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REPORT

ON THE

VLF-EM AND MAGNETOMETER SURVEYS

MOW CLAIM GROUP

ARROWSTONE PROJECT

DEADMAN RIVER VALLEY, BRITISH COLUMBIA

KAMLOOPS MINING DIVISION

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INTRODUCTION

This report describes a VLF-EM and Magnetometer survey conducted October 2-4, 1989, on 11.6 kms of line on the MOW Claim Group. The property consists of 72 units in 4 claims located approximately 60 kms northwest of Kamloops, B.C., in the Deadman River Valley.

The property is held under option by Iron River Resources Limited of Campbell River from the owner Michael Dickens of Savona, B.C.

Copper mineralization was found at two locations on the property by M. Dickens in 1980, with subsequent exploration being done by Canamax Resources and Northair Mines Ltd. in 1983 and 1984. The mineralized areas appear to be located along a major northwest-southeast striking structural break indicated by aero-magnetics. The present geophysical survey was located on the strike of this zone, with the aim of finding new sources of mineralization.

This report concerns the 1989 data collected on lines 10900E thru to 11600E. This data has been combined with the 1988 data for continuity, since it is contiguous data to the west.

LOCATION AND ACCESS

The property is located approximately 60 kms northwest of Kamloops, B.C., in the Mowich Lake area of the Deadman River Valley. Access is by 29 kms of paved and gravel road from the Trans-Canada Highway at a point 5 kms west of the village of Savona.

TOPOGRAPHY AND CLIMATE

The Deadman River Valley is relatively narrow with moderately steep sides. Topography on the claims is moderate to rugged with elevations ranging from 650m to 1200m.

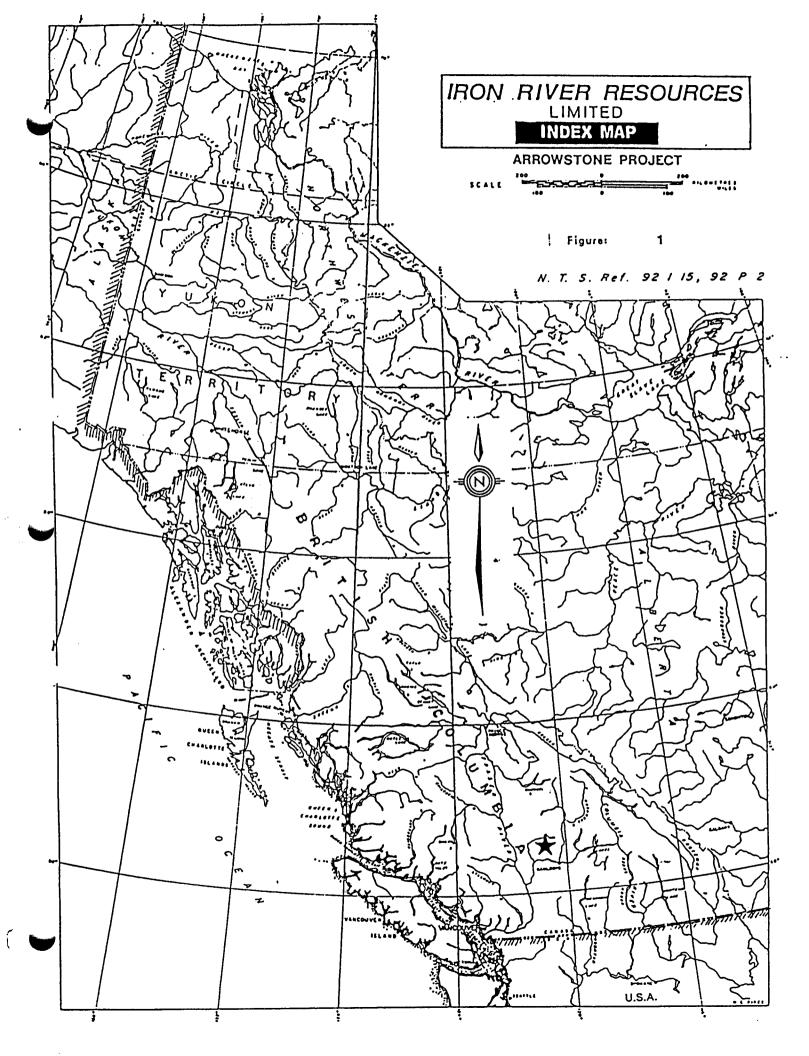
Outcrop is best along cliffs, creeks and road cuts and relatively poor elsewhere. There are very few exposures in the area of the present program.

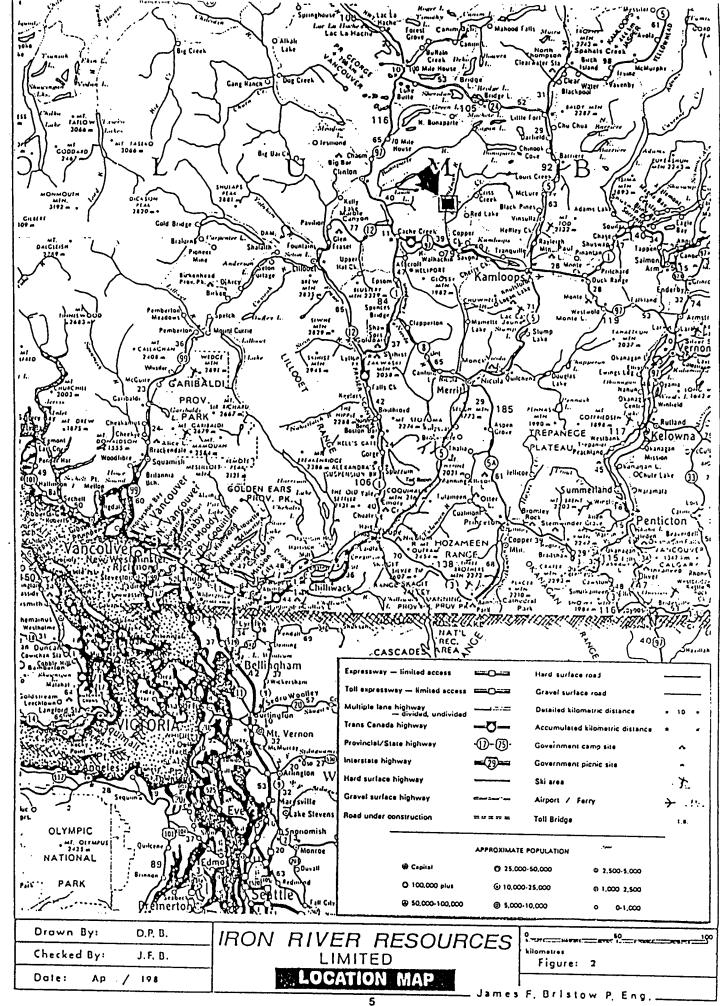
The claims are forested mainly by Lodgepole Pine, with generally light underbrush.

The climate is typical of the interior plateau, with warm summers and cold winters. Snow free conditions usually exist from April to mid-November.

HISTORY

The area has seen sporadic activity since the late 1870's, with the earliest reference in the Index to Annual Reports of the Minister of Mines being 1879. The only major producer in the immediate area was the Vidette Mine located 14 kms north of Mowich Lake. During the 1930's. 54190 tons grading 0.550z/ton gold, 0.860z/ton silver and 0.09% copper were produced from narrow quartz veins.





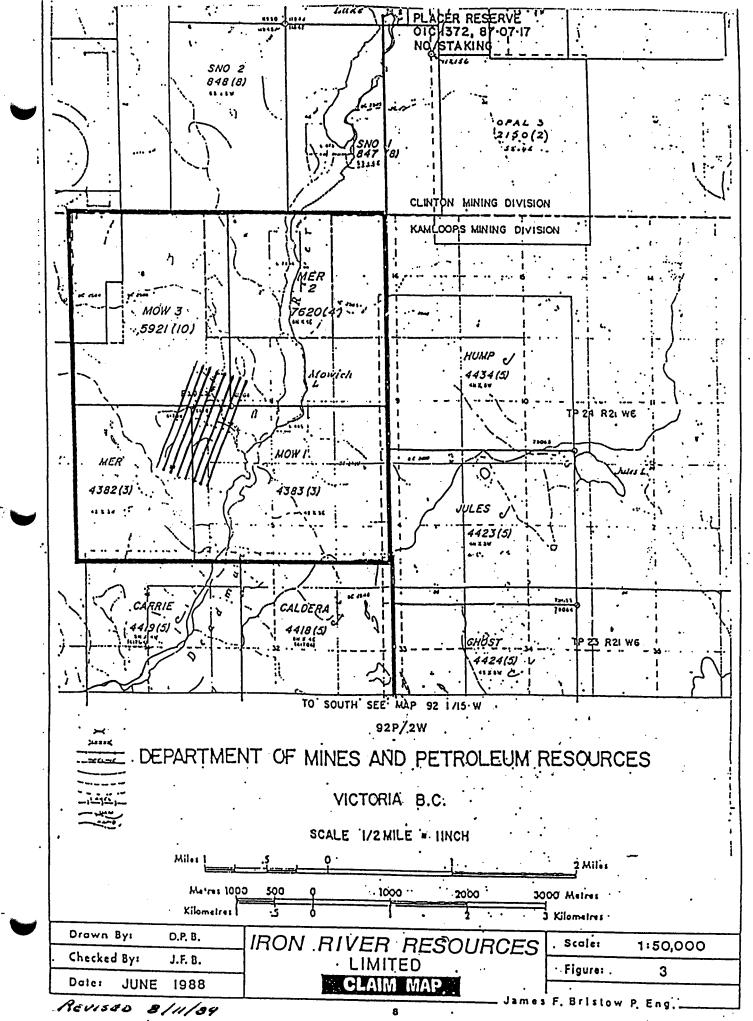
Recent history of the property is as follows:

- 1980 Prospecting and soil sampling by M. Dickens.
- 1983 Preliminary evaluation report by N.L. Tribe.
- 1983 Prospecting, soil sampling, magnetometer and I.P. surveys by Canamax Resources.
- 1984 Road building and trenching by Northair Mines Ltd.
- 1988 Property optioned to Iron River Resources Limited. - Electromagnetic and Magnetometer Surveys.
 - Induced Polarization Survey.

CLAIMS (See Figure #3)

The property consists of four contiguous metric claims totalling 72 units.

<u>Claim</u> <u>N</u>	lame Unit	<u>s</u> <u>Record</u> <u>Date</u>	Record	No. Expiry Date
MOW 1	. 20	23/3/83	4383	23/3/90
MOW 3	3 20	25/10/84	5921	25/10/89
MER	12	23/3/83	4382	23/3/90
MER 2	20	27/4/88	7620	27/4/90



GEOLOGY

REGIONAL GEOLOGY (Figure #4)

The Mowich Lake property is located in the southern segment of the geological zone known as the Quesnel Trough; a northerly trending belt, up to 45 kms wide, of Upper Triassic age Nicola Group volcanic and sedimentary rocks.

The Quesnel Trough units lie between Permian and older volcanics and sediments to the east and Permian Cache Creek limestones to the west. The Nicola Group has been intruded by Triassic/Jurassic age intrusives of the Thuya and Takomkane batholiths and younger Cretaceous alkaline to calcalkaline stocks.

The region is covered by a thin layer of Miocene siliceous ashes and tuffs (Deadman River Formation) and by Eocene plateau basalt.

LOCAL GEOLOGY

The Nicola rocks underlying the Mowich property have been partially exposed by erosion of the plateau basalt and Deadman River Formation along the Deadman River Valley. This recent erosional window traverses the centre of the property in a North-South direction exposing a section of Nicola Group rocks between the younger formations along the properties East and West margins.

A brief description of the rock types (after Canamax Resources 1984) exposed in the immediate area of the claims is as follows:

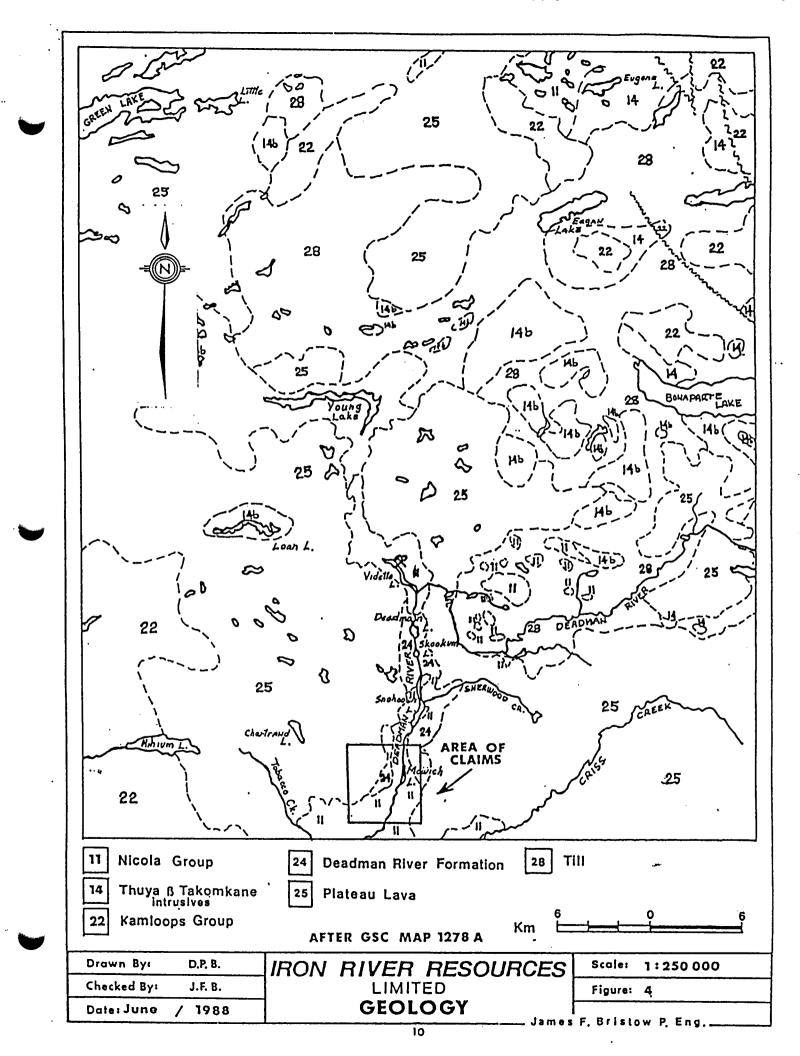
NICOLA GROUP SEDIMENTS

(a) Argillite - generally massive to poorly bedded with occasional thin bedded siltstones.

(b) Greywacke - interbedded with argillites and composed of subangular grains less than 1mm and black to grey in colour depending on the quartz and feldspar content.

(c) Limestone, Chert, Quartzite and Conglomerate occur in minor amounts with argillite and greywacke.





NICOLA GROUP VOLCANICS

(a) Polymictic Breccia - a distinctive maroon to green colour, composed of Fragments to 0.5 metres of sediments, syenodiorites, volcanic andesites and augite porphyry in an andesite groundmass. Hematite and epidote alteration is common.

(b) Andesite Breccia - occurs only along the east side of Mowich Lake and consists of rounded to angular clasts to 20cm of fine grained, light green andesite and augite porphyry with minor limestone. The groundmass is tuffaceous andesite and carbonate.

(c) Augite Porphyry - appears to be a flow rock forming the top of the Nicola Formation. It is massive, dark grey green, aphanitic groundmass with up to 8% phenocrysts of augite crystals to 5mm. It can contain up to 10% amygdaloidal material in brecciated areas.

INTRUSIVE ROCKS

The intrusive outcrops mapped by Canamax Resources all occur to the west of the Deadman River. They are reportedly diorite and syenite in composition with a maximum indicated surface exposure size of 300 metres.

TERTIARY ROCKS

(a) Deadman River Formation - this formation unconformably overlies the Nicola Group Rocks. It is composed of Miocene age non-marine tuffs, ashes and arkoses with minor conglomerates and agglomerates. The arkose unit is poorly consolidated and believed to be quite thin. The tuff is white to yellow in colour, fine grained and in at least one area 30 metres thick.

The Deadman River Formation was apparently deposited on a very uneven land surface. Outcrops are primarily high on the valley walls, but some material is found almost to the valley bottom. Some of the latter may be due to downhill movement of the poorly consolidated tuffaceous material.



(b) Plateau Basalt - probably of Eocene age, dark grey to brown in colour with variable olivine and often vesicular.

STRUCTURES

The Nicola Group rocks strike northerly with moderate to steep dips to the east and west. Mapping to date suggests there is no repetition due to folding. The Deadman River Valley is believed to be underlain by a major fault with possible left lateral movement in the order of 600 metres. Several apparent northwest-southeast faults have been recognized with some suggestion of accompanying block faulting.

Quartz-carbonate veining in the Nicola and Deadman River formations indicate a hydrothermal system was operating in the post-Tertiary period. Serpentinite, ankerite and mariposite alteration found on the property are further evidence of the presence of a deep seated "plumbing" system.

MINERALIZATION

Mineralization is found at two areas on the property. One showing is located 1000 metres east-southeast of the bridge over the Deadman River. Chalcopyrite with low gold values is found in a shear zone striking southeast and in amygdales in augite porphyry over an area roughly 50 by 150 metres. Sampling has indicated average values in the order of 2% copper and 0.018/t gold.

The second showing is located 75 metres southwest of the bridge on the west bank of the Deadman River. Mineralization is exposed in a pit and consists of malachite coated clasts of chalcocite up to 6 cms in diameter. The clasts are in overburden and highly altered sub-outcrop. The material is strongly serpentinized and appears to have come from a shear zone. Values for selected clasts of chalcocite are 50% copper, 8 oz/t silver and 0.25 oz/t gold.



- 6 -

EXPLORATION PROGRAM

The present program was located to cover an area to the northwest of the known mineral showings. Evidence indicates that structural breaks, which may be associates with mineralization, strike in that direction. Outcrops of clastic material located in the area of the MER and MOW 1 legal corner posts and believed to represent the base of the Deadman River formation, are intensely serpentinized and similar in composition to the material containing the chalcocite mineralization 1000 meters to the southeast.

VLF/EM and magnetometer were selected as being the best geophysical tools to locate shear zones and conductive mineralization. The geophysical program was done October 2-4. 1989, by Delta Geoscience Ltd., using two instruments and two operators.

V.L.F.

