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GEOLOGICAL, GEOCHEMICAL and
DIAMOND DRILLING REPORT
ON THE HANK PROPERTY
BALL CREEK AREA, BRITISH COLUMBIA
LIARD MINING DIVISION

NTS : 104 - G / 1 & 2

North Latitude: $57^{\circ} 15'$
West Longitude: $130^{\circ} 30'$

FOR

LAC MINERALS LTD.
1050-1055 West Hastings Street
Vancouver, B.C.
V6E 2E9

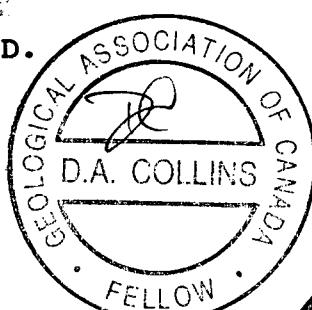
BY

DENIS A. COLLINS, Ph.D., P.Geol., F.G.A.C.

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1500-609 Granville Street
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JANUARY 1990



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TABLE OF CONTENTS

	<u>Page</u>
1.0 SUMMARY	i
2.0 INTRODUCTION	1
2.1 Objectives	1
2.2 General Location and Access	2
2.3 Operations and Communications	2
2.4 Physiography	4
2.5 Claim Status and Ownership	5
3.0 REGIONAL HISTORY	6
4.0 REGIONAL GEOLOGY AND MINERALIZATION	9
5.0 PROPERTY GEOLOGY	14
5.1 Stratigraphy	14
5.2 Alteration	18
5.3 Mineralization and Veining	19
5.4 Structure	22
6.0 DIAMOND DRILLING	30
7.0 GEOCHEMISTRY	39
8.0 CONCLUSIONS	40
9.0 REFERENCES	43



LIST OF FIGURES

		after page
Figure 1:	General Location Map.	2
Figure 2:	Claim Map.	5
Figure 3:	Regional Geology Map.	9
Figure 4:	Property Geology Map 1:5000 . .	in Pocket
Figure 4a:	Property Geology Map 1:2000 . .	"
Figure 4b:	Property Geology Map 1:2000 . .	"
Figure 4c:	Property Geology Map 1:2000 . .	"
Figure 5:	Schematic block diagram of the Hank 2-4 fault scarp. . . .	22
Figure 6:	Schematic bookshelf model for half-graben formation	23
Figure 7:	Stereoplot of creek 10 fault and creek 8 veins and lower zone data	29
Figure 8:	Diamond Drill Hole Locations. .	in Pocket
Figure 9:	Schematic diagram of types of potential mineralization. . . .	41

LIST OF APPENDICES

- APPENDIX I: Statement of Qualifications
- APPENDIX II: Geochemical Preparation and Analytical Procedures
- APPENDIX IIIa: Rock Sample Descriptions
- APPENDIX IIIb: Analytical Data for Rock Samples
- APPENDIX IIIc: Statistical Data for Rock Samples
- APPENDIX IIId: Thin Section Descriptions for Selected Rock Samples
- APPENDIX IVa: Diamond Drill Logs
- APPENDIX IVb: Geotechnical Logs and Analytical Data for Diamond Drill Holes
- APPENDIX IVc: Geological Cross-Sections for Diamond Drill Holes
- APPENDIX V: Statistical Data for Diamond Drill Holes
Correlation Coefficients
Histograms
Scatter Plots
- APPENDIX VI: Survey Point Descriptions and Survey Data
- APPENDIX VIIa: Statement of Costs Hi-Tec Resource Management Ltd.
- APPENDIX VIIb: Statement of Total Project Costs

LIST OF TABLES

	after page
Table 1: Drill Hole Layouts.	31
Table 2: Summary of Lower Alteration Zone Intersections.	36
Table 3: Summary of Lower Alteration Zone Intersections Creek 5 "Flat" zone	36



1.0 SUMMARY

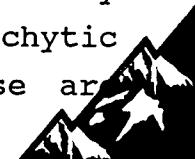
Pursuant to a request by Mr. Robert F. Brown of LAC Minerals Ltd., a two phase exploration program consisting of geological mapping, limited trenching, geochemical sampling and diamond drilling was carried out on the Hank claim group during July to September 1989. The writer supervised the exploration program and researched the literature pertaining to the area.

The property consists of 4 contiguous claims totalling 68 units and is located in the Ball Creek area, Liard Mining Division, British Columbia. The claims are located approximately 16 kilometers west of Highway 37 (the Stewart-Cassiar Highway), 370 kilometers north of Kitwanga, British Columbia. Access is via highway 37 to the Burrage Creek airstrip on the east side of the Iskut River and then by helicopter to the property.

Local topographic relief is moderate to very steep with elevations ranging from approximately 900 meters along Hank Creek to over 1,950 meters in the eastern portion of the property.

The Hank property was previously explored for copper with little attention paid to it's gold potential. Exploration programs have been conducted on the claims since 1983.

The property lies within the westernmost part of the Intermontane Tectonic Belt, close to its boundary with the Coastal Crystalline Tectonic Belt. The Hank claims are situated within the Stikinia accreted terrane of the Canadian Cordillera. The claims are underlain by Upper Triassic, Stuhini Group andesitic to trachytic volcanics, pyroclastics and epiclastics. These are



partially overlain by a leucocratic sequence of totally altered assemblage. Middle Jurassic, Spatsizi Group, stata are also exposed on the property.

Two main zones of alteration and precious metal mineralization, namely the upper and lower alteration zones, have been outlined on the property.

The eastern boundary of the Hank 2 claim, contiguous with the Hank 4 claim, approximately coincides with a major steeply inclined topographic feature. This feature is now believed to represent a major fault scarp. The overall structure of the district implies that the Hank property is situated within a half graben type structure. The presence of a breccia zone, a leucocratic zone, diorite and a vein stockwork within volcanics suggests that the lower and upper alteration zones have formed because of high fluid pressures associated with a magmatic source at depth. The brittle fractures which controlled the upper alteration zone were produced by and during the emplacement and upwelling of fluids. The orientation of the mineralized structures need not have any relationship to the surrounding stratigraphic dip. Steeper dipping structures may be expected to form at deeper depths in the system.

The lower alteration zone appears to be fault controlled and cross-cuts the stratigraphy in this area. The presence of a steeper dipping stratigraphy, related to the infill from primary extrusion events, may have localized the position of some of the later faults.

The Hank claims mineralization forms part of a large epithermal system which has been obliquely cut by



glacial erosion. Deformation and volcanism must have occurred within narrow time constraints. The main Hank 2 - Hank 4 fault appears to provided structural control for and the physical limits to the mineralizing system to the east.

A total of 1610.6 meters were diamond drilled on the lower alteration zone. A vein stockwork was evident in the core. The best mineralization was associated with gouge zones, sphalerite-galena rich veins, and rhodocrosite stained calcite veins. A number of laterally discontinuous mineralized zones have been identified by the drilling program.

One hundred and sixty-eight rock samples and eight hundred and fifteen core samples were collected and all of the samples were submitted to Bondar-Clegg & Company Ltd., in Vancouver, British Columbia.

The potential of volcanic conduit related mesothermal veins at depth exists and should be drill tested. High level stocks with the potential of associated porphyry mineralization may also have formed at depth in the Hank 2 - Hank 4 fault conduit zone.

Additional drill targets are outlined and additional exploration work is recommended to further define the geometry and grade characteristics of the alteration zones.



2.0 INTRODUCTION

2.1 OBJECTIVES

Pursuant to a request by Mr. Robert F. Brown of LAC Minerals Ltd., a two phase exploration program was carried out on the Hank claim group during the period July to September, 1989, by Hi-Tec Resource Management Ltd. Phase I consisted of geological mapping, limited trenching, and rock geochemical sampling and Phase II was predominantly diamond drilling.

The purpose of the exploration program was to:

- a) cut a base-line, reflag the existing grid and establish intermediate lines on the lower portion of the property
- b) install wooden pickets with metal tags to delineate the grid on the upper portion of the claims
- c) flag and supervise the building of a cat road system and drill pads on the lower alteration zone, the refurbishing of existing cat roads and the construction of additional roads on the upper grid area
- d) supervise the surveying of specific points on the property by Marlow Currie of A.A. De Bruyne, Land Surveyors based in Smithers, British Columbia.
- e) map and sample the geology of the property in detail
- f) evaluate the precious metal potential of the Lower Alteration Zone polymetallic vein stockwork by trenching and diamond drilling methods
- and g) propose an exploration program designed to further define the mineral inventory and ore reserve potential of the claim group.



This report is based on the results of the exploration work conducted during July and September 1989 and on the available literature pertaining to the area.

Surveying of specific points on the property demonstrated that significant errors were previously incorporated into the LAC base maps. All of the property base maps had to be re plotted and redrafted to account for the relocation of roads and drill holes.

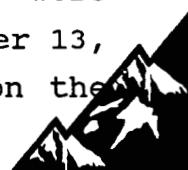
2.2 GENERAL LOCATION AND ACCESS

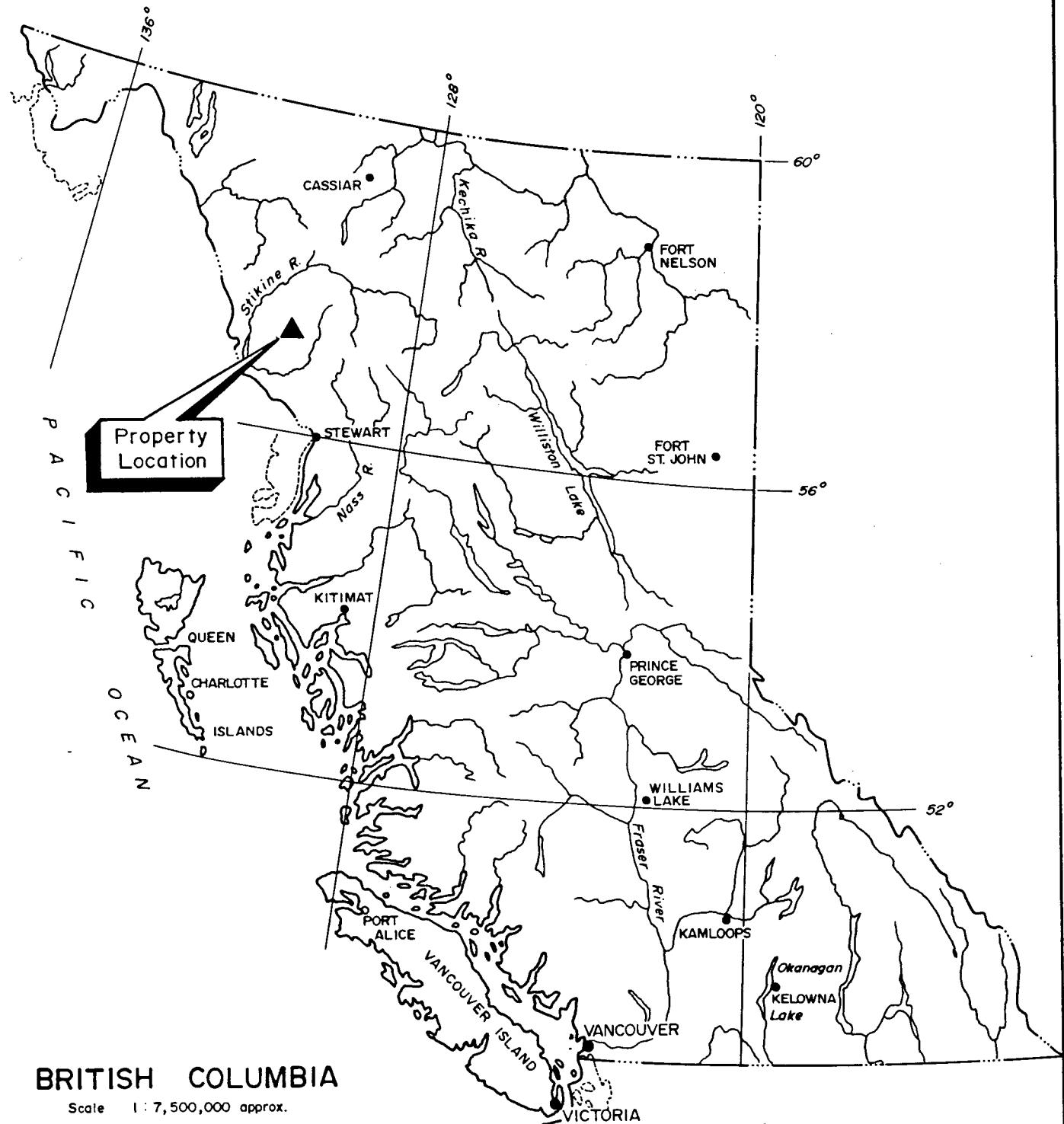
Access to the region is via Highway 37 (the Stewart-Cassiar Highway), to the Burrage Creek emergency landing strip, on the east side of the Iskut River, approximately 370 kilometers north of Kitwanga, British Columbia (Figure 1). The Hank claims are located approximately 16 air kilometers west of Highway 37 along a tributary of Ball Creek, herein termed Hank Creek, and approximately 20 air kilometers south of the Mount Edziza Provincial Park. Helicopter flying time to the property from the Burrage Creek strip is approximately 15 minutes.

An alternative route is via a schedule flight with Central Mountain air from Smithers to Iskut town or Dease Lake airstrips and then by road and helicopter to the claim group.

2.3 OPERATIONS AND COMMUNICATIONS

Mobilization, demobilization and field work were carried out during the period July 10 and September 13, 1989. The field crew established a base camp on the





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HANK PROPERTY

GENERAL LOCATION MAP



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south side of Hank Creek adjacent to Creek 3 (Line 1200N/00E) at an elevation of 930 meters above sea level. A Canadian 206 helicopter, based at Tatogga Lake Resort, was used to mobilize/demobilize and supply the camp in addition to moving the drill equipment. Regular HF radio contact, using a Spilsbury SBX 11, was maintained, from the base camp, with expeditors Jaycox Industries Ltd. in Smithers. Transmission of radio telephone communications via the Bob Quin operator station were only possible from the "felsite dome" area, at an elevation of 1620 meters, using a mobile telephone equipped with a directional antenna.

A D-6 wide-track CAT, contracted from Pickell Construction of Fort St. John, B.C., was walked from the Burrage Creek - Highway 37 bridge intersection across the Iskut river to the property. Access to the claims could not be gained via Hank Creek because of the presence of steep and narrow gorges. Therefore the CAT was walked along the valley southeast of (behind) the property and then onto the southeast corner of the Hank 2 claim.

The D-6 Cat was used for road refurbishing and construction, drill pad preparation and was also planned to be utilized for drill moves. However, the presence of a thick (1-3m) cohesive, silica-clay type layer over much of the southern portion of the property hampered the progress of the road construction. This clay layer made drill moves by D-6 Cat impractical and therefore the 206 helicopter was used.

Adverse weather conditions (heavy fog and rain) and heavily timbered vegetation at lower elevations placed some limitations on the helicopter use during the field work.



Connor's Drilling Ltd., based in Kamloops, B.C., were the drill contractors. All holes were collared with NQ size core and then the holes were completed in BQ size core. Travel to and from the base camp to the drill sites was by 4-Track Honda all-terrain-vehicles.

A rented truck was stationed at Tatogga Lake Resort and used to ferry samples to Smithers airport. Canadian airways provides a special rate for shipments of rock samples to Vancouver, B.C. The samples were shipped to the Bondar-Clegg laboratory for analysis.

Selected points on the property were surveyed by Mr. Marlow Currie of A.A. deBruyne Surveyor's, based in Smithers, B.C.

The base camp was inspected twice during the field season by members of the Inspector of Mines Engineering and Inspecting Branch of the Ministry of Energy, Mines and Petroleum Resources. Garbage disposal, fire stations and first aid facilities were examined on each occasion and declared efficient. By order of the Inspectors, previously occupied camp facilities had to be cleaned up, oil and diesel drums removed and old camp debris burned. A "Class A Burning Permit" (#A50280) was obtained from the Ministry of Forests in accordance with provincial regulations prior to burning.

2.4 PHYSIOGRAPHY

Local topographic relief is moderate to very steep with elevations ranging from approximately 900 meters along Hank Creek to over 1,950 meters in the eastern portion of the property. The area exhibits the characteristics



of typical glaciated physiography, which include wide U-shaped, drift-filled valleys flanked by steep rugged mountains, cirques and deeply incised V-shaped upland valleys.

Vegetation consists mainly of dense alder, willow, and mature conifers such as spruce, fir, and hemlock along the valley slopes. At higher altitudes above timberline, generally between 1,400 meters and 1,600 meters above sea level, the vegetation changes to subalpine and alpine vegetation. The highest parts of the property support only moss and lichen. Glaciers and snowfields occur frequently throughout the area, usually above 1,600 meters. The period of least snow cover occurs between July and mid-September and summers are relatively cool and wet.

2.5 CLAIM STATUS AND OWNERSHIP

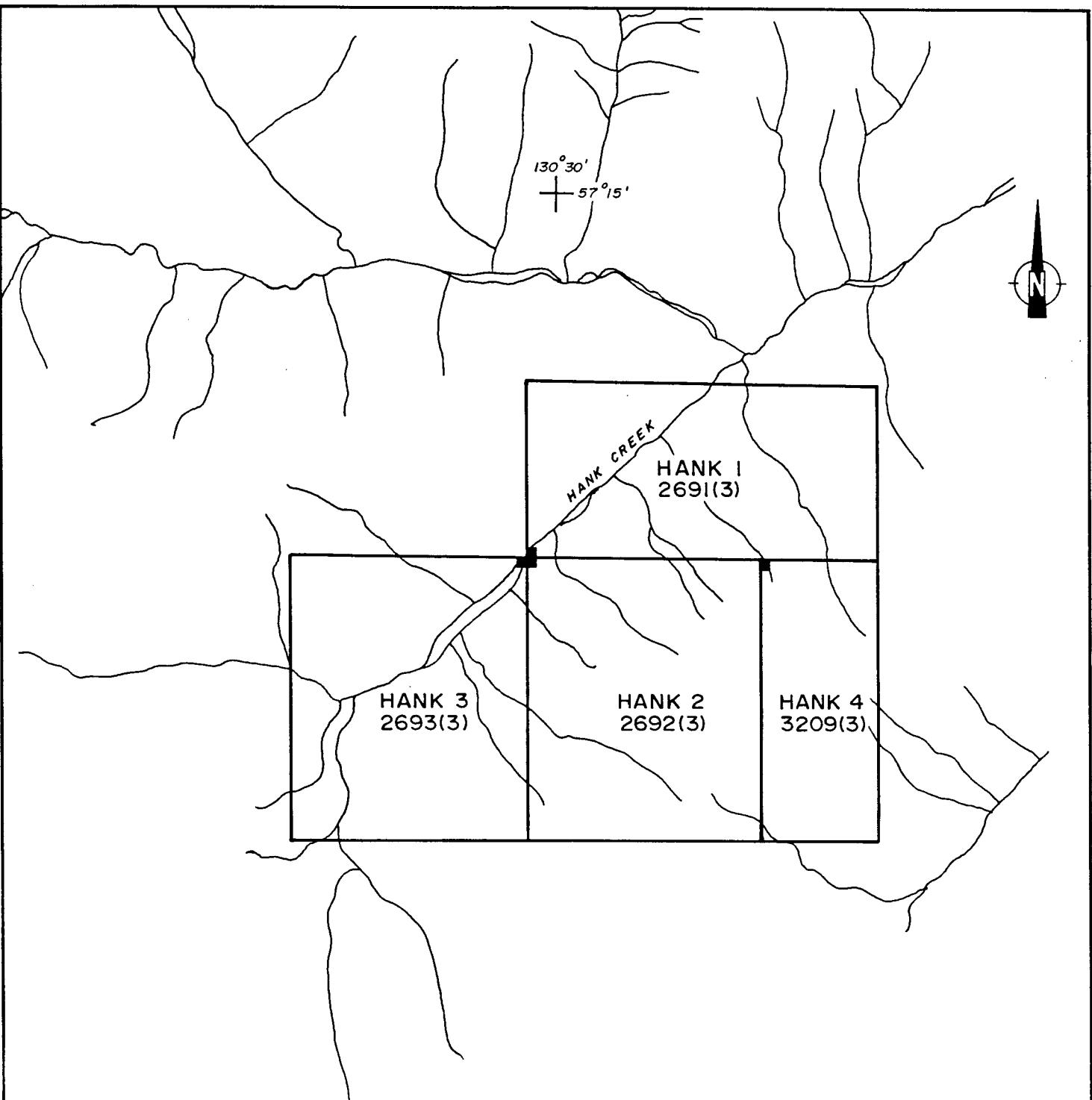
The LAC Minerals Ltd. property consists of 4 contiguous claims totalling 68 units within the Liard Mining Division of British Columbia (Figure 2). Title to the claims is held 100% by LAC Minerals Ltd. The Hank 1, 2 and 3 claims were staked by LAC in March 1983 to cover anomalous gold stream samples collected from gossanous rocks adjacent to Hank Creek. The Hank 4 claim was staked in September 1984 to consolidate the claim group.

Pertinent claim data is summarized below:

<u>Claim Name</u>	<u>No. of Units</u>	<u>Record #</u>	<u>Expiry Date*</u>	<u>N.T.S.</u>
Hank 1	18	2691	March 10, 1995	104G/1W, 2E
Hank 2	20	2692	March 10, 1995	104G/1W, 2E
Hank 3	20	2693	March 10, 1995	104G/2E
Hank 4	10	3209	Oct. 12, 1995	104G/1W

* Prior to filing the 1989 exploration work.





LAC MINERALS LTD. HANK PROPERTY

CLAIM MAP

1.0 0 1.0 2.0 km
Scale 1:50,000



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3.0 REGIONAL HISTORY

Although the Stikine River served as the access route to the placer deposits of the Telegraph Creek-Cassiar area which were discovered in the period 1861 to 1873, there is no record of any prospecting activity in the Iskut River area until 1907. During the 1920's, 1930's and 1940's the exploration for lode deposits was confined to accessible areas along the Stikine River, with a number of small copper occurrences being discovered.

Little work was done in the area until 1954, 1955 when Hudson's Bay Mining and Smelting located the large tonnage copper-gold porphyry deposit at Galore Creek (137 MT grading 1.02% Cu, 0.014 oz/ton Au). In 1957, they also discovered the Copper Canyon copper-gold porphyry deposit (28 MT grading 0.64% Cu, 0.02 oz/ton Au) approximately eight kilometers east of the Galore Creek Central Zone (Grant, 1964).

Hudson's Bay Mining and Smelting also located the Pickaxe showing, and found high grade gold-silver-lead-zinc float on the upper slopes of Johnny Mountain. After performing exploration work on the latter showing in the mid-1950's, Hudson's Bay Mining and Smelting allowed these claims to lapse. These showings are now part of Skyline Exploration's Reg property.

Following the discovery of the Galore Creek Cu-Au deposit, (2 million ounces of contained gold), exploration was increased in the Stikine River area. During the late 1950's and early 1960's, several major mining companies conducted airborne geophysical surveys in the region, on a reconnaissance basis, for potential



porphyry copper-molybdenum deposits. Several new claims were staked in the Stikine River area, on Johnny Mountain and along Sulphurets Creek in that period, while Kennco and Noranda investigated the original showings on Johnny Mountain. The BIK Syndicate (Silver Standard Mines, McIntyre Porcupine and Kerr Addison) also conducted exploration in the region in the late 1950's and early 1960's.

Several of the claims staked by the Syndicate, at that time, covered the Trophy Gold Project property. After performing limited exploration work in the mid-1960's, the lead-zinc rich Ptarmigan showing, with assay values of up to 0.16 oz/t gold and 6.7 oz/t silver, was discovered. Prospectors also located skarn type Cu-Au mineralization at the Hummingbird showing (Forster, 1988). However, the failure to discover another large copper ore body resulted in many of the claims in the area being allowed to lapse.

In 1969, Skyline Explorations Ltd. restaked the Inel property, after having discovered massive sulphide float originating from the head of Bronson Glacier. In 1974, Texas Gulf Inc. investigated the porphyry copper potential of Johnny Mountain.

Teck Corp. conducted a regional reconnaissance stream sediment geochemical survey in the Galore Creek-Stikine River area. They also defined reserves of 185,000 tonnes, grading 4.11 g/t gold, for the Paydirt deposit (Holtby, 1985). Longreach Resources Ltd. commenced underground development and exploration on the Paydirt deposit during 1987.

The discovery of the Snip and Reg deposits in the Iskut River district has provided renewed interest in the



Stikine and Stewart Gold camp areas, due to similarities in their geological setting. Several new mineral showings have been discovered in the area surrounding the Paydirt and Galore Creek deposits during the period 1986 to 1988. According to Awmack (1989), significant precious metals occurrences were discovered on each of the TREK, ICY and JW properties during the 1988 field season. The latter author states that each of these properties had previously been explored for copper during the 1960's with little attention paid to their gold potential.

Exploration for precious metals in the Sulphurets Creek area dates back to the late 1800's when placer gold was discovered in the upper reaches of the Unuk River. Extensive gossans in the upper reaches of Sulphurets Creek attracted Bruce and Jack Johnson to stake claims in this area in 1935. Hence, the name "Brucejack Lake".

The Calpine Resources Inc.-Consolidated Stikine Silver Ltd.'s Eskay Creek property has a long history of exploration by various companies since it's discovery in 1932 by Tom MacKay. In 1985, Kerrisdale Resources Ltd. diamond drilled the #21 and #22 zones, and in 1987 Consolidated Stikine Silver Ltd. conducted a soil sampling and trenching program on the Eskay Creek property. During 1988 and 1989, the Eskay Creek property was extensively drilled by Calpine Resources Inc.-Consolidated Stikine Silver Ltd. and extremely promising results were reported from the #21 zone since hole 88-6 hit 96.5 feet grading 0.73 oz. gold and 1.1 oz. silver (Northern Miner, Nov. 7, 1988).

The Hank property was previously explored for copper with little attention paid to it's gold potential. LAC



Minerals staked the Hank 1,2 and 3 claims in 1983 and the Hank 4 claim in 1984. Exploration programs have been conducted on the claims since 1983. Details of this work are given in the reports by Turna (1985, 1987, 1988) and Brown (1989).

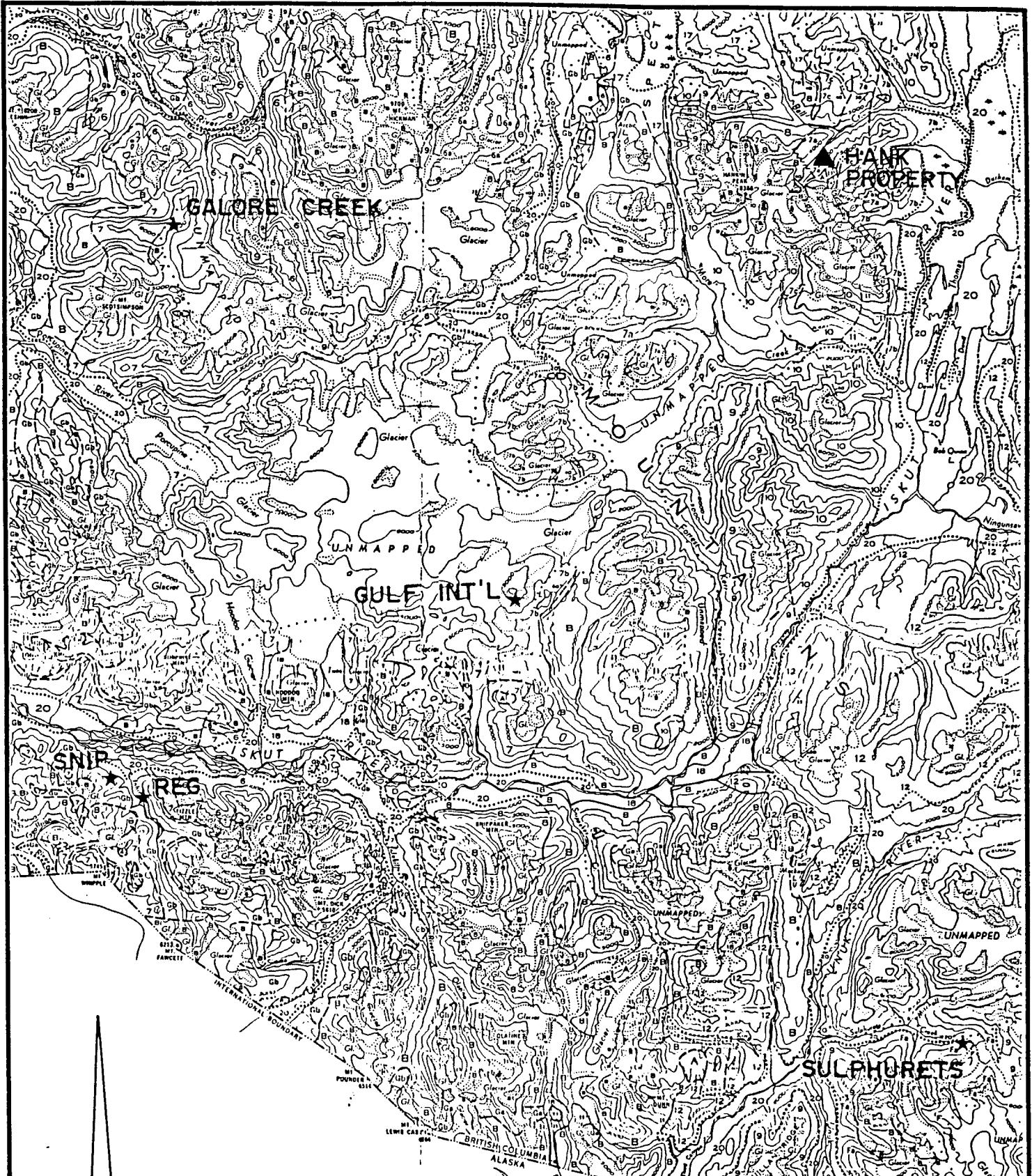
4.0 REGIONAL GEOLOGY AND MINERALIZATION

The property lies within the westernmost part of the Intermontane Tectonic Belt, close to its boundary with the Coastal Crystalline Tectonic Belt. As a result of the proximity of this area to a regional tectonic boundary, geologic relationships tend to be quite complex. The Hank claims are situated within the Stikinia accreted terrane of the Canadian Cordillera. The geology of this area (Figure 3) has been studied by Kerr (1930, 1948), and by Grove (1986), and is represented in Geological Survey of Canada Maps 9-1957, 1418A and 1505A.

The oldest rocks in the region are complexly folded, metamorphosed schists and gneisses of probable mid-Paleozoic age. The metamorphism occurs within and adjacent to a plutonic system. The metamorphic rock is commonly overlain by a white to grey crystalline limestone which is believed to belong to a Late Paleozoic sedimentary sequence that includes some minor greenstone units. This oceanic assemblage is part of the Stewart Complex, a tectonic unit which has been correlated with the Cache Creek Group.

The principal component of the Intermontane Tectonic Belt in the Iskut River area is a Mesozoic volcanic and sedimentary sequence, relative with the time equivalent Stuhini Volcanics; a theory which is supported by the presence of Monotis fossils on the north slope of





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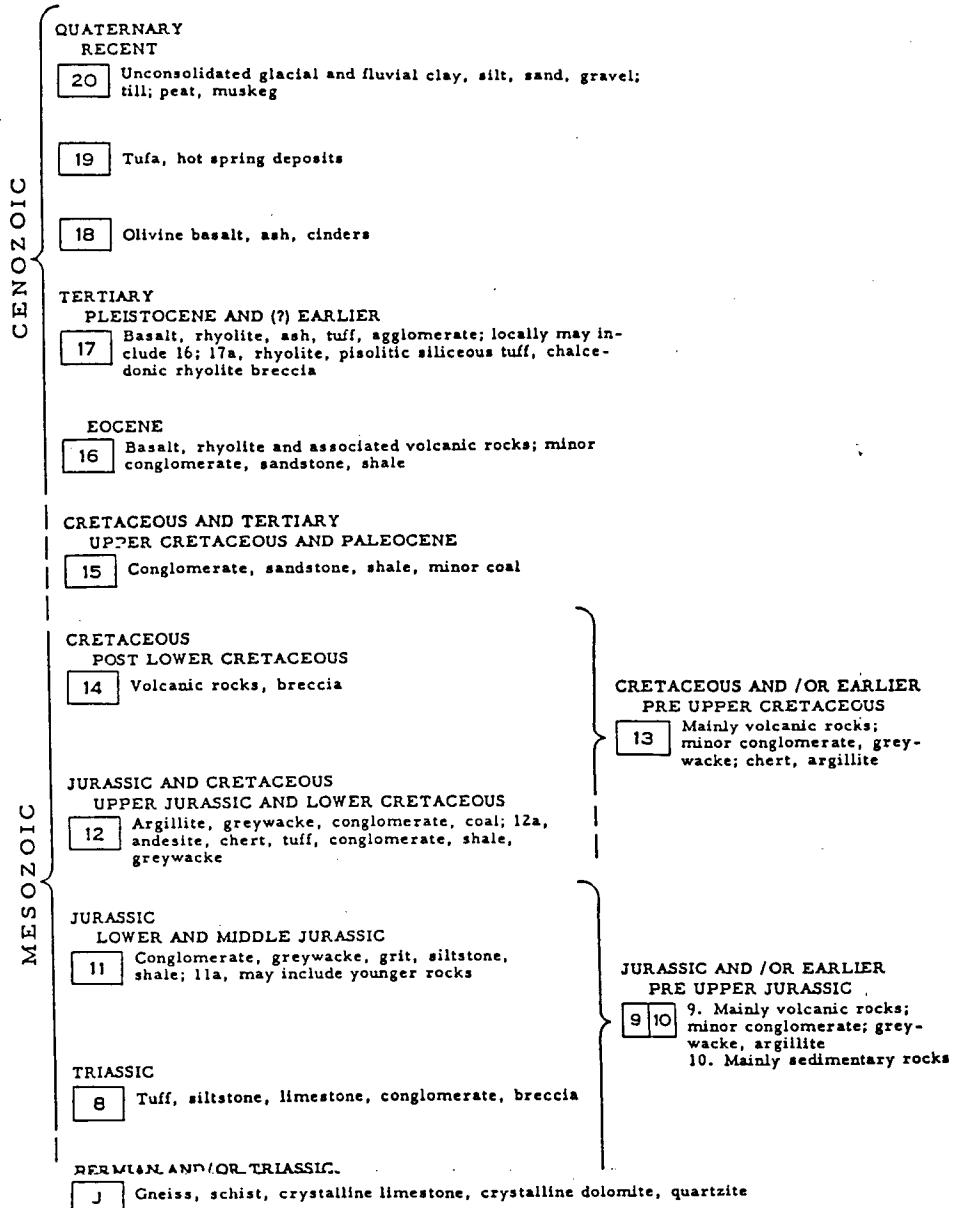
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Figure 3			

LAC MINERALS LTD. HANK PROPERTY

REGIONAL GEOLOGY MAP

LEGEND

SEDIMENTARY AND VOLCANIC ROCKS



- Geological boundary (defined, approximate, assumed)..... — — —
- Limit of geological mapping
- Bedding (horizontal, inclined, vertical, overturned)
(dip, g, gentle; m, medium; s, steep)..... + / X X
- Bedding, inclined (direction of tops unknown, overturning suspected)
- Schistosity, gneissosity (inclined, vertical, dip unknown)..... / X /
- Fault (defined, approximate, assumed)..... ~~~~~ ~ ~
- Anticline (defined, approximate)..... — —
- Syncline (defined, approximate)..... — —
- Anticline, syncline (overturned)
- Trend of complexly folded beds (direction of plunge known, unknown)..... X X
- Belt of quartz diorite and quartz porphyry dykes
- Glacial striae (direction of movement known, unknown)..... P S
- Placer mine
- Mine or prospect
- Cinder cone or recent volcanic crater

Snippaker Peak and to the west of Newmount Lake. Grove (1986), however, correlates this unit with the Middle Jurassic Unuk River Formation of the Stewart Complex. In the Galore Creek area, Souther (1971) mapped the Upper Triassic Hazelton Group as an undifferentiated sequence of island arc volcanics and sediments. The Paydirt gold deposit in the Galore Creek district is hosted within silicified, sericitized and pyritized Upper Triassic volcanics (Holtby, 1985) and is correlated with the sequence which hosts the Snip and Stonehouse gold deposits at Bronson Creek.

On the north slopes of Johnny Mountain and Snippaker Peak, Paleozoic metasedimentary rocks are found to overlie the Mesozoic sequence. These apparently represent the upper plate of a regional, east-west trending thrust fault, which pushed up and over to the south in a manner similar to that of the King Salmon Thrust Fault.

In the Coast Crystalline Tectonic Belt, Paleozoic and Mesozoic sequences are commonly intruded by plutonic rocks of quartz monzonite to quartz diorite composition. These intrusions are Late Cretaceous to Early Tertiary in age. To the east of the main intrusive complex, smaller granitic plugs and stocks are prevalent.

Quaternary flows and ash deposits of olivine basalt are the youngest rocks in the area. Hoodoo Mountain, to the south of the subject property, is underlain by these units, which also occur in parts of the valleys of the Iskut River and Snippaker Creek.

The two most significant mineral deposits subject to current investigation in the Iskut River area are the



Skyline Explorations Ltd. Reg property on the north slope of Johnny Mountain and the Delaware Resources-Cominco Ltd. joint venture Snip property near Bronson Creek. These properties are only five kilometers apart and appear to be similar in nature.

At least seven auriferous, mineral rich quartz veins are known to occur on Skyline's Reg property (Grove, 1986). These are collectively known as the Stonehouse Gold Zone. This zone is hosted in an east-west striking, northerly dipping sequence of Jurassic volcaniclastics and porphyritic flows. A sequence of Middle Jurassic volcanic breccias and well stratified volcanic tuffs and sediments unconformably overlie the mineralized unit. Steeply dipping veins trending 050° - 060° and dipping 70° NE along major fractures are the only known mineralization environment in the Stonehouse Gold Zone. The mineralized zones consist of pods, lenses and quartz veins which contain 20% to 80% sulphides plus K-feldspar, besides native gold and electrum. Adjacent to the zones, extensive wallrock alteration includes very fine biotite and sericite, and extensive massive orthoclase with minor carbonates (Grove, 1986).

On the Delaware-Cominco joint venture Snip property, native gold occurs in a 1-10 meters thick discordant banded shear zone cutting a massively bedded feldspathic greywacke-siltstone sequence. It consists of alternating bands of massive streaky calcite with abundant disseminated to massive pyrite mineralization. Biotite-chlorite, quartz, pyritic to non-pyritic, fault gouge related, alteration is associated with this zone. (Northern Miner, June 13, 1988).



In the Sulphurets area, Shroeter (1983) examined the geology and mineralization in the Brucejack Lake area where hornblende syenites, alkali feldspar syenites and country rocks are cut by many north to northwesterly faults and are intensely altered with sericite, K-feldspar, silica, carbonate and chlorite. Five separate sulphide zones occur along a 7 kilometer belt with mineralization occurring in several styles, including low grade disseminations, epithermal stockworks and veins. Found within these zones are pyrite, chalcopyrite, molybdenite, ruby silver, stephanite, ceragyrite, electrum, native gold, tetrahedrite, freibergite, argentite, galena, sphalerite and bornite.

Within this area, two principal zones were identified. The Peninsula Zone (or Shore Zone) and the West Zone, located about 700 meters southwest of the Peninsula Zone. Shroeter reported ruby silver, freibergite, electrum, native gold, stephanite, galena, pyrite and sphalerite occurring in a stockwork of quartz veinlets in sericitic andesitic tuff.

In the Unuk River Area, the geological cross section of the Calpine/Consolidated Stikine's Eskay Creek property is as follows: the hanging wall consists of interbedded breccias, pillow lavas and andesites up to 100 meters thick. The contact zone, a black argillite containing felsic fragments up to 2 inches across, is 10 to 15 meters thick with mineralization occurring at the base of the unit. It is unclear from published data on the property whether the mineralization in the contact zone is syngenetic or epigenetic. In the north section of the contact #21 Zone, mineralization consists of electrum, aktashite (Cu-Pb-Zn-Ag-Hg sulphosalt) and honey coloured blebs of sphalerite



rimmed with chlorite alteration. Free gold was observed in the core. Disseminations and needles of arsenopyrite predominate in the south section of the #21 contact zone with sections of massive stibnite, veinlets of stibnite and blebby realgar. Gold assays from this contact zone vary from 0.25 oz. Au/t to several oz. Au/t.

The footwall belongs to the Dillworth Formation and consists of a 100 to 150 meters thick rhyolite breccia and lapilli tuff. Along strike to the north the lapilli fragments are finer. Alteration observed is silicification, strong K-spar and white mica. Gold assays from this section vary up to 0.25 oz. Au/t. A 10 to 20 meters thick argillite layer separates the lapilli tuffs from a felsic lithic tuff which varies from 60 to 100 meters thick. This latter unit, which may be the equivalent of the Betty Creek Formation, forms large gossans of pyritic material assaying from 0.15 to 0.25 oz. Au/t. The bottom of the footwall is formed by thickly bedded siltstone containing pelecypods (dating in progress) and locally developed conglomerates. Drill intersections of the north part of the #21 Zone (hole 89-109) were recently reported in the Northern Miner as follows: "682 foot interval grading an average of 0.875 oz. gold, 0.97 oz. silver, 1.12% lead and 2.26% zinc. Within this interval is a 200.1 foot section averaging 2.877 oz. gold, 0.85 oz. silver, 1.86% lead and 3.44% zinc" (Northern Miner, Aug. 28/1989). The Northern Miner reports (Sept. 4, 1989) that drill hole 89-126 intersected at the north end of the #21 Zone a disseminated to massive sulphide mineralized section of 445 feet in width, of which a 30-ft and a 26-ft section consisted of pyrite - galena - sphalerite - chalcopyrite massive sulphide mineralization. No assays are available to date on



this hole. This may indicate a volcanogenic massive sulphide lense off the #21 Zone.

Souther (1971) recognized numerous phases of faulting and shearing in the Stikine River area. Major northerly trending faults and associated subsidiary minor faults occur throughout the area. Normal faulting, initiated during the early Jurassic, is most commonly developed with only minor reverse faulting having been identified (Souther, 1971).

The Hank property region is underlain by a thick succession of Upper Triassic To Middle Jurassic volcano-sedimentary lithologies. The strata have been intruded by a series of plutons which represent different intrusive episodes. These intrusions consist of synvolcanic plugs, dykes and stocks. The Upper Triassic sequence consists of Stuhini Group andesitic tuffs, flows and trachytic volcanics. Middle Jurassic sediments of the Spatsizi Group unconformably overlie the Stuhini Group (Figure 3).

5.0 PROPERTY GEOLOGY

5.1 Stratigraphy

The Hank property lithological assemblage as described by Turna (1988) is largely agreed with by the current writer. Some outcrops mapped by Turna as agglomerate underlying the lower alteration zone were classified as volcaniclastic during the 1989 mapping. Much of the property is underlain by thick alternating monotonous sequences of alternating fine to coarse grained andesitic tuffaceous units. These form massive, crudely layered, compositionally similar exposures.



Because of this, bedding is rarely identifiable in outcrop. Lapilli tuffs are evident in places.

Colour variations are found throughout the sequence. The volcanics underlying the lower alteration zone are predominantly pyritic dark green-grey (chloritic) andesitic tuffaceous and volcaniclastic units. There are interbeds of agglomerate evident in some stream sections below this alteration zone. The basal contact of the lower alteration zone appears to be marked by a transition sequence from the above rocks into a highly altered, deeply weathered orange-yellow coloured "melange" when viewed in the deeply incised creek gullies on the property. Occasional pods of maroon coloured, weakly altered volcanics were noted within the lower alteration zone during the 1989 mapping.

The upper contact of the lower alteration zone is not marked by a distinct break or gouge zone in the area to the southwest of creek 7. A transition zone similar to that at the base is exposed in the creek sections along the upper contact. Overlying the transition zone is a sequence of purple-maroon (hematitic) amygdaloidal lavas and epiclastics. Turna recognized pipe amygdules within this sequence which provided right-way-up criteria. However during the 1989 mapping only flat lying "pipe amygdules" were noted in outcrop. The outcrops also appeared to have undergone a period of pressure solution cleavage formation which has imposed a NE-SW fabric and preferred orientation on the incorporated structures. The distinct maroon colour of the rocks in this area suggests that they may be a separate suite of volcanics. Many of the rocks contain hematite concentrated along fractures. Lateral facies changes and interfingering make tracing the stratigraphy more complex.



The interbedded massive fine and coarse andesitic and agglomeratic units within the stratigraphic succession may imply repeated periods of tectonic activity followed by periods of erosion.

In the area to the northeast of creek 7, there is a distinct linear topographic high which coincides with the incoming of unaltered light green and maroon volcanics into the sequence. This is interpreted as a fault contact and is described in Section 5.4.

The succession between the lower and upper alteration zones is similar to that described above. However, on the well exposed, north facing, steep slope of Camp 3 Peak spheroidal weathering is evident within the dark green volcanics.

The upper alteration zone is capped by a bleached, grey cohesive silica-clay type horizon. This has resulted in very swampy ground conditions in upper parts of creeks 3 and 4.

A breccia zone, in the upper grid area, has been mapped by Turna as a diatreme and is detailed in previous reports. This zone consists of large, coarse, cobble sized breccia clasts many of which are rounded to sub-angular. There is a lateral, tectonic grading of clast size evident in outcrops of this breccia zone. Portions of this zone appear to have a pipe like geometry however, there is a more planar sheet-like geometry also present. This zone is described in Section 5.4. Whether the clay horizon flanks the breccia zone, unconformably overlies it or is intruded by the breccia zone is unclear.



Within the silica-clay horizon there are a series of highly siliceous "cherty" outcrops. Turna (1988) mapped these as his "line of cherts" and a number of diamond drill holes were drilled through the horizon. In core, no chert horizon was intersected and the zone was found to consist of a large "gouge" type layer. During a site visit and discussion with C. Nelsen of LAC Minerals (USA) Inc., during the 1989 field season, the outcrops of chert were examined and recognized as being highly altered andesites. Similar types of alteration may be caused by sulphuric acid fumes that emanate from modern siliceous geothermal springs near Reno, Nevada (Panteleyev, 1986). Minor siliceous zones are evident in a road cut of the clay layer in the upper grid area. This unit may represent an alunite layer unconformably overlying the Stuhini Group volcanics.

A similar type clay, possibly derived from this part of the sequence, covers the lower portions of creeks 6 and 5, within the lower alteration zone. This clay forms an impervious layer and has resulted in an area which, as may now be expected, appeared to host only low gold soil geochemical values. It also made CAT work difficult during heavy rain fall periods.

Overlying the clay layer, in the upper grid portion of the property, is an extrusive, siliceous grey, leucocratic, highly siliceous dacitic? unit. This may be an altered, welded, lapilli tuff unit. It consists of a fine-grained grey matrix, which weathers a brown-yellow colour, with abundant altered feldspar? crystals. In thin section these are seen as crystal pseudomorphs which have been completely altered (Appendix IIId). This dacitic unit may be locally unconformable on the green and maroon coloured Stuhini



Group volcanics. Turna (1988) noted the presence of chalcedony boulders in the upper grid area. This suggests that quartz may have become finer grained upwards in the system.

Intruding the Stuhini Group volcanics are stocks of dioritic to granodioritic composition. These are exposed in the southwest portion of the property. Anderson (1984) mapped the Stikine composite batholiths of the Stikine Arch and dated them as Late Triassic to Middle Jurassic age.

5.2 Alteration

Iron hydroxides are evident on all surface exposures of the lower alteration zone. They impart a yellow - brown colour with earthy material infills in places within the zone. This feature is probably due to oxidation of pre-existing sulphides in the alteration zone. Clusters of euhedral pyrite crystals were noted in places. These were associated with zones where the original lapilli textures of the host rocks could be detected occasionally.

In "fresh" outcrops and in core, the lower alteration zone is a white-grey bleached unit with abundant veinlets and gouge zones. The veinlets appear to form a 30-40 meter wide stockwork which is oriented oblique to the alteration zone contacts. In thin section the lower alteration zone consists of a carbonate-sericite-pyrite assemblage.

The pervasive nature of the alteration within the lower alteration zone makes recognition of discrete alteration stages very difficult in outcrop.



5.3 Mineralization and Veining

Sericitic alteration with pyritization and bleaching have produced an extensive gossan, which is exposed in the creeks, and forms the lower alteration zone. Within the alteration zones disseminated pyrite is the most abundant sulphide. However, fine disseminated pyrite is also ubiquitous within all lithologies on the property. Galena and sphalerite are commonly developed in the veinlets of the lower alteration zone. Precious metal mineralization is confined to the zones of alteration on the property. The green and maroon coloured, competent, epiclastics and volcanics surrounding the alteration zones do not appear to have been affected by the carbonate-sericite-pyrite alteration. However, these lithologies are involved in and affected by the faulting on the property and must have been present during mineralization. This suggests that mineral deposition was concentrated in preferentially suitable lithologies, possibly tuffaceous horizons, around structurally produced conduits.

The vein characteristics of the upper alteration zone and the lower alteration zone are distinctly different. The geochemistry of both zones is also different in that base metal sulphides are more evident in the lower alteration zone. The veins in the upper zone are typically banded quartz-carbonate-siderite-barite veins which can be quite thick in places. Metal deposition was predominantly along the contact of the host rock with the vein margins (see Turna, 1988).

The veins of the upper alteration zone commonly show a banded or "varved" type texture in outcrop. The composition of these veins is predominantly different



from that of the host rock. However, there are lines of wall rock fragments commonly evident along and subparallel to the margins of the veins. The material in these "bands" appears to be derived from the walls of the fissure during fracture initiation. These show the evolution of the veins and mark successive openings along the vein-wall contacts with the "rip-off" of host rock during fluid injection. This process of vein formation is consistent with the description by Ramsay (1980) of veins formed by a crack-seal mechanism. The centers of the veins also have wall rock incorporated within bands but there also appears to be a distinct crustiform texture as a last stage infill. The earlier formed bands display a crinkly or stylolitic type geometry probably induced by pressure solution effects after vein formation.

The accretionary type vein geometry of the upper alteration zone is indicative of formation within a brittle tectonic environment where mineralization tends to border the shear/fault zone rather than being hosted in the zone.

Veins in the lower alteration zone typically form a network of thin, small-scale, anastomosing, discontinuous, cross-cutting carbonate-barite veinlets when viewed in the core. Occasional "pinking" of the veins, due to the presence of rhodochrosite, is evident. Much of this pinking is evident towards the basal contact of the lower alteration zone when seen in the core. The most significant precious metal grades appear to be related to the presence of galena and sphalerite in the veinlets. Sulphides do not appear to be deposited systematically within any particular portion of the veins. One galena-sphalerite rich barite vein, up to 0.5 meters thick, was exposed in a



trench in creek 5 and creek 7. This vein is the most laterally continuous (orientation 048^0) and well mineralized discrete vein uncovered to date. This may mark the site of a subsidiary fracture within the lower alteration zone.

The "varved" textures of the upper alteration zone veins are not evident in the lower zone. Mineralization is often in veined pods of more competent material separated by unmineralized intensely deformed material within veins of the lower alteration zone. Repeated cycles of mineral deposition are evident by the unsystematic distribution of the sulphides within the veins. This type of vein geometry and mineralization is often produced within brittle-ductile shear/fault zones.

The variation in the mechanism of deformation from the lower to the upper zone of alteration is reflected in the vein widths in the two zones. The brittle deformation of the upper zone provided large zones of dilation for metal deposition. The narrower vein widths within a stockwork of thin, small-scale, anastomosing, discontinuous carbonate-barite veinlets in the lower alteration zone were produced in a tectonic regime where there was a component of strike-slip shearing movement associated with normal fault development.

The sigmoidal en-echelon extensional gash veins linked and crosscut by oblique shear veins exposed in creek 8 and detailed in Section 5.4 may represent the type of vein network which exists within but which is not exposed in outcrops of the lower alteration zone. The vein arrays occur as narrow, subparallel-walled sets within the unaltered volcanics. The zones may be



classified as brittle-ductile shear zones (Ramsay, 1980).

5.4 Structure

The eastern boundary of the Hank 2 claim, contiguous with the Hank 4 claim, approximately coincides with a major steeply inclined topographic feature. The land surface morphology of this portion of the property reflects a relatively flat-topped ridge dipping to the east on the Hank 4 claim which is separated from the topographically lower Hank 2 claim by the steeply inclined, north-easterly oriented feature. This feature is now believed to represent a major fault scarp (Figures 4 and 5). The exposed portion of the relatively upthrown Hank 4 claim foot wall block has undergone extensive local erosion of the fault surface. This has resulted in formation of a large scree slope with no outcrop exposure at the base of the scarp. This precludes a definitive interpretation and examination of the fault plane. For mapping and interpretation purposes it is assumed that orientation of the eroded fault scarp coincides closely with the trace of the fault surface.

Additional evidence to support the normal-fault scarp interpretation is that there is a significant lithological change from the "felsite (leucocratic) event" (see Appendix IIId) zone of the Hank 2 claim hanging wall block to the agglomerates of the Hank 4 upthrown, foot wall block area. The absence of leucocratic lithologies within the footwall block implies that faulting occurred prior to deposition of the leucocratic lithologies. The abrupt nature of the dip change at the Hank 4-Hank 2 fault scarp and the absence of hanging wall synform or antiform fold



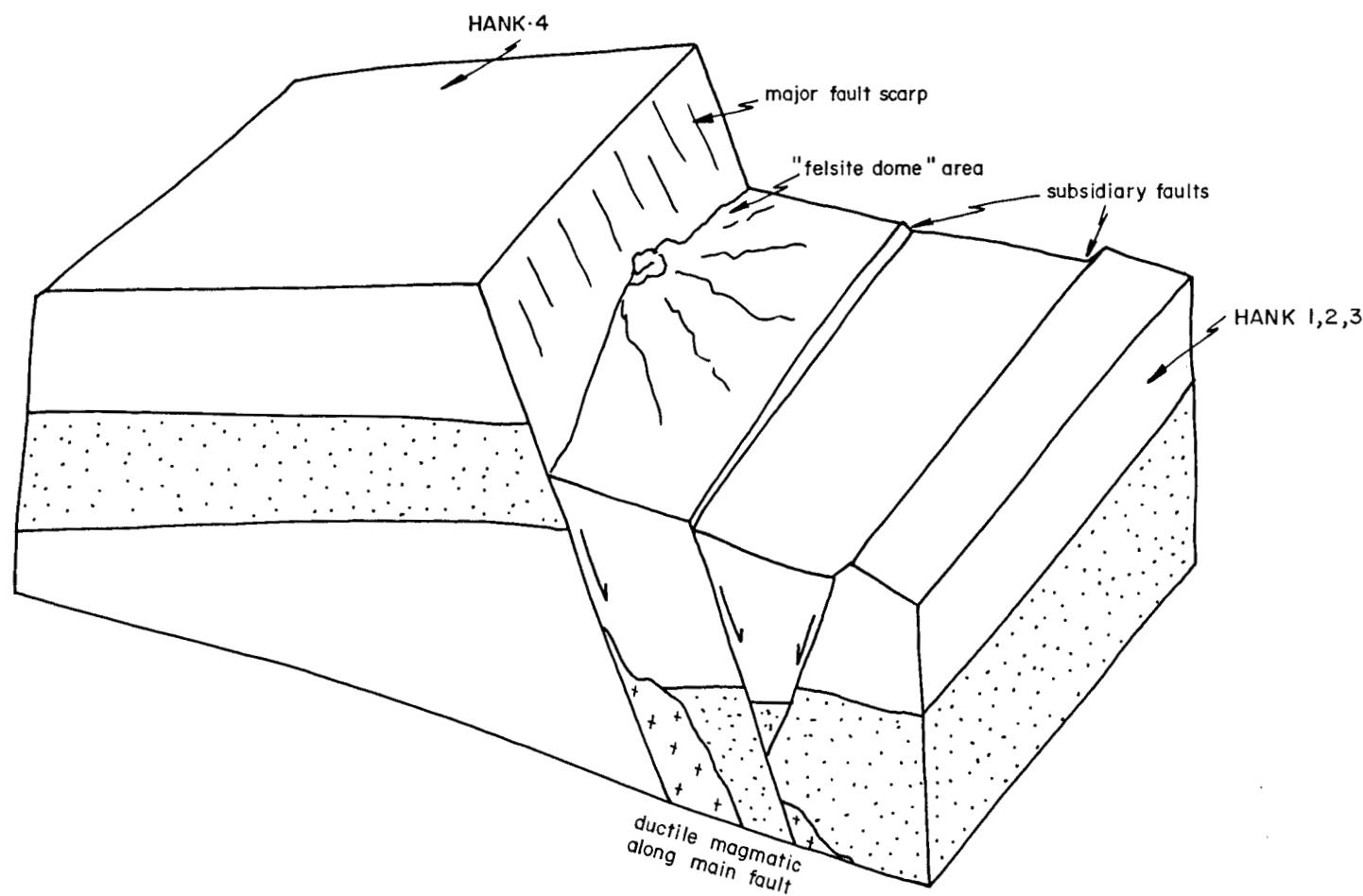


FIGURE 5: Schematic Block Diagram of the Hank 2-Hank 4 Fault Scarp

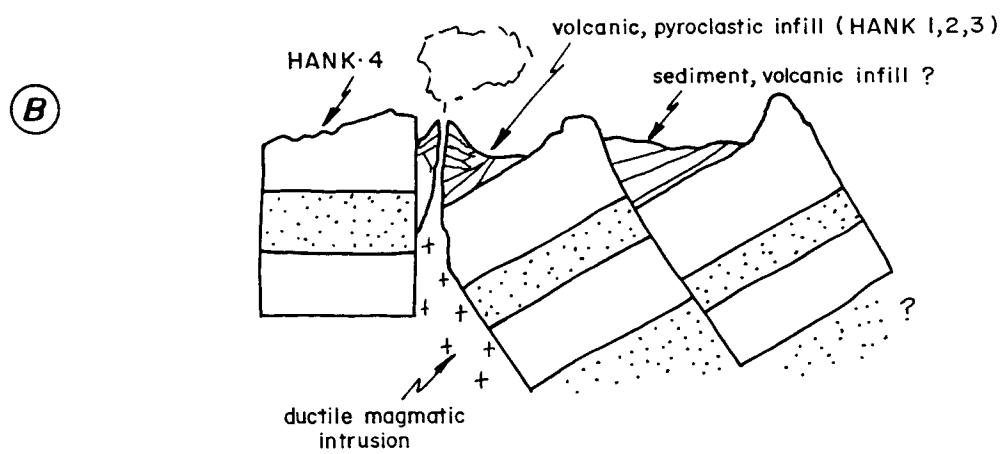
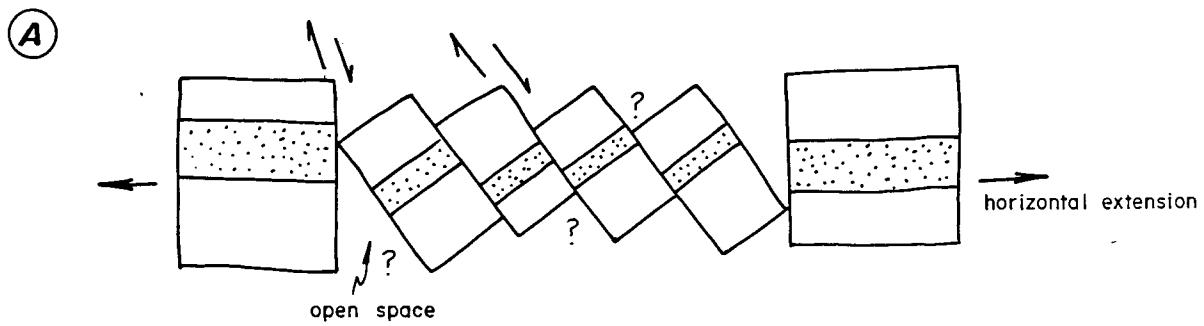
structures within the Hank 2 claim suggest that the major fault is not listric at depth.

R. Brown, P. Eng., of LAC and the writer briefly inspected the area immediately opposite and to the north of the Hank property. The regional dip of bedding in this area is to the southeast and the surface morphology is also similar to that on Hank 4 and Hank 2 claim boundary. It is believed that a major fault scarp is also present in this area which was formed coeval with and sub-parallel to the scarp on the Hank property. This implies that the Hank property is situated within a half graben type feature (Figure 6).

The extensional type tectonic environment which gave rise to the formation of the major Hank 2-Hank 4 normal fault and the sub-parallel fault to the north of the property with the resultant production of a half graben is well documented in structural geology literature (eg. Ramsay, 1967). Extensional regimes of this type have been termed the "domino" or "bookshelf" model. This model demonstrates the sideways collapse of a sequence of fault bounded blocks within an extensional tectonic environment (Figure 6a). In a simplistic model no slip or deformation takes place within each block, each block undergoes a rigid body rotation and the faults remain planar and not listric at depth. However, large openings are produced during rigid rotation of a block and fault geometry constraints imply that such space compatibility problems are not allowable.

Full and half graben structures are commonly associated with regional extension regimes. This phenomenon may lead to the upward migration of fluids. Therefore, the space problem at depth within the bookshelf model may





Section Looking SW

FIGURE 6:

Schematic Bookshelf Model to show the Development of a Half-Graben Structure.
The relative positions of the Hank 1,2,3 claims with the Hank 4 claim are indicated.

A: Extension with resultant space problems.

B: Infilling of Upper Triangular Basins by Volcanic Strata
& possible Magmatic Intrusion into the Lower Block Spaces

be accommodated by the ductile flow of underlying magmatic material into the open spaces produced during extension and the subsequent venting of pyroclastic and volcanic material at surface (Figure 6b).

On the southwest portion of the Hank 3 claim Turna (1988, 1989) has mapped outcrops and talus of dioritic material. Numerous granodioritic float boulders and rare altered dioritic or granodioritic clasts were mapped in the breccia zone outcrops of the "leucocratic" event area of the upper grid portion of the property during the 1989 mapping by HI-TEC. Dioritic banding and brecciation is also reported in the log of diamond drill hole 88-14. The presence of these breccia clasts and the outcrops of diorite? suggests the existence of a magmatic source in the region. The granodiorite and leucocratic volcanic rocks may also have had this common magmatic source. The development of extensional fractures would not be inhibited in such a regime because high fluid pressures associated with such a magmatic source would permit hydrofracturing to occur in the overlying strata.

Many of the breccia clasts in the upper "pipe/sheet" zone are of cobble size and are rounded to sub angular. The exsolution of a fluid phase from a crystallizing magmatic source may rupture the enclosing strata and may vent explosively to the surface at shallow depths (Burnham, 1985). This process frequently causes the formation of breccia pipes and sheet zones which can host rounded intrusive fragments (Allman-Ward et al., 1982). The rounding and brecciation and alteration of the clasts is thought to have occurred during their propagation to the surface by a fluid phase within a breccia pipe or fluid-phase breccia sheet zone which acts as a conduit. This is not termed a diatreme,



sensu stricto, but is a zone of extension and weakness within a volcanic assemblage which forms a channel for the upwelling of underlying material.

There appears to be a correlation between distance from the breccia sheet zone and the intensity of alteration and deformation. The presence of interbedded altered tuffaceous units, some of which appear "aplitic" in outcrop, with progressively decreasing intensity of deformation and alteration away from the breccia zone is indicative of a periodic venting/exhalative environment at the time of deposition.

The final stages of deformation and the initiation of the "leucocratic event" may have occurred once the breccia sheet breached the upper-most strata of the sequence producing a decrease in explosive energy due to a release of confining pressure. This pressure release may correlate with the termination of auriferous mineralization.

From the 1989 mapping, debris flow type units are interpreted to unconformably overlie the leucocratic sequence lithologies. Debris flow movement was presumably initiated by some high energy event or volcanic activity at the last stages of deformation. Late stage reactivation of the fault plane may also be responsible for this unconformable covering.

The exhalative material which infills the uppermost triangular "basins" in the domino model frequently display intraformational unconformities as a result of uneven block rotation rates. Individual strata from the primary extrusion events may also show thickness increases and wedge shapes down dip into the basinal structure. The lower alteration zone of the Hank



property may be analogous to this feature. Later, stratigraphically and structurally higher, infill strata may display a reduction in dip angles. The upper alteration zone may occur within this latter position of the basin infill.

Evidence of intraformational unconformities is found in the creek 3 area, approximately Line 1009N/460E. Here an unconformable contact between unaltered tuff and coarse conglomeratic, possibly agglomeratic material, is exposed in a gully. Altered tuffaceous units above this unconformity are classified as occurring within the lower alteration zone. Other possible unconformable low angle contacts were noted in the creek 6 area near the upper contact of the lower alteration zone.

The creek 3 area appears to have undergone repeated stages of faulting. Poor amounts of exposure and numerous faults in this area of limited outcrop make interpretation of the geology difficult. This zone is in close proximity to the dioritic intrusions mapped by Turna (1989) and has likely undergone additional episodes of faulting related to emplacement of the stocks. Fault orientation and any associated mineralization is likely discontinuous and difficult to define. However, there appears to be a general southward offset associated with the lower alteration zone bottom contact (Figure 4). The faults bounding the intrusion are likely to be steeply dipping.

The formation of half graben structures with steep planar major normal faults, frequently initiate the production of subsidiary faults and structures within the hanging wall basinal-infill strata during later reactivation. Bedding surfaces between different



lithologies may preferentially be the sites of local shearing within the infill units. Evidence for the existence of such structures on the Hank claims has been mapped during the 1989 field season.

At the junction of creek 10 and Hank Creek, an airphoto lineament and topographic linear are interpreted as a fault structure on Figure 4. This lineament may be traced to a 25 cm gouge zone, oriented $014^{\circ}/84^{\circ}$ east, within green volcanics and maroon lava which is exposed at the intersection of creek 8 with the CAT road of the lower alteration zone (approximately Line 2500N/750E). Confirmation of this fault was also made in diamond drill hole 88-21. Turna (1989) reports that this hole intersected the fault at a depth of 227 meters. A fault of similar strike also outcrops near the "chert knoll" at Line 1200N/1850E. The trace of the creek 10 - creek 8 fault may be associated with the latter fault. These structures are interpreted as forming subsidiary faults to the major Hank 4 - Hank 2 fault.

The upper contact of the lower alteration zone in the creek 7 to creek 9 area is marked by another topographic lineament. No exposure exists across the trace of this lineament. Diamond drill hole 88-14 was collared in unaltered andesitic agglomerates on the foot wall side of this subsidiary fault. Dioritic banding and brecciation were noted at a depth of 36 meters in the hole. This provides additional support for the upwelling of magmatic intrusions along fault conduits at depth. The contact of the lower alteration zone in hole 88-14 was at a depth of 71 meters. The upper contact is marked by a gouge zone and core recovery was poor.



On creek 8, an outcrop of green massive unaltered volcanics is exposed in the stream bed at approximately Line 2500N/650E. This hosts a quartz-calcite vein array comprising sigmoidal en-echelon extensional gash veins, with a dextral shear sense, linked and crosscut by oblique shear veins. The vein arrays occur as narrow, subparallel-walled sets within the volcanics. The zones may be classified as brittle-ductile shear zones (Ramsay, 1980). The veins are predominantly infilled with a white calcite/quartz assemblage but pink rhodochrosite staining is evident in places.

Although veins of this type were only exposed in this one locality, the strike orientation of 048^0 of the array was noted in various other outcrops within the lower alteration zone. It is considered valid to infer an overall sense of movement on a locally larger scale (but not regionally) from an interpretation of the geometry and evolution of these vein arrays on outcrop scale.

During the initial shear displacement which produces a system of tension gash arrays, the fissures are oriented perpendicular to the first maximum incremental extension i.e. at an obtuse angle of 135^0 to the shear zone walls. As a consequence of subsequent variations in the amount of shear displacement in the zones from center to edge, the veins become sigmoidal (Ramsay & Huber, 1983; Collins & DePaor, 1986). With increasing shear displacement new cross-cutting veins may form at an angle of 135^0 to the shear zone. The shear veins (oriented at $048^0/90^0$) off-set the sigmoidal extension veins in the creek 8 outcrop and they are oriented at an acute angle of 48^0 (an obtuse angle of approximately 132^0) to the major creek 10 fault (oriented at approximately 005^0 with an assumed dip of 65^0W) as



shown in Figure 7. This relationship to the creek 10 fault and the sigmoidal shape of the cross veins in creek 8 implies that there may be a component of dextral strike slip along this major fault. The veins may form Riedel type shears associated with the creek 10 fault. Therefore, the brittle-ductile textures of the veins in the lower alteration zone were probably induced by the strike slip motion associated with this fault.

Epithermal mineralization is frequently reported from areas of extensional fault-fracture systems undergoing magmatic and/or geothermal activity. Veins textures within such deposits often display a record of repeated extension and precipitation. Ascending magmatic source fluids are not considered critical to the formation of epithermal deposits. The most critical factor is that deposits are formed from dilute to weakly-alkaline chloride water that undergo boiling and fluid mixing as they ascend or migrate laterally (Panteleyev, 1986). However, structurally controlled emplacement of high-level stocks and plutons provide the most suitable fractured environment and geological setting for the formation of epithermal deposits.

The passage of hydrothermal fluids through pre-existing fractures produces structurally controlled zones of alteration. Dilation zones within these structures provide sites for the deposition of precious and base metals. The intrusion of magmatic suites of rocks are coeval with the Upper Triassic Stuhini Group volcanics. Mineralization is also spatially and genetically related to the Stuhini Group volcanics and the intrusive episodes.



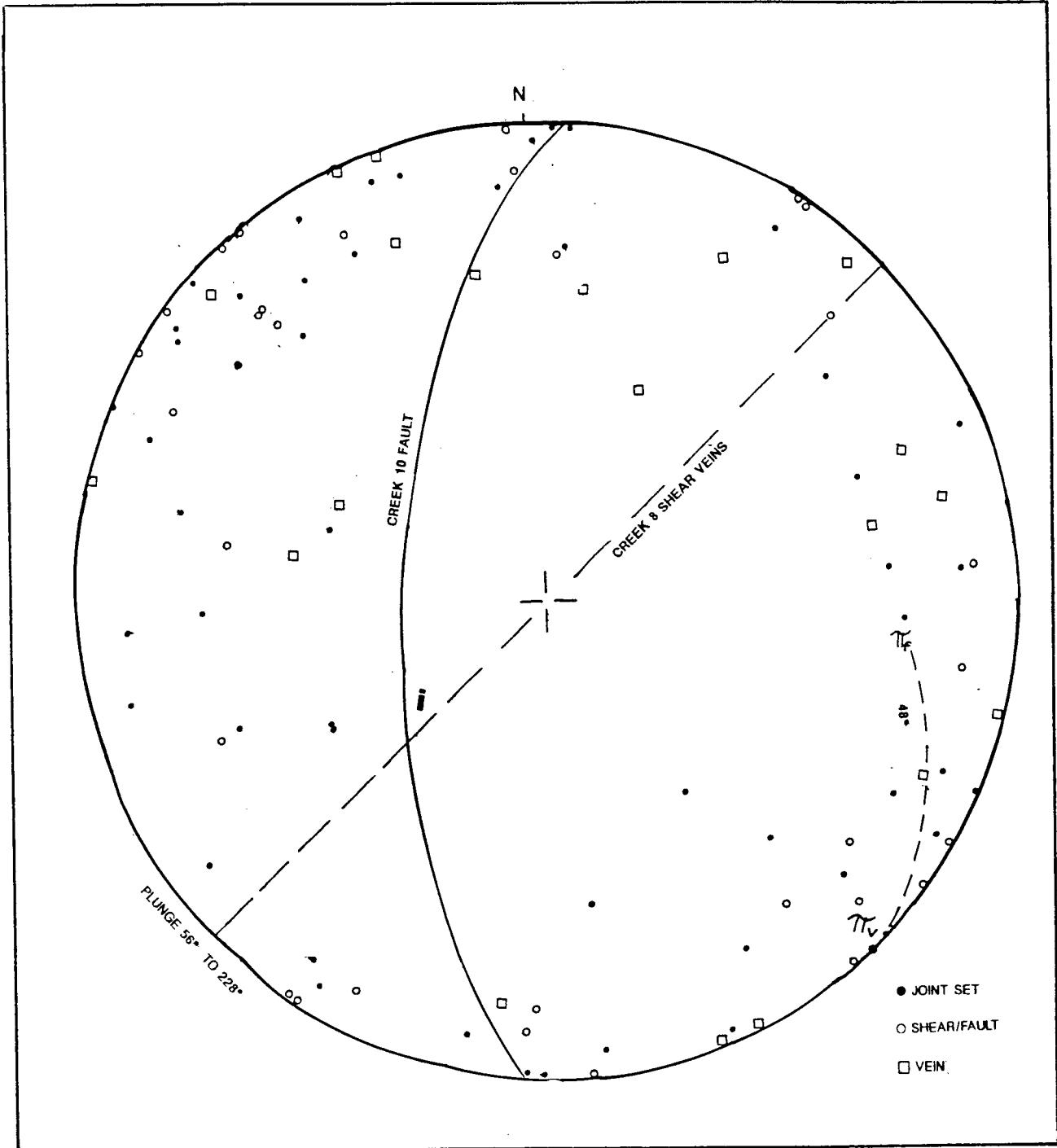


FIGURE 7: Stereoplot of Creek 10 fault/Creek 8 veins and Lower zone data.

The variation in the dips of the upper and lower alteration zones is related to the variation in the types of controlling structures within each zone. The brittle fractures which controlled the upper alteration zone were produced by and during the emplacement and upwelling of fluids. The accompanying "doming" associated with such a high pore fluid pressure event would be accompanied by brittle failure near the surface and the formation of extensional veins. The orientation of the mineralized structures need not have any relationship to the surrounding stratigraphic dip. Steeper dipping structures may be expected to form at deeper depths in the system. The lower alteration zone appears to be fault controlled and cross-cuts the stratigraphy in this area. The presence of a steeper dipping stratigraphy, related to the infill from primary extrusion events, may have localized the position of some of the later faults.

6.0 DIAMOND DRILLING

The drilling contractors were Connors Drilling Ltd. of Kamloops, British Columbia. This company collared all the holes in NQ size core and completed the holes in BQ size core. Problems arose in 5 of the holes due to BQ rods binding and sticking in faults and gouge zones. No problems were encountered while using NQ rods and all future holes should be drilled in NQ size. However, BQ rods should be available on site should any problems arise during deep NQ drilling.

A total of 1610.6 meters were diamond drilled on the claims. All of the core boxes are stored on the property at a leveled site behind the core shack adjacent to hole DDH 88-22.



Each diamond drill hole is summarized below and drill logs, geotechnical logs and geological cross-sections are presented in Appendices IVa, IVb, and IVc respectively. The drill hole layouts are shown in Table 1. The locations of the diamond drill holes are included in Figure 8. The core was logged by Mr. York Ming So under the supervision of the writer.

DDH : 89-1

Bedrock consists mainly of interlayered andesitic breccia, tuffs and flows. Mineralization was confined to the alteration zone and consisted of pyrite, chalcopyrite, sphalerite and galena. There appears to be a correlation between the presence of sphalerite and galena within a vein or gouge zone and anomalous gold values. A geological cross-section which may be overlain with the assay data section in the Brown (1989) report is shown in Appendix IVc. Vein and shear zones are predominantly oriented at steep angles to the core axis. The hole was abandoned at a depth of 95.05m due to down hole problems.

DDH : 89-2

This hole was collared at an angle of -46^0 from the same pad as DDH 89-1 (Appendix IVc). The same stratigraphic sequence as above was intersected. The hole was terminated in intermediate basic volcanic breccia. There is a weakly altered transition zone towards the basal contact of the alteration zone. Some shear zones and veins were intersected that contained appreciable amounts of visible sphalerite and galena.

TABLE 1.
DRILL HOLE LAYOUTS.

Hole Number	Collar Azimuth	Collar Dip	Test Azimuth	Test Dip	Test Depth	Northing	Easting	Elevation	Length (m)	Hole Size	Comments
89-1	320 ⁰	-60 ⁰	310.5 ⁰	-59.5 ⁰	89m	10670.136	10162.749	1116.820	95.05	NQ/BQ	Lost
89-2	320 ⁰	-46 ⁰	319.5 ⁰	-46.5 ⁰	110m	10670.236	10162.349	1116.820	110.03	NQ/BQ	Lost
89-3	320 ⁰	-64 ⁰	315.0 ⁰	-66.0 ⁰	128.6m	10670.036	10163.149	1116.820	130.14	NQ/BQ	Lost
89-4	310 ⁰	-60.5 ⁰	259.5 ⁰	-61.0 ⁰	112.91m	10645.542	10132.445	1110.010	121.91	NQ/BQ	Lost
89-5	310 ⁰	-74.5 ⁰	311.0 ⁰	-75.0 ⁰	156m	10645.342	10132.645	1110.010	157.58	NQ/BQ	Lost
89-6	320 ⁰	-50 ⁰	318.5 ⁰	-51.0 ⁰	110.34m	10573.316	10073.404	1103.950	111.86	NQ/BQ	Lost
89-7	320 ⁰	-70 ⁰				10573.316	10073.404	1103.950	101.20	NQ/BQ	Lost
89-8	313 ⁰	-55 ⁰	333.5 ⁰	-58.0 ⁰	233.25m	10454.401	10037.800	1114.040	233.77	NQ/BQ	Lost
89-9	316.5 ⁰	-62 ⁰	Failed	Failed		11017.406	10434.765	1124.170	270.36	NQ/BQ	Lost
89-10	320 ⁰	-60 ⁰				11449.180	10697.300	1105.270	156.97	NQ/BQ	Lost
89-11	320 ⁰	-65 ⁰				11448.980	10697.500	1105.270	121.62	NQ/BQ	Lost

DDH : 89-3

This hole was drilled to establish a position of the basal contact of the lower alteration zone and to define the continuity of mineralized veins and shears at depth in the Creek 5 area. Pyrite-sericite-carbonate alteration was evident to a depth of approximately 139 meters. The bottom of the hole intersected a series of interlayered unaltered intrusive and extrusive lithologies. Mineralization was largely confined to veins and gouge zones in andesitic breccia horizons. Contacts between contrasting lithologies may have localized shearing to some degree as evidenced by the shearing at a tuff-andesite breccia contact at a depth of approximately 100 meters.

