emphasis on an area a short distance north of the Murray vein. In 1956, the Mt. Washington Copper Company was formed and tested low grade copper mineralization on Murex Creek (about 1.5 km west of the Dove property) by trenching and 152 m of drilling. In 1957 and 1958, Noranda conducted geological mapping, self-potential and electromagnetic geophysical surveys, trenching and diamond drilling totalling 365.8 m in 10 holes in the area later developed as the Mt. Washington Copper open pit mine located 4.5 km west of the Dove property and in the Murex zone.

1963-64: Cominco conducted geological mapping and drilled 3843 m in 22 holes in the open pit and Murex Creek zones of copper mineralization.

1965-67: Mt. Washington Copper Co. Ltd. developed a small mine and mill operation which produced 396,095 short tons of ore from two pits with an average recovered grade of 1.16% Cu, 0.01 oz Au/T and 0.5 oz Ag/T. These pits lie 4.5 km west of the Dove property.

1967-69: Mt. Washington Copper Co. Ltd. explored the Litchie Claims south of Anderson Lake now covered in part by the Dove property (southeast IDEAL 3 and northwest IDEAL 2). One diamond drill hole 30.8 m deep was drilled 1.15 km southwest of Anderson Lake to test a steep-dipping shear zone with chalcopyrite but failed to intersect mineralization.

1968-69: Marietta Resources Co. Ltd. conducted geological mapping, ground and airborne magnetometer surveys, an induced polarization survey and a soil geochemical survey (2134 samples) over an area 4.3 x 7.4 km centered on the Murex copper zone and extending into the area of the current Dove property. Fifteen diamond drill holes totalling 2005 m tested geophysical anomalies, surface mineralization and geological models. Low grade copper mineralization was intersected in some holes testing depth projections of surface showings. Four holes were drilled just inside the west central part of the Dove property with results summarized as follows. No gold assays were reported.

D.D.H. 69/3: 305 m long at -70°S, tested I.P. anomaly, intersected Karmutsen Formation basalt with chalcopyrite in fractures.

D.D.H. 69/4: 305 m long at -70° ENE, tested part of a large magnetic anomaly, intersected Karmutsen Formation with chalcopyrite in fractures and veinlets.

D.D.H. 65/5: 150 m long at -90°, tested I.P. anomaly, intersected Karmutsen Formation.

D.D.H. 69/7: 305 m long at -90°, tested part of a large magnetic anomaly, intersected Tertiary quartz diorite with disseminated and fracture-bound sulphides.

1971: Mt. Washington Copper drilled 5 short holes.

1972-82: Esso Minerals Ltd. conducted geological mapping, I.P. survey (12.1 km), soil silt and water geochemical surveys along 241 km of grid lines, and drilled 31 holes totalling 3198 m. Five of these tested the Meadows zone (now called the West Grid zone by Better Resources) located 0.5 km west of the Murray vein. Gold was not assayed.

1978-81: Esso Minerals conducted pilot plant scale heap leaching tests of low grade copper mineralization after outlining 0.5 to 1 million tons grading 0.5% Cu west of the Dove property.

1983-88: Better Resources Ltd. conducted geological mapping, soil and water geochemistry, trenching and drilled 67 holes. Unlike much previous work this program is directed specifically at evaluating the potential of epithermal precious metal mineralization in the area west of the Dove property which was previously evaluated for porphyry copper mineralization. This drilling has been concentrated on the Murray vein (Domineer zone), and the West Grid and Lakeview zones (Meadows zone) near the top of Mt. Washington with more limited drilling in the Murex Breccia zone 1.5 km west of the Dove property.

1983-84: Placer Development Ltd. conducted a small program of silt sampling (12 bulk silt and 7 panned concentrates) and soil sampling (10 samples) on what is now the IDEAL 12 claim of the Dove property. Anomalous gold was documented in silts and a mineralized float cobble was reported.

1984-87: Proquest Resource Corp., Homestake Development Company and most recently Cactus West Explorations Ltd. conducted exploration on the Lupus claims which adjoin the Dove property on the east side. This work included prospecting, soil geochemistry, trenching and I.P. surveying. A drill program was initiated by Cactus West in April 1987. This program tested epithermal gold vein mineralization 1500 m east of IDEAL 1 and 500 m northeast of IDEAL 12.

In summary, the history of exploration in the area of the Dove project began in the 1940's with exploration for high-grade gold veins. For the next three decades the area received intensive exploration for low-grade or porphyry-type copper deposits. During this period, little attention appears to have been given to quartz veins or gold assays. The 1980's has seen renewed exploration for high-grade lode gold deposits based on an epithermal model. Such mineralization has been documented both east and west of the Dove property.

In 1987, exploration was quite intensive in the area, involving 4 different projects. Better Resources Ltd. continued their evaluation of their Lakeview-West Grid and Domineer zones on Mt. Washington with a diamond drilling program of 8230 m in 105 holes and an underground exploration program consisting of 300 m of adit and crossdrifts. This work resulted in an upgraded ore reserve figure of 979,500 tons drill-indicated at 0.142 oz Au/T and 0.67 oz Ag/T.

Noranda undertook an exploration program on a large block of ground to the west and south of Mt. Washington. This work involved geological mapping, prospecting, soil geochemistry and trenching. Late in the season, Noranda optioned the southern block of claims from Better Resources which cover the Murex breccia gold zone, following up on one hole previously drilled by Better Resources which returned 52.3 ft (15.9 m) of 0.178 oz Au/T plus 8.9 ft (2.7 m) of 0.08 oz Au/T and 10 ft (3.0 m) of 0.11 oz Au/T. Further work is planned by Noranda in 1989.

Cactus West Explorations Ltd. undertook a diamond drilling program on the Lupus Claims around Wolf Lake, to the east of the Dove property. A total of 14 holes were drilled on the Creek zone east of Wolf Lake, and on the Lake zone at the north end of Wolf Lake.

The Westmin/Visible Gold exploration program on the Dove property consisted of an orientation soil geochemistry survey, geological mapping, airborne EM/resistivity/mag survey, linecutting, induced polarization survey, VLF-EM ground survey and a diamond drilling program to test several geophysical anomalies and geological models.

In 1988, exploration continued on several properties in the area. Better Resources Ltd. conducted surface diamond drilling to the north of the Lakeview-West Grid zone and additional drilling is planned for 1989. Noranda drilled the Murex breccia gold zone, optioned from Better Resources, and additional work is also planned for 1989. There was no activity on the Lupus claims in 1988.

The Westmin/Visible Gold exploration program on the Dove Property in 1988 consisted of systematic geological mapping, linecutting, induced polarization, soil geochemistry, and VLF-EM ground surveys. The results of this work are discussed in this report.

F) REGIONAL GEOLOGY AND MINERALIZATION

The geology of the area of the Dove property has been mapped and described by Muller and Carson (1969) and Carson (1973) with revisions and detailing by Benvenuto (1986) and the author (1987). The area is underlain by the Triassic Karmutsen Formation of the Vancouver Group which is unconformably overlain by the Upper Cretaceous Comox Formation of the Nanaimo Group. Both are intruded by Tertiary subvolcanic igneous rocks and diatreme breccias.

The Karmutsen Formation is a pile of tholeiitic basalt up to 6300 m in thickness, which has been subdivided (Muller and Carson, 1969) into a lower half composed of submarine pillowed flows and an upper half composed of massive flows. These thick units are separated by a thinner unit of basaltic pillow breccia and bedded hyaloclastite. The Karmutsen Formation on the Dove property consists of shallow-dipping massive basalt, pillowed basalt and minor hyaloclastite and pillow breccia. The Quatsino limestone, which overlies the Karmutsen elsewhere on Vancouver Island, is absent in the Mt. Washington area, indicating that the upper part of the Karmutsen was eroded before deposition of the Cretaceous sediments.

The Upper Cretaceous Nanaimo Group lies unconformably on the Karmutsen basalts, with significant paleotopographic relief. The Group has been subdivided (Muller 1965) into the basal Benson conglomerate, the Comox Formation and the Trent River Formation. The latter unit outcrops at the Browns River, below the Royston-Duncan Bay main bridge, near the southeast corner of the property, but is not known to occur within the claims. The Comox Formation which forms the bulk of the Nanaimo Group on the property is an assemblage of sandstone, siltstone and black shale with coal horizons. A thin plate of this unit underlies most of the low ground in the east and northeast portions of the property, but is poorly exposed except in incised stream valleys. The basal Benson conglomerate is highly variable in clast size and in overall thickness, being apparently absent in many places, but forming a valley-fill structure up to 150 m thick in the Oyster River area on HARMONY 15. Where the basal conglomerate is intersected in drillholes, it is associated with a soft clay alteration horizon extending into the Karmutsen basalts which is interpreted as an alteration feature, but may in fact be a regolith. This feature is generally not recognized on the surface because of its soft recessive nature.

Tertiary igneous rocks have intruded the Karmutsen and Nanaimo Formations in the general Mt. Washington area. The intrusives have been described by Carson (1973) as dacite porphyry, quartz diorite and diatreme breccias composed of clasts of intrusive and country rocks. The intrusives take the form of dykes, small stocks, sills and laccoliths and are distributed in a semicircular arc about 25 km across and convex to the north. The Dove property lies on the northeast quadrant of this zone of intrusives. A K-Ar date from quartz diorite on Mt. Washington defined an age of 35 million years. This stock post-dates the dacite porphyry which forms prominent sills and laccoliths near the base of the Comox Formation and is in turn post-dated to diatreme breccias which can be divided into two types. The Murex breccia type, including the Murray and Murex breccia bodies, contain angular and rounded fragments of intrusive, Karmutsen and Nanaimo Formation rocks in a comminuted matrix and may resemble crudely-layered conglomerate thus pointing to fluidization in a diatreme system. The Washington breccia type forms steeply dipping zones of angular breccia at the margins of a quartz diorite stock on Mt. Washington. This breccia has a magnetite-actinolite matrix and is interpreted as a possible collapse breccia by Carson.

The following summary of mineralization on properties surrounding the Dove project area is based on Richard Walker's account (1987), with minor changes by the author reflecting more recent information.

1) MOUNT WASHINGTON COPPER MINE (5 km SW of Dove property)

Hydrothermal precious and base metal mineralization is associated with the Mt. Washington igneous system. The old Mt. Washington open pit copper mine located 5 km southwest of the Dove property produced 396,095 tons or ore averaging 1.16% Cu, 0.01 oz Au/T and 0.5 oz Ag/T between 1965 and 1967. This production was from a flat-lying drusy quartz-sulphide vein about 1.5 m thick, varying up to 7.6 m thick. The vein contained chalcopyrite, bornite, arsenopyrite, pyrite, sphalerite and tetrahedrite, and graded 2 to 4% Cu, 0.01 to 0.12 oz Au/T and 1 oz Ag/T. It overlies more extensive low grade disseminated and stringer mineralization grading 0.1 to 0.5% Cu with associated pyrrhotite, pyrite, arsenopyrite, realgar and molybdenite. The host rock is biotitized quartz-diorite sills interlayered with Nanaimo Group siltstone and quartz sandstone. Sericite and chlorite alteration associated with sulphides appears superimposed on earlier biotite alteration.

Mount Washington Copper quoted unmined undergound reserves adjacent the open pit as 337,000 tons of 1.07% Cu down to the elevation of the tunnel level and inferred a substantial tonnage of similar grade to extend below this level (Stevenson, 1970). A zone of low grade copper mineralization extending 2,000 feet south from the open pit and 500 feet wide was indicated by a few holes. The disseminated sulphides here occur in diorite sills and Comox Formation. Vertical hole C-10 on this zone intersected three mineralized intervals comprising 242 feet of 0.20% Cu, 112 feet of 0.28% Cu and 145 feet of 0.12% Cu. These intervals occur at the top, middle and bottom of this 858 foot deep hole.

2) DOMINEER - WEST GRID - LAKEVIEW ZONES

A prominent, shallow-dipping, vein structure has been trenched and drilled on both sides of the north ridge of Mt. Washington by Better Resources Ltd. The eastern exposure has been called the Murray vein or the Domineer zone. It lies 1.5 km south of the north pit of the old Mt. Washington copper mine and may represent the same vein which was the focus of the past mining. At the Domineer zone, Better Resources Ltd. (1987) has estimated reserves of 41,200 tons of 0.21 oz Au/T and 1.94 oz Ag/T using a 0.1 oz Au/T cutoff over a minimum 6 foot thickness. The exposure averages 0.25 oz Au/T, 2.77 oz Ag/T over a 4.4 foot thickness and an exposed strike length of 125 feet. Sampling of this vein by Cominco in 1945 averaged 0.45 oz Au/T, 3.4 oz Ag/T, 0.8% Cu, 0.5% Pb, 0.5% Zn and 4.1% As over 2 feet. This quartz sulphide vein lies in a clay altered gouge zone and is enveloped by clay alteration up to 30 m wide. The vein appears localized along a shallow west-dipping fault zone and cuts the Murray diatreme breccia. Lower grade disseminated and stringer mineralization is described in the footwall.

The West Grid and Lakeview zones (formerly called the Meadows zone) lie along a 500 m strike length within a shallow west-dipping drusy quartz-sulphide vein exposed 520 m west of the Domineer zone and have been correlated as parts of the same vein structure (Better Resources Ltd., 1987). Based on drilling and underground work done in 1987, the reserves in the Lakeview and West Grid zone have been increased to 1.0 million tons grading 0.142 oz Au/T and 0.67 oz Ag/T. The Lakeview-West Grid vein lies within siltstone and sandstone of the Comox Formation

Pyrite and arsenopyrite are the principal sulphides in the gold-bearing quartz veins but chalcopyrite, covellite, sphalerite, galena, tennantite, bornite, wehrlite, hessite, chalcocite, realgar and orpiment are also reported (Carson, 1960). Pyrrhotite, molybdenite and magnetite are present in the area but are of uncertain relationship to the gold-bearing quartz veins.

3) MUREX BRECCIA ZONE

The Murex Breccia zone is approximately 1 km west of the Dove property. Low-grade copper mineralization consisting of disseminated pyrite, chalcopyrite and pyrrhotite is documented in this area south of Murex Creek where Mt. Washington Copper estimated 2,000,000 tons of 0.40% Cu within brecciated Karmutsen basalt. This zone was not defined to the southeast (Stevenson, W.G., 1970).

Better Resources Ltd. reported a drill intersection of 52.3 feet averaging 0.174 oz Au/T in the Murex Breccia. This interval included 22.3 feet of 0.313 oz Au/T (George Cross Newsletter, September 16, 1986). This mineralization comprised breccia cemented with quartz or veined with a quartz stockwork. The Murex Breccia projects towards and may extend onto the Dove property under overburden.

In summary, previous and current work on Mt. Washington, west of the Dove claims, has documented low-grade porphyry copper mineralization and high-grade, gold-bearing quartz-sulphide veins of epithermal character which are shallow-dipping, probably fault controlled, and lie in close proximity to the Cretaceous unconformity. These veins occur in Comox Formation, Tertiary intrusives and diatreme breccia.

4) WOLF LAKE QUARRY (LAKE) SHOWING

East of the Dove property, a sulphidic drusy quartz vein is exposed in a road quarry 1.7 km east of IDEAL 1 claim. Here the vein cuts Karmutsen basalt and dips 25° east at a location considered close to the unconformity. The main vein is 1 to 3 feet thick composed of drusy quartz and contains abundant sphalerite, pyrite, arsenopyrite, galena and carbonate. Associated, sheeted, thin quartz veins and shattered basalt healed by quartz and sulfide extend the thickness of the zone to about 6 feet. Cactus West Explorations Ltd. has reported composite chip samples across this vein of 0.415 oz Au/T, 1.76 oz Ag/T, 1.75% Zn over 1.41 m and 0.357 oz Au/T, 2.01 oz Ag/T, 2.86% Zn over 2.0 m (George Cross Newsletter, April 10, 1987).

5) CREEK SHOWING

The Creek showing is located 600 m northeast of IDEAL 12 claim, on the east side of Wolf Lake. Narrow calcite-sulphide veins up to 10 cm wide strike east-northeast and dip steeply north. Wallrock is sandstone and siltstone of the Nanaimo Formation which is apparently altered and bleached. Wallrock breccia fragments occur within the vein calcite which is mineralized with pyrite, arsenopyrite and realgar. Cactus West Explorations Ltd. reported 14 grab samples taken over 1,000 feet of the poorly exposed Creek showing range from 0.062 oz Au/T to 0.46 oz Au/T (George Cross Newsletter, April 10, 1987).

Diamond drilling in 1987 on this zone intersected narrow widths of low-grade gold, but did not define a coherent zone of mineralization. (pers. comm. Dennis Baxter, Cactus West Explorations Ltd.).

6) WOLF LAKE REALGAR (WOLF) SHOWING

The Wolf Lake Realgar showing or Wolf showing is located approximately 900 m east of IDEAL 1, in a small creek (Wolf Creek) which drains eastward into Wolf Lake at a point 800 m SE of the NW end of the lake. The showings occur between 640 and 685 m upstream from the Royston-Duncan Bay logging main in central Wolf claim.

The showings were first described by Hurst (1927) as occurring in a brecciated andesite zone 2 to 12 feet in width, striking approximately 062° and dipping steeply southeast. The zone contains lenses and veins of calcite up to 6 feet wide which in turn contain lenses of realgar up to 4 feet long and 9 inches wide. Veinlets of arsenopyrite are found in the brecciated wallrock and in andesitic fragments within the calcite veins.

A visit to the showings by the author in 1987 indicates that the showings have changed substantially due to shifts in stream course. The current exposures show a conjugate set of steeply-dipping calcite-filled fractures at 080° and 045° along intersecting normal faults which juxtapose relatively fresh sulphide-bearing andesite on the north side with a buff-coloured siliceous fine-grained rock with magnetite layers to the south which has been interpreted by various workers as a bleached silicified basalt or a siltstone. The proximity of this showing to the Cretaceous unconformity is demonstrated by outliers of conglomerate which occur within 100 m of the showing. Current exposures show only minor amounts of realgar, indicating that such lenses of mineralization are erratically distributed throughout the structure.

G) PROPERTY GEOLOGY AND MINERALIZATION

Geological mapping on the property in 1988 was conducted by A. Weston, and consisted of reconnaissance-scale mapping along creeks and on grid lines, and examination of all showings and areas of specific interest identified in previous work. The results of this work are summarized in Weston's geological report as Appendix I and in Plans 1 to 7 (Volume II).

The oldest unit on the property is the Triassic Karmutsen Formation consisting of porphyritic basalt and andesite, andesitic lapilli tuff and hypabyssal gabbro, based on detailed thin section study. In outcrop, the volcanics are predominantly pillowed, or pillow breccia mixed with hyaloclastite, with lesser amounts of massive flow rocks being recognized. This would imply, based on Muller and Carson's (1969) classification, that the property is predominantly underlain by lower Karmutsen, which is dominated by submarine pillow flows. The absence of Quatsino limestone, which overlies the Karmutsen elsewhere, would also indicate that the upper Karmutsen has been removed, at least in part, by erosion.

The regional metamorphic grade of the volcanic rocks on the property appears to be zeolite grade or lower greenschist, based on the presence of zeolites in amygdules and on chloritization of mafics; however, large areas have been affected by contact metamorphism and metasomatism related to Tertiary intrusive activity. In the area of IDEAL 7, northwest of the old tailings pond, samples of basalt and andesite show replacement patches of plagioclase, actinolite, secondary biotite, quartz veining, ankerite, pyrrhotite, chalcopyrite, pyrite, and k-feldspar. A detailed paragenetic study has not been attempted, but could be considered after examination of additional samples provided by 1989 drilling.

The Karmutsen is unconformably overlain by the Cretaceous Nanaimo Group, which occupies the low ground along the east edge of the property, from the Brown's Main area in the south, along Wolf Lake, to the Helldiver Lake area in the north. On Mt. Washington, the unconformity between Karmutsen and Nanaimo rocks appears to be an important focus for mineralization, and hence the unconformity on the Dove property is considered to be an important target, particularly where it coincides with a major structural element such as a fault, or with an intrusive centre.

The Nanaimo Group comprises an assortment of epiclastic sediments ranging from coarse boulder conglomerates (Benson Fm.) to carbonate-cemented lithic sandstones, black shales and coal (Comox Fm.). These rocks appear relatively fresh and unaltered, except in proximity to several showings, where they are bleached and silicified, and on IDEAL 4 where they are strongly mineralized with iron sulphides. These occurrences are discussed later in this report.

Tertiary intrusive rocks, similar to those found on Mt. Washington, have been mapped. These are of two distinctive types - the first, porphyritic dacite, contains hornblende and feldspar phenocrysts in a fine-grained grey matrix, and occurs in smaller dikes. The second, quartz diorite, is more equigranular in character and probably represents a hypabyssal equivalent of the dacite rather than a separate intrusive episode, since the diorite occurs in larger laccoliths and plugs. A petrographic study of samples from drillcore by J. Payne (Wright, 1988b) describes both dacite porphyry and quartz diorite from the same intrusion which occurs along Dove Creek.

Tertiary intrusions located to date occur in the southern half of the property and include the large quartz diorite laccolith at Wolf Lake, which is well-exposed in a large quarry on the Royston-Duncan Bay Main and extends westward to the Paquet showing where it is in fault contact with Karmutsen basalts. A second, smaller body occurs on Dove Creek, where it was intersected in drilling and which may correlate with two small outcrops of similar material located 500 metres and 1200 metres to the south. A third body or group of bodies occurs at the junction of the Mt. Washington Road with the Tsolum Main, where 4 widely-separated outcrops of white, equigranular quartz diorite and dacite porphyry occur within an area of 1 sq. km. with no evidence of other intervening rock types. Wall rocks in this area show evidence of hornfelsing, silicification and enrichment of sulphides. A fourth, poorly exposed, body occurs at the western edge of IDEAL 7, and is unique in having a small body of fluidized contact breccia along its western margin. This breccia appears to be of the same general type as the Murex Breccia, consisting of subrounded volcanic and intrusive clasts in a fine-grained comminuted rock matrix.

A study of airphotos of the property shows a large number of lineaments, most of which occupy drift-filled valleys and cannot be verified by surface mapping. Many did, however, show up as linear features in the airborne survey. Of the linears that can be seen in outcrop, many do not show clear evidence of displacement, and may only be joints. These features typically consist of a 1 to 5-metre carbonate alteration zone in which the basalt (all such features to date are found in the Karmutsen) is wholly or partially altered to a mixture of ankerite and calcite which weathers a distinctive beige colour. Near the centre of these features is commonly found a more or less continuous planar fracture with calcite and/or quartz filling, often associated with breccia fragments of altered wallrock. This breccia could be interpreted as tectonic, due to fault motion along the fracture, or as hydrofracturing, due to excessive fluid pressures. An example of this type of structure occurs in the headwaters of Rossiter Creek, in the northwest corner of IDEAL 6. This feature, striking NW/SE and dipping shallowly northward can be traced on airphotos over a distance of 4 km. Similar structures on Rossiter Creek and also on Regan Creek appear to parallel this feature, and could represent a series of joints, or of stacked thrusts, if translation can be demonstrated.

Mineralization on the Dove Property consists of numerous sulphide exposures over a large area, but concentrated in the vicinity of the magnetic anomaly north of the old tailings pond. These occurrences, consisting of pyrite, pyrrhotite and traces of chalcopyrite in quartz veinlets in Karmutsen volcanics, are too numerous to discuss in any detail, but the better examples are plotted on the geological maps (Volume II - Plan 1a, b, c).

Showings containing anomalous values for Au, Ag and/or As are of particular significance. These include, from south to north:

a) McDonald Creek Showing
b) Paquet Creek Realgar (Paquet) Showing
c) No. 3 Creek Showing
d) Upper Murex Creek Showings
e) Lower Murex Creek (Murex) Showing
f) McKay Creek Showing
g) Regan Creek Showing

a) **McDonald Creek Showing.**

McDonald Creek is a small intermittent stream draining eastward from the Karmutsen basalts along the west edge of IDEAL 8, about 2 km SSE of Anderson Lake. The showing (Appendix I - Fig. 8) consists of a 4-5 cm quartz, pyrite, chalcopyrite vein striking NS in basalt, the attitude apparently being controlled by subvertical joints. Values up to 0.20 oz Au/T, 6.53 oz Ag/T,356 ppm Bi, 2350 ppm Sb, 7150 ppm As, 0.3% Zn and 1.9% Cu have been found in grab samples along this structure. A sooty black fault gouge zone nearby, as well as a flat-lying breccia zone and other narrow quartz-carbonate veins contain anomalous values in Au, Ag, Cu, Zn, As, Sb and other elements. This showing is enhanced by its proximity to the prominent north-south lineament, about 200 m to the east, which is drift-covered. The numerous gold-bearing veinlets and shears exposed along McDonald Creek could be marginal to a regional-scale structure corresponding to this lineament.

b) **Paquet Creek Realgar (Paquet) Showing.**

The informally named "Paquet" Creek rises in northwest IDEAL 2 claim and drains northeast across IDEAL 12 claim to Wolf Lake. In the creek near the north boundary of IDEAL 2, a prominent fault zone is marked by gouge and sheared rock in a seam 35 cm thick which is veined with carbonate and realgar veinlets and averages several % realgar (Appendix I - Fig. 9). This fault zone contains minor disseminated pyrite and local grey quartz lenses containing realgar (AsS). Veins of massive coarse crystalline realgar range up to 2 cm thick. This fault zone lies on the southwest contact of a large dacite porphyry intrusive against Karmutsen basalt. The fault strikes 110° and dips 55° SW. Basalt and intrusive occur on both sides of the fault in different places and a simple offset relation is not apparent. Slickensides plunge 50° south (dip slip) with a suggestion of hanging wall down. A chip sample across the 35 cm wide gougy shear zone contained 57 ppb Au, 0.6 ppm Ag, 3.61% As, 95 ppm Sb and insignificant base metals. A grab sample contained 154 ppb Au, 599 ppm Zn and 3784 ppm As. The gold content is low but definitely geochemically anomalous. A small, parallel, pyrite and realgar-bearing carbonate and quartz vein 2-5 cm thick was sampled a couple of metres in the footwall of the fault. It contained 2350 ppb Au, (0.069 oz Au/T), 18.4 ppm Ag (0.54 oz Ag/T), 0.3% Cu, 0.2% Pb, 0.8% Zn, 0.5% As and 0.5% Sb.

Veinlets of rusty-weathering carbonate and realgar are found in adjacent carbonate-altered basalt but are much more abundant in the adjacent dacite porphyry. Realgar-bearing carbonate veinlets on joints in the intrusive are found with diminishing abundance up to 100 m northeast along the creek from the fault zone. These joints show recessive-weathering alteration selvages up to 30 cm wide apparently due to clay and/or carbonate alteration. One veinlet up to 3.5 cm wide contains 80% very fine, dark grey to black, submetallic mineral resembling magnetite with quartz and carbonate. This vein contained 4.6% As, 56 ppm Sb and insignificant base and precious metals. Carbonate-realgar veins in the intrusive preferentially occur on joints which strike 095° to 100° and 140° to 150° with steep dips to the north and northeast.

c) **No. 3 Creek Showing**

The informally designated "No. 3" Creek originates west of the tailings pond and drains northward across IDEAL 7 onto IDEAL 1, where it enters Murex Creek at the south end of the Murex Lineament. About 50 metres above BR101E (Appendix I - Fig. 10) an outcrop of massive diabase and basalt contains at least 5 quartz veinlets with coarse patches of pyrite, 2 containing disseminated molybdenite (MoS_2) and patches of realgar. The best-mineralized and strongest structure strikes 045° and dips 65-80°N and varies in thickness from 10 to 30 cm. The showing is unique in its association of realgar with quartz and molybdenite.

d) **Upper Murex Creek Showing**

The area of the junction of Murex Creek with No. 3 Creek contains a remarkable number and variety of showings, many associated with a hornblende-porphyritic dacite dike which parallels the upper portion of Murex Creek (Appendix I - Fig. 11, 12). At 155 m. above the junction, pillow breccias contain disseminated patches of bornite, chalcopyrite, and actinolite in minor amounts. At 286 m., a 25-cm wide sulphide showing containing 50% massive pyrrhotite and chalcopyrite veins with 50% fine-grained basalt screens, with an attitude of 060/vert. A second similar sulphide vein at 296 m., separated from the first by the dacite dike, has an attitude 060/65N. This bearing coincides with the Murex Fault structure.

Further upstream, the creek follows a straight course at 040° along a second fracture zone. Branching off this zone, over a distance of some 100 metres are several calcite-realgar veinlets and quartz-pyrite veinlets. At 532 m., a fault crosses the creek at 060/80S, with a right lateral displacement of about 15 metres, based on the offset of the dacite porphyry dike. This is the only place on the property where a reliable fault offset can be demonstrated.

e) **Lower Murex Creek (Murex) Showing**

On IDEAL 9 claim, float of pyrite and sphalerite-rich drusy vein quartz was found in Murex Creek about 200 m above its confluence with

McKay Creek (Appendix I - Fig. 13). This flat boulder 25 cm across contained 4.347 oz Au/T and 2.7 oz Ag/T. A flat-lying sulphide-poor quartz vein is exposed in bedrock about 50 m upstream from the float sample. This vein is 1 to 4 cm thick and a chip sample contained 0.26 oz Au/T, 0.73 oz Ag/T, 0.05% Cu, 0.82% Pb, 1.18% Zn, 0.39% As. This very narrow vein appears to lie virtually at the unconformity between the Karmutsen and Comox Formations. It may not be the specific source of the more sulfide rich float as it is exposed in the creek bed and only hanging wall basalt conglomerate can be seen.

In 1987, a vertical drillhole located 20 m west of the showing intersected a 40 cm interval of lost core, from which a 2.5 cm thick sample of vein material graded 0.434 oz Au/T, in a bleached, chloritic volcanic breccia close to the contact with conglomerate.

f) **McKay Creek Showing**

Two veins of realgar and stibnite (?) bearing calcite occur within an ankeritic altered shear zone cutting basalt pillow breccia in the bed of McKay Creek in east central IDEAL 5 (Vol. II - Plan 6). Both the veins and shear zone are oriented $105^{o}/70^{o}$ SW. The rusty weathering carbonate alteration zone is exposed over a 5 m thickness and contains two parallel veins separated by 2.7 m of altered basalt. The south calcite vein is 70 cm thick and contains patchy and disseminated realgar and rare patches of a mineral resembling very fine magnetite (?). The northern 7 cm of this vein contains 3-4% fine stibnite (?). A chip sample over the 70 cm thickness contained 2924 ppm As and 14539 ppm Sb with insignificant precious and base metals. The northerly calcite vein is 18 cm thick and contains minor to 2% thin stringers of arsenopyrite, minor pyrite and minor disseminated realgar crystals up to 8 mm long. A chip sample over this 18 cm vein contained 1156 ppm As and 53 ppm Sb with insignificant base and precious metals. The extremely high Sb content of the 70 cm thick vein indicates the presence of a discrete Sb-bearing mineral, possibly stibnite. The occurrence demonstrates epithermal mineralization controlled along a steep roughly east-west, fault.

g) **Regan Creek Showing**

On Regan Creek, which drains northwestward into Regan Lake, in the southwest corner of HARMONY 7, a northeasterly dipping low angle thrust fault is exposed intermittently (Appendix I - Fig. 17). The fault, in Karmutsen basalts has produced a 1 to 3 m-thick buff weathering carbonate alteration zone around a narrow lensoid quartz breccia zone containing a fine-grained grey sulphide. Similar showings occur between 500 and 900 m above the Rossiter Main crossing. High-grade float boulders in the creek, containing coarsely disseminated galena and sphalerite in a quartz breccia matrix, are believed to come from the same structure. A sample of the in situ breccia material from 717 m upstream contained 233.0 ppm Ag (6.8 oz/T) and 43 ppb Au over approximately 20 cm. Float samples contained up to 19.8 oz Ag/T, 0.04 oz Au/T, 5.3% Pb and 4.9% Zn.

This showing, which is poorly exposed in an incised creek gulley, would not be amenable to trenching, but should be evaluated by geophysics followed by diamond drilling.

In addition to these showings, several interesting float occurrences have been found, most notably...

Arsenopyrite Cobble

Prospecting in 1988 by J. Paquet located a fist-sized cobble of massive weathered arsenopyrite in the area east of the old tailings pond and along strike from the Paquet Creek showing. This sample assayed 0.88 oz Au/ton, with 3660 ppm Pb, 766 ppm Sb and 14.3 ppm Ag. Efforts to locate the source of the cobble, by prospecting and boulder tracing were unsuccessful, but it is believed that the source is local, based on a coincident As soil anomaly and moderate VLF-EM conductor at this same location. As overburden appears to be quite shallow in this area, trenching will be undertaken in 1989, followed by diamond drilling if warranted.

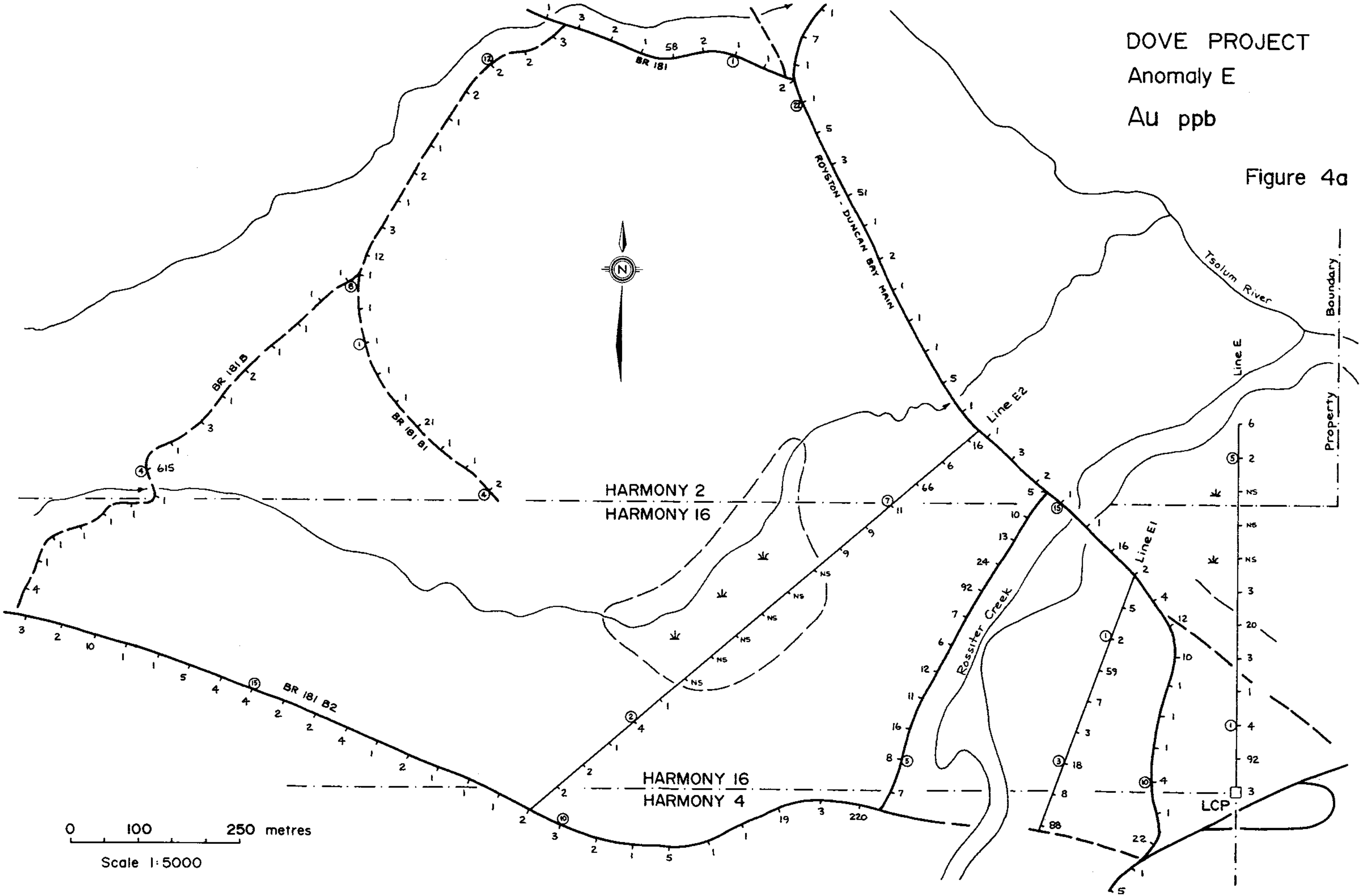
H. GEOCHEMISTRY

A major part of the field program in 1988 was devoted to grid soil geochemistry, in an effort to provide uniform coverage and a sharper focus in areas outlined by the reconnaissance sampling along roads in 1987. Samples of undisturbed "B" horizon soils were collected at 25 m intervals along grid lines spaced from 100 to 200 m apart, and were analyzed by the ICP method for 30 major and trace elements. In addition, Au was analyzed by atomic absorption because of the greater sensitivity of this method. A total of 1677 samples were collected and processed in 1988. These results are tabulated in Appendix II. A geostatistical study of these data is presently underway, and will be reported on at a later date. In the absence of detailed population statistics, it has been found than an empirical approach to anomalies is quite effective - values can be divided by inspection into background, moderately anomalous and highly anomalous ranges based on the coherence of clusterings of high values. It should be noted that a straight statistical approach to thresholds would be suspect anyway, since a bias exists in the data by virtue of the fact that samples are not truly random, but are heavily weighted into areas known to be anomalous since they contain showings, and high values based on prior sampling in 1987.

Based on this approach, the following ranges are assigned for descriptive purposes:

Element:	Au	Ag	As	Sb	Pb	Zn	Cu	Mo
Unit:	ppb	ppm	ppm	ppm	ppm	ppm	ppm	ppm
Background:	1-5	0.1-0.3	10-15	2-5	10-20	25-75	25-75	1-2
Thresholds:								
-Moderately Anomalous:								
	10	0.6	30	10	30	150	150	5
-Highly Anomalous:								
	100	2.0	100	30	?	300	300	10

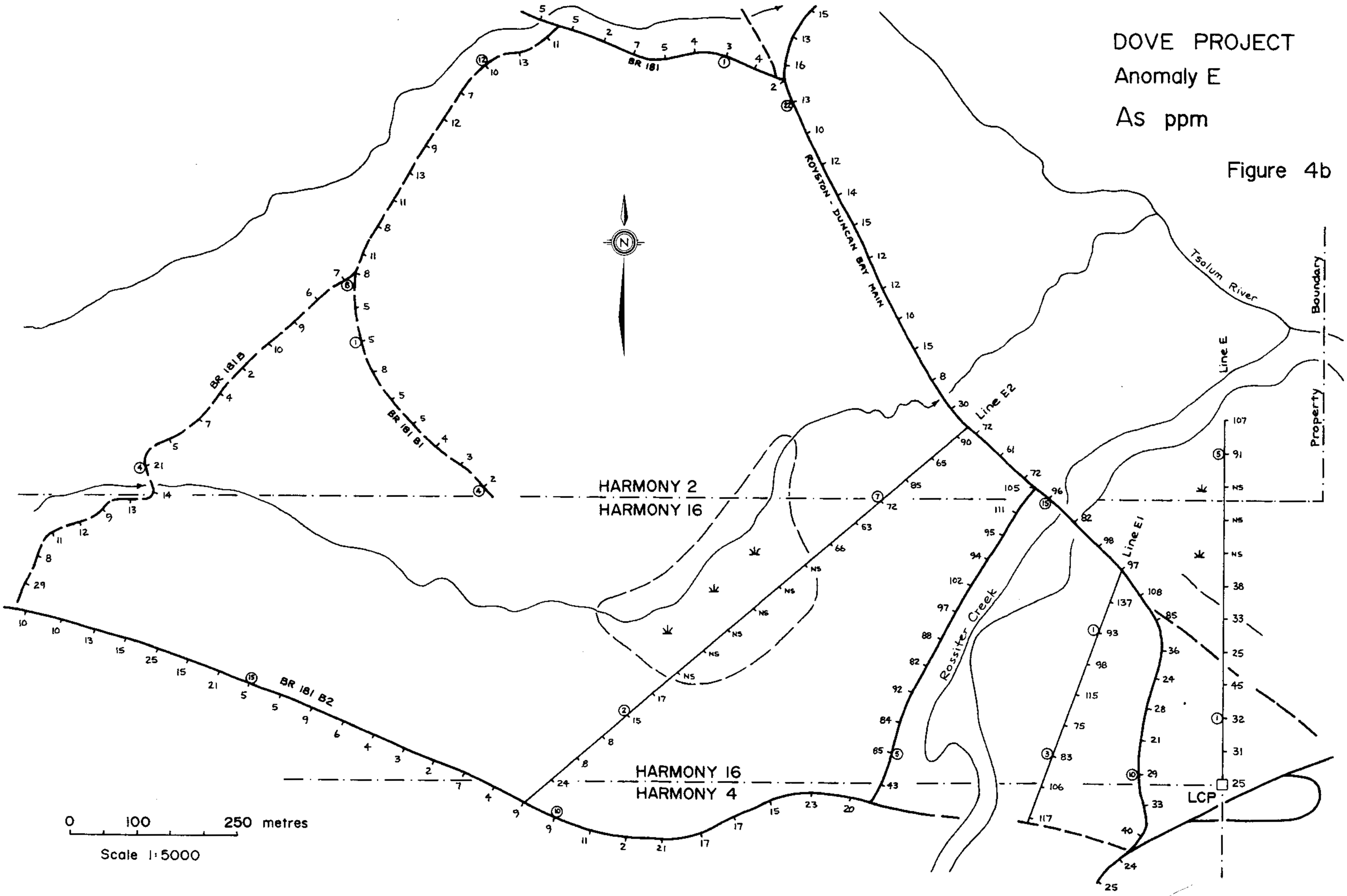
Due to the broad spacing of sample stations, which is 25 to 50 metres on lines 100 to 200 metres apart, relative to the intrinsic soil anomaly size, the data on both regional and grid scales is not considered to be contourable. This was demonstrated in 1987 by detailed fill-in surveys in which a line of 10 anomalous to highly anomalous samples at 50 metre spacing was resampled at 5 metre spacing. The intervening samples ranged from background to highly anomalous, indicating that the original 10 samples did not define a contourable, coherent anomaly, but, in fact, an area of anomalous values 500 metres wide or cluster of smaller anomalies which could not be resolved due to insufficient sampling. This unfortunate state of affairs is dictated by the enormous area of anomalous soil geochemistry on the property - sampling all anomalous areas at a sufficient density (5 m?) to define contourable soil anomalies would be prohibitively time consuming and expensive. Instead, the approach taken is to outline areas of anomalous values and to use other methods such as VLF-EM, IP, and geology, to define workable targets.



DOVE PROJECT
Anomaly E
Au ppb
Figure 4a
BR 181
BR 181 B
BR 181 B1
BR 181 B2
ROYSTON - DUNCAN BAY MAIN
Line E2
Line E1
Line E
Tsolum River
Rossiter Creek
Property Boundary
HARMONY 2
HARMONY 16
HARMONY 16
HARMONY 4
LCP
0 100 250 metres
Scale 1:5000

DOVE PROJECT
Anomaly E
As ppm

Figure 4b



The results can be divided into a number of areas, as follows.

Anomaly E

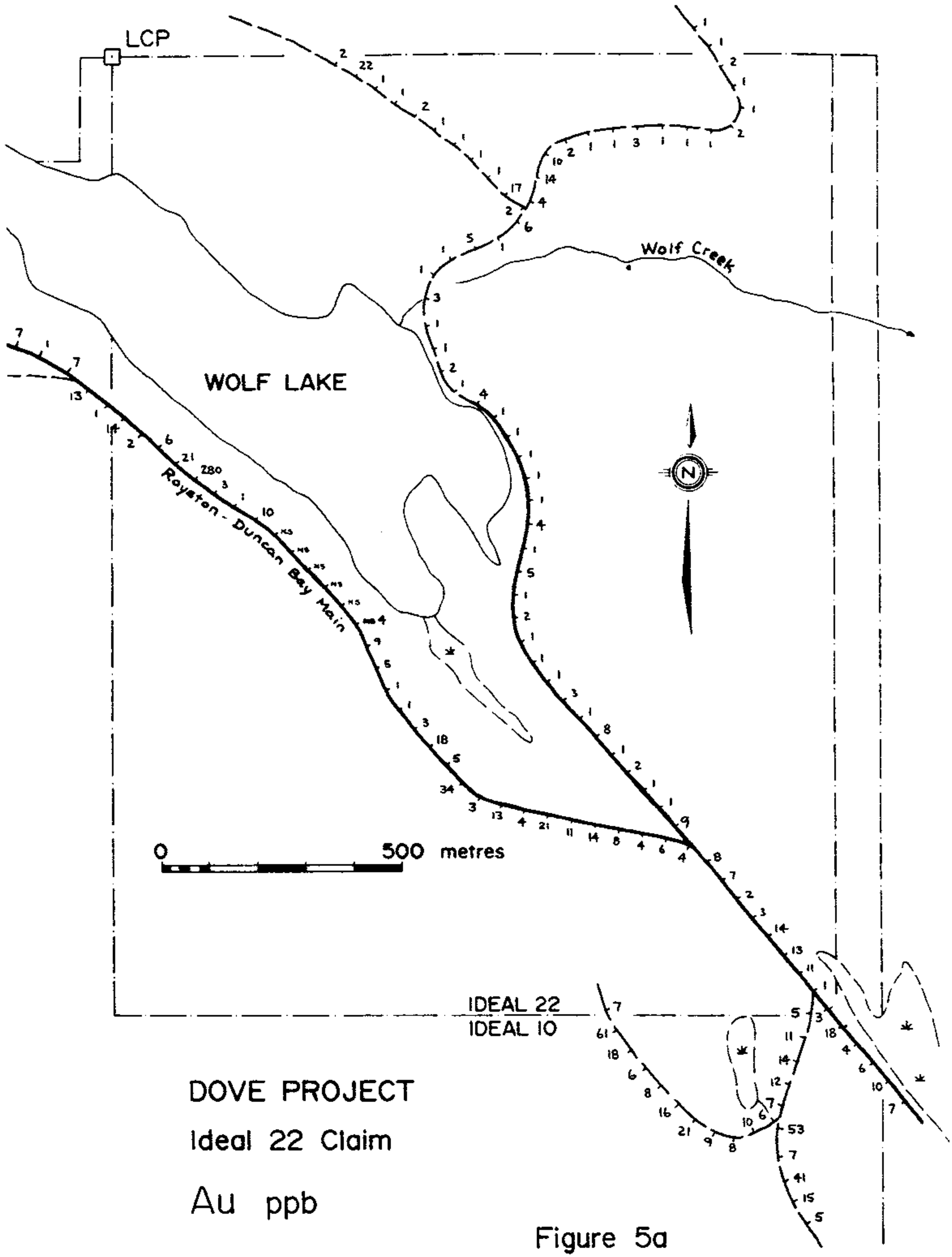
In 1987 high As and Au values, up to 111 ppm and 220 ppb respectively were found in the vicinity of the Rossiter Creek bridge on the Royston-Duncan Bay Main on HARMONY 16. The anomaly was followed up in 1988 by additional roadside samples and by 3 lines run through the bush, for a total of 63 samples. The results (Fig. 4a, 4b) show scattered high values, up to 137 ppm As and 220 ppb Au, but no clear concentration of values. Geological mapping in this area determined that it is underlain by black shales and coal measures of the Comox Fm. with a thick blanket of glacial till. The anomaly could be attributed to a placer in the till, derived from upstream on Mt. Washington, or to organic enrichment in the coal-bearing shales.

IDEAL 22

The IDEAL 22 claim was added to the Dove Property in June, 1988 and reconnaissance soil geochemistry was conducted along all accessible roads in the area. The results (Fig. 5a, 5b) show fairly uniform As values, up to 90 ppm, with erratic Au values from 1 ppb up to 280 ppb at a point on the Royston-Duncan Bay Main. Plotting these results on the regional geochemical map (Volume II, Plan 2a, b) indicates that this area is on the northeast flank of the broad anomaly extending 7 km from the Murex Breccia area, SE to the eastern edge of the property, with values greater than 10 ppb Au and 100 ppm As. No significant anomalies, with the possible exception of the isolated 280 ppb Au value, are seen in the current results.

H Grid Test Line

A single east-west test line on a proposed grid to cover the Karmutsen/Nanaimo unconformity was run along the north edge of HARMONY 1 and 2. The grid was not completed due to numerous swamps, rivers and other

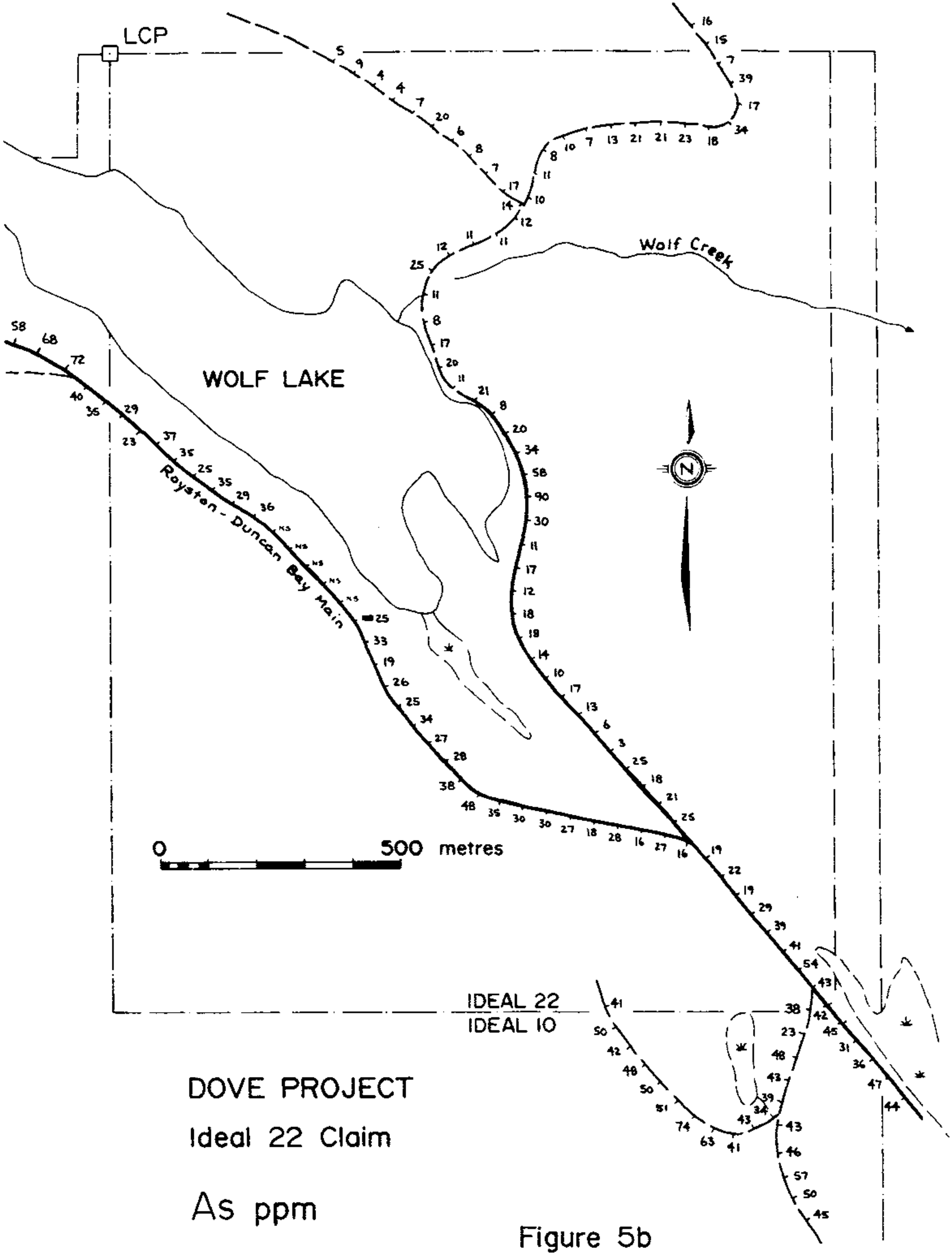


DOVE PROJECT

Ideal 22 Claim

Au ppb

Figure 5a



DOVE PROJECT

Ideal 22 Claim

As ppm

Figure 5b

obstacles, and to higher priorities in other areas. The results (Vol. II, Plan 3a, 3b) show uniformly low As values and erratic Au values up to 21 ppb. The projected unconformity did not show a geochemical signature, as anticipated.

NS Grid

The NS Grid was located to cover Anomalies A and B, and the NS lineament which extends along the western side of IDEAL 8. A total of 524 samples were collected, and these, together with previous data are shown on Plans 8a, b, c and d (Volume II).

Gold values (Plan 8a) greater than 10 ppb are widely-scattered, but show a weak clustering in the area west of the NS lineament (at approx. 200W on the NS Grid) between lines 6N and 20N. A second broad cluster extends southeastward from here toward 0N, 2+00E, ie. Anomaly A (see Vol. II, Plans 2a, 2b). This second cluster underlain by Nanaimo sediments could be due to glacial dispersion, but the first cluster, underlain by Karmutsen volcanics, and centred around the McDonald Showing appears significant. Isolated high values up to 480 ppb are found in this area.

Silver values (Plan 8a) greater than 0.6 ppm show a similar, but better-defined, pattern to gold, with strong clustering around the McDonald Showing area, west of the NS lineament, and high silver values up to 4.7 ppm along the west side of the small unnamed lake south of Weston Lake. Other isolated moderate values elsewhere on the grid would appear to have little significance at this time.

Arsenic values (Plan 8b) over 100 ppm show a very strong clustering around 250E on lines 0N and 2N, ie. Anomaly A, with a suggestion that these values trend northwestward to the McDonald showing area. Values up to 3106 ppm occur along this trend.

Antimony values (Plan 8b) over 10 ppm show a distinct clustering similar to silver, with the highest values, up to 252 ppm, occurring along the west side of the NS lineament, over the Karmutsen basalts. This is consistent with the intersecting of Sb-rich quartz veinlets at the north end of this area, near Dove Creek, in 1987 drilling.

Lead values (Plan 8c) are widely scattered and show only weak evidence of association with other elements. About half of the weakly anomalous values, over 30 ppm, lie in the vicinity of the McDonald Showing. Galena has not been seen in any of the showings or float samples from the property, so it is perhaps not surprising that Pb values are generally low.

Zinc values (Plan 8c) show a distribution similar to arsenic, with a clustering of values west of the NS lineament, extending southeastward to Anomaly A. The highest values, over 200 ppm, form tight clusters around the McDonald showing (which has 0.3% Zn) and around Anomaly A.

Copper values (Plan 8d) are similar to zinc and arsenic, with the highest values, up to 600 ppm, located in a tight cluster around the McDonald Showing.

Molybdenum values (Plan 8d) are generally very low, but values of 10 and 25 ppm were found in samples along the road below the McDonald Showing - an area also showing anomalous Au, Ag, As, Sb, Pb, Zn and Cu values. More work is clearly warranted in this area, corresponding to grid coordinates 14N to 15N/3+00W.

Additional fill-in lines, at 50 m spacing, should be run between 10N and 18N, from the baseline westward. These data would help to further define the anomalous soil geochemistry which, in conjunction with VLF-EM, IP, and geological data, will produce drill targets for further testing.

Paquet Grid

The Paquet Grid, which is that portion of the Main Grid surrounding the Paquet Showing, consists of 25 m samples on lines spaced 100 m apart, for a total of 151 new samples in addition to the approx. 250 samples in this area from 1987 work (Vol. II, Plans 9a, b, c, d)

Gold values (Plan 9a) greater than 10 ppb appear to be almost randomly scattered over the grid and do not indicate any clearly anomalous areas. The highest value, 1165 ppb, does, however, correspond to an area anomalous in other elements, at the base of the slope below the Paquet Showing, at what is believed to be the Karmutsen/Nanaimo unconformity.

Silver values (Plan 9a) are generally low and randomly scattered, the highest value being 1.5 ppm, again, from the anomalous area below the Paquet Showing.

Arsenic values (Plan 9b) show a clear clustering of values in two areas, at the base of the slope below the Paquet Showing and at the north end of the grid in the general vicinity of the arsenopyrite cobble, with values up to 1492 ppm. The Paquet Showing appears to be represented by a 100 ppm 2-line anomaly at least 100 metres long.

Antimony values (Plan 9b) are generally low, with only 5 values exceeding the 10 ppm threshold - these values loosely clustered around the anomalous arsenic zone below the Paquet Showing.

Lead values (Plan 9c) are low in this portion of the property, with no values above the 30 ppm threshold.

Zinc values (Plan 9c) are widely scattered with one distinct cluster up to 210 ppm at the north end of the grid, possibly related to the arsenopyrite cobble.

Copper values (Plan 9d) are scattered throughout the grid, with values up to 263 ppm. No relation to previously described anomalies can be seen.

Molybdenum values (Plan 9d) are generally low with 4 values over 10 ppm, up to 63 ppm, all in the Paquet Creek anomaly zone.

Overall, the results show a zone distinctly anomalous in As, Au and Mo at the break in slope below the Paquet Showing, where the pre-Cretaceous unconformity occurs. This zone will be drill tested in 1989. A clustering of high As and Zn values at the north end of the grid may be related to the arsenopyrite cobble, the source of which will hopefully be determined by additional work in 1989.

McKay Grid

The McKay Grid is the western extension of the Murex Grid of 1987 into the McKay Creek Area, to cover the McKay Showing and the north flank of the regional As/Au geochem anomaly which crosses the property. The west edge of the grid was extended northwards to cover a strong airborne EM conductor located by the 1987 survey. A total of 589 samples were collected at 25 m intervals on lines at 150 m spacing. These, and approx. 150 samples from the 1987 road reconnaissance, are plotted as Plans 10a to 10d, Volume II.

Gold values (Plan 10a) range from 1 to 1030 ppb and are scattered over the grid, with a weak concentration of higher values along the southern edge of the grid, which corresponds to the regional anomaly from previous work. A second poorly-defined cluster of values occurs between 1200N and 1500N, extending from the west edge of the property eastward to the vicinity of the McKay showing at L18+50W. This trend is better defined by other elements.

Silver values (Plan 10a) range from 0.1 to 1.8 ppm and show a scattered pattern similar to gold, with clustering along the south edge of the grid and in the zone extending westward from the McKay Showing.

Arsenic values (Plan 10b) range from 3 up to 805 ppm and, as usual, show a better definition of anomalies, including the regional anomaly on the south edge of the grid, the anomalous zone extending westward from the McKay Showing and 2 parallel zones at 1800N and 2100N in the NW corner of the grid, corresponding to the airborne EM conductors. The East McKay Showing, containing 5900 ppm As, shows up as a 133 ppm soil anomaly, but the McKay Showing, with about 3800 ppm As, does not show up at all.

Antimony values (Plan 10b) are uniformly low, with only 4 samples reaching the threshold value of 10 ppm. Curiously, the McKay Showing, with 1.8% Sb, is not detected in nearby soil values, while the East McKay Showing, with 1100 ppm Sb, shows up as a weak 6 ppm anomaly against a local background of 2 ppm (the detection limit).

Lead values (Plan 10c) are uniformly low, without a single value reaching the 30 ppm threshold defined elsewhere on the property.

Zinc values (Plan 10c) are relatively low, ranging from about 10 to 269 ppm, higher values clustering west of the McKay Showing and in the NW corner of the grid, as with other elements.

Copper values (Plan 10d) range from 15 to 432 ppm with values over 150 ppm concentrated along the south edge of the grid and west of the McKay Showing. Since the entire grid is underlain by Karmutsen basalt and andesite, these variations may reflect varying degrees of alteration of the volcanics resulting in release of trace elements.

Molybdenum values (Plan 10d) range from 1 to 30 ppm with virtually all high values clustering together where L26+00 crosses the Tsolum Main. This enrichment could reflect a small unexposed intrusive centre in this area.

In summary, geochemical patterns show regional scale concentrations along the south side of the grid and west of the McKay Showing, with only As values showing sufficient continuity to trace possible underlying structures. These data will be combined with VLF-EM data in an attempt to trace possible buried mineralized structures.

Regan Grid

The Regan Grid was started in 1987 to cover the Regan Creek Showings (Appendix I, Fig. 17). In 1988, fill-in lines at 75 m spacing were completed, to provide better definition of geochemistry and geophysics, for the purpose of locating drillsites to test the Regan Creek Showings and their along strike projections. A total of 136 samples were collected - these and approx. 200 samples from 1987 are plotted on Plans 11a to d, Volume II.

Gold values (Plan 11a) range from 1 to 365 ppb and are widely scattered, showing no apparent relation to known showings.

Silver values (Plan 11a) range from 0.1 to 1.8 ppm and show a concentration at the northwest corner of the grid in the vicinity of the Regan Creek Showings.

Arsenic values (Plan 11b) range from 2 to 913 ppm and form several clusters of anomalous values, two along the south edge of the grid, two near the Rossiter Main, and one along Regan Creek, the latter being associated with the Regan Creek Showings.

Antimony values (Plan 11b) range up to 25 ppm, high values all occurring along Regan Creek.

Lead values (Plan 11c) are generally low, with the highest value, 32 ppm, located at the Regan Creek crossing of BR 112.

Zinc values (Plan 11c) range up to 191 ppm, all values over 150 ppm being located in a loose cluster around the Regan Creek Showings.

Copper values (Plan 11d), ranging from 15 to 745 ppm, show an almost random distribution of higher values, as on the other grids. A number of high values do appear to loosely cluster around the Regan Creek Showings, reflecting the copper content of this mineralization.

Molybdenum values (Plan 11d) are uniformly low, the highest value being 6 ppm. This probably reflects the apparent absence of felsic intrusions in this area.

In summary, geochemical values are generally subdued relative to the other grids, and known mineralization correlate only weakly with anomalous values. This suggests that additional, more detailed geochemistry would be of limited value in outlining unexposed mineralization. Other methods such as geophysics and diamond drilling are necessary to trace these attractive showings.

I. GEOPHYSICS

1) INDUCED POLARIZATION SURVEY

A total of 25.9 km of induced polarization survey lines were run on the Main, NS, Murex and Regan grids by Scott Geophysics Ltd., using an IPR-11 receiver and pole-dipole array. This survey was designed to detect a variety of anomalous patterns which could reflect underlying mineralization. These could include narrow resistivity highs, which could indicate a silicified zone associated with a fault structure; or moderate resistivity, high chargeability zones, indicating disseminated sulphide mineralization; or low resistivity, with low to moderate chargeability, reflecting possible massive sulphide zones. The Main grid survey completed the central portion of the grid unsurveyed in 1987 due to extremely low resistivities.

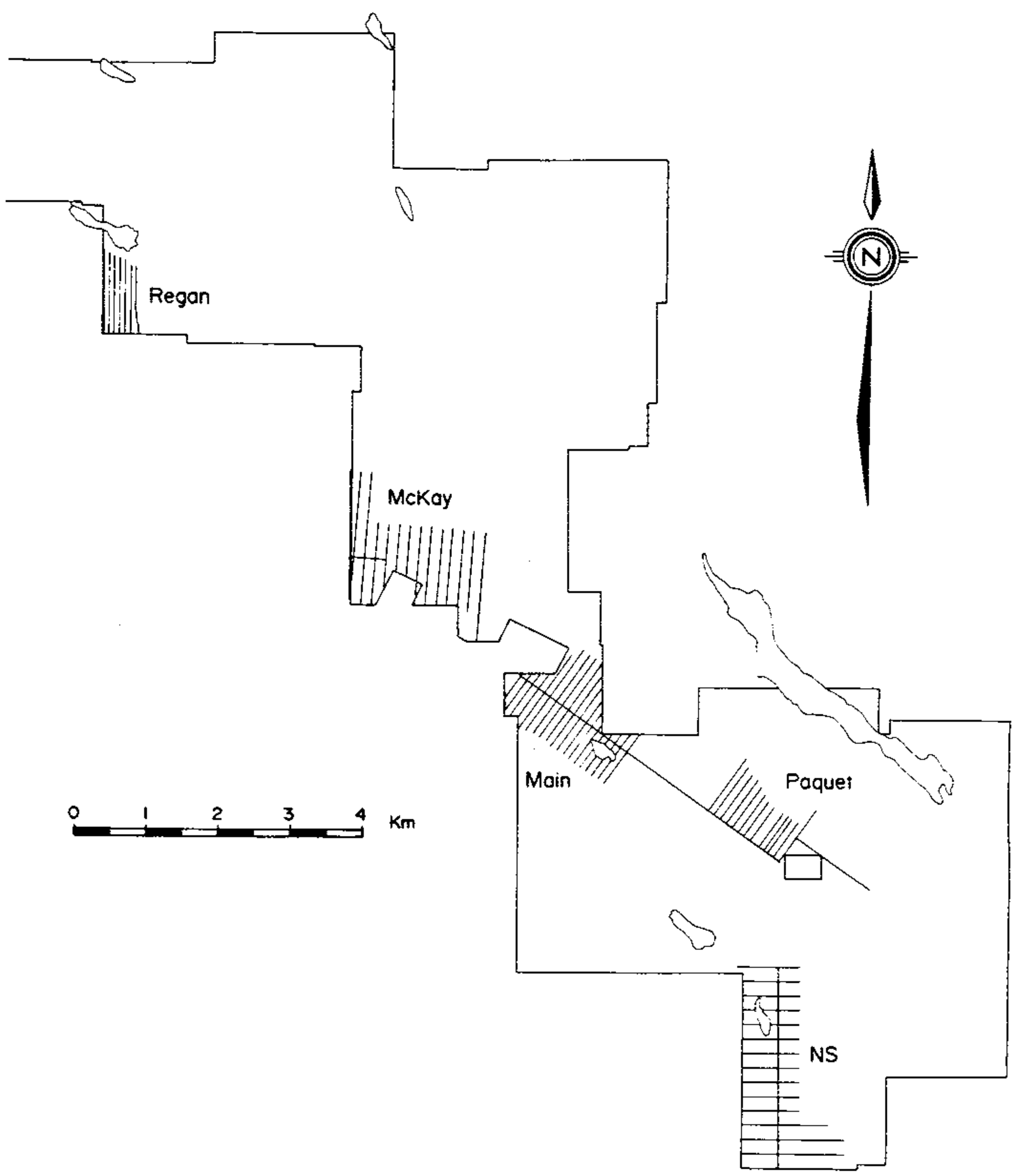


Figure 6. Geophysics - 1988 grid locations for IP, VLF surveys.

The 1988 IP data are summarized in a report, by J.M. Thornton of Scott Geophysics, which is appended to this report (Volume III, Appendix III). The following observations are based on Thornton's report, modified by the author's knowledge of geology and geochemistry, information which was not available to Scott Geophysics.

NS Grid

The NS Grid shows numerous anomalies involving very low resistivities and/or high chargeabilities. Starting at the south end of the grid, lines 0N to 6N show a NW-trending zone of low resistivities coincident with the geochemical trend, Anomaly A, previously discussed under Geochemistry. This anomaly, within the Nanaimo sediments, appears to reflect coal and shale units striking roughly in a NW-SE direction, but the possibility of a poorly-exposed mineralized structure or intrusive centre cannot be ruled out.

Further north, the anomalous soil geochemistry immediately east of the McDonald Showing is marked by a strong chargeability high, with high resistivity (IP Anomaly B). This is considered to be a priority drill target.

On the east side of Weston Lake, a strong to moderate chargeability anomaly with low resistivities, marks the contact of the dacite porphyry sill with the overlying Nanaimo sediments. Patchy geochemistry anomalies associated with this structure (in an area of heavy overburden) make it a promising drill target.