The magnetic and V.L.F. surveys were performed simultaneously, with measurements every 10 meters along the grid lines. The Cutler, Maine V.L.F. station, NAA, transmitting at 24.0 khz was used for this survey. The Annapolis station, NSS, transmitting at 21.4 khz was used for the 1988 survey. Note, that for optimum electromagnetic coupling, the conductor of interest should strike toward the VLF station. For the line orientation and location of the Mow Grid, either transmitter is acceptable and the data is very comparable. East-west and north-west striking conductive features would be well outlined with this transmitter - line orientation geometry.

Three components of the V.L.F. electromagnetic field were measured: the horizontal field strength, vertical inphase and vertical quadrature. All of the vertical in-phase data was subsequently filtered using the Fraser and Hjelt filters. These filtering techniques help to understand the spatial position of conductors, both along strike and downdip. The relevant papers describing these techniques are referred to at the back of this report.

MAGNETICS

Accuracy of the portable magnetometer readings is ± 1 nanotesla. An aluminium staff was used to keep the sensors approximately 2.5 and 3.0 meters above the ground. Magnetic field measurements were corrected for any diurnal variations, through the use of the Omni base station magnetometer.

GRADIOMETER

The magnetic gradiometer is a useful adjunct to magnetic surveying. The gradiometer acts like a filter, in that it enhances local near surface anomalies at the expense of long wavelength regional anomalies. The rate of fall-off of the magnetic field with height is much higher for local sources than for regional sources and therefore a high gradient (rate of change) can be recorded.

Erratic concentrations of near surface magnetite (both within the bedrock and overburden) can create noise for the gradiometer and thus lessen its effectiveness.

A useful feature of the gradiometer data is that it allows a simple calculation to be made for the depth of an anomaly (assuming a dipole field):

> d = -3 (<u>Total Field Anomaly</u>) (Gradient Anomaly)

DATA PRESENTATION

Geophysical data is presented in contoured plans, stacked profile plans, and filtered V.L.F. conductor sections. Contoured plans aid in the spatial view of anomalies.

Stacked profile plans aid in the interpretation of anomalies, since profile shape is largely determined by the depth, dip and width of anomalies. Stacked profile plans also help to give an unbiased view of the line to line correlation of anomalies. Contouring can introduce a bias that may lead to separate anomalies being contoured together. This is especially true in areas of complex geology.

The filtered V.L.F. conductor sections gives an interpretation of the conductors attitude and strength with depth.

EQUIPMENT USED

- 2 EDA Omni Plus systems configured as portable VLF/MAG/GRAD units.
- 1 EDA Omni Base Station Magnetometer.
- 1 Toshiba 3100 Field Computer.
- 1 Fujitsu Printer.

PERSONNEL (DELTA GEOSCIENCE LTD)

Grant Hendrickson		Supervisor/Senior	Geophysicist
Scott Cosman		Geophysicist/Crew	Chief
Tom Bokenfohr	-	Junior Geophysicis	st

Mr. Hendrickson has had 18 years experience in mineral exploration geophysics. Mr. Cosman has worked for Delta Geoscience Ltd. since graduation and has had 4 years field experience. Mr. Bokenfohr is a graduate of the Northern Alberta Institute of Technology, NAIT, geophysics program and has worked for Delta Geoscience for 1 year.

RESULTS

The geophysical data is presented as a series of five maps:

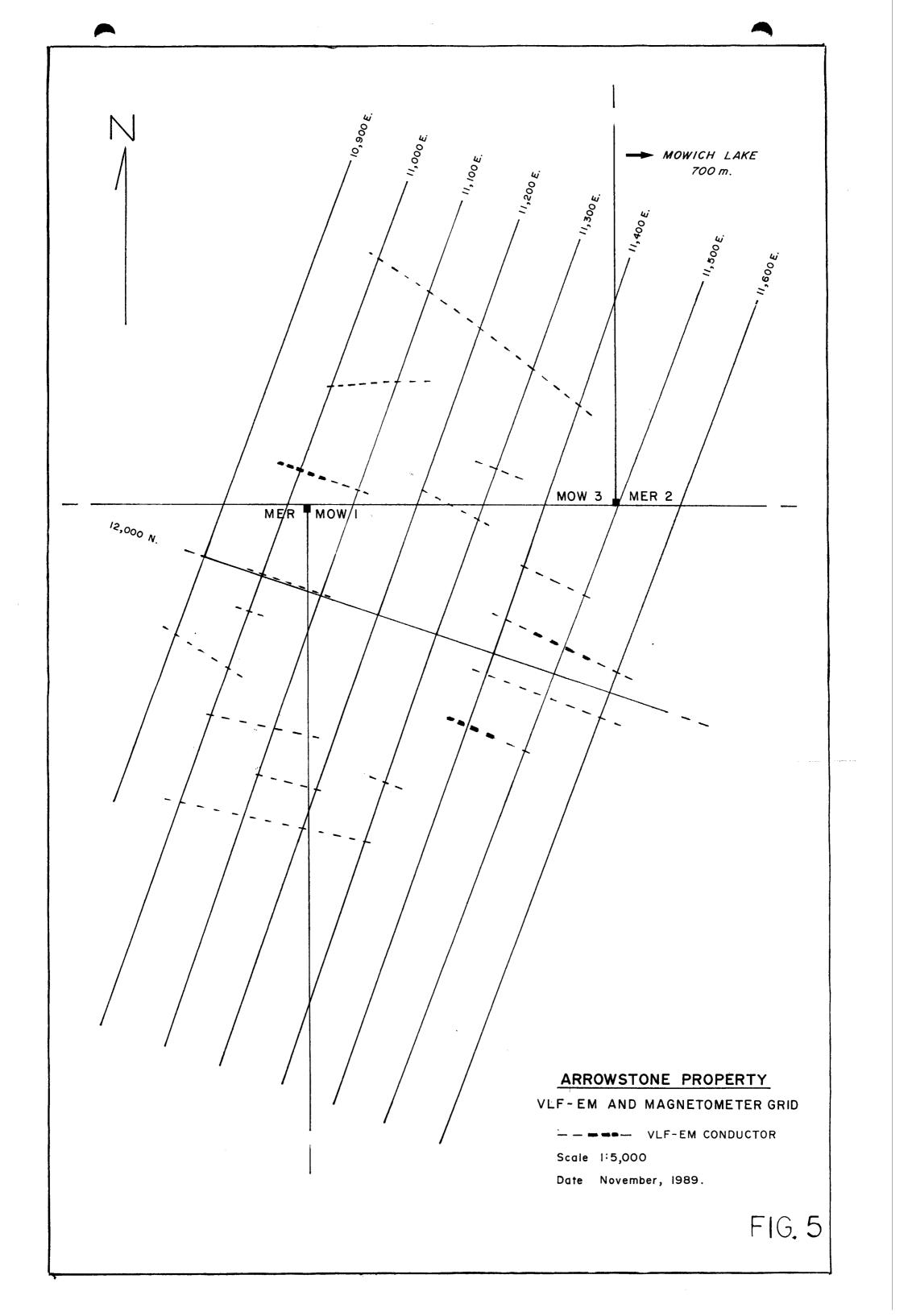
Fig. #6: Total Field Magnetics Plan contoured at a 100 nT interval. The magnetic patterns are complex and show two prominent orientations: (a) east-west and (b) north-northwest.

The east-west orientation may be due to the younger flat lying basalts.

The north-northwest trend may be reflecting magnetic units within the Nicola Group.

- Total field magnetic profiles at 1cm = 500nT and Fig. #7: Fraser filtered VLF profiles at 1cm = 30%. These two data sets have been combined to quickly show the correlation of VLF and magnetic anomalies. Some good sharp correlations exist that deserve more attention. The correlation of a VLF conductor with a magnetic response may be due to a linear concentration of magnetic sulphide minerals, (hydrothermal system). Alternatively the correlation could be due to magnetic dikes (basalt?) injected into a conductive graphitic fault zone. It is also possible to have a combined source. VLF conductors without any magnetic expression may be due to non magnetic sulphide minerals, however it is more likely that most are due to graphitic shear zones, or weakly conductive intercalated sediments.
- Fig. #8: Vertical magnetic gradiometer data. This map accurately shows the near surface distribution of magnetic minerals, in most part the magnetite concentration near surface.
- Fig. #9: Fraser Filtered VLF-EM Plan. This map clearly shows the spatial position, strength and trend of VLF conductors. At times, one should consult the profiles to ensure no contouring bias has been introduced by the computer, particularly if more detailed geological evidence becomes available.

Fig. #10: Vertical in-phase (Tilt Angle) and Horizontal Field Strength Profiles of the VLF data. This map is included to show the actual VLF data. Valid crossovers in the vertical in-phase data will be accompanied by peaks in the horizontal field strength data at the cross-over point. Note that these profiles are plotted increasing (positive) to the right.



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COST STATEMENT

	\$ 4,537.00.
Report Preparation	\$ 450.00.
Line Preparation:	\$ 1,199.00.
Delta Geoscience Ltd	\$ 2,888.00.

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QUALIFICATIONS AND CERTIFICATIONS

I, James F. Bristow, of 9610 Thomas Place, in the Municipality of Richmond, Province of British Columbia, hereby certify as follows:

- 1. I am a graduate of the University of British Columbia with a B.A. Degree (Geology and Physics).
- 2. I am a member of the Canadian Institute of Mining Metallurgy, the Geological Society of South Africa and the Association of Exploration Geochemists.
- 3. I am a Professional Engineer registered in the Province of British Columbia.
- 4. I have actively practiced my profession in mineral exploration and mining since my graduation in 1957.
- 5. That the geological information quoted in this report is based on an examination of the property April 18 and 19, and May 5, 6 and 19, 1988, on data gathered by myself or someone working directly under my supervision and on my personal analysis of the reports and other data listed in the references.
- 6. That I have no interest, either direct or indirect, in the property or securities of Iron River Resources Limited, nor do I expect to receive any.
- 7. That I consent to the use of this report, in or in connections with, prospectus, or a statement of material facts relating to the raising of funds for this project.

Dated at Richmond, British Columbia, this $\underline{\mathcal{IO}}^{\mathcal{T}_{k}}$ day of November, 1989.

James F. Bristow, P.Eng.

STATEMENT OF QUALIFICATION

Grant A. Hendrickson

- B.Science, U.B.C. 1971, Geophysics option.
- For the past 18 years, I have been actively involved in mineral exploration projects throughout Canada, the United States, Europe and Central and South America.
- I am a registered Professional Geophysicist with the Association of Professional Engineers, Geologists and Geophysicists of Alberta.
- I am an active member of the S.E.G., E.A.E.G., and B.C.G.S.

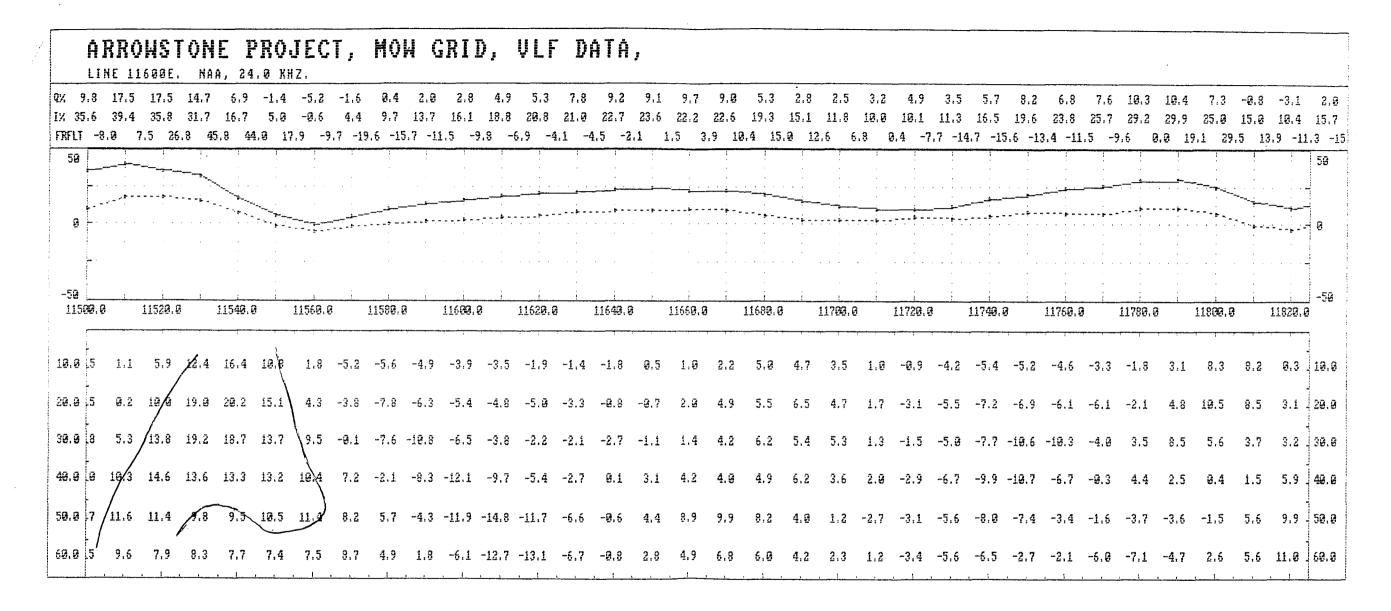
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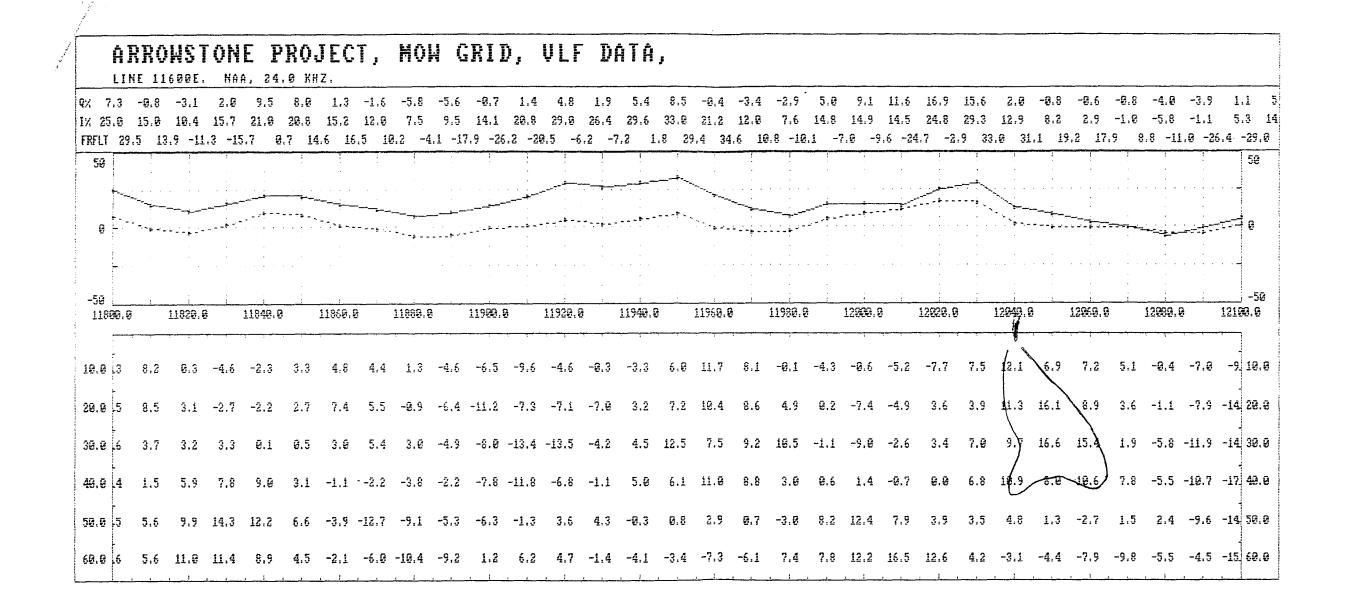
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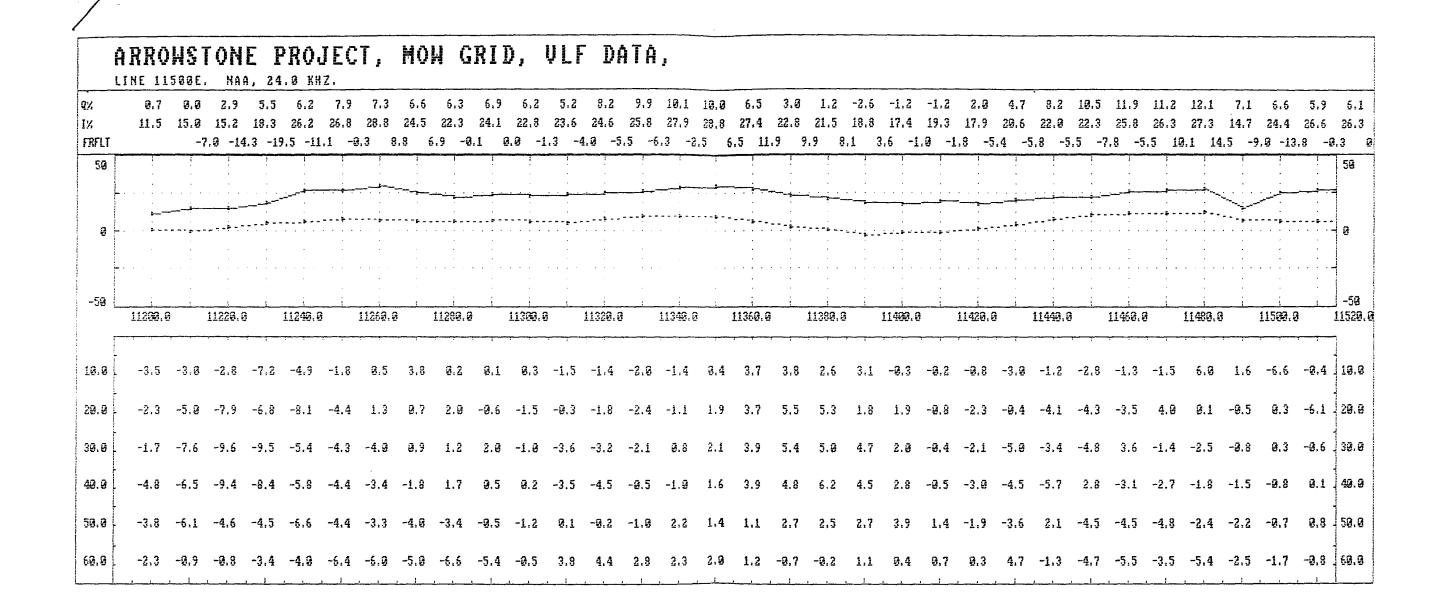
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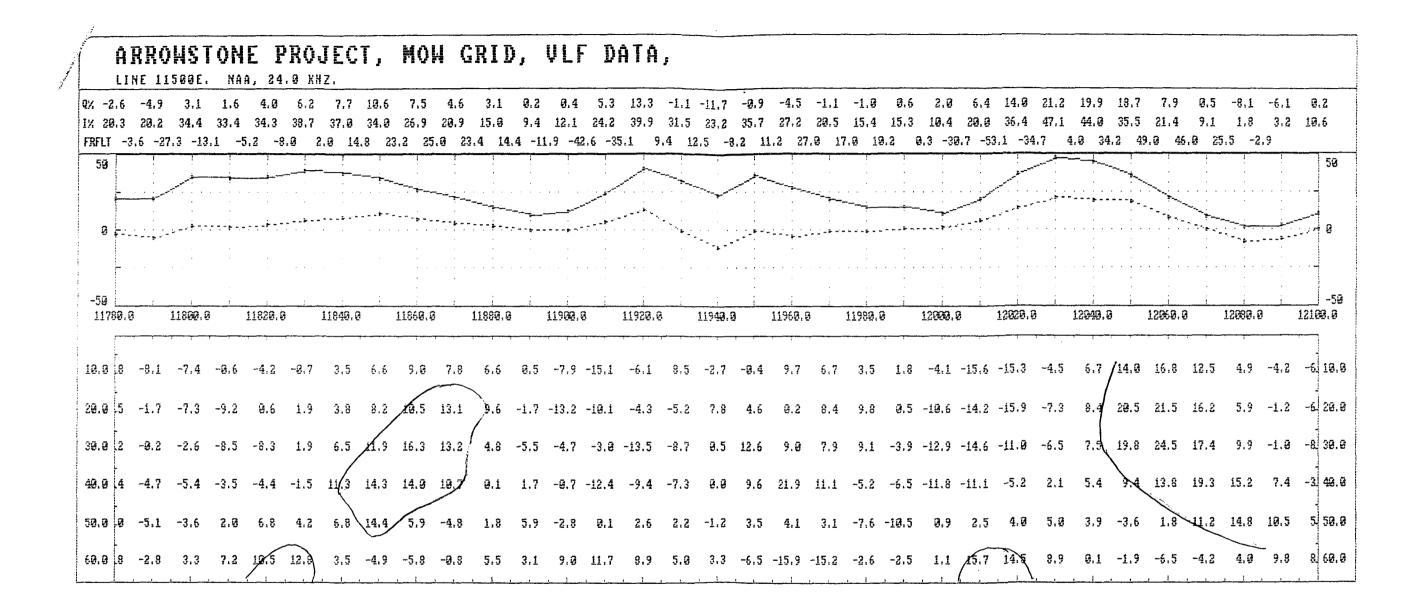
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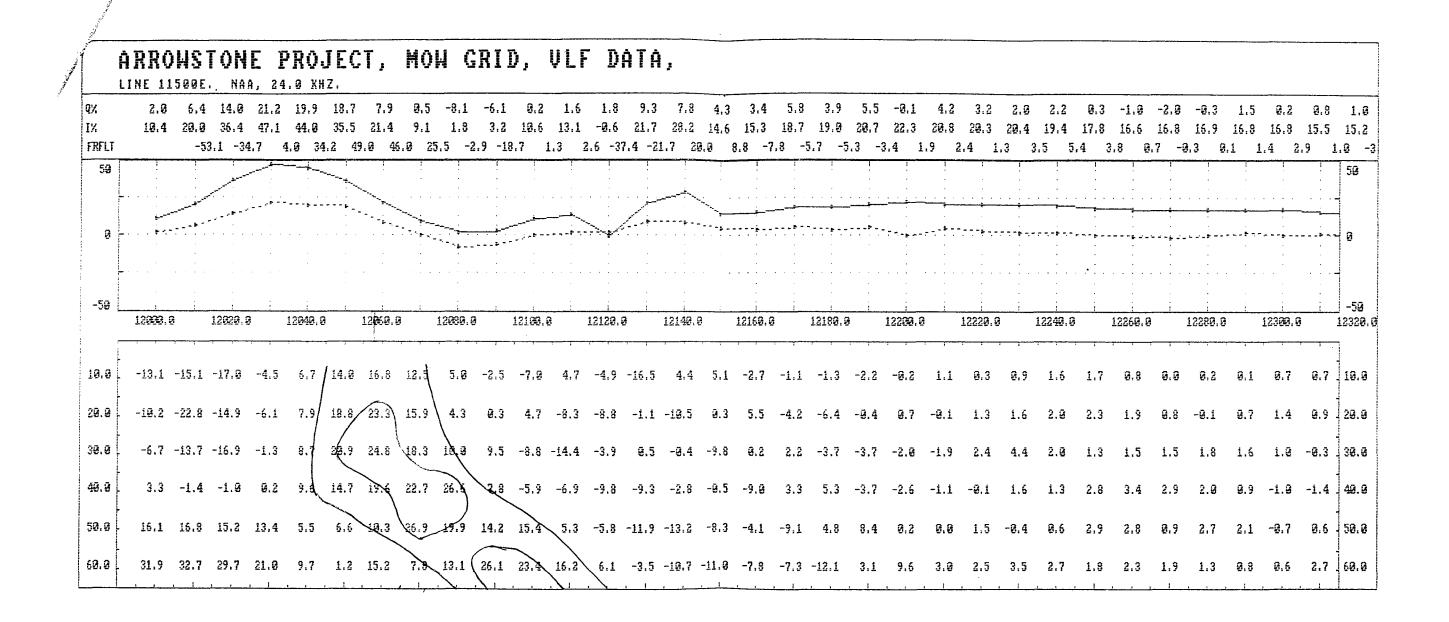






