# KERR PROJECT REPORT - 1989

## VOLUME III OF III

## APPENDICES
(1987-88 Diamond Drill Logs, Lithogeochemistry)



GENERAL CONTENTS

KERR PROJECT REPORT - 1989

VOLUME III OF III

APPENDIX VI

SECTION 1 - 1988 Drill Hole Logs, Lithogeochemistry, Histograms, Microlynx Computer Print-Outs and Cross Sections (in Pocket)(B-Zone Deposit Holes : K88-1,11,14,15,16,17,18, 20, 21 and 22)

SECTION 2 - 1987 Drill Hole Logs, Histograms and Cross Sections (in Pocket)(B-Zone Deposit Holes : K87-5,8)

# DRILL HOLE LOG ABBREVIATIONS

| | | |
|---|---|---|
| Ref | - | Diamond drillhole reference number |
| RL | - | Reference level, elevation |
| RQ | - | Rock quality index |
| ROCKNAME | - | MONZ - monzonite<br>ANDS - andesite<br>PLAG PRPH - Plagioclase Porphyry<br>SRCT SCHT - Sericite Schist<br>SILC SULPH STWK - Silicified Sulphide Stockwork<br>DCIT - Dacite<br>LPLL - Lapilli<br>XTAL - Crystal<br>SLST - Siltstone<br>LMND - Laminated<br>BREC - Brecciated |
| TXT | - | Texture<br>FG - fine grained<br>MG - medium grained<br>CG - coarse grained<br>SHRD - Sheared |

## ALTERATION (%)

| | | |
|---|---|---|
| SI | - | Pervasive silicification |
| QV | - | Quartz veining |
| SE | - | Sericite |
| CY | - | Clay |
| CH | - | Chlorite |
| EP | - | Epidote |
| CB | - | Carbonate |
| GM | - | Ankerite |
| A1 | - | Anhydrite |
| A2 | - | Alteration mineral 2 |
| IN | - | Total rock alteration intensity |

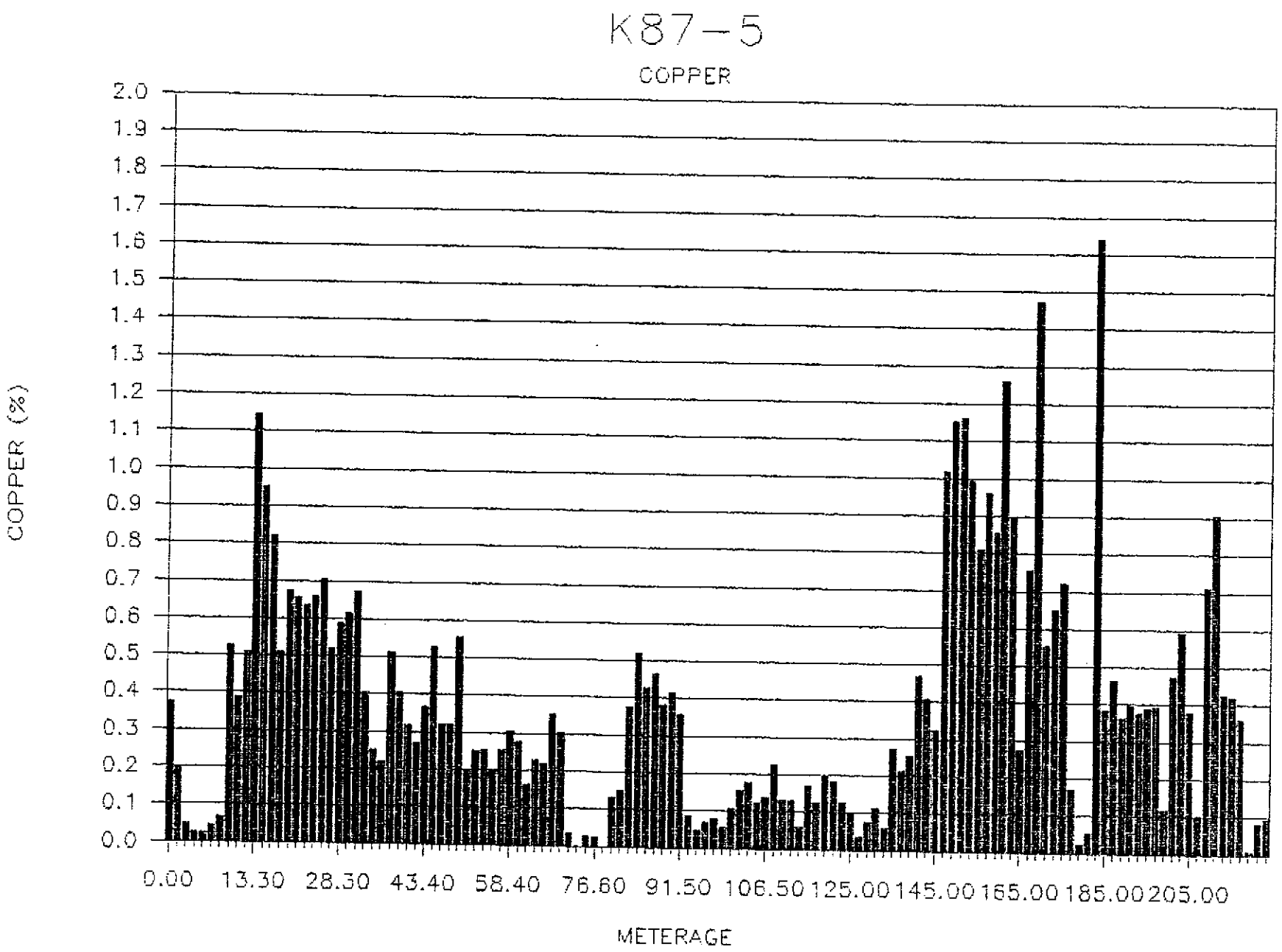
## MINERALIZATION (%)

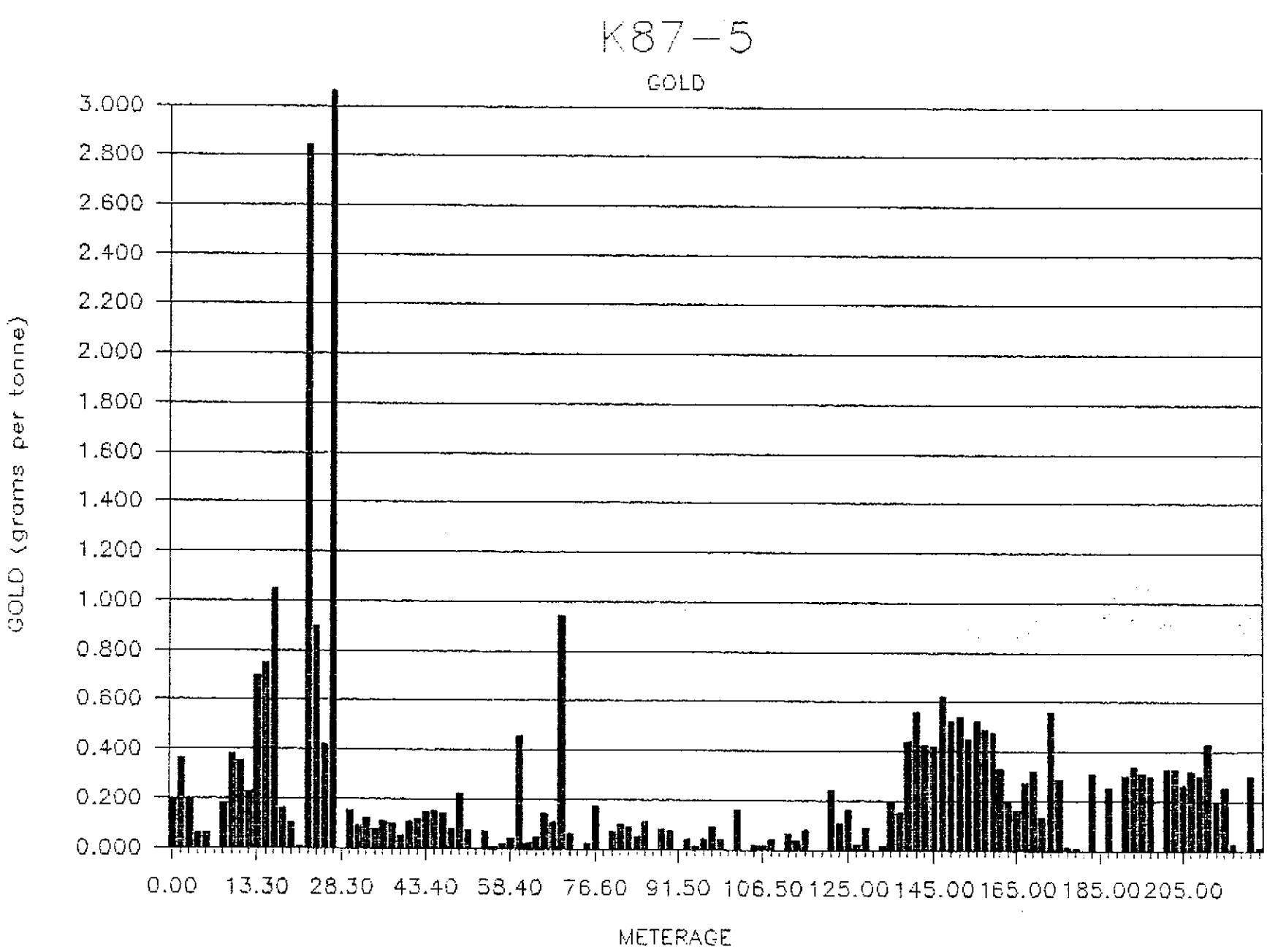
| | | |
|---|---|---|
| PY | - | Pyrite |
| CP | - | Chalcopyrite |
| SP | - | Tennantite |
| CC | - | Chalcocite |
| NC | - | Native copper |
| M1 | - | Bornite |
| M2 | - | Ore mineral 2 |

## GEOCHEMISTRY

| | | |
|---|---|---|
| Au | - | Gold assay in ppb |
| Au oz | - | Gold assay in ounces per ton |
| Ag | - | Silver assay in ppm |
| Ag oz | - | Silver assay in ounces per ton |
| Cu | - | Copper assay in ppm |
| Zn | - | Zinc assay in ppm |
| Fe% | - | Iron assay in percent |
| As | - | Arsenic assay in ppm |
| Mn | - | Manganese assay in ppm |

SECTION I
1987 HOLES


K87-5
COPPER
COPPER (%)
2.0
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
0.00
13.30
28.30
43.40
58.40
76.60
91.50
106.50
125.00
145.00
165.00
185.00
205.00
METERAGE


K87-5
GOLD
GOLD (grams per tonne)
3.000
2.800
2.600
2.400
2.200
2.000
1.800
1.600
1.400
1.200
1.000
0.800
0.600
0.400
0.200
0.000
0.00
13.30
28.30
43.40
58.40
76.60
91.50
106.50
125.00
145.00
165.00
185.00
205.00
METERAGE

PROJECT KERR PROJECT



D.D. HOLE No. K87-5

Depth 219.5 Dip -48° Azimuth

Location Zone B

Collar Lat. 9,742 N

Dep. 10,290 W

Hole Started 1 August 1987

Elev. 1,726

Hole Completed 8 August 1987

Azimuth 60°

Core Recovery As per attached sheets

Dip. -60°

Drilled By Advanced Drilling

Length 228.90

Logged by: John Kowalchuk

Objective: To test geochemical high, if highs and stratigraphy - zone B

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | Veinlets and foliation planes<br>Occasional lapilli and crystalline section<br>15% qtz along with Py in veinlets.<br>10.5m Py stringers (several 10-20/20cm section at 25/c.a.)<br>13.1 - qtz Py veins at 50-55° - Chl-qtz at (-45°)<br>14.2 - 40cm laminated tuff - pale green<br>14.6- broken rusty core for 50cm.<br>- fractures down core axis.<br>14.8- qtz-Py veins 35° to core axis<br>3-4 cm across - containing Py. | | | | | | | | | |
| 15.9 | 28.3 | Lapilli Tuff - Crystalline<br>Medium to coarse grained<br>First 2.0 metres quite chloritic becoming sericitic as you go down the hole.<br>Foliation of 45° shown by Py.<br>Fillings - 10-15% Py in zone.<br>top 70cm - contain about 5% epidote alteration.<br>Tr - 1% Cpy along fractures sub parallel to core axis.<br>16.3 - 1cm qtz Py vein 50° to core axis | 17287 | 16.3 | 17.8 | 1.5 | | 750 | 4.7 | 9491 | 761 |
| | | | 8 | 17.8 | 19.3 | 1.5 | | 1050 | 4.0 | 8209 | 557 |
| | | | 9 | 19.3 | 20.8 | 1.5 | | 160 | 2.0 | 5104 | 258 |
| | | | 17290 | 20.8 | 22.3 | 1.5 | | 100 | 2.6 | 6718 | 194 |
| | | | 1 | 22.3 | 23.8 | 1.5 | | 5 | 2.5 | 6582 | 308 |
| | | | 2 | 23.8 | 25.3 | 1.5 | | 2845 | 3.0 | 6338 | 498 |
| | | | 3 | 25.3 | 26.8 | 1.5 | | 900 | 3.5 | 6602 | 275 |
| | | | 4 | 26.8 | 28.3 | 1.5 | | 420 | 2.9 | 7032 | 234 |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0. | 1.02 | Overburden - Casing | | | | | | | | | |
| 1.02 | 2.29 | Fine Grained Tuff | 17276 | 1.02 | 2.3 | 1.21 | | 200 | 1.6 | 3732 | 371 |
| | | Chloritic | 7 | 2.3 | 3.8 | 1.5 | | 360 | 0.7 | 1980 | 279 |
| | | Dark green colour | 8 | 3.8 | 5.3 | 1.5 | | 200 | 0.1 | 469 | 341 |
| | | 2.20- Qt Py veins at 50° to core axis. | 9 | 5.3 | 6.8 | 1.5 | | 60 | 0.1 | 234 | 257 |
| | | 20% chlorite | 17280 | 6.8 | 8.3 | 1.5 | | 60 | 0.1 | 246 | 193 |
| | | 10% sulphides | 1 | 8.3 | 9.3 | 1.0 | | nd | 0.1 | 443 | 274 |
| | | Veins every 5cm. | 2 | 9.3 | 10.3 | 1.0 | | 180 | 0.4 | 638 | 264 |
| 2.29 | 10.8 | Lapilli Crystal Tuff - Sericitic<br>Pale green colour changing to green<br>- Med to coarse grained.<br>-30% sericite -5-10% chlorite.<br>5% carbonate as veinlets.<br>10-15% sulphides (Py) as fol. and veinlets<br>- mainly in sericitic parts.<br>4.3m - Py on fr. 60°.<br>6.3m - Py on fol. -55°<br>Sericitic zone better fol. at 55° cont. Py. | | | | | | | | | | |
| 10.8 | 15.9 | Ash Tuff - Fine Grained - Dark Green | 17283 | 10.3 | 11.8 | 1.5 | | 380 | 2.1 | 5261 | 440 |
| | | Coloured | 4 | 11.8 | 13.3 | 1.5 | | 350 | 1.5 | 3901 | 563 |
| | | Very chloritic | 5 | 13.3 | 14.8 | 1.5 | | 230 | 2.5 | 5089 | 1080 |
| | | 10-15% sulphides (Py) as fracture filled | 6 | 14.8 | 16.3 | 1.5 | | 700 | 5.4 | 11467 | 3029 |

HOLE NO. K87-5

PROPERTY Kerr Project

SHEET NO. 4 of 12

| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | Lapilli Tuff - grey- 20% Py tr other sulphides<br>approx 30 Py veinlets/m - each veinlet 2mm across.<br>22.4 - veinlets along fol. plane 30°/c.a.<br>23.62 - 1cm qtz Py vein 20°/core axis<br>25.0-27.0 - extensive vuggy qtz veining subparallel to core axis<br>Veins contain some Py and chlorite.<br>27.2 - qtz along fol. at 35°/ core axis | | | | | | | | | |
| 28.3 | 29.9 | Fault or Fracture Zone<br>Rusty and lapilli tuff - broken with qtz<br>Py veins along core axis<br>sericitic<br>up to 20% Py on fractures and fol. planes. | 17295 | 28.3 | 29.9 | 1.6 | | 4010 | 2.4 | 5192 | 219 |
| | | | 6 | 29.9 | 31.4 | 1.5 | | nd | 3.9 | 5887 | 535 |
| | | | 7 | 31.4 | 32.9 | 1.5 | | 150 | 3.6 | 6151 | 399 |
| | | | 8 | 32.9 | 34.4 | 1.5 | | 90 | 2.7 | 6735 | 467 |
| | | | 17299 | 34.4 | 35.9 | 1.5 | | 125 | 1.2 | 4061 | 465 |
| | | | 17300 | 35.9 | 37.4 | 1.5 | | 80 | 0.7 | 2498 | 206 |
| 29.9 | 44.5 | Lapilli Tuff<br>- med - coarse grained<br>Chloritic and sericitic - some epidote<br>-pale green colour<br>Pyrite and quartz along foliation planes 40° to core axis<br>30.5m - 3cm qtz vein 65° to core axis<br>32.2 - 5cm qtz-Py zone - 65° to core axis tr Cpy.<br>33.0- 5cm qtz-Py zone 45° to core axis<br>33.8 - qtz. | 1 | 37.4 | 38.9 | 1.5 | | 110 | 2.0 | 2186 | 1444 |
| | | | 2 | 38.9 | 40.4 | 1.5 | | 100 | 1.6 | 5142 | 354 |
| | | | 3 | 40.4 | 41.9 | 1.5 | | 50 | 1.0 | 4054 | 103 |
| | | | 4 | 41.9 | 43.4 | 1.5 | | 110 | 0.6 | 3184 | 146 |
| | | | 5 | 43.4 | 44.9 | 1.5 | | 120 | 0.8 | 2696 | 97 |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | Lapilli tuff<br>Medium - coarse grained<br>Pale green colour - slightly chloritic<br>35.4-35.8 - several slightly sericitic.<br>5cm massive Py beds 55°/ca<br>total interval 20% Py - tr Cpy.<br>- Generally 10-15% Py as veinlets/to fol.<br>38.4-38.7 - 2cm of calcite veining and flooding. 50° to ca some Py-Cpy with Chl.<br>41.4- qtz vein cutting 10° to core axis. | | | | | | | | | |
| 44.5 | 45.1 | Fault Zone- Lapilli Tuff<br>Rusty-sericitic very sheared<br>Shear directions 55°/core axis<br>Tr Py - bleached | 17306 | 44.9 | 46.4 | 1.5 | | 145 | 1.1 | 3653 | 1042 |
| | | | 7 | 46.4 | 47.9 | 1.5 | | 150 | 2.2 | 5299 | 3725 |
| | | | 8 | 47.9 | 49.4 | 1.5 | | 140 | 0.4 | 3198 | 273 |
| | | | 9 | 49.4 | 50.9 | 1.5 | | 80 | 0.5 | 3203 | 95 |
| | | | 17310 | 50.9 | 52.4 | 1.5 | | 220 | 1.4 | 5553 | 475 |
| 45.1 | 52.57 | Lapilli Tuff - Sericitic - 40% ser.<br>Broken- | 17311 | 52.4 | 53.9 | 1.5 | | 75 | 0.6 | 1965 | 85 |
| | | Light grey colour<br>contains 5-10% sulphides as pyrite.<br>49.0- 65° Py vein 2cm thick<br>foliation generally 55° | 17312 | 53.9 | 55.4 | 1.5 | | nd | 0.7 | 2514 | 88 |
| | | | 3 | 55.4 | 56.9 | 1.5 | | 70 | 0.8 | 2535 | 109 |
| | | | 4 | 56.9 | 58.4 | 1.5 | | 5 | 0.2 | 2008 | 30 |
| | | | 5 | 58.4 | 59.9 | 1.5 | | 15 | 0.4 | 2556 | 130 |
| | | | 6 | 59.9 | 61.4 | 1.5 | | 40 | 1.3 | 3056 | 372 |
| 52.57 | 69.60 | Lapilli Tuff<br>Grey to green in colour<br>coarse to fine grained<br>chloritic- sericitic<br>Py varies from 5-15% - with chloritic section up to 15% | 7 | 61.4 | 62.9 | 1.5 | | 460 | 1.2 | 2763 | 3309 |
| | | | 8 | 62.9 | 64.4 | 1.5 | | 20 | 0.4 | 1628 | 202 |
| | | | 9 | 64.4 | 65.9 | 1.5 | | 45 | 0.3 | 2289 | 122 |
| | | | 17320 | 65.9 | 67.4 | 1.5 | | 140 | 0.5 | 2176 | 177 |
| | | | 1 | 67.4 | 68.9 | 1.5 | | 110 | 1.0 | 3538 | 873 |
| | | | 2 | 68.9 | 69.6 | 0.7 | | 940 | 0.9 | 3010 | 569 |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | sulphides occur primarily along fol. planes.<br>Trace of calcite in some qtz veins.<br>53.5 - Py vein 40° to c.a.<br>54.7 - fol. 45° to core axis.<br>55 - 58.5 - sericitic section - grey colour<br>56.8 - fol. 40° to core axis.<br>59.0 - more chloritic<br>15% sulphide both disseminated and along fol. planes.<br>61.0 - Py along fol. 35° core axis<br>64.0 - fol. 30° to core axis.<br>62.52 - 69.60 extensive chlorite alteration very fine grained thermally altered by dyke.<br>Some green clay mineral.<br>Contact with dyke - 40° | | | | | | | | | |
| 69.60 | 81.1 | Monzonite Dyke - medium grained-equigranular<br>qtz-plag. amphibole rock<br>pale green grey colour<br>5-10 at 55° 0.5cm qtz calcite veins every metre.<br>- some chlorite in veins along same trend<br>Rust covered fractures.<br>Tr. of Py on fractures | 17323 | 69.6 | 71.2 | 1.6 | | 60 | 0.1 | 322 | 517 |
| | | | 17324 | 76.6 | 77.6 | 1.0 | | 20 | 0.1 | 285 | 408 |
| | | | 5 | 77.6 | 79.7 | 2.1 | | 170 | 0.1 | 221 | 212 |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | slight chlorite alteration. otherwise quite fresh looking. 76.6-79.0 - very block containing rust covered fractures - vuggy qtz. Fractures of 20° to core axis. 77.7-79.7 - bleached zone - silicified - 1-2% sulphides Py and Cpy. bottom contact 80° to core axis | | | | | | | | | |
| 81.1 | 96.0 | Lapilli Tuff - Chloritic | 17326 | 81.0 | 82.5 | 1.5 | | 70 | 0.1 | 1309 | 1333 |
| | | fine grained near dyke contact | 7 | 82.5 | 84.0 | 1.5 | | 100 | 0.1 | 1526 | 422 |
| | | 5-15% sulphides primarily as Py | 8 | 84.0 | 85.5 | 1.5 | | 90 | 0.7 | 3766 | 229 |
| | | up to 2% Cpy in narrow sections | 9 | 85.5 | 87.0 | 1.5 | | 50 | 0.8 | 5190 | 221 |
| | | Tr to 1% Cpy throughout. | 17330 | 87.0 | 88.5 | 1.5 | | 110 | 0.7 | 4285 | 250 |
| | | Massive - very weak foliation. | 1 | 88.5 | 90.0 | 1.5 | | nd | 0.9 | 4650 | 279 |
| | | 81.4-82.0 - several qtz-carb veinlets at | 2 | 90.0 | 91.5 | 1.5 | | 80 | 0.7 | 3829 | 196 |
| | | 75° to core axis. | 3 | 91.5 | 93.0 | 1.5 | | 75 | 0.7 | 4134 | 296 |
| | | Bottom 15cm - pale green and bleached | 4 | 93.0 | 94.5 | 1.5 | | nd | 0.6 | 3578 | 259 |
| | | Sulphides disseminated and in fractures | 5 | 94.5 | 96.0 | 1.5 | | 40 | 0.1 | 853 | 85 |
| | | also as pods. 94.80- fol. 50 shown by Py on plane | | | | | | | | | |
| 96.0 | 97.4 | Fine Grained Tuff - Very Chloritic | 17336 | 96.0 | 97.4 | 1.4 | | 10 | 0.1 | 453 | 353 |
| | | dark green colour | | | | | | | | | |
| | | -calcareous - contains carbonate spots throughout. | | | | | | | | | |
| | | upper contact 30° to core axis | | | | | | | | | |
| | | lower contact 40° to core axis | | | | | | | | | |
| | | Unit is calcareous - may be skarnified | | | | | | | | | |
| | | no apparent sulphides. | | | | | | | | | |

HOLE NO. K87-5

PROPERTY Kerr Project

SHEET NO. 8 of 12

| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 97.4 | 99.20 | Lapilli Tuff - Sericitic | 17337 | 97.4 | 99.0 | 1.6 | | 40 | 0.1 | 678 | 135 |
| | | - medium to coarse grained | 8 | 99.0 | 100.5 | 1.5 | | 90 | 0.1 | 777 | 67 |
| | | - well fol. sericite schist | 9 | 100.5 | 102.0 | 1.5 | | 40 | 0.1 | 561 | 71 |
| | | - approx 5% sulphides - all Py | 17340 | 102.0 | 103.5 | 1.5 | | nd | 0.1 | 1062 | 363 |
| | | 100.3-100.8 - qtz-carb vein- 70° to core | 1 | 103.5 | 105.0 | 1.5 | | 160 | 0.1 | 1539 | 132 |
| | | axis | 2 | 105.0 | 106.5 | 1.5 | | nd | 0.1 | 1778 | 315 |
| | | vein carries no apparent sulphides. | 3 | 106.5 | 108 | 1.5 | | 15 | 0.1 | 1243 | 53 |
| | | 101.0- fol. 60° to core axis | 16344 | 108.0 | 109.5 | 1.5 | | 15 | 0.1 | 1346 | 124 |
| | | 108.3 - fol. 50° to core axis | 5 | 109.5 | 111.0 | 1.5 | | 40 | 0.1 | 2263 | 126 |
| | | 111.6 - fol. 50° to core axis | 6 | 111.0 | 113.0 | 2.0 | | nd | 0.1 | 1276 | 169 |
| | | | 7 | 113.0 | 115.0 | 2.0 | | 65 | 0.2 | 1307 | 328 |
| 99.2 | 142.5 | Lapilli Tuff - Sericitic | 8 | 115.0 | 117.0 | 2.0 | | 35 | 0.4 | 587 | 786 |
| | | Some laminated tuff at 119.0 | 9 | 117.0 | 119.0 | 2.0 | | 80 | 0.3 | 1721 | 119 |
| | | lam. at 119.0 -65° | 17350 | 119.0 | 121.0 | 2.0 | | nd | 0.1 | 1253 | 115 |
| | | grey colour - sericite up to 50% | 1 | 121.0 | 123.0 | 2.0 | | nd | 1.6 | 1981 | 485 |
| | | 121.0-slightly broken bull qtz vein 25% | 2 | 123.0 | 125.0 | 2.0 | | 245 | 4.0 | 1845 | 77 |
| | | c.a. | 3 | 125.0 | 127.0 | 2.0 | | 110 | 0.7 | 1268 | 123 |
| | | Py decreases to 2-4% | 4 | 127.0 | 129.0 | 2.0 | | 160 | 0.8 | 1002 | 138 |
| | | 123.0-126.0- ground core | 5 | 129.0 | 131.0 | 2.0 | | 20 | 0.1 | 324 | 162 |
| | | very sheared | 6 | 131.0 | 133.0 | 2.0 | | 90 | 1.1 | 743 | 197 |
| | | fol. 11 to core axis | 7 | 133.0 | 135.0 | 2.0 | | nd | 2.6 | 1140 | 188 |
| | | 128.3 - fol. 60° to core axis | 8 | 135.0 | 137.0 | 2.0 | | 15 | 0.2 | 592 | 571 |
| | | 133.5 - fol. 60° to core axis | 9 | 137.0 | 139.0 | 2.0 | | 200 | 11.3 | 2692 | 1013 |
| | | 138.0 - fol. 55° to core axis | 17360 | 139.0 | 141.0 | 2.0 | | 150 | 1.7 | 2136 | 136 |
| | | 143.0 - Py vein 60° to core axis. | 1 | 141.0 | 143.0 | 2.0 | | 440 | 4.2 | 2551 | 257 |
| | | 146.8 - Py vein along fol. 65° to core axis | | | | | | | | | |
| | | 138-141.5 - very broken core | | | | | | | | | |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 142.5 | 165.3 | 142.5 - Py increases to 20% - less sericitic. | 17462 | 143.0 | 145.0 | 2.0 | | 560 | 2.8 | 4676 | 193 |
| | | - slightly more chloritic - Tr Cpy. | 3 | 145.0 | 147.0 | 2.0 | | 425 | 4.3 | 4083 | 216 |
| | | becoming coarse grained | 4 | 147.0 | 149.0 | 2.0 | | 420 | 2.4 | 3254 | 380 |
| | | Crystalline - Lapilli tuff | 5 | 149.0 | 151.0 | 2.0 | | 620 | 3.9 | 10167 | 618 |
| | | 156.0 - fol. 50° | 6 | 151.0 | 153.0 | 2.0 | | 520 | 3.8 | 11513 | 535 |
| | | 158.0 - broken core | 7 | 153.0 | 155.0 | 2.0 | | 540 | 3.9 | 11617 | 1367 |
| | | 165. - fol. 65°. | 8 | 155.0 | 157.0 | 2.0 | | 450 | 5.9 | 9937 | 612 |
| | | | 9 | 157.0 | 159.0 | 2.0 | | 520 | 2.6 | 8105 | 568 |
| | | | 17370 | 159.0 | 161.0 | 2.0 | | 485 | 1.6 | 9599 | 302 |
| 165.3 | 171.4 | Sheared - Lapilli Tuff - Less Crystalline | 1 | 161.0 | 163.0 | 2.0 | | 470 | 1.8 | 8561 | 525 |
| | | Very sericitic some chlorite | 17372 | 163.0 | 165.0 | 2.0 | | 330 | 3.5 | 12609 | 456 |
| | | coarse grained - slightly less Py -5% | 17373 | 165.0 | 167.0 | 2.0 | | 195 | 2.7 | 8984 | 348 |
| | | very soft core. | 4 | 167.0 | 169.0 | 2.0 | | 160 | 1.6 | 2739 | 221 |
| | | 170.8 - fol. 60°/ core axis | 5 | 169.0 | 171.0 | 2.0 | | 270 | 2.4 | 7576 | 525 |
| 171.4 | 174.2 | Well Fol. Crystal Lapilli Tuff | 17376 | 171.0 | 173.0 | 2.0 | | 320 | 4.4 | 14704 | 789 |
| | | Sericitized - grey colour | 7 | 173.0 | 175.0 | 2.0 | | 130 | 2.0 | 5534 | 545 |
| | | fol. 45° to core axis | | | | | | | | | |
| | | slightly more competent than previous lapilli Tuff | | | | | | | | | |
| | | 5% sulphides (Py) | | | | | | | | | |
| 174.2 | 178.3 | crystal Lapilli Tuff | 17378 | 175.0 | 177.0 | 2.0 | | 560 | 7.1 | 6516 | 687 |
| | | sheared and broken | 9 | 177.0 | 179.0 | 2.0 | | 285 | 3.0 | 7217 | 499 |
| | | Sericitic (40% ser) 10% chlorite | | | | | | | | | |
| | | fine to coarse grained | | | | | | | | | |
| | | Fol. 45° to core axis | | | | | | | | | |
| | | Bottom 1.5 metres very chloritic to contact with dyke. | | | | | | | | | |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 178.3 | 185.2 | Feldspar Porphyry Dyke - medium grained<br>Contact with tuff 50°<br>no sulphides<br>very chloritic top 1.5 metres green<br>very strong foliation 60° to core axis<br>several qtz-carb veins 1cm thick -35° to core axis<br>feldspars saussuritized - euhedral<br>1.5 metres - quite chlorite -green<br>Central portion of dyke slightly purple<br>180.44 - rusty qtz carb veining broken<br>185.0-185.25 - qtz vein along contact<br>rusty - vuggy | 17380 | 179.0 | 181.0 | 2.0 | | 10 | 0.1 | 1706 | 232 |
| | | | 1 | 181.0 | 183.0 | 2.0 | | 5 | 0.1 | 229 | 138 |
| | | | 2 | 183.0 | 185.0 | 2.0 | | nd | 0.1 | 518 | 259 |
| 185.0 | 212.0 | Crystal Lapilli Tuff<br>very sericitic - 40-50% sericite<br>quite sheared in places with even more sericite.<br>up to 55 Py along fol. planes.<br>185.4 - fol. 35° to core axis<br>186-189.28 - very contorted and sheared<br>fol.varies from 11 to 70° to core axis.<br>190.8 - 191.22 - sheared core fol. contorted.<br>191.8 - Fol. - 60° to core axis<br>194.5 - fol. -60° to core axis<br>198.9 - fol. -60° to core axis<br>201.1-203.2 - sheared and contorted very sericitic. | 17383 | 185.0 | 187.0 | 2.0 | | 310 | 0.6 | 16430 | 166 |
| | | | 4 | 187.0 | 189.0 | 2.0 | | nd | 0.3 | 3826 | 53 |
| | | | 5 | 189.0 | 191.0 | 2.0 | | 250 | 0.6 | 4627 | 117 |
| | | | 6 | 191.0 | 193.0 | 2.0 | | nd | 0.5 | 3616 | 100 |
| | | | 7 | 193.0 | 195.0 | 2.0 | | 300 | 0.7 | 3939 | 89 |
| | | | 8 | 195.0 | 197.0 | 2.0 | | 340 | 0.5 | 3750 | 99 |
| | | | 9 | 197.0 | 199.0 | 2.0 | | 310 | 0.6 | 3893 | 250 |
| | | | 17390 | 199.0 | 201.0 | 2.0 | | 300 | 0.3 | 3905 | 84 |
| | | | 1 | 201.0 | 203.0 | 2.0 | | nd | 0.1 | 1156 | 160 |
| | | | 2 | 203.0 | 205.0 | 2.0 | | 330 | 1.1 | 4744 | 33 |
| | | | 3 | 205.0 | 207.0 | 2.0 | | 330 | 1.2 | 5936 | 38 |
| | | | 4 | 207.0 | 209.0 | 2.0 | | 260 | 1.1 | 3784 | 161 |
| | | | 5 | 209.0 | 211.0 | 2.0 | | 320 | 0.2 | 998 | 175 |
| | | | 6 | 211.0 | 213.0 | 2.0 | | 300 | 1.0 | 7110 | 162 |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | 203.7-205 - sheared and contorted - very sericitic flood. varies from 60° to 0". 207m - fol. 55° to core axis. 210m - fol. 70° to core axis 2-5% Py dissem along fol. planes bottom 1 metre - 5-10% chloritic alt. 211.25-21153 - (possible dyke) dark green andesitic Very chloritic Contact 60° to core axis | | | | | | | | | |
| 212.0 | 227.7 | Lapilli Tuff sericitic - crystalline in places sheared in places 2-5% Py. 212=219.8 - sheared and broken core very contorted foliation varies from 60° to 0° Minor chlorite alteration 50% sericite. 221.3-224.5 - very chloritic slight increase in pyrite - tr Cpy 222.7 - fol. - 60° to core axis 224.5 - sericitic to end of lapilli tuff section. | 17397 | 213.0 | 215.0 | 2.0 | | 430 | 1.7 | 9071 | 44 |
| | | | 8 | 215.0 | 220.0 | 5.0 | | 200 | 1.1 | 4254 | 56 |
| | | | 9 | 220.0 | 222.0 | 2.0 | | 250 | 1.2 | 4190 | 151 |
| | | | 17400 | 222.0 | 224.0 | 2.0 | | 28 | 0.3 | 3580 | 60 |
| | | | 1 | 224.0 | 226.0 | 2.0 | | nd | 1.2 | 78 | 1454 |
| | | | 2 | 226.0 | 227.7 | 1.7 | | 300 | 2.9 | 827 | 884 |
| | | | 3 | 227.7 | 228.9 | 1.2 | | 10 | 3.7 | 960 | 381 |

HOLE NO. K87-5

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | SAMPLING From | SAMPLING To | SAMPLING m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 227.7 | 228.9 | Fine Grained Ash Tuff<br>Dark green colour<br>massive<br>fol. 55°<br>5% Py and tr Cpy | | | | | | | | | |
| | 228.9 | ----------End of Hole---------- | | | | | | | | | |

## Core Recovery K87-5

| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY |
|---|---|---|---|---|
| 0 | 2.29 | 2.29 | 1.27 | 55 |
| 2.29 | 3.05 | .76 | .35 | 46 |
| 3.05 | 3.96 | .91 | .63 | 69 |
| 3.96 | 4.57 | .61 | 1.11 | 182 |
| 4.57 | 5.49 | .92 | .73 | 79 |
| 5.49 | 6.71 | 1.22 | 1.14 | 93 |
| 6.71 | 8.08 | 1.37 | 1.73 | 126 |
| 8.08 | 9.30 | 1.22 | .76 | 62 |
| 9.30 | 11.28 | 1.98 | 2.19 | 111 |
| 11.28 | 12.95 | 1.67 | 1.55 | 93 |
| 12.95 | 15.85 | 2.90 | 2.94 | 101 |
| 15.85 | 16.76 | .91 | 1.24 | 136 |
| 16.76 | 18.29 | 1.53 | 1.48 | 97 |
| 18.29 | 20.12 | 1.83 | 1.72 | 94 |
| 20.12 | 21.49 | 1.37 | 1.31 | 96 |
| 21.49 | 23.62 | 2.13 | 2.20 | 103 |
| 23.62 | 25.60 | 1.98 | 1.87 | 94 |
| 25.60 | 28.04 | 2.44 | 2.45 | 100 |
| 28.04 | 30.48 | 2.4 | 2.41 | 99 |
| 30.48 | 32.31 | 1.83 | 1.75 | 96 |
| 32.31 | 34.90 | 2.59 | 2.69 | 103 |
| 34.90 | 37.64 | 2.74 | 2.52 | 92 |
| 37.64 | 38.40 | .76 | .80 | 105 |
| 38.40 | 41.45 | 3.05 | 2.94 | 96 |
| 41.45 | 44.5 | 3.05 | 2.77 | 91 |
| 44.5 | 45.11 | .61 | .69 | 113 |
| 45.11 | 46.32 | 1.21 | 1.0 | 83 |
| 46.32 | 47.54 | 1.22 | 1.08 | 89 |
| 47.54 | 48.00 | .46 | .66 | 143 |
| 48.0 | 49.07 | 1.07 | .92 | 86 |
| 49.07 | 49.68 | .61 | .71 | 116 |
| 49.68 | 50.90 | 1.22 | .99 | 81 |
| 50.90 | 51.51 | .61 | .54 | 89 |
| 51.51 | 52.57 | 1.06 | 1.10 | 4 |
| 52.57 | 54.86 | 2.29 | 2.30 | 100 |

## Core Recovery K87-5

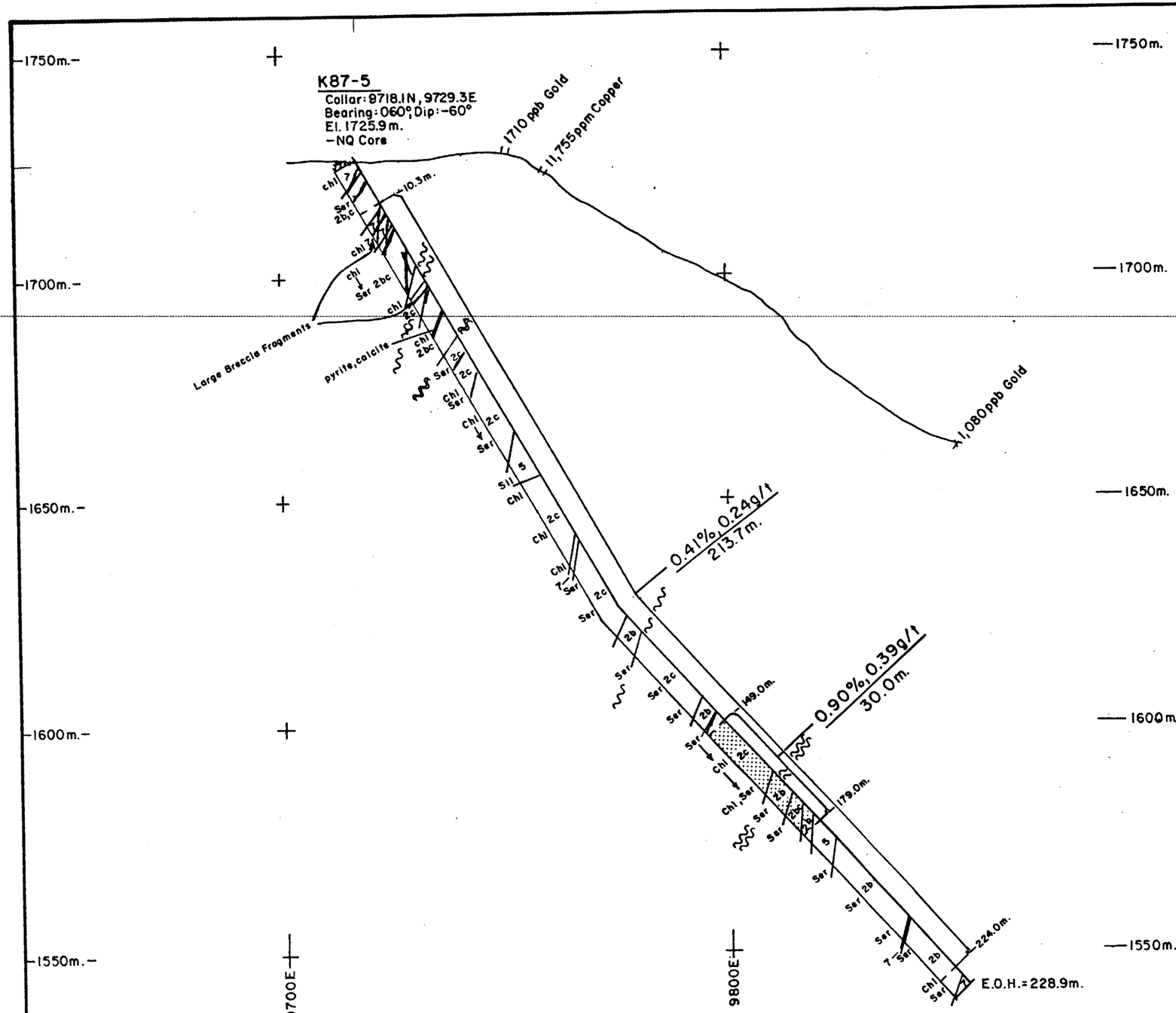
| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY |
|---|---|---|---|---|
| 56.69 | 59.59 | 2.90 | 2.77 | 96 |
| 59.59 | 62.63 | 3.04 | 3.20 | 105 |
| 62.63 | 64.31 | .68 | 1.66 | 99 |
| 64.31 | 67.06 | 2.75 | 2.80 | 102 |
| 67.06 | 67.97 | .91 | 1.16 | 127 |
| 67.97 | 68.88 | .91 | .97 | 107 |
| 68.88 | 71.32 | 2.44 | 2.41 | 99 |
| 71.32 | 74.07 | 2.75 | 2.73 | 99 |
| 74.07 | 75.29 | 1.22 | 1.05 | 86 |
| 75.29 | 76.05 | .76 | .62 | 82 |
| 76.05 | 77.42 | 1.37 | 1.40 | 102 |
| 77.42 | 79.55 | 2.13 | 1.90 | 89 |
| 79.55 | 80.47 | .92 | .96 | 104 |
| 80.47 | 81.08 | .61 | .66 | 108 |
| 81.08 | 83.06 | 2.02 | 1.78 | 88 |
| 83.06 | 84.12 | 1.06 | .95 | 90 |
| 84.12 | 87.17 | 3.05 | 3.05 | 100 |
| 87.17 | 89.76 | 2.59 | 2.59 | 100 |
| 89.76 | 90.68 | .92 | .92 | 100 |
| 90.68 | 93.27 | 2.59 | 2.54 | 98 |
| 93.27 | 94.64 | 1.37 | 1.37 | 100 |
| 94.64 | 96.62 | 1.98 | 1.87 | 94 |
| 96.62 | 98.60 | 1.98 | 1.85 | 93 |
| 98.60 | 101.50 | 2.90 | 2.73 | 94 |
| 101.5 | 103.02 | 1.52 | 1.38 | 91 |
| 103.02 | 104.24 | 1.22 | 1.15 | 94 |
| 104.24 | 106.07 | 1.83 | 1.54 | 84 |
| 106.07 | 108.36 | 2.29 | 2.29 | 100 |
| 108.36 | 111.56 | 3.20 | 3.03 | 95 |
| 111.56 | 114.60 | 3.04 | 3.04 | 100 |
| 114.60 | 117.60 | 3.05 | 2.80 | 92 |
| 117.60 | 118.87 | 1.22 | .87 | 71 |
| 118.87 | 119.79 | .92 | .80 | 71 |
| 119.79 | 119.94 | .15 | .14 | 93 |
| 119.94 | 121.46 | 1.52 | 1.44 | 95 |

## Core Recovery K87-5

| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY |
|---|---|---|---|---|
| 121.46 | 123.44 | 1.98 | 1.72 | 87 |
| 123.44 | 124.82 | 1.38 | 1.19 | 86 |
| 124.82 | 125.27 | .45 | .49 | 109 |
| 125.27 | 126.19 | .92 | 1.06 | 115 |
| 126.19 | 127.25 | 1.06 | .90 | 85 |
| 127.25 | 128.32 | 1.07 | .74 | 69 |
| 128.32 | 129.08 | .76 | .51 | 67 |
| 129.08 | 130.61 | 1.53 | 1.73 | 113 |
| 130.61 | 131.82 | 1.21 | 1.22 | 101 |
| 131.82 | 132.89 | 1.07 | 1.03 | 96 |
| 132.89 | 134.26 | 1.37 | 1.44 | 105 |
| 134.26 | 135.64 | 1.38 | 1.32 | 96 |
| 135.64 | 136.25 | .61 | .52 | 85 |
| 136.25 | 137.01 | .76 | .56 | 74 |
| 137.01 | 138.68 | 1.67 | 1.53 | 92 |
| 138.68 | 139.45 | .77 | .26 | 34 |
| 139.45 | 140.21 | .76 | .45 | 59 |
| 140.21 | 141.27 | 1.06 | .93 | 87 |
| 141.27 | 142.30 | 1.03 | 1.03 | 100 |
| 142.30 | 143.26 | .96 | .91 | 95 |
| 143.26 | 146.30 | 3.04 | 2.98 | 98 |
| 146.30 | 148.14 | 1.84 | 1.66 | 90 |
| 148.14 | 149.35 | 1.22 | 1.33 | 109 |
| 149.35 | 152.10 | 2.75 | 2.33 | 85 |
| 152.10 | 153.62 | 1.52 | 1.64 | 108 |
| 153.62 | 156.67 | 3.05 | 2.98 | 98 |
| 156.67 | 157.28 | .61 | .74 | 121 |
| 157.28 | 159.11 | 1.83 | 1.41 | 77 |
| 159.11 | 160.63 | 1.52 | 1.50 | 99 |
| 160.63 | 163.37 | 2.74 | 2.35 | 86 |
| 163.37 | 164.90 | 1.53 | 1.28 | 84 |
| 164.90 | 166.42 | 1.52 | .73 | 48 |
| 166.42 | 167.64 | 1.22 | .70 | 57 |
| 167.64 | 170.69 | 3.05 | 1.23 | 40 |
| 170.69 | 173.43 | 2.74 | 1.98 | 72 |

## Core Recovery K87-5

| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY | |
|---|---|---|---|---|---|
| 173.43 | 174.65 | 1.22 | .92 | 75 | |
| 174.65 | 175.56 | .91 | .22 | 24 | |
| 175.56 | 177.09 | 1.53 | .90 | 59 | |
| 177.09 | 178.16 | 1.07 | .65 | 61 | |
| 178.16 | 180.44 | 2.28 | 2.23 | 98 | |
| 180.44 | 181.66 | 1.22 | 1.18 | 97 | |
| 181.66 | 184.71 | 3.05 | 2.88 | 94 | |
| 184.71 | 187.76 | 3.05 | 1.23 | 40 | |
| 187.76 | 189.28 | 1.52 | .53 | 35 | |
| 189.28 | 190.35 | 1.07 | .87 | 81 | |
| 190.35 | 191.26 | .91 | .69 | 76 | |
| 191.26 | 191.72 | .46 | .37 | 80 | |
| 191.72 | 193.85 | 2.13 | 1.78 | 84 | |
| 193.85 | 196.90 | 3.05 | 2.46 | 81 | |
| 196.90 | 198.88 | .98 | 1.88 | 95 | |
| 198.88 | 201.02 | 2.14 | 1.88 | 88 | |
| 201.02 | 202.54 | 1.52 | 1.29 | 85 | |
| 202.54 | 203.15 | .61 | .30 | 49 | |
| 203.15 | 203.76 | .61 | .58 | 95 | |
| 203.76 | 205.13 | 1.37 | .88 | 64 | |
| 205.13 | 206.65 | 1.52 | .88 | 58 | |
| 206.65 | 208.94 | 2.29 | 1.69 | 74 | |
| 208.94 | 211.53 | 2.59 | 2.12 | 82 | |
| 211.53 | 212.90 | 1.37 | .67 | 49 | |
| 212.90 | 215.79 | 2.89 | .73 | 25 | |
| 215.79 | 219.71 | 3.92 | .19 | 5 | lost core |
| 219.71 | 221.28 | 1.57 | 1.55 | 99 | |
| 221.28 | 224.33 | 3.05 | 2.54 | 83 | |
| 224.33 | 225.55 | 1.22 | 1.16 | 95 | |
| 225.55 | 227.68 | 2.13 | .76 | 37 | |
| 227.68 | 228.44 | .76 | .66 | 87 | |
| 228.44 | 228.90 | .46 | .24 | 52 | |




## LEGEND

Fault

0.13%, 113g/t / 10.3m. — %Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Interval defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE – fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a)/MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST – foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) – interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE – interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

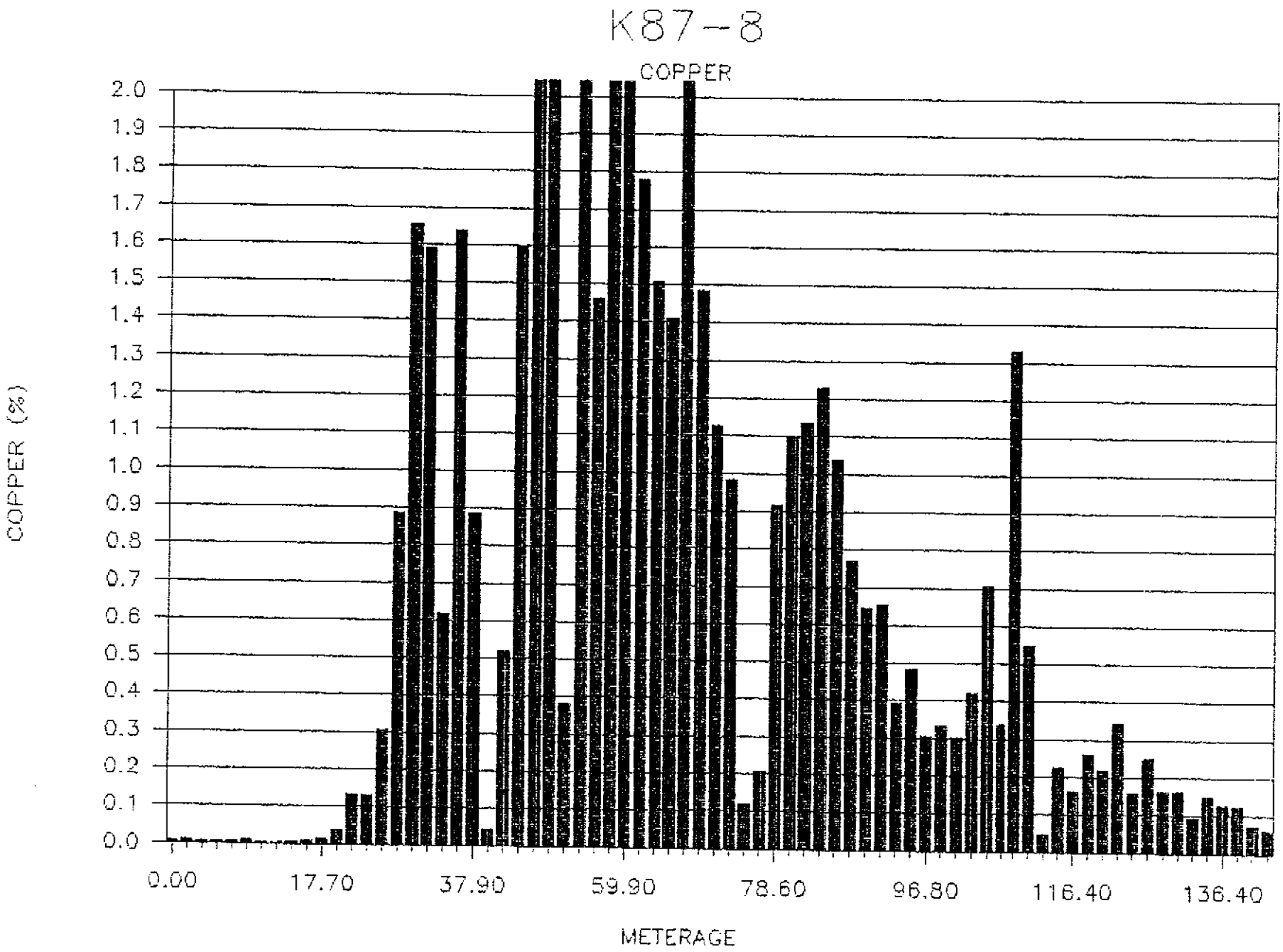
Chl chlorite
Ser sericite
quartz/pyrite veins or fracture filling

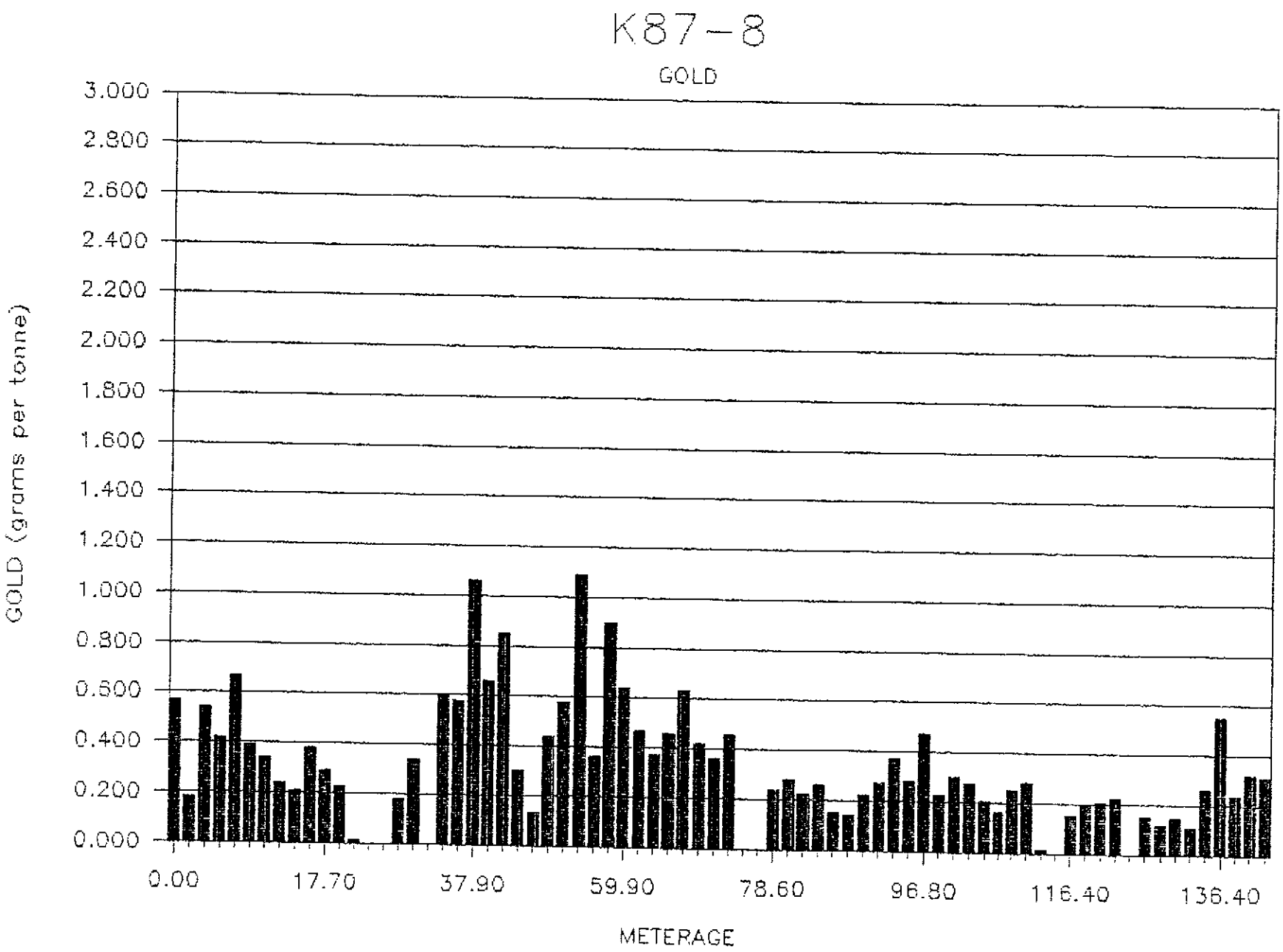
1:1000
SCALE 0 10 20 30 40 Metres

# SULPHURETS GOLD
CORPORATION
1989 KERR PROJECT

SECTION 9718N
DDH K87-5

Report No. 1065 Figure No.


K87-8
COPPER
COPPER (%)
2.0
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
0.00
17.70
37.90
59.90
78.60
96.80
116.40
136.40
METERAGE


K87-8
GOLD
GOLD (grams per tonne)
3.000
2.800
2.600
2.400
2.200
2.000
1.800
1.600
1.400
1.200
1.000
0.800
0.600
0.400
0.200
0.000
0.00
17.70
37.90
59.90
78.60
96.80
116.40
136.40
METERAGE

PROJECT KERR PROJECT



D.D. HOLE No. K87-8

Depth 147.22m Dip -60° Azimuth

Location Zone B

Collar Lat. 9,686 N

Dep. 10,166 W

Hole Started 23 August 1987

Elev. 1,638.5

Hole Completed 28 August 1987

Azimuth 90°

Core Recovery As per attached sheets

Dip. 58°

Drilled By Advanced Drilling

Length 147.22

Logged by: J.M. Kowalchuk

Objective: Test Ip anomaly - charge high - resist low

HOLE NO. K87-8

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 0. | 2.73 | Overburden - Casing | | | | | | | | | |
| 2.73 | 24.4 | Crystal Tuff - Very sericitic - 50-60% sericite | 3556 | 2.7 | 3.7 | 1.0 | | 570 | 2.6 | 51 | 13 |
| | | Very strong shear foliation - original textures largely destroyed - schistose. | 7 | 3.7 | 4.7 | 1.0 | | 180 | 2.2 | 70 | 14 |
| | | 0-7.5 - Mostly qtz veins material-silicified | 8 | 4.7 | 6.7 | 2.0 | | 540 | 1.1 | 41 | 9 |
| | | 50% quartz veining. | 9 | 6.7 | 7.7 | 1.0 | | 420 | 1.6 | 52 | 17 |
| | | Tr-5% pyrite along shear planes | 3560 | 7.7 | 9.7 | 2.0 | | 670 | 0.7 | 35 | 6 |
| | | Rock quite broken with most of schist material removed. | 1 | 9.7 | 11.7 | 2.0 | | 390 | 0.2 | 67 | 6 |
| | | A green clay material in among all the quartz | 2 | 11.7 | 13.7 | 2.0 | | 340 | 0.1 | 27 | 5 |
| | | Qtz veins are at 60% to core axis | 3 | 13.7 | 15.7 | 2.0 | | 240 | 0.1 | 11 | 8 |
| | | Rock very sheared and broken | 4 | 15.7 | 17.7 | 2.0 | | 210 | 5.5 | 44 | 9 |
| | | 9.4-10.36 - Ground core. | 5 | 17.7 | 19.7 | 2.0 | | 380 | 0.8 | 82 | 11 |
| | | 11.8-24.4 - Fault zone - Ground and sheared core. | 6 | 19.7 | 21.7 | 2.0 | | 290 | 2.1 | 137 | 10 |
| | | 21.5 - Shear foliation 40° to core axis | 7 | 21.7 | 24.4 | 2.7 | | 230 | 0.5 | 374 | 24 |
| | | Qtz vein material and possibly lapilli oriented along shear foliation | | | | | | | | | |
| 24.4 | 29.9 | Feldspar Porphyry Dyke - | 3568 | 24.4 | 26.4 | 2.0 | | 10 | 0.1 | 1313 | 195 |
| | | Green - medium grain size - chloritic | 9 | 26.4 | 28.4 | 2.0 | | nd | 0.1 | 1287 | 217 |
| | | Porphyritic with large feldspar phenocrysts up to 1cm across - feldspars are orthoclase? | 3570 | 28.4 | 29.9 | 1.5 | | nd | 0.1 | 3059 | 309 |

HOLE NO. K87-8

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | Upper contact of dyke is 30° to core axis at 27.0 - Foliation is 50° to core axis<br>Several fractures 5mm-5cm across<br>Cut rock at 15-20° to core axis contain qtz & Py.<br>Feldspar phenocrysts and groundmass oriented along foliation planes.<br>near qtz veins dyke rock is bleached white.<br>This unit is blocky but not as sheared and ground up like above sericite-quartz schist<br>Bottom contact no clear. | | | | | | | | | |
| 29.9 | 57.9 | Fault Zone - Crystal or Lapilli Tuff | 3571 | 29.9 | 31.9 | 2.0 | | 180 | 0.1 | 8840 | 442 |
| | | All volcanic textures gone | 2 | 31.9 | 33.9 | 2.0 | | 340 | 1.8 | 16525 | 89 |
| | | Now a qtz-sericite pyrite rock | 3573 | 33.9 | 35.9 | 2.0 | | nd | 1.1 | 15884 | 81 |
| | | 40% ser. - 30% qtz - 20% Py. | 4 | 35.9 | 37.9 | 2.0 | | 600 | 8.1 | 6182 | 55 |
| | | 10% chl in places. | 5 | 37.9 | 39.9 | 2.0 | | 580 | 1.4 | 16387 | 31 |
| | | Rock completely grounded up by faulting. | 6 | 39.9 | 41.9 | 2.0 | | 1060 | 1.1 | 8871 | 13 |
| | | With in many places just qtz remaining | 7 | 41.9 | 44.9 | 3.0 | | 660 | 1.1 | 425 | 10 |
| | | Significant part of sericite gone to clay | 8 | 44.9 | 46.9 | 2.0 | | 850 | 3.5 | 5194 | 23 |
| | | 40% of pyrite main sulphide some Cpy. | 9 | 46.9 | 48.9 | 2.0 | | 300 | 0.5 | 15975 | 41 |
| | | Cpy increases with depth - may be some. | 3580 | 48.9 | 51.9 | 3.0 | | 130 | 0.8 | 22989 | 69 |
| | | 31.5-36.5 - 20-30% sulphides Sulphosalts. | 3581 | 51.9 | 54.9 | 3.0 | | 440 | 1.4 | 29009 | 70 |
| | | | 2 | 54.9 | 56.9 | 2.0 | | 580 | 2.9 | 3807 | 70 |
| | | Fault Zone - Sericite -Qtz-Py-Rock | 3 | 56.9 | 57.9 | 1.0 | | 1090 | 8.3 | 21217 | 304 |
| | | Broken and sheared<br>47.0-Increases in chlorite content also increase in Cpy.<br>51.8- Core is quite chloritic-running 5% Cpy. | | | | | | | | | |

HOLE NO. K87-8

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 57.9 | 58.1 | Sandy Tuff | 3584 | 57.9 | 59.9 | 2.0 | | 360 | 2.9 | 14620 | 57 |
| | | - Dark grey coloured | 5 | 59.9 | 61.9 | 2.0 | | 900 | 4.8 | 21341 | 53 |
| | | - No apparent sulphides | 6 | 61.9 | 63.9 | 2.0 | | 640 | 4.4 | 21895 | 58 |
| | | Contains small vescicles and feldspar later | 3587 | 63.9 | 65.9 | 2.0 | | 465 | 2.4 | 17772 | 42 |
| | | may be a dyke. | 8 | 65.9 | 67.9 | 2.0 | | 370 | 1.9 | 15080 | 57 |
| | | | 9 | 67.9 | 69.9 | 2.0 | | 460 | 1.9 | 14107 | 37 |
| 58.1 | 77.1 | Fault Zone - Sericite-Qtz-Py Rock | 3590 | 69.9 | 71.9 | 2.0 | | 630 | 5.1 | 24845 | 68 |
| | | Rock ground such that only sand remaining | 1 | 71.9 | 73.9 | 2.0 | | 420 | 2.2 | 14827 | 89 |
| | | Strong shear foliation 60° to core axis. | 2 | 73.9 | 75.9 | 2.0 | | 360 | 2.2 | 11268 | 53 |
| | | 10-15% Py throughout along with qtz | 3 | 75.9 | 77.1 | 1.2 | | 460 | 1.7 | 9820 | 42 |
| | | segregations in schistose rock | | | | | | | | | |
| | | 61.56-61.70 - remains of qtz vein. | | | | | | | | | |
| | | 64.46-65.8 - chloritic alteration | | | | | | | | | |
| | | 75.0- end - Rock much more competent. | | | | | | | | | |
| | | 76.2 - Rock becomes chloritic near contact | | | | | | | | | |
| | | Foliation 60° to core axis | | | | | | | | | |
| | | 15% Py. | | | | | | | | | |
| 77.1 | 80.1 | Andesite Dyke | 3594 | 77.1 | 78.6 | 1.5 | | nd | 0.1 | 1197 | 175 |
| | | - Very fine grained | 5 | 78.6 | 80.1 | 1.5 | | nd | 0.1 | 2071 | 163 |
| | | -Green chloritic - slightly blocky | | | | | | | | | |
| | | 78.5 - Possible native copper in dyke- | | | | | | | | | |
| | | probable | | | | | | | | | |
| | | no apparent sulphides - trace pyrite | | | | | | | | | |
| | | Unitform texture - Massive | | | | | | | | | |
| | | Very chloritic. | | | | | | | | | |

HOLE NO. K87-8

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| 80.1 | 94.8 | Fault Zone Sericite-Quartz-Pyrite+ Chloritic Rock | 3596 | 80.1 | 82.1 | 2.0 | | 240 | 0.7 | 9165 | 125 |
| | | Up to 20% sulphides primarily as pyrite also very sheared with strong foliation. A black crystal contorted and gouged in places. ?sphal? Tr Cpy | 3597 | 82.1 | 84.1 | 2.0 | | 280 | 1.1 | 10992 | 137 |
| | | | 8 | 84.1 | 86.1 | 2.0 | | 220 | 1.5 | 11352 | 314 |
| | | | 9 | 86.1 | 88.1 | 2.0 | | 260 | 1.3 | 12280 | 94 |
| | | | 3600 | 88.1 | 90.1 | 2.0 | | 150 | 1.2 | 10362 | 43 |
| | | | 1 | 90.1 | 92.1 | 2.0 | | 140 | 0.7 | 7681 | 78 |
| | | Chloritic near top broken core to 87.3 | 2 | 92.1 | 93.6 | 1.5 | | 225 | 2.4 | 6434 | 171 |
| | | Possible originally a lapilli tuff. | 3 | 93.6 | 94.8 | 1.2 | | 270 | 8.0 | 6530 | 2005 |
| | | 87.3 - Rock becomes more competent foliation 55° to core axis. | | | | | | | | | |
| | | 90.46-90.74 - Green andesite dyke. Upper contact (85° to core axis)-very fine grained. | | | | | | | | | |
| | | 91.7-93.1 - Broken core. | | | | | | | | | |
| | | 93.1 - Some blue clay minerals occurring | | | | | | | | | |
| | | 94.1 - Intense shearing stops | | | | | | | | | |
| | | Rusty - slightly sheared tuff to 94.8 | | | | | | | | | |
| 94.8 | 115.12 | Crystal Lapilli Tuff - grey | 3604 | 94.8 | 96.8 | 2.0 | | 370 | 4.8 | 3909 | 1313 |
| | | Silicified - not nearly as much sericite | 5 | 96.8 | 98.8 | 2.0 | | 280 | 1.2 | 4832 | 211 |
| | | 20-25% Py up to 2% Cpy in places | 6 | 98.8 | 100.8 | 2.0 | | 470 | 1.7 | 3065 | 274 |
| | | Pyrite is dissem throughout with bandsd | 7 | 100.8 | 102.8 | 2.0 | | 230 | 2.3 | 3346 | 68 |
| | | parallel to foliation up to 10cm across | 8 | 102.8 | 104.8 | 2.0 | | 300 | 0.6 | 3028 | 65 |
| | | that run 40%. | 9 | 104.8 | 106.8 | 2.0 | | 275 | 1.2 | 4218 | 196 |
| | | A black mineral occurs in places | 3610 | 106.8 | 108.8 | 2.0 | | 205 | 0.4 | 7031 | 133 |
| | | Several narrow qtz-$CO_3$ veins up to 1cm | 1 | 108.8 | 110.8 | 2.0 | | 160 | 0.4 | 3365 | 353 |
| | | across | 2 | 110.8 | 112.5 | 1.7 | | 250 | 1.6 | 13309 | 739 |
| | | | 3 | 112.5 | 115.1 | 2.6 | | 280 | 2.0 | 5474 | 3548 |

HOLE NO. K87-8

PROPERTY Kerr Project



| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | Follow along the foliation.<br>These often have a core of pyrite<br>The feldspar in the rock are generally saussuritized giving the rock an epidote green colour in places. - Rock relatively massive.<br>95.9 - Foliation 60°.<br>101 - Increae in silica and weakly foliated pyrite. Several massive pyrite veins. 2-5cm across running parallel to foliation direction 60°.<br>105-115.1 - 30-35% pyrite in veins and fractures<br>Tr Cpy and perhaps sphal - tetrahedrite<br>Tr native copper.<br>103.7 - Native gold. Cpy, Py, tetrahedrite sample taken | | | | | | | | | |
| 115.12 | 116.35 | Andesite Dyke - Green<br>Fine grained - chloritic<br>Massive - contains several qtz-carb-chl veins crossing at 60° to core axis<br>Trace of pyrite. | 3614 | 115.1 | 116.4 | 1.5 | | 10 | 0.1 | 464 | 270 |
| 116.35 | 147.22 | Crystal Lapilli Tuff - Silicified<br>Sericitized<br>Grey-pale yellow-green<br>Feldspars saussuritized | 3615 | 116.4 | 118.4 | 2.0 | | nd | 0.1 | 2265 | 144 |
| | | | 6 | 118.4 | 120.4 | 2.0 | | 150 | 0.1 | 1620 | 91 |
| | | | 7 | 120.4 | 122.4 | 2.0 | | 200 | 0.8 | 2615 | 685 |

HOLE NO. K87-8

PROPERTY Kerr Project

SHEET NO. 7 of 7

| METERS From | METERS To | DESCRIPTION | SAMPLING Spl.# | From | To | m | Rec % | Au ppb | Ag ppm | Cu ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | | 20-25% sulphides as pyrite both as dissem | 3618 | 122.4 | 124.4 | 2.0 | | 205 | 0.4 | 2192 | 346 |
| | | and as qtz carbonite veins. | 9 | 124.4 | 126.4 | 2.0 | | 220 | 0.1 | 3448 | 172 |
| | | Tr Cpy and tetrahedrite and sphalerite. | 3620 | 126.4 | 128.4 | 2.0 | | nd | 0.1 | 1569 | 70 |
| | | Veins criss-crossing at 60° and 30°. | 1 | 128.4 | 130.4 | 2.0 | | 150 | 0.1 | 2504 | 93 |
| | | Approx 40 veinlets each 5mm across/m | 2 | 130.4 | 132.4 | 2.0 | | 120 | 1.0 | 1615 | 136 |
| | | Some sericitic massive pyrite sections | 3 | 132.4 | 134.4 | 2.0 | | 145 | 0.6 | 1629 | 310 |
| | | 122.0- Native copper along fractues running | 3624 | 134.4 | 136.4 | 2.0 | | 110 | 0.4 | 949 | 447 |
| | | down core axis. | 5 | 136.4 | 138.4 | 2.0 | | 260 | 0.3 | 1490 | 235 |
| | | 126.4 - Py-qtz vein 70° to core axis | 6 | 138.4 | 140.4 | 2.0 | | 550 | 1.3 | 1266 | 156 |
| | | 135.0 - decrease in silicification | 7 | 140.4 | 142.4 | 2.0 | | 240 | 1.3 | 1228 | 1730 |
| | | - increase in chlorite alteration | 8 | 142.4 | 144.4 | 2.0 | | 320 | 0.9 | 717 | 2333 |
| | | - less quartz veining | 9 | 144.4 | 147.2 | 2.8 | | 310 | 3.9 | 591 | 3702 |
| | | - mostly carbonatees veining | | | | | | | | | |
| | | - decrease in sulphide to 10% | | | | | | | | | |
| | | (Gradual Changes) | | | | | | | | | |
| | | - decrease in sulphide to 10% | | | | | | | | | |
| | | - becomes green coloured | | | | | | | | | |
| 147.22 | | ----------End of Hole---------- | | | | | | | | | |

## Core Recovery K87- 8

| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY |
|---|---|---|---|---|
| Start | 3.05 | 3.05 | 2.73 | 90 |
| 3.05 | 4.88 | 1.83 | 1.30 | 71 |
| 4.88 | 5.79 | .91 | .20 | 22 |
| 5.79 | 6.86 | 1.07 | .64 | 60 |
| 6.86 | 7.62 | .76 | .67 | 88 |
| 7.62 | 8.84 | 1.22 | .39 | 32 |
| 8.84 | 10.36 | 1.52 | .66 | 43 |
| 10.36 | 11.88 | 1.52 | .38 | 25 |
| 11.88 | 13.72 | 1.84 | .22 | 12 |
| 13.72 | 15.54 | 1.82 | .22 | 12 |
| 15.54 | 16.76 | 1.22 | .27 | 22 |
| 16.76 | 19.20 | 2.44 | .32 | 13 |
| 19.20 | 20.12 | .92 | .46 | 50 |
| 20.12 | 21.03 | .91 | .73 | 80 |
| 21.03 | 22.4 | 1.37 | 1.08 | 79 |
| 22.4 | 23.16 | .76 | .29 | 38 |
| 23.16 | 24.38 | 1.22 | .88 | 72 |
| 24.38 | 26.37 | 1.99 | 1.83 | 92 |
| 26.37 | 27.58 | 1.21 | .94 | 78 |
| 27.58 | 29.57 | 1.99 | 2.08 | 105 |
| 29.57 | 30.33 | .76 | .52 | 68 |
| 30.33 | 31.55 | 1.22 | .65 | 53 |
| 31.55 | 32.46 | .91 | .58 | 64 |
| 32.46 | 32.92 | .46 | .13 | 28 |
| 32.92 | 33.68 | .76 | .50 | 66 |
| 33.68 | 34.75 | 1.07 | .48 | 45 |
| 34.75 | 36.58 | 1.83 | .22 | 12 |
| 36.58 | 37.8 | 1.22 | .40 | 33 |
| 37.8 | 38.4 | .6 | .52 | 87 |
| 38.4 | 39.17 | .77 | .27 | 35 |
| 39.17 | 41 | 1.07 | .24 | 22 |
| 41.0 | 41.76 | .76 | .22 | 29 |
| 41.76 | 44.5 | 2.74 | .18 | 7 |
| 44.5 | 45.26 | .76 | .15 | 20 |

## Core Recovery K87- 8

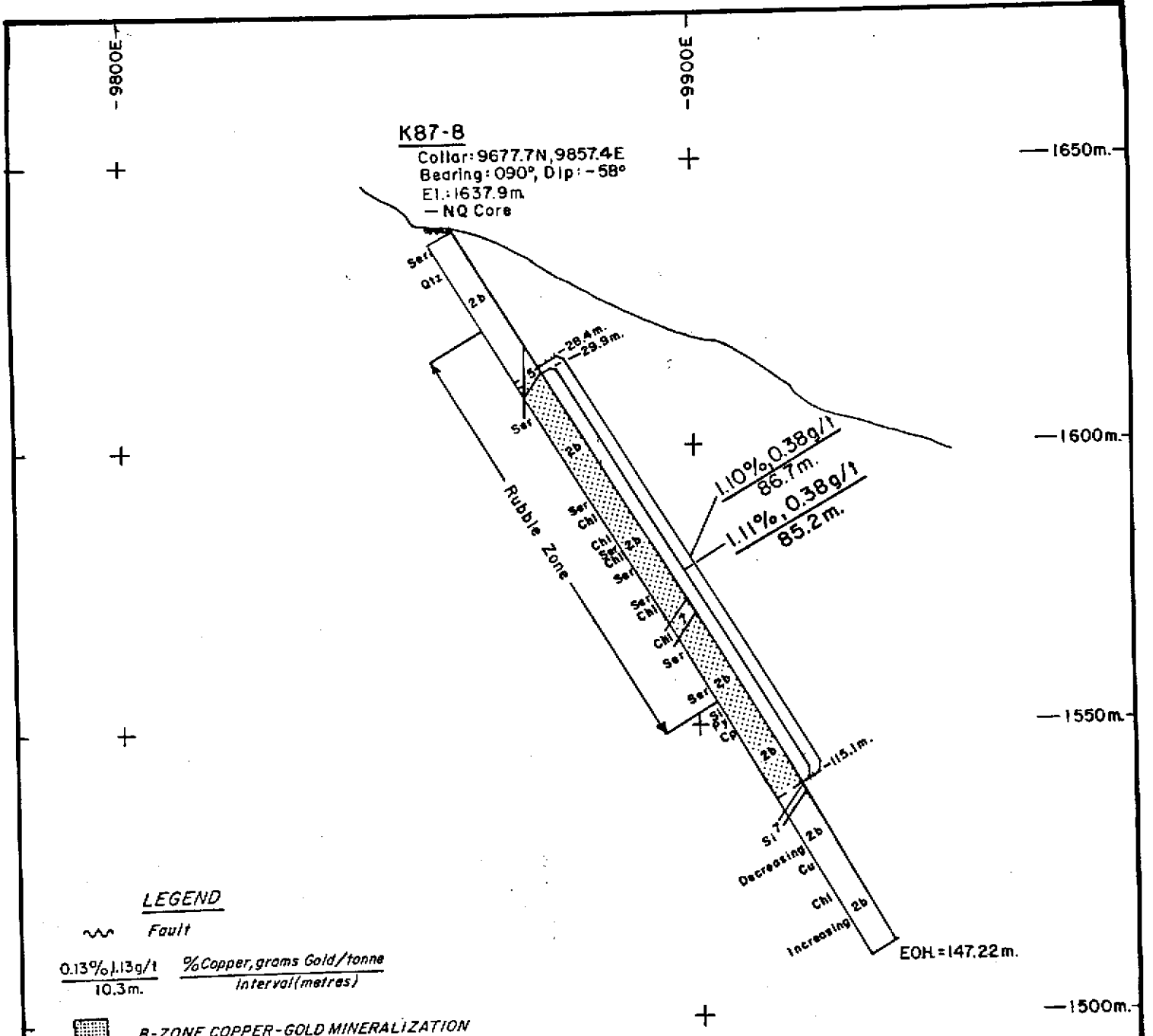
| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY |
|---|---|---|---|---|
| 45.26 | 45.57 | .31 | .23 | 74 |
| 45.57 | 45.72 | .15 | .11 | 73 |
| 45.72 | 46.33 | .61 | .06 | 10 |
| 46.33 | 47.09 | .76 | .35 | 46 |
| 47.09 | 48.92 | 1.83 | .22 | 12 |
| 48.92 | 50.6 | 1.68 | .09 | 5 |
| 50.6 | 51.82 | 1.22 | .13 | 11 |
| 51.82 | 53.64 | 1.82 | .13 | 7 |
| 53.64 | 54.86 | 1.22 | .1 | 8 |
| 54.86 | 55.78 | .92 | .24 | 26 |
| 55.78 | 56.69 | .91 | .39 | 43 |
| 56.69 | 58.22 | 1.53 | .40 | 26 |
| 58.22 | 60.35 | 2.13 | 1.50 | 70 |
| 60.35 | 61.41 | 1.04 | .74 | 71 |
| 61.41 | 61.56 | .15 | .09 | 60 |
| 61.56 | 61.72 | 0.16 | .10 | 63 |
| 61.72 | 62.33 | .61 | .42 | 67 |
| 62.33 | 63.24 | .91 | .21 | 23 |
| 62.24 | 64.00 | .76 | .52 | 68 |
| 64.0 | 64.46 | .46 | .23 | 50 |
| 64.46 | 65.83 | 1.37 | .71 | 52 |
| 65.83 | 66.25 | .42 | .36 | 86 |
| 66.25 | 67.51 | 1.26 | .45 | 36 |
| 67.51 | 68.27 | .76 | .36 | 47 |
| 68.27 | 68.88 | .61 | .26 | 43 |
| 68.88 | 69.79 | .91 | .24 | 26 |
| 69.79 | 70.40 | .61 | .25 | 41 |
| 70.40 | 71.32 | .92 | .18 | 19 |
| 71.32 | 71.93 | .61 | .37 | 61 |
| 71.93 | 72.84 | .91 | .30 | 32 |
| 72.84 | 73.45 | .61 | .25 | 41 |
| 73.45 | 74.98 | 1.53 | .95 | 62 |
| 74.98 | 76.20 | 1.22 | .90 | 74 |

## Core Recovery K87- 8

| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY |
|---|---|---|---|---|
| 76.20 | 77.87 | 1.67 | 1.25 | 75 |
| 77.87 | 78.63 | .76 | .55 | 72 |
| 78.63 | 79.71 | 1.08 | .69 | 64 |
| 79.71 | 81.08 | 1.37 | .51 | 37 |
| 81.08 | 81.99 | .91 | .25 | 27 |
| 81.99 | 83.82 | 1.83 | 1.36 | 74 |
| 83.82 | 84.58 | .76 | .38 | 50 |
| 84.58 | 85.83 | 1.25 | .39 | 31 |
| 85.83 | 87.33 | 1.5 | .14 | 9 |
| 87.33 | 90.22 | 2.89 | 1.37 | 47 |
| 90.22 | 93.12 | 2.9 | 1.85 | 64 |
| 93.12 | 94.03 | .91 | .75 | 82 |
| 94.03 | 95.86 | 1.83 | 1.6 | 87 |
| 95.86 | 98.76 | 2.9 | 2.86 | 99 |
| 98.76 | 101.8 | 3.04 | 3.02 | 99 |
| 101.8 | 102.4 | .6 | .56 | 93 |
| 102.4 | 105.2 | 3.4 | 2.58 | 76 |
| 105.2 | 108.2 | 3.0 | 2.66 | 89 |
| 108.2 | 109.6 | 1.4 | .96 | 69 |
| 109.6 | 110.8 | 1.2 | 1.03 | 86 |
| 110.8 | 112.5 | 1.7 | 1.17 | 69 |
| 112.5 | 114.6 | 2.1 | 1.93 | 92 |
| 114.6 | 115.8 | 1.2 | 1.14 | 95 |
| 115.8 | 117. | 1.2 | 1.2 | 100 |
| 117.0 | 118.3 | 1.3 | .98 | .75 |
| 118.3 | 120.1 | 1.8 | 1.77 | 98 |
| 120.1 | 122.8 | 2.7 | 2.08 | 77 |
| 122.8 | 123.75 | .95 | .95 | 100 |
| 123.75 | 124.05 | .30 | .30 | 100 |
| 124.05 | 125.73 | 1.68 | 1.63 | 97 |
| 125.73 | 126.34 | .61 | .47 | 77 |
| 126.34 | 126.80 | .46 | .41 | 89 |
| 126.80 | 129.54 | 2.74 | 2.64 | 96 |
| 129.54 | 132.74 | 3.2 | 2.85 | 89 |
| 132.74 | 133.96 | 1.22 | .84 | 69 |

## Core Recovery K87- 8

| FROM | TO | INTERVAL LENGTH | CORE LENGTH | PERCENT RECOVERY |
|---|---|---|---|---|
| 133.96 | 134.72 | .76 | .74 | 97 |
| 134.72 | 135.33 | .61 | .38 | 62 |
| 135.33 | 136.25 | .92 | .65 | 71 |
| 136.25 | 137.46 | 1.21 | 1.04 | 86 |
| 137.46 | 138.99 | 1.53 | 1.53 | 100 |
| 138.99 | 140.51 | 1.52 | .85 | 56 |
| 140.51 | 141.43 | .92 | .84 | 91 |
| 141.43 | 141.58 | .15 | .07 | 47 |
| 141.58 | 142.04 | .46 | .22 | 48 |
| 142.04 | 143.56 | 1.52 | 1.12 | 74 |
| 143.56 | 144.78 | 1.22 | 1.22 | 100 |
| 144.78 | 146.46 | 1.68 | 1.55 | 92 |
| 146.46 | 147.22 | .76 | .52 | 68 |




## LEGEND

~~ Fault

0.13% | 1.13g/t / 10.3m. — % Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Interval defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE – fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a) / MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST – foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) – interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE – interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

| | |
|---|---|
| Chl | Chlorite |
| Ser | Sericite |
| Py | Pyrite |
| Qtz | Quartz |
| Cu | Copper |

**SULPHURETS GOLD CORPORATION**

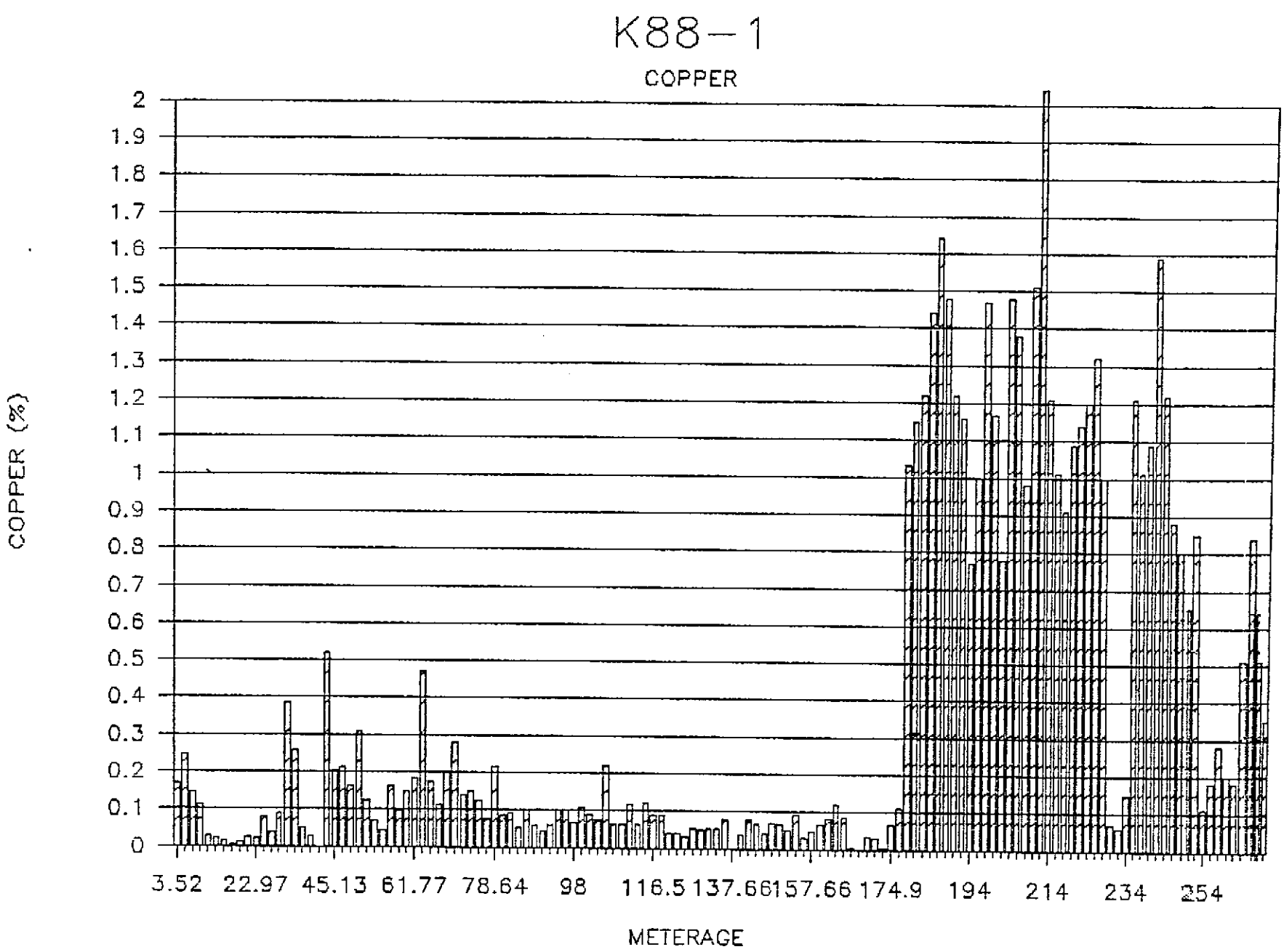
# 1989 KERR PROJECT

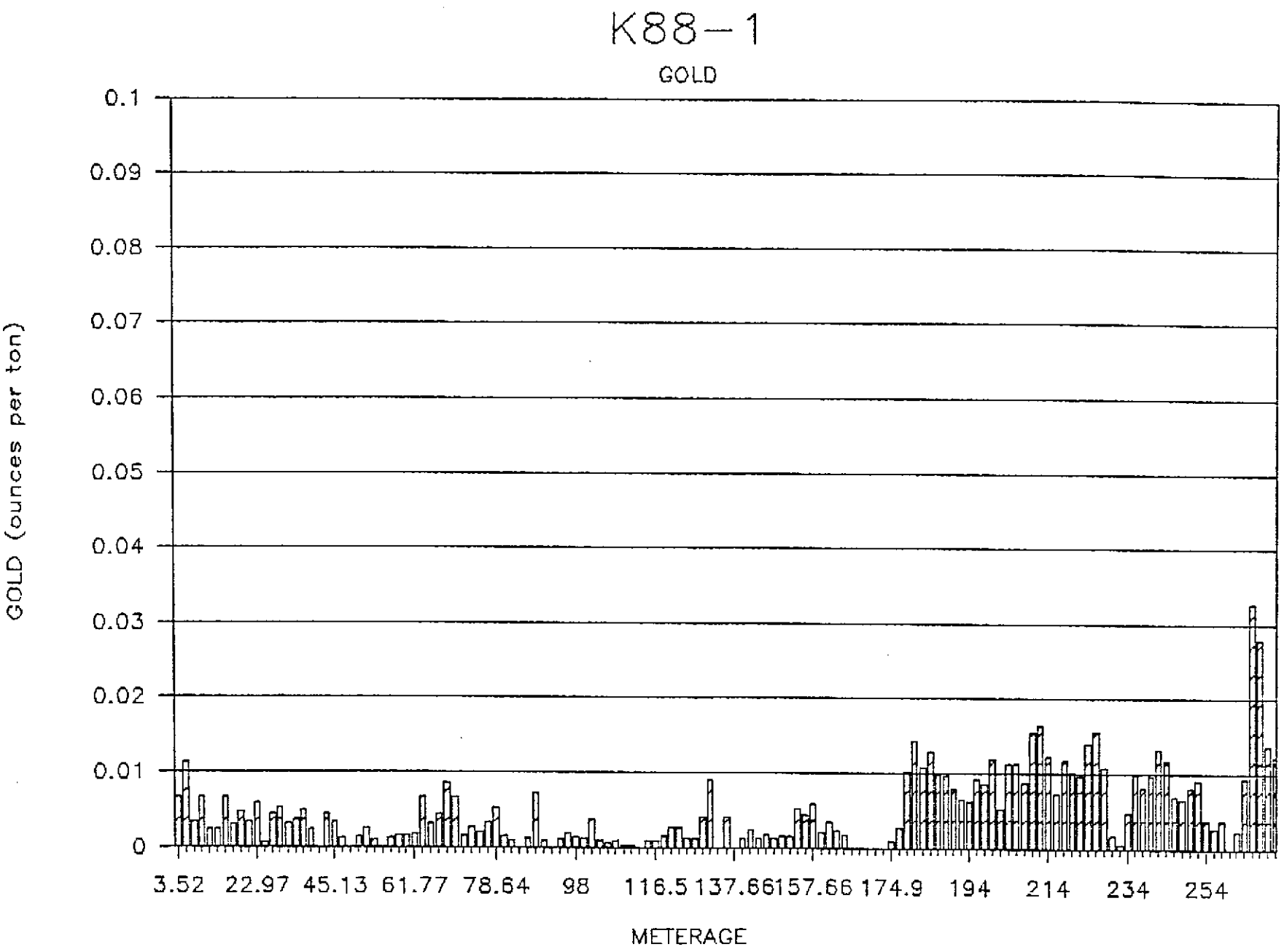
## SECTION 9677N
## DDH K87-8

Scale 0 10 20 30 40 METRES

RPT: 1065 | FIGURE

SECTION 2
1988 HOLES


K88-1
COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
3.52
22.97
45.13
61.77
78.64
98
116.5
137.66
157.66
174.9
194
214
234
254
METERAGE


K88-1
GOLD
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
GOLD (ounces per ton)
3.52
22.97
45.13
61.77
78.64
98
116.5
137.66
157.66
174.9
194
214
234
254
METERAGE

KERR PROJECT D.D.HOLE K-88-1

| | | | |
|---|---|---|---|
| LOCATION | B-ZONE SOUTH | COLLAR LAT. | 9632.3 NORTH |
| DATE STARTED | JULY 3, 1988 | LONG. | 9715.6 EAST |
| DATE COMPLETED | JULY 7, 1988 | ELEVATION | 1712.0 m |
| CORE RECOVERY | 76.93% | AZIMUTH | 090 DIP -62 deg |
| DRILLED BY | FALCON DRILLING LTD. | LENGTH | 272.80 m |
| LOGGED BY | S. CASSELMAN | HOR. PROJ. | 155.73 m |
| OBJECTIVE | TEST FOR CU MIN.WEST OF K.87-11 | VERT.PROJ. | 222.35 m |
| DIP TEST DEPTH | 215.8 m DIP-50.5 deg | | |
| DEPTH | DIP deg | | |

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 1.52 | 1.52 | OVERBURDEN |
| 1.52 | 9.84 | 8.32 | DACITIC LAPILLI TUFF<br>- medium intense chloritization, with 15% pyrite as 1 to 5 mm stringers of medium to coarse crystalline, subhedral grains, which parallel foliation at 30 deg to core axis (C.A.)<br>- occasional quartz vein up to 1 cm wide, generally pitted and weathered<br>- pyrite veinlets generally with quartz rim |
| 9.84 | 14.44 | 4.60 | HORNBLENDE PORPHYRY DIORITE DYKE<br>- fine to medium grained, inequigranular<br>- bleached and clay altered plagioclase, with hornblende altered to chlorite<br>- 3% fine-grained euhedral pyrite |
| 14.44 | 31.01 | 16.57 | DACITE LAPILLI TUFF<br>- intensely altered, chloritized at upper and lower contact with dyke for 30 cm becoming increasingly sericitic<br>- 3 - 5% pyrite as fine-grained to aphanitic disseminations which are dark grey to black |

KERR PROJECT D.D.HOLE K-88-1

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - 10 cm quartz vein which is weathered, pitted and limonitic<br>- abundant limonite on fracture surfaces foliation at 45 deg to C.A.<br>at 18.97 to 22.97 - FAULT ZONE<br>- sericite schist is quite fractured and soft<br>- intensely brecciated in a few sections for 20 cm<br>- intensely sericitized margin around fault zone<br>- pyrite occurs as fine-grained dark grey masses<br>- sample 9011 contains a 5 cm white quartz vein<br>- sample 9014 contains 4 sections of 1 to 2 cm wide limonite welded breccia at 20 deg to C.A.<br>28.6 to 31.01 - tuff is intensely chloritized as it approaches contact with diorite dyke, much less sericite<br>- pyrite content increases to 10%, as stringers and coarse disseminations<br><br>- sample 9016 contains 2 quartz veins 1 to 2 cm and 1 to 5 cm wide at 30 deg to C.A. |
| 31.01 | 41.13 | 10.12 | HORNBLENDE PORPHYRY DIORITE DYKE<br>- similar to dyke in section 9.84 to 14.44<br>- quite altered, bleached with limonitic sections up to 10 cm wide with 1 or 2 small quartz stringers<br><br>31.01 to 35.00 - intensely altered and bleached, with chlorite and sericite - sheared<br>35.00 to 41.13 - 3% bull white quartz veins, no sulphides, moderately altered dyke, occasional gossanous limonitic section<br>- contacts at 35 deg to C.A. |
| 41.13 | 50.48 | 9.35 | DACITE LAPILLI TUFF<br>- moderate to intense chloritization patches of intense sericite |

KERR PROJECT D.D.HOLE K-88-1

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - increasing sericitization towards lower contact<br>- 1 to 5% pyrite as veinlets (up to 2 mm wide) and coarse disseminations |
| 50.48 | 58.77 | 8.29 | FAULT ZONE - SERICITE SCHIST<br><br>- intense sericitization, quite fractured, believed to be fault zone<br>- fractures at 45 deg to C.A.<br>- 10 to 15% pyrite as fine stringers paralleling foliation and as fine-grained, dark grey masses<br>- 0.5% chalcocite occurs as fine-grained dark blue-grey around pyrite |
| 58.77 | 63.29 | 4.52 | SERICITE SCHIST<br>- less fractured than overlying schist, becoming more chloritic away from fault zone and towards dyke<br>- protolith believed to be dacitic lapilli tuff<br>- sample 9030 and 9031 each contain 1 cm weather and pitted quartz box-work veins |
| 63.29 | 67.62 | 4.33 | HORNBLENDE PORPHYRY DIORITE DYKE<br>- as in sections 9.84 to 14.44 and 31.01 to 41.13 altered and bleached- upper contact at 50 deg to C.A., lower contact at 15 deg to C.A. |
| 67.62 | 69.95 | 2.33 | DACITIC CRYSTAL LAPILLI TUFF<br>- less altered than overlying tuff sections, slightly chloritized<br>- contains less lapilli fragments and more crystals in the matrix increasing amount of crystals towards lower contact<br>- 5% pyrite, traces of chalcocite |
| 69.95 | 72.05 | 2.10 | HORNBLENDE PORPHYRY DIORITE DYKE<br>- as in above sections of diorite dyke, sericitized and clay altered<br>- slightly less altered, with plagioclase altering to clay and sericite and hornblende to chlorite, limonite on fracture surfaces<br>- 1 cm quartz - clay - limonite vein |

KERR PROJECT D.D.HOLE K-88-1

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | in core of dyke<br>- upper contact at 90 deg to C.A., lower contact at 70 deg to C.A. |
| 72.05 | 78.64 | 6.59 | DACITIC CRYSTAL LAPILLI TUFF<br>- as in section 67.62 to 69.95- increasing amount of crystals towards lower contact<br>- moderate sericitization and chloritization |
| 78.64 | 106.00 | 27.36 | LAMINATED DACITIC CRYSTAL TUFF<br>- medium grey colour, abundance of lapilli fragments, mostly dark grey colour, numerous pyritic lapilli<br>- distinct lamination<br>- carbonate occurs in small discontinuous stringers and cavities<br>- feldspar with quartz in veins 90.41 to 90.55 - broken zone<br>- 94.56 - lapilli crystal tuff very similar to above, except noticeably finer lamination and fewer but large lapilli, some ash beds included, more sericitic alteration<br>102.11 to 102.41 - porous quartz vein with fragments of tuff included- very rusty<br>106.21 to 107.35 - brecciated zone prior to consolidation<br>- abundant large angular clasts and lapilli up to 3 cm long |
| 106.00 | 116.50 | 10.50 | LAMINATED LAPILLI TUFF<br>- increased abundance of lapilli fragments, decrease in crystals<br>- greater intensity of alteration |
| 116.50 | 120.50 | 4.00 | FAULT ZONE - SERICITE SCHIST<br>- intensely sericitized and sheared with abundant fault gauge<br>- probable protolith of laminated lapilli tuff<br>- gradational upper contact at 60 deg to C.A.<br>- sharp lower contact at 60 deg to C.A. |
| 120.50 | 133.73 | 13.23 | LAMINATED CRYSTAL TUFF<br>- as in section 78.64 to 106.00 with |

KERR PROJECT D.D.HOLE K-88-1

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | a greater abundance of lapilli<br>- variable dark grey - green colour<br>- 1% quartz stringers to 1 cm wide<br>- dendritic native copper on fracture surface at 126.24 m (sample # 9065)<br>127.40 to 129.60 - brecciated and distorted lapilli tuff prior to consolidation. Fine-grained sulphides as matrix<br>- abundant lapilli up to 3 cm long<br>- occasional, rare, vuggy quartz vein up to 3 cm<br>- at lower contact with andesite dyke have a 25 cm bull white quartz vein with minor calcite and potassium feldspar, with no sulphides<br>- at 133.27 occurs a 10 cm quartz-calcite vein with 10% pyrite and 1% chalcocite in sample # 9069 |
| 133.73 | 137.66 | 3.93 | ANDESITE DYKE<br>- fine-grained, homogeneous, pervasive medium grey<br>- minor sericite and chlorite alteration, trace to 1% pyrite<br>- sharp upper contact at 30 deg to C.A.<br>- gradational lower contact at 55 deg to C.A. |
| 137.66 | 164.66 | 27.00 | LAPILLI CRYSTAL TUFF<br>- abundant large lapilli and angular fragments<br>- chloritized, sericitized and pyritized<br>- gradational upper contact with dyke<br>- fine-grained crystal tuff<br>- quite mottled and messed up from 138 to 139.25, very dark grey to blue, angular fragments<br>141.80 to 142.64 - intensely sheared and sericitized quartz - carbonate-potassium feldspar veins up to 2 cm wide containing 25% pyrite and 2 - 3% chalcocite, very soft<br>- sections of regularly spaced abundant (60%) lapilli which have been chloritized with minor sericite |

KERR PROJECT D.D.HOLE K-88-1

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | and pyritization<br>- slightly foliated<br>- pyrite occurs as disseminated, 1-3 mm coarse veins and veins and blebs to 5 cm wide with very fine-grained dark grey sulphides<br>- lower section of tuff appears to be laminated<br>- sheared and sericitized near lower contact with plagioclase porphyry dyke, abundant quartz - calcite -k-feldspar veins for 1 m from contact |
| 164.66 | 174.90 | 10.24 | PLAGIOCLASE PORPHYRY DYKE<br>- plagioclase (oligoclase?) phenocrysts to 2 cm square<br>- 20% phenocrysts in a fine- to medium-grained, dark grey to green matrix<br>- occasional 1 to 2 mm hornblende crystal, sometimes chloritized-feldspars altered to sericite-abundant calcite veins and stringers at 171.90 - 10 cm quartz - carbonate -k-feldspar vein at 20 deg to C.A. with native copper on fracture surface, with no other sulphides<br>- lower contact at 70 deg to C.A., bleached for 2 cm from contact<br>- sharp lower contact |
| 174.90 | 176.17 | 1.27 | FRACTURED LAPILLI TUFF<br>- quite fractured tuff between porphyry dyke and fault zone sericite schist<br>- abundant quartz - calcite veins and sulphides, quite altered<br>- contact with sericite schist is fairly sharp, but gradual at 85 deg to C.A. |
| 176.17 | 228.25 | 52.08 | FAULT ZONE - QUARTZ -SERICITE-PYRITE SCHIST<br>- intensely faulted and fractured sericitic zone, comprised virtually of 5 cm chips, sand and gauge<br>- quite soft sericitic gauge, most competent sections are quartz - |

KERR PROJECT D.D.HOLE K-88-1

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | pyrite veins<br>- 25% pyrite, 1% combined chalcopyrite and chalcocite<br>- chalcopyrite occurs mainly in quartz veins, while chalcocite occurs as blue - black wisps and as a coating on pyrite crystals<br>- pyrite occurs as veins, disseminations and very fine-grained blebs and bands up to 2 cm wide<br>- minor gypsum (0.01%)<br>202.00 to 228.00 - pervasive deep blue colour in quartz, especially where associated with very fine-grained sulphides - chalcocite<br>- rate malachite spots<br>at 215.80 - 21 cm andesite dyke, fine-grained to aphanitic, medium grey to green, unaltered, barren of sulphides<br>- contacts at 80 deg to C.A.<br>224.20 to 228.25 - 60% quartz-pyrite - chalcopyrite - chalcocite vein continues to contact with andesite dyke |
| 228.25 | 234.00 | 5.75 | ANDESITE DYKE<br>- fine-grained to aphanitic, medium to dark grey - green<br>- fractured and clay altered<br>- large (2 to 5 cm) quartz - calcite, with 3% pyrite, veins at 232.47 (sample # 9118)<br>- similar to dyke at 133.73 to 137.66, but finer grained and more chloritic |
| 234.00 | 272.80 | 38.80 | FAULT ZONE - QUARTZ - SERICITE-PYRITE SCHIST<br>- as in section 176.77 to 228.25<br>- intensely fractured and sericitized<br>234.00 to 256.00 - 60% quartz, pyrite chalcopyrite, chalcocite along contact with dyke, as in section 224 to 228<br>260.00 to 272.80 EOH - increasing clay alteration and sericite relic lapilli altered to clay and sericite |

KERR PROJECT D.D.HOLE K-88-1

| FROM (m) | TO (m) | WDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - abundant chalcocite mineralization with copper mineralization continuing to bottom of hole<br>- hole ends in copper mineralization |

