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REPORT ON DIAMOND DRILL PROGRAM AND METALLURGICAL TESTWORK J&L PROPERTY, BRITISH COLUMBIA NTS 82M/8E

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December, 1989

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1. <u>SUMMARY</u>

This report summarizes the existing data base on the J&L desposit located near Revelstoke, B.C., including results of a drilling, bulk sampling and metallurgical program carried out by Equinox Resources Ltd. from November, 1988 to May, 1989 under an option agreement with Pan American Mineral Corp.

The J&L property contains a significant arsenical gold-zinc deposit with minor silver and lead credits. The deposit has a surface strike length in excess of 3.3 km and vertical extent in excess of 0.5 km while still open in all directions developed to date.

Considerable work has been carried out to date on the property, including 116 underground drill holes, 1,012 m of drifts, 100 m of raises and extensive surface and metallurgical work. Equinox's program was designed to place the higher grade ore zones into proven and probable reserves and to develop a metallurgical flowsheet using drill hole composites. Only the 1988-89 drill data is presented in detail in this report.

Due to the sucess of the Equinox drilling and metallurgical program, a conceptual mining and milling study was completed to enable a determination of mineable reserves. The study indicates that a good potential exists for the development of an operating mine in the near future on the J&L deposit. It is recommended that work proceed into pilot plant metallurgical testwork and then development of additional reserves in order that a production decision may be achieved in the near-term.

The Main Zone of the J&L deposit comprises a "vein" or sheet-like massive sulphide body of remarkable continuity within a highly deformed shear zone in phyllite and limestone of the Cambrian Hamill Group. The Main Zone has an average strike of 143° , an average dip of 55° and an average width of 2.7 m. Numerous other untested mineralized zones exist on the property of which the A & E and Roseberry are the best known.

Undiluted geological reserves in the Main Zone have been calculated at 808,100 tonnes proven and probable grading 7.2 g/t Au, 65.7 g/t Ag, 5.2% Zn, 2.57% Pb and 4.7% As, and 669,800 tonnes possible (50 m beyond probable ore zones) grading 8.8 g/t Au, 58.3 g/t Ag, 4.2% Zn, 2.2% Pb and 4.5% As. Only a small portion of the total mineralized zone has been developed to date and considerable potential exists to expand reserves. Possible reserve estimates by BP-Selco and Noranda are in excess of 10,000,000 tons though these are purely hypothetical and the true reserves could be significantly larger or smaller.

Metallurgical testwork has confirmed the amenability of the ore to upgrading using coarse gravity techniques. Rejection of approximately 50% by weight of the feed with less than 5% of the metal values was proven on bulk sample material.

The flowsheet evolved from drill composite testwork done by Lakefield Research involves selective lead and zinc flotation at fine grinds. Arsenic rejection to levels below 1% are achievable in the zinc concentrate, but at the expense of zinc recovery. Lead concentration facilitates low arsenic zinc concentrates but is likely to be only partially saleable due to arsenic levels. NSR calculations show offshore container sales of lead concentrate generate more revenue per tonne but successful pressure leaching and straight cyanidation tests on the concentrates showed only slightly lower NSRs and were used in all projections.

Both the arsenopyrite concentrate or bulk zinc tails are amenable to pressure leaching with high recoveries (90-95%) of gold and moderate (55%) recoveries of silver. The proposed flowsheet utilizes bulk tails for feed to the pressure leach circuit because higher overall gold recoveries are obtained with minimal impact on capital and operating costs. The production of a non-acid generating tailing is also obtained.

The ore zone exhibits clean (low arsenic) banded sphalerite in specific areas most notably the east end, and around section 10500. When present this material readily produces high grade zinc concentrates with a low iron content and metal recoveries of more than ninety percent. Table 1 illustrates the average metallurgical balance.

	Assay					Dis	tributi	lon		
	tonnes	Au g/t	Ag g/t	Zn %	РЬ %	Аз %	Au %	Ag %	2n %	РЬ %
Mining Reserve	532,430	7.83	62.3	4.94	2.29	4.67				
Lead Concentrate	15,925	21.05	1,082.0	9.13	50.00	4.50	8.1	52.1	5.6	65.6
Zinc Concentrate	34,970	5.37	85.0	54.00	1.42	0.90	4.5	9.0	72.2	4.1
Doré -Au (oz.)	106,000						79.8	18.4		
Doré -Ag (oz.)	195,000	ļ								

TABLE 1 METALLURGICAL BALANCE

2. INTRODUCTION

This report summarizes results of a 1988-89 exploration program carried out by Equinox Resources Ltd. under an option agreement with Pan American Minerals Corp. on the J&L polymetallic arsenical gold deposit located in southeastern British Columbia. The report also reviews previous activities on the property.

Equinox's program (Phase I) attempted to place higher grade ore zones into the proven and probable ore reserves categories by underground diamond drilling from three existing crosscuts. Metallurgical testwork was conducted on all drill hole composites using a standard flowsheet to determine the response. In addition, four bulk samples were taken (three underground) representative of the major ore types for a Phase II pilot metallurgical program if Phase I was successful.

3. LOCATION, ACCESS AND SETTING

The property is located along and north of Carnes Creek, approximately 32 air km north of the town of Revelstoke (see Figures 1 and 2), at latitude $51^{0}17$ 'N and longitude $118^{0}08$ 'W.

Access is provided by approximately 35 km of paved road (Highway #23), and then a 10 km all-weather road to the property. Helicopter services is also available from Revelstoke. A rough four-wheel drive road and several overgrown walking trails are found within the property.

Maximum relief in the area of the property is 2.349 m (3.050 to 701 meters). The J&L adits are found at 830 meter elevation and the 986 elevation respectively, and are accessible by road and/or trail. Access throughout most of the property is difficult and slow. The bedrock controlled valley slopes reach 30 to 40 degrees and are densely covered with rotting cedar and hemlock trees. Locally, windfall, deadfall, alders, devils club, stinging nettles and second growth are extensive. Treeline is approximately the 1.980 meter elevation and permanent glaciers are found above 2.286 meters. The property is drained on the south and east by Carnes and McKinnon Creeks and on the west by Kelly Creek.

The winters are long and relatively mild with snowfall from 1 to 4 meters. The summers are moderate with an average rainfall of 65 cm/year and temperatures ranging from 16 to 30 degrees centigrade.

4. PROJECT HISTORY

- 1865 Placer gold discovered in Carnes Creek
- 1896 Surface showings staked by prospectors "Jim" and "Lee" (hence "J&L" property). Property staked on behalf of Roseberry Consolidated Mines.
- 1897-1900 The Roseberry Zone was extensively developed by the Carnes Creek Consolidated Co. Ltd., with 272 meters of drifting and cross cutting on three levels.
- 1898 Active placer operations on Carnes Creek. As many as five companies involved.
- 1912 The original Main Zone discovery was made on the property.
- 1924-1927 The property was owned by Mr. E.E. McBean of Revelstoke. Optioned to Porcupine Goldfields Development and Finance Co. Ltd: completed 43 meters of drifting on two adits.
- 1927 The road along the Columbia River was advanced to Carnes Creek.





- 1929 A short adit was driven on the A & E claims which were owned by A. Kitson and the E. McBean estate.
- 1933 Work continued on the A & E zone involving two open cuts and advancing the adit.
- 1934 T.E. Arnold acquires the J&L claim group. The claims were converted to crown grants.
- 1935-1946 Raindor Gold Mines optioned the property and completed 152 m of drifting on the 986 level, two shallow shafts and several trenches. In 1946 log cabins were erected which are still standing.
- 1962-1967 Property optioned to Westairs Mines Ltd., which conducted exploration and development in a joint venture with East Ventures Ltd., and Stairs Exploration & Mining Co. Ltd.. Work included geological mapping, prospecting and trenching of the J&L, A & E and Roseberry zones. Westairs Mines Ltd. reported to have completed 306 meters of diamond drilling on the Roseberry and A & E targets. In addition, a 98 meter drift was driven north of the old workings on the A & E property and the 1830 elevation adit were driven to 81 meters to facilitate drilling. This activity was serviced by a helicopter from a base camp on Burke Creek.

Westairs completed 272 meters of drifting on the J&L property at the 830 level. The middle vein was drifted on initially and then a cross cut was driven to intersect the main vein. A total of 183 meters of underground AX diamond drilling was completed from the level. Other work included the construction of 12.4 km. of road to the site from the Columbia River Highway.

- 1979 Stelladoro Mines Ltd. optioned the property. A program of exploration and development was recommended but not pursued.
- 1980 Pan American Minerals acquired the property under lease from T. Arnold.
- 1981 BP-Selco Ltd. optioned the property.
- 1982-1985 BP-Selco Ltd. actively explored and developed the main J&L zone including:
 - road construction
 - 1,095 km airborne EM survey
 - extensive mapping, surface geochemistry and geophysics
 - 671 meters of underground drifting on vein on the 830 level and 353 meters of crosscutting for drilling
 - 2,640 meters underground drilling in 64 holes
 - major metallurgical investigation at Lakefield Research
- 1986-1987 Noranda Mines optioned the property and completed the collection of 28-200kg underground samples for metallurgical

testing at Noranda Research. J.D. Williams reported on ore reserves and potential.

1987-1988 Pan American Minerals completed 1,904 meters of underground diamond drilling from the previous crosscuts. Four raises were driven on ore for approximately 30 meters each. Extensive metallurgical investigations were completed by several laboratories. A new portal was driven for 165 meters width trackless equipment and an Alimak raise was advanced for approximately 30 meters towards the 987 level.

- 1988 Equinox Resources optioned the property from Pan American Minerals and completed diamond drilling, bulk sampling and metallurgical studies as described herein in detail.
 - 3,000 meters of underground drilling in 32 holes
 - 3 bulk samples from section 818.5-821.5, 637-639 and 460-462.5 totalling 270 tonnes
 - metallurgical testwork on drill core composites
 - gravity test bulk sample from previous raise material

5. <u>CLAIM DESCRIPTION AND OWNERSHIP</u>

The J&L property is comprised of (A) 10 crown granted mineral claims, patented claims or lots, whose taxes are assessed by the Vernon Assessment District; (B) eight single unit mineral claims, and (C) 24 multi-unit claim blocks consisting of 349 mineral units. The property totals 367 mineral claim units. All of the claims are located on National Topographic Series map sheet 82M8 - Salmon Arm. The status of these claims was recently reviewed and Figure 3, Claim Map represents the general layout of these claims. Note that one crown grant claim (M-56 L-4815) is currently not part of the property. Appendix A details the claim numbers and names.

The crown granted claims are owned by Mr. T. E. Arnold of New Jersey, U.S.A. and are under lease to Pan American Minerals Ltd. subject to 11% net profits royalty after capital, interest and operating costs payback. All other claims are held 100% by Pan American and are subject to the Arnold agreement. The only other agreement in effect on the above mentioned claims is the Equinox-Pan American agreement.

For assessment purposes the exploration activities have been preportioned between the Arty 1 and Tom claim groups. Approximately 8.4% of the drilling was completed on the L14827 crown grant and costs of exploration have been distributed accordingly. Also on this unit one bulk sample of the three was taken. Consequently, 33% of the costs of the sampling and metallurgical investigation are applied towards it.

The remaining work was completed on crown grants L14825 and L14823.



6. <u>REGIONAL GEOLOGY AND MINERALIZATION</u>

The regional area of the J&L property occupies the Goldstream slice of the Selkirk Mountain Range and lies in the hanging wall of the Columbia River fault zone, a major north-north-westerly structural feature. The Goldstream slice includes rocks of the Hadrynian Horsechief Creek Group. Lower Cambrian Hamill Group and Badshot Formation and presumed lower Paleozoic Lardeau Group. Within the slice at least two phases of isoclinal folding and subsequent faulting have occurred, resulting in structural complexity and obscured stratigraphic relationships. The stratigraphy over the property area consists of folded and faulted Lardeau, Mohican and Hamill metasediments and metavolcanics and Badshot limestones.

The Lardeau Group consists of graphite-quartz phyllite with minor chloritegraphite and graphite phyllite. The phyllites contain minor amounts of pyrite and iron oxide and local calcareous lenses and fracture fillings.

The Hamill Group comprises of quartzite, chlorite-quartz, quartz-chlorite, chlorite-seicite-quartz, and quartz sericite phyllite. The quartzites are clean to dirty, massive to well foliated and contain minor calcareous fracture fillings; especially near the contact with the Badshot limestones. The anticlinal Hamill stratigraphy pinches on surface to the northwest of the Roseberry grid, where exposures of Badshot limestone are found.

The Badshot Formation overlies the Mohican Formation and is predominantly medium to fine grained, recrystallized, grey banded limestone with local medium-grained calcite veinlets. Calcareous sericite phyllite occupies a number of shear zones and host numerous, but erratic tan weathering quartz-carbonate lenses.

The overlying Mohican Formation is a calcareous phyllite unit which is comprised of limestones, tan weathering dolomites, calcareous grits and phyllites, and minor calcareous quartzites.

In the region several prospects are known for lead-zinc, copper, and gold mineralization (refer to Figure 4). The only significant producers in the area were the Mastodon (SE of J&L) and Goldstream (NW of J&L) deposits.

The Mastodon Highland Bell mine produced 6,112 ounces of silver, 90.2 tons of lead, 2,956 tons of zinc, and 12.1 tons of cadmium from 31,900 tons of ore. Most of the production occurred in the early 1950's. The ore bodies are replacement of calcareous rocks, principally by sphalerite and are at or near the contact of limestones and green phyllites. All rocks are isoclinally folded and strongly sheared. The property is currently held by Teck Corporation.

The Goldstream deposit is located approximately 43 km northwest of the J&L and has a diluted reserve of 3.5 million tons grading 3.5% copper and 2.5% zinc. The continuous bed of massive and disseminated sulphides is hosted at or near the contact of grey green phyllites and metamorphic limestone. Production from 1980 to 1983 was 492,700 grading 3.4% copper and 2.2% zinc. The property has recently been purchased from Noranda.

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siltatone, and quartzite; dark grey limy slate, rusty weathering buff slate; dark grey and rusty siliconus	lee tee
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G Quartz-mica schist, micaceous quartzate, graphitic quartz- sericite schist, andalusite schist, minor aplite and pegmatite (may be part of Mount Ida Group) Intermittent river and lake	
F Granitic pneiss and phundhati pegnatile, paragneiss; Fa, quartz-feidspar-biotile paragneiss, quartzite, marble calc-silicate rocks; Fb, migmatite complex composed of quartz-feidspar-biotile paragneiss containing sillimanite, lineated leucogranite, aplite, pegmatile; foliated hornblende-biotile granodiocite, granite-gneiss, amphibolite, calc-silicate rocks, nebulitic pneiss and agmatite; Fe, marble Contours (interval 500 feet) Base-map compiled and drawn by the Surveys and Mapping Branch, 1964, Fe, marble D D Fe, marble GI D D Fe, marble Fe, marble Base-map compiled and drawn by the Geological Survey of Canadh D	10 - 00 - 00 - 00 - 00 - 00 - 00 - 00 -
E Quartz-biotite-feldspar paragneiss (commonly containing garnet and sillimanite), micaceous quartzite, amphibulite, calc-silicate rocks, all abundantly locul with pegmatite; Mean magnétic declination 23*32' East decreasing 3.3' annually. Readings vary from 23*00' in the SE corner to 24*00' in the SE corner of the map-area B C 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 00 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10 10	<u> </u>
Quartz-biotite-feldspar schist and paragneiss (commonly containing garnet, kyanite, and sillimanite), amphibolite, harnblendic gneiss, quartzite, marble, cale-silicate rocks; minor pegmatile; Da, marble; Db, quartzite	G/
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A locally pegmatitic, through biotite > hornbiende granite- and granediorite-gneiss ato quartz diorite-gneiss and amphibolite and variously occurring as banded gneiss, streaky gneiss, veined gneass, wavy and folded gneiss Geological boundary (defined, approximate or 2880 moth).	10 10 10 10 10
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7. PROPERTY GEOLOGY AND MINERALIZATION

The main sulphide zone is hosted by northwest trending, east dipping metasediments of the upper part of the Lower Cambrian Hamill Group. These rocks include a cyclical sequence of quartzite, quartz-rich schists and phyllites and chlorite-sericite schists and phyllite. Within these cycles are bands of grey to carbonaceous limestone. It is at or near the contacts of limestone and metasediments that the main zone occurs. The zone can be described as a massive sulphide sheet confined within a highly deformed shear zone. The structural feature is very persistent with the mineralization consisting of bands, lenses and stringers of massive sulphides comprising pyrite, arsenopyrite, sphalerite and galena. On surface the zone has been traced for a strike length of 3.34 km and is still open to the north and at depth. Width of mineralization varies from millimeters on surface, up to 12 m in diamond drill holes.

The property's geology and location of mineralized areas is presented in Figure 5. Other principal mineralized zones on the J&L property include the A & E and Roseberry zones. The A & E zone is found on the north-east slope of Roseberry Mountain (elevation. 2,167 m). The property was developed in the 1920 - 30s with drifting at the 1,830 elevation and open cuts along the outcrops. The average of samples from underground, surface and talus grabs was 5.8 g/t Au, 188.6 g/t Ag, 10.3% Zn, and 4.6% Pb. Arsenic values were not reported.

The A & E mineralization comprises two sulphide zones at the contact of limestone and schist. The maximum reported width from BP-Selco's reports is 2.74 meters of massive sulphide and 6.1 meters of disseminated material. Zone "A" has been traced for 503 meters horizontally and 183 meters vertically. Average grade from BP-Selco's work was 3.4 g/t Au, 284.9 g/t Ag, 12.3% Zn, and 7.5% Pb. Zone "B" is approximately 122 meters west of the above zone and parallels it. The average grade is 8.6 g/t Au, 91.9 g/t Ag, 8.4% Zn and 1.8% Pb. The A & E zone represents a very attractive exploration target.

The Roseberry Zone is located north-west of the J&L and west-south-west of the A & E zone. It is noted in old government reports that gold values were encountered across 15 meters, with 1.5 meters of high grade sulfides. During 1962 - 67, Westairs Mines Ltd. conducted an exploration program of geological mapping, prospecting and diamond drilling. However the work was not filed for assessment purposes and is not available for review.

Other mineralized showings on the J&L property include the North Zone which may represent the continuation of the Main Zone and was uncovered by BP-Selco. It occurs north of McKinnon Creek alone the southern slopes of Roseberry Mountain. In 1984, the discovery of 44 mineralized occurrences extended the north zone by 1,150 meters. Most of the mineralization consisted of arsenopyrite and pyrite with minor amounts of scorodite and jarosite hosted by quartzites and phyllites of the Hamill Group. The host rocks were well sheared and fractured with a strong to moderate sericite halo. To date only low values have been returned in the sampling. Assays indicate arsenic/gold mineralization with low values of zinc and lead. The most significant results are 3.1 g/t Au, 20.8 g/t Ag, 0.09% Zn, 1.88% As and 0.27% Pb over 2.1 meters true width. No surface diamond drilling has been completed on this target.



Other zones of interest include the East Zone, the Far East Zone, and the Copper Zone, all in close proximity to the trace of the Main Zone on Goat Mountain.

The East Zone is located approximately 10 meters north east of the Main Zone on surface and consists of discontinuous arsenical bands and lenses. Assay results, through surface sampling only, were low grade.

The Far East Zone is located approximately 800 meters north-east of the Main Zone on surface and comprises two occurrences within folded Hamill Group quartzites. The mineralization consists of disseminated scorodite, jarasite, arsenopyrite, and pyrite. The lower showing was traced for 27 meters along strike with a maximum thickness of 3.5 meters. Assay results, however, are poor to date.

The Copper Zone is located approximately 150-180 meters southwest of the Main Zone and was investigated by BP-Selco in 1982. The zone comprises narrow sulphide mineralization in sheared and fractured quartzites. A narrow arsenopyrite band was traced for 225 meters horizontally and 80 meters vertically, returning low assay results.

A map compiled from Westairs Mining Ltd. data in 1965-66 indicates four parallel mineralized zones north east of the Main Zone at the 830 meter level. The zones vary in thickness from 3.0 meters to .2 meters, however the source and reliability of the data is not known.

8. UNDERGROUND GEOLOGY AND MINERALIZATION, J&L MAIN ZONE

The Main Zone is hosted in a highly deformed shear zone which exhibits a close spatial relationship to the contact between phyllite and limestone units of the Hamill Group. The hanging wall geology generally comprises quartzites, sericitic and chloritic phyllites and sericitic schists. Local lenses and discontinuous narrow bands of carbonaceous limestones also occur in the hanging wall sequences. The quartzite units consist of clean to dirty, creamy white quartzites which are fine grained, massively to weakly banded, with minor sericite along foliation planes. The sericitic and chloritic phyllite are moderately to well foliated. Banding is poorly developed in the phyllites and bedding cannot be recognized with assurance. Although the chlorite component is minor in the unit its presence is presumed responsible for the distinctive green hue. Certain sections of phyllite have been bleached, due to sericitization and to a lesser extent silicification. Because colour appears to have little or no stratigraphic significance and because of structural complexities, lithological subdivisions of the phyllites have not been made.

The carbonaceous to grey banded limestone is found as the structural footwall to the Main Zone over most of the economically significant portion. The carbonaceous unit is fine to medium grained, dark grey to black in colour, and often contain fracture filling carbonate. This unit is weakly to moderately foliated but often intensely jointed. The grey band limestones are medium grained, moderately to well banded recrystallized rocks. At approximately 10740 E to 10820 E, the limestone unit pinches out and the Main Zone lies within sericitic-quartz to sericite phyllites and schist. This feature is observed vertically, as the limestone units are absent above the drift and thicken below the drift. Structurally, underlying the limestone units are an intercalated sequences of quartzites, phyllites, schists and argillaceous metagreywackes.

The mineralized zone underground has an average strike of 143° (132-150°) and an average dip of $55^{\circ}E$ (45-65°). The mineralization consists of remarkably continuous bands, lenses, stringers and pods of massive and disseminated sulphide comprising pyrite, arsenopyrite, and lesser amounts of sphalerite and galena. Other minerals noted in minor to trace amounts include chalcopyrite, pyrrhotite, tetrahedtrite and lead antimony sulphosalts.

At least two distinct types of mineralization have been noted. The first comprises massive bands and lenses in a sericitic shear zone. The sulphides frequently have a "milled" texture consisting of fine to coarse grained, rounded to subrounded pyrite, arsenopyrite and/or quartz in a very fine grained sulphide matrix. This milled feature is interpreted as a mylonite texture developed by reworking within a structurally active shear zone. The mineralized zone bifurcates occasionally into two to four subzones separated by 1 to 10 meters of waste comprising usually sericititic phyllite and schists, and more rarely Lateral sulphide zonation varies considerably for the massive limestone. component in the area from 10330 to 10900 E. However, generally the footwall portions have lower grade gold, zinc and lead values and higher Au:As ratios. This trend is notable reversed in the area below the 350 crosscut, where high values of gold, zinc, lead and arsenic are indicated in the footwall zone.

The second distinct type of mineralization comprises narrow stringers and fine to medium disseminations of principally sphalerite, with lesser amounts of galena and pyrite and very little arsenopyrite. This is best observed underground at the eastern face of the 830 drift where the host limestone is saturated with abundant, red to honey, fine grained sphalerite. This mineralization comprises the hanging wall portion of this area below the level and represents a "clean" zinc, metallurgically. However, although it can reach widths of 6-10 meters it appears to have limited extent both along strike and vertically (50 x 80 meters). This type of mineralization may be similar to the Mastodon ore bodies located SE of the J&L where limestone and dolomite have been replaced by sphalerite.

The massive sulphide zones frequently exhibit complex deformation textures and variations of sulphide zonation may be a result of intense folding with the shear zone. At least five phases of deformation have been recognized, of which the D_3 is the most significant. The F_3 folds are near isoclinal and trend NW-SE with variable plunges. The D_3 deformation has produced significant synmetamorphic faults-tectonic slides as observed on a small scale structures in the undergound workings. A penetrative S_3 foliation has been transposed on all rock types and is the most readily recognizable feature. Pervasive sericitic alteration is extensively developed within the shear zone and its immediate hanging wall and footwall sequences. The sericitic envelope ranges from 2.0 to 20 meters wide. Intense structural deformation has obscured stratigraphic relationships and no distinct primary features have been observed. Appendix B presents six cross sections of the deposit illustrating the geology.

9. GEOLOGICAL SETTING AND GENESIS

Based on observations of core and undergound workings and on previous studies the following comments regarding geological setting of the J&L Main Zone can be summarized:

- 1) The Main Zone is sheet-like in geometry with an average dip of 55° and a strike of 143° .
- 2) It occurs in a shear zone with persistent continuity in both the vertical and horizontal component. (3.34 km surface strike indicated, 0.5 km vertically from surface exposure to deepest drill hole.)
- 3) It has been intensely deformed resulting in tectonic banding and brecciated and mylonitic textures of the sulphide zones. Areas of thickening and thinning may be related to tectonic mechanisms.
- 4) Pervasive, sericitic alteration occurs in the shear zone and the host rocks. The sericitic alteration is strong to intense in the Main Zone.
- 5) The shear zone is closely related to the contact between limestones and phyllites. However, it does deviate from this contact on several occasions with little variation in mineralization.
- 6) The Main Zone represents an unusual and distinct polymetallic deposit with significant values of gold and zinc and lesser values of silver and lead.

The structural and metallurgical complexities make genesis of the deposit unclear. Debate continues over whether the J&L was originally a vein or seclex type deposit. Based on our observation we favour a model based on metal bearing fluids emplaced along the foliation planes of a major structural feature. This shear zone is in close proximity to the contact between phyllites and limestone, but not limited to it. The entire sequence was subsequently intensely deformed, resulting in variations in thickness and metallurgy of the mineralization. The possibility exists of two or more distinct mineralizing periods, however more study is required to determine this. The other mineralized zones on the property require further investigation to establish their economic significance, and to determine whether they have a structural or depositional genesis.

10. <u>1988-89 PROGRAM</u>

The recent exploration program was initiated on November 15, 1988 and consisted of two principal field components, underground diamond drilling and bulk sampling for metallurgical purposes.

11. UNDERGROUND DIAMOND DRILLING

Underground diamond drilling from the previously established crosscuts was completed on the 350,670 and 820 crosscuts. Drilling started on November 25, 1988 and was completed on February 19, 1989. A total of 32 holes were drilled comprising 2,984.9 meters. The longest hole was hole 88-32 at 145.5 meters, with the average length being 93.3 meters. R.J. Fry Ltd. of Delta, B.C. was responsible for all drilling, rehabilitation and mining activities. Drilling was completed using a modified electric drill and a compressed air driven BBU-2 drill. Appendix B details the drill program results including a drill hole location map. The holes were logged and mineralized sections split with the core stored in racks at the site. A small amount of core was sawn with a diamond saw. This method is recommended for future drilling as a better split is obtained.

12. BULK SAMPLING

The second activity involved bulk sampling of ore material at three specific underground locations which indicated differing metallurgical properties. This involved drilling off the ore zone which was then blasted and mucked into 45 gallon metal barrels. On two occasions preliminary side slashes were required in order to sample the entire width of the zone. The bulk samples were taken at section 10818.5-10821.5, 10637-10639, and 10460-10462.5. A fourth bulk sample for gravity testwork was taken from a 500 tonne stockpile mined out during Pan American's raise program. The bulk samples were then transported to Lakefield Laboratories at Lakefield, Ontario.

13. <u>GEOLOGICAL RESERVES</u>

Undiluted geological ore reserves in the proven and probable category from the 10,330 section to 10,930 section and from elevation 710 m to 860 m are calculated at 808,100 tonnes grading 7.2 g/t Au, 65.7 g/t Ag, 5.2% Zn, 2.5% Pb and 4.7% As. (Imperial equivalents are 890,500 tons at 0.21 oz/t Au and 1.92 oz/t Ag).

Undiluted geological ore reserves in the possible category (50 m beyond probable ore) are calculated at 669,800 tonnes grading 8.8 g/t Au, 58.3 g/t Ag, 4.2% Zn, 2.2% and 4.3% As.

Total combined geological ore reserves for all categories are calculated at 1,477,900 tonnes grading 7.9 g/t Au, 62.2 g/t Ag, 4.7% Zn, 2.3% Pb, and 4.5% As.

14. METHODOLOGY AND CATEGORIES

The geological ore reserves were calculated using a combination of diamond drilling data and chip sampling from the 830 m drift. The strong continuity of the Main Zone allows sectional interpretation of an area from 10,330 East to 10,990 East, and from an approximate elevation 735 to 855 m. The drill density in this area averages 25-35 m centers. Where continuity is good the ore zone was interpreted on sections at 10 to 25 m intervals and the ore blocked out into mineable blocks at 25 m elevation levels. A minimum horizontal mining width of 1.6 m was required with a minimum gold equivalent grade of 6.0 g/t. Specific area blocks were weighted with respect to the grades of all metals and the data entered into a spreadsheet computer program for compilation. All areas calculated by the sectional method are classified as probable or proven, and are considered to have a high degree of confidence. Some areas such as those fully drifted on, and where the vein has been tested by raising have sufficient sampling to be classified as proven.

Drifting on the 830 level was generally on vein, however it often did not delineate the full extent of the zone. BP-Selco completed considerable drilling of short holes on either side of the drift to approximate spacings of 20 m to determine the full width. These holes, along with chip sampling of the face were utilized to establish complete data points at 15-20 m spacings on the level for use both in sectional calculations and in polygon construction where applicable.

Fringe areas beyond the limit of the sectional compilation, or areas without proven continuity, were determined by polygon construction and were designated as probable reserves. Polygons were taken to the midpoint if less than or equal to 25 m. In areas of limited data the polygons were closed off using a 25 m influence vertically, horizontally and diagonally.

For all the possible category, an additional 50 m range of influence was applied on the fringe diamond drill data. The four specific areas were calculated weighted accordingly. The possible reserves are heavily influenced by the high grade intersections indicated in the lower 350 section area.

Areas for both the sectional method and the polygons were determined and checked using trigonometric and/or a planimeter. A longitudinal section of the area of ore reserves has been compiled to illustrate the areas of sectional and polygonal calculations (refer to Fig 6).

A specific gravity of 3.45 was used for most of the deposit. In areas of "clean zinc" a specific gravity of 3.00 was used, based on previous testwork. A study of variance in specific gravity within the deposit is in progress.

All assay values were utilized without a cutting factor. The frequency at high grade values (eg. over 34.3 g/t or 1 oz/t) is relatively low.



15. DETAILED GEOLOGICAL RESERVES

Table 2 summarizes the results of the detailed calculation by section areas and category.

		· · · · · · · · · · · · · · · · · · ·					1
Reserves			Au	Ag	Zn	Pb	As
Туре	Area	Tonnes	g/t	g/t	%	%	%
Proven & Pr	obable						
Sectional	350	123,350	11.1	67.2	3.8	1.9	6.5
	500	116,400	4.7	71.0	5.4	2.2	3.3
	670	150,140	8.4	63.5	4.4	2.9	5.8
	800	162,130	4.3	53.3	6.9	2.3	3.2
	Total	552,020	7.0	62.9	5.2	2.4	4.7
Average horizor	stal width 3.0) meters					
Polygonal	350	38 120	aa	72 9	Q 1	20	55
1 orygoniai	500	32,990	64	76.4	6.8	2.0	3.0
	670	54 520	85	84.8	53	3.0	J.⊈ / Q
	800	130 500	67	64.0	5.0	2.0	4.0
	Total	256 130	75	716	<u> </u>	2.0	<u>4.5</u> 1.8
Average horizon	ital width 2.4	meters	7.0	71.0	0.1	2.1	4.0
5							
Total Prove	n and Pro	bable					
	350	161,470	10.8	68.5	3.6	1.9	6.3
	500	149,390	5.1	72.2	5.7	2.4	3.3
	670	204,660	8.4	69.2	4.6	2.9	5.5
	<u>800</u>	292,630	5.4	58.3	6.1	2.4	4.0
	Total	808,150	7.2	65.7	5.2	2.5	4.7
Possible	350	201,700	13.6	60.1	4.1	2.2	6.1
	500	75,800	4.6	92.7	9.3	3.7	3.2
	670	129,900	7.9	68.9	4.5	2.6	5.2
	800	262,400	6.7	41.6	2.7	1.6	2.9
	Total	669,800	8.8	58.3	4.2	2.2	4.3
Average horizon	ital width 2. ϵ	i meters					
All Categorie	s						
0	350	363,100	12.4	63.8	3.9	2.1	6.2
	500	225,200	4.9	79.1	6.9	2.8	3.3
	670	334.600	8.2	69.1	4.6	2.8	54
	800	555.000	6.0	50.4	4.5	2.0	3.5
Gran	d Total	1,477,900	7.9	62.2	4.7	2.3	4.5
Average horizon	tal width 2.7	meters					

TABLE 2SUMMARY OF GEOLOGICAL ORE RESERVES



16. METALLURGY

The property has been extensively tested metallurgically by previous operators, in particular BP-Selco and Pan American Minerals. Previous testwork samples were derived from back sampling in the drifts, or raise material.

Processes tested to date include:

Concentrate Processes:	Pb-Zn differential flotation Pb-Zn bulk flotation
Gold Processes:	Pressure Leaching Bio Leaching Arseno Process Cashman Process

Historically, difficulties have been encountered with Pb-Zn flotation with respect to arsenic content in cleaner concentrates. The variability of the mineralogy further complicates this problem as occasional samples produced relatively clean concentrates yet the identical flowsheets on other samples showed poor recoveries.

Gold extraction using any of the gold processes except the Cashman process were successful with greater than 90% extraction. The Cashman process testwork failed mechanically so gold extraction rates are unknown.

17. <u>TESTWORK-PHASE I</u>

Equinox's 1988-1989 metallurgical program had many targets which included mineralogical determination flowsheet development and concentrate grade determinations.

Testwork conducted by Lakefield Research commenced with batch flotation tests and sink-float tests on drill holes. Pressure leaching tests on composites of arsenopyrite concentrates, lead concentrates and bulk tails were also undertaken. A bulk sample (-50mm) was subjected to gravity separation at a 3.0SG to produce a size versus metal deportment curve. Drill holes were then composited based on location, mineralogy and metallurgical response and subjected to optimizing conditions and finally locked cycle tests. Pressure leaching testwork for pilot plant design was also included in Phase I work.

18. FLOTATION

The batch flotation flowsheet allowed predictions of metallurgy to the overall deposit when used in conjunction with mineralogy. This was aided by testwork on 6 selected drill holes from BP and Pan American drilling. As a result of the testwork four major rock types were identified and are shown:

Type Description

- 1 Arsenopyrite: gold rich, little or no base metals
- 2 Arsenopyrite: Massive Sulphide: high arsenic, (+5%) Au, Pb, Zn
- 3 Massive Sulphide-Arsenopyrite: lower arsenic, (-5%) Au, Pb, Zn
- 4 Sphalerite Massive Sulphide: high zinc, low arsenic (-2%)

The flotation results are described by location in the ore zone. In general the arsenopyrite-massive sulphide milled zones produce dirty lead and zinc concentrates while the sphalerite zone produces clean concentrates. The presence of the sphalerite is not restricted to one area and frequently can carry the arsenopyrite zones where the ore mix is discreet bands of gold-rich arsenopyrite and sphalerite.

<u>10350 Zone</u>

The upper levels (above 780 meter) produce dirty concentrates and are classified as composite A material. The lower levels with high gold and arsenic produce zinc concentrates with arsenic value from .25 to 1.90% on batch work. This area demonstrates clean banded sphalerite with arsenopyrite and is classed as composite B ore.

10500 Zone

Both the upper and lower levels of this zone have clean zinc ore. In particular hole 84-02 indicates the possibility of another zinc zone with a hanging wall of 4.5 m of 8% zinc and 0.1% arsenic. Batch testwork gave ranges of 0.5 to 1.5% arsenic on areas tested and is classified as composite B ore.

10670 Zone

This material in all areas is classified as composite A ore. The ore throughout is milled arsenopyrite - massive sulphides. The base metal values are largely contained in a fine grained arsenopyrite matrix.

10820 Zone

This zone is the thickest on the property and demonstrates a sphalerite zone which pinches out and is replaced by the arsenopyrite-massive sulphide ore. The sphalerite ore produced values in both lead and zinc concentrates of less than 0.1% arsenic and is composite B ore. The arsenopyrite-massive sulphide lower levels (below 750 m) are similar to 670 material and are classed as composite A ore.

The results on individual drill holes are shown in Table 3, Appendix D with the flowsheet illustrated in Figure 8. Typical results for the two composites are:



Fig. 8

	Co	mposite A					
Assay Recovery							
	% Pb % Zn % As P						
Zinc Concentrate	3	40	3-6	5	70-85		
Lead Concentrate	40	10	5-10	7	10		
	Co	mposite B					
	Average	Assay		Rec	overy		
	% Pb	% Zn	% As	Pb	Zn		
Zinc Concentrate	2	53	0.1-2	1-5	75-92		
Lead Concentrate	45	3	0.1-5	70-85	8-10		

TABLE 3 COMPOSITE RESULTS

19. GRAVITY TESTWORK

The bulk sample taken from raise material mined in December 1987 by Pan American Minerals was to confirm previous gravity testwork results obtained by Lakefield Research which indicated high weight reduction with small metal losses. The sample material was weathered due to surface oxidation from 1987 to January 1989, and was shipped frozen which accounts for the fine size consistency. Table 4 summarizes the results while Table 5, Appendix D provides full details. The testwork confirmed previous results with rejection of 60% by weight of +.65 mm (1/4") material with approximately 3% metal content.

TABLE 4 SINK-FLOAT BULK SAMPLE

Wei	ght %			Ass	ays			Distribut	tion (%)	
Size of Sa	ample		Au g/t	As%	РЬ%	Zn%	Au	As	Pb	Zn
-50mm	4.7	Sink	14.4	6.39	6.03	9.23	97.6	91.3	96.1	97.7
+1.9mm	6.5	Float	.25	-44	.17	.16	2,4	8.7	3.9	2.3
	11.2	Feed.	6.19	2.94	2.63	3.97	100.0	100.0	100.0	100.0
-1.9mm	17.5	Sink	10.3	8.32	5.96	8.65	97.8	93.1	96.4	95.3
+ .65mm	25.6	Float	.16	.42	.13	.29	2.2	6,9	3,6	4.7
	43.1	Feed	4.28	3.63	2.51	3.68	100.0	100.0	100.0	100.0

Drill core sink-float testwork (Table 4. Appendix D) supported these results although results with large weight rejection (i.e. floats) suffered from entrainment of metal values due to both the volume and the particle size (-10 mesh) of test material. Weight reductions reached 75% with 2% metal loss.

Bulk sample testwork is intended to confirm projection of approximately 50% weight reduction and 3% metal losses during production.

20. ASSAYING

Drill holes were split and assayed in individual components by Acme Analytical of Vancouver. Drill hole composite assays were calculated by multiplying meterage times assays, with no attempt to consider specific gravity variations. This has been the practice followed by all previous operators. The ore zone is typical of a massive sulphide deposit as bands, lenses, and stringers together with the arsenopyrite vein make up the ore zone. Interbedded in this mixture is internal dilution largely of a schist nature with a specific gravity of less that 3.0 as compared to arsenopyrite's S.G. of 6.8. Improved assay results were expected on a composite basis.

The remaining splits were sent to Lakefield Research for metallurgical testwork. After crushing the specific drill core to minus 10 mesh, composite head samples were cut. Table 1, Appendix D presents composite values from Lakefield. These composites were rechecked by both Chemex and Acme with good agreement.

Utilizing polygonal reserve estimates centered on drill holes the average grade variation for the principal metals was:

Au	Ag	<u>Zn</u>	<u>Pb</u>
+9.0%	+5.0%	+5.0%	+5.0%

It is felt that this grade increase is due to specific gravity variations within the mineralized zone and was expected. Although the higher grades were not used in this study, future drilling results should be composited for true assay values.

Table 5 summarizes Acme's results and identifies drill holes with composite data for all testwork. All reserve estimates are based on arithmetic assays (i.e. Acme) although arsenic levels in concentrate are based on actual testwork. Assay comparisons can be checked by comparing Lakefield data (Table 1, Appendix D) with Acme data using common composite numbers.

Drill Hole Composite # Section Au g/t Au g/t Ag $9/t$ Pb $2n$ As 4 1 630 15.3 116 4.0 6.0 5.6 9 2 650 11.7 50 2.4 3.5 7.8 8 3 650 19.5 84 3.0 4.4 11.8 7 4 630 26.3 157 5.9 6.9 13.1 6 5 630 16.0 58 2.6 3.7 9.3 10 7 650 3.4 21 1.0 1.8 3.3 11 8 630 7.3 9.0 3.6 6.4 4.8 27 9 730 9.5 120 5.4 7.3 5.3 28 10 730 3.4 54 2.4 2.8 2.7 29 11 670 7.3 118 6.5 11.7	Сог	nposite Sam	estwork	Head Assay (Acme))	
41 630 15.3 116 4.0 6.0 5.6 92 650 11.7 50 2.4 3.5 7.8 83 650 19.5 84 3.0 4.4 11.8 74 630 26.3 157 5.9 6.9 13.1 65 630 17.8 115 4.9 8.8 10.9 56 630 16.0 58 2.6 3.7 9.3 107 650 3.4 21 1.0 1.8 3.3 11 8 630 7.3 90 3.6 6.4 4.8 27 9 730 9.5 120 5.4 7.3 5.3 28 10 730 3.4 54 2.4 2.8 2.7 29 11 670 7.3 118 6.5 11.7 3.6 18 12 780 7.1 71 3.1 7.7 5.6 30 13 670 11.3 35 1.15 0.8 8.5 14 14 780 4.45 43 1.7 4.5 3.2 21 19 880 4.77 31 1.07 2.5 2.9 21 19 880 3.77 31 1.07 2.5 2.9 21 19 880 8.65 97 3.1 6.4 7.0 22 18 880 3.77	Drill Hole #	Composite #	Section	g/t Au	g/t Ag	% Pb	% Zn	% As
9265011.7502.43.57.88365019.5843.04.411.87463026.31575.96.913.16563016.0582.63.79.31076503.4211.01.83.31186307.3903.66.44.82797309.51205.47.35.328107303.4542.42.82.729116707.31186.511.73.618127807.1713.17.75.6301367011.3351.150.88.514147804.45431.74.53.231157007.01102.24.65.324169103.8612.02.93.525179108.15582.44.64.922188603.77311.072.52.921198804.8431.61.75.720208808.05973.16.47.0322137016.45551.96.69.3222368.033.1423.04.	4	1	630	15.3	116	4.0	6.0	5.6
8365019.5843.04.411.87463026.31575.96.913.16563017.81154.98.810.95663016.0582.63.79.31076503.4211.01.83.31186307.3903.66.44.82797309.51205.47.35.328107303.4542.42.82.729116707.31186.511.73.618127807.1713.17.75.6301367011.3351.150.88.514147804.45431.74.53.231157007.01102.24.65.324169108.15582.44.64.922188803.77311.072.52.921198804.8431.61.75.720208808.05973.16.47.0322137016.45551.96.69.32223706.17240.72.04.41 FW233503.1423.04.7<	9	2	650	11.7	50	2.4	3.5	7.8
7463026.31575.96.913.16563017.81154.98.810.95663016.0582.63.79.31076503.4211.01.83.31186307.3903.66.44.82797309.51205.47.35.328107303.4542.42.82.729116707.31186.511.73.618127807.1713.17.75.6301367011.3351.150.88.514147804.45431.74.53.231157007.01102.24.65.324169108.15582.44.64.922188803.77311.072.52.921198804.8431.61.75.720208808.05973.16.69.32223706.17240.72.04.41 FW233503.1423.04.72.332268809.551516.27.75.626279305.73941.82.9	8	3	650	19.5	84	3.0	4.4	11.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	7	4	630	26.3	157	5.9	6.9	13.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	6	5	630	17,8	115	4.9	8.8	10.9
107 650 3.4 21 1.0 1.8 3.3 11 8 630 7.3 90 3.6 6.4 4.8 27 9 730 9.5 120 5.4 7.3 5.3 28 10 730 3.4 54 2.4 2.8 2.7 29 11 670 7.3 118 6.5 11.7 3.6 18 12 780 7.1 71 3.1 7.7 5.6 30 13 670 11.3 35 1.15 0.8 8.5 14 14 780 4.45 43 1.7 4.5 3.2 31 15 700 7.0 110 2.2 4.6 5.3 24 16 910 3.8 61 2.0 2.9 3.5 25 17 910 8.15 58 2.4 4.6 4.9 22 18 880 3.77 31 1.07 2.5 2.9 21 19 880 4.8 43 1.6 1.7 5.7 20 20 880 8.05 97 3.1 6.4 7.0 3 21 370 16.45 55 1.9 6.6 9.3 2 22 370 6.17 24 0.7 2.0 4.4 1 FW 23 350 40.4 141 6.2 12.6 15.6 1 HW <td< td=""><td>5</td><td>6</td><td>630</td><td>16.0</td><td>58</td><td>2.6</td><td>3.7</td><td>9.3</td></td<>	5	6	630	16.0	58	2.6	3.7	9.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10	7	650	3.4	21	1.0	1.8	3.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	11	8	630	7.3	90	3.6	6.4	4.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	27	9	730	9.5	120	5.4	7.3	5.3
2911 670 7.3 118 6.5 11.7 3.6 1812 780 7.1 71 3.1 7.7 5.6 3013 670 11.3 35 1.15 0.8 8.5 1414 780 4.45 43 1.7 4.5 3.2 31 15 700 7.0 110 2.2 4.6 5.3 24 16 910 3.8 61 2.0 2.9 3.5 25 17 910 8.15 58 2.4 4.6 4.9 22 18 880 3.77 31 1.07 2.5 2.9 21 19 880 4.8 43 1.6 1.7 5.7 20 20 880 8.05 97 3.1 6.4 7.0 3 21 370 16.45 55 1.9 6.6 9.3 2 22 370 6.17 24 0.7 2.0 4.4 1 FW 23 350 40.4 141 6.2 12.6 15.6 1 HW $23A$ 350 3.1 42 3.0 4.7 2.3 32 24 930 7.6 51.7 1.3 2.5 7.2 19 25 850 8.82 34.3 1.3 5.0 5.9 23 26 880 9.55 151 6.2 7.7 5.6 26 27	28	10	730	3.4	54	2.4	2.8	2.7
18127807.1713.17.75.6301367011.3351.150.88.514147804.45431.74.53.231157007.01102.24.65.324169103.8612.02.93.525179108.15582.44.64.922188803.77311.072.52.921198804.8431.61.75.720208808.05973.16.47.032137016.45551.96.69.32223706.17240.72.04.41 FW2335040.41416.212.615.61 HW23A3503.1423.04.72.332249307.651.71.32.57.219258508.8234.31.35.05.923268809.551516.27.75.626279305.73941.82.93.817 HW288000.40392.212.40.1417 FW28B80013.9743.77.86.615 HW298200.32.3 </td <td>29</td> <td>11</td> <td>670</td> <td>7.3</td> <td>118</td> <td>6.5</td> <td>11.7</td> <td>3.6</td>	29	11	670	7.3	118	6.5	11.7	3.6
3013 670 11.3 35 1.15 0.8 8.5 14 14 780 4.45 43 1.7 4.5 3.2 31 15 700 7.0 110 2.2 4.6 5.3 24 16 910 3.8 61 2.0 2.9 3.5 25 17 910 8.15 58 2.4 4.6 4.9 22 18 880 3.77 31 1.07 2.5 2.9 21 19 880 4.8 43 1.6 1.7 5.7 20 20 880 8.05 97 3.1 6.4 7.0 3 21 370 16.45 55 1.9 6.6 9.3 2 22 370 6.17 24 0.7 2.0 4.4 1 FW 23 350 40.4 141 6.2 12.6 15.6 1 HW $23A$ 350 3.1 42 3.0 4.7 2.3 32 24 930 7.6 51.7 1.3 2.5 7.2 19 25 850 8.82 34.3 1.3 5.0 5.9 23 26 880 9.55 151 6.2 7.7 5.6 26 27 930 5.73 94 1.8 2.9 3.8 17 HW 28 800 13.9 74 3.7 7.8 6.6 <tr< td=""><td>18</td><td>12</td><td>780</td><td>7.1</td><td>71</td><td>3.1</td><td>7.7</td><td>5.6</td></tr<>	18	12	780	7.1	71	3.1	7.7	5.6
14 14 780 4.45 43 1.7 4.5 3.2 31 15 700 7.0 110 2.2 4.6 5.3 24 16 910 3.8 61 2.0 2.9 3.5 25 17 910 8.15 58 2.4 4.6 4.9 22 18 880 3.77 31 1.07 2.5 2.9 21 19 880 4.8 43 1.6 1.7 5.7 20 20 880 8.05 97 3.1 6.4 7.0 3 21 370 16.45 55 1.9 6.6 9.3 2 22 370 6.17 24 0.7 2.0 4.4 1 FW 23 350 40.4 141 6.2 12.6 15.6 1 HW $23A$ 350 3.1 42 3.0 4.7 2.3 32 24 930 7.6 51.7 1.3 2.5 7.2 19 25 850 8.82 34.3 1.3 5.0 5.9 23 26 880 9.55 151 6.2 7.7 5.6 26 27 930 5.73 94 1.8 2.9 3.8 17 HW 28 800 13.9 74 3.7 7.8 6.6 15 HW 29 820 0.3 23 1.05 8.7 0.11 <td>30</td> <td>13</td> <td>670</td> <td>11.3</td> <td>35</td> <td>1.15</td> <td>0.8</td> <td>8.5</td>	30	13	670	11.3	35	1.15	0.8	8.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	14	14	780	4.45	43	1.7	4.5	3.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	31	15	700	7.0	110	2.2	4.6	5.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	24	16	910	3.8	61	2.0	2.9	3.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	25	17	910	8.15	58	2.4	4.6	4.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22	18	880	3.77	31	1.07	2.5	2.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	21	19	880	4.8	43	1.6	1.7	5.7
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	20	880	8.05	97	3.1	6.4	7.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3	21	370	16.45	55	1.9	6.6	9.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2	22	370	6.17	24	0.7	2.0	4.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 FW	23	350	40.4	141	6.2	12.6	15.6
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1 HW	23A	350	3.1	42	3.0	4.7	2.3
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	32	24	930	7.6	51.7	1.3	2.5	7.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	19	25	850	8.82	34.3	1.3	5.0	5.9
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17 HW288000.40392.212.40.1417 FW28B80013.9743.77.86.615 HW298200.3231.058.7.0115.FW29B8203.26784.712.91.213308203.0452.35.71.912317807.71064.65.74.816328004.45341.84.22.1	26	27	930	5.73	94	1.8	2.9	3.8
17 FW28B80013.9743.77.86.615 HW298200.3231.058.7.0115.FW29B8203.26784.712.91.213308203.0452.35.71.912317807.71064.65.74.816328004.45341.84.22.1	17 HW	28	800	0.40	39	2.2	12.4	0.14
15 HW298200.3231.058.7.0115.FW29B8203.26784.712.91.213308203.0452.35.71.912317807.71064.65.74.816328004.45341.84.22.1	17 FW	28B	800	13.9	74	3.7	7.8	6.6
15.FW29B8203.26784.712.91.213308203.0452.35.71.912317807.71064.65.74.816328004.45341.84.22.1	15 HW	29	820	0.3	23	1.05	8.7	.01
13308203.0452.35.71.912317807.71064.65.74.816328004.45341.84.22.1	15.FW	29B	820	3.26	78	4.7	12.9	1.2
12 31 780 7.7 106 4.6 5.7 4.8 16 32 800 4.45 34 1.8 4.2 2.1	13	30	820	3.0	45	2.3	5.7	1.9
16 32 800 4.45 34 1.8 4.2 2.1	12	31	780	7.7	106	4.6	5.7	4.8
	16	32	800	4.45	34	1.8	4.2	2.1

TABLE 5 COMPOSITE SAMPLES FOR TESTWORK

21. PRESSURE LEACHING

Pressure leaching testwork has largely been of a scoping nature to ascertain parameters for pilot plant testwork. Parameters investigated include leach time, percent solids, oxygen pressure and temperature. Ongoing testwork is being directed at bulk tails from major drill composites (i.e. composite A & B ore) and lead concentrates and is in progress. Pressure leaching involves the use of elevated temperatures, oxygen enrichment and moderate and pressure to oxidize the sulfur component of arsenopyrite thus liberating the gold for cyanide leaching.

Table 6 summarizes the results of the first five tests which were largely performed on arsenopyrite concentrates (exception PL4, Sink material from drill hole composite; no grinding).

						Extra	iction %
Test	% Solids	Temp ^o C	Time	°2	% Oxidation	Au	Ag
PL1	20	150	4	100	89.4	53.4	14.0
PL2	15	200	2	225	98.9	92.7	4.2
PL3	15	200	1	100	78.8	95.7	57.1
PL4	10	200	1	150		49.4	11.7
PL5	15	190	1	100	64.4	94,1	53.5

 TABLE 6

 PRELIMINARY PRESSURE LEACH RESULTS

22. FLOWSHEET OPTIMIZATION

Ongoing testwork is examining both flowsheet variations and flotation reagents schemes on two composite samples. Composite A represents the arsenopyritemassive sulphide material which produced high arsenic in zinc concentrates, while composite B represents arsenopyrite-sphalerite zones.

Although the work has just begun, removing the lead first cleaner tails from the zinc circuit dropped the average arsenic content in zinc concentrate from 6.7% to 2.2% while reducing recovery from 74% zinc to 64% zinc. Metallurgical projections for revenue calculations have continued to reduce both recovery and arsenic content in concentrates.

The decision to treat bulk tails as opposed to arsenopyrite concentrate in pressure leach will facilitate arsenic rejection to concentrates as well, due to the ability to depress arsenopyrite and not have to reactivate it.

23. ACID GENERATION TESTWORK

Preliminary testwork at Lakefield has been conducted for acid generating potential on waste streams. Testwork has shown the alkaline nature of gangue material and the unlikely generation of acidic effluent from waste streams. Results to date are tabulated below (detailed test results are in Appendix E):

Sample	Acid Consuming	Acid Generating
Bulk sample $+1/4$ " flotation material	138.2 kg/t	37.7 kg/t
Arsenopyrite float tails	79.4 kg/t	43.2 kg/t

Further testwork for waste stream characterization will be conducted during pilot plant testing.

24. PROCESS DESCRIPTION

The flowsheet developed during preliminary metallurgical testwork includes:

-crushing and screening to minus .6 mm.

-heavy media preconcentration on the plus .6 mm. fraction.

-primary grinding to 80% minus 80 micron.

-lead flotation with concentrate directed to pressure leach circuit.

-zinc flotation and regrind from lead tails with 3-4 cleaning stages.

-bulk tails to pressure leach circuit for oxidation.

-pressure leach residue to cyanidation circuit for precious metal recoveries after neutralization.

-cyanidation destruction circuit and arsenic precipitation circuit (as required) on final plant tailings.

Possible modifications to the circuit include atmospheric leaching of the lead concentrate to reduce contaminants and allow marketing, and possible bulk flotation of tails ahead of the pressure leach circuit as required for sulphur feed levels to the auto clave.

25. WORK IN PROGRESS

Ongoing Lakefield testwork is directed at reducing the arsenic content in zinc concentrates and establishing operating parameters for pressure leach pilot work. Individual drill holes were composited into two major samples (A and B) reflecting variance in metallurgy. Clean zinc drill holes were not included in these composites.

Latest results on composite A have produced zinc concentrates assaying 55% zinc and 0.5% arsenic with approximately 45% metal recovery. Composite B has produced similar concentrate grades with 70% metal recovery. Testwork has indicated that conditioning lead rougher tails with copper sulphate followed by flotation produces superior results as compared to elevating the PH and adding an arsenic depressant. Locked cycle tests to determine the metals balance and concentrate quality are now in progress.

Pressure leaching testwork has determined that $200^{\rm C}$ is required to prevent elemental sulphur from forming during leaching. In addition, oxygen partial pressure of 100 psi is adequate for gold recovery as oxidation levels of 65% have demonstrated recoveries greater than 93%. Final batch tests are underway examining pulp density, retention time and the effect of different neutralization flowsheets on gold and silver recovery, and arsenic balance.

26. <u>METALLURGICAL POTENTIAL</u>

This report has used conservative metal recoveries base on batch flotation testwork. Ongoing testwork utilizing various reagent schemes has produced saleable arsenic zinc concentrates from all areas of the deposit. Locked cycle tests will provide a better estimation of metal recovery and deportment and are expected to improve recoveries.

27. <u>CONCLUSIONS</u>

This report summarizes the diamond drilling and metallurgical program completed on the J&L arsenical sulphide deposit. The 1988-89 Phase I program established the continuity of the higher grade gold zones (10330-10420 and 10560-10760), by drilling from the 350 and 670 crosscuts. In addition, the program outlined the extent of the high grade sphalerite zone (10800 area). The metallurgical program which is ongoing identified the mineralogical controls and effect on flotation concentrate quality and metal recoveries.

The continuity of the ore zone both laterally and vertically indicates little risk associated with increasing reserves by further exploration. The fringe holes of the drilled area possess higher grade intercepts that the average indicating that maintaining grade will is highly probable.