On the west side of Weston Lake, Thornton interprets a moderate chargeability zone (Anomaly A) within the Karmutsen volcanics. This could be the northward extension, at depth, of the zone near the McDonald Showing about 500 m to the south.

The remaining resistivity and/or chargeability anomalies, such as Anomalies C, D, E, F, G and H, are underlain by Nanaimo sediments and could therefore be due to barren sulphide concentrations in the shales. These are given a low priority, pending results from further work on geochem Anomaly A.

Main Grid

The results of the Main Grid survey (Volume III, Plan 7) show numerous strong anomalies in an area underlain by Nanaimo Group sediments. These anomalies do not reflect the Tertiary sills which intrude the sediments, or the major fault intersected in drilling in 1987. Due to the wide spacing of lines (200 m) and the resulting ambiguity of correlations, this is not seen as a problem, since correlations could be made which reflect this geological interpretation. In the absence of substantiating trenches or drillholes, the present interpretation is left to stand.

Of particular interest is a strong IP anomaly, J, which is 100 m along strike from the location of the Arsenopyrite cobble at approx. 2500N/200E. This zone, which correlates with geochemical values and VLF anomalies, is viewed as a good drill target, after refining by additional prospecting and boulder tracing.

Murex Creek Grid

Two adjacent test lines, L8+00W and L9+50W, were run on the Murex Creek grid to determine the viability of a larger survey at a later date. Previous VLF-EM data and numerous sulphide occurrences led to the expectation of many anomalies. This proved to be the case, as seen in the pseudosections (Volume III, Plan 8) which show a broad zone of very high chargeability, up to 126 milliseconds, with corresponding low resistivities.

On Line 8+00W, the chalcopyrite/pyrrhotite showing on Murex Creek at 4+75N, shows up as the south edge of a larger zone extending northward to about 7+00N. On Line 9+50W, a similar anomaly extends from 3+25N to

5+75N. In both cases, the south edge of the anomaly is the projection of the Murex Fault. The highest chargeabilities on the test line occur in a second anomaly to the north, inside the loop of BR 102. This area is poorly exposed but is apparently underlain by Karmutsen volcanics.

Lower Murex Test

To the test the feasibility of tracing structures under the thick overburden in the vicinity of the Lower Murex Creek Showing, a test line was run along the Rossiter Main, starting on the dry land sort and going westward one kilometre. The results show a moderate chargeability anomaly associated with Murex Creek and a strong chargeability high and corresponding resistivity high associated with McKay Creek. This latter anomaly could be a mineralized, silicified zone near the pre-Cretaceous unconformity which is located in this area, and in view of its proximity to the Lower Murex Creek Showings, should be tested by drilling.

Regan Creek Grid

Two adjacent lines on the Regan Creek Grid were run to determine whether the mineralization on Regan Creek could be detected and traced using IP. The results (Volume III, Plan 9) show a moderate chargeability anomaly on Line 0+75E at 4+00N, about 75 metres north of the showings along the creek. A resistivity high at 3+25N clearly marks the structure. A similar signature occurs at 1+50N on Line 1+50E, corresponding to the projected position of the mineralized fault zone. In this case, however, a chargeability high (Anomaly B) occurs on the south side of the projected structure, apparently indicating mineralization in the footwall.

It appears that IP can be used as a means of tracing the mineralized structures in the Regan Creek Area, and pending favourable drilling results, additional IP surveys should be conducted on this grid.

2) VLF-EM SURVEY

A ground VLF-EM Survey was conducted over the NS, Main, Paquet, McKay and Regan grids in an effort to locate and trace narrow conductive zones which could be due to faults or sulphide concentrations. The instrument used for this work was a Sabre VLF-EM receiver tuned to the transmitters at Jim Creek (Seattle) or Hawaii, depending on the anticipated orientation of the structural features under study and on the availability of a signal, Seattle being shut down on several occasions for unscheduled maintenance.

A total of 97.25 km of VLF-EM lines were run in 1988. The profiles and Fraser filter data are contained in Volume IV - Appendix IV, and the grid plans are in Volume II, Plans 12 to 16. A number of correlations can be made on the basis of geological mapping and IP profiles, where available.

On the **NS Grid** (Vol. II, Plan 12), three prominent anomalies, with Fraser Filter values greater than 30, can be seen. In the NW corner of the grid, an anomaly at 5+00W on L28N correlates with an anomaly on line 0+00 on the Dove Grid from 1987. This zone probably represents the resistivity contrast between the Tertiary intrusive sill and overlying sediments. This contact is marked by a fault which may contribute some conductivity to the anomaly. The second anomaly at the south end of lines 0+00 and 100S of the Dove Grid is also detected on 24N at about 3+75W. This zone is the clay altered unconformity and shear zone between the Nanaimo sediments and underlying Karmutsen volcanics, referred to as the Anderson Lineament in earlier reports. The third anomaly, on the east side of Weston Lake, corresponds to the Upper contact of the Tertiary sill with the Nanaimo sediments. The zone also is detected as a strong to moderate chargeability anomaly with low resistivities. This, therefore, appears to be a zone of disseminated sulphide concentration at the top contact of the Tertiary dacite porphyry sill, and will be drilled in 1989. Other weaker, discontinuous anomalies occur throughout the area - many probably result from conductive layers in the Nanaimo sediments.

On the **Paquet Grid** (Vol II, Plan 13) a moderately strong EW anomaly marks the Paquet Fault, extending from Line 200S to Line 600N. Other weaker anomalies in the area appear to parallel this structure. The strongest anomaly, however, is near the base of the slope below the Paquet showing, an area previously noted as having significant soil geochemistry anomalies. This VLF anomaly trends northwestward to BR 94A, the site of the MG Cobble, reported by Pentland and Gareau (1984) to contain arsenopyrite and chalcopyrite with 860 ppb Au and 124 ppm Ag. Diamond drilling is planned for this area in 1989.

On the **Main Grid - North** (Vol II, Plan 14), numerous moderate to strong VLF-EM anomalies can be seen. These appear to result from EW striking structures, but due to the frequency of anomalies, unequivocal correlations are not possible. The strongest anomalies should be followed up by detailed prospecting and, where warranted, trenching. It is clear that even moderate anomalies can be significant, since the 3 metre-wide fault zone intersected in drilling in 1987 on BR 101, appears as a series of moderate anomalies along the south side of the pond, extending from L33N to at least L22N. Clearly any of these anomalies could represent a significant structure and should be followed up, particularly when associated with coincident mineralized float, soil geochemistry or IP anomalies.

On the **McKay Grid** (Vol II, Plan 15) a substantial number of moderate to strong VLF-EM anomalies are found. Again, due to the high number of anomalies and relatively wide line spacing (150 m), correlations are generally not unequivocal. Several tentative correlations are shown on the plan, others could be attempted. The nature of these apparent structures is unknown - they do not show up as linears or as mappable structures based on limited outcrop in this area. Of particular interest are the strong parallel structures in the NW corner of the grid, which coincide with soil geochemistry anomalies previously described. These also showed up on the airborne survey done in 1987 (McConnell, 1988). It is interesting to note that the McKay Showing does not appear as an anomaly, but a strong anomaly is located 50 m to the south on the ridge between McKay and East McKay Creeks. Similarly, the East McKay Showing is not clearly anomalous.

On the **Regan Grid** (Vol II, Plan 16) the VLF-EM response was generally low compared to previous grids. Fill-in lines were run at 75 m spacing, in an attempt to remove the ambiguity of earlier results. The results show a reasonably good correlation between Hawaii and Seattle data, although the Hawaii signal was about an order of magnitude weaker and lead to much less distinct anomalies. The data based on the Seattle station show a strong conductor along the Regan Creek Lineament with several questionable east-west structures. The strongest response comes from the vicinity of the Regan Creek showings, which implies that the zone is 'strongest' at this point - the logical place to look for an improvement in overall grade-thickness from the showings is immediately down dip to the northeast (rather than along strike). This would best be accomplished by drilling.

In summary, the VLF-EM data on the various grids, show a large number of anomalies, many of which are probably produced by bedrock conductors, others being due to conductive overburden. Anomalies which correlate with soil geochemistry anomalies and/or induced polarization anomalies are considered prime targets for further work, including detailed prospecting, trenching (where feasible) and diamond drilling.

J) CONCLUSIONS

Since this is mainly a progress report on an ongoing program, few conclusions will be drawn at this stage; however, it is clear from the 1988 results that the Dove property presents a complex geological problem largely obscured by overburden in critical areas. Continuing work on the property is aimed at providing a focus into smaller areas where detailed geochemistry, geophysics and diamond drilling can be undertaken.

The target for this work remains the same - epithermal or mesothermal precious metal mineralization associated with dilatant zones or faults, and particularly fault intersections, which were active in the Tertiary, during emplacement of subvolcanic intrusions and diatreme breccias. Areas on the property which appear to hold the most promise for significant mineralization of this type include, from south to north, not necessarily in order of perceived importance:

Anomaly A. This feature, on the south edge of IDEAL 8, shows anomalous Arsenic soil geochemistry in an area underlain by sediments. Although believed to be due to organic enrichment in black shales, it is possible that a buried Tertiary intrusion occurs in this area, and that the arsenic anomaly represents a zone within a precious metal-bearing hydrothermal halo. IP and VLF surveys in 1988 showed several anomalies in this area, but failed to localize the anomaly further.

NS Lineament. This feature, along the west side of IDEAL 8, is largely a geological target at this point, but associated mineralization on McDonald Creek striking parallel to this buried lineament supports the model that this is a major structure along which economic mineralization could be found. The intersection of this structure with the Anderson Lineament and Dove Creek Lineament is a particularly attractive target in view of the coincident Tertiary intrusion and numerous EM and VLF-EM conductors in this area. Work on the NS grid in 1988 demonstrated two anomalous areas with coincident soil geochemistry, VLF-EM and IP anomalies, namely the sill/sediment contact east of Weston Lake, and the area between the McDonald Showing and the NS Lineament.

Paquet Showing. This impressive showing, with massive realgar mineralization in a clearly-defined large-scale fault structure, with associated gold mineralization in footwall veinlets, is viewed as an As-rich zone along a major fault which could contain a precious metal-rich zone. The structure can be seen in both IP and VLF-EM surveys as extending at least 1 kilometre along strike, and is possibly detected by high arsenic and gold values in soils nearby. Work on the Paquet Grid in 1988 located a second area anomalous in VLF-EM and in soil geochemistry, near the base of the slope below the Paquet Showing, in an area believed to be on the unconformity between Karmutsen volcanics and Cretaceous Nanaimo Gp. sediments, possibly complicated by the large Tertiary sill/laccolith which occurs at the Paquet Showing. More detailed work in this area, including diamond drilling, is required.

Tailings Pond Area. This geologically complex area appears to be a hydrothermal system centered on a cluster of Tertiary intrusions with some associated fluidized breccias. This area is expressed in the airborne geophysics as a circular resistivity low, with values as low as 1 ohm-metre, and coincident magnetic low, around a central magnetic high with moderate resistivity values. Soil geochemistry surveys show that this area is the northwest end of a 6-kilometre-long anomaly which extends southeastward through the Paquet Showing. Numerous sulphide showings, including realgar occurrences at the No. 3 Showing, in diamond drillholes 87-1, 87-7, 87-2 and 87-3, and the Wolf Showing, all point to an active hydrothermal system in the Tertiary, with anomalous Cu, Mo, As, Au and Ag concentrations. This process, acting in an environment of intersecting fault structures and dilatant zones, as well as porous Cretaceous sediments, could well lead to an economic precious metal deposit, which is our prime target. Work completed in 1988 succeeded in locating arsenopyrite float containing 0.88 oz Au/ton and 14.3 ppm Ag in an area with VLF-EM, IP, and soil geochemistry anomalies. Additional work in 1989 will be designed to locate the bedrock source of the float by trenching and/or diamond drilling.

Murex Showing. This promising showing consists of a locally-derived float boulder of pyrite and sphalerite-rich drusy quartz grading 4.35 oz Au/T and 2.7 oz Ag/T, and mineralogically similar material in outcrop and drill intersections nearby, grading 0.43 oz Au/T and 0.9 oz Ag/T. The area, at the north end of the Murex Lineament, is covered by outwash material from Murex Creek, with thicknesses locally in excess of 25 metres, and is therefore a difficult target for geochemistry and geophysics. The best approach for tracing these gold-bearing structures is by diamond drilling. Work in 1988 consisted of an IP test line along the Rossiter Main which detected a moderate chargeability anomaly associated with the Murex Lineament and a stronger anomaly over McKay Creek nearby. The potential for meaningful results from an IP survey is therefore demonstrated, however, this remains a difficult target area due to deeply-incised topography and large creeks.

McKay Creek Realgar Showing. This occurrence of stibnite and realgar in calcite veins on a regional-scale structure striking 105°, requires additional work to assess its significance. The structure lies along the south edge of a local magnetic high and resistivity low, and is radial to the large anomaly of the tailings pond area. Work on the McKay grid in 1988 showed that this structure, although clearly a major feature of economic significance, did not produce either a distinct soil geochemistry or VLF-EM anomaly. We must therefore rely on trenching or diamond drilling to test this structure.

Also significant in this area are the strong parallel conductors with associated anomalous soil geochemistry at the NW corner of the grid. These will be further evaluated by detailed prospecting in 1989.

Regan Creek Showing. This promising showing consisting of high-grade silver-lead-zinc mineralization, both as float and in situ, appears to be a northeastward-dipping thrust fault of regional proportions. Work in 1988 on the Regan Grid indicated a VLF-EM conductor along the Regan Creek Lineament, an IP anomaly in the vicinity of the known showings, and a soil geochemistry response in the general area of the showings, but all failed to give indications of a better zone, either along strike or down dip, than the presently known narrow structures. It therefore appears that drilling down dip and along strike is the best means presently available to test for thickening of the mineralized structure.

Other Areas. In addition to the aforementioned areas, other areas which satisfy some of the exploration model criteria, but do not contain known showings, should receive additional work. These include the major lineaments on the property, such as the Wolf Lake Lineament, the Blue Grouse Lineament, the Lupus Lineament and the Lost Lake Lineament. Another potential target is the unconformity between Karmutsen and Nanaimo formations which can be traced northward from Murex Creek to Helldiver Lake. This unconformity is an important focus of mineralization on Mt. Washington to the southwest.

K) RECOMMENDATIONS

It is recommended that the Dove Project be continued in 1989, focusing on areas indicated by the work in 1987 and 1988. This work should include:

-in the area of the McDonald Showing, additional fill-in soil sampling and VLF-EM to provide better definition of targets for drilling,

-on the Murex Grid, additional fill-in soil sampling and VLF-EM at 75 m spacing, to provide clearer picture of structural trends in the area,

-around the arsenopyrite cobble, additional fill-in soil sampling and VLF-EM, along with detailed prospecting, boulder tracing and trenching in order to define a source for this interesting mineralized float,

-in the NW McKay Grid area, soil sampling and VLF-EM should be done on fill-in lines at 75 m spacing (maximum) as well as extending coverage eastward to follow the anomalies in this area. Prospecting and detailed geological mapping should be undertaken in an effort to find mineralized showings or at least float, to justify additional effort,

-due to limitations of time and personnel, the 1987 drillcore received only an adequate logging and representative sampling. It is recommended that this drillcore be re-logged in detail and that additional sampling be done prior to the 1989 drill program. To facilitate systematic logging and recovery of data, a computerized database should be considered,

-once targets have been sufficiently refined by a combination of soil geochemistry, VLF-EM, prospecting, geological mapping, boulder tracing, or any other means appropriate to the circumstances, a program of diamond drilling should be undertaken. Targets to be included, not necessarily in order of priority, are:

- -the McDonald Showing area on IDEAL 8, immediately west of the NS Lineament,
- -the sill/sediment contact east of Weston Lake on IDEAL 8, where coincident IP, VLF-EM and soil geochemistry anomalies were found,
- -the Paquet Showing and projected extensions of the Paquet Fault should be tested along strike and down dip by drilling,
- -the area below the Paquet Showing on IDEAL 12, where coincident VLF-EM and soil geochemistry anomalies occur at the pre Cretaceous unconformity,
- -the arsenopyrite cobble area, assuming a source can be located,
- -the Lower Murex Creek Showing should be tested for continuity by a series of short vertical and inclined holes,
- -the McKay Showing and parallel conductors to the northwest should be tested if justified by proposed preliminary work,
- -the Regan Creek Showings should be tested down dip to the northeast.

L) REFERENCES

Benvenuto, G. (1986), Geology and Mineralization of the Dove Property and Area Near Mount Washington, Vancouver Island, B.C. Assessment Report, 68 p.

Benvenuto, G. (1986), Geology and Mineralization of the Dove Property and Area Near Mt. Washington, Vancouver Island, B. C. Westmin Resources Limited Internal Report.

Carson, D.J.T. (1960), Geology of Mount Washington, Vancouver Island, British Columbia. Unpublished M.Sc. Thesis, Univ. of B. C., 118 p.

Carson, D.J.T. (1973), The Plutonic Rocks of Vancouver Island, British Columbia: Their Petrography, Chemistry, Age and Emplacement. G.S.C. Paper 72-44, 70 p.

Hurst, M.E. (1927), Arsenic Bearing Deposits in Canada, Geol. Surv. Can., Econ. Geol. Series #4, pp. 36-38.

McConnell, D.L. (1988), Dighem III Survey for Westmin Resources Limited, Mount Washington Area, B. C. NTS 92F/11, 14. Report by Dighem Surveys and Processing Inc.

McGuigan, P.J. (1975), Certain Breccias of Mount Washington Property, Vancouver Island. Unpublished B.Sc. Thesis, Univ. of B. C., 66 p.

Muller, J.E. and Carson, D.J.T. (1969), Geology and Mineral Deposits of the Alberni Area, British Columbia. Geol. Surv. Can. Paper 68-50.

Pentland, W.S. and Gareau, M.B. (1984), Geological and Geochemical Assessment Report for the M.G. Claim. Placer Development Ltd., Assessment Report No. 12,212, 13 p.

Peto, P. (1984), Geochemical Assessment Report on the Wolf Claim. St. James Minerals Ltd. Assessment Report 12015, 15 p.

Scott, A.R. (1987), IPR-11 Survey, Dove Project, Courtenay, B. C., Report to Westmin Resources Ltd. by Scott Geophysics Ltd.

Stevenson, W.G. (1969), Exploration Report on the Property Within C.P.O.G. Lease Agreement No. 25 (Litchie Property). Report to Mt. Washington Copper Ltd. and for D.W. Litchie and Associates; Geological Branch Open File, Victoria, 11 p.

Stevenson, W.G. (1970), Mount Washington Exploration Project, Mt. Washington Copper Ltd. Report from Geological Branch Open File, Victoria, 66 p.

Walker, R.R. (1987), Report on the Dove Property. Report for Visible Gold Inc., 29 p.

Wright, R.L. (1988a), Geological Report on the Dove Project for Visible Gold Inc., 48 p.

Wright, R.L. (1988b), 1987 Year End Report on the Dove Project, 70 p. 8 volumes.

Wright, R.L. (1989), Geological Report on the Dove Project for Visible Gold Inc. 44 p.

Appendix I

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GEOLOGICAL REPORT

on the

DOVE PROJECT

Courtenay, B.C.
Nanaimo Mining Division
NTS: 92F/11 & 92F/14
Lat: 49° 45'N
Long: 125° 13'W

for

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by

A. Weston

November 7, 1988

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LEGEND FOR GEOLOGY PLANS

Tqd	Tertiary Quartz Diorite - grey equigranular and porphyritic intrusions.
Tdp	Tertiary Dacite Porphyry - grey hornblende porphyritic subvolcanic intrusions.
KN	Cretaceous Nanaimo Group - sandstone, siltstone, shale, coal, conglomerate.
	Unconformity
TRK	Triassic Karmutsen Fm. - basalt/andesite massive flows, pillow lavas, breccias, hyaloclastite.

	Fault	↑	high
		↓	low/minor
	Geological contact.	×	float (F)

Abbreviations:

congl.	= conglomerate	B	= basalt
ss	= sandstone	a	= amygdaloidal
sst	= siltstone	h	= hyaloclastic
sh	= shale	m	= massive
ss (m)	= metasandstone	p	= porphyritic
Ank	= Ankerite	Mn	= Manganese
Bo	= Bornite	Po	= Pyrrhotite
Ca	= Calcite	Py	= Pyrite
Cp	= Chalcopyrite	Qtz	= Quartz
I	= Intrusive	v	= vein
Lm	= Limonite		

INTRODUCTION

The oldest rocks on the claim are the Triassic rocks of the Karmutsen Formation. This thick sequence of assorted volcanic rocks is predominantly massive flows and pillow lavas. Unconformably overlying these volcanic rocks is the Nanaimo Group, which consists of conglomerates, sandstones, siltstones, shale, and coal. These rocks form a monocline gently dipping to the east-northeast. Tertiary activity includes a large intrusive center (laccolith) to the northeast (Constitution Hill), with extensive quartz diorite/dacite porphyry dykes and sills peripheral to this intrusion. These Tertiary intrusions are generally considered to be the source of the various Tertiary mineral deposits.

The Quaternary saw extensive glaciation of the region, leaving a thick glacial till blanketing the property. With this extensive cover, rock exposures are generally confined to ridges (for the resistant volcanics), road cuts and deeply-incised creeks.

1. Lithology/Structure

a) Karmutsen Formation

The oldest (late Triassic) and most extensive unit on the claim group is the Karmutsen Formation. This unit consists of thick sections of massive basaltic flows, pillow basalt, pillow breccias, hyaloclastites with minor agglomerate and lapilli tuffs. This suite of rocks is generally basaltic to andesitic in composition. They are generally grey-green to dark green-black. Local variations (especially pillow lavas) include a light grey-green to a very dark green black. These rocks are porphyritic or amygdaloidal with many being both porphyritic and amygdaloidal. Phenocrysts are euhedral to subhedral plagioclase ($\pm$ minor mafics), on average several millimeters in size. Amygdules are comprised of one or more of the following: quartz, chlorite, epidote, plagioclase, calcite and various zeolites. They can reach several centimeters in diameter, with flows often displaying amygdule-rich bands. The Karmutsen rocks are consistently fine-grained to aphanitic with the groundmass dominated by chlorite. They are generally moderately magnetic with local strongly magnetic areas (i.e. Fig. 5 - Main grid west of the tailings pond), and occasional weakly to non-magnetic areas. Sulphide mineralization (i.e. pyrite, pyrrhotite) is selectively pervasive throughout the Ideal group of claims, and almost non-existent in the

Harmony group.

Structurally, this formation consists of numerous massive to pillowy flows that gently dip (5-25^{o} on average) to the east-northeast. The contacts (?) between the various flows appear to have acted as favourable paths for the Tertiary mineralizing fluids and are often the source of extensive quartz-calcite-ankerite alteration.

b) Nanaimo Group

Overlying the volcanic rocks of the Karmutsen Formation are the clastic rocks of the Nanaimo Group. These thick continental or shallow marine sediments have an age of upper Cretaceous. In order of abundance this group is comprised of various-sized conglomerates, sandstones, siltstones, shales and coal. This group rests unconformably on the Karmutsen Formation forming a gently-dipping monocline, dipping 5-25^{o} E/NE. Overall these rocks appear unmetamorphosed and little-deformed (except where local faulting has disturbed the sediments). The unconformable contact runs the length of the property (Fig. 1, 2, and 3) from the southwest corner of Ideal 8 to just east of Hell Diver Lake (Harmony 5) in the north, a distance of some 20 km. This irregular contact has numerous embayments with occasional small sedimentary outliers. The contact is extensively drift-covered and is only visible in major incised creeks (i.e. Murex Creek (Fig. 13), Tsolum River (Fig. 3)). This contact, like the 'flow boundaries' of the Karmutsen volcanics also acted as a favourable path for Tertiary mineralizing fluids (i.e. Murex Creek showing (Fig. 13)).

Conglomerates

Conglomerates are generally pebble to cobble in size, with occasional boulder to coarse boulder conglomerates. Clasts are generally well-rounded with occasional subangular sections. They are of a heterolithic nature, with clasts being predominantly assorted volcanic rocks of the underlying Karmutsen Formation. Minor amounts of intrusives, and various sedimentary clasts are also present. A basal conglomerate (regolith?) is sometimes found at the base of the Nanaimo Formation. This conglomerate is a heterolithic mixture of mainly subangular fragments of the underlying volcanics. This basal conglomerate filled paleo valleys (?) and hence, its thickness and lateral extent are quite variable. It is not always present at the contact.

Sandstones

The sandstones range in colour from a light greyish white to a dark grey to a bluish grey. They form large extensive regions of massive, homogeneous outcroppings (i.e. eastern half of Ideal 8, Fig. 4). Occasional cross-bedded sections are present (Tsolum River near Branch 182, Fig. 3). Grain size is amazingly consistent being medium-fine to medium-coarse grained, with occasional coarse-grained quartzose sandstones. The sandstones are generally fresh and unaltered except near intrusive bodies, where the individual quartz/feldspar grains are partially or completely recrystallized. In several locations recrystallization has produced a very hard, siliceous, metaquartzite (?). Other locations an incomplete (?) recrystallization has produced a saccharoidal, meta quartzo-feldspathic sandstone that is sometimes difficult to distinguish from the dacite porphyry.

Siltstones/Shales

They are a greyish brown to dark grey to black. These units are relatively thin and have limited lateral extent. They are usually found interbedded with the sandstones. They are often carbonaceous and often contain numerous small (< 5 mm) interbedded coal seams. The shales are occasionally fissile, and rarely fossiliferous, containing poorly-preserved plant remains (i.e. Dove Creek near Branch 53, Fig. 4).

Coal

Coal is a relatively minor constituent of the Nanaimo Group. It is generally seen as very small seams within the carbonaceous shales. Seams greater than several centimeters are rare, however one outcrop of shaley coal in the South Tsolum River (Fig. 3) was several meters in length.

c) Tertiary Intrusions

Quartz Diorite

Large areas of the claims flanking the south end of Constitution Hill/Wolf Lake are underlain by a large quartz diorite intrusion (Fig. 1). This major body of Tertiary age is assumed to be a laccolith or sill in the Constitution Hill area (overlying the sediments of the Nanaimo Group at that point). This quartz diorite body is typically an off-white to various shades of grey-white in colour. It is medium to medium coarse-grained, and generally weakly to non-magnetic with local variations. Some of the contact breccias have a strongly magnetic matrix and magnetite-rich selvages along some dyke contacts are relatively common (i.e. Main grid west of the tailings pond, Fig. 5). Mafics comprise 10-15% of the rock. Minor disseminated pyrite, pyrrhotite, chalcopyrite and arsenopyrite occur locally and are sometimes fracture-filling.

Quartz diorite dykes are common throughout selective areas (i.e. Ideal 4). The frequency of dykes naturally tends to increase toward intrusive centers. A small quartz diorite intrusion located in the extreme northwest corner of Ideal 4 (Fig. 1), appears to be the center for extensive dyking peripheral to this intrusion. Intrusive dykes are common throughout the Murex grid and the Main grid west of the tailings pond (Fig. 5).

Generally dykes show evidence of forceful injection into the surrounding host rocks. Contacts are generally sharp [planar (fracture/fault filling) to irregular shaped] with brecciated margins most uncommon. Occasionally, these brecciated margins show extensive, post-intrusion, multi-phase quartz veining, occasionally carrying trace amounts of pyrite, pyrrhotite and chalcopyrite.

Metamorphism of the host rocks appears to be negligible and the intrusions show little or no quench texture at contacts.

Dacite Porphyry

The dacite Porphyry is an off-white to greyish-white in colour and is fairly homogeneous throughout its extent. A typical sample is comprised of hornblende phenocrysts (< 10%) in a fine-grained matrix of quartz and plagioclase. The hornblende occurs as euhedral to subhedral prismatic phenocrysts, and ranges in size from several millimeters to 1 centimeter (average 3-5 mm). They form distinct elongate dark crystals that are generally partially or completely altered to chlorite. Minor phenocrysts of plagioclase or quartz are sometimes present. This unit sometimes has a slight saccharoidal texture in weathered surfaces and is very similar to some of the meta-sandstones. Local, very finely-disseminated pyrite is common.

Structurally the dacite porphyry may form dykes (upper Murex Creek, Fig. 11), or concordant sill-like bodies within the sediments. In several locations (i.e. Main grid L18-L22, approx. 700 W, Fig. 5), sandstone outcrops of the Nanaimo Group are found within 20-30 m of an extensive dacite porphyry outcrop. In each instance the dacite porphyry occupies the higher ground (ridge), indicating a steep vertical contact or more likely a sill-like relationship.

Other Tertiary (?) Intrusions

Other intrusive bodies include a small coarse-grained gabbroic (?) intrusion at the south end of Anderson Lake (Fig. 1). This magnetic body may be the source of a local aeromagnetic high.

Occasional fine-grained, sometimes hornblende porphyritic dykes are occasionally found. Several small, fine-grained, hornblende-porphyritic, magnetic dykes occur in the extreme south-central part of the Harmony 3 claim (Fig. 3). This area of extensive pillow-breccias is also an aeromagnetic high, which may be due in part to these dykes.

2. NS Grid

This grid is located in the western half of Ideal 8, Ideal 13 and 14, and the extreme southern part of Ideal 2 (Fig. 1). The grid is centered on a major north/south topographical depression (NS lineament (Fig. 4). The western part of the grid is underlain by volcanics of the Karmutsen Formation. These rocks range from massive flows to pillow basalt to minor hyaloclastic-pillow breccias. They form a resistant ridge running up the western edge of the grid. In contact with the volcanics are the Nanaimo Group sediments which unconformably overlie them. The contact appears to run down the NS lineament which is covered by 2 lakes and an extensive drift-filled, swampy valley.

The Nanaimo Group sediments are predominantly massive/homogenous sandstones, except in several of the incised creeks, where interbedded siltstones and shales are exposed. The basal (?) conglomerate is exposed in the extreme southwestern part of the grid. The southeastern part of the grid is predominantly a gently-dipping sandstone, whose surface has been glaciated smooth. Numerous striations indicate an easterly glacier direction (076-118°).

Located between the Karmutsen volcanics and Nanaimo sediments is an intrusive body of dacite porphory (L10+00N northward). This intrusive body appears to be located at or near the volcanic/sedimentary unconformity. South of L10+00N this body is lost in overburden and is assumed to die out. To the northwest it follows the contacts off the grid and is lost in overburden east of Anderson Lake. This intrusive body may be a concordant (?)/sill-like (?) body that pinches and swells. In the area around Branch 53D/53 the body appears to be fairly wide which may be a function of its thickness or its orientation. To the south it appears to wedge out, and to the northwest it may join with the dacite porphyry of the Main grid or be truncated by the Dove Creek fault.

A drill hole (87-5) located just north of Dove Creek (Branch 53/53B) was drilled at 220°/-45°. This hole intersected a 59 m (not true width) section of a dacite porphyry intrusion at 54.7-113.5 m. This intrusion had sheared contacts and was surrounded top and bottom by Nanaimo sediments. As a series of dacite porphyry outcrops are located to the southeast, this would tend to support a shallow-dipping, concordant, sill-like body (see cross-section, Fig. 4).

a) MacDonald Creek

The MacDonald Creek showing is located in a small creek in the extreme west/central part of the NS grid (Ideal 8 claim) (Fig. 4). The creek runs from the west (off the property) in a south-easterly direction into a prominent drift-covered north/south lineament (NS lineament) that runs up the central part of the NS grid (Fig. 8). The showing is located 150 m upstream of Branch 53E. This showing consists of a 10 m wide zone of numerous quartz-carbonate (ankerite?) veins within the host Karmutsen volcanics. These range in size from several centimeters up to 20 cm, and strike north-northwest (008-048) dipping between 80-90 W. Several of the veins are truncated by an altered, flat lying, brecciated zone containing quartz-calcite-ankerite-pyrite ± chalcopyrite.

Several other small quartz-carbonate veins and alteration zones are located at the

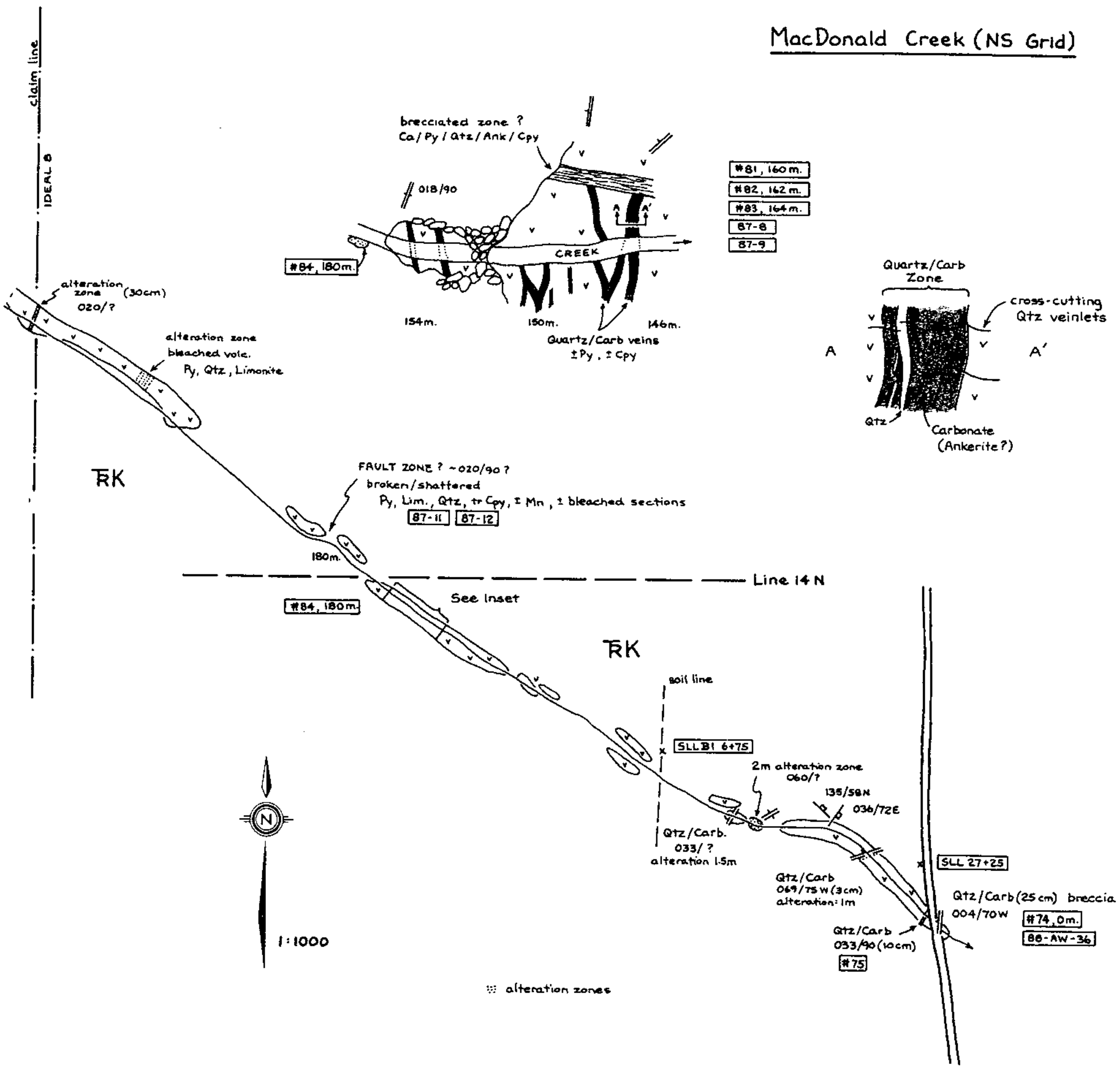

MacDonald Creek (NS Grid)
claim line
IDEAL 8
brecciated zone ?
Ca / Py / Qtz / Ank / Cpy
018/90
#81, 160 m.
#82, 162 m.
#83, 164 m.
87-8
87-9
CREEK
#84, 180m.
154m.
150m.
146m.
Quartz/Carb veins
± Py, ± Cpy
Quartz/Carb
Zone
cross-cutting
Qtz veinlets
A
A'
Qtz
Carbonate
(Ankerite ?)
alteration zone (30cm)
020/?
alteration zone
bleached volc.
Py, Qtz, Limonite
TRK
FAULT ZONE ? ~020/90 ?
broken/shattered
Py, Lim., Qtz, tr Cpy, ± Mn, ± bleached sections
87-11
87-12
180m.
Line 14 N
#84, 180m.
See Inset
TRK
soil line
SLLB1 6+75
2m alteration zone
060/?
135/58N
036/72E
Qtz/Carb.
033/ ?
alteration 1.5m
SLL 27+25
Qtz/Carb
069/75 W (3cm)
alteration: 1m
Qtz/Carb (25 cm) breccia
004/70W
#74, 0m.
86-AW-36
Qtz/Carb
033/90 (10cm)
#75
N
1:1000
alteration zones

Figure 8

lower end of the creek around Branch 53E. These veins have a similar orientation (004-069), dipping 70-90 W (28 ppb Au, .9 ppm Ag).

3. Main grid

The main grid runs in a northwest (306°)/southeast (126°) direction through the Ideal 2, 3, 4, 7 and 12 claims (Fig. 1). The extreme southeastern part of this grid (approx. L0+00S) is underlain by quartz diorite. This large intrusion (part of the Constitution Hill laccolith?) is in contact with the Karmutsen Volcanics to the northwest. The only visible contacts are located in and around Paquet Creek. At the head of Paquet Creek (Fig. 9) the intrusion is in fault contact (?) (100/55 S) or the fault cuts the contact at this point. Immediately to the north the contact is a sharp/irregular boundary that becomes a fault contact (002/80 W) to the north. Minor coarse, unmineralized, drusy quartz veining occurs around the contact at this point. To the northwest (approx. L8 N to approx. L18 N) is a largely drift-covered area, to the northwest of which are the Nanaimo Group sediments. The area between L14 N (?) and L32 N is an area predominantly sedimentary (meta-sedimentary) with at least 3 dacite porphyry intrusive bodies, that may be an extension of the NS grid - 'dacite porphyry sill (?)'. Separating the bodies is a small drift-covered valley that is part of the Pond Lineament (Paquet fault?). Drill holes 87-2 and 87-3 have shown that a major fault does traverse the valley and that the valley is underlain by flat-lying sediments. This valley has numerous brecciated intrusive (contact breccias) boulders, especially in the region bounded by L24 N, L26 N, approx. 350 W and the baseline. Several of these carried anomalous Au values (101, 320 ppb Au). To the northwest of the tailings pond (approx. L32 N), is an area underlain by a magnetite-rich basalt of the Karmutsen Formation. Extensive quartz veining and numerous quartz diorite dykes occur in this largely drift-covered region.

In the area around Br 54 B and L6 S a very small outcrop (?) of massive pyrrhotite produced an anomalous 340 ppb Au. However no other outcrops could be found in this area assumed to be underlain by quartz diorite.

a) Paquet Creek

The Paquet Creek showing (Fig. 9) is located in the extreme north-central part of

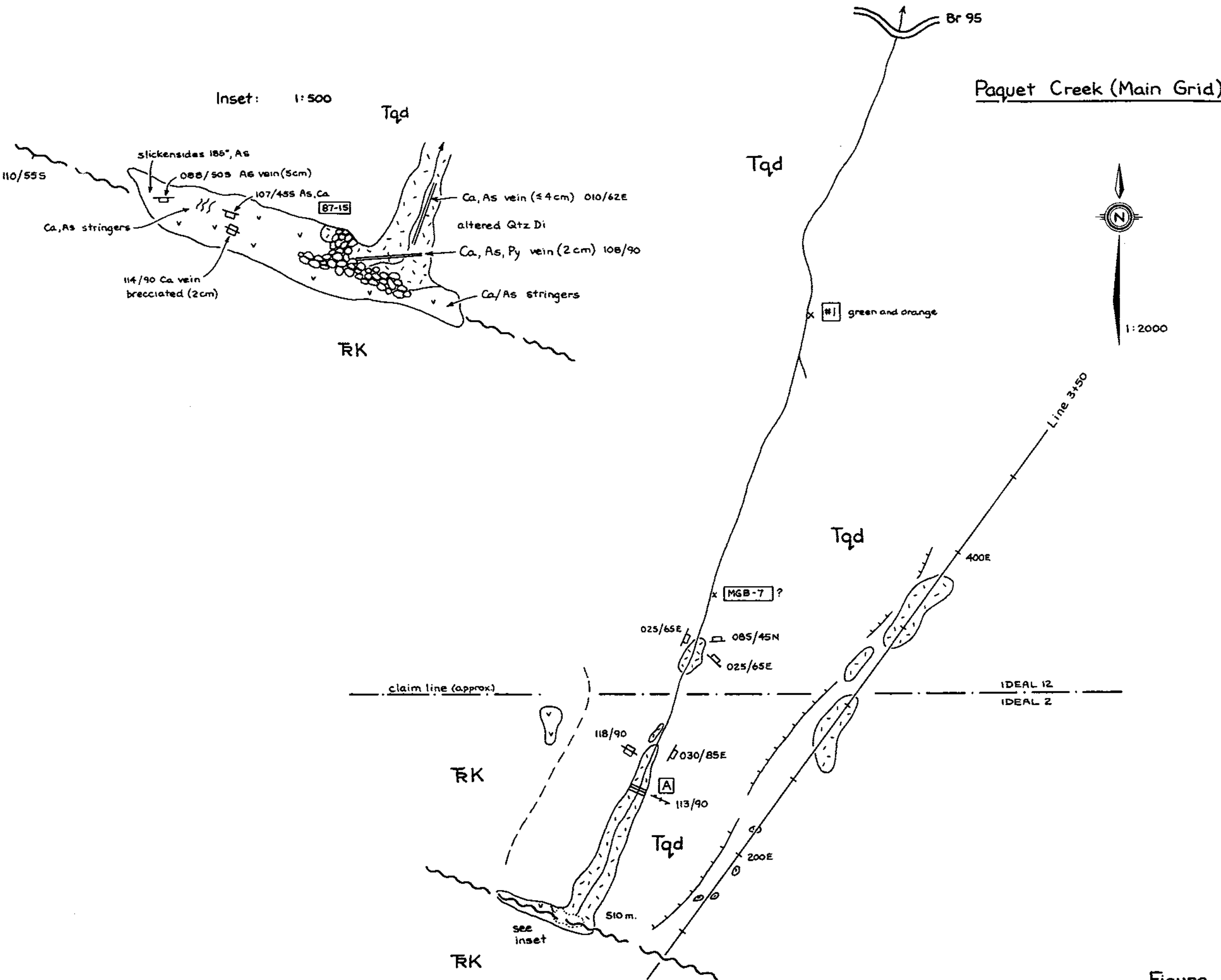

Paquet Creek (Main Grid)
Br 95
Tqd
N
1:2000
#1 green and orange
Line 3+50
400E
200E
MGB-7 ?
025/65E
085/45N
025/65E
claim line (approx.)
IDEAL 12
IDEAL 2
118/90
030/85E
A
113/90
ŦRK
510 m.
see inset
Inset: 1:500
slickensides 186°, As
110/55S
088/50S As vein (5cm)
107/45S As, Ca
87-15
Ca, As stringers
Ca, As vein (≤4cm) 010/62E
altered Qtz Di
Ca, As, Py vein (2cm) 108/90
114/90 Ca vein brecciated (2cm)
Ca/As stringers

Figure 9

No.3 Creek (Murex Grid)

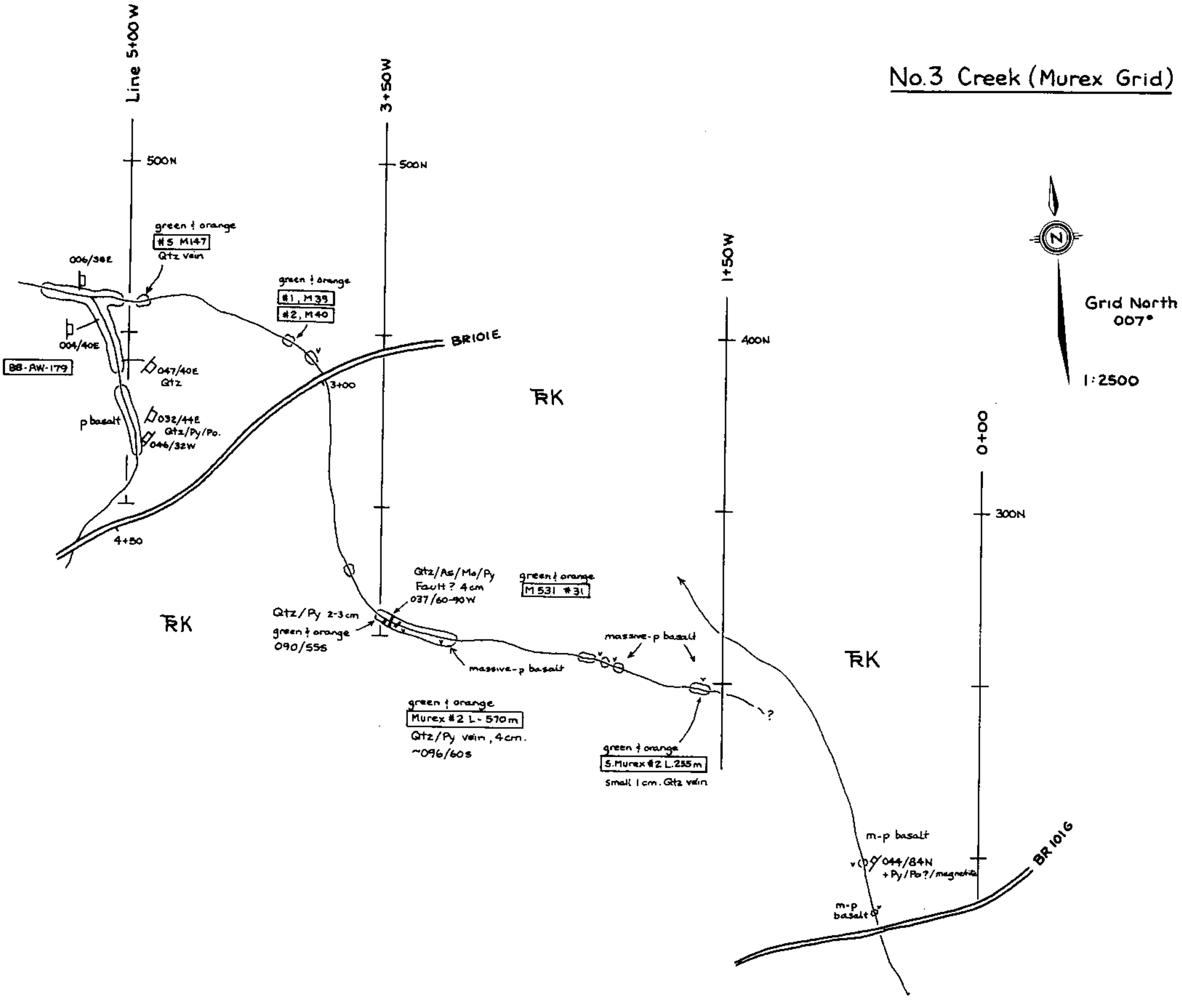


Figure 10

the Ideal 2 claim, between lines 3+50 N and 5+00N on the Main grid. The showing is within Paquet Creek at a point where the creek makes a sharp 90° turn to the west (approx. 510 m up from Wolf Main). At this point a fault/shear zone that is part of a major topographical lineament passes through the creek, offsetting its course by some 30 m. This fault (Pond Lineament) appears to run from just south of the tailings pond across road 101 through Paquet Creek and is lost to the southeast. At Paquet Creek the fault has an orientation of approx. 110/55 S. The fault appears to cut-across (or form?) the contacts between the Karmutsen volcanics to the south and the quartz diorite to the north. The hanging wall is the amygdaloidal to porphyritic rocks of the Karmutsen Formation. The footwall is also volcanic, however the quartz diorite occurs within several meters and is actually in contact (?) with the fault in places.

The fault zone is composed of a half meter wide gouge zone (recessively weathered), with a coarsely crystalline massive carbonate/realgar (orpiment) vein (approx. 1.5 cm wide) along the footwall. Numerous cargonate (ankerite?)/realgar stringers are located along the fault within both the volcanics and intrusive. Veining density and hydrothermal alteration of the intrusive decreases away from the fault diminishing after 40/50 m downstream.

4. Murex Grid (Upper Murex Creek)

The Murex grid is located in the extreme southern part of the Ideal 1 claim (Fig. 1, 5). This grid is underlain by the volcanic rocks of the Karmutsen Formation. These rocks are predominately pillow-lavas and hyaloclastite/pillow breccias in this area. Throughout this grid (increasing to the southeast?) are extensive Tertiary quartz diorite/dacite porphyry dykes, and related quartz veining. Due to an extensive cover of drift, most rock exposures are confined to road cuts and deeply-incised creeks. One of the best locations is Murex Creek (south of its junction with No. 3 creek). The upper part of this creek (Fig. 11, 12) from L6+50 south is an area containing extensive dyking, numerous small fault zones, extensive quartz veining, and sulphide mineralization. In the area between L6+50 and L8+00 (Fig. 12) a quartz diorite dyke runs down the creek for approx. 100 m with the ends obscured by overburden. The host volcanic rocks exhibit abundant disseminated pyrite ± pyrrhotite, ± chalcopyrite along its length. At least 4 massive pyrrhotite (+ minor

Upper Murex Creek (Murex Grid)

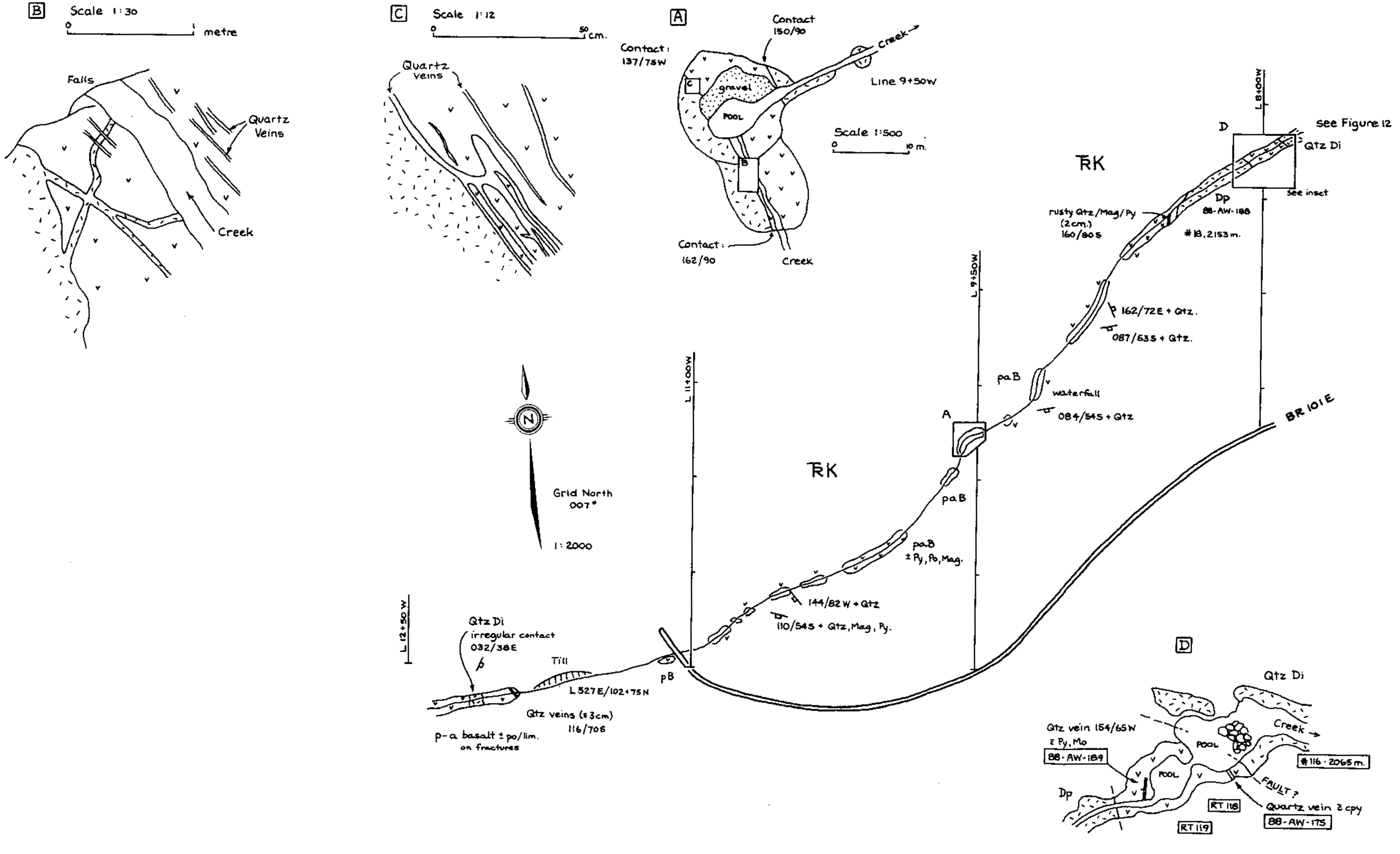


Figure 11

Upper Murex Creek (Murex Grid)

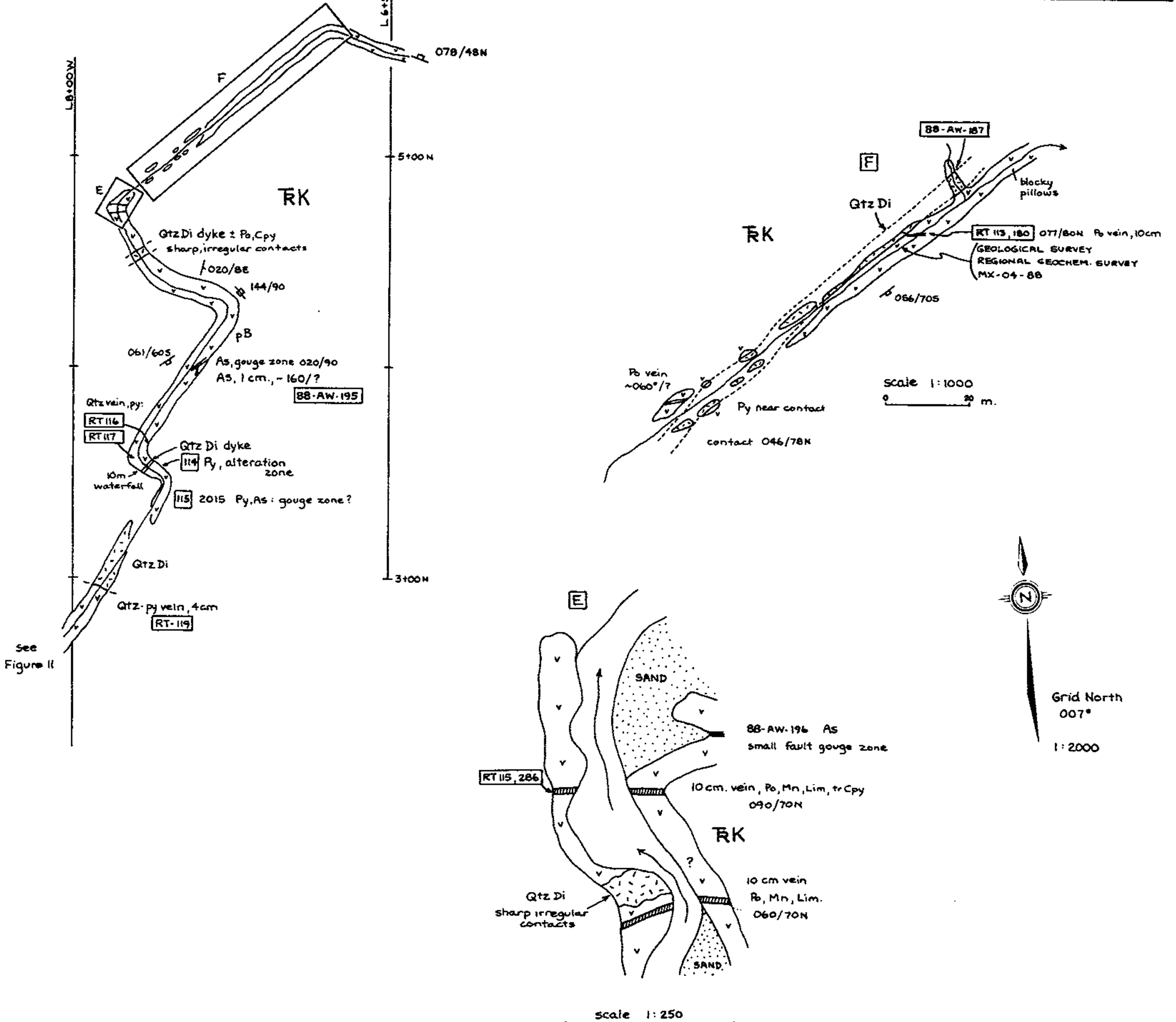


Figure 12

chalcopyrite) veins, 10 cm wide and orientated 060-090/70-80N occur along its length. Occasional small realgar/orpiment-rich fault/gouge zones and occasional massive realgar/orpiment veins (< 2 cm) occur. Quartz veining is prevalent through the upper part of the creek, often containing one or more of the following: pyrite, pyrrhotite, magnetite, realgar/orpiment, molybdenite, arsenopyrite (?).

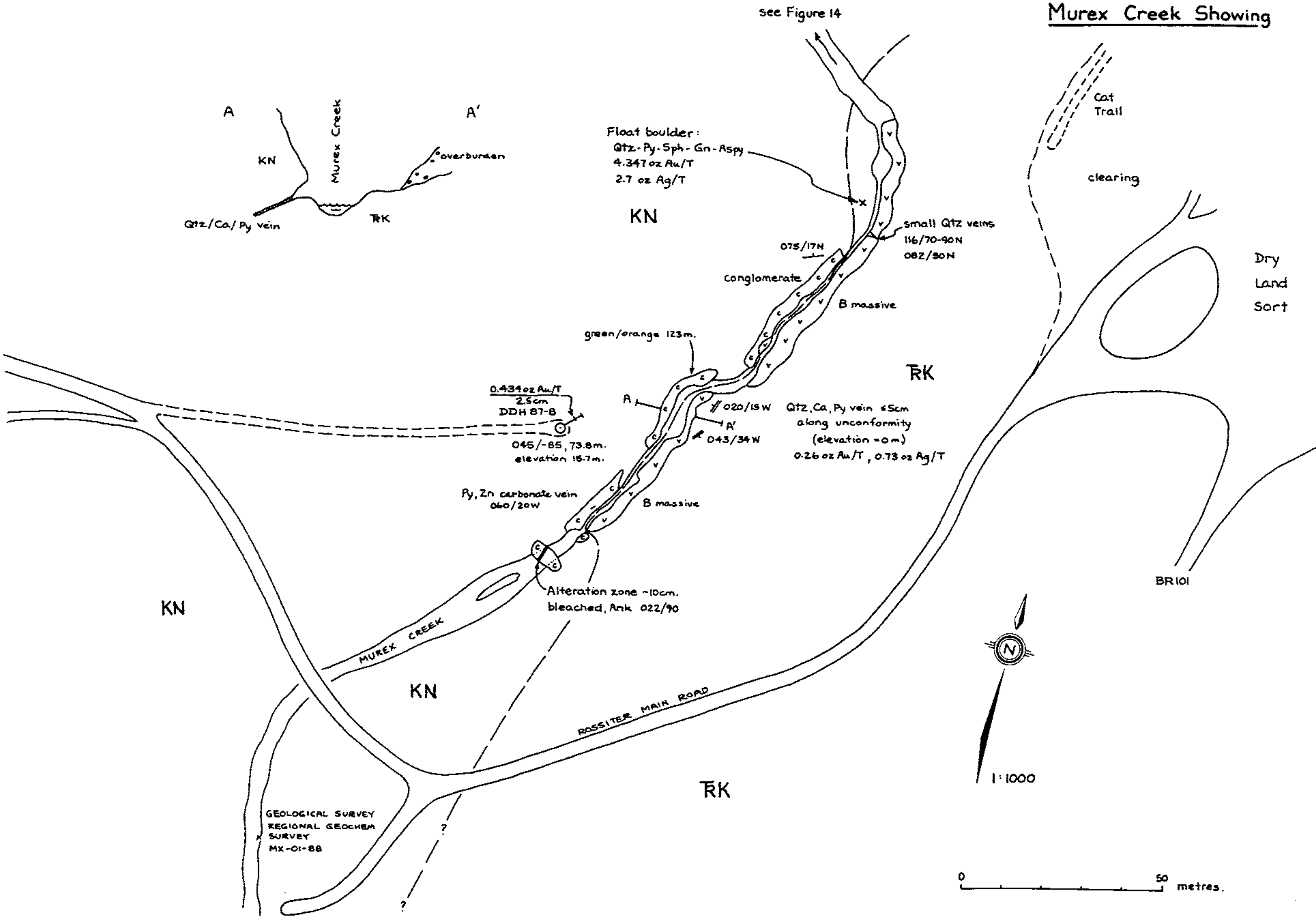
At the extreme southern edge of Ideal 1 (and Murex grid) a small creek (No. 3 Creek) (Fig. 10) runs through the end of L3+50 at 235 N. At this point the creek has exposed several narrow quartz veins. Three of the larger veins (approx. 2-4 cm wide) contain abundant pyrite, with one containing minor realgar and molybdenite. Two of these veins are orientated at 090-096/55-60 S, with the third at 037/60-90 W.

5. Lower Murex Creek Showing

The Murex Creek showing is located in the lower part of Murex Creek, 100-120 m downstream of the Rossiter Main Road, within the Ideal 9 claim (Fig. 13). This showing is a recessively-weathered quartz-calcite-pyrite ± galena ± sphalerite ± chalcopyrite vein averaging several centimeters in width. This vein is located along the unconformable contact between the overlying conglomerates of the Nanaimo Group and the underlying Karmutsen volcanics. At this point the creek runs along the contact for approx. 100 m exposing approx. 40 m of the vein. This thin vein follows the undulating paleoerosional surface of the Karmutsen volcanics, and has an orientation in the range of (020-060/(15-34) W.

6. Harmony Group

The Harmony Group of claims (Fig. 3) consists almost entirely of the Karmutsen volcanics, except for the eastern portion of Harmony 2, 4, 16, which is underlain by the Nanaimo Group sediments. The Karmutsen Formation/Nanaimo Group unconformity runs from just west of the Rossiter Creek/South Tsolum River junction northward (through Harmony 4, 16, 2) to the area just east of Harmony 5 (Hell Diver Lake). The sediments (east of the unconformity) are comprised mainly of sandstone, conglomerates, siltstone, shale and minor coal. These sediments are basically undisturbed except for local



Murex Creek Showing
see Figure 14
A
A'
Murex Creek
KN
overburden
Qtz/Ca/Py vein
TRK
Float boulder:
Qtz-Py-Sph-Gn-Aspy
4.347 oz Au/T
2.7 oz Ag/T
KN
Cat Trail
clearing
small Qtz veins
116/70-90N
082/30N
075/17N
conglomerate
B massive
Dry
Land
Sort
green/orange 123m.
TRK
0.434 oz Au/T
2.5cm
DDH 87-8
045/-85, 73.8m.
elevation 15.7m.
020/15W
043/34W
Qtz, Ca, Py vein ≤5cm
along unconformity
(elevation =0m)
0.26 oz Au/T, 0.73 oz Ag/T
Py, Zn carbonate vein
060/20W
B massive
Alteration zone ~10cm.
bleached, Ank 022/90
KN
MUREX CREEK
KN
BR101
ROSSITER MAIN ROAD
TRK
1:1000
GEOLOGICAL SURVEY
REGIONAL GEOCHEM
SURVEY
MX-01-88
0
50
metres.

Figure 13

faulting, and show no evidence of metamorphism. The general topography east of the contact is relatively flat (low relief), with an extensive drift cover. Outcrops are predominantly confined to incised creek valleys, or road cuts.

Along the Tsolum River (Fig. 3), approximately 1120 m upstream of Branch 181, the contact is exposed in a deeply-incised section of the river. At this point, conglomerates of the Nanaimo Group unconformably overlie the Karmutsen volcanics. This contact has a gentle (approx. 20° apparent) dip to the east. A small unmineralized calcite vein is located immediately between the two units, very similar to the Murex Creek showing, however assay values were low (13 ppb Au, .2 ppm Ag).

West of this contact, the Harmony claims consist entirely of the Karmutsen volcanics. These rocks are predominantly massive/homogeneous basaltic flows, with lesser amounts of hyaloclastite-pillow basalts and pillow breccias. In each instance where the massive flows and pillow lavas are found together the massive flows are stratigraphically above the pillow lavas. Whether this is a function of selective weathering or a sub-dividable unit is unknown.

As a generalization the volcanic rocks of the Harmony group are notable for: their lack of any veining (except in major fault zones); their lack of sulphide mineralization (i.e. pyrite, pyrrhotite); its lack of any Tertiary intrusive dykes.

The upper part of the Tsolum River (Harmony 1, 5 10), which forms a very pronounced linear feature (Blue Grouse Lineament), is a major fault zone. This fault zone consists of highly fractured/broken rock with numerous parallel to sub-parallel minor faults (splays). Local erratic, unmineralized calcite or quartz veining occurs within the immediate fault zone or close to it.