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| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 881 | 9632.3 | 9715.6 | 1712 | 90 | 62 | 272.80 | | Intersect B Zone ;Chargeability High ; X-Section #HOLE |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1.52 | 1.52 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 1.52 | 3.52 | 2 | 44 | DCIT LPLL TUFF | | F-CG | .5 | 1 | 8 | 3 | 30 | 1 | | | | | 30 | 15 | | | | | | |
| 3.52 | 5.52 | 2 | 39 | DCIT LPLL TUFF | | F-CG | .5 | 3 | 8 | 3 | 30 | 1 | | | | | 30 | 12 | | | | | | |
| 5.52 | 7.52 | 2 | 35 | DCIT LPLL TUFF | | F-CG | .5 | 3 | 8 | 3 | 30 | 2 | | | | | 30 | 8 | | | | | | |
| 7.52 | 9.84 | 2.32 | 42 | DCIT LPLL TUFF | | F-CG | .5 | 2 | 15 | 5 | 25 | 2 | | | | | 40 | 8 | | | | | | |
| 9.84 | 12.14 | 2.3 | 28 | PLAG HBLD PRPH | | M-CG | | | | 15 | 5 | | | | | | 50 | 3 | | | | | | |
| 12.14 | 14.44 | 2.3 | 26 | PLAG HBLD PRPH | | M-CG | | | | 15 | 5 | | | | | | 50 | 3 | | | | | | |
| 14.44 | 15.95 | 1.51 | 40 | DCIT LPLL TUFF | | F-CG | | 2 | 30 | 6 | 15 | 2 | | | | | 60 | 3 | | | | | | |
| 15.95 | 17.46 | 1.51 | 37 | DCIT LPLL TUFF | | F-CG | 1 | 3 | 50 | 3 | 3 | | | | | | 65 | 3 | .1 | | .5 | | | |
| 17.46 | 18.97 | 1.51 | 32 | DCIT LPLL TUFF | | F-CG | 1 | 3 | 50 | 3 | 8 | | | | | | 70 | 3 | .1 | | .1 | | | |
| 18.97 | 20.97 | 2 | 25 | SRCT SCST FAULT | | FG | | 3 | 50 | 10 | 3 | | | | | | 70 | 2 | | | .5 | | | |
| 20.97 | 22.97 | 2.02 | 30 | SRCT SCST FAULT | | FG | | 3 | 50 | 10 | 3 | | | | | | 70 | 1 | | | | | | |
| 22.97 | 25 | 2.03 | 40 | SRCT SCST | | FG | | 1 | 45 | 1 | 10 | | | | | | 60 | 3 | | | | | | |
| 25 | 27 | 2 | 35 | SRCT SCST | | FG | | .5 | 40 | 2 | 12 | | | | | | 60 | 5 | | | .5 | | | |
| 27 | 28.6 | 1.6 | 35 | SRCT SCST | | FG | | 1 | 40 | 10 | 15 | | | | | | 65 | 5 | | | .5 | | | |
| 28.6 | 29.8 | 1.2 | 43 | DCIT LPLL TUFF | | F-CG | | 1 | 10 | 2 | 30 | 3 | | | | | 40 | 10 | | | | | | |
| 29.8 | 31.01 | 1.21 | 40 | DCIT LPLL TUFF | | F-CG | | 2 | 5 | 5 | 35 | 2 | | | | | 50 | 2 | | | | | | |
| 31.01 | 33 | 1.99 | 40 | HBLD PLAG PRPH | | M-CG | 1 | 2 | 3 | 10 | 3 | | | | | | 40 | 4 | | | | | | |
| 33 | 35 | 2 | 43 | HBLD PLAG PRPH | | M-CG | | 2 | 15 | 10 | 2 | | | | | | 50 | 2 | | | | | | |
| 35 | 38.06 | 3.06 | 40 | HBLD PLAG PRPH | | M-CG | 1 | 3 | 2 | 5 | 10 | 2 | | | | | 25 | 2 | | | | | | |
| 38.06 | 41.13 | 3.07 | 40 | HRNB PLAG PRPH | | M-CG | 1 | 3 | 2 | 5 | 10 | 2 | | | | | 25 | 2 | | | | | | |
| 41.13 | 43.13 | 2 | 47 | DCIT LPLL TUFF | | F-CG | .5 | 1 | 2 | 2 | 35 | | | | | | 40 | 4 | | | | | | |
| 45.13 | 45.13 | 2 | 46 | DCIT LPLL TUFF | | F-CG | .5 | .5 | 1 | 1 | 30 | | | | | | 35 | 7 | | | | | | |
| 47.13 | 47.13 | 2 | 41 | DCIT LPLL TUFF | | F-CG | 1 | 2 | 8 | 5 | 30 | 1 | | | | | 40 | 5 | .5 | | .5 | | | |
| 49 | 49.13 | 2 | 48 | DCIT LPLL TUFF | | F-CG | | .5 | 3 | 3 | 30 | 1 | | | | | 35 | 8 | .1 | | .1 | | | |
| 13 | 50.48 | 1.35 | 47 | DCIT LPLL TUFF | | F-CG | | 2 | 8 | 2 | 25 | 1 | | | | | 40 | 10 | .5 | | .5 | | | |
| 50.48 | 52.48 | 2 | 33 | DCIT LPLL TUFF | | FG | | 2 | 50 | 3 | 5 | | | | | | 75 | 6 | | | .5 | | | |
| 52.48 | 54.48 | 2 | 30 | SRCT SCST FAULT | | FG | | 2 | 50 | 2 | 5 | | | | | | 75 | 12 | | | .5 | | | |
| 54.48 | 55.91 | 1.43 | 31 | SRCT SCST FAULT | | FG | | 2 | 50 | 5 | 5 | | | | | | 75 | 12 | | | .5 | | | |
| 55.91 | 57.34 | 1.43 | 38 | SRCT SCST FAULT | | FG | | 2 | 40 | 3 | 8 | 1 | | | | | 75 | 15 | | | .3 | | | |
| 57.34 | 58.77 | 1.43 | 34 | SRCT SCST FAULT | | FG | | 3 | 40 | 5 | 10 | | | | | | 75 | 12 | | | .3 | | | |
| 58.77 | 60.27 | 1.5 | 34 | SRCT SCST | | FG | | 2 | 35 | 1 | 15 | 1 | | | | | 70 | 12 | .1 | | .8 | | | |
| 60.27 | 61.77 | 1.5 | 38 | SRCT SCST | | FG | | 2 | 35 | 2 | 15 | 1 | | | | | 70 | 15 | .1 | | .3 | | | |
| 61.77 | 63.29 | 1.52 | 34 | SRCT SCST | | FG | | 1 | 25 | 1 | 30 | 1 | | | | | 65 | 12 | | | .5 | | | |
| 63.29 | 65.45 | 2.16 | 31 | PLAG HBLD PRPH | | M-CG | | 1 | 5 | 8 | 10 | 1 | | | | | 50 | 5 | | | .3 | | | |
| 65.45 | 67.62 | 2.17 | 24 | PLAG HBLD PRPH | | M-CG | | | 5 | 10 | 10 | | | | | | 50 | 4 | | | .1 | | | |
| 67.62 | 68.78 | 1.16 | 33 | XTAL LPLL TUFF | | F-MG | | .5 | 2 | 2 | 20 | | | | | | 30 | 5 | | | .2 | | | |
| 68.78 | 69.95 | 1.17 | 44 | XTAL LPLL TUFF | | F-MG | | 3 | 2 | 2 | 20 | | | | | | 30 | 5 | | | .1 | | | |
| 69.95 | 72.05 | 2.1 | 30 | PLAG HBDL PRPH | | FG | | 2 | | 3 | 5 | | | | | | 15 | 1 | | | | | | |
| 72.05 | 74 | 1.95 | 37 | XTAL LPLL TUFF | | FG | | 1 | 3 | 1 | 20 | | | | | | 25 | 7 | | | .1 | | | |
| 74 | 76 | 2 | 38 | XTAL LPLL TUFF | | FG | | 1 | 5 | 1 | 20 | 1 | | | | | 25 | 5 | | | | | | |
| 76 | 78 | 2 | 45 | XTAL LPLL TUFF | | FG | | 1 | 5 | .5 | 15 | | | | | | 25 | 12 | | | .1 | | | |
| 78 | 78.64 | .64 | 49 | XTAL LPLL TUFF | | FG | | 1 | 10 | 1 | 15 | 1 | | | | | 25 | 15 | | | .5 | | | |
| 78.64 | 80 | 1.36 | 49 | LMND XTAL TUFF | | F-MG | | .1 | 15 | | | | | | | | 15 | 20 | | | .1 | | | |
| 80 | 82 | 2 | 38 | LMND XTAL TUFF | | F-MG | | | 15 | | | | | | | | 15 | 20 | | | .1 | | | |
| 82 | 84 | 2 | 39 | LMND XTAL TUFF | | F-MG | | 1 | 15 | | | | | | | | 15 | 12 | | | | | | |
| 84 | 86 | 2 | 35 | LMND XTAL TUFF | | F-MG | | .1 | 15 | .1 | | | | | | | 15 | 10 | | | .3 | | | |
| 86 | 88.9 | 2 | 32 | LMND XTAL TUFF | | F-MG | | 1 | 20 | .1 | | | | | | | 20 | 8 | | | .1 | | | |
| 88 | 90 | 2 | 36 | LMND XTAL TUFF | | F-MG | | .1 | 20 | .1 | | | | | | | 20 | 7 | | | .1 | | | |
| 90 | 92 | 2 | 29 | LMND XTAL TUFF | | F-MG | | .1 | 20 | | .5 | | | | | | 21 | 8 | | | .1 | | | |
| 92 | 94 | 2 | 31 | LMND XTAL TUFF | | F-MG | | .1 | 20 | .1 | | .1 | | | | | 30 | 7 | | | .1 | | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 881 | 9632.3 | 9715.6 | 1712 | 90 | 62 | 272.80 | | Intersect B Zone ;Chargeability High ; X-Section | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 96 | 98 | 2 | 30 | LMND XTAL TUFF | | F-MG | | .2 | 20 | | | | | | | | 30 | 5 | | | .1 | | | |
| 98 | 100 | 2 | 32 | LMND XTAL TUFF | | F-MG | | | 20 | | .1 | | | | | | 30 | 5 | | | .1 | | | |
| 100 | 102 | 2 | 37 | LMND XTAL TUFF | | F-MG | | 1 | 20 | | | | | | | | 30 | 5 | | | | | | |
| 102 | 104 | 2 | 25 | LMND XTAL TUFF | | F-MG | | 15 | 20 | | | | | | | | 30 | 5 | | | | | | |
| 104 | 106 | 2 | 28 | LMND XTAL TUFF | | F-MG | | 10 | 20 | | | | | | | | 30 | 5 | | | .1 | | | |
| 106 | 108 | 2 | 36 | DCIT LPLL TUFF | | F-MG | | 1 | 15 | | 10 | | | | | | 30 | 6 | | | | | | |
| 108 | 110 | 2 | 31 | LMND LPLL TUFF | | F-MG | | 2 | 15 | | 5 | | | | | | 30 | 6 | | | | | | |
| 110 | 112 | 2 | 21 | LMND LPLL TUFF | | F-MG | | | 20 | 1 | 8 | | | | | | 30 | 7 | .1 | | .2 | | | |
| 112 | 114 | 2 | 24 | LMND LPLL TUFF | | F-MG | | 1 | 15 | 1 | 10 | 1 | | | | | 40 | 7 | .1 | | .2 | | | |
| 114 | 115.25 | 1.25 | 24 | LMND LPLL TUFF | | F-MG | | | 15 | 3 | 8 | 1 | | | | | 45 | 8 | | | .5 | | | |
| 115.25 | 116.5 | 1.25 | 30 | LMND LPLL TUFF | | F-MG | | | 25 | 3 | 8 | 1 | | | | | 45 | 12 | | | .1 | | | |
| 116.5 | 118.5 | 2 | 10 | FAULT LPLL TUFF | | VFG | | | 80 | 10 | 1 | | | | | | 95 | 12 | | | .2 | | | |
| 118.5 | 120.5 | 2 | 15 | FAULT LPLL TUFF | | VFG | 3 | 10 | 65 | 1 | | | | | | | 95 | 20 | | | .5 | | | |
| 120.5 | 122.5 | 2 | 36 | LMND XTAL TUFF | | VFG | | 1 | 25 | | 3 | | | | | | 35 | 12 | | | .5 | | | |
| 122.5 | 124.5 | 2 | 40 | LMND XTAL TUFF | | VFG | | .5 | 25 | | 3 | | | | | | 38 | 15 | | | .5 | | | |
| 124.5 | 126.5 | 2 | 39 | LMND XTAL TUFF | | VFG | | .5 | 40 | 1 | 3 | | | | | | 45 | 15 | .5 | | .3 | | | |
| 126.5 | 128.5 | 2 | 33 | LMND XTAL TUFF | | VFG | | 1 | 35 | | 5 | | | | | | 40 | 15 | | | .1 | | | |
| 128.5 | 130.5 | 2 | 16 | LMND XTAL TUFF | | VFG | | .5 | 35 | 1 | 5 | | | | | | 40 | 15 | | | .3 | | | |
| 130.5 | 132.5 | 2 | 39 | LMND XTAL TUFF | | VFG | | 2 | 25 | | 10 | | | | | | 35 | 15 | | | | | | |
| 132.5 | 133.73 | 1.23 | 37 | LMND XTAL TUFF | | VFG | | 20 | 20 | | 8 | | | | | | 40 | 15 | | | .5 | | | |
| 133.73 | 135.73 | 2.0 | 43 | ANDS DYKE | | FG | | .1 | 15 | | 5 | | | | | | 20 | 1 | | | | | | |
| 135.73 | 137.66 | 1.93 | 43 | ANDS DYKE | | FG | | .1 | 15 | | 5 | | | | | | 20 | 1 | | | | | | |
| 137.66 | 139.66 | 2 | 35 | LPLL XTAL TUFF | | F-MG | | | 30 | | 5 | | | | | | 40 | 8 | | | .5 | | | |
| 139.66 | 141.66 | 2 | 42 | LPLL XTAL TUFF | | F-MG | | | 30 | | 3 | | | | | | 40 | 10 | | | .1 | | | |
| 141.66 | 143.66 | 2 | 13 | LPLL XTAL TUFF | | F-MG | | 3 | 55 | 1 | 2 | | | | | | 70 | 15 | | | .8 | | | |
| 143.66 | 145.66 | 2 | 33 | LPLL XTAL TUFF | | F-MG | | .5 | 30 | | 5 | | | | | | 40 | 8 | .1 | | .5 | | | |
| 145.66 | 147.66 | 2 | 46 | LPLL XTAL TUFF | | F-MG | | 2 | 30 | | 5 | | | | | | 40 | 15 | .1 | | .2 | | | |
| 147.66 | 149.66 | 2 | 32 | LPLL XTAL TUFF | | F-MG | 2 | 1 | 30 | | 5 | | | | | | 40 | 15 | | | .5 | | | |
| 149.66 | 151.66 | 2 | 33 | LPLL XTAL TUFF | | F-MG | .5 | 1 | 50 | | 3 | | | | | | 55 | 12 | .5 | | .8 | | | |
| 151.66 | 153.66 | 2 | 34 | LPLL XTAL TUFF | | F-MG | 2 | 1 | 55 | | 3 | .5 | | | | | 65 | 8 | | | .8 | | | |
| 153.66 | 155.66 | 2 | 28 | LPLL XTAL TUFF | | F-MG | 1 | .5 | 40 | .5 | 5 | .5 | | | | | 50 | 10 | | | 1 | | | |
| 155.66 | 157.66 | 2 | 33 | LPLL XTAL TUFF | | F-MG | | .5 | 35 | .5 | 7 | | | | | | 45 | 12 | | | .5 | | | |
| 157.66 | 159.66 | 2 | 29 | LPLL XTAL TUFF | | F-MG | | .5 | 35 | .5 | 5 | | | | | | 45 | 17 | | | .8 | | | |
| 159.66 | 161.66 | 2 | 34 | LPLL XTAL TUFF | | F-MG | | 1 | 35 | 1 | 8 | | | | | | 45 | 12 | .1 | | .5 | | | |
| 161.66 | 163.66 | 2 | 31 | LPLL XTAL TUFF | | F-MG | | 1 | 40 | 1 | 3 | | | | | | 60 | 8 | | | .1 | | | |
| 163.66 | 164.66 | 1 | 10 | LPLL XTAL TUFF | | F-MG | | 15 | 60 | | 1 | | | | | | 85 | 10 | | | | | | |
| 164.66 | 165.66 | 1 | 39 | PLAG PRPH | | F-MG | | 2 | 5 | | 3 | | | | | | 15 | .5 | | | | | | |
| 165.66 | 168.3 | 1.64 | 35 | PLAG PRPH | | F-MG | | .5 | 5 | | 5 | | | | | | 15 | .5 | | | | | | |
| 168.3 | 169.3 | 2 | 38 | PLAG PRPH | | F-MG | | 2 | 5 | 1 | 5 | | | | | | 15 | .5 | | | | | | |
| 169.3 | 171.3 | 2 | 32 | PLAG PRPH | | F-MG | | 1 | 5 | 1 | 5 | | | | | | 15 | .5 | | | | | | |
| 171.3 | 173.3 | 2 | 48 | PLAG PRPH | | F-MG | | 6 | 3 | 2 | 5 | | | | | | 18 | .5 | | | .1 | | | |
| 172.3 | 174.9 | 1.6 | 41 | PLAG PRPH | | F-MG | | 2 | 7 | 4 | 3 | | | | | | 25 | .5 | | | | | | |
| 174.9 | 176.17 | 1.27 | 22 | FAULT LPLL TUFF | | F-MG | 2 | 8 | 35 | | 8 | | | | | | 45 | 18 | | | .1 | | | |
| 176.17 | 178.0 | 1.83 | 24 | FAULT SRCT SCST | | F-MG | | 15 | 55 | | | | | | | | 100 | 25 | .8 | | .5 | | | |
| 178 | 180 | 2 | 23 | FAULT SRCT SCST | | F-MG | | 10 | 60 | 2 | | | | | | | 100 | 25 | 1.5 | | .5 | | | |
| 180 | 182 | 2 | 19 | FAULT SRCT SCST | | F-MG | | 8 | 60 | 4 | | | | | | | 100 | 25 | 1 | | .5 | | | |
| 182 | 184 | 2 | 22 | FAULT SRCT SCST | | F-MG | | 12 | 50 | 2 | | | | | | | 100 | 20 | 1 | | .5 | | | |
| 184 | 186 | 2 | 19 | FAULT SRCT SCST | | F-MG | | 9 | 60 | 4 | | | | | | | 100 | 20 | 1.5 | | .5 | | | |
| 186 | 188 | 2 | 14 | FAULT SRCT SCST | | F-MG | | 9 | 70 | | | | | | | | 100 | 20 | .2 | | .5 | | | |
| 188 | 190 | 2 | 10 | FAULT SRCT SCST | | F-MG | | 4 | 65 | | | | | | | | 100 | 27 | .1 | | 2 | | | |
| 190 | 192 | 2 | 10 | FAULT SRCT SCST | | FG | | 2 | 70 | | | | | | | | 100 | 25 | .1 | | 2 | | | |
| 192 | 194 | 2 | 10 | FAULT SRCT SCST | | FG | | 2 | 70 | | | | | | | | 100 | 25 | .1 | | 1.5 | | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 881 | 9632.3 | 9715.6 | 1712 | 90 | 62 | 272.80 | | Intersect B Zone ;Chargeability High ; X-Section #HOL |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 194 | 196 | 2 | 14 | FAULT SRCT SCST | | FG | | 8 | 65 | 2 | 1 | | | | | | 100 | 22 | | | 1 | | | |
| 196 | 198 | 2 | 22 | FAULT SRCT SCST | | FG | 5 | 30 | 35 | | | | | | | | 100 | 25 | .8 | | 1 | | | |
| 198 | 200 | 2 | 22 | FAULT SRCT SCST | | FG | 2 | 20 | 48 | | | | | | | | 100 | 25 | 1 | | 1.5 | | | |
| 200 | 202 | 2 | 22 | FAULT SRCT SCST | | FG | 1 | 5 | 65 | | | | | | | | 100 | 22 | | | 2 | | | |
| 202 | 204 | 2 | 18 | FAULT SRCT SCST | | FG | 5 | 15 | 50 | | 2 | | | | | | 100 | 22 | .5 | | 3 | | | |
| 204 | 206 | 2 | 27 | FAULT SRCT SCST | | FG | 2 | 8 | 40 | | 5 | | | | | | 100 | 20 | .1 | | 3 | | | |
| 206 | 208 | 2 | 23 | FAULT SRCT SCST | | FG | 5 | 10 | 40 | | 5 | | | | | | 100 | 20 | .5 | | 3 | | | |
| 208 | 210 | 2 | 24 | FAULT SRCT SCST | | FG | 5 | 30 | 35 | | | | | | | | 100 | 25 | .1 | | 3 | | | |
| 210 | 212 | 2 | 19 | FAULT SRCT SCST | | FG | 5 | 30 | 35 | | | | | | | | 100 | 25 | .1 | | 3 | | | |
| 212 | 214 | 2 | 19 | FAULT SRCT SCST | | FG | 3 | 30 | 35 | | | | | | | | 100 | 25 | 2 | | 5 | | | |
| 214 | 216 | 2 | 19 | FAULT SRCT SCST | | FG | 3 | 30 | 30 | | | | | | | | 90 | 22 | .5 | | 5 | | | |
| 216 | 218 | 2 | 21 | FAULT SRCT SCST | | FG | 3 | 30 | 35 | | | | | | | | 100 | 25 | 2 | | 5 | | | |
| 218 | 220 | 2 | 19 | FAULT SRCT SCST | | FG | 3 | 30 | 35 | | | | | | | | 100 | 25 | 2 | | 5 | 0.1 | | |
| 220 | 222 | 2 | 19 | FAULT SRCT SCST | | FG | 2 | 25 | 40 | | | | | | | | 100 | 25 | 2 | | 5 | | | |
| 222 | 224 | 2 | 19 | FAULT SRCT SCST | | FG | | 15 | 55 | 2 | | | | | | | 100 | 20 | .1 | | 3 | | | |
| 224 | 226 | 2 | 22 | FAULT SRCT SCST | | FG | | 55 | 10 | | | | | | | | 100 | 30 | 2 | | 3 | | | |
| 226 | 228.25 | 2.25 | 28 | FAULT SRCT SCST | | FG | | 45 | 24 | | | | | | | | 100 | 25 | 1 | | 5 | | | |
| 228.25 | 230 | 1.75 | 28 | ANDS DYKE | | VFG | | | 15 | 5 | 20 | | | | | | 40 | .5 | | | | | | |
| 230 | 232 | 2 | 37 | ANDS DYKE | | VFG | | 1 | 15 | 5 | 20 | | | | | | 40 | .5 | | | | | | |
| 232 | 234 | 2 | 23 | ANDS DYKE | | VFG | | 8 | 15 | 5 | 20 | | | | | | 50 | 1 | | | | | | |
| 234 | 236 | 2 | 20 | FAULT SCRT SCST | | FG | | 35 | 25 | 2 | | | | | | | 100 | 30 | 2 | | 5 | | | |
| 236 | 238 | 2 | 13 | FAULT SCRT SCST | | FG | | 30 | 25 | 2 | | | | | | | 100 | 25 | 1 | | 5 | | | |
| 238 | 240 | 2 | 17 | FAULT SCRT SCST | | FG | | 35 | 38 | | | | | | | | 100 | 22 | .5 | | 3 | | | |
| 240 | 242 | 2 | 17 | FAULT SCRT SCST | | FG | | 35 | 35 | | | | | | | | 100 | 22 | 1 | | 5 | | | |
| 242 | 244 | 2 | 17 | FAULT SCRT SCST | | FG | | 35 | 40 | | | | | | | | 100 | 20 | .5 | | 3 | | | |
| 244 | 246 | 2 | 17 | FAULT SCRT SCST | | FG | | 25 | 60 | 1 | | | | | | | 100 | 18 | .1 | | 2 | | | |
| 246 | 248 | 2 | 17 | FAULT SCRT SCST | | FG | | 25 | 45 | | | | | | | | 100 | 20 | .5 | | 5 | | | |
| 248 | 250 | 2 | 13 | FAULT SCRT SCST | | FG | | 15 | 55 | | | | | | | | 100 | 20 | .1 | | 5 | | | |
| 250 | 252 | 2 | 10 | FAULT SCRT SCST | | FG | | 15 | 55 | | | | | | | | 100 | 20 | .1 | | 5 | | | |
| 252 | 254 | 2 | 20 | FAULT SCRT SCST | | FG | | 15 | 55 | | | | | | | | 100 | 18 | .1 | | 5 | | | |
| 254 | 256 | 2 | 20 | FAULT SCRT SCST | | FG | | 10 | 60 | 1 | | | | | | | 100 | 15 | | | 4 | | | |
| 256 | 258 | 2 | 12 | FAULT SCRT SCST | | FG | | 3 | 60 | 5 | | 1 | | | | | 100 | 20 | .2 | | 4 | | | |
| 258 | 260 | 2 | 12 | FAULT SCRT SCST | | FG | | 2 | 65 | 5 | | | | | | | 100 | 15 | | | 3 | | | |
| 260 | 262 | 2 | 13 | FAULT SCRT SCST | | FG | | 1 | 65 | 10 | | | | | | | 90 | 15 | .1 | | 2 | | | |
| 262 | 264 | 2 | 10 | FAULT SCRT SCST | | FG | | 3 | 60 | 10 | | | | | | | 100 | 20 | | | 5 | | | |
| 264 | 266 | 2 | 12 | FAULT SCRT SCST | | FG | | 5 | 45 | 8 | | | | | | | 100 | 30 | .2 | | 7 | | | |
| 266 | 268 | 2 | 10 | FAULT SCRT SCST | | FG | | 3 | 60 | 3 | | | | | | | 100 | 25 | | | 3 | | | |
| 268 | 270 | 2 | 10 | FAULT SCRT SCST | | FG | | 2 | 65 | 1 | | | | | | | 100 | 22 | | | 2 | | | |
| 270 | 272.80 | 2.80 | 15 | FAULT SCRT SCST | | FG | | 2 | 65 | 3 | | | | | | | 100 | 20 | | | 4 | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 07:06:26 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | # |
|---|---|---|---|---|---|---|---|---|---|
| 881 | 9632.3 | 9715.6 | 1712 | 90 | 62 | 272.80 | | Intersect B Zone ;Chargeability High ; X-Section | #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | 1.52 | | 1.52 | 0 | | | | | | | | | | | |
| 1.52 | 3.52 | 9001 | 2 | 1.96 | 230 | | .3 | | 1689 | 169 | 5.79 | 65 | 983 | | |
| 3.52 | 5.52 | 9002 | 2 | 1.94 | 390 | | .4 | | 2449 | 87 | 6.27 | 61 | 1092 | | |
| 5.52 | 7.52 | 9003 | 2 | 1.8 | 110 | | .1 | | 1456 | 64 | 5.07 | 25 | 817 | | |
| 7.52 | 9.84 | 9004 | 2.32 | 2.24 | 225 | | .1 | | 1104 | 49 | 4.91 | 42 | 432 | | |
| 9.84 | 12.14 | 9005 | 2.3 | 1.26 | 80 | | .1 | | 258 | 108 | 4.3 | 2 | 1450 | | |
| 12.14 | 14.44 | 9006 | 2.3 | 1.56 | 80 | | .1 | | 216 | 131 | 3.97 | 2 | 1677 | | |
| 14.44 | 15.95 | 9007 | 1.51 | 1.42 | 225 | | .1 | | 135 | 14 | 2.66 | 25 | 74 | | |
| 15.95 | 17.46 | 9008 | 1.51 | 1.48 | 100 | | .1 | | 58 | 10 | 1.54 | 21 | 46 | | |
| 17.46 | 18.97 | 9009 | 1.51 | 1.48 | 160 | | .1 | | 107 | 12 | 2.66 | 43 | 37 | | |
| 18.97 | 20.97 | 9010 | 2 | 1.23 | 110 | | .1 | | 241 | 19 | 3.82 | 56 | 50 | | |
| 20.97 | 22.97 | 9011 | 2.02 | 1.93 | 200 | | .4 | | 199 | 29 | 4.01 | 99 | 33 | | |
| 22.97 | 25 | 9012 | 2.03 | 1.93 | 20 | | .1 | | 791 | 44 | 3.17 | 40 | 30 | | |
| 25 | 27 | 9013 | 2 | 1.91 | 150 | | .3 | | 358 | 15 | 2.79 | 50 | 22 | | |
| 27 | 28.6 | 9014 | 1.6 | 1.58 | 180 | | .4 | | 871 | 49 | 5.75 | 74 | 112 | | |
| 28.6 | 29.8 | 9015 | 1.2 | 1.15 | 105 | | .4 | | 3847 | 78 | 4.14 | 86 | 365 | | |
| 29.8 | 31.01 | 9016 | 1.21 | 1.2 | 125 | | .8 | | 2576 | 81 | 3.74 | 66 | 251 | | |
| 31.01 | 33 | 9017 | 1.99 | 1.85 | 170 | | .4 | | 511 | 109 | 6.60 | 28 | 476 | | |
| 33 | 35 | 9018 | 2 | 1.99 | 80 | | .1 | | 284 | 59 | 4.27 | 29 | 363 | | |
| 35 | 38.06 | 8413 | 3.06 | 3.0 | 100 | | .3 | | 353 | 114 | 4.37 | 26 | 680 | | |
| 38.06 | 41.13 | 8414 | 3.07 | 3 | 65 | | .3 | | 384 | 172 | 4.35 | 24 | 1083 | | |
| 41.13 | 43.13 | 9019 | 2 | 1.96 | 150 | | .8 | | 5187 | 139 | 4.2 | 67 | 286 | | |
| 45.13 | 45.13 | 9020 | 2 | 1.91 | 110 | | .1 | | 2022 | 111 | 4.55 | 87 | 265 | | |
| 47.13 | 47.13 | 9021 | 2 | 1.58 | 40 | | .1 | | 2115 | 88 | 4.45 | 35 | 81 | | |
| 49 | 49.13 | 9022 | 2 | 1.15 | 1 | | .1 | | 1617 | 258 | 5.37 | 75 | 233 | | |
| 13 | 50.48 | 9023 | 1.35 | 1.2 | 45 | | .1 | | 3081 | 115 | 4.14 | 85 | 163 | | |
| 50.48 | 52.48 | 9024 | 2 | 1.85 | 85 | | .1 | | 1250 | 22 | 3.97 | 71 | 29 | | |
| 52.48 | 54.48 | 9025 | 2 | 1.99 | 30 | | .1 | | 681 | 34 | 5.41 | 35 | 172 | | |
| 54.48 | 55.91 | 9026 | 1.43 | 1.27 | 1 | | .1 | | 432 | 39 | 4.01 | 42 | 197 | | |
| 55.91 | 57.34 | 9027 | 1.43 | 1.27 | 40 | | .1 | | 1622 | 24 | 6.86 | 37 | 131 | | |
| 57.34 | 58.77 | 9028 | 1.43 | 1.09 | 50 | | .1 | | 969 | 14 | 7.25 | 50 | 38 | | |
| 58.77 | 60.27 | 9029 | 1.5 | 1.39 | 50 | | .1 | | 1492 | 18 | 6.07 | 40 | 48 | | |
| 60.27 | 61.77 | 9030 | 1.5 | 1.29 | 55 | | .1 | | 1845 | 36 | 6.48 | 82 | 58 | | |
| 61.77 | 63.29 | 9031 | 1.52 | 1.44 | 230 | | 1.1 | | 4705 | 79 | 5.05 | 49 | 676 | | |
| 63.29 | 65.45 | 9032 | 2.16 | 1.54 | 105 | | .1 | | 1739 | 238 | 5.16 | 17 | 1666 | | |
| 65.45 | 67.62 | 9033 | 2.17 | 1.65 | 150 | | .8 | | 1138 | 51 | 4.55 | 33 | 341 | | |
| 67.62 | 68.78 | 9034 | 1.16 | 0.98 | 295 | | 1.6 | | 2043 | 148 | 4.76 | 57 | 854 | | |
| 68.78 | 69.95 | 9035 | 1.17 | 0.94 | 225 | | 1.6 | | 2785 | 303 | 3 | 83 | 284 | | |
| 69.95 | 72.05 | 9036 | 2.1 | 1.28 | 50 | | .8 | | 1399 | 158 | 4.3 | 2 | 30 | | |
| 72.05 | 74 | 9037 | 1.95 | 1.8 | 90 | | .8 | | 1475 | 88 | 4.26 | 174 | 381 | | |
| 74 | 76 | 9038 | 2 | 1.75 | 70 | | .8 | | 1224 | 49 | 4.12 | 76 | 154 | | |
| 76 | 78 | 9039 | 2 | 1.83 | 110 | | .8 | | 755 | 38 | 5.27 | 67 | 160 | | |
| 78 | 78.64 | 9040 | .64 | 0.6 | 180 | | .5 | | 2154 | 40 | 6.83 | 85 | 205 | | |
| 78.64 | 80 | 9041 | 1.36 | 1.34 | 50 | | .1 | | 835 | 14 | 7.94 | 45 | 36 | | |
| 80 | 82 | 9042 | 2 | 1.88 | 30 | | .1 | | 918 | 24 | 7.05 | 62 | 33 | | |
| 82 | 84 | 9043 | 2 | 1.96 | 1 | | .1 | | 516 | 13 | 6.76 | 41 | 34 | | |
| 84 | 86 | 9044 | 2 | 1.9 | 40 | | .1 | | 1020 | 9 | 6.37 | 28 | 34 | | |
| 86 | 88.9 | 9045 | 2 | 1.88 | 250 | | .3 | | 582 | 36 | 5.99 | 37 | 473 | | |
| 88 | 90 | 9046 | 2 | 1.9 | 30 | | .1 | | 440 | 36 | 6.2 | 31 | 220 | | |
| 90 | 92 | 9047 | 2 | 1.33 | 1 | | .1 | | 586 | 32 | 7.06 | 29 | 186 | | |
| 92 | 94 | 9048 | 2 | 1.6 | 35 | | .1 | | 1007 | 65 | 6.85 | 40 | 345 | | |
| 94 | 96 | 9049 | 2 | 1.96 | 65 | | .1 | | 1008 | 107 | 6.88 | 33 | 182 | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | # |
|---|---|---|---|---|---|---|---|---|---|
| 881 | 9632.3 | 9715.6 | 1712 | 90 | 62 | 272.80 | | Intersect B Zone ;Chargeability High ; X-Section | #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 96 | 98 | 9050 | 2 | 1.89 | 45 | | .1 | | 654 | 75 | 6.25 | 63 | 47 | | |
| 98 | 100 | 9051 | 2 | 1.80 | 40 | | .1 | | 1064 | 78 | 6.41 | 115 | 81 | | |
| 100 | 102 | 9052 | 2 | 1.87 | 130 | | .1 | | 874 | 29 | 6.25 | 53 | 31 | | |
| 102 | 104 | 9053 | 2 | 1.80 | 30 | | .1 | | 769 | 44 | 6.79 | 69 | 77 | | |
| 104 | 106 | 9054 | 2 | 1.98 | 20 | | .1 | | 2186 | 199 | 8.33 | 133 | 2085 | | |
| 106 | 108 | 9055 | 2 | 1.99 | 30 | | .1 | | 613 | 79 | 6.15 | 63 | 476 | | |
| 108 | 110 | 9056 | 2 | 1.83 | 10 | | .1 | | 618 | 111 | 6.15 | 76 | 635 | | |
| 110 | 112 | 9057 | 2 | 1.87 | 10 | | .1 | | 1184 | 171 | 6.25 | 75 | 273 | | |
| 112 | 114 | 9058 | 2 | 1.89 | 1 | | .1 | | 617 | 123 | 5 | 88 | 1198 | | |
| 114 | 115.25 | 9059 | 1.25 | 1.14 | 30 | | .1 | | 1218 | 246 | 6.19 | 117 | 2112 | | |
| 115.25 | 116.5 | 9060 | 1.25 | 1.10 | 30 | | .1 | | 873 | 150 | 5.59 | 130 | 805 | | |
| 116.5 | 118.5 | 9061 | 2 | 1.51 | 50 | | .3 | | 873 | 288 | 7.01 | 136 | 98 | | |
| 118.5 | 120.5 | 9062 | 2 | 1.08 | 90 | | .1 | | 396 | 173 | 10.0 | 80 | 975 | | |
| 120.5 | 122.5 | 9063 | 2 | 1.81 | 90 | | .1 | | 399 | 69 | 6.58 | 52 | 490 | | |
| 122.5 | 124.5 | 9064 | 2 | 1.98 | 40 | | .1 | | 309 | 101 | 6.75 | 40 | 868 | | |
| 124.5 | 126.5 | 9065 | 2 | 1.96 | 40 | | .6 | | 516 | 177 | 6.49 | 70 | 1968 | | |
| 126.5 | 128.5 | 9066 | 2 | 1.93 | 140 | | 2.7 | | 506 | 365 | 6.07 | 68 | 468 | | |
| 128.5 | 130.5 | 9067 | 2 | 1.90 | 310 | | .3 | | 512 | 165 | 6.08 | 77 | 327 | | |
| 130.5 | 132.5 | 9068 | 2 | 1.95 | 1 | | .1 | | 525 | 121 | 7.08 | 68 | 370 | | |
| 132.5 | 133.73 | 9069 | 1.23 | 1.14 | 140 | | .1 | | 771 | 659 | 4.8 | 75 | 4087 | | |
| 133.73 | 135.73 | 8415 | 2.0 | 1.81 | 100 | | .1 | | 47 | 132 | 3.67 | 64 | 1629 | | |
| 135.73 | 137.66 | 8416 | 1.93 | 1.8 | 5 | | .1 | | 75 | 173 | 3.70 | 21 | 1947 | | |
| 137.66 | 139.66 | 9070 | 2 | 2.00 | 40 | | .1 | | 363 | 57 | 3.95 | 826 | 204 | | |
| 139.66 | 141.66 | 9071 | 2 | 2.00 | 80 | | .1 | | 786 | 78 | 6.39 | 74 | 195 | | |
| 141.66 | 143.66 | 9072 | 2 | 1.95 | 40 | | .1 | | 644 | 116 | 5.41 | 63 | 1171 | | |
| 143.66 | 145.66 | 9073 | 2 | 1.87 | 55 | | .1 | | 411 | 132 | 5.69 | 42 | 382 | | |
| 145.66 | 147.66 | 9074 | 2 | 1.96 | 40 | | .1 | | 696 | 175 | 6.17 | 74 | 846 | | |
| 147.66 | 149.66 | 9075 | 2 | 1.76 | 50 | | .1 | | 656 | 283 | 6.4 | 51 | 610 | | |
| 149.66 | 151.66 | 9076 | 2 | 1.89 | 500 | | .1 | | 487 | 165 | 5.91 | 46 | 890 | | |
| 151.66 | 153.66 | 9077 | 2 | 1.78 | 180 | | .1 | | 903 | 136 | 5.01 | 43 | 1593 | | |
| 153.66 | 155.66 | 9078 | 2 | 1.80 | 150 | | .1 | | 313 | 307 | 6.16 | 51 | 2272 | | |
| 155.66 | 157.66 | 9079 | 2 | 1.83 | 1 | | .1 | | 472 | 470 | 5.45 | 118 | 2036 | | |
| 157.66 | 159.66 | 9080 | 2 | 1.97 | 200 | | .2 | | 657 | 272 | 5.66 | 100 | 997 | | |
| 159.66 | 161.66 | 9081 | 2 | 1.95 | 70 | | .1 | | 833 | 132 | 6.41 | 161 | 595 | | |
| 161.66 | 163.66 | 9082 | 2 | 1.82 | 120 | | .1 | | 1212 | 258 | 4.79 | 179 | 1732 | | |
| 163.66 | 164.66 | 9083 | 1 | 0.92 | 80 | | .4 | | 858 | 141 | 4.26 | 214 | 1637 | | |
| 164.66 | 165.66 | 9084 | 1 | 0.92 | 55 | | .1 | | 53 | 99 | 2.49 | 3 | 1492 | | |
| 165.66 | 168.3 | 8417 | 1.64 | 2.36 | 1 | | .1 | | 12 | 139 | 2.82 | 3 | 1227 | | |
| 168.3 | 169.3 | 9085 | 2 | 0.89 | 1 | | .1 | | 329 | 293 | 4.12 | 3 | 2771 | | |
| 169.3 | 171.3 | 9086 | 2 | 1.62 | 1 | | .1 | | 289 | 313 | 3.95 | 8 | 2753 | | |
| 171.3 | 173.3 | 9087 | 2 | 1.78 | 1 | | .1 | | 43 | 236 | 2.97 | 3 | 1923 | | |
| 172.3 | 174.9 | 9088 | 1.6 | 1.51 | 30 | | .1 | | 643 | 266 | 3.95 | 5 | 2132 | | |
| 174.9 | 176.17 | 9089 | 1.27 | 1.09 | 90 | | .1 | | 1024 | 291 | 3.64 | 5 | 2430 | .11 | |
| 176.17 | 178.0 | 9090 | 1.83 | 1.14 | 350 | | 3.1 | | 9081 | 126 | 7.5 | 119 | 129 | 1.03 | |
| 178 | 180 | 9091 | 2 | 1.43 | 490 | | 2.9 | | 10895 | 94 | 9.42 | 43 | 400 | 1.15 | |
| 180 | 182 | 9092 | 2 | 1.95 | 370 | | 2.9 | | 12894 | 55 | 6.68 | 18 | 649 | 1.22 | |
| 182 | 184 | 9093 | 2 | 1.39 | 440 | | 2.2 | | 14999 | 29 | 7.5 | 11 | 85 | 1.44 | |
| 184 | 186 | 9094 | 2 | 1.10 | 340 | | 3.2 | | 16351 | 99 | 7.79 | 16 | 113 | 1.64 | |
| 186 | 188 | 9095 | 2 | 0.70 | 330 | | 3.1 | | 15812 | 18 | 7.41 | 17 | 35 | 1.48 | |
| 188 | 190 | 9096 | 2 | 0.90 | 270 | | 2.2 | | 14029 | 28 | 9.19 | 203 | 27 | 1.22 | |
| 190 | 192 | 9097 | 2 | 1.12 | 220 | | 1.5 | | 11981 | 14 | 6.94 | 46 | 23 | 1.16 | |
| 192 | 194 | 9098 | 2 | 1.12 | 210 | | .8 | | 8763 | 26 | 8.14 | 16 | 35 | .77 | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | # |
|---|---|---|---|---|---|---|---|---|---|
| 881 | 9632.3 | 9715.6 | 1712 | 90 | 62 | 272.80 | | Intersect B Zone ;Chargeability High ; X-Section | #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 194 | 196 | 9099 | 2 | 1.30 | 315 | | 1.5 | | 11059 | 95 | 7.98 | 11 | 139 | 1 | |
| 196 | 198 | 9100 | 2 | 1.09 | 290 | | 4.1 | | 14095 | 308 | 8.41 | 427 | 172 | 1.47 | |
| 198 | 200 | 9101 | 2 | 0.81 | 410 | | 4.3 | | 12522 | 228 | 7.83 | 578 | 111 | 1.17 | |
| 200 | 202 | 9102 | 2 | 1.12 | 180 | | .8 | | 8440 | 114 | 5.47 | 71 | 193 | .78 | |
| 202 | 204 | 9103 | 2 | 0.73 | 390 | | 2.9 | | 14748 | 88 | 7.44 | 19 | 294 | 1.48 | |
| 204 | 206 | 9104 | 2 | 0.62 | 390 | | 2.5 | | 13942 | 121 | 5.37 | 11 | 503 | 1.38 | |
| 206 | 208 | 9105 | 2 | 0.59 | 300 | | 1.8 | | 12515 | 116 | 6.17 | 18 | 489 | .98 | |
| 208 | 210 | 9106 | 2 | 0.39 | 1 | | 3.5 | | 19117 | 49 | 7.9 | 17 | 275 | 1.51 | |
| 210 | 212 | 9107 | 2 | 0.27 | 1 | | 3.4 | | 20000 | 42 | 6.69 | 19 | 241 | 2.01 | |
| 212 | 214 | 9108 | 2 | 0.79 | 420 | | 1.8 | | 14090 | 50 | 6.22 | 20 | 91 | 1.21 | |
| 214 | 216 | 9109 | 2 | 1.00 | 250 | | 1.7 | | 9478 | 56 | 5.39 | 20 | 100 | 1.01 | |
| 216 | 218 | 9110 | 2 | 0.71 | 400 | | 1.8 | | 9591 | 28 | 5.3 | 13 | 41 | .91 | |
| 218 | 220 | 9111 | 2 | 0.99 | 350 | | 2.1 | | 10562 | 38 | 5.22 | 25 | 21 | 1.09 | |
| 220 | 222 | 9112 | 2 | 0.84 | 330 | | 2.7 | | 11540 | 121 | 4.24 | 170 | 68 | 1.14 | |
| 222 | 224 | 9113 | 2 | 1.60 | 480 | | 2.7 | | 12657 | 101 | 5.39 | 29 | 688 | 1.2 | |
| 224 | 226 | 9114 | 2 | 1.73 | 1 | | 3.2 | | 14427 | 136 | 7.03 | 56 | 1172 | 1.32 | |
| 226 | 228.25 | 9115 | 2.25 | 1.80 | 370 | | 2.5 | | 9495 | 192 | 5.83 | 32 | 1029 | 1 | |
| 228.25 | 230 | 9116 | 1.75 | 1.65 | 60 | | .1 | | 1027 | 369 | 10 | 22 | 2666 | .07 | |
| 230 | 232 | 9117 | 2 | 1.79 | 20 | | .1 | | 779 | 297 | 10 | 7 | 3385 | .06 | |
| 232 | 234 | 9118 | 2 | 1.60 | 160 | | .1 | | 1396 | 404 | 10 | 23 | 3404 | .15 | |
| 234 | 236 | 9119 | 2 | 1.08 | 340 | | 2.7 | | 11596 | 211 | 6.96 | 42 | 207 | 1.21 | |
| 236 | 238 | 9120 | 2 | 1.11 | 280 | | 2.7 | | 8797 | 161 | 6.24 | 141 | 547 | 1.01 | |
| 238 | 240 | 9121 | 2 | 0.75 | 330 | | 3.2 | | 11148 | 201 | 7.09 | 481 | 425 | 1.09 | |
| 240 | 242 | 9122 | 2 | 1.48 | 450 | | 4.1 | | 16501 | 106 | 6.75 | 181 | 79 | 1.59 | |
| 242 | 244 | 9123 | 2 | 0.88 | 405 | | 4.8 | | 12932 | 366 | 6 | 544 | 49 | 1.22 | |
| 244 | 246 | 9124 | 2 | 0.84 | 240 | | 3.1 | | 8657 | 75 | 5.97 | 96 | 296 | .88 | |
| 246 | 248 | 9125 | 2 | 0.85 | 220 | | 2.2 | | 8457 | 195 | 6.01 | 54 | 183 | .8 | |
| 248 | 250 | 9126 | 2 | 0.70 | 280 | | 1.7 | | 6002 | 189 | 6.3 | 21 | 938 | .65 | |
| 250 | 252 | 9127 | 2 | 0.44 | 310 | | 1.7 | | 8682 | 128 | 6.24 | 13 | 982 | .85 | |
| 252 | 254 | 9128 | 2 | 1.16 | 130 | | 1.2 | | 1462 | 142 | 7.3 | 27 | 670 | .11 | |
| 254 | 256 | 9129 | 2 | 1.20 | 90 | | .3 | | 1706 | 137 | 6.1 | 25 | 604 | .18 | |
| 256 | 258 | 9130 | 2 | 1.40 | 130 | | .5 | | 2912 | 144 | 6.22 | 42 | 554 | .28 | |
| 258 | 260 | 9131 | 2 | 1.50 | 1 | | .1 | | 2373 | 110 | 5.5 | 76 | 445 | .2 | |
| 260 | 262 | 9132 | 2 | 1.56 | 80 | | .3 | | 2244 | 247 | 6.12 | 148 | 282 | .18 | |
| 262 | 264 | 9133 | 2 | 1.11 | 320 | | 1.8 | | 6417 | 158 | 7.2 | 605 | 48 | .51 | |
| 264 | 266 | 9134 | 2 | 1.44 | 1120 | .045 | 4.5 | | 9467 | 163 | 9.19 | 64 | 199 | .84 | |
| 266 | 268 | 9135 | 2 | 0.77 | 995 | .031 | 3.7 | | 7568 | 124 | 8.89 | 27 | 507 | .64 | |
| 268 | 270 | 9136 | 2 | 0.86 | 470 | | 1.6 | | 6819 | 59 | 6.84 | 107 | 132 | .51 | |
| 270 | 272.80 | 9137 | 2.80 | 1.20 | 420 | | 1.1 | | 5268 | 160 | 7.23 | 30 | 239 | .35 | |

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

REPORT NUMBER: 880843 AA JOB NUMBER: 880843 WESTERN CDN. MINING CORP. 

| SAMPLE # | Cu % |
|---|---|
| C88 - 9089 | .11 |
| C88 - 9090 | 1.03 |
| C88 - 9091 | 1.15 |
| C88 - 9092 | 1.22 |
| C88 - 9093 | 1.44 |
| C88 - 9094 | 1.64 |
| C88 - 9095 | 1.48 |
| C88 - 9096 | 1.22 |
| C88 - 9097 | 1.16 |
| C88 - 9098 | .77 |
| C88 - 9099 | 1.00 |
| C88 - 9100 | 1.47 |
| C88 - 9101 | 1.17 |
| C88 - 9102 | .78 |
| C88 - 9103 | 1.48 |
| C88 - 9104 | 1.38 |
| C88 - 9105 | .98 |
| C88 - 9106 | 1.51 |
| C88 - 9107 | 2.01 |
| C88 - 9108 | 1.21 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88 - 9109 | 1.01 |
| C88 - 9110 | .91 |
| C88 - 9111 | 1.09 |
| C88 - 9112 | 1.14 |
| C88 - 9113 | 1.20 |
| C88 - 9114 | 1.32 |
| C88 - 9115 | 1.00 |
| C88 - 9116 | .07 |
| C88 - 9117 | .06 |
| C88 - 9118 | .15 |
| C88 - 9119 | 1.21 |
| C88 - 9120 | 1.01 |
| C88 - 9121 | 1.09 |
| C88 - 9122 | 1.59 |
| C88 - 9123 | 1.22 |
| C88 - 9124 | .88 |
| C88 - 9125 | .80 |
| C88 - 9126 | .65 |
| C88 - 9127 | .85 |
| C88 - 9128 | .11 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
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Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88 - 9129 | .18 |
| C88 - 9130 | .28 |
| C88 - 9131 | .20 |
| C88 - 9132 | .18 |
| C88 - 9133 | .51 |
| C88 - 9134 | .84 |
| C88 - 9135 | .64 |
| C88 - 9136 | .51 |
| C88 - 9137 | .35 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656


REPORT NUMBER: 880697 AA  JOB NUMBER: 880697  WESTERN CDN. MINING CORP.  

| SAMPLE # | Au oz/st |
|---|---|
| C88 - 9134 | .045 |
| C88 - 9135 | .031 |

DETECTION LIMIT .005

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001% ppm = parts per million  < = less than

signed:

RT #: 880990 PA

WESTERN CDN MINING CORP.



| le Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| 8413 | 0.3 | 1.12 | 26 | 100 | <3 | 9 | <3 | 0.14 | 1.1 | 13 | 39 | 353 | 4.37 | 0.07 | 0.79 | 680 | 4 | 0.02 | 9 | 0.17 | 40 | <3 | <5 | <2 | 5 | 29 | <5 | <3 | 114 |
| 8414 | 0.3 | 1.58 | 24 | 65 | <3 | 33 | 3 | 0.17 | 1.1 | 10 | 33 | 384 | 4.35 | 0.07 | 1.18 | 1083 | 2 | 0.02 | 10 | 0.18 | 29 | <3 | <5 | <2 | 5 | 40 | <5 | <3 | 172 |
| 8415 | 0.1 | 2.32 | 64 | 100 | <3 | 57 | <3 | 2.86 | 0.8 | 15 | 14 | 47 | 3.67 | 0.35 | 1.95 | 1629 | 1 | 0.02 | 8 | 0.25 | 33 | <3 | <5 | <2 | 2 | 76 | <5 | <3 | 132 |
| 8416 | 0.1 | 2.39 | 21 | <5 | <3 | 59 | <3 | 3.53 | 1.2 | 13 | 20 | 75 | 3.70 | 0.41 | 2.05 | 1947 | 1 | 0.02 | 8 | 0.21 | 29 | <3 | <5 | <2 | 3 | 93 | <5 | <3 | 173 |
| 8417 | 0.1 | 1.30 | <3 | <5 | <3 | >1000 | <3 | 1.62 | 0.7 | 10 | 35 | 12 | 2.82 | 0.27 | 0.94 | 1227 | 2 | 0.02 | 6 | 0.12 | 20 | <3 | <5 | <2 | 2 | 120 | <5 | <3 | 139 |

REPORT #: 880687A PA WESTERN CANADIAN 

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C 88 - 9001 | 0.3 | 0.83 | 65 | 230 | <3 | 15 | <3 | 0.29 | 2.2 | 28 | 27 | 1689 | 5.79 | 0.02 | 0.22 | 983 | 15 | 0.01 | 13 | 0.15 | 19 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 169 |
| C 88 - 9002 | 0.4 | 1.16 | 61 | 390 | <3 | 12 | <3 | 0.29 | 1.2 | 41 | 29 | 2449 | 6.27 | 0.03 | 0.44 | 1092 | 22 | 0.01 | 25 | 0.17 | 12 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 87 |
| C 88 - 9003 | 0.1 | 1.08 | 25 | 110 | <3 | 18 | <3 | 0.29 | 1.1 | 21 | 36 | 1456 | 5.07 | 0.02 | 0.38 | 817 | 21 | 0.01 | 18 | 0.17 | 8 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 64 |
| C 88 - 9004 | 0.1 | 0.88 | 42 | 225 | <3 | 29 | <3 | 0.19 | 0.8 | 12 | 42 | 1104 | 4.91 | 0.02 | 0.22 | 432 | 30 | 0.01 | 13 | 0.20 | 8 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 49 |
| C 88 - 9005 | 0.1 | 2.27 | <3 | 80 | <3 | 630 | <3 | 0.16 | 1.1 | 12 | 34 | 258 | 4.30 | 0.01 | 1.08 | 1450 | 5 | 0.01 | 9 | 0.12 | 5 | <3 | <5 | <2 | <2 | 39 | <5 | <3 | 108 |
| C 88 - 9006 | 0.1 | 2.54 | <3 | 80 | <3 | 299 | <3 | 0.17 | 1.1 | 9 | 37 | 216 | 3.97 | 0.01 | 1.23 | 1677 | 4 | 0.01 | 9 | 0.11 | 10 | <3 | <5 | <2 | <2 | 38 | <5 | <3 | 131 |
| C 88 - 9007 | 0.1 | 0.34 | 25 | 225 | <3 | 61 | <3 | 0.01 | 0.4 | 5 | 27 | 135 | 2.66 | 0.01 | 0.05 | 74 | 38 | 0.01 | 1 | 0.06 | 19 | <3 | <5 | <2 | <2 | 27 | <5 | <3 | 14 |
| C 88 - 9008 | 0.1 | 0.40 | 21 | 100 | <3 | 103 | <3 | 0.01 | 0.3 | 3 | 41 | 58 | 1.54 | 0.01 | 0.03 | 46 | 16 | 0.01 | 1 | 0.02 | 41 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 10 |
| C 88 - 9009 | 0.1 | 0.27 | 43 | 160 | <3 | 67 | <3 | 0.01 | 0.3 | 10 | 19 | 107 | 2.66 | 0.01 | 0.03 | 37 | 20 | 0.01 | 7 | 0.07 | 17 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 12 |
| C 88 - 9010 | 0.1 | 0.44 | 56 | 110 | <3 | 57 | <3 | 0.01 | 0.6 | 10 | 47 | 241 | 3.82 | 0.01 | 0.05 | 50 | 30 | 0.01 | 7 | 0.11 | 19 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 19 |
| C 88 - 9011 | 0.4 | 0.30 | 99 | 200 | <3 | 154 | <3 | 0.01 | 0.8 | 2 | 57 | 199 | 4.01 | 0.01 | 0.02 | 33 | 36 | 0.01 | 7 | 0.56 | 35 | <3 | <5 | <2 | <2 | 35 | <5 | <3 | 29 |
| C 88 - 9012 | 0.1 | 0.39 | 40 | 20 | <3 | 21 | <3 | 0.01 | 0.8 | 17 | 42 | 791 | 3.17 | 0.01 | 0.03 | 30 | 19 | 0.01 | 13 | 0.03 | 15 | <3 | <5 | <2 | <2 | 3 | <5 | <3 | 44 |
| C 88 - 9013 | 0.3 | 0.26 | 50 | 150 | <3 | 47 | <3 | 0.01 | 0.6 | 9 | 18 | 358 | 2.97 | 0.01 | 0.02 | 22 | 57 | 0.01 | 7 | 0.10 | 27 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 15 |
| C 88 - 9014 | 0.4 | 0.63 | 74 | 180 | <3 | 77 | <3 | 0.02 | 1.1 | 7 | 42 | 871 | 5.75 | 0.01 | 0.08 | 112 | 87 | 0.01 | 4 | 0.32 | 44 | <3 | <5 | <2 | <2 | 37 | <5 | <3 | 49 |
| C 88 - 9015 | 0.4 | 1.11 | 86 | 105 | <3 | 20 | <3 | 0.15 | 0.8 | 25 | 41 | 3847 | 4.14 | 0.01 | 0.36 | 365 | 68 | 0.01 | 10 | 0.24 | 41 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 78 |
| C 88 - 9016 | 0.8 | 0.98 | 66 | 125 | <3 | 78 | <3 | 0.12 | 0.8 | 13 | 61 | 2576 | 3.74 | 0.01 | 0.17 | 251 | 53 | 0.01 | 6 | 0.24 | 49 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 81 |
| C 88 - 9017 | 0.4 | 1.10 | 28 | 170 | <3 | 93 | <3 | 0.04 | 1.3 | 8 | 19 | 511 | 6.60 | 0.01 | 0.50 | 476 | 7 | 0.01 | 4 | 0.24 | 14 | <3 | <5 | <2 | <2 | 30 | <5 | <3 | 109 |
| C 88 - 9018 | 0.1 | 0.71 | 29 | 80 | <3 | 28 | <3 | 0.11 | 0.8 | 8 | 31 | 284 | 4.27 | 0.01 | 0.34 | 363 | 4 | 0.01 | 4 | 0.11 | 14 | <3 | <5 | <2 | <2 | 37 | <5 | <3 | 59 |
| C 88 - 9019 | 0.8 | 0.96 | 67 | 150 | <3 | 23 | <3 | 0.24 | 1.6 | 20 | 49 | 5187 | 4.20 | 0.01 | 0.24 | 286 | 128 | 0.01 | 10 | 0.15 | 7 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 139 |
| C 88 - 9020 | 0.1 | 0.98 | 87 | 110 | <3 | 21 | <3 | 0.27 | 1.5 | 25 | 38 | 2022 | 4.55 | 0.02 | 0.28 | 265 | 92 | 0.01 | 13 | 0.17 | 10 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 111 |
| C 88 - 9021 | 0.1 | 0.45 | 35 | 40 | <3 | 16 | <3 | 0.17 | 1.5 | 24 | 30 | 2115 | 4.45 | 0.01 | 0.08 | 81 | 37 | 0.01 | 22 | 0.13 | 26 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 88 |
| C 88 - 9022 | 0.1 | 0.83 | 75 | <5 | <3 | 14 | <3 | 0.30 | 2.4 | 26 | 42 | 1617 | 5.37 | 0.02 | 0.20 | 233 | 23 | 0.01 | 21 | 0.17 | 22 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 258 |
| C 88 - 9023 | 0.1 | 0.71 | 85 | 45 | <3 | 17 | <3 | 0.28 | 1.2 | 21 | 43 | 3081 | 4.14 | 0.02 | 0.13 | 163 | 57 | 0.01 | 16 | 0.17 | 21 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 115 |
| C 88 - 9024 | 0.1 | 0.29 | 71 | 85 | <3 | 22 | <3 | 0.01 | 0.6 | 22 | 28 | 1250 | 3.97 | 0.01 | 0.02 | 29 | 54 | 0.01 | 12 | 0.06 | 26 | <3 | <5 | <2 | <2 | 25 | <5 | <3 | 22 |
| C 88 - 9025 | 0.1 | 0.64 | 35 | 30 | <3 | 16 | <3 | 0.08 | 1.1 | 26 | 40 | 681 | 5.41 | 0.01 | 0.26 | 172 | 38 | 0.01 | 17 | 0.22 | 27 | <3 | <5 | <2 | <2 | 50 | <5 | <3 | 34 |
| C 88 - 9026 | 0.1 | 0.86 | 42 | <5 | <3 | 12 | <3 | 0.08 | 1.1 | 26 | 74 | 432 | 6.01 | 0.01 | 0.45 | 197 | 24 | 0.01 | 18 | 0.20 | 20 | <3 | <5 | <2 | <2 | 25 | <5 | <3 | 39 |
| C 88 - 9027 | 0.1 | 0.72 | 37 | 40 | <3 | 9 | <3 | 0.11 | 1.2 | 36 | 75 | 1622 | 6.86 | 0.01 | 0.29 | 131 | 25 | 0.01 | 23 | 0.11 | 10 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 24 |
| C 88 - 9028 | 0.1 | 0.41 | 50 | 50 | <3 | 8 | <3 | 0.06 | 1.2 | 29 | 46 | 969 | 7.25 | 0.01 | 0.10 | 38 | 23 | 0.01 | 17 | 0.22 | 22 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 14 |
| C 88 - 9029 | 0.1 | 0.46 | 40 | 50 | <3 | 10 | <3 | 0.08 | 1.1 | 31 | 55 | 1492 | 6.07 | 0.02 | 0.11 | 48 | 71 | 0.01 | 21 | 0.10 | 15 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 18 |
| C 88 - 9030 | 0.1 | 0.51 | 82 | 55 | <3 | 7 | <3 | 0.17 | 1.3 | 29 | 55 | 1845 | 6.48 | 0.02 | 0.10 | 58 | 27 | 0.01 | 20 | 0.16 | 12 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 36 |
| C 88 - 9031 | 1.1 | 0.96 | 49 | 230 | <3 | 14 | <3 | 0.25 | 1.2 | 33 | 53 | 4705 | 5.05 | 0.02 | 0.32 | 676 | 90 | 0.01 | 21 | 0.13 | 5 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 79 |
| C 88 - 9032 | 0.1 | 1.39 | 17 | 105 | <3 | 11 | <3 | 0.24 | 2.4 | 23 | 47 | 1739 | 5.16 | 0.02 | 0.61 | 1666 | 27 | 0.01 | 13 | 0.15 | 25 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 238 |
| C 88 - 9033 | 0.8 | 1.20 | 33 | 150 | <3 | 12 | <3 | 0.10 | 1.2 | 26 | 41 | 1138 | 4.55 | 0.02 | 0.51 | 341 | 37 | 0.01 | 14 | 0.13 | 31 | <3 | <5 | <2 | <2 | 30 | <5 | <3 | 51 |
| C 88 - 9034 | 1.6 | 1.48 | 57 | 295 | <3 | 16 | <3 | 0.25 | 1.5 | 23 | 35 | 2043 | 4.76 | 0.03 | 0.61 | 854 | 188 | 0.01 | 17 | 0.17 | 54 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 148 |
| C 88 - 9035 | 1.6 | 0.98 | 83 | 225 | <3 | 23 | <3 | 0.29 | 3.2 | 24 | 35 | 2785 | 3.00 | 0.03 | 0.22 | 284 | 28 | 0.01 | 11 | 0.17 | 169 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 303 |
| C 88 - 9036 | 0.8 | 2.40 | <3 | 50 | <3 | 23 | <3 | 0.32 | 1.3 | 18 | 40 | 1399 | 4.30 | 0.04 | 1.45 | 1130 | 6 | 0.01 | 10 | 0.15 | 231 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 158 |
| C 88 - 9037 | 0.8 | 1.06 | 174 | 90 | <3 | 22 | <3 | 0.30 | 1.1 | 34 | 35 | 1475 | 4.26 | 0.03 | 0.32 | 381 | 55 | 0.01 | 15 | 0.17 | 21 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 88 |
| C 88 - 9038 | 0.8 | 0.73 | 76 | 70 | <3 | 15 | <3 | 0.30 | 1.2 | 23 | 30 | 1224 | 4.12 | 0.03 | 0.17 | 154 | 18 | 0.01 | 13 | 0.17 | 32 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 49 |
| C 88 - 9039 | 0.8 | 0.72 | 67 | 110 | <3 | 14 | <3 | 0.32 | 1.1 | 25 | 37 | 755 | 5.27 | 0.04 | 0.17 | 160 | 12 | 0.01 | 16 | 0.17 | 13 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 38 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum is = Insufficient Sample ns = No sample > = Greater than Maximum AuFA = Fire assay/AAS

REPORT #: 880687A PA

WESTERN CANADIAN

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C 88 - 9040 | 0.5 | 0.85 | 85 | 180 | <3 | 13 | <3 | 0.28 | 1.2 | 36 | 45 | 2154 | 6.83 | 0.03 | 0.22 | 205 | 30 | 0.01 | 25 | 0.17 | 19 | <3 | <5 | <2 | <2 | 25 | <5 | <3 | 40 |
| C 88 - 9041 | 0.1 | 0.38 | 45 | 50 | <3 | 12 | <3 | 0.26 | 1.5 | 30 | 38 | 855 | 7.94 | 0.02 | 0.04 | 36 | 8 | 0.01 | 27 | 0.15 | 18 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 14 |
| C 88 - 9042 | 0.1 | 0.46 | 62 | 30 | <3 | 13 | <3 | 0.30 | 1.5 | 27 | 38 | 918 | 7.05 | 0.02 | 0.02 | 33 | 7 | 0.01 | 24 | 0.17 | 28 | <3 | <5 | <2 | <2 | 36 | <5 | <3 | 24 |
| C 88 - 9043 | 0.1 | 0.41 | 41 | <5 | <3 | 14 | <3 | 0.26 | 1.2 | 26 | 41 | 516 | 6.76 | 0.02 | 0.02 | 34 | 10 | 0.01 | 17 | 0.15 | 22 | <3 | <5 | <2 | <2 | 21 | <5 | <3 | 13 |
| C 88 - 9044 | 0.1 | 0.50 | 28 | 40 | <3 | 16 | <3 | 0.30 | 1.3 | 24 | 41 | 1020 | 6.37 | 0.02 | 0.03 | 34 | 12 | 0.01 | 14 | 0.20 | 14 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 9 |
| C 88 - 9045 | 0.3 | 0.44 | 37 | 250 | <3 | 16 | <3 | 0.60 | 1.2 | 21 | 47 | 582 | 5.99 | 0.05 | 0.05 | 473 | 9 | 0.01 | 12 | 0.12 | 22 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 36 |
| C 88 - 9046 | 0.1 | 0.48 | 31 | 30 | <3 | 18 | <3 | 0.44 | 1.3 | 22 | 35 | 440 | 6.20 | 0.03 | 0.15 | 220 | 4 | 0.01 | 14 | 0.17 | 25 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 36 |
| C 88 - 9047 | 0.1 | 0.44 | 29 | <5 | <3 | 14 | <3 | 0.38 | 1.3 | 28 | 27 | 586 | 7.06 | 0.03 | 0.12 | 186 | 7 | 0.01 | 19 | 0.16 | 24 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 32 |
| C 88 - 9048 | 0.1 | 0.54 | 40 | 35 | <3 | 16 | <3 | 0.40 | 1.7 | 25 | 28 | 1007 | 6.85 | 0.03 | 0.24 | 345 | 7 | 0.01 | 17 | 0.17 | 28 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 65 |
| C 88 - 9049 | 0.1 | 0.60 | 33 | 65 | <3 | 14 | <3 | 0.34 | 1.7 | 25 | 55 | 1008 | 6.88 | 0.02 | 0.22 | 182 | 12 | 0.01 | 15 | 0.17 | 39 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 107 |
| C 88 - 9050 | 0.1 | 0.43 | 63 | 45 | <3 | 12 | <3 | 0.27 | 1.2 | 28 | 38 | 654 | 6.25 | 0.01 | 0.12 | 47 | 8 | 0.01 | 17 | 0.17 | 11 | <3 | <5 | <2 | <2 | 5 | <5 | <3 | 75 |
| C 88 - 9051 | 0.1 | 0.56 | 115 | 40 | <3 | 9 | <3 | 0.28 | 1.2 | 22 | 22 | 1064 | 6.41 | 0.01 | 0.25 | 81 | 6 | 0.01 | 15 | 0.20 | 22 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 78 |
| C 88 - 9052 | 0.1 | 0.29 | 53 | 130 | <3 | 15 | <3 | 0.22 | 1.1 | 22 | 9 | 874 | 6.25 | 0.01 | 0.06 | 31 | 3 | 0.01 | 16 | 0.17 | 27 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 29 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

EPORT #: 880697 PA WESTERN CANADIAN 

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| 88 - 9053 | 0.1 | 0.43 | 69 | 30 | <3 | 13 | <3 | 0.29 | 1.7 | 21 | 8 | 769 | 6.79 | 0.03 | 0.19 | 77 | 2 | 0.01 | 21 | 0.27 | 58 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 44 |
| 88 - 9054 | 0.1 | 1.25 | 133 | 20 | <3 | 42 | <3 | 2.25 | 2.9 | 28 | 9 | 2186 | 8.33 | 0.13 | 0.81 | 2085 | 3 | 0.01 | 21 | 0.26 | 48 | <3 | <5 | <2 | <2 | 38 | <5 | <3 | 199 |
| 88 - 9055 | 0.1 | 0.78 | 63 | 30 | <3 | 27 | <3 | 0.50 | 1.5 | 21 | 6 | 613 | 6.15 | 0.03 | 0.55 | 476 | 2 | 0.01 | 13 | 0.20 | 20 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 79 |
| 88 - 9056 | 0.1 | 0.68 | 76 | 10 | <3 | 30 | <3 | 0.71 | 1.3 | 20 | 6 | 618 | 6.15 | 0.05 | 0.60 | 635 | 2 | 0.01 | 11 | 0.20 | 36 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 111 |
| 88 - 9057 | 0.1 | 0.83 | 75 | 10 | <3 | 12 | <3 | 0.32 | 2.1 | 21 | 9 | 1184 | 6.25 | 0.04 | 0.38 | 273 | 4 | 0.01 | 12 | 0.19 | 67 | 3 | <5 | <2 | <2 | 12 | <5 | <3 | 171 |
| 88 - 9058 | 0.1 | 0.61 | 88 | <5 | <3 | 26 | <3 | 0.65 | 1.1 | 19 | 5 | 617 | 5.00 | 0.05 | 0.56 | 1198 | 2 | 0.01 | 9 | 0.20 | 31 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 123 |
| 88 - 9059 | 0.1 | 0.90 | 117 | 30 | <3 | 31 | <3 | 0.79 | 2.4 | 25 | 5 | 1218 | 6.19 | 0.06 | 0.94 | 2112 | 4 | 0.01 | 9 | 0.20 | 40 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 246 |
| 88 - 9060 | 0.1 | 0.64 | 130 | 30 | <3 | 27 | <3 | 0.52 | 3.1 | 23 | 8 | 873 | 5.59 | 0.04 | 0.45 | 805 | 4 | 0.01 | 8 | 0.17 | 45 | 4 | <5 | <2 | <2 | 7 | <5 | <3 | 150 |
| 88 - 9061 | 0.3 | 0.40 | 136 | 50 | <3 | 16 | <3 | 0.05 | 3.1 | 15 | 7 | 873 | 7.01 | 0.02 | 0.07 | 98 | 7 | 0.01 | 8 | 0.25 | 44 | 6 | <5 | <2 | 2 | 41 | <5 | <3 | 288 |
| 88 - 9062 | 0.1 | 0.31 | 80 | 90 | <3 | 10 | <3 | 0.40 | 2.2 | 52 | 13 | 396 | >10.00 | 0.04 | 0.29 | 975 | 9 | 0.01 | 7 | 0.08 | 96 | 4 | <5 | <2 | 3 | 9 | <5 | <3 | 173 |
| 88 - 9063 | 0.1 | 0.67 | 52 | 90 | <3 | 14 | <3 | 0.61 | 1.7 | 20 | 16 | 399 | 6.58 | 0.05 | 0.48 | 490 | 4 | 0.01 | 16 | 0.20 | 35 | 3 | <5 | <2 | 2 | 10 | <5 | <3 | 69 |
| 88 - 9064 | 0.1 | 0.64 | 40 | 40 | <3 | 12 | <3 | 0.68 | 1.6 | 19 | 12 | 309 | 6.75 | 0.05 | 0.56 | 868 | 3 | 0.01 | 13 | 0.17 | 51 | 3 | <5 | <2 | <2 | 10 | <5 | <3 | 101 |
| 88 - 9065 | 0.1 | 0.87 | 70 | 40 | <3 | 19 | <3 | 0.81 | 1.7 | 22 | 19 | 516 | 6.49 | 0.06 | 0.72 | 1968 | 4 | 0.01 | 10 | 0.20 | 65 | <3 | <5 | <2 | 2 | 11 | <5 | <3 | 177 |
| 88 - 9066 | 0.6 | 0.67 | 68 | 140 | <3 | 16 | <3 | 0.48 | 3.2 | 21 | 18 | 506 | 6.07 | 0.05 | 0.32 | 468 | 6 | 0.01 | 8 | 0.20 | 119 | 6 | <5 | <2 | 2 | 8 | <5 | <3 | 365 |
| 88 - 9067 | 2.7 | 0.44 | 77 | 310 | <3 | 12 | <3 | 0.44 | 2.1 | 23 | 12 | 512 | 6.08 | 0.04 | 0.08 | 327 | 12 | 0.01 | 11 | 0.20 | 87 | 7 | <5 | <2 | 3 | 10 | <5 | <3 | 165 |
| 88 - 9068 | 0.3 | 0.54 | 68 | <5 | <3 | 10 | <3 | 0.44 | 1.7 | 19 | 18 | 525 | 7.08 | 0.04 | 0.20 | 370 | 4 | 0.01 | 8 | 0.19 | 112 | 5 | <5 | <2 | 4 | 8 | <5 | <3 | 121 |
| 88 - 9069 | 0.1 | 0.92 | 75 | 140 | <3 | 48 | <3 | 6.10 | 3.7 | 17 | 8 | 771 | 4.80 | 0.25 | 0.60 | 4087 | 1 | 0.01 | 5 | 0.16 | 147 | <3 | <5 | <2 | <2 | 133 | 24 | <3 | 659 |
| 88 - 9070 | 0.1 | 0.47 | 826 | 40 | <3 | 27 | <3 | 0.58 | 1.3 | 15 | 10 | 363 | 3.95 | 0.05 | 0.14 | 204 | 6 | 0.01 | 6 | 0.20 | 56 | 6 | <5 | <2 | 2 | 39 | <5 | <3 | 57 |
| 88 - 9071 | 0.1 | 0.56 | 74 | 80 | <3 | 17 | <3 | 0.46 | 1.3 | 21 | 16 | 786 | 6.39 | 0.04 | 0.20 | 195 | 4 | 0.01 | 12 | 0.20 | 67 | 5 | <5 | <2 | 3 | 8 | <5 | <3 | 78 |
| 88 - 9072 | 0.1 | 0.55 | 63 | 40 | <3 | 23 | <3 | 1.60 | 1.2 | 18 | 8 | 644 | 5.41 | 0.10 | 0.58 | 1171 | 2 | 0.01 | 8 | 0.17 | 66 | <3 | <5 | <2 | 3 | 34 | <5 | <3 | 116 |
| 88 - 9073 | 0.1 | 0.75 | 42 | 55 | <3 | 21 | <3 | 0.51 | 2.5 | 21 | 17 | 411 | 5.69 | 0.05 | 0.44 | 382 | 5 | 0.01 | 25 | 0.20 | 71 | 5 | <5 | <2 | 3 | 10 | <5 | <3 | 132 |
| 88 - 9074 | 0.1 | 0.86 | 74 | 40 | <3 | 20 | <3 | 0.63 | 2.1 | 18 | 17 | 696 | 6.17 | 0.05 | 0.68 | 846 | 4 | 0.01 | 15 | 0.20 | 87 | 5 | <5 | <2 | 4 | 9 | <5 | <3 | 175 |
| 88 - 9075 | 0.1 | 0.80 | 51 | 50 | <3 | 18 | <3 | 0.58 | 2.7 | 21 | 16 | 656 | 6.40 | 0.05 | 0.51 | 610 | 5 | 0.01 | 13 | 0.20 | 104 | 6 | <5 | <2 | 3 | 10 | <5 | <3 | 283 |
| 88 - 9076 | 0.1 | 0.64 | 46 | 50 | <3 | 18 | <3 | 0.61 | 1.7 | 21 | 19 | 487 | 5.91 | 0.05 | 0.40 | 899 | 7 | 0.01 | 11 | 0.20 | 68 | 6 | <5 | <2 | 3 | 11 | <5 | <3 | 165 |
| 88 - 9077 | 0.1 | 1.10 | 43 | 180 | <3 | 33 | <3 | 2.33 | 1.2 | 16 | 14 | 903 | 5.01 | 0.13 | 1.08 | 1593 | 12 | 0.01 | 8 | 0.17 | 39 | <3 | <5 | <2 | 3 | 50 | <5 | <3 | 136 |
| 88 - 9078 | 0.1 | 1.70 | 51 | 150 | <3 | 36 | <3 | 1.08 | 2.2 | 24 | 17 | 313 | 6.16 | 0.07 | 1.50 | 2272 | 17 | 0.01 | 8 | 0.20 | 68 | 3 | <5 | <2 | 2 | 20 | <5 | <3 | 307 |
| 88 - 9079 | 0.1 | 1.43 | 118 | 200 | <3 | 25 | <3 | 1.50 | 3.1 | 20 | 15 | 472 | 5.45 | 0.08 | 1.23 | 2036 | 4 | 0.01 | 7 | 0.19 | 136 | <3 | <5 | <2 | <2 | 36 | <5 | <3 | 470 |
| 88 - 9080 | 0.2 | 0.88 | 100 | 70 | <3 | 21 | <3 | 0.63 | 2.1 | 20 | 16 | 657 | 5.66 | 0.05 | 0.64 | 997 | 5 | 0.01 | 9 | 0.20 | 116 | 5 | <5 | <2 | 3 | 11 | <5 | <3 | 272 |
| 88 - 9081 | 0.1 | 1.31 | 161 | 120 | <3 | 23 | <3 | 0.48 | 2.1 | 23 | 18 | 833 | 6.41 | 0.04 | 1.01 | 595 | 4 | 0.01 | 8 | 0.20 | 75 | 5 | <5 | <2 | 2 | 14 | <5 | <3 | 132 |
| 88 - 9082 | 0.1 | 1.81 | 179 | 80 | <3 | 51 | <3 | 1.54 | 2.1 | 18 | 9 | 1212 | 4.79 | 0.10 | 1.62 | 1732 | 5 | 0.01 | 6 | 0.20 | 87 | 3 | <5 | <2 | 2 | 37 | <5 | <3 | 258 |
| 88 - 9083 | 0.4 | 0.31 | 214 | 55 | <3 | 10 | <3 | 3.27 | 1.5 | 13 | 7 | 858 | 4.26 | 0.17 | 0.75 | 1637 | 8 | 0.01 | 6 | 0.14 | 62 | <3 | <5 | 14 | 4 | 78 | <5 | <3 | 141 |
| 88 - 9084 | 0.1 | 1.39 | 3 | <5 | <3 | 952 | <3 | 3.27 | 0.6 | 7 | 6 | 53 | 2.49 | 0.17 | 1.08 | 1492 | 2 | 0.01 | 1 | 0.08 | 35 | <3 | <5 | <2 | 2 | 127 | <5 | <3 | 99 |
| 88 - 9085 | 0.1 | 1.35 | <3 | <5 | <3 | >1000 | <3 | 0.41 | 1.3 | 16 | 7 | 329 | 4.12 | 0.04 | 0.79 | 2771 | 3 | 0.01 | 6 | 0.10 | 48 | 5 | <5 | <2 | 4 | 30 | <5 | <3 | 293 |
| 88 - 9086 | 0.1 | 1.27 | 8 | <5 | <3 | 605 | <3 | 0.79 | 1.2 | 15 | 6 | 289 | 3.95 | 0.06 | 0.78 | 2753 | 3 | 0.01 | 5 | 0.10 | 43 | 4 | <5 | <2 | 3 | 31 | <5 | <3 | 313 |
| 88 - 9087 | 0.1 | 1.33 | <3 | <5 | <3 | 560 | <3 | 1.36 | 0.8 | 11 | 12 | 43 | 2.97 | 0.08 | 0.73 | 1923 | 3 | 0.01 | 3 | 0.08 | 42 | 4 | <5 | <2 | 3 | 48 | <5 | <3 | 236 |
| 88 - 9088 | 0.1 | 1.12 | 5 | 30 | <3 | 134 | <3 | 1.16 | 1.3 | 14 | 13 | 643 | 3.95 | 0.08 | 0.60 | 2132 | 4 | 0.01 | 4 | 0.10 | 47 | 4 | <5 | <2 | 3 | 34 | <5 | <3 | 266 |
| 88 - 9089 | 0.1 | 1.00 | 5 | 90 | <3 | 217 | <3 | 1.86 | 1.2 | 13 | 13 | 1024 | 3.64 | 0.11 | 0.56 | 2430 | 4 | 0.01 | 3 | 0.10 | 41 | <3 | <5 | <2 | 3 | 43 | <5 | <3 | 291 |
| 88 - 9090 | 3.1 | 0.38 | 119 | 350 | <3 | 15 | <3 | 0.27 | 2.1 | 14 | 20 | 9081 | 7.50 | 0.04 | 0.04 | 129 | 6 | 0.01 | 5 | 0.12 | 79 | 7 | <5 | <2 | 5 | 22 | <5 | <3 | 126 |
| 88 - 9091 | 2.9 | 0.40 | 43 | 490 | <3 | 9 | <3 | 0.20 | 2.5 | 13 | 17 | 10895 | 9.42 | 0.03 | 0.08 | 400 | 7 | 0.01 | 5 | 0.08 | 77 | 7 | <5 | <2 | 5 | 14 | <5 | <3 | 94 |
| inimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| aximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum is = Insufficient Sample ns = No sample > = Greater than Maximum AuFA = Fire assay/AAS

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88 - 9092 | 2.9 | 0.29 | 18 | 370 | <3 | 11 | <3 | 0.29 | 2.1 | 14 | 13 | 12894 | 6.68 | 0.03 | 0.03 | 649 | 3 | 0.01 | 9 | 0.12 | 6 | <3 | <5 | <2 | 2 | 6 | <5 | <3 | 55 |
| C88 - 9093 | 2.2 | 0.69 | 11 | 440 | <3 | 9 | <3 | 0.25 | 2.7 | 14 | 16 | 14999 | 7.50 | 0.02 | 0.29 | 85 | 5 | 0.01 | 8 | 0.17 | 29 | <3 | <5 | <2 | 2 | 6 | <5 | <3 | 29 |
| C88 - 9094 | 3.2 | 0.86 | 16 | 340 | <3 | 11 | <3 | 0.22 | 2.2 | 15 | 17 | 16351 | 7.79 | 0.02 | 0.43 | 113 | 7 | 0.01 | 5 | 0.16 | 34 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 99 |
| C88 - 9095 | 3.1 | 0.48 | 17 | 330 | <3 | 15 | <3 | 0.25 | 1.7 | 16 | 21 | 15812 | 7.41 | 0.03 | 0.05 | 35 | 10 | 0.01 | 5 | 0.20 | 22 | <3 | <5 | <2 | <2 | 25 | <5 | <3 | 18 |
| C88 - 9096 | 2.2 | 0.46 | 203 | 270 | <3 | 10 | <3 | 0.25 | 1.7 | 18 | 17 | 14029 | 9.19 | 0.03 | 0.02 | 27 | 9 | 0.01 | 5 | 0.17 | 24 | <3 | <5 | <2 | 2 | 37 | <5 | <3 | 28 |
| C88 - 9097 | 1.5 | 0.40 | 46 | 220 | <3 | 8 | <3 | 0.22 | 1.3 | 15 | 18 | 11981 | 6.94 | 0.02 | 0.04 | 23 | 9 | 0.01 | 5 | 0.15 | 28 | <3 | <5 | <2 | 2 | 38 | <5 | <3 | 14 |
| C88 - 9098 | 0.8 | 0.53 | 16 | 210 | <3 | 10 | <3 | 0.24 | 1.7 | 19 | 15 | 8763 | 8.14 | 0.02 | 0.11 | 35 | 13 | 0.01 | 4 | 0.20 | 13 | <3 | <5 | <2 | 2 | 31 | <5 | <3 | 26 |
| C88 - 9099 | 1.5 | 1.12 | 11 | 315 | <3 | 9 | <3 | 0.25 | 1.7 | 16 | 60 | 11059 | 7.98 | 0.02 | 0.46 | 139 | 9 | 0.01 | 5 | 0.17 | 21 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 95 |
| C88 - 9100 | 4.1 | 0.44 | 427 | 290 | <3 | 9 | <3 | 0.24 | 5.5 | 17 | 37 | 14095 | 8.41 | 0.02 | 0.06 | 172 | 7 | 0.01 | 4 | 0.15 | 373 | <3 | <5 | 6 | 2 | 10 | <5 | <3 | 308 |
| C88 - 9101 | 4.3 | 1.47 | 578 | 410 | <3 | 13 | <3 | 0.22 | 2.5 | 14 | 73 | 12522 | 7.83 | 0.02 | 0.40 | 111 | 19 | 0.01 | 5 | 0.30 | 89 | <3 | <5 | 15 | <2 | 110 | <5 | <3 | 228 |
| C88 - 9102 | 0.8 | 1.41 | 71 | 180 | <3 | 21 | <3 | 0.32 | 1.8 | 14 | 30 | 8440 | 5.47 | 0.02 | 0.85 | 193 | 13 | 0.01 | 10 | 0.27 | 27 | <3 | <5 | <2 | <2 | 193 | <5 | <3 | 114 |
| C88 - 9103 | 2.9 | 1.52 | 19 | 390 | <3 | 14 | <3 | 0.29 | 2.1 | 12 | 18 | 14748 | 7.44 | 0.03 | 0.97 | 294 | 12 | 0.01 | 7 | 0.25 | 22 | <3 | <5 | <2 | <2 | 180 | <5 | <3 | 88 |
| C88 - 9104 | 2.5 | 2.33 | 11 | 390 | <3 | 30 | <3 | 0.28 | 1.2 | 10 | 44 | 13942 | 5.37 | 0.02 | 1.47 | 503 | 9 | 0.01 | 5 | 0.25 | 25 | <3 | <5 | <2 | <2 | 196 | <5 | <3 | 121 |
| C88 - 9105 | 1.8 | 2.36 | 18 | 300 | <3 | 33 | <3 | 0.34 | 1.7 | 12 | 36 | 12515 | 6.17 | 0.03 | 1.56 | 489 | 16 | 0.01 | 5 | 0.26 | 30 | <3 | <5 | <2 | <2 | 139 | <5 | <3 | 116 |
| C88 - 9106 | 3.5 | 1.82 | 17 | 530 | <3 | 17 | <3 | 0.30 | 2.1 | 19 | 96 | 19117 | 7.90 | 0.02 | 1.03 | 275 | 16 | 0.01 | 4 | 0.19 | 23 | <3 | <5 | <2 | <2 | 35 | <5 | <3 | 49 |
| C88 - 9107 | 3.4 | 1.53 | 19 | 560 | <3 | 15 | <3 | 0.24 | 1.7 | 15 | 21 | >20000 | 6.69 | 0.02 | 0.91 | 241 | 8 | 0.01 | 3 | 0.15 | 17 | <3 | <5 | <2 | <2 | 26 | <5 | <3 | 42 |
| C88 - 9108 | 1.8 | 0.83 | 20 | 420 | <3 | 11 | <3 | 0.20 | 1.5 | 15 | 54 | 14090 | 6.22 | 0.03 | 0.52 | 91 | 7 | 0.01 | 5 | 0.14 | 32 | <3 | <5 | <2 | 2 | 20 | <5 | <3 | 50 |
| C88 - 9109 | 1.7 | 1.12 | 19 | 250 | <3 | 15 | <3 | 0.30 | 1.2 | 14 | 45 | 9478 | 5.39 | 0.03 | 0.58 | 100 | 7 | 0.01 | 11 | 0.26 | 19 | <3 | <5 | <2 | 2 | 67 | <5 | <3 | 56 |
| C88 - 9110 | 1.8 | 0.51 | 13 | 400 | <3 | 17 | <3 | 0.28 | 3.2 | 13 | 26 | 9591 | 5.30 | 0.03 | 0.14 | 41 | 5 | 0.01 | 4 | 0.17 | 21 | <3 | <5 | <2 | 2 | 35 | <5 | <3 | 28 |
| C88 - 9111 | 2.1 | 0.39 | 25 | 350 | <3 | 13 | <3 | 0.22 | 5.6 | 12 | 48 | 10562 | 5.22 | 0.02 | 0.05 | 21 | 17 | 0.01 | 3 | 0.13 | 40 | <3 | <5 | <2 | <2 | 19 | <5 | <3 | 38 |
| C88 - 9112 | 2.7 | 0.71 | 170 | 330 | <3 | 21 | <3 | 0.28 | 1.8 | 13 | 55 | 11540 | 4.24 | 0.03 | 0.17 | 68 | 14 | 0.01 | 22 | 0.16 | 37 | <3 | <5 | <2 | 2 | 14 | <5 | <3 | 121 |
| C88 - 9113 | 2.7 | 0.73 | 29 | 480 | <3 | 19 | <3 | 0.34 | 1.7 | 17 | 47 | 12657 | 5.39 | 0.03 | 0.17 | 688 | 15 | 0.01 | 14 | 0.17 | 19 | <3 | <5 | <2 | 2 | 9 | <5 | <3 | 101 |
| C88 - 9114 | 3.2 | 0.29 | 56 | 535 | <3 | 18 | <3 | 0.28 | 2.2 | 19 | 39 | 14427 | 7.03 | 0.03 | 0.05 | 1172 | 7 | 0.01 | 11 | 0.11 | 52 | <3 | <5 | <2 | 3 | 8 | <5 | <3 | 136 |
| C88 - 9115 | 2.5 | 0.48 | 32 | 370 | <3 | 12 | <3 | 0.19 | 3.1 | 18 | 92 | 9495 | 5.83 | 0.03 | 0.14 | 1029 | 9 | 0.01 | 8 | 0.07 | 38 | <3 | <5 | <2 | 2 | 6 | <5 | <3 | 192 |
| C88 - 9116 | 0.1 | 5.00 | 22 | 60 | <3 | 270 | 20 | 0.61 | 2.5 | 37 | 20 | 1027 | >10.00 | 0.05 | 3.00 | 2666 | 7 | 0.01 | 5 | 0.17 | 58 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 369 |
| C88 - 9117 | 0.1 | 4.94 | 7 | 20 | <3 | 384 | 24 | 1.39 | 2.5 | 45 | 20 | 779 | >10.00 | 0.08 | 3.07 | 3385 | 6 | 0.01 | 2 | 0.12 | 46 | <3 | <5 | <2 | 3 | 27 | <5 | <3 | 297 |
| C88 - 9118 | 0.1 | 4.12 | 23 | 160 | <3 | 128 | 22 | 0.80 | 2.5 | 40 | 36 | 1396 | >10.00 | 0.06 | 2.47 | 3404 | 8 | 0.02 | 12 | 0.17 | 51 | <3 | <5 | <2 | 3 | 23 | <5 | <3 | 404 |
| C88 - 9119 | 2.7 | 0.71 | 42 | 340 | <3 | 17 | <3 | 0.27 | 3.5 | 26 | 35 | 11596 | 6.96 | 0.03 | 0.15 | 207 | 43 | 0.01 | 25 | 0.13 | 200 | <3 | <5 | <2 | 3 | 14 | <5 | <3 | 211 |
| C88 - 9120 | 2.7 | 0.40 | 141 | 280 | <3 | 24 | <3 | 0.30 | 2.5 | 20 | 41 | 8797 | 6.24 | 0.04 | 0.10 | 547 | 13 | 0.01 | 12 | 0.13 | 68 | <3 | <5 | <2 | 3 | 8 | <5 | <3 | 161 |
| C88 - 9121 | 3.2 | 0.30 | 481 | 330 | <3 | 19 | <3 | 0.27 | 2.4 | 15 | 60 | 11148 | 7.09 | 0.03 | 0.06 | 425 | 4 | 0.01 | 6 | 0.11 | 62 | <3 | <5 | <2 | 3 | 9 | <5 | <3 | 201 |
| C88 - 9122 | 4.1 | 0.34 | 181 | 450 | <3 | 19 | <3 | 0.24 | 1.7 | 17 | 69 | 16501 | 6.75 | 0.02 | 0.04 | 79 | 7 | 0.01 | 8 | 0.11 | 83 | <3 | <5 | <2 | 4 | 10 | <5 | <3 | 106 |
| C88 - 9123 | 4.8 | 0.32 | 544 | 405 | <3 | 9 | <3 | 0.24 | 2.7 | 15 | 41 | 12932 | 6.00 | 0.03 | 0.06 | 49 | 6 | 0.01 | 5 | 0.11 | 137 | <3 | <5 | <2 | 4 | 7 | <5 | <3 | 366 |
| C88 - 9124 | 3.1 | 0.32 | 96 | 240 | <3 | 19 | <3 | 0.30 | 1.7 | 16 | 47 | 8657 | 5.97 | 0.03 | 0.03 | 296 | 10 | 0.01 | 7 | 0.14 | 49 | <3 | <5 | <2 | 3 | 10 | <5 | <3 | 75 |
| C88 - 9125 | 2.2 | 0.39 | 54 | 220 | <3 | 16 | <3 | 0.35 | 2.4 | 17 | 45 | 8457 | 6.01 | 0.03 | 0.07 | 183 | 19 | 0.01 | 6 | 0.17 | 85 | <3 | <5 | <2 | 3 | 13 | <5 | <3 | 195 |
| C88 - 9126 | 1.7 | 0.81 | 21 | 280 | <3 | 13 | <3 | 0.32 | 1.3 | 24 | 65 | 6002 | 6.30 | 0.04 | 0.38 | 938 | 46 | 0.01 | 10 | 0.14 | 21 | <3 | <5 | <2 | 3 | 13 | <5 | <3 | 189 |
| C88 - 9127 | 1.7 | 1.98 | 13 | 310 | <3 | 28 | <3 | 0.30 | 1.8 | 27 | 58 | 8682 | 6.24 | 0.03 | 2.20 | 982 | 35 | 0.01 | 27 | 0.14 | 25 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 128 |
| C88 - 9128 | 1.2 | 1.56 | 27 | 130 | <3 | 14 | <3 | 0.32 | 1.6 | 23 | 41 | 1462 | 7.30 | 0.02 | 1.64 | 670 | 12 | 0.01 | 15 | 0.16 | 29 | <3 | <5 | <2 | <2 | 23 | <5 | <3 | 142 |
| C88 - 9129 | 0.3 | 1.37 | 25 | 90 | <3 | 20 | 6 | 0.30 | 1.5 | 23 | 38 | 1706 | 6.10 | 0.04 | 1.41 | 604 | 11 | 0.01 | 15 | 0.16 | 24 | <3 | <5 | <2 | <2 | 32 | <5 | <3 | 137 |
| C88 - 9130 | 0.5 | 1.33 | 42 | 130 | <3 | 15 | <3 | 0.32 | 1.7 | 24 | 68 | 2912 | 6.22 | 0.03 | 1.29 | 554 | 33 | 0.01 | 40 | 0.19 | 29 | <3 | <5 | <2 | 2 | 55 | <5 | <3 | 144 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum is = Insufficient Sample ns = No sample > = Greater than Maximum AuFA = Fire assay/AAS

REPORT I: 880697 PA

WESTERN CANADIAN

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88 - 9131 | 0.1 | 1.08 | 76 | <5 | <3 | 17 | <3 | 0.32 | 1.3 | 20 | 20 | 2373 | 5.50 | 0.03 | 1.02 | 455 | 10 | 0.01 | 16 | 0.20 | 16 | <3 | <5 | <2 | <2 | 41 | <5 | <3 | 110 |
| C88 - 9132 | 0.3 | 0.91 | 148 | 80 | <3 | 16 | <3 | 0.28 | 1.3 | 23 | 40 | 2244 | 6.12 | 0.02 | 0.64 | 282 | 11 | 0.01 | 19 | 0.19 | 23 | <3 | <5 | <2 | <2 | 37 | <5 | <3 | 247 |
| C88 - 9133 | 1.8 | 0.69 | 605 | 320 | <3 | 15 | <3 | 0.32 | 1.5 | 31 | 16 | 6417 | 7.20 | 0.03 | 0.10 | 48 | 85 | 0.01 | 46 | 0.20 | 79 | <3 | <5 | <2 | <2 | 32 | <5 | <3 | 158 |
| C88 - 9134 | 4.5 | 1.29 | 64 | 1120 | <3 | 17 | 9 | 0.41 | 2.2 | 48 | 29 | 9467 | 9.19 | 0.03 | 0.73 | 199 | 131 | 0.01 | 77 | 0.27 | 61 | <3 | <5 | <2 | <2 | 24 | <5 | <3 | 163 |
| C88 - 9135 | 3.7 | 1.66 | 27 | 955 | <3 | 17 | 3 | 0.40 | 1.6 | 52 | 38 | 7568 | 8.89 | 0.03 | 1.22 | 507 | 109 | 0.01 | 67 | 0.22 | 51 | <3 | <5 | <2 | <2 | 38 | <5 | <3 | 124 |
| C88 - 9136 | 1.6 | 0.80 | 107 | 470 | <3 | 19 | <3 | 0.26 | 1.2 | 34 | 36 | 6819 | 6.84 | 0.03 | 0.22 | 132 | 87 | 0.01 | 27 | 0.17 | 43 | <3 | <5 | <2 | <2 | 80 | <5 | <3 | 59 |
| C88 - 9137 | 1.1 | 0.89 | 30 | 420 | <3 | 19 | <3 | 0.29 | 1.7 | 36 | 20 | 5268 | 7.23 | 0.03 | 0.63 | 239 | 84 | 0.01 | 31 | 0.16 | 55 | <3 | <5 | <2 | <2 | 47 | <5 | <3 | 160 |

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: SEP 1 1988
DATE REPORT MAILED: Sept 9/88

# GEOCHEMICAL ANALYSIS CERTIFICATE

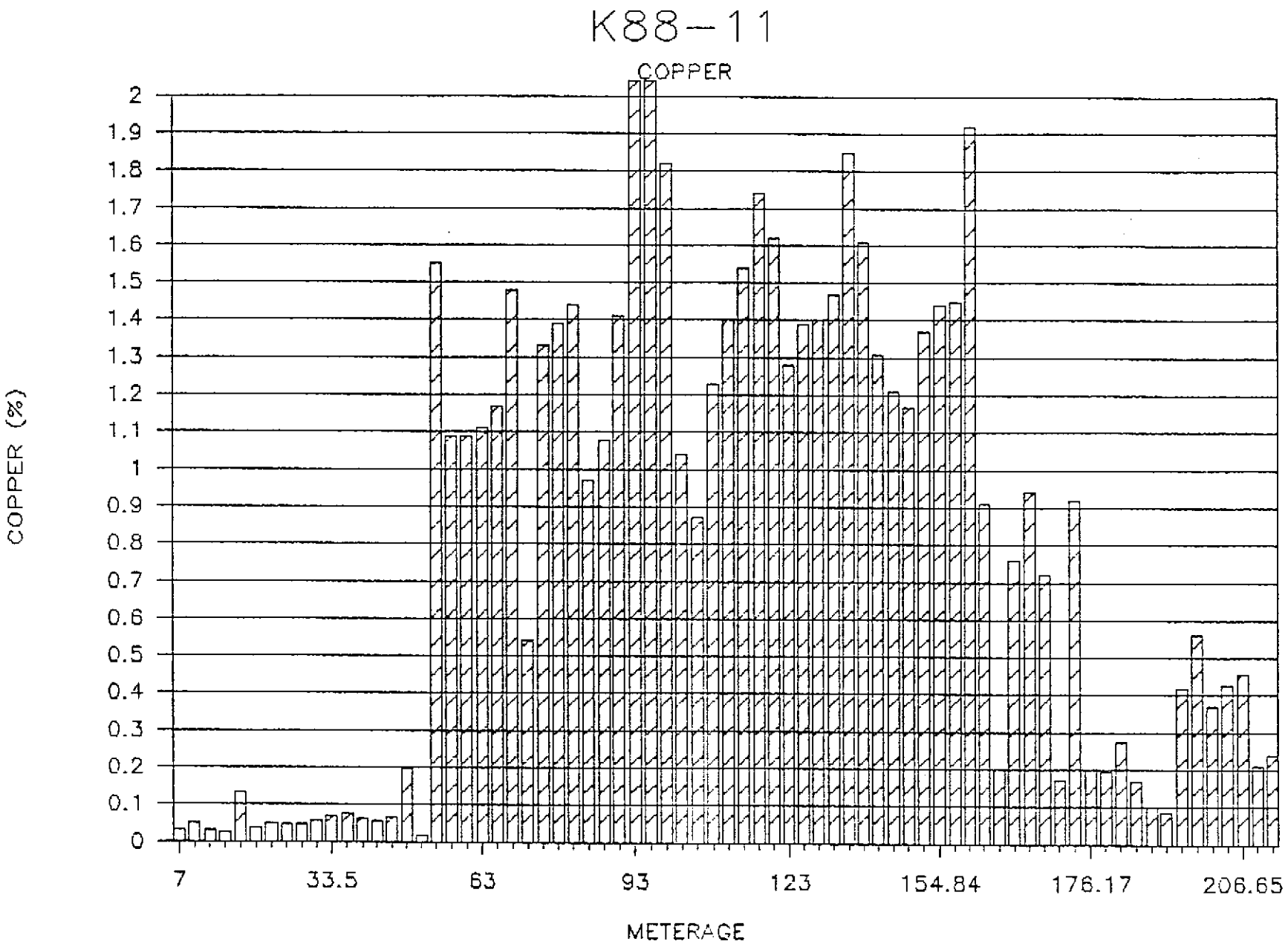
ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Rock Chips AU** PT** PD** RH** BY FA-MS.