At this time, the most significant risks appear to be proving the metallurgical balance and salability of concentrates and establishing the arsenic effluent treatment program and its associated costs. These risks should be eliminated prior to embarking on the major exploration program discussed below.

28. <u>RECOMMENDATIONS</u>

It is recommended that Equinox proceed with the pilot plant to determine recoveries and concentration specifications. Further feasibility evaluations should be done when the pilot plant is completed to establish both capital and operating costs. Stage I work with respect to data collection and pilot plant work waste analysis should also proceed to enable mine permitting to proceed.

This phase of work will require four to six months to complete after financing and if positive will provide the go ahead for the next underground exploration program on the J&L Main Zone. A summer exploration program on the A & E Zone is recommended and should proceed immediately that the weather is suitable (see attached report of A & E program).

28.1 Introduction

The recommended work is broken down into phase II and phase III. Phase II is designed to eliminate the metallurgical and environmental risks associated with the project. Phase III is designed to increase the reserves sufficiently to make a production decision feasible and to provide an economic basis on which to obtain debt financing.

28.2 Phase II - Pilot Plant

Bulk samples representative of the major ore types were taken during the 1988-89 winter program. The pilot plant will subject each individual bulk sample to:

- a) batch heavy media testing using ferro-silicon as the media;
- b) continuous lead-zinc flotation utilizing the flowsheet developed in Phase I testwork;
- c) pressure leaching/cyanidation of bulk tails from each bulk sample pilot run.

In addition, approximately 30% of each sample will be retained and blended together to form a joint composite. The final composite will also be tested as described above to examine the interaction of variable mineralogy.

Process waste streams from all plant circuits (ie. heavy media, pressure leach liquor neutralization, final cyanidation tails) will be characterized to determine effluent treatment requirements and associated costs. Upon completion of the program, a smelter survey utilizing concentrates produced in the pilot runs will be conducted to determine the marketability of the concentrates.

During pilot plant work, preliminary work on site layout and in particular tailings dam start-up costs will be conducted. Ongoing Stage I baseline data will be collected with particular emphasis on water quality.

Positive evaluation of this phase of the work together with a more rigorous capital and operating cost estimate at various production rates will provide recommendations for proceeding with Phase III testwork. An estimate of the cost of this phase is 350,000 to 400,000 excluding the summer exploration program on A & E.

28.3 Phase III - Underground Exploration

This phase of the program is designed to provide sufficient reserves to enable a production decision at a rate of 175,000 tpy.

An exploration decline which will later be converted to the main production haulway will be driven to the 730 meter level ASL, approximately 100 meters below the existing drift. The decline will commence at the face of the crosscut drive that was begun by Pan American Minerals and will be driven at 15% in the footwall of the ore zone. On the 730 level, a hanging wall drill drift will be driven to provide drill stations for approximately 12,000 meters of BQ drilling. This program will allow for drifting on the ore zone at the 730 and 780 level as well as raises on ore on both these levels.

As the program proceeds, a detailed feasibility study will be carried out and the Stage I permitting report finalized. The total underground program will take 10-12 months, with the feasibility and Stage I report scheduled to be completed at the same time.

An estimate of the cost of this underground is \$6.4 million and is summarized in Table 7.

	\$M
Access decline	2.00
Drill drift	.80
Drilling	1.00
On vein drifting	1.00
Raising on vein	.80
Stage I study	.30
Feasibility study	
	\$6.40

TABLE 7 ESTIMATED EXPLORATION PROGRAM

29. STATEMENT OF QUALIFICATIONS

29.1 Statement of Qualifications

I, J.H. Wright, hereby certify:

- That I am a practicing professional engineer with offices at #900-625 1. Howe Street, Vancouver, B.C.
- That I am a member in good standing of the Association of Professional 2. Engineers of the Province of British Columbia.
- That I am a graduate of Queen's University, Kingston, Ontario in 3. Honours B. Sc. Applied Metallurgy, 1975.
- That I have personally visited the property, examined background data, 4. designed the metallurgical program and reviewed the results.

Dated at Vancouver, B. C. this 14th day of December, 1989.

John H. Wright, P. Eng.

29.2 STATEMENT OF QUALIFICATIONS

I, Robert F. Weicker, hereby certify:

- 1. That I am a practicing geologist employed by Equinox Resources Ltd., #900-625 Howe Street, Vancouver, B.C. My position is chief mining geologist.
- 2. That I am a graduate of the University of Waterloo, Waterloo, Ontario in Honours Earth Science (B.Sc. 1977).
- 3. That I have practiced exploration and mining in Canada and the United States since 1977 while employed by Lac Minerals Ltd., Noranda Exploration, Pamour Porcupine Mines and Asarco Exploration.
- 4. That I have personally supervised the work carried out and the observations and opinions expressed herein are base on my personal examinations of the property and on a review of available data and reports.
- 5. That I have no interest in the properties included in this report.

Dated at Vancouver, B.C. this 14th day of December, 1989.

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Robert F. Weicker, B. Sc.
30. COST STATEMENT

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Arty 1 Group

Note: Costs prorated for the period December - February at 8.4% (diamond drilling) and 33.3% for March 1989 (bulk sampling) and any period after March.

Personnel		
Bill Sanders - Labourer		\$ 908.00
John Wright - Operations Manager		1,356.00
Rene Albert - Geologist		1,272.00
Gail Ringwwood - Drafting		314.00
Robert Weicker - Chief Geologist		1,204.00
Toivo Taal - Geologist		<u>2.233.00</u>
	Subtotal	\$ 7,287.00
Support		
Camp Maintenance		\$ 12.00
Camp Rental		3,846.00
Caterers - Food		4,534.00
Generator & Fuel		1,786.00
Propane		325.00
Truck Rental		2,635.00
Road Maintenance - Snow Removal		2,140.00
Telephone - Vancouver		88.00
Telephone - Site		1,815.00
Truck Fuel		156.00
Site Operation Cost		247.00
Supervision		83.00
Reproductions		53.00
Drafting Supplies		128.00
Postage/Photocopying		87.80
Report Preparation		<u>1,083.00</u>
	Subtotal	\$19,048.00
Assaying	Subtotal	\$ 2,078.00
Diamond Drilling		
Broco Drilling Ltd., Delta, B.C.		
Drilling	\$26,470.00	
Moves	1,187.00	
Field Supplies	43.00	
Mobilization	3,804.00	
Rehabilitation	66.00	
	Subtotal	\$31,570.00
Bulk Sampling Mining	Subtotal	<u>\$19,416.00</u>
-	Total	\$70 300 AA
	TOLAI	\$79,400.00

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<u>Arty 1 Group</u> (after April 17, 1989)

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Assaying		\$ 822.00
Report Preparation Metallurgical Costs		\$1,927.00 <u>3,742.00</u>
	Total	<u>\$6,491.00</u>
		<u>\$6,500.00</u>

Arty 3 Group

Note: costs are prorated for the period December 1988 to February 1989 at 91.6% (diamond drilling) and 66.7% for March 1989 (bulk sampling) based on the specific amount of work completed on each group.

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Personnel		
Bill Sanders - Labourer		\$ 6,896.00
John Wright - Operations Manager		19,444.00
Rene Albert - Geologist		12,496.00
Gail Ringwood - Drafting		3,426.00
Robert Weicker - Chief Geologist		16,046.00
Toivo Taal - Geologist		<u> 19,906.00</u>
	Subtotal	\$ 78,214.00
Support		
Camp Maintenance/Rental		\$ 39,047.00
Caterers - Food		49,442,00
Personnel Mobilization		6,088.00
Vehicle Maintenance		4,216.00
Telephone		634.00
Road Maintenance		2,140.00
Truck Rental		28,732.00
Geological Supplies		3,170.00
Site Operation Costs		120,00
Supervision		10,537.00
Drafting Supplies		1,262.00
Photocopying and Postage		802.00
Supplies		284.00
	Subtotal	\$146,474.00
Assaying		
Acme Laboratories, Vancouver		\$ 13,694.00
Diamond Drilling		
Broco Drilling Ltd., Delta, B.C.		
Drilling	\$287,044.00	
Moves	12,963.00	
Mobilization	41,488.00	
Rehabilitation	6,173.00	
	Subtotal	\$347,668.00
Bulk Sampling		* •• •• •• ••
wining		<u>a 38.884.00</u>
	Total	\$624,934.00
		<u>\$625,000.00</u>

APPENDIX A CLAIM DESCRIPTION AND OWNERSHIP

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Schedule "A"

THE PROPERTY

The J&L property is comprised of: (A) 10 crown granted mineral claims, patented claims or lots, whose taxes are assessed by the Vernon Assessment District; (B) eight single unit mineral claims, and (C) 24 multi-unit claim blocks consisting of 349 mineral units for a grand total of 367 mineral claim units. Details are as follows:

A. <u>Crown Grants</u>

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Lot Number

<u>Name</u>

L14821	Goat Fraction
L14822	Goat No. 2 Fraction
L14823	Goat No. 3 Fraction
L14824	Goat No. 4 Fraction
L14825	Goat No. 5 Fraction
L14826	Goat No. 6 Fraction
L14827	View Fraction
L14828	View No. 2 Fraction
L14829	Creek Fraction
L7408	Aberdeen

B. Single Unit Claims

C.

	Record	Date	No.	Expiry
<u>Name</u>	<u>No.</u>	Recorded	<u>Units</u>	Date
Mary	1545	Nov. 30/82	1	Nov. 30/93
Mary No. 1	1546	Nov. 30/82	1	Nov. 30/93
Mary No. 2	1547	Nov. 30/82	1	Nov. 30/93
Mary No. 3	1548	Nov. 30/82	1	Nov. 30/93
Mary No. 4	757	Oct. 10/79	1	Oct. 10/90
Mary No. 5	758	Oct. 10/79	1	Oct. 10/90
Mary No. 6	759	Oct. 10/79	1	Oct. 10/90
Mary No. 7	760	Oct. 10/79	1	Oct. 10/90
<u>Multi-Unit Clain</u>	1 Blocks			
G.D.	603	April 17/79	16	April 17/93
Min	604	April 17/79	8	April 17/90
Tom	605	April 17/79	20	April 17/94
Kirk	606	April 17/79	20	April 17/93
Shannon 100	1140	Dec. 17/80	12	Dec. 17/93
Shannon 200	1141	Dec. 17/80	12	Dec. 17/93
Shannon 300	1142	Dec. 17/80	16	Dec. 17/93
Shannon 400	1143	Dec. 17/80	20	Dec. 17/93
Shannon 500	1144	Dec. 17/80	20	Dec. 17/93
Shannon 600	1145	Dec. 17/80	16	Dec. 17/93

Shannon 700	1146	Dec. 17/80	18	Dec. 17/90
Shannon 800	1147	Dec. 17/80	8	Dec. 17/90
Shannon 900	1148	Dec. 17/80	20	Dec. 17/90
Shannon 1000	1149	Dec. 17/80	10	Dec. 17/90
Shannon 1100	1150	Dec. 17/80	6	Dec. 17/90
Arty No. 1	1219	June 10/81	12	June 10/89
Arty No. 2	1220	June 10/81	20	June 10/89
Arty No. 3	1221	June 10/81	20	June 10/89
Arty No. 4	1222	June 10/81	20	June 10/89
Burke No. 1	1485	Sept. 30/82	9	Sept. 30/90
Burke No. 2	1486	Sept. 30/82	15	Sept. 30/90
Burke No. 3	1487	Sept. 30/82	15	Sept. 30/90
Sam	1549	Nov. 30/82	8	Nov. 30/93
Sam No. 1	1550	Nov. 30/82	8	Nov. 30/93

All of the claims are located on National Topographic Series map sheet 82M8.

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APPENDIX B GEOLOGICAL DATA

-Drill Hole Location Map -Drill Hole Results -Longitudinal Section -Cross Sections (10350-10820)

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10020,00	63-36	63-		<i>Lt</i> 64-03 87-27	500 Crosscut	
10000.00	830 Level Portai	83-06 83-06 83-06	15 83-07 15 83-32 88-02 83-30 83-28	97-28 97-28 67-25 63-24 0 0 0 0 0 0 0 0 0 0 0 0 0	97-19 67-18 68-07 88-11	VERTICAL S
9950.00			83+33 83-34 83-31 83-34 83-31 83-15	83-29 83-27 83-27 83-27 83-27 83-27 83-25 83-23 83-23	83-20 84-30 83-21 83-21 83-21 83-21 84-28 84-28 84-26 98-05 88-05 88-05	88-24 84-22 964-20 87-11 80-28 87-10
920.00		987 Level Portal		87-30 83-18	84-23 87-21 87-21 84-25 84-23 84-23 84-23	88-09 87-12 84-18 87-09 84-17 84-17 84-17 88-17 88-17 88-17 88-17 88-17 84-15 84-15 84-15
880'00	0.0 20.0 10.0 80.0 80.0 motors EQUINOX RESOURCES LTD. J & L PROJECT	(blasted no entry)	1 B3-16	B3-19	87-22	88-31 84-13 84-13 88-31 84-16 84-07 84-05 84-01 84-14 84-12 84-10
840.00	JY EQUINOX - PAN AMERICAN DRILL HOLE LOCATION PLAN STALE DIT MAP NO					88-15
00038/		E +102 + 40.00 E + 101 60.00 E + 102 - 40.00 E + 102 - 40.00 E + 102 - 40.00 E + 102 - 40.00	E+10280.00 E+10280.00 E+10380.00 E+10380.00 E+10380.00 E+10380.00 E+10380.00 E+10380.00 E+10280.00 E+10080000 E+1008000000 E+10080000000000000000000000000000000000	E+13420.00 E+13420.00 E+13450.00 E+13450.00 E+13530.00 E+13530.00	E+1025000 E+1025000 E	E+L0643.00 E+L0700.00 E+L070

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J&L Drill Results - 1988-1989 Program *

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Hole	Drill Interval m	True Width m	Gold oz/ton	Silver oz/ton	Lead %	Zinc %
88-1	3.5	2,7	1.18	4.1	6.2	12.7
88-2	5.0	3.0	0.18	0.7	0.7	2.0
88-3	4.2	2.2	0.48	1.6	1.9	6.6
88-4	2.1	1.5	0.45	3.4	4.0	6.0
88-5	5.7	4.2	0.47	1.7	2.6	3.7
88-6	0.3	0.3	0,52	3.4	4.9	8.8
88-7	2.0	0.4	0.77	4.6	5.9	6.9
88-8	1.7	1.2	0.57	2.5	3.0	4.4
88-9	2.6	2.6	0.65	2.5	4.5	5.8
88-10	0.7	0.5	0.43	3.2	5.5	11.1
88-11	2.3	0.5	0.21	2.7	3.6	6.4
88-12	2.9	1.6	0.22	3.1	4.6	5.7
88-13	5.1	5.0	0.09	1.3	2.3	5.6
88-14	10.5	4.5	0.13	1.3	1.7	4.5
88-15	2.1	1.6	0.10	2.3	4.8	13.0
88-16	1.2	0.5	0.13	1.0	1.8	4.2
88-17	2.5	1.8	0.41	2.2	3.7	7.8
88-18	7.6	3.0	0.21	2.1	3.1	7.7
88-19	2.0	1.6	0.26	1.0	1.3	5.4
88-20	6.2	4.0	0.24	2.8	3.1	6.4
88-21	7.2	4.5	0.14	1.3	1.6	1.7
88-22	7.4	1.3	0.11	0.9	1.1	2.5
88-23	1.8	1.1	0.28	4.4	6.2	7.7
88-24	3.6	1.2	0.14	2.4	2.6	3.2
88-25	8.1	1.4	0.28	1.9	2.6	4.7
88-26	3.6	0.9	0.17	2.8	1.8	3.0
88-27	4.2	2.0	0.28	3.5	5.4	7.3
88-28	2.3	1.4	0.14	1.9	3.9	5.4
88-29	2.9	2.2	0.21	3.5	6.5	11.7
88-30	1.4	1.4	0.33	1.0	1.2	0.8
88-31	1.5	1.2	0.20	3.2	2.2	4.7
88-32	1.2	0.5	0.36	2,4	2.1	4.2
Averages	3.6	1.9	0.32	2.4	3.3	6.0

*Not necessarily same intersections as used for reserve estimations.

















APPENDIX C 1988-89 DIAMOND DRILL LOGS

APPENDIX D 1988-89 SUMMARY OF ASSAYS

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HOLE-ID	FROM	то	%Pb	¥Zn	oz/tAg	oz/tAu	g/tAg	g/tAu	%Fe	%As
/ 13-08	20.67	21.69	.01	.01	- 00	.000	3.400	.100	.02	.06
80-6	21.69	21.75	.01	.02	.00	.000	4.100	.200	.03	.55
83-08	21./5	22.15	.01	.01	.00	.000	1.000	.100	.02	.02
83-08	33.95	34.93	.02	.01	- 00	.000	1.400	.100	.03	.06
83-08	35 29	36 29	. 02	.01	.00	.000	4 800	.200	.05	20. 00
83-08	36 29	37 00		.01	.00	.000	2 700	100	.12	. 50
83-08	37 00	38 00	01	.01	.00	.000	3 400	100	.02	.04
83-08	43.85	44.09	.09	.04	.00	.000	5,100	030	13	.10
83-08	46.60	47.28	.01	.01	.00	.000	2,000	.100	. 02	.00
83-08	47.28	47.85	.01	.01	.00	.000	1.700	.700	.02	1.38
83-08	47.85	48.24	.04	.05	.00	.000	2.000	.300	.09	1.61
83-08	48.24	48.84	.29	.47	.00	.000	19.900	.500	.76	1.33
83-08	48.84	49.84	.02	.02	.00	.000	1.400	.200	.04	.21
83-08	66.60	67.03	.03	.01	.00	.000	4.800	.200	.04	.01
83-08	67.03	67.15	.69	3.97	.00	.000	22.300	.300	4.66	.02
83-08	67.15	67.38	.17	.11	.00	.000	20.500	.300	.28	.06
83-08	67.38	67.50	7.78	12.00	.00	.000	266.300	23.100	19.78	5.74
83-08	67.50	67.59	.23	.62	.00	.000	14.100	2.400	.85	.28
83-08	67.59	67.63	13	2.32	.00	.000	44.000	3.300	3.49	8.35
83-08	68 19	68 76	.13	.00	.00	.000	2 000	.300	.41	.20
83-08	71.06	71.91	.01	.01	.00	.000	2.700	.100	.02	.09
83-08	71.91	72.75	.01	.02	.00	.000	2,000	.200	.03	.05
83-08	72.75	73.40	.01	.01	.00	.000	1.700	.200	.02	.27
83-08	73.40	74.04	.01	.02	.00	.000	2.400	.200	.03	.10
A3-08	74.04	74.27	.75	.94	.00	.000	21.600	1.600	1.69	2.69
3-08	74.27	74.98	.13	.19	.00	.000	5.100	.400	.32	.56
83-08	74.98	75.58	.01	.02	.00	.000	4.800	.300	.03	.23
83-08	75.58	76.18	.01	.01	.00	.000	3.400	.200	.02	.09
83-08.	76.18	76.83	.01	.01	.00	.000	1.400	.100	.02	.11
83-08	70.03	79 50	.01	.01	.00	.000	1,400	.100	.02	.05
83-08	78 52	79.52	.01	.02	.00	.000	2 700	.200	.03	.13
83-08	79.50	80.15	.03	.02	.00	.000	4 400	500	.02	.01
83-08	80.15	80.86	.01	.01	.00	.000	2.700	.100	.02	. 92
83-08	80.86	81.86	.01	.01	.00	.000	2.400	.100	.02	.02
83-08	81.86	82.86	.01	.01	.00	.000	1.400	.010	.02	.00
83-08	82.86	83.52	.11	.38	.00	.000	4.800	.200	.49	.19
83-08	87.42	88.07	.02	.08	.00	.000	4.100	.200	.10	.14
83-08	88.07	88.74	.01	.01	.00	.000	3.400	.200	.02	.02
83-08	88.74	89.74	.11	.01	.00	.000	7.900	.300	.12	1.71
83-08	89.74	90.74	10.	.01	.00	.000	2.000	.300	.02	.45
83-08	90.74	91.43 92 21	.10	.03	.00	.000	5.800	.400	.13	1.44
83-08	92 21	92.21	.04	.02	.00	.000	1 400	.300	.00	.90
83-08	92.99	93.27	.01	.01	.00	.000	1.400	. 400	.03	.30
83-08	93.27	93.36	.29	. 66	.00	.000	27.400	43.900	.02	12.40
83-08	93.36	93.49	.01	.03	.00	.000	3.400	.700	.04	.34
83-08	93.49	94.18	.01	.01	.00	.000	1.400	.700	.02	.17
83-08	94.18	94.45	.02	.01	.00	.000	3.400	.100	.03	.03
83-08	98.16	99.17	.01	.01	.00	.000	1.000	.100	.02	.04
3-08	99.17	100.02	.01	.01	.00	.000	3.400	.300	.02	.53
J3-08	100.02	100.99	.01	.01	.00	.000	1,400	.200	.02	.03

HOLE-ID	FROM	то	&Pb	% Zn	oz/tAg	oz/tAu	g/tAg	g/tAu	%Fe	%As
	22.60	23.52	.01	.01	.00	.000	1.400	.010	.02	.00
10–3د	23.52	23.60	.01	.01	.00	.000	4.100	3.300	.02	15.10
83-10	23.60	23.74	.01	.01	.00	.000	2.000	.100	.02	.11
83-10	23.74	24.38	.01	.01	.00	.000	1.400	.100	.02	.00
83-10	24.38	25.33	.01	.01	00	.000	1.000	.100	.02	.00
83-10	49.36	50.33	.01	.01	.00	.000	1.000	.100	.02	.00
83-10	50.33	50.75	.54	2.06	5.00	.000	13.700	.100	2.60	.00
83-10	56.04	56.36	.01	.03	s .00	.000	1.400	.100	.04	.03
83-10	56.50	57 20	.04	.03	.00	.000	1 400	.100	.07	.00
83-10	57 29	57 66	15	.01	00	.000	4 800	.100	.02	.10
83-10	57.66	58.01	.03	.01	00	.000	1 000	100	.10	.00
83-10	64.10	64.95	.01	.01	00	.000	.700	.100	.02	.00
83-10	64.95	65.20	.01	.04	.00	.000	2.000	.100	.05	.01
83-10	65.20	65.90	.78	6.10	.00	.000	21.200	.300	6.88	.21
83-10	65.90	66.69	.03	.06	5.00	.000	3.400	.100	.09	.02
83-10	66.69	67.69	.08	.76	5.00	.000	10.300	.200	.84	.01
83-10	67.69	68.20	.10	.10	.00	.000	4.100	2.500	.20	1.96
83-10	68.20	69.20	.01	.01	00	.000	1.400	.300	.02	.21
83-10	69.20	70.43	.01	.01	00	.000	.700	.100	.02	.02
83-10	71 42	/1.43	.01	.05		.000	1.400	.100	.06	.01
83-10	71.45	72.30	.01	.03		.000	2.000	.100	.06	.02
83-10	72.30	74 30	.01	.03	, .00	.000	2.000	.100	-04	.00
83-10	74.30	74.73	.01	.01	00	.000	1 400	100	.02	.00
83-10	74.73	75.38	.01	.14	.00	.000	5.500	.100	.15	.00
83-10	75.38	75.74	.01	.01	.00	.000	1.700	.100	.02	.00
:3-10	75.74	76.87	.01	.01	.00	.000	1.000	.100	.02	.03
83-10	76.87	77.87	.01	.01	00	.000	2.000	.100	.02	.00
83-10	77.87	78.06	1.96	5.22	.00	.000	81.600	14.900	7.18	11.80
83~10	78.06	78.66	.02	.03	.00	.000	1.400	.200	.05	.15
83-10	/8.66	/9.47	.01	.01	00	.000	1.400	.200	.02	.14
83-10	92.90	93.80	.01	.04		.000	2.400	.500	.05	.43
83-10	94 64	24.04 95 39	.01	.03		.000	2.000	.100	.04	.09
83-10	95.39	96.14	.01	.00	, .00	.000	2 700	200	.04	.10
83-10	96.14	96.91	.01	.01	00	.000	2,700	.200	.02	.08
83-10	96.61	97.70	.01	.01	.00	.000	2.000	.100	.02	.01
83-10	97.70	98.49	.01	.01	00	.000	2.400	.600	.02	.57
83-10	98.49	99.28	.06	.62	.00	.000	4.400	.400	.68	.48
83-10	99.28	100.28	.01	.04	.00	.000	4.400	.800	.05	.50
83-10	108.22	109.22	.02	.02	.00	.000	1.400	.200	.04	.12
83-10	109.22	109.78	.63	.30	.00	.000	14.400	.100	.93	.17
83-10	110 71	111 64	.10	.05		.000	4.100	.300	.19	.30
83-10	111 64	111 71	1 51	1 64		.000	74 400	.400	.54	.55
83-10	111.71	112.58	10	1.04		000	5 500	300	2.55	.20
83-10	112.58	113.37	.09	. 0.5	5.00	.000	6.800	100	14	.50
83-10	113.37	114.08	.06	.03	3.00	.000	4,100	.300	.09	. 42
83-10	114.08	114.90	.02	.03	.00	.000	2.000	.300	.05	.09
83-11	5.88	6.52	.01	.01	. 00	.000	2.000	.200	.02	.00
83-11	6.52	6.92	.01	.01	00	.000	2.700	.100	.02	.00
3-11	6.92	7.27	.03	.01	00	.000	3.400	.200	.04	.01
J 3-11	7.27	7.45	.08	.01	00	.000	2.700	.100	.09	.00

HOLE-ID	FROM	TO	&Pb	%Zn	oz/tAg	oz/tAu	g/tAg	g/tAu	%Fe	% As
, n3−11	7.45	8.58	.01	.01	.00	.000	2.000	.300	.02	.00
.3-11	8.58	8.74	.01	.01	.00	.000	1.400	.100	.02	.00
83-11	8.74	9.54	.01	.01	.00	.000	.300	.100	.02	.00
83-11	24.78	25.81	.00	.00	.00	.000	.700	.010	.00	.00
83-11	25.81	26.54	.00	.00	.00	.000	.300	.100	.00	.00
83-11	48.85	50.29	.01	.01	00	.000	2.700	.100	.02	.00
83-11	77.60	78.60	.01	.01	00	.000	3.400	.100	.02	.02
83-11	78.60	79.61	.01	.01	00	.000	2.700	.200	.02	.69
83-11	79.61	80.62	.21	.28	.00	.000	7.500	.300	.49	.88
83-11	80.62	81.53	.01	.07	.00	.000	1.400	.200	.08	.38
83-11	81.53	81.89	.01	.01	00	.000	3.400	.100	.02	.01
83-11	81.89	82.62	.01	.01	00	.000	2.700	.100	.02	.00
83-11	97.16	98.16	.04	.03	.00	.000	1.400	.100	.07	.03
83-11	98.16	98.60	.01	.01	00	.000	.300	.100	.02	.01
83-11	98.60	99.40	.03	.13		.000	.300	.100	d1.	.19
93-11	100 20	100.20	.UI 50	.02		.000	18 700	1 200	.03	.05
83-11	100.20	101.20 102.20	.59	1.13		.000	18.700	1.200	15	. 92
83-11	102.20	102.20	12	.00		000	2 300	1 100	.10	• 90 8 Q
83-11	102.20	103 80	01	.01	00	.000	2.500	100	.21	.09
83-11	103.80	104.80	.01	. 01		.000	1,400	.100	02	.00
83-11	104.80	105.80	.01	. 01	00	.000	.700	.100	.02	.03
83-11	105.80	106.40	.01	.01	.00	.000	.700	.100	.02	.05
83-11	106.40	107.00	.12	. 01	00	.000	3.800	1.000	.13	1.11
83-11	107.00	108.00	.01	.01	.00	.000	1.400	.100	.02	.05
83-11	108.00	108.35	.27	.14	.00	.000	24.000	19.200	.41	19.40
83-11	108.35	109.35	.01	.01	.00	.000	.300	.100	.02	.29
3-11	109.35	110.35	.01	.01	00	.000	.300	.100	.02	.05
83-11	110.35	111.35	.01	.01	. 00	.000	1.400	.100	.02	.09
83-11	111.35	112.35	.01	.01	00	.000	1.400	.100	.02	.28
83-11	112.35	113.35	.01	.01	.00	.000	1.400	.100	.02	.01
83-11	113.35	114.30	.01	.01	00	.000	2.700	.100	.02	.02
83-11	114.30	115.30	.01	.01	00	.000	2.600	.100	.02	.85
83-11	115.30	115.30	.01	.01	00	.000	1.400	.100	.02	.17
83-11	117 20	110 20	.01	.01	00	.000	3.600	1.200	.02	1.91
03-11 93-11	119 30	110.30	.01	.01	00	.000	2 700	.100	.02	.08
83-11	119.50	120 05	.01	.01	00	.000	2.700	.100	.02	.23
83-11	120.05	121 00	01	.01	00	.000	2 700	100	.02	.50
83-11	121.00	122.00	.02	.01	.00	.000	.500	1.500	.03	1.03
83-11	122.00	123.00	.01	.01	.00	.000	2,200	.500	.02	.99
83-11	123.00	124.00	.01	.01	.00	.000	.300	.100	.02	.38
83-11	124.00	125.00	.01	.01	.00	.000	2.700	.100	.02	.75
83-11	125.00	126.00	.01	.01	.00	.000	2.000	.100	.02	.34
83-11	126.00	127.00	.01	.01	00	.000	2.000	.100	.02	.20
83-11	127.00	128.00	.02	.01	.00	.000	3.200	.200	.03	.72
83-11	128.00	129.00	.01	.01	00	.000	2.700	.100	.02	.11
83-11	129.00	130.00	.01	.01	00	.000	2.000	.100	.02	.11
83-11	130.00	131.00	.01	.01	00	.000	1.400	.100	.02	.01
83-11	131.00	132.00	.01	.01	00	.000	.700	.100	.02	.02
83-11	132.00	133.00	.10	.11	00	.000	1.400	1.300	.21	1.74
23-11	134.00	134.00	.01	.02	00	.000	3.400	.100	.03	.44
3-11 .3-11	135 00	136 00	.08		00	.000	2.900	.500	.19	1.15
10.11	100.00	10.00	.01	.01		.000	1.400	.200	.02	.05

	HOLE-ID	FROM	TO	%Pb	%Zn	oz/tAg	oz/tAu	g/tAg	g/tAu	%Fe	&As
	HOLE-ID 83-11	FROM 136.00 136.63 137.26 138.26 139.26 140.26 141.26 142.26 142.26 142.26 142.26 143.26 144.26 145.26 150.26 151.26 151.26 151.26 155.26	TO 136.63 137.26 138.26 139.26 140.26 141.26 142.26 142.26 143.26 144.26 145.26 145.26 145.26 145.26 145.26 149.26 150.26 151.26 151.26	<pre>%Pb .01 .01 .01 .01 .01 .01 .01 .03 .03 .19 .01 .02 .01 .02 .01 .02 .01 .02 .01 .01 </pre>	<pre>%Zn .01 .01 .01 .02 .01 .01 .01 .01 .01 .01 .01 .01 .01 .01</pre>	oz/tAg .00 .00 .00 .00 .00 .00 .00 .00 .00 .0	oz/tAu .000 .000 .000 .000 .000 .000 .000 .0	g/tAg 1.700 2.400 3.400 3.400 5.800 4.100 4.100 3.400 8.200 1.400 2.700 3.400 3.700 2.700 8.200 2.400 1.700	g/tAu .200 .100 .100 .200 .100 .100 .100 .200 .2	%Fe .02 .02 .03 .02 .03 .02 .02 .06 .05 .40 .02 .02 .03 .02 .03 .41 .02 .02	<pre>%As . 28 . 05 . 05 . 94 . 49 . 01 . 04 . 10 . 25 . 07 . 05 . 06 . 00 . 06 . 25 . 00 . 00 . 00</pre>
-	83-11 83-11 83-11 83-11 83-11 83-11 83-11 83-11 83-11 83-11 83-11 83-12	152.30 153.30 154.30 155.30 156.20 157.30 158.30 159.30 160.30 161.30 162.30 1.00 2.00 3.00 4.00 5.07 6.07 7.07 8.07 9.16	$153.30 \\ 154.30 \\ 155.30 \\ 156.20 \\ 157.30 \\ 158.30 \\ 159.30 \\ 160.30 \\ 161.30 \\ 162.30 \\ 162.76 \\ 2.00 \\ 3.00 \\ 4.00 \\ 5.07 \\ 6.07 \\ 7.07 \\ 8.07 \\ 9.16 \\ 10 16 \\ 1$.01 .01 .01 .01 .01 .01 .01 .01 .01 .01	.01 .01 .01 .01 .01 .01 .01 .01 .01 .01	.00 .00 .00 .00 .00 .00 .00 .00 .00 .00	.000 .000 .000 .000 .000 .000 .000 .00	2.400 2.000 1.400 3.400 1.700 2.000 1.400 1.000 2.000 1.700 1.400 .700 12.300 .300 .700 2.000 1.400 3.400 1.900	.100 .100 .100 .100 .100 .200 .200 .100 .1	.02 .02 .02 .02 .02 .02 .02 .02 .02 .02	.00 .00 .00 .00 .00 .16 .03 .01 .03 .01 .03 .00 .00 .00 .00 .00 .00
	83-12 83-12	10.16 11.15 12.15 13.15 14.12 14.44 14.87 15.18 16.15 17.18 18.18 19.18 20.18 21.18 22.18 23.18 23.18	11.15 12.15 13.15 14.12 14.44 14.87 15.18 16.15 17.18 18.18 19.18 20.18 21.18 22.18 23.18 23.83 24.83	.00 .00 .00 .00 .00 .00 .00 .00 .00 .00		.00 .00 .00 .00 .00 .00 .00 .00 .00 .00	.000 .000 .000 .000 .000 .000 .000 .00	2.500 2.000 3.300 4.800 3.900 3.400 4.100 3.400 1.800 8.200 11.500 1.700 1.800 .300 .300 1.400 .700 .700	.200 .100 .100 .200 .100 .100 .100 .100	.00 .00 .00 .00 .00 .00 .00 .00 .00 .00	.00 .00 .00 .00 .00 .00 .00 .00 .00 .00

HOLE-ID	FROM	TO	%Pb	%Zn o	z/tAg	oz/tAu	g/tAg	g/tAu	% Fe	%As
83-12	24 83	25 83	00	0.0	0.0	000	1 400	100	0.0	0.0
83-12	25 83	26 83	00		00	000	1 400	100	00	.00
83-12	26.83	27.83	.00	.00	.00	000	1 400	100	.00	00
83-12	27.93	28.46	.00	.00	.00	000	2 000	100	.00	.00
03-12	29.46	20.40	.00	.00	- 00	.000	2.000	100	.00	.00
03-12	20.40	29.40	.00	.00	.00	.000	2 000	.100	.00	.00
03-12	29.40	31 46	.00	.00	.00	.000	2.000	.100	.00	.00
03-12	31 46	32.40	.00	.00	.00	.000	2.000	.100	.00	.00
0J-12 93_12	32 46	32.40	.00	.00	.00	.000	2 600	.300	.00	.00
03-12	22.40	33.40	.00	.00	.00	.000	2.000	.100	.00	.00
03-12	33.40	34.40	.00	.00	.00	.000	.700	.100	.00	.00
93-12	34.40	37 97	.00	.00	.00	.000	2 000	.100	.00	.00
93-12	37 97	39.07	.00	.00	.00	.000	2.000	.100	.00	.00
0J~12 93-12	39 87	30.07	.00	.00	.00	.000	2.700	.100	.00	.00
83-12	30.07	40 53	.00	.00	.00	.000	2 000	.100	.00	.00
83-12	40 53	41 53	.00	.00	.00	.000	2,000	.100	.00	.00
83-12	41 53	42 53	.00	- 00	.00	.000	2 700	100	.00	.00
83-12	42 53	42.00	.00	00	.00	.000	4 800	100	.00	.00
83-12	43 53	44 53	.00	00	.00	.000	4.000	700	.00	.00
83-12	44 53	45 53	00	.00	.00	.000	2 400	300	.00	.00
83-12	45 53	46 53	.00	.00	.00	.000	2.400	100	.00	.00
83-12	46 53	47.53	.00	.00	.00	.000	10 000	5 100	.00	.00
83-12	47 53	48 53	.00	.00	.00	.000	1 900	100	.00	.00
83-12	48.53	49.53	.00	.00	.00	.000	2 700	100	.00	.00
83-12	49.53	50.43	.00	.00			2 000	100	.00	.00
83-12	50.43	51.43	.00	00	.00	000	20 400	100	.00	.00
83-12	51.43	51.99	.00	.00	.00	.000	4 000	100	.00	00.
83-12	51.99	52.99	.00	.00	00		2 700	100	.00	.00
83-12	52.99	53.99	.00	.00	.00	.000	1,000	- 400	00	.00
83-12	53.99	54.92	.00	.00	.00	.000	1,300	.700	. 00	.00
83-12	54.92	55.92	.00	.00	.00	.000	2.000	.700	.00	.00
83-12	55.92	56.92	.00	.00	.00	.000	2.300	.400	.00	.00
83-12	56.92	58.04	.00	.00	.00	.000	3.400	.100	.00	.00
83-12	58.04	58.88	.00	.00	.00	.000	2.700	.100	.00	.00
83-12	58.88	59.71	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	59.71	60.10	.00	.00	.00	.000	2.700	.100	.00	.00
83-12	60.10	61.01	.00	.00	.00	.000	4.100	.100	.00	.00
83-12	61.01	62.01	.00	.00	.00	.000	1.900	.100	.00	.00
83-12	62.01	63.01	.00	.00	.00	.000	2.700	.100	.00	.00
83-12	63.01	63.54	.00	.00	.00	.000	.300	.100	.00	.00
83-12	63.54	64.54	.00	.00	.00	.000	1.700	.100	.00	.00
83-12	64.54	65.54	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	65.54	66.54	.00	.00	.00	.000	.700	.100	.00	.00
83-12	66.54	67.49	.00	.00	.00	.000	1.000	.100	.00	.00
83-12	67.49	67.84	.00	.00	.00	.000	2.700	.100	.00	.00
83-12	67.84	68.84	.00	.00	.00	.000	1.000	.100	.00	.00
83-12	68.84	69.13	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	69.13	69.50	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	69.50 70 FA	70.50	.00	.00	.00	.000	1.700	.100	.00	.00
03-12	70.50	71.29	.00	.00	.00	.000	2.000	.100	.00	.00
03-12 93 10	71.29	71.94	.00	.00	.00	.000	2.700	.100	.00	.00
03-12	71.94	12.42	.00	.00	.00	.000	2.700	.200	.00	.00
03~12 03_12	72.42	72.84	.00	.00	.00	.000	.300	.100	.00	.00
05-14	12.04	13.04	.00	+00	.00	.000	.300	.100	.00	.00

HOLE-ID	FROM	TO	%Pb	%Zn ∘	oz/tAg	oz/tAu	g/tAg	g/tAu	%Fe	%As
/ 93-12	73.84	74.56	.00	.00	.00	.000	.300	.100	.00	.00
33-12	74.56	75.57	.00	.00	.00	.000	.700	.100	.00	.00
83-12	75.57	76.57	.00	.00	.00	.000	.300	.100	.00	.00
83-12	76.57	77.57	.00	.00	.00	.000	1.000	.100	.00	.00
83-12	77.57	78.57	.00	.00	.00	.000	1.000	.100	.00	.00
83-12	78.57	79.57	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	79.57	80.05	.00	.00	.00	.000	.300	.100	.00	.00
83-12	80.05	81.05	.00	.00	.00	.000	.300	.100	.00	.00
83-12	81.05	82.05	.00	.00	.00	.000	1.000	.100	.00	.00
83-12	82.05	83.38	.00	.00	.00	.000	1.700	.100	.00	.00
83-12	83.38	84.38	.00	.00	.00	.000	2.700	.100	.00	.00
83-12	84.38	85.38	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	85.38	86.38	.00	.00	.00	.000	1.000	.100	.00	.00
83-12	86.38	87.38	.00	.00	.00	.000	.300	.100	.00	.00
83-12	87.38	88.50	.00	.00	.00	.000	.300	.100	.00	.00
83-12	88.50	89.50	.00	.00	.00	.000	.300	.100	.00	.00
83-12	89.50	90.50	.00	.00	.00	.000	.300	.100	.00	.00
83-12	90.50	91.50	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	91.50	92.50	.00	.00	.00	.000	.300	.100	.00	.00
03~12	92.50	93.50	.00	.00	.00	.000	1.000	.100	.00	.00
03-12	93.30	94, 34	.00	.00	.00	.000	.300	.100	.00	.00
03-12	24.24	90.34	.00	.00	.00	.000	1.400	.100	.00	.00
03-12	93.34	20.34	.00	.00	.00	.000	1.700	.100	.00	.00
83-12	90.34	97.34	.00	.00	.00	.000	1.700	.100	.00	.00
83-12	97.04	99.84	.00	.00	.00	.000	1.000	100	.00	.00
83-12	99.84	100 84	.00	.00	.00	.000	.300	100	.00	.00
33-12	100.84	101.84	.00	.00	.00	000	300	100	.00	.00
83-12	101.84	102.88	.00	.00	.00	000	2 700	100	.00	.00
83-12	102.88	103.57	.00	.00	.00	.000	1.000	100	.00	.00
83-12	103.57	104.18	. 00	.00	.00	.000	1.700	100	.00	.00
83-12	104.18	104.78	.00	.00	.00	.000	1,400	.100	.00	.00
83-12	104.78	105.27	.00	.00	.00	.000	.300	.100	. 00	. 00
83-12	105.27	106.27	.00	.00	.00	.000	1,400	.100	.00	.00
83-12	106.27	106.80	.00	.00	.00	.000	.300	.100	.00	.00
83-12	106.80	107.33	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	107.33	108.19	.00	.00	.00	.000	.300	.100	.00	.00
83-12	108.19	108.84	.00	.00	.00	.000	.700	.100	.00	.00
83-12	108.84	109.46	.00	.00	.00	.000	1.000	.100	.00	.00
83-12	109.46	110.46	.00	.00	.00	.000	3.300	.100	.00	.00
83-12	110.46	111.46	.00	.00	.00	.000	2.700	.100	.00	.00
83-12	111.46	112.46	.00	.00	.00	.000	2.100	.100	.00	.00
83-12	112.46	113.46	.00	.00	.00	.000	2.000	.100	.00	.00
83-12	113.46	114.46	.00	.00	.00	.000	4.000	.100	.00	.00
83-12	114.46	115.46	.00	.00	.00	.000	3.400	.100	.00	.00
83-12	115.46	116.46	.00	.00	.00	.000	2.100	.100	.00	.00
83-12	116.46	117.46	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	117.46	118.46	.00	.00	.00	.000	2.100	.100	.00	.00
83-12	118.46	118.90	.00	.00	.00	.000	.300	.100	.00	.00
83-12	118.90	119.30	.00	.00	.00	.000	.300	.100	.00	.00
83-12	119.30	120.30	.00	.00	.00	.000	.300	.100	.00	.00
83-12	120.30	121.30	.00	.00	.00	.000	.300	.100	.00	.00
93-12	121.30	121.73	.00	.00	.00	.000	.300	.100	.00	.00
33-12	121.73	122.73	.00	.00	.00	.000	.300	.100	.00	.00

HOLE-ID	FROM	TO	%Pb	&Zn	oz/tAg	oz/tAu	ıg∕tAg	g/tAu	ŧFе	%As
83-12	122.73	123.73	.00	.00	.00	.000	.300	.100	.00	.00
83-12	123.73	124.73	.00	.00	.00	.000	.300	.100	.00	.00
83-12	124.73	125.73	.00	.00	.00	.000	.700	.100	.00	.00
83-12	125.73	125.80	.00	.00	.00	.000	.700	.100	.00	.00
83-12	125.80	126.80	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	126.80	127.80	.00	.00	.00	.000	2.100	.100	.00	.00
83-12	127.80	128.75	.00	.00	.00	.000	.300	.100	.00	.00
83-12	128.75	129.40	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	129.40	130.40	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	130.40	131.40	.00	.00	.00	.000	.700	.100	.00	.00
83-12	131.40	132.40	.00	.00	.00	.000	.300	.100	.00	.00
83-12	132.40	133.40	.00	.00	.00	.000	.300	.100	.00	.00
83~12	133.40	134.40	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	134.40	135.40	.00	.00	.00	.000	.700	.300	.00	.00
03-12 93-12	135.40	132.03	.00	.00	.00	.000	.300	.100	.00	.00
03-12 93-12	136 93	137 93	.00	.00	.00	.000	2.100	.100	.00	.00
83-12	130.05	138 83	.00	.00	.00	.000	.300	100	.00	.00
83-12	138 83	139 50	.00	.00	.00	.000	.300	100	.00	.00
83-12	139.50	140.06	.10	.05	.00	000	4 800	100	.00	.00
83-12	140.06	140.16	6.25	.15	.00	.000	139,800	2.600	6 40	1 36
83-12	140.16	140.90	.03	.01	.00	.000	3,400	.200	.04	1.00
83-12	140.90	141.90	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	141.90	142.90	.00	.00	.00	.000	3.400	.100	.00	.00
83-12	142.90	143.70	.01	.01	.00	.000	2.700	.100	.02	.00
83-12	143.70	144.00	.01	.01	.00	.000	2.700	.100	.02	.00
83-12	144.00	144.22	.01	.01	.00	.000	4.100	.100	.02	.00
83-12	144.22	145.37	.01	.01	.00	.000	2.700	.100	.02	.00
83-12	145.37	146.42	.00	.00	.00	.000	.700	.100	.00	.00
83-12	146.42	147.42	.00	.00	.00	.000	.700	.600	.00	.00
83-12	147.42	148.42	.00	.00	.00	.000	2.400	.400	.00	.00
83-12	148.42	149.42	.00	.00	.00	.000	2.700	.100	.00	.00
83-12 83 12	149.42	150.42	.00	.00	.00	.000	1.400	.100	.00	.00
83-12	151 42	151.42	.00	.00	.00	.000	.700	.100	.00	.00
83-12	151 64	152 70	.00	.00	.00	.000	.700	.100	.00	.00
83-13	101.04	1 52	2 74	6 94	.00	.000	83 000	6 600	.00	.00
83-13	1.52	3.00	1.63	8.52	.00	.000	82.200	3 500	10 15	2 97
83-14	1.50	2.35	.00	.00	.00	.000	2.700	.100	.00	2. 00
83-14	2.35	3.20	.00	.00	.00	.000	2.000	.100	.00	.00
83-14	3.20	3.89	.00	.00	.00	.000	1.700	.100	.00	.00
83-14	3.89	4.59	.00	.00	.00	.000	1.400	.100	.00	.00
83-14	4.59	4.85	.00	.00	.00	.000	1.400	.100	.00	.00
83-14	4.85	5.44	.00	.00	.00	.000	1.000	.100	.00	.00
83-14	5.44	6.04	.00	.00	.00	.000	1.700	.100	.00	.00
83-14	6.04	6.73	.01	.01	.00	.000	1.400	.100	.02	.00
83-14	6.73	7.42	.01	.01	.00	.000	1.000	.100	.02	.00
83-14	7.42	8.42	.01	.01	.00	.000	.700	.100	.02	.00
03-14 03-14	8.42	9.39	.01	.01	.00	.000	.700	.100	.02	.00
03-14	3.39	11.01	.01	.01	.00	.000	1.000	.100	.02	.00
03-14	11 21	11 00	.00	.00	.00	.000	1.400	.100	.00	.00
03-14 93-14	11 00	12 23	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	12 63	12.00	.00	.00	.00	.000	2.400	+100	.00	.00
~~ . ~		TO . OO		.00	.00	+ U U U	. / 0 0	. 100	.00	.00

HOLE-ID	FROM	то	%₽b	%Zn	oz/tAg	oz/tA	u g/tAg	g/tAu	%Fe	&As
00.14										
93-14	13.63	14.36	- 00	.00	.00	.000	2.000	.100	.00	.00
33-14	14.30	15.09	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	16 09	17 00	.00	.00	.00	.000	.300	.100	.00	.00
83-14	17.09	18 09	.00	.00	.00	.000	.300	.100	.00	.00
83-14	18.09	19.09	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	19.09	20.09	.00	.00	.00	.000	2 700	100	.00	.00
83-14	20.09	21.09	.00	.00	.00	.000	4,100	.100	.00	.00
83-14	21.09	22.09	.00	.00	.00	.000	4.800	.100	.00	.00
83-14	22.09	23.09	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	23.09	24.09	.00	.00	.00	.000	4.700	.100	.00	.00
83~14	24.09	25.09	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	25.09	25.78	.00	.00	.00	.000	2.100	.100	.00	.00
83-14	25.18	20.47	.00	.00	.00	.000	5.300	.200	.00	.00
83-14	20.47	28 25	- 00	.00	.00	.000	2.500	.200	.00	.00
83-14	28.25	29.04	.00	.00	.00	.000	3.300	.100	.00	.00
83-14	29.04	30.01	. õõ	.00	.00	.000	2 700	100	.00	.00
83-14	30.01	31.01	.00	.00	.00	.000	3.300	.100	.00	.00
83-14	31.01	32.01	.00	.00	.00	.000	4.100	.100	.00	.00
83-14	32.01	32.50	.00	.00	.00	.000	1.100	.300	.00	.00
83-14	32.50	33.50	.00	.00	.00	.000	1.400	.100	.00	.00
83-14	33.50	34.50	.00	.00	.00	.000	4.800	.100	.00	.00
03-14 93-14	34.50	35.00	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	35.00	36 19	.00	.00	.00	.000	3.400	.100	.00	.00
83-14	36.19	36.76	.00	.00	.00	.000	2.100	.100	.00	.00
3-14	36.76	37.33	.00	.00	.00	.000	2 100	.100	.00	.00
83-14	37.33	38.22	.00	.00	.00	.000	1.800	.300	.00	00.
83-14	38.22	39.22	.00	.00	.00	.000	4.800	.100	.00	.00
83-14	39.22	40.22	.01	.01	.00	.000	1.400	.100	.02	.00
83-14	40.22	41.22	.01	.01	.00	.000	1.700	.100	.02	.00
83-14	41.22	41.28	.05	.01	.00	.000	12.300	2.700	.06	22.20
83-14	42.05	42.05	.01	.01	.00	.000	2.700	.100	.02	.11
83-14	43.00	43.08	25	5 40	.00	.000	4.100	.100	- 02	.12
83-14	43.08	43.24	.04	.06	.00	.000	3 400	13.500	5.65	12.00
83-14	43.24	43.37	.01	.02	.00	.000	1.700	100	.10	1.22
83-14	43.37	44.01	.01	.01	.00	.000	1.700	.100	.02	22
83-14	44.01	44.72	.01	.01	.00	.000	2.000	.100	.02	.04
83-14	44.72	45.46	.01	.01	.00	.000	1.700	.100	.02	.20
83-14	45.46	46.21	.01	.01	.00	.000	2.400	.200	.02	.18
83-14	40.21	47.21 48 21	.03	.04	.00	.000	2.000	.200	.07	.34
83-14	48.21	48.21	10	.02	.00	.000	4.500	.200	.04	.14
83-14	48.28	48.59	.04	.01	.00	.000	12.300	8.200	.11	21.50
83-14	48.59	49.32	1.31	3.53	.00	.000	32 900	.200	.12	.38
83-14	49.32	50.16	6.42 1	13.50	.00	.000	439.800	10.400	4.04	1.99
83-14	50.16	50.31	.10	.23	.00	.000	3.400	.200	33	25
83-14	50.31	50.54	.16	.08	.00	.000	12.700	6.600	.24	8.28
83-14	50.54	51.54	.05	.02	.00	.000	9.600	1.200	.07	2.88
03-14	51.54	52.54	.09	.01	.00	.000	21.900	2.000	.10	3.66
3-14	52.54	53.17 53 01	.01	.01	.00	.000	2.400	.200	.02	.65
)) IA	55.17	22.0T	.08	.01	.00	.000	2.400	.500	.09	1.57

HOLE-ID	FROM	TO	%Pb	%Zn ⟨	oz/tAg	oz/tAu	ıg/tAg	g/tAu	%Fe	%As
3-14	53.81	54.81	.05	.03	.00	.000	2.400	.500	.08	.34
33-14	54.81	55.81	.12	.04	.00	.000	3.700	1.000	.16	.82
83-14	55.81	56.81	.01	.01	.00	.000	1.700	.200	.02	.16
83-14	56.81	57.42	.04	.02	.00	.000	4.800	.100	.06	.14
83-14	57.42	58.04	.07	.02	.00	.000	5.100	.200	.09	.19
83-14	58.04	58.10	.16	.01	.00	.000	11.600	10.100	.17	8.16
83-14	58.10	58.62	.01	11.50	.00	.000	2.400	.300	.02	.59
83-14	58.62	59.30	7.14	11.50	.00	.000	303.000	9.500	18.64	2.72
83~14	59.30	60.30	.10	.08	.00	.000	2.000	.400	.18	.28
83-14	60.30	61.30	.11	.08	.00	.000	1.400	.200	.19	.13
83-14	61.30	62.30	.29	.14	.00	.000	1.400	.200	.43	.12
03-14	62.30	63.30	.01	.14	.00	.000	1.400	.100	.15	.08
03-14	63.30	64.30	.01	.01	.00	.000	1 400	.100	.02	.00
83-14	64.30	66 25	.00	.00	.00	.000	1.400	.100	.00	.00
03-14 93-14	65.30	67 29	.00	.00	.00	.000	1 400	.100	.00	.00
83-14	67 28	67 84	.00	.00	.00	.000	1.400	.100	.00	.00
83-14	67 84	68 40	.00	.00	.00	.000	.700	.100	-00	.00
83-14	68 40	68 62	- 00	.00	.00	.000	1 000	100	.00	.00
83-14	68 62	69 62	.00	- 00	.00	.000	2 700	100	- 00	.00
83-14	69.62	70.22	. 00	.00	.00	.000	2 100	100	.00	00
83-14	70.22	70.75	.00	.00	.00		2 700	100	.00	.00
83-14	70.75	71.75	.00	.00	.00	.000	3.400	.100	.00	.00
83-14	71.75	72.75	.00	.00	.00	.000	2.700	100	.00	.00
83-14	72.75	73.75	.00	.00	.00	.000	3.400	.100	.00	.00
83-14	73.75	74.75	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	74.75	75.75	.00	.00	.00	.000	1.400	.100	.00	.00
.3-14	75.75	76.75	.00	.00	.00	.000	1.400	.100	.00	.00
83-14	76.75	77.58	.00	.00	.00	.000	.700	.100	.00	.00
83-14	77.58	78.58	.00	.00	.00	.000	2.700	.100	.00	.00
83-14	78.58	79.58	.00	.00	.00	.000	.700	.100	.00	.00
83-14	79.58	80.58	.00	.00	.00	.000	.300	.100	.00	.00
83-14	80.58	81.58	.00	.00	.00	.000	1.400	.200	.00	.00
83-14	81.58	82.48	.00	.00	.00	.000	.700	.300	.00	.00
83-14	82.58	83.58	.00	.00	.00	.000	2.100	.100	.00	.00
83-14	83.58	84.58	.00	.00	.00	.000	2.100	.100	.00	.00
83-14	84.58	85.58	.00	.00	.00	.000	3.400	.100	.00	.00
83-14	85.58	85.86	.00	.00	.00	.000	6.200	.100	.00	.00
03-14	00.00	00.00	.00	.00	.00	.000	.700	.100	.00	.00
93-14	00.00	0/.1/ 00 17	.00	.00	.00	.000	2.700	.100	.00	.00
03-14 93-14	0/.1/	00.17	.00	.00	.00	.000	4.100	.100	.00	.00
83-14	89.17	90 17	.00	.00	.00	.000	6.200	.100	.00	.00
83-14	90 17	90.17	.00	.00	.00	.000	3 100	.300	.00	.00
83-14	90.17	91 74	.00	.00	.00	.000	2 700	.300	.00	.00
83-14	91 74	92 30	.00	.00	.00	.000	3 400	.100	-00	.00
83-14	92 30	93 30	.00	.00	.00	.000	4 100	.100	.00	.00
83-14	93.30	94.30	00	.00	.00	,000	2 700	100	.00	.00
83-14	94.30	95.30	.00	.00	.00	.000	1 300	100	.00	.00
83-14	95.30	96.30	.00	.00	- 00	,000	1.400	100	.00	100
83-14	96.30	97.30	.00	. 00	- 00	.000	1,400	.100	.00	.00
83-14	97.30	98.30	.00	.00	.00	.000	3,400	.100	.00	.00
`3-14	98.30	98.45	.00	.00	.00	.000	3.000	.400	_ 00	.00
J3-14	98.45	99.45	.00	.00	.00	.000	1.400	.100	.00	.00