Two locations of interest along the Tsolum River are located approx. 5200 m and 7350 m upstream of Branch 181. Both of these locations have a small altered zone similar to the Murex Creek showing. In both cases an intensively bleached zone is located between the flow (?) boundary of a lower, very distinct pillow basalt, and an overlying massive basaltic flow. The alteration consists of an intensively bleached

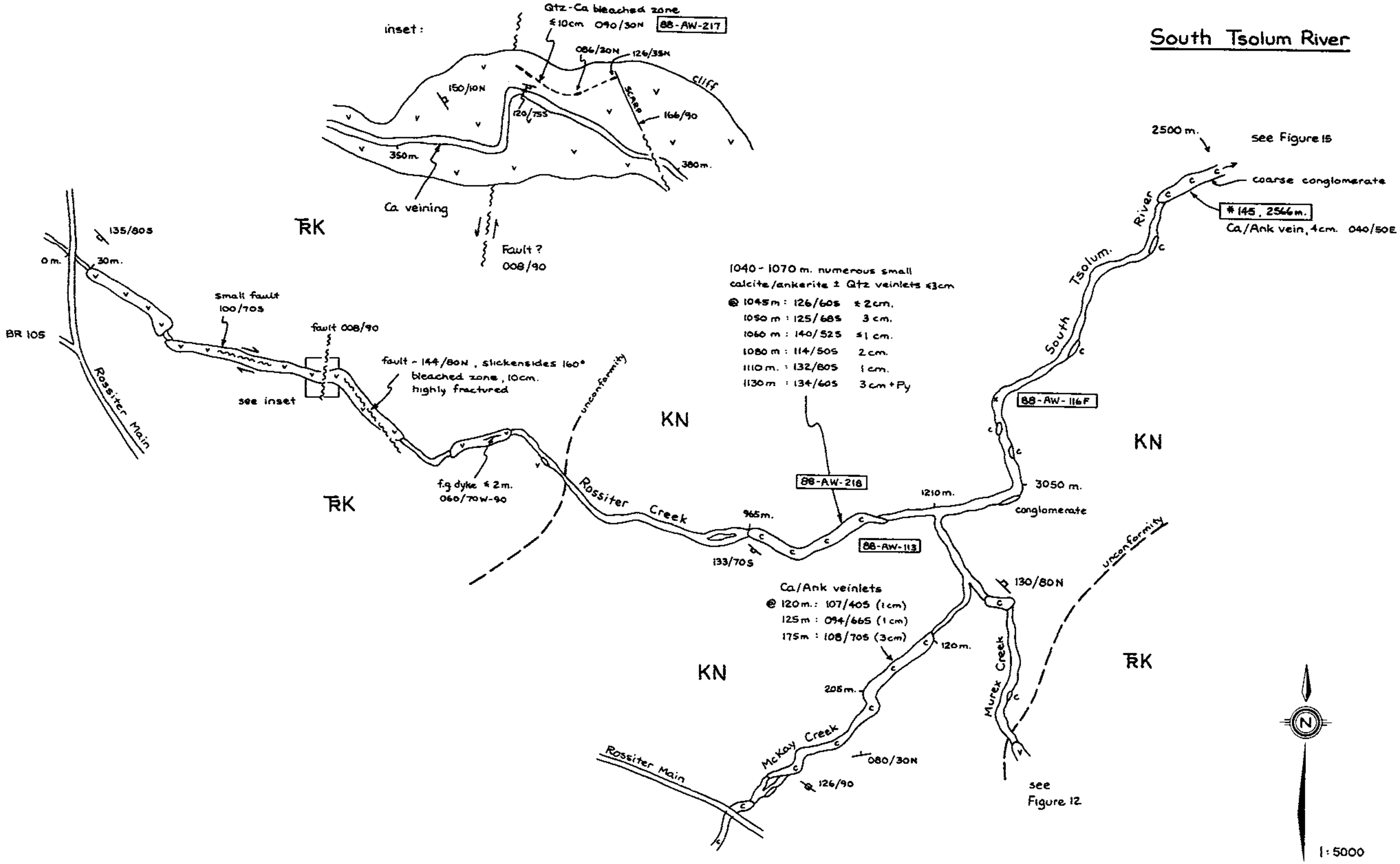
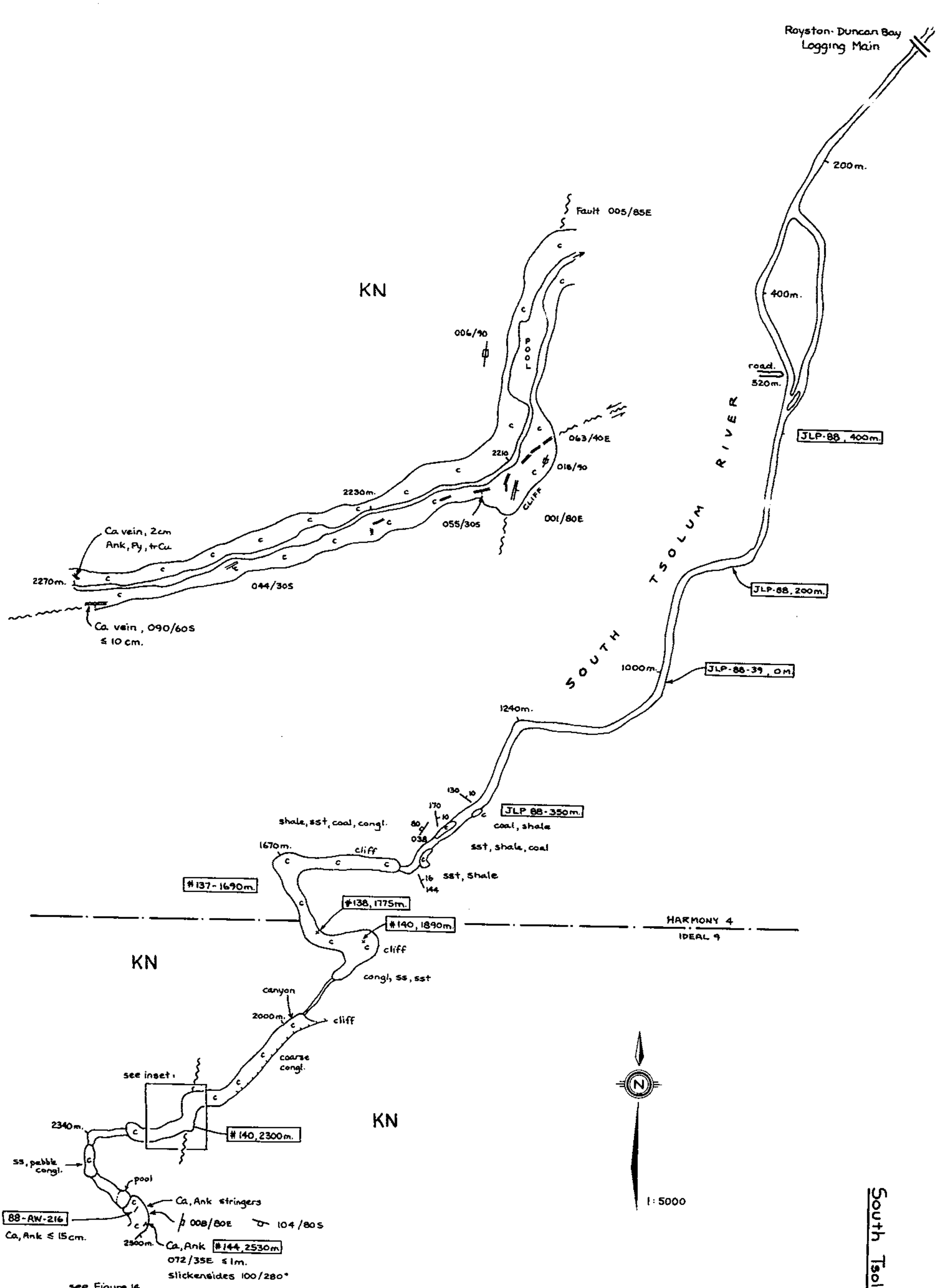

South Tsolum River
inset:
Qtz-Ca bleached zone
≤10cm 090/30N
88-AW-217
086/30N
126/35N
cliff
150/10N
120/75S
scarp
166/90
350m.
380m.
Ca veining
Fault ?
008/90
TRK
135/80S
0m.
30m.
BR 105
Rossiter Main
small fault
100/70S
fault 008/90
see inset
fault - 144/80N, slickensides 160°
bleached zone, 10cm.
highly fractured
f.g. dyke ≤ 2m.
060/70W-90
TRK
unconformity
KN
Rossiter Creek
965m.
133/70S
88-AW-113
1040 - 1070 m. numerous small
calcite/ankerite ± Qtz veinlets ≤3cm
@ 1045m : 126/60S ≤ 2cm.
1050 m : 125/68S 3 cm.
1060 m : 140/52S ≤1 cm.
1080 m : 114/50S 2cm.
1110 m. : 132/80S 1 cm.
1130 m : 134/60S 3 cm + Py
88-AW-218
1210m.
2500 m.
see Figure 15
coarse conglomerate
#145, 2566m.
Ca/Ank vein, 4cm. 040/50E
South Tsolum River
88-AW-116F
KN
3050 m.
conglomerate
130/80N
unconformity
Ca/Ank veinlets
@ 120m.: 107/40S (1cm)
125m : 094/66S (1cm)
175m : 108/70S (3cm)
120m.
205m.
KN
McKay Creek
080/30N
126/90
Rossiter Main
Murex Creek
see
Figure 12
TRK
N
1:5000

Figure 14



South Tsolum River

Figure 15

(quartz-calcite-ankerite) zone. These zones are located along a very irregular undulating surface, orientated at approx,. 130/34 N (5200 m) and approx. 030/30 W (7350m). Assay values were insignificant (< 3 ppb Au).

a) Regan Creek Showing/Grid

The one area in the Harmony claims showing extensive veining and mineralization is within Regan Creek (Fig. 7). This creek is a small creek which runs northward through the Harmony 7 claim into Regan Lake. The showings are located within the section of this creek that traverses the extreme southwestern part of this claim.

The showings consist of at least 4 small quartz-breccia veins (?). These 4 veins are located 575, 820, 845 and 900 m upstream from the Rossiter Main Road , (Fig. 17) with the latter 3 located up the western branch of the creek. These quartz-breccia veins consist of a grey-white to a white milky quartz to a very fine-grained (chalcedonic?) quartz. Occasional vuggy sections are present. These veins which range in size from 2-30 cm (average 15 cm) contain brecciated/intensively bleached country rock (Karmutsen volcanics). Between the volcanic clasts within the quartz are varying amounts of the following: pyrite, galena, sphalerite, ± realgar, ± arsenopyrite, ± chalcopyrite. These brecciated veins are usually central to a wider more extensive, pervasive carbonate (ankerite ?) alteration zone, often extending several meters either side of the central vein. The veins appear to be relatively flat-lying, striking between 024-140° and dipping between 10° S-16° N. The latter 3 brecciated zones appear to be co-planar bodies, following alternating (?) flow boundaries. Numerous other carbonate-altered zones are found along the creek.

The host rocks are the massive amygdaloidal to porphyritic volcanic rocks of the Karmutsen Formation. Several hyaloclastic-pillow basalt outcrops were noted just off the northeast end of the grid, near the junction of Rossiter Main and Branch 112. Quartz veining is common throughout the grid, however it is generally of an erratic nature, fracture-filling and limited lateral extent. Most of the veins (outside of the creek) are less than several centimeters in width, occasionally carrying trace amounts of bornite or chalcopyrite.

Rossiter Creek

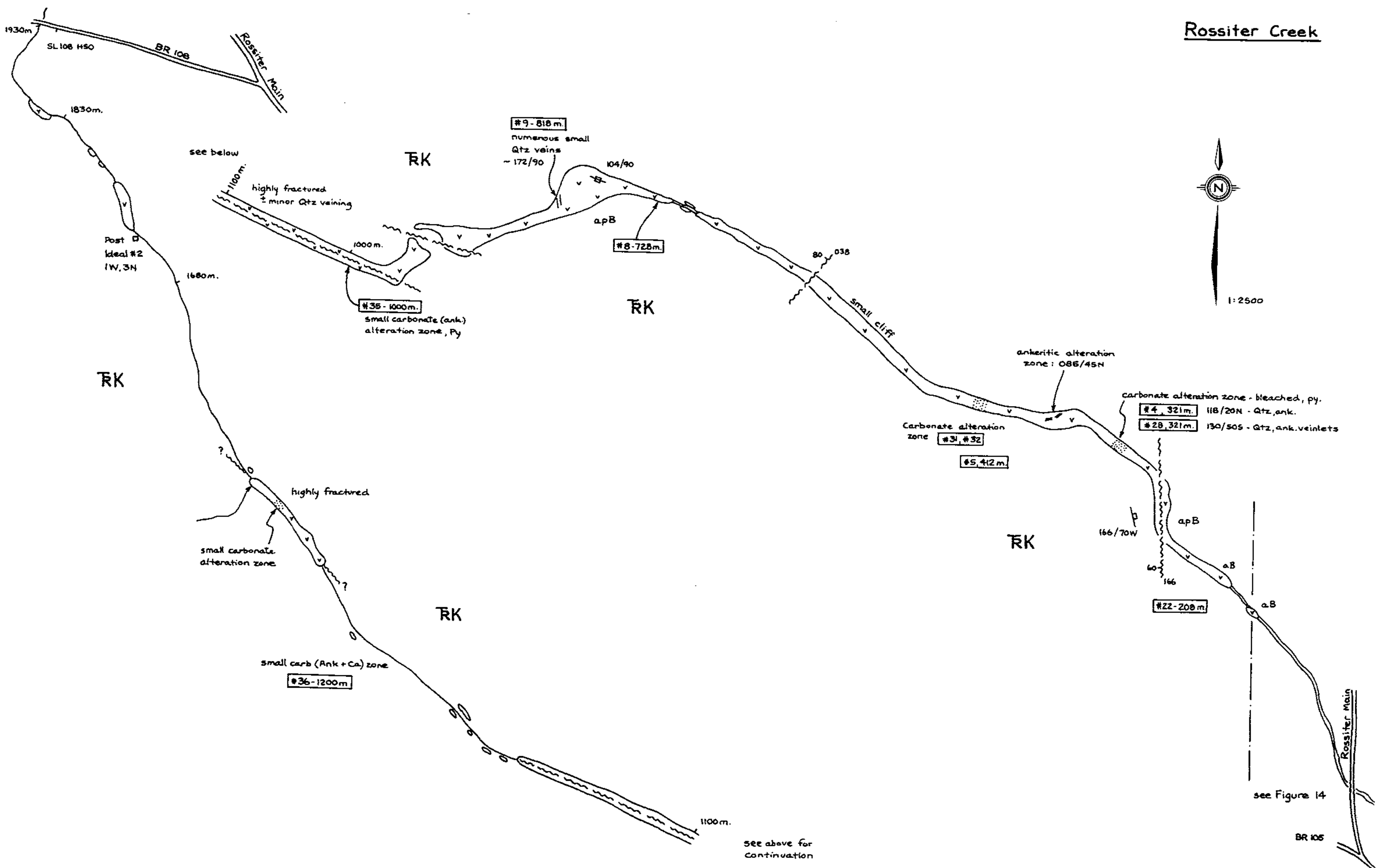


Figure 16

Regan Creek

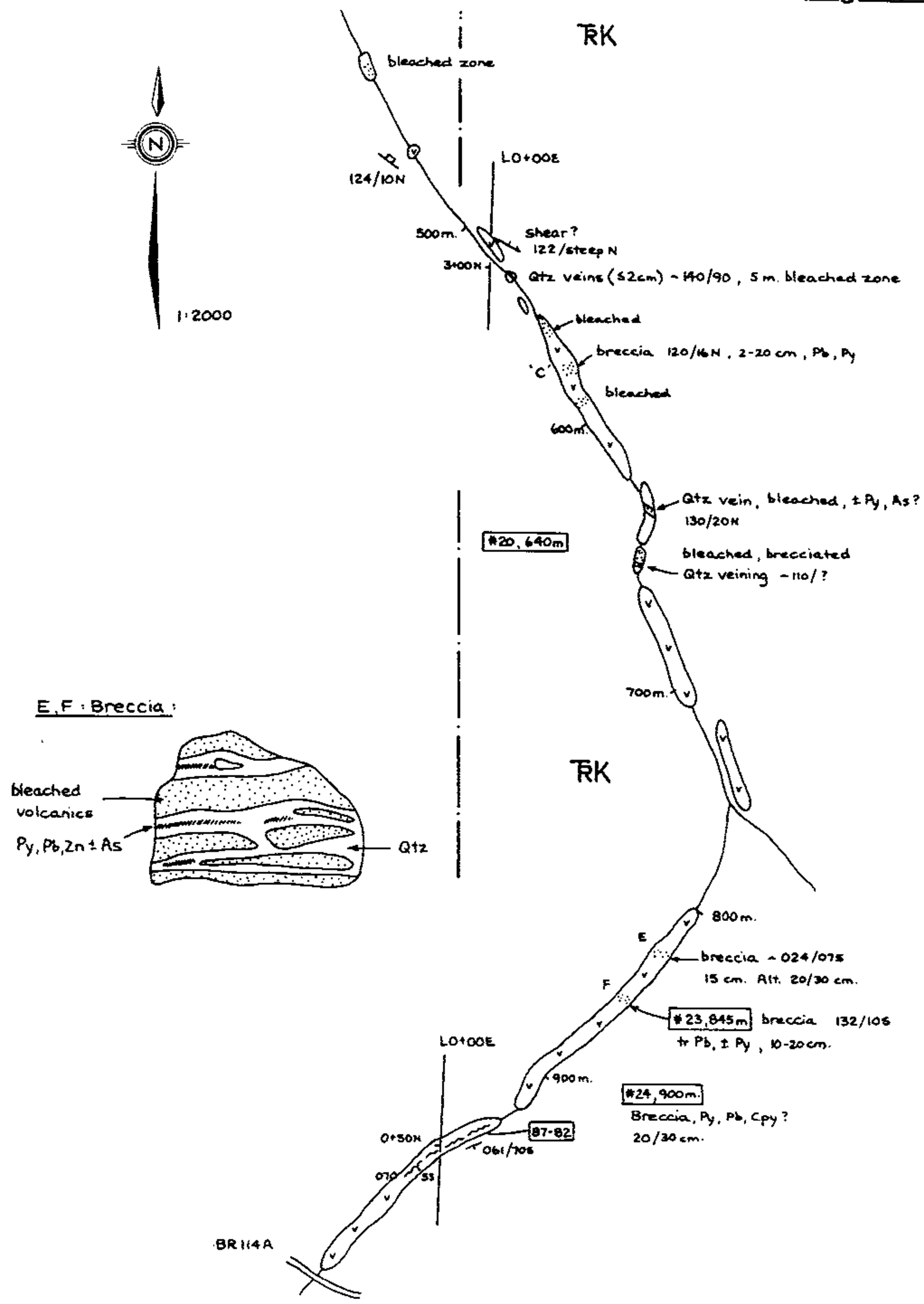


Figure 17

References

Benvenuto, G. (1986), Geology and Mineralization of the Dove Property and area near Mt. Washington, Vancouver Island, B.C. Assessment Report, 68 p.

Carson, D.J.T. (1973), The Plutonic Rocks of Vancouver Island, British Columbia: Their Petrography, Chemistry, Age and Emplacement. G.S.C. Paper 72-44, 70 p.

McConnell, D.L. (1988), Dighem III Survey for Westmin Resources Limited, Mt. Washington Area, B.C. NTS 92F/11, 14. Report by Dighem Surveys and Processing Inc.

Stevenson, W.G. (1970), Mt. Washington Exploration Project, Mt. Washington Copper Ltd. Report from Geological Branch Open File, Victoria, 66 p.

Wright, R.L. (1988), Geological Report on the Dove Project for Westmin Resources Ltd. and Visible Gold Inc., 48 p.

Appendix II

Geochemistry Results

LIST OF FIGURES

Figure 1a. Anomaly E - Soil Sample Locations

	Sample Numbers	Job Number
Initial Sampling:	RDM 4+00 to 24+00	87-4877
	BR 181 - 0+00 to 5+00	87-4627
	BR 181B2 - 0+00 to 20+00	87-5242
Followup Sampling:	line E0+00 to 5+50	88-2608
	line E1 0+50 to 4+00	
	line E2 0+50 to 8+50	
	181B - 0+50 to 13+00	
	181B1 - 0+00 to 4+00	

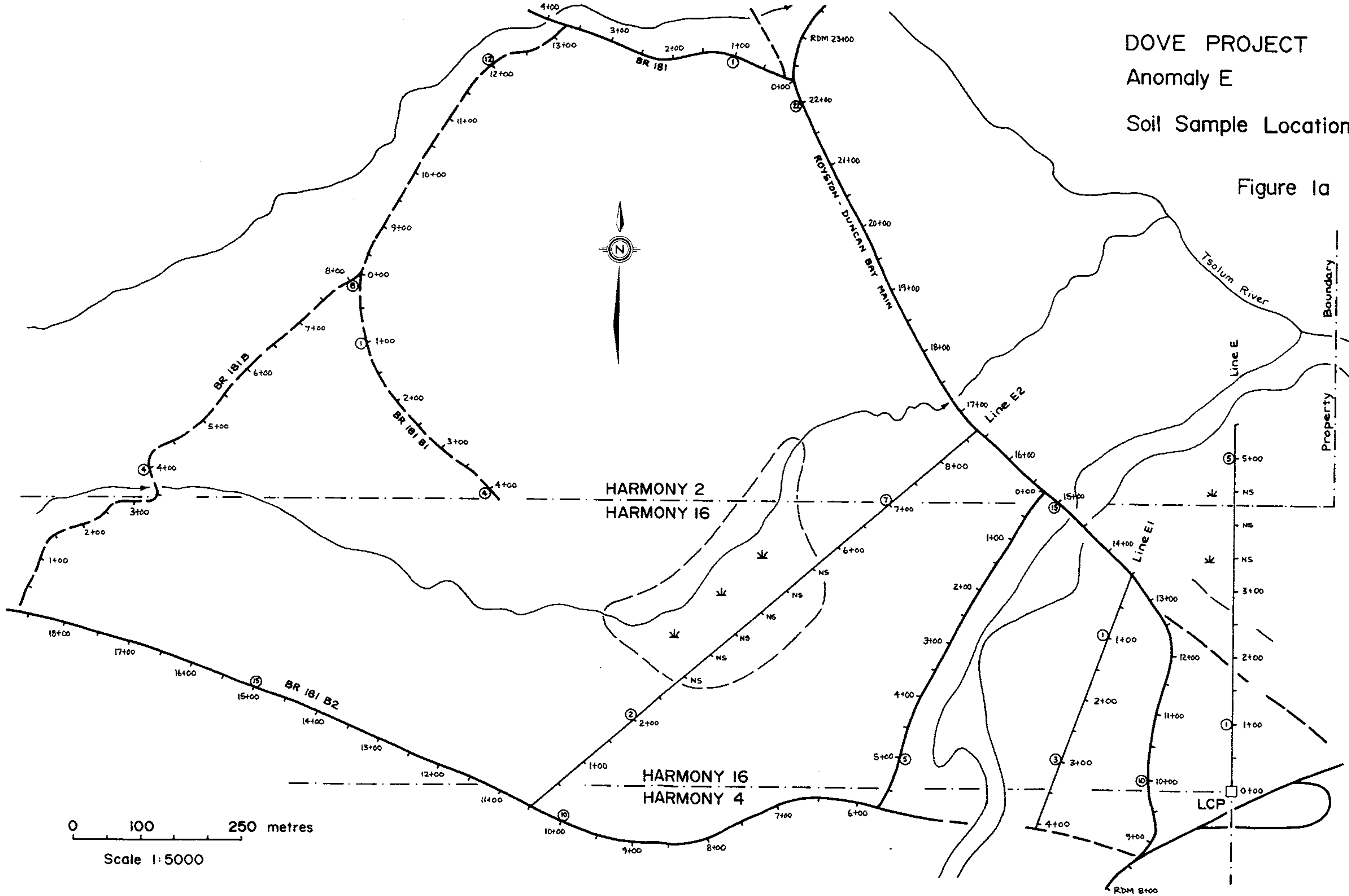
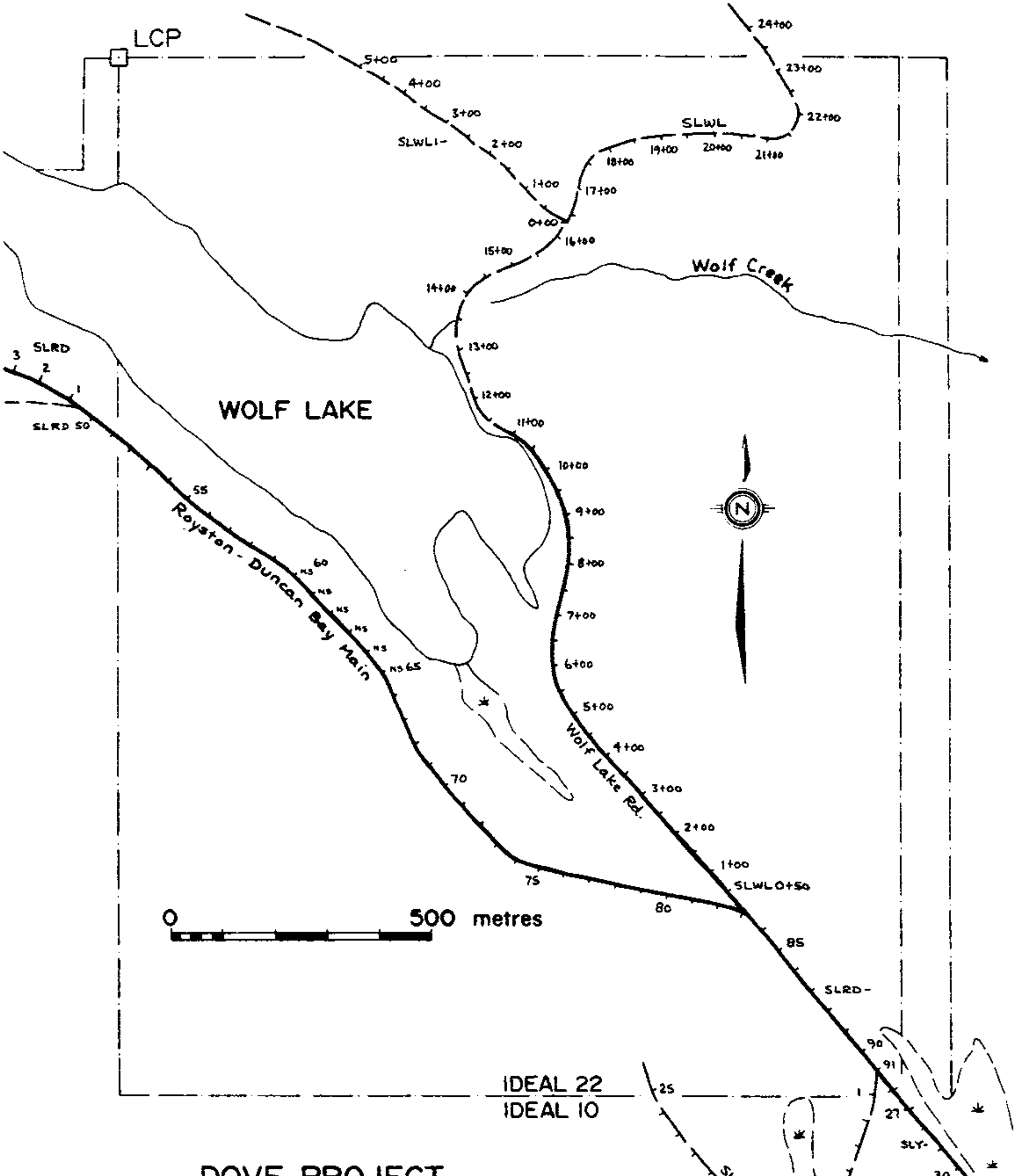

DOVE PROJECT
Anomaly E
Soil Sample Locations
Figure 1a
BR 181
BR 181 B
BR 181 B1
BR 181 B2
ROYSTON - DUNCAN BAY MAIN
RDM 23+00
RDM 8+00
Line E
Line E1
Line E2
Tsolum River
Property Boundary
HARMONY 2
HARMONY 16
HARMONY 16
HARMONY 4
LCP
N
0 100 250 metres
Scale 1:5000

Figure 1b. Ideal 22 claim - Soil Sample Locations

Road	Sample Numbers	Job Number
Royston-Duncan Bay Main	SLRD - 1 to 10	87-3362
	SLY - 26 to 33	87-3733
	SLRD - 50 to 91	88-3557
Wolf Lake Road	SLWL 0+50 to 24+00	88-3557
Trail, Constitution Hill	SLWL1 0+00 to 5+00	88-3557
unnamed	RDT - 1 to 20	87-3362
unnamed	SLY - 1 to 25	87-3733



DOVE PROJECT

Ideal 22 Claim

Soil Sample Locations

Figure 1b

NS Grid: Soil Sample Locations

Line	Samples	Job Number
L 0+00N	5+50W to 9+00E	88-4741
L 2+00N	5+50W to 9+00E	88-4741
L 4+00N	5+50W to 9+00E	88-4741
L 6+00N	5+50W to 8+50E	88-4741
L 8+00N	5+50W to 2+00E	88-4741
L 10+00N	5+50W to 2+00E	88-4741
L 12+00N	2+25W to 2+50E	88-4741
	5+50W to 2+50W	88-5079
L 14+00N	5+50W to 2+25E	88-5079
L 16+00N	5+50W to 2+50E	88-5079
L 18+00N	5+50W to 2+00E	88-5079
L 20+00N	5+50W to 2+00E	88-5079
L 22+00N	5+50W to 2+00E	88-5079
L 24+00N	5+50W to 2+00E	88-5079
L 26+00N	5+50W to 3+00E	88-5079
L 28+00N	5+50W to 3+00E	88-5079

Paquet Grid: Soil Sample Locations

Line	Samples	Job Number
L 11+00N	0+25W to 8+50E	88-4521
L 9+00N	0+32W to 7+75E	88-4521
L 7+00N	0+50W to 6+75E	88-4365
L 5+00N	0+25W to 6+00E	88-4365
L 2+75N	B/L to 6+25E	88-4365
L 1+00N	11+75N to 0+25N	88-4365

McKay Grid: Soil Sample Locations

Line	Samples	Job Number
L 31+00W	23+25N to 10+00N	88-5601
L 30+50W	21+50N to 3+50N	88-5601
L 29+00W	20+50N to 3+50N	88-5601
L 27+50W	15+00N to 3+50N	88-5601
L 26+00W	15+00N to 3+50N	88-5601
L 24+50W	15+00N to 3+50N	88-5601
L 23+00W	15+00N to 6+75N	88-5601
L 21+50W	15+00N to 5+50N	88-5601
L 20+00W	15+00N to 3+50N	88-5601
L 18+50W	15+00N to 3+50N	88-5601
L 17+00W	15+00N to 3+50N	88-5601
L 15+50W	14+70N to 3+50N	88-5601
L 14+00W	15+00N to 3+50N	88-5601
L 12+50W	15+00N to 3+50N	88-5601

Regan Grid: Soil Sample Locations

Line	Samples	Job Number
L 0+75E	7+25N to 4+25S	88-4521
L 2+25E	6+50N to 5+75S	88-4521
L 3+75E	5+25N to 6+00S	88-4521

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JULY 12 1988 DATE REPORT MAILED: July 15/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT-DOVE File # 88-2608 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
E-0+00	1	56	13	71	.2	18	11	518	6.15	25	5	ND	1	10	1	4	2	160	.60	.076	3	50	.26	21	.33	4	2.88	.01	.03	1	3
E-0+50	1	74	13	73	.1	25	12	846	4.63	31	5	ND	1	15	1	3	2	144	.97	.057	4	53	.47	31	.27	5	2.89	.01	.04	1	92
E-1+00	1	44	15	75	.1	18	11	504	5.44	32	5	ND	1	12	1	3	2	152	.66	.089	2	48	.32	24	.33	5	2.31	.01	.03	1	4
E-1+50	2	186	45	90	.2	31	19	1490	5.30	45	5	ND	1	21	1	4	2	130	.92	.174	4	51	.57	32	.26	9	4.82	.01	.04	1	1
E-2+00	2	43	13	102	.1	26	16	646	5.90	25	5	ND	1	14	1	2	2	164	.78	.052	3	51	.41	27	.40	4	2.74	.01	.04	1	3
E-2+50	1	30	13	61	.1	13	8	469	5.25	33	5	ND	1	10	1	2	3	159	.52	.057	3	47	.20	22	.32	4	1.49	.02	.02	1	20
E-3+00	1	105	7	68	.1	37	17	463	5.35	38	5	ND	1	10	1	2	2	170	.95	.028	5	66	.78	31	.36	9	3.59	.01	.03	1	3
E-5+00	2	143	14	74	.2	35	21	960	5.08	91	5	ND	1	18	1	2	2	120	1.06	.038	5	44	.86	39	.21	7	2.68	.01	.04	1	2
E-5+50	3	260	19	97	.3	37	22	942	5.05	107	5	ND	1	21	1	2	3	112	.96	.054	5	45	.82	41	.16	9	2.58	.02	.05	2	6
E1-0+50	3	151	10	96	.3	34	24	846	6.04	137	5	ND	1	17	1	3	2	132	.80	.029	4	56	.73	58	.21	5	3.00	.01	.04	1	5
E1-1+00	2	160	12	84	.2	40	24	815	6.30	93	5	ND	1	14	1	2	2	143	.91	.033	4	54	.85	38	.25	6	3.79	.01	.04	1	2
E1-1+50	2	153	9	73	.1	34	19	542	5.32	98	5	ND	1	10	1	3	2	130	.74	.017	4	48	.86	31	.22	7	3.16	.01	.03	1	59
E1-2+00	2	158	10	81	.2	37	21	800	5.44	115	5	ND	1	12	1	3	3	124	.79	.033	4	49	.89	41	.20	5	3.13	.01	.04	1	7
E1-2+50	2	137	9	76	.2	37	20	762	5.38	75	5	ND	1	14	1	3	2	137	1.10	.028	4	46	.91	34	.27	7	3.21	.01	.04	1	3
E1-3+00	2	147	11	77	.1	41	19	680	5.51	83	5	ND	1	13	1	2	2	130	.92	.029	4	47	.88	43	.21	6	3.12	.01	.03	1	18
E1-3+50	3	153	12	82	.2	35	22	932	5.71	106	5	ND	1	15	1	2	3	135	.79	.040	5	52	.82	40	.20	7	3.38	.01	.03	1	8
E1-4+00	2	162	11	85	.1	38	21	820	5.59	117	5	ND	1	17	1	3	2	133	1.09	.029	5	48	.93	44	.23	11	3.19	.02	.04	1	88
E2-0+5-0	1	105	15	141	.4	64	28	1935	8.04	24	5	ND	1	31	1	2	2	225	.98	.062	9	120	.89	293	.45	6	5.52	.01	.04	1	2
E2-1+00	1	43	12	69	.1	29	13	199	5.40	8	5	ND	1	13	1	2	2	161	.76	.043	4	72	.42	61	.38	8	3.30	.01	.01	1	2
E2-1+50	1	59	12	103	.2	37	19	687	5.64	8	5	ND	1	21	1	2	2	161	1.18	.038	6	81	.72	94	.34	5	3.53	.01	.03	1	1
E2-2+00	1	55	7	60	.1	30	15	331	4.91	15	5	ND	1	12	1	2	2	165	.80	.031	6	80	.52	40	.39	7	3.18	.01	.02	1	4
E2-2+50	1	60	7	69	.3	29	16	666	5.52	17	5	ND	1	18	1	3	2	173	1.05	.025	7	64	.61	34	.35	5	2.88	.01	.04	1	1
E2-6+00	1	112	9	83	.2	30	16	857	5.44	66	5	ND	1	9	1	2	2	143	.64	.066	4	52	.57	41	.25	4	3.44	.01	.03	1	9
E2-6+50	1	58	13	76	.1	20	13	652	6.11	53	5	ND	1	7	1	2	2	162	.51	.131	3	50	.30	28	.28	5	2.85	.01	.02	1	9
E2-7+00	2	141	11	83	.1	35	17	668	5.80	72	5	ND	1	9	1	2	2	152	.70	.049	3	58	.64	30	.28	9	3.96	.01	.03	1	11
E2-7+50	2	132	19	116	.2	41	20	713	6.12	85	5	ND	1	11	1	3	2	156	.75	.058	4	62	.66	38	.29	4	4.12	.01	.04	1	66
E2-8+00	2	82	12	104	.2	26	20	2200	5.53	65	5	ND	1	15	1	2	2	147	.77	.031	4	54	.52	66	.24	9	2.62	.01	.04	1	6
E2-8+50	2	155	13	76	.5	34	18	514	5.32	90	5	ND	1	12	1	2	3	140	.74	.046	6	55	.77	31	.26	11	3.75	.01	.03	1	16
181B-0+50	1	62	10	82	.1	22	13	536	5.97	29	5	ND	1	10	1	2	2	168	.58	.115	4	52	.38	30	.41	6	3.70	.01	.03	1	4
181B-1+00	1	82	12	90	.1	32	16	524	6.04	8	5	ND	1	14	1	2	2	183	1.05	.082	3	55	.53	24	.58	7	4.10	.01	.03	1	1
181B-1+50	1	40	15	75	.1	21	10	433	6.68	11	5	ND	1	14	1	2	2	198	.82	.057	3	56	.30	33	.54	7	2.63	.01	.03	1	1
181B-2+00	1	55	15	108	.1	36	20	1155	7.16	12	5	ND	1	12	1	2	2	203	.78	.075	4	67	.50	34	.60	8	4.04	.01	.03	1	1
181B-2+50	1	30	21	125	.1	19	19	1224	6.71	9	5	ND	1	13	1	2	2	170	.92	.261	3	52	.34	35	.45	3	2.52	.01	.02	1	1
181B-3+00	1	32	18	96	.1	16	14	1016	6.98	13	5	ND	1	16	1	2	2	208	.98	.139	3	42	.35	30	.54	4	2.35	.01	.03	1	1
181B-3+50	1	47	13	106	.1	22	14	689	7.38	14	5	ND	1	12	1	2	2	221	.91	.053	3	56	.44	26	.57	9	2.65	.01	.03	1	1
181B-4+00	1	100	10	66	.3	28	15	820	5.70	21	5	ND	1	14	1	2	3	201	1.39	.102	7	38	.76	15	.43	12	4.33	.01	.03	1	615
STD C/AU-S	17	57	40	132	6.6	68	28	1046	4.00	44	20	6	37	47	17	17	20	55	.49	.093	38	56	.91	175	.06	34	1.94	.06	.15	11	52

WESTMIN RESOURCES LTD. PROJECT-DOVE FILE # 88-2608

SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mg	Ba	Ti	B	Al	Na	K	W	Au*
	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	PPM	%	%	PPM	PPM	%	PPM	%	PPM	%	%	%	PPM	PPB
181B-4+50	1	52	15	82	.2	27	16	754	6.57	5	5	ND	1	16	1	2	2	213	.90	.051	3	60	.37	32	.60	6	2.93	.01	.03	1	1
181B-5+00	1	92	9	52	.3	29	14	610	5.22	7	5	ND	1	17	1	2	2	184	1.47	.036	7	31	.82	16	.45	6	3.02	.02	.03	1	3
181B-5+50	1	51	12	65	.2	27	18	733	6.92	4	5	ND	1	14	1	2	2	225	.83	.056	3	55	.38	29	.63	7	3.48	.02	.03	1	1
181B-6+00	1	65	10	72	.1	37	17	491	5.83	2	5	ND	1	12	1	2	2	175	.94	.045	3	61	.52	29	.55	3	3.74	.02	.02	1	2
181B-6+50	1	52	20	102	.1	28	16	734	5.99	10	5	ND	1	16	1	2	2	172	.97	.092	3	43	.53	28	.47	4	2.91	.02	.02	1	1
181B-7+00	1	80	11	59	.1	33	16	605	5.43	9	5	ND	1	15	1	2	2	181	1.04	.043	5	52	.70	31	.44	10	3.57	.02	.03	1	1
181B-7+50	1	38	12	62	.1	25	14	570	5.33	6	5	ND	1	12	1	3	2	167	.92	.052	3	46	.39	31	.47	10	3.02	.02	.01	1	1
181B-8+00	1	90	10	60	.1	41	18	602	5.55	7	5	ND	1	13	1	2	3	180	1.01	.034	3	67	.78	39	.44	5	4.11	.01	.02	1	1
181B-8+50	1	37	19	70	.1	16	12	1067	4.57	11	5	ND	1	17	1	2	2	141	.91	.125	2	36	.34	46	.42	4	2.13	.01	.02	1	12
181B-9+00	1	73	8	51	.1	27	14	529	4.72	8	5	ND	1	16	1	2	2	142	1.17	.027	5	40	.70	28	.35	6	2.63	.03	.01	2	3
181B-9+50	1	99	9	54	.2	30	16	723	5.03	11	5	ND	1	18	1	2	2	152	1.40	.039	5	41	.86	27	.33	11	2.75	.02	.03	1	1
181B-10+00	1	72	10	54	.2	31	16	813	5.14	13	5	ND	1	21	1	2	2	158	1.50	.031	5	41	.91	34	.35	6	2.65	.02	.03	1	2
181B-10+50	1	84	11	55	.2	32	15	638	4.70	9	5	ND	1	21	1	3	2	144	1.39	.028	6	41	.92	33	.34	6	2.81	.01	.02	1	1
181B-11+00	1	66	8	65	.1	28	15	833	4.80	12	5	ND	1	22	1	2	2	143	1.30	.047	5	42	.74	36	.33	10	2.33	.03	.02	1	1
181B-11+50	1	64	10	67	.1	32	16	894	4.83	7	5	ND	1	23	1	2	2	141	1.42	.025	4	45	.92	41	.33	7	2.54	.01	.02	1	2
181B-12+00	1	72	10	59	.2	30	16	817	4.87	10	5	ND	1	21	1	2	2	144	1.37	.029	4	41	.88	28	.34	5	2.61	.02	.03	1	2
181B-12+50	1	65	8	75	.1	30	17	896	4.99	13	5	ND	1	27	1	2	2	141	1.36	.075	4	48	.86	85	.33	10	2.64	.02	.03	1	2
181B-13+00	1	72	10	57	.2	30	15	737	4.48	11	5	ND	1	20	1	2	2	132	1.32	.033	6	44	.81	34	.31	5	2.54	.02	.04	1	3
181B1-0+00	1	51	11	70	.1	26	15	775	5.19	8	5	ND	1	11	1	2	2	154	1.02	.096	3	43	.44	26	.42	3	3.31	.01	.01	1	1
181B1-0+50	1	40	12	70	.1	23	11	358	5.84	5	5	ND	1	12	1	2	2	175	.91	.082	2	54	.45	26	.44	4	2.96	.01	.01	1	1
181B1-1+00	1	71	10	64	.1	44	18	393	5.76	5	5	ND	1	13	1	2	2	175	1.06	.041	3	61	.79	24	.44	11	3.82	.01	.02	1	1
181B1-1+50	1	34	15	84	.1	21	12	448	6.04	8	5	ND	1	11	1	2	2	173	.78	.130	3	46	.33	30	.49	4	3.40	.02	.02	1	1
181B1-2+00	1	42	12	78	.1	21	14	612	5.62	5	5	ND	1	13	1	3	2	170	.98	.043	3	52	.37	40	.51	3	2.56	.02	.02	1	1
181B1-2+50	1	83	12	70	.2	39	18	501	5.80	5	5	ND	1	14	1	2	2	183	.88	.038	6	65	.64	35	.47	3	4.15	.02	.03	1	21
181B1-3+00	1	63	17	73	.1	26	15	1102	5.35	4	5	ND	1	14	1	2	3	159	.92	.066	3	50	.44	31	.46	5	3.04	.03	.02	1	1
181B1-3+50	1	76	16	103	.1	30	18	1551	6.08	3	5	ND	1	12	1	2	2	169	.84	.116	3	57	.49	37	.52	4	4.12	.03	.02	1	1
181B1-4+00	1	99	18	81	.1	36	18	873	5.62	2	5	ND	1	13	1	2	2	158	.88	.085	3	54	.57	29	.50	3	4.41	.01	.03	1	2
STD C/AU-S	17	59	39	131	6.6	67	28	1062	4.06	38	18	6	35	48	17	16	19	56	.49	.083	39	56	.91	174	.06	34	1.96	.06	.14	13	47

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: AUG 12 1988 DATE REPORT MAILED: Aug 24/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-3557 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
SLRD 50	2	93	12	71	.3	27	17	592	5.03	40	5	ND	1	9	1	3	3	133	.63	.054	6	41	.49	26	.28	3	3.37	.01	.02	1	13
SLRD 51	2	106	8	52	.2	29	18	643	4.74	35	5	ND	1	12	1	3	2	127	.86	.045	6	37	.70	28	.27	5	3.21	.01	.04	1	1
SLRD 52	2	113	2	72	.4	37	17	611	4.89	29	5	ND	1	15	1	2	2	127	.75	.040	6	45	.69	49	.24	6	3.40	.01	.05	1	14
SLRD 53	1	73	6	62	.2	25	14	394	4.90	23	5	ND	1	9	1	2	2	142	.56	.031	6	44	.47	23	.27	3	3.04	.01	.02	1	2
SLRD 54	1	111	7	77	.4	45	18	538	5.08	37	5	ND	1	18	1	2	2	146	.56	.044	6	59	.63	60	.24	2	3.93	.01	.03	1	6
SLRD 55	1	121	9	70	.2	39	20	796	5.12	35	5	ND	1	22	1	2	2	142	1.03	.034	8	50	.84	38	.30	7	3.22	.01	.04	1	21
SLRD 56	2	92	6	86	.3	38	19	408	5.08	25	5	ND	1	9	1	3	2	137	.66	.042	6	47	.56	35	.30	5	3.55	.01	.03	1	280
SLRD 57	1	108	7	78	.2	39	19	348	5.42	35	5	ND	1	9	1	2	2	145	.44	.039	5	55	.59	39	.23	5	4.26	.01	.03	1	3
SLRD 58	2	54	11	77	.4	24	18	660	4.90	29	5	ND	1	11	1	4	2	123	.52	.032	6	37	.40	34	.24	5	2.78	.01	.03	1	1
SLRD 59	2	79	8	99	.5	36	20	520	5.44	36	5	ND	1	11	1	3	2	134	.54	.056	6	43	.50	38	.25	4	3.94	.01	.03	1	10
SLRD 65	1	66	2	75	.2	19	14	759	4.85	25	5	ND	1	8	1	2	4	132	.42	.040	5	36	.32	36	.22	2	2.64	.01	.04	1	4
SLRD 66	1	73	7	80	.3	36	16	478	5.25	33	5	ND	1	17	1	2	4	130	.64	.026	5	49	.62	56	.21	2	3.45	.01	.04	1	9
SLRD 67	1	33	5	48	.2	10	6	216	3.85	19	5	ND	1	9	1	2	2	97	.29	.025	4	25	.20	22	.11	2	1.87	.01	.02	1	5
SLRD 68	1	56	9	65	.3	22	12	317	4.45	26	5	ND	1	16	1	2	2	123	.58	.035	5	34	.42	31	.17	9	2.61	.01	.03	1	1
SLRD 69	1	54	11	74	.2	24	12	703	4.17	25	5	ND	1	14	1	2	2	104	.58	.055	5	32	.40	36	.14	2	2.60	.01	.03	1	1
SLRD 70	1	95	6	93	.4	42	17	408	4.99	34	5	ND	1	14	1	2	3	117	.57	.050	5	47	.70	61	.18	5	4.15	.01	.05	1	3
SLRD 71	1	63	5	62	.2	30	15	454	4.02	27	5	ND	1	16	1	2	3	98	.60	.021	5	41	.64	43	.14	2	3.04	.01	.03	1	18
SLRD 72	1	45	6	47	.1	16	10	413	4.41	28	5	ND	1	11	1	2	3	109	.33	.028	4	37	.25	27	.14	3	2.29	.01	.02	2	5
SLRD 73	1	84	9	64	.2	27	15	458	4.58	38	5	ND	1	12	1	2	2	114	.57	.031	5	37	.56	38	.18	5	2.83	.01	.03	1	34
SLRD 74	3	79	6	88	.3	33	19	405	6.11	48	5	ND	1	10	1	2	2	158	.43	.047	5	49	.41	45	.23	4	3.75	.01	.05	1	3
SLRD 75	2	71	12	66	.3	22	15	434	5.36	35	5	ND	1	12	1	4	2	145	.68	.039	4	44	.56	26	.26	2	2.83	.01	.03	1	13
SLRD 76	1	74	2	59	.3	31	15	214	4.76	30	5	ND	1	9	1	4	2	121	.44	.028	5	47	.43	27	.23	4	3.23	.01	.02	1	4
SLRD 77	1	97	13	60	.1	34	17	677	4.52	30	5	ND	1	14	1	2	2	117	.97	.028	5	42	.81	33	.25	9	2.89	.01	.03	1	21
SLRD 78	1	67	10	54	.3	25	12	288	4.21	27	5	ND	1	8	1	3	2	107	.46	.026	4	39	.45	27	.17	2	2.73	.01	.02	1	11
SLRD 79	2	87	13	50	.3	35	12	235	3.28	18	5	ND	1	14	1	2	2	79	.48	.033	5	46	.55	66	.13	3	3.49	.01	.03	2	14
SLRD 80	1	107	3	65	.3	36	16	343	5.25	28	5	ND	1	11	1	3	5	124	.51	.024	6	58	.68	46	.18	3	3.35	.01	.04	1	8
SLRD 81	1	73	9	73	.4	30	16	423	5.56	16	5	ND	1	11	1	2	2	156	.62	.047	6	49	.53	43	.32	2	3.37	.01	.03	1	4
SLRD 82	1	112	10	68	.2	37	19	915	5.13	27	5	ND	1	23	1	2	2	128	1.04	.033	7	48	.84	42	.25	3	3.07	.01	.04	1	6
SLRD 83	1	55	8	63	.3	21	14	288	6.08	16	5	ND	1	10	1	3	2	171	.53	.044	4	44	.35	27	.29	2	3.38	.01	.02	1	4
SLRD 84	1	103	14	61	.5	33	18	952	5.13	19	5	ND	1	17	1	2	2	151	1.01	.032	6	47	.76	36	.34	8	3.39	.01	.02	1	8
SLRD 85	1	103	9	71	.4	34	18	953	4.96	22	5	ND	1	20	1	2	2	138	1.11	.063	7	45	.77	40	.30	6	3.37	.01	.04	1	7
SLRD 86	1	88	8	64	.4	30	16	456	4.87	19	5	ND	1	16	1	2	2	139	1.01	.042	5	39	.63	26	.30	7	2.97	.01	.04	1	2
SLRD 87	1	49	6	38	.3	16	8	272	3.98	29	5	ND	1	5	1	2	4	99	.20	.021	7	29	.23	25	.08	2	2.31	.01	.03	2	3
SLRD 88	2	96	13	64	.4	31	17	540	4.76	39	5	ND	1	8	1	5	2	114	.45	.040	5	43	.54	38	.16	7	3.84	.01	.03	1	14
SLRD 89	2	66	5	71	.6	23	17	586	5.14	41	5	ND	1	14	1	4	2	120	.37	.040	5	38	.33	42	.13	3	3.16	.01	.03	1	13
SLRD 90	2	94	10	70	.5	33	19	596	4.77	54	5	ND	1	21	1	3	2	93	.48	.034	6	41	.55	54	.12	7	3.55	.01	.04	1	11
SLRD 91	2	93	8	67	.3	30	19	1132	4.51	43	5	ND	1	17	1	4	2	87	.47	.036	7	37	.56	54	.10	6	3.31	.01	.04	1	1
STD C/AU-S	17	58	37	127	7.1	68	27	1050	4.03	38	18	8	37	47	17	16	19	56	.47	.086	39	54	.92	172	.06	34	1.94	.06	.13	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
SLWL 0+50	1	119	18	59	.2	33	19	634	4.60	25	5	ND	1	12	1	2	2	140	.92	.029	6	37	.75	32	.32	2	3.19	.01	.03	1	9
SLWL 1+00	1	94	13	70	.3	29	15	438	4.97	21	5	ND	1	10	1	2	2	149	.67	.035	5	41	.57	42	.31	2	3.14	.01	.02	1	1
SLWL 1+50	1	39	14	61	.2	16	9	209	4.97	18	5	ND	1	16	1	2	2	159	.53	.023	3	38	.29	25	.27	2	1.99	.01	.02	1	1
SLWL 2+00	1	109	10	62	.3	36	16	312	4.89	25	5	ND	1	10	1	2	2	146	.64	.030	4	51	.60	37	.30	3	3.34	.01	.01	1	2
SLWL 2+50 P	1	17	6	56	.2	7	2	25	.56	3	5	ND	1	29	1	2	4	11	.56	.077	6	4	.05	24	.01	2	.52	.01	.02	1	1
SLWL 3+00	1	38	8	25	.2	15	6	199	1.89	6	5	ND	1	21	1	2	2	57	.70	.015	9	30	.23	31	.16	2	1.98	.01	.01	1	8
SLWL 3+50	1	61	15	55	.2	22	12	402	4.47	13	5	ND	1	10	1	2	2	139	.51	.025	4	37	.39	34	.23	2	2.55	.01	.02	1	1
SLWL 4+00	1	34	17	45	.3	16	8	217	4.53	17	5	ND	1	7	1	2	2	149	.40	.031	3	33	.21	23	.28	2	1.87	.01	.01	2	3
SLWL 4+50	1	46	19	45	.3	25	11	171	3.57	10	5	ND	1	9	1	3	2	130	.55	.013	7	42	.42	45	.24	2	2.79	.01	.02	1	1
SLWL 5+00	1	48	12	47	.7	23	12	224	5.27	14	5	ND	1	8	1	2	3	167	.50	.025	4	53	.40	25	.34	2	3.35	.01	.02	1	1
SLWL 5+50	1	91	12	66	.2	31	16	365	4.86	18	5	ND	1	11	1	2	2	145	.67	.031	4	42	.57	36	.28	2	3.02	.01	.02	1	1
SLWL 6+00	1	68	16	66	.3	28	16	596	4.92	18	5	ND	1	11	1	2	4	145	.56	.042	5	46	.45	45	.27	4	2.94	.01	.02	1	2
SLWL 6+50	1	50	12	71	.4	25	14	341	5.35	12	5	ND	1	12	1	2	2	160	.66	.035	4	47	.38	36	.33	2	2.89	.01	.03	1	1
SLWL 7+00	1	80	12	66	.2	28	15	289	4.98	17	5	ND	1	11	1	2	2	143	.64	.023	5	49	.57	42	.22	3	3.23	.01	.01	1	5
SLWL 7+50	1	71	10	55	.2	34	16	258	4.77	11	5	ND	1	10	1	2	2	150	.59	.018	4	58	.59	38	.23	2	3.90	.01	.02	1	1
SLWL 8+00	2	98	14	83	.3	43	20	413	6.05	30	5	ND	1	13	1	4	2	149	.54	.027	6	74	.79	59	.20	3	4.34	.01	.04	1	4
SLWL 8+50	2	89	9	70	.4	37	17	394	5.32	90	5	ND	1	15	1	3	2	131	.58	.024	6	60	.68	50	.18	4	3.56	.01	.04	1	1
SLWL 9+00	2	33	17	98	.2	24	15	525	4.75	58	5	ND	1	19	1	2	2	103	.58	.034	6	42	.37	48	.16	2	3.01	.01	.03	1	1
SLWL 9+50	3	39	19	99	.2	33	17	647	5.32	34	5	ND	1	20	1	3	2	110	.41	.031	6	49	.32	73	.16	2	3.98	.01	.04	1	1
SLWL 10+00	2	60	14	73	.3	31	15	365	5.02	20	5	ND	1	15	1	2	2	119	.52	.029	7	40	.59	45	.17	2	3.63	.01	.04	1	1
SLWL 10+50	1	38	9	66	.1	20	12	387	4.36	8	5	ND	1	12	1	3	3	101	.36	.024	6	33	.24	50	.15	3	2.89	.01	.02	1	1
SLWL 11+00	1	95	8	63	.2	39	18	346	5.31	21	5	ND	1	11	1	2	2	142	.61	.020	5	50	.76	36	.28	2	3.69	.01	.03	1	4
SLWL 11+50	1	53	11	72	.3	22	11	277	4.74	11	5	ND	1	9	1	2	2	124	.47	.040	5	35	.33	34	.25	3	2.88	.01	.02	1	1
SLWL 12+00	1	89	13	79	.3	38	17	275	6.23	20	5	ND	1	10	1	2	2	161	.41	.023	7	64	.47	41	.26	4	4.61	.01	.04	1	2
SLWL 12+50	1	88	8	59	.3	36	16	330	5.21	17	5	ND	1	13	1	2	2	141	.54	.019	6	54	.59	46	.22	2	3.77	.01	.04	1	1
SLWL 13+00	1	58	7	61	.2	23	13	252	4.98	8	5	ND	1	10	1	2	2	149	.61	.024	4	38	.42	25	.32	2	3.01	.01	.01	1	1
SLWL 13+50	1	61	12	66	.1	31	15	400	5.50	11	5	ND	1	13	1	2	2	167	.67	.026	4	43	.43	37	.33	2	3.04	.01	.02	1	3
SLWL 14+00	2	73	32	107	.4	56	27	3260	5.71	25	5	ND	1	36	1	3	2	149	.76	.098	6	74	.37	101	.46	2	5.39	.01	.04	1	1
SLWL 14+50	1	56	13	57	.2	28	14	631	4.17	12	5	ND	1	15	1	2	2	118	.70	.026	6	37	.48	33	.27	4	2.98	.01	.03	1	1
SLWL 15+00	1	67	11	58	.3	28	14	378	4.45	11	5	ND	1	9	1	2	2	120	.49	.046	5	39	.45	34	.27	3	4.04	.01	.03	1	5
SLWL 15+50	1	58	14	61	.1	27	14	441	4.44	11	6	ND	1	13	1	3	2	120	.60	.028	4	37	.45	39	.27	4	3.16	.01	.02	1	1
SLWL 16+00	1	60	13	58	.1	27	15	428	4.80	12	5	ND	1	14	1	2	2	142	.68	.035	6	37	.43	28	.30	2	2.90	.01	.01	1	6
SLWL 16+50	1	38	9	135	.1	24	16	512	5.16	10	5	ND	1	11	1	2	2	143	.64	.033	3	37	.35	36	.33	2	2.74	.01	.01	1	4
SLWL 17+00	1	50	12	64	.3	31	16	425	5.40	11	5	ND	1	16	1	2	2	160	.71	.030	7	42	.49	34	.30	6	1.84	.01	.02	1	14
SLWL 17+50	2	31	11	57	.1	18	11	279	4.00	8	5	ND	1	11	1	2	2	109	.48	.042	3	28	.30	24	.22	4	2.79	.01	.02	1	10
STD C/AU-S	17	57	38	132	7.2	68	27	1038	4.00	38	16	8	36	47	16	16	19	56	.46	.088	39	54	.91	173	.06	32	1.90	.06	.14	13	47

P - 20MESH, PULVERIZED

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-3557

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
SLWL 18+00	1	19	16	46	.1	19	8	343	2.99	10	5	ND	1	14	1	2	2	78	.53	.014	4	27	.36	30	.10	3	2.11	.01	.04	1	2
SLWL 18+50	1	11	14	49	.1	10	6	376	2.25	7	5	ND	1	13	1	2	2	58	.43	.024	3	14	.22	23	.07	2	1.55	.01	.02	2	1
SLWL 19+00	1	27	5	57	.1	20	11	310	3.14	13	5	ND	1	12	1	2	2	78	.49	.032	4	27	.44	42	.12	4	2.81	.01	.03	1	1
SLWL 19+50	1	26	20	49	.1	16	8	797	2.68	21	5	ND	1	19	1	2	2	65	.52	.025	3	24	.40	43	.09	2	2.30	.01	.02	2	3
SLWL 20+00	1	22	9	47	.1	16	8	336	2.73	21	5	ND	1	11	1	2	2	66	.38	.017	4	22	.35	39	.10	5	2.72	.01	.04	1	1
SLWL 20+50	1	40	10	57	.1	28	12	313	3.38	23	5	ND	1	15	1	3	2	81	.45	.026	4	29	.53	50	.15	3	3.40	.01	.03	1	1
SLWL 21+00	1	32	15	63	.2	31	13	327	4.02	18	5	ND	1	14	1	2	2	99	.44	.021	6	37	.48	55	.18	7	3.84	.01	.02	1	1
SLWL 21+50	1	61	15	64	.1	30	13	399	4.40	34	5	ND	1	19	1	2	2	114	.48	.027	6	37	.62	80	.20	5	4.42	.01	.03	1	2
SLWL 22+00	1	21	14	88	.1	14	8	1727	3.13	17	5	ND	1	16	1	2	2	67	.38	.114	4	19	.17	85	.13	3	3.07	.01	.03	1	1
SLWL 22+50	1	40	16	67	.1	22	13	599	4.02	39	5	ND	1	12	1	2	2	95	.42	.058	4	31	.40	56	.16	2	4.70	.01	.04	1	1
SLWL 23+00	1	15	18	48	.1	12	8	1032	2.80	7	5	ND	1	13	1	3	2	72	.40	.024	4	20	.21	51	.13	3	2.28	.01	.03	2	2
SLWL 23+50	1	40	18	81	.1	29	15	1102	4.29	15	5	ND	1	14	1	2	2	107	.49	.053	4	37	.43	66	.21	2	4.17	.01	.04	1	1
SLWL 24+00	1	27	11	49	.2	16	8	466	2.96	16	5	ND	1	12	1	2	2	79	.43	.027	4	23	.28	43	.14	3	2.45	.01	.02	1	1
SLWL1 0+00	1	63	20	58	.1	30	15	406	5.09	14	5	ND	1	11	1	2	2	149	.64	.029	4	43	.44	29	.33	4	3.32	.01	.03	1	2
SLWL1 0+50	1	76	8	62	.1	29	14	336	5.19	17	5	ND	1	9	1	2	2	136	.60	.026	4	42	.37	26	.30	7	3.06	.01	.02	1	17
SLWL1 1+00	1	31	20	61	.1	21	13	790	3.97	7	5	ND	1	17	1	2	2	102	.68	.022	4	31	.38	43	.23	4	2.69	.01	.06	1	1
SLWL1 1+50	1	45	17	72	.1	23	16	930	4.97	8	5	ND	1	13	1	2	2	127	.54	.041	4	42	.40	57	.23	2	3.65	.01	.02	1	1
SLWL1 2+00	1	19	28	83	.1	13	11	2237	4.43	6	5	ND	1	17	1	2	2	116	.66	.035	4	28	.22	68	.21	2	2.01	.01	.02	1	1
SLWL1 2+50	4	25	22	66	.2	20	16	2171	4.27	20	5	ND	1	34	1	2	2	106	.84	.041	14	35	.33	49	.21	7	4.40	.01	.02	1	1
SLWL1 3+00	4	14	13	40	.1	13	10	282	3.50	7	5	ND	1	14	1	2	2	94	.41	.015	5	24	.24	26	.18	5	2.77	.01	.01	1	2
SLWL1 3+50	2	28	16	66	.1	16	12	370	4.59	4	5	ND	1	14	1	2	2	125	.60	.029	3	29	.28	30	.26	5	2.68	.01	.02	1	1
SLWL1 4+00	2	19	15	64	.1	11	10	668	4.13	4	5	ND	1	14	1	2	3	102	.52	.043	5	25	.22	38	.23	4	2.17	.01	.03	1	1
SLWL1 4+50	2	44	20	93	.1	27	16	283	5.39	9	5	ND	1	11	1	3	2	132	.46	.050	4	44	.33	44	.27	3	4.80	.01	.02	1	22
SLWL1 5+00	1	21	12	77	.1	12	10	1677	3.41	5	5	ND	1	13	1	2	2	89	.57	.045	4	23	.22	53	.19	4	2.07	.01	.02	1	2
H 1+00S 6+75E	1	58	10	73	.2	39	17	388	5.18	6	5	ND	1	19	1	2	2	161	.96	.032	4	59	.55	77	.38	7	3.16	.01	.02	1	2
H 1+00S 7+00E	1	36	12	78	.3	24	22	1845	5.55	2	5	ND	1	19	1	2	2	157	.97	.027	8	46	.35	33	.47	2	2.78	.01	.02	1	1
H 1+00S 7+25E	1	265	31	108	.4	68	31	1721	7.82	2	5	ND	1	21	1	2	2	222	.58	.062	11	82	.71	57	.30	5	7.99	.01	.04	1	1
H 1+00S 7+50E	1	99	19	93	.3	33	25	1712	6.49	5	5	ND	1	21	1	2	2	179	.73	.044	18	57	.35	43	.49	4	4.04	.01	.04	1	1
H 1+00S 7+75E	1	99	11	77	.3	29	19	575	6.21	7	5	ND	1	20	1	2	2	201	.94	.055	5	38	.63	24	.54	5	4.17	.01	.02	1	8
H 1+00S 8+00E	1	51	12	148	.2	19	24	2466	6.36	8	5	ND	1	16	1	2	2	155	.87	.325	3	35	.28	48	.46	4	3.52	.01	.03	1	1
H 1+00S 8+25E	1	34	13	98	.2	17	19	2706	5.43	6	5	ND	1	14	1	2	2	139	1.04	.263	3	35	.30	47	.44	5	3.01	.01	.02	1	1
H 1+00S 8+50E	1	31	17	112	.1	24	24	4717	5.80	4	5	ND	1	15	1	2	2	153	.97	.176	3	36	.35	83	.55	5	3.21	.01	.02	1	1
H 1+00S 8+75E	1	44	19	108	.1	27	21	2524	5.66	7	5	ND	1	12	1	2	2	162	.93	.148	4	42	.50	54	.56	3	3.84	.01	.03	1	11
H 1+00S 9+00E	1	41	17	91	.1	26	21	2096	6.03	3	5	ND	1	11	1	2	2	172	.82	.172	3	41	.47	46	.57	3	4.13	.01	.03	1	1
H 1+00S 9+25E	1	46	17	100	.2	21	18	1306	6.47	5	5	ND	1	15	1	2	2	191	.97	.110	3	38	.40	43	.62	5	3.10	.01	.04	1	1
H 1+00S 9+50E	1	16	18	58	.2	7	11	1105	6.92	5	5	ND	1	8	1	2	2	200	1.54	.046	4	31	.18	19	.70	5	2.22	.01	.02	1	12
STD C/AU-S	18	57	38	128	7.0	68	27	1032	4.00	38	17	7	36	47	16	18	19	55	.46	.080	38	54	.91	176	.06	34	1.90	.06	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
H 1+00S 9+75E	1	52	13	89	.1	20	23	1350	10.07	2	5	ND	1	12	1	2	2	248	2.04	.053	4	43	.64	27	.74	3	3.17	.01	.03	1	2
H 1+00S 10+00E	1	60	61	135	.1	26	29	5282	8.39	3	5	ND	1	15	1	2	2	168	1.18	.088	4	37	.25	55	.38	4	2.24	.01	.03	1	10
H 1+00S 10+25E	1	31	13	81	.1	21	14	555	5.80	3	5	ND	1	14	1	2	2	169	1.06	.124	3	31	.46	34	.54	4	2.50	.01	.03	1	1
H 1+00S 10+50E	1	76	9	102	.1	53	24	1031	6.59	2	5	ND	1	15	1	2	2	186	.68	.057	7	65	.57	68	.53	8	5.23	.01	.03	1	1
H 1+00S 10+75E	1	526	6	165	.1	61	33	746	12.15	2	5	ND	1	8	1	2	3	249	.21	.143	3	87	1.21	51	.01	2	5.36	.01	.04	1	5
H 1+00S 11+00E	1	66	16	83	.1	41	18	1129	5.76	4	5	ND	1	14	1	2	2	173	.92	.055	6	54	.66	49	.47	9	3.96	.01	.03	1	1
H 1+00S 11+25E	1	52	19	97	.2	25	16	1302	4.97	2	5	ND	1	24	1	2	2	152	1.03	.077	4	34	.40	75	.42	5	2.68	.01	.04	1	1
H 1+00S 11+50E	1	20	11	85	.1	15	17	1659	5.43	3	5	ND	1	15	1	2	3	156	1.16	.121	3	32	.27	39	.55	4	2.08	.01	.03	1	2
H 1+00S 11+75E	1	26	12	133	.2	14	18	3779	4.98	5	5	ND	1	12	1	2	3	118	.90	.258	3	33	.24	73	.34	6	2.63	.01	.03	1	1
H 1+00S 12+00E	1	33	6	60	.1	18	13	338	5.40	2	5	ND	1	14	1	2	2	174	.89	.038	2	30	.41	20	.57	4	2.39	.01	.03	1	4
H 1+00S 12+25E	1	52	3	41	.2	20	31	939	5.02	2	5	ND	1	18	1	2	4	196	1.11	.029	14	46	.41	13	.48	5	3.35	.01	.01	1	2
H 1+00S 12+50E	1	65	14	58	.1	22	15	443	7.70	2	5	ND	1	8	1	3	2	202	.33	.040	3	43	.29	46	.07	2	1.96	.01	.02	1	1
H 1+00S 12+75E	1	54	20	98	.1	41	28	1932	7.80	2	5	ND	1	12	1	2	2	175	.51	.069	5	47	.63	109	.05	4	2.39	.01	.03	1	1
H 1+00S 13+00E	1	55	26	126	.1	38	30	6812	4.64	2	5	ND	1	9	1	2	2	129	.21	.064	6	32	.10	166	.01	2	2.58	.01	.04	1	1
H 1+00S 13+25E	1	73	12	107	.1	38	38	4239	4.28	2	5	ND	1	8	1	2	4	119	.31	.059	27	53	.37	148	.11	3	3.36	.01	.03	1	4
H 1+00S 13+50E	1	27	7	89	.1	21	17	1467	6.88	2	5	ND	1	6	1	2	2	189	.11	.060	2	48	.29	80	.01	2	1.86	.01	.03	1	1
H 1+00S 13+75E	1	118	8	63	.5	53	19	242	4.28	4	5	ND	1	12	1	3	2	127	.53	.047	49	69	.58	60	.25	6	5.57	.01	.02	1	11
H 1+00S 14+00E	1	88	15	117	.5	31	40	1956	4.79	2	5	ND	1	14	1	2	3	119	.50	.111	13	59	.29	52	.17	6	5.24	.01	.04	1	1
H 1+00S 14+25E	1	82	11	100	.1	22	26	2880	6.12	2	5	ND	1	9	1	2	2	135	.24	.112	8	64	.41	79	.04	5	2.40	.01	.03	1	1
H 1+00S 14+50E	1	44	9	73	.1	31	15	378	4.82	5	5	ND	1	15	1	3	4	146	.83	.040	4	49	.44	58	.36	4	2.87	.01	.02	1	7
H 1+00S 14+75E	1	52	11	64	.1	30	18	615	4.68	4	5	ND	1	17	1	2	2	140	.89	.034	4	51	.54	49	.25	5	2.69	.01	.03	1	1
H 1+00S 15+00E	1	59	9	66	.2	40	20	716	5.09	4	5	ND	1	21	1	2	2	158	1.03	.025	5	62	.78	95	.32	4	3.19	.01	.04	1	21
H 1+00S 15+25E	1	41	8	67	.1	30	17	450	5.10	3	5	ND	1	19	1	2	2	162	1.09	.023	3	50	.58	56	.37	8	2.70	.01	.02	1	5
H 1+00S 15+50E	1	79	5	65	.2	36	17	531	4.79	7	5	ND	1	35	1	2	2	139	1.53	.032	7	45	.69	47	.32	8	2.19	.02	.04	1	8
H 1+00S 15+75E	1	32	5	64	.1	27	18	413	4.52	3	5	ND	1	20	1	2	2	137	1.10	.015	4	52	.74	43	.27	5	2.71	.01	.04	1	15
H 1+00S 19+00E	1	7	7	29	.1	4	3	93	2.28	2	5	ND	1	7	1	2	3	55	.18	.016	3	7	.14	60	.01	2	1.13	.01	.03	2	1
H 1+00S 19+25E	1	38	11	50	.2	26	15	302	4.86	4	5	ND	1	14	1	2	2	153	.86	.016	5	43	.55	63	.32	7	2.75	.01	.02	2	7
H 1+00S 19+50E	1	51	8	61	.1	37	17	357	5.65	5	5	ND	1	14	1	2	2	175	.95	.030	5	51	.65	42	.43	4	3.65	.01	.03	1	11
H 1+00S 21+00E	1	8	11	30	.1	3	5	392	1.22	3	5	ND	1	9	1	2	2	28	.17	.012	6	5	.11	108	.01	4	.81	.01	.07	2	8
H 1+00S 21+25E	1	19	13	71	.2	8	7	329	1.75	4	5	ND	1	5	1	2	2	31	.16	.051	8	8	.22	55	.01	2	1.39	.01	.06	1	1
H 1+00S 21+50E	1	5	6	23	.1	2	2	384	.72	2	5	ND	2	3	1	2	2	16	.04	.028	7	4	.05	57	.01	2	.74	.01	.03	2	16
H 1+00S 21+75E	1	9	9	53	.3	5	4	371	1.07	2	5	ND	1	3	1	2	2	23	.06	.029	5	5	.10	42	.01	2	1.29	.01	.04	2	2
H 1+00S 22+00E	1	36	19	81	.1	18	13	2409	3.76	4	5	ND	1	15	1	2	3	95	.63	.095	5	27	.37	130	.14	3	2.39	.01	.04	1	12
H 1+00S 22+25E	1	8	11	75	.1	5	5	3241	1.13	3	5	ND	1	8	1	2	4	26	.13	.057	5	6	.12	173	.01	2	1.79	.01	.04	1	5
H 1+00S 22+50E	1	33	13	98	.2	17	12	1140	3.51	5	5	ND	2	10	1	2	2	76	.39	.063	4	21	.37	100	.04	2	2.43	.01	.04	1	3
H 1+00S 22+75E	1	55	12	92	.1	25	18	1375	5.68	6	5	ND	1	11	1	2	2	141	.53	.092	4	36	.41	84	.19	2	3.61	.01	.04	1	1
STD C/AU-S	18	57	39	132	7.1	68	28	1077	4.08	38	18	8	36	47	18	16	20	56	.48	.088	39	55	.95	174	.06	32	2.00	.06	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
H 1+00S 23+00E	1	54	12	92	.1	35	15	317	5.47	7	5	ND	1	13	1	2	2	152	.55	.028	4	53	.47	99	.24	2	3.66	.01	.04	1	2
H 1+00S 23+25E	1	59	6	98	.1	36	14	476	3.85	2	5	ND	1	20	1	2	2	134	.95	.027	7	83	.64	255	.31	2	3.68	.01	.03	1	1