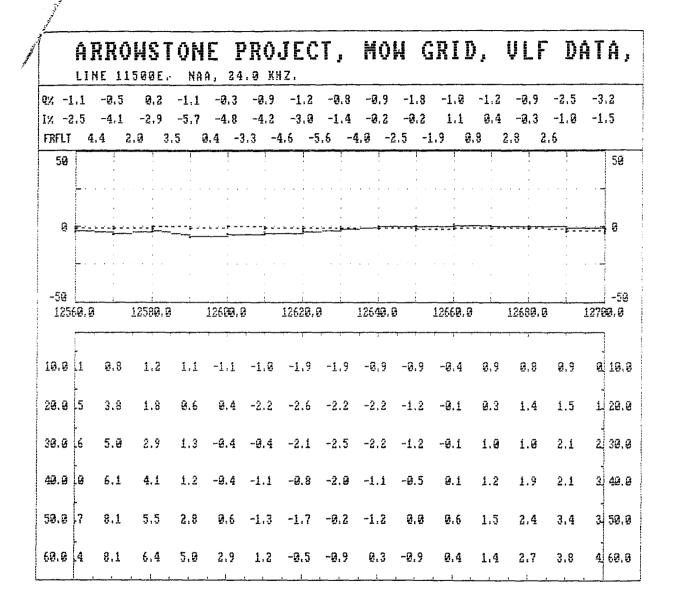
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[11509.0	} 	11520.0	}	11548.8) 	11569.9) ,	11580.0	; ;	11689.0	· · · · ·	11620.0		11649.9	11	.669.0 	116	0.0	11709.	9	11720.(11749.0		11760.0	3	11789.	0	11899,1	
.8 .		···· ; ···	-0.4	11520.0 	-0.6	11540.0 0.0	8,9	11569.9 9.1	9.2		,	-9.3			Ø.5	· ; • •					117 89 .	·····			-1.5	······ 1	, , , , , , , , , , , , , , , , , , , 		~~~~	· • · · · • · ·	·	[
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8 9) <u>1</u> .6 -9.5 i -9.8	-6.6 9.3 9.3	-0.4 -6.1	0,0 -1.5	-0.6	8.8 8.6	8,9 -1.2	0.1 9.7 -0.2	0.2 ~9.4	-2.5 -2.5 -1.6	-0.6 -0.7 -9.7	-9.9 -9.6	-2.1 -2.8 -3.2	-9.5 8.4 8.1	0.5 0.4 0.6	1.3 9.4	0.1 9.8 0.5	9.9 9.1 - 8.9 -	8.1 -1 2.8 -9 3.8 -2	0 -0. 6 -2. 7 0.) -1.9 1 -1.8	-0.4 -1.3 -2.6	8.3 -8.8 -3.6	-1.9 -9.2	-1.5 -4.8	-0.4 -2.7 2.7	9,4 4.6 4.9	5.0 5.4 -2.5	5.8 -2.5 -9.2	-8.1	-7.4 -7.3 -2.6	
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	0.0 4	0.7 0.9	-9,5 -9,5	-1.3 -1.9	-1.6 -8.4	1.2 1.8	2.8	1.1 3.6	1.3 1.1	-0.5 0.1	- <u>1</u> .4 - 2 .9	-0,3	-0.4 2.9	3.8 3.4	4. <u>1</u> 3.6	9.3 4.9	9.7 -9.2	-1.0 -0.8	-1.6 -8.8	-1,1 9.3	8.6 2.2	3.0 4.0	3.3 6.6	3.9 6.7	4.3 7.0	4.0 6.4	3.1 4.5	0.8 3.8	1.2	1.1 9.6	-1.1 8.4	-1.0	-1.9 -2.6	[
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Q%	-2.0	-2.8	3 -1.6	1.3	3 2	1.5	3.7	3.7	2.0	1.2	2.5	3.2	9.6	-0.2	0.0	-0.6	-1.0	-9.5	2.1	3.8	3.0	3.2	4.1	5.6	7.1	9.7	7.6	5.5	4.8	4.8	6,1	7.0	6.6	8.0
IX	27.4	24.1	L 21.2	18.	8 16	.8	14.6	12.3	9.2	6.5	9,4	10.5	8,9	8.7	8.2	8.7	9.0	8,4	10.2	12.5	12.1	9,8	8,8	8,1	7.7	7.8	8.1	7.3	8.3	10.2	11.9	13.3	15.4	17.6
FRFLT		2	11.5	9.7	8.6	8.5	79.	.9 11	.2 5	i.6 -4	.2 -3	1.5 2	.3 1	2.5 0	1.7 -1	0.8 -(1.5 -1	8,9 -5	5.3 -	6.0 0	1.8	6.9 5	i.0 2	2.8 1	.4 -().1 g).1 0	8.3 -3	.1 -6	5.5 -6	.7 -6	.5 -7	'.8 -'	7.1 -3
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-	11200.0	ļ ,	11229.	0	112	49.9	1	11260.0) ,;	11280.0		11300.0		11320.0	3 	11349,1	3	11360.4	8	11380.0	} 	11400.(ð 	11420.0) 	11449.0	3 	11469.0]	11480.0	} 	11568.1	9 9	11520.(7
10.0	3.7	3,9	4.0	3.4	4 3	.4	3.5	3,4	3.6	9,4	-1.9	6,5	8.7	8,3	0.2	-0.6	-9.1	-0.8	-2.2	-1.0	1,5	1.8	1.2	0.9	8,4	-9,2	0,1	-9,4	-2.0	-2.4	-2.4	-2.5	-2.8	19.0
29,9	3.5	6.9	6.6	5.6	55	.5	6.7	7.1	4.0	1.3	9.8	-8.6	i.1	i.i	-8.3	-9.1	-8.9	-1.8	-1.6	-9.7	6.7	2.6	2.4	0.6	9.9	8.4	-9.5	-1.8	-2.6	-3.8	-4.4	-4.6	-4.1	28.0
30.0	2.6	5.3	8.3	8.3	38	.4	8.3	5.7	4.5	4.5	3.0	1.3	-0.3	1.3	2.2	0.2	-1.7	-2.2	-0.8	8.2	0.2	1.9	2.1	1.6	0.6	-0.6	-2.9	-2.7	-3.1	-4,3	-6.2	-6.1	-5.8	30.0
49.9	1.2	4.5	5 7.6	11.1	l 11	.1	7.5	5.2	4.9	4.6	4.4	3.5	2.0	0.5	0.8	9.9	-9.8	9.1	-9.1	9.9	9.1	-9.7	0.5	2.4	1.6	-9.7	-2.4	-3.8	-5.1	-6.3	-6.1	-5.8	-5.3	49.8
50.0	0.4	3.5	i 6.9	9.9) 10). <u>2</u>	8.3	7.5	6.3	5.5	4.2	3.1	2.7	0,3	-2.3	-0.2	1.4	9.6	9.7	0.6	0,5	0.3	9.4	0.6	0,5	-9,4	-2.5	-4,3	-5.7	-6.4	-6.3	-5,8	-6.6	50.0
69.0	-1.0	2.5	6.1	6.5	57	.7	19.6	9.2	7.8	5.9	4.4	3.5	1.2	-1.1	-2.3	-2.3	0,3	1.9	1.8	1.5	Ø.9	1.6	8.8	-1.0	-1.1	-0.4	-2.9	-5.0	-5.5	-5.7	-6.9	-6.7	-6.7	68.0

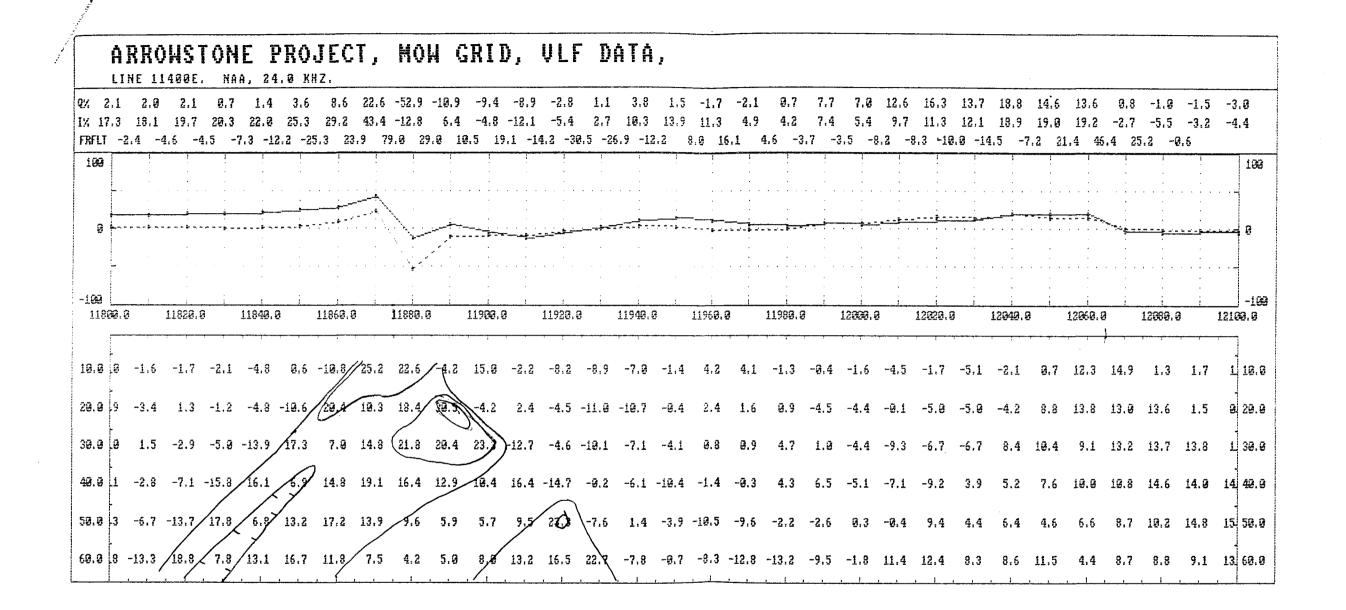
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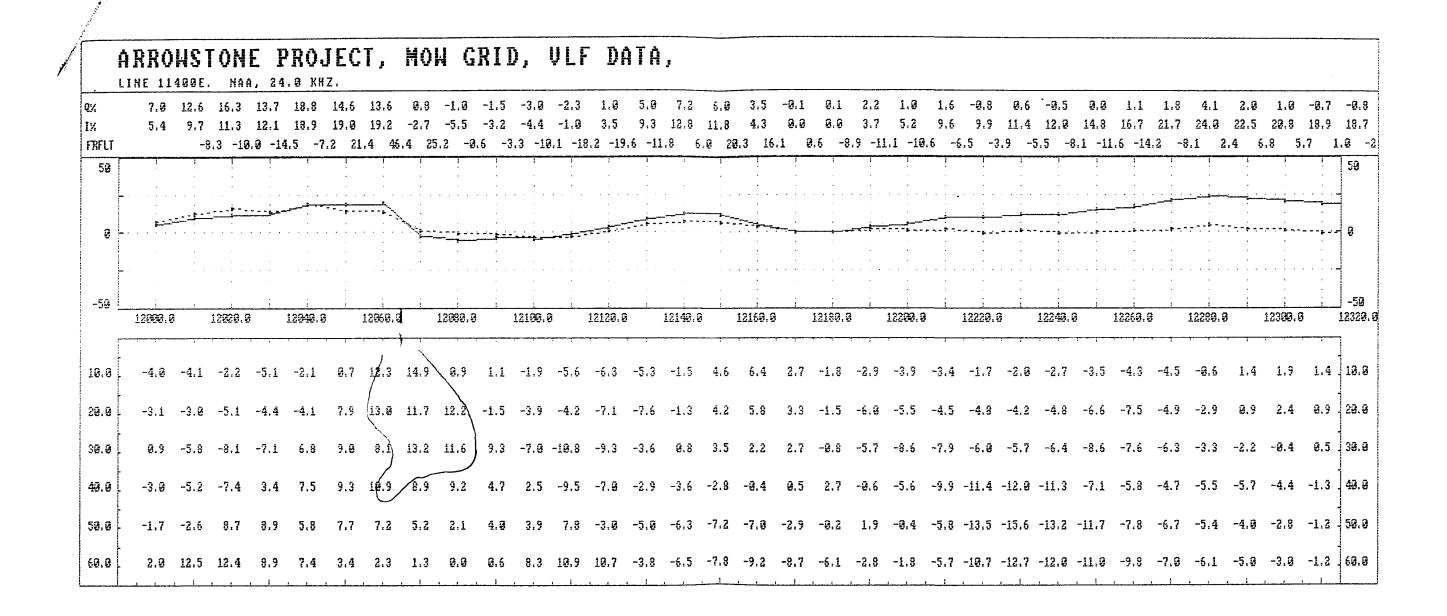
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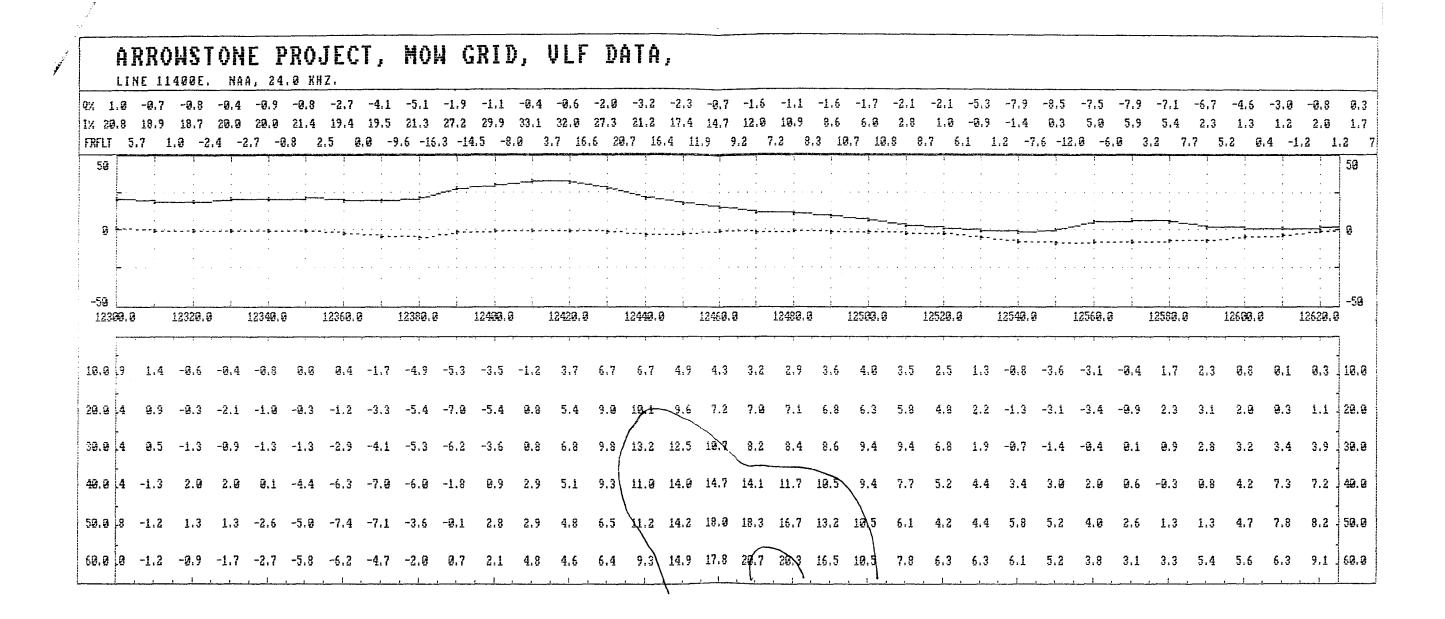
10 Jan