HOLE-ID	FROM	TO	%₽b	%Zn	oz/tAg	oz/tAu	ı g/tAg	g/tAu	ŧГе	%As
< <u>13-14</u>	99 25	100 45	0.0	0.0	00	000	2 500	200	00	0.0
3-14	100 45	100.45	.00	.00	00	.000	4 100	.200	.00	.00
83-14	100.40	101 70	.00	.00	00	000	2 700	100	.00	.00
83-14	101 70	102 70	00	00.	00	.000	2 400	300	.00	.00
83-14	102.70	103.70	.00	.00	.00	.000	3,200	200	.00	00.
83-14	103.70	104.70	.00		.00	.000	2,100	100	.00	00.
83-14	104.70	105.70	.00	.00	.00	.000	.700	.100	.00	.00
83-14	105.70	106.70	.00	.00	.00	.000	3.400	.100	.00	.00
83-14	106.70	107.70	.00	.00	.00	.000	3.400	.100	.00	.00
83-14	107.70	108.70	.00	.00	.00	.000	2.400	.300	.00	.00
83-14	108.70	108.82	.00	.00	.00	.000	4.800	.100	.00	.00
83-14	108.82	109.82	.00	.00	.00	.000	2.400	.300	.00	.00
83-14	109.82	110.03	.00	.00	.00	.000	2.600	.100	.00	.00
83-15	78.46	79.46	.01	.01	.00	.000	1.400	.010	.02	.01
83-15	79.46	79.61	.06	.01	.00	.000	3.800	18.800	.07	14.20
83-15	79.61	80.16	.01	.03	.00	.000	3.300	.100	.04	.27
83-15	80.16	81.18	3.32	2.32	.00	.000	159.600	19.300	5.64	12.50
03-15	01.10	82.05	.51	.41	.00	.000	17.000	.200	.92	.58
83-15	82.03	83 55	1 79	1 70		.000	11.400	.300	. 2 /	. 66
83-15	83 55	84 18	4 20	6 94	00	.000	164 600	15 000	11 11	9.49
83-15	84.18	84.53	1.12	. 82	.00	000	35 800	10.000	1 04	9.30 76
83-15	84.53	84.63	5.80	10.50	.00	.000	277.400	9 200	16 30	6 93
83-15	84.63	85.63	.23	.10	.00	.000	4.500	.300	.33	.53
83-16	140.70	141.65	.01	.01	.00	.000	.300	.100	.02	.01
83-16	141.65	142.34	.10	.49	.00	.000	4.800	.100	.59	.00
-93-16	142.34	143.34	.01	.02	.00	.000	.300	.100	.03	.00
3-16	143.34	144.06	.03	.23	.00	.000	.700	.100	.26	.00
83-16	144.06	145.00	.01	.01	.00	.000	.300	.100	.02	.00
03-10 83-16	150.94	151.94	.01	.01	.00	.000	.300	.100	.02	.00
83-16	157 65	152.05	.02	.01	.00	.000	1.400	.100	.03	.09
83-16	153 25	153.85	1 75	.01	.00	.000	2.000	. 600	0C.	2.17
83-16	153.85	154.27	3.44	2.46	.00	.000	128 200	8 200	5 90	18 60
83-16	154.27	155.27	.06	.02	.00	.000	1.400	100	0.08	19
83-16	155.27	156.27	.04	.01	.00	.000	1.400	.100	.05	.17
83-17	1.60	2.24	.00	.00	.00	.000	2.000	.100	.00	.00
83-17	2.24	2.76	.00	.00	.00	.000	4.500	.100	.00	.00
83-17	2.76	3.21	.00	.00	.00	.000	4.500	.100	.00	.00
83-17	3.21	4.21	.00	.00	.00	.000	4.800	.100	.00	.00
83-17	4.21	5.21	.00	.00	.00	.000	8.200	.100	.00	.00
83-17	5.21	0.21	.00	.00	.00	.000	5.500	.100	.00	.00
83-17	7.21	8.21	.00	.00	.00	000	4.800	.100	.00	.00
83-17	8.21	9.21	.00	.00	.00	000	4 100	.100	.00	.00
83-17	9.21	10.21	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	10.21	11.21	.00	.00	.00	.000	3.400	.100	.00	.00
83-17	11.21	12.21	.00	.00	.00	.000	1.000	.100	.00	.00
83-17	12.21	13.21	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	13.21	14.21	.00	.00	.00	.000	1.000	.100	.00	.00
83-17	14.21	15.21	.00	.00	.00	.000	.700	.100	.00	.00
ბე∽1/ ავ.17	15.21	16.23	.00	.00	.00	.000	3.400	.100	.00	.00
3-17	16.23	16.80	.00	.00	.00	.000	1.400	.100	.00	.00
23-17	10.80	T1.80	+00	.00	.00	.000	2.000	.100	.00	.00

HOLE-ID	FROM	TO	%Pb	% Zn	oz/tAg	oz/tAu	g/tAg	g/tAu	%Fe	%As
83-17	17 80	18 50	00	0.0	0.0	000	7 500	100	00	0.0
33-17	18.50	19.15	.00	.00	.00	.000	3,100	.100	.00	.00
83-17	19.15	19.85	.00	.00	.00	.000	3.400	.100	.00	.00
83-17	19.85	20.75	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	20.75	21.75	.00	.00	.00	.000	2.400	.100	.00	.00
83-17	21.75	22.75	.00	.00	.00	.000	2.000	.100	.00	.00
83-17	22.75	23.75	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	23.75	24.60	.01	.01	.00	.000	1.700	.100	.02	.00
83-17	24.60	25.60	.01	.01	.00	.000	2.000	.100	.02	.01
83-17	25.60	26.60	.01	.01	.00	.000	1.700	.100	.02	.00
83-17	26.60	27.60	.01	.01	.00	.000	1.400	.100	.02	.00
83-17	27.60	28.60	.01	.01	.00	.000	1.000	.100	.02	.00
83-17	28.60	29.60	.01	.01	.00	.000	2.000	.100	.02	.00
83-17	29.60	30.60	.01	.01	.00	.000	.700	.100	.02	.00
83-17	30.00	31.60	.01	.01	+ 00	.000	1.000	.100	.02	.00
03-17 93-17	32 60	32.00	.01	.01	.00	.000	2.400	.100	.02	.00
83-17	32.00	33.30	.01	.01	.00	.000	1 000	.100	.02	.00
83-17	33.30	33.70	01	.01	.00	.000	700	100	.02	.00
83-17	34.70	35.70	.01	.01	.00	.000	1,400	.100	02	.00
83-17	35.70	36.40	.01	.01	.00	.000	1.000	.100	. 02	.00
83-17	36.40	36.95	.16	.01	.00	.000	4.100	.100	.17	.00
83-17	36.95	37.95	.01	.01	.00	.000	.700	.100	.02	.00
83-17	37.95	38.95	.35	.14	.00	.000	5.800	.100	.49	.09
83-17	38.95	39.95	.01	.01	.00	.000	2.000	.100	.02	.00
83-17	39.95	40.95	.01	.01	.00	.000	1.700	.100	.02	.01
83-17	40.95	41.95	.01	.01	.00	.000	1.700	.100	.02	.01
33-17	41.95	42.95	.01	.01	.00	.000	1.400	.100	.02	.01
83-17	42.95	43.95	.01	.01	.00	.000	1.400	.100	.02	.00
83-17	43.95	44.95	.01	.01	.00	.000	1.400	.100	.02	.04
83-17	44.90	40.00	.01	.01	.00	.000	2.700	.100	.02	.03
83-17	40.00	47.00	.01	.01	.00	.000	3.400	.100	.02	.04
83-17	48 00	48.80	01	.01	.00	.000	2 700	.100	.02	.00
83-17	48.80	49.01	.26	.01	00	.000	21 200	200	.UZ २५	.12
83-17	49.01	49.67	.03	.03	.00	.000	4.400	.100	06	.05
83-17	49.67	50.67	.01	.01	.00	.000	1.400	.100	.02	.00
83-17	50.67	51.67	.03	.01	.00	.000	1.000	.100	.04	.00
83-17	51.67	52.66	.03	.12	.00	.000	.700	.100	.15	.00
83-17	52.66	53.08	.05	.08	.00	.000	2.700	.100	.13	.42
83-17	53.08	53.46	1.63	3.58	.00	.000	211.200	4.600	5.21	4.09
83-17	53.46	54.46	.16	.05	.00	.000	18.500	.700	.21	2.52
83-17	54.46	55.38	.31	.03	.00	.000	73.300	2.700	.34	10.10
83-17	55.38	56.04	3.36	6.94	.00	.000	151.800	17.300	10.30	7.74
83-17	56.04	56.65	.09	.03	.00	.000	2.700	.100	.12	.26
0J-17 83-17	30.03 57 75	57.35 57.62	.04	.04	.00	.000	1.400	.200	.08	.16
83-17	57 62	58 63	.00	.00	.00	.000	./00	100	.00	.00
83-17	58 63	59 63	.00	.00	.00	.000	./00	001.	.00	.00
83-17	59.63	60.63	.00	.00	00.	000	.700	100	.00	.00
83-17	60.63	61.57	.00	00	00	.000	1 000	100	.00	.00
83-17	61.57	62.57	.00	.00	.00	.000	1.000	200	00	.00
93-17	62.57	63.57	.00	.00	.00	.000	3,400	.500	,00	00
3-17	63.57	64.57	.00	.00	.00	.000	1.400	.100	.00	.00

HOLE-ID	FROM	то	%₽b	%Zn	oz/tAg	oz/tAu	ıg∕tAg	g/tAu	%Fe	&As
83-17	64.57	65.57	.00	.00	.00	.000	1.700	.100	.00	.00
83-17	65.57	66.57	.00	.00	.00	.000	1.000	.100	.00	.00
83-17	66.57	67.44	.00	.00	.00	.000	1.400	.200	.00	.00
83-17	67.44	68.44	.00	.00	.00	.000	1.400	.200	.00	.00
83-17	68.44	69.44	.00	.00	.00	.000	1.000	.100	.00	.00
83-17	69.44	70.44	.00	.00	.00	.000	10.300	.100	.00	.00
83~17	70.44	71.44	.00	.00		.000	1.000	.100	.00	.00
83-17	72.44	73 11	.00	.00		.000	1.700 6 800	100	.00	.00
83-17	73.44	74.44	.00	.00	.00	.000	1.400	.100	.00	00.
83-17	74.44	75.35	.00	.00	.00	.000	1.000	.100	.00	.00
83-17	75.35	76.35	.00	.00	.00	.000	2.400	.200	.00	.00
83-17	76.35	77.35	.00	.00	.00	.000	2.000	.300	.00	.00
83-17	77.35	78.35	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	78.35	79.35	.00	.00	.00	.000	.700	.100	.00	.00
83-17	79.35	80.35	.00	.00	.00	.000	1.000	.100	.00	.00
83-17	01 25	81.33	.00	.00		.000	1.400	100	.00	.00
83-17	82 35	83 35	.00	.00		000	1 000	100	.00	.00
83-17	83.35	84.35	.00	.00	.00	.000	1.000	100	00	.00
83-17	84.35	85.28	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	85.28	86.28	.00	.00	.00	.000	.700	.100	.00	.00
83-17	86.28	87.28	.00	.00	.00	.000	2.700	.100	.00	.00
83-17	87.28	87.74	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	87.74	88.74	.00	.00	.00	.000	2.000	.100	.00	.00
83-17	88.74	89.74	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	89.74	90.74	.00	.00	.00	.000	2.000	.100	.00	.00
83~17	90.74	91.74	.00	.00	.00	.000	.700	.100	.00	.00
83-17	91.74	92.74	.00	.00		.000	1 000	.100	.00	.00
83-17	93.28	94.28	.00	- 00		.000	2 700	100	.00	.00
83-17	94.28	95.28	.00	.00	.00	.000	1.400	.100	.00	.00
83-17	95.28	96.28	.00	.00	.00	.000	2.000	.100	.00	.00
83-17	96.28	97.28	.00	.00	.00	.000	1.700	.100	.00	.00
83-17	97.28	98.28	.00	.00	.00	.000	3.100	.100	.00	.00
83-17	98.28	99.28	.00	.00	.00	.000	1.700	.100	.00	.00
83-17	99.28	100.28	.00	.00	.00	.000	2.000	.100	.00	.00
83-17	100.28	101.28	.00	.00	.00	.000	1.000	.100	.00	.00
83-17	51 61	52 61	.00	.00	.00	.000	1.000	.100	.00	.00
83-18	52.61	53.54	.03	.01	00	000	8 200	100	.02	10
83-18	53.54	54.54	.01	.01	.00	.000	4,100	.100	.02	00
83-18	62.96	63.96	.01	.01	.00	.000	4.100	.100	.02	.00
83-18	63.96	64.20	.09	.01	.00	.000	17.100	.100	.10	2.83
83-18	64.20	65.20	.01	.01	.00	.000	5.500	.100	.02	.02
83-18	65.20	66.20	.01	.01	.00	.000	4.100	.100	.02	.01
83-18	66.20	66.88	.02	.01	.00	.000	5.500	.100	.03	.20
83-18 83-19	66.88	67.21	1.78	7.05	.00	.000	53.500	6,800	8.83	5.30
83-18 83-18	67.21	68 20	1 71	1.43	.00	,000	4.100	./00	1.51	.61
83-18	68 20	68 71	9,16	20 20	00	000	244 800	7 500	29.21	2,40
83-18	68.71	69.48	1.87	5.92	.00	.000	33.400	200	29.00	1 60
93-18	69.48	70.15	2.06	5.22	.00	.000	33.500	.100	7.28	_ 05
33-18	70.15	70.35	.26	1,37	.00	.000	6.200	.100	1.63	.01

HOLE-ID	FROM	TO	%₽b	₹Zn	oz/tAg	oz/tAu	ı g/tAg	g/tAu	% Fe	%As
/ 83-18	70.35	/1.35	.03	.04	.00	.000	.300	.100	.07	.02
83-19	89.74	89.88	.05	.01	.00	.000	7.500	.100	.06	.00
83-19	89.88	90.74	.00	.00	.00	.000	6.800	.100	.00	.00
83-19	90.74	91.70	.00	.00	.00	.000	4.800	.100	.00	.00
83-19	91.70	92.70	.00	.00		.000	2.000	.100	.00	.00
03-19	92.70	93.30	.00	.00		.000	2.000	100	.00	.00
83-19	93.30	94 68	.00	.00		.000	3 400	100	.00	.00
83-19	94 68	95 48	.00	.00	00	000	3 400	100	.00	.00
83-19	95.48	96.20	. 00	.00	.00	.000	1,400	100	.00	.00
83-19	96.20	96.86	. 00	.00		000	2.000	100	.00	.00
83-19	96.86	97.38	.00	.00	.00	.000	1.400	.100	.00	.00
83-19	97.38	98.37	.00	.00	.00	.000	.300	.100	.00	.00
83-19	98.37	99.00	.00	.00	.00	.000	.700	.100	.00	.00
83-19	99.00	99.49	.00	.00	.00	.000	.300	.100	.00	.00
83-19	99.49	99.84	.03	.01	.00	.000	10.100	1.500	.04	1.89
83-19	99.84	100.96	.01	.01	.00	.000	4.800	.100	.02	.88
83-19	100.96	101.30	.00	.00	.00	.000	4.300	2.500	.00	.00
83-19	101.30	101.80	.00	.00	.00	.000	.300	.100	.00	.00
83-19	101.80	102.80	.00	.00	.00	.000	.300	.100	.00	.00
83-19	102.80	103.80	.00	.00	.00	.000	.300	.100	.00	.00
83-19	103.80	104.70	.00	.00	.00	.000	1.400	.100	.00	.00
83-19	104.70	105.25	.00	.00	.00	.000	2.100	.100	.00	.00
83-19	105.25	105.95	.01	.01	00	.000	.300	.100	.02	.02
83-19	105.95	106.03	.01	.01	00	.000	.300	.100	.02	. /9
03-19 93-10	106.03	108.98	.01	.01		.000	4.100	.100	.02	.01
33-19	108.00	108.00	1 95	6 52	, 100 , 00	.000	64 300	2 900	8 17	2 97
83-19	108.48	100.40	2 28	1 04	00	000	28 800	2.900	3 32	2.07
83-19	109.00	109.70	.17	1.59	.00	.000	4,100	100	1 76	1.42
83-19	109.70	109.86	4.28	2.36	5 .00	.000	110.500	6.700	6.64	5.44
83-19	109.86	110.47	.13	.94	.00	.000	3.000	1,100	1.07	. 42
83-19	110.47	110.58	1.14	4.11	.00	.000	66.900	4.400	5.25	4.48
83-19	110.58	110.79	.40	1.24	.00	.000	6.900	1.300	1.64	1.34
83-19	110.79	111.34	.29	.38	.00	.000	3.300	.800	.67	.38
83-19	111.34	112.00	.54	.58	.00	.000	16.200	3.800	1.12	2.04
83-19	112.00	112.36	.02	.01	00	.000	4.100	.100	.03	.02
83-19	112.36	113.36	.01	.01	.00	.000	.700	.100	.02	.00
83-19	113.36	114.36	.00	.00	.00	.000	.300	.100	.00	.00
83-19	114.36	115.36	.00	.00	.00	.000	.300	.100	.00	.00
83-20	.00	. /4	.02	.03	.00	.000	.300	.100	.05	.01
83-20	. /4	1.58	.01	.02	.00	.000	4.100	.100	.03	.00
83-20	1.58	1.76	.23	.02	.00	.000	24.700	5.500	.25	13.60
83-20	2.76	2.70	.01	.01	00	.000	2.700	.100	.02	.05
83-20	3 76	4 76	01	.01	00	.000	2.000	100	.03	.01
83-20	4 76	5 76	01	.01	00	.000	3 400	100	.02	12
83-20	5.76	6.76	.01	.01	00	.000	3.400	100	.02	04
83-20	6.76	7.76	.01	.01	00	.000	.300	100	02	.04
83-20	7.76	8.71	.01	.01	.00	.000	1.400	.100	.02	.00
83-20	8.71	8.98	.01	.01	.00	.000	2.400	1.000	.02	2.22
83-20	8.98	9.60	.01	.01	.00	.000	7,300	.200	.02	.02
33-20	9.60	10.21	.01	.01	.00	.000	2.000	.100	,02	.01
-3-21	.00	.13	.08	.08	.00	.000	8.800	.100	.16	.06

HOLE-ID	FROM	то	%Pb	%2n (oz/tAg	oz/tA	u g/tAg	g/tAu	%Fe	%As
< 33-21	.13	.19	13.30	15.30	.00	.000	353.500	5.700	28.60	3.08
3-21	.19	1.03	.25	1.84	.00	.000	12.500	1.200	2.09	2.11
83-21	1.03	2.03	.02	.05	.00	.000	2.000	.100	.07	.01
83-21	2.03	3.03	.05	.01	.00	.000	1.700	.100	.06	.03
83-21	3.03	4.03	.16	.01	.00	.000	1.700	.100	.17	.00
83-21	4.03	5.03	.01	.01	.00	.000	2.000	.100	. 02	.00
83-21	5.03	6.03	.01	.01	.00	.000	.300	.100	.02	.00
83-21	6.03	7.03	.01	.01	.00	.000	.300	.100	. 02	.00
83-21	7.03	8.03	.01	.01	.00	.000	.300	.100	. 02	.00
83-21	8.03	9.03	.01	.01	.00	.000	.300	.100	.02	.00
83-21	9.03	9.58	.01	.01	.00	.000	.300	.100	.02	.00
83-22	.00	.84	. 32	.30	.00	.000	8.400	1.200	. 62	1.46
83-22	.84	1.55	3.77	10.30	.00	.000	202.800	4.400	14.07	1.17
83-22	1.55	2.10	2.02	1.37	.00	.000	32.100	.100	3.39	.17
83-22	2.10	2.30	1.12	2.09	.00	.000	13.700	.100	3.21	.06
83-22	2.30	2.90	2.33	5.40	.00	.000	27.400	.100	7.73	.59
83-22	2.90	3.20	.89	1.11	.00	.000	7.600	2.000	2.00	1.64
83-22	3.20	3.54	3.26	9.03	.00	.000	43.200	6.200	12.29	3.57
83-22	3.54	3.97	.19	.12	.00	.000	23.100	3.600	.31	9.49
83-22	3.97	4.84	.03	.02	.00	.000	.300	.100	.05	.55
83-22	4.84	5.70	.01	.01	.00	.000	2.000	.100	.02	.12
83-22	5.70	6.70	.01	.01	.00	.000	4.100	.100	.02	.07
83-22	6.70	7.70	.01	.01	.00	.000	.300	.100	.02	.01
83-22	7.70	8.70	.03	.01	.00	.000	2.000	.100	.04	.15
83-22	8.70	9.31	.01	.01	.00	.000	2.000	.100	.02	.55
83-22	9.31	9.91	.01	.02	.00	.000	1.400	.100	.03	.65
83-23	.00	.37	.25	.72	.00	.000	.300	.100	.97	.00
,3-23	.37	1.37	.02	.02	.00	.000	.300	.100	.04	.00
83-23	1.37	2.37	.01	.01	.00	.000	.300	.100	.02	.00
83-23	2.37	3.37	.01	.01	.00	.000	.300	.100	.02	.00
83-23	3.37	4.37	.01	.01	.00	.000	.300	.100	.02	.00
83-23	4.37	5.37	.01	.01	.00	.000	.300	.100	.02	.00
83-23	5.37	6.32	.01	.01	.00	.000	.300	.100	.02	.00
83-23	6.32	6.99	.01	.01	.00	.000	1.400	.100	.02	.01
83-23	6.99	7.99	.02	.23	.00	.000	1.400	.100	.25	.06
83-23	7.99	8.63	.01	.01	.00	.000	.300	.100	.02	.00
83-23	8.63	9.35	.04	.01	.00	.000	4.100	.100	.05	.01
03-23	9.30	10.06	.02	.01	.00	.000	3.400	.100	.03	.01
83-24	.00	.3/	.01	.01	.00	.000	1.400	.100	.02	.00
83-24	1 27	1.37	.01	.01	.00	.000	5.500	.100	.02	.28
83-24	2.37	2.31	.01	.01	.00	.000	3.400	.100	.02	.00
83-24	2.37	3.37	- 01	.01	.00	.000	2.700	.100	.02	.00
83-24	1 37	5 37	.01	.01	.00	.000	3.400	.100	.02	.02
83-24	5 37	6 37	.01	.01	.00	.000	2.700	.100	.02	.04
83-24	6 37	רביר	.01	.01	.00	.000	1.400	.100	.02	.01
83-24	0.31	1.57	.01	.01	.00	.000	.300	.100	.02	.00
83-24	9.37	0.37	.01	.01	.00	.000	1.400	.100	.02	.00
83-24	0.31 Q 77	10 06	.01	.01	.00	.000	1 400	+ 1 0 0	.02	.00
83-25	00	10.00 01	15 00	.U1 7 AF	.00	.000.	230 600	20 000	.02	.00
83-25	.00	•41 1 01	15.00	1.00	.00	.000	233,000	20.800	22.05	6.82
83-25	· 4 1 } 21	2 21	.13	1 00	.00	.000	1 000	.100	.21	.12
00-20 13-25	2 21	2.21	.07	1 04	.00	.000	1.000	.100	1.07	.04
J-2J (3-25	2.21	J.IJ / 16	.1/	1.04	.00	.000	.700	.100	1.21	.02
00 <u>2</u> 0	0.10	4.10	+ 0 0	.02	.00	.000	.700	.100	.08	.01

HOLE-ID	FROM	TO	%Pb	%Zn o	z/tAg	oz/tAu	g/tAg	g/tAu	%Fe	%As
· 93-25	4.15	5.15	.02	.01	.00	.000	1.000	.100	.03	.01
83-25	5.15	6.15	.01	.01	.00	.000	1.000	.100	.02	.00
83-25	6.15	7.15	.01	.01	.00	.000	.700	.100	.02	.00
83-25	7.15	8.15	.01	.01	.00	.000	1.000	.100	.02	.00
83-25	8.15	8.43	.01	.01	.00	.000	.700	.100	.02	.01
83-25	8.43	9.43	.08	.62	.00	.000	3.400	.100	.70	.09
83-25	9.43	10.05	.19	.06	.00	.000	6.800	.200	.25	.01
83-26	.00	.39	.23	.01	.00	.000	21.900	5.400	.24	15.80
83-26	.39	1.39	.02	.03	.00	.000	2.400	.100	.05	.18
83-26	1.39	2.39	.10	.08	.00	.000	7.500	.200	.18	.16
83-26	2.39	3.39	.06	.02	.00	.000	6.200	.200	.08	.61
83-26	3.39	4.39	.01	.01	.00	.000	4.100	.100	.02	.02
83-26	4.39	5.39	.01	.01	.00	.000	2.700	.100	.02	.03
83-26	5.39	6.39	.01	.01	.00	.000	6.200	.300	.02	.96
83-26	6.39	7.39	.01	.01	.00	.000	3.800	.100	.02	.05
83-26	7.39	8.39	.01	.01	.00	.000	3.100	.100	.02	.03
83-26	8.39	9.39	.01	.01	.00	.000	1.400	.100	.02	.00
83-26	9.39	10.39	.01	.01	.00	.000	1.700	.100	.02	.00
83-26	10.39	11.39	.01	.01	.00	.000	1.400	.100	.02	.00
83-26	11.39	12.39	.01	.01	.00	.000	1.000	.100	.02	.00
83-26	12.39	13.39	.01	.01	.00	.000	2,400	.100	.02	.00
83-26	13.39	14.25	.01	.01	.00	.000	2.700	.100	.02	.00
83-26	14.25	15,25	.01	.01	.00	.000	3.400	.100	.02	.00
83-26	15.25	16.10	.01	.01	.00	.000	2.000	.100	.02	.00
83-26	16.10	17.10	.01	.01	.00	.000	1.400	.100	.02	.00
83-26	10 10	18.10	.01	.01	.00	.000	1.000	.100	.02	.03
03-20	10.10	19.10	.01	.01	.00	.000	. 700	.100	.02	.01
33-20	20 10	20.10	.01	.01	.00	.000	1.400	.100	.02	.00
83-26	20.10	21.10	.01	.01	.00	-000	2.400	.100	.02	.01
83-26	22 10	23 10	.03	.03	.00	-000	2.000	.100	.00	.05
83-26	23.10	24 10	05	04	.00	.000	3 400	100	.02	.01
83-26	24 10	25 10	.00	.04	.00	.000	16 100	.100	.09	.05
83-26	25.10	26.10	.01	.02	.00	.000	1 400	100	.02	.00
83-26	26.10	27.10	.01	.01	.00	000	700	100	.03	.01
83-26	27.10	28.10	. 01	.01	.00	.000	4 100	100	.02	02
83-26	28.10	29.10	.01	.01	.00	.000	1.400	.100	02	.02
83-26	29.10	29.87	.01	.01	.00	.000	5.000	1.800	02	.02
83-27	.00	1.00	.01	.06	.00	.000	.700	.100	.07	.00
83-27	1.00	2.00	.01	.01	.00	.000	13.200	3.200	.02	. 00
83-27	2.00	3.00	.01	.01	.00	.000	.700	.100	.02	.02
83-27	3.00	4.00	.01	.01	.00	.000	.300	.100	.02	.00
83-27	4.00	4.37	.01	.01	.00	.000	.300	.100	.02	.05
83-27	4.37	5.37	.01	.01	.00	.000	.300	.100	.02	.00
83-27	5.37	6.15	.01	.01	.00	.000	.300	.100	.02	.11
83-27	6.15	7.15	.01	.01	.00	.000	.300	.100	.02	.12
83-27	7.15	8.15	.03	.03	.00	.000	.300	.100	.06	.13
83-27	8.15	9.15	.01	.01	.00	.000	.700	.100	.02	.00
83-27	9.15	10.15	.01	.01	.00	.000	.300	.100	.02	.03
83-27	10.15	10.75	.01	.54	.00	.000	.700	.100	.55	.12
83-28	.00	.73	.13	.02	.00	.000	79.500	.200	.15	3.72
83-28	.73	.91	.02	.02	.00	.000	13.700	18.500	.04	20.60
3-28	.91	1.36	.01	.01	.00	.000	17,100	.100	.02	.53
ა3-28	1.36	1.52	.07	.01	.00	.000	.300	.100	.08	4.79

FROM	то	%Pb	€Zn	oz/tAg	oz/tAu	g/tAg	g/tAu	%Fe	&As
1 50	2 53	01	0.1	0.0	000	200	100	0.0	C 1
2 52	2.52	• • • • • • •	.01	.00	.000	.300	.100	.02	-01 21
3.52	4.52	.01	.01	.00	.000	. 300	100	02	.51
4.52	5.52	.01	.01	.00	.000	.300	.100	.02	.01
5.52	6.52	.01	.01	.00	.000	.300	.100	.02	.00
6.52	7.32	.01	.01	.00	.000	.300	.100	.02	.00
7.32	7.70	.01	.01	.00	.000	.300	.100	.02	.00
7.70	8.70	.01	.01	.00	.000	1.400	.100	.02	.00
8.70	9.70	.01	.01	.00	.000	1.400	.100	.02	.00
9.70	10.06	.01	.01	.00	.000	1.400	.100	.02	.00
1 00	2 00	.01	.01	.00	.000	.300	.100	.02	.01
2.00	3 00	01	.01	00.	.000	.300	.100	.02	.02
3.00	4.00	.01	.01	.00	.000	.300	.100	.02	.00
4.00	5.00	.01	.02	.00	.000	.300	.100	.03	.00
5.00	5.79	.01	.01	.00	.000	.300	.100	.02	.00
5.79	6.25	.01	.01	.00	.000	.300	.100	.02	.05
6.25	7.25	.01	.01	.00	.000	.300	.100	.02	.06
1.25 9.25	0.25	.01	.02	.00	.000	.300	.100	.03	.00
9 25	9.25	.01	.01	.00	.000	.300	.100	.02	.00
.00	.35	.01	.01	.00	.000	1,400	.100	02	.00
.35	1.13	.02	.01	.õõ	.000	2.100	.300	.03	1.06
1.13	1.70	1.63	4.52	.00	.000	50.100	22.100	6.15	15.10
1.70	2.70	.29	1.00	.00	.000	7.500	.600	1.29	.34
2.70	3.06	.04	.02	.00	.000	2.700	2.300	.06	1.82
3.00	4.06	.01	.01	.00	.000	. 700	.100	.02	.07
5.06	5.00	.05	.01	.00	.000	4.800	.100	.06	.09
6.06	6.80	.01	.13	.00	.000	2.100	.100	.02	.01 06
6.80	7.80	.01	.01	.00	.000	1.400	.100	.02	.01
7.80	8.80	.01	.01	.00	.000	1.400	.100	.02	.01
8.80	9.14	.01	.01	.00	.000	.300	.100	.02	.03
.00	1.00	.01	.01	.00	.000	.300	.100	.02	.03
2 00	2.00	.01	.01	-00	.000	.300	.100	.02	.01
3.00	4.00	.01	.01	.00	.000	1 400	.100	.02	.00
4.00	5.00	.01	.01	.00	.000	.300	.100	.02	.00
5.00	5.37	.01	.01	.00	.000	.300	.100	.02	.01
5.37	5.90	.06	.04	.00	.000	1.400	.100	.10	.01
5.90	6.90	.03	.04	.00	.000	.700	.100	.07	.03
5.90 7 00	/.90	.01	.01	.00	.000	.300	.100	.02	.00
7.90 8 90	0.90 9.75	.02	.01	.00	.000	1.400	.100	.03	.00
.00	.90	.02	.01	.00	000	1 400	1 000	.05	.00
.90	1.53	2.90	2.39	.00	.000	137.800	13,700	5.29	7 24
1.53	2.53	.07	.10	.00	.000	4.800	.400	.17	.28
2.53	3.53	.02	.02	.00	.000	.700	.300	.04	.31
3.53	4.53	.01	.01	.00	.000	1.400	.100	.02	.06
4.53	4.80	.02	.01	.00	.000	1.900	.100	.03	.38
4.0U 5 16	5.10 6 14	1.39	.48	.00	.000	55.000	10.100	1.87	11.20
6,16	6 91	.02	.01	.00	.000	3.300	.100	.05	.27
6.91	7.45	.01	.01	.00	.000	4.100	.100	.04	.10
	FROM 2222222000000000000000000000000000000	FROMTO 1.52 2.52 2.52 3.52 3.52 4.52 4.52 5.52 6.52 7.32 7.32 7.70 7.70 8.70 9.70 9.70 9.70 9.70 9.70 10.06 $.00$ 1.00 1.00 2.00 3.00 4.00 5.00 5.79 6.25 7.25 8.25 9.25 9.25 9.60 $.00$ $.35$ 1.13 1.70 1.70 2.70 3.06 4.06 5.06 6.00 5.00 5.00 5.37 5.90 6.90 7.90 8.90 8.90 9.75 0.0 9.00 1.53 <td>FROMTO$\\$Pb$1.522.52.012.523.52.013.524.52.014.525.52.015.526.52.016.527.32.017.327.70.017.70$\\$,70$.019.7010.06.01.001.00.011.002.00.012.003.00.013.004.00.014.005.00.015.796.25.016.257.25.017.25$\\$,25$.019.259.60.01.00.35.01.351.13.021.131.701.631.702.70.292.703.06.043.064.06.014.065.06.055.066.06.016.807.80.017.80$\\$,80$.018.80.01$\\$,80$.018.80.01.011.002.00.012.00.02.013.004.00.011.002.00.012.003.00.015.375.90.065.906.90.036.907.90.017.908.90.02.901.532.901.532.53.072.533.53.02</td> <td>FROMTO%Pb%Zn$1.52$$2.52$.01.01$2.52$$3.52$.01.01$3.52$$4.52$.01.01$5.52$$6.52$.01.01$5.52$$6.52$.01.01$7.32$$7.70$.01.01$7.70$$8.70$.01.01$7.70$$8.70$.01.01$9.70$$10.06$.01.01$9.70$$10.06$.01.01$1.00$$2.00$.01.01$2.00$$3.00$.01.01$2.00$$3.00$.01.01$3.00$$4.00$.01.01$4.00$$5.00$.01.01$5.79$$6.25$.01.01$7.25$$8.25$.01.01$7.25$$8.25$.01.01$9.25$$9.60$.01.01$9.25$$9.60$.01.01$9.25$$9.60$.01.01$1.13$$1.70$$1.63$$4.52$$1.70$$2.70$$2.9$$1.00$$2.70$$3.06$.04.02$3.06$$4.06$.01.01$6.06$.01.01$6.06$.01.01$7.80$$8.80$.01.01$7.80$$8.80$.01.01$7.90$$8.90$.02.01$7.90$$8.90$.02.01$7.90$$8.90$.02<td>FROMTO$\\$Pb$$\\$Zn$$oz/tAg$$1.52$$2.52$$.01$$.01$$.00$$2.52$$3.52$$.01$$.01$$.00$$3.52$$4.52$$.01$$.01$$.00$$4.52$$5.52$$.01$$.01$$.00$$5.52$$6.52$$.01$$.01$$.00$$7.32$$7.70$$.01$$.01$$.00$$7.32$$7.70$$.01$$.01$$.00$$7.70$$8.70$$.01$$.01$$.00$$9.70$$10.06$$.01$$.01$$.00$$2.00$$3.00$$.01$$.01$$.00$$2.00$$3.00$$.01$$.01$$.00$$3.00$$4.00$$.01$$.01$$.00$$5.00$$5.79$$.01$$.01$$.00$$5.00$$5.79$$.01$$.01$$.00$$7.25$$8.25$$.01$$.01$$.00$$7.25$$8.25$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.70$$3.06$$.04$$.02$$.00$$3.06$$.04$$.02$$.00$$3.06$$.04$$.02$$.00$$3.06$$.04$$.02$$.00$$7.70$$3.06$$.01$$.01$<!--</td--><td>FROM TO %Pb %Zn oz/tAg oz/tAg 1.52 2.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 4.52 5.52 .01 .01 .00 .000 5.52 6.52 .01 .01 .00 .000 7.70 8.70 .01 .01 .00 .000 9.70 10.66 .01 .01 .00 .000 .00 1.00 .01 .00 .000 .000 .00 1.00 .01 .01 .00 .000 .00 3.00 .01 .01 .00 .000 .00 5.00 .01 .01 .00 .000 .01 .01 .00 .000 .000 .000 .02 9.60 .01 .01 .00</td><td>FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg$1.52$$2.52$$.01$$.01$$.00$$.000$$.300$$2.52$$3.52$$.4.52$$.01$$.01$$.00$$.000$$.300$$4.52$$5.52$$.01$$.01$$.00$$.000$$.300$$5.52$$6.52$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.400$$8.70$$9.70$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.300$$1.00$$2.00$$.01$$.01$$.00$$.000$$.300$$1.00$$2.00$$.01$$.01$$.00$$.300$$3.00$$4.00$$.01$$.01$$.00$$.300$$4.00$$5.00$$.01$$.02$$.00$$.300$$5.00$$5.79$$0.25$$.01$$.01$$.00$$.300$$5.25$$.01$$.01$$.00$$.300$$.300$$7.25$$8.25$$.01$$.01$$.00$$.300$$7.25$$8.25$$.01$$.01$$.00$$.300$$7.25$$.01$$.01$$.00$$.300$$7.27$$3.06$$.01$$.01$$.00$$.300$$7.27$$3.06$$.01$$.01$$.00$</td><td>FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg g/tAu$1.52$$2.52$.01.01.00.000.300.100$3.52$$4.52$.01.01.00.000.300.100$4.52$$5.52$.01.01.00.000.300.100$4.52$$5.52$.01.01.00.000.300.100$5.52$$6.52$.01.01.00.000.300.100$7.32$$7.70$.01.01.00.0001.400.100$7.70$$8.70$.01.01.00.0001.400.100$9.70$10.66.01.01.00.000.300.100$1.00$.001.01.00.000.300.100$1.00$.001.01.00.000.300.100$2.00$.001.01.00.000.300.100$3.00$.01.01.00.000.300.100$4.00$.01.01.00.000.300.100$5.00$$5.79$.01.01.00.000.300.100$5.00$.02.01.01.00.000.300.100$6.25$.01.01.00.000.300.100$6.25$.01.01.00.000.300.100$7.25$$8.25$.01.02.00.000.300$7.27$</td><td>FROMTO4Pb3Zn oz/tAg oz/tAu g/tAgg/tAu%Fe1.522.52.01.01.00.000.300.100.023.524.52.01.01.00.000.300.100.024.525.52.01.01.00.000.300.100.025.526.52.01.01.00.000.300.100.025.737.72.01.01.00.000.300.100.027.737.70.01.01.00.000.1400.100.028.709.70.01.01.00.000.1400.100.029.7010.06.01.01.00.000.300.100.021.002.00.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.004.00.01.01.00.000.300.100.024.005.00.01.02.00.000.300.100.024.259.25.01.01.00.000.300.100.022.728.25.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.01.01.00.000.300.100.02<</td></td></td>	FROMTO $\$Pb$ 1.522.52.012.523.52.013.524.52.014.525.52.015.526.52.016.527.32.017.327.70.017.70 $\$,70$.019.7010.06.01.001.00.011.002.00.012.003.00.013.004.00.014.005.00.015.796.25.016.257.25.017.25 $\$,25$.019.259.60.01.00.35.01.351.13.021.131.701.631.702.70.292.703.06.043.064.06.014.065.06.055.066.06.016.807.80.017.80 $\$,80$.018.80.01 $\$,80$.018.80.01.011.002.00.012.00.02.013.004.00.011.002.00.012.003.00.015.375.90.065.906.90.036.907.90.017.908.90.02.901.532.901.532.53.072.533.53.02	FROMTO%Pb%Zn 1.52 2.52 .01.01 2.52 3.52 .01.01 3.52 4.52 .01.01 5.52 6.52 .01.01 5.52 6.52 .01.01 7.32 7.70 .01.01 7.70 8.70 .01.01 7.70 8.70 .01.01 9.70 10.06 .01.01 9.70 10.06 .01.01 1.00 2.00 .01.01 2.00 3.00 .01.01 2.00 3.00 .01.01 3.00 4.00 .01.01 4.00 5.00 .01.01 5.79 6.25 .01.01 7.25 8.25 .01.01 7.25 8.25 .01.01 9.25 9.60 .01.01 9.25 9.60 .01.01 9.25 9.60 .01.01 1.13 1.70 1.63 4.52 1.70 2.70 2.9 1.00 2.70 3.06 .04.02 3.06 4.06 .01.01 6.06 .01.01 6.06 .01.01 7.80 8.80 .01.01 7.80 8.80 .01.01 7.90 8.90 .02.01 7.90 8.90 .02.01 7.90 8.90 .02 <td>FROMTO$\\$Pb$$\\$Zn$$oz/tAg$$1.52$$2.52$$.01$$.01$$.00$$2.52$$3.52$$.01$$.01$$.00$$3.52$$4.52$$.01$$.01$$.00$$4.52$$5.52$$.01$$.01$$.00$$5.52$$6.52$$.01$$.01$$.00$$7.32$$7.70$$.01$$.01$$.00$$7.32$$7.70$$.01$$.01$$.00$$7.70$$8.70$$.01$$.01$$.00$$9.70$$10.06$$.01$$.01$$.00$$2.00$$3.00$$.01$$.01$$.00$$2.00$$3.00$$.01$$.01$$.00$$3.00$$4.00$$.01$$.01$$.00$$5.00$$5.79$$.01$$.01$$.00$$5.00$$5.79$$.01$$.01$$.00$$7.25$$8.25$$.01$$.01$$.00$$7.25$$8.25$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.25$$9.60$$.01$$.01$$.00$$7.70$$3.06$$.04$$.02$$.00$$3.06$$.04$$.02$$.00$$3.06$$.04$$.02$$.00$$3.06$$.04$$.02$$.00$$7.70$$3.06$$.01$$.01$<!--</td--><td>FROM TO %Pb %Zn oz/tAg oz/tAg 1.52 2.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 4.52 5.52 .01 .01 .00 .000 5.52 6.52 .01 .01 .00 .000 7.70 8.70 .01 .01 .00 .000 9.70 10.66 .01 .01 .00 .000 .00 1.00 .01 .00 .000 .000 .00 1.00 .01 .01 .00 .000 .00 3.00 .01 .01 .00 .000 .00 5.00 .01 .01 .00 .000 .01 .01 .00 .000 .000 .000 .02 9.60 .01 .01 .00</td><td>FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg$1.52$$2.52$$.01$$.01$$.00$$.000$$.300$$2.52$$3.52$$.4.52$$.01$$.01$$.00$$.000$$.300$$4.52$$5.52$$.01$$.01$$.00$$.000$$.300$$5.52$$6.52$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.400$$8.70$$9.70$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.300$$1.00$$2.00$$.01$$.01$$.00$$.000$$.300$$1.00$$2.00$$.01$$.01$$.00$$.300$$3.00$$4.00$$.01$$.01$$.00$$.300$$4.00$$5.00$$.01$$.02$$.00$$.300$$5.00$$5.79$$0.25$$.01$$.01$$.00$$.300$$5.25$$.01$$.01$$.00$$.300$$.300$$7.25$$8.25$$.01$$.01$$.00$$.300$$7.25$$8.25$$.01$$.01$$.00$$.300$$7.25$$.01$$.01$$.00$$.300$$7.27$$3.06$$.01$$.01$$.00$$.300$$7.27$$3.06$$.01$$.01$$.00$</td><td>FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg g/tAu$1.52$$2.52$.01.01.00.000.300.100$3.52$$4.52$.01.01.00.000.300.100$4.52$$5.52$.01.01.00.000.300.100$4.52$$5.52$.01.01.00.000.300.100$5.52$$6.52$.01.01.00.000.300.100$7.32$$7.70$.01.01.00.0001.400.100$7.70$$8.70$.01.01.00.0001.400.100$9.70$10.66.01.01.00.000.300.100$1.00$.001.01.00.000.300.100$1.00$.001.01.00.000.300.100$2.00$.001.01.00.000.300.100$3.00$.01.01.00.000.300.100$4.00$.01.01.00.000.300.100$5.00$$5.79$.01.01.00.000.300.100$5.00$.02.01.01.00.000.300.100$6.25$.01.01.00.000.300.100$6.25$.01.01.00.000.300.100$7.25$$8.25$.01.02.00.000.300$7.27$</td><td>FROMTO4Pb3Zn oz/tAg oz/tAu g/tAgg/tAu%Fe1.522.52.01.01.00.000.300.100.023.524.52.01.01.00.000.300.100.024.525.52.01.01.00.000.300.100.025.526.52.01.01.00.000.300.100.025.737.72.01.01.00.000.300.100.027.737.70.01.01.00.000.1400.100.028.709.70.01.01.00.000.1400.100.029.7010.06.01.01.00.000.300.100.021.002.00.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.004.00.01.01.00.000.300.100.024.005.00.01.02.00.000.300.100.024.259.25.01.01.00.000.300.100.022.728.25.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.01.01.00.000.300.100.02<</td></td>	FROMTO $\$Pb$ $\$Zn$ oz/tAg 1.52 2.52 $.01$ $.01$ $.00$ 2.52 3.52 $.01$ $.01$ $.00$ 3.52 4.52 $.01$ $.01$ $.00$ 4.52 5.52 $.01$ $.01$ $.00$ 5.52 6.52 $.01$ $.01$ $.00$ 7.32 7.70 $.01$ $.01$ $.00$ 7.32 7.70 $.01$ $.01$ $.00$ 7.70 8.70 $.01$ $.01$ $.00$ 9.70 10.06 $.01$ $.01$ $.00$ 2.00 3.00 $.01$ $.01$ $.00$ 2.00 3.00 $.01$ $.01$ $.00$ 3.00 4.00 $.01$ $.01$ $.00$ 5.00 5.79 $.01$ $.01$ $.00$ 5.00 5.79 $.01$ $.01$ $.00$ 7.25 8.25 $.01$ $.01$ $.00$ 7.25 8.25 $.01$ $.01$ $.00$ 7.25 9.60 $.01$ $.01$ $.00$ 7.25 9.60 $.01$ $.01$ $.00$ 7.25 9.60 $.01$ $.01$ $.00$ 7.25 9.60 $.01$ $.01$ $.00$ 7.70 3.06 $.04$ $.02$ $.00$ 3.06 $.04$ $.02$ $.00$ 3.06 $.04$ $.02$ $.00$ 3.06 $.04$ $.02$ $.00$ 7.70 3.06 $.01$ $.01$ </td <td>FROM TO %Pb %Zn oz/tAg oz/tAg 1.52 2.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 4.52 5.52 .01 .01 .00 .000 5.52 6.52 .01 .01 .00 .000 7.70 8.70 .01 .01 .00 .000 9.70 10.66 .01 .01 .00 .000 .00 1.00 .01 .00 .000 .000 .00 1.00 .01 .01 .00 .000 .00 3.00 .01 .01 .00 .000 .00 5.00 .01 .01 .00 .000 .01 .01 .00 .000 .000 .000 .02 9.60 .01 .01 .00</td> <td>FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg$1.52$$2.52$$.01$$.01$$.00$$.000$$.300$$2.52$$3.52$$.4.52$$.01$$.01$$.00$$.000$$.300$$4.52$$5.52$$.01$$.01$$.00$$.000$$.300$$5.52$$6.52$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.400$$8.70$$9.70$$.01$$.01$$.00$$.000$$.300$$7.70$$8.70$$.01$$.01$$.00$$.000$$.300$$1.00$$2.00$$.01$$.01$$.00$$.000$$.300$$1.00$$2.00$$.01$$.01$$.00$$.300$$3.00$$4.00$$.01$$.01$$.00$$.300$$4.00$$5.00$$.01$$.02$$.00$$.300$$5.00$$5.79$$0.25$$.01$$.01$$.00$$.300$$5.25$$.01$$.01$$.00$$.300$$.300$$7.25$$8.25$$.01$$.01$$.00$$.300$$7.25$$8.25$$.01$$.01$$.00$$.300$$7.25$$.01$$.01$$.00$$.300$$7.27$$3.06$$.01$$.01$$.00$$.300$$7.27$$3.06$$.01$$.01$$.00$</td> <td>FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg g/tAu$1.52$$2.52$.01.01.00.000.300.100$3.52$$4.52$.01.01.00.000.300.100$4.52$$5.52$.01.01.00.000.300.100$4.52$$5.52$.01.01.00.000.300.100$5.52$$6.52$.01.01.00.000.300.100$7.32$$7.70$.01.01.00.0001.400.100$7.70$$8.70$.01.01.00.0001.400.100$9.70$10.66.01.01.00.000.300.100$1.00$.001.01.00.000.300.100$1.00$.001.01.00.000.300.100$2.00$.001.01.00.000.300.100$3.00$.01.01.00.000.300.100$4.00$.01.01.00.000.300.100$5.00$$5.79$.01.01.00.000.300.100$5.00$.02.01.01.00.000.300.100$6.25$.01.01.00.000.300.100$6.25$.01.01.00.000.300.100$7.25$$8.25$.01.02.00.000.300$7.27$</td> <td>FROMTO4Pb3Zn oz/tAg oz/tAu g/tAgg/tAu%Fe1.522.52.01.01.00.000.300.100.023.524.52.01.01.00.000.300.100.024.525.52.01.01.00.000.300.100.025.526.52.01.01.00.000.300.100.025.737.72.01.01.00.000.300.100.027.737.70.01.01.00.000.1400.100.028.709.70.01.01.00.000.1400.100.029.7010.06.01.01.00.000.300.100.021.002.00.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.004.00.01.01.00.000.300.100.024.005.00.01.02.00.000.300.100.024.259.25.01.01.00.000.300.100.022.728.25.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.01.01.00.000.300.100.02<</td>	FROM TO %Pb %Zn oz/tAg oz/tAg 1.52 2.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 3.52 4.52 .01 .01 .00 .000 4.52 5.52 .01 .01 .00 .000 5.52 6.52 .01 .01 .00 .000 7.70 8.70 .01 .01 .00 .000 9.70 10.66 .01 .01 .00 .000 .00 1.00 .01 .00 .000 .000 .00 1.00 .01 .01 .00 .000 .00 3.00 .01 .01 .00 .000 .00 5.00 .01 .01 .00 .000 .01 .01 .00 .000 .000 .000 .02 9.60 .01 .01 .00	FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg 1.52 2.52 $.01$ $.01$ $.00$ $.000$ $.300$ 2.52 3.52 $.4.52$ $.01$ $.01$ $.00$ $.000$ $.300$ 4.52 5.52 $.01$ $.01$ $.00$ $.000$ $.300$ 5.52 6.52 $.01$ $.01$ $.00$ $.000$ $.300$ 7.70 8.70 $.01$ $.01$ $.00$ $.000$ $.300$ 7.70 8.70 $.01$ $.01$ $.00$ $.000$ $.400$ 8.70 9.70 $.01$ $.01$ $.00$ $.000$ $.300$ 7.70 8.70 $.01$ $.01$ $.00$ $.000$ $.300$ 1.00 2.00 $.01$ $.01$ $.00$ $.000$ $.300$ 1.00 2.00 $.01$ $.01$ $.00$ $.300$ 3.00 4.00 $.01$ $.01$ $.00$ $.300$ 4.00 5.00 $.01$ $.02$ $.00$ $.300$ 5.00 5.79 0.25 $.01$ $.01$ $.00$ $.300$ 5.25 $.01$ $.01$ $.00$ $.300$ $.300$ 7.25 8.25 $.01$ $.01$ $.00$ $.300$ 7.25 8.25 $.01$ $.01$ $.00$ $.300$ 7.25 $.01$ $.01$ $.00$ $.300$ 7.27 3.06 $.01$ $.01$ $.00$ $.300$ 7.27 3.06 $.01$ $.01$ $.00$	FROMTO%Pb%Zn oz/tAg oz/tAu g/tAg g/tAu 1.52 2.52 .01.01.00.000.300.100 3.52 4.52 .01.01.00.000.300.100 4.52 5.52 .01.01.00.000.300.100 4.52 5.52 .01.01.00.000.300.100 5.52 6.52 .01.01.00.000.300.100 7.32 7.70 .01.01.00.0001.400.100 7.70 8.70 .01.01.00.0001.400.100 9.70 10.66.01.01.00.000.300.100 1.00 .001.01.00.000.300.100 1.00 .001.01.00.000.300.100 2.00 .001.01.00.000.300.100 3.00 .01.01.00.000.300.100 4.00 .01.01.00.000.300.100 5.00 5.79 .01.01.00.000.300.100 5.00 .02.01.01.00.000.300.100 6.25 .01.01.00.000.300.100 6.25 .01.01.00.000.300.100 7.25 8.25 .01.02.00.000.300 7.27	FROMTO 4Pb3 Zn oz/tAg oz/tAu g/tAg g/tAu %Fe 1.522.52.01.01.00.000.300.100.023.524.52.01.01.00.000.300.100.024.525.52.01.01.00.000.300.100.025.526.52.01.01.00.000.300.100.025.737.72.01.01.00.000.300.100.027.737.70.01.01.00.000.1400.100.028.709.70.01.01.00.000.1400.100.029.7010.06.01.01.00.000.300.100.021.002.00.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.004.00.01.01.00.000.300.100.024.005.00.01.02.00.000.300.100.024.259.25.01.01.00.000.300.100.022.728.25.01.01.00.000.300.100.022.003.00.01.01.00.000.300.100.023.01.01.00.000.300.100.02<