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: SEP 9 1988 DATE REPORT MAILED: Sept 15/88 ASSAYER. C. Leong ..D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-4365 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L7+00N 0+50W	6	226	17	62	.1	34	11	222	6.26	49	5	ND	1	7	1	2	2	111	.12	.025	4	71	.63	91	.08	2	6.38	.01	.04	1	10
L7+00N 0+25W	4	141	16	56	.3	24	8	179	6.61	42	5	ND	1	5	1	2	2	124	.11	.040	5	66	.41	50	.06	2	5.29	.01	.04	1	69
L7+00N 0+00E	4	217	19	50	.7	19	7	131	5.57	57	5	ND	1	4	1	3	3	82	.08	.042	3	58	.53	36	.09	2	7.13	.01	.05	2	14
L7+00N 0+25E	4	235	18	53	.5	20	8	143	5.40	57	5	ND	1	4	1	2	2	82	.09	.040	3	59	.54	40	.09	2	7.41	.01	.03	1	12
L7+00N 0+50E	3	116	15	72	.4	24	9	228	6.70	42	5	ND	2	5	1	2	4	110	.13	.044	5	65	.45	41	.06	2	5.79	.01	.05	1	3
L7+00N 0+75E	5	239	13	63	.3	20	7	260	4.78	52	5	ND	1	5	1	2	2	75	.10	.070	3	52	.57	49	.07	2	6.09	.01	.04	1	16
L7+00N 1+00E	4	145	14	62	.3	22	8	156	5.22	41	5	ND	1	5	1	2	2	97	.14	.048	4	50	.36	34	.06	2	4.80	.01	.02	1	7
L7+00N 1+25E	4	187	17	68	.1	29	11	334	5.32	60	5	ND	1	7	1	2	2	91	.15	.070	6	55	.63	68	.08	2	5.08	.01	.06	1	20
L7+00N 1+50E	3	208	12	78	.2	21	10	687	4.94	50	5	ND	1	6	1	2	3	99	.17	.042	4	44	.33	54	.06	2	3.62	.01	.01	1	17
L7+00N 1+75E	3	81	10	54	.4	17	7	259	4.84	45	5	ND	1	6	1	2	3	106	.21	.037	4	39	.30	30	.07	2	3.32	.01	.03	1	4
L7+00N 2+00E	1	41	10	38	.3	10	4	132	4.59	39	5	ND	1	6	1	2	3	128	.20	.026	4	33	.20	17	.09	2	2.06	.01	.03	1	2
L7+00N 2+25E	1	80	17	54	.1	12	6	170	3.71	53	5	ND	1	7	1	2	2	104	.21	.024	4	31	.18	29	.09	3	2.37	.01	.03	1	15
L7+00N 2+50E	2	145	17	79	.1	36	13	259	5.35	68	5	ND	2	7	1	2	2	111	.27	.025	4	54	.65	63	.16	4	5.07	.01	.04	1	19
L7+00N 2+75E	2	98	15	73	.1	30	18	235	4.39	73	5	ND	2	10	1	2	2	114	.25	.027	5	45	.41	42	.10	2	3.62	.01	.05	1	12
L7+00N 3+00E	2	87	14	57	.1	21	8	162	5.52	48	5	ND	1	7	1	2	3	124	.21	.034	4	46	.29	37	.12	2	4.16	.01	.04	1	4
L7+00N 3+25E	1	26	20	53	.1	14	33	930	3.96	21	5	ND	1	10	1	2	2	97	.23	.043	6	33	.34	32	.14	2	1.66	.01	.05	1	42
L7+00N 3+50E	2	52	16	169	.2	28	28	2647	6.81	53	5	ND	2	12	1	2	3	140	.34	.059	7	71	.47	64	.13	2	3.96	.01	.05	1	10
L7+00N 3+75E	2	125	14	123	.6	52	33	2865	4.85	1492	5	ND	2	19	1	2	2	77	.56	.070	8	70	.43	63	.06	3	5.95	.01	.04	1	3
L7+00N 4+00E	2	98	16	93	.4	28	31	1678	4.26	381	5	ND	3	17	1	2	2	78	.46	.052	7	45	.38	53	.08	2	4.12	.01	.04	1	35
L7+00N 4+25E	2	119	10	68	.1	25	13	363	4.69	137	5	ND	2	12	1	2	2	105	.35	.025	5	46	.55	58	.12	2	3.31	.01	.06	1	39
L7+00N 4+50E	3	78	10	54	.1	18	9	316	4.03	64	5	ND	1	9	1	2	2	99	.32	.022	5	36	.41	41	.10	2	2.44	.01	.04	1	17
L7+00N 4+75E	2	152	12	62	.1	29	15	420	4.37	71	5	ND	2	11	1	2	2	92	.36	.021	5	46	.65	63	.13	2	3.62	.01	.06	1	19
L7+00N 5+00E	2	66	14	46	.1	16	6	152	4.49	88	5	ND	2	7	1	2	2	109	.26	.022	4	39	.29	25	.14	2	2.76	.01	.04	1	14
L7+00N 5+25E	3	68	12	72	.1	19	9	337	5.17	566	5	ND	2	13	1	2	2	116	.41	.025	6	41	.36	37	.11	2	2.73	.01	.05	1	11
L7+00N 5+50E	3	87	16	78	.5	39	28	909	4.52	1073	5	ND	2	20	1	2	2	79	.58	.039	9	63	.46	48	.10	2	5.18	.01	.04	1	30
L7+00N 5+75E	2	56	11	60	.3	27	14	267	3.51	414	5	ND	2	12	1	2	2	73	.45	.017	5	44	.51	37	.11	2	3.17	.01	.04	1	16
L7+00N 6+25E	2	41	10	45	.3	9	4	97	5.72	44	5	ND	1	4	1	2	2	138	.11	.043	5	42	.23	16	.11	2	2.98	.01	.03	1	29
L7+00N 6+50E	2	106	16	74	.3	21	8	156	5.26	43	5	ND	1	5	1	2	2	97	.15	.060	4	49	.32	29	.10	2	5.28	.01	.03	1	7
L7+00N 6+75E	3	154	16	79	.5	22	9	203	4.54	39	5	ND	1	6	1	2	2	88	.16	.051	4	40	.41	37	.09	2	4.66	.01	.05	1	20
L5+00N 0+25W	1	25	11	43	.2	8	3	109	4.84	16	5	ND	1	6	1	2	2	114	.17	.031	5	31	.14	14	.08	2	1.57	.01	.04	1	3
L5+00N B/L W	1	27	12	34	.1	10	4	130	5.47	19	5	ND	1	6	1	2	2	122	.17	.032	6	36	.18	14	.08	2	1.75	.01	.05	2	11
L5+00N 0+00E	4	30	11	26	.3	5	2	134	2.15	27	5	ND	1	5	1	2	2	71	.12	.022	4	18	.09	13	.06	2	1.03	.01	.04	1	6
L5+00N 0+25E	4	62	19	42	.2	14	5	143	4.57	36	5	ND	1	5	1	2	2	97	.11	.029	6	34	.26	27	.04	2	2.28	.01	.05	1	12
L5+00N 0+75E	2	58	11	44	.1	15	6	118	6.58	32	5	ND	2	6	1	2	3	153	.16	.037	5	49	.22	18	.10	2	2.56	.01	.05	1	4
L5+00N 1+00E	5	85	11	38	.5	13	5	101	4.06	47	5	ND	1	5	1	3	2	94	.13	.031	4	34	.22	23	.04	2	2.45	.01	.05	2	5
L5+00N 1+25E	6	169	19	64	.4	28	11	195	5.62	70	5	ND	1	6	1	2	2	106	.13	.037	5	54	.50	58	.06	2	4.95	.01	.05	1	40
STD C/AU-S	18	57	42	132	6.8	67	29	1059	4.16	38	16	8	38	48	18	16	19	59	.49	.088	39	56	.88	181	.07	32	1.98	.06	.14	12	52

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-4365

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+00N 1+50E	5	124	14	64	.3	17	6	138	5.34	51	5	ND	1	5	1	2	2	100	.12	.048	4	44	.28	32	.05	2	3.75	.01	.05	1	16
L5+00N 1+75E	2	94	12	53	.3	17	7	148	5.27	35	5	ND	1	5	1	2	2	105	.11	.035	5	46	.23	29	.03	2	3.73	.01	.05	1	11
L5+00N 2+00E	3	27	6	22	.1	4	2	54	4.15	33	5	ND	1	3	1	2	2	106	.06	.026	5	26	.04	8	.08	2	1.13	.01	.05	2	9
L5+00N 2+50E	1	24	13	45	.1	12	6	133	4.03	18	5	ND	1	8	1	2	2	113	.23	.023	5	32	.23	25	.12	2	2.31	.01	.03	1	2
L5+00N 2+75E	1	86	20	79	.1	45	19	721	7.24	41	5	ND	2	13	1	2	2	135	.36	.054	3	78	.58	32	.05	7	3.81	.01	.03	1	49
L5+00N 3+00E	1	66	17	76	.1	36	15	602	5.36	32	5	ND	2	13	1	2	2	135	.49	.058	3	70	.55	38	.09	6	3.58	.01	.04	1	7
L5+00N 3+50E	1	10	4	20	.1	4	4	190	2.38	23	5	ND	1	11	1	2	2	53	.28	.044	3	11	.08	24	.01	4	.90	.01	.04	1	1
L5+00N 3+75E	1	19	9	48	.1	5	5	230	4.10	123	5	ND	1	8	1	2	2	129	.25	.068	4	40	.20	20	.18	3	1.22	.01	.03	2	1
L5+00N 4+00E	2	47	13	55	.1	15	6	278	4.51	69	5	ND	2	8	1	3	2	119	.27	.056	4	36	.25	25	.13	2	2.42	.01	.05	1	13
L5+00N 4+25E	2	29	7	31	.1	8	4	152	4.51	77	5	ND	1	5	1	2	2	146	.12	.031	4	35	.13	20	.15	2	1.95	.01	.04	1	1
L5+00N 4+50E	3	15	7	27	.1	6	3	73	3.55	64	5	ND	1	5	1	2	2	170	.13	.012	4	32	.12	12	.20	2	1.02	.01	.02	1	3
L5+00N 4+75E	2	19	4	48	.1	5	4	147	2.65	132	5	ND	1	9	1	3	2	49	.22	.021	3	14	.11	20	.01	2	1.24	.01	.03	2	27
L5+00N 5+00E	2	49	10	72	.1	15	14	664	3.90	226	5	ND	2	14	1	5	2	65	.39	.029	5	29	.37	42	.02	5	1.76	.01	.05	1	4
L5+00N 5+25E	2	86	8	92	.1	24	19	441	4.29	215	5	ND	2	32	1	2	2	74	.37	.024	4	37	.51	46	.05	3	2.49	.01	.06	1	15
L5+00N 5+50E	2	65	7	73	.1	19	11	283	4.32	220	5	ND	1	8	1	2	2	75	.23	.022	4	34	.39	57	.02	3	2.47	.01	.03	1	3
L5+00N 5+75E	2	131	12	58	.1	31	15	288	4.10	48	5	ND	1	10	1	2	2	94	.31	.023	6	49	.66	55	.15	2	3.55	.01	.04	1	5
L5+00N 6+00E	2	52	5	35	.1	11	5	123	3.61	29	5	ND	1	4	1	2	2	88	.13	.021	5	28	.21	22	.04	2	2.06	.01	.04	1	7
L2+75N B/L	2	86	19	75	.4	23	8	272	5.15	46	5	ND	4	13	1	2	2	100	.89	.055	5	45	.41	49	.05	2	3.02	.01	.06	1	15
L2+75N 0+75E	4	97	7	32	.1	11	4	75	4.11	76	5	ND	1	4	1	2	3	94	.06	.021	4	29	.20	26	.05	2	2.30	.01	.04	1	26
L2+75N 1+00E	3	83	15	75	.1	24	7	131	8.09	61	5	ND	1	4	1	2	2	152	.10	.042	5	83	.47	26	.08	2	3.98	.01	.06	1	1
L2+75N 1+25E	5	158	17	64	.3	25	8	159	6.36	55	5	ND	2	5	1	2	2	116	.12	.042	5	62	.38	52	.04	2	5.65	.01	.05	1	153
L2+75N 1+50E	5	141	10	83	.2	35	11	247	7.04	59	5	ND	1	8	1	2	2	132	.18	.044	6	53	.65	66	.07	2	4.27	.01	.05	1	5
L2+75N 1+75E	4	103	11	78	.1	29	10	264	5.99	119	5	ND	2	6	1	2	2	106	.18	.028	5	50	.63	68	.05	2	3.38	.01	.05	1	4
L2+75N 2+00E	3	130	15	82	.2	32	12	219	5.73	40	5	ND	2	5	1	2	2	102	.16	.034	4	56	.53	36	.06	2	5.35	.01	.05	1	11
L2+75N 2+25E	2	99	11	50	.2	19	6	135	4.37	84	5	ND	1	5	1	2	2	103	.16	.025	4	43	.34	26	.09	2	3.89	.01	.04	1	8
L2+75N 2+50E	3	100	10	39	.6	14	4	95	3.49	69	5	ND	1	5	1	2	2	88	.13	.021	4	33	.26	20	.08	2	2.71	.01	.04	1	29
L2+75N 2+75E	2	68	10	43	.3	13	4	107	3.49	59	5	ND	1	4	1	2	2	83	.15	.024	4	29	.22	21	.08	2	2.65	.01	.04	2	12
L2+75N 3+00E	2	57	15	41	.5	10	4	87	5.43	75	5	ND	1	5	1	2	3	120	.14	.086	3	45	.23	13	.14	2	4.02	.01	.04	1	7
L2+75N 3+25E	1	29	8	37	.3	9	3	91	4.40	62	5	ND	1	4	1	2	2	111	.15	.065	4	30	.15	14	.12	2	1.79	.01	.02	1	21
L2+75N 3+50E	1	86	10	62	.4	25	10	250	4.32	45	5	ND	2	6	1	2	2	95	.26	.047	4	39	.43	44	.12	2	3.50	.01	.05	1	14
L2+75N 3+75E	1	90	10	67	.3	18	11	740	4.03	45	5	ND	2	6	1	2	2	90	.21	.066	5	39	.28	32	.10	2	2.90	.01	.04	1	6
L2+75N 4+00E	2	54	11	76	.2	17	15	482	5.50	87	5	ND	2	8	1	2	2	122	.20	.041	4	44	.19	43	.11	2	3.06	.01	.03	1	8
L2+75N 4+25E	3	95	11	85	.2	30	31	1101	4.99	95	5	ND	2	8	1	3	3	96	.27	.034	7	48	.47	50	.12	2	4.04	.01	.05	1	11
L2+75N 4+50E	2	36	11	68	.4	11	5	143	4.32	38	5	ND	2	6	1	2	2	108	.15	.041	5	29	.20	28	.07	2	2.48	.01	.04	1	6
L2+75N 4+75E	1	35	9	34	.1	8	3	99	3.89	23	5	ND	2	3	1	2	2	102	.12	.033	5	28	.13	15	.07	2	1.51	.01	.02	1	3
L2+75N 5+00E	2	67	9	55	.1	14	5	125	3.84	26	5	ND	1	4	1	2	2	87	.09	.037	5	34	.20	22	.04	2	2.83	.01	.02	1	4
STD C/AU-S	18	58	44	132	6.6	68	29	1014	4.12	42	19	7	38	48	18	17	18	59	.50	.090	39	56	.89	181	.07	32	2.00	.06	.13	12	51

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-4365

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L2+75N 5+25E	2	67	10	55	.4	16	6	181	4.62	49	5	ND	3	5	1	2	3	106	.17	.042	5	34	.29	23	.08	2	3.22	.01	.03	1	42
L2+75N 5+50E	2	62	14	76	.5	16	6	131	5.40	48	5	ND	3	5	1	2	2	139	.16	.046	4	45	.28	22	.10	2	4.45	.01	.02	1	79
L2+75N 5+75E	2	54	9	59	.1	17	5	132	4.25	45	5	ND	2	6	1	2	2	97	.19	.032	5	31	.24	26	.08	2	2.71	.01	.03	1	2
L2+75N 6+00E	2	71	16	63	.3	24	8	222	4.14	53	5	ND	3	7	1	2	2	92	.24	.038	4	36	.37	30	.10	3	3.52	.01	.05	1	1
L2+75N 6+25E	2	55	11	41	.1	16	6	217	4.46	46	5	ND	2	6	1	2	2	112	.20	.029	4	34	.22	24	.10	3	2.73	.01	.04	1	3
L1+00N 0+41W	2	87	12	50	.1	20	7	164	6.15	36	5	ND	2	4	1	2	2	120	.14	.038	5	48	.35	26	.07	2	3.90	.01	.03	1	1
L1+00N 0+25W	2	47	10	48	.1	13	5	111	5.45	33	5	ND	2	5	1	2	2	122	.15	.029	6	34	.23	24	.04	3	2.55	.01	.02	2	1
L1+00N 0+00E	1	45	10	51	.1	12	5	117	6.51	26	5	ND	2	4	1	2	2	137	.13	.041	5	42	.19	12	.05	2	2.21	.01	.03	2	6
L1+00N 0+50E	1	41	11	36	.1	10	7	130	4.39	21	5	ND	2	5	1	2	2	110	.11	.026	7	30	.13	19	.03	2	2.12	.01	.03	1	1
L1+00N 0+75E	2	107	13	89	.2	36	16	276	6.71	36	5	ND	4	7	1	2	2	123	.23	.037	5	58	.49	43	.07	2	5.03	.01	.05	1	1
L1+00N 1+00E	2	96	18	79	.1	31	14	333	5.77	40	5	ND	3	7	1	2	2	116	.24	.041	6	48	.48	42	.05	2	3.92	.01	.04	1	2
L1+00N 1+25E	3	137	12	92	.1	42	19	350	6.35	62	5	ND	2	6	1	2	2	120	.19	.048	6	53	.63	55	.07	2	4.68	.01	.04	1	1
L1+00N 1+50E	2	139	18	80	.1	40	14	309	5.60	64	5	ND	4	6	1	2	2	107	.23	.038	5	52	.67	47	.12	3	5.35	.01	.05	1	1
L1+00N 1+75E	3	40	14	41	.1	14	5	134	4.72	43	5	ND	2	6	1	2	2	124	.19	.033	5	31	.22	21	.06	2	1.77	.01	.03	1	1
L1+00N 2+00E	3	90	11	71	.2	25	12	278	5.35	52	5	ND	3	6	1	2	2	122	.22	.044	5	43	.37	32	.10	3	3.58	.01	.04	1	3
L1+00N 2+25E	3	64	17	51	.2	17	7	245	4.37	42	5	ND	3	7	1	2	2	92	.19	.034	5	32	.30	41	.05	2	2.65	.01	.04	1	2
L1+00N 2+50E	2	80	21	64	.2	22	9	224	4.25	45	5	ND	3	9	1	2	3	94	.26	.043	4	35	.35	45	.08	3	3.31	.01	.04	1	1
L1+00N 2+75E	3	110	13	73	.1	31	13	249	5.19	51	5	ND	3	8	1	3	2	112	.28	.038	4	46	.46	39	.13	2	4.74	.01	.04	1	5
L1+00N 3+00E	2	85	23	74	.1	27	11	384	4.52	45	5	ND	3	9	1	2	3	94	.31	.033	5	38	.51	45	.10	3	3.47	.01	.05	1	28
L1+00N 3+25E	3	190	14	88	.1	44	18	315	5.77	80	5	ND	3	8	1	3	2	113	.26	.036	5	56	.71	68	.13	3	5.87	.01	.06	1	8
L1+00N 3+50E	2	65	11	57	.1	19	8	250	4.76	45	5	ND	3	9	1	2	2	108	.22	.037	5	34	.31	40	.07	2	2.83	.01	.06	1	18
L1+00N 3+75E	2	78	11	62	.1	26	13	270	4.23	33	5	ND	3	9	1	2	3	94	.23	.036	6	36	.39	37	.05	3	3.18	.01	.04	1	42
L1+00N 4+00E	2	96	12	73	.2	29	16	537	4.67	43	5	ND	3	12	1	2	2	93	.30	.034	7	40	.54	46	.06	2	3.78	.01	.05	1	11
L1+00N 4+25E	3	182	15	81	.1	40	17	339	5.46	71	5	ND	3	13	1	2	2	107	.28	.040	6	50	.64	78	.08	2	5.08	.01	.07	1	8
L1+00N 4+50E	3	94	10	43	.1	20	7	173	5.83	73	5	ND	3	7	1	3	3	124	.17	.025	5	43	.37	35	.07	2	3.59	.01	.05	1	34
L1+00N 5+00E	4	113	15	89	.5	33	13	264	4.93	30	5	ND	2	10	1	2	2	98	.15	.043	5	44	.50	58	.05	3	4.80	.01	.06	1	7
L1+00N 5+25E	2	62	11	50	.1	16	6	146	5.02	39	5	ND	2	5	1	2	2	109	.12	.035	6	40	.28	28	.04	2	2.93	.01	.03	1	8
L1+00N 5+50E	1	35	12	37	.2	9	4	151	4.43	26	5	ND	2	5	1	2	3	108	.13	.028	5	29	.18	20	.05	2	2.21	.01	.02	1	3
L1+00N 5+75E	3	128	14	69	.1	32	11	279	5.05	50	5	ND	3	5	1	2	2	93	.17	.040	4	47	.49	39	.06	3	5.48	.01	.05	1	6
L1+00N 6+00E	2	80	12	53	.4	15	6	170	3.82	49	5	ND	3	5	1	2	2	87	.16	.031	5	31	.32	26	.07	2	2.75	.01	.05	1	11
L1+00N 6+25E	2	167	11	72	.1	37	18	503	4.95	67	5	ND	4	26	1	3	3	108	.53	.034	7	51	.75	46	.15	3	3.66	.01	.07	1	10
L1+00N 6+50E	2	121	18	56	.3	24	8	257	4.13	46	5	ND	3	7	1	3	2	83	.21	.037	5	37	.41	38	.06	5	3.57	.01	.06	1	5
BL 4+50E 11+75N	2	83	14	58	.2	22	10	263	4.96	62	5	ND	3	9	1	3	3	111	.23	.022	6	43	.40	44	.08	2	3.44	.01	.05	1	6
BL 4+50E 11+50N	5	61	10	44	.2	15	11	138	4.15	47	5	ND	3	6	1	3	2	94	.22	.024	5	30	.23	23	.12	2	2.58	.01	.04	1	11
BL 4+50E 11+25N	3	73	10	61	.1	21	8	206	5.41	51	5	ND	3	7	1	2	2	111	.22	.030	5	40	.42	32	.10	2	2.72	.01	.02	1	16
STD C/AU-S	18	59	41	132	6.7	67	29	1020	4.12	38	21	8	40	49	18	17	19	60	.49	.090	40	56	.88	179	.07	33	2.04	.06	.14	13	48

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-4365

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
BL 4+50E 11+00N	3	59	5	40	.1	15	6	219	3.98	30	5	ND	1	5	1	2	3	82	.17	.021	4	31	.30	24	.07	2	2.12	.01	.03	1	1
BL 4+50E 10+75N	3	89	11	63	.1	23	9	207	5.10	45	5	ND	1	7	1	2	2	101	.19	.029	4	43	.40	35	.08	2	3.34	.01	.04	1	33
BL 4+50E 10+50N	3	86	12	68	.3	24	9	167	5.36	43	5	ND	1	6	1	2	2	114	.18	.036	4	44	.32	31	.11	2	3.59	.01	.04	1	22
BL 4+50E 10+25N	2	146	13	56	.1	30	16	463	4.28	64	5	ND	2	11	1	2	2	89	.39	.030	4	43	.62	47	.13	2	3.02	.01	.05	1	27
BL 4+50E 10+00N	4	84	11	72	.2	31	22	956	4.45	34	5	ND	2	13	1	2	2	95	.39	.029	6	46	.64	52	.16	2	3.40	.01	.06	1	6
BL 4+50E 9+75N	2	69	8	45	.1	19	9	363	3.88	34	5	ND	1	9	1	2	2	98	.35	.024	5	35	.39	28	.15	2	2.37	.01	.02	1	12
BL 4+50E 9+50N	2	120	12	69	.2	28	12	276	4.22	42	5	ND	1	7	1	2	2	97	.28	.023	4	46	.53	35	.15	2	3.66	.01	.04	1	1
BL 4+50E 9+25N	2	44	9	60	.3	11	6	130	4.62	45	5	ND	1	6	1	3	3	118	.23	.047	5	42	.23	21	.17	4	2.74	.01	.03	1	4
BL 4+50E 9+00N	2	58	7	45	.2	16	7	219	4.34	37	5	ND	1	6	1	2	2	121	.25	.033	4	39	.29	20	.16	2	2.41	.01	.03	1	6
BL 4+50E 8+75N	2	44	9	44	.1	13	6	271	3.65	54	5	ND	1	7	1	2	2	100	.23	.036	4	31	.23	20	.11	2	1.82	.01	.02	1	42
BL 4+50E 8+50N	2	63	10	48	.4	15	6	388	4.53	60	5	ND	1	7	1	2	4	114	.26	.040	4	38	.30	22	.13	2	2.59	.01	.02	1	5
BL 4+50E 8+25N	3	127	17	70	.3	26	12	413	4.38	65	5	ND	1	10	1	2	2	86	.22	.034	4	40	.41	47	.08	2	3.57	.01	.04	1	4
BL 4+50E 8+00N	2	110	10	74	.2	31	28	834	4.85	56	5	ND	2	11	1	2	3	96	.35	.027	5	45	.58	56	.12	2	3.19	.01	.05	1	11
BL 4+50E 7+75N	3	124	9	69	.2	23	14	402	4.62	37	5	ND	1	8	1	2	2	98	.29	.033	5	51	.59	39	.13	2	4.18	.01	.02	1	10
BL 4+50E 7+50N	3	109	12	64	.3	24	11	412	4.56	72	5	ND	1	8	1	3	2	103	.27	.047	4	45	.42	41	.11	2	3.48	.01	.05	1	67
BL 4+50E 7+25N	2	127	9	60	.3	25	13	545	4.10	70	5	ND	1	9	1	2	2	92	.31	.024	4	43	.53	47	.12	2	3.07	.01	.05	1	25
BL 4+50E 7+00N	2	137	14	61	.1	29	15	494	4.06	62	5	ND	1	11	1	3	2	87	.38	.033	5	42	.61	50	.13	2	3.14	.01	.05	1	23
BL 4+50E 6+75N	2	150	11	58	.2	30	16	612	4.26	82	5	ND	2	14	1	2	2	93	.47	.037	5	44	.67	56	.14	5	3.41	.01	.04	1	13
BL 4+50E 6+50N	3	49	7	31	.1	15	5	109	4.85	74	5	ND	1	6	1	2	2	143	.16	.025	4	42	.19	25	.15	2	2.37	.01	.01	1	11
BL 4+50E 6+25N	5	52	8	55	.4	18	7	132	3.86	78	5	ND	1	6	1	2	2	98	.17	.036	4	38	.24	30	.07	2	3.02	.01	.02	1	6
BL 4+50E 6+00N	5	78	12	86	.2	28	11	216	5.84	131	5	ND	1	8	1	2	2	114	.25	.053	4	54	.39	39	.14	2	4.34	.01	.03	1	1
BL 4+50E 5+75N	2	58	9	49	.5	14	6	155	5.31	42	5	ND	1	7	1	2	2	145	.19	.069	4	52	.24	23	.15	3	3.35	.01	.04	2	1
BL 4+50E 5+50N	11	42	12	62	.1	19	7	197	3.61	106	5	ND	1	9	1	2	2	79	.22	.030	4	38	.40	33	.11	3	3.01	.01	.04	1	14
BL 4+50E 5+25N	10	31	12	43	.1	18	8	139	3.06	46	5	ND	1	13	1	2	2	129	.38	.023	5	47	.45	29	.13	2	3.32	.01	.02	1	13
BL 4+50E 5+00N	3	12	5	23	.1	5	2	78	3.60	45	5	ND	1	5	1	3	2	157	.14	.012	4	32	.09	11	.21	2	1.04	.01	.02	1	1
BL 4+50E 4+75N	2	70	7	141	.1	23	20	855	4.56	315	5	ND	1	16	1	14	2	75	.45	.027	4	38	.46	50	.03	9	2.33	.01	.03	1	10
BL 4+50E 4+50N	1	109	9	66	.2	28	16	402	4.03	46	5	ND	2	13	1	2	2	85	.51	.033	5	40	.71	45	.13	2	2.66	.02	.05	1	9
BL 4+50E 4+25N	2	178	12	60	.2	31	16	331	4.32	52	5	ND	1	15	1	2	2	89	.31	.025	8	49	.70	56	.13	2	3.41	.01	.05	1	36
BL 4+50E 4+00N	3	79	18	75	.2	15	6	157	6.56	64	5	ND	1	6	1	2	2	111	.10	.258	3	67	.21	22	.11	2	10.54	.01	.03	2	1
BL 4+50E 3+75N	3	108	11	68	.5	25	11	334	4.78	38	5	ND	1	7	1	3	2	96	.19	.051	6	45	.51	48	.06	2	3.51	.01	.05	1	30
BL 4+50E 3+50N	4	105	14	57	.2	22	7	190	5.92	62	5	ND	1	6	1	2	2	153	.14	.051	5	54	.27	37	.09	2	3.69	.01	.04	1	1
BL 4+50E 3+25N	2	72	10	74	.7	25	9	227	4.43	30	5	ND	1	6	1	2	2	99	.25	.040	5	44	.40	38	.11	2	4.03	.01	.04	1	1
BL 4+50E 3+00N	3	124	14	115	.2	35	14	244	6.42	57	5	ND	2	6	1	2	2	128	.20	.070	4	59	.44	50	.09	2	5.08	.01	.05	1	3
BL 4+50E 2+75N	2	36	11	60	.3	12	5	121	4.69	36	5	ND	1	5	1	3	2	123	.12	.041	5	34	.18	26	.09	2	2.32	.01	.02	1	1
BL 4+50E 2+50N	4	116	12	69	.6	30	12	215	5.00	40	5	ND	1	8	1	2	2	102	.22	.034	5	46	.41	48	.07	2	4.06	.01	.03	1	4
BL 4+50E 2+25N	3	98	11	83	.5	19	9	135	6.24	51	5	ND	1	6	1	2	2	127	.16	.048	7	53	.27	53	.10	2	3.57	.01	.02	1	5
STD C/AU-S	13	58	40	132	6.8	68	29	1056	4.09	39	18	8	38	49	17	17	18	59	.50	.090	40	57	.89	181	.07	32	2.01	.06	.14	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
BL 4+50E 2+00N	2	27	7	34	.1	9	4	263	3.81	26	5	ND	1	6	1	2	2	101	.20	.039	6	29	.20	22	.07	2	1.52	.01	.03	1	20
BL 4+50E 1+75N	5	235	14	93	.6	58	21	333	6.13	54	5	ND	1	9	1	13	2	117	.18	.042	5	69	.70	102	.06	2	6.06	.01	.08	4	11
BL 4+50E 1+50N	3	117	15	94	.1	31	11	304	5.72	60	5	ND	1	7	1	5	2	106	.18	.055	5	51	.49	45	.07	2	4.06	.01	.06	1	16
BL 4+50E 1+25N	4	69	3	53	.4	22	22	1069	3.65	29	5	ND	1	14	1	2	2	82	.28	.022	10	35	.50	35	.06	3	2.37	.01	.05	1	135
BL 4+50E 1+00N	3	83	16	44	.3	21	8	195	5.02	61	5	ND	1	9	1	3	2	108	.16	.028	6	39	.34	39	.07	2	2.76	.01	.05	1	21
BL 4+50E 0+75N	3	138	12	58	.1	25	10	203	5.57	62	5	ND	1	6	1	3	2	113	.16	.039	5	53	.44	32	.06	2	4.09	.01	.03	1	14
BL 4+50E 0+50N	3	51	14	45	.1	14	6	127	5.27	44	5	ND	1	6	1	2	2	116	.15	.048	5	38	.22	39	.05	2	2.57	.01	.02	1	38
BL 4+50E 0+25N	2	30	5	29	.1	11	4	118	4.61	48	5	ND	1	7	1	2	2	122	.19	.034	5	33	.20	18	.10	2	1.57	.01	.03	1	9

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: SEP 15 1988 DATE REPORT MAILED: ASSAYER.........D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-4521 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L11+00N 0+25W	1	76	16	55	.3	18	8	245	5.34	35	5	ND	2	6	1	2	2	95	.13	.049	3	37	.22	29	.05	2	3.02	.01	.06	1	8
L11+00N 0+00E	3	122	7	75	.3	36	10	245	5.47	41	5	ND	1	6	1	4	2	91	.15	.044	2	47	.50	76	.06	4	3.85	.01	.07	1	18
L11+00N 0+25E	1	150	12	103	.2	46	17	279	5.20	54	5	ND	2	7	1	2	2	108	.24	.034	4	51	.62	64	.14	7	4.97	.01	.08	1	172
L11+00N 0+50E	1	91	11	47	.3	13	6	108	4.00	57	5	ND	1	8	1	7	2	83	.13	.053	3	33	.27	37	.06	4	2.70	.01	.06	2	32
L11+00N 0+75E	1	177	9	97	.1	41	18	343	4.62	80	5	ND	1	7	1	6	2	86	.21	.052	4	44	.61	55	.10	5	4.74	.01	.05	3	24
L11+00N 1+00E	1	124	7	82	.1	27	12	234	5.37	72	5	ND	1	6	1	2	2	117	.20	.051	4	46	.44	43	.12	4	4.21	.01	.04	1	45
L11+00N 1+25E	1	56	7	54	.3	16	6	185	4.92	28	5	ND	2	7	1	2	3	107	.21	.045	4	36	.25	25	.08	2	2.78	.01	.06	1	19
L11+00N 1+50E	1	70	10	45	.2	12	6	137	4.60	26	5	ND	1	6	1	2	5	95	.13	.034	3	31	.22	25	.05	4	2.41	.01	.04	1	38
L11+00N 1+75E	1	71	11	60	.1	14	7	107	6.17	50	5	ND	1	6	1	7	2	121	.12	.046	3	38	.25	25	.06	2	2.82	.01	.04	2	22
L11+00N 2+00E	2	103	9	65	.1	25	11	278	5.04	33	5	ND	1	6	1	2	2	98	.15	.034	4	37	.37	45	.07	5	3.57	.01	.06	1	8
L11+00N 2+25E	2	89	4	66	.1	23	13	262	5.08	38	5	ND	1	7	1	2	2	104	.17	.034	5	35	.31	44	.07	4	3.49	.01	.05	1	22
L11+00N 2+50E	1	56	9	45	.2	14	6	272	3.76	28	5	ND	1	5	1	2	2	92	.16	.017	5	29	.29	29	.07	3	2.20	.01	.06	1	15
L11+00N 2+75E	2	53	12	55	.1	17	10	385	4.33	27	5	ND	1	8	1	2	4	88	.21	.024	5	31	.38	38	.07	3	2.14	.01	.03	1	23
L11+00N 3+00E	2	99	4	86	.2	31	12	273	5.37	50	5	ND	1	6	1	3	2	99	.20	.028	4	43	.51	54	.11	4	3.97	.01	.05	1	4
L11+00N 3+25E	2	115	15	78	.1	24	9	245	5.01	60	5	ND	1	7	1	8	2	100	.18	.045	3	40	.39	46	.08	5	3.70	.01	.04	4	22
L11+00N 3+50E	1	86	5	59	.1	19	8	230	5.32	46	5	ND	2	5	1	2	2	103	.16	.035	3	37	.30	29	.08	4	3.36	.01	.04	1	8
L11+00N 3+75E	2	108	10	85	.2	32	15	437	4.90	52	5	ND	1	11	1	3	3	92	.21	.035	4	35	.43	51	.07	2	3.12	.01	.07	1	6
L11+00N 4+00E	1	163	8	69	.1	37	19	482	4.42	75	5	ND	1	13	1	2	2	93	.37	.032	4	45	.68	62	.13	2	3.45	.01	.07	1	24
L11+00N 4+25E	3	64	6	54	.1	17	16	291	4.27	41	5	ND	1	10	1	8	3	101	.24	.015	5	31	.30	29	.08	5	2.40	.01	.03	2	17
L11+00N 4+50E	3	69	6	49	.1	17	5	225	4.48	36	5	ND	1	5	1	2	3	91	.17	.027	4	33	.36	30	.08	2	2.46	.01	.05	2	19
L11+00N 4+75E	5	101	14	80	.3	31	17	257	6.02	51	5	ND	1	7	1	3	2	116	.15	.046	4	46	.40	43	.09	3	4.35	.01	.06	1	12
L11+00N 5+00E	2	74	5	56	.1	20	8	161	6.35	60	5	ND	2	5	1	2	2	122	.13	.039	3	49	.30	33	.09	2	4.26	.01	.07	1	115
L11+00N 5+25E	1	61	7	51	.1	16	7	187	4.85	46	5	ND	1	6	1	2	2	106	.15	.037	4	34	.25	25	.07	2	2.77	.01	.04	1	121
L11+00N 5+50E	2	39	6	29	.1	13	6	131	3.22	31	5	ND	1	6	1	2	2	88	.16	.019	5	23	.15	24	.09	5	1.63	.01	.03	1	60
L11+00N 5+75E	2	48	9	42	.1	17	13	373	3.37	26	5	ND	1	8	1	2	4	80	.23	.021	4	28	.32	28	.08	2	1.57	.01	.04	1	14
L11+00N 6+00E	2	129	11	76	.1	35	14	298	5.31	76	5	ND	1	7	1	2	2	115	.25	.032	3	46	.55	41	.15	3	3.98	.01	.05	1	11
L11+00N 6+25E	1	120	12	71	.1	32	13	240	5.33	77	5	ND	1	7	1	3	2	126	.23	.036	4	53	.48	36	.16	3	5.30	.01	.08	1	17
L11+00N 6+50E	1	72	13	50	.1	22	9	211	4.23	59	5	ND	1	6	1	8	2	120	.20	.030	3	40	.30	30	.14	4	2.79	.01	.01	4	16
L11+00N 6+75E	1	50	12	51	.1	17	13	331	3.88	51	5	ND	1	8	1	7	2	98	.23	.020	4	34	.31	31	.11	2	2.18	.01	.03	1	14
L11+00N 7+00E	1	39	6	39	.1	16	7	129	3.11	40	5	ND	1	6	1	2	2	92	.19	.015	4	26	.18	17	.11	2	1.66	.01	.02	1	25
L11+00N 7+25E	2	87	7	66	.1	28	12	301	4.32	64	5	ND	1	11	1	3	2	106	.28	.019	4	43	.56	38	.12	4	2.76	.01	.04	1	40
L11+00N 7+50E	1	69	15	46	.1	21	10	454	3.60	56	5	ND	1	6	1	2	2	56	.23	.024	6	22	.35	42	.11	2	2.35	.01	.04	1	8
L11+00N 7+75E	2	155	16	75	.1	34	14	296	4.21	74	5	ND	1	9	1	2	2	99	.26	.024	3	47	.63	44	.13	4	4.16	.01	.05	1	27
L11+00N 8+00E	1	65	11	63	.1	23	12	527	4.96	62	5	ND	1	11	1	2	3	131	.30	.026	3	43	.36	39	.14	2	2.64	.01	.05	1	11
L11+00N 8+25E	1	75	8	75	.1	24	14	383	4.85	63	5	ND	1	7	1	2	3	124	.23	.031	3	44	.34	29	.12	2	3.48	.01	.04	1	6
L11+00N 8+50E	2	75	11	82	.1	22	18	303	4.76	63	5	ND	1	7	1	10	4	144	.27	.026	5	49	.38	37	.12	3	3.24	.01	.08	2	5
STD C/AU-S	18	60	41	133	7.1	71	31	1047	3.94	41	18	7	38	50	18	17	24	61	.50	.084	40	56	.96	183	.07	32	1.94	.06	.14	12	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L9+00N 0+25W	2	55	15	46	.2	14	4	239	5.35	56	5	ND	2	5	1	3	2	115	.26	.036	3	34	.22	24	.10	2	2.34	.01	.06	2	7
L9+00N 0+00E	1	122	20	56	.4	26	9	173	6.61	67	5	ND	2	5	1	3	12	109	.17	.048	1	60	.41	21	.06	2	4.72	.01	.05	1	3
L9+00N 0+25E	1	105	18	64	.2	27	5	201	7.12	72	5	ND	2	6	1	3	2	122	.16	.043	5	56	.44	32	.05	2	4.64	.02	.05	1	1
L9+00N 0+50E	2	162	15	62	.4	24	6	246	5.52	76	5	ND	2	4	1	2	3	97	.22	.062	3	52	.43	30	.07	2	5.61	.01	.05	1	5
L9+00N 0+75E	1	73	12	58	.2	17	7	222	4.82	40	5	ND	2	4	1	11	2	117	.16	.043	4	38	.15	23	.06	7	3.66	.01	.14	2	3
L9+00N 1+00E	2	143	14	70	.1	32	14	347	5.54	51	5	ND	2	5	1	4	2	97	.22	.042	4	48	.52	52	.06	2	4.57	.02	.06	2	6
L9+00N 1+25E	2	165	12	66	.3	25	10	194	4.55	46	5	ND	2	4	1	5	2	62	.10	.024	4	36	.54	45	.06	3	3.67	.01	.07	1	6
L9+00N 1+50E	1	121	15	47	.3	16	7	130	4.91	64	5	ND	2	4	1	4	4	97	.14	.042	3	38	.30	27	.08	3	3.61	.01	.04	2	14
L9+00N 1+75E	1	83	16	65	.3	23	7	256	5.17	45	5	ND	2	6	1	3	12	117	.22	.046	3	41	.34	31	.15	2	3.25	.01	.05	1	3
L9+00N 2+25E	1	45	12	42	.3	14	6	135	4.08	36	5	ND	2	6	1	3	3	117	.23	.016	4	31	.29	25	.16	3	2.36	.01	.03	1	4
L9+00N 2+50E	1	154	14	70	.3	41	15	225	6.48	114	6	ND	3	6	1	2	15	125	.20	.046	4	56	.58	57	.13	7	6.37	.01	.07	1	16
L9+00N 2+75E	1	66	11	50	.4	13	5	122	4.33	71	5	ND	2	6	1	3	2	100	.16	.032	3	34	.16	33	.06	4	2.63	.01	.04	1	11
L9+00N 3+00E	2	63	9	47	.2	15	7	167	5.02	62	5	ND	2	6	1	2	2	123	.20	.045	3	36	.30	25	.13	3	2.84	.01	.05	1	16
L9+00N 3+25E	1	88	13	54	.1	15	8	207	4.15	74	5	ND	2	6	1	2	3	133	.17	.041	3	44	.26	31	.12	6	3.69	.01	.04	1	2
L9+00N 3+50E	1	67	8	58	.6	18	8	164	4.33	50	5	ND	1	7	1	3	12	99	.24	.034	3	36	.39	23	.14	7	2.99	.01	.03	1	20
L9+00N 3+75E	1	59	9	64	.2	16	9	213	3.34	40	5	ND	1	10	1	2	4	72	.24	.035	4	27	.37	27	.08	4	2.12	.01	.03	1	2
L9+00N 4+00E	2	54	11	42	.1	12	6	366	4.17	66	5	ND	1	5	1	2	4	108	.21	.043	3	32	.25	19	.14	5	1.94	.01	.02	2	18
L9+00N 4+25E	1	91	9	62	.2	23	9	253	4.16	57	5	ND	1	6	1	2	2	90	.25	.056	3	39	.37	22	.13	2	3.86	.01	.02	1	18
L9+00N 4+50E	1	56	12	44	.2	15	8	163	4.56	47	5	ND	1	6	1	2	2	134	.23	.030	4	38	.27	19	.17	3	2.53	.01	.03	2	10
L9+00N 4+75E	1	66	9	49	.3	15	7	147	4.46	59	5	ND	1	5	1	2	2	116	.21	.035	4	38	.33	19	.16	5	2.76	.01	.03	1	13
L9+00N 5+00E	1	135	14	61	.1	32	10	195	6.21	85	5	ND	1	6	1	2	3	131	.13	.031	3	49	.43	54	.10	3	4.68	.01	.04	1	9
L9+00N 5+25E	1	80	8	45	.3	16	6	197	3.71	58	5	ND	1	6	1	2	2	85	.15	.024	4	30	.21	23	.07	6	2.40	.01	.04	2	13
L9+00N 5+50E	2	134	10	56	.3	25	13	360	4.49	69	5	ND	1	9	1	2	2	94	.20	.035	5	38	.42	30	.09	2	3.73	.01	.04	1	21
L9+00N 5+75E	1	73	9	46	.2	22	8	245	4.57	62	5	ND	1	10	1	3	2	109	.28	.023	4	35	.39	35	.12	3	2.60	.01	.05	1	11
L9+00N 6+00E	1	43	9	44	.1	13	6	163	3.60	55	5	ND	1	9	1	2	2	108	.23	.026	4	29	.24	16	.15	2	1.68	.01	.03	1	9
L9+00N 6+25E	1	69	11	43	.1	16	6	145	4.59	71	5	ND	1	5	1	3	3	105	.13	.038	3	33	.23	22	.09	3	2.46	.01	.02	1	6
L9+00N 6+50E	1	47	9	43	.1	12	6	173	4.04	45	5	ND	1	5	1	2	2	101	.11	.034	3	31	.15	20	.09	4	2.33	.01	.02	3	160
L9+00N 6+75E	1	131	12	74	.1	32	11	227	4.55	88	5	ND	1	7	1	2	3	102	.22	.029	3	44	.49	41	.14	2	3.91	.01	.03	1	11
L9+00N 7+00E	2	112	9	76	.1	32	13	372	4.97	126	5	ND	1	10	1	2	2	100	.29	.015	4	46	.56	45	.13	2	3.66	.01	.03	1	26
L9+00N 7+25E	1	71	6	53	.1	17	5	176	4.12	80	5	ND	1	7	1	2	3	94	.23	.016	4	34	.33	27	.11	2	2.94	.01	.01	1	14
L9+00N 7+50E	2	82	14	51	.1	19	7	158	5.03	128	5	ND	1	6	1	3	2	106	.16	.024	2	40	.29	26	.12	2	4.24	.01	.02	1	13
L9+00N 7+75E	2	50	13	55	.1	27	10	167	5.33	147	5	ND	1	6	1	2	2	106	.18	.019	3	41	.41	50	.12	3	4.84	.01	.04	1	11
L3+75E 5+25N	1	43	10	54	.1	13	13	372	7.03	36	5	ND	1	10	1	2	2	250	.70	.022	2	82	.36	17	.68	2	2.42	.01	.01	1	6
L3+75E 5+00N	1	44	13	58	.1	15	11	301	6.54	33	5	ND	1	6	1	2	2	237	.55	.038	2	53	.25	16	.55	3	2.70	.01	.02	2	2
L3+75E 4+75N	1	67	14	75	.1	28	16	302	8.02	28	5	ND	1	3	1	2	2	217	.75	.042	2	74	.63	17	.64	3	3.93	.01	.01	1	11
L3+75E 4+50N	1	70	10	68	.1	22	12	211	7.65	63	5	ND	1	10	1	2	2	230	.63	.030	3	52	.41	23	.53	2	3.06	.01	.02	1	3
STD C/AU-S	18	61	42	132	6.8	69	31	1024	4.11	41	18	8	39	51	18	21	19	61	.49	.090	41	59	.96	179	.07	32	1.97	.06	.13	12	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L3+75E 4+25N	1	37	5	55	.1	21	13	225	6.25	12	5	ND	1	6	1	4	2	216	.64	.032	3	71	.66	15	.42	2	3.32	.01	.01	1	3
L3+75E 3+75N	2	61	8	94	.1	33	17	226	6.96	21	5	ND	1	7	1	3	2	246	.49	.034	3	57	.37	26	.48	4	4.66	.01	.02	1	1
L3+75E 3+50N	1	65	11	81	.1	35	24	552	6.00	27	5	ND	1	5	1	2	2	222	.57	.045	3	72	.54	34	.50	2	4.48	.01	.02	1	1
L3+75E 3+25N	1	226	13	93	.1	39	20	297	8.65	26	5	ND	1	1	1	4	2	247	.63	.045	1	95	.53	26	.56	4	6.37	.01	.02	1	1
L3+75E 3+00N	1	80	12	82	.1	26	15	383	8.04	25	5	ND	1	6	1	4	2	202	.32	.048	3	85	.43	27	.34	4	5.18	.01	.02	2	2
L3+75E 2+75N	1	75	11	83	.1	25	17	239	10.70	26	5	ND	1	6	1	2	2	316	.48	.046	3	53	.32	23	.67	6	4.02	.01	.01	1	1
L3+75E 2+50N	1	51	15	70	.2	22	13	445	5.69	24	5	ND	1	7	1	2	2	291	.65	.052	2	55	.22	17	.61	2	3.77	.01	.02	1	2
L3+75E 2+25N	1	36	13	50	.2	14	9	163	8.45	17	5	ND	1	5	1	2	2	324	.43	.033	2	67	.14	14	.60	2	2.06	.01	.01	1	1
L3+75E 2+00N	1	33	15	62	.1	16	19	594	5.94	16	5	ND	1	11	1	4	2	212	.74	.041	3	51	.31	20	.36	3	2.03	.01	.02	2	3
L3+75E 1+75N	1	53	5	77	.1	26	24	450	5.15	11	5	ND	1	5	1	3	3	156	.62	.025	4	76	.45	20	.52	3	3.41	.01	.01	2	2
L3+75E 1+50N	1	42	3	56	.2	18	10	180	7.03	14	5	ND	1	5	1	2	2	237	.50	.025	2	64	.23	23	.51	2	3.26	.01	.01	1	1
L3+75E 1+25N	1	41	9	59	.2	17	11	206	5.37	16	5	ND	1	7	1	2	2	286	.48	.042	2	74	.22	11	.61	2	2.56	.01	.01	1	1
L3+75E 1+00N	1	88	17	74	.1	27	17	337	8.92	16	5	ND	1	7	1	2	2	287	.53	.040	3	56	.44	18	.64	2	4.52	.01	.01	1	3
L3+75E 0+75N	1	73	9	76	.2	24	14	232	11.22	24	5	ND	1	7	1	3	2	311	.39	.049	2	103	.33	19	.73	2	4.93	.01	.02	1	2
L3+75E 0+50N	1	67	11	76	.2	23	14	205	6.62	12	5	ND	1	7	1	2	2	276	.45	.027	3	74	.27	18	.65	3	3.25	.01	.01	1	4
L3+75E 0+25N	1	67	13	77	.2	25	14	218	8.60	18	5	ND	1	6	1	2	2	275	.32	.033	3	76	.29	20	.60	3	4.31	.01	.01	2	2
L3+75E 0+00N	1	93	13	69	.2	32	19	241	9.48	27	5	ND	1	7	1	4	2	256	.38	.042	3	97	.40	24	.63	2	6.26	.01	.01	2	3
L3+75E 0+50S	1	50	14	64	.2	14	11	128	10.94	21	5	ND	1	6	1	2	2	329	.35	.036	2	85	.19	14	.82	2	3.20	.01	.01	1	6
L3+75E 0+75S	1	75	16	77	.2	20	13	202	9.73	26	5	ND	1	7	1	3	2	265	.41	.055	3	94	.29	19	.53	2	4.99	.01	.01	2	1
L3+75E 1+00S	1	66	11	63	.2	20	12	157	8.76	21	5	ND	1	7	1	3	2	273	.44	.022	3	77	.28	15	.64	3	3.41	.01	.01	1	2
L3+75E 1+75S	1	111	10	67	.1	31	15	247	6.65	506	5	ND	1	6	1	2	2	176	.55	.024	4	62	.57	28	.34	2	3.63	.01	.01	1	3
L3+75E 2+00S	1	36	10	53	.1	14	9	167	8.56	16	5	ND	1	7	1	2	2	265	.40	.031	2	60	.16	14	.60	2	2.05	.01	.01	1	6
L3+75E 2+25S	1	44	6	63	.2	14	10	176	6.71	16	5	ND	1	7	1	3	3	260	.41	.030	2	64	.20	14	.60	2	2.55	.01	.01	1	3
L3+75E 2+50S	1	60	11	74	.2	22	19	529	8.50	17	5	ND	1	13	1	2	2	245	.61	.022	5	64	.35	24	.57	2	2.67	.01	.02	1	5
L3+75E 2+75S	1	125	15	52	.1	46	25	493	6.36	36	5	ND	1	10	1	2	2	259	.65	.046	5	65	.76	26	.64	7	4.06	.01	.02	2	4
L3+75E 3+00S	1	58	12	78	.2	22	14	273	8.83	41	5	ND	1	6	1	2	2	270	.51	.041	2	65	.41	24	.64	4	2.99	.01	.01	1	1
L3+75E 3+50S	1	59	10	88	.1	25	20	314	5.12	15	5	ND	1	7	1	2	2	284	.46	.038	5	62	.30	24	.56	2	3.41	.01	.02	1	6
L3+75E 3+75S	1	70	5	85	.1	31	23	327	9.61	20	5	ND	1	7	1	2	2	253	.39	.041	5	69	.35	26	.63	3	3.92	.01	.01	1	10
L3+75E 4+00S	1	32	7	57	.1	11	10	177	7.50	13	5	ND	1	8	1	2	2	255	.30	.032	5	46	.13	29	.51	2	2.13	.01	.01	1	5
L3+75E 4+25S	1	39	13	67	.1	17	13	205	7.63	12	5	ND	1	8	1	2	2	254	.33	.036	4	49	.16	28	.52	2	1.66	.01	.01	1	2
L3+75E 4+50S	1	55	6	72	.1	31	20	435	8.10	26	5	ND	1	7	1	2	2	215	.44	.054	4	76	.60	25	.44	4	4.76	.01	.02	1	3
L3+75E 4+75S	1	72	12	84	.1	23	15	335	6.40	17	5	ND	1	7	1	3	2	245	.32	.034	4	67	.28	26	.37	2	3.87	.01	.02	1	4
L3+75E 5+00S	1	64	10	71	.1	25	15	342	6.38	25	5	ND	1	6	1	2	2	230	.41	.066	3	78	.40	23	.43	2	4.69	.01	.01	1	8
L3+75E 5+25S	1	47	9	59	.1	16	10	243	8.85	17	5	ND	1	5	1	2	2	286	.28	.043	2	68	.23	17	.57	4	3.22	.01	.01	1	5
L3+75E 5+50S	1	27	15	44	.1	12	8	243	7.84	23	5	ND	1	6	1	2	2	301	.22	.070	2	47	.10	19	.54	2	1.37	.01	.02	1	5
L3+75E 5+75S	1	126	14	62	.1	37	18	359	8.15	25	5	ND	1	6	1	2	2	222	.44	.048	3	83	.61	27	.44	4	5.51	.01	.02	1	2
STD C/AU-S	18	59	36	133	6.7	66	30	1021	4.22	40	17	7	38	46	18	17	22	59	.48	.052	40	57	.92	177	.07	33	2.04	.06	.13	11	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L3+75E 6+00S	1	87	21	76	.2	28	18	750	6.45	15	5	ND	1	14	1	2	2	195	.62	.044	3	55	.53	32	.36	6	3.43	.01	.02	1	11
L2+25E 6+50N	1	28	14	36	.1	10	6	244	4.56	32	5	ND	1	9	1	2	2	165	.41	.025	2	31	.22	18	.33	2	1.07	.01	.02	1	29
L2+25E 6+25N	1	38	10	48	.1	10	5	160	6.34	17	5	ND	2	6	1	2	2	279	.35	.045	2	54	.15	12	.47	4	2.17	.01	.02	1	2
L2+25E 6+00N	1	66	15	67	.1	20	14	366	6.01	25	5	ND	1	8	1	2	2	244	.47	.041	2	60	.35	20	.44	5	3.16	.01	.01	1	1
L2+25E 5+75N	1	34	11	55	.2	19	13	223	6.22	17	5	ND	1	11	1	2	2	214	.56	.026	2	45	.25	16	.44	3	2.07	.01	.02	1	1
L2+25E 5+50N	1	36	20	80	.1	14	162	3172	6.55	15	5	ND	1	8	1	3	2	170	.43	.047	3	35	.24	26	.25	5	3.11	.01	.02	1	1
L2+25E 5+25N	1	25	7	40	.1	9	9	172	6.13	8	5	ND	1	8	1	2	2	228	.35	.033	2	37	.15	13	.42	2	1.54	.01	.01	2	1
L2+25E 5+00N	1	29	16	46	.1	9	7	241	6.45	8	5	ND	2	11	1	2	2	245	.37	.038	2	40	.14	42	.33	2	1.51	.01	.02	1	1
L2+25E 4+75N	1	79	11	52	.1	21	12	272	7.05	14	5	ND	1	6	1	3	2	209	.40	.035	2	60	.32	18	.40	2	4.54	.01	.01	1	2
L2+25E 4+50N	1	55	17	49	.1	18	11	210	10.42	15	5	ND	1	6	1	3	4	357	.36	.030	2	66	.15	16	.62	4	2.85	.01	.01	2	1
L2+25E 4+25N	1	174	14	88	.1	58	25	323	7.30	62	5	ND	1	7	1	2	2	184	.69	.029	3	85	.84	27	.34	11	6.24	.01	.02	1	7
L2+25E 4+00N	1	108	22	65	.2	31	15	264	7.22	30	5	ND	2	7	1	3	2	197	.47	.034	2	84	.43	20	.40	4	6.63	.01	.02	1	5
L2+25E 3+75N	1	82	15	106	.1	22	15	395	9.16	17	5	ND	2	12	1	2	2	280	.59	.051	2	79	.41	34	.51	5	4.16	.01	.03	1	1
L2+25E 3+50N	1	140	19	79	.1	43	24	375	7.35	32	5	ND	1	8	1	2	2	230	.66	.048	4	75	.70	25	.54	5	5.72	.01	.02	1	9
L2+25E 3+25N	1	40	9	43	.1	11	8	236	6.65	6	5	ND	1	7	1	2	2	235	.41	.022	3	46	.18	17	.44	4	2.14	.01	.01	1	8
L2+25E 3+00N	1	103	14	68	.1	25	15	242	7.45	29	5	ND	1	7	1	3	6	224	.46	.032	2	78	.45	16	.37	5	5.50	.01	.01	1	9
L2+25E 2+75N	1	83	18	76	.1	23	20	338	7.74	28	5	ND	1	6	1	3	2	206	.33	.043	2	72	.46	25	.24	3	3.93	.01	.04	1	3
L2+25E 2+50N	1	75	15	78	.1	18	12	210	8.79	22	5	ND	1	6	1	2	2	261	.42	.040	2	75	.25	20	.35	2	3.84	.01	.02	1	2
L2+25E 2+25N	1	65	15	57	.1	20	13	196	7.76	19	5	ND	1	6	1	3	2	259	.38	.029	2	66	.28	14	.54	4	3.46	.01	.02	2	1
L2+25E 2+00N	1	70	15	61	.1	22	15	296	8.26	17	5	ND	1	8	1	3	4	282	.43	.035	2	61	.30	21	.51	7	3.07	.01	.01	1	7
L2+25E 1+75N	1	62	9	77	.1	26	16	283	8.90	16	5	ND	1	7	1	2	2	282	.44	.037	2	71	.30	21	.55	2	3.84	.01	.02	1	3
L2+25E 1+50N	1	108	17	85	.1	33	18	317	9.16	22	5	ND	1	8	1	3	5	261	.56	.053	2	66	.56	23	.54	4	5.55	.01	.03	1	4
L2+25E 1+25N	1	121	19	94	.1	41	21	388	9.01	34	5	ND	1	6	1	6	2	245	.39	.045	2	82	.48	32	.26	3	5.58	.01	.02	3	6
L2+25E 1+00N	1	92	12	61	.1	23	15	299	11.17	18	5	ND	2	6	1	2	4	296	.46	.063	2	100	.45	16	.47	6	6.08	.01	.03	1	1
L2+25E 0+75N	1	88	13	63	.1	24	14	214	9.17	21	5	ND	1	6	1	2	2	291	.46	.046	2	80	.34	15	.60	4	4.25	.01	.03	1	1
L2+25E 0+25N	1	20	11	36	.1	10	7	167	6.36	4	5	ND	1	4	1	3	4	255	.48	.032	2	40	.16	6	.49	4	1.43	.01	.01	2	1
L2+25E 0+00N	1	154	13	84	.2	42	18	224	6.24	53	5	ND	1	6	1	2	2	159	.57	.024	2	56	.56	18	.35	4	5.97	.01	.01	1	9
L2+25E 0+25S	1	207	9	87	.1	37	17	250	7.12	68	5	ND	1	8	1	3	2	186	.54	.038	2	63	.56	21	.36	13	3.70	.01	.01	1	1
L2+25E 0+50S	1	72	19	125	.2	24	33	761	7.40	22	5	ND	1	8	1	2	2	199	.58	.041	4	57	.34	30	.56	8	3.20	.01	.03	1	1
L2+25E 0+75S	1	81	12	96	.1	35	22	265	7.53	23	5	ND	1	7	1	4	2	217	.58	.045	2	72	.54	25	.43	6	4.21	.01	.02	1	4
L2+25E 1+00S	1	37	13	62	.1	14	11	238	5.76	14	5	ND	2	7	1	2	2	348	.45	.036	2	66	.17	15	.76	4	2.54	.01	.02	1	4
L2+25E 1+25S	1	51	11	69	.1	19	18	812	8.52	13	5	ND	1	11	1	2	2	300	.59	.047	3	59	.29	22	.66	6	2.38	.01	.02	1	1
L2+25E 1+50S	1	104	15	132	.1	54	26	556	7.87	24	5	ND	1	11	1	2	2	234	.80	.040	3	76	.75	35	.63	6	5.00	.01	.03	1	1
L2+25E 1+75S	1	78	8	65	.1	29	16	303	7.72	15	5	ND	1	6	1	2	2	262	.59	.036	2	66	.39	21	.66	5	4.02	.01	.02	1	2
L2+25E 2+00S	1	54	12	66	.1	20	13	358	6.64	12	5	ND	1	7	1	2	4	223	.44	.057	2	56	.23	17	.48	3	2.66	.01	.02	1	2
L2+25E 2+25S	1	31	16	46	.1	10	10	242	9.50	15	5	ND	1	7	1	2	4	379	.32	.047	2	60	.11	14	.78	7	1.56	.01	.02	1	1
STD C/AU-S	18	60	40	133	6.8	70	31	1025	4.14	43	15	7	38	50	16	17	15	61	.47	.056	40	55	.52	160	.07	34	1.95	.06	.14	12	48

