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Property and Assessment  
for the  
1989 Work Program  
on the  
Spring Property  
(Venture 232)

VOLUME I

- Mineral Claims:  
Spring 3  
Boomer 1 - 4  
Pick 1 - 6  
Pick Fr. 6 - 8  
AK 1 to 4

Similkameen Mining Division

N.T.S. 92H/16

Latitude: 49° 47' N, Longitude: 120° 08' W

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December, 1989

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

19,420 part 1 of 2

TABLE OF CONTENTS

<u>VOLUME I</u>	<u>Page</u>
1.0 SUMMARY . . . . .	1
2.0 DESCRIPTION OF PROPERTY . . . . .	2
2.1 Objectives . . . . .	2
2.2 Location and Access . . . . .	3
2.3 Physiography and Climate . . . . .	3
2.4 Claim Status . . . . .	7
2.5 History . . . . .	7
3.0 DESCRIPTION OF WORK PROGRAM . . . . .	8
3.1 Linecutting and Grid Establishment . . . . .	8
3.2 Geologic Mapping and Rock Sampling . . . . .	9
3.3 Soil Sampling . . . . .	9
3.4 Geophysical Surveys . . . . .	11
3.5 Surface Trenching . . . . .	13
4.0 REGIONAL GEOLOGICAL SETTING . . . . .	14
5.0 PROPERTY GEOLOGY . . . . .	15
5.1 Lithologies . . . . .	15
5.2 Distribution . . . . .	16
5.3 Structure . . . . .	17
5.4 Alteration . . . . .	18
5.5 Mineralization . . . . .	18
6.0 DETAILED GEOLOGIC MAPPING AND SAMPLING . . . . .	19
6.1 Rock Geochemistry . . . . .	19
6.2 Outcrop Descriptions, Results, and Interpretation	20
6.2.1 Zone C . . . . .	21
6.2.2 Zone N2 . . . . .	22
6.2.3 Zone P4 . . . . .	24
6.3 Trench Descriptions and Results . . . . .	26
Zone 2 Area . . . . .	26
6.3.1 Trench 785E . . . . .	26
6.3.2 Trench 825E . . . . .	27
6.3.3 Trench 842E . . . . .	27
6.3.4 Trench 858E . . . . .	28
6.3.5 Trench 1388E . . . . .	28
6.3.6 Trench 1393E . . . . .	29
Zone 4 Area . . . . .	29
6.3.7 Trench 1010W . . . . .	29
6.3.8 Trench 1335W . . . . .	30
6.3.9 Trench 1378W . . . . .	31
6.3.10 Trench 1565W . . . . .	32
North Trout Creek Area . . . . .	33
6.3.11 Trench 001E . . . . .	33
6.3.12 Trench 170W . . . . .	33
6.3.13 Trench 265N . . . . .	34

6.3.14 Trench 837N . . . . .	34
6.3.15 Trench 847N . . . . .	35
6.3.16 Trench 930N . . . . .	35
6.3.17 Trench 969N . . . . .	36
East Zone Area . . . . .	36
6.3.18 Trench 3228E . . . . .	36
6.3.19 Trench 3427E . . . . .	37
6.4 Interpretation of Trenching Results . . . . .	37
7.0 SOIL GEOCHEMISTRY . . . . .	38
7.1 Results . . . . .	38
7.2 Interpretation . . . . .	40
8.0 GEOPHYSICAL SURVEYS: RESULTS AND INTERPRETATION . . . . .	41
8.1 VLF-EM Survey . . . . .	41
8.2 Magnetometer Survey . . . . .	42
8.3 Induced Polarization and Resistivity Survey . . . . .	44
8.3.1 Zone 2 . . . . .	44
8.3.2 Zone 4 . . . . .	44
8.3.3 Line 200 West . . . . .	44
9.0 CONCLUSIONS . . . . .	45
10.0 RECOMMENDATIONS . . . . .	46
11.0 STATEMENT OF EXPENDITURES . . . . .	46
12.0 REFERENCES . . . . .	48
13.0 STATEMENTS OF QUALIFICATION . . . . .	49
13.1 Statement of Qualification, M. Deschenes . . . . .	49
13.2 Statement of Qualification, R. W. Cannon . . . . .	50
13.3 Statement of Qualification, H. Letient . . . . .	51
13.4 Statement of Qualification, R. Pease . . . . .	52

## LIST OF FIGURES

Figure 1.	Property Location Map . . . . .	5
Figure 2.	Claim Map . . . . .	6
Figure 3.	Grid Location . . . . .	Volume II
Figure 4.	Geology . . . . .	"
Figure 5.	Sample, Trench and Outcrop Location . .	"
Figure 6.	North Trout Creek Area: Sample, Trench and Outcrop Location . . . . .	"
Figure 7.	Detailed Sketch of Sampling Zone C and Geochemical Sample Analysis . . . . .	"
Figure 8.	Detailed Sketch of Sampling Zone N2 and Geochemical Sample Analysis . . . . .	23
Figure 9.	Detailed Sketch of Sampling Zone P4 and Geochemical Sample Analysis . . . . .	25
Figure 10.	Trench Plan, Zone 2 Area West Half: TR0785E, TR0825E, TR0842E, TR0858E . .	Volume II
Figure 11.	Trench Plan, Zone 2 Area East Half: TR1388E, TR1393E . . . . .	"
Figure 12.	Trench Plan, Zone 4 Area: TR1010W . . .	"
Figure 13.	Trench Plan, Zone 4 Area: TR1335W TR1378W . . . . .	"
Figure 14.	Trench Plan, Zone 4 Area: TR1565W . . .	"
Figure 15.	Trench Plan, North Trout Creek Area: TR001E . . . . .	"
Figure 16.	Trench Plan, North Trout Creek Area: TR0170W, TR0265N . . . . .	"
Figure 17.	Trench Plan, North Trout Creek Area Central Zone: TR0837N, TR0847N . . . .	"
Figure 18.	Trench Plan, North Trout Creek Area North Zone: TR0930N, TR0969N . . . . .	"
Figure 19.	Trench Plan, East Zone Area: TR3228E . .	"
Figure 20.	Trench Plan, East Zone Area: TR3427E . .	"
Figure 21.	Gold in Soil - Symbol Plot . . . . .	"
Figure 22.	Copper in Soil - Symbol Plot . . . . .	"
Figure 23.	Zinc in Soil - Symbol Plot . . . . .	"
Figure 24.	Lead in Soil - Symbol Plot . . . . .	"
Figure 25.	Silver in Soil - Symbol Plot . . . . .	"
Figure 26.	Stacked VLF Profiles - Main Grid . . . .	"
Figure 27.	Stacked VLF Profiles - NW Grid . . . . .	"
Figure 28.	Stacked Magnetic Profiles - Main Grid . .	"
Figure 29.	Stacked Magnetic Profiles - NW Grid . .	"
Figure 30.	Real Time Imaging Package . . . . .	43

## LIST OF TABLES - Volume I

Table 1. Mineral Claim Schedule . . . . .	7
Table 2. Selected Anomalous Rock Samples In Outcrops . . . . .	20
Table 3. Selected Anomalous Rock Samples in Trenches . . . . .	20
Table 4. Statement of Expenditures . . . . .	47

## LIST OF APPENDICES

APPENDIX I	Petrographical Report
APPENDIX II	Listing of Rock Sample Data
APPENDIX III	Rock Sample Statistical Summary and Histograms
APPENDIX IV	Trench Logs
APPENDIX V	Listing of Trench Soil Profile Sample Data
APPENDIX VI	Listing of Soil Sample Data
APPENDIX VII	Soil Sample Statistical Summary and Histograms
APPENDIX VIII	Seismic Refraction Survey
APPENDIX IX	Contour Resistivity and Chargeability Pseudosections

## 1.0 SUMMARY

The Spring Property is owned by Golden Pick Resources Limited and is currently under option to Placer Dome Inc. The property is located 30 kilometres west of the village of Peachland, in south-central British Columbia. The target mineralization is a structurally controlled lode gold deposit, possibly the source of gold bearing placer deposits known to occur on the property.

The Spring Property is almost entirely underlain by acidic intrusive rocks. These rocks fall into two groups, one an older Jurassic granite, and the other a more complex, generally altered, Tertiary monzonite. Large scale regional faults transect the property. Faults and/or shear zones would provide channels for mineralizing fluids and structural traps for deposit formation. Mineralization would likely be associated with a Tertiary event.

Placer Dome Inc. executed a work program between May 16 and August 15 1989. The surveys consisted of the following projects:

- (i) 102 kilometres of grid establishment and linecutting (extension of the 1988 grid)
- (ii) Geological mapping at 1:10,000 scale
- (iii) Detailed geological mapping at 1:50 scale of three specific alteration zones anomalous in precious/base metals
- (iv) Collection of 2367 soil samples for geochemical analysis
- (v) Collection of 850 rock samples for geochemical analysis
- (vi) Induced Polarization survey over 15.2 kilometres of line
- (vii) Magnetometer and VLF-EM surveys over 75 kilometres of line
- (viii) Excavation of 19 trenches totalling 1133 metres, and 49 test pits, in four specific target areas.

Detailed fill-in soil sampling and IP surveys were conducted to identify trench targets in areas where gold-in-soil anomalies had been determined in 1988. Soil sampling,

magnetometer and VLF-EM surveys were conducted on new claims added to the northwestern portion of the property.

The fill-in soil sampling failed to confirm anomalous trends, partially due to excessive overburden. No significant soil anomalies were determined on the new claims. Results from fill-in soil sampling, trenching, and overburden profile sampling all indicate that soil anomalies in areas of thick overburden must be considered suspect.

Induced Polarization surveys revealed three areas of interest. The most significant being the 700 metre long Zone 2 anomaly, however, thick overburden prevented complete trench testing. The magnetometer and VLF-EM surveys were particularly useful in delineating geologic contacts and structures on the new claims in the northern portion of the property.

Anomalous metal values generally correlate with argillic alteration, shearing, and an increase in fracture intensity. Sampling of outcrop in Zone C detected a 7.7 metre interval averaging 88 ppb gold along a sheared and clay altered contact between an andesite dyke and a tectonic breccia. Trench 1010W yielded a maximum of 300 ppb gold across 1.5 metres of a clay altered shear zone. Significant silver, lead, and zinc anomalies were also determined in these zones. Anomalous levels of lead, zinc, antimony, and silver were determined in trench 001E excavated across the Main alteration zone.

The rock geochemistry and IP anomalies were determined of sufficient tenor to warrant a small program of drill testing. Targets are defined as follows;

- (i) Zone 2 IP anomaly between lines 6+00E and 10+00E.
- (ii) Strike extensions of the Main alteration zone.
- (iii) Depth extension of Zone C.
- (iv) Anomalous gold geochemistry in Trench 1010W.

## 2.0 DESCRIPTION OF PROPERTY

### 2.1 Objectives

The target mineralization on the property is epithermal high-grade gold (plus silver, lead, and zinc) bearing structures possibly associated with argillic altered fault

or shear zones. The other possible target type is a large tonnage-low grade gold bearing "porphyry" system. The objectives of the 1989 work program were four-fold: Firstly, to conduct detailed geologic mapping and systematic rock chip sampling in lithologically anomalous gold zones C, N, and P. Secondly, to conduct detailed geologic mapping, prospecting, fill-in soil sampling, magnetometer, VLF-EM, and IP surveys over areas of previous anomalous gold-in-soil values. Thirdly, conduct a program of surface trenching to test specific geochemical and geophysical anomalies, and identify drill targets. Fourthly, to extend the 1988 grid, geologic map, prospect, soil sample, and conduct VLF-EM and magnetometer surveys over the newly staked northern claims. This would add to the existing database and assist in the targeting of other areas for more detailed work.

## 2.2 Location and Access

The Spring project is located 30 kilometers west of Peachland, B.C., on NTS map sheet 92H/16 (see Figure 1). The claim block is roughly centred on the triple junction of Trout Creek, North Trout Creek, and Spring Creek.

Road access to the property can be gained from several directions. The route via Peachland is west on the Brenda Mine road to the Headwaters road, followed by a left turn on this road and thence on to the junction with the Trout Creek Main logging road. A left turn is made on to the Trout Creek road, and it can be followed into the property. An alternate route from Princeton is east on the Princeton-Summerland road, past the village of Bankeir, followed by a left turn onto the Trout Creek Main logging road, and on into the property. Old and new logging roads and trails provide excellent access around the property.

## 2.3 Physiography and Climate

The property lies within the southern portion of the Thompson Plateau. The terrain is gentle to moderate over most of the property, except for North Trout Creek and portions of Spring Creek which flow through steep-sided ravines. Also, the terrain north and east of Trout Creek rises sharply up the northwestern slope of Mount Kathleen. Elevation ranges from 1200 to 1600 metres.

Vegetation consists of mainly open to moderately dense stands of spruce, poplar, pine, and fir with light underbrush. Approximately 50% of the property has been



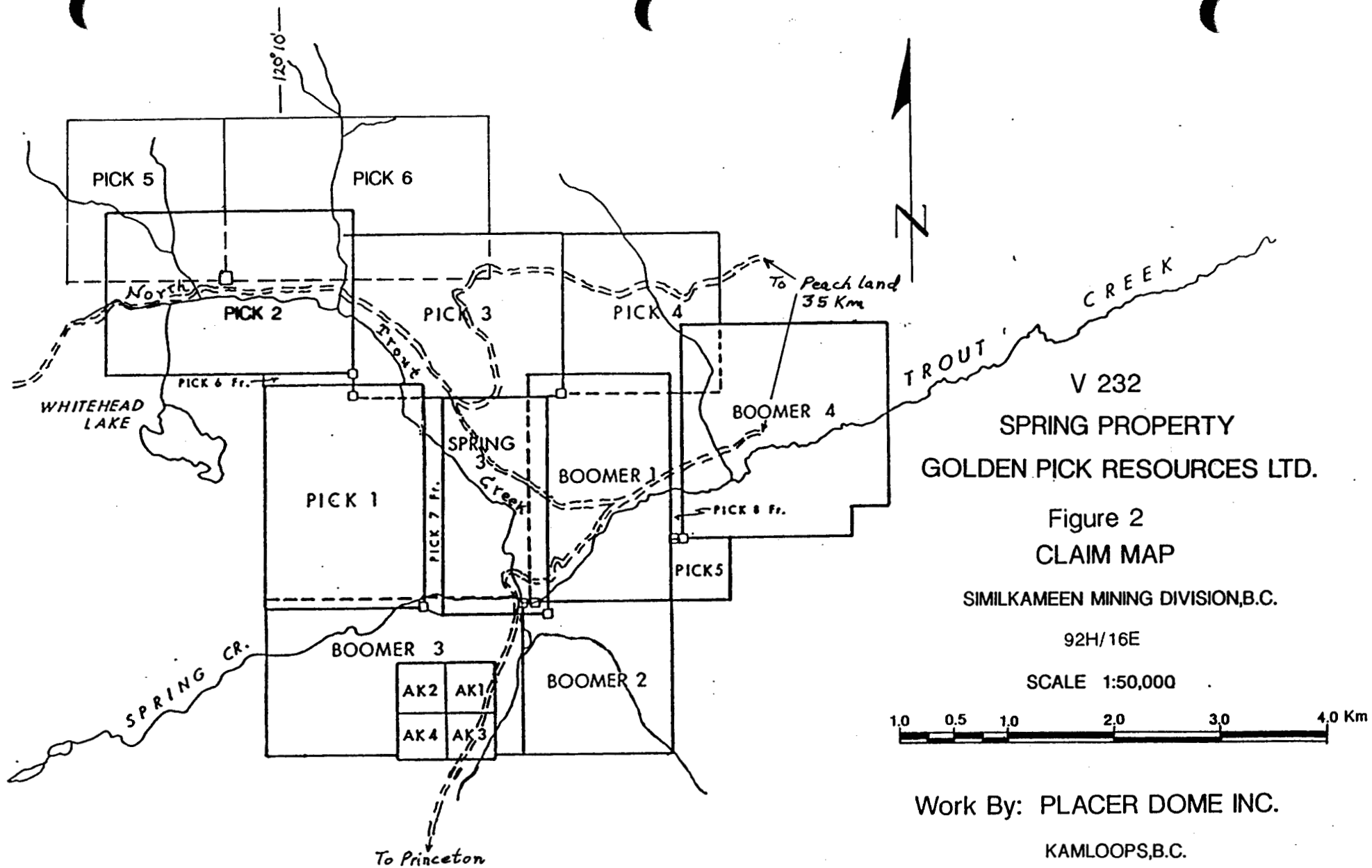
logged, mainly north of Trout Creek. The Trout Creek valley, east of the North Trout Creek junction, tends to be swampy.

Reasonable weather conditions for exploration work can be expected from early May to mid October. Winter snow pack can reach 1.5 metres.



**PLACER DOME INC.**  
 Figure 1  
**PROPERTY LOCATION MAP**

100 0 100 200  
 MILES



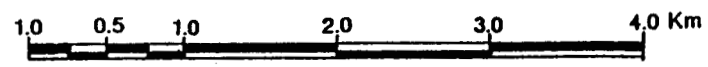
V 232  
 SPRING PROPERTY  
 GOLDEN PICK RESOURCES LTD.

Figure 2  
 CLAIM MAP

SIMILKAMEEN MINING DIVISION, B.C.

92H/16E

SCALE 1:50,000



Work By: PLACER DOME INC.

KAMLOOPS, B.C.

SEPTEMBER, 1989

— 49°45' —

## 2.4 Claim Status

Two new claims were staked on the northern border of the property to cover the extension of strong VLF-EM conductors. The Spring property covers approximately 3500 hectares. It consists of nineteen contiguous mineral claims totalling 140 units as shown on Figures 2, 3, 4 and 5, and as listed in Table 1. All of the claims are wholly owned by Golden Pick Resources Ltd.

Table 1. Mineral Claim Schedule

<u>Claim Name</u>	<u>No. of Units</u>	<u>Record Number</u>	<u>Expiry Date</u>
Spring 3	8	1466	July 13, 1994
Boomer 1	12	2425	July 31, 1994
Boomer 2	9	2426	July 31, 1994
Boomer 3	15	2427	July 31, 1994
Boomer 4	16	3063	November 13, 1994
Pick 1	12	3129	June 23, 1993
Pick 2	15	3130	June 23, 1993
Pick 3	12	3252	November 23, 1989
Pick 4	9	3253	November 24, 1989
Pick 5	1	3254	November 24, 1989
Pick 6 Fr.	1	3255	November 24, 1989
Pick 7 Fr.	1	3256	November 24, 1989
Pick 8 Fr.	1	3257	November 24, 1989
AK 1	1	3135	June 29, 1994
AK 2	1	3136	June 29, 1994
AK 3	1	3137	June 29, 1994
AK 4	1	3138	June 29, 1994
Pick 5	9	3439	July 9, 1990
Pick 6	15	3440	July 16, 1990

## 2.5 History

A local prospector, Don Agur, placer mined gold from several small pits in North Trout Creek. These pits were located on the present Spring 3 mineral claim.

Prior to 1985, portions of the present claim block had been explored for "porphyry" Cu-Mo potential during 1972 and 1981 by Pan Ocean Oil and Brenda Mines respectively. Anomalous lead and zinc values in soils were determined, but never followed-up.

Boomer Resources (now Golden Pick Resources) acquired the property in 1985. By trenching with an excavator, they discovered two zones of intense clay alteration in the vicinity of Don Agur's old placer pits. These zones

contained anomalous lead and zinc values, and occasional traces of gold. Three short diamond drill holes were drilled into one zone located approximately 100 metres north of the North Trout/Trout Creek junction, near 0+00 on the baseline of the present grid. These holes intersected sporadic anomalous lead-zinc-silver mineralization, within an intensely clay altered porphyritic monzonite. This area was named the Main alteration zone.

Placer Dome optioned the property in 1988, and subsequently executed a work program of geologic mapping and sampling, grid establishment, bulk stream sediment sampling, soil sampling, magnetometer, and VLF-EM. Two separate zones of altered bedrock were determined to contain anomalous gold concentrations with significant silver, lead, and zinc anomalies. The anomalies seem to be associated with a Tertiary quartz-feldspar porphyry or argillic altered cross-cutting fault or shear structures. A soil sample survey partially defined as many as ten anomalous gold zones or trends, varying from 400 to 1000 metres in length, at several locations on the property.

### 3.0 DESCRIPTION OF WORK PROGRAM

#### 3.1 Linecutting and Grid Establishment

Approximately 102 kilometres of base and cross lines, including fill-in soil sample lines, were constructed and tied into the 1988 grid (see Figure 3). Linecutting work on all base lines, totalling 7.0 kilometres, was done under contract by Grassroots Explorations Services of Kamloops. Base lines 27+00N, 50+00N, 55+00E, and 60+00N were brushed out, blazed, and flagged to "IP" standards, to provide control for other surveys.

Base line 27+00N was extended 2500 metres at 070 degrees. A new grid was established in the northwestern corner of the claim block with east-west oriented base lines to facilitate survey control (see Figure 3). These base lines were controlled by Silva compass and tight chain measurements. Perpendicular cross lines were positioned at 200 metre intervals, flagged and controlled by Silva compass and hip chain measurements. Stations were marked with black felt pens on orange flagging or white shipping tags, and established at 25 metre intervals.

Fill-in soil sample lines, totalling 31 kilometres, were positioned at 100 metre intervals in areas of anomalous gold-in-soil values. Line intervals of 50 metres were used

adjacent to values exceeding 100 ppb gold to better define these anomalous zones.

### 3.2 Geologic Mapping and Rock Sampling

Outcrop locations were mapped and plotted at 1:10,000 scale shown on Figure 5. An enlarged view of the North Trout Creek area is shown on Figure 6. A geological map shown on Figure 4, was interpreted using field notes and geophysical data. The cut lines and 1:20,000 scale airphotos were used for geologic mapping control.

Outcrops are more abundant in the steeper creek ravines and along some road cuts. Generally, the outcrop density is comparatively sparse. Overburden depth likely varies from 1.0 to 15.0 metres.

A total of 125 rock samples (grab and/or chip) were collected. Sample locations were identified in the field with flagging tape, and are plotted on Figure 5. Notes were recorded at each sample site regarding lithology, texture, alteration, and mineralization.

Rock samples were shipped to Placer Dome's Geochem Laboratory in Vancouver for geochemical analysis of gold, silver, copper, lead, zinc, arsenic, and antimony. A summary of the rock sample data is listed in Appendix II.

A total of five character rock samples were sent to Vancouver Petrographics Ltd. of Vancouver for petrographic analysis. A detailed report is listed in Appendix I.

More detailed geologic mapping and systematic rock chip sampling were repeated in areas of lithological gold anomalies, specifically Zones C, N2, and P4. These outcropping alteration zones were mapped and re-sampled across, above, and below anomalous samples which were determined in 1988. Figures 7, 8, and 9 are sketch maps for each zone mapped at 1:50 scale with tabulated geochemical results. A statistical summary and histograms of the combined 1988 and 1989 lithogeochemical results are listed in Appendix III. The rock chip samples were taken over intervals averaging 1.5 metres and marked with red fluorescent spray paint.

### 3.3 Soil Sampling

Overburden thickness and composition varies on the Spring property. Generally, the area east of North Trout Creek is covered by glacial till, and to the west is

covered by colluvium. The major stream valleys, Trout and North Trout Creeks, are in-filled with alluvial deposits. In any of these cases, overburden thickness likely varies from 1.0 to 15 metres.

Soil development is very consistent. A thin layer of A1-horizon soil consisting of decomposing organic material typically 2.0 to 5.0 cm thick overlies a very thin, if present at all, leached greyish white A2-horizon. Soil below this leached horizon, and down to a depth of 50 cm, is composed of a reddish-brown, sandy clay, B2-horizon.

Conventional soil sampling as an exploration technique may be suspect in areas like the Spring property which do appear to be covered by glacial till and/or relatively thick deposits of colluvium or alluvium. However, sampling the B-horizon soil and analyzing the -80 mesh fraction for base metals and gold, has proven to be a successful exploration technique on a nearby property. This property has similar geology and overburden characteristics as the Spring property.

A total of 2367 soil samples was collected on the property, 1177 of these from fill-in lines over areas of previous gold anomalies. Fill-in samples were collected at 25 metre intervals on 100 metre spaced lines or 50 metre spaced lines adjacent to gold values >100 ppb. Samples were collected at 50 metre intervals on the new grid lines.

Samples of B2-horizon material were collected from 15 to 50 cm deep holes excavated with narrow-bladed, short-handled (tree planting) shovels. The B2-horizon was generally well developed and easily recognized as a reddish-brown sandy clay beneath the shallow organic and leached horizons.

Samples were placed in brown kraft paper envelopes, and labelled with line and station for identification. Notes were recorded at each sample site regarding site conditions, sample depth, soil composition and grain size, and rock fragment composition.

Samples were shipped to Placer Dome's Geochem Laboratory in Vancouver for geochemical analysis of copper, lead, zinc, silver, and gold. The samples were dried in a hot-air dryer and sieved to extract the -80 mesh fraction. After digestion in aqua-regia solution, analysis was completed by atomic absorption.

The geochemical results of the soil sample survey are listed in Appendix VI. These results were combined with the 1988 soil geochemical results to produce statistical

summaries and histogram plots for each metal, which are presented in Appendix VII. Figures 21 through 25 are location plots for each metal, with the size of the plot symbol scaled to the magnitude of the geochem value. The 1988 and 1989 soil survey data were plotted together using different plot symbols. Anomalous trends and/or anomalous areas are also interpreted on these plots. The field grid coordinate for each soil sample has been converted into a UTM based coordinate system to facilitate accurate plotting.

### 3.4 Geophysical Surveys

Magnetometer and VLF-EM surveys were carried out along 75.62 kilometres of line, 35.4 kilometres of extension line on the 1988 grid and 40.22 kilometres of line on the new grid in the northwest portion of the claim block. The field grid co-ordinates for each reading were converted into a UTM based co-ordinate system to facilitate accurate plotting.

A limited Induced Polarization and Resistivity survey was conducted over areas of previous gold-in-soil anomalies and covered 15.15 kilometres of line on the 1988 grid.

An experimental seismic refraction survey was conducted over areas of geochemical and geophysical anomalies in order to establish the overburden thickness at potential trenching sites. Results and interpretation are discussed in Appendix VIII.

The VLF-EM survey was conducted using a Geonics EM-16. Along the northwest trending extension lines of the 1988 grid, the survey employed the transmitting station at Jim Creek (near Seattle), Washington. Along the north trending lines of the northwest grid, the survey employed the transmitting station at Cutler, Maine, except on lines 37+00E and 39+00E between 50+25N and 59+75N where the Annapolis station was used. Readings were taken facing northerly along the lines at 25 metre intervals. Crossovers are therefore in the sense of positive to negative as one traverses north along the lines. Positive values are plotted on the west side of the profile plots. VLF readings were entered onto disk in a Zenith laptop portable computer in the field. The stored data was later transferred to a Sun computer system for final processing and plotting.

The magnetometer survey was conducted using two Geometrics G-856 portable proton magnetometers. One was used in field mode while the other was used in a base station mode. The internal clocks were synchronized before the commencement of the survey and subsequent daily readings were dumped out to disk in a Zenith laptop portable



computer. Magnetometer readings were taken at 12.5 metre stations and corrections for diurnal changes were made by use of the base station recordings and an established base station value. The corrected results were stored on disk for eventual transfer to a Sun computer system for final processing and plotting.

The data was also processed using the Real Time Imaging Package (see Figure 30). RTI is a state of the art, 256 colour VGA processing package developed by Geopak Systems, the software division of Urquhart-Dvorak Limited, in association with Aerodat Limited. The RTI package greatly assists comprehensive data interpretation through the use of high speed algorithms and screen drivers. It requires any XT, AT, or 386 computer with extended high resolution VGA capability and a math co-processor. Gridded (digital) geophysical data or its derivatives may be manipulated interactively on screen, either singulary or in stacked multiple grid format, by a mouse driven interface.

Colour or grey shadow displays of survey data may be varied according to selected colour tones and contrast. Inclination and declination of the "sun angle" in shadow mapping may be varied in real time (i.e. as the cursor moves - driven by the mouse - so does the apparent shadow produced by the "sun"). The on-screen image is three dimensional in nature and gives a pseudo topographic view of the data set. Controlled changes in the "sun angel" greatly enhance structural features, geological contacts and lithologic changes, and assist the interpreter (user) in identifying subtle trends not readily apparent in the hard copy map products usually associated with geophysical data.

The Induced Polarization and Resistivity survey was conducted using a Scintrex IPR-11 time domain, microprocessor based receiver and a Scintrex IPC7 2.5 kilowatt transmitter. Readings were taken using a two second alternating square wave. The chargeability for channel 8 (690 to 1050 milliseconds after shut off; midpoint at 870 milliseconds) is the value that has been plotted on the accompanying plans and pseudosections shown in Appendix IX.

The pole dipole electrode array was used for the survey, with readings taken at an "a" spacing of 25 metres and "n" separations of 1, 2, 3, 4, and 5. The current electrode was to the south of the potential electrodes on all survey lines.

The survey data was put in archive, processed and plotted using a Sharp PC7000 microcomputer running Scintrex Soft II, IGS and proprietary software. All chargeability

values were analyzed for their spectral characteristics using a curve matching procedure (Soft II). The Cole-Cole parameters, "c" and "tau" were calculated along with a goodness-of-fit. This fit parameter is a measure of the data quality, in as much as the data can be seen to conform to pre-established waveforms. Large "tau" values are indicative of large "grain" size. The "c" parameter is a measure of the variability or homogeneity of the "grain" size.

### 3.5 Surface Trenching

Nineteen trenches totalling 1133 metres were excavated in four separate target areas to test geochemical and/or geophysical anomalies and aimed at identifying drill targets. A total of 49 test pits were dug, and immediately reclaimed, where bedrock could not be reached due to deep overburden. Excavation was done under contract by Dobbin Construction Ltd. of Kelowna, B.C. Trench and test pit locations are shown on Figure 5.

Bedrock was attained in most of the trenches although irregular rock surfaces and deep overburden sometimes slowed progress. Depth of trenches varied from 0.5 to 5.0 metres.

All trenches were dug using a Cat D205 excavator with two types of buckets. An 18 inch toothed bucket was used for digging through overburden and a 36 inch smooth edge bucket for cleaning soil and clay from the bedrock surface. A Gardner 170 CFM air compressor and hose were used to clean the remaining soil from trench floors. A Briggs & Stratton diaphragm pump and hose were used to dewater flooded sections of trenches.

Each trench was surveyed, mapped in detail and plotted at 1:250 scale, chip sampled, and overburden profile sampled. Trench plans are shown on Figures 10 through 20. Trenches were surveyed using a Silva compass, a 50 metre fibreglass tape, and tied into the field grid. Geologic and sample data were logged on coded forms using the "GEOLOG" system and transferred onto a computer for plotting of plan maps and further processing. The logs were used to record trench identity information, survey data, geologic data, sample data, and geochemical analysis results. Details of the logs along with a logging code explanation are listed in Appendix IV.

A total of 725 rock chip and grab samples were collected from the trenches. Continuous chip samples were systematically taken over intervals averaging 1.5 metres over areas of altered or favourable looking bedrock. Sample

intervals were marked with red fluorescent spray paint along trench walls. Each sample contained approximately 2 to 5 kilograms of chips, ranging from sand size to five centimetres, which were placed in plastic bags.

Rock samples were shipped to Eco-Tech Laboratories Ltd. in Kamloops, British Columbia for geochemical analysis of gold, silver, copper, lead, zinc, arsenic, and antimony. A summary of the geochemical results is included in the trench logs listed in Appendix IV. Significant metal values were plotted on the trench plan maps shown on Figures 10 through 20. Statistical summaries and histograms for each metal were included in Appendix IV.

Overburden sample profiles were collected from the trench walls at 10 metre stations. A total of 326 soil samples were collected from the B and C horizons and at the bedrock interface. In each profile, samples were collected down the wall of the trench at 1.0 metre depth intervals. A sample of the B2-horizon material, labelled A, was first collected and subsequent samples were collected in the C-horizon and labelled B, C, D, etcetera, until bedrock was reached. Samples were placed in brown kraft paper envelopes and labelled with the trench name, grid location and depth, denoted by a letter. Overburden data was recorded in the same manner as the soil survey.

Samples were shipped to Placer Dome's Geochem laboratory in Vancouver for geochemical analysis of copper, lead, zinc, silver, and gold. A summary of the trench overburden sample profile data is listed in Appendix V. Significant metal values were plotted on the trench plan maps shown on Figures 10 through 20.

All trenches were reclaimed, grass seeded, and fertilized. Trenches are now identified in the field by a 2x4 inch wooden post marked with florescent red paint. An aluminum tag stating the trench name and collar position is fixed to the post.

#### 4.0 REGIONAL GEOLOGICAL SETTING

The regional geological setting of the Spring property area is relatively simple. The oldest rocks in the vicinity of the property are large xenoliths of basement rocks of Paleozoic age rafted within the younger intrusives.

They are composed of weakly to moderately foliated biotite and hornblende gneiss.

The Paleozoic rocks are structurally underlain by the Jurassic rocks of the Coast Intrusions which dominate the region. They form a large batholith of granitic to dioritic composition.

The Jurassic plutonic rocks are cut by Late Cretaceous to Tertiary intrusions of granite, monzonite, and diorite, and injected by a series of andesitic dykes. Some of these were likely emplaced in the Eocene during extensional strain. Large scale linears trending 070 and 150 degrees are likely associated with this strain. Mineralizing events were possibly associated with this strain as well, making the Tertiary intrusions and nearby structures good exploration targets.

## 5.0 PROPERTY GEOLOGY

### 5.1 Lithologies

The property geology is illustrated on Figure 4. Seven rock units were identified and are briefly described.

#### (i) Unit 1 Porphyritic Quartz-Feldspar Monzonite

Petrographic analysis determined this rock type to be of monzonitic composition. Quartz eyes, often composing 5.0 to 10.0% of the rock, reach up to 1.5 centimetres in diameter. Subhedral feldspar phenocrysts, composing up to 30% of the rock, were noted up to 4.0 centimetres in length. The matrix is commonly fine grained, and usually a chalky tan to grey colour. Outcrops often weather to a rusty brown colour, especially with increasing pyrite content, and tend to be fractured with occasional cross-cutting shear zones.

#### (ii) Unit 2 Biotite-Hornblende Quartz-Diorite

The diorite is a medium grained, equigranular aggregate of plagioclase, quartz with less biotite. Mafic minerals are often altered to chlorite and plagioclase is altered slightly to sericite. Outcrops tend to be fractured with occasional cross-cutting shear zones and weather grey-brown to green.

#### (iii) Unit 3 Sheared Porphyritic Rhyodacite

Only one outcrop of this rock type occurs on the property. Relatively small, up to 2.5 millimetres,

phenocrysts of plagioclase are set in a fine grey matrix. Chlorite alteration is light to moderate. The rock is characterized by a stockwork of quartz-opaque and displays some degree of magnetism. Outcrops tend to be fractured and sheared and weather dark grey to rusty brown colour.

(iv) Unit 4 Tectonic Breccia

Well rounded fragments, up to 30 centimetres in diameter, composed of Unit 1 and Unit 3 are set in an open matrix of the same composition. The fragments and groundmass are all altered to a yellowish white colour. The outcrops tend to be massive with a distinguishing black and rusty brown weathering colour.

(v) Unit 5 Hypabyssal Andesite Dyke

A few small outcrops of this rock type occur on the property. It is a dark green, fine-grained andesite dyke with a few small, elongate hornblende phenocrysts averaging 1.5 millimetres long. Chlorite alteration is pervasive and carbonate alteration is minor. The rock is very fractured and weathers rusty brown.

(vi) Unit 6 Granite Pegmatite

Unit 6 is a relatively coarse grained, fresh looking granite. Subhedral feldspar grains up to 1.0 centimetres long, set in a matrix of quartz, biotite, and hornblende, dominate the rock. Outcrops are usually massive and fresh but can weather to a buff brown colour.

(vii) Unit 7 Plagioclase-Quartz-Biotite/Hornblende Gneiss

The gneiss is relatively fine grained, dark grey to black in colour, and composed of plagioclase, quartz, biotite and/or hornblende. The biotite gneiss displays moderate foliation and weathers to a rusty brown colour. The hornblende gneiss shows a weak foliation and outcrops are fresh looking.

## 5.2 Distribution

The Unit 1 and 2 dominate the southern portion of the property. They are also exposed as scattered outcrops along

the creeks flowing across the Pick 5 and 6 claims. This distribution is also reflected by the low magnetic signature as shown on Figures 28 and 29. Both units are believed to be Tertiary. Due to the frequent intermixing of these two units, such as seen in trench 1565W (Figure 14) and their predominant potassic composition, both Units 1 and 2 have been grouped on the geology map (Figure 4).

The Unit 3, a sheared porphyritic rhyodacite with a quartz stockwork, is exposed along North Trout Creek (Zone N2 on Figure 6). It likely is related to a structural event due to the sheared nature of the rock and its associated stockwork.

Outcrops of Unit 4 (tectonic breccia) are exposed along North Trout Creek in the Spring 3 claim (Zone C and P4 on Figure 6). The outcrop in Zone P4 displays a more brecciated texture and is characterized by heavy, black coloured pyrolusite staining.

The Unit 5, andesite dykes, are exposed as a few scattered outcrops in the western portion of the property. The largest exposure is located along North Trout Creek in the northern portion of the Spring 3 claim (Zone C on Figure 6). The contact with the underlying tectonic breccia is sheared and intensely clay altered.

The Unit 6 granite pegmatite dominates the northwestern portion of the claim block. A few scattered outcrops are also exposed in the Boomer 4 claim. It tends to have a higher magnetic signature which can be outlined on Figures 28 and 29. Unit 6 is interpreted to be part of the Jurassic Coast Intrusions.

Unit 7, biotite and hornblende gneisses, are believed to occur as large xenoliths of basement rocks, rafted within the younger intrusives. Exposures of the biotite gneiss are located in the middle of the Boomer 4 claim and as a few scattered outcrops in the northern portion of the Pick 2 claim. Exposures of the hornblende gneiss occur as scattered outcrops in the northern portion of the claim block where the Unit 6 granite is predominant. Outcrops also occur along North Trout Creek in the southwest corner of the Pick 3 claim, and in the southeast corner of the Boomer 4 claim. This unit represents the oldest rock type on the property and clearly shows a higher magnetic response on Figures 28 and 29.

### 5.3 Structure

Regional lineaments trending 070 and 150 degrees are reflected on a more detailed scale across the property.

Specifically, Trout, North Trout, and Spring Creeks are recognizable linears. These features can be outlined by the Real Time Imaging Package on Figure 30. They are also reflected by the major offsets in VLF trends as shown on Figures 26 and 27.

Trout Creek is interpreted to be a fault structure along the 070 degree trend and can be detected intermittently along strike by VLF conductors shown on Figures 26 and 27. Also, the Unit 6/Unit 1 contact at the northern portion of North Trout Creek, near the Pick 2/Pick 3 claim boundary, is interpreted as being fault bounded. The south flowing creek which crosses the Pick 4 and Boomer 4 claims is believed to be a fault structure. North Trout Creek is also interpreted to be a fault structure along the 150 degree trend across the Spring 3 and Pick 3 claims..

#### 5.4 Alteration

The dominate alteration assemblage observed on the property can be classified as argillic. The Unit 1 porphyritic quartz-feldspar monzonite is the most altered of all the map Units. Sericite alteration is prevalent, and occurs as replacement of feldspar phenocrysts and/or a pervasive alteration of the matrix. The Unit 2 biotite-hornblende quartz-diorite also displays sericite alteration of plagioclase. Mafic minerals, mainly biotite are often altered to chlorite. Low levels of silicification, chloritization, and carbonatization are also present in the Tertiary rocks, as well as varying degrees of limonite and pyrolusite staining.

Numerous shear zones displaying intense clay alteration were located in outcrops and trenches. These shear zones are usually less than 1.0 metre wide. Within the shear, original rock fabric is completely replaced by soft, white to blueish white, clay. The shear zones usually trend between 020 and 150 degrees and dip steeply.

Specific outcrops and trenches of altered bedrock are discussed individually in Sections 6.2 and 6.3 of this report.

#### 5.5 Mineralization

Rocks which are geochemically anomalous in gold, silver, copper, lead and zinc have been identified. These occurrences are discussed in Sections 6.2 and 6.3 of this report. No values which could be generally considered to

represent ore grade mineralization are known on the property.

Disseminated pyrite, up to 5.0 %, is common in Unit 1 porphyritic quartz-feldspar monzonite. Increased pyrite mineralization often is combined with an increased degree of sericite alteration, and in turn, these rocks often carry anomalous precious and/or base metal values.

Traces of disseminated chalcopyrite were found in Zones C and N2, and traces of disseminated galena were noted within the andesite dyke at Zone C. Small stockworks of magnetite were observed in Zones N2.

## 6.0 DETAILED GEOLOGIC MAPPING AND SAMPLING

### 6.1 Rock Geochemistry

Samples collected from outcrops and trenches during the 1988 and 1989 work programs were combined to undertake statistical analysis of the geochemical results. This was done to determine threshold levels which can be used to separate the anomalous population from the background. The following thresholds were determined; gold 45 ppb, copper 75 ppm, lead 550 ppm, zinc 750 ppm, silver 5.0 ppm, arsenic 75 ppm, antimony 1.0 ppm (see Appendix III).

Correlation between different metals is quite low. The correlation matrix indicates that all metals appear to behave quite independently except for lead and zinc which have a higher degree of correlation. However, correlation improves when samples are combined into similar lithological groups. Units 1 and 2 were combined due to their compositional similarities while the remaining samples of Units 3 to 7 were combined into a second group. The first group shows a strong correlation between copper and antimony, and lead and silver, while zinc and silver, and arsenic and silver also display good correlation. In the second group, gold and arsenic, and lead and zinc show a high degree of correlation.

Selected anomalous samples in outcrops and trenches are summarized in Table 2 and Table 3 respectively. Significant

metal values are also discussed in Section 6.2 with the outcrop descriptions and in Section 6.3 with the trench descriptions.



Table 2. Selected Anomalous Rock Samples In Outcrops

Zone	Length (Metre)	Au (ppb)	Ag (ppm)	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Sb (ppm)
N2	1.5	-	3.9	-	-	-	155	-
"	1.5	-	3.8	-	-	-	118	-
"	1.5	-	10.0	-	710	-	-	-
P4	1.5	-	-	-	-	1010	-	-
"	1.0	-	2.7	-	449	-	-	-
C1	0.5	-	-	-	1355	1390	-	-
"	4.5	103	5.1	-	-	-	540	-
"	0.75	85	4.5	-	-	1315	305	-
"	7.7	88	7.6	-	2868	1614	566	-
C3	1.5	75	27.0	90	5500	3300	290	-
"	3.2	-	6.0	-	2748	3280	-	-
"	1.5	-	3.3	109	2000	6500	-	-
C4	1.5	-	6.0	70	2070	3800	143	-
"	6.0	-	4.1	-	1080	1850	110	-

Table 3. Selected Anomalous Rock Samples in Trenches

Trench	Length (Metre)	Au (ppb)	Ag (ppm)	Cu (ppm)	Pb (ppm)	Zn (ppm)	As (ppm)	Sb (ppm)
TR0785E	1.5	-	8.2	-	393	668	-	-
TR0825E	4.5	-	1.9	-	256	1463	-	-
TR1388E	1.5	-	3.4	-	989	-	-	2.6
TR1393E	1.5	70	-	-	-	-	-	-
TR1010W	6.0	-	3.8	-	-	442	-	-
"	1.5	80	-	-	-	-	-	-
"	1.5	300	2.2	-	-	-	-	-
TR1565W	1.5	90	-	-	-	-	-	-
"	1.0	-	5.2	-	-	590	-	-
TR001E	1.5	-	6.1	-	394	725	-	6.8
"	1.5	-	-	-	1800	382	-	-
TR0847N	6.5	-	3.3	-	715	1757	-	-
TR9830N	4.5	-	-	-	-	900	-	-
TR3228E	1.5	-	-	76	-	-	42	10.5
TR3427E	1.5	-	1.0	711	-	350	41	-

## 6.2 Outcrop Descriptions, Results, and Interpretation

More detailed geologic mapping and systematic rock chip sampling were repeated in three specific alteration zones, in which anomalous precious and base metal values were determined in 1988. The following is a brief description,

summary of results, and interpretation of each zone. These naturally occurring outcrops were mapped at 1:50 scale and are shown on Figures 7, 8, and 9 along with tabulated geochemical results.

#### 6.2.1 Zone C

The zone occurs over a 50 metre length across an outcrop of Unit 5 (an altered hypabyssal andesite dyke) in contact with an underlying Unit 4 "tectonic breccia" (Figure 7). The zone is located along North Trout Creek road in the northern portion of the Spring 3 claim (see Figure 6). The contact is sheared, intensely clay altered, strikes 180 degrees and dips 030 to 045 degrees east. The andesite dyke is partially silicified, chloritized and carbonatized with minor amounts of disseminated pyrite and galena.

The "tectonic breccia" is interpreted as a sericite altered brecciated intrusive with fragments of Units 1, porphyritic quartz-feldspar monzonite and Unit 2, quartz diorite. Texture is locally vuggy and weathering is displayed as a high degree of limonite and pyrolusite staining. Mineralization occurs as minor amounts of disseminated pyrite and chalcopyrite.

Several anomalous metal values were detected on and/or near the contact zone. These include; 7.7 metres averaging 88 ppb gold, 7.6 ppm silver, 2868 ppm lead, 1614 ppm zinc, 566 ppm arsenic; and 4.5 metres averaging 103 ppb gold, 5.1 ppm silver, 540 ppm arsenic. Lead and zinc values were generally anomalous throughout the entire zone. Anomalous arsenic values seem to coincide with the higher gold and silver values.

Gold, silver, lead, zinc, silver, and arsenic anomalies seem to occur along the sheared and altered contact between the andesite dyke and tectonic breccia. The shearing, silica flooding and vuggy texture displayed in this zone are characteristic of epithermal systems. Zone C occurs along the North Trout Creek fault structure (see Figure 4) which possibly provided channels for mineralizing fluids or a structural trap for deposit formation.

This zone warrants further testing due to the anomalous geochemistry. Therefore, a short drill program is warranted to try and determine the extent of the structure and test for ore grade mineralization.

### 6.2.2 Zone N2

This alteration zone occurs over a seven metre length across a contact between the Unit 1, a highly clay altered porphyritic quartz-feldspar monzonite and the Unit 3, porphyritic rhyodacite (Figure 8). The zone is located along a talus slope in the North Trout Creek canyon (see Figure 6). The contact is sheared and intensely clay altered with narrow shear zones of soft blue clay. Limonite and pyrolusite staining occur throughout this zone. The quartz-feldspar porphyry displays patches of disseminated pyrite. The porphyritic rhyodacite is fractured, sheared, moderately chloritized and carbonatized with minor amounts of disseminated pyrite and magnetite. Petrographic examination of this unit showed it to be cut and replaced by veins of quartz (plus opaque minerals) and replacement patches of pyrite and sericite.

Chip sampling of a blue clay alteration zone over 1.5 metres detected 10 ppm silver and 710 ppm lead. A 1.5 metre vertical intersection near the contact averaged 3.9 ppm silver and 155 ppm arsenic. No geochemical gold anomalies were determined.

Silver and arsenic anomalies seem to occur on and/or near the sheared and clay altered contact zone between the two units. Anomalous arsenic values seem to coincide with anomalous silver and elevated gold values. Zone N2 also occurs in close proximity to the North Trout Creek and Trout Creek fault structures. Due to low level metal values, Zone N2 should be assigned a lower priority for follow-up.

# LEGEND

| 42832 |

CHIP SAMPLING INTERVAL

△ L. 0+90E  
1+50N

SAMPLING CONTROL STATION



GROUND SURFACE



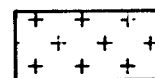
GEOLOGICAL CONTACT (KNOWN, INFERRED)



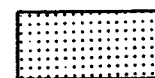
FAULT GOUGE



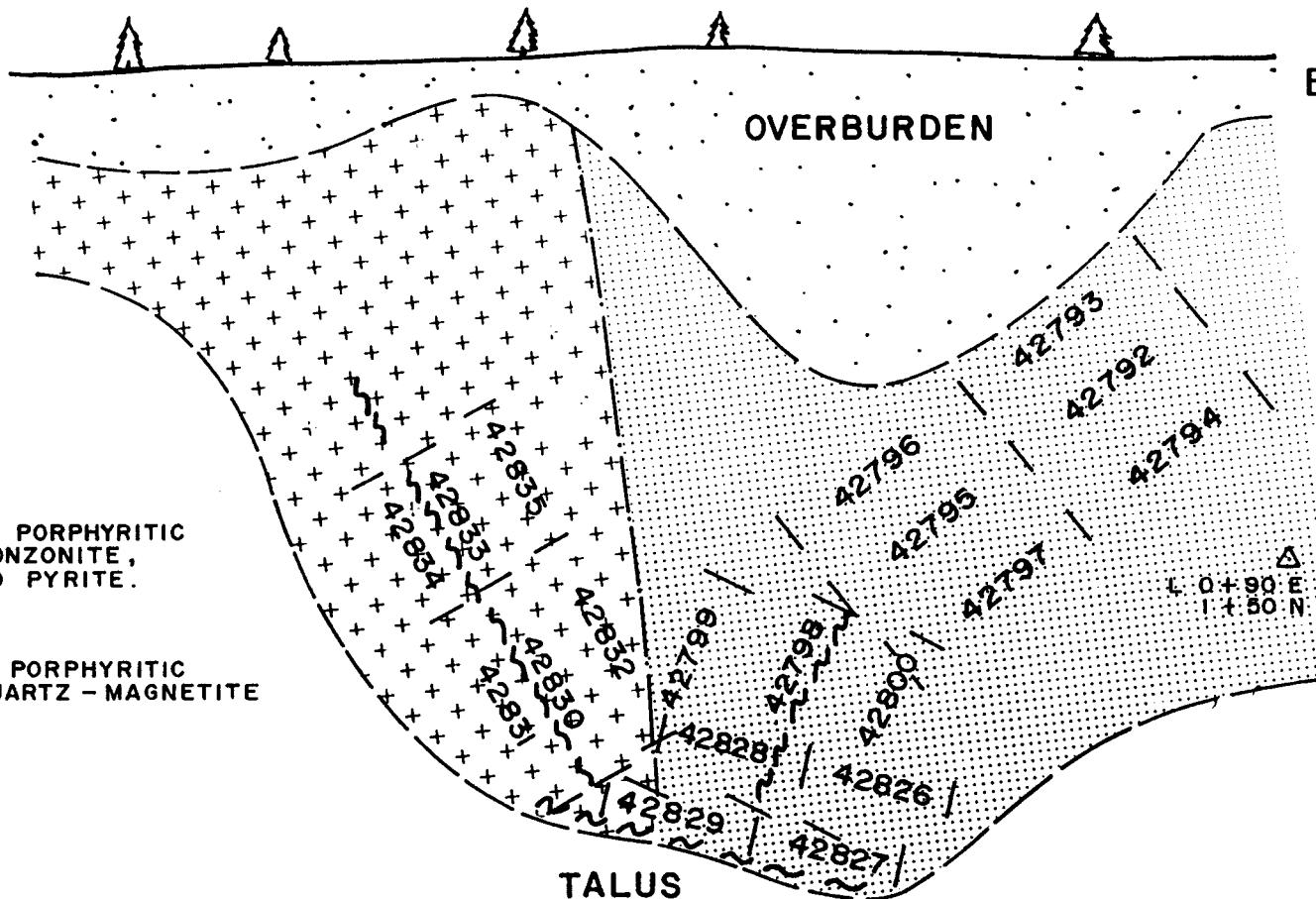
OUTCROP BOUNDARY



HIGHLY CLAY ALTERED PORPHYRITIC QUARTZ-FELDSPAR MONZONITE, 2-3% DISSEMINATED PYRITE.



SHEARED & ALTERED PORPHYRITIC RHYODACITE WITH QUARTZ-MAGNETITE STOCKWORK.



( CROSS - SECTIONAL VIEW )

SPRING PROJECT - ZONE N2

1989 GEOCHEM RESULTS

Samp	Qi (ppm)	Fb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	As (ppm)	Sb (ppm)
42792	27	56	367	1.0	15	1	1.0
42793	28	126	265	.8	3	38	1.0
42793	29	133	272	.8	3	38	1.0
42794	18	45	302	.9	10	23	1.0
42795	24	40	332	.9	3	24	1.0
42796	24	37	292	.5	3	21	1.0
42797	15	16	246	.4	3	6	1.0
42798	23	100	150	4.0	3	152	1.0
42799	23	75	207	4.3	3	162	1.0
42800	17	60	107	3.5	10	150	1.0
42826	27	68	92	2.9	55	113	1.0
42827	12	28	97	1.1	20	78	1.0
42828	9	50	64	2.0	15	78	1.0
42829	14	55	43	2.7	15	150	2.0
42829	14	55	46	2.8	10	155	2.0
42830	9	710	98	10.0	10	51	1.0
42831	10	41	92	2.5	3	19	1.0
42832	16	106	158	5.3	20	124	1.0
42833	22	157	120	4.1	10	20	1.0
42834	25	95	200	1.0	3	8	1.0
42835	10	118	61	4.8	10	155	1.0

PLACER DOME INC.

SPRING PROJECT '89  
V - 232

Sampling Zone N2

FIGURE NO. 8

NORTH TROUT CREEK TRAIL 2

### 6.2.3 Zone P4

Zone P4 consists of an exposure of the Unit 4 tectonic breccia (Figure 9). The brecciated texture is characterized by well rounded fragments of quartz-feldspar porphyry and porphyritic rhyodacite set in a matrix of similar composition. The breccia displays a moderate degree of sericite alteration and a high level of weathering in the form of heavy pyrolusite and limonite staining. Up to 5% disseminated pyrite was present throughout most of the zone. Zone P4 displays a narrow (less than 1.0 metre wide) highly clay altered shear zone trending 070 degrees. The zone is located along a road-cut above North Trout Creek in the Spring 3 claim (see Figure 6).

Lead and zinc values are elevated throughout the zone but not highly anomalous. A 1.5 metre vertical intersection averaged 2.7 ppm silver and 449 ppm lead. A 1.5 metre interval detected 1010 ppm zinc. A 1.5 metre interval returned 6.0 ppm antimony. No significant gold values were detected.

The tectonic breccia may have been related to a structural event due to it's close proximity to the North Trout Creek and Trout Creek fault structures. Generally metal values were low in this zone, therefore, no immediate follow-up is recommended.

# LEGEND

| 42832 |

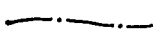
CHIP SAMPLING INTERVAL

△ L. 0+90E  
1+50N

SAMPLING CONTROL STATION



GROUND SURFACE



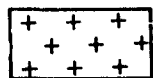
GEOLOGICAL CONTACT (KNOWN, INFERRED)



FAULT GOUGE



OUTCROP BOUNDARY

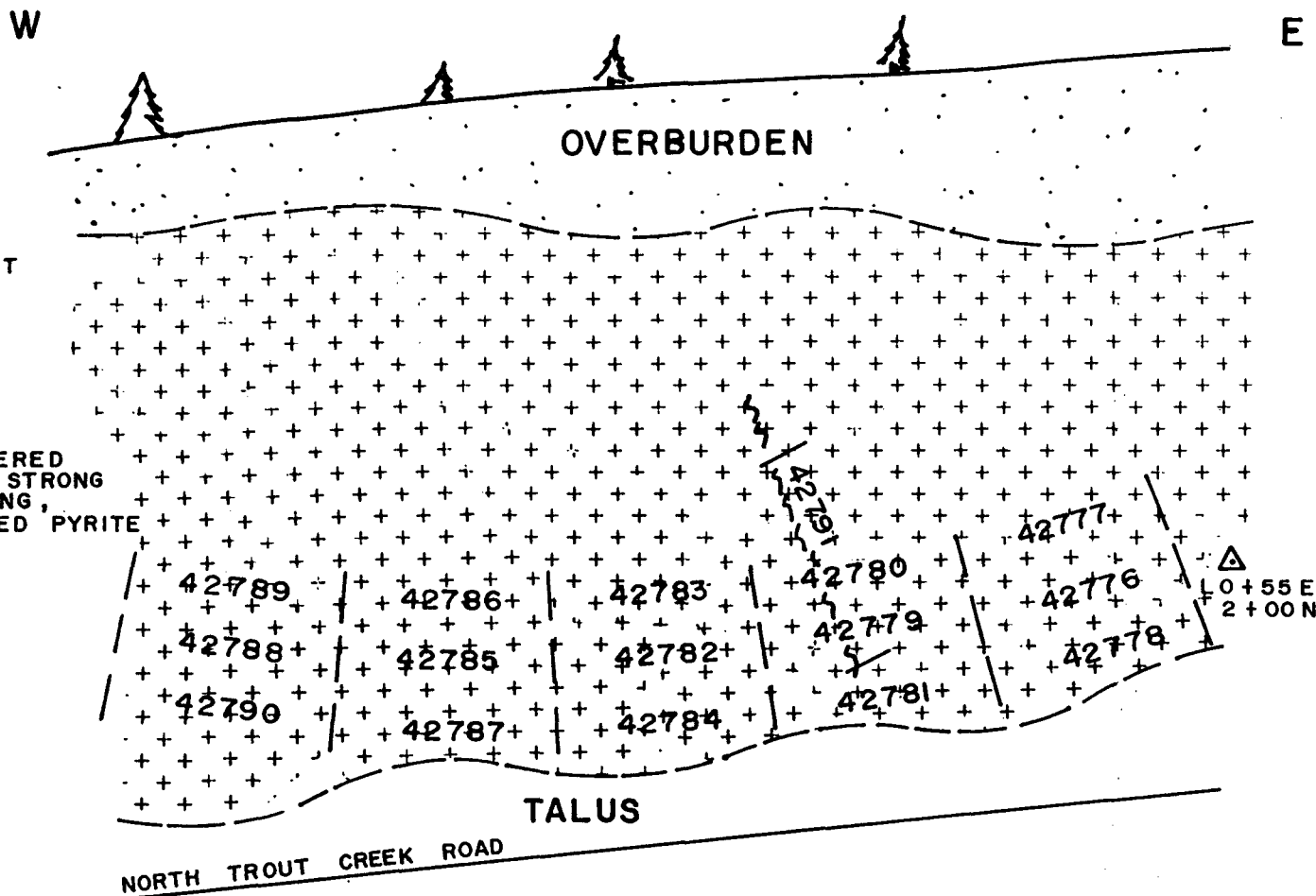


ALTERED & WEATHERED TECTONIC BRECCIA, STRONG PYROLUSITE STAINING, ± 5% DISSEMINATED PYRITE

0.5 0 1m 2m



BAR SCALE : 1 : 50



PLACER DOME INC.

SPRING PROJECT '89  
V - 232

Sampling Zone P4

FIGURE NO. 9

(CROSS SECTIONAL VIEW)

SPRING PROJECT - ZONE P4

1989 ROCK GEOCHEM RESULTS

Sampl	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	As (ppm)	Sb (ppm)
42776	12	328	119	1.9	3	12	6.0
42777	11	251	113	1.5	3	10	1.0
42778	12	297	103	1.3	3	15	1.0
42779	13	313	323	1.5	3	12	1.0
42780	13	265	166	1.5	3	17	1.0
42781	10	166	240	1.3	3	20	1.0
42782	20	234	610	1.3	3	5	1.0
42783	26	298	322	1.8	3	5	1.0
42784	17	283	700	1.6	3	15	1.0
42784	14	240	600	1.3	3	7	1.0
42785	30	307	550	1.5	3	9	1.0
42786	30	313	340	2.7	3	7	1.0
42787	25	260	1010	1.7	3	18	1.0
42788	35	190	253	2.6	3	19	1.0
42789	22	580	203	2.4	3	18	1.0
42790	43	378	293	3.2	3	23	1.0
42791	17	550	177	1.0	3	24	1.0

### 6.3 Trench Descriptions and Results

The following is a brief description of each trench and a summary of the geochemical results. In the Zone 2 Area, six north-south trenches tested an 800 metre by 500 metre gold-in-soil anomaly with an associated moderate IP response. Four north-south trenches were excavated in the Zone 4 Area to test a 700 metre by 250 metre multi-element soil anomaly trending 110 degrees. In the North Trout Creek Area, a 1000 metre by 200 metre north-south trending multi-element soil anomaly was cut by seven east-west trenches. In the East Zone Area, two trenches, 200 metres apart, tested a 500 metre long gold-in-soil anomaly trending north-east.

The trenching program was sometimes plagued by problems with relatively thick overburden. Many areas which were targeted by soil geochemistry, geophysics, or geology could not be adequately tested. A practical limit to the overburden thickness which can be effectively trenched is approximately 5.0 metres. Past this limit, the cost of excavating a trench to safe standards exceeds the cost of drill testing. Many of the trenches were prematurely terminated because of deep overburden. A total of 49 test pits were dug to depths of approximately 8.0 metres, as bedrock was never reached in these target areas.

#### Zone 2 Area

##### 6.3.1 Trench 785E

This trench was excavated to test the source of an IP anomaly between 550N and 560N. It exposed gently, south sloping bedrock of the Unit 1 porphyritic quartz-feldspar monzonite (see Figure 10). The rock is partially silicified and moderately clay altered. A narrow (less than 1.0 metre wide) shear zone, striking at 020 degrees, displays intense blue clay alteration. Up to 8.0% disseminated pyrite occurs throughout the trench with selected grab samples displaying up to 20% pyrite. Deep weathering, up to 50 centimetres in depth, is displayed as prominent limonite and pyrolusite staining. This trench was discontinued due to the proximity of the creek at 650N.

Chip sampling determined some anomalous silver values and weak gold, lead, and zinc values. A weak antimony anomaly averaging 1.5 ppm was detected over 9.0 meters in highly silicified and rusty quartz-feldspar porphyry. One sample along an intensely clay altered shear zone was found to contain 8.2 ppm silver,

393 ppm lead, and 668 ppm zinc over 1.5 meters. Un-sampled intervals were due to overburden in-filling the irregular bedrock surface.

Overburden profile sampling returned sporadic metal values. Values of 0.7 ppm silver and 125 ppb lead were detected at 675N on the bedrock interface in proximity of an intensely clay altered fault gouge.

### 6.3.2 Trench 825E

This trench tests the source of an IP anomaly which is interpreted as projecting through the south end of the trench. The trench exposes a sericite altered and silicified Unit 1 (porphyritic quartz-feldspar porphyry) intermixed with an eight metre zone of biotite-quartz monzonite (mapped as Unit 2), displaying moderate chloritic alteration (see Figure 10). Limonite and pyrolusite staining are prominent. Pyrite occurs as disseminations and fracture fillings up to 20% in the porphyry unit and only in minor disseminated amounts in the biotite quartz monzonite. Excavation was discontinued as bedrock could not be reached through thickening overburden.

Chip sampling determined very high zinc values throughout the trench, with some anomalous silver and weak lead values coming from the quartz-feldspar porphyry. A high zinc anomaly averaging 1252 ppm was detected over 12 meters and three continuous chip samples averaged 1.9 ppm silver, 256 ppm lead, 1463 ppm zinc over 4.5 metres, all in highly altered and weathered quartz-feldspar porphyry.

### 6.3.3 Trench 842E

This trench was excavated to test a 100 metre long IP anomaly. The exposed bedrock consists entirely of the Unit 1 porphyritic quartz-feldspar monzonite, moderately to highly silicified with high levels of sericite alteration (see Figure 10). The north end of the trench displays weathering as heavy limonite staining. The south end shows more prominent feldspar phenocrysts (up to 20%). Numerous narrow (less than 1.0 metre wide) intensely clay altered shear zones occur throughout the trench and trend 035, 040 and 090 degrees, dipping steeply. Mineralization occurs as disseminated and boxwork pyrite from 5 to 10% in selected grab samples. This trench was discontinued due to thick overburden.



Chip sampling detected stronger silver, lead, and zinc values over 12 metres as well as along four separate narrow shear zones all occurring in a more silicified, sericitic and rusty quartz-feldspar porphyry. Precious and base metal values were not anomalous.

#### 6.3.4 Trench 858E

This trench was dug to trace a prominent alteration zone projecting from the north end of trench 842E, and also to test a gold-in-soil anomaly. The trench exposed south dipping bedrock of the Unit 1 porphyritic quartz-feldspar monzonite (see Figure 10). The rock is generally highly silicified with moderate argillic and sericite alteration and minor chloritization. Bedrock is mineralized with up to 3% disseminated pyrite. Weathering is displayed as heavy limonite staining throughout the trench. Irregular bedrock surface in-filled with overburden caused some interruptions with mapping and sampling. The trench was discontinued due to thick overburden.

Chip sampling determined stronger lead and zinc values to the north end of the trench in highly silicified and rusty quartz-feldspar porphyry. No significant metal values were detected.

#### 6.3.5 Trench 1388E

This trench tested the source of a gold-in-soil anomaly over 125 metres long, associated with a weak IP response. The exposed bedrock consists of weakly altered, locally fractured porphyritic quartz-feldspar monzonite (Unit 1). The north end of the trench displays a higher degree of weathering and sericite alteration. Three separate shear zones, up to 1.0 metre wide, of intense clay alteration occur in the north half of the trench (see Figure 11). Minor disseminated pyrite is present. Sericite alteration is moderate but increases at the south end of the trench. Changes in fracturing and alteration are subtle and marked by deep weathering surfaces. This trench was discontinued as it joined with the collar of trench 1393E.

Chip sampling produced some low-level anomalous lead and zinc values from the north half of the trench, but weak gold, silver values. One chip sample at the

northern extremity of the trench returned values of 3.4 ppm silver , 989 ppm lead, 2.6 ppm antimony from a silicified and weathered quartz-feldspar porphyry. A 1.5 metre sample across an intensely clay altered shear zone detected a weak anomaly of 400 ppm zinc.

Overburden profile sampling determined low-level metal values throughout the trench. A value of 50 ppb gold was detected at 750N in the till overlying the bedrock. This reflects the multi-element anomaly at this location.

#### 6.3.6 Trench 1393E

This trench was dug to test a 100 metre long gold-in-soil anomalous trend. The exposure consists of the Unit 1 porphyritic quartz-feldspar monzonite (see Figure 11). Alteration is dominated by high levels of pervasive and fracture filling silicification with some moderate sericitization. Weathering is displayed as moderate limonite and pyrolusite staining. Minor disseminated pyrite occurs throughout the trench. The trench was discontinued due to thick oberburden.

Chip sampling determined low-level base metal values. One anomalous gold value of 70 ppb over 1.5 metres occurred in a highly altered and weathered quartz-feldspar porphyry.

#### Zone 4 Area

#### 6.3.7 Trench 1010W

This trench was dug to test the source of a 100 metre linear gold-in-soil anomalous trend. Trenching exposed undulating bedrock consisting of intermixed Unit 1, porphyritic quartz-feldspar monzonite, and Unit 2, biotite-hornblende quartz diorite (see Figure 12).

The north end of the trench displays fresh looking, coarse-grained quartz-feldspar porphyry. This rock grades into a highly weathered, moderately silicified and sericitized equigranular quartz diorite with a stockwork of silica and minor disseminated pyrite. This zone located at the 21 to 28 metre interval, is marked by an obvious two metre wide shear zone, striking at 034 degrees which is intensely clay altered and limonite stained.

The central zone of the trench is characterized by a band of moderately fractured and silicified quartz-feldspar porphyry grading back into a slightly weathered quartz diorite with weak sericite and chlorite alteration. This area displays multiple narrow (less than 2.0 metre wide) shear zones, moderately to highly clay altered, and trend 060 and 085 degrees. Minor amounts of disseminated pyrite occur throughout this zone.

The southern end of the trench consists of a fresh looking, equigranular quartz diorite, weakly fractured and with traces of pyrite. This trench was discontinued due to the limit of the anomalous soil geochemical trend.

Chip sampling determined some anomalous gold, silver, zinc with weak copper values in a highly clay altered shear zone of the quartz diorite in the 21 to 28 metre interval. Averages of 3.8 ppm silver and 422 ppm zinc over 6.0 metres were detected. The southern extremity of the alteration zone returned an 80 ppb gold value over 1.5 metres. Within this zone, a 1.5 metre chip sample across a clay altered shear zone yielded 300 ppb gold and 2.2 ppm silver.

A separate shear zone at the 43 metre interval detected anomalous gold, silver, and zinc values, 40 ppb gold, 1.3 ppm silver, and 758 ppm zinc over 1.5 metres.

Overburden profile sampling detected anomalous silver values at the bedrock interface throughout the trench. Higher silver values were located at the north end of the trench, reflecting the altered shear zone at the 25 metre interval. Lead values display a similar pattern as silver.

#### 6.3.8 Trench 1335W

This trench was excavated to test the source of a 300 metre long multi-element soil anomaly. The exposed bedrock consisted mainly of Unit 1 porphyritic quartz-feldspar monzonite, highly silicified, partially sericitized with limonite and pyrolusite staining. Silicification increases to the south (see Figure 13). Mineralization occurs as minor disseminated pyrite. The last three metres of the trench consists of Unit 2 quartz diorite, highly silicified, with minor limonite and pyrolusite staining. This trench was ended due to the limit of the soil geochemical anomaly.

Chip sampling determined elevated silver, copper, lead, and zinc values to the south end of the trench, but they still are not considered highly anomalous.

Overburden profile sampling showed a weak lead anomaly in the C horizon at a 200 centimetre depth. The anomaly displays a dispersion over a 25 metre length to the south.

#### 6.3.9 Trench 1378W

This trench was excavated to test the northern extremity of the same multi-element soil anomaly tested by trench 1335W. Trenching exposed bedrock consisting of Unit 2 quartz diorite to the north and Unit 1 porphyritic quartz-feldspar monzonite to the south (see Figure 13). The quartz diorite displays high silicification and moderate chloritization with minor amounts of disseminated pyrite. Fracturing is more prominent in the 10 to 14 metre interval. The quartz-feldspar porphyry unit is highly silicified and moderately sericitized. Limonite and pyrolusite staining are moderate and disseminated pyrite occurs up to 3%. Irregular bedrock surfaces infilled with overburden throughout the trench caused unsampled intervals. The trench was discontinued at a road crossing.

Chip sampling determined mostly low-level anomalous gold, silver, lead, and zinc values throughout the trench. Lead, zinc, and arsenic values were elevated in the central zone of the trench, over 18 metres, across the contact of the two rock units. One chip sample yielded anomalous silver, 2.8 ppm silver over 1.5 metres and a cross-cutting silicified fracture in the same interval returned 2.1 ppm silver over 1.5 metres. A low-level gold anomaly averaged 30 ppm over 5.5 metres in the altered quartz-feldspar porphyry.

Overburden profile sampling showed weak anomalous silver and lead values at the bedrock interface throughout the trench. Higher values occur in the central area, of the trench over a 20 metre interval. This anomaly is clearly related to the underlying anomalous bedrock.

### 6.3.10 Trench 1565W

This trench tests a 300 metre long multi-element soil anomaly. The exposed bedrock can be summarized simply as intermixed zones of Unit 1 quartz-feldspar porphyry (monzonite) and Unit 2 quartz diorite (see Figure 14). Both units seem to have similar alteration patterns displayed by varying levels of sericitization and silicification. Up to 3% disseminated pyrite was noted in the porphyry unit. Moderate to high levels of limonite and pyrolusite staining are prominent in the central zone of the trench while the southern and northern extremities display fresher rock.

Numerous narrow (less than 1.5 metre wide) shear zones of intense whitish clay alteration occur throughout the trench, and trend 045, 060, 070, 095, or 110 degrees. The shear zones often display varying intensities of fracturing and sometimes occur along or nearby a contact zone between the two host rocks. A five centimetre wide quartz vein trending 135 degrees occurs in sericite altered quartz diorite. This trench ends due to the limit of the anomalous soil geochemical trend.

Chip sampling determined sporadic low-level gold, silver, lead, and zinc anomalies. Two separate chip samples in the proximity of shear zones, yielded anomalous values of 50 ppb gold, 1.0 ppm silver, 700 ppm zinc, and 5.2 ppm silver, respectively.

The interval between 158 and 220 metres displayed some very high lead values and some anomalous gold, silver, and zinc values across shear zones of intense clay alteration. Three separate 1.5 metre chip samples in these shears detected 100 ppm lead, 580 ppm zinc in rusty quartz-feldspar porphyry, 90 ppb gold, and 1200 ppm lead in sericite altered and rusty quartz diorite, respectively.

Overburden profile sampling detected stronger silver, gold, and lead values to the north and dispersing down-slope to the south over 100 metres. One B2-horizon sample, highly anomalous in gold yielded 400 ppb gold at 765N; overlying moderately fractured and silicified quartz-feldspar porphyry.

## North Trout Creek Area

### 6.3.11 Trench 001E

This trench was excavated to test the Main alteration zone discovered during a previous drilling program by Golden Pick Resources. Trenching exposed a highly clay altered and weathered Unit 1, quartz-feldspar porphyry (see Figure 15). Silicification is minor and weathering is displayed as strong limonite and pyrolusite staining. Numerous narrow (less than 2.0 metre wide) shear zones of intensely rusty clay alteration occur throughout the trench and trend 040, 075, 085, or 105 degrees. Mineralization occurs as disseminated pyrite up to 3%. This trench was discontinued due to flooding of water.

Some very high lead, elevated zinc, and very high antimony (north end) values, with weaker silver and copper values, were detected in the chip sampling. Two separate 1.5 metre chip samples yielded values of 1.4 ppm silver, 574 zinc, 4.7 ppm antimony and 1800 ppm lead, 382 ppm zinc, and 7.3 ppm antimony respectively. Both occurred in highly clay altered quartz-feldspar porphyry.

Shear zones yielded anomalous silver and zinc and weaker copper values with associated elevated antimony values. A 1.5 metre sample detected anomalous values of 6.1 ppm silver 394 ppm lead, and 725 ppm zinc.

Overburden profile sampling at the bedrock interface (1 metre depth) determined a very high lead and zinc anomalies 30 metres from the trench collar with values of 640 ppm lead and 4200 ppm zinc. These values reflect the anomalous lead and zinc values occurring in the bedrock where clay alteration is intense.

### 6.3.12 Trench 170W

This trench was excavated to test the sources of a gold-in-soil and previously detected IP anomalies. The exposed bedrock consists of Unit 1 porphyritic quartz-feldspar monzonite (see Figure 16). Silicification is strong with moderate sericite alteration, moderate fracturing and some limonite staining. One 8.0 centimetre wide shear zone of intense clay alteration occurs at the 2.9 metre interval and trends 120 degrees. This trench was interrupted due to a road crossing.

Chip sampling determined one weak silver value of 1.4 ppm silver over 1.5 metres. Lead and zinc values seem stronger to the east of the trench but not anomalous. One chip sample along an eight centimetre

zone cross-cutting the above silver anomaly, returned values of 35 ppb gold, 1.7 ppm silver, and 403 ppm lead.

Overburden profile sampling at the trench collar detected a 620 ppm zinc value at a 10 centimetre depth and a 104 ppm lead value at the bedrock interface. These low-level anomalous values possibly originate from the nearby clay altered shear zone.

#### 6.3.13 Trench 265N

This trench is an extension of trench 170W, testing soil geochemical and IP anomalies. Trench 265N consists of Unit 1, porphyritic quartz-feldspar monzonite (see Figure 16). Alteration is displayed as high silicification and minor sericitization. Weathering occurs as moderate limonite with less pyrolusite staining. Minor disseminated pyrite occurs throughout the trench. The trench was ended due to thick overburden.

Chip sampling determined higher silver, lead, and zinc values occurring towards the east end of the trench.

Overburden profile sampling detected elevated zinc values and weak gold values in the B horizon and at the bedrock interface. The source of these elevated values is not the immediate underlying bedrock.

#### 6.3.14 Trench 837N

This trench was excavated to test the source of a multi-element soil anomaly. It consists of Unit 1 porphyritic quartz-feldspar monzonite; deeply weathered to the west end with limonite and pyrolusite staining and strongly fractured (see Figure 17). Alteration occurs as high levels of silicification and sericitization. Mineralization consists of up to 10% pyrite, occurring as blebs, disseminations and microveins. The porphyry unit becomes less altered to the east end. A couple of narrow (less than 1.0 metre wide) shear zones of intense clay alteration are present and trend 020 degrees.

Chip sampling determined higher zinc values, but they are not considered anomalous. A 1.5 metre chip sample along a clay altered shear zone showed values of 1.9 ppm silver and 449 ppm zinc.