Based on the three drill holes from this site the alteration zone bottom contact appears to dip at 77^0 to the southeast. The lower portions of holes 89-2 and 89-3 are altered and "cooked" by a possible intermediate to mafic volcanic intrusion. Zones of sphalerite-galena-chalcopyrite evident in the core from each hole yielded the best anomalous results. These zones are traceable down dip between holes.

DDH : 89-4

A similar assemblage of andesites and andesitic breccia as above was intersected in this hole. One well developed series of 3mm quartz-carbonate veins within pale green andesite between 53.67 and 54.61m yielded the best anomalous gold values obtained during the drilling program (Appendices IVb and IVc). This andesite was only weakly altered when viewed in the core.

DDH : 89-5

Although many of the veins and gouge zones of DDH-89-4 can be projected into DDH-89-5, the highly anomalous values of hole 89-4 were not repeated in 89-5 (Appendices IVb and IVc). The lower portions of holes 89-4 and 89-5 display the same altered and "cooked" texture as is evident in holes 89-2 and 89-3. This suggests that the intermediate to mafic volcanic intrusion is present in this zone. The footwall to the lower alteration zone dips at approximately 83^0 to the southeast in these holes.

DDH : 89-6

This hole was collared at an angle of -50^0 and intersected the footwall of the lower alteration zone at a depth of approximately 86 m (Appendix IVc). This lower contact is marked by a gouge zone with a core axis of 45^0 . The hole was stopped in intermediate-basic volcanics. An andesitic intrusion was intersected at the contact of the footwall to the alteration zone. This is similar to the intrusion intersected in the previous holes. High angled quartz-carbonate veinlets and gouge zones were intersected in the core. The highest precious metal values were associated with sphalerite-galena mineralization in veinlets (Appendix IVb and Appendix IVc). At 32.62 m a lapilli horizon was intersected which may act as a possible marker bed (see 89-7). No core axis could be measured for the contacts of this unit.

DDH : 89-7

This hole was collared at an angle of -70^0 from the same drill pad as DDH 89-6. The hole was terminated short of it's target depth due to the BQ rods binding and tightening in the hole. At a depth of 35.28 m a



lapilli horizon was intersected which is similar to that recovered in DDH 89-6 (Appendix IVc). Core axes of 30° and 32° were recorded for the upper and lower contacts of the unit, respectively. These contacts appear to be stratigraphic and therefore, the mineralized veins and shear zones in the core cross-cut the stratigraphy.

DDH : 89-8

There is a change in the intensity of alteration and lithology between the previous holes and 89-8. This hole contains an alternating, thinly bedded sequence of more competent grey altered andesites, andesite breccias and tuffs than the previous holes. Two intersections of andesitic dykes or sills within the lower alteration zone were recovered in the core (Appendix IVc). The andesitic intrusion which was intersected at the contact of the footwall to the alteration zone in the previous holes was not present in DDH 89-8.

DDH : 89-9

This hole was collared adjacent to the upper contact of the lower alteration zone. The major portion of this hole appears to be only weakly altered, however, the veining intensity is similar to other holes. Porphyritic andesite was recovered in two places in the upper 65m of this hole. This porphyritic lithology was not found in the previous holes which were collared in the lower portion of the lower alteration zone. At a depth of 235 m, a pinkish, 1 cm wide rhodochrosite veinlet with core axis of 300 was intersected in the core. This marks the top position of a rhodochrosite veinlet zone. This extended to a depth of 270.36 m, at



which point the hole was abandoned due to the BQ rods binding, tightening-up and the near loss of a rod string.

DDH : 89-10

This hole was collared adjacent to the upper contact of the lower alteration zone at an angle of -60^0 . The veining intensity is higher than the previous hole. Porphyritic andesite was not recovered in this hole. Mineralized shears, veins and gouge zones are predominantly oriented at high angles to the core axis. This hole was lost due to binding in a gouge zone at a depth of 156.97m.

DDH : 89-11

This hole was collared from the same site as hole 89-10, at an angle of -65^0 . It was intended that this hole would intersect and penetrate the gouge zone intersected in the previous hole. However, this hole was also abandoned at a depth of 121.62m.

The lower alteration zone drill program has been discussed in an interim LAC Minerals Ltd. report dated November 1989, by R. F. Brown, P.Eng. The current writer endorses the content of this interim report and part of this discussion is included here for completeness. All of the drill sections referred to in the following discussion were included with the interim report and are not appended to the current report.

LOWER ALTERATION ZONE DRILLING 1989

.....In total 1610.6m was drilled in 1989.

Due to broken to shattered outcrop near surface the holes were started using N.Q. rods to a 50 m depth, then converting to B.Q. to finish the hole. This worked very well in penetrating the shattered



surface rocks but faults and gouge zones often hampered B.Q. drilling. Future drilling should be strictly of N.Q. size, this will improve productivity, lessen the necessary parts inventory and lower the gross weight of equipment.

The thrust of the 1989 drilling was to detail one of the high grade areas from previous drilling (namely the 88-4 to 87-3 area) and continue on strike exploration in the lower alteration zone. Holes 89-1 to 89-8 were to test around the 87-3 and 88-4 intersections while 89-9 tested high grade Au, Ag, Pb, Zn carbonate veins in Creek 7 and 89-10, 11 tested the on strike continuation of 88-14 which had a broad "high background" section of Au values.

DISCUSSION OF LOWER ALTERATION ZONE DRILLING

Combined with the holes drilled in 1987 and 1988 and there are now 25 holes in the LAZ. As such, an attempt at interpretation of the mineralization zones is given below.

Interpretation is based primarily on drill core orientations (perpendicular to core axis); intensity of veining, alteration, % pyrite; and abundance of Zn, Pb, Ag, Cu mineralization. Shear-vein outcrops in Creek 5 and 7 along with shears in Creeks 4, 6, 8 indicate a gross NE trend with steep (70^0) SE dip for the mineralization. Drill core orientations were thus preferentially oriented into a steep dip position, the exception is the Creek 5 Flat zone which is interpreted from drill core orientations as a NE trending, $15^0 - 20^0$ SE dipping zone.

Within "high background" sections 11 zones have been defined [Tables #2 and #3 Hi-Tec report]. These zones can be traced vertically from hole to hole (on section) and horizontally from section to section.

The Creek 5 "A", "B", "C", "D" zones are all within a 50 m thick high background section along the north boundary of the LAZ in the section 950 E to 1000 E. area.

Creek 5 "A" zone occurs only in 89-4 and 89-5 on section 950E and consists of a strongly veined area with modest gold values.

Creek 5 "B" zone has modest Au values in holes 89-2 and the deeper 89-1 (section 1000E) but is not correlatable further down dip onto 89-3. There is a strong possibility that a high grade intersection in 89-4 (70.86 g/t Au over 0.63 m) is again the Creek 5



TABLE 2
SUMMARY OF LOWER ALTERATION ZONE INTERSECTIONS
CREEK 5 "A" ZONE

Hole	From (m)	To (m)	Interval (m)	True Width (m)	Au* GMT	Ag ¹ GMT	Pb ¹ %	Zn ¹ %
89-4	20.83	22.93	2.10	1.41	1.37			
89-5?	33.98	35.66	1.68	0.79	5.11	114.9	0.32	1.00
89-5?	38.17	39.48	1.58	0.74	2.51	18.5	0.49	0.68

CREEK 5 "B" ZONE

89-1	61.63	63.19	1.56	1.10	2.74			
89-2	49.00	59.49	1.49	1.60	1.89			
89-4	53.67	54.61	0.94	0.63	70.86			

CREEK 5 "C" ZONE

89-1	82.16	82.37	0.21	0.15	95.28			
89-2	66.71	68.00	1.29	0.85	1.41			
89-3	89.57	92.49	2.92	1.80	1.78	31.20	0.08	0.25
89-4	64.46	70.69	6.23	4.17	5.26			
89-5	96.28	98.40	2.12	1.00	10.22	175.50	0.13	0.13
89-3	45.37	49.38	4.01	3.40	16.83	incomp.	-	0.66

CREEK 5 "D" ZONE

89-1	88.85	92.00	3.12	2.23	0.91			
89-3	98.85	101.91	4.06	2.50	1.60	31.20	0.09	0.35
89-4	78.00	79.00	1.00	0.67	3.53			
89-5?	117.70	118.84	1.24	0.58	5.86	93.90	0.02	0.04

CREEK 5 "88-4 DEEP"

88-4	117.85	316.99	9.14	5.88	13.39	132.30	1.00	1.57
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* Au Intersection uses Fire Assay and Metallic Assay Data

1 Ag, Pb, Zn Intersection uses Fire Assay and Geochemical Analysis

TABLE 3
SUMMARY OF LOWER ALTERATION ZONE INTERSECTIONS
CREEK 5 "FLAT" ZONE

Hole	From (m)	To (m)	Interval (m)	True Width (m)	Au* GMT	Ag ¹ GMT	Pb ¹ %	Zn ¹ %
89-6?	57.84	59.10	1.26	1.18	1.16			
89-7?	46.91	48.84	1.93	1.92	3.40			
89-8	84.77	86.31	1.54	1.47	5.51	144.20	0.68	1.29
89-4	140.00	143.00	3.00	2.93	18.27	132.90	0.04	0.08
88-22	47.58	49.98	2.40	2.38	4.97	123.40	0.08	0.13

CREEK 5 "88-6 DEEP" ZONE

88-6	376.43	376.43	1.97	1.10	66.19	530.40
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CREEK 8 "A" ZONE

89-9?	High Background							
89-10	80.00	82.00	2.00	1.29	3.15	30.50	0.04	0.17
89-11	82.00	89.42	7.42	4.26	5.77	35.20	-	0.44
88-14	166.64	167.64	1.00	0.50	2.14			

CREEK 8 "B" ZONE

89-11	106.27	108.66	4.15	2.38	12.00	257.20	-	0.98
88-14?	191.00	192.00	1.00	0.50	3.19	3.19	0.06	1.43
88-14	195.00	198.00	3.00	1.50	3.12	13.5	0.05	0.41

CREEK 8 "C" ZONE

88-14?	227.00	229.00	2.00	1.00	2.38	11.5	0.03	2.77
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CREEK 8 "D"

89-10	153.95	156.07	2.12	1.36	1.36	23.5	0.74	2.05
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* Au Intersection uses Fire Assay and Metallic Assay Data

¹ Ag, Pb, Zn Intersection uses Fire Assay and Geochemical Analysis

"B" zone. Unfortunately the high grade in 89-4 is not traceable up dip to 87-3 or down dip to 89-5.

Creek 5 "C" zone is the strongest most continuous vein-shear system and is found on section 950E in holes 87-3, 89-4 and 89-5. The best values and widths are in the upper two holes. On section 1000 E Creek 5 "C" zone is narrower and of lesser Au grade.

The Creek 5 "D" zone on section 1000 E is found in 89-1 and 89-3 and is open to depth and N.E. True widths of approximately 2.5 m were intersected although gold grade is low. To the SW on section 950E "D" zone was narrower with intersections in 89-4 and 89-5 again gold grade is low.

The Creek 5 "88-4 Deep" Zone seems to occur in a NW flexure of the north side of the LAZ on section 800E. Updip projection of 100 m to 88-22 shows a "high background" section with low gold values. Updip and to the S.W. hole 89-8 (section 750E) has no significant values and no similar flexure in the LAZ.

The Creek 5 "Flat" zone was intersected by five holes. Holes 89-8 (section 750E) and 88-4 and 88-22 (section 800E) have good core orientations to suggest this "flat" feature, striking NE, dipping 150 - 200 SE. The intersection on section 850E lines up well with the implied flat zone orientation but the core orientations are less affirmative (i.e. lost core in 89-6). Widths are from 1-3 m with the best grade in 88-4 (18.27 g/t Au/2.93 m), the other four holes had modest grades.

The Creek 5 "88-6 Deep" zone was not tested in 1989. The intersection is on section 1100 E in an area of high background values. Updip holes 88-19, 19A did not intersect the high background values. This zone is open on strike as it is SE of the Creek 5 A to D zones.

The Creek 8 "A, B, C, D" zones are found within a 50 meter wide high background area in relative proximity to the SE side of the LAZ. Connection of the zones between section 1800E and 1925 is tenuous at best. Nonetheless, using the postulated linear contact (fault) of the LAZ, a NE zone trend and an assumed steep SE dip, zones were connected between sections.

Creek 8 "A" zone is narrow and low grade in hole 88-14 on section 1800E. On section 1925E holes 89-10



and 89-11 are drilled close together. Hole 89-10 is believed to be drilled nearly down a strong fracture system and was terminated in a gouge zone. Hole 89-11 was an attempt at a steeper angle to penetrate deeper than 89-10 but failed in a gouge zone well short of its projected mark. Although both holes intersected the high background area high grade shear-vein zones cannot be projected hole to hole.

Creek 8 "B" zone on section 1925E shows a vast difference between the deeper 89-11 (strong vein-shears, 2.38m @ 12.0 g/t Au) and 89-10, 14 meters updip which is high background. On section 1800E, hole 88-4 intersected a wide zone of modest values which may be "B" zone.

Creek 8 "C" zone is a modest gold intersection only in 88-14 on section 1800E.

Creek 8 "D" zone is a modest gold intersection on section 1925E, which in only partially tested by hole 89-10 before the hole was lost in a gouge zone.

Several other "high background" sections exist elsewhere in the LAZ which are potential targets for high grade vein-shear zones. In particular are the high background sections in holes 89-9 (at the end of the hole) and 88-12A on sections 1450E and 1550E, these sections may be the SE continuation of the Creek 8 A, B, C, D zones 250 m to the NE.

Of interest is the observation that the S.W. portion of the LAZ (SW of 88-8) has high background sections and vein-shears with Pb-Zn-Au, Ag, Cu values while NE of 88-8 the high background sections and vein shears are prominently Zn, Au, Ag with minor Pb, Cu.

....The best intersections are summarized in Table[s #2 and #3.]

.....There are several targets which have good strike and dip length potential that still have to be adequately detailed. Namely the Creek 5 "flat" zone; Creek 5 "Deep 88-4" zone; Creek 5 "Deep 88-6" zone; down dip and NE strike extension of Creek 5 "A-D" zones; and the NE and SW extensions of the Creek 8 "A-D" zones. This would entail an extensive drill program covering over 1100m of LAZ strike length, drill down dip over 300 meters.



7.0 GEOCHEMISTRY

One hundred and sixty-eight rock samples and eight hundred and fifteen core samples were collected and all of the samples were submitted to Bondar-Clegg & Company Ltd., in Vancouver, British Columbia. All of the rock samples and four hundred and seventy-eight core samples were analyzed for Au (plasma), Ag, As, Cd, Cu, Fe, Mn, Mo, Ni, Pb, Zn, Hg and Sb by geochemical methods. Three hundred and thirty-seven core samples were analyzed by geochemical methods for gold. Selected core samples were additionally analyzed gold and silver by the Fire Assay (F.A.) technique. Analytical procedures are reported in Appendix II and analytical data can be found in Appendices IIIb and IVb.

Statistical treatment of data was possible for each analyzed element. Statistical methods, data, correlation coefficients, histograms and scatter plots are listed in Appendices IIIc and V for rock and core samples respectively.

The relationships between various elements are provided by the correlation coefficient matrices and scatter plots for the rock and core samples in the latter Appendices. A scatter plot of Au GMT against Au ppb for all of the rock samples is included in Appendix IIIc (File: AuRock). There is a strong linear relationship for the data set in the lower value range up to 10,000 ppb.

Au values of 10,000 ppb were removed from the data set prior to additional statistical analysis. There is a moderate to strong correlation between Au, Ag and Pb content in the rock samples. Ag and Hg also show a moderate correlation (Appendix IIIc, File: Rock).



A histogram of the gold values for the rock samples, showing the frequency of values and the total number of Au values, is provided in Appendix IIIc (File: STROCK).

Six of the diamond drill holes had their samples analyzed for multi-elements. The correlation coefficients for eight of these element variables were calculated and are provide in Appendix V. In DDH 89-3, there is a strong correlation between the Zn and Hg values. Au and Ag show a moderate to strong correlation. Au-Pb and Ag-Cu have moderate correlations. In DDH 89-5, Au-Ag and Pb-Zn rate strong correlations while Ag-Hg, Ag-Cu, Ag-Zn, Ag-Pb and Cu-Zn rate moderate correlation coefficients. Similar results are provided by the correlation coefficients matrices for holes DDH 89-8, 9, 10, and 11. Overall there appears to be only a weak correlation between As and Au.

A histogram of the all the gold values for all of the diamond drill hole samples, showing the frequency of values and the total number of Au values, is provided in Appendix V (File: HistDDH).

Scatter plots of Au GMT against Au ppb for most of drill hole samples is included in Appendix V. There are strong linear relationship for the data sets.

8.0 CONCLUSIONS

The proposed model is based on mapping and drilling conducted on the Hank property during the 1989 field season and previous work by R. Turna. Insufficient



exposure in the upper grid zone of the property precludes definitive statements regarding the origin of the textures and lithologies in the area. Many of the events outlined above were approximately coeval and form part of the one event.

The Hank claims mineralization forms part of a large epithermal system which has been obliquely cut by glacial erosion. Deformation and volcanism must have occurred within narrow time constraints. The main Hank 2 - Hank 4 fault appears to provided structural control for and the physical limits to the mineralizing system to the east. The potential of volcanic conduit related mesothermal veins at depth exists and should be drill tested. High level stocks with the potential of associated porphyry mineralization may also have formed at depth in the Hank 2 - Hank 4 fault conduit zone (Figure 9).

This fault zone may provide a similar environment for mineralization to that which exists on the Calpine/Consolidated Stikine's Eskay Creek property. If the mineralization in the contact zone of the latter property is epigenetic in origin then the potential for a similar zone, at the contact of the leucocratic volcanics and volcano-sedimentary footwall assemblage along the Hank 2 - Hank 4 fault zone, exists.

Mineral deposition paragenesis on the Hank property tentatively appears to have been (a) precipitation of pyrite (b) deposition of quartz-carbonate veins in several stages and (c) deposition of sphalerite, galena, chalcopyrite and micron-size gold. Additional mineralogical analysis would have to be conducted to verify the paragenesis and genetic model for the deposit.



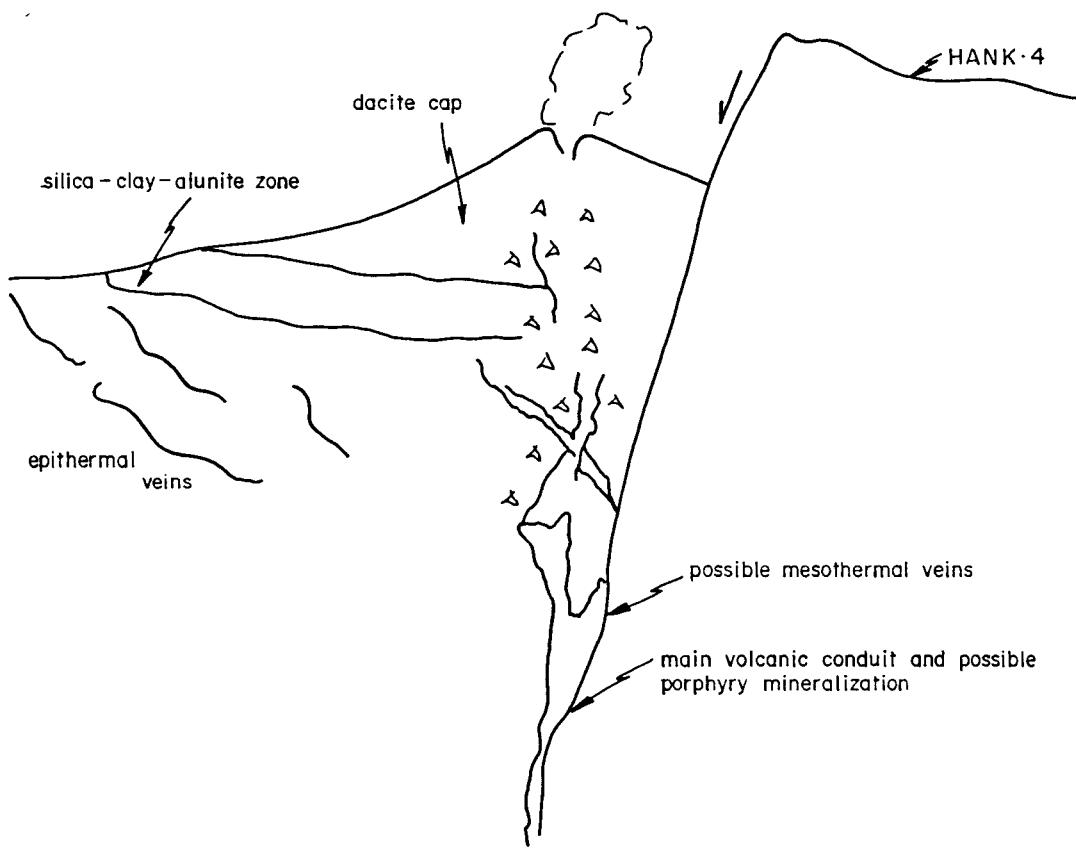


FIGURE 9: SCHEMATIC DIAGRAM OF TYPES OF POTENTIAL MINERALIZATION

The contacts of the lower alteration zone and the mineralized veins and shear zones within it cross-cut the stratigraphic dip as evidenced by the lapilli horizon in holes 89-6 and 89-7.

The lower alteration zone appears to be within a structurally controlled block. Complex faulting occurs in the west of the zone due to the intrusion of dioritic stocks. This portion of the alteration zone has only been tested by hole 88-23 to date. This was collared at an angle of -62° to test a strong bulls-eye chargeability anomaly (Turna, 1989). Highly pyritic alteration zone rocks with occasional elevated gold values were intersected. The footwall to the lower alteration zone was intersected at a depth of approximately 220 meters in this hole. This concurs with the pattern of southward stepping faults which were mapped in this area during the current exploration program. This portion of the lower alteration zone, west of creek 4, has not been adequately tested by drilling in previous programs.

Respectfully submitted,
HI-TEC RESOURCE MANAGEMENT LTD.



Denis A. Collins, Ph.D., P.Geol., F.G.A.C.

January, 1990



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APPENDIX I
STATEMENT OF QUALIFICATIONS



STATEMENT OF QUALIFICATIONS

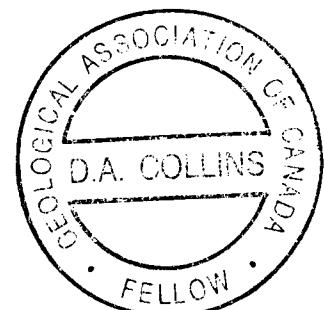
I, DENIS A. COLLINS, of the District of North Vancouver, Province of British Columbia, hereby certify:

1. THAT I am a geologist employed by Hi-Tec Resource Management Ltd. at 1500-609 Granville Street, Vancouver, British Columbia, Canada, V7Y 1G5.
2. THAT I obtained a Bachelor of Science degree in Geology from University College Cork, Ireland in 1980 and a Ph.D. in Structural Geology from the same university in 1985.
3. THAT I have been practicing my profession as a geologist in Ireland, South Africa and Canada since 1980.
4. THAT I am a Fellow, in good standing, with the Geological Association of Canada.
5. THAT I am a registered Professional Geologist, in good standing, with a license to practice, with the Association of Professional Engineers, Geologists and Geophysicists of the Northwest Territories.

Dated in Vancouver, British Columbia, this 9 th day of January, 1990.

Denis Collins

Denis A. Collins, Ph.D., P. Geol., F.G.A.C.



APPENDIX II

GEOCHEMICAL PREPARATION AND ANALYTICAL PROCEDURES



LABORATORY AND ANALYTICAL METHODS

Geochemical samples were processed by Bondar-Clegg and Company Ltd. at 130 Pemberton Avenue, North Vancouver, B.C., V7P 2R5 employing the following procedures.

After initial preparation, samples were analyzed by the Inductively Coupled Plasma (ICP) method. Gold was determined by the fire assay and atomic absorption method.

Rock/core samples were put through a jaw crusher and a ceramic-plotted pulverizer.

For ICP analyses, 1.0 gram of sample material was digested for 6 hours with a hot HNO_3 - HClO_4 mixture. After cooling, samples were diluted to a standard volume. The solutions were then analyzed by a computer-operated Jarrell Ash ICP Analyzer. Reports are formatted by a route computer dotline printout.

For Au analyses, a suitable sample weight of 15 or 30 grams was fire assay preconcentrated. Samples were then digested with an Aqua Regia solution and then taken up to suitable volume by adding a 25% HCl solution. Further oxidation and treatment of at least 75% of the original sample solutions are made suitable for extraction of gold with methyl isobutyl ketone. Gold is analyzed by Atomic Absorption instruments using a suitable standard solution. The detection limit is 1 ppb.

APPENDIX IIIa
ROCK SAMPLE DESCRIPTIONS



ROCK SAMPLE DATA HANK CLAIMS, Hi-Tec Project No.: 89-BC-019

Total Number of rock samples : 168

SAMPLE NO.	LOCATION	DESCRIPTION
89 Hank	5001 K1 88-22 Start at K1 east side of road. 1.5m sample. 0/1.5m DB 3m thick, alt tuff, local maroon clast, py<5% disseminated blebs & fracture fillings. Alt int=7, pale whiteish grey.	
89 Hank	5002 1.5/3m N 1.5m long. Rock as above.	
89 Hank	5003 3/4.5m N 1.5m long. Rock as above.	
89 Hank	5004 Creek 8 Grab of carbonatized/silicified green pyroclastic tuff. Sample is of rare calcite veinlet found within rusty green/grey o/c. 5% py	
89 Hank	5005 Creek 3 Highly weathered pyroclastics. No mineralization.	
89 Hank	5006 Creek 3 Pyroclastics, no mineralization.	
89 Hank	5007 Creek 3 Pyroclastics, <1% pyrite, manganese stain.	
89 Hank	5008 Creek 3 Alteration zone, sample is carbonatized and silicified, with 2% pyrite.	
89 Hank	5009 Creek 3 Bleached altered rock.	
89 Hank	5010 L27N/75E 1m chip from face of rusty buff weathered grey/white altered sericitic tuff. Sample is highly weathered & leached with minimal sulphs	
89 Hank	5011 Creek 8 Taken 11-15.5m N of L26N intersection with creek 8. 4.5m long chip, consisting of 0.5% Pyrite, fair limonite stain at joints (2%).	
89 Hank	5012 Creek 3 L1200N, 29SE. 5m chip, across part of outcrop. Fine grained tuff, 0.5% to 1.0% Pyrite showing CB alteration.	
89 Hank	5013 Creek 3 S wall of creek, 4m chip of fn gr tuff, 0.5% - 1.0% Pyrite, unit is competent and unaltered.	
89 Hank	5014 Creek 3 4m long. Rock as above.	
89 Hank	5015 Creek 3 (99m up from '14) Grab sample from strongly altered whitish tuff, 3% Pyrite as cubes.'	
89 Hank	5016 Creek 3 (142m up from '14) 2m chip sample from S wall of strongly CB altered, white rock, with 5% Pyrite as cubes.	
89 Hank	5017 Creek 3 (228m up from '14) 1.5m chip sample from S wall of Rock as above.	
89 Hank	5018 L19N/168E 4.0m long chip. Sample is of unaltered intermediate volcanics, weathered clastic tuffaceous unit with no sulfides.	
89 Hank	5019 L1907N/ 275E 4.0 m long chip. Rock as above, except with tr. to 0.5% Pyrite.	
89 Hank	5020 L1900N/ 708E Grab sample from grey, unaltered andesitic volcanic rock. No sulfides.	
89 Hank	5021 L2100N/ 464E 3m chip sample, from altered rock with limonite and pyrite.	
89 Hank	5022 L2100N/ 467E 3m chip sample. Rock as above.	
89 Hank	5023 L2100N/ 442E Grab sample. Rock as above.	
89 Hank	5024 L2100N/ 424E (E wall). Grab sample from, altered competent outcrop, with 2.5% Pyrite and limonite.	
89 Hank	5025 L2100N/ 379E Grab sample from light green, grey, moderately altered tuff containing a trace of pyrite.	
89 Hank	5026 L2500N/ Grab sample from outcrop of white altered	

	304E	rock, containing 2.5% quartz, carbonate veins with a trace pyrite and 1% limonite.
89 Hank	5027 L2500N/ 328E	4m chip sample from altered rock, containing a trace pyrite and 2% limonite.
89 Hank	5028 L2500N/ 332E	4m chip sample. Rock as above.
89 Hank	5029 L2200N/ 400E	(73m E of Co-ord) Grab sample from fine grained pale yellow, brown clastic rock (tuffaceous ?). Sample contains 1% Pyrite.
89 Hank	5030 L2013N/ 483E	3m chip sample, outcrop under 10cm of overburden, unit is strongly altered with 5% pyrite and limonite.
89 Hank	5031 L2600N/ 142E	(10m W of Co-ord) 4m chip sample from whitish altered rock containing 3-5% limonite.
89 Hank	5032 L2600N/ 142E	(14m W of Co-ord) 4m chip sample. Rock as above.
89 Hank	5033 L2600N/ 22E	(6m SW of Co-ord) 4m chip sample across weakly altered, light green, grey, white, clastic tuff, with a trace pyrite and 2.5% to 5.0% Ti-oxides.
89 Hank	5034 Creek 5 89-TR-1	(0.0m - 1.4m) Grab sample from CB altered grey clay zone. Samples contain 1% CB veins with galena, sphalerite, chalcopyrite, and pyrite.
89 Hank	5035 Creek 5 89-TR-1	(1.4m - 2.4m) Rock as above.
89 Hank	5036 Creek 5 89-TR-1	(2.4m - 3.4m) Rock as above.
89 Hank	5037 Creek 5 89-TR-1	(3.4m - 4.9m) Rock as above. Unit is less clay altered, more CB and pyrite altered, more competent.
89 Hank	5038 Road ~ 1835N/675E	Grab. Mafic unit, (dyke?), light green, dark green altered minerals (hbl). Weakly altered, no sulfides.
89 Hank	5039 Road ~2000N/690E	Grab. Andesite lava, pale green, moderate alteration, with carbonate(green) and chert (milky) amydales. Unit is sheared, contains 1% pyrite cubes.
89 Hank	5040 Creek 4	Float. Carbonate alteration, veining. Abundant py. Occ weathered at margins.
89 Hank	5041 Creek 4	Composite sample of float from creek. Calcite veining with py/gn. Some 2cm long crystals of calcite.
89 Hank	5042 Creek 4	D/C? Cavy. veining at base of alteration zone. Py, Po, GN in calcite. Orientation 072/90
89 Hank	5043 Creek 4	Thin Calcite vein x-cutting 1m wide shear zone.
89 Hank	5044 Creek 6	Float sample. Abundant massive Py around altered nodule approx. 10cm long.
89 Hank	5045 Creek 8	Vein sample. Pinkish tinge with trace Gn/Py Host is massive green volc. clastic.
89 Hank	5046 Creek 8	Massive Py in siliceous nodule up to 0.5m diam. Prov. incorporated within movement zone. Sample is composite chip over 3m parallel to NE side of creek and 1m perpendicular to creek
89 Hank	5047 Road ~ 2005N/685E	4.5m chip sample, of andesite lava, light green with limonitic clots (alt py) to 1% and minor amydales.
89 Hank	5048 Road ~ 2005N/685E	4.5m chip sample. Rock as above.
89 Hank	5049 Road ~2012N/670E	2.5m chip sample, of andesite lava, green with manganese oxide (black) amydales to 5%, generally 3 - 4cm in diameter.
89 Hank	5050 Road by ~L2600N/ 477E	3m chip sample, of green - grey andesite volcanic with 0.3% - 1.0% pyrite.

89 Hank 5051 As 3m chip sample. Rock as above.
Above

89 Hank 5052 Road 3m chip sample. Green intermediate volcanic with Creek 8E limonite and a trace pyrite.

89 Hank 5053 Road " 3m chip sample. Rock as above.

89 Hank 5054 Road " 3m chip sample. Rock as above.

89 Hank 5055 Road " 3m chip sample. Shear, altered, white with 10% limonite.

89 Hank 5056 Road " 3m chip sample. Rock as above.

89 Hank 5057 Road 1.2m chip sample of white altered rock, containing ~L2840N/250E 10% limonite, no pyrite (vuggy remnants) and 50% OB.

89 Hank 5058 Road 2.0m chip sample of fine grained Andesite, light ~L2590N/225E whitish grey, moderately altered.

89 Hank 5059 Road " 2.0m chip sample. Rock as above.

89 Hank 5060 Road " 2.0m chip sample. Rock as above.

89 Hank 5061 Road " 2.0m chip sample. Rock as above.

89 Hank 5062 Road " 2.0m chip sample. Rock as above.

89 Hank 5063 Road " 2.0m chip sample. Rock as above.

89 Hank 5064 Road 2.0m chip sample, of moderately altered intermediate or ~L2550N/440E andesitic volcanic, greenish grey in color, fine grained, with 2.5% pyrite and 5.0% limonite.

89 Hank 5065 Road " 2.0m chip sample. Rock as above.

89 Hank 5066 Road " 2.0m chip sample. Rock as above.

89 Hank 5067 Road " 2.0m chip sample. Rock as above.

89 Hank 5068 Road " 2.0m chip sample. Rock as above.

89 Hank 5069 Road " 2.0m chip sample. Rock as above.

89 Hank 5070 Road 5.0m chip sample, of green lava containing 5.0% pyrite ~L2000N/650E as amygdales and fracture fill. Very limonitic.

89 Hank 5071 Road " 5.0m chip sample. Rock as above.

89 Hank 5072 Road " 5.0m chip sample. Rock as above.

89 Hank 5073 Road " 5.0m chip sample. Rock as above.

89 Hank 5074 Road " 3.0m chip sample. Rock as above.

89 Hank 5075 Road 0.4m chip sample, of green lava with 10% pyrite. ~L2005N/620E

89 Hank 5076 Road Grab sample from white altered rock, containing ~L2070N/500E 5.0% pyrite stringers, OB and sericite.

89 Hank 5077 Road 2.0m chip sample of pale green altered andesite with ~L2058N/472E 0.5% pyrite.

89 Hank 5078 Road 2.0m chip sample. Rock as above. ~L2062N/466E

89 Hank 5079 Road Grab sample. Taken from outcrop of altered whitish rock, ~L2162N/515E containing 5.0% pyrite cubes.

89 Hank 5080 Upr Grid 2m chip across outcrop face. Sample is of rusty weathered, grey fresh, silicified porphyroclastic tuff. Sample contains <3% fine dis. pyrite. Unit is generally massive, highly fractured.

89 Hank 5081 Upr Grid Grab sample from outcrop of fine - medium grained porphyroclastic tuff. Unit is red to buff weathered, dark grey fresh, and contains minor calcite and siderite. Sample contains <1% pyrite.

89 Hank 5082 Upr Grid 1m chip across outcrop of dark grey fine grained silicified tuff. Sample contains up to 6% pyrite as blebs.

89 Hank 5083 Road Grab sample? Taken from outcrop of altered whitish rock ~L2168N/506E containing 5.0% pyrite cubes.

89 Hank 5084 Road 2.0m chip sample taken from pale green to Creek 7 whitish grey altered andesite, sample contains 5.0% pyrite.

89 Hank	5085 Road "	2.0m chip sample. Rock as above.
89 Hank	5086 Road "	2.0m chip sample. Rock as above.
89 Hank	5087 Road "	2.0m chip sample. Rock as above.
89 Hank	5088 Road "	2.0m chip sample. Rock as above.
89 Hank	5089 Road "	2.0m chip sample. Rock as above.
89 Hank	5090 Road "	2.0m chip sample. Rock as above.
89 Hank	5091 Road "	2.0m chip sample. Rock as above.
89 Hank	5092 Road "	Grab sample taken from outcrop of 12cm barite vein, containing 5% sphalerite, galena, TT bornite and 2.5% pyrite. Vein contains some quartz vugs.
89 Hank	5093 Road "	Select sample. Rock as above.
89 Hank	5094 Road	1.0m chip sample from outcrop of light green - grey moderately altered andesite, containing 5.0% pyrite and localized lenses (2mm to 30mm thick) of sphalerite and galena.
89 Hank	5095 Road "	1.0m chip sample. Rock as above.
89 Hank	5096 Road "	1.0m chip sample. Rock as above. (5.0% SP+GN)
89 Hank	5097 Road "	1.0m chip sample. Rock as above. (2.5% SP+GN)
89 Hank	5098 Road "	1.0m chip sample. Rock as above.
89 Hank	5099 Road	(0m - 1m) 1.0m chip sample, across outcrop of 10cm Creek 7 Trenching to 30cm wide vein. Vein is composed of barite with minor quartz and calcite, 5.0% - 10.0% pyrite and local masses of galena, sphalerite, TT and MA.
89 Hank	5100 Road "	(1m - 2m) 1.0m chip sample. 2.5% grey sulfides.
89 Hank	5101 Road "	(2m - 3m) 1.0m chip sample. 5.0% grey sulfides.
89 Hank	5102 Road "	(3m - 4m) 1.0m chip sample. 10% galena and sphalerite.
89 Hank	5103 Road "	(4m - 5m) 1.0m chip sample. Barite vein, 1.0% pyrite.
89 Hank	5104 Road "	(5m - 6m) 1.0m chip sample. Rock as above.
89 Hank	5105 Road "	(6m - 7.3m) 1.3m chip sample. Rock as above.
89 Hank	5106 Road "	(12.2m - 13m) 0.8m chip sample. 60% GN, 2.5% Ti-oxides 0.5% SP.
89 Hank	5107 Road "	(13m - 14m) 1.0m chip sample. 10% Ti-oxides, 5% GN+SP.
89 Hank	5108 Road "	(14m - 15m) 1.0m chip sample. 30% grey sulfides.
89 Hank	5109 Road "	(15m - 16m) 1.0m chip sample. 3.0% grey sulfides.
89 Hank	5110 Road "	3.0m chip sample perpendicular to above at 8.2cm. Light to pale grey altered andesite with 5.0% pyrite.
89 Hank	5111 Road "	2.0m chip sample perpendicular to above at 12 cm. Rock as above.
89 Hank	5112 Creek 5	1.0m chip sample across an outcrop of a quartz, barite vein stockwork, within a dark grey weathered, grey green fresh, coarse grained (tuff) agglomerate. Sample shows strong chloritization and contains 6% pyrite as stringers and blebs. Manganese stain is present along fractures.
89 Hank	5113 Creek 4	Altered tuff with massive & stringer pyrite. May be incorporated within shear zone 15cm thick. Lenticular nodules of variable comp. with 2mm veinlets in places. Abundant py in overlying beds
89 Hank	5114 Creek 4	Carb-ser alt. material with relict lapilli.
89 Hank	5115 Creek 4	Maroon/green alt. material. Maroon portions more siliceous. <4% py.
89 Hank	5116 Creek 5	1.0m grab sample, across grey clay altered outcrop 89-TR-1 hosting unaltered tuffaceous clasts and minor carbonate veins. NVM.
89 Hank	5117 Creek 5	1.0m grab sample, across grey clay altered outcrop 89-TR-1 hosting unaltered tuffaceous clasts and to 75% mineralized carbonate veins (GN>PY>SP>CPY).
89 Hank	5118 Creek 6	Barite veining + abundant py-dissemination vugs <1cm diam. Maroon siliceous laminae.

- Agglomerate associated with veining.
- 89 Hank 5119 Creek 6 1.0m chip sample across outcrop of a silicified unit with 5.0% pyrite and 1.0% grey sulfide.
- 89 Hank 5120 Creek 6 Gouge and altered tuffaceous unit. Chloritic with < 5% disseminated py.
- 89 Hank 5121 Creek 6 Float in creek base. Gr volcanic breccia with calcite matrix. Galena/py infilling vugs. Breccia clasts <0.5cm.
- 89 Hank 5122 Creek 7 2m down stream from "vein 2229" Disseminated galena/sp/py in altered volcanics.
- 89 Hank 5123 Site 6 Float. Galena/py/cp rich calcite/barite vein material. Same as Galena vein 2229 Creek 7.
- 89 Hank 5124 Creek 4 0.40m chip sample across outcrop of rusty purple weathered, white fresh Barite>Quartz>Calcite vein L1253N/607E vein, sample contains <6% pyrite, minor limonite.
- 89 Hank 5125 Creek 4 1.0m chip sample perpendicular to rusty weathered white fresh, Barite>Quartz>Calcite vein, which is hosted by a silicified, strongly altered white tuff(?). Sample contains <3% pyrite, <1% galena, minor malachite. L1250N/607E
- 89 Hank 5126 Creek 4 Grab sample from outcrop of rusty weathered, white L1243N/606E fresh, very strongly silicified, altered tuff(?). Sample contains <4% pyrite as blebs and along fractures, <1.5% galena as blebs. Minor carbonate as "blasts".
- 89 Hank 5127 Creek 4 Grab sample from outcrop located approx. 5m, down cliff North face. Sample is 0.04m wide quartz veinlet, rusty weathered and white fresh, within silicified/ altered tuff(?). Sample contains 5% pyrite, 10% limonite and <1% grey sulfide.
- 89 Hank 5128 Creek 4 Grab sample from rubble, of rusty weathered, white/grey North fresh, quartz>barite>calcite vein with up to 6% pyrite, bank. 6% limonite and , <2% grey sulfide.
- 89 Hank 5129 Creek 4 1.00m chip sample across rusty weathered, white North grey fresh, 0.40m wide barite vein, within altered bank. tuff(?) host. Sample is barite>quartz>calcite with abundant limonite, <2% pyrite and <2% grey sulfide.
- 89 Hank 5130 Creek 4 Grab sample from outcrop of 0.10m wide quartz>calcite>barite North bleb, within altered tuffaceous(?) host. Sample contains bank. <4% pyrite and <3% galena as blebs.
- 89 Hank 5131 Creek 3 0.40m chip sample across rusty, black weathered, white L1009N (?) fresh, erosive, altered(?) or sheared(?) tuff. 498E Sample contains <20% limonite, <2% pyrite and abundant carbonate as massive "blebs" to 0.5cm.
- 89 Hank 5132 Creek 3 2.00m chip sample across buff, brown weathered, L1010N boulder conglomerate, with rusty weathered matrix. 498E Boulders consist of light green fresh, fine grained unaltered tuffaceous material with <2% pyrite/limonite.
- 89 Hank 5133 Creek3 1.50m chip sample across black weathered, grey L1015N fresh, fine grained tuff with <2% pyrite and limonite. 500E
- 89 Hank 5134 Creek 3 Grab sample from outcrop of 15cm to 20cm wide calcite, L1015N quartz vein hosted by altered tuffs. Sample contains 605E approximately 6% pyrite, 3% malachite, 1% azurite, 1% chalcopyrite, 1% galena and up to 10% limonite.
- 89 Hank 5135 Upr Grid Grab. Road cut/trench, grey/white clay with weathered felsite? ~L2000N/1725E, road cut
- 89 Hank 5136 Upr Grid 2.7m chip. Clay, abundant clasts of rusty weathered gy-brown Road cut silicified felsite? Abundant limonite, minor cherty fragments
- 89 Hank 5137 Upr Grid Grab. Cherty zone along road cut. <2% py, <6% limonite.

Road cut
89 Hank 5138 Upr Grid 1m chip in clay zone. Leached limonite, minimal chert clasts
Road cut
89 Hank 5139 Upr Grid Grab. Clay, 35% limonite seams, 3% chert clasts, <3% py.
Road cut
89 Hank 5140 Upr Grid 3m chip. 80% dacite, rusty weathered light gy, Dark gy
~L2100N/1800E cat road when fresh, <1% py.
89 Hank 5141 Upr Grid Grab. rusty weathered grey fresh O/C. <2% py, cherty.
Cat road
89 Hank 5142 Upr Grid Grab. Felsite, fine/med grained, porphroblastic, siliceous,
Cat road 2% py disseminated.
89 Hank 5143 Upr Grid Grab. Breccia with flow type banding, white/buff, light gy when
Cat road fresh, fine/coarse grained, <4% hem staining, <1% py as
fracture filling, Up to 10% chert in outcrop.
89 Hank 5144 Upr Grid Grab. Dark brn/dk gy fine grained tuff. <3% hem, <4% py.
L2400N/1700E
89 Hank 5145 Upr Grid Grab. Rusty weathered maroon, silicified tuff, fine/med grained
L2435N/1910E Clasts <1cm diam. Debris flow type unit (medial). <5% py dis'm
89 Hank 5146 Upr Grid 30 cm chip. Gy weathered limonitic gouge? with fine grained
L2050N/2115E clasts of grey/blue aphanitic tuff
89 Hank 5147 Upr Grid Grab. Brown/buff pink rusty, fine grained siliceous altered
L2100N/2153E andesitic tuff?
89 Hank 5148 no sample
89 Hank 5149 no sample
89 Hank 5150 Creek 8 Float. Carbonate/barite veining. Py/Gn in vugs.
Barite is last stage infill in centre of vein.
89 Hank 5151 Creek 8 Carb/barite veining in shear zone. Gy siliceous alt.
Siliceous zones contain abundant Rx py. Cubes <2-3mm.
89 Hank 5152 Creek 8 Similar mineral assemblage to above with Gn/sp in vugs.
89 Hank 5153 Creek 8 Float. Veining with pinkish tinge. Spotty Gn/py/Cp
89 Hank 5154 Creek 8 Float composite. Massive Cp trace Gn/Malachite/azurite
in well formed calcite crys. Prob. pressure soln seam.
89 Hank 5155 Creek 8 Float composite. Massive Gn in calcite. Same zone as above
89 Hank 5156 Creek 8 O/C. Gn/rodocrosite in white alt.
89 Hank 5157 Creek 9 Float. Carbonate/calcite vein material in gy/gr altered volcanic
Abundant py in vugs within calcite. May be some CP included.
89 Hank 5158 Creek 5 2m trench sample. Highly altered, whiteish grey, 5-10% py,
few calcite veinlets, some py stringers.
Trenched down 4m from surface.
89 Hank 5159 Creek 5 As above @ 2m interval.
89 Hank 5160 Creek 5 As above @ 2m interval.
89 Hank 5161 Creek 5 As above @ 2m interval.
89 Hank 5162 Creek 5 As above @ 2m interval.
89 Hank 5163 Creek 5 As above @ 2m interval.
89 Hank 5164 Creek 5 As above @ 2m interval.
89 Hank 5165 Creek 5 As above @ 2m interval.
89 Hank 5166 Creek 5 As above @ 2m interval.
89 Hank 5167 Creek 5 As above @ 2m interval.
89 Hank 5168 Creek 5 As above @ 2m interval.
89 Hank 5169 Creek 5 As above @ 2m interval.
89 Hank 5170 Creek 5 As above @ 2m interval.

APPENDIX IIIb
ANALYTICAL DATA FOR ROCK SAMPLES



Rock sample geochemistry project 89-BC-019. HANK claims.

Sample ID	ppb	GMT	GMT	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppm	ppm	pct	ppm	ppm	pct	ppb
	Au	Au	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn	Hg			
89 HANK 5001	38			0.8	75	-1	71	5.64	1196	2	15	16		-5	32			25		
89 HANK 5002	41			1.7	86	2	185	5.97	1130	2	18	43		-5	107			40		
89 HANK 5003	13			0.7	31	2	82	5.25	1119	2	17	40		-5	86			60		
89 HANK 5004	25			1.4	21	-1	113	3.86	2847	-1	5	12		15	15			80		
89 HANK 5005	2			-0.2	-5	1	4	3.05	1156	-1	2	-2		-5	83			5		
89 HANK 5006	3			-0.2	10	-1	8	3.67	1531	-1	1	-2		-5	98			25		
89 HANK 5007	25			0.6	20	1	9	4.97	1747	5	3	-2		-5	109			15		
89 HANK 5008	41			0.2	41	-1	11	4.32	1974	-1	2	-2		-5	60			25		
89 HANK 5009	132			0.4	38	1	3	3.84	3021	-1	4	-2		-5	30			30		
89 HANK 5010	70			0.6	30	-1	6	0.98	28	-1	2	20		-5	18			15		
89 HANK 5011	23			0.4	43	-1	52	6.96	1427	3	12	-2		-5	93			15		
89 HANK 5012	21			0.2	26	-1	13	4.12	1221	-1	2	-2		-5	82			40		
89 HANK 5013	1			-0.2	24	-1	14	5.8	1150	2	-1	-2		-5	100			10		
89 HANK 5014	-1			-0.2	19	-1	17	5.97	1211	2	1	16		-5	93			10		
89 HANK 5015	31			0.3	63	-1	12	3.77	1568	1	2	28		-5	190			40		
89 HANK 5016	75			2.5	119	-1	33	4.88	254	1	1	69		-5	108			55		
89 HANK 5017	7			0.3	30	-1	8	3.55	1193	-1	2	34		-5	82			10		
89 HANK 5018	-1			-0.2	15	2	49	5.71	1100	2	9	-2		-5	72			10		
89 HANK 5019	1			-0.2	-5	3	68	7.69	1177	1	15	-2		-5	80			5		
89 HANK 5020	-1			-0.2	10	2	4	3.67	1359	1	4	-2		-5	65			15		
89 HANK 5021	98			1.6	80	-1	50	6.33	420	3	6	-2		-5	50			30		
89 HANK 5022	10			0.3	24	2	61	6.54	476	3	18	-2		-5	62			20		
89 HANK 5023	5			0.5	44	-1	38	6.38	24	2	2	100		-5	102			125		
89 HANK 5024	51			0.6	177	7	60	2.56	1123	1	3	631		-5	837			30		
89 HANK 5025	-1			0.3	7	2	54	4.94	1745	-1	13	6		-5	104			30		
89 HANK 5026	247	0.31		1.3	24	-1	5	0.55	31	-1	2	734		-5	36			105		
89 HANK 5027	13			0.2	30	1	13	4.84	483	2	3	13		-5	60			25		
89 HANK 5028	24			0.2	35	2	15	5.05	328	1	4	12		-5	53			20		
89 HANK 5029	20			0.2	82	-1	41	4.39	826	2	13	5		-5	47			60		
89 HANK 5030	15			0.9	68	1	16	4.79	42	2	2	106		-5	46			50		
89 HANK 5031	5			-0.2	30	-1	24	6.08	686	1	-1	40		-5	119			30		
89 HANK 5032	45			0.7	38	-1	13	4.3	398	2	3	16		-5	59			20		
89 HANK 5033	54			0.4	57	-1	61	5.22	1340	-1	7	9		-5	129			20		
89 HANK 5034	2180	2.95		40.5	68	13	146	6.07	1104	4	10	679		-5	1525			220		
89 HANK 5035	96			1.1	22	3	19	4.71	1103	2	14	175		-5	326			100		
89 HANK 5036	98			1	22	2	17	4.69	1449	3	10	115		-5	240			80		
89 HANK 5037	79			1.1	14	2	25	4.29	1233	2	29	98		-5	279			75		
89 HANK 5038	1			0.2	-5	-1	9	4.86	2738	2	-1	-2		-5	92			30		
89 HANK 5039	19			0.3	-5	-1	162	5.98	847	3	20	-2		-5	117			35		
89 HANK 5040	1021	0.96		7.5	340	-1	500	2.1	5736	-1	3	18		11	58			295		
89 HANK 5041	2721	2.71	100.8	50	185	92	3180	0.53	11774	-1	-1	4084		1940	11128			5000		
89 HANK 5042	1424	1.54	34.29	50	62	1	463	2.99	2176	-1	4	87		268	143			295		
89 HANK 5043	107			0.7	73	-1	18	3.21	3507	2	1	14		-5	101			130		
89 HANK 5044	292	0.31		1.7	522	4	338	10	697	13	31	57		-5	236			55		
89 HANK 5045	16			0.7	28	2	98	4.32	1674	1	15	-2		-5	178			55		
89 HANK 5046	510	0.45		7.7	1259	-1	35	10	310	4	12	53		36	20			1100		
89HANK 5047	31			0.3	-5	-1	122	4.43	943	3	17	-2		-5	101			45		
89HANK 5048	19			0.4	-5	-1	63	4.35	877	2	18	17		-5	82			35		
89HANK 5049	1			0.2	-5	-1	63	4.4	1022	3	22	-2		-5	86			35		
89HANK 5050	-1			0.2	-5	1	98	7.54	1519	3	13	-2		-5	118			65		
89HANK 5051	-1			-0.2	-5	1	83	7.3	1591	3	12	-2		-5	107			40		
89HANK 5052	4			-0.2	-5	1	19	7.47	1530	3	10	-2		-5	108			50		
89HANK 5053	5			-0.2	-5	1	63	7.43	1361	3	12	-2		-5	97			30		
89HANK 5054	598	0.75		1.9	330	1	56	5.69	253	3	-1	22		-5	40			310		

Rock sample geochemistry project 89-BC-019. HANK claims.

Sample ID	ppb	GMT	GMT	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppm	ppm	pct	ppm	ppm	pct	ppb
	Au	Au	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn	Hg			
89HANK 5055	30			0.6	20	-1	103	6.63	1532	3	11	-2		-5	113		60			
89HANK 5056	168	0.17		1.2	322	-1	60	5.06	340	3	3	11		11	59		170			
89HANK 5057	92			0.7	85	-1	19	4.6	81	2	1	107		-5	43		60			
89HANK 5058	73			0.5	37	-1	93	7.93	150	3	2	5		-5	68		40			
89HANK 5059	413	0.51		0.3	15	-1	81	6.77	382	2	3	-2		-5	88		30			
89HANK 5060	137			0.5	-5	-1	64	7.57	685	3	5	-2		-5	88		50			
89HANK 5061	140			1	34	-1	96	8.58	347	3	3	-2		-5	73		40			
89HANK 5062	315	0.34		1.2	162	-1	114	10	373	4	3	57		-5	126		40			
89HANK 5063	163	0.17		0.7	51	-1	88	8.95	509	3	3	145		-5	141		45			
89HANK 5064	98			0.5	20	-1	100	6.91	761	3	2	36		-5	111		40			
89HANK 5065	39			0.4	33	-1	115	7.32	1029	3	5	19		-5	127		30			
89HANK 5066	39			0.3	35	-1	106	6.88	1062	2	4	11		-5	133		30			
89HANK 5067	37			0.2	16	1	73	6.61	1285	2	9	25		-5	223		30			
89HANK 5068	17			0.2	-5	2	124	6.23	1473	3	10	7		-5	243		25			
89HANK 5069	51			0.4	7	-1	58	6.65	618	4	3	10		-5	127		30			
89HANK 5070	3			0.3	-5	-1	211	8.49	2394	6	26	21		-5	159		50			
89HANK 5071	3			0.2	-5	-1	144	6.51	2416	4	23	30		-5	141		40			
89HANK 5072	6			0.3	-5	-1	93	6.35	1761	3	18	13		-5	120		35			
89HANK 5073	26			1	35	-1	113	7.47	1778	4	16	38		-5	130		75			
89HANK 5074	33			1.4	61	-1	76	5.84	1230	4	13	51		-5	85		125			
89HANK 5075	52			1.2	145	-1	115	10	1094	7	22	42		10	103		30			
89HANK 5076	47			1.8	94	-1	45	7.68	121	3	8	89		6	138		80			
89HANK 5077	8			0.4	34	3	40	6.39	2845	3	22	150		-5	386		60			
89HANK 5078	4			0.6	31	2	104	7.43	3429	3	23	43		-5	307		75			
89HANK 5079	83			0.6	94	3	221	4.28	1520	2	18	96		-5	314		70			
89HANK 5080	2			-0.2	8	-1	12	3.52	69	3	-1	10		-5	10		1600			
89HANK 5081	-1			-0.2	9	-1	3	2.35	12	1	1	-2		-5	4		1250			
89HANK 5082	23			-0.2	211	-1	28	5.67	31	18	-1	60		14	3		2100			
89HANK 5083	338	0.38		6.1	283	2	131	7.18	511	3	4	577		8	248		190			
89HANK 5084	30			0.8	51	-1	99	5.53	358	3	2	146		-5	93		100			
89HANK 5085	44			1.1	39	-1	153	8.13	580	3	6	38		-5	125		65			
89HANK 5086	16			0.7	18	-1	102	8.18	167	4	2	82		-5	99		50			
89HANK 5087	368	0.41		3.2	209	-1	119	7.77	801	4	2	1064		8	100		140			
89HANK 5088	198	0.21		1.3	82	-1	71	6.38	189	3	2	70		-5	65		100			
89HANK 5089	131			1.1	126	-1	79	5.76	579	3	5	64		-5	101		50			
89HANK 5090	440	0.48		2.3	519	2	182	7.41	519	3	6	54		8	113		110			
89HANK 5091	97			1.1	108	-1	111	7.9	1053	3	16	64		-5	95		60			
89HANK 5092	5110	4.73	77.8	50	215	193	1952	2.67	368	1	2	8553		1250	18231		4000			
89HANK 5093	10000	45.02	613.4	50	300	344	3827	3.14	532	-1	-1	10000	1.66	2000	20000	3.44	5000			
89HANK 5094	1500	0.75		13.3	21	9	159	6.61	170	3	8	527		46	961		300			
89HANK 5095	787	0.75		10.8	66	5	68	6.96	132	3	7	445		30	491		180			
89HANK 5096	10000	39.36	849.9	50	55	351	2417	9.96	370	3	9	10000	3.6	152	20000	4.53	3650			
89HANK 5097	299	0.34		14.4	118	144	782	8.32	625	2	10	10000	0.94	42	15618		600			
89HANK 5098	670	0.69		27.4	15	171	512	5.07	573	1	7	10000	1.26	49	18657		400			
89HANK 5099	2370	2.57		21.8	179	59	429	5.39	954	3	6	1281		93	6692		1550			
89HANK 5100	4860	4.77	34.6	50	184	244	964	5.32	550	4	5	7851		104	20000	2.28	2700			
89HANK 5101	8120	7.17	105.6	50	597	244	3511	6.5	667	3	-1	6465		218	20000	2.13	1800			
89HANK 5102	10000	25.71	349.7	50	207	441	2831	3.3	910	3	-1	10000	1.59	1102	20000	4.04	3700			
89HANK 5103	972	1.13		19.1	428	225	2672	6.98	1587	2	6	10000		1369	20000		270			
89HANK 5104	1464	1.54		12.4	95	5	83	4.03	158	3	6	859		26	516		300			
89HANK 5105	524	0.58		3.7	90	2	27	5.83	81	7	7	191		9	164		70			
89HANK 5106	10000	36.86	541	50	438	228	2659	7.58	1624	3	3	10000	3.26	1408	20000	2.47	5000			
89HANK 5107	9760	9.02	149.1	50	241	293	3384	5.35	798	3	11	10000	1.21	587	20000	3.36	5000			
89HANK 5108	10000	10.87	223.5	50	230	590	6785	6.69	780	5	-1	10000	5.28	311	20000	6.01	5000			

Rock sample geochemistry project 89-BC-019. HANK claims.

Sample ID	ppb	GMT	GMT	ppm	ppm	ppm	pct	ppm	ppm	ppm	pct	ppm	ppm	pct	ppm	ppm	pct	ppb
	Au	Au	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn	Hg	
89HANK 5109	2750	3.09		49.2	176	325	2341	4.74	540	1	7	10000	1.32	147	20000	3.35	4700	
89HANK 5110	267	0.31		2.6	89	5	110	5.25	644	3	8	341		9	559		170	
89HANK 5111	306	0.34		2.9	148	2	158	4.83	237	4	7	203		12	260		65	
89HANK 5112	446	0.62		2.6	46	2	85	1.61	189	2	12	170		5	381		165	
89HANK 5113	21			2.5	48	1	47	5.91	1338	4	2	171		-5	138		10	
89HANK 5114	38			0.8	13	-1	43	3.07	424	1	24	20		-5	28		40	
89HANK 5115	1750	1.37		2.3	47	-1	7	2.84	29	-1	51	96		-5	38		90	
89HANK 5116	188	0.21		4.2	64	23	72	5.87	2011	1	24	1349		6	2859		330	
89HANK 5117	10000	18.24	323.7	50	114	1262	2951	8.34	3172	-1	-1	10000	5	372	20000	14.37	5000	
89HANK 5118	95			1.9	118	5	135	4.47	551	2	17	202		-5	748		140	
89HANK 5119	406	0.45		10.8	21	5	30	1.71	31	2	6	507		6	642		120	
89HANK 5120	18			1.4	31	1	157	4.12	855	1	12	325		-5	186		15	
89HANK 5121	2200	2.26	87.1	50	22	470	2700	2.22	6056	1	9	10000	1.13	188	20000	4.75	4500	
89HANK 5122	1572	1.71		26.3	221	9	145	3.71	111	2	4	900		15	990		210	
89HANK 5123	401	0.45		2.4	311	1	20	3.94	104	2	4	57		9	106		70	
89HANK 5124	980	0.96	48.7	50	338	-1	71	3.6	31	1	3	80		204	32		2600	
89HANK 5125	224	0.14	38.4	50	52	-1	15	0.46	16	-1	2	399		37	22		750	
89HANK 5126	89			37.2	62	4	62	1.95	161	-1	3	520		31	662		370	
89HANK 5127	2417	2.67		14.8	838	-1	29	1.61	1239	-1	4	129		16	59		120	
89HANK 5128	2422	2.74		21.5	2000	-1	31	1.33	550	-1	5	81		54	147		150	
89HANK 5129	4851	5.86		45	2000	-1	82	1.65	817	1	4	158		123	54		650	
89HANK 5130	685	0.62		5	158	14	90	1.33	77	1	3	1254		8	2065		220	
89HANK 5131	22			0.7	67	-1	4	2.76	271	1	2	14		-5	44		115	
89HANK 5132	24			0.4	51	-1	10	4.33	1580	1	2	-2		-5	96		60	
89HANK 5133	7			0.3	19	1	11	4.5	1684	2	1	-2		-5	98		70	
89HANK 5134	1414	1.68	323	50	123	95	3323	3.24	9155	2	1	8166		140	9299		2800	
89HANK-5135	42			-0.2	36	-1	1	0.84	20	2	-1	26		7	7		180	
89HANK-5136	19			-0.2	-5	-1	16	5.83	4313	6	-1	12		10	210		90	
89HANK-5137	121			0.6	-5	-1	9	1.33	43	2	4	23		17	16		1600	
89HANK-5138	13			-0.2	298	2	6	10	32	27	-1	-2		-5	-1		70	
89HANK-5139	399	0.41		0.5	15	-1	21	5.7	24	213	-1	41		17	56		190	
89HANK 5140	15			-0.2	-5	-1	9	1.14	24	4	1	18		-5	5		3700	
89HANK 5141	12			-0.2	11	-1	9	1.51	17	6	2	17		-5	3		3700	
89HANK 5142	12			-0.2	5	-1	11	1.3	9	4	1	4		-5	14		1500	
89HANK 5143	7			-0.2	-5	-1	5	0.69	26	6	5	5		-5	1		220	
89HANK 5144	-1			-0.2	-5	-1	10	5.89	2116	2	-1	-2		-5	89		100	
89HANK 5145	-1			-0.2	-5	-1	14	4.76	213	3	-1	-2		-5	26		1500	
89HANK 5146	72			-0.2	98	-1	6	1.49	39	4	2	148		18	3		5000	
89HANK 5147	4			-0.2	-5	-1	2	0.3	3	-1	-1	4		-5	5		2400	
89HANK 5150	223	0.21		7.3	23	17	42	0.89	65	-1	3	262		18	2322		115	
89HANK 5151	588	0.51		2.7	120	16	35	3.51	328	1	5	172		8	2190		190	
89HANK 5152	635	0.55		10.4	55	143	184	1.79	137	-1	4	503		60	18198		1350	
89HANK 5153	2154	2.13		29.3	216	31	1021	4.8	287	2	5	10000	2.13	22	3583		300	
89HANK 5154	2000	0.89		13.5	70	237	11647	4.91	2354	-1	5	5523		-5	20000	3.16	700	
89HANK 5155	795	0.75	60.7	50	57	790	1359	3.49	1856	-1	3	10000	4.8	163	20000	10.11	2050	
89HANK 5156	463	1.44		36.4	54	9	6249	2.72	510	49	2	10000	1.32	7	913		190	
89HANK-5157	193	0.27		1.2	121	-1	3	2.23	9593	2	-1	10		28	5		590	
89HANK-5158	60			1	7	-1	11	6.74	1208	2	7	91		9	126		50	
89HANK-5159	894	1.2		14.2	17	14	224	4.79	2340	1	10	1865		20	1668		290	
89HANK-5160	102			2.2	18	13	95	3.31	1536	1	14	627		10	1573		310	
89HANK-5161	1628	2.06	1.4	50	31	25	337	4.44	1811	2	14	2131		15	2895		540	
89HANK-5162	137			3.2	23	10	68	2.5	972	1	19	226		10	1224		250	
89HANK-5163	791	0.93		11.1	31	-1	2100	5.89	1001	1	6	164		8	83		70	
89HANK-5164	79			1.1	-5	-1	54	3.93	848	1	10	28		-5	108		80	

Rock sample geochemistry project 89-BC-019. HANK claims.

Sample ID	ppb	GMT Au	GMT Au	ppm	ppm	ppm	pct	ppm	ppm	ppm	pct	ppm	ppm	pct	ppm	ppm	pct	ppb
	Au	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn	Hg		
89HANK-5165	68			0.3	27	-1	13	4.96	920	1	6	2	-5	69		100		
89HANK-5166	125				1.1	71	-1	25	7.44	710	2	8	9	6	79		60	
89HANK-5167	25			0.2	-5	-1	96	6.84	854	2	10	-2	-5	68		55		
89HANK-5168	16			-0.2	-5	-1	321	5.29	1275	1	7	-2	5	55		50		
89HANK-5169	40			0.3	7	-1	47	6.44	1223	1	29	4	5	51		40		
89HANK-5170	40			0.6	79	-1	79	7.6	1151	2	51	8	-5	69		30		

APPENDIX IIIC
STATISTICAL DATA FOR ROCK SAMPLES



STATISTICAL TREATMENT OF DATA

Histograms were produced for each element. The number of intervals (K) in the data population was determined by using the following formula (Levinson, A.A., 1974: Introduction to Exploration Geochemistry, p. 563), which is valid for a population greater than 30.

$$K = 10 (\log_{10} N)$$

K = Number of intervals

N = Number of samples

The interval width was found by dividing the largest value in the population (N) by the number of intervals (K)

$$\text{Intervals width} = \frac{\text{largest value in the population}}{K}$$

In all cases the results were statistically treated on the basis of a lognormal distribution. The mean (x) and the standard deviation (s) were calculated using the following formulas:

$$\text{mean } (x) = \frac{\sum x}{n}$$

n = Number of samples

$\sum x$ = Total of samples

$\sum x^2$ = Sum of squares of samples

$$\text{standard deviation } (s) = \sqrt{\frac{\sum x^2 - n \bar{x}^2}{n}}$$

The threshold (t) was calculated as being equal to the mean (x) plus 2.5 times the standard deviation (s)

$$t = x + 2.5s$$

CORRELATION COEFFICIENTS

	Au	Ag	As	Pb	Cu	Zn	Sb
Au	1.000	0.003	-0.144	0.029	0.111	0.0002	-0.036
Ag		1.000	-0.322	0.275	0.187	0.450	0.017
As			1.000	0.127	-0.209	-0.008	0.358
Pb				1.000	0.317	0.371	-0.028
Cu					1.000	0.111	-0.057
Zn						1.000	0.291
Sb							1.000

Rating:	0.000	to	(+/-)	0.300	Weak
	(+/-) 0.301	to	(+/-)	0.550	Slight
	(+/-) 0.551	to	(+/-)	0.800	Moderate
	(+/-) 0.801	to	(+/-)	1.000	Strong

SQUARES OF CORRELATION COEFFICIENTS (To express the interaction in percentile)

	Au	Ag	As	Pb	Cu	Zn	Sb
Au	100.0	0.00	2.00	0.08	1.20	0.00	0.10
Ag		100.0	10.30	7.50	3.40	20.20	0.02
As			100.0	1.60	4.30	0.00	12.80
Pb				100.0	10.00	13.70	0.07
Cu					100.0	1.20	0.30
Zn						100.0	8.40
Sb							100.0

Rating:	0.0%	to	9.0%	Weak
	9.1%	to	30.2%	Slight
	30.3%	to	64.0%	Moderate
	64.0%	to	100.0%	Strong

file: ROCK

COMMAND: CORR MISSING VALUE TREATMENT: PAIRWISE

(NUMBER OF VALID CASES APPEARS UNDER COEFFICIENT)

*** CORRELATION MATRIX ***

VARIABLES:

1 AU_PPB	1.00000						
2 AG	0.72055	1.00000					
	162						
3 AS	0.42402	0.30182	1.00000				
	162	168					
4 CU	0.44368	0.55861	0.08220	1.00000			
	162	168	168				
5 PB	0.72655	0.66379	0.09125	0.63213	1.00000		
	153	153	153	153			
6 ZN	0.26764	0.31436	-0.01060	0.23982	0.52333	1.00000	
	150	150	150	150	148		
7 HG	0.44116	0.60654	0.08843	0.38540	0.51863	0.22874	1.00000
	161	164	164	164	153	150	
1 AU_PPB	2 AG	3 AS	4 CU	5 PB	6 ZN	7 HG	

file: ROCK

COMMAND: DESC MISSING VALUE TREATMENT: VARWISE

*** DESCRIPTIVE STATISTICS ***

THERE ARE 7 VARIABLES AND 172 CASES IN THE DATA SET

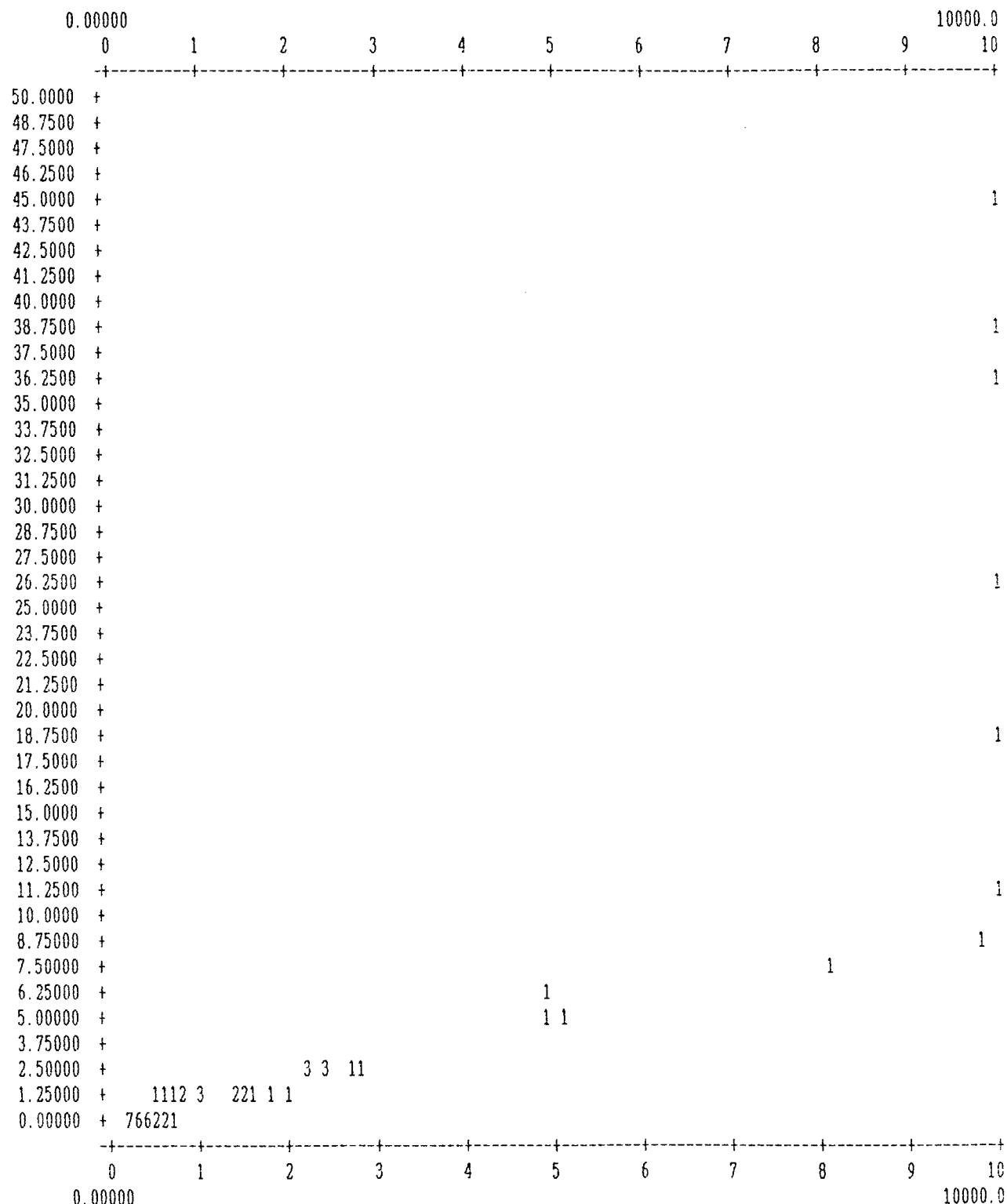
VARIABLE	VALID CASES	NUMBER MISSING	% MISSING
1 AU_PPB	162	10	5.8
2 AG	168	4	2.3
3 AS	168	4	2.3
4 CU	168	4	2.3
5 PB	153	19	11.0
6 ZN	150	22	12.8
7 HG	164	8	4.7

STD ERROR COEFF OF

VARIABLE	MEAN	STD. DEV.	VARIANCE	OF MEAN	VARIATION
1 AU_PPB	530.333	1287.29	1657117	101.139	242.732
2 AG	8.96845	16.5782	274.836	1.27903	184.850
3 AS	115.071	258.122	66627.0	19.9145	224.315
4 CU	477.714	1354.40	1834395	104.494	283.516
5 PB	416.817	1367.05	1868827	110.519	327.974
6 ZN	507.420	1803.06	3251032	147.219	355.339
7 HG	530.854	1114.05	1241114	86.9929	209.861

file: AUROCK

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE



TOTAL POINTS PLOTTED: 58

1 AU_PPB

file: STROCK

COMMAND: HIST MISSING VALUE TREATMENT: VARWISE

VARIABLE: 1 AU AUTO/22

APPENDIX III

THIN SECTION DESCRIPTIONS FOR ROCK SAMPLES





RECEIVED NOV 21 1989

Vancouver Petrographics Ltd.

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JOHN G. PAYNE, Ph.D. Geologist

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Report for: Robert Brown,
Lac Minerals Ltd.,
1050-1055 West Hastings St.,
Vancouver, B.C.
V6E 2E9

Invoice 8613

November 17th, 1989

Samples:

9 rock samples for sectioning and petrographic examination.

The samples come from 4 sites, and are arbitrarily designated A, B, C etc. in each case. They are distinguished as follows:

89R-61	A	Diatreme
89R-61	B	Diatreme
89R-61	C	Diatreme
89R-61	D	Diatreme
89R-62	A	Red felsite
89R-62	B	Grey felsite
89R-63		Cherty knoll
89R-64	A	Cherty knoll ("Big Knob")
89R-64	B	Andesitic host rock

Summary:

Except for 89R-64-B, which is recognizable as a partially altered, abundantly porphyritic andesite, the rocks of this suite are all intensely altered, and contain virtually no recognizable primary minerals.

The relict textures are clearly those of glassy volcanic and/or derived fragmentals. No remnant quartz phenocrysts are recognizable, suggesting that the original rocks may have been andesitic rather than rhyolitic or dacitic in composition. The lack of secondary mafic products like chlorite indicates a leucocratic primary character.

The rocks now consist of cryptocrystalline altered glass, cherty silica and felted kaolinite, in various proportions and modes of intergrowth (pseudomorphing primary vitric, fragmental and porphyritic textures).

X-ray diffraction scans were run on a number of the apparent multi-phase samples. Compositions in all cases were indicated as quartz (cherty silicification) and kaolinite (from alteration of feldspars) - except in 62B, where quartz is apparently absent. Residual non-crystalline material (glass) does not yield an XRD response.

Based on textural observations, the samples from 89R-61 are altered glassy fragmentals (possibly tuffs or diatreme breccias), except for Sample C which is a chert - possibly representing complete silicification of a volcanic or tuff. Samples A and D contain recognizable altered biotite flakes.

The samples from 89R-62 are porphyritic rather than fragmental in texture. One of them contains minor accessory barite associated with kaolinized pseudomorphs.