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-4521

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L2+25E 2+50S	1	86	18	66	.1	37	22	587	6.73	16	5	ND	1	10	1	2	2	237	.71	.034	5	60	.55	26	.63	5	3.56	.01	.05	1	2
L2+25E 2+75S	1	45	10	39	.1	16	11	249	7.16	13	5	ND	1	8	1	2	3	262	.32	.041	2	55	.21	16	.59	2	2.16	.01	.04	2	10
L2+25E 3+00S	1	79	8	58	.1	33	17	351	6.41	14	5	ND	1	8	1	2	3	204	.49	.046	2	58	.46	26	.42	4	3.40	.01	.02	1	15
L2+25E 3+25S	1	34	11	41	.1	7	7	182	7.07	6	5	ND	1	5	1	2	2	334	.30	.052	2	44	.12	10	.71	2	1.45	.01	.03	1	4
L2+25E 3+50S	1	62	5	91	.1	35	34	866	6.66	14	5	ND	1	10	1	2	2	215	.57	.045	4	60	.58	30	.51	2	3.59	.01	.03	1	3
L2+25E 3+75S	1	136	15	81	.1	47	22	412	6.97	14	5	ND	1	8	1	2	2	228	.54	.014	2	76	.68	35	.54	4	5.32	.01	.03	1	8
L2+25E 4+00S	1	71	6	72	.1	32	17	532	6.53	8	5	ND	1	10	1	2	2	227	.73	.019	3	61	.45	32	.67	2	3.15	.01	.02	1	4
L2+25E 4+25S	1	57	12	55	.1	16	11	456	10.09	18	5	ND	1	5	1	2	2	351	.63	.066	2	82	.33	16	.76	2	2.93	.01	.04	1	2
L2+25E 4+50S	1	61	14	49	.1	16	13	591	6.56	21	5	ND	1	6	1	2	3	246	.41	.026	2	64	.33	17	.39	4	2.84	.01	.02	1	4
L2+25E 4+75S	1	65	9	70	.1	27	18	272	5.76	20	5	ND	1	6	1	2	2	161	.37	.028	4	54	.52	18	.28	2	3.39	.01	.02	1	1
L2+25E 5+00S	1	40	11	42	.1	13	10	167	7.52	9	5	ND	1	7	1	2	2	266	.67	.031	2	57	.23	13	.50	4	2.35	.01	.03	1	2
L2+25E 5+25S	1	73	6	60	.1	21	14	260	8.22	49	5	ND	1	5	1	2	2	269	.54	.023	2	70	.44	17	.61	2	3.59	.01	.03	1	6
L2+25E 5+50S	1	37	10	59	.1	17	11	315	7.26	46	5	ND	2	10	1	2	2	257	.53	.027	2	55	.29	19	.67	2	1.96	.01	.04	1	1
L2+25E 5+75S	1	74	16	65	.1	21	13	507	7.12	18	5	ND	1	10	1	3	2	269	.56	.031	2	56	.34	21	.69	4	2.59	.01	.03	1	3
L0+75E 7+25N	1	120	9	79	.1	40	19	522	6.74	26	5	ND	1	12	1	2	2	210	.81	.042	3	70	.75	34	.45	3	3.78	.01	.05	1	5
L0+75E 7+00N	1	76	7	68	.1	34	19	452	5.44	13	5	ND	1	11	1	2	2	181	.60	.030	3	55	.52	43	.39	2	3.06	.01	.03	1	1
L0+75E 6+75N	1	148	8	75	.1	51	24	379	7.23	21	5	ND	1	10	1	2	2	228	.69	.018	3	74	.73	43	.54	5	4.59	.01	.01	1	1
L0+75E 6+50N	1	34	10	64	.1	17	7	154	5.23	18	5	ND	1	7	1	2	4	133	.22	.034	2	44	.24	27	.18	4	3.03	.01	.02	2	1
L0+75E 6+25N	1	44	15	51	.1	13	10	165	7.72	15	5	ND	1	7	1	2	2	261	.27	.031	2	51	.19	18	.53	5	2.25	.01	.03	1	1
L0+75E 6+00N	1	40	9	43	.1	18	12	202	5.89	83	5	ND	1	12	1	2	4	216	.55	.019	4	44	.30	26	.42	5	1.95	.01	.02	2	1
L0+75E 5+75N	1	36	10	59	.1	14	12	254	7.05	13	5	ND	1	9	1	2	2	225	.56	.025	2	54	.26	17	.47	4	2.30	.01	.02	1	2
L0+75E 5+50N	1	23	8	32	.1	5	8	203	5.75	7	5	ND	1	5	1	2	2	222	1.14	.033	2	42	.21	8	.74	2	1.74	.01	.01	1	1
L0+75E 5+25N	1	40	9	61	.1	15	11	222	6.59	13	5	ND	1	6	1	2	2	185	.32	.040	2	44	.33	15	.36	4	2.37	.01	.01	1	1
L0+75E 5+00N	1	17	10	53	.1	17	14	569	5.85	3	5	ND	1	11	1	2	2	225	2.98	.042	2	53	.46	16	.65	3	3.03	.01	.02	1	1
L0+75E 4+75N	1	106	17	103	.1	40	21	312	8.05	17	5	ND	1	8	1	2	2	259	.57	.037	2	70	.55	35	.59	4	4.46	.01	.01	1	1
L0+75E 4+50N	1	67	8	64	.1	24	14	310	7.80	20	5	ND	1	7	1	2	2	241	.62	.055	2	62	.46	20	.40	5	3.17	.01	.03	1	1
L0+75E 4+25N	1	85	14	85	.1	30	17	452	6.78	22	5	ND	1	8	1	2	2	271	.48	.078	2	65	.50	25	.53	2	4.60	.01	.04	1	2
L0+75E 4+00N	1	23	11	45	.1	10	8	223	8.42	42	5	ND	1	6	1	2	2	314	.59	.046	2	64	.21	11	.45	5	1.66	.01	.03	1	1
L0+75E 3+75N	2	62	7	63	.1	16	13	181	7.49	25	5	ND	1	7	1	2	4	205	.39	.044	2	63	.30	17	.42	2	3.43	.01	.01	1	4
L0+75E 3+50N	1	135	7	65	.1	42	21	348	5.81	20	5	ND	1	8	1	2	2	178	.69	.020	3	55	.70	24	.37	5	3.36	.01	.02	1	1
L0+75E 3+25N	1	90	3	56	.2	24	11	228	5.99	17	5	ND	1	7	1	2	2	200	.52	.027	2	44	.37	16	.41	7	2.30	.01	.02	1	4
L0+75E 3+00N	1	27	4	76	.1	46	20	299	7.50	18	5	ND	1	4	1	3	2	174	.27	.021	2	161	.86	17	.02	5	2.89	.01	.02	1	8
L0+75E 2+75N	1	211	16	84	.1	50	29	504	6.88	28	5	ND	1	9	1	2	2	206	.66	.022	3	64	.71	56	.41	4	3.97	.01	.03	1	6
L0+75E 2+50N	1	178	11	75	.1	45	24	314	5.62	27	5	ND	1	8	1	3	2	171	.62	.017	3	56	.68	23	.34	6	3.29	.01	.02	2	45
L0+75E 2+25N	1	34	10	46	.1	11	9	166	8.81	5	5	ND	1	5	1	2	4	351	.26	.025	2	55	.11	13	.79	3	1.44	.01	.02	1	4
L0+75E 2+00N	1	142	7	86	.1	38	20	366	7.61	18	5	ND	1	9	1	2	2	239	.66	.036	3	68	.57	26	.56	3	3.97	.01	.03	1	12
STD C/AU-S	20	59	37	132	6.8	68	31	1035	4.08	43	18	8	39	50	19	15	16	61	.48	.097	40	55	.89	179	.07	33	1.97	.06	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L0+75E 1+75N	1	745	12	98	.2	32	25	1010	6.84	28	5	ND	1	15	1	2	4	216	.73	.047	4	60	.63	29	.46	7	3.00	.01	.02	1	5
L0+75E 1+50N	1	34	13	45	.1	8	6	136	7.58	5	5	ND	1	7	1	2	2	303	.37	.022	2	51	.14	11	.71	5	1.40	.01	.02	1	5
L0+75E 1+25N	1	41	10	61	.2	16	11	181	7.45	14	5	ND	1	7	1	2	2	244	.47	.051	2	54	.22	12	.56	2	2.76	.01	.02	1	4
L0+75E 1+00N	1	306	13	86	.1	29	21	316	7.20	45	5	ND	1	5	1	2	2	198	.61	.025	7	72	.53	25	.32	2	4.20	.01	.05	1	2
L0+75E 0+75N	1	84	9	75	.1	25	17	226	7.71	12	5	ND	1	6	1	2	4	246	.16	.027	2	115	1.13	31	.02	2	4.18	.01	.05	1	1
L0+75E 0+50N	1	66	12	85	.1	29	20	1134	5.63	16	5	ND	1	14	1	2	3	184	.75	.025	4	51	.52	25	.34	6	2.68	.01	.02	1	1
L0+75E 0+25N	1	126	12	80	.1	24	15	236	7.37	19	5	ND	1	7	1	2	2	213	.52	.042	2	74	.42	18	.51	7	3.58	.01	.02	1	1
L0+75E 0+00N	1	47	9	71	.2	22	14	249	6.61	13	5	ND	1	8	1	2	2	214	.69	.042	2	61	.38	18	.54	4	2.57	.01	.03	1	1
L0+75E 0+25S	1	47	15	68	.1	19	16	1057	6.01	11	5	ND	1	16	1	3	5	206	.81	.030	5	49	.36	29	.38	8	2.39	.01	.02	1	2
L0+75E 0+50S	1	65	15	63	.1	14	13	259	9.18	18	5	ND	1	8	1	2	2	246	.39	.056	2	63	.38	21	.54	10	3.74	.01	.03	1	3
L0+75E 0+75S	1	38	17	49	.1	9	10	199	9.76	16	5	ND	1	8	1	2	2	309	.31	.050	2	74	.16	18	.61	3	2.04	.01	.04	1	2
L0+75E 1+00S	1	65	6	64	.1	25	15	227	6.84	14	5	ND	1	7	1	3	2	217	.47	.022	3	76	.47	30	.41	3	4.06	.01	.02	1	45
L0+75E 1+25S	1	44	11	50	.1	12	9	167	6.36	11	5	ND	1	6	1	2	2	209	.32	.032	2	51	.28	21	.43	6	2.46	.01	.02	3	6
L0+75E 1+75S	1	22	10	51	.1	8	10	164	6.46	9	5	ND	1	6	1	2	2	295	.58	.058	2	64	.18	11	.60	3	2.07	.01	.03	1	1
L0+75E 2+00S	1	30	7	71	.1	15	30	610	7.31	9	5	ND	1	10	1	2	2	244	.65	.053	4	61	.43	29	.47	4	2.39	.01	.03	1	1
L0+75E 2+25S	1	49	13	57	.1	19	13	272	6.64	15	5	ND	1	7	1	2	2	234	.52	.042	2	62	.37	16	.49	4	2.72	.01	.02	1	2
L0+75E 2+50S	1	87	13	65	.1	32	20	333	7.16	15	5	ND	1	8	1	2	2	225	.55	.033	3	70	.45	26	.47	7	4.15	.01	.01	1	2
L0+75E 2+75S	1	19	14	35	.1	5	3	151	5.44	2	5	ND	1	4	1	2	2	303	.09	.013	2	31	.05	9	.61	8	.67	.01	.01	1	2
L0+75E 3+00S	1	82	12	88	.2	30	22	566	6.07	14	5	ND	1	8	1	2	2	179	.42	.062	6	60	.46	27	.34	7	4.75	.01	.02	1	3
L0+75E 3+25S	1	37	12	52	.1	11	9	253	7.68	6	5	ND	1	7	1	2	2	297	.37	.031	2	62	.16	21	.60	9	2.13	.01	.01	1	1
L0+75E 3+50S	1	46	16	56	.1	15	12	212	9.18	14	5	ND	1	6	1	2	3	281	.39	.055	2	85	.26	13	.54	9	3.46	.01	.01	1	4
L0+75E 3+75S	1	126	7	89	.1	42	21	573	7.03	16	5	ND	1	9	1	2	2	218	.62	.043	3	78	.74	32	.46	11	5.08	.01	.04	1	1
L0+75E 4+00S	1	30	8	32	.1	6	7	171	6.33	5	5	ND	1	5	1	2	2	265	.17	.015	2	46	.10	12	.53	3	1.48	.01	.02	1	9
L0+75E 4+25S	1	31	12	36	.1	9	8	134	8.04	7	5	ND	1	5	1	2	2	295	.25	.021	2	65	.15	8	.55	6	1.63	.01	.01	1	5
STD C/AU-S	18	58	39	131	7.1	67	29	1004	3.74	42	20	7	35	46	16	17	19	56	.44	.082	35	55	.83	174	.06	33	1.84	.06	.13	12	48

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: SEP 23 1988 DATE REPORT MAILED: Oct 3/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-4741 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L12+00N 2+25W	1	50	9	115	.4	21	12	327	9.15	21	5	ND	1	18	1	3	2	247	.65	.069	5	70	.37	45	.52	2	2.69	.01	.03	1	3
L12+00N 2+00W	1	106	18	114	.3	30	19	654	8.04	172	5	ND	1	18	1	21	2	166	1.04	.036	6	51	.51	43	.04	3	3.15	.01	.04	1	18
L12+00N 1+75W	1	46	11	99	.5	16	8	242	9.13	21	5	ND	1	19	1	2	2	253	.65	.066	5	65	.28	41	.53	2	2.41	.01	.02	1	15
L12+00N 1+50W	1	55	20	144	.4	28	45	3777	7.36	29	5	ND	1	21	1	2	3	168	.83	.052	4	57	.61	60	.32	2	2.79	.01	.04	1	10
L12+00N 1+25W	1	100	14	129	.5	38	15	364	11.12	22	5	ND	1	8	1	2	2	243	.43	.082	3	105	.67	40	.47	2	5.71	.01	.03	1	1
L12+00N 1+00W	1	82	7	107	.3	33	13	317	12.57	23	5	ND	2	8	1	8	2	280	.41	.078	3	102	.59	36	.51	2	4.69	.01	.03	1	4
L12+00N 0+75W	1	17	2	58	.1	7	5	165	3.77	9	5	ND	1	5	1	2	2	79	.12	.041	3	19	.27	41	.01	2	2.79	.01	.02	1	1
L12+00N 0+50W	1	78	13	78	.1	18	8	192	5.18	15	5	ND	1	7	1	2	2	129	.28	.047	3	42	.24	29	.17	2	4.29	.01	.03	1	3
L12+00N 0+25W	1	65	21	77	.1	18	8	222	7.06	27	5	ND	1	7	1	4	2	164	.21	.061	4	51	.24	32	.11	2	3.93	.01	.03	2	1
L12+00N 0+00W	1	19	3	38	.2	6	4	163	5.57	15	5	ND	1	6	1	3	2	179	.15	.023	3	31	.10	17	.24	2	2.00	.01	.02	1	16
L12+00N 0+25E	1	55	3	57	.1	16	8	176	5.83	14	5	ND	1	6	1	2	2	145	.22	.014	3	38	.26	33	.09	2	3.10	.01	.02	1	8
L12+00N 0+50E	1	53	11	57	.1	16	8	169	5.80	15	5	ND	1	6	1	2	2	142	.22	.017	3	37	.25	29	.09	2	2.98	.01	.02	1	5
L12+00N 0+75E	1	16	5	69	.1	8	10	155	4.02	14	5	ND	1	2	2	2	3	69	.05	.029	2	7	.04	14	.01	2	1.33	.01	.03	1	1
L12+00N 1+00E	1	44	26	80	.1	23	15	264	6.62	23	5	ND	1	5	1	4	2	136	.18	.079	2	33	.19	53	.01	2	3.82	.01	.03	1	3
L12+00N 1+25E	1	35	12	63	.1	13	10	353	4.98	11	5	ND	1	5	1	2	2	132	.20	.027	3	28	.17	57	.02	2	2.68	.01	.02	1	1
L12+00N 1+50E	3	26	24	70	.1	13	10	345	5.40	20	5	ND	1	4	1	2	2	81	.06	.034	2	15	.07	42	.01	2	1.70	.01	.04	1	2
L12+00N 1+75E	1	69	12	77	.2	26	11	390	7.57	16	5	ND	1	6	1	2	2	180	.34	.030	3	53	.38	41	.27	2	3.94	.01	.03	1	1
L12+00N 2+00E	1	60	16	77	.1	19	9	254	5.73	18	5	ND	1	10	1	3	2	155	.33	.039	3	43	.27	47	.12	2	2.53	.01	.03	2	1
L12+00N 2+25E	1	34	2	42	.1	8	6	182	5.22	19	5	ND	1	6	1	3	2	185	.18	.026	3	31	.13	20	.10	2	2.07	.01	.01	2	1
L12+00N 2+50E	1	56	2	70	.1	16	8	277	7.63	18	5	ND	2	6	1	2	2	207	.23	.030	3	46	.20	38	.19	2	3.51	.01	.03	1	2
L10+00N 5+50W	1	71	23	69	.4	23	10	829	10.02	26	5	ND	1	10	1	3	3	315	.69	.047	3	67	.33	19	.50	2	2.33	.01	.03	1	1
L10+00N 5+25W	1	187	7	101	.6	73	29	491	9.67	102	5	ND	1	11	1	4	2	246	1.34	.025	3	109	1.68	37	.75	2	6.11	.01	.02	1	1
L10+00N 5+00W	1	177	12	127	.8	61	24	415	11.01	226	5	ND	1	9	1	15	2	254	.97	.034	4	97	1.09	29	.55	2	5.70	.01	.02	1	8
L10+00N 4+75W	1	49	12	77	.5	17	8	248	12.09	23	5	ND	2	10	1	3	2	328	.73	.060	3	90	.34	18	.75	2	3.60	.01	.03	1	1
L10+00N 4+50W	1	181	12	97	.3	56	22	506	9.47	20	5	ND	1	9	1	4	2	250	1.09	.091	3	106	1.43	17	.67	2	7.11	.01	.02	1	1
L10+00N 4+25W	1	152	18	96	.4	45	19	472	10.35	15	5	ND	1	10	1	5	4	269	.98	.064	4	112	1.00	22	.73	2	6.05	.01	.02	1	28
L10+00N 4+00W	1	128	4	119	.5	71	26	548	9.57	75	5	ND	1	12	1	13	2	240	1.61	.044	3	95	1.73	19	.78	2	4.97	.01	.02	1	1
L10+00N 3+75W	1	157	24	137	.5	87	28	1424	9.73	216	5	ND	1	16	1	13	2	203	1.44	.069	5	102	1.39	35	.53	5	6.36	.01	.03	1	1
L10+00N 3+50W	1	130	13	109	.7	53	27	1397	9.19	205	5	ND	1	11	1	14	3	209	.97	.051	8	82	1.05	27	.65	3	5.87	.01	.03	1	5
L10+00N 3+25W	1	170	10	87	.5	53	23	446	8.95	64	5	ND	1	9	1	4	2	210	.87	.029	3	86	1.30	24	.53	2	4.98	.01	.02	1	7
L10+00N 3+00W	1	85	17	132	.5	43	39	8791	8.27	255	5	ND	1	20	1	8	2	207	1.50	.053	8	73	.98	75	.52	4	4.35	.01	.03	1	3
L10+00N 2+75W	2	139	17	168	.7	51	45	10029	5.06	272	5	ND	1	18	1	8	2	220	1.04	.039	8	95	1.21	77	.51	4	5.50	.01	.04	1	5
L10+00N 2+50W	1	5	2	23	.1	4	2	169	1.06	12	5	ND	1	6	1	2	3	27	.10	.008	2	4	.04	19	.01	2	.46	.01	.01	2	2
L10+00N 2+25W	1	40	8	73	1.6	10	6	294	6.47	19	5	ND	1	10	1	2	2	154	.41	.037	3	37	.20	25	.24	2	3.48	.01	.02	1	8
L10+00N 2+00W	1	132	9	125	.2	54	36	3364	6.11	181	5	ND	1	11	1	13	2	136	.56	.054	7	51	.58	47	.04	3	3.20	.01	.04	1	230
L10+00N 1+50W	1	120	7	146	.3	50	21	678	8.71	54	5	ND	1	9	1	2	3	229	.42	.068	4	79	.66	51	.33	3	4.20	.01	.04	1	10
STD C/AU-S	19	56	42	132	6.7	66	30	1023	4.01	39	18	8	37	47	20	18	19	60	.47	.091	39	55	.84	177	.07	33	1.94	.06	.14	12	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L10+00N 1+25W	1	164	14	113	.5	59	25	378	6.05	51	5	ND	1	9	1	4	2	155	.52	.038	4	51	1.06	55	.24	6	4.71	.01	.06	1	8
L10+00N 1+00W	1	64	6	94	.4	20	13	463	7.40	33	5	ND	1	14	1	3	2	194	.45	.046	4	60	.30	25	.20	2	3.05	.01	.02	1	1
L10+00N 0+75W	1	111	8	87	.7	32	15	469	9.36	20	5	ND	1	10	1	6	2	166	.45	.054	4	52	.44	23	.52	6	4.44	.01	.03	2	7
L10+00N 0+50W	1	22	2	57	.1	7	6	130	4.78	16	5	ND	1	4	1	2	2	130	.10	.042	2	14	.06	14	.05	2	1.26	.01	.02	1	1
L10+00N 0+25W	1	171	22	127	.4	63	28	939	5.07	36	5	ND	2	10	2	5	2	210	.62	.069	4	85	1.29	45	.42	5	5.63	.01	.05	1	4
L10+00N 0+00W	1	15	19	28	.2	6	2	201	4.65	15	5	ND	1	10	1	2	3	211	.13	.023	2	25	.08	12	.35	2	.80	.01	.03	1	10
L10+00N 0+25E	1	88	19	65	.8	26	9	232	12.19	17	5	ND	1	13	1	7	2	335	.55	.039	2	93	.48	24	.67	2	3.86	.01	.03	2	4
L10+00N 0+50E	1	25	8	38	.1	7	4	104	3.55	23	5	ND	1	7	1	3	2	122	.18	.022	2	17	.07	13	.10	7	.89	.01	.03	1	1
L10+00N 0+75E	1	17	9	26	.3	5	3	126	4.56	15	5	ND	1	7	1	3	2	173	.19	.018	2	16	.07	11	.24	2	.91	.01	.02	1	1
L10+00N 1+05E	1	42	13	61	.5	13	6	185	8.04	25	5	ND	2	11	1	7	3	157	.34	.046	2	51	.20	22	.37	3	2.85	.01	.03	2	27
L10+00N 1+50E	1	46	10	58	.3	14	6	160	5.78	14	5	ND	1	19	1	3	2	186	.56	.039	3	23	.31	44	.33	2	1.95	.01	.03	1	1
L10+00N 1+75E	1	12	7	25	.1	5	3	157	2.61	12	5	ND	1	6	1	2	2	134	.20	.014	2	8	.05	14	.11	3	.62	.01	.02	1	1
L10+00N 2+00E	1	46	11	54	.3	15	11	271	5.49	24	5	ND	1	7	1	2	2	170	.23	.042	4	44	.26	30	.13	2	3.53	.01	.03	4	1
L8+00N 5+50W	1	163	14	115	.9	69	27	521	10.75	16	5	ND	2	11	2	14	2	292	1.32	.074	4	123	1.76	15	.63	8	7.15	.01	.03	2	1
L8+00N 5+25W	1	100	13	54	.9	41	15	372	11.92	16	5	ND	3	9	1	14	2	318	.96	.110	2	118	.50	16	.85	4	7.52	.01	.03	5	1
L8+00N 5+00W	1	57	15	162	.6	51	19	439	10.61	61	5	ND	1	6	1	5	2	217	.31	.056	2	97	.61	27	.62	2	4.69	.01	.04	1	1
L8+00N 4+75W	1	162	29	272	3.3	45	17	512	11.40	115	5	ND	2	11	2	15	2	254	.97	.053	2	107	.67	21	.63	2	5.15	.01	.03	3	12
L8+00N 4+50W	1	117	12	140	1.0	36	17	340	13.02	28	5	ND	2	9	3	4	2	344	1.00	.075	3	113	.78	21	.63	3	5.86	.01	.03	2	3
L8+00N 4+25W	1	216	3	123	.5	68	26	500	10.89	221	5	ND	1	5	3	65	2	157	.27	.040	3	55	.54	24	.03	7	3.27	.01	.03	1	7
L8+00N 4+00W	1	76	9	98	.6	52	15	574	9.25	45	5	ND	1	11	1	2	2	295	.92	.071	3	79	.70	21	.76	3	4.08	.01	.03	1	6
L8+00N 3+75W	1	68	23	61	1.0	17	8	402	12.43	13	5	ND	2	13	1	2	3	440	.81	.065	2	95	.25	33	.95	2	2.18	.01	.03	1	2
L8+00N 3+25W	1	33	11	65	.2	15	9	459	6.27	77	5	ND	1	11	2	12	2	186	.70	.035	3	36	.17	35	.13	3	2.00	.01	.02	1	4
L8+00N 2+50W	2	75	11	61	.4	39	20	445	8.45	3106	5	ND	2	13	1	5	2	173	.67	.044	3	83	.60	36	.50	7	5.44	.01	.03	25	7
L8+00N 2+75W	2	61	26	60	.4	22	11	309	7.26	698	5	ND	1	14	2	5	2	152	.62	.028	3	46	.27	27	.36	7	2.62	.01	.04	2	26
L8+00N 1+75W	1	35	6	90	.9	24	5	186	13.63	20	5	ND	3	16	2	2	2	344	.65	.083	3	53	.25	24	.64	6	3.19	.01	.03	1	5
L8+00N 1+50W	1	50	4	102	.5	34	14	526	6.31	79	5	ND	1	11	2	3	2	165	.46	.050	2	51	.36	34	.14	5	2.16	.01	.05	2	1
L8+00N 1+25W	1	56	16	169	1.1	47	14	256	12.66	34	5	ND	2	6	1	15	2	319	.63	.075	2	122	.67	22	.83	3	6.03	.01	.03	4	2
L8+00N 1+00W	1	77	12	163	.9	44	16	465	9.92	38	5	ND	1	8	2	12	2	252	.63	.098	3	105	.79	34	.56	2	5.34	.01	.03	1	6
L8+00N 0+75W	1	52	8	46	.3	16	8	362	9.91	23	5	ND	1	6	2	6	2	337	.28	.049	2	70	.19	13	.60	5	2.03	.01	.01	4	6
L8+00N 0+50W	1	55	15	86	.3	21	16	845	5.98	42	5	ND	1	7	3	2	2	146	.34	.047	3	41	.22	33	.06	3	1.42	.01	.04	1	13
L8+00N 0+00W	1	72	6	63	.4	22	9	306	7.10	27	5	ND	2	6	2	2	2	192	.29	.045	2	52	.30	26	.17	5	3.12	.01	.03	2	345
L8+00N 0+25E	1	41	10	50	.5	12	6	174	7.01	29	5	ND	2	6	3	3	2	220	.18	.052	2	31	.09	16	.17	6	1.69	.01	.03	1	3
L8+00N 0+50E	1	62	7	71	.5	20	8	247	7.45	45	5	ND	3	7	4	3	2	209	.27	.043	2	48	.22	24	.19	6	2.73	.01	.03	1	1
L8+00N 1+00E	3	72	16	67	.4	17	7	151	7.62	82	5	ND	1	10	3	2	2	155	.19	.047	2	35	.16	27	.09	8	2.06	.01	.02	1	5
L8+00N 1+25E	1	67	5	96	.4	25	14	452	5.57	42	5	ND	2	7	3	2	2	238	.31	.072	3	70	.34	28	.26	5	4.11	.01	.08	1	1
L8+00N 1+50E	1	112	2	87	.4	36	16	445	6.71	33	5	ND	2	7	2	2	2	225	.35	.059	3	74	.51	33	.23	6	4.27	.01	.05	1	3
STD C/AU-S	20	59	40	132	7.2	70	32	1030	4.16	40	24	6	39	49	18	17	20	61	.46	.099	41	56	.91	181	.07	33	1.95	.06	.16	12	49

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-4741

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
16+00N 1+75E	1	70	22	82	.2	25	16	485	6.99	32	5	ND	1	8	2	5	2	164	.25	.041	3	45	.28	25	.08	4	3.35	.01	.04	2	1
16+00N 2+00E	1	54	29	75	.4	23	8	1661	6.04	33	5	ND	2	14	2	2	2	166	.60	.088	5	56	.23	31	.28	2	3.06	.02	.06	2	2
16+00N 5+50W	2	127	7	137	.8	45	22	610	11.00	32	5	ND	3	11	3	2	2	302	1.27	.069	2	100	1.27	25	.86	4	6.05	.01	.04	1	6
16+00N 5+25W	1	110	16	152	.8	50	23	918	10.94	14	5	ND	2	11	2	6	2	303	1.33	.067	3	107	1.11	30	.79	2	5.66	.01	.03	1	3
16+00N 5+00W	1	146	6	98	.4	71	29	564	9.18	14	5	ND	1	11	1	2	2	252	1.60	.048	3	102	2.05	15	.69	6	6.76	.01	.02	1	1
16+00N 4+75W	2	94	28	116	.4	43	19	448	9.27	30	5	ND	2	8	4	2	3	269	.97	.046	2	97	.92	23	.67	4	6.03	.01	.03	1	1
16+00N 4+50W	1	111	7	127	.7	36	17	414	11.16	25	5	ND	2	11	4	2	2	353	1.08	.065	2	98	.93	24	.66	4	5.21	.01	.03	1	2
16+00N 4+25W	1	124	10	82	.7	36	18	342	11.12	14	5	ND	3	7	2	2	2	318	.62	.082	3	115	.84	16	.76	4	7.12	.01	.03	1	5
16+00N 4+00W	1	85	32	114	1.1	29	14	315	13.77	7	5	ND	3	9	3	11	2	421	.79	.047	2	117	.52	18	.98	7	5.58	.01	.02	1	6
16+00N 3+75W	1	109	28	120	1.1	40	25	788	10.63	56	5	ND	1	13	2	12	2	352	1.00	.063	7	106	.74	26	.81	3	6.38	.01	.02	4	3
16+00N 3+50W	1	145	43	161	.5	60	36	2460	7.94	104	5	ND	1	21	1	8	2	185	1.23	.066	8	81	1.36	58	.34	4	6.14	.02	.09	1	5
16+00N 2+75W	1	129	58	179	.5	50	40	929	9.52	347	5	ND	1	10	1	25	2	210	.62	.048	6	89	.63	36	.23	3	6.39	.01	.04	4	12
16+00N 2+25W	1	150	15	107	.7	97	35	338	5.66	86	5	ND	1	10	2	6	2	260	.76	.023	4	57	1.46	64	.60	3	7.26	.01	.02	2	4
16+00N 1+75W	1	44	7	40	.5	19	6	122	8.56	33	5	ND	1	6	3	7	2	380	.21	.037	2	45	.08	6	.61	3	1.06	.01	.02	1	1
16+00N 1+50W	1	128	23	112	.7	66	17	297	10.16	58	5	ND	2	6	1	11	2	154	.65	.106	4	87	.57	25	.26	4	5.16	.01	.04	2	1
16+00N 1+25W	1	133	23	140	.7	129	37	1663	8.41	59	5	ND	1	8	1	12	2	203	.48	.068	4	76	.51	40	.34	4	4.43	.01	.04	4	1
16+00N 1+00W	1	105	21	95	.5	60	16	285	6.67	33	5	ND	3	7	2	6	4	144	.37	.061	2	74	.58	49	.08	2	4.70	.01	.02	4	1
16+00N 0+75W	1	96	24	62	.5	29	5	521	7.58	50	5	ND	1	10	1	7	2	194	.67	.054	2	76	.30	30	.19	2	3.49	.01	.03	2	1
16+00N 0+25W	1	70	21	77	.5	25	9	377	10.02	20	5	ND	2	7	1	4	3	256	.40	.034	2	72	.25	20	.49	2	3.40	.01	.02	1	1
16+00N 0+00W	1	58	20	59	.7	16	8	156	11.84	63	5	ND	2	7	1	10	2	300	.25	.037	2	72	.12	16	.50	4	1.52	.01	.02	2	2
16+00N 0+75E	1	30	11	60	.1	5	7	361	4.24	8	5	ND	1	2	1	2	5	66	.04	.037	2	6	.04	12	.01	2	.59	.01	.02	1	2
16+00N 1+00E	2	56	14	75	.2	20	10	227	5.01	21	5	ND	1	4	1	4	3	108	.10	.028	2	18	.07	20	.01	2	1.45	.01	.03	1	2
16+00N 1+25E	2	100	16	121	.5	41	20	340	7.65	36	5	ND	2	10	2	6	2	159	.20	.043	3	57	.22	34	.06	3	1.57	.01	.03	5	2
16+00N 1+50E	2	31	16	43	.3	11	5	156	5.19	21	5	ND	1	7	1	3	4	143	.09	.027	3	19	.04	20	.05	2	1.32	.01	.02	4	1
16+00N 1+75E	1	65	17	55	.2	21	10	167	5.71	25	5	ND	1	6	1	4	2	103	.18	.035	2	27	.17	36	.01	2	1.90	.01	.03	2	2
16+00N 2+00E	1	73	15	74	.2	24	10	197	7.69	35	5	ND	1	11	2	4	2	141	.36	.049	2	47	.22	27	.02	2	2.69	.01	.04	2	2
16+00N 2+25E	1	56	16	58	.1	14	7	292	6.17	35	5	ND	1	8	1	6	2	275	.26	.068	2	45	.17	18	.06	2	2.18	.01	.03	3	1
16+00N 2+50E	1	23	12	42	.2	8	6	210	4.01	12	5	ND	1	5	1	2	2	56	.12	.035	2	15	.08	26	.01	2	2.30	.01	.03	1	1
16+00N 2+75E	1	46	11	56	.1	14	6	175	5.66	26	5	ND	1	5	1	2	4	132	.15	.025	2	28	.15	17	.02	2	2.14	.01	.02	2	1
16+00N 3+00E	1	11	4	19	.1	3	2	58	2.89	9	5	ND	1	2	1	3	2	95	.02	.014	2	7	.03	17	.01	2	1.48	.01	.02	2	1
16+00N 3+25E	2	80	33	94	.5	15	12	247	11.22	33	5	ND	2	63	1	10	2	152	.06	.069	7	44	.05	64	.01	2	5.11	.01	.03	6	2
16+00N 3+50E	1	26	12	47	.1	10	7	204	6.55	21	5	ND	1	4	1	3	2	115	.09	.041	2	18	.09	19	.01	2	1.62	.01	.02	2	2
16+00N 3+75E	1	47	16	95	.2	22	10	501	5.64	23	5	ND	1	7	1	2	2	123	.21	.046	3	38	.16	50	.02	2	1.45	.01	.03	1	4
16+00N 4+00E	1	19	12	25	.1	5	3	105	3.09	9	5	ND	1	2	1	2	2	89	.05	.018	2	9	.06	11	.01	2	1.31	.01	.03	2	3
16+00N 4+25E	1	77	16	56	.4	27	13	233	7.09	25	5	ND	1	7	1	4	2	152	.27	.039	3	48	.31	49	.05	4	2.74	.01	.03	2	2
16+00N 4+50E	1	30	5	46	.1	5	5	154	4.10	9	5	ND	1	4	1	2	2	73	.12	.017	2	17	.30	25	.01	2	2.53	.01	.02	3	1
STD C/AU-S	19	62	42	132	7.2	72	31	1051	4.34	42	17	8	38	52	17	16	18	60	.49	.093	40	58	.93	182	.08	32	2.06	.06	.15	12	50

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-4741

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti	B PPM	Al %	Na %	K %	W PPM	Au* PPB
16+00N 4+75E	1	20	18	28	.1	4	3	104	3.33	7	5	ND	1	4	1	2	2	66	.10	.023	2	9	.05	34	.01	5	1.70	.01	.04	2	1
16+00N 5+25E	1	67	22	86	.4	25	11	286	8.26	28	5	ND	2	12	2	6	2	183	.54	.040	3	52	.33	47	.06	6	3.51	.01	.05	4	1
16+00N 5+50E	1	66	16	137	.4	33	14	262	9.37	35	5	ND	2	8	1	7	4	197	.32	.043	3	74	.45	50	.16	7	5.00	.01	.04	4	1
16+00N 5+75E	1	83	14	92	.2	27	13	341	7.36	34	5	ND	2	8	1	4	2	158	.28	.038	3	54	.40	48	.02	5	4.56	.01	.04	3	6
16+00N 6+00E	1	88	17	83	.3	25	11	286	5.17	31	5	ND	2	7	1	7	2	169	.26	.046	3	65	.27	27	.30	4	4.05	.01	.03	4	1
16+00N 6+25E	1	106	16	62	.3	29	12	251	6.65	35	5	ND	2	8	1	5	2	198	.35	.044	3	65	.39	40	.14	7	4.60	.01	.04	2	1
16+00N 6+50E	1	45	10	65	.3	19	16	576	6.27	17	5	ND	2	11	1	2	2	141	.40	.032	3	43	.31	60	.02	4	3.45	.01	.04	1	2
16+00N 6+75E	1	7	5	25	.1	4	6	140	1.90	16	5	ND	1	3	1	3	2	51	.07	.011	4	5	.06	34	.01	3	1.42	.01	.05	2	1
16+00N 7+00E	1	23	12	59	.1	8	6	311	2.82	3	5	ND	1	11	1	4	2	64	.33	.016	4	13	.15	75	.01	2	2.52	.01	.05	1	1
16+00N 7+50E	2	115	13	83	.3	26	11	182	7.33	31	5	ND	2	13	1	6	2	149	.27	.038	3	49	.30	52	.04	2	3.98	.01	.05	2	1
16+00N 7+75E	1	82	11	84	.2	27	11	384	7.42	40	5	ND	1	11	1	2	2	189	.45	.036	4	46	.27	41	.10	4	2.86	.01	.04	3	1
16+00N 8+00E	1	107	16	95	.4	32	12	241	9.00	80	5	ND	2	8	1	6	2	224	.38	.035	5	66	.31	31	.19	6	3.50	.01	.03	2	2
16+00N 8+25E	1	84	14	87	.7	40	14	471	6.98	54	5	ND	2	13	1	6	2	225	.82	.035	6	89	.51	38	.34	5	3.85	.01	.04	3	1
16+00N 8+50E	1	141	16	141	.5	76	25	777	8.55	62	5	ND	2	12	1	5	2	210	.65	.039	5	96	1.02	83	.33	7	5.52	.01	.06	3	1
14+00N 5+50W	1	142	11	114	.6	56	34	1029	11.84	77	5	ND	3	21	1	12	2	348	1.40	.077	7	100	1.42	32	.64	5	6.43	.01	.04	3	1
14+00N 5+25W	1	79	11	136	.7	38	24	654	11.68	21	5	ND	2	14	1	3	2	331	1.13	.071	6	106	.65	44	.79	5	7.08	.01	.04	1	5
14+00N 4+75W	1	111	8	90	.6	55	24	467	10.99	29	5	ND	2	6	1	25	2	259	.52	.051	4	102	1.27	33	.20	8	5.13	.01	.04	2	2
14+00N 4+50W	1	155	13	117	.8	69	25	569	10.68	28	5	ND	2	13	1	15	2	284	1.22	.078	6	124	1.59	33	.56	12	7.65	.01	.04	2	3
14+00N 4+25W	1	153	7	128	1.3	74	25	723	11.40	28	5	ND	1	11	1	19	2	298	1.23	.062	4	128	1.94	39	.66	5	7.36	.01	.03	6	1
14+00N 4+00W	1	146	19	162	2.0	75	34	762	9.82	36	5	ND	1	15	1	16	2	243	1.37	.044	8	115	1.75	40	.77	4	7.20	.01	.04	5	1
14+00N 3+75W	1	125	7	77	.4	46	25	363	9.93	59	5	ND	1	4	1	35	2	362	.12	.036	2	61	.21	15	.05	6	2.46	.01	.02	1	1
14+00N 3+50W	1	54	19	100	1.1	28	14	322	15.25	17	5	ND	2	11	1	17	2	399	.83	.065	4	112	.54	25	.80	7	3.95	.01	.02	4	1
14+00N 3+25W	1	82	11	98	1.1	42	38	246	12.03	15	5	ND	2	11	1	14	2	329	.96	.052	4	117	.61	31	.85	4	5.66	.01	.03	2	2
14+00N 3+00W	1	88	14	153	.9	41	18	292	12.47	19	5	ND	2	11	1	13	2	358	.38	.074	4	113	.75	36	.92	6	5.38	.01	.03	2	1
14+00N 2+75W	1	98	2	118	.8	50	20	300	12.44	23	5	ND	2	11	1	6	2	354	1.10	.060	3	125	1.07	27	.81	4	5.93	.01	.03	1	1
14+00N 2+50W	1	47	15	140	.5	24	15	779	10.48	147	5	ND	5	21	1	14	2	263	.95	.065	39	62	.23	39	.43	3	2.15	.01	.02	1	1
14+00N 2+25W	1	111	10	91	.8	40	17	397	12.68	15	5	ND	1	9	1	6	2	437	.72	.063	4	125	.87	28	.63	4	6.02	.01	.02	2	3
14+00N 2+00W	1	186	14	122	1.4	55	25	384	10.52	48	5	ND	1	10	1	19	2	320	1.14	.154	5	127	1.27	22	.82	3	7.20	.01	.03	5	1
14+00N 1+75W	1	122	12	97	.4	46	16	315	6.30	235	5	ND	1	7	1	4	2	215	.32	.076	6	73	.30	30	.25	2	3.69	.01	.02	2	2
14+00N 1+50W	1	102	12	132	.4	51	18	2429	8.28	172	5	ND	3	7	1	5	2	205	.34	.141	7	83	.29	28	.20	3	4.41	.01	.02	3	2
14+00N 1+25W	1	60	10	92	.1	47	12	393	8.38	118	5	ND	1	5	1	2	3	158	.09	.044	3	65	.12	19	.06	2	1.83	.01	.02	1	1
14+00N 1+00W	1	104	16	69	.4	53	10	200	8.16	95	5	ND	1	7	1	14	2	212	.55	.070	7	94	.40	17	.39	2	5.53	.01	.02	6	2
14+00N 0+75W	1	151	5	120	.3	52	17	224	9.25	137	5	ND	2	7	1	3	2	240	.46	.034	10	99	.65	38	.37	2	5.03	.01	.03	1	1
14+00N 0+50W	1	107	20	128	.2	48	36	2215	8.75	224	5	ND	1	10	1	5	2	149	.42	.051	8	61	.56	51	.03	3	3.90	.01	.04	1	8
14+00N 0+25W	1	58	20	62	.2	24	9	192	9.78	257	5	ND	1	6	1	2	2	244	.14	.015	5	66	.16	30	.05	2	2.17	.01	.02	1	1
14+00N 0+00W	1	90	11	65	1.0	24	10	146	5.06	25	5	ND	2	5	1	2	2	173	.05	.025	5	78	.03	14	.01	2	3.83	.01	.01	1	17
STD C/AU-S	20	62	43	132	7.0	71	31	1031	4.32	43	17	6	40	51	18	17	19	64	.51	.091	42	60	.94	180	.08	32	2.05	.06	.16	12	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
14+00N 0+25E	1	47	9	46	.7	19	8	329	6.85	46	5	ND	3	4	2	4	2	215	.14	.037	7	46	.06	10	.22	3	1.62	.01	.02	1	2
14+00N 0+50E	1	167	10	148	.4	41	19	358	6.88	104	5	ND	5	8	2	3	2	135	.25	.040	2	58	.26	15	.10	6	2.22	.01	.02	2	1
14+00N 0+75E	1	98	11	78	.2	26	10	202	6.98	118	5	ND	3	6	1	2	2	192	.24	.044	6	61	.17	13	.13	4	2.12	.01	.02	1	1
14+00N 1+00E	1	30	14	64	.1	7	11	570	2.59	26	5	ND	1	5	1	2	2	58	.34	.017	5	14	.07	35	.01	5	1.18	.01	.04	1	1
14+00N 1+25E	1	122	8	108	.7	42	13	221	7.46	123	5	ND	4	6	2	2	2	169	.41	.048	8	75	.42	25	.23	6	3.91	.01	.02	1	2
14+00N 1+50E	1	101	9	77	.3	33	10	456	5.12	161	5	ND	4	5	1	7	2	237	.34	.060	11	78	.25	12	.34	4	3.66	.01	.03	1	1
14+00N 1+75E	1	64	7	52	.3	17	7	201	6.20	80	5	ND	3	5	1	6	2	190	.17	.044	5	38	.38	14	.17	2	1.40	.01	.02	2	2
14+00N 2+00E	1	84	8	85	.2	27	11	249	5.54	104	5	ND	3	6	1	3	2	166	.23	.034	9	39	.13	23	.07	5	1.67	.01	.03	1	1
14+00N 2+25E	1	59	13	148	.4	40	34	924	6.64	49	5	ND	3	5	1	2	2	163	.29	.037	8	53	.18	43	.06	2	3.86	.01	.04	2	1
14+00N 2+50E	1	88	24	123	.6	44	23	1000	7.92	38	5	ND	3	12	3	7	2	241	.62	.039	3	89	.73	61	.45	4	3.42	.01	.04	1	1
14+00N 2+75E	1	105	12	187	.5	56	18	274	7.01	79	5	ND	3	22	1	4	2	157	.41	.043	5	57	.38	59	.09	5	3.34	.01	.04	1	1
14+00N 3+00E	1	31	18	68	.1	21	13	256	4.39	60	5	ND	3	4	1	2	2	72	.06	.040	4	31	.04	16	.01	2	1.16	.01	.03	1	2
14+50N 3+25E	1	54	15	65	.4	22	8	293	6.65	63	5	ND	3	8	2	2	2	218	.36	.049	6	56	.17	22	.27	3	2.15	.01	.03	1	1
14+00N 3+50E	1	65	9	67	.3	26	11	307	7.41	63	5	ND	4	6	3	3	3	222	.26	.047	6	62	.17	21	.20	3	2.78	.01	.03	1	4
14+00N 3+75E	1	29	9	35	.5	12	4	145	6.17	36	5	ND	3	5	1	6	2	249	.21	.024	5	41	.08	14	.35	2	1.35	.01	.02	2	1
14+00N 4+00E	1	93	8	52	.3	33	11	542	8.06	61	5	ND	4	8	1	4	2	222	.42	.064	4	75	.36	37	.20	2	4.04	.01	.03	2	4
14+00N 4+25E	1	36	15	48	.3	33	5	215	6.17	26	5	ND	3	7	1	2	2	254	.28	.048	4	60	.14	21	.44	2	2.37	.01	.03	2	3
14+00N 4+50E	1	120	6	93	.1	42	16	341	7.40	47	5	ND	3	7	1	2	2	192	.37	.058	3	74	.56	36	.17	7	4.96	.01	.04	1	2
14+00N 4+75E	1	28	7	51	.2	14	6	241	6.63	27	5	ND	2	8	1	5	3	195	.44	.041	4	46	.17	31	.09	2	2.41	.01	.03	2	2
14+00N 5+00E	1	54	7	53	.2	20	9	340	6.83	30	5	ND	3	5	2	4	3	216	.31	.042	7	44	.16	14	.23	4	2.04	.01	.02	1	1
14+00N 5+25E	1	95	9	57	.2	22	6	196	6.76	46	5	ND	2	6	1	4	2	222	.29	.064	2	82	.24	17	.26	3	4.10	.01	.03	1	1
14+00N 5+50E	1	102	13	80	.4	39	12	254	8.02	60	5	ND	3	7	2	5	2	221	.39	.048	2	89	.37	26	.32	2	4.96	.01	.03	2	3
14+00N 5+75E	1	98	15	86	.3	39	13	324	8.52	39	5	ND	3	7	2	4	3	244	.43	.068	2	87	.50	27	.36	3	4.90	.01	.03	1	1
14+00N 6+00E	1	64	27	67	.1	23	9	280	6.15	30	5	ND	2	6	1	3	2	171	.30	.049	2	56	.30	27	.07	3	3.91	.01	.03	1	1
14+00N 6+25E	1	25	7	46	.1	10	6	164	5.77	23	5	ND	2	6	1	2	3	163	.19	.037	3	33	.13	20	.02	2	2.42	.01	.03	1	3
14+00N 6+50E	1	24	11	46	.1	7	7	299	5.66	15	5	ND	2	2	1	2	2	124	.07	.039	2	17	.09	20	.01	2	1.92	.01	.02	2	2
14+00N 6+75E	1	102	17	52	.4	39	16	936	7.74	34	5	ND	3	9	1	4	3	244	.63	.073	2	66	.56	28	.47	2	4.54	.01	.04	2	4
14+00N 7+00E	2	86	9	66	.2	12	7	171	7.68	32	5	ND	2	6	1	4	2	157	.17	.051	2	43	.14	36	.03	2	3.19	.01	.02	3	1
14+00N 7+25E	1	101	13	70	.2	25	10	402	6.70	35	5	ND	2	9	1	2	2	185	.40	.057	2	60	.31	26	.16	3	2.96	.01	.03	1	1
14+00N 6+75E	1	54	13	88	.1	39	19	600	6.75	48	5	ND	2	8	1	3	2	201	.49	.045	4	73	.46	40	.25	4	3.73	.01	.04	1	1
14+00N 9+00E	1	102	6	106	.2	42	16	329	6.92	45	5	ND	3	6	2	2	3	202	.61	.038	3	70	.60	42	.34	6	3.77	.01	.03	1	1
12+00N 5+50W	1	94	9	90	.4	46	21	613	9.56	47	5	ND	3	11	1	11	2	268	1.32	.070	3	102	.54	25	.77	4	4.19	.01	.03	1	1
12+00N 5+25W	1	108	15	108	.6	61	24	696	6.59	426	5	ND	3	12	1	61	2	245	.84	.039	2	94	.60	36	.27	2	4.06	.01	.03	1	1
12+00N 5+00W	1	123	8	146	.7	67	29	687	8.10	39	5	ND	3	11	2	9	2	274	1.32	.076	2	116	1.44	36	.68	4	6.38	.01	.03	1	20
12+00N 4+75W	1	134	8	203	.1	60	33	2701	7.60	83	5	ND	2	34	1	10	2	196	.90	.045	9	95	1.31	54	.18	4	5.34	.01	.05	1	4
12+00N 4+50W	1	186	9	85	.5	38	19	452	6.18	25	5	ND	3	9	1	6	2	270	.78	.076	3	91	.71	57	.47	4	5.21	.01	.03	1	7
STD C/AU-S	20	63	40	137	7.3	73	31	1062	4.01	40	21	8	40	53	15	17	24	60	.50	.095	40	57	.92	162	.06	33	1.95	.06	.17	12	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L2+00N 4+25W	1	64	27	107	.9	27	10	370	15.56	16	5	ND	3	7	1	2	4	389	.49	.131	3	113	.36	41	.73	2	5.51	.01	.03	1	6
L2+00N 4+00W	1	257	23	133	.6	49	21	562	12.91	15	5	ND	2	6	1	2	2	263	.39	.127	5	114	.65	46	.07	2	6.01	.01	.04	1	1
L2+00N 3+75W	1	103	25	97	.3	38	18	575	9.70	81	5	ND	2	9	1	2	2	236	.49	.088	4	81	.41	50	.10	3	4.45	.01	.05	1	3
L2+00N 3+50W	1	110	27	92	.2	39	22	1564	9.43	18	5	ND	1	10	1	4	2	250	.72	.074	4	92	.69	46	.31	5	5.36	.02	.09	1	4
L2+00N 3+25W	1	66	27	78	.5	22	12	666	9.92	17	5	ND	2	6	1	2	2	256	.35	.073	4	74	.26	39	.06	4	3.85	.01	.03	1	5
L2+00N 3+00W	1	211	21	104	.8	76	37	1008	11.15	20	5	ND	2	9	1	7	2	275	.84	.056	4	130	1.38	45	.55	6	7.11	.01	.03	1	1
L2+00N 2+75W	1	117	34	116	.6	48	24	1613	10.76	48	5	ND	2	14	1	8	2	284	.58	.063	4	112	.89	63	.58	5	5.24	.01	.04	1	17
L2+00N 2+50W	1	72	17	70	.3	30	14	556	7.30	39	5	ND	1	7	1	4	3	220	.51	.041	2	69	.49	25	.44	4	3.03	.01	.02	1	4
L2+00N 2+25W	1	134	21	107	.9	51	24	906	10.10	16	5	ND	3	17	1	5	2	287	.96	.060	4	113	1.01	60	.59	7	5.54	.01	.06	1	1
L2+00N 2+00W	1	121	18	93	.8	46	21	778	9.29	21	5	ND	2	11	1	4	2	264	.84	.067	3	98	.78	37	.54	5	4.64	.01	.03	1	5
L2+00N 1+75W	1	157	21	95	.7	57	20	468	10.55	25	5	ND	2	8	1	2	2	300	.84	.060	3	119	1.01	24	.65	5	5.98	.01	.02	1	1
L2+00N 1+50W	1	103	19	92	.9	62	19	377	11.80	13	5	ND	3	9	1	8	2	350	.66	.056	3	152	.88	18	.77	5	6.78	.01	.02	1	1
L2+00N 1+25W	1	95	19	76	.3	43	17	1077	6.05	21	5	ND	2	8	1	2	2	210	.44	.063	4	83	.85	27	.29	5	3.74	.01	.07	1	1
L2+00N 1+00W	1	43	12	65	.5	29	10	375	7.10	30	5	ND	2	4	1	2	2	164	.20	.054	2	57	.16	17	.09	4	2.67	.01	.02	2	4
L2+00N 0+75W	1	89	25	83	.7	40	15	425	10.56	22	5	ND	3	8	1	6	3	264	.54	.096	2	129	.56	25	.60	2	5.68	.01	.03	1	3
L2+00N 0+50W	1	65	12	88	.1	56	16	250	5.97	78	5	ND	1	5	1	2	2	148	.32	.033	2	71	.44	45	.06	3	3.55	.01	.02	1	1
L2+00N 0+25W	1	113	13	88	.6	46	15	249	10.22	42	5	ND	2	7	1	5	2	249	.49	.056	2	109	.50	25	.46	2	5.16	.01	.02	1	6
L2+00N 0+00W	1	203	17	97	.1	87	44	1365	7.09	150	5	ND	1	10	1	2	2	109	1.11	.074	11	50	.12	48	.01	17	.93	.01	.13	1	3
L2+00N 0+25E	2	134	17	136	.4	54	18	327	9.69	64	5	ND	2	5	1	2	2	213	.36	.066	3	95	.56	35	.25	4	6.53	.01	.03	1	2
L2+00N 0+50E	1	131	20	149	1.0	60	20	333	9.15	78	5	ND	2	7	1	5	2	210	.49	.085	2	101	.68	33	.37	6	5.70	.01	.03	1	1
L2+00N 0+75E	2	92	24	72	.1	39	18	211	4.62	272	5	ND	1	5	1	3	2	141	.19	.023	2	33	.17	27	.06	4	1.76	.01	.02	1	6
L2+00N 1+00E	1	112	20	127	.4	61	18	511	7.92	102	5	ND	2	6	1	2	2	186	.42	.041	3	76	.60	44	.13	3	3.93	.01	.03	1	1
L2+00N 1+25E	1	42	25	58	.3	18	9	587	9.02	63	5	ND	2	5	1	2	2	200	.29	.053	2	45	.19	16	.25	5	2.01	.01	.02	1	2
L2+00N 1+50E	1	84	24	100	.1	32	15	229	6.25	240	5	ND	1	7	1	2	2	172	.24	.028	2	53	.36	54	.06	2	3.36	.01	.02	1	1
L2+00N 1+75E	2	78	17	76	.1	21	10	303	5.46	206	5	ND	1	6	1	2	2	147	.17	.037	2	39	.17	32	.04	2	2.22	.01	.02	1	1
L2+00N 2+00E	1	67	22	65	.1	23	11	653	6.67	185	5	ND	1	8	1	2	3	151	.28	.079	2	52	.21	30	.17	2	2.57	.01	.02	2	1
L2+00N 2+25E	2	107	21	94	.1	34	19	637	6.34	255	5	ND	1	9	1	2	2	166	.29	.043	4	56	.35	49	.09	2	3.25	.01	.03	1	1
L2+00N 2+50E	1	91	13	84	.1	28	16	553	6.04	387	5	ND	1	12	1	2	2	159	.24	.037	4	49	.27	44	.07	2	2.70	.01	.02	1	2
L2+00N 2+75E	5	53	23	54	.3	15	7	252	7.17	632	5	ND	1	9	1	2	2	208	.17	.046	3	50	.17	81	.05	2	2.88	.01	.02	1	5
L2+00N 3+00E	1	59	25	74	.2	16	10	620	6.50	225	5	ND	2	11	1	2	2	119	.24	.099	3	29	.14	29	.03	3	1.91	.01	.03	2	3
L2+00N 3+25E	1	102	22	134	.1	59	25	630	5.54	67	5	ND	2	9	1	2	2	245	.71	.060	4	103	.84	56	.43	2	5.31	.01	.03	1	1
L2+00N 3+50E	1	88	17	123	.1	38	18	362	6.46	231	5	ND	2	10	1	2	2	146	.33	.041	3	58	.39	65	.05	3	3.71	.01	.03	1	1
L2+00N 3+75E	1	133	21	125	.2	47	34	1320	7.09	158	5	ND	2	8	1	2	2	144	.36	.115	4	66	.49	58	.07	7	5.14	.01	.03	1	2
L2+00N 4+00E	1	37	14	63	.1	12	8	262	4.09	44	5	ND	1	4	1	2	2	79	.09	.040	2	17	.09	26	.01	4	1.68	.01	.03	2	1
L2+00N 4+25E	1	71	17	83	.3	25	12	684	7.48	92	5	ND	2	9	1	3	2	185	.40	.059	3	56	.27	41	.13	2	3.29	.01	.04	1	4
L2+00N 4+50E	1	47	11	73	.1	17	12	808	4.84	64	5	ND	1	9	1	2	2	90	.34	.043	3	26	.19	48	.01	3	2.32	.01	.04	1	2
STD C/AU-S	19	58	42	132	6.8	68	31	1023	4.25	38	22	8	37	48	20	18	19	60	.49	.090	39	55	.90	177	.07	33	2.07	.06	.15	11	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L2+00N 4+75E	1	23	27	57	.1	8	6	654	3.31	16	5	ND	1	8	1	2	2	63	.26	.040	2	12	.07	46	.01	3	1.09	.01	.02	1	1
L2+00N 5+00E	1	29	17	64	.1	10	8	752	3.64	24	5	ND	1	5	1	2	2	73	.17	.052	2	15	.14	50	.01	2	2.35	.01	.03	1	2
L2+00N 5+25E	1	52	26	93	.1	15	9	240	6.36	35	5	ND	1	4	1	8	2	110	.19	.099	2	40	.24	53	.01	2	5.10	.01	.03	1	1
L2+00N 5+50E	1	28	13	69	.1	7	5	157	2.94	2	5	ND	1	2	1	2	2	46	.03	.029	2	11	.13	29	.01	2	1.93	.01	.03	1	1
L2+00N 5+75E	1	32	25	81	.1	13	10	330	4.55	11	5	ND	1	2	1	2	3	71	.03	.040	2	20	.09	41	.01	2	3.24	.01	.02	1	1
L2+00N 6+25E	1	111	27	142	.3	42	19	1142	7.14	44	5	ND	1	10	1	5	2	171	.45	.079	2	85	.56	43	.09	3	5.38	.01	.01	4	1
L2+00N 6+50E	1	70	30	110	.7	19	13	1773	7.90	39	5	ND	1	9	1	2	2	185	.45	.122	3	53	.23	68	.17	2	2.85	.01	.03	1	1
L2+00N 7+50E	1	91	19	75	.1	29	11	226	7.37	137	5	ND	1	7	1	10	2	180	.39	.048	2	73	.36	26	.13	3	3.73	.01	.01	2	1
L2+00N 7+75E	1	88	22	102	.3	35	14	591	7.01	92	5	ND	1	7	1	3	3	159	.42	.047	2	80	.47	31	.20	2	5.36	.01	.02	1	7
L2+00N 8+00E	1	91	20	90	.1	38	16	388	6.96	92	5	ND	1	8	1	2	2	166	.54	.045	2	75	.54	36	.19	2	4.42	.01	.02	1	1
L2+00N 8+25E	1	75	12	69	.1	26	10	312	6.40	66	5	ND	1	10	1	2	2	158	.43	.031	3	58	.36	37	.10	2	2.68	.01	.01	1	1
L2+00N 8+50E	1	53	11	55	.1	20	9	242	4.70	20	5	ND	1	6	1	2	2	112	.37	.025	3	46	.31	37	.08	2	3.33	.01	.02	1	1
L2+00N 8+75E	1	63	12	57	.1	18	8	187	5.20	35	5	ND	1	6	1	2	3	131	.24	.029	3	44	.24	32	.07	2	3.01	.01	.02	1	1
L2+00N 9+00E	1	54	13	56	.1	18	8	179	5.59	33	5	ND	1	6	1	2	5	134	.28	.028	4	44	.25	29	.06	2	2.64	.01	.02	1	1
L0+00N 5+50W	1	105	20	79	.1	53	17	343	8.50	10	7	ND	1	10	1	3	2	295	.87	.080	3	117	1.14	14	.67	2	6.97	.01	.02	1	2
L0+00N 5+25W	1	65	16	87	.3	30	14	767	8.24	2	5	ND	1	12	1	2	2	314	.92	.081	3	101	.72	26	.76	2	4.41	.01	.02	1	10
L0+00N 5+00W	1	137	27	92	.2	63	24	534	7.74	31	5	ND	1	11	1	13	2	242	1.05	.093	3	122	1.40	14	.53	4	8.17	.01	.01	5	5
L0+00N 4+75W	1	104	18	102	.2	51	19	416	8.17	13	7	ND	2	11	1	3	2	303	.88	.066	4	119	1.00	27	.67	2	5.98	.01	.02	1	1
L0+00N 4+50W	1	108	11	62	.2	17	10	567	11.18	16	5	ND	1	5	1	2	2	302	.13	.063	4	93	.19	38	.03	2	2.43	.01	.02	1	1
L0+00N 4+25W	1	72	25	83	.3	31	12	518	11.01	14	5	ND	1	7	2	2	2	354	.42	.074	3	139	.45	34	.48	2	4.85	.01	.02	1	2
L0+00N 4+00W	1	127	6	98	.3	51	23	372	6.80	7	5	ND	1	3	1	2	2	166	.11	.051	2	77	.38	39	.02	2	3.32	.01	.02	1	1
L0+00N 3+75W	1	145	18	82	.1	64	27	490	8.94	5	5	ND	1	8	2	2	2	273	.79	.044	4	118	1.06	48	.47	3	6.22	.01	.02	1	1
L0+00N 3+50W	1	58	17	85	.2	25	16	1396	8.50	7	5	ND	1	9	1	2	2	276	.76	.076	2	90	.54	33	.65	2	4.14	.01	.03	1	1
L0+00N 3+25W	1	89	13	80	.1	38	15	433	8.04	10	6	ND	1	10	1	2	2	245	.70	.059	3	103	.64	45	.25	2	4.38	.01	.03	1	1
L0+00N 3+00W	1	146	14	91	.1	65	27	865	8.13	2	5	ND	1	9	1	2	2	241	.84	.052	3	118	1.46	42	.45	2	5.82	.01	.02	1	4
L0+00N 2+75W	1	122	27	114	.1	70	26	561	9.06	29	5	ND	1	9	2	11	2	259	.53	.060	4	131	.97	59	.24	5	6.06	.01	.01	5	1
L0+00N 2+50W	1	109	18	94	.1	44	38	359	9.10	13	5	ND	2	6	1	2	2	278	.53	.046	4	114	.58	35	.36	2	5.15	.01	.02	1	1
L0+00N 2+25W	1	190	16	106	.1	68	26	475	8.45	20	6	ND	1	8	1	2	3	233	.66	.053	3	119	1.00	61	.28	4	5.69	.01	.02	1	2
L0+00N 2+00W	1	88	14	78	.2	23	13	474	9.29	11	6	ND	1	8	1	2	2	355	.67	.044	3	96	.46	27	.61	3	3.68	.01	.02	1	1
L0+00N 1+75W	1	57	20	60	.1	18	7	161	11.31	4	7	ND	1	7	1	4	2	435	.42	.040	7	133	.38	24	.73	2	4.12	.01	.02	1	4
L0+00N 1+25W	1	84	18	110	.4	35	15	414	9.56	17	5	ND	1	7	1	2	2	297	.62	.048	3	110	.47	33	.44	2	4.73	.01	.02	1	1
L0+00N 1+00W	1	73	11	133	.4	45	15	357	9.03	42	5	ND	1	8	1	2	2	248	.61	.060	3	103	.66	34	.42	2	4.38	.01	.02	1	1
L0+00N 0+75W	1	108	15	116	.3	47	16	568	8.05	94	5	ND	1	6	1	2	3	175	.43	.108	3	66	.48	40	.15	2	4.10	.01	.03	1	1
L0+00N 0+50W	1	89	18	88	.1	33	13	755	8.24	34	5	ND	1	6	1	2	4	230	.52	.082	2	89	.39	23	.32	2	3.94	.01	.01	1	1
L0+00N 0+25W	1	65	18	66	.3	21	7	252	8.98	30	5	ND	1	6	1	2	2	291	.40	.079	3	88	.35	20	.46	2	3.22	.01	.01	1	2
L0+00N 0+00W	1	86	20	108	.5	52	26	612	6.86	43	5	ND	1	10	1	10	2	249	.72	.070	4	93	.66	50	.36	3	4.48	.01	.01	4	1
STD C/AU-S	18	59	42	132	7.2	66	29	1034	4.11	43	18	8	36	47	19	17	22	57	.51	.095	37	55	.91	175	.07	34	1.95	.06	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L0+00N 0+25E	1	88	2	124	.3	91	24	366	6.68	35	5	ND	2	11	1	2	2	197	1.03	.038	3	96	.88	53	.36	4	4.77	.01	.03	1	1
L0+00N 0+50E	1	43	4	76	.1	36	11	158	4.66	35	5	ND	2	3	1	2	2	145	.11	.019	2	33	.10	17	.06	6	3.48	.01	.02	2	2
L0+00N 0+75E	1	72	11	117	.9	42	17	697	10.65	19	5	ND	4	11	1	2	3	251	.49	.126	2	122	.61	26	.59	6	6.09	.01	.04	1	61
L0+00N 1+00E	1	103	15	126	.5	59	22	464	10.59	52	5	ND	3	7	1	2	2	239	.49	.057	2	115	.75	40	.33	4	5.80	.01	.03	1	4
L0+00N 1+25E	1	138	23	107	.5	51	18	525	10.47	52	5	ND	3	7	1	6	3	230	.51	.089	2	121	.61	28	.35	7	6.47	.01	.04	2	2
L0+00N 1+50E	1	153	17	121	.5	64	21	289	9.12	112	5	ND	3	7	1	4	2	218	.49	.055	3	102	.75	42	.23	8	5.50	.01	.03	1	1
L0+00N 1+75E	1	55	16	62	.3	20	7	260	10.08	151	5	ND	3	8	1	5	3	270	.36	.068	3	73	.20	22	.33	6	2.42	.01	.04	2	3
L0+00N 2+00E	1	58	13	56	.5	24	6	219	9.13	59	5	ND	3	7	2	2	2	273	.43	.049	2	76	.28	17	.39	4	2.48	.01	.03	1	1
L0+00N 2+25E	1	158	9	145	.3	69	21	338	8.87	51	5	ND	3	7	1	2	2	223	.66	.089	2	105	.66	38	.36	6	6.55	.01	.03	1	6
L0+00N 2+50E	1	158	19	217	.2	128	25	2860	8.55	232	5	ND	2	13	1	2	2	188	.52	.048	5	102	1.19	75	.27	6	4.58	.01	.04	2	1
L0+00N 2+75E	1	58	29	87	.5	26	9	419	10.91	314	5	ND	3	7	1	2	2	260	.44	.106	2	91	.30	23	.35	5	2.98	.01	.04	1	4
L0+00N 3+00E	1	39	14	97	.2	25	12	375	7.69	353	5	ND	3	13	1	2	2	209	.50	.038	4	60	.27	37	.30	6	2.14	.01	.03	1	2
L0+00N 3+25E	1	37	16	82	.4	24	11	268	7.19	104	5	ND	2	14	1	2	2	186	.63	.048	4	66	.24	33	.30	4	2.15	.01	.03	1	1
L0+00N 3+50E	1	78	9	59	.4	27	9	190	9.13	95	5	ND	3	9	1	2	2	235	.46	.064	2	75	.35	22	.23	2	2.65	.01	.03	1	1
L0+00N 3+75E	1	153	13	142	.5	71	24	318	9.00	148	5	ND	3	8	1	2	2	203	.46	.065	4	103	.81	47	.22	8	6.42	.01	.06	1	2
L0+00N 4+50E	1	128	19	285	.9	119	41	638	8.85	117	5	ND	3	8	1	5	2	173	.42	.056	3	103	.85	56	.21	4	6.33	.01	.05	1	1
L0+00N 4+75E	1	116	16	106	.4	49	17	310	5.82	75	5	ND	3	7	1	2	2	235	.39	.068	3	100	.56	37	.23	7	4.95	.01	.03	1	1
L0+00N 5+00E	1	193	13	106	.5	67	26	328	6.54	65	5	ND	2	7	1	5	2	208	.53	.041	4	102	1.00	66	.16	9	5.16	.01	.03	3	1
L0+00N 5+25E	1	85	9	78	.6	35	11	156	6.44	75	5	ND	3	10	1	2	2	236	.55	.087	3	62	.50	23	.34	4	3.47	.01	.03	1	2
L0+00N 5+50E	1	38	19	70	.4	21	10	603	7.77	37	5	ND	1	10	1	5	2	207	.52	.052	4	75	.23	23	.30	2	2.98	.01	.03	1	1
L0+00N 5+75E	1	105	39	111	.1	50	16	259	7.71	77	5	ND	3	7	1	2	2	186	.39	.054	3	76	.42	43	.15	5	4.42	.01	.05	1	5
L0+00N 6+25E	1	26	15	34	.3	14	5	464	7.47	46	5	ND	3	5	2	5	2	255	.22	.043	3	45	.09	11	.34	8	1.18	.01	.03	1	2
L0+00N 6+50E	1	139	11	102	.3	70	28	635	8.83	56	5	ND	3	8	1	2	2	219	.60	.041	5	105	.98	52	.32	6	5.45	.01	.03	1	3
L0+00N 6+75E	1	102	15	81	.1	41	14	295	9.45	71	5	ND	2	7	1	2	2	219	.52	.043	2	88	.50	28	.18	4	3.75	.01	.03	1	1
L0+00N 7+25E	1	56	14	80	.3	36	15	333	6.27	39	5	ND	2	15	1	2	2	160	.74	.030	4	61	.41	32	.17	6	2.84	.01	.03	1	2
L0+00N 7+50E	1	33	5	64	.4	24	12	349	5.90	27	5	ND	3	13	1	2	3	152	.69	.036	4	51	.29	22	.25	6	2.08	.01	.04	1	2
L0+00N 7+75E	1	75	15	128	.3	60	25	1049	7.28	66	5	ND	2	11	1	2	2	172	.52	.046	4	66	.38	34	.11	7	2.60	.01	.03	1	1
L0+00N 8+00E	1	121	6	127	.3	67	26	546	8.44	54	5	ND	2	9	1	4	2	194	.48	.041	4	105	.65	54	.21	5	5.18	.01	.04	1	1
L0+00N 8+25E	1	103	4	105	.3	42	16	401	8.69	55	5	ND	3	8	1	2	2	212	.46	.064	2	81	.49	29	.26	6	4.30	.01	.03	1	1
L0+00N 8+50E	1	124	7	139	.4	71	28	383	8.33	54	5	ND	2	9	1	2	2	177	.42	.036	5	91	.69	67	.19	3	5.11	.01	.04	1	2
L0+00N 8+75E	1	106	12	164	.6	75	33	3984	5.12	56	5	ND	2	20	1	6	2	183	.56	.068	8	106	.56	100	.24	4	5.69	.01	.06	2	1
L0+00N 9+00E	1	48	8	97	.2	37	17	798	5.69	38	5	ND	2	14	1	2	2	126	.62	.033	5	57	.44	48	.15	6	2.66	.01	.03	1	2
STD C/AU-S	19	60	39	132	6.8	70	30	1027	4.19	43	22	8	39	49	19	20	21	61	.49	.092	40	55	.50	181	.07	34	1.98	.06	.15	12	46

