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GEOPHYSICAL REPORT

INDUCED POLARIZATION/RESISTIVITY SURVEYS

DOME MOUNTAIN PROPERTY, SMITHERS AREA

OMINECA MINING DIVISION, BRITISH COLUMBIA

Latitude: 54° 45' N Longitude: 126° 39' W NTS 93L/10 & 15

on behalf of

TEESHIN REOURCES LTD. 100 - 581 Argus Road Oakville, Ontario L6J 3J4

Field work completed: September 12 to October 4, 1989

by seried from 6 ZC Alan Scott, Geophysicist 🗲 💁 SCOTT GEOPHYSICS LTD. 4013 West 14th Avenue 00 A. Vancouver, B.C. V6R 2X3 james franci ₹ 2. December 15, 1989 \bigcirc Ο 6 0 0 🔿 🕐 (L) (C) 5 4

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ACCOMPANYING MAPS

General Location Map	(body of report)		figure	1
	Plan (2nd separation) Plan (2nd separation)	1:5000 scale 1:5000 scale 1:5000 scale 1:5000 scale	figure figure figure figure	3 4

Chargeability and Resistivity Pseudosections

West side:	Lines	9500N	to	9800N	(n=1-5)	1:2000 scale	figure 6
West side:	Lines	9900n	to	10200N	(n=1-5)	1:2000 scale	figure 7
West side:	Lines	10300N	to	10600N	(n=1-5)	1:2000 scale	figure 8
East side:	Lines	9500N	to	9800N	(n=1-5)	1:2000 scale	figure 9
East side:	Lines	9900n	and	10000N	(n=1-10)	1:2000 scale	figure 10
East side:	Lines	10100N	and	10200N	(n=1-10)	1:2000 scale	figure 11
East side:	Lines	10300N	to	10500N	(n=1-10)	1:2000 scale	figure 12
East side:	Lines	10600N	to	10800N	(n=1-5)	1:2000 scale	figure 13

1. INTRODUCTION

Induced polarization and resistivity surveys were conducted over portions of the Dome Mountain Property, Smithers Area, B.C., within the period September 12 to October 4, 1989. The work was conducted by Scott Geophysics Ltd. on behalf of Teeshin Resources Ltd.

The pole dipole electrode array was used on the induced polarization surveys, with an "a" spacing of 20 meters. Readings were taken routinely at "n" separations of 1 to 5, but at "n" separations of 1 to 10 for portions of lines 9900N to 10500N.

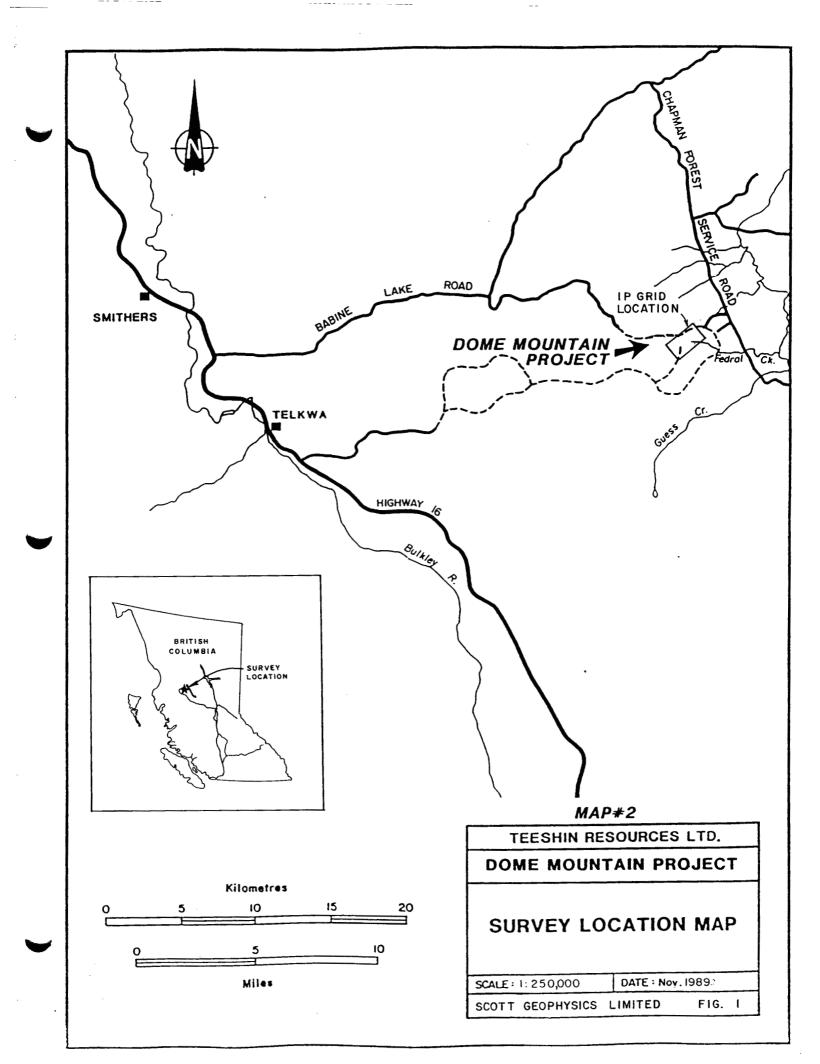
This report describes the instrumentation and procedures used on the surveys, and discusses the results obtained.

2. CLAIMS LOCATION AND ACCESS

The Dome Mountain Property is located some 31 kilometers east of Smithers, B.C. (location map - figure 1). Access to the vicinity of the claims is via the Chapman Forest Service Road. A four wheel drive access road to the survey area leaves the Chapman Forest Service Road at approximately kilometer 67.5. The induced polarization survey was conducted over portions of the following mineral claims:

Claim Name	Record No.	Claim Name	Record No.
Grizzly	1530	New York	1554
Josie	1531	No. 2	155 7
Telkwa	1533	No. 1	1559
Triangle Fr.	1537	Wallace	1560
Dome	1538	No. 4	1561
Vancouver	1539	Wallace Fr.	1562
No. 3	1540	Dome B	3566
No. 6	1541	Boo Fr.	3950
No. 5	1544	Boo 1	3951
Victoria Fr.	1545	Boo 2	3952
Freda	1546	Cope 1	4500
Trail Fr.	1547	Cope 2	4501
Elk	1552	Cope 3	4502
Bertha Fr.	1553	-	

Teeshin Resources Ltd., 100-581 Argus Road, Oakville, Ontario, L6J 3J4, is the recorded holder of the claims, subject to various agreements.



3. PREVIOUS WORK

Mineral occurrences on Dome Mountain were first staked in 1898. Considerable work, both surface and underground, was done in 1923 - 1924 by Dome Mountain Gold Mining Co. Little work was done after that until 1984 when Noranda Exploration Co. Ltd. optioned the claims and initiated a comprehensive program of geological, geochemical, and geophysical surveys, along with diamond drilling (Myers, 1986). This work is still in progress under the direction of MPD Consultants Inc.

4. PHYSIOGRAPHY

Dome Mountain is a glacially rounded summit that reaches an elevation of 1753 meters, and marks the most southeasterly alpine elevations of the Babine Range. The slopes of the mountain vary from gentle to steep, but cliffs are rare. The middle and lower slopes support stands of Balsam Fir, Spruce, and Pine, as well as a few deciduous species.

Several creeks, including Federal Creek and its major tributary, Boulder Creek, run all year.

5. GEOLOGY

Dome Mountain is on the Skeena Arch, near the southern edge of the Bowser Basin. The area is mainly underlain by Lower to Middle Jurassic eugeosynclinal volcanic and sedimentary rocks, which are cut by a few granitic to dioritic intrusions.

The geology has been mapped by Tipper (1976) and the regional geological setting discussed by Tipper and Richards (1976).

Quartz veins containing gold, silver, and pyrite occur in both volcanic and sedimentary rocks and are the principal exploration target. The "Boulder Zone" is the most promising such occurrence on the property found to date.

6. SURVEY GRID AND SURVEY COVERAGE

The location of the lines surveyed is indicated on accompanying figure 2. A total of 26.9 line kilometers of induced polarization survey was performed on the Dome Mountain Property, 22.9 kilometers at n=1 to 5, and 4.0 kilometers at n=1 to 10.

7. PERSONNEL

Ken Moir, technician, was the party chief on the survey and operated the IPR11 receiver. Tony L'Orsa, geologist, was the Teeshin Resources' representative on site for the duration of the survey.

8. INSTRUMENTATION AND PROCEDURES

A Scintrex IPR11 time domain, microprocessor based receiver, and a Scintrex 10 kw TSQ4 transmitter were used for the induced polarization survey. Readings were taken using a 2 second alternating square wave. The chargeability for the eighth slice (690 to 1050 milliseconds after shutoff; midpoint at 870 milliseconds) is the value that has been plotted on the accompanying plans and pseudosections.

The survey data was archived, processed, and plotted using a Sharp PC7000 microcomputer running Scintrex Soft II, IGS, and proprietory software. All chargeability responses were analyzed for their spectral characteristics (cole-cole intrinsic chargeability, time constant, and frequency dependence) using Johnson's curve matching procedure (Scintrex Soft II).

The pole dipole electrode array was used on the survey, with an interelectrode ("a") spacing of 20 meters. The current electrode was to the east of the potential electrodes on all survey lines.

9. DISCUSSION OF RESULTS

The results of the survey are presented as pseudosections of the chargeability and resistivity on accompanying figures 6 to 13, and as contour plans for the second separation on accompanying figures 3 and 4. Figure 5 is an interpretation plan showing the location of chargeability highs as defined from the pseudosections.

Chargeability highs have been categorized as defined below:

يتستقلع	strong	chargeability	high	
2272	moderate	chargeability	high	
	weak	chargeability	high	
	weak	chargeability	hìgh	(poorly defined)
	long time	e constant chai	rgeabi	lity high

The "n" separation at which the chargeability high has been interpreted is indicated with the anomaly bar (e.g. n=2,3).

Chargeability and resistivity measurements represent an averaged value of a large volume of materials, and the anomaly bars do not imply a width for the target. The probable axis for many of the anomalies has been indicated by a small vertical arrow on the pseudosections. However, the accuracy in choosing the center of a given anomaly is determined by the electrode spacing (20 meters in this case).

The primary objective of the induced polarization survey was to map the extent of the Boulder Zone (quartz/sulphide vein system), and to search for similar targets in the survey area.

The moderately strong, well defined chargeability high located at 10310 east on line 10600 north is coincident with the Boulder Zone and is taken as the target model for interpretaion of these results. This chargeability high is characterized by short (<1 second) time constants, suggesting a fine grained source, such as disseminated sulphides.

As indicated on the interpretation plan, a large area of moderate to strong chargeability response covers the southern portion of the survey area. The heavy dashed line outlines those responses which are characterized by long time constants (>10 seconds), and includes all but a few responses near the edges. Long time constants suggest that the source is coarse grained, and in particular, are often associated with graphitic sediments. This area is also associated with relatively low resistivity, which is also typical of graphitic sediments.

While this area cannot be eliminated as a possible host for quartz/sulphide vein systems, the much higher amplitude response from these (presumed) graphitic sediments, effectively masks the delineation of more subtle sulphide responses that may be present (within or below the sediments). However, ongoing correlation of these results to geological mapping and/or diamond drilling may help to define structures cutting the sediments, which could be important ore controls.

A zone of weak to moderate chargeability response, associated with short time constants, extends from line 10700N (10200E-10260E) to line 10100N (10440E-10680E). It is labelled as feature A on the interpretation plan. This zone includes the above mentioned response on line 10600N (10300E-10340E) over the Boulder Zone. Any untested chargebility highs within this zone are considered to be very high priority targets for diamond drilling. The zone may extend under the (presumed) sediments to the southeast, but any response to it is masked by the graphite within these sediments.

A weak, poorly defined, chargeability high is outlined on line 10400N to line 10500N at about 10270E, and is labelled as feature A' on the interpretation plan. Although it is very weak, given its proximity to the boulder zone, it is recommended for diamond dirlling. A weak to moderate chargeability high, characterized by long time constants, is outlined from line 10400N/10780E to 10600N/10880E, and is open to the northeast. It is labelled as feature B. The shape suggests a relatively narrow, steeply dipping feature, and may represent a southwest trending structure.

Feature C is a weak to moderate chargeability high, characterized by short time constants, located on line 10000N/10270E to line 9900N/10170E. It may lie along the same postulated southwest/northeast trending structure as feature B.

Feature D is a weak to moderate chargeability high, characterized by short time constants, from line 10200N/10340E to 10000N/9840E. This trend is somewhat speculative as the respnses on lines 10000N and 10100N are very near the contact to the sediments, and could represent sdieways viewing to those sediments. Further IP surveying to test this postulated west southwest trending structure is recommended prior to drill testing.

Feature E is a weak, poorly defined, chargeability high, characterized by short time constants. It extends from line 10300N/9200E and bifurcates to line 10600N/9050E and 10600N/9160N. It has a similar southeasterly trend to the Boulder Zone (feature A), and is open to the north. It would be masked (if present) by the sediments to the south. Further IP surveying to the north, and fill in surveying on lines 10350N and 10550N, is recommended prior to drill testing.

Features E, F, G, and H are all open chargeability highs, characterized by short time constants, that also require further IP survey prior to drill testing.

Short time constant chargeability highs occassionally occur at the periphery of the presumed sedimentary boundary (such as line 10300N/8950E, line 10100N/9580E, and line 10000N/9760E). These responses are considered to be too isolated to recommend for testing solely on the basis of time constant values.