The single sample from 89R-63 is a cherty, intensely silicified rock - probably of fragmental or porphyritic origin, like the others. It contains barite as a trace accessory.

The cherty sample from 89R-64 shows crackle-type microbrecciation. Relict primary textures are absent.

The style and intensity of alteration (to fine-grained silica, kaolinite, minor barite and pyrite) exhibited by these rocks of glassy volcanic and fragmental affinities appears typical of a high-level epithermal system.

Individual petrographic descriptions are attached.



J.F. Harris Ph.D.

(929-5867)

SAMPLE 89-R-61-A

ALTERED GLASSY FRAGMENTAL

This rock is a heterogenous, streaky/fragmental melange of unidentifiable cryptocrystalline material.

In thin section it is seen to include streaky, brownish/opaque zones showing flow banding, sometimes apparently highly contorted; similar material also forms angular, elongate fragments to 5mm or more.

The majority of the rock consists of a cryptocrystalline to minutely felsitic material which is probably altered glass. This contains more or less abundant, sub-prismatic and diffuse ovoid bodies, 0.2 - 2.0mm in size, of slightly better crystallized material - sometimes recognizable as cherty silica, and sometimes apparently clays. Some of these features may represent original feldspar phenocrysts.

Occasional ghost relics of original biotite flakes are seen, now represented by lamellar masses of leucoxene.

XRD analysis yields strong peaks of kaolinite and quartz, and very minor peaks of biotite and possible montmorillonite.

SAMPLE 89R-61-B

ALTERED GLASSY FRAGMENTAL

This rock is of similar general appearance to 61A in thin section, consisting of cryptocrystalline, streaky/pelletty or flecked, brownish material - clearly representing altered glass.

It lacks the zones of strongly developed flow banding seen in 61A, and (best observed macroscopically in the thin section) contains abundant, clearly defined, sub-angular fragments, 0.2 - 10mm or more in size. It is somewhat vesicular.

These clasts are found, in thin section, to be composed of minutely cherty/siliceous material (of grain size 2 - 20 microns). A few of the smaller ones (possibly pseudomorphs of feldspar crystals) are composed of compact aggregates of probable clays.

The rock contains traces of very fine-grained pyrite - generally as more or less dense disseminations in certain clasts.

XRD sanalysis yields a pattern consisting of strong peaks for quartz and minor peaks of kaolinite.

This sample appears to be a breccia or coarse tuff of altered glassy volcanic material.

SAMPLE 89R-61-C**CHERT (SILICIFIED VOLCANIC)**

This rock is of very different appearance in thin section to the previous two samples from 89R-61.

It consists of a featureless anhedral/interlocking aggregate of chert, showing diffuse patchy variations in grain size. Much of it is in the grain size range 2 - 5 microns, varying up to 20 microns or so. Rare, pockety segregations of microgranular quartz, of grain size 20 - 100 microns, are also seen.

Locally the patches of different grain size show sub-prismatic shapes, and may represent original phenocrysts or fragments in a totally silicified volcanic. This feature is best observed under low magnification in the off-cut block, where the different grain sizes of chert show varying degrees of whitish etch.

The only other component is minutely fine-grained, disseminated, opaque material, occurring as clusters of ragged granules, 10 - 50 microns in size. These show no crystal form and, in fact, appear to be "fluffy" aggregates of micron-sized dust (sulfides? carbon?). The opaque granules partly concentrate as small patches or clumps - clearly favouring areas of the most minutely fine-grained chert.

SAMPLE 89R-61-D**ALTERED TUFF**

This is a rock of somewhat similar macroscopic appearance to 61A and B - though less coarsely fragmental.

In thin section, it is seen to be composed of minutely felsitic/ cryptocrystalline material (probably weakly devitrified siliceous glass). Sub-prismatic pseudomorphs - 0.1 - 1.0mm in size and composed of colourless to brownish felted material, which appears to be compact clay - are abundant. These mainly look like totally altered feldspar crystals - sometimes showing preferred orientation suggestive of flow. In some cases, however, they show relict streaky vitric textures indicative of their being glassy lithic fragments.

Leucoxenized relict biotite flakes (as in 61A) are a notable trace constituent. There are also some irregular to sub-prismatic patches of compact leucoxene.

Disseminated pyrite is relatively abundant. It occurs as compact clumps of micron-sized granules, only rarely showing typical cubic form (as rare grains to 0.1mm). The pyrite tends to form irregular clusters, often associated with altered biotite and leucoxene.

The X-ray diffraction pattern yielded by this sample is a simple combination of strong peaks of kaolinite and quartz.

This rock appears to be a tuff of argillized crystals and glassy clasts in a siliceous glassy matrix.

SAMPLE 89R-62-A

ALTERED PORPHYRITIC VOLCANIC

This is another totally altered rock showing abundant, patchy, crypto-fragmental or pseudomorphic forms (clearly visible in low-power examination of the etched off-cut).

In thin section, these are found to be predominantly of sharply prismatic form and to range in size from 0.1 - 2.0mm. They are mostly composed of brownish felted material (having the appearance of clay), sometimes with intergrown cherty to microgranular quartz. Small patches of barite are a notable minor constituent in some of the pseudomorphs.

Irregular patches and lamellar relics (after biotite) of leucoxene are also rather common, and the rock contains minutely fine-grained disseminated pyrite (as described in 61-D).

The altered pseudomorphs are set in a cherty/felsitic matrix. Some irregular/amoeboid patches of the brown clay have the appearance of amygdules.

XRD analysis gives a pattern essentially identical to that of previous rocks of the suite, indicative of a mixture of kaolinite and quartz.

The fabric of this rock is dominated by geometric forms which are clearly crystal pseudomorphs. Lithic clasts are not evident. It appears to be a totally altered porphyry.

SAMPLE 89R-62-B

ALTERED PORPHYRITIC VOLCANIC

This rock consists predominantly of a homogenous, minutely felsitic/cryptocrystalline matrix, with rather sparse, ill-defined, sub-prismatic forms, 0.2 - 2.0mm in size, pseudomorphous after original phenocrysts.

The matrix appears to be composed predominantly of compact clays (probably representing altered glass) - probably with accessory proportions of intergrown chlorite, leucoxene and cherty silica.

The pseudomorphs are of similar composition except that they lack the darker sub-opaque components (chlorite/leucoxene) and the grain size of the constituent aggregate is slightly coarser (5 - 50 microns) compared to that of the matrix (1 - 10 microns).

This rock is also distinguished by rather high content of disseminated pyrite. This occurs as coalescent clusters of minute granules, 2 - 10 microns in size, with some more distinct individual grains up to 100 microns. The distribution of the pyrite clusters appears random, and is independent of the pseudomorphed porphyritic texture (i.e. pyrite occurs both in the matrix and the pseudomorphs, or extends across contacts from one to the other).

XRD analysis yields strong peaks of kaolinite. Quartz peaks are notably absent.

This rock appears to be an altered (intensely kaolinized) porphyritic volcanic.

SAMPLE 89R-63

CHERT (SILICIFIED VOLCANIC)

This rock is a chert composed essentially of microcrystalline silica, of grain size 2 - 50 microns. It shows diffuse patchy, pockety and veniform development of the coarser grain sizes, in a predominant, minutely fine-grained matrix.

Barite is a minor accessory, as small, randomly disseminated granular clumps and thread-like veinlets of subhedral crystals, 0.1 - 1.0mm in size. The larger of these tend to occur in the areas of slightly better-crystallized chert.

Another accessory is a clay mineral (or possibly compact, minutely felted sericite), occurring as a few irregular patches up to 2mm or more in size. The clay component is occasionally seen associated with the barite, but is mostly independent.

Minor proportions of micron-sized, disseminated, brown sub-opaque material, and possibly a little pyrite, are the remaining components.

Macroscopic examination of the cut-off block shows ill-defined, angular, patchy features which suggest that this rock is of secondary origin - i.e. a totally silicified fragmental or porphyritic volcanic (similar to 61-C).

SAMPLE 89R-64-A

CHERT

This rock has the macroscopic appearance of a silicified crackle breccia or micro-stockwork.

In thin section, it is found to be composed essentially of monomineralic chert, of grain size 5 - 20 microns. This shows patchy/pockety variations to coarser and finer grain sizes, and is cut by a network of microfractures and hairline veinlets - again defined by coarser or finer grain size in the chert.

The only other component is a trace of micron-sized opaques (< 1-5 microns in size), which occur as diffuse dusty patches and veniform segregations.

Estimated mode

Phenocrysts

Plagioclase	30
Sericite	18
Clays)	5
Epidote)	5
Chlorite	5
Opaques	8
Groundmass	
Plagioclase	25
Chlorite	5
Sericite	5
Rutile)	1
Leucoxene)	

This sample is the only one of the suite where positive optical identification of the constituent minerals and estimation of their relative proportions are possible.

Though quite strongly altered, it is readily recognizable as an abundantly porphyritic volcanic of andesitic composition - possibly of minor intrusive (dyke rock) character.

Phenocrysts, 0.1 - 1.0mm in size, are of stumpy, euhedral/prismatic form, and are randomly oriented. They consist predominantly of plagioclase, showing rather strong pervasive alteration to fine-grained sericite and minor saussuritic products (clays, cryptocrystalline epidote).

There is also a component of what are probably totally altered mafic phenocrysts - now composed of indeterminate, fine-grained secondary products (including chlorite, clays and rutile/leucoxene) and clusters of tiny granules of opaques - probably mainly pyrite.

The groundmass is a turbid felsitic aggregate of partially sericitized plagioclase, of grain size 10 - 50 microns, with intergrown fine-grained chlorite and micron-sized granules of opaques and sub-opaques.

The tendency for the fine-grained sulfides to concentrate in the altered mafic phenocrysts is a notable feature of this rock.

APPENDIX IVa
DIAMOND DRILL LOGS



HI-TEC RESOURCE MANAGEMENT LTD.

DIAMOND DRILL LOG

Property Name:	HANK	Client Name:	LAC MINERALS LTD.	Borehole Test Method:	Tropari
Hole No:	89-DDH-01	Azimuth:	320	Test Azimuth:	310.5
Northing:	10670.136	Dip:	-60	Test Dip:	-59.5
Easting:	10162.749			Date Started:	d: August 13, 1989
Elevation:	1116.820m	Length:	95.05 m	Test Depth:	89 m
				Date Completed:	ted: August 17, 1989

Overall impression of hole

LITHOLOGY

FROM (m)	TO (m)	WIDTH (m)	
12.00	18.35	6.35	Andesite breccia
18.35	20.20	1.85	Tuff
20.20	30.37	10.17	Andesite
30.37	65.53	35.16	Andesite Breccia
65.53	75.67	10.14	Andesite
75.67	76.28	0.61	Andesite Dyke (?)
76.28	79.12	2.84	Andesite Breccia
79.12	80.11	0.99	Clastic Tuff
80.11	95.09	14.98	Andesite Breccia

ALTERATION

12.00	65.00	53.00	Mainly moderate strong CB-PY-sericite alteration
73.00	95.09	22.09	Asaboe
65.00	73.00	8.00	Weak altered

MINERALIZATION

PY % is good all through this hole

42.00	54.00	12.00)
82.16	95.09	12.93) Major zones of SP-GN appearances
61.63	63.19	1.56)
88.95	92.00	3.05) Major CB vein zone, possibly high Au
94.68	95.09	0.41)
0.00	12.19	12.19	Casing
0.00	12.00	12.00	Overburden
14.32	14.32		First feetage mark
13.30	13.30		Measured back from 14.32 m
12.00	14.00	2.00	Minor limonite on fracture surfaces
12.00	18.35	6.35	Andesite Breccia
			Pale greenish grey with greenish breccias and pale
			grey-maroon matrix
0.00	25.30	25.30	N Q Core
25.30	95.09	69.79	B Q Core
12.00	14.00	2.00	20% gouge , 50% greyish, matrix, disseminated & blebs
			PY replaced mafic minerals
14.00	16.00	2.00	20% gouge, 40% sheared, shear plane at 42
16.00	18.00	2.00	10% sheared sections at 30-45
			16.56-16.61: Two quartz vein 1/2 cm at 3
			17.37-17.5: 20% maroon silicious fragments in sheared
			section
18.35	20.20	1.85	Tuff (ash) plae green
18.00	20.00	2.00	19-19.2 m: 20% greyish andesitic veins 2-4 cm
			at 15-40 , associated with some banded PY at 10

20.20	30.37	10.17	Andesite, local clastic
20.00	22.00	2.00	40% sheared sections, 10% gouge at 60 and other directions 20.9 m : minor blackish mineral
20.20	25.00	4.80	60% sheared sections, 30% gouge
22.00	24.00	2.00	60% gouge
24.00	25.30	1.30	30% sheared, at 24°40'
25.30	27.00	1.70	10% sheared sections at 40 & 60 25.3 m: 4 cm silicified & feldsparhized section
27.00	29.00	2.00	5% gouge at 10 & 45' 27.85 m: minor SP blebs associated at tiny quartz vein 1mm, 45'
29.00	31.00	2.00	50% gouge
30.37	37.86	7.49	Sheared & gouge zone, 75% sheared sections 15% gouge not included wash off mud
30.37	65.53	35.16	Andesite Breccia
31.00	37.86	6.86	Shear fractures, gougey mainly at 30-60
32.86	34.21	1.35	33.45°33.81m: Silicified with 10% quartz veinlets 1~5 mm thids at 30 contacts with 0.1% GN + SP, trace CP 32.25°33.35m: 5% GN + SP + CP associated with quartz CB reinlets 2mm at 60 33.92m : 4mm quartz vein associated with 40 GN SP
34.21	36.00	1.79	30% gouge at 55 34.21°34.35: Tuff, upper contact = 60
36.00	38.00	2.00	Few quartz - CB veinlets 1~6 mm at 60
38.00	45.00	7.00	Moderate competent core
38.00	40.00	2.00	1% gouge at 80
40.00	42.05	2.05	No comment
42.05	42.56	0.51	42.10: QZ-CB vein 1cm 2 with SP GN selvage 1mm 42.18: QZ-CB vein 1cm, 45, some SP, GN, CP 42.44: QZ-CB vein 1 cm. 55
42.56	44.00	1.44	Brecciated up with 20 pale greyish-maroon matrix 6 cm sheared at 30
44.00	46.00	2.00	30 sheared sections at 20 & 40, 5% gouge trace GN-SP in sheared section
45.35	46.48	1.13	Sheared gougey
46.00	48.00	2.00	48.62 m : 8 cm banding with CB-QZ, associated and GN and blackish mineral at 50
48.00	50.00	2.00	48.9°50.57 m: 50% sheared at 45, 20% shattered 48.9 m: 1.5 cm spot of QZ-CB with SP
50.00	52.00	2.00	20% sheared sections at 10, 40 & 60 Two CB veinlets 2 & 8 mm 10 , 20
52.00	54.00	2.00	54°52.6 m: slightly sheared at 40 & 60, some quartz veinlets 2mm at 40 minor blackish mineral 53.83 m: 1mm SP-GN vein at 20 53.84°54 m: Pervasive PY alteration at 70
54.00	55.65	1.65	55.03°55.57: Sheared & shattered 54.39: 1 cm banded PY at 45
55.65	56.18	0.53	Intruded by 30% CB-QZ veins 2 mm to 2 cm at 20, 1 CB vein 8 mm cross cutting a CB-QZ vein at 50
56.18	57.00	0.82	QZ-CB veinlets 1-4 mm at 30
57.00	59.00	2.00	57.57°58.38 m: 30% clasts, subround to round, 2°30 mm in diameters, grey & maroon
59.00	61.63	2.63	20% pale greyish matrix

60.33 m: CB vein 2.5 cm 42
 61.63 63.19 1.56 shear section
 61.63 62.36 0.73 Hanging wall with CB-QZ-BA veins and brecciated sections. Two veins 2 & 4 mm 32 with some CP blebs and TT GN envelop
 62.06~62.23 m: vein-breccia section, upper contact 40 lower contact 50
 62.35: 2 cm silicified section
 62.36 62.70 0.34 Sheared section, with PY banding 48, some silicious spots about 1.5 cm in diameters
 62.70 63.19 0.49 Footwall: 62.78~62.99 m: silicified section at 30 with BA-CA-QZ vein at 30, 1% CP, 2.5% SP, some GN
 63.19 65.00 1.81 Few quartz veinlets and CB-QZ veinlets 1-4 mm at 40
 65.00 67.00 2.00 Alteration is locally 3 or 4
 Quartz veinlets 1~8 mm generally at 20, one at 65
 66.53~67 m: some slightly bleached sections due to quartz veinlet intrusion
 65.53 75.67 10.14 Andesite: crystalline, fine to medium grain green, magnetic when altered to grey, nonmagnetic PY generally accured as mafic mineral replacement and sheeting
 67.00 69.00 2.00 QZ veins 1~10 mm generally at 40
 69.00 71.00 2.00 Green, magnetic, strong chloritized
 71.00 73.00 2.00 QZ veinlets and QZ-CB veinlets 1~10 mm, 10-40 common at 20 unmineralized
 72.2 m: 85 fracture, rich in PY
 73.00 75.00 2.00 Unmineralized CB-QZ vein as above
 75.00 77.00 2.00 75.66~75.84 m: maroon layers 70% at 10-20
 Start grey color
 75.67 76.28 0.61 Andesitic Dyke C
 76.28 79.12 2.84 Andesite Breccia
 79.12 80.11 0.99 Tuff, clastic
 77.00 79.00 2.00 30% sheared at 40, 2.5% gouge
 80.11 95.09 14.98 Andesite breccia
 79.00 81.00 2.00 30% sheared sections at 50
 Minor SP at a fracture 60
 81.00 82.16 1.16 Slightly sheared at 45
 82.16 82.37 0.21 CB vein with shear fractures upper contact = 6 lower contact = 32, 2 1/2 SP some CP pale pinkish color
 82.37 84.00 1.63 10% matrix
 84.00 86.00 2.00 50% matrix
 85.5 m: 1 mm fracture filling 70
 85.41 m: CB vein 2 cm: 47 associated with SP
 86.00 88.00 2.00 20% greyish matrix
 Two barren quartz U CR vein 1 cm at 45
 88.00 88.85 0.85 No comment
 88.85 89.13 0.28 Four QZ-CB veinlets 1cm, 1.8cm, 1cm, 3mm associated with SP, GN, PY at 30
 89.13 89.72 0.59 Trace SP at some CB sheared fractures at 45
 89.72 90.52 0.80 89.72~89.91 m: sheared at 35, gougey 10% PY some SP and blackish mineral
 90.52 92.00 1.48 Sheared & shattered, some quartz silicified fragment 60% gouge with some quartz and SP at 38
 92.00 92.00 is measured back from 93.57 mark
 92.00 93.57 1.57 60% sheared at 40-45

93.57 94.68 1.11 sheared and shattered, gougey
94.68 95.09 0.41 Ground core.
Mainly quartz vein silicified section
At the end, a piece of ground core has 8mm CB vein
with SP GN CP
95.09 Left a drill bit in hole try to drill through on
Aug. 14 & 17 for 1/2 day rod is tight, give up end
of hole at 95.09m

HI-TEC RESOURCE MANAGEMENT LTD.

DIAMOND DRILL LOG

Property Name:	HANK	Client Name:	LAC MINERALS LTD.	Borehole Test Method:	Tropari		
Hole No:	89-DDH-02	Azimuth:	320	Test Azimuth:	319.5	Core Size:	NQ & BQ
Northing:	10670.236	Dip:	-46	Test Dip:	-46.5	Date Started:	d: August 14, 1989
Easting:	10162.349			Test Depth:	110 m	Date Completed:	ted: August 17, 1989
Elevation:	1116.820m	Length:	110.03 m				

Overall impression of hole

LITHOLOGY

FROM (m) TO (m) WIDTH (m)

20.17	47.30	27.13	Andesite Breccia
47.30	60.00	12.70	Crystalline Andesite
60.00	78.52	18.52	Andesite Breccia
78.52	80.58	2.06	Intermediate-basic volcanic breccia
80.58	83.63	3.05	Tuff
83.63	85.95	2.32	Andesitic intrusion
85.95	97.80	11.85	Intermediate -basic volcanic breccia
97.80	100.30	2.50	Andesitic (?) intrusion
100.30	110.03	9.73	Intermediate-basic volcanic breccia

ALTERATION

20.17	78.52	58.35	Moderate strong CB-PY-Sericite alteration
78.52	110.03	31.51	Unaltered zone

MINERALIZATION

44.80	69.28	24.48	Major SP, GN, TT, CP appearances Two main sections of CR-QZ vein as below
49.00	50.49	1.49	40 to core normal
66.71	69.28	2.57	40 to core normal
0.00	21.33	21.33	Casing
0.00	40.23	40.23	N.Q. core
40.23	110.03	69.80	B.Q core
20.42			First footage mark
20.17			Start sampling, measured from 20.42 m
20.42	20.42	39 cm recording, three pieces maroon x-line andesite, one piece silicified rock	

No limonite zone

20.17	47.30	27.13	Andesite Breccia, Pale green to grey clasts moderate altered, matrix is grey and pale greyish maroon in locals
20.17	34.00	13.83	30% sheared sections gougey
20.17	23.47	3.30	90% sheared, 70% gouge, one shear fracture at 45
23.47	26.00	2.53	40% sheared mainly at 35, 10% gouge
26.00	28.00	2.00	20% sheared sections 45-85, 5% gouge
28.00	30.00	2.00	30% sheared sections, one shear fracture at 48, 10% gouge Pale maroon matrix 20%
30.00	32.00	2.00	20% sheared sections 10-45, Major at 15-20 10% gouge, pale green
32.00	34.00	2.00	10% sheared sections, 1 CB vein 5 mm at 40 20% grey matrix, clasts have abundant altered mafic

mineral 2 mm - 4 mm in diamters (sericitized)

34.00	36.00	2.00	36.77 m: a silicified section 11 cm lag 15, 20% irregular quartz veins Two gougey fractures at 20
36.00	38.00	2.00	5% sheared sections at 20, 45 37.69-38.71 m gougey
38.00	40.23	2.23	3% silicious grey matrix
40.23	42.32	2.09	Core ground as at 40.23 m: when changed to B.Q Bit
42.32	44.80	2.48	Low recovery 20% gouge, some sheared at 42 42.59 m: QZ-CB vein 2 cm, 45
44.80	46.21	1.41	30% sheared at 20-40, 10 gouge 45.61 m: QZ vein 1 cm at 55 with 30% SP 20% PY, minor GN, CP
46.21	48.00	1.79	47.43 m: 4 cm pyritic vein at contact 40
47.30	60.00	12.70	Andesite, crystalline altered (pale), phenocrysts 30%, 1-2 mm in diameters
48.00	49.00	1.00	48.54 m: 2 mm QZ vein, 38% with SP, GN 48.9 m: 2 mm QZ vein 05 with SP GN TT
49.00	50.49	1.49	49.12-49.54 m: main QZ-CB vein section at 40, minor SP GN selvage 50.2 m: /cm thick QZ-CB vein with 2.5% SP minor GN
50.49	52.53	2.04	51.7-52.65: pale green
52.53	55.00	2.47	40% sheared sections at 10 & 40, 5% gouge 54.16 m, QZ vein, 6 cm thick at 45
55.00	57.00	2.00	55-56.4 m: pale green 55.4-55.76 m: cooked up with 20% QZ 55-76-56 m: brecciated up by 20% grey silicious matrix
57.00	58.92	1.92	57-57.20 m: cooked up with 30% pale maroon volcanics, silicious 58.57 m: sheared fracture 38 minor SP
58.92	60.00	1.08	5% sheared at 40 49.8 m, 6 cm silicified vein at 40
60.00	78.52	18.52	Andesite Breccia
60.00	61.31	1.31	Irregular QZ-CB veinlets 1-7 mm, mainly 20 with some SP, GN
61.31	62.40	1.09	40% matrix 5% gouge, 2-5 cm thick 35-40
62.40	64.69	2.29	50% matrix
64.69	66.71	2.02	30% matrix
67.71	68.00	0.29	Moderate silicified, some quartz veinlets associated with SP, GN, TT, CP 67.88 m: a quartz lens 6-20 mm, 20 & 45 with 40% SP 30% PY 20% gouge
68.00	69.28	1.28	70% sheared sections at 40 78.71 m: 2 mm QZ lens with some GN SP
69.28	70.14	0.86	Pale green 69.28-69.59 m: slightly sheared at 40
60.14	72.00	11.86	Light green beccias in 20% grey matrix
72.00	74.00	2.00	Light green & 20% matrix as above 73.67-74 m sheared at 25, gouges
74.00	76.45	2.45	Pale green
76.45	77.45	1.00	70% sheared, 60% gouge 76.71 m: QZ lens 1 cm, 40 with SP
77.45	78.52	1.07	77.07-78.52 m: silicified, upper contact 47

lower contact = 38

78.52 80.58 2.06 Intermediate to basic volcanic breccia grey cooked up & brecciated up with tuff (?) unaltered. Porphyritic looking, felsic minerals about 70%, fine to coarse grain; matrix is grey fine grain local medium grain mafic minerals

80.58 83.65 3.07 Tuff: pale green, 50% fine recrystalline feldspars, 5-10% clast, < 1 mm to 3 cm in diameters and to surround. Grey green maroon colors, lower contact = 25

79.00 105.00 26.00 Competent core

83.63 85.95 2.32 Andesitic c intrusion light grey fine grain (Subvolcanics)

80.58 83.58 3.00 81.51-81.65: 2 cm QZ veins & silicified section associated with PY contacts are 40
83.5 cm: 6 mm QZ vein, 40 with PY

83.58 86.63 3.05 86.28-82.63: greenish grey color slightly cooked by the greyish volcanics

85.95 97.80 11.85 Intermediate-basic volcanic breccia as above

86.63 90.00 3.37 No comment

90.00 93.00 3.00 No comment

93.00 95.00 2.00 Local dark grey holes with diameters = 10^14 cm

95.00 97.80 2.80 95.49-95.68 m: shear fractures 28 with PY some QZ spots and veinlets

97.80 100.30 2.50 Andesitic intrusion (Dyke ?): Fine grain with 10% altered (sericitized) greenish phenocrysts = 1.5 mm long. Matrix is massive, pale pink, green, grey colors Upper contact = 20, lower contact = 5

100.30 110.03 9.73 Intermediate-basic volcanic breccia as above (with tuffaceous ? clasts)

100.30 103.00 2.70 No comment

103.00 106.00 3.00 105.89-106.09 m: Gouge at 20 & 42

106.00 107.72 1.72 10% sheared sections at 42

107.72 110.03 2.31 A 1 cm thick CB/V = 90

HI-TEC RESOURCE MANAGEMENT LTD.

DIAMOND DRILL LOG

Property Name:	HANK	Client Name:	LAC MINERALS LTD.	Borehole Test Method:	Tropari
Hole No:	89-DDH-03	Azimuth:	320	Test Azimuth:	315
Northing:	10670.036	Dip:	-64	Test Dip:	-66
Easting:	10163.149			Test Depth:	128.6 m
Elevation:	1116.820m	Length:	130.14 m	Date Started:	August 17, 1989
				Date Completed:	August 19, 1989

Overall impression of hole

LITHOLOGY

FROM TO WIDTH (m)

12.19	19.07	6.88	Andesite Breccia
19.07	23.25	4.18	Tuff
23.25	37.73	14.48	Andesite
37.73	48.00	10.27	Andesite Breccia
48.00	51.91	3.91	Andesite
51.91	69.19	17.28	Andesite Breccia
69.19	77.27	8.08	Andesite
77.27	101.91	24.64	Andesite Breccia
101.91	103.95	2.04	Tuff
103.95	112.11	8.16	Andesite Breccia
112.11	113.04	0.93	Pale Green Lava
113.04	115.61	2.57	Andesitic Intrusion
115.61	117.95	2.34	Latite (?)
117.95	125.52	7.57	Andesite
125.52	130.14	4.62	Andesite Brecciated by Intermediate-Basic Volcanics

ALTERATION

12.19	109.12	96.93	Carbonate-PY-Sericite altered
109.12	103.14	-5.98	Unaltered

MINERALIZATION

82.52	101.20	18.68	Major QZ-CB veins and GN, SP, CP, TT appearances
			Three main QZ-CB vein zones as below
82.52	83.89	1.37	75 to core normal
89.57	92.49	2.92	80 to core normal
97.85	101.20	3.35	70 to core normal

12.19	12.19	Casing
12.00	12.00	Overburden
17.37	17.37	First footage mark
18.49	41.76	23.27 NQ core
41.76	130.14	88.38 BQ core
		No visible limonite zone
12.19	17.37	5.18 Mismatch. Very low recovery (4%)

12.19	19.07	6.88	Andesite Breccia
17.37	19.07	1.70	17.37-17.77: moderate broken up and 5 cm sheared
19.07	23.25	4.18	Tuff, pale green, 2 1/2% clast less than 1 cm
19.07	21.05	1.98	19.55-19.90: shattered
			19.36-19.53 m: some pale greyish maroon silicic intrusion

21.05	23.25	2.20 22.9-23.8 m: sheared at 30, 2 cm gouge
23.25	37.73	14.48 Andesite minor clast in locals
23.25	26.00	2.75 Sheared 30% gouge
26.00	28.00	2.00 0.1% blackish mineral 27.25-27.44 m: sheared at 45 gougey
28.00	30.00	2.00 28-28.8 m: slightly sheared 2.5% clasts
30.00	32.00	2.00 .3% blackish mineral dissemination Some fractures at 45
32.00	34.00	2.00 33-33.70 m: sheared at 42 2.5% clasts
34.00	36.00	2.00 34-35.18 m: moderate sheared at 45 1 cm QZ lens attached to 6 cm silicified section 10% gouge
37.73	48.00	10.27 Andesite Breccia
36.00	38.00	2.00 Two QZ-CB vein 1 cm thick 65-70 Once QZ-CB vein 6 mm at 45
38.00	39.83	1.83 38.71-39 m: silicified and brecciated with QZ veins 2 mm to 1.5 cm
39.83	41.00	1.17 4.15 m: QZ-CB vein 2 cm 40 40.9 m: QZ-CR vein 1.5 cm 45 with SP, PY
41.00	41.76	0.76 40% pale greyish maroon, matrix
41.76	44.80	3.04 41.76-44 m: altered from maroon porphyritic andesite 42.75-44 m: sheared gouge at 90
44.80	46.87	2.07 45-46 m: slightly sheared at 45, 5% gouge
46.87	48.00	1.13 Sheared at 33%, 5% gouge 47.88 mQZ vein 5 cm 38 with 20% PY
48.00	51.91	3.91 Andesite pale greenish grey
48.00	50.00	2.00 49.49 m: 1 cm QZ-CB vein 45 with SP, GN
50.00	51.00	1.00 50.32-50.42 m: some banding at 45 50 m: CB vein 1 cm at 30 50.88-50.9 m: Few QZ-CB veinlets 1-2 mm 20-40
51.00	52.00	1.00 51-51.3 m: Three major CB vein 1 cm, 5 cm, are at 30 unmineralized. 51.32-51.40 m: Gouge at 22 51.48-51.84 m: Porphyritic texture
51.91	69.19	17.28 Andesite breccia
52.00	53.70	1.70 20% sheared sections
53.70	54.70	1.00 54 m: 2 cm CB vein, no sulfide at 42
54.70	56.18	1.48 10% sheared at 10, 45, 5% gouge 55.59-56.02: Moderate silicified with QZ veinlets
56.18	58.00	1.82 20% pale grey matrix
58.00	60.00	2.00 50% matrix. Few QZ veinlets 2-3 mm 70
60.00	62.00	2.00 60.04-60.85 m: Moderate carbonatized with QZ-CB veinlets 2- 8 mm 50-75
62.00	64.00	2.00 Weakly sheared with CB veinlets and stringers
64.00	66.00	2.00 20% matrix
66.00	68.00	2.00 40% matrix
68.00	70.00	2.00 Alteration intensity = 4.5 69.13 m: shear fracture 70, some SP 69.25 m: QZ-CB vein 1.3 cm 120 no sulfide 69.37 m: QZ-CB vein 1 mm 40 some SP 68.72 m: QZ-CB vein 60, some SP, GN
69.19	77.27	8.08 Andesite: Local weak altered magnetic, green hematitized mafic minerals = 1 mm long
70.00	72.00	2.00 Light greenish grey, Bleaching bands = 40 70-70.15 m: green magnetic

70.56 m: 1 cm QZ-CB vein 65
 71.27-71.40 m: weakly silicified with QZ veinlets
 and spots
 71.58-71.7 m: some brownish intrusive veinlets
 72.00 74.00 2.00 72 m: two 2 mm QZ vein 45
 72-73.25 m: Light to pale brownish pervasive alteration
 74.00 74.64 0.64 20% CB veinlet network
 74.64 75.45 0.81 Few QZ-CB veinlets 1-6 mm at 5, 42, 60
 75.45 76.68 1.23 75.55-75.72 m: QZ-CB veinlet network 2-4 mm
 with some disseminated GN, SP
 76.02-76.68 m: some shear fractures at 45, 65
 76.68 78.33 1.65 77.62: QZ-CB vein 1.2 cm 50 no sulfide
 77.27 101.91 24.64 Andesite Breccia
 78.33 79.69 1.36 20% matrix
 78.52-78.77 m: Blacked with QZ-CB veinlets 1-3 mm
 10, 42, 80
 79.69 81.18 1.49 Some weakly sheared fractures at 10, 30, 50, 80
 81.18 82.52 1.34 81.18 m: Sheare fracture 4 cm, 70 with PY and QZ-CB lens
 QZ-CB veinlets and lens 1-12 mm at 10-45
 82.52 83.89 1.37 QZ-CB vein and alteration zone with .1% GN dissemination
 and Tr SP
 82.66 m - 83 m: main QZ-CB vein section, upper
 contact = 75, lower contact not clear
 83.29-83.52 m: QZ-CB vein section with 1% GN
 dissemination, upper contact 47, lower contact = 45
 83.6-83.89 m: CB vein 5 mm at 82
 The whole section is weakly sheared at 70-80
 83.89 84.43 0.54 83.89-84.2 m: Weakly sheared
 83.16 m: Sheared fracture 75 with 6 mm
 QZ-CB vein at 75
 84.4 m: CB vein 6 mm at 75
 84.43 85.89 1.46 50% matrix
 85.89 86.49 0.60 86.06 m: QZ-CB vein 5 cm 40 with SP 5%
 86.19 m: QZ-CB vein 1.5 mm 60 with SP
 86.49 87.47 0.98 50% matrix
 87.49 88.19 0.70 87.63 m: 4 cm thick QZ vein (two 1 cm thick vein) and
 altered section with SP, GN at 45
 87.94-88.19 m: sheared at 45 one QZ-CB vein
 3 mm with GN, SP
 88.19 89.57 1.38 88.8-89.2 m: Some greyish matrix banding at 42
 Three 2 mm QZ-CB vein at 42-45 with some GN, SP
 89.57 92.28 2.71 Shear zone with 20% QZ-CB veins and alterations
 associated with 0.3% GN & SP
 89.57 m: Sheared upper contact 45
 92.28 m: Sheared lower contact at 80
 89.57 90.60 1.03 89.57-90.05 m: sheared at 45-50
 90.14 m: Minor SP at CB fracture
 90.14-90.40 m: 40% irregular QZ-CB lenses
 (intruded in shear zone and welded) at 85
 90.40 m: QZ-CB terminated at 45 shear fracture
 minor CP
 90.60 91.82 1.22 Major QZ-CB vein & alteration zone
 90.6-90.9 m: 80% QZ-CB, minor SP, GN, TT, CP
 Upper contact = 25, lower contact = 75
 90.9-91.45 m: 10% QZ-CB small patches up to 4 cm in
 diameters and veinlets 1-2 mm associated with some SP, GN

94.45-91.82 m: 50% high angle QZ-CB veins with disseminated
 GN, TT, SP, CP
 91.45-91.53 m: 2mm and 15 mm QZ-CB veins at 45
 91.53-91.77 m: QZ-CB vein 25 mm at 90
 91.77-91.82 m: 1.7 cm QZ-CB vein at 50
 91.82 92.49 0.67 Shear zone. Fractures 75-90
 92.49 94.00 1.51 40% green clast 60% grey matrix
 94.00 96.00 2.00 60% matrix
 95.1 m: 2 mm QZ-CB lens with SP, TT
 96.00 97.85 1.85 50% matrix
 98.17 101.91 3.74 Shear zone accompanied with QZ-CB veins and silicification
 98.17 m: upper contact of QZ-CB vein at 70
 101.91 m: shattered
 97.85 98.72 0.87 97.97-98.02 m: Slightly bleached at 70 with SP, TT, GN
 at 5, 2 mm veinlet
 98.17-98.42 m: QZ-CB vein contacts are 70 disseminated
 with minor CP, TT
 98.17-98.64 m: moderate silicified and carbonatized
 5% PY
 98.64-97.70 m: QZ-CB vein at 70
 98.72 99.66 0.94 Shear zone at 70, 30, gouge
 99.66 101.20 1.54 80% silicified with quartz stringers
 101.20 101.91 0.71 Shattered gougey, low recovery
 101.91 103.95 2.04 Tuff: upper contact is not sure because of strong
 silicified shattered and gougey. Lower Contact = 80
 101.91 102.82 0.91 1% QZ veinlets 1-2 mm at 20-45
 102.82 103.88 1.06 102.82-103.3 m: Strongly silicified, some quartz
 veinlets 2 mm at 30 with minor SP
 103.56-103.73 m: Strongly silicified.
 Brecciated by QZ vein intrusion
 103.88 105.86 1.98 Strongly silicified and brecciated
 103.95 109.12 5.17 Andesite Breccia
 105.86 106.09 0.23 100% fault gouge, surrounded by 4-5 mm
 drill mud, (contaminated)
 106.09 109.12 3.03 106.09-107 m: Moderate shattered
 106.88-107 m: Silicified with QZ veinlets
 108.62-109.01 m: Silicified
 109.01-109.12 m: Sheared at 15
 109.12 112.11 2.99 Andesite breccia: 10% cooked up with or brecciated
 with dark grey intermediate to mafic volcanics
 111.45 - 111.70 m: Sheared at 30
 111.70-111.86 m: Silicified
 111.86-112.11 m: Sheared
 112.11 112.52 0.41 Pale green lava: with 10% amygdale filled with dark
 grey intermediate - mafic volcanics and some with PY
 Size up to 1 cm long, 2-4 mm wide
 The bubble elongated directions = 45%
 112.11 m: Upper contact = 25
 112.52 m: Lower contact = 32
 112.52 113.04 0.52 The above lava & cone andesite, 60% cooked up with the
 dark grey intermediate-mafic volcanics
 113.04 m: Contact = 42
 113.04 114.78 1.74 Andesitic intrusion as in DDH89-1, but with 20-20% pale
 green to grey altered mafic mineral flakes 2 1/2 mm long
 1 mm wide matrix is altered to light pinkish
 114.78 m: contact -55 cut by quartz vein

114.78 115.61 0.83 Silicified section. Lower contact =45
115.61 117.95 2.34 Latite: brownish, fine grain massive
115.61-116.69 m: 5% felsic mineral (feldspar ?)
Few CB and PY veinlets
117.95 m: Lower contact = 47
117.95 125.52 7.57 Andesite: Carbonate amygdalites in locals magnetic at
the unaltered greenish sections. Crystalline
117.95 121.00 3.05 117.95-118.51 m: 5% calcite amygdalites 1-15 mm long
1-6 mm wide. Bubbles elongated at 5
118.52 m: some brownish latite veins 2-8 mm
119.78-119.49 m: 1% calcite amygdalites
120.46-121 m: 20% dark grey intermediate-mafic
volcanics
Two calcite veins 8 mm, 10 mm at 45
121.00 124.05 3.05 Locally (10%) cooked up with dark grey intermediate-
mafic volcanic intrusion
121-121.25 m: Latite at 90
122.53-122.63 m: Latite at 35
123.24 m: 4 cm Latite at 20
124.05 127.10 3.05 124.68-125.52 m: 2.5% hematite dots < 1-2 mm in
diameters
125.52 130.14 4.62 Andesite brecciated up by dark grey intermediate-basic
volcanics
Andesite clast = 80-90%

Property Name:	HANK	Client Name:	LAC MINERALS LTD.	Borehole Test Method:	Tropari
Hole No:	89-DDH-04	Azimuth:	310	Test Azimuth:	259.5 (unreliable)
Northing:	10645.542	Dip:	-60.5	Test Dip:	-61
Easting:	10132.445	Length:	121.91 m	Test Depth:	112.91 m
Elevation:	1110.010m			Date Started:	August 19, 1989
				Date Completed:	August 20, 1989

Overall impression of hole

LITHOLOGY

FROM TO WIDTH (m)

11.28	47.00	35.72 Andesite Breccia
47.00	56.63	9.63 Andesite
56.63	63.12	6.49 Andesite Breccia
63.12	72.23	9.11 Andesite
72.23	90.76	18.53 Andesite Breccia
90.76	92.44	1.68 Intermediate-Basic Volcanics
92.44	104.04	11.6 Andesite
104.04	108.12	4.08 Andesitic Intrusion and Pale Green Lava
108.12	110.81	2.69 Andesitic Breccia
110.81	112.74	1.83 Pale green lava
112.74	121.91	9.17 Andesite and andesitic brecciated and cooked with intermediate-basic volcanics

ALTERATION

11.28	90.76	79.48 PY-CB-Sericite altered (41-56.63 m: weakly altered)
90.76	121.91	31.15 Unaltered

MINERALIZATION

20.83	73.83	53 Major SP, GN, TT, CP apperances
20.83	22.93	2.1 Major QZ-CB vein and SP, GN, TT, CP, zones
65.90	68.65	2.75 }
73.31	73.83	0.52 Veins of massive sulphides
10.67	10.67	Casing
11.28	11.28	First footage mark
11.28	11.28	29 cm recovery, 80% unaltered andesite fragments
11.28	11.28	Start sampling
11.28	18.00	6.72 Minor limonite on some fracture surfaces
31.39	31.39	No core
31.39	121.91	90.52 BQ Core
11.28	47.00	35.72 Andesite breccia; grey to pale green clast in grey matrix
11.28	14.32	3.04 Sheared at 50, 80, 10% gouge 11.28-12.28 m: Intruded by 25 QZ-maroon veins and lenses (brecciated up) 14 m: 30 cm silicified with QZ veins (40 ?)
14.32	16.00	1.68 40% sheared, 20% 15.7-16.1 m: Andesite
16.00	18.00	2 20% sheared and shattered, 10% gouge
18.00	19.50	1.5 40% sheared and shattered, 10% gouge at 45, 90 Minor blackish mineral
20.83	22.93	2.1 Shear zone with calite-QZ veins and sulfides
19.50	20.83	1.33 Competent, 20% matrix

20.83	22.16	1.33	50% sheared at 50-70, 20% gouge 20.83 m: shear fracture 60 21.37-21.76 m: weakly silicified with QZ-CB stringers with minor SP
22.16	27.93	5.77	22.16-27.29 m: sheared at 22 22.29-22.40 m: brecciated by SP-PY-and blackish mineral 40% at 42-45 22.59-22.81 m: RZ-CB vein 20, with 5% SP, some CP, TT, GN, PY 22.93 m: 3 cm silicified section with QZ-CB, some SP, CP, (at 42)
22.93	25.00	2.07	22.47-25 m: highly carbontized 22.4-22.70 m: QZ-CB vein (1 cm) network, Tr, SP, 24.38 m: 4 cm BA-CA-QZ vein 30, no sulfide 24.82 m: gouge 4 cm at 43
25.00	27.27	2.27	50% grey matrix
27.07	28.07	1	27.3-28.74 m: moderate silicified and carbonatized with QZ-CB veins with 0.1% SP, TT, GN. Upper contact at 47 Lower contact at 43
28.07	29.21	1.14	Shear fracture 85, gougey Minor SP at 1 mm QZ-CB veinlet at 50
29.21	31.39	2.18	29.85-30.5 m: sheared 29.85-31.39 m: 30% grey silicicous matrix
31.39	33.00	1.61	Few calcite and QZ-CB veinlets 2-5 mm, 50, 40
33.00	35.00	2	No comment
35.00	37.00	2	Weakly sheared at 20-45
37.00	38.55	1.55	80% matrix, 20% pale green clasts
38.55	39.13	0.58	QZ-CB vein and SP, GN section 5% SP 38.71 m: 18 mm QZ-CB vein 45 with SP, GN selvage 38.76 m: 18 mm QZ-CB vein 45 with SP, GN selvage 38.84-39.11 m: QZ-CB vein >1 cm 90 with SP, GN, selvage
39.13	41.00	1.87	41.47-41.49 m: 2 QZ-CB veinlets 3 mm 45 with SP, GN
41.00	43.00	2	42.32 m: QZ-CB vein 8 mm 45 with SP, GN, 30% grey matrix
43.00	45.00	2	40% grey matrix 60% pale green clasts
45.00	47.00	2	20% grey matrix, 80% pale green clasts
47.00	56.63	9.63	Andesite: greenish gray to light grey, local magnetic at greenish color sections
47.00	49.00	2	47.68 m: 3 mm QZ-CB spot with SP
49.00	51.00	2	One 3 cm clast 50.7-51 m: 1% hematite altered mafic minerals
51.00	53.67	2.67	50% green section, fine to medium grain magnetic
53.67	54.61	0.94	1% of SP, some CP, GN, TT associated with QZ-CB veins 53.71-53.80 m: QZ-CB vein, upper contact 75 Lower contact 38 54.03-54.13 m: QZ-CB vein. Upper contact 45 Lower contact = 38 54.13-54.32 m: QZ-CB vein 3 mm, 80 54.38 m: & 54.42 m: 1.5 mm veins at 10 & 30 54.55 m: 1.5 cm vein 45 All the above veins have SP, TT, GN, CP, PY
54.61	56.63	2.02	54.98-55.5 m: some pale maroon banding at 40 55.6-55.90 m: 3% hematitized mafic minerals
56.63	63.12	6.49	Andesite breccia Higher alteration intensity
56.63	58.03	1.4	50% sheared at 45 56.70-56.93 m: some QZ lens at shear fracture with

minor SP, GN
 57.32 m: gouge 6 cm at 45
 58.03 60.00 1.97 Slightly sheared 30%
 58.52-58.73 m: some SP at QZ-CB veinlets 2 mm at 40-45
 60.00 62.00 2 61.52-62 m: shear section (61.61-61.72 m)
 with QZ silicified section (61.52-61.61 m)
 61.86-62 m: brecciated with 10% QZ, some blackish
 mineral dissemination
 62.00 64.66 2.66 62.45 m: QZ vein 3 cm at 45 ? some PY
 63.13 m: QZ vein 2 mm with abundant SP at 50
 63.7 m: QZ-CB lenses 3 mm thick 12 mm long with SP
 63.64-64.35 m: light green andesite
 63.12 72.23 9.11 Andesite
 64.46 65.90 1.44 1% QZ-CB veinlets 1-2 mm 20, 40 and 90 with SP
 65.8-65.9 m: 2.5% hematite disseminated alteration and
 and tiny fracture filling
 65.90 66.25 0.35 5% SP, GN, TT minor CP associated with QZ-CB veins
 65.93 m: SP, TT, GN vein with CB-QZ 2 mm at 65
 65.97-66.23 m: Main QZ-CB veins sections with
 SP, TT, GN, CP. Upper contact 43
 Lower contact = 47
 66.25 67.25 1 66.49 m: QZ-CB vein 1 cm 90, Tr, GN
 66.86 m: 2.5 cm QZ-CB vein at 80 minor PY
 67 m: 2.5 cm QZ-CB vein at 52 with SP, CP, PY
 67.25 68.65 1.4 69.79-68.91 m: 3 mm QZ-CB vein 65 with 80% SP, TT, GN
 68.33 m: 4 mm wide QZ-CB lens 3 cm long at 35 with 60% SP
 68.54 m: 1.8 cm QZ-CB vein Tr. SP
 68.65 70.69 2.04 100% sheared
 70.09 m: some SP associated with CB veinlets at 35
 (four 1 mm thick veinlets)
 70.69 72.23 1.54 72.2 m: 2 cm cooked up with pale maroon vein at 45
 72.23 73.31 1.08 10% sheared at 35, 55, 90
 72.70-72.82 m: weakly silicified
 73.31 73.83 0.52 73.38 m: 1 cm massive SP, GN, TT, CP, vein at 70
 73.45 m: 2 cm (square) thodachrosite spot
 73.57 m: 1 cm thick 3 cm long massive sulfide vein at 70
 73.79-73.80 m: 5 cm true thickness of massive sulfide
 vein at 50
 72.23 90.76 18.53 Andesite breccia
 73.83 75.00 1.17 Sheared at 70-85
 75.00 77.00 2 Very pale altered (a different stage of volcanics ?)
 77.00 78.00 1 As above, but some fadé clastic texture (?)
 78.00 79.00 1 78.70 m: 1 cm QZ-CB vein 40 with 50% SP
 Brecciated
 79.00 80.00 1 79.3 m: 5 cm altered vein, 50 with 10% PY
 80.00 82.00 2 Fadé casts 70%
 82.00 84.43 2.43 83.85-84.68 m: sheared, gougey
 84.43 85.46 1.03 84.84 m: 1 mm GN, SP, CB at fracture 80
 84.94 m: same as above but at 35
 85.36 m: CB lens 3 mm at 30 with SP
 85.46 86.46 1 40% sheared at 45, 90, gougey
 86.46 89.00 2.54 88.22-89.47 m gougey at 50
 89.00 90.76 1.76 90.57-90.66: sheared at 55 PY and blackish mineral
 90.76 90.76 Ground core or washedaway mud at contact lost 0.74 m
 90.76 92.44 1.68 Intermediate to basic volcanics, dark grey with 50%
 feldspar 1-1/2 mm long, 1/2 mm wide, matrix is dark grey

non magnetic, 2.5% black argillite clasts
 90.76-91 m: 2.5% PY blebs
 94.42 m: 5 cm maroon gouge at 0 (?)
 92.44 104.04 11.6 Andesite (dark grey)
 Colored up by dark grey intermediate-mafic volcanics;
 also contains or cooked up some black argillite clasts
 from few mm to 30 cm. Mainly weakly altered by the
 intermediate-basic volcanic activity
 90.76 90.76 Start unaltered rock
 92.44 95.00 2.56 Mainly QZ veinlets 1-2 mm 5-20 few at 45
 95.00 98.00 3 Few QZ-CB veinlets 1-3 mm at 40 one with PY selvage
 98.00 101.00 3 10% argillite clasts
 98.43-98.76 m: sheared at 80
 98.8-99 m: Pervasive PY-CB
 100.25-100.48 m: pervasive PY-CB
 Mainly QZ & QZ-CB veinlets 1-5 mm 20-45 few at 70-80
 101.00 103.95 2.95 101.02 m: two small PY veins 9 mm & 1 mm at 30
 102.9-103.56 m: 10% QZ-CB veinlets network
 Two calcite lens, 2 1/2 cm in diameters no sulfide
 104.04 106.46 2.42 Andesitic Intrusion
 Pale green and pale pinkish locally cooked by the later
 dark gray intermediate-basic volcanic with 20% mafic mineral
 flakes 1-2 mm long, 1/2 mm wide, usually epidolized or
 sericitized matrix is massive, very fine
 106.46 107.16 0.7 Pale green lava as in hole 89-3 but no amygdales. Locally
 brecciated by the above andesitic intrusion and locally
 cooked up by the intermediate-basic volcanics
 Upper contact =32; Lower contact =70
 107.16 108.12 0.96 Andesite intrusion as above
 Lower contact =45
 108.12 110.91 2.79 Andesitic breccia
 Cooked up and brecciated up with dark grey intermediate
 mafic volcanics lower contact =10
 103.95 106.24 2.29 10% QZ-CB veinlet network. No sulphide
 103.95-104.76 m: the vein zone is about 70
 106-106.14 m: vein zone is at 45
 108.12 110.91 2.79 Pale grey to dark grey
 110.91 112.74 1.83 Pale green lava as above
 Lower contact = 5 (irregular)
 112.08 m: QZ-CB veinlet 5 mm, 55 some PY
 112.74 121.91 9.17 Andesite brecciated to cooked up to dark grey
 intermediate-basic volcanics (some andesite breccia)
 Dark grey & pale green color
 121.35 121.91 0.55 Sheared and shattered for 70% of sections
 121.74 116.00 5.74 113.74-113.91 m: gouge at 3
 116.00 118.00 2 116.4 m: QZ vein 5 mm, 30 with SP
 117.7 -11.95 m: shattered
 118.00 121.91 3.91 70% shattered
 180.6 m QZ vein 9 mm at 65

HI-TEC RESOURCE MANAGEMENT LTD.

DIAMOND DRILL LOG

Property Name: HANK Client Name: LAC MINERALS LTD.
 Hole No: 89-DDH-05 Azimuth: 310 Borehole Test Method: Tropari
 Northing:10645.342 Dip: -74.5 Test Azimuth: 311 Core Size: NQ & BQ
 Easting: 10132.645 Length: 157.58 m Test Dip: -75 Date Started: August 21, 1989
 Elevation:1110.010m

Overall impression of hole
 LITHOLOGY

FROM TO WIDTH (m)

8.23	40.00	31.77 Andesite Breccia
40.00	53.13	13.13 Andesite
53.13	141.60	88.47 Andesite Breccia
141.60	146.68	5.08 Andesite
146.68	157.57	10.89 Andesite (cooked up by intermediate-basic volcanics)

ALTERATION

8.23	45.00	36.77 C
49.00	146.48	97.48 (Moderate to high PY-CB-sericite alteration
30.68	36.13	5.45 C
38.17	39.75	1.58 C
61.49	62.60	1.11 C
89.99	98.40	8.41 (Are the possibly high Au mineralization zone, with SP, GN, CP, TI, in parts
	7.62	7.62 Casing
	7.00	7.00 Overburden
8.23		8.23 First footage mark
8.23		8.23 32 cm recovered, 10 pieces of core 2-4 cm long, 60% unaltered green andesite 40% altered andesite
8.23		8.23 Start sampling
8.23	8.50	0.27 Minor limonite on fracture surfaces
	31.15	31.15 NQ core
31.15	157.58	126.43 BQ core
8.23	40.00	31.77 Andesite Breccia; grey altered
8.23	11.00	2.77 8.79-9.10 m: fractures 90 and 45. moderate shattered
12.79	23.90	11.11 Sheared and shattered 40% gouge
11.00	12.79	1.79 Intruded and cooked up by maroon volcanics 5%
12.79	14.32	1.53 80% gouge some visible fractures at 40 & 80 1% maroon volcanics interstitial
14.32	17.37	3.05 60% gouge, 2.5% maroon volcanic veins (3 cm at 20) blebs and interstitial
17.37	18.37	1.00 90% gouge
18.37	20.42	2.05 Shattered
20.42	23.47	3.05 40% shattered, 2.5% gouge at 45 & 80
23.47	25.64	2.17 One CB vein 1 cm 45, no sulfide 25.21 m: shear fracture 45 some CB and blackish mineral
25.64	26.77	1.13 Sheared and 30% shattered, 5% gouge at 20, 40 and 80, minor CB veinlets with gouge.
27.52	29.90	2.38 Few CB veinlets 1-2 mm at 25-45 One gougey fracture at 45 20% grey matrix 80% pale whiteish clast

29.90	30.68	0.78 50% sheared at 50 29.9-30.18 m: shattered, washed away gouge (?) some calcite veinlets
30.68	31.15	0.47 Sheared, some SP, GN associated with calcite veinlets mainly at 85 about 4 mm (?) some irregular filled in fractures 4-6 mm, 20-30, SP = 2.5%
31.15	32.61	1.46 Soft ground, ground and washed away a lot low recovery BB start at 31.15 m.
30.68	39.75	9.07 Calcite and QZ-CB vein zone contains 2 main sections associated with SP, GN
31.50		31.50 Changed to BB bit, ground some core here, also broekn up and gougey, low recovery
31.50	32.61	1.11 Very low recovery. Shattered gougey
32.61	33.98	1.37 32.61-32.71 m: moderate silicified with 1.5 cm QZ vein, 42, some PY 32.76 m: 12 mm QZ-CB vein at 80, no sulphide 32.81 m: 4 cm gouge at 45 32.95-33.09 m: sheared and rich calcite 33.12-33.98 m: QZ-CB veinlets (one pink), 1-4 mm 70-80 with some SP, PY
33.98	35.66	1.68 Mainly high angle veins 33.98-34.23 m: QZ vein 5 mm, 90 with minor SP, GN 35.17-35.66 m: some QZ-CB veinlets 2- 3 mm 45 & 90 with some SP
35.66	36.13	0.47 Sheared at 75 & 90 with some QZ-CB veinlets 1-3 mm at 75
36.13	37.11	0.98 10% grey silicious matrix two gougey fractures at 45
37.11	38.17	1.06 20% grey silicious matrix 80% pale green andesite clast
38.17	38.75	0.58 38.17-38.26 m: gouge 0 38.26-38.34 m: QZ-CB veinlet network 38.34-38.54 m: QZ-CB veins and alteration at 45 with 20% SP some GN, CP 38.58-38.72 m: 30% SP associated with QZ-CB veins 2.5 cm (3 veins) at 45 accompany with shearings
38.75	39.48	0.73 Totally brecciated up by QZ CB intrusion upper contact 45, lower contact 42
39.48	39.75	0.27 QZ-CB vein associated with SP, GN (1% SP) Upper contact = lower contact = 30
40.00	53.13	13.13 Andesite; grey to pale green
39.75	40.74	0.99 40.59-40.65 m: Irregular QZ, CB vein at 15 with GN, SP 40.67-40.76 m: some greenish banding 2-3 mm on 5
40.74	42.00	1.26 Grey, 41.92-42 m: shear fractures at 20-30
42.00	44.00	2.00 Grey, good andesitic crystalline texture = 50% altered feldspar phenocryst about 2 mm in diameters Local hematitic altered mafic minerals
44.00	45.00	1.00 44.49 m: 2 1/2 QZ vein 45 with some SP, GN 44.8 m: 2 mm QZ vein 45 with SP, GN
45.00	47.00	2.00 Bleached, with hematite altered mafic minerals
46.78	49.20	2.42 Green unaltered andesite, magnetic crystalline
47.00	49.00	2.00 Mainly dark green andesite, magnetic
49.00	51.00	2.00 49.17-49.48 m: bleached at 45 as a 2 cm QZ vein 45 at 49.45 m 50.15-50.21 m: some grey silicious veins 0 50.31-50.53 m: matrix is pale maroon altered
51.00	53.00	2.00 51.1-51.63 m: sheared at 60 51.63-52.36 m: pale maroon altered matrix

53.00	55.00	2.00 53.05-53.13 m: sheared at 45
53.13	141.60	88.47 Andesite breccia: greyish matrix and pale or whiteish clasts
55.00	57.00	2.00 5% of andesitic clasts were whiteish altered
57.00	59.00	2.00 60% pale grey matrix
59.00	61.49	2.49 30% matrix
61.49	62.60	1.11 A 1-1.2 cm QZ-CB vein 85 strike along whole section; associated with SP, GN, TT, CP 62.6 m: vein terminated at 30 shear fracture
62.60	64.00	1.40 Few shear fractures 35-45 Few QZ-CB veinlets 1-2 mm 35-45
64.00	66.00	2.00 54.7-65.1 m: slightly bleached with a 3 mm QZ-CB vein at 85 associate with PY
66.00	68.00	2.00 20% matrix grey 67.35 m: 3 mm QZ-CB vein 45 at shear fracture
68.00	70.00	2.00 30% matrix, pale or whiteish clasts
70.00	72.00	2.00 70.14-71.47 m: weakly sheared, higher carbonatized
72.00	74.00	2.00 40% matrix, some shear fractures at 45 & 65
74.00	76.00	2.00 40% matrix pale whiteish clast 74.21-74.36 m: sheared at 45
76.00	77.05	1.05 QZ-CB veins 2-20 mm at 10 77.02 m: 1 cm QZ-CB vein 65 with PY
77.05	79.00	1.95 40% matrix
79.00	81.30	2.30 79.72-69.74 m: two QZ-CB veins 3 and 1 mm at 8 with SP 80.95-31.15 m: one CB veinlet, 1 mm 65 with SP
81.30	81.91	0.61 No comment
81.91	83.09	1.18 82 m: 1-2 mm QZ-CB veinlet 75 with SP
83.09	83.90	0.81 One higle angle 80-90 QZ-CB vein 2-15 mm associated with SP, PY SP=2.5% 1% disseminated blackish mineral
83.90	85.00	1.10 83.9-84.3 m: 0.3% disseminated blackish mineral
85.00	86.00	1.00 85.75-85.9 M slightly sheared 45 and 80
86.00	87.00	1.00 86-86.18 m: sheared 20, gougey 86.7-86.91 m: sheared at 35 with few QZ-CB veinlets 1-5 mm
87.00	88.00	1.00 60% pale grey matrix
88.00	89.00	1.00 88.25 m: 5 cm QZ vein 55 baren
89.00	89.99	0.99 88.79-89.34 m: 2 mm QZ-CB vein, 85, baren
89.99	98.38	8.39 Shear zone with strong carbonatization and associated with some SP, GN, CP, TT, at about 75 in general
89.99	91.00	1.01 89.99-90.24 m: sheared 60 gougey with 1 cm QZ-CB lens at 80 with SP 90.74 m: 1 cm calcite vein at 0
91.00	92.00	1.00 70% sheared at 40-130, 20, 70 gougey 91.72-91.82 m: QZ-CB veinlets at 45 and 135
92.00	93.00	1.00 Sheared, 30% gouge, highly carbonatized some calcite veinlets and QZ-CB veinlets 45-70 associated with minor SP
93.00	94.35	1.35 30% sheared, 10% gouge
94.35	94.76	0.41 Gouge, 94.35 m: contact 0. Some SP and blackish mafic mineral. One CB lens, 12 mm, 45
94.76	95.24	0.48 94.76-94.83 m: sheared at 70 gougey some SP 94.89 m: 3 cm silicified with QZ-CB veinlets at 60 94.89-95.13 m: massive sulfide vein, 40% QZ-CB veinlet network, 50% SP, 2.5% CP, 2.5% PY some GN, TT, lower contact is irregular 0 (95.13-95.20 m has the above vein extention >2 mm at 85) 93.89-95.24 m: gouge

95.24	96.28	1.04 Sheared gougey
96.28	97.67	1.39 96.28-96.62 m: competent andesite breccia 96.62-97.67 m: sheared, 10% gouge some QZ-CB veinlets 2-10 mm at 45, 50 with SP, PY
97.67	98.40	0.73 97.67-97.85 m: competent section, minor SP around 97.85 m 97.85-97.98 m: gouge, upper contact at 45 Lower contact = 68, some PY minor SP 97.98-98.07 m: vein consists of 10% QZ-CB, 20% SP 1% CP, 5% Py, 1 cm banded texture at upper contact (some QZ and dark grey seams) Lower contact of vein = 55 98-98.37 m: moderate silicified, minor SP
98.40	99.40	1.00 99.04-99.34 m: Andesite upper contact = 45 Lower contact = 5
99.40	101.00	1.60 Some QZ-CB veinlets 1-6 mm at 10, 45
101.00	103.00	2.00 Few shear fractures 40-45
103.00	105.00	2.00 103-104 m: few high angle fractures 104-104.2 m: trace SP, 1% blackish mineral dissemination
105.00	105.69	0.69 40% matrix 105.55 m: QZ vein 3 mm 45
105.69	106.30	0.61 Sheared, bleached high angle gougey
106.30	107.51	1.21 106.95 m: 3 mm SP, GN vein with minor QZ at 80 107-107.51 m: 5% QZ-CB stringers 1% blackish mineral dissemination, trace SP
107.51	108.81	1.30 108.62 m: 9 mm QZ-CB vein 80 with some PY
108.81	111.00	2.19 50% grey matrix, 50% pale clast
113.00	115.00	2.00 113-113.25 m: high angle silicified (1/2 core) 113.58-113.81 m: 1% disseminated blackish mineral 114.2 m: gouge at 60
115.00	117.60	2.60 20% sheared sections, 40 & 68 gougey 115.38-115.55 m: 1% disseminated blackish mineral 115.78-116.5 m: 30% gouge 116.3 m: CB vein 7 mm 48 with PY 116.61 m: shattered CB/V
117.60	120.33	2.73 CB vein and QZ-CB-vein zone on top of shear zone
120.33	126.59	6.26 Shear zone. 126.59 m: shear contact 30
117.60	118.84	1.24 117.64 m: QZ-CB vein 4 cm, 65 118.47 m: QZ-CB vein 4 cm at 15 118.56 m: QZ-CB vein 1 cm 30 118.63 m: QZ-CB vein 3 cm 50 118.52-118.84 m: moderate silicified
118.84	120.33	1.49 Totally cooked up, carbonatized and silicified with QZ-CB vein intrusion 118.84 m: QZ-CB vein 15 mm at 45 contact 120.18 m: Lower contact 30 120.18-120.31 m: Dark grey silicilous matrix brecciated up andesite
120.33	121.33	1.00 80% sheared, 60% gouge 120.33-120.50 m: weakly silicified
121.33	122.33	1.00 Gouge, gray
122.23	123.33	1.10 90% gouge
123.33	124.33	1.00 90% gouge
124.33	126.59	2.26 90% gouge. Some broken up CB vein, some PY cubes
126.59	127.51	0.92 50% greyish matrix
127.51	129.01	1.50 Very low recovery, ground core and muddy soft ground just round rubbles of 1-4 cm in diameters were recovered,

		some QZ-CB with massive SP, 2 cm in diameter
129.01	130.14	1.13 Few QZ-CB veinlets 2 mm 45-50
130.14	131.63	1.49 40% sheared sections at 45 131.28-131.40 m: some QZ veins = 1 cm 40
131.63	133.00	1.37 A weakly sheared fracture 85-90 associated with some QZ passing through the whole section
133.00	134.64	1.64 134.08-134.64 m: sheared
134.64	138.94	4.30 Silicified. Upper contact 70. Lower contact 60
134.64	136.46	1.82 136.14 m: weakly silicified, grey matrix pale clasts. Some QZ spot, 5 cm round (this high ample, QZ vein) 136.14-136.46 m: strongly silicified 136.24 m: contact = 75 (silicified vein)
136.46	139.94	2.48 Totally silicified matrix, pale whiteish grey Partial silicified clasts
139.94	151.60	12.66 Few QZ-CB veinlets 1-2 mm with PY at 30, 60, 75
141.60	146.48	4.88 Andesite, upper contact = 75 Grey altered
151.60	143.60	8.00 144.6-141.9 m: slightly sheared at 80 142.54 m: shear fracture 65 with QZ-CB vein 1 cm 142.81-143 m: sheared at 85
143.60	146.48	2.98 143.17-143.72 m: weakly sheared at 70 144.45m: Three QZ-CB veinlets 2-3 mm, 68 145.38-145.77 m: Intruded and cooked up with dark grey intermediate-basic volcanics 145.46 at 75, some shear fracture 146-146.48 m: 2-3 mm high angle QZ veinlet cut by some low angle 0-10 QZ-CB veinlets 1 mm. These veinlets all cut the dark grey fractures
146.48	157.57	11.09 Andesite: Mainly altered, intruded, and cooked up by the dark grey intermediate-basic volcanics. Pale grey & dark grey
146.48	148.00	1.52 30% cooked with intermediate-basic volcanics high PY in locals
149.00	150.00	2.00 80% cooked up or brecciated with the intermediate-basic volcanics 148.7-149 m: QZ vein 3 mm 80, with some GN, SP, CP 149.3-150 m: 5% PY veinlets 45 and dissemination
150.00	152.00	2.00 Some high angle and low angle quartz veinlets
152.00	153.55	1.55 Bleached, 20% silicified sections with quartz veins 70 high PY
153.55	156.00	2.45 153.55-155.47 m: Moderately silicified with QZ veinlet network 155.47-156 m: strongly silicified
156.00	157.57	1.57 157.19-157.57 m: brecciated up by intermediate-basic volcanics QZ-CB veinlets, baren, 1-6 mm, 30-60

Property Name:	HANK	Client Name:	LAC MINERALS LTD.	Borehole Test Method:	Tropari
Hole No:	89-DDH-06	Azimuth:	320	Test Azimuth:	318.5
Northing:	10573.316	Dip:	-50	Test Dip:	-51
Easting:	10073.404	Length:	111.86 m	Test Depth:	110.34 m
Elevation:	1103.950m				Date Started: August 23, 19
					Date Completed: August 25, 19

LITHOLOGY

FROM TO WIDTH (m)

12.88	18.72	5.84 Andesite Breccia
18.72	32.60	13.88 Andesite; 32.6-35.5 m: Lapilli
35.50	44.32	8.82 Andesite Breccia
44.32	57.30	12.98 Andesite
57.30	68.63	11.33 Andesite Breccia
68.63	74.20	5.57 Andesite (local clasts)
74.20	82.34	8.14 Andesite Breccia
82.34	95.11	2.77 Andesite
85.11	86.86	1.75 Latite
86.86	91.38	4.52 Andesite (cooked up and/or brecciated up by intermediate-basic volcanics)
91.38	92.54	1.16 Andesitic Intrusion
92.54	92.84	0.30 Pale Lava (?)
92.84	111.86	19.02 Andesite (Cooked up and/or brecciated up by intermediate-basic volcanics)

ALTERATION

12.88	44.32	31.44)
50.90	81.38	Moderate or strong PY-CB-Sericite alteration

MINERALIZATION

40.00	44.32	4.32 Shear zone, high carbonatized (?) whiteish grey color could be good gold (?) mineralization
57.84	59.10	1.26 Veins of GN, SP, CP, TT appearances, but very low recovery
12.19	12.19	Casing overburden should be less than 12 m
14.32	14.32	First footage mark
12.88	12.88	Measure back from 14.32 m
12.88	12.88	Start sampling
	12.88	12.88 32 cm recovered, 5 pieces altered and unaltered core 3-6 cm long
	31.39	31.39 NQ Core
31.39	111.86	80.47 BQ core
12.88	13.00	0.12 Minor limonite
12.88	18.72	5.84 Andesite breccia; altered light grey to pale grey 50% sheared, 20% gouge, contains 0.62 m QZ-CB vein section
12.88	14.32	1.44 Sheared, 60% gouge at 10 (?)
14.32	16.00	1.68 30% sheared at 10 & 45, 5% gouge 14.84-14.96 m: silicified, grey, upper contact 40 Lower contact 300
16.00	17.37	1.37 16-16.61 m: QZ-CB vein zone, 70% QZ-CB veins mainly at 45 16.06 m: 5 cm QZ-CB vein 30 16.24-16.45 cm QZ-CB vein upper contact at 43. Lower

		contact 317
17.37	18.72	1.35 Sheared at 55. Crumbly.
18.72	32.62	13.90 Andesite; altered, grey-pale grey
20.33	21.12	0.79 Andesite breccia
18.72	21.00	2.28 Minor QZ-pink CB veinlets at 19.85 m and 21 m
21.00	23.00	2.00 Few QZ-CB veinlets 2 mm at 10-40 21.2 m: QZ-CB vein 5 cm 35
23.00	25.00	2.00 23.98-24 m: sheared at 10 gougey some black mineral lenses 2 mm 10 24.54-24.68 m: 10% PY pervasive 24.55 m: 1 cm QZ-CB vein 45
25.00	27.00	2.00 26.32-27.15 m: sheared gougey 26.69-26.85 m: 5% maroon volcanics (?) associated with 5% PY
27.00	29.00	2.00 27.7 m: 4 cm gouge 45 28.05-28.18 m: sheared at 10
29.00	31.39	2.39 30.9 m: 5 cm sheared at 32
31.39	33.00	1.61 31.80-31.89 m: gougey, lost core here 32.1 m: 2 cm silicified vein at 35
33.00	35.00	2.00 10% sheared, local blackish mineral dissemination 33-33.1 m: shattered, some limonitic fractures
35.00	37.00	2.00 35.53-35.9 m: 5% maroon volcanics, weakly silicified 35.53-36.19 m: weakly sheared 36.22 m & 36.47 m: some QZ veinlets associated with PY 10-30
37.00	39.00	2.00 37-38 m: weakly silicified with some QZ veinlets 37.49 m: & 37.8 m: high PY spots 38.3 m: 12 mm QZ-CB vein 25, trace SP
32.62	35.50	2.88 Lapilli (possible marker horizon - correlate with 89-7)
35.50	44.32	8.82 Andesite breccia: altered, grey-pale grey
39.00	41.00	2.00 40% sheared 0-10, 20% gouge
40.25	44.32	4.07 Shear zone, white, grey highly carbonatized but no distinct veining sheared at 1-10
41.00	43.00	2.00 90% sheared, 10% gouge, trace SP
43.00	44.32	1.32 80% sheared 43.18 m: QZ-CB vein 8 mm 45 43.32-43.47 m: moderate silicified with QZ-CB lens and PY 44.2-44.1 m: QZ-CB vein with 20% PY upper contact 45, lower contact 20
44.32	57.30	12.98 Andesite; weak altered, pale green minor grey clasts (argillite ?) 50.9- : grey color
44.32	46.00	1.68 45-45.7 m: slightly sheared 45.3 m: few blebs of SP with QZ-CB veinlet 45.69 m: 3 mm QZ-CB veinlet 43 with SP
46.00	48.00	2.00 1% grey argillaceous clasts < 1 cm 46.82 m: minor SP in 1 mm QZ-CB veinlet 45
48.00	50.90	2.90 50.22-50.9 m: slightly sheared 50.22 m: 8 mm calcite rhodochrosite vein 45 50.48-50.75 m: gouge at 40
50.90	53.00	2.10 50.9-51.08 m: slightly sheared, trace SP with calcite veinlet 51.47-51.61 m: sheared at 45
53.00	55.00	2.00 One 90 fracture
55.00	56.72	1.72 55.52-55.63 m: bleached, with some PY and grey bandings 45
55.73	57.30	1.57 Prophyritic andesite
57.30	68.63	11.33 Andesite breccia
56.72	57.84	1.12 57.26 m: gouge 1.5 cm 75

		57.51-57.84 m: shattered
57.84	58.88	1.04 Very low recovery; shattered, rubble size 1-4 cm QZ-CB veins associated with massive GN-SP some CP, TT
58.88	59.10	0.22 QZ vein: lower contact = 10, upper contact not clear with a 3 mm QZ-CB veinlet and PY bands at 47, 2.5% SP some GN, CP, TT
59.10	60.00	0.90 20% clasts
60.00	62.00	2.00 60.4-61.6 m: fracture with 3 mm QZ vein , 90 minor blackening mineral in locals 40% clasts, 60% matrix
62.00	64.00	2.00 62.68 m: QZ-CB vein 1 cm, 65 with PY 50% matrix
64.00	66.00	2.00 30% clasts, few pale maroon and grey clasts
66.00	68.00	2.00 10% slightly sheared, 30% pale whiteish clasts
68.00	70.00	2.00 60% sheared section, 5% gouge, sheared at 40-45 68.21 m: QZ-CB vein 1.5 cm 45 69-70 m: strongly sheared
69.00	87.00	18.00 Broken up, 50% sheared, 30% shattered, 20% gouge
68.63	74.20	5.57 Andesite, local clasts
70.00	74.00	4.00 70% sheared, 20% shattered, 5% gouge
72.00	74.00	2.00 30% sheared, 5% gouge 73.66 m: some SP along fracture 50 73.42-73.66 m: three QZ veins 1 cm at 50, 70, 45
74.00	76.00	2.00 30% sheared, 5% gouge
74.20	82.34	8.14 Andesite breccia
76.00	78.00	2.00 90% sheared at 60, 80, 30% gouge 77.9 m: 15 mm QZ vein at 77
78.00	81.38	3.38 79.68-80.2 m: mud, grey 78-79.15 m: 30% shattered
81.38	84.00	2.62 20% sheared sections at 10-40, 5% gouge
82.34	85.11	2.77 Andesite; pale green
85.11	86.86	1.75 Latite: brownish, upper contact = 45 (?)
84.20	84.20	Major CB-PY-Sericite altered zone end
84.00	86.86	2.86 85-86.86 m: 30% gouge at 45
86.86	91.38	4.52 Andesite strongly cooked up and/or brecciated up by dark grey intermediate-basic volcanics
86.86	89.00	2.14 PY flooded with some calcite veinlets and blebs
89.00	91.00	2.00 QZ-CB veinlet network 1 mm- 3 mm. PY occurred as above
91.00	93.00	2.00 92.52-93 m: 5% QZ-CB veinlets (1-3 mm) with minor PY
91.38	92.54	1.16 Andesitic Intrusion Pale slightly cooked by the dark grey intermediate-basic volcanics, with 20% pale to prey phenocryst flakes (altered mafic minerals) as in Hole 89-2 to 5. Lower contact =75
92.54	92.84	0.30 Pale lava (?)
92.84	111.86	19.02 Andesite; cooked up and/or brecciated up by the dark grey intermediate-basic volcanics
93.00	96.00	3.00 93.66-94.15 m: fracture 90 with 2mm QZ veinlet
96.00	96.00	
96.00	99.00	3.00 96.8 m: two QZ-CB veins, 8 mm at 43 96.7-96.95 m: sheared at 45 gougey 97.12 m: 3 cm gouge 50 97.52-97.58 m: QZ vein, upper contact 43 Lower contact 40 97.59-97.74 m: gouge
99.00	102.00	3.00 100.53 m: QZ vein 16 mm 10

100.9-101.57 m: slightly bleached & weakly sheared with
QZ-CB veinlets

102.00 105.00 3.00 Few CB veinlets 1 mm at 75

105.00 108.81 3.81 105.37 m: QZ vein 2 cm, 63 with PY
105.34-105.8 m: slightly bleached
108.67-108.81 m: shattered grits, washed away gouge (?)
low recovery

108.81 111.86 3.05 111.70-111.85 m: rubbles (shattered)

Property Name:	HANK	Client Name:	LAC MINERALS LTD.
Hole No:	89-DDH-07	Azimuth:	320
Northing:	10573.316	Dip:	-70
Easting:	10073.404	Length:	101.20 m
Elevation:	1103.950m		
		Borehole Test Method:	None
		Test Azimuth:	
		Test Dip:	
		Test Depth:	
		Core Size:	NQ & BQ
		Date Started:	August 25, 1989
		Date Completed:	August 27, 1989

LITHOLOGY

FROM	TO	WIDTH (m)
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10.32	21.69	11.37 Andesite breccia
21.69	35.28	13.59 Andesite
35.28	38.06	2.78 Lapilli
38.06	51.40	13.34 Andesite
51.40	101.20	49.80 Andesite breccia

ALTERATION

10.32	51.40	41.08)
75.00	101.20	26.20 (are the moderate high PY-CB-Sericite alteration zone

MINERALIZATION

46.91	47.81	0.90)
88.35	88.75)Two small sections with good SP, GN, CP, TT, associated with QZ-CB veins

1.00	9.14	8.14 Casing. Overburden should be than 9 m.
11.28		11.28 First footage mark
10.32		10.32 Measured back from 11.28 m
	31.39	31.39 NQ core
31.39	101.20	59.81 BQ core
	10.32	10.32 19 cm recovery, 7 pieces

No distinct limonite zone in core

10.32	21.69	11.37 Andesite breccia, grey altered
12.16	20.02	7.86 Shear zone
10.32	12.16	1.84 10.32-11.18 m: silicified 10.53-10.70 m: sheared and shattered 11.25-11.5 m: sheared at 40 12-12.16 m: bleached
12.16	12.84	0.68 Gouge at 7 to Core Axis 0.00 12.75 m: 6 mm SP, GN, CP vein with QZ-CB lens at 45
12.84	13.84	1.00 13-13.54 m: 50% sheared, gougey
13.84	15.00	1.16 50% sheared at 10-40 Minor SP with CB in gouge
15.00	17.00	2.00 BQ% sheared, 50% gouge 16.58-16.65 m: silicified
17.00	19.00	2.00 BQ% sheared, 70% gouge One QZ-CB lens 6 mm, 58%
19.00	20.02	1.02 19.06-19.15 m: grey seam sheared at 50 19.43 m: sheared at 78 with CB vein 4 mm 19.81 m: sheared at 45

20.02	21.69	1.67 Moderate silicified 20.23-20.52 m: a irregular PY vein 3-10 mm = 80 21.36 m: 12 mm QZ-CB vein at 45
21.69	35.28	13.59 Andesite; pale grey
21.69	23.78	2.09 Bleached 23.22-23.46 m: cooked up with 50% maroon volcanics 23.52-23.69 m: maroon volcanics, contact = 60
23.78	24.50	0.72 Bleached with QZ vein intrusion 23.78-23.88 m: QZ vein, barren 23.88-24.53 m: 80% silicified with QZ veinlets
24.53	26.52	1.99 24.53-24.91 m: cooked up with 60% maroon volcanics 25.18 m: 4 cm gouge at 70 25.28 m: 2.5 cm QZ-CB vein 45
26.52	27.52	1.00 20% maroon volcanics Two QZ-CB veinlets 2 mm, 10, 45 with PY-SP
27.52	29.56	2.04 27.52-28.15 m: 20% maroon volcanics
29.56	31.39	1.83 Few QZ-CB veinlets 1 mm associated with high PY at 5 & 45
31.39	33.48	2.09 31.73-33.14 m: 40% maroon volcanics, some QZ veinlets 4 mm at 80 and 45
33.48	34.23	0.75 2.5% blackish mineral dissemination Two calcite vein 6 mm & 18 mm, 45 trace SP
34.23	35.28	1.05 Weakly sheared, 5% maroon volcanics
35.28	38.06	2.78 Lapilli Mainly white (90%) clasts and some grey (10%) clasts 1-20 mm in diameter angular to subround, some shards, clasts orientation at 45 (bedding) Upper contact = 30, Lower contact = 32 36.7 m: some rhodochrosite
38.06	51.40	13.34 Andesite; pale grey - whiteish grey
38.06	39.31	1.25 38.06-38.14 m: silicified at 35 and 325 38.14-38.46 m: gouge 38.46-39.31 m: cooked up with 50% maroon volcanics Some gouge at 10 39.22 m: QZ-CB vein 4 cm 27
39.31	41.57	2.26 Strong carbonatization and weak silicification 20% weakly sheared sections at 45, one at 90 39.35 & 34.37 m: 1 cm thick QZ vein 10 39.57 m: 2 cm QZ vein at 20, trace SP 39.85-41.57 m QZ vein network 2-6 mm
41.57	43.00	1.43 Few QZ & QZ-CB veinlets 1-3 mm at 40, 45, 60
43.00	45.00	2.00 44.04-45.54 m: sheared at 40 44.9-45 m: shattered
45.00	46.91	1.91 Sheared, 20% gouge mainly at 30-45
46.91	47.56	0.65 46.91-47.19 m: slightly silicified 47.20-47.4 m: calcite vein at 43, barren 47.4-47.47 m: slightly silicified
47.56	47.81	0.25 10% SP zone GN, CP, TT massive veinlet at 47.62-47.69 m, 47 47.85 m: 4 mm calcite vein, 60 with some above sulphides
47.87	48.84	0.97 40% sheared and shattered, 2.5% gouge
48.84	51.40	2.56 49.18-49.29 m: gouge at 45 50-50.7 m: broken along fractures 90 and 45 51-51.4 m: gouge
51.40	76.00	24.60 Andesite breccia; weak altered pale to light green clast in pale maroon-grey matrix
51.40	54.00	2.60 Bright greenish chloritized mafic minerals in clasts

			2.5% matrix
			53.8-54 m: some pyritic amygdales
54.00	56.00	2.00	54-54.6 m: some amygdale filled with PY-CB-QZ 55.76-56.1 m: sheared and shattered
56.00	58.00	2.00	40% pale maroon-grey matrix
58.00	60.00	2.00	70% matrix
60.00	63.00	3.00	60.04-60.38 m: ash (?) 60.38-61.38 m: sheared at 70 61.38-63 m: 40% maroon volcanics
63.00	66.00	3.00	40% matrix 63.26-64.67 m: sheared and shattered at 33
66.00	69.00	3.00	30% matrix 66.78-67.13 m: sheared at 10, gougey 68-69 m: some bright green clasts
69.00	72.00	3.00	69-69.2 m: some baren QZ-CB veinlets 2-10 mm 45
72.00	75.00	3.00	73.58-74 m: sheared 74.15 m: baren QZ-CB vein 12 mm 60 72-73.3 m: some bright green clasts (highly chloritized)
75.00	77.00	2.00	76 m: 1 cm QZ-CB vein 45
77.00	79.00	2.00	30% matrix
79.00	80.00	1.00	40% matrix. Some QZ-CB veinlets 2 mm 45-65
80.00	81.38	1.38	Sheared, 5% gouge 80 m: gouge 4 cm at 40
81.38	84.10	2.72	81.74-84.1 m: sheared at 35, 10% gouge 82.26-82.31 m: 2 mm QZ-CB vein with SP at 75
84.10	86.16	2.06	84.1-84.43 m: sheared, 5% gouge 84.93-85.70 m: some QZ veinlets 1 mm 85.70-85.80 m: PY veinlet 1 mm Pocket of PY 1 cm 85.80-86.16 m: QZ-CB veinlets at 50-70, 2 mm
86.16	87.47	1.31	Less altered QZ-CB veinlets < 1 mm 86.34-86.74 m: SP veinlets (with QZ-CB) 1 mm @ 45
87.47	88.36	0.89	PY less disseminated more concentrated 87.47-88.04 m: some QZ-CB veinlets Few PY rich veinlets < 1 mm @ 25-35 Few SP-PY rich veinlets < 1-3 mm @ 20, 50 & 310
88.36	88.75	0.39	QZ-CB veinlets < 1 mm - 2 cm 88.42-88.48 m: PY-SP rich veinlets @ 25 & 70 PY = 2.5% SP = 5% 88.62-88.75 m: SP - rich veinlets @ 55 SP = 5% GM = 0.3%
88.75	90.52	1.77	88.75-89.10 m: veinlet of SP & PY < 1 mm @ 85 SP = 1% PY = 0.3% 89.10-89.45 : bleached and altered zones QZ-CB veinlets < 1 mm - 2 mm 89.45 - 90.17: QZ-CB veinlets < 1-2 mm @ 310, 330, 10 90.17-90.52: many QZ-CB veinlets < 1-2 mm some SP & PY rich < 1 m @ 280, 320 highly altered
90.52	92.54	2.02	90.52-91.18: veinlets of PY < 1 mm @ 310, 40 91.18-92.54: 10% pale clasts Few QZ-CB & 1 mm @ 70 Few PY veinlets < 1 mm @ 310, 90, 70
92.54	93.57	1.03	20% pale clasts

92.78-93.20: gouge
93.57 95.28 1.71 93.57-94.17: pale clasts 20%
94.17-94.41: bleached QZ-CB veinlet 3 mm
(broken section)
94.41-95.10: pale clasts 10%
QZ-CB veinlets 2 mm @ 45, 60, PY = 2.5%
95.10-95.28: shear & QZ-CB veinlet @ 310,
veinlet SP = 1%
95.28 96.23 0.95 Gouge, shear
QZ-CB veinlet 2 mm (broken up)
96.23 98.00 1.77 96.62-97 m: fractures 85, 50% sheared and 30% shattered
97.36 m: QZ-CB lens 8 mm, 80
97.82 m: QZ-CB veinlets 2 mm 80 with minor PY
99.00 99.66 1.66 30% sheared at 30-45, 60, 2.5% gouge
99.66 101.20 1.54 100.38-101.10 m: shattered
101.20 101.20 Binding rods, Try to go down for 13 hours but couldn't
make it. Finally lost 14 rods and a core barrel

HI-TEC RESOURCE MANAGEMENT LTD.