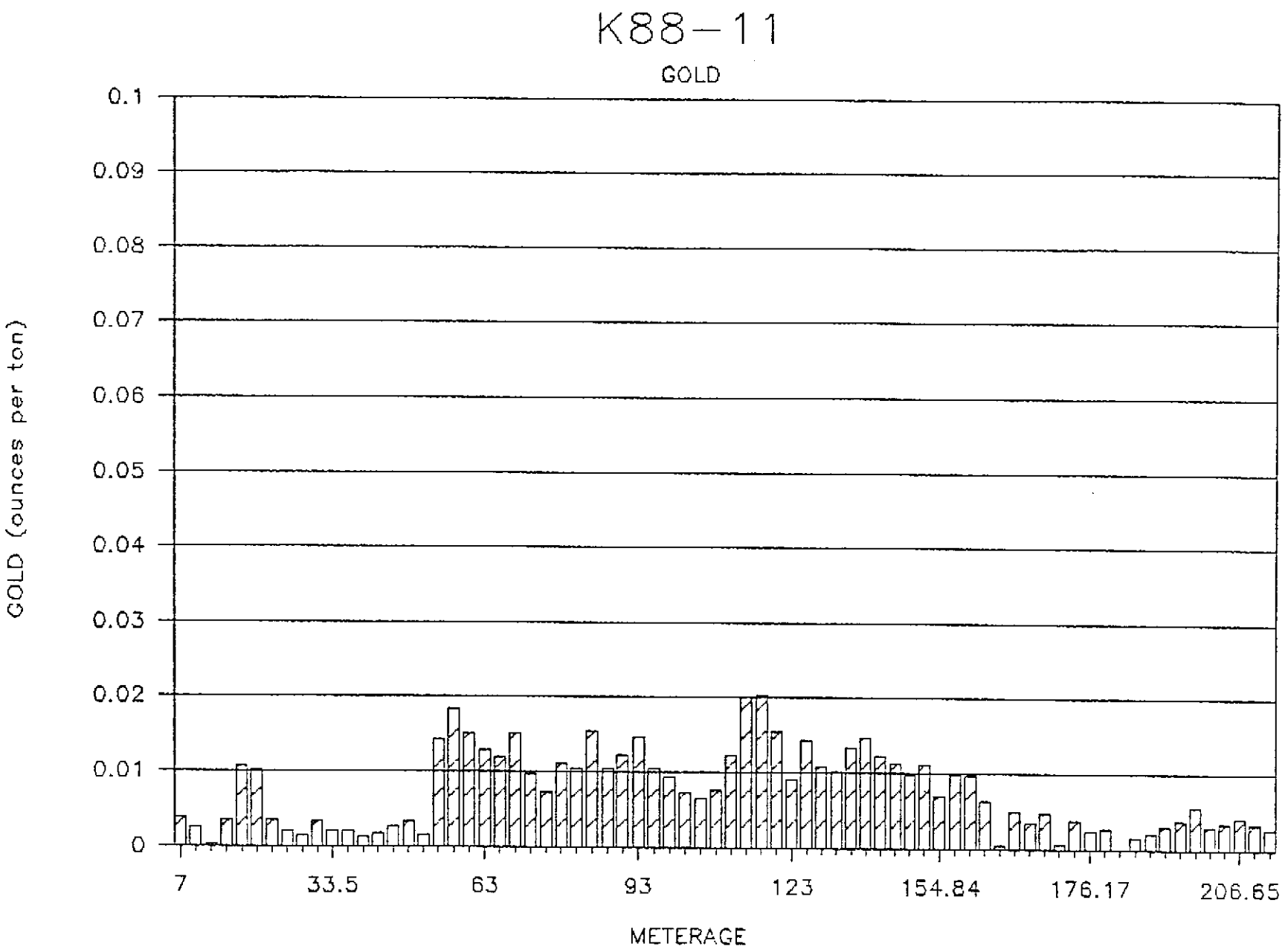
ASSAYER: C. Leong. D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTERN CANADIAN MINING CORP. PROJECT 9101-12 FILE # 88-4147 Page 1

| SAMPLE# | Cu PPM | Ag PPM | Au** PPB | Pt** PPB | Pd** PPB | Rh** PPB |
|---|---|---|---|---|---|---|
| C88-9088 | 9462 | 2.4 | 399 | 2 | 2 | 2 |
| C88-9089 | 1650 | .5 | 66 | 1 | 2 | 2 |
| C88-9090 | 10169 | 3.2 | 220 | 1 | 2 | 2 |
| C88-9091 | 13422 | 4.6 | 402 | 1 | 2 | 2 |
| C88-9092 | 14221 | 3.3 | 288 | 1 | 9 | 2 |
| C88-9093 | 15838 | 3.1 | 527 | 3 | 2 | 6 |
| C88-9094 | 19439 | 3.7 | 515 | 2 | 2 | 2 |
| C88-9095 | 16370 | 3.4 | 482 | 2 | 4 | 2 |
| C88-9096 | 13143 | 2.9 | 466 | 3 | 2 | 2 |
| C88-9097 | 11946 | 1.8 | 282 | 2 | 2 | 2 |
| C88-9098 | 10049 | 1.6 | 299 | 3 | 2 | 2 |
| C88-9099 | 11825 | 2.1 | 511 | 3 | 2 | 2 |
| C88-9100 | 14739 | 4.6 | 422 | 2 | 3 | 2 |
| C88-9101 | 13452 | 6.3 | 632 | 3 | 2 | 2 |
| C88-9102 | 8435 | 1.6 | 255 | 3 | 3 | 2 |
| C88-9103 | 15457 | 3.2 | 560 | 3 | 2 | 2 |
| C88-9104 | 13649 | 3.3 | 553 | 3 | 3 | 2 |
| C88-9105 | 11991 | 2.5 | 482 | 4 | 2 | 2 |
| C88-9106 | 18184 | 3.4 | 752 | 4 | 2 | 2 |
| C88-9107 | 21927 | 3.6 | 715 | 3 | 2 | 2 |
| C88-9108 | 13844 | 2.2 | 607 | 10 | 14 | 2 |
| C88-9109 | 9409 | 2.0 | 385 | 2 | 2 | 2 |
| C88-9110 | 10141 | 2.0 | 663 | 3 | 2 | 2 |
| C88-9111 | 11200 | 2.2 | 611 | 1 | 3 | 2 |
| C88-9112 | 13164 | 2.7 | 439 | 3 | 4 | 2 |
| C88-9113 | 14629 | 2.6 | 808 | 3 | 2 | 2 |
| C88-9114 | 13827 | 2.5 | 735 | 3 | 5 | 2 |
| C88-9115 | 10349 | 2.3 | 483 | 2 | 18 | 2 |
| C88-9116 | 842 | .5 | 47 | 1 | 2 | 2 |
| C88-9117 | 794 | .6 | 24 | 1 | 2 | 2 |
| C88-9118 | 1672 | .6 | 305 | 1 | 2 | 2 |
| C88-9119 | 12519 | 2.6 | 449 | 4 | 3 | 2 |
| C88-9120 | 10656 | 2.8 | 367 | 6 | 2 | 2 |
| C88-9121 | 12140 | 3.0 | 558 | 2 | 2 | 2 |
| C88-9122 | 17336 | 3.5 | 595 | 2 | 2 | 2 |
| C88-9123 | 12966 | 3.5 | 463 | 1 | 2 | 2 |
| STD C/FA-5X | 63 | 6.9 | 104 | 102 | 97 | 23 |

| SAMPLE# | Cu PPM | Ag PPM | Au** PPB | Pt** PPB | Pd** PPB | Rh** PPB |
|---|---|---|---|---|---|---|
| C88-9124 | 8740 | 2.5 | 288 | 1 | 2 | 2 |
| C88-9125 | 7958 | 2.2 | 225 | 1 | 4 | 2 |
| C88-9126 | 6722 | 1.7 | 287 | 1 | 2 | 2 |
| C88-9127 | 7948 | 2.0 | 358 | 3 | 2 | 2 |


K88-11
COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
7
33.5
63
93
123
154.84
176.17
206.65
METERAGE


K88-11
GOLD
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
GOLD (ounces per ton)
7
33.5
63
93
123
154.84
176.17
206.65
METERAGE

KERR PROJECT D.D.HOLE K-88-11

LOCATION B-ZONE 100 m SOUTH OF K88-1 COLLAR LAT. 9570.1 NORTH
DATE STARTED JULY 19, 1988 LONG. 9810.9 EAST
DATE COMPLETED JULY 21, 1988 ELEVATION 1634.3 m
CORE RECOVERY 68.10% AZIMUTH 090 DIP -60 deg
DRILLED BY FALCON DRILLING LTD. LENGTH 212.75 m
LOGGED BY S. CASSELMAN HOR. PROJ. 106.38 m
OBJECTIVE Intersect B-Zone Fault Mineralization
VERT. PROJ. 184.25 m
DIP TEST DEPTH _____ DIP _____deg
DEPTH _____m DIP _____deg

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 3.05 | 3.05 | OVERBURDEN |
| 3.05 | 7.00 | 3.95 | SERICITE SCHIST<br>- overall light grey to medium grey-green<br>- strong foliation at 50 deg to C.A.<br>- intensely sericitized, minor chlorite<br>- 20% pyrite as stringers paralleling foliation, and as fine disseminations<br>- .5% chalcocite associated with pyrite stringers<br>- occasional silica band |
| 7.00 | 11.75 | 4.75 | HORNBLENDE PORPHYRY DIORITE DYKE<br>- chloritized hornblende crystals become prominent towards contact with fault<br>- also overall more chloritic towards fault<br>- abundant limonitic clay on fracture surfaces<br>- surfaces at 50 deg to 65 deg to C.A. |
| 11.75 | 15.50 | 3.75 | FAULT SERICITE SCHIST<br>- light grey, very intense sericitization<br>- 40% fault gouge, foliation at 65 deg to C.A.<br>- 20% pyrite, 1% chalcocite<br>- intense shearing near more competent dyke |
| 15.50 | 48.40 | 32.90 | SERICITE SCHIST<br>- as in 3.05 - 11.75 m<br>- well foliated at 55 deg to C.A.<br>- intense sericite, minor chlorite and silica<br>- 20% pyrite as stringers, 1% chalcocite<br>- light blue grey colour |
| 48.40 | 51.00 | 2.60 | ANDESITE DYKE<br>- medium to dark green, fine-grained to aphanitic<br>- moderate to intense chloritization<br>- 1% calcite veins and stringers |

KERR PROJECT D.D.HOLE K-88-11

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - upper contact at 60 deg, lower contact at 60 deg<br>- contains 1 quartz vein with weathered vugs of limonite (2 cm wide), and a 20 cm section of quartz-clay limonite vugs |
| 51.00 | 63.00 | 12.00 | QUARTZ-SERICITE SCHIST<br>- sericite schist as above, however, much more siliceous, more pyrite, and more chalcopyrite<br>- 3 to 15% quartz veining, 20 to 30% sulphides (pyrite, chalcopyrite, chalcocite)<br>- some calcite (< 1%)<br>- well foliated at 40 deg to C.A.<br>- 3 to 7 % copper minerals<br>- silica is blue grey colour which is interesting in that it is believed to carry gold<br>- unit is quite fractured, average core length of about 15 cm<br>- grades into fault zone from throughout interval<br>- fault zone is arbitrarily chosen as 63.0 m; after which average core length drops to approximately 5 to 10 cm |
| 63.00 | 111.00 | 48.00 | FAULT ZONE - QUARTZ SERICITE - PYRITE-CHALCOCITE - CHALCOPYRITE SCHIST<br>- intensely fractured quartz - sericite-pyrite - chalcocite - chalcopyrite schist<br>- average size 5 cm<br>- numerous pyrite veins, stringers, blebs, and irregular masses generally with chalcocite coating or association<br>- pitted surface to core<br>- blue-grey colour<br>- occasional sections with intense limonite staining<br>- rare fractures filled with powdery white mineral-gypsum (?)<br>- from 84 to 111 and from 120 to recovery is less than 30% - rock is extremely fractured-average core size is approximately 2-5 cm wide<br>- abundant limonite in fractures<br>- secondary stockwork quartz veining with contained chalcocite |

KERR PROJECT D.D.HOLE K-88-11

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 111.00 | 120.00 | 9.00 | QUARTZ - SERICITE - PYRITE - CHALCOPYRITE-CHALCOCITE STOCKWORK<br>- 20 - 45% quartz<br>- with 20 to 30% pyrite<br>- 1 to 3% chalcopyrite<br>- 1 to 4% chalcocite<br>- sulfide grey colour with white to blue-grey quartz<br>- massive, quite competent - good recovery |
| 120.00 | 132.00 | 12.00 | QUARTZ-SERICITE-PYRITE SCHIST - FAULT ZONE<br>- as in 63 - 114<br>- major core loss between (129.84 to 130.45) where there was no recovery<br>- trace malachite at 132 m |
| 132.00 | 135.90 | 3.90 | SERICITIZED SULPHIDE BRECCIA ZONE<br>- complete core loss between 132.2 to 133.5 (large cavity)<br>- rather competent (silicified) section with good core recovery - approximately 20% pyrite, .5 to 1% chalcopyrite, and 3% chalcocite<br>- 2 mm quartz breccia fragments characteristic of unit<br>- unit appears as a previous fault zone annealed with quartz and sulphides |
| 135.90 | 147.20 | 11.30 | QUARTZ SERICITE PYRITE SCHIST<br>- unit has cored well but intense fracturing of some sections has resulted in much broken core - actual recoveries are probably better than can be estimated visually - almost all pieces are angular and can be fitted back together with others close by, indicating they were not turning inside the core tube and were therefore cored as rock 'in place' - the core fell 'apart' into pieces only after being removed from the core tube<br>- unit resembles a sericitized and silicified laminated dacitic (?) tuff<br>- core angles of 48 deg at 138.4 m<br>46 deg at 143.2 m<br>- 5 cm band of massive pyrite coated with a dusting of chalcocite<br>- gypsum traces along fractures from 137.4 to 139 m |

KERR PROJECT D.D.HOLE K-88-11

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - protolith resembles interbedded dacite crystal tuff and lapilli tuff |
| 147.20 | 152.10 | 4.90 | QUARTZ-SERICITE-MARIPOSITE-PYRITE SCHIST<br>- gradational contacts<br>- protolith is probably dacitic crystal tuff or fine-grained plagioclase porphyry equivalent<br>- a rather competent piece of core at 151.9 m would indicate the host is quite brecciated<br>- noticeable increase in pyrite |
| 152.10 | 160.93 | 8.83 | CHALCOCITE QUARTZ ZONE<br>- abundant dusting of pyrite grains with chalcocite especially along foliation planes (1 to 5%) marks this sub-unit of quartz sericite pyrite schist<br>- blue grey coloured unit with minor disseminated hematite and chlorite (159.6 m)<br>- protolith is well foliated and altered dacitic crystal tuff or fine-grained equivalent of plagioclase porphyry<br>- 2-5 cm quartz sulphide breccia layers are evident, however, core is quite badly broken and the only intact band is at 153.0 m<br>- angular quartz clasts are cement with pyrite (clast supported)<br>- chalcopyrite is not readily visible, however, discoloration of pyrite and more irregular masses of pyrite may suggest that it is in exsolution with pyrite |
| 160.93 | 163.80 | 2.87 | QUARTZ-SERICITE-PYRITE SCHIST<br>- protolith is as above and below<br>- resembles highly altered plagioclase porphyry and its fine-grained equivalent and/or dacitic crystal tuff<br>- unit is evenly pyritized and takes on a blue grey colour<br>- gradational upper contact is arbitrarily chosen |
| 163.80 | 166.15 | 2.35 | ANDESITE DYKE<br>- massive aphanitic green grey andesitic to dacitic (bleached dyke)<br>- upper contact 38 deg to C.A., lower at 36 deg<br>- 2 rotten vuggy quartz veins (5 and 10 cm) in centre of dyke. |

KERR PROJECT D.D.HOLE K-88-11

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 166.15 | 171.00 | 4.85 | QUARTZ-SERICITE-PYRITE SCHIST<br>- protolith largely well foliated and altered plagioclase phenocrysts and finer grained equivalents<br>- relict plagioclase phenocrysts as well as chloritized and sericitized smaller hornblende and plagioclase crystals are found at 171.9 m, close to the upper contact of the dyke |
| 171.00 | 171.80 | 0.80 | GREEN ANDESITIC (MAFIC) DYKE<br>- green massive aphanitic, altered mostly to chlorite and minor epidote<br>- upper contact has 28 deg core angle |
| 171.80 | 191.00 | 19.20 | QUARTZ SERICITE PYRITE SCHIST (BLUE)<br>- protolith dacitic lapilli tuff and/or diorite<br>- well foliated<br>- cores well but is quite heavily fractured<br>- chlorite content varies considerably<br>- lapilli fragments vary in shape from elongate to equant angular fragments |
| 191.00 | 193.10 | 2.10 | QUARTZ-SERICITE-PYRITE SCHIST (BLUE GREY)<br>- protolith resembles fine- to medium-grained diorite at 191.3 m and grades to dacitic crystal tuff above and below<br>- probably all sheared foliated fine-grained plagioclase porphyry equivalent<br>- boundaries are gradational |
| 193.10 | 193.40 | 0.30 | GREEN ANDESITE DYKE<br>- aphanitic green buff coloured with hornblende laths |
| 193.40 | 195.80 | 2.40 | BUFF QUARTZ-SERICITE-PYRITE SCHIST<br>- protolith is probably felsic tuff<br>- chalcocite at 195 m and 193.8 m<br>- mariposite at 194.4 to 194.7 m |
| 195.80 | 212.75 | 16.95 | QUARTZ-SERICITE-CHLORITE-PYRITE SCHIST (BLUE GREEN)<br>- protolith could have been grey blue dacitic crystal tuff or the chilled equivalent of the plagioclase porphyry<br>- the sequence resembles a foliated version of dioritic to dacitic tuffs on the A-zone north<br>- see last column for foliation core angles |
| | E.O.H. | | - well foliated but quite broken unit |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 11:17:30 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8811 | 9570.1 | 9810.8 | 1634.4 | 90 | 60 | 212.75 | | STRIKE EXTENT OF B-ZONE MINERALIZATION. NO ACID TEST. #HOL |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0.00 | 3.05 | 3.05 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 3.05 | 7 | 3.95 | 32 | SRCT SCHT | | FG | 1 | 1 | 75 | 2 | 2 | | | | | | 95 | 20 | | | .5 | | | |
| 7 | 9 | 2 | 35 | SHRD HBLD PLAG | | FG | | 1 | 50 | 1 | 20 | | 1 | | | | 80 | 10 | | | .2 | | | |
| 9 | 11.75 | 2.75 | 35 | SHRD HBLD PLAG | | FG | | 1 | 50 | 1 | 20 | | 1 | | | | 80 | 10 | | | .2 | | | |
| 11.75 | 13.75 | 2 | 10 | FAULT SRCT SCHT | | FG | | 1 | 60 | 1 | 2 | | | | | | 100 | 15 | | | 1 | | | |
| 13.75 | 15.5 | 1.75 | 10 | FAULT SRCT SCHT | | FG | | 1 | 80 | 1 | 2 | | | | | | 100 | 15 | | | 1 | | | |
| 15.5 | 18.5 | 3 | 29 | SRCT SCHT | | FG | | .5 | 75 | | 3 | | | | | | 95 | 20 | | | .5 | | | |
| 18.5 | 21.5 | 3 | 22 | SRCT SCHT | | FG | | .5 | 80 | 1 | 3 | | | | | | 95 | 20 | | | .5 | | | |
| 21.5 | 24.5 | 3 | 19 | SRCT SCHT | | FG | | .5 | 65 | | 3 | | | | | | 95 | 25 | | | 2 | | | |
| 24.5 | 27.5 | 3 | 31 | SRCT SCHT | | FG | | .5 | 65 | | 3 | | | | | | 98 | 25 | | | 3 | | | |
| 27.5 | 30.5 | 3 | 30 | SRCT SCHT | | FG | | .5 | 70 | | 1 | | | | | | 98 | 20 | | | 3 | | | |
| 30.5 | 33.5 | 3 | 31 | SRCT SCHT | | FG | | .5 | 70 | | 1 | | | | | | 98 | 20 | | | 3 | | | |
| 33.5 | 36.5 | 3 | 31 | SRCT SCHT | | FG | | .5 | 68 | | 2 | | | | | | 98 | 25 | | | 3 | | | |
| 36.5 | 39.5 | 3 | 33 | SRCT SCHT | | FG | | 1 | 70 | | 5 | | | | | | 98 | 20 | | | 4 | | | |
| 39.5 | 42.5 | 3 | 29 | SRCT SCHT | | FG | | 1 | 69 | 1 | 3 | | | | | | 98 | 23 | | | 3 | | | |
| 42.5 | 45.5 | 3 | 10 | SRCT SCHT | | FG | | 1 | 75 | 1 | 1 | | | | | | 98 | 20 | | | 2 | | | |
| 45.5 | 48.4 | 2.9 | 13 | SRCT SCHT | | FG | | 3 | 65 | 2 | 2 | | | | | | 98 | 25 | .1 | | 3 | | | |
| 48.4 | 51.0 | 2.6 | 35 | ANDS DYKE | | VFG | | 5 | 5 | 5 | 40 | | 1 | | | | 60 | 2 | | | | | | |
| 51.0 | 54 | 3 | 34 | SRCT SCHT | | FG | 1 | 12 | 45 | 1 | | | 1 | | | | 100 | 30 | 5 | | 3 | | | |
| 54 | 57 | 3 | 17 | SRCT SCHT | | FG | 1 | 4 | 55 | 1 | 5 | | 1 | | | | 100 | 25 | 1 | | 4 | | | |
| 57 | 60 | 3 | 40 | SRCT SCHT | | FG | | 6 | 50 | 2 | 3 | | | | | | 100 | 32 | 1 | | 5 | | | |
| 60 | 63 | 3 | 34 | SRCT SCHT | | FG | | 3 | 55 | 2 | 5 | | | | | | 100 | 28 | .5 | | 5 | | | |
| 63 | 66 | 3 | 19 | SRCT SCHT | | FG | | 5 | 55 | 2 | 2 | | | | | | 100 | 28 | 1 | | 5 | | | |
| 66 | 69 | 3 | 18 | SRCT SCHT | | FG | | 5 | 55 | 1 | 2 | | | | | | 100 | 30 | .8 | | 5 | | | |
| 69 | 72 | 3 | 23 | SRCT SCHT | | FG | | 3 | 60 | 5 | 2 | | | | | | 100 | 25 | .1 | | 2 | | | |
| 72 | 75 | 3 | 11 | SRCT SCHT | | FG | | 5 | 60 | 1 | 1 | | | | | | 100 | 28 | .8 | | 4 | | | |
| 75 | 78 | 3 | 23 | SRCT SCHT | | FG | | 5 | 60 | 2 | 2 | | | | | | 100 | 25 | .2 | | 4 | | | |
| 78 | 81 | 3 | 23 | SRCT SCHT | | FG | | 3 | 60 | 1 | 1 | | | | | | 100 | 28 | .8 | | 5 | | | |
| 81 | 84 | 3 | 23 | SRCT SCHT | | FG | | 2 | 65 | 1 | 2 | | | | | | 100 | 23 | .2 | | 3 | | | |
| 84 | 87 | 3 | 23 | SRCT SCHT | | FG | | 2 | 65 | 1 | 5 | | | | | | 100 | 23 | .2 | | 3 | | | |
| 87 | 90 | 3 | 23 | SRCT SCHT | | FG | | 1 | 60 | 1 | 8 | | | | | | 100 | 25 | .2 | | 4 | | | |
| 90 | 93 | 3 | 18 | SRCT SCHT | | FG | | 5 | 45 | 3 | 8 | | | | | | 100 | 28 | .2 | | 5 | | | |
| 93 | 96 | 3 | 19 | SRCT SCHT | | FG | | 1 | 45 | 5 | 8 | | | | | | 100 | 30 | 1 | | 5 | | | |
| 96 | 99 | 3 | 10 | SRCT SCHT | | FG | | 10 | 55 | 2 | 5 | | | | | | 100 | 20 | .5 | | 5 | | | |
| 99 | 102 | 3 | 19 | SRCT SCHT | | FG | | 10 | 55 | 2 | 5 | | | | | | 100 | 25 | .5 | | 5 | | | |
| 102 | 105 | 3 | 10 | SRCT SCHT | | FG | | 2 | 70 | 1 | 1 | | | | | | 100 | 20 | .2 | | 5 | | | |
| 105 | 108 | 3 | 19 | SRCT SCHT | | FG | | 3 | 65 | 1 | 3 | | | | | | 100 | 20 | .2 | | 5 | | | |
| 108 | 111 | 3 | 10 | SRCT SCHT | | FG | | 3 | 65 | 1 | 3 | | | | | | 100 | 20 | .2 | | 5 | | | |
| 111 | 114 | 3 | 23 | SRCT SCHT | | FG | | 45 | 20 | | | | | | | | 100 | 30 | 2 | | 2 | | | |
| 114 | 117 | 3 | 23 | SRCT SCHT | | FG | | 30 | 25 | | | | | | | | 100 | 35 | 2 | | 4 | | | |
| 117 | 120 | 3 | 23 | SRCT SCHT | | FG | | 30 | 25 | | | | | | | | 100 | 35 | 2 | | 4 | | | |
| 120 | 123 | 3 | 19 | SRCT SCHT | FAULT | FG | | 2 | 65 | 1 | 1 | | | | | | 100 | 25 | .5 | | 5 | | | |
| 123 | 126 | 3 | 10 | SRCT SCHT | | FG | | 2 | 60 | 3 | 1 | | | | | | 100 | 25 | .1 | | 5 | | | |
| 126 | 129 | 3 | 10 | SRCT SCHT | | FG | | 2 | 65 | 2 | 1 | | | | | | 100 | 22 | 1 | | 5 | | | |
| 129 | 132 | 3 | 20 | SRCT SCHT | | FG | | 2 | 65 | 2 | 2 | | | | | | 100 | 22 | 1 | | 5 | | | |
| 132 | 135 | 3 | 21 | SRCT SCHT | | FG | | 25 | 30 | | 10 | | | | | | 100 | 20 | 1 | | 10 | | | |
| 135 | 138 | 3 | 25 | SRCT SCHT | | FG | | 15 | 40 | 1 | 10 | | | | | | 100 | 25 | .5 | | 8 | | | |
| 138 | 141 | 3 | 21 | SRCT SCHT | | FG | 1 | 3 | 60 | 1 | 8 | | | | | | 100 | 25 | .2 | | 2 | | | |
| 141 | 144 | 3 | 19 | SRCT SCHT | | FG | 1 | 2 | 65 | 1 | 3 | | | | | | 100 | 25 | 1 | | 1 | | | |
| 144 | 147.2 | 3.2 | 10 | SRCT SCHT | | FRAC | 15 | | 40 | | 10 | | | | | | | 30 | | | | | | |
| 147.2 | 152.1 | 4.7 | 10 | SRCT SCHT | | FRAC | 12 | .1 | 50 | | 8 | | | | | | | 30 | | | | | | |
| 151.1 | 154.84 | 2.74 | 10 | SRCT SCHT | | FRAC | 12 | | 55 | | 5 | | | | | | | 30 | | | | | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8811 | 9570.1 | 9810.8 | 1634.4 | 90 | 60 | 212.75 | | STRIKE EXTENT OF B-ZONE MINERALIZATION. NO ACID TEST. #HOI |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | | | | | FRAC | 12 | | 55 | | 5 | | | | | | | 30 | | | | | | |
| 154.84 | 157.89 | 3.1 | 10 | SRCT SCHT | | FRAC | 12 | | 55 | | 5 | | | | | | | 30 | | | | | | |
| 157.89 | 160.93 | 3.1 | 10 | SRCT SCHT | | FRAC | 12 | | 55 | | 2 | | | | | | | 28 | | | | | | |
| 160.93 | 163.85 | 2.92 | 10 | SRCT SCHT | | FRAC | 5 | 10 | 55 | | 45 | .1 | | | | | 50 | .1 | | | | | | |
| 163.85 | 166.15 | 2.3 | 43 | ANDS DYKE | | FRAC | 12 | .1 | 55 | 1 | 3 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 166.15 | 167.03 | .88 | 12 | SRCT SCHT | | FRAC | 12 | 1 | 55 | 1 | 3 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 167.03 | 170.08 | 3.05 | 19 | SRCT SCHT | | FRAC | 12 | .1 | 55 | 1 | | | | | | | 100 | 28 | .1 | | .1 | | | |
| 170.08 | 171 | .92 | 19 | SRCT SCHT | | FRAC | | | | | 40 | .1 | | | | | 50 | .1 | | | | | | |
| 171 | 171.8 | .8 | 33 | ANDS DYKE | | FRAC | 13 | .1 | 53 | 1 | 3 | | | | | | 100 | 23 | .1 | | .1 | | | |
| 171.8 | 173.3 | 1.5 | 10 | SRCT SCHT | | FRAC | 15 | .1 | 53 | 1 | 5 | | | | | | 100 | 23 | .1 | | .1 | | | |
| 173.3 | 176.17 | 2.87 | 10 | SRCT SCHT | | FRAC | 13 | .1 | 53 | 1 | 5 | | | | | | 100 | 23 | .1 | | .1 | | | |
| 176.17 | 179.22 | 3.05 | 19 | SRCT SCHT | | FRAC | 13 | .1 | 50 | 2 | 4 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 179.22 | 182.27 | 3.05 | 19 | SRCT SCHT | | FRAC | | .1 | 50 | | | | | | | | 100 | 25 | .1 | | .1 | | | |
| 182.27 | 185.38 | 3.11 | 12 | SRCT SCHT | | FRAC | 20 | 1 | 50 | 2 | 2 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 185.38 | 188.37 | 2.99 | 19 | SRCT SCHT | | FRAC | 18 | .1 | 50 | 1 | 3 | | | | | | 100 | 28 | .1 | | 1 | | | |
| 188.37 | 191.41 | 3.04 | 12 | SRCT SCHT | | FRAC | 15 | .1 | 50 | 1 | 4 | | | 1 | | | 100 | 28 | .1 | | 1 | | | |
| 191.41 | 194.46 | 3.05 | 10 | SRCT SCHT | | FRAC | 13 | .1 | 50 | 1 | 10 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 194.46 | 197.51 | 3.05 | 10 | SRCT SCHT | | FRAC | 13 | 1 | 50 | 1 | 10 | | | | | | 100 | 25 | .1 | | 1 | | | |
| 197.71 | 200.58 | 3.07 | 10 | SRCT SCHT | | FRAC | 13 | .1 | 50 | 1 | 10 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 200.58 | 205.67 | 3.03 | 10 | SRCT SCHT | | FRAC | 13 | .1 | 50 | 1 | 10 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 205.67 | 206.65 | 3.04 | 12 | SRCT SCHT | | FRAC | 12 | .1 | 50 | 1 | 10 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 206.65 | 209.7 | 3.05 | 19 | SRCT SCHT | FAULT | FRAC | 12 | 2 | 50 | 1 | 10 | | | | | | 100 | 25 | .1 | | .1 | | | |
| 209.7 | 212.75 | 2.95 | 19 | SRCT SCHT | FAULT | | | | | | | | | | | | | | | | | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 08:49:11 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8811 | 9570.1 | 9810.8 | 1634.4 | 90 | 60 | 212.75 | | STRIKE EXTENT OF B-ZONE MINERALIZATION. NO ACID TEST. #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0.00 | 3.05 | | 3.05 | | | | | | | | | | | | |
| 3.05 | 7 | 9652 | 3.95 | 3.46 | 130 | | .1 | | 314 | 66 | 5.07 | 40 | 115 | | |
| 7 | 9 | 9653 | 2 | 1.48 | 85 | | .1 | | 494 | 485 | 4.29 | 48 | 1644 | | |
| 9 | 11.75 | 9654 | 2.75 | 2.58 | 10 | | .1 | | 305 | 339 | 3.94 | 99 | 2243 | | |
| 11.75 | 13.75 | 9655 | 2 | .64 | 120 | | .1 | | 226 | 21 | 3.93 | 44 | 36 | | |
| 13.75 | 15.5 | 9656 | 1.75 | .98 | 365 | | 1.1 | | 1316 | 86 | 4.92 | 48 | 246 | | |
| 15.5 | 18.5 | 9657 | 3 | 2.66 | 350 | | 1.9 | | 385 | 305 | 4.54 | 38 | 513 | | |
| 18.5 | 21.5 | 9658 | 3 | 2.78 | 120 | | .4 | | 485 | 262 | 4.94 | 44 | 485 | | |
| 21.5 | 24.5 | 9659 | 3 | 2.65 | 70 | | .1 | | 447 | 189 | 4.91 | 31 | 1515 | | |
| 24.5 | 27.5 | 9660 | 3 | 2.85 | 45 | | .1 | | 450 | 159 | 4.88 | 30 | 613 | | |
| 27.5 | 30.5 | 9661 | 3 | 2.74 | 110 | | .7 | | 547 | 803 | 4.93 | 40 | 279 | | |
| 30.5 | 33.5 | 9662 | 3 | 2.54 | 70 | | .1 | | 690 | 73 | 4.73 | 29 | 434 | | |
| 33.5 | 36.5 | 9663 | 3 | 2.23 | 70 | | .1 | | 753 | 143 | 5.17 | 73 | 627 | | |
| 36.5 | 39.5 | 9664 | 3 | 3 | 40 | | .1 | | 616 | 172 | 4.81 | 49 | 970 | | |
| 39.5 | 42.5 | 9665 | 3 | 2.85 | 60 | | .1 | | 574 | 134 | 4.32 | 43 | 1003 | | |
| 42.5 | 45.5 | 9666 | 3 | 2.8 | 90 | | .1 | | 662 | 221 | 4.58 | 56 | 1068 | | |
| 45.5 | 48.4 | 9667 | 2.9 | 2.18 | 110 | | .1 | | 1952 | 155 | 4.68 | 37 | 1183 | | |
| 48.4 | 51.0 | 9668 | 2.6 | 1.85 | 50 | | .1 | | 192 | 450 | 9.00 | 17 | 2783 | | |
| 51.0 | 54 | 9669 | 3 | 2.65 | 490 | | 4.2 | | 13384 | 112 | 7.65 | 153 | 242 | 1.39 | |
| 54 | 57 | 9670 | 3 | 2.65 | 630 | | 2.4 | | 11899 | 99 | 6.32 | 19 | 849 | 1.22 | |
| 57 | 60 | 9671 | 3 | 2.72 | 520 | | 3.7 | | 11216 | 343 | 6.48 | 110 | 1842 | 1.15 | |
| 60 | 63 | 9672 | 3 | 2.54 | 440 | | 3.1 | | 9426 | 132 | 5.52 | 31 | 1410 | 1.05 | |
| 63 | 66 | 9673 | 3 | 2.4 | 410 | | 2.6 | | 10126 | 121 | 5.26 | 29 | 612 | 1.06 | |
| 66 | 69 | 9674 | 3 | 2.1 | 520 | | 2.4 | | 13759 | 51 | 5.04 | 18 | 145 | 1.33 | |
| 69 | 72 | 9675 | 3 | .79 | 330 | | 2.5 | | 5265 | 42 | 4.35 | 18 | 48 | .57 | |
| 72 | 75 | 9676 | 3 | 1.42 | 250 | | 2.3 | | 11101 | 32 | 5.09 | 25 | 24 | 1.19 | |
| 75 | 78 | 9677 | 3 | 1.9 | 380 | | 2.5 | | 12301 | 114 | 5.08 | 38 | 127 | 1.24 | |
| 78 | 81 | 9678 | 3 | 2.16 | 360 | | 2.5 | | 12124 | 383 | 5.24 | 32 | 35 | 1.27 | |
| 81 | 84 | 9679 | 3 | 1.21 | 530 | | 1.6 | | 8979 | 101 | 5.72 | 30 | 158 | .97 | |
| 84 | 87 | 9680 | 3 | 1.25 | 360 | | 1.9 | | 8762 | 129 | 4.46 | 54 | 138 | .96 | |
| 87 | 90 | 9681 | 3 | 1.6 | 420 | | 2.2 | | 13110 | 89 | 5.42 | 28 | 103 | 1.35 | |
| 90 | 93 | 9682 | 3 | .79 | 500 | | 3.8 | | 20000 | 107 | 6.82 | 25 | 117 | 3.06 | |
| 93 | 96 | 9683 | 3 | .39 | 360 | | 2.4 | | 18472 | 76 | 4.60 | 43 | 66 | 1.94 | |
| 96 | 99 | 9684 | 3 | .46 | 320 | | 2.6 | | 14157 | 175 | 4.44 | 28 | 236 | 1.47 | |
| 99 | 102 | 9685 | 3 | .35 | 250 | | 2.1 | | 9497 | 106 | 3.94 | 23 | 258 | 1.01 | |
| 102 | 105 | 9686 | 3 | .6 | 220 | | 1.6 | | 7460 | 90 | 3.42 | 20 | 213 | .81 | |
| 105 | 108 | 9687 | 3 | .47 | 260 | | 2.9 | | 11347 | 100 | 4.8 | 20 | 143 | 1.24 | |
| 108 | 111 | 9688 | 3 | .7 | 420 | | .1 | | 11831 | 212 | 5.97 | 211 | 39 | 1.29 | |
| 111 | 114 | 9689 | 3 | 2.87 | 690 | | 9.3 | | 12369 | 441 | 8.67 | 566 | 38 | 1.30 | |
| 114 | 117 | 9690 | 3 | 2.43 | 700 | | 4.1 | | 14060 | 188 | 6.75 | 21 | 193 | 1.51 | |
| 117 | 120 | 9691 | 3 | 2.07 | 530 | | 5.2 | | 13519 | 1825 | 5.34 | 444 | 86 | 1.44 | |
| 120 | 123 | 9692 | 3 | .79 | 310 | | 1.9 | | 10947 | 40 | 3.49 | 20 | 26 | 1.28 | |
| 123 | 126 | 9693 | 3 | .74 | 490 | | 2.6 | | 12860 | 132 | 3.98 | 38 | 209 | 1.34 | |
| 126 | 129 | 9694 | 3 | .7 | 370 | | 2.6 | | 12357 | 46 | 2.60 | 43 | 15 | 1.38 | |
| 129 | 132 | 9695 | 3 | .5 | 350 | | 2.2 | | 13794 | 91 | 4.16 | 22 | 94 | 1.35 | |
| 132 | 135 | 9696 | 3 | 1.5 | 460 | | 2.9 | | 15355 | 28 | 4.15 | 37 | 32 | 1.7 | |
| 135 | 138 | 9697 | 3 | 2.7 | 500 | | 2.9 | | 12793 | 37 | 5.35 | 30 | 33 | 1.41 | |
| 138 | 141 | 9698 | 3 | 2.5 | 420 | | 1.9 | | 10990 | 14 | 4.41 | 31 | 48 | 1.22 | |
| 141 | 144 | 9699 | 3 | 2.84 | 390 | | 1.9 | | 11326 | 44 | 4.86 | 36 | 31 | 1.17 | |
| 144 | 147.2 | 9700 | 3.2 | 3.3 | 340 | | 1.6 | | 9276 | 110 | 4.66 | 44 | 33 | 1.06 | |
| 147.2 | 152.1 | 9701 | 4.7 | 4.3 | 380 | | 1.4 | | 11942 | 61 | 4.95 | 22 | 55 | 1.24 | |
| 151.1 | 154.84 | 9702 | 2.74 | 3.2 | 240 | | 1.3 | | 13943 | 21 | 5.07 | 19 | 27 | 1.37 | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8811 | 9570.1 | 9810.8 | 1634.4 | 90 | 60 | 212.75 | | STRIKE EXTENT OF B-ZONE MINERALIZATION. NO ACID TEST. #HO |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 154.84 | 157.89 | 9703 | 3.1 | 3.9 | 340 | | 2.9 | | 15828 | 315 | 7.25 | 849 | 11 | 1.42 | |
| 157.89 | 160.93 | 9704 | 3.1 | 3.1 | 330 | | 1.8 | | 20000 | 32 | 5.40 | 37 | 32 | 1.80 | |
| 160.93 | 163.85 | 9705 | 2.92 | 2.3 | 215 | | 1.5 | | 10333 | 157 | 3.92 | 157 | 195 | .85 | |
| 163.85 | 166.15 | 9706 | 2.3 | 1.52 | 15 | | .1 | | 1897 | 200 | 2.73 | 19 | 984 | .18 | |
| 166.15 | 167.03 | 9707 | .88 | .85 | 170 | | 1.3 | | 6806 | 87 | 3.87 | 180 | 83 | .7 | |
| 167.03 | 170.08 | 9708 | 3.05 | 2.4 | 120 | | 1.1 | | 8923 | 87 | 3.55 | 104 | 501 | .93 | |
| 170.08 | 171 | 9709 | .92 | .8 | 160 | | .7 | | 6490 | 11 | 4.89 | 33 | 35 | .69 | |
| 171 | 171.8 | 9710 | .8 | .8 | 20 | | .1 | | 1594 | 237 | 6.65 | 46 | 1375 | .16 | |
| 171.8 | 173.3 | 9711 | 1.5 | 1.2 | 130 | | .8 | | 8072 | 86 | 3.82 | 61 | 526 | .88 | |
| 173.3 | 176.17 | 9712 | 2.87 | 2.7 | 80 | | .1 | | 1796 | 126 | 4.66 | 34 | 762 | .20 | |
| 176.17 | 179.22 | 9713 | 3.05 | 3 | 90 | | .1 | | 1935 | 112 | 5.13 | 32 | 963 | .20 | |
| 179.22 | 182.27 | 9714 | 3.05 | 2.8 | 1 | | .1 | | 2746 | 140 | 5.45 | 37 | 1303 | .28 | |
| 182.27 | 185.38 | 9715 | 3.11 | 3 | 50 | | .1 | | 1686 | 1174 | 5.17 | 41 | 1633 | .17 | |
| 185.38 | 188.37 | 9716 | 2.99 | 2.9 | 70 | | .2 | | 1019 | 272 | 4.80 | 38 | 1367 | .11 | |
| 188.37 | 191.41 | 9717 | 3.04 | 2.9 | 100 | | 2.1 | | 851 | 899 | 4.60 | 54 | 1197 | .09 | |
| 191.41 | 194.46 | 9718 | 3.05 | 2.95 | 130 | | .8 | | 4155 | 312 | 7.12 | 160 | 745 | .41 | |
| 194.46 | 197.51 | 9719 | 3.05 | 2.7 | 190 | | .3 | | 5596 | 164 | 7.34 | 27 | 793 | .61 | |
| 197.71 | 200.58 | 9720 | 3.07 | 2.59 | 100 | | 1.1 | | 3701 | 269 | 7.57 | 151 | 961 | .38 | |
| 200.58 | 205.67 | 9721 | 3.09 | 1.98 | 120 | | 1.1 | | 4282 | 210 | 6.13 | 53 | 688 | .49 | |
| 205.67 | 206.65 | 9722 | 3.04 | 1 | 140 | | .2 | | 4544 | 173 | 7.31 | 52 | 410 | .48 | |
| 206.65 | 209.7 | 9723 | 3.05 | .28 | 110 | | 1.1 | | 2086 | 86 | 8.14 | 86 | 158 | .22 | |
| 209.7 | 212.75 | 9724 | 2.95 | .28 | 90 | | .1 | | 2391 | 69 | 5.90 | 13 | 187 | .26 | |

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656

REPORT NUMBER: 881035 AA JOB NUMBER: 881035 WESTERN CON. MINING CORP. 

| SAMPLE # | Cu % |
|---|---|
| C88-9675 | .57 |
| C88-9676 | 1.19 |
| C88-9677 | 1.24 |
| C88-9678 | 1.27 |
| C88-9679 | .97 |
| C88-9680 | .96 |
| C88-9681 | 1.35 |
| C88-9682 | 3.06 |
| C88-9683 | 1.94 |
| C88-9684 | 1.47 |
| C88-9685 | 1.01 |
| C88-9686 | .81 |
| C88-9687 | 1.24 |
| C88-9688 | 1.29 |
| C88-9689 | 1.30 |
| C88-9690 | 1.51 |
| C88-9691 | 1.44 |
| C88-9692 | 1.28 |
| C88-9693 | 1.34 |
| C88-9694 | 1.36 |



DETECTION LIMIT .01
1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed:

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-9695 | 1.35 |
| C88-9696 | 1.70 |
| C88-9697 | 1.41 |
| C88-9698 | 1.22 |
| C88-9699 | 1.17 |
| C88-9700 | 1.06 |
| C88-9701 | 1.24 |
| C88-9702 | 1.37 |
| C88-9703 | 1.42 |
| C88-9704 | 1.80 |
| C88-9705 | .85 |
| C88-9706 | .18 |
| C88-9707 | .70 |
| C88-9708 | .93 |
| C88-9709 | .69 |
| C88-9710 | .16 |
| C88-9711 | .88 |
| C88-9712 | .20 |
| C88-9713 | .20 |
| C88-9714 | .28 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-9715 | .17 |
| C88-9716 | .11 |
| C88-9717 | .09 |
| C88-9718 | .41 |
| C88-9719 | .61 |
| C88-9720 | .38 |
| C88-9721 | .49 |
| C88-9722 | .48 |
| C88-9723 | .22 |
| C88-9724 | .26 |
| C88-9669 | 1.39 |
| C88-9670 | 1.22 |
| C88-9671 | 1.15 |
| C88-9672 | 1.05 |
| C88-9673 | 1.06 |
| C88-9674 | 1.33 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717



REPORT #: 881151 PA

WESTERN CANADIAN MINING CORP.

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88 - 9652 | 0.1 | 0.72 | 40 | 130 | <3 | 14 | 4 | 0.18 | 0.7 | 14 | 24 | 314 | 5.07 | 0.05 | 0.44 | 115 | 4 | 0.01 | 5 | 0.22 | 26 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 66 |
| C88 - 9653 | 0.1 | 2.29 | 48 | 85 | <3 | 68 | 6 | 0.33 | 2.7 | 12 | 13 | 494 | 4.29 | 0.07 | 1.89 | 1644 | 4 | 0.02 | 5 | 0.24 | 51 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 485 |
| C88 - 9654 | 0.1 | 2.37 | 99 | 10 | <3 | 73 | 3 | 1.46 | 1.2 | 15 | 14 | 305 | 3.94 | 0.22 | 1.96 | 2243 | 2 | 0.01 | 5 | 0.22 | 26 | <3 | <5 | <2 | <2 | 59 | <5 | <3 | 339 |
| C88 - 9655 | 0.1 | 0.36 | 44 | 120 | <3 | 18 | <3 | 0.02 | 0.5 | 9 | 34 | 226 | 3.93 | 0.01 | 0.06 | 36 | 4 | 0.01 | 4 | 0.05 | 70 | <3 | <5 | <2 | <2 | 5 | <5 | <3 | 21 |
| C88 - 9656 | 1.1 | 0.28 | 48 | 365 | <3 | 17 | <3 | 0.02 | 1.0 | 11 | 25 | 1316 | 4.92 | 0.02 | 0.11 | 246 | 6 | 0.02 | 5 | 0.03 | 36 | <3 | <5 | <2 | <2 | 2 | <5 | <3 | 86 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: BB115I PA

WESTERN CANADIAN MINING CORP.



| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88 - 9669 | 4.2 | 0.41 | 153 | 490 | <3 | 11 | 4 | 0.23 | 1.4 | 10 | 96 | 13384 | 7.65 | 0.07 | 0.08 | 242 | 6 | 0.01 | 3 | 0.15 | 30 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 112 |
| C88 - 9670 | 2.4 | 0.69 | 19 | 630 | <3 | 12 | <3 | 0.54 | 2.1 | 13 | 95 | 11899 | 6.32 | 0.12 | 0.24 | 849 | 9 | 0.01 | 3 | 0.14 | <2 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 99 |
| C88 - 9671 | 3.7 | 0.35 | 110 | 520 | <3 | 10 | <3 | 0.39 | 1.8 | 17 | 60 | 11216 | 6.48 | 0.09 | 0.11 | 1842 | 5 | 0.01 | 2 | 0.14 | 22 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 343 |
| C88 - 9672 | 3.1 | 0.27 | 31 | 440 | <3 | 12 | <3 | 0.32 | 1.2 | 15 | 59 | 9426 | 5.52 | 0.07 | 0.04 | 1410 | 5 | 0.01 | 3 | 0.12 | 18 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 132 |
| C88 - 9673 | 2.6 | 0.39 | 29 | 410 | <3 | 12 | <3 | 0.23 | 1.9 | 11 | 115 | 10126 | 5.26 | 0.06 | 0.03 | 612 | 9 | 0.01 | 4 | 0.13 | 52 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 121 |
| C88 - 9674 | 2.4 | 0.91 | 18 | 520 | <3 | 13 | <3 | 0.14 | 1.1 | 10 | 64 | 13759 | 5.04 | 0.04 | 0.30 | 145 | 7 | 0.01 | 3 | 0.16 | 6 | <3 | <5 | <2 | <2 | 17 | <5 | <3 | 51 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

ANOMALOUS RESULTS:
FURTHER ANALYSES
BY ALTERNATE

VANGEOCHEM LAB LIM
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5

REPORT #: 880849 PA

WESTERN CON MINING CORP.



| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88 - 9657 | 1.9 | 0.33 | 36 | 350 | <3 | 26 | <3 | 0.33 | 3.2 | 13 | 15 | 385 | 4.54 | 0.08 | 0.21 | 513 | 2 | 0.02 | 5 | 0.17 | 194 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 305 |
| C88 - 9658 | 0.4 | 0.45 | 44 | 120 | <3 | 27 | <3 | 0.29 | 2.4 | 13 | 36 | 485 | 4.94 | 0.08 | 0.27 | 485 | 3 | 0.02 | 6 | 0.17 | 130 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 262 |
| C88 - 9659 | 0.1 | 0.62 | 31 | 70 | <3 | 34 | <3 | 0.70 | 1.9 | 17 | 16 | 447 | 4.91 | 0.15 | 0.86 | 1515 | 3 | 0.02 | 6 | 0.19 | 55 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 189 |
| C88 - 9660 | 0.1 | 0.52 | 30 | 45 | <3 | 27 | <3 | 0.45 | 1.9 | 14 | 24 | 450 | 4.88 | 0.11 | 0.48 | 613 | 2 | 0.02 | 5 | 0.19 | 64 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 159 |
| C88 - 9661 | 0.7 | 0.58 | 40 | 110 | <3 | 23 | <3 | 0.31 | 5.3 | 15 | 25 | 547 | 4.93 | 0.08 | 0.34 | 279 | 4 | 0.03 | 7 | 0.21 | 260 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 803 |
| C88 - 9662 | 0.1 | 0.69 | 29 | 70 | <3 | 27 | <3 | 0.41 | 1.7 | 15 | 25 | 690 | 4.73 | 0.10 | 0.59 | 424 | 2 | 0.01 | 6 | 0.21 | 39 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 73 |
| C88 - 9663 | 0.1 | 0.96 | 73 | 70 | <3 | 25 | <3 | 0.49 | 1.6 | 15 | 23 | 753 | 5.17 | 0.12 | 0.94 | 627 | 4 | 0.02 | 8 | 0.21 | 39 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 143 |
| C88 - 9664 | 0.1 | 1.06 | 49 | 40 | <3 | 26 | <3 | 0.53 | 1.6 | 16 | 28 | 616 | 4.81 | 0.12 | 1.16 | 970 | 3 | 0.01 | 7 | 0.20 | 38 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 172 |
| C88 - 9665 | 0.1 | 1.09 | 43 | 60 | <3 | 25 | <3 | 0.62 | 1.2 | 13 | 37 | 574 | 4.32 | 0.14 | 1.12 | 1003 | 4 | 0.01 | 6 | 0.19 | 32 | <3 | <5 | <2 | <2 | 18 | <5 | <3 | 134 |
| C88 - 9666 | 0.1 | 0.89 | 56 | 90 | <3 | 27 | <3 | 0.61 | 1.7 | 16 | 37 | 662 | 4.58 | 0.13 | 0.94 | 1068 | 3 | 0.01 | 7 | 0.20 | 53 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 221 |
| C88 - 9667 | 0.1 | 0.41 | 37 | 110 | <3 | 23 | <3 | 0.64 | 1.4 | 15 | 35 | 1952 | 4.68 | 0.13 | 0.52 | 1183 | 5 | 0.01 | 5 | 0.17 | 47 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 155 |
| C88 - 9668 | 0.1 | 3.81 | 17 | 50 | <3 | 354 | 6 | 0.55 | 2.7 | 35 | 20 | 192 | 9.00 | 0.13 | 2.25 | 2783 | 7 | 0.03 | 1 | <0.01 | 19 | <3 | <5 | <2 | <2 | 23 | <5 | <3 | 450 |
| C88 - 9675 | 2.5 | 0.44 | 18 | 330 | <3 | 23 | <3 | 0.03 | 1.1 | 9 | 58 | 5265 | 4.35 | 0.03 | 0.09 | 48 | 8 | 0.02 | 1 | 0.08 | 25 | <3 | <5 | <2 | <2 | 5 | <5 | <3 | 42 |
| C88 - 9676 | 2.3 | 0.22 | 25 | 250 | <3 | 14 | <3 | 0.01 | 1.4 | 9 | 66 | 11101 | 5.09 | 0.04 | 0.04 | 24 | 7 | 0.02 | 3 | 0.03 | 26 | <3 | <5 | <2 | <2 | 3 | <5 | <3 | 32 |
| C88 - 9677 | 2.5 | 0.81 | 38 | 380 | <3 | 16 | 4 | 0.11 | 1.7 | 9 | 77 | 12301 | 5.08 | 0.05 | 0.27 | 127 | 9 | 0.02 | 3 | 0.17 | 34 | <3 | <5 | <2 | <2 | 5 | <5 | <3 | 114 |
| C88 - 9678 | 2.5 | 0.84 | 32 | 360 | <3 | 14 | 4 | 0.13 | 3.4 | 15 | 84 | 12124 | 5.24 | 0.05 | 0.08 | 35 | 10 | 0.02 | 5 | 0.25 | 46 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 382 |
| C88 - 9679 | 1.6 | 1.21 | 30 | 530 | <3 | 13 | 4 | 0.17 | 1.4 | 15 | 55 | 8979 | 5.72 | 0.07 | 0.63 | 158 | 10 | 0.02 | 4 | 0.24 | 17 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 101 |
| C88 - 9680 | 1.9 | 1.08 | 54 | 360 | <3 | 18 | 3 | 0.17 | 1.1 | 12 | 62 | 8762 | 4.46 | 0.06 | 0.51 | 138 | 8 | 0.02 | 6 | 0.22 | 102 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 129 |
| C88 - 9681 | 2.2 | 0.91 | 28 | 420 | <3 | 15 | 5 | 0.15 | 1.4 | 13 | 55 | 13110 | 5.42 | 0.06 | 0.35 | 103 | 11 | 0.02 | 3 | 0.22 | 97 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 89 |
| C88 - 9682 | 3.8 | 1.01 | 25 | 500 | <3 | 12 | 12 | 0.08 | 2.6 | 14 | 104 | >20000 | 6.82 | 0.04 | 0.49 | 117 | 11 | 0.02 | 5 | 0.16 | 93 | <3 | <5 | <2 | <2 | 4 | <5 | <3 | 107 |
| C88 - 9683 | 2.4 | 0.86 | 43 | 360 | <3 | 14 | 5 | 0.14 | 1.1 | 11 | 80 | 18472 | 4.60 | 0.06 | 0.21 | 66 | 11 | 0.02 | 10 | <0.01 | 107 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 76 |
| C88 - 9684 | 2.6 | 0.93 | 28 | 320 | <3 | 15 | 4 | 0.17 | 3.0 | 11 | 62 | 14157 | 4.44 | 0.06 | 0.19 | 236 | 7 | 0.02 | 6 | 0.21 | 133 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 175 |
| C88 - 9685 | 2.1 | 1.08 | 23 | 250 | <3 | 17 | <3 | 0.17 | 1.2 | 9 | 49 | 9497 | 3.94 | 0.06 | 0.76 | 258 | 7 | 0.01 | 4 | 0.19 | 27 | <3 | <5 | <2 | <2 | 34 | <5 | <3 | 106 |
| C88 - 9686 | 1.6 | 1.28 | 20 | 220 | <3 | 21 | <3 | 0.18 | 1.5 | 9 | 70 | 7460 | 3.42 | 0.06 | 0.84 | 213 | 5 | 0.01 | 5 | 0.19 | 23 | <3 | <5 | <2 | <2 | 53 | <5 | <3 | 90 |
| C88 - 9687 | 2.9 | 1.10 | 20 | 260 | <3 | 15 | 6 | 0.15 | 1.7 | 13 | 107 | 11347 | 4.88 | 0.06 | 0.65 | 143 | 8 | 0.02 | 4 | 0.15 | 13 | <3 | <5 | <2 | <2 | 78 | <5 | <3 | 100 |
| C88 - 9688 | 0.1 | 0.38 | 211 | 420 | <3 | 15 | 5 | 0.15 | 1.7 | 12 | 88 | 11831 | 5.97 | 0.06 | 0.06 | 39 | 5 | 0.02 | 3 | 0.14 | 101 | <3 | <5 | <2 | <2 | 27 | <5 | <3 | 212 |
| C88 - 9689 | 9.3 | 0.15 | 566 | 690 | <3 | 10 | 11 | 0.13 | 1.6 | 12 | 36 | 12369 | 8.67 | 0.06 | 0.02 | 38 | 14 | 0.03 | 1 | 0.13 | 367 | <3 | <5 | <2 | <2 | 5 | <5 | <3 | 441 |
| C88 - 9690 | 4.1 | 0.18 | 21 | 700 | <3 | 11 | 10 | 0.14 | 2.4 | 10 | 61 | 14060 | 6.75 | 0.06 | 0.02 | 193 | 6 | 0.02 | 1 | 0.13 | 107 | <3 | <5 | <2 | 2 | 8 | <5 | <3 | 188 |
| C88 - 9691 | 5.2 | 0.32 | 444 | 520 | <3 | 12 | 3 | 0.15 | 4.8 | 10 | 102 | 13519 | 5.34 | 0.06 | 0.03 | 86 | 14 | 0.06 | 2 | 0.15 | 1047 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 1825 |
| C88 - 9692 | 1.9 | 0.45 | 20 | 310 | <3 | 15 | <3 | 0.16 | 1.1 | 9 | 83 | 10947 | 3.49 | 0.06 | 0.03 | 26 | 9 | 0.01 | 3 | 0.16 | 26 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 40 |
| C88 - 9693 | 2.6 | 0.68 | 38 | 490 | <3 | 13 | <3 | 0.16 | 3.9 | 11 | 51 | 12860 | 3.98 | 0.05 | 0.02 | 209 | 20 | 0.02 | 7 | 0.22 | 71 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 132 |
| C88 - 9694 | 2.6 | 0.44 | 43 | 370 | <3 | 18 | <3 | 0.16 | 1.8 | 11 | 24 | 12357 | 2.60 | 0.05 | 0.02 | 15 | 20 | 0.01 | 4 | 0.19 | 45 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 46 |
| C88 - 9695 | 2.2 | 1.06 | 22 | 350 | <3 | 17 | 7 | 0.24 | 1.5 | 22 | 86 | 13794 | 4.16 | 0.07 | 0.58 | 94 | 27 | 0.01 | 12 | 0.25 | 16 | <3 | <5 | <2 | <2 | 30 | <5 | <3 | 91 |
| C88 - 9696 | 2.9 | 0.36 | 37 | 460 | <3 | 13 | 3 | 0.16 | 1.2 | 13 | 88 | 15355 | 4.15 | 0.05 | 0.04 | 32 | 23 | 0.01 | 12 | 0.19 | 13 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 28 |
| C88 - 9697 | 2.9 | 0.39 | 30 | 500 | <3 | 12 | 6 | 0.19 | 1.3 | 21 | 41 | 12793 | 5.35 | 0.07 | 0.04 | 33 | 26 | 0.02 | 15 | 0.22 | 11 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 37 |
| C88 - 9698 | 1.9 | 0.42 | 31 | 420 | <3 | 13 | <3 | 0.22 | 1.1 | 23 | 51 | 10990 | 4.41 | 0.07 | 0.03 | 48 | 38 | 0.01 | 17 | 0.24 | 7 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 14 |
| C88 - 9699 | 1.9 | 0.46 | 36 | 390 | <3 | 11 | <3 | 0.19 | 1.7 | 15 | 52 | 11326 | 4.86 | 0.06 | 0.03 | 31 | 29 | 0.01 | 19 | 0.20 | 27 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 44 |
| C88 - 9700 | 1.6 | 0.46 | 44 | 340 | <3 | 11 | <3 | 0.17 | 1.6 | 14 | 53 | 9276 | 4.66 | 0.07 | 0.10 | 33 | 26 | 0.02 | 6 | 0.19 | 26 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 110 |
| C88 - 9701 | 1.4 | 0.89 | 22 | 380 | <3 | 12 | 6 | 0.14 | 1.3 | 15 | 52 | 11942 | 4.95 | 0.05 | 0.51 | 55 | 19 | 0.01 | 13 | 0.25 | 23 | <3 | <5 | <2 | <2 | 153 | <5 | <3 | 61 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

( = Less than Minimum  is = Insufficient Sample  ns = No sample  ) = Greater than Maximum  AuFA = Fire assay/AAS

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5



REPORT #: 890849 PA

WESTERN CDN MINING CORP.

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88 - 9702 | 1.3 | 0.57 | 19 | 240 | <3 | 17 | 6 | 0.19 | 1.5 | 24 | 50 | 13943 | 5.07 | 0.05 | 0.10 | 27 | 26 | 0.01 | 18 | 0.28 | 12 | <3 | <5 | <2 | <2 | 221 | <5 | <3 |
| C88 - 9703 | 2.9 | 0.52 | 849 | 340 | <3 | 17 | 11 | 0.09 | 0.1 | 13 | 46 | 15828 | 7.25 | 0.04 | 0.02 | 11 | 12 | 0.02 | 13 | 0.24 | 92 | <3 | <5 | <2 | <2 | 335 | <5 | <3 |
| C88 - 9704 | 1.8 | 0.65 | 37 | 320 | <3 | 12 | 10 | 0.12 | 1.3 | 13 | 58 | >20000 | 5.40 | 0.04 | 0.12 | 32 | 14 | 0.01 | 8 | 0.26 | 5 | <3 | <5 | <2 | <2 | 415 | <5 | <3 |
| C88 - 9705 | 1.5 | 1.00 | 157 | 215 | <3 | 17 | <3 | 0.15 | 1.1 | 12 | 32 | 10333 | 3.92 | 0.04 | 0.63 | 195 | 31 | 0.01 | 9 | 0.27 | 27 | <3 | <5 | <2 | <2 | 398 | <5 | <3 |
| C88 - 9706 | 0.1 | 0.94 | 19 | 15 | <3 | 365 | <3 | 0.15 | 1.2 | 9 | 62 | 1897 | 2.73 | 0.05 | 0.33 | 984 | 5 | 0.02 | 4 | 0.10 | 12 | <3 | <5 | <2 | <2 | 61 | <5 | <3 |
| C88 - 9707 | 1.3 | 0.57 | 180 | 170 | <3 | 19 | <3 | 0.16 | 0.9 | 18 | 110 | 6806 | 3.87 | 0.04 | 0.19 | 83 | 19 | 0.01 | 14 | 0.16 | 18 | <3 | <5 | <2 | <2 | 22 | <5 | <3 |
| C88 - 9708 | 1.1 | 1.18 | 104 | 120 | <3 | 20 | <3 | 0.19 | 1.1 | 13 | 59 | 8923 | 3.55 | 0.05 | 1.40 | 501 | 15 | 0.01 | 12 | 0.20 | 13 | <3 | <5 | <2 | <2 | 21 | <5 | <3 |
| C88 - 9709 | 0.7 | 0.44 | 33 | 160 | <3 | 15 | <3 | 0.18 | 0.9 | 15 | 60 | 5490 | 4.89 | 0.05 | 0.03 | 35 | 33 | 0.01 | 10 | 0.18 | 12 | <3 | <5 | <2 | <2 | 25 | <5 | <3 |
| C88 - 9710 | 0.1 | 3.37 | 46 | 20 | <3 | 146 | 5 | 0.31 | 1.5 | 13 | 35 | 1594 | 6.65 | 0.07 | 1.92 | 1375 | 10 | 0.02 | <1 | 0.29 | 15 | <3 | <5 | <2 | <2 | 28 | <5 | <3 |
| C88 - 9711 | 0.8 | 1.64 | 61 | 130 | <3 | 17 | <3 | 0.17 | 1.0 | 13 | 71 | 8072 | 3.82 | 0.04 | 1.24 | 526 | 32 | 0.01 | 10 | 0.26 | 21 | <3 | <5 | <2 | <2 | 81 | <5 | <3 |
| C88 - 9712 | 0.1 | 1.56 | 34 | 80 | <3 | 17 | <3 | 0.15 | 1.3 | 14 | 45 | 1796 | 4.66 | 0.03 | 1.90 | 762 | 8 | 0.01 | 9 | 0.16 | 13 | <3 | <5 | <2 | <2 | 13 | <5 | <3 |
| C88 - 9713 | 0.1 | 1.61 | 32 | 90 | <3 | 15 | <3 | 0.17 | 1.5 | 17 | 23 | 1935 | 5.13 | 0.05 | 2.02 | 963 | 7 | 0.01 | 11 | 0.17 | 15 | <3 | <5 | <2 | <2 | 15 | <5 | <3 |
| C88 - 9714 | 0.1 | 1.74 | 37 | <5 | <3 | 14 | <3 | 0.18 | 1.5 | 16 | 33 | 2746 | 5.45 | 0.04 | 2.06 | 1303 | 17 | 0.01 | 11 | 0.18 | 12 | <3 | <5 | <2 | <2 | 17 | <5 | <3 |
| C88 - 9715 | 0.1 | 2.21 | 41 | 50 | <3 | 13 | 3 | 0.18 | 4.4 | 16 | 46 | 1686 | 5.17 | 0.05 | 2.80 | 1633 | 8 | 0.04 | 10 | 0.19 | 22 | <3 | <5 | <2 | <2 | 26 | <5 | <3 |
| C88 - 9716 | 0.2 | 1.93 | 38 | 70 | <3 | 14 | <3 | 0.19 | 1.5 | 13 | 38 | 1019 | 4.80 | 0.04 | 2.42 | 1367 | 4 | 0.01 | 7 | 0.20 | 15 | <3 | <5 | <2 | <2 | 36 | <5 | <3 |
| C88 - 9717 | 2.1 | 1.48 | 54 | 100 | <3 | 14 | <3 | 0.17 | 3.1 | 15 | 21 | 851 | 4.60 | 0.04 | 1.78 | 1197 | 5 | 0.03 | 10 | 0.19 | 63 | <3 | <5 | <2 | <2 | 69 | <5 | <3 |
| C88 - 9718 | 0.8 | 1.31 | 160 | 130 | <3 | 14 | 5 | 0.19 | 1.6 | 20 | 31 | 4155 | 7.12 | 0.06 | 1.08 | 745 | 16 | 0.02 | 12 | 0.23 | 64 | <3 | <5 | <2 | <2 | 197 | <5 | <3 |
| C88 - 9719 | 0.3 | 2.14 | 27 | 190 | <3 | 19 | 10 | 0.20 | 1.6 | 32 | 30 | 5596 | 7.34 | 0.06 | 1.82 | 793 | 36 | 0.02 | 19 | 0.37 | 10 | <3 | <5 | <2 | <2 | 899 | <5 | <3 |
| C88 - 9720 | 1.1 | 2.04 | 151 | 100 | <3 | 21 | 9 | 0.20 | 1.7 | 32 | 35 | 3701 | 7.57 | 0.06 | 2.19 | 961 | 22 | 0.02 | 19 | 0.24 | 21 | <3 | <5 | <2 | <2 | 232 | <5 | <3 |
| C88 - 9721 | 1.1 | 1.81 | 53 | 120 | <3 | 22 | 8 | 0.21 | 1.8 | 28 | 28 | 4232 | 6.13 | 0.05 | 1.82 | 688 | 25 | 0.02 | 15 | 0.26 | 17 | <3 | <5 | <2 | <2 | 228 | <5 | <3 |
| C88 - 9722 | 0.2 | 1.63 | 52 | 140 | <3 | 19 | 6 | 0.22 | 1.9 | 31 | 58 | 4544 | 7.31 | 0.06 | 1.60 | 410 | 13 | 0.02 | 30 | 0.24 | 8 | <3 | <5 | <2 | <2 | 185 | <5 | <3 |
| C88 - 9723 | 1.1 | 1.11 | 86 | 110 | <3 | 18 | 3 | 0.15 | 2.1 | 21 | 159 | 2086 | 8.14 | 0.05 | 1.11 | 158 | 6 | 0.02 | 117 | 0.17 | 21 | <3 | <5 | <2 | <2 | 164 | <5 | <3 |
| C88 - 9724 | 0.1 | 1.35 | 13 | 90 | <3 | 15 | <3 | 0.20 | 1.4 | 23 | 137 | 2391 | 5.90 | 0.06 | 1.28 | 187 | 10 | 0.01 | 88 | 0.20 | 11 | <3 | <5 | <2 | <2 | 88 | <5 | <3 |

ACME ANALYTICAL LABORATORIES LTD.
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DATE RECEIVED: SEP 2 1988
DATE REPORT MAILED: Sept. 8/88.

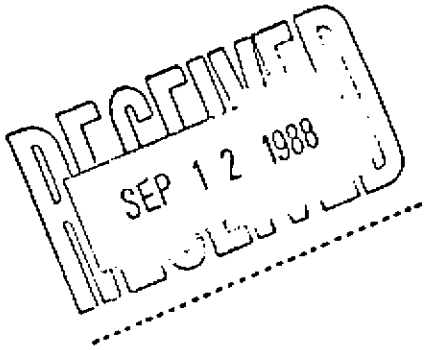
# GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK PULP AU** PT** PD** & RH** BY FA-MS.

ASSAYER: C. Leong, D.TOYE OR C.LEONG, CERTIFIED B.C. ASSAYERS

WESTERN CANADIAN MINING CORP. PROJECT 9101-12 FILE # 88-4171

| SAMPLE# | Cu PPM | Ag PPM | Au** PPB | Pt** PPB | Pd** PPB | Rh** PPB |
|---|---|---|---|---|---|---|
| C88-9669 | 14759 | 3.7 | 559 | 2 | 1 | 2 |
| C88-9670 | 12947 | 2.7 | 608 | 1 | 2 | 2 |
| C88-9671 | 11460 | 3.5 | 540 | 1 | 1 | 2 |
| C88-9672 | 10421 | 2.7 | 514 | 2 | 3 | 2 |
| C88-9673 | 10773 | 2.5 | 484 | 1 | 1 | 2 |
| C88-9674 | 14706 | 2.4 | 632 | 1 | 2 | 2 |
| C88-9724 | 2553 | .5 | 84 | 4 | 4 | 2 |
| STD C/FA-5X | 62 | 7.2 | 98 | 102 | 99 | 24 |



| SAMPLE# | Cu PPM | Ag PPM | Au** PPB | Pt** PPB | Pd** PPB | Rh** PPB |
|---|---|---|---|---|---|---|
| C88-9675 | 5412 | 2.3 | 280 | 1 | 4 | 2 |
| C88-9676 | 12533 | 2.7 | 304 | 1 | 11 | 2 |
| C88-9677 | 13027 | 2.6 | 381 | 2 | 2 | 2 |
| C88-9678 | 13063 | 2.5 | 390 | 1 | 9 | 2 |
| C88-9679 | 8553 | 1.9 | 456 | 3 | 2 | 2 |
| C88-9680 | 11012 | 2.7 | 448 | 2 | 2 | 2 |
| C88-9681 | 13627 | 2.4 | 540 | 2 | 8 | 2 |
| C88-9682 | 29533 | 3.1 | 676 | 1 | 2 | 2 |
| C88-9683 | 21543 | 2.4 | 430 | 3 | 2 | 2 |
| C88-9684 | 16860 | 2.4 | 336 | 2 | 2 | 2 |
| C88-9685 | 9877 | 2.4 | 316 | 1 | 4 | 2 |
| C88-9686 | 8089 | 2.2 | 244 | 2 | 2 | 2 |
| C88-9687 | 11456 | 3.1 | 280 | 6 | 17 | 2 |
| C88-9688 | 13647 | 5.6 | 482 | 4 | 3 | 2 |
| C88-9689 | 13960 | 11.7 | 884 | 6 | 2 | 2 |
| C88-9690 | 15905 | 5.1 | 1030 | 2 | 3 | 2 |
| C88-9691 | 15013 | 5.6 | 508 | 3 | 8 | 2 |
| C88-9692 | 12089 | 2.2 | 411 | 2 | 3 | 2 |
| C88-9693 | 12980 | 2.7 | 469 | 2 | 2 | 2 |
| C88-9694 | 13369 | 2.5 | 363 | 3 | 12 | 2 |
| C88-9695 | 13737 | 2.1 | 306 | 3 | 15 | 2 |
| C88-9696 | 15930 | 3.0 | 691 | 5 | 2 | 2 |
| C88-9697 | 14045 | 3.0 | 617 | 3 | 13 | 2 |
| C88-9698 | 12314 | 2.3 | 527 | 3 | 6 | 2 |
| C88-9699 | 12089 | 2.1 | 482 | 2 | 2 | 2 |
| C88-9700 | 10972 | 2.0 | 426 | 2 | 6 | 2 |
| C88-9701 | 13105 | 1.7 | 362 | 3 | 5 | 2 |
| C88-9702 | 12977 | 1.4 | 284 | 4 | 7 | 2 |
| C88-9703 | 13904 | 2.9 | 355 | 4 | 4 | 2 |
| C88-9704 | 18372 | 1.7 | 385 | 2 | 2 | 2 |
| C88-9705 | 8663 | 1.6 | 233 | 15 | 47 | 2 |
| C88-9706 | 2062 | .1 | 12 | 1 | 2 | 2 |
| STD C/FA-5X | 63 | 7.2 | 98 | 103 | 99 | 22 |

- ASSAY REQUIRED FOR CORRECT RESULT for Cu >10,000 ppm

| SAMPLE# | Cu PPM | Ag PPM | Au** PPB | Pt** PPB | Pd** PPB | Rh** PPB |
|---|---|---|---|---|---|---|
| C88-9707 | 7385 | 1.5 | 196 | 8 | 28 | 2 |
| C88-9708 | 9532 | 1.5 | 153 | 5 | 23 | 2 |
| C88-9709 | 6825 | 1.0 | 160 | 5 | 6 | 2 |
| C88-9710 | 1529 | .1 | 16 | 1 | 2 | 2 |
| C88-9711 | 8420 | 1.6 | 147 | 4 | 5 | 2 |
| C88-9712 | 1722 | .4 | 80 | 3 | 2 | 2 |
| C88-9713 | 1904 | .7 | 73 | 3 | 5 | 2 |
| C88-9714 | 2768 | 1.4 | 80 | 2 | 4 | 2 |
| C88-9715 | 1429 | 1.2 | 82 | 3 | 3 | 2 |
| C88-9716 | 967 | 1.5 | 79 | 2 | 2 | 2 |
| C88-9717 | 896 | 2.6 | 108 | 2 | 2 | 2 |
| C88-9718 | 3860 | 1.7 | 138 | 2 | 2 | 2 |
| C88-9719 | 6198 | 1.5 | 214 | 2 | 5 | 2 |
| C88-9720 | 4065 | 2.3 | 264 | 2 | 4 | 2 |
| C88-9721 | 4813 | 2.5 | 152 | 2 | 3 | 2 |
| C88-9722 | 4699 | 1.4 | 164 | 3 | 7 | 2 |
| C88-9723 | 1966 | 1.6 | 78 | 3 | 2 | 2 |
| STD C/FA-5X | 57 | 6.9 | 96 | 101 | 98 | 24 |

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BONDAR-CLEGG

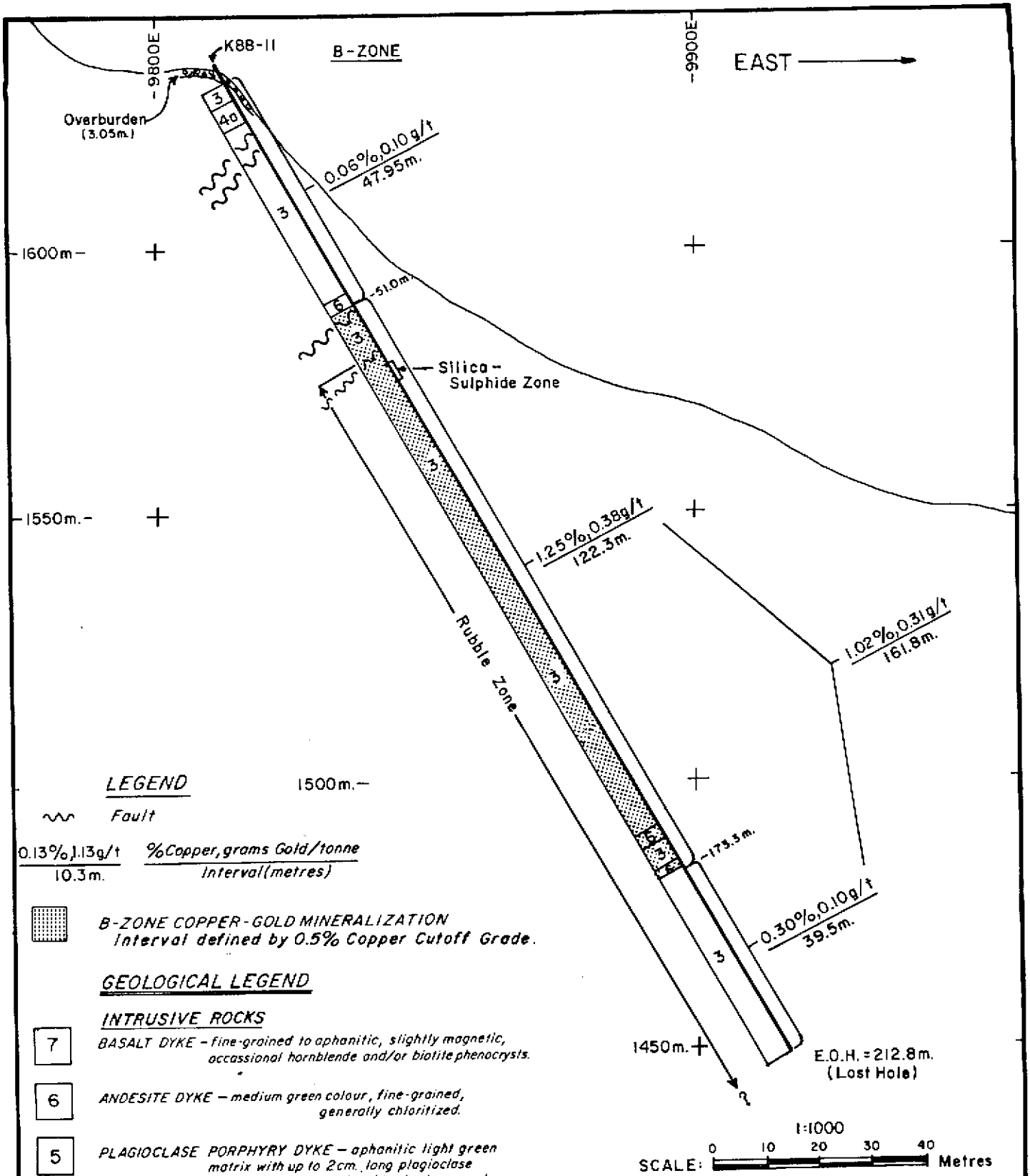
Certificate of Analysis

REPORT: V88-09373.4

PROJECT: NONE GIVEN PAGE 1

| SAMPLE NUMBER | ELEMENT UNITS | Au OPT | Cu PCT |
|---|---|---|---|
| P4 C88-9683 | | 0.010 | 2.12 |
| P4 C88-9684 | | 0.011 | 1.51 |
| P4 C88-9690 | | 0.029 | 1.63 |
| P4 C88-9696 | | 0.015 | 1.78 |
| P4 C88-9704 | | 0.022 | 1.77 |

Registered Assayer, Province of British Columbia




*LEGEND*

*Fault*

0.13%,1.13g/t / 10.3m. — *%Copper, grams Gold/tonne / Interval (metres)*

*B-ZONE COPPER-GOLD MINERALIZATION*
*Interval defined by 0.5% Copper Cutoff Grade.*

*GEOLOGICAL LEGEND*

*INTRUSIVE ROCKS*

7 — *BASALT DYKE – fine-grained to aphanitic, slightly magnetic, accassional hornblende and/or biotite phenocrysts.*

6 — *ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.*

5 — *PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.*

4 — *DIORITE(4a)/MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.*

*VOLCANIC and SEDIMENTARY ROCKS*

3 — *SERICITE-QUARTZ-PYRITE SCHIST – foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.*

2 — *DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF (2c)) – interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.*

1 — *SILTSTONE/SHALE/SANDSTONE – interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.*

SCALE: 1:1000 — 0 10 20 30 40 Metres

# SULPHURETS GOLD CORPORATION

## 1989 KERR PROJECT

## D.D.H. K88-11

## SECTION

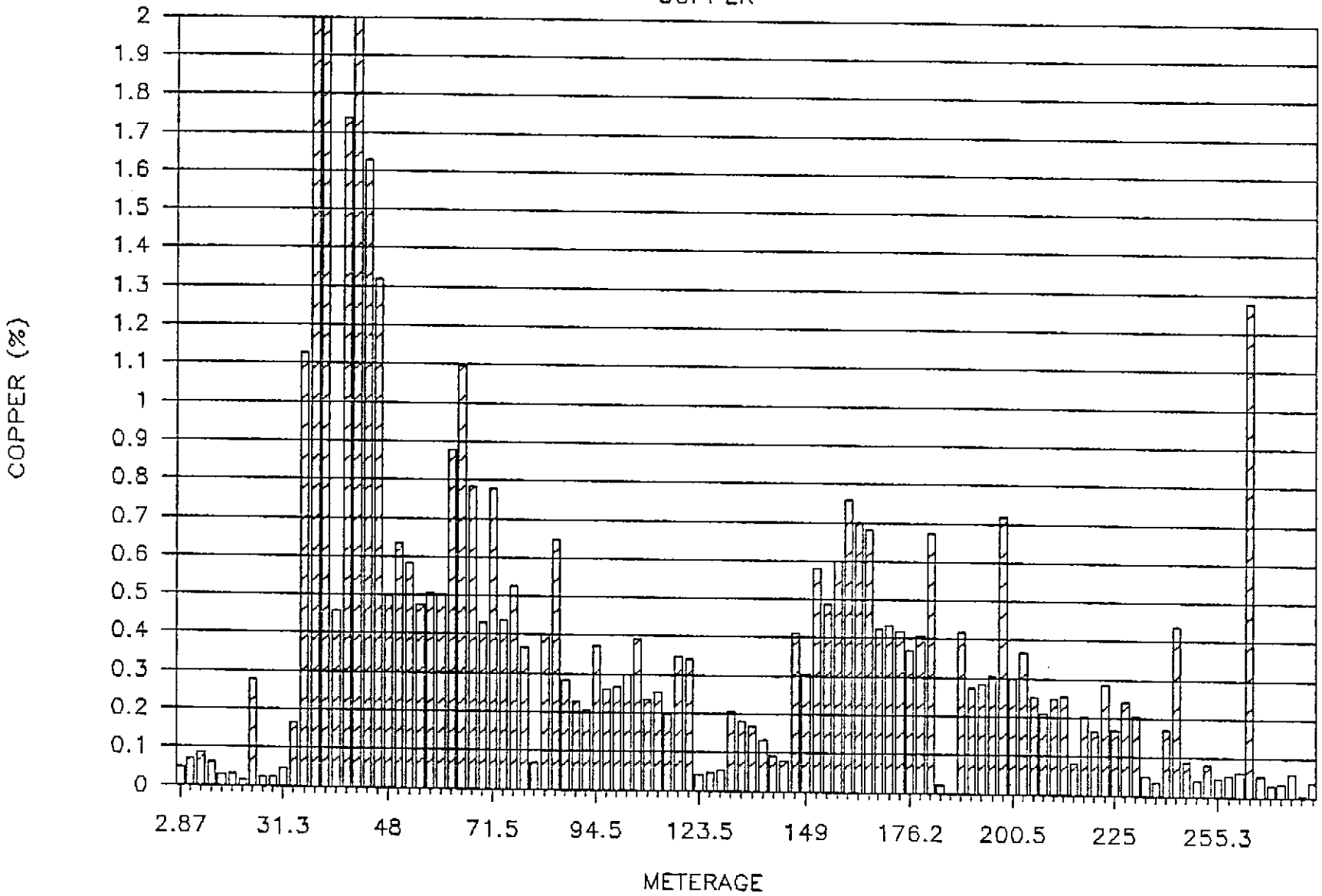
COLLAR: -9570.1N, 9810.9E

BEARING: 090° DIP: -60°

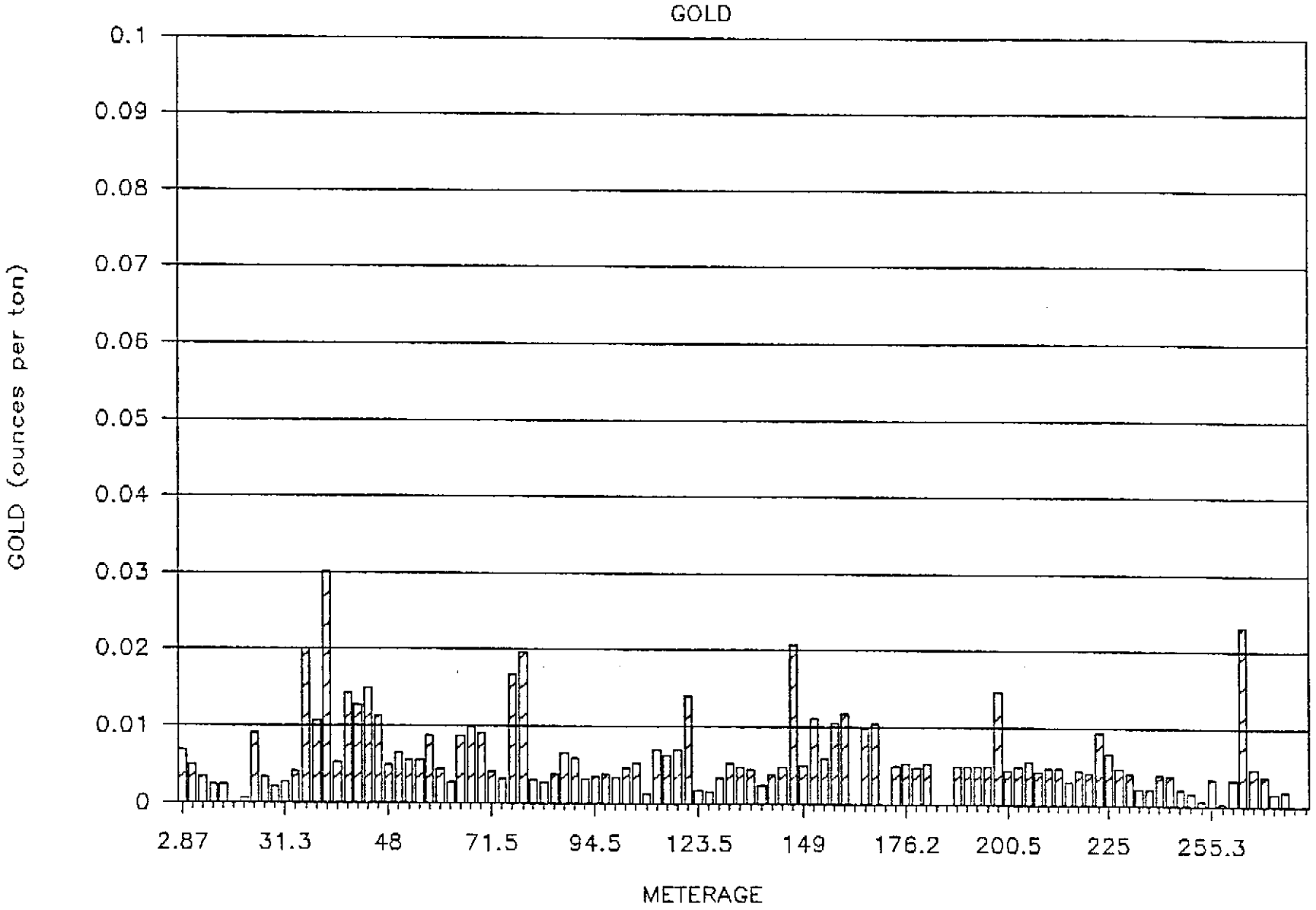
ELEVATION: 1634.3m.

REPORT 1065 FIGURE No.

# K88-14


COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
2.87
31.3
48
71.5
94.5
123.5
149
176.2
200.5
225
255.3
METERAGE

# K88-14


GOLD
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
GOLD (ounces per ton)
2.87
31.3
48
71.5
94.5
123.5
149
176.2
200.5
225
255.3
METERAGE

KERR PROJECT D.D.HOLE K-88-14

LOCATION TOP OF GLACIER NORTH SLOPE - BETWEEN A + B-ZONES
COLLAR LAT. 9847.3 NORTH
DATE STARTED JULY 25, 1988
LONG. 9650.2
DATE COMPLETED JULY 27, 1988
ELEVATION 1700.6 m
CORE RECOVERY 95.12%
AZIMUTH 090 DIP -60 deg
DRILLED BY FALCON DRILLING LTD.
LENGTH 272.80 m
LOGGED BY M. JEREMA
HOR. PROJ. 136.40 m
OBJECTIVE TO TEST THE NORTH WESTERLY EXTENSION OF THE B-ZONE
VERT. PROJ. 236.25 m
DIP TEST DEPTH _____m DIP_____deg
DEPTH _____m DIP_____deg

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 2.13 | 2.13 | OVERBURDEN / CASING |
| 2.13 | 10.87 | 8.74 | GREY BRECCIATED DACITIC CRYSTAL TUFF<br>- medium- to coarse-grained brecciated massive tuff; quite altered<br>- abundant disseminated pyrite and patches, wisps, blebs, and bands of cupriferous pyrite and minor blebs of chalcopyrite (traces to 5%) starting at the collar (2.4 m)<br>- blue grey to grey in colour<br>- no quartz-carbonate veining at all (protolith equivalent is probably chilled plagioclase porphyry) |
| 10.87 | 11.83 | 0.96 | ANDESITE DYKE<br>- medium green, massive, aphanitic, competent andesitic unit<br>- what appears to be amygdules at the top 15 cm of the unit, may indicate that these andesites are flows instead of dykes<br>- upper contact has a 62 deg core angle<br>- minor hairline tension fractures as well as 1 mm phenocrysts are filled with quartz-carbonate<br>- no pyrite present<br>- upper and lower contacts have bleached, rusty borders |
| 11.83 | 20.57 | 8.74 | PLAGIOCLASE PORPHYRY<br>- medium-grained blue-green groundmass with 2-3 mm feldspar phenocrysts (1-2%)<br>- chloritic hornblende crystals are quite visible in the groundmass and are weakly to moderately foliated<br>- minor quartz-carbonate in tension fractures |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 20.57 | 31.30 | 10.73 | GREY BRECCIATED DACITIC CRYSTAL TUFF<br>- same unit as described above in (2.13-10.87 m)<br>- medium-grained rather massive but auto-brecciated and weak to moderate foliation<br>- approximately 5-10% disseminated pyrite and 10 to 15% aggregated pyrite in the forms of wisps, patches, blebs, stringers, and foliated bands<br>- good traces of quartz-carbonate in foliated bands associated with pyrite - little quartz veining<br>- much of the banded and patchy pyrite may be cupriferous - such pyrite masks the presence of chalcopyrite extremely well<br>- no definite traces of chalcopyrite were observed |
| 31.30 | 33.00 | 1.70 | MOTTLED DACITIC LAPILLI TUFF<br>- (could be a very well foliated version of the brecciated dacite unit described above and not a lapilli tuff)<br>- foliation and a mottling of colours gives the impression of a well-foliated heterolithic lapilli tuff<br>- no quartz-carbonate as veining or matrix<br>- wisps and bands of pyrite to 15% and up to 5% disseminated pyrite<br>- gradational upper and lower contacts |
| 33.00 | 45.00 | 12.00 | PURPLE SULPHIDE STRINGER ZONE<br>- highly mineralized, sheared, and foliated version of the brecciated dacitic tuff unit described above<br>- a combination of a high sulphide content, lots of trace chalcocite, and chlorite gives the wet core a purplish hue - the purple colour and the visible chalcopyrite are characteristic of the unit<br>- quite siliceous, chloritic, and well foliated and mineralized<br>- 22 to 32% pyrite as wisps, patches, stringers, and bands, and from 1 to 10% chalcopyrite as blebs and stringers throughout<br>- chalcocite rims the chalcopyrite blebs<br>- from 1 to 10% quartz veining with good sulphide contents that fragment the veinlets, giving them a brecciated or clastic texture |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - good recovery and quite competent section with gradational contacts<br>- at 33.5 m is a 24 cm (true thickness) quartz sulphide vein with 'foliated' bands (44 deg to 47 deg to C.A.) of pyrite and chalcopyrite and some chloritic 'knots,' both of which appear to brecciate the vein<br>- absolutely no traces of carbonate in this section<br>- polished thin section sample taken from 36.55 m |
| 45.00 | 56.00 | 11.00 | GREY BRECCIATED DACITIC CRYSTAL TUFF<br>- same unit as previously described in the log<br>- it is also a less altered version of the tuff, hosting the purple chalcopyrite stringer zone<br>- medium-grained, massive, and partially foliated<br>- variably siliceous with minor chlorite alteration<br>- strong foliated cupriferous sulphides trace to 2% chalcopyrite with traces of chalcocite |
| 56.00 | 60.50 | 4.50 | PURPLE SULPHIDE (CHALCOPYRITE AND PYRITE) ZONE<br>- as described previously; just a more highly altered and mineralized section of brecciated grey dacitic crystal tuff - the tuff itself may actually be a well-foliated, chilled version of the feldspar porphyry<br>- greater than 2% chalcopyrite blebs and stringers, set with disseminated, banded, cupriferous pyrite up to 30%<br>- 1% chalcocite traces<br>- greater overall silicification and quartz veining, and much more chloritization<br>- distinct absence of carbonate |
| 60.50 | 65.00 | 4.50 | BRECCIATED GRAY DACITIC LAPILLI TUFF<br>- moderate to well foliated, brecciated, massive dacitic crystal tuff as described previously<br>- could be logged as less altered version of purple sulphide (chalcopyrite and pyrite) zone<br>- contains a great deal (2-3%) of more recognizable blebs and stringers of chalcopyrite than in the purple sulphide zone |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - some traces of chalcocite and a minor trace of native copper rimming chalcopyrite blebs and stringers<br>- polished thin section sample taken from 64.65 m with (chalcopyrite + chalcocite + native copper + pyrite + quartz + chlorite)<br>- gradational upper and lower contacts |
| 65.00 | 66.50 | 1.50 | FOLIATED HORNBLENDE CRYSTAL TUFF<br>- well foliated non-brecciated section of dacitic crystal tuff - massive; some grey-buff colour mottling<br>- still quite well mineralized with up to 3% chalcopyrite - no carbonate and only 1 patchy quartz vein<br>- suspect traces of chalcocite<br>- probably blue discoloration of quartz by extremely fine-grained pyrite |
| 66.50 | 69.50 | 3.00 | COARSE-GRAINED GREEN DIORITE<br>- medium to dark green colour due to the chloritization of hornblende crystals<br>- equivalent to plagioclase porphyry minus the plagioclase phenocryst<br>- 18 - 22% disseminated and banded pyrite, 1 to 2% chalcopyrite as traces, blebs, and minor stringers<br>- minor single trace of quart-carbonate<br>- gradational upper and lower contacts |
| 69.50 | 71.50 | 2.00 | PLAGIOCLASE PORPHYRY<br>- essentially: the diorite with large plagioclase phenocrysts<br>- minor reduction in sulphide content<br>- plagioclase phenocrysts replaced by silica<br>- traces of chalcopyrite as minor blebs,associated with pyrite<br>- quite competent; weak to moderately foliated hornblende phenocrysts give core angles of 56 deg |
| 71.50 | 74.20 | 2.70 | COARSE-GRAINED DIORITE<br>- identical to (66.50 - 69.50 m) above<br>- equivalent to porphyry minus the plagioclase phenocrysts |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 74.20 | 75.75 | 1.55 | SULPHIDE BRECCIA ZONE<br>- possibly an annealed fault breccia<br>- highly brecciated diorite to dacitic hornblende crystal tuff with 35% massive pyrite annealing breccia fragments as the matrix<br>- no chalcopyrite was positively identified, however, the pyrite appears cupriferous (probably contains 1-3% chalcopyrite)<br>- fragments are weakly aligned with a core angle of 42 deg to 51 deg |
| 75.25 | 76.20 | 0.95 | QUARTZ VEIN / FAULT<br>- brecciated quartz vein material annealed with a matrix of chlorite traces of chalcopyrite and pyrite<br>- possible minor reactivated fault, related in part to the sulphide breccia above it |
| 76.20 | 77.60 | 1.40 | MEDIUM-GRAINED GREEN GREY HORNBLENDE CRYSTAL TUFF<br>- could actually be a chilled section of diorite or plagioclase porphyry<br>- moderately foliated with 44 deg core angle<br>- only about 5% pyrite, disseminated, with an extremely minor trace of chalcopyrite<br>- no quartz-carbonate veining |
| 77.60 | 91.10 | 13.50 | DIORITE / PLAGIOCLASE PORPHYRY<br>- identical texture and composition as units described in (66.50 to 69.50 m) and (71.50 to 74.20 m)<br>- occasional plagioclase phenocrysts identify this unit as diorite to plagioclase porphyry<br>- sulphide content is somewhat reduced and pyrite stringers seem to be confined to hairline fractures<br>- chalcopyrite is very difficult to identify in this unit; it is largely fine-grained disseminated; possibly trace to 1% - a few 2-3 mm sized blebs are scattered throughout<br>- no quartz-carbonate and very minor veining<br>- 1 cm quartz veinlet at (82.15 m) with 2 mm bands of chalcopyrite on the outside edges<br>- very weak to non-foliated<br>- C.A. 55 deg at 82.30 m<br>- pyrite might be quite cupriferous<br>- no traces of chalcocite or native copper |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 91.10 | 109.50 | 18.40 | BRECCIATED GREY DACITIC CRYSTAL TUFF<br>- protolith most likely a chilled version of feldspar porphyry with hornblende crystals more developed (large and more abundant) than feldspar<br>- foliation is weak to moderate and a 'brecciated' or mottled appearance is caused by a clumping of mafic minerals into angular masses resembling fragments and sometimes lapilli<br>- banded cupriferous pyrite is much more abundant than the fine-grained disseminated brassy pyrite - total 'sulphide' content is approximately 25%<br>- chalcopyrite is difficult to identify and thus to estimate an actual percentage - much chalcopyrite is found disseminated with more massive pyrite bands and stringers- chalcopyrite content could vary from trace to 2%<br>- identifiable chalcopyrite usually associated with quartz-carbonate veinlets<br>- the odd 'ghost' feldspar phenocryst is present, adding evidence of an plagioclase porphyry protolith<br>- traces carbonate with .5 to 2 cm quartz-carbonate veinlets<br>- significant reduction in chlorite content from the above diorite / P.P. unit<br>- gradational lower and upper contents<br>- unit very competent with 100% recovery<br>- some sections are quite brecciated and look more like a monolithic lapilli tuff instead of a crystal tuff |
| 109.50 | 115.50 | 6.00 | GREY DACITIC TUFF - BRECCIA<br>- grey and buff coloured angular dacitic breccia (0.2 to 7.0 cm) fragments annealed with a darker dacitic tufaceous material and bands, wisps, patches, and stringers of cupriferous pyrite<br>- gradational upper and lower contacts<br>- unit probably is just a more highly brecciated and disturbed form of the brecciated dacitic crystal tuff unit above, therefore this tuff breccia may have the same chilled plagioclase porphyry protolith |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - chalcopyrite difficult to discern but positively identified chalcopyrite varies from trace to 1% throughout the unit - visual estimates of chalcopyrite are probably quite inaccurate<br>- no carbonate present |
| 115.50 | 128.00 | 12.50 | GREY MASSIVE DACITIC HORNBLENDE CRYSTAL TUFF<br>- protolith : probably chilled plagioclase porphyry<br>- top half of unit mottled and moderately foliated while lower half (from 120.5 m) is quite massive and weakly to non-foliated<br>- only a minor trace of carbonate<br>- traces to 2% chalcopyrite - most blebs chalcopyrite associated with quartz veins-.10 cm quartz vein with pyrite and 8% chalcopyrite plus 1% chalcocite at 120.25 m with a 52 deg core angle<br>- pyrite up to 25% of which only 5-8% is fine-grained disseminated - the rest as wisps, patches, stringers, and bands<br>- medium-grained, fairly competent unit with gradational upper and lower contacts |
| 128.00 | 142.50 | 14.50 | PURPLE SULPHIDE (PYRITE AND CHALCOPYRITE) STRINGER ZONE<br>- identical to unit described in interval (33.00 to 45.00 m) - protolith probably just sheared chilled plagioclase porphyry<br>- weak to well foliated, some crenulation foliation at 132.3 m, 190.0 m, and 140.6 m<br>- very thinly laminated and/or foliated-alternating layers of chlorite and quartz-sericite with most of the sulphides residing amongst the dark purple chloritic layers (from 139.4 to 142.5 m)<br>- (128.0 to 139.4 m) unit appears more sheared to brecciated with light to medium grey dacitic tuff (chilled P.P.) fragments annealed with dark blue / purple chlorite and pyrite / chalcopyrite wisps, patches, and stringers<br>- no carbonate traces |
| 142.50 | 145.50 | 3.00 | MASSIVE GREY DACITIC CRYSTAL TUFF<br>- non to well foliated grey plagioclase and hornblende crystal tuff - upper half from (142.5 to 143.3 m) is well foliated and from |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | 143.3 to 145.5 is massive and weak to non-foliated<br>- no carbonate present<br>- less than 20% disseminated and stringer pyrite - patchy and stringer sulphides are most likely cupriferous (up to 1% chalcopyrite in places) |
| 145.50 | 146.00 | 0.50 | MASSIVE SULPHIDE VEIN AND GREY DACITE TUFF<br>- (145.50 to 145.69 m) 19 cm band of massive sulphide (38% pyrite and 12% chalcopyrite) and quartz - 31 cm of dacitic tuff included with the sulphide vein to get a minimum half meter sample |
| 146.00 | 168.20 | 22.20 | GRAY BRECCIATED DACITIC CRYSTAL TUFF<br>- protolith chilled plagioclase porphyry<br>- quite sericitic and siliceous - borders on being quartz-sericite-pyrite schist<br>- 1 to 2% chalcopyrite as blebs, wisps, disseminations, and stringers<br>- this section is more mottled in appearance than other sections logged with the same name<br>- upper half from 146.0 to 156.0 m is carbonaceous - the rest of unit has no traces of carbonate at all<br>- traces to 2% saussurite?<br>- (164 to 167.2 m) contains numerous brecciated siliceous sections that contain a noticeable amount of chalcopyrite, more than the tuff itself<br>- unit is fairly competent with good recoveries |
| 168.20 | 182.40 | 14.20 | FOLIATED CHLORITIZED FELDSPAR PORPHYRY<br>- medium- to coarse-grained, medium green in colour<br>- quite altered; chloritized, pyritized, silicified with some clay alteration<br>- (167.2 to 168.2 m) the only competent and non-foliated section. Also the most readily identifiable portion of the unit; 2 - 3 mm silicified feldspar phenocrysts are scattered throughout this section - 1 to 5% quartz veinlets |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - (168.2 to 182.4 m) very well foliated to the point that the unit cleaves into 3 to 10 mm pieces, thus reducing competency and rock quality<br>- no carbonate noted<br>- pyrite up to 18% occurs as fine- to medium-grained disseminations and as stringers, wisps, patches, and bands, largely following foliation<br>- competency is moderate to poor<br>- traces of chalcopyrite occur with silicification and quartz veining (1%) - an 8 cm quartz vein with trace to 1% chalcopyrite at 171.8 m |
| 182.40 | 185.32 | 2.92 | PLAGIOCLASE PORPHYRY<br>- massive, competent unit, definite P.P. - has 5 to 20 mm 'snowflake' plagioclase phenocrysts scattered in dioritic (plagioclase-rich) matrix<br>- medium green colour, hornblende altered to chlorite<br>- trace pyrite only - some weathered out sulphides associated with narrow (2-4 mm) quartz veinlets<br>- no carbonate detected |
| 185.32 | 188.37 | 3.05 | TUBE FAILURE / FAULT ?<br>- absolutely no core recovered over interval-possible driller error (i.e., did not have core tube locked in the core barrel) - core below looks very fractured and it would have been ground and washed away if the tube was not locked |
| 188.37 | 190.50 | 2.13 | FOLIATED CHLORITIZED FELDSPAR PORPHYRY<br>- identical to unit above with same name in (167.20 to 182.40 m) - no carbonate noted<br>- good dendritic native copper occurring along fracture at 190.28 m<br>- possible traces of chalcocite throughout<br>- good traces gypsum along fractures - medium green colour and foliated broken core are characteristic of the unit<br>- pyrite largely disseminated fine-grained and blebs; some patches, bands, and stringers, all totalling approximately 18% |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 190.50 | 195.40 | 4.90 | GREY MASSIVE DACITIC CRYSTAL TUFF<br>- grey massive dacitic tufaceous unit<br>- appears laminated due to the narrow bands of sulphides and quartz-carbonate<br>- pyrite to 20% as fine-grained disseminations, wisps, patches, bands, and stringers; most of which is probably cupriferous<br>- carbonate to 2%; approximately the same for quartz veinlets<br>- weakly to non-foliated |
| 195.40 | 197.50 | 2.10 | QUARTZ SULPHIDE BRECCIA IN DACITIC TUFF<br>- quite small (20 to 40 cm) quartz sulphide breccia 'veins' in a grey, massive, partially foliated dacitic tuff, equivalent to unit immediately above and below<br>- quartz veins are brecciated with 35-40% pyrite / chalcopyrite - chalcopyrite content is difficult to discern but is around 3-5% at the least<br>- possible traces chalcocite |
| 197.50 | 228.00 | 30.50 | MASSIVE GREY DACITIC CRYSTAL TUFF<br>- protolith is chilled version of plagioclase porphyry (some relict plagioclase phenocrysts are scattered throughout the unit)<br>- a pseudo-laminated appearance is the result of a weak to moderate foliation, quartz-carbonate veining, bands, and stringers of sulphides, mostly pyrite<br>- pyrite is about 20 to 25% of which 10-15% is disseminated and the rest is a cupriferous pyrite, present as wisps, patches, bands, and crosscutting stringers<br>- chalcopyrite is tied up with pyrite and is possibly present in the amounts of 1 to 2%<br>- unit is quite competent; coring well with almost 100% recovery<br>- quartz patches and veins make up at least 1 to 2% of rock volume<br>- (218 to 220.05) - chloritic massive crystal tuffs - blue-green colour, gradational contacts, essentially part of the same unbroken series of dacitic tuffs with slightly different alteration assemblage<br>- at (225.10 m) minor trace of molybdenum or graphite (?) along a fracture surface |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - (216.0 to 248.0 m) wildly fluctuating core angles throughout - rocks in this interval are quite foliated, intensely sericitic, and variably pyritic - such core angles may reflect folding caused by intense shearing within this interval |
| 228.00 | 231.00 | 3.00 | SAUSSURITIZED PLAGIOCLASE PORPHYRY<br>- relict plagioclase phenocryst identify this portion of the unit as intensely altered P.P<br>- core angles appear to be from 70 deg to 90 deg - much banding caused by clear quartz filling fractures, patches of chlorite and sulphides with saussuritization throughout<br>- traces carbonate as quartz-carbonate patches |
| 231.00 | 246.00 | 15.00 | SAUSSURITIZED CHLORITIZED MASSIVE DACITIC CRYSTAL TUFF<br>- protolith chilled feldspar porphyry<br>- saussuritized sections appear intensely folded and extremely altered (pale olive green in colour)<br>- chloritic sections are less altered and more readily identifiable as hornblende crystal tuffs - blue grey in colour<br>- traces carbonate throughout<br>- less pyrite as stringers - essentially 15% as fine- to medium-grained disseminated pyrite and disseminated blebs and 8% as bands or patches - much of the blebs and banded pyrite may be cupriferous although chalcopyrite is not readily identifiable<br>- 237.47 to 237.70 cm and 231.0 to 234.0 m and 237.0 to 242.60 m dark green massive hornblende andesite dyke - chloritic sections<br>- 237.0 to 242.6 m section has wildly fluctuating core angles<br>- 234.0 to 237.0 and 242.6 to 246.0 m- saussuritized sections |
| 246.00 | 249.00 | 3.00 | GREY MASSIVE DACITIC CRYSTAL TUFF<br>- as described in 197.5 to 228.0 m<br>- highly sericitic although not as altered as the saussuritized sections above and below<br>- gradational contacts<br>- traces carbonate and .2 to 10 mm quartz veinlets |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 249.00 | 255.30 | 6.30 | SAUSSURITIZED DACITIC LAPILLI TUFF<br>- foliated angular fragments or highly brecciated fragments distinguish this unit from the more intrusive P.P. or tufaceous looking tuffs<br>- approximately 20% pale olive green saussurite throughout<br>- good traces of chalcopyrite (1% [?]) with cupriferous pyrite - pyrite is more globular (forms blebs) and disseminated - minor pyrite as stringers and bands<br>- good traces carbonate throughout |
| 255.30 | 259.50 | 4.20 | MASSIVE GREY DACITIC CRYSTAL TUFF<br>- as described above in 197.5 to 228.0 m and 246.0 to 249.0 m<br>- reduced pyrite content (15%)<br>- minor traces carbonate<br>- minor trace saussurite<br>- 2 cm band of cupriferous pyrite at 256.15 m<br>- reduction of quartz veinlets |
| 259.50 | 261.50 | 2.00 | GREY DACITIC LAPILLI TUFF<br>- protolith is difficult to distinguish<br>- highly brecciated section of dacitic tuff (?) or highly altered lapilli tuff<br>- numerous quartz veins and quartz-carbonate alteration<br>- 259.5 to 260.5 m - 40% sulphides as massive bands with 80 deg core angles, intercalated with quartz-carbonate and dacitic (sericitic) tuff material, contains 10% chalcopyrite with 30% pyrite<br>- probably some secondary chalcocite up to 1% |
| 260.50 | 270.25 | 9.75 | MASSIVE GRAY DACITIC CRYSTAL TUFF<br>- as described above<br>- unit becomes increasingly more altered down section with quartz veining and quartz-carbonate alteration - also pyrite is probably cupriferous between 268.0 to 270.25 m<br>- unit is weak to moderately foliated<br>- very minor trace of green mica at 269.75 metres |

KERR PROJECT D.D.HOLE K-88-14

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 270.25 | 271.60 | 1.35 | HORNBLENDE ANDESITE DYKE<br>- dark forest green colour, massive, largely aphanitic groundmass with 1-3% <1 mm hornblende phenocrysts and some minor plagioclase phenocrysts - no sulphides or carbonate<br>- unit is slightly magnetic |
| 271.60 | 272.80 | 1.20 | MASSIVE GREY DACITIC CRYSTAL TUFF<br>- as described above in 260.5 to 270.25 m<br>- more pyrite and quartz-carbonate alteration<br>- probably cupriferous pyrite<br><br>272.8 m - E.O.H. |

