N.T.S.: 104 A/4 W
Latitude: 56' 10'N
Longitude: 1~~30' 02~~'W
129° 56'

GEOLOGICAL, GEOCHEMICAL, AND GEOPHYSICAL REPORT ON THE STRIKE 1, 2, AND 3 CLAIM GROUP

Skeena Mining Division
British Columbia

For

WHITE CHANNEL RESOURCES INCORPORATED
#718 - 744 West Hastings Street
Vancouver, B.C.
V6C 1A5

By

Fayz F. Yacoub, B.Sc., F.G.A.C.

and

Andris Kikauka, B.Sc. (Hons.)

OCTOBER 30, 1989

ITEMIZED COST STATEMENT

STRIKE 1,2, and 3 Claims

September and October, 1989

Mob/Demob (includes transportation, freight, and wages)		$ 1,600.00
Field Crew:		
White Channel Resources Inc. Personnel:		
Project Geologist (A. Kikauka)		
@ $350/day x 10 days	$ 3,500.00	
Geotechnician (I. Rose) @ $150/day x 10 days	1,500.00	
Ashworth Explorations Ltd. Personnel:		
Geologist (F. Yacoub) @ $350/day x 4 days	1,400.00	
Geotechnician (R. Paeseler) @ $200/day x 4 days	800.00	
Geotechnician (T. Kovacs) @ $200/days x 4 days	800.00	
Geotechnician (A. Molnar) @ $150/day x 4 days	600.00	
		8,600.00
Field Costs:		
Helicopter (VIH - Stewart, B.C.)		
@ $650/hr x 2.7 hours	1.755.00	
Geophysical equipment (EDA Omni Mag VLF)		
@ $150/day x 4 days	600.00	
Room and Board @ $45/day/man x 36 man days	1,620.00	
Communications @ $25/day x 10 days	250.00	
1 4x4 truck @ $70/day x 10 days	700.00	
Supplies	50.00	
		4,975.00
Lab Analysis:		
102 Rock chip samples (Cu, Pb, Zn, Ag, Au assay)		
@ $34.40 sample	3,406.80	
236 soil and 10 silt		
(30 element ICP, gold by FA/AA) @ $16.75\sample	4,120.50	
		7,527.30
Report:		
Report writing	1,000.00	
Drafting and plotting	750.00	
Word processing, copying, and binding	150.00	
		2,100.00
TOTAL		$ 24,802.30

SUMMARY

The Strike Claim Group consists of three contiguous mineral claims comprising 48 units. The property is situated in the Skeena Mining Division approximately 20 kilometres north of Stewart, B.C.

The claims lie within the "Golden Crescent" of the Stewart Complex. This area is receiving an increase of attention with world class gold-silver deposits which currently represents the most active exploration area in the Western Cordillera.

The property is underlain by Middle Jurassic argillaceous siltstone, greywackes, volcanic breccia and lithic tuff. This sequence is cut locally by a series of dykes and high level stocks forming part of the Portland Canal dyke swarm.

Twelve quartz-sulphide veins, concentrated along the axial plane of a north plunging anticline, which have been exposed over a strike length of 700 metres, have an average width of 1 metre. A rock chip sample across 40 cm. on one vein, returned an assay of 22.42 g/t Au, 447.3 g/t Ag, 1.5% Pb, .96% Zn. The average assay values are in the range of: 1-2 g/t Au, 30-60 g/t Ag, and 6% combined Pb-Zn.

The geochemical talus fines survey outlined a broad, strong Pb-Zn-Ag anomaly and a moderate to strong Cu-Au anomaly. These anomalies correspond to known showings and extend into areas of overburden.

The geophysical survey located 6 VLF-EM conductors that roughly matched surface exposures of quartz sulphide veins. The five magnetic anomalies were weak and roughly corresponded to dykes.

A Phase II program of diamond drilling, UTEM geophysics, trenching, and geological mapping has been recommended. Approximate cost would be $250,000.

Contingent on the Phase II results, a Phase III program of detailed diamond drilling and trenching is recommended.