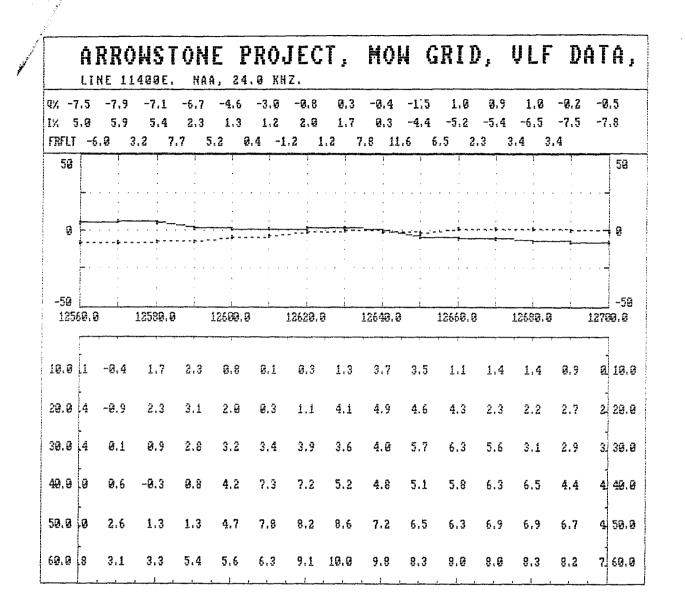
Q% 7.1	36.	6	8.0	6.7	5.0	5.9	6.6	9.2	8.5	9.9	9,9	9.4	5.8	3.7	3.1	1.8	8.5	0.8	-0.6	-3.5	-3.9	-1.4	0.0	-0.2	0.7	1.7	2.2	5,1	4.1	2.5	2.1	2.0	2.1	Ø
	-																		18.7												17.3			
FRFLT	-7.8	-7.1	-3.2	-0,	2 -0	.2 -1	.8 -3	<u>,1</u> -	2.4 -:	1.4 -	1.5 2	.2	5.3 2	2.0 -	1.5 -6	.2 (1.5 0	.9 2	.7 4	7 0		.3 -2	2.7 -1	.9 -2	2.4 -1	.5 -2	1.1 0	1.9 :	2.1 1	.7 9	1.6 -2	.4 -4		
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11500	1.0	113	20,0	<u>1</u>	1549.0		11560.(ð	11580.	2	11699.0	3	11620.0	2	11640.0	3	11660.0		11680.0		11700.0		11720.0		11748.0	I	11760.0	3	11780.0		11800.0	ł	11820.0	0
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19.0	5 -2.	8 -	1.9 -	0.6	-0.2	-0.4	-8.9	-1.1	-8.5	-0.2	-0.4	1,6	2.0	-0.7	0.3	-9,1	0,5	0.3	1.2	1.4	-1.0	~0.8	-0.8	-0.6	-1.1	8.1	-0.2	9.7	8.6	9 ,2	0.0	-1.6	-1.7	1
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20.0 16	5 -4.	i -:	8.5 -	2.2	-1.1	-i.3	-1.4	-1.2	-1.5	-0.8	1.2	1.4	9.9	2.0	-0.5	9.2	9.4	1.8	1.4	9.2	0,4	-1.5	-1.3	-1.2	-9.3	-1.1	9.2	8.2	0.5	-9.1	-1.9	-3.4	1.3	20
	_	_																			- <i>i</i>					- ·		~ ~						-
30.0 []	- ð .	9 -	1.9 -	3.2	-2.6	-2.1	-1.8	-2.3	-2.1	-0.2	1.1	8.7	1.5	0.7	1.8	-0.8	1.3	1.5	0.8	1.0	U.1	9.8	-2.4	-1.5	-1.3	-0.1	-8.9	6.8	-2,1	3.8	1.8	1.3	-2.9	1 38
ŀ	-5.	3 -4	1.9 -	ā. ā	-4 3	-3.1	-9 å	-1.9	-0.5	-9.5	-1.1	Ø. 1	-04.1	1.1	1.9	3.1	9.8	0.5	9.6	9.1	9 .2	~1.Ø	-9.3	-2.8	-2.8	-3.3	3.8	1.5	2.8	3.9	-1.1	-2.8	-7.1	يە [
401.01		•						1.17	010	0.0		012	0.1		1.0	0.1			0.0				0.0		2.2			2.0	2.0					
49.0																																		
-	; -6.	6 -1	5.4 -	5.6	-4.2	-4.3	-3.2	-0.6	-9.2	-1.6	-0.8	-1.5	9.1	9,9	2.3	2,2	2.2	-0.3	-0.3	-2,4	-1.7	-1.2	-3.4	4.0	~0.2	2.5	3.1	3.9	-1.9	-1.3	-4,3	-6.7	-13.7	15
-	; -6.	6 -1	5.4 -	5.6	-4.2	-4.3	-3.2	-0.6	-9.2	-1.6	-0.8	-1.5	0.1	0.0	2.3	2,2	2.2	-0,3	-0.3	-9,4	-1.7	-1.2	-3.4	4.0	-9.2	2.5	3.1	3.0	-1.9	-1.3	-4,3	-6.7	-13.7	- 5

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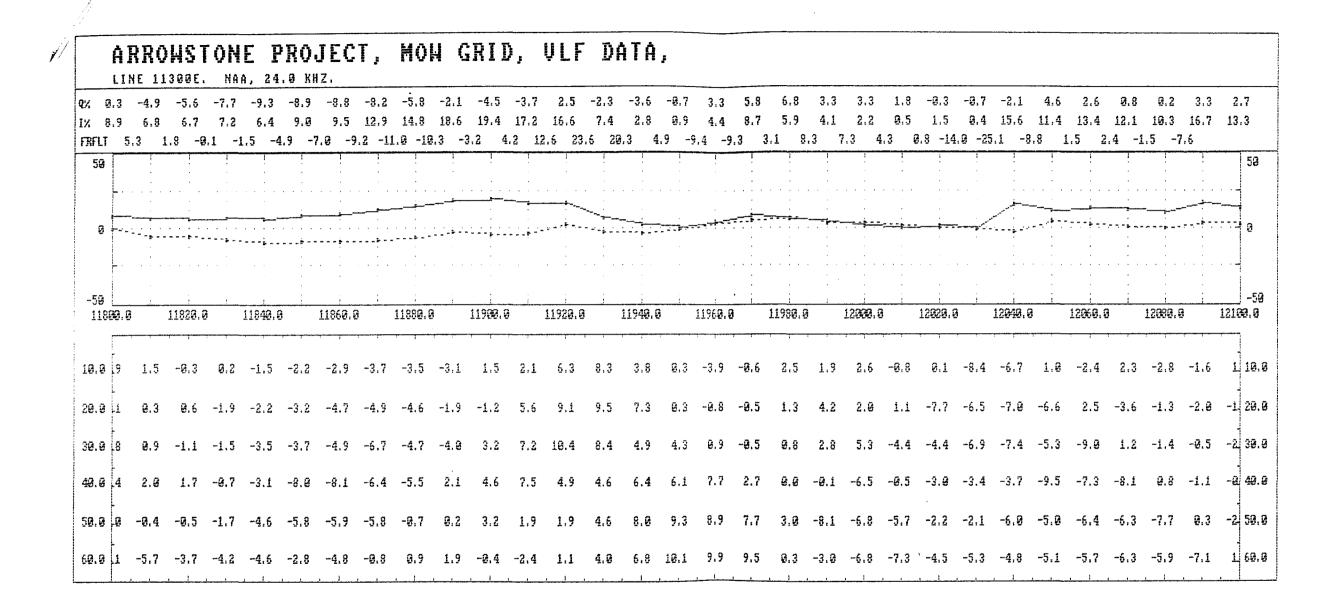


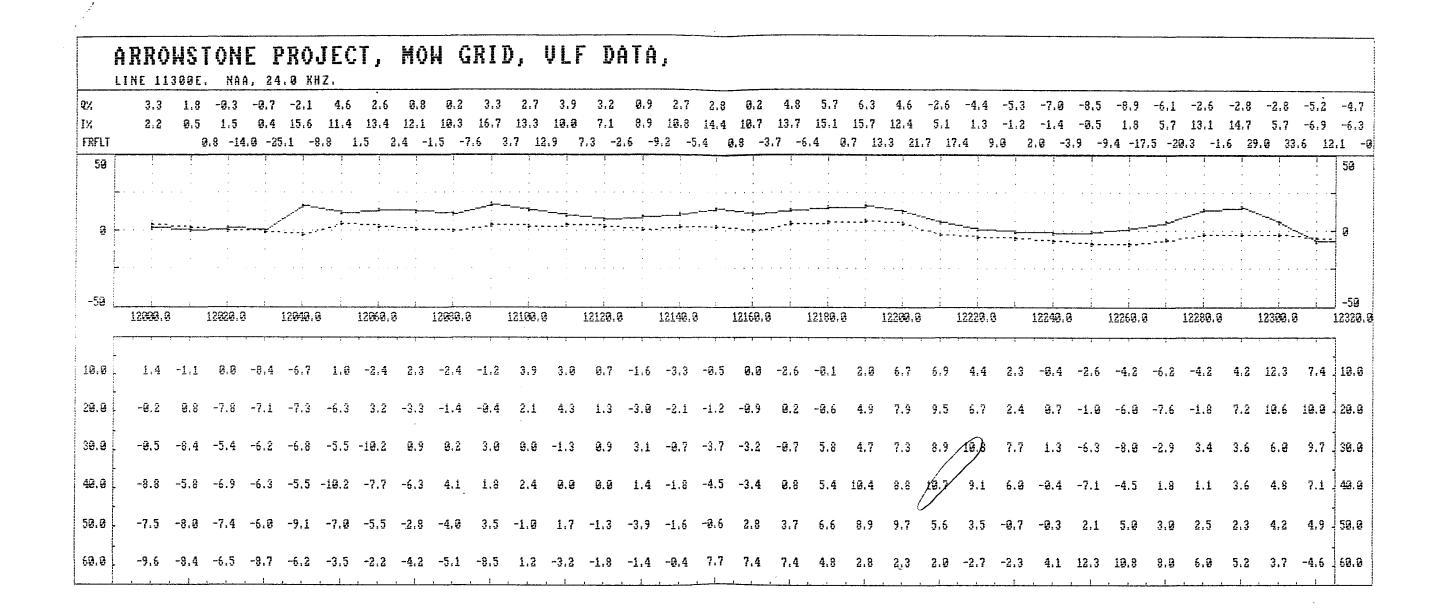


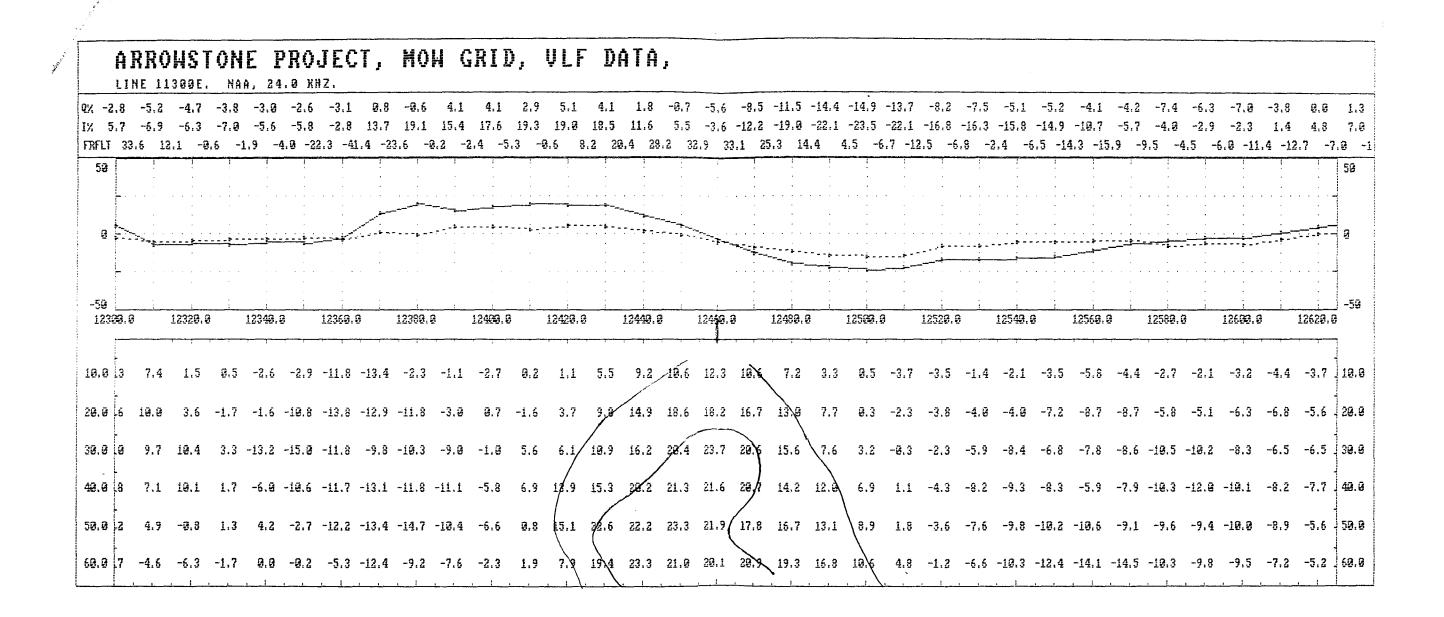
7% I% FRFLT	-8.2 15.6	10.9	7.4	7.4	-5.5 8.4 5.0 13	-1.6	-4.0 -4.5 .4 8	-6.1	-4.1 -8.4 .9 4.	-9.1	-9.9	-10.2	-10.8	-9.7		-7.4	-3.1	-3.7	-5,9	-2.6		-1.3	1.1	5.5 2.8 .6 -3	6.5 3.6 1.9 -2	5.9 4.2 .3 -1	5.6 4.5 1.4 2	5.4 4.7 1.4	4.7 3.6 2.1	3.5	2.6	7.4 2.8 1.2	
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18.0	4.6	5.5	3.2	5.2	6.1	3.6	3.7	2.8	2.2	1.2	0.9	0.4	-9,3	-2.1	-1.5	-2,9	-2.7	1.1	-1.1	-3.1	-1.0	-1.8	-2.7	-1.5	-1.2	-9.6	-0,4		9.7		8,4	0.8	10.
18.0 29.9	4.6 4.7	5.5	3.2 9.1	5.2	6.1 7.9	3.6 9,4	3.7	2.8 5.3	2.2	1.2 3.3	0.8 1.5	g.4 g.5			-1.5 -4.8										-1.2 -2.5							0.8 -9.2	
29.9		6.9		7.7			3.7 6.6 9.7	2.8 5.3 6.5	2.2 3.9 6.2	1.2 3.3 4.9			-9.6	-1.6	-4.8	-3.7	-1.7	-3.5	-2.2	-2.2	-4.8	-3.8	-2.6	-3.4		-1.3	-9.1	9.6 9.9	9.6	9.8	0.7		29.
+	4.7 2.3	6.9 8.3	9.1 11.5	7.7	7.9	9,4 8.8	3.7 6.6 9.7 9.1	2.8 5.3 6.5 9.1	2.2 3.9 6.2 6.1	1.2 3.3 4.9 5.8	1.5	29.5 29.5	-9.6 -9.1	-1.6 -3.7	-4.8 -3,7	-3.7 -3.1	-1.7	-3.5	-2.2 -4.0	-2.2 -2.9	-4.8 -4.3	-3.8 -6.9	-2.6 -4.7	-3.4 -3.5	-2.5 -3.9	-1.3 -1.8	-9.1 -1.2	9.6 9.9 -9.8	9.6 -9.3	9.8 9.9	0.7	-9.2 -9.6	29.
29.9 30.9	4.7 2.3	6.9 8.3	9.1 11.5 18.1	7.7 11.3 13.1	7.9 9.5	9,4 8.8 10,1	6.6 9.7	5.3	3.9	3.3 4.9 5.8	1.5 3.2 2.7	2.5 2.5 1.8	-9.6 -9.1 -1.8	-1.6 -3.7 -2.3	-4.8 -3.7 -1.6	-3.7 -3.1 -3.5	-1.7 -4.4 -5.2	-3.5 -4.5 -4.4	-2.2 -4.0 -5.0	-2.2 -2.9 -5.8	-4.3 -4.3 -3.9	-3.8 -6.9 -4.9	-2.6 -4.7 -6.6	-3.4 -3.5 -5.0	-2.5 -3.9 -4.4	-1.3 -1.8 -4.2	-9.1 -1.2 -2.1	9.5 9.9 -9.8 -1.4	9.6 -9.3 9.9	9.8 9.9 ~9.1	9.7 9.2	-9.2 -9.6 -9.8	29. 38. 49.