#### 6.3.15 Trench 847N

This trench is an extension of trench 837N and tests multi-element soil anomalies. The Unit 1, quartz-feldspar porphyry (monzonite) is the dominant rock type and displays deep weathering and high levels of alteration (see Figure 17). Silicification and limonite staining are prominent and up to 10% disseminated pyrite occurs throughout the trench. A small, two centimetre wide lens of galena occurs at the 27 metre interval, reflected by a highly anomalous lead value of 3000 ppm. This trench was discontinued due to thick overburden.

Chip sampling determined very anomalous silver, lead, zinc, and weaker copper values at the east end of the trench. A 6.5 metre interval averaged 3.3 ppm silver, 715 ppm lead, and 1757 ppm zinc in a highly altered and weathered quartz-feldspar porphyry.

Overburden profile sampling throughout both trenches 837N and 847N determined very anomalous zinc and lead and weak gold and silver values coming from both the B horizon and the bedrock interface. These values reflect the intensely altered anomalous zone at the eastern end of the trench as well as other possible sources further up-slope.

#### 6.3.16 Trench 930N

This short trench exposed bedrock of the Unit 1 porphyritic quartz-feldspar monzonite (see Figure 18). Silicification is high and sericite alteration is moderate. Weathering is displayed as heavy hematite staining and disseminated pyrite occurs in minor amounts throughout the trench. One narrow (less than 1.0 metre wide) fault gouge of extreme clay alteration occurs in the central zone and displays an intense fracture set. The trench was discontinued due to deep overburden.

Chip sampling determined anomalous zinc values at the western extremity of the trench averaging 900 ppm zinc over 4.5 metres.



Overburden profile sampling the C-horizon at the bedrock interface detected two highly anomalous zinc values reflecting the anomalous zinc values observed in the chip sampling.

#### 6.3.17 Trench 969N

This trench was excavated to test the source of a multi-element soil anomaly, and the projection of intense alteration zones exposed along a nearby road-cut. The exposure consists of Unit 1 porphyritic quartz-feldspar monzonite (see Figure 18). Alteration displays moderate to high levels of silicification and sericitization. Weathering, displayed as hematite and limonite staining seems to increase towards the east end of the trench as does the intensity of fracturing. Mineralization occurs as minor disseminated fine grained pyrite throughout the trench. Several highly clay altered and cross-cutting shear zones occur at the eastern end. This trench was ended at a road crossing.

Chip sampling detected one weak silver value of 1.3 ppm over 1.5 metres in clay altered microveins in an extremely weathered quartz-feldspar porphyry. All other metal values were non-significant.

Overburden profile sampling determined highly anomalous lead and zinc and weaker gold and silver values in the B and C horizons throughout the trench. The lack of anomalous metal values in the bedrock chip sampling suggests the source is further up-slope, or the anomaly has been transported either glacially or hydromorphically.

#### East Zone Area

#### 6.3.18 Trench 3228E

This trench was excavated to test a northeast trending gold-in-soil anomaly. The exposed bedrock is undulating and consists mainly of Unit 7a quartz-biotite gneiss with a two metre exposure of Unit 6, granite pegmatite (see Figure 19). The gneiss displays moderate foliation, some fracturing over a two metre zone, a coarse-grained texture and weak alteration. Mineralization occurs as minor disseminated pyrite. The granite is rather fresh looking. Hornfelsed textures are observed near the contact zones of the two rock units. Two narrow (less than 1.0 metre) shear

zones of intense clay alteration with associated fracturing occur in the gneiss. The trench was ended as it covered the extent of the soil anomaly.

Chip sampling determined no significant metal values except for a very weak copper anomaly (76 ppm copper over 1.5 metres). Background antimony levels are much higher in the biotite gneiss.

#### 6.3.19 Trench 3427E

This trench was dug to test the source of a gold-in-soil anomaly trending in a northeast direction. The exposure consists of undulating bedrock of Unit 7a quartz-biotite gneiss (see Figure 20). The gneiss is moderately foliated and silicified, with some weathering displayed by stronger limonite staining. Mineralization occurs as minor disseminated pyrite throughout this unit. A 10 metre section in the central portion of the trench exposes a fresh, coarse-grained granite (Unit 6). One narrow (less than 1.0 metre) clay altered fault gouge zone occurs in the gneiss at the top of the trench. The trench was interrupted at a road crossing and was continued an additional 15 metres to cover the extent of the soil anomaly.

Chip sampling determined anomalous gold, silver, copper, zinc, and arsenic values at the north end of the trench along or near the clay altered shear zone. Copper values are anomalous and average 380 ppm copper over 7.6 metres. Zinc and arsenic values are stronger but not anomalous. The antimony levels again are higher in the gneiss unit. A 1.5 metre sample along the shear zone detected 20 ppb gold, 1.0 ppm silver, 711 ppm copper, 350 ppm zinc, and 41 ppm arsenic.

#### 6.4 Interpretation of Trenching Results

Gold, silver, lead, and zinc anomalies all seem to occur within highly altered and weathered porphyritic quartz-feldspar monzonite (Unit 1) or in intensely argillic altered shear structures. These shear zones also seem to be associated with an increase in fracture intensity.

In the Zone 2 area, the high concentrations of disseminated pyrite would likely be sufficient to explain portions of the IP anomaly. Anomalous metal concentrations in the Zone 4 and North Trout Creek areas, detected along or near altered shear zones, is sufficient to explain the

observed soil anomalies. The trend of several of these structures reflect the regional structural trends.

In the East Zone area, anomalous concentrations of copper are associated with highly altered zones within a quartz-biotite gneiss (Unit 7a). This rock unit also carries more elevated antimony values. Both Zones 2 and 4 and the East Zone areas occur in close proximity to the Trout Creek fault (see Figure 4) possibly suggesting some regional structural control to the anomalous metal concentrations.

The North Trout Creek area trenches showed anomalous concentrations of lead, zinc, and silver but gold values were non-significant. The anomalous zones lie in close proximity to the North Trout Creek fault, again possibly suggesting some regional structural control.

Overburden profile sampling determined some anomalous metal values predominantly at the overburden-bedrock interface. However, results were sporadic and often scattered. Overburden profile sampling often did not reflect the values observed in chip sampling the bedrock. This demonstrates that in-situ rock anomalies will not necessarily be reflected in the overlying overburden or soil. Therefore, the source of soil anomalies cannot readily be considered in-situ.

## 7.0 SOIL GEOCHEMISTRY

### 7.1 Results

Statistical analysis of the combined 1988 and 1989 soil metal values was undertaken to determine threshold levels. These levels can be applied to separate the anomalous, if present, population from the background values. The following thresholds were determined; gold 20 ppb, copper 65 ppm, zinc 600 ppm, lead 60 ppm, and silver 1.0 ppm (see Appendix VII).

In general terms, gold and copper appear to behave quite independently, while zinc, lead and silver have a much higher degree of correlation.

The fill-in soil sampling over areas of previous gold-in-soil anomalies, determined that results are suspect in areas of thick glacial till and/or thick deposits of colluvium or alluvium. This can best be seen in the Zone 2 area in relation to gold-in-soil anomalies. Here fill-in soil sampling at 50 and 100 metre line spacings failed to confirm the previously inferred anomalous trends (see Figure

21). Line 14+00 East was also re-sampled from 5+00 to 11+00 North over a previous anomalous segment and gold anomalous values failed to be repeated. Other anomalous gold trends which were unconfirmed include the Zone 4 and the East Zone areas.

Gold values range from less than the detection limit of 5.0 ppb to a maximum of 770 ppb. Approximately 90% of the samples returned values less than the detection limit, and approximately 565 samples had values in excess of the 20 ppb threshold level. The anomalous gold values define approximately twelve narrow trends and several single station "spot" anomalies (see Figure 21). The most significant in terms of length and magnitude, is the trend on line 1+00 West between 1+00 and 6+00 North. Other significant trends defined include: between lines 7+00 and 13+00 East at approximately 10+00 South and between lines 4+00 and 6+00 East at approximately 7+50 North.

The gold anomalies on the western portion of the grid tend to be peripheral to the anomalous patterns displayed by zinc and lead.

Copper values ranged from 2.0 to 333 ppm. Approximately 100 samples had values in excess of the 65 ppm threshold level. These samples define a few small areas and narrow trends as well as one station wide, multi-line anomalous trends as shown on Figure 22. The most significant of these in terms of size and magnitude, are two small areas crossing from line 13+00 to 1500 East, one centered on 9+00 North and the other centered on 3+50 North both covering approximately 200 square metre areas. The northernmost anomaly seems to project east into a narrow (one station wide) trend to line 18+00 East at 11+00 North, and the same trend continues from lines 23+63 to 27+92 East. A few other single-station "spot" anomalies were determined, as shown on Figure 22.

Zinc values range from 4.0 to 9800 ppm. Approximately 220 samples had values in excess of the 600 ppm threshold. These anomalous values generally define a large area in the southwest portion of the grid (see Figure 23). This pattern is even more striking when the above 300 ppm zinc values are considered. It is difficult to define more precise, higher order, anomalous trends within this large anomalous area. Other anomalous areas are also defined at the southern end of lines 0+00 to 10+00 East, and between lines 23+63 and 27+92 East at approximately 6+00 North.

Lead values range from 1.0 to 650 ppm. Approximately 170 samples had values in excess of the 60 ppm threshold level. These samples generally define an area in the

southwest portion of the grid, similar to the zinc pattern, but smaller in extent (see Figure 24). The anomalous zone is better-defined if the greater than 30 ppm values are considered. A southeast/northwest anomalous trend is defined from lines 6+00 to 10+00 West, approximately centred at 27+00 North. Anomalous areas are also defined; between lines 16+00 to 18+00 East from 0+00 to 5+00 North, and a very irregular area extending from lines 23+63 to 36+47 East centred around the baseline.

Silver values range from less than the detection limit of 0.2 ppm to a maximum of 14 ppm. Approximately 55 % of the samples returned values below the detection limit, and approximately 150 samples had values in excess of the 1.0 ppm threshold level. The anomalous samples are generally restricted to the southwest portion of the grid, similar to the pattern displayed by lead (see Figure 25), except that narrower trends are defined.

## 7.2 Interpretation

Anomalous metal values were defined, and they demonstrate trends and/or anomalous areas as shown on Figures 21 through 25. These Figures can be overlain on Figures 3, 4, and 5 to reference geology, line numbers, topography, streams, and claim boundaries.

Unfortunately, the fill-in soil sampling over areas of previous gold-in-soil anomalies, particularly Zone 2, Zone 4 and the East Zone, failed to confirm the previously inferred anomalous trends (Pease, R.B., 1989). This erratic behaviour of anomalous gold values is likely due to thick glacial overburden and/or glacial transport from a distant source. Zone 2 in particular displays increased thicknesses of glacial till revealed by the numerous test pits excavated in this area as well as the low resistivities detected by the IP survey. Therefore, anomalous metal values should be considered suspect in areas of thick overburden.

Gold anomalies could all be considered suspect in light of the fill-in soil sampling results. Chip sampling in the trenches of Zone 2, Zone 4 and the North Trout Creek areas failed to detect any significant gold values. This does not correlate with the observed soil anomalies. However, in the Zone 4 area, the IP survey revealed an increase in resistivity values reflecting a general thinning of the overburden as compared to Zone 2. Sampling in trench 1010W detected elevated gold values associated with an altered shear zone which is likely sufficient to explain the observed "spot" soil anomaly in this area. Although the

three other trenches in Zone 4 yielded scattered low-level anomalous gold values of up to 50 ppb gold, these results were insufficient to explain the overlying gold-in-soil anomalies. Therefore, other anomalous gold trends inferred from the soil survey should be considered suspect and do not warrant direct follow-up.

The anomalies displayed by copper in the Zone 2 area may also be considered suspect, although fill-in soil sampling did confirm two small anomalous areas centered on line 14+00 East. The anomalous area at 9+00 North does seem to correlate with the previous northeasterly trend projecting through to line 18+00 East. However, in the East Zone area, soil geochemical copper values weakly reflected the anomalous copper values detected in trench 3427E of up to 870 ppm copper. One small discrete copper anomaly between lines 9+00 and 10+00 East just south of the baseline does seem to correlate with a weak IP anomaly, but overburden is likely thick in this area.

The patterns displayed by lead, zinc, and silver all define relatively large areas of anomalous soils in the southwest portion of the grid where overburden cover is interpreted to be thinnest. This is very likely due to relatively low-level anomalous concentrations of these metals in the underlying Unit 1 Tertiary porphyritic quartz-feldspar monzonite and Unit 2 Tertiary quartz diorite. Fill-in soil sampling in the Zone 4 area seems to confirm the anomalous patterns displayed by lead, zinc, and silver. The observed soil anomalies of these metals also seem to reflect moderately well the anomalous lithochemical metal values detected particularly in trenches 1010W and 1565W. Similar correlations apply in the North Trout Creek area where seven trenches were excavated over areas of lead, zinc, and silver anomalies. Surprisingly, the area overlying trench 825E in the Zone 2 area showed only a "spot" soil anomaly for each lead, zinc, and silver while rock chip samples from the trench itself returned anomalous lead, zinc, and silver values throughout the trench. Once again, this poor correlation is probably due to generally thick overburden in this area or glacial transport of the anomalous soil values. No direct follow-up of these anomalies is recommended.

## 8.0 GEOPHYSICAL SURVEYS: RESULTS AND INTERPRETATION

### 8.1 VLF-EM Survey

The VLF-EM survey results were plotted as stacked In-phase, Quadrature and Fraser Filter profiles at a scale of

1:10000 shown on Figures 26 and 27. The Fraser Filter data was calculated as per the method put forth by Fraser (1969).

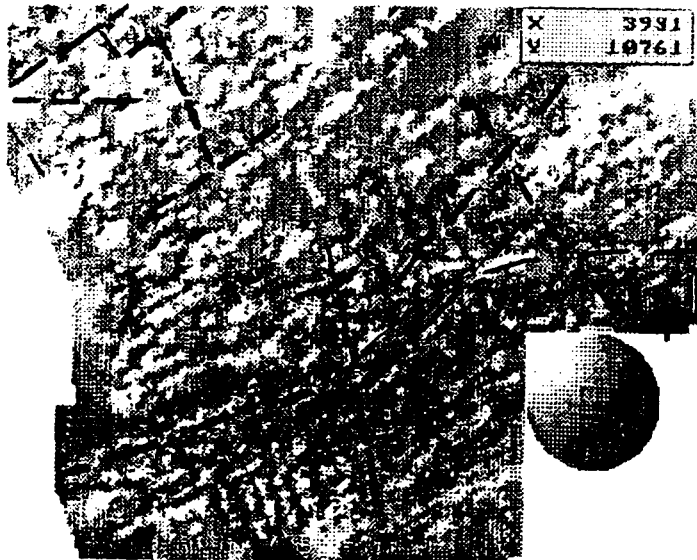
Numerous conductors were detected with the VLF survey which confirmed the 1988 observations. The predominant direction of these conductor axes is  $060^{\circ}$  Azimuth. Several offsets which trend  $010^{\circ}$  Azimuth have been outlined on Figures 26 and 27. There appears to be no obvious connection between the VLF conductors and the anomalous geochemical values. The fault controlling Trout Creek can be detected intermittently along strike. The VLF-EM survey also confirmed the presence of weak to moderate chargeability anomalies detected by the Induced Polarization and Resistivity survey. These areas occur in Zone 2, Zone 4, and line 2+00 West and are discussed in detail in Section 8.3.

## 8.2 Magnetometer Survey

The magnetometer survey results were plotted as plan maps of stacked profiles at a scale of 1:10000 shown on Figures 28 and 29.

Rock units 2 (Biotite-Hornblende Quartz Diorite), 6 (Granite Pegmatite), and 7 (Quartz-Biotite [Hornblende] Gneiss) have a higher magnetic signature and can be outlined by the magnetic survey shown on Figures 28 and 29. A number of linear zones of low magnetic readings were detected by use of the RTI processing package. The breaks reflect the regional lineaments trending  $070$  and  $150$  degrees and have been outlined on Figure 30.

RTI Aerodat/General    SELECT    FILES    COLOUR    ENHANCE    DISTANCE    2000    X



**PLACER DOME INC.**  
**SPRING PROPERTY**  
FIGURE 30.  
**REAL TIME IMAGING PACKAGE**



### 8.3 Induced Polarization and Resistivity Survey

Contoured resistivity and chargeability data for slice M7 (channel 8) are presented as pseudosections at a scale of 1:2500 shown in Appendix IX.

#### 8.3.1 Zone 2

The above survey detected an area of anomalous chargeabilities on lines 7+00 through 14+00 East. This can best be seen on the N=3 and N=5 contoured chargeability maps. The resistivities are quite low on this grid due to increased thicknesses of glacial till. In the vicinity of the anomalous zone, it is evident that the till layer is the thinnest on lines 7+00 and 8+00 East with the thickest area being on lines 10+00 through 12+00 East on the south side of the anomaly. This anomaly was partially tested by trench 825E.

Line 10+00 East was also covered with IP south of the base line. A weak anomaly was detected between the baseline and 100 South. Test pits were excavated to test this anomaly, but they failed to reach bedrock.

There was no significant correlation between the IP survey results and the geochemical soil anomalies.

#### 8.3.2 Zone 4

A weak chargeability anomaly was detected on the south ends of lines 8+00 and 10+00 West. The increase in resistivity values on this grid reflects a general thinning of the overburden on this grid as compared to Zone 2. This target was not trenched due to the weakness of the anomaly.

#### 8.3.3 Line 200 West

A moderate anomaly centered at 32+00 North was detected. The resistivity results on this line are indicative of increased overburden as can be seen from the layering on the IP pseudosections. Thick overburden was confirmed as test pits failed to reach bedrock.

## 9.0 CONCLUSIONS

1. The Spring Property is almost entirely underlain by acidic intrusive rocks, which fall into two groups: a Jurassic granite and a younger Tertiary Monzonite.
2. Alteration and possible mineralization are likely associated with a Tertiary event and appear to be spatially related to regional structural lineaments.
3. Rock geochemistry has revealed anomalous concentrations of precious and base metals as exposed in trenches or outcrops. Anomalous metal values correlate with argillic alteration, and/or increased fracturing and shearing. Areas of determined interest are; Zone C, Main zone, and trench 1010W.
4. Induced Polarization and resistivity surveys revealed three areas of weak to moderate anomalous chargeabilities. The most significant in terms of length (over 700 metres) and magnitude is located in Zone 2. Trench 825E exposed pyrite concentrations sufficient to explain a portion of the anomaly. However, most of this IP anomaly remains to be tested.
5. The magnetometer and EM-VLF surveys were particularly useful in aiding geologic and structural interpretation.
6. In areas of relatively thin overburden, such as portions of Zone 4 and North Trout Creek, soil geochemistry has proven to be an effective tool. Fill-in sampling confirms previously determined anomalies, and trenching has shown that anomalous soil values can be generally traced through the overburden to their source at bedrock.
7. Soil geochemistry has been shown to be an unreliable technique in areas of thick overburden, such as Zone 2. Fill-in and duplicate soil sampling failed to repeat previously defined anomalies. Overburden profile sampling did not demonstrate any continuation of surface anomalies to depth.

## 10.0 RECOMMENDATIONS

1. A short diamond drill hole program should be conducted in the following areas.
  - (i) The Zone 2 IP anomaly between lines 6+00E and 10+00E should be tested. A fence of holes should be angled at 45 degrees towards the northwest and positioned across the anomaly.
  - (ii) The Main alteration zone strike extensions should be tested. Holes should be angled at 45 degrees towards the north and positioned at approximately 100 metre step-outs to the east and west from the section drill tested by Golden Pick in 1985.
  - (iii) The depth extension of Zone C should be tested. A hole collared east of the zone and angled at 45 degrees towards the west would intersect the target.
  - (iv) The anomalous gold zone in trench 1010W should be tested. A hole collared south of the zone and angled at 45 degrees towards the northwest would intersect the target.
2. Induced Polarization surveys should be extended to the east and west of the anomaly determined on line 2+00 West centered at 32+00 North.

## 11.0 STATEMENT OF EXPENDITURES

The following lists the approximate expenditures which Placer Dome has incurred on the Spring Property during the 1989 work program.

Table 4. Statement of Expenditures

1.	Grid Construction: 15km @ \$300/km. . . . .	\$ 4,500.00
2.	Camp Costs: 725 man days @ \$50/man/day . . . . .	36,250.00
3.	Vehicle Costs: Two pick-ups, 90 days @ \$40/day . . . . . Two ATV's, 90 days @ \$20/day . . . . .	7,200.00 3,600.00
4.	Report Preparation: M. Deschenes, 30 days @ \$250/day . . . . . Drafting, Copying . . . . .	7,500.00 1,000.00
5.	Salaries:	
	(i) Geological:	
	M. Deschenes, 64 days @ \$250/day . . . . .	16,000.00
	R. MacGillivray, 80 days @ \$200/day . . . . .	16,000.00
	(ii) Geochemical:	
	D. Turner, 80 days @ \$150/day . . . . .	12,000.00
	J. Pflanz, 80 days @ \$150/day . . . . .	12,000.00
	M. Jeffreys, 80 days @ \$150/day . . . . .	12,000.00
	C. Fischer, 80 days @ \$150/day . . . . .	12,000.00
	(iii) Geophysical:	
	H. Letient, 20 days @ \$250/day . . . . .	5,000.00
	K. Everard, 20 days @ \$250/day . . . . .	5,000.00
	IP Survey crew, 10 days @ \$1,000/day . . . . .	10,000.00
	(iv) Supervision:	
	R. Pease, 25 days @ \$350/day . . . . .	8,750.00
6.	Trenching: Backhoe and Operator 80 days @ \$500/day . . . . .	40,000.00
7.	Soil Geochem Analysis: (Cu,Pb,Zn,Ag,Au) 2917 samples @ \$12 each . . . . .	35,000.00
8.	Rock Geochem Analysis: (Cu,Pb,Zn,Ag,Au,As,Sb) 1000 samples @ \$20 each . . . . .	20,000.00
9.	Consulting: Vancouver Petrographics: 5 samples @ \$240 each . . . . .	<u>1,200.00</u>
	Total	\$ <u>270,000.00</u>

## 12.0 REFERENCES

- Burton, A. (1986): Drilling Assessment Report on the Spring and Boomer Claims. B. C. Assessment Report #14989.
- Burton, A. (1988): Report on the Spring Property, North Trout Creek, Peachland Area, B.C. Private Report to Golden Pick Resources.
- Cannon, R.; Deschenes, M.; Pease, R. (1989): 1988 Work Program Report of the Spring Property VOLUME I-II. Private Report to Placer Dome Inc.
- Dawson, J. M. (1972): Geological, Geochemical, and Geophysical Report on the TC-PO Claims. B. C. Assessment Report #4335.
- Fraser, D.C. (1969): Contouring of VLF-EM Data. Geophysics, V. 34, p. 958-967.
- Pease, R.B. (1989): Assessment Report for Grid Construction and the geology and Soil Geochemistry of the Spring Property. B.C. Assessment Report #18401.
- Pollmer, A. R. (1982): Grid Lines and Geochemical Soil Survey on the Trout Creek Property. B. C. Assessment Report #10108.

### 13.0 STATEMENTS OF QUALIFICATION

#### 13.1 Statement of Qualification, M. Deschenes

I, Marc Deschenes, of the city of Castlegar, B.C., do hereby certify that:

1. I am a graduate from l'Ecole Polytechnique de Montreal, Montreal, Quebec, where I received a B.A.Sc. in Geological Engineering (Exploration Option), in May 1984.
2. From 1980 until the present, I have been involved in studying geology or working in the mineral exploration field in various regions of Canada. I have been employed by Placer Dome Inc. temporarily since May 1988.
3. I am a member of the Order of Engineers of Quebec.
4. I personally participated in the field work described in this report, and have compiled, reviewed, and assessed the resulting data.

Respectfully Submitted,



---

Marc Deschenes, B. Eng.

## STATEMENT OF QUALIFICATIONS

I, Richard W. Cannon, of the City of Vancouver, Province of British Columbia, hereby certify as follows:

1. I am a graduate of the University of British Columbia where I received a B. A. Sc. in Geological Engineering (Geophysics Option) in May, 1966.
2. I am a member of the Association of Professional Engineers of British Columbia and have been so since 1968. Registration No. 6742.
3. I am a member of the Canadian Institute of Mining and Metallurgy, Society of Exploration Geophysicists, and the B. C. Geophysical Society.
4. I have practised my profession since 1966.

Respectfully Submitted,

*R. W. Cannon, P. Eng*  
\_\_\_\_\_  
R. W. Cannon, P. Eng.

## STATEMENT OF QUALIFICATIONS

I, Henri F. Letient, of the City of Vancouver, Province of British Columbia, hereby certify as follows:

1. I am a graduate of the University of British Columbia where I received a B. A. Sc. in Geological Engineering (Geophysics Option) in May 1989.
2. I am currently employed by Placer Dome Inc. under the supervision of Richard W. Cannon.
3. I personally participated in the magnetometer and VLF-EM surveys conducted on the Spring Property during the summer of 1989. I have compiled and reviewed the data as discussed in this report.



H. F. Letient



#### 13.4 Statement of Qualification, R. Pease

I, Robert B. Pease, of 1872 Whistler Court, Kamloops B. C., do hereby certify that:

1. I graduated from the University of Waterloo, Waterloo Ontario, with an Honours B. Sc. degree in Earth Sciences, in 1981.
2. From 1976 until the present, I have been engaged study geology, or working in mineral exploration and mine geology in various regions of Canada. I have been employed by Placer Dome Inc., or subsidiaries, continuously since 1982.
3. I am a member of the Canadian Institute of Mining and Metallurgy, and an Associate of the Geological Association of Canada.
4. I personally supervised the field work described in this report, and have assessed the resulting data.

Respectfully Submitted,



Robert B. Pease, B. Sc.

**APPENDIX I**  
Petrographical Report  
Vancouver Petrographics Ltd.



# Vancouver Petrographics Ltd.

JAMES VINNELL, Manager  
JOHN G. PAYNE, Ph.D. Geologist  
CRAIG LEITCH, Ph.D. Geologist  
JEFF HARRIS, Ph.D. Geologist  
KEN E. NORTHCOTE, Ph.D. Geologist

P.O. BOX 39  
8080 GLOVER ROAD,  
FORT LANGLEY, B.C.  
VOX 1J0  
PHONE (604) 888-1323  
FAX. (604) 888-3642

Report for: Robert Pease (Marc Deschenes),  
Placer Dome Inc.,  
401 - 1450 Pearson Place,  
KAMLOOPS, B.C., V1S 1J9

Invoice 8239  
June 1989

Samples: 59761 - 59765

## Summary:

Samples are of five distinct rock units. Most have been affected by one or more of alteration, shear deformation, replacement and veining. Many samples contain moderately abundant opaque. The composition of some of these has been guessed from textures and examination of the hand sample. Proper identification of opaque minerals would require a polished thin section.

- 59761 porphyritic rhyodacite: Phenocrysts of plagioclase are set in a groundmass of K-feldspar-plagioclase-quartz-chlorite. The rock is cut and replaced by irregular patches and a few veins of quartz-opaque, and is cut by a banded vein zone dominated by quartz with less lenses and seams of opaque and lenses of sericite-(quartz). Late seams are dominated by chlorite with minor carbonate.
- 59762 metamorphosed granodiorite: Plagioclase with less K-feldspar and quartz are intergrown in a metamorphic texture; the original rock probably was plutonic. Pegmatitic patches consists of coarse grained feldspars and less quartz. The rock was moderately granulated in patches by cataclastic deformation producing a much finer grained matrix surrounding relic coarser grained aggregates. Feldspars are altered moderately to ankerite (both) and sericite (plagioclase). Sulfides include pyrite and sphalerite, and possibly chalcopyrite.
- 59763 biotite-hornblende-(sphene) potassic quartz diorite: Medium to locally coarse grained aggregate of plagioclase and quartz with less biotite, K-feldspar, and hornblende, and moderately abundant opaque and sphene. Mafic minerals and sphene are altered completely, and plagioclase is altered slightly.

(continued)

- 59764 altered hypabyssal andesite: Scattered hornblende phenocrysts are set in a groundmass of elongate hornblende grains surrounded by equant, interlocking plagioclase grains and minor apatite and opaque. Minor amygdules are dominated by ankerite with less quartz, plagioclase, chlorite, and sphalerite-(chalcopyrite). The rock was granulated along sharply defined seams up to 2.5 mm wide. Veins along the seams are of ankerite-(plagioclase). Later veinlets are of calcite, with or without minor chlorite or quartz.
- 59765 breccia: Fragments up to several cm across are of a few types of porphyritic rhyodacite/latite containing phenocrysts of plagioclase, quartz, K-feldspar, and less biotite in a groundmass dominated by feldspars. One metamorphic granodiorite(?) fragment is of quartz-plagioclase-K-feldspar. The groundmass contains fragments of single mineral grains (fragmented phenocryst) and porphyry groundmass surrounded by sericite with seams and patches of hematite.

*John G. Payne*

John G. Payne  
604-986-2928

Sample 59761      **Porphyritic Rhyodacite; Sheared, replaced by Banded Vein Zone of Quartz-Opaque-(Sericite-Chlorite) and Veins of Quartz-Opaque; Late Seams of Chlorite-Carbonate**

Phenocrysts of plagioclase are set in a groundmass of K-feldspar-plagioclase-quartz-chlorite. The rock is cut and replaced by irregular patches and a few veins of quartz-opaque, and is cut by a banded vein zone dominated by quartz with less lenses and seams of opaque and lenses of sericite-(quartz). Late seams are dominated by chlorite with minor carbonate.

phenocrysts			
plagioclase	10-12%	veins and replacement patches	
hornblende	minor	quartz	45-50%
groundmass		opaque	5- 7
K-feldspar	8-10	sericite	3- 4
quartz	8-10	chlorite	0.5
plagioclase	7- 8	apatite	trace
chlorite	3- 4	ankerite	trace
opaque	1	late seams	
sericite	0.5	chlorite	0.3
zircon	trace	ankerite	minor

Plagioclase forms ragged anhedral phenocrysts averaging 1-2.5 mm in size, and one up to several mm long. Alteration is slight to moderate to patches of extremely fine grained chlorite.

One patch 0.8 mm long of extremely fine grained chlorite may be after a prismatic phenocryst of hornblende.

The groundmass is dominated by aggregates of anhedral, slightly interlocking K-feldspar, quartz, and plagioclase averaging 0.02-0.07 mm in size. Chlorite forms irregular patches averaging 0.05-0.3 mm in size intergrown with other groundmass minerals. Opaque forms disseminated patches averaging 0.1-0.5 mm in size of extremely fine to very fine grains intergrown slightly to moderately with chlorite and less commonly with other groundmass minerals. Sericite forms scattered patches of extremely fine grained flakes, in part associated with chlorite. Zircon forms a few elongate, euhedral prismatic grains up to 0.05 mm long.

The rock is cut and replaced by patches and veinlets up to 1 mm wide dominated by quartz and opaque. Opaque forms patches up to 2 mm in size. Apatite forms an equant grain 0.15 mm across with opaque. Ankerite forms scattered, anhedral grains up to 0.2 mm long. Sericite forms scattered flakes up to 0.1 mm in size disseminated in quartz.

The main vein zone is banded and dominated by submosaic quartz grains averaging 0.07-0.15 mm in size. Grain size varies moderately from band to band. Opaque forms ragged lenses parallel to banding, ranging up to 2 mm in length of extremely fine to very fine grains. Most of the opaque is an unknown sulfide or sulfosalt. A few equant, subhedral grains from 0.1-0.2 mm in size are of pyrite. Sericite forms discontinuous seams parallel to banding averaging 0.05-0.2 mm wide. These may represent strongly altered host rock. Chlorite forms patches of extremely fine grains intergrown with opaque.

The veins are cut by a few late seams up to 0.2 mm wide in which grains are granulated to aggregates averaging 0.03-0.07 mm in size.

A few late seams up to 0.07 mm wide are of extremely fine grained, medium to dark green chlorite with minor to moderately abundant, very fine grained ankerite and a few lenses of extremely fine grained sericite.

**Sample 59762****Meta-Granodiorite with Pegmatitic Patches;  
Partly Cataclastically Deformed;  
Disseminated Pyrite-Sphalerite**

Plagioclase with less K-feldspar and quartz are intergrown in a metamorphic texture; the original rock probably was plutonic. Pegmatitic patches consists of coarse grained feldspars and less quartz. The rock was moderately granulated in patches by cataclastic deformation producing a much finer grained matrix surrounding relic coarser grained aggregates. Feldspars are altered moderately to ankerite (both) and sericite (plagioclase). Sulfides include pyrite and sphalerite, and possibly chalcopyrite.

plagioclase	50-55%	
K-feldspar	20-25	
quartz	20-25	
pyrite	1- 2	(possibly includes some chalcopyrite)
sphalerite	1	
opaque (oxide?)	0.5	(difficult to distinguish from pyrite)
ankerite	0.5	
apatite	0.3	
Ti-oxide	0.2	
zircon	minor	

Plagioclase forms anhedral to subhedral prismatic grains, which in much of the rock average 0.3-0.7 mm in size. In the pegmatitic patches, plagioclase forms subhedral prismatic grains averaging 1.5-2.5 mm in size, with a few up to 5 mm long. Interstitial to these are finer grains of plagioclase and quartz averaging 0.3-0.7 mm in size. Alteration is slight to moderate to disseminated flakes and patches of sericite and less abundant patches of ankerite. Locally, sericite forms dense patches up to 1 mm in size along borders of plagioclase grains, commonly associated with pyrite and sphalerite.

K-feldspar forms anhedral grains averaging 0.3-0.8 mm in size in the main rock, and in pegmatitic patches forms grains up to 3 mm across. Grains commonly appeared slightly crushed and distorted. Alteration is moderate to locally strong in irregular patches and veinlets to ankerite.

Quartz forms patches up to a few mm across of grains averaging 0.7-2 mm in size, and smaller patches of grains averaging 0.2-0.8 mm in size. In a few patches, quartz is recrystallized partly to coarse subgrain aggregates and partly along grain borders to much finer subgrain aggregates.

Pyrite forms disseminated grains and clusters of grains averaging 0.05-0.2 mm in size, with a few subhedral to euhedral grains up to 0.6 mm across. Some anhedral opaque patches may contain chalcopyrite.

Sphalerite forms irregular patches averaging 0.05-0.2 mm in size and a few from 0.3-0.6 mm across, mainly associated with pyrite, and also partly associated with ankerite, and patches of sericite. It is medium orange in color.

Opaque (probably oxide) forms clusters up to 1.2 mm in size of equant grains averaging 0.05-0.1 mm in size.

Apatite forms subhedral, prismatic grains averaging 0.05-0.1 mm long, and acicular grains up to 0.2 mm long in some coarser grained patches of plagioclase. Associated with opaque oxide it forms clusters of equant to subhedral prismatic grains averaging 0.03-0.07 mm in size.

Ti-oxide forms patches up to 0.5 mm in size of extremely fine grained, nearly opaque aggregates. Commonly these patches surround opaque (ilmenite?) patches (grains?) averaging 0.1-0.15 mm in size.

Zircon forms one euhedral, prismatic grain 0.5 mm long, several anhedral to subhedral grains averaging 0.03-0.06 mm in size, and a few euhedral, prismatic grains up to 0.03 mm long.

About 10% of the rock was granulated during cataclastic deformation to patches averaging 0.03-0.07 mm in grain size. Alteration of feldspars is moderate to locally strong to sericite and ankerite.

The rock is a medium grained to locally coarse grained aggregate of plagioclase and quartz with less biotite, K-feldspar, and hornblende, and moderately abundant opaque and sphene. Mafic minerals and sphene are altered completely, and plagioclase is altered slightly.

plagioclase	60-65%	opaque	1- 2%
quartz	17-20	sphene/Ti-oxide	1
biotite	5- 7	apatite	0.3
K-feldspar	5- 7	calcite	minor
hornblende	3- 4	zircon	trace

Plagioclase forms anhedral to subhedral grains averaging 0.5-1.5 mm in size. Composition is in the range andesite/oligoclase. Many show moderate growth zoning towards more-sodic rims, with minor oscillatory zoning. Alteration is slight to disseminated grains, patches, and seams of sericite and less patches and seams of calcite.

Quartz forms patches up to 2.5 mm across of anhedral grains averaging 0.5-2 mm in size.

K-feldspar forms interstitial grains averaging 0.5-1.5 mm in size, with a few up to 2.5 mm across. Many show cross-hatched microcline twins. A few coarse grains contain minor, exsolution lenses of plagioclase. Adjacent to K-feldspar grains, plagioclase commonly contains patches of myrmekite up to 0.3 mm in size.

Biotite forms flakes averaging 0.5-1 mm in length, and a few up to 1.7 mm across. Some grains are fresh or contain minor to abundant relic patches of fresh biotite, with pleochroism from pale to dark brown. Biotite generally is altered strongly to completely to pseudomorphic chlorite with disseminated patches of leucoxene/Ti-oxide. Chlorite is pleochroic from pale to light green, and has purple to brown interference color.

Hornblende forms subhedral to euhedral grains up to 1 mm long. Alteration is complete to an intimate intergrowth of extremely fine grained chlorite and carbonate, with moderately abundant disseminated opaque. A very few grains also contain moderately abundant patches of very fine grained quartz.

Sphene forms euhedral wedge-shaped grains up to 1 mm long, and anhedral patches averaging 0.2-0.5 mm in size. Alteration is complete to Ti-oxide with minor disseminated calcite. Other patches up to 0.4 mm across of Ti-oxide may be after ilmenite or sphene.

Opaque forms anhedral grains and clusters of grains averaging 0.2-0.6 mm in size. Some of these are associated with Ti-oxide, and many contain minor to moderately abundant grains of apatite.

Apatite forms subhedral grains and clusters of grains averaging 0.05-0.07 mm in size, a few prismatic grains up to 0.13 mm long, and a few euhedral grains with cross sections up to 0.18 mm across. It commonly is associated with mafic minerals and opaque.

Calcite forms a few patches up to 0.3 mm in size of very fine grained aggregates associated with opaque and apatite.

Zircon forms a few subhedral prismatic grains up to 0.1 mm long.

A few wispy veinlets up to 0.07 mm wide are of calcite with moderately abundant, extremely fine grained, disseminated opaque. Alteration of mafic minerals may be associated genetically with these veins.



Sample 59764**Altered Hypabyssal Andesite; Cut by Seams of Cataclastic Deformation and Veins of Ankerite-(Plagioclase) and Late Veins of Calcite**

Scattered hornblende phenocrysts are set in a groundmass of elongate hornblende grains surrounded by equant, interlocking plagioclase grains and minor apatite and opaque. Minor amygdules are dominated by ankerite with less quartz, plagioclase, chlorite, and sphalerite-(chalcopryrite). The rock was granulated along sharply defined seams up to 2.5 mm wide. Veins along the seams are of ankerite-(plagioclase). Later veinlets are of calcite, with or without minor chlorite or quartz.

phenocrysts	
hornblende	2%
groundmass	
plagioclase	55-60
hornblende	20-25
ankerite	4- 5
opaque	0.5
apatite	0.5
amygdules	
ankerite-(quartz-chlorite-plagioclase-sphalerite/chalcopryrite)	0.3
deformed seams	4- 5
veins	
ankerite-(plagioclase)	2
calcite-(chlorite)	0.5

Hornblende forms a few elongate, subhedral to anhedral phenocrysts averaging 1-1.8 mm long and a few equant, anhedral phenocrysts averaging 0.3-0.7 mm across. These are replaced by subparallel to irregular aggregates of extremely fine grained tremolite. One large phenocryst contains minor lenses of chlorite parallel to the c-axis. Some smaller ones are surrounded by ragged rims of ankerite. One large phenocryst is cut along its length by a veinlet of calcite-(chlorite). One cluster up to 2 mm across of stubby prismatic hornblende grains averaging 0.3-0.5 mm in size is altered to intimate intergrowths of ankerite and chlorite.

Plagioclase forms anhedral, moderately interlocking grains averaging 0.3-0.7 mm in size. Alteration is slight to moderate to irregular patches of ankerite and dusty hematite. A few interstitial patches from 0.1-0.7 mm in size are of unaltered, possibly more sodic plagioclase.

Hornblende forms elongate, subhedral, prismatic grains averaging 0.2-0.5 mm long, and a few up to 1.2 mm long. Alteration is complete to chlorite with abundant extremely fine grained, disseminated Ti-oxide spots, and locally to chlorite-quartz(?).

Opaque (in part pyrite) forms disseminated patches averaging 0.05-0.15 mm in size, and a few up to 0.5 mm across.

Apatite forms disseminated prismatic grains averaging 0.07-0.15 mm in size, with a few up to 0.27 mm long, and acicular grains averaging 0.07-0.15 mm long, mainly in plagioclase.

A few rounded replacement patches or amygdules average 0.8 mm across. Some are dominated by ankerite with less quartz and chlorite. One of these contains an irregular patch of sphalerite(?) 0.3 mm across. Sphalerite contains abundant exsolution blebs of chalcopryrite. Another contains a radiating fan of plagioclase 0.25 mm in radius.

(continued)

One granulated seam 1.5 mm across is dominated by extremely fine grained chlorite with angular fragments of plagioclase averaging 0.02-0.05 mm in size. It is cut by a vein dominated by irregular, fine grained ankerite grains with patches of extremely fine to very fine grained plagioclase. The other seam is up to 2.5 mm wide and contains coarser and similar fragments of the host rock in a similar groundmass. Associated with it is a discontinuous veinlike zone up to 0.8 mm wide of interlocking, very fine to fine grained ankerite with minor pyrite.

Several late veinlets averaging 0.05-0.08 mm wide are of calcite, with or without minor chlorite or quartz.

Sample 59765**Breccia: Fragments of Porphyritic Rhyodacite/Latite, Metamorphic Granodiorite(?); Groundmass Dominated by Sericite; Seams of Hematite and Quartz**

Fragments up to several cm across are of a few types of porphyritic rhyodacite/latite containing phenocrysts of plagioclase, quartz, K-feldspar, and less biotite in a groundmass dominated by feldspars. One metamorphic granodiorite(?) fragment is of quartz-plagioclase-K-feldspar. The groundmass contains fragments of single mineral grains (fragmented phenocryst) and porphyry groundmass surrounded by sericite with seams and patches of hematite.

fragments	
porphyritic rhyodacite/latite	65-70%
metamorphosed granodiorite(?)	10-12
other	1- 2
groundmass	17-20
veins and replacements	
quartz-(sericite)	0.5
hematite-(limonite)	1- 2

rhyodacite/latite fragments

Major phenocrysts are of plagioclase, with less quartz, and K-feldspar. Plagioclase phenocrysts average 0.5-2.5 mm in size and are altered slightly to moderately to sericite. Quartz phenocrysts range from angular to rounded and from 0.3-2 mm in size. Some have resorbed borders against the groundmass. K-feldspar phenocrysts are from 1-2 mm in size; alteration is slight on fractures to sericite. One K-feldspar phenocryst containing a few inclusions of plagioclase phenocrysts is rimmed by a zone 0.2-0.3 mm wide of plagioclase. In some fragments biotite (2-3%) forms slender flakes up to 0.7 mm long. Alteration is complete to pseudomorphic muscovite and minor Ti-oxide. Apatite forms scattered subhedral to euhedral phenocrysts up to 0.3 mm across. Zircon forms a few grains up to 0.18 mm long, and several elongate prismatic grains averaging 0.03 mm in length; the latter occur in feldspar phenocrysts.

The groundmass is variable, being mainly granular, with grains averaging from 0.01-0.03 mm in grain size, and being dominated by plagioclase in some and by K-feldspar in others (see stained offcut block). In one fragment, the groundmass is dominated by moderately to strongly interlocking plagioclase grains averaging 0.03-0.07 mm in size. Opaque and Ti-oxide each form equant patches averaging 0.07-0.12 mm in size.

A few replacement patches up to 0.3 mm in size are of very fine grained quartz, with or without very fine grained sericite.

One porphyritic rhyolite(?) fragment contains a quartz phenocryst 2 mm in size and a plagioclase phenocryst 1 mm across (altered completely to sericite) in a groundmass consisting of equant quartz grains 0.03-0.07 mm in size surrounded by poikilitic K-feldspar grains averaging 0.1-0.5 mm in size and patches of sericite (after plagioclase), also interstitial to groundmass quartz.

other fragments

A few fragments up to 1.5 mm in size consist of aggregates of equant grains of K-feldspar, quartz, and lesser plagioclase averaging 0.05-0.07 mm in size. Other fragments of similar texture and probably of metamorphic origin consists of quartz with minor dusty hematite.

(continued)

The main metamorphic fragment up to 1 cm across contains patches of medium grained quartz-plagioclase-(K-feldspar) intergrown with patches of very fine grained feldspars and sericite. K-feldspar grains commonly are very irregular against quartz. Hematite forms scattered patches up to 0.6 mm across. Apatite and zircon are common accessory minerals in grains less than 0.03 mm in size.

The groundmass contains angular fragments averaging 0.2-0.5 mm in size of plagioclase, quartz and minor biotite phenocrysts, and fragments up to 1 mm in size of a few types of latite/rhyodacite groundmass. These are enclosed in an aggregate of extremely fine grained sericite, with scattered patches of extremely fine grained kaolinite. Locally, the groundmass is stained orange by limonite.

Minor veinlets and patches up to a few mm across are dominated by very fine to fine grained quartz and patches of sericite and of hematite/limonite.

A few seams up to 0.25 mm wide are of opaque to red-brown hematite and less orange-brown limonite.

**APPENDIX II**

**Listing of Rock Sample Data**

ROCK SAMPLE DATA

- LEGEND -

LOCATIONS & DESCRIPTIONS

ABUN	: ABUNDANT	MAL	: MALACHITE
ALT'D/ALT'N	: ALTERED/ALTERATION	MASS	: MASSIVE
ALT'G	: ALTERNATING	MED	: MEDIUM
ASS'TD	: ASSORTED	META-SEDS	: META-SEDIMENTS
BAND'G	: BANDING	MF	: MAFIC
BIOT	: BIOTITE	MG	: MAGNETITE
BLB	: BLEBS	M-GR	: MEDIUM GRAINED
BLDR	: BOULDER	MIN	: MINOR
BTW	: BETWEEN	MOD	: MODERATE
CA	: CALCITE	MTX	: MATRIX
CARB'D	: CARBONATIZED	NRW	: NARROW
C-GR	: COARSE GRAINED	OTC	: OUTCROP
CHL/CHL'D	: CHLORITIZATION/CHLORITIZED	OXYD	: OXIDATION
CONGL	: CONGLOMERATE	PERV	: PERVASIVE
CP	: CHALCOOPYRITE	PL	: PYROLUSITIC
CTC	: CONTACT	PORPH	: PORPHYRITIC
CU	: COPPER	POSS	: POSSIBLE
DR	: DIORITE	POTAS	: POTASSIC
DISS	: DISSEMINATED	PR	: PYRRHOTITE
ERR	: ERRATIC	PROP	: PROPERTY
EM	: EQUIGRANULAR-MEDIUM	PY	: PYRITE
FELS	: FELSIC	QFP	: QUARTZ-FELDSPAR PORPHYRY
FF	: FRACTURE FILLING	QV	: QUARTZ VEIN
FGM	: FRAGMENTS	QZ	: QUARTZ
F-GR	: FINE GRAINED	RD	: ROAD
FN	: FINE	RECRYST'D	: RECRYSTALLIZED
FRACT'D	: FRACTURED	RUST'D	: RUSTED
GL	: GALENA	RX	: ROCK
GRAPH	: GRAPHITE	SCHT	: SCHISTOSE
GRDIO'TE	: GRANODIORITE	SHEAR'G	: SHEARING
GT	: GRANITE	SIL/SIL'D	: SILICIFICATION/SILICIFIED
HEM	: HEMATITIC	SK	: STOCKWORK
HG'LY	: HIGHLY	SLP	: SLOPE
HNFLS	: HORNFELS	SIN'D/SIN'G	: STAINED/STAINING
INIM	: INTERMEDIATE	SULF	: SULFIDES
INTR	: INTRUSIVE	TEXT	: TEXTURE
JCT	: JUNCTION	TR	: TRACE
LAM	: LAMINATED	VOLC	: VOLCANICS
LCP	: LEGAL CORNER POST	VN	: VEIN
LI	: LIMONITIC	W	: WITH
LG	: LARGE	WD	: WIDE
LK	: LAKE	WEATH'D	: WEATHERED
LWR	: LOWER	WH	: WHITEHEAD
MAGN	: MAGNETIC	WK'GS	: WORKINGS
		ZN	: ZONE

ROCK SAMPLE DATA

- LEGEND -

LITHOLOGY CODES

BREC : TECTONIC BRECCIA  
GRAN : GRANITE PEGMATITE  
HAND : HYPABBYSAL ANDESITE DYKE  
PPFQ : PORPHYRITIC QUARTZ-FELDSPAR MONZONITE  
PRHD : PORPHYRITIC RHYODACITE  
QBGN : QUARTZ-HORNBLLENDE GNEISS  
QZDR : QUARTZ DIORITE

SPRING PROJECT  
1989 ROCK SAMPLES, A LISTING FILE

LAB NO.	SAMP.	APPROXIMATE LOCATION	LITH	ABBREVIATED DESCRIPTION	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	As (ppm)	Sb (ppm)
9114	42776	Zone P4: L.0+55E,2+00N	BREC	1.5m chip,alt'd tectonic brec.w. pl,li stn'g,5%dis py	12	328	119	1.9	3	12	6.0
9114	42777	0.3m above 42776	BREC	as 42776	11	251	113	1.5	3	10	1.0
9114	42778	0.3m below 42776	BREC	as 42776	12	297	103	1.3	3	15	1.0
9114	42779	1.5m west of 42776	BREC	as 42776	13	313	323	1.5	3	12	1.0
9114	42780	0.5m above 42779	BREC	as 42776	13	265	166	1.5	3	17	1.0
9114	42781	0.5m below 42779	BREC	as 42776	10	166	240	1.3	3	20	1.0
9114	42782	1.5m west of 42779	BREC	as 42776	20	234	610	1.3	3	5	1.0
9114	42783	0.3m above 42782	BREC	as 42776	26	298	322	1.8	3	15	1.0
9114	42784	0.3m below 42782	BREC	as 42776	17	283	700	1.6	3	7	1.0
9114	*42784	duplicate analyses			14	240	600	1.3	3	9	1.0
9114	42785	1.5m west of 42782	BREC	as 42776	30	307	550	1.5	3	7	1.0
9114	42786	0.5m above 42785	BREC	as 42776	30	333	340	2.7	3	18	1.0
9114	42787	0.5m below 42785	BREC	as 42776	25	260	1010	1.7	3	19	1.0
9114	42788	1.5m west of 42785	BREC	as 42776	35	390	253	2.6	3	18	1.0
9114	42789	0.5m above 42788	BREC	as 42776	22	580	203	2.4	3	23	1.0
9114	42790	0.5m below 42788	BREC	as 42788	43	378	293	3.2	3	24	1.0
9114	42791	as 42779	BREC	1.5m chip,in highly alt'd fault gouge	17	550	177	1.0	3	8	1.0
9114	42792	Zone N2,L.0+90E,1+50N	PRHD	1.5m chip,sil'd mafic volc,5-10% qz-mg sk,pl-li stn'g	27	56	367	1.0	15	1	1.0
9114	42793	0.3m above 42792	PRHD	as 42792	28	126	265	.8	3	38	1.0
9114	*42793	duplicate analyses			29	133	272	.8	3	38	1.0
9114	42794	0.3m below 42792	PRHD	as 42792	18	45	302	.9	10	23	1.0
9114	42795	1.5m west of 42792	PRHD	as 42792	24	40	332	.9	3	24	1.0
9114	42796	0.3m above 42795	PRHD	as 42792	24	37	292	.5	3	21	1.0
9114	42797	0.3m below 42797	PRHD	as 42792	15	16	246	.4	3	6	1.0
9114	42798	1.5m north of 42795	PRHD	1.5m chip,clay alt'd fault gouge in mafic volc	23	100	150	4.0	3	152	1.0
9114	42799	0.5m north of 42798	PRHD	1.5m chip,fract'd,sil'd mafic volc.w.pl-li stn'g	23	75	207	4.3	3	162	1.0
9114	42800	0.5m south of 42798	PRHD	1.5m chip,highly clay alt'd volc,5% diss & patches py	17	60	107	3.5	10	150	1.0
9114	42801	Zone C1,L.0+75W,10+63N	BREC	1.2m chip,clay alt'd fault gouge in tectonic brec	25	1660	1540	2.3	3	44	1.0
9114	42802	0.3m below 42801	BREC	1.4m chip,med-gr sil'd brec w.pl-li stn'g,5% diss py	21	1050	1240	2.2	3	15	1.0
9114	*42802	duplicate analyses			22	1080	1280	2.3	3	15	1.0
9114	42803	Zone C3,L.0+75W,10+45N	HAND	1.5m chip,clay alt'd fault gouge w.strong li stn'g	90	5500	3300	27.0	75	290	2.0
9114	42804	0.3m above 42803	HAND	1.5m chip,mod.fract'd,sil'd andesite,5% diss py	5	82	770	.6	35	52	1.0
9114	42805	0.2m below 42803	HAND	0.75m chip,as 42804 w. 10% li-py stn'g	20	1150	3200	2.0	15	36	1.0
9114	42806	0.3m below 42803	HAND	0.75m chip,as 42804	16	310	1970	.4	3	6	1.0



LAB NO.	SAMP.	APPROXIMATE LOCATION	LITH	ABBREVIATED DESCRIPTION	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	As (ppm)	Sb (ppm)
9114	42807	0.2m below 42805	HAND	0.5m chip,clay alt'd fault gouge w.li stn'g	78	3900	3600	6.0	50	71	3.0
9114	42808	Zone C2,L.0+75W,10+50N	BREC	1.5m chip,as 42807 w. 3% diss py	18	1150	660	3.6	15	122	1.0
9114	42809	1.5m south of 42808	BREC	as 42808	15	960	610	2.5	3	66	1.0
9114	42810	1.5m south of 42809	BREC	as 42808	26	1540	1920	3.0	3	53	1.0
9114	42811	1.5m south of 42810	BREC	as 42808	74	4400	4400	13.0	15	68	1.0
9114	42812	as 42803	BREC	1.5m chip,clay alt'd fault gouge w.5% diss py	7	600	510	4.8	3	98	1.0
9114	42813	1.5m south of 42812	BREC	as 42812	9	700	304	4.0	15	75	1.0
9114	*42813	duplicate analyses			9	680	301	3.8	3	80	1.0
9114	42814	1.5m south of 42813	BREC	as 42812	16	540	820	3.8	30	143	1.0
9114	42815	1.5m south of 42814	BREC	as 42812	22	520	1900	3.0	15	77	1.0
9114	42816	1.5m south of 42815	BREC	as 42812	30	990	1620	3.3	20	87	1.0
9114	42817	1.5m south of 42816	BREC	1.5m chip,alt'd shear zone along andesite-brec contac	26	640	1050	3.0	25	160	1.0
9114	42818	Zone C2,L.0+75W,10+53N	BREC	1.5m chip,across clay alt'd,rusty fault gouge,3%dis p	14	1470	540	2.8	15	95	1.0
9114	42819	Zone C2,L.0+75W,10+50N	BREC	as 42818	38	1650	1700	9.0	20	75	1.0
9114	42820	Zone C3,L.0+75W,10+47N	BREC	1.5m chip across multiple fault gouge,dis py(5%)gl(2%	56	4000	4600	3.7	20	56	1.0
9114	42821	Taken across sample 42820	BREC	1.5m chip along alt'd shear zone (andesite-brec ctc)	109	2000	6500	3.3	10	54	1.0
9114	42822	0.2m south of 42821	BREC	1.3m chip across clay alt'd shear zone	102	850	4500	2.8	15	54	1.0
9114	*42822	duplicate analyses			106	870	4500	2.7	10	54	1.0
9114	42823	1.5m south of 42822	BREC	1.0m chip as 42822 w.5%diss py	19	690	710	3.0	10	103	1.0
9114	42824	1.5m south of 42823	BREC	0.8m chip,as 42823	31	335	1520	2.1	3	100	1.0
9114	42825	1.5m south of 42824	BREC	1.0m chip,as 42824	30	1520	2100	4.2	10	110	1.0
9114	42826	Zone N2:L.0+90E,1+53N	PRHD	1.0m chip in clay alt'd porph,sil'd volc,qz-mg sk	27	68	92	2.9	55	113	1.0
9114	42827	0.5m below 42826	PRHD	as 42826	12	28	97	1.1	20	78	1.0
9114	42828	1.0m north of 42826	PRHD	as 42826	9	50	64	2.0	15	78	1.0
9114	42829	0.5m below 42828	PRHD	as 42826	14	55	43	2.7	15	150	2.0
9114	*42829	duplicate analyses			14	55	46	2.8	10	155	2.0
9114	42830	0.5m north of 42829	PRHD	1.5m chip in highly clay alt'd fault gouge	9	710	98	10.0	10	51	1.0
9114	42831	0.3m below 42830	BREC	footwall of fault gouge in alt'd tectonic brec	10	41	92	2.5	3	19	1.0
9114	42832	0.3m above 42830	BREC	hangingwall of fault gouge in alt'd tectonic brec	16	106	158	5.3	20	124	1.0
9114	42833	0.5m north of 42830	BREC	1.0m chip,as 42830	22	157	120	4.1	10	20	1.0
9114	42834	0.5m below 42833	BREC	footwall of fault gouge in alt'd tectonic brec	25	95	200	1.0	3	8	1.0
9114	42835	0.5m above 42833	BREC	hangingwall of fault gouge in alt'd tectonic brec	10	118	61	4.8	10	155	1.0
9114	42836	Zone C1:L.0+75W,10+72N	HAND	1.6m chip,alt'd fault gouge in rusty weath'd andesite	40	85	216	2.9	40	215	1.0
9114	42837	0.3m above 42836	HAND	1.7m chip,mod fract'd,alt'd andesite w.5% diss py	46	47	173	.7	3	11	1.0
9114	42838	0.3m below 42836	HAND	1.6m chip as 42836	40	47	180	3.0	40	360	1.0
9114	42839	1.5m south of 42836	HAND	1.5m chip,as 42837	46	225	720	1.5	15	62	1.0
9114	42840	0.3m above 42839	HAND	as 42839	69	680	930	1.4	3	16	1.0
9114	42841	0.3m below 42839	HAND	1.5m chip,as 42836 w. 5% diss py	24	340	870	7.0	135	680	1.0

LAB NO.	SAMP.	APPROXIMATE LOCATION	LITH	ABBREVIATED DESCRIPTION	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	As (ppm)	Sb (ppm)
9114	42842	1.5m south of 42839	HAND	1.5m chip,as 42837	29	100	301	1.0	10	53	1.0
9114	42843	0.3m below 42842	HAND	1.5m chip,as 42836 (contact)w. 5% diss py	54	295	570	5.2	135	580	1.0
9114	42844	0.3m below 42843	BREC	1.6m chip,siliceous tectonic brec,carb'd,5% diss py	24	206	394	.3	25	12	1.0
9114	42845	3.0m south of 42840	HAND	1.6m chip,as 42837	20	840	1130	5.0	110	330	1.0
9114	42846	0.3m below 42845	HAND	1.0m chip,as 42843	90	1330	1500	4.0	60	280	1.0
9114	42847	0.3m below 42846	BREC	1.0m chip,highly alt'd fault gouge w. minor py							
9114	*42847	duplicate analyses			28	205	1420	1.7	20	130	1.0
9114	42848	0.3m below 42847	BREC	1.3m chip,as 42844	22	138	325	.5	10	26	1.0
9114	42849	Zone C1:L.0+75W,10+65N	HAND	1.5m chip,alt'd andesite,li stn'g,minor py	10	86	382	.6	3	24	1.0
9114	42850	0.3m below 42849	HAND	1.8m chip,clay alt'd fault gouge,andesite-brec ctc	20	1280	580	2.0	150	720	2.0
9114	42851	Zone C3:L.0+75W,10+40N	BREC	1.5m chip across clay alt'd rusty shear zone,5% dis p	36	810	1250	2.8	3	81	1.0
9114	42852	1.5m south of 42851	BREC	1.0m chip,as 42851	41	830	1420	3.6	3	74	1.0
9114	42853	Zone C1: 1.5m south of 42850	HAND	1.5m chip along rusty fault gouge(and-brec ctc),min p	57	1960	1900	5.0	75	540	1.0
9114	42854	Zone C2: 1.5m south of 42853	HAND	as 42853	50	3100	2000	14.0	125	870	1.0
9114	42855	1.5m south of 42854	HAND	as 42853	49	4200	1700	9.0	30	310	1.0
9114	42856	1.5m south of 42855	HAND	as 42853	44	3800	1890	8.0	60	390	1.0
9114	*42856	duplicate analyses			44	3800	1900	7.0	75	400	1.0
9114	42857	Zone C4:L.0+75W,10+38N	BREC	1.5m chip,as 42853	37	650	1340	.7	3	18	1.0
9114	42858	1.5m south of 42857	BREC	1.5m chip as 42853	70	2070	3800	6.0	10	143	1.0
9114	42859	Zone C4:L.0+75W,10+35N	BREC	1.5m chip along rusty fault gouge,weath'd,sil'd brec	27	740	1360	1.7	3	40	1.0
9114	42860	1.5m south of 42859	BREC	as 42859	21	960	910	5.3	25	170	1.0
9114	42861	1.5m south of 42860	BREC	as 42859	39	980	3300	2.3	10	36	1.0
9114	42862	1.5m south of 42861	BREC	as 42859	63	1640	1830	7.0	25	195	1.0
9114	42863	1.5m south of 42862	BREC	as 42859	15	272	540	1.9	10	163	1.0
9114	42864	1.5m south of 42863	BREC	as 42859	11	312	282	1.2	3	44	1.0
9114	42865	1.5m south of 42864	BREC	as 42859	14	1180	930	2.3	3	36	1.0
9114	42866	taken across sample 42859	BREC	1.5m chip across rusty fault gouge,minor py	25	238	1130	1.1	3	46	1.0
9114	42867	taken across sample 42860	BREC	1.3m chip,as 42866	53	580	2150	1.6	3	38	17.0
9114	42868	taken across sample 42862	BREC	1.2m chip,as 42866	12	402	386	1.4	3	116	1.0
9114	42869	taken across sample 42864	BREC	1.1m chip,as 42866	5	85	177	.3	3	11	1.0
9114	*42869	duplicate analyses			5	80	170	.3	3	11	1.0
9114	42870	L.9+30W,7+75S	QZDR	Float,gneissic hnfls,carb'd,sil'd,3% diss py & gl	196	261	2800	2.2	3	1	1.0
9114	42871	L.9+80W,5+75S	QZDR	Float,sil'd,carb'd,f-gr qz-dr w. qz stockwork	96	3100	2000	70.0	20	1	1.0
9114	42876	L.10+50W,8+50S	PPFQ	Grab,grey,mass,porph monzonite,min py	4	52	68	.1	3	1	1.0
9114	42877	L.10+50W,8+00S	QZDR	Grab,brown,mass,porph qz-dr w.pl stn'g	3	21	56	.1	3	1	1.0
9114	42878	L.13+52W,8+21S	PPFQ	Grab,white,mass,porph monzonite,min py	9	90	81	.1	3	1	1.0
9114	42879	L.15+00W,8+50S	PPFQ	Grab,white-brown,mass,sil'd porph monzonite,min py	3	32	51	.2	15	1	1.0
9114	42880	L.15+15W,8+50S	PPFQ	as 42879	2	30	134	.1	3	1	1.0

LAB NO.	SAMP.	APPROXIMATE LOCATION	LITH	ABBREVIATED DESCRIPTION	Cu (ppm)	Pb (ppm)	Zn (ppm)	Ag (ppm)	Au (ppb)	As (ppm)	Sb (ppm)
9114	42881	L.15+25W,8+50S	PPFQ	as 42879	3	26	136	.1	3	1	1.0
9114	42882	L.15+73W,9+55S	PPFQ	Grab,mass,sil'd porph monzonite,sil'd	2	20	35	.1	3	1	1.0
9122	42883	L.4+00E,31+00N	QBGN	Grab,gneissic,m-gr,meta-sediment w. qz veining	36	9	28	.1	3	5	-
9122	42884	L.0+50E,7+25S	PPFQ	Float,grey-white porph qz-monzonite w.3cm qz vein	12	15	35	.1	3	1	-
323-62	42994	L.8+05E,4+76N	PPFQ	Grab,grey-green,sil'd porph qz-monzonite	3	29	106	.05	3	1	.1
323-63	42995	L.8+00E,5+23N	PPFQ	Grab,grey-white,porph qz-monzonite	2	7	18	.05	3	2	.1
323-64	42996	L.8+00E,5+50N	PPFQ	1.5m chip,brown-white porph monzonite w.li stn'g	4	125	414	.1	3	7	.4
323-65	42997	as 42996	PPFQ	as 42996	3	163	482	.4	3	49	1.1
323-66	42998	as 42996	PPFQ	as 42996	2	53	297	.05	3	13	.5
323-67	42999	as 42996	PPFQ	as 42996	5	121	423	.05	3	27	.9
323-68	43000	as 42996	PPFQ	as 42996	5	63	234	.05	3	17	.7
606- 1	43033	L.67+00E,70+00N	HAND	Grab,dark-grey,f-gr,andesite dyke w. minor py	64	13	73	.2	3	3	.2
606- 2	43034	as 43033	GRAN	Grab,red-white,hematitic,c-gr granite	42	8	58	.05	3	5	.4
357- 1	43075	L.2+00W,8+98N	PPFQ	1.5m chip,white-grey,clay alt'd porph monz.min py & g	4	34	123	.5	3	8	-
606- 4	53626	L.42+90E,57+15N	GRAN	Grab,2cm wide qz vein in hematitic c-gr gt,min py	5	11	67	.05	5	2	.1
606- 5	53627	L.42+90E,57+25N	GRAN	0.9m chip along 15cm wide fault gouge in c-gr granite	9	16	36	.05	5	3	.1
606- 6	53628	L.42+90E,58+90N	HAND	Grab,2m wide,dark grey-green andesite dyke,min mg	30	5	61	.05	15	2	.1
606-13	53635	L.5+75W,33+10N	GRAN	Grab,sil'd biot-gt/hb-gneiss ctc, min py	22	3	46	.05	3	3	.1
606-14	53636	L.47+42E,70+35N	HAND	Grab,chlor'd,f-gr andesite dyke,min sil	36	6	108	.1	3	4	.1
606-15	53640	L.73+00E,63+20N	GRAN	Grab,red-brown gneissic granite	41	3	31	.05	10	6	.1
606-16	53641	L.84+00E,64+00N	GRAN	Grab,red-brown,clay alt'd,li stn'd gt w. min py	8	4	17	.05	3	2	.1
606-18	53643	L.46+80E,64+40N	QHGN	Grab,greyish,li stn'd,f-gr qz-hornblende gneiss	29	6	57	.1	3	2	.1
606-19	53644	L.67+00E,70+00N	QBGN	Grab,greyish,f-gr,sil'd,qz-biot gneiss w. min py	118	11	103	.4	15	4	.1
606-24	53649	L.70+50E,79+50N	GRAN	Grab,orange-grey,li stn'd granite	29	8	162	.05	20	4	.1
606-25	53650	as 53649	GRAN	Grab,white,hematitic granite	56	14	106	.05	10	6	.1

APPENDIX III  
Rock Sample Statistical Summary  
and  
Histograms

PLACER    DO ME    INC.