Feature I defines the relatively discrete series of weak to moderate chargeability highs at the eastern boundary of the presumed graphitic sediments (line 9500N/11120E to line 9900N/11030E, and possibly line 10100N/10980E). This feature may represent a north/south structural boundary of the sediments, and is recommended for drill testing.

10. RECOMMENDATIONS

The induced polarization survey on the Dome Mountain Property detected weak to moderate chargeability highs that merit further investigation. These responses are discussed in the previous section, and are labelled on the interpretation plan as features A to I.

Any untested chargeability highs within Feature A, which includes the Boulder Zone, are considered to be very high priority targets for diamond drilling. Owing to its proximity to the Boulder Zone, Feature A' is also recommended as a drill target.

It is postulated that Feature B and C lie along a southwest/northeast trending structure. Feature B may be near enough to surface to test by trenching (strongest response at the 1st separation). Feature C is recommended for testing by diamond drilling.

Features D, E, F, G, and H all require further IP surveying prior to drill testing.

Feature I defines a relatively discrete series of weak to moderate chargeability highs at the eastern boundary of the presumed graphitic sediments. This feature may represent a north/south structural boundary of the sediments, and is recommended for drill testing.

The area outlined on the interpretation plan to the south and east of the heavy dashed line is characterized by moderate to strong chargeability response, long time constants, and low resistivity. Such response is typical of graphitic sediments. While this area cannot be eliminated as a possible host for quartz/sulphide vein systems, the geophysical response to any such systems present within or under the sediments, is effectively masked by the strong graphitic response.

These recommendations are made subject to correlation of these results to geological and geochemical information that may be available.

Respectfully Submitted,

ausil

Alan Scott, Geophysicist

References

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- Tipper, H.W., 1976, Smithers map area, British Columbia: Geological Survey of Canada, O.F. 351 (Geological Map).
- Tipper, H.W. and Richards, T.A., 1976, Jurassic stratigraphy and history of north-central British Columbia: Geological Survey of Canada, Bulletin 270.

Statement of Qualifications

I, Alan Scott, of 4013 West 14th Avenue, Vancouver, B.C., V6R 2X3, do hereby certify that:

- 1 I graduated from the University of British Columbia with a B. Sc. degree (Geophysics) in 1970, and with an MBA (evening program) in 1982.
- 2 That I am a member of the Society of Professional Engineers, Geologists and Geophysicists of the Province of Saskatchewan, the Society of Exploration Geophysicists, and the B.C. Geophysical Society.
- 3 That I have been practising by profession as an Exploration Geophysicist since graduation from the University of British Columbia in 1970.
- 4 That I supervised the geophysical work discussed in this report.

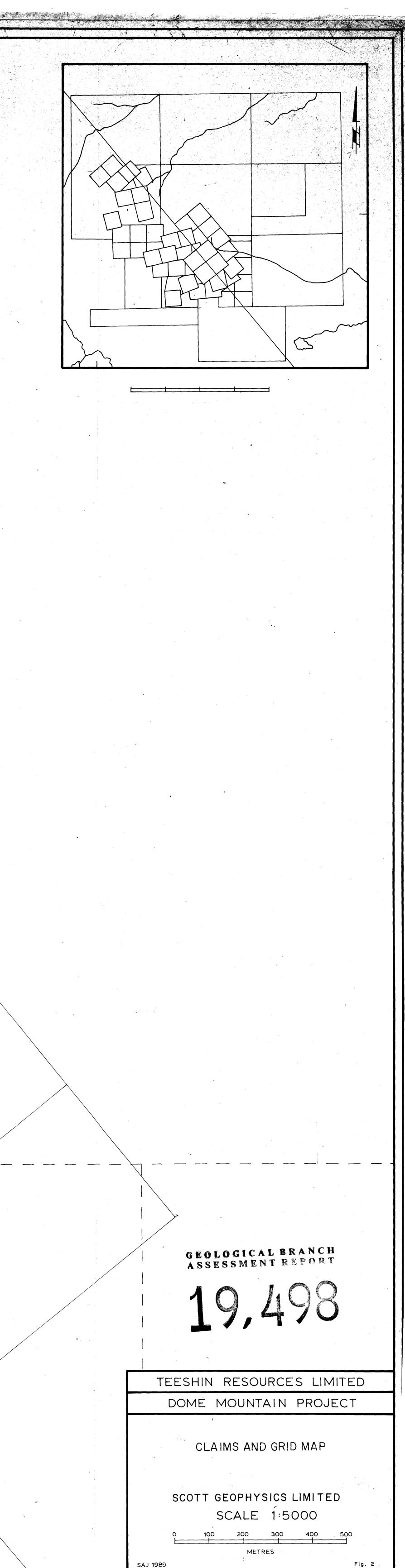
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Alan Scott, Geophysicist

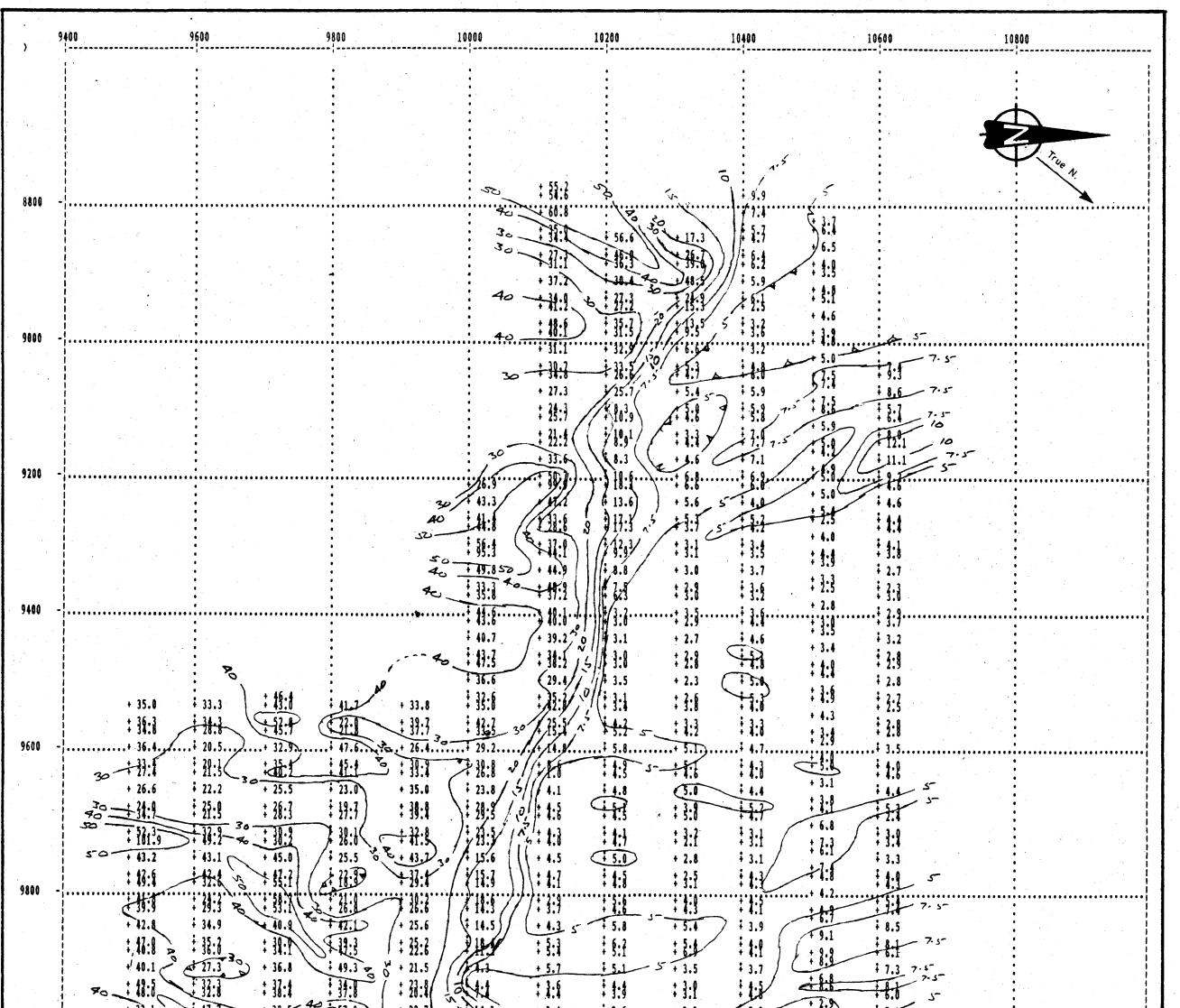
Statement of Costs

IP Survey:	20 field days @ \$1796.08/day	\$35,921.54						
	(Includes mob. and demob.)							
	Reports and interpretation	2,232.39						
Supervision: A. L'Orsa, geologist,								
	3 days @ \$300/day	900.00						
Vehicle:	Truck, 2 days @ \$50/day	100.00						
		\$39,153.93						

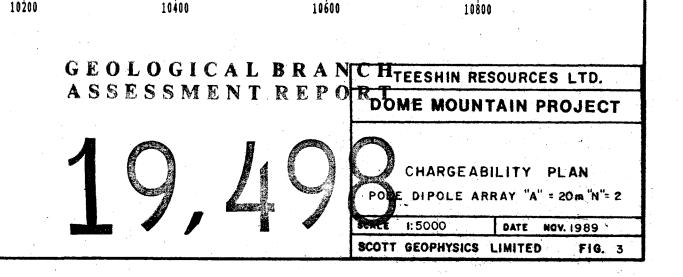




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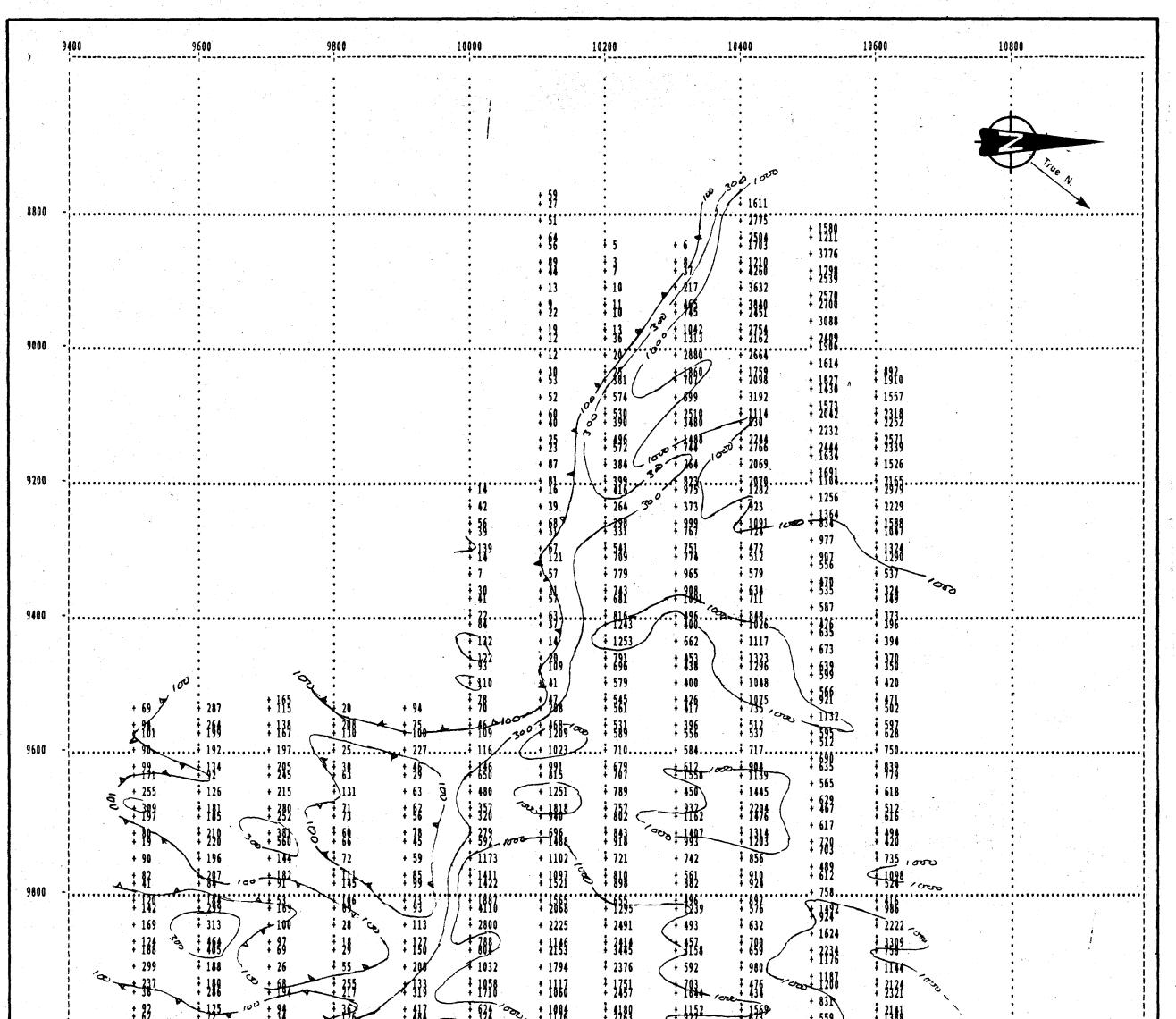