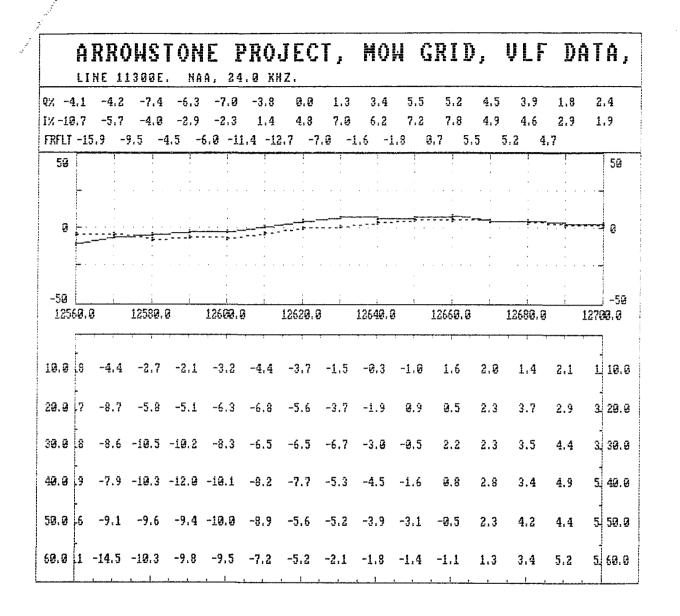
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Q% I% FRFL		2.8	1.1	2.9	4.0	5.0	3.2 10.2 0.5 -4	9.3	2.0 19.1	10.7		10.4		8.5	7.8	3.1		6.7	8.8 7.8 2.2 5		3.8	2.0	0.7	5.3 -2.5	6.8 6.7 4.2 -10	6.1 1.7 8 -19	7.3		18.3	0.8 9.9	9.3 8.9 1.5 5	-4.9 6.8	6.7	-7.7 7.2 9.1 -1
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10.9	4	8,8	-0.1	-2,3	-1.3	-4,9	-2,8	0,9	-1.5	1.2	8,2	-0.5	1.8	9,8	3.1	2.1	-1.7	-1.5	8.9	2.3	3.3	2.9	2.7	-0,4	-2,9	-3.9	-5.7	-2.9	0.0	0.6	1.9	1.5	-0.3	10.0
20.0 30.0	1				-5.1 -3.8		-3.7					0.7		4.3			ũ.4			3.0	3.8	3.2			-3.4									_
	L							-2.1 -4.3		9.9 -1.5	0.2 2.9	1.1 4.2		2.4 2.2			2.2 1.8		9.1 4.1			4.5 3.2		-1.7 -2.7			-7.8				9.8 9.4		-1.1 1.7	
50.0	ı Q	-3.2	-3.2	-4,7	-4.6	-3.7	-4.6	-4,4	-2.4	-1.7	1.4	3.1	8 .8	0.3	2.2	1,6	4.1	4.3	5.7	3.7	0.4	-1.9	-2.8	-2.0	-3.5	-3,7	-3.1	-3.8	-4.9	-1.9	-3.0	-0,4	-0.5	50.0
69.9	7	-3.7	-3.8	-4.1	-2.8	-3.8	-4.1	-3.6	-4.6	-1.5	-1.2	-2.0	0.7	2.0	3.7 	5.1	4.3	7.0	4.0	2.6	-1.3	-6.1	-5.2	-3.1	-1.3	-0.4	-0.5	-1.0	-1.9	-5.7	-4.1	-5.7	-3.7	60.0

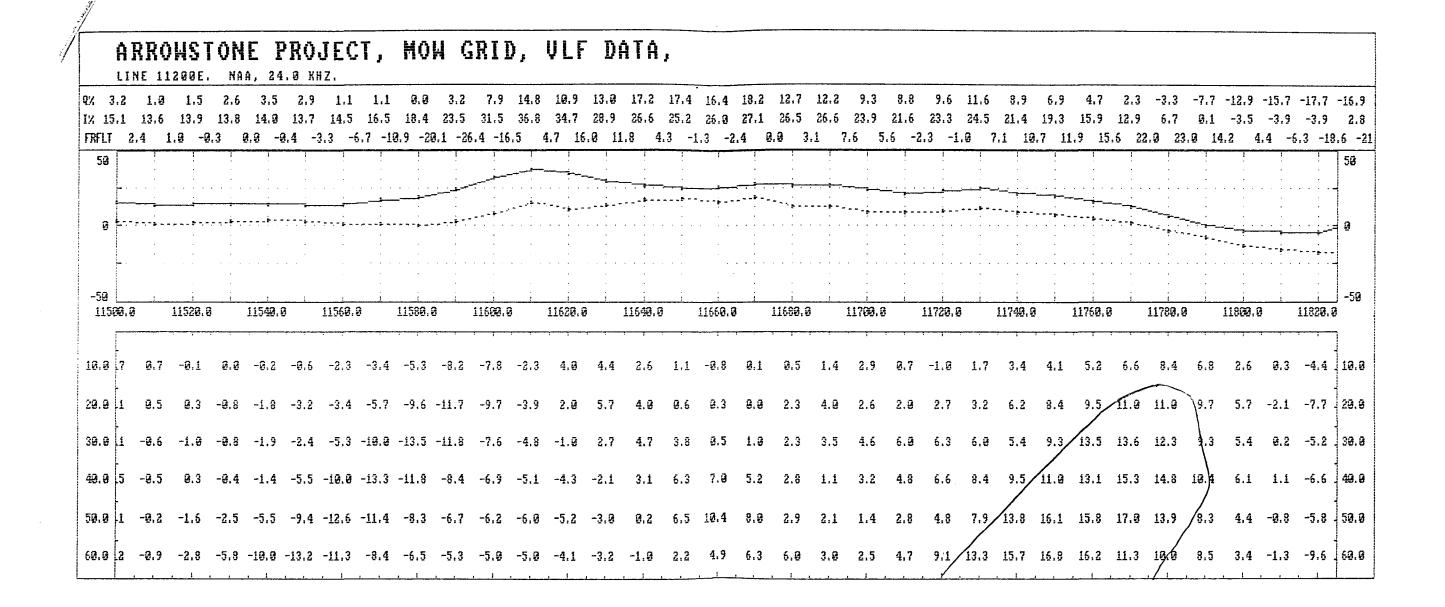


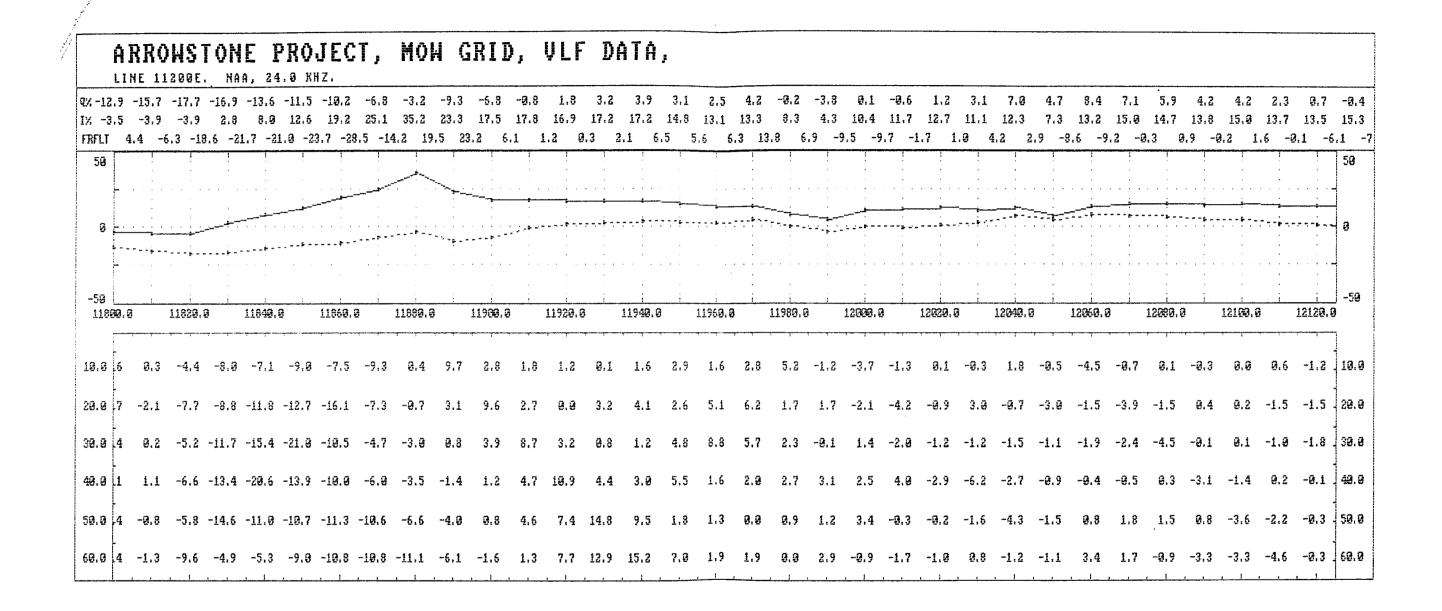


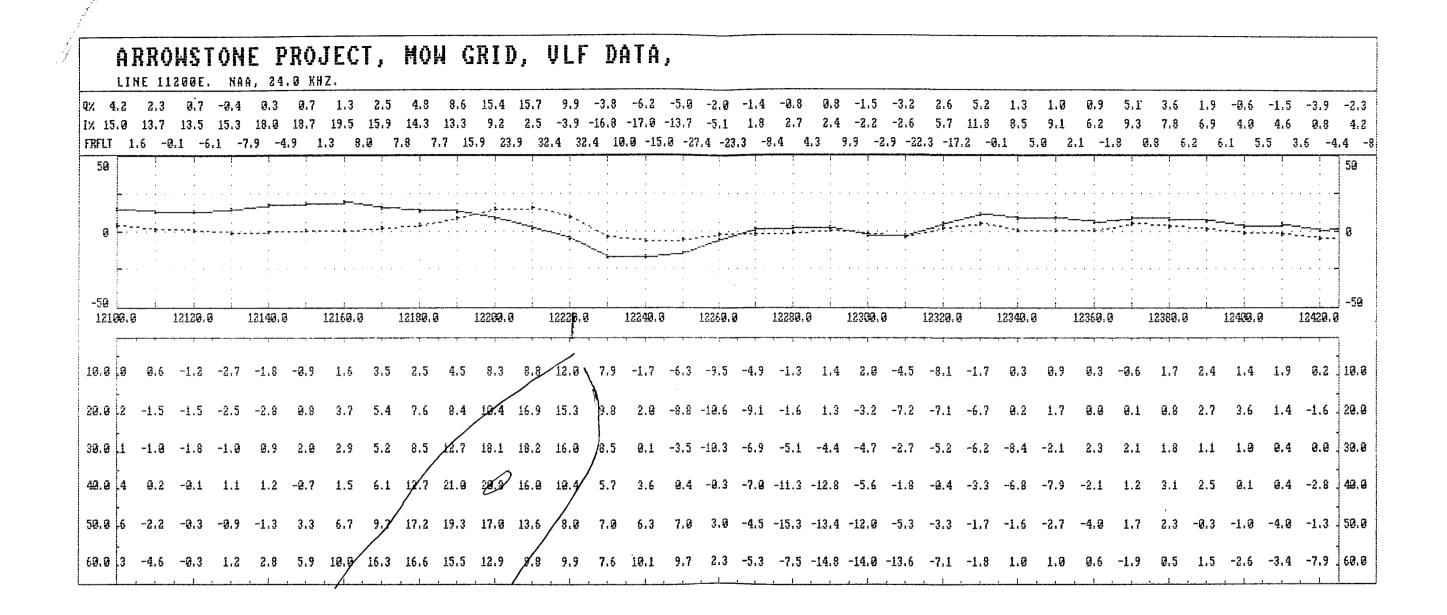


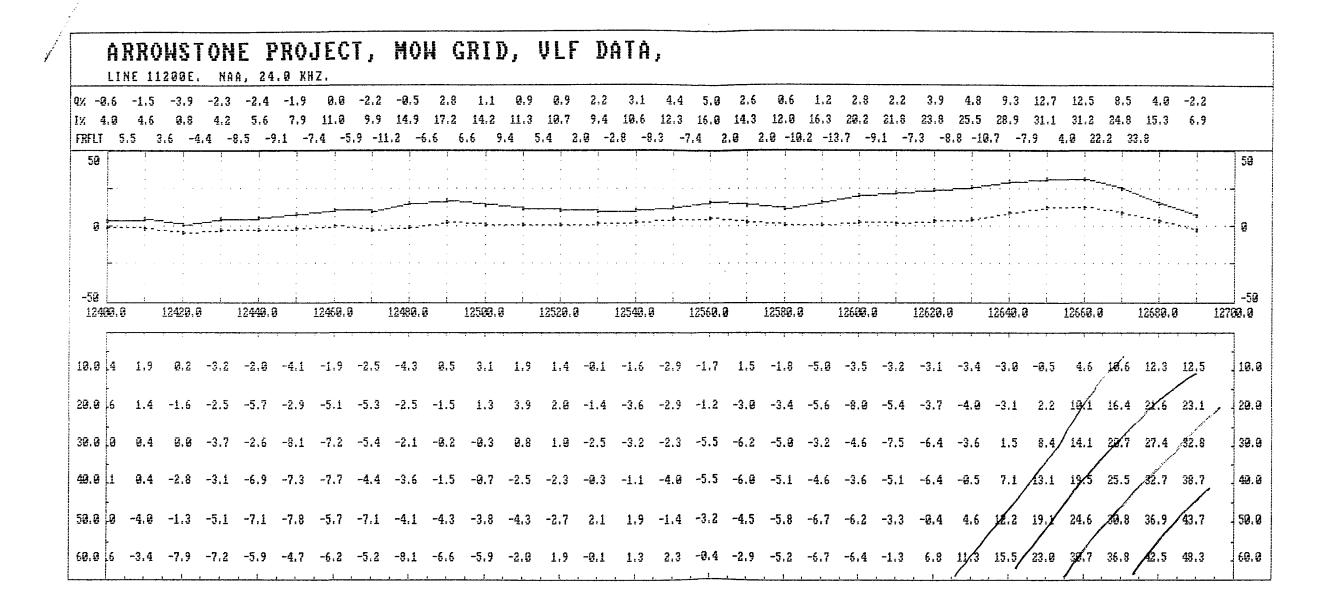


	RRO																																
% % RFLT	-7.2 4.5	-5.6 5.1 4		-0.5 1.5 4 0	0.1 1.9).9 0		0.1	-0.6	2.1 -0.9 .3 -1		3.0 1.3 .4 -7	2.3	5.1	7.1	8,1	9.7		11.8	13.6		17.5	19,4	19.1				15.3			14.8	3.2 15.1 .4 2.	1.0 13.6 4 1	
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1.0	0.2	0.5	2.1	1.3	-8.1	1.4	1.8	0.4	6.2	-1.6	-2.2	-2.6	-3,4	-2.1	-2.1	-1.6	-1.7	-2.7	-2,5	-2.7	-2.8	-1.1	-9.1	0.5	1.6	1.8	1.5	0.2	0.3	0.2	0.7	0.7	
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1.0	-9.2	0.5	9.9	1.0	0.2	0.0	-1.6	-2.2	-3,2	-5.1	-5.1	-5.7	-8.1	-9,3	-10.7	-11.6	-10.2	-9.7	-7.5	-5,9	-4.7	-4.2	-5,3	-4.5	-3.8	-1.5	-0.2	1.3	1.6	2.1	1.2	-0.9	