HOLE-ID	FROM	TO	% Pb	%Zn c	oz/tAg	oz/tAu	n g∕tAg	g/tAu	%Fe	%As
13-32	7.45	8.45	.01	.01	.00	.000	3.000	.100	. 02	03
.3-32	8.45	9.45	.01	.01	.00	.000	2.000	.100	.02	.05
83-32	9.45	10.06	.03	.02	.00	.000	2.000	.100	.05	.03
83-33	.00	.73	.91	5.06	.00	.000	29.500	4.000	5.97	1,49
83-33	.73	1.52	.10	.80	.00	.000	3.400	.300	.90	.08
83-33	1.52	2.52	.01	.02	.00	.000	1.400	.100	.03	.01
83-33	2.52	3.52	.01	.02	.00	.000	.300	.100	.03	.00
83-33	3.52	4.52	.01	.01	.00	.000	.700	.100	.02	.00
83-33	4.52	5.52	.01	.01	.00	.000	.700	.100	.02	.00
83-33	5.52	5.79	.01	.01	.00	.000	.300	.100	.02	.01
83-33	5.79	6.55	.01	.01	.00	.000	1.400	.100	.02	.00
03-33	0.00 7.20	7.52	.01	.01	.00	.000	1 400	.100	.02	.01
83-33	7.52	8 62	01	.01	.00	.000	1.400	.100	.02	.04
83-33	8 62	9.62	01	.01	.00	000	300	100	+ 0 2	.00
83-33	9.62	10.06	.01	.01	.00	.000	300	100	.02	.00
83-34	.00	.85	.01	.01	.00	.000	2,000	.100	. 02	.00
83-34	.85	1.72	.77	1.41	.00	.000	16.100	.300	2.18	.39
83-34	1.72	2.80	.27	.85	.00	.000	1.700	.100	1.12	.03
83-34	2.80	3.14	2.78	4.60	.00	.000	131.300	20.800	7.38	13.20
83-34	3.14	3.70	.70	.38	.00	.000	26.400	10.400	1.08	6.06
83-34	3.70	4.40	.03	.02	.00	.000	1.400	.200	.05	.17
83-34	4.40	5.04	.06	.01	.00	.000	15.800	1.400	.07	2.97
83-34	5.04	5.60	.17	.20	.00	.000	4.800	2.200	.37	3.85
83-34	5.60	5.66	.09	16 20	.00	.000	4.100	.900	.11	2.03
83-34	5.60	5.8Z	.19	10.30	.00	.000	9.900	10.900	16,49	11.50
3-34	6.27	6 63	.23	.57	.00	.000	3 100	.500	.02	.30
83-34	6.63	6.78	.07	.03	.00	000	4 500	500	10	.29
83-34	6.78	7.23	.01	.02	.00	.000	1.000	.200	.03	.05
83-34	7.23	8.23	.01	.01	.00	.000	1.400	.100	.02	.02
83-34	8.23	9.23	.01	.01	.00	.000	2.000	.100	.02	.01
83-34	9.23	10.23	.01	.01	.00	.000	.300	.100	.02	.00
83-34	10.23	11.23	.01	.01	.00	.000	.300	.100	.02	.00
83-34	11.23	11.98	.01	.01	.00	.000	.300	.100	.02	.00
83-34	11.98	12.90	.01	.01	.00	.000	.300	.100	.02	.00
83~34	12.90	13.90	.01	.02	.00	.000	.300	.100	.03	.06
83-34	14 90	14.90 15 QA	.01	.01	.00	.000	2 000	.100	.02	.00
83-34	15,90	16 90	01	.01	.00	.000	2.000	.100	.02	.00
83-34	16.90	17.56	.01	.02	.00	.000	300	100	.02	.00
83-34	17.56	17.88	.01	.01	.00	.000	1.700	.100	.02	.00
83-34	17.88	17.98	.01	.01	.00	.000	2.000	.100	.02	.00
83-34	17.98	18.98	.01	.01	.00	.000	.300	.100	.02	.00
83-34	18.98	19.98	.01	.01	.00	.000	.300	.100	.02	.00
83-34	19.98	20.42	.01	.08	.00	.000	.300	.100	.09	.00
83-35	.00	1.00	.01	.01	.00	.000	2.000	.100	.02	.01
03-32	2 00	2.00	.01	.01	.00	.000	1./00	.100	.02	.01
87-75	2.00	2 00	.01	.UI 01	.00	.000	1.400	.100	.02	.04
83-35	4 00	4 78	.01	.01	.00	000	1 700	.100	.02	.11
83-35	4 38	5,38	.01	.01	.00	000	1 700	100	.02	.V5 00
13 - 35	5.38	6.38	.01	_ 01	.00	.000	200	100	.02	.00
-3-35	6.38	7.38	.01	.01	.00	.000	.300	.100	.02	.19
HOLE-ID	FROM	TO	%Pb	%Zn	oz/tAg	oz/tAu	ı g/tAg	g/tAu	%Fe	%As
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83-35	7.38	8.38	.01	.01	.00	.000	4.100	.100	.02	.03
33-35	8.38	9.40	.01	.01	.00	.000	3.700	.100	.02	.03
83-36	.00	1.00	.01	.01	.00	.000	2.000	.100	.02	.09
83-36	1.00	1.35	.01	.01	.00	.000	2.000	.100	.02	.09
83-36	1.35	2.25	.01	.01	.00	.000	1.400	.100	.02	.00
83-36	2.20	3.20	.01	10.	.00	.000	1.400	.100	.02	.00
83-36	J.20 4 25	4.20	.01	.01	.00	.000	3.100	.100	.02	.00
83-36	5 25	6 25	.01	101	.00	.000	2 000	100	.02	.02
83-36	6.25	7.25	.01	.01	.00	.000	1.400	.100	.04	.41
83-36	7.25	8.09	.02	.01	.00	.000	1.700	.100	.03	.38
83-36	8.09	9.09	.01	.01	.00	.000	2.000	.100	.02	.33
83-36	9.09	9.75	.02	.01	.00	.000	2.000	3.600	.03	.03
84-02	63.50	64.50	.01	.01	.00	.000	1.700	.400	.02	.97
84-02	64.50	64.56	.18	.01	.00	.000	12.300	2.200	.19	22.50
84-02	64.56	65.53	1.42	3.58	.00	.000	26.400	.300	5.00	.31
84-02	65.53	66.01	.21	1.23	.00	.000	8.600	.300	1.44	.03
84-02	66.01	6/.01	2.42	14.80	.00	.000	50.900	.500	17.22	.01
84-02 84-02	67.01 69.01	60.01	2.31	8.86	.00	.000	32.700	.200	10.17	.01
84-02	69 01		2.30	7.94	.00	.000	25.500	.400	10.30	.02
84-02	70.00	70 66	2.24	1.54	.00	.000	2 600	.500	10.10	.04
84-02	70.66	71.66	. 0.5	.04	.00	.000	4.400	400	.07	.03
84-02	71.66	72.30	.28	.30	.00	.000	7.300	.200	.58	.90
84-02	72.30	72.73	.19	1.00	.00	.000	3.700	.400	1.19	.11
84-02	72.73	72.92	.04	.07	.00	.000	1.900	.200	.11	.06
84-02	72.92	73.13	.03	.04	.00	.000	3.000	.400	.07	.05
34-02	73.13	73.39	.02	.03	.00	.000	.300	.200	.05	.06
84-02	73.39	73.87	.04	1.30	.00	.000	3.000	1.700	1.34	1.81
84-02	73.87	74.47	.84	5.54	.00	.000	15.400	8.800	6.38	7.99
84-02	/4.4/	75.12	.30	1.16	.00	.000	3.800	2.300	1.46	3.65
84-02	75.12	76 03	6 96	24 00	.00	.000	126 100	10.000	20.06	3.21
84~02	76.03	77 11	6.50	24.00	.00	.000	12 700	4.700	1 10	1.24
84-02	77.11	77.86	.08	.08	.00	.000	4.800	100	1,19	. 37
84-02	77.86	78.16	1.06	10.70	.00	.000	30.800	1,600	11.76	.89
84-02	78.16	79.16	.08	.13	.00	.000	5.500	.700	.21	.85
84-02	79.16	80.16	.04	.13	.00	.000	3.400	1.000	.17	2.47
84-02	80.16	80.56	.04	.02	.00	.000	2.700	.900	.06	1.77
84-02	80.56	80.91	2.50	2.96	.00	.000	50.700	11.100	5.46	6.12
84-02	80.91	81.69	.04	.05	.00	.000	.300	.300	.09	.09
84-04	47.1V 97 56	47.24	.08	.09	.00	.000	2.200	4.700	.17	4.21
84-04	88 08	80.00 89 N8	.29	.09	.00	.000	5.300	.200	.38	.02
84~04	89.08	89.96	10 30	12 50	.00	.000	217 600	14 100	22 80	.31
84-04	89.96	90.79	16.60	12.50	.00	.000	355 600	12 600	29 10	3 64
84-04	90.79	90.92	37.30	15.30	.00	.000	725,700	12.000	52.60	1.07
84-04	90.92	91.01	7.99	22.20	.00	.000	154.300	8.200	30.19	1.43
84-04	91.01	91.88	.53	7.05	.00	.000	14.400	.700	7.58	.63
84-04	91.88	92.54	.81	3.15	.00	.000	12.000	1.700	3.96	1.04
84-04	92.54	93.54	.06	.17	.00	.000	.100	.200	.23	.16
84-04	93.54	94.54	.04	.03	.00	.000	5.900	.300	.07	.93
94-04	94.54	95.54	.02	.02	.00	.000	3.200	.300	.04	.64
44-04	95.54	96.54	.01	.02	.00	.000	3.400	.100	.03	.02

HOLE-ID	FROM	TO	%₽b	%Zn	oz/tAg	oz/tAu	ıg/tAg	g/tAu	%Fe	%As
- 84-04	96.54	97.54	.01	.01	.00	.000	.100	.100	.02	.00
4-04	97.54	98.40	.01	.03	.00	.000	2.700	.700	.04	2.15
84-04	98.40	99.41	.01	.01	.00	.000	2.500	.200	.02	.11
84-04	99.41	100.41	.01	.01	.00	.000	4.600	.200	.02	.04
84-04	100.41	101.41	.01	.01	.00	.000	4.500	.300	.02	.01
84-04	101.41	102.41	.01	.01	.00	.000	4.100	.100	.02	.01
84-04	102.41	103.40	.01	.01	.00	.000	4.000	.100	.02	.00
84-04	103.40	104.01	.01	.01	.00	.000	2.500	.300	.02	.00
84-04	104.01	104.71	.03	.01	.00	.000	3.100	.300	.04	.21
84-04	104.71	105.51	.19	.19	.00	.000	6.700	2.200	.38	1.30
84-04	105.51	106.20	.16	.06	.00	.000	8.600	.300	.22	2.78
84-04	106.20	107.06	.01	.01	.00	.000	.300	.500	.02	.02
84~04	107.06	108.02	.01	.02	.00	.000	3.900	.200	.03	.01
84-04	108.02	108.78	.01	.01	.00	.000	5.300	.200	.02	.47
84-04	108.78	109.62	.01	.01	.00	.000	1,200	.100	.02	.07
84-04	109.62	109.99	.01	.01	.00	.000	1.900	.200	.02	.07
84-04	109.99	110.75	.01	.01	.00	.000	2.500	.300	.02	.43
84-04	110.75	111.45	.09	.21	.00	.000	5.900	.300	.30	.24
84-04	111.45	112.35	.07	.01	.00	.000	2.600	.100	.08	.02
84-04	112.35	113.25	.12	.04	.00	.000	5.000	1.200	.16	.89
84-04	113.25	114.04	.02	.04	.00	.000	3.300	.100	.06	.06
84-04	114.04	114.82	.01	.06	.00	.000	3.800	.300	.07	.17
84-04	114.82	115.82	.01	.01	.00	.000	2.600	.100	.02	.01
84-04	115.82	116.82	.01	.01	.00	.000	2.400	.300	.02	.19
84-05	25.18	26.18	.01	.01	.00	.000	1.100	.030	.02	.01
84-05	26.18	26.35	.02	.03	.00	.000	2.500	.200	.05	.01
84~05	26.35	26.56	3.70	±2.70	.00	.000	55.900	1.600	16.40	.94
4-05	26.56	27.12	.03	.09	.00	.000	4.100	.200	.12	.01
84-05	27.12	28.12	.01	.01	.00	.000	2.600	.100	.02	.00
84-05	20.12	29.12	.01	.03	.00	.000	2.100	.100	.04	.00
84-05	29.12	29.52	.02	.01	.00	.000	2.300	.500	.03	.98
84-05	29.52	30.52	.01	.01	.00	.000	.500	.100	.02	.01
04-05 04-05	41.10	40.70	.01	.01	.00	.000	.500	.200	.02	.01
84-05	40.70	49.79	.Ui	.US 9 59	00	.000	220 100	13 000	10 22	. LU
84-05	50 27	50.27	7 49	11 50	.00	.000	179 200	13.000	10.23	2.30
84-05	50.27	50.40	1.40	11.50	.00	.000	10 300	700	1 15	4.05
84-05	50.81	50.01	66	.50	.00	000	9 300	21 500	1 22	14 40
84-05	50.88	51 58	.00	3 26	.00	000	1 800	1 400	4 23	1 23
84-05	51.58	52.06	5.51	9,20	.00	.000	86.800	31 800	14 71	18 10
84-05	52.06	52.87	.18	.17	.00	.000	6.200	2.000	.35	1,16
84-05	52.87	53.68	.39	.40	.00	.000	10.700	. 900	.79	72
84-05	53.68	54.49	.04	.04	.00	.000	1.000	.400	.08	.09
84-05	54.49	55.67	.15	.13	.00	.000	3.600	.500	.28	1.40
84-05	55.67	56.07	2.28	2.39	.00	.000	70.500	23.400	4.67	17.10
84-05	56.07	56.59	.11	.05	.00	.000	6.300	.500	.16	.46
84-05	56.59	57.48	.30	.06	.00	.000	14.900	.900	.36	1.10
84-05	57.48	57.99	.71	.33	.00	.000	48.300	3.100	1.04	4.54
84-05	57.99	58.71	.16	.03	.00	.000	6.700	2.200	.19	.53
84-05	58.71	59.42	.64	.70	.00	.000	15.700	.700	1.34	.59
84-05	59.42	60.05	.30	.28	.00	.000	12.000	1.000	.58	.32
84-05	60.05	60.82	.90	.06	.00	.000	5.100	.400	.96	.14
94-05	60.82	61.34	.20	.09	.00	.000	8.000	.900	.29	.47
4-05	61.34	62.34	.01	.01	.00	.000	1.100	.300	.02	.02

HOLE-ID	FROM	то	%Pb	%Zn	oz/tAg	oz/tAu	n g∕tAg	g/tAu	% Fe	%As
64-05	62.34	63.28	.01	.01	.00	.000	.700	.100	.02	.01
84-05	63.28	64.25	.01	.04	.00	.000	.900	.500	.05	.05
84-05	64.25	65.10	.05	.04	.00	.000	3.800	.300	.09	.13
84-05	89 90	90.00	.01	10.	.00	.000	.300	.400	.02	.14
84-06	81.28	82.28	.01	.01	.00	.000	1.800	.300	. 02	.01
84-06	82.28	83.06	.01	.02	.00	.000	2.500	.200	.03	.02
84-06	83.06	83.14	5.00	9.58	.00	.000	147.600	9.400	14.58	7.67
84-06	83.14	83.28	.57	1.28	.00	.000	31.700	18.400	1.85	12.90
84-06	83.28	83.57	.06	.64	.00	.000	3.400	2.100	.70	3.41
84-06	83.5/	83.62	5.52	11.30	.00	.000	110.500	5.400	16.82	1.50
84-06	8/ 11	8A 27	5 00	.00 ר ר	.00	.000	195 100	.600	12 01	.//
84-06	84.27	84.85	.12	. 21	00.	.000	5 900	3.500	12.01	2.04
84-06	84.85	85.56	.13	.13	.00	.000	3,200	.300	.26	.07
84-06	85.56	85.64	.68	.23	.00	.000	22.200	3.800	.91	9.03
84-06	85.64	85.79	.20	.37	.00	.000	8.200	.100	.57	.79
84-06	85.79	85.84	7.91	.62	.00	.000	140.900	6.500	8.53	8.79
84-06	85.84	86.84	.05	.52	.00	.000	3.700	.400	.57	.11
84-06	86.84	87.84	.03	.02	.00	.000	.300	.100	.05	.01
84-06	88 84	89.84	.01	+01	.00	.000	2 500	.100	.02	.00
84-06	89.84	90.84	.18	.01	.00	.000	2.300	4.400	.02	2.78
84-06	90.84	91.84	.01	.01	.00	.000	2,600	.100	. 02	.02
84-06	91.84	92.84	.07	.02	.00	.000	1.900	.200	.09	.12
84-06	92.84	93.84	.05	.02	.00	.000	5.400	2.100	.07	1.18
- 84-06	93.84	94.84	.04	.06	.00	.000	.300	.400	.10	.52
34-06	94.84	95.84	.08	.07	.00	.000	3.900	.200	.15	.13
84-06	95.84	90.04 07 01	.03	.03	.00	.000	1.400	.100	.06	.01
84-06	97 84	98.84	.01	.05	.00	.000	1.700	.300	.05	.12
84-06	98.84	99.84	.01	.01	.00	.000	.300	.100	.02	.01
84-06	99.84	100.84	.01	.01	.00	.000	.700	.100	.02	.01
84-07	39.08	39.88	.01	.01	.00	.000	2.100	.100	.02	.00
84-07	39.88	40.88	.01	.01	.00	.000	.070	.100	.02	.00
84-07	40.88	41.88	.01	.03	.00	.000	1.400	.100	.04	.00
84-07	41.88	42.23	1.14	4.11	.00	.000	25.100	.300	5.25	.00
84-07	42.28	43.31	.04	7 16	.00	.000	13.200	.500	37.34	.00
84-07	43.31	43.95	.18	2.92	.00	.000	4.800	.100	3 10	.00
84-07	43.95	44.50	.04	.33	.00	.000	3.400	.100	.37	.00
84-07	44.50	45.05	.01	.26	.00	.000	.300	.400	.27	.01
84-07	45.05	45.23	.03	.29	.00	.000	1.500	1.900	.32	.02
84-07	45.23	45.72	.72	14.40	.00	.000	12.700	.300	15.12	.02
84-07	45.72	46.24	13.70	16.80	.00	.000	193.900	.400	30.50	.05
84-07	46.24	40.84	1.03	11 10	.00	.000	14.800	.300	2.06	.57
84-07	46.96	40.90	32.30	5 64	.00	.000	15 600	1.900	43.60	.07
84-07	47.24	47.93	2.24	9.03	.00	.000	40.100	11.300	11 27	02. 9 NR
84-07	47.93	48.36	.40	.86	.00	.000	14.300	4.200	1.26	5.04
84-07	48.36	48.60	2.96	11.70	.00	.000	120.700	22,600	14.66	6.84
84-07	48.60	49.10	.66	6.94	.00	.000	13.300	1.100	7.60	.78
34-07	49.10	49.67	1.22	6.20	.00	.000	34.900	9.000	7.42	8.30
d4-07	49.67	50.62	2.42	3.58	.00	.000	78.700	11.100	6.00	17.70

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84-08 64.82 65.48 01 01 00 000 2.700 100 02 $84-08$ 65.48 65.67 $c5.88$ 16 02 00 000 24.400 1.000 18 2 $84-08$ 65.67 65.88 66.63 10 01 00 000 24.400 1.000 18 2 $84-08$ 65.67 65.88 66.63 10 01 00 000 14.600 500 11 1 $84-08$ 66.63 67.38 15 09 00 000 14.600 500 11 1 $84-08$ 67.38 68.12 04 12.00 00 000 14.600 500 110 18.04 $84-08$ 68.12 68.39 60.4 12.00 00 000 152.000 9.100 18.04 4 $84-08$ 69.06 69.37 48 90 00 000 17.300 3.200 1.38 8 $84-08$ 69.27 69.88 3.68 26.60 00 000 17.300 3.200 1.38 8 $84-08$ 70.27 71.37 13 1.06 00 000 10.700 7.100 1.19 7 $84-08$ 71.97 72.73 $.05$ $.34$ 00 000 5.300 2.200 $.39$ 1 $84-08$ 71.97 72.73 $.05$ $.34$ 00 000 5.300 $2.$	01
84-08 65.48 65.67 .01 .01 .00 .000 6.900 .600 .02 84-08 65.67 65.88 .16 .02 .00 .000 24.400 1.000 .18 2 84-08 65.88 66.63 .10 .01 .00 .000 14.600 .500 .11 1 84-08 66.63 67.38 .15 .09 .00 .000 18.500 .700 .24 84-08 67.38 68.12 .04 .01 .00 .000 18.500 .700 .24 84-08 68.12 68.39 6.04 12.00 .00 .000 152.000 9.100 18.04 4 84-08 68.39 69.06 .08 .05 .00 .000 1.000 .13 84-08 69.37 69.88 3.68 26.60 .00 .000 1.100 4.83 1 84-08 69.88 70.27 .23 4.60 .00 .000 10.700 7.100 1.19	01
84-08 65.67 65.88 $.16$ $.02$ $.00$ $.000$ 24.400 1.000 $.18$ 2 $84-08$ 65.88 66.63 $.10$ $.01$ $.00$ $.000$ 14.600 $.500$ $.11$ 1 $84-08$ 66.63 67.38 $.15$ $.09$ $.00$ $.000$ 18.500 $.700$ $.24$ $84-08$ 67.38 68.12 $.04$ $.01$ $.00$ $.000$ 4.300 1.200 $.05$ $84-08$ 68.12 68.39 6.04 12.00 $.00$ $.000$ 152.000 9.100 18.04 4 $84-08$ 68.39 69.06 $.08$ $.05$ $.00$ $.000$ 1.300 3.200 1.38 8 $84-08$ 69.06 69.37 $.48$ $.90$ $.00$ $.000$ 17.300 3.200 1.38 8 $84-08$ 69.37 69.88 3.68 26.60 $.00$ $.000$ 7.800 1.100 4.83 1 $84-08$ 70.27 71.37 $.13$ 1.06 $.00$ $.000$ 7.800 1.100 4.83 1 $84-08$ 71.97 72.73 $.05$ $.34$ $.00$ $.000$ 5.300 2.200 $.39$ 1 $.4-08$ 72.73 73.49 $.13$ $.17$ $.00$ $.000$ 37.800 2.000 $.369$ 1 $84-08$ 74.25 74.60 1.90 9.60 $.00$ $.000$ 7.800 2.000 $.3$	01
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64 - 08 68.39 69.06 $.08$ $.05$ $.000$ 132.000 9.100 18.04 4 $84 - 08$ 69.06 69.37 $.48$ $.90$ $.00$ $.000$ 17.300 3.200 1.38 8 $84 - 08$ 69.37 69.88 3.68 26.60 $.00$ $.000$ 81.400 5.600 30.28 2 $84 - 08$ 69.37 69.88 3.68 26.60 $.00$ $.000$ 81.400 5.600 30.28 2 $84 - 08$ 69.88 70.27 $.23$ 4.60 $.00$ $.000$ 10.700 7.100 1.19 7 $84 - 08$ 70.27 71.37 $.13$ 1.06 $.00$ $.000$ 23.800 24.900 9.40 13 $84 - 08$ 71.37 71.97 $.27$ 9.13 $.00$ $.000$ 5.300 2.200 $.39$ 1 $84 - 08$ 71.97 72.73 $.05$ $.34$ $.00$ $.000$ 5.300 2.000 $.369$ 1 $4 - 08$ 73.49 74.25 $.95$ 2.74 $.00$ $.000$ 37.800 2.000 3.69 1 $84 - 08$ 74.25 74.60 1.90 9.60 $.00$ $.000$ 71.800 7.100 11.50 5 $84 - 08$ 74.60 75.32 1.60 $.92$ $.00$ $.000$ 52.700 3.600 2.52 4 $84 - 08$ 76.14 76.89 1.17 3.05 $.00$ <	. 29 1 26
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84-08 69.37 69.88 3.68 26.60 $.00$ $.000$ 81.400 5.600 30.28 2 $84-08$ 69.88 70.27 $.23$ 4.60 $.00$ $.000$ 7.800 1.100 4.83 1 $84-08$ 70.27 71.37 $.13$ 1.06 $.00$ $.000$ 10.700 7.100 1.19 $84-08$ 71.37 71.97 $.27$ 9.13 $.00$ $.000$ 23.800 24.900 9.40 13 $84-08$ 71.97 72.73 $.05$ $.34$ $.00$ $.000$ 5.300 2.200 $.39$ 1 $.4-08$ 72.73 73.49 $.13$ $.17$ $.00$ $.000$ 11.300 3.100 $.30$ 2 $84-08$ 73.49 74.25 $.95$ 2.74 $.00$ $.000$ 37.800 2.000 3.69 1 $84-08$ 74.25 74.60 1.90 9.60 $.00$ $.000$ 71.800 7.100 11.50 5 $84-08$ 74.60 75.32 1.60 $.92$ $.00$ $.000$ 52.700 3.600 2.52 4 $84-08$ 75.32 76.14 $.93$ 12.70 $.00$ $.000$ 35.000 7.500 13.63 11 $84-08$ 76.14 76.89 1.17 3.05 $.00$ $.000$ 27.600 4.000 4.22 6	.42
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84-08 73.49 74.25 .95 2.74 .00 .000 37.800 2.000 3.69 1 84-08 74.25 74.60 1.90 9.60 .00 .000 71.800 7.100 11.50 5 84-08 74.60 75.32 1.60 .92 .00 .000 52.700 3.600 2.52 4 84-08 75.32 76.14 .93 12.70 .00 .000 35.000 7.500 13.63 11 84-08 76.14 76.89 1.17 3.05 .00 .000 27.600 4.000 4.22 6	2.21
84-08 74.25 74.60 1.90 9.60 .00 .000 71.800 7.100 11.50 5 84~08 74.60 75.32 1.60 .92 .00 .000 52.700 3.600 2.52 4 84~08 75.32 76.14 .93 12.70 .00 .000 35.000 7.500 13.63 11 84-08 76.14 76.89 1.17 3.05 .00 .000 27.600 4.000 4.22 6	1.44
84~08 74.60 75.32 1.60 .92 .00 .000 52.700 3.600 2.52 4 84~08 75.32 76.14 .93 12.70 .00 .000 35.000 7.500 13.63 11 84~08 76.14 76.89 1.17 3.05 .00 .000 27.600 4.000 4.22 6	5.13
84-08 75.32 76.14 .93 12.70 .00 .000 35.000 7.500 13.63 11 84-08 76.14 76.89 1.17 3.05 .00 .000 27.600 4.000 4.22 6	4.54
84-08 76.14 76.89 1.17 3.05 .00 .000 27.600 4.000 4.22 6	1.60
	5.75
84-08 76.89 77.64 1.31 6.30 .00 .000 26.500 4.400 7.61 5	5.17
84-08 77.64 78.21 .27 6.52 .00 .000 7.700 .500 6.79	.80
84-08 78.21 78.43 5.43 9.93 .00 .000 140.900 10.600 15.36 7	7.60
84-08 78.43 78.75 .25 .89 .00 .000 10.400 .500 1.14	.50
84-08 78.75 79.25 5.15 15.30 .00 .000 120.800 2.600 20.45 1	L.79
84-08 79.29 79.55 .30 .78 .00 .000 4.700 1.500 1.08 3	3.84
84-08 79.55 79.73 10.80 9.60 .00 .000 271.600 10.800 20.40 5	5.00
84-08 79.73 80.16 1.45 1.22 .00 .000 26.300 1.100 2.67	.78
84-08 80.16 80.67 .21 .26 .00 .000 9.400 .200 .47	.19
84-08 80.67 81.25 .12 .10 .00 .000 9.400 .200 .22	.25
84-08 81.25 81.37 1.12 30.00 .00 .000 42.600 .500 31.12	.07
84-08 81.37 82.37 .06 1.08 .00 .000 1.500 .200 1.14	.13
84~08 82.37 83.37 .32 .50 .00 .000 18.700 .500 .82	.20
84-08 83.37 83.68 .24 .30 .00 .000 9.300 2.300 .54 4	1.23
84-09 78.38 79.38 .22 .45 .00 .000 2.400 .300 .67	.03
84-09 79.38 80.34 .31 1.43 .00 .000 3.600 .500 1.74	.20
84-09 80.34 80.66 .05 .14 .00 .000 .900 .500 .19	.01
84-09 80.66 80.83 2.26 8.52 .00 .000 42.200 1.000 10.78	.04
84-09 80.83 81.80 .07 .29 .00 .000 2.400 .300 36	.12
`4-09 81.80 82.80 .21 1.30 .00 .000 3.800 .300 1 51	. 22
J4-09 82.80 83.66 .16 1.00 .00 .000 3.900 .200 1.16	.36

HOLE-ID	FROM	TO	%Pb	%Zn	oz/tAg	oz/tAu	ı g/tAg	g/tAu	% Fe	%As
< 84-09	83 66	84.20	2.78	9,03	. 00	.000	30.500	3.800	11.81	. 32
84-09	84.20	85.20	.33	1.11	.00	.000	4.900	.500	1.44	.31
84-09	85.20	86.20	.11	.23	.00	.000	5.300	.200	.34	.21
84-09	86.20	87.20	.31	.48	.00	.000	15.400	1.700	.79	4.43
84-09	87.20	88.20	.08	.11	.00	.000	5.500	.700	.19	.50
84-10	.00	1.00	.03	.03	.00	.000	5.200	.300	.06	.13
84-10	1.00	2.00	.54	.45	.00	.000	17.100	.800	.99	.54
84-11	.00	.18	13.70	15.80		.000	108.300	2.100	29.50	.05
84-11	.10	1 62	25	9.03		.000	6 400	.000	12.50	.49
84-11	1.62	2.49	.04	.14	.00	.000	1,400	.700	.18	.03
84-11	2.49	3.37	.06	.39	.00	.000	6.900	.100	.45	.01
84-11	3.37	4.21	.01	.02	.00	.000	1.400	.100	.03	.01
84-11	4.21	4.70	.01	.02	.00	.000	3.400	.100	.03	.00
84-11	4.70	5.70	.03	.13	.00	.000	.300	.400	.16	.02
84-11	5.70	6.23	.01	.01	.00	.000	2.300	.500	.02	.02
84-11	6.23	6.55	10.	.08	.00	.000	6.900	.100	.09	.00
84-11	0.00 7 30	8 30	.03	1.34	00	.000	2.700	.100	1.37	.06
84-13	.30	.46	.02	.00	.00	.000	2.700	100	.08	.00
84-13	.46	1.46	.01	.01	.00	.000	1.000	.400	.02	.03
84-13	1.46	2.46	.04	.04	.00	.000	2.100	.700	.08	1.47
84-13	2.46	3.46	.01	.01	.00	.000	2.100	.500	.02	.01
84-13	3.46	3.86	.06	.07	.00	.000	5.500	.100	.13	.01
84-13	3.86	4.16	.86	6.72	.00	.000	16.000	.500	7.58	.09
84-13	4.10	4.73	.22	1.15	.00	.000	7.300	.300	1.37	.47
84-15	4.73	5.3U 78	.26	3.21	00	.000	1 400	.300	3.47	.01
84-15	. 78	1.78	.00	.21	.00	.000	5.500	.100	. 27	.00
84-15	1.78	2.78	.04	.10	.00	.000	4.100	.100	.14	.00
84-15	2.78	3.78	.03	.13	.00	.000	3.400	.100	.16	.01
84-15	3.78	4.29	.13	.44	.00	.000	4.800	.100	.57	.00
84-15	4.29	4.52	2.68	10.70	.00	.000	48.500	.200	13.38	.03
84-15	4.52	5.09	.11	.45	.00	.000	4.800	.100	.56	.20
84~17 84-17	.50	.80	1 02	.10		.000	21.300	2 000	.51	.31
84-17	.00	1 36	1.93	1.90		.000	6 400	1 900	9.49 28	2,42 1 81
84-17	1.36	1.83	1.10	4.92	.00	.000	35.700	8.200	6.02	9,93
84-17	1.83	2.49	.03	.04	.00	.000	2.300	.500	.07	.11
84~18	.00	.67	.74	.28	.00	.000	19.100	6.200	1.02	12.70
84-18	.67	.93	.05	.92	.00	.000	5.800	.400	.97	.11
84-18	.93	1.93	.03	.03	.00	.000	7.300	.300	.06	.71
84-18	1.93	2.93	.01	.01	00	.000	5.300	.200	.02	.45
04-10 84-18	2.90	3.39	.00	.43		.000	213 600	20 200	.49	.50
84-18	3.82	4.19	.23	. 52	.00	.000	10 600	1 700	17.10	1 16
84~18	4.19	4.82	.02	.04	.00	.000	3.000	.400	.06	.15
84-19	.00	.43	.02	.02	.00	.000	4.000	.100	.04	.10
84-19	.43	.58	1.75	1.62	.00	.000	69.600	7.200	3.37	7.62
84-19	.58	.83	2.40	5.54	.00	.000	79.200	14.700	7.94	8.68
84-19	.83	1.43	.57	1.43	.00	.000	23.500	2.500	2.00	3.33
84-19	1.43	2.18	2.17	4.43	.00	.000	72,200	10.800	6.60	7.75
54-19 21-19	2.10	2.93	7.1/	10.60 13 70		.000	101./00	17.200	25.77	9.29
07 ¥.7		-			• • • •	.000	00.000	TD*000	TO+04	1.00

HOLE-ID	FROM	то	%Pb	%Zn d	oz/tAg	oz/tAı	ı g/tAg	g/tAu	%Fe	%As
94_10	2 69	1 24	21	90	0.0	000	5 500	200	1 10	2.4
24-19	3.00	4,24	. 2 1	.09	.00	.000	5.500	.700	1.10	.37
34-19	4.24	5,24	.04	.10	.00	.000	4.400	.400	.14	.12
84-21	.00	11.	. 33	1 50	.00	.000	10.700	1.600	.43	3.67
84-21	.17	. 97	. / 1	1.09	.00	.000	25.100	7.800	2.30	11.90
84-21	.97	1.30	.40	.31	.00	.000	14.400	8.200	. 19	4.36
84-21	1.30	1.54	1.20	1.64	.00	.000	24.200	3.200	2.84	2.58
84-21	1.54	1./1	. / /	.55	.00	.000	24.500	3.600	1.32	3.53
04-21	1.71	2.60	.30	.03	.00	.000	9.000	3.400	.99	2.45
04-22	.00	.07	. / 4	1.03	.00	.000	27.800	9.900	2.37	6.78
94-22	.07	1.10	0 0 0	0.09	.00	.000	260.200	10 500	10 05	.14
94-22	1,10	1.30	20.00	9.20	.00	.000	209.200	19.500	10.05	13.20
84-22	1.30	2 46	.50	.30	.00	.000	11.500	.800	.00	.4/
84-23	1.71	2.40	.00	.00	.00	.000	2 500	.100	.12	.11
84-23	.00	1 52	.07	.00	.00	.000	2.500 9.500	. 500	54	.04
84-23	1 52	1 98	10 30	15 00	.00	.000	249 000	11 500	25 30	5 32
84-23	1,98	2 98	10.00	40	.00	.000	1 600	500	23.30	32
84-25	.00	1.00	.03	.10	.00	.000	4,700	5,600	13	2 87
84-26	. 00	.09	7,49	8.52	.00	.000	204.700	18,900	16 01	10 20
84-26	.09	.47	1.78	.76	. 00	.000	34,600	1.700	2.54	2.39
84-26	.47	.76	.16	.11	.00	.000	8,100	24.100	.27	9.04
84-26	.76	1.23	4.56	10.50	.00	.000	103.000	36,900	15.06	14.40
84-26	1.23	1.72	.38	.57	.00	.000	12.000	1.700	. 95	1.09
84-26	1.72	2.23	.29	.12	.00	.000	7.700	.500	. 41	.18
84-27	.00	.56	.50	.10	.00	.000	67.600	2.300	. 60	4.18
84-27	.56	.92	.04	.03	.00	.000	2.600	.100	.07	.12
84-27	.92	1.92	.55	.82	.00	.000	13.800	1.900	1.37	1.29
34-28	.00	.30	.05	.02	.00	.000	16.200	1.600	.07	15.10
84-28	.30	1.15	.02	.02	.00	.000	8.600	.300	.04	1.22
84-28	1.15	1.45	.01	.01	.00	.000	2.500	.200	.02	.10
84-28	1.45	2.45	.01	.01	.00	.000	4.100	.100	.02	.09
84-30	.00	.25	6.14	11.10	.00	.000	203.600	29.500	17.24	11.90
84-30	.25	.82	1.93	5.54	.00	.000	54.600	4.400	7.47	2.87
84~30	.82	1.56	.12	.22	.00	.000	3.500	.600	.34	.69
87-01	81.70	82.20	.03	.86	.00	.001	.000	.034	.00	.00
87-01	84.00	96 00	.00	.01	.00	.000	.000	.000	.00	.00
87-01	86.00	87 80	.00	.02	.00	.000	.000	.000	.00	.00
87-01	87 80	89.00	.00	11	.00	.019	.000	.001	.00	.00
87-01	89 00	90 00	.00	.14	.00	.000	1 029	.000	.00	.02
87-01	90.00	92 00	.00	.05	20	000	6 857	274	.00	2 22
87-01	92.00	94.00	.59	. 62	26	006	8 914	206	.00	2.55
87-01	94.00	95.30	.16	2.11	.14	.001	4,800	.034	.00	.00
87-01	95.30	96.60	.01	.08	.00	.067	.000	2.297	.00	2 52
87-01	96.60	98.00	.16	.15	.11	.014	3.771	.480	.00	1.74
87-01	98.00	99.00	5.22	8.89	4.46	.309	152.916	10.594	.00	6.51
87-01	99.00	100.50	10.80	15.90	8.98	.181	307.888	6.206	.00	5.28
87-01	100.50	102.00	.51	.79	1.08	.122	37.029	4.183	.00	3.30
87-01	102.00	103.60	.01	.08	.00	.000	.000	.000	.00	.16
87-02	59.00	59.70	.00	.07	.00	.000	.000	.000	.00	.08
87-02	59.70	60.50	.05	3.45	.08	.000	2.743	.000	.00	.00
87-02	60.50	63.20	.01	.06	.00	.000	.000	.000	.00	.00
97-02	63.20	64.50	5.00	6.67	2.57	.021	88.115	.720	.00	7.92
37-02	64.50	66.00	.10	.58	.03	.000	1.029	.000	.00	.07

HOLE-ID	FROM	TO	%Pb	%2n ⟨	oz/tAg	oz/tAu	u g/tAg	g/tAu	%Fe	%As
-87-02	66.00	67.30	2.55	8.28	1.08	.104	37.029	3.566	.00	2.53
7-02	67.30	70.00	.20	.42	.00	.000	.000	.000	.00	.32
87-02	70.00	72.00	.13	.36	.00	.014	.000	.480	.00	1.32
87-02	72.00	73.30	7.44	19.10	4.17	.107	142.973	3.669	.00	3.48
87-02	73.30	75.60	1.86	3.10	5.25	.164	180.001	5.623	.00	10.00
87-02	75.60	77.00	.05	.05	.09	.003	3.086	.103	.00	.44
87-03	52.00	53.20	.00	1 60	.00	.000	.000	.000	.00	.03
87-03	54 30	55 00		19 30	1 49	.000	51 086	.000	.00	.00
87-03	55.00	56.30	.10	. 82	.00	.000	.000	. 000	.00	.00
87-03	56.30	58.00	.06	1.18	.00	.000	.000	.000	.00	.00
87-03	58.00	59.90	.07	.26	.00	.000	.000	.000	.00	.36
87-03	59.90	62.00	3.00	4.95	1.05	.093	36.000	3.189	.00	5.18
87-03	62.00	64.00	.04	.31	.00	.000	.000	.000	.00	.22
87-03	64.00	65.00	.60	4.37	.44	.016	15.086	.549	.00	.68
87-03	65.00	66.00	8.99	14.70	6.27	.277	214.973	9.497	.00	5.45
87-03	66.00 67 E0	67.50	.08	.13	.08	.014	2.743	.480	.00	3.69
87-03	51 50	52 00	.12	.10	202	.013	1./14	.446	.00	.24
87-04	52.00	54.00	.00	.00	.00	001	.034 343	.034	.00	.00
87-04	54.00	56.00	.01	.01	.01	.001	.343	.034	.00	.01
87-04	56.00	57.00	.01	.01	.01	.001	.343	.034	.00	.02
87-04	57.00	57.70	.14	.80	.06	.001	2.057	.034	.00	.01
87-04	57.70	59.70	1.04	27.30	.44	.002	15.086	.069	.00	.01
87-04	59.70	61.40	.44	.86	.17	.001	5.829	.034	.00	.04
87-04	61.40	62.70	1.60	18.80	.90	.004	30.857	.137	.00	.01
87-04	62.70	64.30	.15	.94	1 05	.003	2.743	.103	.00	.32
47-04	66 00	67 30	.14	5.20	4 08	.078	139 887	2.0/4	.00	2.52
87-04	67.30	69.00	.09	.09	.06	.002	2.057	.069	.00	26
87-04	69.00	70.50	.03	.01	.00	.016	.000	.549	.00	1.54
87-04	70.50	72.00	.05	.13	.00	.018	.000	.617	.00	.74
87-04	72.00	74.00	.03	.11	.00	.014	.000	.480	.00	.51
87-04	74.00	75.50	.00	.02	.00	.000	.000	.000	.00	.00
87-09	60.40	61.40	.01	.01	.01	.006	.343	.206	.00	.01
87-09	61.40	62.40	.10	.//	.05	.014	1.714	.480	.00	.31
87-09	62.40	65.40	4.02	3.99 Na	2.21 08	.059	2 7 1 2	2.023	.00	.00
87-09	65.40	66.00	.16	.16	.00	.001	480	.034	.00	.00
87-09	66.00	67.50	1.06	3.10	.82	.080	28.115	2.743	.00	.00
87-09	67.50	68.00	4.83	6.96	2.74	.183	93.944	6.274	.00	.00
87-09	68.00	69.00	.30	.69	.29	.011	9.943	.377	.00	.32
87-09	69.00	70.50	.37	.12	.34	.019	11.657	.651	.00	.52
87-09	70.50	72.00	.01	.03	.01	.001	.343	.034	.00	.01
87-10	73.00	74.00	.01	.01	1 40	.001	.343	.034	.00	.01
87-10	75 10	76 10	3 87	4.79	1 63	.343	48.000	11.760	.00	.00
87-10	76.10	77.10	.04	.08	.01	.001	.343	.034	.00	.00
87-10	77.10	78.10	3.23	6.27	2.33	.399	79.886	13.680	.00	.00
87-10	78.10	80.10	.20	.27	.14	.002	4.800	.069	.00	.00
87-10	80.10	81.00	.26	.34	.20	.025	6.857	.857	.00	.00
87-10	81.00	81.60	4.77	11.10	5.25	.700	180.001	24.000	.00	.00
87-10	81.60	82.60	.29	.28	.29	.123	9.943	4.217	.00	4.08
1-10	82.60	83.60	.07	.14	.09	.026	3.086	.891	.00	1.28

HOLE-II	FROM	то	%Pb	%Zn o	oz/tAg	oz/tAu	ı g/tAg	g/tAu	%Fe	&As
97-10	83.60	84.60	.01	.04	.01	.001	.343	.034	.00	.01
37-11	73.50	74.50	.01	.02	.01	.003	.343	.103	.00	.01
87-11	74.50	75.80	.06	.02	.03	.010	1.029	.343	.00	.42
87-11	75.80	76.50	6.29	8.65	5.83	.301	199.887	10.320	.00	.00
87-11	76.50	78.50	.34	.16	.11	.007	3.771	.240	.00	.00
87-11	78.50	80.50	.07	.10	.06	.008	2.057	.274	.00	.00
87-11	80.50	82.30	.33	.13	.23	.024	7.886	.823	.00	.00
87-11	82.30	82.90	9.20	14.70	5.54	.082	189.944	2.811	.00	.00
87-11	82.90	83.60	2.20	.62	1.40	.001	48.000	.034	.00	.01
87-11	83.60	85.00	.08	.06	.01	.001	.343	.034	.00	.01
87-12	57.20	58.20	.01	.03	.01	.005	.343	.171	.00	.01
87-12	58.20	58.70	.10	.28	.05	.018	1.714	.617	.00	1.10
87-12	58.70	59.20	6.83	11.50	5.39	.440	184.802	15.086	.00	.00
87-12	59.20	61.20	.10	.78	.08	.022	2.743	.754	.00	.00
87-12	61.20	63.20	.55	.71	.08	.001	2.743	.034	.00	.10
87-12	63.20	64.00	1.90	4.22	.55	.137	18.857	4.697	.00	.00
87-12	64.00	64.60	3.80	6.28	2.62	.360	89.829	12.343	.00	.00
87-12	64.60	65.60	.31	.21	.08	.005	2.743	.171	.00	.46
87-17	42.30	42.90	.00	.00	.05	.001	1./14	.034	.00	.00
87-17	72.80	73.80	.01	.01	.01	.008	.343	.274	.00	.37
8/~1/	73.80	74.30	3.10	/.14	2./4	.650	93.944	22.286	.00	.00
8/~1/	74.30	75.00	- 10	.27	.1/	.034	5.829	1.166	.00	.00
07-17	75.00	76.00	2.00	5.30	1.52	.234	52.115	8.023	.00	+ 0 0
8/-1/	76.00	70.90	1 05	.03	.41	.038	14.057	1.303	.00	.00
07-17	79 00	70.90	1.95	3.32	1.75	.420	60.000	14.400	.00	.00
87-17 97-17	70.90	79.90	. 55	. / 2	• / •	.193	20.057	0.617	.00	.00
7-19	79.90	76 90	.09	.13	.23	.020	7.000	.000	.00	.49
87-18	75.90	70.90	5 50	0 30 • VI	.UO 5 21	.012	192 050	.4±1 26 057	.00	1.00
87-18	77 90	80.00	32	0.00	11	./00	102.059	20.057	.00	.00
87-18	80.00	82 00	. 52	.44	- 41 58	.010	19 996	1 227	.00	.00
87-18	82.00	83 00	-21	2 25	2 04	058	69 9/3	1 989	.00	.00
87-18	83.00	84 00	1 05	2.23	1 57	138	53 829	1 731	.00	.00
87-18	84.00	86.00	. 94	61	1 57	.100	53 829	3 120	- 00	.00
87-18	86.00	88.00	.15	.14	.28	.019	9 600	651	.00	.00
87-18	88.00	90.00	.18	.50	.34	.024	11.657	.823	.00	.00
87-18	90.00	92.00	.26	.29	.34	.013	11.657	.446	.00	.00
87-18	92.00	93.10	.66	3.08	.76	.095	26.057	3.257	.00	.00
87-18	93.10	95.00	.01	.05	.01	.005	.343	.171	.00	.54
87-18	95.00	96.00	.01	.01	.01	.001	.343	.034	.00	.03
87-19	82.30	84.80	.15	.51	.29	.018	9.943	.617	.00	.72
87-19	84.80	86.00	4.78	14.50	4.43	.191	151.887	6.549	.00	1.50
87-19	86.00	88.00	1.18	3.85	2.10	.526	72.001	18.034	.00	6.21
87-19	88.00	90.00	.09	.28	.23	.033	7.886	1.131	.00	5.10
87-19	90.00	92.00	.13	.08	.69	.042	23.657	1.440	.00	5.30
87-19	92.00	94.00	.10	.09	.23	.020	7.886	.686	.00	1.66
87-19	94.00	96.00	.19	.45	.29	.026	9.943	.891	.00	.86
87-19	96.00	98.00	.06	.08	.23	.031	7.886	1.063	.00	2.02
87-19	98.00	100.00	.04	.28	.11	.002	3.771	.069	.00	.30
87-19	100.00	102.00	.26	.20	.23	.005	7.886	.171	.00	.16
07-19	102.00	103.50	1.14	2.21	.99	.088	33.943	3.017	.00	3.02
8/-19	103.50	104.50	.01	.01	.01	.002	.343	.069	.00	.10
7-20	58.00	59.00	.04	.04	.01	.001	.343	.034	.00	.03
57-20	59.00	60.20	1.26	2.93	1.16	.025	39.772	.857	.00	1.59

HOLE-ID	FROM	TO	%₽b	%Zn	oz/tAg	oz/tA	ıg∕tAg	g/tAu	%Fe	&As
/ 87-20	60.20	61.80	3.76	12.70	4.61	.179	158.058	6.137	.00	6.01
87-20	61.80	63.00	.56	.40	. 47	.260	16.114	8.914	.00	7.71
87-20	63.00	63.60	.29	.33	.52	.239	17.829	8.194	.00	7.60
87-20	63.60	64.60	.02	.36	.11	.038	3.771	1.303	.00	1.83
87-21	69.00	70.00	.02	.02	. 11	.016	3.771	.549	.00	2.78
07-21	70.00	72.00	.01	.01	.01	.001	.343	.034	.00	.06
07-21	72.00	74.00	.01	.01	.01	.001	.343	.034	.00	.01
87-21	74.00	75.00	.01	10.00	.01	.001	.343	.034	.00	.02
07-21	75.00	70.20	3.32	1 20	4./2	.147	101.830	5.040	.00	2.45
97-22	70.20	97 10	.50	1 11	.00	.000	19.000	2.949	.00	2.65
87-22	87 10	88 40	10 60	17 70	5 25	-UZ9 252	100 001	. 994	.00	1.52
87-22	88 40	89.40	10.00	1/./U 53	21	,200	7 200	2 001	.00	2.14
87-22	58 00	59.40	•4Z	.55	.21	.001	7.200	2.091	- 00	1.74
87-25	59.00	61 00	.04	.01	.01	.001	· 545 7/3	.034	.00	.12
87-25	61 00	62 10	1 71	6 10	10 20	-005	245. 717 018	10 514	.00	.50
87-25	62 10	63 10	4.71	79	10.20	.303	5 920	12.014	.00	4.04
87-26	83 00	84 00	.13	. / /	.17	0014	5.029	.400	.00	.04
87-26	84 00	85 40	.00 03	.01	.02	.001	.000	1 097	.00	2 00
87-26	85 40	86 50	6 61	6 70	2 74	062	128 230	2 126	.00	2.00
87-26	86.50	87.20	. 09	.03	11	030	3 771	1 029	.00	1 30
87-26	87.20	87.60	11.00	11.20	8.41	.316	288 345	10 834	00	5 92
87-26	87.60	88.70	.10	.01	.01	.076	.343	2 606	00	2 15
87-26	88.70	89.50	.10	.04	.17	.003	5.829	103	.00	2.10
87-26	89.50	90.00	4.15	.20	1.63	.038	55.886	1,303	.00	1 42
87-26	90.00	91.00	.10	.19	.16	.001	5.486	.034	.00	. 02
87-27	64.50	66.00	.10	.20	.01	.016	.343	.549	.00	. 94
37-27	66.00	67.50	.18	.04	.01	.063	.343	2.160	.00	2.68
87-27	67.50	69.00	.01	.01	.01	.014	.343	.480	.00	.92
87-27	69.00	70.00	3.38	6.82	3.15	.300	108.001	10.286	.00	4.74
87-27	70.00	71.50	.16	.02	.17	.156	5.829	5.349	.00	4.24
87-27	71.50	73.00	.04	.04	.01	.005	.343	.171	.00	.06
87-27	73.00	74.50	.24	.01	.13	.067	4.594	2.297	.00	4.96
87-27	74.50	76.50	.10	.01	.03	.029	1.029	.994	.00	2.32
87-27	76.50	77.50	.30	.01	.94	.171	32.229	5.863	.00	6.84
87-27	77.50	79.20	3.16	9.90	3.79	.550	129.944	18.857	.00	8.86
87-27	79.20	80.20	.52	3.76	.82	.250	28.115	8.571	.00	7.02
87-27	80.20	81.60	3.20	2.22	4.08	.400	139.887	13.714	.00	7.20
87-27	81.60	82.60	.02	.01	.11	.005	3.771	.171	.00	.22
87-27	92.00	93.00	.01	.10	.01	.001	.343	.034	.00	.05
87-28	60.00	60.50	1.91	4.27	2.27	.001	77.829	.034	.00	3.42
87-28	60.50	62.50	.12	.12	.32	.172	10.972	5.897	.00	4.34
87-28	62.50	63.00	1.94	4.27	2.01	.176	68.915	6.034	.00	4.92
87-20	63.00	64.00	.07	.25	.14	.119	4.800	4.080	.00	.28
07-29	97.00	90.00	.01	.01	.01	.002	.343	.069	.00	.07
87-29	90.00	100 50	.01	.01	.01	.003	.343	.103	.00	.21
87-29	100 50	102.00	.13	2 00	1 05	. 277	21.943	9.497	.00	8.35
87-29	102.00	102.00	1 74	1 66	2 80	.071	36.000	2.434	.00	3.44
87-29	103 70	105 00	2.14	1.00	2.00	.103	20.001 6 0E7	0.343	.00	0.60
87-29	107 00	108 00	,20 00	1 61	.20	.002	0.007	.UOY	.00	.19
87-30	111 50	112 50	.00	1.04	.00 06	001	2 057	.3//	.00	.00
97-30	112 50	113 50	.01	.01	.00 26	160	2.UD/ 2 01/	.UJ4 5 704	.00	.07
J7-30	113.50	114.50	1.56	6.10	1 92	787	65 820	5./94 13 166	.00	0.4J 5 20
				~ • <i>•</i> •		• • • • • •	00.027	TO'TOO	.00	J. 22

HOLE-ID	FROM	TO	%Pb	%Zn	oz/tAg	oz/tAu	ı g/tAg	g/tAu	% Fe	%As
97-30	114.50	115.50	.62	1.60	.82	.073	28.115	2.503	.00	2.01
37-30	115.50	116.50	.01	.01	.17	.001	5.829	.034	.00	.01
88-01	53.45	54.22	.28	.15	.43	.051	14.743	1.749	4.38	2.34
88-01	54.22	54.91	.22	.38	.25	.148	8.571	5.074	8.66	8.56
88-01	54.91	55.37	.02	.01	.05	.018	1.714	.617	4.71	1.95
88-01	59.00	60.20	.05	.14	.07	.035	2.400	1.200	2.75	1.17
88-01	60.20	61.30	.01	.05	.02	.005	.686	.171	1.77	.33
88-01	61.30	61.50	.06	.01	.17	.146	5.829	5.006	12.89	13.55
88-01	61.50	63.00	.01	.01	.01	.002	.343	.069	1.73	.03
88-01	63.00	64.51	.01	.01	.01	.002	.343	.069	2.22	.03
88-01	64.51	66.01	.02	.03	.03	.016	1.029	.549	2.97	.83
88-01	66.01	66.62	2.58	9.05	2.00	.130	68.572	4.457	11.68	2.24
88-01	66.62	67.34	.03	2.72	.05	.080	1.714	2.743	3.24	2.73
88-01	66.34	67.88	.10	8.47	.06	.021	2.057	.720	1.63	.66
88-01	67.88	68.35	.02	.05	.01	.016	.343	.549	2.13	.97
88-01	68.35	68.96	.38	.63	.14	.020	4.800	.686	1,71	.72
88-01	68.96	69.52	2.38	5.38	.84	.217	28.800	7.440	8.23	6.22
88-01	69.52	69.79	30.41	8.27	10.56	.180	362.060	6.171	4.02	2.22
88-01	69.79	70.89	.54	.61	.17	.015	5.829	.514	1.42	.72
88-01	70.89	72.37	.45	.09	.21	.079	7.200	2.709	5.12	3.95
88-01	72.37	73.81	.03	.02	.03	.023	1.029	.789	2.19	1.02
88-01	73.81	75.35	.09	.01	.14	.036	4.800	1.234	4.75	2.22
88-01	75.35	76.87	.24	.01	.91	.019	31.200	.651	3.18	1.29
88-01	76.87	78.46	.03	.01	.07	.003	2.400	.103	1.62	.10
88-01	78.46	79.97	.07	.07	.10	.012	3.429	.411	2.27	.48
88-01	79.97	80.67	1.66	5.08	1.19	1.100	40.800	37.715	18.50	15,21
88-01	80.67	81.34	3.02	16.34	3.19	1.300	109.372	44.572	24.95	15.72
38-01	81.34	82.48	5.45	7.80	3.18	1.620	109.029	55.543	22.94	22.34
88-01	82.48	83.50	12.25	20.89	7.81	.656	267.774	22.492	17.95	8.22
88-01	83.50	84.32	.04	.23	.05	.022	1.714	.754	.34	.26
88-01	84.32	85.80	.06	.09	.05	.003	1.714	.103	.09	.03
88-02	47.65	48.43	.01	.05	.03	.004	1.029	.137	2.52	.21
88-02	48.43	48.98	.01	.01	.01	.003	.343	.103	3.00	.23
88-02	48.98	49.98	.01	.01	.03	.004	1.029	.137	2.82	.25
88-02	49.98	50.65	.01	.01	.02	.001	.686	.034	2.18	.01
88-02	51.39	52.38	.03	.01	.05	.003	1.714	.103	2.59	.45
88-02	52.38	53.26	.02	.01	.06	.007	2.057	.240	2.33	.46
88-02	53.26	53.63	4.25	5.52	3.79	.640	129.944	21.943	19.67	10.90
88-02	53.63	54.26	.77	.47	.61	.176	20,914	6.034	8.15	6.15
88-02	54.26	55.03	.13	.05	.28	.076	9.600	2.606	7.63	4.85
88-02	55.03	56.00	.04	.01	.18	.009	6.171	.309	3.98	.49
88-02	56.00	56.83	.04	.02	.14	.013	4.800	.446	4.49	1.02
88-02	56.83	57.40	.06	.12	.25	.067	8.571	2.297	6.19	3.67
88-02	57.40	57.79	3.00	19.09	2.47	1.006	84.686	34.492	22.40	14.18
88-02	57.79	58.16	.03	.05	.05	.113	1.714	3.874	2.31	2.10
88-02	58.16	59.16	.02	.05	.03	.025	1.029	.857	1.57	.72
88-02	59.16	60.05	.01	.01	.02	.013	.686	.446	.04	.03
88-03	69.21	70.21	.02	.01	.05	.005	1.714	.171	2.99	.25
88-03	70.21	71.18	.01	.04	.02	.001	.686	.034	2.56	.08
88-03	71.18	72.19	.12	.01	.87	.177	29.829	6.069	8.12	7.42
88-03	72.19	72.80	.25	.05	5.94	.064	203.659	2.194	17.23	12.13
88-03	72.80	74.00	.03	.01	.16	.020	5.486	.686	2.66	.95
8-03	74.00	74.99	.01	.01	.03	.001	1.029	.034	1.96	.16
d 8 -03	74.99	76.01	.01	.01	.01	.008	.343	.274	2.44	.53