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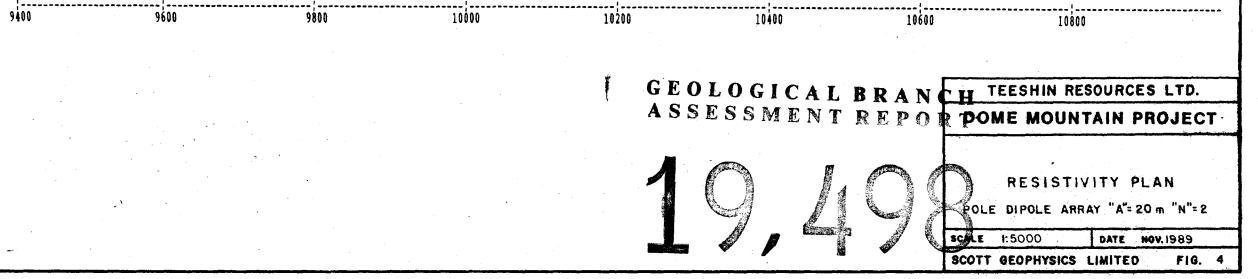


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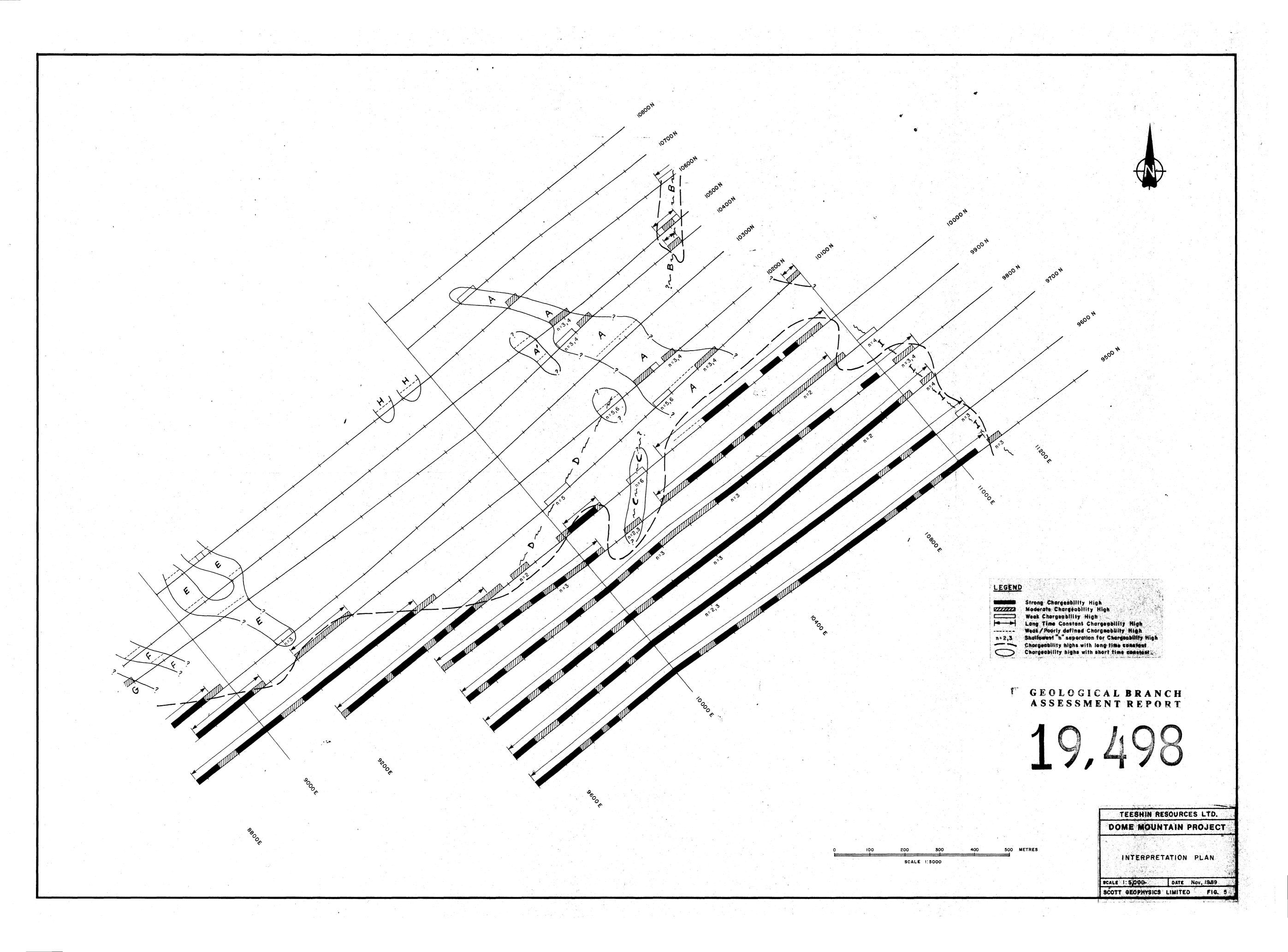
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10400 -	3-20 + 199	+ 116 + 75 + 117 + 85 + 130 - +	+ 108 + 29	278 ÷ 757	÷ 278 ÷ 242 + 310 ÷ 267 ÷ 299 • 299		+ 1079 + 1045 + 1078 + 1335 + 1773 + 1014	+ 11330 + 11023 + 072
20100	+ 534 + 485	+ 142 + 123 + 118 + 162	+ 149	+ 178 + 501	$ \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c}$	i 356i 534 i 441 + 275	+ 1723+ 1014 + 1523+ 569 + 550 + 859	
•		÷ 129 ÷ 159	÷ 118 ÷ 76	1 188/ 51110	÷ 1899 = ÷ 518	1978 - 1917	1911 115	÷ 533
•	+ 504	+ 182 + 190	+ 128 + 64	+ 228 + 1099	÷ 3750 ² + 525	+ 1431 + 3009	+ 1339 + 2478	423
	· /		1 - 69 - 107 100 -		3852	+ 3575 + 1978 + 3504 + 2647	- 1859 - 2887	
10600 -	+ 738 + 951 + 672	+ 196 + 156+ 175	· · · · · · · · · · · · · · · · · · ·	$\begin{array}{c c} & 1 \\ + \\ + \\ 1 \\ + \\ 1 \\ + \\ 1 \\ 1 \\ 1 \\$	÷ 2528 ÷ 1183 ÷ 2171	+ 2763 + 3728 + 1649 + 3728 + 2503 + 2167	+ 2600 + 1732 + 3969 + 2472 + 1616 + 1483	1192
TARAA	: 185 /		+ + + + + + + + + + + + + + + + + + + +		₩157 ÷ 828	+ 2503+ 2167 - 2973 + 3893	+ 1616+ 1463 + 2563 + 1463 + 3239 + 2776	+ 144/ = 2892 = 1835
	300 + 155	+ 188 + 99	+ 49 + 70	+ 194 3 + 518	÷ 863 + 1202		+ 3248 + 4080	÷ 1643
		+ 158 (a. 00 + 102 (c.)	· 78 0+ 101	· 227 : 519	333 6438	÷ 885 ÷ 795	÷ 2733 ÷ 2897	÷ 3133
	100 112	198 1199	*	1991 - + + + + +	+ 898	· 117 · 352 · Gro.		÷ 2634
	+ 163 + 191 + 217	$ \begin{array}{c} $	+ 62 + 114 + 197 + 197	+ 297 + 933 + 265 + 1548 ~~~	÷ 537 + 1331 ÷ 948 + 1474	+ 618 + 459 + 607 + 468 + 553 + 852	+ 623 (+ 1397 + 464 (+ 1542	
10800 -				203	+ 1146- + 1364	+ 553 + 852 + 1231 + 396	+ 433 (* 1542 + 50) + 75+	+ 2315 + 1958 + 3530
	+ 182	+ 123 + 89	+ 162 + 144	÷ 135 + 479	÷ 614 + 1949		+ 447 + 554	+ 3530 + 2570
	‡ <u>211</u> ‡ 178	· 118 - : 82	1111 100 + 112 m	+ 136 / + 354	+ 845 (+ 1722)	+ 862 + 1 <u>257</u>	÷ 398 + 721	∓ 1068 •
	+ 199 + 232 + 183 - 4	+ 76 + 62 + 52 + 59	+ 64 + 61 + 157	$\begin{array}{c} + 144 \\ + 126 \\ + 126 \\ + 127 \\ + 270 \\ \hline \end{array} $	م م	OE-S	0.5	oar
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11000 -	+ 33	+ 105 + 152 + 194	+ 155 + 140	+ 152	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •	• • • • • • • • • • • • • • • • • • • •
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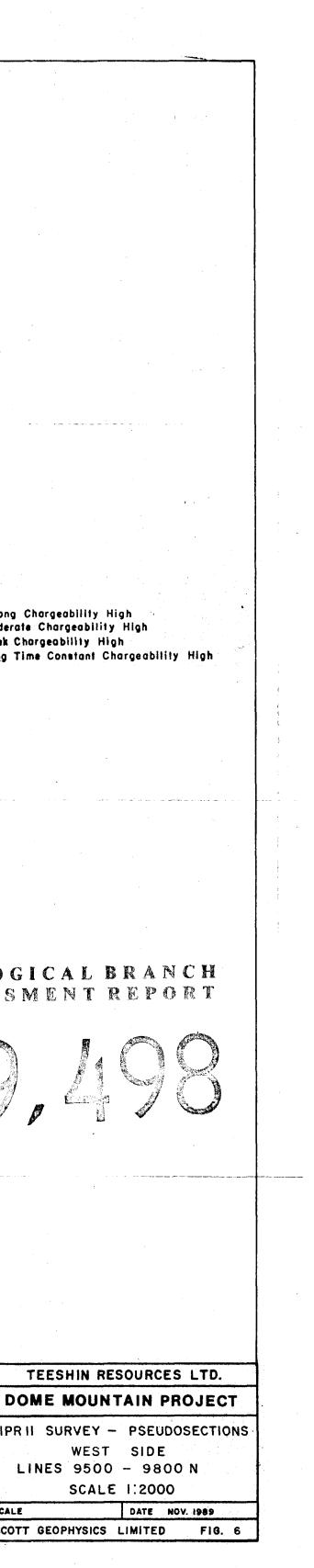