Placer Data Analysis System - STATS  
run on 89:10:30 at 13:05:10  
SPRING ROCKS 1988 AND 1989 PROGRAMS

Summary of data from file : statrcks.89

This data file contains an internal header: ( 5 records)  
Data grouped into 9 fields  
with format: (A8,4X,A5,7F10.2)

Character ID fields:  
PROJ SAMP

Coordinate fields:

Other data fields:  
AG AS AU CU PB SB ZN

Missing data indicated by NULL value 99999.0

BASIC STATISTICS OF SELECTED DATA FIELDS:

NAME	NDATA	NULLS	MINIMUM	MAXIMUM	MEAN	STD. DEV.	GEOM. MEAN	DISPERSION
AG	1452	0	.500000E-01	81.0000	.991290	3.34539	.320409	.777266E-01 1.32081
AS	1452	0	.500000E-01	870.000	25.4450	64.2072	7.26740	1.15957 45.5472
AU	1452	0	3.00000	1070.00	12.4194	34.0194	7.04710	2.86784 17.3167
CU	1452	0	1.00000	8900.00	25.3994	238.465	9.14485	3.01712 27.7179
PB	1452	0	1.00000	8600.00	186.653	507.687	57.9515	14.0819 238.489
SB	1449	3	.500000E-01	17.0000	.516901	1.32992	.191706	.629705E-01 .583626
ZN	1452	0	2.00000	6500.00	274.712	519.042	126.117	39.2043 405.708





HISTO:

SPRING ROCKS 1988 AND 1989 PROGRAMS

RUN ON 89:10:30 AT 13:05:10

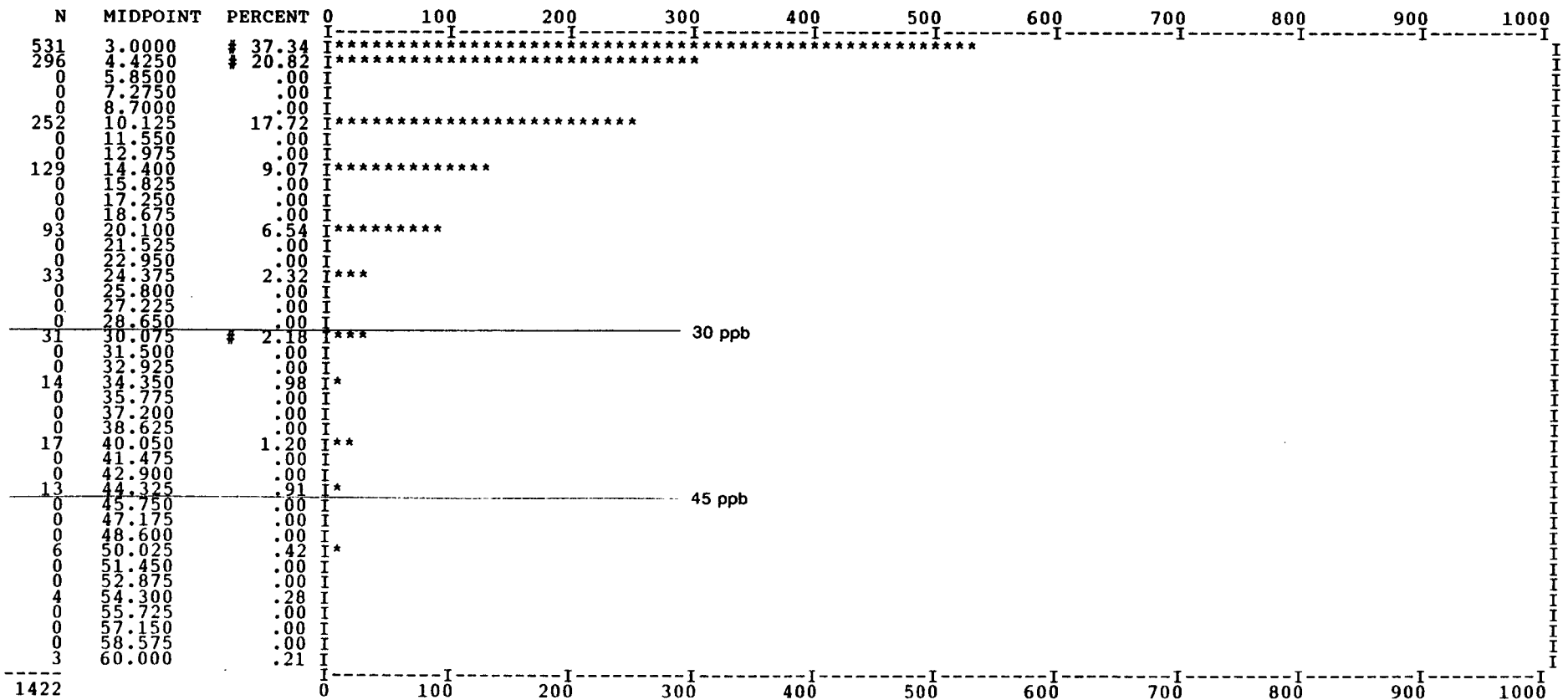
File: statrcks.89 Field name: AU LOG = 0 REPVAL = .00100

1452 SAMPLES WITH AU MINIMUM: 3.00000 MAXIMUM: 1070.00

1422 VALUES PLOTTED: 30 NOT IN RANGE 3.00000 to 60.0000

MEAN: 9.56259 STD. DEV.: 9.58946

SCALE OF HISTOGRAM IS 10.00 COUNTS /PRINT POSITION # = 5,50,95%





HISTO:

SPRING ROCKS 1988 AND 1989 PROGRAMS

RUN ON 89:10:30 AT 13:05:10

File: statrcks.89

Field name: CU

LOG = 0 REPVAL = .00100

1452 SAMPLES WITH CU

MINIMUM: 1.00000

MAXIMUM: 8900.00

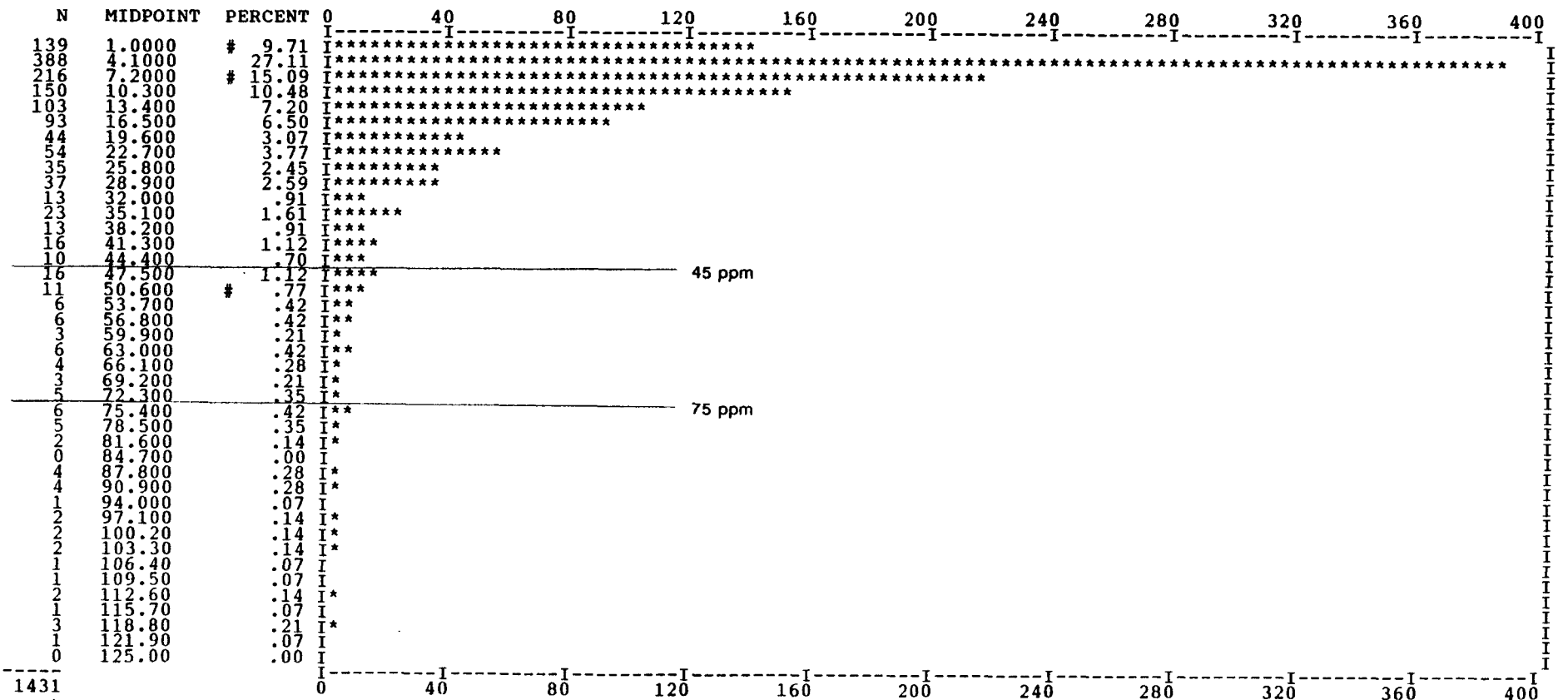
1431 VALUES PLOTTED:

21 NOT IN RANGE 1.00000 to 125.000

MEAN: 14.9008

STD. DEV.: 18.4395

SCALE OF HISTOGRAM IS 4.00 COUNTS /PRINT POSITION # = 5,50,95%



1431

HISTO:

SPRING ROCKS 1988 AND 1989 PROGRAMS

RUN ON 89:10:30 AT 13:05:10

File: statrcks.89

Field name: PB

LOG = 0 REPVAL = .00100

1452 SAMPLES WITH PB

MINIMUM: 1.00000

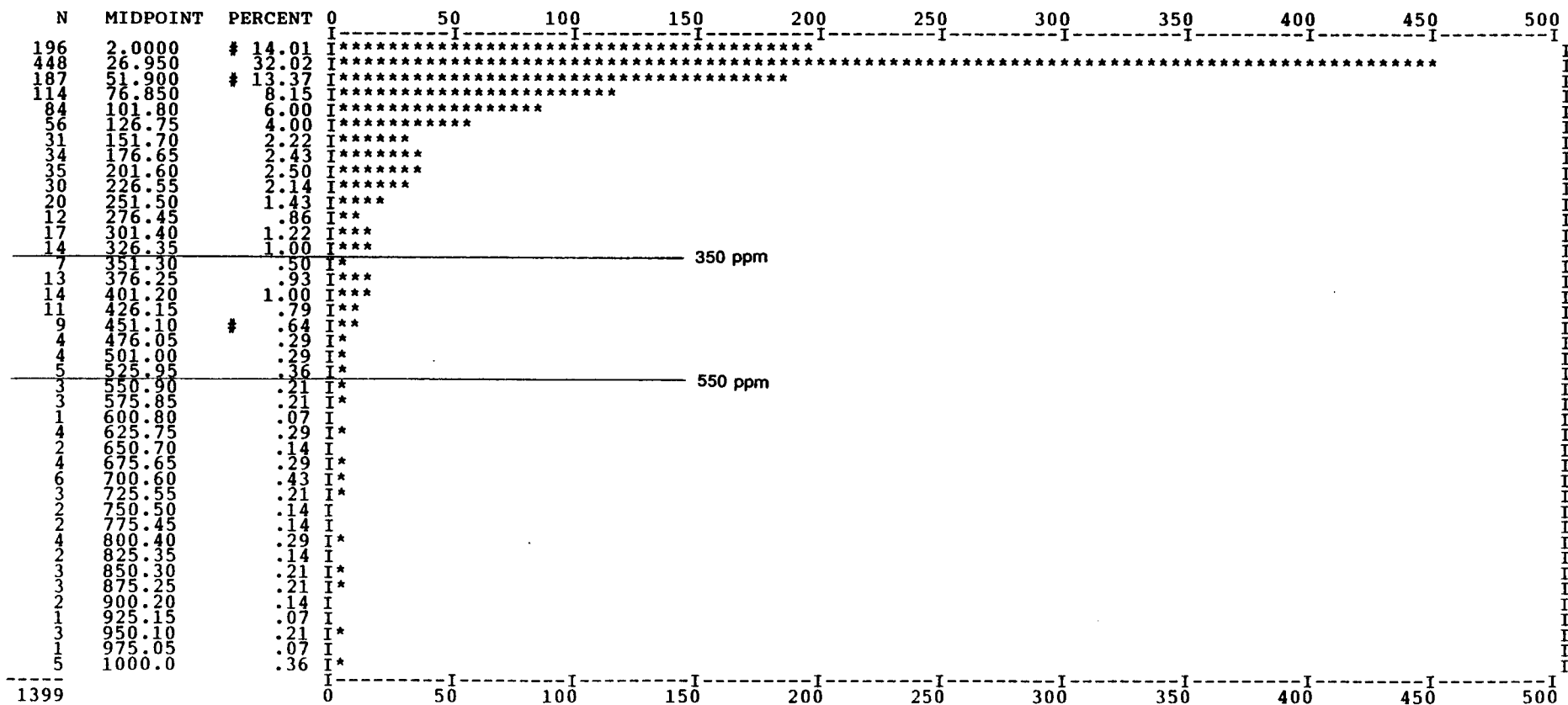
MAXIMUM: 8600.00

1399 VALUES PLOTTED:

53 NOT IN RANGE 2.00000 to 1000.00

MEAN: 113.948 STD. DEV.: 169.204

SCALE OF HISTOGRAM IS 5.00 COUNTS /PRINT POSITION # = 5,50,95%



1399

HISTO:

SPRING ROCKS 1988 AND 1989 PROGRAMS

RUN ON 89:10:30 AT 13:05:10

File: statrcks.89

Field name: ZN

LOG = 0 REPVAL = .00100

1452 SAMPLES WITH ZN

MINIMUM: 2.00000

MAXIMUM: 6500.00

1370 VALUES PLOTTED:

82 NOT IN RANGE

2.00000

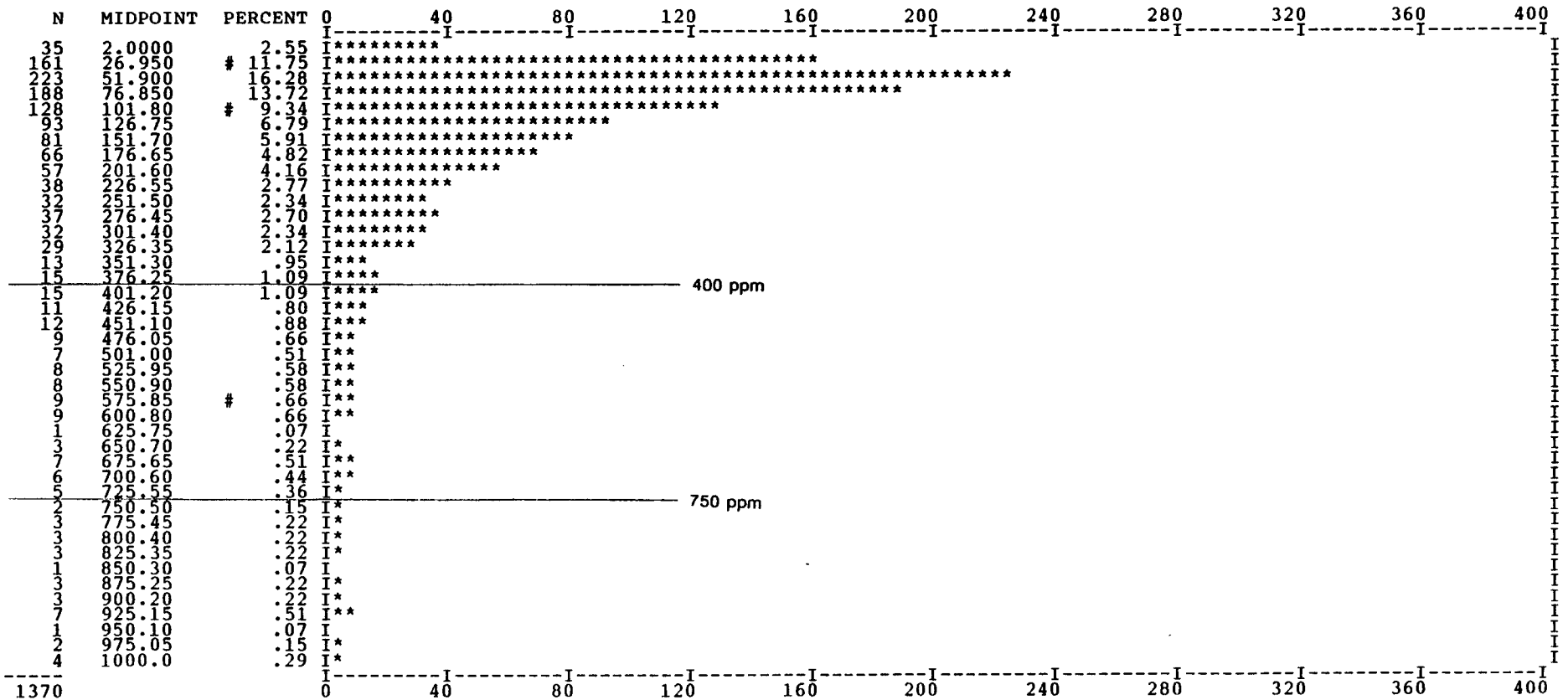
to 1000.00

MEAN:

170.491

STD. DEV.: 180.370

SCALE OF HISTOGRAM IS 4.00 COUNTS /PRINT POSITION # = 5,50,95%



HISTO:

SPRING ROCKS 1988 AND 1989 PROGRAMS

RUN ON 89:10:30 AT 13:05:10

File: statrcks.89

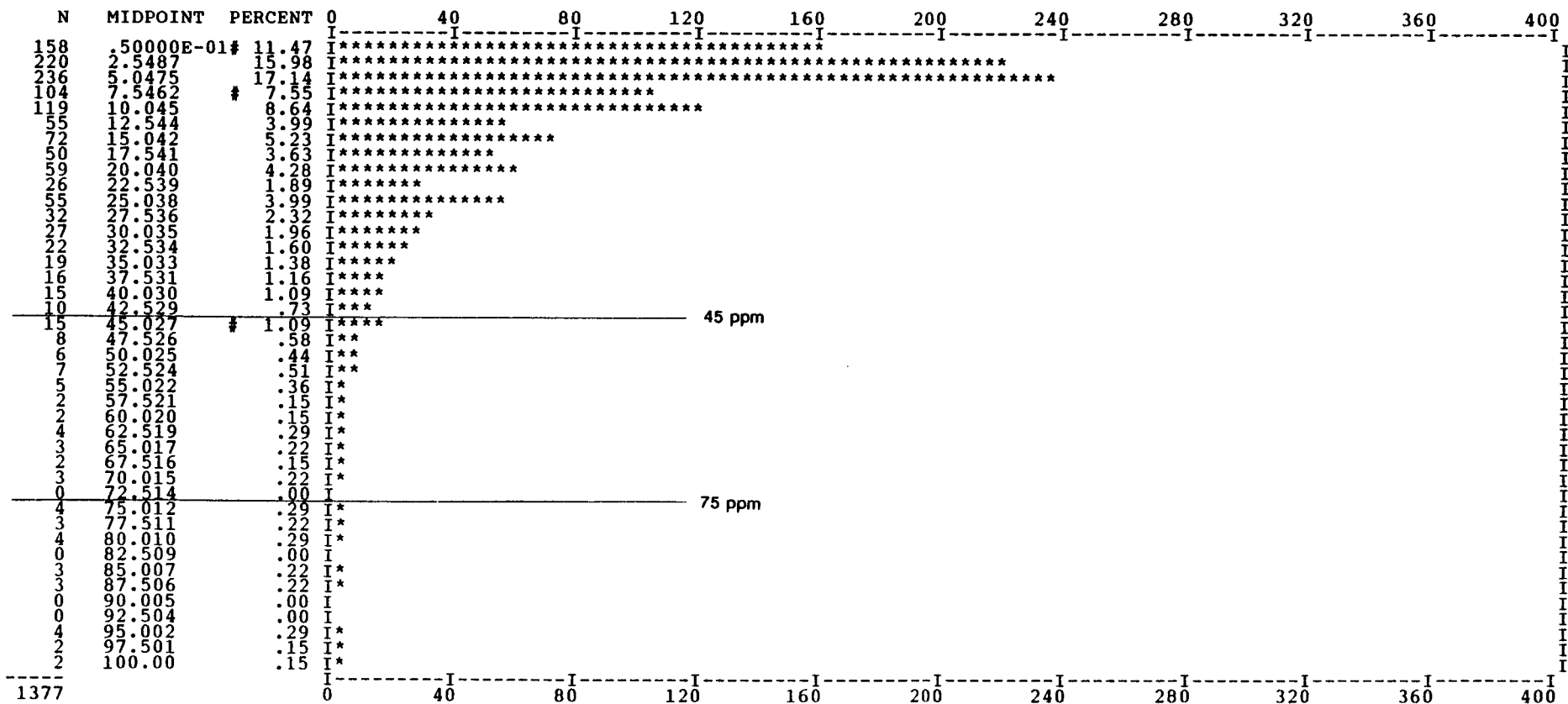
Field name: AS LOG = 0 REPVAL = .00100

1452 SAMPLES WITH AS MINIMUM: .500000E-01 MAXIMUM: 870.000

1377 VALUES PLOTTED: 75 NOT IN RANGE .500000E-01 to 100.000

MEAN: 14.0488 STD. DEV.: 16.4417

SCALE OF HISTOGRAM IS 4.00 COUNTS /PRINT POSITION # = 5,50,95%



1377

HISTO:

SPRING ROCKS 1988 AND 1989 PROGRAMS

RUN ON 89:10:30 AT 13:05:10

File: statrcks.89

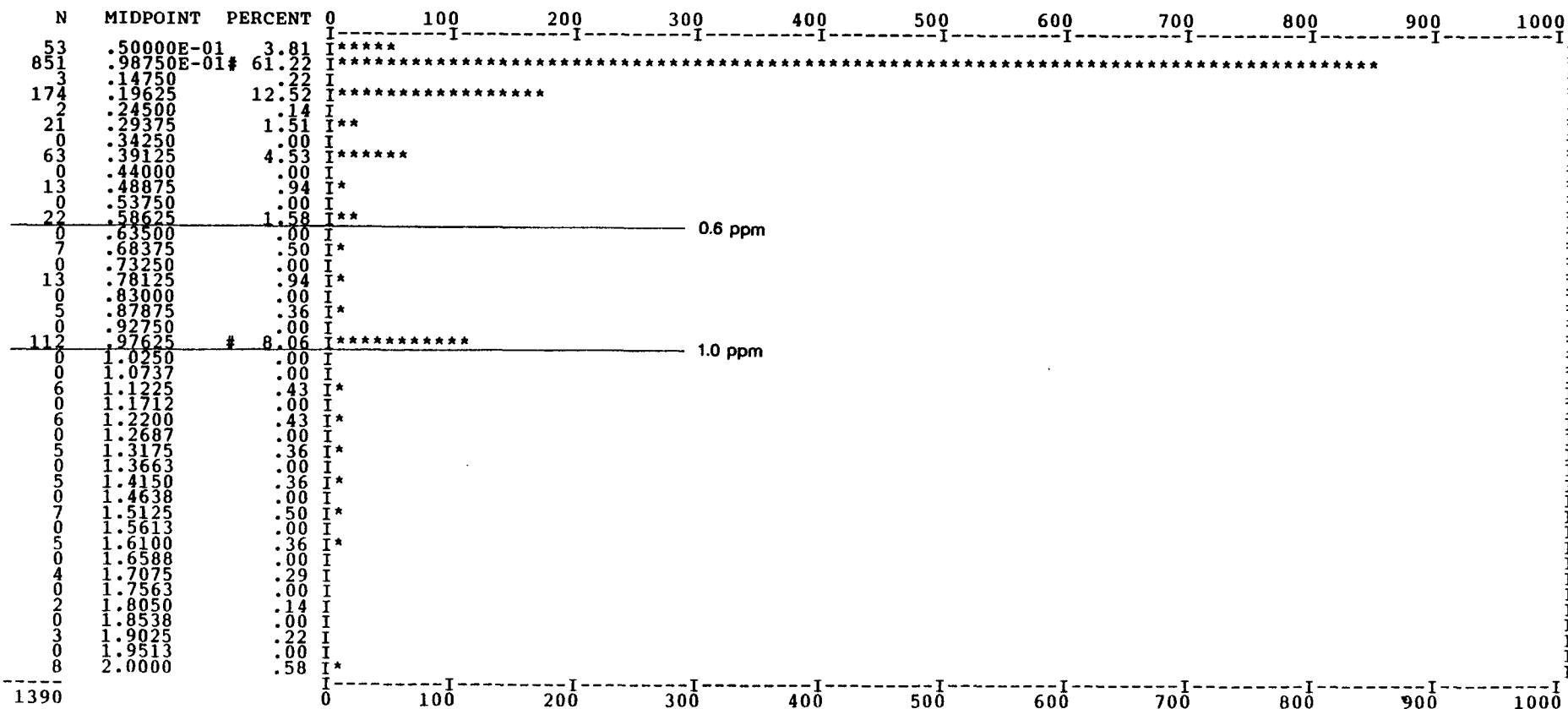
Field name: SB LOG = 0 REPVAL = .00100

1449 SAMPLES WITH SB MINIMUM: .500000E-01 MAXIMUM: 17.0000

1390 VALUES PLOTTED: 59 NOT IN RANGE .500000E-01 to 2.00000

MEAN: .276550 STD. DEV.: .363957

SCALE OF HISTOGRAM IS 10.00 COUNTS /PRINT POSITION # = 5,50,95%



**APPENDIX IV**

**Trench Logs**

## LOGGING CODE EXPLANATION

Column 1 is a key which indicates the type of data or information on each line.

I - Identity information/data  
S - Survey data  
/ - Upper tier geologic data  
L - Lower tier geologic data  
R - Free form remarks  
A - Assay and analysis data

### I DATA

Each trench has two I lines at the start.

The first line indicates:

Col. 11 to 16 - ID of Project  
Col. 17 to 24 - Trench Name  
Col. 29 to 35 - Day/Month/Year Logged  
Col. 36 to 38 - Logger's Initials  
Col. 39 to 41 - Helper's Initials (if any)  
Col. 60 to 62 - Coordinate system  
Col. 63 to 68 - Grid Azimuth (0.0 if True North)

The second line indicates.

Col. 5 to 45 - Company Name  
Col. 46 to 69 - Property or Project or Sub Project Name

### S DATA

The S000 line is the collar survey data. Subsequent S Lines (S001, S002, etc.) are down-the-trench surveys.

Col. 5 to 10 - From (a decimal point is inferred between column 8 and 9)  
Col. 11 to 16 - To (a decimal point is inferred between column 14 and 15)  
Col. 17 to 18 - Units; MT (metres), FT (feet)  
Col. 20 to 26 - Total Length  
Col. 27 to 32 - Azimuth  
Col. 33 to 38 - Dip  
Col. 51 to 60 - Northing  
Col. 61 to 70 - Easting  
Col. 71 to 80 - Elevation

## Logging Code Explanation, continued

### / AND L DATA

Two lines are available to describe a geologic interval, the upper line (/) and the lower line (L). The /NAM line defines the mineral fields for the upper line.

#### ST Geocode - upper (/NAM) line

Col. 57, 58 SI - Silicious  
Col. 59, 60 CY - Clay  
Col. 61, 62 KA - Kaolin  
Col. 63, 64 CB - Carbonates, general  
Col. 65, 66 CL - Chlorite  
Col. 67, 68 PY - Pyrite  
Col. 69, 70 CP - Chalcopyrite  
Col. 71, 72 CG - Galena  
Col. 73, 74 SL - Sphalerite

#### ST Geocode - Lower (LNAM) Line

Col. 57, 58 LE - Limonite  
Col. 59, 60 PL - Pyrolusite  
Col. 61, 62 HE - Hematite  
Col. 63, 64 MG - Magnetite

#### Upper (/) Geologic Data

Col. 5 to 10 - From (decimal inferred between 8 and 9)  
Col. 11 to 16 - To (decimal inferred between 14 and 15)  
Col. 24 to 27 - Rock Type Code - See Rock Type Chart  
Col. 28 to 29 - Typifying Mineral 1 - see Mineral Chart  
Col. 30 to 31 - Typifying Mineral 2 - see Mineral Chart  
Col. 32 to 33 - Main Rock Forming Mineral 1 - See Mineral Chart  
Col. 34 - Rock Forming Mineral Field, Amount of Occurrences, See G Scale Chart  
Col. 35 to 36 - Texture 1 - see Texture Chart  
Col. 37 to 38 - Texture 2 - see Texture Chart  
Col. 47 - Essentially always a "P" which stands for Principle Geologic Interval. If "D", it stands for Ditto Interval which means all of the above interval description applies, except as noted.  
Col. 49 to 50 - Structure 1 - see Structure Chart  
Col. 51 to 53 - Azimuth of Structure 1.  
Col. 54 to 56 - Dip of Structure 1.  
Col. 57 - Mineral Field, Mode of Occurrence - See H Scale Chart  
Col. 58 - Mineral Field, Amount of Occurrence - See G Scale Chart



## Logging Code Explanation, continued

Col. 59 to 74 - Mineral Fields, same pattern continues (ie. G. Scale How, Amount) as in columns 57, 58.

### Lower (L) Geologic Data

Col. 28 to 29 - Colour Code - See Colour Chart  
Col. 30 to 31 - Typifying Mineral 3 - See Mineral Chart  
Col. 32 to 33 - Main Rock Forming Mineral 2 - See Mineral Chart  
Col. 34 - Rock Forming Mineral Field - Amount of Occurrence - See G Scale Chart  
Col. 35 to 36 - Texture 3 - see Texture Chart  
Col. 43 - Count of Fractures at Steep Angle to Trench Axis - See F Scale  
Col. 44 - Count of Fractures at Medium Angle to Trench Axis - See F Scale  
Col. 45 - Count of Fracture at Low Angle to Trench Axis - See F Scale  
Col. 49 to 50 - Structure 2 - See Structure Chart  
Col. 51 to 53 - Azimuth of Structure 2  
Col. 54 - Dip of Structure 2  
Col. 55 to 56 - Angle to Core Axis of Structure 2  
Col. 57 to 64 - Mineral Fields, as in upper (/) Data

Note: Columns 43 to 46 not always used

### R DATA

These are free form remarks written by the logger to further describe the geologic interval. Note that Rock Type Codes (see Rock Type Charts are often used.

### A DATA

This last type of data lists the assay information for the trench.

Note that remarks are also used.

The first line, A001, defines a "set" of chip samples. A002 defines grab samples. A003 defines extra samples taken along structures (i.e. fault gouges, etc.). A004 defines repeat sample taken along specific intervals. The following lines describe and list the assay data.

ALAB Col. 17 to 80 - Define Laboratory  
ATYP Col. 17 to 30 - Define Type of Determination  
AUMM Col. 17 to 80 - Define Assay Fields  
A00? Col. 1 to 4 - Defines Sample Type

## Logging Code Explanation, continued

A001 Col. 5 to 10 - From (decimal inferred between 8 and 9)  
Col. 11 to 16 - To (decimal inferred between 14 and 15)  
Col. 17 to 20 - Sample Length  
Col. 21 to 26 - Sample Number  
Col. 27 to 32 - Gold ppb  
Col. 33 to 38 - Silver ppm  
Col. 39 to 44 - Copper ppm  
Col. 45 to 50 - Lead ppm  
Col. 51 to 56 - Zinc ppm  
Col. 57 to 62 - Arsenic ppm  
Col. 63 to 68 - Antimony ppm

## CHARTS

### 1. Rock Type Chart

A four letter code is used to describe rock types. The first four letters of a rock type name is its preferred code. If the fourth letter is a vowel, the vowel is replaced by the next consonant.

#### Letter Code

#### Lithology

OVBN	Overburden
PPFQ	Porphyry Feldspar Quartz
PPFX	Porphyry Feldspar
PPQZ	Porphyry Quartz
AN/D	Andesite Dyke
BRFQ	Breccia Feldspar Quartz
FAUL	Fault (Sampled Gouge)
GNIS	Gneiss
GRAN	Granite
MONZ	Monzonite
MTSD	Metasediments
QZMZ	Quartz Diorite
QBGN	Biotite Quartz Gneiss
CGGN	Coarse Grained Gneiss
DYKE	Fine Grained Dyke Rock
VEIN	Vein
TILL	Till
BQMZ	Biotite Quartz Monzonite
QZDR	Quartz Diorite

Logging Code Explanation, continued

2. Mineral Chart (ie. Mineral short-forms)

PY - Pyrite  
SL - Sphalerite  
GL - Galena  
PO - Pyrrhotite  
CP - Chalcopyrite  
CL - Chlorite  
EP - Epidote  
MG - Magnetite  
BI - Biotite  
MS - Sericite  
CB - Carbonate  
LI - Limonite  
SI - Silicification  
PL - Pyrolusite  
MM - Manganese  
CY - Clay  
PF - Plagioclase  
HE - Hematite  
KA - Kaolinite  
QZ - Quartz  
FX - Feldspar  
KF - Orthoclase Feldspar  
HB - Hornblende  
PH - Phlogopite

3. Texture Chart (ie. Texture Short Forms)

BN - Banded  
BD - Bedded  
BR - Brecciated  
QV - Quartz Veins  
SH - Shear Zone  
MX - Massive  
<< - Microveins  
>> - Macroveins  
FZ - Fault

Logging Code Explanation, continued

4. Structure Chart (ie. Structure Short-Forms)

SC Schist  
BN Banded  
PH - Phyllite  
MX - Massive  
WB - Wavey Bands  
FZ - Fault or Shear Zone  
<< - Microveins  
>> - Macroveins  
VG - Vuggy  
LM - Laminated  
BR - Brecciated  
PP - Porphyritic  
EQ - Equigranular  
SH - Shear  
R2 - Slightly Reworked  
R5 - Mod. Reworked  
R7 - Strongly Reworked  
RW - Reworked  
AG - Augen Structured  
SK - Stockworked  
GT - Granitic

Logging Code Explanation, continued

5. How Chart or H Scale

<u>Symbol</u>	<u>Most Dominant Mode of Occurrence</u>
A	Amygdaloids, cavity fillings
B	Blebs
#	Breccia Fillings
C	Coatings & Encrustations
*	Clasts
D	Disseminations & Scat.x'ls
E	Envelopes
F	Framework Crystals
G	Gouge
H	Halos
I	Eyes, Augen
J	Interstitial
K	Stockwork
L	Laminated/bedded
M	Massive
N	Nodules
O	Spots
Q	Patches, as in quilts'
R	Rosettes & x'tls clusters
S	Selvages
\$	Sheeting
T	Stainings, as in tarnish
U	Euhedral
V	Veins
>	Macroveins
<	Microveins
W	Boxwork
X	Massive and/or laminated/bedding
Y	Dalmationite
Z	Fresh, primary rock
+	Flooding

Logging Code Explanation, continued

<u>Symbol</u>	<u>Description</u>
0	Fresh, primary rock(Z) (z for Zero)
1	Amygdaloids(A), minor Macroveins(>) and/or scattered Crystals(D)
2	Macroveins(>) and Veins(V)
3	Veins(V) and Dalmationite(Y) -Spots(O) or Patches(Q) (as in Quilts)
4	Veins(V), and/or occasional Envelopes(E)
5	Veins(V), and/or abundant Envelopes(E)
6	Pervasive(P) or Disseminations (D) less than Veins(V), Microveins(<), Selvages(S), Envelopes(E)
7	Pervasive(P) or Disseminations (D) equal to Veins(V), Disseminations(D) equal to Veins(V), Microveins(<), Selvages(S), Envelopes(E)
8	Pervasive(P) or Disseminations (D) greater than Veins(V), Microveins(<), Selvages(S), Envelopes(E)
9	Pervasive(P) or Disseminations (D), Veins(V), Microveins(<) Selvages(S) and Envelopes(E) with much Breccia filling (#), Stockwork(K) and/or Sheeting(\$)
X	Massive(M) and/or Laminated/Bedded(L)

Logging Code Explanation, continued

6. G Scale or Amount Chart

<u>Code</u>	<u>Assigned Value</u>	<u>Range</u>
X	100	100 %
9	90	85 to 99
8	80	75 to <85
7	70	65 to <75
6	60	55 to <65
5	50	45 to <55
4	40	35 to <45
3	30	25 to <35
2	20	15 to <25
1	10	7 to <15
=	5	4 to < 7
+	3	2 to < 4
)	1	.5 to < 2
*	.3	.2 to <.5
(	.1	.05 to <.2
-	.03	.02 to <.05
.	.01	Trace = <.02
0	0	Nil, Absent
/	.07	Present: Estimate impossible
?	0	Possibly Present

## Logging Code Explanation, continued

### 7. Colour Chart

The colour chart can be used in two ways. A lightness can be combined with colour, or two colours can be combined.

eg. 3U - Dark Brown  
or  
RU - Reddish Brown

<u>Lightness</u>		<u>Colour</u>	
<u>Symbol</u>	<u>Value</u>	<u>Symbol</u>	<u>Colour</u>
9	palest	R	Red
8	pale	U	Brown (Umber)
7	light	O	Orange
6	lighter	T	Tan (khaki)
5	medium	Y	Yellow
4	darker	L	Lime (Y-G)
3	dark	G	Green
2	very dark	Q	Aqua (B-P)
1	darkest	B	Blue
		V	Violet (B-P)
		P	Purple
		M	Mauve
		W	White
		A	Grey
		N	Black (Noir)

### 8. F Scale or Fractures and Joints Intensity Chart

<u>Range</u>	<u>Assigned</u>	<u>Symbol</u>	<u>Description</u>
<u>Values</u>	<u>Values</u>		
	0	0	Unfractured
0 - 2	1	1	Extremely low intensity
2 - 4	3	2	Very low intensity
4 - 8	6	3	Low intensity
8 - 12	10	4	Moderately low intensity
12 - 18	15	5	Moderate
18 - 24	21	6	Fairly high intensity
24 - 32	28	7	High intensity
32 - 40	36	8	Very intense
40 - 50	45	9	Extremely intense
> 50	55	X	Shattered



TRENCH 0785E

-----  
 IDEN6B0201 232TR0785E 12JUN89MJDRGM UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 250 MT 56.0 162.0 -4.0 705.0 785.0 1310.00  
 S001 250 560 56.0 151.0 -2.0

R From To  
 R THIS TRENCH TESTS AN IP ANOMALY EXTENDING FROM 550N TO 650N.  
 / 00 30 OVBN P  
 / 30 90 PPFQ FX2PP P P1F1 J\* D)  
 L TA QZ= C+  
 / 90 105 PPFQ QZ+ P P)P5 D)  
 L WA FX+ C1<1  
 / 105 120 PPFQ FX1PPVG P P)P5 D)  
 L AU QZ+ C1<\*  
 / 120 135 PPFQ FX3PP P J3C1 J\* D)  
 L AW QZ+ C)<)  
 / 135 265 PPFQ FX2PP P J3C) D)  
 L AW QZ1 C1C)  
 / 265 285 PPFQ QZ4PP P J4D3 D)  
 L AW FX2  
 R MARKED DIFF IN CLAY ALT. "WHITE ZONE" REMOB OF QZ INTO MATRIX  
 / 285 300 PPFQ FX2PP P J3C2 D\*  
 L AW QZ2 C3  
 / 292 293 XFAUL QZ1 D SH020 P8  
 L BA P1  
 / 300 370 PPFQ FX2PP P J2C) D+  
 L AW QZ= P2  
 / 370 425 OVBN P  
 / 425 530 PPFQ FX4PP P J3C+ D+  
 L WA QZ) C+C+  
 / 530 560 OVBN P

R THIS TRENCH ENDED AS IT APPROACHED THE CREEK AT L790E 649N

A001

AUMM	LNG SAMPLE		Au	Ag	Cu	Pb	Zn	As	Sb		
R	From	To	ppb	ppm	ppm	ppm	ppm	ppm	ppm		
ALAB Echo Tech - Kamloops											
ATYP Chip Samples											
R	00	30	No Sample - OVBN								
A001	30	45	1.5	42873	3	.1	2	2	28	3	.1
A001	45	60	1.5	42913	3	.1	9	9	33	2	.4
A001	60	75	1.5	42914	3	.1	3	12	20	2	.1
A001	75	90	1.5	42915	3	.1	9	34	52	2	.1
A001	90	105	1.5	42874	3	.2	13	68	132	4	.2
A001	105	120	1.5	42875	3	.6	16	52	131	8	.1
A001	120	135	1.5	42886	3	.3	12	23	69	3	.1
A001	135	150	1.5	42887	3	.1	5	12	61	1	.1
A001	150	165	1.5	42888	3	.3	4	24	55	1	.1
A001	165	180	1.5	42889	3	.8	3	34	50	1	.1
A001	180	195	1.5	42890	3	.1	4	7	55	2	.1
A001	195	210	1.5	42891	3	.1	2	2	56	4	.1

A001	210	225	1.5	53590	3	.4	8	28	79	3	.9
A001	225	240	1.5	53591	3	.2	7	24	39	5	1.6
A001	240	255	1.5	53592	3	.2	5	40	35	3	1.4
A001	255	265	1.0	53593	3	.1	6	47	35	3	1.2
A001	265	275	1.0	53594	3	.8	5	36	17	2	1.7
A001	275	285	1.0	53595	3	1.1	7	76	54	5	1.5
A001	285	300	1.5	53596	3	.5	3	142	83	4	1.8
A001	300	315	1.5	53597	3	.4	7	70	62	3	1.0
A001	315	330	1.5	42900	3	.1	6	5	64	2	.1
A001	330	345	1.5	42902	3	.1	5	25	77	2	.1
A001	345	360	1.5	42903	3	.3	6	30	58	1	.1
R	360	425	No Sample - OVBN								
A001	425	440	1.5	42904	3	.1	5	37	69	2	.1
A001	440	455	1.5	42905	3	.2	6	62	95	2	.1
A001	455	470	1.5	42906	3	.2	5	16	29	3	.1
A001	470	485	1.5	42907	3	.1	6	9	29	2	.1
A001	485	500	1.5	42908	3	.1	2	1	25	2	.1
A001	500	515	1.5	42909	3	.3	5	28	32	3	.1
A001	515	525	1.0	42910	3	.1	4	10	38	3	.1
R	525	560	No Sample - OVBN								
R	END OF A001 Samples										

A002											
AUMM	LNG SAMPLE			Au	Ag	Cu	Pb	Zn	As	Sb	
ALAB	Echo Tech - Kamloops										
ATYP	Grab Samples										
A002	55	55	59051	5	1.5	7	153	143	11	.1	
R	Grab sample of PPFQ w. 10% diss. PY										
A002	117	117	42872	3	.1	6	32	61	6	.1	
R	Grab sample of PPFQ w. 15% diss. PY and weak carbonate alt.										
A002	322	322	42901	3	.1	3	2	40	2	.1	
R	Grab sample of LI stained,high SI alt,10% diss.PY,mod.clay alt,1-2% celadonite.										
A002	410	410	59502	3	.1	5	21	34	6	.1	
R	Representative grab sample of PPFQ										
A002	463	463	42911	3	0.1	4	16	31	3	.1	
R	Grey-white alt'd PPFQ w. fine-gr.fresh & oxydized,10% diss py										
A002	500	500	59053	5	1.5	12	284	186	7	.2	
R	PPFQ w. 20% diss py and 20% pervasive clay alt.										
A002	517	517	42912	3	0.1	6	8	27	1	.1	
R	Grey-white,mod. clay alt'd PPFQ w. 10%,coarse diss py										
A003											
AUMM	LNG SAMPLE			Au	Ag	Cu	Pb	Zn	As	Sb	
ALAB	Echo Tech - Kamloops										
ATYP	Extra Samples Taken Along Structures, Etc.										
A003	292	293	42898	3	8.2	24	393	668	4	.1	
R	Sample taken along fault gouge striking at 020,minor diss py										
/END											

TRENCH 0825E

-----

IDEN6B0201 V232TR0825E 16JUN89RGM UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 1430MT 30.00160.00 0.00 580.0 825.0 1300.00  
 S001 1430 2320 30.00135.00-03.00  
 S002 2320 3000 30.00130.00-21.00

R From To  
 R THIS TRENCH TESTS AN IP ANOMALY EXTENDING FROM 550N TO 650N.  
 / 00 58 PPFQCY QZ3PPR5 P P3P2 D2  
 L AW FX4 C1C+  
 R EXTREME REMOB.OF SI,EMPLACEM.OF PY BLEBS,MIXING OF SI AND KF  
 / 05 10 XFAUL CYXR7 D PX  
 / 58 143 BQMZBIPFQZ2EQR2 P P2 D2D)  
 L 3AKFFX5 D2P2P2  
 / 143 300 PPFQCY QZ3PPR5 P J3P2 D1U2 D)  
 L AW FX4 C1C+<1  
 R ESSENTIALLY THE SAME ROCK AS PGI 0.0 to 5.8  
 R CL ALT IS FROM PRIMARY BI  
 R PY OCCURS AS MICROVEINS & DISS. IN ALL INTERVALS  
 R TRENCH ENDS DUE TO STEEPLY DIPPING BEDROCK AND DEEP OVBN

A001

AUMM	From	To	LNG SAMPLE	AU ppb	AG ppm	CU ppm	PB ppm	ZN ppm	AS ppm	SB ppm
ALAB	Echo Tech - Kamloops									
ATYP	Chip Samples									
A001	00	15	1.5 43051	3	.1	5	49	147	7	.1
A001	15	30	1.5 43053	3	.1	10	104	319	9	.5
A001	30	45	1.5 43054	3	.5	8	210	474	34	.1
A001	45	60	1.5 43055	3	1.3	16	401	712	32	1.2
A001	60	75	1.5 43056	3	.9	9	315	1200	39	1.5
A001	75	90	1.5 43057	3	.3	7	145	523	33	1.5
A001	90	105	1.5 43058	3	.1	14	97	372	15	.9
A001	105	120	1.5 43059	3	.1	12	63	278	12	.5
A001	120	135	1.5 43060	3	.1	9	107	447	20	.7
A001	135	150	1.5 43061	3	1.3	14	321	1100	37	1.5
A001	150	165	1.5 43062	3	.4	11	138	530	38	1.2
A001	165	180	1.5 43063	3	.2	9	92	481	26	.8
A001	180	195	1.5 43064	3	1.5	16	298	989	24	.1
A001	195	210	1.5 43065	3	2.3	18	301	1500	21	1.1
A001	210	225	1.5 43066	3	1.9	18	168	1900	9	.7
A001	225	240	1.5 43067	3	.4	9	90	1100	7	.5
A001	240	255	1.5 43068	3	.9	11	171	1100	6	.5
A001	255	270	1.5 43069	3	.7	8	135	927	9	.5
A001	270	285	1.5 43070	3	.8	9	211	1200	5	.6
A001	285	300	1.5 43071	3	.9	10	173	1300	7	.5

A002

AUMM	From	To	SAMPLE	Au	Ag	Cu	Pb	Zn	As	Sb
ALAB	Echo Tech - Kamloops									
ATYP	Grab Samples									
A002	100	100	43073	3	.2	4	74	477	6	.6

R														
				Grab sample of hematite rich, dark intrusive										
A002	280	280	43074	3	.8	8	202	706	4				.3	
R				Grab sample of reworked PPFQ w. 20% diss.PY										
A003														
AUMM			LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB				
ALAB			Echo Tech - Kamloops											
ATYP			Extra Samples Taken Along Structures, Etc.											
A003	5	10	0.5 43072	3	.2	3	85	239	5				.4	
R			Sample along fault gouge w. extreme clay alt.											
A004														
AUMM			LNG SAMPLE	Au	Ag	Cu	Pb	Zn	As	Sb				
ALAB			Echo Tech - Kamloops											
ATYP			Repeat samples taken along intervals											
A004	0	15	1.5 43052	3	.1	3	19	79	8				.3	
R			Re-sample of 43051											
/END														

TRENCH 0842E

-----  
 IDEN6B0201V232 TR0842E 13JUN89MJDRGM UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG

/SCL MT.2  
 LSCL LCTM  
 S000 00 233 MT 40.0 160.0 -10.00 700.0 842.0 1305.00  
 S001 233 400 40.0 160.0 -15.00

R From To  
 R THIS TRENCH WAS DUG TO TEST AN IP ANOMALY FROM 550N TO 650N

/ 00 10 OVBN P  
 / 10 25 PPFQ FX2PP P P4F1 D=  
 L AW QZ1 C1  
 / 25 73 PPFQ FX1 P SH P5 D)  
 L RO QZ1 C3P1C+  
 / 32 32 XFAUL QZ1 D SH040 75 P8  
 L BA C1  
 / 44 44 XFAUL QZ1 D SH040 30 P8  
 L BA C1  
 / 73 81 PPFQ FX3PP P P2F2 W1  
 L AW QZ1 C1  
 / 81 90 PPFQ QZ2PP P SH P5 B+  
 L RO FX1 P2 C+

R STRONGLY WEATHERED AND RUSTED PPFQ  
 / 90 102 PPFQ FX4PP P P1F2 D+  
 L AW QZ1 C=  
 / 102 118 PPFQ FX4PP P P1F2 D=  
 L AW QZ2 C=  
 / 118 233 PPFQ FX4PP P P3F1 D)  
 L AW QZ1 C+ O=

R MED GRND PPFQ MOD. TO STRONGLY SILICIFIED & CLAY ALT MATRIX  
 / 130 145 XPPFQ QZ1 D SH P6 D\*  
 L BW P3  
 / 190 200 XPPFQ FX3PP D P3F2 D+  
 L AW QZ2 C+  
 / 233 233 XFAUL QZ1 D SH035 P6  
 L OA P3 P+  
 / 233 385 PPFQ FX3PP P P4F2 D=  
 L AW QZ1VG C=

R AT 270 FX PHENOS BECOME MORE PROMINENT, RANGING ABOUT 20%  
 R BETWEEN 27.5-28.5, LI OCCURS AS COATINGS IN THE 10% RANGE.  
 / 340 340 XFAUL QZ1 D SH090 P6  
 L BA P3  
 / 385 400 OVBN P

R THIS TRENCH ENDS DUE TO DEEP OVBN; STEEP DIPPING BR.

A001  
 AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
 R From To ppb ppm ppm ppm ppm ppm ppm

ALAB Echo Tech - Kamloops  
 ATYP Chip Samples

R 00 10 No Sample - OVBN  
 A001 10 25 1.5 42916 5 .1 6 11 57 3 .1  
 A001 25 40 1.5 42917 3 .1 5 15 80 3 .1

A001	40	55	1.5	42919	3	.1	5	10	49	6	.1
A001	55	70	1.5	42921	3	.6	5	92	137	15	.3
A001	70	85	1.5	42922	3	.3	4	87	62	8	.2
A001	85	100	1.5	42923	3	.9	4	73	86	12	.2
A001	100	115	1.5	42924	3	.1	4	28	63	13	.1
A001	115	130	1.5	42925	3	.1	3	38	83	15	.1
A001	130	145	1.5	42976	3	.1	3	48	51	9	.1
A001	145	160	1.5	42977	3	.1	3	17	32	6	.1
A001	160	175	1.5	42978	3	.2	6	62	40	6	.1
A001	175	190	1.5	42979	3	.6	7	69	50	7	.1
A001	190	205	1.5	42980	3	.1	4	22	35	6	.1
A001	205	220	1.5	42981	3	.1	6	41	39	6	.1
A001	220	235	1.5	42982	3	.4	5	89	57	5	.1
A001	235	250	1.5	42984	3	.2	3	75	78	6	.1
A001	250	265	1.5	42985	3	.3	6	60	90	7	.1
A001	265	280	1.5	42986	3	.7	3	38	55	6	.1
A001	280	295	1.5	42987	3	.1	2	12	50	6	.1
A001	295	310	1.5	42988	3	.1	2	12	42	5	.1
A001	310	325	1.5	42989	3	.1	3	24	57	6	.1
A001	325	340	1.5	42990	3	.1	2	31	62	6	.1
A001	340	355	1.5	42991	3	.1	1	8	38	5	.1
A001	355	370	1.5	42992	3	.1	1	27	57	5	.1
A001	370	385	1.5	42993	3	.1	1	23	61	3	.1
R	385	400	No Samples - OVBN								

A002

AUMM SAMPLE Au Ag Cu Pb Zn As Sb

ALAB Echo Tech - Kamloops

ATYP Grab Samples

A002 10 10 43028 3 .5 2 42 74 10 .1

R Grab sample showing grey/white,mod.clay alt.,mod. sil'd PPFQ  
R w.5% diss.PY

A002 85 85 43032 3 .3 1 42 60 5 .1

R Limonite stained,clay alt'd PPFQ w.5% diss. PY

A002 105 105 43031 3 .1 2 22 46 5 .1

R Grab sample showing 10% diss.PY & fracture filling PY in PPFQ

A002 235 235 43030 3 .1 1 31 63 14 .1

R Grey-green,strongly clay sil'd PPFQ w. coarse euhedral,clay  
R alt.FX & 5% PY

A002 270 270 43029 3 .1 2 17 22 5 .1

R Same as 43030

A003

AUMM LNG SAMPLE AU AG CU PB ZN AS SB

ALAB Echo Tech - Kamloops

ATYP Extra Samples Taken Along Structures, Etc.

A003 28 28 1.5 42918 3 .2 3 65 169 8 .1

R Fault gouge trending 050,extreme clay alt.

A003 43 43 1.0 42920 3 .3 8 60 71 7 .1

R Fault gouge,same as 42918

A003 233 233 1.0 43026 3 .1 7 153 197 4 .1

R Fault gouge w. extreme clay alt.and rust staining in a PPFQ

A003 340 340 1.0 43027 3 .2 2 53 84 3 .1

R Fault gouge,same as 43026

A004

AUMM LNG SAMPLE Au Ag Cu Pb Zn As Sb

ALAB Echo Tech - Kamloops

ATYP Repeat samples taken along intervals

A004 220 235 1.5 42983 3 .1 2 35 40 5 .2  
R Sample 42983 is a re-sample of 42982  
/END

TRENCH 0858E

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IDEN680201 V232TR0858E 19JUN89RGMMD utm340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG

/SCL MT.2  
 LSCL LCTM  
 S000 00 335 MT 33.5 164.0 -04.0 807.0 858.0 1314.00

R From To  
 R THIS TRENCH WAS TO TRACE A PROMINENT ALTERATION ZONE PROJECTING  
 R FROM TR0842E AND TO TEST A GOLD-IN-SOIL ANOMALY

/ 00 165 PPFQLICYQZ4PPR5 P P4 C1 D+  
 L WA FX4 C2 O)

/ 15 30 XOVBN D  
 / 165 183 PPFQ QZ6PPR7 P P6 C2 D+  
 L 7A FX3 C2

/ 183 335 PPFQLICYQZ4PPR5 P P4 C1 D+  
 L WA FX4 C2 O)

R THIS INTERVAL IS ESSENTIALLY SAME ROCK TYPE AS PGI 0.0-16.5

R 150 165 EXTREME WEATHERING IN BEDROCK TROUGHS

R 183 217 WEATHERING RIND SHOWS BREAKDOWN OF MAFICS TO CHLORITE SPOTS

/ 200 208 XOVBN D

/ 228 238 XOVBN D

R THIS TRENCH ENDS DUE TO A SHARP DIP IN THE BEDROCK

A001

AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
 R From To ppb ppm ppm ppm ppm ppm ppm

ALAB Eco Tech - Kamloops  
 ATYP Chip Samples

A001 00 15 1.5 53201 3 .1 4 31 37 7 .2  
 R 15 30 No Sample - OVBN

A001 30 45 1.5 53202 3 .1 5 39 46 6 .2

A001 45 60 1.5 53203 3 .1 5 21 21 5 .1

A001 60 75 1.5 53204 3 .1 6 38 50 6 .1

A001 75 90 1.5 53205 3 .1 7 44 44 5 .1

A001 90 105 1.5 53206 3 .1 6 38 36 4 .1

A001 105 120 1.5 53207 3 .1 4 28 31 4 .1

A001 120 135 1.5 53208 3 .1 4 26 41 7 .1

A001 135 150 1.5 53209 3 .1 12 34 52 7 .1

A001 150 165 1.5 53210 3 .1 7 53 91 9 .2

A001 165 183 1.8 53211 15 .1 6 26 33 14 .1

A001 183 200 1.7 53212 3 .1 7 37 38 9 .2

R 200 208 No Sample - OVBN

A001 208 218 1.0 53213 5 .1 4 22 20 7 .1

A001 218 228 1.0 53214 3 .1 3 18 12 3 .1

R 228 238 No Sample - OVBN

A001 238 253 1.5 53215 5 .1 7 55 52 6 .1

A001 253 265 1.2 53216 10 .1 3 26 26 11 .1

A001 265 280 1.5 53217 5 .1 4 18 10 4 .1

A001 280 295 1.5 53218 3 .1 3 22 12 8 .1

A001 295 310 1.5 53219 3 .1 3 23 7 7 .1

A001 310 320 1.0 53220 5 .1 2 20 15 6 .1

A001 320 335 1.5 53221 3 .1 3 17 7 5 .1

/END



TRENCH 1010W

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IDEN680201V232 TR1010W 30JUN89RGMMD UTM340.0

IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT

/NAM SICYKACBCLPYCPGLSL

LNAM LIPLHEMG

/SCL MT.2

LSC LCTM

S000	00	225	MT	98.0	170.0	-04.0		-1065.0	-1010.0	1315.00
S001	225	310		98.0	170.0	015.0				
S002	310	655		98.0	170.0	03.0				
S003	655	980		98.0	165.0	-12.0				

R From To

R THIS TRENCH WAS DUG TO TEST A 100M GOLD-IN-SOIL ANOMALY

/ 00 155 PPFQZ FX4PPAG P MX P2 D\*

L AG KF3RW <(T)

R FRESH, COARSELY-GR. PPFQ IN A FINER-GR. FELDSPATIC MATRIX. KF

R PHENOS OCCUR AS EUHEDRAL X-TALS UP TO 3 CM. QZ EYES REACH 1.5 CM

R WEATHERING COLOUR IS LIGHT GREENISH (KF ALT.) & RUSTY-BROWN (LI)

/ 155 284 QZDRBIKFFX5EQPP 5 P P2C\* D=<

L GA Q2RWSK C1

R WEATHERED EQUIGRANULAR QZ-DIORITE, MOD. SILIC, D W. DARK ORANGE-

R BROWN COATINGS & FRACT. FILLINGS. QZ X-TALS OCCUR AS SMALL EYES

R OR AS MICROVEINS CONTAINING 1% PY.

/ 224 242 XQZDR Q22EQ D SH034 J5

L FX2 C2 O=

R STRONGLY CLAY-ALT'D & WEATHERED SHEAR ZONE IN QZDR

R CONTACT OCCURS AT 28.4M, STRIKING AT 130 DEGREES

/ 284 400 PPFQZ FX4PPSH P MX P2 D\* D+

L AG KF3RWAG 45 <(T)

R SIMILAR ROCK UNIT AS 0.0-15.5, BUT MORE FRACT. & SLICK'SLIDE TEXT

/ 400 405 XFAUL Q22 D SH085 P7

L WU C1T)

R EXTREMELY CLAY ALT'D FAULT GOUGE WHERE CONTACT OCCURS W. QZDR

/ 400 646 QZDRBIKFFX5EQPP 57 P P=T+

L WG Q22 C=T) D=D)

R SIMILAR ROCK UNIT AS 15.5-28.4 BUT LESS SIL'D, >BI, >LI, >ALT.

/ 431 434 XFAUL Q22 D SH085 P4

L WU C1T)

R MODERATELY CLAY ALT'D & RUSTY SHEAR ZONE (0.4 M WIDE)

/ 594 597 XQZDR Q22EQ D SH065 P4 O=

L YW FX2 C1 C+

R STRONGLY CLAY-ALT'D QZ-DIORITE W. RUSTY-BROWN WEATHER'G COLOUR

/ 613 619 XQZDR Q22EQ D SH060 P4 O=

L YW FX2 C1 C+

R SAME AS ABOVE

/ 626 646 XQZDR Q22EQ D SH060 P5 O=

L YW FX1 C1 C+

R SAME AS ABOVE

/ 646 980 QZDRBI FX5EQAG 5 5 P P) O1D)

L AU Q22RW C1

R FRESH EQUIGRANULAR, WEAKLY ALT'D QZ-DIORITE W. MINOR DISS. PY

/ 880 980 XQZDRBI FX5EQ<< 7 5 D P+ O1D(

L WG Q22RW T\* C+

R QZ-DIORITE UNIT W. > % OF LARGE FRACTURES; WEAKLY ALT'D; > CHLORITE

R THIS TRENCH WAS DISCONTINUED DUE TO THE EXTENT OF THE SOIL ANOM

A001	AUMM		LNG	SAMPLE	AU	AG	CU	PB	ZN	AS	SB
R	From	To			ppb	ppm	ppm	ppm	ppm	ppm	ppm
ALAB			Eco Tech - Kamloops								
ATYP			Chip Samples								
A001	00	15	1.5	53355	10	.1	3	49	47	6	.1
A001	15	30	1.5	53356	10	.1	2	29	34	1	.1
A001	30	45	1.5	53357	5	.1	3	21	59	1	.1
A001	45	60	1.5	53358	5	.1	5	18	83	1	.1
A001	60	75	1.5	53359	10	.1	4	22	95	5	.1
A001	75	90	1.5	53360	10	.1	4	27	72	3	.1
A001	90	105	1.5	53361	10	.1	3	26	77	4	.1
A001	105	120	1.5	53362	10	.1	4	28	72	1	.1
A001	120	135	1.5	53363	5	.1	3	33	76	4	.1
A001	135	155	2.0	53364	10	.1	3	34	44	6	.1
A001	155	165	1.0	53365	5	.1	4	41	207	5	.1
A001	165	180	1.5	53366	5	.1	4	56	242	1	.1
A001	180	195	1.5	53367	5	.1	5	42	427	2	.1
R	195	210	NO SAMPLE-OVBN								
A001	210	225	1.5	53368	10	3.0	54	159	727	1	.1
A001	225	240	1.5	53369	15	.4	34	33	382	1	.1
A001	240	255	1.5	53370	20	10.5	51	131	338	7	.1
A001	255	270	1.5	53371	5	1.1	15	40	239	5	.1
A001	270	285	1.5	53372	80	.1	6	32	160	1	.1
A001	285	300	1.5	53373	5	.1	4	26	75	3	.1
A001	300	315	1.5	53374	5	.1	5	25	92	5	.1
A001	315	330	1.5	53375	5	.1	3	24	43	1	.1
A001	330	345	1.5	53376	5	.4	13	36	49	5	.1
A001	345	360	1.5	53377	10	.1	4	27	40	4	.1
A001	360	375	1.5	53378	5	.1	4	29	42	4	.1
A001	375	390	1.5	53379	5	.1	4	32	54	5	.1
A001	390	400	1.0	53380	5	.1	4	37	35	15	.1
A001	400	415	1.5	53381	10	.1	7	23	80	5	.1
A001	415	430	1.5	53382	5	.6	14	18	80	6	.1
A001	430	445	1.5	53383	5	.1	11	15	92	5	.1
A001	445	460	1.5	53384	5	.1	12	14	68	3	.1
A001	460	475	1.5	53385	5	.1	13	16	73	4	.1
A001	475	490	1.5	53386	5	.1	10	18	68	5	.1
A001	490	500	1.0	53387	5	.2	11	26	138	4	.1
A001	500	515	1.5	53388	5	.4	10	39	274	4	.1
A001	515	530	1.5	53389	5	.3	9	49	251	8	.1
A001	530	545	1.5	53390	5	.2	11	35	131	7	.1
A001	545	560	1.5	53391	5	.1	8	26	79	4	.1
A001	560	575	1.5	53392	5	.1	9	19	72	6	.1
A001	575	590	1.5	53393	10	.2	13	37	138	4	.1
A001	590	614	2.4	53394	5	.1	13	83	259	2	.1
A001	614	626	1.2	53395	45	.2	16	92	402	2	.1
A001	626	646	2.0	53396	5	.2	28	48	80	3	.1
A001	646	660	1.4	53397	5	.1	10	15	94	1	.1
A001	660	675	1.5	53398	3	.1	14	13	71	1	.1
R	675	715	NO SAMPLE-FRESH ROCK								
A001	715	730	1.5	53408	5	.2	14	15	92	7	.1
R	730	765	NO SAMPLE-FRESH ROCK								
A001	765	780	1.5	53409	5	.3	12	12	86	4	.1
R	780	815	NO SAMPLE-FRESH ROCK								



TRENCH 1335W

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IDEN680201 V232TR1335w 05JUL89RGMJD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG

/SCL MT.2  
 LSCL LCTM  
 S000 00 270 MT 27.0 153.0 -02.0 -1150.0 -1335.0 1310.00

R From To  
 R THIS TRENCH TESTS A MULTI-ELEMENT SOIL ANOMALY OVER 300M  
 / 00 20 OVBN P  
 / 20 207 PPFQPYLQZ4PPR5 P P5C) D+D.  
 L WALIFX3 C\*C\*  
 R SILICA OCCURS AS REMNANT AUGENS AS WELL AS PERVASIVELY IN THE  
 R MATRIX  
 R FELDSPARS ARE REWORKED AND MIXED INTO THE MATRIX IE NO PRIMARY  
 R FX CRYSTALS OCCUR IN THIS TRENCH.

/ 30 50 XOVBN D  
 / 207 230 PPFQPYLIQZ6PPR7 P P6C( D\*  
 L A FX2 C\*C(  
 / 230 237 PPFQPYLIQZ5PPR5 P P5C( D1  
 L UACYFX3 C1C(  
 / 237 270 QZDRLIFXQZ6EQGT P P6  
 L WAPLB11 C)C(  
 R PYROLUSITE OCCURS AS DISSEMINATIONS AS WELL AS DENDRITIC  
 R COATINGS  
 R THIS TRENCH ENDS DUE TO THE EXTENT OF THE GOLD-IN-SOIL ANOMALY

A001

AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
 R From To ppb ppm ppm ppm ppm ppm ppm

ALAB Eco Tech - Kamloops  
 ATYP Chip Samples

			LNG	AU	AG	CU	PB	ZN	AS	SB
	From	To		ppb	ppm	ppm	ppm	ppm	ppm	ppm
R	00	20	NO SAMPLE-OVBN							
A001	20	30	1.0 53414	10	.1	3	10	23	4	.1
R	30	50	NO SAMPLE-OVBN							
A001	50	65	1.5 53415	10	.1	2	6	52	3	.1
A001	65	80	1.5 53416	15	.1	2	8	31	2	.1
A001	80	95	1.5 53417	5	.1	2	11	31	4	.1
A001	95	110	1.5 53418	20	.1	2	10	46	3	.1
A001	110	125	1.5 53419	5	.1	2	16	33	4	.1
A001	125	140	1.5 53420	5	.1	2	7	34	3	.1
A001	140	155	1.5 53421	10	.2	2	10	35	3	.1
A001	155	170	1.5 53422	10	.1	3	8	69	5	.1
A001	170	180	1.5 53423	10	.1	2	9	57	4	.1
A001	180	200	2.0 53424	5	.1	2	4	40	3	.1
A001	200	207	0.7 53425	15	.1	2	10	37	4	.1
A001	207	215	0.8 53426	5	.1	1	12	50	4	.1
A001	215	230	1.5 53427	10	.1	3	9	80	4	.1
A001	230	237	0.7 53428	15	.1	8	34	151	3	.1
A001	237	255	1.8 53429	10	.4	53	44	127	6	.1
A001	255	267	1.2 53430	5	.3	20	45	124	3	.1
R	267	270	NO SAMPLE-OVBN							

/END

TRENCH 1378W

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IDEN6B0201 V232TR1378W 06JUL89RGMMD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 300 MT 49.0 158.0 -01.0 -1072.0 -1378.0 1310.00  
 S001 300 490 49.0 154.0 -03.0

R From To

R THIS TRENCH TESTS MULTI-ELEMENT SOIL ANOMALIES OVER 300M

/ 00 05 OVBN P  
 / 05 106 QZDRFXPLQZ6EQGT P P6 <\*D\*  
 L W B12 C(  
 / 35 50 XQZDRFXPLQZ6EQGT D P5 P2D\*  
 L GACLB12 C\*C+  
 / 50 69 XOVBN D  
 / 106 125 QZDRFXPLQZ6EQGT 567 P P6 P2  
 L WA B11R5 C\*+<

R SOME PIECES IN THIS SECTION ARE VERY SILICIFIED AND CONTAIN QTZ  
R AUGENS

/ 125 136 QZDRFXCLQZ5EQGT 667 P P5 P1D\*  
 L UA B11 C2C2  
 / 136 147 QZDRCYLIQZ5EQGT P P5P2 D)  
 L WPLFX3R7 D)C)

R MAFIC MINERALS ARE GONE

/ 147 490 PPFQPLLIQZ6PPR5 P P6C\* D+  
 L UACYFX3 D=D\*

R FX CRYSTALS HAVE BEEN REWORKED INTO MATRIX

/ 167 180 XOVBN D  
 / 210 255 XOVBN D  
 / 268 292 XPPFQLICYQZ6PPR7 D P6 D+  
 L A FX2 <1D)  
 / 330 345 XOVBN D  
 / 405 420 XOVBN D  
 / 435 445 XOVBN D  
 / 460 475 XOVBN D

R THIS TRENCH ENDS DUE TO ROAD CROSSING

A001

AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
 R From To ppb ppm ppm ppm ppm ppm ppm

ALAB Eco Tech - Kamloops  
 ATYP Chip Samples

R 00 05 1.5 NO SAMPLE-OVBN  
 A001 05 20 1.5 53431 15 2.8 5 19 74 4 .1  
 A001 35 50 1.5 53433 10 .1 3 12 87 3 .1  
 A001 69 83 1.4 53434 15 .1 3 5 85 2 .1  
 A001 83 106 2.3 53435 5 .1 3 5 67 3 .1  
 A001 106 125 1.9 53436 10 .2 5 18 73 3 .1  
 A001 125 136 1.1 53437 10 .1 4 10 65 2 .1  
 A001 136 147 1.1 53438 10 .2 4 255 432 4 .1  
 A001 147 167 2.0 53439 5 .1 5 120 173 4 .1  
 A001 180 195 1.5 53440 10 .1 3 16 74 48 .1  
 A001 195 210 1.5 53441 5 .1 3 10 71 47 .1

A001	255	268	1.3	53442	5	.2	5	32	490	44	.1
A001	268	280	1.2	53443	5	.2	6	41	317	3	.1
A001	280	292	1.2	53444	10	.1	2	36	100	48	.1
A001	292	307	1.5	53445	10	.1	1	12	40	46	.1
A001	307	320	1.3	53446	5	.1	2	28	97	47	.1
A001	320	330	1.0	53447	5	.1	2	18	82	4	.1
A001	345	360	1.5	53448	40	.1	2	16	87	3	.1
A001	360	375	1.5	53449	10	.1	1	14	50	3	.1
A001	375	390	1.5	53450	45	.2	2	16	43	4	.1
A001	390	405	1.5	53451	20	.1	1	12	36	3	.1
A001	420	435	1.5	53452	15	.1	2	12	36	4	.1
A001	445	460	1.5	53453	15	.1	1	6	39	4	.1
A001	475	490	1.5	53454	10	.1	1	13	27	6	.1
A003											
AUMM			LNG	SAMPLE	AU	AG	CU	PB	ZN	AS	SB
ALAB			Echo Tech - Kamloops								
ATYP			Extra Samples Taken Along Structures, Etc.								
A003	15	15	0.7	53432	5	2.1	5	108	126	3	.1
R			Sample along silicified fracture filling, e-w trend								
/END											

TRENCH 1388E

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IDEN680201 V232TR1388E 13AUG89RGMMD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 620 MT 132.5 165.0 -05.0 750.0 1388.0 1320.00  
 S001 620 795 132.5 165.0 -08.0  
 S002 795 1075 132.5 168.0 -12.0  
 S003 1075 1325 132.5 168.0 -13.0

R From To  
 R THIS TRENCH WAS DUG TO TEST A GOLD-IN-SOIL ANOMALY OVER 125M  
 R WITH A WEAK IP RESPONSE  
 / 00 609 PPFQLIPLQZ3R5PP P D+ D)  
 L OW FX5 888 D=P+  
 R SECTION IS EXTR. WEATHERED;ROCK HAS HAD FX REWORKED INTO MATRIX  
 / 172 185 XFAULLICY D P7  
 L YW 888 SH034 P3  
 R THIS SECTION WAS PANEL SAMPLED- A003, IN TWO SEPARATE SAMPLES  
 / 163 172 XFAULLICY D P7  
 L YW SH007 P3  
 / 199 211 XFAULLICY D P7  
 L YW SH024 P3  
 / 278 379 XPPFQ R7 D  
 L 888  
 R PHENOS BECOME SMALLER;MORE REWORKED BUT STILL PRESENT ~20%  
 / 379 609 XPPFQ R7 D <)P5  
 L 888 P2  
 R PHENOS ALMOST LOST;CLAY ALTERATION INCREASES  
 / 609 748 PPFQCY Q22R5PP P <)P3  
 L OW FX4 888 D2  
 / 748 1325 PPFQCYLIFX4R5PP P <)P)  
 L OW QZ3 254 D2D+  
 / 880 940 XPPFQ D P2  
 L 567 P3  
 R OVERALL THIS TRENCH COMPRISED OF ONE PARENT ROCK; THE CHANGES  
 R HERE TRY TO REFLECT CHANGES IN REWORKING/FRACTURING/ALTERATION.  
 R THE CHANGES ARE SUBTLE, MIXED AND MASKED BY DEEP WEATHERING  
 R SURFACES WHICH IN THEMSELVES VARY THROUGH THE TRENCH.  
 R THIS TRENCH IS DISCONTINUED AS IT JOINS THE COLLAR OF TR1393E.

A001

AUMM	From	To	LNG SAMPLE	Au ppb	Ag ppm	Cu ppm	Pb ppm	Zn ppm	As ppm	Sb ppm
ALAB			Eco Tech - Kamloops							
ATYP			Chip Samples							
A001	00	15	1.5 53826	10	3.4	17	989	210	7	2.6
A001	15	30	1.5 53827	5	.3	5	30	64	6	.1
A001	30	45	1.5 53828	3	.1	10	66	60	10	.2
A001	45	60	1.5 53829	35	.1	17	51	95	11	.1
A001	60	75	1.5 53830	5	.1	23	154	275	6	.1
A001	75	90	1.5 53831	5	.1	11	40	260	10	.1
A001	90	103	1.3 53832	10	.3	8	20	72	17	.1
A001	103	118	1.5 53833	10	.2	4	19	60	6	.1

A001	118	134	1.6	53834	10	.05	4	14	39	8	.1
A001	134	148	1.4	53835	15	.1	6	17	68	7	.1
A001	148	163	1.5	53836	25	.5	6	34	170	44	.1
A001	163	177	1.4	53837	15	.3	7	61	280	21	.1
R				INTERVAL 17.7 TO 18.6 WAS				PANEL	SAMPLED (A003)		
A001	186	194	0.8	53838	20	.4	10	42	360	17	.1
A001	194	208	1.4	53839	10	.1	9	37	250	12	.1
A001	208	224	1.6	53840	10	.2	5	27	88	16	.2
A001	224	239	1.5	53841	15	.05	5	15	101	17	.1
A001	239	255	1.6	53842	20	.3	10	26	140	10	.1
A001	255	268	1.3	53843	20	.2	12	33	109	8	.1
A001	268	278	1.0	53844	10	.1	11	48	104	10	.1
A001	278	295	1.7	53845	15	.05	8	48	100	9	.1
A001	295	310	1.5	53846	10	.4	10	95	110	7	.1
A001	310	325	1.5	53847	15	.2	8	51	86	10	.1
A001	325	340	1.5	53848	10	.3	6	41	130	14	.1
A001	340	355	1.5	53849	15	.2	6	85	175	7	.2
A001	355	370	1.5	53850	5	.1	11	67	107	6	.1
A001	370	380	1.0	53851	10	.1	14	127	103	5	.1
A001	380	395	1.5	53852	30	.1	5	43	60	6	.1
A001	395	410	1.5	53853	15	.05	5	28	61	8	.1
A001	410	425	1.5	53854	10	.3	10	41	100	6	.1
A001	425	440	1.5	53855	15	.05	8	23	46	12	.1
A001	440	455	1.5	53856	20	.2	9	22	32	5	.1
A001	455	470	1.5	53857	30	.1	9	48	74	7	.1
A001	470	480	1.0	53858	20	.05	12	79	104	6	.1
A001	480	495	1.5	53859	10	.2	22	114	200	6	.1
A001	495	510	1.5	53860	15	.3	21	97	129	7	.1
A001	510	525	1.5	53861	10	.05	19	113	138	7	.1
A001	525	540	1.5	53862	20	.05	20	109	145	6	.1
A001	540	560	2.0	53863	15	.2	21	58	106	8	.1
A001	560	575	1.5	53864	10	.05	14	29	78	9	.1
A001	575	590	1.5	53865	10	.05	19	32	138	7	.1
A001	590	605	1.5	53866	10	.2	13	17	78	10	.1
A001	605	620	1.5	53867	5	.1	17	27	67	7	.1
A001	620	635	1.5	53868	5	.1	12	26	58	6	.1
A001	635	650	1.5	53869	20	.3	10	29	76	13	.1
A001	650	665	1.5	53870	10	.05	18	43	210	23	.1
A001	665	680	1.5	53871	10	.4	17	31	135	19	.1
A001	680	695	1.5	53872	15	.3	19	35	120	24	.1
A001	695	716	2.1	53873	15	.05	24	44	140	18	.1
A001	716	731	1.5	53874	10	.1	41	38	104	21	.1
A001	731	749	1.8	53875	10	.05	16	24	44	8	.1
A001	749	765	1.6	53876	15	.1	10	21	23	7	.1
A001	765	780	1.5	53877	10	.05	11	23	40	6	.1
A001	780	795	1.5	53878	3	.05	22	25	80	7	.1
A001	795	810	1.5	53879	10	.2	12	39	92	11	.1
A001	810	825	1.5	53880	3	.05	13	23	77	5	.1
A001	825	840	1.5	53881	15	.05	10	22	96	8	.1
A001	840	855	1.5	53882	20	.1	14	27	150	7	.1
R	855	865	1.0	NO SAMPLE-FRESH ROCK							
A001	865	880	1.5	53883	15	.05	8	20	52	5	.1
A001	880	895	1.5	53884	10	.05	9	27	78	5	.1
R	895	910	1.5	NO SAMPLE-FRESH ROCK							
A001	910	925	1.5	53885	20	.05	10	51	67	6	.1
A001	925	940	1.5	53886	10	.3	19	52	70	8	.1



A001	940	955	1.5	53887	20	.4	11	42	51	7	.1
R	955	970	1.5	NO SAMPLE-FRESH ROCK							
A001	970	985	1.5	53888	41	.1	5	43	42	6	.1
R	985	1000	1.5	NO SAMPLE-FRESH ROCK							
A001	1000	1015	1.5	53889	10	.3	4	33	40	4	.1
R	1015	1039	2.4	NO SAMPLE-FRESH ROCK							
A001	1039	1055	1.6	53890	10	.2	8	78	49	17	.1
R	1055	1080	2.5	NO SAMPLE-FRESH ROCK							
A001	1080	1092	1.2	53891	15	.1	14	142	66	32	1.0
R	1092	1110	1.8	NO SAMPLE-FRESH ROCK							
A001	1110	1125	1.5	53892	10	.05	5	25	36	5	.1
R	1125	1180	5.5	NO SAMPLE-FRESH ROCK							
A001	1180	1200	2.0	53893	3	.1	7	18	30	4	.1
R	1200	1210	1.0	NO SAMPLE-FRESH ROCK							
A001	1210	1225	1.5	53894	15	.05	10	34	54	8	.1
R	1225	1260	3.5	NO SAMPLE-FRESH ROCK							
A001	1260	1275	1.5	53895	20	.3	13	57	148	3	.1
R	1275	1310	3.5	NO SAMPLE-FRESH ROCK							
A001	1310	1325	1.5	53896	10	.05	27	105	84	4	.1
R	SAMPLING WAS DONE AT ALTERNATING INTERVALS WHERE ROCK WAS										
R	FRESHER LOOKING; APPROX. FROM 86.0M										
A003											
AUMM	LNG SAMPLE AU AG CU PB ZN AS SB										
ALAB	Echo Tech - Kamloops										
ATYP	Extra Samples Taken Along Structures, Etc.										
A003	163	172	0.9	53926	10	.05	10	77	400	11	.1
R	CLAY ALT'D FAULT GOUGE IN A PPFQ,4CM WIDE AND STRIKING 007										
A003	172	181	0.6	53927	15	.2	74	70	370	18	.4
R	PANEL SAMPLE (0.8 X 0.9M) TAKEN OVER HALF OF A 0.6M WIDE CLAY										
R	ALT'D FAULT GOUGE STRIKING 034										
A003	181	182	0.7	53928	35	.7	28	46	330	12	.2
R	AS 53927 OVER AN AREA OF 0.7 X 0.8 M)										
A003	199	211	1.2	53929	20	.2	7	33	96	15	.1
R	5 CM WIDE CLAY ALT'D FAULT GOUGE IN A PPFQ STRIKING 024										
/END											

TRENCH 1393E

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 IDEN680201 V232TR1393E 21JUN89RGM UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 255 MT 33.50164.0 -17.0 614.0 1393.0 1300.00  
 S001 255 335 33.50164.0 -38.0

R From To  
 R THIS TRENCH TESTS A 125M GOLD-IN-SOIL ANOMALY  
 / 00 05 OVBN P  
 / 05 176 PPFQCYLIFX3PPBR P P5P3 D)  
 L YA Q25<<R5 D2C)  
 R SILICA FLOODING OCCURS IN FRACTURES RANGING FROM 0.1CM-2.5CM  
 / 39 52 XFAUL D  
 L 8 FZ004  
 / 176 208 PPFQLICYFX3PPR5 P P5P3  
 L 4APLQ25<<BN D3C) D)  
 R SILICA OCCURANCE IS CHARACTERIZED BY AUGENS AND PERVASIVENESS  
 / 208 335 PPFQ FX4PP P P3P4  
 L 4APLQ25 D2C)  
 R THIS TRENCH ENDS DUE TO STEEPLY DIPPING BEDROCK

A001

AUMM	From	To	LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB	
R				ppb	ppm	ppm	ppm	ppm	ppm	ppm	
ALAB	Eco Tech - Kamloops										
ATYP	Chip Samples										
R	00	05	0.5	NO SAMPLE - OVBN							
A001	05	20	1.5	53226	3	.1	5	22	28	2	.1
A001	20	39	1.9	53227	3	.1	5	24	35	2	.1
A001	39	52	1.3	53228	3	.1	6	33	31	2	.1
A001	52	65	1.5	53229	3	.1	5	28	38	2	.1
A001	65	80	1.5	53230	3	.1	7	65	60	2	.1
A001	80	95	1.5	53231	3	.1	4	32	48	2	.1
A001	95	110	1.5	53232	3	.1	6	56	42	3	.1
A001	110	125	1.5	53233	3	.1	8	54	57	3	.1
A001	125	140	1.5	53234	5	.1	5	33	39	1	.1
A001	140	155	1.5	53235	3	.1	3	36	55	2	.1
A001	155	165	1.0	53236	3	.1	2	22	32	3	.1
A001	165	176	1.1	53237	3	.1	4	31	59	3	.1
A001	176	190	1.4	53238	3	.1	5	104	72	2	.1
A001	190	208	1.8	53239	3	.1	3	69	54	1	.1
A001	208	220	1.2	53240	3	.1	3	36	42	2	.1
A001	220	235	1.5	53241	3	.1	7	62	87	2	.1
A001	235	250	1.5	53242	70	.1	6	44	71	2	.1
A001	250	265	1.5	53250	5	.1	7	91	92	5	.1
A001	265	280	1.5	53243	3	.1	7	30	102	4	.1
A001	280	295	1.5	53244	5	.1	6	31	80	6	.1
A001	295	310	1.5	53245	10	.1	5	29	81	6	.1
A001	310	320	1.0	53246	3	.1	10	31	103	7	.1
A001	320	335	1.5	53247	3	.1	13	189	137	6	.1

A003

AUMM	From	To	LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB
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ALAB      Echo-Tech - Kamloops
ATYP      Extra samples taken along structures,etc.
A003  165  200  3.5  53249    3   .1  15  148  142   5   .1
R         53249 SELECTIVE SAMPLING OF FRACTURE INFILLING MATERIAL,
R         QTZ FLOODING?
A004
AUMM      LNG SAMPLE   Au   Ag   Cu   Pb   Zn   As   Sb
ALAB      Echo-Tech - Kamloops
ATYP      Repeat samples taken along intervals
A004  05   20  1.5  53248    3   .1   6  59  63   5   .1
R         RE-SAMPLE OF 53226 : POSSIBLE QUARTZ FLOODING OR
R         ZENOLITH. FINER GRAINED SILICA RICH MATRIX OF QFP.
/END
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TRENCH 1565W

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IDEN6B0201 V232TR1565W 07AUG89RGMMJD UTM340.0
IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT
/NAM SICYKACBCLPYCPGLSL
LNAM LIPLHEMG
/SCL MT.2
LSC LCTM
S000 00 600 MT 278.5 345.0 15.0 -1015.0 -1565.0 1400.00
S001 600 780 278.5 340.0 -06.0
S002 780 1670 278.5 343.0 13.0
S003 1670 1820 278.5 316.0 02.0
S004 1820 1910 278.5 332.0 06.0
S005 1910 2080 278.5 346.0 -07.0
S006 2080 2180 278.5 345.0 12.0
S007 2180 2300 278.5 336.0 -04.0
S008 2300 2560 278.5 340.0 14.0
S009 2560 2785 278.5 340.0 06.0
R From To
R THIS TRENCH TESTS MULTI-ELEMENT SOIL ANOMALIES OVER 300M
/ 00 40 OVBN P
/ 40 489 QZDRCYFXQZ5GTEQ P <= <+
L WACLB11 444
R SX SEEM TO BE PRESENT BUT ARE TOO FINELY DISS TO BE IDENTIFIED
/ 400 437 XFAULLICY D 070 P2 D+
L OYPY 457 C1
R FRACTURES AND ALTERATION INCREASE COINCIDENTLY AND OCCUR
R BETWEEN ROCK CONTACTS
/ 466 489 XFAULLICY D 072 P4 D)
L OYPY 678 P2
/ 489 603 PPFQCLLIQZ3PP P P3P* P)D*
L GACYFX4 222 C+
/ 603 624 PPFQCLPYQZ6PPR5 P P6 D+
L A FX3 475 D)
R QZ AND FX HAVE BEEN REWORKED INTO THE MATRIX
/ 624 897 QZDRFXLIQZ5GTEQ P P5 <*D*
L WAPYB12 C)
/ 624 653 XFAULCYLI D 096 P1 D)
L OA 467 C=
/ 705 710 XFAULCYLI D 094 P1 D)
L OY 567 C1
/ 865 874 XFAULCYLI D 070 P3 D+
L OY 888 C3
/ 897 1001 PPFQCY QZ5PPR5 P P3P2
L WA FX3 <+
R IT IS DIFFICULT TO NAME PARENT ROCK OF HEAVILY ALT/FRACTURED
R ZONE AT CONTACTS
/ 994 1001 XFAULLICY D 070 P3
L OY 687 C3
/ 1001 1454 QZDRCLFXQZ4GTEQ P <)
L AW B12 246 <+
R SMALL ZENOLITHS OF GNIS
/ 1085 1088 XFAULCYLI D 070 P3
L WY P2
/ 1300 1308 XFAULLICY D 076 P1

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L YA 247 P1  
 R THIS STRUCTURE ISNT AS HEAVILY FRACTURED/ALTERED  
 / 1454 1710 PPFQLI QZ4PPR2 P C) D+  
 L 5A FX4 225 D)C)  
 R PRIMARY EUHEDRAL FX CRYSTALS NEAR MID SECTION. ROCK IS A LITTLE  
 R REWORKED NEAR CONTACTS WITH QZDR  
 / 1329 1332 XFAULLICY D 060 P2  
 L OA 457 C3  
 / 1205 1208 XFAULLIPL D 060 P3  
 L YUCY P2<1  
 R NEXT THREE STRUCTURES SAMPLED ARE IDENTICAL TO 1205-1207 (1215,  
 R 1225, 1274)  
 / 1390 1400 XFAULPLLI D 076 P3  
 L OWCY 568 P2<1  
 / 1442 1454 XFAULLICY D 044 C3  
 L OY 678 P4  
 R FRACTURE ZONE TYPICAL OF ROCK CHANGE/CONTACT  
 / 1710 1835 QZDRFXLIQZ5R2GT P <+  
 L WACLB12 C+  
 R THIS SECTION THE QZDR CHANGES TEXTURE SLIGHTLY SHOWING A  
 R REWORKED MATRIX WITH REMOBILIZATION OF QTZ; BI REMAINS, THIS  
 R SECTION HAS SOME LOCALIZED FRACTURE INTENSIFICATION.  
 / 1832 1834 XFAULLICY D 072 C1  
 L WO 678 P2  
 R MINOR FRACTURED SECTION  
 / 1835 1895 PPFQLIPYQZ4PPR2 P D\*  
 L WA FX3 223 D+C+  
 / 1895 2710 QZDRCLLIQZ4GTEQ P P1 D)  
 L AWCYB12 356 D+  
 / 1900 1975 XFAUL D 062 P3  
 L 7A 678 P2<=  
 / 2035 2060 XFAUL D 112 P3  
 L OA 678 P2<+  
 / 2060 2090 XOVCN D  
 / 2196 2201 XFAUL D 070 P6  
 L OW P4  
 / 2274 2275 XVEIN D 138 PX D)  
 R VEIN IS 5CM. AT WIDEST POINT, BUT PINCHES OUT AT ONE END AND  
 R FAULTS AWAY AT THE OTHER.  
 / 2710 2785 PPFQCY QZ R5PP P D) D(  
 L WA FX 223  
 R TRENCH ENDS DUE TO TARGET LIMITS. MAY BE OPENED FURTHER.