HOLE-ID	FROM	то	%Pb	%Zn	oz/tAg	oz/tAu	ıg∕tAg	g/tAu	%Fe	%As
88-03	76 01	77 00	03	01	27	004	12 606	1 2 7	2 00	57
88-03	77 00	78 00	.05	.01		.004	12.000	103	2.03	
88-03	78 00	79 00	.01	.01	12	001	2 400	.103	3 04	.57
88-03	79 00	80 05	04	.01	07	007	3 086	240	3 62	.00 20
88-03	80.05	80.78	.37	.19		332	19 886	11 282	12 91	10 47
88-03	80.78	81.58	.70	. 4 9	1.01	.450	34,629	15.429	12.11	11.25
88-03	81.58	82.24	2.30	6.75	.95	1.090	32.572	37.372	22.34	16.65
88-03	82.24	82.78	.22	.85	.21	.292	7.200	10.012	16.91	5.98
88-03	82.78	83.71	4.08	18.73	2.98	.372	102.172	12.754	20.41	5.38
88-03	83.71	84.29	2.34	6.73	3.80	.350	130.287	12.000	28.67	4.86
88-03	84.29	85.15	.01	.02	.08	.033	2.743	1.131	3.25	.89
88-03	85.15	86.00	.10	.21	.35	.026	12.000	.891	2.51	.23
88-03	86.00	87.00	.07	.19	.12	.011	4.114	.377	1.11	.34
88-03	64.29	65.29	.01	.05	.02	.002	.686	.069	3.52	.12
88-03	65.29	60.44	.01	.06	.01	.004	.343	.137	1.65	.19
88-03	67 44	67.44	1 15	2 24	01	.002	.343	.069	2.97	.07
88-03	67.84	68.21	11 14	14 16	6 81	314	20.914	10 766	20 42	5.10
88-03	68.21	69.21	.02	.03	. 02	.004	. 686	137	20.42	19
88-04	71.83	72.42	.03	.10	.01	.007	.343	.240	1.32	1.03
88-04	72.42	73.54	7.27	10.67	4.56	.606	156.344	20.777	15.03	7.11
88-04	73.54	74.37	.04	.37	2.22	.282	76.115	9.669	3.27	4.20
88-05	55.78	56.30	.03	.01	.10	.009	3.429	.309	7.67	.02
88-05	56.30	56.77	4.89	8.21	4.78	.522	163.887	17.897	21.41	8.48
88-05	56.//	57.03	1.43	1.58	1.18	.211	40.457	7.234	10.58	5.28
88-05	57.05	57.10	2 20	2 51	2 00	.024	5.143	.823	2.20	.79
88-05	57 29	58 88	1 19	1 11	3.00	2.150	22 272	13.115	20.77	10.09
88-05	58.88	59.17	1.88	2.42	.81	996	27.772	34 149	20 71	17 28
88-05	59.17	59.77	6.57	7.14	3.32	.930	113.830	31.886	19.23	16.05
88-05	59.77	60.75	.64	3.00	.40	.035	13.714	1.200	4.09	.99
88-05	60.75	61.05	3.69	3.24	2.31	1.110	79.201	38.057	29.40	19.51
88-05	61.05	62.00	3.54	5.28	2.36	.726	80.915	24.892	20.88	17.10
88-05	65.27	66.79	.06	.06	.06	.016	2.057	.549	5.05	.28
88-06	54.50	55.50	.01	.01	.02	.003	.686	.103	3.59	.02
88-06	55.50	55.64	4.74	6.71	4.13	.658	141.601	22.560	20.38	13.78
88-06	55.04 55.02	56 00	5.10	10.43	2.74	.410	93.944	14.057	13.95	7.51
88-06	56 09	56 70	.00	.10	.00	.011	2.743	.3//	2.28	.63
88-06	56.70	57.10	.03	.04	06	.003	2.057	343	2.70	.10
88-06	57.10	57.80	.05	.01	.06	.005	2.057	.171	2.87	32
88-06	57.80	59.00	.05	.42	.05	.003	1.714	.103	2.71	.19
88-07	66.57	67.53	.02	.02	.02	002	.686	.069	1.37	.09
88-07	67.53	67.86	.01	.03	.01	.011	.343	.377	2.55	1.96
88-07	67.86	68.96	6.46	7.76	5.57	1.106	190.973	37.920	22.17	12.27
88-07	68.96	69.31	9,99	11.23	6.20	.440	212.573	15.086	21.87	8.18
88-07	69.31	70 60	.50	.14	.30	.115	10.286	3.943	17.80	20.34
88-07	70 60	70.00	.11	+20 17	.21	.042	9.25/	1.440	3.20	1.88
88-07	71.60	72.60	.20	יבי 1 ק	• Z J 2 A	.009 AR1	2.243 8 220	1 042	2 . 40	1.10
88-07	72.60	73.63	.02	.02	.01	.004	.343	.137	2.09	1.20
88-07	73.63	74.42	.07	.06	.13	.002	4.457	.069	1,40	.19
98-07	74.42	75.00	.73	.02	1.35	.054	46.286	1.851	11.90	10.30
8-07	75.00	75.80	.30	.14	.84	.022	28.800	.754	5.50	3.81

HOLE-ID	FROM	то	%₽b	%Zn	oz/tAg	oz/tA	u g/tAg	g/tAu	%Fe	%As
88-07	75.80	76.45	2.86	.81	2.94	.334	100.801	11.452	20.14	20.83
88-07	76.45	77.70	2.03	.94	.16	.081	5.451	2.777	10.87	11.10
88-07	77.70	78.60	.44	1.10	.44	.078	15.086	2.674	7.59	7.63
88-07	78.60	79.55	2.50	1.39	3.96	.035	135.773	1.200	4.86	3.77
88-07	79.55	80.50	.28	.16	.31	.012	10.629	.411	2.53	1.49
88-07	80.50	81.50	.12	.16	.11	.003	3.771	.103	2.22	.09
88-07	81.50	82.47	.37	1.75	.32	.002	10.972	.069	3.49	.01
88-08	77.70	78.30	.11	.11	.08	.026	2.743	.891	4.22	3.73
88-08	78.30	78.57	.15	.01	.13	.066	4.45/	2.263	21.79	25.32
88-08	10.01	70 05	.3/	10 69	.20	.039	8.914	1.337	2.19	1.55
88-08	79.23	19.90	/.11	10.00	2.30	.300	131.310	19.200	20.37	9.37
88-08	80 72	80.72	1 02	-01	. 30	1 300	13.029	10.252	10.37	20.06
88-08	80.98	81 50	1.02	.00	1.10	030	JJ.42J A 457	1 337	1 72	29.90
88-09	49.21	49.85	.01	. 05	.27	.031	9.257	1.063	214	. 50
88-09	49.85	50.33	2.57	5.64	2.41	.346	82.629	11.863	30 48	8 23
88-09	50.33	51.72	.26	.83	.22	.016	7.543	.549	2,96	1.18
88-09	51.72	52.79	.14	.12	.05	.018	1.714	.617	2.83	.76
88-09	52.79	53.38	2.75	3.55	.12	.620	4.183	21.257	22.74	15.69
88-09	53.38	53.83	5.81	8.09	2.87	.782	98.401	26.812	18.33	15.51
88-09	53.83	54.09	.26	.43	.19	.028	6.514	.960	4.07	1.67
88-09	54.09	55.00	6.86	7.79	4.03	.820	138.173	28.115	27.07	15.56
88-09	55.00	55.40	2.82	5.74	1.88	.544	64.458	18.652	19.38	14.40
88-09	56.08	56.41	1.30	1.69	1.10	.103	37.715	3.531	4.43	3.14
88-09	62.18 52 AC	62,83 53,00	.13	.21	.05	.012	1.714	.411	4.31	.37
89-10	53.40	53.90 57 57	2 27	.03	.05	.013	1./14	.446	4.15	2.32
88-10	54 54	54.54	1 33	21 36	3.00	.300	123.487	13.303	20.64	13.59
88-10	54.65	56.43	.41	21.30	24	.002	8 229	20.040	14.20	11.13 50
88-10	56.43	58.20	.09	.26	.07	.031	2.400	1.063	3.00	.59
88-10	58.20	59.78	.67	.64	.50	.127	17.143	4.354	8.71	4.71
88-10	59.78	60.74	.06	.07	.04	.005	1.371	.171	3.42	.05
88-10	60.74	62.03	.58	.92	.43	.031	14.743	1.063	5.42	2.83
88-10	62.03	63.45	.24	.19	.19	.022	6,514	.754	5.62	1.41
88-10	63.45	64.88	.05	.02	.11	.113	3.771	3.874	9.72	8.48
88-11	75.68	76.10	.01	.01	.04	.046	1.371	1.577	7.93	1.92
88-11	76.10	76.35	2.58	14.95	1.76	.372	60.343	12.754	20.93	8.82
88-11	76.35	75.65	5.00	12.81	3.78	.255	129.601	8,743	14.99	4.19
00-11 99-11	20.00	77.02	D./Z	0.32	3.58	.278	122.744	9.532	17.39	5.67
88-11	77.02 92 FF	70 36	.00	- 62	.53	.081	18.1/2	2.111	1.99	2.48
88-11	78 36	70.30	0.00	27	4.90	.272	108.001	9.326	10.08	4.54
88-11	79 47	80 88	.23	. 27	.21	.004	3 096	.137	2.04	.19
88-11	85.20	86.08	.82	.10		.001	12 343	.034	2.20	• L L 1 1
88-11	86.08	87.75	.30	.30	.17	.004	5 829	137	2.39	.11
88-11	87.75	89.42	.04	.05	.04	.005	1,371	.171	3 28	2 28
88-11	89.42	90.61	.54	.11	.35	.086	12.000	2.949	16.56	19.69
88-11	90.61	91.80	.04	.01	.11	.036	3.771	1.234	14.50	17.04
88-11	91.80	92.37	.04	.05	.05	.009	1.714	.309	4.08	.20
88-11	92.37	92.86	2.39	2.66	1.34	.098	45.943	3.360	9.27	4.69
88-11	92.86	94.05	.03	.04	.02	.011	.686	.377	3.21	.55
88-11	94.05	94.65	.30	.55	.26	.118	8.914	4.046	8.16	5.76
88-11	94.65	95.35	.13	.89	.12	.006	4.114	.206	2.97	.31
99-15	50.16	50.90	.02	.01	.05	.002	1.714	.069	3.29	.20

HOLE-ID	FROM	TO	%₽b	₹Zn	oz/tAg	oz/tA	u g/tAg	g/tAu	%Fe	&As
88-12	50.90	51.17	12.37	11.38	4.61	.011	158.058	.377	1.36	.01
88-12	52.03	52.03	.06	.27	.01	.001	.343	.034	2,26	.01
88-12	53.30	54.86	.02	.22	.01	.002	.343	.069	1.59	.15
88-12	54.86	55.50	.24	.87	.17	.006	5.829	.206	3.01	1.69
88-12	55.50	55.95	.51	.34	.24	.024	8.229	.823	4.19	2.64
88-12	56.39	56.66	.20	1.33	2.69	.700	3 429	24.000	18.42	13.61
88-12	56.66	57.46	6.38	5.91	5.22	.145	178.973	4.971	2.60	5.13
88-12	57.46	57.80	12.73	13.91	7.41	.261	254.059	8.949	8.50	1.93
88-12	57.80	58.90	1.49	3.33	.99	.121	33.943	4.149	9.77	2.85
88-13	34.54	36.12	.09	.07	.13	.014	4.45/	.480	2.19	.59
88-13	40.62	40.88	.04	.20	.01	.001	.343	.069	.74	.02
88-13	40.88	41.36	2.80	2.45	1.06	.003	36.343	.103	1.49	.01
88-13	41.36	41.79	.44	1.68	.16	.002	5.486	.069	2.34	.53
88-13 88-13	41.79	42.98	.01	,42 3 99	.01	.002	.343	.069	1.02	.01
88-13	43.39	44.54	.10	1.00	.07	.001	2.400	.034	4.45	.02
88-13	44.54	45.72	3.91	10.97	1.67	.014	57.258	.480	2.41	.15
88-13	45.72	46.98	1.39	6.08	.67	.021	22.972	.720	3.05	.75
88-13	46.98	47.78	.43	1.81	.32	.047	10.972	1.611	4.73	2.34
88-13	47.70	40.75	1.30	2.84	3 21	.098	24.686	3.360	6.53	1.79
88-13	49.63	50.61	.62	.44	.42	.031	14.400	1.063	2.24	.32
88-13	50.61	51.30	.07	.14	.06	.005	2.057	.171	2.70	.19
~ 88-13	51.30	52.71	.02	.02	.03	.002	1.029	.069	1.87	.12
88-13	52.71 73.59	54.11 74 21	.04	.01	.04	.011	1.371	.377	1.65	.49
88-14	74.21	74.67	.61	4.85	.63	.184	21.600	6.309	6.46	4.07
88-14	74.67	75.13	3.96	21.38	3.96	.516	135.773	17.692	7.75	6.77
88-14	75.13	76.45	.20	.35	.08	.008	2.743	.274	2.25	.61
88-14 88-14	77 86	77.86	.30	.19	.13	.003	4.457	.103	2.48	.13
88-14	78.88	79.52	2.48	2.88	2.59	.910	2.057	31 200	3.62	23 09
88-14	79.52	80.40	.47	2.43	.23	.012	7.886	.411	2.08	.18
88-14	80.40	80.94	5.41	12.25	2.47	.304	84.686	10.423	10.75	6.82
88-14	80.94	82.13	.04	.28	.03	.010	1.029	.343	2.59	.39
88-14	82.70	83.63	2.41	6.55	1.43	.028	49.029	4,423	8.13	5.61
88-14	83.63	84.68	5.58	8.74	4.14	.090	141.944	3.086	9.09	2.31
88 - 14	84.68	85.31	.04	.11	.05	.003	1.714	.103	1.21	.34
88-14	86.56	87.04	.06 3.59	1 00/	.08	.006	2.743	.206	3.65	.30
88-14	87.04	88.55	.32	.31	.52	.036	17.829	1.234	8.45	2.15
88-14	88.55	89.53	.10	.02	.25	.015	8.571	.514	6.04	1.01
88-14	89.53	90.04	.28	.05	.76	.034	26.057	1.166	28.45	2.35
88-14	90.04	91.48	.61 15	.04	1.34	.065	45.943	2,229	8.39	2.36
88-14	92.79	93.79	.01	.01	.29	.001	3.943	.377	4.69	- 83
88-14	93.79	94.70	.01	.01	.02	.001	.686	.034	7.31	.01
88-14	94.70	95.29	.01	.01	.03	.001	1.029	.034	5.48	.02
88-14	95.29	97.18	.01	.01	.02	.001	.686	.034	1.20	.01
99-12	00.04	09.98	.03	.10	.02	.001	.686	.034	3.24	.01

HOLE-ID	FROM	TO	%Pb	%Zn √	oz/tAg	oz/tAu	ı g/tAg	g/tAu	% Fe	% As
2 98-15	69,98	70.82	.01	.01	.01	.001	. 343	.034	3.77	- 0.4
38-15	70.82	70.99	3.63	16.95	1.95	.005	66.858	.171	2.84	.01
88-15	70.99	71.62	.29	1.35	.15	.001	5.143	.034	.51	.01
88-15	71.62	71.78	1.24	21.38	1.14	.031	39.086	1.063	1.43	.01
88-15	71.78	73.21	.05	.38	.02	.001	.686	.034	2.33	.03
88-15	73.21	74.68	.04	.16	.03	.002	1.029	.069	2.18	.16
88-15	74.68	75.84	.17	1.42	.07	.001	2.400	.034	1.17	.04
88-15	75.54	75.77	8.64	19.57	3.52	.110	120.687	3.771	2.85	.86
88-15	75.77	76.63	2.07	9.57	.97	.052	33.25/	1.783	3.67	.94
88-15 99-15	70.03	77.59	0.10	14.37	3.10	.130	1 271	4,437	2.00	1.50
88-16	39 37	40 65	.03	.03	.04 03	.003	1 029	069	J. JO 1 17	.10
88-16	40 65	41 61	.09	1 61	.03	001	1 371	034	1,4/ 99	.01
88-16	41.61	42.84	.06	.09	.07	.004	2,400	.137	2.81	.78
88-16	42.84	43.70	.01	.07	.01	.001	.343	.034	1.90	.01
88-16	43.70	43.94	.23	.46	.25	.036	8.571	1.234	6.39	5.17
88-16	43.94	44.92	.01	.05	.01	.002	.343	.069	2.09	.02
88-16	44.92	45.18	7.91	14.45	3.01	.010	103.201	.343	1.67	.03
88-16	45.18	46.67	.11	.34	.08	.001	2.743	.034	1.15	.03
88-16	46.67	48.16	.01	.02	.01	.001	.343	.034	2.55	.01
88-16	48.16	49.72	.08	.26	.04	.002	1.371	.069	1.89	.11
88-16	49.72	49.98	3.25	8.80	1.43	.103	49.029	3.531	6.22	1.69
88-16	49.98	50./1	.25	1.59	.21	.064	112 920	12 202	3.33	1.10
88-16 88-16	50.71	50.92	5.07	1.50	3.32	.300	113.830	13.303	19.14	0.53
88-16	51 87	52 52	12	.02	.09	.010	3.000 8 914	.343	4.84	1 04
88-16	52.52	53.81	.12	.18	10	013	3 429	.025	3 84	1.04
38-17	44.73	46.00	.03	.10	.01	.001	.343	.034	. 66	.00
88-17	46.00	46.60	2.04	4.82	.68	.003	23.314	.103	1.65	.01
88-17	46.60	46.97	.86	41.42	.37	.002	12.686	.069	.95	.01
88-17	46.97	47.55	3.84	6.18	2.54	.027	87.086	.926	1.72	.21
88-17	47.55	48.29	.22	.53	.13	.003	4.457	.103	2.46	.30
88-17	48.29	48.59	6.37	33.25	2.85	.031	97.715	1.063	2.38	.01
88-17	48.59	49.79	.35	.95	.11	.001	3.771	.034	1.52	.01
88-17	49.79	52 00	.00	.21	.02	.001	.000	.034	1.90	.01
88-17	52.00	52.00	1 94	12 26	1 24	456	4.457	15 634	13 50	1.00
88-17	52.62	53.39	.40	1.24	.40	.042	13.714	1.440	2.80	1,15
88-17	53.39	54.47	7.11	9.88	3.96	.634	135.773	21.737	16.91	9.79
88-17	54.47	55.55	.10	.14	.23	.013	7.886	.446	4.85	.49
88-17	55.55	56.77	.17	.80	.32	.015	10.972	.514	4.78	.63
88-17	56.17	58.14	.06	.03	.32	.008	10.972	.274	1.49	.28
88-17	58.14	59.58	.01	.01	.01	.001	.343	.034	1.69	.03
88-17	59.58	61.04	.01	.01	.01	.001	.343	.034	.95	.07
88-17	61.04	62.43	.01	.01	.05	.002	1.714	.069	1.62	.12
00-17 99-17	62.43	63.94	.01	.01	.81	.001	21.112	.034	.81	.07
88-18	69 76	70 52	64	.01	.01	.001	, 343 23 314	3 304	.43	1 00
88-18	70.52	70.90	. 51	.73	4 15	1 085	142 287	37 200	26 00	26 65
88-18	70.90	72.03	.34	.52	.40	.043	13.714	1.474	4.46	1.92
88-18	72.03	72.42	1.82	10.81	1.03	.147	35.315	5.040	6.65	6.14
88-18	72.42	73.06	1.15	4.57	.57	.637	19.543	21.840	22.13	19.84
98-18	73.06	73.82	.08	.86	.09	.016	3.086	.549	1.79	.67
38-18	73.82	74.47	.68	8.25	.52	.150	17.829	5.143	9.96	1.77

∠ 88-18	74.47	75.30	2.39	13.30	3.76	.177	128.915	6.069	13.62	4.77
38-18	75.30	76.15	8.73	18.05	4.14	.155	141.944	5.314	15.47	5.02
88-18	76.15	76.63	1.10	7.76	.41	.176	14.057	6.034	11.32	4.54
88-18	76.63	77.23	.57	1.37	.28	.009	9.600	.309	3.02	. 82
88-18	77.23	79 07	19.95	12.33	9.59	.132	328.803	4.526	5.30	.72
88-18	78.07	79.40	2.72	1 22	2.75	008	5 486	9.320 271	20.73	2.61
88-18	79.40	80.32	.32	. 98	.18	.006	6.171	.206	1.99	.54
88-18	80.32	80.92	.61	.55	.32	.096	10.972	3.291	9.52	3.17
88-18	80.92	81.34	1.74	3.99	.97	.052	33.257	1.783	1.93	.67
88-18	81.34	81.78	13.87	21.05	6.79	.296	232.802	10.149	15.32	4.03
88-18	81.78	83.25	.11	.05	.12	.046	4.114	1.577	4.01	1.80
88-18	83.25	84.74	1.15	.55	1.03	.058	35.315	1.989	5.42	2.26
88-19	77.54	78.33	.21	1.99	.14	.001	4.800	.034	1 43	2.05
88-19	78.33	78.84	2.38	17.12	1.67	.063	57.258	2.160	6.76	2.53
88-19	78.84	79.27	.20	.79	.31	.027	10.629	.926	7.42	3.10
88-19	79.27	79.66	2.45	3.62	1.58	.960	54.172	32.915	21.06	18.02
88-19	79.66	80.33	.54	.36	.55	.142	18.857	4.869	10.28	3.09
88-19	81 42	81.42	. 1 /	.36	./1	.030	24.343	1.029	4.68	.69
88-19	82.98	84 56	.01	.01	.04	.007	1.371	.240	3.18	.15
88-19	84.56	86.00	.04	.07	.03	.002	1.029	.069	4.26	.34
88-19	86.00	86.87	.08	.03	.06	.011	2.057	.377	2.70	.49
88-20	79.95	80.48	.02	.01	.07	.001	2.400	.034	2.34	.01
88-20	80.48	81.64	.02	.04	.11	.003	3.771	.103	2.44	.46
88-20	81.64	82.68	.01	.02	.02	.001	.686	.034	2.23	.01
88-20	82 22	84 74	1.47	.49	.64	.003	21.943	.103	2.71	.36
88-20	84.74	86.34	.07	.05	.03	.007	4.457	240	4 27	1 39
88-20	86.34	86.52	.14	.02	.15	.120	5.143	4.114	13.99	13.56
88-20	86.52	87.93	.48	4.83	.34	.007	11.657	.240	2.56	.39
88-20	87.93	88.44	.63	2.28	.60	.049	20.572	1.680	8.56	2.96
88-20	88.44	88.84	5.59	16.98	4.17	.127	142.973	4.354	13.79	3.46
88-20	88.84	90 00	5.62	9.22	3.99	.508	136.801	17.417	18.63	11.54
88-20	90.00	90.70	9.88	13.82	6.59	.378	225 945	12.960	20 70	4.75
88-20	90.70	91.39	.80	.43	1.04	.140	35.657	4.800	20.91	13.88
88-20	91.39	91.95	4.55	9.61	9.04	.578	309.945	19.817	19.10	12.84
88-20	91.95	92.58	.61	2.05	1.32	.116	45.258	3.977	21.34	5.96
88-20	92.58	93.65	.01	.01	.01	.011	.343	.377	2.68	.11
88-21	79.00 81 48	83 00	.01	.03	.01	.004	.343	.137	2.72	.01
88-21	83.00	84.63	.05	.10	.03	.002	1.029	.089	2.25	.10
88-21	84.63	85.26	.95	.46	.56	.530	19.200	18.172	18.66	14.78
88-21	85.26	86.48	.40	2.82	.24	.014	8.229	.480	3.17	.68
88-21	86.48	86.90	5.09	5.02	3.95	.239	135.430	8.194	22.39	9.81
88-21	86.90	87.60	1.88	.47	1.15	.049	39.429	1.680	10.12	6.24
88-21	07.0U 88.28	00.20 89.17	9.98 1∥	8.23 02	6.3/ 20	.404	218.402	13.852	20.82	10.25
88-21	89.17	90.44	.14 .06	.02	. 30	.024 012	13.029	.023 11	10.01	3.40 04
88-21	90.44	90.99	.17	.02	1.19	.158	40,800	5.417	15.45	14 95
?8-21	90.99	91.58	.01	.01	.06	.004	2.057	.137	5.03	.04
/8 - 21	91.58	91.84	.42	1.27	1.38	404	47.315	13,852	20 06	าจำัต

%Pb %Zn oz/tAg oz/tAu g/tAg g/tAu

%Fe

%As

HOLE-ID

FROM

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HOLE-ID FROM TO %Pb %Zn oz/tAg oz/tAu g	g/tAg g/tAu	%Fe %As	
	.686 .103	3.23 .10	6
38-21 93.34 94.50 .03 .12 .04 .003	1.371 .103	1.81 .1	5
88-21 94.50 95.76 .01 .01 .01 .008	.343 .274	3.60 .01	9
88-22 78.48 79.37 .04 .01 .05 .007	1.714 .240	4.32 1.6	9
88-22 79.37 80.13 .01 .02 .01 .001	.343 .034	1.83 .10	0
88-22 80.13 81.08 .03 .44 .03 .002	1.029 .069	3.45 .4	1
88-22 81.08 81.91 .01 .01 .01 .001	.343 .034	4.37 .01	ĩ
88-22 81.91 83.00 .01 .01 .01 .001	.343 .034	4.10 .0	1
88-22 83.00 83.83 .01 .01 .01 .001	.343 .034	2.80 .01	ī
88-22 83.83 84.80 .15 .05 .06 .001	2.057 .034	2.99 .1	5
88-22 84.80 85.20 .49 1.51 .27 .057	9.257 1.954	5.72 2.22	2
88-22 85.20 85.87 2.02 10.05 1.20 .080 4	1.143 2.743	7.96 2.40	6
88-22 85.87 87.02 .15 .64 .05 .004	1.714 .137	1.40 .1	š
88-22 87.02 87.88 .02 .03 .01 .001	.343 .034	1.07 04	4
88-22 87.88 88.51 1.08 3.40 .44 .117 1	5.086 4.011	8.65 2.60	ń
88-22 88.51 89.14 1.08 2.82 .90 .167 3	30.857 5.726	11.34 3.50	ň
88-22 89.14 90.02 .04 .08 .02 .004	.686 .137	2.34 04	4
88-22 90.02 90.84 .14 .19 .18 .156	6.171 5.349	6.62 3.5	Â
88-22 90.84 91.51 1.71 4.22 2.08 .364 7	1.315 12.480	13.83 9.91	ž
88-22 91.51 91.77 .14 .08 .13 .060	4.457 2.057	4.38 3.00	ñ
88-22 91.77 91.99 1.77 4.68 2.36 .281 8	0.915 9.634	18,16 15 1	7
88-22 91.99 92.35 .63 .27 .65 .112 2	2.286 3.840	4.96 3.4	Ś
88-22 92.35 92.58 14.37 13.97 11.40 .356 39	0.860 12.206	21.56 4.64	Δ
88-22 92.58 93.45 .01 .01 .05 .001	1.714 .034	4 91 0	1
88-22 93.45 94.05 .32 .31 .30 .030 1	0.286 1.029	6.33 1 1	à.
88-22 94.05 94.80 .01 .01 .01 .008	.343 .274	3.15 0	ĩ
-88-22 94.80 95.40 .01 .01 .02 .002	.686 .069	3.74 22	2
38-22 95.40 96.00 .15 .38 .31 .376 1	0.629 12.892	7.81 5.24	Δ
88-22 96.00 96.59 .01 .01 .01 .02	.343 .069	3.83 01	1
88-22 96.59 97.40 .01 .01 .01 .02	.343 .069	4 07 01	ì
88-22 97.40 98.13 .02 .03 .01 .013	.343 .446	3.37 2	7
88-23 101.05 102.01 .01 .01 .01 .001	.343 .034	3 41 01	í
88-23 102.01 102.95 .01 .01 .01 .001	.343 .034	3.84 01	1
88-23 102.95 103.66 1.33 .02 .97 .001 3	3.257 .034	2.34 01	ī
88-23 103.66 105.15 .62 .06 .47 .001 1	6.114 .034	.75 .01	ī
88-23 105.15 106.40 .01 .01 .01 .001	.343 .034	.25 01	î
88-23 106.40 107.52 .26 .06 .20 .001	6.857 .034	2.56 01	ì
88-23 107.52 108.53 .60 1.40 .42 .001 1	4.400 .034	4.53 .01	ĩ
88-23 108.53 109.66 .07 .05 .05 .005	1.714 .171	3.07 .64	4
88-23 109.66 110.57 11.09 14.16 7.47 .340 25	6.116 11.657	18.71 4.20	Ô.
88-23 110.57 111.12 .10 .07 .06 .016	2.057 .549	2.52 .73	3
88-23 111.12 111.46 2.92 2.85 3.21 .536 11	0.058 18.377	24.42 17.16	6
88-23 111.46 113.70 .02 .04 .01 .026	.343 .891	3.44 .11	ĩ
88-24 97.32 97.57 .01 4.24 .01 .007	.343 .240	4.46 .01	1
88-24 97.54 100.36 .03 .01 .07 .003	2.400 .103	5.19 .27	7
88-24 100.36 101.00 .01 .01 .01 .001	.343 .034	2.78 .01	i
88-24 101.00 102.50 .01 .01 .01 .001	.343 .034	3.75 .15	5
88-24 102.50 104.00 .01 .01 .01 .003	.343 .103	3.45 .47	7
88-24 104.00 105.50 .01 .01 .01 .001	.343 .034	3.03 .03	3
88-24 105.50 106.93 .01 .01 .01 .006	.343 .206	3.15 .03	3
88-24 106.93 107.83 .01 .01 .01 .001	.343 .034	3.53 .01	Í
88-24 107.83 108.90 .08 1.21 .04 .002	1.371 .069	1.33 .05	5
8-24 108.90 110.40 .55 2.16 .34 .038 1	1.657 1.303	4.83 1.31	í
38-24 110.40 110.96 7.91 7.83 5.89 .312 20	1.945 10.697	16.31 4.10)

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%Pb %2n oz/tAg oz/tAu g/tAg g/tAu %Fe

%As

<u>~ 88-24</u>	110.96	111.37	9.53	15.45	6.56	.389	224.916	13.337	21.94	5.26
24–8د ′	111.37	112.56	.09	.05	.12	.016	4.114	.549	4.03	2.82
88-24	112.56	113.70	85	26	1 54	075	52 800	2 571	9 03	2 89
88-24	113 70	11/ 03	52	1 70	2 21	224	70 201	7 600	27 60	14 15
00 24	114 03	114.00		1.70	2.51		79.201	1.000	27.09	14.15
00-24	114.05	115.40	.02	.06	.06	.003	2.057	.103	4.18	• 1 1
88-24	115.40	116.70	.01	.01	.01	.003	.343	.103	3,40	.04
88-25	106.07	107.35	.04	.07	.05	.003	1.714	.103	1.85	.46
88~25	107.35	108.64	.77	1.66	.32	.003	10.972	.103	1.84	.30
88-25	108.64	110.06	.01	.01	.01	.001	.343	.034	3.58	.01
88-25	110.06	111.26	01	01	01	001	343	034	A 73	.01
88-25	111 26	112 73	01	01	01	001	343	034	4.75	.01
00 20	110 70	114 26	.01	.01	.01	.001		.034	4,40	.01
00-25	112.75	114.20	.01	.01	.01	.001	.343	.034	3.87	.01
88-25	114.26	115.25	.04	.01	.04	.004	1.371	.137	4.63	.26
88-25	115.25	116.00	.02	.02	.02	.001	.686	.034	1.97	.01
88-25	116.00	116.66	3.34	5.31	1.36	.028	46.629	.960	3.03	1.37
88-25	116.66	117.50	.09	3.20	.01	.003	.343	.103	.98	.04
88-25	117.50	117.80	.10	13.97	. 02	.005	. 686	.171	1 64	01
88-25	117.80	118.04	01	12	01	001	343	034	1 5 9	.01
88-25	118 04	118 51		2 12	.01	1 2 7	12 272	1 607	2.39	2 2 2 2
00 25	110.04	110.04	.02	3.43		.13/	100 070	4.697	0.38	3.23
00-25	110.54	119.21	5.27	1.00	3.19	.414	109.372	14,194	20.28	8.51
88-25	119.21	119.98	4.08	7.60	2.38	.258	81.601	8.846	9.53	3.68
88-25	119.98	120.35	.14	.11	.09	.045	3.086	1.543	7.25	5.57
88-25	120.35	120.59	.91	1.99	1.25	1.606	42.857	55.063	28.53	29.03
88-25	120.59	121.47	.15	.02	.14	.043	4.800	1.474	2.55	1.54
88-25	121.47	122.18	- 48	.06	.52	1.180	17.829	40.457	22 42	21 09
88-25	122.18	123 47	09	24	11	022	3 771	754	2 50	1 /0
88-25	122.10	124 40	.05	2 0 2		.022	14 742	1 004	2.50	1.40
00-25	123.47	124.40	10 60	15 00	.45	.030	14.743	1.234	4.71	2.47
>0-25	124.40	125.55	10.68	15.92	8.43	.318	289.031	10.903	17.60	5.49
88-25	125.55	126.88	.05	.04	.13	.018	4.457	.617	4.00	2.81
88-25	126.88	128.29	.08	.08	.19	.011	6.514	.377	2.59	.28
88-25	128.29	128.52	.30	.13	1.45	.099	49.715	3.394	18.76	13.25
88-25	128.52	129.78	.03	.01	.01	.002	.343	.069	2.10	. 01
88-25	129.78	130.11	. 45	1.04	1.21	074	41.486	2 537	5 08	1 79
88-25	130.11	131.38	. 01	01	01	001	343	034	3 16	111
88-25	132 00	132 51	01	.01	01	.001		102	5.10	.01
99-25	133 52	134 00	.01	.02	.01	.003	.343	.105	5.20	.07
00.20	115.72	117 00	• 10	.00	.13	.041	4.457	1.406	5.26	.61
00-20	115.74	11/.00	.07	.09	.07	.002	2.400	.069	2.03	.03
88-26	117.00	118.00	.40	.16	.21	.004	7.200	.137	2.44	.06
88-26	118.00	118.77	.14	.11	.08	.003	2.743	.103	3.33	.09
88-26	118.77	119.14	1.80	3.41	.78	.026	26.743	.891	3.15	.78
88-26	119.14	119.82	6.73	11.12	4.58	.442	157.030	15.154	20.71	9.03
88-26	119.82	120.40	.76	.57	4.83	.246	165.601	8.434	6 98	4 08
88-26	120.40	121.46	14	.12	46	019	15 772	651	1 76	4.00
88-26	121 46	122 70		1 72	2 67	104	01 544	2 5 6 6	10 11	.00
99-26	122 70	122.70		1.72	2.07	.104	91,044	3.300	10.11	3.52
00-20	102.70	123.25	.03	.00	.09	.006	3.086	.206	3.03	. 33
88-26	123,25	124.28	.01	.01	•01	.002	.343	.069	3.78	.03
88-26	124.28	125.38	.01	.01	.01	.001	.343	.034	2.95	.02
88-27	78.03	78.95	.05	.01	.03	.003	1.029	.103	2.84	.01
88-27	78.95	79.39	1.80	.66	1.15	.010	39.429	.343	2.70	10
88-27	79.39	79.55	17.86	13.17	12.82	,211	439 547	7 234	20 39	1 66
88-27	79.55	79 74	3 5 8	5 25	2 20	177	78 515	6 060	Q 10	1 25
88-27	70 7/	80 1F	11 70	12 71	0.21	2ED	220.010	10.009	22 00	1.40
00 27	00 16	00.10	12.10	12.14	2.04	.352	520.231	12.009	23.02	3.6/
	01.10	01.33	.13	· 1 1	.13	.053	4.457	1.817	4.99	3.66
18-21	81.33	81.94	8.08	8.87	4.36	.674	149.487	23.109	19.00	14.14

HOLE-ID	E	R	C	ŀŀ	1
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1	98-27	81.94	82.40	7.67	6.57	4.28	.167	146.744	5.726	7.35	1.41
•	8-27	82.40	82.91	.29	1.47	.21	006	7.200	.206	2.53	.19
	88-27	82.91	83.60	7.92	18.88	5.09	.572	174.516	19 612	14 18	9.78
	88-27	83 60	84 43	27	40.00	J.UJ /11	036	14 057	1 234	4 04	1 25
	00-27	03.00	04.40	10	.97	10	.030	14.037	1.234	4.04	1.35
	00-27	04.43	00.49	.10	.16	.19	.071	6.514	2.434	5.88	4.73
	88-27	85.49	86.33	.04	.02	.06	.010	2.057	.343	4.92	1.41
	88-27	86.33	86.86	2,22	3.70	1.30	.043	44.572	1.474	6.33	3.41
	88-27	86.86	88.42	.07	.13	.07	.018	2.400	.617	3.81	1.81
	88-27	88.42	89.00	.62	2.26	.81	.081	27.772	2.777	10.85	8.44
	88-28	77.48	78.35	.01	.06	.02	.003	.686	.103	2.98	15
	88-28	78.35	78.70	13.08	9.12	10.48	352	359.317	12 069	23 84	2 07
	88-28	78 70	79 45	15	56	15	056	5 143	1 920	3 / 9	1 90
	88-28	70.15	80.00			1 21	1 1 1	44 015	4 027	17 02	1.07
	00-20	20.40	80.00		.49	1.01	• 1 4 4	44.915	4.937	17.02	5.31
	00-20	80.00	80.70	.1/	.03	•1/	.019	5.829	.651	3.40	.81
	88-28	80.70	81.93	.05	.03	.05	.001	1.714	.034	1.41	.06
	88-28	81.93	82.56	7.49	9.21	2.94	.324	100.801	11.109	12.66	5.24
	88-28	82.56	83.60	.33	.66	.37	.066	12.686	2.263	8.43	4.67
	88-28	83.60	84.20	6.20	9.46	3.57	.071	122.401	2.434	6.96	3.48
	88-28	84.20	85.20	.09	1.50	.06	.002	2.057	.069	1.86	.13
	88-28	85.20	85.93	-23	4.37	.15	003	5,143	103	1 93	02
	88-28	85.93	86.35	.05	0.9	03	002	1 029	069	2 25	
	88-28	86 35	86 60	56	1 7	52	062	17 829	2 1 2 6	<u>0</u> 07	5 27
	88-28	86 60	97 25	.00	1.71		.002	242	2.120	9.07	J.Z/
	00-20	65 22	67.20	.02	.23	+ U I	.001	.343	.034	3.22	.04
	00-29	65.23	65.90	.31	.02	.21	.013	9.257	.446	4.39	1.10
	88-29	65.99	66.81	10.99	12.49	6.95	.568	238.288	19.474	13.77	10.24
	88-29	66.81	67.08	8.62	4.61	4,27	.273	146.401	9.360	7.37	4.98
	88-29	67.08	67.25	14.07	19.71	7.17	.214	245.831	7.337	8.55	2.29
	38-29	67.25	68.88	3.18	11.62	1.18	.025	40.457	.857	1.97	,22
	88-29	68.88	69.33	.06	.01	.03	.004	1.029	.137	3.00	.38
	88-29	69.33	70.41	.04	.34	.05	.001	1.714	.034	2.33	.05
	88-29	70.41	70.81	14	2.84	14	009	4 800	309	6 74	1 05
	88-29	70 81	71 85	01	07		.003	3/3	103	3 65	1.00
	88-29	71 95	72 01	.01	.07	.01	.005	1 020	.103	3.05	.4/
	00 29	72 01	72.91	.01	.03	.03	.002	1.029	.069	3.91	.31
	00-29	72.91	73.40	• 2 2	.08	.52	-012	17.829	.411	4.89	2.95
	88-29	13.46	/4.85	.08	.01	.14	.037	4.800	1,269	13.46	12.92
	88-29	74.85	75.25	1.02	.64	1.30	.068	44.572	2.331	23.14	24.99
	88-29	75.25	75.43	.09	.04	.06	.006	2.057	.206	3.67	3.02
	88-29	75.43	75.85	.77	.08	.85	.039	29.143	1.337	15.67	15.16
	88-29	75.85	76.13	5.00	.19	5.73	.163	196.459	5.589	25.75	26.03
	88-29	76.13	77.04	1.02	.25	.79	.002	27.086	.069	7.51	24
	88-29	77.04	77.24	4.24	8.32	2.85	004	97 715	137	13 96	05
	88-29	77 24	78 20	10	13	05	001	1 714	034	2 52	.00
	88-29	78 20	79 20	01	.1.0	.05	.001	1./13	.0.04	2.00	.01
	88-30	15 97	17 65	.01	.01	.01		.343	.034	2.11	.01
	00 30	43.07	47.00	.01	.01	.01	.002	.343	.069	3.04	.02
	00-30	47.00	47.97	5.35	6.09	4.23	.346	145.030	11.863	18.71	9.89
	88-30	47.97	49.00	.19	.34	.14	.003	4.800	.103	2.20	.03
	88-30	49.00	50.00	.24	.82	.14	.006	4.800	.206	2.39	.29
	88-30	50.00	51.11	.08	.46	.06	.003	2.057	.103	2.59	.13
	88-30	51.11	51.84	.75	.93	.60	.070	20.572	2.400	7.12	5.46
	88-30	51.84	52.05	2.31	.61	2.63	1.436	90,172	49,235	22.15	26 75
	88-30	52.05	52.48	1.28	65	95	228	32 572	7 817	μ. 1 C	1 00
	88-30	52 AR	53 00	<u></u> 01	.00		000	1 020	,.01/	C.T.	7.07
	78-30	52.40	53.00	.01	• • • •	.03	.009	11 255	- 309	5.32	.3/
	0-20	53.00	55.40	• ८ म	.05	.34	.025	11.65/	.857	8.89	2.93
	00-30	53.48	54.LU	.05	.04	.07	.010	2.400	.343	4.08	.35

HOLE-ID	FROM	TO	%₽b	%Zn	oz/tAg	oz/tAu	a g/tAg	g/tAu	%Fe	&As
88-30	54.10	54.64	.72	1.38	.35	.027	12.000	.926	3.34	1.14
38-30	54.64	55.43	.18	.19	.14	.015	4.800	.514	4.28	1.41
88-30	55.43	56.00	.04	.01	.03	.006	1.029	.206	3.16	.27
88-30	56.00	57.00	.06	.01	.07	.006	2.400	.206	3.72	.33
88-30	57.00	57.97	.05	.03	.05	.008	1.714	.274	4.13	.48
88-30	57.97	59.00	.11	.03	.18	.008	6.171	.274	2.62	.72
88-30	59.00	60.00	.29	.98	.27	.059	9.257	2.023	4.87	3.18
88-30	60.00	61.00	.10	.05	.07	.009	2.400	.309	2.71	.53
88-30	61.00	62.00	.43	.59	.18	.015	6.171	.514	3.24	.84
88-30	62.00	63.00	.10	.21	.10	.009	3.429	.309	4.37	.27
88-30	63.00	64.00	.04	.26	.08	.006	2.743	.206	3.17	.36
88-30	64.00	64.58	.17	.01	.25	.016	8.571	.549	7.70	.72
88-30	64.58	65.22	.03	.02	.02	.001	.686	.034	3.13	.04
88-30	65.22	66.00	.01	.01	.02	.005	.686	.171	2.76	.22
88-31	84.00	85.19	.01	.01	.02	.001	.686	.034	2.22	.03
88-31	85.19	85.93	.01	.01	.02	.001	.686	.034	3.13	.15
88-31	85.93	86.20	.81	1.13	.81	.586	27.772	20.092	17.24	16.43
88-31	86.20	86.62	6.46	14.25	8.74	.229	299.660	7.851	18.04	3.94
88-31	86.62	87.25	.05	.05	.09	.003	3.086	.103	3.77	.19
88-31	87.25	87.47	1.74	3.79	4.52	.265	154.973	9.086	18.83	9.25
88-31	87.47	88.70	.01	.01	.02	.003	.686	.103	.23	.09
88-31	88.70	90.00	.29	.53	.19	.071	6.514	2.434	1.26	1.34
88-31	90.00	91.21	.06	.12	.05	.020	1.714	.686	.44	.34
88-32	73.10	74.12	.01	.02	.02	.001	.686	.034	2.47	.02
88-32	124.94	126.63	.01	.01	.01	.002	.343	.069	4.58	.01
88-32	126.63	127.47	.02	.01	.02	.009	.686	.309	4.58	1.43
88-32	127.47	128.19	.10	.07	.14	.025	4.800	.857	6.02	1.51
38-32	128.19	129.04	2.49	5.57	2.51	.210	86.058	7.200	16.21	6.47
88-32	129.04	129.36	1.05	.51	2.36	.760	80.915	26.057	25.30	25.00
88-32	129.36	130.13	.01	.02	.05	.016	1.714	.549	.39	.44
88-32	130.13	131.61	.01	.02	.04	.010	1.371	.343	4.23	.21

APPENDIX E ASSAY

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ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: DEC 12 1988 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: D.e.c...b.e.c...b.e.c...b.e.c.

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MM FE SR CA F LA CR MG BA TI B W AND LIMITED FOR MA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: CORE AU* AMALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

EQUINOX RESOURCES LTD. FILE # 88-6223

S	AMPLE#	Pb PPM	Zn PPM	Ag PPM	Fe %	AS PPM	Au* PPB
D D D	33151 33152 33153	14 18351 22428	36 57344 99999	.5 119.9 89.9	3.81 12.51 8.36	336 86331 52311	79 22550 12445
D D	33154 33155	966 568	107 4 567	3.8 2.4	2.29 2.90	7306 1814	285 129
ם ם ם	33156 33157 33158 33159	395 600 577 409	81 137 3566 77	1.7 2.0 2.1 3.5	1.96 3.03 2.76 7.11	6608 3762 2170 251	265 235 109 225
D	33160	20088	73268	119.9	8 95	54553 47190	17700 6725
	33162 33163 33164 33165	1638 1638 21345 11496 16700	2006 30395 12581 19747	5.0 111.0 24.6 24.1	2.32 12.11 6.00 11.64	9903 99999 35551 99999	775 68700 3550 34600
ם ם ם ם	33166 33167 33168 33169 33170	18659 6412 21036 26392 604	64368 27145 27272 41753 551	105.6 12.8 70.1 65.0 1.1	13.50 3.92 18.24 14.67 4.97	999999 9803 99999 99999 3061	31750 1120 37600 24500 445
S	TD C/AU-R	39	132	7.4	4.08	40	520

- ASSAY REQUIRED FOR CORRECT RESULT - for Pb. 2n, As 7 1/. Ag 7 35 pm ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: DEC 12 1988 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: Dec 1/6./K.:

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GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HMC3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SE CA P LA CE MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: COTE AU* AMALTSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

SIGNED BY. C. D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS

EQUINOX RESOURCES LTD. FILE # 88-6223

S	AMPLE#	Pb PPM	Zn PPM	Ag PPM	Fe %	As PPM	Au* PPB
ם ם ם ם	33151 33152 33153 33154 33155	14 18351 22428 966 568	36 57344 99999 1074 567	.5 119.9 89.9 3.8 2.4	3.81 12.51 8.36 2.29 2.90	336 86331 52311 7306 1814	79 22550 12445 285 129
ם ם ם ם	33156 33157 33158 33159 33160	395 600 577 409 20088	81 137 3566 77 73268	1.7 2.0 2.1 3.5 119.9	1.96 3.03 2.76 7.11 11.27	6608 3762 2170 251 54553	265 235 109 225 17700
ם ם ם ם	33161 33162 33163 33164 33165	13078 1638 21345 11496 16700	13202 2006 30395 12581 19747	33.1 5.0 111.0 24.6 24.1	8.95 2.32 12.11 6.00 11.64	47190 9903 99999 35551 99999	6725 775 68700 3550 34600
ם ם ם ם	33166 33167 33168 33169 33170	18659 6412 21036 26392 604	64368 27145 27272 41753 551	105.6 12.8 70.1 65.0 1.1	13.50 3.92 18.24 14.67 4.97	99999 9803 99999 99999 3061	31750 1120 37600 24500 445
S	TD C/AU-R	39	132	7.4	4.08	40	520

- ASSAY REQUIRED FOR CORRECT RESULT for Pb. 2n, As 7 1/. Ag 7 35 pm ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: JAN 3 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: Jan. 6./8.9

ASSAY CERTIFICATE

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- SAMPLE TYPE: Core

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0015 Page 1

S.	AMPLE#	Pb %	Zn مج	Ag OZ/T	Au OZ/T	Fe %	As %
ם ם ם ם	33601 33602 33603 33604 33605	6.46 9.99 .50 .11 .25	7.76 11.23 .14 .26 .17	5.57 6.20 .30 .27 .29	1.106 .440 .115 .042 .009	22.17 21.87 17.80 3.20 2.20	12.27 8.18 20.34 1.88 1.10
ם ם ם ם	33606 33607 33608 33609 33610	.23 .02 .07 .73 .30	.13 .02 .06 .02 .14	.24 .01 .13 1.35 .84	.031 .004 .002 .054 .022	2.89 .98 1.40 11.90 5.50	1.38 .18 .19 10.30 3.81
ם ם ם ם	33611 33612 33613 33614 33615	2.86 2.03 .44 2.50 .28	.81 .94 1.10 1.39 .16	2.94 1.59 .44 3.96 .31	.334 .081 .078 .035 .012	20.14 10.87 7.59 4.86 2.53	20.83 11.10 7.63 3.77 1.49
ם ם ם ם	33616 33617 33618 33619 33620	.12 .37 .03 7.27 .04	.16 1.75 .10 10.67 .37	.11 .32 .01 4.56 2.22	.003 .002 .007 .606 .282	2.22 3.49 1.32 15.03 3.27	.09 .01 1.03 7.11 4.20
ם ם ם ם	33621 33622 33623 33624 33625	.01 2.57 .26 .14 2.75	.05 5.64 .83 .12 3.55	.27 2.41 .22 .05 1.22	.031 .346 .016 .018 .620	2.14 30.48 2.96 2.83 22.74	.41 8.23 1.18 .76 15.69
ם ם ם ם	33626 33627 33628 33629 33630	5.81 .26 6.86 2.82 1.30	8.09 .43 7.79 5.74 1.69	2.87 .19 4.03 1.88 1.10	.782 .028 .820 .544 .103	18.33 4.07 27.07 19.38 4.43	15.51 1.67 15.56 14.40 3.14
ם ם ם ם ם	33631 33632 33633 33634 33635	.13 .11 .15 .37 7.11	.21 .11 .01 .04 10.68	.05 .08 .13 .26 5.58	.012 .026 .066 .039 .560	4.31 4.22 21.79 2.19 26.37	.37 3.73 25.32 1.55 9.37
D	33636	.45	.61	.38	.299	10.37	7.66

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0015 Page 2

SAMPLE#	Pb	Zn	Ag	Au	Fe	As
	%	مج	OZ/T	OZ/T	%	%
D 33637	1.02	.60	1.15	1.390	26.13	29.96
D 33638	.14	.07	.13	.039	1.12	.96

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: .4

ASSAY CERTIFICATE

- SAMPLE TYPE: Pulp

EQUINOX RESOURCES LTD. FILE # 88-6223R

37	AMPLE≓	Pb %	Zn %	Ag .OZ/T	F e १,	AS *;	Au OZ/T	
E)	33151	. 01	.01	.02	3.59	.02	.003)
D	33152	4.74	6.71	4.13	20.38	13.78	.658	1.
D	33153	5.10	10.43	2.74	13.95	7.51	.410	1.
D	33154	.08	.10	.08	2.28	.63	.011	i.
D	33155	.05	.04	.06	2.76	. 15	.003/	
							· · · · (
D	33156	.03	.01	.06	2.01	. 59	.010	>
D	33157	.05	.01	.06	2.87	.32	.005	[
D	33158	.05	.42	.05	2.71	.19	.003	1
D	33159	.03	.01	.10	7.67	.02	.0095	Į –
D	33160	4.39	8.21	4.78	21.41	8.48	.522	$\lambda =$
D	33161	1.43	1.58	1.18	10.58	5.28	.211	1.12
Ð	33162	. 14	.19	.15	2.20	.79	.024	
D	33163	3.39	3.51	3.80	20.77	18.89	2.150	1-13
D	33164	L.19	1.41	.67	5.98	3.31	.106	· .*
Ð	33165	1.88	2.42	.81	20.71	17.28	.996	
D	33166	6.57	7.14	3.32	19.23	16.05	.930	,
D	33167	.64	3.00	.40	4.09	.99	.035	1
D	33168	3.69	3.24	2.31	29.40	19.51	1.110	
D	33169	3.54	5.28	2.36	20.88	17.10	.726	1
D	33170	.06	.06	.06	5.05	. 28	.016	

JAN 10 1989

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: JAN 19 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE (604) 253-3158 FAX (604) 253-1716 DATE REPORT MAILED: $\int \frac{\partial n}{\partial n} \frac{\partial n}$

ASSAY CERTIFICATE

- SAMPLE TYPE: Core AU - 10 GN REGULAR ASSAY. SIGNED BY.......D.TOTE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS EQUINOX RESOURCES LTD. PROJECT #220 FILE # 89-0114 Page 1

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S	AMPLE#	Pb %	Zn م	Ag OZ/T	Au OZ/T	Fe %	AS %
ם ם ם ם	33639 33640 33641 33642 33643	.05 1.80 17.86 3.58 11.78	.01 .66 13.17 5.35 12.74	.03 1.15 12.82 2.29 9.34	.003 .010 .211 .177 .352	2.84 2.70 20.39 9.10 23.02	.01 .10 1.66 1.25 3.67
ם ם ם ם	33644 33645 33646 33647 33648	.13 8.08 7.67 .29 7.92	.11 8.87 6.57 1.47 18.88	.13 4.36 4.28 .21 5.09	.053 .674 1 .167 .006 .572 1	4.99 19.00 7.35 2.53 14.18	3.66 14.14 1.41 .19 9.78
ם ם ם ם	33649 33650 33651 33652 33653	.37 .18 .04 2.22 .07	.97 .16 .02 3.70 .13	.41 .19 .06 1.30 .07	.036 .071 .010 .043 .018	4.04 5.88 4.92 6.33 3.81	1.35 4.73 1.41 3.41 1.81
ם ם ם ם	33654 33655 33656 33657 33658	.62 .01 13.08 .15 .55	2.26 .06 9.12 .56 .49	.81 .02 10.48 .15 1.31	.081 1 .003 .352 2 .056 .144 1	.0.85 2.98 3.84 3.49 7.02	8.44 .15 2.07 1.89 5.31
ם ם ם ם ם	33659 33660 33661 33662 33663	.17 .05 7.49 .33 6.20	.03 .03 9.21 .66 9.46	.17 .05 2.94 .37 3.57	.019 .001 .324 1 .066 .071	3.40 1.41 2.66 8.43 6.96	.81 .06 5.24 4.67 3.48
ם ם ם ם	33664 33665 33666 33667 33668	.09 .23 .05 .56 .02	1.50 4.37 .09 1.71 .23	.06 .15 .03 .52 .01	.002 .003 .002 .062 .001	1.86 1.93 2.35 9.07 3.22	.13 .02 .29 5.27 .04
D D D D D	33669 33670 33671 33672 33673	.31 10.99 8.62 14.07 3.18	.02 12.49 4.61 19.71 11.62	.27 6.95 4.27 7.17 1.18	.013 .568 1 .273 .214 .025	4.39 8.77 7.37 8.55 1.97	1.10 10.24 4.98 2.29 .22
Ð	33674	.22	.08	.52	.012	4.89	2.95

EQUINOX RESOURCES LTD. PROJECT #220 FILE # 89-0114 Page 2

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S.	AMPLE#	PD %	Zn %	Ag OZ/T	Au OZ/T	Fe %	As %
ם ם ם ם	33675 33676 33677 33678 33679	.08 1.02 .09 .77 5.00	.01 .64 .04 .08 .19	.14 1.30 .06 .85 5.73	.037 .068 .006 .039 .163	13.46 23.14 3.67 15.67 25.75	12.92 24.99 3.02 15.16 26.03
D D	33680 33681	1.02 4.24	.25 8.32	.79 2.85	.002 .004	7.51 13.96	.24 .05

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED:

1

JAN 25 1989 Jan 27/89.

ASSAY CERTIFICATE

- SAMPLE TYPE: CORE AU - 10 GN REGULAR ASSAY. SIGNED BY..... D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0166 Page 1

S	AMPLE#	Pb %	Zn %	Ag .OZ/T	Au OZ/T	Fe %	As १
ם ם ם ם	33682 33683 33684 33685 33685 33686	.01 .01 .03 .01 .01	.01 .01 .05 .01 .10	.01 .01 .06 .01 .01	.006 .001 .006 .013 .003	.74 .04 1.44 .51 .11	.40 .03 .40 .44 .06
ם ם ם ם	33687 33688 33689 33690 33691	.13 .55 .08 1.40 .07	.14 .78 .02 1.10 .07	.10 .42 .07 .98 .08	.110 .217 .011 .201 .005	6.40 9.92 4.09 10.91 .73	5.06 8.17 .66 4.93 .18
ם ם ם ם	33692 33693 33694 33695 33695 33696	.03 .23 .41 .01 .16	.09 .46 .51 .01 .15	.05 .18 .25 .05 .37	.005 .012 .030 .004 .051	3.49 6.29 5.64 3.96 10.41	.20 .71 2.00 .21 5.99
0000	33697 33698 33699 33700 34451	.09 .02 .06 .04 .64	.02 .11 .09 .03 .73	.24 .04 .08 .06 .68	.021 .004 .013 .006 .099	4.88 3.41 3.99 2.44 4.91	1.49 .26 1.24 .33 1.99
00000	34452 34453 34454 34455 34455 34456	.51 .34 1.82 1.15 .08	.23 .52 10.81 4.57 .86	4.15 .40 1.03 .57 .09	1.085 .043 .147 .637 .016	26.00 4.46 6.65 22.13 1.79	26.65 1.92 6.14 19.84 .67
00000	34457 34458 34459 34460 34461	.68 2.39 8.73 1.10 .57	8.25 13.30 18.05 7.76 1.37	.52 3.76 4.14 .41 .28	.150 .177 .155 .176 .009	9.96 13.62 15.47 11.32 3.02	1.77 4.77 5.02 4.54 .82
00000	34462 34463 34464 34465 34465	19.95 2.72 .29 .32 .61	18.33 12.83 1.22 .98 .55	9.59 2.73 .16 .18 .32	.132 .272 .008 .006 .096	5.30 26.73 3.04 1.99 9.52	.72 5.61 .34 .66 3.17
с	34467	1.74	3.99	.97	.052	1.93	.67

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0166 Page 2

SAMPLE#		Pb	Zn	Ag	Au	Fe	As
		چ	%	OZ/T	OZ/T	%	१
00000	34468	13.87	21.05	6.79	.296	15.32	4.03
	34469	.11	.05	.12	.046	4.01	1.80
	34470	1.15	.55	1.03	.058	5.42	2.26
	34471	.54	.45	.54	.038	5.51	2.09
	34472	.01	.01	.01	.002	3.04	.02
00000	34473	5.35	6.09	4.23	.346	18.71	9.89
	34474	.19	.34	.14	.003	2.20	.03
	34475	.24	.82	.14	.006	2.39	.29
	34476	.08	.46	.06	.003	2.59	.13
	34477	.75	.93	.60	.070	7.12	5.46
0 0 0 0 0 0	34478 34479 34480 34481 34482	2.31 1.28 .01 .21 .05	.61 .65 .01 .05 .04	2.63 .95 .03 .34 .07	1.436 .228 .009 .025 .010	22.15 6.15 5.32 8.89 4.08	26.75 4.89 .37 2.93 .35
00000	34483 34484 34485 34486 34486 34487	.72 .18 .04 .06 .05	1.38 .19 .01 .01 .03	.35 .14 .03 .07 .05	.027 .015 .006 .006 .008	3.34 4.28 3.16 3.72 4.13	1.14 1.41 .27 .33 .48
00000	34488	.11	.03	.18	.008	2.62	.72
	34489	.29	.98	.27	.059	4.87	3.18
	34490	.10	.05	.07	.009	2.71	.53
	34491	.43	.59	.18	.015	3.24	.84
	34492	.10	.21	.10	.009	4.37	.27
C C C C C	34493 34494 34495 34496	.04 .17 .03 .01	.26 .01 .02 .01	.08 .25 .02 .02	.006 .016 .001 .005	3.17 7.70 3.13 2.76	.36 .72 .04 .22

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ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: JAN 27 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: F.b..././.?.