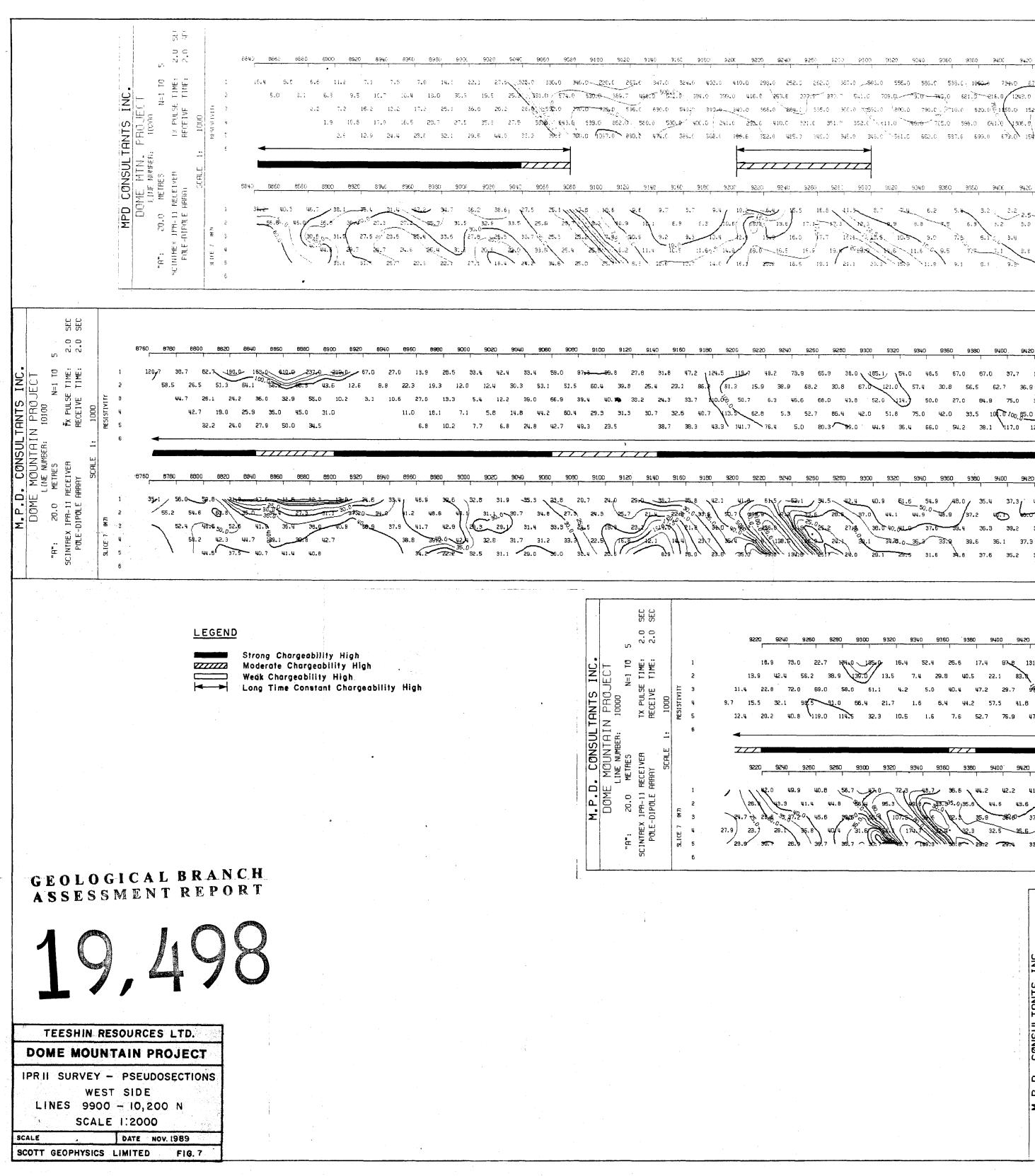
SEC 2.0 ŝ M.P.D. CONSULTANTS INC. DOME MOUNTAIN PROJECT LINE NUMBER: 9800 20.0 METRES N=1 TO EX IPR-11 RECEIVER TX PULSE TIME: E-DIPOLE ARRAY RECEIVE TIME: Jour N=1 TO TX PULSE TIME: RECEIVE TIME: 156.3 116.7 124.0 < 178.0 303.0 29.8 68.6 24.9 130.9 71.4 73.0 60.2 66.1 71.8 145.0 106 28.0 17.6 29.2 255.0 217.4 36.2 49.2 22.1 100.09 43.7 19.8 48.7 65.3 1050 47.7 70.4 42.6 61.2 75.6 00 22.6 64.2 72.4 56.2 (13).3, 87.9 80.3 21.5 59.9 25.9 59.1 32.9 73.7 SCALE n=2,3 9720 9740 9780 9760 "A": 20.0 CINTHEX IPA-11 F POLE-DIPOLE A 45.4 57.0 Ξ 3 55.8 -10.0 - ⁴⁰38.3 38.2 43.0 32.8 33.0 34.1 36.5 38.5 37.7 35620_34. 44.2 -24.7 46.9 49.2-49. * ۲۵۲۶ ۶ 32.2 33.8 32.2 36.9 33.2 35.3 38.0 37.6 36.3 43.2 47.4 37.8 36.5 4 6 SEC ۰. 5 2.0 2.0 M.P.D. CONSULTANTS INC. DOME MOUNTAIN PROJECT LINE NUMBER: 9700 "A": 20.0 METRES N=1 T0 SCINTREX IPR-11 RECEIVER TX PULSE TIME: POLE-DIPOLE ARRAY RECEIVE TIME: =1 T0 T1ME T1ME 500.0/ 372.0 389.0 215.1 280.4 251.9 3 380.6 560 ير الا 115.1 138.3 167.0 182.0 N=. TX PULSE T RECEIVE T 180. Cy 106.0 C 289.0 2233.0 277.0 278.0 212.0 190.0 256.0 353.0 235.0 107.0 58. 50.0 52.0 61.0 39.2 1153.6 157.0 128.0 1902 244.5 219.3 179.0 45.3 34.0 50.0 35.1 50. HE. 1 93.0~ ₹**7.**0 55.3 159.0 -807.0 ~289.0 80,7 155.0 171.9 103.0 312.0 148.7 179.0 48.2 75.8 182.3 9740 9760 9780 9800 9900 996D 43.0 40.3 52.8 45. 26.7 36.8 46.4 43.0 32.9 55.1 38.5 58.7 37.4 38.4 28.3 45.0 47.2 51.9 50.47.0 48.4 42.0 40.0 tony 37.1 <u>_53.</u>⊮ 31.4 27.2 33,9 44.4 41.8 37.6 <u></u>⊊94, 5 26.6 36-5.0 39.2 ં રૂ૩.૩ /38.6 3557 34.3 - 36.1 30.5 3326 × 42.5 27.4 42.7 47.3 38.4 (43.2 29/6 30.8 -24.8 27.2 30.7 33.1 ka.3 27.7 33.9 41.9 38.9 34.6 25.4 44.3 40:4 ۱_{31.1} SEC 5 2.0 2.0 sbuu N=1 TO TX PuLSE TIME: RECEIVE TIME: P.D. CONSULTANTS INC. OME MOUNTAIN PROJECT LINE NUMBER: 9600 3.0 METHES N=1 TO 110.7 102.4 159.0 276.0 204.0 325.0 202.0 181.3 185.0 210.0 220.0 193.9 287.0 264. 191.8 (91.5) 126.3 208. 240.0 44.0 68.0 153. 268.0 330.0 540,b 200.0 179.0 109.0 240.0 240.0 220.0 206.0 196.0 195.0 175.0 169.2 186.0 187.0 158.0 119.0 174.0 246.0 270.0 206.0 233.0 44.1 17.5 54.0 142 0 300.0 367.0 366.0 380.0 405.0 196.0 167.0 141.0 192.0 525.0 250.0 159.0 59.3 358.0 256.5 163.7 181.4 186.0 18.3 10.7 53.0 170.0 520.0 n = 2 RECI 22,2 24.9 21.2 16.0 13.2 2.0 11.1 11.6 24.9 45.2 43.9 8.4 🕰 35.7 26.9, 36.0 - 42.9 35.4/ 0 3 4 **Μ.** 00 "A": 20. CINTAEX IPA-POLE-DIPOL Ê 3 SLICE 7 5 f ក្ល 6 -----SEC 5 2.0 2.0 3660 9680 9700 9720 9740 9760 9780 9600 9820 9840 9860 M. P. D. CONSULTANTS INC. DOME MOUNTAIN PROJECT LINE NUMBER: 9500 20.0 METRES N=1 T0 EX IPR-11 RECEIVER TX PULSE TIME: EX IPR-11 RECEIVER TX PULSE TIME: TX PULSE TIME: RECEIVE TIME: 99.1 108-3 69.1 89.5 821 40.5 19.6 141 158.6 123.9 188.0 299.0 236 17 (5.7° (91.9 89.8 93.5 6 9540 9560 9580 9600 9620 9640 9660 9680 9700 9720 9740 9760 9780 9800 9820 9840 9860 9880 9900 9920 9520 RECE ARRA` "A": 20.0 SCINTREX IPA-11 POLE-DIPOLE 1 Ε. Ξ. s⊾ICE 7 ज ≓ 6

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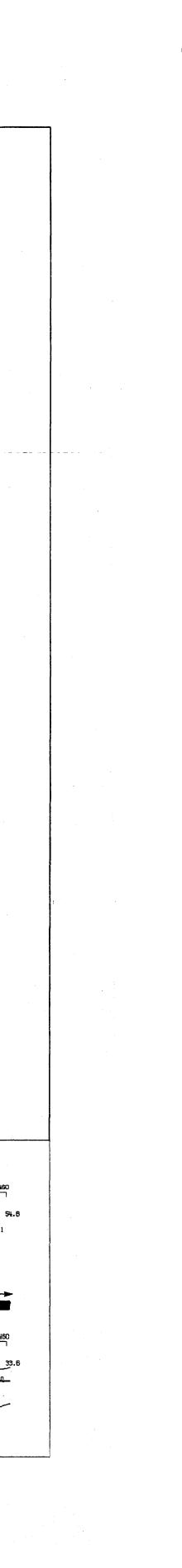
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4.5 6.5 7.8 6.9 6.3 4.2 4.0 3.1 4.7 4.5 4.4 2.2 3.4 3.3 2.7 2.5 2.0 2.4 2.4 2.2 2.8 3.8 3.3 3.8 3.5 2.1 2.5 2.9 3.0 2.1 2.8 4.0 4.6 7.2 6.2 6.3 3.6 3.7 3.1 3.8 9.7 9.6 8.6

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5.6 -2.1 1.6 -3.2 -2.9 2.9 3.6 -4.3 -4.1 -4.8 6.0 6.7 6.4 5.4 5.8 3.3 4.1 -3.6 -222 - 2.4 2.6 3.0 3.8 5.2 4.4 4.4 4.2 3.1 2.8 3.7 3.7 3.5 4.8 2.8 3.7 3.7 2.5 2.8 2.8 2.8 2.7 2.5 2.7 3.0 3.3 3.2 3.6 3.7 4.0 4.1 3.1 2.0 2.3 5.9 6.1 3.2 3.6 3.2 4.9 6.0 5.9 5.9 5.8 7.0 7.7 7.1 6.9 6.0 4.0 6.9 4.2 3.4 3.5 3.7 3.6 3.2 3.6 3.7 3.6 3.2 3.6 4.0 4.6 4

495.0 400.0 652.0 453.0 438.0 400.0 425.0 417.0 395.0 555.0 594.0 612.0 (1559.0) 490.0 932.0 1162.0 1407.0 955.0 594.0 612.0 (1559.0) 490.0 1120.0 935.0 743.0 561.0 (882.0) 496.0 (239.0) 498.0 457.0 896.0 (39.0) 498.0 (39.0) 498.0

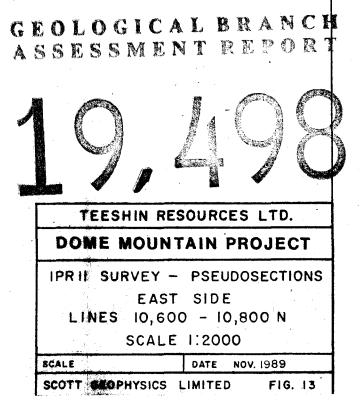
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3.1 2.8 1.7 2.3 2.1 2.3 2.6 3.4 4.6 4.0 5.8 5.3 2.7 2.7 2.5 2.5 3.1 4.0 4.3 5.4 5.4 6.9 3.5 3.0 3.1 5.5 5.8 5.4 5.7 7.9 5.6 5.9 4.5 4.4 3.7 3.4 3.2 4.0 4.0 3.5 2.6 3.3 2.4 2.0 3.5 4.3 5.5 5.8 5.4 5.5 5.8 5.4 5.5 5.6 3.4 3.8 2.3 4.6 4.8 5.5 6.7 6.2 7.1 5.4.1 4.0

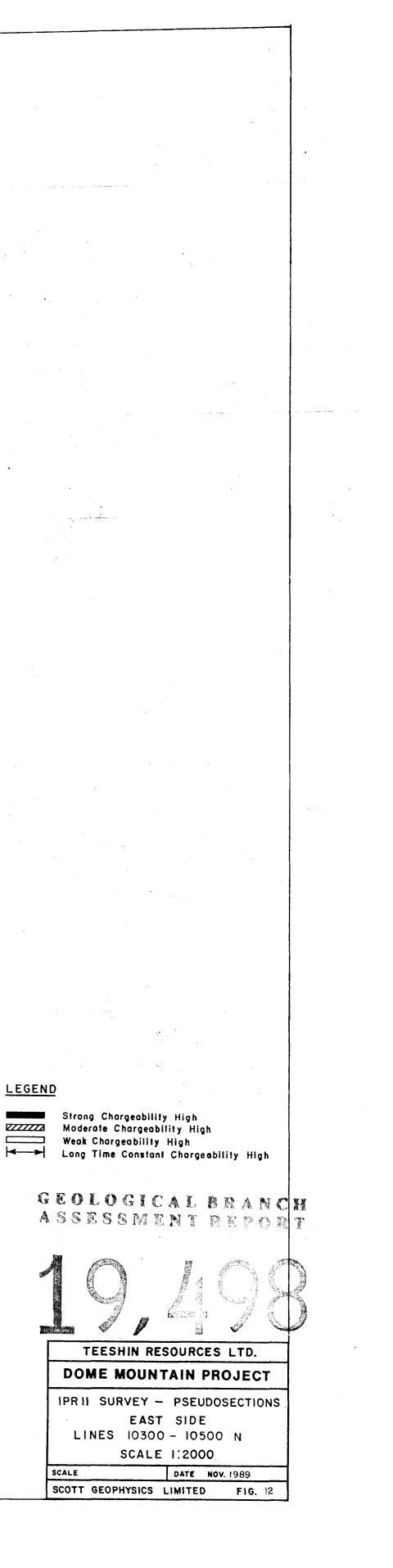
_____ 4.6 4.5 5.5 LEGEND Strong Chargeability High Moderate Chargeability High Weak Chargeability High Long Time Constant Chargeability High 1164.9. 2080.0 1856.0 1958.0 ----- -----7.9 10.0 , 2.0 .7 1.3 TEESHIN RESOURCES LTD. **DOME MOUNTAIN PROJECT** IPRII SURVEY - PSEUDOSECTIONS WEST SIDE LINES 10300 - 10600 N SCALE 1:2000 SCALE DATE NOV. 1989 SCOTT GEOPHYSICS LIMITED FIG. 8