DIAMOND DRILL LOG

Property Name:	HANK	Client Name:	LAC MINERALS LTD.
Hole No:	89-DDH-08	Borehole Test Method:	None
		Test Azimuth:	333.5 (?)
Northing:	10454.401	Dip:	-55
Easting:	10037.800	Test Dip:	-58
Elevation:	1114.040m	Length:	233.77 m
		Test Depth:	233.25 m
Date Started: August 27, 1989			
Date Completed: August 30, 1989			

LITHOLOGY:

FROM	TO	WIDTH (m)	LITHOLOGY
26.52	55.38	28.86	Andesite
55.38	61.83	6.45	Andesite breccia
61.83	66.85	5.02	Andesite
66.85	69.76	2.91	Tuff (= 65)
69.76	72.50	2.74	Andesite
72.50	81.50	9.00	Andesite breccia
81.50	84.77	3.27	Andesite
84.77	139.22	54.45	Andesite breccia
139.22	147.25	8.03	Andesite
147.25	151.29	4.04	Andesite dyke ? or sill
151.29	157.62	6.33	Andesite
157.62	163.75	6.13	Andesite breccia
163.75	194.15	30.40	Andesite
194.15	221.63	27.48	Clastic andesite
221.63	224.07	2.44	Andesite
224.07	233.77	9.70	Clastic andesite

ALTERATION:

26.52	145.00	118.48	}
151.29	193.84	42.55) Moderate or strong PY-CB-Sericite alteration

MINERALIZATION

53.33	53.77	0.44	QZ-CB veins associated with SP, GN, TT, CP
84.77	86.31	1.54	Shear zone, QZ-CB veins associated with SP, GN, CP
92.64	93.17	0.53	QZ-CB veins with SP, GN
	18.29	18.29	Casing
26.52	26.52	5.18	m core recovered
61.87	61.87	NQ core	
61.87	233.77	171.90	BB core
26.52	40.00	13.48	Limonite existent. (33-40 m minor limonite)
20.42		20.42	First footage mark
26.52	55.38	28.86	Andesite; altered grey locally, intruded or cooked by maroon volcanics, silicious
26.52	38.28	11.76	Shear zone
26.52	29.56	3.04	Sheared and shattered, 20% gouge low recovery, limonite gouge and fracture, shattered
29.56	32.61	3.05	Sheared, 30% shattered, 30% gouge One 1 cm QZ-CB spot with GN 31.7: 2 cm QZ vein 48 Minor maroon volcanics, limonite as above
32.61	35.66	3.05	32.61-33.4 m: sheared and shattered, limonitic 33.4-34.9 m: solid andesite, brecciated by 5%

maroon volcanics, silicious
 34.9-35.66 m: gouge
 35.66 38.71 3.05 20% gouge
 38.25-38.71 m: few maroon volcanic veinlets 1 mm 5, 38
 38.71 41.00 2.29 40% sheared sections, 5% gouge
 40.38-41.10 m: maroon volcanics veins,
 Upper contact = 45, lower contact = 85
 41.00 43.00 2.00 41.34 m: gouge 4 cm at 60
 5% maroon silicious volcanics
 43.00 45.00 2.00 20% sheared at 40, 60, 10% gouge 2.5% maroon volcanics
 44.35-45.2 m: 1% hematitic - pyritic altered mafic minerals
 45.00 47.00 2.00 5% maroon silicious volcanics cooked up and some
 veinlets 1 mm at 40
 46 m: 2 mm QZ-CB vein barren at 60 to Core axis
 46.64-47 m: sheared at 60
 47.00 48.76 1.76 70% of section cooked with maroon volcanics
 48.76 62.36 13.60 Shear zone.
 48.76 50.76 2.00 Sheared, 20% gouge, high angles & low angles whiteish
 color
 50.76 51.76 1.00 70% gouge
 51.76 53.33 1.57 30% sheared at 40, 10% gouge
 50% sections cooked up with maroon volcanics
 53.33 53.77 0.44 2.5% SP, with some CP, TT, GN associated with a 3 mm
 QZ-CB vein 72, 5 brench QZ-CB veinlets 3 mm at 8
 53.77 55.48 1.71 Sheared, very low recovery
 55.39 61.83 6.45 Andesite breccia. Lower contact = 63
 55.48 56.68 1.20 55.48-56.27 = 60% silicified
 55.48-55.54 m: 3 cm QZ vein at 48
 55.86-55.99 m: irregular QZ vein roughly 30
 56.27-56.66 m: sheared at 25, 80% gouge
 56.66 57.67 1.01 56.77-56.83 m: gouge 65
 56.83-56.99 m: QZ-CB vein at 70 contacts, baven
 56.99-57.67 m: silicified, slightly sheared
 57.67 60.04 2.37 Moderate sheared at 70, 45, crumbly
 60.04 61.87 1.83 Weakly sheared, 60% crumbly sections
 61.87 64.00 2.13 61.87-62.4 m: shear fractures 85-90
 64.00 66.00 2.00 Few QZ veinlets at 45 1-5 mm
 61.83 66.85 5.02 Andesite
 66.00 68.00 2.00 66.85-68 m: some strong carbonate altered banding and
 beddings at 50
 66.85 69.76 2.91 Tuff (ash)
 Upper contact = 65, lower contact not clear
 cooked up by maroon volcanics and calcite veins pale
 green grey - highly sericitized
 68.00 70.00 2.00 69.19-70.4 m: 80% cooked up with maroon volcanics
 68-68.2 m and 69-16.19 m: shattered
 68.82 m: QZ-CB vein 2 cm 47, trace SP
 69.76 72.50 2.74 Andesite; pale greenish grey (highly sericitized)
 70.00 72.00 2.00 30% cooked with maroon volcanics
 Some QZ-CB veinlets 2-9 mm, 20-35
 72.00 73.11 1.11 72.49-72.82 m: silicified
 72.42 m: gouge 2 cm at 85
 72.61 m: one QZ feldspar spot 2 cm in diameter
 white & brown
 72.50 81.50 9.00 Andesite breccia; pale grey
 72.36 76.63 4.27 Shear zone

73.11	73.80	0.69	80% silicified with 1/2% SP concentrated at QZ vein (irregular 1-3 mm)
		73.31	m: upper contact of silicification at 45
		73.75	m: lower contact = 60
73.80	75.29	1.49	Gouge
75.29	76.63	1.34	Sheared, 60% gouge 75.9 m: 2-3 mm calcite/rhodochrosite vein 80
76.63	78.00	1.37	Clasts are faded Some sheared fractures at 30 and 45
78.00	80.00	2.00	Weakly sheared at 30
80.00	82.00	2.00	81.3-82 m: sheared at 45, some calcite veinlets 2-3 mm at 45
81.50	84.77	3.27	Andesite; pale grey
82.00	84.00	2.00	82-82.7 m: slightly sheared at 30 and 60, some gouge 83.47 m: 1.5 cm QZ-CB lens 8
84.00	84.77	0.77	Whiteish color, few shear fractures at 80, 30, 40
84.77	86.31	1.54	Shear zone with QZ-CB veins, SP, GN
84.77	85.46	0.69	Sheared 85.07-85.47 m: gouge, upper contact at 42 = lower contact Trace SP
85.46	86.07	0.61	Brecciated and weakly silicified with QZ vein 85.47-85.56 m: carbonatized and weakly silicified at 30, some SP 85.56-85.63: dark grey matrix with 10% clasts and some GN, PY at 30 85.67-77 m: QZ vein at 30, minor PY 85.77-86.07 m: grey matrix with 80% small clasts (5 mm), minor CP
86.07	86.31	0.24	5% SP, some GN 86.17-86.28 m: QZ-CB vein 30 with SP, PY, GN
84.77	139.22	54.45	Andesite breccia
86.31	87.16	0.85	Some maroon carbonate (siderite ?) or PY rims around some of the clasts Few fractures 60, 80
87.16	88.03	0.87	80% clast, very pale green, highly sericitized and carbonatized, 20% greyish matrix
88.03	90.00	1.97	Clast as above 88.03-88.57 m: weakly sheared at 30, 45
89.84	90.30	0.46	Dyke of latite (?) contacts at 38, very fine grain 0.00 brown & greyish
90.00	92.64	2.64	Only 10% matrix 90.98-91.08 m: sheared at 10 92.34-92.45 m: sheared at 20, 40 gougey
92.64	93.17	0.53	1% SP, some GN 92.82 m: QZ-CB veinlet 3 mm, 53 with SP, GN 92.85 and 92.89 m: 1 mm QZ-CB vein 45 & 10 with SP 92.95 m: QZ-CB vein 1 cm, 43 with SP, GN 93.2 and 93.15 m: some PY lenses, 5 mm and 10 mm thick
93.17	95.00	1.83	Weakly sheared, minor SP at some shear fracture 94.55 m: QZ-CB veinlet 3 mm at 0 with SP 94.64-94.71 m: some irregular QZ-CB spots and veinlets
95.00	97.00	2.00	Very pale greenish grey soft altered clasts-sericite, carbonate & talc (?) alteration intensity is 4-5
97.00	99.00	2.00	As above

99.00	101.00	2.00 As above
101.00	103.00	2.00 As above
103.00	105.00	2.00 As above, but only 20% clasts
105.00	107.00	2.00 As above
107.00	109.00	2.00 50% clasts as above 107.6 m: 2 cm gouge
109.00	111.00	2.00 As above, 40% clast
111.00	113.00	2.00 111.74-112 m: sheared, gougey
113.00	115.00	2.00 20% weakly sheared sections at 40, 70 113.16-113.26 m: 50% gouge at 40
115.00	117.00	2.00 20% clasts, 10% sheared sections, some gougey fractures at 20, 60
117.00	119.00	2.00 20% clasts as above, 20% sheared sections 10, 45, 5% gouge
119.00	121.00	2.00 119.08-119.73 m: gouge. Some shear fractures 50, 60 0.00 120.47 m: 6 mm QZ vein, 45 some PY 0.00 120.78 m: 2 cm QZ lens at 10 0.00 120.66 m: two grey clasts (argillite ?)
121.00	122.81	1.81 Grey plus pale green sections 121.23-122.06 m: Few QZ veinlets 2-5 mm at 20-40 122.30 m: QZ vein 2 cm, 10
122.81	124.05	1.24 Pale green. Some QZ veinlets 3-10 mm at 10, 30, 60
124.05	126.00	1.95 124.09-124.38 m: QZ vein 43 with 0.3% PY 124.38-125 m: 70% sheared, at 30, 45, gougey 125.92-126.06 m: gouge
126.00	126.74	0.74 126.08-126.74 m: Intruded and brecciated up with QZ-CB veins contact angles are not clear because of shattered contacts. This section consists of three major veins, 4 cm thick at 25 and some other irregular veins
126.74	129.00	2.26 127.21-127.52 m: some maroon matrix Whiteish clasts 30%, pale grey and pale maroon matrix
129.00	131.00	2.00 70% whiteish clasts, 30% pale maroon, grey matrix
131.00	133.00	2.00 As above
133.00	135.00	2.00 As above
135.00	137.00	2.00 40% clasts
137.00	139.00	2.00 137.94-138.21 m: some low angle PY-QZ veinlets at 65-80, 2-3 mm, some irregular lenses, 1-2 cm
139.22	147.25	8.03 Andesite; altered, pale color, massive
139.00	141.00	2.00 No comment
141.00	143.00	2.00 141.38 and 141.44 m: PY-QZ veinlets 4 mm & 2 mm are at 60 142.86-143: sheared and shattered at 75
143.00	145.00	2.00 Few QZ-PY veinlets 2 mm - 3 mm, 70-90
145.00	147.25	2.25 Gradually changed to unaltered section of andesite Few 1 cm thick calcite veins, 20-30 146.87-147.05 m: some maroon bandings at 38
147.25	151.29	4.04 Andesite (dyke or sill) Fine grains, dark green, massive, magnetic, both contact are 42. The contacts show gradually changing because of cool up.
147.25	149.26	2.01 Dark greyish green
149.26	151.29	2.03 As above. Some calcite and QZ-CB veinlets 0.5-4 mm mainly 30-45
151.29	157.62	6.33 Andesite (?); altered, pale color, maroon banding in locals
151.29	153.00	1.71 151.85-152.07 m: sheared and shattered 151.29-151.9 m: alteration intensity is 4 152.07-153.2 m: some maroon bandings and fracturings
153.00	155.00	2.00 Rich PY fracture fillings and dissemination

155.00 157.00 2.00 156.6 m: 4 cm PY/silicious bandings at 34
 157.26-157.42 m: broken up along high angle fracture
 157.47 and 157.555 m: 1 cm QZ-CB veins at 47
 157.00 159.00 2.00 157-159.39 m: = shattered
 158.68 and 158.89 m: some PY and maroon bandings at 28
 157.62 163.75 6.13 Andesite breccia; pale color
 157.67 Mis latch
 159.00 161.00 2.00 160.21-161 m: PY is very fine disseminated
 161.00 163.00 2.00 Pale green
 163.00 165.57 2.57 163.34-163.78 m: shear fracture 80-90, 10% PY minor
 blackish mineral, 2 mm calcite veinlet
 165.15-165.26 m: and 165.5-165.58 m: shattered
 168.28-168.47 m: 5% maroon banding 45, 80
 163.75 194.15 30.40 Andesite; mainly altered, grey but
 165.57-168 m: green, weakly altered
 176-183 m: pale greenish grey
 165.57 167.94 2.37 Green, local magnetic
 167.48-167.61 m: sheared and shattered, gouges
 167.94 169.00 1.06 Cooked up with 10% maroon volcanics
 169.00 171.00 2.00 Sheared, some fracture at 45, 90, 50%
 171.00 173.00 2.00 5% maroon bandings at 10
 Some QZ-CB and calcite veinlet at 80
 172.97 m: 2 cm gouge at 12.
 173.00 176.00 3.00 173.1-174.47 m: sheared at 55, with calcite and PY veinlets
 Few QZ-CB veinlets 2-8 mm 20-32
 176.00 179.00 3.00 Pale greenish grey
 176.16 m: 5 mm gouge at 0
 176.88 m: 2 cm QZ-CB vein 45 with some PY
 177.21 m: sheared at 65
 177.35 m: QZ vein 2 mm 60, rich PY
 179.00 182.00 3.00 Pale greenish grey as above
 180.1-180.43 m: slightly sheared at 75
 182.00 184.00 2.00 As above. Few QZ veins and QZ-CB veins 1-3 mm at 30, 60
 184.00 185.85 1.85 Pale greyish color
 185.85 186.37 0.52 Weakly silicified with QZ veinlet 1 mm-15 mm mainly
 at 40 and 32
 186.37 188.24 1.87 Pale grey. Few QZ-CB veinlets 1 mm 30, 45
 188.24 190.00 1.76 Few QZ-CB veinlets 25, 42
 Four PY-CB veinlets 1-2 mm, 45, one at 75
 188.24-189.30 m: grey
 189.30-190 m: pale greenish grey, slightly bleached
 190.00 191.32 1.32 Slightly bleached
 190.21 m: QZ-CB vein >4 mm, 87 with trace SP, GN
 190.59-190.72 m: QZ silicified vein, 10% PY
 at 40 and 320 contacts
 191.32 191.93 0.61 Moderately silicified by QZ veinlet network contacts
 are at 75
 191.93 193.84 1.91 Bleached. Pale grey, local PY spots up to 3 cm and
 veins, 3 mm thick
 192.94-193.21 m: weakly silicified and brecciated
 dark grey contacts at 15.
 193.21-193.84 m: sheared at 75
 194.15 221.63 27.48 Clastic andesite weakly altered. Pale to light green
 andesitic clast in pale grey intermediate (andesitic
 also ?) matrix, this rock type R. Turna used to call it
 agglomerate, York called it clastic andesite

in 1988. Since the clasts were unique and brecciated from the interbedded andesite could be subvolcanic formation or intrusive.

193.84	196.14	2.30 Pale green, 50% sheared, 1% blackish mineral 194-194.3 m: shattered 195.25-196.12 m: sheared at 90, gougey shattered, rich PY
196.14	198.00	1.86 Bleached, pale grey, 30% sheared and shattered
198.00	201.00	3.00 20% clast 198.34m: 8 mm QZ-CB vein at 30 200-200.24 m: shattered
201.00	203.00	2.00 20% clasts, major PY in the blebs, altered in clasts
203.00	206.00	3.00 10% shattered in locals 20% green clast
206.00	209.00	3.00 20% green clast 206.73 m: 8 cm altered section, with PY and 5% carbonate, dark grey at 30 207.85-209.35 m: 5% CB veinlets 1-8 mm at 45-50
209.00	210.97	1.97 A shear fracture 95 with QZ-CB vein 5 mm
210.97	214.00	3.03 40% light green andesitic clasts
214.00	217.00	3.00 20% clast as above
217.00	220.00	3.00 20% clast as above 219-220 m: 5% QZ vein 2-8 mm at 0, 45
221.63	224.07	2.44 Andesite; light green, weakly altered with some yellowish disseminated carbonate, upper contact = 8, lower contact = 5
220.00	223.00	3.00 No comment
223.00	226.00	3.00 224.31-224.37 m: sheared at 45 with 5 mm QZ-CB vein 90% clast
224.07	233.77	9.70 Clastic andesite as above
226.00	228.65	2.65 10% clast 227 m: 10 cm sheared at 70
228.65	229.48	0.83 228.65 m: sheared at 50 gouge 1 cm 228.76-228.36 m: silicified with QZ veins contacts are 40
229.48	231.76	2.28 20% clast
231.76	233.77	2.01 20% clast 233.49-233.63 m: 10% blackish disseminated mineral

Property Name:	HANK	Client Name:	LAC MINERALS LTD.	Borehole Test Method:	Tropari
Hole No:	89-DDH-09	Azimuth:	316.5	Test Azimuth:	Failed
Northing:	11017.406	Dip:	-62	Test Dip:	Failed
Easting:	10434.765			Date Started:	August 31, 1989
Elevation:	1124.170m	Length:	270.36 m	Test Depth:	
				Date Completed:	September 3, 1989

LITHOLOGY

FROM TO WIDTH (m)

5.18	21.16	15.98	Andesite (green)
21.16	24.47	3.31	Andesite & unaltered intrusive Dyke (?)
24.47	26.75	2.28	PPAN
26.75	61.23	34.48	Andesite breccia
61.23	64.24	3.01	PPAN
64.24	128.88	64.64	Andesite breccia
128.88	136.00	7.12	Andesite
136.00	137.75	1.75	Andesite breccia
137.25	153.55	16.30	Andesite
153.55	216.46	62.91	Andesite breccia
216.46	221.85	5.39	Intermediate subvolcanics
221.85	270.36	48.51	Clastic andesite

ALTERATION

5.18	246.37	241.19	Weak PY-CB-Sericite alteration
246.37	270.36	23.99	Strong PY-CB-Sericite alteration

MINERALIZATION

Most of the andesite breccia (with greenish andesitic clasts) zones are with 2.5% PY

255.11	269.74	14.63	OZ-CB vein zone
259.00	264.00	5.00	Major SP, GN appearances
1.00	4.57	3.57	Casing
	31.39	31.39	NQ core
31.39	270.36	238.97	BQ core
5.18		5.18	First footage mark
4.57	5.18	0.61	0.64 m: dark greenish grey clastic tuff
4.57	10.00	5.43	Minor limonite on fracture surfaces
5.18	21.16	15.98	Andesite; pale greenish color in general, with about 20-40% pale to light greenish sericite-carbonate and pyrite replacement of the mafic (?) minerals 1-2 mm in diameter. Matrix is also pale green but whiteish grey in locals. Minor small clasts-green or grey in parts. Alteration intensity is between 4 to 5
5.18	7.00	1.82	5.18-5.84 m: silicified, some high angle fractures
7.00	9.00	2.00	Few argillite (?) clasts 0.5-1 cm
9.00	11.00	2.00	As above.
11.00	13.00	2.00	As above.
13.00	15.00	2.00	10% sheared actions at 30, 5% gouge 14.62 m: 3 mm CB veinlet 41 with SP, GN
15.00	17.00	2.00	16.92-17.07 m: weakly silicified at 40 17 m: a pale green-carbonate vein 12 mm at 75 rich

chlorite

17.00 19.00 2.00 30% moderately sheared sections, 30-45, 2.5% gouge
 19.00 21.00 2.00 19.38-19.48 m: bleached, with 3 mm QZ-CB vein at 45
 21.16 24.47 3.31 Andesite; cooked and brecciated up by 10-20% of the dark brownish grey (fresh) andesite dyke.
 21.00 23.00 2.00 21.52-23.3 m: greenish and pale maroon
 23.00 24.47 1.47 Pale green
 23.15-23.47 m: sheared at 47, gougey
 24.06 m: some SP with 2 mm calcite veinlet 38
 24.47 26.75 2.28 Dark brownish grey andesite, magnetic, very fine grain, but has 0.3-1% local phenocrysts of mafic mineral (pseudomorphed by biotite) 1-3 mm, so its porphyritic texture in parts. This could be the undifferentiated PPAN
 Upper contact = 10. Lower contact = 80
 24.47-26.1 m: pale to light green-maroon, 5% clast
 26.01-26.5 m: dark brownish grey magnetic unaltered.
 26.75 28.76 2.01 Breccia; 10% andesitic clasts brecciated with the above maroon-grey matrix, 1% 1-3 mm mafic mineral phenocrysts
 28.76 31.23 32.47 Andesite breccia; pale grey, very pale green or whiteish clasts in pale maroon-grey or grey matrix. Alteration intensity is between 4 & 5
 28.76 30.00 1.24 29.28 m: QZ vein 1 cm 45 with PY
 30.00 31.39 1.39 30.11-20.30 m: Irregular 1 cm QZ vein = 70, minor PY
 31.39 33.00 1.61 Few fracture, 65-75
 33.00 35.00 2.00 20% greenish clasts
 33.82-33.94 m: 20% calcite veinlets 2-4 mm with some SP.
 One calcite lens 2.5 cm thick
 35.00 37.00 2.00 60% clasts
 36.4-36.76 m: sheared 20, 40
 36.4 m: some SP, GN at 1 cm shear fracture 20
 37.00 39.00 2.00 37.3 m: 5 mm gouge 4
 60% clasts as above.
 39.00 41.00 2.00 50% clast. Few QZ-CB veinlets 1-2 mm
 41.00 43.00 2.00 60% clast
 43.00 45.00 2.00 44.03-44.17 m: weakly silicified with QZ vein 1 cm at 38. Silicified section contacts are 32. Some SP, GN associated with QZ vein
 44.95 m: 1 mm QZ-CB veinlet 40 with GN
 45.00 47.00 2.00 70% clast
 47.00 49.00 2.00 40% clast
 47.58 m: 5 cm sheared at 45
 47.5-47.68 m: silicified, 45, with minor SP at tiny QZ-CB vein 1/2 mm.
 47.74-47.78 m: some SP in QZ-CB spots 1 cm
 48.71 m: 3 mm QZ-CB veinlets 47 with CP
 49.00 51.00 2.00 30% clast
 49 at: 12 mm gouge at 7
 49.53 m: 1.5 cm QZ-CB vein 42 with some PY
 50.52 m: 4 cm sheared and shattered
 51.00 53.00 2.00 51.33 m: 1 cm rhodochrosite lens
 51.98 m: 1 mm CB veinlet with minor SP
 52.16-52.42 m: Sheared at 37, 50% gouge
 53.00 55.00 2.00 60% clast
 54.56-54.53 m: sheared gougey
 55.00 56.23 11.23 Light greenish clasts
 55.47 60.50 5.03 Silicic matrix, greyish

55.00	57.00	2.00 80% green clast
57.00	59.00	2.00 As above
59.00	61.00	2.00 70% green clast 60.63 and 60.68 m: 3 mm barren QZ-CB vein 35
61.23	64.24	3.01 Andesite. Dark greenish grey. (same as PPAN ?) 61.23-61.53 m: magnetic
61.00	63.00	2.00 61-61.23 m: shattered 62.74 m: 1.5 cm QZ-CB vein 45 with 10% SP
63.00	65.00	2.00 63.64-64 m: sheared, 40% shattered, 5% gouge 63.70 m: 3 mm calcite veinlet 40 with SP, GN
64.24	128.88	64.64 Andesite breccia as above; green-whiteish clasts in grey matrix
65.00	67.00	2.00 60% greenish clast
67.00	69.00	2.00 40% clasts 67.98 m: 5 cm gouge with calcite vein at 45 minor SP, CP
69.00	71.00	2.00 69.61-70.02 m: green, andesite contacts are 5 70.08 m: 6 cm dark brownish grey alt vein at 20 70.28 m: 5 mm QZ-CB vein 30, some SP 70.64 m: 12 mm QZ-CB vein 40 minor GN
71.00	73.00	2.00 70% clast 72.76 m: QZ-CB vein 3 mm 40 with SP, GN 72.81-73.23 m: a 90 fracture with minor GN, SP
73.00	75.00	2.00 50% clast
75.00	77.00	2.00 80% clast
77.00	79.00	2.00 90% clasts 78.18 m: 2 mm barite lens with SP 78.12 m: 2 mm QZ-CB vein 42 with PY
79.00	81.00	2.00 80% clasts
81.00	83.00	2.00 82.31 m: 1 mm CB veinlet, 50 with GN 82.37-82.52 m: sheared and shattered
83.00	85.00	2.00 80% clasts 84.59 m: minor QZ-pink carbonate at fracture 45 84.32 m: 1 cm gouge at 45
85.00	87.00	2.00 60% clasts 86.34 m: & 86.77 M are slightly shattered
87.00	89.00	2.00 90% clasts
89.00	91.00	2.00 30% clasts 90.72m: 6 mm QZ vein 38 90.68-90.88 m: greyish alteration
91.00	93.00	2.00 40% clasts
93.00	95.00	2.00 93.45-95.79 m: sheared 95.75 m: 1 cm gouge 6, high PY
94.62	95.25	0.63 Dyke. Dark brownish grey very fine grain massive. Upper contact = 40. Lower contact = 43 94.85 m: 6 cm hand sample
95.00	97.00	2.00 60% clasts
97.00	99.00	2.00 20% clasts
99.00	101.30	2.30 40% clasts
101.10	104.30	3.20 Low recovery (washed away mud). 30% sheared at 50, 10% gouge 101.3-102.7 m: sheared gougey 102.84-102.96 m: gouge 103.28 m: fracture 80 with little chodochrosite lens
104.30	106.00	1.70 40% clasts, minor rhodochrosite at fractures
106.00	106.87	0.87 70% clasts, few fractures 5, 38 with minor

		calcite fillings.
106.87	107.15	0.28 30% sheared at 50, 1% SP 107.03 m: 2 cm QZ vein 42 with SP and GN
107.15	108.00	0.85 Calcite veinlets 1 mm at 30
108.00	110.20	2.20 70% clast. Few calcite veinlets and two gypsum veinlets
110.20	110.43	0.23 110.2-110.33 m: is shape QZ-CB vein 1-1.2 cm thick with 70% SP, minor GN 110.31 m: shear gouge at 45 with QZ-CB vein 5% SP for this section
110.43	112.00	1.57 30% clasts
112.00	114.00	2.00 2.5% gypsum veins - 1-20 mm, 5% 80, 75
114.00	115.70	1.70 20% clasts, few gypsum veinlets
115.70	117.49	1.79 Sheared at 45-50, 20% gouge, 0.1% rhodochrosite
117.49	119.00	1.51 30% clasts Few calcite veinlets 2 mm at 45 118.44-118.57 m: bleached at 45 118.7 m: 3 cm sheared at 45 118.91-119.02 m: bleached, 2 cm silicified at 0
119.00	121.00	2.00 30% clasts 2.5% gypsum veins 1 cm, 45, 60, 2 mm at 45, 75
121.00	123.00	2.00 121.47 m: 6 cm sheared at 45, 1 cm gouge, 6 mm gypsum vein 121.62 m: 12 mm gouge at 45
123.00	125.00	2.00 30% clast, 10% gypsum veinlets 124.25 m: QZ-CB vein 1 cm at 50
125.00	127.10	2.10 125.35-126.1 m: sheared at 30, 10% gouge Few gypsum veinlets
127.20	136.00	8.80 Grey color, higher alteration intensity, very fade texture
127.10	129.00	1.90 90% sheared at 60-80, 20% gouge
129.00	131.00	2.00 1% gypsum veinlets 1-2 mm
128.88	136.00	7.12 Andesite Upper contact at 80 (?). Lower contact 47
131.00	133.00	2.00 2.5% gypsum veinlets
132.00	135.00	2.00 1% gypsum veinlets
135.00	136.00	1.00 136 m: 8 cm sheared (contact) at 47
136.00	137.25	1.25 Andesite breccia; light green andesitic clast in light maroon-grey matrix
137.25	153.55	16.30 Andesite; local brecciated, light green, minor clasts
136.00	138.00	2.00 40% clasts. Few shear fractures at 45, 50. 137.39 m: minor SP at shear fracture 45
138.00	140.00	2.00 40% clasts 2.5% gypsum veinlets
140.00	142.00	2.00 2.5% gypsum veinlets, 70% clasts
142.00	144.00	2.00 142.31 m: gypsum vein 2 cm, 35
144.00	146.00	2.00 10% matrix 0.3% gypsum veinlets
146.00	148.00	2.00 5% matrix, 0.3% gypsum veinlets
148.00	150.00	2.00 2.5% matrix, few whiteish clasts, 3 mm 1% gypsum veinlets 149.59 m: 3 mm QZ-CB gypsum veins at 20 & 30
150.00	152.00	2.00 1% gypsum veinlets 1-13 mm mainly 40
152.00	154.00	2.00 152.69-152.80 m: silicified at 42
153.55	216.46	62.91 Andesite breccia, upper contact 66 Pale greenish to whiteish clast in grey matrix
154.00	156.00	2.00 70% faded cast 156 m: 1 cm QZ-CB vein 38 with PY
156.00	157.58	1.58 70% casts

156.76 m: 1 cm QZ-CB vein 47
 157.58 159.53 1.95 90% sheared at 50 (?), 20% gouge, Minor SP, GN, at some
 gougey fractures
 Two rhodochrosite lens 2 mm and 5 mm
 159.53 159.91 0.38 Dyke; dark green, fine grain, massive, unaltered
 Upper contact = 40. Lower contact = 35 (gougey)
 159.53 160.28 0.75 160.06-160.28 m: shattered
 160.28 162.00 1.72 30% (?) clasts. Matrix is partially crystallized
 162.00 164.00 2.00 20% clasts
 162.34 m: 4 cm shattered
 164.00 167.00 3.00 30% clasts, 3% gypsum veinlets.
 165.47 m: 5 cm bleached, at 47, two QZ-CB-gypsum
 veinlets
 167.00 170.00 3.00 30% clasts
 169.31-169.60 m: sheared at 60, few gypsum veinlets
 170.00 173.00 3.00 10% clast, 0.3% gypsum veinlets
 Matrix has 2.5% blueish green altered mafic phenocrysts
 173.00 176.00 3.00 20% clasts, matrix as above
 172-173.15 m: sheared at 65 with 10% gypsum veins
 1-6 mm 65.
 176.00 179.00 3.00 90% clasts matrix as above
 176.24 m: 6 mm gypsum vein at gougey fracture 42
 177.09 m: 1 cm gypsum-carbonate vein 59
 179.00 181.12 2.12 40% clasts, 0.3% gypsum veinlets
 181.12 182.33 1.21 181.15 m: 1.5 cm sheared at 45 with some QZ-CB
 181.92-182.31 cm sheared at 45, gougey
 182.33 185.00 2.67 30% clasts. Few gypsum veinlets 3 mm, 5 mm, 47
 185.00 188.00 3.00 10% clast
 186.5-188.59 m: cooked up with another stage
 (Third stage) of maroon dyke (?), massive very fine grain
 188.00 191.00 3.00 188.48-189 m: 78% maroon silicious veins, main at 10-20
 189.16 m: 18 mm QZ-CB shear vein at 18
 190.3-190.52 m: silicified and sheared at 30
 190.91-191.10 M sheared at 48
 191.00 194.00 3.00 Clear clasts 50%
 194.00 197.00 3.00 50% clasts as above
 195.86-198.87 m: weakly sheared
 196.3 m: 4 cm gouge at 43
 196.31-196.42 m: moderately silicified at 43
 197 m: 6 cm silicious vein at 40 & 340
 197.00 200.00 3.00 197.52 m: sheared at 45, gougey
 199.01 199.47 0.46 Lapilli in fine dark grey ash, clasts consists of green
 gray, whiteish and pale brown, total 80%, round to
 angular. This lapilli also slightly intruded by the
 greyish intermediate (?) subvolcanics, it is as interbed
 of the green andesite
 200.00 203.00 3.00 20% matrix, 1% gypsum veinlets
 203.00 206.00 3.00 As above
 206.00 209.00 3.00 50% matrix
 209.00 212.00 3.00 70% matrix
 210.56-210.62 m: 3 cm silicified with PY stringers
 at 45 and 285 respectively
 212.00 215.00 3.00 70% matrix
 213.51-213.82 m: 7 cm long silicified at 48
 7 cm long gouge and then 5 cm long QZ-CB gypsum vein
 at 45

			214.5 m: 5 cm carbonatized (calcite and siderite) section of 45
215.00	218.00	3.00	1% gypsum veinlets
216.46	221.85	5.39	Mainly intermediate subvolcanics (one stage of the andesites). The matrix of above breccia fine grain, greenish grey and maroon-grey with mafic phenocrysts (altered) 1-2.5% in locals. Minor breccia in parts. Upper contact not clear. Lower contact 5.
218.00	221.00	3.00	1% clasts, 1% gypsum stringers
221.00	224.00	3.00	221.85-224 m: 60% matrix
221.85	270.36	48.51	Clastic andesite; (green clasts)
224.00	227.00	3.00	90% matrix 226.2 m: shear fracture 40 226.43-226.55 m: shear at 75
227.00	229.59	2.59	90% matrix
229.59	233.14	3.55	Moderately sheared
229.59	231.00	1.41	80% sheared, 20% gouge 229.67 m: sheared at 45 230.40-231 m: gouge at 80
231.00	233.14	2.14	20% sheared at 75-80 20% clasts
233.14	235.00	1.86	20% clasts 233.86-233.93 m: gouge at 30 and 330
235.00	237.02	2.02	30% clasts 235.47 m: 1 cm rhodochrosite-gypsum vein 30
237.02	239.20	2.18	20% clasts 239.7-239.2 m: bleached, 4 mm QZ-CB vein at 80, gouges
239.20	241.00	1.80	30% clasts Few rhodochrosite veinlets 2 mm at 5
241.00	243.00	2.00	40% clasts 1% carbonate veinlets associated with gypsum at 30 & 50
243.00	245.00	2.00	5% clasts 243-243.47 m: moderate sheared at 45, gougey 243.44 m: 5 cm altered vein, bleached, at 42 243.69-243.88 m: sheared at 75 and 40 244.27-244.88 m: calcite veinlets 1-5 mm at 5, 45, & 315
245.00	246.37	1.37	5% clasts 245-245.5 m: 5% carbonate stringers, 1% rhodochrosite
246.37	270.36	23.99	Strong alteration, gray color
246.37	247.76	1.39	246.56 m: calcite vein > 1 mm 86 with SP
247.76	249.01	1.25	40% sheared sections at 40-65 247.93 m: shear fracture 65 with SP 248.2-248.25 m: 5% interstitial SP, GN at shear section 248.75 m: 2 cm QZ vein 25, trace GN 249.94: 2 cm calcite rhodochrosite vein 45
249.01	250.70	1.69	249.17-249.23 m: some elongated SP blebs 3 mm long 0.5 mm thick at 75 trending 249.25-249.3 m: GN-SP 2 mm at fracture 86 250 m: 1 mm GN SP at irregular fracture 250.33-250.48 m: 6 GN, SP veinlets 1-2 mm at 81 250.6-250.66: minor GN, SP, at shear section
250.70	252.06	1.36	251.75 m: 1 cm QZ-CB vein at 40, minor PY 251.82 m: 1 cm QZ-CB vein 5, some PY
252.06	253.00	0.94	Few gougey fractures at 32, 45

Three QZ-CB veinlets 4 mm at 20, 30, 290
252.83-253.1 m: 10% PY blebs 2 mm to 20 mm

253.00 254.00 1.00 10% pale green clay mineral (CB-sericite) alteration
in parts are concentrated with PY
253.29 m: some SP dissemination

254.00 255.11 1.11 PY occurred as above
254.60 m: QZ vein 12 mm, 35

255.11 256.74 1.63 Irregular QZ-CB veining zone; lens blebs stockwork, etc

255.11 256.00 0.89 255.26 m: 2 cm QZ-CB vein 50 with 3 cm gouge below

256.00 257.00 1.00 QZ-CB veinlets concentrate at 256.79-257.03 m:

257.00 258.00 1.00 15% QZ-CB lens, stringers and stockwork, trace SP

257.10 258.50 1.40 Brecciated up with QZ-CB

258.00 259.00 1.00 Moderately sheared 50-80
Irregular QZ-CB, lens, stockwork, blebs veinlets

259.00 260.00 1.00 40% sheared 60-80, 5% gouge
259.48-259.60 m: SP along QZ-CB vein and shear
fracture 80

260.00 261.00 1.00 Sheared
260.57-261 m: some SP, GN, blebs = 2% in sheared parts

261.00 262.00 1.00 261.3 m: 14 mm thick QZ-CB lens at 30 with SP
261.5 m: 2 cm QZ-CB vein 42 with SP
261.83 m: 3.5 cm QZ-CB vein 39 with SP

262.00 263.00 1.00 262-262.85 m: QZ-CB vein breccia, upper contact = 38
Lower contact = 10, trace SP

263.00 264.00 1.00 263-263.28 m: 20% QZ-CB lenses and stockwork, some GN
SP
263.93 m: 2 cm QZ-CB vein 28 with PY

264.00 265.00 1.00 264-264.25 m: bleached

265.00 266.00 1.00 265.67-266.2 m: 20% QZ-CB stockwork

266.00 267.00 1.00 266.81 m: QZ-CB vein > 3 mm 30, trace SP
266.92 m: QZ-CB vein, 8 mm 42

267.00 268.00 1.00 266.97-267.13 m: 15% PY in bleached section
267.5-267.64 m: QZ-CB vein at 45, trace SP at lower
contact

268.00 269.12 1.12 268.9-269.05 m: sheared 45, 90, gougey some
QZ-CB stockwork
269.09 m: 8 mm QZ-CB vein 20

269.12 270.36 1.24 267.70 m: 6 mm QZ-CB vein 50

Property Name: HANK Client Name: LAC MINERALS LTD.
 Hole No: 89-DDH-10 Azimuth: 320 Borehole Test Method: None
 Northing: 11449.180 Dip: -60 Test Azimuth: Core Size: NQ & BQ
 Easting: 10697.300 Length: 156.97 m Test Depth: Date Started: September 3, 1989
 Elevation: 1105.270m

LITHOLOGY:

FROM	TO	WIDTH
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6.83	99.82	92.99 Andesite breccia
99.82	113.27	13.45 Andesite
113.27	118.67	5.40 Tuff
118.67	156.97	38.30 Clastic andesite

ALTERATION

PY-CB-Sericite alteration is moderate to high in general

MINERALIZATION

153.95	156.07	2.12 Shear zone, with DZ-CB vein associated with SP, GN
	6.10	6.10 Casing
	4.54	4.54 NQ core
40.54	156.97	116.43 BQ core
	8.23	8.23 First footage mark
	6.83	6.83 Measured back from 8.23 m
	53.00	56.17 Limonite existent zone Limonite mainly on fracture surfaces
	99.82	92.99 Andesite breccia Light green or pale whiteish green andesitic clasts in greyish matrix (intermediate or andesitic)
6.83	16.86	10.03 60% sheared sections, 20% gouge
6.83	8.23	1.40 70% sheared 6.83-7.45 m: some high angle shear fractures 85 7.83-7.92 m: gouge at 45 8.9-9.48 m: gouge at 87
6.23	11.28	5.05 60% sheared, 30% shattered sections 2.5% gouge
11.28	14.32	3.04 11.28-11.4 m: shattered 11.62-11.75 m: shattered
14.32	17.37	3.05 14.58-16.25 m: moderate shattered very limonite and crumbly small fault
17.37	20.42	3.05 Very limonitic fracture, mainly 40-50, some at 90
20.42	23.47	3.05 21.8-22.5 m: shattered and sheared, very limonitic & gougey
22.00	42.00	20.00 Clasts are whiteish grey or grey altered
23.47	26.52	3.05 24.93 m: 5 mm PY vein, 2 26.4-26.7 m: shattered
26.52	29.56	3.04 Only few clasts 28.52-29 m: very limonitic sheared and shattered
29.56	31.00	1.44 30% sheared and shattered, very limonitic fractures 2.5% gouge
31.00	33.00	2.00 20% clasts
33.00	35.00	2.00 10% clasts

		33-33.25 m: gouge at 87
35.00	37.00	2.00 Very faded clasts 35.66 m: 1 mm PY on fracture surface 48
		35.8-37.2 m: a very limonitic fracture 90
37.00	39.00	2.00 5% clasts fractures mainly at 28
39.00	40.54	1.54 20% clasts 40.13 m: 6 cm gouge at 70
40.54	41.76	1.22 41.28-41.76 m: moderately shattered, very limonitic
42.00	104.00	62.00 Very faded clasts
41.76	44.00	2.24 41.92-42.8 m: a 90 fracture, very limonitic
44.00	46.00	2.00 About 10% faded clasts. Minor blackish mineral dissemination 44.72-44.8 m: shattered
46.00	48.00	2.00 46.05 and 46.27 m: some disseminated blackish mineral 46.35-46.52 m: and 47.70-47.85 m: shattered and limonitic fracture 85
48.00	50.00	2.00 48.45-49.35 m: one very limonitic fracture at 90 49.44 m: one QZ vein 1 cm, 0, barren
50.00	52.00	2.00 51.55-51.65 m: purpleish grey silicified section at 4, with PY blebs in vugs 3 mm in diameters
52.00	53.95	1.95 53.44-53.63 m: sheared and shattered, gougey
53.95	56.99	2.04 54.19-54.66 m: sheared at 90 54.56-54.66 m: shattered 55-56.48 m: moderate sheared at 90, gougey 56.88-56.99 m: shattered
56.99	60.04	3.05 57.67-58.22 m: sheared and shattered 59.64-60.04 m: sheared at 75-85, shattered, gougey
60.04	62.00	1.96 50% clasts 60.52-60.76 m: sheared, some PY stringers
62.00	64.00	2.00 30% faded clasts. Two QZ-CB veinlets 2 & 7 mm 50, 38
64.00	66.00	2.00 64-65.52 m: 80% clasts 65.18 m: 1 cm gouge 75
65.52	66.67	1.15 No clast, pale grey, upper contact = 70, lower contact sheared and shattered
66.00	68.00	2.00 Lower recovery 66.52-66.66 m: bleached section 50, with 10% PY and some blackish mineral 66.66-67.93 m: moderately shattered and sheared minor QZ-CB (pink) veinlet
68.00	70.00	2.00 69.92-70 m: some disseminated blackish mineral
70.00	72.00	2.00 40% clasts 71.57-72 m: silicified upper contact 40, lower contact not clear, shattered
72.00	74.00	2.00 Few rhodochrosite stringers 73.68-74.3 m: sheared and shattered, gougey
74.00	76.00	2.00 1% QZ-CB stringers 0.5-2 mm, 35-45
76.00	78.00	2.00 77.32-77.38 m: 2.5% blackish mineral 77.39-77.48 m: bleached vein at 43
78.00	80.00	2.00 79.66 m: 3 mm shear fracture with CB and SP, 45
80.00	82.00	2.00 1% calcite and QZ-CB stringers 80.59 m: 3 cm altered vein with 3 mm QZ-CB vein at 12 80.68-81.28 m: some disseminated blackish mineral in parts
82.00	84.00	2.00 20% sheared at 40, 10% shattered, 5% gouge
84.00	86.00	2.00 85.67-86.18 m: sheared and shattered, gougey
86.00	88.00	2.00 20% faded clast, very strong seritized
88.00	90.00	2.00 50% clasts

82.37 m: 3 mm QZ-CB veinlet at 24
 90.00 92.00 2.00 91.19 m: 5 cm pale green altered section (strong PY-CB-Sericite alteration) at 22, with, 20% PY
 92.57 m: 6 cm section as above at 47
 92.00 94.00 2.00 93.19-93.4 m: sheared at 60, 2 cm gouge
 93.9 m: some disseminated blackish mineral
 94.00 96.00 2.00 95.04 m: 4 mm QZ-CB vein 60, trace SP
 95.36 m: 3 mm QZ-CB stringer, 20 with SP
 96.00 98.00 2.00 1 mm QZ-CB veinlet 90 with some PY
 98.00 98.92 0.92 98.91: 1 cm gouge at 25
 98.92 100.00 1.08 98.92-99.19 m: some calcite stringers 1 mm at 38, 2
 99.43-100 m: sheared at 60, gougey
 99.82 108.81 8.99 Andesite (?): highly altered, grey
 100.00 102.12 2.12 100.62-102.12 m: sheared, 20% shattered, 50%
 gouge, low recovery
 102.12 104.04 1.92 103.29-104.04 m: some high angle shear fracture 85;
 gougey
 104.04 105.76 1.72 .3% disseminated blackish mineral
 105.55-105.76 m: 30% gouge at 70
 105.76 108.81 3.05 108.49-109.66 m: sheared and shattered
 108.81 113.27 4.46 Andesite: light to pale green
 108.81 111.86 3.05 108.85 and 111 m: some ground rubbles have SP
 with QZ-CB ground or washed away about 40% of core
 111.86 113.27 1.41 Grey slightly sheared 85
 113.27 118.67 5.40 Tuff: 113.27-114.18 m: ash, some fine grain, pale green
 sections with 1% recrystalline and altered euhedral
 phenocrysts interbed with some coarse grain layers >2-4 cm
 green altered, bedding 28-30
 114.18-118.67 m: cooked up by the greyish subvolcanics
 (matrix of the andesite breccia)
 113.27 115.67 2.40 See above.
 115.67 118.67 3.00 Minor QZ-CB stringers, few clasts up to 9 cm long
 118.67 121.90 3.23 Bleached moderately sheared
 118.67 119.67 1.00 118.67 m: 1 cm, QZ-CB vein 38 with 50% SP, attached
 with 1 cm gouge
 QZ-CB stringers are in network
 119-119.67 m: fractures are 60, 30, 90
 119.67 121.00 1.33 Shear fracture 90 gougey with QZ-CB veinlets
 (one pink vein 3 mm 80)
 118.67 156.97 38.30 Clastic andesitic (Intermediate) (alteration intensity
 between 4 & 5)
 121.00 121.09 0.09 Weakly sheared at 30, 40, gougey
 121.09 124.00 2.91 20% clasts, 123.76-124.07 m: shear fractures 20-45
 124.00 126.00 2.00 30% clasts
 126.00 128.00 2.00 10% clasts
 128.00 130.00 2.00 120 clast, 129.33-129.52 m: shattered
 130.00 132.00 2.00 10% clast 130.74 m: 4 mm QZ-rhodochrosite 10
 132.00 134.00 2.00 20% clast, 132.1 m: 4 mm calcite at fracture 84
 134.00 136.00 2.00 10% clast
 134.34 m: 3 mm QZ-CB veinlet 60 with 50% SP-GN
 136.00 138.00 2.00 20% clasts
 138.54 m: 5 mm QZ-CB veinlet 0, some PY
 138.00 139.46 1.46 10% clast, 1% QZ-CB stringers 0.5-2 cm
 139.29 142.33 3.04 Recovery = 67.76%
 Core ground and/or washed away at 139.9 m, 140.5 m
 and 142.3 m.

139.46	140.33	0.87 140.33 m: only a roughly guessed mark 139.75-140 m: ground core, shattered, a piece of 4 cm section has a 1.1 cm QZ-CB vein 48 with SP and GN
140.33	141.31	0.98 Very low recovery, sheared and shattered some QZ-CB vein 14 mm with 70% SP, GN salvages = 75
141.31	141.94	0.63 10% clast, pale grey and some QZ-CB stringers
141.94	143.41	1.47 Sheared and shattered, very low recovery, 60% gouge 141.94-142.33 m: gouge at 82, with SP and CB vein at upper contact >12 mm (?)
143.41	145.00	1.59 Pale green grey matrix, 10% clasts, local clasts have blackish mineral replacement
145.00	147.00	2.00 Pale green, only few clasts
147.00	149.00	2.00 10% clast 148.85 m: 4 mm rhodochrosite at 18
149.00	151.00	2.00 5% clasts Few QZ-CB stringers 1-2 mm 10 150.35 m: 2 mm QZ-CB stringer 45, with SP, GN
151.00	153.00	2.00 20% clasts 151.6 m: 5 mm rhodochrosite vein at 12
152.00	153.95	0.95 10% clasts
153.95	154.53	0.58 153.95-154.28 m: gouge 72 154.28-154.53 m: weakly silicified and carbonatized with 5% SP, some GN, at 40 and 85-90
154.53	155.90	1.37 Few clasts 154.62-154.79 m: sheared and shattered
155.90	156.07	0.17 50% SP and GN associated with QZ-CB vein at 56
156.07	156.97	0.90 Bleached 156.47 m: 0.5 mm QZ-CB stringer 82 with SP 156.84-156.97 m: gouge 156.97 End of Hole. Lost one shell and bit. No trophy test

HI-TEC RESOURCE MANAGEMENT LTD.

DIAMOND DRILL LOG

Property Name:	HANK	Client Name:	LAC MINERALS LTD.
Hole No:	89-DDH-11	Azimuth:	320
Northing:	11448.980	Dip:	-65
Easting:	10697.500	Test Dip:	
Elevation:	1105.270m	Length:	121.52 m
		Test Depth:	
		Date Started:	September 6, 1989
		Date Completed:	September 9, 1989

LITHOLOGY:

FROM	TO	WIDTH
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8.23	110.42	102.19 Andesite breccia
110.42	112.40	1.98 PPAN
112.40	121.62	9.22 Andesite breccia

ALTERATION:

PY-CB-Sericite alteration is moderate to high in general

MINERALIZATION

72.30	76.70	4.40 Shear zone with minor SP about 10% PY, silicified in parts
84.00	89.42	5.42 Shear zone with some rhodochrosite veinlets locally silicified some SP associated with CB veins
104.48	104.82	0.34 SP associated with QZ-CB veins
108.32	110.42	2.10 Shear zone, massive SP-PY vein, associated with some QZ-CB 7.62 7.62 Casing. Overburden should be less than 6.1 m
	61.87	61.87 NQ core
61.87	121.62	59.75 BB core
8.23		8.23 First footage mark
	8.23	8.23 Only 23 cm recovered, included overburden casing
	60.00	60.00 Limonite existent zone. Mainly along on fracture surfaces
8.23	110.42	102.19 Andesite breccia
8.23	9.41	1.18 70% sheared 8.82-9.01 m: gouge
8.23	13.92	5.69 Rare limonite
9.41	11.00	1.59 Sheared at 55, 75-90, gougey fractures (5%) 9.77 m: 5 mm calcite vein 42 with SP
11.00	13.10	2.10 20% sheared
13.10	15.00	1.90 10% clasts 13.62-13.81 m: gouge 14.14 m: QZ spot 1 cm with SP
13.92	60.00	46.08 Rich limonite in some fractures and sheared sections
15.00	17.00	2.00 2.5% limonite on fracture surface
17.00	19.00	2.00 10% greenish grey clasts (andesitic) 17-17.37 m: some high angle shear fracture 85 very limonitic
19.00	21.00	2.00 20% clasts 19.24-19.32 m: very limonitic gouge at 36
21.00	23.00	2.00 21.14-21.33 m: sheared and shattered, limonitic 22.12-22.31 m: very limonitic gouge
23.00	25.00	2.00 20% clasts 24-24.92 m: sheared at 75-85 very limonitic gougey
25.00	27.00	2.00 Some porphyritic texture, 1% altered mafic phenocrysts 1-2 mm in diameters, 5% clasts

		25-25.45 m: sheared
		25.06 m: 5 cm gouge at 36
27.00	29.00	2.00 30% clasts. Limonitic fractures at 40, 65-75
29.00	31.00	2.00 50% clasts
31.00	33.00	2.00 20% clasts
33.00	35.00	2.00 5% clast, some porphyritic texture in matrix
35.00	37.00	2.00 60% clast
37.00	39.00	2.00 30% clasts
39.00	41.00	2.00 70% clasts
41.00	43.00	2.00 30% clasts 41.2 m: 2 cm gouge at 63 42.18-42.33 m: gouge at 45
43.00	45.00	2.00 50% clasts, few dark grey clasts, mainly whiteish Some fractures 70
45.00	47.00	2.00 30% clasts, whiteish with PY rims 45.6-46.6 m: a fracture 90, limonitic
47.00	49.00	2.00 70% whiteish clasts as above 48.4-48.55 m: a limonitic fracture 85, some 35-45 Limonitic fractures
49.00	51.00	2.00 10% matrix more or less silicious 50.25 m: 12 mm limonitic gouge at 80
51.00	53.00	2.00 5% matrix, 2.5% limonitic, fractures are 20, 45, 70
53.00	55.00	2.00 5% matrix 53.45-53.53 m: sheared and shattered 53-53.74 m: limonitic fracture 90 Some other fractures 10, 50-60
55.00	57.00	2.00 10% matrix 56.08-56.35 m: sheared at 80, gougey
57.00	59.00	2.00 5% matrix 57.45-59.54 m: fractures subparallel to core axis
59.00	61.87	2.87 59-60.9 m: 30% matrix 60.9-61.94 m: bleached, no visible clast Still have high angle fractures subparallel to core axis
61.87	63.09	1.22 61.87 m: ground some core, change of BQ bit 61.87-61.93 m: shattered (?) gougey 61.87-63.09 m: some shattered rubbles (20%)
63.00	65.30	2.30 Very pale clast, matrix is more or less silicious
63.09	65.00	1.91 10% matrix, one 80 fracture and some at 10, 45
65.00	67.00	2.00 20% matrix as above, pale green high sericitized clasts with feldspar phenocrysts 0.5 mm fractures mainly 50
67.00	69.00	2.00 5% matrix, clast as above 67.09-67.59 m: some high angle fractures 80-90 and some at 10 68.98 m: 2 mm PY with calcite stringer at 45, 4 cm bleached
69.00	71.00	2.00 60% clast whitish, 40% matrix as above 69.88-70.01 m: some rhodochrosite lens (5%) 70.68 m: minor GM at fracture 73, one rhodochrosite lens 2 cm long, 4 mm thick beside it
71.00	72.30	1.30 30% matrix
72.30	73.80	3.50 Shear and silicified zone
72.30	75.28	2.98 50% sheared, 5% gouge at 10, 40, 70 10% shattered, 1% blackish mineral dissemination, trace SP 72.38-72.72 m: moderately silicified
75.28	76.70	1.42 75.28-75.8 m: sheared at 80, 50, 30% gouge 75.8-76.7 m: 1% disseminated blackish mineral Tr, SP

76.70	78.00	1.30 1% disseminated blackish mineral in locals - trace SP 77.82 M 6 cm sheared at 52
78.00	80.00	2.00 20% matrix, very strong sericitized, pale green 79.36-79.59 m: bleached section at 45, with 2.5% rhodochrosite veinlets and spots, 2.5% blackish mineral dissemination
80.00	82.00	2.00 50% clasts. Pale green and white, rich PY replacement 80.27-80.47 m: bleached, 1% blackish mineral dissemination Upper contact 50, Lower contact 80
82.00	84.00	2.00 20% clasts 82.67 m: 5 mm QZ- pink CB lens, 45 83-83.48 m: alteration vein, sheared and silicified in parts, 5% blackish mineral 83-83.13 m: strongly sericitized pale green 83.13-83.17 m: feldspar vein 40 with some blackish mineral SP and green fragments 83.17-83.24 m: gouge 45 83.24-83.36 m: silicified vein at 50, with 5 mm black mineral-SP-GN vein at the middle.
84.00	85.66	1.66 30% clast, strongly bleached, Few rhodochrosite stringers 84.61 m: 3 mm altered vein with minor SP
85.66	89.42	3.76 Shear zone with 5% carbonate veins included rhodochrosite and QZ-CB veins, locally silicified, some SP
85.66	87.47	1.81 85.66-85.85 m: shear fractures at 30, 30% gouge with some rhodochrosite and SP 85.98 m: 6 mm QZ vein at 46 with some SP and blackish mineral 86-86.26 m: shear fracture 60 change to 90 with QZ-pink CB 8 mm, 5% blackish mineral and some SP 86.23 m: QZ-pink CB vein 1.7 cm at 33% 86.87 m: 1 cm pink CB vein at 48
87.47	89.42	1.95 80% sheared 20% shattered 88.11-88.29 m: QZ-CB pervasively altered, at 43 88.27 m: 22 mm massive PY 88.52-89.42 m: 60% shattered, some blackish mineral and rhodochrosite
89.42	91.00	1.58 20% clasts
91.00	93.00	2.00 30% clasts 92.68-93 m: some shear fractures at 80, 45
93.00	95.00	2.00 20% clasts. Some QZ-CB stringers 1 mm at 5-10 93.26 m: two 1 mm QZ-CB stringers with SP at 70
95.00	97.00	2.00 50% clasts
97.00	99.00	2.00 60% clasts 98.63 m: calcite vein (lens) 2-10 mm, 35 (vug) 97.57-97.72 m: cooked up with some maroon volcanics (?) banding at 0. (pale maroon)
99.00	101.00	2.00 20% clasts 99.54 m: 2 cm QZ-CB vein at 20; barren
101.00	103.00	2.00 10% clasts 102.83 m: two QZ-pink CB veinlet 4 mm at 20 102-102.19 m: 2.5% SP associated with QZ-CB stringers 70, 295, 1 mm - 5 mm 102.34-102.40 m: SP-QZ-CB stringers as above at 65 and 295 102.9 m: 1 mm SP-QZ-CB stringer at 45
103.00	104.48	1.48 Local minor blackish mineral

104.08 104.82 0.74 104.5-104.63 m: 1 mm QZ-CB veinlet at fracture 75 with SP, PY
104.69-104.82 m: one 2.5 cm QZ-CB vein 63 with 20% SP

104.82 106.27 1.45 104.95-105.40 m: one 87 fracture, gougey
105.63-105.93 m: 5% QZ-CB veinlets 1-5 mm 0, 30
106.12 m: QZ-CB vein 1 cm 25, pale pink
106.05 m: 1 mm SP vein at 40

106.27 108.32 2.05 107.33-107.6 m: shattered

108.32 108.66 0.34 5% SP minor CP
108.42-108.58 m: massive SP-PY associated with 10% CB upper contact sheared at 70. Lower contact = 67
108.58-108.66 m: sheared

108.66 110.43 1.77 108.66,109.17 m: sheared
108.86 m: 12 mm & 30 mm QZ lens with SP
109.17-109.52 m: silicified with 10% QZ veinlets lens and stockworks, upper contact 45, lower contact 295
110.29-110.42 m: gouge

110.42 112.40 1.98 PPAN
Pale green with 40% altered felsic phenocrysts
(feldspar) 2-3 mm in locals. Mafic mineral are pale green
altered 1-3 mm long
111.92 m: 7 mm QZ-pink CB vein at 20
112.09-112.25 m: shattered

112.40 121.62 9.22 Andesite breccia

112.40 114.07 1.67 Sheared 30% gouge trace SP

114.07 115.62 1.55 70% sheared, 30% gouge
114.96 m: 2.3 cm QZ vein 32

115.62 117.95 2.33 115.62-117.73 m: 40% clasts
117.73-117.89 m: PPAN
117.89-117.95 m: shattered

117.95 118.87 0.92 Pale greenish grey 0.3% SP associated with calcite
stringers 1-2 mm, some pink carbonate, weakly sheared

118.87 120.00 1.13 Light green, 40% clasts
119.67 m: 6 mm calcite vein 10

120.00 121.62 1.62 Light green, 60% clasts

121.62 End of hole

Hole caved in, 2 bits gone, no drilling-rod pulled out, no trophy test

APPENDIX IVb
GEOTECHNICAL LOGS AND ANALYTICAL DATA FOR
DIAMOND DRILL HOLES



HOLE NUMBER	DDH 89-1	SAMPLE					Sample		ppb	GMT	ME
	R.O.D.	From	To	Width (m)	PYI	VnI	A	F Number	Au	Au	Gi
Recovery											
0.78/2=39%	(0.78-0.22)/2=28%	12.00	14.00	2.00	2.50	0.00	5	5 101001	23		
1.46/2=73%	(1.46-0.25)/2=60.5%	14.00	16.00	2.00	2.50	0.30	5	7 101002	29		
2/2=100%	(2-0.3)/2=85%	16.00	18.00	2.00	2.50	1.00	5	5 101003	110		
1.96/2=98%	(1.96-0.72)/2=62%	18.00	20.00	2.00	2.50	Tr	5	3 101004	39		
1.89/2=94.5%	(1.89-0.56)/2=66.5%	20.00	22.00	2.00	2.50	1.00	5	5 101005	200	0.21	
2.09/2=104.5%	(2.09-0.45)/2=82%	22.00	24.00	2.00	2.50	Tr	5	7 101006	32		
(1.25/1.3=96.15%)	(1.25-0.47)/1.3=28.33%	24.00	25.30	1.30	1.00	Tr	5	5 101007	35		
1.63/1.7=95.88%	(1.63-0.32)/1.7=77.06%	25.30	27.00	1.70	2.50	1.00	5	4 101008	35		
2/2=100%	(2-0.83)/2=58.5%	27.00	29.00	2.00	5.00	Tr	5	3 101009 SP	36		
1.84/2=92%	(1.84-0.4)/2=72%	29.00	31.00	2.00	2.50	0.30	8	9 101010	170	0.21	
1.33/1.86=71.51%	(1.33-0)/1.86=71.51%	31.00	32.86	1.86	5.00	Tr	6	8 101011	248	0.27	
1.33/1.35=98.52%	(1.35-0.34)/1.35=74.81%	32.86	34.21	1.35	5.00	5.00	7	5 101012	1018	0.62	
1.7/1.79=94.97%	(1.7-0.1)/1.79=89.39%	34.21	36.00	1.79	5.00	0.03	6	7 101013	117		
0.9/2=45%	(0.9-0.1)/2=40%	36.00	38.00	2.00	5.00	2.50	6	6 101014	260	0.27	
2/2=100%	(2-0.42)/2=69%	38.00	40.00	2.00	5.00	0.10	5	3 101015	153	0.17	
1.85/2.05=90.24%	(1.85-0.25)/2.05=78.05%	40.00	42.05	2.05	2.50	0.30	5	3 101016	32		
0.51/0.51=100%	(0.51-0.26)/0.51=49.02%	42.05	42.56	0.51	5.00	10.00	5	2 101017 SP,GN,CP	140		
1.46/1.44=101.4%	(1.46-1.2)/1.44=18.06%	42.56	44.00	1.44	5.00	0.10	5	5 101018	19		
1.97/2=98.5%	(1.97-0.37)/2=80%	44.00	46.00	2.00	5.00	0.10	5	5 101019 Tr,SP,GN	90		
1.89/2=94.5%	(1.89-0.48)/2=70.5%	46.00	48.00	2.00	5.00	0.30	5	4 101020 Tr,SP,GN	130		
2/2=100%	(2-0.61)/2=69.5%	48.00	50.00	2.00	5.00	0.30	5	3 101021 SP	189	0.21	
1.64/2=82%	(1.64-0.36)/2=64%	50.00	52.00	2.00	5.00	1.00	5	6 101022	52		
1.77/2=88.5%	(1.77-0.73)/2=52%	52.00	54.00	2.00	5.00	0.30	5	3 101023 SP,GN	214	0.24	
1.51/1.65=91.52%	(1.51-0.67)/2=42%	54.00	55.65	1.65	5.00	1.00	5	4 101024	262	0.31	
0.53/0.53=100%	(0.50-0.38)/8.53=28.30%	55.65	56.18	0.53	2.50	30.00	5	2 101025	103		
0.81/0.82=98.78%	(0.81-0.42)/0.82=47.56%	56.18	57.00	0.82	5.00	2.50	5	3 101026	315	0.45	
1.98/2=99%	(1.98-1.38)/2=30%	57.00	59.00	2.00	2.50	0.30	5	3 101027	525	0.62	
2.63/2.63=100%	(2.63-1.71)/2.63=34.98%	59.00	61.63	2.63	2.50	2.50	5	3 101028	66		
0.66/0.73=90.42%	(0.66-0.2)/0.73=63.01%	61.63	62.36	0.73	2.50	20.00	7	4 101029 CP,TT,GN	4990	5.18	2.7
0.31/0.34=91.18%	(0.31-0)/0.34=91.18%	62.36	62.70	0.34	5.00	Tr	9	4 101030	202	0.24	
0.48/0.49=97.96%	(0.48-0.32)/0.49=32.65%	72.70	63.19	0.49	5.00	10.00	7	3 101031 CP,SP,GN	2871	2.78	2.5
1.81/1.81=100%	(1.81-1.59)/1.81=12.15%	63.19	65.00	1.81	5.00	1.00	5	2 101032	53		
2/2=100%	(2-1.6)/2=20%	65.00	67.00	2.00	2.50	1.00	4	2 101033	86		
1.95/2=97.5%	(1.95-1.51)/2=19%	67.00	69.00	2.00	2.50	2.50	4	2 101034	120		
2.06/2=103%	(2.06-1.78)/2=14%	69.00	71.00	2.00	1.00	1.00	3	2 101035	138		
2/2=100%	(2-1.51)/2=24.5%	71.00	73.00	2.00	1.00	5.00	4	2 101036	145		
1.92/2=91%	(1.92-1.4)/2=26%	73.00	75.00	2.00	2.50	5.00	5	2 101037	884	0.27	
2.06/2=103%	(2.06-1.61)/2=22.5%	75.00	77.00	2.00	2.50	2.50	5	2 101038 Tr,SP	255	0.41	
2/2=100%	(2-1.6)/2=20%	77.00	79.00	2.00	2.50	1.00	5	3 101039	43		
1.96/2=98%	(1.96-0.88)/2=54%	79.00	81.00	2.00	5.00	2.50	5	4 101040 Tr,SP	139		
1.08/1.16=93.1%	(1.08-0.96)/1.16=10.34%	81.00	82.16	1.16	5.00	0.30	5	2 101041	154	0.27	
0.21/0.21=100%	(0.21-0)/0.21=100%	82.16	82.37	0.21	5.00	80.00	9	5 101042 SP,CP	10000	95.28	
1.62/1.63=99.39%	(1.62-0.72)/1.63=55.21%	82.37	84.00	1.63	5.00	0.30	5	3 101043	124		
1.95/2=97.5	(1.95-1.2)/2=37.5%	84.00	86.00	2.00	2.50	1.00	5	2 101044	183	0.17	
2/2=100%	(2-1.68)/2=16%	86.00	88.00	2.00	2.50	2.50	5	2 101045	281	0.48	
0.85/0.85=100%	(0.85-0.74)/0.85=12.94%	88.00	88.85	0.85	5.00	1.00	5	2 101046	180	0.17	
0.28/0.28=1000%	(0.28-0.1)/0.28=64.29%	88.85	89.13	0.28	5.00	5.00	7	5 101047 2.5%SP&GN	2822	2.88	1.5
0.59/0.59=100%	(0.59-0.16)/0.59=72.88%	89.13	89.72	0.59	5.00	5.00	5	3 101048 Tr,SP	311	0.41	
0.58/0.58=72.5%	(0.58-0.16)/0.58=52.5%	89.72	90.52	0.80	5.00	2.50	6	5 101049 SP,GN	1474	1.61	
0.82/1.48=55.44%	(0.82-0)/1.48=55.41%	90.52	92.00	1.48	10.00	2.50	9	10 101050 SP	388	0.48	
1.38/1.57=87.90%	(1.38-0.14)/1.57=78.98%	92.00	93.57	1.57	10.00	2.50	7	8 101051	94		
0.96/1.11=86.49%	(0.96-0.1)/1.11=86.49%	93.57	94.68	1.11	10.00	0.00	8	9 101052	65		
0.37/0.41=90.24%	(0.37-0)/0.41=90.24%	94.68	95.09	0.04	1.00	90.00	9	5 101053 GN,SP,CP	272	0.31	