1988 KERR EXPLORATION PROGRAM

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| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8814 | 9847.3 | 9650.2 | 1700.6 | 90 | 60 | 272.8 | B-Zone | TO TEST THE NORTHWESTERLY EXTENSION OF THE B-ZONE | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0.00 | 2.13 | 2.13 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 2.13 | 2.87 | 0.74 | 40 | BREC DCIT XTAL | MG | | 15 | 1 | 40 | | 1 | | 0 | 0 | | | 85 | 18 | 0.2 | | 0 | | | |
| 2.87 | 5.87 | 3.00 | 35 | BREC DCIT XTAL | MG | | 18 | 0.1 | 40 | | 1 | | 0 | 0 | | | 85 | 20 | 0.1 | | 0 | | | |
| 5.87 | 8.87 | 3.00 | 31 | BREC DCIT XTAL | MG | | 18 | 0.1 | 35 | | 0.1 | | 0 | 0 | | | 85 | 28 | 1.0 | | 0 | | | |
| 8.87 | 10.87 | 2.00 | 35 | BREC DCIT XTAL | MG | | 18 | 0.5 | 35 | | 0.1 | | 0 | 0 | | | 85 | 23 | 0.1 | | 0 | | | |
| 10.87 | 14.00 | 3.13 | 29 | PLAG PRPH DYKE | CG | | 1 | 0.1 | 10 | | 80 | | 0.2 | 0 | | | 70 | 8 | 0 | | 0 | | | |
| 14.00 | 17.00 | 3.00 | 30 | PLAG PRPH DYKE | CG | | 8 | 0.1 | 35 | 1 | 25 | | 0.2 | 0 | | | 75 | 8 | 0 | | 0 | | | |
| 17.00 | 20.50 | 3.50 | 40 | PLAG PRPH DYKE | CG | | 8 | 0.5 | 35 | 0 | 25 | | 0.2 | 0 | | | 75 | 8 | 0 | | 0 | | | |
| 20.50 | 23.50 | 3.00 | 28 | PLAG PRPH DYKE | CG | | 18 | 0.5 | 40 | 0 | 0.1 | | 0.5 | 0 | | | 85 | 25 | 1 | | 0 | | | |
| 23.50 | 26.50 | 3.00 | 34 | BREC DCIT XTAL | CG | | 18 | 0.5 | 40 | 0 | 0.1 | | 0.5 | 0 | | | 85 | 25 | 1 | | 0 | | | |
| 26.50 | 29.50 | 3.00 | 33 | BREC DCIT XTAL | CG | | 18 | 20 | 40 | 0 | 0.1 | | 1 | 0 | | | 85 | 28 | 1 | | 0 | | | |
| 29.50 | 31.30 | 1.80 | 20 | BREC DCIT XTAL | CG | | 18 | 0.2 | 40 | 0 | 0.1 | | 1 | 0 | | | 85 | 25 | 1 | | 0 | | | |
| 31.30 | 33.00 | 1.70 | 28 | DCIT LPLL TUFF | FOL | | 18 | 1 | 35 | 0 | 0.1 | | 0 | 0 | | | 90 | 22 | 0.1 | | 0 | | | |
| 33.00 | 34.00 | 1.00 | 41 | SULP BREC | CG | | 18 | 25 | 5 | 0 | 10 | | 0 | 0 | | | 100 | 30 | 10 | | 1 | | | |
| 34.00 | 36.00 | 2.00 | 39 | SULP BREC | CG | | 18 | 1 | 20 | 0 | 3 | | 0 | 0 | | | 100 | 25 | 8 | | 0.1 | | | |
| 36.00 | 37.50 | 1.50 | 44 | SULP BREC | CG | | 15 | 10 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 28 | 10 | | 1 | | | |
| 37.50 | 38.50 | 1.00 | 45 | SULP BREC | CG | | 18 | 0.1 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 22 | 1 | | 0.1 | | | |
| 38.50 | 40.00 | 1.50 | 31 | SULP BREC | CG | | 25 | 10 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 28 | 10 | | 1 | | | |
| 40.00 | 41.50 | 1.50 | 32 | SULP BREC | CG | | 25 | 10 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 28 | 10 | | 1 | | | |
| 41.50 | 43.50 | 2.00 | 39 | SULP BREC | CG | | 25 | 1.0 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 25 | 6 | | 1 | | | |
| 43.50 | 45.00 | 1.50 | 39 | SULP BREC | CG | | 20 | 2 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 24 | 5 | | 0.1 | | | |
| 45.00 | 48.00 | 3.00 | 38 | BREC DCIT XTAL | MG | | 22 | 0.5 | 35 | 0 | 3 | | 0 | 0 | | | 85 | 24 | 1 | | 0.1 | | | |
| 48.00 | 51.00 | 3.00 | 37 | BREC DCIT XTAL | MG | | 22 | 0.2 | 35 | 0 | 2 | | 0 | 0.1 | | | 90 | 24 | 1 | | 0.2 | | | |
| 51.00 | 54.00 | 3.00 | 38 | BREC DCIT XTAL | MG | | 22 | 0.2 | 35 | 0 | 2 | | 0 | 0 | | | 90 | 22 | 2 | | 0.2 | | | |
| 54.00 | 56.00 | 2.00 | 34 | SULP BREC | MG | | 22 | 0.2 | 35 | 0 | 3 | | 0 | 0 | | | 90 | 26 | 2 | | 0.2 | | | |
| 56.00 | 58.00 | 2.00 | 35 | SULP BREC | MG | | 25 | 0.2 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 28 | 2 | | 1 | | | |
| 58.00 | 60.50 | 2.50 | 38 | SULP BREC | CG | | 20 | 2 | 20 | 0 | 8 | | 0 | 0 | | | 100 | 30 | 2 | | 1 | | | |
| 60.5 | 63 | 2.5 | 39 | BREC DCIT LPLL | MG | | 18 | .2 | 35 | | 3 | | | | | | 100 | 28 | 3 | | | | | |
| 63 | 65 | 2 | 38 | BREC DCIT LPLL | MG | | 18 | .5 | 35 | | 1 | | | | | | 100 | 25 | 3 | | | | | |
| 65 | 66.5 | 1.5 | 38 | HBLD XTAL TUFF | MG | | 15 | .5 | 40 | | 1 | | | | | | 100 | 22 | 2.5 | | | | | |
| 66.5 | 69.5 | 3 | 39 | DIOR | CG | | 15 | .5 | 25 | | 20 | | .1 | | | | 80 | 18 | 1.5 | | | | | |
| 69.5 | 71.5 | 2 | 43 | PLAG PRPH | CG | | 15 | .1 | 25 | | 20 | | | | | | 80 | 20 | .5 | | | | | |
| 71.5 | 74.2 | 2.7 | 53 | DIOR | CG | | 15 | .5 | 25 | | 20 | | | | | | 80 | 18 | .5 | | | | | |
| 74.2 | 75.75 | 1.55 | 50 | SULP BREC | BX | | 15 | | 25 | | 15 | | | | | | 90 | 35 | | | | | | |
| 75.75 | 76.2 | .45 | 33 | FAULT | CG | | 18 | 35 | 25 | | 30 | | | | | | 100 | 5 | .1 | | | | | |
| 76.2 | 77.6 | 1.4 | 35 | HBLD XTAL TUFF | MG | | 15 | .5 | 40 | | 1 | | | | | | 90 | 18 | .5 | | | | | |
| 77.6 | 80.6 | 3 | 40 | DIOR PLAG PRPH | CG | | 15 | .2 | 20 | | 20 | | | | | | 80 | 18 | .5 | | | | | |
| 80.6 | 83.6 | 3 | 43 | DIOR PLAG PRPH | CG | | 15 | .2 | 20 | | 20 | | | | | | 80 | 18 | .5 | | | | | |
| 93.6 | 86.6 | 3 | 44 | DIOR PLAG PRPH | CG | | 15 | .5 | 20 | | 20 | | | | | | 80 | 20 | .2 | | | | | |
| 86.6 | 88.6 | 2 | 46 | DIOR PLAG PRPH | CG | | 15 | .5 | 20 | | 20 | | | | | | 80 | 26 | .2 | | | | | |
| 88.6 | 91.1 | 2.5 | 49 | DIOR PLAG PRPH | CG | | 15 | .5 | 20 | | 20 | | .2 | | | | 90 | 25 | .2 | | | | | |
| 91.1 | 94.5 | 3.4 | 35 | BREC DCIT XTAL | BX | | 13 | .3 | 35 | | 5 | | .1 | | | | 75 | 26 | 1 | | | | | |
| 94.5 | 97.5 | 3 | 34 | BREC DCIT XTAL | BX | | 13 | 1 | 35 | | 1 | | .2 | | | | 75 | 25 | 1 | | | | | |
| 97.5 | 100.5 | 3 | 34 | BREC DCIT XTAL | BX | | 13 | 1 | 35 | | 3 | | .5 | | | | 75 | 24 | 1 | | | | | |
| 100.5 | 103.5 | 3 | 37 | BREC DCIT XTAL | BX | | 13 | .2 | 35 | | 3 | | .5 | | | | 75 | 23 | 1 | | | | | |
| 103.5 | 106.5 | 3 | 35 | BREC DCIT XTAL | BX | | 13 | .2 | 35 | | 3 | | | | | | 75 | 23 | 1 | | | | | |
| 106.5 | 109.5 | 3 | 36 | BREC DCIT XTAL | BX | | 13 | .2 | 35 | | 3 | | | | | | 75 | 22 | 1 | | | | | |
| 109.5 | 112.5 | 3 | 40 | BREC DCIT TUFF | BX | | 15 | | 35 | | 3 | | | | | | 75 | 28 | 15 | | | | | |
| 112.5 | 115.5 | 3 | 31 | BREC DCIT TUFF | BX | | 15 | | 35 | | 3 | | | | | | 75 | 24 | 1 | | | | | |
| 115.5 | 118 | 2.5 | 18 | HBLD XTAL TUFF | MG | | 15 | .5 | 35 | 2 | 3 | | | | | | 70 | 23 | 1 | | | | | |
| 118.5 | 120.5 | 2.5 | 26 | HBLD XTAL TUFF | CG | | 18 | 4 | | 3 | 3 | | .1 | | | | 70 | 25 | 2 | | | | | |
| 120.5 | 123.5 | 3 | 28 | HBLD XTAL TUFF | MG | | 15 | 2 | | | 3 | | | | | | 70 | 20 | 2 | | | | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8814 | 9847.3 | 9650.2 | 1700.6 | 90 | 60 | 272.8 | B-Zone | TO TEST THE NORTHWESTERLY EXTENSION OF THE B-ZONE | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 123.5 | 126 | 2.5 | 33 | HBLD XTAL TUFF | | MG | 15 | .5 | | | 3 | | | | | | 70 | 20 | 2 | | | | | |
| 126 | 128 | 2 | 23 | HBLD XTAL TUFF | | MG | 15 | .1 | | | 3 | | | | | | 70 | 20 | 2 | | | | | |
| 128 | 130.5 | 2.5 | 26 | SULP BREC | | BX | 8 | 1 | 35 | | 30 | | | | | | 100 | 20 | 5 | | 1 | | | |
| 130.5 | 133.5 | 3 | 33 | SULP BREC | | BX | 8 | .1 | 35 | | 30 | | | | | | 100 | 24 | 5 | | 1 | | | |
| 133.5 | 136.5 | 3 | 37 | SULP BREC | | BX | 8 | .1 | 35 | | 30 | | | | | | 100 | 25 | 6 | | 1 | | | |
| 136.5 | 139.5 | 3 | 33 | SULP BREC | | BX | 8 | .1 | 35 | | 30 | | | | | | 100 | 22 | 4 | | 1 | | | |
| 139.5 | 142.5 | 3 | 25 | SULP BREC | | BX | 8 | .1 | 35 | | 30 | | | | | | 100 | 20 | 3 | | 1 | | | |
| 142.5 | 145.5 | 3 | 28 | DCIT XTAL TUFF | | MG | 15 | | 35 | | | | | | | | 85 | 22 | 1 | | | | | |
| 145.6 | 146 | .5 | 32 | MASS SULP | | MG | 15 | 30 | 35 | | | | 2 | | | | 85 | 35 | 12 | | | | | |
| 146 | 149 | 3 | 24 | BREC DCIT XTAL | | MG | 15 | 1 | 35 | | | | 2 | | | | 85 | 18 | 2 | | | | | |
| 149 | 152 | 3 | 36 | BREC DCIT XTAL | | MG | 25 | 1 | 35 | | | | 2 | | | | 85 | 18 | 2 | | | | | |
| 152 | 155 | 3 | 32 | BREC DCIT XTAL | | MG | 25 | 1 | 35 | | | | | | | | 85 | 18 | 2 | | | | | |
| 155 | 158 | 3 | 37 | BREC DCIT XTAL | | MG | 20 | 2 | 35 | | | | .2 | | | | 85 | 18 | 2 | | | | | |
| 158 | 161 | 3 | 23 | BREC DCIT XTAL | | CG | 20 | .5 | 35 | | | | | | | | 85 | 18 | 2 | | | | | |
| 161 | 164 | 3 | 24 | BREC DCIT XTAL | | MG | 20 | 8 | 30 | 1 | 1 | | | | | | 85 | 20 | 3 | | | | | |
| 164 | 167.2 | 3.2 | 17 | BREC DCIT XTAL | | MG | 18 | .5 | 35 | | 3 | | | | | | 85 | 18 | 2 | | | | | |
| 167.2 | 168.2 | 1 | 32 | PLAG PRPH | | CG | 18 | 3 | 30 | | 30 | | | | | | 80 | 18 | .5 | | | | | |
| 168.2 | 170.2 | 2 | 24 | PLAG PRPH | | CG | 15 | 1 | 30 | | 30 | | | | | | 80 | 18 | .5 | | | | | |
| 170.2 | 173.2 | 3 | 23 | PLAG PRPH | | CG | 15 | 1 | 30 | | 30 | | | | | | 80 | 18 | .5 | | | | | |
| 173.2 | 176.2 | 3 | 22 | PLAG PRPH | | CG | 15 | 1 | 30 | | 30 | | | | | | 80 | 18 | .5 | | .1 | | | |
| 176.2 | 179.2 | 3 | 20 | PLAG PRPH | | CG | 15 | 1 | 30 | | 30 | | | | | | 80 | 18 | 1 | | .2 | | | |
| 179.2 | 182.4 | 3.2 | 25 | PLAG PRPH | | CG | 18 | .1 | 35 | | 25 | | | | | | 80 | 18 | 1 | | .5 | | | |
| 182.4 | 185.32 | 2.92 | 38 | PLAG PRPH | | CG | 8 | 5 | 25 | | 35 | | .1 | | | | 60 | | | | | | | |
| 185.32 | 188.37 | 3.05 | 4 | FAULT | | | | | | | | | | | | | | | | | | | | |
| 188.37 | 190.5 | 2.13 | 22 | PLAG PRPH | | CG | 15 | .1 | 25 | | 35 | | | | | | 80 | 18 | .5 | | .1 | .2 | | |
| 190.5 | 191.4 | .9 | 25 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | 3 | | 2 | | | | 85 | 20 | .5 | | .2 | | | |
| 191.4 | 194.4 | 3 | 29 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | 3 | | 2 | | | | 85 | 20 | .5 | | | | | |
| 194.4 | 195.4 | 1 | 22 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | 1 | | 2 | | | | 85 | 20 | .5 | | .2 | | | |
| 195.4 | 197.5 | 2.1 | 32 | SULP BREC | | MG | 18 | 10 | 30 | | 1 | | | | | | 85 | 25 | 3 | | .2 | | | |
| 197.5 | 200.5 | 3 | 33 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | 2 | | .1 | | | | 85 | 23 | 2 | | .2 | | | |
| 200.5 | 203.5 | 3 | 22 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | .1 | | .1 | | | | 85 | 24 | 2 | | .2 | | | |
| 203.5 | 206.5 | 3 | 39 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | .5 | | .1 | | | | 85 | 22 | 2 | | .1 | | | |
| 206.5 | 209.5 | 3 | 39 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | .1 | | .1 | | | | 85 | 20 | 2 | | .2 | | | |
| 209.5 | 212.5 | 3 | 39 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | .1 | | .1 | | | | 85 | 18 | 1.5 | | | | | |
| 212.5 | 215.5 | 3 | 37 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | | | 2 | | | | 85 | 15 | | .5 | | | | |
| 215.5 | 217 | 1.5 | 31 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | | | 2 | | | | 85 | 18 | | 1 | | | | |
| 217 | 218.9 | 1.9 | 10 | DCIT XTAL TUFF | | CG | 18 | 10 | 35 | | | | | | | | 85 | 22 | | 2 | .1 | | | |
| 218.9 | 220.05 | 1.15 | 29 | DCIT XTAL TUFF | | CG | 20 | 2 | 20 | | 25 | | | | | | 80 | 18 | | .1 | | | | |
| 220.05 | 223 | 2.95 | 27 | DCIT XTAL TUFF | | MG | 18 | 2 | 35 | | .1 | | | | | | 85 | 18 | | .5 | .1 | | | |
| 223 | 225 | 3 | 31 | DCIT XTAL TUFF | | MG | 18 | 1 | 35 | | 1 | | .2 | | | | 85 | 15 | | .1 | | | | |
| 225 | 228 | 3 | 31 | DCIT XTAL TUFF | | MG | 18 | 1 | 20 | | 15 | | .5 | | | | 85 | 20 | | 1 | | | | |
| 228 | 231 | 3 | 33 | PLAG PRPH | | CG | 20 | 1 | 35 | | 5 | | .5 | | | | 90 | 23 | | 1.5 | | | | |
| 231 | 234 | 3 | 36 | DCIT XTAL TUFF | | CG | 20 | 1 | 30 | | 15 | | .5 | | | | 85 | 18 | | .1 | | | | |
| 234 | 237 | 3 | 36 | DCIT XTAL TUFF | | CG | 22 | .5 | 25 | | 5 | | .5 | | | | 100 | 23 | | .5 | | | | |
| 237 | 240 | 3 | 27 | DCIT XTAL TUFF | | CG | 18 | .2 | 35 | | 5 | | .2 | | | | 85 | 2 | | .1 | | | | |
| 240 | 242.6 | 2.6 | 31 | DCIT XTAL TUFF | | MG | 18 | 1 | 35 | | 5 | | .2 | | | | 85 | | | .1 | | | | |
| 242.6 | 246 | 3.4 | 33 | DCIT XTAL TUFF | | CG | 20 | .2 | 25 | | | | .2 | | | | 100 | | | | | | | |
| 246 | 249 | 3 | 24 | DCIT XTAL TUFF | | CG | 18 | .2 | 40 | 5 | .1 | | | | | | 80 | | | | | | | |
| 249 | 252 | 3 | 36 | DCIT LPLL TUFF | | CG | 20 | 5 | 25 | | | | | | | | 100 | 20 | | 1 | | | | |
| 252 | 255.3 | 3.3 | 36 | DCIT LPLL TUFF | | CG | 20 | 5 | 25 | | | | 2 | | | | 100 | 20 | | 1 | | | | |
| 255.3 | 257 | 1.7 | 37 | DCIT XTAL TUFF | | MG | 18 | 1 | 35 | | | | 3 | | | | 80 | 18 | | .5 | | | | |
| 257 | 259.5 | 2.5 | 33 | DCIT XTAL TUFF | | MG | 18 | 1 | 35 | | | | 3 | | | | 80 | 15 | | .1 | | | | |

1988 KERR EXPLORATION PROGRAM

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| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8814 | 9847.3 | 9650.2 | 1700.6 | 90 | 60 | 272.8 | B-Zone | TO TEST THE NORTHWESTERLY EXTENSION OF THE B-ZONE #HC |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 259.5 | 260.5 | 1 | 21 | DCIT LPLL TUFF | | CG | 20 | 10 | 30 | 5 | 1 | | 5 | | | | 100 | 30 | | 10 | 1 | 1 | | |
| 260.5 | 261.5 | 1 | 37 | DCIT LPLL TUFF | | CG | 18 | 8 | 30 | | 1 | | 5 | | | | 80 | 22 | | 1 | .1 | .1 | | |
| 261.5 | 264.5 | 3 | 35 | DCIT XTAL TUFF | | CG | 15 | 1 | 35 | | | | | | | | 80 | 18 | | | | | | |
| 264.5 | 267.5 | 3 | 30 | DCIT XTAL TUFF | | MG | 20 | 4 | 35 | | | | 4 | | | | 85 | 18 | | | | | | |
| 267.5 | 270.25 | 2.75 | 31 | DCIT XTAL TUFF | | | 20 | 8 | 35 | | | | 2 | .1 | | | 100 | 22 | | 2 | | | | |
| 270.25 | 271.6 | 1.35 | 33 | ANDS DYKE | | VFG | | | | | 70 | | | | | | 80 | | | | | | | |
| 271.6 | 272.8 | 1.2 | 33 | DCIT XTAL TUFF | | CG | 20 | 10 | 35 | | | | 2 | | | | 100 | 23 | | 1 | | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 09:15:25 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| B814 | 9847.3 | 9650.2 | 1700.6 | 90 | 60 | 272.8 | B-Zone | TO TEST THE NORTHWESTERLY EXTENSION OF THE B-ZONE #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0.00 | 2.13 | | 2.13 | 0 | | | | | | | | | | | |
| 2.13 | 2.87 | 9866 | 0.74 | 0.72 | 235 | | .5 | | 475 | 136 | 5.05 | 208 | 647 | | |
| 2.87 | 5.87 | 9867 | 3.00 | 2.89 | 170 | | 1.1 | | 701 | 337 | 6.58 | 121 | 48 | | |
| 5.87 | 8.87 | 9868 | 3.00 | 2.97 | 110 | | 1.5 | | 849 | 1100 | 8.05 | 19 | 51 | | |
| 8.87 | 10.87 | 9869 | 2.00 | 2.00 | 80 | | 1.1 | | 608 | 674 | 8.68 | 92 | 34 | | |
| 10.87 | 14.00 | 9870 | 3.13 | 2.93 | 80 | | .1 | | 253 | 438 | 5.35 | 764 | 3368 | | |
| 14.00 | 17.00 | 9871 | 3.00 | 2.84 | 0 | | .1 | | 291 | 207 | 4.26 | 28 | 2759 | | |
| 17.00 | 20.50 | 9872 | 3.50 | 3.34 | 20 | | .5 | | 161 | 135 | 3.87 | 142 | 2034 | | |
| 20.50 | 23.50 | 9873 | 3.00 | 2.90 | 310 | | 5.1 | | 276 | 312 | 8.46 | 919 | 552 | | |
| 23.50 | 26.50 | 9874 | 3.00 | 3.00 | 110 | | 5.1 | | 226 | 109 | 6.16 | 74 | 365 | | |
| 26.50 | 29.50 | 9875 | 3.00 | 2.90 | 70 | | .2 | | 235 | 169 | 8.97 | 95 | 491 | | |
| 29.50 | 31.30 | 9876 | 1.80 | 1.80 | 90 | | .6 | | 469 | 137 | 8.63 | 156 | 484 | | |
| 31.30 | 33.00 | 9877 | 1.70 | 1.61 | 140 | | 1.5 | | 1635 | 216 | 8.35 | 107 | 1025 | | |
| 33.00 | 34.00 | 9878 | 1.00 | 0.98 | 690 | | 7.3 | | 11261 | 101 | 10 | 206 | 563 | | |
| 34.00 | 36.00 | 9879 | 2.00 | 1.97 | 365 | | 9.3 | | 20000 | 292 | 4.51 | 45 | 121 | | |
| 36.00 | 37.50 | 9880 | 1.50 | 1.50 | 1030 | | 6.8 | | 20000 | 725 | 6.79 | 85 | 206 | | |
| 37.50 | 38.50 | 9881 | 1.00 | 1.00 | 180 | | 1.9 | | 4573 | 1257 | 8.34 | 119 | 376 | | |
| 38.50 | 40.00 | 9882 | 1.50 | 1.46 | 490 | | 4.6 | | 17382 | 441 | 7.8 | 85 | 163 | | |
| 40.00 | 41.50 | 9883 | 1.50 | 1.48 | 435 | | 6.4 | | 200000 | 702 | 6.32 | 86 | 170 | | |
| 41.50 | 43.50 | 9884 | 2.00 | 1.93 | 510 | | 5.6 | | 16267 | 315 | 4.81 | 114 | 112 | | |
| 43.50 | 45.00 | 9885 | 1.50 | 1.48 | 390 | | 5.3 | | 13191 | 376 | 4.7 | 110 | 149 | | |
| 45.00 | 48.00 | 9886 | 3.00 | 3.00 | 170 | | 2.9 | | 4962 | 361 | 5.86 | 79 | 57 | | |
| 48.00 | 51.00 | 9887 | 3.00 | 3.00 | 220 | | 4.9 | | 6349 | 242 | 5.1 | 945 | 43 | | |
| 51.00 | 54.00 | 9888 | 3.00 | 2.97 | 190 | | 6.8 | | 5831 | 183 | 4.31 | 853 | 46 | | |
| 54.00 | 56.00 | 9889 | 2.00 | 1.94 | 190 | | 8.1 | | 4746 | 1131 | 3.74 | 764 | 62 | | |
| 56.00 | 58.00 | 9890 | 2.00 | 2.00 | 300 | | 15.2 | | 5056 | 4369 | 4.6 | 183 | 26 | | |
| 58.00 | 60.50 | 9891 | 2.50 | 2.50 | 150 | | 4.1 | | 5047 | 531 | 5.03 | 328 | 75 | | |
| 60.5 | 63 | 9892 | 2.5 | 2.48 | 90 | | .2 | | 8781 | 294 | 3.88 | 231 | 358 | | |
| 63 | 65 | 9893 | 2 | 1.89 | 300 | | 2.2 | | 10994 | 964 | 5.75 | 103 | 507 | | |
| 65 | 66.5 | 9894 | 1.5 | 1.5 | 340 | | .5 | | 7854 | 266 | 5.37 | 688 | 1307 | | |
| 66.5 | 69.5 | 9895 | 3 | 3 | 310 | | .7 | | 4320 | 748 | 5.5 | 691 | 1438 | | |
| 69.5 | 71.5 | 9896 | 2 | 2 | 140 | | .1 | | 7770 | 485 | 4.58 | 394 | 1097 | | |
| 71.5 | 74.2 | 9897 | 2.7 | 2.67 | 105 | | .1 | | 4362 | 166 | 4.22 | 153 | 836 | | |
| 74.2 | 75.75 | 9898 | 1.55 | 1.51 | 575 | | 1.2 | | 5245 | 250 | 6.37 | 268 | 461 | | |
| 75.75 | 76.2 | 9899 | .45 | .43 | 670 | | 1.2 | | 3658 | 2675 | 4.1 | 95 | 367 | | |
| 76.2 | 77.6 | 9900 | 1.4 | 1.4 | 100 | | .1 | | 690 | 324 | 4.04 | 57 | 2353 | | |
| 77.6 | 80.6 | 9901 | 3 | 2.98 | 90 | | .5 | | 4016 | 151 | 5.4 | 68 | 1609 | | |
| 80.6 | 83.6 | 9902 | 3 | 3 | 130 | | .7 | | 6480 | 134 | 5.18 | 92 | 1035 | | |
| 93.6 | 86.6 | 9903 | 3 | 2.94 | 220 | | .3 | | 2833 | 100 | 5.62 | 73 | 1233 | | |
| 86.6 | 88.6 | 9904 | 2 | 2 | 200 | | .1 | | 2278 | 114 | 6.96 | 112 | 2466 | | |
| 88.6 | 91.1 | 9905 | 2.5 | 2.42 | 105 | | .1 | | 2072 | 111 | 4.77 | 99 | 1459 | | |
| 91.1 | 94.5 | 9906 | 3.4 | 3.33 | 120 | | .5 | | 3728 | 324 | 4.95 | 51 | 898 | | |
| 94.5 | 97.5 | 9907 | 3 | 2.98 | 130 | | .1 | | 2607 | 108 | 5.29 | 37 | 1032 | | |
| 97.5 | 100.5 | 9908 | 3 | 2.97 | 110 | | .1 | | 2658 | 130 | 3.98 | 65 | 2518 | | |
| 100.5 | 103.5 | 9909 | 3 | 3 | 155 | | .6 | | 2988 | 260 | 5.78 | 61 | 1324 | | |
| 103.5 | 106.5 | 9910 | 3 | 2.96 | 180 | | 2.1 | | 3921 | 1345 | 4.67 | 84 | 728 | | |
| 106.5 | 109.5 | 9911 | 3 | 3 | 40 | | .6 | | 2352 | 179 | 5.07 | 45 | 612 | | |
| 109.5 | 112.5 | 9912 | 3 | 3 | 240 | | 1.2 | | 2531 | 106 | 5.19 | 83 | 155 | | |
| 112.5 | 115.5 | 9913 | 3 | 3 | 210 | | .6 | | 1958 | 70 | 5.38 | 75 | 147 | | |
| 115.5 | 118 | 9914 | 2.5 | 2.5 | 240 | | 1.2 | | 3459 | 173 | 4.25 | 73 | 156 | | |
| 118.5 | 120.5 | 9915 | 2.5 | 2.5 | 480 | | .1 | | 3394 | 177 | 4.26 | 425 | 144 | | |
| 120.5 | 123.5 | 9916 | 3 | 2.99 | 60 | | .2 | | 388 | 165 | 4.13 | 99 | 1016 | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8814 | 9847.3 | 9650.2 | 1700.6 | 90 | 60 | 272.8 | B-Zone | TO TEST THE NORTHWESTERLY EXTENSION OF THE B-ZONE #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 123.5 | 126 | 9917 | 2.5 | 2.46 | 50 | | .1 | | 453 | 296 | 3.87 | 107 | 1001 | | |
| 126 | 128 | 9918 | 2 | 1.87 | 110 | | .2 | | 534 | 312 | 4.18 | 69 | 1934 | | |
| 128 | 130.5 | 9919 | 2.5 | 1.67 | 180 | | 1.5 | | 2064 | 601 | 3.8 | 326 | 315 | | |
| 130.5 | 133.5 | 9920 | 3 | 3 | 160 | | 1.1 | | 1807 | 67 | 4.05 | 94 | 182 | | |
| 133.5 | 136.5 | 9921 | 3 | 3 | 150 | | 1.1 | | 1668 | 99 | 5.75 | 84 | 272 | | |
| 136.5 | 139.5 | 9922 | 3 | 2.98 | 80 | | .4 | | 1310 | 68 | 5.75 | 72 | 267 | | |
| 139.5 | 142.5 | 9923 | 3 | 2.55 | 130 | | .4 | | 903 | 626 | 4.23 | 63 | 528 | | |
| 142.5 | 145.5 | 9924 | 3 | 2.98 | 160 | | 1.5 | | 789 | 110 | 4.04 | 143 | 445 | | |
| 145.6 | 146 | 9925 | .5 | .5 | 710 | | 15.1 | | 4126 | 659 | 8.6 | 1000 | 1725 | | |
| 146 | 149 | 9926 | 3 | 3 | 170 | | 3.3 | | 3057 | 228 | 4.21 | 196 | 818 | | |
| 149 | 152 | 9927 | 3 | 2.96 | 380 | | 3.3 | | 5788 | 177 | 3.82 | 186 | 400 | | |
| 152 | 155 | 9928 | 3 | 3 | 200 | | 1.6 | | 4882 | 193 | 3.87 | 31 | 534 | | |
| 155 | 158 | 9929 | 3 | 2.87 | 360 | | 2.7 | | 5976 | 163 | 3.75 | 34 | 659 | | |
| 158 | 161 | 9930 | 3 | 2.9 | 400 | | 2.2 | | 7605 | 374 | 3.77 | 37 | 517 | | |
| 161 | 164 | 9931 | 3 | 3 | 0 | | 1.1 | | 7016 | 230 | 3.74 | 60 | 981 | | |
| 164 | 167.2 | 9932 | 3.2 | 2.77 | 340 | | 2.5 | | 6813 | 1655 | 4.17 | 60 | 1214 | | |
| 167.2 | 168.2 | 9933 | 1 | 1 | 360 | | 1.8 | | 4235 | 730 | 5.29 | 79 | 2178 | | |
| 168.2 | 170.2 | 9934 | 2 | .93 | 0 | | 3.1 | | 4339 | 506 | 4.93 | 65 | 1504 | | |
| 170.2 | 173.2 | 9935 | 3 | 2.07 | 170 | | 1.1 | | 4171 | 360 | 4.72 | 99 | 1111 | | |
| 173.2 | 176.2 | 9936 | 3 | .65 | 180 | | .9 | | 3708 | 456 | 4.73 | 102 | 824 | | |
| 176.2 | 179.2 | 9937 | 3 | 2.43 | 160 | | 1.3 | | 4093 | 482 | 4.25 | 133 | 448 | | |
| 179.2 | 182.4 | 9938 | 3.2 | 2.73 | 180 | | 3.3 | | 6719 | 573 | 4.39 | 210 | 388 | | |
| 182.4 | 185.32 | 9939 | 2.92 | 2.84 | 0 | | .1 | | 198 | 230 | 2.7 | 18 | 1664 | | |
| 185.32 | 188.37 | | 3.05 | 0 | | | | | | | | | | | |
| 188.37 | 190.5 | 9940 | 2.13 | 2.03 | 170 | | .3 | | 4160 | 131 | 5.05 | 39 | 294 | | |
| 190.5 | 191.4 | 9941 | .9 | .9 | 170 | | .4 | | 2727 | 74 | 5.53 | 23 | 645 | | |
| 191.4 | 194.4 | 9942 | 3 | 2.93 | 170 | | .1 | | 2828 | 88 | 4.81 | 35 | 694 | | |
| 194.4 | 195.4 | 9943 | 1 | 1 | 170 | | .1 | | 3064 | 143 | 5.61 | 54 | 719 | | |
| 195.4 | 197.5 | 9944 | 2.1 | 2.04 | 500 | | .1 | | 7166 | 74 | 6.92 | 109 | 452 | | |
| 197.5 | 200.5 | 9945 | 3 | 2.93 | 150 | | .1 | | 2998 | 76 | 4.6 | 16 | 647 | | |
| 200.5 | 203.5 | 9946 | 3 | 3 | 170 | | .1 | | 3661 | 65 | 5.84 | 33 | 1104 | | |
| 203.5 | 206.5 | 9947 | 3 | 2.98 | 190 | | .1 | | 2515 | 203 | 5.24 | 20 | 612 | | |
| 206.5 | 209.5 | 9948 | 3 | 2.97 | 145 | | .1 | | 2093 | 84 | 4.72 | 270 | 61 | | |
| 209.5 | 212.5 | 9949 | 3 | 2.86 | 160 | | .1 | | 2467 | 45 | 5.81 | 43 | 445 | | |
| 212.5 | 215.5 | 9950 | 3 | 3 | 160 | | .1 | | 2523 | 82 | 5.37 | 60 | 640 | | |
| 215.5 | 217 | 9951 | 1.5 | 1.59 | 100 | | .1 | | 823 | 37 | 5.31 | 57 | 262 | | |
| 217 | 218.9 | 9952 | 1.9 | 1.59 | 150 | | .9 | | 2045 | 95 | 5.65 | 98 | 343 | | |
| 218.9 | 220.05 | 9953 | 1.15 | 1.15 | 140 | | .1 | | 1644 | 96 | 4.03 | 11 | 289 | | |
| 220.05 | 223 | 9954 | 2.95 | 2.91 | 320 | | .1 | | 2857 | 58 | 4.24 | 19 | 438 | | |
| 223 | 225 | 9955 | 3 | 2.93 | 230 | | .1 | | 1665 | 78 | 4.16 | 11 | 968 | | |
| 225 | 228 | 9956 | 3 | 3 | 160 | | .1 | | 2423 | 57 | 4.26 | 14 | 330 | | |
| 228 | 231 | 9957 | 3 | 3 | 140 | | ..1 | | 2068 | 46 | 5.22 | 19 | 238 | | |
| 231 | 234 | 9958 | 3 | 3 | 70 | | .1 | | 484 | 177 | 4.27 | 8 | 680 | | |
| 234 | 237 | 9959 | 3 | 3 | 70 | | .1 | | 343 | 83 | 4.37 | 20 | 242 | | |
| 237 | 240 | 9960 | 3 | 2.97 | 135 | | .1 | | 1716 | 125 | 3.99 | 19 | 378 | | |
| 240 | 242.6 | 9961 | 2.6 | 2.6 | 130 | | 1.1 | | 4352 | 34 | 4.69 | 20 | 184 | | |
| 242.6 | 246 | 9962 | 3.4 | 3.4 | 70 | | .1 | | 680 | 100 | 5.07 | 29 | 401 | | |
| 246 | 249 | 9963 | 3 | 2.95 | 50 | | .1 | | 395 | 123 | 4.28 | 54 | 630 | | |
| 249 | 252 | 9964 | 3 | 3 | 20 | | .1 | | 829 | 75 | 6.06 | 42 | 202 | | |
| 252 | 255.3 | 9965 | 3.3 | 3.3 | 120 | | .1 | | 466 | 47 | 6.04 | 37 | 749 | | |
| 255.3 | 257 | 9966 | 1.7 | 1.64 | 110 | | .9 | | 512 | 63 | 4.37 | 30 | 463 | | |
| 257 | 259.5 | 9967 | 2.5 | 2.5 | 10 | | 2.5 | | 624 | 102 | 4.26 | 85 | 445 | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8814 | 9847.3 | 9650.2 | 1700.6 | 90 | 60 | 272.8 | B-Zone | TO TEST THE NORTHWESTERLY EXTENSION OF THE B-ZONE #HC |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 259.5 | 260.5 | 9968 | 1 | 1 | 800 | | 11.6 | | 12762 | 1530 | 9.81 | 419 | 1281 | | |
| 260.5 | 261.5 | 9969 | 1 | 1 | 160 | | .1 | | 522 | 142 | 5.87 | 41 | 1132 | | |
| 261.5 | 264.5 | 9970 | 3 | 2.95 | 130 | | .5 | | 313 | 263 | 4.37 | 11 | 1116 | | |
| 264.5 | 267.5 | 9971 | 3 | 2.97 | 50 | | .1 | | 343 | 244 | 3.98 | 0 | 1671 | | |
| 267.5 | 270.25 | 9972 | 2.75 | 2.53 | 65 | | .6 | | 583 | 131 | 4.72 | 71 | 1146 | | |
| 270.25 | 271.6 | 9973 | 1.35 | .85 | 0 | | .4 | | 58 | 115 | 4.74 | 9 | 895 | | |
| 271.6 | 272.8 | 9974 | 1.2 | 1.17 | 0 | | .4 | | 381 | 93 | 4.12 | 12 | 1039 | | |

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1969 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656


REPORT NUMBER: 880914 AA  JOB NUMBER: 880914  WESTERN CDN. MINING CORP.  

| SAMPLE # | Au oz/st |
|---|---|
| C88-9880 | .024 |

DETECTION LIMIT .005

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1968 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-9877 | .18 |
| C88-9878 | 1.11 |
| C88-9879 | 2.08 |
| C88-9880 | 2.65 |
| C88-9881 | .52 |
| C88-9882 | 1.95 |
| C88-9883 | 2.88 |
| C88-9884 | 1.65 |
| C88-9885 | 1.31 |
| C88-9886 | .51 |
| C88-9887 | .64 |
| C88-9888 | .76 |
| C88-9889 | .61 |
| C88-9890 | .70 |
| C88-9891 | .46 |
| C88-9892 | .46 |
| C88-9893 | .85 |
| C88-9894 | 1.02 |
| C88-9895 | .41 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1966 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-9896 | .69 |
| C88-9897 | .41 |
| C88-9898 | .59 |
| C88-9899 | .40 |
| C88-9900 | .09 |
| C88-9901 | .45 |
| C88-9902 | .71 |
| C88-9903 | .32 |
| C88-9904 | .23 |
| C88-9905 | .20 |
| C88-9906 | .41 |
| C88-9907 | .28 |
| C88-9908 | .29 |
| C88-9909 | .38 |
| C88-9910 | .43 |
| C88-9911 | .25 |
| C88-9912 | .27 |
| C88-9913 | .21 |
| C88-9914 | .35 |
| C88-9915 | .35 |
| DETECTION LIMIT | .01 |

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-9916 | .04 |
| C88-9917 | .05 |
| C88-9918 | .06 |
| C88-9919 | .22 |
| C88-9920 | .19 |
| C88-9921 | .18 |
| C88-9922 | .14 |
| C88-9923 | .11 |
| C88-9924 | .10 |
| C88-9925 | .51 |
| C88-9926 | .32 |
| C88-9927 | .67 |
| C88-9928 | .60 |
| C88-9929 | .73 |
| C88-9930 | .87 |
| C88-9931 | .72 |
| C88-9932 | .75 |
| C88-9933 | .47 |
| C88-9934 | .49 |
| C88-9935 | .45 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1966 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-9936 | .46 |
| C88-9937 | .47 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: BB1151 PA  WESTERN CANADIAN MINING CORP.  

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Y ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-9866 | 0.5 | 1.44 | 208 | 235 | <3 | 17 | <3 | 0.28 | 1.8 | 34 | 39 | 475 | 5.05 | 0.09 | 0.71 | 647 | <1 | 0.02 | 29 | 0.18 | 51 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 13 |
| C88-9867 | 1.1 | 0.30 | 121 | 170 | <3 | 11 | <3 | 0.19 | 4.0 | 27 | 42 | 701 | 6.58 | 0.08 | 0.08 | 48 | <1 | 0.03 | 22 | 0.17 | 61 | <3 | <5 | <2 | <2 | 32 | <5 | <3 | 33 |
| C88-9868 | 1.5 | 0.23 | 119 | 110 | <3 | 10 | <3 | 0.21 | 9.5 | 31 | 48 | 849 | 8.05 | 0.08 | 0.06 | 51 | <1 | 0.06 | 38 | 0.17 | 81 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 110 |
| C88-9869 | 1.1 | 0.35 | 92 | 80 | <3 | 13 | <3 | 0.17 | 7.9 | 27 | 73 | 608 | 8.68 | 0.08 | 0.04 | 34 | <1 | 0.04 | 32 | 0.17 | 52 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 67 |
| C88-9870 | 0.1 | 2.30 | 764 | 80 | <3 | 20 | <3 | 1.34 | 1.1 | 19 | 26 | 253 | 5.35 | 0.21 | 1.39 | 3368 | <1 | 0.03 | 9 | 0.21 | 63 | <3 | <5 | <2 | <2 | 57 | <5 | <3 | 43 |
| C88-9871 | 0.1 | 2.53 | 28 | <5 | <3 | 80 | <3 | 2.47 | 2.5 | 18 | 33 | 291 | 4.26 | 0.29 | 1.54 | 2759 | <1 | 0.02 | 9 | 0.20 | 35 | <3 | <5 | <2 | <2 | 111 | <5 | <3 | 20 |
| C88-9872 | 0.5 | 1.90 | 142 | 20 | <3 | 27 | <3 | 2.67 | 2.2 | 14 | 27 | 161 | 3.87 | 0.31 | 1.50 | 2034 | <1 | 0.02 | 8 | 0.20 | 38 | <3 | <5 | <2 | <2 | 139 | <5 | <3 | 17 |
| C88-9873 | 5.1 | 0.44 | 919 | 310 | <3 | 9 | 12 | 0.62 | 1.9 | 25 | 56 | 2768 | 8.46 | 0.18 | 0.23 | 552 | <1 | 0.04 | 21 | 0.19 | 132 | <3 | <5 | 221 | <2 | 44 | <5 | <3 | 1 |
| C88-9874 | 5.1 | 0.29 | 74 | 110 | <3 | 8 | <3 | 0.34 | 3.3 | 30 | 54 | 226 | 6.16 | 0.16 | 0.18 | 365 | <1 | 0.04 | 25 | 0.13 | 70 | <3 | <5 | <2 | <2 | 23 | <5 | <3 | 1v |
| C88-9875 | 0.2 | 0.48 | 95 | 70 | <3 | 10 | <3 | 0.54 | 3.6 | 28 | 83 | 235 | 8.97 | 0.13 | 0.22 | 491 | <1 | 0.03 | 25 | 0.20 | 56 | <3 | <5 | <2 | <2 | 43 | <5 | <3 | 16 |
| C88-9876 | 0.6 | 0.35 | 156 | 90 | <3 | 10 | <3 | 0.48 | 3.1 | 25 | 63 | 469 | 8.63 | 0.12 | 0.20 | 484 | <1 | 0.02 | 24 | 0.16 | 70 | <3 | <5 | <2 | <2 | 41 | <5 | <3 | 13 |
| C88-9877 | 1.5 | 0.42 | 107 | 140 | <3 | 12 | <3 | 0.71 | 3.9 | 34 | 60 | 1635 | 8.35 | 0.14 | 0.35 | 1025 | <1 | 0.03 | 43 | 0.20 | 59 | <3 | <5 | <2 | <2 | 70 | <5 | <3 | 21 |
| C88-9878 | 7.3 | 1.13 | 206 | 690 | <3 | 12 | 20 | 0.45 | 4.6 | 23 | 129 | 11261 | >10.00 | 0.13 | 0.34 | 563 | <1 | 0.04 | 18 | 0.35 | 34 | <3 | <5 | <2 | <2 | 136 | <5 | <3 | 10 |
| C88-9879 | 9.3 | 0.47 | 45 | 365 | <3 | 18 | <3 | 0.22 | 2.9 | 10 | 102 | >20000 | 4.51 | 0.06 | 0.09 | 121 | <1 | 0.02 | 13 | 0.21 | 20 | <3 | <5 | <2 | <2 | 148 | <5 | <3 | 29 |
| C88-9880 | 6.8 | 0.74 | 85 | 1030 | <3 | 13 | <3 | 0.20 | 5.5 | 15 | 101 | >20000 | 6.79 | 0.07 | 0.25 | 206 | <1 | 0.04 | 11 | 0.17 | 15 | <3 | <5 | <2 | <2 | 18 | <5 | <3 | 72 |
| C88-9881 | 1.9 | 1.11 | 119 | 180 | <3 | 12 | <3 | 0.39 | 7.5 | 39 | 69 | 4573 | 8.34 | 0.12 | 0.33 | 376 | <1 | 0.06 | 13 | 0.33 | 46 | <3 | <5 | <2 | <2 | 30 | <5 | <3 | 125 |
| C88-9882 | 4.6 | 0.71 | 85 | 490 | <3 | 11 | <3 | 0.20 | 4.6 | 22 | 104 | 17382 | 7.80 | 0.09 | 0.20 | 163 | <1 | 0.04 | 10 | 0.18 | 33 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 44 |
| C88-9883 | 6.4 | 1.62 | 86 | 435 | <3 | 16 | <3 | 0.23 | 4.6 | 14 | 104 | >20000 | 6.32 | 0.08 | 0.21 | 170 | <1 | 0.04 | 13 | 0.31 | 58 | <3 | <5 | <2 | <2 | 195 | <5 | <3 | 70 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 2000 |

( = Less than Minimum  is = Insufficient Sample  ns = No sample  ) = Greater than Maximum  AuFA = Fire assay/AAS

VANCOUVER B.C. V5R 1R5

REPORT #: 880914 PA  WESTERN CND MINING  

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-9884 | 5.6 | 0.49 | 114 | 510 | <3 | 11 | <3 | 0.25 | 2.9 | 19 | 53 | 16367 | 4.81 | 0.09 | 0.06 | 112 | <1 | 0.03 | 17 | 0.22 | 50 | <3 | <5 | <2 | <2 | 24 | <5 | <3 | 315 |
| C88-9885 | 5.3 | 0.68 | 110 | 330 | <3 | 16 | <3 | 0.33 | 2.7 | 16 | 44 | 13131 | 4.70 | 0.09 | 0.11 | 149 | <1 | 0.03 | 13 | 0.27 | 45 | <3 | <5 | <2 | <2 | 71 | <5 | <3 | 376 |
| C88-9886 | 2.9 | 0.44 | 79 | 170 | <3 | 15 | <3 | 0.25 | 3.0 | 30 | 48 | 4562 | 5.66 | 0.10 | 0.03 | 57 | <1 | 0.04 | 16 | 0.23 | 62 | <3 | <5 | <2 | <2 | 95 | <5 | <3 | 361 |
| C88-9887 | 4.9 | 0.48 | 945 | 220 | <3 | 14 | <3 | 0.33 | 0.1 | 23 | 39 | 6349 | 5.10 | 0.13 | 0.02 | 43 | <1 | 0.04 | 15 | 0.26 | 79 | <3 | <5 | 111 | <2 | 52 | <5 | <3 | 242 |
| C88-9888 | 6.8 | 0.34 | 853 | 190 | <3 | 12 | <3 | 0.27 | 0.1 | 17 | 31 | 5831 | 4.31 | 0.16 | 0.02 | 46 | <1 | 0.04 | 12 | 0.30 | 125 | <3 | <5 | <2 | <2 | 52 | <5 | <3 | 183 |
| C88-9889 | 8.1 | 0.33 | 764 | 190 | <3 | 11 | <3 | 0.25 | 3.0 | 18 | 36 | 4746 | 3.74 | 0.15 | 0.02 | 62 | <1 | 0.07 | 12 | 0.21 | 176 | <3 | <5 | <2 | <2 | 31 | <5 | <3 | 1131 |
| C88-9890 | 15.2 | 0.24 | 182 | 300 | <3 | 11 | 16 | 0.17 | 22.3 | 23 | 25 | 5056 | 4.60 | 0.23 | 0.02 | 26 | <1 | 0.21 | 17 | 0.15 | 457 | <3 | <5 | 33 | <2 | 24 | <5 | <3 | 4365 |
| C88-9891 | 4.1 | 0.49 | 328 | 150 | <3 | 16 | <3 | 0.32 | 1.6 | 20 | 88 | 5047 | 5.03 | 0.06 | 0.05 | 75 | <1 | 0.02 | 11 | 0.26 | 230 | <3 | <5 | <2 | <2 | 112 | <5 | <3 | 531 |
| C88-9892 | 0.2 | 0.83 | 231 | 90 | <3 | 23 | <3 | 0.31 | 1.5 | 14 | 49 | 8781 | 3.88 | 0.06 | 0.22 | 358 | 12 | 0.01 | 11 | 0.25 | 43 | <3 | <5 | <2 | <2 | 34 | <5 | <3 | 294 |
| C88-9893 | 2.2 | 0.64 | 103 | 300 | <3 | 15 | <3 | 0.28 | 4.9 | 18 | 57 | 10994 | 5.75 | 0.06 | 0.25 | 567 | <1 | 0.04 | 13 | 0.22 | 174 | <3 | <5 | <2 | <2 | 19 | <5 | <3 | 964 |
| C88-9894 | 0.5 | 0.87 | 688 | 340 | <3 | 18 | <3 | 0.40 | 0.1 | 17 | 56 | 7854 | 5.37 | 0.08 | 0.27 | 1307 | <1 | 0.02 | 12 | 0.23 | 53 | <3 | <5 | <2 | <2 | 28 | <5 | <3 | 148 |
| C88-9895 | 0.7 | 0.82 | 691 | 310 | <3 | 17 | <3 | 0.47 | 2.6 | 18 | 47 | 4320 | 5.50 | 0.09 | 0.31 | 1438 | <1 | 0.03 | 11 | 0.21 | 81 | <3 | <5 | <2 | <2 | 39 | <5 | <3 | 148 |
| C88-9896 | 0.1 | 1.06 | 394 | 140 | <3 | 25 | <3 | 0.30 | 1.9 | 21 | 42 | 7770 | 4.58 | 0.05 | 0.39 | 1097 | <1 | 0.02 | 12 | 0.23 | 102 | <3 | <5 | <2 | <2 | 18 | <5 | <3 | 485 |
| C88-9897 | 0.1 | 0.72 | 153 | 105 | <3 | 17 | <3 | 0.28 | 1.2 | 23 | 58 | 4362 | 4.22 | 0.05 | 0.22 | 836 | <1 | 0.01 | 11 | 0.22 | 38 | <3 | <5 | <2 | <2 | 18 | <5 | <3 | 166 |
| C88-9898 | 1.2 | 0.72 | 268 | 575 | <3 | 11 | <3 | 0.19 | 2.3 | 21 | 52 | 5245 | 6.37 | 0.06 | 0.14 | 461 | <1 | 0.03 | 12 | 0.15 | 34 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 250 |
| C88-9899 | 1.2 | 1.04 | 95 | 670 | <3 | 15 | <3 | 0.14 | 16.0 | 18 | 146 | 3658 | 4.10 | 0.05 | 0.46 | 367 | 75 | 0.10 | 10 | 0.14 | 431 | <3 | <5 | <2 | <2 | 50 | <5 | <3 | 2675 |
| C88-9900 | 0.1 | 1.97 | 57 | 100 | <3 | 35 | <3 | 1.15 | 2.3 | 15 | 26 | 690 | 4.04 | 0.18 | 1.24 | 2353 | <1 | 0.02 | 10 | 0.19 | 88 | <3 | <5 | <2 | <2 | 152 | <5 | <3 | 324 |
| C88-9901 | 0.5 | 0.87 | 68 | 90 | <3 | 12 | <3 | 0.38 | 2.1 | 28 | 49 | 4016 | 5.40 | 0.09 | 0.48 | 1609 | 4 | 0.02 | 17 | 0.17 | 42 | <3 | <5 | <2 | <2 | 29 | <5 | <3 | 151 |
| C88-9902 | 0.7 | 0.64 | 92 | 130 | <3 | 13 | <3 | 0.28 | 2.0 | 23 | 34 | 6480 | 5.18 | 0.07 | 0.24 | 1035 | <1 | 0.02 | 12 | 0.18 | 35 | <3 | <5 | <2 | <2 | 24 | <5 | <3 | 134 |
| C88-9903 | 0.3 | 0.60 | 73 | 220 | <3 | 11 | <3 | 0.31 | 1.9 | 34 | 28 | 2833 | 5.62 | 0.09 | 0.28 | 1233 | 10 | 0.02 | 18 | 0.18 | 45 | <3 | <5 | <2 | <2 | 31 | <5 | <3 | 100 |
| C88-9904 | 0.1 | 0.74 | 112 | 200 | <3 | 9 | <3 | 0.36 | 2.4 | 40 | 34 | 2278 | 6.96 | 0.10 | 0.28 | 2466 | <1 | 0.02 | 24 | 0.19 | 38 | <3 | <5 | <2 | <2 | 30 | <5 | <3 | 114 |
| C88-9905 | 0.1 | 0.82 | 99 | 105 | <3 | 14 | <3 | 0.39 | 1.6 | 23 | 30 | 2072 | 4.77 | 0.10 | 0.47 | 1459 | <1 | 0.02 | 21 | 0.18 | 33 | <3 | <5 | <2 | <2 | 32 | <5 | <3 | 111 |
| C88-9906 | 0.5 | 0.26 | 51 | 120 | <3 | 12 | <3 | 0.33 | 3.0 | 24 | 42 | 3728 | 4.95 | 0.08 | 0.05 | 898 | <1 | 0.02 | 19 | 0.17 | 201 | <3 | <5 | <2 | <2 | 30 | <5 | <3 | 324 |
| C88-9907 | 0.1 | 0.24 | 37 | 130 | <3 | 10 | <3 | 0.39 | 2.1 | 25 | 31 | 2607 | 5.29 | 0.09 | 0.04 | 1022 | <1 | 0.02 | 17 | 0.17 | 40 | <3 | <5 | <2 | <2 | 44 | <5 | <3 | 109 |
| C88-9908 | 0.1 | 0.38 | 65 | 110 | <3 | 12 | <3 | 0.99 | 1.6 | 18 | 39 | 2658 | 3.98 | 0.17 | 0.22 | 2518 | <1 | 0.01 | 12 | 0.18 | 53 | <3 | <5 | <2 | <2 | 85 | <5 | <3 | 130 |
| C88-9909 | 0.6 | 0.39 | 61 | 155 | <3 | 10 | <3 | 0.38 | 2.9 | 31 | 33 | 2988 | 5.78 | 0.09 | 0.20 | 1324 | <1 | 0.03 | 17 | 0.18 | 64 | <3 | <5 | <2 | <2 | 35 | <5 | <3 | 260 |
| C88-9910 | 2.1 | 0.47 | 84 | 180 | <3 | 10 | <3 | 0.28 | 8.6 | 30 | 35 | 3921 | 4.67 | 0.08 | 0.18 | 728 | <1 | 0.06 | 19 | 0.17 | 864 | <3 | <5 | <2 | <2 | 25 | <5 | <3 | 1345 |
| C88-9911 | 0.6 | 0.41 | 45 | 40 | <3 | 13 | <3 | 0.33 | 2.4 | 34 | 43 | 2352 | 5.07 | 0.09 | 0.14 | 612 | <1 | 0.02 | 24 | 0.20 | 70 | <3 | <5 | <2 | <2 | 39 | <5 | <3 | 179 |
| C88-9912 | 1.2 | 0.16 | 83 | 240 | <3 | 9 | <3 | 0.24 | 2.1 | 29 | 22 | 2531 | 5.19 | 0.08 | 0.02 | 155 | <1 | 0.02 | 20 | 0.18 | 125 | <3 | <5 | <2 | <2 | 58 | <5 | <3 | 148 |
| C88-9913 | 0.6 | 0.29 | 75 | 210 | <3 | 11 | <3 | 0.25 | 2.0 | 26 | 40 | 1958 | 5.38 | 0.08 | 0.09 | 147 | <1 | 0.02 | 20 | 0.18 | 35 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 148 |
| C88-9914 | 1.2 | 0.30 | 73 | 240 | <3 | 11 | <3 | 0.26 | 2.0 | 20 | 22 | 3459 | 4.25 | 0.08 | 0.11 | 156 | <1 | 0.02 | 15 | 0.19 | 85 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 173 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

7-14

ANOMALOUS RESULTS:
FURTHER ANALYSES
BY ALTERNATE
METHODS SUGGESTED

VANGEOCHEM LAB LIM.
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717



REPORT #: BB1151 PA

WESTERN CANADIAN MINING CORP.

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| CBB-9915 | 0.1 | 0.40 | 425 | 480 | <3 | 20 | <3 | 0.23 | 1.2 | 19 | 44 | 3394 | 4.26 | 0.09 | 0.20 | 144 | 27 | 0.03 | 19 | 0.18 | 91 | <3 | <5 | <2 | 4 | 12 | <5 | <3 |
| CBB-9916 | 0.2 | 0.36 | 99 | 60 | <3 | 21 | <3 | 0.60 | 1.1 | 17 | 22 | 388 | 4.13 | 0.15 | 0.40 | 1016 | 4 | 0.03 | 10 | 0.20 | 57 | <3 | <5 | <2 | 4 | 20 | <5 | <3 |
| CBB-9917 | 0.1 | 0.83 | 107 | 50 | <3 | 26 | 4 | 0.48 | 1.7 | 17 | 28 | 453 | 3.87 | 0.13 | 0.67 | 1001 | 4 | 0.04 | 9 | 0.20 | 87 | <3 | <5 | <2 | 4 | 12 | <5 | <3 |
| CBB-9918 | 0.2 | 0.67 | 69 | 110 | <3 | 30 | 4 | 0.73 | 1.7 | 16 | 40 | 534 | 4.18 | 0.14 | 0.86 | 1934 | 4 | 0.04 | 7 | 0.19 | 70 | <3 | <5 | <2 | 3 | 16 | <5 | <3 |
| CBB-9919 | 1.5 | 0.29 | 326 | 180 | <3 | 20 | <3 | 0.40 | 2.6 | 16 | 20 | 2064 | 3.80 | 0.11 | 0.21 | 315 | 10 | 0.06 | 12 | 0.18 | 172 | <3 | <5 | <2 | 3 | 11 | <5 | <3 |
| CBB-9920 | 1.1 | 0.34 | 94 | 160 | <3 | 20 | <3 | 0.28 | 0.7 | 20 | 40 | 1807 | 4.05 | 0.09 | 0.21 | 182 | 12 | 0.02 | 14 | 0.19 | 40 | <3 | <5 | <2 | 3 | 8 | <5 | <3 |
| CBB-9921 | 1.1 | 0.47 | 84 | 150 | <3 | 17 | 5 | 0.26 | 1.3 | 22 | 43 | 1668 | 5.75 | 0.10 | 0.32 | 272 | 29 | 0.03 | 17 | 0.17 | 66 | <3 | <5 | <2 | 4 | 7 | <5 | <3 |
| CBB-9922 | 0.4 | 0.64 | 72 | 80 | <3 | 14 | 5 | 0.24 | 1.2 | 28 | 30 | 1310 | 5.75 | 0.10 | 0.39 | 267 | 14 | 0.03 | 19 | 0.19 | 43 | <3 | <5 | <2 | 4 | 7 | <5 | <3 |
| CBB-9923 | 0.4 | 0.19 | 63 | 130 | <3 | 15 | <3 | 0.53 | 2.8 | 19 | 46 | 903 | 4.23 | 0.13 | 0.23 | 528 | 15 | 0.06 | 11 | 0.18 | 112 | <3 | <5 | <2 | 3 | 17 | <5 | <3 |
| CBB-9924 | 1.5 | 0.17 | 143 | 160 | <3 | 14 | <3 | 0.76 | 0.7 | 15 | 40 | 789 | 4.04 | 0.16 | 0.14 | 445 | 9 | 0.02 | 8 | 0.18 | 57 | <3 | <5 | <2 | 6 | 21 | <5 | |
| CBB-9925 | 15.1 | 0.28 | >1000 | 710 | <3 | 12 | 9 | 1.89 | 4.1 | 14 | 46 | 4126 | 8.60 | 0.32 | 0.39 | 1725 | 6 | 0.09 | 9 | 0.12 | 357 | <3 | <5 | 67 | 6 | 75 | <5 | |
| CBB-9926 | 3.3 | 0.16 | 196 | 170 | <3 | 13 | <3 | 1.43 | 2.1 | 18 | 39 | 3057 | 4.21 | 0.27 | 0.24 | 818 | 20 | 0.04 | 7 | 0.16 | 156 | <3 | <5 | <2 | 4 | 50 | <5 | <3 |
| CBB-9927 | 3.3 | 0.15 | 186 | 380 | <3 | 13 | 3 | 0.66 | 1.5 | 17 | 58 | 5788 | 3.82 | 0.18 | 0.16 | 400 | 18 | 0.03 | 7 | 0.15 | 73 | <3 | <5 | <2 | 5 | 57 | <5 | <3 |
| CBB-9928 | 1.6 | 0.19 | 31 | 200 | <3 | 11 | 3 | 0.45 | 1.3 | 23 | 54 | 4882 | 3.87 | 0.14 | 0.20 | 534 | 18 | 0.03 | 6 | 0.15 | 50 | <3 | <5 | <2 | 4 | 24 | <5 | <3 |
| CBB-9929 | 2.7 | 0.22 | 34 | 360 | <3 | 10 | 4 | 0.45 | 1.2 | 19 | 32 | 5976 | 3.75 | 0.15 | 0.24 | 659 | 13 | 0.03 | 7 | 0.15 | 75 | <3 | <5 | <2 | 5 | 20 | <5 | <3 |
| CBB-9930 | 2.2 | 0.14 | 37 | 400 | <3 | 13 | 5 | 0.43 | 2.1 | 20 | 43 | 7605 | 3.77 | 0.14 | 0.20 | 517 | 19 | 0.05 | 8 | 0.15 | 70 | <3 | <5 | <2 | 5 | 16 | <5 | <3 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88-9931 | 1.1 | 0.18 | 60 | <5 | <3 | 14 | <3 | 0.78 | 3.1 | 22 | 53 | 7016 | 3.74 | 0.14 | 0.46 | 981 | 23 | 0.04 | 10 | 0.13 | 48 | <3 | <5 | <2 | 2 | 19 | <5 | <3 | 230 |
| C88-9932 | 2.5 | 0.20 | 60 | 340 | <3 | 15 | <3 | 0.55 | 6.8 | 13 | 64 | 6813 | 4.17 | 0.10 | 0.35 | 1214 | 16 | 0.14 | 5 | 0.13 | 115 | <3 | <5 | <2 | 2 | 16 | <5 | <3 | 1655 |
| C88-9933 | 1.8 | 1.40 | 79 | 360 | <3 | 18 | 8 | 0.44 | 4.1 | 12 | 28 | 4235 | 5.29 | 0.09 | 1.61 | 2178 | 7 | 0.08 | 6 | 0.16 | 109 | <3 | <5 | <2 | 2 | 15 | <5 | <3 | 730 |
| C88-9934 | 3.1 | 1.17 | 65 | <5 | <3 | 18 | 5 | 0.26 | 3.4 | 13 | 83 | 4339 | 4.93 | 0.08 | 1.22 | 1504 | 10 | 0.06 | 7 | 0.15 | 65 | <3 | <5 | <2 | 3 | 14 | <5 | <3 | 506 |
| C88-9935 | 1.1 | 1.25 | 99 | 170 | <3 | 18 | 4 | 0.24 | 2.9 | 13 | 60 | 4171 | 4.72 | 0.08 | 1.36 | 1111 | 7 | 0.05 | 6 | 0.17 | 60 | <3 | <5 | <2 | 3 | 10 | <5 | <3 | 360 |
| C88-9936 | 0.9 | 1.71 | 102 | 180 | <3 | 19 | 6 | 0.19 | 2.2 | 11 | 41 | 3708 | 4.73 | 0.07 | 1.66 | 824 | 6 | 0.06 | 5 | 0.16 | 50 | <3 | <5 | <2 | 3 | 6 | <5 | <3 | 456 |
| C88-9937 | 1.3 | 0.98 | 133 | 160 | <3 | 15 | 5 | 0.19 | 3.1 | 15 | 47 | 4093 | 4.25 | 0.07 | 0.93 | 448 | 29 | 0.06 | 6 | 0.20 | 85 | <3 | <5 | <2 | 3 | 5 | <5 | <3 | 482 |
| C88-9938 | 3.3 | 1.11 | 210 | 180 | <3 | 15 | 6 | 0.18 | 3.2 | 13 | 57 | 6719 | 4.39 | 0.10 | 0.84 | 388 | 13 | 0.06 | 7 | 0.18 | 97 | <3 | <5 | <2 | 4 | 12 | <5 | <3 | 573 |
| C88-9939 | 0.1 | 0.98 | 18 | <5 | <3 | 690 | <3 | 1.13 | 1.8 | 12 | 18 | 198 | 2.70 | 0.24 | 0.64 | 1664 | 4 | 0.03 | 4 | 0.10 | 35 | <3 | <5 | <2 | 3 | 64 | <5 | <3 | 230 |
| C88-9940 | 0.3 | 1.23 | 39 | 170 | <3 | 18 | 4 | 0.22 | 2.3 | 16 | 49 | 4160 | 5.05 | 0.09 | 0.93 | 294 | 20 | 0.03 | 5 | 0.24 | 38 | <3 | <5 | <2 | 3 | 58 | <5 | <3 | 131 |
| C88-9941 | 0.4 | 0.28 | 23 | 170 | <3 | 15 | 4 | 0.43 | 2.2 | 16 | 58 | 2727 | 5.53 | 0.12 | 0.12 | 645 | 14 | 0.03 | 6 | 0.15 | 33 | <3 | <5 | <2 | 3 | 15 | <5 | <3 | 74 |
| C88-9942 | 0.1 | 0.30 | 35 | 170 | <3 | 14 | <3 | 0.97 | 1.9 | 17 | 34 | 2828 | 4.81 | 0.19 | 0.26 | 694 | 13 | 0.03 | 6 | 0.15 | 21 | <3 | <5 | <2 | 3 | 19 | <5 | <3 | 86 |
| C88-9943 | 0.1 | 0.30 | 54 | 170 | <3 | 12 | <3 | 0.65 | 2.1 | 18 | 60 | 3064 | 5.61 | 0.12 | 0.15 | 719 | 11 | 0.03 | 5 | 0.18 | 32 | <3 | <5 | <2 | 2 | 18 | <5 | <3 | 143 |
| C88-9944 | 0.1 | 0.21 | 109 | 500 | <3 | 10 | 5 | 0.46 | 2.6 | 18 | 70 | 7166 | 6.92 | 0.10 | 0.21 | 452 | 41 | 0.04 | 12 | 0.11 | 24 | <3 | <5 | <2 | 3 | 14 | <5 | <3 | 74 |
| C88-9945 | 0.1 | 0.37 | 16 | 150 | <3 | 13 | <3 | 0.93 | 1.5 | 16 | 20 | 2998 | 4.60 | 0.16 | 0.28 | 647 | 22 | 0.03 | 5 | 0.13 | 17 | <3 | <5 | <2 | 2 | <1 | <5 | <3 | 76 |
| C88-9946 | 0.1 | 0.34 | 33 | 170 | <3 | 11 | 4 | 1.31 | 2.1 | 15 | 54 | 3661 | 5.84 | 0.22 | 0.59 | 1104 | 20 | 0.03 | 6 | 0.10 | 22 | <3 | <5 | <2 | 2 | 27 | <5 | <3 | 85 |
| C88-9947 | 0.1 | 0.18 | 20 | 190 | <3 | 11 | <3 | 0.79 | 1.7 | 16 | 35 | 2515 | 5.24 | 0.15 | 0.31 | 612 | 13 | 0.04 | 6 | 0.13 | 31 | <3 | <5 | <2 | 2 | 24 | <5 | <3 | 203 |
| C88-9948 | 0.1 | 0.17 | 270 | 145 | <3 | 12 | <3 | 0.27 | 1.5 | 15 | 45 | 2093 | 4.72 | 0.07 | 0.06 | 61 | 21 | 0.02 | 4 | 0.17 | 74 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 84 |
| C88-9949 | 0.1 | 0.28 | 43 | 160 | <3 | 8 | 3 | 0.70 | 2.2 | 17 | 36 | 2467 | 5.81 | 0.15 | 0.21 | 445 | 32 | 0.03 | 6 | 0.13 | 30 | <3 | <5 | <2 | 3 | 31 | <5 | <3 | 45 |
| C88-9950 | 0.1 | 0.19 | 60 | 160 | <3 | 12 | <3 | 0.87 | 2.1 | 17 | 50 | 2523 | 5.37 | 0.17 | 0.40 | 640 | 17 | 0.03 | 5 | 0.14 | 29 | <3 | <5 | <2 | 2 | 35 | <5 | <3 | 82 |
| C88-9951 | 0.1 | 0.14 | 57 | 100 | <3 | 12 | 3 | 0.52 | 1.7 | 16 | 50 | 823 | 5.31 | 0.13 | 0.20 | 262 | 33 | 0.02 | 12 | 0.16 | 31 | <3 | <5 | <2 | 3 | 17 | <5 | <3 | 37 |
| C88-9952 | 0.9 | 0.21 | 98 | 150 | <3 | 10 | 3 | 0.72 | 2.6 | 18 | 34 | 2045 | 5.65 | 0.16 | 0.18 | 343 | 13 | 0.03 | 10 | 0.14 | 68 | <3 | <5 | <2 | 3 | 28 | <5 | <3 | 95 |
| C88-9953 | 0.1 | 0.95 | 11 | 140 | <3 | 12 | <3 | 0.46 | 1.5 | 14 | 24 | 1644 | 4.03 | 0.09 | 0.96 | 289 | 4 | 0.03 | 4 | 0.17 | 16 | <3 | <5 | <2 | 2 | 16 | <5 | <3 | 96 |
| C88-9954 | 0.1 | 0.26 | 19 | 320 | <3 | 12 | <3 | 0.74 | 1.8 | 13 | 22 | 2857 | 4.24 | 0.14 | 0.40 | 438 | 16 | 0.02 | 4 | 0.16 | 31 | <3 | <5 | <2 | 2 | 27 | <5 | <3 | 58 |
| C88-9955 | 0.1 | 0.43 | 11 | 230 | <3 | 10 | <3 | 1.32 | 1.5 | 13 | 34 | 1665 | 4.16 | 0.21 | 0.44 | 958 | 7 | 0.02 | 3 | 0.17 | 32 | <3 | <5 | <2 | <2 | 36 | <5 | <3 | 78 |
| C88-9956 | 0.1 | 0.70 | 14 | 160 | <3 | 11 | <3 | 0.61 | 1.6 | 13 | 31 | 2423 | 4.26 | 0.13 | 0.59 | 330 | 15 | 0.02 | 4 | 0.15 | 17 | <3 | <5 | <2 | 2 | 31 | <5 | <3 | 57 |
| C88-9957 | 0.1 | 0.39 | 19 | 140 | <3 | 8 | <3 | 1.72 | 1.7 | 12 | 52 | 2068 | 5.22 | 0.27 | 0.41 | 238 | 6 | 0.03 | 6 | 0.13 | 20 | <3 | <5 | <2 | <2 | 150 | <5 | <3 | 46 |
| C88-9958 | 0.1 | 1.01 | 8 | 70 | <3 | 10 | <3 | 1.30 | 1.9 | 12 | 31 | 484 | 4.27 | 0.21 | 1.22 | 680 | 2 | 0.04 | 6 | 0.15 | 33 | <3 | <5 | <2 | 2 | 106 | <5 | <3 | 177 |
| C88-9959 | 0.1 | 0.54 | 20 | 70 | <3 | 12 | 3 | 1.91 | 1.9 | 13 | 30 | 343 | 4.37 | 0.30 | 0.63 | 242 | 4 | 0.03 | 8 | 0.13 | 32 | <3 | <5 | <2 | <2 | 222 | <5 | <3 | 83 |
| C88-9960 | 0.1 | 0.97 | 19 | 135 | <3 | 12 | 3 | 0.92 | 2.1 | 14 | 44 | 1716 | 3.99 | 0.18 | 1.09 | 378 | 7 | 0.03 | 10 | 0.15 | 23 | <3 | <5 | <2 | 2 | 87 | <5 | <3 | 125 |
| C88-9961 | 1.1 | 0.27 | 20 | 130 | <3 | 10 | 3 | 0.78 | 1.8 | 14 | 58 | 4352 | 4.69 | 0.18 | 0.17 | 184 | 8 | 0.02 | 7 | 0.15 | 24 | <3 | <5 | <2 | 3 | 58 | <5 | <3 | 34 |
| C88-9962 | 0.1 | 0.71 | 29 | 70 | <3 | 12 | 4 | 2.11 | 2.1 | 15 | 65 | 880 | 5.07 | 0.33 | 0.93 | 401 | 7 | 0.03 | 13 | 0.14 | 37 | <3 | <5 | <2 | 3 | 241 | <5 | <3 | 100 |
| C88-9963 | 0.1 | 0.56 | 54 | 50 | <3 | 11 | <3 | 1.49 | 2.1 | 11 | 33 | 395 | 4.28 | 0.26 | 0.79 | 630 | 2 | 0.03 | 5 | 0.15 | 54 | <3 | <5 | <2 | 2 | 105 | <5 | <3 | 123 |
| C88-9964 | 0.1 | 0.58 | 42 | 20 | <3 | 10 | 5 | 0.61 | 2.3 | 19 | 39 | 829 | 6.06 | 0.14 | 0.63 | 202 | 4 | 0.03 | 19 | 0.18 | 31 | <3 | <5 | <2 | 3 | 52 | <5 | <3 | 75 |
| C88-9965 | 0.1 | 0.32 | 37 | 120 | <3 | 9 | 5 | 2.21 | 2.1 | 20 | 45 | 466 | 6.04 | 0.35 | 0.29 | 749 | 5 | 0.03 | 19 | 0.16 | 29 | <3 | <5 | <2 | 3 | 102 | <5 | <3 | 77 |
| C88-9966 | 0.9 | 0.33 | 30 | 110 | <3 | 10 | <3 | 0.94 | 1.9 | 14 | 36 | 512 | 4.37 | 0.20 | 0.29 | 463 | 3 | 0.02 | 5 | 0.15 | 41 | <3 | <5 | <2 | 3 | 41 | <5 | <3 | 63 |
| C88-9967 | 2.5 | 0.19 | 85 | 10 | <3 | 12 | <3 | 1.05 | 2.3 | 15 | 49 | 624 | 4.26 | 0.24 | 0.07 | 445 | 3 | 0.03 | 6 | 0.18 | 577 | <3 | <5 | <2 | 4 | 31 | <5 | <3 | 102 |
| C88-9968 | 11.6 | 0.11 | 419 | 800 | <3 | 11 | 8 | 2.60 | 10.4 | 11 | 50 | 12762 | 9.81 | 0.39 | 0.05 | 1281 | 4 | 0.16 | 7 | 0.14 | 425 | <3 | <5 | <2 | 4 | 60 | <5 | <3 | 1530 |
| C88-9969 | 0.1 | 0.21 | 41 | 160 | <3 | 12 | <3 | 2.27 | 2.7 | 11 | 48 | 522 | 5.87 | 0.35 | 0.15 | 1132 | 4 | 0.04 | 4 | 0.15 | 211 | <3 | <5 | <2 | 2 | 53 | <5 | <3 | 142 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

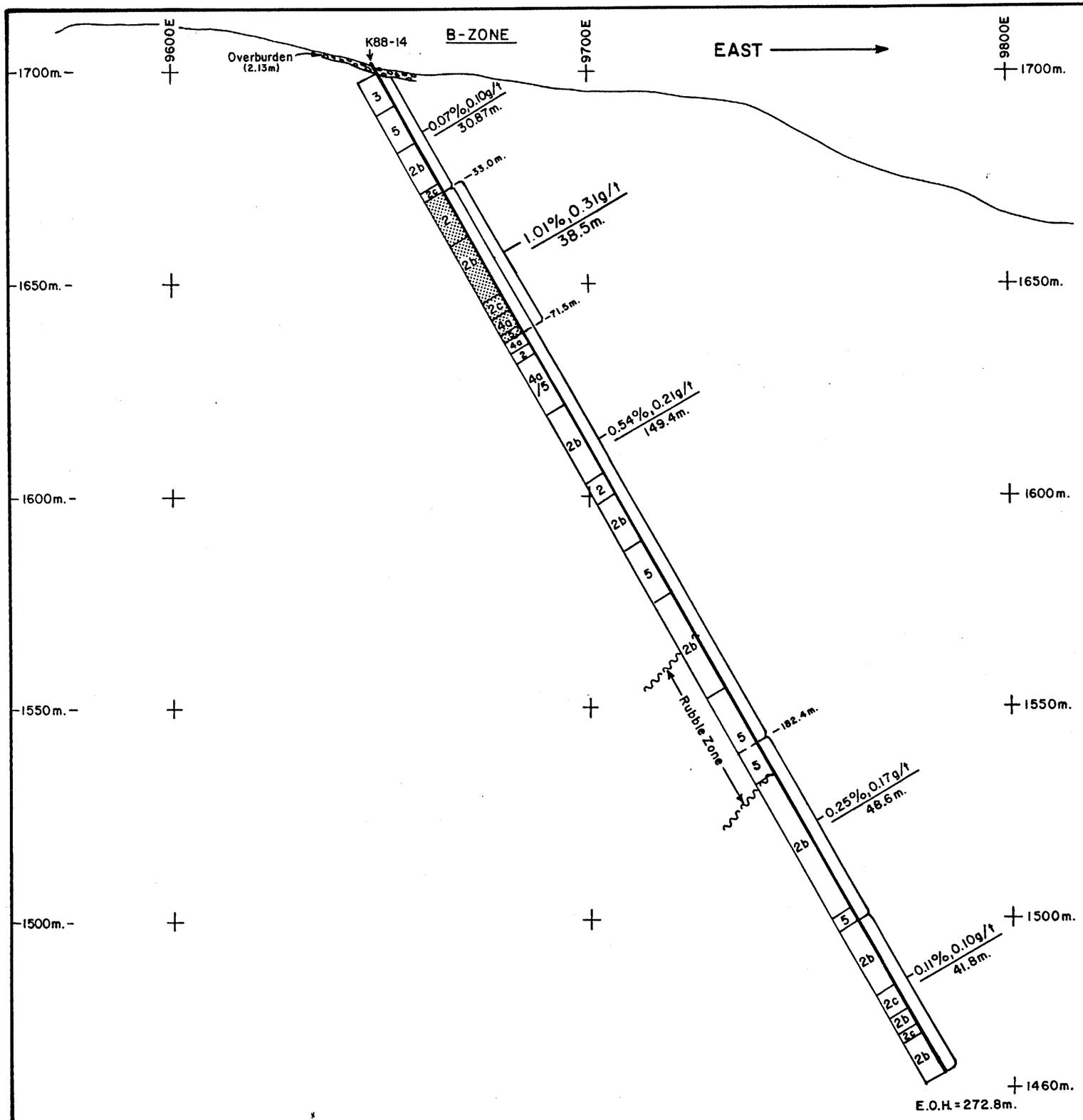
< = Less than Minimum is = Insufficient Sample ns = No sample > = Greater than Maximum AuFA = Fire assay/AAS

| | Al | | Au | As | | Bi | | Cd | | | | | | | | | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | % | | ppb | ppm | | ppm | | ppm | | ppm | | % | | % | | ppm | | ppm | | ppm | | ppm | | ppm | | ppm | |
| C88-9970 | 0.5 | 0.66 | 11 | 130 | <3 | 23 | 3 | 1.70 | 1.7 | 14 | 34 | 1 | 4.37 | 0.27 | 0.75 | 1116 | 2 | 0.04 | 5 | 0.17 | 44 | <3 | <5 | <2 | | 35 | <5 | <3 |
| C88-9971 | 0.1 | 0.94 | <3 | 50 | <3 | 34 | <3 | 2.18 | 1.2 | 10 | 38 | <1 | 3.98 | 0.29 | 0.96 | 1671 | 1 | 0.04 | 4 | 0.14 | 4 | <3 | <5 | <2 | | 44 | <5 | <3 |
| C88-9972 | 0.6 | 0.76 | 71 | 65 | <3 | 27 | <3 | 1.98 | 1.1 | 12 | 36 | 583 | 4.72 | 0.28 | 0.97 | 1146 | 2 | 0.03 | 7 | 0.17 | 25 | <3 | <5 | <2 | 2 | 45 | <5 | <3 |
| C88-9973 | 0.4 | 2.39 | 9 | <5 | <3 | 635 | 9 | 2.66 | 1.4 | 29 | 114 | 58 | 4.74 | 0.34 | 3.62 | 895 | 3 | 0.04 | 81 | 0.47 | 28 | <3 | <5 | <2 | 5 | 163 | <5 | <3 |
| C88-9974 | 0.4 | 0.59 | 12 | <5 | <3 | 26 | <3 | 1.92 | 1.1 | 13 | 48 | 381 | 4.12 | 0.28 | 0.35 | 1039 | 2 | 0.02 | 7 | 0.18 | 14 | <3 | <5 | <2 | 3 | 130 | <5 | <3 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

## ANOMALOUS RESULTS:

FURTHER ANALYSES
BY ALTERNATE
METHODS SUGGESTED




## LEGEND

Fault

0.13%, 1.13g/t / 10.3m. — %Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Interval defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE - fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE — medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE — aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a)/MONZONITE(4b) — medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST — foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) — interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE — interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

1:1000

SCALE 0 10 20 30 40 Metres

# SULPHURETS GOLD CORPORATION

1989 KERR PROJECT

D.D.H. K88-14

SECTION

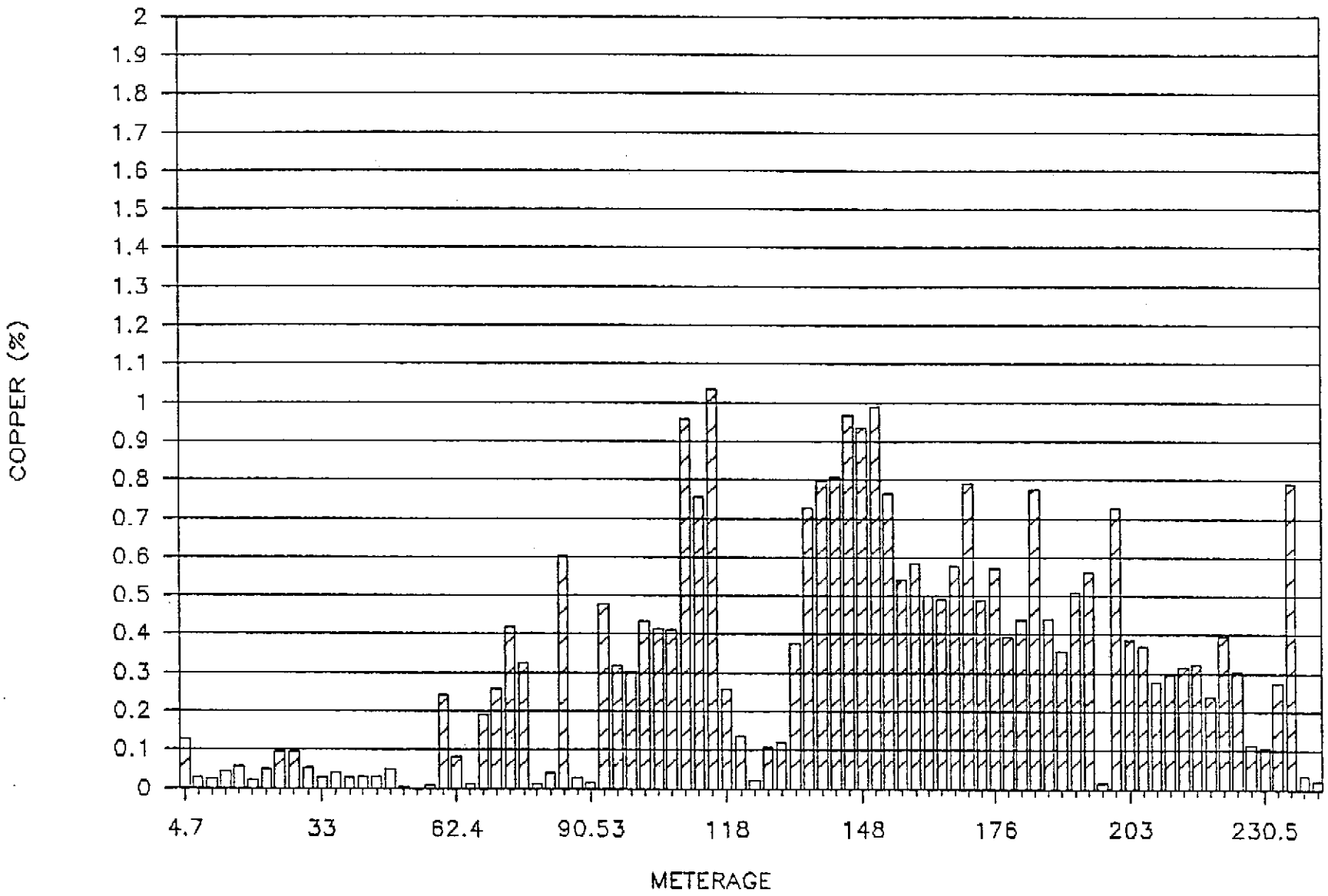
COLLAR:- 9847.3N, 9650.2E

BEARING: 090° DIP: -60°

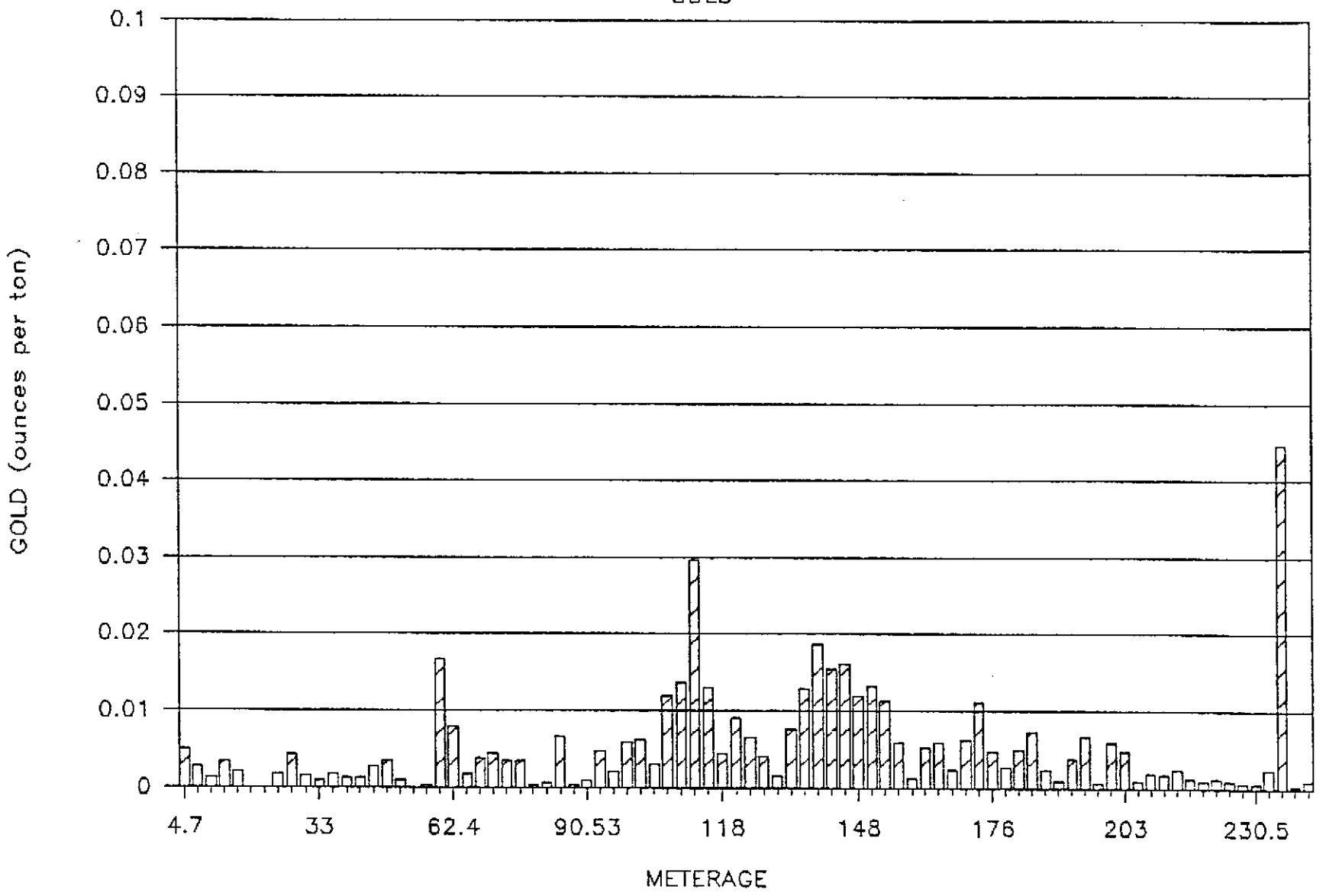
ELEVATION: 1700.6m.

REPORT 1065 FIGURE No.