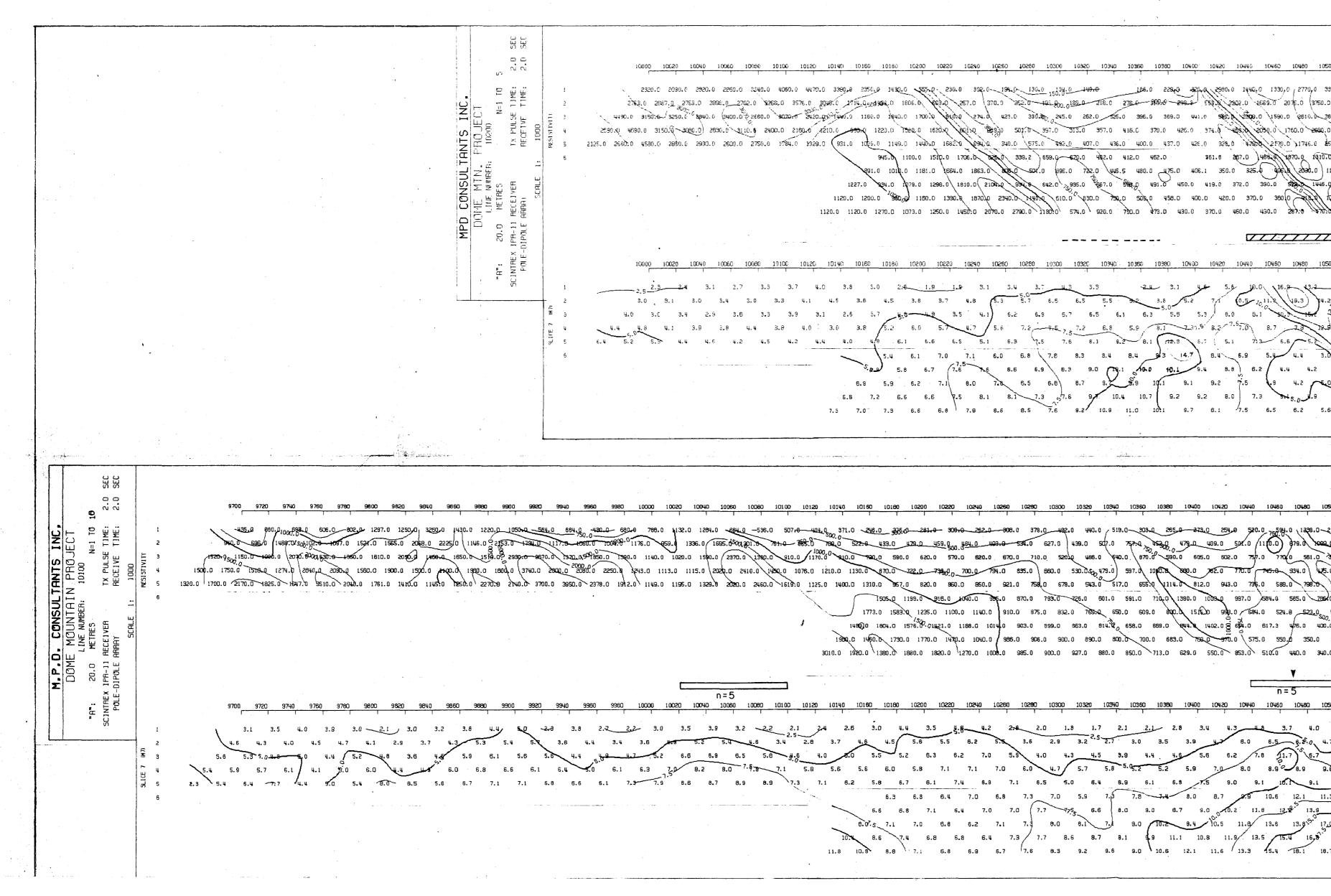
SEC SEC 5 2.0 2.0 10360 10380 10400 10420 10448 10460 10480 1056 460.0 260.0 234.0 224.0 214.0 242.0 204.0 253.0 318.0 358.0 263.0 315.0 385.0 639.0 113.0 1730.0 1250.0 792.6 501.0 474.0 285.0 324.0 228.0 273.0 357.0 605.0 821.1 1580.0 390.0 1730.0 1270.0 2200.0 2180.0 1940.0 1910.0 1910.0 200.0 1940.0 1910.0 190.0 1910.0 190.0 1910.0 190.0M. P. D. CONSULTANTS INC. DOME MOUNTAIN PROJECT LINE NUMBER: 10800 20.0 METRES N=1 TO =1 TO TIME: TIME: TX PULSE RECEIVE 1493.0 979.0 749.0 814.0 849.0 832.0 887.0 1053.0 1427.0 1705.0 1319.0 951.0 785.0 813.0 1479.0 2450.0 1494.0 1527.0 1920.0 1178.0 835.0 959.0 729.0 -763.0 1064.0 1419.0 2470.0 1671.0 2060.0 2104.0 200.0 3120.0 10020 10040 10060 10080 10100 10120 10140 10160 10180 10200 10220 10240 10260 10440 10460 10480 10500 10520 10540 10560 10580 10600 10620 10640 10660 10680 10700 10720 10740 10760 10780 10800 <u>10820</u> REC ARRI $2.8 \quad 1.8 \quad 1.9 \quad 3.0 \quad 3.3 \quad 2.3 \quad 1.5 \quad 1.5 \quad 1.8 \quad 2.8 \quad 2.7 \quad 2.5 \quad 2.6 \quad 2.7 \quad 3.5 \quad 3.9 \quad 3.7 \quad 3.1 \quad 1.9 \quad 1.3 \quad 1.5 \quad 1.5 \quad 2.0 \quad 2.3 \quad 2.8 \quad 3.3 \quad 4.0 \quad 3.2 \quad 3.3 \quad 4.4 \quad 3.5 \quad 4.3 \quad 3.6 \quad 4.4 \quad 3.7 \quad 3.9 \quad 3.4 \quad 2.8 \quad 2.8 \quad 3.7 \quad 3.4 \quad 2.9 \quad 4.1 \quad 3.5 \quad 4.3 \quad 3.6 \quad 4.4 \quad 3.7 \quad 3.9 \quad 3.4 \quad 2.8 \quad 2.8 \quad 3.7 \quad 3.4 \quad 2.9 \quad 4.1 \quad 3.5 \quad 4.3 \quad 3.2 \quad 2.4 \quad 2.8^{55} \quad 2.9 \quad 3.5 \quad 3.6 \quad 3.3 \quad 3.4 \quad 4.0 \quad 4.4 \quad 5^{50} \quad 6.6 \quad 4.3 \quad 4.0 \quad 2.6 \quad 2.0 \quad 2.1 \quad 2.6 \quad 3.1 \quad 4.0 \quad 4.1 \quad 5.4 \quad 4.8 \quad 5.6 \quad 4.3 \quad 4.1 \quad 5.2^{5.0} \quad 4.8 \quad 5.3 \quad 4.1 \quad 5.2^{5.0} \quad 4.8 \quad 5.3 \quad 4.1 \quad 5.2^{5.0} \quad 4.8 \quad 5.3 \quad 4.1 \quad 3.5 \quad 4.2 \quad 4.4 \quad 4.2 \quad 4.5 \quad 4.3 \quad 4.1 \quad 4.3 \quad 4.0 \quad 4.7 \quad 4.7 \quad 4.7 \quad 5.4 \quad 6.0 \quad 5.1 \quad 5.7 \quad 5.2 \quad 5.6 \quad 5.1 \quad 4.9 \quad 4.1 \quad 5.2^{5.0} \quad 4.8 \quad 5.6 \quad 5.3 \quad 6.1 \quad 5.7 \quad 5.2^{5.0} \quad 4.8 \quad 5.4 \quad 5.5 \quad 5.4 \quad 5.5 \quad 5.4 \quad 5.7 \quad 5.6 \quad 5.1 \quad 4.9 \quad 4.8 \quad 5.6 \quad 5.1 \quad 4.9 \quad 4.8 \quad 5.6 \quad 5.1 \quad 5.7 \quad 5.2^{5.0} \quad 5.9 \quad 5.4 \quad 5.6 \quad 5.1 \quad 5.7 \quad 5.2 \quad 5.9 \quad 5.9 \quad 5.4 \quad 5.8 \quad 5.4 \quad 5.8 \quad 5.$ 1.5 1.5 1.8 2.8 2.7 2.5 2.6 2.7 3.5 3.9 3.7 3.1 1.9 1.3 1.5 1.5 2.0 2.3 2.8 3.3 4.3 4.0 3.2 3.3 4.4 3.5 4.3 3.6 4.4 3.7 3.9 3.4 2.8 2.8 3.7 3.4 2.9 4.0 "A": 20.0 CINTREX IPR-11 POLE-DIPOLE SLICE 7 7:8 8.0 6.3 5.7 7.1 5.1 5.3 5.3 5.4 5.5 5.8 5.5 5.6 5.6 5.6 6.1 6.8 6.3 6.4 5:3 3.8 3.8 3.8 3.7 4.1 4.2 4.6 5.0 6.9 6.9 6.6 6.1 6.0 6.1 7.1 6.9 6.9 6.9 6.5 6.1 5.7 SEC SEC LEGEND 5 2.0 2.0 822.0 800.0 807.0 527.0 1224.0 100.0 500.0 276.0 300.0 500.0 276.0 301.0 527.0 301.0 527.0 301.0 527.0 500.0 =1 TO TIME: TIME: 822.0 800.0 897.0 CONSULTANTS INC. OUNTAIN PROJECT E NUMBER: 10700 N= TX PULSE T 1000 HESterr n = 2 10180 10200 10220 10240 10260 10280 10300 REC M. P. D. DOME 3.0 3.5 3.2 3.7 2.9 3.0 3.6 3.8 3.3 3.3 2.8 2.6 2.5 1.4 1.8 1.8 1.8 1.9 2.0 2.1 4.7 3.2 20.0 IPA-11 -DIPOLE 4.1 4.2 4.1 4.2 3.5 3.6 4.0 4.2 4.0 4.3 3.5 3.2 3.4 245 2.3 2.2 2.2 2.5 2.7 4.3 5.7 5.04.9 26.9 5.5 5.7 "A": SCINTREX POLE-I SLICE 7 6.7 5.9 6.3 6.2 5.5 6.5 7.6 8.4 8.3 9. SEC 2.0 2.0 - CONSULTANTS INC. MOUNTAIN PROJECT LINE NUMBER: =1 TO TIME: TIME: N= PULSE CETVE ΗŰ TITT -----10260 10280 10300 10320 10340 10360 10380 HEC ARRI M. P.D. DOME 3.3 2.7 <u>2.4</u> 2.2 2.7 3.3 3.5 3.3 3.8 3.3 2.9 2.7 3.4 <u>1.9</u> 3.0 <u>1.7</u> 1.9 2.1 3.1 3.7 6.2 9.6 12.1 1.6 4.2 3.5 3.0 3.2 4.1 4.1 <u>4.4 4.6 4.6 4.6 4.0 3.5 3.6 3.6 3.9 2.9 2.5 3.2 3.7 4.7 5.5 7.0 7.5.8.0</u> - 20.0 1PR-11 -DIPOLE 1 $\begin{array}{c} 3.5 \\ 10.2 \\ 3.5 \\ 3.5 \\ 10.2 \\ 3.5 \\ 10.6 \\ 11. \\ 10$ 13 9.1 6.0^{5.0} 5.1 4.6 4.5 5.5 S.0 4.7 4.1 3.9 3.6 3.4 2.8⁵ 2.9 3.4 4.9 5.6 "R": CINTREX POLE-5.4 6.3 6.0 4 33175 5 7.1 5.4 5.4 5.5 6.7 6.2 5.7

Strong Chargeability High Moderate Chargeability High Weak Chargeability High Long Time Constant Chargeability High