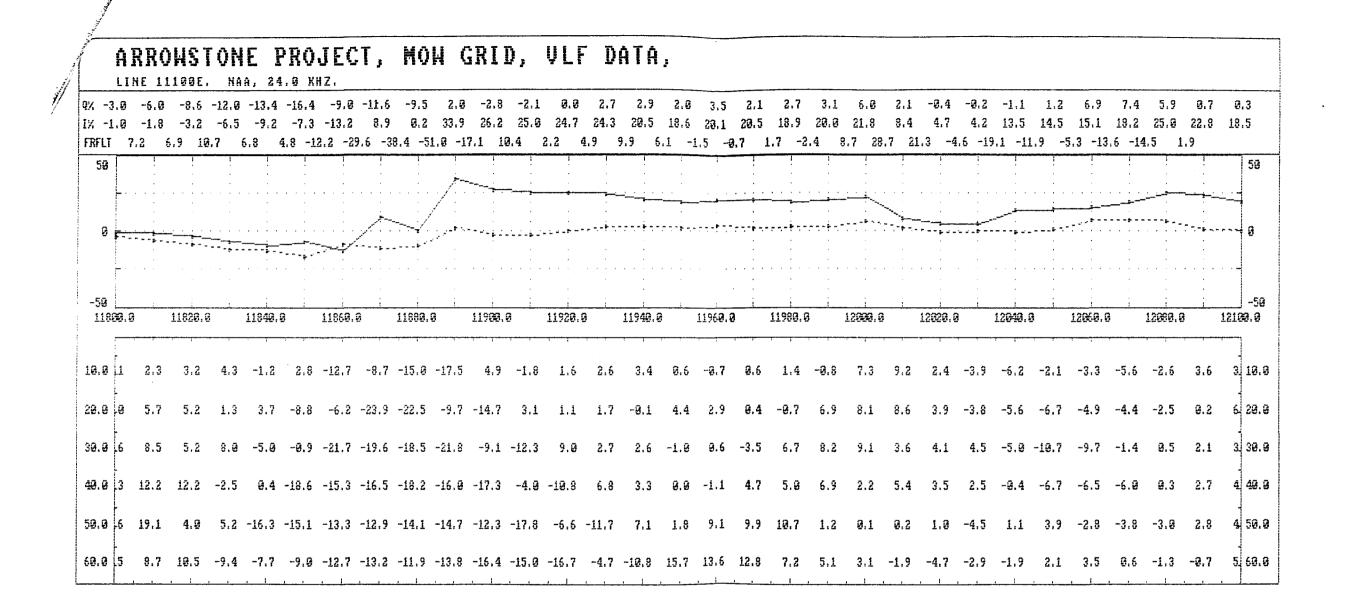


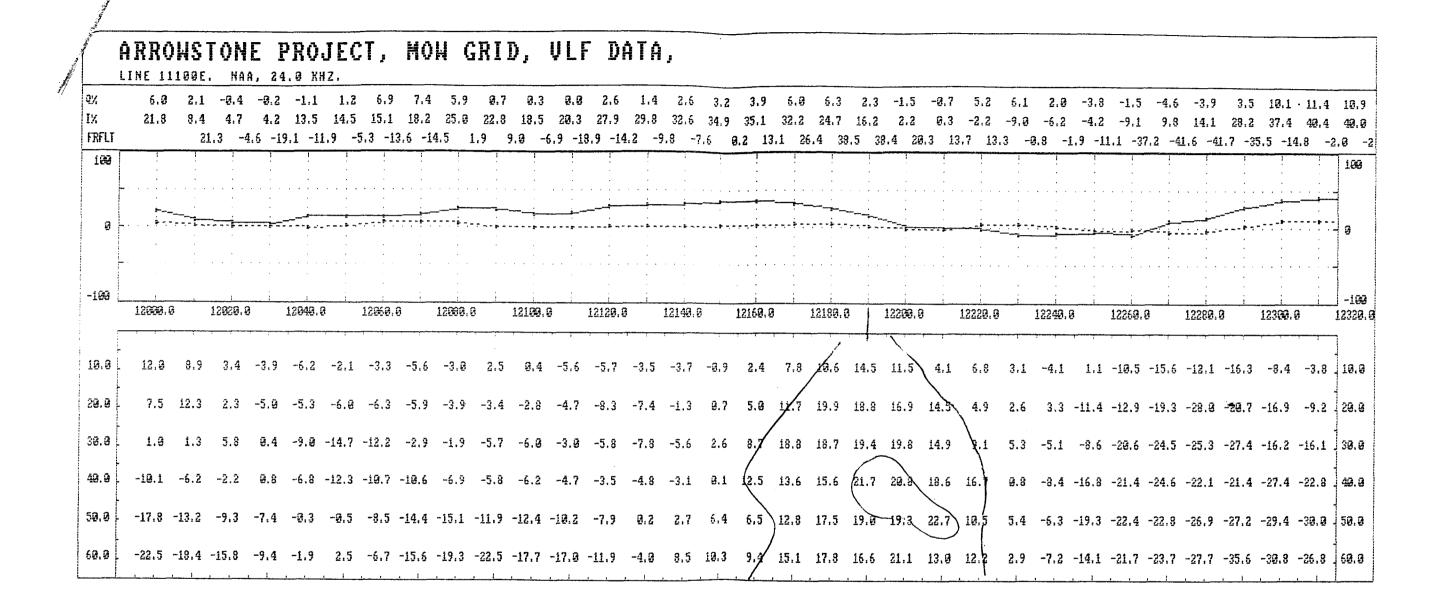




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9.9	-1.8	-1.?	-3.7	-3.6	2.	.9	8.4	2.6	-9.7	-7.1	-9.2	-8.0	-1.6	-1.5	-2.2	-4.6	-4.2	-5.3	-4.1	-2.0	-2.8	-2.4	-1.4	-9.4	<u>9</u> .4	9.7	9.9	-1.9	-3,9	-5.2	-6.9	-4.6	-2.2	20.0
ø.ø [-8.6	-4.3	-6.9	8.1	2.	.4	2.6	-4.4	-3.9	-4.6	-9.5	-8.4	-7.8	-3.8	-4.6	-2.5	-5.2	-6.6	-7.2	-5.i	-3,4	-3.6	-2.2	-1.0	-0.5	-0.2	-9.8	-2.9	-5.6	-8.4	-7.i	-5.5	-2.7	30.0
9.9	-1.8	-3.4	0.9	-0.6	-9.	.5 -	3.6	-4.1	-7.1	-4.6	-3.3	-8.7	-10.1	-11.7	-5.8	-5.2	-4.8	-5.2	-7.8	-8.9	-7.7	-4.3	-2.3	-9.8	-0.5	-2.6	-4.1	-5.9	-7.8	-6.7	-6.4	-4.5	-5.2	49.0
0.0	-0.9	3.0	1.7	-0.2	-6.	.8 -	6.6	-5,9	-5.2	-5.7	-2.9	-3.6	-11.6	-11.5	- <u>12</u> .5	-8,9	-8,5	-6.6	-6.8	-7.4	-6.6	-4.1	-3,4	-4.4	-5.1	-5.3	-6.5	-7.5	-5,5	-4.5	-4.1	-6.8	-8.6	50.0
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F		-2,4	-2,4	-1.8	-4.9	-7.4	-8.8	-5.1	0.4	2.4	3.6	3.1	1.7	-1.7	Ø.5	1.7	5.3	9.2	8.9	9.4	7.8	6.0	6.3	8.8	13.9	17.1	16.6	13.8	12.2	7.6	8.5 5	.2]:
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9.9 L) -9.2	-6.0	-6.5	-5.3	-4.9	4,4	14.9	13.2	18.6	5.2	-3.3	-3.5	-ñ.8	-2.3	-1.7	-2.2	2.9	2.9	10.1	6.8	4.6	j8.8	14.7	19.4	9.8	-1.5	-5.6	-7.5	2.4	0.2	-6.7	-4.2	12
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9.9 li	-16.1	-13.8	-8.1	-6.0	-1.9	5.6	8.6	12.8	11.4	8.3	2.3	-2.9	-4.7	-2.6	-1.3	7.1	4.7	6.2	2.0	8.9	13.4	18.0	19.5	7.6	7.4	9.2	1.9	-4.5	-11.4	-5.2	2.8	3.8	3
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a.a [-30.0	-18.7	-19.8	3.0	7.0	8.2	6.0	2.6	4.7	10.1	6.5	5.2	-1.9	-1.8	-4.1	2.5	-0.3	7.5	13.4	22.4	22.7/	18.2	11.5	10.1	9.3	9.4	7.5	4.4	0.4	-1.7	-10.7	-7.8]5
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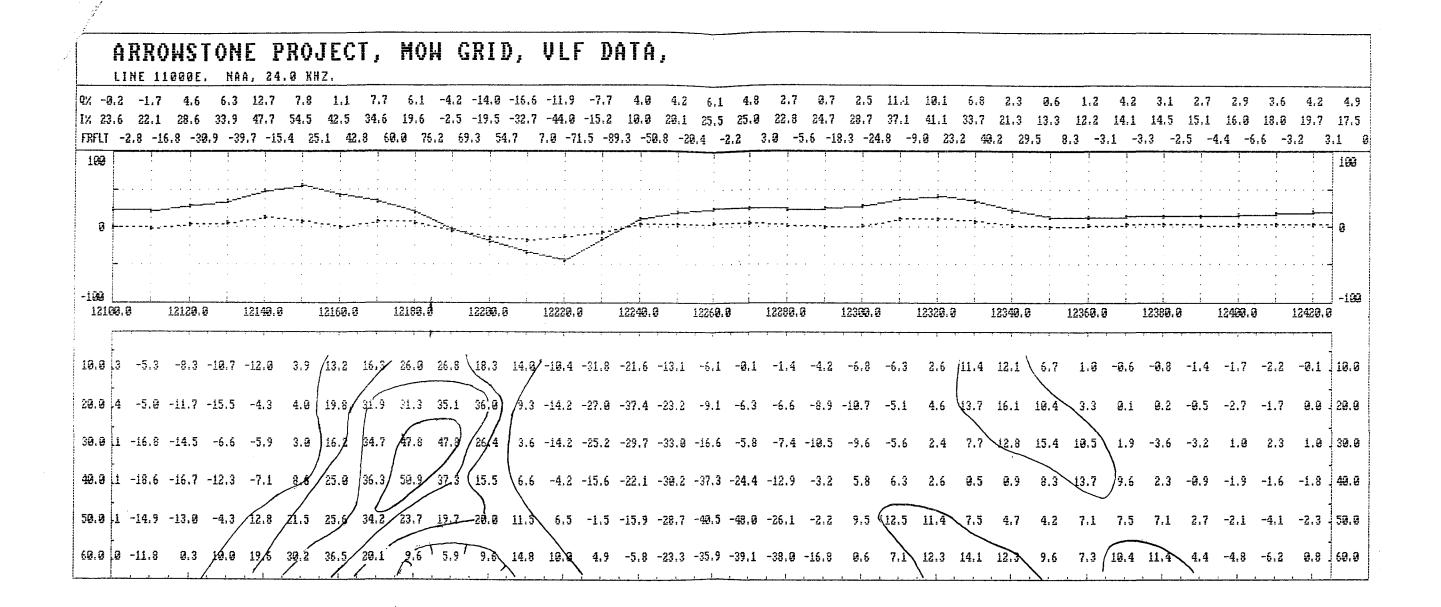
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	-3.1	-4.6	-5.5	-7.4	-8.6	-10.0	-10.9	-11,1	-9.8	-19.5	-12.2	-11.8	-11.9	-9.6	-10.7	-9.4	-7.0	-9.9	-10.9	-13.2	-11.1	-7.5	-4.4	-3.1	-4.1	-0.5	0.1	3.2	4.9	-9.3	-4.9	-5.6	49.0
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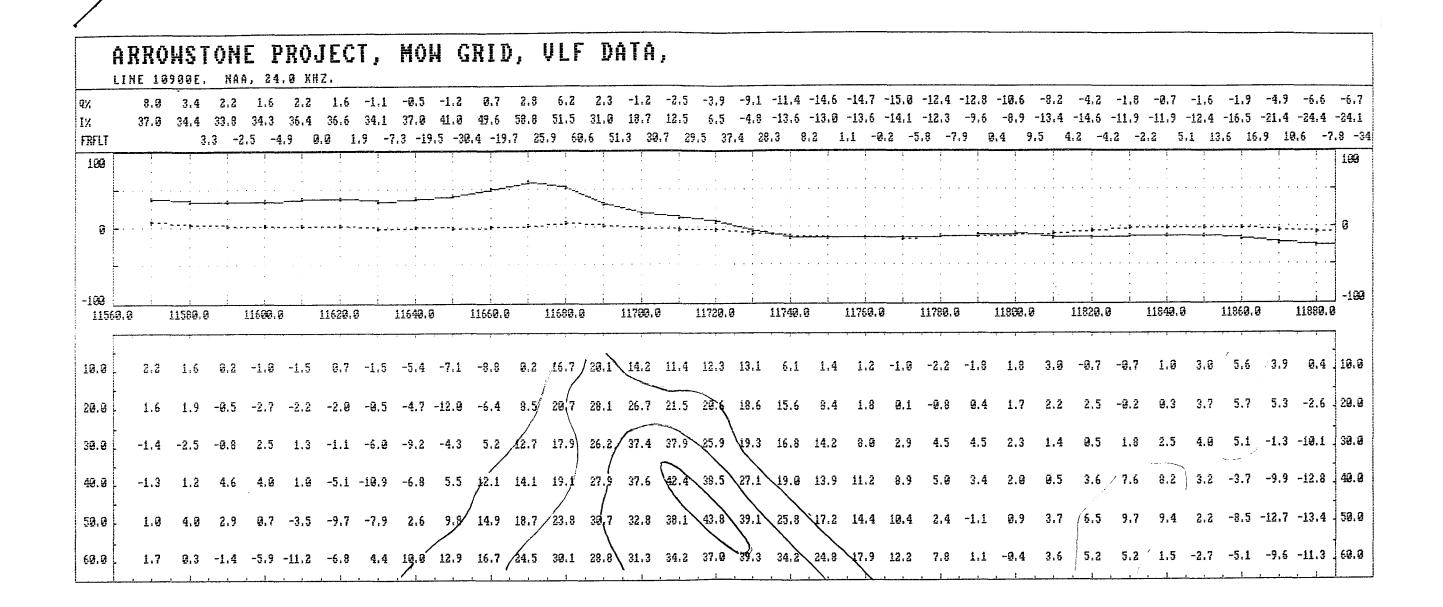
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11500.	0 	11520.0	ļ 	11540.(3	11560.0) 	11580.0	l •	11600.0	}	11628.4	<u>}</u>	11640.0	2	11660.0	} 	11680.2) ,,	11700.0) 	11720.(<u>?</u>	11740.0	9	11760.0	1	1789.0	11: 	.809.0	1
18.0 1	0.5	-2.2	-4,3	-3,6	-1.7	0.1	4.7	-1,8	4. <u>1</u>	9,5	1,2	3.5	2.7	0.3	-4.3	-7.1	-1.2	-4.2	-2.6	2.7	-4.2	-9,1	5.1	3.9	6.1	6.7	4.9	4.0	2.9	1.2	1.9
				- -		
20.0 5	-2.9	-2.4	-5.1	-5.5	-1.1	2.5	-8.9	7.2	6.4	4.9	10.1	4.7	2.9	-1.1	-3.9	-6.2	-9.6	-2.8	-6.8	-5.5	1.5	1.3	2.5	¥.6	9.5	<u> </u>		7.5	5.6	3.4	2.1
30.0 1	-4.8	-4.5	-2.3	-2.2	-1.1	-4.8	4.7	6.2	7.3	6.8	6.7	10.6	-0.6	-3.1	-1.9	-7.2	-5.4	-4,4	-4.8	-9,4	0.1	4.4	4.8	7.)	13.5	12.6	11.3	18.5	6.7	4.7	6.0
49.9 9	_5 Z	-7.6		_0.5	-5.2	4 0	3.3	5.8	8.5	9.6	8.3	2.7	A 0	-0.7	_5.5	-19	-4 4	_0 A	_5 7	_0.4	2.2	51	11 0	10.2	10.0	14 5	11 E	10 1	8.5	67	7 2
	-1.9	-1.0	-4.3	-0.3	-3.2	1.0	3.3	3.0	0.J	7.0	9.3	2.1	4.0	-0.1	-3.3	÷14	1.1	-0.7	-3.1	-0.0	3.3	3.1		10.3	10.0	17.J	11.3	Ie.d	0.3	0.1	1.3
50.0 3	-6.5	-6.4	-5.1	-9.7	0.9	2.4	2.0	6.7	10.6	10.1	7.3	4.9	3.1	2.8	-1.6	-3.5	-7.0	-6.0	-5.0	-2.6	5.4	8.9	9.9	15.5	11.1	10.1	12.7	9.5	1.0 1	3.8 1	1.0
68.0 7	-19	-27	-9.4	-2 6	-9.4	24	44	55	9 I	75	6 6	9.0	12	17	<u>4</u> 9	-6.0	-4 २	-2.2	-3.2	-95	17	79	(a 1	<u> 9</u> 9	12.2	10.7	12 4 1	19.1	7.1 1	6.2 1	3.5
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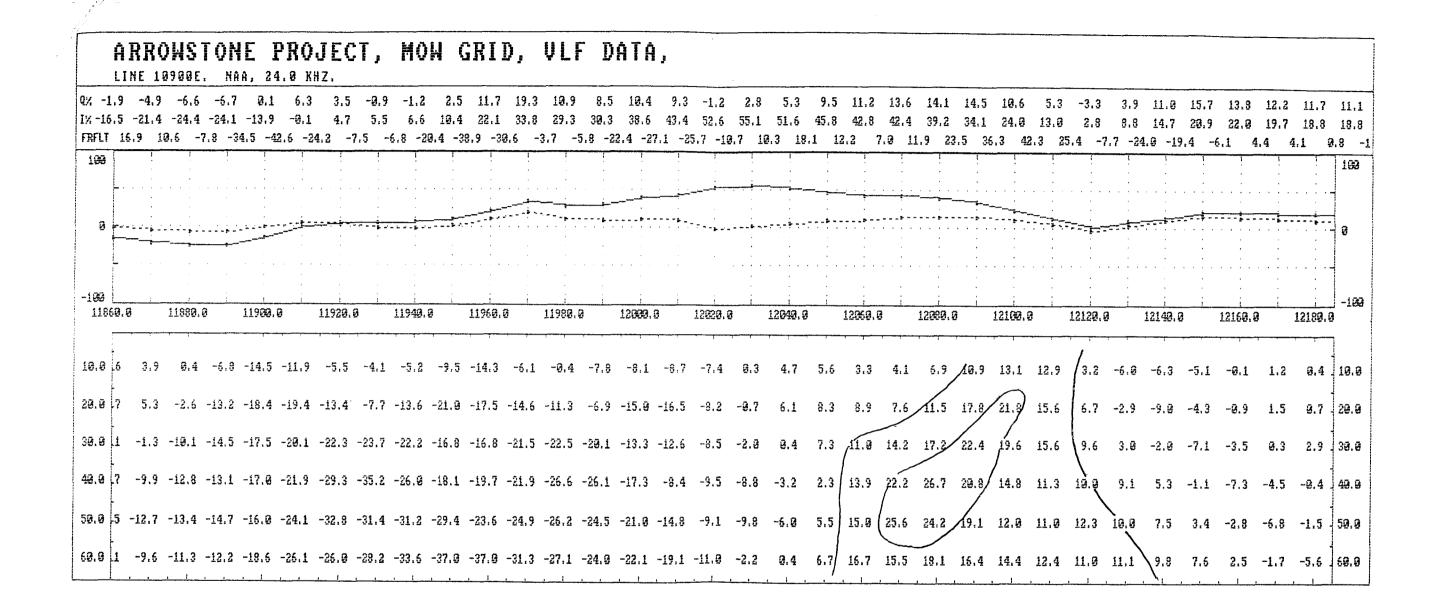
2.5 0.8	4.9 9.6	7.4 0.4	7.9 0.9	3.1 -5.1	-7.4	-7.9	-6.5	-8.3	-8.0	-8,9	7.5	15.6	15,4	10.7	2.4	-5.1 -9.1	-2.0 -1	.6 0	.9 0.3	3 -14.7	-27.4	-7,9	7.2	16.9	22.4		-7.3 17.3					
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3.0 2	1.8	0.4	3.5	4.9	2.9	0.3	-8.2	-0,3	-5.7	-9.5	-9.8	-4.8	2,4	7.3	6.8	3.2	1.8 2	.1 1	.0 7.7	14.2	-5.5	-19.8	-13.8	-11.6	-3.2	1.6	-4.0	-3.9	0.3	-5.3	-8.3	10
3.9 4	2.1	4.6	5.5	4.5	3.1	9.2	-9.8	-3.8	-6.7	-12.8	-13.1	-6.7	2.5	7.9	19.1	8.7	0.5 -1	.6 6	.4 13.7	4.9	-4.2	-19.4	-29.5	-13.9	-5.5	-7.4	-7.1	-7.6	-8.4	-5.0	-11.7	20
3.8 7	6.9	5.6	4.3	4.0	5.2	6.3	-1.1	-7.4	-12,9	-12.1	-10.3	-3.9	2.3	5.8	7.7	4.2	1.8 6	13	5 1.8	-4.8	-8.6	-12.7	-29.1	-28.7	-21.7	-10.8	-1,9	-1.8	-8.1	-16.8	-14.5	30
3.0 7	7.3	6.9	6.0	8.1	7.7	3.2	-2.8	-10.6	-10.7	-7.4	-4.1	-4.9	-5.5	-3.0	1.9	7.2	15.1 19	.5 3.	/ .0 -7.8	-14.4	-17.7	-13.2	-10.6	-21.7	-26.6	-12.7	-7.5	-3.5	-7.1	-18.6	-16.7	49
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Q%	2.9	3.6	4.	2 4	1.9	3.4	3.7	5.3	3 2	2.7	5.7	9.0	11.7	7.4	6.6	34,	.3 2.	8 0	.4 -	-6.9 -	-15.4	-7.2	-9,4	-1,4	4.4	7.8	6.7	5.0	3,	8 3.3	3.1	2 0.4		
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FRFI	.T -I	6.6 -	3.2	3.1	Ø.'	9 -6	.6 -	5.7	10.6	22.	6 13	.5 1	9.6 19).3 1	3.8	2.5	1.0	8.1	13.6	13.	5 2	.7 -13	- 0.	2.1 ·	·5.9 -2	8.1 -1	3.9 -	4.1 -1	3.8 -	22.6 -1	4.7			
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-19	4 (<u> </u>	8	12429	1.0	<u>،</u> 1	: 2449.0	i }	12469	1.0		: 2480.0		12569.0		12520	1, Ø	1254	0.0	: 12	560.0	L	12580.6	<u> </u>	12689	.0	12620	.0	12640.	8	12660	.0	12680.0	127	_ -199 199.0
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10.	9 7	-2.2	-0,:	19	,9	-1.0	-1.7	8.1	L 6	.7	7.4	2.7	6.1	5.8	2.2	1.	4 1.	54	.7	3.4	4.1	-1.1	-6.8	3.9	-8.8	-9,3	0.0	-6.3	-4.2	2 -8.6	-0.7	4.6		10.0
20.	8 7	-1.7	9.(2 9	.2	-1.0	-0.5	4.9) 6	.9	8.8	11.8	8.7	7.9	8.7	3.	94.	96	.4	7.6	0.8	-1.5	1.9	-13.0	-6.2	-7.0	-12.4	-5.6	-11.4	1 -6.4	-4.9	9.2		20.0
30.	8 6	2.3	1.(3 -i	.2	0.i	5.7	5.6	56	.2	j1.8	15.9	13.4	8.3	7.9	9.	46.	87	.9	3.4	2.4	4.5	-8.4	-7.3	-11.5	-7.9	-11,1	-19.5	-5.0	ð -7.1	-5.6	-3.8		30.0
40.	9 9	-1.6	-1.{	3 0	.6	7.3	8.7	9.2	10	.4	11.6	13.2	12.5	13.2	10.9	i a.	9 13.	32	.4	2.4	6.7	-3.4	-1.1	-6.8	-9.4	-15.5	-15.9	-11.3	-14.6	5 -3.2	-5.8	-4.7		49.9
50.1	8 1	-4,1	-2.3	3 4	.0	5.3	7.0	13.7	14	.?	12.5	11.4	12.0	15.6	15.5	14.	1 8.	0 8,	.2	7.8	-3,9	-1.6	-3,0	-5.1	-10,4	-16.1	-15.4	-10.0	-10.0	0 -13.8	-3.0	-4.6		50.0
60.	3 8	-6.2	0.8	3 4	.0	2.5	7.9	10.2	12	.0	12.9	11.9	17.1	18.0	21.5	4.	3 9.	5 13. \	.0	1.5	-0.7	-4.0	-5.1	-7.4	-13.2	-11.5	-11.3	-13.6	-8.3	3 -9.3	-12.7	-1.4		60.0