ASSAY CERTIFICATE

- SAMPLE TYPE: CORE SIGNED BY. D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0189

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S.	AMPLE#	PD %	Zn %	Ag .0Z/T	Au OZ/T	Fe %	As %
ם ם ם ם	34497 34498 34499 34500 33551	.01 .61 3.96 .20 .30	.01 4.85 21.38 .35 .19	.01 .63 3.96 .08 .13	.001 .184 .516 .008 .003	.71 6.46 7.75 2.25 2.48	.05 4.07 6.77 .61 .13
ם ם ם ם	33552 33553 33554 33555 33556	.08 2.48 .47 5.41 .04	.04 2.88 2.43 12.25 .28	.06 2.59 .23 2.47 .03	.041 .910 .012 .304 .010	3.62 21.10 2.08 10.75 2.59	1.57 23.08 .18 6.82 .39
ם ם ם ם	33557 33558 33559 33560 33561	3.57 2.41 5.58 .04 .06	14.91 6.55 8.74 .11 .07	2.43 1.43 4.14 .05 .08	.129 .028 .090 .003 .006	14.26 8.13 9.09 1.21 3.65	5.63 .75 2.31 .34 .30
ם ם ם ם	33562 33563 33564 33565 33565 33566	3.59 .32 .10 .28 .61	1.09 .31 .02 .05 .04	3.12 .52 .25 .76 1.34	.216 .036 .015 .034 .065	11.22 8.45 6.04 28.45 8.39	7.36 2.15 1.01 2.35 2.36
ם ם ם ם	33567 33568 33569 33570 33571	.15 .01 .01 .01 .01	.15 .01 .01 .01 .01	.29 .01 .02 .03 .02	.011 .001 .001 .001 .001	4.69 1.51 7.31 5.48 1.20	.83 .01 .01 .02 .01
ם ם ם ם	33572 33573 33574 33575 33576	.01 .01 .81 6.46 .05	.01 .01 1.13 14.25 .05	.02 .02 .81 8.74 .09	.001 .001 .586 .229 .003	2.22 3.13 17.24 18.04 3.77	.03 .15 16.43 3.94 .19
D D D D	33577 33578 33579 33580	1.74 .01 .29 .06	3.79 .01 .53 .12	4.52 .02 .19 .05	.265 .003 .071 .020	18.83 .23 1.26 .44	9.25 .09 1.34 .34

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: JAN 31 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: Jeb. 6.184.

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ASSAY CERTIFICATE

- SAMPLE TYPE: Core

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SIGNED BY. N. . D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0223

S	AMPLE#	Pb	Zn	Ag	Au	Fe	As
		%	%	OZ/T	OZ/T	0,0	0%
D	33701	.22	.01	.07	.001	.10	.01
D	33702	.01	.01	.01	.001	.07	.01
D	33703	.18	.23	.19	.035	1.49	.91
D	33704	.15	.28	.11	.003	1.97	.12
D	33705	.06	.19	.08	.001	4.32	.12
D	33706	.02	.07	.03	.002	5.07	. 04
D	33707	.34	.50	.21	.017	3.43	.76
D	33708	.11	.03	.09	.031	4.67	.26
D	33709	.04	.08	.06	.012	4.32	.56
D	33710	.01	.02	.01	.004	3.23	.06
D	33711	. 04	. 01	. 06	. 001	2.76	. 01
ñ	33712	.01	.01	.01	.001	2.87	.07
D	33713	.34	.64	.52	.009	4.56	.44
D	33714	.06	.07	.04	.001	4.55	.09
D	33715	.08	.56	.03	.003	1.31	.04
D	33716	.01	.03	.04	.002	3.61	.16

ACME ANALYTICAL LABORATORIES LTD. DA 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 DATE RECEIVED: FEB 7 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: F.C. 1989

ASSAY CERTIFICATE

- SAMPLE TYPE: Core

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SIGNED BY.

, D.TOYE, C.LEONG, B.CHAN, J.WANG; CERTIFIED B.C. ASSAYERS

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0257

SAMPLE#		Pb	Zn	Ag	Au	Fe	As
		8	8	OZ/T	OZ/T	%	8
				•	• -	-	-
С	34401	.04	.01	.05	.007	4.32	1.69
С	34402	.01	.02	.01	.001	1.83	.10
С	34403	.03	.44	.03	.002	3.45	.41
С	34404	.01	.01	.01	.001	4.37	.01
С	34405	.01	.01	.01	.001	4.10	.01
С	34406	.01	.01	.01	.001	2.80	.01
С	34407	.15	.05	.06	.001	2,99	.15
С	34408	.49	1.51	.27	.057	5.72	2.22
С	34409	2.02	10.05	1.20	.080	7.96	2.46
С	34410	.15	.64	.05	.004	1.40	.13
С	34411	.02	.03	.01	.001	1.07	.04
Ç	34412	1.08	3.40	.44	.117	8.65	2.60
С	34413	1.08	2.82	.90	.167	11.34	3.50
С	34414	.04	.08	.02	.004	2.34	.04
С	34415	.14	.19	.18	.156	6.62	3.58
С	34416	1.71	4.22	2.08	.364	13.83	9.93
С	34417	.14	.08	.13	.060	4.38	3.00
С	34418	1.77	4.68	2.36	.281	18.16	15.17
С	34419	.63	. 27	.65	.112	4.96	3.45

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: FEB 6 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: July 13, 1989

ASSAY CERTIFICATE

- SAMPLE TYPE: Core

SIGNED BY ... A. C. C. P. D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0252 Page 1

Ş,	AMPLE#	Pb %	Zn %	Ag OZ/T	Au OZ/T	Fe %	As %
D	33581	.01	.03	.03	.002	3.91	.31
D D	33583	.01	.01	.03	.001	2.55	.01
D	33585	.03	.01	.07	.003	5.19	.27
D D	33586 33587	.01 .01	.01 .01	.01 .01	.001	2.78 3.75	.01
Ð	33588	.01	.01	.01	.003	3.45	.47
D	33589	.01	.01	.01	.001	3.03	.03
D	33590	.01	.01	.01	.006	3.15	.03
D	33591	.01	.01	.01	.001	3.53	.01
Ð	33592	.08	1.21	.04	.002	1.33	.05
D	33593	.55	2.16	.34	.038	4.83	1.31
ц П	33595	9 53	15 45	5.89	320	21 94	4.10
2	55555	3.33	13.45	0.00		41,94	9.20
D	33596	.09	.05	.12	.016	4.03	2.82
D D	33551	.80 50	.20	1.04	.0/5	9.03	2.89
D	33599	.02	.06	.06	. 2 2 4	4.18	14,15
D	33600	.01	.01	.01	.003	3.40	.04
D	33717	.04	.07	.05	.003	1.85	.46
D	33718	.77	1.66	.32	.003	1.84	.30
D D	33/19	.01	.01	.01	.001	3.58	.01
'n	33720	.01	.01	.01	001	4.75	.01
_		.01	.01			1.10	.01
D	33722	.01	.01	.01	.001	3.87	.01
D D	33123	.04	.01	.04	.004	4.63	.25
n n	33724	3 34	5 31	1 36	0.28	3 03	1 37
ם	33726	.09	3.20	.01	.003	.98	.04
D	33727	.10	13.97	.02	.005	1.64	.01
D	33728	.01	.12	.01	.001	1.59	.01
D	33729	.82	3.43	.39	.137	6.38	3.23
ц л	33730	5.27	7.06	3.19	.414	20.28	8.51
U	33/31	4.08	1.00	2.30	.238	9.33	3.08
D	33732	. 14	. 11	. 09	.045	7.25	5.57

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0252 Page 2

SAMPLE#		Pb %	Zn %	Ag OZ/T	Au OZ/T	Fe %	As %	
D D	33733 33734	.91 .15	1.99	1.25	1.606	28.53	29.03 1.54	
D D D	33735 33736 33737	.48 .09 .58	.06 .24 2.03	.52 .11 .43	1.180 .022 .036	22.42 2.50 4.71	$21.09 \\ 1.48 \\ 2.47$	
ם ם ם	33738 33739 33740 33741	10.68 .05 .08	15.92 .04 .08	8.43 .13 .19	.318 .018 .011	17.60 4.00 2.59	5.49 2.81 .28 13.25	
D	33742	.03	.01	.01	.002	2.10	.01	
ם ם ם ם	33743 33744 33745 33746 33747	.45 .01 .01 .10 .06	1.04 .01 .02 .08 .01	1.21 .01 .13 .03	.074 .001 .003 .041 .004	5.08 3.16 5.28 5.26 3.00	1.79 .01 .07 .61 .38	
D D D	33748 33749 33750	.04 .14 .01	.34 2.84 .07	.05 .14 .01	.001 .009 .003	2.33 6.74 3.65	.05 1.05 .47	

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ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: FEB 10 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: July 15,1989

ASSAY CERTIFICATE

- SAMPLE TYPE: Core

SIGNED BY. . A. Chip: . D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS EQUINOX RESOURCES LTD. PROJECT #220 FILE # 89-0294 Page 1

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SA	AMPLE#	Cu %	Pb %	Zn ۶	Ag OZ/T	Au OZ/T	Fe %	As چ
ם ם ם	33751 33752 33753 33754 33755	.01 .01 .06 .40 .02	.02 .01 .12 .25 .03	.01 .04 .01 .05 .01	.05 .02 .87 5.94 .16	.005 .001 .177 .064 .020	2.99 2.56 8.12 17.23 2.66	.25 .08 7.42 12.13 .95
ם ם ם ס	33756 33757 33758 33759 33760	.01 .01 .02 .01 .01	.01 .01 .03 .01 .01	.01 .01 .01 .01 .01	.03 .01 .37 .12 .07	.001 .008 .004 .003 .001	1.96 2.44 3.09 2.93 3.04	.16 .53 .56 .37 .06
ם ם ם	33761 33762 33763 33764 33765	.02 .06 .08 .08 .02	.04 .37 .70 2.30 .22	.01 .19 .49 6.75 .85	.09 .58 1.01 .95 .21	.007 .332 .450 1.090 .292	3.62 12.91 12.11 22.34 16.91	.69 10.47 11.25 16.65 5.98
ם ם ם מ	33766 33767 33768 33769 33770	.19 .47 .01 .03 .01	4.08 2.34 .01 .10 .07	18.73 6.73 .02 .21 .19	2.98 3.80 .08 .35 .12	.372 .350 .033 .026 .011	20.41 28.67 3.25 2.51 1.11	5.38 4.86 .89 .23 .34
ת ם ם ם	33771 33772 33773 33774 33775	.01 .01 .01 .01 .01	.02 .02 .01 1.47 .02	.01 .04 .02 .49 .05	.07 .11 .02 .64 .05	.001 .003 .001 .003 .001	2.34 2.44 2.23 2.71 1.85	.01 .46 .01 .36 .09
D D D D D	33776 33777 33778 33779 33779 33780	.01 .01 .01 .05 .31	.07 .14 .48 .63 5.59	.11 .02 4.83 2.28 16.98	.13 .15 .34 .60 4.17	.007 .120 .007 .049 .127	4.27 13.99 2.56 8.56 13.79	1.38 13.56 .39 2.96 3.46
D D D D D	33781 33782 33783 33783 33784 33785	.27 .03 .26 .43 .57	5.62 1.55 9.88 .80 4.55	9.22 .56 13.82 .43 9.61	3.99 1.39 6.59 1.04 9.04	.508 .378 .428 .140 .578	18.63 5.87 20.70 20.91 19.10	11.54 4.79 7.32 13.88 12.84
D	33786	.42	.61	2.05	1.32	.116	21.34	5.96

EQUINOX RESOURCES LTD. PROJECT #220 FILE # 89-0294 Page 2

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S	AMPLE#	Cu %	Pb %	Zn %	Ag OZ/T	Au OZ/T	Fe ۶	As %
ם ם ם	33787 34420 34421 34422 34423	.01 .23 .10 .10 .02	.01 14.37 .01 .32 .01	.01 13.97 .01 .31 .01	.01 11.40 .05 .30 .01	.011 .356 .001 .030 .008	2.68 21.56 4.91 6.33 3.15	.11 4.64 .01 1.13 .01
ם ם ם ם	34424 34425 34426 34427 34428	.05 .09 .01 .01 .01	.01 .15 .01 .01 .02	.01 .38 .01 .01 .03	.02 .31 .01 .01 .01	.002 .376 .002 .002 .013	3.74 7.81 3.83 4.07 3.37	.22 5.24 .01 .01 .27
ם ם ם ם	34429 34430 34431 34432 34433	.01 .01 .01 .02 .03	.01 .09 .05 .95 .40	.03 .28 .10 .46 2.82	.01 .05 .03 .56 .24	.004 .002 .005 .530 .014	2.72 2.25 2.86 18.66 3.17	.01 .10 .23 14.78 .68
ם ם ם ם	34434 34435 34436 34437 34438	.42 .11 .33 .17 .12	5.09 1.88 9.98 .14 .06	5.02 .47 8.23 .02 .03	3.95 1.15 6.37 .38 .22	.239 .049 .404 .024 .012	22.39 10.12 20.82 10.01 2.23	9.81 6.24 10.25 3.40 .86
ם ם ם ם	34439 34440 34441 34442 34443	.37 .09 .64 .02 .01	.17 .01 .42 .01 .03	.02 .01 1.27 .02 .12	1.19 .06 1.38 .02 .04	.158 .004 .404 .003 .003	15.45 5.03 20.06 3.23 1.81	14.95 .04 13.19 .16 .15
ם ם ם ם	34444 34445 34446 34447 34448	.01 .01 .01 .01 .03	.01 .01 .01 .01 1.15	.01 .05 .06 .01 2.34	.01 .02 .01 .01 .61	.008 .002 .004 .002 .210	3.60 3.52 1.65 2.97 8.41	.09 .12 .19 .07 5.18
D D	34449 34450	.46 .01	11.14	14.16	6.81 .02	.314	20.42	5.14 .19
JUL ASSAN

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: FEB 17 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: Feb 20, 1989

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ASSAY CERTIFICATE

- SAMPLE TYPE: Core

SIGNED BY ... Achefy. D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS

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EQUINOX RESOURCES LTD. PROJECT #220 FILE # 89-0358

S	AMPLE#	Pb	Zn	: Ag	Fe	As	Au
		010	20	OZ/T	96	010	OZ/T
D	33788	.01	.05	.03	2.52	.21	.004
D	33789	.01	.01	.01	3,00	.23	.003
D	33790	.01	.01	.03	2.82	. 25	.004
D	33791	.01	.01	. 02	2.18	.01	.001
D	33792	.03	.01	.05	2.59	.45	.003
D	33793	.02	.01	.06	2.33	.46	.007
D	33794	4.25	5.52	3.79	19.67	10.90	.640
D	33795	.77	.47	.61	8.15	6.15	.176
D	33796	.13	.05	.28	7.63	4.85	.076
D	33797	.04	.01	.18	3.98	.49	.009
D	33798	.04	.02	.14	4.49	1.02	.013
D	33799	.06	.12	.25	6.19	3.67	.067
D	33800	3.00	19.09	2.47	22.40	14.18	1.006
D	33801	.03	.05	.05	2.31	2.10	.113
D	33802	.02	.05	.03	1.57	.72	.025
Ð	33803	.01	.01	.02	. 04	.03	.013
D	33804	.28	.15	.43	4.38	2.34	.051
Ð	33805	.22	.38	. 25	8.66	8.56	.148
D	33806	.02	.01	.05	4.71	1.95	.018
Ď	33807	.05	.14	.07	2.75	1.17	.035
D	33808	.01	.05	.02	1.77	. 33	.005
D	33809	.06	.01	.17	12.89	13.55	.146
D	33810	. 01	. 01	. 01	1.73	. 0.3	.002

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: FEB 26 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED:

ASSAY CERTIFICATE

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- SAMPLE TYPE: Core

SIGNED BY. S. D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0439

S	AMPLE#	Pb %	Zn ج	Ag OZ/T	Fe %	As %	Au OZ/T
D D D D D	33875 33876 33877 33878 33879	.03 2.04 .86 3.84 .22	.10 4.82 41.42 6.18 .53	.01 .68 .37 2.54 .13	.66 1.65 .95 1.72 2.46	.01 .01 .21 .30	.001 .003 .002 .027 .003
ם ם ם ם	33880 33881 33882 33883 33883 33884	6.37 .35 .06 .28 1.94	33.25 .95 .21 .95 12.26	2.85 .11 .02 .13 1.24	2.38 1.52 1.90 3.58 13.59	.01 .01 .01 1.65 7.79	.031 .001 .001 .031 .456
D D D D D	33885 33886 33887 33888 33888 33888	.40 7.11 .10 .17 .06	1.24 9.88 .14 .80 .03	.40 3.96 .23 .32 .32	2.80 16.91 4.85 4.78 1.49	1.15 9.79 .49 .63 .28	.042 .634 .013 .015 .008
ם ם ם ם	33890 33891 33892 33893 33894	.01 .01 .01 .01 .01	.01 .01 .01 .01 .01	.01 .01 .05 .01 .01	1.69 .95 1.62 .81 .43	.03 .07 .12 .07 .01	.001 .001 .002 .001 .001
ם ם ם ם	33895 33896 33897 33898 33898 33899	.03 .01 3.63 .29 1.24	.10 .01 16.95 1.35 21.38	.02 .01 1.95 .15 1.14	3.24 3.77 2.84 .51 1.43	.01 .04 .01 .01 .01	.001 .001 .005 .001 .031
ם ם ם מ	33900 33901 33902 33903 33904	.05 .04 .17 8.65 2.07	.38 .16 1.42 19.57 9.57	.02 .03 .07 3.52 .97	2.33 2.18 1.17 2.85 3.67	.03 .16 .04 .86 .97	.001 .002 .001 .110 .052
D D	33905 33906	6.16 .03	14.37 .05	3.16 .04	5.47 3.98	1.50 .10	.130

MAR 0 3 1989

ASSAY CERTIFICATE

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- SAMPLE TYPE: Core

EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0405 Page 1

SA	MPLE#	Pb %	Zn %	Ag OZ/T	Fe %	As %	Au OZ/T
D D D D D	33811 33812 33813 33814 33814 33815	.01 .02 2.58 .03 .10	.01 .03 9.05 2.72 8.47	.01 .03 2.00 .05 .06	2.22 2.97 11.58 3.24 1.63	.03 .83 2.24 2.73 .66	.002 .016 .130 .080 .021
D D D D D	33816 33817 33818 33819 33820	.02 .38 2.38 30.41 .54	.05 .63 5.38 8.27 .61	.01 .14 .84 10.56 .17	2.13 1.71 8.23 4.02 1.42	.97 .72 6.22 2.22 .72	.016 .020 .217 .180 .015
ם ם ם ם ם	33821 33822 33823 33824 33825	.45 .03 .09 .24 .03	.09 .02 .01 .01 .01	.21 .03 .14 .91 .07	5.12 2.19 4.75 3.18 1.62	3.95 1.02 2.22 1.29 .10	.079 .023 .036 .019 .003
D D D D D	33826 33827 33828 33829 33830	.07 1.66 3.02 5.45 12.25	.07 5.08 16.34 7.80 20.89	.10 1.19 3.19 3.18 7.81	2.27 18.50 24.95 22.94 17.95	.48 15.21 15.72 22.34 8.22	.012 1.100 1.300 1.620 .656
ם ם ם ם ם ם	33831 33832 33833 33834 33835	.04 .06 .01 .01 .02	.23 .09 .02 .01 .01	.05 .05 .02 .01 .02	.34 .09 2.47 4.58 4.58	.26 .03 .02 .01 1.43	.022 .003 .001 .002 .009
D 3 D 3 D 3 D 3 D 3	33836 33837 33838 33838 33839 33840	.10 2.49 1.05 .01 .01	.07 5.57 .51 .02 .02	.14 2.51 2.36 .05 .04	6.02 16.21 25.30 3.91 4.23	1.51 6.47 25.00 .44 .21	.025 .210 .760 .016 .010
D 3 D 3 D 3 D 3 D 3	33841 33842 33843 33844 33844 33845	.21 2.38 .20 2.45 .54	1.99 17.12 .79 3.62 .36	.14 1.67 .31 1.58 .55	1.43 6.76 7.42 21.06 10.28	.02 2.53 3.10 18.02 3.09	.001 .063 .027 .960 .142
D 3	33846	.17	.36	.71	4.68	.69	.030

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EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0405 Page 2

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S.	AMPLE#	Cu ع	Pb %	Zn %	Ag OZ/T	Fe %	As %	Au OZ/T
D D D D D	33847 33848 33849 33850 33851	- - -	.01 .03 .04 .08 .01	.01 .08 .07 .03 .01	.04 .04 .03 .06 .01	3.18 2.98 4.26 2.70 3.41	.15 .34 .07 .49 .01	.007 .009 .002 .011 .001
ם ם ם ם	33852 33853 33854 33855 33855 33856	. 03	.01 1.33 .62 .01 .26	.01 .02 .06 .01 .06	.01 .97 .47 .01 .20	3.84 2.34 .75 .25 2.56	.01 .01 .01 .01 .01	.001 .001 .001 .001 .001
ם ם ם ם ם	33857 33858 33859 33860 33861	- .50 .70	.60 .07 11.09 .10 2.92	1.40 .05 14.16 .07 2.85	.42 .05 7.47 .06 3.21	4.53 3.07 18.71 2.52 24.42	.01 .64 4.20 .73 17.16	.001 .005 .340 .016 .536
ם מ ח ח ח	33862 33863 33864 33865 33865 33866	- - -	.02 .02 .07 .40 .14	.04 .02 .09 .16 .11	.01 .02 .07 .21 .08	3.44 4.31 2.03 2.44 3.33	.11 .13 .03 .06 .09	.026 .008 .002 .004 .003
ם ם ם ם	33867 33868 33869 33870 33871	- - -	1.80 6.73 .76 .14 .97	3.41 11.12 .57 .12 1.72	.78 4.58 4.83 .46 2.67	3.15 20.71 6.98 1.76 10.11	.78 9.03 4.08 .65 3.52	.026 .442 .246 .019 .104
D D D	33872 33873 33874		.03 .01 .01	.08 .01 .01	.09 .01 .01	3.03 3,78 2.95	.33 .03 .02	.006 .002 .001

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: FEB 27 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: Magach. 3/19

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ASSAY CERTIFICATE

- SAMPLE TYPE: ROCK PULP

MAR 0 6 1989

file

SIGNED BY D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS

EQUINOX RESOURCES LTD. FILE # 89-0441

SAMPLE#	Pb	Zn	Ag	As	Au
	%	%	GM/T	چ	GM/T
#1	4.63	7.37	101.0	5.60	15.30
#2	3.03	4.28	56.5	7.96	14.34
#5	4.83	7.41	117.5	11.16	21.80
#11	6.16	9.07	134.0	3.47	7.06
#12	2.65	6.85	64.0	5.86	8.97
#13	1.45	1.03	39.0	8.73	15.90
#15	2.09	3.24	63.5	5.22	9.19

ACME ANALYTICAL LABORATORIES LTD. DATE RECEIVED: MAR 1 1989 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED: MARL, 1.989

ASSAY CERTIFICATE

- SAMPLE TYPE: Core

SIGNED BY Stonard Chan D. TOYE, C. LEONG, B. CHAN, J. WANG; CERTIFIED B.C. ASSAYERS

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EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0466 Page 1

SAMPLE#	Pb	Zn	Ag	Au	Fe	As
	%	%	:02/T	OZ/T	%	%
D 33907	01.	.25	.01	.001	5.78	.02
D 33908	04.	.20	.01	.002	.74	.01
D 33909	2.80.	2.45	1.06	.003	1.49	.01
D 33910	44.	1.68	.16	.002	2.34	.53
D 33911	01.	.42	.01	.002	1.02	.01
D 33912	.16	3.88	.07	.001	4.45	.02
D 33913	.10	1.00	.04	.001	.83	.01
D 33914	3.91	10.97	1.67	.014	2.41	.15
D 33915	1.39	6.08	.67	.021	3.05	.75
D 33916	.43	1.81	.32	.047	4.73	2.34
D 33917	1.38	4.31	.72	.098	6.53	1.79
D 33918	4.17	2.84	3.21	.307	12.54	5.37
D 33919	.62	.44	.42	.031	2.24	.32
D 33920	.07	.14	.06	.005	2.70	.19
D 33921	.02	.02	.03	.002	1.87	.12
D 33922	.04	.01	.04	.011	1.65	.49
D 33923	.02	.01	.05	.002	3.29	.20
D 33924	12.37	11.38	4.61	.011	1.36	.01
D 33925	.06	.27	.01	.001	2.26	.01
D 33926	.06	.13	.04	.001	2.53	.04
D 33927	.02	.22	.01	.002	1.59	.15
D 33928	.24	.87	.17	.006	3.01	1.69
D 33929	.51	.34	.24	.024	4.19	2.64
D 33930	5.22	7.17	2.69	.700	18.42	13.61
D 33931	.20	1.33	.10	.015	2.80	.64
D 33932	6.38	5.91	5.22	.145	9.64	5.13
D 33933	12.73	13.91	7.41	.261	8.50	1.93
D 33934	1.49	3.33	.99	.121	9.77	2.85
D 33935	.09	.07	.13	.014	2.19	.59
D 33936	.09	.08	.03	.002	1.47	.01
D 33937	.17	1.61	.04	.001	.99	.01
D 33938	.06	.09	.07	.004	2.81	.78
D 33939	.01	.07	.01	.001	1.90	.01
D 33940	.23	.46	.25	.036	6.39	5.17
D 33941	.01	.05	.01	.002	2.09	.02
D 33942	7.91	14.45	3.01	.010	1.67	.03

EQUINOX RESOURCES PROJECT - 220 FILE # 88-0466 Page 2

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Sž	AMPLE#	Pb	Zn	Ag	Au	Fe	As
		*	8	OZ/T	OZ/T	40	0,6
D	33943	.11	.34	.08	.001	1.15	.03
D	33944	.01	.02	.01	.001	2.55	.01
D	33945	.08	.26	.04	.002	1.89	.11
D	33946	3.25	8.80	1.43	.103	6.22	1.69
ם	33947	.25	1.59	.21	.064	3.33	1.10
D	33948	5.07	7.50	3.32	.388	19.14	6.53
Ď	33949	.04	.02	.09	.010	2.84	.50
D	33950	.12	.07	.26	.024	4.62	1.04
D	33951	.12	.18	.10	.013	3.84	.35

DATE RECEIVED: MAR 27 1989 ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716 DATE REPORT MAILED:

March 30/89

ASSAY CERTIFICATE

- SAMPLE TYPE: Core [D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS SIGNED BY EQUINOX RESOURCES LTD. PROJECT 220 FILE # 89-0654 SAMPLE# Pb Zn Ag Au Fe As % % OZ/T OZ/T 8 ૠ

D 33952 1.84 4.09 1.74 .186 8.55 2.91

APPENDIX F METALLURGICAL RESULTS

Table 1	Head Analysis Lakefield Research
Table 2	Bulk Sample Gravity Testwork
Table 3	Drill Core Gravity Testwork
Table 4	Flotation of Drill Holes
	Results on Low Arsenic Zinc Concentrates

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Table No. 1 : Head Analysis

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		Assays,%,g/						
Element	Bulk	Comp 1	Comp 2	Comp 2A	Comp 3			
Lead,% Pb	1.73	4.30	2.76	0.43	2.75			
Zinc, % Zn	2.77	7.90	4.04	0.54	5.08			
Arsenic,% As	2.66	6.51	9.15	1.01	12.1			
Gold, art Au	4.47	10.3	15.0	1.32	19.1			
Silver, g/t Ag	46.9	103	60.1	14.8	86.0			
Specific Gravity.o/cm3	3.09	3.41	3.56	2.81	3.72			
		.l						

	Assays,%,0/1							
Element	Comp 4	Comp 4B	Comp 5	Comp 6	Comp 7			
Lead,% Pb	6.41	0.68	4.61	2.68	1.07			
Zinc, % Zn	8.15	0.50	8.10	3.88	2.11			
Arsenic,% As	13.4	5.59	12.1	9.81	3.54			
Gold. a/t Au	23.5	3.12	20.3	20.2	4.25			
Silver, o/t Ao	155	41.0	117	66.6	25.8			
Specific Gravity.g/cm ³	4.21	3.02	3.90	3.57	3.02			

	Assays,%,01							
Element	Comp 8	Comp 9	Comp 10	Comp 11	Comp 11A			
Lead.% Pb	3.70	6.34	2.56	5.63	0.92			
Zinc, % Zn	6.84	9.48	3.29	10.2	0.66			
Arsenic,% As	5.76	6.37	3.57	4.23	12.3			
Gold, a/t Au	6.80	9.79	4.55	7.85	1.40			
Silver, g/t Ag	88.0	152	67.3	138	36.0			
Specific Gravity,g/cm ³	3.54	3.58	3.22	3.44	3.38			

	Assays,%,0/1							
Element	Comp 12	Comp 13	Comp 14	Comp 15	Comp 16			
Lead.% Pb	2.57	1.30	1.76	1.93	2.38			
Zinc, % Zn	7.43	0.92	4.94	3.01	3.47			
Arsenic.% As	7.16	9.97	3.88	6.24	5.74			
Gold, an Au	9.27	15,2	5.50	8.63	5.93			
Silver, o/t Ag	61.3	37.8	45.0	55.4	85.2			
Specific Gravity.g/cm ³	3.25	3.27	3.11	3.38	3.33			

	Assays,%,01									
Element	Comp 17	Comp 18	Comp 19	Comp 20	Comp					
Lead.% Pb	2.42	1.38	1.93	3.30						
Zinc, % Zn	4.88	2.49	2.32	6.07						
Areenio,% As	4.92	3.56	6.18	8.59						
Gold, git Au	8.74	3.80	6.03	10.3						
Silver, o/t Ag	62.2	35.6	55.9	108						
Specific Gravity,g/om ³	3.21	3.06	3.30	3.63						

	Assays,%,g/t									
Element	Comp 17	Comp 18	Comp 19	Comp 20	Comp 21					
Lead,% Pb	2.42	1.38	1.93	3.30	1.93					
Zinc, % Zn	4.88	2.49	2.32	6.07	8.17					
Arsenic,% As	4.92	3.56	6.18	8.59	8.74					
Gold, g/t Au	6.74	3.80	6.03	10.3	19.9					
Silver, g/t Ag	62.2	35.5	55.9	108	65.0					
Specific Gravity.g/cm ³	3.21	3.06	3,30	3.63	3.85					

			Assays,%,o/		
Element	Comp 21A1	Comp 21A ₂	Comp 22	Comp 23	Comp 23A
Lead,% Pb	0.92	0.066	0.78	4.49	3.10
Zinc, % Zn	1.07	0.055	2.35	12.4	5.15
Arsenic,% As	3.65	0.62	4.82	18.4	3 33
Gold, g/t Au	2.83	0.23	6.37	37.7	3.89
Silver, g/t Ag	52.1	5.00	24.1	130	52.2
Specific Gravity.a/cm ³	3.05	2.88	3.19	4.55	3.19

	Assays, %, g/t									
Element	Comp 23B1	Comp 23B2	Comp 24	Comp 25	Comp 26					
Lead.% Pb	0.11	0.14	1.20	1.09	5.58					
Zinc, % Zn	0.15	0.12	2.45	4.80	7.04					
Arsenic,% As	1.18	0.70	9.94	8.42	5.83					
Gold, g/t Au	0.75	0.42	7.69	10.7	9.06					
Silver, g/t Ag	2.30	4,50	53.2	32.6	152					
Specific Gravity,g/cm ³	2.86	2.84	3.55	3.39	3.67					
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		Assays,%,g/t									
Element	Comp 27	Comp 28	Comp 28A	Comp 28B	Comp 29						
Lead,% Pb	1.77	2.84	0.26	4.81	1.25						
Zinc, % Zn	2.76	13.7	0.66	8.82	7,93						
Arsenic,% As	4.29	0.28	1.03	8.57	0.046						
Gold, g/t Au	5.56	0.52	1.03	17.0	0.18						
Silver, g/t Ag	101	52.2	4.70	88.9	20.1						
Specific Gravity.g/cm ³	3.24	3.12	2.91	3.69	3.02						

میں میں بینے میں میں بینے کر بینے میں وج چین میں م			Assays,%,0/		•
Element	Comp 29A	Comp 29B	Comp 30	Comp 31	Comp 32
Lead.% Pb	0.15	4.31	1.95	4,47	1.82
Zino, % Zn	0.67	14.1	4.80	7.29	4.66
Arsenic.% As	0.25	1.58	2.37	6.32	2.53
Gold. a/t Au	0.19	4.17	3.15	7,52	3.23
Silver, a/t Aa	3.30	73.8	41.1	84.3	37.5
Specific Gravity,g/cm3	2.81	3.27	3.05	3.48	3.15

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Element	Comp 33	Comp 34	Assays,%,0/t Comp 35	Comp 36	Comp 3
Lead.% Pb	9.13	2.05	4.97	1.384	3.58
Zinc, % Zn	8.49	5.67	5,10	3.67	7.36*
Arsenic.% As	3.39	5.19	2.37	1.90	4.13
Gold. a/t Au	7.02	6.36	3.26	2.54	4.15
Silver, a/t Aa	141	89.6	106	58.5	38.7
Specific Gravity.o/cm3	3.63	3.32	3.20	3.04	3.08

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Sink/Float Investigation on Selected Drill Holes at S.G. 3.0

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Composite	Product	Weid		Assays,%,g/t					% Distribution				
		a	~~~ \	Ръ I	Zn	As	Aul	Aa	РЫ	Znĺl	As	Aul	Aa
[Sink	340.9	68.5	3.94	5.84	13.0	20.2	79.5	96.1	96.8	97.6	96.9	93.6
2	Float	157.1	31.5	0.35	0.42	0.68	1,39	11.7	3.9	3.2	2.4	3.1	6.4
	Head(Calc)	498.0	100.0	2.81	4.13	9.11	14.3	58.1	100.0	100.0	100.0	100.0	100.0
<u></u>	Sink	27.4	5.5	4.35	5.99	13.4	16.0	142	55.7	60.1	74.2	66.3	59.5
[2A	Float	473.6	94.5	0.20	0.23	0.27	0.47	5.6	44.3	39.9	25.8	33.7	40.5
	Head(Calc)	501.0	100.0	0.43	0.55	0.99	1.32	13.1	100.0	100.0	100.0	100.0	100.0
· · · ·	Sink	169.1	33.8	4.10	4.85	17.8	17.1	113	79.2	83.2	87.5	89.0	75.8
4B	Float	330.6	66.2	0.55	0.50	1.30	1.08	18.5	20.8	16.8	12.5	11.0	24.2
•	Head(Calc)	499.7	100.0	1.75	1.97	6.88	6.50	50.5	100.0	100.0	100.0	100.0	100.0
	Sink	296.1	59.3	3.93	5.78	15.7	28.7	89.9	89.1	88.9	94.3	95.7	88.9
6	Float	203.5	40.7	0.70	1.05	1.39	1.87	16.4	10.9	11.1	5.7	4.3	11.1
[Head(Calc)	499.6	100.0	2.61	3.85	9.87	17.8	60.0	100.0	100.0	100.0	100.0	100.0
	Sink	122.7	24.7	3.59	7.41	12.4	15.2	80.1	80.8	84.9	87.3	86.4	78.7
7	Float	374.9	75.3	0.28	0.43	0.59	0.78	7.10	19.2	15.1	12.7	13.6	21.3
1	Head(Calc)	497.6	100.0	1.10	2.15	3.50	4.34	25.1	100.0	100.0	100.0	100.0	100.0
	Sink	330.0	67.2	8.74	13.5	9.06	15.4	193	97.2	97.9	98.8	98.4	95.5
9	Float	161.2	32.8	0.52	0.59	0.22	0.50	18.8	2.8	2.1	1.2	1.6	4.5
	Head(Calc)	491.2	100.0	6.04	9.26	6.16	10.5	136	100.0	100.0	100.0	100.0	100.0
	Sink	182.0	36.7	5,96	7.66	8.73	13.6	142	87.1	87.9	90.4	93.7	83.1
10	Float	314.0	63.3	0.51	0.61	0.54	0.53	16.7	12.9	12.1	9.6	6.3	16.9
1	Head(Calc)	496.0	100.0	2.51	3.20	3.55	5.33	62.7	100.0	100.0	100.0	100.0	100.0
	Sink	307.9	63.4	1.30	0.99	18.8	2.47	45.0	90.0	91.9	97.2	96,2	82.2
11A	Float	178.0	36.6	0.25	0.15	0.94	0.17	16.8	10.0	8.1	2.8	3.8	17.8
	Head(Calc)	485.9	100.0	0.92	0.68	12.3	1.63	34.7	100.0	100.0	100.0	100.0	100.0
	Sink	173.0	34.6	4.39	12.8	10.6	15.5	113	82.9	84.4	90.6	92.0	79.5
12	Float	_327.0	65.4	0.48	1.25	0.58	0.71	15.4	17.1	15.6	9.4	8.0	20.5
	Head(Calc)	500.0	100.0	1.83	5.25	4.05	5.83	49.2	100.0	100.0	100.0	100.0	100.0
	Sink	142.4	28.7	4.63	13.5	11.1	17.5	123	77.9	80.7	87.3	89.5	80.4
14	Float	353.0	71.3	0.53	1.30	0.65	0.83	12.1	22.1	19.3	12.7	10.5	19.6
	Head(Calc)	495.4	100.0	1.71	4.81	3.65	5.62	44.0	100.0	100.0	100.0	100.0	100.0
	Sink	857.4	43.0	4.71	7.06	11.6	13.0	169	84.9	85.8	86.9	89.9	84.3
16	Float	1136.3	57.0	0.63	0.88	1.32	1.10	23.8	15.1	14.2	_13.1	10.1	15.7
	Head(Calc)	1993.7	100.0	2.38	3.54	_ 5.74	6.22	86.2	100.0	100.0	100.0	100.0	100.0
_	Sink	1188.3	57.6	3.24	6.07	14.1	25.2	91.1	93.0	94.1	97.5	98.8	94.7
17	Float	875.8	42.4	0.33	0.52	0.50	0.40	6.90	7.0	5.9	2.5	1.2	5.3
	Head(Calc)	2064.1	100.0	2.01	3.72	8.33	14.7	55.4	100.0	100.0	100.0	100.0	100.0
	Sink	679.2	33.8	3.67	6.56	9.10	10.1	93.5	83.9	81.7	85.5	84.4	82.4
18	Float	1331.7	66.2	0.36	0.75	0.79	0.95	10.2	16.1	18.3	_ 14.5	15.6	17.6
	Head(Calc)	2010.9	100.0	1.48	2.71	3.60	4.04	38.3	100.0	100.0	100.0	100.0	100.0
	Sink	1168.7	58.5	3.06	3.67	10.3	12.7	87.9	92.5	92.3	95.7	97.3	91.9
19	Float	827.5	41.5	0.35	0.43	0.66	0.49	10.9	7.5	7.7	4.3	2.7	8.1
	Head(Calc)	1996.2	100.0	1.94	2.33	6.30	7.64	56.0	100.0	100.0	100.0	100.0	100.0
	Sink	1517.0	75.5	4.27	7.94	10.7	13.4	143	96.8	97.3	98.0	98.9	96.5
20	Float	492.0	24.5	0.43	0.69	0.66	0,46	16.1	3.2	2.7	2,0	1.1	3.5
	Head(Calc)	2009.0	100.0	3.33	6.16	8.24	10.2	112	100.0	100.0	100.0	100.0	100.0
	Sink	1533.5	78.0	2.38	10.3	5.64	25.5	74.7	96.1	97.3	94.7	98.4	94.7
21	Float	432.5	22.0	0,34	1.01	1.12	1,49	14.8	3.9	2.7	5.3	1.6	5.3
	Head(Calc)	1966.0	100.0	1.93	8.26	4.65	20.2	61.5	100.0	100.0	100.0	100.0	100.0
	Sink	512.0	25.8	3.12	3.85	14.2	9.67	165	85.8	87.6	90.8	90.3	78.4
21A		1469.9	/4.2	0.18	0.19	0.50	0.36	15.8	14.2	12.4	9.2	9.7	400.0
	Head(Calc)	1981.9	100.0	0.94	1.14	4.04	2./7	3			100.0	00.0	- 04 6
	SINK	1533.5	78.0	2.04	b.50	/.13	17.7	60.8	96./	97.9	90.4	98,4	34.0 E A
22	rioat	432.5	22.0	-0.25	0.49	0.95	1.00	12.3	3.3	2.1	3.0	100.0	100.0
	Mead(Calc)	1966.0	100.0	1.65	5.18	5.77	14.0	50.1	100.0	100.0	100.0	01.0	g7 c
	SIRK	817.1	41,1	0.69	10.6	3.50	8,13	112	87.3	84.1	10.0	31.2	47.0 12 6
23		1169.0	58.9	0.68	1.40	0.59	0.50	- 11.2	12.7	10.9	19.4	100.0	100.0
	Head(Calc)	1986.1	100.0	3.15	5.18	1.79	3.67	52.7	100.0	100.0	100.0	100.0	100.0

TABLE	3
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Composite	Product	Weig	int [As	says.%.	g/t			%	Dístribu	tion	
		L a	%	Pb	Zn	As	Au	Ag	РЪ	Zn	As	Au	Aa
	Sink	791.0	85.0	6.64	10.7	7.34	8.27	117	98.2	97.7	98.5	98.8	98.0
23A	Float	140.0	15.0	0.68	1.43	0.63	0.58	13.6	1.8	2.3	1.5	1.2	2.0
	Head(Calc)	931.0	100.0	5.74	9.31	6.33	7.11	101	100.0	100.0	100.0	100.0	100.0
_	Sink	139.2	7.0	0.56	0.99	11.5	1.51	17.7	29.5	51.1	68.3	35.0	100.0
23B	Float	1860.0	93.0	0.10	0.071	0,40	0.21		70.5	48.9	31.7	65.0	0.0
	Head(Calc)	1999.2	100.0	0.13	0.13	1.17	0.30	1.2	100.0	100.0	100.0	100.0	100.0
	Sink	123.4	9.6	0.70	1.24	8.23	5.43	30.3	33.1	61.3	82.1	82.7	43.3
23B2	Float	1164.9	90.4	0.15	0.083	0.19	0.12	4.20	66,9	38.7	17.9	17.3	<u> </u>
	Head(Calc)	1288.3	100.0	0.20	0.19	0.96	0.63	6,70	100.0	100.0	100.0	100.0	100.0
	Sink	1266.2	63.5	1.87	3.82	7.72	11.7	73.5	94.2	94.9	93.7	96.5	91.3
24	Float	728.6	36.5	0.20	0.36	0.90	0.73	12.1	5.8	5.1	6.3	3,5	8.7
	Head(Calc)	1994.8	100.0	1.26	2.56	5.23	7.67	51.1	100.0	100.0	100.0	100.0	100.0
	Sink	1081.1	54.4	1.85	8.27	7.39	19.5	50.5	87.7	90.8	91.8	97.2	87.2
25	Float	907.7	45.6	0.31	1.00	0.79	0.67	8.80	12.3	9.2	8.2	2.8	12.8
	Head(Calc)	1988.8	100.0	1.15	4.95	4.38	10.9	31.5	100.0	100.0	100.0	100.0	100.0
	Sink	1492.4	75.0	7.35	9.40	3.97	12.1	210	97.7	98.2	95.9	98.1	97.0
26	Float	497.7	25.0	0.51	0.52	0.51	0.69	19.4	2.3	1.8	4.1	1.9	3.0
	Head(Calc)	1990.1	100.0	5.64	7.18	3.10	9.25	162	100.0	100.0	100.0	100.0	100.0
	Sink	958.6	48.2	3.32	5.20	8.57	11.3	177	87.8	89.3	92.4	93.0	79.6
27	Float	1029.7	51.8	0.43	0.58	0.66	0.79	42.1	12.2	10.7	7.6	7.0	20.4
	Head(Caic)	1988.3	100.0	1.82	2.81	4.47	5.86	107	100.0	100.0	100.0	100.0	100.0
	Sink	658.3	33.2	6.34	36.7	0,65	1.82	124	81.0	88.2	87.1	90.0	81.5
28	Float	1325.4	66.8	0.74	2.45	0.048	0.10	14.0	19.0	11.8	12.9	10.0	18.5
	Head(Calc)	1983.7	100.0	2.60	_13.8	0.25	0.67	50.5	100.0	100.0	100.0	100.0	100.0
	Sink	151.4	7.6	1.71	5.00	5.77	11.6	24.1	48.5	60.4	69.4	82.8	48.6
28A	Float	1834.6	92.4	0.15	0.27	0.21	0.20	2.10	51.5	39.6	30.6	17.2	51.4
	Head(Calc)	1986.0	100.0	0.27	0.63	0.63	1.07	3.78	100.0	100.0	100.0	100.0	100.0
	Sink	1396.5	70.2	6,32	12.0	5.86	23.5	118	96.2	96.9	95.8	98.8	93.6
28B	Float	592.9	29.8	0,59	0.89	0.61	0.68	_19.0	_ 3.8	3.1	4.2	1.2	_6.4
	Head(Calc)	1989.4	100.0	4.61	8.69	4.30	16.7	88.5	100.0	100.0	100.0	100.0	100.0
	Sink	63.0	3.2	1.44	11.7	2.74	2.15	25.5	28.3	50.3	53.6	54.1	16.6
29A	Float	1918.3	96.8	0.12	0.38	0.078	0.06	4.20	71.7	49.7	46.4	45.9	83.4
	Head(Calc)	1981.3	100.0	0,16	0.74	0.16	0.13	4.88	100.0	100.0	100.0	100.0	100.0
	Sink	1374.9	68.9	5.94	19.6	1.13	4.67	107	92.6	92.4	90.9	95.9	91.0
298	Float	619.8	<u>31.1</u>	1.06	3.57	0.25	0.44	23.5	7.4	7.6	9.1	4.1	<u>9.0</u>
	Head(Calc)	1994.7	100.0	4.42	14,6	0.86	3,36	81.1	100.0	100.0	100.0	100.0	100.0

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TABLE 4

Flotation of Selected Drill Holes

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Test	Composite	Product	Weight Assays %. g/t					% Distribution					
No			e 1	Ph	70	1 Ac 1	Γ. Δι.	ا مه ا	Dh Í	ا ۳۰۰ ا	Ac		-
	ŧ	Ph and Cl Coord	6.2	20 1	19.1	2 75	20.0	969	64 1	14.8	27	465	<u> </u>
	•	Ph 2nd Cl Cond	7 4	26.1	10.1	2.70	23.3	700	67.7	17.0	2.1	10.5	00.1
		7e 2rd Ct Cone	40.7	30.3	50.0	3,24	29.4	193	07.7	71.0	3.0	10.4	63.2
1		Zi Sid Ci Colic	10.7	4.32	30.0	2,40	9.27	120	12.2	1.3	4. 1	8.8	15.1
F4	! '	Zn 2nd Ci Cond	12.0	4.76	47.7	3.17	10.2	136	15.0	74.8	5.9	10.8	18.2
(E	ASPY Ho Conc	23.7	2.30	2.11	20.7	29.1	56.1	14.3	0.0	76.3	60.9	14.9
1	1	ASPY HO Tall	57.2	0.20	0.11	1.61	1.95	5.70	3.0	0.8	14.3	9.8	3.7
	[Head(Calc)	100.0	3.81	7.64	6.44	11.3	89.1	100.0	100.0	100.0	100.0	100.0
1		Pb 3rd Cl Cond	4.1	38.3	6.19	10.5	43.5	634	65,5	6.3	4.8	14.8	45.5
	i	Pb 2nd Cl Cond	4.8	33.7	6.55	11.8	42.1	562	68.5	8.0	6.4	17.0	47.9
Į	· ·	Zn 3rd Cl Conc	8.6	2.82	39,6	7.40	12.6	99.4	10.1	85.2	7.1	9.0	15.0
F5	2	Zn 2nd Cl Conc	10.3	2.98	33.5	9.57	15,6	98.1	12.9	87.0	11.1	13.4	17.9
		AsPy Ro Conc	32.8	1.01	0.49	20.1	22.9	48.7	13.9	4.0	73.8	62.7	28.2
i		AsPy Ro Tail	52.1	0.21	0.08	1.50	1.59	6.50	4.6	1.0	8.7	6.9	6.0
		Head(Calc)	100.0	2.38	3.97	8.93	12.0	56.6	100.0	100.0	100.0	100.0	100.0
		Pb 3rd Cl Cono	2.3	9.63	1.37	1.81	4,15	181	59,6	5,9	4.5	8.3	39.5
1		Pb 2nd Cl Cond	3.4	6.92	1.20	1,59	3.18	132	63.4	7.6	5.9	9.4	42.7
ł		Zn 3rd Cl Conc	3.3	2.08	13.8	19.2	23.5	82.4	18.9	86.7	70.3	68.7	26.4
F13	2A	Zn 2nd Cl Conc	3.5	2.08	13.0	18.6	22.7	79.1	20.1	87.2	72.4	70.6	27.0
1		AsPy Ro Conc	15.7	0.31	0.12	1.16	1.30	6.70	13.3	3.6	20. t	18.0	10.2
1	4 (AsPy Ro Tail	77.3	0.015	0.011	0.020	0.030	2 70	3 2	1 6	1 7	2 0	20 1
		Head(Calc)	100.0	0.37	0.53	0 91	1.14	10 4	100.0	100.0	100.0	100.0	100.0
		Pb 3rd Cl Cond	4.7	38.7	5.27	12.1	55 1	808	74 1	5 1	4 0	14 5	64 8
	1	Pb 2nd Cl Cond	5.9	32.9	5.69	†⊿ ∩	51 5	708	78.2	6.8	7 1	16.9	70 6
}		Zn 3rd Cl Conc	9.2	1 64	46.6	5 80	11 0	67 4	6 1	87 ti	4 E	5.6	10.0
E12		Zn 2nd Cl Cond	10.5	1 73	A1 6	9,00	12.0	60.1	7 3	99.1	7 2	0.0	10.0
1	1 1	AsPy Bo Conc	A1 7	0.71	0.50	22.5	31.0	18.9	120	A 2	20.6	71 7	14.3
1 .	ł (AsPy Bo Tail	41 0	0.15	0.00	+ 20	1 50	E 50	2.5	- 0.0	500.0		13.3
	1	Head(Calc)	100.0	2 40	4.06	1.35	100	5.30	100.0	100.0	+00.0	3.5	3.9
		Pb 3rd Ct Cond	10.0	44.6	10.6	4 27	10.0	39.2	90.0	100.0	100.0	100.0	100.0
4		Ph 2nd Cl Cond	10.5	27 4	10.5	4,37	32.0	0.00	00.2	10.3	3.4	17.4	71.1
1		Zo 2rd Cl Cono	44.0	37.4	90.0	5.30	34.1	922	04.0	19.1	0.0	23.3	/5.4
-			14.2	2.00	39.0	5.28	13.6	121	5.9	/1.4	5.7	10.2	10.9
	4	AnD: Do Coone	10.0	2.78	35./	6,30	13.4	118	1.1	/3.5	7.6	11.3	11.9
		AsPy Ho Conc	44.5	0.79	1.15	22.0	24.0	35.9	6.1	6.6	74.1	56.4	10.1
		ASPY NO Tall	26.4	0.33	0.25	6.46	6.44	15.5	1,5	0.9	12,9	9.0	2.6
		Head(Ualc)	100.0	5.74	7.77	13.3	19.0	159	100.0	100.0	100.0	100.0	100.0
		Po 3rd Cl Cond	8.5	44,6	8.65	3.70	30.7	1139	68.7	9.6	2.4	12.9	64.8
1		Po 2no Ci Cono	12.4	35.1	10.4	5.61	37,1	892	79,1	16.9	5,4	22.8	74.3
1 18	4	Zh 3rd Cl Conc	11.0	3.38	41.3	4.32	13.4	115	6.7	59.3	3.7	7.3	8.5
1		Zn Ho Conc	28.4	2.83	20.7	10.4	18.0	95.4	14.6	76.8	22.7	25.4	18.2
		Zn Ro Tail	59,1	0.59	0.81	15.8	17.7	19.2	6.3	6.3	71.9	51.8	7.6
<u></u>	Į	Head(calc)	100.0	_5.52	7.65	13.0	20.2	149	100,0	100.0	100.0	100.0	100.0
		Pb 3rd Cl Cond	6.9	36.7	11.3	8,30	22.0	758	57.2	9.8	4.6	7.7	47.8
		Pb 2nd Cl Cond	10.2	29.8	12.5	9.58	23.4	633	69.3	16.1	7.9	12.2	58.8
		Zri 3rd Cl Conc	18.3	4.53	33.1	7.77	16.7	147	18.9	76.5	11.6	15.6	24.4
F17	5	Zn 2nd Cl Conc	20.3	4.43	30.5	8.82	18.1	144	20.4	77.8	14.5	18.7	26.4
1	[AsPy Ro Conc	39.0	0.90	0.99	22.2	31.7	[30.9	8.0	4.9	70.2	62.9	10.9
1	1	AsPy Ro Tail	<u>30.</u> 6	0.33	0,31	2,98	4.01	13.9	2.3	1.2	7.4	6.3	3.9
		Head(Calc)	100.0	4.40	7.93	12.3	19.6	110	100.0	100.0	100.0	100.0	100.0
		Pb 3rd Cl Conc	3.7	40.9	5.96	12.1	47.7	882	68.4	5.8	4.7	11.7	46.7
		Pb 2nd Cl Cond	5.3	31.7	6.66	15.2	52.5	701	75.8	9.3	8.5	18.4	53.2
		Zri 3rd Cl Conc	8.4	2.26	38,2	9,12	20.2	133	8.7	85.t	8.1	11.3	16.2
F8	6	Zn 2nd Cl Conc	10.6	2.14	30.6	12.1	17.0	121	10.3	86.1	13.6	12.0	18.5
	1	AsPy Ro Conc	32.2	0.72	0.39	21.1	30.3	43.7	10.5	3.3	71.4	64.7	20.2
1		AsPy Ro Tail	51.9	0.14	0.10	1 20	1 41	10 B	3.3	14	6.6	4.0	8.1
		Head(Calc)	100 0	2 20	3 70	9 50	15.0	69.6	100.0	100.0	100.0	100 0	100.0
	1	Pb 3rd Cl Conc	3.9	44 2	6 20	11 5	35 1	878	75 6	6 7	4 7	8 2	58.3
		Ph 2nd Cl Conc	5.1	35.0	6.24	14.1	A1 6	724	70.0	0.1 0.5	7 5	1 1 2 7	61 7
Eno		7n 3rd Cl Care	7 2	1 20	10.01	6 0e	17 0	100	13.3 E 1	5.5 1 1 1	1.5	7 4	12 2
1 100			26 0	1.03	92.4		22.0	40.0	3.2	04.4	4.0	70.0	10.0
]		50.0	0.90	0.90	19.3	33.0	49.0	10.2	00.9	72.0	12.0	20.1
	1	Zn Moltali	58.9	0,19	0.097	3.25	4.10	6.20	4.9	1.6	20.0	14.5	0.2
	i '	mead(caic)	100.0	2.28	3.63	9.60	16.6	58.7	0.001	0.001 נ	100.0	100.0	

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Test	Composite	Product	Weight	_	As	says,%.	g/t			%	Distribut	tion ,	
No.			%	РЬ	Zn	As	Au	<u>A</u>	Pb	Zn	As	Au	<u>Ag</u>
į		Pb 3rd Cl Cond	1.8	35.1	8.73	6.49	25.9	686	71.3	8.0	3,5	13.0	53.4
		Pb 2nd Cl Cond	2.9	24.6	9.18	8,62	26.8	505	80.5	13.6	7.5	21.6	63.
		Zn 3rd Cl Conc	7.1	1.26	22.4	15.8	18.5	61.1	10.2	82.0	33,9	36.9	19.1
F9	7	Zn 2nd Cl Cond	8.5	1.17	18.9	17.5	15.6	58.7	11.4	82.8	44.9	37.4	22.
		AsPy Ro Conc	16,1	0.32	0.31	9.35	8.67	15.3	5.9	2.6	45.4	39.2	10.
		AsPy Ro Tail	72.5	0.028	0.027	0.10	0.09	1.10	2.3	1.0	2.2	1.8	3.
		Head(Calc)	100.0	0.88	1.94	3.32	3.57	22.8	100.0	100.0	100.0	100.0	100.
		Pb 3rd Cl Cong	1.4	36.6	9,10	6.14	17.90	593	57.8	6.7	2.6	6.7	40.
		Pb 2nd Cl Cond	2.4	26.2	9.75	7.87	20.1	462	69.6	12.1	5.6	12.8	52
•		Zn 3rd Cl Conc	4.7	2.76	34.3	8.28	16.6	111	14.3	83.2	11.5	20.5	24
F98	7	Zn Bo Conc	22.3	0.90	7 54	13.0	13.2	33.7	22 1	86.8	86.3	77.5	35
	·	Zn Ro Tail	75.3	0.10	0.027	0.36	0 49	3 20	8.3	1 1	9 1	9.7	41
		Head(calc)	100.0	0 90	1 0 2	2 76	3 70	21.0	100.0	100.0	100.0	100 0	100
		Ph 3rd Cl Cond	7.6	310	11 6	3,30	12 1	752	74 1	12 6	5 2	16.0	100,
		Pb 2nd Cl Cond	10.6	26.2	12.4	1.02	4.4.4	507	82.0	20.2	9.2 0.4	13.3	00. 72
		70 2nd Cl Cond	10.0	20.0	12.4	4,03	14.1	00 f	62.0	20.3	9.1	23.0	/3.
			10.3	2.00	44.1	3.14	0.50	88.5	0.0	70.2	२. ८	13.5	10.
F2	8			2.18	39.9	3.70	8.83	89.3	<u> </u>	/2.4	1.7	15.9	12,
		ASHY HO CONC	27.3	0.92	1.52	12.7	11.4	31.8	7.7	6,4	61.5	47.7	10.
		ASPY HO Tall	50.4	0.16	0.11	2.42	1.73	7.00	2.5	0.9	21.7	13.4	4.
		Head(Calc)	100.0	3.27	6.48	5.63	6.51	86.0	100.0	100.0	100.0	100.0	100.
		Pb 3rd Cl Conq	4.0	38.6	10.4	2.88	16.7	870	49.5	6.6	2.1	9.5	44.
		Pb 2nd Cl Cond	6,1	31.8	11.6	3.82	16.6	711	61.8	11.1	4.2	14.3	55.
F28	8	Zn 3rd Cl Cond	11.2	4.66	42.7	2.86	10.7	157	16.5	74.9	5.8	16.8	22.
		Zn Ro Conc	26.3	3.59	20.6	7.15	12.1	108	30.0	85.1	34.1	44.7	36.
		Zn Ro Tail	67.5	0.38	0.35	5.05	4.31	9.30	8.1	3.7	61.7	41.0	8.
_		Head(calc)	100.0	3.15	6.36	5.53	7.10	78.3	100.0	100,0	100.0	100.0	100.
		Pb 3rd Cl Cond	8.3	50.2	14.1	2.62	16.7	980	74.3	13.2	3.6	15.0	63.2
		Pb 2nd Cl Cond	10.9	42.9	16.6	3.56	16.9	849	83.4	20.4	6.5	19.9	72.0
		Zn 3rd Cl Cond	14.1	3.81	45.9	3.34	10.7	157	9,6	73.2	7.9	16.3	17.2
F11-1	9	Zn 2nd Cl Conc	15.6	3.92	42.5	4.34	11.5	157	10.9	75.0	11.3	19.4	19.0
		AsPy Ro Conc	29.9	0.91	1.18	15.6	18.0	31.8	4.8	4.0	77.9	58.0	7.4
		AsPy Ro Tail	43.6	0,10	0.11	0.59	0.58	4.70	0.8	0.5	4.3	2.7	1.6
	ł	Head(Calc)	100.0	5.60	8.85	5.98	9.26	129	100.0	100.0	100.0	100.0	100.
		Pb 3rd CI Cond	8.2	48.7	14.4	3.15	9.27	970	71.6	13 3	4.3	8.6	61
	ł	Pb 2nd Cl Cond	12.8	38.0	17.6	4 88	14 1	792	87 1	25 4	10.3	20.3	78
E118	•	7n 3rd Cl Conc	13.2	3 34	47.0	3 65	121	140	7 9	70.2	9.0	19.0	15
11,5		Za Ba Corr	27 5	2 1 6	22.0	0.00	15 8	90.1	10.6	70.2	44.2	40.0	10.
		Za Po Tail	E0.7	6.10	23.1	3.73	19.0		0.0	13,4	44.3	40.7	19.
			100.0	5 5 9	9.17	4,30	4.00	120	2.2	100.0	40.0	30.9	2.
		Distant Ci Cond	100.0	3,50	0.00	6.04	0.00	700	100.0	100.0	100.0	100.0	100.
		Po are Ci Cono	0.0	34.2	10.4	5.32	19.0	700	90.2	32.2	10.1	32.0	81.
		Po 2nd Ci Cano	7.0	32.4	15.2	5.60	18.5	/31	90,9	33.9	1.2	33.1	82.
		Zh 3rd Ci Cond	4.2	1.84	45./	4.55	5.00	108	3.1	61.7	5.6	5.4	7.
F10	10	Zn 2nd Cl Cond	4.4	1.81	43.9	5.23	4.79	104	3.2	61.8	1.1	5.4	7.
		AsPy Ro Conc	24.8	0.36	0.31	11.2	9.11	18.4	3.6	2,4	79.9	57.7	7.
		AsPy Ro Tail	63.8	0.089	_0.09	0.12	0.23	3.00	2.3	1.9	2.2	3.8	3.
		Head(Calc)	100.0	2.49	3.14	3.47	3.91	62.1	100.0	100.0	100.0	100.0	100.
		Pb 3rd Cl Cond	4.1	43.1	15.2	3,13	11.8	918	78.2	21.3	3.8	12.3	70.
1	ł	Pb 2nd CI Cond	5.2	36.6	15.8	4.15	12.8	790	84.3	28,2	6.3	16.9	76.
F10B	10	Zn 3rd Cl Conc	4.1	3.66	48.3	1.67	10.6	157	6.7	69.1	2.0	11.1	12.
1	ł	Zn Ro Conc	17.7	1.42	11.7	11.0	13.0	56.0	11.2	71.0	57.1	58.7	18.
	}	Zn Ro Tail	77.1	0.13	0.03	1.61	1.24	3.40	4.5	0.8	36.5	24.4	4.
	(Head(calc)	100.0	2.25	2.91	3,40	3.92	53.5	100.0	100.0	100.0	100.0	100
		Pb 3rd Cl Cond	7.5	53.9	11.6	1_36	20.8	1192	75.1	8.6	2.6	25.6	68.
1	1	Pb 2nd Cl Cond	9.9	45.6	14.8	2.19	19.7	1030	83.4	14.5	5.6	31.8	77.
	Į	Zn 3rd Cl Conc	13.6	2.53	53.1	0 72	2.07	78.4	6.4	71 6	2.5	4.6	8
53	1 11	7n 2nd Cl Conc	15 2	2 84	50.6	1 10	2 44	89.4	8 0	76.4	4 3	6 1	10
		Aspy Bo Com	30 F	1 24	20.0	10.5	11 2	46.2	7 6	4.0, 4	82.6	56.5	10
	ł	AcPu Ha Tail	44 3	0 1 2	0.10	33.0	0 77	3 60	1.0	0.0	7 5	5 6	1
1		Hond/Cate	100.0	5 40	10.10	2 9 9	6 11	121	100.0	100.0	100.0	100.0	100
		I DRAUNADC)	E IVV.U	r 3.40	U. U	i J.06	i 0.ill			100.0			190.