A001

AUMM	From	To	LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB
				ppb	ppm	ppm	ppm	ppm	ppm	ppm
ALAB	Eco Tech - Kamloops									
ATYP	Chip Samples									
A001	00	40	4.0 NO SAMPLE-OVCN							
A001	40	55	1.5 53701	5.0	.1	2.0	11.	120.	1.0	.1
R	55	70	1.5 NO SAMPLE							
A001	70	85	1.5 53702	3.0	.05	2.0	5.0	84.	2.0	.1
R	85	100	1.5 NO SAMPLE							
A001	100	115	1.5 53703	3.0	.1	3.0	10.0	122.	1.0	.1
R	115	130	1.5 NO SAMPLE							
A001	130	145	1.5 53704	3.0	.1	2.0	7.0	91.	2.0	.1
R	145	160	1.5 NO SAMPLE							

A001	160	175	1.5	53705	3.0	.1	2.0	5.0	70.	1.0	.1
R	175	190	1.5	NOSAMPLE							
A001	190	205	1.5	53706	3.0	.2	1.0	5.0	68.	2.0	.1
R	205	220	1.5	NO SAMPLE							
A001	220	235	1.5	53707	5.0	.1	2.0	31.	202.	2.0	.1
R	235	250	1.5	NO SAMPLE							
A001	250	265	1.5	53708	10.0	.1	2.0	69.	290.	1.0	.1
R	265	280	1.5	NO SAMPLE							
A001	280	295	1.5	53709	3.0	.1	1.0	7.0	105.	.5	.1
R	215	310	1.5	NO SAMPLE							
A001	310	325	1.5	53710	5.0	.2	4.0	16.	87.	.5	.1
R	325	340	1.5	NO SAMPLE							
A001	340	355	1.5	53711	3.0	.1	8.0	22.	123.	2.0	.1
R	355	370	1.5	NO SAMPLE							
A001	370	384	1.4	53712	5.0	.1	5.0	32.	131.	3.0	.1
A001	384	400	1.6	53713	10.0	.1	6.0	5.0	96.	2.0	.1
A001	400	410	1.0	53714	5.0	.2	6.0	23.	128.	5.0	.1
A001	410	423	1.3	53715	10.0	.8	4.0	49.	36.	3.0	.1
A001	423	437	1.4	53716	3.0	.2	4.0	14.	83.	2.0	.1
A001	437	447	1.0	53717	3.0	.1	4.0	11.	90.	2.0	.1
A001	450	460	1.0	53718	3.0	.05	3.0	13.	114.	2.0	.1
A001	460	470	1.0	53719	3.0	.1	7.0	22.	170.	2.0	.1
A001	470	480	1.0	53720	3.0	.1	9.0	189.	164.	5.0	.1
R	480	489	0.9	NO SAMPLE							
A001	489	505	1.6	53721	5.0	.1	3.0	67.	160.	4.0	.1
A001	505	520	1.5	53722	5.0	.1	1.0	32.	39.	2.0	.1
R	520	565	4.5	NO SAMPLE							
A001	565	580	1.5	53723	3.0	.05	.5	15.	20.	2.0	.1
R	580	593	1.3	NO SAMPLE							
A001	593	603	1.0	53724	3.0	.1	.5	19.	66.	3.0	.1
R	603	609	0.6	NO SAMPLE							
A001	609	624	1.6	53725	5.0	.2	2.0	47.	231.	4.0	.1
A001	624	640	1.6	53726	3.0	.1	4.0	19.	84.	4.0	.1
A001	640	653	1.3	53727	5.0	.05	1.0	5.0	47.	4.0	.1
A001	653	665	1.2	53728	3.0	.05	1.0	6.0	38.	2.0	.1
A001	665	680	1.5	53729	5.0	.05	3.0	6.0	35.	3.0	.1
A001	680	695	1.5	53730	5.0	.1	6.0	5.0	34.	4.0	.1
A001	695	705	1.0	53731	15.	.1	2.0	17.	47.	3.0	.1
R	705	710	0.5	NO SAMPLE							
A001	710	720	1.0	53732	10.0	.1	3.0	13.	29.	2.0	.1
A001	720	735	1.5	53733	20.	.05	5.0	10.0	30.	2.0	.1
A001	735	750	1.5	53734	25.	.4	5.0	29.	45.	2.0	.1
A001	750	765	1.5	53735	20.	.1	5.0	13.	52.	3.0	.1
R	765	780	1.5	NO SAMPLE							
A001	780	795	1.5	53736	3.0	.1	3.0	10.0	98.	2.0	.1
R	795	810	1.5	NO SAMPLE							
A001	810	825	1.5	53737	5.0	.1	2.0	8.0	92.	2.0	.1
R	825	840	1.5	NO SAMPLE							
A001	840	855	1.5	53738	3.0	.1	5.0	8.0	103.	2.0	.1
A001	855	865	1.0	53739	10.0	.1	.5	7.0	98.	2.0	.1
A001	865	874	0.9	53740	3.0	.3	4.0	34.	70.	9.0	.1
A001	874	890	1.6	53741	5.0	.1	1.0	37.	132.	4.0	.1
A001	890	897	0.7	53742	5.0	.1	2.0	21.	157.	2.0	.1
A001	897	908	1.1	53743	20.	.1	3.0	59.	179.	3.0	.1
A001	908	920	1.2	53744	10.0	.1	2.0	73.	237.	4.0	.1
A001	920	935	1.5	53745	25.	.1	2.0	78.	125.	2.0	.1

A001	935	950	1.5	53746	10.0	.1	5.0	37.	65.	2.0	.1
R	950	980	3.0	NO SAMPLE							
A001	980	994	1.4	53747	5.0	.05	4.0	39.	38.	2.0	.1
A001	994	1001	0.7	53748	10.0	.6	7.0	94.	66.	2.0	.1
A001	1001	1018	1.7	53749	5.0	.2	6.0	65.	132.	2.0	.1
A001	1018	1030	1.2	53750	5.0	.1	5.0	15.	121.	2.0	.1
R	1030	1045	1.5	NO SAMPLE							
A001	1045	1060	1.5	53751	20.	.1	6.0	61.	249.	2.0	.1
R	1060	1075	1.5	NO SAMPLE							
A001	1075	1085	1.0	53752	35.	.05	4.0	6.0	70.	2.0	.1
A001	1085	1100	1.5	53753	10.0	.05	6.0	5.0	85.	2.0	.1
R	1100	1115	1.5	NO SAMPLE							
A001	1115	1130	1.5	53754	5.0	.1	5.0	9.0	112.	2.0	.1
R	1130	1145	1.5	NO SAMPLE							
A001	1145	1160	1.5	53755	3.0	.1	4.0	6.0	80.	.5	.1
R	1160	1175	1.5	NO SAMPLE							
A001	1175	1190	1.5	53756	5.0	.1	8.0	4.0	114.	1.0	.1
A001	1190	1205	1.5	53757	5.0	.05	9.0	7.0	163.	2.0	.1
A001	1205	1220	1.5	53758	10.0	.05	6.0	11.	179.	2.0	.1
A001	1220	1235	1.5	53759	10.0	.1	2.0	8.0	142.	5.0	.1
R	1235	1250	1.5	NO SAMPLE							
A001	1250	1265	1.5	53760	5.0	.1	3.0	12.	124.	2.0	.1
A001	1265	1280	1.5	53761	5.0	.1	2.0	10.0	68.	.5	.1
A001	1280	1300	2.0	53762	5.0	.05	3.0	8.0	74.	2.0	.1
A001	1300	1308	0.8	53763	15.	.2	3.0	98.	224.	2.0	.1
A001	1308	1320	1.2	53764	10.0	.1	2.0	6.0	89.	2.0	.1
A001	1320	1330	1.0	53765	10.0	.1	3.0	13.	125.	2.0	.1
A001	1330	1345	1.5	53766	5.0	.1	3.0	14.	163.	.5	.1
R	1345	1360	1.5	NO SAMPLE							
A001	1360	1375	1.5	53767	10.0	.4	2.0	52.	250.	2.0	.1
A001	1375	1390	1.5	53768	10.0	.6	4.0	211.	317.	1.0	.1
A001	1390	1400	1.0	53769	10.0	.2	5.0	86.	220.	2.0	.4
A001	1400	1415	1.5	53760	5.0	.1	3.0	12.	124.	2.0	.1
R	1415	1430	1.5	NO SAMPLE							
A001	1430	1442	1.2	53771	5.0	.3	12.	45.	270.	.5	.1
A001	1442	1454	1.2	53772	10.0	.9	49.	398.	460.	2.0	.1
A001	1454	1468	1.4	53773	30.	.2	3.0	428.	310.	1.0	.2
R	1468	1500	3.2	NO SAMPLE							
A001	1500	1515	1.5	53774	25.	.05	5.0	204.	84.	1.0	.2
R	1515	1565	5.0	NO SAMPLE							
A001	1565	1580	1.5	53775	20.	.05	6.0	66.	155.	1.0	.1
A001	1580	1595	1.5	53776	20.	.05	5.0	80.	107.	1.0	.1
R	1595	1625	3.0	NO SAMPLE							
A001	1625	1640	1.5	53777	30.	.05	6.0	260.	325.	1.0	.2
A001	1640	1655	1.5	53778	25.	.05	5.0	335.	220.	1.0	.1
R	1655	1675	2.0	NO SAMPLE							
A001	1675	1690	1.5	53779	50.	1.0	3.0	700.	289.	1.0	.1
A001	1690	1710	2.0	53780	10.0	.05	8.0	389.	258.	1.0	.2
A001	1710	1720	1.0	53781	20.	.05	9.0	238.	190.	1.0	.1
R	1720	1730	1.0	NO SAMPLE							
A001	1730	1745	1.5	53782	3.0	.2	8.0	30.	132.	1.0	.2
R	1745	1775	3.0	NO SAMPLE							
A001	1775	1790	1.5	53783	3.0	.05	30.	45.	110.	1.0	.05
R	1790	1820	3.0	NO SAMPLE							
A001	1820	1835	1.5	53784	5.0	.05	4.0	41.	139.	1.0	.05
A001	1835	1850	1.5	53785	5.0	.05	2.0	78.	320.	1.0	.2

R	1850	1880	3.0	NO SAMPLE							
A001	1880	1895	1.5	53786	3.0	.05	2.0	94.	306.	1.0	.2
R	1895	1900	0.5	NO SAMPLE							
A001	1900	1915	1.5	53787	5.0	5.2	8.0	128.	590.	1.0	.2
A001	1915	1930	1.5	53788	3.0	.05	13.	23.	144.	1.0	.2
A001	1930	1945	1.5	53789	3.0	.5	4.0	41.	221.	1.0	.2
A001	1945	1960	1.5	53790	3.0	.2	5.0	75.	371.	1.0	.1
A001	1960	1975	1.5	53791	5.0	.1	3.0	78.	188.	1.0	.2
A001	1975	1990	1.5	53792	3.0	.1	2.0	83.	240.	1.0	.1
A001	1990	2005	1.5	53793	3.0	.2	16.	209.	338.	1.0	.1
A001	2005	2020	1.5	53794	5.0	.3	8.0	74.	390.	1.0	.2
A001	2020	2035	1.5	53795	5.0	.4	9.0	80.	225.	1.0	.1
A001	2035	2045	1.0	53796	5.0	.1	10.0	67.	199.	1.0	.1
R	2045	2090	4.5	NO SAMPLE							
A001	2090	2105	1.5	53797	10.0	.3	3.0	32.	175.	1.0	.05
A001	2105	2122	1.5	NO SAMPLE							
A001	2122	2135	1.3	53798	15.	.05	2.0	86.	230.	1.0	.1
R	2135	2150	1.5	NO SAMPLE							
A001	2150	2165	1.5	53799	20.	.1	2.0	58.	136.	1.0	.2
A001	2165	2180	1.5	53800	15.	.2	1.0	49.	116.	1.0	.1
A001	2180	2200	2.0	53801	10.0	.3	2.0	47.	200.	1.0	.1
A001	2200	2215	1.5	53802	15.	.1	1.0	64.	196.	1.0	.1
R	2215	2230	1.5	NO SAMPLE							
A001	2230	2245	1.5	53803	10.0	.1	3.0	23.	79.	1.0	.2
R	2245	2260	1.5	NO SAMPLE							
A001	2260	2275	1.5	53804	15.	.3	11.	77.	280.	1.0	.1
A001	2275	2290	1.5	53805	10.0	.1	4.0	39.	115.	3.0	.05
A001	2290	2305	1.5	53806	5.0	.05	2.0	59.	200.	1.0	.05
R	2305	2320	1.5	NO SAMPLE							
A001	2320	2335	1.5	53807	15.	.1	1.0	32.	180.	1.0	.05
R	2335	2350	1.5	NO SAMPLE							
A001	2350	2365	1.5	53808	20.	.4	2.0	20.	115.	1.0	.2
R	2365	2380	1.5	NO SAMPLE							
A001	2380	2395	1.5	53809	10.0	.1	2.0	19.	110.	1.0	.1
R	2395	2410	2.5	NO SAMPLE							
A001	2410	2425	1.5	53810	40.	.1	2.0	44.	330.	1.0	.2
A001	2425	2440	1.5	53811	15.	.3	3.0	104.	425.	1.0	.1
R	2440	2445	0.5	NO SAMPLE							
A001	2445	2470	1.5	53812	15.	.05	2.0	136.	299.	1.0	.1
R	2470	2485	1.5	NO SAMPLE							
A001	2485	2490	1.5	53813	20.	.05	3.0	114.	400.	1.0	.1
R	2490	2515	2.5	NO SAMPLE							
A001	2515	2530	1.5	53814	15.	.1	4.0	60.	264.	1.0	.1
R	2530	2545	1.5	NO SAMPLE							
A001	2545	2560	1.5	53825	3.0	.1	2.0	26.	123.	1.0	.1
A001	2560	2575	1.5	53815	45.	.6	3.0	125.	297.	1.0	.05
A001	2575	2590	1.5	53816	25.	.4	13.	61.	232.	1.0	.05
A001	2590	2605	1.5	53817	20.	.2	2.0	21.	120.	1.0	.05
R	2605	2620	1.5	NO SAMPLE							
A001	2620	2635	1.5	53818	15.	.05	1.0	28.	65.	1.0	.2
R	2635	2650	1.5	NO SAMPLE							
A001	2650	2665	1.5	53819	5.0	.05	1.0	27.	145.	1.0	.2
R	2665	2680	1.5	NO SAMPLE							
A001	2680	2695	1.5	53820	20.	.2	2.0	56.	160.	1.0	.1
A001	2695	2710	1.5	53821	15.	.1	1.0	85.	154.	1.0	.1
A001	2710	2725	1.5	53822	3.0	.3	1.0	47.	64.	1.0	.1



R	2725	2740	1.5	NO SAMPLE								
A001	2740	2755	1.5	53823	3.0	.2	1.0	99.	112.	1.0	.1	
R	2755	2770	1.5	NO SAMPLE								
A001	2770	2785	1.5	53824	15.	.1	1.0	102.	107.	1.0	.1	
R	ALL THE ABOVE UNSAMPLED INTERVALS WERE DUE TO UNALTERED OR											
R	UNFAVOURABLE LOOKING BEDROCK.											
A002												
AUMM				SAMPLE	AU	AG	CU	PB	ZN	AS	SB	
ALAB	Echo Tech - Kamloops											
ATYP	Grab Samples											
A002	2615	2615	0.0	53692	3.0	.05	4.0	25.	48.	2.0	.1	
A003												
AUMM				LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB	
ALAB	Echo Tech - Kamloops											
ATYP	Extra Samples Taken Along Structures, Etc.											
A003	29	33	0.4	53654	10.0	.05	5.0	16.	99.	5.0	.1	
A003	66	68	0.2	53655	15.	.05	5.0	54.	183.	3.0	.1	
A003	220	225	0.5	53656	5.0	.2	3.0	97.	296.	2.0	.1	
A003	273	275	0.2	53657	5.0	.2	4.0	199.	368.	2.0	.1	
A003	360	365	0.5	53658	3.0	.2	4.0	10.0	85.	2.0	.1	
A003	447	450	0.3	53659	30.	.4	3.0	24.	69.	3.0	.1	
A003	483	489	0.6	53660	10.0	.2	3.0	124.	108.	2.0	.1	
A003	603	609	0.6	53661	3.0	.1	3.0	21.	104.	4.0	.1	
A003	705	710	0.5	53662	5.0	.5	2.0	37.	64.	4.0	.1	
A003	735	743	0.8	53663	5.0	.3	4.0	26.	114.	4.0	.1	
A003	750	752	0.2	53664	5.0	.2	5.0	22.	159.	4.0	.1	
A003	1085	1088	0.3	53665	3.0	.2	3.0	263.	240.	3.0	.1	
A003	1205	1208	0.3	53666	10.0	.3	4.0	19.	330.	3.0	.1	
A003	1215	1217	0.2	53667	3.0	.3	5.0	21.	312.	3.0	.1	
A003	1225	1228	0.3	53668	3.0	.2	4.0	2.0	214.	2.0	.1	
A003	1274	1276	0.2	53669	15.	.2	3.0	18.	176.	1.0	.1	
A003	1329	1332	0.3	53670	10.0	.05	3.0	4.0	96.	2.0	.1	
A003	1390	1393	0.3	53671	30.	1.9	6.0	219.	198.	6.0	1.7	
A003	1397	1400	0.3	53672	25.	.05	13.	148.	274.	5.0	.3	
A003	1442	1445	0.3	53673	15.	.05	4.0	88.	237.	2.0	.2	
A003	1485	1493	0.8	53693	20.	.05	7.0	353.	158.	1.0	.3	
A003	1579	1580	0.1	53674	30.	.05	37.	140.	580.	2.0	.3	
A003	1638	1640	0.2	53675	20.	.5	50.	1000.	498.	2.0	.3	
A003	1690	1692	0.2	53676	25.	.05	31.	627.	412.	2.0	.4	
A003	1832	1834	0.2	53677	90.	.05	11.	146.	300.	3.0	.3	
A003	1912	1917	0.5	53678	25.	.5	52.	95.	540.	2.0	.2	
A003	2050	2060	1.0	53679	20.	.05	10.0	219.	380.	2.0	.2	
A003	2105	2122	1.7	53680	20.	.05	8.0	64.	196.	1.0	.3	
A003	2159	2165	0.6	53681	15.	.05	3.0	21.	101.	1.0	.2	
A003	2196	2201	0.5	53682	30.	.1	7.0	1200.	430.	1.0	.1	
A003	2274	2275	0.1	53683	25.	.05	3.0	32.	201.	1.0	.5	
A003	2292	2298	0.6	53684	10.0	.05	6.0	453.	196.	1.0	.2	
A003	2329	2336	0.7	53685	15.	.05	5.0	27.	149.	1.0	.2	
A003	2346	2349	0.3	53686	20.	.05	5.0	18.	148.	1.0	.1	
A003	2421	2423	0.2	53687	20.	.05	6.0	56.	392.	1.0	.1	
A003	2583	2584	0.1	53688	10.0	.05	3.0	175.	320.	2.0	.2	
A003	2605	2620	1.5	53689	20.	.05	7.0	78.	54.	2.0	.05	
A003	2710	2722	1.2	53690	15.	.05	8.0	44.	120.	3.0	.5	
R	Sample along structures.											
/END												

TRENCH 001E

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IDEN680201 V232TR001E 13JUL89RGM UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 175 MT 70.4 111.0 -01.0 -43.00 01.00 1310.00  
 S001 175 290 70.4 125.0 -01.0  
 S002 290 435 70.4 166.0 -04.0  
 S003 435 704 70.4 176.0 -10.0  
 R From To  
 R THIS TRENCH WAS DUG TO TEST FOR ALTERATION ZONE DISCOVERED  
 R DURING A PREVIOUS DRILLING PROGRAM BY GOLDEN PICK RESOURCES  
 / 00 60 PPFQ QZ5 P P5 D1  
 L BA FX3 656 <1<+  
 R CY ALT IS PRESENT THROUGHOUT THIS SECTION ON WEATHERED SURFACES  
 R FX HAS BEEN WORKED SO THAT LITTLE PRIMARY FX REMAINS  
 / 60 266 PPFQKFPYFX3PP P P2 D+  
 L WACYQZ4 C=<1  
 / 00 15 XOVBN D  
 / 75 94 XOVBN D  
 / 110 117 XFAUL CY6 D P6  
 L N PL4 106 P4  
 / 158 266 XPPFQ D C4  
 L OU C4  
 R THIS INT IS EXTREMELY WEATHERED CLAY AND LI ARE ABUNDANT. THIS  
 R BORDERS ON PROMINENT FAULT ZONE FROM 26.6-27.07 AND CONTAINS A  
 R FAULTED SECTION 21.7-22.0  
 / 217 220 XFAUL LI4 D P1P6  
 L OU CY6 888 074 P4  
 R ORIGINAL ROCK WAS PPFQ  
 / 266 270 FAULLI CY4 P P3P4  
 L OU QZ3 888 084 C3  
 / 266 266 XFAUL CY6 D P6  
 L N PL4 084 P4  
 / 266 267 XFAULLI CY9 D P9  
 L Y LI1 084 P1  
 / 270 270 XFAUL CYX D PX  
 L 7A 084  
 / 270 355 PPFQCL QZ6R5 P P6 P=D+  
 L GA FX3 C+  
 R REMNANT QZ AUGENS ARE FINELY DISS IN THIS MATRIX, ROCK ALT IS  
 R SIGNIFICANTLY DIFFERENT ACCROSS FAULT ZONE.  
 / 310 311 XFAULCY D PX  
 L 7A 040  
 / 349 349 XFAULCY D PX  
 L 7A 040  
 / 355 704 PPFQCL QZ6R5 P P6 P=D+  
 L GA FX3 C+  
 R 355 467 FX ARE STILL PRESERVED KA ALT IS JUST STARTING  
 / 355 355 XFAUL CYX D PX

L 058  
 / 407 407 XFAUL CYX D PX  
 L 7A 074  
 / 409 409 XFAUL CYX D PX  
 L 7A 074  
 / 467 480 XPPFQPLCYQZ5R7 D P5P2 D\*  
 L AG FX3 P)C+  
 R ORIGINAL TEXTURES ARE STRONGLY REWORKED  
 / 480 500 XOVBN D  
 / 500 704 XPPFQCYFX D P4  
 L WAKA  
 / 560 579 XOVBN D  
 / 615 640 XDYKEYCLQZ3EQ D P3P1 P2D1  
 L 5ABIFX3 P+  
 / 677 687 XFAULLI CY8 D P8  
 L UY LI2 P2  
 R THIS TRENCH WAS DISCONTINUED DUE TO FLOODING FROM THE  
 R WATER TABLE

A001

AUMM	From	To	LNG SAMPLE	Au ppb	Ag ppm	Cu ppm	Pb ppm	Zn ppm	As ppm	Sb ppm
ALAB	Eco Tech - Kamloops									
ATYP	Chip Samples									
R	00	15	1.5 NO SAMPLE-OVBN							
A001	15	30	1.5 53549	3	1.0	17	142	270	1	6.6
A001	30	45	1.5 53550	3	.3	6	94	212	1	6.1
A001	45	60	1.5 53551	3	.1	15	197	800	1	6.0
A001	60	75	1.5 53552	3	.2	14	37	135	1	6.1
R	75	94	NO SAMPLE-OVBN							
A001	94	105	1.1 53553	3	.4	10	36	98	1	6.2
A001	105	120	1.5 53554	5	.3	26	22	459	1	5.0
A001	120	135	1.5 53555	3	.3	11	126	549	1	5.1
A001	135	150	1.5 53556	3	1.4	8	203	574	1	4.7
A001	150	160	1.0 53557	5	.9	4	87	391	1	6.8
A001	160	167	0.7 53558	3	.4	13	86	287	1	7.2
A001	167	176	0.9 53565	3	.3	21	36	555	1	6.2
A001	176	192	1.6 53559	3	.2	22	43	324	1	9.1
A001	192	206	1.4 53560	3	.3	57	35	178	1	8.8
A001	206	222	1.6 53561	3	1.3	40	19	475	1	6.2
A001	222	236	1.4 53562	3	.9	29	78	210	1	8.0
A001	236	252	1.6 53563	3	.7	24	26	309	1	7.6
R	252	296	SAMPLED AS STUCTURES (A003)							
A001	296	310	1.4 53566	3	.1	8	131	568	1	6.7
A001	310	325	1.5 53567	3	.1	5	121	464	1	8.1
A001	325	340	1.5 53568	3	.3	6	56	338	1	7.1
A001	340	355	1.5 53569	3	.1	7	143	410	1	7.8
A001	355	370	1.5 53570	3	.1	27	1800	382	1	7.3
A001	370	385	1.5 53571	3	.7	21	336	393	1	6.5
A001	385	396	1.1 53572	3	.4	27	28	555	1	6.1
A001	396	410	1.4 53573	5	.1	28	18	166	1	8.1
A001	410	425	1.5 53574	3	.5	50	59	788	1	8.7
A001	425	440	1.5 53575	3	.2	48	53	374	1	8.5
A001	440	454	1.4 53576	3	.1	26	14	294	1	8.0
A001	454	467	1.3 53577	10	.2	21	13	104	4	2.0

A001	467	480	1.3	53578	3	.3	65	49	733	3	1.5
R	480	500	NO SAMPLE-OVBN								
A001	500	515	1.5	53579	5	.1	39	17	139	2	1.9
A001	515	530	1.5	53580	3	.1	43	21	206	3	1.2
A001	530	545	1.5	53581	3	.2	40	36	479	5	1.0
A001	545	560	1.5	53582	3	.1	30	24	236	3	1.6
R	560	579	NO SAMPLE-OVBN								
A001	579	595	1.6	53583	3	.1	25	42	731	2	1.0
A001	595	615	1.6	53584	3	.1	23	18	180	2	.7
A001	615	640	2.0	53585	5	.2	18	45	133	17	2.1
A001	640	655	1.5	53586	3	.3	13	52	157	11	2.0
A001	655	677	2.2	53587	5	.2	9	47	179	4	1.7
A001	677	687	1.0	53588	3	.1	9	18	93	5	1.6
A001	687	704	0.7	53589	3	.1	6	14	65	2	.8
A003											
AUMM	LNG SAMPLE AU AG CU PB ZN AS SB										
ALAB	Echo Tech - Kamloops										
ATYP	Extra Samples Taken Along Structures.										
A003	110	117	0.7	53539	5	.4	35	68	669	1	8.3
R	THIS STRUCTURE RUNS PARRALELL TO TRENCH, 110 TO 117, 0.02M WIDE										
A003	217	220	0.3	53540	15	6.1	19	394	725	1	6.8
A003	266	266	0.0	53541	3	.7	9	99	591	1	7.0
A003	266	267	0.1	53542	3	.2	6	103	512	1	7.1
A003	267	270	0.3	53543	3	.4	11	107	214	1	8.2
A003	270	270	0.0	53544	3	.1	7	95	348	1	6.0
R	266	270	REPRESENTS DIVISIONS OF THE PROMINENT STRUCTURE IN THIS TRENCH								
A003	310	311	0.1	53545	3	.1	9	203	527	1	5.4
A003	349	349	0.0	53546	3	.2	11	335	892	1	4.9
A003	355	355	0.0	53547	3	.1	17	701	804	1	6.7
A003	409	409	0.0	53548	3	.5	72	102	443	1	5.3
A003	407	407	0.0	53564	3	.3	6	56	338	1	7.1
/END											

TRENCH 0170W

-----  
 IDEN6B0201 V232TR0170W 07JUL89RGMMD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 200 MT 39.7 018.0 2.0 184.0 -170.0 1310.00

R From To  
 R THIS TRENCH IS AN EXTENSION OF TR0265N WHICH TESTS SOIL AND AN  
 R IP ANOMALIES  
 / 00 09 OVBN P  
 / 09 397 PPFQLIPYQZ6PPR5 P P6P= D)  
 L 7ACYFX3 445 C2  
 R REMNANT FX CRYSTALS MAY OCCASIONALLY BE SEEN BUT ARE THOURGHLY  
 R ALTERED TO KA  
 R THE MATRIX IS EXTREMELY SILICIFIED AND APHANITIC, QTZ ALSO  
 R OCCURS AS AUGENS  
 / 61 68 XPPFQLIPYQZ6PPR5 D P6P2 D)  
 L 7ACYFX3 777 C2  
 / 216 216 XPPFQLIPYQZ4PPR5 D P4P1 D+  
 L WACYFX4 <=  
 R GRAB SAMPLE OF HEAVIER PYRITE  
 R AT 2.9 M, SHEAR ZONE TRENDING 120 DEGREES, 8 CM WIDE.  
 R TRENCH ENDS DUE TO ROAD CROSSING

A001

AUMM	From	To	LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB
R				ppb	ppm	ppm	ppm	ppm	ppm	ppm
ALAB			Eco Tech - Kamloops							
ATYP			Chip Samples							
R	00	09	NO SAMPLE-OVBN							
A001	09	25	1.6 53455	5	.7	7	156	182	4	.1
A001	25	40	1.5 53456	5	1.4	5	97	70	7	.1
A001	40	61	2.1 53457	10	.7	6	165	82	14	.1
A001	61	68	0.7 53458	10	.4	4	230	72	23	.1
A001	68	84	1.6 53459	10	.2	3	64	48	7	.1
A001	84	100	1.6 53460	5	.5	2	34	53	4	.1
A001	100	115	1.5 53461	5	.1	2	33	42	14	.1
A001	115	130	1.5 53462	5	.3	3	53	33	6	.1
A001	130	145	1.5 53463	5	.2	4	41	99	12	.1
A001	145	160	1.5 53464	5	.3	4	30	114	7	.1
A001	160	175	1.5 53465	10	.1	6	40	71	6	.1
A001	175	190	1.5 53466	10	.1	9	45	59	12	.1
A001	190	205	1.5 53467	5	.2	2	68	32	8	.1
A001	205	220	1.5 53468	5	.1	3	125	41	11	.1
A001	220	235	1.5 53470	5	.4	2	56	31	17	.1
A001	235	250	1.5 53471	10	.2	1	36	26	30	.1
A001	250	265	1.5 53472	5	.1	4	40	83	15	.1
A001	265	280	1.5 53473	5	.1	12	52	69	6	.1
A001	280	295	1.5 53474	5	.1	4	98	99	7	.1
A001	295	310	1.5 53475	5	.1	2	98	70	10	.1
A001	310	325	1.5 53476	10	.2	3	63	102	3	.1
A001	325	340	1.5 53477	5	.8	7	115	192	6	.1
A001	340	355	1.5 53478	5	.7	9	114	176	12	.1

A001	355	370	1.5	53479	10	.7	6	157	177	14	.1
A001	370	385	1.5	53480	5	.9	6	110	158	6	.1
A001	385	397	1.2	53481	5	.7	3	136	136	7	.1
A002											
AUMM	SAMPLE				Au	Ag	Cu	Pb	Zn	As	Sb
ALAB	Echo Tech - Kamloops										
ATYP	Grab Samples										
A002	216	216		53469	5	.3	3	250	11	14	.1
R	Grab sample of pyrite rich ppfq, relatively (=4%)										
A003											
AUMM	LNG SAMPLE				Au	Ag	Cu	Pb	Zn	As	Sb
ALAB	Echo Tech - Kamloops										
ATYP	Extra Samples Taken Along Structures, Etc.										
A003	29	29	0.8	53653	35	1.7	2.8	403	140	6	0.1
R	Sample taken along fault gouge										
/END											

TRENCH 0265N

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IDEN6B0201 V232TR0265N 29JUN89RGMMD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 100 MT 29.5 015.0 -08.0 265.0 -130.0 1270.00  
 S001 100 250 29.5 015.0 03.0  
 S002 250 295 29.5 015.0 -18.0

R From To (mt)  
 R THIS TRENCH IS TO TEST A PROJECTION OF AN OLD IP ANOMALY AS  
 R WELL AS A GOLD-IN-SOIL ANOMALY  
 / 00 115 PPFQ KF2PPRW P P4U1 D=  
 L AU QZ2AG C1T+  
 R STRONG LI COATINGS & FRACT.FILLINGS;SILIC'D PPFQ W. MINOR PY  
 / 75 83 XPPFQ FX2PPRW D P6F1 D\*  
 L AW QZ2 T=  
 R STRONGLY SILICIFIED, PL STAINED PPFQ W. MINOR DISS. PY  
 / 115 295 PPFQ QZ2PPRW P P4U1 D=  
 L AU FX1VG <1T\*  
 R PY ALSO OCCURS AS BOXWORK TEXT.,LI COATS KF XTALS  
 / 275 295 XPPFQ QZ2PPRW D P5F+ D1  
 L AW FX1AG C+  
 R STRONGLY SILICIFIED PPFQ W. DISS. & PATCHES OF PY  
 R THIS TRENCH WAS DISCONTINUED DUE TO DEEP OVBN

A001

AUMM	From	To	LNG SAMPLE	Au ppb	Ag ppm	Cu ppm	Pb ppm	Zn ppm	As ppm	Sb ppm
ALAB	Eco Tech - Kamloops									
ATYP	Chip Samples									
A001	00	15	1.5 53335	15	.5	3	20	56	6	.1
A001	15	30	1.5 53336	15	.3	3	21	55	5	.1
A001	30	45	1.5 53337	10	.4	3	30	63	10	.1
A001	45	60	1.5 53338	5	.5	3	27	67	6	.1
A001	60	75	1.5 53339	10	.5	2	34	52	7	.1
A001	75	83	0.8 53340	10	.1	2	10	28	13	.1
A001	83	100	1.7 53341	15	.5	3	48	49	8	.1
A001	100	115	1.5 53342	10	.5	3	33	53	1	.1
A001	115	130	1.5 53343	20	.7	4	69	58	1	.1
A001	130	145	1.5 53344	5	.7	4	59	67	13	.1
A001	145	160	1.5 53345	15	.9	4	139	76	26	.1
A001	160	175	1.5 53346	10	.7	5	143	65	7	.1
A001	175	190	1.5 53347	10	.6	5	199	68	20	.1
A001	190	205	1.5 53348	5	1.1	5	463	77	18	.1
A001	205	220	1.5 53349	10	.8	5	383	63	14	.1
A001	220	235	1.5 53350	10	1.3	6	445	100	14	.1
A001	235	250	1.5 53351	15	1.1	4	218	41	11	.1
A001	250	265	1.5 53352	15	.9	8	312	88	13	.1
A001	265	275	1.0 53353	10	.6	10	219	109	11	.1
A001	275	295	2.0 53354	10	.9	5	620	156	16	.1

/END

TRENCH 0837N

-----  
 IDEN680201 V232TR0837N 29JUN89RGMMD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG

/SCL MT.2  
 LSCL LCTM  
 S000 00 100 MT 17.8 060.0 -18.0 837.0 -255.0 1310.00  
 S001 100 178 17.8 060.0 -05.0

R From To  
 R THIS TRENCH IS AN EXTENSION OF TR0847N TO TEST A MULTI-  
 R ELEMENT SOIL ANOMALY  
 / 00 15 PPFQKF FX2PPRW P P5F= < D\*  
 L AG Q22AG C=C+  
 / 15 100 PPFQ FX2PPRW P P4F+ D+  
 L AU Q22AG 7 C=T3T=  
 R STRONGLY FRACTURED, WEATHERED AND PL STAINED PPFQ  
 R FRACTURES ARE NUMEROUS AND STRIKE 010-025 DEGREES  
 R TRENCH WAS DUG 60 CM THROUGH EXTREMELY WEATHERED BEDROCK  
 / 20 25 XPPFQ FX2PPRW D P4F2 D+  
 L AW Q22AG C)  
 R SHORT INTERVAL OF SLIGHTLY WEATHERED, REWORKED PPFQ  
 / 100 140 PPFQ FX2PPRW P P4F2 D1  
 L AW Q22AG<< 7 C)T+T\*  
 R PY OCCURS AS BLEBS, DISS & MICROVEINS. SILICA MICROVEINS PRESENT  
 / 126 133 XFAUL Q22AG D SH018 P7  
 L WA T1  
 / 140 178 PPFQFX Q22PPRW P P3F\* D=  
 L AW KF2AG C=T1  
 R A COARSER-GR., FRESHER PPFQ, MOD. SILICIFIED W. MINOR PL STAINING  
 / 155 165 XFAUL Q22AG D SH015 P7  
 L WA T\*T)  
 R THIS TRENCH ENDS 10 SOUTH OF WHERE TR0847N BEGINS.

A001  
 AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
 R From To ppb ppm ppm ppm ppm ppm ppm

ALAB Eco Tech - Kamloops  
 ATYP Chip Samples

A001	From	To	LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB
				ppb	ppm	ppm	ppm	ppm	ppm	ppm
A001	00	15	1.5 53319	5	.2	7	31	607	5	.1
A001	15	30	1.5 53321	10	.4	8	162	294	10	.1
A001	30	45	1.5 53322	5	.4	7	105	255	10	.1
A001	45	60	1.5 53323	10	.2	6	73	297	6	.1
A001	60	75	1.5 53324	10	.3	7	123	284	6	.1
A001	75	90	1.5 53325	5	.3	6	131	307	15	.1
A001	90	100	1.5 53326	5	.3	6	98	265	7	.1
A001	100	115	1.5 53327	5	.5	5	91	215	13	.1
A001	115	130	1.5 53328	10	.9	10	136	589	16	.1
A001	130	140	1.0 53330	10	.6	10	72	327	40	.1
A001	140	155	1.5 53331	10	.5	7	64	345	12	.1
A001	155	170	1.5 53332	5	.7	8	48	421	19	.1
A001	170	178	0.8 53333	5	.6	3	15	94	10	.1

A003  
 AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
 ALAB Echo Tech - Kamloops



ATYP                    Extra Samples Taken Along Structures, Etc.  
A003 24    24 1.0 53320    10   .2    7   31   607   5   .1  
R                    WHITE-GREY,SILIC,D PPFQ X-CUTTING TRENCH,WEAK CLAY ALT.  
A003 126   133 0.7 53329    5   1.9   11   50   449   39   .1  
R                    CLAY ALT'D FAULT GOUGE  
A003 155   165 1.0 53334    20   1.2    7   35   268   23   .1  
R                    CLAY ALT'D FAULT GOUGE  
/END

TRENCH 0847N

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IDEN680201 V232TR0847N 29JUN89RGMJD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG

/SCL MT.2  
 LSCL LCTM  
 S000 00 275 MT 32.3 065.0 -10.0 847.0 -230.0 1305.00  
 S001 275 323 32.3 065.0 -10.0

R From To  
 R THIS TRENCH WAS DUG TO TEST A MULTI-ELEMENT SOIL ANOMALY  
 / 00 18 PPFQPPYFX3PP P P4 D=D)  
 L WAPLQZ4 6 C+C+  
 R QTZ ALSO OCCURS IN EUHEDRAL X-TALS UP TO 1.5 CM  
 / 18 37 PPFQPYCYFX3PPR5 6 P P6 D1  
 L UW QZ5 C1  
 R WEATHERING COLOUR CHANGES HERE;FROM BLACKISH(PL) TO YEL-BRW(LI)  
 R INTERVAL 1.8-3.7 BORDERS ON VEINING;TRENDS N-S  
 / 37 210 PPFQPYPLFX3PP 7 P P4 D+  
 L WA QZ4 C)C)  
 / 70 70 XFAUL CYX D PX  
 L W  
 R EXTREMELY CLAY-ALT'D FAULT GOUGE IN PPFQ  
 / 210 323 PPFQPYLIQZ4PPR7 P P4 D3 D1  
 L WAKAFX3 C+  
 R CHANGE IN ROCK TYPE IS COINCIDENT WITH A STEEP DIP IN BEDROCK  
 / 271 271 XPPFQ D  
 R ENCOUNTERED A SINGLE LENS/VEIN OF GALENA?  
 R THIS TRENCH ENDS DUE TO A STEEP DROP IN THE BEDROCK.

A001		ALAB									
AUMM		Eco Tech - Kamloops									
R		Chip Samples									
	From	To	LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB	
				ppb	ppm	ppm	ppm	ppm	ppm	ppm	
A001	00	17	1.7 53222	10	.7	3	64	305	46	.1	
A001	17	37	2.0 53223	10	1.5	2	68	186	18	.1	
A001	37	50	1.3 53224	3	.6	4	108	282	26	.1	
A001	50	65	1.5 53225	3	.6	3	131	221	10	.1	
A001	65	80	1.5 53251	3	.8	8	90	447	16	.1	
A001	80	95	1.5 53253	3	.6	5	83	352	13	.1	
A001	95	110	1.5 53254	3	.6	3	71	215	10	.1	
A001	110	125	1.5 53255	10	1.8	7	117	295	18	.1	
A001	125	140	1.5 53256	10	1.3	7	213	241	13	.1	
A001	140	155	1.5 53257	3	.1	4	201	166	14	.1	
A001	155	170	1.5 53258	5	.1	7	341	229	13	.1	
A001	170	185	1.5 53259	10	.1	6	95	212	14	.1	
A001	185	200	1.5 53260	3	.8	7	76	202	13	.1	
A001	200	215	1.5 53261	3	.9	6	85	258	17	.1	
A001	215	230	1.5 53262	5	1.1	7	61	311	12	.1	
A001	230	245	1.5 53263	10	5.1	45	56	3000	20	.1	
A001	245	260	1.5 53264	15	1.8	23	66	1200	15	1.0	
A001	260	275	1.5 53265	5	1.8	15	233	783	12	.1	
A001	275	290	1.5 53266	20	6.3	55	3000	2300	14	.4	
A001	290	305	1.5 53267	5	1.5	41	218	1500	10	.1	

R 305 323 NO SAMPLE-OVBN  
A003  
AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
ALAB Echo Tech - Kamloops  
ATYP Extra Samples Taken Along Structures, Etc.  
A003 70 70 53252 3 .7 7 53 178 7 .1  
R SAMPLE TAKEN ALONG FAULT GOUGE,EXTREME CLAY ALT.  
/END

TRENCH 0930N

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IDEN680201 V232TR0930N 28JUN89RGMMJD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG

/SCL MT.2  
 LSCL LCTM  
 S000 00 105 MT 10.5 64.0 -04.0 930.0 -206.0 1300.00

R From To  
 R THIS TRENCH WAS DUG TO TEST A MULTI-ELEMENT SOIL ANOMALY AND  
 R TO ATTEMPT TO EXPOSE AN ALTERATION ZONE VISIBLE ON THE ROAD  
 / 00 105 PPFQ FX3PP P P6C) D\*  
 L RA QZ6 6 C+C+P2  
 R THE FX AND QZ PHENOS ARE VERY SMALL;REWORKED,AND THE KF PHENOS.  
 R ARE HE/LI STAINED. HE STAINING IS ALSO PERVASIVE THROUGHOUT THE  
 R FINE GRAINED MATRIX.  
 / 50 76 XFAUL D  
 L 888  
 R EXTREMELY CLAY-ALTERED FAULT GOUGE  
 R FRACTURE SET IS VERY DISTINCT & PL WEATHERING COLOUR ALSO  
 R DISTINCT BETWEEN 0.0-5.0  
 R SMALL WHITE CLAY ALT'D VEINS BETWEEN 7.2-7.6  
 R THIS TRENCH WAS DISCONTINUED DUE TO DEEP OVBN.

A001

AUMM	From	To	LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB
R				ppb	ppm	ppm	ppm	ppm	ppm	ppm
ALAB	Eco Tech - Kamloops									
ATYP	Chip Samples									
R	00	05	NO SAMPLE-OVBN							
A001	05	20	1.5 53312	3	.1	10	20	1000	9	.1
A001	20	35	1.5 53313	5	.1	14	35	700	10	.1
A001	35	50	1.5 53314	3	.1	13	25	1000	17	.1
A001	50	65	1.5 53315	5	.6	9	78	260	8	.1
A001	65	76	1.1 53316	3	.4	7	59	211	17	.1
A001	76	90	1.4 53317	5	.3	8	29	360	24	.1
A001	90	105	1.5 53318	5	.2	11	19	347	30	.1

/END

TRENCH 0969N

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IDEN680201 V232TR0969N 27JUN89RGMMD UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 58 MT 58.0 095.0 -20.0 969.0 -330.0 1305.00  
 S001 58 195 MT 58.0 085.0 -07.0  
 S002 195 580 MT 58.0 075.0 -12.0

R From To  
 R THIS TRENCH TESTS A MULTI-ELEMENT SOIL ANOMALY AND TO TEST THE  
 R EXTENT OF INTENSE ALTERATION ZONE EXPOSED ALONG A NEARBY ROAD  
 / 00 97 PPFQHECYFX4PPR5 P P4C\* D\* D\*  
 L AR Q24 4 C)C)P2  
 R HEMATITE? STAINING IS PERVASIVE IN THE MATRIX.  
 R PY AND POSSIBLY GL ARE DISS. IN FINE GRAINS THROUGHOUT MATRIX.  
 / 46 60 XPPFQ D  
 L 6  
 R THIS INTERVAL REFLECTS AN INCREASE IN FRACTURE INTENSITY.  
 / 60 97 XPPFQ D  
 L 7 C1  
 R THIS SECTION SHOWS AN EVEN HIGHER FRACTURE INTENSITY AND INC-  
 R REASE IN LIMONITE CONTENT.  
 / 97 113 XOVBN P  
 / 113 369 PPFQPLLIFX3PP P P5C\* D\*  
 L WA Q25 4 4 C)C\*O\*  
 / 369 446 PPFQCYLIFX3 P P5<1 D)  
 L UA Q25 76 C1D)  
 R CLAY ALT. IN MICROVEINS REFERS TO (THIS) PGI SCALE  
 R PL OCCURS AS D AND C  
 R PY IS EXT. FINE GRAINED  
 R EXTREMELY WEATHERED SECTION  
 / 446 550 PPFQHEPLFX3PP P P5C\* D)  
 L AR Q25 6 C)C=O2  
 R HEMATITE STAINING IS PERVASIVE ENOUGH TO CAUSE A COLOUR CHANGE  
 R IN THE MATRIX.  
 R PL SHOWS A DENDRITIC WEATHERING PATTERN AS WELL AS C AND DISS  
 / 486 550 XPPFQ D  
 L 7  
 R UNIQUE FRACTURE PATTERN,HIGH INTENSITY AND STRIKING E-W  
 / 550 580 PPFQLICYFX3PPR5 P P5C1 D)  
 L 1U Q25 888 C2  
 R EXTREME WEATHERING LI AND CY ALT.,INCREASE IN FRACTURING W. SI  
 R FLOODING IN SOME FRACTURES.  
 R SECTIONS OF EXTREMELY WEATHERED ROCK AND MORE LI AND CY ALT.  
 R SEEM TO BE FAULT RELATED AS THEY ARE COMPOSITIONALLY VERY SIMILAR  
 R I.E. PY CONCENTRATION IS CONSISTENTLY SPARSE.  
 R TRENCH ENDS BECAUSE OF ROAD X-ING.

A001  
 AUMM LNG SAMPLE AU AG CU PB ZN AS SB  
 R From To ppb ppm ppm ppm ppm ppm ppm  
 ALAB Eco Tech - Kamloops  
 ATYP Chip Samples

A001	00	15	1.5	53268	15	.1	4	21	360	9	.1
A001	15	30	1.5	53269	10	.1	4	17	270	8	.1
A001	30	46	1.6	53270	5	.1	3	16	283	10	.1
A001	46	60	1.4	53271	15	.2	4	29	228	30	.1
A001	60	75	1.5	53272	5	.6	3	34	130	44	.1
A001	75	85	1.0	53273	5	.5	4	29	110	50	.1
A001	85	97	1.2	53274	10	.6	3	32	109	47	.1
R	97	113	1.7	NO SAMPLE-OVBN							
A001	113	130	1.5	53275	5	.1	3	40	205	14	.3
A001	130	145	1.5	53276	5	.1	3	22	170	9	.1
A001	145	160	1.5	53277	3	.1	3	21	150	7	.1
A001	160	175	1.5	53278	5	.1	3	28	182	6	.1
A001	175	190	1.5	53279	5	.1	3	32	195	25	.1
A001	190	205	1.5	53280	5	.1	3	20	194	8	.1
A001	205	220	1.5	53281	5	.1	5	39	190	6	.1
A001	220	235	1.5	53282	5	.1	3	27	237	5	.1
A001	235	250	1.5	53283	5	.1	3	19	148	5	.1
A001	250	265	1.5	53284	35	.1	3	22	116	6	.1
A001	265	280	1.5	53285	5	.1	3	17	160	7	.1
A001	280	295	1.5	53286	5	.1	2	21	172	3	.1
A001	295	310	1.5	53287	5	.1	2	20	177	11	.1
A001	310	325	1.5	53288	5	.1	3	29	205	12	.1
A001	325	340	1.5	53289	3	.1	3	23	55	7	.1
A001	340	355	1.5	53290	5	.1	2	19	168	6	.1
A001	355	369	1.4	53291	5	.1	2	23	227	11	.1
A001	369	385	1.6	53292	5	.2	4	43	169	18	.1
A001	385	400	1.5	53293	5	.1	3	32	250	15	.1
A001	400	415	1.5	53294	5	.4	6	107	230	15	.1
A001	415	430	1.5	53295	5	1.3	10	145	232	40	.1
A001	430	446	1.6	53296	5	.1	4	22	156	30	.1
A001	446	460	1.4	53297	5	.1	5	20	183	34	.1
A001	460	475	1.5	53298	5	.1	4	22	200	12	.1
A001	475	490	1.5	53299	10	.1	3	20	200	11	.1
A001	490	503	1.3	53300	5	.1	2	26	215	9	.1
A001	503	518	1.5	53301	3	.1	2	27	180	10	.1
A001	518	533	1.5	53303	10	.1	2	15	125	6	.1
A001	533	550	1.8	53305	10	.1	2	21	138	20	.1
A001	550	565	1.5	53306	10	.1	7	16	85	38	.1
A001	565	580	1.5	53311	5	.5	7	21	122	33	.1
A002											
AUMM	SAMPLE				Au	Ag	Cu	Pb	Zn	As	Sb
ALAB	Eco Tech - Kamloops										
ATYP	Grab Samples										
A002	565	565	53309	3	.1	7	8	54	4	.1	
R	MOD. CLAY ALT'D & SILICIFIED PPFQ										
A002	573	573	53310	3	.2	5	11	32	7	.1	
R	SAME AS ABOVE										
A003											
AUMM	LNG SAMPLE				AU	AG	CU	PB	ZN	AS	SB
ALAB	Eco Tech - Kamloops										
ATYP	Samples taken along structures										
A003	510	518	0.8	53302	15	.2	3	32	231	9	.1
R	CLAY ALT'D FAULT GOUGE										
A003	518	527	0.9	53304	5	.2	2	29	155	6	.1
R	SAME AS ABOVE										
A003	551	560	0.9	53307	20	.8	7	42	190	43	.1

R SAME AS ABOVE  
A004  
AUMM LNG SAMPLE Au Ag Cu Pb Zn As Sb  
ALAB Eco Tech - Kamloops  
ATYP Repeat samples taken along intervals  
A004 550 575 2.5 53308 5 .3 6 14 117 27 .1  
R REPEAT SAMPLE OF 53306-53307  
/END

TRENCH 3228E

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 IDEN680201 V232TR3228E 12JUL89RGM UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 270 MT 27.0 158.0 -18.0 629.0 3228.0 1320.00

R From To  
 R THIS TRENCH WAS DUG TO TEST A GOLD-IN-SOIL GEOCHEM ANOMALY  
 / 00 08 OVBN P  
 / 08 37 CGGNFXLIQZ4GT P  
 L YN B14 <+  
 / 08 37 5QBGNFX QZ3EQ D  
 L 3A B13  
 / 37 57 QBGNFXLIQZ3EQR2 P P1P1 D(  
 L 3APYB13 557 P3  
 / 55 55 XFAUL D P2  
 L 777 P4  
 / 57 78 CGGNFX QZ5EQGT P P2 D+  
 L WNPYB13R2 <+  
 / 78 144 QBGNFX QZ6EQR5 P P6 D)  
 L 4A B13 <1  
 R HORNFELED TEXTURES ARE SEEN NEAR THE GN GR CONTACTS  
 / 144 164 GRANFXHBQZ3EQGT P  
 L WN B14 334  
 / 164 176 OVBN P  
 / 190 270 QBGNFXPYQZ4EQR2 P P1 D\*  
 L 3ALIB13 334 <1  
 / 214 219 XFAUL D  
 L 778 P4

R THIS TRENCH WAS ENDED DUE TO THE EXTENT OF THE SOIL ANOMALY

A001

AUMM LNG SAMPLE Au Ag Cu Pb Zn As Sb  
 R From To ppb ppm ppm ppm ppm ppm ppm  
 ALAB Eco Tech - Kamloops  
 ATYP Chip Samples

R 00 08 0.8 NO SAMPLE-OVBN  
 A001 08 20 1.2 53517 5 .1 16 15 78 10 .6  
 A001 20 37 1.7 53518 3 .1 8 10 64 8 .6  
 A001 37 45 0.8 53519 3 .1 17 18 106 5 .5  
 A001 45 57 1.2 53520 3 .1 12 16 135 7 .3  
 A001 57 78 2.1 53522 3 .2 1 20 112 32 2.3  
 A001 78 90 1.2 53525 3 .2 18 35 250 48 5.1  
 A001 90 105 1.5 53526 10 .2 10 17 111 13 .4  
 A001 105 120 1.5 53527 3 .2 4 12 91 19 .7  
 A001 120 135 1.5 53528 3 .1 1 11 117 44 3.4  
 A001 135 144 0.9 53529 3 .2 76 14 266 42 10.5  
 A001 144 164 2.0 53530 3 .2 2 24 229 14 2.8  
 R 164 176 1.2 NO SAMPLE-OVBN  
 A001 176 190 1.4 53531 3 .1 10 20 81 9 .5  
 A001 190 205 1.5 53532 5 .1 2 26 111 8 .3  
 A001 205 214 0.9 53533 3 .1 1 26 77 10 .2  
 A001 214 219 0.5 53534 10 .2 27 16 267 16 1.1



A001	219	230	1.1	53535	5	.1	10	25	198	27	1.8
A001	230	245	1.5	53536	3	.1	24	17	231	28	2.2
A001	245	260	1.5	53537	3	.1	34	15	135	20	1.5
A001	260	270	1.0	53538	5	.1	23	7	89	7	.6
A003											
AUMM				LNG SAMPLE	AU	AG	CU	PB	ZN	AS	SB
ALAB				Echo Tech - Kamloops							
ATYP				Extra Samples Taken Along Structures, Etc.							
A003	57	57	1.0	53521	3	.2	2	9	485	14	2.0
R				Sample along fault gouge ie heavy clay alt.							
/END											

TRENCH 3427E

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IDEN6B0201 V232TR3427E 11JUL89RGM UTM340.0  
 IPRJ PLACER DOME INC., KAMLOOPS OFFICE SPRING PROJECT  
 /NAM SICYKACBCLPYCPGLSL  
 LNAM LIPLHEMG  
 /SCL MT.2  
 LSCL LCTM  
 S000 00 50 MT 69.5 169.0 -24.0 690.0 3427.0 1340.00  
 S001 50 97 169.0 14.0  
 S002 97 175 169.0 0.0  
 S003 175 400 153.0 -18.0  
 S004 400 555 153.0 0.0  
 S005 555 695 164.0 -05.0

R From To  
 R THIS TRENCH WAS DUG TO TEST A GOLD-IN-SOIL GEOCHEM ANOMALY  
 / 00 195 QBGNLIPHQZ4EQSC P P4 D(  
 L UNPYBI3 424 P1  
 R LI IS ALSO OCCURRING AS MICROFRACTURE INFILLINGS AND COATINGS  
 / 31 150 XQBGN D P1  
 L 437 C2  
 R THIS INTERVAL HAS A RECCESIVE WEATHERING PATTERN AND THEREFORE  
 R AN INCREASE IN LI STAINING AND CY ALT DUE TO INCREASED  
 R FRACTURING.  
 / 34 34 XFAUL CY4 D 090 P1P4  
 L WJ LI4 P4  
 / 90 102 XOVBN D  
 / 195 298 GRANHBPHQZ3 P  
 L W BI3  
 / 245 247 XQBGN D P5 D)  
 R THIS INTERVAL CLOSELY RESEMBLES 00 TO 195, WITH HIGHER PY AND  
 R SILICIFICATION (ZENOLITH), GRAB TAKEN.  
 / 298 405 QBGNLIPHQZ4EQSC P P4 D(  
 L UNPYBI3 424 P1  
 / 405 555 OVBN P  
 R TRENCH CROSSES A LOGGING ROAD  
 / 555 675 QBGNLIPHQZ4 P P4 D)  
 L UN BI3 536  
 / 575 589 XQBGN D P5  
 L 223  
 R THIS INTERVAL IS A COMPETENT SECTION OF THE ROCK DESCRIBED  
 R PROBABLY DUE TO AN INCREASE IN SILICA CONTENT, GRAB TAKEN.  
 / 675 695 OVBN P  
 R TRENCH ENDS DUE TO THE EXTENT OF THE SOIL ANOMALY

A001

AUMM	From	To	LNG SAMPLE	Au ppb	Ag ppm	Cu ppm	Pb ppm	Zn ppm	As ppm	Sb ppm
ALAB	Eco Tech - Kamloops									
ATYP	Chip Samples									
A001	00	15	1.5 53482	5	.1	246	15	87	24	1.5
A001	15	31	1.5 53483	3	.1	137	20	78	23	.9
A001	31	37	0.6 53484	3	.3	869	15	99	41	2.8
A001	37	46	0.9 53486	5	.5	811	15	130	46	1.3
A001	46	58	1.2 53487	3	.1	36	12	166	15	1.2
A001	58	76	1.8 53488	10	.1	185	11	103	37	1.3



**APPENDIX V**

**Listing of Trench Soil Profile Sample Data**

SPRING PROJECT SOIL PROFILES  
1989 TRENCHES

LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9285	TR001E	0+43 SA	30	0.1	2.5	30	106	280
9285	TR001E	0+43 SB	100	0.1	2.5	15	25	105
9285	TR001E	0+43 SA	30	0.4	2.5	32	50	170
9285	TR001E	0+43 SB	120	1.6	2.5	2	97	81
9285	TR001E	0+43 SA	30	0.4	2.5	43	93	221
9285	TR001E	0+43 SB	60	0.4	2.5	42	87	290
9285	TR001E	0+43 SA	30	0.4	2.5	34	44	156
9285	TR001E	0+43 SB	100	0.2	2.5	28	640	4200
9285	TR001E	0+53 SA	30	0.4	2.5	25	57	206
9285	TR001E	0+53 SA*	70	0.4	2.5	26	58	211
9285	TR001E	0+53 SB	70	0.2	2.5	27	44	148
9285	TR001E	0+50 NA	15	0.1	2.5	15	24	123
9285	TR001E	0+50 NB	70	0.1	5	25	47	181
9285	TR001E	0+50 NC	150	0.4	5	144	64	770
9285	TR001E	0+60 NA	15	0.2	2.5	17	32	130
9285	TR001E	0+60 NB	80	0.4	5	24	34	160
9285	TR001E	0+60 NC	200	0.8	2.5	54	55	218
9285	TR001E	0+70 NA	20	0.6	5	22	42	151
9285	TR001E	0+70 NA*	20	0.6	10	23	48	170
9285	TR001E	0+70 NB	70	0.1	2.5	18	24	108
9285	TR001E	0+70 NC	175	0.1	2.5	7	15	124
9212	TR0170W	1+84 NA	10	0.3	5	14	48	620
9212	TR0170W	1+84 NB	130	0.2	5	28	104	291
9212	TR0170W	1+94 NA	10	0.3	10	10	35	460
9212	TR0170W	1+94 NB	70	0.1	10	14	44	190
9212	TR0170W	2+04 NA	10	0.3	15	9	32	350
9212	TR0170W	2+04 NB	110	0.1	2.5	21	62	157
9212	TR0170W	2+14 NA	10	0.2	15	9	44	490
9212	TR0170W	2+14 NB	100	0.1	10	16	93	265
9212	TR0170W	2+24 NA	25	0.2	10	12	57	358
9212	TR0170W	2+24 NA*	25	0.3	10	11	56	353
9212	TR1335W	11+50 SA	20	1.2	2.5	7	24	325
9212	TR1335W	11+50 SB	120	0.4	2.5	10	54	165
9212	TR1335W	11+50 SC	220	0.4	2.5	17	137	350
9212	TR1335W	11+50 SD	300	0.4	2.5	12	68	257
9212	TR1335W	11+60 SA	20	0.4	2.5	6	38	256
9212	TR1335W	11+60 SB	120	0.2	2.5	6	60	230
9212	TR1335W	11+60 SC	220	0.5	2.5	15	135	343
9212	TR1335W	11+60 SD	320	0.2	2.5	8	58	141
9212	TR1335W	11+70 SA	20	0.4	2.5	7	36	300
9212	TR1335W	11+70 SB	120	0.4	2.5	9	71	203
9212	TR1335W	11+70 SC	220	1.2	2.5	17	76	358
9212	TR1335W	11+70 SD	320	0.2	2.5	13	66	234
9212	TR1335W	11+77 SA	20	0.8	2.5	7	32	245
9212	TR1335W	11+77 SB	120	0.3	2.5	3	18	80
9212	TR1335W	11+77 SC	220	0.4	30	39	77	173
9212	TR1378W	10+72 SA	20	1.0	20	8	35	354
9212	TR1378W	10+72 SB	160	0.7	20	10	80	254

LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9212	TR1378W	10+82 SA	20	0.7	5	6	27	347
9212	TR1378W	10+82 SA*	20	0.7	5	6	26	320
9212	TR1378W	10+82 SB	160	0.3	10	8	77	200
9212	TR1378W	10+82 SC	200	10.0	5	18	102	195
9212	TR1378W	10+92 SA	20	0.8	2.5	7	33	276
9212	TR1378W	10+92 SB	160	6.0	2.5	23	254	334
9212	TR1378W	11+02 SA	20	1.1	2.5	8	25	260
9212	TR1378W	11+02 SB	160	8.0	2.5	21	106	190
9212	TR1378W	11+12 SA	20	1.0	2.5	12	41	330
9212	TR1378W	11+12 SB	160	1.6	2.5	12	92	204
9212	TR1378W	11+24 SA	20	1.0	2.5	9	30	338
9212	TR1378W	11+24 SA*	20	0.9	2.5	8	30	333
9212	TR1378W	11+24 SB	160	1.5	2.5	16	78	223
9212	TR1378W	11+24 SB*	160	1.6	2.5	16	80	228
9191	TR0265N	1+00 WA	30	0.4	25	12	128	600
9191	TR0265N	1+00 WB	100	0.7	35	26	3.4	1100
9191	TR0265N	1+10 WA	30	0.2	20	12	72	630
9191	TR0265N	1+20 WA	30	0.3	20	9	51	620
9191	TR0265N	1+20 WB	100	0.1	2.5	10	26	380
9191	TR0265N	1+30 WA	30	0.4	5	10	34	580
9191	TR0265N	1+30 WB	100	0.4	30	40	80	550
9191	TR0837N	2+40 WA	30	0.2	10	16	104	1100
9191	TR0837N	2+40 WB	120	0.2	40	23	210	1230
9191	TR0837N	2+55 WA	20	0.6	25	7	46	640
9191	TR0837N	2+55 WB	120	0.1	40	24	207	1030
9191	TR0847N	2+00 WA	15	1.1	35	8	32	600
9191	TR0847N	2+00 WB	100	0.5	45	44	167	1050
9191	TR0847N	2+00 WC	200	0.2	50	21	62	900
9191	TR0847N	2+10 WA	15	1.0	35	6	24	700
9191	TR0847N	2+10 WB	115	0.5	25	10	102	620
9191	TR0847N	2+20 WA	15	0.2	10	12	56	1000
9191	TR0847N	2+20 WB	115	0.3	25	26	124	1320
9191	TR0847N	2+20 WB*	115	0.3	15	29	134	1400
9191	TR0847N	2+20 WC	155	0.8	20	41	161	1680
9191	TR0847N	2+30 WA	15	1.2	10	21	21	800
9191	TR0847N	2+30 WB	115	0.4	30	24	62	1030
9191	TR0847N	2+30 WC	155	0.4	10	36	206	1540
9191	TR0930N	1+96 WA	30	0.2	10	44	36	1320
9191	TR0930N	1+96 WB	100	0.1	10	34	17	1530
9191	TR0930N	2+06 WA	30	0.3	2.5	6	20	403
9191	TR0930N	2+06 WB	130	0.3	20	26	61	850
9191	TR0969N	2+72 WA	30	0.5	40	17	186	790
9191	TR0969N	2+72 WA*	30	0.5	60	16	190	800
9191	TR0969N	2+80 WA	30	1.1	35	6	32	1000
9191	TR0969N	2+80 WB	120	1.1	40	24	120	1000
9191	TR0969N	2+90 WA	30	0.8	20	7	35	1100
9191	TR0969N	2+90 WB	130	0.6	50	27	570	1130

LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9191	TR0969N	3+00 WA	30	0.4	35	8	40	1270
9191	TR0969N	3+00 WB	120	0.3	35	16	78	920
9191	TR0969N	3+10 WA	30	0.4	10	5	26	720
9191	TR0969N	3+10 WB	100	0.6	20	17	62	860
9191	TR0969N	3+20 WA	30	0.4	2.5	6	41	740
9191	TR0969N	3+20 WA*	30	0.2	2.5	6	38	700
9191	TR0969N	3+20 WB	100	1.0	10	14	205	840
9191	TR0969N	3+30 WA	30	0.7	2.5	8	91	700
9191	TR0969N	3+30 WB	120	0.9	2.5	36	1020	1560
9191	TR1010W	10+65 SA	30	0.8	2.5	8	53	360
9191	TR1010W	10+65 SB	80	0.7	2.5	19	64	401
9191	TR1010W	10+65 SC	250	0.8	5	22	120	343
9191	TR1010W	10+75 SA	30	0.8	2.5	8	56	540
9191	TR1010W	10+75 SB	80	1.9	2.5	35	98	570
9191	TR1010W	10+75 SC	200	1.8	2.5	65	56	382
9191	TR1010W	10+75 SC*	200	1.8	5	55	56	360
9191	TR1010W	10+85 SA	30	1.2	2.5	7	47	369
9191	TR1010W	10+85 SB	80	2.1	10	24	51	251
9191	TR1010W	10+85 SC	180	0.8	5	27	110	610
9191	TR1010W	10+95 SA	30	1.1	10	12	80	394
9191	TR1010W	10+95 SB	100	0.4	10	23	58	300
9191	TR1010W	11+05 SA	25	0.7	5	9	50	392
9191	TR1010W	11+05 SB	125	0.5	2.5	38	88	340
9191	TR1010W	11+05 SC	245	1.2	10	38	85	370
9191	TR1010W	11+15 SA	25	0.5	5	10	47	366
9191	TR1010W	11+15 SA*	25	0.4	2.5	9	42	343
9191	TR1010W	11+15 SB	125	0.2	2.5	23	61	210
9191	TR1010W	11+15 SC	165	1.1	30	26	47	187
9191	TR1010W	11+25 SA	25	0.3	2.5	9	32	285
9191	TR1010W	11+25 SB	60	1.7	40	53	91	360
9191	TR1010W	11+35 SA	20	0.3	5	8	32	312
9191	TR1010W	11+35 SB	70	0.8	10	21	71	364
9191	TR1010W	11+45 SA	20	0.2	10	6	29	330
9191	TR1010W	11+45 SB	120	1.3	2.5	34	81	285
9191	TR1010W	11+55 SA	30	1.5	10	12	51	520
9191	TR1010W	11+55 SA*	30	1.5	10	13	52	550
9191	TR1010W	11+65 SA	30	1.0	15	11	48	353
9191	TR1010W	11+65 SB	80	1.7	10	23	73	404
9148	TR785E	6+55 NA	20	<0.2	<5	17	5	54
9148	TR785E	6+55 NB	100	<0.2	<5	76	5	43
9148	TR785E	6+55 NC	180	<0.2	<5	30	12	76
9148	TR785E	6+55 ND	350	<0.2	<5	6	21	120
9148	TR785E	6+65 NA	20	<0.2	30	22	5	68
9148	TR785E	6+65 NB	120	<0.2	<5	17	4	22
9148	TR785E	6+65 NC	180	<0.2	<5	34	6	58
9148	TR785E	6+65 ND	290	<0.2	<5	7	8	35
9148	TR785E	6+75 NA	20	<0.2	<5	12	5	52

LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9148	TR785E	6+75 NB	120	<0.2	15	15	5	19
9148	TR785E	6+75 NC	180	<0.2	15	22	8	30
9148	TR785E	6+75 ND	290	0.7	10	9	125	86
9148	TR785E	6+85 NA	30	0.2	<5	19	9	75
9148	TR785E	6+85 NB	100	<0.2	15	28	7	35
9148	TR785E	6+85 NC	200	<0.2	<5	12	7	43
9148	TR785E	6+85 NC*	200	<0.2	<5	12	7	40
9148	TR785E	6+85 ND	230	<0.2	<5	3	8	41
9148	TR785E	6+95 NA	25	<0.2	<5	16	7	78
9148	TR785E	6+95 NB	50	<0.2	<5	21	7	33
9148	TR785E	6+95 NC	130	<0.2	<5	22	13	66
9148	TR785E	6+95 NC*	130	<0.2	<5	21	12	65
9148	TR785E	7+05 NA	20	0.2	<5	14	7	87
9148	TR785E	7+05 NB	95	<0.2	<5	29	15	61
9148	TR785E	7+05 NC	180	<0.2	<5	23	14	81
9148	TR785E	7+05 ND	225	<0.2	10	13	24	97
9148	TR842E	6+62 NA	15	<0.2	<5	34	5	40
9148	TR842E	6+62 NB	150	<0.2	<5	18	7	22
9148	TR842E	6+62 NC	500	<0.2	<5	25	18	62
9148	TR842E	6+62 ND	750	<0.2	<5	92	20	87
9148	TR842E	6+70 NA	20	<0.2	<5	34	6	38
9148	TR842E	6+70 NA*	20	<0.2	<5	32	6	35
9148	TR842E	6+70 NB	130	<0.2	<5	14	5	20
9148	TR842E	6+70 NC	260	<0.2	<5	35	15	60
9148	TR842E	6+70 ND	500	<0.2	<5	12	12	40
9148	TR842E	6+80 NA	15	<0.2	15	19	6	30
9148	TR842E	6+80 NB	100	<0.2	<5	26	6	28
9148	TR842E	6+80 NC	250	<0.2	<5	11	8	28
9148	TR842E	6+90 NA	15	<0.2	<5	22	6	83
9148	TR842E	6+90 NB	200	<0.2	<5	17	6	23
9148	TR842E	6+90 NC	270	0.4	<5	11	95	118
9148	TR842E	6+90 NC*	270	0.4	<5	10	93	120
9148	TR842E	7+00 NA	10	<0.2	<5	15	6	80
9148	TR842E	7+00 NB	100	<0.2	<5	14	4	24
9148	TR842E	7+00 NC	150	<0.2	<5	13	8	44
9156	TR825E	5+80 NA	10	<0.2	15	12	3	30
9156	TR825E	5+80 NB	110	<0.2	10	11	4	22
9156	TR825E	5+80 NC	300	<0.2	15	21	20	55
9156	TR825E	5+70 NA	15	<0.2	<5	17	5	40
9156	TR825E	5+70 NB	50	<0.2	10	34	6	42
9156	TR825E	5+70 NC	100	<0.2	10	10	10	27
9156	TR825E	5+70 NC*	100	<0.2	10	9	11	27
9156	TR825E	5+60 NA	8	0.2	10	28	2	47
9156	TR825E	5+60 NB	48	<0.2	15	27	20	37
9156	TR825E	5+60 NC	110	<0.2	10	21	6	57
9156	TR825E	5+50 NA	20	<0.2	<5	18	4	40



LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9156	TR825E	5+50 NB	100	<0.2	15	14	6	34
9156	TR825E	5+50 NC	200	<0.2	20	34	30	118
9156	TR825E	5+50 ND	300	<0.2	10	13	63	161
9156	TR858E	7+77 NA	20	<0.2	<5	18	5	60
9156	TR858E	7+77 NB	100	<0.2	5	28	4	27
9156	TR858E	7+77 NB*	100	<0.2	10	28	4	26
9156	TR858E	7+77 NC	200	<0.2	<5	21	8	29
9156	TR858E	7+77 ND	250	<0.2	<5	14	10	33
9156	TR858E	7+89 NA	10	<0.2	<5	19	4	45
9156	TR858E	7+89 NB	50	<0.2	10	53	2	36
9156	TR858E	7+89 NC	150	<0.2	<5	31	4	30
9156	TR858E	7+89 ND	250	<0.2	10	18	23	60
9156	TR858E	7+97 NA	10	<0.2	15	21	4	36
9156	TR858E	7+97 NB	100	<0.2	30	63	3	32
9156	TR858E	7+97 NC	200	<0.2	15	16	5	22
9156	TR858E	7+97 ND	300	<0.2	<5	13	9	28
9156	TR858E	8+07 NA	10	<0.2	<5	16	5	42
9156	TR858E	8+07 NB	100	<0.2	<5	71	6	35
9156	TR858E	8+07 NC	200	<0.2	<5	15	5	25
9156	TR858E	8+07 ND	300	<0.2	<5	6	6	50
9384	TR1388E	6+30 NA	30	0.1	2.5	15	8	94
9384	TR1388E	6+30 NB	80	0.1	5	25	39	83
9384	TR1388E	6+40 NA	20	0.1	2.5	9	4	75
9384	TR1388E	6+40 NB	80	0.1	5	19	3	42
9384	TR1388E	6+50 NA	30	0.1	2.5	12	4	71
9384	TR1388E	6+50 NB	100	0.1	2.5	17	4	43
9384	TR1388E	6+60 NA	30	0.1	2.5	12	3	77
9384	TR1388E	6+60 NB	80	0.1	2.5	22	7	52
9384	TR1388E	6+70 NA	30	0.1	2.5	20	6	65
9384	TR1388E	6+70 NA*	30	0.1	10	20	6	66
9384	TR1388E	6+70 NB	80	0.1	2.5	32	3	57
9384	TR1388E	6+80 NA	30	0.1	2.5	20	2	72
9384	TR1388E	6+80 NB	80	0.1	2.5	26	5	49
9384	TR1388E	6+90 NA	30	0.1	2.5	21	3	65
9384	TR1388E	6+90 NB	100	0.1	15	22	6	44
9384	TR1388E	7+00 NA	30	0.1	2.5	12	2	76
9384	TR1388E	7+00 NB	100	0.1	2.5	18	4	52
9384	TR1388E	7+10 NA	30	0.1	2.5	17	3	63
9384	TR1388E	7+10 NA*	30	0.1	2.5	18	2	66
9384	TR1388E	7+10 NB	100	0.1	2.5	22	5	38
9384	TR1388E	7+10 NC	180	0.1	5	19	8	47
9384	TR1388E	7+20 NA	30	0.2	10	17	2	64
9384	TR1388E	7+20 NB	100	0.1	10	19	5	38
9384	TR1388E	7+20 NC	200	0.1	2.5	23	13	49
9384	TR1388E	7+30 NA	30	0.3	2.5	18	2	69
9384	TR1388E	7+30 NB	100	0.1	2.5	18	7	46

LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9384	TR1388E	7+30 NC	200	0.1	2.5	14	14	156
9384	TR1388E	7+40 NA	30	0.3	2.5	17	2	68
9384	TR1388E	7+40 NB	100	0.1	2.5	14	6	27
9384	TR1388E	7+40 NC	200	0.1	2.5	11	16	174
9384	TR1388E	7+50 NA	30	0.1	2.5	27	4	53
9384	TR1388E	7+50 NB	100	0.1	2.5	42	5	62
9384	TR1388E	7+50 NC	170	0.1	30	18	31	143
9384	TR1388E	7+50 NC*	170	0.1	50	17	32	143
9335	TR1565W	7+35 SA	30	0.3	2.5	10	58	252
9335	TR1565W	7+35 SA*	30	0.3	2.5	9	58	247
9335	TR1565W	7+45 SA	3	0.4	10	9	37	267
9335	TR1565W	7+45 SB	10	0.3	2.5	16	49	190
9335	TR1565W	7+55 SA	5	0.4	25	9	50	342
9335	TR1565W	7+55 SB	20	0.3	2.5	14	31	188
9335	TR1565W	7+65 SA	30	0.5	400	13	85	380
9335	TR1565W	7+65 SB	60	0.6	2.5	15	234	430
9335	TR1565W	7+75 SA	30	0.5	15	8	55	420
9335	TR1565W	7+75 SB	110	0.2	30	10	61	205
9335	TR1565W	7+85 SA	30	1.3	2.5	12	29	520
9335	TR1565W	7+85 SB	80	1.1	5	21	47	217
9335	TR1565W	7+85 SC	150	1.2	20	29	148	333
9335	TR1565W	7+95 SA	30	0.6	2.5	10	36	367
9335	TR1565W	7+95 SB	80	0.4	15	7	36	202
9335	TR1565W	7+95 SC	160	1.1	25	20	140	190
9335	TR1565W	8+05 SA	30	0.7	15	9	23	410
9335	TR1565W	8+05 SB	120	0.7	2.5	8	27	290
9335	TR1565W	8+05 SC	250	0.4	10	22	118	400
9335	TR1565W	8+15 SA	30	0.7	155	11	27	340
9335	TR1565W	8+15 SA*	30	0.7	10	10	25	332
9335	TR1565W	8+15 SB	120	1.0	110	11	56	170
9335	TR1565W	8+25 SA	30	1.1	2.5	11	33	360
9335	TR1565W	8+35 SA	30	0.5	2.5	9	31	191
9335	TR1565W	8+45 SA	30	0.5	2.5	12	65	400
9335	TR1565W	8+55 SA	40	0.2	2.5	11	31	197
9335	TR1565W	8+65 SA	40	0.3	10	11	18	155
9335	TR1565W	8+65 SB	150	0.3	15	14	34	160
9335	TR1565W	8+75 SA	30	0.5	2.5	11	40	400
9335	TR1565W	8+75 SB	100	0.3	20	8	38	164
9335	TR1565W	8+75 SB*	100	0.3	2.5	9	40	170
9335	TR1565W	8+75 SC	190	0.1	2.5	16	142	345
9335	TR1565W	8+85 SA	30	0.4	35	11	35	387
9335	TR1565W	8+85 SB	130	0.8	30	20	144	270
9335	TR1565W	8+95 SA	30	1.2	10	25	41	530
9335	TR1565W	8+95 SB	100	0.2	2.5	17	37	400
9335	TR1565W	9+05 SA	40	0.2	2.5	9	26	142
9335	TR1565W	9+05 SB	80	0.1	2.5	9	170	150

LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9335	TR1565W	9+05 SC	170	0.6	2.5	16	44	205
9335	TR1565W	9+15 SA	40	0.7	2.5	10	67	91
9335	TR1565W	9+25 SA	30	1.4	2.5	14	46	160
9335	TR1565W	9+25 SB	70	0.3	2.5	13	81	175
9335	TR1565W	9+25 SC	150	0.3	2.5	12	30	235
9335	TR1565W	9+35 SA	30	0.2	2.5	10	21	178
9335	TR1565W	9+35 SB	100	0.2	2.5	9	80	147
9335	TR1565W	9+35 SC	250	0.5	2.5	15	71	196
9335	TR1565W	9+45 SA	40	0.3	2.5	12	31	127
9335	TR1565W	9+45 SB	110	0.1	2.5	25	70	179
9335	TR1565W	9+55 SA	25	0.3	2.5	12	36	247
9335	TR1565W	9+55 SA*	25	0.3	2.5	12	40	270
9335	TR1565W	9+65 SA	40	0.3	2.5	12	32	130
9335	TR1565W	9+75 SA	30	0.1	2.5	22	25	112
9335	TR1565W	9+75 SB	140	0.5	2.5	30	52	138
9335	TR1565W	9+85 SA	30	0.3	2.5	13	28	300
9335	TR1565W	9+85 SB	140	0.4	5	15	116	225
9335	TR1565W	9+95 SA	30	0.2	2.5	10	16	153
9335	TR1565W	9+95 SB	120	0.2	5	12	52	142
9335	TR1565W	9+95 SC	250	0.3	2.5	20	130	234
9335	TR1565W	10+05 SA	30	0.6	2.5	12	23	291
9335	TR1565W	10+05 SA*	30	0.7	10	11	23	297
9335	TR1565W	10+05 SB	120	0.3	2.5	17	51	168
9335	TR1565W	10+05 SC	270	0.3	2.5	12	58	142
9335	TR1565W	10+15 SA	30	0.3	15	9	19	183
9335	TR1565W	10+15 SB	100	0.1	10	8	47	125
9335	TR1565W	10+15 SC	250	0.1	30	9	51	133
9335	TR1565W	10+15 SC*	250	0.1	35	9	50	130
ET443	TR3228E	6+02 NA	10	<.1	5	16	15	163
ET443	TR3228E	6+02 NB	90	<.1	<5	36	15	94
ET443	TR3228E	6+02 NC	180	<.1	<5	34	22	103
ET443	TR3228E	6+09 NA	15	<.1	50	14	16	160
ET443	TR3228E	6+09 NB	120	<.1	5	34	16	114
ET443	TR3228E	6+09 NC	220	<.1	15	36	26	113
ET443	TR3228E	6+19 NA	150	<.1	<5	16	14	133
ET443	TR3228E	6+19 NB	115	<.1	<5	32	17	91
ET443	TR3228E	6+19 NC	240	<.1	15	33	25	117
ET443	TR3427E	6+25 NA	30	.1	10	23	15	162
ET443	TR3427E	6+25 NB	125	<.1	<5	138	30	113
ET443	TR3427E	6+35 NA	30	<.1	<5	23	15	120
ET443	TR3427E	6+35 NB	100	<.1	5	64	14	73
ET443	TR3427E	6+50 NA	30	<.1	5	28	15	136
ET443	TR3427E	6+50 NB	90	<.1	<5	63	31	144
ET443	TR3427E	6+60 NA	30	<.1	<5	31	13	134
ET443	TR3427E	6+70 NA	20	<.1	<5	24	9	190
ET443	TR3427E	6+80 NA	30	<.1	<5	46	15	134

LAB PROJ.	TRENCH	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
ET443	TR3427E	6+80 NB	100	.2	10	55	35	140
ET443	TR3427E	6+80 NC	200	<.1	<5	83	100	341
ET443	TR3427E	6+90 NA	30	<.1	<5	31	16	172
ET443	TR3427E	6+90 NB	100	.1	5	91	33	150

TEST PITS  
SOIL SAMPLE PROFILES

LAB PROJ.	TEST PIT	FIELD GRID STATION	SAMPLE DEPTH (cm)	Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
9285	125W	0+25 N	25	0.1	2.5	8	18	171
9285	125W	0+25 N*	25	0.1	2.5	8	18	176
9384	200W	32+00 NA	45	0.1	2.5	19	5	60
9384	200W	32+00 NB	150	0.1	2.5	24	9	54
9384	200W	32+00 NC	400	0.1	2.5	61	21	164
9384	200W	32+00 ND	600	0.1	2.5	58	22	162
9384	200W	32+50 NA	20	0.1	2.5	13	6	50
9384	200W	32+50 NB	100	0.1	2.5	13	4	27
9384	200W	32+50 NC	200	0.2	2.5	55	15	122
9384	200W	32+50 ND	400	0.1	2.5	63	20	143
9384	200W	33+25 NA	25	0.1	2.5	14	6	50
9384	200W	33+25 NA*	25	0.1	2.5	13	4	48
9384	200W	33+25 NB	100	0.1	2.5	19	8	53
9384	200W	33+25 NC	200	0.2	2.5	96	26	213
9384	200W	33+25 ND	400	0.3	2.5	125	43	310
9335	1600E	2+65 SA	30	0.2	2.5	13	7	58
9335	1600E	2+65 SB	200	0.1	2.5	13	7	22
9335	1600E	2+90 SA	30	0.2	20	11	12	66
9335	1600E	2+90 SB	100	0.1	2.5	15	11	40
9335	1600E	2+90 SC	300	0.1	2.5	15	8	41
9335	1600E	3+35 SA	30	0.2	2.5	24	5	58
9335	1600E	3+35 SB	100	0.1	2.5	16	9	40
9335	1600E	3+35 SC	300	0.1	2.5	16	10	45

NOTE: \*are duplicate analysis

**APPENDIX VI**

**Listing of Soil Sample Data**

SPRING PROJECT SOIL SAMPLE DATA

1989 PROGRAM

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9135	5 W	1000 N	5811.87	8630.13	0.10	15.0	7	40	95
9135	7 W	600 N	5895.44	8251.25	0.20	10.0	8	18	92
9135	25 W	400 N	5964.28	8062.37	0.20	50.0	9	20	90
9135	25 W	600 N	5885.81	8247.29	0.30	15.0	6	11	223
9135	25 W	1200 N	5788.96	8823.05	0.10	3.0	17	12	46
9135	25 W	1400 N	5726.46	9015.98	0.10	3.0	10	11	109
9135	25 W	1800 N	5575.73	9412.21	0.10	15.0	12	8	61
9135	25 W	2000 N	5494.18	9609.79	0.10	3.0	17	12	132
9135	30 W	1000 N	5789.48	8621.08	0.10	3.0	5	6	105
9135	50 W	400 N	5939.00	8053.18	0.30	10.0	6	18	212
9135	50 W	600 N	5860.13	8238.14	0.40	30.0	9	15	223
9108	50 W	350 S	6243.52	7334.11	0.00	0.4	11	14	325
9108	50 W	425 S	6268.76	7263.77	0.00	0.5	23	136	620
9108	50 W	450 S	6277.18	7240.32	0.00	0.3	10	28	112
9108	50 W	575 S	6319.25	7123.08	0.00	0.2	10	31	207
9108	50 W	600 S	6327.66	7099.63	0.00	0.5	14	88	500
9108	50 W	625 S	6336.07	7076.19	0.00	0.2	28	20	128
9108	50 W	650 S	6344.49	7052.74	0.00	0.2	20	16	74
9108	50 W	675 S	6352.90	7029.29	0.00	0.2	19	20	91
9108	50 W	700 S	6361.32	7005.85	0.00	0.2	11	11	74
9108	50 W	725 S	6369.73	6982.40	0.00	0.1	12	15	74
9108	50 W	750 S	6378.14	6958.95	0.00	0.4	33	25	246
9108	50 W	775 S	6386.56	6935.50	0.00	0.5	17	34	620
9108	50 W	800 S	6394.97	6912.06	0.00	0.3	12	20	250
9108	50 W	825 S	6403.39	6888.61	0.00	0.6	15	22	278
9108	50 W	850 S	6411.80	6865.16	0.00	0.1	7	8	40
9135	50 W	1200 N	5765.69	8813.84	0.10	3.0	37	15	85
9135	50 W	1400 N	5703.08	9007.07	0.10	3.0	9	12	73
9135	50 W	1600 N	5638.01	9203.83	0.10	3.0	10	10	42
9135	50 W	1800 N	5551.58	9406.46	0.10	3.0	13	9	67
9135	50 W	2000 N	5470.05	9603.21	0.10	3.0	13	17	130
9135	75 W	600 N	5834.45	8228.99	0.60	3.0	18	42	670
9135	75 W	1200 N	5742.41	8804.64	0.10	3.0	16	9	50
9135	75 W	1400 N	5679.71	8998.17	0.20	3.0	9	7	92
9135	75 W	1600 N	5614.49	9195.37	0.10	10.0	14	13	52
9135	75 W	1800 N	5527.43	9400.71	0.10	10.0	53	9	63
9135	75 W	2000 N	5445.92	9596.64	0.20	30.0	15	23	98
9135	85 W	200 N	5980.94	7851.92	0.10	10.0	9	20	127
9135	100 W	200 N	5969.18	7847.88	0.10	15.0	8	8	121
9135	100 W	400 N	5888.45	8034.80	0.30	3.0	9	21	470
9135	100 W	600 N	5808.78	8219.83	0.30	3.0	7	36	371
9135	100 W	800 N	5721.48	8402.40	0.10	3.0	9	27	229
9108	100 W	450 S	6232.91	7224.54	0.00	0.3	18	18	177

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	100 W	500 S	6249.59	7177.55	0.00	0.2	11	14	127
9108	100 W	525 S	6257.93	7154.06	0.00	0.6	23	20	166
9108	100 W	550 S	6266.27	7130.56	0.00	0.1	14	15	135
9108	100 W	575 S	6274.61	7107.07	0.02	0.0	45	42	640
9108	100 W	600 S	6282.95	7083.58	0.00	0.4	12	17	238
9108	100 W	625 S	6291.29	7060.08	0.00	0.5	11	11	106
9108	100 W	650 S	6299.63	7036.59	0.00	0.3	13	12	170
9108	100 W	675 S	6307.97	7013.10	0.00	0.3	14	12	181
9108	100 W	700 S	6316.31	6989.60	0.00	0.2	10	10	75
9108	100 W	725 S	6324.65	6966.11	0.00	0.3	19	18	142
9108	100 W	750 S	6332.98	6942.61	0.00	0.2	9	10	40
9108	100 W	775 S	6341.32	6919.12	0.00	0.1	9	10	50
9108	100 W	800 S	6349.66	6895.63	0.00	0.3	16	20	92
9108	100 W	825 S	6358.00	6872.13	0.00	0.5	12	17	300
9108	100 W	850 S	6366.34	6848.64	0.00	0.5	22	23	108
9108	100 W	875 S	6374.68	6825.15	0.00	0.3	11	16	306
9108	100 W	900 S	6383.02	6801.65	0.00	0.3	12	14	174
9108	100 W	925 S	6391.36	6778.16	0.00	0.3	11	12	136
9108	100 W	950 S	6399.70	6754.66	0.00	0.3	11	13	134
9108	100 W	975 S	6408.04	6731.17	0.00	0.4	11	13	110
9135	100 W	1200 N	5719.13	8795.43	0.10	3.0	23	10	53
9135	100 W	1400 N	5656.33	8989.26	0.10	3.0	9	9	91
9135	100 W	1600 N	5590.96	9186.92	0.10	3.0	9	8	29
9135	100 W	1800 N	5503.29	9394.96	0.10	15.0	10	7	55
9135	100 W	2000 N	5421.79	9590.06	0.10	3.0	11	15	190
9108	100 W	2125 N	5342.22	9679.16	0.10	3.0	15	10	167
9108	100 W	2150 N	5333.07	9702.90	0.10	3.0	8	11	382
9108	100 W	2175 N	5323.91	9726.65	0.40	3.0	11	8	88
9108	100 W	2200 N	5314.76	9750.39	0.10	3.0	13	10	110
9108	100 W	2225 N	5305.60	9774.14	0.10	3.0	11	8	65
9108	100 W	2250 N	5296.45	9797.88	0.10	3.0	12	7	69
9108	100 W	2275 N	5287.30	9821.62	0.10	3.0	12	7	80
9108	100 W	2300 N	5278.14	9845.37	0.10	3.0	16	7	85
9108	100 W	2325 N	5268.99	9869.11	0.10	3.0	19	4	51
9108	100 W	2350 N	5259.84	9892.85	0.10	3.0	17	4	36
9108	100 W	2375 N	5250.68	9916.60	0.10	3.0	23	4	33
9108	100 W	2400 N	5241.53	9940.34	0.10	3.0	18	3	34
9108	100 W	2425 N	5232.37	9964.09	0.10	3.0	28	4	40
9108	100 W	2450 N	5223.22	9987.83	0.10	10.0	29	5	43
9108	100 W	2475 N	5214.07	10011.57	0.10	3.0	29	5	40
9108	100 W	2500 N	5204.91	10035.32	0.10	3.0	28	4	40
9108	100 W	2525 N	5195.76	10059.06	0.10	3.0	28	4	50
9108	100 W	2550 N	5186.61	10082.80	0.10	10.0	26	4	40
9108	100 W	2575 N	5177.45	10106.55	0.10	25.0	29	5	47
9108	100 W	2600 N	5168.30	10130.29	0.10	3.0	28	5	35
9108	100 W	2625 N	5159.14	10154.04	0.10	3.0	24	4	32
9108	100 W	2650 N	5149.99	10177.78	0.10	3.0	22	4	38
9108	100 W	2925 N	5013.88	10363.91	0.10	3.0	20	6	34

Continued....



Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	100 W	2950 N	5004.52	10387.01	0.10	3.0	18	4	38
9108	100 W	2975 N	4995.15	10410.10	0.10	3.0	22	5	37
9108	100 W	3000 N	4985.79	10433.20	0.10	3.0	23	5	37
9108	100 W	3025 N	4976.43	10456.30	0.10	3.0	21	6	42
9108	100 W	3050 N	4967.06	10479.39	0.10	3.0	35	6	50
9108	100 W	3075 N	4957.70	10502.49	0.20	3.0	32	6	55
9108	100 W	3100 N	4948.34	10525.59	0.10	3.0	21	5	40
9108	100 W	3125 N	4938.98	10548.68	0.10	3.0	19	5	45
9108	100 W	3150 N	4929.61	10571.78	0.10	3.0	18	6	42
9108	100 W	3175 N	4920.25	10594.88	0.10	3.0	19	6	44
9108	100 W	3200 N	4910.89	10617.97	0.10	3.0	16	5	50
9108	100 W	3225 N	4901.52	10641.07	0.10	3.0	15	5	50
9108	100 W	3250 N	4892.16	10664.16	0.10	3.0	24	6	50
9108	100 W	3275 N	4882.80	10687.26	0.10	3.0	14	5	53
9108	100 W	3300 N	4873.44	10710.36	0.10	3.0	15	6	65
9108	100 W	3325 N	4864.07	10733.45	0.10	3.0	12	5	48
9108	100 W	3350 N	4854.71	10756.55	0.30	10.0	35	8	68
9108	100 W	3375 N	4845.35	10779.65	0.20	10.0	40	8	69
9108	100 W	3400 N	4835.98	10802.74	0.10	10.0	21	7	51
9108	100 W	3425 N	4826.62	10825.84	0.10	3.0	18	5	65
9135	125 W	200 N	5944.23	7838.51	0.20	15.0	7	17	470
9135	125 W	400 N	5863.17	8025.60	0.30	3.0	10	32	320
9135	125 W	600 N	5783.10	8210.67	0.30	3.0	7	37	294
9135	125 W	800 N	5697.31	8393.90	0.20	3.0	8	35	347
9135	125 W	1400 N	5632.96	8980.35	0.10	3.0	7	13	43
9135	125 W	1600 N	5567.44	9178.46	0.10	3.0	8	8	43
9135	125 W	1800 N	5479.14	9389.21	0.10	10.0	11	9	68
9135	125 W	2000 N	5397.66	9583.49	0.20	10.0	11	14	180
9135	150 W	200 N	5919.29	7829.15	0.20	115.0	11	45	233
9135	150 W	400 N	5837.89	8016.41	0.30	10.0	8	13	345
9135	150 W	600 N	5757.42	8201.52	0.20	15.0	6	29	257
9135	150 W	800 N	5673.14	8385.39	1.50	3.0	15	140	1120
9135	150 W	1000 N	5593.71	8575.17	0.10	3.0	16	8	73
9135	150 W	1400 N	5609.59	8971.45	0.10	3.0	8	8	40
9135	150 W	1600 N	5543.92	9170.00	0.10	10.0	50	11	50
9135	150 W	1800 N	5454.99	9383.46	0.10	3.0	7	9	51
9135	150 W	2000 N	5373.53	9576.91	0.10	3.0	9	7	158
9108	150 W	2125 N	5297.91	9662.79	0.10	10.0	17	6	72
9108	150 W	2150 N	5288.70	9686.41	0.10	10.0	15	6	60
9108	150 W	2175 N	5279.48	9710.04	0.10	3.0	20	7	76
9108	150 W	2200 N	5270.27	9733.66	0.10	3.0	13	6	58
9108	150 W	2225 N	5261.05	9757.28	0.20	15.0	14	6	64
9108	150 W	2250 N	5251.84	9780.91	0.10	10.0	11	5	52
9108	150 W	2275 N	5242.63	9804.53	0.20	10.0	14	5	58
9108	150 W	2300 N	5233.41	9828.15	0.10	10.0	12	6	58
9108	150 W	2325 N	5224.20	9851.78	0.20	3.0	21	5	72
9108	150 W	2350 N	5214.99	9875.40	0.10	3.0	18	4	68
9108	150 W	2375 N	5205.77	9899.02	0.10	3.0	18	5	62

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	150 W	2400 N	5196.56	9922.65	0.10	3.0	12	3	40
9108	150 W	2425 N	5187.34	9946.27	0.20	10.0	24	6	85
9108	150 W	2450 N	5178.13	9969.89	0.20	10.0	21	5	48
9108	150 W	2475 N	5168.92	9993.52	0.10	3.0	15	5	32
9108	150 W	2500 N	5159.70	10017.14	0.10	10.0	22	4	40
9108	150 W	2525 N	5150.49	10040.76	0.10	25.0	28	4	55
9108	150 W	2550 N	5141.28	10064.39	0.20	15.0	23	4	59
9108	150 W	2575 N	5132.06	10088.01	0.10	20.0	21	3	44
9108	150 W	2600 N	5122.85	10111.63	0.10	10.0	18	5	40
9108	150 W	2625 N	5113.63	10135.26	0.10	3.0	18	4	40
9108	150 W	2650 N	5104.42	10158.88	0.10	3.0	23	4	44
9135	175 W	200 N	5894.34	7819.79	0.20	10.0	6	30	550
9135	175 W	300 N	5853.44	7913.02	0.50	3.0	22	54	900
9135	175 W	400 N	5812.62	8007.22	0.50	15.0	7	22	322
9135	175 W	600 N	5731.75	8192.37	0.20	3.0	6	24	287
9135	175 W	800 N	5648.97	8376.89	0.40	10.0	9	78	480
9135	175 W	1000 N	5568.83	8565.78	0.10	15.0	10	9	58
9135	175 W	1400 N	5586.21	8962.54	0.10	3.0	13	7	38
9135	175 W	1600 N	5520.40	9161.55	0.20	25.0	8	10	71
9135	175 W	1800 N	5430.84	9377.71	0.10	3.0	13	9	57
9135	175 W	2000 N	5349.40	9570.33	0.10	3.0	10	7	91
9135	200 W	1400 N	5562.84	8953.63	0.10	3.0	7	7	84
9135	200 W	1600 N	5496.88	9153.09	0.10	3.0	8	8	71
9135	200 W	1800 N	5406.69	9371.96	0.10	10.0	11	5	50
9135	200 W	2000 N	5325.27	9563.76	0.20	3.0	16	7	122
9135	225 W	1800 N	5382.54	9366.22	0.10	3.0	17	6	62
9135	225 W	2000 N	5301.14	9557.19	0.10	3.0	13	7	180
9135	250 W	1800 N	5358.39	9360.47	0.10	10.0	12	6	50
9135	250 W	2000 N	5277.01	9550.61	0.10	3.0	15	7	109
9135	275 W	1800 N	5334.24	9354.72	0.10	3.0	10	5	44
9135	275 W	2000 N	5252.88	9544.04	0.10	3.0	11	6	44
9108	300 W	700 S	6180.03	6916.83	0.90	3.0	25	41	540
9108	300 W	725 S	6189.33	6893.54	0.80	3.0	35	34	1000
9108	300 W	750 S	6198.63	6870.26	1.50	3.0	20	25	650
9108	300 W	800 S	6217.23	6823.69	1.30	3.0	27	45	1400
9108	300 W	825 S	6226.53	6800.40	0.40	3.0	18	30	335
9108	300 W	850 S	6235.83	6777.11	0.30	3.0	15	17	244
9108	300 W	875 S	6245.13	6753.83	0.30	3.0	13	10	81
9108	300 W	900 S	6254.43	6730.54	0.30	3.0	11	11	84
9108	300 W	925 S	6263.73	6707.25	0.10	3.0	27	15	1080
9108	300 W	950 S	6273.02	6683.97	0.30	3.0	27	24	123
9108	300 W	975 S	6282.32	6660.68	0.10	3.0	9	14	63
9108	300 W	995 S	6289.76	6642.05	0.10	3.0	10	14	63
9135	300 W	1200 N	5464.70	8743.54	0.10	3.0	7	11	78
9135	300 W	1400 N	5384.98	8923.91	0.10	3.0	35	14	75
9135	300 W	1800 N	5310.09	9348.97	0.10	10.0	9	5	46
9135	300 W	2000 N	5228.75	9537.46	0.10	3.0	15	7	65
9108	300 W	2925 N	4831.60	10293.37	0.10	3.0	30	6	72

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	300 W	2950 N	4822.30	10316.66	0.20	3.0	22	4	47
9108	300 W	2975 N	4813.00	10339.94	0.10	3.0	24	5	55
9108	300 W	3000 N	4803.70	10363.23	0.10	3.0	23	6	72
9108	300 W	3025 N	4794.40	10386.52	0.20	3.0	25	5	50
9108	300 W	3050 N	4785.10	10409.80	0.10	3.0	30	4	46
9108	300 W	3075 N	4775.80	10433.09	0.10	3.0	25	5	50
9108	300 W	3100 N	4766.50	10456.38	0.10	3.0	24	6	47
9108	300 W	3125 N	4757.20	10479.66	0.10	3.0	21	6	52
9108	300 W	3150 N	4747.90	10502.95	0.10	3.0	23	6	41
9108	300 W	3180 N	4736.75	10530.89	0.10	3.0	18	6	51
9108	300 W	3200 N	4729.31	10549.52	0.10	3.0	20	6	62
9108	300 W	3225 N	4720.01	10572.81	0.10	3.0	18	6	50
9108	300 W	3250 N	4710.71	10596.09	0.10	3.0	19	3	43
9108	300 W	3275 N	4701.41	10619.38	0.10	3.0	14	6	44
9108	300 W	3300 N	4692.11	10642.67	0.30	3.0	20	5	55
9108	300 W	3325 N	4682.81	10665.95	0.10	3.0	20	8	58
9108	300 W	3350 N	4673.51	10689.24	0.10	3.0	21	6	60
9108	300 W	3375 N	4664.21	10712.53	0.10	3.0	14	6	35
9108	300 W	3400 N	4654.91	10735.81	0.10	3.0	22	5	41
9108	300 W	3425 N	4645.61	10759.10	0.10	3.0	36	10	60
9135	325 W	1200 N	5439.08	8729.25	0.10	3.0	9	14	250
9135	325 W	1400 N	5360.48	8912.31	0.10	3.0	8	9	58
9135	325 W	1800 N	5285.95	9343.22	0.10	10.0	11	5	49
9135	325 W	2000 N	5204.62	9530.88	0.10	3.0	13	6	58
9135	340 W	1200 N	5423.71	8720.68	0.10	3.0	12	12	235
9135	350 W	1400 N	5335.99	8900.71	0.10	3.0	10	11	96
9135	350 W	1800 N	5261.80	9337.47	0.10	3.0	10	8	60
9135	350 W	2000 N	5180.49	9524.31	0.10	3.0	15	7	62
9108	350 W	2900 N	4797.35	10254.22	0.10	3.0	29	5	60
9108	350 W	2925 N	4787.84	10277.72	0.10	3.0	21	5	50
9108	350 W	2950 N	4778.32	10301.23	0.10	3.0	25	5	54
9108	350 W	2975 N	4768.81	10324.73	0.10	3.0	24	5	47
9108	350 W	3000 N	4759.29	10348.23	0.10	3.0	30	5	63
9108	350 W	3025 N	4749.78	10371.73	0.10	3.0	32	5	61
9108	350 W	3050 N	4740.26	10395.24	0.10	3.0	30	5	64
9108	350 W	3075 N	4730.75	10418.74	0.10	3.0	28	6	72
9135	375 W	1200 N	5387.84	8700.67	0.30	3.0	4	41	600
9135	375 W	1400 N	5311.50	8889.11	0.10	3.0	10	12	127
9135	375 W	1800 N	5237.65	9331.72	0.10	10.0	9	9	60
9135	375 W	2000 N	5156.36	9517.74	0.10	3.0	15	8	74
9135	395 W	1400 N	5291.90	8879.83	0.10	3.0	8	14	395
9135	400 W	2000 N	5132.23	9511.16	0.10	3.0	13	7	76
9108	450 W	2850 N	4717.46	10164.55	0.10	3.0	14	6	58
9108	450 W	2900 N	4699.16	10211.59	0.10	3.0	20	5	64
9108	450 W	2925 N	4690.01	10235.12	0.10	3.0	15	6	80
9108	450 W	2950 N	4680.86	10258.64	0.10	3.0	18	5	74
9108	450 W	2975 N	4671.70	10282.16	0.10	3.0	26	5	63
9108	450 W	3000 N	4662.55	10305.68	0.30	3.0	23	6	66

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	450 W	3025 N	4653.40	10329.20	0.10	3.0	20	6	73
9108	450 W	3050 N	4644.25	10352.72	0.10	3.0	25	5	102
9108	450 W	3080 N	4633.27	10380.95	0.20	3.0	62	6	73
358- 11	500 W	675 N	5463.56	8154.94	0.20	5.0	9	23	120
358- 12	500 W	700 N	5453.82	8179.62	0.10	5.0	8	11	118
358- 13	500 W	725 N	5444.08	8204.29	0.40	5.0	11	17	137
358- 14	500 W	750 N	5434.35	8228.97	0.10	3.0	8	18	129
358- 15	500 W	775 N	5424.61	8253.65	0.30	5.0	9	17	140
9108	500 W	2200 N	4938.55	9503.60	0.10	3.0	13	9	75
9108	500 W	2225 N	4930.02	9525.53	0.10	3.0	12	9	74
9108	500 W	2250 N	4921.49	9547.46	0.10	3.0	12	7	87
9108	500 W	2275 N	4912.97	9569.39	0.10	3.0	15	10	86
9108	500 W	2300 N	4904.44	9591.32	0.10	3.0	12	11	80
9108	500 W	2325 N	4891.24	9622.96	0.10	3.0	13	12	70
9108	500 W	2350 N	4878.04	9654.60	0.10	3.0	13	24	91
9108	500 W	2375 N	4864.84	9686.24	0.10	3.0	14	11	93
9108	500 W	2400 N	4851.64	9717.88	0.10	3.0	15	10	92
9108	500 W	2725 N	4717.13	10034.28	0.10	3.0	15	10	63
9108	500 W	2750 N	4707.96	10057.44	0.10	3.0	13	6	28
9108	500 W	2775 N	4698.78	10080.60	0.10	3.0	11	4	26
9108	500 W	2800 N	4689.61	10103.76	0.30	3.0	14	9	109
9108	500 W	2825 N	4680.44	10126.92	0.10	3.0	16	7	86
9108	500 W	2850 N	4671.26	10150.08	0.10	3.0	12	8	148
9108	500 W	2930 N	4641.91	10224.18	0.10	3.0	16	4	53
9108	500 W	2950 N	4634.57	10242.71	0.10	3.0	13	5	55
9108	500 W	2975 N	4625.40	10265.87	0.10	3.0	18	3	51
358- 16	550 W	675 N	5417.98	8133.51	0.10	3.0	9	15	96
358- 17	550 W	700 N	5408.87	8157.87	0.10	3.0	12	11	97
358- 18	550 W	725 N	5399.76	8182.23	0.10	3.0	8	16	100
358- 19	550 W	750 N	5390.66	8206.59	0.10	3.0	7	8	82
358- 20	550 W	775 N	5381.55	8230.95	0.10	3.0	9	9	92
9108	550 W	2600 N	4715.50	9890.10	0.10	3.0	16	8	60
9108	550 W	2625 N	4706.33	9913.51	0.20	3.0	13	7	75
9108	550 W	2650 N	4697.15	9936.92	0.10	3.0	13	7	78
9108	550 W	2675 N	4687.98	9960.34	0.10	3.0	12	5	76
9108	550 W	2700 N	4678.81	9983.75	0.50	3.0	43	10	60
9108	550 W	2725 N	4669.63	10007.16	0.80	3.0	33	12	164
9108	550 W	2745 N	4662.30	10025.89	0.10	3.0	12	9	127
9108	550 W	2775 N	4651.29	10053.98	0.10	3.0	32	11	70
9108	550 W	2800 N	4642.12	10077.40	0.10	3.0	13	3	25
9108	550 W	2825 N	4632.94	10100.81	0.10	3.0	11	4	37
9108	550 W	2850 N	4623.77	10124.22	0.40	3.0	26	8	117
358- 21	650 W	675 N	5321.76	8091.92	0.10	3.0	6	11	143
358- 22	650 W	700 N	5312.65	8116.28	0.10	5.0	5	13	186
358- 23	650 W	725 N	5303.55	8140.65	0.10	3.0	5	14	119
358- 24	650 W	750 N	5294.44	8165.01	0.10	3.0	6	12	117
358- 25	650 W	775 N	5285.34	8189.37	0.20	3.0	8	10	134
358- 26	700 W	675 N	5274.92	8070.50	0.20	3.0	9	19	138

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm	
			East	North						
358-	27	700 W	700 N	5265.50	8094.23	0.20	3.0	5	14	144
358-	28	700 W	725 N	5256.07	8117.96	0.10	3.0	11	7	150
358-	29	700 W	750 N	5246.65	8141.68	0.10	3.0	6	14	134
358-	30	700 W	775 N	5237.22	8165.41	0.10	3.0	7	18	187
9108		700 W	2200 N	4715.84	9525.85	0.10	3.0	7	6	65
9108		700 W	2225 N	4706.42	9550.21	0.10	3.0	9	7	106
9108		700 W	2250 N	4697.00	9574.57	0.10	3.0	11	7	123
9108		700 W	2275 N	4687.57	9598.94	0.10	3.0	11	7	128
9108		700 W	2300 N	4678.15	9623.30	0.10	3.0	13	9	103
9108		700 W	2550 N	4583.85	9838.45	0.10	3.0	3	6	80
9108		700 W	2575 N	4576.31	9856.45	0.10	3.0	9	9	154
9108		700 W	2600 N	4568.77	9874.45	0.10	3.0	13	8	142
9108		700 W	2625 N	4561.22	9892.45	0.10	3.0	15	7	107
9108		700 W	2650 N	4553.68	9910.45	0.10	3.0	18	8	106
9108		700 W	2725 N	4531.05	9964.45	0.10	3.0	15	18	94
9108		700 W	2750 N	4523.51	9982.45	0.10	3.0	17	8	81
9108		700 W	2775 N	4515.97	10000.45	0.10	3.0	15	8	71
9108		900 W	2100 N	4568.73	9361.66	0.10	3.0	11	10	90
9108		900 W	2125 N	4560.56	9381.49	0.30	3.0	22	13	106
9108		900 W	2150 N	4552.39	9401.32	0.10	3.0	10	16	123
9108		900 W	2175 N	4544.22	9421.14	0.10	3.0	5	7	108
9108		900 W	2200 N	4536.05	9440.97	0.10	3.0	6	6	136
9108		900 W	2225 N	4527.88	9460.80	0.10	3.0	8	10	151
9099		900 W	1025 S	5803.04	6086.57	0.80	3.0	7	47	303
9099		900 W	1050 S	5794.54	6110.16	0.60	3.0	6	33	253
9099		900 W	1075 S	5786.03	6133.74	0.60	3.0	6	33	262
9099		900 W	1100 S	5777.53	6157.33	0.20	3.0	7	28	315
9099		900 W	1125 S	5769.02	6180.91	0.40	3.0	5	31	250
9099		900 W	1150 S	5760.52	6204.50	0.20	3.0	4	37	153
9099		900 W	1175 S	5752.01	6228.08	0.20	3.0	4	30	196
9099		900 W	1200 S	5743.50	6251.67	0.30	3.0	6	40	272
9099		900 W	1225 S	5735.00	6275.25	0.40	3.0	13	48	352
9099		1100 W	975 S	5565.56	6161.72	0.70	3.0	6	35	384
9099		1100 W	1000 S	5556.83	6185.17	0.40	3.0	4	47	346
9099		1100 W	1025 S	5548.10	6208.61	1.20	3.0	20	80	760
9099		1100 W	1060 S	5535.89	6241.44	0.60	3.0	5	32	316
9099		1100 W	1075 S	5530.65	6255.50	0.50	3.0	4	27	300
9099		1100 W	1100 S	5521.92	6278.95	0.10	3.0	7	36	280
9099		1100 W	1125 S	5513.20	6302.40	0.30	3.0	8	46	242
9099		1100 W	1150 S	5504.47	6325.84	0.20	3.0	10	25	200
9099		1100 W	1175 S	5495.75	6349.29	0.20	3.0	7	28	348
9099		1100 W	1200 S	5487.02	6372.73	0.10	3.0	5	51	364
9099		1275 W	900 S	5392.17	6125.80	0.60	3.0	6	24	268
9099		1275 W	925 S	5383.45	6149.25	0.50	3.0	12	26	630
9099		1275 W	950 S	5374.72	6172.70	0.40	3.0	5	29	354
9099		1275 W	975 S	5365.99	6196.14	1.10	3.0	14	42	970
9099		1275 W	1000 S	5357.27	6219.59	0.80	3.0	8	32	330
9099		1275 W	1025 S	5348.54	6243.03	0.50	3.0	9	35	267

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9099	1275 W	1050 S	5339.81	6266.48	0.50	3.0	8	24	310
9099	1275 W	1075 S	5331.09	6289.93	0.40	3.0	6	18	243
9099	1275 W	1100 S	5322.36	6313.37	0.50	3.0	7	26	213
9099	1275 W	1125 S	5313.64	6336.82	0.50	3.0	6	28	246
9099	1275 W	1150 S	5304.91	6360.26	0.60	3.0	7	32	346
9099	1275 W	1175 S	5296.18	6383.71	0.20	3.0	8	28	205
9099	1275 W	1200 S	5287.46	6407.16	0.40	3.0	9	28	216
9099	1450 W	800 S	5232.11	6128.19	0.90	3.0	11	47	630
9099	1450 W	825 S	5221.98	6154.11	0.50	3.0	9	65	400
9099	1450 W	850 S	5211.85	6180.03	0.60	3.0	12	172	690
9099	1450 W	875 S	5201.73	6205.95	0.70	3.0	8	48	550
9099	1450 W	900 S	5191.60	6231.87	0.50	3.0	7	41	284
9099	1450 W	925 S	5181.48	6257.79	1.30	3.0	7	42	334
9099	1450 W	950 S	5171.35	6283.71	0.70	3.0	7	52	301
9099	1450 W	975 S	5161.22	6309.62	0.40	3.0	6	43	294
9099	1450 W	1000 S	5151.10	6335.54	0.80	3.0	8	34	350
9099	1450 W	1025 S	5140.97	6361.46	1.90	3.0	30	62	700
9099	1450 W	1050 S	5130.85	6387.38	0.50	3.0	8	30	396
9099	1450 W	1075 S	5120.72	6413.30	1.00	3.0	10	30	317
9099	1450 W	1100 S	5110.59	6439.22	0.90	3.0	8	32	318
9099	1450 W	1125 S	5100.47	6465.14	0.40	3.0	10	28	254
9099	1450 W	1150 S	5090.34	6491.06	0.40	3.0	11	30	218
9099	1525 W	750 S	5013.04	6464.54	0.40	3.0	6	48	290
9099	1525 W	775 S	5022.02	6441.22	0.80	3.0	8	54	450
9099	1525 W	800 S	5031.00	6417.91	0.40	3.0	6	36	395
9099	1525 W	825 S	5039.98	6394.59	0.40	3.0	10	70	248
9099	1525 W	850 S	5048.96	6371.27	0.20	3.0	6	29	288
9099	1525 W	875 S	5057.94	6347.95	1.50	3.0	8	50	590
9099	1525 W	900 S	5066.92	6324.64	0.50	3.0	9	37	394
9099	1525 W	925 S	5075.90	6301.32	0.50	3.0	7	27	385
9099	1525 W	950 S	5084.87	6278.00	2.10	3.0	40	80	400
9099	1525 W	975 S	5093.85	6254.69	1.80	3.0	45	71	650
9099	1525 W	1000 S	5102.83	6231.37	0.30	3.0	11	27	273
9099	1525 W	1025 S	5111.81	6208.05	0.40	3.0	10	18	218
9099	1525 W	1055 S	5122.59	6180.07	0.10	3.0	13	20	204
9099	1525 W	1075 S	5129.77	6161.42	0.20	3.0	8	20	205
9099	1525 W	1100 S	5138.75	6138.10	0.20	3.0	6	18	208
9099	1625 W	700 S	4901.92	6475.08	0.50	3.0	6	20	243
9099	1625 W	725 S	4910.83	6451.46	0.10	3.0	8	34	120
9099	1625 W	750 S	4919.73	6427.83	0.40	3.0	8	14	200
9099	1625 W	775 S	4928.64	6404.21	0.30	3.0	11	50	250
9099	1625 W	800 S	4937.55	6380.58	0.40	3.0	8	27	243
9099	1625 W	825 S	4946.45	6356.96	0.10	3.0	7	25	262
9099	1625 W	850 S	4955.36	6333.34	0.20	25.0	7	30	234
9099	1625 W	875 S	4964.27	6309.71	0.20	3.0	7	20	290
9099	1625 W	900 S	4973.17	6286.09	0.20	3.0	8	23	328
9099	1625 W	925 S	4982.08	6262.46	1.00	3.0	20	30	313
9099	1625 W	950 S	4990.99	6238.84	1.60	3.0	32	48	620

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<u>Lab</u> <u>Proj.</u>	<u>Field</u> <u>Line</u>	<u>Grid</u> <u>Station</u>	<u>UTM Grid</u>		<u>Ag</u> <u>ppm</u>	<u>Au</u> <u>ppb</u>	<u>Cu</u> <u>ppm</u>	<u>Pb</u> <u>ppm</u>	<u>Zn</u> <u>ppm</u>
			<u>East</u>	<u>North</u>					
9099	1625 W	975 S	4999.89	6215.22	0.10	3.0	7	22	247
9099	1625 W	1000 S	5008.80	6191.59	0.40	3.0	17	25	203
9099	1625 W	1025 S	5017.71	6167.97	0.10	3.0	11	20	178
9099	1625 W	1045 S	5024.83	6149.07	0.60	3.0	13	24	162
9099	1675 W	700 S	4961.07	6178.43	0.30	3.0	12	26	155
9099	1675 W	725 S	4952.26	6201.71	0.30	3.0	9	21	210
9099	1675 W	750 S	4943.46	6225.00	0.40	3.0	11	20	220
9099	1675 W	775 S	4934.65	6248.29	0.90	3.0	28	39	470
9099	1675 W	800 S	4925.84	6271.57	0.30	3.0	10	31	343
9099	1675 W	825 S	4917.03	6294.86	0.40	3.0	10	22	630
9099	1675 W	850 S	4908.22	6318.14	0.30	3.0	8	27	387
9099	1675 W	875 S	4899.42	6341.43	0.50	3.0	10	34	480
9099	1675 W	900 S	4890.61	6364.72	0.20	3.0	8	20	284
9099	1675 W	925 S	4881.80	6388.00	1.80	3.0	40	63	560
9099	1675 W	950 S	4873.00	6411.29	0.40	3.0	10	25	250
9099	1675 W	975 S	4864.19	6434.58	0.70	3.0	17	28	216
9099	1675 W	1000 S	4855.38	6457.86	0.90	3.0	15	27	190
9099	1675 W	1025 S	4846.57	6481.15	1.40	3.0	35	45	352
9099	1675 W	1050 S	4837.76	6504.44	0.40	3.0	13	28	210
9099	1700 W	800 N	4257.61	7850.77	0.10	3.0	17	20	125
9099	1700 W	825 N	4248.94	7873.80	0.10	3.0	9	13	92
9099	1700 W	850 N	4240.27	7896.84	0.10	3.0	9	17	100
9099	1700 W	875 N	4231.61	7919.87	0.10	3.0	8	19	84
9099	1700 W	900 N	4222.94	7942.90	0.10	3.0	11	21	72
9099	1700 W	925 N	4214.27	7965.94	0.10	3.0	6	10	68
9099	1700 W	950 N	4205.60	7988.97	0.10	3.0	10	20	212
9099	1700 W	975 N	4196.93	8012.00	0.10	3.0	11	13	145
9099	1700 W	1000 N	4188.27	8035.03	0.10	3.0	9	7	53
9099	1700 W	1025 N	4179.60	8058.07	0.10	3.0	9	5	46
9099	1700 W	1050 N	4170.93	8081.10	0.10	3.0	11	6	36
9099	1900 W	800 N	4077.85	7778.97	0.10	3.0	8	75	382
9099	1900 W	825 N	4069.69	7802.38	0.10	3.0	9	43	334
9099	1900 W	850 N	4061.53	7825.79	0.10	3.0	7	13	140
9099	1900 W	875 N	4053.37	7849.20	0.10	3.0	8	13	120
9099	1900 W	925 N	4037.04	7896.03	0.10	3.0	10	10	405
9099	1900 W	950 N	4028.88	7919.44	0.10	3.0	18	16	380
9099	1900 W	975 N	4020.72	7942.85	0.10	3.0	11	14	104
9099	1900 W	1000 N	4012.56	7966.26	0.10	3.0	9	3	75
9099	1900 W	1025 N	4004.40	7989.67	0.10	3.0	8	6	54
9099	1900 W	1050 N	3996.24	8013.08	0.10	3.0	8	4	62
9099	2100 W	800 N	3953.78	7727.31	0.10	3.0	6	11	244
9099	2100 W	825 N	3944.99	7750.83	0.10	3.0	6	12	170
9099	2100 W	900 N	3918.61	7821.38	0.10	3.0	8	13	198
9099	2100 W	925 N	3909.82	7844.89	0.10	3.0	3	36	520
9099	2100 W	950 N	3901.02	7868.41	0.70	3.0	8	75	1710
9099	2100 W	975 N	3892.23	7891.93	1.20	3.0	9	145	1600
9099	2100 W	1000 N	3883.44	7915.44	0.10	3.0	6	32	310
9099	2100 W	1025 N	3874.65	7938.96	0.10	3.0	7	12	195

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9099	2100 W	1050 N	3865.85	7962.48	0.10	3.0	7	5	108
9099	2100 W	1075 N	3857.06	7985.99	0.10	3.0	6	6	90
9099	2100 W	1100 N	3848.27	8009.51	0.10	3.0	6	4	80
9135	E	400 N	5977.10	8064.86	0.20	3.0	8	16	205
9135	20 E	1000 N	5834.26	8639.19	0.10	45.0	10	42	126
9135	45 E	1000 N	5856.65	8648.24	0.10	20.0	13	5	53
9109	50 E	325 S	6331.24	7402.72	0.30	3.0	10	13	242
9109	50 E	400 S	6356.46	7332.27	0.30	3.0	15	29	264
9109	50 E	450 S	6373.27	7285.30	0.10	3.0	11	8	122
9109	50 E	475 S	6381.68	7261.82	0.20	15.0	13	10	133
9109	50 E	500 S	6390.08	7238.34	0.10	3.0	12	10	137
9109	50 E	525 S	6398.49	7214.85	0.10	3.0	9	9	92
9109	50 E	550 S	6406.89	7191.37	0.10	3.0	8	13	60
9109	50 E	575 S	6415.30	7167.88	0.10	3.0	16	8	50
9109	50 E	600 S	6423.71	7144.40	0.10	3.0	11	15	157
9109	50 E	625 S	6432.11	7120.92	0.20	3.0	9	14	134
9109	50 E	650 S	6440.52	7097.43	0.10	3.0	11	12	90
9109	50 E	675 S	6448.92	7073.95	0.10	3.0	26	21	93
9109	50 E	700 S	6457.33	7050.47	0.10	3.0	8	23	315
9109	50 E	725 S	6465.74	7026.98	0.30	3.0	15	24	385
9109	50 E	750 S	6474.14	7003.50	0.10	3.0	8	10	182
9109	50 E	775 S	6482.55	6980.02	0.10	3.0	7	9	188
9109	50 E	800 S	6490.95	6956.53	0.10	3.0	13	6	80
9109	50 E	825 S	6499.36	6933.05	0.10	3.0	13	11	184
9135	50 E	1100 N	5827.35	8724.08	0.10	15.0	31	14	70
9135	70 E	1000 N	5879.04	8657.29	0.10	20.0	6	6	43
9135	75 E	1100 N	5849.55	8734.41	0.10	10.0	8	8	118
9135	95 E	1000 N	5901.43	8666.34	0.10	15.0	5	6	65
9109	100 E	275 S	6363.35	7463.68	0.30	3.0	34	25	275
9109	100 E	350 S	6388.21	7393.71	0.10	3.0	11	8	148
9109	100 E	375 S	6396.50	7370.39	0.10	3.0	11	9	97
9109	100 E	400 S	6404.79	7347.07	0.10	3.0	13	6	90
9109	100 E	425 S	6413.07	7323.75	0.20	3.0	15	10	96
9109	100 E	450 S	6421.36	7300.43	0.20	3.0	12	10	124
9109	100 E	475 S	6429.65	7277.10	0.20	3.0	14	9	88
9109	100 E	500 S	6437.93	7253.78	0.10	3.0	21	16	73
9109	100 E	525 S	6446.22	7230.46	0.10	3.0	15	15	215
9109	100 E	550 S	6454.51	7207.14	0.10	3.0	11	8	95
9109	100 E	575 S	6462.79	7183.82	0.10	3.0	12	8	50
9109	100 E	600 S	6471.08	7160.49	0.20	3.0	12	14	180
9109	100 E	625 S	6479.37	7137.17	0.10	3.0	11	7	81
9109	100 E	650 S	6487.65	7113.85	0.10	3.0	12	8	101
9109	100 E	675 S	6495.94	7090.53	0.20	3.0	13	8	96
9109	100 E	700 S	6504.23	7067.21	0.40	3.0	11	8	205
9109	100 E	725 S	6512.52	7043.88	0.50	3.0	10	18	364
9109	100 E	750 S	6520.80	7020.56	3.40	3.0	52	67	1180
9109	100 E	775 S	6529.09	6997.24	0.30	3.0	15	12	246
9135	100 E	1100 N	5871.75	8744.74	0.10	10.0	7	8	45

Continued....



Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9156	100 E	1700 S	6821.48	6123.50	0.10	3.0	6	14	250
9156	100 E	1725 S	6829.68	6099.55	0.20	3.0	8	53	264
9156	100 E	1750 S	6837.89	6075.60	0.40	10.0	8	26	280
9156	100 E	1775 S	6846.09	6051.66	0.10	3.0	7	15	146
9156	100 E	1800 S	6854.29	6027.71	0.80	10.0	6	37	315
9156	100 E	1825 S	6862.50	6003.76	0.30	3.0	21	74	480
9156	100 E	1850 S	6870.70	5979.81	0.10	3.0	12	25	186
9135	120 E	1000 N	5923.82	8675.40	0.10	20.0	7	6	61
9135	125 E	200 N	6214.47	7939.59	0.20	3.0	6	111	540
9135	125 E	800 N	5988.19	8486.19	0.20	3.0	5	33	264
9135	125 E	1100 N	5893.95	8755.08	0.10	3.0	9	9	113
9135	145 E	1000 N	5946.21	8684.45	0.10	25.0	8	10	35
9135	150 E	200 N	6237.52	7948.27	0.30	3.0	8	111	188
9135	150 E	800 N	6011.80	8495.78	0.10	3.0	12	7	110
9135	150 E	1100 N	5916.15	8765.41	0.10	3.0	10	8	74
9135	160 E	1100 N	5925.03	8769.54	0.10	3.0	13	10	52
9135	170 E	1000 N	5968.60	8693.50	0.10	10.0	6	5	37
9135	175 E	200 N	6260.58	7956.96	0.80	3.0	14	333	157
9135	175 E	800 N	6035.40	8505.37	0.10	15.0	9	6	100
9135	195 E	1000 N	5990.99	8702.55	0.10	3.0	6	4	38
9135	200 E	200 N	6283.63	7965.64	0.10	3.0	8	9	123
9135	200 E	800 N	6059.01	8514.96	0.10	3.0	4	4	42
9135	200 E	1100 N	5960.55	8786.07	0.20	3.0	30	10	52
9115	200 E	1550 N	5830.82	9223.26	0.10	3.0	15	6	70
9115	200 E	1600 N	5811.05	9269.01	0.10	3.0	12	5	62
9115	200 E	1650 N	5791.28	9314.77	0.20	3.0	14	5	62
9115	200 E	1700 N	5771.51	9360.52	0.20	3.0	15	5	64
9115	200 E	1750 N	5751.74	9406.27	0.20	3.0	21	7	86
9115	200 E	1800 N	5731.97	9452.02	0.10	3.0	32	4	58
9115	200 E	1850 N	5712.20	9497.78	0.20	3.0	22	6	104
9115	200 E	1900 N	5692.43	9543.53	0.10	3.0	25	5	72
9115	200 E	1950 N	5672.66	9589.28	0.10	10.0	20	4	87
9115	200 E	2000 N	5652.88	9635.03	0.10	20.0	20	11	115
9115	200 E	2050 N	5633.11	9680.78	0.10	3.0	31	5	128
9115	200 E	2100 N	5613.34	9726.54	0.10	10.0	22	4	48
9115	200 E	2150 N	5593.57	9772.29	0.10	3.0	26	5	51
9115	200 E	2200 N	5573.80	9818.04	0.10	3.0	27	5	56
9115	200 E	2250 N	5554.03	9863.79	0.10	3.0	21	9	70
9115	200 E	2300 N	5534.26	9909.55	0.20	3.0	25	4	44
9115	200 E	2350 N	5514.49	9955.30	0.10	3.0	28	5	40
9115	200 E	2400 N	5494.72	10001.05	0.10	3.0	25	5	37
9115	200 E	2450 N	5474.95	10046.80	0.10	3.0	24	6	46
9115	200 E	2500 N	5455.18	10092.55	0.10	3.0	22	7	52
9115	200 E	2550 N	5435.41	10138.31	0.10	3.0	27	7	56
9115	200 E	2600 N	5415.64	10184.06	0.10	3.0	33	5	48
9115	200 E	2650 N	5395.87	10229.81	0.10	3.0	19	4	45
9115	200 E	2700 N	5376.10	10275.56	0.10	3.0	17	4	46
9115	200 E	2750 N	5356.33	10321.32	0.10	10.0	22	6	66

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9115	200 E	2800 N	5336.56	10367.07	0.10	3.0	10	4	34
9115	200 E	2850 N	5316.79	10412.82	0.10	3.0	9	5	40
9115	200 E	2900 N	5297.02	10458.57	0.10	3.0	14	5	56
9115	200 E	2950 N	5277.25	10504.33	0.10	3.0	12	6	45
9115	200 E	3000 N	5257.48	10550.08	0.10	3.0	17	6	80
9115	200 E	3050 N	5237.70	10595.83	0.10	3.0	14	6	67
9115	200 E	3100 N	5217.93	10641.58	0.10	3.0	11	5	58
9115	200 E	3150 N	5198.16	10687.33	0.10	3.0	16	5	61
9115	200 E	3200 N	5178.39	10733.09	0.10	3.0	17	5	53
9115	200 E	3250 N	5158.62	10778.84	0.10	3.0	14	5	43
9115	200 E	3300 N	5138.85	10824.59	0.10	3.0	13	6	37
9115	200 E	3350 N	5119.08	10870.34	0.10	10.0	14	6	40
9115	200 E	3400 N	5099.31	10916.09	0.10	3.0	11	4	42
9115	200 E	3450 N	5079.54	10961.85	0.10	10.0	11	5	44
9115	200 E	3500 N	5059.77	11007.60	0.10	10.0	12	4	45
9135	220 E	1000 N	6013.38	8711.60	0.10	3.0	9	4	115
9135	225 E	200 N	6306.69	7974.32	0.10	3.0	11	8	82
9135	225 E	400 N	6236.58	8146.32	0.30	20.0	7	20	780
9135	225 E	800 N	6082.62	8524.54	0.10	10.0	6	4	60
9135	225 E	1100 N	5982.75	8796.41	0.10	3.0	27	10	52
9135	250 E	200 N	6329.74	7983.00	0.10	3.0	12	7	118
9135	250 E	400 N	6259.07	8156.65	0.40	3.0	5	34	470
9135	250 E	800 N	6106.23	8534.13	0.10	3.0	6	3	32
9135	250 E	1000 N	6040.25	8722.47	0.10	3.0	8	5	77
9135	250 E	1100 N	6004.95	8806.74	0.10	3.0	11	9	49
9135	275 E	200 N	6352.80	7991.69	0.10	3.0	18	10	76
9135	275 E	400 N	6281.55	8166.98	0.30	3.0	5	47	590
9135	275 E	800 N	6129.83	8543.72	0.10	10.0	6	3	40
9135	275 E	1100 N	6027.15	8817.07	0.10	3.0	10	6	68
9135	300 E	200 N	6375.85	8000.37	0.10	3.0	13	8	75
9135	300 E	400 N	6304.04	8177.31	0.50	3.0	5	224	257
9135	300 E	800 N	6153.44	8553.31	0.10	3.0	8	5	28
9109	300 E	125 S	6487.18	7684.76	0.20	3.0	14	9	92
9109	300 E	150 S	6495.64	7661.23	0.20	3.0	11	6	72
9109	300 E	175 S	6504.09	7637.69	0.20	3.0	13	7	78
9109	300 E	200 S	6512.54	7614.16	0.20	3.0	13	7	67
9109	300 E	250 S	6529.46	7567.09	0.10	20.0	9	10	90
9109	300 E	282 S	6540.28	7536.97	0.20	3.0	22	16	80
9109	300 E	325 S	6554.82	7496.49	0.20	3.0	23	14	114
9135	300 E	1000 N	6085.03	8740.57	0.10	25.0	16	5	53
9135	300 E	1100 N	6049.35	8827.40	0.10	3.0	10	9	60
9156	300 E	1750 S	7019.76	6155.85	0.20	3.0	6	14	142
9156	300 E	1775 S	7028.36	6132.37	0.10	3.0	8	10	180
9156	300 E	1800 S	7036.97	6108.88	0.10	3.0	17	19	151
9156	300 E	1825 S	7045.58	6085.40	0.20	5.0	9	9	121
9156	300 E	1850 S	7054.18	6061.91	0.20	15.0	6	12	256
9135	325 E	200 N	6398.91	8009.05	0.10	3.0	15	6	85
9135	325 E	400 N	6326.53	8187.64	0.20	3.0	8	42	270

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9135	325 E	800 N	6177.05	8562.90	0.10	3.0	7	7	29
9135	325 E	1000 N	6107.42	8749.62	0.10	5.0	20	4	78
9135	325 E	1100 N	6071.55	8837.73	0.10	3.0	16	10	51
9135	350 E	200 N	6421.96	8017.73	0.10	20.0	10	5	52
9135	350 E	400 N	6349.02	8197.97	0.40	3.0	9	27	388
9135	350 E	600 N	6274.53	8382.12	0.30	15.0	7	57	104
9135	350 E	800 N	6200.66	8572.48	0.10	3.0	6	7	70
9135	350 E	1000 N	6129.81	8758.68	0.10	15.0	12	4	50
9135	350 E	1100 N	6093.75	8848.07	0.10	3.0	21	10	47
9135	375 E	200 N	6445.02	8026.42	0.10	10.0	10	6	56
9135	375 E	400 N	6371.50	8208.30	0.20	3.0	10	7	231
9135	375 E	600 N	6298.42	8392.53	0.20	10.0	6	7	27
9135	375 E	800 N	6224.26	8582.07	0.10	160.0	8	5	78
9135	375 E	1000 N	6152.20	8767.73	0.10	10.0	15	4	75
9135	375 E	1100 N	6115.95	8858.40	0.10	3.0	14	9	86
9115	400 E	1550 N	5972.51	9283.81	0.10	3.0	27	4	50
9115	400 E	1600 N	5952.64	9329.62	0.10	3.0	14	5	57
9115	400 E	1650 N	5932.76	9375.42	0.20	3.0	24	5	56
9115	400 E	1700 N	5912.89	9421.23	0.20	3.0	23	4	78
9115	400 E	1750 N	5893.02	9467.04	0.20	3.0	34	3	57
9115	400 E	1800 N	5873.15	9512.85	0.10	3.0	24	2	76
9115	400 E	1850 N	5853.27	9558.66	0.20	3.0	22	4	90
9115	400 E	1900 N	5833.40	9604.47	0.10	3.0	34	6	84
9115	400 E	1950 N	5813.53	9650.28	0.10	3.0	22	6	125
9115	400 E	2000 N	5793.66	9696.08	0.10	3.0	19	4	162
9115	400 E	2050 N	5773.79	9741.89	0.10	3.0	21	3	152
9115	400 E	2100 N	5753.91	9787.70	0.10	3.0	27	5	77
9115	400 E	2150 N	5734.04	9833.51	0.10	3.0	24	4	60
9115	400 E	2200 N	5714.17	9879.32	0.10	3.0	31	4	68
9115	400 E	2250 N	5694.30	9925.13	0.10	3.0	21	4	46
9115	400 E	2300 N	5674.42	9970.93	0.10	3.0	26	5	44
9115	400 E	2350 N	5654.55	10016.74	0.10	3.0	30	5	64
9115	400 E	2400 N	5634.68	10062.55	0.10	3.0	30	5	50
9115	400 E	2450 N	5614.81	10108.36	0.10	3.0	34	4	48
9115	400 E	2500 N	5594.94	10154.17	0.10	3.0	28	4	48
9115	400 E	2550 N	5575.06	10199.97	0.10	3.0	22	4	47
9115	400 E	2600 N	5555.19	10245.78	0.10	3.0	18	4	37
9115	400 E	2650 N	5535.32	10291.59	0.10	3.0	17	3	44
9115	400 E	2700 N	5515.45	10337.40	0.10	3.0	19	4	54
9115	400 E	2750 N	5495.57	10383.21	0.10	3.0	10	4	54
9115	400 E	2850 N	5455.83	10474.82	0.10	3.0	13	3	57
9115	400 E	2900 N	5435.96	10520.63	0.10	3.0	9	4	42
9115	400 E	2950 N	5416.09	10566.44	0.10	3.0	12	3	49
9115	400 E	3000 N	5396.21	10612.25	0.10	3.0	15	4	46
9115	400 E	3050 N	5376.34	10658.06	0.10	3.0	18	4	73
9115	400 E	3100 N	5356.47	10703.87	0.10	3.0	22	4	89
9115	400 E	3150 N	5336.60	10749.67	0.10	3.0	11	4	55
9115	400 E	3200 N	5316.72	10795.48	0.10	3.0	10	5	41

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9115	400 E	3250 N	5296.85	10841.29	0.10	3.0	11	3	41
9115	400 E	3300 N	5276.98	10887.10	0.10	3.0	12	5	35
9099	500 E	700 N	6385.85	8533.79	0.50	3.0	18	3	98
9099	500 E	725 N	6376.78	8557.02	0.30	3.0	17	9	93
9099	500 E	750 N	6367.70	8580.24	0.20	3.0	18	3	96
9099	500 E	775 N	6358.62	8603.46	0.30	20.0	17	7	86
9099	500 E	800 N	6349.54	8626.68	0.30	3.0	14	8	82
9099	500 E	825 N	6340.46	8649.91	0.20	3.0	14	5	79
9099	500 E	850 N	6331.39	8673.13	0.20	3.0	24	3	99
9099	500 E	875 N	6322.31	8696.35	0.20	3.0	14	7	75
9099	500 E	900 N	6313.23	8719.57	0.10	3.0	15	5	88
9099	500 E	925 N	6304.15	8742.80	0.30	3.0	19	6	64
9099	500 E	950 N	6295.07	8766.02	0.10	3.0	12	3	77
9099	500 E	975 N	6286.00	8789.24	0.10	3.0	18	10	87
9099	500 E	1000 N	6276.92	8812.46	0.20	3.0	12	6	68
9099	500 E	1050 N	6258.76	8858.91	0.30	3.0	17	6	84
9099	500 E	1075 N	6249.68	8882.13	0.20	3.0	22	1	85
9099	500 E	1100 N	6240.61	8905.35	0.20	3.0	24	8	65
9099	500 E	1125 N	6231.53	8928.58	0.20	3.0	25	4	47
9099	500 E	1150 N	6222.45	8951.80	0.30	3.0	35	10	42
9099	500 E	1175 N	6213.37	8975.02	0.30	3.0	40	6	48
9099	500 E	1200 N	6204.29	8998.25	0.40	3.0	26	9	64
9099	500 E	1225 N	6195.22	9021.47	0.20	3.0	25	7	49
9099	500 E	1250 N	6186.14	9044.69	0.30	3.0	26	5	48
9099	500 E	1275 N	6177.06	9067.91	0.20	3.0	37	9	61
9099	500 E	1300 N	6167.98	9091.13	0.30	3.0	16	9	57
9099	500 E	1325 N	6158.90	9114.36	0.30	3.0	18	4	73
9099	500 E	1350 N	6149.83	9137.58	0.20	3.0	21	8	81
9099	500 E	1375 N	6140.75	9160.80	0.30	3.0	16	5	69
9099	500 E	1400 N	6131.67	9184.03	0.20	3.0	16	4	50
9099	500 E	1425 N	6122.59	9207.25	0.10	3.0	20	2	58
9099	500 E	1450 N	6113.51	9230.47	0.40	3.0	21	3	73
9099	500 E	1475 N	6104.44	9253.69	0.20	3.0	24	9	77
9099	500 E	1500 N	6095.36	9276.92	0.30	3.0	30	9	94
9156	500 E	1850 S	7311.81	6165.10	0.30	10.0	13	22	530
9156	500 E	1875 S	7320.89	6141.88	0.50	10.0	17	30	1080
9156	500 E	1900 S	7329.96	6118.65	0.30	10.0	8	18	228
9156	500 E	1925 S	7339.04	6095.43	0.20	10.0	23	23	226
9156	500 E	1950 S	7348.12	6072.21	0.70	5.0	22	21	400
9115	600 E	1550 N	6171.27	9360.86	0.10	3.0	22	5	72
9115	600 E	1600 N	6150.16	9405.62	0.10	3.0	22	3	58
9115	600 E	1650 N	6129.04	9450.38	0.10	3.0	17	3	80
9115	600 E	1700 N	6107.92	9495.14	0.10	3.0	27	4	70
9115	600 E	1750 N	6086.80	9539.90	0.10	3.0	24	5	65
9115	600 E	1800 N	6065.69	9584.66	0.10	3.0	11	4	62
9115	600 E	1850 N	6044.57	9629.42	0.10	10.0	15	5	75
9115	600 E	1900 N	6023.45	9674.18	0.10	3.0	14	6	60
9115	600 E	1950 N	6002.33	9718.94	0.10	3.0	18	6	62

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9115	600 E	2000 N	5981.22	9763.70	0.10	5.0	23	4	46
9115	600 E	2050 N	5960.10	9808.46	0.10	3.0	20	3	35
9115	600 E	2100 N	5938.98	9853.22	0.10	3.0	28	4	47
9115	600 E	2150 N	5917.87	9897.98	0.10	3.0	26	4	49
9115	600 E	2200 N	5896.75	9942.74	0.10	3.0	21	3	46
9115	600 E	2250 N	5875.63	9987.50	0.10	3.0	27	3	60
9115	600 E	2300 N	5854.51	10032.25	0.10	3.0	35	5	120
9115	600 E	2350 N	5833.40	10077.01	0.10	3.0	14	7	123
9115	600 E	2400 N	5812.28	10121.77	0.10	3.0	11	3	33
9115	600 E	2450 N	5791.16	10166.53	0.10	3.0	16	3	39
9115	600 E	2500 N	5770.04	10211.29	0.10	3.0	60	6	35
9115	600 E	2550 N	5748.93	10256.05	0.10	3.0	8	3	22
9115	600 E	2650 N	5706.69	10345.57	0.10	3.0	8	3	23
9115	600 E	2700 N	5685.58	10390.33	0.10	3.0	12	3	37
9115	600 E	2750 N	5664.46	10435.09	0.10	3.0	25	5	40
9115	600 E	2800 N	5643.34	10479.85	0.10	3.0	11	5	52
9115	600 E	2850 N	5622.22	10524.61	0.10	3.0	19	6	56
9115	600 E	2900 N	5601.11	10569.37	0.10	3.0	11	4	57
9115	600 E	2950 N	5579.99	10614.13	0.10	3.0	12	4	46
9115	600 E	3000 N	5558.87	10658.89	0.10	3.0	8	4	45
9115	600 E	3050 N	5537.75	10703.65	0.10	3.0	10	4	44
9115	600 E	3100 N	5516.64	10748.41	0.10	10.0	7	6	36
9115	600 E	3150 N	5495.52	10793.17	0.10	3.0	10	3	40
9099	700 E	575 N	6612.39	8486.16	0.30	3.0	20	4	88
9099	700 E	600 N	6603.30	8509.34	0.40	3.0	13	8	72
9099	700 E	625 N	6594.22	8532.52	0.30	3.0	14	10	103
9099	700 E	650 N	6585.14	8555.70	0.30	3.0	17	6	99
9099	700 E	675 N	6576.06	8578.89	0.10	3.0	18	2	89
9099	700 E	700 N	6566.98	8602.07	0.10	3.0	23	4	64
9099	700 E	725 N	6557.90	8625.25	0.10	3.0	31	5	88
9099	700 E	750 N	6548.82	8648.43	0.10	3.0	45	5	67
9099	700 E	775 N	6539.74	8671.62	0.20	3.0	53	6	72
9099	700 E	800 N	6530.66	8694.80	0.40	3.0	89	5	47
9099	700 E	825 N	6521.58	8717.98	0.20	3.0	38	3	46
9099	700 E	850 N	6512.49	8741.16	0.10	3.0	104	7	58
9099	700 E	875 N	6503.41	8764.34	0.30	3.0	117	9	61
9099	700 E	900 N	6494.33	8787.53	0.20	3.0	108	10	53
9099	700 E	925 N	6485.25	8810.71	0.10	3.0	52	9	51
9099	700 E	950 N	6476.17	8833.89	0.10	3.0	35	5	58
9099	700 E	975 N	6467.09	8857.07	0.20	3.0	45	5	67
9156	700 E	850 S	7130.01	7164.76	0.10	3.0	9	6	55
9156	700 E	875 S	7139.09	7141.58	0.10	3.0	11	6	92
9156	700 E	900 S	7148.17	7118.39	0.10	3.0	13	12	130
9156	700 E	925 S	7157.25	7095.21	0.10	10.0	10	9	182
9156	700 E	950 S	7166.33	7072.03	0.10	5.0	5	7	100
9156	700 E	975 S	7175.41	7048.85	0.30	3.0	27	8	273
9099	700 E	1000 N	6458.01	8880.26	0.10	3.0	29	5	68
9099	700 E	1025 N	6448.93	8903.44	0.10	3.0	27	9	55

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9099	700 E	1050 N	6439.85	8926.62	0.10	3.0	26	4	66
9099	700 E	1075 N	6430.76	8949.80	0.10	3.0	34	3	50
9099	700 E	1100 N	6421.68	8972.99	0.10	3.0	26	2	51
9099	700 E	1125 N	6412.60	8996.17	0.10	3.0	24	6	54
9099	700 E	1150 N	6403.52	9019.35	0.10	3.0	21	2	55
9099	700 E	1175 N	6394.44	9042.53	0.10	3.0	19	6	55
9099	700 E	1200 N	6385.36	9065.72	0.10	3.0	25	4	63
9099	700 E	1250 N	6367.20	9112.08	0.20	3.0	25	3	53
9099	700 E	1275 N	6358.12	9135.26	0.20	175.0	24	6	72
9099	700 E	1300 N	6349.03	9158.45	0.10	3.0	25	4	48
9099	700 E	1325 N	6339.95	9181.63	0.10	3.0	29	7	75
9099	700 E	1350 N	6330.87	9204.81	0.10	3.0	19	4	64
9099	700 E	1375 N	6321.79	9227.99	0.30	3.0	21	13	77
9099	700 E	1400 N	6312.71	9251.18	0.10	3.0	27	4	78
9099	700 E	1425 N	6303.63	9274.36	0.20	3.0	21	8	65
9099	700 E	1450 N	6294.55	9297.54	0.30	3.0	16	5	49
9099	700 E	1475 N	6285.47	9320.72	0.20	3.0	14	5	41
9099	700 E	1500 N	6276.39	9343.91	0.10	3.0	22	5	69
9156	700 E	1000 S	7184.49	7025.66	0.20	10.0	16	9	148
9156	700 E	1025 S	7193.57	7002.48	0.20	3.0	12	8	92
9156	700 E	1050 S	7202.65	6979.30	0.10	3.0	9	5	48
9156	700 E	1900 S	7511.41	6191.10	1.20	3.0	38	32	610
9156	700 E	1925 S	7520.49	6167.91	0.10	10.0	9	16	236
9156	700 E	1950 S	7529.57	6144.73	0.20	10.0	10	16	244
9156	700 E	1975 S	7538.65	6121.55	0.10	10.0	17	12	74
9156	700 E	2000 S	7547.73	6098.37	0.20	15.0	22	48	128
9156	700 E	2025 S	7556.82	6075.18	0.20	10.0	15	20	177
9156	700 E	2050 S	7565.90	6052.00	0.20	10.0	21	12	182
9099	750 E	575 N	6658.25	8507.18	0.10	3.0	25	4	72
9099	750 E	600 N	6649.16	8530.18	0.10	3.0	23	3	60
9099	750 E	625 N	6640.07	8553.19	0.10	3.0	108	9	68
9099	750 E	650 N	6630.97	8576.19	0.10	3.0	28	3	88
9099	750 E	675 N	6621.88	8599.19	0.20	3.0	31	7	77
9099	750 E	700 N	6612.79	8622.19	0.20	3.0	23	7	74
9099	750 E	725 N	6603.70	8645.20	0.10	3.0	26	7	71
9099	750 E	750 N	6594.61	8668.20	0.30	3.0	35	6	65
9099	750 E	775 N	6585.52	8691.20	0.20	3.0	30	6	71
9099	750 E	800 N	6576.42	8714.21	0.30	3.0	28	4	69
9099	750 E	825 N	6567.33	8737.21	0.20	3.0	30	6	74
9099	750 E	850 N	6558.24	8760.21	0.30	3.0	25	3	47
9099	750 E	875 N	6549.15	8783.22	0.20	3.0	26	4	55
9099	750 E	900 N	6540.06	8806.22	0.10	3.0	20	8	66
9099	750 E	925 N	6530.97	8829.22	0.10	3.0	19	5	42
9099	750 E	950 N	6521.87	8852.22	0.20	3.0	21	4	41
9099	750 E	975 N	6512.78	8875.23	0.10	3.0	25	4	60
9099	750 E	1000 N	6503.69	8898.23	0.10	3.0	20	6	63
9115	800 E	1550 N	6331.36	9427.08	0.10	3.0	31	3	40
9115	800 E	1600 N	6309.55	9471.29	0.10	3.0	33	4	46