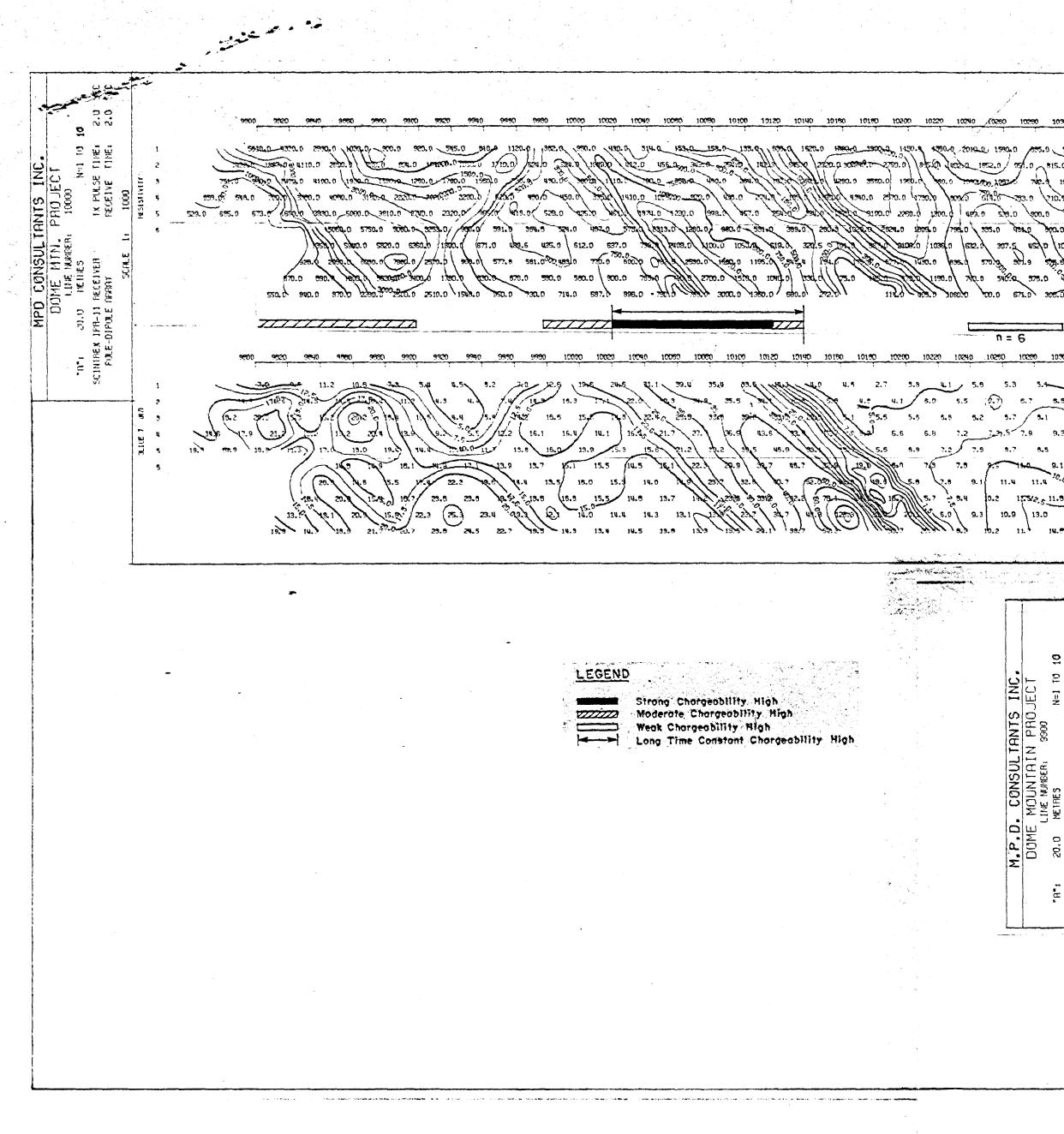


SEC 1**0** 2.0 2.0 200.8 -659.0 1760.0 1251.0 1973.0 2457.0 3260.0 2600.0 2380.0 2130.0 1510.0 1119.0 888.0 775.0 7940 0 522.0 459.0 468.0 85220 30045.0 396.0 846.0 1252.0 251,0 , 1820,0 267.0 597.0 571.0 598.8 639.7 775.0 835.0 1222 220.0) 2363.0 2829.0 2725.0 1946.0 2728.0 2476.0 2636.0 2459.0/ 1488.0 1380.0 942.0 634.0 330.9 274.5 278/1/2/20 3009.0 1978.0 2647.0 3334.0 3720.0) 2167.0 3002.0 1923.0 1923.0 1923.0 M. P. D. CONSULTANTS INC. DOME MOUNTAIN PROJECT LINE NUMBER: 10500 20.0 METRES N=1 TO =1 TO TIME: TIME: 2730.0 2610.0 2000.0 2110.0 2130.0 1640.0 1330.0 1420.0 1250.0 2000 298.0 243.0 430.0 3130.0 3130.0 3130.0 2000 1110.0 1030.0 4800.0 555.8 604.0 592,0 940.0 470.0 582.00 1176.0 1187.0 1200.0 831-0-941.0 1843.0 3190.0 2820.0 2830.0 2740.0 1750.0 2260.0 1830.0 1460.0 1460.0 1740.0 1570.0 736.0 234.0 37.0 174.0 1740.0 1 N=, JLSE T JLSE T 750.0 772.0 841.0 853.0 925.0 924.0 9530 rg0.0 2820.0 1510.0 1370.0 1370.0 0550.0 1140.0 1818.0 3380.0 2840.0 2890.0 2440.0 1533.0 1729.0 1294.0 1322.0 1605.0 1757.0 2130.0 1358.0 878.0 340.0 396.8 399.4 6930.0 3207.0 1900.0 2120.0 2280.0 1703.0 2170.0 1727.0 1810.0 1580.0 1720.0 2410.0 1260.0 1004.0 1153.0 1128.0 1051.0 1155.0 1093.0 1005.0 923.0 550.0 164.0 2080.0 1856.0 1958.0 2940.0 7647.0 1690.8 1268.0 хЩ 1090.0 1550.0 3820.0 2570.0 2480.0 2150.0 1290.0 1331.0 1210.0 1630.0 2080.0 1700.0 +380.0 878.8 1223.0 1020.0 1050.2 3840.0) 2230.0 2160.0 1760.0 968.0 1210.0 1470.0 1890/0 2390.0 1700.0 1930.0 1630.2 1000.0 1277.0 1130.0 1059.0 141030 2770.0 1920.0 1790.0 1272.0 874.8 1450 0 1670.0 (2210.0 1800.0 1920.0) 2190.0 1800.0 1330.0 1170.0 1170.0 (900.0 490.0 1580.0 1330.0 1180.0 1020.0 1800.0 1800.0 1670.0 2008.0 2100.0 2300.0 1610.0 1220.0 1200.0 1000.0 770:0 1020.0 1890.0 1200.0 1250.0 1380.0 1120.0 1940.0 1450.0 1960.0 2100.0 2240.0 "A": 20.0 CINTREX IPR-11 F POLE-DIPOLE F 7777777 _____ n= 3,4 10820 10280 10300 10320 10340 10360 10380 10400 3.9 3.2 2.6 2.0 2.7 3.3 3.9 4,3 3.4 4.0 2.7 2.4 4.0 4.6 4.1 3.7 <u>6.6</u> 3.6 3.7 3.5 4.0 6.5 1.65 2.2 7.9 10.0 6.0 5.7 6.2 6.3 4.6 3.7 3.7 4.4/ 8.9 (6.8) 8.8 2.8 1.2 1.6 killing out the 3.4 5.3 3.7 4.4 6.4 .6 5.2 6.5 6.4 6.6 7.5 6.9 6.4 6,4 5.6 9.6 8.8 8.2 9.3 1.5 4.0 3.2 3.8 5 6 2 1.4 6.6 6.2 6.8 4.6 3.8 5.9 4.3 4.8 5.8 6.7 6.6 6.8 3 7.7 2.9 3.1 3.9 4.1 4.6 5.5 5.1 6.8 7.5 103 4.7 2.0 2.3 (6.6 6.S - 5.75 8.4 9.4 8.6 2.6 13:9 4.6 3.7 6.3 V4.9 / 5.2 5.9 6.6 6.9 8.3 8.2 7.9 10.4 11.0 14.6 15.5 15.7 3.9 6.2 8.5 9.6 5.2 5.2 5.7 5.0 7.8 7.2 11.0 1.9 2.9 2.7 4.1 3.7 2.9 8. 9¹ 15,0 15.9 16.1 8.2 8.5 11.2 12.) 12.5 12.6 5.5 16.2 8.4 8.6 7.9 8.3 8.5 9.4 8.4 8.8 .9 .9 .43.0 13.1 .515.4 16.2 8.3 8.1 7.9 8.4 8.0 8.4 8.0 8.2 8.9 9.8 10.5 13.5 13.7 16.0 6.3 6.9 7.3 8.3 8.3 8.2 8.2 7.8 8.5 9.7 10.4 11.1 13.8 13.6 ខ្លួន 2.0 2.0 10 376.0 479.0 868.0 623.0 554.0 303.0 -248.0 390.0 1540.0 2100.0 2530.0 1970.8 2040,0 1310.0 2470.0 1640.0 1376.0 750.0 433.0 164.0 185.0 =1 TO TIME: TIME: N PROJECT 862.0 (950,0 353.0 1500,0) 1220.0 1340.0, 1370.0 2390.0 2440.0 2950.0, 2810.0 2110.0 2330.0 1360.0, TX PULSE RECEIVE 2012 0 105.0 1070.0 1410.0 1300.0 1310.0 220.0 2710.0 2350.0 2970.0 2450.0 2170.0 2450.0 2170.0 2450.0 2170.0 2450.0 1570.0 2450.0 1570.0 2450.0 1570.0 2450.0 1570.0 2450.0 1570.0 2450.0 1570.0 2450.0 1570.0 1157.0 825.0 1414.0 525.0 1414.0 1525.0 1414.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1414.0 1525.0 1525.0 1525.0 1525.0 1525.0 1525.0 1525.0 1525.0 1525.0 1525.0 1525.0 15 1050,0 473, 0 13210:0 100,0 1280.0 1300.0 1650.0 1480.0 1570.0 2490.0 2910.0 2170.0 2580.0 2488.0 1560.0 1570.0 868.0 1700.0 1461.0 1580.0 2241.0 16000 280,0 576.0 800,0 1860.0 1860.0 1260.0 260.0 260.0 260.0 1860.0 1260.0 1163.0 Jane Jok of puese 1503.0 1230.0 1670.0 1610.0 17190.0 2620.0 2450.0 2050.0 2547.0 1690.0 1400.0 1075.0 1154.0 (1967.0 1680.0) 1478.0 2480.0 2010.0 2010.0 2010.0 2010.0 1580/0 1090.0 1172.0 1045.0 1389.0 \$ 10424 (100.0 1481.0 1244.0 1244.0 1486.0 1536.0 2310.0 2310.0 2310.0 2022.0 1740.0 1540.0 1298.0 4170.0 1538.0 14110 2650.0 2338.0 4230 261.0 569.0 - 269.0 1396.0 1420.8 1400,0 1400,0 1400,0 1400,0 1400,0 1400,0 1400,0 150,0 160,0 120, 1490 10 11931 0 3700 0 1020.0 1510:0 1230.0 1680.0 1250.0 +130.0 1990.0 1500.0 1105.0 1220.0 1230.0 1500.0 1303.0 1800.0 1830:0 2650.0 2190.0 390.0 360.0 360.0 360.0 360.0 ¥ IIIII VIIII n=3,4 10340 10360 10380 10400 H2.9.19.1 5.9 8.3 6.8 7.9 7.9.3 4.5 5.6 6.9 **.**8 7.2 4.1 7.4/ 14.4///3.5 4.9 3.6 3.5 4.3 4.3 6.3 _ 6.3 9.6 (.5 5.0).8 $\begin{array}{c} 9 \\ 9 \\ - 9$ 8.0 0 11.3 ng 3, 10 2 14 30 20 10 5.6 6.4 6.2 4.2 🔥1 4.2 4.4 5.8 6.8 6.8 3.6 5.4 6.1 6.2 4.4 4.0 5.0 5.0 5.0 0.0 4.2 4.7 5.2 5.7 5.7 5.3 5.8 6.5 6.2 (8.7 9.2 10.0 8.8 13.9 11.0 H2.5 6.1 7.6 8.7 8.3 5.7 6.9 6.7 6.9 947 0.0 11.1 10.6 13.5 11.8 12.0 4.1 4.2 4.6 5.2 5.9 6.1 tyge 5.2 5.5 5.4 4.5 4.7 5.2 6.0 5.6 6.6 6.6 7.2 7.3 7.6 7.9 10.4 11.0 A2,5 11.1 13.8 11.9 12.3 is by bed / 6.9 6.9 3.3 14.2 and 5.3 5.8 5.7 5.04.9 5.1 5.8 6.7 6.9 7.9 7.9 7.1 7.9 8.3 8.6 10.8 11. 3 12.5 11.0 3 14.1 12.1 12.2 7.0 7.1 7.1 ⁽, 8, 5 λ**,**β SEC SEC 10 2.0 2.0 LEGEND M.P.D. CONSULTANTS INC. DOME MOUNTAIN PROJECT LINE NUMBER: 10300 20.0 METRES N=1 TO EX IPR-11 RECEIVER TX PULSE TIME: l=1 TO TIME: TIME: 1350.0 1002.0 871, 8 526, 0 280, 0 213.0 215.0 315.0 318.0 560.0 322.0 387.0 311.0 179.0 153.0 159.0 223.7 259.3 324.4 244.2 372.0 361.0 584.0 805.0 752.0 1027.0 857.0 31.0 429.0 620.0 429.0 620.0 429.0 620.0 429.0 1082.0 857.0 311.0 129.0 152. 270 1327.0 1192.0 270 1327.0 1192.0 270 1327.0 1192.0 270. 192.0 291.0 780.0 554.0 554.0 353.9 407.0 518.0 730.0 374.1 (500.0 411.0 296.300.919.0 666.0 524.0 655.0 1652.0 1102.0 409898.0 412.0 823.0 666.0 679.8 4331.0 4630.00 4364.0 1088.0 4088.0 (1949.0 1722.0 IU3UU N= IX PULSE 1 RECEIVE 1 390, 0 1250.0 1180.0 1060.0 940.0 150.0 1060.0 940.0 150.0 1000.0 300.0 (1942, 9 365.0 1370.0 (834.0 639.0 719) 361,0 1360,0 149.0 961,0 1360,0 149.0 130.0 130.0 149.0 582.0 779.0 840.0 \$285.0 \$430.8 (12.0 \$100.0 1259.0 \$68.0 140.0 1259.0 \$68.0 140.0 1259.0 \$68.0 140.0 1148.0 \$148.0 140.0 \$572.0 \$112.0 \$21.0 1054.8 \$572.0 \$112.0 \$21.0 1054.8 \$572.0 \$112.0 \$21.0 1054.8 \$572.0 \$112.0 \$21.0 1054.8 \$572.0 \$112.0 \$21.0 1054.8 \$572.0 \$112.0 \$21.0 \$100.0 \$1863.0 \$100.0 \$1863.0 \$100.0 \$1863.0 \$100.0 \$1863.0 \$100.0 1023.0 1420.0 1680.0 1250.0 1297.0 398.0 780.0 633.0 762.0 701.0 (119.0 794.0 171.0 1201.0 766.0 574.0 540.0 539.0 760.0 916.0 1050.0 1101.0 1290.0 762.0 1658.0 1157.0 1230.0 1157.0 1230.0 1157.0 1230.0 1157.0 1230.0 111.0 1230.0 111.0 1230.0 111.0 1230.0 111.0 1136.0 1574.0 1049.0 11157.0 1230.0 111.0 1136.0 1574.0 1049.0 1057.0 1359.0 1415.0 1230.0 1415.0 159.0 111.0 1134.0 1299.0 1904.0 "A": 20,0 M SCINTREX IPA-11 REC FOLE-DIPOLE ARR 1940.8 1960.0 1390.0 1460.0 1440.0 140.0 1700.0 1120.0 1170.0 800.0 834.0 910.0 990.0 1140.0 1720.0 1160.0 1650.0 1700.0 150.0 654.0 554.0 1510.0 10140 10160 10180 10200 10220 10240 10260 10280 10300 10320 10340 10360 10380 10400 10420 10440 10460 10460 10500 10520 10540 10560 3.0 3.2 2.9 2.8 2.9 2.3 1.6 1.4 2.5 2.4 2.2 2.7 2.0 2.4 2.4 2.4 2.6 2.8 3.1 4.2 4.3 3.8 3.8 5.5 4.2 3.9 4.4 3.8 4.4 3.5 2.8 2.9 3.3 3.4 3.4 3.1 3.4 4.9 5.6 6.2 6.3 - 4.7 6.1 7.0 8.4 1.8 3.3 3.0 .3 3.1 3.1 2.6 4.0 3.7 4.6 5.1 6.2 6.4 5.5 6.0 6.9 6.4 5.8 6.5 5.9 6.0 8.4 4.4 3.5 4.4 4.3 0 6.9 7.5.8 7.3 6.7 5.8 7.5 7.2 7.6 3.9 2.8 3.2 2.1 3.1 3.7 3.6 2,9 3.4 3.2 1.3 3.5 3.9 3.6 4.4 3.8 3.8 4.7 4.5 5.7 6.1 6.1 6.9 7.8 6.8 6.4 7.7 7.5 7.6 6.7 6.9 5.7 5.4 5.3 6.3 (8.7 8.3 7.0 8.3 8.6 8.5 `র_০4.1 4.0 3.5 3.3 × 6.2 7.1 4.7 5.8 5 5.3 6.5 7.0 7.5 8.0 8.5 8.7 9.0 8.7 9.7 19.0 8.1 B.0 9.0 9.2 9.1 5. 3^{°,0} 4. 9 5.4 5.4 5 5.8 5.1 5.2 5.4 5.2 5.8 3.2 7.3 6.⁶ 7.2 1.3 1.⁵7.7 7.9 8.1 8.4 9.2 9.4 9.2 9.3 9.3 9.7 9.8 8.3 8.3 9.2 8.0 5.9 5.3 5.4 6.3 5.8 6.6 7.7 · .3 · 7.8 7.9 8.5 8.2 8.7 9.0 9.5 9.6 9.2 9.2 8.8 9.5 **^1**0.0 8.1 8.3