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Test	Composite	Product	Weight		Ac	savs %			<u> </u>	<u>%</u>	Distribu	tion	
No	Composito		₩.	Ph	77	Δc	An I	an l	25	7 [°]			60
<u> </u>	<u>{</u>	Ph 3rd Cl Cond	3.3	517	7 85	3 10	31 4	1226	81 3	3.6	1 5	126	72 1
i		Pb 2nd Cl Cond	37	47 7	8 73	3 95	30.6	1128	82.8	A A	21	+2.0	72.2
1	ſ	Zn 3rd Ci Conc	12.3	1 50	55.2	1 61	5 00	61 4	87	02 2	2.1	7 3	10.0
56	12	Zn 2nd Cl Conc	12.8	1.52	53.2	2 44	5 79	63 7	9 t	92.5	A 4	8.0	14.4
1		AsPy Bo Conc	36.0	0.44	0.53	17 9	17.6	16.8	74	2.6	01 2	75 7	10.6
		AsPy Ro Tail	476	0.03	0.08	0 34	0.34	2 00	0.7	0.5	2.3	1 0	1 1 7
	i i	Head(Calc)	100.0	2.12	7.34	7.06	8.36	56.7	100.0	100.0	100.0	100 0	100.0
·	1	Pb 3rd Cl Cond	4.8	44.4	10.7	5.58	26.9	1021	91.0	7 2	3.9	15.0	74 0
4.		Pb 2nd Cl Cond	5.1	41.8	10.9	6.07	26.3	967	91 3	7.9	4.5	15.7	75.7
F6B	12	Zn 3rd Cl Conc	11.1	0.52	56.4	0.95	1.65	36.0	2 5	88 7	1.5	2 1	6 1
		Zn Ro Conc	22.6	0.57	51.6	2.70	14.6	82.0	3.0	89.4	4.8	38.3	19.7
1	1	Zn Ro Tail	72.3	0.12	0.09	5.72	5.50	5 10	37	0.9	59.6	46 1	5.6
1		Head(calc)	100.0	2.34	7 08	6 94	8 62	65.4	100.0	100.0	100.0	100.0	100.0
		Pb 3rd Cl Cond	2.3	37.0	4.05	17.9	31.3	873	67 1	10.5	4 2	5.3	58 7
	I	Pb 2nd Ct Cond	3.2	28.8	4.24	20.0	34.2	686	72 9	15.4	6.6	9.1	64.5
		Zn 3rd Ci Conc	13.1	1.59	5.60	34.2	50.5	59 1	16.2	82.0	45.5	48 1	22 4
F14	13	Zn 2nd Cl Conc	13.9	1.53	5.28	34.2	49_1	57.7	16.6	82 ∡	48 4	49.0	23.9
		AsPy Ro Conc	22.8	0.27	0.047	18.6	23.2	11.4	4 8	1 2	43.2	38.6	7.5
1		AsPy Ro Tail	60.0	0.12	0.015	0.30	0.78	2.70	5.6	1.0	1.8	3.4	47
		Head(Calc)	100.0	1.28	0.89	9.83	13.7	34.5	100.0	100.0	100.0	100.0	100 0
	1	Pb 3rd Cl Cond	4.2	25.5	4.55	22.1	37.0	611	82.5	22.2	9.2	11.3	75.7
		Pb 2nd Cl Cond	6.0	18.8	4.41	23.0	36.8	459	87.2	30.9	13.6	15.9	80.8
]	Zn 3rd Cl Conc	1.8	2.32	28.2	16.6	29.0	113	3.2	58.6	2.9	3.7	5.8
F20	13	Zn 2nd Cl Conc	3.2	1.80	16.9	24.1	36.6	82.4	4.4	62.1	7.5	8.2	7.5
	1	AsPy Ro Conc	33.0	0.21	0.14	23.8	32.2	8,60	5.3	5.4	77.2	74.7	8.1
	t I	AsPy Ro Tail	57.8	0.070	0.025	0.29	0.29	2.20	3.1	1.7	1.6	1.2	3.6
	8	Head(Calc)	100.0	1.30	0.86	10.2	14.2	35.0	100.0	100.0	100.0	100.0	100.0
		Pb 3rd Cl Conq	2.7	43.6	13.6	4.37	20.4	1085	82,3	7.9	3.2	10.6	70.3
		Pb 2nd Cl Cond	3.3	37.4	15.0	5.74	22.0	946	86.3	10.7	5.1	13.9	74.9
	[Zn 3rd Cl Conc	7.4	1.03	53.9	1.22	4.48	79.8	5.3	85.7	. 2.4	6.4	14.2
F7	14	Zn 2nd Cl Canc	8.0	1.09	50.2	2.48	6.25	78.9	6.1	86.4	5.4	9.6	15.2
	}	AsPy Ro Conc	22.7	0.41	0.50	14.4	17.2	14.3	6.5	2.4	87.6	74.6	7.7
	1	AsPy Ro Tail	66.0	0.024	0.036	0.11	0.15	1,40	1.1	0.5	1.9	1.9	2.2
ļ	1	Head(Calc)	100.0	1.44	4.68	3.73	5.23	41.9	100.0	100.0	100.0	100.0	100.0
1	{	Pb 3rd Cl Cond	2.9	45.3	14.2	4.35	15.8	1017	80.5	8.6	3.3	9.2	71.5
		Pb 2nd Cl Cond	3.8	37.3	15.6	5.78	18.2	861	85.6	12.2	5.7	13.6	78.1
F78	1 14	Zn 3rd Cl Conc	7.9	1,39	52.8	1.39	5.07	73.2	6.6	85.8	2.9	7.9	13.8
	1	Zn Ho Conc	23.7	0.74	17.8	10.0	12.7	32.4	10.6	87.3	62.4	59.2	18.4
	{ 1		72.5	0.086	0.033	1.68	1,90	2.00	3.8	0.5	31.8	27.1	3.5
<u> </u>		Head(calc)	100.0	1.65	4.85	3.82	5.07	41.8	100.0	100.0	100,0	100.0	100.0
	i -	PD 3rd Cl Cond	3.8	31.9	14,0	7.14	14.7	796	71.2	19.0	4.5	7.0	58.2
1	ļ	Po 2nd Ci Cond	4.7	27.8	14,1	7.73	15.2	702	76.9	23.8	6.0	9.0	63.6
Erc		Zn ard Ci Cond	5.9	3.79	34.2	6.23	12.7	180	13.2	/2.1	6.1	9.4	20.5
617	1.2	AnD I Do Conc	0.4	3,64	31.8	7.21	13.6		13.7	/2.5	7.6	10.9	21.2
		Astry no Conc	33.5	0.42	0.25	15.2	18.8	19.3	8.2	3.0	83.6	77.9	12.4
		Head(Cale)	100.0	1 74	0.037	0.30	0.33	2.70	1.2	0.7	2.7	2.3	2.9
		Ph ard CL Cond	100.0	94 7	4.02	6.10	12 0	045	100.0	100.0	100.0		100.0
		Pb 2nd Cl Cone	3.9 E A	31./	14.0	9.90	12.2	615	77 0	18.1	4.2	1.2	20.2
FIER	31	Zn 3rd Cl Conc	5.9	4 0.4 4 0.4	14.0 36.4	0.10 5.10	19.7	192	17.2	61.4 50 0	1.5	11.1 e A	67.8 19.4
1,00		Zn Bo Corr	26.2	1 34	8 26	47.13	22.0	64 7	14.1	71 4	70 5	0.0	10.1 9£4
		Zn Bn Tail	87 0	0.12	0.20	2 10	2 40	5 10	10.0	1 0	20.0	10 0	20.1
		Head(catc)	100.0	1 90	3 02	6 46	8 3 2	57 0	100.0	100.0	100.0	100 0	100.0
L	1		100.0		0.00		0.00		100.0	100.0	1.00.0		100.0

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6	No	Composite	FIGULEL	weidtirt	96	70	says, 7e,	արու Դերել 1	مما	9h	70			1
	- 140.	}	Ph and Cl Cond	2 9	43.0	120	2 4 2	- 22 2	1240	72 5	126	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	10.0	- 49
	[í	Pb 2nd Cl Cond	5.0	36 1	12.0	4.52	23.5	1100	91.0	20 4	4.2	22 6	76.9
	}	1	Zo 3rd Cl Cood	5 4	2 72		2.61	8 14	152	6.3	71 0	25	6.2	10.4
	E15	16	7n 2nd Cl Conc	5.9	2.72	A1 6	3 30	8 9 2	151	7 1	72.9	2.5	11 1	14.6
		1	As Py Bo Com	34.0	0.56	0.60	14 6	9.52	24.5	8.5	6.2	01 2		44.2
	· ·		AcPy Co Tail	53.0	0.50	0.00	0 1 2	0.00	27.5	0.0	0.2	1 1 2	04.0	11.2
	ł	1	Head(Calc)	100 0	2 2 1	3 36	5 60	4 6 8	76 7	100.0	100.0	100.0	100.0	
	╞━・──	[Ph 2rd Cl Cana	100.0	42.01	11 7	2 90	4.00	10.3	76 9	100.0	100.0		100.0
		1	Pb 2nd Cl Coord		93.2	10.7	5,00	23.0	1331	70.0	21.0	E./	10.3	99.1
	E160		70 2rd Cl Cond	3.0	39.1	14.7	2.30	24.1	1007	04.J	21.1	5.3	26.4	(1.1
	FIDD		Zh Siù Ci Conc	4.9	2.32	40.2	4.39	0.20	12/	5.1	00.U	2.1	0.0	8.1
	i i		Za Do Tail	80.0	1.79	21.0	0.03	1.04	00.2	9.0	/4./		17.3	13.3
	Į			100.0	0.10	0.1/	0.01	3,40	0.90	0.0	4.4	80.7	100.0	9.0
	<u> </u>		Read(calc)	100.0	2.23	3.34	2.00	5.09	76.9	100.0	100.0	100.0	100.0	100.0
	}		Po Sid Ci Cono	4.3	41.0	11./	5,95	27.0	940	80.3	11.2	4.0	17.1	73.9
]	Po 2nd Cl Cond	6.3	30,7	11.9	8.05	28.2	705	80.8	10.0	9.2	25.6	80.6
			Zh 3rd Ci Conc	0./	1.41	51.3	1.70	8.19	64.1	4.3	/6.4	2.1	7.9	7.8
	1-18	17	Zn 2nd Ci Conc	7.0	1,47	49,8	2.01	8.29	54.9	4./	//.5	2.5	8.4	8.3
			ASPY HO CONC	33.2	0.47	0.67	14.4	13.5	15.2	7.1	5.0	86.6	65.1	9.2
			ASPY NO TAM	53.5	0.06	0.076	0.17	0.12	1.90	1,5	0.9	1.6	0.9	1,9
		· · -	Head(Calc)	100.0	2.22	4.50	5.51	6.91	54.8	100.0	100.0	100.0	100.0	100.0
			PD 2nd Ci Cond	3.0	33.1	11.4	5.2/	21.9	828	78.9	15.1	4.8	20.3	73.2
		i i	Po 1st Ci Coner	3.7	27.8	11.3	2.99	20.2	690	82.2	18.0	6.7	23.3	75.9
	-		Zh ard Ci Conc	3.3	2.03	52.1	1.12	4.40	84.3	5.4	/4.4	1.1	4.5	8.3
	113	15	Zri Zna Ci Cono	3.4	2.06	51.0	1.09	4.31	82.0	5 .6	75.0	1.1	4,5	8.3
			ASPY HO CONC	25.8	0.46	0.52	11.4	8.57	16.2	9.5	5.8	89.7	59.2	12.5
			ASPY HO 1211	5/.1	0.049	0.041	0.12	0,14	1.70	2.6	1.2	2.5	2.9	3.4
			Head(Calc)	100.0	1.25	2.31	3.28	3.20	33.6	100.0	100.0	100.0	100.0	100.0
		N	Pb 3rd Cl Cond	3,8	46.2	11.2	2.55	15.5	1080	62.9	7.5	1.2	6,7	43.7
			Po 2nd Ci Cond	5.8	36.7	13.2	5.26	21.7	959	75.2	13.3	3.7	14.2	58.5
			Zn 3rd Cl Cond	10.8	3.44	42.5	3.52	15.3	232	13.1	80.0	4.8	18.7	26.4
6	F21	20	Zh 2ha Ci Cond	11.8	3.48	39.5	4.75	15.6	227	14.6	81.6	5.9	20.9	28.3
` .			ASPY Ho Conc	39.9	0.56	0.63	17.2	13.7	25.0	7.9	4.4	84.3	61.6	10.5
1			AsPy Ro Tail	42.4	0.15	0.092	0.97	0.69	6.00	2.3	0.7	5.1	3.3	2.7
			Head (Calc)	100.0	2.82	5.73	8.15	8.86	94.9	100.0	100.0	100.0	100.0	100.0
			Po 3rd Ci Conq	1.5	47.4	6.85	7.39	32.8	813	46.7	1.3	1.3	3.1	22.8
			Po 2no Ci Conq	2.5	37.0	8.07	9.80	48.9	750	61,6	2.5	2.9	7,9	35.6
			Zn 3rd Ci Conq	12.5	1.65	56.9	0.74	12.3	168	13.4	88.3	1.1	9.7	39.0
ļ	F22	21	Zn 2nd Ci Cond	13.3	1.85	55.1	1.17	12.8	172	16	91.0	1.8	10.6	42.5
			ASPY Ho Conc	47.4	0.58	0.96	16.1	25.3	20.7	17.8	5.6	87.6	75.2	18.2
1			AsPy Ro (all	36.7	0.19	0.18	1.84	2.75	5,60	4.5	0.8	7.8	6.3	3.8
-			Head(Calc)	100.0	1.54	8.07	8.71	15.0	54.0	100.0	100.0	100.0	100.0	100.0
i			Pb 3rd Ci Cond	0.6	37.2	8.90	8.90	32.7	871	35.2	2.2	1.1	3.2	24.8
			Po 2nd Ci Cond	1.5	23.8	9.46	11.6	33.0	614	57.6	6.1	3.6	8.3	44.9
			Zri 3ra Ci Conq	3.9	2.29	52.0	2.44	12.0	152	14.5	87.8	2.0	7.9	29.1
	F23	22	Zn 2nd Ci Conc	4.4	2,54	45.9	3,86	14.3	151	18.3	90.1	3.5	10.7	52.9
			ASPY HO CONC	27.8	0,35	0.16	10.7	10.5	12.7	15.8	1.9	90.2	79.0	A 9
			ASPY RO Tall	100.0	0.076	0.066	0.20	5.00	1.3	8.2	1.9	2.7	1.9	100.0
			Readicalc)	100.0	0.02	2.31	4.00	3.92	20	100.0	100.0	100.0		
			Pb 3rd Ci Cond	2. I A E	60.0	7 67	5.30	12 5	1100	62.4	2.0	4 5	4 7	19.5
			70 2nd Cl Cond	10.1	20.0	50.0	1.00	6 60	1190	17 4	2.0	1.5	2.4	42.0
			Zh 3rd Ci Cond	13.1	3.00	20.9	1.90	7.00	218	17.4	11.1	4.1	3.4	33,1
	F24	23	Zri Zha Ci Cona	21.9	4.21	40.1	3.17	7.98	220	22.1	84.0	3.0	4.0	10.2
· 1			ASPY HO CONC	20.0	1.04	2.87	28.5	20.0	41.0	13.8	12.7	07.4	07.0	10.1
			ASPY HO Tall	18.00	0.32	0.35	7.32	13.0	6.80	1.4	0.5	7.3	0.0	100.0
			Head(Galc)	100.0	4.18	12.5	18.1	36.2	126	100.0	100.0	100.0	100.0	100.0
			Po 3rd Cl Cond	3.3	63.4	6.01	2.73	8.60	930	70.6	3.9	2.7	8.3	
			PD 2nd Ci Cond	5.1	49.8	0.40	4.62	10.5	/49	85.6	8.5	<u>, , 1</u>	15.6	
	Ì		Zn ara Cl Cond	8.1	1.84	54.5	0.99	2.50	66.5	5.0	87.5	2.4	6.1	
	F25	23A	21 2nd CI Conc	8.6	2.13	52.3	1.45	3.06	67.4	0.2	88.7	3.8	/.6	
{			ASPY HO CONC	22.3	0.75	0.51	12.6	11.3	12.2	5.6	2.2	85.0	73.1	
	Į		ASPY Ro Tail	63.9	0.12	0.043	0.21	0.20		2.6	0.5	4,1	3.7	100.0
. 1		• •	Head(Caic)	100.0	2.98	5.08	3.31	3.45		100.0	100.0	100.0	Ι ΤΟΟ.Ο	100.0

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_ [Test	Composite	Product	Weight	· · · · ·	Å	save.%.	a/t			*	Distribu	tion	
(No.			*	РЪ	Zn	As .	Au	A 0	Pb	Zn	A	Au	
1			Pb 3rd CI Cond	3.3	63.4	6.01	2.73	8.60	930	70.6	3.9	2.7	8.3	64.4
			Pb 2nd Cl Cond	5.1	49.8	8.40	4.62	10.5	749	85.6	8.5	7.1	15.6	79.9
			Zn 3rd Cl Cono	6.1	1.84	54.5	0,99	2.60	68.5	5.0	87.5	2.4	6.1	11.3
1	F26	23A	Zn 2nd Cl Cond	8,6	2.13	52.3	1.45	3.06	67.4	6.2	88.7	3.8	7.6	12.1
1	_		AsPy Ro Conc	22.3	0.75	0.51	12.6	11.3	12.2	5.8	2.2	85.0	73.1	5.7
			AsPy Ro Tall	_63.9	0.12	0.043	0.21	0.20	1.70	2.6	0.5	4,1	3.7	2.3
			Hoad(Calc)	100.0	2.98	5.08	3,31	3.45	48.0	100.0	100.0	100.0	100.0	100.0
Ī			Pb 3rd Cl Cond	1.7	35.1	4,71	11.1	30.6	338	55.0	3.3	1.9	9.0	17.2
- 1			Pb 2nd Cl Cond	3.2	22.8	4.95	13.9	26.2	372	66.1	8.5	4.4	14.4	35.3
			Zn 3rd Cl Cond	8.3	1.69	21.4	8.67	19.1	138	12.8	73.6	7.2	27.3	33.5
	F26	24	Zn 2nd Cl Cond	11.7	1.47	16.1	12.4	17.3	108	15.8	78.5	14.6	35.1	37.9
Ì			AsPy Ro Conc	35.4	0.43	0.87	21.6	7,70	16.4	14.0	12.8	76.8	47.3	17.3
			AsPy Ro Tak	49.7	0.090	0.10	0.63	0,37	6.40	4.1	2.1	4.1	3.2	<u>9.6</u>
ļ			Hoad(Calc)	100.0	1.09	2.40	9,96	5.77	33.5	100.0	100.0	100.0	100.0	100.0
Í		1	PB 3rd Ci Cond	1.4	43.6	11.5	3,20	10.0	055	59.9	12.4	4.0	9.4	35.9
			PD 2nd CI Cond	10.1	30.0	12.5	4,34	12.1	633	69.4	18.5	7.4	15.5	47.7
		20	Zh 3rd Ci Conc	13.0	0.73	33,7	3,43	12.9	325	13.9	54.0	7.5	21.3	31.5
	· 2/	20	As Dr. Do Conc	24.0	3.70	1 04	4,50	12.2	290	17.0	70.9	12.0	29.7	36.5
1			AsPy Ro Cold	- 34.2 70 t	0.20	5.00	0.64	0 4 2	2 00	1.5	9.0	2 6	50./	13.8
			Head(Calc)	100.0	5 37	A AA	5 64	7 89	136	100.0	100.0	100.0	100.0	100.0
			Ph 3rd Cl Cond	1 9	45.2	8 59	5.05	22 0	2018	66.7	6.0	2 3	0.2	44 7
	ĺ		Pb 2nd Cl Cond	3.0	34.9	9,64	6.69	27.1	1722	69.7	10.8	4.8	174	60 A
1			Zn 3rd Cl Conc	6.6	3.44	34.4	5.21	20.3	344	15.0	63.9	8.2	28.3	26.5
- 1	F28	27	Zn 2nd Cl Conc	7.9	3.26	29.4	7,32	20.2	307	16.9	85.3	13.7	33.5	28.2
1			AsPy Ro Conc	24.7	0.46	0.32	13.3	9.00	21.9	7,4	2.9	77.8	48.7	6.3
	1		AsPy Ro Tail	64.3	0.14	0.042	0.24	0.18	6.40	5.9	1.0	3,7	2.4	4.8
			Head(Calc)	100.0	1.53	2.72	4.22	4,76	86.4	100.0	100.0	100.0	100.0	100.0
			Pb 3rd Cl Cond	2.1	54.4	7.90	4,60	15.6	1048	37.1	3.4	1.1	2.6	26.5
- }]		Pb 2nd CI Cond	4.6	46.3	9.68	6.66	19.5	932	68.8	9.0	3.3	7,0	51.4
_]			Pb Ro Conc	19.9	14.3	10.1	12.8	23.9	313	92.5	40.8	27.8	37.2	75.1
\int			Zn 3rd Cl Conc	4.9	0.81	62.8	2.66	4.83	69.8	1.3	52.6	1.4	1.8	4.1
· 1	F20	1 to 7	Zn 2nd Cl Cond	5.0	0.84	51.9	2.58	5.39	70.6	1.4	53.3	1.4	2.1	4.0
			Zn Ro Conc	8.2	0.87	33.5	6.23	9.76	59.6	2.3	55.9	5.6	6.3	5.9
- [AsPy Ro Conc	26.3	0.42	0.52	21.9	25.9	44.6	3.6	2.8	62.6	53.2	14.1
			ASPY HO Tall	45.5	0.11	0.055	0.82	0.92	8.90	1.8	0.5	4.1	3.3	4.9
ŀ			Head(Calc)	100.0	3.09	4.91	9 20	12.8	83.1	100.0	100.0	100.0	100.0	100.0
			PD 3rd CI Cond	1.3	00.4	8.50	0.050	2.90	949	36.7	0.8	0.3	8.8	24.9
			75 2nd Ci Cond	22.2	04.0	10.3 66.0	0.099	2.02	105	23.3	1.2	U.O 5 4	57.0	35.0
	520		Zn 3rd Cl Conc	22.0	4.02	50.0 K/ 0	0.039	1.00	103	40.5	04.0		57.1 60.3	51.5
	FJU	69	AcPV So Conc	15.0	0.54	2 98	1 4 2	0.73	26.8	0.8 	3.3	977	25 6	93.V
{			AsPy Ro Tall	50.0	0.085	0.065	0.014	0.70	1 70	2.0	0.3	3.5	2 A	2 2
Ì			Head/Calc)	100.0	2 28	13 4	0.24	0.42	45 5	100.0	100.0	100.0	100.0	100 0
ł			Ph 3rd Cl Cond	6 1	47.2	14 5	3 18	16.8	7243	69.7	10.9	2.5	7.9	56.5
	-		Ph 2nd Cl Cond	8.3	39.9	16.2	4.49	17.9	635	79.4	18.3	4.7	12.1	65.5
}			Zn 3rd Cl Conc	13.1	3.38	48.6	2.70	17.8	1243	10.7	74.9	4.5	19.2	20.3
- {	E31	288	Zn 2nd Ci Conc	14.0	3.50	44.8	3.21	17.6	125	11.8	76.8	5.7	20.3	21.9
		200	AsPy Ro Conc	34.9	0.83	1.46	19.4	22.6	23.1	7.0	6.2	85.1	64 5	10.1
1			AsPy Ro Tall	42.8	0.17	0.11	0.84	0.86	4.70	1.8	0.6	4.5	3.0	2.5
			Head(Caic)	100.0	4.15	8.18	7.95	12.2	80.0	100.0	100.0	100.0	100.0	100 0
ł			Po 3rd Cl Cond	0.5	63.8	11.4	0.042	3.56	610	33.6	0.7	0.4	8.9	15.5
			Pb 2nd Cl Cond	0.8	57.2	13.8	0.027	4.05	573	47.4	1.4	0,4	15.8	22.8
			Zn 3rd Cl Conc	13.3	2.27	65.0	0.014	0.77	88.6	32.9	95.7	4.0	52.6	61.8
1	F32	29	Zn 2nd Cl Conc	13.6	2.37	53.9	0.021	0.80	88.9	35.3	96.6	8.3	56.1	63.8
			AsPy Ro Conc	15.0	0.49	0.79	0.27	0.27	11.3	8.0	1.6	87.2	20.9	8.9
- 1			AsPy Ro Tall	70.6	0,12	0.051	0.004	0.020	1.20	9.3	0.5	6.1	7.3	4.5
	1		Head(Calc)	100.0	0.91	7.82	0.046	0.19	19.0	100.0	100. <u>0</u>	100.0	100.0	100.0

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TABLE 4

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1	Test	Composile	Product	Weight		Ăc	LOVE Y.	n/t				Distribu	line	·
۱. 	No	Composite	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Υ_	Ph	70		Au	ا مد ا	еь 1	7.			
}			Ph 3rd Cl Cood	2 5	50.6	10 2	2 74	18.6	700	74 0	 		14.2	- 24 - 6
			Ph 2nd CI Cond	3 1	43.1	11.0	9 77	17.3	723	91 7	7.6	J	10.2	6 0 3
			Zo 3rd Cl Cond	8 3	47	40.2	4 1 2	a 4.5	727	7 4	49.4	15.0	28.1	10.0
	599	30	Ze 2nd Ci Cono	0.5	1 60	40.0		+0.03	71 5	6.1	00.0	22.0	20.1	10.0
	F 3 3	30		22.0	0.36	96.0	7 47	5 50	0 70	E 2	• • •	71.0	45.0	
			ASPY FO COIL	23.3	0.30	0.30	1.4/	2,59		0.0	1,0	11.2	40.9	0.9
			Hand(Cale)	100.0	4 86	4 66	0.001	0.030		100 0	100 0	1.0	100.0	2.2
ł		·····	Ph 2rd Cl Cond	E 7	60.6	4,00	e.44	4.05	202	74 6	44 6	100.0	100.0	100.0
			Ph and Cl Cane	2.4	42.7	10.0	3,32	10.0	790	14.0	4 8 4		36.1	30.0
			7a 3rd Cl Conc	4 4 4	2 70	10.0	9.07	8 10.5	109	03.4	70.4	9.7		10.5
- 1	644		Zn Sed Cl Conc	4+ 6	2 70	46.0	2.00	0.10	100		20.7		94.1	
]	F34		As Py Ba Com	20.8	0.77	0.0	4,00	0.00	31.3	6.0	20.1	9.V #11	14.0	15.5
			AsPy Bo Tail	51 1	0.18	0.02	0 7 3	0.67	4 60	24	4./ 0.7	63.1		2 0
			Hond (Cale)	100.0	3 80	A 76	6 0 7	2 01	82 0	100.0	100.0	200 0	100.0	100.0
- F			Ph 3rd Ci Cond	2 0	35 4	110	4 4 4	22.6	642	a na	8.6	6 1	21.1	61 D
- [Ph 2nd Cl Cond	4.7	97 4	14.2	5 70	20.4	501	75.0	45.1	11 0	20.1	51.5
1			Zn 3rd Cl Cond	6 1	2 65	38 1	3 07	7 48	86 1	14.0	70 8	14.5	20,1	03.0
	F75	2.2	Zn 2nd Cl Cond	10.9	2 60	33.5	5 4 9	8 64	81.6	16.4	R1 8	24 0	20 4	24 0
1		52	AsPy Ba Conc	24 5	0 4 4	0 4 2	8.10	5 4 9	13 1	6.3	2 1	63.0	40.7	9.7
[AsPy Ro Tall	50.9	0.067	0 059	0.083	0.040	2 10	2 3	ń. 8	2.0	0.7	2.4
- 1			Head(Caic)	100.0	1 72	4 45	2 48	3 10	16 0	100.0	100.0	100.0	100.0	100.0
			Ph 3rd Cl Cond	18.2	45.7	15.3	2.48	25.0	644	82.0	26.9	12.6	45.8	76 1
			Pb 2nd Cl Cond	18.8	41.6	15.7	2.95	23.9	592	86.3	32.0	174	50.7	At 0
			Zn 3rd Cl Conc	10.6	3.14	52.8	1.47	4 77	79.4	3.7	60.9	4 9	5.7	6.2
1	F36	33	Zn 2nd Cl Canc	12 5	4 23	47.3	2 28	6 94	97.3	5 A	63.9	8.9	6.8	
- 1		•••	AsPy Bo Conc	32.7	1.92	1.05	8.81	10.1	37.1	6.9	3.7	6.93	37 4	8.8
	j		AsPy Ro Tail	36.1	0.23	0 1 1	0 34	0.51	5 00	0.9	0.4	3.9	21	1 1
1	1		Head(Calc)	100.0	9.04	9 23	3.19	6.64	137	100.0	100 0	100 0	100.0	100 0
- F		·	Pb 3rd Ci Cond	2.6	39.3	9.77	5.46	23.6	1418	55.3	4.7	2.8	10.8	45.2
_			Pb 2nd Cl Cond	4,5	30.5	11.1	6.57	19.8	1187	72.8	9 . 5	5.7	15.3	64.3
(`		Zn 3rd Cl Cond	8 8	1,52	51.4	1.90	5.16	t 4 8	7 .1	83.t	3.2	7.9	15.7
ì	F37	34	Zn 2nd Cl Conc	9.5	1.74	48.5	2.42	5.69	156	8.9	85.2	4.5	9.4	18.1
			AsPy Ro Conc	39.3	0.69	0.68	11.3	10.7	31.9	14.6	4.9	86.8	73.0	15.3
- 1			AsPy Ro Tail	46.7	0.15	0.083	0.33	0.27	4.00	3.8	0.7	3.0	2.2	2.3
1			Head(Cale)	100.0	1.86	5.42	5.12	5.74	82.1	100.0	100.0	100.0	100.0	100.0
ſ			Pb 3rd Cl Cond	8.7	48.4	12.6	3.65	10.0	914	85.9	22.6	13.5	28.3	80.3
- í			Pb 2nd Cl Cond	10.8	41.3	14.1	4,60	10.5	799	90.7	31.4	21.1	34.0	86.8
1			Zn 3rd Cl Conc	8.1	2.60	61,4	1.64	3,43	85.6	3.2	64.6	4,3	6.3	5.3
[F388	35	Zn 2nd Cl Cond	6.4	2.73	49.2	2.06	3.91	89.6	3.6	65.2	5.7	7.6	5.8
		:	AsPy Ro Conc	30,9	0.66	0.45	5.37	6.10	20.1	4.2	2.9	70.8	56.8	6.3
			AsPy Ro Tall	52.0	0,15	0.042	0,11	0,10	2.20	1.6	0.5	2.4	1.6	1.2
			Head(Calc)	100.0	4.90	4.84	2.34	3.31	99.0	100.0	100.0	100.0	100.0	100.0
- F			Pb 3rd Cl Cond	9.3	30.2	22.3	3.79	10.5	456	60.3	29.6	19.7	45.2	76.7
			Pb 2nd CI Cond	13.3	23.6	22.9	4.30	9.18	365	90.1	43.6	32.0	56.4	87,9
			Zn 3rd Cl Cond	6.2	0,78	59.3	0,53	0.77	25.3	1,4	52.6	1.8	2.2	2.8
I	F39	36	Zn 2nd Cl Cond	6.5	0.94	57.9	0.73	1.06	28.8	1.7	53.6	2.7	3.2	3.4
- 1			AsPy Ro Conc	24.2	0.86	0.67	4.67	3.53	15.4	5.9	2.3	63.2	39.4	7.2
- 1			AsPy Ro Tail	56.0	0.14	0 058	0.068	0.040	1.50	2.2	0.5	2.1	1.0	15
			Head(Calc)	100.0	3,50	7.00	1.79	2.17	55.4	100.0	100 0	100.0	100.0	100.0
- r			Pb 3rd Cl Cond	2.2	42.3	11.3	4.64	23.9	929	76.0	7.0	2.5	13.5	67.5
Į]		Pb 2nd Cl Cond	3.0	33.B	12.1	6.06	22.4	770	82.0	10.2	4.5	17.1	75.5
			Zn 3rd Cl Conc	\$.5	1.15	53.7	1.56	3.55	62.2	5.2	84,6	2.1	5.1	11.4
	F40	37	Zn 2nd Cl Conc	6.1	1.32	49.5	2.97	4.98	64.5	6.7	86.5	4.5	7.9	13.1
- [AsPy Ro Conc	34,0	0.29	0.25	10.6	8.40	7.50	8.1	2.4	89.7	74.0	85
			AsPy Ro Tail	56.9	0.07	0.054	0.091	0.070	1.50	3.3	0.9	1.3	1.0	28
- 1			Head(Calc)	100.0	1.22	3.51	4.02	3.86	30.1	100.0	100.0	100.0	100.0	100.0

Test F55 COMPOSITE A.

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Product	Welg	ht	Ass	ays,%, g/t		% Distributio		on
	8	%	Pb	Zn	As	Pb	Zn	As
Pb Cl Conc	101.3	5.1	44.0	11.8	7.54	82.2	12.2	4.7
Pb 4th Cl Tali	20.4	1.0	9.93	14.9	17.5	3.7	3.1	2.2
Pb 3rd Cl Tail	17.5	0.9	5.88	13.3	18.4	1.9	2.4	2.0
Pb 2nd Cl Tall	55.1	2.8	2.83	11.0	16.4	2.9	6.2	5.5
Zn Cl Conc.	50.7	2.5	0.39	56.6	0.23	0.4	29.2	0.1
Zn 2nd Cl Tali	22.8	1.1	0.67	50.8	1.23	0.3	11.8	0.2
Zn 1st Cl Scav Conc.	15.7	0.8	0.70	45.9	2.11	0.2	7.3	0.2
Zn 1st Cl Scav Tall	30.9	1.5	0.83	23.2	7.40	0.5	7.3	1.4
Zn Ro Scav. Cl Conc.	13.2	0.7	1.01	39.0	4.54	0.2	5.2	0.4
Zn Ro Scav. Cl Tall	26.3	1.3	0.89	13.8	7.78	0.4	3.7	1.3
Zn Ro Scav.Tall	1640.0	82.3	0.24	0.70	8.16	7.3	11.7	82.1
Head(Calc)	1993.9	100.0	2.72	4.93	8.17	100.0	100.0	100.0
Combined Products								
Pb 3rd Cl Conc(1+2	2)	6.1	38.3	12.3	9.21	86.0	15.3	6.9
Pb 2nd Cl Conc(1 to	3)	7.0	34.2	12.4	10.4	87.9	17.6	8.9
Pb 1st CI Conc(1 to	4)	9.7	25.3	12.0	12.1	90.7	23.8	14.4
Zn 1st Ci Conc(5+6)	3.7	0.48	54.8	0.54	0.8	41.0	0.2
Zn Ro Conc(5 to 8)		6.0	0.60	45.5	2.51	1.3	55.6	1.9
Zn Ro Scav Conc (9	+10)	2.0	0.93	22.2	6.70	0.7	8,9	1.6
Zn Comb Conc (5 to	10)	8.0	0.68	39.7	3.55	2.0	64.5	3.5
	Product Pb CI Conc Pb 4th CI Tall Pb 3rd CI Tall Pb 2nd CI Tall Zn CI Conc. Zn 2nd CI Tall Zn 1st CI Scav Conc. Zn 1st CI Scav Conc. Zn 1st CI Scav Conc. Zn Ro Scav. CI Conc. Tall Head(Calc) Combined Products Pb 3rd CI Conc(1+4 Pb 2nd CI Conc(1+4 Pb 2nd CI Conc(1 to Zn Ro Scav Conc (1 to Zn Ro Scav Conc (5 to 8) Zn Ro Scav Conc (9) Zn Comb Conc (5 to	ProductWeig9Pb CI Conc101.3Pb 4th CI Tali20.4Pb 3rd CI Tali17.5Pb 2nd CI Tali55.1Zn CI Conc.50.7Zn 2nd CI Tali22.8Zn 1st CI Scav Conc.15.7Zn 1st CI Scav Conc.13.2Zn Ro Scav. CI Conc.13.2Zn Ro Scav. CI Conc.13.2Zn Ro Scav. CI Conc.13.2Zn Ro Scav. CI Tali26.3Zn Ro Scav. Tali1640.0Head(Calc)1993.9Combined ProductsPb 3rd CI Conc(1+2)Pb 2nd CI Conc(1+2)Pb 1st CI Conc(1 to 3)Pb 1st CI Conc(5 to 8)Zn Ro Scav Conc (9+10)Zn Comb Conc (5 to 10)	Product Weight g % Pb CI Conc 101.3 5.1 Pb 4th CI Tali 20.4 1.0 Pb 3rd CI Tali 17.5 0.9 Pb 2nd CI Tali 55.1 2.8 Zn CI Conc. 50.7 2.5 Zn CI Conc. 50.7 2.5 Zn CI Conc. 15.7 0.8 Zn 1st CI Scav Conc. 15.7 0.8 Zn 1st CI Scav Conc. 13.2 0.7 Zn Ro Scav. CI Tali 26.3 1.3 Zn Ro Scav.Tali 1640.0 82.3 Head(Calc) 1993.9 100.0 Combined Products 7.0 Pb 3rd Cl Conc(1+2) 6.1 Pb 2nd Cl Conc(1 to 3) 7.0 Pb 1st Cl Conc(5+6) 3.7 Zn Ro Conc(5 to 8) 6.0 Zn Ro Scav Conc (9+10) 2.0 Zn Comb Conc	ProductWeight gAss Pb g %PbPb CI Conc101.35.144.0Pb 4th CI Tali20.41.09.93Pb 3rd CI Tali17.50.95.88Pb 2nd CI Tali55.12.82.83Zn CI Conc.50.72.50.39Zn 2nd CI Tali22.81.10.67Zn 1st CI Scav Conc.15.70.80.70Zn 1st CI Scav Conc.13.20.71.01Zn Ro Scav. CI Conc.13.20.71.01Zn Ro Scav. CI Conc.13.20.71.01Zn Ro Scav. CI Tali26.31.30.89Zn Ro Scav. Tali1640.082.30.24Head(Calc)1993.9100.02.72Combined Products7034.2Pb 3rd Cl Conc(1+2)6.138.3Pb 2nd Cl Conc(1 to 3)7.034.2Pb 1st Cl Conc(5+6)3.70.48Zn Ro Conc(5 to 8)6.00.60Zn Ro Scav Conc (9+10)2.00.93Zn Comb Conc (5 to 10)8.00.68	ProductWeight gAssays,%, g Pb Zn Zn Pb Cl Conc101.35.144.011.8Pb 4th Cl Tall20.41.09.9314.9Pb 3rd Ci Tall17.50.95.8813.3Pb 2nd Cl Tall55.12.82.8311.0Zn Cl Conc.50.72.50.3956.6Zn 2nd Cl Tall22.81.10.6750.8Zn 1st Cl Scav Conc.15.70.80.7045.9Zn 1st Cl Scav Conc.13.20.71.0139.0Zn Ro Scav. Cl Conc.13.20.71.0139.0Zn Ro Scav. Cl Conc.13.20.71.0139.0Zn Ro Scav. Cl Tall26.31.30.8913.8Zn Ro Scav. Tall1640.082.30.240.70Head(Calc)1993.9100.02.724.93Combined Products7.034.212.4Pb 3rd Cl Conc(1+2)6.138.312.3Pb 2nd Cl Conc(1 to 3)7.034.212.4Pb 1st Cl Conc(1 to 4)9.725.312.0Zn 1st Cl Conc(5+6)3.70.4854.8Zn Ro Scav Conc (9+10)2.00.9322.2Zn Comb Conc (5 to 10)8.00.6839.7	ProductWeight gAssays,%, g/t PbZnAsPb Cl Conc101.35.144.011.87.54Pb 4th Cl Tall20.41.09.9314.917.5Pb 3rd Cl Tall17.50.95.8813.318.4Pb 2nd Cl Tall55.12.82.8311.016.4Zn Cl Conc.50.72.50.3956.60.23Zn 2nd Cl Tall22.81.10.6750.81.23Zn 1st Cl Scav Conc.15.70.80.7045.92.11Zn 1st Cl Scav Tall30.91.50.8323.27.40Zn Ro Scav. Cl Conc.13.20.71.0139.04.54Zn Ro Scav. Cl Conc.13.20.71.0139.04.54Zn Ro Scav. Cl Tall26.31.30.8913.87.78Zn Ro Scav. Cl Tall1640.082.30.240.708.16Head(Calc)1993.9100.02.724.938.17Combined Products7.034.212.410.4Pb 3rd Cl Conc(1+2)6.138.312.39.21Pb 2nd Cl Conc(1 to 3)7.034.212.410.4Pb 1st Cl Conc(1 to 4)9.725.312.012.1Zn tst Cl Conc(5+6)3.70.4854.80.54Zn Ro Conc(5 to 8)6.00.6045.52.51Zn Ro Conc(5 to 8)6.00.6039.73.55	ProductWeight gAssays,%, g/t% Ig%PbZnAsPbPb CI Conc101.35.144.011.87.5482.2Pb 4th CI Tall20.41.09.9314.917.53.7Pb 3rd CI Tall17.50.95.8813.318.41.9Pb 2nd CI Tall55.12.82.8311.016.42.9Zn CI Conc.50.72.50.3956.60.230.4Zn 2nd CI Tall22.81.10.6750.81.230.3Zn 1st CI Scav Conc.15.70.80.7045.92.110.2Zn 1st CI Scav Tall30.91.50.8323.27.400.5Zn Ro Scav. CI Conc.13.20.71.0139.04.540.2Zn Ro Scav. CI Tall26.31.30.8913.87.780.4Zn Ro Scav. CI Tall26.31.30.8913.87.780.4Zn Ro Scav. CI Tall1640.082.30.240.708.167.3Head(Calc)1993.9100.02.724.938.17100.0Combined Products73.512.012.190.7Zn 1st CI Conc(1+2)6.138.312.39.2186.0Pb 3rd Cl Conc(1 to 3)7.034.212.410.487.9Pb 1st Cl Conc(5+6)3.70.4854.80.540.6Zn Ro Conc(5 to 8)6.0	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

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Test F58 Composite B

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	Product	Weig	ht	Ass	ays,%, (g/t	%	Distributi	ion
		9	%	Pb	Zn	As	РЬ	Zn	As
1	Pb Cl Conc	97.1	4.9	30.0	13.8	6.17	87.8	11.8	5.8
2	Pb 4th CI Tail	10.6	0.5	4.23	14.3	13.6	1.4	1.3	1.4
3	Pb 3rd Cl Tail	15.1	0.8	2.52	12.3	12.2	1.1	1.6	1.8
4	Pb 2nd Cl Tall	45.2	2.3	1.08	10.1	10.2	1.5	4.0	4.5
5	Zn Cl Conc.	84.9	4.3	0.31	57.4	0.15	0.8	42.9	0.1
6	Zn 2nd Cl Tail	51.5	2.6	0.57	48.7	1.31	0.9	22.1	0.7
7	Zn 1st Cl Scav Conc.	26.1	1.3	0.58	36.3	3.35	0.5	8.3	0.8
8	Zn 1st Cl Scav Tall	55.2	2.8	0.46	9.55	5.65	0.8	4.6	3.0
9	Zn Ro Scav. Cl Conc.	8.3	0.4	0.62	6.37	4.80	0.2	0.5	0.4
10	Zn Ro Scav, Cl Tail	78.1	3.9	0.27	1.25	3.85	0.6	0.9	2.9
11	Zn Ro Scav.Tail	1513.6	76.2	0.10	0.15	5.38	4.6	2.0	78.7
	Head(Calc)	1985.7	100.0	1.67	5.72	5.21	100.0	100.0	100.0
	Combined Products								
	Pb 3rd Ci Conc(1+2	2)	5.4	27.5	13.8	6.90	89.1	13.1	7.2
	Pb 2nd Cl Conc(1 to	3)	6.2	24.4	13.7	7.55	90.3	14.8	9.0
	Pb 1st Cl Conc(1 to	4)	8.5	18.1	12.7	8.27	91.7	18.8	13.4
	Zn 1st Cl Conc(5+6)	6.9	0.41	54.1	0.59	1.7	64.9	0.6
	Zn Ro Conc(5 to 8)	-	11.0	0.44	40.7	2.20	2.9	77.9	4.6
	Zn Ro Scav Conc (9	+10)	4.4	0.30	1.74	3.94	0.8	1.3	3.3
	Zn Comb Conc (5 to	10)	15.3	0.40	29.6	2.70	3.7	79.2	7.9

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APPENDIX G ACID GENERATION TESTWORK

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Test AP 1	-Gravity Plant Reject Stream
Test AP 2	-Flotation Tailings
AG #1 To AG #42	-Underground Footwall, Hanging Wall Samples

Test No. AP1

Purpose: To determine the acid producing potential of the + 1/4 inch Float sample.

- Procedure: Duplicate 10 gram samples were pulped in 100 mL of distilled water and titrated while mixing to a pH of 3.5 with 1.0 N H₂SO4. The pH was maintained with acid additions until the variation in pH was <0.1 over a 4 hour period.
- Feed: 2 x 10 grams pulverized +1/4 inch Float from Bulk Sample Heavy Media Separation.