HOLE NUMBER	DDH 89-2	R.B.D.	SAMPLE						A	F	Sample Number	ppb Au
			From	To	Width (m)	PYI	VnZ	A				
1.82/3.3=55.15%	(1.82-0.14)/3.3 = 50.91%		20.17	23.47	3.30	2.50	0.30	9	10	41201	193	
2.49/2.53=98.42%	(2.49-0.36)/2.53=84.19%		23.47	26.00	2.53	2.50	0.30	8	9	41202	204	
1.73/2=86.5%	(1.73-0.167)/2=78.5%		26.00	28.00	2.00	5.00	1.00	6	6	41203	273	
2/2 = 100%	(2-0.22)/2=89%		28.00	30.00	2.00	5.00	0.30	5	5	41204	67	
1.75/2=87.5%	(1.75-0.68)/2=53.5%		30.00	32.00	2.00	5.00	Tr	5	5	41205	143	
1.96/2=98%	(1.96-0.59)/2=68.5%		32.00	34.00	2.00	5.00	Tr	5	4	41206	37	
2/2=100%	(2-0.34)/2=83%		34.00	36.00	2.00	5.00	1.00	5	5	41207	96	
1.93/2=96.5%	(1.93-0.58)/2=67.5%		36.00	38.00	2.00	2.50	1.00	5	4	41208	169	
2.23/2.23=100%	(2.23-0.81)/2=71%		38.00	40.23	2.23	2.50	0.30	5	6	41209	55	
1.24/2.09=59.33%	(1.24-0.46)/2.09=37.32%		40.23	42.32	2.09	5.00	Tr	5	4	41210	89	
0.82/2.48=33.06%	(0.82-0.1)/2.48=29.03%		42.32	44.80	2.48	2.50	1.00	7	10	41211	106	
1.37/1.41=97.16%	(1.37-0.35)/1.41=72.34%		44.80	46.21	1.41	5.00	2.50	5	5	41212 SP,GN,CP	579	
1.76/1.79=98.32%	(1.76-1.3)/1.79=25.7%		46.21	48.00	1.79	5.00	0.30	5	2	41213	308	
1/1=100%	(1-0.23)/2=77%		48.00	49.00	1.00	2.50	0.30	5	3	41214 SP,GN,TT	282	
1.34/1.49=89.93%	(1.34-0.12)/1.49=81.88%		49.00	50.49	1.49	5.00	10.00	5	4	41215 SP,GN	1509	
2.04/2.04=100%	(2.04-1.62)/2.04=20.59%		50.49	52.53	2.04	2.50	0.30	5	2	41216	173	
2.3/2.47=93.12%	(2.3-0.11)/2.47=88.66%		52.53	55.00	2.47	5.00	2.50	6	6	41217	908	
2.06/2=103%	(2.06-1.63)/2=21.5%		55.00	57.00	2.00	5.00	2.50	5	2	41218	340	
1.91/1.92=99.48%	(1.91-0.85)/2.92=55.21%		57.00	58.92	1.92	5.00	Tr	5	3	41219 SP	127	
1/1.08=92.59%	(1-0.16)/1.08=77.78%		58.92	60.00	1.08	5.00	1.00	5	4	41220	286	
1.27/1.31=96.95%	(1.27-0.37)/1.31=68.70%		60.00	61.31	1.31	5.00	5.00	5	5	41221 SP,GN	799	
0.98/1.09=89.91%	(0.98-0.3)/1.09=62.39%		61.31	62.40	1.09	5.00	2.50	5	4	41222	38	
2.29/2.29=100%	(2.29-1.51)/2.29=34.06%		62.40	64.69	2.29	5.00	0.10	5	3	41223	80	
1.92/2.02=95.05%	(1.92-1.45)/2.02=23.27%		64.69	66.71	2.02	2.50	1.00	5	2	41224	61	
1.29/1.29=100%	(1.29-0.1)/1.29=92.25%		66.71	68.00	1.29	5.00	10.00	7	3	41225 SpGnCp,TT	1456	
1.11/1.28=86.72%	(1.11-0.42)/1.28=53.91%		68.00	69.28	1.28	2.50	1.00	6	7	41226 SP,GN	375	
0.86/0.86=100%	(0.86-0.78)/0.86=9.3%		69.28	70.14	0.86	2.50	1.00	5	2	41227	261	
1.90/1.86=102.15%	(1.90-1.32)/1.86=31.18%		70.14	72.00	1.86	2.50	0.10	4	2	41228	43	
2/2=100%	(2-1.51)/2=24.5%		72.00	74.00	2.00	2.50	1.00	4	3	41229	136	
2.35/2.45=95.92%	(2.35-1.74)/2.45=24.90M		74.00	76.45	2.45	2.50	1.00	5	2	41230	95	
0.94/1=94%	(10.94-0)/1=94%		76.45	77.45	1.00	5.00	1.00	8	10	41231 SP	181	
1.1/1.07=102.80%	1.1-0.32)/1.07=72.9%		77.45	78.52	1.07	5.00	2.50	8	3	41232	617	
2.06/2.06=100%	(2.06-1.47)/2.06=28.64%		78.52	80.58	2.06	Tr	0.30	3	3	41233	40	
2.98/3=99.33%	(2.98-2.67)/3=10.33%		80.58	83.58	3.00	0.10	1.00	3	2	41234	13	
3.02/3.05=99.02%	3.02-2.87)/3.05=4.92%		83.58	86.63	3.05	Tr	Tr	3	2	41235	-5	
3.43/3.37=101.78%	(3.43-2.85)/3.37=17.21%		86.63	90.00	3.37	Tr	0.10	3	2	41236	12	
2.97/3=99%	(2.97-2.8)/3=5.67%		90.00	93.00	3.00	Tr	0.10	3	2	41237	-5	
2/2=100%	(2-1.36)/2=32%		93.00	95.00	2.00	Tr	0.10	3	2	41238	-5	
2.73/2.8=97.5%	(2.73-1.91)/2.8=29.29%		95.00	97.80	2.80	Tr	0.30	3	2	41239	-5	
2.17/2.23=97.31%	(2.17-0.58)/2.23=71.3%		97.80	100.30	2.50	0.30	0.30	3	3	41240	-5	
2.9/2.97=97.64%	(2.9-2.46)/2.97=11.81%		100.30	103.00	2.70	Tr	0.10	3	2	41241	-5	
2.92/3=94%	(2.92-1.68)/3=41.33%		103.00	106.00	3.00	Tr	0.10	3	3	41242	-5	
1.78/1.72=103.49%	(1.78-0.62)/1.72=67.44%		106.00	107.72	1.72	Tr	Tr	3	3	41243	179	
2.29/2.31=99.13%	(2.29-1.44)/2.31=36.80%		107.72	110.03	2.31	Tr	2.50	3	3	41244	-5	

Recovery	HOLE NUMBER	DDH 89-3						SAMPLE NUMBER	MET																
		R.G.D.	FROM	TO	WIDTH (m)	PY%	Vn%	A	F	ppb Au	GMT Au	GMT Au	ppm Ag	ppm As	ppm Cu	pct Fe	ppm Mn	ppm Mo	ppm Ni	ppm Pb	ppm Sb	ppm Zn	ppb Hg		
0.21/5.18=4.05%	(0.21)/5.18=4.05%		12.19	17.37	5.18	2.50	Tr	5	9	41245	67		1.1	45	-1	308	4.89	784	2	17	78	11	147	70	
1.17/1.17=100%	(1.17-0.13)/1.17=88.89%		17.37	19.07	1.70	2.50	Tr	5	4	41246	52		2.8	69	2	149	5.91	325	4	21	197	14	271	65	
1.98/1.38=100%	(1.98-0.27)/1.98=86.36%		19.07	21.05	1.98	1.00	Tr	5	5	41247	40		1.7	34	1	126	2.3	60	3	22	127	14	149	55	
2.20/2.20=100%	(2.2-1.57)/2.20=28.64%		21.05	23.25	2.20	2.50	0.10	5	2	41248	93		2.1	34	4	89	3.3	166	2	24	273	14	518	105	
2.43/2.75=88.36%	(2.43-0)/2.75=88.36%		23.25	26.00	2.75	2.50	Tr	8	9	41249	93		2.9	112	4	196	5.12	397	2	33	384	15	446	110	
1.96/2=98%	(1.96-1.43)/2=26.5%		26.00	28.00	2.00	2.50	Tr	5	3	41250	61		1.5	136	6	171	5.83	789	2	24	483	19	767	210	
2/2=100%	(2-1.3)/2=35%		28.00	30.00	2.00	2.50	1.00	5	2	41251	30		1	85	-1	90	3.62	1097	-1	23	127	15	120	65	
1.91/2=95.5%	(1.91-0.56)/2=62.5%		30.00	32.00	2.00	2.50	0.30	5	3	41252	22		1.2	92	6	57	5	1073	2	29	599	16	900	170	
2/2=100%	(2-1.34)/2=18%		32.00	34.00	2.00	2.50	0.30	5	3	41253	73		2.3	100	3	139	5.59	687	2	24	387	14	389	90	
1.88/2=94%	(1.88-1.08)/2=40%		34.00	36.00	2.00	2.50	0.30	6	3	41254	231	0.31	2.6	90	3	85	5.07	314	3	18	274	15	316	85	
1.86/2=93%	(1.86-0.55)/2=65.5%		36.00	38.00	2.00	2.50	1.00	5	3	41255	109		1.6	97	-1	37	6.01	420	3	7	38	13	29	55	
1.83/1.83=100%	(1.83-0.91)/1.83=50.27%		38.00	39.83	1.83	5.00	2.50	6	3	41256	204	0.24	1.5	115	-1	49	6.39	250	4	13	57	11	53	35	
1.01/1.17=91.45%	(1.07-0.76)/1.17=26.50%		39.83	41.00	1.17	10.00	5.00	6	2	41257 SP	697	0.96	3.9	93	9	402	7.16	608	2	7	472	17	1148	120	
0.75/0.76=98.68%	(0.75-0.59)/0.76=21.05%		41.00	41.76	0.76	5.00	1.00	6	2	41258	359	0.45	1.4	86	-1	23	7.23	623	3	12	47	14	52	35	
2.3/3.04=75.66%	(2.3-0.98)/3.04=43.42%		41.76	44.80	3.04	5.00	0.50	5	3	41259	51		0.5	79	-1	117	7.39	682	2	17	32	13	45	30	
1.93/2.07=93.24	(1.93-0.84)/2.07=52.66%		44.80	46.87	2.07	2.50	0.30	5	4	41260	90		1.2	134	-1	112	7.31	866	3	24	115	14	163	40	
1.13/1.13=100%	(1.13-0.14)/1.13=87.61%		46.87	48.00	1.13	5.00	2.50	8	9	41261	167	0.1	1.9	120	1	64	7.71	812	2	29	167	16	178	70	
2/2=100%	(2-1.59)/2=20.5%		48.00	50.00	2.00	2.50	0.30	5	2	41262 SP,GN	127		1.5	111	5	243	6.68	707	2	32	156	18	601	105	
1/1=100%	(1-0.44)/1=56%		50.00	51.00	1.00	1.00	1.00	4	3	41263	214	0.24	3.6	69	3	170	4.8	1085	2	25	325	18	379	130	
1/1=100%	(1-0.41)/1=59%		51.00	52.00	1.00	2.50	10.00	5	3	41264	50		0.9	73	-1	173	6.27	723	2	12	35	14	52	50	
1.4/1.7=82.35%	(1.4-0.44)/1.7=56.47%		52.00	53.70	1.70	1.00	0.10	5	3	41265	28		0.4	49	-1	159	4.66	946	-1	9	30	14	61	50	
0.98/1=98%	(53.7-0.42)/1=53.28%		53.70	54.70	1.00	5.00	2.50	5	3	41266	437	0.55	1.5	105	1	23	7.18	395	4	11	100	16	162	45	
1.35/1.48=91.22%	(1.35-0.45)/1.48=60.81%		54.70	56.18	1.48	2.50	2.50	5	4	41267	512	0.62	3.2	129	3	59	6.05	343	5	14	265	16	422	65	
1.76/1.82=96.70%	(1.76-0.74)/1.82=56.04%		56.18	58.00	1.82	2.50	0.30	5	3	41268	189	0.24	0.8	89	-1	25	6.17	693	3	13	299	17	61	20	
1.78/2=89%	(1.78-1.1)/2=34%		58.00	60.00	2.00	2.50	1.00	5	3	41269	455	0.51	1.5	121	-1	64	5.13	637	3	11	50	16	72	35	
2/2=100%	(2-0.71)/2=64.5%		60.00	62.00	2.00	2.50	2.50	5	3	41270	874	1.03	2.3	181	-1	107	6.5	449	3	15	71	18	58	35	
1.95/2=97.5%	(1.95-1.28)/2=35%		62.00	64.00	2.00	2.50	2.50	5	3	41271	146		1.1	74	-1	61	6.18	688	2	9	30	16	41	25	
2/2=100%	(2-1.4)/2=30%		64.00	66.00	2.00	2.50	0.30	5	2	41272	124		0.9	113	-1	45	5.29	596	2	9	28	18	36	25	
1.93/2=96.5%	(1.93-1.21)/2=36%		66.00	68.00	2.00	2.50	0.30	5	2	41273	334	0.38	3.5	145	-1	114	6.19	688	2	10	61	15	76	30	
2/2=100%	(2-1.62)/2=15.5%		68.00	70.00	2.00	1.00	2.50	4	2	41274 SP,GN	449	0.41	4.7	82	12	191	5.72	949	2	17	592	18	1609	225	
1.96/2=98%	(1.96-1.62)/2=17%		70.00	72.00	2.00	2.50	1.00	4	2	41275	37		1.9	61	-1	175	6.03	1126	2	31	52	13	70	70	
2/2=100%	(2-1.38)/2=31%		72.00	74.00	2.00	2.50	0.30	5	2	41276	21		0.7	61	-1	11	5.94	596	2	20	40	13	28	20	
0.59/0.64=92.19%	(0.59-0.59)/2=0%		74.00	74.64	0.64	2.50	20.00	6	1	41277	27		0.5	36	-1	6	4.53	278	2	11	37	13	7	25	
0.81/0.81=100%	(0.81-0.63)/0.81=22.22%		74.64	75.45	0.81	2.50	2.50	5	2	41278	80		0.5	55	-1	15	6.06	367	2	14	52	12	18	15	
1.23/1.23=100%	(1.23-0.43)/1.23=65.04%		75.45	76.68	1.23	10.00	2.50	6	4	41279 SP,GN	334	0.21	0.6	57	-1	18	7.31	487	2	10	420	12	15	15	
1.6/1.65=96.97%	(1.6-0.63)/1.65=58.79%		76.68	78.33	1.65	5.00	1.00	5	3	41280	48		0.5	48	-1	22	6.7	480	3	10	44	15	23	20	
1.35/1.36=99.26%	(1.35-1.2)/1.36=11.03%		78.33	79.69	1.36	5.00	0.10	6	1	41281	19		0.4	24	-1	12	6.46	710	2	10	15	-5	25	25	
1.49/1.49=100%	(1.49-1.12)/1.49=24.83%		79.69	81.18	1.49	2.50	0.10	5	2	41282	59		0.7	33	-1	43	4.67	651	2	11	17	-5	44	40	
1.36/1.34=101.49%	(1.36-0.88)/1.34=35.82%		81.18	82.52	1.34	2.50	2.50	6	3	41283	236	0.31	3.3	40	3	62	5.5	603	3	10	263	-5	417	65	
1.27/1.37=92.70%	(1.27-0.71)/1.37=40.88%		82.52	83.89	1.37	2.50	40.00	8	4	41284 SP,GN	2172	2.66	3.12	2.9	37	6	87	3.5	592	2	8	3287	7	775	110
0.56/0.54=103.70%	(0.56-0.2)/0.54=66.67%		83.89	84.43	0.54	2.50	5.00	6	3	41285	433	0.62	2.6	47	5	40	5.41	842	2	9	241	-5	630	120	
1.45/1.46=99.32%	(1.45-1.03)/1.46=28.77%		84.43	85.89	1.46	5.00	0.30	5	2	41286	54		2.1	68	1	90	6.42	1166	2	10	155	-5	230	65	
0.6/0.6=100%	(0.6-0.47)/0.6=21.67%		85.89	86.49	0.60	5.00	10.00	6	2	41287 SP	296	0.34	11.6	139	94	339	8.12	1122	2	12	1200	23	11270	950	
0.97/0.98=98.98%	(0.97-0.52)/0.98=45.92%		86.49	87.47	0.98	5.00	0.30	5	3	41288	324	0.21	2.5	80	2	33	6.32	928	2	11	164	-5	258	55	
0.72/0.72=100%	(0.72-0.5)/0.72=30.56%		87.47	88.19	0.72	2.50	2.50	6	3	41289 SP,GN	355	0.48	9.5	90	51	207	4.45	677	3	12	2807	14	6159	650	
1.32/1.38=95.65%	(1.32-1)/1.32=24.24%		88.19	89.57	1.38	2.50	0.30	5	2	41290 GN,SP	301	0.38	13.5	47	9	188	5.76	894	2	9	483	5	1119	180	
1/1.03=97.09%	(1-0.26)/1.03=71.84%		89.57	90.60	1.03	2.50	10.00	8	5	41291 SP,CP	1377	1.82	2.16	32.6	91	11	167	6	777	2	9	261	8	1332	245
1.26/1.22=103.29%	(1.26-0.66)/1.22=49.18%		90.60	91.82	1.22</td																				

Recovery	HOLE NUMBER R.Q.D.	DDH 89-3						SAMPLE (#)	MET																
		FROM	TO	WIDTH	PYZ	Vn%	A	F	ppb	GMT	GMT	GMT	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	ppm	ppm	ppb	ppb	ppb
0.67/0.94=71.28%	(0.67-0)/0.94=71.28%	98.72	99.66	0.94	5.00	0.00	9	9	41298	1245	1.38	1.41	29.8	115	10	263	8.36	263	3	11	315	7	1296	160	
1.54/1.54=100%	(1.54-0.34)/1.54=77.92%	99.66	101.20	1.54	2.50	5.00	9	3	41299	1046	1.01	1.13	17	105	49	266	3.29	304	4	7	1105	19	6106	600	
0.3/0.71=0.42, Z25	(0.3-0)/1.71=42.25%	101.20	101.91	0.71	2.50	0.00	7	10	41300	3306	2.48	3.5	42.9	50	104	26	278	6.56	633	5	8	1388	13	3213	400
0.9/.91=98.90%	(0.9-0.74)/0.91=17.58%	101.91	102.82	0.91	2.50	1.00	5	2	41301	148			1.8	64	-1	106	5.46	198	4	11	62	-5	107	95	
1.04/1.06=98.11%	(1.04-1)/1.06=3.77%	102.82	103.88	1.06	2.50	5.00	5	1	41302 SP	236		0.27	4.2	84	2	113	3.47	399	4	7	126	-5	312	75	
1.93/1.98=97.47%	(1.93-1.41)/1.98=26.26%	103.88	105.86	1.98	1.00	5.00	8	2	41303	401		0.48	4.1	46	2	98	2.8	333	6	10	166	-5	271	110	
0.22/0.23=95.65%	(0.22-0)/1.23=95.65%	105.86	106.09	0.23	2.50	0.00	10	10	41304	508		0.58	14.7	89	6	281	7.35	845	3	13	422	6	776	505	
2.25/3.03=74.26%	(2.25-0.44)/3.03=59.74%	106.09	109.12	3.03	2.50	2.50	5	6	41305	562		0.65	11.2	120	5	306	5.74	522	3	12	298	5	626	310	
2.57/2.99=85.95%	(2.57-0.84)/2.99=57.86%	109.12	112.11	2.99	1.00	0.30	4	4	41306	391		0.38	1.7	232	-1	133	5.54	797	3	28	23	6	99	110	
0.93/0.93=100%	(0.93-0.41)/0.93=55.91%	112.11	113.04	0.93	1.00	0.30	4	3	41307	40			2	70	-1	142	2.43	456	3	15	16	8	59	90	
1.76/1.74=101.15%	(1.76-1.38)/1.74=21.84%	113.04	114.78	1.74	Tr	0.30	4	2	41308	178		0.17	2.1	64	-1	146	4.8	657	3	18	15	-5	56	60	
0.71/0.71=100%	(10.71-0.54)/0.71=23.94%	114.78	115.61	0.83	5.00	40.00	9	2	41309	1633		1.58	9.6	642	8	111	6.22	293	14	27	431	19	927	310	
2.24/2.34=95.73%	(2.24-1.83)/2.34=21.79%	115.61	117.95	2.34	0.30	0.30	3	2	41310	32			0.6	63	-1	152	5.79	791	1	29	14	11	72	170	
2.97/3.05=97.37%	(2.97-2)/3.05=31.80%	117.95	121.00	3.05	Tr	0.30	4	2	41311	8			0.2	39	-1	92	6.62	1542	2	29	4	8	74	290	
3.01/3.05=98.69%	(3.01-2.46)/3.05=18.03%	121.00	124.05	3.05	Tr	0.30	4	2	41312	5			0.2	40	-1	94	6.38	1358	2	37	9	7	76	140	
3/3.05=98.36%	(3-2.28)/3.05=23.61%	124.05	127.10	3.05	Tr	0.30	4	2	41313	7			0.3	38	-1	103	7.16	1418	2	36	6	9	80	80	
2.91/3.04=95.72%	(2.91-2.27)/3.04=21.05%	127.10	130.14	3.04	0.30	0.10	4	2	41314	10			0.7	77	-1	147	8.22	1510	2	39	12	12	111	495	

HOLE NUMBER	DDH 89-4									SAMPLE	MET
RECOVERY %	R.G.D. %	FROM	TO	WIDTH (m)	PY%	Vn%	A	F	NUMBER	ppb	GMT
										Au	Au
1.68/3.04=55.26%	(1.68-0)/3.04=55.26%	11.28	14.32	3.04	2.50	1.00	7	8	41315	53	
1.67/1.68=99.40%	(1.67-0.18)/1.68=88.69%	14.32	16.00	1.68	2.50	0.10	7	7	41316	59	
2/2=100%	(2-0.1)/2=95%	16.00	18.00	2.00	2.50	0.30	6	6	41317	41	
1.3/1.5=86.67%	(1.3-0)/1.5=86.67%	18.00	19.50	1.50	2.50	0.00	6	8	41318	12	
1.32/1.33=99.25%	(1.32-0.7)/1.33=46.62%	19.50	20.83	1.33	5.00	0.00	5	3	41319	65	
1.35/1.33=101.50%	(1.35-0.21)/1.33=85.71%	20.83	22.16	1.33	2.50	5.00	9	7	41320 SP	428	0.55
0.77/0.77=100%	(0.77-0.41)/0.77=46.75%	22.16	22.93	0.77	1.00	30.00	9	3	41321 SpGnCpTT	2521	2.78
2.07/2.07=100%	(2.07-1.11)/2.07=46.38%	22.93	25.00	2.07	2.50	5.00	6	3	41322 SP	107	
2.25/2.27=99.12%	(2.25-1.32)/2.27=40.97%	25.00	27.27	2.27	2.50	2.50	6	3	41323	172	0.17
0.8/0.8=100%	(0.8-0.59)/0.8=26.25%	27.27	28.07	0.80	1.00	30.00	9	2	41324 SP,GN,TT	436	0.51
1.01/1.14=86.32%	(1.01-0.14)/1.14=76.32%	28.07	29.21	1.14	2.50	1.00	6	5	41325 SP	80	
2.07/2.18=94.95%	(2.07-1)/2.18=49.08%	29.21	31.39	2.18	5.00	0.30	5	4	41326	62	
1.49/1.61=92.54%	(1.49-1.04)/1.61=27.95%	31.39	33.00	1.61	5.00	0.30	5	3	41327	26	
2.02/2=101%	(2.02-1.3)/2=0.36%	33.00	35.00	2.00	5.00	0.10	5	2	41328	89	
1.97/2=98.5%	(1.97-0.65)/2=66%	35.00	37.00	2.00	5.00	0.30	5	3	41329	221	0.27
1.48/1.55=94.58%	(1.48-0.72)/1.55=49.03%	37.00	38.55	1.55	2.50	0.30	5	3	41330	174	0.17
0.57/0.58=98.28%	(0.57-0.1)/0.58=81.03%	38.55	39.13	0.58	2.50	30.00	8	4	41331 SP,GN	1870	2.02
1.85/1.87=98.93%	(1.85-0.72)/1.87=41.71%	39.13	41.00	1.87	2.50	0.30	5	3	41332 SP,GN	161	0.24
1.96/2=98%	(1.96-1.11)/2=42.5%	41.00	43.00	2.00	2.50	0.30	4	3	41333 SP,GN	172	0.17
1.96/2=98%	(1.96-1.18)/2=39%	43.00	45.00	2.00	2.50	0.30	4	2	41334	180	0.17
1.96/2=98%	(1.96-1.9)/2=3%	45.00	47.00	2.00	2.50	Tr	4	1	41335	96	
2/2=100%	(2-1.31)/2=34.5%	47.00	49.00	2.00	2.50	1.00	4	2	41336 SP	120	
2.03/2=101.5%	(2.03-1.2)/2=41.5%	49.00	51.00	2.00	2.50	0.30	4	3	41337	51	
2.64/2.67=98.88%	(2.64-0.88)/2.67=65.92%	51.00	53.67	2.67	0.30	0.30	4	3	41338	55	
0.92/0.94=97.87%	(0.92-0.6)/0.94=34.04%	53.67	54.61	0.94	1.00	5.00	4	3	41339 SpGnCpTT	10000	64.46 77.2%
1.83/2.02=90.59%	(1.83-1.24)/2.02=29.21%	54.61	56.63	2.02	1.00	0.30	4	3	41340	142	
1.43/1.4=1.02%	(1.43-0.32)/1.4=79.29%	56.63	58.03	1.40	2.50	1.00	6	5	41341 GN,SP	245	0.31
1.81/1.97=91.88%	(1.81-1.13)/1.97=34.52%	58.03	60.00	1.97	2.50	0.30	6	3	41342 SP	153	0.14
2.05/2=102.5%	(2.05-1.61)/2=22%	60.00	62.00	2.00	2.50	1.00	5	2	41343	102	
2.44/2.666=91.73%	(2.44-0.35)/2.66=78.57%	62.00	64.66	2.66	1.00	2.50	4	3	41344 SP	337	0.48
1.3/1.44=90.28%	1.3-1.05)/1.44=17.36%	64.66	65.90	1.24	2.50	1.00	5	2	41345 SP	1163	1.23 1.3%
0.35/0.35=100%	(0.35-0.26)/0.35=25.71%	65.90	66.25	0.35	1.00	70.00	9	2	41346 SpGnCpTT	5393	6.48 4.65
1/1=100%	(1-0.89)/1=11%	66.25	67.25	1.00	2.50	5.00	5	2	41347 SpGnCp	990	1.1 1.28
1.4/1.4=100%	(1.4-1.18)/1.4=15.71%	67.25	68.65	1.40	2.50	2.50	5	2	41348 SpGnTT	10000	19.61 15.52
1.8/2.04=88.24%	(1.8-0)/2.4=88.24%	68.65	70.69	2.04	5.00	0.30	8	9	41349 SP,GN	1550	1.85 1.26
1.43/1.54=92.86%	(1.43-0.63)/1.54=51.95%	70.69	72.23	1.54	2.50	Tr	5	3	41350	127	
1.05/1.08=97.22%	(1.05-0.31)/1.08=68.52%	72.23	73.31	1.08	2.50	2.50	6	4	41351	106	
0.52/0.52=100%	(0.52-0.2)/0.52=61.54%	73.31	73.83	0.52	2.50	2.50	8	3	41352 20ZSpGnCp	1233	1.3
1.16/1.17=99.15%	(1.16-0)/1.17=99.15%	73.83	75.00	1.17	5.00	0.30	8	7	41353	122	
2/2=100%	(2-0.68)/2=66%	75.00	77.00	2.00	5.00	0.30	6	3	41354	38	
1/1=100%	(1-0.47)/1=53%	77.00	78.00	1.00	5.00	0.00	6	3	41355	103	
1/1=100%	(1-0.65)/1=35%	78.00	79.00	1.00	5.00	1.00	6	2	41356 SP	3448	3.53
1/1=100%	(1-0.61)/1=39%	79.00	80.00	1.00	5.00	0.30	6	2	41357	173	0.21
1.79/2=89.5%	(1.78-1.25)/2=27%	80.00	82.00	2.00	5.00	0.10	6	2	41358	79	
2.43/2.43=100%	(2.43-1.33)/2.43=45.27%	82.00	84.43	2.43	5.00	0.10	5	4	41359	159	0.14
1.03/1.03=100%	(1.03-0.51)/1.03=50.49%	84.43	85.46	1.03	5.00	0.30	6	4	41360 SP,GN	73	
0.74/1=74%	(0.74-0.1)/1=64%	85.46	86.46	1.00	2.50	Tr	7	6	41361	46	
2.45/2.54=96.46%	(2.45-1.02)/2.54=56.30%	86.46	89.00	2.54	2.50	1.00	6	3	41362	37	
1.75/1.76=99.43%	(1.75-0.74)/1.76=57.39%	89.00	90.76	1.76	2.50	0.30	6	3	41363	33	
0.92/1.68=54.76%	(0.92-0.37)/1.68=32.74%	90.76	92.44	1.68	0.30	1.00	2	3	41364	469	0.48
2.53/2.56=98.83%	(2.53-1.9)/2.56=24.61%	92.44	95.00	2.56	2.50	2.50	4	2	41365	75	
3.09/3=103%	(3.09-1.51)/3=49.67%	95.00	98.00	3.00	Tr	1.00	4	3	41366	84	
3/3=100%	(3-2.48)/3=17.33%	98.00	101.00	3.00	2.50	2.50	4	2	41367	30	

HOLE NUMBER	DDH 89-4							SAMPLE		MET	
RECOVERY %	R.Q.D. %	FROM	TO	WIDTH (m)	PY%	Vn%	A	F	NUMBER	ppb	GMT
										Au	Au
2.82/2.95=95.59%	(2.82-1.88)/2.95=31.86%	101.00	103.95	2.95	0.30	1.00	4	3	41368	16	
2.29/2.29=100%	(2.29-1.49)/2.29=34.93%	103.95	106.24	2.29	Tr	10.00	4	3	41369	78	
1.88/1.88=100%	(1.88-1.74)/1.88=7.44%	106.24	108.12	1.88	0.10	2.50	4	2	41370	22	
2.87/2.79=102.87%	(2.87-2.36)/2.79=18.28%	108.12	110.91	2.79	Tr	0.10	4	2	41371	14	
1.86/1.93=96.37%	(1.86-1.11)/1.93=38.86%	110.91	112.74	1.83	0.10	2.50	4	3	41372	17	
3.05/3.26=93.56%	(3.05-0.85)/3.26=67.48%	112.74	116.00	3.26	Tr	0.10	4	5	41373	30	
1.12/2=56%	(1.12-0.33)/2=39.5%	116.00	118.00	2.00	2.50	0.30	4	6	41374 SP	265	0.27
2.23/3.91=57.03%	(2.23-0.21)/3.91=51.66%	118.00	121.91	3.91	0.10	0.10	3	7	41375	534	0.48

HOLE NUMBER	DDH 89-5	RECOVERY	R.Q.D.	FROM	TO	WIDTH	PY%	VN%	A	F	SAMPLE	MET																
												(a)	ppb	GMT	GMT	GMT	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppb	
												Au	Au	Au	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn	Hg
2.35/2.77=84.84%	(2.35-0.76)/2.77=57.4%	8.23	11.00	2.77	5.00	0.10	6	5	41376		12				0.4	58	-1	121	5.47	1060	3	17	-2	-5	33	45		
1.78/1.79=99.44%	(1.78-0.61)/1.79=65.36%	11.00	12.79	1.79	5.00	Tr	6	3	41377		20				0.7	84	-1	132	6.3	956	3	20	41	-5	104	50		
1.27/1.53=83.01%	(1.27-0)/1.53=83.01%	12.79	14.32	1.53	2.50	0.00	10	10	41378		70				1.7	81	2	123	5.33	945	3	18	176	-5	315	90		
2.28/3.05=74.75%	(2.28-0)/3.05=74.75%	14.32	17.37	3.05	2.50	Tr	9	10	41379		95				2.7	87	3	263	5.95	583	3	22	225	-5	413	95		
0.93/1=93%	(0.93-0)/1=93%	17.37	18.37	1.00	2.50	Tr	10	10	41380		1398		1.92		25.9	77	14	83	5.28	777	3	20	2001	10	1573	200		
1.15/2.05=56.10%	(1.15-0)/2.05=56.15%	18.37	20.42	2.05	2.50	Tr	6	8	41381		36				0.5	29	-1	10	5.4	1060	1	11	19	-5	63	40		
2.30/3.05=65.57%	(2.3-0.13)/3.05=71.14%	20.42	23.47	3.05	2.50	Tr	6	7	41382		31				0.5	33	-1	36	5.55	1025	2	7	70	-5	168	50		
2.17/2.17=100%	(2.17-0.94)/2.17=56.68%	23.47	25.64	2.17	2.50	0.10	6	4	41383		47				0.5	41	-1	98	5.36	986	2	10	36	-5	100	55		
1.12/1.13=99.12%	(1.12-0)/1.13=99.12%	25.64	26.77	1.13	2.50	0.30	7	8	41384		33				1.1	34	-1	68	5.28	783	2	9	7	-5	80	40		
0.74/0.75=98.67%	(0.74-0.13)/0.75=81.33%	26.77	27.52	0.75	5.00	0.30	7	8	41385		79				1.5	55	-1	121	4.49	1381	1	9	42	-5	187	75		
2.32/2.38=97.48%	(2.32-0.78)/2.38=64.71%	27.52	29.90	2.38	2.50	0.30	6	4	41386		65				1	57	-1	124	5.07	1343	2	10	55	-5	175	55		
0.75/1.48=50.68%	(0.75-0.14)/1.48=41.22%	29.90	30.68	0.78	2.50	1.00	7	6	41387		152		0.17		2.6	81	4	146	5.75	1187	1	10	254	-5	555	110		
0.45/0.47=95.74%	(0.45-0)/0.47=95.74%	30.68	31.15	0.47	2.50	2.50	8	9	41388	SP,GN	837		0.82		20.5	123	109	866	4.68	808	1	10	8642	23	12811	1900		
0.38/1.46=26.03%	(31.15-0)/1.46=26.03%	31.15	32.61	1.46	2.50	2.50	7	9	41389		252		0.41		2.2	41	3	51	3.58	1060	1	7	776	-5	429	70		
1.32/1.37=96.35%	(1.32-0.39)/1.37=67.88	32.61	33.98	1.37	5.00	5.00	7	4	41390	SP	359		0.41		3.9	89	11	106	4.47	934	2	5	864	-5	1438	310		
1.18/1.68=70.24%	(1.18-0)/1.68=70.24%	33.98	35.66	1.68	2.50	5.00	7	6	41391	SP, GN	5657		5.11	114.9	50	63	88	323	4.36	2759	1	8	3174	15	10019	2150		
0.47/0.47=100%	(0.47-0)/0.47=100%	35.66	36.13	0.47	5.00	5.00	7	7	41392		304		0.45		2	68	-1	16	5.92	855	2	12	40	-5	318	115		
0.98/0.98=100%	(0.87-0.23)/0.98=76.53%	36.13	37.11	0.98	5.00	1.00	6	4	41393		193		0.21		1.5	86	-1	17	6.35	928	2	16	34	-5	138	35		
1.06/1.06=100%	(1.06-0.25)/1.06=76.42%	37.11	38.17	1.06	5.00	0.10	5	3	41394		58		0.8		34	-1	40	5.66	1093	3	28	19	-5	95	30			
0.54/0.58=92.10%	(0.54-0)/0.58=93.10%	38.17	38.75	0.58	2.50	70.00	9	5	41395	10%5pCpGn	2627		2.43		42.5	87	152	1526	4.33	3174	2	8	10000	1.31	89	17858	1950	
0.73/0.73=100%	(0.73-0.5)/0.73=31.51%	38.75	39.48	0.73	1.00	70.00	9	2	41396		2496		2.88		6.3	96	3	114	3.48	4955	1	5	343	-5	484	190		
0.27/0.27=100%	(0.27-0.27)/0.27=0%	39.48	39.75	0.27	1.00	80.00	9	1	41397	SP, GN	1548		1.68		24.1	102	161	668	4.28	5915	-1	8	9101	35	18664	2450		
0.98/0.99=98.99%	(0.98-0.27)/0.99=71.72%	39.75	40.74	0.99	5.00	2.50	5	3	41398	GN, SP	507		0.58		19.6	119	7	92	6.88	1835	3	34	4052	-5	904	210		
1.28/1.26=101.59%	(1.28-0.74)/1.26=42.86%	40.74	42.00	1.26	5.00	0.30	5	3	41399		107				1.7	68	-1	22	7.09	1525	2	33	107	-5	146	60		
1.93/2=96.5%	(1.93-0.66)/2=63.5%	42.00	44.00	2.00	2.50	0.10	5	3	41400		401		0.41		1.3	50	-1	74	6.33	1073	3	31	75	-5	121	30		
1/1=100%	(1-0.8)/1=20%	44.00	45.00	1.00	2.50	2.50	5	2	41401	SP, GN	388		0.38		7.2	89	40	258	5.87	1467	2	28	2446	5	4761	270		
2/2=100%	(2-0.66)/2=67%	45.00	47.00	2.00	2.50	2.50	4	3	41402		91				0.7	99	-1	144	6.49	1674	1	30	12	-5	82	40		
2/2=100%	(2-1.26)/2=37%	47.00	49.00	2.00	Tr	0.30	3	2	41403		39				1.3	74	-1	227	7.2	1381	4	35	-2	-5	66	105		
1.97/2=98.5%	(1.97-1.24)/2=36.5%	49.00	51.00	2.00	2.50	1.00	5	3	41404		78				0.6	40	-1	123	7.01	1088	3	27	-2	-5	37	35		
2.09/2=104.5%	(2.09-0.44)/2=82.5%	51.00	53.00	2.00	2.50	Tr	6	4	41405		147				0.3	47	-1	12	4.91	842	3	20	-2	-5	45	25		
2/2=100%	(2-1.31)/2=34.5%	53.00	55.00	2.00	5.00	0.30	5	3	41406		29				-0.2	15	-1	10	6.01	925	2	14	-2	-5	38	20		
1.89/2=94.5%	(1.89-1.5)/2=19.5%	55.00	57.00	2.00	2.50	0.10	5	2	41407		58				0.2	44	-1	58	8.77	841	2	13	-2	-5	51	30		
2/2=100%	(2-1.28)/2=36%	57.00	59.00	2.00	2.50	0.10	5	3	41408		41				0.3	15	-1	29	6.32	960	2	9	25	-5	68	35		
2.47/2.49=99.20%	(2.47-1.28)/2.49=17.79%	59.00	61.49	2.49	2.50	Tr	5	3	41409		53				2	19	2	32	6.61	757	2	11	144	-5	218	30		
1.11/1.11=100%	(1.11-0.63)/1.22=43.24%	61.49	62.60	1.11	5.00	30.00	6	3	41410	SpTT,CpGn	1115		1.06	52.5	50	101	265	4119	6.92	748	6	5	10000	1.54	66	20000	2.92	750
1.2/1.4=85.71%	(1.2-0.51)/1.4=49.29%	62.60	64.00	1.40	5.00	0.30	6	4	41411		49				1.6	20	1	20	7.33	688	3	10	75	-5	165	20		
1.92/2=96%	(1.92-0.98)/2=47%	64.00	66.00	2.00	2.50	0.30	5	3	41412		434		0.58		1.6	34	-1	24	7.71	678	5	9	47	-5	133	25		
2/2=100%	(2-0.9)/2=55%	66.00	68.00	2.00	2.50	0.10	5	3	41413		135				1.3	26	-1	11	6.18	728	3	10	73	-5	49	30		
1.99/2=99.5%	(1.99-1.08)/2=45%	68.00	70.00	2.00	5.00	0.00	5	3	41414		43				1.1	18	3	19	7.48	782	4	10	145	-5	344	40		
2/2=100%	(2-0.84)/2=58%	70.00	72.00	2.00	5.00	0.00	6	4	41415		36				0.5	13	2	21	7.61	777	3	9	143	-5	233	45		
1.85/2=92.5%	(1.85-0.38)/2=73.5%	72.00	74.00	2.00	5.00	0.10	6	4	41416		34				0.5	20	-1	24	6.47	714	3	10	18	-5	58	25		
1.99/2=99.5%	(1.99-1.1)/2=44.5%	74.00	76.00	2.00	2.50	0.30	5	3	41417		130				0.7	40	-1	55	6.69	773	3	10	-2	-5	39	20		
1.07/1.05=101.9%	(1.07-0.69)/1.05=36.19%	76.00	77.05	1.05	2.50	5.00	6	3	41418		1304		1.71		1.3	33	2	15	4.62	477	3	9	82	-5	274	40		
1.89/1.95=96.92%	(1.89-1.1)/1.95=40.51%	77.05	79.00	1.95	2.50	0.30	5	3	41419		230		0.27		1.2	45	-1	22	6.1	774	4	11	10	-5	39	40		
2.34/2.3=101.74%	(2.34-1.																											

HOLE NUMBER	DDH 89-5																									
	RECOVERY	R.Q.D.	FROM	TO	WIDTH (m)	PY%	VN%	A	F NUMBER	SAMPLE	MET															
										ppb	gmt	gmt	gmt	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppm	pct	ppb
										Au	Au	Au	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn
0.92/0.99=92.93%	(0.92-0.47)/0.99=45.45%	89.00	89.99	0.99	2.50	1.00	6	2	41429	64				1.3	31	-1	41	6.38	1413	3	8	-2	-5	61	30	
1/1.01=99%	(1-0.3)/1.1=69.31%	89.99	91.00	1.01	5.00	2.50	6	3	41430 SP	282	0.31			2	17	3	336	5.82	1048	3	10	58	-5	394	150	
1/1=100%	(1-0)/1=100%	91.00	92.00	1.00	5.00	5.00	7	8	41431	162	0.17			3.7	58	2	52	7.79	1478	5	9	220	-5	285	90	
1.02/1.10=92%	(1.02-0.1)/1=92%	92.00	93.00	1.00	5.00	2.50	8	9	41432 SP	447	0.51			8	100	20	151	5.75	965	3	12	767	-5	2362	310	
1.27/1.35=94.07%	(1.27-0.52)/1.35=55.56%	93.00	94.35	1.35	5.00	0.30	7	5	41433	313	0.34			12.9	110	3	380	5.81	1011	3	9	270	-5	402	145	
0.41/0.41=100%	(0.41-0)/0.41=100%	94.35	94.76	0.41	2.50	2.50	9	10	41434 SP	688	0.72			16.5	61	59	245	6.42	708	5	11	1018	17	7402	1000	
0.48/0.48=100%	(0.48-0.12)/0.48=75%	94.76	95.24	0.48	5.00	20.00	9	9	41435 SpCpGn, TT	2636	2.98	161.5	50	107	418	4495	8.29	2256	5	14	1216	261	20000	4.84	4300	
0.61/1.04=58.65%	(0.61-0)/1.04=58.65%	95.24	96.28	1.04	5.00	1.00	8	10	41436	36				2.5	21	6	61	6.79	1656	3	10	52	-5	815	100	
1.21/1.39=87.05%	(1.21-0.26)/1.39=75.54%	96.28	97.67	1.39	5.00	2.50	7	8	41437 SP	2875	3.22	3.57		27.9	53	40	92	8.75	1266	3	9	496	5	5078	490	
0.73/0.73=100%	(0.73-0.42)/0.73=42.47%	97.67	98.40	0.73	5.00	2.50	7	3	41438	10000	27.99	17.59	456.7	50	144	195	1657	7.35	1651	7	7	2722	77	20000	2.31	5000
1/1=100%	(1-0.68)/1=32%	98.40	99.40	1.00	5.00	1.00	6	2	41439	186	0.31			5.1	99	3	126	6.3	1042	3	8	271	-5	390	240	
1.6/1.6=100%	(1.6-1.11)/1.6=30.63%	99.40	101.00	1.60	2.50	1.00	5	3	41440	47				1.7	39	-1	94	6.07	1105	3	7	-2	-5	83	130	
2/2=100%	(2-0.53)/2=73.5%	101.00	103.00	2.00	2.50	0.10	5	4	41441	20				0.6	41	-1	48	7.39	924	3	9	6	-5	70	50	
1.9/2=95%	(1.9-0.74)=58%	103.00	105.00	2.00	2.50	0.30	5	3	41442 SP	101				2.3	31	1	71	7.01	888	3	10	145	-5	213	475	
0.69/0.69=100%	(0.69-0.38)/0.69=44.92%	105.00	105.69	0.69	5.00	1.00	6	2	41443	33				0.8	44	-1	161	7.94	1085	3	10	8	-5	95	700	
0.59/0.61=96.72%	(0.59-0)/0.61=96.72%	105.69	106.30	0.61	5.00	1.00	7	8	41444 SP	38				2.4	26	9	143	6.78	943	3	10	509	-5	1053	1300	
1.19/1.21=98.35%	(1.19-0.58)/1.21=50.41%	106.30	107.51	1.21	5.00	2.50	6	3	41445 SP, GN	77				6.9	25	34	104	7.66	1069	3	8	3864	-5	3947	3200	
1.3/1.31=99.24%	(1.3-0.86)/1.31=33.59%	107.51	108.81	1.30	5.00	2.50	6	2	41446	33				1.7	11	5	110	7.49	1123	4	8	425	-5	634	580	
2.13/2.19=97.26%	(2.13-1.62)/2.19=23.29%	108.81	111.00	2.19	5.00	0.10	6	2	41447	20				0.8	13	-1	150	8.66	1037	4	9	114	-5	114	470	
1.98/2=99%	(1.98-0.65)/2=66.5%	111.00	113.00	2.00	5.00	0.30	6	3	41448	27				0.6	30	-1	117	8.17	1019	4	7	75	-5	109	545	
1.89/2=94.5%	(1.89-0.63)/2=63%	113.00	115.00	2.00	5.00	0.30	6	3	41449	53				1.8	47	9	163	6.35	818	3	8	731	-5	1213	1100	
2.3/2.6=88.46%	(2.3-0.59)/2.6=65.77%	115.00	117.60	2.60	5.00	0.30	6	5	41450	214	0.21			4.8	77	12	301	6.8	723	4	10	678	-5	1478	1900	
1.24/1.24=100%	(1.24-0.32)/1.24=74.19%	117.60	118.84	1.24	2.50	10.00	8	5	41451	5831	5.86	93.9	50	79	4	759	4.29	298	5	5	227	-5	440	1300		
1.32/1.49=88.59%	(1.32-0.1)/1.49=81.88%	118.84	120.33	1.49	1.00	90.00	10	4	41452	450	0.55			5	26	5	63	1.89	310	4	7	116	-5	732	150	
0.98/1=98%	(0.98-0.11)/0.98=78.57%	120.33	121.33	1.00	2.50	1.00	8	8	41453	132				6.3	13	2	460	4.45	347	9	31	119	-5	206	155	
1/1=100%	(1-0)/1=100%	121.33	122.33	1.00	2.50	0.10	9	10	41454	122				2.5	64	-1	32	7.08	776	3	9	44	-5	107	180	
0.98/1=98%	(0.98-0)/1=98%	122.33	123.33	1.00	2.50	0.30	9	10	41455	268	0.34			1.8	58	-1	108	4.71	1131	3	7	21	-5	93	155	
1/1=100%	(1-0)/1=100%	123.33	124.33	1.00	5.00	0.30	9	10	41456	138				1.4	84	-1	37	5.54	888	3	9	25	-5	116	225	
1.33/2.26=58.85%	(1.33-0)/2.26=58.85%	124.33	126.59	2.26	5.00	1.00	9	10	41457	123				3.5	87	3	83	6.67	963	4	12	107	-5	424	290	
0.9/0.92=97.83%	(0.9-0.34)/0.92=60.87%	126.59	127.51	0.92	5.00	0.30	6	3	41458	114				2.3	17	2	27	7.28	1123	3	10	23	-5	289	65	
0.37/1.5=24.67%	(0.37-0)/1.5=24.67%	127.51	129.01	1.50	5.00	5.00	6	9	41459	1016	1.13			19.8	32	156	139	5.74	2213	2	-1	1611	30	17150	1550	
1.13/1.13=100%	(1.13-0.54)/1.13=52.21%	129.01	130.14	1.13	5.00	0.30	6	3	41460	145				2.5	29	5	30	6.38	926	2	7	21	-5	693	175	
1.49/1.49=100%	(1.49-0.48)/1.49=67.79%	130.14	131.63	1.49	5.00	2.50	6	4	41461	424	0.48			6.2	54	6	42	7.4	1189	3	10	35	-5	687	150	
1.29/1.37=94.16%	(1.29-1.15)/1.37=10.22%	131.63	133.00	1.37	2.50	1.00	6	2	41462	72				1.7	30	-1	33	7.26	896	3	10	30	-5	167	80	
1.55/1.64=94.51%	(1.55-0.61)/1.64=57.32%	133.00	134.64	1.64	2.50	1.00	6	3	41463	39				0.8	17	-1	25	6.27	930	3	8	-2	-5	53	70	
1.79/1.82=98.35%	(1.79-1.23)/1.82=30.77%	134.64	136.46	1.82	2.50	1.00	6	2	41464	187	0.24			2.5	58	-1	114	5.98	756	3	10	171	-5	91	50	
2.41/2.48=97.18%	(2.41-1.56)/2.48=34.27%	136.46	138.94	2.48	1.00	1.00	6	2	41465	353	0.31			1.8	50	1	70	3.26	533	3	6	107	-5	183	30	
2.66/2.66=100%	(2.66-1.37)/2.66=48.5%	138.94	141.60	2.66	2.50	0.30	5	3	41466	25				0.3	21	-1	101	7.28	819	3	9	5	-5	47	160	
1.98/2=99%	(1.98-1.26)/2=36%	141.60	143.60	2.00	2.50	0.10	5	3	41467	65				1.1	39	-1	62	6.41	1029	3	9	4	-5	50	90	
2.85/2.88=98.96%	(2.85-1.28)/2.88=54.51%	143.60	146.48	2.88	2.50	1.00	5	3	41468	71				1.5	67	3	118	7.26	727	4	10	159	-5	507	275	
1.49/1.52=98.03%	(1.49-0.89)/1.52=39.47%	146.48	148.00	1.52	1.00	2.50	4	2	41469	117				3.5	64	-1	184	6.94	728	5	11	23	-5	91	240	
1.97/2=98.5%	(1.97-1.11)/2=43%	148.00	150.00	2.00	2.50	2.50	4	2	41470	GN,SP,CP	255	0.31			5.4	229	3	66	8	934	4	12	2910	-5	423	165
2.02/2=101%	(2.02-1.76)/2=13%	150.00	152.00	2.00	5.00	2.50	4	2	41471	210	0.24			1.5	242	1	83	7.49	554	6	9	53	-5	98	100	
1.5/1.55=96.77%	(1.5-1.39)/1.55=7.1%	152.00	153.55	1.55	5.00	1.00	4	1	41472	518	0.58			2.2	357	2	63	8.93	466	10	11	68	7	129	210	
2.42/2.45=98																										

HOLE NUMBER		DDH 89-6		SAMPLE						ppb Au	GMT Au	
RECOVERY	R.Q.D.	FROM	TO	WIDTH (m)	PYZ	VNZ	A	F	NUMBER			
1.44/1.44=100%	(1.44-0.22)/1.44=84.72%	12.88	14.32	1.44	2.50	0.00	8	9	41475	37		
1.66/1.68=98.81%	(1.66-0.6)/1.68=63.10%	14.32	16.00	1.68	2.50	1.00	6	4	41476	108		
1.37/1.37=100%	(1.37-0.86)/1.37=37.23%	16.00	17.37	1.37	2.50	20.00	7	3	41477	40		
1.34/1.35=99.26%	(1.34/0.12)/1.35=90.37%	17.37	18.72	1.35	2.50	0.00	9	9	41478	110		
2.21/2.28=96.93%	(2.21-1.2)/2.28=44.30%	18.72	21.00	2.28	2.50	1.00	6	3	41479	100		
2/2=100%	(2-0.88)/2=56%	21.00	23.00	2.00	2.50	2.50	6	3	41480	37		
1.92/2=96%	(1.92-1.28)/2=32%	23.00	25.00	2.00	2.50	0.30	6	3	41481	174	0.24	
2/2=100%	(2-1)/2=50%	25.00	27.00	2.00	2.50	Tr	6	3	41482	23		
2/2=100%	(2-0.81)/2=59.5%	27.00	29.00	2.00	2.50	Tr	6	3	41483	29		
2.39/2.39=100%	(2.39-1.95)/2.39=18.41%	29.00	31.39	2.39	2.50	0.10	6	2	41484	40		
1.37/1.61=85.09%	(1.37-0.56)/1.61=50.31%	31.39	33.00	1.61	5.00	Tr	6	3	41485	49		
1.27/2=63.5%	(1.27-0.34)/2=46.5%	33.00	35.00	2.00	5.00	Tr	6	4	41486	93		
1.98/2=99%	(1.98-0.62)/2=68%	35.00	37.00	2.00	2.50	0.30	6	3	41487	196	0.24	
2/2=100%	(2-0.96)/2=52%	37.00	39.00	2.00	2.50	1.00	6	3	41488	Tr, SP	159	0.21
1.74/2=87%	(1.74-0.21)/2=76.5%	39.00	41.00	2.00	5.00	1.00	7	5	41489	303	0.34	
2/2=100%	(2-0.1)/2=95%	41.00	43.00	2.00	2.50	0.30	9	8	41490	SP	147	
1.31/1.32=99%	(1.31-0)/1.32=99.24%	43.00	44.32	1.32	5.00	2.50	9	8	41491	69		
1.65/1.68=98.21%	(1.65-0.4)/1.68=74.4%	44.32	46.00	1.68	1.00	0.30	4	3	41492	101		
1.95/2=97.5%	(1.95-0.97)/2=49%	46.00	48.00	2.00	2.50	0.10	4	3	41493	30		
2.35/2.9=81.03%	(2.35-1.03)/2.9=45.52%	48.00	50.90	2.90	2.50	0.10	4	3	41494	127		
2.08/2.1=99.05%	(2.08-1.67)/2.1=19.52%	50.90	53.00	2.10	2.50	0.10	5	2	41495	Tr, SP	19	
2.2/2=100%	(2-1.12)/2=44%	53.00	55.00	2.00	2.50	0.10	5	3	41496	11		
1.72/1.72=100%	(1.72-1.08)/1.72=37.21%	55.00	56.72	1.72	2.50	0.10	5	2	41497	26		
1.12/1.12=100%	(1.12-0.29)/1.12=74.11%	56.72	57.84	1.12	2.50	0.10	5	4	41498	42		
0.17/1.04=16.34%	(0.17-0)/1.04=16.34%	57.84	58.88	1.04	0.25	5.00	6	10	41499	GnSpCPTT	1342	1.27
0.22/0.22=100%	(0.22-0)/0.22=100%	58.88	59.10	0.22	2.50	90.00	6	3	41500	GnSpCPTT	431	0.62
0.9/0.9=100%	(0.9-0.32)/0.9=64.44%	59.10	60.00	0.90	2.50	1.00	6	3	41501	56		
1.92/2=96%	(1.92-0.31)=80.5%	60.00	62.00	2.00	5.00	5.00	6	3	41502	28		
2/2=100%	(2-0.77)/2=61.5%	62.00	64.00	2.00	2.50	1.00	6	3	41503	30		
1.91/2=95.5%	(1.91-0.91)/2=50%	64.00	65.00	2.00	2.50	0.10	5	3	41504	31		
1.93/2=96.5%	(1.93-0.37)/2=78%	66.00	68.00	2.00	2.50	0.10	6	4	41505	47		
1.96/2=98%	(1.96-0.6)/2=68%	68.00	70.00	2.00	2.50	0.30	6	6	41506	29		
1.89/2=94.5%	(1.89-0)/2=94.5%	70.00	72.00	2.00	2.50	0.10	5	8	41507	47		
2/2=100%	(2-0.23)/2=88.5%	72.00	74.00	2.00	2.50	1.00	6	7	41508	SP	103	
1.55/2=77.5%	(1.55-0.19)/2=68%	74.00	76.00	2.00	2.50	0.00	6	6	41509	27		
1.23/2=61.5%	(1.23-0)/2=61.5%	76.00	78.00	2.00	2.50	1.00	6	9	41510	53		
3.12/3.38=98.11%	(3.12-0.48)/3.38=78.11%	78.00	81.38	3.38	2.50	0.30	6	9	41511	135		
2.43/2.62=92.75%	(2.43-0.51)/2.62=73.28%	81.38	84.00	2.62	2.50	1.00	4	5	41512	104		
2.05/2.86=71.68%	(2.05-0)/2.86=71.68%	84.00	86.86	2.86	0.30	0.10	4	4	41513	67		
2.18/2.14=101.87%	(2.18-1.38)/2.14=37.37%	86.86	89.00	2.14	1.00	0.30	3	2	41514	65		
2/2=100%	(2-1.39)/2=30.5%	89.00	91.00	2.00	2.50	2.50	3	2	41515	94		
2.05/2=102.5%	(2.05-1.19)/2=43%	91.00	93.00	2.00	0.30	0.30	3	3	41516	19		
3.08/3=102.67%	(3.08-1.46)/3=54%	93.00	96.00	3.00	0.10	0.30	3	3	41517	27		
3/3=100%	(3-1.89)/3=37%	96.00	99.00	3.00	0.10	2.50	3	3	41518	16		
2.97/3=99%	(2.97-2.52)/3=15%	99.00	102.00	3.00	0.10	2.50	3	2	41519	79		
2.78/3=92.67%	(2.78-1.83)/3=31.67%	102.00	105.00	3.00	Tr	1.00	3	3	41520	7		
2.65/3.81=69.55%	(2.65-1.06)/3.81=41.73%	105.00	108.81	3.81	0.10	3.00	3	4	41521	46		
2.15/3.05=70.49%	(2.15-1.05)/3.05=36.07%	108.81	111.86	3.05	0.10	0.10	3	3	41522	2		

HOLE NUMBER		DDH 89-7			SAMPLE						MET		
RECOVERY	R.Q.D.	FROM	TO	WIDTH (m)	PYZ	VNZ	A	F NUMBER	ppb	GMT	GMT		
									Au	Au	Au		
1.81/1.84=98.37%	(1.81-0.86)/1.84=51.63%	10.32	12.16	1.84	5.00	2.50	6	3 41523	111				
0.68/0.68=100%	(0.68-0)/0.68=100%	12.16	12.84	0.68	2.50	0.30	9	10 41524 SP, GN, CP	272	0.31			
0.88/1=88%	(0.88)/1=74.14%	12.84	13.84	1.00	1.00	Tr	7	6 41525	172	0.21			
1.16/1.16=100%	(1.16-0.3)/1.16=74.14%	13.84	15.00	1.16	1.00	Tr	7	5 41526 SP	48				
2.02/2=101%	(2.02-0.4)/2=81%	15.00	17.00	2.00	2.50	1.00	8	8 41527	44				
1.95/2=97.5%	(1.95-0.1)/2=92.5%	17.00	19.00	2.00	2.50	2.50	9	10 41528	95				
1/1.02=98.04%	(1-0)/1.02=98.04%	19.00	20.02	1.02	5.00	2.50	9	9 41529	95				
1.66/1.67=99.4%	(1.66-0.56)/1.67=67.87%	20.02	21.69	1.67	5.00	1.00	6	3 41530	159	0.17			
2.14/2.09=102.39%	(2.14-1.06)/2.09=51.67%	21.69	23.78	2.09	5.00	0.10	7	3 41531	98				
0.74/0.75=98.67%	(0.74-0.49)/0.25=33.33%	23.78	24.53	0.75	5.00	30.00	7	2 41532	265	0.17			
2.05/1.99=103.02%	(2.05-1.22)/1.99=41.71%	24.53	26.52	1.99	5.00	2.50	7	3 41533	93				
1/1=100%	(1-0.7)/1=30%	26.52	27.52	1.00	5.00	0.30	7	3 41534 SP	80				
1.9/2.04=93.14%	(1.9-1.32)/2.04=28.43%	27.52	29.56	2.04	5.00	0.10	7	2 41535	155	0.21			
1.76/1.83=96.17%	(1.76-0.72)/1.83=56.83%	29.56	31.39	1.83	5.00	0.30	7	3 41536	81				
1.93/2.09=92.34%	(1.93-1.38)/2.09=26.32%	31.39	33.48	2.09	5.00	5.00	7	3 41537	311	0.34			
0.75/0.75=100%	(0.75-0.49)/0.75=34.67%	33.48	34.23	0.75	10.00	5.00	7	2 41538 SP	2516	3.46			
0.96/1.05=91.43%	(0.96-0.73)/1.05=21.9%	34.23	35.28	1.05	10.00	1.00	7	3 41539	759	0.96			
2.62/2.78=94.24%	(2.62-2.05)/2.78=27.70%	35.28	38.06	2.78	0.30	0.10	4	2 41540	72				
1.25/1.25=100%	(1.25-0.33)/1.25=73.6%	38.06	39.31	1.25	2.50	2.50	5	5 41541	113				
2.17/2.26=96.02%	(2.17-1.2)/2.26=42.9%	39.31	41.57	2.26	2.50	20.00	8	3 41542 SP	182	0.24			
1.43/1.43=100%	(1.43-0.25)/1.43=82.52%	41.57	43.00	1.43	2.50	1.00	7	3 41543	100				
1.93/2=96.5%	(1.93-0.77)/2=58%	43.00	45.00	2.00	2.50	0.30	6	4 41544	148				
1.86/1.91=97.38%	(1.86-0.34)/1.91=79.58%	45.00	46.91	1.91	2.50	0.10	7	7 41545	97				
0.64/0.65=98.46%	(0.64-0.36)/0.65=43.08%	46.91	47.56	0.65	1.00	20.00	6	3 41546	1035	1.17	1.42		
0.31/0.31=100%	(0.31-0.12)/0.31=61.29%	47.56	47.87	0.31	2.50	5.00	6	3 41547 SpGnCpTT	10000	12.75	15.77		
0.97/0.97=100%	(0.97-0.18)/0.97=81.44%	47.87	48.84	0.97	2.50	0.00	6	6 41548	1272	1.37	1.3		
2.26/2.56=88.28%	(2.26-0.31)/2.56=76.17%	48.84	51.40	2.56	2.50	0.30	6	6 41549	65				
2.38/2.6=91.54%	(2.38-1.38)/2.6=38.46%	51.40	54.00	2.60	2.50	0.10	4	3 41550	132				
1.33/2=66.5%	(1.33-0.3)/2=51%	54.00	56.00	2.00	2.50	0.10	4	5 41551	42				
2/2=100%	(2-0.76)/2=62%	56.00	59.00	2.00	2.50	Tr	4	3 41552	41				
2/2=100%	(2-1.14)/2=43%	58.00	60.00	2.00	1.00	0.30	4	2 41553	48				
2.99/3=99.67%	(2.99-1.16)/3=61%	60.00	63.00	3.00	2.50	0.30	4	3 41554	201	0.27			
2.8/3=93.33%	(2.8-1.04)/3=58.67%	63.00	66.00	3.00	2.50	0.30	4	5 41555	48				
2.89/3=96.33%	(2.89-1.54)/3=45%	66.00	69.00	3.00	2.50	0.10	4	4 41556	74				
2.79/3=93%	(2.79-1.84)/3=38.67%	69.00	72.00	3.00	1.00	0.30	4	2 41557	33				
2.92/3=97.33%	(2.92-1.53)/3=46.33%	72.00	75.00	3.00	2.50	0.30	4	3 41558	773	0.99			
2/2=100%	(2-1.34)/2=33%	75.00	77.00	2.00	2.50	1.00	5	2 41559	290	0.27			
2/2=100%	(2-1.77)/2=16.5%	77.00	79.00	2.00	2.50	0.30	5	2 41560	87				
1/1=100%	(1-0.84)/1=16%	79.00	80.00	1.00	2.50	1.00	5	2 41561	133				
1.35/1.38=97.83%	(1.35-0.12)/1.38=9.42%	80.00	81.38	1.38	5.00	Tr	7	9 41562	27				
1.95/2.72=72.43%	(1.95-0.25)/2.72=65.5%	81.38	84.10	2.72	2.50	0.30	7	7 41563	289	0.38			
1.88/2.06=91.26%	(1.88-0.79)/2.06=52.9%	84.10	86.16	2.06	2.50	0.10	5	4 41564	40				
1.22/1.31=93.13%	(1.22-0.84)/1.31=29%	86.16	87.47	1.31	2.50	0.10	5	2 41565	58				
0.85/0.89=95.51%	(0.85-0.74)/0.89=12.36%	87.47	88.36	0.89	2.50	0.30	5	2 41566	174	0.24			
0.39/0.39=100%	(0.39-0.29)/0.39=25.64%	88.36	88.75	0.39	2.50	5.00	7	4 41567 SP, PY, GN	623	0.79			
1.68/1.77=94.92%	(1.68-1.20)/1.77=27.12%	88.75	90.52	1.77	2.50	0.30	6	3 41568	124				
1.95/2.02=96.53%	(1.95-1.76)/2.02=9.41%	90.52	92.54	2.02	5.00	0.10	4	1 41569	19				
0.66/1.03=64.08%	(0.66-0.38)/1.03=27.18%	92.54	93.57	1.03	2.50	0.00	5	3 41570	17				
1.69/1.71=98.83%	(1.69-1.14)/1.71=32.16%	93.57	95.28	1.71	2.50	1.00	5	3 41571	114				
0.35/0.95=36.84%	(0.35-0)/0.95=36.84%	95.28	96.23	0.95	2.50	2.50	7	5 41572	113				
1.68/1.77=94.92%	(1.68-1.17)/1.77=28.81%	96.23	98.00	1.77	2.50	1.00	5	4 41573	68				
1.20/1.66=72.29%	(1.20-0)/1.66=72.29%	98.00	99.66	1.66	2.50	0.30	5	5 41574	36				
1.35/1.54=87.66%	(1.35-0.18)/1.54=75.97%	99.66	101.20	1.54	2.50	0.30	6	9 41575	121				

RECOVERY	R.O.D.	SAMPLE										ppb	GMT	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	pct	ppb																	
		FROM	TO	WIDTH	Py%	Vn%	A	F	NUMBER																																			
1.22/3.04=40.13%	(1.22-0)/3.04=40.13%	26.52	29.56	3.04	1.00	0.30	7	10	41576	33	1.8	9	-1	198	5.04	64	4	18	60	11	46	40																						
1.34/3.05=43.93%	(1.34-0)/3.05=43.93%	29.56	32.61	3.05	1.00	0.30	7	10	41577 GN	61	1.6	57	2	57	7.8	113	4	22	220	9	151	60																						
2.4/3.05=78.69%	(2.4-0.38)/3.05=66.23%	32.61	35.66	3.05	5.00	0.00	7	8	41578	83	1.8	26	-1	137	6.54	433	2	26	68	17	65	50																						
1.72/3.05=56.39%	(1.72-0.28)/3.05=47.21%	35.66	38.71	3.05	2.50	0.10	6	8	41579	67	1.2	36	-1	242	6.13	223	2	23	24	10	33	45																						
2/2.29=87.33%	(2-0.28)/2.29=75.11%	38.71	41.00	2.29	2.50	0.00	5	6	41580	39	0.8	36	-1	61	4.56	691	2	21	36	7	23	45																						
2/2=100%	(2-0.93)/2=53.5%	41.00	43.00	2.00	2.50	0.10	5	3	41581	51	1.4	61	-1	126	5.2	894	2	17	43	10	26	40																						
1.69/2=84.5%	(1.69-0.39)/2=65%	43.00	45.00	2.00	2.50	0.00	5	5	41582	151	0.21	2.2	121	-1	146	7.9	1450	2	50	42	10	75	110																					
1.81/2=90.5%	(1.81-1)/2=40.5%	45.00	47.00	2.00	2.50	0.30	5	3	41583	118	4.6	63	12	165	6.87	1328	2	56	133	8	1242	130																						
1.78/1.76=101.14%	(1.78-0.69)/1.76=61.93%	47.00	48.76	1.76	2.50	0.10	5	3	41584	41	1	49	-1	35	4.78	1376	2	19	76	7	64	40																						
1.82/2=90.5%	(1.81-0.12)/2=80.5%	48.76	50.76	2.00	5.00	0.00	7	9	41585	62	0.8	120	-1	30	5.76	882	2	15	62	9	79	55																						
1/1=100%	(1-0.1)/1=90%	50.76	51.76	1.00	2.50	2.50	8	9	41586	50	1.4	155	1	26	5.38	1242	2	26	119	-5	149	50																						
1.31/1.57=83.44%	(1.31-0.37)/1.57=59.87%	51.76	53.33	1.57	2.50	0.10	6	4	41587	201	0.21	5.3	183	10	333	5.72	830	2	40	756	8	1004	2400																					
0.44/0.44=100%	(0.44-0.17)/0.44=61.36%	53.33	53.77	0.44	5.00	5.00	6	4	41588 SpGnCpTT	1111	1.47	49.9	184	394	2297	5.93	887	-1	36	10000	1.39	153	20000	3.51	170																			
0.55/1.71=32.16%	(0.55-0)/1.71=32.16%	53.77	55.48	1.71	5.00	0.30	7	8	41589	147	3.5	147	3	131	5.05	342	2	37	154	6	353	125																						
1.18/1.18=100%	(1.18-0.28)/1.18=76.27%	55.48	56.66	1.18	2.50	10.00	7	5	41590	170	0.21	4.1	109	2	125	3.77	985	2	22	277	7	210	85																					
1.01/1.01=100%	(1.01-0.57)/1.01=43.56%	56.66	57.67	1.01	2.50	10.00	6	4	41591	114	1.7	106	3	47	4.16	4901	1	1	131	6	349	90																						
2.38/2.37=100.42%	(2.38-1.42)/2.37=40.51%	57.67	60.04	2.37	2.50	1.00	7	5	41592	63	1.5	126	1	45	4.39	788	2	2	77	-5	149	50																						
1.86/1.83=101.64%	(1.86-1.33)/1.83=28.96%	60.04	61.87	1.83	2.50	0.10	7	4	41593	89	5.6	91	5	267	4.39	693	3	51	307	-5	631	125																						
1.96/2.13=92.02%	(1.96-0.79)/2.13=54.93%	61.87	64.00	2.13	2.50	0.30	5	3	41594	301	0.45	3.2	139	4	96	4.76	342	3	12	338	-5	580	100																					
1.87/2=93.5%	(1.87-0.94)/2=46.5%	64.00	66.00	2.00	2.50	1.00	5	3	41595	76	4.6	110	4	413	6.16	537	2	56	243	-5	466	100																						
2/2=100%	(2-0.74)/2=63%	66.00	68.00	2.00	5.00	1.00	6	3	41596	90	2.8	108	-1	66	6.36	82	4	49	41	-5	73	15																						
1.88/2=94%	(1.88-0.98)/2=45%	68.00	70.00	2.00	5.00	1.00	6	3	41597 SP	258	0.31	5.2	80	3	303	6.07	93	4	46	41	-5	313	35																					
2.02/2=101%	(2.02-1.51)/2=25.5%	70.00	72.00	2.00	5.00	2.50	6	3	41598	172	0.17	5.1	172	1	240	6.11	326	3	36	107	5	146	45																					
1.11/1.11=100%	(1.11-0.56)/1.11=49.55%	72.00	73.11	1.11	2.50	1.00	6	3	41599	150	0.21	2.9	111	2	91	4.7	190	3	22	118	-5	254	60																					
0.64/0.69=92.75%	(0.64-0.55)/0.69=13.04%	73.11	73.80	0.69	1.00	5.00	6	2	41600 SP	794	0.99	22.1	93	41	520	3.05	307	4	9	2314	20	5236	600																					
1.36/1.49=91.28%	(1.36-0)/1.49=91.28%	73.80	75.29	1.49	5.00	0.00	9	10	41601	38	9.9	137	5	773	4.77	718	4	10	304	320	599	250																						
1.34/1.34=100%	(1.34-0)/1.34=100%	75.29	76.63	1.34	5.00	0.30	9	10	41602	8	0.9	63	-1	10	4.15	852	3	2	48	-5	38	15																						
1.3/1.37=94.89%	(1.3-1.05)/1.37=18.25%	76.63	78.00	1.37	2.50	0.30	7	3	41603	7	0.4	37	2	15	3.46	838	2	2	50	6	195	70																						
2/2=100%	(2-0.13)/2=93.5%	78.00	80.00	2.00	2.50	0.10	7	4	41604	20	0.8	51	-1	11	4.26	828	2	3	23	-5	77	40																						
2.01/2=100.5%	(2.01-1.15)/2=43%	80.00	82.00	2.00	2.50	0.30	6	3	41605	25	0.9	41	2	8	2.71	757	2	2	77	-5	174	30																						
1.99/2=99.5%	(1.99-0.77)/2=61%	82.00	84.00	2.00	2.50	0.30	6	3	41606	24	1.1	53	-1	12	3.68	906	2	1	21	5	24	40																						
0.78/0.77=101.30%	(0.78-0.27)/0.77=66.23%	84.00	84.77	0.77	5.00	0.30	6	3	41607	36	1.5	58	-1	5	3.73	628	2	2	85	-5	98	40																						
0.69/0.69=100%	(0.69-0)/0.69=100%	84.77	85.46	0.69	5.00	0.00	9	10	41608 SP	396	0.65	19.2	72	5	89	4.12	658	3	2	1487	43	571	230																					
0.61/0.61=100%	(0.61-0.46)/0.61=24.59%	85.46	86.07	0.61	5.00	20.00	8	3	41609 SP,GN,CP	1419	2.02	70.9	50	199	148	1302	5.17	825	3	10	10000	1.18	54	16998	1900																			
0.24/0.24=100%	(0.24-0.14)/0.24=41.67%	86.07	86.31	0.24	2.50	40.00	8	3	41610 SP, GN	10000	28.35	689.5	50	118	329	1460	4.29	1253	-1	8	9297	100	20000	3.65	2400																			
0.85/0.85=100%	(0.85-0.24)/0.85=71.76%	86.31	87.16	0.85	10.00	0.30	7	4	41611	132	2.7	51	3	58	4.88	620	2	10	212	-5	292	280																						
0.87/0.87=100%	(0.87-0.42)/0.87=51.72%	87.16	88.03	0.87	5.00	0.10	7	3	41612	107	1.1	83	-1	72	7.74	1340	3	9	13	-5	88	190																						
1.95/1.97=99.49%	(1.95-0.62)/1.97=68.02%	88.03	90.00	1.97	5.00	0.30	6	4	41613	126	0.8	66	-1	136	6.47	837	2	11	18	5	32	110																						
2.61/2.64=98.86%	(2.61-1.35)/2.64=47.73%	90.00	92.64	2.64	5.00	0.10	6	3	41614	60	0.4	29	-1	162	6.53	1225	3	13	45	-5	56	60																						
0.53/0.53=100%	(0.53-0.39)/0.53=26.42%	92.64	93.17	0.53	5.00	2.50	6	2	41615 SP, GN	594	1.1	28.8	29.8	104	95	884	5.83	1306	3	15	9432	67	10966	1400																				
1.83/1.83=100%	(1.83-0.46)/1.83=74.86%	93.17	95.00	1.83	5.00	2.50	7	4	41616 SP	173	0.24	9.5	93	15	160	5.56	891	4	11	695	13	1812	270																					
2/2=100%</																																												