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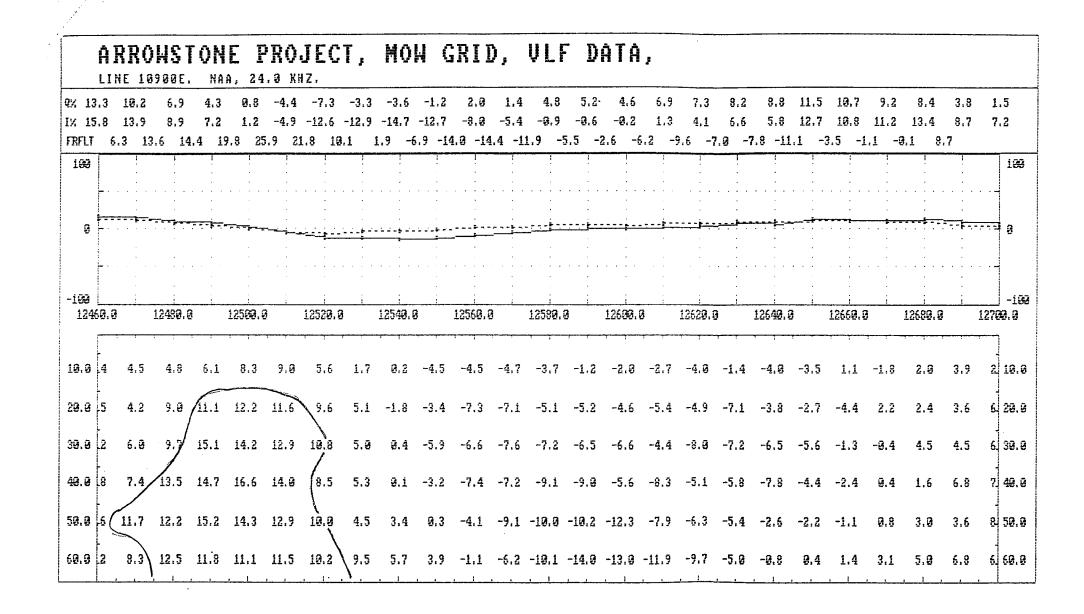


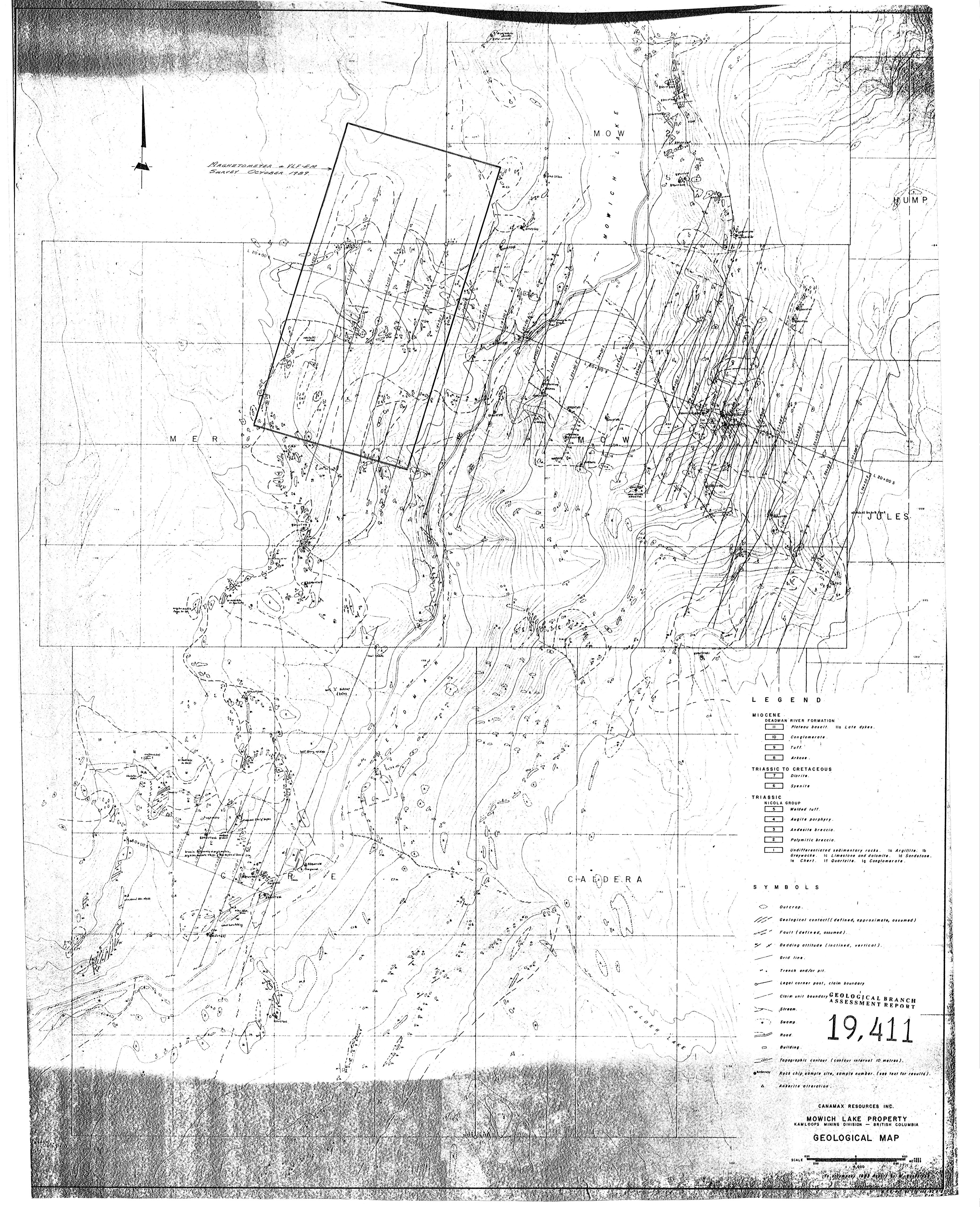


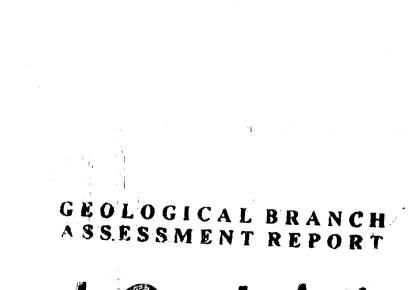
2% 13.8 1% 22.0				11.1 18.9		12.7 19.2	7.1 16.7	4.4 15.9	7.1 18.7	3.1 15.5	4.8 18.7	7.1 29.9	8.3 [.] 20.1	5.1 17.3		2.4 15.8	3.0 15.0	3.1 13.5	2.3 11.9	0.1 6.9	-1.4 5.3	0.3 3.8	2.1 2.5	3,2 2,6	2.9 1.9	3.3 7.2	4.5 7.7		11.5 13.3	13.3 15.8	10.2 13.9	6.9 8.9	4. 7.
FRFLT	4,4	4.1 (3.8 -	1.2 -1	.4 2	.9 6	.5 1	1.3 -1	6 6	8.4 -5	.4 -	5.8 2	.2 6	.5 4	.4 2	.7 3	,4 6,	.3 10.	8 13	39,	75	.9 4.	01	.8 -4	.0 -1(a.4 -9	9.9 -	9.7 -10	9.1 -	5.1 6	.3 13.	6 14	.4
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12160	9	12180.	9	12200.0)	12220.0	3	12249.0	}	12260.0	; }	12280.0		12309.0	<u>i</u>	1232 9.9	1	2340.0	<u>1</u>	2360.0		12380.0	<u> </u>	12400.0	, (}	12420.1	3	12440.1	3	12460.0	<u>} 1</u>	2480.0	
12160	9	12180.	0	12200.0) ; ;	12220.0	; }	12249.0	} }	12260.0	. ! } 	12289.0	,	12309.0	<u>i</u>	12320.0		12349.9		2350.0	<u></u>	12380.0		12409.0	; ;	12429.1	<u>, </u>	12449.(3	12460.0	, <u>1</u>	2480.0	
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	1.2		9.2	-8.3	· · ·	12220.0	2.1	-1.2	0.2	•	-3.1	-0.5	;	1.6	1.3	· · · ; · · ;	2.9	3.9	4.4	4.5		:	0.4	0.3	-3.0	-3.8	-3.0	· • · · · · ·	-2.3	-8.4	4.5		10
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10.0	1.2 1.5 9.3	8.4 8.7 2.9	8.2 -1.4 -2.5	-8.3 -9.7 1.9	0.0 1.3	1.6 1.6	2.1 9.6 1.8	- <u>1</u> .2 2.3 1.1	0.2 -0.9 -0.2	-0.1 -2.6 -1.3	-3.1 -8.4 8.2	-0.5 -0.4 1.9	1.9 1.2	1.6	1.3	1.3 2.4 5.4	2.9 3.8	3.9 6.1	4.4 7.8	4.5 5.7 7.5	2.3 5.4 6.1	2.3	0.4 1.9 8.5	0.3 -1.9	-3.0 -2.6 -2.6	-3.8 -4.4 -3.8	-3.0 -5.9 -4.6	-3.9 -4.2 -4.4	-2.3 -2.4	-0.4 2.5	4.5 4.2 6.0	4.8 9.0	10
10.0 1 20.0 9 30.0 5 40.0 3	1.2 1.5 9.3 -4.5	8.4 8.7 2.9 -9.4	8.2 -1.4 2.5 5.3	-0.3 -0.7 1.0 6.9	0.0 1.3 9.9 3.1	1.6 1.6 -0.9 3.1	2.1 9.6 1.8 -9.1	- <u>1</u> .2 2.3 1.1 -1.9	9.2 -9.9 -9.2 9.9	-0.1 -2.6 -1.3 1.9	-3.1 -9.4 9.2 1.2	-9.5 -9.4 1.9 1.3	1.9 1.2 1.1 2.5	1.6 3.7 2.8 1.3	1,3 3.3 5.9 4.1	1.3 2.4 5.4 7.8	2.9 3.8 5.8 8.9	3.0 6.1 6.7 7.4	4.4 7.8 6.1 7.9	4.5 5.7 7.5 7.6	2.3 5.4 6.1 8.7	2.3 2.5 6.9 5.9	0.4 1.9 0.5 4.6	0.3 -1.9 -9.2 0.5	-3.0 -2.6 -2.6 -1.6	-3.8 -4.4 -3.8 -4.2	-3.0 -5.9 -4.6 -4.3	-3.9 -4.2 -4.4 -2.3	-2.3 -2.4 9.8 -1.9	-9.4 2.5 1.2 3.8	4.5 4.2 6.0	4.8 9.0 9.7 13.5	10

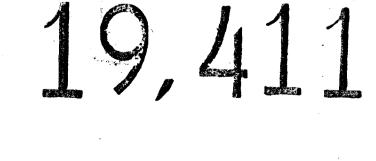
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IRON RIVER RESOURCES LIMITED