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9115	800 E	1650 N	6287.74	9515.50	0.10	3.0	22	4	38
9115	800 E	1700 N	6265.94	9559.71	0.10	3.0	28	4	50
9115	800 E	1750 N	6244.13	9603.92	0.10	3.0	26	4	53
9115	800 E	1800 N	6222.32	9648.13	0.10	10.0	26	4	54
9115	800 E	1850 N	6200.51	9692.33	0.10	10.0	20	4	56
9115	800 E	1900 N	6178.70	9736.54	0.10	3.0	20	3	57
9115	800 E	1950 N	6156.89	9780.75	0.20	3.0	38	4	52
9115	800 E	2000 N	6135.09	9824.96	0.10	3.0	25	4	42
9115	800 E	2050 N	6113.28	9869.17	0.40	3.0	34	5	48
9115	800 E	2100 N	6091.47	9913.38	0.20	3.0	35	5	52
9115	800 E	2150 N	6069.66	9957.59	0.10	3.0	23	4	70
9115	800 E	2200 N	6047.85	10001.80	0.10	3.0	15	9	63
9115	800 E	2250 N	6026.04	10046.01	0.10	3.0	13	8	55
9115	800 E	2300 N	6004.24	10090.22	0.10	3.0	16	5	48
9115	800 E	2400 N	5960.62	10178.64	0.30	3.0	104	6	24
9115	800 E	2450 N	5938.81	10222.85	0.10	3.0	36	5	42
9115	800 E	2500 N	5917.00	10267.06	0.10	3.0	20	3	41
9115	800 E	2550 N	5895.19	10311.26	0.10	3.0	15	3	42
9115	800 E	2600 N	5873.38	10355.47	0.10	3.0	11	2	15
9115	800 E	2650 N	5851.58	10399.68	0.30	3.0	62	7	44
9115	800 E	2700 N	5829.77	10443.89	0.10	3.0	10	6	34
9115	800 E	2750 N	5807.96	10488.10	0.10	3.0	18	5	27
9115	800 E	2800 N	5786.15	10532.31	0.30	3.0	43	5	53
9115	800 E	2850 N	5764.34	10576.52	0.30	3.0	27	6	62
9115	800 E	2900 N	5742.53	10620.73	0.10	3.0	18	6	49
9115	800 E	2950 N	5720.73	10664.94	0.10	3.0	15	4	48
9115	800 E	3000 N	5698.92	10709.15	0.10	3.0	19	5	43
9115	800 E	3050 N	5677.11	10753.36	0.10	3.0	16	6	102
9115	800 E	3100 N	5655.30	10797.57	0.10	3.0	14	3	57
9115	800 E	3150 N	5633.49	10841.78	0.10	3.0	10	3	33
9115	800 E	3200 N	5611.68	10885.99	0.10	3.0	14	4	53
9099	850 E	375 N	6804.56	8352.65	0.10	3.0	16	13	173
9099	850 E	400 N	6795.87	8375.99	0.10	3.0	13	10	132
9099	850 E	425 N	6787.18	8399.32	0.10	3.0	18	9	72
9099	850 E	475 N	6769.79	8445.99	0.10	3.0	31	4	51
9099	850 E	500 N	6761.10	8469.33	0.10	3.0	32	5	48
9099	850 E	525 N	6752.41	8492.66	0.10	3.0	44	4	56
9099	850 E	550 N	6743.72	8516.00	0.20	3.0	49	7	72
9099	850 E	575 N	6735.02	8539.33	0.30	3.0	53	10	77
9099	850 E	600 N	6726.33	8562.67	0.30	3.0	45	2	63
9099	850 E	625 N	6717.64	8586.01	0.20	3.0	28	4	67
9099	850 E	650 N	6708.95	8609.34	0.30	3.0	30	6	67
9099	850 E	675 N	6700.26	8632.68	0.40	3.0	48	6	60
9099	850 E	700 N	6691.56	8656.01	0.20	3.0	39	4	61
9099	850 E	725 N	6682.87	8679.35	0.40	3.0	25	9	56
9099	850 E	750 N	6674.18	8702.68	0.30	3.0	54	5	67
9099	850 E	775 N	6665.49	8726.02	0.20	3.0	27	6	83
9099	850 E	800 N	6656.80	8749.36	0.40	3.0	26	4	64

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9099	850 E	825 N	6648.10	8772.69	0.20	3.0	24	3	80
9099	850 E	850 N	6639.41	8796.03	0.20	3.0	26	5	61
9099	850 E	875 N	6630.72	8819.36	0.40	3.0	19	5	86
9099	850 E	900 N	6622.03	8842.70	0.30	3.0	14	3	54
9099	850 E	925 N	6613.34	8866.03	0.20	3.0	22	5	88
9099	850 E	950 N	6604.64	8889.37	0.30	3.0	19	4	75
9099	850 E	975 N	6595.95	8912.70	0.20	3.0	29	6	64
9099	850 E	1000 N	6587.26	8936.04	0.20	110.0	24	7	47
9108	900 E	00	7008.59	8020.96	0.10	3.0	103	4	61
9108	900 E	25 S	7017.23	7997.57	0.10	3.0	13	14	73
9108	900 E	50 S	7025.87	7974.18	0.10	3.0	36	11	163
9108	900 E	65 S	7031.05	7960.14	0.10	3.0	50	10	108
9099	900 E	375 N	6878.99	8371.85	0.40	3.0	60	6	50
9099	900 E	400 N	6870.35	8395.24	0.40	3.0	44	6	47
9099	900 E	425 N	6861.71	8418.63	0.40	3.0	28	5	37
9099	900 E	450 N	6853.07	8442.02	0.10	3.0	29	5	41
9099	900 E	475 N	6844.43	8465.42	0.20	3.0	47	6	60
9099	900 E	500 N	6835.79	8488.81	0.20	35.0	25	5	62
9099	900 E	525 N	6827.15	8512.20	0.40	3.0	26	5	46
9099	900 E	550 N	6818.51	8535.59	0.20	3.0	30	6	46
9099	900 E	575 N	6809.87	8558.99	0.40	3.0	41	7	45
9099	900 E	600 N	6801.23	8582.38	0.30	3.0	52	7	54
9099	900 E	625 N	6792.59	8605.77	0.10	3.0	35	5	45
9099	900 E	650 N	6783.95	8629.16	0.10	3.0	27	6	42
9099	900 E	675 N	6775.31	8652.56	0.20	3.0	35	5	42
9099	900 E	700 N	6766.67	8675.95	0.10	3.0	22	5	60
9099	900 E	725 N	6758.03	8699.34	0.10	3.0	29	4	60
9099	900 E	750 N	6749.39	8722.73	0.10	3.0	31	6	50
9099	900 E	775 N	6740.75	8746.13	0.10	3.0	22	4	42
9099	900 E	800 N	6732.11	8769.52	0.10	3.0	29	6	46
9099	900 E	825 N	6723.47	8792.91	0.10	3.0	27	6	53
9099	900 E	850 N	6714.83	8816.30	0.10	3.0	27	5	48
9099	900 E	875 N	6706.20	8839.70	0.10	3.0	32	7	52
9099	900 E	900 N	6697.56	8863.09	0.10	3.0	29	6	48
9099	900 E	925 N	6688.92	8886.48	0.10	3.0	22	5	55
9099	900 E	950 N	6680.28	8909.87	0.10	3.0	27	5	50
9099	900 E	975 N	6671.64	8933.26	0.20	3.0	22	5	62
9108	900 E	100 S	7043.15	7927.39	0.10	3.0	37	9	66
9108	900 E	125 S	7051.79	7904.00	0.10	3.0	19	5	80
9108	900 E	150 S	7060.43	7880.61	0.10	3.0	35	11	62
9108	900 E	175 S	7069.07	7857.21	0.10	3.0	20	6	43
9108	900 E	200 S	7077.71	7833.82	0.10	3.0	29	8	70
9108	900 E	225 S	7086.35	7810.43	0.10	3.0	20	5	80
9108	900 E	250 S	7094.99	7787.04	0.10	3.0	20	5	82
9108	900 E	275 S	7103.63	7763.64	0.10	3.0	20	5	68
9108	900 E	300 S	7112.27	7740.25	0.10	3.0	16	6	80
9108	900 E	325 S	7120.91	7716.86	0.10	3.0	15	4	71
9108	900 E	350 S	7129.55	7693.47	0.10	3.0	21	2	75

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	900 E	375 S	7138.19	7670.07	0.10	5.0	11	6	70
9108	900 E	400 S	7146.83	7646.68	0.10	3.0	11	7	110
9108	900 E	425 S	7155.47	7623.29	0.10	3.0	12	6	25
9108	900 E	450 S	7164.11	7599.90	0.10	3.0	14	5	25
9108	900 E	475 S	7172.75	7576.50	0.10	3.0	14	4	60
9108	900 E	500 S	7181.39	7553.11	0.10	3.0	15	7	228
9156	900 E	850 S	7302.34	7225.62	0.50	20.0	35	6	307
9156	900 E	875 S	7310.98	7202.23	1.40	15.0	69	10	840
9156	900 E	900 S	7319.62	7178.83	2.20	20.0	95	10	760
9156	900 E	925 S	7328.26	7155.44	1.60	5.0	83	12	294
9156	900 E	950 S	7336.90	7132.05	0.40	3.0	15	10	122
9156	900 E	975 S	7345.54	7108.66	0.60	10.0	14	11	123
9099	900 E	1000 N	6663.00	8956.66	0.20	3.0	30	8	53
9099	900 E	1025 N	6654.36	8980.05	0.30	3.0	77	9	50
9099	900 E	1050 N	6645.72	9003.44	0.40	3.0	124	10	43
9099	900 E	1075 N	6637.08	9026.83	0.30	3.0	84	8	50
9099	900 E	1100 N	6628.44	9050.23	0.30	3.0	77	8	58
9099	900 E	1150 N	6611.16	9097.01	0.30	3.0	128	6	40
9099	900 E	1175 N	6602.52	9120.40	0.10	3.0	40	6	40
9099	900 E	1200 N	6593.88	9143.80	0.10	3.0	28	4	37
9099	900 E	1225 N	6585.24	9167.19	0.10	3.0	23	5	42
9099	900 E	1250 N	6576.60	9190.58	0.20	3.0	113	6	44
9099	900 E	1275 N	6567.96	9213.97	0.10	3.0	65	6	46
9099	900 E	1300 N	6559.32	9237.37	0.30	3.0	66	9	50
9099	900 E	1325 N	6550.68	9260.76	0.10	3.0	32	6	51
9099	900 E	1350 N	6542.04	9284.15	0.10	3.0	42	8	42
9099	900 E	1375 N	6533.40	9307.54	0.10	3.0	43	6	53
9099	900 E	1400 N	6524.76	9330.94	0.10	3.0	43	7	44
9099	900 E	1425 N	6516.12	9354.33	0.10	3.0	34	7	40
9099	900 E	1450 N	6507.48	9377.72	0.10	3.0	35	28	77
9099	900 E	1475 N	6498.84	9401.11	0.10	3.0	26	5	51
9099	900 E	1500 N	6490.20	9424.51	0.10	3.0	31	5	44
9099	900 E	1525 N	6481.56	9447.90	0.60	3.0	124	7	62
9099	900 E	1550 N	6472.92	9471.29	0.40	3.0	78	8	43
9099	900 E	1575 N	6464.28	9494.68	0.30	3.0	70	8	47
9099	900 E	1600 N	6455.64	9518.08	0.10	3.0	42	6	46
9123	900 E	1650 N	6438.36	9564.86	0.20	3.0	48	6	48
9156	900 E	1000 S	7354.18	7085.26	1.20	3.0	20	13	188
9156	900 E	1025 S	7362.82	7061.87	1.10	3.0	28	11	150
9156	900 E	1050 S	7371.46	7038.48	0.50	10.0	11	9	135
9099	1000 E	1525 N	6578.36	9484.65	0.10	3.0	28	5	42
9099	1000 E	1550 N	6568.12	9507.11	0.10	3.0	36	5	37
9099	1000 E	1575 N	6557.89	9529.58	0.10	3.0	30	5	36
9099	1000 E	1600 N	6547.66	9552.04	0.10	3.0	28	4	44
9115	1000 E	1650 N	6527.19	9596.97	0.10	3.0	27	3	50
9115	1000 E	1700 N	6506.73	9641.91	0.10	3.0	33	3	46
9115	1000 E	1750 N	6486.26	9686.84	0.10	3.0	188	5	68
9115	1000 E	1800 N	6465.80	9731.77	0.10	3.0	26	4	61

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9115	1000 E	1850 N	6445.33	9776.70	0.10	3.0	172	6	80
9115	1000 E	1900 N	6424.87	9821.63	0.30	3.0	93	10	70
9115	1000 E	2000 N	6383.94	9911.49	0.10	3.0	50	6	50
9115	1000 E	2050 N	6363.47	9956.42	0.30	3.0	170	7	61
9115	1000 E	2100 N	6343.00	10001.36	0.10	3.0	147	13	67
9115	1000 E	2150 N	6322.54	10046.29	0.20	3.0	26	7	45
9115	1000 E	2200 N	6302.07	10091.22	0.20	3.0	20	3	51
9115	1000 E	2250 N	6281.61	10136.15	0.10	3.0	26	5	49
9115	1000 E	2300 N	6261.14	10181.08	0.10	3.0	26	6	48
9115	1000 E	2350 N	6240.68	10226.01	0.20	3.0	23	7	37
9115	1000 E	2400 N	6220.21	10270.94	0.20	3.0	17	6	35
9115	1000 E	2450 N	6199.75	10315.88	0.10	3.0	10	5	30
9115	1000 E	2500 N	6179.28	10360.81	0.10	3.0	11	4	35
9115	1000 E	2550 N	6158.82	10405.74	0.10	3.0	14	4	28
9115	1000 E	2576 N	6148.17	10429.10	0.10	3.0	23	7	26
9123	1000 E	2615 N	6177.99	10480.14	0.10	3.0	13	4	32
9123	1000 E	2650 N	6166.34	10512.90	0.10	3.0	11	4	27
9123	1000 E	2700 N	6149.71	10559.70	0.10	3.0	9	3	26
9123	1000 E	2750 N	6133.07	10606.49	0.10	3.0	13	5	33
9123	1000 E	2800 N	6116.43	10653.29	0.10	3.0	13	4	32
9123	1000 E	2850 N	6099.79	10700.09	0.10	3.0	10	3	36
9123	1000 E	2900 N	6083.15	10746.88	0.20	10.0	55	8	42
9123	1000 E	2950 N	6066.51	10793.68	0.30	10.0	46	8	48
9123	1000 E	3000 N	6049.87	10840.48	0.20	10.0	38	7	31
9123	1000 E	3050 N	6033.23	10887.27	0.10	3.0	32	6	34
9123	1000 E	3100 N	6016.60	10934.07	0.10	10.0	17	6	30
9123	1000 E	3150 N	5999.96	10980.87	0.10	15.0	13	4	26
9123	1000 E	3200 N	5983.32	11027.66	0.10	10.0	52	7	36
9108	1100 E	25 S	7204.70	8066.74	0.10	3.0	19	7	68
9108	1100 E	50 S	7213.48	8043.25	0.10	3.0	16	7	64
9108	1100 E	75 S	7222.25	8019.76	0.10	3.0	22	7	55
9109	1100 E	100 N	7160.83	8184.18	0.20	3.0	20	6	80
9109	1100 E	125 N	7152.06	8207.67	0.20	3.0	18	6	62
9109	1100 E	150 N	7143.29	8231.16	0.20	3.0	10	10	74
9109	1100 E	175 N	7134.51	8254.65	0.30	3.0	23	7	104
9109	1100 E	225 N	7116.97	8301.63	0.20	3.0	17	5	56
9109	1100 E	250 N	7108.19	8325.12	0.10	3.0	27	4	63
9109	1100 E	275 N	7099.42	8348.60	0.20	3.0	28	6	61
9109	1100 E	300 N	7090.64	8372.09	0.20	3.0	22	6	66
9109	1100 E	325 N	7081.87	8395.58	0.20	3.0	21	6	62
9109	1100 E	350 N	7073.10	8419.07	0.20	3.0	23	6	70
9109	1100 E	375 N	7064.32	8442.56	0.10	3.0	20	6	72
9109	1100 E	400 N	7055.55	8466.05	0.10	3.0	17	6	81
9109	1100 E	425 N	7046.78	8489.53	0.10	3.0	18	5	53
9109	1100 E	450 N	7038.00	8513.02	0.10	3.0	17	4	65
9109	1100 E	475 N	7029.23	8536.51	0.10	3.0	16	5	90
9109	1100 E	500 N	7020.45	8560.00	0.10	3.0	16	5	80
9109	1100 E	525 N	7011.68	8583.49	0.10	3.0	13	6	66

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9109	1100 E	550 N	7002.91	8606.98	0.10	3.0	20	5	70
9109	1100 E	575 N	6994.13	8630.46	0.10	3.0	20	4	66
9109	1100 E	600 N	6985.36	8653.95	0.10	3.0	16	4	67
9109	1100 E	625 N	6976.59	8677.44	0.20	3.0	24	7	52
9109	1100 E	650 N	6967.81	8700.93	0.10	3.0	18	5	84
9109	1100 E	675 N	6959.04	8724.42	0.10	3.0	26	4	72
9109	1100 E	700 N	6950.26	8747.91	0.10	3.0	28	4	66
9109	1100 E	725 N	6941.49	8771.40	0.10	3.0	21	5	76
9109	1100 E	750 N	6932.72	8794.88	0.10	3.0	20	5	70
9109	1100 E	775 N	6923.94	8818.37	0.10	3.0	26	4	65
9109	1100 E	800 N	6915.17	8841.86	0.10	3.0	27	6	70
9099	1100 E	825 N	6906.40	8865.35	0.10	3.0	20	5	58
9099	1100 E	850 N	6897.62	8888.84	0.10	3.0	24	5	50
9099	1100 E	875 N	6888.85	8912.33	0.10	3.0	25	4	58
9099	1100 E	900 N	6880.07	8935.82	0.10	3.0	31	5	52
9099	1100 E	925 N	6871.30	8959.30	0.10	3.0	38	4	62
9099	1100 E	950 N	6862.53	8982.79	0.10	3.0	34	5	57
9099	1100 E	975 N	6853.75	9006.28	0.10	3.0	35	5	41
9108	1100 E	100 S	7231.03	7996.28	0.10	3.0	18	5	66
9108	1100 E	125 S	7239.80	7972.79	0.10	3.0	25	5	53
9108	1100 E	150 S	7248.57	7949.30	0.10	3.0	23	5	62
9108	1100 E	175 S	7257.35	7925.81	0.10	3.0	24	7	46
9108	1100 E	200 S	7266.12	7902.32	0.10	3.0	17	5	56
9108	1100 E	225 S	7274.89	7878.83	0.10	3.0	13	8	88
9108	1100 E	250 S	7283.67	7855.35	0.10	3.0	18	8	110
9108	1100 E	275 S	7292.44	7831.86	0.10	3.0	11	4	75
9108	1100 E	310 S	7304.73	7798.97	0.10	3.0	8	4	82
9108	1100 E	325 S	7309.99	7784.88	0.10	3.0	11	5	76
9108	1100 E	350 S	7318.76	7761.39	0.10	3.0	17	4	70
9108	1100 E	375 S	7327.54	7737.90	0.10	3.0	7	5	38
9108	1100 E	400 S	7336.31	7714.41	0.10	3.0	11	8	55
9108	1100 E	425 S	7345.08	7690.93	0.10	3.0	23	6	47
9108	1100 E	450 S	7353.86	7667.44	0.10	3.0	23	4	48
9108	1100 E	475 S	7362.63	7643.95	0.10	3.0	16	5	62
9108	1100 E	500 S	7371.41	7620.46	0.10	3.0	17	8	97
9156	1100 E	850 S	7494.24	7291.62	0.10	10.0	16	5	56
9156	1100 E	875 S	7503.01	7268.13	0.10	15.0	8	5	75
9156	1100 E	900 S	7511.79	7244.64	0.30	5.0	14	6	58
9156	1100 E	925 S	7520.56	7221.16	0.10	10.0	10	4	35
9156	1100 E	950 S	7529.33	7197.67	0.10	5.0	16	5	63
9156	1100 E	975 S	7538.11	7174.18	0.10	15.0	13	5	69
9099	1100 E	1000 N	6844.98	9029.77	0.10	3.0	37	5	46
9099	1100 E	1025 N	6836.20	9053.26	0.10	3.0	22	5	47
9099	1100 E	1075 N	6818.66	9100.23	0.10	3.0	22	5	46
9099	1100 E	1100 N	6809.88	9123.72	0.10	3.0	30	7	43
9099	1100 E	1125 N	6801.11	9147.21	0.10	3.0	21	6	40
9099	1100 E	1150 N	6792.34	9170.70	0.10	3.0	48	6	40
9099	1100 E	1175 N	6783.56	9194.19	0.10	3.0	34	6	38

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9099	1100 E	1200 N	6774.79	9217.68	0.10	3.0	44	6	47
9099	1100 E	1225 N	6766.01	9241.17	0.10	3.0	47	7	46
9099	1100 E	1250 N	6757.24	9264.65	0.10	3.0	25	6	38
9099	1100 E	1275 N	6748.47	9288.14	0.10	3.0	33	5	43
9099	1100 E	1300 N	6739.69	9311.63	0.10	3.0	34	8	52
9099	1100 E	1325 N	6730.92	9335.12	0.10	3.0	27	6	61
9099	1100 E	1350 N	6722.15	9358.61	0.10	3.0	26	6	52
9099	1100 E	1375 N	6713.37	9382.10	0.10	3.0	28	6	44
9099	1100 E	1400 N	6704.60	9405.58	0.10	3.0	38	5	40
9099	1100 E	1425 N	6695.82	9429.07	0.10	3.0	33	5	44
9099	1100 E	1450 N	6687.05	9452.56	0.10	3.0	31	6	40
9099	1100 E	1475 N	6678.28	9476.05	0.10	3.0	30	6	45
9099	1100 E	1500 N	6669.50	9499.54	0.10	3.0	30	5	40
9099	1100 E	1525 N	6660.73	9523.03	0.10	3.0	333	5	40
9099	1100 E	1550 N	6651.96	9546.52	0.10	3.0	30	6	39
9099	1100 E	1575 N	6643.18	9570.00	0.10	3.0	20	6	24
9099	1100 E	1600 N	6634.41	9593.49	0.10	3.0	33	7	35
9156	1100 E	1000 S	7546.88	7150.69	0.10	15.0	13	5	73
9156	1100 E	1025 S	7555.66	7127.20	0.10	10.0	18	4	51
9156	1100 E	1050 S	7564.43	7103.71	0.50	10.0	49	10	69
9123	1200 E	1550 N	6745.90	9571.04	0.10	10.0	27	7	57
9123	1200 E	1600 N	6724.75	9615.69	0.10	3.0	11	5	45
9123	1200 E	1650 N	6703.59	9660.33	0.10	3.0	9	5	25
9123	1200 E	1700 N	6682.44	9704.98	0.10	3.0	13	4	31
9123	1200 E	1750 N	6661.28	9749.63	0.10	3.0	27	3	42
9123	1200 E	1800 N	6640.12	9794.27	0.10	3.0	27	3	40
9123	1200 E	1850 N	6618.97	9838.92	0.10	10.0	24	4	45
9123	1200 E	1900 N	6597.81	9883.56	0.10	3.0	31	4	42
9123	1200 E	1950 N	6576.66	9928.21	0.10	3.0	18	3	34
9123	1200 E	2000 N	6555.50	9972.85	0.10	3.0	23	4	45
9123	1200 E	2050 N	6534.34	10017.50	0.10	3.0	18	4	33
9123	1200 E	2100 N	6513.19	10062.14	0.10	3.0	17	5	27
9123	1200 E	2150 N	6492.03	10106.79	0.10	3.0	16	5	38
9123	1200 E	2200 N	6470.88	10151.43	0.10	3.0	12	4	28
9123	1200 E	2250 N	6449.72	10196.08	0.10	3.0	15	5	27
9123	1200 E	2305 N	6426.45	10245.18	0.10	3.0	9	3	16
9123	1200 E	2350 N	6407.41	10285.37	0.10	3.0	14	5	46
9123	1200 E	2600 N	6369.08	10532.73	0.10	3.0	16	4	31
9123	1200 E	2650 N	6352.28	10579.43	0.10	3.0	10	4	30
9123	1200 E	2700 N	6335.51	10626.02	0.10	3.0	16	4	29
9123	1200 E	2750 N	6318.74	10672.60	0.10	3.0	36	7	31
9123	1200 E	2800 N	6301.97	10719.18	0.10	3.0	30	7	36
9123	1200 E	2850 N	6285.19	10765.77	0.10	3.0	20	6	29
9123	1200 E	2900 N	6268.42	10812.35	0.10	3.0	16	4	50
9123	1200 E	2950 N	6251.65	10858.93	0.10	3.0	14	4	31
9123	1200 E	3000 N	6234.88	10905.52	0.10	5.0	19	4	32
9123	1200 E	3050 N	6218.11	10952.10	0.10	5.0	15	4	30
9123	1200 E	3100 N	6201.33	10998.68	0.10	3.0	10	3	22

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9123	1200 E	3150 N	6184.56	11045.27	0.10	10.0	15	4	26
9123	1200 E	3200 N	6167.79	11091.85	0.10	3.0	10	3	22
9109	1300 E	275 N	7285.92	8417.97	0.10	10.0	28	6	63
9109	1300 E	300 N	7277.29	8441.47	0.20	3.0	40	8	55
9109	1300 E	325 N	7268.67	8464.97	0.10	3.0	60	5	62
9109	1300 E	350 N	7260.05	8488.47	0.20	3.0	28	5	70
9109	1300 E	375 N	7251.43	8511.97	0.10	10.0	26	5	78
9109	1300 E	400 N	7242.81	8535.46	0.30	10.0	58	8	68
9109	1300 E	425 N	7234.19	8558.96	0.10	3.0	14	9	53
9109	1300 E	450 N	7225.57	8582.46	0.10	3.0	24	7	67
9109	1300 E	475 N	7216.95	8605.96	0.10	3.0	15	5	71
9109	1300 E	500 N	7208.33	8629.46	0.20	3.0	31	7	73
9109	1300 E	525 N	7199.71	8652.95	0.10	3.0	18	6	48
9109	1300 E	550 N	7191.09	8676.45	0.10	3.0	16	6	70
9109	1300 E	575 N	7182.47	8699.95	0.20	3.0	17	6	53
9109	1300 E	600 N	7173.85	8723.45	0.30	3.0	72	8	64
9109	1300 E	625 N	7165.23	8746.94	0.20	3.0	32	5	54
9109	1300 E	650 N	7156.61	8770.44	0.10	3.0	44	5	83
9109	1300 E	675 N	7147.99	8793.94	0.10	3.0	22	6	74
9109	1300 E	700 N	7139.37	8817.44	0.10	3.0	25	4	76
9109	1300 E	725 N	7130.75	8840.93	0.20	3.0	14	6	64
9109	1300 E	750 N	7122.13	8864.43	99999.00	3.0	99999	9 9999	99999
9109	1300 E	775 N	7113.51	8887.93	0.20	3.0	45	6	64
9109	1300 E	800 N	7104.89	8911.43	0.20	3.0	47	7	62
9109	1300 E	825 N	7096.27	8934.93	0.20	3.0	53	6	58
9109	1300 E	850 N	7087.64	8958.42	0.20	3.0	100	6	53
9109	1300 E	875 N	7079.02	8981.92	0.20	3.0	58	6	58
9109	1300 E	900 N	7070.40	9005.42	0.20	3.0	50	8	60
9109	1300 E	925 N	7061.78	9028.92	0.10	3.0	63	6	70
9109	1300 E	950 N	7053.16	9052.41	0.10	3.0	44	5	62
9109	1300 E	1000 N	7035.92	9099.41	0.10	3.0	50	6	53
9156	1300 E	850 S	7673.84	7360.58	0.10	3.0	11	5	50
9156	1300 E	875 S	7682.46	7337.08	0.10	3.0	21	4	55
9156	1300 E	900 S	7691.08	7313.58	0.10	3.0	14	4	53
9156	1300 E	925 S	7699.70	7290.08	0.10	10.0	21	4	33
9156	1300 E	950 S	7708.32	7266.59	0.20	3.0	10	4	43
9156	1300 E	975 S	7716.94	7243.09	0.20	3.0	11	5	68
9156	1300 E	1000 S	7725.56	7219.59	0.10	10.0	11	6	60
9156	1300 E	1025 S	7734.18	7196.09	0.10	3.0	18	4	43
9156	1300 E	1050 S	7742.80	7172.60	0.20	3.0	13	6	38
9109	1350 E	200 N	7359.76	8364.42	0.10	3.0	17	15	92
9109	1350 E	225 N	7351.16	8387.83	0.40	3.0	115	30	114
9109	1350 E	250 N	7342.57	8411.24	0.10	3.0	20	20	95
9109	1350 E	275 N	7333.97	8434.65	0.10	3.0	37	18	90
9109	1350 E	300 N	7325.38	8458.07	0.10	3.0	16	12	61
9109	1350 E	325 N	7316.78	8481.48	0.10	3.0	49	5	71
9109	1350 E	350 N	7308.19	8504.89	0.20	3.0	27	6	59
9109	1350 E	375 N	7299.59	8528.30	0.10	3.0	32	5	80

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9109	1350 E	400 N	7291.00	8551.71	0.20	3.0	309	7	44
9109	1350 E	425 N	7282.40	8575.12	0.10	3.0	22	5	68
9109	1350 E	450 N	7273.80	8598.54	0.20	3.0	25	6	81
9109	1350 E	475 N	7265.21	8621.95	0.20	3.0	33	7	92
9109	1350 E	500 N	7256.61	8645.36	0.10	3.0	24	7	122
9109	1350 E	525 N	7248.02	8668.77	0.20	3.0	18	10	120
9109	1350 E	550 N	7239.42	8692.18	0.20	3.0	18	6	74
9109	1350 E	575 N	7230.83	8715.59	0.10	3.0	22	6	45
9109	1350 E	600 N	7222.23	8739.00	0.10	3.0	15	6	70
9109	1350 E	625 N	7213.63	8762.42	0.10	3.0	21	7	94
9109	1350 E	650 N	7205.04	8785.83	0.20	3.0	19	5	98
9109	1350 E	675 N	7196.44	8809.24	0.10	3.0	20	6	125
9109	1350 E	700 N	7187.85	8832.65	0.10	3.0	21	7	130
9109	1350 E	725 N	7179.25	8856.06	0.10	3.0	22	6	73
9109	1350 E	750 N	7170.66	8879.47	0.10	3.0	26	5	77
9109	1350 E	775 N	7162.06	8902.89	0.10	3.0	30	5	72
9109	1350 E	800 N	7153.46	8926.30	0.10	3.0	24	4	82
9109	1350 E	825 N	7144.87	8949.71	0.10	3.0	27	5	61
9109	1350 E	850 N	7136.27	8973.12	0.10	3.0	25	5	52
9109	1350 E	875 N	7127.68	8996.53	0.20	3.0	32	5	52
9109	1350 E	900 N	7119.08	9019.94	0.10	5.0	32	4	58
9109	1350 E	925 N	7110.49	9043.36	0.10	3.0	31	6	47
9109	1350 E	950 N	7101.89	9066.77	0.20	3.0	45	5	58
9109	1350 E	975 N	7093.30	9090.18	0.10	3.0	45	4	51
9109	1350 E	1000 N	7084.70	9113.59	0.40	3.0	94	11	71
9109	1400 E	500 N	7292.22	8660.48	0.10	3.0	24	5	50
9109	1400 E	550 N	7274.84	8706.88	0.20	3.0	24	4	62
9109	1400 E	575 N	7266.16	8730.08	0.30	3.0	25	7	110
9109	1400 E	600 N	7257.47	8753.28	0.20	3.0	20	7	108
9109	1400 E	625 N	7248.78	8776.48	0.10	5.0	25	8	103
9109	1400 E	650 N	7240.09	8799.69	0.10	3.0	21	5	60
9109	1400 E	675 N	7231.40	8822.89	0.10	3.0	22	4	76
9109	1400 E	700 N	7222.71	8846.09	0.10	3.0	17	5	104
9109	1400 E	725 N	7214.03	8869.29	0.20	3.0	21	4	82
9109	1400 E	750 N	7205.34	8892.49	0.10	3.0	21	4	66
9109	1400 E	775 N	7196.65	8915.69	0.10	3.0	21	4	72
9109	1400 E	800 N	7187.96	8938.89	0.10	3.0	24	5	87
9109	1400 E	825 N	7179.27	8962.09	0.10	3.0	25	5	107
9109	1400 E	850 N	7170.58	8985.29	0.10	3.0	38	5	74
9109	1400 E	900 N	7153.21	9031.69	0.30	3.0	116	9	54
9109	1400 E	925 N	7144.52	9054.89	0.40	3.0	83	9	66
9109	1400 E	950 N	7135.83	9078.09	0.40	3.0	78	10	71
9109	1400 E	975 N	7127.14	9101.30	0.50	3.0	74	11	62
9109	1400 E	1000 N	7118.45	9124.50	0.30	3.0	100	10	74
9109	1400 E	1025 N	7109.77	9147.70	0.10	3.0	20	4	60
9109	1400 E	1050 N	7101.08	9170.90	0.10	3.0	17	5	59
9109	1400 E	1075 N	7092.39	9194.10	0.10	3.0	16	5	58
9109	1400 E	1100 N	7083.70	9217.30	0.10	3.0	12	6	43

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9123	1400 E	1550 N	6933.37	9641.97	0.10	3.0	15	3	40
9123	1400 E	1600 N	6913.59	9687.02	0.10	3.0	20	5	39
9123	1400 E	1650 N	6893.81	9732.06	0.10	3.0	22	4	47
9123	1400 E	1700 N	6874.04	9777.11	0.10	3.0	23	4	54
9123	1400 E	1750 N	6854.27	9822.15	0.10	3.0	19	3	54
9123	1400 E	1800 N	6834.49	9867.20	0.10	3.0	22	5	43
9123	1400 E	1850 N	6814.71	9912.25	0.10	3.0	26	3	47
9123	1400 E	1900 N	6794.94	9957.29	0.10	3.0	26	3	36
9123	1400 E	1950 N	6775.17	10002.33	0.10	3.0	13	4	33
9123	1400 E	2000 N	6755.39	10047.38	0.10	3.0	10	5	35
9123	1400 E	2050 N	6735.62	10092.42	0.10	3.0	10	3	36
9123	1400 E	2100 N	6715.84	10137.47	0.10	3.0	38	5	25
9123	1400 E	2150 N	6696.06	10182.51	0.10	3.0	42	6	30
9123	1400 E	2200 N	6676.29	10227.56	0.10	3.0	43	6	29
9123	1400 E	2250 N	6656.52	10272.60	0.10	3.0	9	3	29
9123	1400 E	2300 N	6636.74	10317.65	0.10	3.0	20	3	31
9123	1400 E	2350 N	6616.96	10362.70	0.10	10.0	28	5	33
9123	1400 E	2400 N	6597.19	10407.74	0.10	3.0	11	4	33
9123	1400 E	2450 N	6577.42	10452.79	0.20	5.0	48	6	34
9123	1400 E	2500 N	6557.64	10497.83	0.10	5.0	30	4	34
9123	1400 E	2550 N	6537.86	10542.88	0.10	3.0	20	6	30
9123	1400 E	2590 N	6522.04	10578.91	0.10	3.0	12	5	26
9123	1400 E	2600 N	6555.09	10601.12	0.10	3.0	8	3	22
9123	1400 E	2650 N	6537.77	10648.50	0.10	3.0	17	4	38
9123	1400 E	2700 N	6520.41	10696.18	0.10	3.0	6	4	21
9123	1400 E	2750 N	6503.04	10743.86	0.10	3.0	8	2	18
9123	1400 E	2815 N	6480.46	10805.84	0.10	3.0	12	5	37
9123	1400 E	2850 N	6468.31	10839.21	0.10	3.0	12	5	42
9123	1400 E	2900 N	6450.94	10886.89	0.10	3.0	10	3	28
9123	1400 E	2950 N	6433.58	10934.57	0.10	3.0	12	4	30
9123	1400 E	3000 N	6416.21	10982.25	0.10	5.0	10	4	38
9123	1400 E	3050 N	6398.85	11029.92	0.10	10.0	13	4	31
9123	1400 E	3110 N	6381.48	11077.60	0.10	3.0	21	15	30
9109	1450 E	200 N	7452.17	8402.22	0.10	3.0	16	19	106
9109	1450 E	225 N	7443.53	8425.55	0.10	3.0	12	13	75
9109	1450 E	250 N	7434.90	8448.88	0.10	3.0	25	5	56
9109	1450 E	275 N	7426.26	8472.22	0.10	3.0	19	4	64
9109	1450 E	300 N	7417.63	8495.55	0.10	3.0	24	6	67
9109	1450 E	325 N	7408.99	8518.88	0.10	3.0	25	6	55
9109	1450 E	350 N	7400.36	8542.21	0.20	3.0	37	6	48
9109	1450 E	375 N	7391.72	8565.55	0.30	3.0	184	5	61
9109	1450 E	400 N	7383.09	8588.88	0.10	3.0	26	5	68
9109	1450 E	425 N	7374.45	8612.21	0.40	3.0	49	10	120
9109	1450 E	450 N	7365.82	8635.54	0.30	3.0	35	9	110
9109	1450 E	475 N	7357.18	8658.88	0.10	3.0	14	5	82
9109	1450 E	500 N	7348.55	8682.21	0.10	3.0	16	6	89
9109	1450 E	525 N	7339.91	8705.54	0.10	3.0	13	9	108
9109	1450 E	550 N	7331.28	8728.88	0.10	3.0	12	7	83

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9109	1450 E	575 N	7322.64	8752.21	0.10	3.0	14	6	115
9109	1450 E	600 N	7314.00	8775.54	0.10	3.0	16	6	78
9109	1450 E	625 N	7305.37	8798.87	0.10	3.0	16	5	68
9109	1450 E	650 N	7296.73	8822.21	0.10	3.0	15	6	70
9109	1450 E	675 N	7288.10	8845.54	0.10	3.0	23	5	73
9109	1450 E	700 N	7279.46	8868.87	0.10	3.0	18	5	95
9109	1450 E	725 N	7270.83	8892.20	0.10	3.0	18	4	80
9109	1450 E	750 N	7262.19	8915.54	0.10	3.0	20	4	105
9109	1450 E	775 N	7253.56	8938.87	0.10	3.0	21	6	127
9109	1450 E	800 N	7244.92	8962.20	0.10	3.0	18	6	138
9109	1450 E	825 N	7236.29	8985.53	0.10	3.0	38	7	47
9109	1450 E	850 N	7227.65	9008.87	0.20	3.0	127	9	44
9109	1450 E	875 N	7219.02	9032.20	0.70	3.0	150	10	60
9109	1450 E	900 N	7210.38	9055.53	0.40	3.0	57	8	57
9109	1450 E	925 N	7201.75	9078.86	0.30	3.0	45	8	109
9109	1450 E	950 N	7193.11	9102.20	0.10	3.0	14	6	110
9109	1450 E	975 N	7184.48	9125.53	0.10	3.0	13	24	345
9109	1450 E	1000 N	7175.84	9148.86	0.20	3.0	13	6	80
9109	1500 E	200 N	7498.19	8418.13	0.20	3.0	21	23	124
9109	1500 E	225 N	7489.46	8441.48	0.30	3.0	29	13	88
9109	1500 E	250 N	7480.72	8464.83	0.20	3.0	22	6	54
9109	1500 E	275 N	7471.99	8488.19	0.10	3.0	27	4	60
9109	1500 E	300 N	7463.25	8511.54	0.10	3.0	57	5	53
9109	1500 E	325 N	7454.52	8534.90	0.10	3.0	30	5	42
9109	1500 E	350 N	7445.78	8558.25	0.10	3.0	60	6	45
9109	1500 E	375 N	7437.04	8581.60	0.20	3.0	37	6	48
9109	1500 E	400 N	7428.31	8604.96	0.20	3.0	74	7	67
9109	1500 E	425 N	7419.57	8628.31	0.10	3.0	36	7	56
9109	1500 E	450 N	7410.84	8651.67	0.20	3.0	37	8	76
9109	1500 E	475 N	7402.10	8675.02	0.10	3.0	40	8	88
9109	1500 E	500 N	7393.37	8698.38	0.10	3.0	18	6	68
9109	1500 E	525 N	7384.63	8721.73	0.10	3.0	17	6	84
9109	1500 E	550 N	7375.90	8745.08	0.10	3.0	15	8	74
9109	1500 E	575 N	7367.16	8768.44	0.10	3.0	17	9	110
9109	1500 E	600 N	7358.42	8791.79	0.10	3.0	20	7	105
9109	1500 E	625 N	7349.69	8815.15	0.10	3.0	19	7	91
9109	1500 E	650 N	7340.95	8838.50	0.10	3.0	21	10	84
9109	1500 E	675 N	7332.22	8861.86	0.10	3.0	22	7	54
9109	1500 E	700 N	7323.48	8885.21	0.10	3.0	15	6	88
9109	1500 E	725 N	7314.75	8908.57	0.10	3.0	16	4	57
9109	1500 E	750 N	7306.01	8931.92	0.10	3.0	20	5	86
9109	1500 E	775 N	7297.27	8955.27	0.10	3.0	23	5	86
9109	1500 E	800 N	7288.54	8978.63	0.20	3.0	19	6	162
9109	1500 E	825 N	7279.80	9001.98	0.10	3.0	13	7	230
9109	1500 E	850 N	7271.07	9025.34	0.20	3.0	12	12	83
9109	1500 E	875 N	7262.33	9048.69	0.10	3.0	40	7	44
9109	1500 E	925 N	7244.86	9095.40	0.10	3.0	30	7	33
9109	1500 E	950 N	7236.12	9118.75	0.20	3.0	40	8	38

Continued....



Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	1500 E	300 S	7672.91	7951.04	0.10	3.0	21	6	65
9108	1500 E	325 S	7681.64	7927.68	0.10	3.0	20	5	52
9108	1500 E	350 S	7690.38	7904.33	0.10	3.0	15	5	41
9108	1500 E	375 S	7699.12	7880.98	0.10	3.0	20	4	51
9108	1500 E	400 S	7707.85	7857.62	0.10	3.0	16	5	37
9108	1500 E	425 S	7716.59	7834.27	0.10	3.0	22	5	35
9108	1500 E	450 S	7725.32	7810.91	0.10	3.0	20	4	32
9108	1500 E	525 S	7751.53	7740.85	0.10	3.0	14	5	41
9108	1500 E	550 S	7760.27	7717.50	0.10	3.0	21	5	41
9108	1500 E	575 S	7769.00	7694.14	0.10	3.0	19	5	55
9108	1500 E	600 S	7777.74	7670.79	0.10	3.0	15	7	106
9108	1500 E	625 S	7786.47	7647.43	0.10	3.0	7	7	96
9108	1500 E	650 S	7795.21	7624.08	0.10	3.0	15	10	106
9108	1500 E	675 S	7803.94	7600.72	0.10	3.0	10	8	178
9109	1500 E	1000 N	7218.65	9165.46	0.10	3.0	18	8	104
9123	1600 E	1550 N	7120.98	9712.43	0.10	3.0	14	4	31
9123	1600 E	1600 N	7099.57	9756.82	0.10	10.0	13	5	36
9123	1600 E	1650 N	7078.15	9801.21	0.10	10.0	13	5	40
9123	1600 E	1700 N	7056.73	9845.60	0.10	3.0	48	8	51
9123	1600 E	1750 N	7035.32	9889.99	0.10	3.0	14	4	32
9123	1600 E	1800 N	7013.90	9934.38	0.10	5.0	12	4	34
9123	1600 E	1850 N	6992.49	9978.77	0.10	3.0	10	4	32
9123	1600 E	1900 N	6971.07	10023.16	0.10	3.0	10	5	18
9123	1600 E	2005 N	6926.10	10116.37	0.10	3.0	15	3	29
9123	1600 E	2050 N	6906.82	10156.32	0.10	3.0	15	3	28
9123	1600 E	2100 N	6885.41	10200.71	0.10	3.0	9	2	16
9123	1600 E	2150 N	6863.99	10245.10	0.10	3.0	8	3	16
9123	1600 E	2200 N	6842.58	10289.49	0.10	3.0	13	4	32
9123	1600 E	2250 N	6821.16	10333.88	0.10	3.0	16	5	20
9123	1600 E	2300 N	6799.74	10378.27	0.10	3.0	9	3	23
9123	1600 E	2350 N	6778.33	10422.66	0.10	3.0	12	4	24
9123	1600 E	2400 N	6756.91	10467.04	0.10	3.0	12	5	41
9123	1600 E	2500 N	6714.08	10555.82	0.10	3.0	11	5	28
9123	1600 E	2550 N	6692.67	10600.21	0.10	3.0	17	4	27
9123	1600 E	2598 N	6672.11	10642.82	0.10	3.0	13	3	25
9123	1600 E	2600 N	6742.45	10670.10	0.10	10.0	11	4	33
9123	1600 E	2650 N	6725.78	10717.20	0.20	3.0	11	6	72
9123	1600 E	2700 N	6709.10	10764.30	0.20	3.0	17	6	74
9123	1600 E	2750 N	6692.43	10811.39	0.20	10.0	13	11	149
9123	1600 E	2800 N	6675.75	10858.49	0.20	10.0	13	5	104
9123	1600 E	2850 N	6659.07	10905.59	0.20	3.0	30	3	95
9123	1600 E	2900 N	6642.39	10952.69	0.20	3.0	21	4	74
9123	1600 E	2950 N	6625.71	10999.79	0.10	3.0	19	4	41
9123	1600 E	3000 N	6609.03	11046.89	0.20	3.0	18	3	32
9108	1700 E	200 S	7822.77	8113.72	0.10	3.0	19	9	60
9108	1700 E	225 S	7831.53	8090.28	0.10	3.0	18	7	77
9108	1700 E	250 S	7840.28	8066.85	0.10	3.0	14	8	143
9108	1700 E	275 S	7849.04	8043.41	0.10	3.0	13	10	71

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9108	1700 E	300 S	7857.79	8019.98	0.10	3.0	10	9	130
9108	1700 E	325 S	7866.55	7996.54	0.10	3.0	10	13	93
9108	1700 E	350 S	7875.31	7973.10	0.10	3.0	10	13	118
9108	1700 E	375 S	7884.06	7949.67	0.10	3.0	12	9	83
9108	1700 E	400 S	7892.82	7926.23	0.10	3.0	18	18	160
358- 31	1750 E	100 N	7763.28	8405.52	0.10	5.0	23	25	142
358- 32	1750 E	125 N	7755.33	8429.14	0.30	5.0	22	23	164
358- 33	1750 E	150 N	7747.38	8452.76	0.40	3.0	36	28	153
358- 34	1750 E	175 N	7739.43	8476.38	1.80	3.0	104	47	218
358- 35	1750 E	200 N	7731.48	8500.01	1.80	5.0	24	28	113
358- 36	1750 E	225 N	7723.53	8523.63	1.80	10.0	28	31	99
358- 37	1750 E	250 N	7715.58	8547.25	0.20	3.0	58	23	93
9156	1800 E	175 N	7788.16	8488.38	0.20	15.0	23	21	88
9123	1800 E	1550 N	7336.92	9789.09	0.10	3.0	13	4	42
9123	1800 E	1600 N	7313.11	9832.64	0.10	3.0	13	5	23
9123	1800 E	1650 N	7289.31	9876.20	0.10	3.0	10	5	28
9123	1800 E	1700 N	7265.51	9919.76	0.10	10.0	13	5	50
9123	1800 E	1750 N	7241.71	9963.31	0.10	10.0	10	5	46
9123	1800 E	1800 N	7217.90	10006.87	0.10	15.0	9	6	43
9123	1800 E	1850 N	7194.10	10050.43	0.10	15.0	9	5	60
9123	1800 E	1900 N	7170.30	10093.98	0.20	20.0	15	6	42
9123	1800 E	1950 N	7146.50	10137.54	0.10	10.0	15	5	32
9123	1800 E	2000 N	7122.69	10181.10	0.10	3.0	34	7	32
9123	1800 E	2050 N	7098.89	10224.66	0.10	3.0	3	3	13
9123	1800 E	2100 N	7075.09	10268.21	0.10	10.0	8	6	28
9123	1800 E	2150 N	7051.28	10311.77	0.40	3.0	42	9	33
9123	1800 E	2200 N	7027.48	10355.33	0.10	3.0	8	5	24
9123	1800 E	2250 N	7003.68	10398.88	0.10	3.0	7	6	24
9123	1800 E	2300 N	6979.88	10442.44	0.10	3.0	14	7	23
9123	1800 E	2350 N	6956.07	10486.00	0.10	3.0	14	7	25
9123	1800 E	2400 N	6932.27	10529.55	0.10	3.0	14	6	42
9123	1800 E	2450 N	6908.47	10573.11	0.10	3.0	14	7	50
9123	1800 E	2500 N	6884.67	10616.67	0.10	3.0	10	5	44
9123	1800 E	2550 N	6860.86	10660.22	0.10	3.0	13	6	68
9123	1800 E	2598 N	6838.01	10702.04	0.10	3.0	12	6	64
9123	1800 E	2600 N	6837.06	10703.78	0.10	3.0	9	8	40
9123	1800 E	2650 N	6915.94	10785.88	0.10	3.0	18	8	85
9123	1800 E	2700 N	6899.55	10832.38	0.10	3.0	12	6	58
9123	1800 E	2750 N	6883.17	10878.88	0.10	3.0	20	6	70
9123	1800 E	2800 N	6866.78	10925.38	0.20	3.0	35	8	53
9123	1800 E	2850 N	6850.39	10971.88	0.20	3.0	15	5	46
9156	1850 E	100 N	7863.26	8436.98	0.30	10.0	39	22	118
9156	1850 E	125 N	7854.47	8461.45	0.40	10.0	20	25	83
9156	1850 E	150 N	7845.68	8485.91	0.20	20.0	25	27	96
9156	1850 E	175 N	7836.89	8510.38	0.10	10.0	20	9	98
9156	1850 E	200 N	7828.10	8534.84	0.10	15.0	16	12	108
9156	1850 E	225 N	7819.31	8559.30	0.10	10.0	10	9	55
9156	1850 E	250 N	7810.52	8583.77	0.10	10.0	8	6	38

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9135	2000 E	1550 N	7494.93	9851.45	0.10	10.0	12	6	43
9135	2000 E	1600 N	7473.43	9895.63	0.10	3.0	15	7	52
9135	2000 E	1650 N	7451.92	9939.82	0.10	3.0	20	7	48
9135	2000 E	1700 N	7430.42	9984.00	0.10	3.0	12	4	32
9135	2000 E	1750 N	7408.92	10028.19	0.10	3.0	20	6	38
9135	2000 E	1800 N	7387.42	10072.37	0.10	3.0	11	7	58
9135	2000 E	1850 N	7365.92	10116.56	0.10	3.0	10	6	46
9135	2000 E	1900 N	7344.42	10160.74	0.10	3.0	12	6	54
9135	2000 E	1950 N	7322.91	10204.93	0.10	3.0	12	5	72
9135	2000 E	2000 N	7301.41	10249.11	0.10	3.0	7	7	28
9135	2000 E	2050 N	7279.91	10293.30	0.10	3.0	15	7	70
9135	2000 E	2100 N	7258.41	10337.49	0.10	3.0	14	9	88
9135	2000 E	2150 N	7236.91	10381.67	0.10	3.0	10	6	58
9135	2000 E	2200 N	7215.40	10425.86	0.10	3.0	9	3	32
9135	2000 E	2250 N	7193.90	10470.04	0.10	3.0	15	5	48
9135	2000 E	2300 N	7172.40	10514.23	0.10	3.0	25	5	76
9135	2000 E	2350 N	7150.90	10558.41	0.10	3.0	25	5	75
9135	2000 E	2600 N	7043.39	10779.34	0.10	3.0	22	5	60
9135	2000 E	2650 N	7105.03	10851.63	0.20	3.0	28	8	48
9135	2000 E	2710 N	7085.97	10904.69	0.40	3.0	67	8	65
9135	2000 E	2750 N	7073.26	10940.07	0.10	3.0	33	7	50
9135	2000 E	2800 N	7057.38	10984.28	0.10	3.0	22	7	64
9148	2200 E	300 N	8181.48	8752.66	0.20	35.0	21	7	55
9148	2200 E	345 N	8165.23	8796.51	0.20	15.0	33	12	102
9148	2200 E	400 N	8145.37	8850.10	0.10	10.0	11	6	60
9148	2200 E	450 N	8127.31	8898.83	0.10	10.0	8	6	54
9148	2200 E	500 N	8109.26	8947.55	0.10	15.0	8	5	27
9148	2200 E	550 N	8091.20	8996.27	0.10	10.0	6	6	36
9148	2200 E	600 N	8073.15	9044.99	0.10	3.0	5	5	27
9148	2200 E	650 N	8055.09	9093.71	0.10	3.0	9	6	18
9148	2200 E	700 N	8037.03	9142.43	0.10	3.0	6	5	39
9148	2200 E	800 N	8000.92	9239.88	0.10	3.0	8	6	45
9148	2200 E	850 N	7982.87	9288.60	0.10	3.0	5	5	25
9148	2200 E	900 N	7964.81	9337.32	0.30	3.0	64	9	56
9148	2200 E	945 N	7948.56	9381.17	0.10	3.0	8	8	58
9148	2200 E	1000 N	7928.70	9434.76	0.10	3.0	5	5	43
9148	2200 E	1050 N	7910.64	9483.49	0.10	3.0	15	5	35
9148	2200 E	1095 N	7894.39	9527.33	0.20	3.0	8	8	51
9148	2200 E	1150 N	7874.53	9580.93	0.10	10.0	7	5	32
9148	2200 E	1200 N	7856.48	9629.65	0.20	3.0	4	6	55
9148	2200 E	1250 N	7838.42	9678.37	0.10	3.0	7	5	30
9148	2200 E	1300 N	7820.36	9727.09	0.10	3.0	6	4	28
9148	2200 E	1350 N	7802.31	9775.82	0.10	3.0	9	4	37
9148	2200 E	1400 N	7784.25	9824.54	0.10	3.0	9	6	42
9148	2200 E	1450 N	7766.20	9873.26	0.10	3.0	7	5	46
9148	2200 E	1500 N	7748.14	9921.98	0.20	3.0	25	8	31
9148	2200 E	1550 N	7728.25	9965.36	0.10	3.0	9	5	42
9148	2200 E	1600 N	7708.35	10008.74	0.10	15.0	9	5	40

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9148	2200 E	1650 N	7688.46	10052.12	0.10	10.0	10	6	45
9148	2200 E	1700 N	7668.56	10095.49	0.10	15.0	6	4	40
9148	2200 E	1750 N	7648.67	10138.87	0.10	3.0	10	4	30
9148	2200 E	1800 N	7628.78	10182.25	0.10	3.0	6	5	22
9148	2200 E	1850 N	7608.88	10225.63	0.20	3.0	53	8	51
9148	2200 E	1900 N	7588.99	10269.01	0.20	3.0	15	6	35
9148	2200 E	1950 N	7569.09	10312.38	0.20	3.0	12	6	46
9148	2200 E	2000 N	7549.20	10355.76	0.10	10.0	11	11	50
9148	2200 E	2050 N	7529.31	10399.14	0.10	10.0	15	4	24
9148	2200 E	2100 N	7509.41	10442.52	0.10	3.0	19	5	50
9148	2200 E	2150 N	7489.52	10485.90	0.10	20.0	14	7	40
9148	2200 E	2200 N	7469.62	10529.27	0.10	3.0	16	5	23
9148	2200 E	2250 N	7449.73	10572.65	0.10	15.0	20	5	35
9148	2200 E	2300 N	7429.83	10616.03	0.10	40.0	22	6	34
9148	2200 E	2350 N	7409.94	10659.41	0.10	10.0	24	6	30
9148	2200 E	2400 N	7390.05	10702.79	0.10	10.0	36	6	27
9148	2200 E	2450 N	7370.15	10746.17	0.10	3.0	32	6	44
9148	2200 E	2500 N	7350.26	10789.54	0.10	3.0	37	6	42
9148	2200 E	2550 N	7330.36	10832.92	0.10	10.0	11	5	40
9148	2200 E	2600 N	7310.47	10876.30	0.10	15.0	15	6	87
9148	2200 E	2650 N	7292.25	10921.23	0.10	3.0	17	5	55
9148	2363 E	1550 N	7807.24	9993.57	0.10	10.0	10	5	34
9148	2363 E	1650 N	7763.43	10078.84	0.10	10.0	9	7	50
9148	2363 E	1700 N	7741.52	10121.48	0.10	15.0	16	9	55
9148	2363 E	1750 N	7719.61	10164.11	0.10	20.0	16	8	52
9148	2363 E	1800 N	7697.70	10206.75	0.10	3.0	29	8	54
9148	2363 E	1850 N	7675.79	10249.38	0.10	3.0	23	7	43
9148	2363 E	1900 N	7653.88	10292.01	0.20	3.0	55	12	49
9148	2363 E	1950 N	7631.98	10334.65	0.10	3.0	30	9	57
9148	2363 E	2000 N	7610.07	10377.28	0.10	3.0	24	8	52
9148	2363 E	2050 N	7588.16	10419.92	0.10	3.0	14	6	71
9148	2363 E	2100 N	7566.25	10462.55	0.10	3.0	8	4	30
9148	2363 E	2150 N	7544.34	10505.18	0.10	3.0	17	2	35
9148	2363 E	2200 N	7522.44	10547.82	0.10	3.0	24	6	44
9148	2363 E	2250 N	7500.53	10590.45	0.10	3.0	50	4	58
9148	2363 E	2300 N	7478.62	10633.08	0.10	3.0	20	9	36
9148	2363 E	2350 N	7456.71	10675.72	0.10	3.0	27	5	43
9148	2363 E	2400 N	7434.80	10718.35	0.10	20.0	31	5	61
9148	2363 E	2450 N	7412.89	10760.99	0.10	3.0	15	5	36
9148	2363 E	2500 N	7390.99	10803.62	0.10	3.0	14	5	52
9148	2363 E	2523 N	7380.91	10823.23	0.10	3.0	21	5	67
9156	2500 E	250 S	8601.35	8374.09	0.10	10.0	7	9	48
9156	2500 E	275 S	8611.87	8351.89	0.10	3.0	8	8	53
9156	2500 E	300 S	8622.38	8329.69	0.20	10.0	10	7	60
9156	2500 E	325 S	8632.89	8307.49	0.20	15.0	11	12	76
9156	2500 E	350 S	8643.41	8285.29	0.20	10.0	11	10	77
9148	2568 E	1550 N	7989.05	10058.54	0.10	3.0	10	6	58
9148	2568 E	1600 N	7969.22	10101.92	0.10	3.0	10	7	90

Continued....

Lab Proj.	Field Line	Grid Station	UIM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9148	2568 E	1650 N	7949.38	10145.29	0.20	5.0	8	4	60
9148	2568 E	1700 N	7929.54	10188.67	0.20	3.0	12	5	64
9148	2568 E	1750 N	7909.71	10232.05	0.10	3.0	15	4	67
9148	2568 E	1810 N	7885.90	10284.10	0.10	10.0	11	4	71
9148	2568 E	1850 N	7870.03	10318.81	0.10	3.0	13	4	63
9148	2568 E	1900 N	7850.20	10362.19	0.10	3.0	13	4	74
9148	2568 E	1950 N	7830.36	10405.56	0.20	7.0	12	4	63
9148	2568 E	2000 N	7810.52	10448.94	0.10	3.0	24	6	38
9148	2568 E	2050 N	7790.69	10492.32	0.10	3.0	19	4	44
9148	2568 E	2100 N	7770.85	10535.70	0.10	3.0	15	4	47
9148	2568 E	2150 N	7751.01	10579.08	0.10	3.0	28	5	62
9148	2568 E	2200 N	7731.17	10622.46	0.10	3.0	22	4	70
9148	2568 E	2250 N	7711.34	10665.83	0.20	3.0	14	7	51
9148	2568 E	2300 N	7691.50	10709.21	0.10	3.0	21	4	48
9148	2568 E	2350 N	7671.66	10752.59	0.10	3.0	12	4	40
9148	2568 E	2400 N	7651.83	10795.97	0.20	3.0	21	5	43
9148	2568 E	2450 N	7631.99	10839.35	0.20	3.0	19	5	56
9148	2568 E	2500 N	7612.15	10882.72	0.10	3.0	16	4	43
9148	2568 E	2550 N	7592.32	10926.10	0.10	3.0	17	5	40
9148	2568 E	2579 N	7580.81	10951.26	0.10	3.0	22	5	42
9156	2600 E	275 S	8704.35	8391.84	0.10	15.0	11	8	51
9156	2692 E	18 N	8658.74	8697.92	0.10	10.0	8	11	51
9156	2692 E	25 N	8656.27	8704.06	0.10	20.0	8	13	81
9156	2692 E	50 N	8647.45	8726.01	0.10	10.0	8	17	111
9156	2692 E	75 N	8638.63	8747.95	0.10	3.0	12	19	120
9156	2692 E	100 N	8629.82	8769.89	0.20	10.0	15	10	108
9156	2692 E	125 N	8621.00	8791.84	0.10	10.0	10	10	94
9156	2692 E	150 N	8612.18	8813.78	0.10	3.0	10	51	120
9156	2692 E	175 N	8603.36	8835.72	0.10	15.0	10	37	113
9156	2692 E	200 N	8594.54	8857.67	0.40	15.0	23	54	141
9156	2692 E	225 N	8585.72	8879.61	0.20	10.0	14	40	110
9156	2692 E	250 N	8576.90	8901.56	0.20	10.0	20	50	143
9156	2692 E	275 N	8568.09	8923.50	0.20	20.0	22	41	120
9156	2692 E	300 N	8559.27	8945.44	0.20	30.0	20	30	97
9156	2692 E	325 N	8550.45	8967.39	0.60	25.0	20	37	237
9156	2692 E	350 N	8541.63	8989.33	0.30	30.0	17	40	240
9156	2700 E	250 S	8788.02	8454.56	0.10	30.0	8	10	49
9156	2700 E	275 S	8797.84	8432.47	0.10	25.0	13	10	61
9156	2700 E	300 S	8807.65	8410.38	0.10	25.0	12	9	65
9156	2700 E	325 S	8817.47	8388.28	0.10	15.0	8	7	46
9156	2700 E	350 S	8827.29	8366.19	0.10	3.0	8	7	37
9156	2892 E	00 N	8855.53	8734.54	0.10	3.0	10	27	102
9156	2892 E	25 N	8846.29	8757.77	0.20	15.0	8	14	98
9156	2892 E	50 N	8837.06	8781.01	0.10	3.0	10	10	100
9156	2892 E	75 N	8827.82	8804.24	0.40	3.0	18	47	123
9156	2892 E	100 N	8818.58	8827.47	0.30	3.0	21	63	138
9156	2892 E	125 N	8809.35	8850.71	0.10	15.0	14	53	130
9156	2892 E	150 N	8800.11	8873.94	0.30	3.0	26	73	142

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9156	2892 E	175 N	8790.88	8897.17	0.20	3.0	17	50	130
9156	2892 E	200 N	8781.64	8920.41	0.10	3.0	15	50	105
9156	2892 E	225 N	8772.40	8943.64	0.30	3.0	30	22	143
9156	2892 E	265 N	8757.62	8980.82	0.20	3.0	22	16	60
9156	2892 E	275 N	8753.93	8990.11	0.40	3.0	16	30	164
9156	2892 E	300 N	8744.69	9013.34	0.20	15.0	17	22	194
9156	2892 E	325 N	8735.46	9036.58	0.20	15.0	16	15	125
9156	2892 E	350 N	8726.22	9059.81	0.20	30.0	16	11	65
358- 38	2940 E	1175 N	8444.94	9825.39	0.10	3.0	14	13	69
358- 39	2940 E	1200 N	8435.63	9847.98	0.20	5.0	29	8	61
358- 40	2940 E	1225 N	8426.31	9870.57	0.20	5.0	13	7	66
358- 41	2940 E	1250 N	8417.00	9893.16	0.10	10.0	12	9	57
358- 42	2940 E	1275 N	8407.68	9915.75	0.10	10.0	15	7	69
358- 43	2990 E	1175 N	8492.32	9847.40	0.10	5.0	14	10	67
358- 44	2990 E	1200 N	8483.22	9871.39	0.10	5.0	16	11	60
358- 45	2990 E	1225 N	8474.12	9895.38	0.10	3.0	16	12	42
358- 46	2990 E	1250 N	8465.01	9919.37	0.10	3.0	11	12	53
358- 47	2990 E	1275 N	8455.91	9943.36	0.10	5.0	13	10	42
358- 48	3090 E	1175 N	8582.31	9893.87	0.10	3.0	17	10	62
358- 49	3090 E	1200 N	8573.39	9916.25	0.10	3.0	13	9	53
358- 50	3090 E	1225 N	8564.48	9938.64	0.10	3.0	18	11	59
358- 51	3090 E	1250 N	8555.57	9961.03	0.10	3.0	14	12	74
358- 52	3090 E	1275 N	8546.65	9983.41	0.10	3.0	22	8	71
9148	3121 E	500 N	8892.65	9305.33	0.10	3.0	13	8	120
9148	3121 E	525 N	8885.02	9325.31	0.20	3.0	18	9	130
9148	3121 E	550 N	8877.38	9345.28	0.10	3.0	22	9	127
9148	3121 E	575 N	8869.75	9365.26	0.20	3.0	15	11	123
9148	3121 E	600 N	8862.11	9385.23	0.20	3.0	21	12	185
9148	3121 E	625 N	8854.48	9405.21	0.10	10.0	12	12	134
9148	3121 E	650 N	8846.84	9425.19	0.20	3.0	14	13	147
9148	3121 E	675 N	8839.21	9445.16	0.10	20.0	16	13	146
9148	3121 E	700 N	8831.57	9465.14	0.10	3.0	16	14	133
358- 53	3140 E	1175 N	8630.47	9913.47	0.20	5.0	14	9	65
358- 54	3140 E	1200 N	8621.25	9935.76	0.10	5.0	18	14	61
358- 55	3140 E	1225 N	8612.04	9958.05	0.10	3.0	11	9	57
358- 56	3140 E	1250 N	8602.83	9980.34	0.10	3.0	11	9	57
358- 57	3140 E	1275 N	8593.61	10002.63	0.10	3.0	14	14	51
9156	3337 E	00 N	9307.51	8899.02	0.10	10.0	12	7	65
9156	3337 E	25 N	9297.75	8921.96	0.10	5.0	14	20	128
9156	3337 E	50 N	9287.99	8944.91	0.10	5.0	11	7	49
9156	3337 E	75 N	9278.23	8967.85	0.10	5.0	14	7	38
9156	3337 E	25 S	9317.27	8876.07	0.10	15.0	12	6	43
9156	3337 E	60 S	9330.93	8843.95	0.40	3.0	28	35	233
9156	3337 E	75 S	9336.79	8830.18	0.20	3.0	11	23	170
9156	3337 E	100 N	9268.46	8990.80	0.20	3.0	19	32	138
9156	3337 E	125 N	9258.70	9013.74	0.70	15.0	62	22	215
9156	3337 E	150 N	9248.94	9036.69	0.50	10.0	41	37	204
9156	3337 E	175 N	9234.91	9045.11	0.40	10.0	35	39	254

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9148	3337 E	500 N	9107.48	9356.35	0.10	10.0	10	9	76
9148	3337 E	525 N	9098.32	9379.49	0.10	10.0	13	10	102
9148	3337 E	550 N	9089.16	9402.63	0.10	5.0	15	12	97
9148	3337 E	575 N	9080.00	9425.77	0.10	3.0	11	12	100
9148	3337 E	600 N	9070.85	9448.91	0.10	3.0	18	14	150
9148	3337 E	625 N	9061.69	9472.05	0.10	3.0	16	14	97
9148	3337 E	650 N	9052.53	9495.19	0.10	3.0	14	12	132
9148	3337 E	675 N	9043.37	9518.33	0.10	3.0	10	13	110
9148	3337 E	700 N	9034.21	9541.47	0.10	3.0	13	17	138
9156	3337 E	100 S	9346.55	8807.24	0.10	3.0	9	9	68
9148	3547 E	00 N	9492.26	8965.40	0.20	3.0	20	24	134
9148	3547 E	25 N	9483.75	8988.71	0.20	3.0	18	25	131
9148	3547 E	50 N	9475.25	9012.01	0.10	3.0	14	20	116
9148	3547 E	75 N	9466.74	9035.32	0.10	10.0	13	20	126
9148	3547 E	25 S	9500.77	8942.09	0.10	3.0	20	28	124
9148	3547 E	50 S	9509.28	8918.78	0.10	3.0	15	22	113
9148	3547 E	75 S	9517.78	8895.47	0.10	3.0	11	26	100
9148	3547 E	100 N	9458.23	9058.63	0.40	3.0	25	34	147
9148	3547 E	200 N	9423.80	9151.57	0.20	15.0	23	33	178
9148	3547 E	450 N	9340.55	9388.00	0.10	3.0	20	10	67
9148	3547 E	475 N	9331.90	9411.00	0.10	3.0	13	9	72
9148	3547 E	500 N	9323.25	9434.01	0.10	3.0	20	13	105
9148	3547 E	525 N	9314.60	9457.01	0.10	3.0	17	13	112
9148	3547 E	550 N	9305.95	9480.02	0.10	3.0	22	20	121
9148	3547 E	575 N	9297.30	9503.03	0.10	3.0	15	14	135
9148	3547 E	600 N	9288.65	9526.03	0.10	3.0	17	13	107
9148	3547 E	625 N	9280.00	9549.04	0.10	3.0	18	12	147
9148	3547 E	650 N	9271.35	9572.04	0.10	3.0	16	11	117
9148	3547 E	675 N	9262.70	9595.04	0.10	3.0	21	12	108
9148	3547 E	700 N	9254.05	9618.05	0.10	3.0	25	12	127
9148	3547 E	100 S	9526.29	8872.16	0.10	3.0	12	21	100
585	67 3700 E	6050 N	2012.16	10186.12	0.05	0.5	9	6	87
585	68 3700 E	6100 N	2007.33	10238.13	0.10	1.0	13	6	69
585	69 3700 E	6150 N	2002.49	10290.14	0.10	3.0	10	8	71
585	70 3700 E	6200 N	1997.66	10342.14	0.10	1.0	12	9	54
585	71 3700 E	6250 N	1992.83	10394.15	0.20	1.5	11	9	50
585	72 3700 E	6300 N	1987.99	10446.16	0.05	1.5	9	9	41
585	73 3700 E	6350 N	1983.16	10498.17	0.10	1.5	10	8	42
585	74 3700 E	6400 N	1978.32	10550.17	0.05	1.5	11	9	40
585	75 3700 E	6450 N	1973.49	10602.18	0.10	2.0	12	11	44
585	76 3700 E	6500 N	1968.66	10654.19	0.20	1.5	11	11	55
585	77 3700 E	6550 N	1963.82	10706.20	0.05	1.5	11	12	74
585	78 3700 E	6600 N	1958.99	10758.21	0.05	2.0	12	10	70
585	79 3700 E	6650 N	1954.16	10810.21	0.05	2.5	10	11	62
585	80 3700 E	6700 N	1949.32	10862.22	0.05	1.0	11	10	49
585	81 3700 E	6750 N	1944.49	10914.23	0.05	2.0	14	11	60
585	82 3700 E	6800 N	1939.66	10966.24	0.05	1.0	15	12	67
585	83 3700 E	6850 N	1934.82	11018.25	0.05	1.5	13	12	79

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm	
			East	North						
585	84	3700 E	6900 N	1929.99	11070.25	0.05	1.0	13	11	104
585	85	3700 E	6950 N	1925.15	11122.26	0.05	1.5	12	9	55
585	86	3700 E	7000 N	1920.32	11174.27	0.10	1.0	10	12	86
585	87	3700 E	7050 N	1915.49	11226.28	0.05	1.0	12	7	79
585	88	3700 E	7100 N	1910.65	11278.29	0.05	1.5	10	10	128
585	89	3700 E	7150 N	1905.82	11330.29	0.05	1.0	11	12	88
585	90	3700 E	7200 N	1900.99	11382.30	0.05	2.5	12	9	76
585	91	3700 E	7250 N	1896.15	11434.31	0.05	2.0	11	11	74
585	92	3700 E	7300 N	1891.32	11486.32	0.05	1.5	10	9	99
585	93	3700 E	7350 N	1886.49	11538.33	0.05	2.0	13	17	70
585	94	3700 E	7400 N	1881.65	11590.33	0.05	1.0	11	7	88
585	95	3700 E	7450 N	1876.82	11642.34	0.05	8.5	13	9	99
585	96	3700 E	7500 N	1871.98	11694.35	0.05	1.0	10	14	152
585	97	3700 E	7550 N	1867.15	11746.36	0.05	1.5	16	12	129
585	98	3700 E	7600 N	1862.32	11798.36	0.05	1.0	11	11	112
585	99	3700 E	7650 N	1857.48	11850.37	0.05	1.5	8	22	98
585	100	3700 E	7700 N	1852.65	11902.38	0.05	2.0	9	8	59
9148	3747	E	450 N	9530.34	9458.84	0.10	3.0	19	12	120
9148	3747	E	475 N	9521.33	9482.13	0.10	3.0	14	11	88
9148	3747	E	500 N	9512.33	9505.42	0.10	3.0	13	10	90
9148	3747	E	525 N	9503.32	9528.70	0.10	3.0	14	14	117
9148	3747	E	550 N	9494.31	9551.99	0.10	3.0	15	9	76
9148	3747	E	575 N	9485.30	9575.28	0.20	30.0	17	8	80
9148	3747	E	600 N	9476.30	9598.57	0.10	3.0	15	8	72
9148	3747	E	625 N	9467.29	9621.86	0.10	3.0	17	9	96
9148	3747	E	650 N	9458.28	9645.14	0.10	3.0	20	6	75
9148	3747	E	700 N	9440.27	9691.72	0.30	165.0	30	7	103
487-218	3900	E	5000 N	2132.00	9193.56	0.05	3.0	12	12	26
487-219	3900	E	5050 N	2131.08	9243.81	0.05	5.0	26	19	20
487-220	3900	E	5100 N	2130.16	9294.05	0.05	5.0	12	14	26
487-221	3900	E	5150 N	2129.25	9344.30	0.05	3.0	18	5	18
487-222	3900	E	5200 N	2128.33	9394.54	0.05	10.0	8	7	28
487-223	3900	E	5250 N	2127.41	9444.79	0.05	3.0	8	2	30
487-224	3900	E	5300 N	2126.49	9495.04	0.05	3.0	14	6	24
487-225	3900	E	5350 N	2125.58	9545.28	0.10	3.0	10	9	11
487-226	3900	E	5400 N	2124.66	9595.53	0.05	3.0	8	4	9
487-227	3900	E	5450 N	2123.74	9645.77	0.20	5.0	10	10	15
487-228	3900	E	5500 N	2122.82	9696.02	0.20	3.0	10	9	14
487-229	3900	E	5550 N	2121.91	9746.27	0.05	3.0	10	7	24
487-230	3900	E	5600 N	2120.99	9796.51	0.05	3.0	10	9	56
487-231	3900	E	5650 N	2120.07	9846.76	0.05	5.0	10	10	45
487-232	3900	E	5700 N	2119.15	9897.00	0.40	3.0	8	9	42
487-233	3900	E	5750 N	2118.23	9947.25	0.10	3.0	16	15	80
487-234	3900	E	5800 N	2117.32	9997.50	0.05	3.0	10	8	47
487-235	3900	E	5850 N	2116.40	10047.74	0.05	3.0	10	15	69
487-236	3900	E	5900 N	2115.48	10097.99	0.10	3.0	8	9	45
487-237	3900	E	5950 N	2114.56	10148.23	0.20	3.0	12	14	54
487-238	3900	E	5990 N	2113.83	10188.43	0.10	3.0	16	10	61