RECOVERY	R.D.O.	SAMPLE																								
		FROM	TO	WIDTH (M)	P _{Y%}	Vn _Z	A	F	NUMBER	ppb	GMT	GMT	ppm	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	pct	ppm	pct	ppb	
										Au	Au	Ag	Ag	As	Cd	Cu	Fe	Mn	Mn	Ni	Pb	Pb	Sb	Zn	Zn	Hg
2/2=100%	(2-0.93)/2=53.5%	119.00	121.00	2.00	2.50	2.50	6	7	41629	98			3.5	136	-1	33	4.15	442	2	2	41	5	118	60		
1.79/1.81=98.90%	(1.79-1.65)/1.81=7.73%	121.00	122.81	1.81	2.50	1.00	5	2	41630	104			3.2	112	2	171	3.4	127	2	14	97	7	296	60		
1.19/1.24=95.97%	(1.19-0.79)/1.24=32.26%	122.81	124.05	1.24	2.50	2.50	5	2	41631	193	0.27		4.8	155	7	97	3.2	200	2	19	281	11	1045	160		
1.92/1.95=98.46%	(1.92-0.87)/1.95=53.85%	124.05	126.00	1.95	1.00	20.00	5	4	41632	219	0.31		3.5	180	-1	54	4.28	1405	3	13	51	-5	85	60		
0.56/0.74=75.68%	(0.56-0.27)/0.74=39.19%	126.00	126.74	0.74	5.00	70.00	9	5	41633	1021	1.3		4.5	513	-1	103	6.04	4836	2	8	146	10	75	50		
2.29/2.26=101.33%	(2.29-1.83)/2.26=20.35%	126.74	129.00	2.26	5.00	0.10	6	3	41634	80			2.1	100	-1	320	7.62	2376	3	16	2	-5	73	35		
2/2=100%	(2-1.59)/2=20.5%	129.00	131.00	2.00	5.00	0.10	6	2	41635	79			3.6	78	-1	651	8.21	2611	2	17	9	-5	90	25		
1.94/2=97%	(1.94-1.35)/2=29.5%	131.00	133.00	2.00	5.00	0.10	6	2	41636	61			3.3	78	1	597	8.73	2762	3	17	117	-5	160	40		
1.83/2=91.5%	(1.83-0.9)/2=46.5%	133.00	135.00	2.00	5.00	1.00	6	3	41637	19			0.7	53	-1	205	8.2	2721	3	17	11	-5	76	30		
2/2=100%	(2-1.62)/2=19%	135.00	137.00	2.00	5.00	0.10	5	2	41638	113			2	104	-1	183	7.6	1814	2	12	26	-5	72	50		
2.04/2=102%	(2.04-1.99)/2=2.5%	137.00	139.00	2.00	2.50	0.10	5	1	41639	122			3	106	-1	73	6.24	1824	3	12	15	-5	35	20		
2/2=100%	(2-1.51)/2=24.5%	139.00	141.00	2.00	2.50	Tr	5	2	41640	45			1.5	62	-1	81	4.73	1652	3	10	4	-5	38	30		
2/2=100%	(2-1.88)/2=6%	141.00	143.00	2.00	2.50	Tr	5	3	41641	27			0.9	67	-1	49	4.93	1582	2	11	6	-5	45	30		
2/2=100%	(2-1.55)/2=22.5%	143.00	145.00	2.00	2.50	0.10	5	2	41642	116			2.2	128	-1	231	6.76	1797	2	14	3	-5	57	40		
2.26/2.25=100.44%	(2.26-1.56)/2.22=31.11%	145.00	147.25	2.25	2.50	1.00	4	2	41643	30			0.9	57	-1	62	5.99	1970	1	11	36	-5	155	40		
2.1/2.1=100%	(2.1-1.28)/2.1=39.05%	147.25	149.26	2.01	0.30	0.30	2	3	41644	11			0.5	13	1	88	5.89	1593	2	11	16	-5	187	20		
2.02/2.03=99.51%	(2.02-1.21)/2.03=40.39%	149.26	151.29	2.03	0.30	1.00	2	3	41645	12			0.8	12	1	136	6.02	1933	2	11	27	-5	195	30		
1.1/1.71=64.33%	(1.2-0.42)/1.71=39.76%	151.29	153.00	1.71	2.50	0.30	5	5	41646	35			1	51	-1	212	6.3	2115	2	11	8	-5	86	35		
2/2=100%	(2-1.68)/2=16%	153.00	155.00	2.00	5.00	1.00	6	2	41647	32			1.2	198	-1	158	7.92	1802	2	13	9	-5	54	20		
1.77/2=88.5%	(1.77-1.16)/2=30.5%	155.00	157.00	2.00	5.00	1.00	6	3	41648	56			1.2	85	-1	97	7.16	1802	5	9	16	-5	55	35		
1.9/2=95%	(1.9-1.28)/2=31%	157.00	159.00	2.00	5.00	0.10	6	4	41649	50			1.8	102	-1	138	7.48	1203	3	12	19	-5	32	30		
1.8/2=90%	(1.8-0.9)/2=45%	159.00	161.00	2.00	2.50	Tr	5	3	41650	236	0.31		2.5	84	-1	410	5.07	1556	3	10	66	-5	101	50		
2.08/2=104%	(2.08-1.37)/2=35.5%	161.00	163.00	2.00	1.00	0.00	4	3	41651	32			0.4	17	-1	98	2.9	1352	2	7	-2	-5	37	30		
2.39/2.57=93%	(2.39-0.62)/2=88.5%	163.00	165.57	2.57	5.00	0.30	5	5	41652	50			1.9	67	4	77	7.14	1476	4	9	182	-5	535	25		
2.35/2.37=99.16%	(2.35-1.02)/2.37=56.12%	165.57	167.94	2.37	2.50	0.10	3	3	41653	43			1.7	22	-1	212	6.14	1868	2	9	12	-5	103	55		
1.09/1.06=102.83%	(1.09-0.72)/1.06=34.91%	167.94	169.00	1.06	2.50	1.00	4	3	41654	73			1.2	67	3	120	6.27	1556	2	9	48	-5	425	30		
1.62/2=81%	(1.62-0.02)/2=81%	169.00	171.00	2.00	2.50	0.30	8	10	41655	61			2	97	3	175	5.19	1607	2	8	67	-5	550	120		
1.95/2=97.5%	(1.95-0.77)/2=59%	171.00	173.00	2.00	2.50	0.30	5	3	41656	51			1.4	82	-1	67	5.12	1463	2	9	49	-5	144	40		
2.83/3=94.33%	(2.83-1.52)/3=43.67%	173.00	176.00	3.00	2.50	1.00	5	4	41657	59			0.8	65	-1	39	4.38	921	2	6	28	-5	26	30		
3/3=100%	(3-2.23)/3=25.67%	176.00	179.00	3.00	1.00	0.30	4	2	41658	26			0.7	49	-1	51	4.24	981	2	7	83	-5	45	10		
2.98/3=99.33%	(2.98-2.62)/3=12%	179.00	182.00	3.00	1.00	0.30	4	2	41659	39			0.8	57	-1	81	4.63	1143	3	8	19	-5	29	20		
2.06/2=103%	(2.06-2.06)/2=0%	182.00	184.00	2.00	1.00	1.00	4	1	41660	24			0.7	27	-1	118	3.86	1442	2	7	13	-5	95	15		
1.85/1.85=100%	(1.85-1.84)/1.85=0.5%	184.00	185.85	1.85	2.50	0.03	5	1	41661	44			0.8	42	-1	87	5.14	1518	1	7	8	-5	46	10		
0.52/0.52=100%	(0.52-0.49)/0.52=5.77%	185.85	186.37	0.52	2.50	10.00	6	1	41662	832	1.41		3.1	91	-1	71	4.92	1586	1	7	258	-5	68	15		
1.89/1.87=101.07%	(1.89-1.64)/1.87=13.37%	186.37	188.24	1.87	2.50	0.30	5	2	41663	32			1.1	39	-1	54	5.2	1352	2	9	10	-5	36	25		
1.74/1.76=98.86%	(1.74-1.52)/1.76=12.5%	188.24	190.00	1.76	2.50	0.30	5	2	41664	62			2	54	-1	238	4.65	947	2	9	40	-5	49	30		
1.31/1.32=99.24%	(1.31-0.75)/1.32=42.42%	190.00	191.32	1.32	5.00	2.50	5	3	41665	180	0.21		2.7	85	-1	108	5.23	713	3	8	53	-5	92	40		
0.62/0.61=101.64%	(0.62-0.31)/0.61=50.82%	191.32	191.93	0.61	2.50	10.00	7	3	41666	1037	1.1		3.8	104	-1	1490	5.82	993	3	6	189	-5	82	60		
1.91/1.91=100%	(1.91-0.87)/1.91=54.45%	191.93	193.84	1.91	2.50	2.50	7	5	41667	153	0.27		1.4	86	-1	70	4.97	931	4	6	46	-5	90	135		
2.2/2.3=95.65%	(2.2-0.61)/2.3=69.13%	193.84	196.14	2.30	2.50	1.00	4	7	41668	101			1.7	65	2	98	5.94	1551	3	7	210	-5	384	90		
1.76/1.86=94.62%	(1.76-1.12)/1.86=88.17%	196.14	198.00	1.96	2.50	Tr	5	8	41669	27			0.7	86	2	54	4.34	1824	3	7	99	-5	317	40		
2.34/3=98%	(2.34-1.42)/3=50.67%	198.00	201.00	3.00	1.00	0.19	4	4	41670	31			1.3	83	4	67	6.05	1667	2	8	153	-5	668	70		
1.86/2=93%	(1.86-1.41)/2=23%	201.00	203.00	2.00	1.00	Tr	4	3	41671	39			1.5	105	1	115	6.75	1530	7	8	99	-5	263	30		
2.95/3=98.33%	(2.95-0.75)/3=73.33%	203.00	206.00	3.00	0.30	0.10	4	4	41672	33			1.4	41	-1	118	5.62	1753	1	6	67	-5	201	30		
2.91/3=97%	(2.91-1.06)/3=61.67%	206.00	209.00	3.00	0.30	1.00	4	4	41673	15			0.7	17	1	62	4.87	1929	1	6	89	-5	228	30		
1.9/1.97=96.45%	(1.9-0.56)/1.97=68.02%	209.00	210.97	1.97	1.00	5.00	4	7	41674	21			2	21	3	101	5.59	2720	-1	7	169	-5	453	90		
3.03/3.03=100%	(3.03-2.13)/3.03=29.7%	210.97	214.00	3.03	0.30	0.30	4	2	41675	4			0.6	8	1	74	5.19	1725	1	6	124	-5	275	80		
2.98/3=99.33%	(2.98-1.61)/3=45.67%	214.00	217.00	3.00	0.30	Tr	4	2	41676	11			0.4	-5	1	56	5	2220								

HOLE NUMBER DDH-B									SAMPLE																
RECOVERY	R.Q.D.	FROM	TO	WIDTH (M)	Py%	Vn%	A	F NUMBER	ppb	GMT	GMT	ppm	ppm	ppm	pct	ppm	ppm	ppm	pct	ppm	ppm	pct	ppb		
									Au	Au	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn	Hg
2.24/2.28=98.25% (2.24-1.73)/2.28=22.37%		229.48	231.76	2.28	0.30	1.00	4	2 41682	74			0.9	16	-1	43	4.58	1021	1	4	-2	-5	47		80	
1.96/2.01=97.51% (1.96-1.54)/2.01=20.9%		231.76	233.77	2.01	0.30	1.00	4	2 41683	83			1.6	14	-1	49	4.15	1204	4	3	2	-5	46		80	

HOLE NUMBER	DDH-9										SAMPLE NUMBER	SAMPLE																	
	RECOVERY	R.Q.D.	FROM	TO	WIDTH (m)	PY%	VNZ	A	F	ppb		GMT	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	ppm	ppb	
										Au	Au	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Hg					
1.65/1.82=90.66%	(1.65-0.88)/1.82=42.31%	5.18	7.00	1.82	2.50	0.00	4	3	41684	69	1.5	72	-1	57	3.24	600	1	21	227	-5	85	65							
2/2=100%	(2-1.48)/2=26%	7.00	9.00	2.00	2.50	0.00	4	2	41685	34	0.6	88	-1	39	4.21	721	2	26	62	-5	45	70							
1.92/2=96%	(1.92-1.62)/2=15%	9.00	11.00	2.00	2.50	0.10	4	2	41686	195	0.31	4.3	65	3	179	4.21	692	1	23	362	21	390	140						
1.93/2=96.5%	(1.93-1.46)/2=23.5%	11.00	13.00	2.00	2.50	0.00	4	2	41687	28	0.7	20	-1	259	3.35	1048	1	21	16	-5	74	65							
1.99/2=99.5%	(1.99-0.75)/2=62%	13.00	15.00	2.00	2.50	0.10	4	4	41688 GN, SP	120	2.1	49	4	53	3.98	700	1	23	447	-5	488	130							
2/2=100%	(2-0.5)/2=75%	15.00	17.00	2.00	2.50	0.10	4	4	41689	62	0.5	63	-1	101	3.63	1315	1	20	15	-5	62	55							
2/2=100%	(2-1.23)/2=38.5%	15.00	19.00	4.00	2.50	0.00	4	3	41690	142	0.8	60	-1	68	3.31	818	2	14	33	-5	44	45							
1.99/2=99.5%	(1.99-1.75)/2=12%	19.00	21.00	2.00	2.50	0.10	4	2	41691	125	0.5	64	-1	320	4.14	652	2	19	11	-5	20	45							
1.97/2=98.5%	(1.97-1.44)/2=26.5%	21.00	23.00	2.00	2.50	0.10	4	2	41692	95	0.9	41	2	76	3.15	739	2	13	140	-5	215	65							
1.46/1.47=99.32%	(1.46-1.08)/1.47=25.85%	23.00	24.47	1.47	2.50	0.30	4	3	41693 SP	287	0.48	4.8	139	7	293	5.87	994	3	12	894	-5	822	170						
2.28/2.28=100%	(2.28-1.36)/2.28=40.35%	24.47	26.75	2.28	1.00	Tr	3	2	41694	18	0.2	34	-1	172	4.33	1007	2	9	32	-5	80	40							
1.92/2.01=95.52%	(1.92-1.37)/2.01=27.36%	26.75	28.76	2.01	2.50	Tr	3	2	41695	6	-0.2	36	-1	38	5.07	1059	2	12	45	-5	71	35							
1.3/1.24=104.84%	(1.3-1)/1.24=24.19%	28.76	30.00	1.24	5.00	0.30	5	2	41696	45	0.4	80	-1	113	5.16	1402	2	8	33	-5	58	30							
1.26/1.39=90.65%	(1.26-0.59)/1.39=48.2%	30.00	31.39	1.39	5.00	2.50	5	2	41697	114	1.2	92	-1	99	4.84	1121	2	11	33	-5	47	40							
1.65/1.61=102.48%	(1.65-0.55)/1.61=68.32%	31.39	33.00	1.61	5.00	0.00	5	3	41698	53	0.4	108	-1	29	4.45	1445	1	7	37	-5	85	30							
2/2=100%	(2-1.12)/2=44%	33.00	35.00	2.00	2.50	1.00	5	3	41699 SP	74	1.3	56	-1	113	4.73	1545	1	6	159	-5	261	60							
1.99/2=99.5%	(1.99-1.21)/2=39.5%	35.00	37.00	2.00	2.50	0.10	5	3	41700 GN, SP	159	0.24	9.9	103	-1	39	5.67	1585	2	7	271	-5	170	50						
1.79/2=89.5%	(1.79-1.21)/2=29%	37.00	39.00	2.00	2.50	0.10	4	2	41701	91	0.7	121	6	32	7.13	1534	2	11	77	-5	787	90							
2/2=100%	(2-1.61)/2=19.5%	39.00	41.00	2.00	2.50	0.30	4	2	41702	46	0.3	90	-1	83	6.42	1675	3	15	111	-5	82	30							
2/2=100%	(2-1.46)/2=27%	41.00	43.00	2.00	5.00	0.30	4	2	41703	59	0.3	85	-1	373	6.2	1545	2	11	96	-5	116	50							
1.96/2=98%	(1.96-1.54)/2=21%	43.00	45.00	2.00	5.00	0.30	4	3	41704 SP, GN	98	1.1	72	11	122	5.15	1331	2	8	939	-5	1388	130							
1.67/2=83.5%	(1.67-0.9)/2=38.5%	45.00	47.00	2.00	5.00	0.10	4	3	41705	142	2	52	2	270	5.63	1276	2	11	249	-5	394	70							
2/2=100%	(2-0.5)/2=75%	47.00	49.00	2.00	2.50	0.30	4	3	41706 SP, CP	265	0.48	4.3	77	18	431	5.15	1027	1	10	1171	-5	2145	190						
1.87/2=93.5%	(1.87-0.58)/2=64.5%	49.00	51.00	2.00	2.50	0.30	4	4	41707	37	0.2	56	-1	49	5.33	1283	2	11	241	-5	149	70							
1.96/2=98%	(1.96-1.34)/2=31%	51.00	53.00	2.00	2.50	0.30	4	3	41708 SP	26	0.3	38	2	39	5.1	1519	2	9	133	-5	288	80							
2/2=100%	(2-1.43)/2=28.9%	53.00	55.00	2.00	2.50	Tr	4	3	41709	41	0.4	43	-1	83	5.53	1717	1	11	43	-5	158	60							
1.88/2=94%	(1.88-1.47)/2=20.5%	55.00	57.00	2.00	2.50	0.10	4	2	41710	81	0.9	18	1	120	5.3	1241	4	23	117	-5	259	65							
2/2=100%	(2-1.77)/2=11.5%	57.00	59.00	2.00	2.50	0.10	4	2	41711	42	0.4	43	-1	58	5.94	1681	2	26	97	-5	210	60							
2/2=100%	(2-1.68)/2=16%	59.00	61.00	2.00	2.50	0.30	4	2	41712	28	0.4	30	-1	202	5.32	1515	2	26	19	-5	101	60							
1.92/2=96%	(1.92-1.04)/2=44%	61.00	63.00	2.00	2.50	0.10	4	3	41713 SP	50	1	-5	23	405	6.05	1921	2	31	29	-5	2256	95							
1.97/2=98.5%	(1.97-1.31)/2=34%	63.00	65.00	2.00	2.50	1.00	4	4	41714 SP, GN	182	0.24	4.2	119	15	189	5.88	1162	-1	17	915	-5	1731	310						
2/2=100%	(2-1.85)/2=7.5%	65.00	67.00	2.00	2.50	0.10	4	2	41715	13	0.2	14	-1	135	6.3	1225	2	9	5	-5	70	60							
1.9/2=95%	(1.9-1.22)/2=34%	67.00	69.00	2.00	2.50	0.10	4	3	41716 SP, CP	72	1.7	60	8	82	5.37	1370	1	9	139	-5	1045	140							
2/2=100%	(2-1.47)/2=26.5%	69.00	71.00	2.00	2.50	1.00	4	2	41717 SP, GN	115	4.4	86	24	175	5.07	1470	2	7	1057	-5	2610	310							
2/2=100%	(2-1)/2=50%	71.00	73.00	2.00	2.50	0.10	4	3	41718 SP, GN	130	2.3	138	11	243	5.42	1313	2	7	1314	-5	1190	150							
1.96/2=98%	(1.96-0.87)/2=54.5%	73.00	75.00	2.00	2.50	Tr	4	3	41719 SP, GN	70	1.8	95	13	116	6.05	1229	2	7	1221	-5	1458	120							
1.96/2=98%	(1.96-0.37)/2=79.5%	75.00	77.00	2.00	2.50	0.10	4	4	41720	127	2.7	114	19	137	5.34	1381	2	5	2848	-5	2161	170							
1.81/2=90.5%	(1.81-0.48)/2=66.5%	77.00	79.00	2.00	2.50	0.10	4	5	41721 SP	355	0.65	14.8	93	19	240	6.43	1682	2	9	1546	-5	2179	145						
1.93/2=96.5%	(1.93-1.18)/2=37.5%	79.00	81.00	2.00	1.00	0.10	4	3	41722	30	1.1	-5	4	115	4.65	1642	-1	8	299	-5	551	80							
2/2=100%	(2-1.09)/2=45.5%	81.00	83.00	2.00	2.50	0.10	4	3	41723 GN	66	1.9	50	4	130	4.78	1205	2	7	799	-5	527	90							
1.81/2=90.5%	(1.81-0.75)/2=53%	83.00	85.00	2.00	2.50	Tr	4	3	41724	82	0.6	48	-1	69	5.22	1328	2	7	64	-5	145	65							
1.72/2=86%	(1.72-0.6)/2=56%	85.00	87.00	2.00	2.50	Tr	4	3	41725	81	1.9	-5	3	455	5.69	1486	2	8	267	-5	503	90							
1.95/2=97.5%	(1.95-1.37)/2=29%	87.00	89.00	2.00	2.50	Tr	4	3	41726	58	1.8	35	6	73	5.28	1222	1	8	415	-5	685	80							
2/2=100%	(2-1.27)/2=36.5%	89.00	91.00	2.00	2.50	0.10	4	2	41727	710	0.62	42.3	28	4	84	5.66	1268	3	9	84	-5	562	120						
1.75/2=87.5%	(1.75-1.4)/2=17.5%	91.00	93.00	2.00																									

RECOVERY	R.Q.D.	FROM	TO	WIDTH (m)	PY%	VN%	A	F	NUMBER	ppb	GMT	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppb	
											Au															
0.84/0.85=98.82%	(0.84-0.76)/0.85=9.41%	107.15	108.00	0.85	2.50	2.50	5	2	41737	8	-0.2	18	-1	15	4.5	844	1	7	51	-5	93	50				
2.19/2.20=99.55%	(2.19-1.87)/2.2=91.36%	108.00	110.20	2.20	2.50	0.30	4	2	41738	21	0.4	52	-1	63	5.21	793	2	9	37	-5	94	55				
0.23/0.23=100%	(0.23-0.11)/0.23=52.17%	110.20	110.43	0.23	2.50	5.00	4	3	41739 SP, GN	226	0.31	21.1	93	177	2294	5.58	661	-1	9	10000	1.22	39	18841	1050		
1.52/1.57=96.82%	(1.52-1.05)/1.57=29.94%	110.43	112.00	1.57	1.00	0.30	4	3	41740	30	0.5	77	1	86	5.22	820	2	10	123	-5	225	60				
1.94/2=97%	(1.94-1.74)/2=10%	112.00	114.00	2.00	2.50	0.10	4	2	41741	52	0.6	92	-1	186	4.52	860	1	7	36	-5	114	35				
1.7/1.7=100%	(1.7-0.76)/1.7=55.29%	114.00	115.70	1.70	1.00	0.10	4	3	41742	63	1.2	68	-1	31	3.64	672	2	6	65	-5	192	50				
1.74-1.79=97.21%	(1.74-0.29)/1.79=81.01%	115.70	117.49	1.79	2.50	0.30	7	10	41743	207	0.27	2.6	71	-1	95	4.04	679	3	6	49	-5	41	180			
1.51/1.51=100%	(1.51-0.58)/1.51=61.59%	117.49	119.00	1.51	1.00	0.30	4	3	41744	263	0.34	7.4	40	2	13	4.5	731	2	7	81	-5	284	50			
1.95/2=97.5%	(1.95-1.28)/2=33.5%	119.00	121.00	2.00	2.50	0.10	4	3	41745	32	-0.2	40	-1	12	4.82	665	2	8	7	-5	51	40				
1.93/2=96.5%	(1.93-1.33)/2=30%	121.00	123.00	2.00	2.50	Tr	4	3	41746	22	-0.2	43	-1	87	4.72	778	2	8	2	-5	55	30				
2.01/2=100.5%	(2.01-1.3)/2=35.5%	123.00	125.00	2.00	1.00	0.30	4	3	41747	6	-0.2	33	-1	15	3.86	743	2	6	-2	-5	69	40				
1.83-2.1=87.14%	(1.83-0.35)/2=70.47%	125.00	127.10	2.10	2.50	0.10	4	5	41748	18	-0.2	68	-1	46	4.42	971	3	5	44	-5	96	45				
1.77/1.9=93.16%	(1.77-0.15)/1.9=85.26%	127.10	129.00	1.90	2.50	0.10	7	9	41749	145	5.5	47	-1	39	4.82	676	1	7	48	-5	113	60				
2/2=100%	(2-1.06)/2=48%	129.00	131.00	2.00	2.50	Tr	5	3	41750	8	-0.2	37	-1	21	4.23	534	1	6	7	-5	34	55				
1.94/2=97%	(1.94-1.44)/2=25%	131.00	133.00	2.00	1.00	Tr	5	2	41751	2	-0.2	21	-1	8	4.81	412	1	6	6	-5	36	40				
2/2=100%	(2-1.66)/2=17%	133.00	135.00	2.00	2.50	0.10	5	2	41752	4	-0.2	17	-1	13	4.84	382	1	4	11	-5	24	25				
1/1=100%	(1-0.75)/1=25%	135.00	136.00	1.00	5.00	0.00	5	2	41753	5	-0.2	20	-1	15	5.93	430	1	7	26	-5	30	45				
2.04/2=102%	(2.04-1.16)/2=44%	136.00	138.00	2.00	2.50	0.10	4	3	41754 SP	89	0.9	52	-1	44	4.05	654	1	4	35	-5	68	45				
2.05/2=102.5%	(2.05-1.77)/2=11.5%	138.00	140.00	2.00	2.50	Tr	4	2	41755	43	0.2	54	-1	8	5.21	797	2	3	19	-5	59	50				
1.95/2=97.5%	(1.95-1.63)/2=16%	140.00	142.00	2.00	1.00	0.10	4	2	41756	47	0.2	46	-1	92	4.23	997	1	4	37	-5	89	40				
2/2=100%	(2-1.83)/2=8.5%	142.00	144.00	2.00	2.50	0.10	4	2	41757	59	0.2	58	-1	45	4.7	1239	2	4	73	-5	124	80				
2/2=100%	(2-1.66)/2=17%	144.00	146.00	2.00	1.00	0.00	4	2	41758	26	0.3	38	-1	24	4.06	1137	-1	3	77	-5	120	70				
2.03/2=101.5%	(2.03-1.84)/2=9.5%	146.00	148.00	2.00	2.50	Tr	4	2	41759	20	0.3	37	-1	25	4.49	1249	2	4	18	-5	120	75				
2.02/2=101%	(2.02-1.94)/2=4%	148.00	150.00	2.00	2.50	Tr	4	2	41760	92	0.2	43	-1	64	4.19	1022	1	4	14	-5	87	50				
2/2=100%	(2-1.96)/2=2%	150.00	152.00	2.00	2.50	0.10	4	2	41761	10	-0.2	41	-1	67	4.3	1082	2	5	3	-5	90	50				
2/2=100%	(2-1.66)/2=17%	152.00	154.00	2.00	2.50	0.10	4	2	41762	19	-0.2	46	-1	64	4.74	940	2	6	3	-5	64	50				
1.94/2=97%	(1.94-1.48)/2=23%	154.00	156.00	2.00	2.50	0.30	5	2	41763	7	-0.2	34	-1	84	5.17	616	2	4	15	-5	43	40				
1.58/1.58=100%	(1.58-1.34)/1.58=15.19%	156.00	157.58	1.58	2.50	0.30	5	2	41764	19	-0.2	32	-1	39	4.15	600	1	4	17	-5	30	45				
1.86/1.95=95.38%	(1.86-0.71)/1.86=95.38%	157.58	159.53	1.95	2.50	0.30	7	9	41765 SP, GN	688	0.86	14.8	53	29	154	4.99	593	2	5	3335	9	2882	290			
0.72/0.75=96%	(0.72-0.7)/0.75=96%	159.53	160.28	0.75	2.50	Tr	5	8	41766	46	0.4	56	1	66	4.98	1004	-1	5	164	-5	264	75				
1.72/1.72=100%	(1.72-1.33)/1.72=22.67%	160.28	162.00	1.72	2.50	0.10	5	2	41767	18	0.2	54	-1	90	4.79	606	2	4	50	-5	100	100				
1.82/2=91%	(1.82-1.5)/2=16%	162.00	164.00	2.00	2.50	0.10	4	2	41768	40	0.3	73	-1	73	4.5	770	2	5	30	-5	116	60				
3.06/3=102%	(3.06-2.75)/3=10.33%	164.00	167.00	3.00	1.00	0.10	4	2	41769	37	0.3	44	-1	8	4.34	606	2	7	19	-5	50	50				
2.93/3=97.67%	(2.93-2.05)/3=29.33%	167.00	170.00	3.00	2.50	Tr	4	2	41770	64	0.4	78	-1	7	4.45	923	1	5	-2	-5	69	55				
3.05/3=101.67%	(3.05-2.66)/3=13%	170.00	173.00	3.00	1.00	Tr	4	2	41771	37	0.2	55	-1	36	4.38	845	2	6	-2	-5	53	50				
3/3=100%	(3-2.33)/3=22.33%	173.00	176.00	3.00	1.00	Tr	4	2	41772	35	-0.2	38	-1	13	3.35	711	-1	5	-2	-5	50	30				
2.95/3=98.33%	(2.95-2.27)/3=22.67%	176.00	179.00	3.00	2.50	2.50	4	2	41773	46	-0.2	28	-1	12	3.16	796	1	3	-2	-5	55	40				
1.99/2.12=93.87%	(1.99-1.69)/2.12=14.15%	179.00	181.12	2.12	1.00	Tr	4	2	41774	49	0.3	30	-1	29	3.33	908	1	6	18	-5	75	40				
1.21/1.21=100%	(1.21-1.21)/1.21=45.45%	181.12	182.33	1.21	2.50	1.00	6	6	41775	100	1.3	56	8	67	4.55	715	2	5	777	-5	1133	150				
2.75/2.67=103%	(2.75-1.92)/2.67=31.09%	182.33	185.00	2.67	1.00	Tr	4	2	41776	28	0.2	37	-1	5	3.83	736	1	8	-2	-5	48	50				
2.96/3=98.67%	(2.96-2.46)/3=16.67%	185.00	188.00	3.00	1.00	0.10	4	2	41777	20	0.3	34	-1	6	3.47	594	1	10	15	-5	90	60				
3/3=100%	(3-1.42)/3=52.67%	188.00	191.00	3.00	2.50	1.00	4	3	41778	65	0.5	52	-1	13	3.55	699	-1	7	71	-5	145	50				
2.94/3=98%	(2.94-2.1)/3=28%	191.00	194.00	3.00	2.50	Tr	4	2	41779	17	-0.2	37	-1	10	3.45	733	2	4	-2	-5	56	40				
3/3=100%	(3-1.61)/3=46.33%	194.00	197.00	3.00	1.00	Tr	4	3	41780	30	-0.2	52	-1	32	3.44	854	2	3	3	-5	55	50				
3.08/3=102.67%	(3.08-1.58)/3=50%	197.00	200.00	3.00	2.50	0.10	4	3	41781	145	2.2	63	4	72	3.36	667	2	3	279	-5	532	180				
2.97/3=99%	(2.97-2.72)/3=8.33%	200.00	203.00	3.00	1.00	Tr	4	2	41782	215	0.24	1.4	47	-1	27	4.47	881	-1	8	5	-5	75	60			
2.74/3=91.33%	(2.74-1.68)/3=35.33%	203.00	206.00	3.00	1.00	Tr	4	2	41783	102	0.3	42	-1	38	3.75	885	-1	7	5	-5						

RECOVERY	R.D.	FROM	TO	WIDTH (m)	PY%	VN%	A	F	NUMBER	ppb	GMT	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppb
										Au	Au	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Hg	
2.62/2.59=1.01%	(2.62-2.18)/2.59=16.99%	227.00	229.59	2.59	1.00	Tr	4	2	41791	66	1	47	-1	82	4.64	809	1	6	7	-5	88	60			
1.39/1.41=98.58%	(1.39-0.1)/1.41=91.49%	229.59	231.00	1.41	2.50	0.10	7	9	41792	74	1	-5	-1	18	3.93	374	2	9	52	-5	135	45			
2.14/2.14=100%	(2.14-0.37)/2.14=82.71%	231.00	233.14	2.14	1.00	0.10	5	5	41793	17	-0.2	-5	-1	4	4.32	706	2	9	-2	-5	56	50			
1.86/1.86=100%	(1.86-0.73)/1.86=60.75%	233.14	235.00	1.86	1.00	0.10	4	4	41794	42	0.2	-5	-1	11	4.41	872	2	9	-2	-5	56	40			
2.06/2.02=101.98%	(2.06-0.89)/2.02=57.92	235.00	237.02	2.02	2.50	0.30	4	3	41795	39	0.2	-5	-1	36	5	848	2	7	-2	-5	60	45			
2.2/2.18=100.92%	(2.2-1.28)/2.18=42.20%	237.02	239.20	2.18	2.50	1.00	4	4	41796	42	0.2	-5	-1	17	4.84	678	-1	6	-2	-5	53	40			
1.73/1.8=96.11%	(1.73-1.23)/1.8=27.78%	239.20	241.00	1.80	2.50	0.30	4	2	41797	33	0.2	-5	-1	23	4.9	779	1	6	-2	-5	60	25			
2/2=100%	(2-1.04)/2=48%	241.00	243.00	2.00	2.50	1.00	4	3	41798	28	0.2	-5	-1	9	4.86	816	1	8	9	-5	57	35			
1.99/2=99.5%	(1.99-0.84)/2=57.5%	243.00	245.00	2.00	1.00	2.50	4	4	41799	29	0.3	-5	-1	6	4.18	928	3	5	-2	-5	94	40			
1.38/1.37=100.73%	(1.38-1.1)/1.37=20.44%	245.00	246.37	1.37	2.50	1.00	4	2	41800	73	0.9	11	-1	63	4.49	859	2	6	98	-5	191	40			
1.4/1.39=100.72%	(1.4-0.94)/1.39=33.03%	246.37	247.76	1.39	5.00	0.10	5	3	41801 SP	193	0.21	1	101	12	14	6.03	457	4	8	518	-5	1476	180		
1.22/1.25=97.6%	(1.22-0.54)/1.25=54.4%	247.76	249.01	1.25	5.00	5.00	7	5	41802 SP, GN	159	0.89	4	47	24	18	3.98	796	2	7	2708	-5	3120	300		
1.59/1.59=100%	(1.59-1.18)/1.59=30.18%	249.01	250.70	1.59	2.50	2.50	6	3	41803 SP, GN	680	1.17	4.3	116	46	45	6.36	585	2	8	3982	15	5856	370		
1.36/1.36=100%	(1.36-0.82)/1.36=39.71%	250.70	252.06	1.36	2.50	2.50	6	3	41804	873	0.21	1.1	84	2	95	4.95	834	2	8	119	-5	229	90		
0.93/0.94=98.94%	(0.93-0.31)/0.94=65.96%	252.06	253.00	0.94	5.00	1.00	6	3	41805	189	0.21	1.1	76	-1	66	4.67	681	-1	8	41	-5	138	80		
1/1=100%	(1-0.44)/1=56%	253.00	254.00	1.00	5.00	1.00	6	3	41806 SP	164	0.24	1.2	73	4	64	5.72	327	1	8	205	-5	650	120		
1.17/1.11=105.4%	(1.17-0.27)/1.11=81.08%	254.00	255.11	1.11	2.50	1.00	6	4	41807	185	0.27	1.1	42	1	75	4.02	283	-1	7	44	-5	259	70		
0.89/0.89=100%	(0.89-0.33)/0.89=62.92%	255.11	256.00	0.89	5.00	2.50	6	3	41808	237	0.17	0.8	35	-1	25	3.87	1425	-1	6	18	-5	94	60		
1/1=100%	(1-0.41)/1=53%	256.00	257.00	1.00	5.00	2.50	6	3	41809	178	0.21	1.6	46	-1	28	4.63	769	2	6	28	-5	77	55		
1/1=100%	(1-0.26)/1=74%	257.00	258.00	1.00	5.00	10.00	7	4	41810	111	0.6	35	-1	12	4.17	1193	1	6	6	-5	29	50			
1/1=100%	(1-0.46)/1=54%	258.00	259.00	1.00	5.00	10.00	8	4	41811	116	1.1	28	-1	25	3.68	2311	2	5	45	7	143	70			
1/1=100%	(1-0)/1=100%	259.00	260.00	1.00	5.00	5.00	7	7	41812 SP	175	0.24	0.7	41	16	25	6.02	785	2	7	121	6	2065	220		
1.04/1=104%	(1.04-0.36)/1=68%	260.00	261.00	1.00	10.00	2.50	7	7	41813 SP, GN	278	0.34	1.3	32	15	9	5.57	717	2	8	1146	7	1948	220		
1/1=100%	(1-0.37)/1=63%	261.00	262.00	1.00	5.00	5.00	7	4	41814 SP, GN	234	0.24	0.8	51	9	7	4.7	1751	2	6	409	8	1229	160		
1/1=100%	(1-0.63)/1=37%	262.00	263.00	1.00	5.00	20.00	7	3	41815 SP	205	0.27	1	65	6	5	4.9	1798	3	7	573	-5	832	150		
0.96/1=96%	(0.96-0.65)/1=31%	263.00	264.00	1.00	5.00	5.00	6	3	41816 SP, GN	335	0.51	2.3	35	18	10	5.11	1550	2	6	1712	7	2324	320		
1/1=100%	(1-0.34)/1=66%	264.00	265.00	1.00	5.00	2.50	7	4	41817	254	0.38	0.5	31	-1	2	4.91	231	2	9	52	-5	38	50		
1/1=100%	(1-0.55)/1=45%	265.00	266.00	1.00	2.50	5.00	6	3	41818	154	0.21	0.5	27	-1	5	4.76	1955	1	8	130	5	154	45		
0.94/1=94%	(0.94-0.22)/1=72%	266.00	267.00	1.00	2.50	5.00	6	3	41819 SP	174	0.24	1.3	35	3	10	4.67	2325	2	7	222	5	398	80		
0.99/1=99%	(0.99-0.49)/1=50%	267.00	268.00	1.00	5.00	10.00	7	3	41820 SP	251	0.27	0.9	48	10	23	7.03	1356	2	15	685	10	1214	150		
1.14/1.12=101.79%	(1.14-0.45)/1.12=61.61%	268.00	269.12	1.12	5.00	2.50	6	4	41821	117	0.7	13	-1	109	7.2	906	2	21	105	-5	114	70			
1.25/1.24=100.81%	(1.25-0.62)/1.24=50.81%	269.12	270.36	1.24	5.00	2.50	6	3	41822	134	0.5	27	1	31	6.58	1046	1	20	61	-5	173	60			

Hole No: 89-DDH-10

RECOVERY	R.G.D.	FROM	TO	WIDTH	PY%	VN%	A	F NUMBER	SAMPLE																	
									(M)																	
1.40/1.40=100%	(1.40-0)/1.4=100%	6.83	8.23	1.40	2.50	0.00	6	7 41823	78	Au	0.6	77	1	145	7.55	881	3	15	81	-5	225	Zn	70			
2.37/3.05=77.70%	(2.37-0.33)/3.05=67.87%	8.23	11.28	3.05	2.50	0.10	5	7 41824	24	Au	0.5	57	2	87	6.8	921	2	15	79	-5	377		25			
2.3/3.04=75.66%	(2.3-1.21)/3.04=35.86%	11.28	14.32	3.04	2.50	Tr	4	4 41825	200	0.17	1.4	59	10	48	5.49	1123	2	14	691	-5	1051		85			
2.46/3.05=80.66%	(2.46-0.64)/3.05=59.67%	14.32	17.37	3.05	2.50	Tr	4	6 41826	909	0.89	5.3	106	20	184	6.33	1132	2	12	1752	7	2243		180			
2.57/3.05=84.26%	(2.57-0.73)/3.05=60.33%	17.37	20.42	3.05	2.50	Tr	4	4 41827	433	0.41	2.1	104	6	59	6.17	1395	2	15	304	-5	672		75			
2.59/3.05=84.92%	(2.59-0.3)/3.05=75.08%	20.42	23.47	3.05	2.50	Tr	5	9 41828	326	0.34	1.9	71	8	217	6.6	2224	2	15	769	-5	900		90			
2.96/3.05=97.05%	(2.96-0.98)/3.05=64.92%	23.47	26.52	3.05	2.50	Tr	5	3 41829	224	0.21	1	77	-1	58	7.14	1184	3	13	208	-5	250		70			
2.96/3.04=97.37%	(2.96-0.91)/3.04=67.43%	26.52	29.56	3.04	1.00	Tr	5	5 41830	74		0.7	89	6	145	6.84	1732	2	15	505	-5	575		60			
1.44/1.44=100%	(1.44-0.21)/1.44=85.42%	29.56	31.00	1.44	2.50	Tr	5	5 41831	119		1.1	63	9	247	7.85	1970	2	15	673	-5	888		60			
1.77/2=88.5%	(1.77-0.39)/2=69%	31.00	33.00	2.00	2.50	0.00	5	5 41832	61		0.5	82	6	65	6.34	1328	2	15	354	-5	554		45			
1.91/2=95.5%	(1.91-0.31)/2=80%	33.00	35.00	2.00	2.50	0.00	5	5 41833	87		0.7	68	4	161	6.75	1146	3	14	396	-5	487		35			
1.96/2=98%	(1.96-0.43)/2=76.5%	35.00	37.00	2.00	2.50	0.00	5	4 41834	199	0.17	0.9	107	4	148	8	1395	2	17	188	-5	398		30			
1.75/2=87.5%	(1.75-0.9)/2=42.5%	37.00	39.00	2.00	2.50	0.10	5	3 41835	124		0.8	87	3	55	8.52	1361	9	17	173	-5	388		25			
1.56/1.54=101.3%	(1.56-0.69)/1.54=56.49%	39.00	40.54	1.54	2.50	Tr	5	3 41836	945	0.86	3	137	-1	161	8.92	1371	3	17	131	-5	195		15			
0.7/1.22=58.20%	(0.71-0.16)/1.22=45.08%	40.54	41.76	1.22	2.50	0.00	5	5 41837	148		1.9	124	3	102	8.62	1335	3	15	81	-5	222		20			
2.2/2.24=98.21%	(2.2-0.3)/2.24=84.82%	41.76	44.00	2.24	5.00	Tr	6	3 41838	446	0.17	1	65	4	84	7.63	1481	2	18	327	-5	312		20			
2/2=100%	(2-1.05)/2=47.5%	44.00	46.00	2.00	2.50	Tr	6	3 41839	111		1.2	41	7	102	6.94	1133	2	13	383	-5	763		45			
2/2=100%	(2-0.28)/2=86%	46.00	48.00	2.00	2.50	Tr	6	6 41840	95		1.8	61	15	367	7.93	1203	2	12	757	-5	1471		90			
1.94/2=97%	(1.94-0.48)/2=73%	48.00	50.00	2.00	5.00	0.30	6	4 41841	20		0.8	56	4	103	7.31	962	3	14	212	-5	441		40			
1.96/2=98%	(1.96-0.16)/2=90%	50.00	52.00	2.00	5.00	0.30	6	5 41842	23		0.8	34	2	98	5.36	720	3	14	340	-5	285		50			
1.83/1.95=93.85%	(1.83-0.29)/1.95=78.97%	52.00	53.95	1.95	5.00	Tr	6	4 41843	25		0.6	44	-1	52	5.69	644	2	13	76	-5	135		25			
1.89/3.04=62.17%	(1.89-0)/3.04=62.17%	53.95	56.99	3.04	5.00	Tr	6	5 41844	67		1.3	52	-1	35	7.22	711	2	12	57	-5	141		15			
2.17/3.05=71.15%	(2.17-0.61)/3.05=51.12%	56.99	60.04	3.05	5.00	0.00	6	5 41845	49		1.2	35	2	72	5.36	933	2	12	29	-5	152		25			
1.39/1.96=101.53%	(1.39-1.16)/1.96=42.35%	60.04	62.00	1.96	5.00	0.00	6	3 41846	55		1	40	-1	204	5.92	765	2	16	18	-5	67		15			
2/2=100%	(2-1.6)/2=20%	62.00	64.00	2.00	2.00	0.30	6	2 41847	13		0.3	42	-1	73	6.2	887	1	13	11	-5	53		10			
1.99/2=99.5%	(1.99-1.46)/2=26.5%	64.00	66.00	2.00	5.00	0.10	6	2 41848	21		0.4	42	-1	104	6.18	931	2	13	24	-5	68		35			
1.09/2=54.5%	(1.09-0.28)/2=40.5%	66.00	68.00	2.00	5.00	0.30	7	6 41849	257	0.27	4.7	51	26	152	9.11	387	4	13	971	15	3093		330			
2/2=100%	(2-1.26)/2=37%	68.00	70.00	2.00	5.00	0.00	6	3 41850	212	0.24	2.7	42	5	69	5.98	977	2	13	432	-5	663		85			
2/2=100%	(2-1.4)/2=30%	70.00	72.00	2.00	5.00	0.10	6	3 41851	152	0.24	2.4	41	6	44	6.16	1330	1	13	461	6	772		85			
1.95/2=97.5%	(1.95-1.26)/2=34.5%	72.00	74.00	2.00	5.00	0.30	6	4 41852	98		1.3	36	-1	47	5.64	1055	2	11	182	6	176		20			
1.63/2=61.5%	(1.63-0.43)/2=60%	74.00	76.00	2.00	5.00	1.00	6	4 41853	94		1.5	58	2	76	5.7	1099	2	12	172	-5	337		45			
1.94/2=97%	(1.94-1.31)/2=31.5%	76.00	78.00	2.00	5.00	0.30	6	2 41854	366	0.38	3.7	48	7	166	6.74	825	1	12	15	-5	919		110			
1.92/2=96%	(1.92-1.22)/2=35%	78.00	80.00	2.00	5.00	0.10	6	2 41855 SP	424	0.45	14.2	43	13	331	5.57	1318	2	11	41	5	1656		160			
1.99/2=99.5%	(1.99-1.58)/2=20.5%	80.00	82.00	2.00	5.00	1.00	6	3 41856	4417	3.15	30.5	56	13	254	5.87	1433	2	11	446	5	1699		390			
1.95/2=97.5%	(1.95-0.73)/2=61%	82.00	84.00	2.00	5.00	0.30	6	5 41857	450	0.45	2.3	98	4	122	5.33	1232	2	12	275	-5	558		60			
1.68/2=84%	(1.68-0.58)/2=55%	84.00	86.00	2.00	5.00	0.30	6	5 41858	159	0.14	1	42	-1	50	5.94	1247	1	11	40	-5	81		35			
2/2=100%	(2-1.05)/2=42.5%	86.00	88.00	2.00	5.00	0.30	6	3 41859	250	0.21	1.2	60	2	51	5.97	1363	2	7	183	-5	262		30			
1.67/2=83.5%	(1.67-1.05)/2=31%	88.00	90.00	2.00	5.00	0.30	6	3 41860	266	0.27	1.3	42	2	36	6.19	1286	2	5	85	-5	278		30			
2/2=100%	(2-1.43)/2=28.5%	90.00	92.00	2.00	5.00	0.10	6	2 41861	276	0.34	1.3	40	2	36	7.15	1330	2	6	55	-5	322		25			
1.92/2=96%	(1.92-1.16)/2=38%	92.00	94.00	2.00	5.00	Tr	6	3 41862	377	0.38	2.4	54	18	72	6.58	902	2	9	55	8	2268		170			
1.85/2=92.5%	(1.85-1.05)/2=40%	94.00	96.00	2.00	2.50	0.30	6	3 41863 SP	217	0.21	1.7	35	5	45	4.99	856	2	9	47	-5	641		85			
2/2=100%	(2-1.6)/2=20%	96.00	98.00	2.00	2.50	0.30	6	2 41864	322	0.31	2.5	87	5	148	5.13	1152	2	9	29	-5	780		130			
0.92/0.92=100%	(0.92-0.88)/2=2%	98.00	98.92	0.32	2.50	0.00	6	2 41865	296	0.31	1.9	67	7	88	4.8	818	1	10	51	-5	948		135			
1/1.08=92.5%	(1-0.36)/1.08=59.26%	98.92	100.00	1.08	2.50	2.50	7	5 41866	367	0.38	4.9	90	9	152	5.07	518	2	19	54	-5	1152		125			
1.21/2.12=57.08%	(1.21-0.46)/2.12=35.38%	100.00	102.12	2.12	2.50	2.50	7	5 41867	643	0.62	2.7	142	13	56	6.28	98	2	9	126	-5	1639		120			
1.89/1.92=98.44%	(1.89-0.51)/1.92=71.88%	102.12	104.04	1.92	5.00	1.00	6	3 41868	444	0.41	2.9	232	12	114	6.09	995	4	7	80	-5	1513		160			
1.18/1.72=68.6%	(1.18-0.6)/1.72=33.72%	104.04	105.76	1.72	2.50	Tr	5	3 41869	238	0.24	2.2	130	25	84	5.41	1817	2	7	214	8	3396		280			
2.47/3.05=80.98%	(2.47-1.2)/3.05=41.64%	10																								

RECOVERY	R.Q.D.	FROM (M)	TO (M)	WIDTH MM	PY%	VN%	A	F	NUMBER	ppb	GMT Au	GMT Au	ppm												ppb		
													Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Pb	Sb	Zn	Zn	Hg
1.02/1.33=76.69%	(1.02-0)/1.33=76.69%	119.67	121.00	1.33	2.50	2.50	7	6	41876	132			0.5	111	-1	5	4.64	1941	1	11	81	-5	114	10			
0.9/0.9=100%	(0.9-0.13)/0.9=85.56%	121.00	121.90	0.90	2.50	0.30	5	4	41877	321	0.21		0.7	134	-1	7	5.48	1445	2	13	18	-5	88	15			
2/2.1=95.24%	(2-1.45)/2.1=26.19%	121.90	124.00	2.10	5.00	0.10	5	3	41878	185	0.1		0.5	147	-1	15	6.13	2043	2	11	12	-5	220	55			
1.87/2=93.5%	(1.87-1.16)/2=35.5%	124.00	126.00	2.00	2.50	Tr	5	2	41879	109			0.5	148	-1	18	6.73	2104	2	10	29	-5	201	70			
1.92/2=96%	(1.92-0.78)/2=57%	126.00	128.00	2.00	5.00	Tr	5	3	41880	99			0.4	125	-1	66	6.04	2507	2	9	20	-5	347	130			
2.06/2=103%	(2.06-1.17)/2=44.5%	128.00	130.00	2.00	2.50	0.10	5	4	41881	60			0.5	107	1	78	5.32	2869	2	7	165	-5	367	175			
1.89/2=94.5%	(1.89-1.56)/2=15.5%	130.00	132.00	2.00	2.50	0.30	5	2	41882	96			0.8	108	5	83	5.49	2095	2	8	104	-5	823	80			
2/2=100%	(2-1.26)/2=37%	132.00	134.00	2.00	5.00	0.30	5	2	41883	111			0.9	102	7	105	5.62	2130	2	7	147	8	1119	55			
1.96/2=98%	(1.96-1.43)/2=26.5%	134.00	135.00	2.00	2.50	0.30	4	2	41884 SP, GN	106			1.1	87	16	60	4.72	1762	2	6	520	7	2158	145			
1.96/2=98%	(1.96-1.12)/2=42%	136.00	138.00	2.00	2.50	0.30	5	3	41885	69			0.4	97	4	12	5.27	1715	2	5	34	5	682	60			
1.43/1.46=97.95%	(1.43-0.7)/1.46=50%	138.00	139.46	1.46	5.00	1.00	5	3	41886	61			0.4	89	9	12	6.79	1691	15	8	83	-5	1316	95			
0.78/0.78=89.66%	(0.78-0.23)/0.78=63.22%	139.46	140.33	0.87	2.50	1.00	4	6	41887 SP, GN	79			2.6	73	141	64	8.04	2205	6	22	878	19	18406	520			
0.18/0.98=18.37%	(0.18-0)/0.98=18.37%	140.33	141.31	0.98	2.50	5.00	9	10	41888 SP, GN	35			1.3	58	215	32	4.27	1977	-1	7	1254	49	20000	2.55	600		
0.63/0.64=98.44%	(0.63-0.31)/0.64=50%	141.31	141.94	0.63	2.50	2.50	6	3	41889	54			2.3	79	26	15	5.56	2021	-1	7	1729	-5	3328	250			
0.58/1.47=39.46%	(0.58-0)/1.47=39.46%	141.94	143.41	1.47	2.50	2.50	9	10	41890 SP	166	0.17		4.7	90	99	175	6.66	1646	1	9	3869	26	11188	650			
1.57/1.59=98.74%	(1.57-1.47)/1.59=6.29%	143.41	145.00	1.59	5.00	0.00	4	2	41891	135			2.9	132	26	145	5.85	1637	2	8	1666	7	3483	220			
1.88/2=94%	(1.88-1.3)/2=29%	145.00	147.00	2.00	5.00	0.10	4	3	41892	126			1.9	111	12	112	6.12	1865	2	7	1185	-5	1846	130			
2/2=100%	(2-0.96)/2=52%	147.00	149.00	2.00	5.00	0.30	4	3	41893	161	0.17		2.7	110	25	341	6.55	1943	1	8	1489	6	3393	195			
1.93/2=96.5%	(1.93-1.24)/2=24.5%	149.00	151.00	2.00	5.00	0.30	4	4	41894 SP, GN	161	0.14		3.4	102	51	240	6.7	1922	2	8	2067	14	6312	280			
2/2=100%	(2-0.83)/2=58.5%	151.00	153.00	2.00	2.50	0.30	5	3	41895	115			1.6	97	13	134	5.65	1539	2	13	765	-5	1721	220			
0.88/0.95=92.63%	(0.88-0.21)/0.95=70.53%	153.00	153.95	0.35	5.00	0.10	5	4	41896	165	0.1		1.5	83	13	119	5.97	1293	3	11	203	-5	1763	90			
0.58/0.58=100%	(0.58-0)/0.58=100%	153.95	154.53	0.58	5.00	5.00	8	10	41897 SP, GN	708	0.72		15.4	212	190	197	7.04	1079	3	11	4694	47	20000	2.31	1150		
1.09/1.37=79.56%	(1.09-0.26)/1.37=60.58%	154.53	155.90	1.37	5.00	0.30	6	4	41898	818	1.27		14.4	102	42	71	4.92	966	3	11	2658	12	4907	340			
0.17/0.17=100%	(0.17-0)/0.17=100%	155.90	156.07	0.17	2.50	30.00	9	6	41899 SP, GN	3713	4.22	124.5	50	240	1115	1626	7.51	2915	-1	33	10000	5.5	303	20000	13.7	4600	
0.9/0.9=100%	(0.9-0.2)/0.9=77.78%	156.07	156.97	0.90	2.50	0.30	6	6	41900 SP	234	0.24		2.5	85	23	94	6.05	977	2	16	754	11	2813	135			

RECOVERY	R.D.	SAMPLE													SAMPLE																				
		FROM	TO	WIDTH	PY%	VN%	A	F	NUMBER	ppb		GMT		GMT/FA		GMT/AA		ppm		ppm		ppm		pct		ppm		ppm		ppm		pct		ppb	
										Au	Au	Ag	Ag	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Sb	Zn	Zn	Hg								
1.18/1.18=100%	(1.18-0.24)/1.18=79.66%	8.23	9.41	1.18	2.50	0.10	5	7	41901	34		0.5	86	-1	134	5.88	935	2	13	68	-5	164	5												
1.42/1.59=89.31%	(1.42-0)/1.59=89.31%	9.41	11.00	1.59	2.50	1.00	8	8	41902 SP	18		0.6	86	1	96	6.5	945	2	14	76	-5	278	15												
1.32/2.1=57.14%	(1.32-0.33)/2.1=47.14%	11.00	13.10	2.10	2.50	0.10	7	4	41903	28		0.5	93	-1	43	6.86	853	2	15	66	-5	216	15												
1.08/1.9=98.95%	(1.08-0.31)/1.9=82.63%	13.10	15.00	1.90	2.50	0.10	5	3	41904 SP	112		1.3	84	7	151	5.46	1207	2	12	558	5	828	30												
1.85/2=92.5%	(1.85-0.39)/2=73%	15.00	17.00	2.00	2.50	Tr	5	6	41905	226	0.38	2.3	60	14	130	5.75	947	2	14	601	-5	1416	80												
1.99/2=99.5%	(1.99-1.07)/2=46%	17.00	19.00	2.00	2.50	Tr	4	3	41906	263	0.45	2.3	113	5	161	6.88	1336	2	13	291	-5	590	75												
1.91/2=95.5%	(1.91-0.57)/2=67%	19.00	21.00	2.00	2.50	Tr	4	4	41907	287	0.48	2.4	110	7	164	6.82	1427	3	14	414	-5	710	90												
1.45/2=72.5%	(1.45-0)/2=72.5%	21.00	23.00	2.00	2.50	Tr	4	6	41908	356	0.51	2.8	68	5	182	6.88	1874	2	13	233	-5	649	50												
1.61/2=80.5%	(1.61-0.35)/2=63%	23.00	25.00	2.00	2.50	Tr	4	6	41909	81		1.2	94	10	255	5.88	1231	1	13	976	-5	1146	120												
1.95/2=97.5%	(1.95-0.7)/2=62.5%	25.00	27.00	2.00	2.50	Tr	5	3	41910	152	0.24	1	128	3	35	6.34	1388	3	14	191	-5	313	35												
1.93/2=96.5%	(1.93-0.53)/2=70%	27.00	29.00	2.00	2.50	0.00	5	3	41911	123		1.3	138	5	107	6.93	1298	3	14	670	-5	545	60												
1.92/2=96%	(1.92-0.95)/2=48.5%	29.00	31.00	2.00	2.50	Tr	5	3	41912	337	0.55	2.3	168	4	119	6.87	1284	3	14	181	-5	377	20												
2.06/2=103%	(2.06-1.54)/2=26%	31.00	33.00	2.00	2.50	Tr	5	2	41913	165	0.27	1.3	94	3	228	6.7	1196	3	14	231	-5	410	30												
1.83/2=91.5%	(1.83-1.11)/2=36%	33.00	35.00	2.00	5.00	0.10	5	2	41914	45		0.7	122	4	111	6.67	1062	2	14	287	-5	583	25												
2/2=100%	(2-1.52)/2=24%	35.00	37.00	2.00	5.00	Tr	5	2	41915	68		0.7	93	4	164	7.31	1171	2	17	258	-5	578	30												
1.93/2=96.5%	(1.93-0.84)/2=54.5%	37.00	39.00	2.00	5.00	Tr	5	3	41916	125		0.9	125	2	102	7.49	1028	2	14	81	-5	174	10												
1.85/2=92.5%	(1.85-0.74)/2=55%	39.00	41.00	2.00	2.50	Tr	5	3	41917	85		0.6	70	5	92	7.52	1289	2	13	87	-5	279	10												
2/2=100%	(2-0.13)/2=93.5%	41.00	43.00	2.00	5.00	0.10	6	6	41918	452	0.68	3.5	79	19	285	7.95	769	2	13	1355	-5	1884	80												
2.08/2=104%	(2.08-0.4)/2=84%	43.00	45.00	2.00	5.00	0.00	5	3	41919	68		0.6	57	3	63	6.57	973	2	11	43	-5	234	-5												
1.9/2=95%	(1.9-0.32)/2=73%	45.00	47.00	2.00	5.00	0.00	6	4	41920	74		1.1	67	4	138	6.68	744	2	12	134	-5	429	15												
1.98/2=99%	(1.98-0.66)/2=66%	47.00	49.00	2.00	5.00	0.00	6	3	41921	67		1.1	55	4	101	6.25	980	2	13	137	-5	441	10												
1.93/2=96.5%	(1.93-0.61)/2=66%	49.00	51.00	2.00	5.00	0.10	6	3	41922	44		0.6	50	-1	102	5.65	915	4	13	66	-5	145	15												
1.95/2=97.5%	(1.95-0.5)/2=72.5%	51.00	53.00	2.00	5.00	Tr	6	3	41923	13		0.4	40	-1	168	6.28	749	1	11	65	-5	150	5												
1.97/2=98.5%	(1.97-0.37)/2=80%	53.00	55.00	2.00	5.00	0.00	6	4	41924	10		0.3	41	1	49	5.35	614	2	9	55	-5	107	5												
1.85/2=92.5%	(1.85-0.2)/2=82.5%	55.00	57.00	2.00	5.00	0.10	6	4	41925	28		0.5	56	-1	32	6.14	765	2	16	44	-5	129	10												
2/2=100%	(2-0.53)/2=73.5%	57.00	59.00	2.00	5.00	0.00	5	3	41926	14		0.6	46	4	82	5.29	950	2	12	117	-5	300	10												
2.87/2.87=100%	(2.87-0.43)/2=1.22%	59.00	61.87	2.87	5.00	0.10	6	4	41927	20		0.4	46	1	36	6.05	670	2	13	20	-5	126	10												
0.48/1.22=39.34%	(0.48-0)/1.22=39.34%	61.87	63.09	1.22	5.00	0.10	6	4	41928	54		1.2	60	-1	48	5.7	668	1	14	279	-5	137	5												
1.75/1.91=91.62%	(1.75-0.84)/1.91=47.64%	63.09	65.00	1.91	5.00	Tr	6	3	41929	50		0.9	51	-1	95	6.06	970	2	12	58	-5	159	5												
2/2=100%	(2-1.05)/2=42.5%	65.00	67.00	2.00	5.00	Tr	4	3	41930	25		0.6	49	2	209	5.86	985	2	11	148	-5	346	25												
2/2=100%	(2-1)/2=50%	67.00	69.00	2.00	2.50	0.10	4	3	41931	12		0.8	56	12	91	5.53	1059	1	12	631	-5	1316	60												
2/2=100%	(2-1.27)/2=36.5%	69.00	71.00	2.00	5.00	0.30	5	2	41932 GN	22		0.9	31	5	43	6.44	1106	1	11	250	-5	525	30												
1.28/1.3=98.46%	(1.28-0.75)/1.3=40.77%	71.00	72.30	1.30	5.00	0.00	6	2	41933	32		0.8	33	2	38	5.17	902	2	9	211	-5	262	55												
1.76/2.98=59.06%	(1.76-0.34)/2.98=47.65%	72.30	75.28	2.98	10.00	0.10	7	8	41934 SP	190	0.34	5.2	51	30	83	6.57	314	2	12	1537	9	3467	240												
1.35/1.42=95.07%	(1.35-0.15)/1.42=84.51%	75.28	76.70	1.42	5.00	0.30	7	8	41935 SP	172	0.27	3.3	35	62	170	5.54	357	3	14	321	14	7235	490												
1.29/1.3=99.23%	(1.29-0.59)/1.3=53.85%	76.70	78.00	1.30	2.50	Tr	6	3	41936	187	0.31	2.9	33	26	89	4.29	926	1	9	20	-5	3078	270												
1.98/2=99%	(1.98-1.52)/2=23%	78.00	80.00	2.00	2.50	0.10	5	2	41937	73		1.1	34	10	81	4.02	993	2	8	77	-5	1150	80												
1.94/2=97%	(1.94-1.43)/2=25.5%	80.00	82.00	2.00	5.00	0.00	5	2	41938	146		2.1	40	17	67	5.37	1194	1	10	181	5	2015	130												
1.94/2=97%	(1.94-1.09)/2=42.5%	82.00	84.00	2.00	5.00	0.10	5	3	41939 SP	2486	3.91	31	45	61	265	4.81	1125	1	11	104	15	7489	510												
1.66/1.66=100%	(1.66-1)/1.66=39.76%	84.00	85.66	1.66	5.00	0.10	6	2	41940 SP	541	0.93	8	45	10	263	7.17	740	6	11	19	-5	1283	95												
1.54/1.81=85.08%	(1.54-0.25)/1.81=71.27%	85.66	87.47	1.81	2.50	5.00	7	5	3	41941 SP	4922	4.9	37.7	50	65	259	4.31	1402	-1	9	209	16	7897	850											
1.63/1.95=83.59%	(1.63-0.36)/1.95=65.13%	87.47	89.42	1.95	5.00	5.00	8	9	41942	9311	12.6	60.3	50	37	4	56	4.53	1416	2	10	4	-5	575	185											
1.56/1.58=98.75%	(1.56-1.21)/1.58=22.15%	89.42	91.00	1.58	5.00	0.10	5	2	41943	444	0.65	3	71	25	180	6.73	1489	2	10	12	-5	3106	170												
2/2=100%	(2-1.37)/2=31.5%	91.00	93.00	2.00	5.00	0.10	5	3	41944	274	0.45	1.4	44	17	134	5.67	1224	1	11	3	-5	2115	80												

RECOVERY	R.Q.D.	FROM	TO	WIDTH	PY%	VN%	A	F	NUMBER	ppb	GMT	GMT/FA	GMT/AA	ppm	ppm	ppm	ppm	pct	ppm	ppm	ppm	ppm	ppm	ppm	pct	ppb					
															Au	Au	Ag	Ag	Ag	As	Cd	Cu	Fe	Mn	Mo	Ni	Pb	Sb	Zn	Zn	Hg
															(a)																
0.34/0.34=100%	(0.34-0)/0.34=100%	108.32	108.66	0.34	10.00	10.00	8	7	41954 SP, CP10000	78.5	2058.9			50	295	734	9004	10	1914	9	12	2212	197	20000	9.95	5000					
1.33/1.76=75.57%	(1.33-0.49)/1.76=47.73%	108.66	110.42	1.76	2.50	5.00	7	6	41955 SP	7944	11.4	198.9		50	84	28	367	4.62	1486	2	11	152	11	3632		390					
1.97/1.98=99.49%	(1.97-0.64)/1.98=67.17%	110.42	112.40	1.98	1.00	0.30	4	4	41956	238	0.38			1.4	65	2	216	1.92	1584	-1	7	18	7	264		210					
1.29/1.67=77.25%	(1.29-0)/1.67=77.25%	112.40	114.07	1.67	2.50		Tr	8	10	41957 SP	277	0.58			4.4	111	16	85	4.54	588	3	10	386	10	2150		170				
1.28/1.55=82.58%	(1.28-0.2)/1.55=69.68%	114.07	115.62	1.55	2.50	1.00	7	8	41958	238	0.41			1.3	172	10	150	6.48	1574	2	13	54	9	1357		80					
2.26/2.33=97%	(2.26-1.19)/2.33=45.92%	115.62	117.95	2.33	2.50	1.00	5	3	41959	143				0.9	127	18	112	5.57	1883	2	11	43	13	2461		150					
0.95/0.95=100%	(0.95-0.43)/0.95=54.74%	117.95	118.87	0.92	2.50	1.00	5	4	41960 SP	221	0.41			1.6	119	105	138	4.74	1764	1	12	230	34	12962		530					
1.12/1.13=99.16%	(1.12-0.39)/1.13=64.6%	118.87	120.00	1.13	2.50	0.30	4	3	41961	326	0.51			3	221	12	305	5.32	1673	1	14	803	9	1764		110					
1.65/1.62=101.85%	(1.65-0.61)/1.62=64.2%	120.00	121.62	1.62	2.50	0.10	4	3	41962	238	0.34			2.3	202	12	311	5.15	1702	1	18	590	11	1748		110					

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Geological Lab Report

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-05374.0

DATE PRINTED: 31-AUG-89

PROJECT: 89BC019

PAGE 1B

SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Zn PPM	Hg PPB
R2 89HANK5124		204	32	2600
R2 89HANK5125		37	22	750
R2 89HANK5126		31	662	370
R2 89HANK5127		16	59	120
R2 89HANK5128		54	147	150
R2 89HANK5129		123	54	650
R2 89HANK5130		8	2065	220
R2 89HANK5131		<5	44	115
R2 89HANK5132		<5	96	60
R2 89HANK5133		<5	98	70
R2 89HANK5134		140	9299	2800
R2 89HANK5150		18	2322	115
R2 89HANK5151		8	2190	190
R2 89HANK5152		60	18198	1350
R2 89HANK5153		22	3583	300
R2 89HANK5154		<5	>20000	700
R2 89HANK5155		163	>20000	2050
R2 89HANK5156		7	913	190
D2 41201				
D2 41202				
D2 41203				
D2 41204				
D2 41205				
D2 41206				
D2 41207				
D2 41208				
D2 41209				
D2 41210				
D2 41211				
D2 41212				
D2 41213				
D2 41214				
D2 41215				
D2 41216				
D2 41217				
D2 41218				
D2 41219				
D2 41220				
D2 41221				
D2 41222				

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-05374.0

~~DATE PRINTED: 31 AUG 89~~

PROJECT: 89BC019

PAGE 2A

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**Geochemical
Lab Report**

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-05374.0

DATE PRINTED: 31-AUG-89

PROJECT: 89BC019

PAGE 2B

SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Zn PPM	Hg PPB
------------------	------------------	-----------	-----------	-----------

D2 41223
D2 41224
D2 41225
D2 41226
D2 41227

D2 41228
D2 41229
D2 41230
D2 41231
D2 41232

D2 41233
D2 41234
D2 41235
D2 41236
D2 41237

D2 41238
D2 41239
D2 41240
D2 41241
D2 41242

D2 41243
D2 41244
D2 101001
D2 101002
D2 101003

D2 101004
D2 101005
D2 101006
D2 101007
D2 101008

D2 101009
D2 101010
D2 101011
D2 101012
D2 101013

D2 101014
D2 101015
D2 101016
D2 101017
D2 101018

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-05374.0

DATE PRINTED: 31-AUG-89

PROJECT: 89BC019

PAGE 3A

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-05374.0

DATE PRINTED: 31-AUG-89

PROJECT: 89BC019

PAGE 3B

SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Zn PPM	Hg PPB
------------------	------------------	-----------	-----------	-----------

D2 101019

D2 101020

D2 101021

D2 101022

D2 101023

D2 101024

D2 101025

D2 101026

D2 101027

D2 101028

D2 101029

D2 101030

D2 101031

D2 101032

D2 101033

D2 101034

D2 101035

D2 101036

D2 101037

D2 101038

D2 101039

D2 101040

D2 101041

D2 101042

D2 101043

D2 101044

D2 101045

D2 101046

D2 101047

D2 101048

D2 101049

D2 101050

D2 101051

D2 101052

D2 101053

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

REPORT: V89-06026.0

PROJECT: 89BC019

PAGE 1A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41245		67	1.1	45	<1	308	4.89	784	2	17	78	11
D2 41246		52	2.8	69	2	149	5.91	325	4	21	197	14
D2 41247		40	1.7	34	1	126	2.30	60	3	22	127	14
D2 41248		93	2.1	34	4	89	3.30	166	2	24	273	14
D2 41249		93	2.9	112	4	196	5.12	397	2	33	384	15
D2 41250		61	1.5	136	6	171	5.83	789	2	24	483	19
D2 41251		30	1.0	85	<1	90	3.62	1097	<1	23	127	15
D2 41252		22	1.2	92	6	57	5.00	1073	2	29	599	16
D2 41253		73	2.3	100	3	139	5.59	687	2	24	387	14
D2 41254		231	2.6	90	3	85	5.07	314	3	18	274	15
D2 41255		109	1.6	97	<1	37	6.01	420	3	7	38	13
D2 41256		204	1.5	115	<1	49	6.39	250	4	13	57	11
D2 41257		697	3.9	93	9	402	7.16	608	2	7	472	17
D2 41258		359	1.4	86	<1	23	7.23	623	3	12	47	14
D2 41259		51	0.5	79	<1	117	7.39	682	2	17	32	13
D2 41260		90	1.2	134	<1	112	7.31	866	3	24	115	14
D2 41261		167	1.9	120	1	64	7.71	812	2	29	167	16
D2 41262		127	1.5	111	5	243	6.68	707	2	32	156	18
D2 41263		214	3.6	69	3	170	4.80	1085	2	25	325	18
D2 41264		50	0.9	73	<1	173	6.27	723	2	12	35	14
D2 41265		28	0.4	49	<1	159	4.66	946	<1	9	30	14
D2 41266		437	1.5	105	1	23	7.18	395	4	11	100	16
D2 41267		512	3.2	129	3	59	6.05	343	5	14	265	16
D2 41268		189	0.8	89	<1	25	6.17	693	3	13	299	17
D2 41269		455	1.5	121	<1	64	5.13	637	3	11	50	16
D2 41270		874	2.3	181	<1	107	6.50	449	3	15	71	18
D2 41271		146	1.1	74	<1	61	6.18	688	2	9	30	16
D2 41272		124	0.9	113	<1	45	5.29	596	2	9	28	18
D2 41273		334	3.5	145	<1	114	6.19	688	2	10	61	15
D2 41274		449	4.7	82	12	191	5.72	949	2	17	592	18
D2 41275		37	1.9	61	<1	175	6.03	1126	2	31	52	13
D2 41276		21	0.7	61	<1	11	5.94	596	2	20	40	13
D2 41277		27	0.5	36	<1	6	4.53	278	2	11	37	13
D2 41278		80	0.5	55	<1	15	6.06	367	2	14	52	12
D2 41279		334	0.6	57	<1	18	7.31	487	2	10	420	12
D2 41280		48	0.5	48	<1	22	6.70	480	3	10	44	15
D2 41281		19	0.4	24	<1	12	6.46	710	2	10	15	<5
D2 41282		59	0.7	33	<1	43	4.67	651	2	11	17	<5
D2 41283		236	3.3	40	3	62	5.50	603	3	10	263	<5
D2 41284		2172	2.9	37	6	87	3.50	592	2	8	3287	7

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

PROJECT: 89BC019

PAGE 18

REPORT: V89-06026.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
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D2 41245		147	70
D2 41246		271	65
D2 41247		149	55
D2 41248		518	105
D2 41249		446	110

D2 41250		767	210
D2 41251		120	65
D2 41252		900	170
D2 41253		389	90
D2 41254		316	85

D2 41255		29	55
D2 41256		53	35
D2 41257		1148	120
D2 41258		52	35
D2 41259		45	30

D2 41260		163	40
D2 41261		178	70
D2 41262		601	105
D2 41263		379	130
D2 41264		52	50

D2 41265		61	50
D2 41266		162	45
D2 41267		422	65
D2 41268		61	20
D2 41269		72	35

D2 41270		58	35
D2 41271		41	25
D2 41272		36	25
D2 41273		76	30
D2 41274		1609	225

D2 41275		70	70
D2 41276		28	20
D2 41277		7	25
D2 41278		18	15
D2 41279		15	15

D2 41280		23	20
D2 41281		25	25
D2 41282		44	40
D2 41283		417	65
D2 41284		775	110

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

REPORT: V89-06026.0

PROJECT: 89BC019

PAGE 2A

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

PROJECT: 89BC019

PAGE 28

REPORT: V89-06026.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41285		630	120
D2 41286		230	65
D2 41287		11270	950
D2 41288		258	55
D2 41289		6159	650
D2 41290		1119	180
D2 41291		1332	245
D2 41292		4449	550
D2 41293		872	440
D2 41294		133	45
D2 41295		1161	205
D2 41296		102	40
D2 41297		1724	300
D2 41298		1296	160
D2 41299		6106	600
D2 41300		3213	400
D2 41301		107	95
D2 41302		312	75
D2 41303		271	110
D2 41304		776	505
D2 41305		626	310
D2 41306		99	110
D2 41307		59	90
D2 41308		56	60
D2 41309		927	310
D2 41310		72	170
D2 41311		74	290
D2 41312		76	140
D2 41313		80	80
D2 41314		111	495
D2 41315			
D2 41316			
D2 41317			
D2 41318			
D2 41319			
D2 41320			
D2 41321			
D2 41322			
D2 41323			
D2 41324			

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

REPORT: V89-06026.0

PROJECT: 89BC019

PAGE 3A

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

REPORT: V89-06026.0

PROJECT: 89BC019

PAGE 3B

SAMPLE NUMBER	ELEMENT	Zn PPM	Hg PPB
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D2 41325
D2 41326
D2 41327
D2 41328
D2 41329

D2 41330
D2 41331
D2 41332
D2 41333
D2 41334

D2 41335
D2 41336
D2 41337
D2 41338
D2 41339

D2 41340
D2 41341
D2 41342
D2 41343
D2 41344

D2 41345
D2 41346
D2 41347
D2 41348
D2 41349

D2 41350
D2 41351
D2 41352
D2 41353
D2 41354

D2 41355
D2 41356
D2 41357
D2 41358
D2 41359

D2 41360
D2 41361
D2 41362
D2 41363
D2 41364

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

PROJECT: 89BC019

PAGE 4A

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 7-SEP-89

REPORT: V89-06026.0

PROJECT: 89BC019

PAGE 4B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
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D2 41365
D2 41366
D2 41367
D2 41368
D2 41369

D2 41370
D2 41371
D2 41372
D2 41373
D2 41374

D2 41375

REPORT: V89-D6026.6

DATE PRINTED: 12-SEP-89

PROJECT: 89BC019

PAGE 1

SAMPLE NUMBER	ELEMENT UNITS	Au GMT	Ag GMT	SAMPLE NUMBER	ELEMENT UNITS	Au GMT	Ag GMT
D2 41254		0.31		D2 41329		0.27	
D2 41256		0.24		D2 41330		0.17	
D2 41257		0.96		D2 41331		2.02	
D2 41258		0.45		D2 41332		0.24	
D2 41261		0.10		D2 41333		0.17	
D2 41263		0.24		D2 41334		0.17	
D2 41266		0.55		D2 41339		66.46\$	
D2 41267		0.62		D2 41341		0.31	
D2 41268		0.24		D2 41342		0.14	
D2 41269		0.51		D2 41344		0.48	
D2 41270		1.03		D2 41345		1.23	
D2 41273		0.38		D2 41346		6.48	
D2 41274		0.41		D2 41347		1.10	
D2 41279		0.21		D2 41348		19.61	
D2 41283		0.31		D2 41349		1.85	
D2 41284		3.12\$		D2 41352		1.30	
D2 41285		0.62		D2 41356		3.53	
D2 41287		0.34		D2 41357		0.21	
D2 41288		0.21		D2 41359		0.14	
D2 41289		0.48		D2 41364		0.48	
D2 41290		0.38		D2 41374		0.27	
D2 41291		2.16		D2 41375		0.48	
D2 41292		1.68					
D2 41293		1.89					
D2 41295		0.51					
D2 41297		1.65					
D2 41298		1.41					
D2 41299		1.13					
D2 41300		3.50	42.9				
D2 41302		0.27					
D2 41303		0.48					
D2 41304		0.58					
D2 41305		0.65					
D2 41306		0.38					
D2 41308		0.17					
D2 41309		1.58					
D2 41320		0.55					
D2 41321		2.78					
D2 41323		0.17					
D2 41324		0.51					