# K88-15


COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
4.7
33
62.4
90.53
118
148
176
203
230.5
METERAGE

# K88-15


GOLD
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
GOLD (ounces per ton)
4.7
33
62.4
90.53
118
148
176
203
230.5
METERAGE

KERR PROJECT D.D.HOLE K-88-15

LOCATION SOUTH B-ZONE > G-ZONE TOP OF CLIFFS ABOVE GLACIER
DATE STARTED JULY 27, 1988
DATE COMPLETED JULY 29, 1988
CORE RECOVERY 50.05%
DRILLED BY FALCON DRILLING LTD.
LOGGED BY S. CASSELMAN

COLLAR LAT. 9415.0 NORTH
LONG. 9748.1 EAST
ELEVATION 1594.2 m
AZIMUTH 090 DIP -60 deg
LENGTH 239.88 m
HOR. PROJ. 119.94 m
VERT. PROJ. 207.74 m

OBJECTIVE TRACE B-ZONE FAULT/MINERALIZATION TO SOUTH
DIP TEST DEPTH _____m DIP_____deg
DEPTH _____m DIP_____deg

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 3.05 | 3.05 | OVERBURDEN |
| 3.05 | 4.70 | 1.65 | DACITE CRYSTAL TUFF<br>- light to medium green, sheared, well foliated at 50 deg to C.A.<br>- grades from strong to weak sericite and chlorite<br>- 7% pyrite as fine disseminations and thin (< 1 mm) veinlets |
| 4.70 | 9.60 | 4.90 | HORNBLENDE PLAGIOCLASE DIORITE DYKE<br>- moderate to intense sericitization, weak to moderate chloritization<br>- medium green colour<br>- upper contact bleached and clay altered for 1 m - also quite fractured with limonite on fracture surfaces<br>- upper contact at 50 deg to C.A., lower contact at 70 deg<br>- moderate to well developed foliation at 50 deg<br>- hornblende altered to chlorite, plagioclase altered to sericite<br>- 8 cm bull white quartz vein at 7.5 m- barren of sulphides |
| 9.60 | 24.00 | 14.40 | MEDIUM-GRAINED DACITE CRYSTAL TUFF<br>- overall light to medium green colour, however, it grades from light green to bleached in sheared sections, to medium green in less sheared sections<br>- more sheared, bleached sections are generally more fractured (brecciated)<br>- lower contact with sericite schist is gradational |

KERR PROJECT D.D.HOLE K-88-15

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - sericite schist probably has same protolith, however it is more sheared and sericitized<br>- contact is arbitrary |
| 24.00 | 47.65 | 23.65 | SERICITE SCHIST<br>- light to medium grey, intense sericitization<br>- well developed foliation at 50 deg to C.A.<br>- occasional section of sericitic fault gouge up to 10 cm wide<br>- pyrite as fine disseminations<br>- toward lower contact foliation is wavy in places<br>- within 3 m of lower contact occur abundant limonitic clay bands 1 cm to 10 cm wide in bleached sericite schist<br>- sections of increase chlorite content<br>- possibly some chalcocite associated with pyrite disseminations, however only trace amounts |
| 47.65 | 57.40 | 9.75 | ANDESITE DYKE<br>- medium to dark green, fine- to medium-grained, to aphanitic, partially chloritized and sericitized<br>- 2 - 3% quartz-carbonate veins, barren of sulphides<br>- < 2% sulphides overall<br>- at upper contact have a 20 cm section with coarse-grained (up to 5 mm) plagioclase phenocrysts which grades into the finer andesite dyke<br>- upper contact at 60 deg, lower contact at 55 deg to C.A.<br>- gradational upper and lower contacts<br>- towards lower contact core is more fractured with more quartz veining and bleached<br>- slightly magnetic |
| 57.40 | 62.40 | 5.00 | SERICITE SCHIST<br>- as in section 24.0 to 47.65 m<br>- well developed foliation at 50 deg to C.A.<br>- 10 to 15% pyrite as fine disseminations and stringers<br>- quite fractured nearing intensely faulted zone |

KERR PROJECT D.D.HOLE K-88-15

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 62.40 | 62.65 | 0.25 | ANDESITE DYKE<br>- as in section 47.65 - 57.4 m<br>- upper contact at 70 deg, lower at 35 deg to C.A.<br>- 1 cm chilled margin-sericite |
| 62.65 | 69.19 | 6.54 | SERICITE SCHIST<br>- as in section 57.4 to 62.4 m |
| 69.19 | 71.50 | 2.31 | FAULT ZONE - GOUGE<br>- light brown clayey sand<br>- particle size is 1 mm and less<br>- core comes out as cylindrical mud<br>- occasional 1% rock fragments rounded up to 2.5 cm diameter<br>- this zone probably absorbed all shear forces which were not absorbed by dyke |
| 71.50 | 83.50 | 12.00 | ANDESITE DYKE<br>- 71.5 to 77.5 - quite fractured section, average particle size 2 mm<br>- medium green colour, moderate chloritization, weak sericitization<br>- 5 to 10% finely disseminated pyrite<br>- from 77.5 to 83.5 - dyke is more competent<br>- light to medium green, aphanitic to fine-grained<br>- weak to intense chloritization<br>- weak to moderate sericitization<br>- 5% quartz-calcite-chlorite veins - batten of sulphides - chlorite occurs as large dark green blotches - veins at 35-45 deg to C.A.<br>- < 1% pyrite<br>- upper contact defined by change from fault gouge (sand) to 1-2 cm chips of rock<br>- lower contact marked by gradation to sheared, sericitic schist, which is possibly just more intensely sheared and altered andesite dyke |

KERR PROJECT D.D.HOLE K-88-15

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 83.50 | 85.80 | 2.30 | FAULT ZONE / QUARTZ-SERICITE-PYRITE SCHIST<br>- well developed foliation at 80 deg to C.A.<br>- average particle size is about 3-5 cm long<br>- banded sericite, 10% pyrite, occasional quartz vein<br>- abundant limonite and weathered veins<br>- some rock chips are dark green and appear to be andesitic material |
| 85.80 | 90.53 | 4.73 | ANDESITE DYKE<br>- as in 71.5 to 83.5 m<br>- light to medium green, upper 1 m quite light green - sericitic<br>- 2 to 3% quartz-calcite-chlorite veins up to 5 cm wide<br>- lower contact at 60 deg to C.A. |
| 90.53 | 101.80 | 11.27 | HORNBLENDE-PLAGIOCLASE PORPHYRY DIORITE<br>- quite sheared and altered<br>- possibly could be coarse-grained crystal tuff, however looks more like diorite dyke<br>- well foliated at 50 deg to C.A.<br>- intense sericitization of matrix and plagioclase, chloritization of hornblende crystals<br>- 10 to 15% pyrite as fine disseminations and coatings on slip planes |
| 101.80 | 160.00 | 58.20 | FAULT ZONE / QUARTZ-SERICITE SCHIST<br>- quite fractured, average size 10 cm<br>- overall medium green to blue-grey colour, quite variable appearance<br>- abundant quartz-sulphide veins (pyrite, chalcopyrite, chalcocite, bornite<br>- sections contains patchy epidote<br>- intense sericitization and silicification<br>- sulphides occur as fine disseminations, blebs, stringers, and patches within quartz veins<br>- varied appearance throughout interval<br>- protolith : probably dacitic tuffs<br>- all quite fractured and altered<br>- at 106.7 m - 15 cm vein, massive pyrite with chalcopyrite and minor chalcocite and numerous smaller 2 mm - 1 cm pyrite veins<br><br>- from 121 to 127 less fractured - more homogeneous light green-grey, sericitized |

KERR PROJECT D.D.HOLE K-88-15

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - increased calcite content, less pyrite and quartz<br>- 127 to 136 - quite fractured average particle size 5 cm, poor core recovery, however rock appears to be the same<br>- at 136.5 m 30 cm massive pyrite vein with some quartz and chalcopyrite<br>- 136 to 145 - rock is fairly competent-average size is approximately 5 to 10 cm-fairly silicified<br>- 145 to 160 quite fractured, poor recovery, average size 2 cm<br>- at 145.39 - 30 cm of grey mud - gouge |
| 160.00 | 166.73 | 6.73 | FRACTURED HORNBLENDE PLAGIOCLASE PORPHYRY DIORITE DYKE<br>- average particle size 1 to 2 cm long, all fractured surfaces coated with limonite<br>- 10 to 15% hornblende altered to chlorite, matrix altered to sericite<br>- 8% disseminated pyrite, possibly some chalcocite (< .5%) - no chalcopyrite visible |
| 166.73 | 168.23 | 1.50 | FAULT GOUGE<br>- medium green silty mud (rock flour)<br>- has consistency of pudding |
| 168.23 | 196.00 | 27.77 | FAULT ZONE / QUARTZ-SERICITE-PYRITE SCHIST<br>- as in section 101.8 to 160.0 m<br>- from 168.23 to 173.0 quite silicified with quartz-pyrite, some chalcopyrite veins<br>- average particle size 1 to 2 cm, quite fractured<br>- 10 to 20 deg disseminated pyrite and chalcocite<br>- chalcocite may be just a coating on pyrite |
| 196.00 | 197.00 | 1.00 | ANDESITE DYKE<br>- medium green, fine-grained<br>- 5% quartz-calcite veins / low sulphide content upper contact at 70 deg, lower at 80 deg to C.A. |
| 197.00 | 218.00 | 21.00 | FAULT ZONE / QUARTZ-SERICITE-PYRITE SCHIST<br>- as in section 168.23 to 196.0 m |

KERR PROJECT D.D.HOLE K-88-15

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 218.00 | 221.59 | 3.59 | QUARTZ-SERICITE-PYRITE SCHIST<br>- quite hard and competent<br>- light grey, silicified with clear to white quartz veinlets<br>- 15 to 20% pyrite as fine disseminations and stringers<br>- good recovery |
| 221.59 | 236.30 | 14.71 | FAULT ZONE / QUARTZ-SERICITE SCHIST<br>- as in section 197.0 to 218.0 m<br>- average particle size 1-2 cm wide<br>- quite fractured<br>- at 234.0 m numerous pyrite, chalcopyrite (10% of vein) veins with quartz |
| 236.30 | 239.98 | 3.58 | PLAGIOCLASE PORPHYRY DYKE<br>- fine-grained matrix, plagioclase to 3 mm<br>- 35% plagioclase phenocrysts<br>- densely packed in sections<br>- upper contact marked by decreasing number of phenocrysts to a dark green matrix<br>- abundant sericite and chlorite - 3% quartz-calcite veins - unmineralized<br>- Cu mineralization could continue past dyke<br><br>E.O.H. |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 25 Nov 1988 12:52:58 Page 1

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8815 | 9415.0 | 9748.1 | 1594.2 | 90 | 60 | 239.9 | B-Zone | Test of southern and western contact | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 3.05 | 3.05 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 3.05 | 4.70 | 1.65 | 30 | HBLD PLAG DYKE | | F.MG | | 1 | 30 | 3 | 8 | | | | | | 45 | 5 | | | .1 | | | |
| 4.7 | 7.15 | 2.45 | 29 | HBLD PLAG DYKE | | MG | | 2 | 40 | 10 | 5 | | | | | | 60 | 2 | | | | | | |
| 7.15 | 9.60 | 2.45 | 35 | HBLD PLAG DYKE | | MG | | 2 | 35 | 5 | 15 | | | | | | 60 | 2 | | | | | | |
| 9.6 | 12.0 | 2.4 | 28 | DCIT XTAL TUFF | | MG | | 2 | 35 | 8 | 10 | | | | | | 60 | 7 | | | | | | |
| 12. | 15.0 | 3 | 35 | DCIT XTAL TUFF | | MG | | 1 | 40 | 8 | 12 | | 1 | | | | 65 | 5 | | | .1 | | | |
| 15 | 18 | 3 | 25 | DCIT XTAL TUFF | | MG | | 1 | 40 | 15 | 8 | | | | | | 65 | 7 | | | | | | |
| 18 | 21 | 3 | 34 | DCIT XTAL TUFF | | MG | | .5 | 50 | 5 | 5 | | | | | | 65 | 10 | | | .1 | | | |
| 21 | 24 | 3 | 22 | DCIT XTAL TUFF | | MG | | .5 | 55 | 3 | 5 | | | | | | 65 | 10 | | | | | | |
| 24 | 27 | 3 | 30 | SRCT SCHT | | FG | | .5 | 60 | 1 | 8 | | | | | | 75 | 10 | | | .2 | | | |
| 27 | 30 | 3 | 22 | SRCT SCHT | | FG | | 1 | 75 | 2 | 5 | | | | | | 85 | 12 | | | .1 | | | |
| 30 | 33 | 3 | 14 | SRCT SCHT | | FG | | 1 | 80 | 5 | 3 | | | | | | 100 | 10 | | | | | | |
| 33 | 36 | 3 | 26 | SRCT SCHT | | FG | | .5 | 60 | 3 | 3 | | | | | | 75 | 8 | | | | | | |
| 36 | 39 | 3 | 31 | SRCT SCHT | | FG | | 1 | 60 | 1 | 3 | | | | | | 70 | 8 | | | .1 | | | |
| 39 | 42 | 3 | 31 | SRCT SCHT | | FG | | 2 | 60 | 1 | 3 | | | | | | 70 | 12 | | | .1 | | | |
| 42 | 45 | 3 | 29 | SRCT SCHT | | FG | | .5 | 65 | 1 | 3 | | | | | | 75 | 10 | .2 | | | | | |
| 45 | 47.65 | 2.65 | 17 | SRCT SCHT | | FG | | 1 | 70 | 2 | 1 | | | | | | 80 | 15 | | | .5 | | | |
| 47.65 | 50.0 | 2.35 | 49 | ANDS DYKE | | FG | 1 | 3 | 20 | | 20 | | 1 | | | | 45 | 1 | | | | | | |
| 50. | 54.4 | 4.4 | 51 | ANDS DYKE | | FG | | 1 | 20 | | 20 | | 1 | | | | 45 | 1 | | | | | | |
| 54.4 | 57.4 | 3 | 35 | ANDS DYKE | | FG | | 3 | 30 | 3 | 10 | | 1 | | | | 50 | 1 | | | | | | |
| 57.4 | 59.9 | 2.5 | 29 | SRCT SCHT | | FG | | 1 | 75 | 5 | 3 | | | | | | 95 | 10 | | | .5 | | | |
| 59.9 | 62.4 | 2.5 | 26 | SRCT SCHT | | FG | | 2 | 75 | 5 | 3 | | | | | | 95 | 10 | | | .5 | | | |
| 62.4 | 62.65 | .25 | 31 | ANDS DYKE | | FG | | | 8 | 1 | 30 | | 1 | | | | 40 | 1 | | | | | | |
| 62.65 | 69.19 | 6.54 | 22 | SRCT SCHT | | FG | | 2 | 60 | 8 | 10 | | | | | | 100 | 20 | | | | | | |
| 69.19 | 71.5 | 2.31 | 0 | FAULT ZONE | | FG | | | 60 | 30 | | | | | | | 100 | .5 | | | | | | |
| 71.5 | 74.5 | 3 | 28 | ANDS DYKE | | VFG | | 3 | 15 | 1 | 30 | | 1 | | | | 55 | 10 | | | | | | |
| 74.5 | 77.5 | 3 | 27 | ANDS DYKE | | VFG | | 3 | 20 | 2 | 30 | | 1 | | | | 60 | 8 | | | | | | |
| 77.5 | 80.5 | 3 | 38 | ANDS DYKE | | F.MG | | 5 | 15 | 1 | 40 | | 1 | | | | 55 | 2 | | | | | | |
| 80.5 | 83.5 | 3 | 39 | ANDS DYKE | | F.MG | | 5 | 10 | 1 | 30 | | 1 | | | | 50 | 1 | | | | | | |
| 83.5 | 85.8 | 2.3 | 22 | FAULT ZONE | | FG | | 3 | 35 | 3 | 8 | | | | | | 60 | 12 | | | .2 | | | |
| 85.8 | 88.8 | 3 | 47 | ANDS DYKE | | FG | | 5 | 20 | 2 | 20 | .2 | 2 | | | | 55 | 1 | | | | | | |
| 88.8 | 90.53 | 1.73 | 51 | ANDS DYKE | | FG | | 5 | 20 | 2 | 20 | .2 | 2 | | | | 55 | 1 | | | | | | |
| 90.53 | 93.5 | 2.97 | 23 | FAULT SRCT SCHT | | M.CG | 1 | | 70 | 3 | 10 | | | | | | 85 | 12 | | | .5 | | | |
| 93.5 | 96.5 | 3 | 22 | FAULT SRCT SCHT | | M.CG | | .5 | 70 | 2 | 10 | | | | | | 90 | 12 | | | .5 | | | |
| 96.5 | 99.5 | 3 | 24 | FAULT SRCT SCHT | | M.CG | | .5 | 70 | 2 | 12 | | | | | | 90 | 15 | | | .5 | | | |
| 99.5 | 101.8 | 2.3 | 25 | FAULT SRCT SCHT | | M.CG | | .5 | 70 | 2 | 12 | | | | | | 90 | 15 | | | .5 | | | |
| 101.8 | 103.0 | 1.2 | 38 | FAULT SRCT SCHT | | FG | 1 | 2 | 70 | 1 | 3 | | | | | | 95 | 15 | .5 | | .5 | | | |
| 103 | 106 | 3 | 26 | FAULT SRCT SCHT | | FG | 1 | 3 | 65 | 1 | 3 | | | | | | 100 | 25 | 1 | | 2 | | | |
| 106 | 109 | 3 | 28 | FAULT SRCT SCHT | | FG | 1 | 2 | 70 | 1 | 3 | | | | | | 100 | 20 | .5 | | 2 | | | |
| 109 | 112 | 3 | 28 | FAULT SRCT SCHT | | FG | .5 | 5 | 55 | 1 | 2 | 1 | | | | | 100 | 25 | 1 | | 2 | | | |
| 112 | 115 | 3 | 26 | FAULT SRCT SCHT | | FG | 2 | 3 | 60 | 2 | 2 | 1 | 1 | | | | 100 | 18 | 1 | | 3 | | | |
| 115 | 118 | 3 | 25 | FAULT SRCT SCHT | | FG | 2 | 3 | 60 | 1 | 2 | .2 | 3 | | | | 100 | 15 | .5 | | 1 | | | |
| 118 | 121 | 3 | 30 | FAULT SRCT SCHT | | FG | 1 | 3 | 65 | | 3 | 1 | 2 | | | | 100 | 12 | .2 | | 1 | | | |
| 121 | 124 | 3 | 22 | FAULT SRCT SCHT | | FG | 1 | 2 | 75 | 1 | 1 | .2 | 2 | | | | 100 | 10 | .1 | | .5 | | | |
| 124 | 127 | 3 | 24 | FAULT SRCT SCHT | | FG | 4 | 5 | 70 | | 1 | .2 | 3 | | | | 100 | 12 | .3 | | .5 | | | |
| 127 | 130 | 3 | 25 | FAULT SRCT SCHT | | FG | 10 | 5 | 60 | | 2 | | 5 | | | | 100 | 15 | .5 | | .5 | | | |
| 130 | 133 | 3 | 24 | FAULT SRCT SCHT | | FG | 10 | 5 | 60 | | 2 | | 5 | | | | 100 | 15 | .2 | | .5 | | | |
| 133 | 136 | 3 | 23 | FAULT SRCT SCHT | | FG | 5 | 5 | 60 | | 2 | | 5 | | | | 100 | 15 | .1 | | 2 | | | |
| 136 | 139 | 3 | 30 | FAULT SRCT SCHT | | FG | 15 | 8 | 40 | | 2 | 1 | 5 | | | | 100 | 25 | .5 | | 2 | | | |
| 139 | 142 | 3 | 26 | FAULT SRCT SCHT | | FG | 10 | 8 | 55 | 1 | 3 | .2 | 2 | | | | 100 | 15 | | | 1 | | | |
| 142 | 145 | 3 | 24 | FAULT SRCT SCHT | | FG | 10 | 5 | 70 | | 1 | | 1 | | | | 100 | 10 | | | 2 | | | |
| 145 | 148 | 3 | 7 | FAULT SRCT SCHT | | FG | 30 | 2 | 50 | 2 | 2 | | | | | | 100 | 10 | | | 2 | | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | |
|---|---|---|---|---|---|---|---|---|---|
| 8815 | 9415.0 | 9748.1 | 1594.2 | 90 | 60 | 239.9 | B-Zone | Test of southern and western contact | #HOLE |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 148 | 151 | 3 | 29 | FAULT SRCT SCHT | | FG | 25 | 8 | 45 | | 2 | | | | | | 100 | 15 | | | 3 | | | |
| 151 | 154 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 3 | 65 | 1 | 1 | | | | | | 100 | 15 | | | 2 | | | |
| 154 | 157 | 3 | 21 | FAULT SRCT SCHT | | FG | 15 | 5 | 50 | | 5 | | | | | | 100 | 20 | | | 3 | | | |
| 157 | 160 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 2 | 65 | | 3 | | | | | | 100 | 25 | | | 4 | | | |
| 160 | 163 | 3 | 36 | HBLD PLAG DYKE | | M.CG | 10 | 5 | 50 | 5 | 8 | 1 | | | | | 95 | 15 | | | .5 | | | |
| 163 | 165 | 2 | 36 | HBLD PLAG DYKE | | M.CG | 8 | 3 | 55 | 5 | 8 | 2 | | | | | 95 | 18 | | | .5 | | | |
| 165 | 166.73 | 1.73 | 36 | HBLD PLAG DYKE | | M.CG | 5 | 3 | 60 | 5 | 8 | 2 | | | | | 95 | 15 | | | 1 | | | |
| 166.73 | 168.23 | 1.5 | 0 | FAULT GOUGE | | VFG | | | 85 | 10 | | | | | | | 100 | | | | | | | |
| 168.23 | 170 | 1.77 | 26 | FAULT SRCT SCHT | | FG | 20 | 10 | 40 | 1 | 3 | .2 | | | | | 100 | 22 | .5 | | .5 | | | |
| 170 | 176 | 6 | 10 | FAULT SRCT SCHT | | FG | 10 | 15 | 40 | | 5 | | | | | | 100 | 25 | 1 | | .5 | | | |
| 176 | 179 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 5 | 50 | | 10 | | | | | | 100 | 18 | | | 2 | | | |
| 179 | 182 | 3 | 23 | FAULT SRCT SCHT | | FG | 8 | 2 | 60 | | 10 | | | | | | 100 | 15 | | | 2 | | | |
| 182 | 185 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 2 | 60 | | 8 | | | | | | 100 | 15 | | | 2 | | | |
| 185 | 188 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 2 | 60 | | 3 | | | | | | 100 | 18 | | | 2 | | | |
| 188 | 191 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 2 | 60 | | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 191 | 194 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 2 | 60 | | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 194 | 196 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 2 | 60 | | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 196 | 197 | 1 | 37 | ANDS DYKE | | FG | | 2 | 10 | | 15 | | 5 | | | | 35 | 1 | | | | | | |
| 197 | 200 | 3 | 24 | FAULT SRCT SCHT | | FG | 10 | 5 | 55 | | 2 | | | | | | 100 | 25 | | | 2 | | | |
| 200 | 203 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 5 | 60 | | 2 | | | | | | 100 | 20 | | | 2 | | | |
| 203 | 206 | 3 | 23 | FAULT SRCT SCHT | | FG | 20 | 10 | 45 | | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 206 | 209 | 3 | 23 | FAULT SRCT SCHT | | FG | 20 | 10 | 45 | | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 209 | 212 | 3 | 23 | FAULT SRCT SCHT | | FG | 20 | 10 | 45 | | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 212 | 215 | 3 | 23 | FAULT SRCT SCHT | | FG | 10 | 10 | 55 | 1 | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 215 | 218 | 3 | 23 | FAULT SRCT SCHT | | FG | 15 | 5 | 55 | | 3 | | | | | | 100 | 20 | | | 2 | | | |
| 218 | 220 | 2 | 46 | SRCT SCHT | | FG | 40 | 10 | 30 | | | | | | | | 100 | 18 | | | .1 | | | |
| 220 | 221.59 | 1.59 | 45 | SRCT SCHT | | FG | 40 | 15 | 24 | | | | | | | | 100 | 20 | | | .1 | | | |
| 221.59 | 224.5 | 2.91 | 23 | FAULT SRCT SCHT | | FG | 10 | 3 | 65 | | 3 | | | | | | 100 | 12 | | | 2 | | | |
| 224.5 | 227.5 | 3 | 24 | FAULT SRCT SCHT | | FG | 10 | 3 | 65 | | 3 | | | | | | 100 | 15 | | | 2 | | | |
| 227.5 | 230.5 | 3 | 23 | FAULT SRCT SCHT | | FG | 15 | 5 | 60 | 2 | 3 | | | | | | 100 | 12 | | | 1 | | | |
| 230.5 | 233.5 | 3 | 23 | FAULT SRCT SCHT | | FG | 8 | 5 | 10 | 5 | 5 | 1 | | | | | 100 | 15 | | | 1 | | | |
| 233.5 | 236.3 | 2.8 | 25 | FAULT SRCT SCHT | | FG | 10 | 10 | 50 | | 5 | 1 | | | | | 100 | 20 | 1 | | 1 | | | |
| 236.3 | 238.3 | 2 | 37 | PLAG PRPH DYKE | | F.CG | 8 | 3 | 50 | | 5 | | 5 | | | | 90 | 8 | .5 | | | | | |
| 238.3 | 239.9 | 1.58 | 35 | PLAG PRPH DYKE | | F.CG | 8 | 3 | 50 | | 5 | | 5 | | | | 90 | 8 | .1 | | | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 12:25:42 Page 1

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8815 | 9415.0 | 9748.1 | 1594.2 | 90 | 60 | 239.9 | B-Zone | Test of southern and western contact | |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 3.05 | | 3.05 | 0 | | | | | | | | | | | |
| 3.05 | 4.70 | 3001 | 1.65 | 1.14 | 170 | | .6 | | 1274 | 81 | 3.47 | 42 | 412 | | |
| 4.7 | 7.15 | 3002 | 2.45 | 1.31 | 90 | | .1 | | 255 | 132 | 4.88 | 22 | 838 | | |
| 7.15 | 9.60 | 3003 | 2.45 | 2.05 | 40 | | .1 | | 251 | 149 | 4.07 | 9 | 1480 | | |
| 9.6 | 12.0 | 3004 | 2.4 | 2.06 | 110 | | .1 | | 432 | 62 | 6.15 | 78 | 292 | | |
| 12. | 15.0 | 3005 | 3 | 2.22 | 70 | | .1 | | 556 | 99 | 4.51 | 39 | 1588 | | |
| 15 | 18 | 3006 | 3 | 2.36 | 0 | | .1 | | 206 | 40 | 3.8 | 36 | 297 | | |
| 18 | 21 | 3007 | 3 | 2.69 | 0 | | .1 | | 506 | 70 | 4.77 | 32 | 346 | | |
| 21 | 24 | 3008 | 3 | 2.60 | 60 | | .1 | | 945 | 29 | 5.43 | 29 | 80 | | |
| 24 | 27 | 3009 | 3 | 2.82 | 145 | | .1 | | 958 | 90 | 5.41 | 20 | 551 | | |
| 27 | 30 | 3010 | 3 | 2.46 | 50 | | .5 | | 522 | 56 | 4.88 | 48 | 74 | | |
| 30 | 33 | 3011 | 3 | 2.4 | 30 | | .1 | | 265 | 17 | 4.39 | 21 | 21 | | |
| 33 | 36 | 3012 | 3 | 2.16 | 60 | | .9 | | 400 | 215 | 4.54 | 20 | 1778 | | |
| 36 | 39 | 3013 | 3 | 2.80 | 40 | | .4 | | 278 | 166 | 4.58 | 17 | 1668 | | |
| 39 | 42 | 3014 | 3 | 2.90 | 40 | | .1 | | 308 | 180 | 4.73 | 27 | 3955 | | |
| 42 | 45 | 3015 | 3 | 2.35 | 90 | | 1.1 | | 294 | 138 | 4.74 | 27 | 1672 | | |
| 45 | 47.65 | 3016 | 2.65 | 2.59 | 120 | | 2.2 | | 478 | 146 | 5.04 | 27 | 738 | | |
| 47.65 | 50.0 | 3017 | 2.35 | 2.24 | 30 | | 1.1 | | 29 | 136 | 1.18 | 9 | 483 | | |
| 50. | 54.4 | NS | 4.4 | 4.4 | | | | | | | | | | | |
| 54.4 | 57.4 | 3018 | 3 | 2.35 | 10 | | .9 | | 88 | 49 | 1.54 | 11 | 85 | | |
| 57.4 | 59.9 | 3019 | 2.5 | .82 | 570 | | 1.2 | | 2419 | 215 | 4.08 | 31 | 180 | | |
| 59.9 | 62.4 | 3020 | 2.5 | .67 | 270 | | 1.5 | | 816 | 82 | 4.01 | 26 | 161 | | |
| 62.4 | 62.65 | 3021 | .25 | .25 | 60 | | .9 | | 98 | 608 | 6.85 | 93 | 1659 | | |
| 62.65 | 69.19 | 3022 | 6.54 | .67 | 130 | | 1.8 | | 1894 | 309 | 5.22 | 26 | 1472 | | |
| 69.19 | 71.5 | 3023 | 2.31 | 1.8 | 150 | | .5 | | 2575 | 298 | 6.44 | 42 | 411 | | |
| 71.5 | 74.5 | 3024 | 3 | .58 | 120 | | 1.1 | | 4180 | 146 | 5.10 | 24 | 442 | | |
| 74.5 | 77.5 | 3025 | 3 | .60 | 120 | | 0.6 | | 3264 | 297 | 2.91 | 20 | 1151 | | |
| 77.5 | 80.5 | 3026 | 3 | 2.15 | 10 | | .1 | | 98 | 182 | 2.41 | 18 | 1116 | | |
| 80.5 | 83.5 | 3027 | 3 | 2.23 | 20 | | .2 | | 398 | 298 | 4.37 | 17 | 1208 | | |
| 83.5 | 85.8 | 3028 | 2.3 | 1.2 | 230 | | 2.1 | | 6014 | 185 | 4.24 | 103 | 514 | | |
| 85.8 | 88.8 | 3029 | 3 | 2.7 | 5 | | .2 | | 262 | 135 | 3.06 | 11 | 812 | | |
| 88.8 | 90.53 | 3030 | 1.73 | 1.58 | 30 | | .1 | | 152 | 193 | 3.33 | 14 | 906 | | |
| 90.53 | 93.5 | 3031 | 2.97 | 1.25 | 160 | | 2.1 | | 4788 | 202 | 4.55 | 25 | 1336 | | |
| 93.5 | 96.5 | 3032 | 3 | 1.47 | 70 | | 1.2 | | 3178 | 84 | 4.30 | 34 | 562 | | |
| 96.5 | 99.5 | 3033 | 3 | .99 | 200 | | 1.2 | | 3015 | 151 | 4.99 | 22 | 1536 | | |
| 99.5 | 101.8 | 3034 | 2.3 | .68 | 210 | | 1.5 | | 4321 | 124 | 3.97 | 21 | 1021 | | |
| 101.8 | 103.0 | 3035 | 1.2 | 1.1 | 100 | | 2.2 | | 4141 | 88 | 4.34 | 22 | 813 | | |
| 103 | 106 | 3036 | 3 | 1.77 | 410 | | 1.7 | | 4113 | 85 | 7.65 | 57 | 487 | | |
| 106 | 109 | 3037 | 3 | 1.97 | 470 | | 6.3 | | 9563 | 220 | 4.62 | 209 | 570 | | |
| 109 | 112 | 3038 | 3 | 2.67 | 1020 | | 3.7 | | 7560 | 199 | 5.49 | 87 | 1542 | | |
| 112 | 115 | 3039 | 3 | .84 | 445 | | 2.2 | | 10333 | 143 | 3.79 | 29 | 811 | | |
| 115 | 118 | 3040 | 3 | .42 | 150 | | 1.7 | | 2557 | 27 | 5.49 | 19 | 565 | | |
| 118 | 121 | 3041 | 3 | .86 | 310 | | 1.1 | | 1374 | 167 | 3.09 | 18 | 502 | | |
| 121 | 124 | 3042 | 3 | 2.35 | 220 | | 1.7 | | 214 | 186 | 4.22 | 72 | 1313 | | |
| 124 | 127 | 3043 | 3 | 2.12 | 140 | | 3.7 | | 1079 | 174 | 4.16 | 157 | 2219 | | |
| 127 | 130 | 3044 | 3 | .51 | 50 | | 1.2 | | 1208 | 63 | 2.49 | 34 | 2086 | | |
| 130 | 133 | 3045 | 3 | .25 | 260 | | 7.3 | | 3749 | 109 | 3.29 | 114 | 748 | | |
| 133 | 136 | 3046 | 3 | .70 | 440 | | 7.1 | | 7267 | 78 | 3.29 | 23 | 321 | | |
| 136 | 139 | 3047 | 3 | 2.29 | 640 | | 11.1 | | 7980 | 444 | 6.41 | 58 | 723 | | |
| 139 | 142 | 3048 | 3 | 1.81 | 530 | | 7.1 | | 8067 | 227 | 4.25 | 23 | 515 | | |
| 142 | 145 | 3049 | 3 | 2.23 | 550 | | 8.3 | | 9673 | 42 | 3.59 | 30 | 64 | | |
| 145 | 148 | 3050 | 3 | 1.22 | 410 | | 9.6 | | 9356 | 43 | 3.17 | 22 | 74 | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8815 | 9415.0 | 9748.1 | 1594.2 | 90 | 60 | 239.9 | B-Zone | Test of southern and western contact | |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 148 | 151 | 3051 | 3 | .63 | 450 | | 8.6 | | 9896 | 34 | 2.72 | 22 | 33 | | |
| 151 | 154 | 3052 | 3 | 1.09 | 385 | | 5.5 | | 7645 | 21 | 3.11 | 20 | 27 | | |
| 154 | 157 | 3053 | 3 | .58 | 200 | | 4.1 | | 5402 | 61 | 3.13 | 22 | 168 | | |
| 157 | 160 | 3054 | 3 | .34 | 40 | | 2.9 | | 5844 | 35 | 5.32 | 23 | 119 | | |
| 160 | 163 | 3055 | 3 | 1.05 | 180 | | 1.7 | | 4992 | 62 | 4.00 | 23 | 259 | | |
| 163 | 165 | 3056 | 2 | 0.83 | 200 | | 1.2 | | 4924 | 37 | 3.90 | 19 | 82 | | |
| 165 | 166.73 | 3057 | 1.73 | 1.11 | 80 | | 1.1 | | 5767 | 52 | 4.14 | 23 | 115 | | |
| 166.73 | 168.23 | 3058 | 1.5 | .5 | 210 | | 2.1 | | 7915 | 132 | 5.47 | 29 | 253 | | |
| 168.23 | 170 | 3059 | 1.77 | .81 | 380 | | 2.7 | | 4875 | 63 | 6.16 | 43 | 112 | | |
| 170 | 176 | 3060 | 6 | 1.60 | 160 | | 1.2 | | 5707 | 51 | 3.75 | 15 | 185 | | |
| 176 | 179 | 3061 | 3 | .40 | 90 | | 1.1 | | 3921 | 95 | 3.08 | 19 | 236 | | |
| 179 | 182 | 3062 | 3 | 1.02 | 170 | | 1.2 | | 4345 | 79 | 3.15 | 18 | 200 | | |
| 182 | 185 | 3063 | 3 | .90 | 250 | | 1.7 | | 7755 | 101 | 3.03 | 22 | 135 | | |
| 185 | 188 | 3064 | 3 | 1.4 | 80 | | 1.1 | | 4399 | 200 | 3.58 | 35 | 137 | | |
| 188 | 191 | 3065 | 3 | 1.25 | 30 | | .5 | | 3554 | 91 | 3.19 | 20 | 236 | | |
| 191 | 194 | 3066 | 3 | .69 | 130 | | 1.1 | | 5104 | 71 | 4.47 | 26 | 145 | | |
| 194 | 196 | 3067 | 3 | .70 | 230 | | 1.2 | | 5617 | 60 | 3.12 | 24 | 162 | | |
| 196 | 197 | 3068 | 1 | .87 | 20 | | 1.5 | | 132 | 326 | 8.65 | 108 | 1664 | | |
| 197 | 200 | 3069 | 3 | .62 | 200 | | 1.7 | | 7258 | 149 | 3.79 | 39 | 378 | | |
| 200 | 203 | 3070 | 3 | .77 | 160 | | 1.1 | | 3868 | 104 | 3.73 | 25 | 376 | | |
| 203 | 206 | 3071 | 3 | .83 | 30 | | 1.2 | | 3684 | 35 | 3.64 | 21 | 106 | | |
| 206 | 209 | 3072 | 3 | 1.40 | 65 | | 1.5 | | 2758 | 242 | 4.75 | 26 | 328 | | |
| 209 | 212 | 3073 | 3 | .47 | 60 | | 1.1 | | 2965 | 103 | 3.45 | 23 | 310 | | |
| 212 | 215 | 3074 | 3 | .22 | 80 | | .5 | | 3147 | 62 | 2.94 | 21 | 199 | | |
| 215 | 218 | 3075 | 3 | .22 | 40 | | 1.2 | | 3219 | 59 | 3.98 | 20 | 192 | | |
| 218 | 220 | 3076 | 2 | 1.82 | 30 | | 1.1 | | 2381 | 60 | 4.85 | 14 | 165 | | |
| 220 | 221.59 | 3077 | 1.59 | 1.52 | 40 | | 1.5 | | 3941 | 49 | 3.79 | 13 | 146 | | |
| 221.59 | 224.5 | 3078 | 2.91 | .46 | 30 | | 1.2 | | 3037 | 95 | 4.35 | 27 | 444 | | |
| 224.5 | 227.5 | 3079 | 3 | .72 | 20 | | .7 | | 1130 | 82 | 4.35 | 23 | 275 | | |
| 227.5 | 230.5 | 3080 | 3 | .69 | 20 | | .7 | | 1053 | 128 | 4.77 | 50 | 219 | | |
| 230.5 | 233.5 | 3081 | 3 | 1.6 | 80 | | 1.7 | | 2740 | 218 | 6.52 | 39 | 395 | | |
| 233.5 | 236.3 | 3082 | 2.8 | 1.12 | 1530 | | 26.7 | | 7899 | 1531 | 6.96 | 1000 | 586 | | |
| 236.3 | 238.3 | 3083 | 2 | 1.8 | 10 | | .6 | | 328 | 111 | 2.93 | 151 | 1725 | | |
| 238.3 | 239.9 | 3084 | 1.58 | 1.38 | 30 | | .5 | | 200 | 65 | 2.52 | 174 | 1066 | | |

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1968 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:258-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656


REPORT NUMBER: 881455 AA JOB NUMBER: 881455 WESTERN CDN. MINING CORP. 

| SAMPLE # | Cu % |
|---|---|
| C88-3030 | .01 |
| C88-3031 | .55 |
| C88-3032 | .35 |
| C88-3033 | .34 |
| C88-3034 | .52 |
| C88-3035 | .47 |
| C88-3036 | .43 |
| C88-3037 | 1.07 |
| C88-3038 | .89 |
| C88-3039 | 1.24 |
| C88-3040 | .28 |
| C88-3041 | .15 |
| C88-3042 | .02 |
| C88-3043 | .12 |
| C88-3044 | .14 |
| C88-3045 | .42 |
| C88-3046 | .90 |
| C88-3047 | .94 |
| C88-3048 | .89 |
| C88-3049 | 1.06 |
| DETECTION LIMIT | .01 |

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

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BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-3050 | 1.05 |
| C88-3051 | 1.13 |
| C88-3052 | .90 |
| C88-3053 | .64 |
| C88-3054 | .66 |
| C88-3055 | .55 |
| C88-3056 | .58 |
| C88-3057 | .64 |
| C88-3058 | .94 |
| C88-3059 | .55 |
| C88-3060 | .66 |
| C88-3061 | .44 |
| C88-3062 | .53 |
| C88-3063 | .66 |
| C88-3064 | .45 |
| C88-3065 | .39 |
| C88-3066 | .53 |
| C88-3067 | .63 |
| C88-3068 | .01 |
| C88-3069 | .79 |
| C88-3070 | .42 |
| DETECTION LIMIT | .01 |

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

REPORT #: 880548 PA MESTERN CANADIAN 

| Sample Number | Ag | Al | As | Au/A | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | pp |
| C88-3001 | 0.6 | 0.88 | 42 | 170 | <3 | 29 | <3 | 0.14 | 0.6 | 11 | 33 | 1274 | 3.47 | 0.05 | 0.55 | 412 | 11 | 0.02 | 7 | 0.18 | 44 | <3 | <5 | <2 | 2 | 8 | <5 | < |
| C88-3002 | 0.1 | 1.88 | 22 | 90 | <3 | 350 | 3 | 0.04 | 0.7 | 8 | 53 | 255 | 4.88 | 0.04 | 1.10 | 838 | 3 | 0.03 | 8 | 0.16 | 39 | <3 | <5 | <2 | 2 | 9 | <5 | < |
| C88-3003 | 0.1 | 2.22 | 9 | 40 | <3 | 631 | 3 | 0.12 | 1.1 | 15 | 44 | 251 | 4.07 | 0.06 | 1.35 | 1480 | 3 | 0.03 | 9 | 0.14 | 40 | <3 | <5 | <2 | 2 | 16 | <5 | < |
| C88-3004 | 0.1 | 0.68 | 78 | 110 | <3 | 54 | <3 | 0.05 | 1.1 | 6 | 26 | 432 | 6.15 | 0.05 | 0.32 | 292 | 7 | 0.03 | 6 | 0.23 | 37 | <3 | <5 | <2 | 2 | 11 | <5 | < |
| C88-3005 | 0.1 | 0.94 | 39 | 70 | <3 | 27 | <3 | 0.16 | 0.6 | 12 | 44 | 556 | 4.51 | 0.05 | 0.62 | 1558 | 3 | 0.03 | 8 | 0.19 | 41 | <3 | <5 | <2 | 2 | 9 | <5 | < |
| C88-3006 | 0.1 | 0.68 | 36 | <5 | <3 | 50 | <3 | 0.03 | 0.1 | 6 | 47 | 206 | 3.80 | 0.03 | 0.31 | 297 | 6 | 0.02 | 5 | 0.18 | 29 | <3 | <5 | <2 | 2 | 71 | <5 | < |
| C88-3007 | 0.1 | 0.56 | 32 | <5 | <3 | 18 | <3 | 0.11 | 0.7 | 15 | 36 | 506 | 4.77 | 0.04 | 0.36 | 346 | 4 | 0.02 | 11 | 0.15 | 37 | <3 | <5 | <2 | 3 | 7 | <5 | < |
| C88-3008 | 0.1 | 0.30 | 29 | 60 | <3 | 19 | 3 | 0.08 | 0.7 | 13 | 43 | 945 | 5.43 | 0.05 | 0.15 | 80 | 4 | 0.02 | 8 | 0.20 | 30 | <3 | <5 | <2 | 3 | 5 | <5 | < |
| C88-3009 | 0.1 | 0.36 | 20 | 145 | <3 | 17 | <3 | 0.21 | 1.2 | 14 | 46 | 958 | 5.41 | 0.07 | 0.24 | 551 | 4 | 0.03 | 10 | 0.18 | 30 | <3 | <5 | <2 | 3 | 6 | <5 | < |
| C88-3010 | 0.5 | 0.38 | 48 | 50 | <3 | 17 | <3 | 0.05 | 1.1 | 13 | 74 | 522 | 4.88 | 0.04 | 0.20 | 74 | 6 | 0.02 | 9 | 0.13 | 54 | <3 | <5 | <2 | 3 | 8 | <5 | < |
| C88-3011 | 0.1 | 0.23 | 21 | 30 | <3 | 17 | <3 | 0.02 | 0.6 | 12 | 39 | 265 | 4.39 | 0.03 | 0.09 | 21 | 5 | 0.02 | 7 | 0.14 | 40 | <3 | <5 | <2 | 2 | 12 | <5 | < |
| C88-3012 | 0.9 | 0.34 | 20 | 60 | <3 | 14 | <3 | 0.55 | 1.3 | 17 | 49 | 400 | 4.54 | 0.12 | 0.43 | 1778 | 9 | 0.03 | 8 | 0.14 | 53 | <3 | <5 | <2 | 2 | 14 | <5 | < |
| C88-3013 | 0.4 | 0.39 | 17 | 40 | <3 | 22 | 3 | 0.89 | 1.2 | 17 | 41 | 278 | 4.58 | 0.17 | 0.64 | 1668 | 7 | 0.03 | 9 | 0.15 | 45 | <3 | <5 | <2 | 3 | 19 | <5 | |
| C88-3014 | 0.1 | 0.29 | 27 | 40 | <3 | 21 | 3 | 1.11 | 1.3 | 16 | 43 | 308 | 4.73 | 0.19 | 0.81 | 3955 | 4 | 0.04 | 9 | 0.15 | 45 | <3 | <5 | <2 | 3 | 18 | <5 | |
| C88-3015 | 1.1 | 0.28 | 27 | 90 | <3 | 20 | <3 | 0.73 | 0.7 | 15 | 41 | 294 | 4.74 | 0.15 | 0.61 | 1672 | 6 | 0.03 | 8 | 0.17 | 37 | <3 | <5 | <2 | 3 | 13 | <5 | |
| C88-3016 | 2.2 | 0.53 | 27 | 120 | <3 | 16 | 4 | 0.24 | 1.2 | 15 | 47 | 478 | 5.04 | 0.09 | 0.42 | 738 | 5 | 0.03 | 9 | 0.17 | 50 | <3 | <5 | <2 | 3 | 10 | <5 | < |
| C88-3017 | 1.1 | 0.56 | 9 | 30 | <3 | 445 | <3 | 0.75 | 0.1 | 4 | 82 | 29 | 1.18 | 0.16 | 0.26 | 483 | 6 | 0.01 | 5 | 0.03 | 29 | <3 | <5 | <2 | <2 | 47 | <5 | < |
| C88-3018 | 0.9 | 0.38 | 11 | 10 | <3 | 189 | <3 | 0.04 | 0.1 | 3 | 74 | 88 | 1.54 | 0.05 | 0.10 | 85 | 4 | 0.01 | 5 | 0.05 | 29 | <3 | <5 | <2 | <2 | 6 | <5 | < |
| C88-3019 | 1.2 | 0.64 | 31 | 570 | <3 | 28 | <3 | 0.02 | 0.7 | 7 | 83 | 2419 | 4.08 | 0.03 | 0.32 | 180 | 10 | 0.03 | 6 | 0.11 | 54 | <3 | <5 | <2 | 2 | 5 | <5 | < |
| C88-3020 | 1.5 | 0.41 | 26 | 270 | <3 | 46 | <3 | 0.01 | 0.6 | 3 | 94 | 816 | 4.01 | 0.03 | 0.21 | 161 | 10 | 0.02 | 5 | 0.08 | 69 | <3 | <5 | <2 | 2 | 4 | <5 | < |
| C88-3021 | 0.9 | 2.82 | 93 | 60 | <3 | 36 | 9 | 0.17 | 1.7 | 14 | 23 | 98 | 6.85 | 0.08 | 2.13 | 1659 | 9 | 0.08 | 9 | 0.23 | 107 | <3 | <5 | <2 | 4 | 8 | <5 | < |
| C88-3022 | 1.8 | 1.52 | 26 | 130 | <3 | 40 | 4 | 0.19 | 1.5 | 14 | 56 | 1894 | 5.22 | 0.09 | 0.98 | 1472 | 11 | 0.05 | 7 | 0.20 | 55 | <3 | <5 | <2 | 4 | 4 | <5 | < |
| C88-3023 | 0.5 | 0.94 | 42 | 150 | <3 | 35 | 5 | 0.08 | 2.2 | 11 | 69 | 2575 | 6.44 | 0.07 | 0.55 | 411 | 15 | 0.05 | 18 | 0.32 | 131 | <3 | <5 | <2 | 5 | 20 | <5 | < |

VAN CHEM LAB
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: 880963 PA — WESTERN COM MINING — 

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88-3024 | 1.1 | 2.25 | 24 | 120 | <3 | 110 | 9 | 0.20 | 3.1 | 13 | 56 | 4180 | 5.10 | 0.08 | 1.37 | 442 | 2 | 0.02 | 10 | 0.20 | 48 | <3 | <5 | <2 | <2 | 26 | <5 | <3 | 146 |
| C88-3025 | 0.6 | 1.52 | 20 | 120 | <3 | 74 | <3 | 0.24 | 3.1 | 12 | 42 | 3264 | 2.91 | 0.07 | 1.31 | 1151 | <1 | 0.02 | 7 | 0.17 | 48 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 297 |
| C88-3026 | 0.1 | 0.88 | 18 | 10 | <3 | 428 | <3 | 0.76 | 1.3 | 8 | 89 | 98 | 2.41 | 0.17 | 0.38 | 1116 | <1 | 0.02 | 5 | 0.06 | 27 | <3 | <5 | <2 | <2 | 37 | <5 | <3 | 182 |
| C88-3027 | 0.2 | 1.67 | 17 | 20 | <3 | 131 | <3 | 0.78 | 2.2 | 11 | 60 | 399 | 4.37 | 0.17 | 0.86 | 1208 | <1 | 0.03 | 5 | 0.16 | 35 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 298 |
| C88-3028 | 2.1 | 0.69 | 103 | 230 | <3 | 16 | <3 | 0.36 | 2.7 | 15 | 52 | 6014 | 4.24 | 0.11 | 0.20 | 514 | 3 | 0.02 | 8 | 0.20 | 53 | <3 | <5 | <2 | <2 | 17 | <5 | <3 | 185 |
| C88-3029 | 0.2 | 0.56 | 11 | 5 | <3 | 235 | <3 | 1.18 | 1.6 | 9 | 56 | 262 | 3.06 | 0.22 | 0.46 | 812 | <1 | 0.02 | 4 | 0.15 | 29 | <3 | <5 | <2 | <2 | 36 | <5 | <3 | 135 |
| C88-3030 | 0.1 | 0.83 | 14 | 30 | <3 | 355 | <3 | 1.14 | 1.6 | 10 | 55 | 152 | 3.33 | 0.22 | 0.48 | 906 | <1 | 0.02 | 4 | 0.11 | 36 | <3 | <5 | <2 | <2 | 39 | <5 | <3 | 193 |
| C88-3031 | 2.1 | 0.48 | 25 | 160 | <3 | 15 | <3 | 0.96 | 4.5 | 19 | 89 | 4788 | 4.55 | 0.19 | 0.58 | 1336 | 2 | 0.02 | 8 | 0.16 | 34 | <3 | <5 | <2 | <2 | 17 | <5 | <3 | 202 |
| C88-3032 | 1.2 | 0.40 | 34 | 70 | <3 | 12 | <3 | 0.53 | 2.1 | 14 | 49 | 3178 | 4.30 | 0.13 | 0.43 | 562 | 11 | 0.02 | 6 | 0.16 | 27 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 84 |
| C88-3033 | 1.2 | 0.86 | 22 | 200 | <3 | 12 | 3 | 0.30 | 2.5 | 21 | 85 | 3015 | 4.99 | 0.08 | 0.60 | 1536 | 1 | 0.02 | 9 | 0.17 | 34 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 151 |
| C88-3034 | 1.5 | 1.25 | 21 | 210 | <3 | 17 | <3 | 0.25 | 2.1 | 18 | 58 | 4321 | 3.97 | 0.07 | 1.06 | 1021 | 1 | 0.02 | 9 | 0.16 | 40 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 124 |
| C88-3035 | 2.2 | 0.28 | 22 | 100 | <3 | 12 | <3 | 0.58 | 2.1 | 16 | 89 | 4141 | 4.34 | 0.14 | 0.14 | 813 | <1 | 0.02 | 6 | 0.17 | 34 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 88 |
| C88-3036 | 1.7 | 0.32 | 57 | 410 | <3 | 8 | 6 | 0.26 | 4.1 | 17 | 76 | 4113 | 7.65 | 0.08 | 0.07 | 487 | <1 | 0.03 | 7 | 0.14 | 30 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 85 |
| C88-3037 | 6.3 | 0.56 | 209 | 470 | <3 | 11 | <3 | 0.30 | 2.5 | 14 | 89 | 9563 | 4.62 | 0.08 | 0.27 | 570 | <1 | 0.02 | 8 | 0.15 | 46 | <3 | <5 | 114 | <2 | 8 | <5 | <3 | 220 |
| C88-3038 | 3.7 | 0.27 | 87 | 1020 | <3 | 9 | <3 | 0.40 | 2.7 | 21 | 93 | 7560 | 5.49 | 0.11 | 0.17 | 1542 | <1 | 0.03 | 10 | 0.13 | 96 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 199 |
| C88-3039 | 2.2 | 0.38 | 28 | 445 | <3 | 12 | <3 | 0.50 | 2.5 | 15 | 96 | 10333 | 3.79 | 0.12 | 0.30 | 811 | 10 | 0.02 | 7 | 0.14 | 27 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 143 |
| C88-3040 | 1.7 | 0.48 | 19 | 150 | <3 | 8 | <3 | 1.60 | 2.7 | 18 | 68 | 2557 | 5.49 | 0.28 | 0.59 | 565 | 5 | 0.02 | 7 | 0.14 | 30 | <3 | <5 | <2 | <2 | 29 | <5 | <3 | 27 |
| C88-3041 | 1.1 | 0.29 | 18 | 310 | <3 | 13 | <3 | 1.46 | 2.2 | 15 | 31 | 1374 | 3.09 | 0.25 | 0.59 | 502 | 5 | 0.02 | 5 | 0.17 | 29 | <3 | <5 | <2 | <2 | 27 | <5 | <3 | 167 |
| C88-3042 | 1.7 | 0.24 | 72 | 220 | <3 | 9 | <3 | 1.29 | 2.2 | 14 | 46 | 214 | 4.22 | 0.24 | 0.65 | 1313 | <1 | 0.02 | 9 | 0.16 | 63 | <3 | <5 | <2 | <2 | 25 | <5 | <3 | 196 |
| C88-3043 | 3.7 | 0.56 | 157 | 140 | <3 | 8 | <3 | 2.47 | 2.1 | 10 | 53 | 1079 | 4.16 | 0.34 | 1.18 | 2219 | 9 | 0.02 | 7 | 0.13 | 88 | <3 | <5 | <2 | <2 | 48 | <5 | <3 | 174 |
| C88-3044 | 1.2 | 0.72 | 34 | 50 | <3 | 14 | <3 | 2.70 | 1.5 | 5 | 77 | 1208 | 2.49 | 0.35 | 1.13 | 2086 | 4 | 0.01 | 11 | 0.10 | 26 | <3 | <5 | <2 | <2 | 59 | <5 | 7 | 63 |
| C88-3045 | 7.3 | 0.48 | 114 | 260 | <3 | 10 | <3 | 0.78 | 2.2 | 10 | 103 | 3749 | 3.29 | 0.16 | 0.40 | 748 | 3 | 0.02 | 7 | 0.11 | 27 | <3 | <5 | 6 | <2 | 23 | <5 | <3 | 109 |
| C88-3046 | 7.1 | 0.32 | 23 | 440 | <3 | 11 | <3 | 0.22 | 1.5 | 12 | 95 | 7267 | 3.29 | 0.08 | 0.15 | 321 | <1 | 0.01 | 8 | 0.13 | 40 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 78 |
| C88-3047 | 11.1 | 0.40 | 58 | 640 | <3 | 8 | 6 | 0.40 | 4.3 | 14 | 82 | 7980 | 6.41 | 0.11 | 0.22 | 723 | 2 | 0.04 | 8 | 0.13 | 131 | <3 | <5 | 6 | <2 | 18 | <5 | <3 | 444 |
| C88-3048 | 7.1 | 0.60 | 23 | 530 | <3 | 9 | <3 | 0.25 | 3.2 | 20 | 93 | 8067 | 4.25 | 0.08 | 0.22 | 515 | 8 | 0.02 | 9 | 0.16 | 59 | <3 | <5 | <2 | <2 | 19 | <5 | <3 | 227 |
| C88-3049 | 8.3 | 0.55 | 30 | 550 | <3 | 9 | <3 | 0.20 | 1.6 | 16 | 100 | 9673 | 3.59 | 0.07 | 0.07 | 64 | 7 | 0.01 | 8 | 0.15 | 39 | <3 | <5 | <2 | <2 | 54 | <5 | <3 | 42 |
| C88-3050 | 9.6 | 0.41 | 22 | 410 | <3 | 11 | <3 | 0.22 | 1.5 | 14 | 57 | 9356 | 3.17 | 0.08 | 0.05 | 74 | <1 | 0.01 | 8 | 0.17 | 49 | <3 | <5 | <2 | <2 | 36 | <5 | <3 | 43 |
| C88-3051 | 8.6 | 0.40 | 22 | 450 | <3 | 11 | <3 | 0.17 | 1.5 | 14 | 70 | 9896 | 2.72 | 0.06 | 0.03 | 33 | 54 | 0.01 | 7 | 0.14 | 46 | <3 | <5 | <2 | <2 | 39 | <5 | <3 | 34 |
| C88-3052 | 5.5 | 0.40 | 20 | 385 | <3 | 12 | <3 | 0.25 | 1.3 | 22 | 30 | 7645 | 3.11 | 0.07 | 0.04 | 27 | 26 | 0.01 | 6 | 0.17 | 27 | <3 | <5 | <2 | <2 | 74 | <5 | <3 | 21 |
| C88-3053 | 4.1 | 0.71 | 22 | 200 | <3 | 14 | <3 | 0.27 | 1.5 | 14 | 40 | 5402 | 3.13 | 0.08 | 0.59 | 168 | 11 | 0.01 | 6 | 0.17 | 29 | <3 | <5 | <2 | <2 | 32 | <5 | <3 | 61 |
| C88-3054 | 2.9 | 0.81 | 23 | 40 | <3 | 8 | 3 | 0.25 | 2.2 | 13 | 52 | 5844 | 5.32 | 0.08 | 0.38 | 119 | 5 | 0.02 | 9 | 0.15 | 30 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 35 |
| C88-3055 | 1.7 | 0.98 | 23 | 180 | <3 | 14 | 4 | 0.29 | 1.7 | 15 | 28 | 4992 | 4.00 | 0.08 | 0.93 | 259 | 12 | 0.02 | 7 | 0.19 | 26 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 62 |
| C88-3056 | 1.2 | 0.71 | 19 | 200 | <3 | 10 | <3 | 0.25 | 1.6 | 15 | 38 | 4924 | 3.90 | 0.08 | 0.43 | 82 | 6 | 0.01 | 6 | 0.19 | 66 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 37 |
| C88-3057 | 1.1 | 1.03 | 23 | 80 | <3 | 10 | <3 | 0.26 | 1.7 | 16 | 39 | 5767 | 4.14 | 0.08 | 0.61 | 115 | <1 | 0.02 | 6 | 0.20 | 32 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 52 |
| C88-3058 | 2.1 | 0.81 | 29 | 210 | <3 | 8 | 4 | 0.22 | 2.7 | 17 | 60 | 7915 | 5.47 | 0.08 | 0.35 | 253 | 7 | 0.02 | 14 | 0.17 | 90 | <3 | <5 | <2 | <2 | 10 | <5 | 23 | 132 |
| C88-3059 | 2.7 | 0.29 | 43 | 380 | <3 | 6 | <3 | 0.25 | 3.1 | 15 | 34 | 4875 | 6.16 | 0.08 | 0.12 | 112 | 18 | 0.02 | 6 | 0.17 | 82 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 63 |
| C88-3060 | 1.2 | 0.44 | 15 | 160 | <3 | 8 | <3 | 0.34 | 1.8 | 17 | 54 | 5707 | 3.75 | 0.08 | 0.32 | 185 | 30 | 0.01 | 5 | 0.17 | 22 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 51 |
| C88-3061 | 1.1 | 0.85 | 19 | 90 | <3 | 12 | <3 | 0.22 | 1.7 | 19 | 37 | 3921 | 3.08 | 0.07 | 0.64 | 236 | 18 | 0.01 | 5 | 0.19 | 24 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 95 |
| C88-3062 | 1.2 | 0.72 | 18 | 170 | <3 | 11 | <3 | 0.20 | 2.1 | 19 | 28 | 4345 | 3.15 | 0.08 | 0.56 | 200 | 46 | 0.01 | 6 | 0.17 | 28 | <3 | <5 | <2 | <2 | 17 | <5 | <3 | 79 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

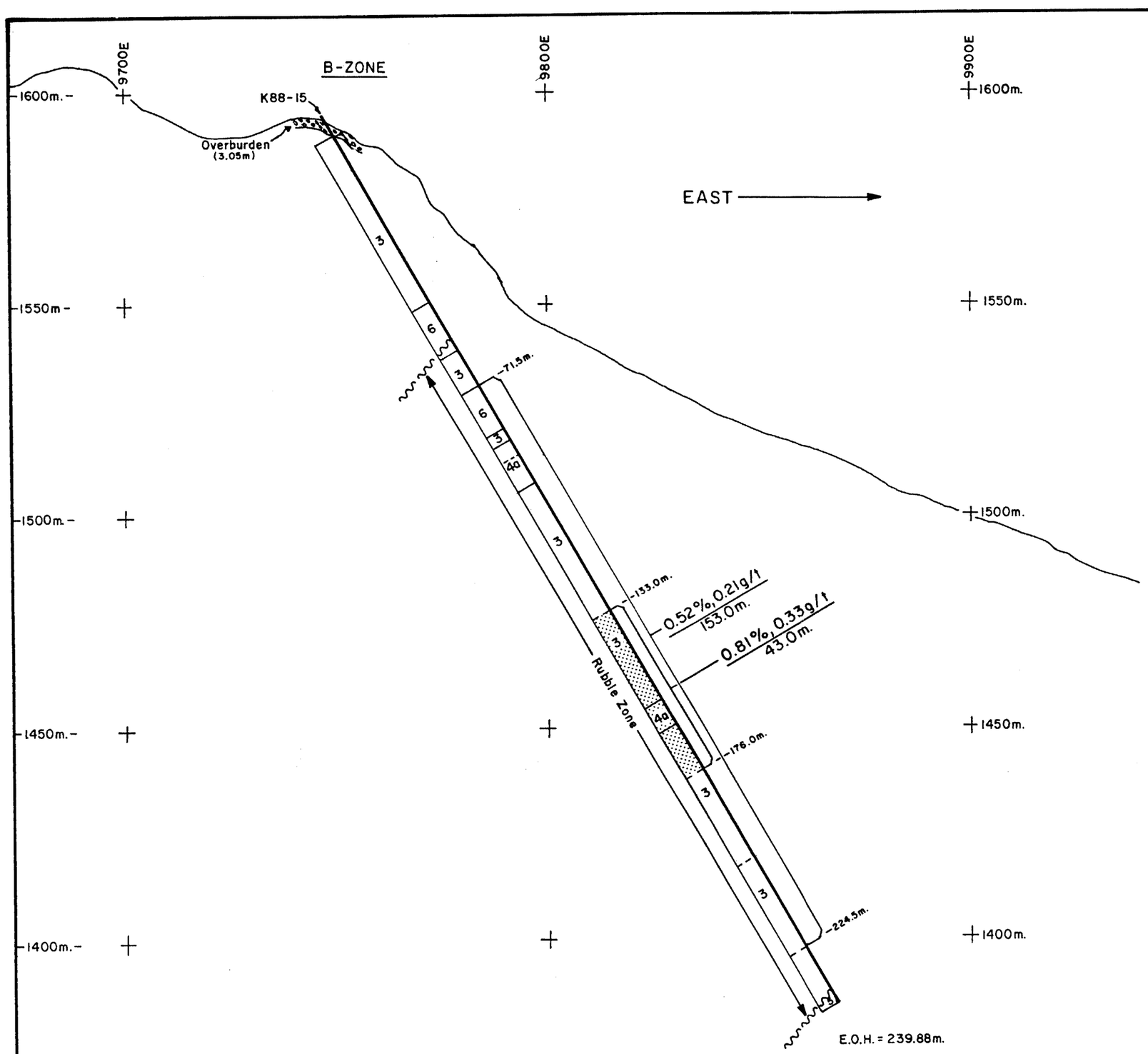
< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

REPORT #: 880953 PA

WESTERN CDN MINING



| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88-3063 | 1.7 | 0.71 | 22 | 250 | <3 | 15 | <3 | 0.25 | 2.7 | 24 | 43 | 7755 | 3.03 | 0.07 | 0.40 | 135 | 33 | 0.01 | 8 | 0.22 | 34 | <3 | <5 | <2 | <2 | 36 | <5 | <3 | 101 |
| C88-3064 | 1.1 | 0.62 | 35 | 80 | <3 | 14 | <3 | 0.21 | 2.4 | 17 | 42 | 4399 | 3.58 | 0.06 | 0.36 | 137 | 48 | 0.02 | 7 | 0.19 | 46 | <3 | <5 | <2 | <2 | 55 | <5 | <3 | 200 |
| C88-3065 | 0.5 | 0.91 | 20 | 30 | <3 | 16 | <3 | 0.21 | 1.6 | 16 | 45 | 3554 | 3.19 | 0.07 | 0.67 | 236 | 37 | 0.01 | 6 | 0.19 | 23 | <3 | <5 | <2 | <2 | 54 | <5 | <3 | 91 |
| C88-3066 | 1.1 | 0.77 | 26 | 130 | <3 | 15 | <3 | 0.24 | 2.3 | 21 | 41 | 5104 | 4.47 | 0.08 | 0.44 | 145 | 23 | 0.02 | 8 | 0.22 | 29 | <3 | <5 | <2 | <2 | 27 | <5 | <3 | 71 |
| C88-3067 | 1.2 | 0.80 | 24 | 230 | <3 | 24 | <3 | 0.27 | 1.5 | 17 | 18 | 5617 | 3.12 | 0.09 | 0.59 | 182 | 12 | 0.01 | 7 | 0.21 | 23 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 60 |
| C88-3068 | 1.5 | 3.41 | 108 | 20 | <3 | 93 | 24 | 0.74 | 3.7 | 41 | 30 | 132 | 8.65 | 0.17 | 2.19 | 1664 | <1 | 0.04 | 13 | 0.20 | 49 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 326 |
| C88-3069 | 1.7 | 1.47 | 39 | 200 | <3 | 20 | <3 | 0.25 | 3.8 | 21 | 50 | 7258 | 3.79 | 0.08 | 0.99 | 378 | 19 | 0.02 | 7 | 0.18 | 32 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 149 |
| C88-3070 | 1.1 | 1.21 | 25 | 160 | <3 | 17 | <3 | 0.25 | 2.1 | 17 | 73 | 3868 | 3.73 | 0.08 | 0.91 | 376 | 19 | 0.02 | 7 | 0.20 | 29 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 104 |
| C88-3071 | 1.2 | 0.59 | 21 | 30 | <3 | 13 | <3 | 0.22 | 1.7 | 24 | 80 | 3684 | 3.64 | 0.07 | 0.21 | 106 | 96 | 0.01 | 6 | 0.17 | 31 | <3 | <5 | <2 | <2 | 31 | <5 | <3 | 35 |
| C88-3072 | 1.5 | 0.87 | 26 | 65 | <3 | 15 | <3 | 0.26 | 3.1 | 16 | 59 | 2758 | 4.75 | 0.09 | 0.74 | 328 | 22 | 0.02 | 7 | 0.20 | 56 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 242 |
| C88-3073 | 1.1 | 0.97 | 23 | 60 | <3 | 21 | <3 | 0.24 | 1.7 | 17 | 66 | 2965 | 3.45 | 0.07 | 0.84 | 310 | 23 | 0.02 | 5 | 0.19 | 31 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 103 |
| C88-3074 | 0.5 | 0.74 | 21 | 80 | <3 | 24 | <3 | 0.22 | 1.5 | 14 | 57 | 3147 | 2.94 | 0.07 | 0.53 | 199 | 23 | 0.01 | 7 | 0.19 | 23 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 62 |
| C88-3075 | 1.2 | 0.80 | 20 | 40 | <3 | 17 | <3 | 0.22 | 1.9 | 14 | 59 | 3219 | 3.88 | 0.07 | 0.64 | 192 | 3 | 0.02 | 9 | 0.18 | 25 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 58 |
| C88-3076 | 1.1 | 0.72 | 14 | 30 | <3 | 18 | <3 | 2.23 | 2.1 | 22 | 66 | 2381 | 4.85 | 0.31 | 0.78 | 165 | 9 | 0.02 | 11 | 0.19 | 41 | <3 | <5 | <2 | <2 | 263 | <5 | <3 | 60 |
| C88-3077 | 1.5 | 0.61 | 13 | 40 | <3 | 20 | <3 | 2.94 | 1.8 | 19 | 55 | 3941 | 3.79 | 0.36 | 0.55 | 146 | 15 | 0.02 | 8 | 0.18 | 25 | <3 | <5 | <2 | <2 | 330 | <5 | <3 | 49 |
| C88-3078 | 1.2 | 1.57 | 27 | 30 | <3 | 26 | 6 | 0.41 | 2.2 | 29 | 67 | 3037 | 4.35 | 0.10 | 1.70 | 444 | 6 | 0.02 | 14 | 0.26 | 30 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 95 |
| C88-3079 | 0.7 | 0.98 | 23 | 20 | <3 | 17 | <3 | 0.29 | 1.8 | 17 | 51 | 1130 | 4.35 | 0.09 | 1.03 | 275 | <1 | 0.02 | 9 | 0.19 | 26 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 82 |
| C88-3080 | 0.7 | 0.80 | 50 | 20 | <3 | 15 | <3 | 0.30 | 2.8 | 15 | 60 | 1053 | 4.77 | 0.09 | 0.92 | 219 | <1 | 0.02 | 7 | 0.20 | 56 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 128 |
| C88-3081 | 1.7 | 1.20 | 39 | 80 | <3 | 12 | 13 | 0.35 | 4.1 | 28 | 80 | 2740 | 6.52 | 0.10 | 1.48 | 395 | 18 | 0.03 | 38 | 0.22 | 40 | <3 | <5 | <2 | <2 | 9 | <5 | <3 | 218 |
| C88-3082 | 26.7 | 0.77 | >1000 | 1530 | <3 | 13 | 11 | 0.34 | 6.9 | 26 | 84 | 7899 | 6.96 | 0.11 | 0.57 | 586 | 17 | 0.08 | 42 | 0.18 | 34 | <3 | <5 | 644 | <2 | 12 | <5 | <3 | 1531 |
| C88-3083 | 0.6 | 1.39 | 151 | 10 | <3 | 26 | <3 | 3.25 | 0.9 | 12 | 53 | 328 | 2.93 | 0.37 | 1.15 | 1725 | <1 | 0.02 | 19 | 0.14 | 33 | <3 | <5 | <2 | <2 | 69 | <5 | <3 | 111 |
| C88-3084 | 0.5 | 1.16 | 174 | 30 | <3 | 37 | <3 | 1.97 | 0.6 | 10 | 80 | 200 | 2.52 | 0.28 | 0.81 | 1066 | <1 | 0.01 | 10 | 0.10 | 31 | <3 | <5 | <2 | <2 | 46 | <5 | <3 | 65 |




## LEGEND

Fault

0.13%, 1.13g/t / 10.3m. — %Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Intervals defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE - fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a) / MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST – foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) – interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE – interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

1:1000

SCALE 0 10 20 30 40 Metres

# SULPHURETS GOLD CORPORATION

1989 KERR PROJECT

D.D.H. K88-15

SECTION

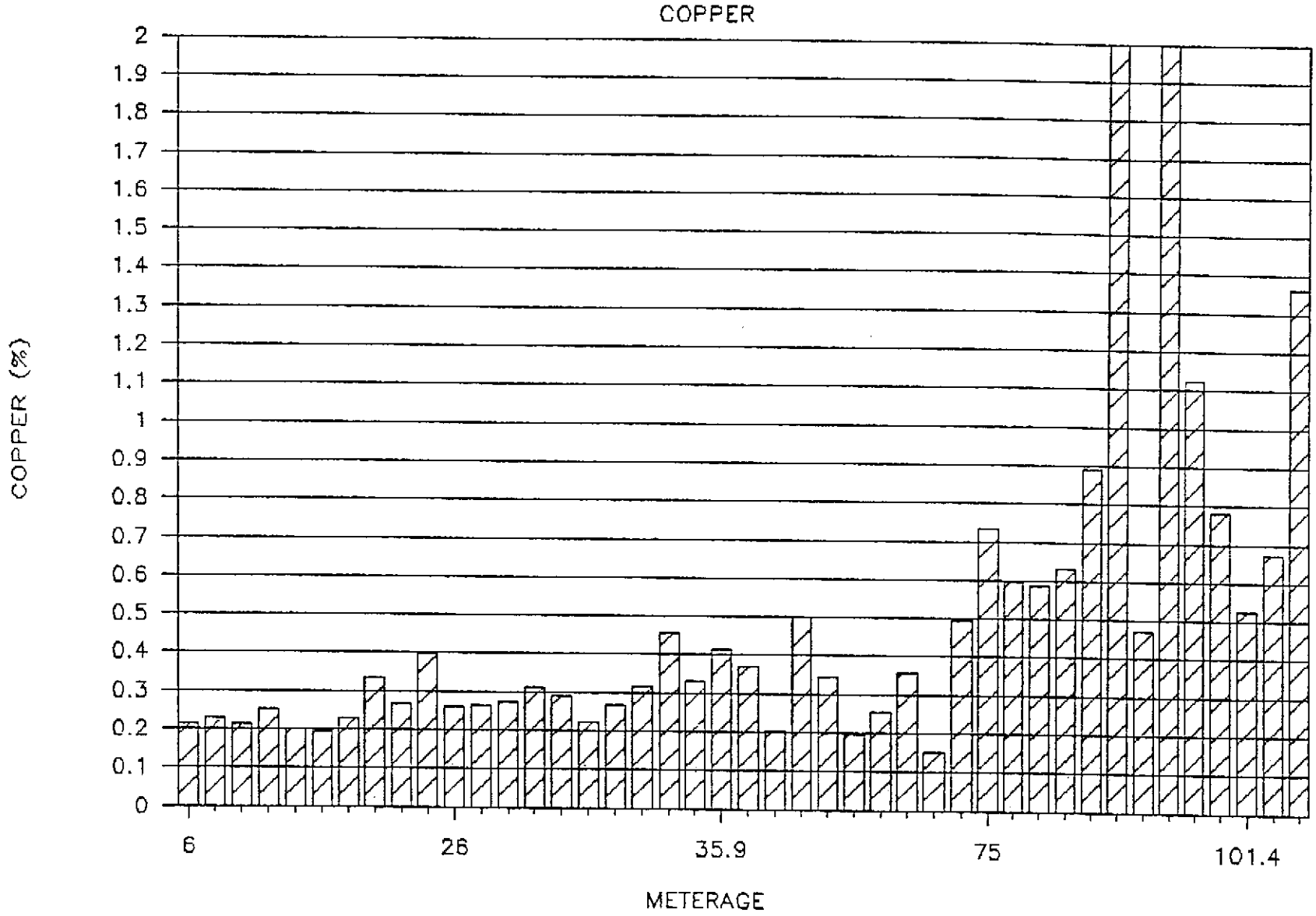
COLLAR:- 9415.0N, 9748.1E

BEARING: 090° DIP: -60°

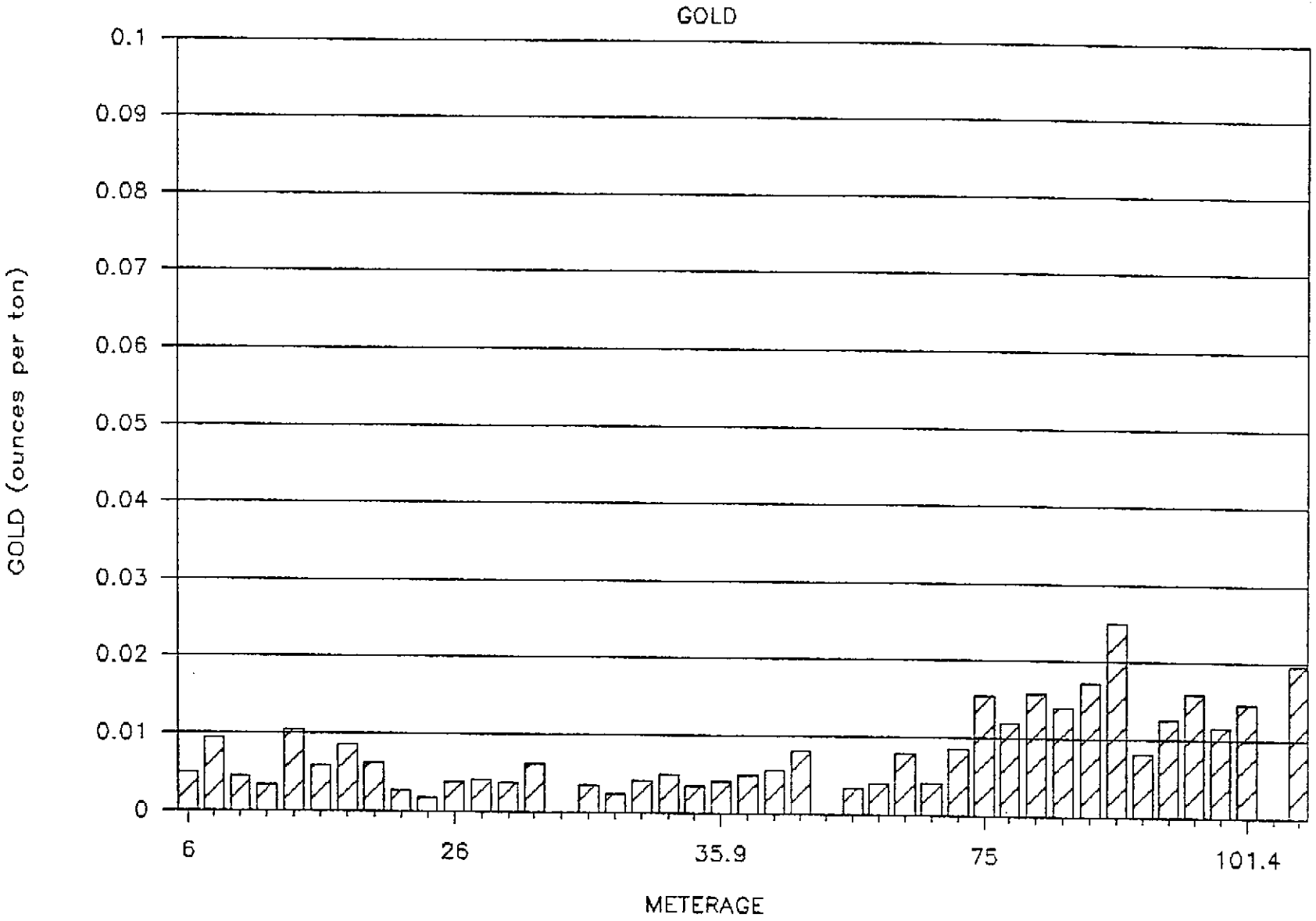
ELEVATION: 1594.2m.

REPORT:1065 FIGURE No.

# K88-16


COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
6
26
35.9
75
101.4
METERAGE

# K88-16


GOLD
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
GOLD (ounces per ton)
6
26
35.9
75
101.4
METERAGE

KERR PROJECT D.D.HOLE K-88-16

LOCATION P-ZONE - BOTTOM OF NORTH GLACIER
COLLAR LAT. 10387.4 NORTH
DATE STARTED JULY 30, 1988
LONG. 9616.9 EAST
DATE COMPLETED JULY 31, 1988
ELEVATION 1412.3 m
CORE RECOVERY 43.59%
AZIMUTH 125 DIP -60 deg
DRILLED BY FALCON DRILLING LTD.
LENGTH 106.07 m
LOGGED BY S. CASSELMAN
HOR. PROJ. 53.04 m
VERT. PROJ. 91.86 m
OBJECTIVE NORTH EXTENSION OF B-ZONE FAULT / MINERALIZATION
DIP TEST DEPTH _____m DIP_____deg
DEPTH _____m DIP_____deg

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 3.05 | 3.05 | OVERBURDEN |
| 3.05 | 35.90 | 32.85 | SERICITE-QUARTZ-PYRITE SCHIST<br>- overall light to medium grey to blue-grey colour in sections<br>- very competent, good recovery<br>- weak foliation at 65 deg to C.A.<br>- intensely sericitized with 1 - 3% quartz veins - generally pitted and contains pyrite<br>- 15 to 25% pyrite as fine disseminations, blebs, stringers, and veins up to 20 cm wide<br>- associated with pyrite are blue halos and patches believed to be chalcocite (1 to 2%)<br>- predominant fracture orientation at 65 deg parallel to foliation<br>- protolith probably dacite tuff or dacite crystal tuff |
| 35.90 | 87.78 | 51.88 | FAULT ZONE / FRACTURED SERICITE SCHIST<br>- overall whitish to light grey colour-mostly sericite - intense sericitization<br>- intensely fractured, average piece 2 to 3 cm long<br>- fractures at roughly 70 deg to C.A.<br>- 1 to 3% chalcocite, possibly occurring as a coating on pyrite or chalcopyrite<br>- sulphides occur as disseminations and 1 mm to 1 cm veins with quartz<br>- from 35.9 to 87.78 m, 51.88 m of intensely fractured core<br>- also 89.25 to 101.4 m, 12 m of intensely fractured core<br>- 35.9 to 87.18 and 89.25 to 93.4 are composed of pyrite-rich sericite schist<br>- 87.78 to 89.25 and 93.4 to 101.4 are |

KERR PROJECT D.D.HOLE K-88-16

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | silicified sulphide-rich (pyrite, chalcopyrite, chalcocite) zones |
| 87.78 | 89.25 | 1.47 | QUARTZ-PYRITE-CHALCOPYRITE STOCKWORK<br>- competent, hard, intensely silicified with 20 to 25% pyrite, 2 to 5% chalcopyrite and 3 to 5% chalcocite<br>- good recovery, average about 15 cm long sections of core<br>- 5% bull white quartz veins<br>- overall steely blue-grey colour - quite distinctive - has similarities to the silicified (pyrite, chalcopyrite, chalcocite) sections in K-88-11 and K-88-14<br>- pyrite occurs as fine, pervasive disseminations and in irregular stringers and blebs<br>- chalcopyrite occurs as wisps, blebs and masses<br>- chalcocite is pervasive, and especially associated with chalcopyrite |
| 89.25 | 93.40 | 4.15 | FAULT ZONE / SERICITE SCHIST<br>- average piece 1 to 2 cm long<br>- mainly sericite (70%)<br>- similar to section 35.9 to 87.78 m |
| 93.40 | 106.07 | 12.67 | BRECCIATED QUARTZ-PYRITE-CHALCOPYRITE STOCKWORK<br>- as in section 87.78 to 89.25 - but brecciated<br>- average particle size 3-5 cm long<br>- bornite on chalcopyrite and chalcocite mineralization at the end of hole<br><br>* Hole shut down because of stuck rods. Lost 160 feet of rods at the end of the hole, mineralization continues |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 11:43:42 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8816 | 10387.4 | 9616.9 | 1412.4 | 125 | 60 | 106.1 | P-Zone | #HOL |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 3.05 | | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 3.05 | 6 | 2.95 | 34 | SRCT SCHT | | F.MG | 5 | 3 | 65 | 1 | 2 | | | | | | 90 | 25 | .1 | | .5 | | | |
| 6 | 9 | 3 | 39 | SRCT SCHT | | F.MG | 5 | 5 | 65 | 1 | 2 | | | | | | 90 | 22 | .1 | | .5 | | | |
| 9 | 12 | 3 | 40 | SRCT SCHT | | F.MG | 5 | 5 | 65 | 1 | 1 | | | | | | 90 | 20 | | | .3 | | | |
| 12 | 15 | 3 | 37 | SRCT SCHT | | F.MG | 3 | 3 | 70 | 2 | 2 | | | | | | 90 | 20 | | | 1 | | | |
| 15 | 18 | 3 | 37 | SRCT SCHT | | F.MG | 2 | 5 | 70 | 1 | 5 | | | | | | 90 | 20 | .1 | | 1 | | | |
| 18 | 21 | 3 | 18 | SRCT SCHT | | F.MG | 2 | 1 | 70 | 2 | 2 | | | | | | 90 | 22 | | | .5 | | | |
| 21 | 22 | 1 | 36 | SRCT SCHT | | F.MG | 5 | 5 | 55 | | 2 | | | | | | 95 | 30 | .1 | | 1 | | | |
| 22 | 23 | 1 | 36 | SRCT SCHT | | F.MG | 5 | 3 | 60 | 1 | 3 | | | | | | 95 | 23 | | | .5 | | | |
| 23 | 24 | 1 | 34 | SRCT SCHT | | F.MG | 3 | 5 | 65 | 1 | 3 | | | | | | 95 | 20 | .5 | | 1 | | | |
| 24 | 25 | 1 | 32 | SRCT SCHT | | F.MG | 2 | 3 | 70 | 1 | 2 | | | | | | 95 | 18 | .1 | | .5 | | | |
| 25 | 26 | 1 | 34 | SRCT SCHT | | F.MG | 8 | 10 | 50 | 1 | 2 | | | | | | 95 | 25 | .3 | | .5 | | | |
| 26 | 27 | 1 | 33 | SRCT SCHT | | F.MG | 5 | 10 | 55 | 1 | 1 | | | | | | 95 | 25 | .3 | | .5 | | | |
| 27 | 28 | 1 | 36 | SRCT SCHT | | F.MG | 3 | 5 | 60 | 1 | 1 | | | | | | 95 | 23 | .1 | | .5 | | | |
| 28 | 29 | 1 | 36 | SRCT SCHT | | F.MG | 3 | 10 | 50 | 1 | 3 | | | | | | 95 | 30 | .1 | | .5 | | | |
| 29 | 30 | 1 | 31 | SRCT SCHT | | F.MG | 2 | 3 | 60 | 1 | 5 | | | | | | 95 | 18 | .1 | | .2 | | | |
| 30 | 31 | 1 | 34 | SRCT SCHT | | F.MG | 2 | 3 | 60 | 1 | 5 | | | | | | 95 | 18 | .1 | | .2 | | | |
| 31 | 32 | 1 | 32 | SRCT SCHT | | F.MG | 2 | 3 | 70 | 1 | 2 | | | | | | 100 | 18 | | | .1 | | | |
| 32 | 33 | 1 | 34 | SRCT SCHT | | F.MG | 1 | 3 | 70 | 1 | 1 | | | | | | 100 | 15 | | | .1 | | | |
| 33 | 34 | 1 | 33 | SRCT SCHT | | F.MG | 1 | 1 | 70 | 1 | 2 | | | | | | 100 | 15 | | | .1 | | | |
| 34 | 35 | 1 | 32 | SRCT SCHT | | F.MG | | 1 | 80 | | 1 | | | | | | 100 | 12 | | | .1 | | | |
| 35 | 35.9 | .9 | 30 | SRCT SCHT | | F.MG | 2 | 8 | 60 | | 2 | | | | | | 100 | 25 | .1 | | .3 | | | |
| 35.9 | 39 | 3.1 | 10 | FAULT SRCT SCHT | | FG | | 5 | 65 | 2 | 1 | | | | | | 100 | 20 | .3 | | 3 | | | |
| 39 | 42 | 3 | 24 | FAULT SRCT SCHT | | FG | | 3 | 70 | 5 | 1 | | | | | | 100 | 18 | .1 | | 2 | | | |
| 42 | 45 | 3 | 24 | FAULT SRCT SCHT | | FG | 2 | 2 | 65 | 3 | 2 | | | | | | 100 | 20 | .1 | | 1 | | | |
| 45 | 48 | 3 | 19 | FAULT SRCT SCHT | | FG | | 1 | 80 | 1 | 3 | | | | | | 100 | 15 | | | 2 | | | |
| 48 | 54 | 6 | 19 | FAULT SRCT SCHT | | FG | | | 80 | 3 | 2 | | | | | | 100 | 10 | | | 1 | | | |
| 54 | 57 | 3 | 23 | FAULT SRCT SCHT | | FG | 3 | 1 | 75 | 1 | 5 | | | | | | 100 | 12 | | | 2 | | | |
| 57 | 60 | 3 | 23 | FAULT SRCT SCHT | | FG | 5 | 1 | 70 | | 5 | | | | | | 100 | 15 | | | 3 | | | |
| 60 | 66 | 6 | 23 | FAULT SRCT SCHT | | FG | 4 | 1 | 70 | | 5 | | | | | | 100 | 18 | | | 2 | | | |
| 66 | 72 | 6 | 22 | FAULT SRCT SCHT | | FG | 5 | 1 | 70 | | 5 | | | | | | 100 | 15 | .1 | | 2 | | | |
| 72 | 75 | 3 | 23 | FAULT SRCT SCHT | | FG | 5 | 5 | 65 | | 3 | | | | | | 100 | 18 | .1 | | 2 | | | |
| 75 | 78 | 3 | 22 | FAULT SRCT SCHT | | FG | 3 | 2 | 65 | 1 | 5 | | | | | | 100 | 20 | | | 3 | | | |
| 78 | 81 | 3 | 20 | FAULT SRCT SCHT | | FG | 2 | 2 | 60 | 2 | 5 | | | | | | 100 | 20 | | | 2 | | | |
| 81 | 84 | 3 | 8 | FAULT SRCT SCHT | | FG | 3 | 3 | 60 | 2 | 5 | | | | | | 100 | 23 | | | 3 | | | |
| 84 | 87.78 | 3.78 | 25 | FAULT SRCT SCHT | | FG | 5 | 3 | 50 | 3 | 8 | | | | | | 100 | 25 | | | 3 | | | |
| 87.78 | 89.25 | 1.47 | 43 | SILC STWK | | FG | 25 | 15 | 25 | | 5 | | | | | | 100 | 20 | 5 | | 3 | | | |
| 89.25 | 93.4 | 4.15 | 18 | FAULT SRCT SCHT | | FG | 3 | | 75 | 2 | 2 | | | | | | 100 | 15 | | | 1 | | | |
| 93.4 | 95.4 | 2 | 23 | BREC SILC STWK | | FG | 40 | 5 | 15 | | 2 | | | | | | 100 | 30 | 3 | | 5 | | | |
| 95.4 | 97.4 | 2 | 25 | BREC SILC STWK | | FG | 40 | 5 | 25 | | 2 | | | | | | 100 | 25 | 1 | | 2 | | | |
| 97.4 | 99.4 | 2 | 23 | BREC SILC STWK | | FG | 35 | 5 | 30 | | 2 | | | | | | 100 | 20 | | | 2 | | | |
| 99.4 | 101.4 | 2 | 25 | BREC SILC STWK | | FG | 20 | 3 | 55 | | 3 | | | | | | 100 | 18 | | | 1 | | | |
| 101.4 | 103.4 | 2 | 24 | BREC SILC STWK | | FG | 8 | 3 | 55 | 2 | 5 | | | | | | 100 | 12 | | | 2 | | | |
| 103.4 | 106.1 | 2.67 | 32 | BREC SILC STWK | | FG | 20 | 5 | 45 | | 5 | | | | | | 100 | 20 | 1 | | 3 | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 09:23:40 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8816 | 10387.4 | 9616.9 | 1412.4 | 125 | 60 | 106.1 | P-Zone | | |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 3.05 | | | | | | | | | | | | | | |
| 3.05 | 6 | 3085 | 2.95 | 2.95 | 170 | | 1.1 | | 2127 | 47 | 4.88 | 55 | 28 | | |
| 6 | 9 | 3086 | 3 | 2.85 | 320 | | 0.5 | | 2297 | 32 | 4.87 | 21 | 39 | | |
| 9 | 12 | 3087 | 3 | 2.86 | 150 | | 0.5 | | 2111 | 33 | 4.59 | 23 | 33 | | |
| 12 | 15 | 3088 | 3 | 2.84 | 110 | | 0.3 | | 2489 | 27 | 4.67 | 38 | 23 | | |
| 15 | 18 | 3089 | 3 | 3 | 360 | | 0.5 | | 1995 | 52 | 4.45 | 28 | 68 | | |
| 18 | 21 | 3090 | 3 | 2.86 | 200 | | 0.7 | | 1921 | 69 | 4.10 | 24 | 34 | | |
| 21 | 22 | 3091 | 1 | .97 | 290 | | 0.6 | | 2294 | 96 | 6.90 | 50 | 42 | | |
| 22 | 23 | 3092 | 1 | .96 | 210 | | 0.5 | | 3341 | 106 | 4.75 | 22 | 45 | | |
| 23 | 24 | 3093 | 1 | 1 | 90 | | 0.7 | | 2659 | 89 | 6.17 | 48 | 22 | | |
| 24 | 25 | 3094 | 1 | .94 | 60 | | 0.8 | | 3985 | 112 | 4.29 | 25 | 38 | | |
| 25 | 26 | 3095 | 1 | .97 | 130 | | 0.8 | | 2612 | 108 | 5.48 | 43 | 227 | | |
| 26 | 27 | 3096 | 1 | .9 | 140 | | 1.1 | | 2640 | 213 | 5.26 | 150 | 129 | | |
| 27 | 28 | 3097 | 1 | .95 | 130 | | 0.7 | | 2727 | 128 | 5.64 | 101 | 130 | | |
| 28 | 29 | 3098 | 1 | .97 | 210 | | 0.8 | | 3126 | 67 | 6.51 | 58 | 272 | | |
| 29 | 30 | 3099 | 1 | .92 | 0 | | 0.6 | | 2889 | 53 | 3.92 | 24 | 155 | | |
| 30 | 31 | 3100 | 1 | .98 | 120 | | 0.7 | | 2211 | 60 | 3.40 | 45 | 128 | | |
| 31 | 32 | 3101 | 1 | .98 | 80 | | 1.2 | | 2686 | 85 | 3.83 | 151 | 85 | | |
| 32 | 33 | 3102 | 1 | .74 | 140 | | 0.1 | | 3143 | 61 | 3.73 | 24 | 55 | | |
| 33 | 34 | 3103 | 1 | .83 | 170 | | 0.1 | | 4564 | 37 | 5.14 | 16 | 20 | | |
| 34 | 35 | 3104 | 1 | .36 | 120 | | 0.1 | | 3313 | 57 | 3.84 | 13 | 28 | | |
| 35 | 35.9 | 3105 | .9 | .45 | 140 | | 0.1 | | 4151 | 61 | 5.71 | 22 | 70 | | |
| 35.9 | 39 | 3106 | 3.1 | 1.2 | 170 | | 0.1 | | 3685 | 13 | 4.81 | 18 | 13 | | |
| 39 | 42 | 3107 | 3 | .2 | 190 | | 0.1 | | 2048 | 152 | 3.53 | 10 | 50 | | |
| 42 | 45 | 3108 | 3 | 1.43 | 280 | | 0.2 | | 4991 | 40 | 4.88 | 22 | 34 | | |
| 45 | 48 | 3109 | 3 | .73 | 0 | | 0.1 | | 3434 | 113 | 3.88 | 20 | 76 | | |
| 48 | 54 | 3110 | 6 | .37 | 110 | | 0.1 | | 1981 | 81 | 3.40 | 13 | 50 | | |
| 54 | 57 | 3111 | 3 | .73 | 135 | | 0.1 | | 2547 | 130 | 3.87 | 22 | 134 | | |
| 57 | 60 | 3112 | 3 | .52 | 270 | | 0.1 | | 3564 | 198 | 4.03 | 23 | 161 | | |
| 60 | 66 | 3113 | 6 | .52 | 140 | | 0.1 | | 1518 | 198 | 3.95 | 21 | 212 | | |
| 66 | 72 | 3114 | 6 | .49 | 290 | | 0.5 | | 4942 | 142 | 4.82 | 25 | 211 | | |
| 72 | 75 | 3115 | 3 | .29 | 530 | | 1.1 | | 7335 | 30 | 8.37 | 154 | 25 | | |
| 75 | 78 | 3116 | 3 | .58 | 410 | | 0.5 | | 5957 | 75 | 6.07 | 30 | 131 | | |
| 78 | 81 | 3117 | 3 | .41 | 540 | | 0.4 | | 5869 | 87 | 5.86 | 34 | 141 | | |
| 81 | 84 | 3118 | 3 | 1.17 | 480 | | 4.1 | | 6328 | 91 | 5.40 | 33 | 58 | | |
| 84 | 87.78 | 3119 | 3.78 | 1.16 | 590 | | 2.1 | | 8912 | 58 | 4.34 | 35 | 53 | | |
| 87.78 | 89.25 | 3120 | 1.47 | 1.4 | 855 | | 2.2 | | 20000 | 36 | 5.26 | 37 | 60 | | |
| 89.25 | 93.4 | 3121 | 4.15 | 1.12 | 280 | | 0.2 | | 4728 | 30 | 3.78 | 24 | 94 | | |
| 93.4 | 95.4 | 3122 | 2 | .62 | 430 | | 7.3 | | 20000 | 293 | 9.86 | 898 | 20 | | |
| 95.4 | 97.4 | 3123 | 2 | .56 | 545 | | 1.4 | | 11245 | 30 | 5.36 | 175 | 24 | | |
| 97.4 | 99.4 | 3124 | 2 | .32 | 395 | | 0.6 | | 7811 | 110 | 4.97 | 34 | 126 | | |
| 99.4 | 101.4 | 3125 | 2 | .7 | 500 | | 0.4 | | 5243 | 285 | 4.98 | 50 | 245 | | |
| 101.4 | 103.4 | 3126 | 2 | .93 | 0 | | 0.1 | | 6744 | 246 | 4.58 | 47 | 445 | | |
| 103.4 | 106.1 | 3127 | 2.67 | .83 | 670 | | 1.1 | | 13629 | 120 | 5.40 | 33 | 161 | | |

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1966 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-3113 | .16 |
| C88-3114 | .53 |
| C88-3115 | .82 |
| C88-3116 | .66 |
| C88-3117 | .68 |
| C88-3118 | .76 |
| C88-3119 | .99 |
| C88-3120 | 2.52 |
| C88-3121 | .55 |
| C88-3122 | 2.76 |
| C88-3123 | 1.31 |
| C88-3124 | .93 |
| C88-3125 | .59 |
| C88-3126 | .77 |
| C88-3127 | 1.47 |

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717



REPORT #: 881151 PA

WESTERN CANADIAN MINING CORP.

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Y ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-3085 | 1.1 | 0.32 | 55 | 170 | <3 | 12 | <3 | 0.19 | 2.1 | 12 | 58 | 2127 | 4.88 | 0.07 | 0.11 | 28 | <1 | 0.02 | 6 | 0.15 | 28 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 4 |
| C88-3086 | 0.5 | 0.45 | 21 | 320 | <3 | 14 | <3 | 0.22 | 2.2 | 12 | 49 | 2297 | 4.87 | 0.07 | 0.16 | 39 | 5 | 0.02 | 7 | 0.18 | 29 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 3 |
| C88-3087 | 0.5 | 0.44 | 23 | 150 | <3 | 16 | <3 | 0.22 | 1.8 | 12 | 51 | 2111 | 4.59 | 0.07 | 0.19 | 33 | <1 | 0.02 | 6 | 0.17 | 26 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 3 |
| C88-3088 | 0.3 | 0.43 | 38 | 110 | <3 | 12 | <3 | 0.18 | 1.9 | 15 | 54 | 2489 | 4.67 | 0.07 | 0.15 | 23 | 1 | 0.02 | 6 | 0.23 | 37 | <3 | <5 | <2 | <2 | 12 | <5 | <3 | 2 |
| C88-3089 | 0.5 | 0.46 | 28 | 360 | <3 | 15 | <3 | 0.22 | 1.6 | 15 | 42 | 1995 | 4.45 | 0.07 | 0.29 | 68 | 2 | 0.02 | 5 | 0.16 | 24 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 5 |
| C88-3090 | 0.7 | 0.54 | 24 | 200 | <3 | 13 | <3 | 0.23 | 1.9 | 16 | 27 | 1921 | 4.10 | 0.08 | 0.33 | 34 | <1 | 0.02 | 6 | 0.19 | 32 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 6 |
| C88-3091 | 0.6 | 0.58 | 50 | 290 | <3 | 8 | 5 | 0.20 | 2.5 | 21 | 37 | 2294 | 6.90 | 0.08 | 0.36 | 42 | 2 | 0.03 | 6 | 0.16 | 36 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 9 |
| C88-3092 | 0.5 | 0.62 | 22 | 210 | <3 | 11 | <3 | 0.20 | 1.8 | 16 | 48 | 3341 | 4.75 | 0.07 | 0.39 | 45 | 4 | 0.02 | 7 | 0.18 | 48 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 10 |
| C88-3093 | 0.7 | 0.47 | 48 | 90 | <3 | 10 | <3 | 0.21 | 2.5 | 14 | 56 | 2659 | 6.17 | 0.08 | 0.25 | 22 | <1 | 0.02 | 7 | 0.20 | 53 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 8 |
| C88-3094 | 0.8 | 0.57 | 25 | 60 | <3 | 13 | <3 | 0.20 | 1.9 | 18 | 31 | 3985 | 4.29 | 0.07 | 0.34 | 38 | <1 | 0.02 | 5 | 0.17 | 30 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 11 |
| C88-3095 | 0.8 | 0.37 | 43 | 130 | <3 | 12 | <3 | 0.35 | 2.6 | 13 | 36 | 2612 | 5.48 | 0.10 | 0.30 | 227 | 3 | 0.02 | 5 | 0.16 | 44 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 10 |
| C88-3096 | 1.1 | 0.44 | 150 | 140 | <3 | 12 | <3 | 0.26 | 2.3 | 13 | 56 | 2640 | 5.26 | 0.09 | 0.24 | 129 | 1 | 0.02 | 6 | 0.16 | 36 | <3 | <5 | <2 | <2 | 15 | <5 | <3 | 21 |
| C88-3097 | 0.7 | 0.42 | 101 | 130 | <3 | 15 | <3 | 0.31 | 2.5 | 16 | 45 | 2727 | 5.64 | 0.08 | 0.32 | 130 | <1 | 0.02 | 7 | 0.15 | 32 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 12 |
| C88-3098 | 0.8 | 0.39 | 58 | 210 | <3 | 9 | <3 | 0.44 | 2.8 | 21 | 45 | 3126 | 6.51 | 0.11 | 0.36 | 272 | <1 | 0.02 | 7 | 0.16 | 44 | <3 | <5 | <2 | <2 | 22 | <5 | <3 | 6 |
| C88-3099 | 0.6 | 0.53 | 24 | <5 | <3 | 16 | <3 | 0.36 | 1.7 | 16 | 51 | 2889 | 3.92 | 0.10 | 0.39 | 155 | 4 | 0.02 | 6 | 0.18 | 32 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 5 |
| C88-3100 | 0.7 | 0.43 | 45 | 120 | <3 | 19 | <3 | 0.31 | 1.5 | 14 | 34 | 2211 | 3.40 | 0.09 | 0.30 | 128 | <1 | 0.01 | 6 | 0.19 | 41 | <3 | <5 | <2 | <2 | 24 | <5 | <3 | 6 |
| C88-3101 | 1.2 | 0.26 | 151 | 80 | <3 | 15 | <3 | 0.21 | 1.9 | 13 | 42 | 2686 | 3.83 | 0.07 | 0.14 | 85 | 17 | 0.02 | 5 | 0.13 | 65 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 8 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 200 |

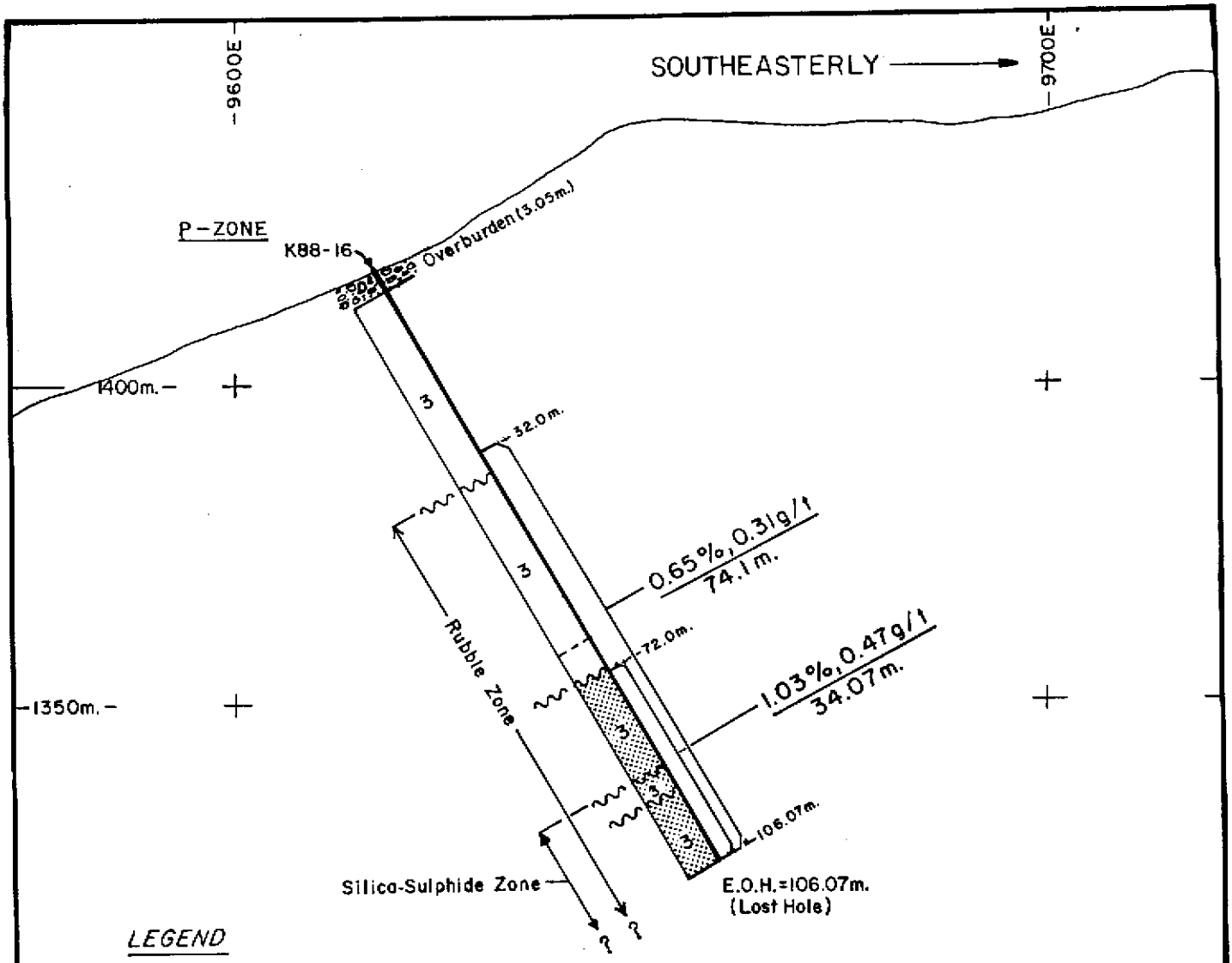
< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

REPORT #: 880963 PA

WESTERN CDN MINING



| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88-3102 | 0.1 | 0.40 | 24 | 140 | <3 | 13 | <3 | 0.21 | 1.5 | 11 | 42 | 3143 | 3.73 | 0.05 | 0.23 | 55 | <1 | 0.01 | 4 | 0.14 | 26 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 61 |
| C88-3103 | 0.1 | 0.28 | 16 | 170 | <3 | 12 | <3 | 0.16 | 1.6 | 16 | 34 | 4564 | 5.14 | 0.05 | 0.13 | 20 | <1 | 0.01 | 4 | 0.14 | 28 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 37 |
| C88-3104 | 0.1 | 0.44 | 13 | 120 | <3 | 22 | <3 | 0.22 | 1.1 | 14 | 41 | 3313 | 3.84 | 0.05 | 0.24 | 28 | 1 | 0.01 | 3 | 0.18 | 20 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 57 |
| C88-3105 | 0.1 | 0.43 | 22 | 140 | <3 | 10 | <3 | 0.20 | 1.6 | 18 | 68 | 4151 | 5.71 | 0.06 | 0.16 | 70 | 10 | 0.01 | 3 | 0.15 | 43 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 61 |
| C88-3106 | 0.1 | 0.20 | 18 | 170 | <3 | 10 | <3 | 0.01 | 1.4 | 16 | 94 | 3685 | 4.81 | 0.02 | 0.01 | 13 | 8 | 0.01 | 6 | 0.03 | 30 | <3 | <5 | <2 | <2 | 5 | <5 | <3 | 12 |
| C88-3107 | 0.1 | 1.00 | 10 | 190 | <3 | 14 | <3 | 0.04 | 1.6 | 12 | 110 | 2048 | 3.53 | 0.03 | 0.40 | 50 | 38 | 0.01 | 6 | 0.22 | 33 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 152 |
| C88-3108 | 0.2 | 0.66 | 22 | 280 | <3 | 10 | <3 | 0.20 | 1.5 | 20 | 60 | 4991 | 4.88 | 0.06 | 0.17 | 34 | 8 | 0.01 | 4 | 0.40 | 40 | <3 | <5 | <2 | <2 | 23 | <5 | <3 | 40 |
| C88-3109 | 0.1 | 1.52 | 20 | <5 | <3 | 21 | <3 | 0.20 | 1.4 | 17 | 35 | 3434 | 3.88 | 0.06 | 0.76 | 76 | 10 | 0.01 | 4 | 0.52 | 32 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 113 |
| C88-3110 | 0.1 | 0.72 | 13 | 110 | <3 | 13 | <3 | 0.06 | 1.2 | 15 | 48 | 1981 | 3.40 | 0.03 | 0.51 | 50 | <1 | 0.01 | 7 | 0.10 | 35 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 81 |
| C88-3111 | 0.1 | 2.11 | 22 | 135 | <3 | 21 | <3 | 0.22 | 1.6 | 10 | 51 | 2547 | 3.87 | 0.06 | 1.53 | 134 | <1 | 0.01 | 4 | 0.38 | 36 | <3 | <5 | <2 | <2 | 17 | <5 | <3 | 130 |
| C88-3112 | 0.1 | 1.82 | 23 | 270 | <3 | 21 | <3 | 0.25 | 2.1 | 13 | 57 | 3564 | 4.03 | 0.07 | 1.41 | 161 | <1 | 0.01 | 6 | 0.25 | 34 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 198 |
| C88-3113 | 0.1 | 2.38 | 21 | 140 | <3 | 21 | <3 | 0.24 | 2.1 | 11 | 60 | 1518 | 3.95 | 0.07 | 2.22 | 212 | <1 | 0.01 | 5 | 0.22 | 38 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 199 |
| C88-3114 | 0.5 | 1.74 | 25 | 290 | <3 | 11 | 3 | 0.22 | 2.1 | 13 | 53 | 4942 | 4.82 | 0.07 | 1.62 | 211 | <1 | 0.01 | 6 | 0.20 | 38 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 142 |
| C88-3115 | 1.1 | 0.41 | 154 | 530 | <3 | 5 | 11 | 0.18 | 2.1 | 14 | 75 | 7335 | 8.37 | 0.08 | 0.10 | 25 | <1 | 0.02 | 5 | 0.15 | 68 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 30 |
| C88-3116 | 0.5 | 1.97 | 30 | 410 | <3 | 10 | 8 | 0.20 | 2.1 | 12 | 98 | 5957 | 6.07 | 0.07 | 1.32 | 131 | 2 | 0.01 | 5 | 0.20 | 45 | <3 | <5 | <2 | <2 | 17 | <5 | <3 | 75 |
| C88-3117 | 0.4 | 2.21 | 34 | 540 | <3 | 14 | 10 | 0.20 | 2.4 | 12 | 65 | 5869 | 5.86 | 0.06 | 1.62 | 141 | <1 | 0.01 | 6 | 0.23 | 44 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 87 |
| C88-3118 | 4.1 | 0.82 | 33 | 480 | <3 | 8 | <3 | 0.18 | 2.1 | 11 | 101 | 6328 | 5.40 | 0.06 | 0.50 | 58 | 3 | 0.01 | 7 | 0.17 | 50 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 91 |
| C88-3119 | 2.1 | 0.80 | 35 | 590 | <3 | 10 | <3 | 0.17 | 1.6 | 11 | 92 | 8912 | 4.34 | 0.04 | 0.47 | 53 | 5 | 0.01 | 5 | 0.17 | 30 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 58 |
| C88-3120 | 2.2 | 0.52 | 37 | 855 | <3 | 7 | 6 | 0.06 | 2.4 | 14 | 125 | >20000 | 5.26 | 0.03 | 0.38 | 60 | <1 | 0.01 | 6 | 0.10 | 20 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 36 |
| C88-3121 | 0.2 | 0.97 | 24 | 280 | <3 | 11 | <3 | 0.10 | 1.2 | 13 | 72 | 4728 | 3.78 | 0.03 | 0.73 | 94 | <1 | 0.01 | 5 | 0.11 | 27 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 30 |
| C88-3122 | 7.3 | 0.21 | 898 | 430 | <3 | 5 | 25 | 0.13 | 1.6 | 8 | 135 | >20000 | 9.86 | 0.06 | 0.02 | 20 | 2 | 0.03 | 12 | 0.13 | 142 | <3 | <5 | 262 | <2 | 24 | <5 | <3 | 293 |
| C88-3123 | 1.4 | 0.28 | 175 | 545 | <3 | 10 | <3 | 0.07 | 1.2 | 10 | 131 | 11245 | 5.36 | 0.04 | 0.02 | 24 | <1 | 0.01 | 4 | 0.07 | 36 | <3 | <5 | <2 | <2 | 4 | <5 | <3 | 30 |
| C88-3124 | 0.6 | 1.36 | 34 | 395 | <3 | 10 | 7 | 0.15 | 2.1 | 11 | 154 | 7811 | 4.97 | 0.06 | 1.00 | 126 | 2 | 0.01 | 6 | 0.17 | 44 | <3 | <5 | <2 | <2 | 21 | <5 | <3 | 110 |
| C88-3125 | 0.4 | 1.79 | 50 | 500 | <3 | 11 | 10 | 0.20 | 2.3 | 16 | 84 | 5243 | 4.98 | 0.06 | 1.77 | 245 | <1 | 0.02 | 8 | 0.20 | 42 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 285 |
| C88-3126 | 0.1 | 1.62 | 47 | <5 | <3 | 10 | 6 | 0.38 | 2.1 | 13 | 53 | 6744 | 4.58 | 0.10 | 1.51 | 445 | <1 | 0.01 | 6 | 0.22 | 42 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 246 |
| C88-3127 | 1.1 | 1.05 | 33 | 670 | <3 | 8 | 13 | 0.15 | 2.3 | 12 | 72 | 13629 | 5.40 | 0.05 | 0.82 | 161 | <1 | 0.01 | 4 | 0.17 | 25 | <3 | <5 | <2 | <2 | 28 | <5 | <3 | 120 |




## LEGEND

Fault

0.13%, 1.13g/t / 10.3m. — %Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Interval defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE – fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a)/MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST — foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) — interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE — interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

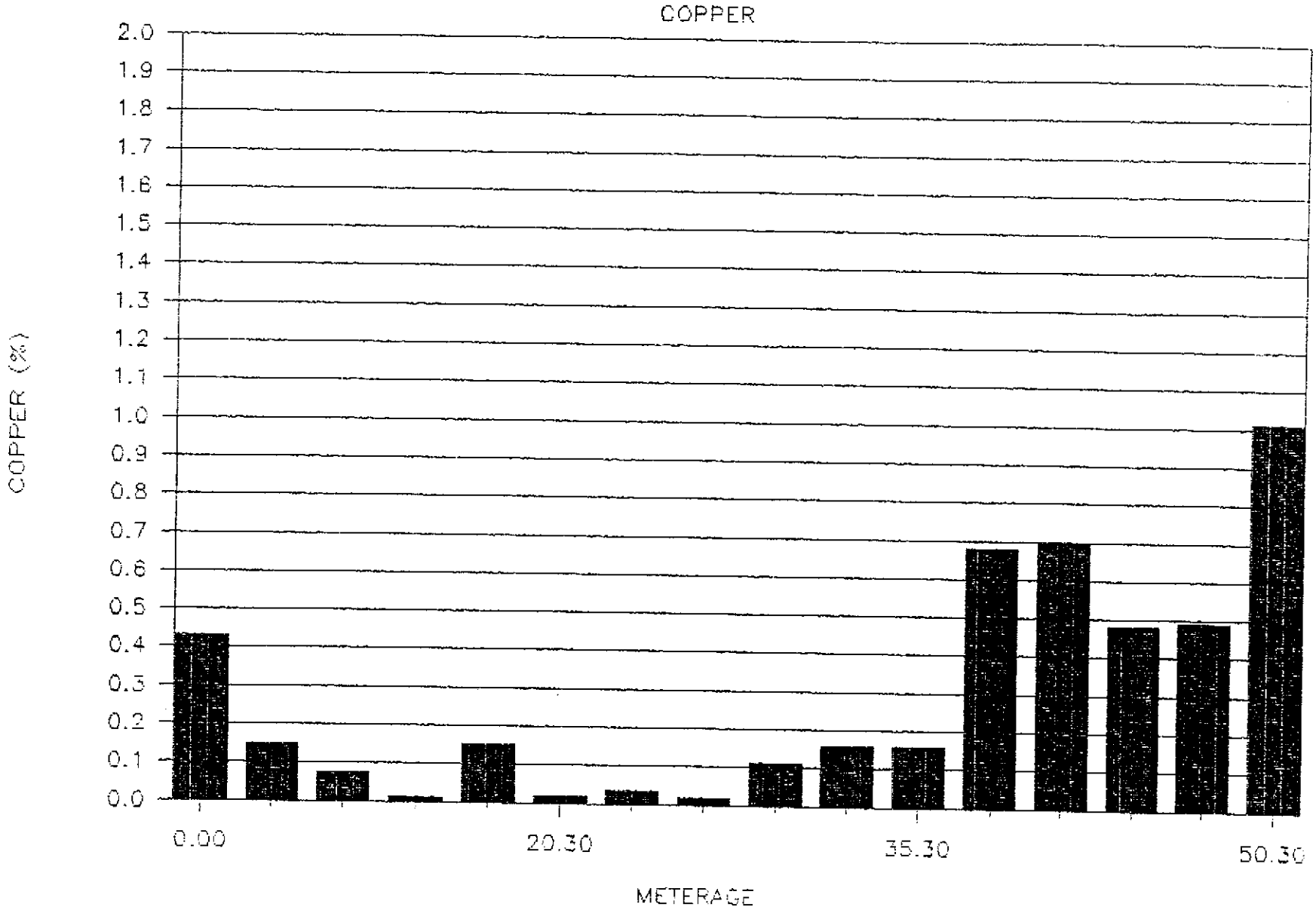
SCALE: 1:1000 — 0 10 20 30 40 Metres

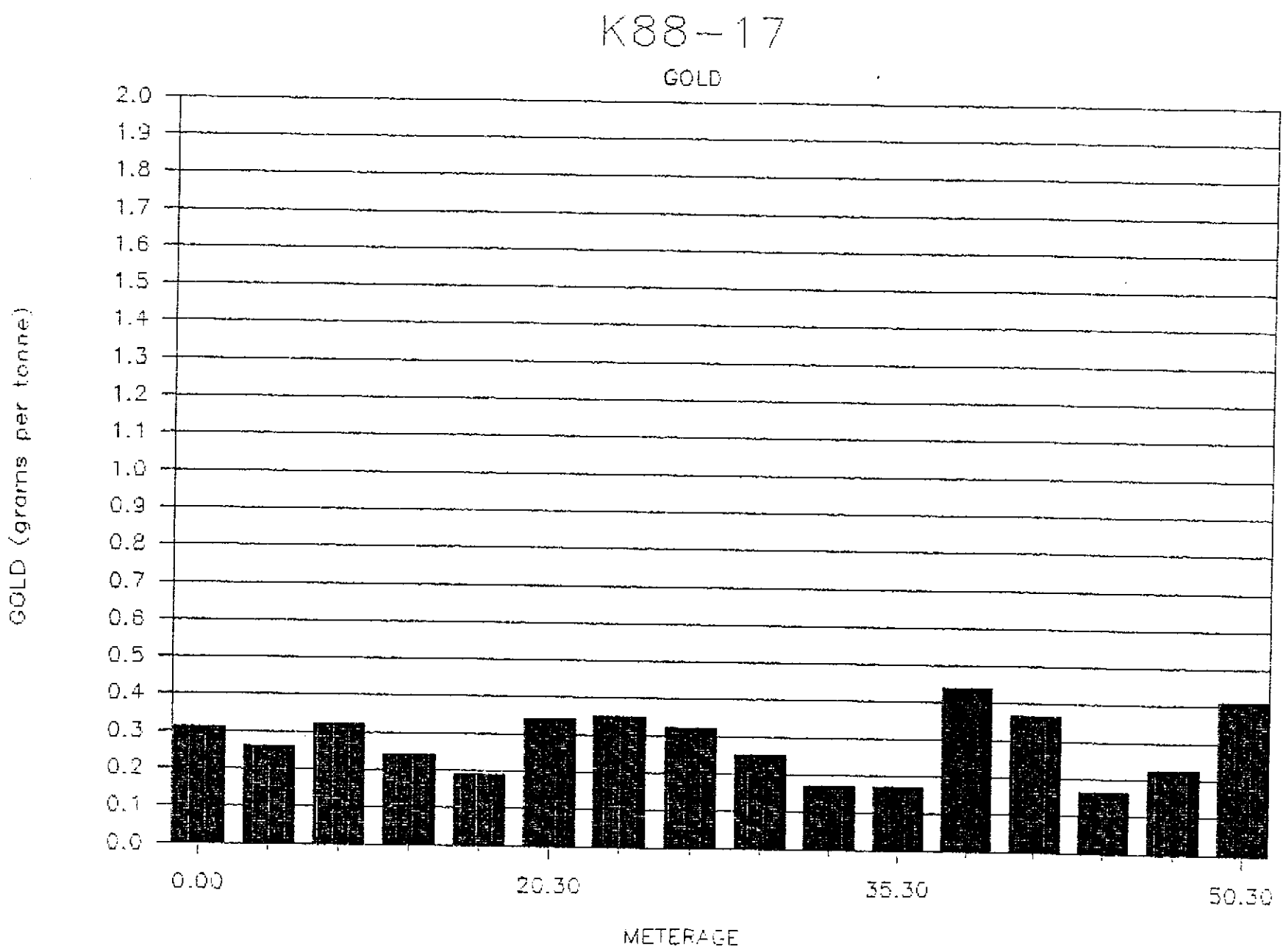
# SULPHURETS GOLD CORPORATION
## 1989 KERR PROJECT
## D.D.H. K88-16
## SECTION

COLLAR:- 10387.4N, 9616.9E
BEARING: 125° DIP: -60°
ELEVATION: 1412.3m.