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
585 101	3900 E	6050 N	2099.86	10188.64	0.05	2.0	11	6	73
585 102	3900 E	6100 N	2096.99	10243.66	0.05	1.5	19	12	94
585 103	3900 E	6150 N	2094.12	10298.67	0.05	1.0	8	8	83
585 104	3900 E	6200 N	2091.24	10353.69	0.05	1.0	16	9	66
585 105	3900 E	6250 N	2088.37	10408.70	0.05	1.5	10	9	65
585 106	3900 E	6300 N	2085.50	10463.72	0.05	1.5	11	8	69
585 107	3900 E	6350 N	2082.63	10518.74	0.05	1.0	17	10	103
585 108	3900 E	6400 N	2079.76	10573.75	0.05	2.0	15	10	85
585 109	3900 E	6450 N	2076.89	10628.77	0.05	1.5	12	9	76
585 110	3900 E	6500 N	2074.01	10683.78	0.05	2.0	11	5	45
585 111	3900 E	6550 N	2071.14	10738.80	0.05	1.5	9	4	49
585 112	3900 E	6600 N	2068.27	10793.82	0.05	1.5	14	7	55
585 113	3900 E	6650 N	2065.40	10848.83	0.05	1.0	14	7	59
585 114	3900 E	6700 N	2062.53	10903.85	0.05	2.0	15	6	61
585 115	3900 E	6750 N	2059.65	10958.86	0.05	3.0	8	9	41
585 116	3900 E	6800 N	2056.78	11013.88	0.05	1.0	4	15	105
585 117	3900 E	6850 N	2053.91	11068.89	0.05	1.0	10	11	104
585 118	3900 E	6900 N	2051.04	11123.91	0.10	1.5	16	13	112
585 119	3900 E	6950 N	2048.17	11178.93	0.05	1.5	12	12	72
585 120	3900 E	7000 N	2045.29	11233.94	0.05	3.0	11	11	100
585 121	3900 E	7050 N	2042.42	11288.96	0.05	1.0	10	12	87
585 122	3900 E	7100 N	2039.55	11343.97	0.05	1.5	11	17	178
585 123	3900 E	7150 N	2036.68	11398.99	0.05	1.0	22	35	304
585 124	3900 E	7200 N	2033.81	11454.01	0.05	1.0	10	18	159
585 125	3900 E	7250 N	2030.94	11509.02	0.05	1.5	9	18	112
585 126	3900 E	7300 N	2028.06	11564.04	0.05	1.0	8	14	90
585 127	3900 E	7350 N	2025.19	11619.05	0.05	1.0	8	9	140
585 128	3900 E	7400 N	2022.32	11674.07	0.05	1.0	11	7	124
585 129	3900 E	7500 N	2037.59	11676.39	0.05	0.3	12	14	260
585 130	3900 E	7550 N	2036.17	11727.58	0.05	1.5	8	12	174
585 131	3900 E	7600 N	2034.75	11778.77	0.05	0.5	9	15	124
585 132	3900 E	7650 N	2033.33	11829.96	0.10	1.0	7	47	70
585 133	3900 E	7700 N	2031.92	11881.14	0.10	0.3	6	19	37
585 134	3900 E	7750 N	2030.50	11932.33	0.05	1.5	4	15	45
585 135	3900 E	7800 N	2029.08	11983.52	0.10	0.3	5	16	39
487-271	4100 E	5000 N	2331.55	9199.51	0.60	3.0	4	14	43
487-272	4100 E	5050 N	2331.18	9254.23	0.20	10.0	4	11	15
487-273	4100 E	5100 N	2330.81	9308.96	0.05	3.0	6	10	24
487-274	4100 E	5150 N	2330.44	9363.68	0.05	3.0	6	10	10
487-275	4100 E	5200 N	2330.07	9418.41	0.05	3.0	6	12	6
487-276	4100 E	5250 N	2329.70	9473.13	0.50	5.0	8	11	23
487-277	4100 E	5300 N	2329.33	9527.85	0.30	3.0	6	3	10
487-278	4100 E	5350 N	2328.96	9582.58	0.20	3.0	6	4	5
487-279	4100 E	5400 N	2328.59	9637.30	0.10	3.0	2	2	6
487-280	4100 E	5450 N	2328.22	9692.03	0.10	3.0	6	3	23
487-281	4100 E	5500 N	2327.85	9746.75	0.50	3.0	6	6	24
487-282	4100 E	5550 N	2327.48	9801.48	0.50	3.0	6	6	34
487-283	4100 E	5600 N	2327.11	9856.20	0.20	3.0	6	11	24

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
487-284	4100 E	5650 N	2326.74	9910.92	0.30	3.0	8	9	23
487-285	4100 E	5700 N	2326.37	9965.65	0.05	3.0	8	11	14
487-286	4100 E	5800 N	2325.63	10075.10	0.10	10.0	14	10	95
487-287	4100 E	5850 N	2325.26	10129.82	0.10	10.0	10	7	48
487-288	4100 E	5910 N	2324.82	10195.49	0.20	5.0	10	8	50
585 136	4100 E	6050 N	2309.58	10195.71	0.05	1.0	10	11	92
585 137	4100 E	6100 N	2307.16	10247.07	0.05	1.0	9	7	118
585 138	4100 E	6150 N	2304.75	10298.42	0.40	1.0	14	12	96
585 139	4100 E	6200 N	2302.33	10349.78	0.30	1.0	9	8	103
585 140	4100 E	6250 N	2299.91	10401.14	0.10	0.5	9	9	85
585 141	4100 E	6300 N	2297.50	10452.50	0.10	1.0	8	8	70
585 142	4100 E	6350 N	2295.08	10503.86	0.20	0.5	14	13	141
585 143	4100 E	6400 N	2292.66	10555.21	0.20	0.3	6	11	118
585 144	4100 E	6450 N	2290.24	10606.57	0.20	1.0	6	12	96
585 145	4100 E	6500 N	2287.83	10657.93	0.05	0.3	6	12	73
585 146	4100 E	6550 N	2285.41	10709.29	0.05	0.5	2	5	20
585 147	4100 E	6600 N	2282.99	10760.64	0.05	0.5	6	17	101
585 148	4100 E	6650 N	2280.58	10812.00	0.05	0.5	5	12	94
585 149	4100 E	6700 N	2278.16	10863.36	0.05	0.3	5	20	96
585 150	4100 E	6750 N	2275.74	10914.72	0.05	0.5	10	9	74
585 151	4100 E	6800 N	2273.33	10966.07	0.05	0.5	6	9	56
585 152	4100 E	6850 N	2270.91	11017.43	0.05	1.0	14	10	134
585 153	4100 E	6900 N	2268.49	11068.79	0.20	0.5	15	7	69
585 154	4100 E	6950 N	2266.07	11120.15	0.20	1.0	9	6	60
585 155	4100 E	7000 N	2263.66	11171.50	0.20	1.0	8	9	112
585 156	4100 E	7050 N	2261.24	11222.86	0.10	0.5	9	7	74
585 157	4100 E	7100 N	2258.82	11274.22	0.05	0.5	6	8	118
585 158	4100 E	7150 N	2256.41	11325.58	0.05	1.5	9	9	144
585 159	4100 E	7200 N	2253.99	11376.93	0.20	2.0	9	8	118
585 160	4100 E	7250 N	2251.57	11428.29	0.10	0.3	10	7	79
585 161	4100 E	7300 N	2249.16	11479.65	0.05	0.5	12	9	61
585 162	4100 E	7350 N	2246.74	11531.01	0.10	1.5	11	8	86
585 163	4100 E	7400 N	2244.32	11582.36	0.10	0.5	12	10	103
585 164	4100 E	7450 N	2241.91	11633.72	0.10	1.0	12	6	48
585 165	4100 E	7500 N	2239.49	11685.08	0.30	0.5	11	9	51
585 166	4100 E	7550 N	2237.07	11736.44	0.40	1.0	18	7	60
585 167	4100 E	7600 N	2234.65	11787.79	0.40	0.5	17	9	94
585 168	4100 E	7650 N	2232.24	11839.15	0.10	1.0	13	8	71
585 169	4100 E	7700 N	2229.82	11890.51	0.05	1.5	10	7	74
487-320	4300 E	5075 N	2564.12	9204.98	0.20	5.0	8	8	48
487-321	4300 E	5100 N	2562.53	9231.92	0.05	10.0	14	9	38
487-322	4300 E	5150 N	2559.35	9285.80	0.05	10.0	9	7	68
487-323	4300 E	5200 N	2556.17	9339.67	0.10	3.0	9	4	42
487-324	4300 E	5250 N	2552.99	9393.55	0.10	3.0	9	6	30
487-325	4300 E	5300 N	2549.81	9447.43	0.20	15.0	10	6	30
487-326	4300 E	5350 N	2546.64	9501.31	0.10	3.0	13	8	28
487-327	4300 E	5400 N	2543.46	9555.19	0.10	5.0	10	5	40
487-328	4300 E	5450 N	2540.28	9609.06	0.10	25.0	6	9	19

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
487-329	4300 E	5500 N	2537.10	9662.94	0.05	3.0	10	6	48
487-330	4300 E	5550 N	2533.92	9716.82	0.05	5.0	9	6	50
487-331	4300 E	5600 N	2530.74	9770.70	0.20	5.0	5	8	31
487-332	4300 E	5650 N	2527.56	9824.58	0.10	10.0	7	9	39
487-333	4300 E	5700 N	2524.38	9878.45	0.20	5.0	8	9	60
487-334	4300 E	5750 N	2521.20	9932.33	0.10	3.0	9	9	41
487-335	4300 E	5800 N	2518.03	9986.21	0.05	3.0	10	8	52
487-336	4300 E	5850 N	2514.85	10040.09	0.10	10.0	24	14	112
487-337	4300 E	5900 N	2511.67	10093.96	0.30	15.0	8	6	24
487-338	4300 E	5950 N	2508.49	10147.84	0.10	10.0	6	9	70
487-339	4300 E	6000 N	2505.31	10201.72	0.30	3.0	9	13	55
585 170	4300 E	6050 N	2527.76	10252.49	0.05	2.0	13	8	75
585 171	4300 E	6100 N	2524.71	10302.09	0.20	0.5	14	8	87
585 172	4300 E	6150 N	2521.66	10351.69	0.10	1.0	12	6	76
585 173	4300 E	6200 N	2518.60	10401.28	0.20	1.0	17	11	90
585 174	4300 E	6250 N	2515.55	10450.88	0.20	1.5	12	12	64
585 175	4300 E	6300 N	2512.50	10500.48	0.10	1.0	14	12	72
585 176	4300 E	6350 N	2509.45	10550.08	0.05	1.0	11	11	96
585 177	4300 E	6400 N	2506.40	10599.67	0.10	1.5	5	9	60
585 178	4300 E	6450 N	2503.35	10649.27	0.05	1.0	10	14	115
585 179	4300 E	6500 N	2500.29	10698.87	0.05	4.5	11	15	56
585 180	4300 E	6550 N	2497.24	10748.46	0.05	1.0	10	10	96
585 181	4300 E	6600 N	2494.19	10798.06	0.20	1.0	9	9	73
585 182	4300 E	6650 N	2491.14	10847.66	0.05	1.0	12	11	108
585 183	4300 E	6700 N	2488.09	10897.25	0.10	1.0	8	13	52
585 184	4300 E	6750 N	2485.04	10946.85	0.30	0.5	28	18	179
585 185	4300 E	6800 N	2481.98	10996.45	0.10	1.0	16	13	120
585 186	4300 E	6850 N	2478.93	11046.04	0.50	1.0	31	16	110
585 187	4300 E	6900 N	2475.88	11095.64	0.10	0.5	13	13	92
585 188	4300 E	6950 N	2472.83	11145.24	0.20	0.5	11	13	88
585 189	4300 E	7000 N	2469.78	11194.83	0.20	0.5	16	12	56
585 190	4300 E	7050 N	2466.73	11244.43	0.10	1.5	12	20	112
585 191	4300 E	7100 N	2463.67	11294.03	0.20	1.0	13	10	103
585 192	4300 E	7150 N	2460.62	11343.62	0.20	1.0	9	6	70
585 193	4300 E	7200 N	2457.57	11393.22	0.10	0.5	11	9	92
585 194	4300 E	7250 N	2454.52	11442.82	0.20	0.5	9	9	71
585 195	4300 E	7300 N	2451.47	11492.41	0.30	0.3	10	5	92
585 196	4300 E	7350 N	2448.42	11542.01	0.10	1.0	8	7	83
585 197	4300 E	7400 N	2445.36	11591.61	0.10	1.0	7	7	101
585 198	4300 E	7450 N	2442.31	11641.20	0.05	0.3	8	8	62
585 199	4300 E	7500 N	2439.26	11690.80	0.05	0.3	20	4	87
585 200	4300 E	7550 N	2437.62	11741.36	0.05	0.5	13	6	65
585 201	4300 E	7600 N	2435.98	11791.92	0.10	0.3	22	5	67
585 202	4300 E	7650 N	2434.34	11842.47	0.05	0.5	12	5	64
585 203	4300 E	7700 N	2432.71	11893.03	0.05	0.3	27	4	71
585 204	4300 E	7750 N	2431.07	11943.59	0.05	0.5	19	7	60
585 205	4300 E	7800 N	2429.43	11994.15	0.05	0.3	12	4	68
487-371	4500 E	5000 N	2730.62	9210.15	0.05	5.0	8	7	35

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
487-372	4500 E	5050 N	2729.09	9259.66	0.05	10.0	5	6	31
487-373	4500 E	5100 N	2727.57	9309.17	0.05	15.0	5	8	30
487-374	4500 E	5150 N	2726.04	9358.69	0.05	5.0	6	5	28
487-375	4500 E	5200 N	2724.52	9408.20	0.05	5.0	12	9	37
487-376	4500 E	5250 N	2722.99	9457.71	0.05	10.0	9	6	48
487-377	4500 E	5350 N	2719.94	9556.73	0.05	15.0	6	7	35
487-378	4500 E	5400 N	2718.42	9606.25	0.05	5.0	8	4	33
487-379	4500 E	5450 N	2716.89	9655.76	0.05	3.0	5	7	31
487-380	4500 E	5500 N	2715.37	9705.27	0.05	3.0	7	8	44
487-381	4500 E	5550 N	2713.84	9754.78	0.05	3.0	7	7	33
487-382	4500 E	5600 N	2712.32	9804.29	0.05	10.0	8	8	32
487-383	4500 E	5650 N	2710.79	9853.80	0.05	5.0	9	7	34
487-384	4500 E	5700 N	2709.27	9903.32	0.05	3.0	13	6	38
487-385	4500 E	5750 N	2707.74	9952.83	0.05	10.0	17	8	32
487-386	4500 E	5800 N	2706.22	10002.34	0.05	3.0	13	7	28
487-387	4500 E	5850 N	2704.69	10051.85	0.05	3.0	10	11	40
487-388	4500 E	5950 N	2701.64	10150.88	0.05	3.0	7	6	40
487-389	4500 E	6010 N	2699.81	10210.29	0.05	3.0	10	7	52
585 206	4500 E	6050 N	2699.09	10250.22	0.05	0.3	11	7	126
585 207	4500 E	6100 N	2698.20	10300.12	0.05	0.3	10	6	89
585 208	4500 E	6150 N	2697.30	10350.03	0.05	1.0	12	5	83
585 209	4500 E	6200 N	2696.41	10399.94	0.05	0.5	9	6	94
585 210	4500 E	6250 N	2695.51	10449.84	0.05	1.0	21	5	79
585 211	4500 E	6300 N	2694.62	10499.75	0.10	0.3	14	6	83
585 212	4500 E	6350 N	2693.72	10549.66	0.10	0.3	10	4	124
585 213	4500 E	6400 N	2692.82	10599.56	0.10	0.5	11	5	174
585 214	4500 E	6450 N	2691.93	10649.47	0.05	0.3	27	4	131
585 215	4500 E	6500 N	2691.03	10699.38	0.05	0.3	18	4	120
585 216	4500 E	6550 N	2690.14	10749.29	0.10	0.5	14	13	118
585 217	4500 E	6600 N	2689.24	10799.19	0.10	0.5	16	6	186
585 218	4500 E	6650 N	2688.35	10849.10	0.05	1.0	10	5	114
585 219	4500 E	6700 N	2687.45	10899.01	0.10	0.5	17	14	134
585 220	4500 E	6750 N	2686.55	10948.91	0.10	0.3	16	10	104
585 221	4500 E	6800 N	2685.66	10998.82	0.20	0.3	17	10	76
585 222	4500 E	6850 N	2684.76	11048.73	0.10	0.5	14	11	77
585 223	4500 E	6900 N	2683.87	11098.63	0.20	1.5	15	13	69
585 224	4500 E	6950 N	2682.97	11148.54	0.30	0.3	12	11	94
585 225	4500 E	7000 N	2682.08	11198.45	0.20	1.0	13	14	105
585 226	4500 E	7050 N	2681.18	11248.36	0.20	1.0	10	14	87
585 227	4500 E	7100 N	2680.29	11298.26	0.10	1.0	11	13	85
585 228	4500 E	7150 N	2679.39	11348.17	0.05	1.0	10	12	55
585 229	4500 E	7200 N	2678.49	11398.08	0.40	1.5	12	11	81
585 230	4500 E	7250 N	2677.60	11447.98	0.20	2.0	10	9	80
585 231	4500 E	7300 N	2676.70	11497.89	0.20	1.5	10	12	88
585 232	4500 E	7350 N	2675.81	11547.80	0.10	0.5	8	10	46
585 233	4500 E	7400 N	2674.91	11597.71	0.05	0.5	7	14	63
585 234	4500 E	7450 N	2674.02	11647.61	0.05	1.0	11	10	91
585 235	4500 E	7500 N	2673.12	11697.52	0.10	1.0	10	12	93

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
585 236	4500 E	7550 N	2643.37	11748.71	0.20	0.3	14	9	80
585 237	4500 E	7600 N	2641.51	11799.22	0.20	1.0	13	8	96
585 238	4500 E	7650 N	2639.65	11849.74	0.10	0.5	12	9	87
585 239	4500 E	7700 N	2637.79	11900.26	0.05	1.0	11	8	85
585 240	4500 E	7750 N	2635.93	11950.77	0.05	3.0	10	16	343
585 241	4500 E	7800 N	2634.07	12001.29	0.05	0.5	12	12	173
487-422	4700 E	5100 N	2927.10	9317.14	0.05	5.0	7	6	29
487-424	4700 E	5150 N	2925.55	9367.02	0.05	3.0	10	4	61
487-425	4700 E	5200 N	2924.01	9416.90	0.10	20.0	10	8	78
487-426	4700 E	5250 N	2922.47	9466.78	0.05	15.0	8	9	58
487-427	4700 E	5300 N	2920.93	9516.66	0.05	3.0	10	8	80
487-428	4700 E	5350 N	2919.39	9566.54	0.05	3.0	10	6	53
487-429	4700 E	5400 N	2917.84	9616.42	0.10	5.0	10	9	55
487-430	4700 E	5450 N	2916.30	9666.30	0.10	5.0	11	6	40
487-431	4700 E	5500 N	2914.76	9716.18	0.20	5.0	13	9	48
487-432	4700 E	5550 N	2913.22	9766.06	0.40	3.0	12	8	34
487-434	4700 E	5600 N	2911.68	9815.94	0.30	5.0	10	9	49
487-433	4700 E	5650 N	2910.13	9865.82	0.10	3.0	11	6	28
487-436	4700 E	5700 N	2908.59	9915.70	0.10	5.0	12	11	48
487-435	4700 E	5750 N	2907.05	9965.58	0.20	5.0	10	7	42
487-438	4700 E	5800 N	2905.51	10015.46	0.30	15.0	9	11	46
487-437	4700 E	5850 N	2903.97	10065.34	0.05	20.0	12	6	32
487-440	4700 E	5900 N	2902.42	10115.22	0.20	10.0	36	25	147
487-439	4700 E	5950 N	2900.88	10165.10	0.20	5.0	14	15	100
487-441	4700 E	6000 N	2899.34	10214.98	0.30	5.0	13	9	77
585 242	4700 E	6050 N	2888.92	10265.29	0.05	3.0	10	8	96
585 243	4700 E	6100 N	2887.34	10315.20	0.05	2.0	16	9	66
585 244	4700 E	6150 N	2885.77	10365.12	0.05	1.0	11	10	90
585 245	4700 E	6200 N	2884.19	10415.03	0.10	1.0	9	10	81
585 246	4700 E	6250 N	2882.61	10464.95	0.10	2.0	13	12	124
585 247	4700 E	6300 N	2881.03	10514.86	0.05	1.0	11	11	123
585 248	4700 E	6350 N	2879.45	10564.78	0.05	1.5	10	12	91
585 249	4700 E	6400 N	2877.87	10614.69	0.05	4.5	12	9	62
585 250	4700 E	6450 N	2876.30	10664.61	0.05	1.0	8	9	143
585 251	4700 E	6500 N	2874.72	10714.52	0.05	1.5	10	8	120
585 252	4700 E	6550 N	2873.14	10764.44	0.05	2.0	9	9	102
585 253	4700 E	6600 N	2871.56	10814.35	0.05	2.5	12	10	106
585 254	4700 E	6650 N	2869.98	10864.27	0.05	2.0	13	8	74
585 255	4700 E	6700 N	2868.40	10914.19	0.05	1.0	8	6	69
585 256	4700 E	6750 N	2866.83	10964.10	0.05	0.5	10	8	79
585 257	4700 E	6800 N	2865.25	11014.02	0.05	1.5	12	11	92
585 258	4700 E	6850 N	2863.67	11063.93	0.05	0.3	11	11	64
585 259	4700 E	6900 N	2862.09	11113.85	0.05	1.5	12	17	112
585 260	4700 E	6950 N	2860.51	11163.76	0.10	0.3	13	10	99
585 261	4700 E	7000 N	2858.93	11213.68	0.10	0.3	14	20	210
585 262	4700 E	7050 N	2857.36	11263.59	0.05	1.0	13	12	116
585 263	4700 E	7100 N	2855.78	11313.51	0.10	1.0	11	11	126
585 264	4700 E	7150 N	2854.20	11363.42	0.10	0.5	9	10	117

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
585 265	4700 E	7200 N	2852.62	11413.34	0.05	2.5	7	12	89
585 266	4700 E	7250 N	2851.04	11463.25	0.05	2.5	8	15	99
585 267	4700 E	7300 N	2849.46	11513.17	0.05	3.0	14	16	99
585 268	4700 E	7350 N	2847.89	11563.08	0.05	1.0	8	10	61
585 269	4700 E	7400 N	2846.31	11613.00	0.10	1.0	9	10	69
585 270	4700 E	7450 N	2844.73	11662.91	0.05	1.5	8	9	52
585 271	4700 E	7500 N	2843.15	11712.83	0.05	1.5	7	8	98
585 272	4700 E	7550 N	2841.57	11762.74	0.05	1.0	8	8	71
585 273	4700 E	7600 N	2839.99	11812.66	0.05	2.5	13	10	68
585 274	4700 E	7650 N	2838.42	11862.57	0.05	1.0	4	7	33
585 275	4700 E	7700 N	2836.84	11912.49	0.05	0.5	7	8	44
585 276	4700 E	7750 N	2835.26	11962.41	0.05	5.5	6	9	51
585 277	4700 E	7800 N	2833.68	12012.32	0.05	6.0	6	7	63
487-455	4900 E	5025 N	3142.43	9223.15	0.05	10.0	10	11	32
487-456	4900 E	5050 N	3141.28	9248.74	0.05	5.0	10	13	30
487-457	4900 E	5100 N	3138.98	9299.90	0.60	3.0	14	5	36
487-458	4900 E	5150 N	3136.68	9351.07	0.60	20.0	21	4	48
487-459	4900 E	5200 N	3134.39	9402.24	0.10	3.0	4	7	54
487-460	4900 E	5300 N	3129.79	9504.58	0.40	40.0	9	2	49
487-461	4900 E	5350 N	3127.49	9555.75	0.10	50.0	8	7	61
487-462	4900 E	5400 N	3125.19	9606.92	0.05	50.0	8	6	72
487-463	4900 E	5450 N	3122.89	9658.09	0.05	35.0	6	6	53
487-464	4900 E	5500 N	3120.59	9709.26	0.05	15.0	12	5	87
487-465	4900 E	5550 N	3118.30	9760.43	0.05	3.0	10	3	68
487-466	4900 E	5600 N	3116.00	9811.60	0.05	3.0	7	8	75
487-467	4900 E	5650 N	3113.70	9862.77	0.05	5.0	11	8	91
487-468	4900 E	5700 N	3111.40	9913.93	0.05	50.0	10	10	169
487-469	4900 E	5750 N	3109.10	9965.10	0.20	45.0	11	4	131
487-470	4900 E	5800 N	3106.80	10016.27	0.10	20.0	21	6	83
487-471	4900 E	5850 N	3104.51	10067.44	0.05	5.0	13	8	48
487-472	4900 E	5900 N	3102.21	10118.61	0.20	15.0	7	4	158
487-473	4900 E	5950 N	3099.91	10169.78	0.20	10.0	11	13	101
487-474	4900 E	6000 N	3097.61	10220.95	0.20	3.0	22	6	68
585 278	4900 E	6050 N	3094.77	10270.59	0.10	1.5	5	14	60
585 279	4900 E	6100 N	3091.94	10320.24	0.10	3.0	6	10	75
585 280	4900 E	6150 N	3089.10	10369.88	0.05	1.0	7	8	148
585 281	4900 E	6200 N	3086.26	10419.53	0.05	1.5	10	9	80
585 282	4900 E	6250 N	3083.43	10469.17	0.05	0.5	9	11	68
585 283	4900 E	6300 N	3080.59	10518.82	0.05	1.5	8	19	98
585 284	4900 E	6350 N	3077.75	10568.46	0.05	0.5	11	10	86
585 285	4900 E	6400 N	3074.92	10618.11	0.05	1.0	8	8	85
585 286	4900 E	6450 N	3072.08	10667.75	0.10	0.3	4	3	24
585 287	4900 E	6500 N	3069.24	10717.40	0.05	0.3	3	6	28
585 288	4900 E	6550 N	3066.41	10767.04	0.05	0.3	2	6	20
585 289	4900 E	6600 N	3063.57	10816.69	0.05	0.3	3	7	21
585 290	4900 E	6650 N	3060.73	10866.33	0.05	0.5	10	6	19
585 291	4900 E	6700 N	3057.90	10915.98	0.05	1.0	7	5	24
585 292	4900 E	6750 N	3055.06	10965.63	0.05	1.0	8	7	34

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
585 293	4900 E	6800 N	3052.22	11015.27	0.05	0.5	7	6	47
585 294	4900 E	6850 N	3049.39	11064.92	0.05	1.0	9	6	30
585 295	4900 E	6900 N	3046.55	11114.56	0.05	1.0	5	9	51
585 296	4900 E	6950 N	3043.71	11164.21	0.05	1.0	11	6	38
585 297	4900 E	7000 N	3040.88	11213.85	0.05	1.0	5	7	17
585 298	4900 E	7050 N	3038.04	11263.50	0.10	1.0	6	6	15
585 299	4900 E	7100 N	3035.20	11313.14	0.05	1.0	6	6	20
585 300	4900 E	7150 N	3032.37	11362.79	0.05	1.5	7	5	22
585 301	4900 E	7200 N	3029.53	11412.43	0.05	0.5	4	4	23
585 302	4900 E	7250 N	3026.69	11462.08	0.05	1.0	6	5	26
585 303	4900 E	7300 N	3023.86	11511.72	0.05	1.0	5	6	24
585 304	4900 E	7350 N	3021.02	11561.37	0.05	2.0	6	5	21
585 305	4900 E	7400 N	3018.18	11611.01	0.05	1.0	8	6	23
585 306	4900 E	7450 N	3015.35	11660.66	0.05	1.0	7	4	29
585 307	4900 E	7500 N	3012.51	11710.30	0.05	1.0	3	3	23
585 308	4900 E	7550 N	3041.61	11761.05	0.05	0.5	21	7	39
585 309	4900 E	7600 N	3040.18	11811.98	0.05	0.5	13	5	29
585 310	4900 E	7650 N	3038.75	11862.92	0.05	2.0	11	9	21
585 311	4900 E	7700 N	3037.32	11913.85	0.05	0.5	6	8	36
585 312	4900 E	7750 N	3035.89	11964.79	0.05	1.0	9	6	23
585 313	4900 E	7800 N	3034.46	12015.72	0.05	1.5	7	6	26
487-475	5100 E	5020 N	3383.28	9184.09	0.10	3.0	16	5	67
487-476	5100 E	5050 N	3380.76	9215.97	0.05	3.0	13	2	77
487-477	5100 E	5100 N	3376.56	9269.11	0.30	10.0	7	3	61
487-478	5100 E	5150 N	3372.36	9322.25	0.10	3.0	7	5	26
487-479	5100 E	5200 N	3368.16	9375.38	0.05	3.0	5	3	32
487-480	5100 E	5250 N	3363.96	9428.52	0.05	3.0	10	7	38
487-481	5100 E	5300 N	3359.76	9481.66	0.05	3.0	8	6	37
487-482	5100 E	5400 N	3351.36	9587.93	0.05	5.0	6	5	44
487-483	5100 E	5450 N	3347.16	9641.07	0.05	3.0	9	10	45
487-484	5100 E	5500 N	3342.96	9694.21	0.05	3.0	7	7	68
487-485	5100 E	5550 N	3338.75	9747.34	0.10	5.0	13	7	86
487-486	5100 E	5600 N	3334.55	9800.48	0.05	5.0	21	15	161
487-487	5100 E	5650 N	3330.35	9853.62	0.05	3.0	12	8	57
487-488	5100 E	5700 N	3326.15	9906.76	0.05	5.0	10	5	52
487-489	5100 E	5750 N	3321.95	9959.89	0.05	3.0	17	3	98
487-490	5100 E	5800 N	3317.75	10013.03	0.05	15.0	6	6	107
487-491	5100 E	5850 N	3313.55	10066.17	0.05	10.0	6	9	62
487-493	5100 E	5900 N	3309.35	10119.31	0.05	10.0	24	16	173
487-494	5100 E	5960 N	3304.31	10183.07	0.05	5.0	34	10	79
487-495	5100 E	6000 N	3300.95	10225.58	0.05	3.0	15	14	82
585 314	5100 E	6050 N	3298.90	10275.42	0.05	4.5	8	9	49
585 315	5100 E	6100 N	3296.86	10325.27	0.05	1.5	7	8	76
585 316	5100 E	6150 N	3294.81	10375.11	0.05	1.0	11	11	78
585 317	5100 E	6200 N	3292.76	10424.95	0.05	1.0	6	5	73
585 318	5100 E	6250 N	3290.71	10474.79	0.05	1.0	5	4	34
585 319	5100 E	6300 N	3288.67	10524.64	0.05	4.5	7	6	47
585 320	5100 E	6350 N	3286.62	10574.48	0.05	1.0	9	6	56

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
585 321	5100 E	6400 N	3284.57	10624.32	0.05	1.0	13	7	52
585 322	5100 E	6450 N	3282.53	10674.16	0.05	1.0	8	5	28
585 323	5100 E	6500 N	3280.48	10724.01	0.05	1.5	10	6	39
585 324	5100 E	6550 N	3278.43	10773.85	0.05	0.5	12	5	25
585 325	5100 E	6600 N	3276.39	10823.69	0.05	1.5	10	2	11
585 326	5100 E	6650 N	3274.34	10873.53	0.05	1.0	13	5	21
585 327	5100 E	6700 N	3272.29	10923.38	0.05	3.0	23	7	28
585 328	5100 E	6750 N	3270.24	10973.22	0.05	1.0	6	5	8
585 329	5100 E	6800 N	3268.20	11023.06	0.05	3.0	11	6	11
585 330	5100 E	6850 N	3266.15	11072.91	0.05	2.5	10	4	14
585 331	5100 E	6900 N	3264.10	11122.75	0.05	2.0	8	3	5
585 332	5100 E	6950 N	3262.06	11172.59	0.05	2.0	9	3	4
585 333	5100 E	7000 N	3260.01	11222.43	0.05	1.5	8	2	18
585 334	5100 E	7050 N	3257.96	11272.28	0.05	1.5	7	4	16
585 335	5100 E	7100 N	3255.91	11322.12	0.05	1.0	8	4	24
585 336	5100 E	7150 N	3253.87	11371.96	0.05	1.0	10	9	31
585 337	5100 E	7200 N	3251.82	11421.80	0.05	1.5	21	11	39
585 338	5100 E	7250 N	3249.77	11471.65	0.05	0.5	16	10	28
585 339	5100 E	7300 N	3247.73	11521.49	0.05	0.5	10	7	23
585 340	5100 E	7350 N	3245.68	11571.33	0.05	0.5	7	7	15
585 341	5100 E	7400 N	3243.63	11621.17	0.05	0.5	8	8	25
585 342	5100 E	7450 N	3241.59	11671.02	0.05	3.5	8	9	21
585 343	5100 E	7500 N	3239.54	11720.86	0.05	0.5	8	7	23
585 344	5100 E	7550 N	3237.49	11770.70	0.05	1.0	9	11	25
585 345	5100 E	7600 N	3235.44	11820.54	0.05	0.5	13	9	24
585 346	5100 E	7650 N	3233.40	11870.39	0.05	1.0	10	8	26
585 347	5100 E	7700 N	3231.35	11920.23	0.05	2.0	23	8	35
487-496	5300 E	5000 N	3531.36	9235.21	0.05	15.0	11	6	34
487-497	5300 E	5050 N	3531.15	9286.15	0.05	3.0	11	9	50
487-498	5300 E	5100 N	3530.94	9337.09	0.05	3.0	13	7	65
487-499	5300 E	5150 N	3530.72	9388.04	0.05	3.0	9	4	45
487-500	5300 E	5250 N	3530.30	9489.92	0.05	3.0	11	6	22
487-501	5300 E	5300 N	3530.09	9540.86	0.05	3.0	11	7	38
487-502	5300 E	5350 N	3529.88	9591.81	0.05	3.0	12	6	53
487-503	5300 E	5400 N	3529.67	9642.75	0.05	3.0	8	7	35
487-504	5300 E	5450 N	3529.45	9693.69	0.05	3.0	11	7	30
487-505	5300 E	5500 N	3529.24	9744.63	0.05	10.0	18	10	36
487-506	5300 E	5550 N	3529.03	9795.58	0.05	3.0	15	4	29
487-507	5300 E	5600 N	3528.82	9846.52	0.05	3.0	15	7	41
487-508	5300 E	5650 N	3528.61	9897.46	0.50	5.0	38	10	99
487-509	5300 E	5700 N	3528.40	9948.40	0.05	20.0	27	11	59
487-510	5300 E	5750 N	3528.18	9999.34	0.05	5.0	10	6	35
487-511	5300 E	5800 N	3527.97	10050.29	0.05	15.0	16	10	60
487-512	5300 E	5850 N	3527.76	10101.23	0.05	15.0	15	6	52
487-513	5300 E	5900 N	3527.55	10152.17	0.10	15.0	16	12	150
487-514	5300 E	5950 N	3527.34	10203.11	0.10	5.0	11	7	89
585 348	5300 E	6050 N	3499.24	10232.82	0.05	0.5	9	11	69
585 349	5300 E	6100 N	3497.25	10284.14	0.05	0.5	7	8	36

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Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
585 350	5300 E	6150 N	3495.27	10335.46	0.05	0.5	4	9	47
585 351	5300 E	6200 N	3493.28	10386.78	0.05	1.0	10	11	86
585 352	5300 E	6250 N	3491.30	10438.09	0.05	1.0	15	9	62
585 353	5300 E	6300 N	3489.31	10489.41	0.05	0.5	8	8	57
585 354	5300 E	6350 N	3487.33	10540.73	0.05	0.5	6	11	28
585 355	5300 E	6400 N	3485.34	10592.05	0.05	0.5	5	7	17
585 356	5300 E	6450 N	3483.36	10643.37	0.05	0.5	13	11	23
585 357	5300 E	6500 N	3481.37	10694.68	0.05	1.0	7	10	32
585 358	5300 E	6550 N	3479.39	10746.00	0.05	2.0	8	10	36
585 359	5300 E	6600 N	3477.40	10797.32	0.05	1.5	4	8	28
585 360	5300 E	6650 N	3475.42	10848.64	0.05	1.0	24	11	18
585 361	5300 E	6700 N	3473.43	10899.96	0.05	0.5	23	12	19
585 362	5300 E	6750 N	3471.45	10951.28	0.05	1.0	18	10	14
585 363	5300 E	6800 N	3469.46	11002.59	0.05	1.0	2	8	26
585 364	5300 E	6850 N	3467.48	11053.91	0.05	1.0	7	7	28
585 365	5300 E	6900 N	3465.49	11105.23	0.05	1.5	4	9	49
585 366	5300 E	6950 N	3463.51	11156.55	0.05	1.5	10	9	35
585 367	5300 E	7000 N	3461.52	11207.87	0.05	1.0	6	6	33
585 368	5300 E	7050 N	3459.54	11259.19	0.05	0.5	8	9	25
585 369	5300 E	7100 N	3457.55	11310.50	0.05	1.0	7	8	26
585 370	5300 E	7150 N	3455.57	11361.82	0.05	1.0	4	7	21
585 371	5300 E	7200 N	3453.58	11413.14	0.05	1.0	25	11	69
585 372	5300 E	7250 N	3451.60	11464.46	0.05	1.5	30	9	54
585 373	5300 E	7300 N	3449.61	11515.78	0.05	1.0	10	7	26
585 374	5300 E	7350 N	3447.63	11567.10	0.05	1.0	7	5	24
585 375	5300 E	7410 N	3445.24	11628.68	0.05	1.0	10	6	26
585 376	5300 E	7550 N	3439.69	11772.37	0.05	1.0	18	8	32
585 377	5300 E	7600 N	3437.70	11823.69	0.05	1.5	16	7	33
585 378	5300 E	7650 N	3435.72	11875.00	0.05	0.5	24	5	68
585 379	5300 E	7730 N	3432.54	11957.11	0.05	1.0	6	8	24
585 380	5300 E	7750 N	3431.75	11977.64	0.05	0.5	6	6	27
585 381	5300 E	7800 N	3429.76	12028.96	0.05	1.0	30	10	64
487-515	5500 E	5000 N	3729.67	9243.72	0.20	3.0	12	8	35
487-516	5500 E	5050 N	3727.90	9293.54	0.10	5.0	11	5	56
487-517	5500 E	5100 N	3726.13	9343.36	0.05	5.0	11	7	42
487-518	5500 E	5150 N	3724.36	9393.18	0.05	5.0	11	7	44
487-519	5500 E	5200 N	3722.59	9443.00	0.05	10.0	10	11	46
487-520	5500 E	5250 N	3720.82	9492.82	0.05	10.0	9	4	25
487-521	5500 E	5300 N	3719.05	9542.64	0.05	10.0	12	7	26
487-522	5500 E	5350 N	3717.28	9592.46	0.05	5.0	8	8	20
487-523	5500 E	5400 N	3715.51	9642.28	0.05	5.0	13	6	22
487-524	5500 E	5450 N	3713.74	9692.10	0.05	10.0	11	4	20
487-525	5500 E	5500 N	3711.97	9741.92	0.05	10.0	39	5	26
487-526	5500 E	5550 N	3710.20	9791.74	0.10	15.0	19	7	42
487-527	5500 E	5600 N	3708.43	9841.56	0.05	15.0	9	4	46
487-528	5500 E	5650 N	3706.66	9891.38	0.05	35.0	10	8	49
487-529	5500 E	5700 N	3704.89	9941.20	0.05	20.0	12	6	70
487-530	5500 E	5750 N	3703.12	9991.02	0.05	25.0	12	8	118

Continued....

Lab Proj.	Field Line	Grid Station	UIM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
487-531	5500 E	5800 N	3701.35	10040.84	0.05	15.0	17	6	64
487-532	5500 E	5850 N	3699.58	10090.66	0.05	15.0	14	3	105
487-533	5500 E	5900 N	3697.81	10140.48	0.05	15.0	52	17	232
487-534	5500 E	5950 N	3696.04	10190.30	0.20	25.0	55	11	88
487-535	5500 E	6000 N	3694.27	10240.12	0.05	20.0	57	9	89
585 382	5500 E	6050 N	3692.50	10289.94	0.05	0.5	10	10	101
585 383	5500 E	6100 N	3690.73	10339.76	0.05	0.5	8	9	124
585 384	5500 E	6150 N	3688.96	10389.58	0.05	0.5	16	8	83
585 385	5500 E	6200 N	3687.19	10439.40	0.05	0.5	11	7	86
585 386	5500 E	6250 N	3685.42	10489.21	0.05	1.0	5	12	182
585 387	5500 E	6300 N	3683.65	10539.04	0.05	1.0	7	12	136
585 388	5500 E	6350 N	3681.88	10588.86	0.40	0.5	5	9	128
585 389	5500 E	6400 N	3680.11	10638.67	1.00	0.5	13	13	84
585 390	5500 E	6450 N	3678.35	10688.49	0.20	1.0	9	14	89
585 391	5500 E	6500 N	3676.58	10738.31	0.05	0.5	5	9	90
585 392	5500 E	6550 N	3674.81	10788.13	0.05	0.5	3	11	104
585 393	5500 E	6600 N	3673.04	10837.95	0.05	1.0	7	13	77
585 394	5500 E	6650 N	3671.27	10887.77	0.05	0.5	9	8	52
585 395	5500 E	6700 N	3669.50	10937.59	0.05	0.3	10	5	50
585 396	5500 E	6750 N	3667.73	10987.41	0.05	1.0	7	6	41
585 397	5500 E	6800 N	3665.96	11037.23	0.05	1.0	8	5	24
585 398	5500 E	6850 N	3664.19	11087.05	0.05	0.5	6	4	26
585 399	5500 E	6900 N	3662.42	11136.87	0.05	1.0	9	5	33
585 400	5500 E	6950 N	3660.65	11186.69	0.05	2.0	14	5	51
585 401	5500 E	7000 N	3658.88	11236.51	0.10	1.0	10	5	35
585 402	5500 E	7050 N	3657.11	11286.33	0.40	1.0	15	6	48
585 403	5500 E	7100 N	3655.34	11336.15	0.20	0.5	10	7	25
585 404	5500 E	7150 N	3653.57	11385.97	0.20	2.0	11	5	27
585 405	5500 E	7200 N	3651.80	11435.79	0.40	1.5	13	6	41
585 406	5500 E	7250 N	3650.03	11485.61	0.05	1.5	14	6	44
585 407	5500 E	7300 N	3648.26	11535.43	0.10	1.5	10	5	53
585 408	5500 E	7350 N	3646.49	11585.25	0.05	1.0	13	8	59
585 409	5500 E	7400 N	3644.72	11635.07	0.20	1.0	12	6	38
585 410	5500 E	7450 N	3642.95	11684.89	0.30	2.0	10	7	30
585 411	5500 E	7500 N	3641.18	11734.71	0.20	1.5	29	10	37
585 412	5500 E	7550 N	3639.41	11784.53	0.05	1.0	14	6	47
585 413	5500 E	7600 N	3637.64	11834.35	0.20	1.5	20	8	54
585 414	5500 E	7650 N	3635.87	11884.17	0.10	0.5	17	6	40
585 415	5500 E	7700 N	3634.10	11933.99	0.05	1.0	14	8	32
585 416	5500 E	7750 N	3632.33	11983.81	0.05	1.0	14	7	63
585 417	5500 E	7800 N	3630.56	12033.63	0.30	0.5	10	6	38
9347	5700 E	6500 N	3879.76	10744.85	0.20	2.5	13	15	224
9347	5700 E	6550 N	3878.28	10794.60	0.10	2.5	7	12	84
9347	5700 E	6600 N	3876.80	10844.35	0.20	2.5	9	9	113
9347	5700 E	6650 N	3875.32	10894.11	0.10	2.5	8	5	72
9347	5700 E	6700 N	3873.84	10943.86	0.20	2.5	9	6	80
9347	5700 E	6750 N	3872.36	10993.61	0.10	2.5	11	6	78
9347	5700 E	6800 N	3870.88	11043.36	0.10	1.5	9	7	93

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9347	5700 E	6850 N	3869.40	11093.11	0.10	0.5	16	6	74
9347	5700 E	6900 N	3867.92	11142.87	0.20	2.5	24	7	142
9347	5700 E	6950 N	3866.44	11192.62	0.20	2.5	24	6	122
9347	5700 E	7000 N	3864.96	11242.37	0.10	2.5	14	8	96
9347	5700 E	7050 N	3863.47	11292.12	0.10	2.5	15	8	54
9347	5700 E	7100 N	3861.99	11341.87	0.10	2.5	14	7	47
9347	5700 E	7150 N	3860.51	11391.63	0.10	2.5	13	8	44
9347	5700 E	7200 N	3859.03	11441.38	0.10	2.5	22	7	51
9347	5700 E	7250 N	3857.55	11491.13	0.20	2.5	19	7	47
9347	5700 E	7300 N	3856.07	11540.88	0.10	2.5	27	7	58
9347	5700 E	7350 N	3854.59	11590.63	0.10	2.5	19	8	38
9347	5700 E	7400 N	3853.11	11640.39	0.20	0.5	24	6	58
9347	5700 E	7450 N	3851.63	11690.14	0.10	2.5	25	6	50
9347	5700 E	7500 N	3850.15	11739.89	0.20	2.5	27	5	48
9347	5700 E	7550 N	3835.64	11791.26	0.20	2.5	22	6	41
9347	5700 E	7600 N	3833.79	11842.21	0.20	2.5	26	7	50
9347	5700 E	7650 N	3831.94	11893.15	0.10	2.5	25	6	39
9347	5700 E	7700 N	3830.09	11944.09	0.20	2.5	24	6	50
9347	5700 E	7750 N	3828.23	11995.04	0.20	2.5	16	6	46
9347	5700 E	7800 N	3826.38	12045.98	0.20	1.5	18	6	45
9347	5900 E	6500 N	4074.27	10754.68	0.10	2.5	7	34	372
9347	5900 E	6550 N	4072.47	10804.18	0.10	2.5	8	18	403
9347	5900 E	6600 N	4070.67	10853.69	0.10	0.5	11	9	113
9347	5900 E	6650 N	4068.87	10903.19	0.10	1.0	7	8	46
9347	5900 E	6700 N	4067.07	10952.69	0.10	2.5	11	8	160
9347	5900 E	6750 N	4065.27	11002.20	0.10	2.5	17	6	92
9347	5900 E	6800 N	4063.46	11051.70	0.30	2.5	32	8	81
9347	5900 E	6850 N	4061.66	11101.20	0.10	2.5	20	6	87
9347	5900 E	6900 N	4059.86	11150.70	0.20	2.5	16	6	63
9347	5900 E	6950 N	4058.06	11200.21	0.20	2.5	17	5	68
9347	5900 E	7000 N	4056.26	11249.71	0.10	2.5	12	6	59
9347	5900 E	7050 N	4054.46	11299.21	0.10	0.5	14	6	81
9347	5900 E	7100 N	4052.66	11348.72	0.10	1.5	13	7	58
9347	5900 E	7150 N	4050.86	11398.22	0.10	2.5	9	6	51
9347	5900 E	7200 N	4049.06	11447.72	0.10	2.5	15	6	46
9347	5900 E	7250 N	4047.25	11497.22	0.10	0.5	26	6	66
9347	5900 E	7300 N	4045.45	11546.73	0.10	2.5	12	5	40
9347	5900 E	7350 N	4043.65	11596.23	0.10	2.5	20	7	49
9347	5900 E	7400 N	4041.85	11645.73	0.20	2.5	11	7	37
9347	5900 E	7450 N	4040.05	11695.24	0.10	2.5	13	6	47
9347	5900 E	7500 N	4038.25	11744.74	0.20	2.5	17	7	60
9347	5900 E	7550 N	4032.63	11795.58	0.10	2.5	14	6	48
9347	5900 E	7600 N	4030.77	11846.10	0.20	0.5	14	6	47
9347	5900 E	7650 N	4028.91	11896.62	0.20	1.0	13	6	42
9347	5900 E	7700 N	4027.05	11947.13	0.10	2.5	12	6	28
9347	5900 E	7750 N	4025.19	11997.65	0.30	2.5	10	5	38
9347	5900 E	7800 N	4023.33	12048.17	0.20	2.5	10	6	36
9347	6100 E	6500 N	4273.83	10761.91	0.10	2.5	13	8	100

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9347	6100 E	6550 N	4272.48	10811.66	0.10	2.5	10	6	93
9347	6100 E	6600 N	4271.12	10861.41	0.60	2.5	68	12	121
9347	6100 E	6650 N	4269.77	10911.16	0.10	4.0	24	5	77
9347	6100 E	6700 N	4268.42	10960.91	0.10	3.0	11	5	55
9347	6100 E	6750 N	4267.06	11010.66	0.10	1.0	14	6	37
9347	6100 E	6800 N	4265.71	11060.41	0.10	2.0	17	4	44
9347	6100 E	6850 N	4264.36	11110.16	0.20	2.5	17	5	34
9347	6100 E	6900 N	4263.01	11159.91	0.20	1.0	17	6	52
9347	6100 E	6950 N	4261.65	11209.66	0.10	2.5	13	6	48
9347	6100 E	7000 N	4260.30	11259.41	0.20	2.5	16	7	60
9347	6100 E	7050 N	4258.95	11309.16	0.20	2.5	14	7	60
9347	6100 E	7100 N	4257.59	11358.91	0.10	2.5	12	6	49
9347	6100 E	7150 N	4256.24	11408.66	0.10	2.5	16	7	71
9347	6100 E	7200 N	4254.89	11458.41	0.20	2.5	16	6	100
9347	6100 E	7250 N	4253.54	11508.16	0.20	2.5	9	6	80
9347	6100 E	7300 N	4252.18	11557.91	0.20	2.5	18	7	72
9347	6100 E	7350 N	4250.83	11607.66	0.20	2.5	11	6	60
9347	6100 E	7400 N	4249.48	11657.41	0.10	2.5	13	6	70
9347	6100 E	7450 N	4248.12	11707.16	0.10	2.5	15	7	55
9347	6100 E	7492 N	4246.99	11748.95	0.20	2.5	17	6	51
9347	6100 E	7550 N	4232.04	11806.61	0.20	2.5	28	7	58
9347	6100 E	7600 N	4229.97	11857.13	0.20	2.5	10	6	47
9347	6100 E	7650 N	4227.90	11907.65	0.10	2.5	6	5	26
9347	6100 E	7700 N	4225.82	11958.17	0.20	2.5	10	5	44
9347	6100 E	7750 N	4223.75	12008.69	0.10	2.5	9	4	43
9347	6100 E	7800 N	4221.68	12059.21	0.20	2.5	9	5	40
9347	6300 E	6512 N	4464.49	10767.99	0.60	2.5	58	12	77
9347	6300 E	6550 N	4463.44	10806.26	0.50	2.5	64	9	51
9347	6300 E	6600 N	4462.05	10856.61	0.10	2.5	20	5	55
9347	6300 E	6650 N	4460.67	10906.96	0.10	2.5	9	7	32
9347	6300 E	6700 N	4459.29	10957.31	0.20	1.5	11	7	64
9347	6300 E	6750 N	4457.90	11007.67	0.20	1.5	32	7	72
9347	6300 E	6800 N	4456.52	11058.02	0.30	1.0	34	8	74
9347	6300 E	6850 N	4455.13	11108.37	0.20	2.5	17	8	67
9347	6300 E	6900 N	4453.75	11158.72	0.10	2.5	9	8	48
9347	6300 E	6950 N	4452.37	11209.07	0.10	2.5	11	7	34
9347	6300 E	7000 N	4450.98	11259.43	0.30	1.5	20	6	47
9347	6300 E	7050 N	4449.60	11309.78	0.10	0.5	15	7	51
9347	6300 E	7100 N	4448.21	11360.13	0.20	2.5	12	7	79
9347	6300 E	7150 N	4446.83	11410.48	0.20	2.5	17	12	70
9347	6300 E	7200 N	4445.45	11460.83	0.20	2.5	11	9	68
9347	6300 E	7250 N	4444.06	11511.19	0.20	2.5	12	6	52
9347	6300 E	7300 N	4442.68	11561.54	0.30	2.5	46	10	65
9347	6300 E	7350 N	4441.30	11611.89	0.30	2.5	11	6	40
9347	6300 E	7400 N	4439.91	11662.24	0.10	2.5	10	6	37
9347	6300 E	7450 N	4438.53	11712.59	0.10	2.5	10	6	42
9347	6300 E	7500 N	4437.14	11762.95	0.30	2.5	10	5	47
9347	6300 E	7550 N	4435.76	11813.30	0.20	2.5	8	5	45

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9347	6300 E	7600 N	4434.38	11863.65	0.20	2.5	10	6	45
9347	6300 E	7650 N	4432.99	11914.00	0.30	2.5	7	6	46
9347	6300 E	7700 N	4431.61	11964.36	0.20	2.5	8	6	50
9347	6300 E	7750 N	4430.22	12014.71	0.20	2.5	15	6	48
9347	6300 E	7800 N	4428.84	12065.06	0.10	2.5	6	4	22
9347	6500 E	6525 N	4722.51	10776.89	0.30	2.5	33	7	45
9347	6500 E	6550 N	4720.32	10802.39	0.20	2.5	22	6	42
9347	6500 E	6600 N	4715.93	10853.40	0.10	2.5	19	5	43
9347	6500 E	6650 N	4711.55	10904.40	0.20	2.5	18	5	46
9347	6500 E	6700 N	4707.16	10955.41	0.10	2.5	15	5	45
9347	6500 E	6750 N	4702.78	11006.41	0.10	2.5	12	6	32
9347	6500 E	6800 N	4698.39	11057.42	0.10	2.5	9	6	26
9347	6500 E	6850 N	4694.01	11108.42	0.10	2.5	9	6	30
9347	6500 E	6900 N	4689.62	11159.43	0.20	2.5	16	7	45
9347	6500 E	6950 N	4685.24	11210.43	0.20	2.5	15	8	52
9347	6500 E	7000 N	4680.85	11261.44	0.20	1.0	17	9	41
9347	6500 E	7050 N	4676.47	11312.44	0.10	2.5	12	8	49
9347	6500 E	7100 N	4672.08	11363.45	0.20	2.5	12	7	43
9347	6500 E	7150 N	4667.70	11414.45	0.30	2.5	21	13	75
9347	6500 E	7200 N	4663.31	11465.46	0.20	0.5	10	7	30
9347	6500 E	7250 N	4658.93	11516.46	0.10	2.5	8	6	37
9347	6500 E	7300 N	4654.54	11567.47	0.20	2.5	9	6	38
9347	6500 E	7350 N	4650.16	11618.47	0.20	2.5	13	7	61
9347	6500 E	7400 N	4645.77	11669.48	0.20	2.5	9	6	44
9347	6500 E	7450 N	4641.39	11720.49	0.20	2.5	16	7	74
9347	6500 E	7500 N	4637.00	11771.49	0.40	2.5	17	8	63
9347	6500 E	7550 N	4635.35	11821.63	0.10	2.5	8	5	42
9347	6500 E	7600 N	4633.71	11871.76	0.20	2.5	10	5	50
9347	6500 E	7650 N	4632.06	11921.89	0.10	2.5	9	4	40
9347	6500 E	7700 N	4630.42	11972.03	0.10	2.5	8	5	30
9347	6500 E	7750 N	4628.77	12022.17	0.20	2.5	16	7	80
9347	6500 E	7800 N	4627.13	12072.30	0.30	2.5	13	9	81
9347	6700 E	6550 N	4868.69	10782.36	0.10	2.5	13	6	75
9347	6700 E	6600 N	4866.91	10834.25	0.10	2.5	11	5	42
9347	6700 E	6650 N	4865.13	10886.14	0.20	5.5	10	5	43
9347	6700 E	6700 N	4863.35	10938.02	0.10	2.5	18	6	48
9347	6700 E	6750 N	4861.56	10989.91	0.10	2.5	15	6	61
9347	6700 E	6800 N	4859.78	11041.80	0.10	2.5	17	8	78
9347	6700 E	6850 N	4858.00	11093.69	0.10	2.5	16	8	75
9347	6700 E	6900 N	4856.22	11145.58	0.10	2.5	13	7	74
9347	6700 E	6950 N	4854.44	11197.46	0.10	2.5	10	6	60
9347	6700 E	7000 N	4852.66	11249.35	0.10	2.5	13	7	74
9347	6700 E	7050 N	4850.88	11301.24	0.10	2.5	9	6	73
9347	6700 E	7100 N	4849.10	11353.13	0.10	2.5	15	7	73
9347	6700 E	7150 N	4847.32	11405.02	0.10	2.5	13	8	82
9347	6700 E	7200 N	4845.53	11456.90	0.10	2.5	13	5	50
9347	6700 E	7250 N	4843.75	11508.79	0.10	2.5	8	4	35
9347	6700 E	7300 N	4841.97	11560.68	0.10	2.5	8	5	31

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Lab Proj.	Field Line	Grid Station	UIM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9347	6700 E	7350 N	4840.19	11612.57	0.10	2.5	12	5	68
9347	6700 E	7400 N	4838.41	11664.46	0.30	2.5	22	7	80
9347	6700 E	7450 N	4836.63	11716.34	0.10	2.5	19	7	72
9347	6700 E	7500 N	4834.85	11768.23	0.10	2.5	15	7	96
9347	6700 E	7550 N	4833.07	11820.12	0.10	2.5	14	7	68
9347	6700 E	7600 N	4831.29	11872.01	0.10	2.5	11	7	38
9347	6700 E	7650 N	4829.50	11923.90	0.10	2.5	13	8	57
9347	6700 E	7700 N	4827.72	11975.78	0.10	2.5	12	8	66
9347	6700 E	7750 N	4825.94	12027.67	0.10	2.5	11	7	56
9347	6700 E	7800 N	4824.16	12079.56	0.10	2.5	9	9	46
9347	6900 E	6500 N	5070.81	10790.82	0.10	2.5	15	8	51
9347	6900 E	6550 N	5069.15	10840.76	0.10	2.5	23	8	44
9347	6900 E	6600 N	5067.48	10890.70	0.10	2.5	14	7	50
9347	6900 E	6650 N	5065.82	10940.64	0.10	2.5	12	8	58
9347	6900 E	6700 N	5064.16	10990.58	0.10	2.5	20	8	64
9347	6900 E	6750 N	5062.49	11040.52	0.10	2.5	15	9	63
9347	6900 E	6800 N	5060.83	11090.46	0.10	2.5	13	8	50
9347	6900 E	6850 N	5059.17	11140.40	0.10	2.5	13	10	73
9347	6900 E	6900 N	5057.50	11190.34	0.10	2.5	13	11	84
9347	6900 E	6950 N	5055.84	11240.28	0.10	2.5	7	10	70
9347	6900 E	7000 N	5054.18	11290.22	0.10	2.5	14	10	52
9347	6900 E	7050 N	5052.51	11340.16	0.20	2.5	21	8	65
9347	6900 E	7100 N	5050.85	11390.10	0.10	1.5	11	8	70
9347	6900 E	7150 N	5049.19	11440.04	0.10	2.5	8	7	61
9347	6900 E	7200 N	5047.52	11489.98	0.10	2.5	4	7	18
9347	6900 E	7250 N	5045.86	11539.92	0.10	0.5	8	8	45
9347	6900 E	7300 N	5044.19	11589.86	0.10	2.5	9	7	67
9347	6900 E	7350 N	5042.53	11639.80	0.10	2.5	7	7	51
9347	6900 E	7400 N	5040.87	11689.74	0.10	2.5	9	3	30
9347	6900 E	7425 N	5040.04	11714.71	0.40	2.5	30	6	74
9347	6900 E	7550 N	5035.88	11839.56	0.10	2.5	8	5	40
9347	6900 E	7600 N	5034.21	11889.50	0.10	2.5	7	5	20
9347	6900 E	7650 N	5032.55	11939.44	0.10	2.5	5	6	23
9347	6900 E	7700 N	5030.89	11989.38	0.10	4.5	5	4	37
9347	6900 E	7750 N	5029.22	12039.32	0.10	0.5	6	4	52
9347	6900 E	7800 N	5027.56	12089.26	0.20	2.5	7	6	32
9347	7100 E	6525 N	5295.80	10798.94	0.10	2.5	7	5	30
9347	7100 E	6550 N	5294.29	10824.46	0.10	2.5	10	6	50
9347	7100 E	6600 N	5291.28	10875.51	0.10	2.5	9	6	40
9347	7100 E	6650 N	5288.26	10926.56	0.10	2.5	7	6	32
9347	7100 E	6700 N	5285.24	10977.61	0.20	2.5	14	12	82
9347	7100 E	6750 N	5282.23	11028.66	0.10	2.5	8	10	140
9347	7100 E	6800 N	5279.21	11079.71	0.10	2.5	9	9	144
9347	7100 E	6850 N	5276.19	11130.76	0.10	2.5	8	7	54
9347	7100 E	6900 N	5273.18	11181.81	0.10	2.5	11	10	59
9347	7100 E	6950 N	5270.16	11232.86	0.10	2.5	9	10	71
9347	7100 E	7000 N	5267.14	11283.91	0.10	2.5	18	10	93
9347	7100 E	7050 N	5264.13	11334.96	0.10	2.5	10	9	65

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag ppm	Au ppb	Cu ppm	Pb ppm	Zn ppm
			East	North					
9347	7100 E	7100 N	5261.11	11386.01	0.10	2.5	10	7	44
9347	7100 E	7150 N	5258.09	11437.06	0.10	2.5	10	8	45
9347	7100 E	7200 N	5255.08	11488.11	0.10	2.5	9	7	40
9347	7100 E	7250 N	5252.06	11539.16	0.10	2.5	10	7	27
9347	7100 E	7300 N	5249.05	11590.21	0.10	2.5	8	6	34
9347	7100 E	7350 N	5246.03	11641.26	0.10	2.5	12	4	50
9347	7100 E	7400 N	5243.01	11692.31	0.10	2.5	11	5	54
9347	7100 E	7450 N	5240.00	11743.36	0.10	2.5	11	4	45
9347	7100 E	7500 N	5236.98	11794.41	0.70	2.5	30	7	52
9347	7100 E	7600 N	5232.40	11893.01	0.30	2.5	24	6	47
9347	7100 E	7650 N	5230.10	11942.30	0.20	2.5	16	4	39
9347	7100 E	7700 N	5227.81	11991.60	0.20	2.5	17	6	41
9347	7100 E	7750 N	5225.52	12040.90	0.30	2.5	19	5	70
9347	7100 E	7800 N	5223.23	12090.20	0.20	2.5	16	5	70
9347	7300 E	6500 N	5466.11	10804.05	0.20	2.5	9	6	62
9347	7300 E	6550 N	5465.78	10853.98	0.40	1.0	54	10	120
9347	7300 E	6600 N	5465.44	10903.90	0.10	2.5	13	10	122
9347	7300 E	6650 N	5465.11	10953.83	0.20	2.5	10	8	72
9347	7300 E	6700 N	5464.77	11003.75	0.20	0.5	9	7	133
9347	7300 E	6750 N	5464.44	11053.68	0.20	2.5	12	8	123
9347	7300 E	6800 N	5464.10	11103.60	0.10	2.5	21	17	251
9347	7300 E	6850 N	5463.77	11153.53	0.10	2.5	8	7	55
9347	7300 E	6900 N	5463.43	11203.45	0.10	1.0	8	7	57
9347	7300 E	6950 N	5463.10	11253.38	0.10	2.5	11	7	45
9347	7300 E	7000 N	5462.76	11303.30	0.20	1.0	9	7	54
9347	7300 E	7050 N	5462.43	11353.23	0.10	2.5	8	7	50
9347	7300 E	7100 N	5462.10	11403.16	0.10	2.5	11	5	75
9347	7300 E	7150 N	5461.76	11453.08	0.20	2.5	25	7	53
9347	7300 E	7200 N	5461.43	11503.01	0.10	2.5	11	4	30
9347	7300 E	7250 N	5461.09	11552.93	0.10	2.5	10	7	34
9347	7300 E	7300 N	5460.76	11602.86	0.10	2.5	9	8	45
9347	7300 E	7350 N	5460.42	11652.78	0.10	2.5	14	7	56
9347	7300 E	7400 N	5460.09	11702.71	0.20	2.5	17	7	71
9347	7300 E	7450 N	5459.75	11752.63	0.10	2.5	12	8	98
9347	7300 E	7500 N	5459.42	11802.56	0.20	2.5	12	8	37
9347	7300 E	7550 N	5434.10	11853.27	0.20	2.5	15	8	64
9347	7300 E	7600 N	5432.87	11903.36	0.20	2.5	15	10	64
9347	7300 E	7650 N	5431.64	11953.44	0.10	2.5	17	9	68
9347	7300 E	7700 N	5430.41	12003.52	0.10	2.5	12	8	33
9347	7300 E	7750 N	5429.19	12053.61	0.10	2.5	21	8	35
9347	7300 E	7800 N	5427.96	12103.69	0.10	2.5	15	7	48
9347	7500 E	6500 N	5652.97	10811.46	0.10	2.5	10	9	52
9347	7500 E	6550 N	5651.75	10861.44	0.10	0.5	8	7	31
9347	7500 E	6600 N	5650.52	10911.43	0.10	2.5	12	7	53
9347	7500 E	6650 N	5649.30	10961.41	0.10	2.5	12	8	51
9347	7500 E	6700 N	5648.08	11011.39	0.10	2.5	8	8	37
9347	7500 E	6750 N	5646.85	11061.37	0.10	1.0	9	7	40
9347	7500 E	6800 N	5645.63	11111.36	0.10	0.5	9	7	39

Continued....

Lab Proj.	Field Line	Grid Station	UTM Grid		Ag <u>ppm</u>	Au <u>ppb</u>	Cu <u>ppm</u>	Pb <u>ppm</u>	Zn <u>ppm</u>
			East	North					
9347	7500 E	6850 N	5644.41	11161.34	0.10	2.5	8	7	42
9347	7500 E	6900 N	5643.19	11211.32	0.10	2.5	7	6	47
9347	7500 E	6950 N	5641.96	11261.30	0.10	2.5	16	14	75
9347	7500 E	7000 N	5640.74	11311.29	0.10	2.5	18	12	83
9347	7500 E	7050 N	5639.52	11361.27	0.10	2.5	6	8	30
9347	7500 E	7100 N	5638.29	11411.25	0.10	2.5	8	7	39
9347	7500 E	7150 N	5637.07	11461.23	0.10	2.5	9	6	30
9347	7500 E	7200 N	5635.85	11511.22	0.10	2.5	16	6	47
9347	7500 E	7250 N	5634.62	11561.20	0.10	2.5	23	7	43
9347	7500 E	7300 N	5633.40	11611.18	0.10	0.5	13	8	62
9347	7500 E	7350 N	5632.18	11661.17	0.10	2.5	16	7	60
9347	7500 E	7400 N	5630.95	11711.15	0.30	0.5	29	9	50
9347	7500 E	7450 N	5629.73	11761.13	0.20	2.5	21	7	60
9347	7500 E	7500 N	5628.51	11811.11	0.10	2.5	12	5	56
9347	7500 E	7550 N	5627.29	11861.10	0.10	2.5	9	4	49
9347	7500 E	7600 N	5626.06	11911.08	0.10	2.5	12	2	25
9347	7500 E	7650 N	5624.84	11961.06	0.20	2.5	11	4	31
9347	7500 E	7700 N	5623.62	12011.04	0.10	2.5	10	7	43
9347	7500 E	7750 N	5622.39	12061.03	0.10	2.5	9	5	55
9347	7500 E	7800 N	5621.17	12111.01	0.10	2.5	10	6	42



**APPENDIX VII**  
**Soil Sample Statistical Summary**  
**and**  
**Histograms**

PLACER DOME INC.  
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Placer Data Analysis System - STATS  
run on 89:11:01 at 10:48:09  
SPRING SOILS, ALL DATA

Summary of data from file : all88-89.sol

This data file contains an internal header: ( 5 records)  
Data grouped into 12 fields  
with format: ( 3A8, 4F10.2, 5F10.2)

Character ID fields:  
PROJ LINE STAT

Coordinate fields:  
XUTM YUTM EAST NRTH

Other data fields:  
CU ZN PB AU AG

Missing data indicated by NULL value 9999.00

BASIC STATISTICS OF SELECTED DATA FIELDS:

NAME	NDATA	NULLS	MINIMUM	MAXIMUM	MEAN	STD. DEV.	GEOM. MEAN	DISPERSION
CU	6792	2	2.00000	333.000	17.0941	15.3913	14.0167	7.84517 25.0431
ZN	6792	2	4.00000	9800.00	162.077	227.760	107.517	46.4717 248.751
PB	6792	2	1.00000	650.000	15.4545	21.7806	10.8618	5.14024 22.9521
AU	6791	3	.000000	770.000	4.83941	14.8291	3.28134	1.68099 6.40526
AG	6792	2	.000000	14.0000	.222670	.336159	.156669	.704714E-01 .348302

CORMAT: RUN ON 89:11:01 AT 10:48:09

Data from file: all88-89.sol

SPRING SOILS, ALL DATA

Correlation matrix for 6794 records with 5 variables

LOG:	CU 0	ZN 0	PB 0	AU 0	AG 0
CU	1.000	-.023	-.016	.028	.202
ZN	-.023	1.000	-.575	-.007	.610
PB	-.016	-.575	1.000	-.010	.402
AU	.028	-.007	-.010	1.000	-.003
AG	.202	.610	.402	-.003	1.000

Number of data pairs contributing to correlation

	CU	ZN	PB	AU	AG
CU	6792	6792	6792	6789	6792
ZN	6792	6792	6792	6789	6792
PB	6792	6792	6792	6789	6792
AU	6789	6789	6789	6791	6789
AG	6792	6792	6792	6789	6792

HISTO:

SPRING SOILS, ALL DATA

RUN ON 89:11:01 AT 10:48:09

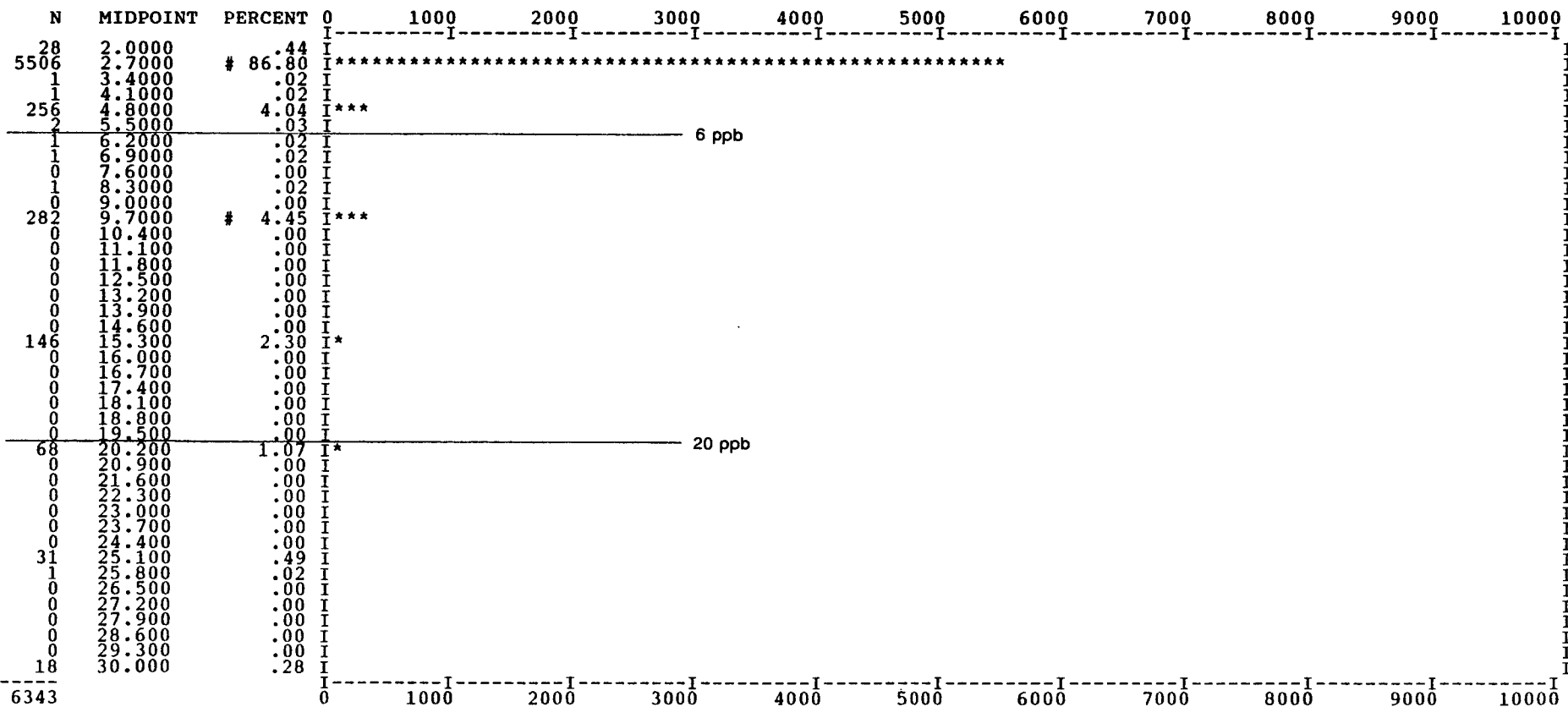
File: all188-89.sol Field name: AU LOG = 0 REPVAL = .00100

6791 SAMPLES WITH AU MINIMUM: .000000 MAXIMUM: 770.000

6343 VALUES PLOTTED: 448 NOT IN RANGE 2.00000 to 30.0000

MEAN: 4.01766 STD. DEV.: 3.50140

SCALE OF HISTOGRAM IS 100.00 COUNTS /PRINT POSITION # = 5,50,95%



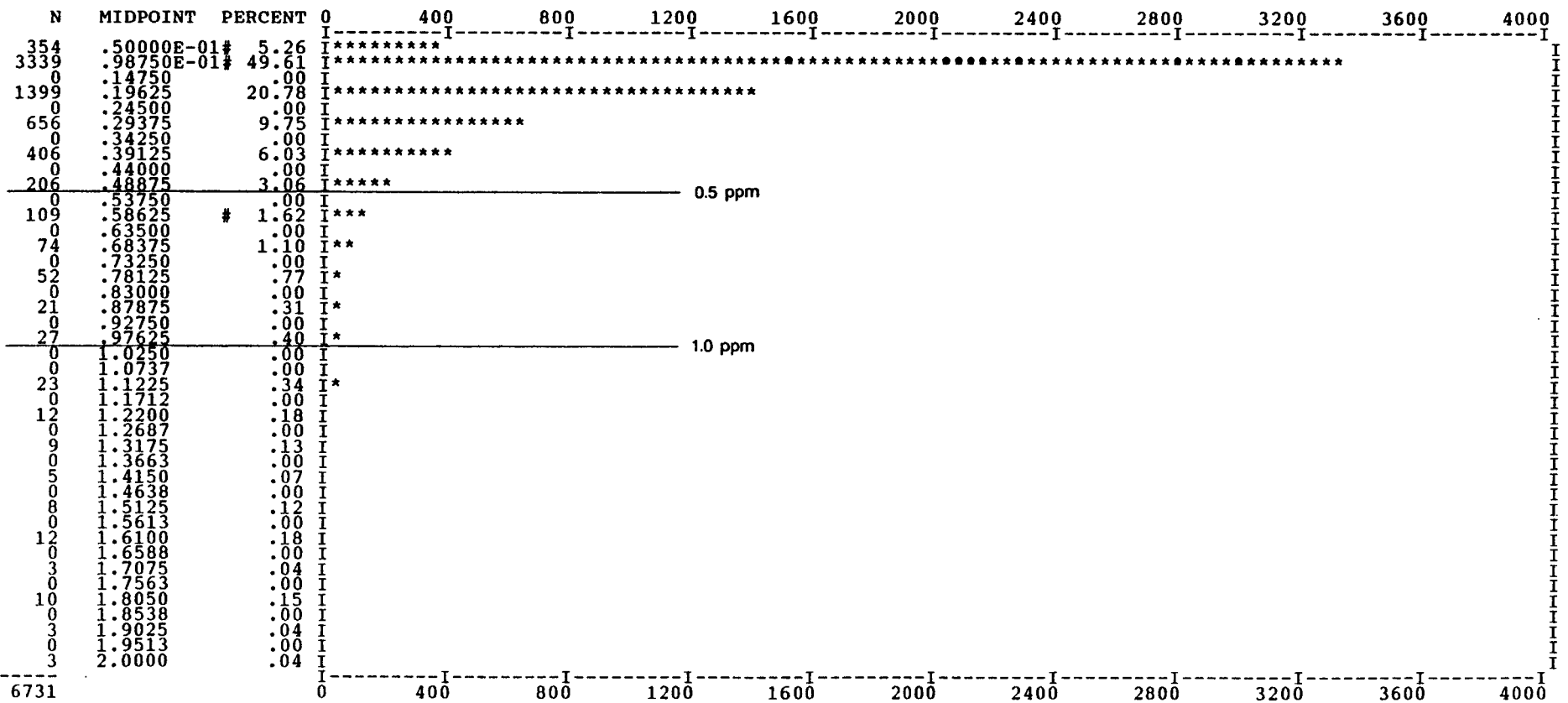
HISTO:

SPRING SOILS, ALL DATA

RUN ON 89:11:01 AT 10:48:09

File: all88-89.sol                    Field name: AG      LOG = 0    REPVAL =    .00100  
 6792 SAMPLES WITH AG                MINIMUM:    .000000        MAXIMUM: 14.0000  
 6731 VALUES PLOTTED:               61 NOT IN RANGE    .500000E-01 to 2.00000  
                                       MEAN:            .211359        STD. DEV.:    .211338

SCALE OF HISTOGRAM IS 40.00 COUNTS /PRINT POSITION # = 5,50,95%





HISTO:

SPRING SOILS, ALL DATA

RUN ON 89:11:01 AT 10:48:09

File: all88-89.sol

Field name: PB

LOG = 0 REPVAL = .00100

6792 SAMPLES WITH PB

MINIMUM: 1.00000

MAXIMUM: 650.000

6740 VALUES PLOTTED:

52 NOT IN RANGE

1.00000

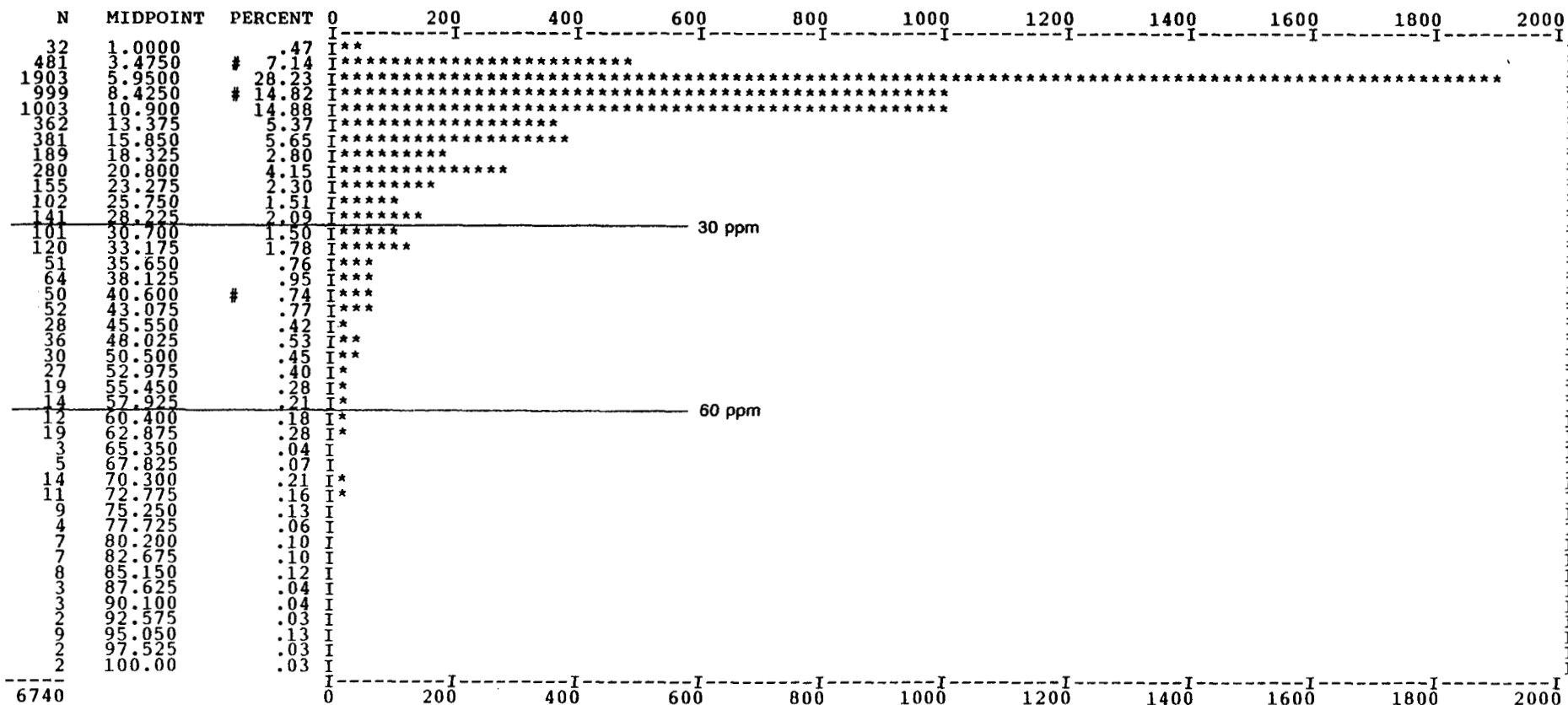
to 100.000

MEAN:

14.1516

STD. DEV.: 13.1963

SCALE OF HISTOGRAM IS 20.00 COUNTS /PRINT POSITION # = 5,50,95%



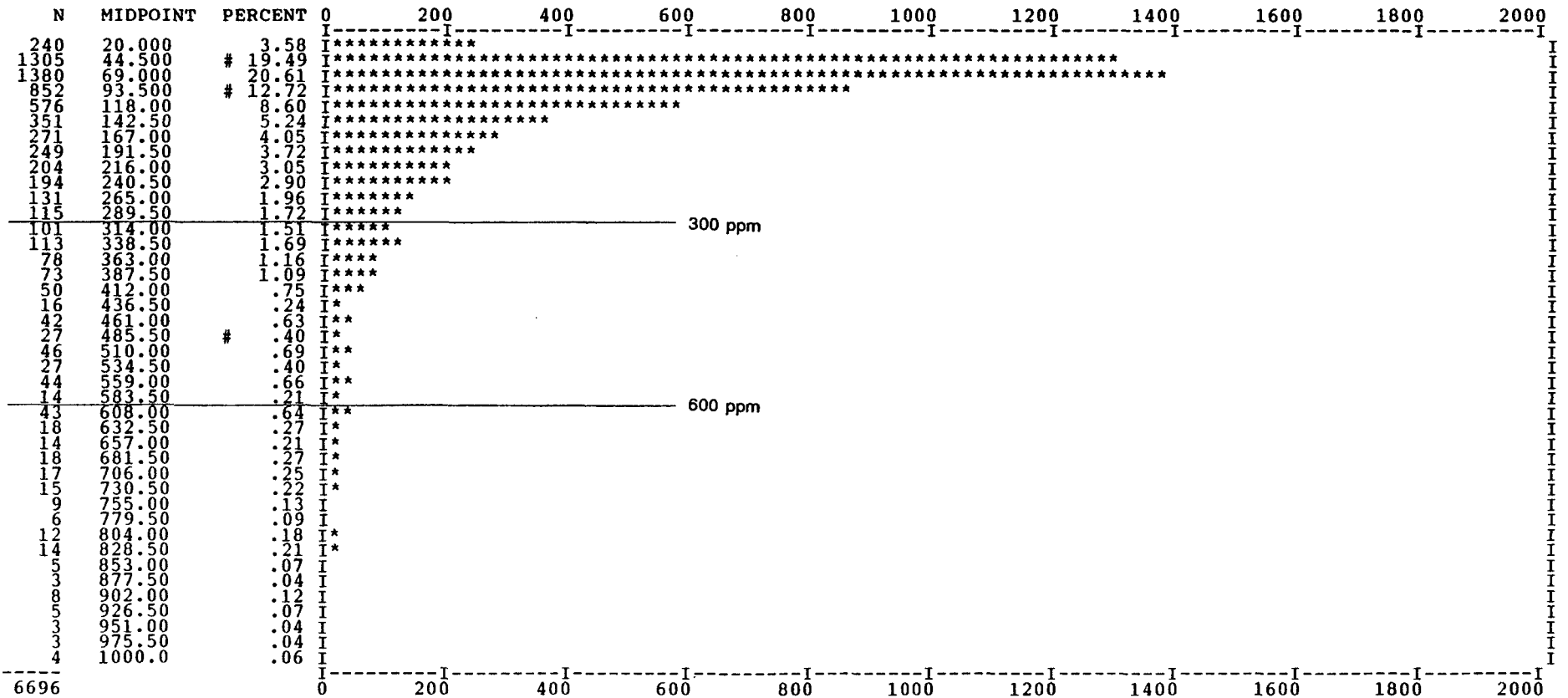
HISTO:

SPRING SOILS, ALL DATA

RUN ON 89:11:01 AT 10:48:09

File: all88-89.sol                    Field name: ZN            LOG = 0    REPVAL =    .00100  
 6792 SAMPLES WITH ZN            MINIMUM: 4.00000            MAXIMUM: 9800.00  
 6696 VALUES PLOTTED:    96 NOT IN RANGE    20.0000    to    1000.00  
                                   MEAN:                    150.606            STD. DEV.: 150.262

SCALE OF HISTOGRAM IS 20.00 COUNTS /PRINT POSITION # = 5,50,95%





**APPENDIX VIII**

**Seismic Refraction Survey**

# SPRING PROPERTY - SEISMIC REFRACTION SURVEY

## PART A - GENERAL

### 1. Introduction

A seismic refraction survey was conducted on the Spring property by Placer Dome Inc. personnel from 28 June to 30 June, 1989. Property access is via forestry trunk road from Princeton or Peachland. A trenching program was being conducted based on data from geochemical (soil) and geophysical (Induced Polarization) surveys. At several sites, bedrock could not be reached due to excessive (> 6 metres) overburden thickness. The seismic refraction survey was conducted in order to establish the overburden thickness at potential trenching sites.