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 1A

REPORT: V89-06051.0

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41376		12	0.4	58	<1	121	5.47	1060	3	17	<2	<5
D2 41377		20	0.7	84	<1	132	6.30	956	3	20	41	<5
D2 41378		70	1.7	81	2	123	5.33	945	3	18	176	<5
D2 41379		95	2.7	87	3	263	5.95	583	3	22	225	<5
D2 41380		1398	25.9	77	14	83	5.28	777	3	20	2001	10
D2 41381		36	0.5	29	<1	10	5.40	1060	1	11	19	<5
D2 41382		31	0.5	33	<1	36	5.55	1025	2	7	70	<5
D2 41383		47	0.5	41	<1	98	5.36	986	2	10	36	<5
D2 41384		33	1.1	34	<1	68	5.28	783	2	9	7	<5
D2 41385		79	1.5	55	<1	121	4.49	1381	1	9	42	<5
D2 41386		65	1.0	57	<1	124	5.07	1343	2	10	55	<5
D2 41387		152	2.6	81	4	146	5.75	1187	1	10	264	<5
D2 41388		837	20.5	123	109	866	4.68	808	1	10	8642	23
D2 41389		252	2.2	41	3	51	3.58	1060	1	7	776	<5
D2 41390		359	3.9	89	11	106	4.47	934	2	5	864	<5
D2 41391		5657	>50.0	63	88	323	4.36	2759	1	8	3174	15
D2 41392		304	2.0	68	<1	16	5.92	855	2	12	40	<5
D2 41393		193	1.5	86	<1	17	6.35	928	2	16	34	<5
D2 41394		58	0.8	34	<1	40	5.66	1093	3	28	19	<5
D2 41395		2627	42.5	87	152	1526	4.33	3174	2	8	>100000	89
D2 41396		2496	6.3	96	3	114	3.48	4955	1	5	343	<5
D2 41397		1548	24.1	102	161	668	4.28	5915	<1	8	9101	35
D2 41398		507	19.6	119	7	92	6.88	1835	3	34	4052	<5
D2 41399		107	1.7	68	<1	22	7.09	1525	2	33	107	<5
D2 41400		401	1.3	50	<1	74	6.33	1073	3	31	75	<5
D2 41401		388	7.2	89	40	258	5.87	1467	2	28	2446	5
D2 41402		91	0.7	99	<1	144	6.49	1674	1	30	12	<5
D2 41403		39	1.3	74	<1	227	7.20	1381	4	35	<2	<5
D2 41404		78	0.6	40	<1	123	7.01	1088	3	27	<2	<5
D2 41405		147	0.3	47	<1	12	4.91	842	3	20	<2	<5
D2 41406		29	<0.2	15	<1	10	6.01	925	2	14	<2	<5
D2 41407		58	0.2	44	<1	58	8.77	841	2	13	<2	<5
D2 41408		41	0.3	15	<1	29	6.32	960	2	9	25	<5
D2 41409		53	2.0	19	2	32	6.61	757	2	11	144	<5
D2 41410		1115	>50.0	101	265	4119	6.92	748	6	5	>100000	66
D2 41411		49	1.6	20	1	20	7.33	688	3	10	75	<5
D2 41412		434	1.6	34	<1	24	7.71	678	5	9	47	<5
D2 41413		135	1.3	26	<1	11	6.18	728	3	10	73	<5
D2 41414		43	1.1	18	3	19	7.48	782	4	10	145	<5
D2 41415		36	0.5	13	2	21	7.61	777	3	9	143	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 1B

REPORT: V89-06051.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41376		33	45
D2 41377		104	50
D2 41378		315	90
D2 41379		413	95
D2 41380		1573	200
D2 41381		63	40
D2 41382		168	50
D2 41383		100	55
D2 41384		80	40
D2 41385		187	75
D2 41386		175	55
D2 41387		555	110
D2 41388		12811	1900
D2 41389		429	70
D2 41390		1438	310
D2 41391		10019	2150
D2 41392		318	115
D2 41393		138	35
D2 41394		95	30
D2 41395		17858	1950
D2 41396		484	190
D2 41397		18664	2450
D2 41398		904	210
D2 41399		146	60
D2 41400		121	30
D2 41401		4761	270
D2 41402		82	40
D2 41403		66	105
D2 41404		37	35
D2 41405		45	25
D2 41406		38	20
D2 41407		51	30
D2 41408		68	35
D2 41409		218	30
D2 41410		>20000	750
D2 41411		165	20
D2 41412		133	25
D2 41413		49	30
D2 41414		344	40
D2 41415		233	45

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 2A

REPORT: V89-06051.0

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41416		34	0.5	20	<1	24	6.47	714	3	10	18	<5
D2 41417		130	0.7	40	<1	55	6.69	773	3	10	<2	<5
D2 41418		1304	1.3	33	2	15	4.62	477	3	9	82	<5
D2 41419		230	1.2	45	<1	22	6.10	774	4	11	10	<5
D2 41420		63	0.9	18	4	43	6.72	876	3	8	122	<5
D2 41421		41	0.9	29	<1	39	7.64	1021	4	10	143	<5
D2 41422		115	2.8	16	35	101	6.62	910	3	8	20000	<5
D2 41423		624	11.0	109	344	633	6.21	1514	5	8	>100000	95
D2 41424		138	2.2	60	9	83	6.69	1279	3	9	636	<5
D2 41425		103	2.1	72	1	32	6.66	1252	4	9	87	<5
D2 41426		52	1.9	17	2	25	6.45	784	4	9	142	<5
D2 41427		87	1.7	22	<1	20	6.40	645	3	9	21	<5
D2 41428		358	1.3	23	2	57	6.31	690	4	9	45	<5
D2 41429		64	1.3	31	<1	41	6.38	1413	3	8	<2	<5
D2 41430		282	2.0	17	3	336	5.82	1048	3	10	58	<5
D2 41431		162	3.7	58	2	52	7.79	1478	5	9	220	<5
D2 41432		447	8.0	100	20	151	5.75	965	3	12	767	<5
D2 41433		313	12.9	110	3	380	5.81	1011	3	9	270	<5
D2 41434		688	16.5	61	59	245	6.42	708	5	11	1018	17
D2 41435		2636	>50.0	107	418	4495	8.29	2256	5	14	1216	261
D2 41436		36	2.5	21	6	61	6.79	1656	3	10	52	<5
D2 41437		2875	27.9	53	40	92	8.75	1266	3	9	496	5
D2 41438		>10000	>50.0	144	195	1657	7.35	1651	7	7	2722	77
D2 41439		186	5.1	99	3	126	6.30	1042	3	8	271	<5
D2 41440		47	1.7	39	<1	94	6.07	1105	3	7	<2	<5
D2 41441		20	0.6	41	<1	48	7.39	924	3	9	6	<5
D2 41442		101	2.3	31	1	71	7.01	888	3	10	145	<5
D2 41443		33	0.8	44	<1	161	7.94	1085	3	10	8	<5
D2 41444		38	2.4	26	9	143	6.78	943	3	10	509	<5
D2 41445		77	6.9	25	34	104	7.66	1069	3	8	3864	<5
D2 41446		33	1.7	11	5	110	7.49	1123	4	8	425	<5
D2 41447		20	0.8	13	<1	150	8.66	1037	4	9	114	<5
D2 41448		27	0.6	30	<1	117	8.17	1019	4	7	75	<5
D2 41449		53	1.8	47	9	163	6.35	818	3	8	731	<5
D2 41450		214	4.8	77	12	301	6.80	723	4	10	678	<5
D2 41451		5831	>50.0	79	4	759	4.29	298	5	5	227	<5
D2 41452		450	5.0	26	5	63	1.89	310	4	7	116	<5
D2 41453		132	6.3	13	2	460	4.45	347	9	31	119	<5
D2 41454		122	2.5	64	<1	32	7.08	776	3	9	44	<5
D2 41455		268	1.8	58	<1	108	4.71	1131	3	7	21	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 2B

REPORT: V89-06051.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41416		58	25
D2 41417		39	20
D2 41418		274	40
D2 41419		39	40
D2 41420		452	55
D2 41421		118	60
D2 41422		3982	425
D2 41423		>20000	2350
D2 41424		1085	160
D2 41425		163	55
D2 41426		265	50
D2 41427		51	30
D2 41428		251	30
D2 41429		61	30
D2 41430		394	150
D2 41431		285	90
D2 41432		2362	310
D2 41433		402	145
D2 41434		7402	1000
D2 41435		>20000	4300
D2 41436		815	100
D2 41437		5078	490
D2 41438		>20000	>5000
D2 41439		390	240
D2 41440		83	130
D2 41441		70	50
D2 41442		213	475
D2 41443		95	700
D2 41444		1053	1300
D2 41445		3947	3200
D2 41446		634	580
D2 41447		114	470
D2 41448		109	545
D2 41449		1213	1100
D2 41450		1478	1900
D2 41451		440	1300
D2 41452		732	150
D2 41453		206	155
D2 41454		107	180
D2 41455		93	155

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 3A

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 38

REPORT: V89-06051.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41456		116	225
D2 41457		424	290
D2 41458		289	65
D2 41459		17150	1550
D2 41460		693	175
D2 41461		687	150
D2 41462		167	80
D2 41463		53	70
D2 41464		91	50
D2 41465		183	30
D2 41466		47	160
D2 41467		50	90
D2 41468		507	275
D2 41469		91	240
D2 41470		423	165
D2 41471		98	100
D2 41472		129	210
D2 41473		68	75
D2 41474		141	185
D2 41475			
D2 41476			
D2 41477			
D2 41478			
D2 41479			
D2 41480			
D2 41481			
D2 41482			
D2 41483			
D2 41484			
D2 41485			
D2 41486			
D2 41487			
D2 41488			
D2 41489			
D2 41490			
D2 41491			
D2 41492			
D2 41493			
D2 41494			
D2 41495			

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BCN19

PAGE 4A

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 4B

REPORT: V89-06051.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
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D2 41496
D2 41497
D2 41498
D2 41499
D2 41500

D2 41501
D2 41502
D2 41503
D2 41504
D2 41505

D2 41506
D2 41507
D2 41508
D2 41509
D2 41510

D2 41511
D2 41512
D2 41513
D2 41514
D2 41515

D2 41516
D2 41517
D2 41518
D2 41519
D2 41520

D2 41521
D2 41522
D2 41523
D2 41524
D2 41525

D2 41526
D2 41527
D2 41528
D2 41529
D2 41530

D2 41531
D2 41532
D2 41533
D2 41534
D2 41535

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SEP-89

PROJECT: 89BC019

PAGE 5A

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Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 16-SFP-89

PROJECT: 89BC019

PAGE 5B

REPORT: V89-06051.R

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
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D2 41536

D2 41537

D2 41538

D2 41539

D2 41540

D2 41541

D2 41542

D2 41543

D2 41544

D2 41545

D2 41546

D2 41547

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A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06051.6

DATE PRINTED: 22-SEP-89

PROJECT: 89BC019

PAGE 1

SAMPLE NUMBER	ELEMENT	AU UNITS	Ag GMT	Pb PCT	Zn PCT	SAMPLE NUMBER	ELEMENT	AU UNITS	Ag GMT	Pb PCT	Zn PCT
D2 41380		1.92				D2 41473		0.69			
D2 41387		0.17				D2 41481		0.24			
41388		0.82				D2 41487		0.24			
D2 41389		0.41				D2 41488		0.21			
D2 41390		0.41				D2 41489		0.34			
D2 41391		5.11*	114.9			D2 41499		1.27			
D2 41392		0.45				D2 41500		0.62			
41393		0.21				D2 41524		0.31			
41395		2.43		1.31		D2 41525		0.21			
D2 41396		2.88				D2 41530		0.17			
D2 41397		1.68				D2 41532		0.17			
D2 41398		0.58				D2 41535		0.21			
D2 41400		0.41				D2 41537		0.34			
41401		0.38				D2 41538		3.46			
D2 41410		1.06	52.5	1.54	2.92	D2 41539		0.96			
D2 41412		0.58				D2 41542		0.24			
41418		1.71				D2 41546		1.17			
D2 41419		0.27				D2 41547		12.75			
D2 41423		0.75		1.55	3.80						
41428		0.45									
D2 41430		0.31									
41431		0.17									
D2 41432		0.51									
D2 41433		0.34									
41434		0.72									
D2 41435		2.98	161.5		4.84						
D2 41437		3.57									
41438		17.59	456.7		2.31						
D2 41439		0.31									
D2 41450		0.21									
D2 41451		5.86	93.9								
D2 41452		0.55									
41455		0.34									
41459		1.13									
D2 41461		0.48									
D2 41464		0.24									
D2 41465		0.31									
D2 41470		0.31									
D2 41471		0.24									
D2 41472		0.58									

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Geological Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 24-SEP-89

REPORT: V89-06097.0

PROJECT: 89BC019

PAGE 1A

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06097.0

DATE PRINTED: 24-SEP-89

PROJECT: 89BC019

PAGE 1B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
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R2 89HANK-5135		7	180
R2 89HANK-5136		210	90
R2 89HANK-5137		16	1600
R2 89HANK-5138		<1	70
R2 89HANK-5139		56	190

R2 89HANK-5157		5	590
R2 89HANK-5158		126	50
R2 89HANK-5159		1668	290
R2 89HANK-5160		1573	310
R2 89HANK-5161		2895	540

R2 89HANK-5162		1224	250
R2 89HANK-5163		83	70
R2 89HANK-5164		108	80
R2 89HANK-5165		69	100
R2 89HANK-5166		79	60

R2 89HANK-5167		68	55
R2 89HANK-5168		55	50
R2 89HANK-5169		51	40
R2 89HANK-5170		69	30
D2 41548			

D2 41549			
D2 41550			
D2 41551			
D2 41552			
D2 41553			

D2 41554			
D2 41555			
D2 41556			
D2 41557			
D2 41558			

D2 41559			
D2 41560			
D2 41561			
D2 41562			
D2 41563			

D2 41564			
D2 41565			
D2 41566			
D2 41567			
D2 41568			

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06097.0

DATE PRINTED: 24-SHP-89

PROJECT: 89BC019

PAGE 2A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41569		19										
D2 41570		17										
D2 41571		114										
D2 41572		113										
D2 41573		68										
D2 41574		36										
D2 41575		121										
D2 41576		33	1.8	9	<1	198	5.04	64	4	18	60	11
D2 41577		61	1.6	57	2	57	7.80	113	4	22	220	9
D2 41578		83	1.8	26	<1	137	6.54	433	2	26	68	17
D2 41579		67	1.2	36	<1	242	6.13	223	2	23	24	10
D2 41580		39	0.8	36	<1	61	4.56	691	2	21	36	7
D2 41581		51	1.4	61	<1	126	5.20	894	2	17	43	10
D2 41582		151	2.2	121	<1	146	7.90	1450	2	50	42	10
D2 41583		118	4.6	63	12	165	6.87	1328	2	56	133	8
D2 41584		41	1.0	49	<1	35	4.78	1376	2	19	76	7
D2 41585		62	0.8	120	<1	30	5.76	882	2	15	62	9
D2 41586		50	1.4	155	1	26	5.38	1242	2	26	119	<5
D2 41587		201	5.3	183	10	333	5.72	830	2	40	756	8
D2 41588		1111	49.9	184	394	2297	5.93	887	<1	36	>100000	153
D2 41589		147	3.5	147	3	131	5.05	342	2	37	154	6
D2 41590		170	4.1	109	2	125	3.77	985	2	22	277	7
D2 41591		114	1.7	106	3	47	4.16	4901	1	1	131	6
D2 41592		63	1.5	126	1	45	4.39	788	2	2	77	<5
D2 41593		89	5.6	91	5	267	4.39	609	3	51	307	<5
D2 41594		301	3.2	139	4	96	4.76	342	3	12	338	<5
D2 41595		76	4.6	110	4	413	6.16	537	2	56	243	<5
D2 41596		90	2.8	108	<1	66	6.36	82	4	49	41	<5
D2 41597		258	5.2	80	3	303	6.07	93	4	46	41	<5
D2 41598		172	5.1	172	1	240	6.11	326	3	36	107	5
D2 41599		150	2.9	111	2	91	4.70	190	3	22	118	<5
D2 41600		794	22.1	93	41	520	3.05	307	4	9	2314	20
D2 41601		38	9.9	137	5	773	4.77	718	4	10	304	320
D2 41602		8	0.9	63	<1	10	4.15	852	3	2	48	<5
D2 41603		7	0.4	37	2	15	3.46	838	2	2	50	6
D2 41604		20	0.8	51	<1	11	4.26	828	2	3	23	<5
D2 41605		25	0.9	41	2	8	2.71	757	2	2	77	<5
D2 41606		24	1.1	53	<1	12	3.68	916	2	1	21	5
D2 41607		36	1.5	58	<1	5	3.73	628	2	2	85	<5
D2 41608		396	19.2	72	5	89	4.12	658	3	2	1487	43

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06097.0

DATE PRINTED: 24-SEP-89

PROJECT: 89BCN19

PAGE 2B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
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D2 41569
D2 41570
D2 41571
D2 41572
D2 41573

D2 41574
D2 41575
D2 41576 46 40
D2 41577 151 60
D2 41578 65 50

D2 41579 33 45
D2 41580 23 45
D2 41581 26 40
D2 41582 75 110
D2 41583 1242 130

D2 41584 64 40
D2 41585 79 55
D2 41586 149 50
D2 41587 1004 2400
D2 41588 >200000 170

D2 41589 353 125
D2 41590 210 85
D2 41591 349 90
D2 41592 149 50
D2 41593 631 125

D2 41594 581 100
D2 41595 466 100
D2 41596 73 15
D2 41597 319 35
D2 41598 146 45

D2 41599 254 60
D2 41600 5236 600
D2 41601 599 250
D2 41602 38 15
D2 41603 195 70

D2 41604 77 40
D2 41605 174 30
D2 41606 24 40
D2 41607 98 40
D2 41608 571 230

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 24-SEP-89

REPORT: V89-06097.0

PROJECT: 89BC019

PAGE 3A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41609		1419	>50.0	199	148	1302	5.17	825	3	10	>10000	54

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 24-SEP-89

PROJECT: 89DC019

PAGE 3B

REPORT: V89-06097.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41609	16998	1900	.

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 1A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
R2 89HANK 5140		15	<0.2	<5	<1	9	1.14	24	4	1	18	<5
R2 89HANK 5141		12	<0.2	11	<1	9	1.51	17	6	2	17	<5
R2 89HANK 5142		12	<0.2	5	<1	11	1.30	9	4	1	4	<5
R2 89HANK 5143		7	<0.2	<5	<1	5	0.69	26	6	5	5	<5
R2 89HANK 5144		<1	<0.2	<5	<1	10	5.89	2116	2	<1	<2	<5
R2 89HANK 5145		<1	<0.2	<5	<1	14	4.76	213	3	<1	<2	<5
R2 89HANK 5146		72	<0.2	98	<1	6	1.49	39	4	2	148	18
R2 89HANK 5147		4	<0.2	<5	<1	2	0.30	3	<1	<1	4	<5
D2 41610	>10000	>50.0	118	329	1460	4.29	1253	<1	8	9297	100	
D2 41611		132	2.7	51	3	58	4.88	620	2	10	212	<5
D2 41612		107	1.1	83	<1	72	7.74	1340	3	9	13	<5
D2 41613		126	0.8	66	<1	136	6.47	837	2	11	18	5
D2 41614		60	0.4	29	<1	162	6.53	1225	3	13	45	<5
D2 41615		594	29.8	104	95	884	6.83	1306	3	15	9432	67
D2 41616		173	9.5	93	15	160	5.56	891	4	11	695	13
D2 41617		10	0.4	52	<1	6	4.85	628	3	<1	15	<5
D2 41618		14	0.5	36	<1	16	3.55	698	2	<1	9	<5
D2 41619		19	0.4	38	<1	4	4.07	551	2	<1	10	<5
D2 41620		13	0.6	53	<1	9	4.53	815	2	<1	21	<5
D2 41621		30	1.2	71	<1	8	4.02	903	3	<1	5	<5
D2 41622		12	0.3	69	<1	2	4.42	1386	4	1	18	<5
D2 41623		21	0.2	65	<1	18	4.87	1108	3	<1	15	<5
D2 41624		37	<0.2	50	<1	4	4.07	1358	5	<1	4	<5
D2 41625		49	0.4	61	<1	8	4.22	1415	1	<1	3	<5
D2 41626		29	0.6	85	<1	3	4.12	859	2	1	14	<5
D2 41627		34	0.8	99	<1	5	4.04	923	1	<1	29	<5
D2 41628		34	1.1	87	<1	9	4.01	1050	3	<1	10	<5
D2 41629		98	3.5	136	<1	33	4.15	442	2	2	41	5
D2 41630		104	3.2	112	2	171	3.40	127	2	14	97	7
D2 41631		193	4.8	155	7	97	3.20	200	2	19	281	11
D2 41632		219	3.5	180	<1	54	4.28	1405	3	13	51	<5
D2 41633		1021	4.5	513	<1	103	6.04	4836	2	8	146	10
D2 41634		80	2.1	100	<1	320	7.62	2376	3	16	2	<5
D2 41635		79	3.6	78	<1	651	8.21	2611	2	17	9	<5
D2 41636		61	3.3	78	1	597	8.73	2762	3	17	117	<5
D2 41637		19	0.7	53	<1	205	8.20	2721	3	17	11	<5
D2 41638		113	2.0	104	<1	183	7.60	1814	2	12	26	<5
D2 41639		122	3.0	106	<1	73	6.24	1824	3	12	15	<5
D2 41640		45	1.5	62	<1	81	4.73	1652	3	10	4	<5
D2 41641		27	0.9	67	<1	49	4.93	1582	2	11	6	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 1B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
R2 89HANK 5140		5	3700
R2 89HANK 5141		3	3700
R2 89HANK 5142		14	1500
R2 89HANK 5143		1	220
R2 89HANK 5144		89	100
R2 89HANK 5145		26	1500
R2 89HANK 5146		3	>5000
R2 89HANK 5147		5	2400
D2 41610		>20000	2400
D2 41611		292	280
D2 41612		88	190
D2 41613		32	110
D2 41614		56	60
D2 41615		10966	1400
D2 41616		1812	270
D2 41617		18	40
D2 41618		6	40
D2 41619		5	60
D2 41620		7	30
D2 41621		16	35
D2 41622		30	20
D2 41623		38	50
D2 41624		39	25
D2 41625		35	40
D2 41626		22	40
D2 41627		26	30
D2 41628		15	10
D2 41629		118	60
D2 41630		296	60
D2 41631		1045	160
D2 41632		85	60
D2 41633		75	50
D2 41634		73	35
D2 41635		90	25
D2 41636		160	40
D2 41637		76	30
D2 41638		72	50
D2 41639		35	20
D2 41640		38	30
D2 41641		45	30

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 2A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41642		116	2.2	128	<1	231	6.76	1797	2	14	3	<5
D2 41643		30	0.9	57	<1	62	5.99	1970	1	11	36	<5
D2 41644		11	0.5	13	1	88	5.89	1593	2	11	16	<5
D2 41645		12	0.8	12	1	136	6.02	1933	2	11	27	<5
D2 41646		35	1.0	51	<1	212	6.30	2115	2	11	8	<5
D2 41647		32	1.2	198	<1	158	7.92	1802	2	13	9	<5
D2 41648		56	1.2	85	<1	97	7.16	1802	5	9	16	<5
D2 41649		50	1.8	102	<1	138	7.48	1203	3	12	19	<5
D2 41650		236	2.5	84	<1	410	5.07	1556	3	10	66	<5
D2 41651		32	0.4	17	<1	98	2.90	1352	2	7	<2	<5
D2 41652		50	1.9	67	4	77	7.14	1476	4	9	182	<5
D2 41653		43	1.7	22	<1	212	6.14	1868	2	9	12	<5
D2 41654		73	1.2	67	3	120	6.27	1556	2	9	48	<5
D2 41655		61	2.0	97	3	175	5.19	1607	2	8	67	<5
D2 41656		51	1.4	82	<1	67	5.12	1463	2	9	49	<5
D2 41657		59	0.8	65	<1	39	4.38	921	2	6	28	<5
D2 41658		26	0.7	49	<1	51	4.24	981	2	7	83	<5
D2 41659		39	0.8	57	<1	81	4.63	1143	3	8	19	<5
D2 41660		24	0.7	27	<1	118	3.86	1442	2	7	13	<5
D2 41661		44	0.8	42	<1	87	5.14	1518	1	7	8	<5
D2 41662		832	3.1	91	<1	71	4.92	1586	1	7	258	<5
D2 41663		32	1.1	39	<1	54	5.20	1352	2	9	10	<5
D2 41664		62	2.0	54	<1	238	4.65	947	2	9	40	<5
D2 41665		180	2.7	85	<1	108	5.23	713	3	8	53	<5
D2 41666		1037	3.8	104	<1	1490	5.82	993	3	6	189	<5
D2 41667		153	1.4	86	<1	70	4.97	931	4	6	46	<5
D2 41668		101	1.7	65	2	98	5.94	1551	3	7	210	<5
D2 41669		27	0.7	86	2	54	4.34	1824	3	7	99	<5
D2 41670		31	1.3	83	4	67	6.05	1667	2	8	153	<5
D2 41671		39	1.5	105	1	115	6.75	1530	7	8	99	<5
D2 41672		33	1.4	41	<1	118	5.62	1753	1	6	67	<5
D2 41673		15	0.7	17	1	62	4.87	1929	1	6	89	<5
D2 41674		21	2.0	21	3	101	5.59	2720	<1	7	169	<5
D2 41675		4	0.6	8	1	74	5.19	1725	1	6	124	<5
D2 41676		11	0.4	<5	1	56	5.00	2220	2	6	62	<5
D2 41677		47	1.2	25	5	70	5.18	2108	<1	5	187	<5
D2 41678		6	0.5	<5	2	50	4.57	1819	<1	4	85	<5
D2 41679		9	0.4	10	1	56	5.34	1935	1	6	79	<5
D2 41680		43	0.9	75	2	40	4.11	1328	2	4	125	<5
D2 41681		167	1.4	90	2	47	3.18	1174	2	3	200	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 28

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41642		57	40
D2 41643		155	40
D2 41644		187	20
D2 41645		195	30
D2 41646		86	35
D2 41647		54	20
D2 41648		55	35
D2 41649		32	30
D2 41650		101	50
D2 41651		37	30
D2 41652		535	25
D2 41653		103	55
D2 41654		425	30
D2 41655		550	120
D2 41656		144	40
D2 41657		26	30
D2 41658		45	10
D2 41659		29	20
D2 41660		95	15
D2 41661		46	10
D2 41662		68	15
D2 41663		36	25
D2 41664		49	30
D2 41665		92	40
D2 41666		82	60
D2 41667		90	135
D2 41668		384	90
D2 41669		317	40
D2 41670		668	70
D2 41671		263	30
D2 41672		201	30
D2 41673		228	30
D2 41674		453	90
D2 41675		275	80
D2 41676		216	35
D2 41677		788	60
D2 41678		326	40
D2 41679		195	45
D2 41680		338	55
D2 41681		293	65

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 3A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41682		74	0.9	16	<1	43	4.58	1021	1	4	<2	<5
D2 41683		83	1.6	14	<1	49	4.15	1204	4	3	2	<5
D2 41684		69	1.5	72	<1	57	3.24	600	1	21	227	<5
D2 41685		34	0.6	88	<1	39	4.21	721	2	26	62	<5
D2 41686		195	4.3	65	3	179	4.21	692	1	23	362	21
D2 41687		28	0.7	20	<1	259	3.35	1048	1	21	16	<5
D2 41688		120	2.1	49	4	53	3.98	700	1	23	447	<5
D2 41689		62	0.5	63	<1	101	3.63	1315	1	20	15	<5
D2 41690		142	0.8	60	<1	68	3.31	818	2	14	33	<5
D2 41691		125	0.5	64	<1	320	4.14	652	2	19	11	<5
D2 41692		95	0.9	41	2	76	3.15	739	2	13	140	<5
D2 41693		287	4.8	139	7	293	5.87	994	3	12	894	<5
D2 41694		18	0.2	34	<1	172	4.33	1007	2	9	32	<5
D2 41695		6	<0.2	36	<1	38	5.07	1059	2	12	45	<5
D2 41696		45	0.4	80	<1	113	5.16	1402	2	8	33	<5
D2 41697		114	1.2	92	<1	99	4.84	1121	2	11	33	<5
D2 41698		53	0.4	108	<1	29	4.45	1445	1	7	37	<5
D2 41699		74	1.3	56	<1	113	4.73	1545	1	6	159	<5
D2 41700		159	0.9	103	<1	39	5.67	1585	2	7	271	<5
D2 41701		91	0.7	121	6	32	7.13	1534	2	11	77	<5
D2 41702		46	0.3	90	<1	83	6.42	1675	3	15	111	<5
D2 41703		59	0.3	85	<1	373	6.20	1545	2	11	96	<5
D2 41704		98	1.1	72	11	122	5.15	1331	2	8	939	<5
D2 41705		142	2.0	52	2	270	5.63	1276	2	11	249	<5
D2 41706		265	4.3	77	18	431	5.15	1027	1	10	1171	<5
D2 41707		37	0.2	56	<1	49	5.33	1283	2	11	241	<5
D2 41708		26	0.3	38	2	39	5.10	1519	2	9	133	<5
D2 41709		41	0.4	43	<1	83	5.53	1717	1	11	43	<5
D2 41710		81	0.9	18	1	120	5.30	1241	4	23	117	<5
D2 41711		42	0.4	43	<1	58	5.94	1681	2	26	97	<5
D2 41712		28	0.4	30	<1	202	5.32	1515	2	26	19	<5
D2 41713		50	1.0	<5	23	405	6.05	1921	2	31	29	<5
D2 41714		182	4.2	119	15	189	5.88	1162	<1	17	915	<5
D2 41715		13	0.2	14	<1	135	6.30	1225	2	9	5	<5
D2 41716		72	1.7	60	8	82	5.37	1370	1	9	139	<5
D2 41717		115	4.4	86	24	175	5.07	1470	2	7	1057	<5
D2 41718		130	2.3	138	11	243	5.42	1313	2	7	1314	<5
D2 41719		70	1.8	95	13	116	6.05	1223	2	7	1221	<5
D2 41720		127	2.7	114	19	137	5.34	1381	2	5	2848	<5
D2 41721		355	14.8	93	19	240	6.43	1682	2	8	1546	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 3B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41682		47	80
D2 41683		46	80
D2 41684		85	65
D2 41685		45	70
D2 41686		390	140
D2 41687		74	65
D2 41688		488	130
D2 41689		62	55
D2 41690		44	45
D2 41691		20	45
D2 41692		215	65
D2 41693		822	170
D2 41694		80	40
D2 41695		71	35
D2 41696		58	30
D2 41697		47	40
D2 41698		85	30
D2 41699		261	60
D2 41700		170	50
D2 41701		787	90
D2 41702		82	30
D2 41703		116	50
D2 41704		1388	130
D2 41705		394	70
D2 41706		2145	190
D2 41707		149	70
D2 41708		288	80
D2 41709		158	60
D2 41710		259	65
D2 41711		210	60
D2 41712		101	60
D2 41713		2256	95
D2 41714		1731	310
D2 41715		70	60
D2 41716		1045	140
D2 41717		2610	310
D2 41718		1190	150
D2 41719		1458	120
D2 41720		2161	170
D2 41721		2179	145

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BCD19

PAGE 4A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41722		30	1.1	<5	4	115	4.65	1642	1	8	299	<5
D2 41723		66	1.9	50	4	130	4.78	1205	2	7	799	<5
D2 41724		82	0.6	48	<1	69	5.22	1328	2	7	64	<5
D2 41725		81	1.9	<5	3	455	5.69	1486	2	8	267	<5
D2 41726		58	1.8	35	6	73	5.28	1222	1	8	415	<5
D2 41727		710	42.3	28	4	84	5.66	1268	3	9	84	<5
D2 41728		25	0.4	7	<1	24	5.41	1426	1	6	35	<5
D2 41729		56	1.0	13	<1	70	5.10	865	2	7	18	<5
D2 41730		4	<0.2	<5	<1	71	5.40	726	2	8	<2	<5
D2 41731		10	<0.2	<5	<1	72	4.34	690	2	6	4	<5
D2 41732		185	6.0	<5	<1	51	4.83	705	1	7	<2	<5
D2 41733		55	2.7	13	<1	63	4.86	809	<1	9	9	<5
D2 41734		23	0.4	75	<1	105	4.60	1023	1	7	51	<5
D2 41735		41	1.1	80	3	158	5.04	1006	2	7	298	<5
D2 41736		294	13.1	95	154	655	5.65	796	2	6	>10000	39
D2 41737		8	<0.2	18	<1	15	4.50	844	1	7	51	<5
D2 41738		21	0.4	52	<1	63	5.21	793	2	9	37	<5
D2 41739		226	21.1	93	177	2294	5.58	661	<1	9	>10000	39
D2 41740		30	0.5	77	1	86	5.22	820	2	10	123	<5
D2 41741		52	0.6	92	<1	186	4.52	860	1	7	36	<5
D2 41742		63	1.2	68	<1	31	3.64	672	2	6	65	<5
D2 41743		207	2.6	71	<1	95	4.04	679	3	6	49	5
D2 41744		263	7.4	40	2	13	4.50	731	2	7	81	<5
D2 41745		32	<0.2	40	<1	12	4.82	665	2	8	7	<5
D2 41746		22	<0.2	43	<1	87	4.72	778	2	8	2	<5
D2 41747		6	<0.2	33	<1	15	3.86	743	2	6	<2	<5
D2 41748		18	<0.2	68	<1	46	4.42	971	3	5	44	<5
D2 41749		145	5.5	47	<1	39	4.82	676	1	7	48	<5
D2 41750		8	<0.2	37	<1	21	4.23	534	1	6	7	<5
D2 41751		2	<0.2	21	<1	8	4.81	412	1	6	6	<5
D2 41752		4	<0.2	17	<1	13	4.84	382	1	4	11	<5
D2 41753		5	<0.2	20	<1	15	5.93	430	1	7	26	<5
D2 41754		89	0.9	52	<1	44	4.05	654	1	4	35	<5
D2 41755		43	0.2	54	<1	8	5.21	797	2	3	19	<5
D2 41756		47	0.2	46	<1	92	4.23	997	1	4	37	<5
D2 41757		59	0.2	58	<1	45	4.70	1239	2	4	73	<5
D2 41758		26	0.3	38	<1	24	4.06	1137	<1	3	77	<5
D2 41759		20	0.3	37	<1	25	4.49	1249	2	4	18	<5
D2 41760		92	0.2	43	<1	64	4.19	1022	1	4	14	<5
D2 41761		10	<0.2	41	<1	67	4.30	1082	2	5	3	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 4B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41722		551	80
D2 41723		527	90
D2 41724		145	65
D2 41725		503	90
D2 41726		685	80
D2 41727		562	120
D2 41728		124	60
D2 41729		47	60
D2 41730		48	50
D2 41731		43	40
D2 41732		52	90
D2 41733		52	40
D2 41734		84	40
D2 41735		410	70
D2 41736		16547	1850
D2 41737		93	50
D2 41738		94	55
D2 41739		18841	1050
D2 41740		225	60
D2 41741		114	35
D2 41742		192	50
D2 41743		41	180
D2 41744		284	50
D2 41745		51	40
D2 41746		55	30
D2 41747		69	40
D2 41748		96	45
D2 41749		113	60
D2 41750		34	55
D2 41751		36	40
D2 41752		24	25
D2 41753		30	45
D2 41754		68	45
D2 41755		59	50
D2 41756		89	40
D2 41757		124	80
D2 41758		120	70
D2 41759		120	75
D2 41760		87	50
D2 41761		90	50

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Geochemical Lab Report

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REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 5A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41762		19	<0.2	46	<1	64	4.74	940	2	6	3	<5
D2 41763		7	<0.2	34	<1	84	5.17	616	2	4	15	<5
D2 41764		19	<0.2	32	<1	39	4.15	600	1	4	17	<5
D2 41765		688	14.8	53	29	154	4.99	593	2	5	3335	9
D2 41766		46	0.4	56	1	66	4.98	1004	<1	5	164	<5
D2 41767		18	0.2	54	<1	90	4.79	606	2	4	50	<5
D2 41768		40	0.3	73	<1	73	4.50	770	2	5	30	<5
D2 41769		37	0.3	44	<1	8	4.34	606	2	7	19	<5
D2 41770		64	0.4	78	<1	7	4.45	923	1	5	<2	<5
D2 41771		37	0.2	55	<1	36	4.38	845	2	6	<2	<5
D2 41772		35	<0.2	38	<1	13	3.35	711	<1	5	<2	<5
D2 41773		46	<0.2	28	<1	12	3.16	796	1	3	<2	<5
D2 41774		49	0.3	30	<1	29	3.33	908	1	6	18	<5
D2 41775		100	1.3	56	8	67	4.55	715	2	5	777	<5
D2 41776		28	0.2	37	<1	5	3.83	736	1	8	<2	<5
D2 41777		20	0.3	34	<1	6	3.47	594	1	10	15	<5
D2 41778		65	0.5	52	<1	13	3.55	699	<1	7	71	<5
D2 41779		17	<0.2	37	<1	10	3.45	733	2	4	<2	<5
D2 41780		30	<0.2	52	<1	32	3.44	854	2	3	3	<5
D2 41781		145	2.2	63	4	72	3.36	667	2	3	279	<5
D2 41782		215	1.4	47	<1	27	4.47	881	<1	8	5	<5
D2 41783		102	0.3	42	<1	38	3.75	865	<1	7	5	<5
D2 41784		24	<0.2	49	<1	87	4.35	901	1	8	6	<5
D2 41785		56	0.3	78	<1	87	4.08	693	2	6	12	<5
D2 41786		96	0.3	44	<1	24	3.70	697	3	6	35	<5
D2 41787		28	<0.2	31	<1	6	3.35	819	<1	7	<2	<5
D2 41788		15	<0.2	11	<1	3	2.73	645	1	4	3	<5
D2 41789		20	0.2	23	<1	5	3.07	692	1	5	<2	<5
D2 41790		34	0.3	30	<1	9	4.20	808	1	5	<2	<5
D2 41791		66	1.0	47	<1	82	4.64	809	1	6	7	<5
D2 41792		74	1.0	<5	<1	18	3.93	374	2	9	52	<5
D2 41793		17	<0.2	<5	<1	4	4.32	706	2	9	<2	<5
D2 41794		42	0.2	<5	<1	11	4.41	872	2	9	<2	<5
D2 41795		39	0.2	<5	<1	36	5.00	848	2	7	<2	<5
D2 41796		42	0.2	<5	<1	17	4.84	678	<1	6	<2	<5
D2 41797		33	0.2	<5	<1	23	4.90	779	1	6	<2	<5
D2 41798		28	0.2	<5	<1	9	4.86	816	1	8	9	<5
D2 41799		29	0.3	<5	<1	6	4.18	928	3	5	<2	<5
D2 41800		73	0.9	11	<1	63	4.49	859	2	6	98	<5
D2 41801		193	1.0	101	12	14	6.03	457	4	8	518	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BCD19

PAGE 5B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41762		64	50
D2 41763		43	40
D2 41764		30	45
D2 41765		2882	290
D2 41766		264	75
D2 41767		100	100
D2 41768		116	60
D2 41769		50	50
D2 41770		69	55
D2 41771		53	50
D2 41772		50	30
D2 41773		55	40
D2 41774		75	40
D2 41775		1133	150
D2 41776		48	50
D2 41777		90	60
D2 41778		145	50
D2 41779		56	40
D2 41780		55	50
D2 41781		532	180
D2 41782		75	60
D2 41783		91	50
D2 41784		101	20
D2 41785		73	30
D2 41786		121	30
D2 41787		103	15
D2 41788		85	25
D2 41789		90	20
D2 41790		97	30
D2 41791		88	60
D2 41792		135	45
D2 41793		56	50
D2 41794		56	40
D2 41795		60	45
D2 41796		53	40
D2 41797		60	25
D2 41798		57	35
D2 41799		94	40
D2 41800		191	40
D2 41801		1476	180

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Geochemical Lab Report

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REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BCD19

PAGE 6A

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41802		159	4.0	47	24	18	3.98	796	2	7	2708	<5
D2 41803		680	4.3	116	46	45	6.96	585	2	8	3982	15
D2 41804		873	1.1	84	2	95	4.95	834	2	8	119	<5
D2 41805		189	1.1	76	<1	66	4.67	681	<1	8	41	<5
D2 41806		164	1.2	73	4	64	5.72	327	1	8	205	<5
D2 41807		185	1.1	42	1	75	4.02	283	<1	7	44	<5
D2 41808		237	0.8	35	<1	25	3.87	1425	<1	6	18	<5
D2 41809		178	1.6	46	<1	28	4.63	769	2	6	28	<5
D2 41810		111	0.6	35	<1	12	4.17	1193	1	6	6	<5
D2 41811		116	1.1	28	<1	25	3.68	2311	2	5	45	7
D2 41812		175	0.7	41	16	25	6.02	786	2	7	121	6
D2 41813		278	1.3	32	15	9	5.57	717	2	8	1146	7
D2 41814		234	0.8	51	9	7	4.70	1751	2	6	409	8
D2 41815		205	1.0	65	6	5	4.90	1798	3	7	573	<5
D2 41816		335	2.3	35	18	10	5.11	1550	2	6	1712	7
D2 41817		254	0.5	31	<1	2	4.91	231	2	9	52	<5
D2 41818		154	0.5	27	<1	5	4.76	1955	1	8	130	5
D2 41819		174	1.3	35	3	10	4.67	2325	2	7	222	5
D2 41820		251	0.9	48	10	23	7.03	1356	2	15	685	10
D2 41821		117	0.7	13	<1	109	7.20	906	2	21	105	<5
D2 41822		134	0.5	27	1	31	6.58	1046	1	20	61	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.0

DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 6B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41802		3120	300
D2 41803		5856	370
D2 41804		229	90
D2 41805		138	80
D2 41806		650	120
D2 41807		259	70
D2 41808		94	60
D2 41809		77	55
D2 41810		29	50
D2 41811		143	70
D2 41812		2065	220
D2 41813		1948	220
D2 41814		1229	160
D2 41815		832	150
D2 41816		2324	320
D2 41817		38	50
D2 41818		154	45
D2 41819		388	80
D2 41820		1214	150
D2 41821		114	70
D2 41822		173	60

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A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06155.6

DATE PRINTED: 29-SEP-89

PROJECT: 89BC019

PAGE 1

SAMPLE NUMBER	ELEMENT UNITS	Au GMT	Ag GMT	Pb PCT	Zn PCT	SAMPLE NUMBER	ELEMENT UNITS	Au GMT	Ag GMT	Pb PCT	Zn PCT
D2 41610		28.35*	689.5		3.65	D2 41817		0.38			
D2 41615		1.10	28.8			D2 41818		0.21			
D2 41616		0.24				D2 41819		0.24			
D2 41631		0.27				D2 41820		0.27			
D2 41632		0.31									
D2 41633		1.30									
D2 41650		0.31									
D2 41662		1.41*									
D2 41665		0.21									
D2 41666		1.10									
D2 41667		0.27									
D2 41681		0.21									
D2 41686		0.31									
D2 41693		0.48									
D2 41700		0.34									
D2 41706		0.48									
D2 41714		0.24									
D2 41721		0.65									
D2 41727		0.62									
D2 41732		0.24									
D2 41736		0.48		1.49							
D2 41739		0.31		1.22							
D2 41743		0.27									
D2 41744		0.34									
D2 41765		0.86									
D2 41782		0.24									
D2 41801		0.21									
D2 41802		0.89									
D2 41803		1.17									
D2 41804		0.21									
D2 41805		0.21									
D2 41806		0.24									
D2 41807		0.27									
D2 41808		0.17									
D2 41809		0.21									
D2 41812		0.24									
D2 41813		0.34									
D2 41814		0.24									
D2 41815		0.27									
D2 41816		0.51									

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Certificate
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REPORT: V89-06171.6

DATE PRINTED: 13-OCT-89

PROJECT: 89BC019

PAGE 1

SAMPLE NUMBER	ELEMENT UNITS	Aln GMT	Ag GMT	Ag GMT	Pb PCT	Zn PCT
D2 41825		> 0.17				
D2 41826		0.89				
D2 41827		0.41				
D2 41828		0.34				
D2 41829		0.21				
D2 41834		0.17				
D2 41836		0.86				
D2 41838		0.17				
D2 41849		0.27				
D2 41850		0.24				
D2 41851		0.24				
D2 41854		0.38				
D2 41855		0.45				
D2 41856		3.15				
D2 41857		0.45				
D2 41858		0.14				
D2 41859		0.21				
D2 41860		0.27				
D2 41861		0.34				
D2 41862		0.38				
D2 41863		0.21				
D2 41864		0.31				
D2 41865		0.31				
D2 41866		0.38				
D2 41867		0.62				
D2 41868		0.41				
D2 41869		0.24				
D2 41870		0.24				
D2 41871		0.17				
D2 41877		0.21				
D2 41878		0.10				
D2 41888					2.55	
D2 41890		0.17				
D2 41893		0.17				
D2 41894		0.14				
D2 41896		0.10				
D2 41897		0.72				
D2 41898		1.27				
D2 41899		4.22	124.5		5.50	13.76
D2 41900		0.24				

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Certificate
of Analysis

DATE PRINTED: 13-OCT-89

PROJECT: 89BC019

PAGE 2

REPORT: V89-06171.6

SAMPLE NUMBER	ELEMENT UNITS	Au GMT	Ag GMT	Ag PCT	Pb PCT	Zn PCT
D2 41941				37.7		
D2 41942				60.3		
D2 41951					9.40	
D2 41954		81.36	2058.9			9.95
D2 41955				198.9		


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REPORT: V89-06171.5

DATA PRINTED: 20-OCT-89

PROJECT: 89BCII19

PAGE 1

SAMPLE NUMBER	ELEMENT UNITS	Au GMT
D2 41905		0.38
D2 41906		0.45
D2 41907		0.48
D2 41908		0.51
D2 41910		0.24
D2 41912		0.55
D2 41913		0.27
D2 41918		0.68
D2 41934		0.34
D2 41935		0.27
D2 41936		0.31
D2 41939		3.91
D2 41940		0.93
D2 41941		4.90
D2 41942		12.62*
D2 41943		0.65
D2 41944		0.45
D2 41945		0.45
D2 41946		0.55
D2 41947		0.27
D2 41948		0.24
D2 41949		0.24
D2 41951		6.58
D2 41952		0.31
D2 41953		1.20
D2 41954		78.51
D2 41955		11.45
D2 41956		0.38
D2 41957		0.58
D2 41958		0.41
D2 41960		0.41
D2 41961		0.51
D2 41962		0.34

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DATE PRINTED: 28-SEP-89

PROJECT: 89BC019

PAGE 1

REPORT: V89-D6026.5

SAMPLE NUMBER	ELEMENT UNITS	WT G	WT-150 G	WT+150 G	Au-150 GMT	Au+150 GMT	Au+150 MG	Au TOT GMT
D2 41284		29.17	292.2	1.75	1.95	120.0	0.210	2.66
D2 41291		29.17	324.7	12.95	1.68	5.3	0.068	1.82
D2 41292		29.17	297.3	3.89	1.47	3.3	0.013	1.50
D2 41293		29.17	334.6	7.44	1.65	5.6	0.042	1.73
D2 41297		29.17	311.9	8.90	1.54	2.1	0.019	1.56
D2 41298		29.17	289.7	2.90	1.37	2.1	0.006	1.38
D2 41299		29.17	307.0	3.61	0.99	2.2	0.008	1.01
D2 41300		29.17	98.3	1.46	2.40	7.5	0.011	2.48
D2 41339		29.17	334.8	8.68	46.59	1259.7	10.934	77.25
D2 41345		29.17	303.7	6.47	1.30	5.4	0.035	1.39
D2 41346		29.17	223.1	1.61	3.87	111.8	0.180	4.65
D2 41347		29.17	299.9	3.78	1.27	2.1	0.008	1.28
D2 41348		29.17	322.4	9.10	15.33	22.3	0.203	15.52
D2 41349		29.17	305.4	3.38	1.23	3.8	0.013	1.26

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A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 28-SEP-89

REPORT: V89-06097.5

PROJECT: 89BC019

PAGE 1

SAMPLE NUMBER	ELEMENT UNITS	WT G	WT-150 G	WT+150 G	Au-150 GMT	Au+150 GMT	Au+150 MG	Au TOT GMT
D2 41548		29.17	282.1	1.14	1.27	7.9	0.009	1.30

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REPORT: V89-06051.5

DATE PRINTED: 2-OCT-89

PROJECT: 89BC019

PAGE 1

SAMPLE NUMBER	ELEMENT UNITS	WT G	WT-150 G	WT+150 G	Au-150 GMT	Au+150 GMT	Au+150 MG	Au TOT GMT
D2 41437		29.17	260.2	7.93	3.22	3.0	0.024	3.22
D2 41438		29.17	392.4	15.21	28.32	19.6	0.298	27.99
D2 41546		29.17	266.2	3.55	1.30	10.1	0.036	1.42
D2 41547		29.17	118.0	1.16	12.96	301.7	0.350	15.77

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 6-OCT-89

PROJECT: 89BCD19

PAGE 1A

REPORT: V89-06171.0

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41823		78	0.6	77	1	145	7.55	881	3	15	81	<5
D2 41824		24	0.5	57	2	87	6.80	921	2	15	79	<5
D2 41825		200	1.4	59	10	48	5.49	1123	2	14	691	<5
D2 41826		909	5.3	106	20	184	6.33	1132	2	12	1752	7
D2 41827		433	2.1	104	6	59	6.17	1395	2	15	304	<5
D2 41828		326	1.9	71	8	217	6.60	2224	2	15	769	<5
D2 41829		224	1.0	77	<1	58	7.14	1184	3	13	208	<5
D2 41830		74	0.7	89	6	145	6.84	1732	2	15	505	<5
D2 41831		119	1.1	63	9	247	7.85	1970	2	15	673	<5
D2 41832		61	0.5	82	6	65	6.34	1328	2	15	354	<5
D2 41833		87	0.7	68	4	161	6.75	1146	3	14	396	<5
D2 41834		199	0.9	107	4	148	8.00	1395	2	17	188	<5
D2 41835		124	0.8	87	3	55	8.52	1361	9	17	173	<5
D2 41836		945	3.0	137	<1	161	8.92	1371	3	17	131	<5
D2 41837		148	1.9	124	3	102	8.62	1335	3	15	81	<5
D2 41838		446	1.0	65	4	84	7.63	1481	2	18	327	<5
D2 41839		111	1.2	41	7	102	6.94	1133	2	13	383	<5
D2 41840		95	1.8	61	15	367	7.93	1203	2	12	757	<5
D2 41841		20	0.8	56	4	103	7.31	962	3	14	212	<5
D2 41842		23	0.8	34	2	98	5.36	720	3	14	340	<5
D2 41843		25	0.6	44	<1	52	5.69	644	2	13	76	<5
D2 41844		67	1.3	52	<1	35	7.22	711	2	12	57	<5
D2 41845		49	1.2	35	2	72	5.36	933	2	12	29	<5
D2 41846		55	1.0	40	<1	204	5.92	765	2	16	18	<5
D2 41847		13	0.3	42	<1	73	6.20	887	1	13	11	<5
D2 41848		21	0.4	42	<1	104	6.18	931	2	13	24	<5
D2 41849		257	4.7	51	28	152	9.11	387	4	13	971	15
D2 41850		212	2.7	42	5	69	5.98	977	2	13	432	<5
D2 41851		152	2.4	41	6	44	6.16	1330	1	13	461	6
D2 41852		98	1.3	36	<1	47	5.64	1055	2	11	182	6
D2 41853		94	1.5	58	2	76	5.70	1089	2	12	172	<5
D2 41854		366	3.7	48	7	166	6.74	825	1	12	15	<5
D2 41855		424	14.2	43	13	331	5.57	1318	2	11	41	5
D2 41856		4417	30.5	56	13	254	5.87	1433	2	11	446	5
D2 41857		450	2.3	98	4	122	5.33	1232	2	12	275	<5
D2 41858		159	1.0	42	<1	50	5.94	1247	1	11	40	<5
D2 41859		250	1.2	60	2	51	5.97	1363	2	7	183	<5
D2 41860		266	1.3	42	2	36	6.19	1286	2	5	85	<5
D2 41861		276	1.3	40	2	36	7.15	1330	2	6	55	<5
D2 41862		377	2.4	54	18	72	6.58	902	2	9	55	8

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Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 6-OCT-89

PROJECT: 89BC019

PAGE 1B

REPORT: V89-06171.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41823		225	70
D2 41824		377	25
D2 41825		1051	85
D2 41826		2243	180
D2 41827		672	75
D2 41828		900	90
D2 41829		250	70
D2 41830		575	60
D2 41831		888	60
D2 41832		554	45
D2 41833		487	35
D2 41834		398	30
D2 41835		388	25
D2 41836		195	15
D2 41837		222	20
D2 41838		312	20
D2 41839		763	45
D2 41840		1471	90
D2 41841		441	40
D2 41842		285	50
D2 41843		135	25
D2 41844		141	15
D2 41845		152	25
D2 41846		67	15
D2 41847		53	10
D2 41848		68	35
D2 41849		3093	330
D2 41850		663	85
D2 41851		772	85
D2 41852		176	20
D2 41853		337	45
D2 41854		919	110
D2 41855		1656	160
D2 41856		1699	390
D2 41857		558	60
D2 41858		81	35
D2 41859		262	30
D2 41860		278	30
D2 41861		322	25
D2 41862		2268	170

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 6-OCT-89

PROJECT: 89BC019

PAGE 2A

REPORT: V89-06171.0

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41863		217	1.7	35	5	45	4.99	856	2	9	47	<5
D2 41864		322	2.5	87	5	148	5.13	1152	2	9	29	<5
D2 41865		296	1.9	67	7	88	4.80	818	1	10	51	<5
D2 41866		367	4.9	90	9	152	5.07	518	2	19	54	<5
D2 41867		643	2.7	142	13	56	6.28	98	2	9	126	<5
D2 41868		444	2.9	232	12	114	6.09	995	4	7	80	<5
D2 41869		238	2.2	130	25	84	5.41	1817	2	7	214	8
D2 41870		260	2.0	126	7	94	4.58	1744	1	5	594	<5
D2 41871		174	0.9	139	7	23	6.38	2078	2	6	74	6
D2 41872		96	0.5	158	6	95	6.24	1944	2	5	34	<5
D2 41873		93	0.5	96	4	119	5.13	2128	2	6	138	<5
D2 41874		90	0.6	114	8	189	6.82	2496	4	11	56	<5
D2 41875		78	0.3	90	1	8	3.78	2198	2	8	17	<5
D2 41876		132	0.5	111	<1	5	4.64	1941	1	11	81	<5
D2 41877		321	0.7	134	<1	7	5.48	1445	2	13	18	<5
D2 41878		185	0.5	147	<1	15	6.13	2043	2	11	12	<5
D2 41879		109	0.5	148	<1	18	6.73	2104	2	10	29	<5
D2 41880		99	0.4	125	<1	66	6.04	2507	2	9	20	<5
D2 41881		60	0.5	107	1	78	5.92	2869	2	7	165	<5
D2 41882		96	0.8	108	5	83	5.49	2095	2	8	104	<5
D2 41883		111	0.9	102	7	105	5.62	2130	2	7	147	8
D2 41884		106	1.1	87	16	60	4.72	1762	2	6	520	7
D2 41885		69	0.4	97	4	12	5.27	1715	2	5	34	5
D2 41886		61	0.4	89	9	12	6.79	1691	15	8	83	<5
D2 41887		79	2.6	73	141	64	8.04	2205	6	22	878	19
D2 41888		35	1.3	58	215	32	4.27	1977	<1	7	1254	49
D2 41889		54	2.3	79	26	15	5.56	2021	<1	7	1729	<5
D2 41890		166	4.7	90	99	175	6.66	1646	1	9	3869	26
D2 41891		135	2.9	132	26	145	5.85	1637	2	8	1666	7
D2 41892		126	1.9	111	12	112	6.12	1865	2	7	1185	<5
D2 41893		161	2.7	110	25	341	6.55	1943	1	8	1489	6
D2 41894		161	3.4	102	51	240	6.70	1922	2	8	2067	14
D2 41895		115	1.6	97	13	134	5.65	1539	2	13	765	<5
D2 41896		165	1.5	83	13	119	5.97	1293	3	11	203	<5
D2 41897		708	15.4	212	190	197	7.04	1079	3	11	4694	47
D2 41898		818	14.4	102	42	71	4.92	966	3	11	2658	12
D2 41899		3713	>50.0	240	1115	1626	7.51	2915	<1	33	>10000	303
D2 41900		234	2.5	85	23	94	6.05	977	2	16	754	11
D2 41901			0.5	86	<1	134	5.88	935	2	13	68	<5
D2 41902			0.6	86	1	96	6.50	945	2	14	76	<5

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 6-OCT-89

PROJECT: 89BC019

PAGE 28

REPORT: V89-06171.0

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
D2 41863		641	85
D2 41864		780	130
D2 41865		948	135
D2 41866		1152	125
D2 41867		1639	120
D2 41868		1513	160
D2 41869		3396	280
D2 41870		1086	105
D2 41871		1103	100
D2 41872		980	65
D2 41873		724	40
D2 41874		1216	80
D2 41875		318	30
D2 41876		114	10
D2 41877		88	15
D2 41878		220	55
D2 41879		201	70
D2 41880		347	130
D2 41881		367	175
D2 41882		823	80
D2 41883		1119	55
D2 41884		2158	145
D2 41885		682	60
D2 41886		1316	95
D2 41887		18406	520
D2 41888		>20000	600
D2 41889		3328	250
D2 41890		11188	650
D2 41891		3483	220
D2 41892		1846	130
D2 41893		3393	195
D2 41894		6312	280
D2 41895		1721	220
D2 41896		1763	90
D2 41897		>20000	1150
D2 41898		4907	340
D2 41899		>20000	4600
D2 41900		2813	135
D2 41901		164	5
D2 41902		278	15

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Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

DATE PRINTED: 6-OCT-89

PROJECT: 89BC019

PAGE 3A

REPORT: V89-06171.0

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	Ag PPM	As PPM	Cd PPM	Cu PPM	Fe PCT	Mn PPM	Mo PPM	Ni PPM	Pb PPM	Sb PPM
D2 41903		0.5	93	<1	43	6.86	853	2	15	66	<5	
D2 41904		1.3	84	7	151	5.46	1207	2	12	558	5	
D2 41905		2.3	60	14	130	5.75	947	2	14	601	<5	
D2 41906		2.3	113	5	161	6.88	1336	2	13	291	<5	
D2 41907		2.4	110	7	164	6.82	1427	3	14	414	<5	
D2 41908		2.8	68	5	182	6.88	1874	2	13	233	<5	
D2 41909		1.2	94	10	255	5.88	1231	1	13	976	<5	
D2 41910		1.0	128	3	35	6.34	1388	3	14	191	<5	
D2 41911		1.3	138	5	107	6.93	1298	3	14	670	<5	
D2 41912		2.3	168	4	119	6.87	1284	3	14	181	<5	
D2 41913		1.3	94	3	228	6.70	1196	3	14	231	<5	
D2 41914		0.7	122	4	111	6.67	1062	2	14	287	<5	
D2 41915		0.7	93	4	164	7.31	1171	2	17	258	<5	
D2 41916		0.9	125	2	102	7.49	1028	2	14	81	<5	
D2 41917		0.6	70	5	92	7.52	1289	2	13	87	<5	
D2 41918		3.5	79	19	285	7.95	769	2	13	1355	<5	
D2 41919		0.6	57	3	63	6.57	973	2	11	43	<5	
D2 41920		1.1	67	4	138	6.68	744	2	12	134	<5	
D2 41921		1.1	55	4	101	6.25	980	2	13	137	<5	
D2 41922		0.6	50	<1	102	5.65	915	4	13	66	<5	
D2 41923		0.4	40	<1	168	6.28	749	1	11	65	<5	
D2 41924		0.3	41	1	49	5.35	614	2	9	55	<5	
D2 41925		0.5	56	<1	32	6.14	765	2	16	44	<5	
D2 41926		0.6	46	4	82	5.29	950	2	12	117	<5	
D2 41927		0.4	46	1	36	6.05	670	2	13	20	<5	
D2 41928		1.2	60	<1	48	5.70	668	1	14	279	<5	
D2 41929		0.9	51	<1	95	6.06	970	2	12	58	<5	
D2 41930		0.6	49	2	209	5.86	985	2	11	148	<5	
D2 41931		0.8	56	12	91	5.53	1059	1	12	631	<5	
D2 41932		0.9	31	5	43	4.64	1106	1	11	250	<5	
D2 41933		0.8	33	2	38	5.17	902	2	9	211	<5	
D2 41934		5.2	51	30	83	6.57	314	2	12	1537	9	
D2 41935		3.3	35	62	170	5.54	357	3	14	321	14	
D2 41936		2.9	33	26	89	4.29	926	1	9	20	<5	
D2 41937		1.1	34	10	81	4.02	993	2	8	77	<5	
D2 41938		2.1	40	17	67	5.37	1194	1	10	181	5	
D2 41939		31.0	45	61	265	4.81	1125	1	11	104	15	
D2 41940		8.0	45	10	263	7.17	740	6	11	19	<5	
D2 41941		>50.0	45	65	259	4.31	1402	<1	9	209	16	
D2 41942		>50.0	37	4	56	4.53	1416	2	10	4	<5	

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06171.0

DATE PRINTED: 6-OCT-89

PROJECT: 89BC019

PAGE 3B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
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D2 41903		216	15
D2 41904		828	30
D2 41905		1416	80
D2 41906		590	75
D2 41907		710	90

D2 41908		649	50
D2 41909		1146	120
D2 41910		313	35
D2 41911		545	60
D2 41912		377	20

D2 41913		410	30
D2 41914		583	25
D2 41915		578	30
D2 41916		174	10
D2 41917		279	10

D2 41918		1884	80
D2 41919		234	<5
D2 41920		429	15
D2 41921		441	10
D2 41922		145	15

D2 41923		150	5
D2 41924		107	5
D2 41925		129	10
D2 41926		300	10
D2 41927		126	10

D2 41928		137	5
D2 41929		159	5
D2 41930		346	25
D2 41931		1316	60
D2 41932		525	30

D2 41933		262	55
D2 41934		3467	240
D2 41935		7235	490
D2 41936		3078	270
D2 41937		1150	80

D2 41938		2015	130
D2 41939		7489	510
D2 41940		1283	95
D2 41941		7897	850
D2 41942		575	185

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Geochemical
Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V89-06171.0

DATE PRINTED: 6-OCT-89

PROJECT: 89BC019

PAGE 4B

SAMPLE NUMBER	ELEMENT UNITS	Zn PPM	Hg PPB
---------------	---------------	--------	--------

D2 41943		3106	170
D2 41944		2115	80
D2 41945		1258	50
D2 41946		5943	325
D2 41947		240	10

D2 41948		314	20
D2 41949		7368	260
D2 41950		1032	70
D2 41951		>20000	3700
D2 41952		2480	120

D2 41953		341	40
D2 41954		>20000	>5000
D2 41955		3632	390
D2 41956		264	210
D2 41957		2150	170

D2 41958		1357	80
D2 41959		2461	150
D2 41960		12962	530
D2 41961		1764	110
D2 41962		1748	110

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DATE PRINTED: 5-OCT-89

PROJECT: 89BC019

PAGE 1

SAMPLE NUMBER	ELEMENT UNITS	WT G	WT-150 G	WT+150 G	Au-150 GMT	Au+150 GMT	Au+150 MG	Au TOT GMT
D2 101029		29.17	293.7	0.61	1.75	480.3	0.293	2.74
D2 101031		29.17	310.0	1.37	2.43	21.2	0.029	2.52
D2 101047		29.17	201.4	1.14	1.47	11.4	0.013	1.53

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Geochemical
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PROJECT: 89BC019

PAGE 1

REPORT: V89-06171.1

SAMPLE NUMBER	ELEMENT UNITS	Au PPB	SAMPLE NUMBER	ELEMENT UNITS	Au PPB
D2 41901		34	D2 41941		4922
D2 41902		18	D2 41942		9311
D2 41903		28	D2 41943		444
D2 41904		112	D2 41944		274
D2 41905		226	D2 41945		204
D2 41906		263	D2 41946		348
D2 41907		287	D2 41947		178
D2 41908		356	D2 41948		151
D2 41909		81	D2 41949		154
D2 41910		152	D2 41950		130
D2 41911		129	D2 41951		4281
D2 41912		337	D2 41952		190
D2 41913		165	D2 41953		804
D2 41914		45	D2 41954		>10000
D2 41915		68	D2 41955		7944
D2 41916		125	D2 41956		238
D2 41917		85	D2 41957		277
D2 41918		452	D2 41958		238
D2 41919		68	D2 41959		143
D2 41920		74	D2 41960		221
D2 41921		67	D2 41961		326
D2 41922		44	D2 41962		238
D2 41923		13			
D2 41924		10			
D2 41925		28			
D2 41926		14			
D2 41927		20			
D2 41928		54			
D2 41929		50			
D2 41930		25			
D2 41931		12			
D2 41932		22			
D2 41933		32			
D2 41934		190			
D2 41935		172			
D2 41936		187			
D2 41937		73			
D2 41938		146			
D2 41939		2486			
D2 41940		541			

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DATE PRINTED: 27-SEP-89

PROJECT: 89BC019

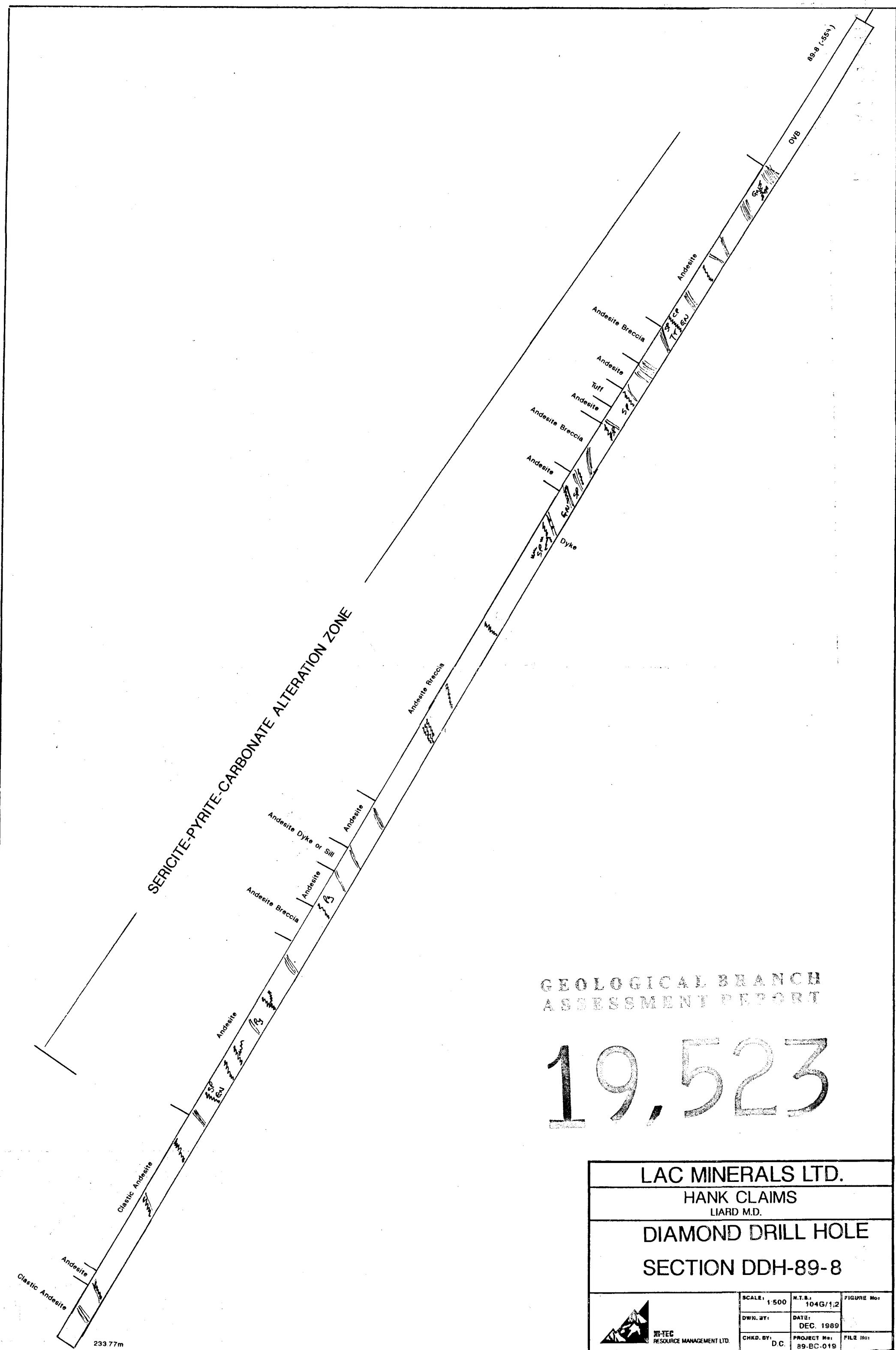
PAGE 1

REPORT: V89-06097.6

SAMPLE NUMBER	ELEMENT UNITS	Au GMT	Ag GMT	Pb PCT	Zn PCT
R2 89HANK-5139		0.41			
R2 89HANK-5157		0.27			
R2 89HANK-5159		1.20			
R2 89HANK-5161		2.06	1.40		
R2 89HANK-5163		0.93			
D2 41548		1.37			
D2 41554		0.27			
D2 41558		0.99			
D2 41559		0.27			
D2 41563		0.38			
D2 41566		0.24			
D2 41567		0.79			
D2 41582		0.21			
D2 41587		0.21			
D2 41588		1.47	1.39	3.51	
D2 41590		0.21			
D2 41594		0.45			
D2 41597		0.31			
D2 41598		0.17			
D2 41599		0.21			
D2 41600		0.99			
D2 41608		0.65			
D2 41609		2.02	2.07	1.18	

APPENDIX IVC
GEOLOGICAL CROSS-SECTIONS FOR
DIAMOND DRILL HOLES





GEOLOGICAL BRANCH AGRICULTURAL RESEARCH

19,523

LAC MINERALS LTD.

HANK CLAIMS
LIARD M.D.

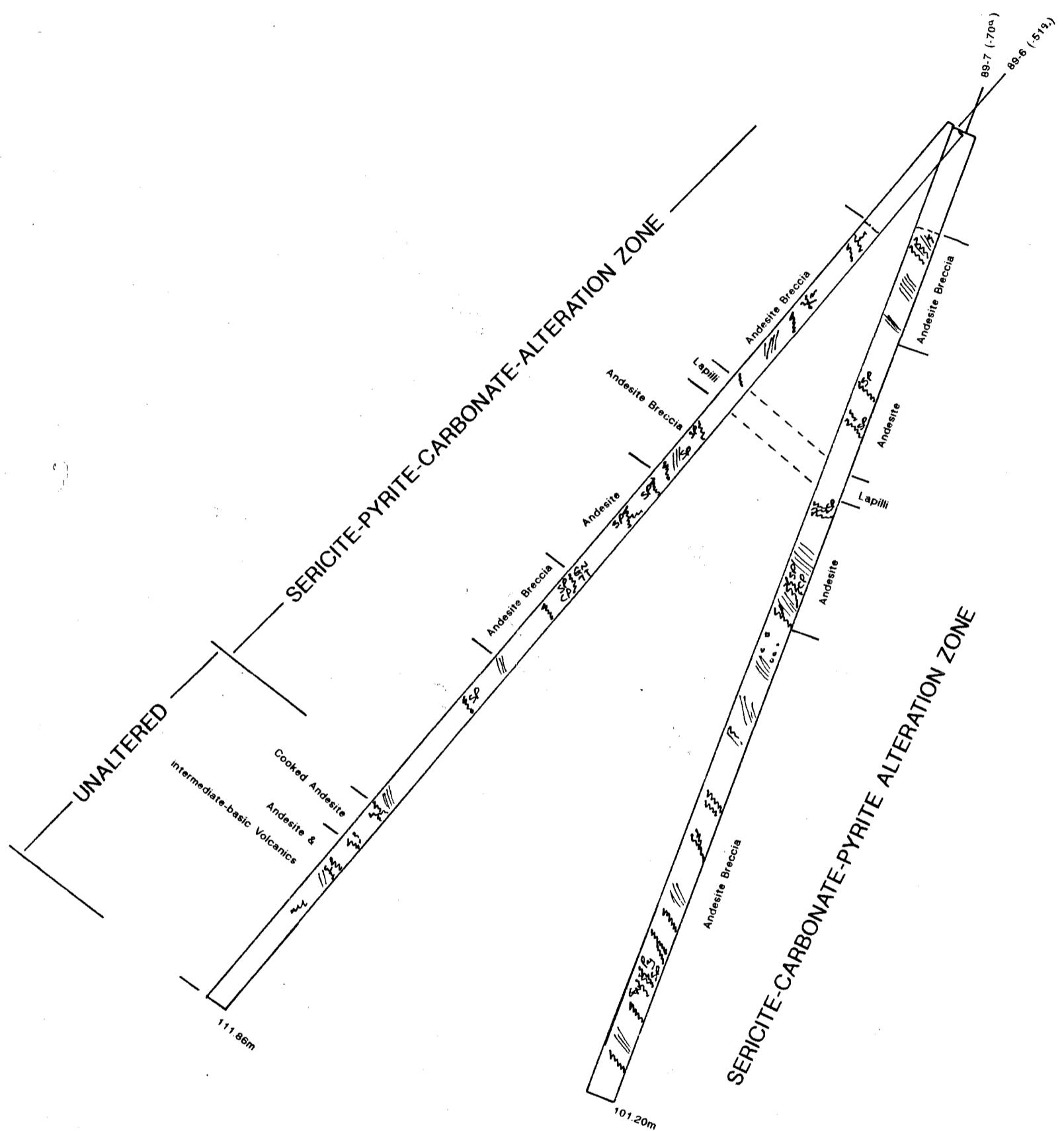
DIAMOND DRILL HOLE

SECTION DDH-89-8



ME-TEC
RESOURCE MANAGEMENT LTD.

SCALE:	1:500	N.T.S.:	104G/12	FIGURE No.:
DRAWN BY:		DATE:	DEC. 1989	
CHKD. BY:	P.C.	PROJECT NO.:		FILE NO.:



GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,523

LAC MINERALS LTD.

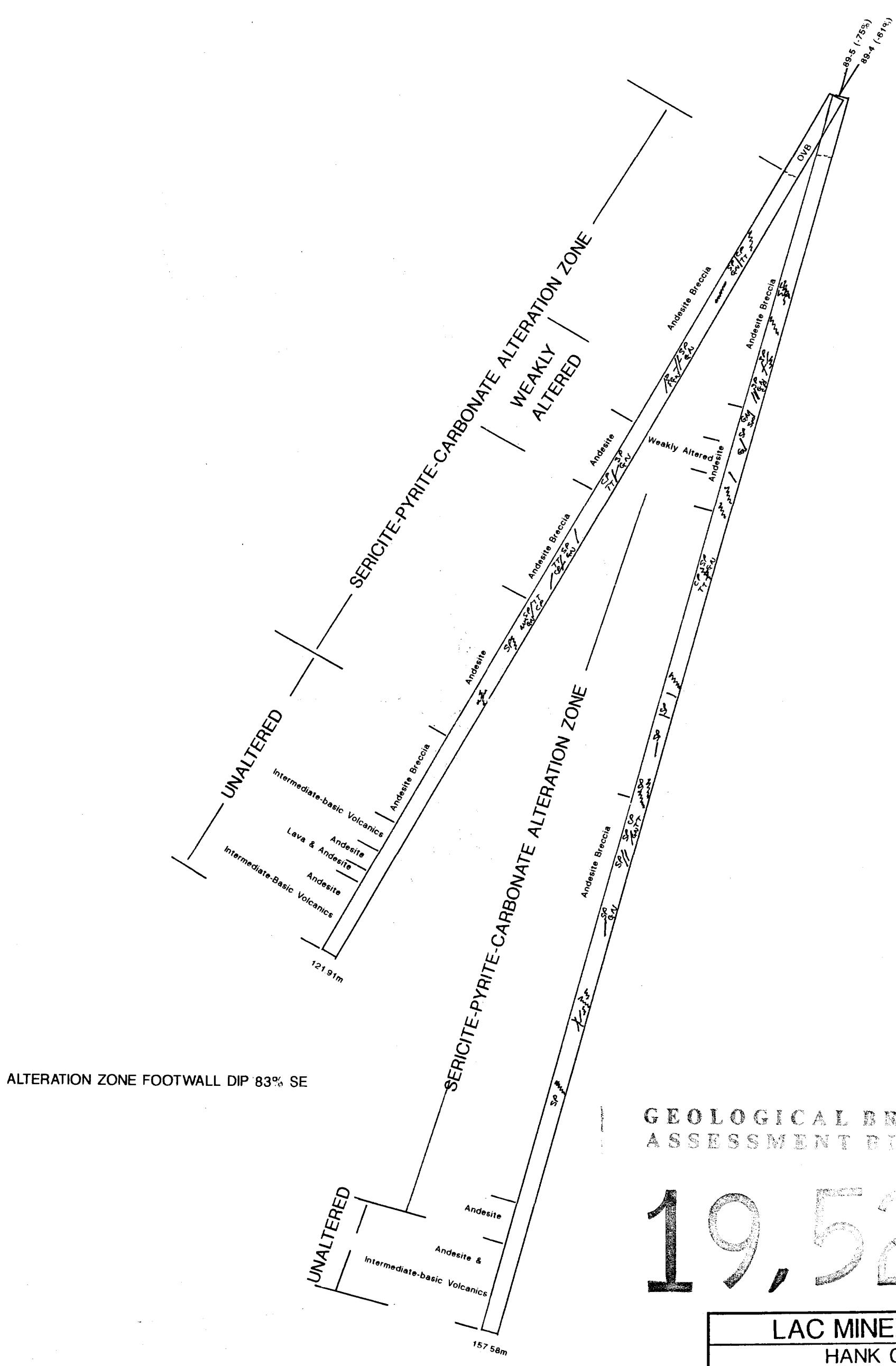
HANK CLAIMS
LIARD M.D.