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Soil -80 Mesh AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: OCT 7 1988 DATE REPORT MAILED: Oct 18/88 SIGNED BY. . . . . D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-5079 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L28N 5+50W	1	82	23	69	.1	30	12	311	8.26	27	5	ND	2	6	1	6	2	181	.33	.061	5	82	.52	51	.18	2	5.10	.01	.02	1	6
L28N 5+25W	1	72	19	64	.1	29	11	258	7.16	24	5	ND	2	6	1	8	2	153	.34	.035	4	85	.48	29	.16	2	5.26	.01	.02	2	7
L28N 5+00W	1	84	19	77	.2	28	12	322	8.98	22	5	ND	2	6	1	9	3	187	.40	.069	4	94	.49	21	.28	2	5.38	.01	.02	1	2
L28N 4+75W	1	90	14	82	.1	35	15	946	8.19	26	5	ND	2	6	1	8	4	164	.43	.047	3	81	.66	20	.25	3	4.01	.01	.03	1	5
L28N 4+50W	1	56	20	56	.5	14	6	229	11.21	18	5	ND	3	6	1	5	2	259	.31	.043	4	79	.22	20	.41	2	3.38	.01	.02	1	3
L28N 4+25W	1	64	14	77	.1	34	14	454	7.43	16	5	ND	2	6	1	5	2	159	.48	.036	4	74	.80	29	.23	3	3.28	.01	.03	1	9
L28N 4+00W	1	46	5	62	.4	13	6	272	9.12	20	5	ND	2	6	1	3	2	215	.26	.050	3	76	.23	18	.23	2	3.05	.01	.02	1	7
L28N 3+75W	1	74	12	104	.3	44	17	532	7.00	28	5	ND	2	9	1	6	3	149	.67	.043	5	93	.90	33	.33	6	4.16	.01	.03	1	5
L28N 3+50W	1	65	12	70	.2	22	10	305	8.54	24	5	ND	2	7	1	2	2	212	.32	.042	5	76	.40	23	.22	2	3.82	.01	.02	1	4
L28N 3+25W	1	55	14	108	.1	33	29	6188	6.54	19	5	ND	1	16	1	5	2	142	.63	.043	5	90	.64	58	.16	3	3.52	.01	.04	1	6
L28N 2+75W	1	29	8	66	.3	9	5	219	9.00	19	5	ND	2	12	1	2	2	215	.35	.046	4	67	.15	17	.26	2	1.91	.01	.02	1	6
L28N 2+50W	1	41	18	74	.1	14	7	270	10.50	30	5	ND	2	11	1	5	2	271	.36	.078	4	67	.23	30	.19	2	2.70	.01	.03	1	1
L28N 2+00W	1	308	11	55	.1	24	8	250	6.98	21	5	ND	2	7	1	6	3	173	.43	.032	3	75	.37	20	.19	2	3.67	.01	.03	1	4
L28N 1+75W	1	112	17	74	.2	38	14	282	6.42	25	5	ND	2	6	1	3	2	143	.37	.032	4	85	.56	32	.15	2	5.80	.01	.03	1	4
L28N 1+50W	1	93	25	66	.2	23	10	311	8.54	26	5	ND	3	5	1	8	4	206	.27	.057	4	87	.37	20	.25	4	5.01	.01	.03	1	8
L28N 1+25W	1	66	11	63	.6	15	6	485	14.21	28	5	ND	3	7	1	9	2	266	.39	.077	3	112	.26	19	.37	4	4.74	.01	.04	1	6
L28N 1+00W	1	86	10	75	.2	41	17	400	6.49	21	5	ND	2	7	1	2	3	148	.45	.032	5	74	.70	37	.17	3	4.20	.01	.03	1	1
L28N 0+25W	1	39	10	37	.2	10	4	146	9.01	17	5	ND	2	6	1	2	3	216	.16	.048	3	63	.15	12	.26	2	3.11	.01	.02	2	1
L28N 0+00BL	1	79	23	80	.2	26	10	943	6.59	24	5	ND	1	9	1	2	2	171	.30	.052	4	72	.34	38	.19	2	3.70	.01	.03	1	5
L28N 0+25E	1	78	17	59	.1	27	9	256	6.75	20	5	ND	2	6	1	2	2	162	.30	.041	4	75	.38	30	.19	2	4.55	.01	.02	1	7
L28N 0+50E	1	64	13	55	.3	23	8	210	5.97	17	5	ND	2	6	1	6	2	164	.31	.034	4	66	.39	29	.24	3	3.51	.01	.02	1	5
L28N 0+75E	1	15	9	20	.1	6	2	113	6.21	9	5	ND	2	4	1	2	2	234	.12	.015	4	48	.05	8	.31	5	1.17	.01	.01	1	4
L28N 1+00E	1	71	18	50	.1	25	11	362	6.01	20	5	ND	1	10	1	2	2	167	.40	.021	4	62	.40	34	.22	2	3.42	.01	.02	1	52
L28N 1+25E	1	41	12	39	.1	16	5	163	7.13	13	5	ND	2	8	1	2	2	191	.34	.016	3	54	.23	21	.30	2	2.98	.01	.03	1	7
L28N 1+50E	1	81	19	61	.1	31	10	228	4.66	21	5	ND	2	5	1	2	3	102	.28	.021	3	54	.45	39	.13	2	4.67	.01	.03	1	19
L28N 1+75E	1	47	17	47	.2	15	8	189	5.55	17	5	ND	1	7	1	5	3	133	.25	.041	6	38	.20	30	.09	3	3.25	.01	.03	1	40
L28N 2+00E	1	22	7	27	.2	8	4	145	2.73	11	5	ND	2	5	1	2	2	91	.19	.014	5	23	.12	20	.11	9	1.66	.01	.03	2	12
L28N 2+25E	1	58	12	43	.2	17	6	161	7.95	22	5	ND	2	4	1	3	2	164	.18	.064	3	63	.25	24	.20	2	3.43	.01	.02	1	5
L28N 2+50E	1	109	30	65	.3	33	14	325	9.17	35	6	ND	3	6	1	11	2	174	.17	.042	4	91	.45	61	.13	3	6.09	.01	.05	1	7
L28N 2+75E	1	74	21	66	.2	24	9	237	7.43	23	5	ND	2	6	1	6	3	153	.32	.047	4	77	.36	23	.18	2	4.55	.01	.03	1	22
L28N 3+00E	1	29	8	42	.2	11	4	166	10.55	20	5	ND	3	5	1	2	3	260	.19	.046	3	68	.15	13	.35	2	2.01	.01	.02	1	5
L26N 5+50W	1	94	23	76	.1	32	11	277	7.54	32	5	ND	2	6	1	7	2	143	.36	.064	4	94	.57	28	.15	5	5.92	.01	.03	1	1
L26N 5+25W	1	58	29	65	.1	20	8	336	5.97	21	5	ND	1	10	1	6	3	158	.33	.052	3	58	.31	29	.17	3	3.07	.01	.03	1	1
L26N 5+00W	1	65	12	78	.4	25	11	302	8.22	20	5	ND	2	12	1	11	2	177	.40	.052	5	80	.26	41	.20	5	4.34	.01	.04	1	1
L26N 4+75W	1	109	21	76	.1	41	16	413	7.46	26	5	ND	2	7	1	8	2	144	.39	.084	5	93	.87	43	.15	5	6.07	.01	.03	1	8
L26N 4+50W	1	81	25	78	.2	28	13	499	8.09	26	5	ND	2	7	1	5	3	167	.33	.075	4	84	.47	24	.15	3	5.40	.01	.03	1	4
STD C/AU-S	18	57	36	132	7.1	67	28	1057	4.01	38	22	7	36	47	16	20	18	56	.48	.091	38	57	.88	172	.07	37	1.92	.06	.14	13	59

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5079

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L26N 4+25W	1	93	13	83	.3	26	16	827	6.14	71	5	ND	2	7	2	2	2	144	.27	.051	4	66	.42	24	.20	2	5.58	.01	.03	1	2
L26N 4+00W	1	45	31	63	.7	14	6	712	12.50	70	5	ND	3	8	1	3	2	259	.29	.084	4	90	.22	22	.40	2	4.22	.01	.03	1	1
L26N 3+75W	1	61	17	67	.4	16	13	1751	9.46	66	5	ND	2	9	1	3	2	223	.38	.083	5	80	.31	30	.33	2	3.82	.01	.06	2	33
L26N 3+50W	1	85	21	75	.3	26	14	429	7.59	49	5	ND	2	6	1	2	2	197	.26	.051	4	76	.38	22	.27	2	5.43	.01	.02	1	3
L26N 3+25W	2	101	21	89	.5	38	19	1034	6.86	63	5	ND	1	8	1	4	2	150	.37	.112	7	82	.64	32	.21	3	6.39	.01	.04	1	1
L26N 3+00W	1	130	14	85	.2	46	20	860	6.56	42	5	ND	1	11	1	2	2	158	.67	.049	6	73	.88	46	.24	4	4.67	.01	.04	1	15
L26N 2+75W	1	79	16	80	.4	31	15	598	6.66	39	5	ND	2	7	1	2	2	168	.40	.045	6	71	.52	32	.24	2	4.28	.01	.03	1	7
L26N 2+50W	1	114	10	95	.3	49	24	481	6.91	39	5	ND	2	6	1	3	2	145	.39	.038	4	92	.81	37	.19	2	5.98	.01	.03	1	8
L26N 2+25W	1	41	15	49	.5	13	7	237	7.71	29	5	ND	2	8	2	2	2	239	.33	.032	6	55	.25	20	.32	4	2.41	.01	.03	2	18
L26N 2+00W	1	81	11	78	.4	30	16	349	8.73	42	5	ND	2	6	2	2	2	191	.33	.061	7	91	.48	33	.21	2	5.91	.01	.03	1	13
L26N 1+75W	1	75	14	85	.3	39	16	372	6.14	33	5	ND	2	7	1	2	2	148	.45	.041	6	74	.69	36	.17	2	4.84	.01	.03	1	9
L26N 1+50W	1	102	19	86	.3	49	19	446	6.41	33	5	ND	2	6	1	2	2	133	.44	.043	8	80	.97	44	.19	6	5.42	.01	.03	1	58
L26N 1+25W	1	49	12	54	.3	18	8	237	7.65	31	5	ND	1	7	1	2	2	234	.33	.032	7	60	.32	23	.31	2	2.95	.01	.02	1	20
L26N 1+00W	1	47	5	55	.3	17	9	257	7.96	34	5	ND	1	11	1	3	2	195	.50	.039	5	60	.40	27	.19	2	2.98	.01	.03	1	1
L26N 0+75W	1	60	20	66	.5	25	10	336	9.81	34	5	ND	2	8	1	2	2	210	.36	.038	4	88	.50	24	.25	2	3.66	.01	.03	1	1
L26N 0+50W	1	84	9	62	.3	31	11	219	7.77	122	5	ND	2	6	1	2	2	180	.34	.042	4	87	.49	26	.24	2	5.33	.01	.03	1	1
L26N 0+25W	1	32	9	38	.5	6	3	81	9.05	96	5	ND	2	4	1	4	2	264	.11	.036	4	66	.09	9	.42	2	2.02	.01	.02	3	3
L26N 0+00BL	1	48	9	50	.4	13	6	151	10.66	42	5	ND	2	6	1	2	3	216	.25	.054	3	80	.28	15	.40	2	3.45	.01	.02	1	5
L26N 0+25E	1	69	7	70	.7	29	12	225	8.63	21	5	ND	2	4	1	2	2	184	.24	.046	4	89	.46	25	.20	2	5.66	.01	.02	1	2
L26N 0+50E	1	45	13	40	.1	13	5	143	6.27	15	5	ND	1	7	1	2	2	181	.19	.041	4	50	.22	18	.21	2	2.63	.01	.04	1	4
L26N 0+75E	1	56	3	66	.5	18	8	205	8.70	25	5	ND	2	5	2	3	2	201	.29	.044	4	82	.33	17	.28	2	4.36	.01	.03	1	2
L26N 1+00E	1	40	44	124	.7	22	206	21225	7.22	35	5	ND	1	22	2	2	2	117	.51	.129	6	50	.13	100	.03	2	4.46	.01	.05	1	1
L26N 1+25E	2	42	9	53	.2	13	23	1922	6.75	35	5	ND	2	6	3	2	2	156	.21	.043	3	40	.20	26	.13	4	3.16	.01	.04	1	16
L26N 1+50E	2	27	16	81	.2	10	9	1329	4.10	18	5	ND	2	10	1	2	2	69	.21	.048	4	31	.09	84	.01	2	3.22	.01	.05	1	1
L26N 1+75E	1	42	16	74	.2	15	14	1675	5.43	31	5	ND	1	13	1	3	2	121	.39	.047	4	34	.20	47	.05	2	2.65	.01	.05	1	1
L26N 2+00E	1	46	12	47	.4	9	5	183	6.99	27	5	ND	2	5	1	2	2	222	.21	.041	3	34	.12	16	.21	2	1.87	.01	.03	1	1
L26N 2+25E	1	27	8	41	.3	8	4	189	6.35	17	5	ND	2	5	2	2	2	218	.16	.023	4	38	.09	18	.24	2	1.54	.01	.03	1	8
L26N 2+50E	1	28	14	46	.4	7	3	130	7.66	29	5	ND	2	7	2	2	2	208	.24	.047	3	40	.10	15	.33	3	1.86	.01	.02	1	1
L26N 2+75E	1	39	8	62	.4	10	6	154	6.48	18	5	ND	2	4	1	2	2	175	.13	.035	3	40	.07	23	.11	2	2.09	.01	.03	1	1
L26N 3+00E	1	39	7	52	.4	14	6	143	8.47	39	5	ND	3	5	1	2	2	164	.21	.043	3	70	.22	16	.24	2	6.28	.01	.03	1	5
L24N 5+50W	1	127	15	86	.2	35	13	323	8.36	35	5	ND	2	6	1	4	2	199	.43	.054	4	78	.63	27	.28	2	5.12	.01	.03	1	3
L24N 5+25W	1	71	20	70	.3	22	11	257	7.76	21	5	ND	2	7	2	5	2	198	.34	.037	5	68	.35	21	.27	2	3.96	.01	.02	1	4
L24N 5+00W	1	124	11	87	.2	45	17	328	6.89	32	5	ND	2	6	1	4	2	152	.50	.032	4	79	.87	27	.29	4	5.57	.01	.03	1	2
L24N 4+75W	1	93	13	63	.4	26	9	221	9.10	30	5	ND	3	6	1	6	2	205	.38	.037	4	85	.53	24	.31	5	4.50	.01	.02	1	1
L24N 4+50W	1	101	21	85	.5	35	13	363	8.03	35	5	ND	3	7	1	6	2	180	.46	.050	4	90	.63	26	.26	4	5.47	.01	.04	1	1
L24N 4+25W	1	72	17	94	.2	31	12	450	7.85	29	5	ND	1	7	1	2	2	197	.38	.081	5	80	.48	32	.22	2	4.42	.01	.03	1	5
STD C/AU-S	18	58	43	132	7.1	68	29	1016	3.94	42	22	7	36	45	18	17	22	56	.48	.092	38	55	.89	174	.07	35	1.90	.06	.14	13	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L24N 4+00W	1	98	20	91	.4	39	16	272	7.77	128	5	ND	2	5	2	11	2	152	.28	.038	5	87	.46	48	.04	4	4.29	.01	.04	2	6
L24N 3+75W	1	121	23	99	.2	52	23	610	7.46	74	5	ND	1	7	1	4	2	156	.49	.035	6	90	.80	50	.15	2	4.43	.01	.03	1	4
L24N 3+25W	1	58	22	54	.3	16	6	137	16.37	53	5	ND	2	5	1	2	2	216	.24	.043	5	93	.25	16	.17	2	3.33	.01	.02	1	1
L24N 3+00W	1	130	24	87	.3	41	18	397	7.66	37	5	ND	2	7	1	10	2	191	.38	.045	5	82	.78	42	.30	2	4.66	.01	.03	2	46
L24N 2+75W	1	89	25	82	.3	27	9	240	8.66	26	5	ND	2	6	1	5	2	186	.35	.042	3	103	.43	26	.29	2	6.08	.01	.02	1	8
L24N 2+50W	1	138	22	93	.1	51	21	444	7.31	29	5	ND	2	7	1	2	2	170	.44	.030	4	98	.98	35	.24	2	5.27	.01	.03	1	3
L24N 2+25W	1	129	28	91	.3	48	21	527	7.37	29	5	ND	2	8	1	3	2	167	.48	.032	3	97	.98	29	.23	2	5.29	.01	.03	1	4
L24N 2+00W	1	53	20	54	.3	13	5	161	8.97	24	5	ND	1	8	1	2	2	254	.28	.052	3	79	.21	16	.42	2	2.92	.01	.02	1	6
L24N 1+75W	1	62	25	50	.5	13	6	165	10.32	34	5	ND	3	7	2	4	3	262	.28	.055	3	93	.24	16	.41	2	3.41	.01	.02	2	3
L24N 1+50W	1	36	23	53	.3	26	10	201	4.37	17	5	ND	2	10	1	3	2	133	.47	.008	4	64	.63	34	.20	4	3.19	.01	.02	1	1
L24N 1+25W	1	67	27	50	.2	18	6	162	9.92	30	5	ND	3	4	1	2	4	247	.21	.042	3	109	.30	16	.42	2	5.31	.01	.02	1	6
L24N 1+00W	1	84	19	58	.2	23	9	172	6.27	35	5	ND	2	6	1	5	2	173	.26	.038	4	73	.35	20	.23	2	4.77	.01	.02	2	3
L24N 0+75W	1	80	27	55	.2	24	9	166	6.00	41	5	ND	2	5	1	4	2	171	.25	.037	4	72	.34	20	.23	2	4.68	.01	.02	3	7
L24N 0+50W	1	70	29	55	.4	18	6	167	11.67	46	5	ND	3	4	1	6	2	185	.20	.063	3	142	.31	17	.36	2	6.49	.01	.02	1	1
L24N 0+25W	1	56	17	50	.4	10	5	131	15.00	40	5	ND	3	3	1	3	2	254	.15	.053	3	115	.19	13	.47	2	3.88	.01	.02	1	3
L24N 0+00BL	1	93	18	107	.3	35	13	276	6.51	44	5	ND	2	6	1	6	2	148	.35	.032	3	77	.60	28	.25	4	5.54	.01	.03	1	2
L24N 0+25E	1	88	24	119	.4	47	18	409	7.40	22	5	ND	2	8	1	3	4	174	.54	.037	5	95	.72	39	.30	2	4.88	.01	.03	1	5
L24N 0+50E	1	67	16	62	.1	23	10	250	6.07	25	5	ND	2	6	1	2	2	159	.20	.039	4	60	.43	40	.12	2	3.53	.01	.02	1	24
L24N 0+75E	1	52	10	73	.1	25	14	344	6.48	28	5	ND	2	6	1	2	2	147	.33	.048	4	62	.42	49	.08	2	3.84	.01	.03	1	1
L24N 1+00E	1	42	11	56	.2	17	9	214	6.48	22	5	ND	2	5	2	2	2	185	.24	.039	4	56	.26	34	.13	2	3.18	.01	.03	1	2
L24N 1+25E	1	32	12	53	.3	12	6	155	7.52	22	5	ND	1	7	1	3	2	175	.29	.046	3	54	.20	26	.19	2	2.18	.01	.02	1	4
L24N 1+50E	1	67	13	107	.1	46	17	1391	5.87	22	5	ND	2	9	1	2	2	113	.51	.036	5	69	.78	47	.14	4	3.23	.01	.04	1	6
L24N 1+75E	1	49	24	92	.2	33	24	720	6.45	20	5	ND	2	7	1	3	2	135	.33	.027	5	65	.37	57	.13	2	3.38	.01	.03	1	2
L24N 2+00E	1	80	10	97	.2	30	11	262	6.80	48	5	ND	1	6	1	2	2	147	.33	.038	3	79	.48	26	.25	2	5.59	.01	.02	1	1
L22N 5+50W	1	102	30	81	.2	34	14	786	7.49	28	5	ND	1	8	1	2	2	185	.52	.078	4	74	.69	27	.27	2	4.20	.01	.03	1	3
L22N 5+25W	1	155	27	105	.4	44	18	751	8.36	27	5	ND	3	8	1	12	2	184	.56	.062	3	96	.80	26	.31	2	6.05	.01	.04	1	4
L22N 5+00W	1	111	23	106	.4	47	18	406	8.55	27	5	ND	2	8	1	4	8	192	.50	.045	5	92	.84	44	.29	2	5.22	.01	.03	1	1
L22N 4+75W	1	93	18	100	.4	30	11	279	10.29	30	5	ND	2	7	1	4	3	212	.33	.052	4	90	.61	39	.27	2	5.08	.01	.03	1	2
L22N 4+25W	1	45	13	46	.3	13	5	130	6.31	18	5	ND	1	6	1	2	4	179	.29	.050	4	49	.22	16	.26	2	2.47	.01	.02	2	10
L22N 4+00W	1	94	13	89	.2	29	13	284	8.27	19	5	ND	2	8	1	2	2	183	.37	.030	6	80	.55	38	.20	2	4.59	.01	.04	1	1
L22N 3+75W	1	22	12	32	.2	7	3	86	4.70	6	5	ND	1	5	1	2	2	173	.20	.010	5	37	.12	14	.27	2	1.64	.01	.02	2	7
L22N 3+50W	1	79	15	80	.3	30	14	246	7.72	24	5	ND	2	9	1	4	2	207	.46	.027	5	69	.50	38	.23	2	3.99	.01	.03	1	13
L22N 2+00W	1	79	23	65	.4	18	8	225	14.00	34	5	ND	3	6	1	6	2	258	.30	.069	4	116	.38	17	.30	2	4.91	.01	.03	1	9
L22N 1+75W	1	83	20	62	.2	19	7	194	12.57	33	5	ND	3	5	1	2	2	243	.21	.066	4	112	.34	18	.27	2	5.43	.01	.03	1	3
L22N 1+50W	1	115	9	91	.2	37	14	239	7.18	46	5	ND	2	5	1	3	3	144	.27	.060	5	84	.51	31	.07	2	5.42	.01	.03	1	1
L22N 1+25W	1	118	17	101	.1	37	14	236	7.63	50	5	ND	2	5	1	2	2	153	.27	.077	5	84	.49	33	.07	2	5.58	.01	.03	1	1
STD C/AU-S	18	57	43	132	6.6	68	29	1059	4.02	40	23	8	36	47	20	18	20	57	.49	.092	38	58	.90	175	.07	39	1.93	.06	.15	11	48

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5079

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L22N 1+00W	1	146	21	86	.1	42	16	353	7.74	38	5	ND	1	5	1	3	2	154	.33	.039	4	97	.90	35	.18	2	6.45	.01	.03	1	8
L22N 0+75W	1	110	6	129	.2	56	33	2610	6.72	45	5	ND	2	7	2	2	2	127	.37	.039	6	71	.72	53	.11	7	4.17	.01	.05	1	11
L22N 0+	1	63	8	117	.1	38	17	328	8.07	36	5	ND	2	7	1	2	3	132	.26	.035	3	55	.31	45	.02	2	3.76	.01	.04	1	1
L22N 0+[illegible]	1	103	10	138	.2	56	22	504	6.98	43	5	ND	1	6	1	1	2	135	.33	.033	5	74	.73	46	.11	2	4.64	.01	.04	1	59
L22N 0+25E	1	51	17	73	.1	19	12	453	7.51	37	5	ND	2	5	1	2	2	167	.19	.040	5	64	.28	33	.08	2	3.53	.01	.02	2	1
L22N 0+50E	1	96	14	80	.1	38	16	369	6.27	31	5	ND	1	5	1	2	3	126	.33	.039	4	84	.65	37	.10	2	5.51	.01	.02	1	7
L22N 0+75E	1	75	5	105	.1	46	24	13515	6.42	28	5	ND	1	10	1	2	2	133	.51	.049	5	71	.72	125	.10	2	4.29	.01	.04	1	5
L22N 1+00E	1	105	12	87	.2	42	17	459	6.31	40	5	ND	1	6	1	2	3	127	.44	.034	4	78	.71	35	.12	4	4.89	.01	.02	1	4
L22N 1+25E	1	42	9	59	.1	14	7	256	6.95	22	5	ND	1	4	1	2	2	183	.20	.039	4	66	.17	15	.14	2	3.69	.01	.01	2	1
L22N 1+50E	1	100	17	112	.2	48	19	384	7.52	39	5	ND	1	6	1	2	4	158	.36	.043	4	83	.67	58	.16	2	4.94	.01	.03	1	8
L22N 1+75E	1	117	5	99	.1	44	18	319	6.90	43	5	ND	1	6	1	2	4	133	.44	.035	4	80	.75	35	.13	2	5.06	.01	.02	1	17
L22N 2+00E	1	63	8	65	.1	18	9	184	7.61	26	5	ND	1	4	1	2	3	190	.20	.038	5	62	.24	29	.12	2	3.47	.01	.02	1	6
L20+00N 5+50W	1	67	18	51	.3	19	10	230	8.23	44	5	ND	2	4	2	252	2	222	.19	.041	3	40	.13	10	.17	3	1.36	.01	.02	4	3
L20+00N 5+25W	1	65	6	55	.3	21	10	231	7.11	20	5	ND	1	6	1	19	3	205	.33	.039	5	59	.39	23	.32	2	2.73	.01	.02	1	4
L20+00N 5+00W	1	112	23	100	.3	42	17	468	8.04	31	5	ND	2	8	1	14	13	184	.45	.049	4	83	.73	29	.29	3	5.40	.01	.04	1	18
L20+00N 4+75W	1	48	16	59	.3	17	8	184	6.97	25	5	ND	1	8	1	29	2	185	.44	.015	5	47	.31	19	.17	2	2.05	.01	.02	1	8
L20+00N 4+50W	1	116	12	102	.2	34	13	290	8.56	27	5	ND	1	6	1	6	3	188	.35	.048	4	80	.61	32	.23	2	4.95	.01	.03	1	5
L20+00N 4+25W	1	109	16	81	.3	30	18	674	7.77	47	5	ND	1	8	1	17	3	191	.45	.044	4	58	.59	22	.21	2	2.70	.01	.03	1	10
L20+00N 4+00W	1	221	15	101	.3	44	26	665	9.26	84	5	ND	2	6	1	41	2	184	.37	.066	5	67	.69	30	.11	2	3.96	.01	.04	1	12
L20+00N 3+75W	1	135	17	66	.1	21	9	209	8.23	27	5	ND	2	5	1	6	2	170	.26	.115	3	84	.32	23	.20	2	7.09	.01	.02	1	16
L20+00N 3+50W	1	90	18	78	.2	23	11	209	9.00	26	5	ND	2	5	1	12	2	219	.28	.077	5	73	.39	30	.23	2	4.87	.01	.03	1	6
L20+00N 3+25W	1	66	18	63	.2	20	9	300	8.20	20	5	ND	2	6	1	3	3	207	.30	.045	4	70	.37	24	.25	2	3.93	.01	.02	1	3
L20+00N 3+00W	1	56	21	56	.2	16	9	266	7.88	23	5	ND	1	8	1	4	2	242	.34	.042	4	55	.30	19	.39	2	2.71	.01	.02	1	6
L20+00N 2+75W	1	56	18	71	.2	14	7	269	10.10	28	5	ND	2	6	1	2	2	243	.22	.036	4	68	.26	26	.38	2	2.94	.01	.02	1	5
L20+00N 0+75W	1	112	20	87	.3	36	12	261	8.04	43	5	ND	2	6	1	13	2	163	.34	.051	3	90	.53	24	.19	3	4.98	.01	.03	1	6
L20+00N 0+50W	1	48	18	152	.2	30	16	309	6.59	29	5	ND	2	5	1	2	2	116	.19	.036	3	51	.34	71	.01	2	4.84	.01	.05	1	1
L20+00N 0+25W	1	26	7	51	.1	9	7	168	5.58	24	5	ND	1	3	1	2	2	92	.10	.021	7	23	.12	24	.01	2	2.18	.01	.03	1	2
L20+00N 0+00BL	1	68	15	80	.1	24	14	210	5.58	31	5	ND	2	3	1	3	2	98	.18	.022	2	39	.35	44	.01	4	2.83	.01	.05	1	5
L20+00N 0+25E	1	72	20	67	.1	20	8	680	6.61	37	5	ND	1	6	1	3	2	151	.24	.049	3	58	.28	26	.09	2	3.14	.01	.02	1	4
L20+00N 0+50E	1	36	12	53	.2	11	6	167	7.99	29	5	ND	1	4	1	3	2	182	.16	.039	3	48	.16	17	.08	2	2.16	.01	.02	1	4
L20+00N 0+75E	1	29	7	49	.1	8	5	113	4.76	22	5	ND	1	5	1	2	5	125	.13	.020	3	25	.08	19	.04	6	1.47	.01	.03	1	3
L20+00N 1+00E	1	8	2	51	.1	7	5	63	1.75	26	5	ND	1	2	1	2	2	67	.02	.011	2	3	.02	15	.01	8	.83	.01	.03	1	1
L20+00N 1+50E	1	25	4	56	.2	10	6	84	3.08	33	5	ND	1	2	1	2	3	61	.04	.014	2	14	.06	19	.01	9	1.34	.01	.03	1	1
L20+00N 1+75E	2	41	7	76	.3	13	8	204	5.77	47	5	ND	1	3	1	3	4	104	.07	.028	2	24	.08	30	.01	3	2.05	.01	.03	1	1
L20+00N 2+00E	1	29	3	74	.1	14	9	207	5.80	52	5	ND	1	3	1	2	4	138	.11	.021	2	26	.11	20	.03	4	1.62	.01	.02	1	2
L18+00N 5+50W	1	167	21	101	.1	53	25	1119	9.53	33	5	ND	1	10	1	2	2	226	.63	.076	3	86	1.31	38	.42	2	5.20	.01	.03	1	7
STD C/AU-S	18	58	38	132	7.1	67	29	1019	4.04	38	17	7	36	47	18	20	19	57	.48	.093	38	55	.89	173	.07	37	1.92	.06	.15	11	47

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5079

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L18+00N 5+25W	1	87	9	60	.1	17	8	300	10.03	37	5	ND	2	5	1	140	2	263	.23	.057	3	55	.18	13	.27	2	1.68	.01	.02	1	3
L18+00N 5+00W	1	201	21	106	.6	46	18	473	7.13	24	5	ND	2	9	1	17	5	182	.59	.044	5	77	.88	31	.38	2	4.32	.01	.03	1	3
L18+00N 4+75W	1	192	13	102	.1	45	21	917	10.49	227	5	ND	2	7	1	92	2	163	.37	.047	5	57	.31	22	.01	2	2.40	.01	.05	1	5
L18+00N 4+50W	1	114	34	77	.1	19	4	2082	.68	11	5	ND	1	26	4	2	2	17	1.83	.149	24	32	.08	32	.01	10	3.89	.01	.05	1	1
L18+00N 4+25W	1	143	24	151	.1	49	28	6066	5.48	22	5	ND	1	19	1	2	2	116	1.24	.072	12	85	.56	51	.24	2	6.85	.01	.04	1	1
L18+00N 4+00W	1	41	25	79	.1	17	9	465	7.70	33	5	ND	2	11	1	17	2	226	.68	.043	6	51	.30	30	.23	2	1.93	.01	.03	1	2
L18+00N 3+75W	1	141	8	110	.1	43	19	434	8.87	38	5	ND	2	8	1	4	2	225	.43	.041	3	92	.86	33	.43	2	5.45	.01	.03	1	4
L18+00N 3+50W	1	96	12	74	.1	24	10	411	8.06	37	5	ND	2	9	1	7	2	230	.51	.041	3	67	.50	21	.42	2	3.38	.01	.03	1	5
L18+00N 3+25W	1	104	13	87	.1	34	14	402	7.70	45	5	ND	2	8	1	2	2	205	.48	.040	3	78	.74	24	.45	2	4.46	.01	.02	1	16
L18+00N 3+00W	1	108	19	87	.1	30	11	286	9.58	47	5	ND	2	7	1	2	2	228	.36	.044	3	107	.55	23	.50	2	6.30	.01	.02	1	2
L18+00N 2+75W	1	37	15	52	.2	12	5	165	8.27	47	5	ND	2	7	1	3	2	278	.29	.030	3	60	.27	16	.57	2	2.32	.01	.02	1	21
L18+00N 2+50W	1	85	16	71	.1	19	8	205	9.99	42	5	ND	2	6	1	2	3	256	.20	.037	4	73	.36	19	.42	2	3.75	.01	.02	1	2
L18+00N 2+00W	1	89	16	76	.1	19	9	222	9.77	43	5	ND	3	6	1	2	2	249	.20	.037	4	72	.39	21	.41	2	3.84	.01	.02	1	1
L18+00N 1+75W	1	73	12	64	.2	16	8	178	9.73	33	5	ND	3	6	1	4	2	251	.23	.027	4	70	.30	16	.43	2	3.08	.01	.02	1	7
L18+00N 1+50W	1	29	13	48	.2	11	5	140	6.71	24	5	ND	2	7	1	2	2	183	.30	.036	3	46	.25	14	.25	2	1.93	.01	.02	1	15
L18+00N 1+25W	1	20	13	41	.1	9	4	112	5.68	17	5	ND	2	7	1	2	2	176	.27	.021	4	38	.17	15	.23	2	1.60	.01	.02	1	1
L18+00N 1+00W	1	98	18	96	.3	32	11	294	7.86	29	5	ND	3	7	2	2	2	156	.37	.054	4	72	.64	35	.16	3	4.19	.01	.03	1	1
L18+00N 0+75W	1	13	13	59	.1	7	4	160	1.96	26	5	ND	2	3	2	2	2	41	.17	.017	2	7	.06	29	.01	10	1.48	.01	.04	1	1
L18+00N 0+50W	1	40	22	83	.4	18	31	1465	6.64	28	5	ND	2	17	1	2	2	161	.53	.035	5	54	.31	64	.17	3	2.78	.01	.03	1	1
L18+00N 0+25W	3	27	6	41	.2	5	4	139	5.79	27	5	ND	2	7	1	8	3	120	.19	.023	3	23	.19	26	.05	4	1.53	.01	.04	2	1
L18+00N 0+00BL	1	27	27	108	1.2	13	777	47255	19.02	43	5	ND	4	8	1	2	2	118	.13	.468	4	72	.01	648	.03	4	3.96	.01	.04	1	4
L18+00N 0+25E	1	113	7	77	.3	38	14	352	7.02	24	5	ND	3	5	2	2	5	134	.34	.034	3	98	.57	21	.11	2	5.53	.01	.03	2	1
L18+00N 0+50E	1	26	6	58	.1	8	7	245	5.30	23	5	ND	2	4	1	2	2	84	.08	.019	2	17	.07	23	.01	4	1.67	.01	.03	2	1
L18+00N 0+75E	1	41	10	46	.1	8	5	116	5.09	13	5	ND	2	3	1	2	2	109	.13	.035	4	40	.15	34	.01	3	3.51	.01	.03	1	1
L18+00N 1+00E	1	84	14	97	.1	31	13	566	7.31	21	5	ND	3	7	1	2	2	170	.31	.045	5	79	.50	44	.17	4	5.15	.02	.09	1	3
L18+00N 1+25E	1	44	31	67	.1	15	8	273	10.00	30	5	ND	2	7	1	2	2	192	.29	.051	3	55	.24	28	.19	2	2.72	.01	.04	1	1
L18+00N 1+50E	1	108	11	105	.3	54	16	349	8.09	27	5	ND	3	7	1	3	5	161	.40	.033	4	86	.83	46	.22	2	4.79	.01	.03	1	1
L18+00N 1+75E	1	29	25	61	.1	16	16	731	5.69	21	5	ND	2	10	1	2	2	138	.44	.021	4	45	.34	42	.06	2	2.39	.01	.04	1	1
L18+00N 2+00E	1	21	17	47	.1	10	12	657	5.64	22	5	ND	2	8	1	2	2	165	.32	.019	4	37	.16	34	.11	2	1.72	.01	.03	1	6
L16+00N 5+50W	1	133	23	102	.2	41	15	439	8.46	16	5	ND	2	8	1	2	2	215	.59	.064	3	95	.99	20	.49	2	5.22	.01	.03	1	1
L16+00N 5+25W	1	35	18	44	.2	11	6	489	7.46	7	5	ND	3	11	1	2	2	262	.39	.049	4	49	.29	15	.63	2	2.12	.01	.02	1	14
L16+00N 5+00W	1	102	18	86	.4	23	13	450	9.43	14	5	ND	3	8	1	2	2	231	.35	.065	4	63	.61	21	.28	2	3.80	.01	.03	1	19
L16+00N 4+75W	1	63	23	81	.4	20	9	377	9.26	17	5	ND	2	8	1	7	2	261	.49	.067	3	76	.41	20	.61	2	3.21	.01	.02	1	1
L16+00N 4+50W	1	65	19	63	.1	13	11	858	9.11	11	5	ND	2	8	1	2	3	244	.35	.089	4	57	.25	25	.45	2	2.40	.01	.03	1	6
L16+00N 4+25W	1	94	20	101	.3	29	16	551	11.94	18	5	ND	3	9	1	3	3	288	.44	.126	4	90	.66	30	.70	2	3.88	.01	.04	1	5
L16+00N 4+00W	1	68	22	88	.3	25	10	344	9.10	21	5	ND	2	11	1	8	2	256	.63	.051	3	81	.53	23	.64	2	3.50	.01	.04	1	1
STD C/AU-S	17	57	41	132	7.2	66	28	1033	3.91	36	20	8	37	47	18	18	21	56	.47	.089	38	56	.86	173	.07	36	1.90	.06	.15	11	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L16+00N 3+75W	1	115	11	96	.3	39	15	356	9.58	21	5	ND	1	10	1	2	2	230	.75	.058	3	88	.82	29	.52	2	5.08	.01	.03	1	4
L16+00N 3+50W	1	95	21	75	.1	42	16	295	9.56	17	5	ND	1	8	1	2	4	260	.68	.032	2	91	.94	20	.63	2	4.71	.01	.02	1	2
L16+00N 3+00W	1	138	10	99	.1	44	22	1492	7.36	39	5	ND	1	16	1	2	2	177	1.42	.041	7	72	1.20	43	.40	7	3.98	.01	.05	1	16
L16+00N 2+00W	1	71	8	50	.4	20	8	246	7.23	23	5	ND	1	6	1	3	2	232	.31	.036	3	57	.42	20	.42	4	3.58	.01	.02	1	7
L16+00N 1+75W	1	35	8	37	.2	10	5	188	4.02	16	5	ND	1	12	1	2	2	143	.45	.025	3	26	.23	16	.36	2	1.32	.01	.02	1	3
L16+00N 1+50W	1	120	14	69	.1	32	12	332	7.66	38	5	ND	1	8	1	2	2	176	.44	.045	2	76	.78	30	.42	2	5.62	.01	.02	1	7
L16+00N 1+25W	1	108	2	66	.1	32	13	288	6.97	19	5	ND	1	6	1	2	3	179	.42	.039	2	66	.74	25	.39	2	4.81	.01	.02	1	6
L16+00N 0+75W	1	114	19	69	.1	30	12	396	6.24	25	5	ND	1	7	1	2	2	147	.44	.067	3	56	.74	27	.31	2	4.79	.01	.02	1	5
L16+00N 0+50W	1	39	9	41	.1	11	4	190	6.74	11	5	ND	1	6	1	2	2	194	.26	.055	2	46	.19	14	.31	2	3.22	.01	.01	1	3
L16+00N 0+25W	1	80	9	66	.2	21	9	197	6.90	19	5	ND	1	6	1	2	3	175	.36	.041	3	69	.40	19	.34	2	4.43	.01	.02	1	1
L16+00N 0+00BL	1	102	14	67	.1	34	16	597	5.27	17	5	ND	1	9	1	2	2	150	.62	.039	3	57	.74	30	.36	3	3.90	.01	.02	1	4
L16+00N 0+25E	1	21	11	61	.1	7	5	203	3.74	6	5	ND	1	2	1	2	2	57	.11	.036	2	11	.11	22	.03	2	1.96	.01	.03	1	1
L16+00N 0+50E	1	18	7	33	.1	6	2	131	6.02	4	5	ND	1	3	1	2	8	188	.16	.025	2	34	.12	14	.35	2	1.64	.01	.01	1	2
L16+00N 0+75E	2	61	4	62	.1	26	9	246	5.58	2	5	ND	1	6	1	2	4	147	.41	.023	2	53	.56	22	.33	2	3.36	.01	.02	1	3
L16+00N 1+00E	1	58	11	65	.1	21	10	277	8.07	19	5	ND	2	5	1	3	2	189	.24	.035	4	61	.29	29	.13	4	3.49	.01	.02	1	1
L16+00N 1+25E	1	53	11	61	.1	16	8	235	7.39	24	5	ND	1	4	1	2	2	167	.18	.040	3	52	.23	25	.03	2	3.74	.01	.04	1	2
L16+00N 1+50E	1	44	5	53	.1	9	6	164	8.72	26	5	ND	1	5	1	2	2	195	.17	.036	3	53	.17	25	.14	2	2.39	.01	.02	1	2
L16+00N 2+50E	1	15	14	44	.1	11	21	735	2.88	9	5	ND	1	7	1	2	2	75	.27	.020	3	17	.17	58	.01	4	2.38	.01	.04	1	1
L14+00N 5+50W	1	183	15	139	1.2	48	22	442	10.06	53	5	ND	2	7	1	20	3	235	.47	.043	3	84	.65	28	.22	5	5.78	.01	.03	1	13
L14+00N 5+25W	1	188	6	81	.5	23	16	269	10.22	58	5	ND	1	4	1	8	2	251	.15	.034	3	47	.57	19	.03	2	3.84	.01	.02	2	5
L14+00N 5+00W	1	51	17	49	.4	12	5	184	9.08	14	5	ND	1	7	1	2	2	303	.37	.043	2	68	.25	10	.54	2	2.60	.01	.01	1	4
L14+00N 4+75W	1	119	19	82	.3	30	12	306	11.26	46	5	ND	2	7	1	14	2	263	.45	.059	2	87	.60	18	.43	6	4.72	.01	.03	1	6
L14+00N 4+50W	1	153	17	127	.3	36	16	346	10.18	40	5	ND	2	8	1	5	2	250	.49	.039	3	80	.68	26	.43	5	4.49	.01	.03	1	19
L14+00N 4+25W	1	193	4	96	.7	40	17	366	9.17	67	5	ND	2	10	1	20	3	219	.53	.036	3	74	.83	30	.28	7	4.60	.01	.03	1	6
L14+00N 4+00W	1	115	22	99	.5	30	12	295	9.55	31	5	ND	2	7	1	3	2	238	.42	.048	2	86	.55	25	.44	2	5.33	.01	.02	1	7
L14+00N 3+75W	1	142	12	135	.5	34	18	672	10.54	62	5	ND	2	6	1	22	2	237	.33	.077	3	74	.50	27	.19	5	4.42	.01	.04	1	2
L14+00N 3+50W	1	30	18	47	.2	12	7	372	9.01	17	5	ND	2	7	1	12	2	329	.33	.062	3	32	.27	13	.67	2	1.71	.01	.02	1	85
L14+00N 3+25W	2	204	20	283	.7	40	27	670	11.80	303	5	ND	2	10	1	24	3	195	.67	.048	5	50	.51	34	.04	4	4.30	.01	.04	1	76
L14+00N 3+00W	1	45	6	52	.1	10	7	281	6.74	21	5	ND	1	6	1	2	4	207	.28	.033	2	40	.20	18	.32	2	2.19	.01	.02	1	350
L14+00N 2+25W	1	63	13	77	.1	21	11	249	7.03	22	5	ND	2	5	1	2	2	159	.23	.052	4	53	.35	40	.10	2	3.71	.01	.03	1	12
L14+00N 1+75W	1	65	7	76	.1	20	10	270	7.26	21	5	ND	2	5	1	2	2	164	.23	.052	4	55	.35	41	.10	2	3.82	.01	.03	1	1
L14+00N 1+50W	1	110	25	86	.1	34	13	297	8.11	27	5	ND	2	6	1	2	4	192	.41	.049	2	84	.71	24	.40	4	5.52	.01	.02	1	5
L14+00N 1+25W	5	134	18	104	1.2	25	15	343	9.25	95	5	ND	2	7	1	26	2	209	.34	.037	4	52	.37	29	.14	7	3.53	.01	.04	1	5
L14+00N 1+00W	1	133	16	95	.4	39	18	453	7.03	25	5	ND	2	7	1	2	2	162	.48	.053	3	72	.97	22	.35	5	5.36	.01	.03	1	7
L14+00N 0+75W	1	102	18	94	.3	34	16	437	6.80	17	5	ND	2	7	1	2	2	164	.42	.046	3	66	.75	27	.36	4	4.73	.01	.02	1	4
L14+00N 0+50W	1	124	12	121	.1	42	19	330	6.03	24	5	ND	2	7	1	2	3	137	.32	.035	3	58	.75	39	.18	2	4.36	.01	.03	1	6
STD C/AU-S	18	57	40	131	7.1	68	28	1015	3.96	38	17	7	36	47	16	18	17	57	.49	.092	38	56	.91	173	.07	35	1.93	.06	.14	13	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L14+00N 0+25W	1	48	11	53	.1	11	7	263	8.77	20	5	ND	2	6	1	3	2	239	.30	.030	2	50	.22	17	.38	2	2.43	.01	.02	1	1
L14+00N 0+00BL	4	149	8	117	1.2	25	17	342	10.71	105	5	ND	2	8	2	33	2	235	.34	.041	4	59	.36	30	.11	2	3.81	.01	.03	2	8
L14+00N 0+25E	1	286	18	167	.3	62	43	1586	9.49	491	5	ND	2	14	2	42	2	161	1.08	.051	9	54	.97	74	.21	9	2.84	.01	.05	1	32
L14+00N 0+50E	1	59	13	67	.3	13	8	267	7.17	22	5	ND	2	5	1	2	2	143	.17	.049	2	39	.21	47	.02	2	2.91	.01	.04	1	1
L14+00N 0+75E	1	32	7	35	.1	6	3	288	5.38	13	5	ND	1	6	1	2	2	155	.14	.027	2	23	.09	25	.11	2	1.61	.01	.02	2	1
L14+00N 1+00E	1	55	14	71	.3	14	8	260	7.30	19	5	ND	2	5	1	6	2	142	.18	.050	2	40	.22	47	.02	2	3.04	.01	.04	3	1
L14+00N 1+25E	1	51	12	82	.1	21	24	1345	5.23	17	5	ND	1	10	1	2	2	106	.42	.044	4	31	.29	47	.06	2	2.26	.01	.05	1	1
L14+00N 1+50E	1	51	6	64	.2	10	7	298	6.61	15	5	ND	1	4	1	2	2	133	.16	.047	2	34	.19	43	.02	2	2.68	.01	.03	1	1
L14+00N 1+75E	1	38	12	40	.1	8	5	399	5.99	13	5	ND	1	6	1	2	2	158	.18	.030	2	27	.12	27	.11	2	1.81	.01	.02	2	1
L14+00N 2+00E	1	50	8	54	.2	11	7	251	9.19	20	5	ND	2	6	2	2	2	230	.28	.039	2	53	.20	18	.37	2	2.59	.01	.03	2	3
L14+00N 2+25E	1	64	17	73	.1	19	10	263	7.43	26	5	ND	2	6	1	3	2	172	.23	.055	4	56	.31	39	.10	3	3.79	.01	.03	4	1
L12+00N 5+50W	1	78	17	78	.6	20	12	496	10.94	33	5	ND	2	9	1	14	2	248	.59	.114	2	66	.45	16	.47	2	3.39	.01	.04	1	30
L12+00N 5+25W	1	124	14	97	.1	38	18	515	9.73	24	5	ND	2	9	1	11	2	249	.66	.086	3	101	.72	24	.45	2	5.11	.01	.03	1	4
L12+00N 5+00W	1	169	5	112	.5	50	19	451	8.59	22	5	ND	2	8	1	9	2	226	.74	.068	2	109	1.10	18	.52	2	6.58	.01	.03	1	1
L12+00N 4+75W	1	100	22	91	.2	34	20	965	11.97	30	5	ND	2	9	1	8	2	277	.74	.106	2	110	.85	17	.64	2	5.73	.01	.03	1	9
L12+00N 4+50W	1	600	18	203	1.6	77	29	514	10.71	296	5	ND	1	9	1	21	2	246	.56	.039	3	101	1.35	57	.48	2	5.96	.01	.03	1	290
L12+00N 4+25W	1	96	13	85	.7	33	14	315	9.66	48	5	ND	2	11	2	9	2	246	.58	.024	3	80	.76	29	.53	2	3.65	.01	.02	1	1
L12+00N 4+00W	1	138	17	150	.5	53	21	506	10.20	31	5	ND	2	10	2	9	2	250	.85	.049	2	92	1.30	30	.60	5	4.99	.01	.03	1	2
L12+00N 3+75W	1	133	24	210	.3	45	21	563	10.47	42	5	ND	2	13	2	7	2	267	.64	.048	3	82	1.09	27	.68	2	4.41	.01	.03	1	1
L12+00N 3+50W	1	70	18	140	.3	24	11	262	12.05	42	5	ND	2	9	1	14	2	329	.49	.048	2	77	.39	23	.54	2	3.04	.01	.02	1	4
L12+00N 3+25W	1	134	21	117	.1	45	20	360	11.06	37	5	ND	2	8	1	3	2	266	.52	.076	3	103	.86	25	.57	2	5.81	.01	.02	1	1
L12+00N 3+00W	2	161	20	147	.5	43	31	1689	8.96	54	5	ND	2	11	3	7	2	205	.59	.062	4	70	.76	32	.40	2	4.19	.01	.04	1	480
L12+00N 2+75W	1	63	22	57	.4	19	8	227	11.54	21	5	ND	2	7	1	9	2	366	.42	.047	2	81	.42	8	.81	2	3.03	.01	.02	1	3
L12+00N 2+50W	1	46	16	112	.5	19	9	281	9.06	21	5	ND	2	17	1	7	2	250	.66	.065	4	71	.39	37	.54	2	2.68	.01	.03	1	8
STD C/AU-S	18	58	41	132	7.1	66	29	1018	3.94	38	17	7	37	47	16	16	23	58	.47	.093	38	56	.85	174	.07	33	1.90	.06	.14	12	53

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Soil -80 Mesh AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: OCT 31 1988 DATE REPORT MAILED: Nov 4/88 SIGNED BY. . . . . . . .D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-5601 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L31+00W 23+25N	1	48	3	47	.2	18	8	246	6.45	12	5	ND	1	9	1	2	2	181	.43	.028	4	47	.35	22	.27	2	2.02	.01	.03	1	5
L31+00W 22+75N	1	56	11	62	.1	27	16	543	5.57	10	5	ND	1	8	1	2	2	169	.49	.023	5	54	.38	26	.22	3	2.92	.01	.02	1	2
L31+00W 22+50N	1	74	10	59	.1	36	12	222	5.93	11	5	ND	1	6	1	2	2	156	.38	.016	3	55	.39	29	.18	3	3.39	.01	.03	1	4
L31+00W 22+25N	1	65	5	53	.1	27	13	314	5.57	11	5	ND	1	6	1	2	2	153	.41	.019	3	45	.42	29	.20	2	2.72	.02	.03	1	2
L31+00W 21+75N	1	48	15	53	.1	22	9	180	6.21	9	5	ND	1	5	1	2	2	178	.33	.021	3	55	.23	18	.27	3	2.91	.01	.02	1	1
L31+00W 21+50N	1	73	4	71	.1	27	10	189	7.33	17	5	ND	1	5	1	2	2	189	.31	.023	3	61	.34	24	.25	2	3.43	.01	.02	1	2
L31+00W 21+25N	1	29	9	37	.1	12	5	169	6.06	335	5	ND	1	5	1	2	2	152	.30	.024	3	40	.14	14	.24	2	1.76	.01	.02	2	1
L31+00W 21+00N	1	114	3	84	.1	42	16	265	6.11	31	5	ND	1	5	1	2	2	136	.36	.030	2	64	.49	27	.14	3	4.56	.01	.03	2	4
L31+00W 20+75N	1	56	8	259	.1	15	12	341	6.56	44	5	ND	1	5	1	2	2	162	.26	.030	3	52	.18	18	.20	2	3.27	.01	.02	1	1
L31+00W 20+50N	1	74	5	71	.1	29	17	434	6.19	43	5	ND	1	6	1	2	2	150	.42	.026	3	61	.45	38	.16	2	2.27	.01	.03	1	1
L31+00W 20+25N	1	56	6	62	.2	24	18	449	5.50	25	5	ND	1	6	1	3	2	168	.37	.026	4	58	.33	28	.16	8	3.14	.01	.03	2	1
L31+00W 20+00N	1	95	11	80	.1	36	15	308	5.73	21	5	ND	1	6	1	2	2	143	.40	.018	3	57	.41	33	.15	3	4.35	.01	.02	1	8
L31+00W 19+75N	1	42	8	70	.1	16	6	157	7.87	73	5	ND	1	5	1	2	2	177	.25	.035	2	61	.18	16	.24	2	3.05	.02	.04	1	1
L31+00W 19+50N	1	35	8	40	.1	9	4	133	8.39	20	5	ND	1	4	1	2	2	236	.21	.029	3	56	.11	13	.25	2	2.90	.01	.02	1	1
L31+00W 19+25N	1	75	7	51	.1	16	8	230	6.66	32	5	ND	1	5	1	3	2	202	.34	.062	3	63	.27	15	.28	2	3.14	.01	.02	1	2
L31+00W 19+00N	1	62	16	59	.3	18	7	159	6.61	305	5	ND	1	6	1	2	2	164	.34	.022	3	57	.30	19	.26	3	3.25	.01	.03	1	1
L31+00W 18+75N	1	74	9	57	.1	14	8	242	6.90	93	5	ND	1	5	1	3	2	186	.22	.027	3	63	.14	15	.34	2	3.98	.01	.02	1	2
L31+00W 18+50N	1	197	6	74	.1	24	10	217	9.51	173	5	ND	2	5	1	2	2	190	.29	.038	2	84	.37	22	.22	2	5.79	.01	.03	1	1
L31+00W 18+25N	1	62	9	42	.1	12	5	124	10.57	31	5	ND	1	4	1	3	2	306	.18	.029	3	72	.19	11	.41	2	2.94	.01	.02	3	19
L31+00W 18+00N	1	115	12	59	.1	21	8	145	8.65	61	5	ND	1	5	1	2	2	183	.27	.025	3	69	.23	16	.22	2	3.90	.01	.02	1	2
L31+00W 17+75N	1	81	3	56	.1	18	7	131	9.47	56	5	ND	1	3	1	2	2	222	.19	.027	2	78	.29	16	.25	2	3.70	.01	.03	1	1
L31+00W 17+50N	1	178	4	32	.2	33	13	199	7.75	39	5	ND	1	4	1	2	2	189	.24	.022	3	69	.32	24	.16	2	4.37	.01	.02	1	1
L31+00W 17+25N	1	129	6	99	.1	39	14	207	7.56	29	5	ND	1	4	1	2	2	164	.29	.029	3	85	.34	27	.15	3	5.83	.01	.02	1	2
L31+00W 17+00N	1	140	12	95	.1	43	30	346	7.53	26	5	ND	1	5	1	2	2	164	.35	.024	3	77	.61	40	.15	2	5.13	.01	.03	1	1
L31+00W 16+75N	1	64	14	51	.1	21	10	339	6.56	24	5	ND	1	6	1	2	2	171	.36	.029	3	52	.33	19	.21	4	2.89	.01	.02	1	2
L31+00W 16+50N	1	125	9	59	.1	26	3	169	8.24	31	5	ND	1	4	1	2	2	182	.24	.028	2	91	.30	22	.21	2	5.14	.01	.02	1	1
L31+00W 16+25N	1	68	16	54	.2	21	8	147	5.51	98	5	ND	1	4	1	2	2	193	.22	.025	2	72	.23	16	.15	3	3.24	.01	.02	1	3
L31+00W 15+50N	1	116	11	72	.1	30	12	171	9.21	32	5	ND	1	4	1	2	2	179	.21	.024	3	75	.35	29	.14	2	4.82	.01	.02	1	395
L31-00W 15+25N	1	120	2	70	.1	30	12	238	7.10	41	5	ND	1	4	1	2	2	157	.26	.017	3	59	.56	26	.09	2	3.94	.01	.03	1	1
L31+00W 14+50N	1	68	9	57	.1	20	9	260	3.17	39	5	ND	1	4	1	3	2	195	.27	.024	3	61	.39	17	.23	2	3.04	.01	.03	1	2
L31+00W 14+25N	1	64	11	51	.1	19	9	286	8.34	42	5	ND	1	5	1	2	2	197	.29	.026	3	60	.37	17	.26	2	3.41	.01	.02	1	1
L31+00W 14+00N	1	98	16	71	.1	25	11	364	10.01	37	5	ND	2	5	1	2	2	239	.31	.078	3	61	.47	22	.34	2	3.67	.01	.02	1	1
L31+00W 13+75N	1	89	8	56	.1	18	7	200	9.57	36	5	ND	1	4	1	2	2	191	.23	.053	2	76	.29	14	.24	2	3.94	.01	.02	1	1
L31+00W 13+50N	2	88	9	63	.1	23	11	221	10.16	47	5	ND	2	5	1	2	2	188	.29	.042	4	76	.46	24	.31	4	4.27	.01	.03	1	1
L31+00W 13+25N	5	132	9	46	.2	16	7	151	9.74	166	5	ND	2	4	1	9	2	169	.13	.032	4	71	.41	17	.29	2	4.48	.01	.03	4	113
L31+00W 13+00N	5	97	8	42	.1	10	5	95	7.13	123	5	ND	1	5	1	2	2	181	.15	.024	4	38	.23	14	.15	2	2.18	.01	.02	1	3
STD C/AU-S	19	61	45	132	6.9	68	30	1029	4.13	42	21	7	37	47	18	17	24	60	.49	.096	39	55	.90	172	.07	37	1.96	.06	.14	11	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L31+00W 12+75N	4	78	7	40	.1	7	4	66	8.22	104	5	ND	1	5	1	2	2	155	.12	.024	2	49	.17	18	.20	2	3.11	.01	.03	3	27
L31+00W 12+50N	2	71	8	36	.1	10	5	85	6.99	34	5	ND	1	4	1	4	2	176	.13	.020	3	41	.26	14	.24	2	2.80	.01	.02	4	15
L31+00W 12+25N	2	62	11	47	.1	8	4	110	13.24	42	5	ND	2	3	1	3	2	288	.10	.069	3	90	.15	14	.41	2	3.66	.01	.03	4	5
L31+00W 12+00N	2	130	14	52	.1	13	6	103	10.23	51	5	ND	2	4	1	4	2	225	.14	.399	3	81	.15	19	.21	2	6.39	.01	.03	4	10
L31+00W 11+25N	3	92	16	64	.1	20	10	453	7.46	43	5	ND	1	7	1	2	2	201	.36	.070	3	51	.39	24	.31	2	3.29	.01	.03	1	11
L31+00W 11+00N	1	34	9	51	.1	14	6	101	11.00	38	5	ND	1	5	1	3	2	253	.25	.070	3	84	.15	19	.40	2	4.35	.01	.03	1	7
L31+00W 10+75N	1	35	10	62	.1	21	3	183	9.01	33	5	ND	1	5	1	2	2	234	.29	.066	2	56	.29	20	.37	2	4.66	.01	.02	1	4
L31+00W 10+50N	1	71	10	57	.1	18	7	151	10.61	34	5	ND	1	5	1	5	2	254	.28	.055	2	79	.23	18	.30	2	3.95	.01	.03	2	5
L31+00W 10+25N	1	69	3	48	.1	14	6	126	7.52	47	5	ND	1	5	1	2	2	221	.33	.045	3	61	.21	15	.31	2	3.53	.01	.02	1	21
L31+00W 10+00N	1	15	5	22	.1	4	2	84	4.17	16	5	ND	1	5	1	2	2	224	.23	.017	3	24	.04	3	.57	2	.83	.01	.01	3	16
L30+50W 21+50N	1	37	10	55	.1	14	7	181	6.35	107	5	ND	1	7	1	3	2	212	.50	.028	3	41	.26	18	.34	2	1.34	.01	.02	1	2
L30+50W 21+25N	1	76	6	100	.1	28	11	436	6.70	26	5	ND	1	6	1	2	2	190	.41	.035	3	56	.39	29	.23	2	3.47	.01	.03	1	3
L30+50W 21+00N	1	51	3	85	.1	24	12	272	6.15	11	5	ND	1	6	1	2	2	130	.40	.020	3	55	.36	24	.24	3	3.11	.01	.02	1	11
L30+50W 20+75N	1	32	6	298	.1	36	21	662	6.31	28	5	ND	1	9	1	2	2	175	.54	.026	4	58	.55	43	.21	2	3.38	.01	.03	1	2
L30+50W 20+50N	1	55	11	85	.1	24	37	970	7.46	613	5	ND	1	7	1	2	2	193	.35	.032	5	55	.31	32	.20	2	2.99	.01	.03	1	2
L30+50W 20+25N	1	45	3	46	.1	14	7	140	6.67	48	5	ND	1	4	1	2	2	192	.32	.030	3	47	.13	15	.23	2	2.45	.01	.02	2	4
L30+50W 20+00N	1	26	5	26	.1	7	6	137	7.13	7	5	ND	1	7	1	2	2	322	1.37	.024	2	40	.15	7	.69	2	1.64	.01	.01	1	7
L30+50W 19+75N	1	40	13	65	.1	15	7	385	8.57	3	5	ND	1	10	1	2	2	203	.44	.120	5	58	.13	40	.36	2	2.56	.02	.11	1	5
L30+50W 19+25N	1	23	25	40	.1	10	8	422	5.29	50	5	ND	1	9	1	2	3	207	.62	.025	4	31	.18	28	.40	2	1.60	.01	.02	1	22
L30+50W 19+00N	1	19	9	23	.1	8	8	200	6.48	26	5	ND	1	6	1	2	2	171	.39	.029	4	42	.14	15	.26	4	2.07	.01	.02	1	2
L30+50W 18+50N	1	49	14	52	.1	14	7	249	11.09	55	5	ND	2	4	1	2	2	277	.25	.063	2	84	.22	18	.28	3	3.61	.01	.02	1	2
L30+50W 18+25N	1	106	12	65	.1	29	11	252	9.74	50	5	ND	1	6	1	2	2	199	.49	.025	3	76	.51	28	.27	4	4.60	.01	.02	1	1
L30+50W 18+00N	1	117	4	106	.1	36	16	253	9.81	485	5	ND	2	5	1	4	2	220	.39	.052	3	35	.47	32	.25	3	5.42	.01	.02	1	7
L30+50W 17+75N	1	49	5	39	.1	15	5	126	6.90	33	5	ND	1	5	1	2	2	238	.31	.021	3	51	.16	11	.36	2	2.34	.01	.02	1	5
L30+50W 17+50N	1	103	3	74	.1	24	10	178	9.12	45	5	ND	1	5	1	5	2	207	.35	.029	3	70	.33	24	.23	5	4.19	.01	.02	1	2
L30+50W 17+25N	1	57	7	54	.1	14	8	153	8.49	46	5	ND	1	5	1	4	2	273	.28	.020	3	64	.23	17	.37	4	2.90	.01	.01	2	1
L30+50W 17+00N	1	123	9	87	.1	33	14	259	9.97	54	5	ND	2	7	1	2	2	217	.39	.028	3	38	.47	32	.22	5	5.24	.01	.03	1	8
L30+50W 16+75N	1	42	12	41	.2	9	5	188	9.18	23	5	ND	2	4	1	3	2	246	.17	.025	3	54	.12	13	.31	4	2.36	.01	.02	2	4
L30+50W 16+50N	1	106	2	64	.1	32	14	276	7.57	37	5	ND	1	6	1	2	2	206	.50	.018	3	71	.56	40	.24	2	3.70	.01	.02	1	16
L30+50W 16+00N	1	134	4	75	.1	39	15	253	7.54	44	5	ND	1	5	1	2	2	192	.34	.029	3	77	.49	29	.17	2	5.05	.01	.02	1	2
L30+50W 15+75N	1	113	7	66	.1	20	9	187	8.35	33	5	ND	2	5	1	4	2	234	.34	.024	3	73	.32	17	.20	2	4.39	.01	.03	2	2
L30+50W 15+50N	1	97	10	69	.1	23	9	173	10.41	39	5	ND	2	4	1	2	2	237	.21	.050	2	109	.34	13	.22	2	5.59	.01	.02	1	4
L30+50W 15+25N	1	187	10	130	.1	52	13	288	5.05	39	5	ND	2	5	1	2	2	183	.23	.033	4	82	.72	56	.09	2	6.23	.01	.03	1	2
L30+50W 14+25N	1	87	18	59	.2	19	5	335	10.24	115	5	ND	2	6	1	7	2	251	.30	.065	3	74	.32	23	.39	5	3.67	.01	.03	2	4
L30+50W 14+00N	2	44	3	29	.1	6	4	102	5.74	89	5	ND	1	5	1	2	2	159	.20	.028	4	21	.13	13	.23	2	1.66	.01	.02	1	37
L30+50W 13+75N	4	116	6	52	.1	20	9	196	10.11	176	5	ND	1	5	1	4	2	226	.27	.044	3	57	.44	18	.34	5	3.01	.01	.03	1	55
STD C/AU-S	19	63	38	133	7.0	69	31	1037	4.22	39	17	7	39	50	19	19	24	61	.52	.098	41	56	.96	182	.07	36	2.03	.06	.15	11	47