REPORT:1065 FIGURE No.

# K88-17


COPPER
COPPER (%)
2.0
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
0.00
20.30
35.30
50.30
METERAGE


K88-17
GOLD
GOLD (grams per tonne)
2.0
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1.0
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0.0
0.00
20.30
35.30
50.30
METERAGE

KERR PROJECT D.D.HOLE K-88-17

| | | | |
|---|---|---|---|
| LOCATION | P-ZONE | COLLAR LAT. | 10352.2 NORTH |
| DATE STARTED | JULY 31, 1988 | LONG. | 9652.3 EAST |
| DATE COMPLETED | AUGUST 1, 1988 | ELEVATION | 1441.2 m |
| CORE RECOVERY | 25.14% | AZIMUTH | 140 DIP -60 deg |
| DRILLED BY | FALCON DRILLING LTD | LENGTH | 57.00 m |
| LOGGED BY | S. CASSELMAN | HOR. PROJ. | 28.50 m |
| OBJECTIVE | TEST P-ZONE SOIL GEOCHEMICAL ANOMALY B-ZONE FAULT MINERALIZATION EXTENSION | VERT. PROJ. | 49.36 m |
| DIP TEST DEPTH | m DIP deg | | |
| DEPTH | m DIP deg | | |

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 8.23 | 8.23 | OVERBURDEN |
| 8.23 | 11.30 | 3.07 | QUARTZ-SERICITE SCHIST<br>- light to medium grey green<br>- moderately foliated at 50 deg to C.A.<br>- 1% weathered out, limonitic clay quartz veins<br>- intense sericitization, weak chloritization<br>- 10 to 15% disseminated and stringer pyrite<br>- may contain up to 2% chalcocite giving core a slight blue tint in sections<br>- chalcocite generally associated with pyrite<br>- fairly competent core, average 10 cm lengths<br>- contact with faulted rock is gradational over 7.0 m<br>- contact is arbitrary - hanging wall is competent grey-green - fault zone is composed of 1 cm to 10 cm pieces (average 1 - 2 cm) of bleached sericitic schist |

KERR PROJECT D.D.HOLE K-88-17

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 11.30 | 57.00 | 45.70 | FAULT ZONE / QUARTZ-SERICITE-PYRITE SCHIST<br>- average core size 2 to 3 cm long<br>- variable appearance - at contact it is quite bleached with limonitic clay, with occasional 10 cm blocks of light grey schist down to 26.3 m<br>- 26.3 to 29.3 m - light blue-grey intense silicification and sericitization - slightly similar to silicified sulphide sections in K-88-11, 14, and 16 - however not as blue-grey and not as many sulphides (pyrite, chalcopyrite, chalcocite), also quite fractured<br>- 29.3 to 41.0 m - sericitic clay blocks with limonite on fracture surfaces and coating on quartz veins<br><br>- 41.0 to 57.0 - light to medium grey-blue chips of core, average 1 cm wide - intensely sheared fault zone at 35 deg to C.A.<br>- very poor recovery<br><br>E.O.H. |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 12:37:25 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8817 | 10352.2 | 9652.4 | 1441.2 | 140 | 60 | 57 | P-Zone | | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | MI | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 8.23 | | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 8.23 | 11.3 | 3.07 | 38 | SRCT SCHT | | F.MG | 3 | 5 | 60 | 3 | 8 | | | | | | 95 | 15 | | | 1 | | | |
| 11.3 | 14.3 | 3 | 24 | FAULT SRCT SCHT | | F.MG | 8 | 2 | 60 | 5 | 2 | | | | | | 100 | 15 | | | 1 | | | |
| 14.3 | 17.3 | 3 | 20 | FAULT SRCT SCHT | | F.MG | 1 | 3 | 75 | 8 | | | | | | | 100 | 8 | | | | | | |
| 17.3 | 20.3 | 3 | 21 | FAULT SRCT SCHT | | F.MG | | 3 | 75 | 8 | | | | | | | 100 | 8 | | | .5 | | | |
| 20.3 | 23.3 | 3 | 21 | FAULT SRCT SCHT | | F.MG | 3 | 5 | 75 | 3 | 1 | | | | | | 100 | 12 | | | 1 | | | |
| 23.3 | 26.3 | 3 | 20 | FAULT SRCT SCHT | | F.MG | | 2 | 70 | 20 | 1 | | | | | | 100 | 5 | | | | | | |
| 26.3 | 29.3 | 3 | 20 | FAULT SRCT SCHT | | F.MG | 10 | 10 | 50 | 5 | 2 | | | | | | 100 | 15 | | | 1 | | | |
| 29.3 | 32.3 | 3 | 20 | FAULT SRCT SCHT | | F.MG | 10 | 5 | 55 | 10 | 3 | | | | | | 100 | 12 | | | .3 | | | |
| 32.3 | 35.3 | 3 | 22 | FAULT SRCT SCHT | | F.MG | 5 | 5 | 55 | 10 | 5 | | | | | | 90 | 12 | | | .3 | | | |
| 35.3 | 38.3 | 3 | 19 | FAULT SRCT SCHT | | F.MG | 2 | 1 | 35 | 3 | 10 | | | | | | 85 | 10 | | | 1 | | | |
| 38.3 | 41.3 | 3 | 20 | FAULT SRCT SCHT | | F.MG | 2 | 2 | 40 | 5 | 15 | | | | | | 85 | 12 | | | 1 | | | |
| 41.3 | 44.3 | 3 | 22 | FAULT SRCT SCHT | | F.MG | 8 | 2 | 50 | | 10 | | | | | | 85 | 12 | | | 2 | | | |
| 44.3 | 47.3 | 3 | 22 | FAULT SRCT SCHT | | F.MG | 8 | 2 | 50 | | 10 | | | | | | 85 | 12 | | | 2 | | | |
| 47.3 | 50.3 | 3 | 22 | FAULT SRCT SCHT | | F.MG | 8 | 2 | 60 | | 10 | | | | | | 85 | 12 | | | 2 | | | |
| 50.3 | 53.3 | 3 | 10 | FAULT SRCT SCHT | | F.MG | 1 | 2 | 70 | 3 | 10 | | | | | | 100 | 8 | | | .5 | | | |
| 53.3 | 57 | 3.7 | 8 | FAULT SRCT SCHT | | F.MG | 5 | 2 | 60 | 3 | 10 | | | | | | 90 | 10 | | | 2 | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 09:25:49 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8817 | 10352.2 | 9652.4 | 1441.2 | 140 | 60 | 57 | P-Zone | | |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 8.23 | | | | | | | | | | | | | | |
| 8.23 | 11.3 | 3128 | 3.07 | 2.62 | 310 | | 0.4 | | 4288 | 45 | 3.95 | 14 | 32 | | |
| 11.3 | 14.3 | 3129 | 3 | 1.03 | 260 | | 0.1 | | 1478 | 10 | 3.17 | 10 | 12 | | |
| 14.3 | 17.3 | 3130 | 3 | .8 | 320 | | 0.1 | | 468 | 10 | 1.35 | 4 | 16 | | |
| 17.3 | 20.3 | 3131 | 3 | 1.08 | 240 | | 0.1 | | 101 | 6 | 1.12 | 4 | 6 | | |
| 20.3 | 23.3 | 3132 | 3 | 1.33 | 190 | | 0.1 | | 1502 | 15 | 2.77 | 11 | 16 | | |
| 23.3 | 26.3 | 3133 | 3 | 1.12 | 340 | | 0.1 | | 196 | 50 | 4.87 | 27 | 33 | | |
| 26.3 | 29.3 | 3134 | 3 | .73 | 350 | | 0.1 | | 333 | 14 | 2.74 | 10 | 18 | | |
| 29.3 | 32.3 | 3135 | 3 | .3 | 320 | | 0.1 | | 184 | 6 | 2.11 | 8 | 14 | | |
| 32.3 | 35.3 | 3136 | 3 | .44 | 250 | | 0.1 | | 1117 | 222 | 4.41 | 27 | 92 | | |
| 35.3 | 38.3 | 3137 | 3 | 1.16 | 170 | | 0.1 | | 1581 | 252 | 3.95 | 20 | 141 | | |
| 38.3 | 41.3 | 3138 | 3 | .47 | 170 | | 0.2 | | 1433 | 96 | 2.93 | 15 | 131 | | |
| 41.3 | 44.3 | 3139 | 3 | .54 | 440 | | 0.5 | | 5659 | 123 | 5.96 | 26 | 264 | | |
| 44.3 | 47.3 | 3140 | 3 | 1.2 | 365 | | 0.5 | | 6282 | 138 | 5.86 | 45 | 325 | | |
| 47.3 | 50.3 | 3141 | 3 | .62 | 165 | | 0.7 | | 4546 | 46 | 6.27 | 45 | 64 | | |
| 50.3 | 53.3 | 3142 | 3 | .42 | 225 | | 0.7 | | 4535 | 28 | 5.60 | 478 | 16 | | |
| 53.3 | 57 | 3143 | 3.7 | .47 | 410 | | 1.6 | | 9847 | 28 | 6.91 | 86 | 6 | | |

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-3138 | .16 |
| C88-3139 | .68 |
| C88-3140 | .70 |
| C88-3141 | .48 |
| C88-3142 | .49 |
| C88-3143 | 1.01 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: BB1151 PA

WESTERN CANADIAN MINING CORP.



| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Z pp |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-3128 | 0.4 | 0.54 | 14 | 310 | <3 | 10 | <3 | 0.15 | 1.6 | 14 | 81 | 4288 | 3.95 | 0.04 | 0.20 | 32 | 17 | 0.01 | 4 | 0.14 | 30 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 4 |
| C88-3129 | 0.1 | 0.20 | 10 | 260 | <3 | 12 | <3 | 0.01 | 1.1 | 10 | 80 | 1478 | 3.17 | 0.01 | 0.01 | 12 | <1 | 0.01 | 4 | 0.03 | 20 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 1 |
| C88-3130 | 0.1 | 0.25 | 4 | 320 | <3 | 127 | <3 | 0.01 | 0.1 | 1 | 101 | 768 | 1.35 | 0.01 | 0.01 | 16 | 4 | 0.01 | 2 | 0.01 | 18 | <3 | <5 | <2 | <2 | 17 | <5 | <3 | 1 |
| C88-3131 | 0.1 | 0.18 | 4 | 240 | <3 | 131 | <3 | 0.01 | 0.1 | 2 | 60 | 101 | 1.12 | 0.01 | 0.01 | 6 | 10 | 0.01 | <1 | 0.07 | 40 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | |
| C88-3132 | 0.1 | 0.35 | 11 | 190 | <3 | 15 | <3 | 0.01 | 0.8 | 8 | 160 | 1502 | 2.77 | 0.01 | 0.01 | 16 | 2 | 0.01 | 4 | 0.03 | 55 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 1 |
| C88-3133 | 0.1 | 0.66 | 27 | 340 | <3 | 283 | <3 | 0.01 | 1.4 | <1 | 101 | 196 | 4.87 | 0.03 | 0.30 | 33 | 13 | 0.01 | 4 | 0.12 | 33 | <3 | <5 | <2 | <2 | 35 | <5 | <3 | 5 |
| C88-3134 | 0.1 | 0.20 | 10 | 350 | <3 | 17 | <3 | 0.01 | 0.8 | 3 | 147 | 333 | 2.74 | 0.01 | 0.01 | 18 | <1 | 0.01 | 2 | 0.03 | 20 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 1 |
| C88-3135 | 0.1 | 0.27 | 8 | 320 | <3 | 140 | <3 | 0.01 | 0.5 | 2 | 160 | 184 | 2.11 | 0.01 | 0.01 | 14 | <1 | 0.01 | 3 | 0.01 | 20 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | |
| C88-3136 | 0.1 | 1.92 | 27 | 250 | <3 | 38 | 3 | 0.14 | 1.8 | 6 | 60 | 1117 | 4.41 | 0.05 | 1.42 | 92 | <1 | 0.01 | 3 | 0.28 | 70 | <3 | <5 | <2 | <2 | 20 | <5 | <3 | 22 |
| C88-3137 | 0.1 | 1.75 | 20 | 170 | <3 | 44 | <3 | 0.10 | 1.6 | 5 | 45 | 1581 | 3.95 | 0.03 | 1.35 | 141 | <1 | 0.01 | 4 | 0.23 | 41 | <3 | <5 | <2 | <2 | 28 | <5 | <3 | 25 |
| C88-3138 | 0.2 | 1.34 | 15 | 170 | <3 | 31 | <3 | 0.07 | 1.1 | 7 | 80 | 1433 | 2.93 | 0.03 | 0.92 | 131 | <1 | 0.01 | 4 | 0.10 | 41 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 9 |
| C88-3139 | 0.5 | 2.22 | 26 | 440 | <3 | 10 | 12 | 0.16 | 2.6 | 12 | 95 | 5659 | 5.96 | 0.06 | 1.66 | 264 | <1 | 0.01 | 5 | 0.16 | 44 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 12 |
| C88-3140 | 0.5 | 2.31 | 45 | 365 | <3 | 10 | 20 | 0.20 | 2.4 | 14 | 63 | 6282 | 5.86 | 0.07 | 1.92 | 325 | <1 | 0.01 | 6 | 0.18 | 44 | <3 | <5 | <2 | <2 | 14 | <5 | <3 | 13 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 2000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

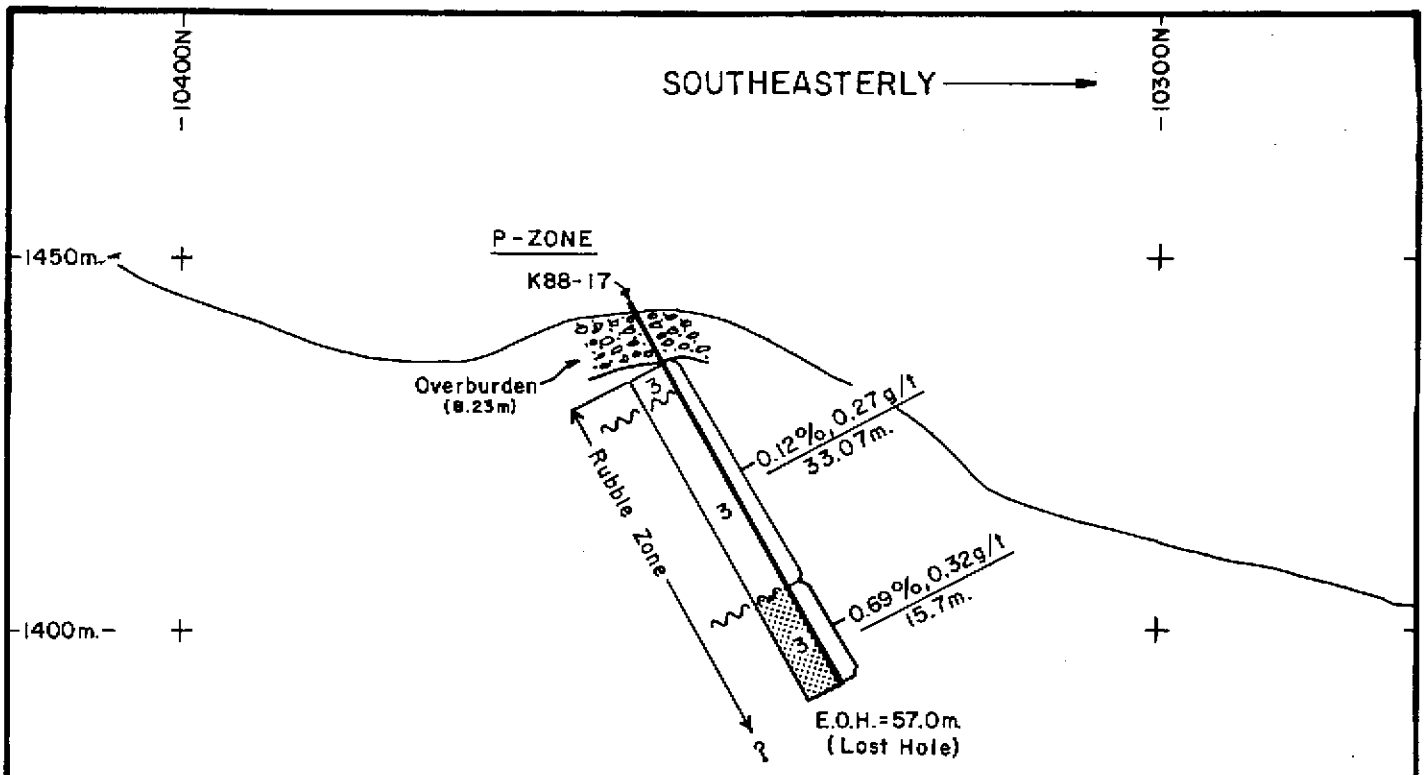
REPORT #: 890963 PA WESTERN CDN MINING



| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88-3141 | 0.7 | 0.65 | 45 | 165 | <3 | 7 | 3 | 0.16 | 2.7 | 16 | 72 | 4546 | 6.27 | 0.07 | 0.43 | 64 | <1 | 0.02 | 8 | 0.14 | 37 | <3 | <5 | <2 | <2 | 10 | <5 | <3 | 46 |
| C88-3142 | 0.7 | 0.32 | 478 | 225 | <3 | 10 | <3 | 0.08 | 0.2 | 17 | 91 | 4535 | 5.60 | 0.06 | 0.07 | 16 | <1 | 0.02 | 9 | 0.08 | 43 | <3 | <5 | <2 | <2 | 11 | <5 | <3 | 28 |
| C88-3143 | 1.6 | 0.16 | 86 | 410 | <3 | 10 | 8 | 0.01 | 2.8 | 16 | 27 | 9647 | 6.91 | 0.05 | 0.02 | 6 | 20 | 0.02 | 5 | 0.03 | 54 | <3 | <5 | <2 | <2 | 6 | <5 | <3 | 28 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum is = Insufficient Sample ns = No sample > = Greater than Maximum AuFA = Fire assay/AAS

ANOMALOUS RESULTS:
FURTHER ANALYSES
BY ALTERNATE
METHODS SUGGESTED




## LEGEND

Fault

0.13% | 1.13g/t / 10.3m. — % Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Interval defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE – fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a)/MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST – foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) – interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE – interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

SCALE: 1:1000 (0, 10, 20, 30, 40 Metres)

# SULPHURETS GOLD CORPORATION

## 1989 KERR PROJECT

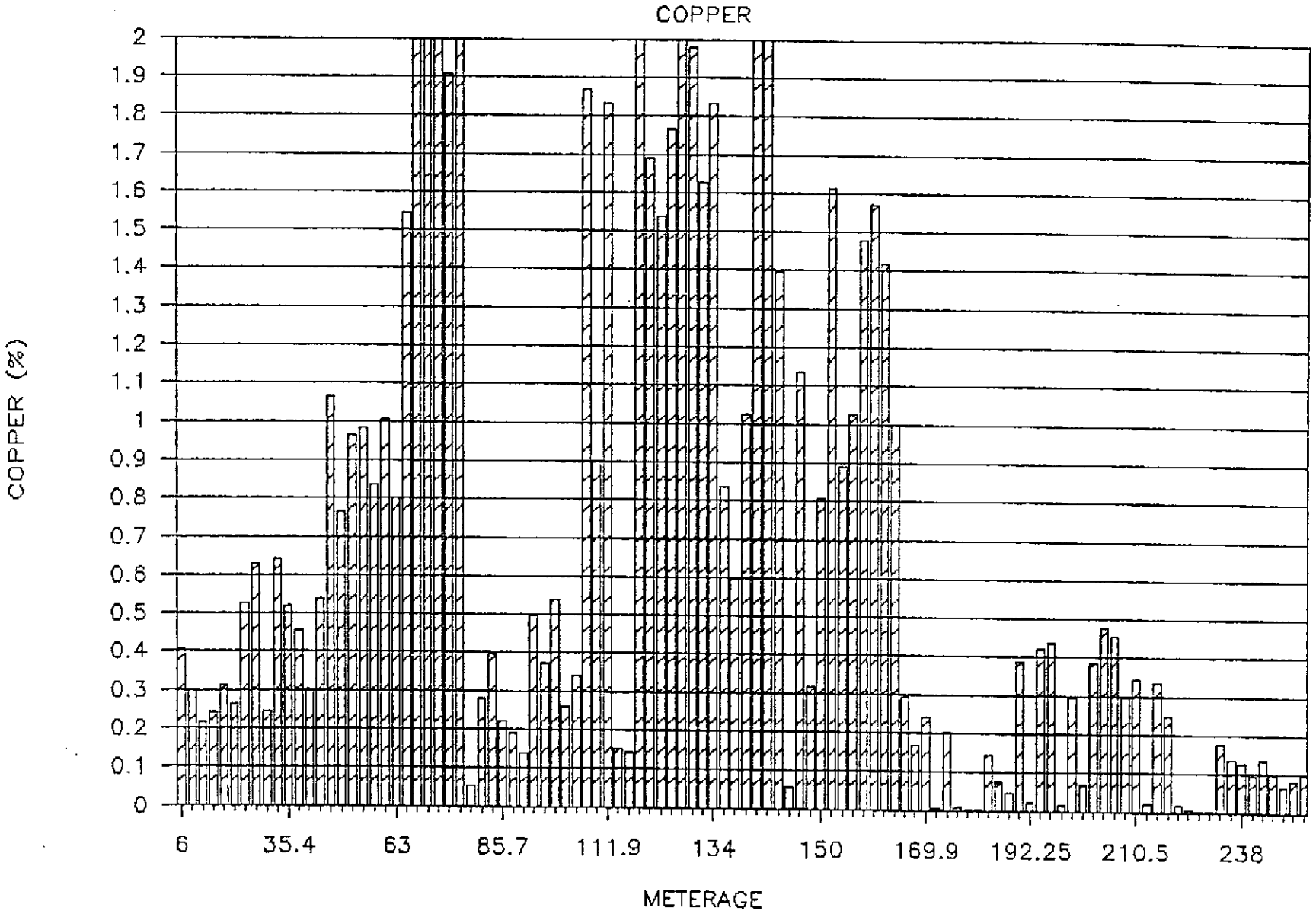
## D.D.H. K88-17

## SECTION

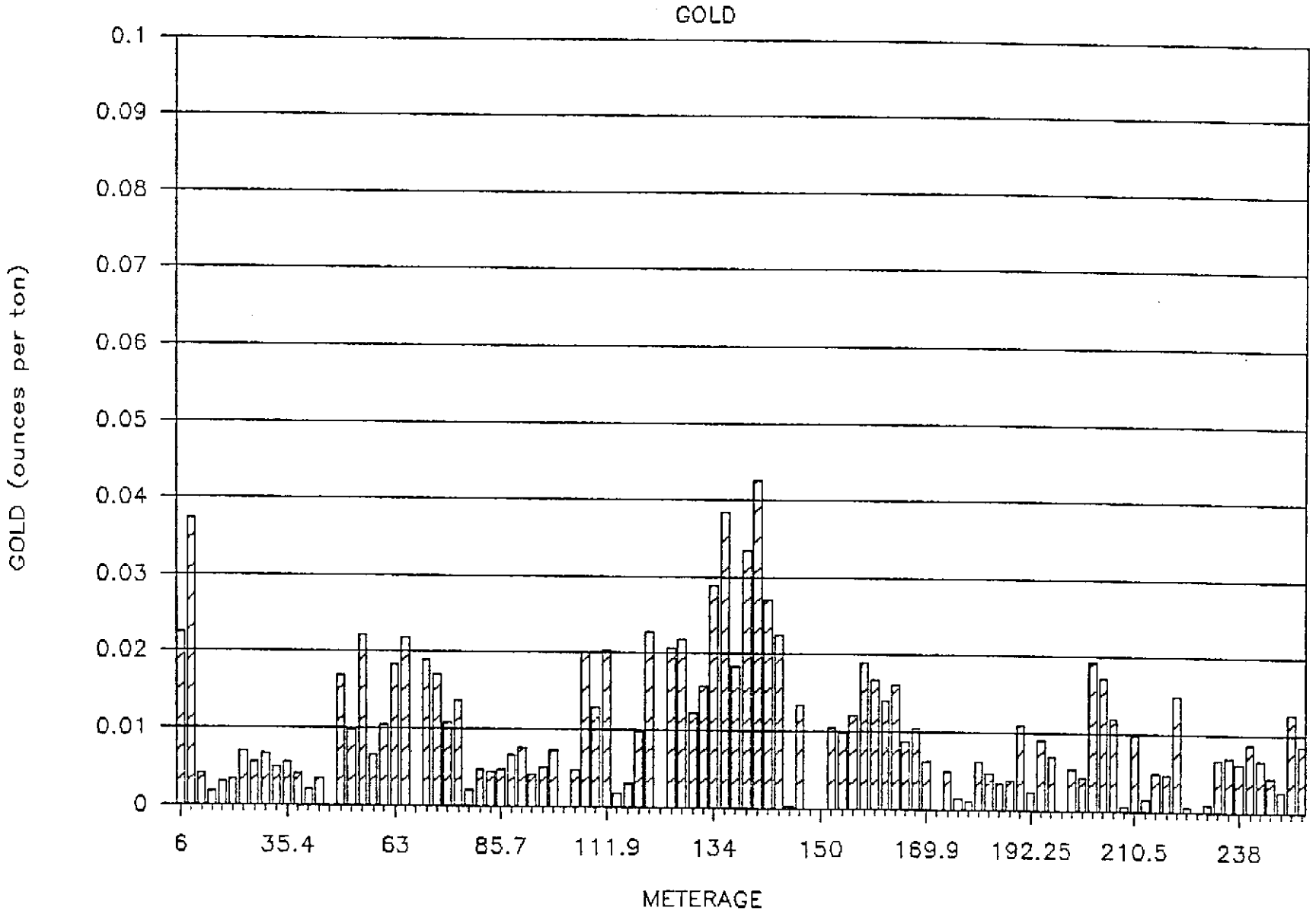
COLLAR:- 10352.2N, 9652.3E
BEARING: 140° DIP: -60°
ELEVATION: 1441.2m.

REPORT: 1065 FIGURE No.

# K88-18


COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
6
35.4
63
85.7
111.9
134
150
169.9
192.25
210.5
238
METERAGE

# K88-18


GOLD
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
GOLD (ounces per ton)
6
35.4
63
85.7
111.9
134
150
169.9
192.25
210.5
238
METERAGE

KERR PROJECT D.D.HOLE K-88-18

| | | | |
|---|---|---|---|
| LOCATION | P-ZONE JUST EAST OF GLACIER | COLLAR LAT. | 10229.1 NORTH |
| DATE STARTED | AUGUST 10, 1988 | LONG. | 9599.5 EAST |
| DATE COMPLETED | AUGUST 12, 1988 | ELEVATION | 1468.8 m |
| CORE RECOVERY | 90.37% | AZIMUTH | 060 DIP -60 deg |
| DRILLED BY | FALCON DRILLING LTD | LENGTH | 255.42 m |
| LOGGED BY | S. CASSELMAN | HOR. PROJ. | 149.31 m |
| OBJECTIVE | INTERSECT NORTH EXTENSION OF B-ZONE FAULT/MINERALIZATION | VERT. PROJ. | 255.42 m |

DIP TEST DEPTH 255.42 m DIP -48 deg
DEPTH _____m DIP_____deg

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 3.05 | 3.05 | OVERBURDEN |
| 3.05 | 26.60 | 23.55 | SERICITE-CHLORITE-PYRITE SCHIST<br>- intensely sericitized and chloritized, well foliated with 10 to 20% pyrite (locally up to 40% pyrite) as wisps and veinlets paralleling foliation<br>- foliated at 40 deg to C.A.<br>- light to medium-grey colour<br>- 1 to 5% quartz-calcite veining (paralleling foliation)<br>- trace to .5% chalcopyrite with chalcocite<br>- 15% spotty chlorite<br>- top 2.0 m of hole is fractured and weathered<br>- limonitic<br>- apart from top 2 m rock is quite competent, with solid core, average length of pieces is about 25 - 30 cm<br>- towards bottom of section (nearing fault) silicification is more prominent - last 4 m is 10 to 15% silicified, in sections 1 cm to 20 cm wide<br>- fault contact at 45 deg to C.A. |
| 26.60 | 35.40 | 8.80 | FAULT ZONE / QUARTZ-SERICITE-PYRITE SCHIST<br>- quite sheared and fractured, soft sericite schist<br>- average pieces 3 to 7 cm long with sections of sericitic gouge |

KERR PROJECT D.D.HOLE K-88-18

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - 2 to 3% silicification, 5% spotty chlorite<br>- 7 to 10% disseminated pyrite with chalcocite rims<br>- limonitic fractures and blocks<br>- foliation at 25 to 50 deg C.A.<br>- trace of epidote<br>- lower contact at 60 deg to C.A.<br>- 1% anhydrite |
| 35.40 | 38.80 | 3.40 | SERICITE SCHIST<br>- as in 3.05 to 26.6<br>- competent sericite schist section - average core length 10 to 15 cm<br>- foliation at 55 deg to C.A.<br>- 10 to 15% pyrite veins and stringers paralleling foliation<br>- trace of chalcopyrite, .5% chalcocite<br>- .5% white gypsum on fracture surfaces<br>- trace of dendritic native copper on fracture surfaces |
| 38.80 | 45.40 | 6.60 | FAULT ZONE / QUARTZ - SERICITE - PYRITE SCHIST<br>- moderately fractured, average piece 5-10 cm long<br>- foliated from 55 to 80 deg to C.A.<br>- fractured at 55 to 80 deg, parallel to foliation<br>- 10 to 15% vuggy silicification with disseminated pyrite and chalcopyrite and a trace of chalcocite - pyrite also occurs in veins<br>- 15% chlorite spots<br>- 1 to 2% limonite on fracture surfaces and in vugs |
| 45.40 | 75.85 | 30.45 | SILICA STOCKWORK - PYRITE - CHALCOPYRITE-CHALCOCITE ZONE<br>- quite competent, average piece 20 to 25 cm<br>- medium grey to green colour with white to light grey silica patches<br>- from 65.0 to 75.85 m massive silica-pyrite-chalcopyrite-chalcocite breccia at 50.0 m - 30 cm bull white quartz vein with 2% chalcopyrite as large (2 cm) blebs<br>- quartz veining and weak foliation at 40 deg<br>- intense silicification and sericitization<br>- pyrite, chalcopyrite and chalcocite occur as disseminations, veinlets, blebs, patches, |

KERR PROJECT D.D.HOLE K-88-18

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | and wispy stringers in brecciated silica zone, sulphides occur as wispy stringers and veins surrounding quartz fragments<br>- pyrite occurs mainly as stringers<br>- chalcopyrite occurs as blebs<br>- chalcocite as fine amorphous dark grey patches, generally around other sulphides |
| 75.85 | 77.70 | 1.85 | ANDESITE DYKE<br>- medium to dark green, moderate chloritization, weak sericitization<br>- 5% quartz-calcite veining<br>- < 1% pyrite |
| 77.70 | 87.78 | 10.08 | SERICITE-CHLORITE SCHIST<br>- medium grey-green colour, mottled and patchy chlorite, pervasive sericite<br>- weak to moderately foliated at 50 deg to C.A.<br>- disseminated and stringer pyrite (10 to 15%)<br>- 1 to 5% quartz veining, generally barren of sulphides<br>- towards bottom (83.7 to 85.7) becomes quite fractured with some fault gouge<br>- possible protolith : medium-grained andesite dyke as in section 9.0 to 26.6 m |
| 87.78 | 89.28 | 1.50 | ANDESITE DYKE<br>- as in 75.85 to 77.7 m<br>- light to medium green<br>- moderate chloritization, weak sericitization<br>- 1% quartz-calcite veining, <1% pyrite<br>- upper contact at 30 deg, lower at 55 deg to C.A. |
| 89.28 | 91.90 | 2.62 | SERICITE-CHLORITE SCHIST<br>- as in 77.7 to 87.78 m |
| 91.90 | 103.25 | 11.35 | SHEARED ANDESITE DYKE<br>- medium-grained<br>- medium to dark green, relic hornblende and plagioclase crystals evident, alteration to chlorite and sericite<br>- moderate chlorite - weak to moderate sericite<br>- contains xenoliths of silicified dacite tuff up to 10 cm long - brecciated with chlorite matrix |

KERR PROJECT D.D.HOLE K-88-18

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - weak foliation defined by alignment of tabular crystals at 40 deg to C.A. parallels fracture planes which are at 40 deg and 70 deg to C.A.<br>- fairly competent core average length 10 to 20 cm |
| 103.25 | 111.90 | 8.65 | DACITE TUFF BRECCIA<br>- similar to breccia in the bottom of hole K-87-13 / K-88-6<br>- medium to dark grey-green<br>- intense chloritization, moderate sericitization<br>- subangular to rounded tuff clasts in a chlorite-sulphide matrix<br>- traces of native copper on fracture surfaces<br>- 5% clayey vugs / veins<br>- 10 to 15% fine disseminated pyrite<br>- trace to 1% chalcopyrite and chalcocite with bornite<br>- 1 to 5% quartz veining (bull white), generally containing sulphides, mainly chalcopyrite and chalcocite<br>- sample # 3183 contains 5% quartz, chalcopyrite, and chalcocite veins from .5 to 8 cm wide<br>- chalcopyrite generally has a chalcocite coating |
| 111.90 | 117.60 | 5.70 | FAULT ZONE / SERICITIZED CHLORITIZED ANDESITE DYKE<br>- intensely sericitized spotty and wispy chlorite<br>- 10% finely disseminated and stringer pyrite<br>- foliated and fractured at 55 deg to C.A.<br>- average piece 5 cm long |
| 117.60 | 145.85 | 28.25 | SILICA STOCKWORK - PYRITE - CHALCOPYRITE-CHALCOCITE ZONE<br>- as in 65.0 to 75.85 - massive silica, pyrite, chalcopyrite, chalcocite, however much more sulphides (especially chalcopyrite) present<br>- light grey to white colour with grey-blue wisps of sulphides throughout<br>- occasional (1%) veins up to 8 cm wide of almost massive chalcopyrite with some pyrite |

KERR PROJECT D.D.HOLE K-88-18

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - most prominent vein orientations are 40 to 60 deg to C.A.<br>- trace of bornite as blebs at 119.0 m to 130.0 m<br>- core is very competent average piece 15 to 20 cm<br>- very intense silica-sulphide stockwork |
| 145.85 | 146.27 | 0.42 | ANDESITE DYKE<br>- medium green, fine-grained as in sections 75.85 to 77.7 m and 87.78 to 89.28 m<br>- upper contact at 20 deg, lower contact at 65 deg to C.A. |
| 146.27 | 147.27 | 1.00 | SILICA STOCKWORK - PYRITE - CHALCOPYRITE-CHALCOCITE ZONE<br>- as in 117.6 to 145.85 m |
| 147.27 | 147.55 | 0.28 | ANDESITE DYKE<br>- as in 145.85 to 146.27 m<br>- upper contact at 60 deg, lower at 20 deg |
| 147.55 | 169.90 | 22.35 | SILICA STOCKWORK - PYRITE - CHALCOPYRITE-CHALCOCITE ZONE<br>- as in sections 117.6 to 145.85 m and 146.27 to 147.27<br>- 1 to 5% chalcopyrite, 1 to 2% chalcocite<br>- from 161 m chalcopyrite and chalcocite content drops off to a maximum of 1% combined<br>- also the silica content drops while the sericite content increases |
| 169.90 | 173.35 | 3.45 | SHEARED ANDESITE DYKE<br>- light to dark green, medium-grained<br>- various intensities of chlorite and sericite alteration<br>- where sheared and schistose becomes more sericitic with alignment of sericite and chlorite bands<br>- competent (unsheared) sections are more chloritic with large globs of massive chlorite in quartz-calcite-ankerite (?) veins to 8%<br>- where rock less sheared, the protolith is recognized as being medium-grained, weakly porphyritic with hornblende crystals up to 2 mm long<br>- the medium-grained andesite dykes differ from the fine-grained andesite dykes in that |

KERR PROJECT D.D.HOLE K-88-18

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | they are an earlier intrusive stage, hence have been sheared and are more altered, and in places are cut by the fine-grained andesite dykes at a later date. The fine-grained dykes are relatively fresh, unsheared, with 1 mm to 1 cm chilled contacts, minor chloritization and sericitization<br>- foliated at 40 deg to C.A. |
| 173.35 | 180.90 | 7.55 | FINE-GRAINED ANDESITE DYKE<br>- medium to dark green moderate chloritization<br>- 3 to 5% quartz-carbonate-chlorite-ankerite veins<br>- < 1% pyrite veins at 20 to 90 deg to C.A.<br>- upper contact at 85 deg, lower contact at 85 deg to C.A.<br>- generally, around quartz veining there is bleaching of the andesite dyke |
| 180.90 | 187.10 | 6.20 | SERICITE-QUARTZ-PYRITE SCHIST<br>- overall light to medium grey with irregular, wavy brighter and darker bands of sericite, sulphides, and minor chlorite and quartz bands<br>- possibly a sheared, altered, medium-grained andesite dyke, however - much more intensely altered than in section 169.9 to 173.35<br>- chlorite spots, may be interpreted to be relic hornblende<br>- silicification forms patches<br>- approximately 15% disseminated and stringer pyrite<br>- traces of epidote |
| 187.10 | 188.70 | 1.60 | ANDESITIC TO MAFIC DYKE<br>- medium to dark green to light grey-green at lower contact where dyke is bleached<br>- abundant chlorite, minor sericite, < 1% pyrite<br>- upper contact at 40 deg, lower contact at 80 deg to C.A.<br>- dyke is slightly magnetic, suggesting composition is probably mafic |
| 188.70 | 191.80 | 3.10 | MEDIUM-GRAINED ANDESITE DYKE<br>- as in 169.9 to 173.35 m<br>- intensely sheared and sericitized, however, relic medium-grained andesitic texture is evident |

KERR PROJECT D.D.HOLE K-88-18

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - foliated at 15 deg to C.A.<br>- medium to dark grey to green colour<br>- 10 to 15% pyrite, 5 to 10% silicified patches |
| 191.80 | 192.25 | 0.45 | PORPHYRITIC ANDESITE DYKE<br>- medium limy green colour, slight foliation developed at 60 deg to C.A., gradational upper and lower contacts<br>- possibly less sheared and altered equivalent of rock above and below |
| 192.25 | 196.45 | 4.20 | SHEARED MEDIUM-GRAINED ANDESITE DYKE / SERICITE SCHIST<br>- as in section 188.7 to 191.8 |
| 196.45 | 197.00 | 0.55 | FINE-GRAINED ANDESITE DYKE<br>- bleached light to medium grey green<br>- as in section 187.1 to 188.7 m<br>- upper contact at 65 deg, lower contact at 55 deg |
| 197.00 | 199.60 | 2.60 | SHEARED MEDIUM-GRAINED ANDESITE DYKE / SERICITE SCHIST<br>- as in 188.7 to 191.8 and 192.25 to 196.45 |
| 199.60 | 200.50 | 0.90 | MEDIUM-GRAINED PORPHYRITIC ANDESITE DYKE<br>- as in 191.8 to 192.25<br>- slight foliation developed at 60 deg to C.A.<br>- gradational upper and lower contacts<br>- appears to be less sheared and altered equivalent of overlying and underlying rock |
| 200.50 | 210.50 | 10.00 | SHEARED MEDIUM-GRAINED ANDESITE DYKE<br>- as in sections 188.7 to 191.8, 192.25 to 196.45, however, narrow sections of fresh, medium-grained, slightly porphyritic andesite dyke have been included in this section<br>- fresh medium-grained dyke occurs at<br>206.9 to 207.45 m<br>207.72 to 208.0 m<br>208.75 to 209.15 m<br>- the section of sheared material contains an increased amount of silica veins and blebs, up to 10 to 15% |

KERR PROJECT D.D.HOLE K-88-18

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 210.50 | 213.50 | 3.00 | MAFIC DYKE<br>- dark green to brownish, homogeneous, fine-grained with 2% 1-5 mm calcite/dolomite amygdules<br>- slightly magnetic, < 1% very fine-grained pyrite<br>- at 211.05 m the core is pulverized to a dark grey flour - small fault zone<br>- fault zone is approximately .70 m wide<br>- upper contact is quite sharp at 90 deg to C.A.<br>- lower contact has a 10 cm bleached chill margin and is at 60 deg to C.A. |
| 213.50 | 218.15 | 4.65 | SHEARED MEDIUM-GRAINED ANDESITE DYKE<br>- as in 200.5 to 210.5 m with sections of fresh medium-grained andesite dyke at<br>215.03 to 215.3 m<br>216.95 to 217.36 m<br>- from 213.5 to 214.5, 10% silica, 15-18% pyrite<br>- remainder is intensely sericitized |
| 218.15 | 229.10 | 10.95 | FINE-GRAINED ANDESITE DYKE<br>- homogeneous medium grey colour<br>- 10 cm chilled contact, very fine-grained greenish at upper and lower contact<br>- core of dyke is coarser grained than previously observed dykes - homogeneous grain size of .5 mm with exception of 228.15 to 229.10 where dyke has been bleached and altered around quartz veining<br>- upper contact at 50 deg, lower contact at 25 deg to C.A. |
| 229.10 | 255.42 | 26.32 | SHEARED ALTERED ANDESITE DYKE / SERICITE SCHIST<br>- as in previous sections, no unaltered medium-grained dyke visible<br>- intensely sericitized, 2 to 8% silica, 10 to 25% pyrite<br>- anhydrite vein 1 cm wide at 246.5 m<br>- well foliated at 50 deg to C.A.<br>- intensely sericitized, moderate chloritization<br><br>E.O.H. |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 12:37:32 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8818 | 10229.1 | 9599.5 | 1468.8 | 60 | 60 | 255.42 | | | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 3.05 | 3.05 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 3.05 | 6.0 | 2.95 | 25 | SRCT SCHT | | F-MG | 2 | 1 | 60 | 5 | 3 | | .5 | | | | 95 | 25 | .2 | | .5 | | | |
| 6.0 | 9.0 | 3.0 | 34 | SRCT SCHT | | F-MG | 2 | 2 | 65 | 3 | 5 | | .1 | | | | 95 | 20 | .1 | | .5 | | | |
| 9.0 | 12.0 | 3.0 | 37 | SRCT SCHT | | MG | 3 | 3 | 60 | 1 | 10 | | 2 | | | | 95 | 18 | .2 | | .2 | | | |
| 12.0 | 15.0 | 3.0 | 39 | SRCT SCHT | | MG | 3 | 5 | 60 | | 10 | | 2 | | | | 95 | 15 | .1 | | .2 | | | |
| 15.0 | 18.0 | 3.0 | 41 | SRCT SCHT | | MG | 2 | 3 | 60 | | 15 | | 2 | | | | 95 | 15 | .1 | | .3 | | | |
| 18.0 | 21.0 | 3.0 | 37 | SRCT SCHT | | MG | 3 | 3 | 60 | | 10 | | 3 | | | | 95 | 15 | .1 | | .1 | | | |
| 21.0 | 24.0 | 3.0 | 39 | SRCT SCHT | | MG | 10 | 5 | 55 | | 5 | | 3 | | | | 100 | 18 | .2 | | 1 | | | |
| 24.0 | 26.6 | 2.6 | 31 | SRCT SCHT | | MG | 8 | 8 | 60 | | 5 | | 2 | | | | 100 | 20 | .1 | | 1 | | | |
| 26.6 | 29.6 | 3.0 | 19 | FAULT SRCT SCHT | | FG | 10 | 5 | 60 | 5 | 3 | | 1 | | | | 100 | 15 | | | .5 | | | |
| 29.6 | 32.6 | 3.0 | 20 | FAULT SRCT SCHT | | FG | 15 | 5 | 59 | 5 | 3 | | | | | | 100 | 12 | | | 1 | | | |
| 32.6 | 35.4 | 2.8 | 19 | FAULT SRCT SCHT | | FG | 10 | 5 | 60 | 5 | 5 | | | | | | 100 | 12 | | | 1 | | | |
| 35.4 | 38.8 | 3.4 | 32 | SRCT SCHT | | MG | 10 | 3 | 55 | .5 | 10 | | | | | | 95 | 18 | .5 | | 1 | .1 | | |
| 38.8 | 40.8 | 2.0 | 27 | FAULT SRCT SCHT | | F-MG | 5 | 2 | 70 | 1 | 8 | | | | | | 100 | 15 | .5 | | 2 | | | |
| 40.8 | 42.8 | 2.0 | 24 | FAULT SRCT SCHT | | F-MG | 8 | 5 | 40 | 5 | 10 | | | | | | 100 | 20 | .5 | | 3 | | | |
| 42.8 | 45.4 | 2.6 | 26 | FAULT SRCT SCHT | | F-MG | 18 | 5 | 40 | | 3 | | | | | | 100 | 18 | .8 | | 2 | .1 | | |
| 45.4 | 48.0 | 2.6 | 34 | SILC STWK | | F-MG | 15 | 5 | 40 | | 15 | | 1 | | | | 100 | 20 | 1 | | 1 | | | |
| 48.0 | 51.0 | 3.0 | 39 | SILC STWK | | F-MG | 12 | 10 | 35 | 2 | 20 | .5 | | | | | 95 | 18 | 1 | | 2 | | | |
| 51.0 | 54.0 | 3.0 | 31 | SILC STWK | | F-MG | 20 | 5 | 40 | | 10 | .1 | | | | | 100 | 20 | 1 | | 2 | | | |
| 54.0 | 57.0 | 3.0 | 30 | SILC STWK | | F-MG | 15 | 5 | 40 | | 15 | | .5 | | | | 100 | 18 | 1.5 | | 1.5 | | | |
| 57.0 | 60.0 | 3.0 | 42 | SILC STWK | | F-MG | 15 | 5 | 40 | | 5 | | 1 | | | | 100 | 28 | 2 | | 1 | .1 | | |
| 60.0 | 63.0 | 3.0 | 47 | SILC STWK | | F-MG | 15 | 5 | 40 | | 5 | | 1 | | | | 100 | 25 | 1.5 | | 1.5 | | | |
| 63.0 | 66.0 | 3.0 | 47 | SILC STWK | | F-MG | 40 | 5 | 25 | | | | | | | | 100 | 25 | 3 | | 2 | | | |
| 66.0 | 68.0 | 2.0 | 43 | SILC STWK | | F-MG | 60 | | 5 | | | | | | | | 100 | 25 | 5 | | 2 | | | |
| 68.0 | 70.0 | 2.0 | 48 | SILC STWK | | F-MG | 60 | | 5 | | | | | | | | 100 | 25 | 3 | | 2 | | | |
| 70.0 | 72.0 | 2.0 | 43 | SILC STWK | | F-MG | 60 | | 5 | | | | | | | | 100 | 25 | 3 | | 2 | | | |
| 72.0 | 74.0 | 2.0 | 46 | SILC STWK | | F-MG | 65 | | 5 | | | | | | | | 100 | 20 | 2 | | 2 | | | |
| 74.0 | 75.85 | 1.85 | 18 | SILC STWK | | F-MG | 65 | | 5 | | | | | | | | 100 | 20 | 2 | | 2 | | | |
| 75.85 | 77.7 | 1.85 | 38 | ANDS DYKE | | FG | | 5 | 20 | | 10 | | 3 | | | | 40 | 1 | | | | .1 | | |
| 77.7 | 80.7 | 3.0 | 37 | SRCT SCHT | | F-MG | | 5 | 35 | 3 | 15 | | | | | | 70 | 10 | .2 | | .1 | | | |
| 80.7 | 83.7 | 3.0 | 25 | SRCT SCHT | | F-MG | 3 | 3 | 50 | 1 | 15 | | | | | | 90 | 12 | 1 | | .5 | | | |
| 83.7 | 85.7 | 2.0 | 10 | SRCT SCHT | | F-MG | 1 | 1 | 60 | 3 | 10 | | | | | | 90 | 10 | .2 | | .3 | | | |
| 85.7 | 87.78 | 2.08 | 42 | SRCT SCHT | | F-MG | 1 | 1 | 50 | 1 | 10 | | 1 | | | | 70 | 5 | | | .5 | | | |
| 87.78 | 89.28 | 1.5 | 38 | ANDS DYKE | | F-MG | | 1 | 15 | | 10 | | 1 | | | | 30 | .5 | | | | | | |
| 89.28 | 91.9 | 2.62 | 33 | SRCT SCHT | | F-MG | 1 | 1 | 50 | 1 | 15 | | | | | | 80 | 12 | | | .5 | | | |
| 91.9 | 95.0 | 3.1 | 35 | ANDS DYKE | | MG | 1 | .5 | 15 | 1 | 15 | .2 | | | | | 35 | 3 | | | | | | |
| 95.0 | 98.0 | 3.0 | 35 | ANDS DYKE | | MG | 1 | .5 | 20 | 1 | 15 | .2 | | | | | 40 | 3 | .1 | | .1 | | | |
| 98.0 | 101.0 | 3.0 | 32 | ANDS DYKE | | MG | | 1 | 20 | 1 | 20 | .5 | | | | | 45 | 5 | | | | | | |
| 101.0 | 103.25 | 2.25 | 30 | ANDS DYKE | | MG | | .5 | 10 | 2 | 25 | .2 | | | | | 40 | 5 | .1 | | .1 | | | |
| 103.25 | 106.0 | 2.75 | 34 | BREC DCIT TUFF | | F-MG | 10 | 2 | 25 | | 35 | | | | | | 80 | 10 | .3 | | .5 | .1 | | |
| 106.0 | 109.0 | 3.0 | 43 | BREC DCIT TUFF | | F-MG | 10 | 5 | 20 | 1 | 35 | | | | | | 95 | 12 | 2 | | 1 | | | |
| 109.0 | 111.9 | 2.9 | 40 | BREC DCIT TUFF | | F-MG | 8 | 2 | 30 | | 25 | | | | | | 80 | 8 | 1 | | .8 | | | |
| 111.9 | 114.9 | 3.0 | 23 | FAULT ZONE | | F-MG | 2 | 1 | 60 | 1 | 8 | | | | | | 90 | 12 | | | | | | |
| 114.9 | 117.6 | 2.7 | 22 | FAULT ZONE | | F-MG | 2 | 1 | 60 | 1 | 10 | | | | | | 90 | 10 | | | | | | |
| 117.6 | 120.0 | 2.4 | 39 | SILC STWK | | F-MG | 55 | | 10 | | | | | | | | 100 | 30 | 2 | | 3 | | .2 | |
| 120.0 | 122.0 | 2.0 | 36 | SILC STWK | | F-MG | 55 | | 10 | | | | | | | | 100 | 30 | 2 | | 3 | | .1 | |
| 122.0 | 124.0 | 2.0 | 29 | SILC STWK | | F-MG | 50 | | 15 | | | | | | | | 100 | 30 | 2 | | 2 | | .1 | |
| 124.0 | 126 | 2.0 | 40 | SILC STWK | | F-MG | 50 | | 15 | | | | | | | | 100 | 28 | 1 | | 1 | | .1 | |
| 126.0 | 128 | 2.0 | 37 | SILC STWK | | F-MG | 50 | | 15 | | | | | | | | 100 | 25 | 5 | | 2 | | .1 | |
| 128.0 | 130 | 2.0 | 32 | SILC STWK | | F-MG | 50 | | 15 | | | | | | | | 100 | 25 | 2 | | 1 | | .1 | |
| 130.0 | 132 | 2.0 | 33 | SILC STWK | | F-MG | 40 | | 25 | | | | | | | | 100 | 25 | 1 | | 2 | | | |
| 132.0 | 134 | 2.0 | 34 | SILC STWK | | F-MG | 45 | | 25 | | | | | | | | 100 | 20 | 3 | | 1 | | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8818 | 10229.1 | 9599.5 | 1468.8 | 60 | 60 | 255.42 | | | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 134.0 | 136 | 2.0 | 31 | SILC STWK | | F-MG | 45 | | 25 | | | | | | | | 100 | 25 | 1 | | 1 | | | |
| 136.0 | 138 | 2.0 | 37 | SILC STWK | | F-MG | 35 | | 35 | | | | | | | | 100 | 20 | 1 | | .5 | | | |
| 138.0 | 140 | 2.0 | 36 | SILC STWK | | F-MG | 40 | | 35 | | | | | | | | 100 | 20 | 1 | | .5 | | | |
| 140.0 | 142 | 2.0 | 47 | SILC STWK | | F-MG | 30 | | 30 | | 10 | | | | | | 100 | 18 | 5 | | 2 | | | |
| 142.0 | 144 | 2.0 | 50 | SILC STWK | | F-MG | 40 | | 25 | | 5 | | | | | | 100 | 20 | 6 | | 1 | | | |
| 144.0 | 145.85 | 1.85 | 44 | SILC STWK | | F-MG | 30 | | 40 | | | | | | | | 100 | 22 | 3 | | 1 | | | |
| 145.85 | 146.27 | .42 | 46 | ANDS DYKE | | FG | | 1 | 10 | | 5 | | 1 | | | | 20 | .1 | | | | | | |
| 146.27 | 147.27 | 1.0 | 36 | SILC STWK | | FG | 35 | | 40 | | 2 | | | | | | 100 | 18 | 2 | | .5 | | | |
| 147.27 | 147.55 | .28 | 48 | ANDS DYKE | | FG | | 5 | 15 | | 15 | | | | | | 35 | .2 | | | | | | |
| 147.55 | 150.0 | 2.45 | 41 | SILC STWK | | FG | 25 | | 40 | | 1 | | | | | | 100 | 30 | 1 | | .5 | | | |
| 150.0 | 152 | 2.0 | 46 | SILC STWK | | FG | 25 | | 45 | | 1 | | | | | | 100 | 23 | 3 | | .2 | | | |
| 152.0 | 154 | 2.0 | 48 | SILC STWK | | FG | 35 | | 35 | | 2 | | | | | | 100 | 25 | 1 | | .5 | | | |
| 154.0 | 156 | 2.0 | 43 | SILC STWK | | FG | 30 | | 40 | | 1 | | | | | | 100 | 25 | 2 | | .5 | | | |
| 156.0 | 158 | 2.0 | 51 | SILC STWK | | FG | 40 | | 35 | | | | | | | | 100 | 25 | 3 | | .5 | | | |
| 158.0 | 160 | 2.0 | 47 | SILC STWK | | FG | 40 | | 35 | | | | | | | | 100 | 25 | 3 | | .5 | | | |
| 160.0 | 162 | 2.0 | 49 | SILC STWK | | FG | 35 | | 45 | | 2 | | | | | | 100 | 20 | 2 | | .5 | | | |
| 162.0 | 164 | 2.0 | 42 | SILC STWK | | FG | 25 | | 45 | | 5 | | | | | | 100 | 20 | 1 | | .5 | | | |
| 164.0 | 166 | 2.0 | 42 | SILC STWK | | FG | 15 | | 55 | | 5 | | | | | | 100 | 25 | .8 | | .2 | | | |
| 166.0 | 168 | 2.0 | 43 | SILC STWK | | FG | 15 | | 60 | | 5 | | | | | | 100 | 15 | .5 | | .2 | | | |
| 168.0 | 169.9 | 1.9 | 33 | SILC STWK | | FG | 25 | | 45 | | 10 | | | | | | 100 | 15 | .8 | | .5 | | | |
| 169.9 | 172 | 2.1 | 32 | ANDS DYKE | | F-MG | | 10 | 10 | 1 | 40 | | 3 | | | | 65 | 2 | | | | | | |
| 172.0 | 173.35 | 1.35 | 30 | ANDS DYKE | | F-MG | | 5 | 30 | 1 | 30 | | 3 | | | | 65 | 3 | | | 1 | | | |
| 173.35 | 176 | 2.65 | 45 | ANDS DYKE | | FG | | 5 | 5 | 1 | 30 | | 3 | | | | 40 | 1 | | | | | | |
| 176.0 | 178 | 2.0 | 56 | ANDS DYKE | | FG | | .2 | 5 | | 30 | | .2 | | | | 40 | 1 | | | | | | |
| 178.0 | 180.9 | 2.9 | 55 | ANDS DYKE | | FG | | 5 | 15 | | 25 | | 5 | | | | 45 | 1 | | | | | | |
| 180.9 | 183.9 | 3.0 | 36 | SRCT SCHT | | FG | 15 | 2 | 60 | | 5 | | 1 | | | | 100 | 15 | | | | | | |
| 183.9 | 187.1 | 3.2 | 30 | SRCT SCHT | | FG | 15 | 3 | 60 | | 5 | | 1 | | | | 100 | 15 | | | | | | |
| 187.1 | 188.7 | 1.6 | 40 | ANDS MAFIC DYKE | | FG | | .5 | 15 | 1 | 20 | 1 | .5 | | | | 40 | 1 | | | | | | |
| 188.7 | 191.8 | 3.1 | 43 | ANDS DYKE | | MG | 15 | 5 | | 2 | 8 | | 3 | | | | 95 | 15 | | | .5 | | | |
| 191.8 | 192.25 | .45 | 33 | PRPH ANDS DYKE | | MG | | | 15 | 2 | 10 | | | | | | 30 | 1 | | | | | | |
| 192.25 | 194.25 | 2.0 | 38 | ANDS DYKE SCHT | | MG | 15 | 3 | 55 | | 5 | 3 | 2 | | | | 100 | 15 | .5 | | .2 | | | |
| 194.25 | 196.45 | 2.2 | 40 | ANDS DYKE SCHT | | MG | 15 | 3 | 60 | | 3 | 2 | 2 | | | | 100 | 12 | .1 | | .2 | | | |
| 196.45 | 197.0 | .55 | 50 | ANDS DYKE | | FG | | | 5 | 1 | 15 | | 1 | | | | 20 | 1 | | | | | | |
| 197.0 | 199.6 | 2.6 | 20 | ANDS DYKE SCHT | | MG | 15 | 1 | 60 | | 5 | | 1 | | | | 100 | 12 | | | .5 | | | |
| 199.6 | 200.5 | .9 | 44 | PRPH ANDS DYKE | | MG | | 5 | 15 | | 25 | | 2 | | | | 50 | 2 | | | | | | |
| 200.5 | 202.5 | 2.0 | 48 | ANDS DYKE | | MG | 10 | 2 | 25 | | 20 | | 1 | | | | 85 | 18 | | | | | | |
| 202.5 | 204.5 | 2.0 | 30 | ANDS DYKE | | MG | 17 | 2 | 50 | | 10 | | 1 | | | | 90 | 15 | .1 | | | | | |
| 204.5 | 206.5 | 2.0 | 45 | ANDS DYKE | | MG | 10 | 2 | 40 | | 20 | | 1 | | | | 95 | 25 | | | | | | |
| 206.5 | 208.5 | 2.0 | 30 | ANDS DYKE | | MG | 8 | 2 | 40 | | 25 | 1 | 1 | | | | 90 | 8 | | | | | | |
| 208.5 | 210.5 | 2.0 | 30 | ANDS DYKE | | MG | 5 | 2 | 40 | | 25 | 1 | 1 | | | | 90 | 8 | | | | | | |
| 210.5 | 213.5 | 3.0 | 13 | MAFIC DYKE | | MG | | 1 | 5 | 1 | 60 | | 3 | | | | 70 | 1 | | | | | | |
| 213.5 | 216.5 | 3.0 | 32 | ANDS DYKE | | MG | 5 | 1 | 50 | | 10 | 2 | 1 | | | | 90 | 20 | | | | | | |
| 216.5 | 218.65 | 2.15 | 29 | ANDS DYKE | | MG | 3 | 1 | 50 | | 15 | 2 | 2 | | | | 90 | 18 | | | | | | |
| 218.65 | 221.0 | 2.35 | 19 | ANDS DYKE | | FG | | 1 | 20 | | 20 | | 5 | | | | 50 | 1 | | | | | | |
| 221.0 | 224.0 | 3.0 | 43 | ANDS DYKE | | FG | | 3 | 20 | | 20 | | 1 | | | | 50 | 1 | | | | | | |
| 224.0 | 227.0 | 3.0 | 40 | ANDS DYKE | | FG | | 5 | 20 | | 20 | | 2 | | | | 50 | 1 | | | | | | |
| 227.0 | 229.1 | 2.1 | 38 | ANDS DYKE | | FG | | 10 | 20 | | 30 | | 5 | | | | 70 | 1 | | | | | | |
| 229.1 | 232.0 | 2.9 | 45 | SRCT SCHT ANDS | | F-MG | 5 | 2 | 60 | 1 | 8 | .1 | 1 | | | | 100 | 20 | | | | | | |
| 232.0 | 235.0 | 3.0 | 47 | SRCT SCHT ANDS | | F-MG | 8 | 2 | 55 | | 5 | .5 | | | | | 100 | 25 | | | | | | |
| 235.0 | 238.0 | 3.0 | 41 | SRCT SCHT ANDS | | F-MG | 5 | 2 | 65 | | 3 | 2 | | | | | 100 | 20 | | | .1 | | | |
| 238.0 | 241.0 | 3.0 | 46 | SRCT SCHT ANDS | | F-MG | 10 | 2 | 55 | | 5 | 2 | | | | | 100 | 25 | | | .1 | | | |
| 241.0 | 244.0 | 3.0 | 47 | SRCT SCHT ANDS | | F-MG | 8 | 3 | 60 | | 5 | 2 | 1 | | | | 100 | 20 | | | .1 | | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8818 | 10229.1 | 9599.5 | 1468.8 | 60 | 60 | 255.42 | | | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 244.0 | 247.0 | 3.0 | 48 | SRCT SCHT ANDS | | F-MG | 8 | 1 | 55 | | 5 | 2 | 1 | | | | 100 | 25 | | | .1 | | | |
| 247.0 | 250.0 | 3.0 | 57 | SRCT SCHT ANDS | | F-MG | 8 | 1 | 65 | | 5 | 2 | | | | | 100 | 15 | | | .1 | | | |
| 250.0 | 253.0 | 3.0 | 49 | SRCT SCHT ANDS | | F-MG | 8 | 1 | 60 | | 5 | 1 | | | | | 100 | 20 | | | .1 | | | |
| 253.0 | 255.42 | 2.42 | 46 | SRCT SCHT ANDS | | F-MG | 8 | 2 | 60 | | 5 | 1 | | | | | 100 | 18 | | | .1 | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 09:35:37 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8818 | 10229.1 | 9599.5 | 1468.8 | 60 | 60 | 255.42 | | | |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 3.05 | | 3.05 | | | | | | | | | | | | |
| 3.05 | 6.0 | 3144 | 2.95 | 2.49 | 770 | | 0.6 | | 4077 | 80 | 6.86 | 131 | 43 | | |
| 6.0 | 9.0 | 3145 | 3.0 | 2.99 | 1280 | | 0.1 | | 2976 | 67 | 7.43 | 39 | 440 | | |
| 9.0 | 12.0 | 3146 | 3.0 | 2.92 | 140 | | 0.1 | | 2146 | 98 | 6.33 | 17 | 411 | | |
| 12.0 | 15.0 | 3147 | 3.0 | 2.93 | 60 | | 0.1 | | 2401 | 157 | 5.61 | 15 | 510 | | |
| 15.0 | 18.0 | 3148 | 3.0 | 2.96 | 100 | | 0.1 | | 3120 | 116 | 5.43 | 14 | 503 | | |
| 18.0 | 21.0 | 3149 | 3.0 | 2.99 | 110 | | 0.1 | | 2645 | 94 | 5.11 | 14 | 655 | | |
| 21.0 | 24.0 | 3150 | 3.0 | 2.96 | 240 | | 0.1 | | 5243 | 68 | 5.68 | 13 | 520 | | |
| 24.0 | 26.6 | 3151 | 2.6 | 1.73 | 190 | | 0.1 | | 6271 | 89 | 6.39 | 15 | 385 | | |
| 26.6 | 29.6 | 3152 | 3.0 | .43 | 230 | | 0.1 | | 2462 | 59 | 3.92 | 25 | 147 | | |
| 29.6 | 32.6 | 3153 | 3.0 | 1.34 | 170 | | 1.1 | | 6406 | 73 | 5.26 | 96 | 177 | | |
| 32.6 | 35.4 | 3154 | 2.8 | 1.27 | 190 | | 1.1 | | 5197 | 57 | 5.60 | 87 | 95 | | |
| 35.4 | 38.8 | 3155 | 3.4 | 3.3 | 140 | | 0.1 | | 4558 | 119 | 4.79 | 18 | 490 | | |
| 38.8 | 40.8 | 3156 | 2.0 | 2.07 | 70 | | 0.1 | | 3019 | 105 | 4.62 | 110 | 427 | | |
| 40.8 | 42.8 | 3157 | 2.0 | 1.69 | 120 | | 0.1 | | 5396 | 192 | 5.11 | 237 | 274 | | |
| 42.8 | 45.4 | 3158 | 2.6 | 2.06 | 0 | | 1.1 | | 10668 | 138 | 6.53 | 20 | 170 | | |
| 45.4 | 48.0 | 3159 | 2.6 | 2.57 | 580 | | 0.1 | | 7639 | 146 | 8.68 | 21 | 555 | | |
| 48.0 | 51.0 | 3160 | 3.0 | 2.91 | 340 | | 0.6 | | 9657 | 123 | 5.76 | 19 | 602 | | |
| 51.0 | 54.0 | 3161 | 3.0 | 2.66 | 760 | | 0.4 | | 9819 | 121 | 5.83 | 18 | 364 | | |
| 54.0 | 57.0 | 3162 | 3.0 | 2.63 | 220 | | 1.1 | | 8376 | 80 | 6.80 | 25 | 300 | | |
| 57.0 | 60.0 | 3163 | 3.0 | 2.97 | 360 | | 0.6 | | 10046 | 153 | 6.34 | 19 | 563 | | |
| 60.0 | 63.0 | 3164 | 3.0 | 3.04 | 630 | | 0.4 | | 7995 | 103 | 6.51 | 15 | 351 | | |
| 63.0 | 66.0 | 3165 | 3.0 | 2.98 | 750 | | 3.7 | | 15452 | 59 | 7.00 | 624 | 251 | | |
| 66.0 | 68.0 | 3166 | 2.0 | 1.92 | 0 | | 4.9 | | 20000 | 124 | 10.00 | 1000 | 31 | | |
| 68.0 | 70.0 | 3167 | 2.0 | 1.96 | 650 | | 0.6 | | 20000 | 44 | 7054 | 207 | 32 | | |
| 70.0 | 72.0 | 3168 | 2.0 | 1.94 | 585 | | 2.7 | | 20222 | 56 | 8037 | 888 | 32 | | |
| 72.0 | 74.0 | 3169 | 2.0 | 1.92 | 370 | | 2.5 | | 19083 | 42 | 10.00 | 505 | 69 | | |
| 74.0 | 75.85 | 3170 | 1.85 | 1.82 | 470 | | 2.1 | | 20000 | 31 | 9.00 | 143 | 44 | | |
| 75.85 | 77.7 | 3171 | 1.85 | 1.85 | 70 | | 0.1 | | 522 | 187 | 5.26 | 38 | 1067 | | |
| 77.7 | 80.7 | 3172 | 3.0 | 2.95 | 160 | | 0.1 | | 2808 | 140 | 5.53 | 37 | 313 | | |
| 80.7 | 83.7 | 3173 | 3.0 | 2.88 | 150 | | 0.1 | | 3942 | 148 | 5.68 | 12 | 353 | | |
| 83.7 | 85.7 | 3174 | 2.0 | 1.76 | 160 | | 0.1 | | 2229 | 146 | 4.94 | 32 | 591 | | |
| 85.7 | 87.78 | 3175 | 2.08 | 2.1 | 230 | | 0.1 | | 1891 | 77 | 3.01 | 26 | 561 | | |
| 87.78 | 89.28 | 3176 | 1.5 | 1.5 | 260 | | 0.1 | | 1402 | 163 | 4.68 | 22 | 1602 | | |
| 89.28 | 91.9 | 3177 | 2.62 | 2.59 | 140 | | 0.1 | | 4976 | 44 | 6.27 | 68 | 75 | | |
| 91.9 | 95.0 | 3178 | 3.1 | 3.1 | 175 | | 0.1 | | 3729 | 230 | 6.86 | 35 | 1824 | | |
| 95.0 | 98.0 | 3179 | 3.0 | 3.07 | 250 | | 0.1 | | 5390 | 179 | 5.74 | 43 | 897 | | |
| 98.0 | 101.0 | 3180 | 3.0 | 3.0 | 0 | | 0.1 | | 2608 | 277 | 6.19 | 19 | 1531 | | |
| 101.0 | 103.25 | 3181 | 2.25 | 2.08 | 160 | | 0.1 | | 3407 | 181 | 4.51 | 38 | 591 | | |
| 103.25 | 106.0 | 3182 | 2.75 | 2.96 | 690 | | 2.5 | | 18689 | 237 | 6.68 | 44 | 532 | | |
| 106.0 | 109.0 | 3183 | 3.0 | 2.91 | 440 | | 0.1 | | 9004 | 184 | 5.67 | 41 | 657 | | |
| 109.0 | 111.9 | 3184 | 2.9 | 2.75 | 700 | | 2.8 | | 18311 | 217 | 7.58 | 47 | 455 | | |
| 111.9 | 114.9 | 3185 | 3.0 | 2.0 | 60 | | 0.1 | | 1532 | 358 | 6.24 | 31 | 1360 | | |
| 114.9 | 117.6 | 3186 | 2.7 | 1.74 | 100 | | 0.1 | | 1433 | 431 | 4.34 | 39 | 1099 | | |
| 117.6 | 120.0 | 3187 | 2.4 | 2.23 | 340 | | 6.2 | | 20000 | 49 | 6.39 | 801 | 48 | | |
| 120.0 | 122.0 | 3188 | 2.0 | 1.92 | 780 | | 1.5 | | 16878 | 98 | 7.38 | 1000 | 19 | | |
| 122.0 | 124.0 | 3189 | 2.0 | 1.56 | 0 | | 3.2 | | 15390 | 35 | 7.99 | 1000 | 35 | | |
| 124.0 | 126 | 3190 | 2.0 | 1.91 | 710 | | 2.3 | | 17662 | 41 | 6.44 | 224 | 41 | | |
| 126.0 | 128 | 3191 | 2.0 | 1.89 | 750 | | 2.3 | | 20000 | 75 | 7.10 | 285 | 32 | | |
| 128.0 | 130 | 3192 | 2.0 | 1.66 | 420 | | 2.3 | | 19793 | 36 | 8.22 | 391 | 19 | | |
| 130.0 | 132 | 3193 | 2.0 | 2.0 | 540 | | 0.9 | | 16286 | 24 | 7.12 | 100 | 38 | | |
| 132.0 | 134 | 3194 | 2.0 | 1.88 | 990 | | 1.5 | | 16319 | 28 | 7.53 | 57 | 32 | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | |
|---|---|---|---|---|---|---|---|---|---|
| 8818 | 10229.1 | 9599.5 | 1468.8 | 60 | 60 | 255.42 | | | #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 134.0 | 136 | 3195 | 2.0 | 1.71 | 1320 | | 2.8 | | 8363 | 107 | 8.32 | 307 | 21 | | |
| 136.0 | 138 | 3196 | 2.0 | 1.91 | 630 | | 0.9 | | 5958 | 23 | 7.01 | 49 | 71 | | |
| 138.0 | 140 | 3197 | 2.0 | 1.94 | 1150 | | 1.1 | | 10244 | 22 | 6.90 | 29 | 123 | | |
| 140.0 | 142 | 3198 | 2.0 | 1.97 | 1460 | | 2.3 | | 20000 | 83 | 6.95 | 26 | 699 | | |
| 142.0 | 144 | 3199 | 2.0 | 2.02 | 930 | | 5.7 | | 20000 | 198 | 9.44 | 349 | 178 | | |
| 144.0 | 145.85 | 3200 | 1.85 | 1.85 | 770 | | 1.1 | | 13947 | 62 | 7.96 | 36 | 286 | | |
| 145.85 | 146.27 | 3201 | .42 | .42 | 5 | | 0.1 | | 547 | 366 | 6.87 | 43 | 1170 | | |
| 146.27 | 147.27 | 3202 | 1.0 | .99 | 460 | | 0.1 | | 11350 | 14 | 9.21 | 16 | 425 | | |
| 147.27 | 147.55 | 3203 | .28 | .28 | 0 | | 0.1 | | 3167 | 272 | 5.65 | 58 | 1163 | | |
| 147.55 | 150.0 | 3204 | 2.45 | 2.46 | 0 | | 0.5 | | 8063 | 31 | 7.50 | 134 | 106 | | |
| 150.0 | 152 | 3205 | 2.0 | 2.0 | 360 | | 2.3 | | 16135 | 45 | 7.94 | 359 | 26 | | |
| 152.0 | 154 | 3206 | 2.0 | 2.0 | 340 | | 0.1 | | 8909 | 7 | 7.27 | 15 | 25 | | |
| 154.0 | 156 | 3207 | 2.0 | 1.98 | 415 | | 0.5 | | 10232 | 24 | 7.11 | 9 | 91 | | |
| 156.0 | 158 | 3208 | 2.0 | 1.95 | 650 | | 1.5 | | 14796 | 33 | 8.70 | 20 | 73 | | |
| 158.0 | 160 | 3209 | 2.0 | 2.05 | 575 | | 2.1 | | 15697 | 27 | 8.50 | 12 | 280 | | |
| 160.0 | 162 | 3210 | 2.0 | 2.06 | 480 | | 1.5 | | 14180 | 43 | 7.56 | 11 | 499 | | |
| 162.0 | 164 | 3211 | 2.0 | 2.0 | 550 | | 1.3 | | 9989 | 55 | 6.66 | 44 | 146 | | |
| 164.0 | 166 | 3212 | 2.0 | 2.0 | 300 | | 0.1 | | 2925 | 15 | 7.07 | 107 | 291 | | |
| 166.0 | 168 | 3213 | 2.0 | 2.0 | 360 | | 0.1 | | 1667 | 20 | 5.74 | 26 | 232 | | |
| 168.0 | 169.9 | 3214 | 1.9 | 1.71 | 210 | | 0.1 | | 2413 | 26 | 4.47 | 10 | 131 | | |
| 169.9 | 172 | 3215 | 2.1 | 2.1 | 0 | | 0.1 | | 61 | 117 | 2.27 | 3 | 1087 | | |
| 172.0 | 173.35 | 3216 | 1.35 | 1.36 | 170 | | 0.1 | | 2044 | 70 | 5.42 | 30 | 650 | | |
| 173.35 | 176 | 3217 | 2.65 | 2.65 | 45 | | 0.1 | | 63 | 168 | 3.15 | 6 | 767 | | |
| 176.0 | 178 | 3218 | 2.0 | 1.98 | 35 | | 0.1 | | 15 | 111 | 1.61 | 3 | 433 | | |
| 178.0 | 180.9 | 3219 | 2.9 | 2.92 | 210 | | 0.1 | | 16 | 73 | 1.12 | 3 | 708 | | |
| 180.9 | 183.9 | 3220 | 3.0 | 2.95 | 160 | | 0.1 | | 1457 | 17 | 6.63 | 14 | 203 | | |
| 183.9 | 187.1 | 3221 | 3.2 | 3.2 | 115 | | 0.1 | | 766 | 6 | 5.61 | 15 | 237 | | |
| 187.1 | 188.7 | 3222 | 1.6 | 1.62 | 130 | | 0.1 | | 496 | 131 | 4.92 | 21 | 877 | | |
| 188.7 | 191.8 | 3223 | 3.1 | 2.9 | 375 | | 0.3 | | 3897 | 100 | 6.08 | 11 | 875 | | |
| 191.8 | 192.25 | 3224 | .45 | .45 | 80 | | 0.1 | | 210 | 856 | 6.40 | 23 | 3068 | | |
| 192.25 | 194.25 | 3225 | 2.0 | 1.95 | 310 | | 0.3 | | 4218 | 74 | 8.49 | 19 | 888 | | |
| 194.25 | 196.45 | 3226 | 2.2 | 2.32 | 240 | | 0.9 | | 4345 | 398 | 7.16 | 573 | 432 | | |
| 196.45 | 197.0 | 3227 | .55 | .55 | 0 | | 0.1 | | 138 | 122 | 4.33 | 47 | 1040 | | |
| 197.0 | 199.6 | 3228 | 2.6 | 2.15 | 185 | | 0.1 | | 2917 | 240 | 6.12 | 146 | 533 | | |
| 199.6 | 200.5 | 3229 | .9 | .91 | 145 | | 0.1 | | 684 | 285 | 7.14 | 26 | 2783 | | |
| 200.5 | 202.5 | 3230 | 2.0 | 1.94 | 660 | | 0.1 | | 3854 | 119 | 7.16 | 16 | 632 | | |
| 202.5 | 204.5 | 3231 | 2.0 | 1.93 | 590 | | 0.9 | | 4770 | 103 | 6.98 | 18 | 770 | | |
| 204.5 | 206.5 | 3232 | 2.0 | 1.92 | 410 | | 0.1 | | 4547 | 136 | 7.24 | 13 | 426 | | |
| 206.5 | 208.5 | 3233 | 2.0 | 1.95 | 20 | | 0.1 | | 2969 | 181 | 6.89 | 20 | 879 | | |
| 208.5 | 210.5 | 3234 | 2.0 | 1.88 | 340 | | 0.1 | | 3430 | 110 | 6.37 | 26 | 521 | | |
| 210.5 | 213.5 | 3235 | 3.0 | 2.51 | 50 | | 3.2 | | 216 | 122 | 4.69 | 26 | 718 | | |
| 213.5 | 216.5 | 3236 | 3.0 | 2.79 | 170 | | 0.1 | | 3341 | 51 | 5.64 | 15 | 570 | | |
| 216.5 | 218.65 | 3237 | 2.15 | 1.28 | 160 | | 0.1 | | 2478 | 120 | 6.08 | 21 | 457 | | |
| 218.65 | 221.0 | 3238 | 2.35 | 1.33 | 510 | | 0.1 | | 185 | 93 | 2.20 | 5 | 883 | | |
| 221.0 | 224.0 | 3239 | 3.0 | 3.06 | 20 | | 0.1 | | 37 | 120 | 2.41 | 3 | 676 | | |
| 224.0 | 227.0 | 3240 | 3.0 | 2.93 | 0 | | 0.1 | | 23 | 120 | 1.72 | 3 | 507 | | |
| 227.0 | 229.1 | 3241 | 2.1 | 2.01 | 30 | | 0.1 | | 22 | 150 | 2.43 | 4 | 992 | | |
| 229.1 | 232.0 | 3242 | 2.9 | 2.78 | 230 | | 0.9 | | 1784 | 27 | 7.75 | 40 | 187 | | |
| 232.0 | 235.0 | 3243 | 3.0 | 2.99 | 240 | | 3.2 | | 1364 | 7 | 8.30 | 20 | 159 | | |
| 235.0 | 238.0 | 3244 | 3.0 | 3.09 | 210 | | 3.8 | | 1260 | 5 | 5.64 | 20 | 92 | | |
| 238.0 | 241.0 | 3245 | 3.0 | 2.92 | 300 | | 0.4 | | 955 | 14 | 6.90 | 68 | 221 | | |
| 241.0 | 244.0 | 3246 | 3.0 | 2.78 | 230 | | 0.1 | | 1359 | 24 | 8.69 | 15 | 231 | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8818 | 10229.1 | 9599.5 | 1468.8 | 60 | 60 | 255.42 | | |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 244.0 | 247.0 | 3247 | 3.0 | 3.09 | 150 | | 0.1 | | 984 | 15 | 10.00 | 3 | 288 | | |
| 247.0 | 250.0 | 3248 | 3.0 | 3.07 | 90 | | 0.1 | | 662 | 5 | 9.60 | 4 | 76 | | |
| 250.0 | 253.0 | 3249 | 3.0 | 3.05 | 435 | | 0.1 | | 837 | 35 | 9.39 | 48 | 127 | | |
| 253.0 | 255.42 | 3250 | 2.42 | 2.42 | 290 | | 0.1 | | 965 | 12 | 9.80 | 3 | 231 | | |

#HOI

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1966 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-3149 | .23 |
| C88-3150 | .46 |
| C88-3151 | .55 |
| C88-3152 | .20 |
| C88-3153 | .52 |
| C88-3154 | .45 |
| C88-3155 | .40 |
| C88-3156 | .28 |
| C88-3157 | .48 |
| C88-3158 | .90 |
| C88-3159 | .64 |
| C88-3160 | .87 |
| C88-3161 | .86 |
| C88-3162 | .71 |
| C88-3163 | .86 |
| C88-3164 | .73 |
| C88-3165 | 1.25 |
| C88-3166 | 2.73 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
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Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-3167 | 1.69 |
| C88-3168 | 1.69 |
| C88-3169 | 1.50 |
| C88-3170 | 1.63 |
| C88-3171 | .03 |
| C88-3172 | .23 |
| C88-3173 | .31 |
| C88-3174 | .20 |
| C88-3175 | .15 |
| C88-3176 | .13 |
| C88-3177 | .39 |
| C88-3178 | .34 |
| C88-3179 | .50 |
| C88-3180 | .24 |
| C88-3181 | .31 |
| C88-3182 | 1.54 |
| C88-3183 | .93 |
| C88-3184 | 1.81 |
| C88-3185 | .14 |
| C88-3186 | .14 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-3187 | 2.47 |
| C88-3188 | 1.59 |
| C88-3189 | 1.45 |
| C88-3190 | 1.59 |
| C88-3191 | 2.08 |
| C88-3192 | 1.73 |
| C88-3193 | 1.52 |
| C88-3194 | 1.60 |
| C88-3195 | .77 |
| C88-3196 | .57 |
| C88-3197 | .96 |
| C88-3198 | 2.34 |
| C88-3199 | 2.75 |
| C88-3200 | 1.31 |
| C88-3201 | .04 |
| C88-3202 | 1.01 |
| C88-3203 | .31 |
| C88-3204 | .82 |
| C88-3205 | 1.34 |
| C88-3206 | .85 |
| DETECTION LIMIT | .01 |

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-3207 | .91 |
| C88-3208 | 1.34 |
| C88-3209 | 1.41 |
| C88-3210 | 1.32 |
| C88-3211 | .90 |
| C88-3212 | .28 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: 881006 PA — WESTERN CANADIAN — 

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-3144 | 0.6 | 0.45 | 131 | 770 | <3 | 5 | <3 | 0.15 | 1.2 | 14 | 90 | 4077 | 6.86 | 0.01 | 0.15 | 43 | 9 | 0.02 | 13 | 0.14 | 60 | <3 | <5 | <2 | 2 | 29 | <5 | <3 | 80 |
| C88-3145 | 0.1 | 1.02 | 39 | 1280 | <3 | 5 | 3 | 0.38 | 2.1 | 20 | 37 | 2976 | 7.43 | 0.01 | 0.88 | 440 | 8 | 0.02 | 7 | 0.19 | 39 | <3 | <5 | <2 | 3 | 22 | <5 | <3 | 67 |
| C88-3146 | 0.1 | 1.68 | 17 | 140 | <3 | 8 | 3 | 0.39 | 1.7 | 15 | 47 | 2146 | 6.33 | 0.01 | 1.56 | 411 | 6 | 0.02 | 7 | 0.22 | 37 | <3 | <5 | <2 | 3 | 13 | <5 | <3 | 98 |
| C88-3147 | 0.1 | 2.42 | 15 | 60 | <3 | 10 | 3 | 0.45 | 1.5 | 14 | 28 | 2401 | 5.61 | 0.01 | 2.25 | 510 | 7 | 0.02 | 6 | 0.22 | 37 | <3 | <5 | <2 | 3 | 11 | <5 | <3 | 157 |
| C88-3148 | 0.1 | 2.49 | 14 | 100 | <3 | 10 | 3 | 0.43 | 1.5 | 14 | 41 | 3120 | 5.43 | 0.01 | 2.40 | 503 | 8 | 0.02 | 7 | 0.25 | 39 | <3 | <5 | <2 | 4 | 12 | <5 | <3 | 116 |
| C88-3149 | 0.1 | 2.49 | 14 | 110 | <3 | 11 | 3 | 0.62 | 1.5 | 14 | 24 | 2645 | 5.11 | 0.01 | 2.30 | 655 | 14 | 0.02 | 7 | 0.21 | 35 | <3 | <5 | <2 | 3 | 19 | <5 | <3 | 94 |
| C88-3150 | 0.1 | 1.93 | 13 | 240 | <3 | 8 | 3 | 0.52 | 1.7 | 13 | 50 | 5243 | 5.68 | 0.01 | 1.81 | 520 | 5 | 0.02 | 7 | 0.19 | 32 | <3 | <5 | <2 | 3 | 14 | <5 | <3 | 68 |
| C88-3151 | 0.1 | 2.08 | 15 | 190 | <3 | 8 | 4 | 0.26 | 1.7 | 13 | 58 | 6271 | 6.39 | 0.01 | 1.81 | 385 | 6 | 0.02 | 8 | 0.19 | 35 | <3 | <5 | <2 | 4 | 24 | <5 | <3 | 89 |
| C88-3152 | 0.1 | 1.28 | 25 | 230 | <3 | 32 | <3 | 0.09 | 0.5 | 4 | 33 | 2462 | 3.92 | 0.01 | 0.90 | 147 | 5 | 0.01 | 5 | 0.25 | 61 | <3 | <5 | <2 | 3 | 165 | <5 | <3 | 59 |
| C88-3153 | 1.1 | 1.92 | 96 | 170 | <3 | 11 | 3 | 0.15 | 1.1 | 12 | 23 | 6406 | 5.26 | 0.01 | 1.23 | 177 | 8 | 0.02 | 7 | 0.49 | 56 | <3 | <5 | <2 | 3 | 46 | <5 | <3 | 73 |
| C88-3154 | 1.1 | 1.33 | 87 | 190 | <3 | 7 | <3 | 0.10 | 1.1 | 9 | 32 | 5197 | 5.60 | 0.01 | 0.73 | 95 | 6 | 0.02 | 4 | 0.70 | 89 | <3 | <5 | <2 | 3 | 71 | <5 | <3 | 57 |
| C88-3155 | 0.1 | 2.18 | 18 | 140 | <3 | 12 | 3 | 0.30 | 1.2 | 14 | 31 | 4558 | 4.79 | 0.01 | 1.87 | 490 | 6 | 0.02 | 5 | 0.24 | 36 | <3 | <5 | <2 | 3 | 16 | <5 | <3 | 119 |
| C88-3156 | 0.1 | 3.15 | 110 | 70 | <3 | 15 | 3 | 0.25 | 1.1 | 12 | 29 | 3019 | 4.62 | 0.01 | 2.14 | 427 | 5 | 0.02 | 7 | 0.35 | 35 | <3 | <5 | <2 | 3 | 57 | <5 | <3 | 105 |
| C88-3157 | 0.1 | 2.82 | 237 | 120 | <3 | 8 | 3 | 0.24 | 0.8 | 12 | 21 | 5396 | 5.11 | 0.01 | 1.58 | 274 | 7 | 0.02 | 4 | 0.56 | 59 | <3 | <5 | <2 | 3 | 32 | <5 | <3 | 192 |
| C88-3158 | 1.1 | 1.34 | 20 | <5 | <3 | 6 | 4 | 0.19 | 1.7 | 12 | 30 | 10668 | 6.53 | 0.01 | 1.03 | 170 | 3 | 0.02 | 5 | 0.21 | 50 | <3 | <5 | <2 | 4 | 28 | <5 | <3 | 138 |
| C88-3159 | 0.1 | 2.79 | 21 | 580 | <3 | 6 | 5 | 0.26 | 2.5 | 14 | 53 | 7639 | 8.68 | 0.01 | 2.36 | 555 | 5 | 0.02 | 5 | 0.18 | 37 | <3 | <5 | <2 | 4 | 17 | <5 | <3 | 146 |
| C88-3160 | 0.6 | 1.81 | 19 | 340 | <3 | 8 | 4 | 0.39 | 1.5 | 14 | 36 | 9657 | 5.76 | 0.01 | 1.82 | 602 | 4 | 0.02 | 6 | 0.20 | 34 | <3 | <5 | <2 | 4 | 28 | <5 | <3 | 123 |
| C88-3161 | 0.4 | 2.11 | 18 | 760 | <3 | 8 | 4 | 0.28 | 1.5 | 14 | 61 | 9819 | 5.83 | 0.01 | 1.98 | 364 | 4 | 0.02 | 6 | 0.21 | 31 | <3 | <5 | <2 | 4 | 9 | <5 | <3 | 121 |
| C88-3162 | 1.1 | 1.58 | 25 | 220 | <3 | 6 | 4 | 0.29 | 1.7 | 16 | 38 | 8376 | 6.80 | 0.01 | 1.54 | 300 | 3 | 0.02 | 7 | 0.20 | 59 | <3 | <5 | <2 | 5 | 15 | <5 | <3 | 80 |
| C88-3163 | 0.6 | 2.21 | 19 | 360 | <3 | 7 | 4 | 0.33 | 2.1 | 14 | 28 | 10046 | 6.34 | 0.01 | 2.17 | 563 | 3 | 0.02 | 7 | 0.23 | 43 | <3 | <5 | <2 | 4 | 13 | <5 | <3 | 153 |
| C88-3164 | 0.4 | 1.35 | 15 | 630 | <3 | 6 | 4 | 0.26 | 2.1 | 15 | 52 | 7995 | 6.51 | 0.01 | 1.25 | 351 | 4 | 0.02 | 14 | 0.18 | 37 | <3 | <5 | <2 | 4 | 13 | <5 | <3 | 103 |
| C88-3165 | 3.7 | 1.23 | 624 | 750 | <3 | 5 | 5 | 0.19 | 0.1 | 13 | 58 | 15452 | 7.00 | 0.01 | 1.06 | 251 | 4 | 0.02 | 8 | 0.14 | 60 | <3 | <5 | <2 | 5 | 12 | <5 | <3 | 59 |
| C88-3166 | 4.9 | 0.17 | >1000 | <5 | <3 | 3 | 4 | 0.04 | 0.1 | 7 | 112 | >20000 | >10.00 | 0.01 | 0.05 | 31 | 6 | 0.03 | 6 | 0.07 | 40 | <3 | <5 | <2 | 4 | 8 | <5 | <3 | 124 |
| C88-3167 | 0.6 | 0.28 | 207 | 650 | <3 | 4 | 4 | 0.07 | 1.1 | 9 | 98 | >20000 | 7.54 | 0.01 | 0.04 | 32 | 4 | 0.02 | 7 | 0.09 | 21 | <3 | <5 | <2 | 4 | 7 | <5 | <3 | 44 |
| C88-3168 | 2.7 | 0.16 | 888 | 585 | <3 | 4 | 4 | 0.02 | 0.1 | 12 | 152 | 20000 | 8.37 | 0.01 | 0.02 | 32 | 8 | 0.02 | 7 | 0.04 | 35 | <3 | <5 | <2 | 5 | 21 | <5 | <3 | 56 |
| C88-3169 | 2.5 | 0.15 | 505 | 370 | <3 | 3 | 5 | 0.03 | 0.5 | 11 | 127 | 19083 | >10.00 | 0.01 | 0.02 | 69 | 4 | 0.03 | 8 | 0.04 | 37 | <3 | <5 | <2 | 5 | 11 | <5 | <3 | 42 |
| C88-3170 | 2.1 | 0.27 | 143 | 470 | <3 | 4 | 4 | 0.06 | 1.8 | 12 | 153 | >20000 | 9.00 | 0.01 | 0.04 | 44 | 7 | 0.02 | 10 | 0.07 | 40 | <3 | <5 | <2 | 4 | 11 | <5 | <3 | 31 |
| C88-3171 | 0.1 | 2.63 | 38 | 70 | <3 | 70 | <3 | 1.52 | 1.1 | 12 | 34 | 522 | 5.26 | 0.01 | 1.35 | 1067 | 6 | 0.02 | 4 | 0.14 | 40 | <3 | <5 | <2 | 3 | 54 | <5 | <3 | 187 |
| C88-3172 | 0.1 | 2.14 | 37 | 160 | <3 | 10 | 3 | 0.28 | 1.2 | 17 | 39 | 2808 | 5.53 | 0.01 | 1.49 | 313 | 15 | 0.02 | 7 | 0.22 | 42 | <3 | <5 | <2 | 4 | 26 | <5 | <3 | 140 |
| C88-3173 | 0.1 | 1.56 | 12 | 150 | <3 | 7 | <3 | 0.42 | 1.5 | 19 | 23 | 3942 | 5.68 | 0.01 | 1.23 | 353 | 4 | 0.02 | 12 | 0.25 | 32 | <3 | <5 | <2 | 4 | 20 | <5 | <3 | 148 |
| C88-3174 | 0.1 | 2.15 | 32 | 160 | <3 | 8 | <3 | 0.38 | 1.2 | 15 | 37 | 2229 | 4.94 | 0.01 | 1.96 | 591 | 5 | 0.02 | 7 | 0.23 | 45 | <3 | <5 | <2 | 4 | 18 | <5 | <3 | 146 |
| C88-3175 | 0.1 | 1.14 | 26 | 230 | <3 | 27 | <3 | 0.32 | 0.3 | 7 | 75 | 1891 | 3.01 | 0.01 | 0.58 | 561 | 7 | 0.01 | 4 | 0.10 | 29 | <3 | <5 | <2 | 2 | 17 | <5 | <3 | 77 |
| C88-3176 | 0.1 | 1.90 | 22 | 260 | <3 | 26 | <3 | 0.93 | 1.1 | 9 | 85 | 1402 | 4.68 | 0.01 | 0.91 | 1602 | 6 | 0.02 | 4 | 0.13 | 33 | <3 | <5 | <2 | 3 | 36 | <5 | <3 | 163 |
| C88-3177 | 0.1 | 0.84 | 68 | 140 | <3 | 5 | <3 | 0.25 | 0.8 | 18 | 66 | 4976 | 6.27 | 0.01 | 0.19 | 75 | 7 | 0.02 | 9 | 0.25 | 43 | <3 | <5 | <2 | 3 | 21 | <5 | <3 | 44 |
| C88-3178 | 0.1 | 3.32 | 35 | 175 | <3 | 13 | 4 | 1.14 | 2.2 | 26 | 101 | 3729 | 6.86 | 0.01 | 2.75 | 1824 | 6 | 0.02 | 86 | 0.35 | 50 | <3 | <5 | <2 | 5 | 91 | <5 | <3 | 230 |
| C88-3179 | 0.1 | 2.92 | 43 | 250 | <3 | 15 | 4 | 0.69 | 1.7 | 19 | 114 | 5390 | 5.74 | 0.01 | 2.32 | 897 | 5 | 0.02 | 51 | 0.24 | 56 | <3 | <5 | <2 | 4 | 113 | <5 | <3 | 179 |
| C88-3180 | 0.1 | 4.15 | 19 | <5 | <3 | 63 | 4 | 1.40 | 2.5 | 24 | 129 | 2608 | 6.19 | 0.01 | 3.51 | 1531 | 3 | 0.03 | 103 | 0.35 | 73 | <3 | <5 | <2 | 4 | 222 | <5 | <3 | 277 |
| C88-3181 | 0.1 | 2.84 | 38 | 160 | <3 | 40 | 3 | 0.21 | 1.3 | 13 | 30 | 3407 | 4.51 | 0.01 | 2.05 | 591 | 4 | 0.02 | 16 | 0.18 | 64 | <3 | <5 | <2 | 4 | 95 | <5 | <3 | 181 |
| C88-3182 | 2.5 | 2.57 | 44 | 690 | <3 | 12 | 6 | 0.24 | 2.5 | 16 | 83 | 18689 | 6.68 | 0.01 | 1.53 | 532 | 6 | 0.02 | 41 | 0.22 | 66 | <3 | <5 | <2 | 5 | 64 | <5 | <3 | 237 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

REPORT #: 881006 PA  WESTERN CANADIAN  

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88-3183 | 0.1 | 2.07 | 41 | 440 | <3 | 12 | <3 | 0.25 | 1.7 | 13 | 36 | 9004 | 5.67 | 0.01 | 1.34 | 657 | 5 | 0.02 | 23 | 0.17 | 30 | <3 | <5 | <2 | 3 | 43 | <5 | <3 | 184 |
| C88-3184 | 2.8 | 2.33 | 47 | 700 | <3 | 9 | 4 | 0.14 | 2.7 | 15 | 57 | 18311 | 7.58 | 0.01 | 1.15 | 455 | 10 | 0.03 | 19 | 0.14 | 42 | <3 | <5 | <2 | 4 | 41 | <5 | <3 | 217 |
| C88-3185 | 0.1 | 3.55 | 31 | 60 | <3 | 10 | 3 | 0.43 | 2.2 | 21 | 122 | 1532 | 6.24 | 0.01 | 3.25 | 1360 | 3 | 0.02 | 69 | 0.32 | 39 | <3 | <5 | <2 | 4 | 80 | <5 | <3 | 358 |
| C88-3186 | 0.1 | 2.37 | 39 | 100 | <3 | 10 | <3 | 0.22 | 1.5 | 13 | 22 | 1433 | 4.34 | 0.01 | 2.54 | 1099 | 2 | 0.02 | 6 | 0.18 | 33 | <3 | <5 | <2 | 4 | 21 | <5 | <3 | 431 |
| C88-3187 | 6.2 | 0.14 | 801 | 340 | <3 | 4 | <3 | 0.08 | 0.1 | 9 | 111 | >20000 | 6.39 | 0.01 | 0.05 | 48 | 4 | 0.02 | 4 | 0.09 | 65 | <3 | <5 | <2 | 3 | 7 | <5 | <3 | 49 |
| C88-3188 | 1.5 | 0.13 | >1000 | 780 | <3 | 4 | 3 | 0.13 | 0.1 | 10 | 41 | 16878 | 7.38 | 0.01 | 0.02 | 19 | 2 | 0.02 | 4 | 0.12 | 29 | <3 | <5 | <2 | 3 | 12 | <5 | <3 | 98 |
| C88-3189 | 3.2 | 0.29 | >1000 | <5 | <3 | 4 | 3 | 0.15 | 0.1 | 10 | 168 | 15390 | 7.99 | 0.01 | 0.03 | 35 | 3 | 0.02 | 5 | 0.14 | 39 | <3 | <5 | <2 | 3 | 15 | <5 | <3 | 35 |
| C88-3190 | 2.3 | 0.17 | 224 | 710 | <3 | 5 | 3 | 0.15 | 0.6 | 12 | 81 | 17662 | 6.44 | 0.01 | 0.03 | 41 | 5 | 0.02 | 3 | 0.15 | 31 | <3 | <5 | <2 | 2 | 29 | <5 | <3 | 41 |
| C88-3191 | 2.3 | 0.12 | 285 | 750 | <3 | 4 | <3 | 0.10 | 0.6 | 12 | 108 | >20000 | 7.10 | 0.01 | 0.02 | 32 | 2 | 0.02 | 6 | 0.10 | 25 | <3 | <5 | <2 | 3 | 20 | <5 | <3 | 75 |
| C88-3192 | 2.3 | 0.15 | 391 | 420 | <3 | 4 | 3 | 0.11 | 0.7 | 10 | 115 | 19793 | 8.22 | 0.01 | 0.02 | 19 | 4 | 0.02 | 4 | 0.12 | 58 | <3 | <5 | <2 | 3 | 13 | <5 | <3 | 36 |
| C88-3193 | 0.9 | 0.26 | 100 | 540 | <3 | 4 | 3 | 0.14 | 1.2 | 13 | 169 | 16286 | 7.12 | 0.01 | 0.02 | 38 | 2 | 0.02 | 5 | 0.13 | 46 | <3 | <5 | <2 | 3 | 19 | <5 | <3 | 24 |
| C88-3194 | 1.5 | 0.19 | 57 | 990 | <3 | 4 | 3 | 0.16 | 1.9 | 12 | 115 | 18319 | 7.53 | 0.01 | 0.02 | 32 | 5 | 0.02 | 4 | 0.15 | 87 | <3 | <5 | <2 | 3 | 19 | <5 | <3 | 28 |
| C88-3195 | 2.8 | 0.16 | 309 | 1320 | <3 | 3 | <3 | 0.17 | 0.7 | 12 | 54 | 8363 | 8.32 | 0.01 | 0.02 | 21 | 1 | 0.02 | 3 | 0.14 | 374 | <3 | <5 | <2 | 3 | 21 | <5 | <3 | 107 |
| C88-3196 | 0.9 | 0.22 | 49 | 630 | <3 | 4 | <3 | 0.24 | 1.2 | 12 | 93 | 5958 | 7.01 | 0.01 | 0.02 | 71 | 4 | 0.02 | 5 | 0.15 | 100 | <3 | <5 | <2 | 2 | 23 | <5 | <3 | 23 |
| C88-3197 | 1.1 | 0.32 | 26 | 1150 | <3 | 4 | <3 | 0.33 | 1.4 | 13 | 86 | 10244 | 6.90 | 0.01 | 0.08 | 123 | 2 | 0.02 | 4 | 0.20 | 53 | <3 | <5 | <2 | 2 | 19 | <5 | <3 | 22 |
| TC-18 C88-3198 | 2.3 | 0.60 | 26 | 1460 | <3 | 5 | 3 | 0.85 | 2.1 | 11 | 101 | >20000 | 6.95 | 0.01 | 0.42 | 699 | 6 | 0.02 | 6 | 0.15 | 14 | <3 | <5 | <2 | 3 | 24 | <5 | <3 | 83 |
| C88-3199 | 5.7 | 0.14 | 349 | 930 | <3 | 3 | 4 | 0.33 | 1.7 | 10 | 87 | >20000 | 9.44 | 0.01 | 0.05 | 178 | 4 | 0.03 | 5 | 0.11 | 33 | <3 | <5 | <2 | 4 | 11 | <5 | <3 | 198 |
| C88-3200 | 1.1 | 0.60 | 36 | 770 | <3 | 4 | 3 | 0.50 | 2.2 | 12 | 86 | 13947 | 7.96 | 0.01 | 0.35 | 286 | 3 | 0.02 | 5 | 0.16 | 18 | <3 | <5 | <2 | 3 | 18 | <5 | <3 | 62 |
| C88-3201 | 0.1 | 4.95 | 43 | 5 | <3 | 44 | 3 | 0.45 | 2.2 | 21 | 37 | 547 | 6.87 | 0.01 | 3.67 | 1170 | 4 | 0.02 | 11 | 0.16 | 41 | <3 | <5 | <2 | 5 | 14 | <5 | <3 | 366 |
| C88-3202 | 0.1 | 0.26 | 16 | 460 | <3 | 4 | 3 | 0.82 | 2.2 | 15 | 113 | 11350 | 9.21 | 0.01 | 0.08 | 425 | 6 | 0.02 | 5 | 0.23 | 27 | <3 | <5 | <2 | 3 | 39 | <5 | <3 | 14 |
| C88-3203 | 0.1 | 4.07 | 58 | <5 | <3 | 55 | 3 | 0.75 | 1.7 | 22 | 38 | 3167 | 5.65 | 0.01 | 3.27 | 1163 | 4 | 0.02 | 20 | 0.23 | 40 | <3 | <5 | <2 | 5 | 32 | <5 | <3 | 272 |
| C88-3204 | 0.5 | 0.26 | 134 | <5 | <3 | 4 | <3 | 0.36 | 1.2 | 13 | 60 | 8063 | 7.50 | 0.01 | 0.08 | 106 | 2 | 0.02 | 5 | 0.17 | 27 | <3 | <5 | <2 | 2 | 24 | <5 | <3 | 31 |
| C88-3205 | 2.3 | 0.22 | 359 | 360 | <3 | 4 | 3 | 0.24 | 1.1 | 13 | 58 | 16135 | 7.94 | 0.01 | 0.03 | 26 | 2 | 0.02 | 4 | 0.19 | 110 | <3 | <5 | <2 | 3 | 22 | <5 | <3 | 45 |
| C88-3206 | 0.1 | 0.17 | 15 | 340 | <3 | 4 | <3 | 0.16 | 1.5 | 9 | 79 | 8309 | 7.27 | 0.07 | 0.03 | 25 | 5 | 0.02 | 2 | 0.11 | 37 | <3 | <5 | <2 | 3 | 10 | <5 | <3 | 7 |
| C88-3207 | 0.5 | 0.44 | 9 | 415 | <3 | 4 | 3 | 0.30 | 1.7 | 11 | 111 | 10232 | 7.11 | 0.10 | 0.13 | 91 | 5 | 0.02 | 5 | 0.15 | 17 | <3 | <5 | <2 | 3 | 22 | <5 | <3 | 24 |
| C88-3208 | 1.5 | 0.18 | 20 | 650 | <3 | 4 | 3 | 0.25 | 2.4 | 11 | 98 | 14796 | 8.70 | 0.20 | 0.04 | 73 | 5 | 0.02 | 4 | 0.12 | 79 | <3 | <5 | <2 | 3 | 17 | <5 | <3 | 33 |
| C88-3209 | 2.1 | 0.19 | 12 | 575 | <3 | 3 | 3 | 0.60 | 2.2 | 10 | 103 | 15697 | 8.50 | 0.18 | 0.06 | 280 | 7 | 0.02 | 5 | 0.11 | 26 | <3 | <5 | <2 | 3 | 21 | <5 | <3 | 27 |
| C88-3210 | 1.5 | 0.32 | 11 | 480 | <3 | 4 | 3 | 0.82 | 1.9 | 9 | 98 | 14180 | 7.56 | 0.15 | 0.13 | 499 | 9 | 0.02 | 5 | 0.14 | 19 | <3 | <5 | <2 | 3 | 25 | <5 | <3 | 43 |
| C88-3211 | 1.3 | 0.32 | 44 | 550 | <3 | 5 | <3 | 0.42 | 1.7 | 10 | 78 | 9989 | 6.66 | 0.22 | 0.04 | 146 | 7 | 0.02 | 5 | 0.21 | 58 | <3 | <5 | <2 | 3 | 19 | <5 | <3 | 55 |
| C88-3212 | 0.1 | 0.21 | 107 | 300 | <3 | 4 | <3 | 0.55 | 1.1 | 13 | 39 | 2925 | 7.07 | 0.30 | 0.06 | 291 | 5 | 0.02 | 3 | 0.17 | 25 | <3 | <5 | <2 | 3 | 23 | <5 | <3 | 15 |
| C88-3213 | 0.1 | 0.31 | 26 | 360 | <3 | 5 | <3 | 0.51 | 1.1 | 13 | 52 | 1667 | 5.74 | 0.29 | 0.08 | 232 | 10 | 0.02 | 3 | 0.17 | 19 | <3 | <5 | <2 | 2 | 27 | <5 | <3 | 20 |
| C88-3214 | 0.1 | 0.38 | 10 | 210 | <3 | 6 | <3 | 0.36 | 0.7 | 15 | 73 | 2413 | 4.47 | 0.26 | 0.13 | 131 | 16 | 0.01 | 6 | 0.19 | 18 | <3 | <5 | <2 | 2 | 59 | <5 | <3 | 26 |
| C88-3215 | 0.1 | 1.52 | <3 | <5 | <3 | 882 | <3 | 2.43 | 0.2 | 7 | 64 | 61 | 2.27 | 0.03 | 0.84 | 1087 | 2 | 0.01 | 3 | 0.11 | 19 | <3 | <5 | <2 | 2 | 311 | <5 | <3 | 117 |
| C88-3216 | 0.1 | 0.74 | 30 | 170 | <3 | 12 | <3 | 1.55 | 1.2 | 21 | 57 | 2044 | 5.42 | 0.29 | 0.33 | 650 | 16 | 0.02 | 28 | 0.13 | 29 | <3 | <5 | <2 | 3 | 74 | <5 | <3 | 70 |
| C88-3217 | 0.1 | 1.48 | 6 | 45 | <3 | 103 | <3 | 1.59 | 0.7 | 6 | 55 | 63 | 3.15 | 0.07 | 0.55 | 767 | 3 | 0.02 | 3 | 0.09 | 21 | <3 | <5 | <2 | 2 | 53 | <5 | <3 | 168 |
| C88-3218 | 0.1 | 0.67 | <3 | 35 | <3 | 157 | <3 | 1.01 | 0.1 | 2 | 53 | 15 | 1.61 | 0.01 | 0.19 | 433 | 3 | 0.02 | 1 | 0.03 | 12 | <3 | <5 | <2 | <2 | 42 | <5 | <3 | 111 |
| C88-3219 | 0.1 | 0.61 | <3 | 210 | <3 | >1000 | <3 | 1.97 | 0.1 | 3 | 92 | 16 | 1.12 | 0.01 | 0.16 | 708 | 1 | 0.02 | 4 | 0.02 | 11 | <3 | <5 | <2 | <2 | 187 | <5 | <3 | 73 |
| C88-3220 | 0.1 | 0.29 | 14 | 160 | <3 | 12 | <3 | 0.60 | 1.5 | 20 | 28 | 1457 | 6.63 | 0.38 | 0.07 | 203 | 15 | 0.02 | 13 | 0.18 | 23 | <3 | <5 | <2 | 2 | 76 | <5 | <3 | 17 |
| C88-3221 | 0.1 | 0.22 | 15 | 115 | <3 | 6 | <3 | 0.70 | 1.1 | 19 | 35 | 766 | 5.61 | 0.49 | 0.03 | 237 | 5 | 0.02 | 15 | 0.19 | 19 | <3 | <5 | <2 | 2 | 27 | <5 | <3 | 6 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

REPORT #: 881006 PA

WESTERN CANADIAN MINING CORP.



| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-3222 | 0.1 | 2.47 | 21 | 130 | <3 | 62 | 4 | 2.47 | 1.2 | 27 | 77 | 469 | 4.92 | 0.29 | 3.40 | 877 | 7 | 0.03 | 74 | 0.44 | 28 | <3 | <5 | <2 | 5 | 257 | <5 | <3 | 131 |
| C88-3223 | 0.3 | 1.25 | 11 | 375 | <3 | 7 | 3 | 1.43 | 1.5 | 29 | 74 | 3897 | 6.08 | 0.22 | 1.06 | 875 | 57 | 0.02 | 51 | 0.17 | 32 | <3 | <5 | <2 | 3 | 87 | <5 | <3 | 100 |
| C88-3224 | 0.1 | 5.64 | 23 | 80 | <3 | 44 | 4 | 4.66 | 1.6 | 28 | 152 | 210 | 6.40 | 0.34 | 5.65 | 3068 | 1 | 0.03 | 130 | 0.56 | 47 | <3 | <5 | <2 | 4 | 282 | <5 | <3 | 856 |
| C88-3225 | 0.3 | 0.56 | 19 | 310 | <3 | 4 | 4 | 1.43 | 2.1 | 35 | 59 | 4218 | 8.49 | 0.22 | 0.34 | 888 | 46 | 0.02 | 59 | 0.20 | 100 | <3 | <5 | <2 | 3 | 44 | <5 | <3 | 74 |
| C88-3226 | 0.9 | 0.27 | 573 | 240 | <3 | 5 | <3 | 0.70 | 2.1 | 31 | 36 | 4345 | 7.16 | 0.14 | 0.16 | 432 | 40 | 0.02 | 13 | 0.19 | 119 | <3 | <5 | <2 | 3 | 54 | <5 | <3 | 398 |
| C88-3227 | 0.1 | 2.32 | 47 | <5 | <3 | 154 | 3 | 3.24 | 0.8 | 24 | 84 | 138 | 4.33 | 0.34 | 3.39 | 1040 | 1 | 0.04 | 74 | 0.46 | 32 | <3 | <5 | <2 | 4 | 403 | <5 | <3 | 122 |
| C88-3228 | 0.1 | 1.10 | 146 | 185 | <3 | 7 | 3 | 0.83 | 1.2 | 30 | 71 | 2971 | 6.12 | 0.17 | 1.06 | 533 | 32 | 0.02 | 32 | 0.22 | 42 | <3 | <5 | <2 | 3 | 105 | <5 | <3 | 240 |
| C88-3229 | 0.1 | 5.29 | 26 | 145 | <3 | 26 | 5 | 6.73 | 2.1 | 35 | 171 | 684 | 7.14 | 0.38 | 5.30 | 2783 | 4 | 0.02 | 150 | 0.51 | 56 | <3 | <5 | <2 | 3 | 228 | <5 | <3 | 285 |
| C88-3230 | 0.1 | 2.20 | 16 | 660 | <3 | 6 | 5 | 0.98 | 1.6 | 35 | 110 | 3854 | 7.16 | 0.17 | 1.93 | 632 | 67 | 0.02 | 51 | 0.20 | 42 | <3 | <5 | <2 | 4 | 61 | <5 | <3 | 119 |
| C88-3231 | 0.9 | 1.29 | 18 | 590 | <3 | 5 | 4 | 1.70 | 1.6 | 28 | 81 | 4770 | 6.98 | 0.26 | 1.02 | 770 | 46 | 0.02 | 35 | 0.20 | 40 | <3 | <5 | <2 | 4 | 64 | <5 | <3 | 103 |
| C88-3232 | 0.1 | 1.43 | 13 | 410 | <3 | 5 | 4 | 0.86 | 1.7 | 26 | 37 | 4547 | 7.24 | 0.17 | 1.25 | 426 | 45 | 0.02 | 17 | 0.20 | 40 | <3 | <5 | <2 | 4 | 76 | <5 | <3 | 136 |
| C88-3233 | 0.1 | 2.36 | 20 | 20 | <3 | 6 | 4 | 2.33 | 2.1 | 32 | 78 | 2969 | 6.89 | 0.30 | 2.12 | 879 | 28 | 0.02 | 66 | 0.32 | 64 | <3 | <5 | <2 | 4 | 106 | <5 | <3 | 181 |
| C88-3234 | 0.1 | 1.18 | 26 | 340 | <3 | 6 | 3 | 1.56 | 1.5 | 32 | 68 | 3430 | 6.37 | 0.26 | 0.91 | 521 | 43 | 0.02 | 51 | 0.25 | 26 | <3 | <5 | <2 | 3 | 94 | <5 | <3 | 110 |
| C88-3235 | 3.2 | 2.37 | 26 | 50 | <3 | 276 | 5 | 1.98 | 1.1 | 31 | 82 | 216 | 4.69 | 0.32 | 3.08 | 718 | 2 | 0.04 | 64 | 0.41 | 31 | <3 | <5 | <2 | 12 | 247 | <5 | <3 | 122 |
| C88-3236 | 0.1 | 1.33 | 15 | 170 | <3 | 9 | <3 | 1.54 | 1.1 | 27 | 74 | 3341 | 5.64 | 0.27 | 0.86 | 570 | 33 | 0.02 | 38 | 0.22 | 27 | <3 | <5 | <2 | 3 | 87 | <5 | <3 | 51 |
| C88-3237 | 0.1 | 2.20 | 21 | 160 | <3 | 8 | 4 | 1.53 | 1.5 | 33 | 114 | 2478 | 6.08 | 0.26 | 2.08 | 457 | 16 | 0.02 | 63 | 0.34 | 32 | <3 | <5 | <2 | 4 | 139 | <5 | <3 | 120 |
| C88-3238 | 0.1 | 1.12 | 5 | 510 | <3 | 231 | <3 | 2.04 | 0.1 | 7 | 55 | 185 | 2.20 | 0.34 | 0.75 | 883 | 18 | 0.02 | 14 | 0.10 | 18 | <3 | <5 | <2 | 2 | 132 | <5 | <3 | 93 |
| C88-3239 | 0.1 | 1.10 | <3 | 20 | <3 | 279 | <3 | 1.26 | 0.1 | 5 | 21 | 37 | 2.41 | 0.26 | 0.46 | 676 | 3 | 0.02 | 2 | 0.06 | 15 | <3 | <5 | <2 | 2 | 71 | <5 | <3 | 120 |
| C88-3240 | 0.1 | 0.71 | 3 | <5 | <3 | 119 | <3 | 1.12 | 0.1 | 3 | 45 | 23 | 1.72 | 0.25 | 0.25 | 507 | 2 | 0.02 | 3 | 0.04 | 13 | <3 | <5 | <2 | 2 | 44 | <5 | <3 | 120 |
| C88-3241 | 0.1 | 1.18 | 4 | 30 | <3 | 261 | <3 | 2.07 | 0.1 | 5 | 68 | 22 | 2.43 | 0.32 | 0.44 | 992 | 1 | 0.02 | 1 | 0.07 | 19 | <3 | <5 | <2 | 2 | 93 | <5 | <3 | 150 |
| C88-3242 | 0.9 | 0.20 | 4 | 230 | <3 | 4 | <3 | 0.61 | 1.5 | 29 | 35 | 1784 | 7.75 | 0.16 | 0.03 | 187 | 91 | 0.02 | 25 | 0.22 | 30 | <3 | <5 | <2 | 3 | 35 | <5 | <3 | 27 |
| C88-3243 | 3.2 | 0.22 | 20 | 240 | <3 | 4 | 4 | 0.44 | 2.2 | 27 | 18 | 1364 | 8.30 | 0.17 | 0.02 | 159 | 19 | 0.03 | 16 | 0.20 | 83 | <3 | <5 | <2 | 5 | 22 | <5 | <3 | 7 |
| C88-3244 | 3.8 | 0.19 | 20 | 210 | <3 | 3 | 3 | 0.32 | 1.2 | 21 | 27 | 1260 | 5.64 | 0.17 | 0.02 | 92 | 8 | 0.03 | 15 | 0.19 | 49 | <3 | <5 | <2 | 5 | 13 | <5 | <3 | 5 |
| C88-3245 | 0.4 | 0.16 | 68 | 300 | <3 | 4 | 10 | 0.55 | 3.4 | 26 | 37 | 955 | 6.90 | 0.41 | 0.04 | 221 | 13 | 0.08 | 24 | 0.19 | 92 | <3 | <5 | <2 | 11 | 36 | <5 | <3 | 14 |
| C88-3246 | 0.1 | 0.38 | 15 | 230 | <3 | 4 | 3 | 0.58 | 1.6 | 22 | 57 | 1359 | 8.69 | 0.12 | 0.08 | 231 | 11 | 0.02 | 12 | 0.22 | 42 | <3 | <5 | <2 | 3 | 27 | <5 | <3 | 24 |
| C88-3247 | 0.1 | 0.26 | 3 | 150 | <3 | 3 | 5 | 0.72 | 2.5 | 36 | 36 | 984 | >10.00 | 0.10 | 0.14 | 288 | 6 | 0.03 | 13 | 0.19 | 22 | <3 | <5 | <2 | 4 | 55 | <5 | <3 | 15 |
| C88-3248 | 0.1 | 0.24 | 4 | 90 | <3 | 3 | 3 | 0.44 | 1.7 | 81 | 30 | 662 | 9.60 | 0.06 | 0.03 | 76 | 4 | 0.02 | 15 | 0.26 | 30 | <3 | <5 | <2 | 3 | 31 | <5 | <3 | 5 |
| C88-3249 | 0.1 | 0.34 | 48 | 435 | <3 | 4 | 3 | 0.41 | 2.1 | 18 | 28 | 837 | 9.39 | 0.06 | 0.04 | 127 | 3 | 0.02 | 13 | 0.22 | 25 | <3 | <5 | <2 | 3 | 17 | <5 | <3 | 35 |
| C88-3250 | 0.1 | 0.29 | <3 | 290 | <3 | 4 | 3 | 0.56 | 2.1 | 24 | 70 | 965 | 9.80 | 0.08 | 0.05 | 231 | 7 | 0.02 | 25 | 0.22 | 25 | <3 | <5 | <2 | 3 | 20 | <5 | <3 | 12 |

1500m.
1450m.
1400m.
1350m.
1300m.
9500E
9600E
9700E
60°
P-ZONE
Overburden (3.0m)
K88-22
K88-19
K88-18
3.05m.
0.28%,0.14g/t
79.95m.
39.0m.
40.8m.
0.86%,0.41g/t
161.0m.
Rubble Zone
69.1m.
0.62%,0.32g/t
96.5m.
1.01%,0.44g/t
123.2m.
0.09%,0.03g/t
89.0m.
1.03%,0.55g/t
39.9m.
Silica-Sulphide Zones
126.5m.
E.O.H.=136.85m.
0.52%,0.28g/t
134.11m.
164.0m.
0.31%,0.17g/t
31.0m.
No Sample
0.15%,0.07g/t
9.82m.
E.O.H. = 220.37m.
0.16%,0.21g/t
91.42m.
E.O.H. = 255.42m.