156.0 228.0 325.0 1740.0 1930.0 2770.0 3350.0 2000.0 1960.0 1960.0 1700.0 1700.0 1540.0 1033.0 551.0 430.0 549.0-2783.0 2887.0 2753.0 2888.0 2702.0 2265.0 3576.0 370.0 256.0 114.0 505.0 278.0 370.0 255.0 4490.0 3150.5 / 250.0 300.0 3150.5 / 250.0 3020.0 3020.0 3020.0 300.0 10 250.0 460.0 3150.0 2000.0 2150.0 2000.0 2150.0 210.0 2000.0 2150.0 210.0 2000.0 2150.0 2125.0 2600.0 4580.0 2880.0 2880.0 2800.0 2750.0 1784.0 1245.0 1245.0 1149.0 1447.0 1212.0 401.0 1447.0 1212.0 1040.0 18220 100.0 407.0 400.0 407.0 400.0 407.0 400.0 407.0 400.0 407.0 400.0 407.0 400.0 407.0 400.0 407.0 400.0 407.0 400.0 407.0 400.0 40 361.8 207.0 466 0 1870.0 1910.0 1830.0 2470.0 1977.0 1311.0 1390.0 873.0 1420,0 -4270.0 945. 1100.0 1510.0 1706.0 820 0 339.2 659.0 620.0 482.0 412.0 462.0 291.0 1010.0 1181.0 1664.0 1863.0 805.0 501.0 896.0 722.0 445.5 480.0 475.0 406.1 350.0 325.0 096.4 2030.0 1178.0 200.0 2634.0 1575.0 1200.0 1199.0 971.0 1860.0 1079.0 1298.0 1810.0 2101.0 994.8 642.0 395.0 \$67.0 \$49.0 491.0 450.0 419.0 372.0 390.0 1446.0 1190.0 1454.0 1990.0 1440.0 1171.0 1290.0 1210.0 1227.0 334.0 1120.0 1200.0 1160.0 1300.1 10.00 1390.2 1870.0 2340.0 140.0 610.0 130.0 130.0 500.0 400.0 458.0 400.0 420.0 370.0 380.0 120.0 120.0 120.0 130 1120.0 1120.0 1270.0 1073.0 1250.0 1450.0 200.0 2790.0 1180.0 574.0 920.0 780.0 430.0 430.0 370.0 460.0 430.0 287.0 120.0 120.0 1150.0 1230.0 1870.0 1440.0 1440.0 _____ n = 3,4 10000 10020 10040 10060 10060 10060 10060 10100 10120 10140 10160 10180 10200 10220 10240 10260 10320 10340 10360 10360 1040 10460 10480 1050 10520 10540 10560 10560 10560 10660 10660 10660 10760 10760 10760 10760 10760 10800 10820 10840 10860 108 ye 5.8 10.0 16.0 13.2 12.4 7.2 3.6 4.0 5.9 3.8 4.0 H.7 5.2 4 49 5.6 5.9 5.8 5.0 5.4 8.1 8.5 3.1 ~____3 Elly 5.8 3.3 4.1 4.5 3.6 4.5 3.8 3.7 4.8 5.3 5.7 6.5 6.5 5.5 3.2 3.6 5.2 7.1 (0.5 + 20, 11.2) (19.3) (4.2 14.7) 10.0 11.9 11.9 (0.0) 3.3 3.9 3.1 2.6 5.7 4.9 3.5 4.1 6.2 6.9 5.7 6.5 6.1 6.3 5.9 5.3 8.0 8.1 40.7 15.7 400 13.2⁴⁹ 5.11.5 11.5 8.6 7. 3.8 4.0 3.0 3.8 5.2 6.0 5.7 4.7 5.6 7.2 7.5 7.2 6.8 5.9 8.1 2.37.5 8.2 7.57.0 8.7 2.3 12.9 11.7 14.7 2516.5 11.5 6.8 6.2 5.5 6.6 6.1 7.5 (6.9 5 7.8 6.2 7.) 6.8 6.5 20 20 4.0 5.6 6.2 7.1 8.3 8.5 8.0 8.2 7.0 6.6 7.9 E.8 E.5 5.1 5.8 2.5 8.0 8.6 LEGEND 4.2 4.5 4.2 4.4 4.0 4.8 6.1 6.6 6.5 5.1 6.3 7.5 7.6 8.1 9.2 8.1 (12.3) 8.7 (5.1 713 6.6 5.2 11.7 12.6 6.1 7.0 Strong Chargeability High Mederate Chargeability High 5.8 = 5.8 = 6.7 5.8 = 6.7 7.6 7.7 7.5 7.5 7.5 7.8 7.5 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.5 7.8 7.6 7.8 7.5 7.8 7.8 7.5 7.8 7.5 7.8Weak Chargeability High \$ 5 NO.6 12 13.4 13.6 5 15. 15 13. 30 Lang Time Constant Chargeability High 13.2 13.2 13.6 Ages e a وللسمي ومحال المراجع والمراجع بوريتيليكي الشاميديكريا المستعمولية ال GEOLOGICAL BRANCH ASSESSMENT REPORT 1505-0 1199.0 916.0 1040.0 396.0 870.0 793.0 226.0 601.0 591.0 710,0 1390.0 1009-0 997.0 584.0 585.0 2860 305.0 404.0 635,0 1990.0 1790.0 1790.0 2030.0 306.0 1773.0 1583.0 1235.0 1100.0 1140.0 910.0 875.0 832.0 765.0 609.0 609.0 800.0 1516.0 998.0 584.0 524.8 523.0 542.0 288.0 402.8 962.0 1950.0 1820.0 1780.0 1850.0 1850.0 11480.0 1850.0 1850.0 1820.0 1780.0 1850.0 11480.0 1950.0 1820.0 1780.0 1850.0 1950.0 1850.0 1950.0 1820.0 1780.0 1850.0 1850.0 1950.0 1850.0 1850.0 1950.0 1820.0 1780.0 1850.0 1950.0 1850.0 1950.0 1850.0 1950.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1950.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1950.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1850.0 1950.0 1850.0 1850.0 1950.0 1950.0 1850.0 1950.0 1850.0 1950.0 1950.0 1950.0 1850.0 1950.0 1850.0 1950.0 1850.0 1950.0 1950.0 1850.0 1950.0 1850.0 1950.0 1850.0 1950.0 1950.0 1950.0 1950.0 1850.0 1950.0 1 1980,0 1460.0, 1730.0 1770.0 1470.0 1040.0 986.0 906.0 900.0 890.0 800.0 700.0 683.0 750.0 575.0 550,0 350.0 370.0 500.0 500.0 190.0 1960.0 1590.0 3010.0 1920.0 1380.0 1880.0 1820.0 1270.0 1000.0 985.0 900.0 927.0 880.0 850.0 713.0 629.0 550.0 853.0 510.0 440.0 340.0 374.0 520.0 297.0 420.0 1010.0 1810.0 n= 3,4 TITI 10120 10140 10160 10180 10200 10220 10240 10260 10260 10300 10320 10340 TEESHIN RESOURCES LTD. 6.0 , 7.4 4.8 5.0 5.5 5.9 5.2 6.8 6.8 7.8 8.3 10.2 15.1 A 4.9 5.2 5.6 5.1 5.3 5.7 6.3 6.6 8.0 DOME MOUNTAIN PROJECT 15.0 11.8 11.3 13.4 15.1 18.0 15.9 19.0 13.8 10.4 7.3 IPRII SURVEY - PSEUDOSECTIONS 6.3 6.8 6.4 7.0 6.8 7.3 7.0 5.9 7.3 7.8 7.4 8.0 8.7 P.9 10.6 12.1 11.3 12-3 12.8 13.9 14.3 15.6 16.0 18.4 16.1 EAST SIDE 13.9 14.2 14.7 6.6 6.8 7.1 6.4 7.0 7.0 7.7 775 6.6 8.0 9.0 8.7 9.0 10.2 11.8 12.8. 16.1 16.3 16.9 19.6 LINES 10,100 and 10,200 N 8.0°.5 7.1 7.0 6.8 6.2 7.1 7.3 8.0 8.1 7. 9.0 10.2 9.4 10.5 11.8 13.6 13.8 17.0 16.2 15.8 15.3 15.7 17.0 17.1 10. 8.6 7.4 6.8 6.8 6.4 7.3 7.7 8.6 8.7 8.1 9 11.1 10.8 11.9 13.5 15.4 16.8 19.0 16.9 17.1 17.4 17.3 17.2 18.0 SCALE 1:2000 11.8 10.8 8.8 7.1 6.8 6.9 5.7 7.6 8.3 9.2 9.6 9.0 10.6 12.1 11.6 13.3 15.4 18.1 18.7 19.3 17.8 17.8 17.0 17.2 17.6 SCALE DATE NOV. 1989 SCOTT GEOPHYSICS LIMITED FIG. 11