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5601

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L30+50W 12+75N	1	69	10	29	.3	12	3	53	5.44	84	5	ND	1	4	1	2	2	141	.14	.014	3	44	.09	7	.17	5	2.96	.01	.01	1	1
L30+50W 12+50N	4	126	10	43	.6	23	10	146	4.82	91	5	ND	1	5	1	2	2	123	.26	.017	4	43	.33	20	.19	5	3.61	.01	.02	1	53
L30+50W 12+25N	1	156	12	57	.5	24	8	125	5.28	100	5	ND	1	5	1	2	2	131	.24	.024	3	54	.28	15	.19	4	4.10	.01	.02	2	260
L30+50W 12+00N	1	60	9	29	.3	8	4	93	5.19	65	5	ND	1	3	1	2	2	156	.12	.024	3	30	.11	10	.22	6	2.40	.01	.02	2	11
L30+50W 11+75N	1	121	6	45	.3	20	7	117	4.66	86	6	ND	1	4	1	2	2	112	.22	.017	3	46	.29	14	.18	5	3.84	.01	.02	2	32
L30+50W 11+50N	1	61	9	46	.2	17	8	176	7.25	38	5	ND	1	7	1	2	2	190	.33	.031	5	51	.24	21	.24	4	2.63	.01	.03	2	9
L30+50W 11+25N	1	150	4	66	.1	32	16	426	6.07	68	5	ND	1	20	1	2	2	145	.67	.033	4	54	.51	24	.18	6	3.68	.01	.04	1	3
L30+50W 11+00N	1	125	12	61	.2	23	12	408	6.18	47	5	ND	1	8	1	2	2	156	.47	.033	4	49	.39	19	.20	6	3.37	.01	.03	1	1
L30+50W 10+75N	1	130	5	87	.1	37	16	254	5.80	39	5	ND	1	6	1	2	2	140	.31	.023	2	60	.53	31	.12	4	4.94	.01	.03	1	1
L30+50W 10+50N	1	74	5	65	.2	22	7	163	6.96	34	5	ND	1	5	1	2	2	185	.29	.029	3	59	.21	14	.16	6	3.15	.01	.02	1	7
L30+50W 10+25N	1	35	7	36	.3	9	4	153	5.08	20	5	ND	1	6	1	2	2	225	.24	.018	4	41	.08	7	.45	5	1.41	.01	.01	1	31
L30+50W 10+00N	1	55	3	54	.3	15	6	136	7.01	31	5	ND	1	6	1	2	2	196	.24	.032	3	52	.14	15	.27	5	2.74	.01	.02	1	1
L30+50W 9+75N	1	101	11	56	.2	22	10	278	6.21	39	5	ND	1	6	1	2	2	136	.51	.032	3	65	.34	18	.37	5	4.12	.01	.02	1	1
L30+50W 9+50N	1	122	12	65	.2	31	12	215	6.78	41	5	ND	1	6	1	4	2	174	.54	.031	3	74	.38	26	.32	9	5.08	.01	.02	2	12
L30+50W 9+25N	1	101	9	65	.1	24	9	181	8.19	69	5	ND	1	5	1	2	2	194	.27	.039	3	83	.30	26	.23	4	4.99	.01	.03	1	3
L30+50W 9+00N	1	43	4	32	.2	3	5	101	7.66	40	5	ND	1	4	1	2	2	210	.12	.025	3	45	.05	7	.29	4	1.34	.01	.02	3	1
L30+50W 8+75N	1	215	6	67	.2	39	13	209	5.97	46	5	ND	2	5	1	2	2	137	.36	.025	3	73	.51	25	.22	5	6.46	.01	.03	1	3
L30+50W 8+50N	1	126	7	61	.4	25	9	161	5.38	45	5	ND	1	5	1	2	2	174	.33	.016	4	66	.34	19	.30	5	3.77	.01	.02	1	6
L30+50W 7+75N	5	165	8	78	.3	26	35	1470	5.53	181	5	ND	1	11	1	2	2	109	.30	.036	4	45	.38	44	.13	5	3.83	.01	.04	1	29
L30+50W 7+50N	4	162	5	60	.5	28	15	346	5.14	184	5	ND	1	10	1	3	2	113	.37	.023	4	45	.52	62	.14	4	3.64	.01	.04	1	8
L30+50W 7+25N	5	121	2	85	.6	19	9	160	7.13	155	5	ND	1	6	1	2	2	146	.22	.053	4	48	.24	24	.26	5	4.63	.01	.04	1	5
L30+50W 7+00N	2	133	12	55	.4	24	10	165	6.80	145	5	ND	1	4	1	2	2	125	.14	.030	4	59	.31	19	.09	4	4.34	.01	.02	2	16
L30+50W 6+75N	2	141	12	75	.5	28	14	277	7.03	161	5	ND	1	7	1	2	2	184	.26	.025	5	57	.39	33	.17	5	4.25	.03	.05	1	50
L30+50W 6+50N	2	199	4	65	.4	30	13	188	5.92	176	5	ND	1	7	1	2	2	115	.24	.028	5	52	.44	36	.16	4	4.76	.01	.03	1	16
L30+50W 6+25N	4	112	12	57	.6	15	7	170	4.22	137	5	ND	1	7	1	2	2	106	.15	.020	4	34	.14	25	.11	4	3.32	.01	.03	1	12
L30+50W 6+00N	3	133	5	53	.5	20	10	167	4.60	162	5	ND	1	8	1	2	2	100	.27	.042	3	40	.35	19	.16	4	4.24	.01	.03	1	12
L30+50W 5+75N	2	135	9	55	.2	30	12	184	5.62	193	5	ND	1	7	1	2	2	142	.28	.027	5	57	.39	27	.25	5	3.80	.01	.03	1	14
L30+50W 5+50N	3	133	10	62	.7	27	11	198	5.30	198	5	ND	1	9	1	10	2	150	.26	.027	5	45	.39	37	.16	4	3.25	.01	.04	1	9
L30+50W 5+25N	1	225	15	68	.4	48	16	273	5.51	217	5	ND	1	8	1	9	2	120	.29	.023	4	60	.67	62	.17	4	4.94	.01	.06	1	16
L30+50W 5+00N	1	233	13	83	.2	46	18	310	6.93	225	5	ND	1	7	1	3	2	155	.27	.018	5	71	.67	56	.18	4	4.59	.01	.06	1	23
L30+50W 4+75N	5	273	15	98	.7	34	52	391	6.78	272	5	ND	1	7	1	3	2	130	.23	.027	5	56	.47	46	.13	3	5.43	.01	.05	1	121
L30+50W 4+50N	1	110	12	44	.4	19	7	119	5.83	177	5	ND	1	5	1	4	2	152	.17	.025	4	48	.24	19	.14	2	3.46	.01	.03	1	22
L30+50W 4+00N	2	192	16	58	1.0	25	9	171	5.72	182	5	ND	1	6	1	4	2	116	.27	.023	4	63	.42	35	.15	5	5.10	.01	.03	2	35
L30+50W 3+75N	1	190	3	61	1.0	32	11	212	5.72	173	5	ND	1	7	1	2	2	114	.30	.026	4	53	.58	51	.15	6	4.65	.01	.04	1	11
L30+50W 3+50N	7	100	7	31	.4	13	5	69	5.36	115	5	ND	1	4	1	3	2	130	.10	.022	4	37	.15	16	.11	4	3.64	.01	.02	4	13
L29+00W 20+50N	1	68	6	92	.1	24	24	420	7.24	91	5	ND	1	9	1	2	2	185	.46	.026	3	53	.21	23	.26	2	3.23	.01	.02	1	1
STD C/AU-S	19	59	38	132	6.9	69	31	1022	4.01	41	17	7	36	48	19	16	21	59	.48	.088	38	56	.89	178	.07	36	1.90	.06	.14	11	47

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5601

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L29+00W 20+25N	1	98	2	95	.1	38	20	505	5.72	45	5	ND	1	9	1	2	2	134	.56	.025	4	53	.52	36	.19	3	3.31	.01	.03	1	1
L29+00W 19+50N	1	40	2	89	.1	17	12	536	6.17	183	5	ND	1	7	1	2	2	148	.44	.023	3	39	.21	26	.25	2	2.20	.01	.02	1	2
L29+00W 19+25N	1	74	9	183	.1	31	28	257	6.65	31	5	ND	1	5	1	2	2	169	.34	.021	3	51	.35	29	.31	3	2.95	.01	.02	1	1
L29+00W 19+00N	1	41	3	79	.1	17	7	135	5.52	17	5	ND	1	4	1	2	2	160	.22	.020	3	44	.17	19	.30	4	2.79	.01	.01	1	9
L29+00W 18+75N	1	92	4	97	.1	29	12	234	6.62	32	5	ND	1	5	1	5	2	166	.38	.021	3	57	.37	32	.31	2	3.88	.01	.02	1	4
L29+00W 18+50N	1	64	5	56	.1	11	5	191	8.32	19	5	ND	1	4	1	2	2	211	.27	.030	3	45	.11	15	.28	2	2.40	.01	.01	2	1
L29+00W 18+25N	1	80	3	64	.1	14	6	384	5.88	53	5	ND	1	5	1	5	2	294	.44	.042	2	58	.23	35	.38	2	2.68	.01	.02	1	1
L29+00W 18+00N	1	121	8	91	.2	27	10	240	6.73	13	5	ND	2	5	1	4	2	165	.33	.027	3	59	.27	20	.33	4	4.12	.01	.03	1	4
L29+00W 17+75N	1	52	2	84	.1	16	15	221	7.58	26	5	ND	1	4	1	5	2	220	.26	.032	3	49	.22	20	.32	5	2.61	.01	.02	1	72
L29+00W 17+50N	1	58	4	49	.1	11	6	134	6.59	14	5	ND	2	4	1	2	2	236	.25	.025	3	55	.16	13	.29	2	2.64	.01	.02	2	3
L29+00W 17+25N	1	64	9	91	.2	16	7	283	12.12	210	5	ND	1	6	1	5	2	359	.37	.031	2	70	.30	15	.55	3	2.94	.01	.02	1	1
L29+00W 17+00N	2	45	3	60	.1	21	9	164	7.19	312	5	ND	1	6	1	2	2	166	.43	.026	3	59	.37	20	.22	2	3.57	.01	.02	1	6
L29+00W 16+75N	1	109	2	65	.1	19	10	337	10.03	155	5	ND	2	5	1	4	2	251	.26	.090	4	65	.33	16	.26	2	4.38	.01	.03	1	3
L29+00W 16+50N	1	61	7	60	.1	20	9	334	9.56	30	5	ND	2	7	1	3	2	241	.29	.050	3	67	.28	13	.31	3	3.33	.01	.02	1	4
L29+00W 16+25N	1	45	2	53	.1	15	8	201	6.38	14	5	ND	1	4	1	5	2	170	.27	.022	3	46	.20	15	.23	2	2.67	.01	.01	1	2
L29+00W 16+00N	1	129	4	82	.1	32	14	226	7.23	29	5	ND	1	4	1	2	2	161	.32	.025	2	66	.41	25	.31	4	5.12	.01	.02	1	1
L29+00W 15+75N	1	37	3	43	.1	10	6	351	7.06	16	5	ND	2	9	1	2	2	256	.29	.029	3	45	.14	16	.47	2	1.64	.01	.01	1	31
L29+00W 15+50N	1	80	7	56	.1	18	8	322	8.23	28	5	ND	2	6	1	5	2	213	.30	.046	3	54	.15	16	.21	3	3.17	.01	.02	1	1
L29+00W 15+00N	1	84	10	62	.1	15	7	215	9.61	11	5	ND	2	4	1	4	2	215	.27	.060	3	70	.17	22	.26	4	4.69	.01	.03	1	7
L29+00W 14+75N	1	132	4	67	.1	23	10	222	6.66	30	5	ND	2	4	1	6	2	167	.27	.069	4	84	.35	18	.21	4	5.02	.01	.03	1	4
L29+00W 14+50N	1	146	2	92	.1	32	13	284	7.59	32	5	ND	2	5	1	5	2	169	.31	.033	3	66	.46	34	.19	2	5.32	.01	.03	1	3
L29+00W 14+25N	1	62	7	49	.1	13	6	149	9.81	36	5	ND	2	3	1	5	2	216	.15	.040	2	65	.17	13	.16	2	3.66	.01	.02	4	19
L29+00W 14+00N	1	82	6	51	.1	17	7	184	8.08	22	5	ND	1	6	1	3	2	199	.31	.036	3	55	.30	15	.27	2	3.46	.01	.02	1	2
L29+00W 13+75N	1	131	5	85	.1	41	20	291	6.22	37	5	ND	2	4	1	2	2	127	.28	.019	3	58	.62	46	.02	3	4.45	.01	.03	1	49
L29+00W 13+50N	1	148	2	99	.1	34	14	223	6.47	34	5	ND	2	4	1	4	2	137	.27	.022	3	54	.43	37	.13	2	4.00	.01	.02	1	2
L29+00W 13+00N	1	74	2	43	.1	17	8	170	5.91	60	5	ND	1	4	1	2	2	150	.29	.021	3	46	.35	15	.25	4	2.78	.01	.02	1	1
L29+00W 12+75N	1	20	5	37	.1	8	7	162	10.45	16	5	ND	2	4	1	6	7	254	.21	.036	3	49	.09	11	.43	2	1.58	.01	.02	2	2
L29+00W 12+50N	1	64	5	43	.1	10	5	137	6.34	50	5	ND	1	4	1	5	2	154	.24	.043	3	42	.13	13	.27	2	3.65	.01	.02	1	5
L29+00W 12+25N	1	34	13	36	.1	9	6	217	3.28	792	5	ND	1	5	1	5	2	188	.23	.049	3	37	.13	15	.30	2	2.10	.01	.02	2	21
L29+00W 12+00N	1	58	8	52	.1	15	7	247	9.29	376	5	ND	2	5	1	4	2	177	.25	.041	3	58	.20	16	.26	3	3.44	.02	.02	1	4
L29+00W 11+75N	1	43	12	31	.1	9	4	98	5.66	27	5	ND	2	5	1	5	4	163	.22	.031	4	37	.15	12	.32	3	2.20	.01	.02	2	7
L29+00W 11+25N	1	122	9	57	.1	20	9	238	8.37	42	5	ND	2	6	1	5	2	167	.31	.040	3	70	.34	22	.22	2	5.67	.01	.04	1	23
L29+00W 11+00N	1	65	7	47	.1	15	7	131	9.02	34	5	ND	2	5	1	5	2	225	.20	.091	3	57	.29	16	.31	2	3.57	.01	.03	2	6
L29+00W 10+50N	1	152	7	94	.1	39	15	249	7.40	55	5	ND	1	4	1	5	2	151	.22	.032	3	64	.53	42	.16	2	5.25	.01	.03	1	4
L29+00W 10+25N	1	48	2	49	.1	15	10	254	5.08	24	5	ND	1	5	1	2	2	142	.29	.022	6	35	.29	26	.16	2	2.36	.01	.02	1	6
L29+00W 10+00N	1	97	7	65	.1	28	16	220	5.85	26	5	ND	1	5	1	2	2	158	.32	.024	4	56	.43	42	.14	2	4.29	.01	.03	1	8
STD C/AU-S	18	62	39	133	7.0	67	30	1052	4.16	39	20	7	38	48	18	20	22	59	.48	.098	39	55	.90	183	.07	36	2.00	.06	.15	12	52

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5601

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L29+00W 9+75N	1	114	10	85	.1	31	14	244	6.94	48	5	ND	2	6	1	3	2	175	.36	.033	3	58	.48	29	.28	2	4.25	.01	.03	1	3
L29+00W 9+50N	1	55	2	40	.1	19	11	173	5.49	25	5	ND	1	4	1	2	3	181	.27	.021	4	46	.22	23	.30	2	2.32	.01	.02	1	1
L29+00W 9+25N	1	104	10	62	.1	29	12	371	5.51	47	5	ND	1	6	1	3	2	141	.34	.025	3	53	.43	32	.16	2	3.58	.01	.03	1	5
L29+00W 8+75N	1	113	4	62	.1	28	11	365	5.45	50	5	ND	1	6	1	2	2	143	.40	.036	3	55	.46	28	.19	2	3.56	.01	.03	1	4
L29+00W 8+50N	1	139	11	57	.1	30	13	338	5.66	56	5	ND	1	6	1	3	2	142	.36	.032	3	55	.52	29	.19	2	3.72	.01	.03	1	1
L29+00W 8+25N	1	123	7	67	.1	31	13	204	6.64	61	5	ND	1	4	1	2	2	155	.24	.027	3	58	.44	28	.11	2	3.87	.01	.03	1	4
L29+00W 8+00N	2	49	5	35	.1	12	4	116	6.33	61	5	ND	1	4	1	2	2	214	.18	.027	3	45	.13	13	.35	2	2.02	.01	.02	2	16
L29+00W 7+50N	1	126	12	56	.5	17	6	106	7.24	85	5	ND	2	3	1	2	2	135	.13	.033	2	65	.22	15	.20	2	5.69	.01	.02	1	4
L29+00W 7+25N	4	229	9	38	.2	20	3	53	5.11	76	5	ND	1	4	1	2	2	114	.10	.023	3	42	.16	11	.17	2	4.14	.01	.02	1	5
L29+00W 6+50N	1	165	7	30	.5	28	13	166	5.99	108	5	ND	2	4	1	2	2	133	.19	.044	4	62	.31	32	.19	2	5.31	.01	.03	1	22
L29+00W 6+25N	1	112	10	57	.3	17	6	122	4.98	105	5	ND	2	5	1	2	2	123	.23	.057	3	41	.24	16	.22	3	4.02	.01	.02	1	90
L29+00W 6+00N	2	194	4	50	.2	22	8	127	5.35	136	5	ND	2	4	1	4	2	107	.17	.024	3	55	.33	23	.16	4	5.58	.01	.02	3	51
L29+00W 5+25N	2	133	10	54	.2	22	7	138	4.69	192	5	ND	1	5	1	8	2	123	.26	.024	3	43	.36	27	.16	3	2.88	.01	.03	1	57
L29+00W 5+00N	2	73	6	36	.4	12	5	87	6.19	152	5	ND	2	5	1	7	2	150	.13	.031	5	40	.15	16	.17	3	2.13	.01	.03	3	10
L29+00W 4+75N	1	133	8	45	.2	18	6	113	6.55	159	5	ND	1	5	1	5	2	152	.17	.032	3	49	.27	26	.20	3	3.43	.01	.02	2	15
L29+00W 4+50N	1	135	15	57	.4	28	9	161	5.74	206	5	ND	1	5	1	8	2	123	.22	.029	4	58	.43	42	.16	4	4.67	.01	.03	1	33
L29+00W 4+25N	2	228	15	87	.3	36	12	203	6.84	188	5	ND	2	4	1	9	2	126	.22	.074	3	70	.55	38	.18	4	6.05	.01	.03	1	17
L29+00W 4+00N	2	145	11	55	.6	16	6	79	5.24	139	5	ND	2	5	1	2	2	80	.11	.074	3	49	.23	24	.13	5	7.04	.01	.02	1	30
L29+00W 3+75N	6	183	16	48	.6	15	6	126	4.91	164	5	ND	2	6	1	4	2	96	.13	.035	2	43	.26	19	.12	4	5.23	.01	.02	5	16
L29+00W 3+50N	9	186	10	57	.5	29	11	246	4.57	123	5	ND	1	5	1	5	2	96	.18	.030	4	43	.43	37	.14	3	4.93	.01	.04	2	22
L27+50W 15+00N	1	65	4	58	.1	26	14	198	5.38	29	5	ND	1	5	1	2	2	146	.32	.021	5	49	.39	36	.13	2	3.20	.01	.02	1	10
L27+50W 14+75N	1	127	11	82	.2	43	17	231	7.22	41	5	ND	2	4	1	2	2	181	.29	.029	3	72	.56	54	.18	4	4.82	.01	.03	1	5
L27+50W 14+50N	1	87	18	49	.1	19	8	142	5.63	33	5	ND	1	5	1	2	2	150	.32	.031	3	49	.30	16	.19	3	2.88	.01	.02	1	6
L27+50W 14+25N	1	32	2	33	.1	8	4	107	5.96	31	5	ND	1	4	1	2	2	193	.19	.015	2	38	.12	10	.29	2	1.47	.01	.01	1	13
L27+50W 14+00N	12	362	15	52	.2	15	8	109	3.57	233	5	ND	1	7	1	5	2	79	.13	.011	5	29	.37	36	.05	4	2.84	.01	.03	1	67
L27+50W 13+75N	6	339	7	54	.3	16	8	130	3.36	271	5	ND	2	10	1	2	2	63	.15	.011	4	26	.42	46	.06	4	2.39	.02	.03	1	66
L27+50W 13+50N	5	409	14	82	.6	21	19	273	3.77	263	5	ND	2	13	1	4	2	66	.21	.015	4	32	.49	60	.06	6	2.68	.02	.04	2	74
L27+50W 12+75N	2	137	9	55	.3	13	8	165	8.02	76	5	ND	2	4	1	2	2	169	.24	.044	3	58	.29	14	.25	3	4.28	.01	.03	1	5
L27+50W 12+50N	1	105	6	59	.2	24	9	172	9.53	56	5	ND	2	6	1	2	2	196	.29	.091	3	75	.37	19	.33	5	3.85	.01	.02	1	1
L27+50W 12+25N	1	67	16	59	.1	20	9	472	7.80	65	5	ND	2	7	1	2	2	187	.39	.065	3	59	.39	18	.29	3	3.31	.01	.03	1	1
L27+50W 11+75N	1	72	17	48	.1	16	8	286	8.53	601	5	ND	2	5	1	2	2	238	.28	.038	3	55	.27	14	.44	4	3.16	.01	.02	1	7
L27+50W 11+50N	1	140	9	95	.2	32	15	394	10.25	68	5	ND	2	7	1	2	2	205	.26	.086	3	72	.56	34	.35	4	5.59	.01	.04	1	1
L27+50W 11+25N	1	131	10	51	.3	16	8	146	9.01	30	5	ND	2	5	1	5	2	172	.21	.087	3	75	.22	14	.26	3	7.26	.01	.02	2	1
L27+50W 11+00N	1	72	12	63	.3	17	21	412	12.35	44	5	ND	2	6	1	3	2	216	.22	.102	4	62	.31	19	.37	4	3.27	.01	.03	1	8
L27+50W 10+75N	1	35	9	23	.2	6	2	76	6.36	26	5	ND	2	3	1	2	3	245	.09	.021	3	35	.09	7	.44	3	1.23	.01	.01	2	9
L27+50W 10+00N	1	93	4	75	.3	25	16	212	6.28	43	5	ND	2	5	1	2	2	151	.23	.020	4	53	.32	30	.15	5	3.68	.01	.02	1	4
STD C/AU-S	18	61	40	132	6.8	67	30	1014	4.15	39	20	7	37	47	18	20	17	59	.49	.095	39	55	.90	171	.07	37	1.98	.06	.14	11	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L27+50W 9+50N	1	77	5	52	.1	19	6	153	6.25	36	5	ND	1	4	1	2	4	134	.24	.025	2	51	.28	21	.15	2	4.16	.01	.02	1	2
L27+50W 9+00N	1	47	8	39	.1	15	7	179	4.76	38	5	ND	1	7	1	2	2	135	.42	.019	3	35	.32	24	.19	2	2.02	.01	.02	1	5
L27+50W 8+75N	1	86	9	65	.1	20	9	179	8.77	60	5	ND	1	4	1	2	2	171	.20	.057	2	67	.19	22	.17	2	4.64	.01	.03	1	1
L27+50W 8+25N	1	92	9	57	.1	24	10	150	5.53	65	5	ND	1	4	1	5	2	133	.24	.020	3	47	.34	33	.11	2	3.75	.01	.02	1	3
L27+50W 8+00N	1	101	7	73	.1	26	10	192	6.60	68	5	ND	1	4	1	2	2	146	.18	.034	3	56	.27	31	.11	2	4.90	.01	.02	1	5
L27+50W 7+75N	1	114	8	62	.1	30	12	226	4.97	71	5	ND	1	5	1	5	4	119	.23	.013	4	52	.47	50	.06	2	3.92	.01	.03	1	2
L27+50W 7+50N	1	100	12	90	.1	24	10	152	5.93	70	5	ND	1	3	1	4	2	115	.15	.026	3	58	.32	22	.02	2	5.69	.01	.03	1	2
L27+50W 7+25N	3	271	9	45	.1	13	6	108	5.47	129	5	ND	1	4	1	5	2	122	.16	.028	3	40	.23	18	.11	2	4.14	.01	.02	2	7
L27+50W 7+00N	2	147	16	38	.1	11	6	89	9.16	105	5	ND	1	3	1	2	2	186	.13	.056	2	72	.20	12	.24	2	5.99	.01	.02	1	16
L27+50W 6+75N	1	143	12	70	.4	24	12	219	5.59	77	5	ND	2	4	1	5	2	147	.15	.049	2	64	.33	33	.10	3	6.04	.01	.03	1	4
L27+50W 6+50N	1	105	8	33	.1	11	6	192	7.02	80	5	ND	1	3	1	6	2	168	.14	.055	3	51	.13	12	.15	2	3.99	.01	.02	2	58
L27+50W 6+25N	3	164	17	70	.1	29	13	208	9.05	104	5	ND	2	3	1	6	2	159	.17	.072	3	97	.33	24	.14	3	6.83	.01	.02	1	27
L27+50W 5+75N	5	158	14	98	.2	31	15	241	5.02	152	5	ND	1	6	1	8	2	112	.23	.019	4	54	.47	33	.12	3	4.69	.01	.03	1	71
L27+50W 5+50N	7	180	13	54	.3	22	10	149	5.43	169	5	ND	1	4	1	7	2	104	.16	.034	4	52	.30	29	.13	4	6.30	.01	.02	1	280
L27+50W 5+25N	13	136	11	57	.2	26	15	292	6.34	221	5	ND	1	6	1	7	2	121	.19	.022	3	51	.41	44	.17	2	4.80	.01	.04	1	61
L27+50W 5+00N	30	206	10	77	.4	27	20	466	5.89	242	5	ND	1	6	1	6	2	103	.19	.021	3	47	.48	49	.11	3	5.24	.01	.05	1	82
L27+50W 4+75N	15	137	10	59	.2	26	14	260	6.95	220	5	ND	1	5	1	6	2	137	.18	.023	3	54	.38	45	.19	3	5.01	.01	.04	1	21
L27+50W 4+50N	2	125	6	51	.2	19	8	170	5.15	160	5	ND	1	5	1	5	2	135	.20	.030	4	42	.30	30	.16	2	3.53	.01	.03	1	22
L27+50W 4+25N	2	128	13	47	.1	18	6	105	5.86	204	5	ND	1	3	1	6	3	157	.15	.025	3	54	.23	16	.15	2	3.78	.01	.03	1	19
L27+50W 4+00N	1	106	15	42	.2	17	6	123	6.01	190	5	ND	1	3	1	7	2	143	.15	.025	3	48	.24	19	.13	2	3.36	.01	.02	1	13
L27+50W 3+75N	5	169	16	67	.3	31	11	292	6.35	201	5	ND	1	5	1	6	2	147	.16	.076	3	49	.28	43	.20	2	4.72	.01	.04	1	31
L27+50W 3+50N	2	171	13	77	.2	23	10	152	4.74	191	5	ND	1	5	1	7	2	106	.20	.041	2	47	.38	20	.17	5	5.53	.01	.02	2	17
L26+00W 15+00N	1	159	8	88	.1	48	19	373	6.30	49	5	ND	1	5	1	2	2	155	.32	.056	3	78	.76	62	.12	2	6.16	.01	.04	1	2
L26+00W 14+75N	1	163	10	106	.1	55	25	417	5.18	51	5	ND	2	5	1	4	2	139	.36	.038	3	71	.70	48	.15	3	6.59	.01	.03	1	3
L26+00W 14+50N	1	64	10	42	.1	18	7	155	6.32	37	5	ND	1	4	1	2	2	169	.22	.031	2	55	.21	17	.16	2	3.52	.01	.02	2	29
L26+00W 14+25N	1	90	13	68	.1	22	10	210	6.15	35	5	ND	2	4	1	2	2	143	.26	.061	2	54	.30	26	.17	2	4.83	.01	.02	1	2
L26+00W 14+00N	1	153	14	86	.1	41	16	287	8.14	49	5	ND	2	5	1	2	4	162	.30	.066	3	80	.62	37	.20	2	6.94	.01	.04	1	2
L26+00W 13+75N	1	25	6	25	.2	7	5	134	4.97	12	5	ND	2	6	1	3	2	225	.21	.019	3	35	.09	11	.49	2	1.53	.01	.02	1	22
L26+00W 13+50N	1	137	10	93	.1	40	16	240	6.17	56	5	ND	2	4	1	2	2	136	.32	.035	3	63	.55	44	.18	5	5.73	.01	.03	1	3
L26+00W 13+25N	1	84	12	65	.1	18	8	168	7.36	41	5	ND	2	4	1	4	2	168	.27	.071	2	79	.24	20	.25	2	5.25	.01	.02	1	3
L26+00W 13+00N	1	77	7	79	.1	17	8	192	6.48	52	5	ND	2	4	1	4	2	168	.28	.069	2	55	.26	20	.34	2	3.97	.01	.02	1	43
L26+00W 12+75N	8	424	15	62	.4	26	10	175	3.90	236	5	ND	2	6	1	9	2	78	.15	.014	3	46	.52	46	.09	2	5.79	.01	.04	3	48
L26+00W 11+75N	1	109	11	75	.1	24	10	171	6.26	234	5	ND	1	11	1	5	2	131	.47	.024	3	49	.31	33	.26	3	4.16	.01	.02	1	35
L26+00W 11+50N	1	139	6	69	.3	29	13	213	5.23	76	5	ND	2	5	1	4	2	112	.31	.019	2	46	.52	27	.13	5	3.95	.01	.03	1	9
L26+00W 11+25N	1	69	3	45	.2	15	8	334	5.72	54	5	ND	1	5	1	4	2	154	.26	.034	3	39	.22	24	.21	2	3.30	.01	.03	2	5
L26+00W 11+00N	1	99	2	62	.1	27	11	257	5.67	59	5	ND	1	5	1	2	2	127	.30	.029	3	54	.53	34	.14	2	3.36	.01	.03	1	4
STD C/AU-S	18	59	37	133	6.7	68	30	1055	4.13	42	20	7	37	47	18	17	23	56	.47	.093	38	57	.94	173	.06	35	1.97	.06	.14	12	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L26+00W 10+75N	1	84	10	62	.1	24	5	183	5.68	45	5	ND	1	4	1	3	2	161	.19	.028	3	48	.25	27	.19	2	3.24	.01	.02	1	15
L26+00W 10+50N	1	125	9	81	.1	39	21	392	5.44	57	5	ND	1	6	1	4	2	131	.35	.013	4	62	.71	68	.07	2	3.67	.01	.03	1	4
L26+00W 10+25N	2	152	10	39	.2	14	6	146	4.87	87	5	ND	1	4	1	5	2	118	.13	.032	3	35	.22	16	.14	2	3.90	.01	.02	2	5
L26+00W 10+00N	1	154	13	82	.1	38	15	209	7.28	56	5	ND	1	4	1	3	2	155	.22	.026	2	71	.47	36	.10	2	5.10	.01	.03	1	3
L26+00W 9+50N	6	46	14	55	.1	18	17	318	5.45	360	5	ND	1	10	1	3	2	158	.28	.027	4	39	.30	30	.26	2	2.78	.01	.03	1	9
L26+00W 9+25N	1	46	14	47	.1	15	5	100	5.97	69	5	ND	1	6	1	4	2	168	.29	.021	3	42	.18	16	.18	2	2.29	.01	.02	1	10
L26+00W 8+50N	2	75	12	44	.1	18	7	129	4.14	144	5	ND	1	4	1	3	2	105	.18	.025	3	36	.20	19	.13	2	3.12	.01	.02	1	8
L26+00W 8+25N	1	140	9	39	.1	32	14	195	5.75	33	5	ND	1	4	1	5	2	130	.20	.040	3	53	.36	39	.09	2	4.95	.01	.03	1	11
L26+00W 8+00N	1	95	10	60	.1	26	9	152	5.08	63	5	ND	1	4	1	4	2	141	.18	.026	3	55	.30	25	.09	2	3.74	.01	.02	1	1
L26+00W 7+75N	1	140	12	75	.1	31	12	245	6.76	82	5	ND	1	5	1	5	2	139	.20	.038	3	61	.40	38	.07	2	4.63	.01	.04	1	8
L26+00W 7+25N	1	105	8	64	.2	24	9	142	6.38	88	5	ND	1	5	1	6	2	137	.16	.029	3	56	.29	39	.05	2	4.61	.01	.03	1	28
L26+00W 7+00N	1	126	12	45	.3	15	5	88	5.92	106	5	ND	2	3	1	4	2	96	.11	.057	2	62	.17	12	.15	2	6.54	.01	.02	2	20
L26+00W 6+75N	2	64	4	49	.1	18	7	131	5.32	63	5	ND	1	4	1	4	2	137	.22	.020	3	42	.24	21	.12	2	2.69	.01	.02	2	3
L26+00W 6+50N	2	57	12	33	.2	10	4	90	7.15	91	5	ND	1	3	1	4	2	179	.12	.026	3	48	.11	11	.17	2	2.70	.01	.02	1	17
L26+00W 6+25N	15	153	10	68	.3	21	11	180	6.94	179	5	ND	1	10	1	5	2	172	.26	.029	3	59	.27	27	.18	2	4.36	.01	.03	1	22
L26+00W 6+00N	9	192	11	70	.2	26	11	255	5.93	157	5	ND	1	5	1	7	2	130	.18	.025	3	60	.37	35	.14	4	5.55	.01	.03	1	18
L26+00W 5+75N	2	157	6	72	.1	33	14	243	7.46	129	5	ND	1	5	1	5	2	148	.21	.026	4	71	.35	21	.14	2	4.45	.01	.02	1	7
L26+00W 5+50N	3	193	13	75	.3	32	13	254	5.53	181	5	ND	1	6	1	9	2	108	.22	.040	3	53	.48	44	.14	2	4.97	.01	.04	1	12
L26+00W 5+25N	5	195	13	100	.3	36	13	300	5.29	193	5	ND	1	5	1	9	2	102	.22	.035	3	55	.49	45	.12	2	5.16	.01	.05	1	28
L26+00W 5+00N	10	157	22	87	.3	37	17	247	5.89	161	5	ND	1	6	1	8	2	131	.22	.035	4	57	.43	56	.07	3	4.42	.01	.04	1	15
L26+00W 4+75N	12	113	14	46	.5	20	7	120	5.22	160	5	ND	1	5	1	9	2	123	.14	.031	4	43	.21	24	.10	2	3.50	.01	.03	3	41
L26+00W 4+50N	1	142	18	88	.5	25	9	164	5.57	185	5	ND	1	5	1	8	2	124	.21	.035	3	56	.32	30	.14	5	4.43	.01	.03	1	29
L26+00W 4+25N	3	145	7	50	.5	24	9	156	4.42	138	5	ND	1	6	1	7	2	106	.27	.033	3	40	.38	26	.16	4	3.36	.01	.03	1	12
L26+00W 4+00N	2	181	10	71	.3	33	9	161	5.70	174	5	ND	1	5	1	8	2	98	.20	.048	2	63	.41	30	.14	2	5.35	.01	.03	2	11
L26+00W 3+75N	7	149	9	49	.7	24	12	150	5.15	198	5	ND	1	6	1	7	2	116	.22	.030	4	46	.34	31	.12	3	4.03	.01	.04	2	19
L26+00W 3+50N	3	100	17	59	.6	17	6	100	6.83	154	5	ND	1	5	1	4	2	141	.15	.070	3	59	.22	21	.18	2	5.01	.01	.04	1	56
L24+50W 15+00N	1	85	18	71	.1	24	10	353	9.10	35	5	ND	2	5	1	5	2	192	.35	.099	3	75	.37	25	.23	2	4.60	.01	.03	1	1
L24+50W 14+75N	1	138	15	88	.1	41	20	912	7.03	49	5	ND	1	5	1	5	2	153	.38	.071	3	68	.57	38	.15	2	5.43	.01	.04	1	122
L24+50W 14+50N	1	124	12	84	.2	44	18	392	6.72	47	5	ND	1	6	1	5	2	156	.39	.034	4	70	.66	55	.13	2	4.71	.01	.04	1	5
L24+50W 14+25N	1	33	12	60	.1	30	11	261	6.58	43	5	ND	1	6	1	2	2	154	.39	.037	3	60	.47	25	.13	2	3.70	.01	.02	1	3
L24+50W 14+00N	1	20	10	31	.1	10	4	146	5.51	22	5	ND	1	6	1	3	2	162	.23	.036	3	37	.10	12	.26	2	1.54	.01	.02	1	260
L24+50W 13+75N	1	168	15	111	.1	55	26	357	7.47	49	5	ND	1	5	1	4	2	172	.29	.065	4	79	.65	58	.13	2	5.04	.01	.05	1	2
L24+50W 13+50N	1	83	12	57	.2	27	10	202	5.87	37	5	ND	1	5	1	4	2	156	.28	.023	3	57	.34	26	.18	4	3.47	.01	.02	1	12
L24+50W 13+25N	1	102	22	75	.1	27	10	255	6.09	23	5	ND	1	5	1	5	2	146	.30	.071	3	65	.30	24	.17	4	5.10	.01	.03	1	1
L24+50W 13+00N	1	190	12	105	.1	49	17	247	5.80	51	5	ND	1	5	1	5	2	127	.32	.032	2	70	.62	46	.15	3	5.88	.01	.04	1	1
L24+50W 12+75N	1	67	10	66	.1	24	20	558	6.40	76	5	ND	1	8	1	3	2	163	.51	.075	4	55	.40	25	.29	2	2.70	.01	.03	1	8
STD C/AU-S	18	59	42	132	5.7	67	29	1055	4.09	41	21	7	36	47	18	17	21	58	.48	.095	38	55	.90	171	.07	38	1.97	.06	.14	11	47

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5601

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L24+50W 12+50N	1	130	2	85	.1	42	13	297	5.21	60	5	ND	1	7	1	2	2	123	.44	.020	3	54	.83	52	.28	2	3.65	.01	.03	1	2
L24+50W 12+25N	1	79	7	72	.2	27	12	176	6.11	48	5	ND	1	6	1	2	2	164	.36	.020	3	55	.38	32	.24	2	3.14	.01	.03	1	1
L24+50W 11+50N	5	335	6	62	.5	22	8	133	5.53	266	5	ND	2	6	1	6	2	112	.13	.032	5	45	.40	36	.12	3	5.24	.01	.04	1	51
L24+50W 11+25N	1	109	12	92	.2	37	16	244	5.91	59	5	ND	1	6	1	4	2	140	.31	.026	2	58	.51	47	.14	2	4.47	.01	.03	1	11
L24+50W 11+00N	1	189	11	92	.5	39	16	273	5.57	65	5	ND	1	6	1	4	2	125	.24	.059	2	57	.66	46	.08	4	5.21	.01	.05	1	7
L24+50W 10+75N	1	133	7	108	.3	50	23	290	6.31	48	5	ND	1	6	1	4	2	146	.34	.024	4	57	.65	46	.12	2	4.63	.01	.04	1	5
L24+50W 10+50N	1	85	7	82	.1	31	17	211	6.30	35	5	ND	1	4	1	2	2	151	.19	.033	4	56	.34	43	.09	2	3.74	.01	.03	1	2
L24+50W 10+25N	1	106	16	79	.3	36	19	271	6.52	50	5	ND	1	6	1	2	2	167	.22	.024	5	68	.40	53	.13	2	4.13	.01	.05	1	1
L24+50W 10+00N	1	148	11	95	.3	45	17	269	6.40	62	5	ND	1	4	1	2	2	142	.27	.031	3	64	.69	62	.10	4	4.71	.01	.05	1	5
L24+50W 9+75N	1	143	9	95	.2	48	22	259	6.18	44	5	ND	1	6	1	2	2	128	.23	.021	4	69	.65	66	.04	3	4.86	.01	.05	1	3
L24+50W 9+50N	1	131	12	51	.3	18	7	97	6.22	124	5	ND	1	4	1	4	2	149	.18	.026	2	60	.22	22	.17	2	4.67	.01	.03	3	27
L24+50W 9+25N	1	157	9	43	1.6	13	7	103	4.73	97	5	ND	1	5	1	6	2	103	.14	.054	2	42	.31	15	.15	3	4.96	.01	.02	3	20
L24+50W 9+00N	1	66	9	65	.4	20	8	120	6.05	62	5	ND	2	5	1	2	2	136	.24	.044	3	46	.31	20	.24	4	3.74	.01	.02	1	3
L24+50W 8+50N	2	80	12	95	.5	25	49	917	4.37	46	5	ND	1	8	1	5	2	136	.21	.060	6	74	.32	43	.13	3	5.12	.01	.05	1	16
L24+50W 8+25N	1	85	2	51	.2	21	9	151	5.93	59	5	ND	1	5	1	2	2	145	.21	.029	4	48	.27	25	.12	2	3.19	.01	.03	1	13
L24+50W 7+50N	1	113	7	68	.2	22	15	331	5.39	80	5	ND	1	8	1	5	2	137	.39	.026	4	52	.49	46	.14	3	3.41	.01	.04	1	23
L24+50W 7+25N	2	52	5	47	.1	19	11	136	5.16	69	5	ND	1	5	1	2	2	154	.16	.029	5	38	.24	31	.25	2	2.66	.01	.02	1	58
L24+50W 7+00N	1	156	13	73	.2	34	14	194	5.80	94	5	ND	1	5	1	5	2	152	.18	.055	4	61	.39	39	.10	2	4.80	.01	.04	1	16
L24+50W 6+75N	1	53	8	45	.1	15	7	150	6.22	55	5	ND	1	4	1	4	2	156	.16	.031	4	46	.27	21	.12	2	2.29	.01	.03	1	2
L24+50W 6+50N	1	129	6	79	.4	25	15	214	5.15	83	5	ND	1	5	1	7	2	129	.22	.024	3	55	.46	43	.13	7	4.14	.01	.05	1	8
L24+50W 6+25N	10	106	11	40	.4	17	21	215	3.81	109	5	ND	1	5	1	7	2	75	.14	.019	3	32	.29	30	.11	9	3.67	.01	.03	2	12
L24+50W 5+50N	2	113	15	53	.5	22	9	142	7.27	164	5	ND	1	6	1	8	2	185	.23	.051	3	54	.32	23	.27	2	3.51	.01	.03	1	9
L24+50W 5+25N	1	193	13	84	.3	44	17	254	5.39	145	5	ND	1	7	1	8	2	120	.26	.042	4	56	.65	53	.16	4	4.97	.01	.05	1	34
L24+50W 5+00N	2	176	18	90	.9	47	13	255	5.21	165	5	ND	1	8	1	6	2	115	.19	.044	4	65	.71	59	.09	2	5.25	.01	.06	2	21
L24+50W 4+75N	1	164	9	66	.4	38	14	243	4.96	153	5	ND	1	8	1	6	2	114	.28	.029	4	51	.69	49	.14	2	3.80	.01	.05	1	24
L24+50W 4+50N	1	113	7	59	.2	31	12	403	4.57	106	5	ND	1	9	1	5	2	107	.32	.028	4	45	.75	44	.14	2	2.72	.01	.04	1	19
L24+50W 4+25N	3	202	18	76	.2	44	18	252	5.47	148	5	ND	1	6	1	5	3	112	.24	.054	4	57	.71	59	.14	2	4.83	.01	.06	1	280
L24+50W 4+00N	1	137	3	74	.4	34	12	178	4.37	125	5	ND	1	6	1	7	2	102	.25	.060	4	55	.43	35	.11	3	4.72	.01	.04	1	9
L24+50W 3+75N	1	198	20	67	.4	37	19	476	4.39	163	5	ND	1	11	1	10	2	111	.32	.039	5	51	.76	50	.19	6	3.67	.01	.07	2	47
L24+50W 3+50N	2	36	12	42	.1	18	8	143	4.30	132	5	ND	1	5	1	5	2	141	.17	.019	5	33	.26	20	.16	4	2.50	.01	.03	2	11
L23+00W 15+00N	1	83	12	100	.4	37	18	398	6.12	37	5	ND	1	7	1	4	2	161	.45	.052	3	54	.42	24	.26	6	3.60	.01	.03	1	8
L23+00W 14+75N	1	116	14	66	.4	32	14	364	5.58	55	5	ND	2	7	1	5	2	127	.41	.032	3	52	.49	24	.23	8	4.19	.01	.03	1	66
L23+00W 14+50N	1	98	16	81	.2	32	15	419	5.25	46	5	ND	1	8	1	3	2	135	.48	.038	4	51	.47	37	.24	3	3.70	.01	.03	1	18
L23+00W 14+25N	1	95	15	88	.2	32	16	393	5.95	42	5	ND	1	7	1	4	2	148	.48	.064	3	55	.51	32	.27	3	3.90	.01	.03	2	2
L23+00W 14+00N	1	78	10	69	.3	30	14	305	6.71	38	5	ND	1	7	1	4	2	175	.42	.058	3	59	.40	31	.28	2	3.48	.01	.03	1	3
L23+00W 13+75N	1	100	7	67	.1	30	15	316	5.71	38	5	ND	1	8	1	2	2	152	.51	.027	4	50	.44	28	.33	5	3.59	.01	.03	1	2
STD C/AU-S	19	58	42	132	6.6	68	29	1038	3.96	40	19	7	36	47	17	20	23	58	.47	.093	38	56	.94	175	.06	34	1.83	.06	.14	12	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L23+00W 13+25N	2	107	9	66	.2	35	16	210	7.50	584	5	ND	2	5	1	2	2	166	.34	.055	2	71	.47	25	.18	3	4.37	.01	.03	1	12
L23+00W 13+00N	1	67	12	61	.2	24	10	142	6.65	41	5	ND	2	6	1	2	2	196	.32	.027	3	59	.28	20	.36	4	3.71	.01	.02	1	5
L23+00W 12+75N	1	71	12	76	.4	25	12	164	5.78	306	5	ND	1	5	1	2	2	168	.35	.022	3	48	.30	22	.28	5	3.05	.01	.02	1	9
L23+00W 12+00N	1	107	13	77	.5	35	18	261	6.64	765	5	ND	1	6	1	4	2	152	.53	.025	3	57	.52	23	.32	5	3.47	.01	.03	2	4
L23+00W 11+75N	1	84	11	40	.3	14	7	87	5.09	69	5	ND	2	4	1	2	2	134	.20	.024	3	42	.16	17	.20	5	3.53	.01	.02	2	24
L23+00W 11+25N	1	84	11	66	.4	31	13	318	6.49	50	5	ND	1	5	1	3	2	157	.31	.027	3	59	.40	25	.10	6	3.35	.01	.03	1	11
L23+00W 10+50N	1	184	16	97	.3	64	24	309	8.75	89	5	ND	2	6	1	3	2	192	.18	.056	3	83	.72	97	.10	4	5.44	.01	.07	1	13
L23+00W 10+25N	1	62	7	44	.2	19	9	149	6.52	45	5	ND	1	4	1	2	2	181	.25	.019	3	50	.26	21	.14	2	2.57	.01	.02	1	33
L23+00W 10+00N	1	135	12	92	.3	43	17	255	7.34	74	5	ND	2	6	1	3	2	180	.36	.059	3	62	.54	56	.23	4	4.23	.01	.05	1	17
L23+00W 9+75N	1	66	12	44	.5	13	6	105	7.30	53	5	ND	1	4	1	2	2	173	.23	.048	2	54	.20	18	.23	4	3.79	.01	.02	1	5
L23+00W 9+50N	1	124	12	65	.4	28	12	164	6.13	69	5	ND	2	4	1	3	2	137	.29	.055	2	64	.37	22	.19	3	5.17	.01	.03	2	8
L23+00W 9+25N	1	71	12	60	.3	22	9	144	5.71	47	5	ND	1	4	1	2	2	163	.22	.032	3	52	.23	23	.14	4	3.34	.01	.02	1	2
L23+00W 9+00N	1	137	12	125	.4	44	20	215	7.48	53	5	ND	2	4	1	2	2	170	.24	.061	3	75	.44	37	.11	3	4.23	.01	.04	1	1
L23+00W 8+75N	1	51	16	41	.3	15	7	122	7.41	65	5	ND	1	4	1	4	2	213	.24	.031	3	49	.17	13	.26	4	2.06	.01	.03	2	1
L23+00W 8+50N	3	122	6	73	.4	36	19	373	5.39	99	5	ND	1	5	1	5	2	148	.31	.031	4	51	.52	37	.12	3	3.45	.01	.04	2	1
L23+00W 8+25N	1	72	7	59	.3	23	11	220	6.00	51	5	ND	1	5	1	2	2	155	.30	.023	3	47	.24	26	.19	2	3.03	.01	.02	1	2
L23+00W 8+00N	1	98	16	74	.3	33	13	262	6.73	98	5	ND	1	5	1	2	2	160	.30	.032	4	60	.41	40	.11	3	3.62	.01	.04	1	16
L23+00W 7+50N	1	181	8	93	.4	48	19	255	6.05	81	5	ND	2	5	1	2	2	123	.22	.029	3	67	.64	71	.04	5	4.91	.01	.05	1	2
L23+00W 7+25N	1	121	13	82	.3	41	16	263	7.46	97	5	ND	1	4	1	3	2	167	.22	.031	4	74	.52	40	.09	4	4.32	.01	.04	1	1
L23+00W 7+00N	1	105	12	46	.4	18	5	123	7.56	101	5	ND	1	4	1	3	2	172	.16	.029	4	62	.17	16	.13	2	3.30	.01	.02	2	1
L23+00W 6+75N	1	83	13	52	.5	22	9	128	6.96	102	5	ND	1	5	1	4	2	136	.20	.054	3	63	.20	19	.12	5	3.89	.01	.03	3	3
L21+50W 15+00N	1	70	21	69	.3	28	15	262	6.34	32	5	ND	1	7	1	2	2	158	.48	.032	3	50	.35	23	.36	3	2.91	.01	.03	1	1
L21+50W 14+75N	3	73	14	89	.5	36	18	1066	5.77	50	5	ND	1	9	1	3	2	159	.55	.031	3	54	.52	45	.33	5	3.17	.01	.03	1	1
L21+50W 14+50N	5	40	13	59	.4	24	11	229	6.51	56	5	ND	1	6	1	2	2	177	.43	.025	3	53	.24	22	.34	5	2.66	.01	.02	1	1
L21+50W 14+25N	4	65	14	49	.4	27	14	416	5.26	43	5	ND	1	11	1	2	2	146	.71	.030	3	46	.44	23	.36	5	2.64	.01	.03	1	2
L21+50W 14+00N	1	73	5	60	.4	31	14	251	5.00	40	5	ND	1	5	1	2	2	133	.56	.022	3	47	.45	30	.26	6	2.90	.01	.03	1	1
L21+50W 13+75N	1	51	2	53	.2	24	11	178	5.01	20	5	ND	2	5	1	2	2	144	.33	.025	3	44	.27	29	.21	7	2.39	.01	.02	1	4
L21+50W 13+50N	1	46	12	54	.2	21	10	206	4.36	27	5	ND	1	6	1	2	2	122	.43	.029	3	41	.26	25	.14	5	2.71	.01	.02	1	1
L21+50W 13+25N	1	59	13	54	.4	25	10	227	6.39	36	5	ND	1	7	1	2	2	166	.39	.032	3	55	.24	24	.23	4	3.03	.01	.02	1	1
L21+50W 13+00N	1	157	11	94	.6	63	27	568	6.97	76	5	ND	2	6	1	3	2	169	.40	.072	5	74	.68	56	.28	8	5.14	.01	.05	1	2
L21+50W 12+75N	1	134	5	103	.3	46	20	357	6.91	51	5	ND	1	6	1	2	2	162	.43	.040	4	71	.59	53	.21	3	4.21	.01	.03	1	1
L21+50W 12+50N	1	68	10	46	.4	20	8	149	5.07	41	5	ND	1	5	1	2	2	143	.33	.025	3	43	.22	21	.24	6	2.95	.01	.02	2	1
L21+50W 12+25N	1	47	9	34	.4	17	7	136	4.76	31	5	ND	2	5	1	2	2	146	.33	.013	3	42	.23	19	.20	4	2.13	.01	.02	1	4
L21+50W 12+00N	1	228	16	64	.8	19	8	124	4.90	87	5	ND	1	5	1	2	2	93	.18	.035	2	41	.33	15	.12	4	4.59	.01	.02	3	39
L21+50W 11+75N	2	94	10	62	.4	23	11	200	4.92	42	5	ND	2	5	1	2	2	131	.29	.023	3	46	.29	26	.14	6	3.09	.01	.03	2	4
L21+50W 11+50N	1	104	8	62	.3	34	13	231	5.48	53	5	ND	1	5	1	2	2	135	.36	.021	3	52	.40	88	.14	4	3.24	.01	.03	1	20
STD C/AU-S	19	59	41	131	7.2	73	31	1017	4.16	39	18	7	37	47	19	16	20	60	.48	.095	37	57	.91	180	.07	35	1.91	.06	.15	12	52

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5601

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L21+50W 11+00N	4	452	20	83	.2	31	12	142	4.19	458	5	ND	1	6	1	4	4	86	.13	.021	3	43	.50	39	.09	2	5.35	.01	.04	1	48
L21+50W 10+75N	1	178	14	95	.1	35	14	363	5.27	96	5	ND	1	5	1	6	2	143	.27	.033	2	54	.41	29	.21	2	5.13	.01	.03	1	10
L21+50W 10+50N	1	90	10	59	.1	23	10	218	5.55	62	5	ND	1	5	1	4	3	172	.24	.023	3	46	.25	20	.19	2	3.29	.01	.03	1	1
L21+50W 10+25N	1	145	8	79	.1	39	14	236	7.87	106	5	ND	1	5	1	2	2	208	.27	.043	3	81	.45	29	.32	2	5.99	.01	.03	1	1
L21+50W 10+00N	1	152	16	102	.1	48	19	315	6.37	91	5	ND	1	6	1	5	2	171	.30	.027	3	69	.58	69	.14	4	5.26	.01	.04	1	13
L21+50W 9+75N	1	34	4	96	.1	31	12	220	5.40	107	5	ND	1	8	1	2	2	150	.33	.023	4	50	.46	35	.15	2	3.05	.01	.34	1	15
L21+50W 9+25N	1	152	11	92	.1	47	15	229	5.94	93	5	ND	1	5	1	6	4	151	.26	.025	3	70	.56	38	.15	2	4.99	.01	.03	1	2
L21+50W 9+00N	1	72	5	63	.1	24	9	171	5.63	67	5	ND	1	6	1	4	2	164	.31	.027	4	49	.31	27	.14	2	2.99	.01	.03	1	14
L21+50W 8+75N	1	79	8	59	.1	23	7	141	6.20	64	5	ND	1	5	1	3	2	181	.21	.040	3	51	.26	25	.18	2	3.02	.01	.02	1	1
L21+50W 8+50N	1	62	10	51	.1	18	7	231	7.27	81	5	ND	1	5	1	2	2	213	.22	.038	3	50	.20	20	.21	2	2.50	.01	.03	1	1
L21+50W 8+25N	1	148	8	78	.1	39	21	792	5.18	84	5	ND	1	11	1	2	3	141	.47	.037	6	56	.59	46	.16	3	3.76	.01	.05	1	1
L21+50W 8+00N	1	97	12	52	.1	25	10	251	5.26	108	5	ND	1	5	1	5	2	189	.23	.033	4	50	.32	29	.19	2	3.17	.01	.03	2	1
L21+50W 7+75N	1	147	11	102	.2	49	19	270	5.90	106	5	ND	2	5	1	5	2	149	.26	.028	5	64	.62	61	.11	4	5.38	.01	.05	1	3
L21+50W 7+25N	6	151	16	52	.4	21	8	116	4.20	167	5	ND	1	5	1	10	2	126	.15	.020	5	46	.23	29	.15	3	5.03	.01	.03	1	12
L21+50W 7+00N	8	184	9	45	.5	20	7	97	6.09	205	5	ND	1	4	1	8	4	159	.11	.020	3	60	.26	24	.20	2	5.94	.01	.03	1	29
L21+50W 6+25N	1	152	13	77	.1	33	12	213	6.22	212	5	ND	1	6	1	9	2	164	.21	.054	4	63	.41	37	.15	2	5.41	.01	.03	2	16
L21+50W 6+00N	1	93	10	59	.1	21	7	114	5.76	192	5	ND	1	4	1	6	3	171	.19	.025	4	54	.22	21	.19	2	3.79	.01	.02	1	19
L21+50W 5+75N	3	171	17	77	.3	36	11	219	6.87	237	5	ND	1	6	1	6	5	159	.23	.031	3	65	.39	41	.19	2	5.59	.01	.03	1	28
L21+50W 5+50N	2	159	11	64	.1	31	11	195	5.10	133	5	ND	1	6	1	10	4	129	.23	.018	4	53	.47	44	.28	2	4.38	.01	.03	1	19
L20+00W 15+00N	1	109	10	78	.1	41	24	795	5.35	59	5	ND	1	16	1	2	2	141	.63	.026	5	59	.67	49	.15	2	3.39	.01	.05	1	1
L20+00W 14+75N	1	108	8	69	.1	37	19	594	4.85	56	5	ND	1	13	1	2	2	139	.65	.029	4	55	.63	42	.21	2	3.12	.01	.04	1	8
L20+00W 14+50N	1	108	6	75	.1	39	18	638	5.00	62	5	ND	1	13	1	2	3	143	.60	.033	4	57	.60	47	.21	5	3.47	.01	.04	1	6
L20+00W 14+00N	1	103	11	78	.1	39	18	521	5.13	61	5	ND	1	10	1	3	2	147	.54	.030	5	55	.59	45	.21	2	3.53	.01	.04	1	1
L20+00W 13+75N	1	79	10	39	.1	41	19	380	5.56	54	5	ND	1	7	1	4	2	158	.44	.036	4	63	.47	41	.19	4	3.92	.01	.04	1	1
L20+00W 13+50N	1	87	12	81	.2	39	18	400	4.79	53	5	ND	1	9	1	5	2	142	.49	.032	5	56	.55	45	.19	2	3.88	.01	.04	1	24
L20+00W 13+25N	1	121	11	75	.1	36	15	296	5.60	67	5	ND	1	8	1	2	2	150	.45	.041	3	57	.45	39	.24	2	4.34	.01	.03	1	13
L20+00W 13+00N	1	72	16	52	.2	25	10	205	4.51	65	5	ND	1	7	1	4	2	146	.33	.025	3	44	.33	28	.18	2	2.94	.01	.03	1	5
L20+00W 12+75N	1	114	18	64	.3	27	12	441	4.39	83	5	ND	1	12	1	5	2	129	.41	.064	3	43	.32	33	.25	3	3.37	.01	.05	1	5
L20+00W 12+50N	1	115	16	64	.2	32	14	307	5.16	86	5	ND	1	7	1	3	2	150	.29	.022	4	50	.43	38	.16	2	3.66	.01	.03	1	8
L20+00W 12+25N	1	167	11	62	.2	34	17	535	4.59	102	5	ND	2	8	1	5	2	129	.39	.034	4	49	.57	37	.19	4	3.84	.01	.04	1	215
L20+00W 12+00N	1	63	14	44	.2	18	8	204	4.25	50	5	ND	1	6	1	3	2	142	.32	.023	3	37	.25	20	.21	2	2.53	.01	.02	2	17
L20+00W 11+75N	1	154	13	75	.1	56	23	316	5.87	84	5	ND	1	5	1	3	2	168	.50	.020	4	68	.76	68	.25	2	5.43	.01	.05	1	3
L20+00W 11+50N	1	123	10	63	.1	43	20	356	5.15	101	5	ND	1	13	1	3	2	155	.50	.017	4	59	.57	55	.21	2	4.17	.01	.03	1	1
L20+00W 11+25N	1	147	16	66	.3	35	15	195	5.32	35	5	ND	1	5	1	4	2	151	.27	.025	3	53	.40	31	.27	5	5.23	.01	.03	1	1
L20+00W 11+00N	1	103	11	72	.1	35	13	221	5.63	74	5	ND	1	5	1	2	4	150	.30	.023	3	58	.49	33	.15	2	3.98	.01	.03	1	1
L20+00W 10+50N	2	222	25	120	.2	64	23	166	6.65	100	5	ND	2	5	1	3	4	174	.18	.056	3	85	.41	77	.14	4	7.20	.01	.04	1	4
STD C/AU-S	20	62	45	133	7.4	72	30	1036	3.94	39	21	8	39	51	19	19	21	64	.46	.096	42	58	.90	180	.07	36	2.00	.06	.25	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L20+00W 10+25N	2	57	9	48	.1	17	12	203	4.22	33	5	ND	1	5	1	2	2	111	.31	.016	4	31	.31	24	.12	2	2.19	.01	.03	1	3
L20+00W 10+00N	1	110	7	76	.1	33	15	565	5.15	57	5	ND	2	7	1	2	2	125	.32	.026	4	46	.52	55	.13	2	3.33	.01	.02	1	4
L20+00W 9+75N	1	108	6	58	.1	41	24	564	6.12	77	5	ND	1	6	1	2	2	149	.28	.038	4	60	.53	51	.11	2	4.29	.01	.04	1	7
L20+00W 9+50N	1	80	3	63	.1	25	11	209	5.79	53	5	ND	1	5	1	3	2	156	.21	.026	4	45	.33	33	.14	2	3.21	.01	.03	1	2
L20+00W 9+25N	1	103	9	59	.1	35	15	440	6.75	65	5	ND	1	4	1	2	2	136	.23	.031	3	53	.40	43	.10	2	4.08	.01	.03	1	5
L20+00W 9+00N	1	74	10	54	.1	23	10	279	4.36	315	5	ND	1	9	1	2	2	117	.32	.026	4	38	.34	54	.12	2	2.31	.01	.03	1	3
L20+00W 8+75N	1	63	7	50	.1	16	6	327	6.45	56	5	ND	2	4	1	2	2	165	.23	.034	2	46	.18	20	.21	2	2.61	.01	.02	2	1
L20+00W 8+50N	1	139	3	92	.1	39	17	286	5.73	63	5	ND	2	6	1	2	2	128	.29	.026	3	54	.63	70	.11	2	4.16	.01	.02	1	8
L20+00W 8+25N	1	126	5	70	.1	23	13	346	5.31	61	5	ND	1	5	1	2	2	134	.25	.027	5	49	.41	39	.13	2	3.62	.01	.03	1	11
L20+00W 8+00N	1	141	9	75	.3	30	14	270	5.30	76	5	ND	2	4	1	4	2	128	.25	.037	3	47	.44	31	.10	3	4.09	.01	.04	1	9
L20+00W 7+75N	1	105	9	70	.1	29	23	377	5.07	62	5	ND	1	5	1	2	2	116	.27	.024	4	44	.49	41	.11	2	3.25	.01	.03	1	3
L20+00W 7+50N	1	120	11	38	.1	37	16	439	7.30	99	5	ND	2	4	1	4	2	169	.16	.062	3	62	.41	54	.13	2	4.67	.01	.04	2	6
L20+00W 7+25N	2	96	14	52	.1	19	7	154	5.52	103	5	ND	2	8	1	4	2	130	.28	.026	3	49	.25	30	.10	2	3.76	.01	.04	1	12
L20+00W 7+00N	1	134	8	59	.3	25	9	168	5.25	135	5	ND	2	4	1	6	2	122	.17	.024	3	49	.34	31	.11	2	3.93	.01	.03	1	14
L20+00W 6+75N	2	111	22	49	.2	18	7	157	7.55	109	5	ND	2	4	1	2	2	174	.17	.028	3	60	.23	21	.14	2	3.34	.01	.03	1	6
L20+00W 6+25N	8	217	12	56	.4	25	10	171	4.44	225	5	ND	2	6	1	4	2	90	.20	.063	4	42	.44	39	.12	2	4.16	.01	.05	2	48
L20+00W 5+75N	2	122	12	58	.2	20	8	163	6.11	154	5	ND	1	4	1	4	2	130	.18	.026	3	52	.30	22	.15	2	4.20	.01	.03	1	57
L20+00W 5+50N	1	146	10	65	.1	35	15	254	5.61	58	5	ND	1	5	1	4	2	115	.24	.016	4	56	.56	61	.03	2	3.97	.01	.03	1	6
L20+00W 5+25N	2	87	12	43	.1	16	7	124	4.66	111	5	ND	1	4	1	4	2	135	.15	.025	4	33	.20	22	.12	2	2.72	.01	.03	1	48
L20+00W 5+00N	4	48	8	31	.1	13	5	120	5.04	113	5	ND	1	4	1	4	2	140	.15	.019	4	34	.20	19	.12	2	1.87	.01	.02	2	10
L20+00W 4+50N	6	76	12	48	.2	17	7	177	5.92	267	5	ND	1	14	1	5	2	141	.32	.022	4	40	.24	31	.12	2	2.56	.01	.03	1	23
L20+00W 4+25N	2	144	12	59	.3	20	8	156	5.30	161	5	ND	2	6	1	6	2	119	.21	.038	3	45	.36	22	.20	4	3.99	.01	.03	2	21
L20+00W 4+00N	2	163	14	59	.7	25	10	381	4.70	179	5	ND	2	7	1	6	2	93	.26	.060	3	43	.39	26	.13	3	4.15	.01	.03	2	3
L20+00W 3+75N	2	143	11	53	.3	21	8	149	4.44	140	5	ND	1	5	1	3	2	103	.18	.061	3	38	.30	25	.13	2	3.93	.01	.03	1	57
L20+00W 3+50N	2	139	11	62	.5	27	11	221	5.04	162	5	ND	1	6	1	5	2	111	.22	.065	5	46	.43	39	.15	2	4.71	.01	.04	1	135
L18+50W 15+00N	1	77	7	59	.2	23	10	201	6.10	43	5	ND	2	5	1	2	2	160	.35	.035	3	50	.38	27	.28	3	3.60	.01	.03	2	7
L18+50W 14+75N	1	75	11	61	.3	27	11	193	6.25	42	5	ND	2	7	1	2	2	163	.27	.026	3	50	.34	34	.14	2	3.30	.01	.04	1	1
L18+50W 14+50N	1	62	3	67	.1	20	9	154	5.73	37	5	ND	2	5	1	4	2	155	.32	.034	3	45	.27	21	.27	2	2.89	.01	.03	1	4
L18+50W 14+00N	1	42	12	52	.2	15	7	166	4.34	29	5	ND	2	6	1	2	2	154	.38	.025	3	37	.23	34	.21	3	1.91	.01	.03	1	9
L18+50W 13+75N	1	20	4	28	.1	10	5	126	3.57	16	5	ND	2	5	1	2	2	125	.35	.020	3	28	.19	12	.16	4	1.29	.01	.02	1	65
L18+50W 13+50N	1	54	5	63	.1	20	10	217	4.59	28	5	ND	2	5	1	2	2	145	.31	.024	3	38	.29	29	.17	3	2.32	.01	.02	1	19
L18+50W 13+25N	1	93	11	81	.3	39	14	299	5.55	46	5	ND	2	6	1	2	2	134	.39	.034	3	54	.59	48	.19	4	3.75	.01	.05	1	5
L18+50W 13+00N	1	73	7	55	.1	24	12	242	3.91	32	5	ND	2	5	1	2	2	112	.38	.032	3	39	.42	36	.15	4	2.69	.02	.06	1	14
L18+50W 12-75N	1	42	6	41	.2	15	7	161	3.38	23	5	ND	2	6	1	2	2	107	.38	.014	3	30	.30	17	.14	5	1.91	.01	.02	1	6
L18+50W 12-50N	1	113	7	77	.1	31	15	239	4.40	36	5	ND	1	6	1	2	2	101	.33	.024	3	45	.51	37	.11	2	3.37	.01	.03	1	7
L18+50W 12-25N	1	64	12	65	.1	24	11	233	4.33	22	5	ND	2	7	1	2	2	111	.55	.018	3	40	.45	23	.09	6	2.49	.01	.03	1	3
STD C/AU-S	18	57	38	132	7.1	67	29	1032	3.90	42	23	7	36	47	18	16	19	57	.46	.092	38	56	.81	174	.06	36	1.91	.06	.13	11	47