DIAMOND DRILL HOLE
SECTION DDH-89-6,7



SCALE: 1:500	N.T.S.: 104G/1,2	FIGURE No:
DRAWN BY:	DATE:	
	DEC. 1989	

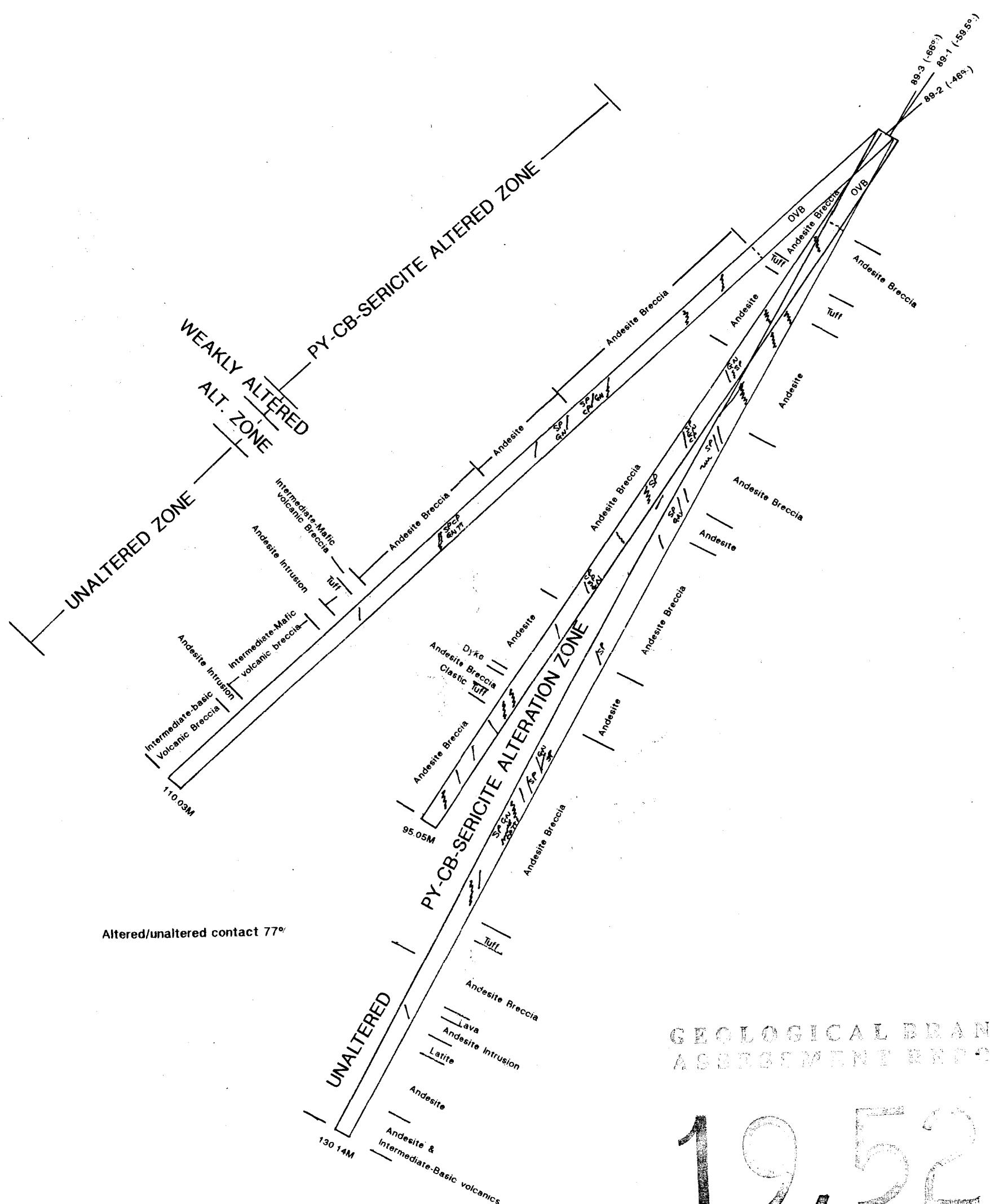
CHKD. BY:	PROJECT No:	FILE No:
D.C.	89-BC-019	



GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,923

LAC MINERALS LTD.		
HANK CLAIMS LIARD M.D.		
DIAMOND DRILL HOLE		
SECTION DDH-89-4,5		
 M-TEC RESOURCE MANAGEMENT LTD.	SCALE: 1:500	M.T.S.: 104G/1.2
	DWN. BY: D.C.	DATE: DEC. 1989
	CHKD. BY: D.C.	PROJECT No: 89-BC-019
		FILE No:

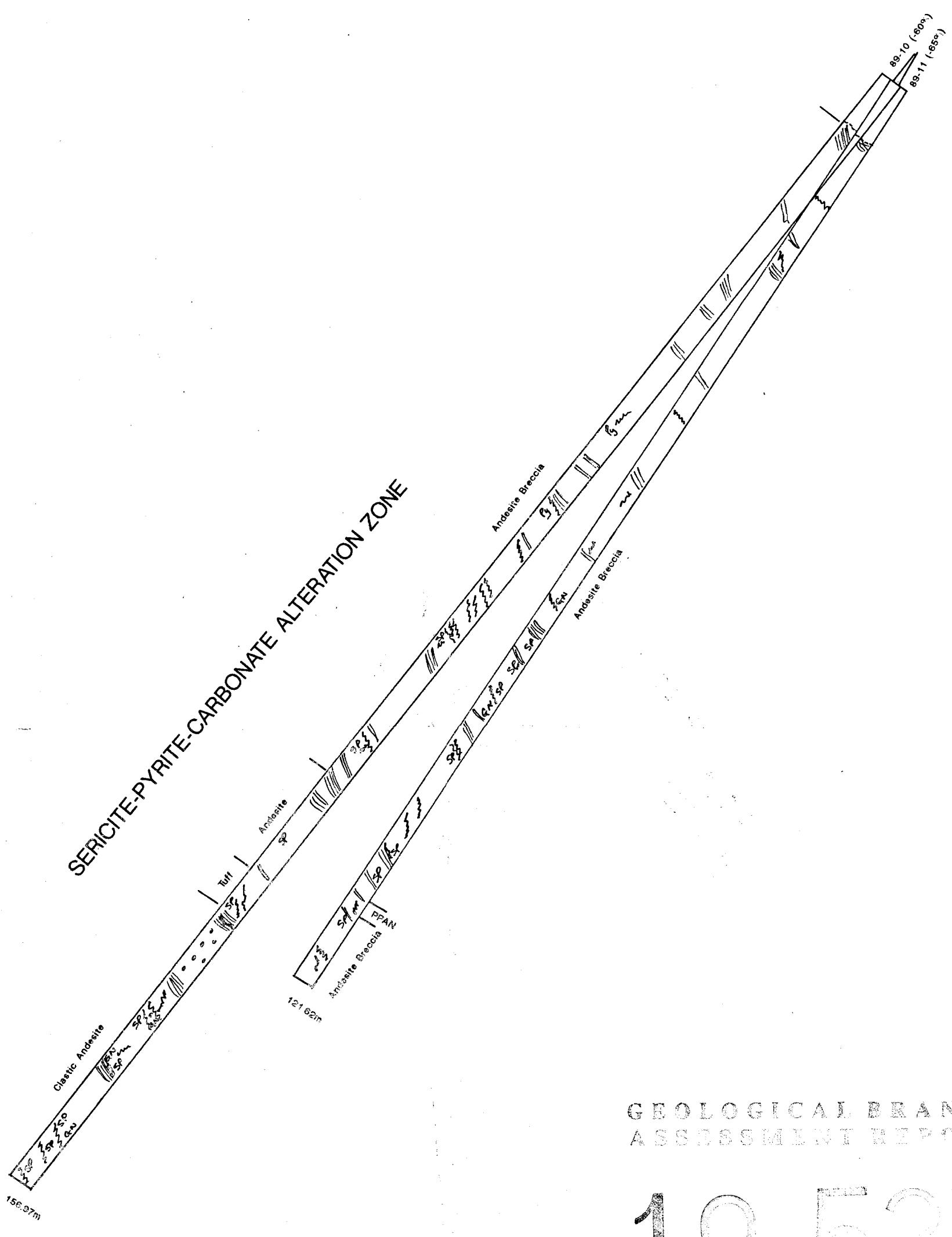


GEOLOGICAL BRANCH
ASSOCIATION OF
INDIA

LAC MINERALS LTD.
HANK CLAIMS
LIARD M.D.
DIAMOND DRILL HOLE
SECTION DDH-89-1,2,3



 M-TEC RESOURCE MANAGEMENT LTD.	SCALE:	1:500	N.T.S.:	104G/1.2	FIGURE No:
	DWN. BY:		DATE:	DEC. 1989	
	CHKD. BY:	D.C.	PROJECT No:	-89-BC-013	



GEOLOGICAL BRANCH
ASSESSMENT REPORT

A horizontal row of five handwritten-style labels. From left to right, they read: '1', '9', '10', '11', and '12'. Each label is enclosed in a small circle.

LAC MINERALS LTD.
HANK CLAIMS
LIARD M.D.
DIAMOND DRILL HOLE
SECTION DDH-89-10,11



 HI-TEC RESOURCE MANAGEMENT LTD.	SCALE:	1:500	N.T.B.I.	104G/1.2	FIGURE NO:
	DRAWN BY:		DATE:	DEC. 1989	
	CHKD. BY:	D.C.	PROJECT No:	89-BC-019	FILE No:

APPENDIX V
STATISTICAL DATA FOR DIAMOND DRILL HOLES



CORRELATION COEFFICIENTS

	Au	Ag	As	Pb	Cu	Zn	Sb
Au	1.000	0.003	-0.144	0.029	0.111	0.0002	-0.036
Ag		1.000	-0.322	0.275	0.187	0.450	0.017
As			1.000	0.127	-0.209	-0.008	0.358
Pb				1.000	0.317	0.371	-0.028
Cu					1.000	0.111	-0.057
Zn						1.000	0.291
Sb							1.000
Rating:	0.000	to	(+/-)	0.300		Weak	
	(+/-) 0.301	to	(+/-)	0.550		Slight	
	(+/-) 0.551	to	(+/-)	0.800		Moderate	
	(+/-) 0.801	to	(+/-)	1.000		Strong	

SQUARES OF CORRELATION COEFFICIENTS (To express the interaction in percentile)

	Au	Ag	As	Pb	Cu	Zn	Sb
Au	100.0	0.00	2.00	0.08	1.20	0.00	0.10
Ag		100.0	10.30	7.50	3.40	20.20	0.02
As			100.0	1.60	4.30	0.00	12.80
Pb				100.0	10.00	13.70	0.07
Cu					100.0	1.20	0.30
Zn						100.0	8.40
Sb							100.0
Rating:	0.0%	to	9.0%		Weak		
	9.1%	to	30.2%		Slight		
	30.3%	to	64.0%		Moderate		
	64.0%	to	100.0%		Strong		

file: DDH03

COMMAND: CORR

*** CORRELATION MATRIX ***

VARIABLES:

1	__AU	1.00000											
2	__AG	0.78953	1.00000										
3	__AS	0.33374	0.14339	1.00000									
5	__CU	0.43517	0.60955	0.11270	1.00000								
9	__PB	0.59060	0.38332	0.04325	0.36044	1.00000							
10	__SB	0.09062	0.03778	0.30021	0.19210	0.15651	1.00000						
11	__ZN	0.33047	0.39053	0.11630	0.51518	0.59480	0.27507	1.00000					
12	__HG	0.39984	0.52037	0.20124	0.65333	0.55856	0.21846	0.85241	1.00000				
	1 __AU	2 __AG	3 __AS	5 __CU	9 __PB	10 __SB	11 __ZN	12 __HG					

DATA SET HAS 70 VALID CASES

file: DDHS

COMMAND: CORR MISSING VALUE TREATMENT: PAIRWISE

(NUMBER OF VALID CASES APPEARS UNDER COEFFICIENT)

*** CORRELATION MATRIX ***

VARIABLES:

1 AU 1.00000

4 AG 0.80684 1.00000

—
—
—

5 AS 0.24298 0.27142 1.00000

1000

7 CU 0.41253 0.73009 0.22331 1.00000

12 PB 0.28501 0.59066 0.28103 0.51826 1.00000

15 ___ZN 0.54771 0.76904 0.24111 0.72647 0.80744 1.00000

17 HG 0.67426 0.70874 0.21562 0.60232 0.54674 0.79736 1.00000

1 ____AU 4 ____AG 5 ____AS 7 ____CU 12 ____PB 15 ____ZN 17 ____HG

file: DDH8

COMMAND: CORR MISSING VALUE TREATMENT: PAIRWISE

(NUMBER OF VALID CASES APPEARS UNDER COEFFICIENT)

*** CORRELATION MATRIX ***

VARIABLES:

1	__AU	1.00000													
4	__AG	0.65649	1.00000												
		108													
5	__AS	0.19436	0.31615	1.00000											
		108	108												
7	__CU	0.52377	0.82129	0.27440	1.00000										
		108	108	108											
12	__PB	0.60405	0.95775	0.24798	0.78748	1.00000									
		108	108	108	108										
15	__ZN	0.68876	0.96614	0.24435	0.81411	0.97404	1.00000								
		108	108	108	108	108									
17	__HG	0.64203	0.69587	0.24986	0.50025	0.70225	0.68426	1.00000							
		108	108	108	108	108	108								
		1	__AU	4	__AG	5	__AS	7	__CU	12	__PB	15	__ZN	17	__HG

file: DDH9.

COMMAND: CORR MISSING VALUE TREATMENT: PAIRWISE

(NUMBER OF VALID CASES APPEARS UNDER COEFFICIENT)

*** CORRELATION MATRIX ***

VARIABLES:

1	__AU	1.00000													
3	__AG	0.61028	1.00000												
		139													
4	__AS	0.30069	0.15349	1.00000											
		139	139												
6	__CU	0.14071	0.43681	0.23547	1.00000										
		139	139	139											
11	__PB	0.37140	0.49179	0.33201	0.73281	1.00000									
		139	139	139	139										
14	__ZN	0.32045	0.48723	0.28440	0.79607	0.97323	1.00000								
		139	139	139	139	139									
15	__HG	0.33696	0.44993	0.29271	0.61175	0.92655	0.93090	1.00000							
		139	139	139	139	139	139								
		1	__AU	3	__AG	4	__AS	6	__CU	11	__PB	14	__ZN	15	__HG

file: DDH10

COMMAND: CORR MISSING VALUE TREATMENT: PAIRWISE

(NUMBER OF VALID CASES APPEARS UNDER COEFFICIENT)

*** CORRELATION MATRIX ***

VARIABLES:

file: DH11

COMMAND: CORR MISSING VALUE TREATMENT: PAIRWISE

(NUMBER OF VALID CASES APPEARS UNDER COEFFICIENT)

*** CORRELATION MATRIX ***

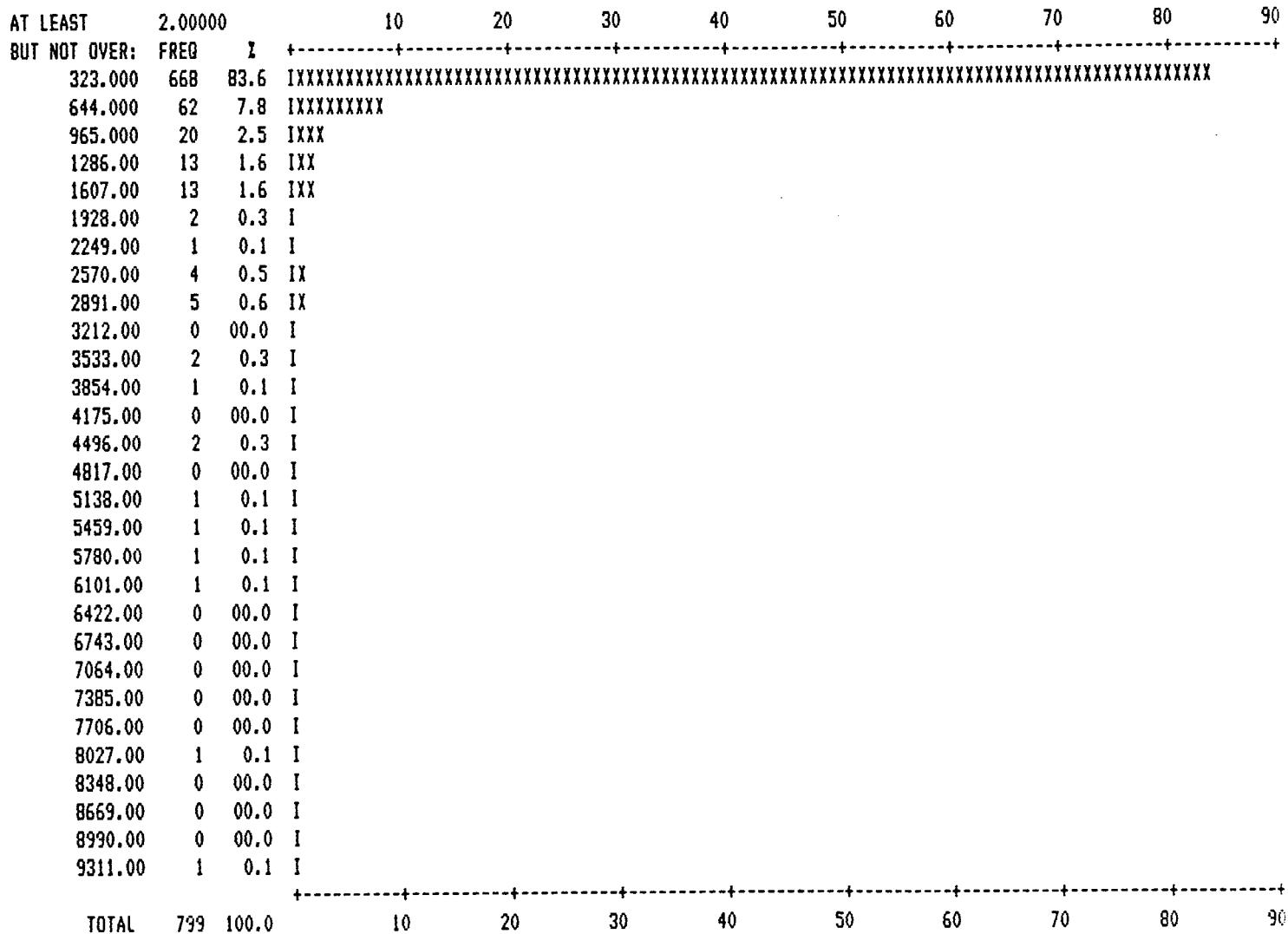
VARIABLES:

1 AU_PPB	1.00000							
5 ___AG	0.96078	1.00000						
	61							
6 ___AS	0.28131	0.14199	1.00000					
	61	62						
8 ___CU	0.62370	0.47123	0.57185	1.00000				
	61	62	62					
13 ___PB	0.33113	0.24422	0.53732	0.65050	1.00000			
	61	62	62	62				
15 ___ZN	0.53418	0.61430	0.29859	0.61680	0.41441	1.00000		
	61	62	62	62	62			
17 ___HG	0.65809	0.65060	0.41851	0.83087	0.53072	0.88276	1.00000	
	61	62	62	62	62	62		
1 AU_PPB	5 ___AG	6 ___AS	8 ___CU	13 ___PB	15 ___ZN	17 ___HG		

file: HISTDDH

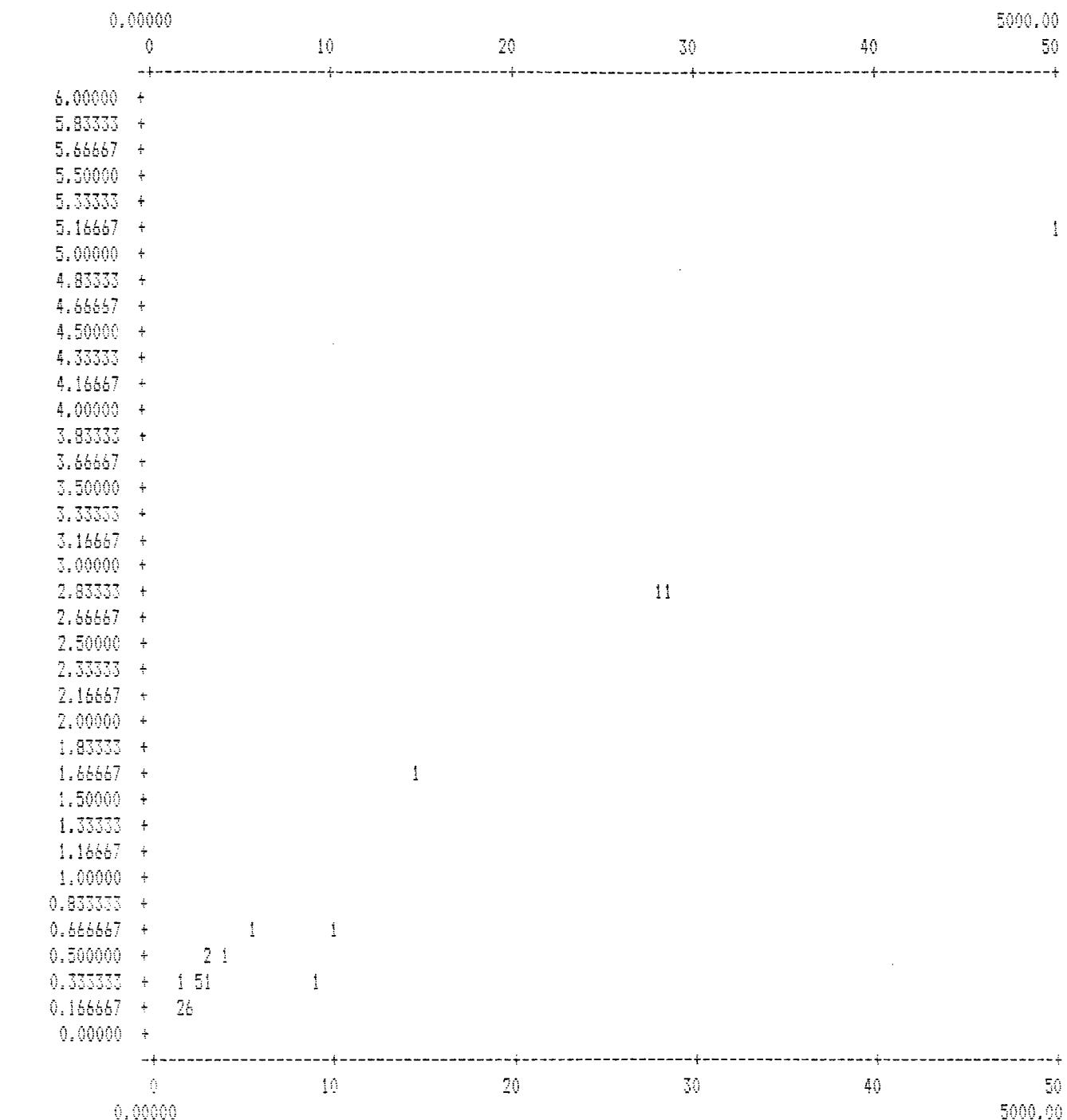
COMMAND: HIST MISSING VALUE TREATMENT: VARWISE

VARIABLE: 1 AU AUTO/29



File: DDW01

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE

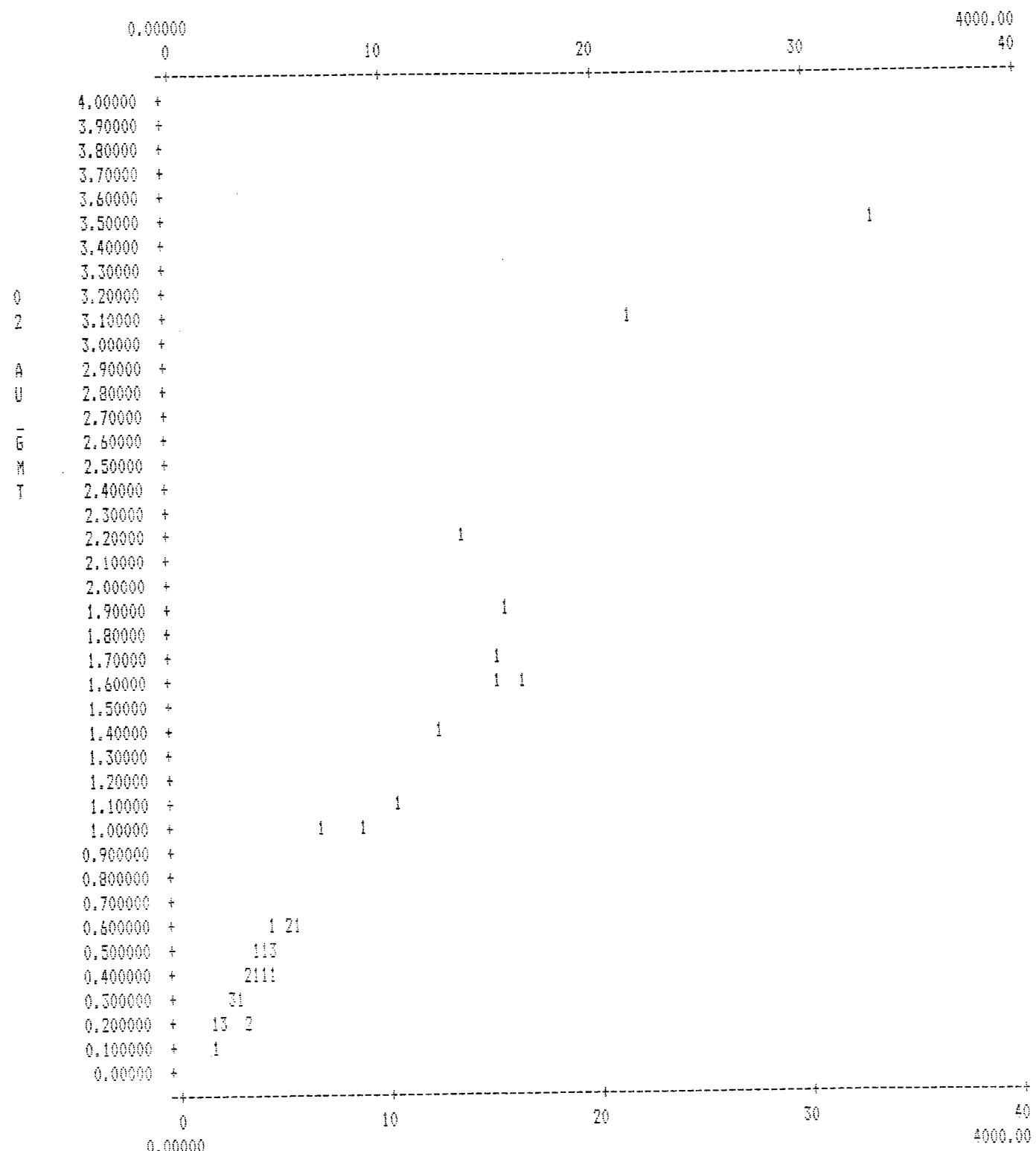


TOTAL POINTS PLOTTED: 25

1 AU_PPB

file: DDHOS

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE

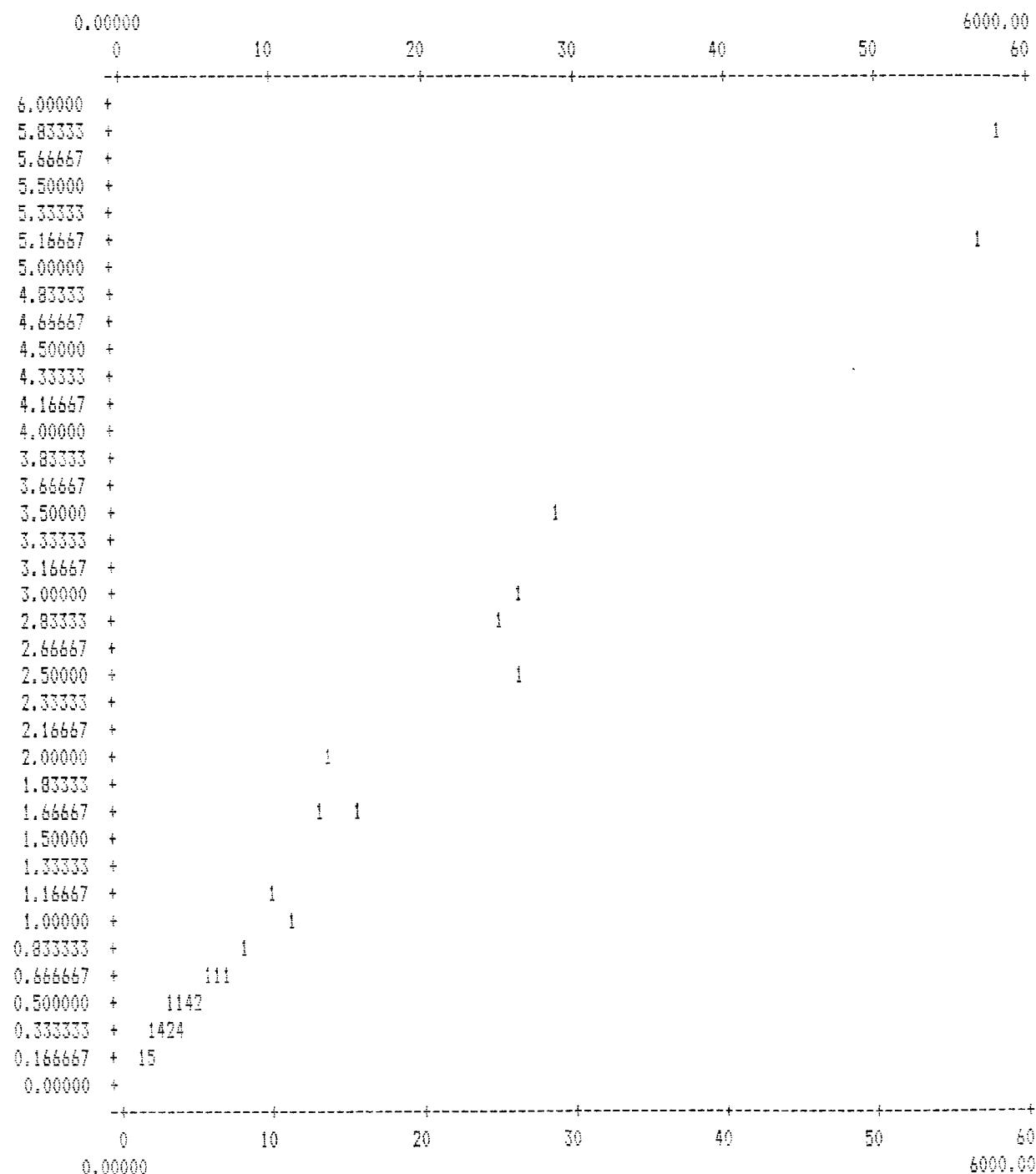


TOTAL POINTS PLOTTED: 36

1 AU_PPB

File: DDH05

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE

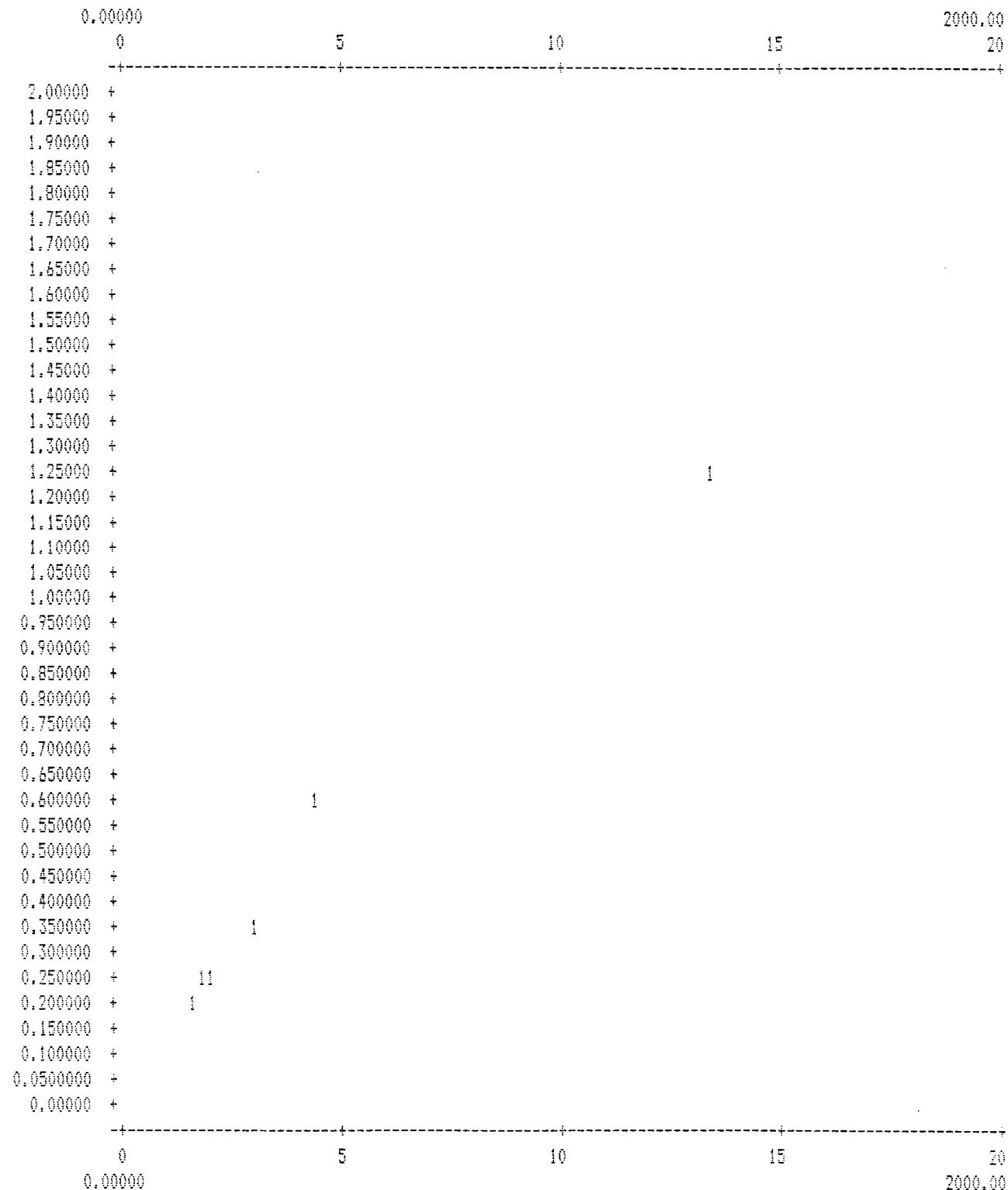


TOTAL POINTS PLOTTED: 40

1 AU_FPB

File: DDH06

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE

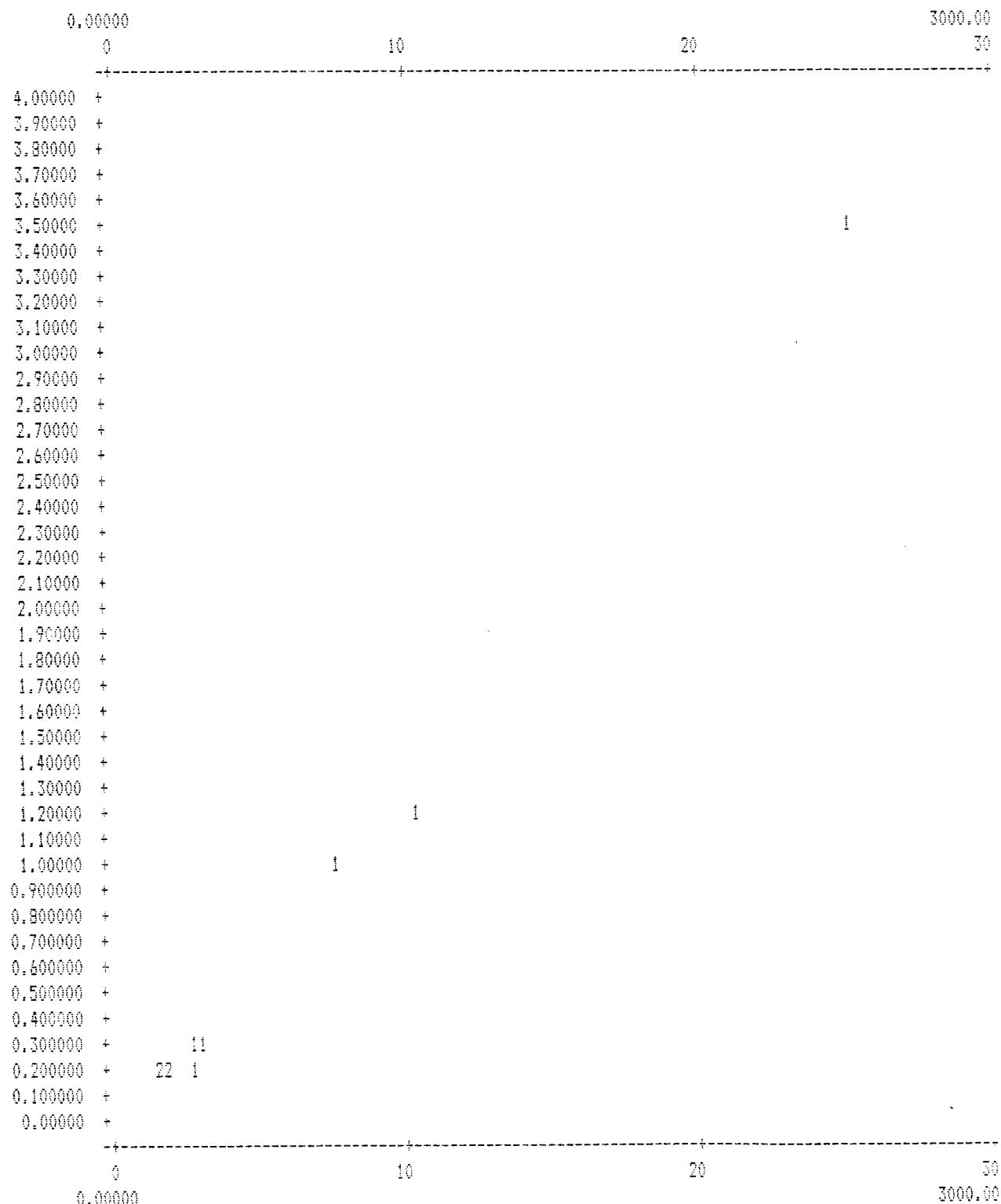


TOTAL POINTS PLOTTED: 6

1 AU_PPB

file: DDH07

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE

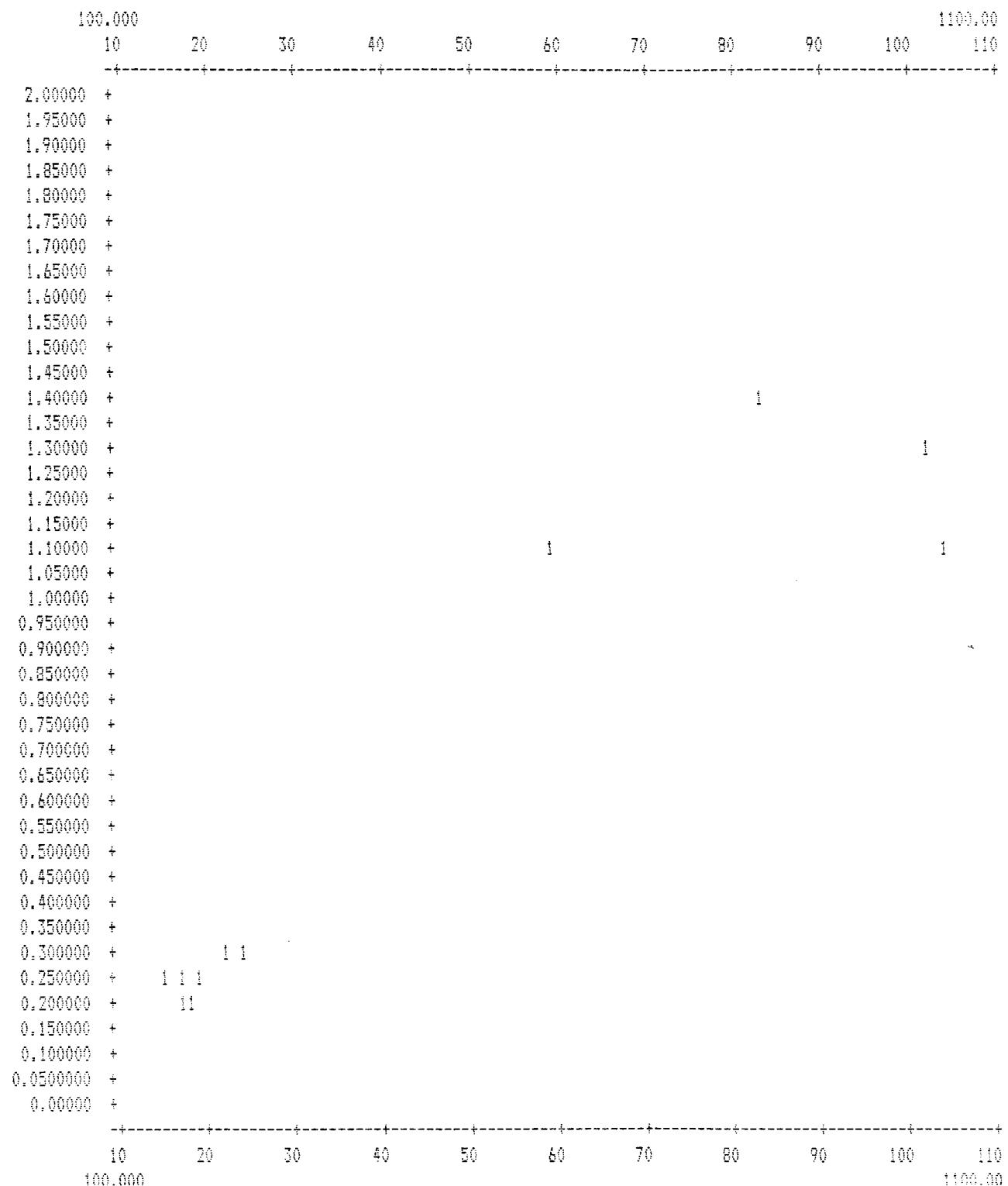


TOTAL POINTS PLOTTED:10

1 AU_PPB

File: DDH08

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE

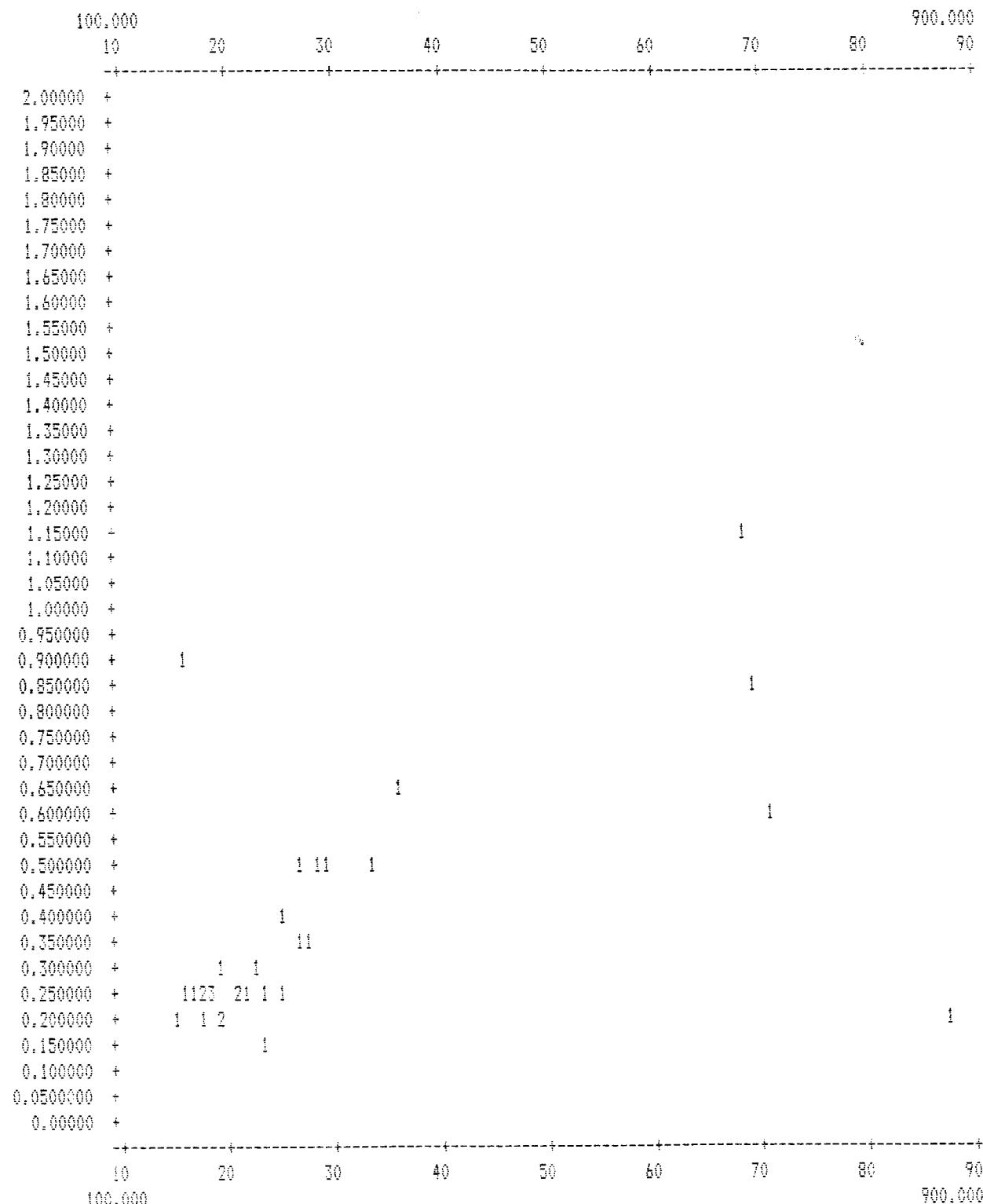


TOTAL POINTS PLOTTED:11

1 AU_PPB

file: DDH07.no

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE

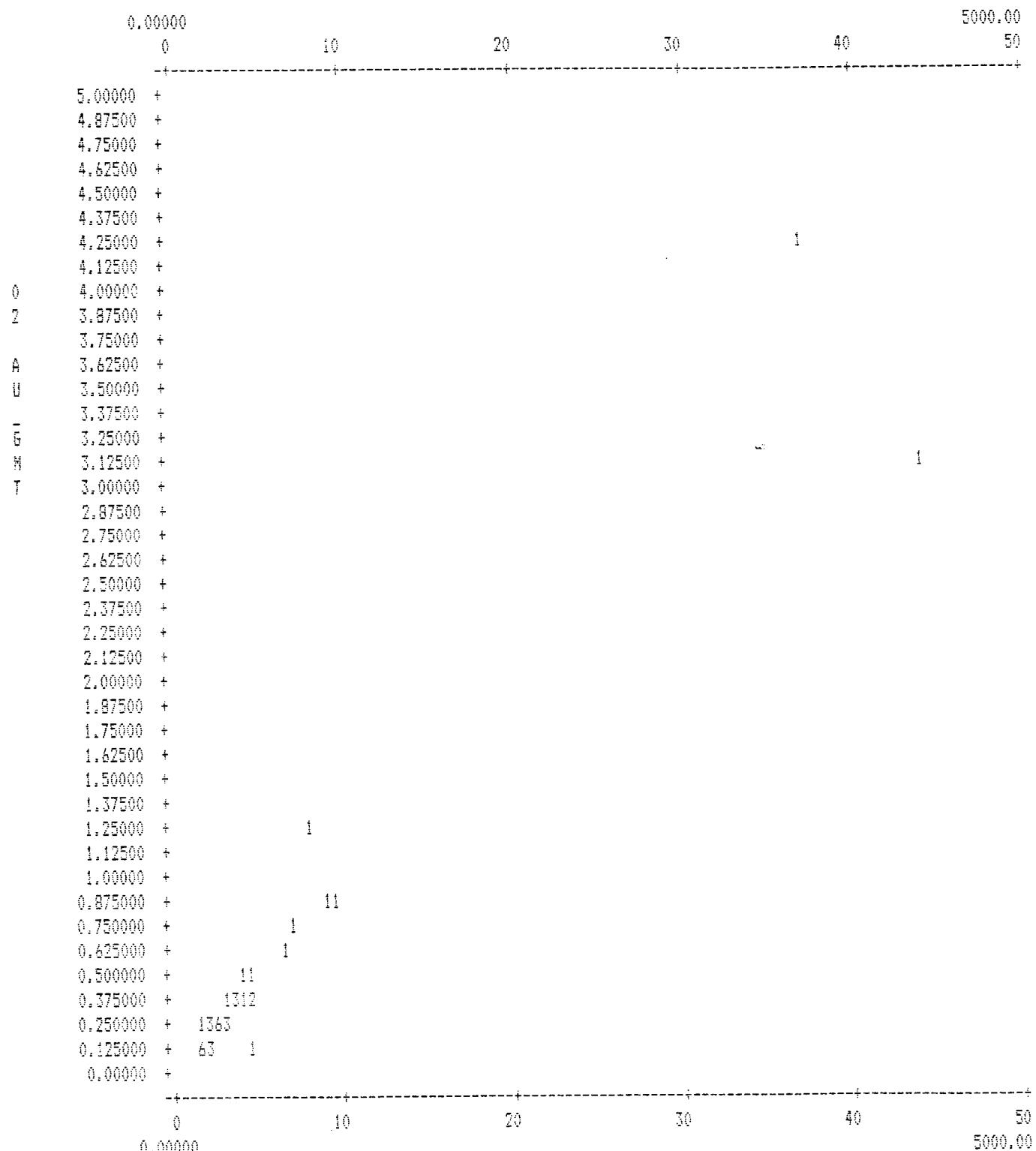


TOTAL POINTS PLOTTED:32

1 AU_PPB

file: DDH10

COMMAND: PLOT MISSING VALUE TREATMENT: LISTWISE



TOTAL POINTS PLOTTED: 39

1 AU_PPB

APPENDIX VI
SURVEY POINT DESCRIPTIONS AND SURVEY DATA



HANK CLAIMS SURVEY DATA: HI-TEC project No. 89-BC-019

Point	Northing	Easting	Elevation	Description
2	10670.136	10162.749	1116.820	89-1
	10670.236	10162.349	1116.820	89-2
	10670.036	10163.149	1116.820	89-3
3	10645.542	10132.445	1110.010	89-4
	10645.342	10132.645	1110.010	89-5
4	10573.316	10073.404	1103.950	89-6
	10573.116	10073.504	1103.950	89-7
5	10545.493	10039.778	1097.350	88-22
6	10454.401	10037.800	1114.040	89-8.
9	10624.119	10424.709	1214.140	88-6
17	11017.406	10434.765	1124.170	89-9.
18	11084.152	10424.19	1107.080	On Ck 7 galena vein trench
24	10230.807	10999.167	1470.310	85-2
26	10269.439	10994.260	1473.840	85-21
27	10345.764	11089.112	1492.710	85-23
28	10252.738	11128.948	1514.350	85-29
30	10433.545	11309.328	1542.100	85-33
34	11347.327	10645.748	1121.510	88-14
35	11449.180	10697.300	1105.270	89-10
	11448.980	10697.500	1105.270	89-11
36	11378.214	10892.921	1142.680	88-21
39	11118.137	10422.858	1093.750	88-10,12
69	9715.732	10424.200	1399.120	88-9
180	10653.705	10240.051	1163.300	88-19
200	11303.470	10000.000	912.310	Hank 1,2,3 LCP
	10460.593	10124.678	1157.350	88-2
	10898.606	10451.465	1159.170	88-8
	10668.142	10143.845	1110.010	87-3
	10667.842	10144.445	1113.010	87-4

Additional points relate to topographic features and are shown on Figure 4 of the current report.

Point : Northing Easting Elevation Description

	Scale	N Shift	1,000000	1,000000	List Points	Z Shift	.000000	E Shift	.000000
1			10805.573		10271.612	1119.330	Pt		
2			10671.536		10159.049	1116.820	Pt		
3			10638.442		10125.345	1110.010	Pt		
4			10571.116		10075.604	1103.950	PT		
5			10545.493		10039.778	1097.350	Pt		
6			10463.301		10042.300	1114.040	Pt		
7			10766.986		10420.048	1176.420	PT		
8			12803.470		10000.000	.000	Pt		
9			10624.119		10424.709	1214.140	PT		
10			10599.917		9858.388	1033.010	Pt		
11			10539.533		10444.413	1229.440	Pt		
12			10285.833		10339.305	1243.020	Pt		
13			10194.906		10421.176	1285.140	Pt		
14			10812.689		10470.504	1188.810	Pt		
15			10133.884		10347.338	1285.700	Pt		
16			10805.947		10412.453	1168.790	Pt		
17			11017.406		10434.765	1124.170	Pt		
18			11084.152		10424.190	1107.080	PT		
19			11165.540		10444.018	1095.440	Pt		
20			11271.173		10546.369	1099.980	PT		
21			10083.740		10403.878	1321.220	PT		
22			10043.899		10436.249	1349.150	Pt		
23			10230.656		10877.575	1463.800	Pt		
24			10320.807		10999.167	1470.310	Pt		
25			12803.470		13000.000	.000	Pt		
26			10269.439		10994.260	1473.840	Pt		
27			10345.764		11089.112	1492.710	Pt		
28			10252.738		11128.948	1514.350	Pt		
29			10243.073		11171.950	1530.230	Pt		
30			10433.545		11309.328	1542.100	Pt		
31			10121.057		11042.475	1497.120	Pt		
32			10205.408		11110.967	1516.610	Pt		
33			11303.470		13000.000	.000	Pt		
34			11347.327		10645.748	1121.510	Pt		
35			11449.180		10697.300	1105.270	Pt		
36			11482.648		10877.947	1142.680	Pt		
37			11303.470		8000.000	.000	Pt		
38			11247.943		10559.007	1105.550	Pt		
39			11169.123		10441.710	1093.750	Pt		
40			11132.139		10778.525	1200.600	Pt		
41			11414.283		10629.829	1094.410	Pt		
42			11341.210		10718.688	1147.500	Pt		
43			11313.491		10735.223	1154.050	Pt		
44			10760.809		10431.679	1184.950	Pt		
45			8803.470		8000.000	.000			
46			8803.470		10000.000	.000			
47			8803.470		12000.000	.000			
48			11303.470		12000.000	.000			
52			10671.012		9351.447	930.800	rebar, camp1		
53			10737.425		9458.905	935.350			
54			10782.318		9435.089	927.000			
55			11324.493		10032.320	914.300			
56			10457.526		11368.860	1549.950			
57			10482.220		11391.444	1550.510			
58			10535.271		11442.474	1569.070			
59			10611.710		11518.761	1579.270			
60			10293.631		11219.540	1533.310			

59 10611.710 11518.761 1579.270
60 10293.631 11219.540 1533.310
61 10226.488 11145.297 1525.540

A. A. DeBRUYEN, B.C.L.S.
File=C:\MSURVEY\89-136
Client: Lac Minerals

Sep. 29, 1989
File size=200
Job 1 Hank group of claims

Point	Northing	Easting	Elevation	Description
62	9897.028	11174.357	1516.600	
63	9894.043	11077.445	1497.270	
64	10060.944	11032.939	1488.630	
65	9957.979	11011.153	1471.060	
66	9768.552	10977.023	1442.560	
67	9574.159	10658.934	1451.670	
68	9552.627	10575.545	1423.890	
69	9776.596	10607.878	1399.120	
100	12605.053	9929.889	1400.000	12" spike
101	13064.369	9990.820	,000	Peak
150	9663.619	10677.130	,000	Peak
180	10686.424	10314.758	1163.300	Pt
198	10198.023	10719.427	1477.270	Wood hub #51
199	10198.252	10712.000	1476.520	12" spike
200	11303.470	10000.000	912.310	L.C.P.

APPENDIX VIIa

STATEMENT OF COSTS HI-TEC RESOURCE MANAGEMENT LTD.



STATEMENT OF COSTS

PROJECT 89BC019

HANK PROPERTY

Period of Field Work: July 10 - Sept.13, 1989

Salaries

D.Collins, Snr.Geologist, 55.0 days @\$300/day	\$ 16,500.00
Y.Ming So, Geologist, 61.0 days @\$200/day	12,200.00
J.Dahrouge, Tech. Phase 1, 37.0 days @\$150/day	5,550.00
J.Cooper, Cook Phase 1, 38.0 days @\$150/day	5,700.00
J.Dahrouge, Assistant Geologist Phase 2, 23.0 days @\$200/day	4,600.00
C.Rogers, Technician, 34.0 days @\$150/day	5,100.00
J.Himmelright, Technician, 34.0 days @\$150/day	5,100.00
P.Daigle, Technician, 61.0 days @\$150/day	9,150.00
J.Cooper, Cook Phase 2, 23.0 days @\$170/day	3,910.00
	\$ 67,810.00

Project Expenses

Project Preparation	5,483.20
 Mobilization/demobilization	
Air Fares, salaries, domicile, truck rental, freight	13,179.82
Helicopter Support 20.9 hours @\$628/hour	13,125.20
	26,305.02
 Domicile	
Camp Rental	
279 man days @\$16.72/man day(Ph.1)	4,664.88
249 man days @\$20.00/man day(Ph.2)	4,980.00
Food	
For Hi-Tec crew 367 man days @\$25.00/man day	9,175.00
For Drillers 116 man days @\$25.00/man day	2,900.00
For LAC personnel 45 man days @\$25.00/man day	1,125.00
	22,844.88
 Geochemistry	
Freight charges	943.84
Hotel charges incurred delivering samples to Smithers	381.27
	1,325.11
 Drilling	
Helicopter and Fuel 38.6 hours @\$628/hour	24,240.80
Core shack and splitter 32 days @\$30/day	960.00
	25,200.80
 Cat Access Route Selection and Examination	
Helicopter and fuel 10.3 Hours @\$628/hour	6,468.40
D.Collins Salary	
Field 2.00 man days @\$300/man day	600.00
Office 2.14 man days @\$300/man day	642.00
Miscellaneous expenses	79.42
	7,789.82
 Helicopter and fuel 48.5 Hours @\$628/hour + 41.14 oil chge	30,499.14

Truck rental and repair 2.5 months @ \$2,007.66/month	5,019.15
ATV rental and repair 2.0 months @\$1,590/month plus repairs	3,450.79
Radio and Radio Telephone rental	2,500.00
Walkie Talkie Rentals 5 Walkie talkies 2.5 months @\$106/mnth	1,325.00
Field Supplies (Includes Lumber, hardware, fuel etc)	8,130.60
Field equipment rental and maintenance	1,228.28

Computer Rental 66 days @\$20/day	1,320.00
Expediting	3,063.93
Accounting, Communications, Freight	4,785.67
Data interpretation and Report writing	8,250.00
Additional costs incurred for replotting and redrafting new base, geology etc. maps required to correct significant errors, as shown by survey, in original LAC maps	8,835.29
Photocopying and reproduction	803.48
15% Project Management Fee	21,811.76

TOTAL COST	\$ 257,781.92
	=====

page two of two pages

APPENDIX VIIb
STATEMENT OF TOTAL PROJECT COSTS



STATEMENT OF COSTS

HANK PROPERTY, LAC MINERALS LTD.
PROJECT B9BC019

SALARIES

D.Collins	Snr. Geologist	55 days @	\$300.00 /day	\$16,500.00
Y. Ming So	Geologist	61 days @	\$200.00 /day	\$12,200.00
J.Dahrouge	Tech. Phase I	37 days @	\$150.00 /day	\$5,550.00
J.Cooper	Cook Phase I	38 days @	\$150.00 /day	\$5,700.00
J.Dahrouge	Ass. Geologist Ph. II	23 days @	\$200.00 /day	\$4,600.00
C. Rogers	Tech. Phase I	34 days @	\$150.00 /day	\$5,100.00
J.Himmelright	Tech. Phase I, II	34 days @	\$150.00 /day	\$5,100.00
P.Daigle	Tech. Phase I, II	61 days @	\$150.00 /day	\$9,150.00
J.Cooper	Cook Phase II	23 days @	\$170.00 /day	\$3,910.00
				\$67,810.00

PROJECT EXPENSES

Project Preparation		\$5,483.20
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MOBILIZATION/DEMOBILIZATION

Air fares, salaries, domicile, truck rental, freight		13179.82
Helicopter support 20.9 hours @ \$628/hour		13125.2
		\$26,305.02

DOMICILE

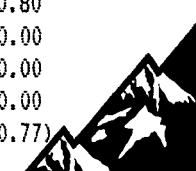
279 man days	@	\$16.72 /man day	Camp Rental Phase I	\$4,664.88
249 man days	@	\$20.00 /man day	Camp Rental Phase II	\$4,980.00
367 man days	@	\$25.00 /man day	Food for Hi-Tec Crew	\$9,175.00
116 man days	@	\$25.00 /man day	Food for Drillers	\$2,900.00
45 man days	@	\$25.00 /man day	Food for LAC personnel	\$1,125.00
				\$22,844.88

GEOCHEMISTRY AND LABORATORY SERVICE (mainly invoiced directly to LAC)

Special Order	25 sample	\$12.75 /Au, Ag FA	\$318.75
Special Order	101 sample	\$8.25 /Au	\$833.25
Special Order	216 sample	\$9.75 /Au	\$2,106.00
Special Order	43 sample	\$7.00 /Pb, Zn	\$301.00
Special Order	3 sample	\$9.75 /Ag	\$29.25
Rocks	168 sample	\$3.75 /sample preparation	\$630.00
	168 sample	\$19.50 /Lac Package	\$3,276.00
Core	478 sample	\$3.75 /sample preparation	\$1,792.50
	478 sample	\$19.50 /Full Lac Package	\$9,321.00
Core	337 sample	\$3.75 /sample preparation	\$1,263.75
	337 sample	\$11.25 /Geochem Au	\$3,791.25
Shipping Charges paid by Bondar-Clegg			\$67.00
Fax service			\$15.00
Freight Charges paid by Hi-Tec			\$943.84
Freight Charges paid by LAC			\$292.00
Hotel charges incurred delivering samples to Smithers			\$381.27
			\$25,361.86

DRILLING

Mob/Demob Drill			\$9,738.76
Diamond Drilling	1610.6 Meters @	\$75.80 /meter	\$122,081.96
Core Boxes and lids	178 Boxes @	\$12.08 /set	\$2,149.35
Helicopter drill in/out	38.6 hours @	\$628.00 /hour	\$24,240.80
Core shack and splitter	32 days @	\$30.00 /day	\$960.00
Cat D-6 time	75 hours @	\$80.00 /hour	\$6,000.00
Pajari tests + rental	8 tests @	\$65.00 /test +	\$600.00 /month rent
Credit for LAC fuel used by Conner's Drilling			\$1,120.00
			(\$2,320.77)



CAT ACCESS ROUTE SELECTION AND EXAMINATION

Locate Route Helicopter	2.7 hours @	\$669.25 /hour	Paid by Lac	\$1,806.98
Transport + manpower for location & costs of LAC supervision visits:				\$2,458.40
2 Airfares @	\$582.00 /each	Paid by Lac		\$1,164.00
2 Airfares @	\$200.00 /each	Northern Mountain to Dease Lk (Paid by Lac)		\$400.00
Hotel in Dease Lk (Paid by Lac)				\$63.72
Miscellaneous Expenses				\$79.42
Expenses Robert Brown of LAC (paid by LAC)				\$201.24
D.Collins Salary (Field)	2 days @	\$300.00 /day		\$600.00
D.Collins Salary (Office)	2.14 days @	\$300.00 /day		\$642.00
Mob/demob D6 cat + cost settlement charges LAC/Pickell (paid by LAC)				\$11,490.27
Cat	184.5 hours @	\$80.00 /hour	(Paid by Lac)	\$14,760.00
Fuel for cat	50 Barrels @	\$100.00 /barrel	(Paid by Lac)	\$5,000.00
Helicopter Operator from cat when walking				
In	10.3 hours @	\$628.00 /hour		\$6,468.40
Helicopter in Fuel	7.1 hours @	\$628.00 /hour	(Invoiced directly to LAC)	\$4,458.80
Helicopter and Fuel	48.5 hours @	\$628.00 /hour + \$41.14 oil		\$30,499.14
Truck Rental & damage repair	2.50 months @	\$2,007.66 /month		\$5,019.15
ATV Rental & repair	2 Months @	\$1,590.00 /month + repairs		\$3,450.79
Radio and Radio Telephone Rental				\$2,500.00
Walkie talkie Rental	2.5 months @	\$530.00 /month		\$1,325.00
FIELD SUPPLIES (includes Lumber, Hardware, fuel etc)				\$8,130.60
Field equipment rental and maintenance				\$1,228.28 \$9,358.88
Computer Rental	66 days @	\$20.00 /day		\$1,320.00
Expediting				\$3,063.93
Accounting, Communications, Freight charges during field work				\$4,785.67
Survey in Points on Property (Paid by LAC)				\$2,140.00
204 Helicopter to move skid (Paid by LAC)				\$3,000.00
LAC expenses from R. Brown for Meals/gas/sundry	Aug. 15,18,19			\$285.70
Data interpretation and Report writing				\$8,250.00
Additional costs incurred for replotting and redrafting new base, geology etc maps required to correct significant errors, as shown by survey, in original LAC maps				\$8,835.29
Photocopying and reproduction				\$803.48
Project Management	15.00%			\$21,811.76

TOTAL COST:

\$467,817.08



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
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
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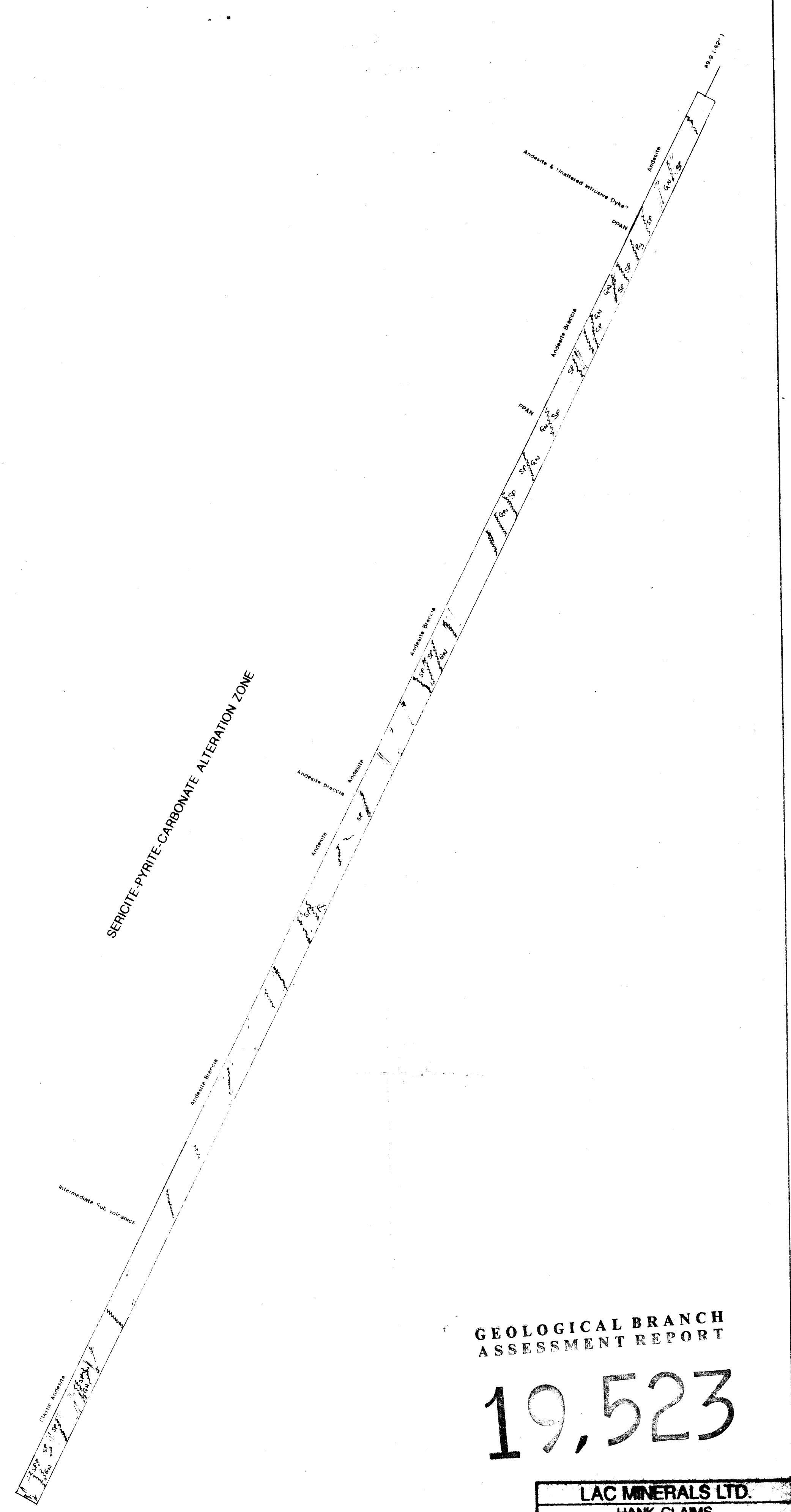
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GEOLOGICAL BRANCH ASSESSMENT REPORT

19,523

LAC MINERALS LTD.

HANK CLAIMS
LARD M.D.


DIAMOND DRILL HOLE

SECTION DDH-89-9

19'523

GEOLoGICAL BRANCH

LITHOLOGIC PROFILE



LEGEND

SAMPLING


- Stream sediment sample
- △ Soil sample (likely contaminated by stream sediments)
- P Soil profile pit
- ✖ Rock sample (grab, float, trenching)
- Grid station
- Diamond drill hole (year-hole no.) DDH 88-1

- CB, QZ, CA
- CP, GN, SP, TT MA
- Mineral showing (chalcopyrite, galena, sphalerite, tetrathedrite, malachite)
- Bedding or contact attitude
- Vein attitude (with main components)
- All attitudes show strike and dip values
- Joint set attitude
- Fault
- Outcrop
- Lithologic major contact (interformational)
- Lithologic minor contact (interformational also surficial boundaries such as talus, ferricrete)
- These contacts and boundaries should be regarded as approx. or inferred

- bxx Breccia
- aggl Agglomerate
- ppan Porphyritic andesite
- pyrc Pyroclastic
- xine Crystalline
- gwyk Greywacke
- sst Sandstone

HANK PROPERTY
LAC MINERALS LTD.

GEOLOGY

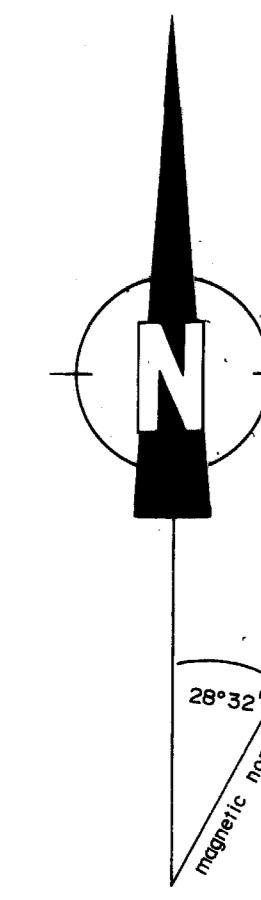


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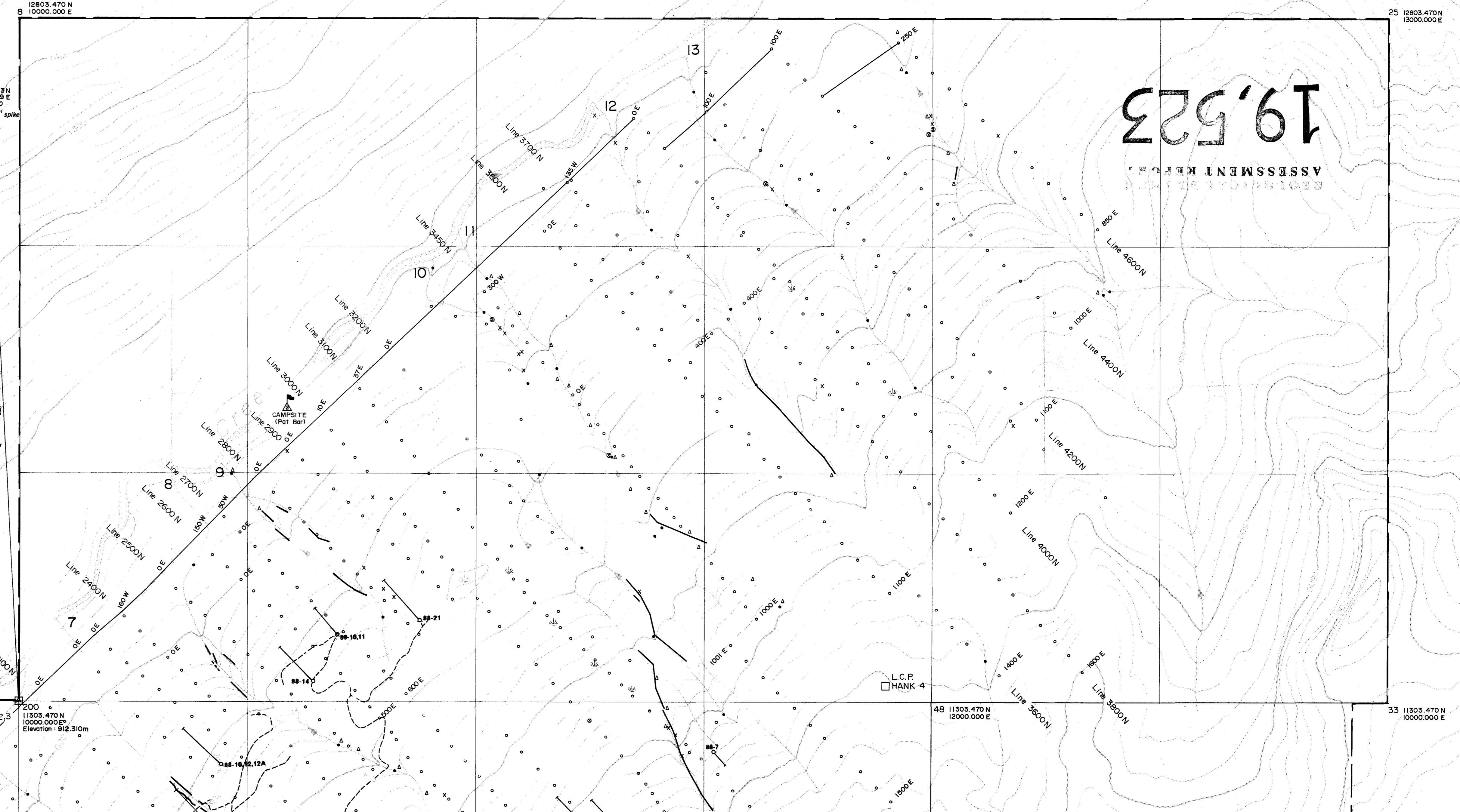
25 12803.470 N
13000.000 E

19'523

ASSESSMENT REPORT



Principled Control Point for Survey
Bearings are stated astronomic
Detailed mapping supplied by
Lac Minerals.
Distances shown are in metres
points denoted marked

LEGEND

- Contours (20m interval)
- Creek
- Sand
- Swamp
- Survey point
- Scarp
- Legal corner post
- Claim group boundary
- Baseline
- Stream sediment sample
- Soil sample (likely contaminated by stream sediments)
- Soil sample
- Soil profile pit
- Rock sample (grab, float, trenching)
- Cat trail
- Drill hole (year-hole number)
- Comsite

0 50 100 200 300 400 500 metres

HANK PROPERTY
LAC MINERALS LTD.

DRILL HOLE LOCATION PLAN

SCALE 1:5000	1:5000	FIGURE NO. 8
DRAWN BY HV	DATE Nov/1989	
CHECKED BY D Collins	DESIGNED BY	PROJECT NO. 2880C219
INTEC RESOURCE MANAGEMENT LTD	FILE NO.	