## LEGEND

Fault

0.13%,1.13g/t / 10.3m. — %Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Interval defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE – fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a)/MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST – foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) – interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE – interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

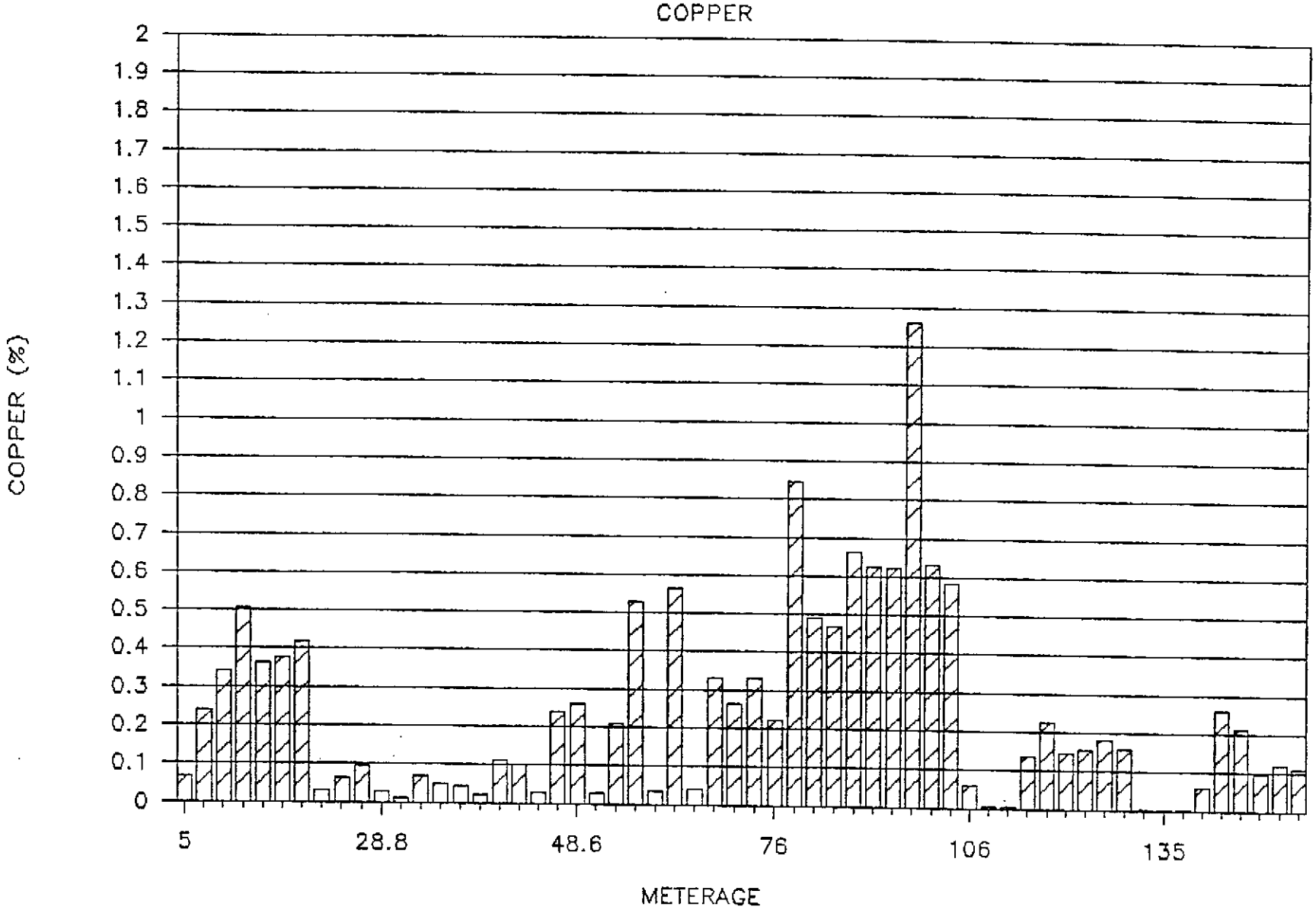
1:1000
SCALE 0 10 20 30 40 Metres

# SULPHURETS GOLD
CORPORATION
1989 KERR PROJECT
D.D.H. K88-18,19,22
SECTION

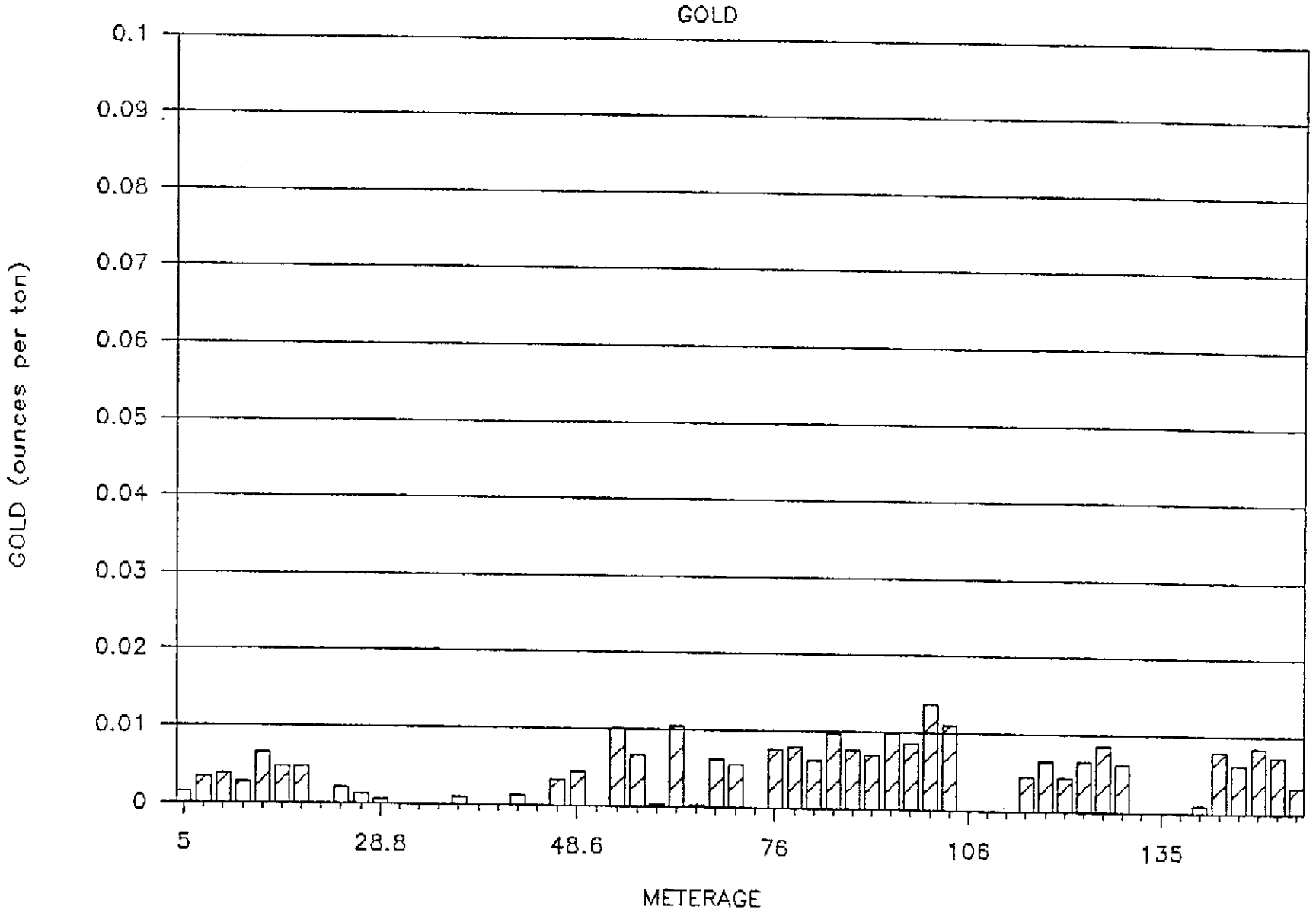
COLLAR:- ≈10228N, 9598E
BEARING: 60°,240°,Vert. DIP: -60°,-90°,-60°
ELEVATION: 1468.8m.

REPORT:1065 FIGURE No.

# K88-20


COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
5
28.8
48.6
76
106
135
METERAGE

# K88-20


GOLD
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
GOLD (ounces per ton)
5
28.8
48.6
76
106
135
METERAGE

KERR PROJECT D.D.HOLE K-88-20

| | | | |
|---|---|---|---|
| LOCATION | NORTH GLACIER N. OF K-88-14 | COLLAR LAT. | 10085.5 NORTH |
| DATE STARTED | AUGUST 15, 1988 | LONG. | 9634.9 EAST |
| DATE COMPLETED | AUGUST 17, 1988 | ELEVATION | 1568.1 m |
| CORE RECOVERY | 74.95% | AZIMUTH | 090 DIP -60 deg |
| DRILLED BY | FALCON DRILLING LTD | LENGTH | 152.09 m |
| LOGGED BY | S. CASSELMAN | HOR. PROJ. | 76.05 m |
| OBJECTIVE | TRACE B-ZONE FAULT / MINERALIZATION BETWEEN HOLES 88-14 AND 88-16, 17, 18, 19 | VERT.PROJ. | 131.71 m |

DIP TEST DEPTH _____m DIP_____deg
DEPTH _____m DIP_____deg

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 2.13 | 2.13 | OVERBURDEN |
| 2.13 | 21.25 | 19.12 | SERICITE SCHIST<br>light to medium grey alternating laminae of light grey sericite, white to grey quartz-calcite, 1 to 10 mm wide pyrite stringers and occasional chlorite<br>- foliated at 45 deg to C.A.<br>- 3 to 15% stockwork silica with pyrite as patches and bands which are white to blue-grey<br>- traces of chalcopyrite and chalcocite<br>- overall 15 to 20% pyrite<br>- pyrite occurs as fine disseminations, coarse stringers, and very fine-grained bands and blebs up to 1.5 cm wide<br>- protolith is unrecognizable but due to fine-grained nature of schist is believed to be dacitic tufaceous volcanics<br>- average piece is 10 to 20 cm long-occasional small section (5 cm) of gouge material |
| 21.25 | 21.65 | 00.40 | FINE-GRAINED ANDESITE DYKE<br>- light grey green, slightly foliated and altered, sharp contacts, 5% quartz-calcite<br>- upper contact at 45 deg, lower at 50 deg to C.A. |
| 21.65 | 28.80 | 7.15 | SERICITE SCHIST<br>- light to medium grey-green<br>- similar to section 2.13 - 21.15, however coarser-grained - possibly indicating an intrusive protolith (diorite?), more chlorite and less sulphides |

KERR PROJECT D.D.HOLE K-88-20

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - 15% pyrite as disseminations and fine stringers<br>- 5 to 10% silicification and 5 to 10% bull white and yellowish quartz-calcite veins<br>- possibly traces of chalcocite and pyrite |
| 28.80 | 32.00 | 3.20 | FINE-GRAINED ANDESITE DYKE<br>- medium grey-green<br>- upper contact at 35 deg to C.A. has 20 cm light green chill margin<br>- 3% quartz-calcite veins in tension gashes at 40 deg to C.A. intruded in hanging walls<br>- lower contact at 30 deg to C.A. |
| 32.00 | 38.80 | 6.80 | SERICITE SCHIST<br>- as in 21.65 to 28.80 m<br>- 10% coarse-grained pyrite and chlorite spots, light to medium grey-greenish<br>- 1% quartz-calcite veins<br>- average piece 5 cm long |
| 38.80 | 39.70 | 00.90 | FRACTURED FINE-GRAINED 'ANDESITE' DYKE<br>- medium grey-green<br>- average piece 5 cm long<br>- intruded along hanging wall contact of fault<br>- composition and appearance similar to section 28.80 - 32.00 m and 21.25 - 21.65 m<br>- upper contact at 35 deg, lower contact at 35 deg to C.A. |
| 39.70 | 44.30 | 4.60 | FAULT ZONE / SERICITE SCHIST<br>- light grey, slight green<br>- average piece 1 to 5 cm long, quite fractured, appears to be same fine-grained material as in sections 21.65 - 28.80 m and 32.00 - 38.80 m<br>- fractures at 50 to 70 deg to C.A.<br>- undulating foliation in places<br>- 10% disseminated pyrite<br>- sections of sericitic gouge<br>- trace to 5% chalcocite |
| 44.30 | 44.70 | 00.40 | FRACTURED ANDESITE DYKE<br>- as in section 38.8 to 39.7 m |
| 44.70 | 48.60 | 3.90 | FAULT ZONE / SERICITE SCHIST<br>- as in section 39.7 to 44.3<br>- average piece approximately 1 to 5 cm long |

KERR PROJECT D.D.HOLE K-88-20

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - foliated at 60 deg to C.A.<br>- fractured at 50 to 80 deg to C.A.<br>- trace to 1% chalcocite, 15% pyrite |
| 48.60 | 51.65 | 3.05 | FRACTURED ANDESITE DYKE<br>- same material as in 38.8 to 39.7 m and 44.3 to 44.7 m<br>- fractured into pieces 1 to 5 cm wide<br>- moderate chlorite and sericite at contact<br>- upper contact at 40 deg, lower contact at 40 deg to C.A. |
| 51.65 | 57.90 | 6.25 | FAULT ZONE / SERICITE SCHIST<br>- as in section 44.7 to 48.6 m<br>- trace to 1.5% chalcocite, 20% pyrite |
| 57.90 | 60.50 | 2.60 | FRACTURED ANDESITE DYKE<br>- as in section 48.6 to 51.65 m<br>- pieces 15 cm long<br>- upper contact at 40 deg, lower at 60 deg to C.A. |
| 60.50 | 63.60 | 3.10 | FAULT ZONE / SERICITE SCHIST<br>- as in sections 44.70 to 48.60 and 51.65 to 57.90 m<br>- average piece 1 to 5 cm long<br>- intense sericitization<br>- 1.5% chalcocite, 18% pyrite |
| 63.60 | 65.50 | 1.90 | FRACTURED ANDESITE DYKE<br>- as in above sections<br>- upper contact at 50 deg, lower contact at 45 deg to C.A. |
| 65.50 | 103.00 | 38.50 | FAULT ZONE / SERICITE SCHIST<br>- as in above sections<br>- average piece 1 to 5 cm long<br>- intense sericitization<br>- trace to 2% chalcocite, 12 to 25% pyrite |
| 103.00 | 112.20 | 9.20 | PLAGIOCLASE PORPHYRY DYKE<br>- medium green colour with white plagioclase phenocrysts to 1 cm long<br>- matrix moderately to intensely chloritized<br>- plagioclase phenocrysts sericitized<br>- slight fabric development at 60 deg to C.A.<br>- upper contact at 40 deg, lower at 50 deg to C.A.<br>- dyke marks footwall contact at fault zone |

KERR PROJECT D.D.HOLE K-88-20

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - 2 to 3% calcite, minor quartz veins<br>- < 1% pyrite |
| 112.20 | 129.00 | 16.80 | BUFF GREEN ALTERED VOLCANICS<br>- light grey to buff-limy green overall colour<br>- green believed due to epidote and fuchsite (mariposite) blades ( .2 cm long)<br>- the green coloration occurs as pervasive epidote with spotty fuchsite, however within the interval there are sections of mainly sericite, with very little lime green colour<br>- this style of mineralization is believed to be characteristic of the C-Zone which comprises the footwall of the B-Zone fault<br>- 3 to 10% silicification as bands and blebs as well as weakly pervasive, 10 to 20% pyrite as fine disseminations and wispy stringers and veinlets 1 mm to 5 mm wide (average 2 mm) which crisscross core at angles of 45 deg and 60 deg to C.A.<br>- traces of chalcopyrite and up to 1% chalcocite associated with pyrite veinlets -- questionable as to whether it is chalcocite<br>- unit quite sheared and sericitic for 20 cm from lower contact |
| 129.00 | 138.00 | 9.00 | PLAGIOCLASE PORPHYRY DYKE<br>- as in section 103.00 to 112.2 m<br>- chloritized matrix, sericitized plagioclase<br>- 3 to 5% calcite-quartz-chlorite veins<br>- < 1% pyrite<br>- upper contact at 45 deg, lower at 50 deg to C.A. |
| 138.00 | 138.65 | 00.65 | BULL WHITE QUARTZ-CALCITE VEIN<br>- contains 10 cm of buff-green volcanics<br>- 3% blebs 1 cm long chalcopyrite in quartz, 5 to 8% pyrite as fine disseminations<br>- 10% contained chlorite |
| 138.65 | 152.00 | 13.35 | BUFF-GREY-GREEN VOLCANICS<br>- less green coloration than 12.2 to 12.9 m<br>- more grey sericite<br>- epidote, fuchsite occurs as patches and bands<br>- with depth, epidote and fuchsite decrease<br>- protolith appears to become coarser-grained with depth as alteration minerals appear as coarse spots - pyrite, chlorite,, sericite, epidote |

KERR PROJECT D.D.HOLE K-88-20

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - possibly some chalcocite associated with pyrite disseminations<br>- 12 to 15% pyrite mainly as fine disseminated aggregates with a few narrow wisps<br>- traces of chalcopyrite<br>- 1 to 3% irregular blebs of calcite<br>- weak patchy silicification<br>- slight foliation at 70 deg to C.A.<br>- fractured at 85 deg to C.A. - fairly competent |
| 152.00 | 152.09 | 00.09 | FINE-GRAINED ANDESITE DYKE<br>- light grey green colour<br>- included in sample # 2377<br>- upper contact at 90 deg to C.A. |
| | | | E.O.H. |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 25 Nov 1988 13:08:47 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8820 | 10085.5 | 9634.9 | 1568.2 | 90 | 60 | 152.09 | | TEST B-ZONE STRIKE EXTENSION. NO TEST. #HOLE |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 2.13 | 2.13 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 2.13 | 5.0 | 2.87 | 14 | SRCT SCHT | | F-MG | 15 | 3 | 50 | 2 | 8 | 0 | 0 | | | | 100 | 17 | 0 | | .2 | | | |
| 5.0 | 8.0 | 3.0 | 31 | SRCT SCHT | | F-MG | 15 | 5 | 45 | 1 | 8 | 0 | 0 | | | | 100 | 20 | .1 | | .5 | | | |
| 8.0 | 11.0 | 3.0 | 28 | SRCT SCHT | | F-MG | 20 | 2 | 45 | 0 | 5 | 0 | 0 | | | | 100 | 22 | 0 | | .2 | | | |
| 11.0 | 14.0 | 3.0 | 37 | SRCT SCHT | | F-MG | 25 | 5 | 35 | 0 | 3 | 0 | 0 | | | | 100 | 25 | .2 | | .5 | | | |
| 14.0 | 17.0 | 3.0 | 35 | SRCT SCHT | | F-MG | 20 | 2 | 50 | 0 | 5 | 0 | 0 | | | | 100 | 18 | .1 | | .1 | | | |
| 17.0 | 19.0 | 2.0 | 37 | SRCT SCHT | | F-MG | 15 | 8 | 50 | 1 | 2 | 0 | 0 | | | | 100 | 20 | 0 | | .2 | | | |
| 19.0 | 21.25 | 2.25 | 24 | SRCT SCHT | | F-MG | 15 | 3 | 50 | 1 | 8 | 0 | 0 | | | | 100 | 20 | 0 | | .2 | | | |
| 21.25 | 21.65 | .40 | 36 | ANDS DYKE | | FG | 0 | 3 | 20 | 0 | 20 | 0 | 3 | | | | 48 | .5 | 0 | | 0 | | | |
| 21.65 | 24.0 | 2.35 | 31 | SRCT SCHT | | F-CG | 5 | 3 | 60 | 1 | 5 | 0 | 3 | | | | 100 | 15 | 0 | | .1 | | | |
| 24.0 | 27.0 | 3.0 | 35 | SRCT SCHT | | F-CG | 5 | 5 | 55 | 0 | 10 | 0 | 3 | | | | 100 | 17 | 0 | | .2 | | | |
| 27.0 | 28.8 | 1.8 | 31 | SRCT SCHT | | F-CG | 2 | 5 | 60 | 0 | 10 | 0 | 5 | | | | 100 | 10 | 0 | | .1 | | | |
| 28.8 | 32.0 | 3.2 | 42 | ANDS DYKE | | FG | 0 | 3 | 15 | 0 | 20 | 0 | 3 | | | | 45 | .5 | 0 | | 0 | | | |
| 32.0 | 35.0 | 3.0 | 35 | SRCT SCHT | | F-CG | 1 | 1 | 50 | 0 | 20 | 0 | 2 | | | | 90 | 8 | 0 | | .1 | | | |
| 35.0 | 37.0 | 2.0 | 34 | SRCT SCHT | | F-CG | 1 | 1 | 50 | 0 | 12 | 0 | 2 | | | | 90 | 8 | 0 | | .1 | | | |
| 37.0 | 38.8 | 1.8 | 32 | SRCT SCHT | | F-CG | 1 | 1 | 50 | 0 | 12 | 0 | 2 | | | | 90 | 6 | 0 | | .1 | | | |
| 38.8 | 39.7 | .9 | 42 | ANDS DYKE | | F-CG | 0 | 1 | 15 | 0 | 20 | 0 | 3 | | | | 40 | .5 | 0 | | | | | |
| 39.7 | 42.0 | 2.3 | 14 | FAULT SRCT SCHT | | F-CG | 0 | 1 | 70 | 1 | 10 | .5 | 1 | | | | 100 | 10 | 0 | | .2 | | | |
| 42.0 | 44.3 | 2.3 | 24 | FAULT SRCT SCHT | | F-CG | 0 | 1 | 70 | 1 | 10 | .5 | 1 | | | | 100 | 12 | 0 | | .2 | | | |
| 44.3 | 44.7 | .4 | 25 | ANDS DYKE | | FG | 0 | 3 | 15 | 0 | 15 | 0 | 3 | | | | 40 | .5 | 0 | | 0 | | | |
| 44.7 | 46.7 | 2.0 | 19 | FAULT SRCT SCHT | | F-MG | 5 | .1 | 65 | 1 | 5 | 0 | 0 | | | | 100 | 15 | 0 | | .2 | | | |
| 46.7 | 48.6 | 1.9 | 18 | FAULT SRCT SCHT | | F-MG | 1 | .5 | 65 | 1 | 8 | 0 | 0 | | | | 100 | 12 | 0 | | 1 | | | |
| 48.6 | 51.65 | 3.05 | 17 | ANDS DYKE | | FG | 0 | 1 | 10 | 0 | 15 | 0 | 1 | | | | 30 | .5 | 0 | | 0 | | | |
| 51.65 | 54.65 | 3.0 | 10 | FAULT SRCT SCHT | | F-MG | 1 | 1 | 70 | 1 | 5 | 0 | 0 | | | | 100 | 18 | 0 | | .5 | | | |
| 54.65 | 57.9 | 3.25 | 10 | FAULT SRCT SCHT | | F-MG | 1 | 0 | 70 | 0 | 5 | 0 | 0 | | | | 100 | 20 | 0 | | 1.5 | | | |
| 57.9 | 60.5 | 2.6 | 32 | ANDS DYKE | | FG | 0 | 1 | 10 | 2 | 20 | 0 | 1 | | | | 35 | .5 | 0 | | 0 | | | |
| 60.5 | 63.6 | 3.1 | 17 | FAULT SRCT SCHT | | F-MG | 1 | 1 | 70 | 1 | 3 | 0 | 0 | | | | 100 | 18 | .1 | | 1.5 | | | |
| 63.6 | 65.5 | 1.9 | 24 | ANDS DYKE | | FG | 0 | 1 | 20 | 2 | 10 | 0 | 0 | | | | 35 | 1 | 0 | | 0 | | | |
| 65.5 | 67.0 | 1.5 | 20 | FAULT SRCT SCHT | | F-MG | 1 | 0 | 80 | 0 | 2 | 0 | 0 | | | | 100 | 12 | 0 | | .2 | | | |
| 67.0 | 70.0 | 3.0 | 20 | FAULT SRCT SCHT | | F-MG | 3 | 2 | 75 | 0 | 8 | 0 | 0 | | | | 100 | 18 | 0 | | .8 | | | |
| 70.0 | 73.0 | 3.0 | 16 | FAULT SRCT SCHT | | F-MG | 1 | 1 | 75 | 0 | 3 | 0 | 0 | | | | 100 | 18 | 0 | | 2 | | | |
| 73.0 | 76 | 3.0 | 16 | FAULT SRCT SCHT | | F-MG | 1 | 2 | 70 | 0 | 7 | 0 | 0 | | | | 100 | 15 | 0 | | 1 | | | |
| 76.0 | 79 | 3.0 | 17 | FAULT SRCT SCHT | | F-MG | 5 | 2 | 65 | 0 | 3 | 0 | 0 | | | | 100 | 20 | .1 | | 2 | | | |
| 79.0 | 82 | 3.0 | 17 | FAULT SRCT SCHT | | F-MG | 1 | 1 | 60 | 3 | 8 | 3 | 1 | .5 | | | 100 | 12 | 0 | | .8 | | | |
| 82.0 | 85 | 3.0 | 21 | FAULT SRCT SCHT | | F-MG | 0 | 2 | 60 | 3 | 10 | 2 | 0 | 1 | | | 100 | 18 | 0 | | 1 | | | |
| 85.0 | 88 | 3.0 | 20 | FAULT SRCT SCHT | | F-MG | 1 | 2 | 60 | 2 | 12 | .1 | 0 | .1 | | | 100 | 15 | .1 | | .8 | | | |
| 88.0 | 91 | 3.0 | 19 | FAULT SRCT SCHT | | F-MG | 1 | 1 | 70 | 0 | 5 | 0 | 0 | | | | 100 | 15 | 0 | | 2 | | | |
| 91.0 | 94 | 3.0 | 17 | FAULT SRCT SCHT | | F-MG | 2 | 2 | 65 | 1 | 3 | .5 | 0 | | | | 100 | 20 | .5 | | 3 | | | |
| 94.0 | 97 | 3.0 | 20 | FAULT SRCT SCHT | | F-MG | 2 | 1 | 60 | 2 | 10 | 1 | 0 | | | | 100 | 18 | 0 | | 2 | | | |
| 97.0 | 100 | 3.0 | 19 | FAULT SRCT SCHT | | F-MG | 5 | 2 | 60 | 1 | 3 | .2 | 0 | | | | 100 | 23 | 0 | | 3 | | | |
| 100.0 | 103 | 3.0 | 23 | FAULT SRCT SCHT | | F-MG | 5 | 2 | 60 | 0 | 2 | 0 | 0 | | | | 100 | 25 | 0 | | 2 | | | |
| 103.0 | 106 | 3.0 | 39 | PLAG PRPH DYKE | | F-CG | 0 | 1 | 30 | 0 | 25 | 3 | 2 | | | | 65 | .5 | 0 | | 0 | | | |
| 106.0 | 109 | 3.0 | 46 | PLAG PRPH DYKE | | F-CG | 0 | 1 | 20 | 0 | 40 | 0 | 5 | | | | 65 | .5 | 0 | | 0 | | | |
| 109.0 | 112.2 | 3.2 | 39 | PLAG PRPH DYKE | | F-CG | 0 | 1 | 15 | 0 | 45 | 0 | 3 | | | | 65 | .5 | 0 | | 0 | | | |
| 112.2 | 115 | 2.8 | 39 | ALTD VOLC | | F-MG | 8 | 5 | 30 | 0 | 8 | 15 | 0 | 3 | | | 95 | 22 | .1 | | .2 | | | |
| 115.0 | 118 | 3.0 | 45 | ALTD VOLC | | F-MG | 8 | 5 | 30 | 0 | 5 | 18 | 0 | 5 | | | 95 | 22 | .1 | | .2 | | | |
| 118.0 | 121 | 3.0 | 35 | ALTD VOLC | | F-MG | 10 | 5 | 45 | 0 | 5 | 5 | 0 | 1 | | | 95 | 22 | .1 | | .5 | | | |
| 121.0 | 124 | 3.0 | 40 | ALTD VOLC | | F-MG | 8 | 5 | 25 | 0 | 3 | 25 | 0 | 8 | | | 100 | 20 | 0 | | .5 | | | |
| 124.0 | 127 | 3.0 | 23 | ALTD VOLC | | F-MG | 5 | 8 | 20 | 0 | 2 | 30 | 1 | 8 | | | 100 | 20 | 0 | | .2 | | | |
| 127.0 | 129.0 | 2.0 | 27 | ALTD VOLC | | F-MG | 5 | 5 | 25 | 1 | 3 | 25 | 1 | 10 | | | 100 | 18 | 0 | | .5 | | | |
| 129.0 | 132.0 | 3.0 | 32 | PLAG PRPH DYKE | | F-CG | 0 | 1 | 15 | 0 | 35 | 0 | 8 | | | | 60 | .5 | 0 | | 0 | | | |
| 132.0 | 135.0 | 3.0 | 50 | PLAG PRPH DYKE | | F-CG | 0 | 5 | 10 | 0 | 35 | 0 | 3 | | | | 55 | .5 | 0 | | 0 | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 25 Nov 1988 13:09:04 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8820 | 10085.5 | 9634.9 | 1568.2 | 90 | 60 | 152.09 | | TEST B-ZONE STRIKE EXTENSION. NO TEST. |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 | #HOLE |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 135.0 | 138.0 | 3.0 | 38 | PLAG PRPH DYKE | | F-CG | 0 | 5 | 10 | 0 | 35 | 0 | 2 | | | | 55 | .5 | 0 | | 0 | | | | |
| 138.0 | 138.65 | .65 | 40 | SILC CLCT VEIN | | MG | 0 | 55 | 5 | 0 | 1 | 15 | 8 | 3 | | | 100 | 8 | 1 | | 0 | | | | |
| 138.65 | 141.0 | 2.35 | 37 | ALTD VOLC | | F-MG | 2 | 2 | 65 | 0 | 3 | 3 | 1 | .1 | | | 100 | 15 | .8 | | .3 | | | | |
| 141.0 | 144.0 | 3.0 | 47 | ALTD VOLC | | F-MG | 2 | 2 | 65 | 0 | 5 | 2 | 2 | .1 | | | 100 | 15 | .1 | | .3 | | | | |
| 144.0 | 147.0 | 3.0 | 45 | ALTD VOLC | | F-MG | 2 | 5 | 60 | 0 | 5 | 5 | 5 | .5 | | | 100 | 15 | .1 | | .3 | | | | |
| 147.0 | 150.0 | 3.0 | 36 | ALTD VOLC | | F-MG | 1 | 1 | 65 | 0 | 8 | 2 | 2 | .1 | | | 100 | 10 | 0 | | .5 | | | | |
| 150.0 | 152.0 | 2.0 | 20 | ALTD VOLC | | F-MG | 1 | 1 | 65 | 0 | 10 | 1 | 2 | | | | 100 | 10 | 0 | | .8 | | | | |
| 152.0 | 152.09 | .09 | | ANDS DYKE | | F-MG | 0 | 1 | 20 | 0 | 10 | 0 | 2 | | | | 35 | .1 | 0 | | 0 | | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 09:43:12 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8820 | 10085.5 | 9634.9 | 1568.2 | 90 | 60 | 152.09 | | TEST B-ZONE STRIKE EXTENSION. NO TEST. |

#HOLE

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 2.13 | | 2.13 | 0 | | | | | | | | | | | |
| 2.13 | 5.0 | 3320 | 2.87 | 2.08 | 45 | | 0.1 | | 640 | 7 | 5.37 | 9 | 12 | | |
| 5.0 | 8.0 | 3321 | 3.0 | 2.57 | 110 | | 0.1 | | 2379 | 12 | 6.80 | 5 | 24 | | |
| 8.0 | 11.0 | 3322 | 3.0 | 2.72 | 130 | | 0.1 | | 3397 | 78 | 6.80 | 112 | 22 | | |
| 11.0 | 14.0 | 3323 | 3.0 | 2.96 | 90 | | 0.5 | | 5053 | 693 | 4.87 | 271 | 27 | | |
| 14.0 | 17.0 | 3324 | 3.0 | 3.0 | 220 | | 0.1 | | 3634 | 37 | 4.84 | 13 | 44 | | |
| 17.0 | 19.0 | 3325 | 2.0 | 1.86 | 160 | | 0.1 | | 3756 | 31 | 7.69 | 20 | 27 | | |
| 19.0 | 21.25 | 3326 | 2.25 | 2.0 | 160 | | 0.1 | | 4153 | 70 | 5.75 | 8 | 306 | | |
| 21.25 | 21.65 | 3327 | .40 | .38 | 5 | | 0.1 | | 291 | 461 | 4.28 | 4 | 693 | | |
| 21.65 | 24.0 | 3328 | 2.35 | 2.1 | 70 | | 0.1 | | 613 | 216 | 4.97 | 49 | 574 | | |
| 24.0 | 27.0 | 3329 | 3.0 | 2.88 | 40 | | 0.1 | | 930 | 324 | 6.18 | 94 | 1307 | | |
| 27.0 | 28.8 | 3330 | 1.8 | 1.7 | 20 | | 2.8 | | 284 | 945 | 4.56 | 42 | 1670 | | |
| 28.8 | 32.0 | 3331 | 3.2 | 2.82 | 5 | | 0.5 | | 122 | 338 | 5.99 | 59 | 1610 | | |
| 32.0 | 35.0 | 3332 | 3.0 | 2.77 | 5 | | 0.4 | | 685 | 125 | 5.38 | 27 | 586 | | |
| 35.0 | 37.0 | 3333 | 2.0 | 1.52 | 5 | | 0.4 | | 487 | 87 | 5.73 | 19 | 766 | | |
| 37.0 | 38.8 | 3334 | 1.8 | 1.8 | 30 | | 0.3 | | 440 | 257 | 5.49 | 20 | 1369 | | |
| 38.8 | 39.7 | 3335 | .9 | .65 | 5 | | 0.1 | | 214 | 405 | 6.04 | 5 | 1957 | | |
| 39.7 | 42.0 | 3336 | 2.3 | 1.29 | 5 | | 0.1 | | 1101 | 206 | 5.84 | 35 | 246 | | |
| 42.0 | 44.3 | 3337 | 2.3 | 1.78 | 40 | | 0.1 | | 1026 | 325 | 6.13 | 19 | 849 | | |
| 44.3 | 44.7 | 3338 | .4 | .24 | 5 | | 0.1 | | 265 | 427 | 8.54 | 6 | 1060 | | |
| 44.7 | 46.7 | 3339 | 2.0 | 1.53 | 110 | | 0.1 | | 2366 | 145 | 6.09 | 45 | 425 | | |
| 46.7 | 48.6 | 3340 | 1.9 | 1.11 | 150 | | 0.4 | | 2615 | 97 | 5.21 | 51 | 316 | | |
| 48.6 | 51.65 | 3341 | 3.05 | 1.94 | 5 | | 0.1 | | 279 | 312 | 7.86 | 73 | 1343 | | |
| 51.65 | 54.65 | 3342 | 3.0 | 1.17 | 350 | | 1.2 | | 2093 | 135 | 6.98 | 52 | 162 | | |
| 54.65 | 57.9 | 3343 | 3.25 | 1.51 | 225 | | 1.2 | | 5279 | 237 | 4.71 | 39 | 393 | | |
| 57.9 | 60.5 | 3344 | 2.6 | 1.93 | 10 | | 0.1 | | 342 | 567 | 6.87 | 13 | 1181 | | |
| 60.5 | 63.6 | 3345 | 3.1 | 1.11 | 360 | | 2.2 | | 5642 | 5766 | 6.64 | 140 | 378 | | |
| 63.6 | 65.5 | 3346 | 1.9 | 1.1 | 5 | | 0.1 | | 399 | 1512 | 6.26 | 48 | 2039 | | |
| 65.5 | 67.0 | 3347 | 1.5 | .47 | 210 | | 0.9 | | 3317 | 534 | 5.14 | 70 | 684 | | |
| 67.0 | 70.0 | 3348 | 3.0 | 1.47 | 190 | | 0.9 | | 2643 | 753 | 5.32 | 73 | 775 | | |
| 70.0 | 73.0 | 3349 | 3.0 | 1.70 | 5 | | 1.2 | | 3301 | 5365 | 4.30 | 76 | 769 | | |
| 73.0 | 76 | 3350 | 3.0 | 1.16 | 260 | | 1.1 | | 2228 | 3133 | 5.41 | 87 | 1422 | | |
| 76.0 | 79 | 3351 | 3.0 | 1.7 | 270 | | 3.1 | | 8456 | 1696 | 5.70 | 308 | 711 | | |
| 79.0 | 82 | 3352 | 3.0 | 2.0 | 210 | | 1.2 | | 4897 | 548 | 5.01 | 228 | 927 | | |
| 82.0 | 85 | 3353 | 3.0 | 1.69 | 330 | | 2.2 | | 4693 | 1567 | 5.24 | 229 | 987 | | |
| 85.0 | 88 | 3354 | 3.0 | .57 | 260 | | 2.2 | | 6633 | 940 | 5.13 | 62 | 1184 | | |
| 88.0 | 91 | 3355 | 3.0 | .69 | 240 | | 4.6 | | 6262 | 15934 | 4.95 | 58 | 557 | | |
| 91.0 | 94 | 3356 | 3.0 | 1.57 | 340 | | 3.8 | | 6197 | 20000 | 6.21 | 107 | 569 | | |
| 94.0 | 97 | 3357 | 3.0 | 1.64 | 290 | | 3.1 | | 12612 | 505 | 4.48 | 72 | 564 | | |
| 97.0 | 100 | 3358 | 3.0 | 1.62 | 470 | | 4.9 | | 6308 | 112 | 5.81 | 60 | 123 | | |
| 100.0 | 103 | 3359 | 3.0 | 2.27 | 375 | | 2.2 | | 5830 | 56 | 5.11 | 29 | 49 | | |
| 103.0 | 106 | 3360 | 3.0 | 2.73 | 5 | | 0.1 | | 596 | 226 | 2.87 | 8 | 1433 | | |
| 106.0 | 109 | 3361 | 3.0 | 2.86 | 5 | | 0.1 | | 34 | 102 | 2.19 | 3 | 1419 | | |
| 109.0 | 112.2 | 3362 | 3.2 | 3.16 | 5 | | 0.1 | | 32 | 145 | 2.15 | 3 | 912 | | |
| 112.2 | 115 | 3363 | 2.8 | 3.04 | 150 | | 0.5 | | 1373 | 60 | 8.77 | 85 | 37 | | |
| 115.0 | 118 | 3364 | 3.0 | 3.0 | 220 | | 0.5 | | 2244 | 71 | 7.99 | 127 | 23 | | |
| 118.0 | 121 | 3365 | 3.0 | 3.0 | 150 | | 0.4 | | 1444 | 95 | 8.28 | 253 | 25 | | |
| 121.0 | 124 | 3366 | 3.0 | 3.0 | 220 | | 0.4 | | 1638 | 34 | 7.99 | 27 | 151 | | |
| 124.0 | 127 | 3367 | 3.0 | 2.78 | 295 | | 0.3 | | 1822 | 34 | 7.95 | 21 | 551 | | |
| 127.0 | 129.0 | 3368 | 2.0 | 1.76 | 210 | | 0.3 | | 1600 | 38 | 7.33 | 16 | 438 | | |
| 129.0 | 132.0 | 3369 | 3.0 | 2.48 | 5 | | 2.1 | | 18 | 859 | 2.13 | 3 | 1097 | | |
| 132.0 | 135.0 | 3370 | 3.0 | 2.81 | 5 | | 0.3 | | 22 | 152 | 2.33 | 3 | 1233 | | |

1988 KERR EXPLORATION PROGRAM



| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 8820 | 10085.5 | 9634.9 | 1568.2 | 90 | 60 | 152.09 | | TEST B-ZONE STRIKE EXTENSION. NO TEST. | |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 135.0 | 138.0 | 3371 | 3.0 | 2.9 | 5 | | 0.3 | | 7 | 159 | 2.02 | 3 | 1200 | | |
| 138.0 | 138.65 | 3372 | .65 | .64 | 30 | | 0.1 | | 591 | 22 | 2.81 | 3 | 2913 | | |
| 138.65 | 141.0 | 3373 | 2.35 | 2.09 | 270 | | 0.6 | | 2608 | 37 | 5.31 | 38 | 377 | | |
| 141.0 | 144.0 | 3374 | 3.0 | 2.89 | 210 | | 0.1 | | 2118 | 25 | 5.92 | 17 | 587 | | |
| 144.0 | 147.0 | 3375 | 3.0 | 2.93 | 285 | | 0.1 | | 987 | 28 | 5.74 | 19 | 1717 | | |
| 147.0 | 150.0 | 3376 | 3.0 | 2.81 | 250 | | 0.1 | | 1207 | 40 | 5.96 | 30 | 623 | | |
| 150.0 | 152.0 | 3377 | 2.0 | 1.93 | 110 | | 0.1 | | 1095 | 36 | 6.37 | 12 | 247 | | |
| 152.0 | 152.09 | | .09 | .09 | | | | | | | | | | | |

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1968 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-3350 | .23 |
| C88-3351 | .87 |
| C88-3352 | .51 |
| C88-3353 | .48 |
| C88-3354 | .70 |
| C88-3355 | .63 |
| C88-3356 | .65 |
| C88-3357 | 1.23 |
| C88-3358 | .63 |
| C88-3359 | .60 |
| C88-3360 | .06 |
| C88-3361 | <.01 |
| C88-3362 | <.01 |
| C88-3363 | .14 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-3364 | .22 |
| C88-3365 | .15 |
| C88-3366 | .15 |
| C88-3367 | .18 |
| C88-3368 | .17 |
| C88-3369 | <.01 |
| C88-3370 | <.01 |
| C88-3371 | <.01 |
| C88-3372 | .06 |
| C88-3373 | .26 |
| C88-3374 | .21 |
| C88-3375 | .09 |
| C88-3376 | .12 |
| C88-3377 | .09 |

DETECTION LIMIT .01

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: 881151 PA  MESTERN CANADIAN MINING CORP.  

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-3320 | 0.1 | 0.11 | 9 | 45 | <3 | 5 | <3 | 0.04 | 0.9 | 19 | 12 | 640 | 5.37 | 0.01 | 0.01 | 12 | 19 | 0.01 | 5 | 0.07 | 30 | <3 | <5 | <2 | 2 | 146 | <5 | <3 |
| C88-3321 | 0.1 | 0.27 | 5 | 110 | <3 | 4 | <3 | 0.17 | 1.1 | 21 | 25 | 2379 | 6.80 | 0.01 | 0.06 | 24 | 23 | 0.01 | 6 | 0.14 | 26 | <3 | <5 | <2 | 2 | 119 | <5 | <3 |
| C88-3322 | 0.1 | 0.29 | 112 | 130 | <3 | 4 | <3 | 0.15 | 1.5 | 24 | 40 | 3397 | 6.80 | 0.01 | 0.05 | 22 | 27 | 0.02 | 7 | 0.14 | 24 | <3 | <5 | <2 | 2 | 55 | <5 | <3 |
| C88-3323 | 0.5 | 0.25 | 271 | 90 | <3 | 5 | <3 | 0.24 | 1.8 | 17 | 26 | 5053 | 4.87 | 0.03 | 0.01 | 27 | 22 | 0.02 | 5 | 0.19 | 37 | <3 | <5 | <2 | 2 | 13 | <5 | <3 |
| C88-3324 | 0.1 | 0.40 | 13 | 220 | <3 | 5 | <3 | 0.23 | 0.6 | 18 | 25 | 3634 | 4.84 | 0.03 | 0.13 | 44 | 39 | 0.01 | 4 | 0.19 | 42 | <3 | <5 | <2 | 2 | 42 | <5 | <3 |
| C88-3325 | 0.1 | 0.39 | 20 | 160 | <3 | 4 | 3 | 0.21 | 1.6 | 17 | 31 | 3756 | 7.69 | 0.03 | 0.07 | 27 | 33 | 0.02 | 4 | 0.17 | 51 | <3 | <5 | <2 | 2 | 24 | <5 | <3 |
| C88-3326 | 0.1 | 0.59 | 8 | 160 | <3 | 5 | <3 | 0.66 | 1.3 | 18 | 49 | 4153 | 5.75 | 0.10 | 0.23 | 306 | 24 | 0.02 | 9 | 0.17 | 23 | <3 | <5 | <2 | 2 | 37 | <5 | <3 |
| C88-3327 | 0.1 | 2.52 | 4 | <5 | <3 | 251 | <3 | 0.37 | 0.9 | 8 | 22 | 291 | 4.28 | 0.09 | 1.25 | 693 | 4 | 0.03 | 3 | 0.16 | 27 | <3 | <5 | <2 | 3 | 23 | <5 | <3 |
| C88-3328 | 0.1 | 0.40 | 49 | 70 | <3 | 8 | <3 | 0.87 | 1.3 | 16 | 34 | 613 | 4.97 | 0.15 | 0.08 | 574 | 2 | 0.02 | 4 | 0.20 | 80 | <3 | <5 | <2 | 2 | 24 | <5 | <3 |
| C88-3329 | 0.1 | 0.27 | 94 | 40 | <3 | 4 | <3 | 1.46 | 2.2 | 18 | 13 | 930 | 6.18 | 0.20 | 0.35 | 1307 | 8 | 0.02 | 4 | 0.18 | 76 | <3 | <5 | <2 | 2 | 35 | <5 | <3 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

ANOMALOUS RESULTS:
FURTHER ANALYSES
BY ALTERNATE
METHODS SUGGESTED

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: 881079 PA — WESTERN CANADIAN MINING CORP. — 

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-3330 | 2.8 | 0.63 | 42 | 20 | <3 | 7 | <3 | 2.80 | 11.6 | 14 | 29 | 284 | 4.56 | 0.27 | 0.41 | 1670 | 3 | 0.03 | 4 | 0.18 | 208 | <3 | <5 | <2 | 2 | 67 | <5 | <3 | 945 |
| C88-3331 | 0.5 | 3.50 | 59 | <5 | <3 | 101 | <3 | 1.98 | 1.4 | 12 | 15 | 122 | 5.99 | 0.24 | 1.94 | 1610 | 7 | 0.02 | 2 | 0.22 | 60 | <3 | <5 | <2 | 3 | 80 | <5 | <3 | 338 |
| C88-3332 | 0.4 | 1.38 | 27 | <5 | <3 | 7 | <3 | 0.47 | 0.8 | 14 | 24 | 685 | 5.38 | 0.09 | 1.20 | 586 | 3 | 0.01 | 3 | 0.19 | 44 | <3 | <5 | <2 | 2 | 57 | <5 | <3 | 125 |
| C88-3333 | 0.4 | 0.99 | 19 | <5 | <3 | 5 | <3 | 0.58 | 1.2 | 14 | 15 | 487 | 5.73 | 0.11 | 1.15 | 766 | 3 | 0.01 | 4 | 0.19 | 58 | <3 | <5 | <2 | 3 | 24 | <5 | <3 | 87 |
| C88-3334 | 0.3 | 2.07 | 20 | 30 | <3 | 8 | <3 | 0.80 | 1.2 | 16 | 42 | 440 | 5.49 | 0.14 | 1.84 | 1369 | 4 | 0.02 | 12 | 0.21 | 39 | <3 | <5 | <2 | 3 | 31 | <5 | <3 | 257 |
| C88-3335 | 0.1 | 3.84 | 5 | <5 | <3 | 233 | 3 | 0.89 | 1.5 | 11 | 17 | 214 | 6.04 | 0.16 | 2.51 | 1957 | 5 | 0.02 | 3 | 0.22 | 38 | <3 | <5 | <2 | 2 | 36 | <5 | <3 | 405 |
| C88-3336 | 1.1 | 1.28 | 35 | <5 | <3 | 8 | <3 | 0.25 | 1.1 | 18 | 14 | 1101 | 5.84 | 0.06 | 1.03 | 246 | 4 | 0.02 | 5 | 0.22 | 45 | <3 | <5 | <2 | 3 | 13 | <5 | <3 | 206 |
| C88-3337 | 0.1 | 1.52 | 19 | 40 | <3 | 7 | <3 | 0.25 | 1.5 | 16 | 30 | 1026 | 6.13 | 0.06 | 0.82 | 849 | 14 | 0.02 | 5 | 0.18 | 35 | <3 | <5 | <2 | 2 | 21 | <5 | <3 | 325 |
| C88-3338 | 0.1 | 6.28 | 6 | <5 | <3 | 280 | 4 | 0.22 | 1.7 | 30 | 31 | 265 | 8.54 | 0.06 | 3.47 | 1060 | 4 | 0.03 | 15 | 0.23 | 56 | <3 | <5 | <2 | 2 | 198 | <5 | <3 | 427 |
| C88-3339 | 0.1 | 2.34 | 45 | 110 | <3 | 12 | <3 | 0.20 | 0.8 | 16 | 31 | 2366 | 6.09 | 0.05 | 1.31 | 425 | 23 | 0.01 | 4 | 0.26 | 52 | <3 | <5 | <2 | 3 | 103 | <5 | <3 | 145 |
| C88-3340 | 0.4 | 1.68 | 51 | 150 | <3 | 11 | <3 | 0.17 | 0.7 | 18 | 46 | 2615 | 5.21 | 0.05 | 0.94 | 316 | 25 | 0.01 | 4 | 0.26 | 57 | <3 | <5 | <2 | 2 | 128 | <5 | <3 | 97 |
| C88-3341 | 0.1 | 5.82 | 73 | <5 | <3 | 318 | 4 | 0.21 | 1.5 | 25 | 19 | 279 | 7.86 | 0.05 | 3.59 | 1343 | 5 | 0.02 | 11 | 0.37 | 59 | <3 | <5 | <2 | 2 | 262 | <5 | <3 | 312 |
| C88-3342 | 1.2 | 0.92 | 52 | 350 | <3 | 10 | <3 | 0.19 | 2.2 | 15 | 21 | 2093 | 6.98 | 0.04 | 0.51 | 162 | 12 | 0.02 | 3 | 0.23 | 64 | <3 | <5 | <2 | 3 | 212 | <5 | <3 | 135 |
| C88-3343 | 1.2 | 1.91 | 39 | 225 | <3 | 12 | 3 | 0.18 | 0.8 | 15 | 39 | 5279 | 4.71 | 0.05 | 1.46 | 393 | 40 | 0.01 | 3 | 0.23 | 42 | <3 | <5 | <2 | 3 | 154 | <5 | <3 | 237 |
| C88-3344 | 0.1 | 3.66 | 13 | 10 | <3 | 768 | 3 | 0.26 | 1.5 | 15 | 39 | 342 | 6.87 | 0.07 | 1.60 | 1181 | 6 | 0.03 | 4 | 0.22 | 36 | <3 | <5 | <2 | 3 | 127 | <5 | <3 | 567 |
| C88-3345 | 2.2 | 1.52 | 140 | 360 | <3 | 12 | 3 | 0.17 | 22.1 | 18 | 28 | 5642 | 6.64 | 0.04 | 1.03 | 378 | 15 | 0.12 | 4 | 0.31 | 210 | <3 | <5 | <2 | 3 | 86 | <5 | <3 | 5766 |
| C88-3346 | 0.1 | 5.17 | 48 | 5 | <3 | 190 | 3 | 0.28 | 2.5 | 14 | 34 | 399 | 6.26 | 0.07 | 3.71 | 2039 | 9 | 0.04 | 1 | 0.40 | 59 | <3 | <5 | <2 | 2 | 322 | <5 | <3 | 1512 |
| C88-3347 | 0.9 | 2.00 | 70 | 210 | <3 | 11 | <3 | 0.16 | 1.1 | 15 | 38 | 3317 | 5.14 | 0.04 | 1.56 | 684 | 8 | 0.02 | 5 | 0.19 | 61 | <3 | <5 | <2 | 3 | 68 | <5 | <3 | 534 |
| C88-3348 | 0.9 | 2.34 | 73 | 190 | <3 | 8 | <3 | 0.19 | 2.2 | 12 | 34 | 2643 | 5.32 | 0.05 | 1.88 | 775 | 11 | 0.02 | 6 | 0.23 | 117 | <3 | <5 | <2 | 3 | 74 | <5 | <3 | 753 |
| C88-3349 | 1.2 | 1.94 | 76 | <5 | <3 | 11 | <3 | 0.16 | 20.4 | 11 | 21 | 3301 | 4.30 | 0.04 | 1.73 | 769 | 22 | 0.10 | 5 | 0.19 | 111 | <3 | <5 | <2 | 3 | 79 | <5 | <3 | 5365 |
| C88-3350 | 1.1 | 2.70 | 87 | 260 | <3 | 8 | <3 | 0.16 | 9.6 | 12 | 48 | 2228 | 5.41 | 0.04 | 2.40 | 1422 | 19 | 0.07 | 11 | 0.17 | 77 | <3 | <5 | <2 | 3 | 91 | <5 | <3 | 3133 |
| C88-3351 | 3.1 | 1.43 | 308 | 270 | <3 | 7 | 3 | 0.15 | 4.8 | 12 | 48 | 8456 | 5.70 | 0.04 | 1.42 | 711 | 12 | 0.04 | 5 | 0.17 | 106 | <3 | <5 | <2 | 3 | 31 | <5 | <3 | 1696 |
| C88-3352 | 1.2 | 2.42 | 228 | 210 | <3 | 7 | 3 | 0.20 | 0.7 | 12 | 39 | 4897 | 5.01 | 0.05 | 2.08 | 927 | 13 | 0.02 | 4 | 0.31 | 66 | <3 | <5 | <2 | 2 | 15 | <5 | <3 | 548 |
| C88-3353 | 2.2 | 2.41 | 229 | 330 | <3 | 7 | 3 | 0.22 | 5.1 | 11 | 39 | 4693 | 5.24 | 0.05 | 2.15 | 987 | 9 | 0.04 | 4 | 0.23 | 75 | <3 | <5 | <2 | 3 | 16 | <5 | <3 | 1567 |
| C88-3354 | 2.2 | 2.78 | 62 | 260 | <3 | 14 | 3 | 0.20 | 2.7 | 14 | 98 | 6633 | 5.13 | 0.06 | 1.91 | 1184 | 14 | 0.03 | 11 | 0.19 | 75 | <3 | <5 | <2 | 9 | 15 | <5 | <3 | 940 |
| C88-3355 | 4.6 | 1.65 | 58 | 240 | <3 | 11 | 3 | 0.19 | 63.1 | 10 | 83 | 6262 | 4.95 | 0.05 | 1.37 | 557 | 14 | 0.33 | 9 | 0.18 | 118 | <3 | <5 | <2 | 3 | 15 | <5 | 21 | 15934 |
| C88-3356 | 3.8 | 1.51 | 107 | 340 | <3 | 11 | 4 | 0.16 | 89.3 | 10 | 41 | 6197 | 6.21 | 0.04 | 1.27 | 569 | 15 | 0.44 | 5 | 0.16 | 84 | <3 | <5 | <2 | 4 | 13 | <5 | 48 | >20000 |
| C88-3357 | 3.1 | 1.60 | 72 | 290 | <3 | 12 | <3 | 0.21 | 1.4 | 11 | 26 | 12612 | 4.48 | 0.05 | 1.36 | 564 | 11 | 0.02 | 6 | 0.24 | 55 | <3 | <5 | <2 | 2 | 34 | <5 | <3 | 505 |
| C88-3358 | 4.9 | 0.61 | 60 | 470 | <3 | 5 | <3 | 0.18 | 0.8 | 12 | 91 | 6308 | 5.81 | 0.05 | 0.29 | 123 | 8 | 0.02 | 6 | 0.17 | 129 | <3 | <5 | <2 | 2 | 10 | <5 | <3 | 112 |
| C88-3359 | 2.2 | 0.37 | 29 | 375 | <3 | 5 | <3 | 0.20 | 0.7 | 11 | 73 | 5830 | 5.11 | 0.05 | 0.09 | 49 | 7 | 0.01 | 4 | 0.17 | 103 | <3 | <5 | <2 | 2 | 21 | <5 | <3 | 56 |
| C88-3360 | 0.1 | 1.44 | 8 | <5 | <3 | 60 | <3 | 1.48 | 0.2 | 10 | 21 | 596 | 2.87 | 0.20 | 0.82 | 1433 | 2 | 0.01 | 3 | 0.11 | 37 | <3 | <5 | <2 | 2 | 86 | <5 | <3 | 226 |
| C88-3361 | 0.1 | 1.47 | <3 | <5 | <3 | 993 | <3 | 2.90 | 0.1 | 6 | 29 | 34 | 2.19 | 0.30 | 0.84 | 1419 | 3 | 0.01 | 2 | 0.10 | 22 | <3 | <5 | <2 | <2 | 196 | <5 | <3 | 102 |
| C88-3362 | 0.1 | 1.39 | <3 | <5 | <3 | 853 | <3 | 1.54 | 0.1 | 6 | 28 | 32 | 2.15 | 0.23 | 0.76 | 912 | 4 | 0.01 | 3 | 0.11 | 19 | <3 | <5 | <2 | <2 | 123 | <5 | <3 | 145 |
| C88-3363 | 0.5 | 0.21 | 85 | 150 | <3 | 10 | <3 | 0.22 | 1.2 | 31 | 39 | 1373 | 8.77 | 0.05 | 0.03 | 37 | 26 | 0.02 | 30 | 0.15 | 45 | <3 | <5 | <2 | 3 | 29 | <5 | <3 | 60 |
| C88-3364 | 0.5 | 0.24 | 127 | 220 | <3 | 4 | <3 | 0.21 | 0.8 | 35 | 57 | 2244 | 7.99 | 0.05 | 0.03 | 23 | 19 | 0.02 | 32 | 0.16 | 30 | <3 | <5 | <2 | 2 | 15 | <5 | <3 | 71 |
| C88-3365 | 0.4 | 0.27 | 253 | 150 | <3 | 3 | <3 | 0.21 | 0.6 | 38 | 57 | 1444 | 8.28 | 0.05 | 0.02 | 25 | 27 | 0.02 | 26 | 0.16 | 43 | <3 | <5 | <2 | 3 | 21 | <5 | <3 | 95 |
| C88-3366 | 0.4 | 0.27 | 27 | 220 | <3 | 4 | <3 | 0.33 | 1.4 | 31 | 36 | 1538 | 7.99 | 0.07 | 0.16 | 151 | 11 | 0.02 | 29 | 0.17 | 25 | <3 | <5 | <2 | 3 | 15 | <5 | <3 | 34 |
| C88-3367 | 0.3 | 0.34 | 21 | 295 | <3 | 4 | <3 | 0.92 | 1.4 | 39 | 73 | 1822 | 7.95 | 0.16 | 0.17 | 551 | 33 | 0.02 | 40 | 0.19 | 28 | <3 | <5 | <2 | 2 | 33 | <5 | <3 | 34 |
| C88-3368 | 0.3 | 0.32 | 16 | 210 | <3 | 4 | <3 | 0.76 | 1.1 | 32 | 89 | 1600 | 7.33 | 0.14 | 0.21 | 438 | 26 | 0.02 | 58 | 0.19 | 35 | <3 | <5 | <2 | 3 | 30 | <5 | <3 | 38 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

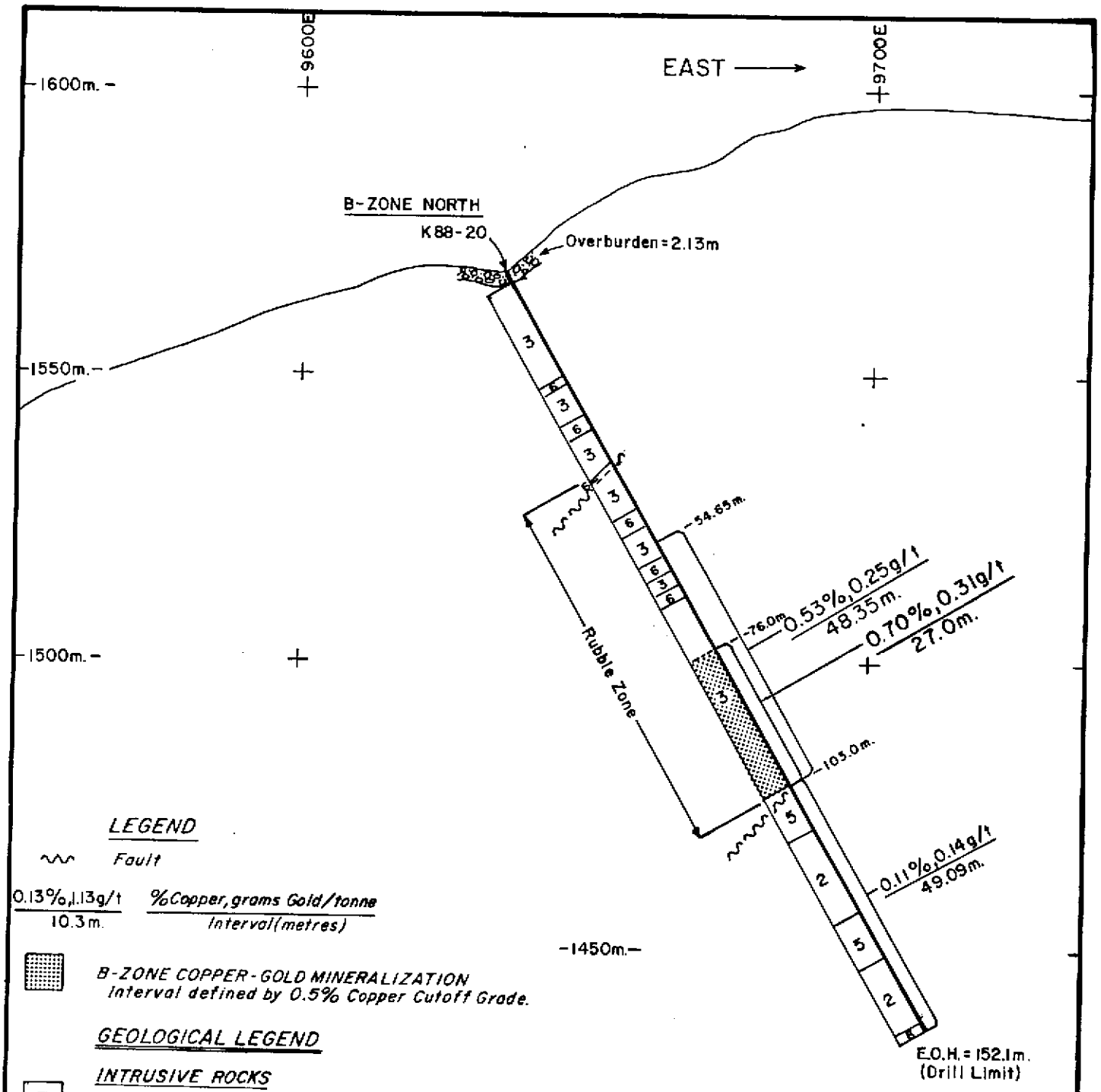
< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

REPORT #: 881079 PA

WESTERN CANADIAN MINING CORP.



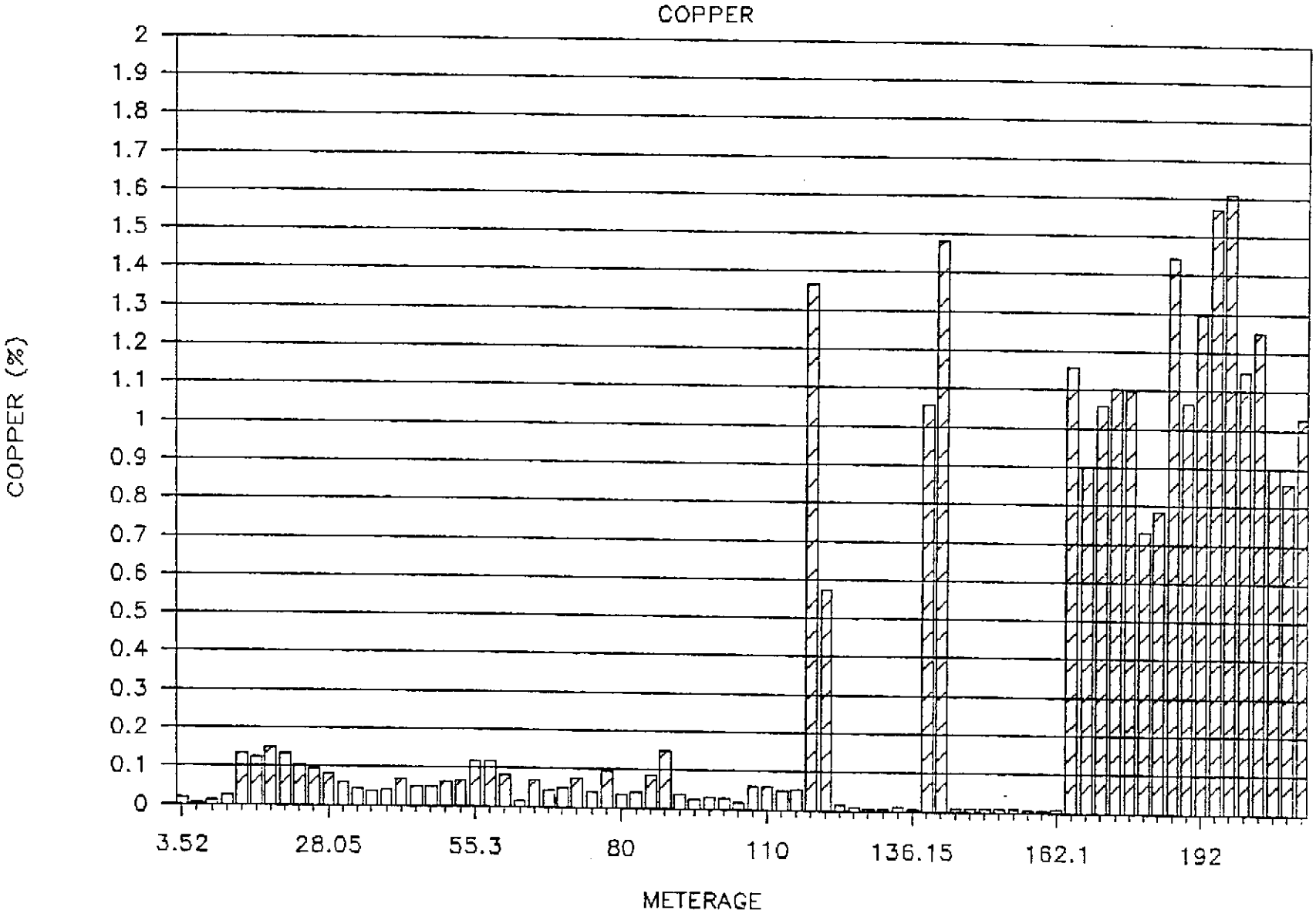
| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88-3369 | 2.1 | 1.04 | <3 | <5 | <3 | 740 | <3 | 1.87 | 11.2 | 6 | 17 | 18 | 2.13 | 0.25 | 0.85 | 1097 | 2 | 0.03 | 4 | 0.10 | 162 | <3 | <5 | <2 | 2 | 124 | <5 | <3 | 859 |
| C88-3370 | 0.3 | 1.51 | <3 | <5 | <3 | >1000 | <3 | 2.06 | 0.5 | 7 | 38 | 22 | 2.33 | 0.27 | 1.02 | 1232 | 2 | 0.01 | 4 | 0.10 | 48 | <3 | <5 | <2 | 2 | 239 | <5 | <3 | 152 |
| C88-3371 | 0.3 | 1.43 | <3 | <5 | <3 | >1000 | <3 | 2.58 | 0.2 | 6 | 37 | 7 | 2.02 | 0.29 | 0.89 | 1200 | 4 | 0.02 | 4 | 0.10 | 32 | <3 | <5 | <2 | <2 | 198 | <5 | <3 | 159 |
| C88-3372 | 0.1 | 0.22 | <3 | 30 | <3 | 38 | <3 | 8.19 | 0.2 | 12 | 144 | 591 | 2.81 | 0.32 | 0.17 | 2913 | 10 | 0.01 | 26 | 0.08 | 35 | <3 | <5 | <2 | <2 | 228 | <5 | <3 | 22 |
| C88-3373 | 0.6 | 0.24 | 38 | 270 | <3 | 9 | <3 | 0.67 | 0.8 | 16 | 38 | 2608 | 5.31 | 0.13 | 0.17 | 377 | 19 | 0.01 | 5 | 0.17 | 55 | <3 | <5 | <2 | 2 | 22 | <5 | <3 | 37 |
| C88-3374 | 0.1 | 0.35 | 17 | 210 | <3 | 5 | <3 | 0.83 | 0.8 | 15 | 77 | 2118 | 5.92 | 0.14 | 0.33 | 587 | 16 | 0.01 | 5 | 0.16 | 40 | <3 | <5 | <2 | 2 | 26 | <5 | <3 | 25 |
| C88-3375 | 0.1 | 0.33 | 19 | 285 | <3 | 5 | 3 | 2.11 | 1.1 | 15 | 42 | 987 | 5.74 | 0.25 | 0.92 | 1717 | 13 | 0.01 | 13 | 0.13 | 27 | <3 | <5 | <2 | 2 | 50 | <5 | <3 | 28 |
| C88-3376 | 0.1 | 0.43 | 30 | 250 | <3 | 5 | <3 | 0.94 | 0.8 | 13 | 59 | 1207 | 5.96 | 0.16 | 0.41 | 623 | 8 | 0.01 | 5 | 0.17 | 26 | <3 | <5 | <2 | 2 | 52 | <5 | <3 | 40 |
| C88-3377 | 0.1 | 0.36 | 12 | 110 | <3 | 5 | <3 | 0.57 | 0.8 | 15 | 24 | 1095 | 6.37 | 0.11 | 0.19 | 247 | 2 | 0.01 | 3 | 0.19 | 32 | <3 | <5 | <2 | 2 | 24 | <5 | <3 | 36 |

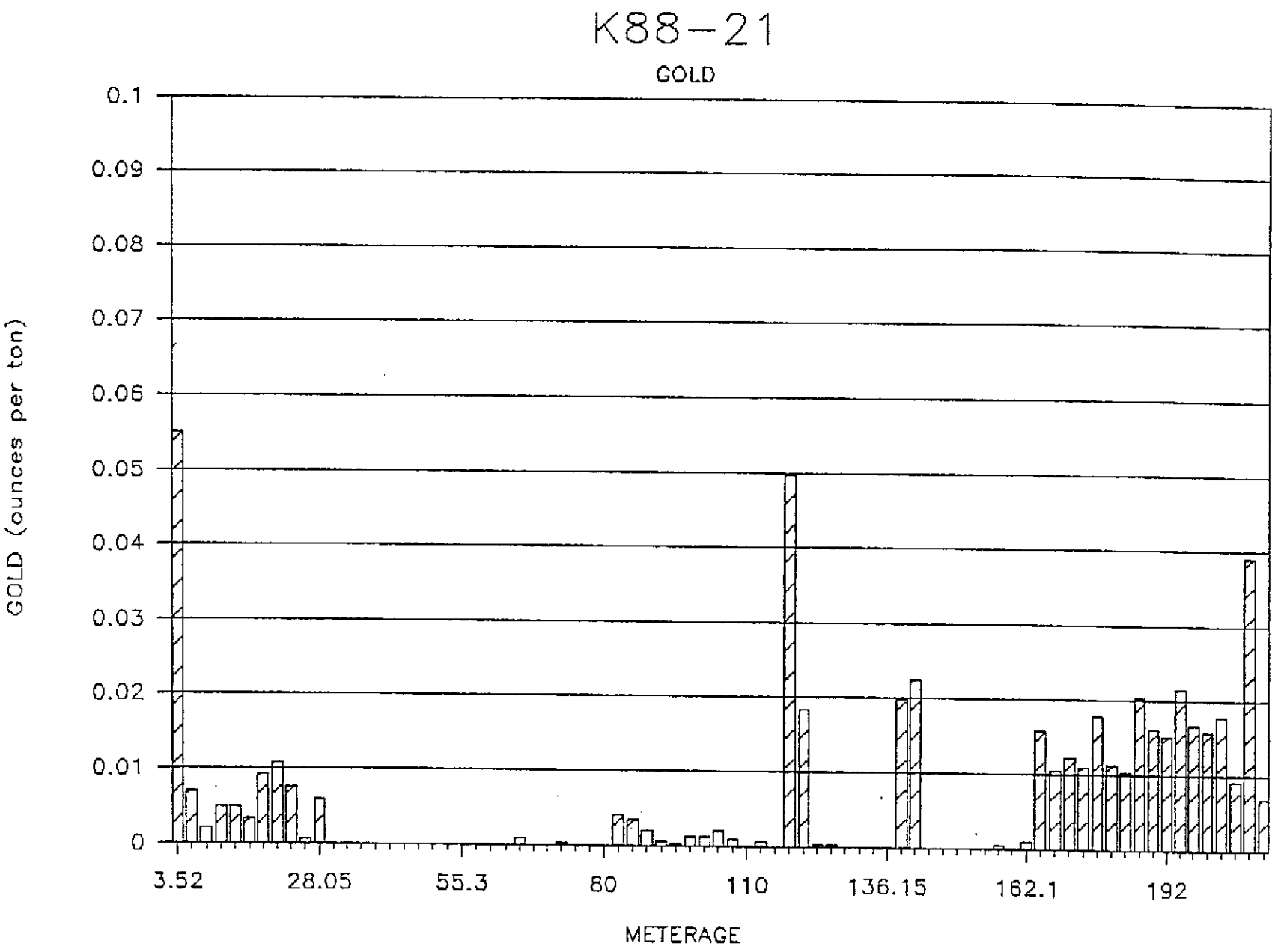



## LEGEND

~~~ Fault

0.13%, 1.13g/t / 10.3m. — %Copper, grams Gold/tonne / Interval (metres)

B-ZONE COPPER-GOLD MINERALIZATION
Interval defined by 0.5% Copper Cutoff Grade.

## GEOLOGICAL LEGEND

### INTRUSIVE ROCKS

7 — BASALT DYKE – fine-grained to aphanitic, slightly magnetic, occassional hornblende and/or biotite phenocrysts.

6 — ANDESITE DYKE – medium green colour, fine-grained, generally chloritized.

5 — PLAGIOCLASE PORPHYRY DYKE – aphanitic light green matrix with up to 2cm. long plagioclase phenocrysts and rare hornblende phenocrysts.

4 — DIORITE(4a)/MONZONITE(4b) – medium to coarse-grained, inequigranular, variable potassium feldspar content.

### VOLCANIC and SEDIMENTARY ROCKS

3 — SERICITE-QUARTZ-PYRITE SCHIST – foliated and intensely sericitized volcaniclastic, subvolcanic and intrusive rocks.

2 — DACITIC VOLCANICS (ASH TUFF(2a), CRYSTAL TUFF(2b), LAPILLI TUFF(2c)) – interbedded and alternating fine-grained Ash Tuff, medium to coarse-grained Crystal Tuff, and Lapilli Tuff.

1 — SILTSTONE/SHALE/SANDSTONE – interlaminated, bedded, dark brown to black, fine to medium-grained sedimentary rocks.

SCALE: 1:1000 (0, 10, 20, 30, 40 Metres)

# SULPHURETS GOLD CORPORATION
## 1989 KERR PROJECT
## D.D.H. K88-20
## SECTION

COLLAR: -10085.5N, 9634.9E
BEARING: 090° DIP: -60°
ELEVATION: 1568.1m.

REPORT: 1065 FIGURE No.
~~~

# K88-21


COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
3.52
28.05
55.3
80
110
136.15
162.1
192
METERAGE


K88-21
GOLD
GOLD (ounces per ton)
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
3.52
28.05
55.3
80
110
136.15
162.1
192
METERAGE

KERR PROJECT D.D.HOLE K-88-21

LOCATION VERTICAL HOLE BETWEEN K-88-1 AND K-88-11
DATE STARTED AUGUST 17, 1988
DATE COMPLETED AUGUST 19, 1988
CORE RECOVERY 87.98%
DRILLED BY FALCON DRILLING LTD
LOGGED BY S. CASSELMAN
OBJECTIVE TEST DOWN DIP EXTENSION OF B-ZONE FAULT / MINERALIZATION
DIP TEST DEPTH _____m DIP_____deg
DEPTH _____m DIP_____deg

COLLAR LAT. 9598.1 NORTH
LONG. 9767.3 EAST
ELEVATION 1674.3 m
AZIMUTH - DIP -90 deg
LENGTH 213.05
HOR. PROJ. 0.00 m
VERT.PROJ. 213.05 m

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 1.52 | 1.52 | OVERBURDEN |
| 1.52 | 9.40 | 7.88 | SERICITE SCHIST<br>- light grey to greenish<br>- variable intensity of schistosity from weak to strong<br>- where developed foliation at 20 deg to C.A.<br>- ghost crystals evident, protolith could be dacitic tuff to crystal tuff or quite possibly intensely altered andesite dyke<br>- top 2 m quite weathered, abundant limonite and quite pitted<br>- core is fairly fractured, average piece 10 to 15 cm<br>- approximately 7% pyrite as fine disseminations and stringers |
| 9.40 | 28.05 | 18.65 | FINE-GRAINED ANDESITE DYKE<br>- dark grey green, homogeneous<br>- intensely chloritized, weak sericitized<br>- quite fractured, average piece 5 to 10 cm<br>- fair amount of limonite on fractures<br>- fractures at 30 to 65 deg to C.A.<br>- patches of up to 30% pyrite for 10 cm width<br>- overall 8 to 10% pyrite<br>- upper contact quite sharp at 30 deg to C.A., marked by 1 cm quartz vein<br>- lower contact gradational at 30 deg to C.A. |
| 28.05 | 55.30 | 7.25 | SERICITE SCHIST<br>- more intensely sericitized and foliated than 1.52 to 9.4 m, especially from 28.05 to 42.0 m<br>- overall light grey colour<br>- foliated at 40 deg to C.A. |

KERR PROJECT D.D.HOLE K-88-21

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - protolith appears to be dacitic lapilli tuff from 36.3 to 37.6 and from 39.3 to 41.5 m, however all appears to be altered dacitic volcanics but definite identification is difficult<br>- approximately 5 to 7% pyrite overall-relatively uninteresting<br>- native copper deposits on fracture surface, especially at 53.0 m |
| 55.30 | 55.80 | 0.50 | FINE-GRAINED ANDESITE DYKE<br>- medium green colour<br>- moderate to strong chloritization, weak sericitization<br>- 5% quartz-calcite veining, 21% pyrite<br>- specs of dendritic native copper on fracture surfaces (.5%)<br>- upper contact at 70 deg, lower contact at 30 deg to C.A. |
| 55.80 | 62.60 | 6.80 | SERICITE-QUARTZ-PYRITE SCHIST<br>- similar to 28.05 to 55.3 m<br>- light to medium grey<br>- 20 cm quartz vein at 59.40 m<br>- slight, wavy foliation, well developed at 30 deg to C.A., defined by sericite, and occasional pyrite laminae<br>- up to 5% chlorite<br>- traces of chalcocite, generally associated with pyrite veinlets<br>- faint traces of native copper on weathered fracture surfaces<br>- protolith appears to be dacitic lapilli tuff |
| 62.60 | 68.00 | 5.40 | FINE-GRAINED ANDESITE DYKE<br>- medium green<br>- 3 to 5% quartz-calcite veins at 40 to 80 deg to C.A., .2 to 2 cm wide generally with wisps and blebs of chlorite<br>- intense chloritization, weak to no sericitization<br>- < 1% pyrite, very faint traces of blood-red native copper on rare weathered fracture surfaces<br>- upper contact at 35 deg, lower contact at 40 deg to C.A. |

KERR PROJECT D.D.HOLE K-88-21

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 68.00 | 119.80 | 51.80 | QUARTZ-SERICITE-PYRITE SCHIST<br>- light to medium grey to grey green<br>- well foliated at 30 deg to C.A.<br>- intensely sericitized<br>- from 72.5 to 81.5 is moderately chloritized, elsewhere is weakly chloritized<br>- also from 72.5 to 81.5 have weak epidotization (1%) as spots and wisps<br>- pyrite occurs mainly as fine disseminations within foliation planes<br>- from 85.0 m begin to get blebs and stringers of pyrite as well as coarse aggregate spots<br>- silicification begins to occur from approximately 85.0 m and becomes quite prominent (10 to 30%) at 116.0 m<br>- traces of chalcocite associated with pyrite<br>- chalcocite increases with silicification (at 116 m) and begins to get chalcopyrite (to .3%) |
| 119.80 | 136.15 | 16.35 | FINE TO MEDIUM-GRAINED ANDESITE DYKE<br>- similar to 62.6 to 68.0 m<br>- medium to dark green colour<br>- intense chlorite, weak sericite<br>- 1 to 3% quartz-calcite veining<br>- chlorite blotches in quartz-calcite veins<br>- 1 to 2% epidote in veins<br>- no native copper visible on fracture surfaces<br>- < 1% pyrite<br>- upper contact at 60 deg, lower at 40 deg to C.A.<br>- quite fractured from 133 to 136.15, average piece 5 to 10 cm long |
| 136.15 | 140.70 | 4.55 | SILICIFIED SULPHIDE BRECCIA<br>- dark blue-grey with abundant milky white to grey silicified sections and quartz veins<br>- 15 to 20% pyrite, up to 1% chalcopyrite as fine blebs,and 1 to 3% chalcocite associated with other sulphides<br>- similar to silicified section between 116.0 and 119.0 m, however more intensely silicified, with greater amount of chalcocite and beginning to get chalcopyrite<br>- moderately to strongly chloritized very weakly to non-sericitized<br>- moderately fractured average piece 10 cm long<br>- fractured at 55 to 65 deg to C.A. |

KERR PROJECT D.D.HOLE K-88-21

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 140.70 | 162.10 | 21.40 | FINE-GRAINED ANDESITE DYKE<br>- dark green colour<br>- as in section 119.8 to 136.15 m<br>- quite fractured, average piece 5 to 10 cm long<br>- fractured at 25 to 50 deg to C.A.<br>- 1 to 3% quartz-calcite veins<br>- < 1% pyrite<br>- traces of native copper on fracture surfaces<br>- upper contact at 65 deg, lower contact at 55 deg to C.A. |
| 162.10 | 213.05 | 50.95 | SILICA STOCKWORK, SULPHIDE ZONE<br>- light to medium grey with faint blue tint, with abundant bull white to light grey silicified bands and patches and quartz veins<br>- silicified zone starts at 116 m to 199.8 m then is interrupted by andesite dyke, zone continues at footwall of dyke, from 136.15 to 140.7 is interrupted by another dyke, then continues throughout this section<br>- this section (162.1 to E.O.H.) is much more mineralized than previous sections, however<br>- approaching core of silica stockwork zone<br>- protolith is probably dacitic volcanic although all evidence has been wiped out by alteration<br>- rock has undergone intense sericitization, weak to moderate chloritization, patches of weak epidotization, as well as pyritization (with some chalcopyrite and chalcocite)<br>- followed by intense silicification which has wiped out much of the previous alteration<br>- with silicification occurs the majority of the chalcopyrite and chalcocite<br>- where sericite and chlorite is present, a strong foliation is developed at 40 deg to C.A.<br>- silicification occurs parallel to, and across foliation at 25 to 70 deg to C.A.<br>- pyrite occurs as fine disseminations, stringers, and bands 1 mm to 10 cm wide, parallel to foliation and as stringers and blebs in silicified zone<br>- chalcopyrite occurs as wispy blebs generally within pyrite veinlets in silicified zones<br>- chalcocite occurs generally associated with other sulphides as very fine-grained masses surrounding other sulphides |

KERR PROJECT D.D.HOLE K-88-21

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - occasional rare limy green epidote stringer |
| | | | E.O.H. |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 12:52:52 Page 1

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | |
|---|---|---|---|---|---|---|---|---|---|
| 8821 | 9598.2 | 9767.3 | 1674.3 | | 90 | 213.05 | | DOWN DIP CONTINUITY,B-ZONE SOUTH. | #HOLE |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 1.52 | 1.52 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 1.52 | 3.52 | 2.0 | 24 | SRCT SCHT | | F-MG | 1 | 1 | 70 | 8 | 0 | 0 | 0 | | | | 90 | 5 | 0 | | 0 | 0 | | |
| 3.52 | 5.25 | 1.73 | 23 | SRCT SCHT | | F-MG | 1 | 1 | 70 | 10 | 0 | 0 | 0 | | | | 90 | 5 | 0 | | 0 | 0 | | |
| 5.25 | 8.0 | 2.75 | 25 | SRCT SCHT | | F-MG | 1 | 1 | 65 | 5 | 3 | 0 | 0 | | | | 85 | 7 | 0 | | 0 | 0 | | |
| 8.0 | 9.4 | 1.4 | 29 | SRCT SCHT | | F-MG | 1 | 3 | 65 | 5 | 3 | 0 | 0 | | | | 90 | 5 | 0 | | 0 | 0 | | |
| 9.4 | 12.0 | 2.6 | 26 | ANDS DYKE | | FG | 0 | 2 | 5 | 5 | 45 | 0 | 0 | | | | 70 | 10 | 0 | | 0 | 0 | | |
| 12.0 | 15.0 | 3.0 | 29 | ANDS DYKE | | FG | 0 | 2 | 3 | 3 | 45 | 0 | 0 | | | | 65 | 1 | 0 | | 0 | 0 | | |
| 15.0 | 18.0 | 3 | 41 | ANDS DYKE | | FG | 0 | 1 | 8 | 2 | 45 | 0 | 0 | | | | 65 | 5 | 0 | | 0 | 0 | | |
| 18.0 | 21.0 | 3 | 36 | ANDS DYKE | | FG | 0 | 2 | 5 | 2 | 45 | 0 | 0 | | | | 70 | 10 | 0 | | 0 | .1 | | |
| 21.0 | 24.0 | 3 | 42 | ANDS DYKE | | FG | 0 | 2 | 10 | 1 | 35 | 0 | 0 | | | | 60 | 5 | 0 | | 0 | .1 | | |
| 24.0 | 27.0 | 3 | 42 | ANDS DYKE | | FG | 0 | 5 | 15 | 1 | 30 | 0 | 0 | | | | 60 | 8 | .1 | | 0 | 0 | | |
| 27.0 | 28.05 | 1.05 | 46 | ANDS DYKE | | FG | 0 | 2 | 20 | 1 | 25 | 0 | 0 | | | | 60 | 5 | 0 | | 0 | 0 | | |
| 28.05 | 30.0 | 1.95 | 21 | SRCT SCHT | | FG | 0 | 0 | 70 | 8 | 5 | 0 | 0 | | | | 100 | 10 | 0 | | 0 | 0 | | |
| 30.0 | 33.0 | 3 | 22 | SRCT SCHT | | FG | 0 | 0 | 70 | 8 | 3 | 0 | 0 | | | | 100 | 12 | 0 | | 0 | 0 | | |
| 33.0 | 36.0 | 3 | 27 | SRCT SCHT | | FG | 0 | 1 | 75 | 3 | 5 | 0 | 0 | | | | 100 | 5 | 0 | | 0 | 0 | | |
| 36.0 | 39.0 | 3 | 28 | SRCT SCHT | | FG | 0 | 0 | 75 | 2 | 10 | 0 | 0 | | | | 100 | 8 | 0 | | 0 | 0 | | |
| 39.0 | 42.0 | 3 | 29 | SRCT SCHT | | FG | 0 | 2 | 75 | 2 | 8 | 0 | 0 | | | | 100 | 8 | 0 | | 0 | 0 | | |
| 42.0 | 45.0 | 3 | 38 | SRCT SCHT | | FG | 0 | 2 | 65 | 1 | 8 | 0 | 0 | | | | 90 | 10 | 0 | | 0 | 0 | | |
| 45.0 | 48.0 | 3 | 48 | SRCT SCHT | | FG | 0 | 1 | 65 | 1 | 8 | 0 | 0 | | | | 90 | 8 | 0 | | 0 | 0 | | |
| 48.0 | 51.0 | 3 | 44 | SRCT SCHT | | FG | 0 | 2 | 65 | 2 | 10 | .5 | 0 | | | | 90 | 8 | 0 | | 0 | 0 | | |
| 51.0 | 54.0 | 3 | 37 | SRCT SCHT | | FG | 1 | 2 | 65 | 1 | 5 | .8 | 0 | | | | 90 | 10 | 0 | | 0 | .1 | | |
| 54.0 | 55.3 | 1.3 | 33 | SRCT SCHT | | FG | 0 | 1 | 60 | 1 | 8 | 1 | 0 | | | | 90 | 5 | 0 | | 0 | .1 | | |
| 55.3 | 55.8 | .5 | 39 | ANDS DYKE | | FG | 0 | 5 | 8 | 2 | 25 | 2 | 5 | | | | 45 | .5 | 0 | | 0 | 0 | | |
| 55.8 | 58.0 | 2.2 | 35 | SRCT SCHT | | F-MG | 2 | 3 | 60 | 1 | 10 | 2 | 0 | | | | 95 | 12 | 0 | | .2 | .1 | | |
| 58.0 | 60.0 | 2 | 29 | SRCT SCHT | | F-MG | 2 | 8 | 60 | 2 | 5 | .5 | 0 | | | | 95 | 12 | 0 | | .5 | 0 | | |
| 60.0 | 62.6 | 2.6 | 24 | SRCT SCHT | | F-MG | 1 | 5 | 60 | 1 | 5 | .5 | 0 | | | | 95 | 15 | 0 | | .8 | .1 | | |
| 62.0 | 65.0 | 2.4 | 39 | ANDS DYKE | | FG | 0 | 3 | 8 | 5 | 25 | 1 | 5 | | | | 45 | 1 | 0 | | 0 | .1 | | |
| 65.0 | 68.0 | 3 | 32 | ANDS DYKE | | FG | 0 | 5 | 15 | 2 | 30 | 2 | 5 | | | | 60 | .5 | 0 | | 0 | 0 | | |
| 68.0 | 71.0 | 3 | 23 | SRCT SCHT | | F-CG | 1 | 2 | 70 | 1 | 5 | .5 | 0 | | | | 95 | 10 | 0 | | .8 | 0 | | |
| 71.0 | 74.0 | 3 | 38 | SRCT SCHT | | F-CG | 1 | 1 | 65 | 1 | 15 | 1 | 0 | | | | 95 | 12 | 0 | | .2 | 0 | | |
| 74.0 | 77 | 3 | 33 | SRCT SCHT | | F-CG | 1 | 1 | 60 | 1 | 20 | 2 | 0 | | | | 100 | 10 | 0 | | .8 | .1 | | |
| 77 | 80 | 3 | 40 | SRCT SCHT | | F-CG | 0 | 1 | 60 | 1 | 18 | 3 | 1 | | | | 100 | 5 | 0 | | 0 | .1 | | |
| 80 | 83 | 3 | 38 | SRCT SCHT | | F-CG | 2 | 1 | 65 | 1 | 15 | 2 | 1 | | | | 100 | 7 | 0 | | 1 | .1 | | |
| 83 | 86 | 3 | 25 | SRCT SCHT | | F-CG | 2 | .5 | 70 | 2 | 10 | 3 | .5 | | | | 100 | 7 | 0 | | .2 | .1 | | |
| 86 | 89 | 3 | 39 | SRCT SCHT | | F-CG | 3 | 2 | 70 | .5 | 5 | .5 | 1 | | | | 100 | 10 | 0 | | .5 | 0 | | |
| 89 | 92 | 3 | 47 | SRCT SCHT | | F-CG | 1 | 1 | 70 | 0 | 8 | .5 | 2 | | | | 100 | 10 | 0 | | .1 | 0 | | |
| 92 | 95 | 3 | 51 | SRCT SCHT | | F-CG | 0 | 1 | 70 | 0 | 10 | .2 | 2 | | | | 100 | 12 | 0 | | .1 | 0 | | |
| 95 | 98 | 3 | 50 | SRCT SCHT | | F-CG | 2 | 0 | 75 | 0 | 8 | 0 | 1 | | | | 100 | 10 | 0 | | .1 | 0 | | |
| 98 | 101 | 3 | 44 | SRCT SCHT | | F-CG | 1 | 1 | 75 | 0 | 5 | 0 | .5 | | | | 100 | 10 | 0 | | .1 | 0 | | |
| 101 | 104 | 3 | 34 | SRCT SCHT | | F-CG | 5 | 1 | 65 | 0 | 10 | 1 | 1 | | | | 100 | 15 | .1 | | .5 | 0 | | |
| 104 | 107 | 3 | 10 | SRCT SCHT | | F-CG | 5 | 2 | 65 | 0 | 10 | 3 | 1 | | | | 100 | 10 | .1 | | .2 | 0 | | |
| 107 | 110 | 3 | 31 | SRCT SCHT | | F-CG | 1 | 5 | 70 | 0 | 8 | 1 | 1 | | | | 100 | 8 | 0 | | .1 | 0 | | |
| 110 | 113 | 3 | 29 | SRCT SCHT | | F-CG | 5 | 8 | 65 | 1 | 3 | 1 | .2 | | | | 100 | 10 | 0 | | .2 | 0 | | |
| 113 | 116 | 3 | 33 | SRCT SCHT | | F-CG | 10 | 1 | 70 | 0 | 3 | .5 | 0 | | | | 100 | 10 | 0 | | .5 | 0 | | |
| 116 | 118 | 2 | 27 | SRCT SCHT | | F-CG | 35 | 2 | 20 | 0 | 15 | .2 | 0 | | | | 100 | 20 | .5 | | 2 | 0 | | |
| 118 | 119.8 | 1.8 | 36 | SRCT SCHT | | F-CG | 25 | 3 | 25 | 0 | 20 | 0 | 0 | | | | 100 | 22 | .5 | | 3 | 0 | | |
| 119.8 | 122 | 2.2 | 40 | ANDS DYKE | | FG | 0 | 1 | 5 | 0 | 35 | 2 | 3 | | | | 50 | .5 | 0 | | 0 | 0 | | |
| 122 | 125.0 | 3 | 40 | ANDS DYKE | | FG | 0 | 2 | 7 | 0 | 30 | 1 | 3 | | | | 45 | .5 | 0 | | 0 | 0 | | |
| 125 | 128.0 | 3 | 36 | ANDS DYKE | | FG | 0 | 1 | 3 | 1 | 30 | 0 | 3 | | | | 40 | .5 | 0 | | 0 | 0 | | |
| 128 | 131.0 | 3 | 46 | ANDS DYKE | | FG | 0 | 1 | 10 | 1 | 35 | 0 | 2 | | | | 50 | .5 | 0 | | 0 | 0 | | |
| 131 | 134.0 | 3 | 35 | ANDS DYKE | | FG | 0 | .5 | 10 | 3 | 30 | 0 | 1 | | | | 45 | .5 | 0 | | 0 | 0 | | |
| 134 | 136.15 | 2.15 | 32 | SILC SULP BREC | | FG | 0 | 0 | 10 | 1 | 25 | .5 | 1 | | | | 40 | .5 | 0 | | 0 | 0 | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 12:56:44 Page 2