Calculations: Acid Consuming Ability $(kg/t) = \frac{mL \text{ of } 1.0 \text{ N} \text{ H}_2\text{SO4} \times 0.049 \times 10^3}{\text{wt of sample in g}}$

$$= \frac{28.2 \times 0.049 \times 10^3}{10}$$

= 138.2

Acid Producing Potential (kg/t) = $\frac{\% S}{100} \times \frac{10^3 \times 98}{32}$

$$= \frac{1.23}{100} \times \frac{10^3 \times \frac{98}{32}}{32}$$

= 37.7

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TimeIndCumIndCum014.0014.09.4-3.814.014.09.4-3.81/41.015.04.8-3.61.015.04.6-3.61/20.415.44.2-3.40.515.54.4-3.610.515.95.0-3.80.516.05.7-3.81.50.316.25.8-3.80.316.65.0-3.420.416.65.8-3.80.316.65.0-3.62.50.517.15.8-3.40.417.05.2-3.230.217.35.4-3.30.217.24.8-3.44.50.518.65.0-3.40.418.15.2-3.650.218.65.8-3.20.318.45.0-3.25.50.219.05.8-3.40.218.65.1-3.560.419.45.6-3.10.419.25.7-3.370.219.65.6-3.10.419.25.7-3.370.219.85.0-3.20.219.65.0-3.280.320.25.6-3.00.319.95.3-3.08.50.520.76.2-3.20.220.15.2-3.090.121.85.2-3.00.221.95.0-3.290.121.45.0-3.00.221.05.0-3.290.121.45.0-3.00.221.05.0-3.2100.1			m]	Ls	pН	_	mĹs	pH
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		Time	Ind	Cum		In	d Cum	
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10.51.5.93.10-3.80.516.05.7-3.820.416.65.8-3.80.316.65.0-3.420.416.65.8-3.80.316.65.0-3.62.50.517.15.8-3.40.417.05.2-3.230.217.35.4-3.30.217.24.8-3.43.50.417.75.2-3.20.417.64.9-3.040.418.15.0-3.40.117.74.8-3.44.50.518.66.0-3.40.418.15.2-3.550.219.05.8-3.40.218.65.1-3.560.419.45.6-3.50.218.85.2-3.46.50.219.65.6-3.10.419.25.7-3.370.219.85.0-3.50.219.65.0-3.280.320.25.6-3.00.319.95.3-3.090.120.84.2-3.50.220.15.2-3.090.120.84.2-3.50.220.55.2-3.0100.121.15.2-3.00.221.05.0-3.09.50.221.05.0-3.00.221.05.0-3.010.50.121.45.0-3.00.121.45.2-3.0100.121.45.0-3.00.121.45.2-3.0100.121.45.0-3.00.121.65.0-3.0 <td></td> <td>1/2</td> <td>0.4</td> <td>15.4</td> <td>4.2-3.4</td> <td>0.</td> <td>5 15.5</td> <td>4.4-3.6</td>		1/2	0.4	15.4	4.2-3.4	0.	5 15.5	4.4-3.6
1.50.316.22.8-3.80.316.35.0-3.420.416.65.8-3.80.316.65.0-3.62.50.517.15.8-3.40.417.05.2-3.230.217.35.4-3.30.217.74.8-3.44.50.417.75.2-3.20.417.64.9-3.040.418.15.0-3.40.418.15.2-3.25.50.218.65.8-3.40.117.74.8-3.44.50.518.66.0-3.40.418.15.2-3.560.419.45.6-3.50.218.65.1-3.560.419.45.6-3.50.219.65.0-3.270.219.85.0-3.20.219.45.0-3.280.320.25.6-3.00.319.95.3-3.08.50.50.221.05.0-3.20.220.55.2-3.090.120.84.2-3.50.220.55.2-3.0100.121.15.2-3.00.121.65.0-3.2100.121.45.0-3.00.221.05.0-3.0120.421.85.6-3.00.221.05.0-3.012.50.121.95.4-3.20.121.45.2-3.4130.122.05.4-3.20.121.55.4-3.2140.122.35.0-3.00.121.65.		1	0.5	15.9	5.0-3.8	0.	5 16.0	5.7-3.8
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		1.5	0.3	16.2	5.8-3.8	0.	3 16.3	5.0-3.4
2.50.517.15.8-3.40.417.05.2-3.230.217.35.4-3.30.217.24.8-3.43.50.417.75.2-3.20.417.64.9-3.040.418.15.0-3.40.117.74.8-3.44.50.518.66.0-3.40.418.15.2-3.650.218.85.8-3.40.218.65.1-3.560.419.45.6-3.50.218.85.2-3.46.50.219.65.6-3.10.419.25.7-3.370.219.85.0-3.50.219.45.0-3.280.320.25.6-3.00.319.95.3-3.08.50.520.76.2-3.20.220.15.2-3.090.120.84.2-3.50.220.35.2-3.090.121.45.0-3.20.220.55.2-3.0100.121.15.2-3.00.221.05.0-3.2110.121.45.0-3.00.221.05.0-3.2120.421.85.6-3.00.221.05.0-3.2110.121.45.0-3.00.121.45.0-3.012.50.121.95.4-3.00.121.45.0-3.012.50.121.95.4-3.00.121.45.0-3.2130.122.35.4-3.20.121.55.6-3.0<		2	0.4	16.6	5.8-3.8	0.	3 16.6	5.0-3.6
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3.5 0.4 17.7 $5.2-5.2$ 0.4 17.7 $4.9-3.0$ 4 0.4 18.1 $5.0-3.4$ 0.1 17.7 $4.8.3.4$ 4.5 0.5 18.6 $6.0-3.4$ 0.4 18.1 $5.2-3.6$ 5 0.2 19.0 $5.8-3.4$ 0.2 18.6 $5.1-3.5$ 6 0.4 19.4 $5.6-3.5$ 0.2 18.8 $5.2-3.4$ 6.5 0.2 19.6 $5.6-3.1$ 0.4 19.2 $5.7-3.3$ 7 0.2 19.8 $5.0-3.5$ 0.2 19.6 $5.0-3.2$ 8 0.3 20.2 $5.6-3.0$ 0.3 19.9 $5.3-3.0$ 8.5 0.5 20.7 $62-3.2$ 0.2 20.1 $5.2-3.0$ 9 0.1 20.8 $42-3.5$ 0.2 20.3 $5.3-3.0$ 9 0.1 20.8 $42-3.5$ 0.2 20.3 $5.3-3.0$ 9 0.1 21.8 $5.6-3.0$ 0.1 20.8 $5.2-3.0$ 10 0.1 21.1 $5.2-3.0$ 0.2 21.0 $5.0-3.2$ 10 0.1 21.4 $5.0-3.0$ 0.2 21.0 $5.0-3.2$ 10 0.1 21.4 $5.0-3.0$ 0.2 21.0 $5.0-3.2$ 10 0.1 21.4 $5.0-3.0$ 0.2 21.0 $5.0-3.0$ 10 0.1 21.4 $5.0-3.0$ 0.1 21.4 $5.2-3.2$ 10 0.1 21.9 $5.4-3.2$ 0.1 21.4		3	0.2	17.3	5.4-3.3	0.	2 17.2	4.8-3.4
4 0.4 16.1 $5.0-5.4$ 0.1 $1.7.7$ $4.8-3.4$ 4.5 0.5 18.8 $5.8-3.4$ 0.2 18.6 $5.1-3.5$ 5 0.2 19.0 $5.8-3.4$ 0.2 18.6 $5.1-3.5$ 6 0.4 19.4 $5.6-3.5$ 0.2 18.8 $5.2-3.4$ 6.5 0.2 19.6 $5.6-3.1$ 0.4 19.2 $5.7-3.3$ 7 0.2 19.6 $5.0-3.2$ 0.2 19.6 $5.0-3.2$ 8 0.3 20.2 $5.6-3.0$ 0.3 19.9 $5.3-3.0$ 8.5 0.5 20.7 $6.2-3.2$ 0.2 20.3 $5.3-3.0$ 9 0.1 20.8 $42-3.5$ 0.2 20.3 $5.3-3.0$ 0.5 0.2 21.0 $5.0-3.2$ 0.2 20.5 $5.2-3.0$ 10 0.1 21.4 $5.0-3.0$ 0.1 21.8 $5.0-3.2$ 10 0.1 21.4 $5.0-3.0$ 0.1		3.3	0.4	17.7	5.2-3.2	0.	4 17.6	4.9-3.0
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7 0.2 19.6 $5.0-3.2$ 0.2 19.4 $5.0-3.2$ 8 0.3 20.2 $5.6-3.0$ 0.3 19.9 $5.3-3.0$ 8.5 0.5 20.7 $6.2-3.2$ 0.2 20.1 $5.2-3.0$ 9 0.1 20.8 $4.2-3.5$ 0.2 20.3 $5.3-3.0$ 9.5 0.2 21.0 $5.0-3.2$ 0.2 20.5 $5.2-3.0$ 10 0.1 21.1 $5.2-3.0$ 0.2 20.5 $5.2-3.0$ 10.5 0.2 21.3 $5.2-3.0$ 0.2 20.5 $5.2-3.0$ 10.5 0.2 21.3 $5.2-3.0$ 0.2 20.7 $5.0-3.0$ 12.5 0.1 21.4 $5.0-3.0$ 0.2 21.0 $5.0-3.0$ 12.5 0.1 21.4 $5.0-3.0$ 0.2 21.2 $5.0-3.0$ 12.5 0.1 21.9 $5.4-3.0$ 0.1 21.4 $5.2-3.2$ 13 0.1 22.0 $5.4-3.2$ 0.1 21.4 $5.2-3.2$ 14 0.1 22.3 $5.4-3.2$ 0.1 21.4 $5.2-3.2$ 14 0.1 22.5 $5.6-3.0$ 0.1 21.8 $4.9-3.0$ 15.5 0.1 22.6 $5.0-3.0$ 0.1 21.9 $5.0-3.2$ 16 0.1 22.7 $5.0-3.0$ 0.1 22.1 $4.4-2.9$ 17 0.2 23.0 $6.2-3.2$ 0.1 22.2 $5.2-3.2$ 16.5 0.1 22.5 $5.0-3.0$ <td></td> <td>7</td> <td>0.2</td> <td>10.8</td> <td>5035</td> <td>0.</td> <td>+ 19.2 7 10.4</td> <td>5.7-3.3</td>		7	0.2	10.8	5035	0.	+ 19.2 7 10.4	5.7-3.3
n = 1, 3 $0, 1$ $19, 3$ $5, 0, 20, 2$ $5, 6-3, 2$ $0, 2$ $19, 9$ $5, 3-3, 0$ $8, 5$ $0, 5$ $20, 7$ $6, 2-3, 2$ $0, 2$ $20, 1$ $5, 2-3, 0$ 9 $0, 1$ $20, 8$ $4, 2-3, 5$ $0, 2$ $20, 3$ $5, 3-3, 0$ $9, 5$ $0, 2$ $21, 0$ $5, 0-3, 2$ $0, 2$ $20, 3$ $5, 3-3, 0$ $9, 5$ $0, 2$ $21, 0$ $5, 0-3, 2$ $0, 2$ $20, 5$ $5, 2-3, 0$ $10, 0, 1$ $21, 1$ $5, 2-3, 0$ $0, 2$ $20, 7$ $5, 0-3, 0$ $10, 5$ $0, 2$ $21, 3$ $5, 2-3, 0$ $0, 1$ $20, 8$ $5, 0-3, 0$ 11 $0, 1$ $21, 4$ $5, 0-3, 0$ $0, 2$ $21, 2$ $5, 0-3, 0$ 12 $0, 4$ $21, 8$ $5, 6-3, 0$ $0, 1$ $21, 3$ $5, 2-3, 2$ 13 $0, 1$ $22, 0$ $5, 4-3, 2$ $0, 1$ $21, 3$ $5, 2-3, 2$ $13, 5$ $0, 2$ $22, 2$ $5, 4-3, 2$ $0, 1$ $21, 4$ $5, 2-3, 2$ 14 $0, 1$ $22, 3$ $5, 6-3, 0$ $0, 1$ $21, 6$ $5, 0-3, 0$ $14, 5$ $0, 1$ $22, 4$ $5, 6-3, 0$ $0, 1$ $21, 7$ $5, 0-3, 2$ $15, 5$ $0, 1$ $22, 6$ $5, 0-3, 0$ $0, 1$ $21, 2$ $5, 2-3, 2$ $16, 5$ $0, 1$ $22, 8$ $5, 2-3, 0$ $0, 1$ $22, 2$ $5, 2-3, 2$ $16, 5$ $0, 1$ $23, 4$ $4, 9-3, 2$ $0, 1$ $22, 4$ $5, 0-3, 2$ 16		7'5	0.2	10.0	50-32	0.	2 19.4 2 10.6	5033
8.5 0.5 20.7 $6.2-3.2$ 0.2 20.1 $5.2-3.0$ 9 0.1 20.8 $4.2-3.5$ 0.2 20.1 $5.2-3.0$ 9 0.1 21.0 $5.0-3.2$ 0.2 20.5 $5.2-3.0$ 10 0.1 21.1 $5.2-3.0$ 0.2 20.7 $5.0-3.0$ 10.5 0.2 21.3 $5.2-3.0$ 0.2 20.7 $5.0-3.0$ 10.5 0.2 21.3 $5.2-3.0$ 0.2 20.7 $5.0-3.0$ 11 0.1 21.4 $5.0-3.0$ 0.2 21.0 $5.0-3.0$ 12.5 0.1 21.4 $5.0-3.0$ 0.2 21.0 $5.0-3.0$ 12.5 0.1 21.4 $5.0-3.0$ 0.1 21.4 $5.2-3.4$ 13.5 0.2 22.2 $5.4-3.2$ 0.1 21.4 $5.2-3.4$ 13.5 0.2 22.2 $5.4-3.2$ 0.1 21.4 $5.2-3.4$ 14 0.1 22.3 $5.4-3.2$ 0.1 21.4 $5.2-3.4$ 14.5 0.1 22.4 $5.6-3.2$ 0.1 21.7 $5.0-3.2$ 15.5 0.1 22.6 $5.0-3.0$ 0.1 21.9 $5.0-3.2$ 16.5 0.1 22.7 $5.0-3.0$ 0.1 22.0 $4.9-3.0$ 16.5 0.1 22.8 $5.2-3.0$ 0.1 22.2 $5.2-3.2$ 17.5 0.1 23.3 $4.9-3.2$ 0.1 22.4 $5.0-3.2$ 16.5 0.1 23.5 <		8	0.1	20.2	5.6-3.0	0. 0	2 19.0	5330
9 0.1 20.8 $4.2-3.5$ 0.2 20.1 $5.2-3.0$ 9.5 0.2 21.0 $5.0-3.2$ 0.2 20.5 $5.2-3.0$ 10 0.1 21.1 $5.2-3.0$ 0.2 20.7 $5.0-3.0$ 10.5 0.2 21.3 $5.2-3.0$ 0.1 20.8 $5.0-3.2$ 11 0.1 21.4 $5.0-3.0$ 0.2 21.0 $5.0-3.0$ 12 0.4 21.8 $5.6-3.0$ 0.2 21.2 $5.0-3.0$ 12.5 0.1 21.9 $5.4-3.2$ 0.1 21.3 $5.2-3.2$ 13 0.1 22.0 $5.4-3.2$ 0.1 21.4 $5.2-3.2$ 13 0.1 22.0 $5.4-3.2$ 0.1 21.5 $5.4-3.2$ 14 0.1 22.3 $5.4-3.0$ 0.1 21.5 $5.4-3.2$ 14 0.1 22.3 $5.6-3.0$ 0.1 21.7 $5.0-3.2$ 15 0.1 22.6 $5.0-3.0$ 0.1 21.9 $5.0-3.2$ 15.5 0.1 22.6 $5.0-3.0$ 0.1 21.9 $5.0-3.2$ 16.5 0.1 22.8 $5.2-3.0$ 0.1 22.0 $4.9-3.0$ 16.5 0.1 22.8 $5.2-3.0$ 0.1 22.2 $5.2-3.2$ 17.5 0.1 23.1 $5.0-3.2$ 0.1 22.2 $5.2-3.2$ 17.5 0.1 23.5 $4.4-3.2$ 0.1 22.7 $5.2-3.2$ 19.5 0.1 23.5 <td< td=""><td></td><td>85</td><td>0.5</td><td>20.2</td><td>6 2 3 2</td><td>0.</td><td>ン 19.9 ク 201</td><td>5730</td></td<>		85	0.5	20.2	6 2 3 2	0.	ン 19.9 ク 201	5730
9.50.221.05.0-3.20.220.55.2-3.0100.121.15.2-3.00.220.55.2-3.010.50.221.35.2-3.00.120.85.0-3.2110.121.45.0-3.00.221.05.0-3.0120.421.85.6-3.00.221.25.0-3.012.50.121.95.4-3.00.121.35.2-3.4130.122.05.4-3.20.121.45.2-3.413.50.222.25.4-3.20.121.55.4-3.2140.122.35.4-3.00.121.65.0-3.014.50.122.45.6-3.00.121.75.0-3.2150.122.65.0-3.00.121.84.9-3.015.50.122.65.0-3.00.121.95.0-3.2160.122.75.0-3.00.122.04.9-3.016.50.123.15.0-3.20.122.25.2-3.217.50.123.15.0-3.20.122.35.0-3.4180.123.25.0-3.00.122.45.0-3.219.50.123.34.9-3.20.122.75.2-3.219.50.123.54.4-3.20.122.85.2-3.2200.223.74.6-3.20.230.05.1-3.221.50.223.94.4-3.00.230.2 </td <td></td> <td>9</td> <td>0.5</td> <td>20.7</td> <td>4 2-3 5</td> <td>0.</td> <td>2 20.1 2 20.3</td> <td>53.30</td>		9	0.5	20.7	4 2-3 5	0.	2 20.1 2 20.3	53.30
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12.5 0.1 21.9 $5.4.3.0$ 0.1 21.3 $5.2.3.2$ 13 0.1 22.0 $5.4.3.2$ 0.1 21.4 $5.2.3.4$ 13.5 0.2 22.2 $5.4.3.2$ 0.1 21.4 $5.2.3.4$ 13.5 0.2 22.2 $5.4.3.2$ 0.1 21.5 $5.4.3.2$ 14 0.1 22.3 $5.4.3.0$ 0.1 21.5 $5.4.3.2$ 14 0.1 22.3 $5.4.3.0$ 0.1 21.5 $5.4.3.2$ 14.5 0.1 22.4 $5.6.3.2$ 0.1 21.7 $5.0.3.2$ 15 0.1 22.5 $5.6.3.0$ 0.1 21.9 $5.0.3.2$ 15.5 0.1 22.6 $5.0.3.0$ 0.1 21.9 $5.0.3.2$ 16 0.1 22.7 $5.0.3.0$ 0.1 22.0 $4.9.3.0$ 16.5 $0,1$ 22.8 $5.2.3.2$ 0.1 22.0 $4.9.3.0$ 17 0.2 23.0 $6.2.3.2$ 0.1 22.2 $5.2.3.2$ 17.5 0.1 23.1 $5.0.3.2$ 0.1 22.3 $5.0.3.4$ 18 0.1 23.2 $5.0.3.0$ 0.1 22.4 $5.0.3.2$ 19.5 0.1 23.3 $4.9.3.2$ 0.2 23.6 $5.0.3.2$ 20 0.2 23.7 $4.6.3.2$ 0.2 30.0 $5.1.3.2$ 20.5 0.2 23.9 $4.4.3.0$ 0.2 30.0 $5.1.3.2$ 20.5 0.2 23.9 <td></td> <td>12</td> <td>0.4</td> <td>21.8</td> <td>5.6-3.0</td> <td>0.</td> <td>2 21.2</td> <td>5.0-3.0</td>		12	0.4	21.8	5.6-3.0	0.	2 21.2	5.0-3.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		12.5	0.1	21.9	5.4-3.0	0.	1 21.3	5.2-3.2
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		14	0.1	22.3	5.4-3.0	0.	1 21.6	5.0-3.0
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		16	0.1	22.7	5.0-3.0	0.	1 22.0	4.9-3.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		16.5	0,1	22.8	5.2-3.0	0.	1 22.1	4.4-2.9
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		17	0.2	23.0	6.2-3.2	0.	1 22.2	5.2-3.2
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		18	0.1	23.2	5.0-3.0	0.	1 22.4	5.0-3.2
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$		22 5	0.5	24.1 21 Q	4.0-3.0	U.	∠ 30,9 2 30,1	J.U-J.U A G 3 O
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24.5 0.2 25.7 4.0-3.0 0.3 30.2 4.2-3.0 25 0.2 25.9 4.0-3.0 0.3 30.5 4.0-3.0		20.0	0.2	25.5	4 2.3 0	0.	2 30.9	4 4.3 0
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		25	0.2	25.9	4.0-3.0	0.	3 30.5	4.0-3.0

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Test No. AP2

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Purpose: To determine the acid producing potential of the Aspy Ro tail sample.

Procedure: Duplicate 10 gram samples were pulped in 100 mL of distilled water and titrated while mixing to a pH of 3.5 with 1.0 N H₂SO4. The pH was maintained with acid additions until the variation in pH was <0.1 over a 4 hour period.

Feed: 2 x 10 grams pulverized Combined AsPy Rougher Tails.

Calculations: Acid Consuming Ability $(kg/t) = \underline{mL \text{ of } 1.0 \text{ N H}_2\text{SO4} \times 0.049 \times 10^3}$ wt of sample in g

<u> =16.2 x</u>	0.049 x	103
	10	
- 794		

Acid Producing Potential (kg/t) = $\frac{\% \text{ S}}{100} \times \frac{10^3 \text{ x}}{32}$

$$= \frac{1.41}{100} \times \frac{10^3 \times \frac{98}{32}}{32}$$

= 43.2

$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	Data:	Sam	ple A		Sa	imple B	
TimeIndCumIndCum08.08.08.8.4.08.08.08.8.4.21/41.29.24.6-3.20.58.54.6-3.81/20.39.54.7-3.30.48.94.8-3.210.49.95.0-3.00.39.25.0-3.41.50.210.14.9-3.30.29.45.0-3.620.110.24.9-3.30.39.74.9-3.22.50.410.64.8-3.00.19.84.8-3.23.50.110.74.2-3.00.210.04.9-3.03.50.111.84.8-3.20.210.24.9-3.240.211.04.9-3.00.110.35.0-3.44.50.311.35.0-2.90.410.75.0-2.850.111.54.6-3.00.211.54.9-3.07.50.212.04.6-3.00.111.64.9-3.07.50.212.04.6-3.00.111.64.9-3.07.50.212.04.6-3.00.112.04.8-3.280.112.15.0-3.50.212.25.0-3.09.50.212.34.9-2.90.112.35.0-3.0100.112.74.2-3.00.112.74.2-2.911.50.212.65.0-3.00.112.74.2-2.911.50.2		m	Ls	pH		mĹs	pН
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1 0.4 9.9 $5.0-3.0$ 0.3 9.2 $5.0-3.4$ 1.5 0.2 10.1 $4.9-3.3$ 0.2 9.4 $5.0-3.6$ 2 0.1 10.2 $4.9-3.3$ 0.3 9.7 $4.9-3.2$ 2.5 0.4 10.6 $4.8-3.0$ 0.1 9.8 $4.8-3.6$ 3 0.1 10.7 $4.2-3.0$ 0.2 10.0 $4.9-3.0$ 3.5 0.1 10.8 $4.8-3.2$ 0.2 10.2 $4.9-3.2$ 4 0.2 11.0 $4.9-3.0$ 0.1 10.3 $5.0-3.4$ 4.5 0.3 11.3 $5.0-2.9$ 0.4 10.7 $5.0-2.8$ 5 0.1 11.4 $4.7-3.4$ 0.6 11.3 $4.9-2.6$ 5.5 0.1 11.5 $4.6-3.0$ 0.1 11.6 $4.9-2.9$ 6.5 0.1 11.7 513.1 0.1 11.7 523.1 7 0.1 11.8 $4.8-3.0$ 0.1 12.0 $4.8-3.2$ 8 0.1 12.1 $50-3.5$ 0.2 12.5 53.0 0.5 0.2 12.3 $4.9-2.9$ 0.1 12.3 $5.0-3.0$ 0.5 0.2 12.6 $5.0-3.0$ 0.1 12.7 $4.2-2.9$ 1.5 0.2 12.6 $5.0-3.0$ 0.1 12.7 $4.2-2.9$ 1.1 0.1 13.0 $4.0-3.0$ 0.1 12.7 $4.2-2.9$ 1.1 0.1 13.0 $4.0-3.0$ 0.1 12.9 <	1/2	0.3	9.5	4.7-3.3	0.4	8.9	4.8-3.2
1.50.210.14.9-3.30.29.45.0-3.620.110.24.9-3.30.39.74.9-3.22.50.410.64.8-3.00.19.84.8-3.630.110.74.2-3.00.210.04.9-3.03.50.110.84.8-3.20.210.24.9-3.240.211.04.9-3.00.110.35.0-3.44.50.311.35.0-2.90.410.75.0-2.850.111.54.6-3.00.211.54.9-3.460.111.64.8-3.00.111.64.9-2.96.50.111.75.1-3.10.111.75.2-3.170.111.84.8-3.40.211.94.9-3.07.50.212.04.6-3.00.112.04.8-3.280.112.15.0-3.50.212.25.0-3.0100.112.45.0-3.00.112.74.2-2.9110.112.74.2-3.00.112.74.2-3.0120.113.44.9-3.00.113.04.2-3.0130.113.24.2-3.00.113.04.2-3.014.50.113.44.2-3.00.113.14.0-3.215.50.113.44.2-3.00.113.43.9-3.014.50.113.54.0-3.00.113.43.9-3.0	1	0.4	9.9	5.0-3.0	0.3	9.2	5.0-3.4
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.5	0.2	10.1	4.9-3.3	0.2	9.4	5.0-3.6
2.5 0.4 10.6 $4.8-3.0$ 0.1 9.8 $4.8-3.6$ 3 0.1 10.7 $4.2-3.0$ 0.2 10.0 $4.9-3.0$ 3.5 0.1 10.8 $4.8-3.2$ 0.2 10.2 $4.9-3.2$ 4 0.2 11.0 $4.9-3.0$ 0.1 10.3 $5.0-3.4$ 4 0.2 11.3 $5.0-2.9$ 0.4 10.7 $5.0-2.8$ 5 0.1 11.4 $4.7-3.4$ 0.6 11.3 $4.9-2.6$ 5.5 0.1 11.5 $4.6-3.0$ 0.1 11.6 $4.9-2.9$ 6.5 0.1 11.7 $5.1-3.1$ 0.1 11.7 $5.2-3.1$ 7 0.1 11.8 $4.8-3.4$ 0.2 11.9 $4.9-3.0$ 7.5 0.2 12.0 $4.6-3.0$ 0.1 12.7 $5.0-3.0$ 9.5 0.2 12.3 $4.9-2.9$ 0.1 12.3 $5.0-3.0$ 10 0.1 12.7 $4.2-3.0$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.9 $4.5-3.0$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.9 $4.5-3.0$ 0.1 12.7 $4.2-2.9$ 11.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 </td <td>2</td> <td>0.1</td> <td>10.2</td> <td>4.9-3.3</td> <td>0.3</td> <td>9.7</td> <td>4.9-3.2</td>	2	0.1	10.2	4.9-3.3	0.3	9.7	4.9-3.2
30.110.7 $4.2\cdot3.0$ 0.210.0 $4.9\cdot3.2$ 40.211.0 $4.9\cdot3.0$ 0.110.3 $5.0\cdot3.4$ 4.50.311.3 $5.0\cdot2.9$ 0.410.7 $5.0\cdot3.4$ 4.50.311.3 $5.0\cdot2.9$ 0.410.7 $5.0\cdot3.4$ 50.111.5 $4.6\cdot3.0$ 0.211.5 $4.9\cdot3.4$ 60.111.6 $4.8\cdot3.0$ 0.111.6 $4.9\cdot2.9$ 6.50.111.5 $4.6\cdot3.0$ 0.111.6 $4.9\cdot2.9$ 6.50.111.8 $4.8\cdot3.4$ 0.211.9 $4.9\cdot3.0$ 7.50.212.0 $4.6\cdot3.0$ 0.111.2 $4.9\cdot3.0$ 7.50.212.0 $4.6\cdot3.0$ 0.112.0 $4.8\cdot3.2$ 80.112.1 $5.0\cdot3.5$ 0.212.2 $5.0\cdot3.0$ 9.50.212.3 $4.9\cdot2.9$ 0.112.7 $4.2\cdot2.9$ 110.112.7 $4.2\cdot3.0$ 0.112.7 $4.2\cdot2.9$ 11.50.212.9 $4.5\cdot3.0$ 0.112.8 $4.2\cdot3.0$ 120.113.0 $4.0\cdot3.0$ 0.113.1 $4.0\cdot3.2$ 130.113.2 $4.2\cdot3.0$ 0.113.1 $4.0\cdot3.2$ 130.113.2 $4.2\cdot3.0$ 0.113.1 $4.0\cdot3.2$ 130.113.4 $4.2\cdot3.0$ 0.113.3 $3.9\cdot3.0$ 150.113.6 $4.0\cdot3.0$ 0.113.4 $3.9\cdot3.0$ 15	2.5	0.4	10.6	4.8-3.0	0.1	9.8	4.8-3.6
3.50.110.84.8-3.20.210.24.9-3.240.211.04.9-3.00.110.35.0-3.44.50.311.35.0-2.90.410.75.0-2.850.111.44.7-3.40.611.34.9-3.460.111.64.8-3.00.111.54.9-3.460.111.64.8-3.00.111.75.2-3.170.111.84.8-3.40.211.94.9-3.07.50.212.04.6-3.00.112.04.8-3.280.112.15.0-3.50.212.25.0-3.09.50.212.34.9-2.90.112.35.0-3.0100.112.45.0-3.00.212.54.8-3.010.50.212.65.0-3.00.112.74.2-2.911.50.212.94.5-3.00.112.74.2-3.0120.113.04.0-3.00.113.04.2-3.012.50.113.14.4-3.00.113.14.0-3.2130.113.24.2-3.00.113.14.0-3.2140.113.44.2-3.00.113.43.9-3.015.50.113.64.0-3.00.113.43.9-3.015.50.113.64.0-3.00.113.63.9-3.015.50.113.64.0-3.00.113.83.6-	3	0.1	10.7	4.2-3.0	0.2	10.0	4.9-3.0
40.211.04.9.3.00.110.35.0.3.44.50.311.35.0.2.90.410.75.0.2.850.111.44.7.3.40.611.34.9.2.65.50.111.54.6.3.00.211.54.9.3.460.111.75.1.3.10.111.64.9.2.96.50.111.75.1.3.10.111.75.2.3.170.111.84.8.3.40.211.94.9.3.07.50.212.34.9.2.90.112.35.0.3.09.50.212.34.9.2.90.112.35.0.3.0100.112.74.2.3.00.112.74.2.2.9110.112.74.2.3.00.112.74.2.2.911.50.212.94.5.3.00.113.04.2.3.0120.113.14.4.3.00.113.04.2.3.0130.113.24.2.3.00.113.14.0.3.213.50.113.14.4.3.00.113.04.2.3.0140.113.44.2.3.00.113.33.9.3.014.50.113.54.0.3.00.113.43.9.3.015.50.113.64.0.3.00.113.63.9.3.015.50.113.64.0.3.00.113.63.9.3.015.50.113.83.6-3.00.113.83	3.5	0.1	10.8	4.8-3.2	0.2	10.2	4.9-3.2
4.50.311.35.0-2.90.410.75.0-2.850.111.44.7.3.40.611.34.9-2.65.50.111.54.6-3.00.211.54.9-3.460.111.64.8-3.00.111.64.9-2.96.50.111.75.1-3.10.111.75.2-3.170.111.84.8-3.40.211.94.9-3.07.50.212.04.6-3.00.112.04.8-3.280.112.15.0-3.50.212.25.0-3.09.50.212.34.9-2.90.112.35.0-3.0100.112.45.0-3.00.212.54.8-3.010.50.212.65.0-3.00.112.74.2-2.911.50.212.94.5-3.00.112.84.2-3.0120.113.04.0-3.00.113.04.2-3.012.50.113.14.4-3.00.113.04.2-3.013.50.113.34.2-3.00.113.24.0-2.9140.113.44.2-3.00.113.53.9-3.015.50.113.74.0-3.00.113.53.9-3.015.50.113.74.0-3.00.113.63.9-3.015.50.113.74.0-3.00.113.63.9-3.015.50.113.74.0-3.00.113.8<	4	0.2	11.0	4.9-3.0	0.1	10.3	5.0-3.4
50.111.4 $4.7.3.4$ 0.611.3 $4.9-2.6$ 5.50.111.5 $4.6.3.0$ 0.211.5 $4.9.3.4$ 60.111.6 $4.8.3.0$ 0.111.6 $4.9-2.9$ 6.50.111.7 $5.1.3.1$ 0.111.7 $5.2.3.1$ 70.111.8 $4.8.3.4$ 0.211.9 $4.9.3.0$ 7.50.212.0 $4.6.3.0$ 0.112.0 $4.8.3.2$ 80.112.1 $5.0.3.5$ 0.212.2 $5.0.3.0$ 9.50.212.3 $4.9.2.9$ 0.112.7 $4.2.2.9$ 100.112.4 $5.0.3.0$ 0.112.7 $4.2.2.9$ 11.50.212.9 $4.5.3.0$ 0.112.7 $4.2.2.9$ 11.50.212.9 $4.5.3.0$ 0.112.9 $4.0.3.0$ 120.113.0 $4.0.3.0$ 0.113.0 $4.2.3.0$ 12.50.113.1 $4.4.3.0$ 0.113.0 $4.2.3.0$ 130.113.2 $4.2.3.0$ 0.113.3 $3.9.3.0$ 14.50.113.4 $4.2.3.0$ 0.113.3 $3.9.3.0$ 15.50.113.7 $4.0.3.0$ 0.113.6 $3.9.3.0$ 15.50.113.6 $4.0.3.0$ 0.113.6 $3.9.3.0$ 15.50.113.8 $3.6-3.0$ 0.113.8 $3.6-3.0$ 160.113.8 $3.6-3.0$ 0.113.9 $3.8.3.0$ 1	4.5	0.3	11.3	5.0-2.9	0.4	10.7	5.0-2.8
5.5 0.1 11.5 $4.6-3.0$ 0.2 11.5 $4.9-3.4$ 6 0.1 11.6 $4.8-3.0$ 0.1 11.7 $5.2-3.1$ 7 0.1 11.8 $4.8-3.4$ 0.2 11.9 $4.9-2.9$ 7.5 0.2 12.0 $4.6-3.0$ 0.1 11.7 $5.2-3.1$ 7 0.1 11.8 $4.8-3.4$ 0.2 11.9 $4.9-3.0$ 7.5 0.2 12.0 $4.6-3.0$ 0.1 12.0 $4.8-3.2$ 8 0.1 12.1 $5.0-3.5$ 0.2 12.3 $5.0-3.0$ 9.5 0.2 12.3 $4.9-2.9$ 0.1 12.3 $5.0-3.0$ 10 0.1 12.4 $5.0-3.0$ 0.1 12.7 $4.2-2.9$ 11 0.1 12.7 $4.2-3.0$ 0.1 12.8 $4.2-3.0$ 12 0.1 13.0 $4.0-3.0$ 0.1 12.8 $4.2-3.0$ 12 0.1 13.0 $4.0-3.0$ 0.1 13.2 $4.0-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.4 $4.3-3.0$ 15 0.1 13.5 $4.0-3.0$ 0.1 13.5 $3.9-3.0$ 15 0.1 13.6 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 15 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 15 0.1 13.8 $3.6-3.0$ <	5	0.1	11.4	4.7-3.4	0.6	11.3	4.9-2.6
60.111.64.8-3.00.111.64.9-2.96.50.111.75.1-3.10.111.75.2-3.170.111.84.8-3.40.211.94.9-3.07.50.212.04.6-3.00.112.04.8-3.280.112.15.0-3.50.212.25.0-3.09.50.212.34.9-2.90.112.35.0-3.0100.112.45.0-3.00.212.54.8-3.010.50.212.65.0-3.00.112.74.2-2.911.50.212.94.5-3.00.112.74.2-3.0120.113.04.0-3.00.112.94.0-3.012.50.113.14.4-3.00.113.04.2-3.0130.113.24.2-3.00.113.24.0-2.9140.113.44.2-3.00.113.24.0-2.9140.113.44.2-3.00.113.53.9-3.015.50.113.74.0-3.00.113.63.9-3.015.50.113.74.0-3.00.113.63.9-3.015.50.113.74.0-3.00.113.63.9-3.0160.113.83.6-2.90.113.93.8-3.017.50.214.14.0-3.20.114.04.6-3.2180.114.24.0-3.20.114.0	5.5	0.1	11.5	4.6-3.0	0.2	11.5	4.9-3.4
6.5 0.1 11.7 $5.1-3.1$ 0.1 11.7 $5.2-3.1$ 7 0.1 11.8 $4.8-3.4$ 0.2 11.9 $4.9-3.0$ 7.5 0.2 12.0 $4.6-3.0$ 0.1 12.0 $4.8-3.2$ 8 0.1 12.1 $5.0-3.5$ 0.2 12.2 $5.0-3.0$ 9.5 0.2 12.3 $4.9-2.9$ 0.1 12.3 $5.0-3.0$ 10 0.1 12.4 $5.0-3.0$ 0.1 12.7 $4.2-2.9$ 11 0.1 12.7 $4.2-2.9$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.6 $5.0-3.0$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.9 $4.5-3.0$ 0.1 12.7 $4.2-2.9$ 12.5 0.1 13.0 $4.0-3.0$ 0.1 13.0 $4.2-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.6 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 14.5 0.1 13.6 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 15.5 0.1 13.8 $3.6-3.0$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 4	6	0.1	11.6	4.8-3.0	0.1	11.6	4.9-2.9
70.111.84.8-3.40.211.94.9-3.07.50.212.04.6-3.00.112.04.8-3.280.112.15.0-3.50.212.25.0-3.09.50.212.34.9-2.90.112.35.0-3.0100.112.45.0-3.00.212.54.8-3.010.50.212.65.0-3.00.112.74.2-2.9110.112.74.2-3.00.112.74.2-3.0120.113.04.0-3.00.112.84.2-3.0120.113.04.0-3.00.113.04.2-3.0130.113.24.2-3.00.113.14.0-3.213.50.113.34.2-3.00.113.24.0-2.9140.113.44.2-3.00.113.24.0-2.9140.113.44.2-3.00.113.43.9-3.015.50.113.74.0-3.00.113.63.9-3.0160.113.83.0-2.90.113.73.6-3.0160.113.83.6-3.00.113.83.6-3.016.50.113.83.6-3.00.114.04.6-3.2180.114.24.0-3.20.114.04.6-3.2180.114.24.0-3.20.114.73.6-3.0200.114.53.6-3.00.214.54.0-3.	6.5	0.1	11.7	5.1-3.1	0.1	11.7	5.2-3.1
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80.112.15.0-3.50.212.25.0-3.09.50.212.34.9-2.90.112.35.0-3.0100.112.45.0-3.00.212.54.8-3.010.50.212.65.0-3.00.112.74.2-2.9110.112.74.2-3.00.112.74.2-2.911.50.212.94.5-3.00.112.74.2-2.912.60.113.04.0-3.00.112.94.0-3.012.50.113.14.4-3.00.113.04.2-3.0130.113.24.2-3.00.113.04.2-3.013.50.113.34.2-3.00.113.24.0-2.9140.113.44.2-3.00.113.53.9-3.015.50.113.64.0-3.00.113.53.9-3.015.50.113.64.0-3.00.113.53.9-3.0160.113.83.6-3.00.113.73.6-3.016.50.113.83.6-3.00.113.93.8-3.017.50.214.14.0-3.20.114.04.6-3.2180.114.24.0-3.00.114.33.9-3.019.50.114.54.0-3.00.214.54.0-3.0200.114.44.0-3.00.114.23.9-3.019.50.114.54.0-3.00.114.2<	7.5	0.2	12.0	4.6-3.0	0.1	12.0	4.8-3.2
9.5 0.2 12.3 $4.9-2.9$ 0.1 12.3 $5.0-3.0$ 10 0.1 12.4 $5.0-3.0$ 0.2 12.5 $4.8-3.0$ 10.5 0.2 12.6 $5.0-3.0$ 0.1 12.7 $4.2-2.9$ 11 0.1 12.7 $4.2-2.9$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.9 $4.5-3.0$ 0.1 12.7 $4.2-2.9$ 12.5 0.1 13.0 $4.0-3.0$ 0.1 12.8 $4.2-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13.5 0.1 13.2 $4.2-3.0$ 0.1 13.0 $4.2-3.0$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-3.2$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.8 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19.5 0.1 14	8	0.1	12.1	5.0-3.5	0.2	12.2	5.0-3.0
10 0.1 12.4 $5.0-3.0$ 0.2 12.5 $4.8-3.0$ 10.5 0.2 12.5 $4.8-3.0$ 0.1 12.7 $4.2-2.9$ 11 0.1 12.7 $4.2-3.0$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.9 $4.5-3.0$ 0.1 12.7 $4.2-2.9$ 12 0.1 13.0 $4.0-3.0$ 0.1 12.8 $4.2-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13.5 0.1 13.2 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.8 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 </td <td>9.5</td> <td>0.2</td> <td>12.3</td> <td>4.9-2.9</td> <td>0.1</td> <td>12.3</td> <td>5.0-3.0</td>	9.5	0.2	12.3	4.9-2.9	0.1	12.3	5.0-3.0
10.5 0.2 12.6 $5.0-3.0$ 0.1 12.7 $4.2-2.9$ 11 0.1 12.7 $4.2-3.0$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.9 $4.5-3.0$ 0.1 12.7 $4.2-3.0$ 12 0.1 13.0 $4.0-3.0$ 0.1 12.8 $4.2-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.6 $4.0-3.0$ 0.1 13.5 $3.9-3.0$ 15.5 0.1 13.6 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 15.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 16 0.1 13.8 $3.6-3.0$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 20.5 0.2 14.4 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 21.5 0.1 14.4 </td <td>10</td> <td>0.1</td> <td>12.4</td> <td>5.0-3.0</td> <td>0.2</td> <td>12.5</td> <td>4.8-3.0</td>	10	0.1	12.4	5.0-3.0	0.2	12.5	4.8-3.0
11 0.1 12.7 $4.2-3.0$ 0.1 12.7 $4.2-2.9$ 11.5 0.2 12.9 $4.5-3.0$ 0.1 12.8 $4.2-3.0$ 12 0.1 13.0 $4.0-3.0$ 0.1 12.9 $4.0-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.0 $4.2-3.0$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 15.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.6 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16 0.1 13.8 $3.6-2.9$ 0.1 13.7 $3.6-3.0$ 16.5 0.1 13.8 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.2 $3.9-3.0$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20.5 0.2 14.8 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20.5 0.2 14.8 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 21.5 0.1 $14.$	10.5	0.2	12.6	5.0-3.0	0.1	12.7	4.2-2.9
11.5 0.2 12.9 $4.5-3.0$ 0.1 12.8 $4.2-3.0$ 12 0.1 13.0 $4.0-3.0$ $0,1$ 12.9 $4.0-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 15.5 0.1 13.8 $3.9-2.9$ 0.1 13.8 $3.6-3.0$ 16 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.4 $4.0-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.4 $4.0-3.0$ 20 0.1 14.5 <	11	0.1	12.7	4.2-3.0	0.1	12.7	4.2-2.9
12 0.1 13.0 $4.0-3.0$ 0.1 12.9 $4.0-3.0$ 12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.3 $3.9-3.0$ 15.5 0.1 13.6 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.6 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18.5 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 21 0.1 14.4 <	11.5	0.2	12.9	4.5-3.0	0.1	12.8	4.2-3.0
12.5 0.1 13.1 $4.4-3.0$ 0.1 13.0 $4.2-3.0$ 13 0.1 13.2 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15 $0,1$ 13.6 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.5 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 21.5 0.1 14.6 <td< td=""><td>12</td><td>0.1</td><td>13.0</td><td>4.0-3.0</td><td>0,1</td><td>12.9</td><td>4.0-3.0</td></td<>	12	0.1	13.0	4.0-3.0	0,1	12.9	4.0-3.0
13 0.1 13.2 $4.2-3.0$ 0.1 13.1 $4.0-3.2$ 13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15 $0,1$ 13.6 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15 $0,1$ 13.6 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 16.5 0.1 13.8 $3.6-2.9$ 0.1 13.8 $3.6-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19.5 0.1 14.3 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 21.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 22.5 0.1 14.4 $4.0-3.0$ 0.1 14.7 $3.6-3.0$ 22.5 0.1 15.0 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 23.5 0.2 14.8 $4.0-3.2$ 0.1 <	12.5	0.1	13.1	4.4-3.0	0.1	13.0	4.2-3.0
13.5 0.1 13.3 $4.2-3.0$ 0.1 13.2 $4.0-2.9$ 14 0.1 13.4 $4.2-3.0$ 0.1 13.3 $3.9-3.0$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15 $0,1$ 13.6 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.5 $3.9-3.0$ 16 0.1 13.8 $3.9-2.9$ 0.1 13.7 $3.6-3.0$ 16.5 0.1 13.8 $3.6-2.9$ 0.1 13.8 $3.6-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.3 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 21 0.1 14.4 $4.0-3.0$ 0.1 14.7 $3.6-3.0$ 22 0.1 14.4 $4.0-3.0$ 0.1 14.7 $3.6-3.0$ 22 0.1 14.6 $3.6-$	13	0.1	13.2	4.2-3.0	0.1	13.1	4.0-3.2
14 0.1 13.4 $4.2-3.0$ 0.1 13.5 $3.9-3.0$ 14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15 0.1 13.6 $4.0-3.0$ 0.1 13.5 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16 0.1 13.8 $3.9-2.9$ 0.1 13.6 $3.9-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.9 $3.8-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.4 $3.6-3.0$ 20 0.1 14.4 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.0 $4.$	13.5	0.1	13.3	4.2-3.0	0.1	13.2	4.0-2.9
14.5 0.1 13.5 $4.0-3.0$ 0.1 13.4 $3.9-3.0$ 15 $0,1$ 13.6 $4.0-3.0$ 0.1 13.5 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16 0.1 13.8 $3.9-2.9$ 0.1 13.7 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.7 $3.6-3.0$ 16.5 0.1 13.8 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.4 $4.0-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.4 $4.0-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21 0.1 14.9 $3.6-3.0$ 0.1 15.0 $4.0-3.0$ 22 0.1 15.1 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 22 0.1 15.2 $3.6-$	14	0.1	13.4	4.2-3.0	0.1	13.3	3.9-3.0
15 $0,1$ 13.6 $4.0-3.0$ 0.1 13.5 $3.9-3.0$ 15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16 0.1 13.8 $3.9-2.9$ 0.1 13.7 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.7 $3.6-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.1 $4.0-3.0$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.5 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.0$ 22 0.1 15.1 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23 0.1 15.0 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 24 0.1 14.9	14.5	U.1	13.5	4.0-3.0	0.1	13.4	3.9-3.0
15.5 0.1 13.7 $4.0-3.0$ 0.1 13.6 $3.9-3.0$ 16 0.1 13.8 $3.9-2.9$ 0.1 13.7 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.7 $3.6-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.3 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.2 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 22 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 22.5 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23.5 0.2 14.8 $4.$	15	0,1	13.0	4.0-3.0	0.1	13.5	3.9-3.0
16 0.1 13.8 $3.9-2.9$ 0.1 13.7 $3.6-3.0$ 16.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.3 $4.0-3.0$ 0.1 14.4 $4.0-3.0$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.5 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.1 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 22 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 24 0.1 14.9 $3.$	15.5	0.1	13.7	4.0-3.0	0.1	13.0	3.9-3.0
16.5 0.1 13.8 $3.6-3.0$ 0.1 13.8 $3.6-3.0$ 17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.1 $4.0-3.0$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.0$ 22 0.1 15.1 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 24.5 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 24.5 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 24.5 0.1 14.9 <td>10</td> <td>0.1</td> <td>13.8</td> <td>3.9-2.9</td> <td>0.1</td> <td>13.7</td> <td>3.0-3.0</td>	10	0.1	13.8	3.9-2.9	0.1	13.7	3.0-3.0
17 0.1 13.9 $3.6-2.9$ 0.1 13.9 $3.8-3.0$ 17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.1 $4.0-3.0$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.0$ 22 0.1 15.1 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 23 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 24 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 24.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.0$	10.5	0.1	13.8	3.0-3.0	0.1	13.8	3.0-3.0
17.5 0.2 14.1 $4.6-3.2$ 0.1 14.0 $4.6-3.2$ 18 0.1 14.2 $4.0-3.2$ 0.1 14.1 $4.0-3.0$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.1 $4.0-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.4 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.0 $4.0-3.2$ 0.1 15.1 $3.6-3.0$ 22 0.1 15.1 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 23 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 24 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 24.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.2$	1/	0.1	13.9	3.0-2.9	0.1	13.9	3.8-3.0
18 0.1 14.2 $4.0-3.2$ 0.1 14.1 $4.0-3.0$ 18.5 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 20 0.1 14.5 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.0$ 22 0.1 15.1 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 22.5 0.1 15.3 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 23 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 24 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 24.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.2$	17.5	0.2	14.1	4.0-3.2	0.1	14.0	4.0-3.2
16.5 0.1 14.3 $4.0-3.0$ 0.1 14.2 $3.9-3.0$ 19 0.1 14.4 $4.0-3.0$ 0.1 14.3 $3.9-3.0$ 19.5 0.1 14.5 $4.0-3.0$ 0.2 14.5 $4.0-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20 0.1 14.6 $3.8-3.0$ 0.1 14.6 $3.6-3.0$ 20.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 21 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 21.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.0$ 22 0.1 15.1 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 22.5 0.1 15.2 $3.6-3.0$ 0.2 15.3 $3.6-3.0$ 23 0.1 15.3 $3.6-3.0$ 0.2 15.5 $3.4-3.0$ 23.5 0.2 14.8 $4.0-3.2$ 0.1 14.7 $3.6-3.0$ 24 0.1 14.9 $3.6-3.0$ 0.2 14.9 $3.6-3.2$ 24.5 0.1 15.0 $4.0-3.2$ 0.1 15.0 $4.0-3.2$	10	0.1	14.2	4.0~3.2	0.1	14.1	3030
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	10.5	0.1	14.5	4.0-3.0	0.1	14.2	3030
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	19	0.1	14.4	4.0-3.0	0.1	14.5	4030
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20	0.1	14.5	38.30	0.2	14.5	3 6-3 0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20 5	0.1	14.0	1032	0.1	14.0	3 6.3 0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	20.5	0.2	14.0	3630	0.1	14.7	3632
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$21 \\ 21 5$	0.1	14.9	40.32	0.2	14.5	4 0.3 0
22.5 0.1 15.2 3.6-3.0 0.1 15.1 3.6-3.0 23 0.1 15.3 3.6-3.0 0.2 15.3 3.6-3.0 23.5 0.2 14.8 4.0-3.2 0.1 14.7 3.6-3.0 24 0.1 14.9 3.6-3.0 0.2 14.9 3.6-3.2 24.5 0.1 15.0 4.0-3.2 0.1 15.0 4.0-3.0	21.3 21	0.1	15.0	36.30	0.1	15.0	3 6-3 0
23 0.1 15.2 3.6-3.0 0.2 15.5 3.4-3.0 23.5 0.2 14.8 4.0-3.2 0.1 14.7 3.6-3.0 24 0.1 14.9 3.6-3.0 0.2 14.9 3.6-3.0 24.5 0.1 15.0 4.0-3.2 0.1 15.0 4.0-3.0	225	0.1	15.2	3 6-3 0	0.1	153	3 6-3 0
23.5 0.2 14.8 4.0-3.2 0.1 14.7 3.6-3.0 24 0.1 14.9 3.6-3.0 0.2 14.9 3.6-3.2 24.5 0.1 15.0 4.0-3.2 0.1 15.0 4.0-3.0	72	0.1 A 1	15.2	36-30	0.2	15.5	34.30
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	22 5	0.1	14.8	4 0.3 2	0.1	14 7	3 6.3 0
245 0.1 150 40-32 0.1 150 40-30	23.5	01	14.0	36-30	0.1	14 9	36.32
	24.5	0.1	15.0	4.0-3.2	0.1	15.0	4.0-3.0

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	Sample n	0:	Location	Lengt	h	HW/FW	Rock Type
	AG #1	500m	Cross-cut		4 . 43m	ны	Chlorite schist
	AG #2	500n	1 Cross-cut		1.90m	H₩t	🏎 Carbonaceous limestone
	AG #3	670m	Cross-cut		8.10m	HW	Carbonaceous limestone
	AG #4	350m	1 Cross-cut		7 . 30m	HW	Quartzite
	AG #5	320m	Cross-cut		4.00m	HW	Quartz sericite schist
	AG #6	350m	I Xcut substation		3.30m	FW	Gray limestone
	AG #7	200m	Cross-cut		5.20m	HW	Quartz sericite chlorite schist
	AG #8	Port	al: Charging Station	1	1.00m	FW G	luartz sericite schist
	AG #9A	DDH	83-15	0.00 -	18.30m	H₩	Sericite quartz schist + quartzite
	AG #98	DDH	83-15	18.30 -	32 . 34m	HW	• • • •
	AG #10/	A DDH 8	93-15	32.34 -	49 . 75a	HW	Chlorite sericite phyllite
	AG #101	B DDH 8	83-15	49.75 -	65 . 30m	HW	Chlorite phyllite + chlorite serici
te phylli	ite						
• •	AG #11	DDH 8	13-15	65.36 -	76.30m	HW	Quartzite + sericite quartz schist
	AG #12	DDH 8	83-15	76.30 -	78 . 40m	HW	Gray limestone
	AG #13	DDH 8	33-12	0.00 -	5.07m	FW	Grav limestone
	AG #14	DDH 8	33-12	5.07 -	28.46m	EW	Quartz sericite schist + sericite
quartz s	chist					• ••	
•	AG #15	DDH 8	13-12	78.46 -	40.53m	FW	Chlorite phyllite + chlorite cerici
te øhvili	te					• •	
	AG #16	DDH 8	33-12	40.53 -	54.92m	FW	Quartzite
1	AG #17	DDH 8	13-12	54.92 -	61.10m	FW	Chlorite sericite phyllite + quartzi
te						• ••	
	AG# 18	DDH 8	13-12	61-10 -	94.46a	FW	Chlorite phyllite + chlorite serici
te phylli	te + ser	icite q	uartz schist				
	AG #19	מאממ	3-12	94.46 - 10	0 7.46 m	FW	Quartz sericite schist + quartzite
	AG #20	DDH 8	33-12	107.46 - 1	21.73m	FW	Sericite guartz schist + chlorite p
hyllite							
•	AG #21	DDH 8	3-12	121.73 - 12	5.80m	FW (Grav limestone
	AG #22	DDH 8	13-12	125.80 - 13	35.83m	FW	Sericite quartz schist +/- chlorite
+ ainor	qzte						
	AG #23	DDH 8	13-12	135.83 - 13	39 . 50m	FW	Gray limestone
	AG #24	DDH 8	3-12	139.50 - 15	52.70m	FW	Quartzite + quartz sericite schist
+sericit	e quartz	schist					
	AG #25	DDH 8	13-17	0.00 -	16.23m	HW	Chlorite phyllite + sericite quartz
schist +	• quantz	sericit	e schist				
	AG #26	DDH 8	13-17	16.23 -	24.40m	HW	Quartzite + sericite quartz schist
	AG #27	DDH 8	3-17	24.60 -	49 01m	HW	Chlorite phyllite + sericite quart
z schist	+ quartz	serici	te schist				
	AG #28	DDH 8	13–17	49.01 -	52.70m	HW	Grav limestone + silicious limesto
ne						•	
	AG #29	DDH 8	3-17	57.00 -	61 . 57m	FW	Gray banded limestone
	AG #30	DDH 8	3-17	61.57 -	75.35m	F₩	Quartz sericite schist + quartzite
	AG #31	אממ	3-17	75,35 - 10)2.72m	FW	Sericite quartz schist + chlorite p
hvllite +	quartz «	ericite	e schist				
	AG #32	DDH 8	4-05	0.00 -	18 . 47m	ΗШ	Chlorite phyllite + quartz sericit
e pr Uite	2		_				
Y	AG #33	DDH 8	4-05	18.47 -	26.35m	ны	Gray limestone + dk gray limeston
2		_					,
			-				

AG #34 DDH 84-05	26.35 - 30.90m	HW	Sericite quartz phyllite + chlorit							
e sericite phyllite										
AG #35 DDH 84-05	30.90 - 40.48m	HW	Quartzite + quartz chlorite phylli							
te chlorite sericite phyllite										
AG #36 DDH 84-05	40.48 - 48.76m	НW	Chlorite sericite phyllite + quart							
z sericite phyllite + chlorite phyllite										
AG #37 DDH 84-05	60.05 - 77.69m	F₩	Quartz sericite phyllite + quartz							
chlorite phyllite + quartzite										
AG #38 DDH 84-05	77 . 69 - 89.90m	FW	Chlorite quartz phyllite + chlorit							
e sericite phyllite										
AG #37A DDH 84-09	0.00 - 18.25m	HW	Chlorite quartz phyllite + quartz							
chlorite phyllite										
AG #39B DDH 84-09	18.25 - 33.83m	HW								
AG #39C DDH 84-09	33.83 - 50.90m	HW								
AG #40 DDH 84-09	50.90 - 54.16m	HW	Quartzite							
AG #41A DDH 84-09	54.16 - 65.07m	ΗW	Quartz chlorite phyllite + chlorite							
quartz phyllite										
AG #41B DDH 84-09	65.07 - 77.54m	HW								
AG #42 DDH 84-09	88.20 - 109.12m	FW	Quartz sericite phyllite + quartz							
chlorite phyllite + chlorite quartz phyllite										

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Analytical Chemists * Geochemists * Registered Assayers

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To : EQUINOX RESOURCES LTD.

900 - 625 HOWE ST. VANCOUVER, BC V6C 2T6 Project : Comments:

**Page : [Tot. Lages: 2 Date :13-APR-89 Invoice # : I-8913667 P.O. # NONE

CERTIFICATE OF ANALYSIS A8913667

SAMPLE DESCRIPTION	PRE COD	P E	S % (Leco)	MAX POT ACID **	Neutral Poten**	PASTE pH						
AG-#1 AG-#2 AG-#3 AG-#4 AG-#5	208 208 208 208 208 208		0.715 1.670 0.197 0.216 1.860	2 2 5 2 6 7 5 8	30 358 800 112 37	7,9 8,3 8,4 8,9 8,5						
AG-#6 AG-#7 AG-#8 AG-#9A AG-#9B	208 208 208 208 208 208		0.011 0.255 0.529 0.448 0.651	0 8 16 14 20	985 42 45 26 24	8 . 8 9 . 1 8 . 2 9 . 1 9 . 2					*	
AG-#10A AG-#10B AG-#11 AG-#12 AG-#13	208 208 208 208 208		0.478 0.623 0.927 0.249 0.060	15 19 29 8 2	25 27 36 770 918	8.9 8.7 8.7 8.5 8.6					*	
AG-#14 AG-#15 AG-#16 AG-#17 AG-#18	208 208 208 208 208 208		0.479 0.165 0.158 0.303 0.302	15 5 9 9	50 28 30 29 22	9.0 9.0 8.8 9.0 9.0						
AG-#19 AG-#20 AG-#21 AG-#22 AG-#23	208 208 208 208 208 208		0.232 0.326 0.205 0.301 0.265	7 10 6 9 8	17 27 816 21 824	9.3 9.0 8.5 9.2 8.5						
AG-#24 AG-#25 AG-#26 AG-#27 AG-#28	208 208 208 208 208 208		0.613 0.703 0.250 0.807 0.693	19 22 8 25 22	27 25 99 29 780	9.0 8.9 9.2 9.1 8.6						
AG-#29 AG-#30 AG-#31 AG-#32 AG-#33	208 208 208 208 208 208		0.069 0.899 0.415 0.443 0.219	2 28 13 14 7	970 54 34 31 730	8.5 8.8 9.0 9.0 8.6						
AG-#34 AG-#35 AG-#36 AG-#37 AG-#38	208 208 208 208 208 208		0.750 0.267 0.420 0.785 0.216	2 3 8 1 3 2 4 7	50 108 19 40 32	9.0 9.2 9.0 9.0 9.1					, / ,	
NOTE: ** UNITS = TONS CACO3 EQUIVALENT PER THOUSAND TONS MATERIAL. ALL ASSAY DETERMINATIONS ARE PERFORMED OR SUPERVISED BY B.C. CERTIFIED ASSAYERS CERTIFICATION : N. M.												



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**Page [:2 Tot. 1 _ss:2 Date :13-APR-89 Invoice # :1-8913667 P.O. # :NONE

CERTIFICATE OF ANALYSIS A8913667

SAMPLE DESCRIPTION	PRE	P E	S % (Leco)	MAX POT ACID **	Neutral Poten**	PASTE pH			,		
AG-#39A AG-#39B AG-#39C AG-#40 AG-#41A	208 208 208 208 208		0.121 0.168 0.487 0.144 0.411	4 5 15 4 13	35 23 15 13 17	9 - 3 8 - 9 8 - 7 9 - 0 8 - 8					
AG-#41B AG-#42	208		0.367	1 1 3 6	35 37	9.0 8.7					
NOTE: ** UNITS = TONS CACOJ EQUIVALENT PER THOUSAND TONS MATERIAL ALL ASSAY DETERMINATIONS ARE PERFORMED OR SUPERVISED BY B.C. CERTIFIED ASSAYERS CERTIFICATION : M. C. M.											