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-5601

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L18+50W 12+00N	1	77	3	57	.1	23	12	365	4.72	24	5	ND	1	6	1	2	2	128	.43	.034	2	48	.42	31	.16	3	2.77	.01	.07	1	17
L18+50W 11+75N	1	68	9	59	.1	20	3	299	5.93	23	5	ND	1	6	1	2	2	142	.46	.036	3	44	.28	23	.27	3	3.05	.01	.03	1	22
L18+50W 11+50N	1	103	6	51	.1	14	5	85	4.61	48	5	ND	1	5	1	2	2	117	.14	.078	2	35	.19	16	.12	3	3.20	.01	.02	2	35
L18+50W 11+25N	1	39	10	41	.1	10	4	319	4.32	23	5	ND	1	6	1	2	3	175	.20	.031	3	44	.18	22	.40	3	1.58	.01	.03	2	40
L18+50W 11+00N	1	69	10	52	.1	25	11	187	4.62	28	5	ND	1	7	1	2	3	141	.46	.013	4	46	.38	30	.23	2	2.93	.01	.02	1	4
L18+50W 10+75N	1	132	11	91	.1	44	19	242	6.34	64	6	ND	1	5	1	2	2	162	.26	.025	5	64	.54	73	.16	2	4.52	.01	.03	1	6
L18+50W 10+50N	1	70	6	40	.1	17	7	139	4.81	45	5	ND	1	3	1	2	3	125	.23	.025	3	38	.26	14	.10	2	2.27	.01	.02	2	5
L18+50W 10+25N	1	63	8	51	.1	14	6	120	6.69	49	5	ND	1	3	1	2	3	176	.31	.029	2	49	.22	20	.27	2	3.17	.01	.02	1	39
L18+50W 10+00N	1	126	5	81	.1	37	19	242	5.03	46	5	ND	1	5	1	2	2	129	.27	.013	3	53	.40	39	.15	2	4.06	.01	.03	1	6
L18+50W 9+50N	1	91	8	51	.1	18	8	147	6.02	79	5	ND	1	4	1	2	3	157	.19	.072	2	51	.25	15	.26	2	3.83	.01	.01	2	19
L18+50W 9+25N	1	139	6	74	.1	34	14	230	5.31	56	5	ND	1	5	1	2	2	123	.34	.027	3	51	.52	35	.16	2	3.80	.01	.02	1	23
L18+50W 8+75N	1	112	6	82	.2	34	15	254	7.29	81	5	ND	1	4	1	2	2	182	.22	.032	4	65	.45	43	.12	4	4.25	.01	.03	1	11
L18+50W 8+50N	1	95	8	69	.1	26	21	214	5.52	59	5	ND	1	4	1	2	2	133	.27	.020	3	56	.37	22	.11	4	3.69	.01	.02	1	2
L18+50W 8+25N	2	120	12	84	.1	38	17	225	5.64	85	5	ND	1	4	1	2	4	134	.26	.023	3	54	.45	34	.13	3	4.48	.01	.03	1	15
L18+50W 7+75N	4	90	2	38	.1	15	6	84	2.97	110	5	ND	1	3	1	2	2	75	.12	.015	2	26	.21	36	.09	3	2.42	.01	.01	1	230
L18+50W 7+50N	5	103	11	66	.1	25	9	144	5.96	103	6	ND	2	4	1	2	3	122	.15	.024	2	48	.33	35	.12	4	4.06	.01	.03	2	12
L18+50W 7+25N	2	122	9	67	.3	26	10	166	5.91	75	5	ND	1	4	1	2	2	145	.18	.030	3	50	.33	35	.15	5	4.21	.01	.03	1	9
L18+50W 7+00N	5	73	7	46	.1	19	8	165	5.09	102	5	ND	1	4	1	2	2	140	.18	.025	3	35	.24	26	.13	3	2.59	.01	.02	2	36
L18+50W 6+75N	4	143	3	63	.1	28	11	192	4.73	64	5	ND	1	3	1	2	2	101	.17	.022	2	42	.40	37	.12	2	4.30	.01	.02	1	19
L18+50W 6+50N	9	175	10	62	.2	24	16	220	4.07	401	5	ND	1	6	1	2	3	68	.16	.023	3	35	.36	41	.10	4	3.87	.01	.04	4	25
L18+50W 6+25N	3	63	2	32	.1	11	5	77	5.35	110	5	ND	1	3	1	2	10	143	.14	.019	2	35	.13	11	.16	3	2.13	.01	.02	1	7
L18+50W 6+00N	1	64	11	37	.4	13	5	150	6.15	96	5	ND	2	4	1	3	2	174	.16	.037	4	43	.14	13	.21	4	2.34	.01	.03	3	13
L18+50W 5+75N	1	111	10	69	.1	24	10	154	5.20	86	5	ND	1	4	1	2	2	138	.19	.029	3	48	.25	22	.11	2	4.10	.01	.02	1	22
L18+50W 5+50N	5	115	7	60	.2	26	11	179	4.69	627	5	ND	1	5	1	2	2	108	.22	.019	3	43	.46	32	.12	2	3.21	.01	.02	1	9
L18+50W 5+25N	4	72	2	47	.1	18	8	127	2.27	614	5	ND	1	3	1	2	2	70	.15	.014	2	28	.29	23	.07	2	2.07	.01	.02	1	21
L18+50W 5+00N	2	102	10	47	.1	15	8	113	5.23	133	5	ND	1	4	1	3	3	139	.16	.030	4	36	.19	24	.15	2	3.12	.01	.02	1	106
L18+50W 4+75N	1	174	5	74	.1	36	14	252	5.18	108	5	ND	1	5	1	2	2	111	.25	.027	3	52	.54	47	.14	4	4.07	.01	.03	2	14
L18+50W 4+50N	2	143	5	80	.1	35	23	402	5.54	125	5	ND	1	7	1	2	2	124	.24	.031	4	54	.51	39	.12	2	4.44	.01	.06	1	11
L18+50W 4+25N	2	164	13	83	.3	42	31	279	5.27	178	5	ND	1	6	1	2	2	119	.23	.024	4	54	.58	48	.14	2	4.83	.01	.05	1	13
L18+50W 4+00N	1	239	16	68	.2	38	14	223	5.08	161	5	ND	1	5	1	2	2	99	.20	.024	3	59	.54	51	.13	2	5.29	.01	.04	2	32
L18+50W 3+75N	2	115	11	53	.2	25	10	205	5.19	141	5	ND	1	13	1	2	2	136	.32	.026	4	42	.41	33	.15	2	2.64	.01	.03	1	7
L18+50W 3+50N	10	129	9	54	1.6	23	39	899	4.83	127	5	ND	1	6	1	2	9	83	.15	.075	5	45	.26	28	.14	3	5.79	.01	.03	1	21
L17+00W 15+00N	3	109	7	45	.3	12	6	93	4.10	112	5	ND	1	5	1	3	2	121	.18	.015	3	31	.19	17	.11	2	2.45	.01	.01	2	45
L17+00W 14+75N	1	71	3	61	.1	15	9	291	4.92	31	5	ND	1	5	1	2	2	149	.31	.027	3	36	.24	21	.22	2	2.22	.01	.02	1	5
L17+00W 14+25N	1	75	9	61	.1	19	8	170	5.25	40	5	ND	1	4	1	2	2	142	.31	.036	2	41	.30	15	.24	2	2.56	.01	.04	1	7
L17+00W 13+50N	1	71	16	71	.1	24	12	590	4.50	31	5	ND	1	7	1	2	2	124	.39	.037	3	41	.38	31	.16	3	2.62	.01	.02	1	11
STD C/AU-S	18	61	42	132	7.2	70	31	1032	4.01	43	24	8	39	49	19	16	23	61	.48	.093	41	57	.84	181	.07	38	1.99	.06	.15	12	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L17+00W 13+25N	1	63	12	62	.2	26	11	213	4.77	26	5	ND	1	5	1	2	2	116	.39	.029	2	47	.41	35	.17	3	3.31	.01	.02	1	1
L17+00W 13+00N	1	66	9	77	.2	29	13	386	5.30	32	5	ND	1	6	1	3	2	141	.38	.027	3	51	.45	32	.19	3	3.13	.01	.02	1	1
L17+00W 12+75N	1	53	7	64	.1	19	11	251	5.07	23	5	ND	1	4	1	2	2	150	.23	.024	2	42	.34	26	.17	2	2.66	.01	.01	1	3
L17+00W 12+50N	1	65	9	79	.2	29	15	336	5.05	32	5	ND	1	6	1	2	2	156	.36	.040	3	53	.41	35	.22	3	3.30	.01	.03	1	1
L17+00W 12+25N	1	107	9	82	.1	37	20	565	5.52	28	5	ND	1	8	1	2	2	135	.50	.016	4	62	.69	64	.11	2	3.46	.01	.02	1	1
L17+00W 12+00N	1	71	8	68	.2	23	11	334	5.14	27	5	ND	1	4	1	2	2	131	.28	.029	3	46	.26	25	.19	2	3.33	.01	.02	1	1
L17+00W 11+75N	1	63	12	62	.2	23	13	222	4.76	19	5	ND	1	5	1	2	2	131	.38	.018	4	45	.26	27	.13	3	3.02	.01	.02	1	47
L17+00W 11+50N	1	43	3	59	.1	15	7	164	4.59	21	5	ND	1	4	1	2	2	132	.29	.017	2	39	.25	20	.13	2	2.41	.01	.02	1	3
L17+00W 11+00N	1	43	2	45	.1	18	9	159	3.44	10	5	ND	1	4	1	2	2	94	.34	.029	2	35	.30	21	.08	2	2.01	.01	.01	1	7
L17+00W 10+75N	1	55	3	56	.2	18	8	174	5.31	33	5	ND	1	7	1	2	2	130	.32	.017	2	40	.28	26	.14	3	2.40	.01	.02	1	11
L17+00W 10+25N	1	59	7	47	.1	16	7	215	4.64	39	5	ND	1	5	1	3	2	139	.25	.019	3	37	.22	21	.16	2	2.36	.01	.02	1	2
L17+00W 10+00N	1	82	6	67	.2	30	13	236	5.33	50	5	ND	1	5	1	2	2	131	.31	.021	3	51	.43	34	.14	2	3.30	.01	.03	1	1
L17+00W 9+75N	1	138	15	69	.2	38	15	234	4.67	56	5	ND	1	5	1	3	2	112	.32	.015	3	59	.69	45	.16	2	3.59	.01	.02	1	15
L17+00W 9+50N	1	61	10	44	.1	15	7	126	5.93	46	5	ND	1	4	1	2	2	190	.19	.014	3	43	.16	21	.24	5	2.25	.01	.02	2	4
L17+00W 9+25N	1	69	10	56	.1	23	10	213	4.88	50	5	ND	1	5	1	2	2	124	.33	.017	4	46	.40	32	.14	2	2.79	.01	.02	1	1
L17+00W 8+75N	1	104	16	54	.2	19	7	145	5.40	72	5	ND	1	5	1	4	2	158	.23	.020	3	44	.23	26	.19	2	3.01	.01	.02	1	10
L17+00W 8+25N	1	74	3	45	.2	12	5	97	5.59	94	5	ND	1	3	1	3	2	179	.12	.021	3	46	.13	16	.18	2	3.27	.01	.01	1	12
L17+00W 8+00N	1	133	11	55	.2	19	8	144	7.51	116	5	ND	1	4	1	2	2	258	.21	.024	3	56	.27	22	.16	4	3.65	.01	.02	1	1
L17+00W 7+75N	1	101	19	83	.3	28	12	309	6.06	95	5	ND	1	5	1	4	2	142	.24	.029	2	55	.40	33	.10	2	4.21	.01	.03	1	28
L17+00W 7+50N	1	109	10	64	.3	31	12	196	5.83	85	5	ND	1	5	1	2	2	131	.22	.029	3	58	.42	40	.09	2	4.16	.01	.03	2	3
L17+00W 7+25N	2	90	12	74	.2	29	15	345	5.69	86	5	ND	1	5	1	2	2	129	.20	.035	3	52	.40	34	.10	2	3.54	.01	.03	1	17
L17+00W 7+00N	1	138	7	59	.1	30	13	204	5.56	100	5	ND	1	4	1	4	2	136	.19	.023	4	49	.42	41	.13	2	3.79	.01	.03	1	8
L17+00W 6+75N	1	52	8	43	.1	14	7	169	3.66	52	5	ND	1	4	1	3	2	119	.23	.024	3	34	.25	14	.20	2	2.22	.01	.02	1	1
L17+00W 6+50N	1	117	9	84	.1	32	15	201	5.17	101	5	ND	1	5	1	4	2	123	.22	.019	5	51	.45	39	.13	2	3.86	.01	.03	1	5
L17+00W 6+00N	2	94	15	57	.2	26	11	187	5.78	97	5	ND	1	4	1	4	2	134	.21	.022	3	52	.31	23	.20	2	3.99	.01	.02	1	21
L17+00W 5+75N	1	111	14	67	.2	29	11	193	5.32	78	5	ND	1	5	1	2	2	125	.26	.022	3	50	.41	33	.14	2	3.65	.01	.03	1	1
L17-00W 4+50N	1	132	11	79	.2	34	14	358	6.07	90	5	ND	1	7	1	2	2	141	.26	.025	4	50	.47	44	.09	2	3.70	.01	.03	1	1
L17+00W 4+25N	1	74	13	56	.1	16	7	140	5.14	92	5	ND	1	8	1	2	2	137	.22	.018	3	42	.22	22	.14	2	2.32	.01	.02	1	1
L17+00W 4+00N	1	71	9	57	.2	19	8	154	6.09	65	5	ND	2	4	1	4	2	155	.19	.020	3	47	.29	23	.17	4	2.82	.01	.02	1	1
L17+00W 3+75N	1	153	13	71	.1	39	16	257	5.97	98	5	ND	1	5	1	3	3	131	.24	.017	3	61	.61	54	.11	2	4.16	.01	.03	1	5
L17+00W 3+50N	1	157	6	78	.1	39	18	282	5.62	100	5	ND	1	6	1	3	2	135	.25	.017	4	58	.60	61	.13	2	3.78	.01	.03	1	6
L15+50W 15+00N	1	28	6	30	.1	9	5	97	3.57	16	5	ND	1	5	1	2	2	125	.37	.012	2	25	.14	15	.24	2	1.40	.01	.01	1	1
L15+50W 14+50N	1	41	8	36	.2	12	6	130	3.96	19	5	ND	1	5	1	2	2	126	.31	.012	3	29	.16	15	.17	2	1.79	.01	.01	1	7
L15+50W 14+25N	1	41	10	34	.2	10	4	102	4.57	27	5	ND	1	5	1	2	2	155	.26	.022	2	31	.16	12	.25	2	1.42	.01	.01	1	1
L15+50W 14+00N	1	21	4	32	.1	8	4	89	3.02	19	5	ND	1	6	1	2	2	108	.30	.015	3	20	.13	15	.20	2	1.07	.01	.01	1	54
L15+50W 13+75N	1	42	4	55	.1	17	11	225	4.51	29	5	ND	1	7	1	2	2	121	.34	.022	4	33	.26	26	.12	2	2.14	.01	.02	1	6
STD C/AU-S	18	58	43	132	6.3	68	30	1008	4.02	42	22	7	37	47	18	16	20	58	.46	.094	38	55	.84	175	.07	37	1.97	.06	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L15+50W 13+50N	1	59	8	67	.1	29	10	938	4.30	35	5	ND	1	7	1	2	2	108	.38	.021	4	41	.48	36	.12	2	2.64	.01	.03	1	6
L15+50W 13+25N	1	66	10	67	.1	24	10	175	5.03	43	5	ND	1	6	1	2	3	107	.30	.026	3	45	.31	31	.13	2	2.97	.01	.02	1	2
L15+50W 13+00N	1	71	8	97	.1	33	18	344	5.44	40	5	ND	1	6	1	2	2	140	.29	.030	3	53	.31	36	.12	2	3.77	.01	.03	1	3
L15+50W 12+75N	1	149	11	99	.1	48	28	303	5.08	55	5	ND	1	5	1	2	2	116	.32	.028	3	55	.59	67	.14	3	4.12	.01	.03	1	9
L15+50W 12+50N	1	28	9	29	.1	11	5	151	3.05	31	5	ND	1	5	1	2	2	141	.26	.021	3	25	.15	14	.18	2	1.21	.01	.02	1	14
L15+50W 12+25N	1	75	12	75	.1	30	13	459	5.69	44	5	ND	1	6	1	2	2	134	.43	.030	3	51	.49	31	.16	3	3.16	.01	.03	1	10
L15+50W 12+00N	1	102	5	77	.1	37	17	256	5.69	45	5	ND	1	6	1	2	2	151	.41	.026	4	56	.52	46	.19	2	3.70	.01	.03	1	5
L15+50W 11+50N	1	44	6	40	.1	11	5	132	5.63	47	5	ND	1	4	1	2	3	154	.22	.030	3	35	.17	19	.15	2	2.16	.01	.02	1	230
L15+50W 11+25N	1	88	13	67	.1	25	14	430	4.50	42	5	ND	1	5	1	2	3	131	.30	.029	4	42	.28	31	.20	3	3.24	.01	.02	1	24
L15+50W 11+00N	1	70	3	78	.1	29	16	239	4.50	28	5	ND	1	7	1	2	2	124	.48	.021	4	47	.41	34	.17	5	2.97	.01	.02	1	14
L15+50W 10+75N	1	112	8	73	.1	36	14	288	5.32	41	5	ND	1	6	1	2	3	125	.45	.024	3	56	.57	46	.13	2	3.42	.01	.03	1	6
L15+50W 10+50N	1	80	10	73	.1	28	12	256	5.45	32	5	ND	1	7	1	2	2	145	.35	.023	3	51	.44	53	.16	2	3.15	.01	.03	1	7
L15+50W 9+50N	1	125	11	91	.1	36	15	232	4.95	53	5	ND	1	6	1	2	3	117	.37	.024	3	47	.51	36	.14	2	3.88	.01	.03	1	29
L15+50W 8+75N	1	135	10	87	.1	38	17	259	5.67	77	5	ND	1	5	1	2	2	134	.28	.027	3	54	.48	44	.14	2	4.09	.01	.02	1	56
L15+50W 8+50N	1	92	11	69	.2	28	16	290	4.79	72	5	ND	1	6	1	2	2	110	.31	.035	2	45	.42	20	.19	2	3.67	.01	.03	1	22
L15+50W 8+00N	1	48	11	45	.1	15	8	265	5.46	64	5	ND	1	3	1	2	2	142	.34	.025	3	42	.28	22	.14	2	2.12	.01	.02	1	7
L15+50W 7+75N	2	103	9	78	.1	32	14	320	4.75	72	5	ND	1	7	1	3	2	121	.32	.026	3	45	.40	40	.11	3	3.53	.01	.03	1	16
L15+50W 7+50N	1	105	12	76	.1	35	17	293	5.50	63	5	ND	1	6	1	2	3	137	.31	.029	4	51	.47	40	.12	2	3.39	.01	.04	1	210
L15+50W 7+25N	1	32	10	66	.1	23	12	345	5.73	62	5	ND	1	5	1	2	2	153	.36	.027	4	56	.47	37	.16	2	3.23	.01	.02	1	9
L15+50W 7+00N	1	74	11	59	.1	24	10	358	5.69	63	5	ND	1	5	1	2	2	158	.29	.032	3	51	.32	27	.15	2	3.26	.01	.02	1	18
L15+50W 6+75N	1	154	9	93	.2	44	16	267	7.02	93	5	ND	1	5	1	2	2	154	.25	.050	3	68	.51	58	.14	3	5.41	.01	.04	1	7
L15+50W 6+25N	1	97	8	71	.1	29	11	271	5.87	73	5	ND	1	12	1	2	3	152	.49	.022	3	53	.50	56	.21	2	2.69	.01	.03	1	6
L15+50W 6+00N	1	91	7	55	.3	20	8	141	5.23	86	5	ND	1	5	1	3	3	134	.20	.024	4	43	.25	27	.13	2	3.35	.01	.02	1	6
L15+50W 5+50N	1	35	9	33	.1	13	6	145	3.13	47	5	ND	1	11	1	3	2	104	.38	.015	4	25	.28	27	.11	2	1.46	.01	.03	1	18
L15+50W 5+25N	5	118	14	82	.6	24	41	1551	4.75	183	5	ND	1	12	1	2	3	91	.30	.029	6	38	.38	54	.09	2	3.53	.01	.04	2	25
L15+50W 4+25N	1	115	5	64	.1	26	14	393	5.16	90	5	ND	1	5	1	2	2	133	.25	.028	4	47	.42	41	.14	2	3.65	.01	.03	1	14
L15+50W 4+00N	2	97	12	51	.2	24	11	222	4.34	101	5	ND	1	6	1	3	2	135	.25	.025	4	49	.38	54	.10	3	2.95	.01	.03	1	7
L15+50W 3+75N	2	148	7	82	.3	35	14	346	7.36	121	5	ND	1	6	1	2	2	152	.21	.144	4	62	.46	46	.12	2	4.62	.01	.04	3	8
L15+50W 3+50N	2	170	9	74	.2	36	14	245	6.28	138	5	ND	2	5	1	2	2	136	.37	.056	3	57	.36	53	.09	2	5.51	.01	.05	1	13
L14+00W 15+00N	1	62	3	65	.1	23	10	202	4.88	43	5	ND	1	7	1	2	2	131	.39	.022	3	38	.37	33	.15	2	2.47	.01	.02	1	3
L14+00W 14+75N	1	52	4	60	.2	23	15	467	4.34	37	5	ND	1	8	1	2	2	129	.43	.025	4	39	.35	28	.17	2	2.40	.01	.03	1	5
L14+00W 14+50N	2	116	8	113	.4	51	26	1452	5.46	52	5	ND	1	10	1	2	2	130	.34	.057	4	61	.51	56	.17	2	5.05	.01	.04	1	8
L14+00W 14+25N	1	76	13	65	.2	21	10	504	4.46	71	5	ND	1	6	1	2	2	120	.37	.036	3	37	.37	27	.22	2	2.65	.01	.02	1	7
L14+00W 14+00N	1	56	7	60	.2	20	18	631	3.98	26	5	ND	1	7	1	2	2	115	.42	.031	4	34	.29	25	.17	2	2.32	.01	.02	1	9
L14+00W 13+75N	1	116	9	75	.2	29	12	345	6.47	54	5	ND	1	6	1	2	3	167	.32	.054	3	51	.33	24	.17	3	3.88	.01	.03	1	8
L14+00W 13+50N	1	84	6	69	.2	33	18	384	5.23	41	5	ND	2	7	1	2	3	132	.42	.023	4	49	.50	41	.14	2	3.43	.01	.04	1	3
STD C/AU-S	17	60	36	132	6.7	64	29	1044	3.99	41	17	7	37	47	18	16	23	58	.48	.093	33	53	.83	173	.07	33	1.96	.06	.14	11	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L14+00W 13+25N	1	62	9	54	.2	22	10	161	4.33	30	5	ND	1	5	1	2	2	120	.41	.020	3	37	.37	21	.16	2	2.46	.01	.02	1	1
L14+00W 13+00N	1	71	11	83	.2	25	11	386	4.98	43	5	ND	1	5	1	3	2	130	.32	.033	3	41	.33	23	.16	2	3.05	.01	.02	1	2
L14+00W 12+75N	1	67	10	57	.2	23	10	262	5.31	36	5	ND	1	6	1	4	2	133	.37	.031	3	47	.34	24	.15	2	3.02	.01	.02	1	9
L14+00W 12+50N	1	97	12	79	.1	39	17	809	5.06	56	5	ND	1	7	1	2	2	130	.37	.026	4	58	.49	46	.16	2	3.68	.01	.03	1	3
L14+00W 12+25N	1	92	10	56	.1	29	12	222	4.64	57	5	ND	1	7	1	2	2	123	.36	.020	3	43	.47	38	.15	2	2.92	.01	.02	1	4
L14+00W 12+00N	1	126	12	83	.1	45	21	199	5.94	51	5	ND	1	5	1	2	2	146	.37	.022	3	67	.64	60	.16	2	4.81	.01	.03	1	2
L14+00W 11+75N	1	99	11	71	.1	38	16	249	5.92	31	5	ND	1	6	1	2	2	154	.45	.016	3	59	.59	46	.15	2	3.75	.01	.03	1	1
L14+00W 11+25N	1	69	5	41	.1	17	7	114	4.28	47	5	ND	1	5	1	2	2	124	.24	.014	2	33	.26	23	.21	2	2.72	.01	.02	1	6
L14+00W 11+00N	3	219	7	99	.1	44	27	240	5.96	73	5	ND	1	4	1	2	2	125	.15	.069	3	63	.39	54	.06	2	6.10	.01	.04	1	1
L14+00W 10+75N	1	91	7	72	.1	31	15	299	4.73	41	5	ND	1	6	1	2	2	110	.09	.021	3	47	.51	48	.05	2	3.24	.01	.03	1	1
L14+00W 10+50N	1	95	6	71	.2	32	13	248	5.65	44	5	ND	1	5	1	2	2	140	.32	.028	3	51	.48	33	.16	3	3.62	.01	.03	1	3
L14+00W 10+25N	3	76	5	60	.4	25	10	210	5.38	46	5	ND	3	7	1	2	2	129	.26	.027	4	46	.33	30	.15	4	3.18	.01	.03	1	1
L14+00W 10+00N	1	65	9	48	.1	17	7	133	5.66	63	5	ND	1	4	1	3	2	153	.21	.025	3	45	.26	21	.16	2	2.80	.01	.02	1	1
L14+00W 9+50N	2	91	7	70	.1	33	14	171	5.03	50	5	ND	1	5	1	2	3	105	.24	.015	2	51	.38	38	.14	2	4.27	.01	.02	1	24
L14+00W 9+25N	2	83	7	63	.2	31	12	194	4.66	58	5	ND	1	5	1	2	2	114	.33	.014	3	47	.45	32	.13	2	3.36	.01	.02	1	2
L14+00W 9+00N	1	96	11	79	.3	26	11	191	5.62	67	5	ND	1	5	1	4	2	151	.29	.021	3	54	.39	23	.16	3	3.74	.01	.03	1	4
L14+00W 8+75N	2	101	14	72	.3	30	33	2600	5.09	73	5	ND	1	6	1	5	2	133	.30	.026	5	50	.43	35	.13	3	3.79	.01	.03	1	14
L14+00W 8+50N	1	67	10	73	.3	26	12	230	5.75	30	5	ND	1	6	1	2	2	140	.25	.027	3	53	.30	25	.21	4	3.69	.01	.02	1	20
L14+00W 8+25N	6	185	14	100	.7	35	42	1160	5.78	151	5	ND	1	7	1	5	2	127	.24	.047	6	58	.47	45	.13	2	5.80	.01	.15	1	9
L14+00W 8+00N	2	130	3	59	.3	16	7	178	7.29	135	5	ND	1	5	1	6	2	178	.22	.036	3	50	.20	21	.19	3	3.29	.01	.02	1	29
L14+00W 7+75N	1	143	11	76	.3	38	16	231	5.89	85	5	ND	1	6	1	5	2	142	.30	.023	3	56	.48	44	.16	3	4.20	.01	.04	1	2
L14+00W 7+50N	1	78	11	75	.3	25	10	202	5.96	73	5	ND	1	6	1	3	3	157	.31	.034	3	48	.32	31	.18	3	3.28	.01	.03	1	1
L14+00W 7+25N	1	78	16	57	.5	21	9	431	5.51	80	5	ND	1	5	1	5	2	144	.22	.033	3	41	.27	29	.12	2	3.30	.01	.03	1	5
L14+00W 7+00N	1	62	7	62	.2	21	11	224	5.17	98	5	ND	1	5	1	2	2	139	.29	.023	4	42	.34	34	.09	2	2.94	.01	.03	1	1
L14+00W 6+75N	1	91	14	89	.2	33	15	308	5.38	67	5	ND	1	5	1	5	2	149	.32	.028	3	56	.45	39	.14	2	3.60	.01	.03	1	4
L14+00W 6+50N	1	104	11	62	.2	27	12	178	5.28	94	5	ND	1	5	1	4	2	137	.23	.027	3	47	.34	35	.17	4	4.09	.01	.03	1	5
L14+00W 6+25N	1	92	9	52	.2	20	8	131	5.03	117	5	ND	1	5	1	4	2	124	.27	.018	3	43	.29	30	.18	3	3.30	.01	.02	1	19
L14+00W 6+00N	2	75	13	59	.2	25	10	197	5.39	82	5	ND	1	5	1	5	2	146	.24	.021	4	41	.36	32	.10	2	2.80	.01	.03	1	16
L14+00W 5+50N	1	93	8	53	.3	23	9	156	5.37	65	5	ND	1	7	1	4	2	121	.30	.018	3	46	.38	35	.10	2	3.10	.01	.03	1	6
L14+00W 5+25N	2	118	13	68	.6	22	8	121	5.77	84	5	ND	1	5	1	2	2	120	.17	.030	3	53	.24	29	.12	3	4.30	.01	.03	1	3
L14+00W 5+00N	1	63	8	45	.3	18	7	124	5.12	70	5	ND	1	4	1	5	2	132	.18	.033	3	39	.27	15	.13	4	2.44	.01	.03	2	5
L14+00W 4+75N	1	95	13	66	.1	28	25	522	4.45	67	5	ND	1	7	1	2	2	117	.26	.017	4	44	.41	42	.11	3	3.45	.01	.02	1	7
L14+00W 4+50N	2	189	14	109	.6	50	31	443	6.04	116	5	ND	1	5	1	5	2	133	.15	.031	4	65	.43	78	.05	3	5.73	.01	.05	1	4
L14+00W 4+25N	1	117	16	72	.4	30	13	393	5.44	84	5	ND	1	5	1	7	2	132	.26	.038	4	49	.41	35	.10	5	3.69	.01	.04	1	11
L14+00W 4+00N	1	155	15	92	.1	43	19	373	5.29	94	5	ND	1	7	1	7	2	121	.32	.029	4	58	.65	66	.13	5	4.10	.01	.04	1	15
L14+00W 3+75N	1	114	15	69	.3	31	14	364	5.08	96	5	ND	1	6	1	4	2	123	.26	.030	4	46	.45	45	.11	3	3.58	.01	.04	1	9
STD C/AU-S	18	59	41	132	6.6	67	30	1018	4.03	40	17	7	36	47	18	16	19	58	.48	.094	38	53	.84	175	.07	33	1.94	.06	.14	11	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L14+50W 3+50N	2	133	12	73	.2	34	12	134	5.22	87	5	ND	1	5	1	4	2	119	.22	.027	3	58	.43	47	.10	2	4.14	.01	.03	2	3
L12+50W 15+00N	1	45	7	54	.1	15	9	450	4.64	38	5	ND	1	5	1	3	2	125	.34	.025	2	33	.22	18	.13	2	1.91	.01	.02	1	3
L12+50W 14+75N	1	89	3	64	.1	31	14	237	5.05	40	5	ND	1	7	1	3	2	133	.40	.024	3	45	.43	36	.19	2	3.07	.01	.03	1	14
L12+50W 14+50N	1	53	2	53	.1	22	9	254	3.56	14	5	ND	1	6	1	2	2	89	.38	.014	3	34	.44	22	.12	2	2.11	.01	.02	1	4
L12+50W 14+25N	1	72	9	72	.1	27	12	469	5.01	29	5	ND	1	6	1	3	2	136	.36	.029	3	46	.40	34	.17	2	2.84	.01	.02	1	2
L12+50W 14+00N	1	60	8	67	.1	23	11	291	4.32	20	5	ND	1	6	1	2	2	119	.44	.022	3	37	.35	25	.17	2	2.61	.01	.02	1	1
L12+50W 13+75N	1	26	9	22	.1	10	5	146	3.39	12	5	ND	1	5	1	2	2	107	.26	.016	2	21	.14	12	.16	2	1.27	.01	.01	1	10
L12+50W 13+50N	1	92	9	57	.1	26	11	201	4.06	25	5	ND	1	5	1	2	2	135	.39	.015	2	33	.39	28	.18	2	2.66	.01	.02	1	2
L12+50W 13+25N	1	60	4	45	.1	20	9	168	3.47	12	5	ND	1	5	1	2	2	91	.40	.012	2	28	.31	23	.13	2	2.25	.01	.02	1	7
L12+50W 13+00N	1	65	5	57	.1	26	12	198	4.58	15	5	ND	1	6	1	2	2	119	.43	.009	3	45	.45	35	.11	2	2.71	.01	.02	1	3
L12+50W 12+50N	6	133	11	61	.3	23	13	178	3.71	133	5	ND	1	16	1	6	2	80	.41	.033	3	34	.50	45	.11	2	2.54	.02	.03	1	17
L12+50W 12+25N	1	65	8	53	.1	13	8	174	5.22	37	5	ND	1	6	1	2	3	161	.27	.025	2	35	.23	27	.24	2	2.36	.01	.02	1	1
L12+50W 12+00N	1	65	10	60	.1	22	9	152	5.77	28	5	ND	1	4	1	2	2	146	.23	.026	2	47	.23	23	.17	2	3.18	.01	.02	1	2
L12+50W 11+75N	1	40	2	35	.1	13	6	91	2.87	10	5	ND	1	2	1	2	2	72	.17	.011	2	21	.17	11	.03	2	1.65	.01	.01	1	87
L12+50W 11+50N	5	129	8	77	.2	45	26	1022	5.06	34	5	ND	1	5	1	2	2	115	.24	.022	3	52	.42	53	.13	2	4.66	.01	.03	1	20
L12+50W 11+25N	3	112	11	84	.1	32	19	582	5.46	57	5	ND	1	9	1	5	2	143	.35	.037	4	49	.36	35	.16	2	3.73	.01	.03	2	23
L12+50W 11+00N	1	93	8	62	.2	25	13	223	5.75	51	5	ND	1	5	1	3	2	153	.34	.025	3	49	.40	26	.21	2	3.39	.01	.02	1	8
L12+50W 10+75N	1	104	6	65	.1	32	19	796	4.68	57	5	ND	1	8	1	3	2	117	.29	.023	4	48	.51	44	.15	2	3.20	.01	.03	1	3
L12+50W 10+50N	1	101	10	63	.2	27	12	232	4.82	62	5	ND	1	5	1	3	2	121	.28	.024	3	44	.38	27	.16	2	3.25	.01	.02	1	10
L12+50W 10+25N	1	46	2	23	.1	12	5	101	3.47	23	5	ND	1	2	1	2	2	85	.15	.016	2	25	.18	14	.11	2	2.19	.01	.01	1	4
L12+50W 10+00N	1	28	2	20	.1	8	4	89	2.00	19	5	ND	1	1	1	2	2	52	.09	.011	2	17	.12	8	.07	2	1.37	.01	.01	1	44
L12+50W 9+75N	1	133	9	59	.1	28	13	206	4.32	78	5	ND	1	6	1	5	2	129	.27	.016	4	44	.47	45	.15	2	3.20	.01	.02	1	5
L12+50W 9+50N	1	110	6	68	.1	34	13	209	6.04	72	5	ND	1	5	1	4	2	148	.25	.013	3	55	.49	49	.13	2	3.90	.01	.03	1	7
L12+50W 9+25N	5	103	11	62	.2	30	22	407	4.60	128	5	ND	1	7	1	5	2	109	.31	.013	5	52	.52	42	.12	2	3.68	.01	.03	1	9
L12+50W 9+00N	1	35	8	44	.2	12	6	173	4.21	43	5	ND	1	10	1	2	2	124	.34	.037	4	31	.22	24	.13	2	1.83	.01	.02	1	1
L12+50W 8+25N	1	44	7	32	.2	10	4	80	4.92	20	5	ND	1	4	1	3	2	137	.17	.020	3	39	.13	15	.14	2	2.05	.01	.02	1	2
L12+50W 8+00N	1	3	2	33	.1	2	1	12	.13	3	5	ND	1	24	1	2	2	4	.26	.020	2	2	.03	35	.01	2	.17	.01	.02	1	1
L12+50W 7+75N	1	33	7	32	.1	10	4	39	5.30	52	5	ND	1	4	1	3	2	142	.21	.020	4	32	.14	17	.16	2	1.46	.01	.02	1	30
L12+50W 7+50N	1	89	10	67	.2	30	12	215	4.65	64	5	ND	1	8	1	5	2	115	.30	.023	3	45	.50	44	.11	3	3.11	.01	.03	1	44
L12+50W 7+25N	1	133	7	100	.1	42	16	234	5.06	68	5	ND	1	5	1	4	2	123	.27	.023	3	50	.48	67	.10	2	3.94	.01	.03	1	10
L12+50W 7+00N	1	89	9	68	.1	30	12	230	5.58	62	5	ND	1	6	1	4	2	141	.31	.024	3	50	.50	41	.17	2	3.12	.01	.03	1	32
L12+50W 6+75N	1	102	12	59	.2	25	10	265	4.74	77	5	ND	1	7	1	4	2	112	.32	.025	3	42	.41	28	.12	2	2.72	.01	.03	1	2
L12+50W 6+50N	1	163	12	83	.2	49	26	378	5.69	92	5	ND	1	7	1	6	2	121	.28	.028	4	60	.61	66	.15	2	5.03	.01	.04	1	8
L12+50W 6+25N	1	44	4	44	.2	10	4	84	4.23	66	5	ND	1	8	1	3	2	128	.15	.021	3	34	.12	15	.14	4	1.76	.01	.02	1	1
L12+50W 6+00N	1	155	12	73	.1	42	20	271	5.12	67	5	ND	1	7	1	6	2	119	.38	.021	5	55	.64	70	.13	5	3.92	.01	.04	1	7
L12+50W 5+75N	1	118	9	85	.3	32	16	185	5.12	62	5	ND	2	7	1	4	2	124	.33	.018	3	48	.43	43	.12	4	3.52	.01	.03	1	12
STD C/AU-S	18	56	41	132	6.9	68	30	1015	4.38	42	22	7	37	47	18	19	21	58	.49	.094	39	55	.86	175	.07	38	1.98	.06	.14	11	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L12+50W 5+50N	1	152	9	61	.1	31	12	184	5.29	82	5	ND	2	5	1	2	2	119	.23	.027	3	51	.47	34	.13	2	4.29	.01	.04	1	5
L12+50W 5+25N	1	74	5	62	.1	26	35	1273	4.19	61	5	ND	1	10	1	2	4	91	.26	.027	5	43	.44	39	.09	2	2.78	.01	.04	1	12
L12+50W 4+75N	2	91	8	44	.1	19	9	203	4.38	81	5	ND	1	6	1	2	2	138	.21	.021	3	45	.28	22	.15	2	3.55	.01	.04	1	6
L12+50W 4+50N	1	27	8	31	.2	7	4	69	3.90	60	6	ND	2	5	1	2	2	110	.19	.024	3	31	.10	9	.16	2	1.78	.01	.03	1	18
L12+50W 4+25N	1	87	7	55	.2	26	9	213	4.37	94	5	ND	1	11	1	2	2	106	.33	.020	4	41	.49	40	.10	2	2.58	.01	.03	1	4
L12+50W 4+00N	1	97	10	53	.2	23	9	132	4.93	106	5	ND	1	6	1	2	2	110	.21	.022	3	41	.32	23	.15	2	3.23	.01	.02	1	10
L12+50W 3+75N	1	101	11	56	.2	22	10	420	4.59	76	5	ND	1	10	1	2	2	116	.43	.049	4	38	.38	27	.14	2	2.76	.01	.02	1	21
L12+50W 3+50N	1	112	14	56	.1	22	9	255	4.67	39	5	ND	1	8	1	2	2	111	.26	.044	3	40	.34	31	.12	2	3.11	.01	.04	1	24
STD C/AU-S	18	60	40	132	6.9	72	30	1036	4.35	42	23	8	38	49	19	19	20	61	.51	.098	39	56	.94	182	.07	37	2.07	.06	.14	13	52

Append II
Fig 2a

Part 1 of 5

R L WRIGHT & ASSOCIATES

DOVE PROJECT

Mt. Washington, B.C.

IDEAL CLAIMS

Rock Sample Locations

Scale 1:10,000	Date 26 July 1988

Fig 2b Appendix II

R L WRIGHT & ASSOCIATES

DOVE PROJECT

Mt. Washington, B.C.

HARMONY CLAIMS

Rock Sample Locations

Scale 1:10,000 | Date 25 July 1988

Part 1 of 5

17087

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMLESS AA.

DATE RECEIVED: JUL 12 1988 DATE REPORT MAILED: July 19/88 ASSAYER. C. Leong . D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-2610

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
88AW-36	1	43	9	31	.9	15	9	2862	7.39	88	5	ND	1	45	2	2	2	25	14.14	.021	2	4	3.61	6	.01	9	.08	.01	.06	2	28	160
88AW-65	1	12	15	43	.1	9	9	591	2.57	47	5	ND	1	73	1	2	2	40	2.04	.046	7	21	1.16	21	.01	2	2.06	.07	.03	1	1	130
88AW-75	1	58	4	48	.1	32	23	623	5.94	12	5	ND	1	21	1	2	2	146	1.85	.056	3	30	1.36	7	.33	2	1.47	.07	.03	1	1	50
88AW-81	1	76	2	26	.1	14	15	408	3.60	24	5	ND	1	97	1	2	2	105	2.20	.042	2	47	1.74	30	.13	5	1.53	.12	.05	2	3	70
88AW-86	1	129	7	31	.4	14	10	2437	7.93	21	5	ND	1	53	1	2	2	56	16.74	.005	5	7	3.77	7	.01	2	.30	.01	.03	1	1	80
88AW-97	1	51	12	75	.1	15	9	188	2.26	13	5	ND	1	13	1	2	2	25	.30	.008	4	22	.58	94	.01	4	1.80	.01	.12	1	1	110
88AW-103	1	124	4	40	.2	20	12	9456	4.37	4	5	ND	1	148	3	2	2	93	23.33	.002	8	39	.33	21	.01	4	1.49	.01	.01	3	13	20
88AW-105	1	30	22	42	.1	24	9	5102	23.05	5	5	ND	4	53	2	2	2	82	4.15	.076	9	29	1.67	45	.01	2	.74	.01	.05	2	1	160
88AW-105F	1	413	8	79	.3	34	18	626	4.32	138	5	ND	3	42	1	23	2	97	11.20	.021	2	62	2.91	3	.01	5	.30	.01	.01	1	1	8800
88AW-113	1	81	4	66	.1	41	24	2193	7.42	29	5	ND	1	48	1	2	2	109	8.14	.019	4	30	2.20	8	.01	7	.32	.01	.02	1	1	2200
88AW-116F	28	163	4	46	.2	35	28	1554	2.30	1489	5	ND	1	100	3	9	2	54	24.73	.042	4	8	.30	6	.01	2	.17	.01	.02	2	4	960
88AW-123	1	128	17	100	.2	17	31	1071	28.88	26	5	ND	19	2	1	2	3	1301	.18	.021	11	197	.59	4	.14	2	2.66	.01	.01	2	340	50
88AW-129F	1	5	6	39	.1	45	21	1248	4.86	28	5	ND	1	4	1	2	2	110	.27	.038	3	121	1.22	34	.01	4	1.60	.01	.03	2	13	30
88AW-130	1	5	36	175	.1	35	15	1317	4.30	16	5	ND	1	13	1	2	2	80	2.66	.017	2	88	1.81	6	.01	10	1.75	.01	.02	1	2	430
88AW-140	1	2169	6	75	4.3	3	2	89	2.64	2713	5	ND	1	1	2	30	60	4	.03	.001	2	3	.02	3	.01	2	.01	.01	.01	1	93	5
RLW 88-1	1	6190	56	269	24.1	10	66	904	13.09	50575	5	28	2	19	3	48	24	2	2.32	.029	2	1	.56	16	.01	9	.24	.01	.14	1	15230	5
STD C/AU-R	18	58	38	127	7.0	67	27	1029	3.70	36	17	7	35	48	16	17	17	53	.45	.087	36	53	.87	170	.06	34	1.81	.06	.13	12	495	1300

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMLESS AA.

DATE RECEIVED: AUG 25 1988 DATE REPORT MAILED: Aug 30/88 ASSAYER. C. Leong .D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-3895

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
JLP 88-12	2	22	21	19	.1	7	1	84	.78	559	5	ND	1	6	1	32	2	2	.03	.001	4	6	.01	27	.01	4	.23	.01	.10	1	26	3700
JLP 88-13	1	86	2	7	.1	40	14	25	.85	14	5	ND	1	1	1	2	2	5	.01	.001	3	4	.01	26	.01	5	.23	.01	.10	1	4	30
JLP 88-15	2	119	3	44	.1	12	13	244	3.99	6	5	ND	1	59	1	2	2	48	.64	.035	2	30	1.42	16	.07	2	2.91	.15	.04	1	16	40
JLP 88-16	1	4751	52	170	17.1	6	49	843	9.56	12302	5	3	1	23	1	28	2	3	3.32	.024	2	1	.57	22	.01	15	.39	.01	.23	1	3757	5
JLP 88-17	2	1031	5	37	.4	15	45	125	4.17	135	5	ND	1	58	1	2	2	42	.64	.037	2	18	1.08	29	.05	2	2.08	.11	.24	1	72	10
JLP 88-18	2	910	10	24	.2	10	24	98	3.81	164	5	ND	1	70	1	2	2	41	.68	.038	2	17	1.13	67	.06	4	2.32	.16	.52	1	20	10
JLP 88-19	2	1774	23	53	6.4	9	25	628	5.21	370	5	ND	1	13	1	2	2	5	.89	.041	2	5	.21	23	.01	2	.54	.01	.31	1	680	5
JLP 88-20	1	7564	5	187	12.4	7	32	678	4.02	146	5	ND	1	5	1	4	2	4	.46	.041	2	2	.22	27	.01	11	.39	.01	.25	1	39	10
JLP 88-21	1	50925	5	811	113.6	9	68	27	7.21	2600	5	ND	1	1	7	2	2	2	.09	.029	2	1	.01	36	.01	12	.27	.01	.17	1	308	5
JLP 88-22	1	667	3	19	.5	7	17	77	3.67	177	5	ND	1	97	1	2	2	47	.87	.040	2	16	1.08	33	.03	9	3.01	.24	.26	1	22	5
JLP 88-23	2	640	2	22	.4	7	8	103	3.36	23	5	ND	1	74	1	3	2	40	.59	.040	2	20	1.16	26	.04	2	2.37	.16	.14	1	29	5
JLP 88-24	1	1529	23	35	.1	156	74	244	7.08	11	5	ND	1	72	1	2	2	65	4.58	.139	2	51	.27	7	.06	7	5.74	.26	.03	1	35	20
JLP 88-25	1	535	9	16	.1	15	14	126	3.66	35	5	ND	1	109	1	2	2	39	1.15	.044	2	18	1.06	29	.03	8	3.00	.26	.17	1	6	10
JLP 88-27	1	4951	7	111	3.4	17	26	149	3.85	19	5	ND	1	45	1	2	2	58	.40	.046	2	29	1.12	45	.07	4	2.26	.11	.48	5	122	5
JLP 88-29	3	5510	18	152	26.5	8	18	289	3.79	426	5	20	1	6	1	2	5	3	.53	.039	3	3	.14	20	.01	5	.41	.01	.28	1	2012	10
JLP 88-29	5	520	2	26	.4	8	12	93	2.70	10	5	ND	1	76	1	2	2	44	.75	.040	2	16	1.00	65	.07	2	2.17	.18	.41	1	22	10
JLP 88-30	1	55346	2	1073	119.7	7	82	369	11.70	173	5	ND	1	7	8	2	2	7	.55	.019	2	2	.29	24	.01	9	.57	.01	.26	1	562	5
JLP 88-31	5	4602	3	64	47.3	19	269	64	2.06	4638	5	3	1	4	1	176	2	2	.02	.004	2	4	.02	5	.01	5	.09	.01	.05	1	1657	20
JLP 88-32	2	2946	20	90	7.5	16	62	14	5.87	12613	5	3	1	2	1	42	2	3	.07	.030	2	5	.03	34	.01	9	.46	.01	.29	1	3030	5
JLP 88-41	1	6107	26	388	3.1	101	82	1993	21.30	235	5	ND	1	1	1	30	2	302	.72	.247	3	156	1.12	1	.02	14	9.11	.01	.02	1	87	20
JLP 88-42	1	550	10	25	.2	75	44	253	5.74	48	5	ND	1	80	1	3	2	99	4.32	.048	2	39	.26	10	.23	2	5.40	.40	.05	1	26	10
JLP 88-43	1	594	5	39	.2	20	39	272	6.39	11	5	ND	1	27	1	2	2	94	1.00	.006	2	46	.85	6	.04	12	3.01	.10	.04	1	18	10
JLP 88-44	58	2513	6	80	2.1	21	13	209	4.28	58	5	ND	1	1	1	2	2	38	.05	.017	2	17	.32	1	.01	2	.73	.01	.01	1	12	10
JLP 88-45	2	2601	3	48	1.0	16	23	86	3.40	5	5	ND	1	57	1	2	2	60	.46	.083	3	31	1.40	123	.12	6	2.44	.16	.99	1	109	10
JLP 88-46	1	529	14	19	.2	23	31	147	4.44	3	5	ND	1	137	1	2	6	27	4.01	.044	2	10	.22	23	.04	9	5.65	.39	.05	1	5	10
JLP 88-47	2	1560	6	47	3.6	15	8	61	3.02	12	5	ND	1	4	1	2	13	12	.06	.016	4	11	.33	41	.01	6	.61	.01	.13	2	29	5
JLP 88-48	4	285	8	42	2.5	1	4	28	1.28	580	5	ND	1	7	1	239	2	4	.04	.012	4	3	.02	19	.01	2	.25	.01	.14	2	62	210
JLP 88-49	6	219	6	38	.1	15	10	318	4.84	19	5	ND	1	24	1	2	2	117	.43	.021	3	37	.68	17	.09	3	2.56	.11	.11	2	10	5
JLP 88-50	1	732	6	47	.1	6	26	196	6.77	4	5	ND	1	32	1	2	2	60	.53	.026	3	19	.74	13	.03	4	2.32	.16	.07	2	7	5
JLP 88-52	3	1502	72	859	16.3	11	11	32	5.85	10954	5	2	2	8	5	231	7	9	.02	.003	2	10	.04	22	.01	10	.27	.01	.10	1	2156	5
JLP 88-53	30	1364	25	49	.6	65	43	181	17.27	66	5	ND	1	198	1	32	2	159	3.68	.019	2	105	.25	8	.06	13	8.59	.70	.11	1	31	10
JLP 88-54	3	276	3659	637	14.3	12	10	41	25.74	13001	62	37	11	5	6	766	2	6	.02	.003	3	8	.01	15	.01	21	.16	.01	.15	1	30660	30
JLP 88-101 PIT	5	520	12	28	.2	21	12	308	4.75	1110	5	ND	1	13	1	2	2	47	.31	.070	3	15	1.17	39	.01	9	1.96	.05	.12	1	99	5
RLW 88-3	2	94	121	55	.6	10	3	135	2.38	5682	5	ND	1	13	1	23	2	52	.21	.021	5	23	.55	14	.02	2	1.11	.06	.08	1	787	10
RLW 88-4	1	64574	226	1113	329.8	5	66	160	19.27	1408	5	4	2	5	8	6	1255	4	.54	.001	2	1	.10	15	.01	2	.27	.01	.10	1	5745	5
COOK CK 43	2	22326	9	39	4.9	22	12	538	2.94	538	5	ND	1	116	1	19	2	73	4.51	.001	2	18	1.36	101	.01	12	.15	.01	.05	1	40	12500
STD C/AU-R	18	63	38	133	6.8	73	30	1056	4.18	39	18	8	36	49	18	19	22	60	.47	.087	41	60	.92	183	.07	37	2.02	.06	.15	12	510	1300

\- ASSAY REQUIRED FOR CORRECT RESULT for Cu >10,000 ppm

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMLESS AA.

DATE RECEIVED: OCT 14 1988 DATE REPORT MAILED: Oct 19/88 SIGNED BY. .D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE File # 88-5211

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	Hg PPB
88-AW-145	83	777	9	31	1.5	32	23	201	5.02	39	5	ND	1	8	1	2	2	126	.56	.035	2	26	.37	8	.13	2	.72	.06	.04	4	235	10
88-AW-155	1	27	37	42	.2	5	4	192	1.27	5	5	ND	1	219	1	2	2	45	4.38	.154	8	6	.28	45	.07	6	5.34	.25	.01	1	23	5
88-AW-156	610	533	6	24	.6	26	11	61	11.56	2	5	ND	2	27	1	2	2	58	.40	.069	2	15	.29	20	.03	3	.86	.06	.08	1	320	5
88-AW-157	9	814	6	34	.7	12	10	155	2.97	4	5	ND	1	22	1	2	2	23	.34	.046	4	12	1.03	30	.09	6	1.52	.06	.36	1	101	5
88-AW-159	4	70	59	9	1.8	10	13	14	6.43	6197	5	ND	1	1	1	27	3	2	.01	.004	2	5	.01	13	.01	4	.16	.01	.11	1	945	5
88-AW-175	275	2729	9	83	1.5	42	20	324	5.39	8	5	ND	1	15	1	2	1	90	.89	.014	2	71	1.39	43	.10	6	1.82	.06	.54	5	12	5
88-AW-179	77	850	11	32	.3	67	44	165	4.35	66	5	ND	1	39	1	2	2	45	1.22	.021	2	38	.71	10	.08	5	2.02	.17	.07	1	5	5
88-AW-181	2	2272	5	74	1.2	24	116	370	13.13	9	5	ND	1	19	1	2	2	34	.82	.012	2	13	.29	8	.17	8	.82	.09	.02	1	24	5
88-AW-184	13	1363	12	23	.4	70	62	128	5.91	45	5	ND	1	37	1	2	2	37	1.32	.027	2	29	.46	7	.11	4	1.71	.15	.02	1	3	5
88-AW-185	17	275	17	55	.3	82	49	286	18.50	17	5	ND	1	18	1	6	2	188	.58	.016	2	59	1.03	30	.13	11	1.80	.05	.18	1	4	5
88-AW-187	3	737	10	25	.3	94	36	90	3.77	52	5	ND	1	79	1	2	2	39	2.25	.024	2	50	.35	11	.07	5	3.38	.32	.08	3	8	5
88-AW-189	887	1564	4	26	.6	62	24	162	2.83	4	5	ND	1	18	1	2	2	23	.58	.003	2	23	.57	7	.02	6	.59	.01	.04	4	10	5
88-AW-153	9	1487	55	20	7.3	31	107	20	7.78	250	5	ND	1	12	1	7	2	3	.01	.003	2	6	.01	16	.01	4	.19	.01	.14	1	93	40
88-AW-194	489	831	9	26	.4	23	13	73	12.41	15	5	ND	2	24	1	2	2	88	.35	.043	2	22	.13	6	.03	4	.78	.07	.02	1	65	10
88-AW-195	6	133	6	50	.2	32	14	1032	5.17	99999	5	ND	1	44	1	417	2	76	3.92	.018	2	39	.52	14	.02	11	1.98	.07	.06	1	3	5
88-AW-196	77	1738	13	26	.5	81	76	81	8.70	99999	5	ND	1	143	1	74	2	41	2.73	.033	2	33	.22	25	.01	13	5.53	.15	.04	1	9	5
88-AW-197	1	66	5	44	.1	26	11	989	2.68	1017	5	ND	1	92	1	2	2	58	23.24	.017	5	68	1.09	7	.03	4	1.75	.01	.05	1	8	30
88-AW-199	1	495	2	15	.1	9	5	3314	1.33	1135	5	ND	1	83	1	2	2	40	25.83	.012	9	18	.37	5	.01	5	.55	.01	.02	1	6	80
88-AW-201	1	256	2	29	.1	20	11	1188	3.20	76	5	ND	1	26	1	2	3	83	8.16	.027	4	24	1.75	8	.01	6	.39	.01	.04	2	2	60
88-AW-203	1	166	7	62	.2	36	16	959	4.01	282	5	ND	1	40	1	15	2	124	15.18	.021	2	33	2.39	6	.01	4	.25	.01	.01	1	3	2400
88-AW-204	1	152	2	77	.1	47	33	1459	8.98	24	5	ND	2	4	1	2	2	240	.23	.062	8	71	.10	13	.01	7	.51	.01	.01	1	7	30
88-AW-206	1	150	5	38	.1	30	12	349	2.74	31	5	ND	1	23	1	2	2	80	3.41	.032	4	9	.61	10	.43	10	1.89	.06	.02	1	11	20
88-AW-207	1	105	2	74	.1	43	20	1067	4.98	310	5	ND	1	75	1	2	2	76	12.90	.014	3	44	2.76	11	.01	14	.31	.01	.09	1	3	760
88-AW-208	1	15751	9	38	9.4	32	13	391	3.19	84	5	ND	1	46	2	2	2	80	21.05	.010	3	68	1.02	2	.15	8	2.65	.01	.01	1	37	80
88-AW-209	2	180	161	98	4.2	38	17	496	2.84	101	5	ND	1	3	1	61	2	39	.15	.008	2	21	.07	9	.01	12	.26	.01	.09	1	24	130
88-AW-210	1	15843	7	36	5.0	44	17	345	3.55	12	5	ND	1	16	1	2	2	101	5.70	.017	3	27	1.32	4	.22	18	3.86	.01	.01	1	38	60
88-AW-211	1	126	9	27	.2	21	12	497	3.24	11	5	ND	1	10	1	2	2	95	6.05	.029	5	12	.68	9	.33	11	3.50	.01	.01	1	7	30
88-AW-212	1	322	6	57	.1	15	9	2572	2.62	20	5	ND	3	58	1	2	2	24	27.79	.013	7	12	.66	11	.01	7	.69	.02	.01	1	5	40
88-AW-215	1	162	13	56	.1	47	29	975	6.30	48	5	ND	1	53	1	5	2	118	8.19	.031	5	55	2.32	129	.01	11	1.47	.01	.10	1	6	1900
88-AW-216	1	337	5	53	.7	22	20	2011	5.74	9	5	ND	1	103	1	2	2	82	12.97	.013	6	17	1.86	735	.01	4	.45	.01	.04	1	4	20
88-AW-217	1	383	5	70	.1	36	20	1214	4.59	27	5	ND	1	64	1	2	2	112	11.67	.038	8	38	1.16	16	.01	7	1.46	.01	.05	1	3	40
88-AW-218	1	87	5	69	.1	33	23	1865	6.54	25	5	ND	1	60	1	2	2	106	11.24	.014	5	18	2.96	22	.01	8	.23	.01	.01	1	5	1800
88-AW-219	1	115	13	137	.1	83	49	1468	9.82	48	5	ND	1	30	1	122	2	205	2.60	.048	7	73	1.18	28	.01	17	.50	.01	.09	3	3	15600
88-AW-220	1	156	12	231	.3	85	52	1348	9.45	232	5	ND	1	36	1	100	2	121	2.96	.051	4	47	1.81	32	.01	22	.47	.01	.11	2	2	5600
88-AW-221	1	106	9	75	.1	60	27	1184	5.81	7	5	ND	1	58	1	2	2	134	10.15	.026	4	81	3.02	18	.01	7	2.93	.01	.03	1	7	150
88-AW-222	3	15037	4	266	31.0	39	454	105	5.50	1258	5	4	1	2	3	2	2	9	.18	.004	2	9	.09	6	.01	5	.16	.01	.01	1	4345	70
RLW-88-5	2	882	8	29	.2	13	15	131	3.49	75	5	ND	1	68	1	2	2	42	.99	.042	2	19	1.18	19	.03	4	1.87	.14	.09	2	14	60
STD C/AU-R	18	60	42	133	6.7	69	31	1017	4.15	37	19	8	39	49	18	16	22	60	.49	.093	40	54	.95	180	.07	33	1.90	.06	.13	12	520	1300

___ Assay required for correct result for Cu, As > 1%.

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: SEP 1 1988
DATE REPORT MAILED: Sept. 8/88.

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp AU** BY FIRE ASSAY FROM 1/2 A.T.

ASSAYER: C. Leong. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT DOVE FILE # 88-3895R

SAMPLE#	AU** oz/t
JLP 88-16	.112
JLP 88-28	.053
JLP 88-31	.050
JLP 88-32	.079
JLP 88-52	.058
JLP 88-54	.876
RLW 88-4	.158

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: OCT 24 1988
DATE REPORT MAILED: Oct 27/88

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp AU** BY FIRE ASSAY FROM 1/2 A.T.

SIGNED BY.......... D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT-DOVE FILE # 88-5211R

SAMPLE#	AU** oz/t
88-AW-222	.125

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: JUNE 24 1988
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: July 14/88

GEOCHEMICAL ANALYSIS CERTIFICATE

- SAMPLE TYPE: REJECT HG ANALYSIS BY FLAMLESS AA.

ASSAYER: C. Leong D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. File # 87-3362R

SAMPLE#	HG ppb
RT-36	5
RT-52	10
RT-70	5
RT-106	160
RT-108	2500
87-51	20
87-52	20
87-53	5
87-55	5
87-58	5
87-59	40
87-60	340
87-62	10
87-64	20
87-67	30

ACME ANALYTICAL LABORATORIES LTD.
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DATE RECEIVED: JUNE 24 1988
DATE REPORT MAILED: July 14/88

GEOCHEMICAL ANALYSIS CERTIFICATE

- SAMPLE TYPE: REJECT HG ANALYSIS BY FLAMLESS AA.

ASSAYER: C. Leong .... D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. PROJECT-DOVE File # 87-4215R

SAMPLE#	HG ppb
RT-111	10
RT-113	20
RT-114	20
✓ RT-116	20
✓ RT-117	30
✓ RT-118	5
✓ RT-119	5
RT-121	250
87-68	30
✓ 87-69	10
87-70	380
87-73	470
✓ 87-75	120
✓ JLP-95	420
✓ JLP-96	210
JLP-97	120
JLP-100	450
✓ JLP-101	30
✓ JLP-104	40
JLP-106	70
JLP-107	40
JLP-108	90
✓ JLP-111	10
JLP-113	10
JLP-114	60
JLP-116	5
JLP-117	5
JLP-118	5
JLP-124	10
JLP-125	5
JLP-126	5
JLP-127	5
JLP-128	30

✓ from pulp.

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DATE RECEIVED: JUNE 24 1988
DATE REPORT MAILED: July 11/88.

GEOCHEMICAL ANALYSIS CERTIFICATE

- SAMPLE TYPE: Pulp HG ANALYSIS BY FLAMLESS AA.

ASSAYER: C. Leong. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. File # 87-3096R

SAMPLE#	HG ppb
87-20	5
87-23	5
87-24	350
87-28	5
87-30	5
87-33	5
87-34	5
87-39	10
87-44	30
87-49	60
87-50	30
RT-39	10
RT-43	5
RT-91	2800
RT-94	20

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DATE RECEIVED: JUNE 24 1988
DATE REPORT MAILED: July 14/88.

GEOCHEMICAL ANALYSIS CERTIFICATE

- SAMPLE TYPE: REJECT HG ANALYSIS BY FLAMLESS AA.

ASSAYER: C. Leong. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTMIN RESOURCES LTD. File # 87-2290R

SAMPLE#	HG ppb
HR-1	15000
HR-2	9300
HR-3	5800
HR-4	100
HR-5	150
HR-6	110
HR-7	82000
HR-8	4000
HR-9	45000
HR-10	860
HR-11	6800
HR-12	47000
JLP-47	220
JLP-53	16000
JLP-56	1800
JLP-77	120
✓JLP-83	8600
✓JLP-84	33100
✓JLP-85	44400
JLP-89	5
JLP-91	5
JLP-92	2800
RLW-87-6	20
✓RLW-87-7	146300
RLW-87-8	500
RLW-87-9	3600
RLW-87-10	9800
✓RLW-87-11	70900
RLW-87-12	7800
RLW-87-13	1600
RLW-87-14	1100
✓RLW-87-17	8200

✓ from pulp.