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8821 | 9598.2 | 9767.3 | 1674.3 | | 90 | 213.05 | | DOWN DIP CONTINUITY,B-ZONE SOUTH. #HOLE |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 136.15 | 138.5 | 2.35 | 17 | SILC SULP BREC | | F-MG | 25 | 5 | 18 | 0 | 20 | 3 | 0 | | | | 100 | 25 | 1.5 | | 1.5 | 0 | | |
| 138.5 | 140.7 | 2.2 | 33 | SILC SULP BREC | | F-MG | 30 | 10 | 10 | 0 | 18 | 2 | 0 | | | | 100 | 25 | 1.5 | | 1.5 | 0 | | |
| 140.7 | 143.0 | 2.3 | 33 | ANDS DYKE | | FG | 0 | 1 | 8 | 1 | 25 | .5 | 2 | | | | 40 | .5 | 0 | | 0 | 0 | | |
| 143.0 | 146.0 | 3 | 36 | ANDS DYKE | | FG | 0 | 5 | 10 | 1 | 20 | 5 | 2 | | | | 45 | .5 | 0 | | 0 | 0 | | |
| 146.0 | 149.0 | 3 | 38 | ANDS DYKE | | FG | 0 | 4 | 5 | 2 | 30 | 2 | 1 | | | | 45 | .5 | 0 | | 0 | 0 | | |
| 149.0 | 152.0 | 3 | 37 | ANDS DYKE | | FG | 0 | 5 | 10 | 2 | 20 | 2 | 2 | | | | 45 | .5 | 0 | | 0 | 0 | | |
| 152.0 | 155.0 | 3 | 38 | ANDS DYKE | | FG | 0 | 5 | 3 | 1 | 30 | 3 | 2 | | | | 45 | .5 | 0 | | 0 | 0 | | |
| 155.0 | 158.0 | 3 | 39 | ANDS DYKE | | FG | 0 | 3 | 8 | 1 | 25 | 8 | 3 | | | | 50 | 1 | 0 | | 0 | .1 | | |
| 158.0 | 160.0 | 2 | 36 | ANDS DYKE | | FG | 0 | 2 | 5 | 1 | 25 | 3 | 1 | | | | 40 | .5 | 0 | | 0 | 0 | | |
| 160 | 162.1 | 2.1 | 32 | ANDS DYKE | | FG | 0 | 1 | 5 | 2 | 25 | 3 | 1 | | | | 40 | .5 | 0 | | 0 | 0 | | |
| 162.1 | 165.0 | 2.9 | 26 | SILC SULP STWK | | F-MG | 25 | 5 | 40 | 1 | 2 | 1 | 0 | | | | 100 | 20 | 1.5 | | 1.5 | 0 | | |
| 165.0 | 168 | 3 | 24 | SILC SULP STWK | | F-MG | 10 | 5 | 55 | 1 | 5 | 2 | 0 | | | | 100 | 15 | .5 | | 2 | 0 | | |
| 168 | 171 | 3 | 28 | SILC SULP STWK | | F-MG | 25 | 5 | 35 | 0 | 5 | 1 | 0 | | | | 100 | 22 | 1.5 | | 3 | 0 | | |
| 171 | 174 | 3 | 34 | SILC SULP STWK | | F-MG | 30 | 5 | 35 | 1 | 2 | 2 | 0 | | | | 100 | 20 | 1 | | 3 | 0 | | |
| 174 | 177 | 3 | 34 | SILC SULP STWK | | F-MG | 20 | 5 | 40 | 1 | 5 | 2 | 0 | | | | 100 | 20 | 1.5 | | 3 | 0 | | |
| 177 | 180 | 3 | 32 | SILC SULP STWK | | F-MG | 30 | 5 | 35 | 1 | 5 | 1 | 0 | | | | 100 | 20 | .8 | | 2 | 0 | | |
| 180 | 183 | 3 | 10 | SILC SULP STWK | | F-MG | 20 | 3 | 45 | 2 | 5 | 3 | 0 | | | | 100 | 18 | .8 | | 2 | 0 | | |
| 183 | 186 | 3 | 24 | SILC SULP STWK | | F-MG | 20 | 5 | 30 | 2 | 8 | 1 | 1 | | | | 100 | 25 | 1.5 | | 3 | 0 | | |
| 186 | 189 | 3 | 29 | SILC SULP STWK | | F-MG | 20 | 8 | 35 | 0 | 8 | .5 | 2 | | | | 100 | 22 | 1.5 | | 2 | 0 | | |
| 189 | 192 | 3 | 33 | SILC SULP STWK | | F-MG | 30 | 5 | 25 | 1 | 5 | .5 | 1 | | | | 100 | 25 | 1.5 | | 3 | 0 | | |
| 192 | 195 | 3 | 25 | SILC SULP STWK | | F-MG | 30 | 5 | 25 | 1 | 8 | .2 | 1 | | | | 100 | 20 | 2 | | 3 | 0 | | |
| 195 | 198 | 3 | 26 | SILC SULP STWK | | F-MG | 25 | 3 | 35 | 1 | 8 | .2 | 0 | | | | 100 | 20 | 2 | | 3 | 0 | | |
| 198 | 201 | 3 | 33 | SILC SULP STWK | | F-MG | 20 | 3 | 45 | 2 | 5 | 0 | 0 | | | | 100 | 20 | 1 | | 2 | 0 | | |
| 201 | 204 | 3 | 29 | SILC SULP STWK | | F-MG | 25 | 3 | 40 | 1 | 2 | 1 | 0 | | | | 100 | 22 | 1 | | 1.5 | 0 | | |
| 204 | 207 | 3 | 16 | SILC SULP STWK | | F-MG | 25 | 3 | 40 | 2 | 3 | 1 | 0 | | | | 100 | 22 | 1 | | 1.5 | 0 | | |
| 207 | 210 | 3 | 10 | SILC SULP STWK | | F-MG | 20 | 5 | 40 | 3 | 3 | 1 | 0 | | | | 100 | 25 | .5 | | 1.5 | 0 | | |
| 210 | 213.05 | 3.05 | 22 | SILC SULP STWK | | F-MG | 15 | 5 | 50 | 1 | 5 | .5 | 0 | | | | 100 | 18 | 1 | | 2 | 0 | | |

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8821 | 9598.2 | 9767.3 | 1674.3 | | 90 | 213.05 | | DOWN DIP CONTINUITY,B-ZONE SOUTH. #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 1.52 | | 1.52 | 0 | | | | | | | | | | | |
| 1.52 | 3.52 | 3378 | 2.0 | .46 | 1890 | | 25.8 | | 194 | 35 | 5.83 | 52 | 145 | | |
| 3.52 | 5.25 | 3379 | 1.73 | 1.45 | 240 | | 19.1 | | 55 | 9 | 3.54 | 23 | 10 | | |
| 5.25 | 8.0 | 3380 | 2.75 | 2.29 | 70 | | 1.1 | | 119 | 25 | 3.10 | 41 | 12 | | |
| 8.0 | 9.4 | 3381 | 1.4 | 1.3 | 165 | | 1.1 | | 238 | 12 | 1.77 | 55 | 9 | | |
| 9.4 | 12.0 | 3382 | 2.6 | 2.02 | 170 | | 1.1 | | 1319 | 192 | 6.70 | 47 | 913 | | |
| 12.0 | 15.0 | 3383 | 3.0 | 2.7 | 110 | | 0.1 | | 1249 | 215 | 4.56 | 30 | 1552 | | |
| 15.0 | 18.0 | 3384 | 3 | 3.0 | 315 | | 0.1 | | 1494 | 96 | 4.99 | 119 | 644 | | |
| 18.0 | 21.0 | 3385 | 3 | 2.83 | 370 | | 0.3 | | 1309 | 116 | 4.59 | 60 | 809 | | |
| 21.0 | 24.0 | 3386 | 3 | 2.8 | 260 | | 0.2 | | 1042 | 98 | 4.64 | 141 | 585 | | |
| 24.0 | 27.0 | 3387 | 3 | 2.74 | 20 | | 0.1 | | 960 | 95 | 4.97 | 219 | 291 | | |
| 27.0 | 28.05 | 3388 | 1.05 | 1.05 | 200 | | 0.1 | | 836 | 66 | 5.89 | 16 | 320 | | |
| 28.05 | 30.0 | 3389 | 1.95 | 1.95 | 5 | | 0.1 | | 609 | 31 | 4.74 | 18 | 45 | | |
| 30.0 | 33.0 | 3390 | 3 | 1.45 | 5 | | 0.1 | | 432 | 18 | 4.93 | 22 | 14 | | |
| 33.0 | 36.0 | 3391 | 3 | 2.52 | 5 | | 0.1 | | 368 | 15 | 4.47 | 34 | 7 | | |
| 36.0 | 39.0 | 3392 | 3 | 2.80 | 5 | | 0.1 | | 404 | 13 | 4.69 | 19 | 18 | | |
| 39.0 | 42.0 | 3393 | 3 | 2.90 | 5 | | 0.1 | | 676 | 58 | 6.67 | 31 | 440 | | |
| 42.0 | 45.0 | 3394 | 3 | 2.92 | 5 | | 0.1 | | 481 | 28 | 6.39 | 37 | 33 | | |
| 45.0 | 48.0 | 3395 | 3 | 2.88 | 5 | | 0.1 | | 482 | 15 | 5.53 | 34 | 24 | | |
| 48.0 | 51.0 | 3396 | 3 | 3.0 | 5 | | 0.1 | | 621 | 56 | 5.80 | 25 | 451 | | |
| 51.0 | 54.0 | 3397 | 3 | 2.78 | 5 | | 0.1 | | 658 | 14 | 6.25 | 24 | 40 | | |
| 54.0 | 55.3 | 3398 | 1.3 | 1.24 | 5 | | 0.1 | | 1167 | 194 | 5.70 | 38 | 950 | | |
| 55.3 | 55.8 | 3399 | .5 | .46 | 5 | | 0.1 | | 1153 | 489 | 8.87 | 21 | 2461 | | |
| 55.8 | 58.0 | 3400 | 2.2 | 2.03 | 5 | | 0.1 | | 829 | 42 | 4.98 | 22 | 111 | | |
| 58.0 | 60.0 | 3401 | 2 | 1.90 | 5 | | 0.1 | | 156 | 8 | 4.66 | 41 | 18 | | |
| 60.0 | 62.6 | 3402 | 2.6 | 2.28 | 30 | | 0.1 | | 701 | 97 | 6.11 | 32 | 27 | | |
| 62.0 | 65.0 | 3403 | 2.4 | 2.25 | 5 | | 0.1 | | 440 | 252 | 8.23 | 3 | 2386 | | |
| 65.0 | 68.0 | 3404 | 3 | 2.24 | 5 | | 0.1 | | 483 | 446 | 8.35 | 26 | 2837 | | |
| 68.0 | 71.0 | 3405 | 3 | 2.48 | 10 | | 0.1 | | 738 | 109 | 5.41 | 34 | 125 | | |
| 71.0 | 74.0 | 3406 | 3 | 2.46 | 5 | | 0.1 | | 417 | 227 | 4.36 | 52 | 1907 | | |
| 74.0 | 77 | 3407 | 3 | 2.82 | 5 | | 0.1 | | 952 | 322 | 3.67 | 52 | 2319 | | |
| 77 | 80 | 3408 | 3 | 2.86 | 5 | | 0.1 | | 334 | 422 | 3.98 | 43 | 2954 | | |
| 80 | 83 | 3409 | 3 | 2.87 | 140 | | 0.1 | | 420 | 586 | 4.49 | 47 | 3330 | | |
| 83 | 86 | 3410 | 3 | 2.98 | 120 | | 0.1 | | 851 | 323 | 4.88 | 115 | 1399 | | |
| 86 | 89 | 3411 | 3 | 2.94 | 70 | | 0.1 | | 1483 | 499 | 4.64 | 64 | 796 | | |
| 89 | 92 | 3412 | 3 | 2.97 | 20 | | 0.1 | | 374 | 150 | 4.88 | 35 | 755 | | |
| 92 | 95 | 3413 | 3 | 2.96 | 10 | | 0.1 | | 238 | 77 | 4.51 | 19 | 585 | | |
| 95 | 98 | 3414 | 3 | 2.94 | 40 | | 0.1 | | 300 | 107 | 5.03 | 25 | 887 | | |
| 98 | 101 | 3415 | 3 | 2.99 | 40 | | 0.1 | | 285 | 107 | 4.93 | 36 | 836 | | |
| 101 | 104 | 3416 | 3 | 2.91 | 70 | | 0.1 | | 193 | 103 | 5.73 | 59 | 604 | | |
| 104 | 107 | 3417 | 3 | 2.90 | 30 | | 0.1 | | 582 | 290 | 4.80 | 188 | 709 | | |
| 107 | 110 | 3418 | 3 | 2.86 | 5 | | 0.1 | | 608 | 129 | 5.30 | 121 | 1264 | | |
| 110 | 113 | 3419 | 3 | 2.16 | 20 | | 1.1 | | 504 | 1235 | 4.57 | 90 | 1074 | | |
| 113 | 116 | 3420 | 3 | 2.93 | 5 | | 0.1 | | 538 | 89 | 4.79 | 59 | 981 | | |
| 116 | 118 | 3421 | 2 | 1.86 | 1700 | | 3.4 | | 13679 | 89 | 3.86 | 8 | 883 | | |
| 118 | 119.8 | 3422 | 1.8 | 1.56 | 630 | | 2.2 | | 5747 | 449 | 4.71 | 22 | 1275 | | |
| 119.8 | 122 | 3423 | 2.2 | 1.96 | 5 | | 0.1 | | 146 | 358 | 9.45 | 23 | 3038 | | |
| 122 | 125.0 | 3424 | 3 | 2.85 | 10 | | 2.2 | | 68 | 182 | 8.00 | 18 | 2064 | | |
| 125 | 128.0 | 3425 | 3 | 3.0 | 5 | | 1.9 | | 41 | 199 | 8.39 | 41 | 2318 | | |
| 128 | 131.0 | 3426 | 3 | 2.9 | 5 | | 1.2 | | 55 | 315 | 8.68 | 42 | 2603 | | |
| 131 | 134.0 | 3427 | 3 | 2.9 | 5 | | 1.2 | | 99 | 388 | 9.10 | 67 | 2773 | | |
| 134 | 136.15 | 3428 | 2.15 | 1.85 | 5 | | 0.1 | | 40 | 653 | 10.00 | 92 | 4424 | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 09:50:23 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8821 | 9598.2 | 9767.3 | 1674.3 | | 90 | 213.05 | | DOWN DIP CONTINUITY, B-ZONE SOUTH. |

#HOL

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 136.15 | 138.5 | 3429 | 2.35 | 2.22 | 680 | | 4.8 | | 10553 | 383 | 6.03 | 29 | 852 | | |
| 138.5 | 140.7 | 3430 | 2.2 | 2.02 | 770 | | 6.4 | | 14814 | 111 | 9.44 | 28 | 529 | | |
| 140.7 | 143.0 | 3431 | 2.3 | 2.3 | 5 | | 0.1 | | 77 | 368 | 8.81 | 18 | 2617 | | |
| 143.0 | 146.0 | 3432 | 3 | 2.79 | 5 | | 1.1 | | 62 | 338 | 7.70 | 31 | 2762 | | |
| 146.0 | 149.0 | 3433 | 3 | 2.89 | 5 | | 2.1 | | 69 | 459 | 9.36 | 49 | 3784 | | |
| 149.0 | 152.0 | 3434 | 3 | 2.95 | 5 | | 2.1 | | 66 | 415 | 9.44 | 48 | 3311 | | |
| 152.0 | 155.0 | 3435 | 3 | 2.9 | 5 | | 2.1 | | 71 | 326 | 9.42 | 28 | 3362 | | |
| 155.0 | 158.0 | 3436 | 3 | 2.89 | 15 | | 2.1 | | 43 | 350 | 8.90 | 32 | 2772 | | |
| 158.0 | 160.0 | 3437 | 2 | 1.9 | 5 | | 2.1 | | 48 | 307 | 9.62 | 34 | 2578 | | |
| 160 | 162.1 | 3438 | 2.1 | 2.03 | 30 | | 2.3 | | 81 | 581 | 10.00 | 75 | 5921 | | |
| 162.1 | 165.0 | 3439 | 2.9 | 2.35 | 540 | | 3.1 | | 11577 | 156 | 6.15 | 38 | 611 | | |
| 165.0 | 168 | 3440 | 3 | 2.44 | 360 | | 2.1 | | 9010 | 111 | 3.90 | 20 | 415 | | |
| 168 | 171 | 3441 | 3 | 2.86 | 420 | | 1.2 | | 10596 | 71 | 4.89 | 139 | 61 | | |
| 171 | 174 | 3442 | 3 | 2.93 | 375 | | 2.7 | | 11032 | 106 | 5.57 | 260 | 83 | | |
| 174 | 177 | 3443 | 3 | 2.83 | 610 | | 2.1 | | 10984 | 114 | 6.58 | 16 | 485 | | |
| 177 | 180 | 3444 | 3 | 2.97 | 390 | | 1.2 | | 7292 | 161 | 5.54 | 12 | 612 | | |
| 180 | 183 | 3445 | 3 | 2.0 | 355 | | 1.1 | | 7846 | 135 | 6.55 | 12 | 1467 | | |
| 183 | 186 | 3446 | 3 | 2.52 | 700 | | 3.1 | | 14432 | 161 | 5.73 | 8 | 910 | | |
| 186 | 189 | 3447 | 3 | 2.92 | 550 | | 3.1 | | 10661 | 229 | 4.74 | 17 | 699 | | |
| 189 | 192 | 3448 | 3 | 2.92 | 520 | | 3.3 | | 12960 | 94 | 6.68 | 17 | 678 | | |
| 192 | 195 | 3449 | 3 | 2.92 | 740 | | 5.7 | | 15707 | 156 | 7.87 | 33 | 770 | | |
| 195 | 198 | 3450 | 3 | 2.34 | 570 | | 4.3 | | 16077 | 194 | 6.23 | 14 | 647 | | |
| 198 | 201 | 3451 | 3 | 2.9 | 540 | | 3.3 | | 11498 | 271 | 6.25 | 30 | 385 | | |
| 201 | 204 | 3452 | 3 | 2.75 | 610 | | 3.1 | | 12503 | 94 | 6.09 | 6 | 598 | | |
| 204 | 207 | 3453 | 3 | .22 | 315 | | 2.1 | | 9011 | 95 | 4.61 | 34 | 559 | | |
| 207 | 210 | 3454 | 3 | .88 | 1340 | 0.043 | 3.1 | | 8601 | 238 | 5.95 | 176 | 522 | | |
| 210 | 213.05 | 3455 | 3.05 | 1.58 | 235 | | 2.1 | | 12078 | 93 | 4.05 | 1000 | 85 | | |

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656


REPORT NUMBER: 881151 AA JOB NUMBER: 881151 WESTERN CON. MINING CORP. PAGE 1 OF 1

| SAMPLE # | Au oz/st |
|---|---|
| C88 - 3454 | .043 |

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-3438 | .01 |
| C88-3439 | 1.22 |
| C88-3440 | .96 |
| C88-3441 | 1.18 |
| C88-3442 | 1.18 |
| C88-3443 | 1.14 |
| C88-3444 | .79 |
| C88-3445 | .79 |
| C88-3446 | 1.47 |
| C88-3447 | 1.10 |
| C88-3448 | 1.44 |
| C88-3449 | 1.51 |
| C88-3450 | 1.71 |
| C88-3451 | 1.27 |
| C88-3452 | 1.30 |
| C88-3453 | .87 |
| C88-3454 | .86 |
| C88-3455 | 1.08 |
| DETECTION LIMIT | .01 |

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

Signed: _____

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

REPORT #: BB1151 PA WESTERN CANADIAN MINING CORP. 

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88-3378 | 25.8 | 0.55 | 52 | 1890 | <3 | 99 | <3 | 0.05 | 0.6 | 1 | 45 | 194 | 5.83 | 0.03 | 0.16 | 145 | 16 | 0.01 | 2 | 0.16 | 121 | <3 | <5 | <2 | 3 | 20 | <5 | <3 | 35 |
| C88-3379 | 19.1 | 0.19 | 23 | 240 | <3 | 43 | <3 | 0.01 | 0.1 | 3 | 14 | 55 | 3.54 | 0.01 | 0.01 | 10 | 12 | 0.01 | 1 | 0.07 | 269 | <3 | <5 | <2 | 2 | 11 | <5 | <3 | 9 |
| C88-3380 | 1.1 | 0.33 | 41 | 70 | <3 | 18 | <3 | 0.01 | 0.1 | 9 | 43 | 119 | 3.10 | 0.01 | 0.02 | 12 | 5 | 0.01 | 5 | 0.05 | 117 | <3 | <5 | <2 | <2 | 5 | <5 | <3 | 25 |
| C88-3381 | 1.1 | 0.20 | 55 | 165 | <3 | 54 | <3 | 0.01 | 0.1 | 8 | 13 | 238 | 1.77 | 0.01 | 0.01 | 9 | 12 | 0.01 | 4 | 0.06 | 439 | <3 | <5 | <2 | <2 | 7 | <5 | <3 | 12 |
| C88-3382 | 1.1 | 2.04 | 47 | 170 | <3 | 9 | 6 | 0.21 | 1.3 | 23 | 57 | 1319 | 6.70 | 0.05 | 1.04 | 913 | 10 | 0.02 | 10 | 0.26 | 136 | <3 | <5 | <2 | 4 | 24 | <5 | <3 | 192 |
| C88-3383 | 0.1 | 2.37 | 30 | 110 | <3 | 25 | 3 | 0.27 | 1.6 | 18 | 26 | 1249 | 4.56 | 0.07 | 1.34 | 1552 | 4 | 0.01 | 10 | 0.18 | 40 | <3 | <5 | <2 | 4 | 25 | <5 | <3 | 215 |
| C88-3384 | 0.1 | 1.31 | 119 | 315 | <3 | 15 | <3 | 0.23 | 0.3 | 29 | 32 | 1494 | 4.99 | 0.06 | 0.32 | 644 | 7 | 0.01 | 10 | 0.21 | 30 | <3 | <5 | <2 | 2 | 9 | <5 | <3 | 96 |
| C88-3385 | 0.3 | 1.18 | 60 | 370 | <3 | 15 | <3 | 0.25 | 0.7 | 21 | 43 | 1309 | 4.59 | 0.06 | 0.37 | 809 | 9 | 0.01 | 10 | 0.23 | 33 | <3 | <5 | <2 | 2 | 14 | <5 | <3 | 116 |
| C88-3386 | 0.2 | 1.27 | 141 | 260 | <3 | 14 | <3 | 0.26 | 0.5 | 18 | 22 | 1042 | 4.64 | 0.07 | 0.38 | 585 | 8 | 0.01 | 10 | 0.23 | 39 | <3 | <5 | <2 | 2 | 8 | <5 | <3 | 98 |
| C88-3387 | 0.1 | 0.72 | 219 | 20 | <3 | 11 | <3 | 0.26 | 0.3 | 20 | 29 | 960 | 4.97 | 0.07 | 0.20 | 291 | 5 | 0.01 | 10 | 0.23 | 29 | <3 | <5 | <2 | 2 | 5 | <5 | <3 | 95 |
| C88-3388 | 0.1 | 0.59 | 16 | 200 | <3 | 8 | <3 | 0.28 | 1.1 | 22 | 56 | 836 | 5.89 | 0.07 | 0.18 | 320 | 6 | 0.01 | 13 | 0.22 | 25 | <3 | <5 | <2 | 2 | 5 | <5 | <3 | 66 |
| C88-3389 | 0.1 | 0.41 | 18 | <5 | <3 | 13 | <3 | 0.08 | 0.5 | 15 | 18 | 609 | 4.74 | 0.03 | 0.06 | 45 | 5 | 0.01 | 15 | 0.15 | 60 | <3 | <5 | <2 | <2 | 16 | <5 | <3 | 31 |
| C88-3390 | 0.1 | 0.25 | 22 | <5 | <3 | 10 | <3 | 0.01 | 0.3 | 13 | 39 | 432 | 4.93 | 0.01 | 0.02 | 14 | 18 | 0.01 | 8 | 0.13 | 45 | <3 | <5 | <2 | <2 | 13 | <5 | <3 | 18 |
| C88-3391 | 0.1 | 0.25 | 34 | <5 | <3 | 10 | <3 | 0.01 | 0.3 | 12 | 10 | 368 | 4.47 | 0.01 | 0.02 | 7 | 4 | 0.01 | 8 | 0.06 | 20 | <3 | <5 | <2 | <2 | 4 | <5 | <3 | 15 |
| C88-3392 | 0.1 | 0.22 | 19 | <5 | <3 | 12 | <3 | 0.07 | 0.5 | 15 | 31 | 404 | 4.69 | 0.02 | 0.03 | 18 | 5 | 0.01 | 9 | 0.08 | 18 | <3 | <5 | <2 | <2 | 3 | <5 | <3 | 13 |
| C88-3393 | 0.1 | 0.40 | 31 | <5 | <3 | 7 | <3 | 0.17 | 1.1 | 19 | 55 | 676 | 6.67 | 0.05 | 0.10 | 440 | 11 | 0.02 | 12 | 0.19 | 60 | <3 | <5 | <2 | 2 | 8 | <5 | <3 | 58 |
| C88-3394 | 0.1 | 0.45 | 37 | <5 | <3 | 8 | <3 | 0.15 | 0.8 | 19 | 32 | 481 | 6.39 | 0.04 | 0.10 | 33 | 5 | 0.02 | 9 | 0.19 | 37 | <3 | <5 | <2 | 2 | 6 | <5 | <3 | 28 |
| C88-3395 | 0.1 | 0.38 | 34 | <5 | <3 | 8 | <3 | 0.25 | 0.8 | 17 | 47 | 482 | 5.53 | 0.06 | 0.05 | 24 | 4 | 0.01 | 10 | 0.22 | 21 | <3 | <5 | <2 | <2 | 8 | <5 | <3 | 15 |
| C88-3396 | 0.1 | 0.67 | 25 | <5 | <3 | 8 | <3 | 0.27 | 1.1 | 19 | 50 | 621 | 5.80 | 0.06 | 0.45 | 451 | 6 | 0.01 | 10 | 0.23 | 23 | <3 | <5 | <2 | 2 | 7 | <5 | <3 | 56 |
| C88-3397 | 0.1 | 0.38 | 24 | <5 | <3 | 6 | <3 | 0.15 | 0.8 | 19 | 23 | 658 | 6.25 | 0.04 | 0.18 | 40 | 3 | 0.01 | 15 | 0.19 | 27 | <3 | <5 | <2 | 2 | 17 | <5 | <3 | 14 |
| C88-3398 | 0.1 | 1.74 | 38 | <5 | <3 | 12 | 5 | 0.25 | 1.6 | 21 | 22 | 1167 | 5.70 | 0.06 | 1.33 | 950 | 3 | 0.02 | 11 | 0.24 | 27 | <3 | <5 | <2 | 3 | 15 | <5 | <3 | 194 |
| C88-3399 | 0.1 | 4.28 | 21 | <5 | <3 | 39 | 10 | 0.27 | 4.1 | 34 | 35 | 1153 | 8.87 | 0.06 | 2.43 | 2461 | 6 | 0.03 | 5 | 0.16 | 39 | <3 | <5 | <2 | 3 | 8 | <5 | <3 | 489 |
| C88-3400 | 0.1 | 0.74 | 22 | 5 | <3 | 10 | <3 | 0.25 | 0.8 | 14 | 63 | 829 | 4.98 | 0.06 | 0.31 | 111 | 4 | 0.01 | 8 | 0.22 | 18 | <3 | <5 | <2 | 2 | 6 | <5 | <3 | 42 |
| C88-3401 | 0.1 | 0.29 | 41 | <5 | <3 | 12 | <3 | 0.16 | 0.2 | 14 | 38 | 156 | 4.66 | 0.04 | 0.02 | 18 | 4 | 0.01 | 10 | 0.17 | 17 | <3 | <5 | <2 | 2 | 15 | <5 | <3 | 8 |
| C88-3402 | 0.1 | 0.26 | 32 | 30 | <3 | 10 | <3 | 0.14 | 2.2 | 17 | 20 | 701 | 6.11 | 0.03 | 0.04 | 27 | 3 | 0.02 | 9 | 0.16 | 44 | <3 | <5 | <2 | 2 | 6 | <5 | <3 | 97 |
| C88-3403 | 0.1 | 4.38 | 3 | <5 | <3 | 415 | 9 | 3.00 | 2.5 | 30 | 17 | 440 | 8.23 | 0.30 | 2.41 | 2386 | 4 | 0.03 | 4 | 0.16 | 34 | <3 | <5 | <2 | 3 | 112 | <5 | <3 | 252 |
| C88-3404 | 0.1 | 4.09 | 26 | <5 | <3 | 21 | 9 | 1.73 | 3.6 | 36 | 76 | 483 | 8.35 | 0.24 | 2.63 | 2837 | 7 | 0.03 | 14 | 0.18 | 41 | <3 | <5 | <2 | 3 | 68 | <5 | <3 | 446 |
| C88-3405 | 0.1 | 0.51 | 34 | 10 | <3 | 10 | <3 | 0.28 | 1.3 | 15 | 62 | 738 | 5.41 | 0.07 | 0.14 | 125 | 5 | 0.01 | 9 | 0.23 | 44 | <3 | <5 | <2 | 2 | 11 | <5 | <3 | 109 |
| C88-3406 | 0.1 | 1.58 | 52 | <5 | <3 | 16 | <3 | 1.02 | 1.1 | 16 | 51 | 417 | 4.36 | 0.17 | 1.38 | 1907 | 3 | 0.01 | 9 | 0.24 | 55 | <3 | <5 | <2 | 2 | 30 | <5 | <3 | 227 |
| C88-3407 | 0.1 | 2.12 | 52 | <5 | <3 | 45 | <3 | 1.62 | 0.8 | 15 | 28 | 952 | 3.67 | 0.23 | 1.91 | 2319 | 2 | 0.02 | 9 | 0.27 | 37 | <3 | <5 | <2 | 2 | 42 | <5 | <3 | 322 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum is = Insufficient Sample ns = No sample > = Greater than Maximum AuFA = Fire assay/AAS

REPORT #: BB1079 PA  WESTERN CANADIAN MINING CORP.  

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| BB-3408 | 0.1 | 2.12 | 43 | <5 | <3 | 37 | <3 | 1.95 | 1.5 | 18 | 13 | 334 | 3.98 | 0.26 | 1.78 | 2954 | 2 | 0.02 | 14 | 0.23 | 42 | <3 | <5 | <2 | 2 | 51 | <5 | <3 | 422 |
| BB-3409 | 0.1 | 1.98 | 47 | 140 | <3 | 26 | <3 | 1.81 | 2.9 | 23 | 19 | 420 | 4.49 | 0.25 | 1.61 | 3330 | 3 | 0.02 | 10 | 0.24 | 167 | <3 | <5 | <2 | 2 | 49 | <5 | <3 | 586 |
| BB-3410 | 0.1 | 0.73 | 115 | 120 | <3 | 12 | <3 | 0.72 | 2.3 | 25 | 15 | 851 | 4.88 | 0.14 | 0.30 | 1399 | 11 | 0.02 | 12 | 0.24 | 128 | <3 | <5 | <2 | 2 | 20 | <5 | <3 | 323 |
| BB-3411 | 0.1 | 0.83 | 64 | 70 | <3 | 12 | <3 | 0.52 | 3.2 | 21 | 33 | 1483 | 4.64 | 0.11 | 0.44 | 796 | 8 | 0.02 | 9 | 0.26 | 105 | <3 | <5 | <2 | 2 | 19 | <5 | <3 | 499 |
| BB-3412 | 0.1 | 1.16 | 35 | 20 | <3 | 12 | <3 | 1.23 | 1.3 | 15 | 19 | 374 | 4.88 | 0.20 | 1.04 | 755 | 5 | 0.02 | 8 | 0.24 | 43 | <3 | <5 | <2 | 2 | 39 | <5 | <3 | 130 |
| BB-3413 | 0.1 | 1.32 | 19 | 10 | <3 | 14 | <3 | 1.31 | 1.1 | 15 | 24 | 238 | 4.51 | 0.21 | 1.38 | 585 | 3 | 0.02 | 7 | 0.22 | 41 | <3 | <5 | <2 | 2 | 43 | <5 | <3 | 77 |
| BB-3414 | 0.1 | 1.44 | 25 | 40 | <3 | 15 | <3 | 1.49 | 1.1 | 16 | 16 | 300 | 5.03 | 0.22 | 1.44 | 887 | 2 | 0.01 | 7 | 0.24 | 65 | <3 | <5 | <2 | 2 | 46 | <5 | <3 | 107 |
| BB-3415 | 0.1 | 1.22 | 36 | 40 | <3 | 12 | <3 | 1.24 | 1.1 | 15 | 26 | 285 | 4.93 | 0.19 | 1.44 | 836 | 2 | 0.01 | 8 | 0.23 | 73 | <3 | <5 | <2 | 2 | 30 | <5 | <3 | 107 |
| BB-3416 | 0.1 | 0.67 | 59 | 70 | <3 | 6 | <3 | 0.77 | 1.3 | 15 | 21 | 193 | 5.73 | 0.14 | 0.60 | 604 | 4 | 0.02 | 8 | 0.22 | 74 | <3 | <5 | <2 | 2 | 22 | <5 | <3 | 103 |
| BB-3417 | 0.1 | 0.65 | 188 | 30 | <3 | 11 | <3 | 0.76 | 1.1 | 17 | 33 | 582 | 4.80 | 0.14 | 0.70 | 709 | 5 | 0.02 | 11 | 0.23 | 62 | <3 | <5 | <2 | 2 | 17 | <5 | <3 | 290 |
| BB-3418 | 0.1 | 0.68 | 121 | <5 | <3 | 13 | <3 | 1.41 | 1.1 | 15 | 20 | 608 | 5.30 | 0.22 | 0.98 | 1264 | 4 | 0.02 | 9 | 0.21 | 65 | <3 | <5 | <2 | 2 | 40 | <5 | <3 | 129 |
| BB-3419 | 1.1 | 0.87 | 90 | 20 | <3 | 15 | <3 | 1.10 | 7.6 | 16 | 39 | 504 | 4.57 | 0.18 | 1.21 | 1074 | 8 | 0.04 | 9 | 0.20 | 98 | <3 | <5 | <2 | 2 | 31 | <5 | <3 | 1235 |
| BB-3420 | 0.1 | 0.44 | 59 | <5 | <3 | 13 | <3 | 1.22 | 0.8 | 15 | 20 | 538 | 4.79 | 0.20 | 0.79 | 981 | 7 | 0.01 | 9 | 0.22 | 35 | <3 | <5 | <2 | 2 | 25 | <5 | <3 | 89 |
| BB-3421 | 3.4 | 0.52 | 8 | 1700 | <3 | 11 | <3 | 2.20 | 0.8 | 14 | 56 | 13679 | 3.86 | 0.27 | 0.46 | 883 | 5 | 0.01 | 6 | 0.12 | 19 | <3 | <5 | <2 | 2 | 74 | <5 | <3 | 89 |
| BB-3422 | 2.2 | 1.47 | 22 | 630 | <3 | 8 | <3 | 1.80 | 3.2 | 12 | 29 | 5747 | 4.71 | 0.25 | 1.06 | 1275 | 9 | 0.02 | 5 | 0.15 | 60 | <3 | <5 | <2 | 2 | 51 | <5 | <3 | 449 |
| BB-3423 | 0.1 | 4.46 | 23 | 5 | <3 | 70 | 3 | 2.26 | 2.3 | 30 | 26 | 146 | 9.45 | 0.28 | 2.40 | 3038 | 6 | 0.04 | 1 | 0.15 | 45 | <3 | <5 | <2 | 4 | 51 | <5 | <3 | 358 |
| BB-3424 | 2.2 | 4.42 | 18 | 10 | <3 | 604 | 3 | 3.02 | 1.8 | 35 | 11 | 68 | 8.00 | 0.32 | 2.79 | 2064 | 4 | 0.04 | 1 | 0.12 | 42 | <3 | <5 | <2 | 9 | 82 | <5 | <3 | 182 |
| BB-3425 | 1.9 | 4.22 | 41 | <5 | <3 | 80 | 3 | 3.27 | 2.1 | 27 | 8 | 41 | 8.39 | 0.32 | 2.16 | 2318 | 5 | 0.04 | 1 | 0.16 | 44 | <3 | <5 | <2 | 8 | 52 | <5 | <3 | 199 |
| BB-3426 | 1.2 | 4.03 | 42 | <5 | <3 | 76 | 3 | 1.65 | 2.6 | 29 | 18 | 55 | 8.68 | 0.25 | 2.05 | 2603 | 6 | 0.04 | 2 | 0.16 | 43 | <3 | <5 | <2 | 8 | 33 | <5 | <3 | 315 |
| BB-3427 | 1.2 | 3.74 | 67 | <5 | <3 | 125 | 3 | 1.49 | 2.2 | 34 | 11 | 99 | 9.10 | 0.24 | 1.87 | 2773 | 5 | 0.04 | 2 | 0.16 | 42 | <3 | <5 | <2 | 7 | 29 | <5 | <3 | 388 |
| BB-3428 | 0.1 | 4.46 | 92 | <5 | <3 | 59 | 3 | 0.78 | 2.5 | 35 | 10 | 40 | >10.00 | 0.15 | 2.71 | 4424 | 6 | 0.05 | 9 | 0.16 | 42 | <3 | <5 | <2 | 3 | 15 | <5 | <3 | 653 |
| BB-3429 | 4.8 | 0.40 | 29 | 680 | <3 | 5 | <3 | 0.40 | 3.7 | 16 | 31 | 10553 | 6.03 | 0.09 | 0.16 | 852 | 18 | 0.03 | 5 | 0.15 | 73 | <3 | <5 | <2 | 2 | 10 | <5 | <3 | 383 |
| BB-3430 | 6.4 | 0.45 | 28 | 770 | <3 | 3 | 3 | 0.30 | 2.6 | 13 | 51 | 14814 | 9.44 | 0.07 | 0.13 | 529 | 8 | 0.03 | 3 | 0.14 | 28 | <3 | <5 | <2 | 3 | 7 | <5 | <3 | 111 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

ANOMALOUS RESULTS:
FURTHER ANALYSES
BY ALTERNATE
METHODS SUGGESTED

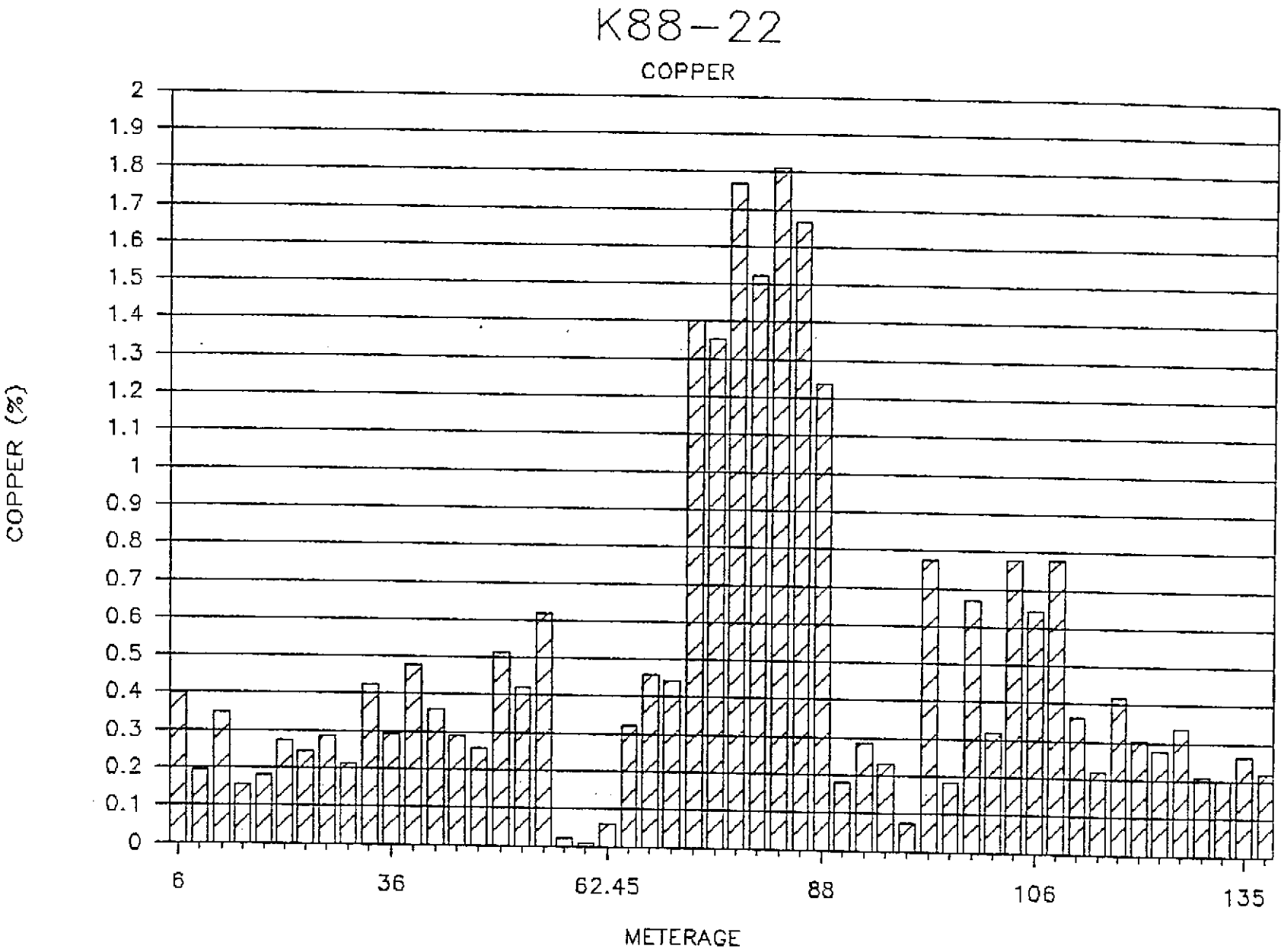
VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717

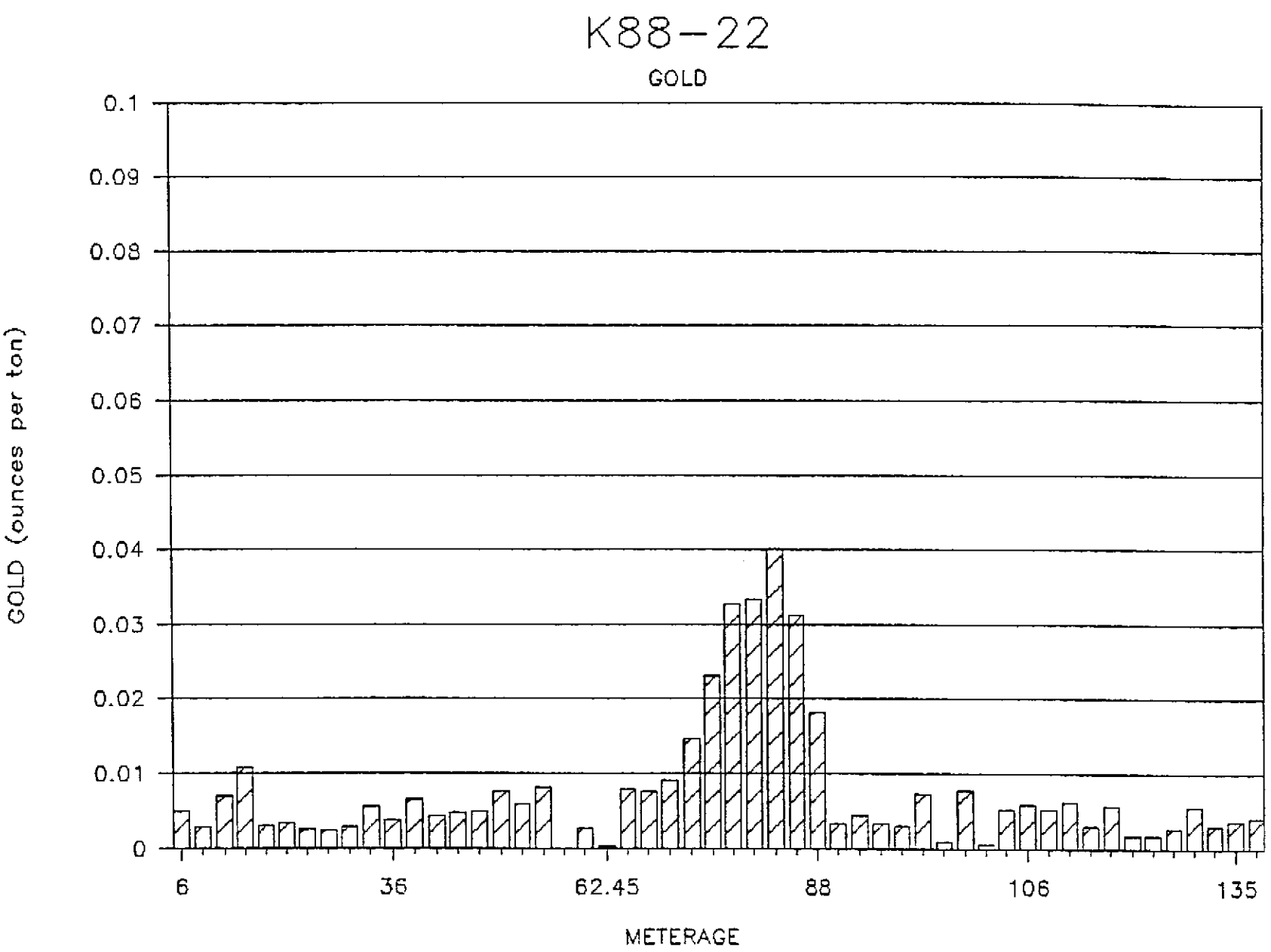


REPORT #: 881151 PA

WESTERN CANADIAN MINING CORP.

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88 - 3431 | 0.1 | 3.55 | 18 | <5 | <3 | 248 | 6 | 0.75 | 2.2 | 29 | 23 | 77 | 8.81 | 0.14 | 1.87 | 2617 | 4 | 0.02 | 10 | 0.15 | 47 | <3 | <5 | 42 | 5 | 20 | <5 | <3 | 368 |
| C88 - 3432 | 1.1 | 3.46 | 31 | <5 | <3 | 104 | 7 | 0.87 | 1.7 | 33 | 34 | 62 | 7.70 | 0.16 | 1.88 | 2762 | 3 | 0.02 | 3 | 0.14 | 47 | <3 | <5 | 37 | 12 | 46 | <5 | <3 | 339 |
| C88 - 3433 | 2.1 | 4.42 | 49 | <5 | <3 | 172 | 9 | 0.96 | 2.2 | 45 | 22 | 69 | 9.36 | 0.17 | 2.88 | 3784 | 3 | 0.03 | 3 | 0.12 | 53 | <3 | <5 | 52 | 14 | 21 | <5 | <3 | 459 |
| C88 - 3434 | 2.1 | 4.20 | 48 | <5 | <3 | 177 | 9 | 0.98 | 2.2 | 41 | 26 | 66 | 9.44 | 0.17 | 2.38 | 3311 | 4 | 0.03 | 3 | 0.13 | 55 | <3 | <5 | 49 | 15 | 25 | <5 | <3 | 415 |
| C88 - 3435 | 2.1 | 4.92 | 28 | <5 | <3 | 354 | 9 | 0.65 | 2.6 | 45 | 16 | 71 | 9.42 | 0.13 | 3.17 | 3362 | 3 | 0.03 | 2 | 0.12 | 57 | <3 | <5 | 56 | 15 | 32 | <5 | <3 | 326 |
| C88 - 3436 | 2.1 | 4.51 | 32 | 15 | <3 | 335 | 9 | 0.77 | 2.2 | 43 | 37 | <3 | 8.90 | 0.14 | 2.33 | 2772 | 3 | 0.03 | 3 | 0.14 | 52 | <3 | <5 | 51 | 16 | 74 | <5 | <3 | 351 |
| C88 - 3437 | 2.1 | 4.50 | 34 | <5 | <3 | 109 | 9 | 1.03 | 2.4 | 41 | 22 | 48 | 9.62 | 0.18 | 2.51 | 2578 | 4 | 0.03 | 2 | 0.16 | 61 | <3 | <5 | 54 | 16 | 20 | <5 | <3 | 307 |
| C88 - 3438 | 2.3 | 3.92 | 75 | 30 | <3 | 219 | 10 | 0.80 | 2.4 | 50 | 28 | 81 | >10.00 | 0.15 | 2.05 | 5921 | 5 | 0.04 | 4 | 0.15 | 64 | <3 | <5 | 55 | 17 | 16 | <5 | <3 | 582 |
| C88 - 3439 | 3.1 | 1.04 | 38 | 540 | <3 | 8 | <3 | 0.20 | 2.2 | 13 | 47 | 11577 | 6.15 | 0.05 | 0.38 | 611 | 2 | 0.01 | 5 | 0.16 | 72 | <3 | <5 | 13 | 3 | 25 | <5 | <3 | 158 |
| C88 - 3440 | 2.1 | 0.96 | 20 | 360 | <3 | 9 | <3 | 0.21 | 1.2 | 12 | 62 | 9010 | 3.90 | 0.06 | 0.38 | 415 | 2 | 0.01 | 4 | 0.20 | 24 | <3 | <5 | 2 | 3 | 102 | <5 | <3 | 111 |
| C88 - 3441 | 1.2 | 0.48 | 135 | 420 | <3 | 5 | <3 | 0.17 | 1.2 | 12 | 65 | 10596 | 4.89 | 0.05 | 0.05 | 61 | 5 | 0.01 | 3 | 0.15 | 52 | <3 | <5 | 9 | 3 | 29 | <5 | <3 | 79 |
| C88 - 3442 | 2.7 | 0.29 | 260 | 375 | <3 | 4 | <3 | 0.12 | 2.2 | 11 | 46 | 11032 | 5.57 | 0.04 | 0.02 | 63 | 3 | 0.01 | 3 | 0.11 | 53 | <3 | <5 | 19 | 2 | 14 | <5 | <3 | 105 |
| C88 - 3443 | 2.1 | 1.10 | 16 | 610 | <3 | 5 | 3 | 0.17 | 3.1 | 13 | 65 | 10984 | 6.58 | 0.05 | 0.49 | 485 | 5 | 0.01 | 3 | 0.15 | 27 | <3 | <5 | 12 | 3 | 10 | <5 | <3 | 114 |
| C88 - 3444 | 1.2 | 1.01 | 12 | 390 | <3 | 5 | <3 | 0.22 | 1.5 | 14 | 56 | 7292 | 5.54 | 0.05 | 0.52 | 612 | 11 | 0.01 | 4 | 0.18 | 27 | <3 | <5 | 6 | 3 | 15 | <5 | <3 | 161 |
| C88 - 3445 | 1.1 | 0.54 | 12 | 355 | <3 | 4 | <3 | 0.32 | 1.2 | 16 | 107 | 7846 | 6.55 | 0.07 | 0.12 | 1467 | 9 | 0.01 | 4 | 0.14 | 21 | <3 | <5 | 4 | 3 | 8 | <5 | <3 | 233 |
| C88 - 3446 | 3.1 | 0.25 | 8 | 700 | <3 | 4 | <3 | 0.29 | 0.9 | 12 | 47 | 14432 | 5.73 | 0.07 | 0.09 | 910 | 3 | 0.01 | 3 | 0.11 | 25 | <3 | <5 | <2 | 3 | 8 | <5 | <3 | 16 |
| C88 - 3447 | 3.1 | 0.46 | 17 | 550 | <3 | 5 | <3 | 0.98 | 1.9 | 10 | 81 | 10861 | 4.74 | 0.17 | 0.27 | 699 | 7 | 0.01 | 4 | 0.11 | 36 | <3 | <5 | 3 | 2 | 24 | <5 | <3 | 227 |
| C88 - 3448 | 3.3 | 0.21 | 17 | 520 | <3 | 3 | 3 | 0.43 | 1.6 | 12 | 65 | 12960 | 6.68 | 0.10 | 0.09 | 678 | 6 | 0.02 | 4 | 0.09 | 28 | <3 | <5 | 8 | 3 | 16 | <5 | <3 | 9 |
| C88 - 3449 | 5.7 | 0.61 | 33 | 740 | <3 | 4 | 3 | 0.95 | 2.1 | 12 | 106 | 15707 | 7.87 | 0.17 | 0.31 | 770 | 8 | 0.02 | 4 | 0.10 | 118 | <3 | <5 | 18 | 4 | 20 | <5 | <3 | 154 |
| C88 - 3450 | 4.3 | 0.63 | 14 | 570 | <3 | 4 | 3 | 0.16 | 1.4 | 11 | 49 | 16077 | 6.23 | 0.04 | 0.47 | 647 | 5 | 0.01 | 3 | 0.07 | 37 | <3 | <5 | 9 | 3 | 5 | <5 | <3 | 191 |
| C88 - 3451 | 3.3 | 0.53 | 30 | 540 | <3 | 4 | <3 | 0.14 | 2.1 | 13 | 92 | 11498 | 6.25 | 0.05 | 0.28 | 385 | 7 | 0.02 | 11 | 0.08 | 159 | <3 | <5 | 20 | 3 | 7 | <5 | <3 | 271 |
| C88 - 3452 | 3.1 | 0.30 | 6 | 610 | <3 | 4 | <3 | 0.25 | 1.2 | 12 | 80 | 12503 | 6.09 | 0.06 | 0.10 | 598 | 2 | 0.01 | 4 | 0.09 | 28 | <3 | <5 | 4 | 3 | 7 | <5 | <3 | 91 |
| C88 - 3453 | 2.1 | 0.40 | 34 | 315 | <3 | 6 | <3 | 0.36 | 1.1 | 10 | 128 | 9011 | 4.61 | 0.09 | 0.23 | 559 | 24 | 0.01 | <5 | 0.11 | 66 | <3 | <5 | 20 | 3 | 16 | <5 | <3 | 93 |
| C88 - 3454 | 3.1 | 0.28 | 176 | 1340 | <3 | 4 | <3 | 0.44 | 2.5 | 15 | 44 | 8601 | 5.95 | 0.10 | 0.24 | 522 | 14 | 0.02 | 4 | 0.15 | 182 | <3 | <5 | 287 | 3 | 17 | <5 | <3 | 233 |
| C88 - 3455 | 2.1 | 0.37 | >1000 | 235 | <3 | 5 | <3 | 0.21 | 1.5 | 13 | 71 | 10278 | 4.05 | 0.06 | 0.05 | 85 | 21 | 0.01 | 6 | 0.15 | 47 | <3 | <5 | 708 | 2 | 18 | <5 | <3 | 91 |


K88-22
COPPER
COPPER (%)
2
1.9
1.8
1.7
1.6
1.5
1.4
1.3
1.2
1.1
1
0.9
0.8
0.7
0.6
0.5
0.4
0.3
0.2
0.1
0
6
36
62.45
88
106
135
METERAGE


K88-22
GOLD
GOLD (ounces per ton)
0.1
0.09
0.08
0.07
0.06
0.05
0.04
0.03
0.02
0.01
0
6
36
62.45
88
106
135
METERAGE

KERR PROJECT D.D.HOLE K-88-22

LOCATION P-ZONE VERTICAL AT K88-18,19
DATE STARTED AUGUST 20, 1988
DATE COMPLETED AUGUST 21, 1988
CORE RECOVERY 73.36%
DRILLED BY FALCON DRILLING LTD
LOGGED BY S. CASSELMAN
OBJECTIVE TEST DOWN DIP EXTENSION OF B-ZONE FAULT / MINERALIZATION
DIP TEST DEPTH _____m DIP_____deg
DEPTH _____m DIP_____deg

COLLAR LAT. 10227.2 NORTH
LONG. 9596.6 EAST
ELEVATION 1468.9 m
AZIMUTH - DIP -90 deg
LENGTH 136.85 m
HOR. PROJ. 0.00 m
VERT.PROJ. 136.85 m

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 0.00 | 2.74 | 2.74 | OVERBURDEN |
| 2.74 | 55.00 | 52.26 | SERICITE SCHIST<br>- light to medium grey to grey green<br>- weak to moderately foliated at 40 deg to C.A.<br>- intense sericitization,weak to moderate chloritization - as spots generally associated with pyrite<br>- patchy silicification (1 to 5%), increasing to bottom of section<br>- 10 to 25% pyrite as fine, spotty disseminations, wispy stringers and veins from 1 mm to 2 cm wide, veins generally parallel foliation<br>- 1 to 5% quartz-calcite veins, parallel foliation<br>- top 5 m of core quite weathered and limonitic and fractured - average piece 15 cm long - fractured at 35 to 90 deg to C.A.<br>- from 5.0 to 47.0 m core is quite competent-average piece 25 to 30 cm long<br>- from 47.0 to 55.0 m core is very fractured and faulted adjacent to dyke<br>- average piece 2 to 5 cm long<br>- in intensely fractured zone core is well foliated at 30 deg to C.A. and fractured at 45 deg to C.A.<br>- traces of native copper on fracture surfaces |
| 55.00 | 62.45 | 7.45 | FINE-GRAINED ANDESITE DYKE<br>- slightly foliated at 30 deg to C.A.<br>- moderate to strongly chloritized weak to moderately sericitized |

KERR PROJECT D.D.HOLE K-88-22

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - 1 to 5% quartz-calcite veining at 30 deg to C.A.<br>- < 1% pyrite, rare traces of native copper on fracture surfaces<br>- quite competent, average piece 20 to 35 cm long<br>- dyke marks hanging wall contact of intense silica stockwork zone in fault<br>- upper contact at 30 deg, lower at 30 deg to C.A. |
| 62.45 | 69.10 | 6.65 | CHLORITE-SERICITE-QUARTZ SCHIST<br>- medium to dark green with white to grey siliceous bands<br>- intensely chloritized, moderately sericitized and silicified gradational zone between andesite dyke and silica-sulphide stockwork zone<br>- wavy, undulating bands - foliation of sericite, chlorite and quartz<br>- 10 to 20% pyrite, up to .8% chalcocite and traces of chalcopyrite<br>- gradational contact with silica stockwork zone arbitrarily taken to be where massive silica, pyrite, chalcopyrite,and chalcocite start |
| 69.10 | 88.00 | 18.90 | SILICA STOCKWORK, SULPHIDE ZONE<br>- light to medium white to grey with abundant pyrite and massive chalcopyrite and chalcocite bands and sections of sericitic grey-green<br>- most silicified sections have a pervasive blue-grey appearance which is believed to be from disseminated and micro-fracture filling chalcocite<br>- very intensely silicified and abundant sulphides<br>- wispy chlorite and sections of intense sericite<br>- from 69.1 to 73.0 m have 5% massive chalcopyrite veins up to 2 cm wide<br>- chalcocite is in abundance (1 to 5%) throughout interval<br>- possible richest Cu intersection to date-definitely looks interesting<br>- quite fractured and broken (i.e., faulted) from 70.0 m to end of section, average piece 3 to 5 cm long<br>- fractures at 50 deg to C.A. |

KERR PROJECT D.D.HOLE K-88-22

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| 88.00 | 95.10 | 7.10 | FAULT ZONE / QUARTZ-SERICITE-PYRITE-CHALCOCITE SCHIST<br>- light to medium grey, intensely fractured at 50 deg to C.A., average piece 1 to 5 cm long<br>- 20% pyrite as coarse, euhedral aggregates and stringers<br>- .5 to 1.5% chalcocite, generally associated with pyrite, no chalcopyrite visible<br>- silicification drops off to < 10% |
| 95.10 | 96.10 | 1.00 | FINE-GRAINED ANDESITE DYKE<br>- light to medium grey green<br>- moderate chlorite, moderate sericite<br>- 1% quartz-calcite veining, < 1% pyrite<br>- upper contact at 50 deg, lower at 15 deg to C.A.<br>- quite fractured and faulted, average piece 5 cm long |
| 96.10 | 97.30 | 1.20 | FAULT ZONE / SERICITE SCHIST<br>- as in section 88.0 to 95.1 m<br>- slightly more silicified and competent- average pieces 5 to 10 cm long |
| 97.30 | 97.50 | 0.20 | FINE-GRAINED ANDESITE DYKE<br>- light to medium grey-green, as in 95.1 to 96.1 m<br>- upper contact at 60 deg, lower at 75 deg to C.A.<br>- quite fractured - faulted |
| 97.50 | 100.35 | 2.85 | FAULT ZONE / QUARTZ-SERICITE-PYRITE-CHALCOCITE SCHIST<br>- as in 88 to 95.1 m and in 96.1 to 97.3 m<br>- slightly more chloritized, up to 20% pyrite<br>- 1.5% chalcocite<br>- average piece 5 cm long, fractured at 40 deg to C.A. |
| 100.35 | 100.90 | 0.55 | FINE-GRAINED ANDESITE DYKE<br>- medium to dark green<br>- as in 95.1 to 96.1 m and 97.3 to 97.55 m<br>- slightly more chloritic<br>- no quartz-carbonate veining, < 1% pyrite<br>- upper contact at 60 deg, lower at 60 deg to C.A. |
| 100.90 | 126.50 | 25.60 | FAULT ZONE / QUARTZ-SERICITE-PYRITE-CHALCOCITE SCHIST |

KERR PROJECT D.D.HOLE K-88-22

| FROM (m) | TO (m) | WIDTH (m) | DESCRIPTION |
|---|---|---|---|
| | | | - light to medium grey-green as in above fault zone sections<br>- intensely sericitized (50 to 60%)<br>- moderately silicified (10 to 20%)<br>- 15 to 22% pyrite, .5 to 3% chalcocite, rare chalcopyrite<br>- weakly chloritized, slightly foliated<br>- fractured at 40 deg to 70 deg to C.A.<br>- vuggy - especially silica, generally vugs contain chalcocite |
| 126.50 | 136.85 | 10.35 | SERICITIC-CHLORITIC DIORITE ?<br>- light to medium grey-green<br>- much more competent than faulted zone, except for interval between 127.0 and 128.0 m which is quite fractured - average piece 1 cm long<br>- in competent section average piece 25 to 30 cm long<br>- intensely sericitized, weak to moderately chloritized<br>- 1% quartz-calcite veining<br>- little to no silica<br>- 10 to 18% coarse disseminated, stringer and vein pyrite<br>- traces of chalcocite, rare to no chalcopyrite<br>- possibly could be interval which was intersected in K-88-18 which lay between mineralized breccia zones<br>- 1 cm anhydrite, white to cloudy translucent vein at 128.0 m<br>- at 130.5 m, 1 cm anhydrite vein - overall 1 to 2% anhydrite<br>- anhydrite is not noted in competent core separating faulted zones in K-88-18<br>- this section has similarities to propylitic alteration zone of K-88-19 - at bottom of hole where anhydrite was noted, however this section is less chloritized<br>- the protolith appears to be a coarse-grained, possible dioritic rock, with 2 mm hornblende laths altered to chlorite evident, especially at bottom of hole<br><br>E.O.H. |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 12:58:55 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks | #HOLE |
|---|---|---|---|---|---|---|---|---|---|
| 6822 | 10227.2 | 9596.6 | 1469.0 | | 90 | 136.85 | | | |

| FROM | Dist | WDTH | RQ | ROCKNAME | UNT | TXT | SI | QV | SE | CY | CH | EP | CB | GM | A1 | A2 | IN | PY | CP | SP | CC | NC | M1 | M2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 2.74 | 2.74 | | OVERBURDEN | | | | | | | | | | | | | | | | | | | | |
| 2.74 | 6 | 3.26 | 33 | SRCT SCHT | | F-CG | 2 | 3 | 60 | 5 | 7 | 0 | 0 | | | | 95 | 20 | 0 | | 1 | | | |
| 6 | 9 | 3 | 29 | SRCT SCHT | | F-CG | 2 | 3 | 55 | 3 | 7 | 0 | 0 | | | | 95 | 23 | .1 | | .8 | | | |
| 9 | 12 | 3 | 30 | SRCT SCHT | | F-CG | 1 | 7 | 50 | 2 | 5 | 0 | 2 | | | | 100 | 25 | 0 | | 1 | | | |
| 12 | 15 | 3 | 44 | SRCT SCHT | | F-CG | 1 | 5 | 55 | 1 | 10 | 0 | 3 | | | | 100 | 20 | .1 | | .3 | | | |
| 15 | 18 | 3 | 37 | SRCT SCHT | | F-CG | 1 | 5 | 55 | 1 | 12 | 0 | 3 | | | | 100 | 18 | 0 | | .2 | | | |
| 18 | 21 | 3 | 42 | SRCT SCHT | | F-CG | 2 | 2 | 55 | 1 | 8 | 0 | 1 | | | | 100 | 22 | .2 | | 0 | | | |
| 21 | 24 | 3 | 43 | SRCT SCHT | | F-CG | 1 | 5 | 65 | 1 | 8 | 0 | 1 | | | | 100 | 12 | .5 | | .1 | | | |
| 24 | 27 | 3 | 37 | SRCT SCHT | | F-CG | 8 | 7 | 45 | 0 | 12 | 0 | 2 | | | | 100 | 22 | .5 | | .8 | | | |
| 27 | 30 | 3 | 38 | SRCT SCHT | | F-CG | 2 | 2 | 60 | 1 | 12 | 0 | 1 | | | | 100 | 15 | .1 | | .5 | | | |
| 30 | 33 | 3 | 35 | SRCT SCHT | | F-CG | 5 | 2 | 55 | 1 | 15 | 0 | 1 | | | | 100 | 17 | 0 | | .8 | | | |
| 33 | 36 | 3 | 32 | SRCT SCHT | | F-CG | 1 | 1 | 65 | 0 | 12 | 0 | .5 | | | | 100 | 15 | .1 | | .8 | | | |
| 36 | 39 | 3 | 36 | SRCT SCHT | | F-CG | 3 | 5 | 65 | 0 | 7 | 0 | 1 | | | | 100 | 15 | .8 | | .5 | | | |
| 39 | 42 | 3 | 38 | SRCT SCHT | | F-CG | 1 | 2 | 60 | 0 | 12 | .5 | 1 | | | | 100 | 18 | .1 | | .8 | .1 | | |
| 42 | 45 | 3 | 24 | SRCT SCHT | | F-CG | 3 | 5 | 60 | 0 | 12 | 1 | 1 | | | | 100 | 15 | .5 | | .8 | .2 | | |
| 45 | 48 | 3 | 17 | SRCT SCHT | | F-CG | 5 | 2 | 60 | 1 | 8 | .5 | 1 | | | | 100 | 12 | .2 | | .8 | | | |
| 48 | 51 | 3 | 19 | SRCT SCHT | | F-CG | 1 | 5 | 60 | 1 | 5 | .5 | 0 | | | | 100 | 25 | 0 | | 2 | | | |
| 51 | 53 | 2 | 19 | SRCT SCHT | | F-CG | 1 | 2 | 60 | 0 | 10 | 0 | 0 | | | | 100 | 20 | 0 | | 2 | | | |
| 53 | 55 | 2 | 22 | SRCT SCHT | | F-CG | 5 | 2 | 60 | 1 | 8 | 0 | 0 | | | | 100 | 20 | 0 | | 2 | | | |
| 55 | 58 | 3 | 45 | ANDS DYKE | | FG | 0 | 3 | 15 | 1 | 30 | 0 | 2 | | | | 50 | .5 | 0 | | 0 | | | |
| 58 | 61 | 3 | 51 | ANDS DYKE | | FG | 0 | 2 | 18 | 0 | 25 | 0 | 2 | | | | 50 | .5 | 0 | | 0 | | | |
| 61 | 62.45 | 1.45 | 54 | ANDS DYKE | | FG | 0 | 1 | 15 | 0 | 25 | 0 | 1 | | | | 45 | .5 | 0 | | 0 | | | |
| 62.45 | 65 | 2.55 | 36 | SRCT SCHT | | F-MG | 8 | 5 | 30 | 1 | 30 | 0 | 1 | | | | 90 | 15 | 0 | | .8 | | | |
| 65 | 67 | 2 | 32 | SRCT SCHT | | F-MG | 8 | 5 | 30 | 1 | 25 | 0 | 2 | | | | 90 | 15 | .5 | | 1 | | | |
| 67 | 69.1 | 2.1 | 49 | SRCT SCHT | | F-MG | 8 | 5 | 30 | 0 | 30 | 0 | 1 | | | | 90 | 15 | .2 | | .5 | | | |
| 69.1 | 71 | 1.9 | 42 | SILC SULP STWK | | F-MG | 45 | 5 | 10 | 0 | 15 | 0 | 0 | | | | 100 | 18 | 3 | | 2 | | | |
| 71 | 73 | 2 | 34 | SILC SULP STWK | | F-MG | 45 | 5 | 10 | 0 | 10 | 0 | 0 | | | | 100 | 18 | 4 | | 3 | | | |
| 73 | 76 | 3 | 32 | SILC SULP STWK | | F-MG | 55 | 0 | 10 | 0 | 8 | 0 | 0 | | | | 100 | 20 | 1.5 | | 4 | | | |
| 76 | 79 | 3 | 28 | SILC SULP STWK | | F-MG | 55 | 0 | 12 | 0 | 2 | 0 | 0 | | | | 100 | 22 | 1 | | 4 | | | |
| 79 | 82 | 3 | 26 | SILC SULP STWK | | F-MG | 60 | 0 | 15 | 0 | 1 | 0 | 0 | | | | 100 | 20 | .8 | | 3 | | | |
| 82 | 85 | 3 | 29 | SILC SULP STWK | | F-MG | 55 | 0 | 15 | 1 | 2 | 0 | 0 | | | | 100 | 22 | .1 | | 3 | | | |
| 85 | 88 | 3 | 29 | SILC SULP STWK | | F-MG | 30 | 0 | 35 | 0 | 5 | 0 | 0 | | | | 100 | 25 | .5 | | 3 | | | |
| 88 | 90.5 | 2.5 | 19 | FAULT SRCT SCHT | | F-MG | 2 | 2 | 65 | 1 | 2 | 0 | 0 | | | | 100 | 18 | 0 | | 1.5 | | | |
| 90.5 | 93 | 2.5 | 19 | FAULT SRCT SCHT | | F-MG | 2 | 2 | 65 | 2 | 3 | 0 | 0 | | | | 100 | 20 | 0 | | 1.5 | | | |
| 93 | 95.1 | 2.1 | 22 | FAULT SRCT SCHT | | F-MG | 2 | 3 | 65 | 2 | 2 | 0 | 0 | | | | 100 | 18 | 0 | | 1 | | | |
| 95.1 | 96.1 | 1 | 19 | ANDS DYKE | | FG | 0 | 1 | 20 | 2 | 10 | 0 | 1 | | | | 35 | .5 | 0 | | 0 | | | |
| 96.1 | 97.3 | 1.2 | 22 | FAULT SRCT SCHT | | F-MG | 15 | 2 | 45 | 3 | 5 | 0 | 0 | | | | 100 | 25 | .1 | | 2 | | | |
| 97.3 | 97.5 | .2 | 35 | ANDS DYKE | | FG | 0 | 1 | 20 | 0 | 10 | 0 | 1 | | | | 35 | .5 | 0 | | 0 | | | |
| 97.5 | 100.35 | 2.85 | 21 | FAULT SRCT SCHT | | F-MG | 15 | 5 | 45 | 3 | 8 | 0 | .5 | | | | 100 | 20 | 0 | | 2 | | | |
| 100.35 | 100.9 | .55 | 37 | ANDS DYKE | | FG | 0 | 0 | 15 | 5 | 15 | 0 | 0 | | | | 35 | .5 | 0 | | 0 | | | |
| 100.9 | 103 | 2.1 | 21 | FAULT SRCT SCHT | | F-MG | 30 | 3 | 30 | 2 | 8 | 0 | 0 | | | | 100 | 22 | .1 | | 2 | | | |
| 103 | 106 | 3 | 23 | FAULT SRCT SCHT | | F-MG | 25 | 3 | 40 | 1 | 8 | 0 | 0 | | | | 100 | 20 | .1 | | 2 | | | |
| 106 | 109 | 3 | 23 | FAULT SRCT SCHT | | F-MG | 8 | 3 | 50 | 3 | 7 | 0 | 0 | | | | 100 | 25 | .3 | | 3 | | | |
| 109 | 112 | 3 | 23 | FAULT SRCT SCHT | | F-MG | 5 | 2 | 50 | 2 | 15 | 0 | 0 | | | | 100 | 18 | 0 | | 2 | | | |
| 112 | 115 | 3 | 25 | FAULT SRCT SCHT | | F-MG | 0 | 2 | 50 | 3 | 25 | 0 | 0 | | | | 100 | 15 | 0 | | 1 | | | |
| 115 | 118 | 3 | 22 | FAULT SRCT SCHT | | F-MG | 0 | 1 | 45 | 8 | 30 | 0 | 0 | | | | 100 | 15 | 0 | | .2 | | | |
| 118 | 121 | 3 | 22 | FAULT SRCT SCHT | | F-MG | 0 | 1 | 45 | 8 | 30 | 0 | 0 | | | | 100 | 15 | 0 | | .2 | | | |
| 121 | 124 | 3 | 20 | FAULT SRCT SCHT | | F-MG | 0 | 1 | 55 | 2 | 25 | 0 | 0 | | | | 100 | 15 | 0 | | .5 | | | |
| 124 | 126.5 | 2.5 | 10 | FAULT SRCT SCHT | | F-MG | 0 | 1 | 65 | 1 | 8 | 0 | 0 | | | | 100 | 15 | 0 | | 5 | | | |
| 126.5 | 129 | 2.5 | 27 | ALTD DICR | | F-MG | 2 | 2 | 60 | 2 | 10 | 1 | 1 | | 2 | | 100 | 15 | .1 | | .2 | | | |
| 129 | 132 | 3 | 51 | ALTD DICR | | F-MG | 1 | 3 | 55 | 0 | 15 | .5 | 0 | | 3 | | 100 | 18 | .1 | | 0 | | | |
| 132 | 135 | 3 | 55 | ALTD DICR | | F-MG | 0 | 3 | 55 | 0 | 15 | 0 | 0 | | 3 | | 100 | 15 | .1 | | 0 | | | |
| 135 | 136.85 | 1.85 | 59 | ALTD DICR | | F-MG | 0 | 3 | 55 | 0 | 15 | 0 | 0 | | 3 | | 100 | 18 | .1 | | 0 | | | |

1988 KERR EXPLORATION PROGRAM

Western Canadian Mining Corporation - 21 Nov 1988 10:02:08 

| Ref | North | East | RL | Azim | Dip | Length | Category | Remarks |
|---|---|---|---|---|---|---|---|---|
| 8822 | 10227.2 | 9596.6 | 1469.0 | | 90 | 136.85 | | #HOLE |

| FROM | Dist | SampNo | WDTH | REC | Au | Auoz | Ag | Agoz | Cu | Zn | Fe% | As | Mn | E1 | E2 |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| 0 | 2.74 | | 2.74 | 0 | | | | | | | | | | | |
| 2.74 | 6 | 3456 | 3.26 | 2.84 | 170 | | 0.6 | | 3961 | 123 | 5.71 | 323 | 66 | | |
| 6 | 9 | 3457 | 3 | 2.64 | 95 | | 0.1 | | 1937 | 78 | 6.06 | 230 | 66 | | |
| 9 | 12 | 3458 | 3 | 2.48 | 240 | | 0.2 | | 3472 | 73 | 7.11 | 81 | 457 | | |
| 12 | 15 | 3459 | 3 | 2.97 | 370 | | 0.1 | | 1553 | 94 | 5.02 | 17 | 476 | | |
| 15 | 18 | 3460 | 3 | 2.91 | 100 | | 0.1 | | 1813 | 128 | 5.42 | 22 | 323 | | |
| 18 | 21 | 3461 | 3 | 2.92 | 110 | | 0.2 | | 2721 | 91 | 4.93 | 18 | 264 | | |
| 21 | 24 | 3462 | 3 | 2.96 | 85 | | 0.1 | | 2443 | 128 | 4.83 | 16 | 494 | | |
| 24 | 27 | 3463 | 3 | 2.92 | 80 | | 0.2 | | 2852 | 96 | 4.47 | 17 | 473 | | |
| 27 | 30 | 3464 | 3 | 2.96 | 95 | | 0.1 | | 2116 | 95 | 4.60 | 20 | 467 | | |
| 30 | 33 | 3465 | 3 | 2.95 | 190 | | 1.1 | | 4224 | 73 | 6.23 | 24 | 370 | | |
| 33 | 36 | 3466 | 3 | 2.92 | 130 | | 0.6 | | 2911 | 60 | 5.37 | 17 | 207 | | |
| 36 | 39 | 3467 | 3 | 2.96 | 220 | | 0.6 | | 4764 | 84 | 4.82 | 19 | 474 | | |
| 39 | 42 | 3468 | 3 | 3 | 145 | | 0.2 | | 3595 | 125 | 4.77 | 21 | 515 | | |
| 42 | 45 | 3469 | 3 | 2.58 | 160 | | 0.1 | | 2900 | 128 | 3.76 | 20 | 521 | | |
| 45 | 48 | 3470 | 3 | 2.62 | 170 | | 0.9 | | 2657 | 85 | 5.25 | 35 | 207 | | |
| 48 | 51 | 3471 | 3 | 1.91 | 260 | | 0.4 | | 5145 | 119 | 5.65 | 40 | 183 | | |
| 51 | 53 | 3472 | 2 | 1.09 | 200 | | 0.1 | | 4186 | 138 | 5.63 | 26 | 253 | | |
| 53 | 55 | 3473 | 2 | .85 | 280 | | 0.4 | | 6189 | 195 | 5.86 | 27 | 371 | | |
| 55 | 58 | 3474 | 3 | 2.62 | 5 | | 0.1 | | 209 | 142 | 1.67 | 3 | 590 | | |
| 58 | 61 | 3475 | 3 | 3 | 90 | | 0.1 | | 86 | 166 | 2.67 | 3 | 619 | | |
| 61 | 62.45 | 3476 | 1.45 | 1.45 | 5 | | 0.1 | | 597 | 302 | 6.30 | 3 | 1589 | | |
| 62.45 | 65 | 3477 | 2.55 | 2.47 | 270 | | 0.4 | | 3197 | 259 | 5.58 | 20 | 620 | | |
| 65 | 67 | 3478 | 2 | 1.96 | 260 | | 1.1 | | 4575 | 327 | 5.64 | 18 | 845 | | |
| 67 | 69.1 | 3479 | 2.1 | 2.1 | 310 | | 0.9 | | 4424 | 191 | 5.44 | 16 | 483 | | |
| 69.1 | 71 | 3480 | 1.9 | 1.8 | 500 | | 2.8 | | 14001 | 78 | 6.84 | 16 | 245 | | |
| 71 | 73 | 3481 | 2 | 1.7 | 790 | | 2.8 | | 13551 | 113 | 6.90 | 20 | 263 | | |
| 73 | 76 | 3482 | 3 | 2.3 | 1120 | 0.036 | 3.5 | | 17695 | 86 | 8.08 | 32 | 263 | | |
| 76 | 79 | 3483 | 3 | 2.3 | 1140 | 0.037 | 2.1 | | 15220 | 46 | 7.33 | 23 | 153 | | |
| 79 | 82 | 3484 | 3 | 1.47 | 1380 | 0.043 | 2.5 | | 18112 | 17 | 7.29 | 23 | 21 | | |
| 82 | 85 | 3485 | 3 | 2.01 | 1070 | 0.037 | 2.1 | | 16670 | 49 | 6.67 | 37 | 585 | | |
| 85 | 88 | 3486 | 3 | 1.92 | 620 | | 2.1 | | 12395 | 73 | 6.24 | 30 | 615 | | |
| 88 | 90.5 | 3487 | 2.5 | .72 | 110 | | 0.1 | | 1812 | 16 | 5.38 | 13 | 33 | | |
| 90.5 | 93 | 3488 | 2.5 | 1.33 | 150 | | 0.4 | | 2854 | 17 | 5.93 | 20 | 26 | | |
| 93 | 95.1 | 3489 | 2.1 | 1.42 | 110 | | 0.1 | | 2304 | 71 | 5.38 | 33 | 188 | | |
| 95.1 | 96.1 | 3490 | 1 | 1 | 100 | | 0.1 | | 766 | 349 | 6.55 | 49 | 2114 | | |
| 96.1 | 97.3 | 3491 | 1.2 | .98 | 250 | | 0.9 | | 7753 | 43 | 6.79 | 76 | 122 | | |
| 97.3 | 97.5 | 3492 | .2 | .18 | 30 | | 0.1 | | 1848 | 577 | 7.44 | 153 | 1764 | | |
| 97.5 | 100.35 | 3493 | 2.85 | 1.36 | 265 | | 1.1 | | 6681 | 114 | 6.29 | 60 | 300 | | |
| 100.35 | 100.9 | 3494 | .55 | .49 | 20 | | 0.1 | | 3169 | 397 | 6.85 | 83 | 1301 | | |
| 100.9 | 103 | 3495 | 2.1 | 1.46 | 180 | | 0.1 | | 7803 | 71 | 6.12 | 188 | 143 | | |
| 103 | 106 | 3496 | 3 | 1.94 | 200 | | 1.1 | | 6437 | 283 | 5.43 | 225 | 390 | | |
| 106 | 109 | 3497 | 3 | 1.56 | 180 | | 2.1 | | 7792 | 69 | 6.05 | 189 | 201 | | |
| 109 | 112 | 3498 | 3 | 1.09 | 210 | | 0.4 | | 3624 | 278 | 5.34 | 157 | 964 | | |
| 112 | 115 | 3499 | 3 | 1.6 | 100 | | 0.1 | | 2186 | 195 | 4.03 | 122 | 879 | | |
| 115 | 118 | 3500 | 3 | 1.12 | 195 | | 1.2 | | 4153 | 285 | 5.09 | 68 | 596 | | |
| 118 | 121 | 8448 | 3 | .36 | 55 | | 0.1 | | 3019 | 264 | 4.00 | 20 | 914 | | |
| 121 | 124 | 8449 | 3 | .22 | 60 | | 0.4 | | 2759 | 258 | 3.18 | 19 | 643 | | |
| 124 | 126.5 | 8450 | 2.5 | .57 | 90 | | 0.9 | | 3361 | 272 | 3.69 | 33 | 620 | | |
| 126.5 | 129 | 8451 | 2.5 | 1.62 | 190 | | 1.1 | | 2106 | 186 | 3.39 | 16 | 1191 | | |
| 129 | 132 | 8452 | 3 | 2.95 | 100 | | 0.9 | | 2003 | 606 | 3.39 | 21 | 1653 | | |
| 132 | 135 | 8453 | 3 | 3 | 125 | | 0.9 | | 2674 | 160 | 4.22 | 18 | 568 | | |
| 135 | 136.85 | 8454 | 1.85 | 1.85 | 140 | | 1.2 | | 2193 | 529 | 4.41 | 40 | 1097 | | |

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656


REPORT NUMBER: 881151 AA JOB NUMBER: 881151 WESTERN CDN. MINING CORP. 

| SAMPLE # | Au oz/st |
|---|---|
| C88 - 3482 | .038 |
| C88 - 3483 | .037 |
| C88 - 3484 | .043 |
| C88 - 3485 | .037 |

DETECTION LIMIT .005

1 Troy oz/short ton = 34.28 ppm 1 ppm = 0.0001% ppm = parts per million < = less than

signed: _____

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1989 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5656 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656




| SAMPLE # | Cu % |
|---|---|
| C88-3479 | .45 |
| C88-3480 | 1.44 |
| C88-3481 | 1.32 |
| C88-3482 | 1.73 |
| C88-3483 | 1.65 |
| C88-3484 | 1.75 |
| C88-3485 | 1.61 |
| C88-3486 | 1.33 |
| C88-3487 | .18 |
| C88-3488 | .30 |
| C88-3489 | .26 |
| C88-3490 | .10 |
| C88-3491 | .82 |
| C88-3492 | .21 |
| C88-3493 | .74 |
| C88-3494 | .43 |
| C88-3495 | .85 |
| C88-3496 | .71 |
| C88-3497 | .81 |
| C88-3498 | .39 |
| C88-3499 | .26 |
| C88-3500 | .46 |
| DETECTION LIMIT | .01 |

1 Troy oz/short ton = 34.28 ppm  1 ppm = 0.0001%  ppm = parts per million  < = less than

signed: _____

VGC

# VANGEOCHEM LAB LIMITED

MAIN OFFICE AND LABORATORY
1988 Triumph Street
Vancouver, B.C. V5L 1K5
(604)251-5838 FAX:254-5717

BRANCH OFFICE
1630 PANDORA ST.
VANCOUVER, B.C. V5L 1L6
(604) 251-5656



| SAMPLE # | Cu % |
|---|---|
| C88-8448 | .36 |
| C88-8449 | .30 |
| C88-8450 | .41 |
| C88-8451 | .23 |
| C88-8452 | .24 |
| C88-8453 | .30 |
| C88-8454 | .26 |

VANGEOCHEM LAB LIMITED
1988 TRIUMPH STREET
VANCOUVER, B.C. V5L 1K5
(604) 251-5656 FAX (604) 254-5717



REPORT #: 881151 PA  WESTERN CANADIAN MINING CORP.

| Sample Number | Ag ppm | Al % | As ppm | AuFA ppb | Au ppm | Ba ppm | Bi ppm | Ca % | Cd ppm | Co ppm | Cr ppm | Cu ppm | Fe % | K % | Mg % | Mn ppm | Mo ppm | Na % | Ni ppm | P % | Pb ppm | Pd ppm | Pt ppm | Sb ppm | Sn ppm | Sr ppm | U ppm | W ppm | Zn ppm |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| C88 - 3456 | 0.6 | 0.42 | 323 | 170 | <3 | 5 | <3 | 0.14 | 1.4 | 13 | 51 | 3961 | 5.71 | 0.05 | 0.18 | 66 | 15 | 0.01 | 3 | 0.21 | 45 | <3 | <5 | 59 | 3 | 31 | <5 | <3 | 123 |
| C88 - 3457 | 0.1 | 0.49 | 230 | 95 | <3 | 5 | <3 | 0.25 | 1.2 | 13 | 79 | 1937 | 6.08 | 0.06 | 0.15 | 66 | 6 | 0.01 | 3 | 0.23 | 58 | <3 | <5 | 32 | 3 | 13 | <5 | <3 | 76 |
| C88 - 3458 | 0.2 | 0.35 | 81 | 240 | <3 | 5 | <3 | 2.17 | 1.5 | 16 | 53 | 3472 | 7.11 | 0.28 | 0.16 | 457 | 2 | 0.01 | 3 | 0.19 | 41 | <3 | <5 | 14 | 3 | 37 | <5 | <3 | 72 |
| C88 - 3459 | 0.1 | 1.13 | 17 | 370 | <3 | 6 | <3 | 1.18 | 0.9 | 15 | 45 | 1553 | 5.02 | 0.20 | 0.77 | 476 | 4 | 0.01 | 3 | 0.18 | 23 | <3 | <5 | 7 | 3 | 22 | <5 | <3 | 94 |
| C88 - 3460 | 0.1 | 1.70 | 22 | 100 | <3 | 8 | 3 | 0.32 | 1.1 | 16 | 39 | 1813 | 5.42 | 0.08 | 1.64 | 323 | 3 | 0.01 | 4 | 0.19 | 32 | <3 | <5 | 14 | 4 | 7 | <5 | <3 | 128 |
| C88 - 3461 | 0.2 | 1.32 | 18 | 110 | <3 | 6 | 3 | 0.25 | 0.9 | 14 | 52 | 2721 | 4.93 | 0.07 | 1.15 | 264 | 4 | 0.01 | 3 | 0.18 | 45 | <3 | <5 | 9 | 3 | 7 | <5 | <3 | 91 |
| C88 - 3462 | 0.1 | 1.50 | 16 | 85 | <3 | 7 | 3 | 0.36 | 1.1 | 14 | 19 | 2443 | 4.83 | 0.08 | 2.00 | 494 | 3 | 0.01 | 4 | 0.18 | 33 | <3 | <5 | 13 | 4 | 10 | <5 | <3 | 125 |
| C88 - 3463 | 0.2 | 1.78 | 17 | 80 | <3 | 7 | <3 | 0.33 | 1.1 | 11 | 41 | 2852 | 4.47 | 0.08 | 1.69 | 473 | 7 | 0.01 | 3 | 0.18 | 32 | <3 | <5 | 11 | 3 | 20 | <5 | <3 | 99 |
| C88 - 3464 | 0.1 | 1.73 | 20 | 95 | <3 | 8 | <3 | 0.35 | 1.1 | 14 | 30 | 2116 | 4.60 | 0.08 | 1.71 | 467 | 8 | 0.01 | 4 | 0.20 | 30 | <3 | <5 | 12 | 3 | 14 | <5 | <3 | 95 |
| C88 - 3465 | 1.1 | 1.38 | 24 | 190 | <3 | 5 | 4 | 0.35 | 1.9 | 12 | 56 | 4224 | 6.23 | 0.09 | 1.25 | 370 | 6 | 0.01 | 4 | 0.18 | 70 | <3 | <5 | 17 | 4 | 17 | <5 | <3 | 72 |
| C88 - 3466 | 0.6 | 1.03 | 17 | 130 | <3 | 5 | <3 | 0.26 | 1.1 | 15 | 16 | 2911 | 5.37 | 0.07 | <0.01 | 207 | 4 | 0.01 | 4 | 0.18 | 26 | <3 | <5 | 8 | 3 | 14 | <5 | <3 | 61 |
| C88 - 3467 | 0.6 | 1.48 | 19 | 220 | <3 | 6 | 3 | 0.38 | 1.1 | 18 | 43 | 4764 | 4.82 | 0.09 | 1.34 | 474 | 6 | 0.01 | 4 | 0.16 | 40 | <3 | <5 | 11 | 4 | 19 | <5 | <3 | 84 |
| C88 - 3468 | 0.2 | 2.24 | 21 | 145 | <3 | 9 | 3 | 0.27 | 1.2 | 13 | 32 | 3595 | 4.77 | 0.07 | 2.06 | 515 | 6 | 0.01 | 3 | 0.19 | 35 | <3 | <5 | 18 | 4 | 21 | <5 | <3 | 122 |
| C88 - 3469 | 0.1 | 2.20 | 20 | 160 | <3 | 15 | <3 | 0.28 | 0.6 | 14 | 52 | 2900 | 3.76 | 0.09 | 1.89 | 521 | 11 | 0.01 | 4 | 0.19 | 35 | <3 | <5 | 15 | 3 | 17 | <5 | <3 | 120 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 2000 |

< = Less than Minimum  is = Insufficient Sample  ns = No sample  > = Greater than Maximum  AuFA = Fire assay/AAS

REPORT #: 881151 PA

WESTERN CANADIAN MINING CORP.

| Sample Number | Ag | Al | As | AuFA | Au | Ba | Bi | Ca | Cd | Co | Cr | Cu | Fe | K | Mg | Mn | Mo | Na | Ni | P | Pb | Pd | Pt | Sb | Sn | Sr | U | W | Zn |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | ppm | % | ppm | ppb | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | % | % | % | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| C88 - 3470 | 0.9 | 1.27 | 35 | 170 | <3 | 5 | <3 | 0.30 | 1.1 | 13 | 28 | 2657 | 5.25 | 0.07 | 0.92 | 207 | 5 | 0.01 | 6 | 0.26 | 91 | <3 | <5 | <2 | 3 | 20 | <5 | <3 | 85 |
| C88 - 3471 | 0.4 | 1.81 | 40 | 260 | <3 | 5 | 3 | 0.23 | 1.2 | 16 | 77 | 5145 | 5.65 | 0.06 | 1.22 | 183 | 5 | 0.01 | 7 | 0.24 | 54 | <3 | <5 | <2 | 4 | 13 | <5 | <3 | 119 |
| C88 - 3472 | 0.1 | 1.88 | 26 | 200 | <3 | 6 | 3 | 0.23 | 1.4 | 12 | 49 | 4186 | 5.63 | 0.06 | 1.48 | 253 | 2 | 0.01 | 6 | 0.22 | 51 | <3 | <5 | <2 | 3 | 14 | <5 | <3 | 138 |
| C88 - 3473 | 0.4 | 2.52 | 27 | 280 | <3 | 7 | 4 | 0.22 | 1.5 | 12 | 71 | 6189 | 5.86 | 0.06 | 2.02 | 371 | 3 | 0.01 | 6 | 0.21 | 43 | <3 | <5 | <2 | 4 | 22 | <5 | <3 | 195 |
| C88 - 3474 | 0.1 | 0.95 | <3 | <5 | <3 | 234 | <3 | 1.05 | 0.1 | 2 | 57 | 209 | 1.67 | 0.19 | 0.37 | 590 | 2 | 0.03 | 3 | 0.02 | 16 | <3 | <5 | <2 | <2 | 40 | <5 | <3 | 142 |
| C88 - 3475 | 0.1 | 1.23 | <3 | 90 | <3 | 722 | <3 | 1.15 | 0.4 | 4 | 24 | 86 | 2.67 | 0.20 | 0.44 | 619 | <1 | 0.03 | 1 | 0.06 | 21 | <3 | <5 | <2 | 2 | 79 | <5 | <3 | 166 |
| C88 - 3476 | 0.1 | 3.44 | 3 | 5 | <3 | 543 | 3 | 2.02 | 1.7 | 13 | 22 | 597 | 6.30 | 0.26 | 1.49 | 1589 | 3 | 0.03 | 2 | 0.20 | 43 | <3 | <5 | <2 | 3 | 73 | <5 | <3 | 302 |
| C88 - 3477 | 0.4 | 2.32 | 20 | 270 | <3 | 17 | 3 | 0.40 | 1.5 | 13 | 31 | 3197 | 5.58 | 0.09 | 1.86 | 620 | 4 | 0.01 | 4 | 0.19 | 39 | <3 | <5 | <2 | 3 | 20 | <5 | <3 | 259 |
| C88 - 3478 | 1.1 | 1.64 | 18 | 260 | <3 | 7 | 3 | 1.05 | 1.5 | 12 | 47 | 4575 | 5.64 | 0.18 | 1.36 | 845 | 3 | 0.02 | 4 | 0.18 | 33 | <3 | <5 | <2 | 3 | 46 | <5 | <3 | 327 |
| C88 - 3479 | 0.9 | 1.96 | 16 | 310 | <3 | 7 | 3 | 0.34 | 1.4 | 11 | 26 | 4424 | 5.44 | 0.08 | 1.82 | 483 | 1 | 0.01 | 4 | 0.18 | 32 | <3 | <5 | <2 | 3 | 29 | <5 | <3 | 191 |
| C88 - 3480 | 2.8 | 1.07 | 16 | 500 | <3 | 4 | 4 | 0.22 | 1.9 | 12 | 107 | 14001 | 6.84 | 0.06 | 0.82 | 245 | 2 | 0.01 | 4 | 0.12 | 35 | <3 | <5 | <2 | 3 | 39 | <5 | <3 | 78 |
| C88 - 3481 | 2.8 | 1.51 | 20 | 790 | <3 | 5 | 4 | 0.19 | 2.1 | 12 | 86 | 13551 | 6.90 | 0.05 | 1.24 | 263 | 2 | 0.01 | 5 | 0.12 | 46 | <3 | <5 | <2 | 4 | 28 | <5 | <3 | 113 |
| C88 - 3482 | 3.5 | 1.94 | 32 | 1120 | <3 | 5 | 5 | 0.12 | 2.4 | 13 | 142 | 17695 | 8.08 | 0.04 | 1.25 | 263 | 8 | 0.01 | 5 | 0.11 | 42 | <3 | <5 | <2 | 4 | 64 | <5 | <3 | 86 |
| C88 - 3483 | 2.1 | 0.97 | 23 | 1140 | <3 | 4 | 4 | 0.13 | 1.9 | 14 | 46 | 15220 | 7.33 | 0.04 | 0.62 | 153 | 3 | 0.01 | 4 | 0.13 | 36 | <3 | <5 | <2 | 3 | 92 | <5 | <3 | 46 |
| C88 - 3484 | 2.5 | 0.28 | 23 | 1380 | <3 | 4 | <3 | 0.08 | 1.6 | 13 | 126 | 18112 | 7.29 | 0.03 | 0.04 | 21 | 5 | 0.01 | 5 | 0.09 | 52 | <3 | <5 | <2 | 3 | 95 | <5 | <3 | 17 |
| C88 - 3485 | 2.1 | 1.72 | 37 | 1070 | <3 | 5 | 5 | 0.14 | 1.9 | 11 | 129 | 16670 | 6.67 | 0.05 | 1.19 | 585 | 5 | 0.01 | 6 | 0.15 | 53 | <3 | <5 | <2 | 4 | 82 | <5 | <3 | 49 |
| C88 - 3486 | 2.1 | 2.02 | 30 | 620 | <3 | 6 | 4 | 0.17 | 1.7 | 12 | 157 | 12395 | 6.24 | 0.05 | 1.60 | 615 | 8 | 0.01 | 6 | 0.18 | 60 | <3 | <5 | <2 | 4 | 75 | <5 | <3 | 73 |
| C88 - 3487 | 0.1 | 0.37 | 13 | 110 | <3 | 4 | <3 | 0.19 | 0.8 | 15 | 53 | 1812 | 5.38 | 0.06 | 0.08 | 33 | 2 | 0.01 | 4 | 0.20 | 135 | <3 | <5 | <2 | 2 | 33 | <5 | <3 | 16 |
| C88 - 3488 | 0.4 | 0.48 | 20 | 150 | <3 | 4 | <3 | 0.18 | 1.1 | 20 | 103 | 2854 | 5.93 | 0.06 | 0.06 | 26 | 4 | 0.01 | 6 | 0.17 | 113 | <3 | <5 | <2 | 2 | 15 | <5 | <3 | 17 |
| C88 - 3489 | 0.1 | 0.96 | 33 | 110 | <3 | 5 | <3 | 0.22 | 1.1 | 18 | 39 | 2304 | 5.38 | 0.06 | 0.67 | 188 | 2 | 0.01 | 4 | 0.29 | 94 | <3 | <5 | <2 | 3 | 14 | <5 | <3 | 71 |
| C88 - 3490 | 0.1 | 5.20 | 49 | 100 | <3 | 162 | 4 | 0.49 | 1.7 | 28 | 37 | 766 | 6.55 | 0.11 | 3.94 | 2114 | 3 | 0.02 | 19 | 0.31 | 80 | <3 | <5 | <2 | 4 | 30 | <5 | <3 | 349 |
| C88 - 3491 | 0.9 | 0.70 | 76 | 250 | <3 | 6 | 3 | 0.14 | 1.5 | 14 | 59 | 7753 | 6.79 | 0.05 | 0.31 | 122 | 3 | 0.01 | 6 | 0.30 | 70 | <3 | <5 | <2 | 3 | 8 | <5 | <3 | 43 |
| C88 - 3492 | 0.1 | 8.37 | 153 | 30 | <3 | 32 | 4 | 0.72 | 1.7 | 35 | 274 | 1848 | 7.44 | 0.15 | 8.59 | 1764 | 1 | 0.02 | 196 | 0.98 | 228 | <3 | <5 | <2 | 4 | 87 | <5 | <3 | 577 |
| C88 - 3493 | 1.1 | 1.81 | 60 | 265 | <3 | 5 | 4 | 0.20 | 1.6 | 16 | 144 | 6681 | 6.29 | 0.06 | 1.58 | 300 | 3 | 0.01 | 25 | 0.42 | 80 | <3 | <5 | <2 | 4 | 16 | <5 | <3 | 114 |
| C88 - 3494 | 0.1 | 6.87 | 83 | 20 | <3 | 35 | 5 | 0.58 | 1.6 | 33 | 225 | 3169 | 6.85 | 0.13 | 6.88 | 1301 | 2 | 0.02 | 172 | 0.55 | 144 | <3 | <5 | <2 | 4 | 98 | <5 | <3 | 397 |
| C88 - 3495 | 0.1 | 1.25 | 188 | 180 | <3 | 5 | <3 | 0.22 | 1.2 | 12 | 30 | 7803 | 6.12 | 0.04 | 0.69 | 143 | 3 | 0.01 | 8 | 0.55 | 176 | <3 | <5 | <2 | 3 | 18 | <5 | <3 | 71 |
| C88 - 3496 | 1.1 | 2.37 | 225 | 200 | <3 | 6 | 3 | 0.18 | 2.2 | 12 | 66 | 6437 | 5.43 | 0.06 | 1.28 | 390 | 8 | 0.02 | 6 | 0.67 | 341 | <3 | <5 | <2 | 4 | 21 | <5 | <3 | 283 |
| C88 - 3497 | 2.1 | 1.37 | 189 | 180 | <3 | 5 | 3 | 0.17 | 1.5 | 14 | 80 | 7792 | 6.05 | 0.06 | 0.54 | 201 | 7 | 0.01 | 5 | 0.38 | 209 | <3 | <5 | <2 | 4 | 9 | <5 | <3 | 69 |
| C88 - 3498 | 0.4 | 2.81 | 157 | 210 | <3 | 13 | 3 | 0.21 | 1.2 | 13 | 43 | 3624 | 5.34 | 0.06 | 2.22 | 964 | 10 | 0.01 | 5 | 0.24 | 73 | <3 | <5 | <2 | 3 | 9 | <5 | <3 | 278 |
| C88 - 3499 | 0.1 | 2.91 | 122 | 100 | <3 | 17 | <3 | 0.22 | 0.9 | 10 | 51 | 2186 | 4.03 | 0.07 | 1.96 | 879 | 11 | 0.01 | 5 | 0.24 | 84 | <3 | <5 | <2 | 3 | 16 | <5 | <3 | 195 |
| C88 - 3500 | 1.2 | 2.23 | 68 | 195 | <3 | 6 | <3 | 0.20 | 1.4 | 12 | 59 | 4153 | 5.09 | 0.06 | 1.47 | 596 | 21 | 0.02 | 5 | 0.18 | 93 | <3 | <5 | <2 | 4 | 15 | <5 | <3 | 285 |
| C88 - 8448 | 0.1 | 3.07 | 20 | 55 | <3 | 22 | <3 | 0.23 | 1.1 | 9 | 58 | 3019 | 4.00 | 0.07 | 2.31 | 914 | 7 | 0.01 | 5 | 0.19 | 91 | <3 | <5 | <2 | 3 | 19 | <5 | <3 | 264 |
| C88 - 8449 | 0.4 | 2.01 | 19 | 60 | <3 | 14 | <3 | 0.25 | 0.9 | 8 | 24 | 2759 | 3.18 | 0.08 | 2.02 | 643 | 1 | 0.01 | 5 | 0.21 | 122 | <3 | <5 | <2 | 3 | 12 | <5 | <3 | 258 |
| C88 - 8450 | 0.9 | 1.80 | 33 | 90 | <3 | 9 | <3 | 0.27 | 0.9 | 9 | 45 | 3361 | 3.69 | 0.08 | 1.67 | 620 | 4 | 0.01 | 4 | 0.21 | 276 | <3 | <5 | <2 | 3 | 19 | <5 | <3 | 272 |
| C88 - 8451 | 1.1 | 1.39 | 16 | 190 | <3 | 6 | <3 | 1.99 | 0.9 | 10 | 32 | 2106 | 3.39 | 0.26 | 1.36 | 1191 | 3 | 0.01 | 4 | 0.16 | 42 | <3 | <5 | <2 | 2 | 147 | <5 | <3 | 186 |
| C88 - 8452 | 0.9 | 1.61 | 21 | 100 | <3 | 7 | <3 | 2.39 | 2.6 | 10 | 34 | 2003 | 3.39 | 0.28 | 1.60 | 1653 | 6 | 0.02 | 4 | 0.16 | 68 | <3 | <5 | <2 | 3 | 181 | <5 | <3 | 606 |
| C88 - 8453 | 0.9 | 0.77 | 18 | 125 | <3 | 7 | <3 | 3.01 | 1.2 | 9 | 21 | 2674 | 4.22 | 0.30 | 0.71 | 568 | 6 | 0.02 | 3 | 0.13 | 54 | <3 | <5 | <2 | 2 | 262 | <5 | <3 | 160 |
| C88 - 8454 | 1.2 | 1.04 | 40 | 140 | <3 | 8 | <3 | 2.42 | 2.7 | 11 | 38 | 2193 | 4.41 | 0.28 | 0.97 | 1097 | 8 | 0.02 | 4 | 0.15 | 52 | <3 | <5 | <2 | 2 | 211 | <5 | <3 | 529 |
| Minimum Detection | 0.1 | 0.01 | 3 | 5 | 3 | 1 | 3 | 0.01 | 0.1 | 1 | 1 | 1 | 0.01 | 0.01 | 0.01 | 1 | 1 | 0.01 | 1 | 0.01 | 2 | 3 | 5 | 2 | 2 | 1 | 5 | 3 | 1 |
| Maximum Detection | 50.0 | 10.00 | 1000 | 10000 | 1000 | 1000 | 1000 | 20.00 | 100.0 | 20000 | 1000 | 20000 | 10.00 | 10.00 | 10.00 | 20000 | 1000 | 10.00 | 20000 | 10.00 | 20000 | 100 | 100 | 1000 | 100 | 10000 | 100 | 1000 | 20000 |

( = Less than Minimum  is = Insufficient Sample  ns = No sample  ) = Greater than Maximum  AuFA = Fire assay/AAS

**ANOMALOUS RESULTS:**
FURTHER ANALYSES
BY ALTERNATE
METHODS SUGGESTED