### 2. Physiography

The local topography is mountainous with low relief. Valley slopes are gentle and are generally mantled by glacial sediment of variable thickness. Rock outcroppings are uncommon, although bedrock may be exposed in roadcuts.

With the exception of logged areas, the terrain is covered by mature spruce and pine forest.

### 3. Stratigraphy

Complete stratigraphic sections were exposed in some trenches. Unlithified sediment sequences are conformable. Individual units may exhibit variability in composition. A typical stratigraphic sequence is listed following:

- A veneer of organic soil varying in thickness from 5 to 30 cm.
- An unconsolidated to lightly consolidated sandy till unit with observed thicknesses of 1.0 metres in trenches exposing bedrock to 3.0 metres in test pits.
- A highly over-consolidated (basal) sandy clay-till unit that may be present in trenches exposing bedrock and is commonly present in unknown thicknesses at test pits where bedrock has not been exposed.
- A rind of weathered bedrock up to 1.0 metres in thickness consisting of angular rock and mineral fragments. Particles vary in size from 1 mm to several tens of cm.
- Bedrock.

\* The glacially deposited units may contain a significant quantity of sub-angular to rounded boulders of variable size.

#### 4. Equipment and Survey Procedure

The survey was conducted with an OYO Model 1814 PS-1 digital seismometer. The PS-1 instrument utilizes a single geophone and has a maximum array dimension of 30 metres. The seismic source was a 12 lb. sledge hammer used with a steel strike plate. Several geophone array spacings were tried. The optimum was found to consist of 0.5 metre stations from 0.5 to 3.0 metres, 1.0 metre stations from 3.0 to 10.0 metres and 2.0 metre stations from 10.0 to 30.0 metres. Five to ten instrument readings were taken at each array station to verify consistency. The arithmetic mean of the readings was used if the individual readings exhibited significant variability. Instrument readings were found to more consistent when the geophone and the strike plate were firmly embedded in mineral soil. In addition, it was noted that moderate rainfall created sufficient noise to render the instrument readings unusable.

#### PART B - RESULTS AND DISCUSSION

A total of 16 seismic lines were run, including 10 trial lines at sites where excavation had already been performed. Interval times for each station were noted and time-distance field plots were constructed (see end of report). Seismic velocities and refractor depths calculated from the field plots are listed in Table 2. Summary statistics for the velocity data are listed in Table 3.

Trial seismic lines numbered T-1, T-3, T-3A, T-4, T-5, T-6, and T-9 were performed at sites where bedrock was known to be at a depth of less than two (2) metres. Trial seismic lines numbered T-2, T-7 and T-8 were performed at sites where bedrock was known to be deeper than six (6) metres. With the exception of trial line T-2, the trial seismic lines yielded a distinct two-layer stratigraphy: an upper unit with a mean seismic velocity of 312 m/s and a lower unit with a mean seismic velocity of 1448 m/s. The three layer interpretation in seismic trial T-2 is questionable due to significant data scatter. For this reason it is excluded from the statistical analysis in Table 3.

The seismic velocities at those sites with known depth to bedrock do not differ significantly from those sites where the depth to bedrock is unknown. It is noted that this observation is necessarily limited by the relatively small sample sizes.

A total of six (6) seismic lines were performed at potential trenching sites. All of these lines were performed in a target area within the Spring claim known as Zone 4. Lines numbered S-1, S-3, and S-4 yielded a three layer stratigraphy while line number S-2 yielded a two layer stratigraphy. Lines numbered S-5 and S-6 are believed to be in an area of thick overburden and did not yield well-defined velocity traces. Seismic velocities have not been calculated for these two plots.

The V1 and V2 mean seismic velocities for these lines, both with line S-2 included and excluded, are significantly lower than those values tabulated for the trial lines (see Table 2). It is noted that the sample size is small (4 and 3).

Test pits excavated after the seismic work on seismic lines S-1, S-2 and S-3 revealed bedrock at depths of 2.5, 1.5 and 2.5 metres respectively. These depths vary significantly from those calculated from the seismic data. Inspection of the test pits failed to reveal a definable three-layer stratigraphy as predicted.

#### PART C - CONCLUSIONS

At this site the application of the seismic refraction method for determining overburden thickness is not recommended. The similarity of seismic velocities noted for both bedrock and consolidated sandy till limits the use of depth calculations.

Topographic expression appears to be dominantly bedrock controlled. The overburden is of minimal depth in areas of pronounced hummocky topography. Overburden appears to be thickest at downhill slope breaks and on smooth, gently sloping till plains. The use of geomorphic interpretation is strongly recommended as the primary tool for siting trenches.

Report submitted by K. Everard and H. Letient. July 1989.

TABLE 1 - TABULATED DATA

x = distance from source to geophone		travel time (msec)				
x (metres)	T-1	T-2	T-3	T-3a	T-4	T-5
1	3.3	3.6	5.7	4.0	5.3	3.3
2	6.7	6.6	8.1	7.0	10.2	6.0
3	9.7	9.9	12.2	10.1	12.0	9.4
4	12.3	12.3	17.5	13.3	15.1	12.3
5	15.1	15.1	21.1	16.3	15.2	15.1
6	16.8	14.5	22.5	20.4	16.9	17.5
7	19.2	16.7	20.8	18.3	13.8	18.3
8	20.9	16.7	21.7	21.5	14.5	18.5
9	21.9	20.4	22.3	23.8	14.8	20.6
10	22.4	20.1	23.8	25.1	19.8	21.9
12	24.9	24.3	23.8	26.3	21.2	23.6
14	27.0	31.1	24.1	35.9	20.6	25.6
16	29.8	67.4	25.8	29.0	33.9	28.0
18	32.2	37.5	25.9	29.9	33.8	28.9
20	31.9	28.4	27.5	31.2	56.0	29.5
22	33.9	30.5	25.7	?	?	33.6
24	35.7	31.1	30.1	?	28.6	35.4
26	37.4	33.2	66.8	82.3	33.2	36.0
28	38.4	37.0	78.0	44.5	28.8	33.8
30	62.0	60.2	-	42.0	29.9	38.1
	T-6	T-7	T-8	T-9		
0.5	2.2	1.6	1.6	2.2		
1	4.0	3.2	3.6	4.0		
1.5	5.3	5.1	5.2	5.5		
2	7.3	6.7	7.1	7.2		
2.5	6.4	8.2	8.1	8.8		
3	9.4	9.9	10.1	9.0		
4	8.2	11.7	13.4	9.7		
5	9.3	13.0	15.1	10.1		
6	12.2	13.6	15.6	11.3		
7	11.8	15.0	14.8	13.5		
8	10.4	15.5	15.9	13.1		
9	13.3	15.8	15.8	14.1		
10	15.2	15.6	17.2	15.0		
11	-	17.3	-	16.0		
12	14.6	19.1	18.0	17.0		
13	-	18.4	-	-		
14	13.8	19.4	22.2	19.6		
15	-	19.4	-	-		
16	15.5	22.4	23.2	20.4		
18	18.1	24.1	25.5	21.0		
20	19.2	26.2	25.5	21.7		
22	21.7	26.6	25.9	24.2		
24	20.3	27.9	26.2	24.4		
26	19.7	28.7	26.6	27.1		
28	25.3	29.5	-	28.5		
30	28.0	29.1	-	27.6		

TABLE 1 - CONTINUED

x (metres)	travel time (msec)					
	S-1	S-2	S-3	S-4	S-5	S-5
0.5	1.7	2.1	2.1	1.7	2.0	1.5
1	3.8	4.3	4.0	3.4	3.4	3.6
1.5	5.3	8.4	5.6	5.5	5.0	5.9
2	7.3	8.8	6.9	7.0	6.6	9.9
2.5	9.3	10.0	8.6	10.7	8.5	14.2
3	12.1	9.6	9.9	11.2	9.9	13.4
4	13.0	13.8	12.2	11.9	12.6	10.7
5	14.5	13.5	13.0	13.9	12.4	13.6
6	14.3	14.9	13.8	14.0	14.5	15.8
7	17.4	14.7	14.7	18.1	17.1	17.6
8	18.6	15.2	15.6	17.6	19.3	21.0
9	20.9	17.6	16.1	17.6	15.5	18.9
10	21.5	18.9	17.0	19.2	16.0	19.6
12	19.6	18.3	17.7	20.3	16.8	22.5
14	21.2	19.4	18.6	22.2	17.6	24.7
16	20.0	20.6	19.7	25.2	21.4	25.2
18	20.7	24.8	22.7	25.6	19.8	21.4
20	22.4	28.1	21.5	27.0	23.8	24.2
22	25.5	26.9	22.0	25.5	21.3	26.5
24	26.7	-	23.0	24.7	24.2	-
26	23.0	-	23.7	27.3	24.0	36.0
28	25.7	-	25.0	25.7	24.4	25.0
30	27.0	-	23.0	30.1	21.0	26.1

TABLE 2 - TABULATED RESULTS

Line #	V1	V2	V3	D1	D2
T-1	369	1105	-	2.5	-
T-2	353	494	995	-	-
T-3	393	1617	-	2.8	-
T-3a	305	1357	-	1.3	-
T-4	242	2121	-	2.2	-
T-5	341	1067	-	2.2	-
T-6	274	1667	-	1.1	-
T-7	302	1284	-	1.4	-
T-8	286	1500	-	1.6	-
T-9	298	1310	-	1.0	-
S-1	231	643	2963	1.0	4.0
S-2	217	1244	-	1.0	-
S-3	312	1250	2333	1.7	4.0
S-4	274	943	4923	-	-

TABLE 3 - SUMMARY STATISTICS

Trial Lines  
(Line T-2 Excluded)

	# Pnts.	Max	Min	Mean
V1-All	9	393	242	312
V2-All	9	2121	1067	1448
V1-Bedrock	7	393	242	317
V2-Bedrock	7	2121	1067	1463
V1-Till	2	302	286	294
V2-Till	2	1500	1284	1392

Seismic Lines  
(Line S-2 Included)

	# Pnts.	Max	Min	Mean
V1-All	4	312	217	258
V2-All	4	1250	643	1020
V3-All	3	4923	2333	3406

(Line S-2 Excluded)

	# Pnts.	Max	Min	Mean
V1-All	3	312	231	272
V2-All	3	1250	643	945
V3-All	3	4923	2333	3406

SEISMIC REF TIME - DISTANCE [SEISMIC LINE TRIAL - SBIS #1]

June 28

TRIAL # 5 (REVERSE OF #1)

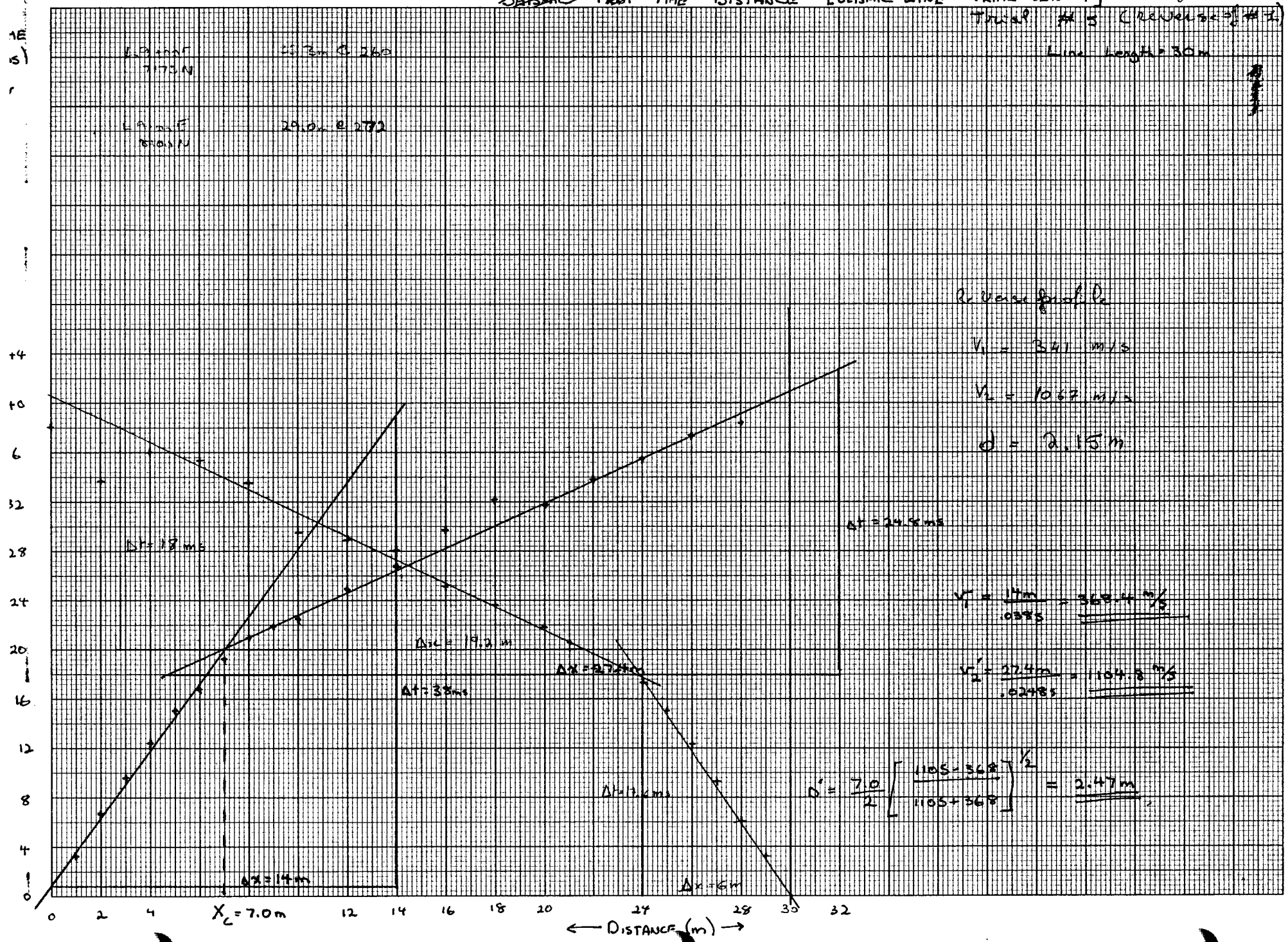
Line length = 30m

L.P. 1225  
7.75 m

29.0 @ 260

L.P. 1225  
18.0 m

29.0 @ 272



Reverse of P1

$$V_1 = 361 \text{ m/s}$$

$$V_2 = 1067 \text{ m/s}$$

$$d = 2.15 \text{ m}$$

$$\Delta t = 24.5 \text{ ms}$$

$$V_1 = \frac{17m}{0.047s} = 361.7 \text{ m/s}$$

$$V_2 = \frac{27.4m}{0.0258s} = 1062 \text{ m/s}$$

$$d' = \frac{7.0}{2} \left[ \frac{1105 - 368}{1105 + 368} \right]^{1/2} = 2.47 \text{ m}$$

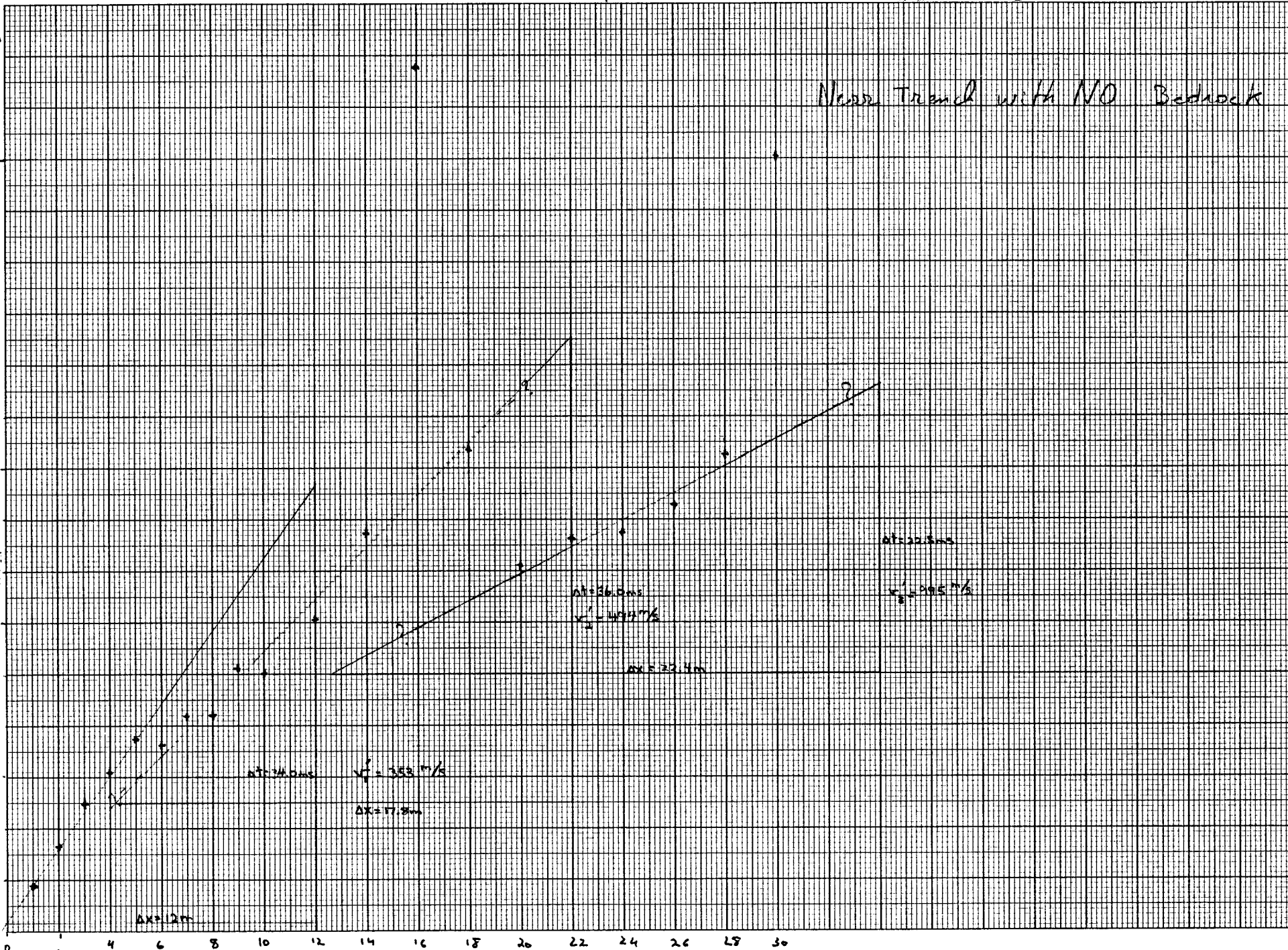
461510



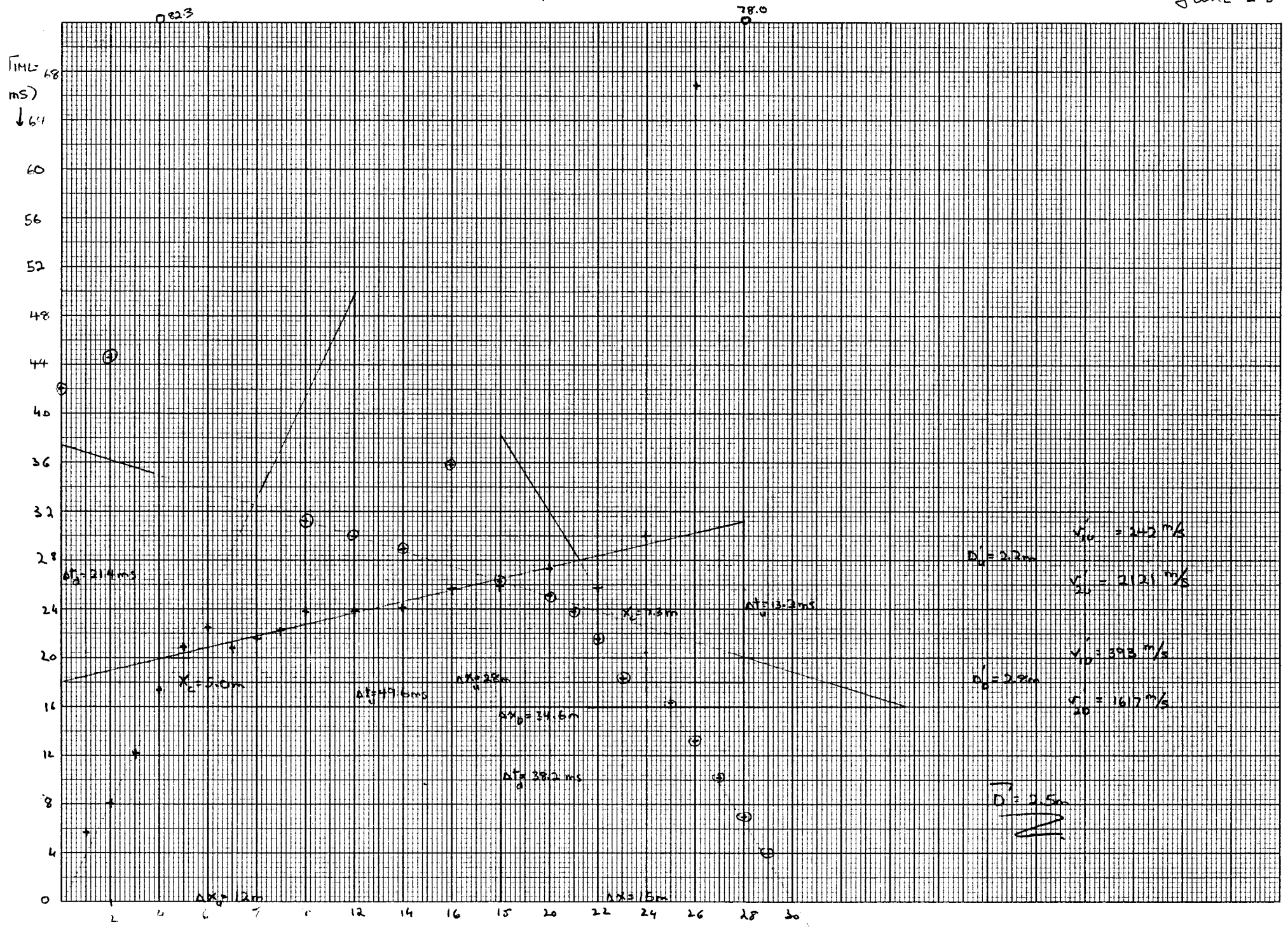
Narrow Trench with NO Bedrock

time ↑  
msec)

60  
40  
36  
32  
28  
24  
20  
16  
12  
8  
4  
0



distance from shot hole.

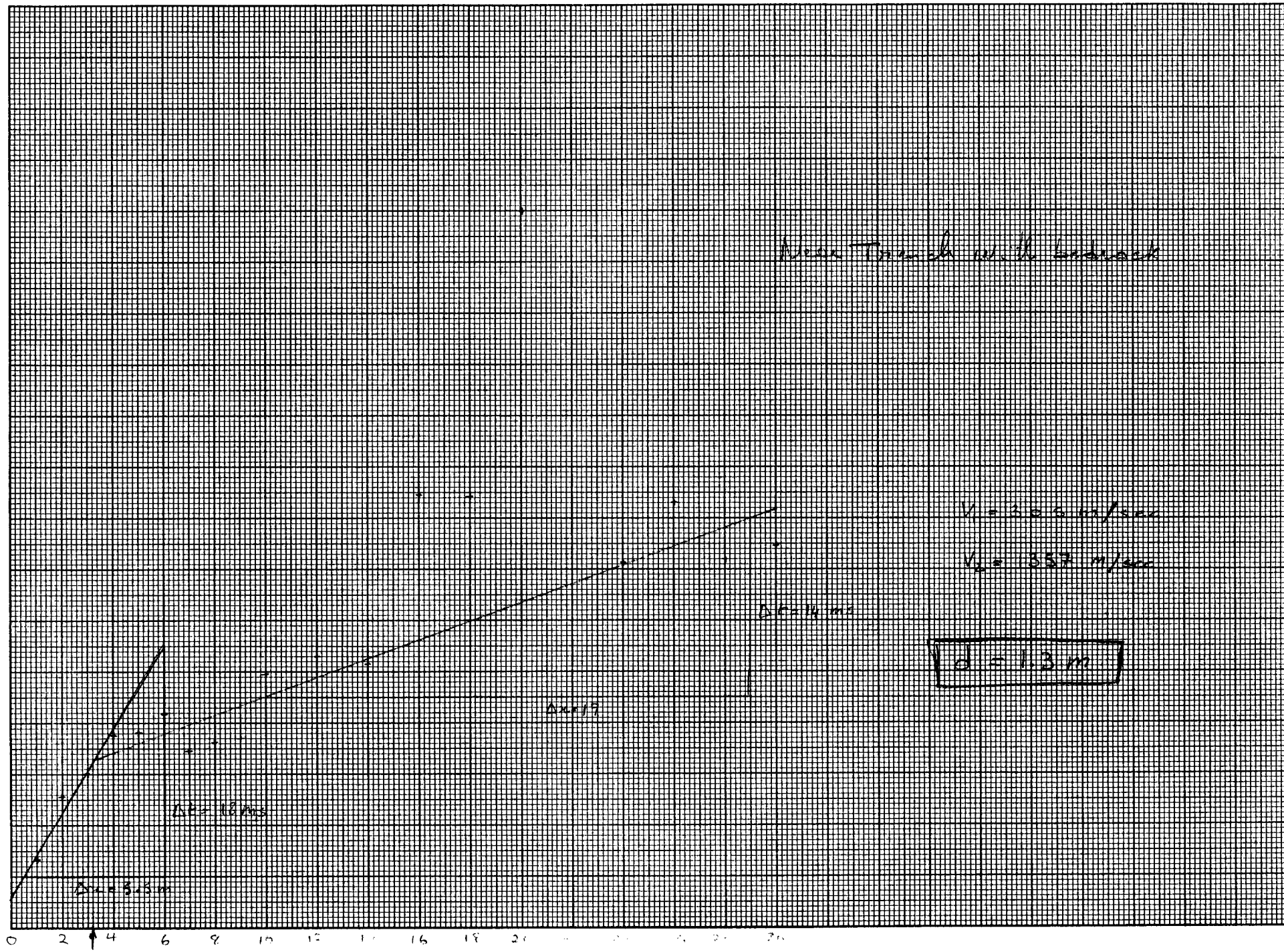


461510

K&E 10 X 10 TO THE CENTIMETER 18 X 25 CM KEUFFEL & ESSER CO. MADE IN U.S.A.

TIME (ms)  
↓

Area Track with bedrock



$V_1 = 3.5 \text{ m/sec}$   
 $V_2 = 557 \text{ m/sec}$

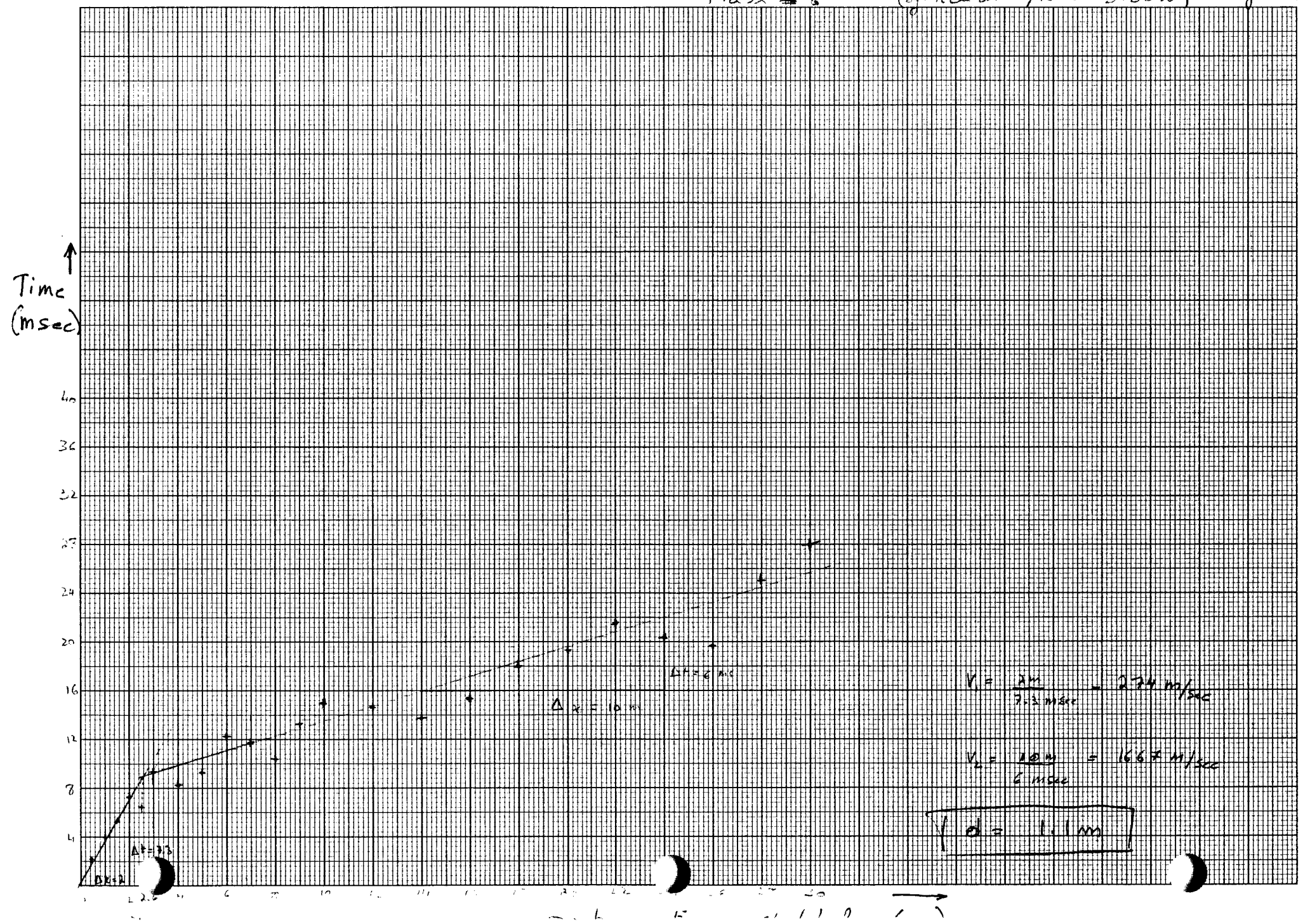
$d = 1.3 \text{ m}$

0 2 4 6 8 10 12 14 16 18 20 22 24 26 28

$x_c = 3.2 \text{ m}$

← Distance (m) →

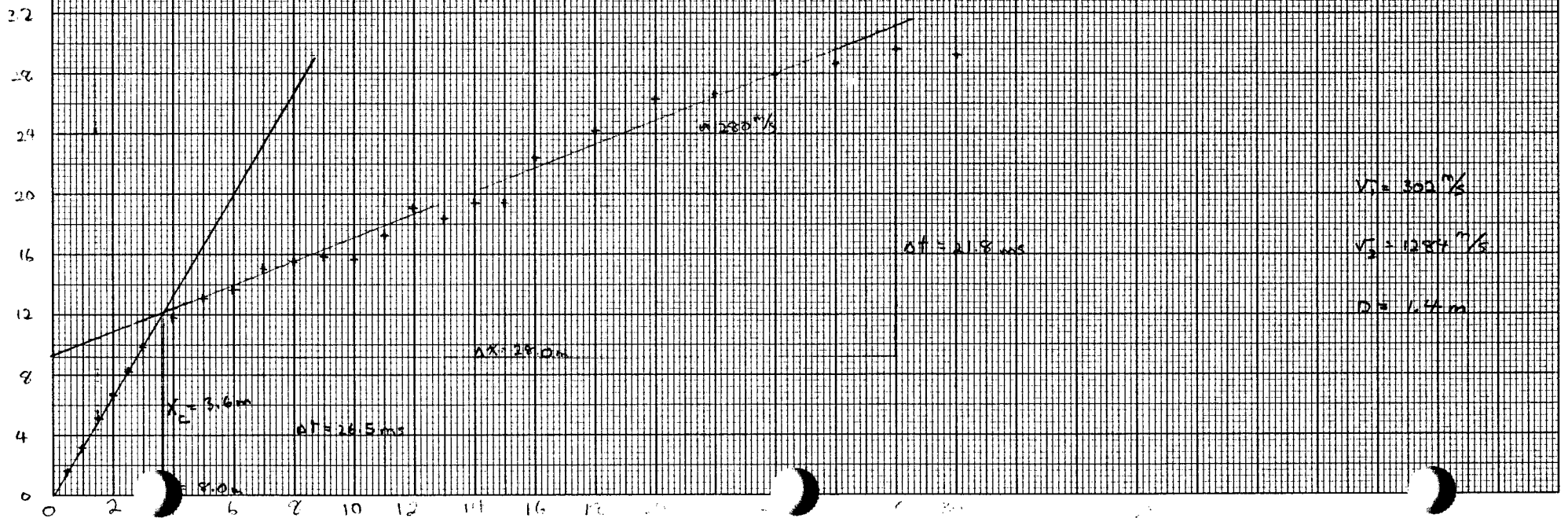
Trial # 5 (by Trench 990 N 3430 W) June 29



TRIAL #7 -

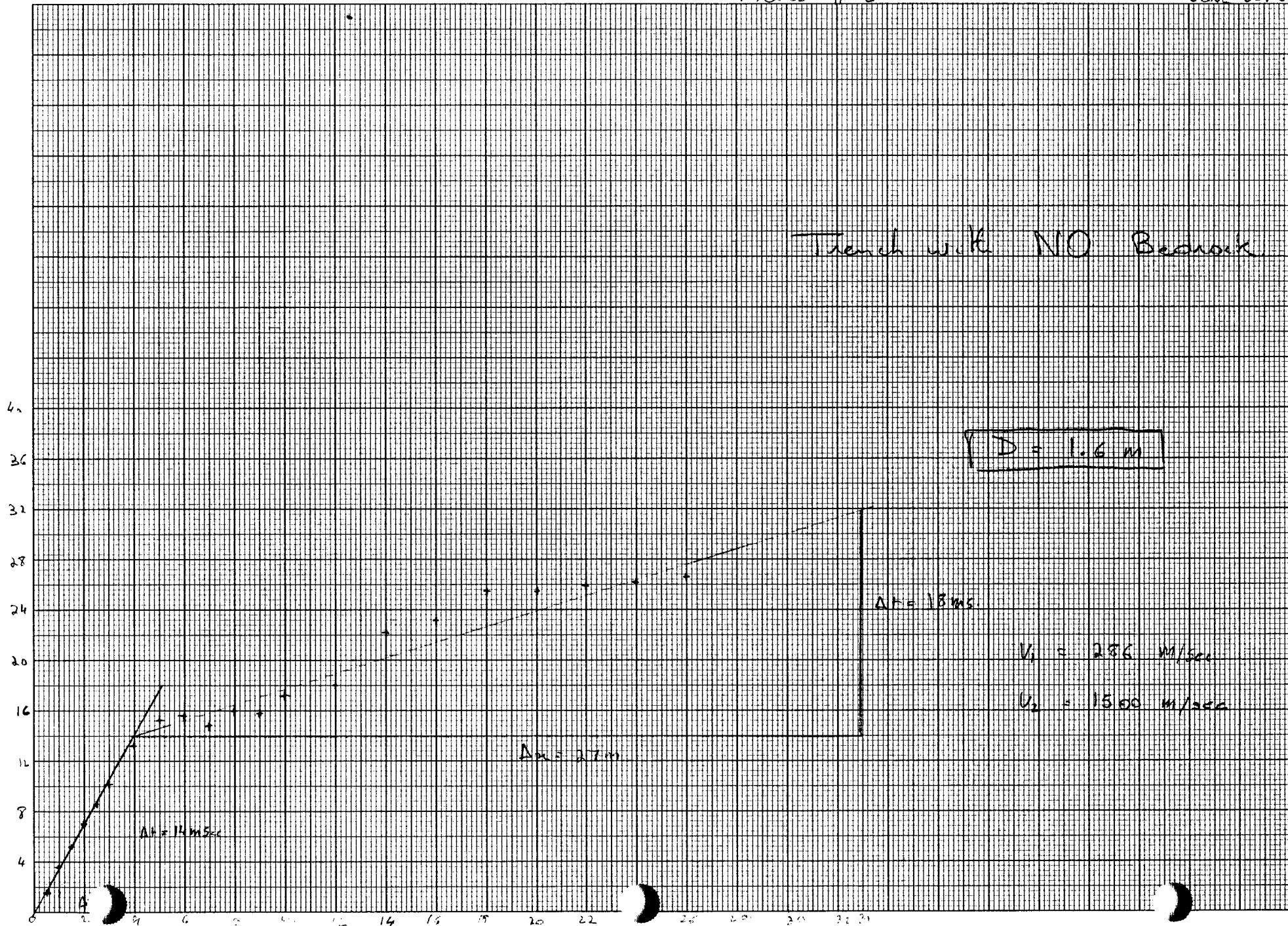
JUNE 20/69

Trench with NO Bedrock



Trial # 8

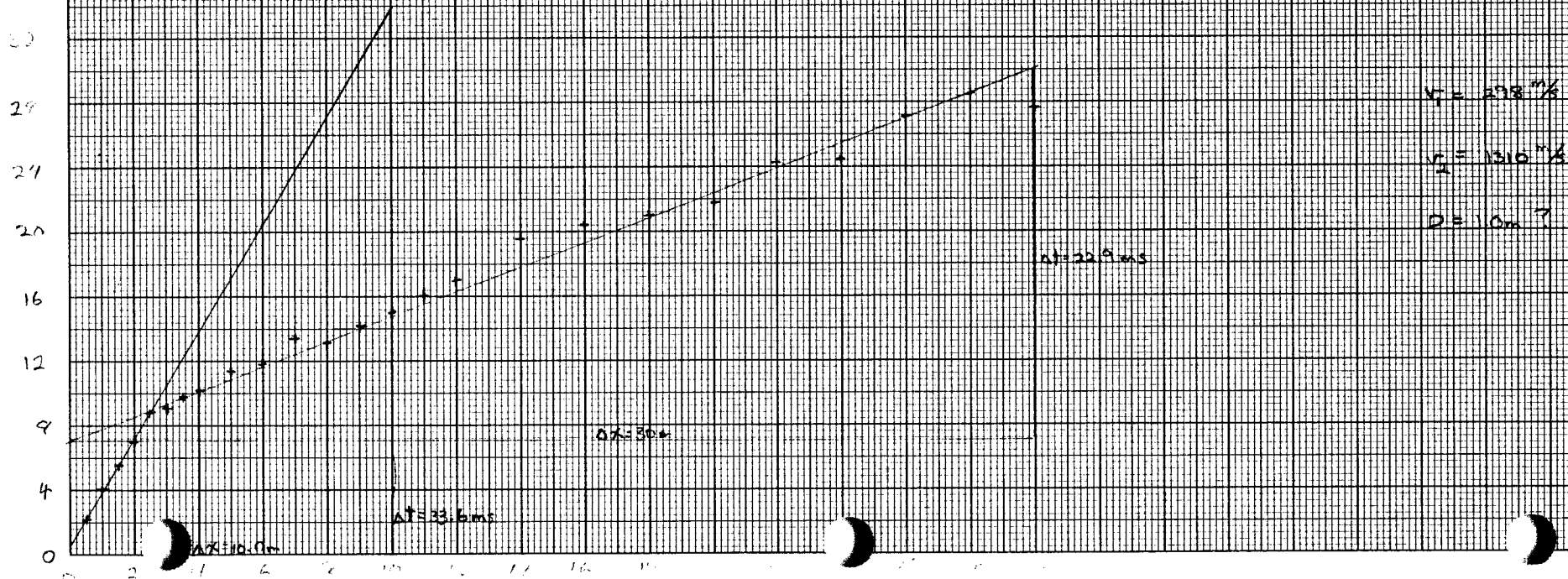
JUNE 30/67



TRIAL #7

JUNE 30/69

Trench with berlock (1.5-2m)



JUN-27/87

ZONE 4 - SEISMIC #1

3 layers - case :  $D_1 = \frac{X_{c1}}{2} \sqrt{\frac{V_2 - V_1}{V_2 + V_1}}$

$D_2 = 0.8 D_1 + \frac{X_{c2}}{2} \sqrt{\frac{V_3 - V_2}{V_3 + V_2}}$

$D_3 = 1 m$

$D_4 = 4 m$

Time (msec)

40

36

32

28

24

20

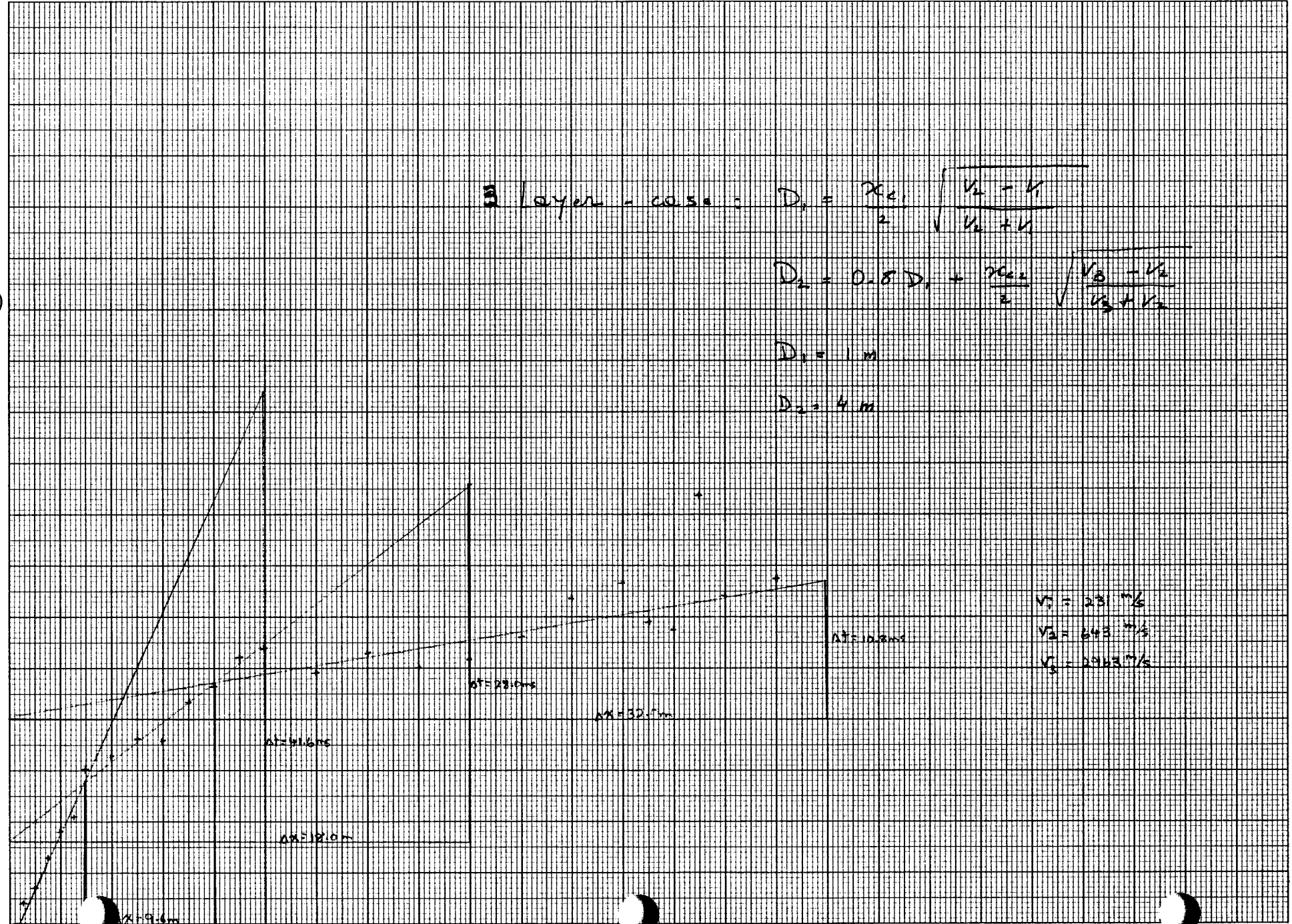
16

12

8

4

0



$V_1 = 231 \text{ m/s}$

$V_2 = 643 \text{ m/s}$

$V_3 = 2943 \text{ m/s}$

$K=9.6m$

$K=18.0m$

$K=32.0m$

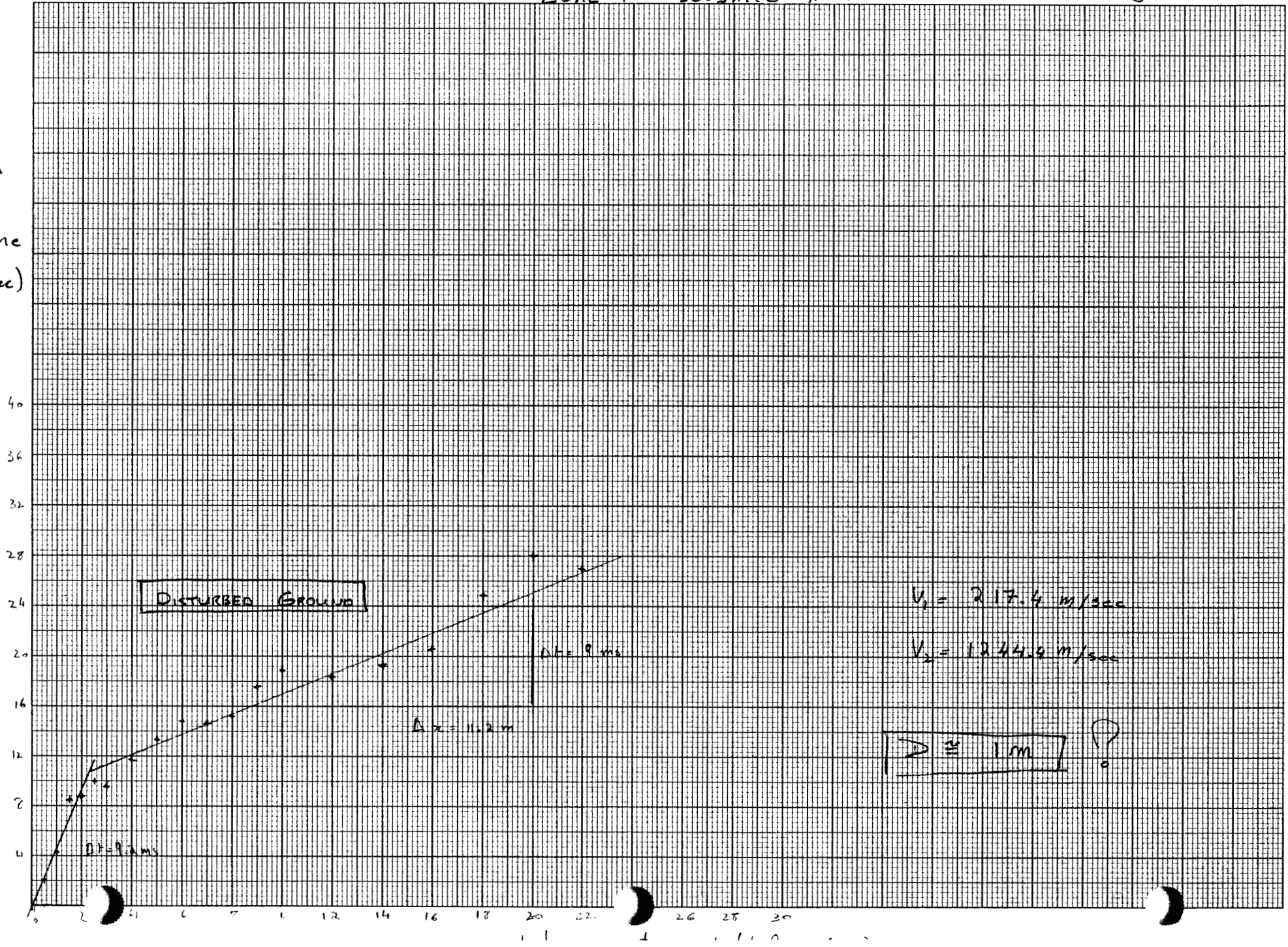
AT=10.2ms



Zone 4 - seismic # 2

June 29

↑  
 Time  
 (m sec)



ZONE 4 - SEISMIC LINE #3

JUN 29 / 89

↑  
 Time  
 (msec)

3 Layer - case

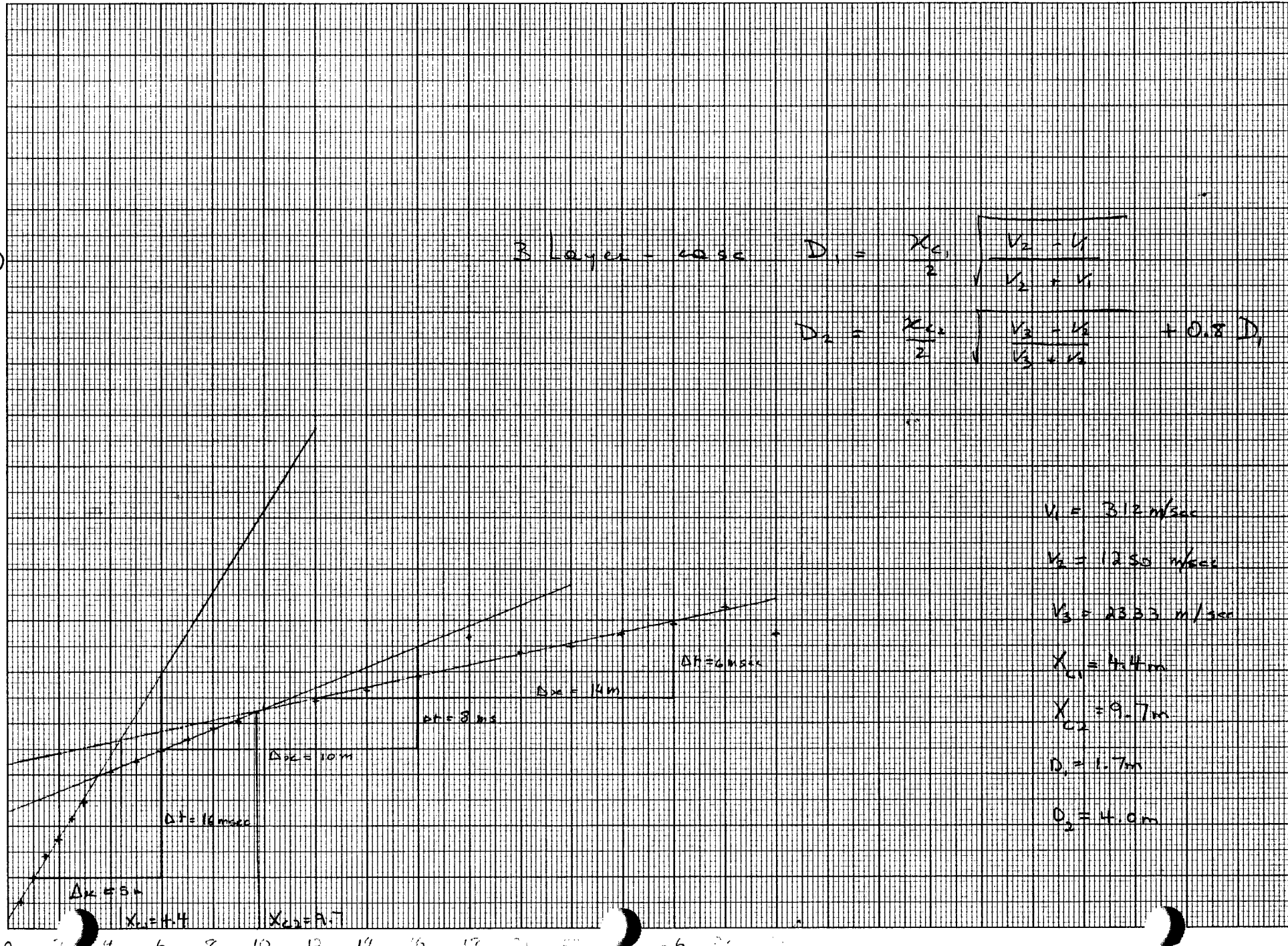
$$D_1 = \frac{X_{C1}}{2}$$

$$\sqrt{\frac{V_2 - V_1}{V_2 + V_1}}$$

$$D_2 = \frac{X_{C2}}{2}$$

$$\sqrt{\frac{V_3 - V_2}{V_3 + V_2}} + 0.8 D_1$$

40  
 36  
 32  
 28  
 24  
 20  
 16  
 12  
 8  
 4  
 0



$$V_1 = 312 \text{ m/sec}$$

$$V_2 = 1250 \text{ m/sec}$$

$$V_3 = 2333 \text{ m/sec}$$

$$X_{C1} = 4.4 \text{ m}$$

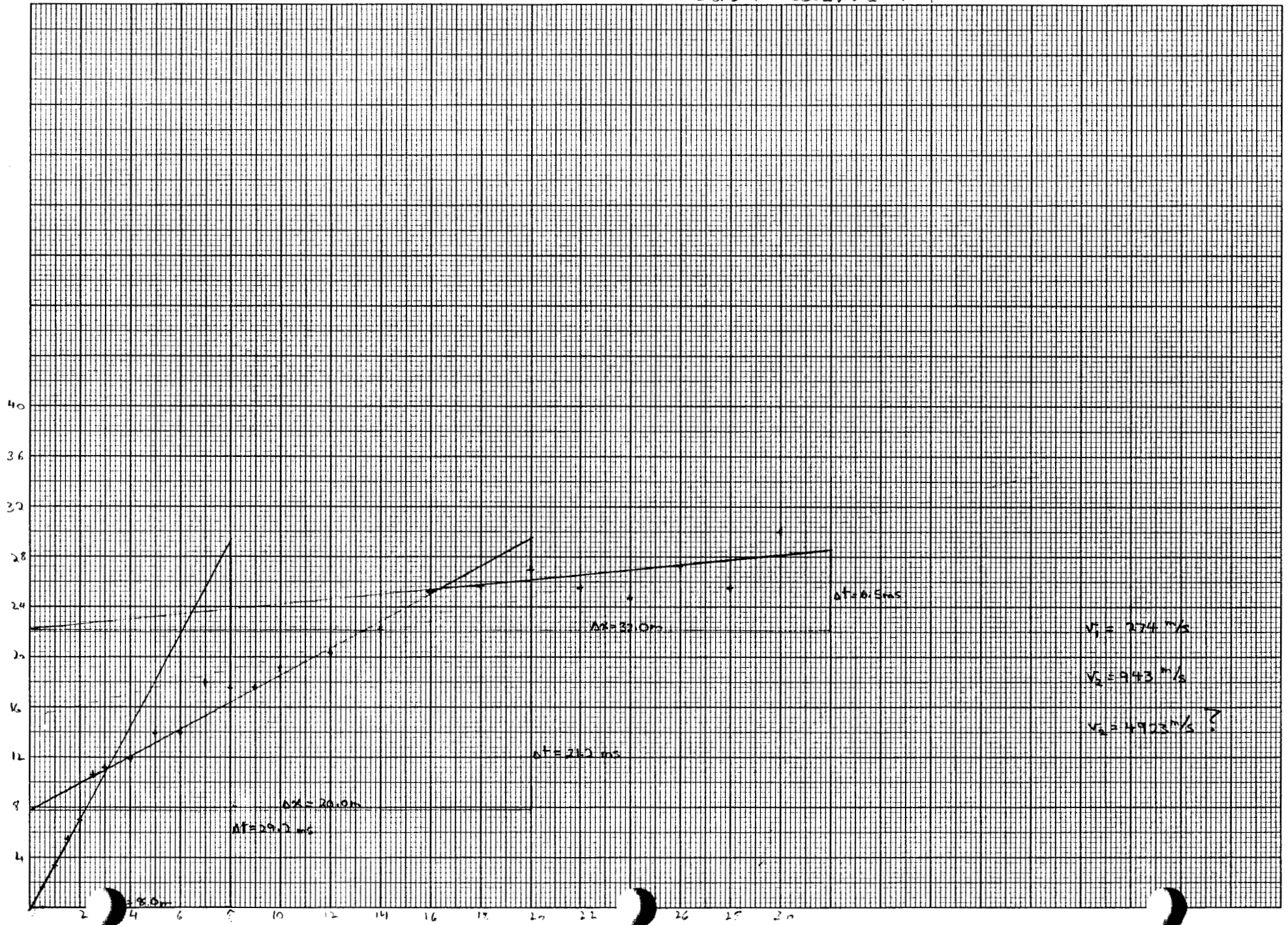
$$X_{C2} = 9.7 \text{ m}$$

$$D_1 = 1.7 \text{ m}$$

$$D_2 = 4.0 \text{ m}$$

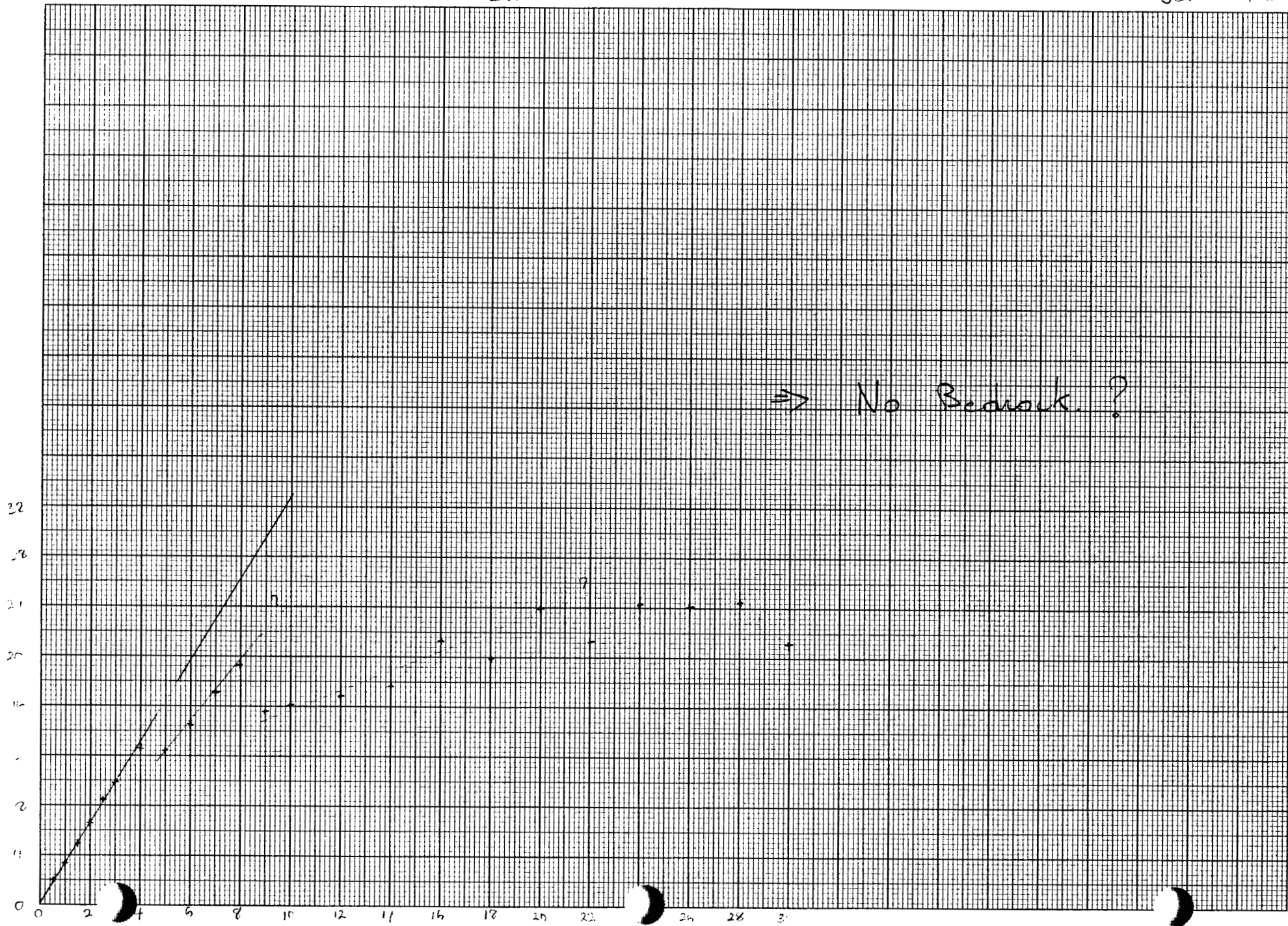
Zone 4 sensor # 4

June 29 / 89



ZONE 4 - SEISMIC #5

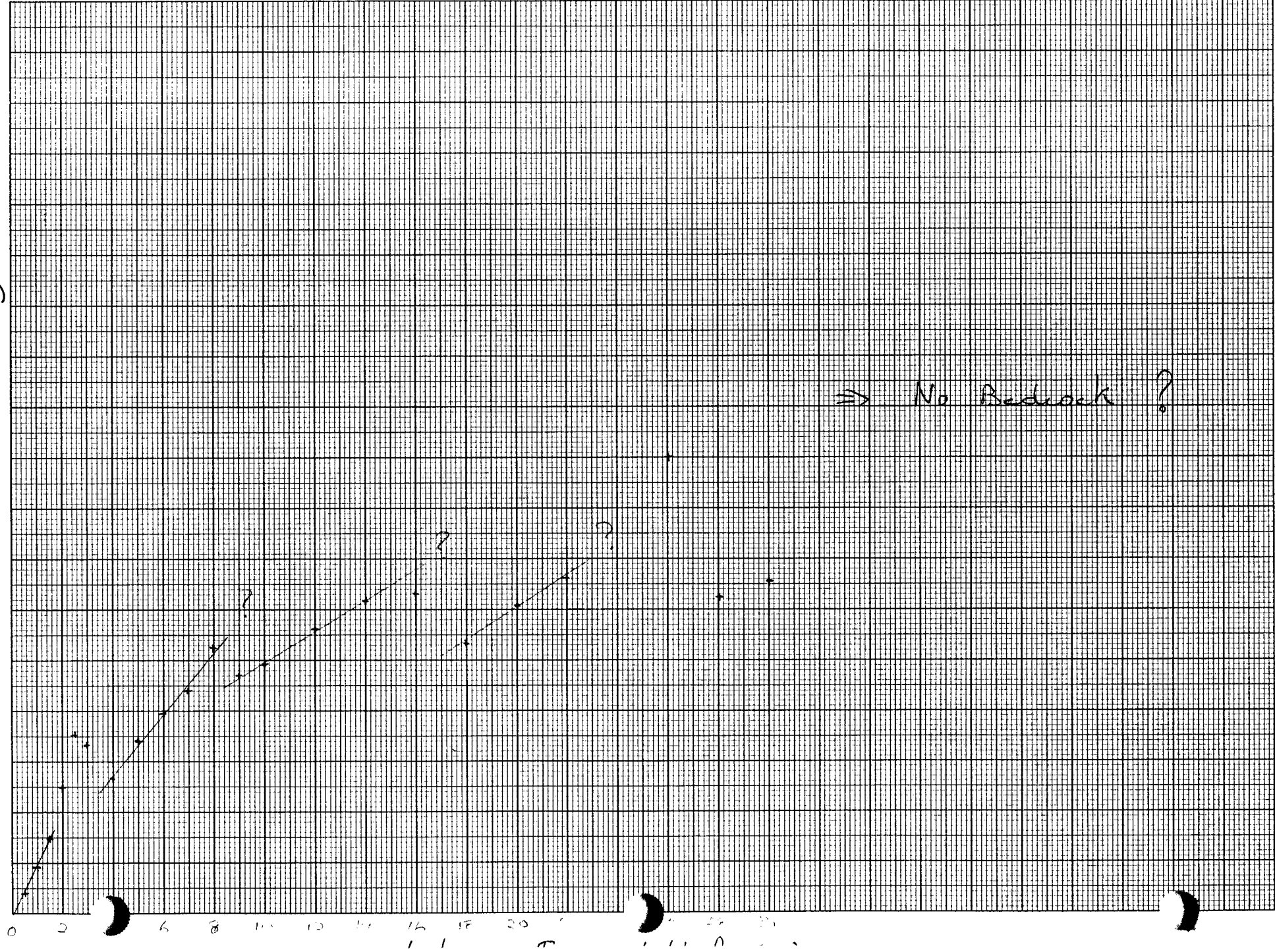
JUNE 29/77



ZONE 4 - SEISMIC #6

JUNE 29/89

↑  
nc  
(Sec)



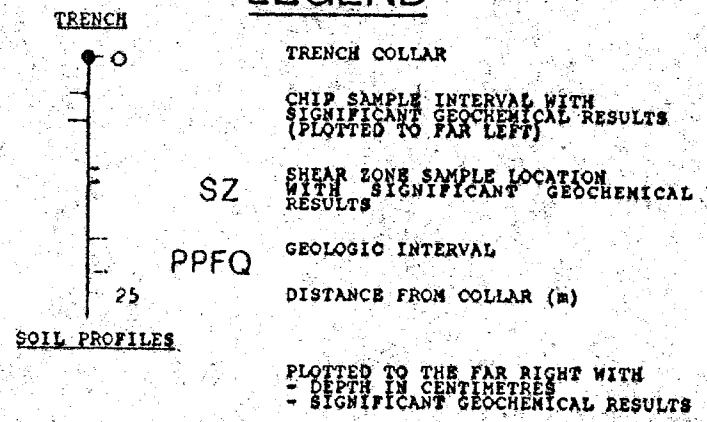
**APPENDIX IX**  
**Contour Resistivity**  
**and**  
**Chargeability Pseudosections**

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

19,420

Part 2  
of 2

LEGEND



ROCK TYPE CODES

- CGGN : COARSE-GRAINED BIOTITE GNEISS
- FAUL : FAULT OR SHEAR ZONE
- GRAN : GRANITE PEGMATITE
- OVBN : OVERBURDEN
- PPFQ : PORPHYRITIC QUARTZ-FELDSPAR MONZONITE
- QBGN : PLAGIOCLASE-QUARTZ-BIOTITE GNEISS

FIGURE 19. TRENCH PLAN: TR3228E

DATA FILE:

POSTED DATA	
ASSAYS	ROCK TYPE
CU	PGI
ZN	RI
AS	

PLACER DOME INC.

DRAWN NEM  
DATE 89:11:07  
SCALE 1:250

SPRING PROJECT '89  
EAST ZONE AREA

NO. PLATE