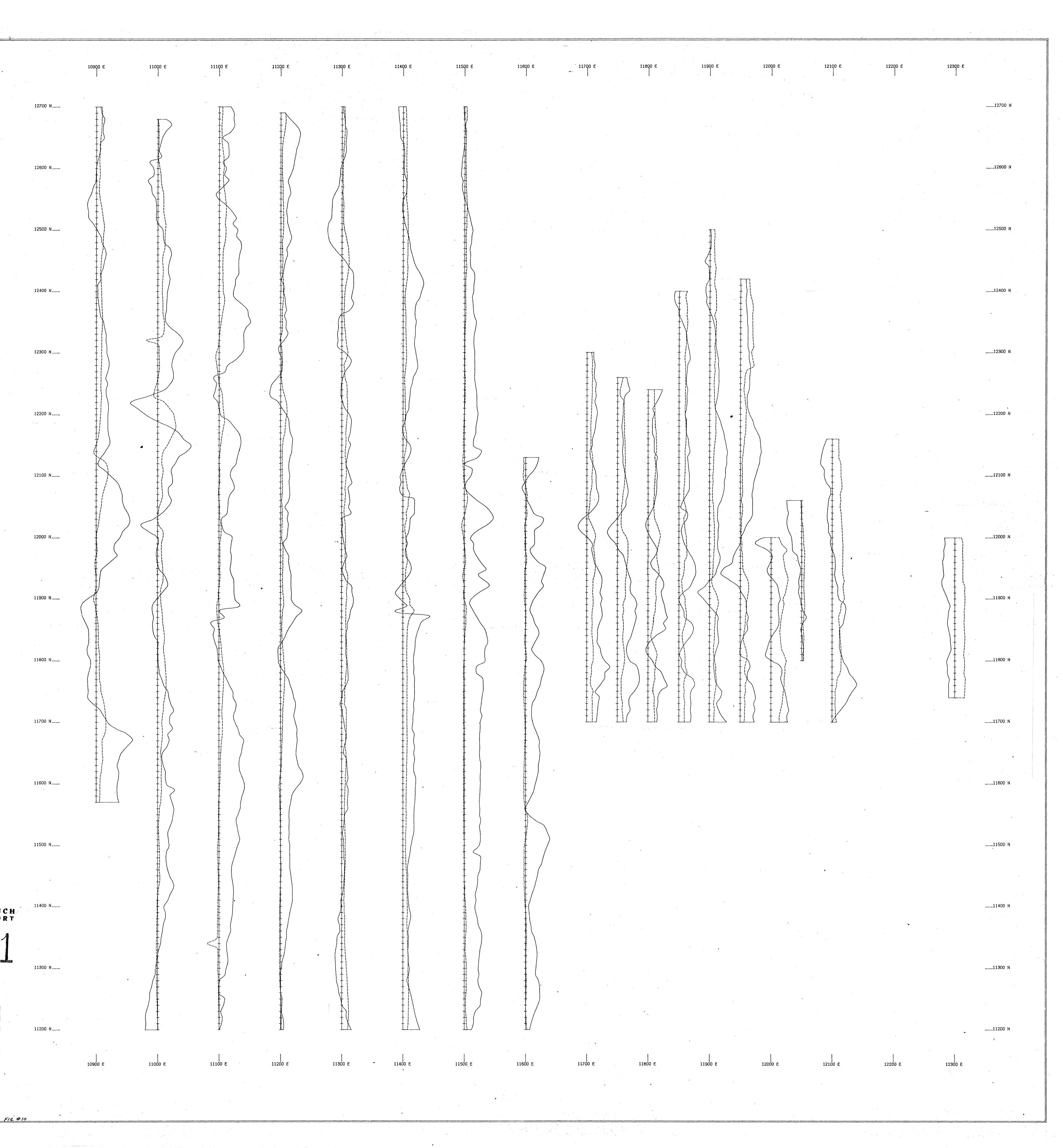
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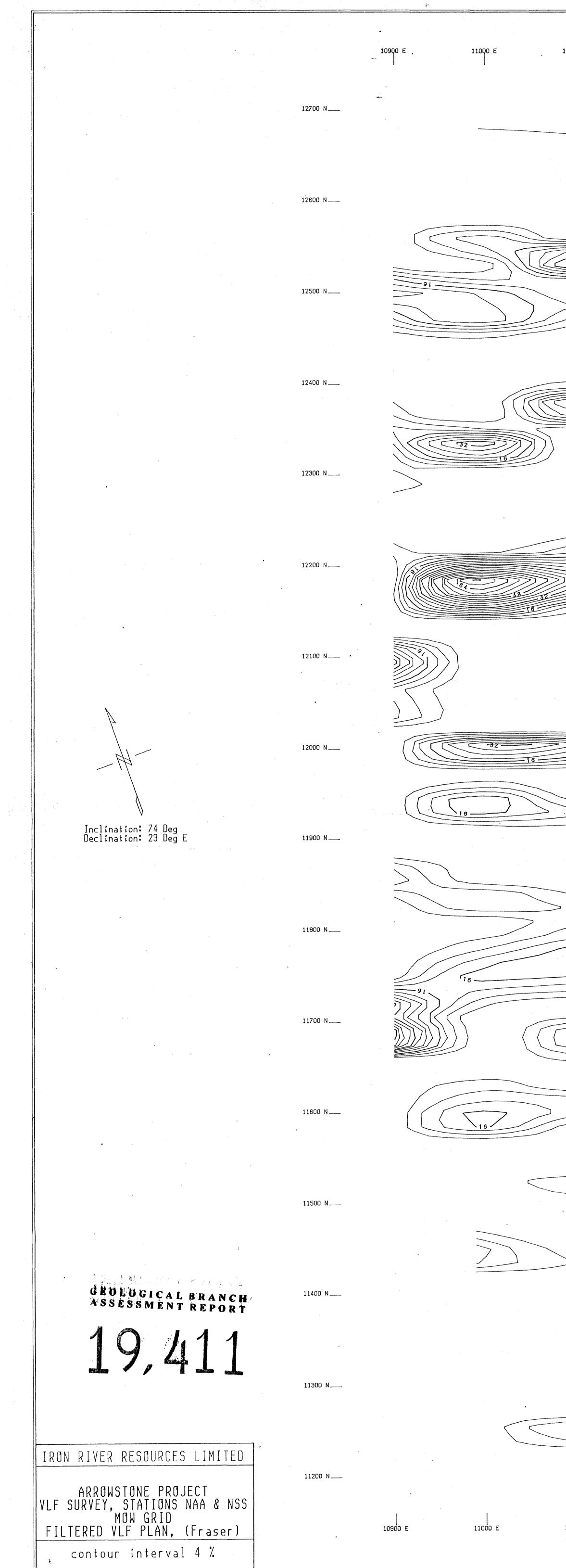
Inclination: 74 Deg Declination: 23 Deg E

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ARROWSTONE PROJECT VLF SURVEY, STATIONS NAA,24.0 khz & NSS,21.4 khz Vertical inphase & Horizontal field strength profiles

vertical inphase solid line @ 1 cm = 20%, base 0 horoz. field dashed line @ 1 cm = 5, base 5 SCALE 1:2000 DELTA GEOSCIENCE LTD





SCALE 1:2000 DELTA GEOSCIENCE LTD

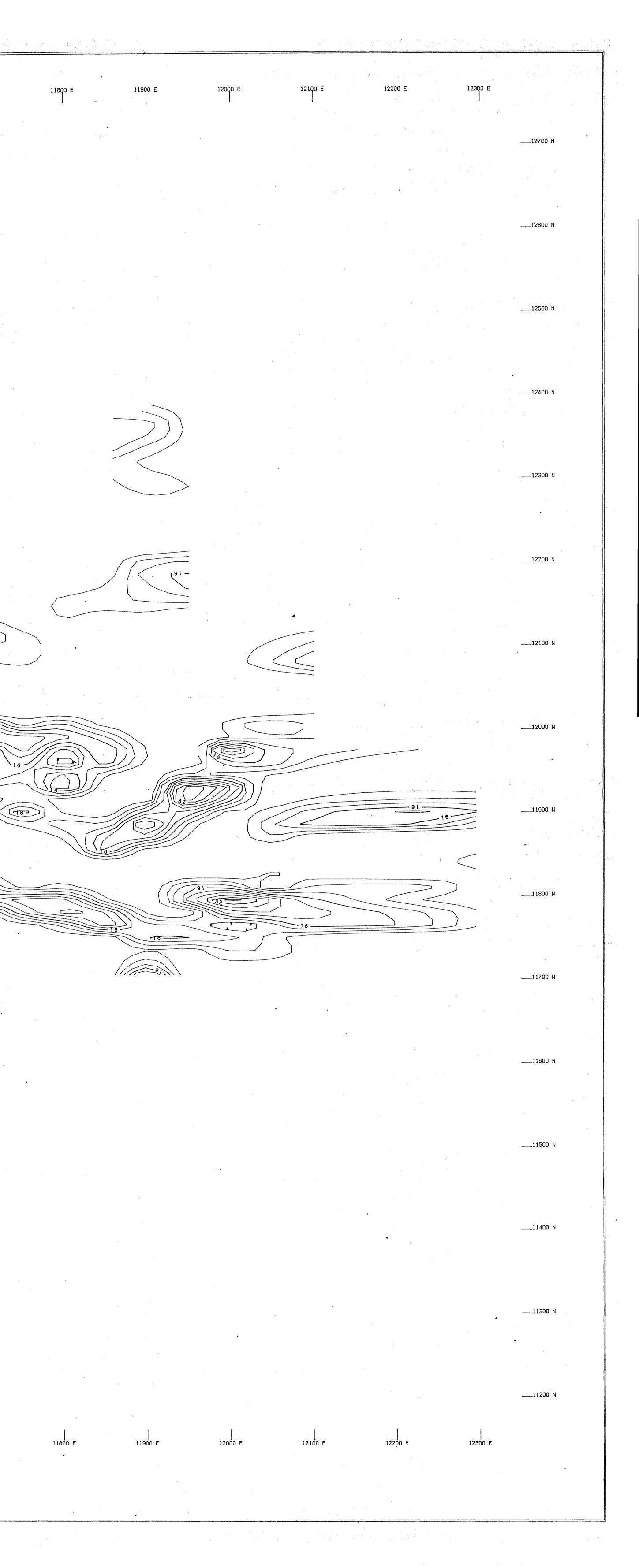
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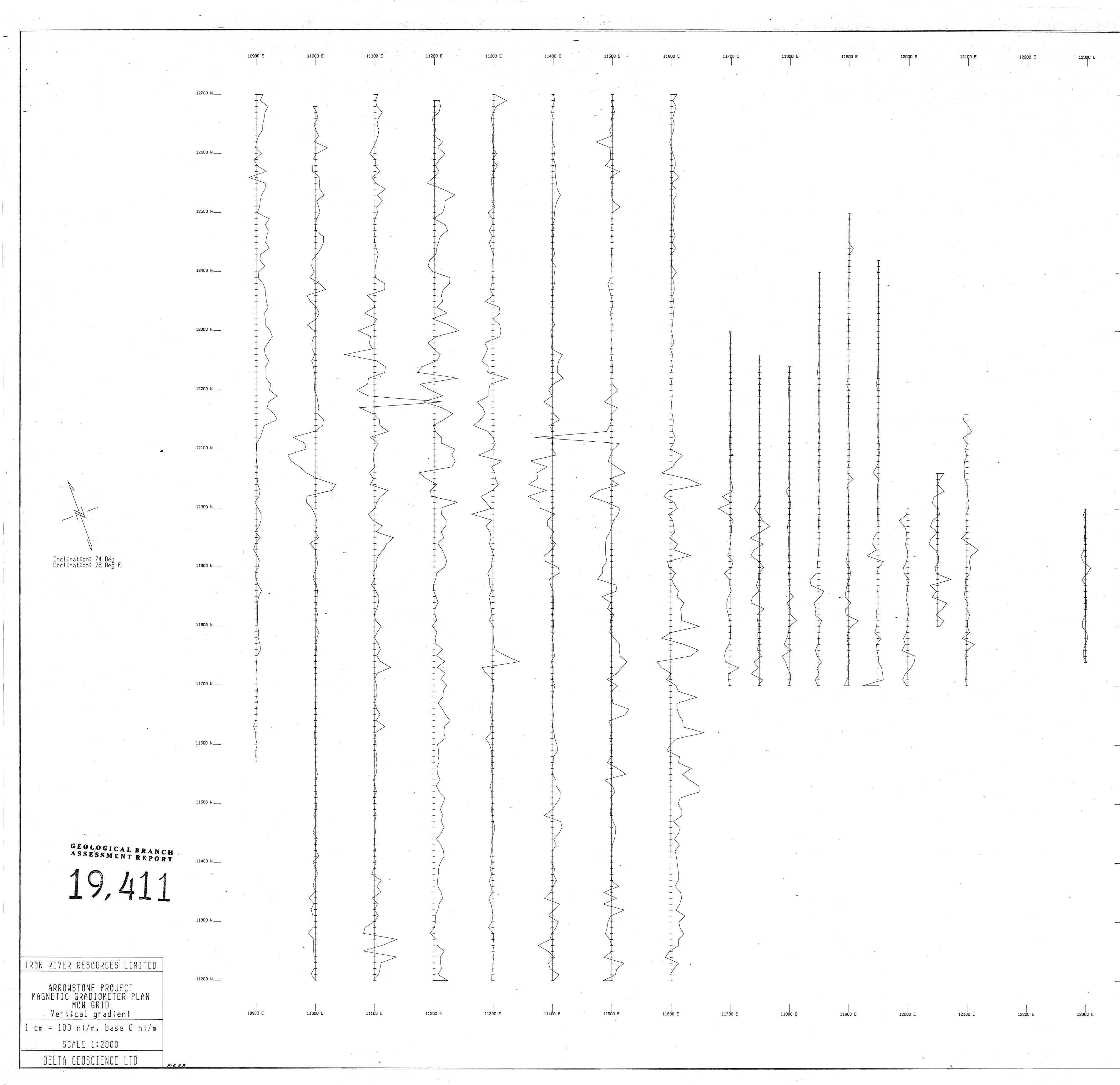
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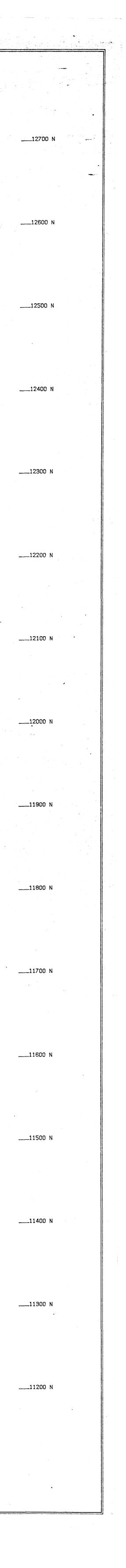
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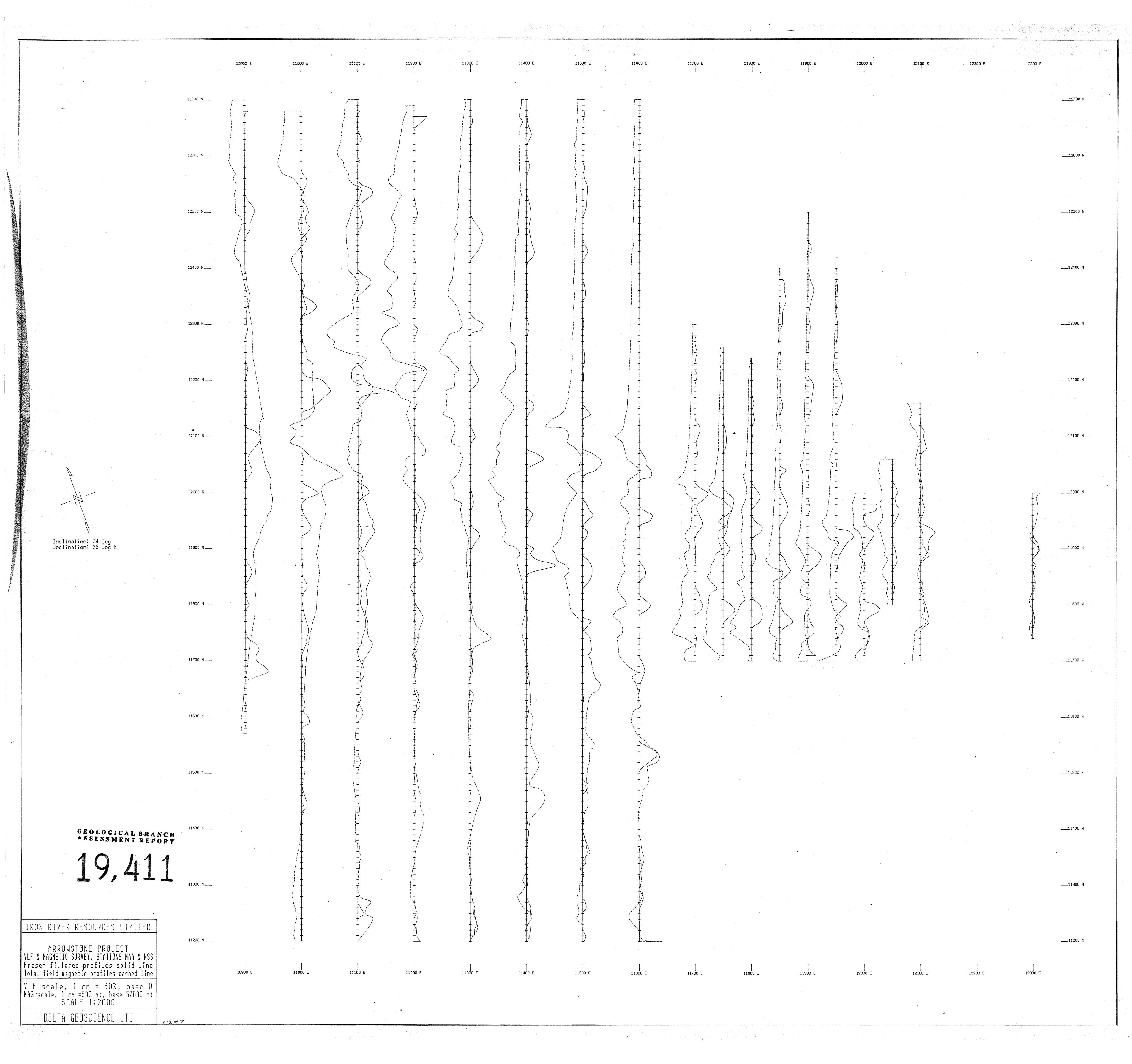
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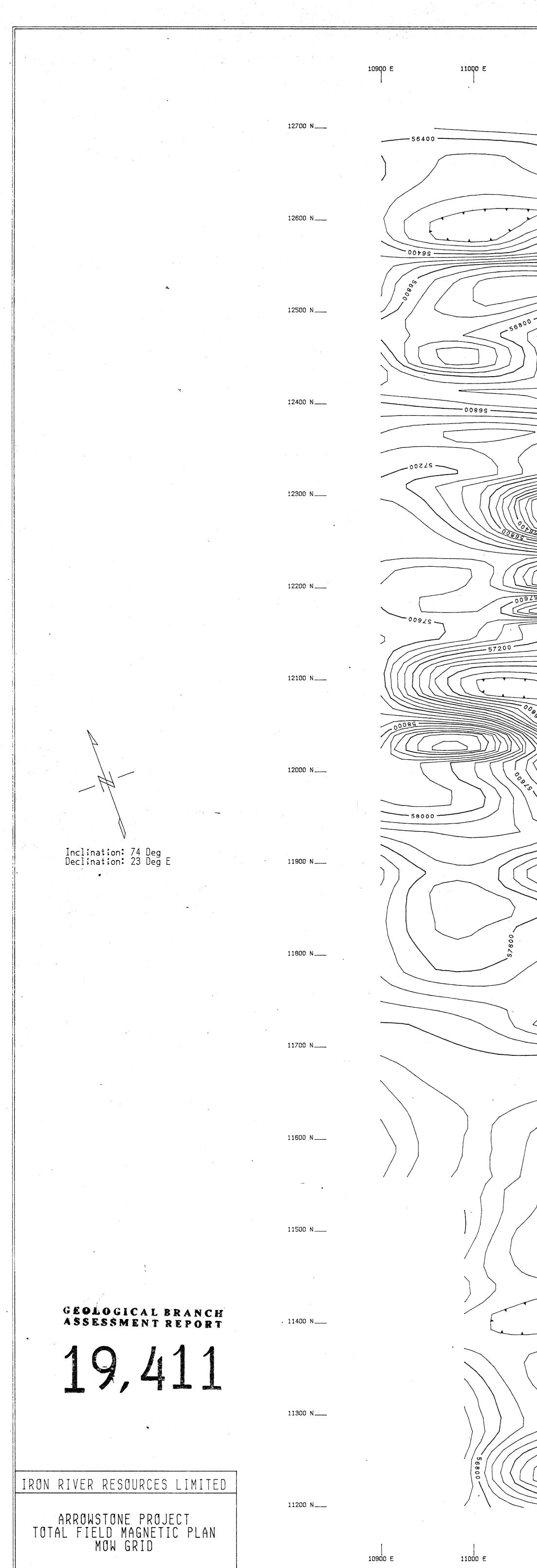
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contour interval 100 nt SCALE 1:2000 DELTA GEOSCIENCE LTD

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