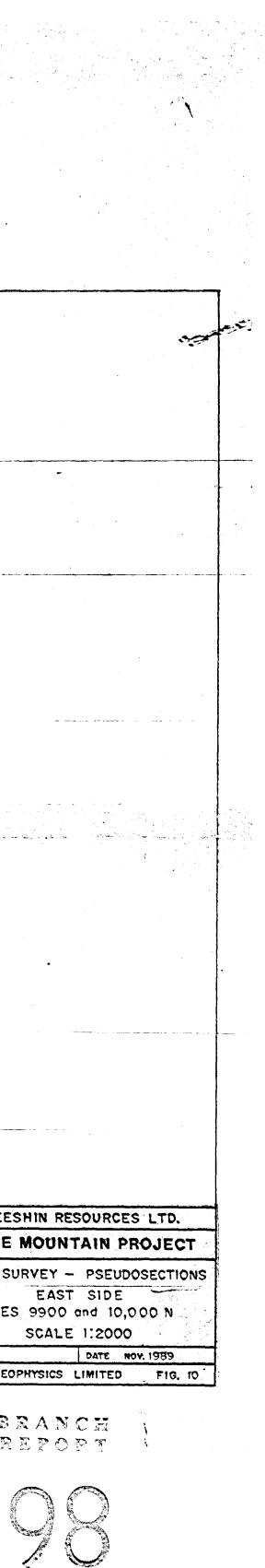


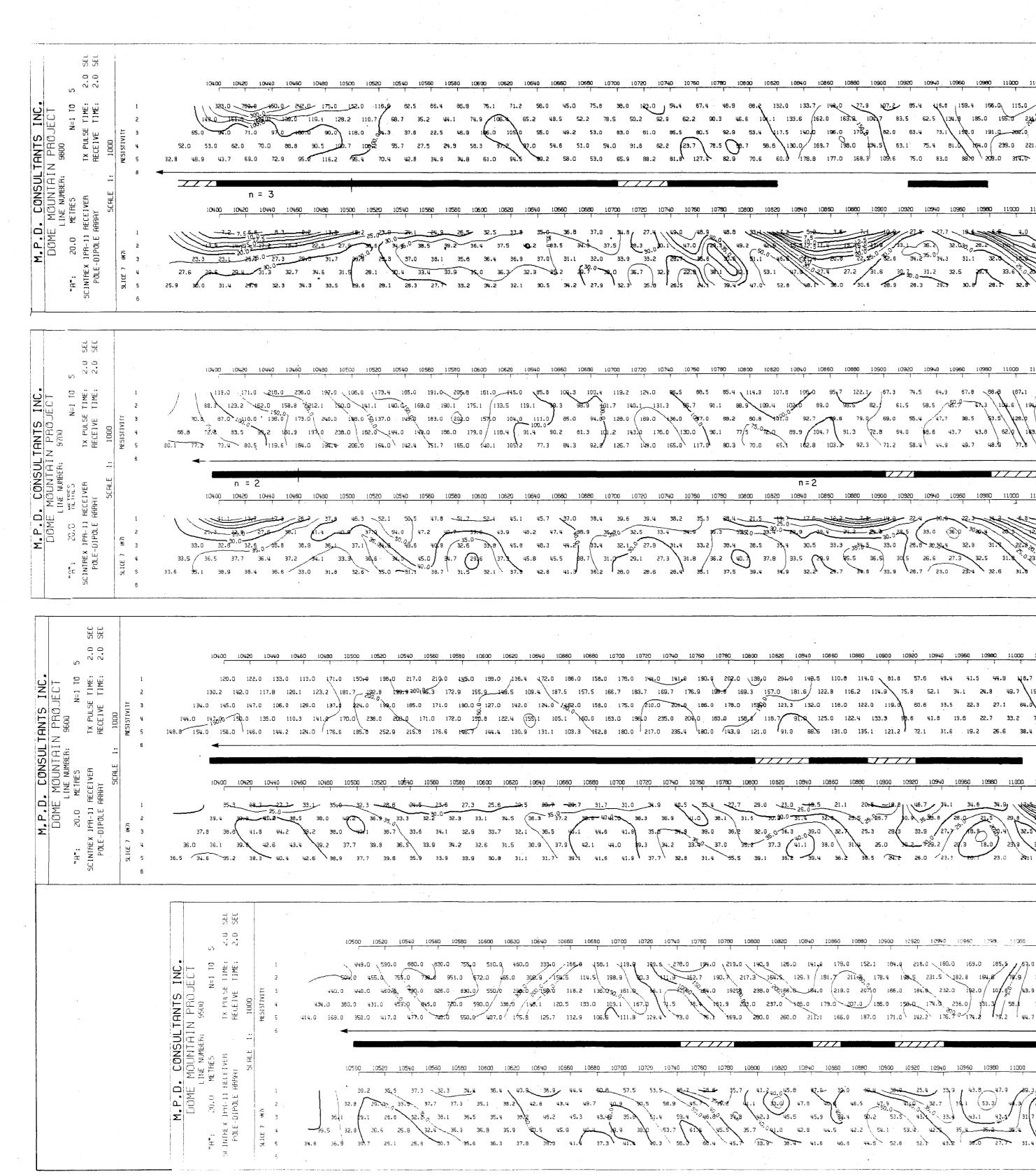
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10940 10560 10680 10700 10720 10740 10760 10780 10800 108 ---n = 6 m=7-10420 10440 10460 10450 10500 10520 10540 10590 10590 10500 10620 10640 10560 10660 10700 10720 10740 10750 10760 10500 10520 .8 4.1 5.8 5.3 5.4 J.F 6.0 5.5 (0.7) 6.7 5.9 5.7 3.1 4.4 - 4.4 5.4 5.0 5.0 5.0 - 2.3 5.4 - 4.0 5.7 1.2 23× 2.5 22 ----البصابية الدابي والمستهد والمتحدات ۵۵۰۰ (۲۰۰۰) ۲۰۰۰ ۲۰۰۰ (۲۰۰۰) ۲۰۰۰ (۲۰۰۰) ۲۰۰۰ (۲۰۰۰) and a second SEC 10 2.0 2.0 TANTS INC. IN PROJECT 3900 N=1 T0 1X PULSE TIME: RECEIVE TIME: 13.5 19.7 31.1 54.8 75.5 75.0 132.0 123.4 132.1 105.0 114.0 126.0 70.4 75.4 125.4 134.9 138.0 96.0 114.0 98.0 130.0 : 16.1 20.0 13.6 31.1 76.4 64.0 80.5 106.5 (^{100.10}, 78.4 82.3) 127.3 130.6 70.4 89.6 100.8 124.6 120.6 113.6 106.8 125.3 126.1 22.8 23.7 21.2 12.0 47.0 73.0 53.2 50.8 119 52.0 50.0 96.0 154.0 122.0 77.4 91.5 \$124.0 128.0 145.0 121.0 133.0 147.0 134. 25.5 32.2 23.2 20.5 18.9 46.0 76.5 73.9 51.6 73.0 52.0 61.0 104.3 148.9 135.5 78.0 61.0 136.0 136.0 157.0 151.0 143.0 35.4 37.7 26.9 36.0 21.0 49.3 85.9 78.9 77.1 67.0 54.8 71.7 97.0 (176.0 134.0) 78.7 88.8 137.0 157.0 191.0 187.0 186.0 20 44.1 24.6 56.9 194.8 72.2 73.3 21. 25.7 74.7 10.2 154.3 29.5 74.5 194.6 134.9 204.9 203.9 216.1 212.3 J L E 63.8 NJ.9 24.6 67.6 97.6 17.0 x05.2 96.2 65.6 79.6 114.2 171.7 NUL2 82.6 146.9 15.7 217.2 247.8 239.6 10.3 112.4 P.1 93.8 69.3 64.2 2120.5 174.4 15303 (20.5 2120.1 189.7) 260.4 278.0 290.5 94, 6 124.0 19570 251.0 326.0 37.8 73.5 147.0 104.0 0203.0 100.0 16.1 90.0 121.0 174.0 164.8 16. 92.0 88.0 100 13.9 12.2 106.6 137.0 106.0 111.0 109.0 82.0 10480 10500 10520 10540 10560 10580 10600 10620 10640 10660 10680 10720 10740 10760 10780 10800 1082 36.3 37.4 37.4 42.5 324 30ng 28.1 26.3 25.6 25.8 3200 139.0 39.1 33.5 5, 2 37.5 40.0 38.2 31.2 29.5 26.1 25.7 25.9 25.5 29.4 28.0 32.4 33.2 35.9 38.7 37.1 31.3 28.5 25.7 25.1 24.9 34.7 36.6 37.1 32.9 30.5 31.0 31.2 36.9 35.5 30.4 28.5 25.4 24.5 29.1 42.5 37.1 33.4 28.5 33.1 35.3 33.8 32.5 28.8 29-2 32.3 35.8 35.8 35.8 30.3 28.5 44.6 24.2~ 35.5 42.5 8 37. 7 31. 27.5 331.7 35. 34.6 23.1 27.1 28.4 31.1 35.9 37.9 39.3 27.3 324.1 23.8 36.5 42.9 35.9 35.7 26.5 35.1 59.1.7 Jau. 5 31.3 26.1 28.0 2.3 a 31.9 35/2 7.8.3 27.2 23.9 25,8 26.4 26.9 96. 43.4 39.6 29.8 21.0 0.1 33.5 27.9 28.0 24.9 27.8 30.1 34.5 34.4 29.4 28.3

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ASSESSMENT REPORT





132.0 133.7 144.0 77.9 h07.2 85.4 4,6.8 159.4 166.0 115.0 161.4 127.2 550.0 376.0 , 683.0 78.5 50.2 92.9 62.2 90.3 46.6 10.1 133.6 (162.0 163.2 104)7 83.5 62.5 (134.8 185.0 155.0 24.8 150.0 117.6 124.1 161.0 135.4 77.0 10+34800.0000. T 583.0 858.0 1457.0 179190/ 224.0 261.0 294.4 343.1 413.0 582.0 52.0 53.0 62.0 116 n = 3,4 $\frac{1}{3} + 1 + 24 + 265}{31.6} + 35.0 + 36.8 + 37.0 + 4.0 + 2.0 +$.3.7 3.6 $r_{s}6.5$ 3.78 1.8 1.4 1.7 (2.7 2.5 3.1 3.4 3.3 3.4 3.7 4.1 77.0 35.0 37.0 $113.8 \\ 152.0 \\ 185.0 \\ 290.0 \\ 334.0 \\ 257.0 \\ 336.0 \\ 230.0 \\ 270.0 \\ 230.0 \\ 270.0 \\ 291.0 \\ 337.0 \\ 337.0 \\ 391.0 \\ 601.0 \\ 601.0 \\ 601.0 \\ -206.0 \\ 960.0 \\ 2050.0 \\ 1310.0 \\ 870.0 \\ 1160.0 \\ 100.0 \\$ 88.5 85.4 114.3 107.8 106-0 95 7 122.1 67.3 74.5 67.8 88.8 167.1 187.0 105.0 -93.0 64.9 88.3 123.2 LE2.0 158.8 2312.1 100.0 141.1 140.0 169.0 190.1 175.1 133.5 119.1 90.3 95.9 40.1 71.0 100.0 110. n=4 n = 2 1.8 129 1.8 1.9 +9:7 17.6 122 24 00.9 22.3 H2 6.8 2.8 -25.0 1.5 1.5 1.5 1.4 1.8 1.9 2.2 2.1 2.0 2.2 1.7 2.8 2.7 2.6 2.8 3.5 95820 33.4 30.5 33.3 33.6 28.8 30.0 28.8 30.0 28.8 30.0 28.8 30.0 28.8 30.0 28.8 30.0 28.8 30.30.4 32 2.8 2.0 2.2 .3 1.9 2.4 2.5 2.8 2.4 2.7 2.2 2.7 3.4 3.6 3.3 4.1 4.9 3.8 224 2.9 2.9 2.5 3.1 3.1 3.3 3.6 3.6 4.0 4.1 766.0 980.0 870.0 120.0 169.0 148.0 114.0 110.0 105.0 102.0 103.0 121.0 219.0 - 219.0 - 249.0 - 249.0 - 219.0 - 413.0 413.0 n=3 11060 11080 11100 11120 11140 11160 11180 11200 2.4 1.9 1.6 2.5 2.6 2.3 2.0 2.4 2.5 1.2 1.0 1.3 1.7 1.7 2.3 2.2 1.6 2.2 2.2 2.2 2.3 2.6 2.5 2.3 2.7 1.3 1.9 2,4, 2.4 2.4 2.1 2.0 2.3 2.9 3.2 2.5 1.0 1.5 1.5 1.5 2.3 1.7 2.4 2.5 2.3 2.5 2.1 1.8 2.6 3.4 3.1 5.7 5.2 4.7 2.3 2. 7.5 7.6 4.4 3.5 2.0 1.7 1.7 2.2 2.5 2.3 2.6 2.4 2.4 2.3 3.5 3.3 2.7 .:)60 11080 11100 11120 11140 11160 11180 11200 11220 11240 11260 200.0 163.5 185.3 153.0 167.0 144.0 138.0 274.0 370.0 400.0 610.0 680.0 770.0 -735.0 827.0 804.0 141,0 179.0 152.1 184.0 218.0 160.0 169.0 185.5 157.0 29.4 90.5 105.7 180.0 198.1 308.9 /154.5 114.5 198.9 0.3 11.9 162.7 190.7 217.3 164.5 129.3 (181.7 21163 178.4 198.5 231.5 182.8 164.8 /9.9 33.3 29.5 75.5 115.5 199.2 (232.1 226.3 247.0 276.0 284.0 468.00 594.0 664.0 690.0 946.0 942.0 826.0 914.0 786.0 515.0 297.0 364.0 1922 238.0 3166. 0 144.0 (219.0 207/0 166.0 184.8 232.0 192.0 / 10/.8 43.9 26.8 34.3 32.0 99.9 471.0 243.0 310.0 310.0 310.0 350.0 360.0 500.0 760.0 760.0 910.0 910.0 840.0 1.5 18. 19. 5 18. 19. 0 237.0 186.0 179.0 207.0 186.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 150.0 578.0 330.0 50.0 442.0 460.0 40.0 40.0 40.0 40.0 40.0 40.0 570.0 5 280.0 260.0 211:1 166.0 187.0 171.0 142.2 176.7 0 174.2 179.2 44.7 32.1 - 31.0 46.8 205.5 347.0 498.0 462.0 600.0 550.0 540.0 480.0 670.0 700.0 840.0 732.0 844.0 -776.0 863.0 494.0 367.0 777777 n = 3 10900 10920 10940 10960 10980 11000 11020 11040 11060 11080 11100 11120 11140 11160 11180 11200 $\begin{array}{c} 89.3_{35,0} + 0.7 \\ 33.6 \\ 31.4 \\ 27.3 \\ 20.7 \\ 40.2 \\ 31.4 \\ 27.3 \\ 20.7 \\ 40.2 \\ 31.6 \\ 31.4 \\ 27.3 \\ 20.7 \\ 40.2 \\ 37.6 \\ 10.2 \\ 37.6 \\ 10.2 \\ 37.6 \\ 10.2 \\ 37.6 \\ 10.2 \\ 10.$ 42. 3 45.5 45. 7.8 40 **(** 46) 45.9 **(** 3.5 2.8 3.2 (43.1 43 1.6 2.8 3.4 3.6 2.9 3.1 2.3 2.4 3.3 3.3 3.1 2.4 4.5 5.3 53.4, 42.5 35<u>4 35.2 35</u>.4 42.8 _**42.2 ∖ 54.1** ′ 44.5 30.0 27.7 3.1 3.0 2.22.5 2.6 4.8 5.7 £.EE 52.1 52.6 38.4 41.6 46.8 43.2