TABLE OF CONTENTS

LIST OF FIGURES, PLATES, MAPS, AND APPENDICES

1. INTRODUCTION

This report summarizes geological-geochemical-geophysical surveys carried out between September 7, 1989 to October 3, 1989. One of the authors, Mr. Andris Kikauka, planned and supervised all fieldwork and was project geologist on the subject claims from September 7-13, 21-23, 1989. The co-author, Mr. Fayz Yacoub, was present on the subject claims from September 26-29, 1989.

2. LOCATION, ACCESS, AND PHYSIOGRAPHY

The Strike 1, 2, and 3 Claim Group is located approximately 20 kilometres north of Stewart, B.C. The property lies within the Skeena Mining Division on NTS mapsheet 104 A/4 W. (Figure 1).

Elevations on the claim group range from 1175 to 1675 metres. Slopes are generally moderate at the southern portion of the Claim Group and steep to moderate in the north. The slopes are generally bare with only a thin overburden/talus cover.

The area of detailed field work is located in the southern portion of the Strike 2 Claim. This was referred to by Grove (1971) as the Silver Crown mineral occurrence.

The Silver Crown showing is exposed at 1375 - 1525 metres elevation on a moderate slope 1.5 kilometres east of the present north tip of Long Lake. There is road access to Long Lake (1000 metre elevation) with relatively easy, above treeline access to the Silver Crown. This area is one of the most accessible access routes to the alpine zone in the Stewart mining camp. It is located 12 kilometres from the new mill at the Silbak-Premier Mine via Moniter Lake and Cooper Creek.

3. PROPERTY STATUS

The Strike 1, 2 and 3 Claim Group consists of 3 continguous claims, located in the Skeena Mining Division. The claims are owned by White Channel Resources Incorporated. (Figure 1).

Claim Name	# of Units	Record #	Record Date	Expiry Date
Strike 1	18	7569	April 24, 1989	April 24, 1990
Strike 2	18	7570	April 24, 1989	April 24, 1990
Strike 3	12	7571	April 24, 1989	April 24, 1990
Total	48			

The total area, correcting for overlap, is approximately 1,050 hectacres.

4. AREA HISTORY

Exploration activity in the Stewart gold-silver district continues to be one of the most active mineral exploration areas of North America demonstrated by numerous projects being carried out by major and junior mining companies.

Westmin Resources is mining the Silbak-Premier and Big Missourri gold-silver properties. Newhawk Gold Mines is approaching production of their Brucejack Lake property. Skyline Gold Corp. is mining their Stonehouse gold deposit. Cominco-Prime are approaching production on the Snip deposit. Con. Stikine-Calpine are rapidly inferring a world class gold-silver deposit. Westmin-Tenajon are now mining the Silver Butte deposit. Other deposits are approaching feasibility, including: Echo Bay-Magna-Silver Princess Doc property, Catear Golden Wedge, Bond Gold Red Mountain.

Many of the 500 gold-silver mines, prospects and new discoveries will receive more attention in the Stewart area over the next decade.

5. PROPERTY HISTORY

The Silver Crown Showing was discovered in 1965. The ablation of the glacial ice in the alpine area exposed this showing approximately 25 years ago. Work performed during 1965 included trenching and sampling. Work at that time included blasting and sampling 33 trenches over a length of 200 metres along a mineralized zone extending over 450 metres. One selected sample was reported to assay 0.01 oz/ton Au, 6.0 oz/ton Ag, 0.02% Cu, 13.37% Pb, 43.9% Zn, and 0.59% Cd over a width of 1 metre (Grove, 1971).

In 1982, an assessment report was filed for Teuton Resources Ltd. This program was hampered by bad weather and heavy snow accumulation.

Trace element analysis of sulphides from the Silver Crown were compared to other Stewart mineral deposits (Grove, 1971). Pyrite from the Silver Crown had relatively high Cu-Pb-Zn values as did pyrite from the Silbak-Premier and Indian mines. Sphalerite from the Silver Crown contained relatively high Cu-Pvb values as did samples from the Silbak-Premier, Silver Tip, Indian and Dunwell mines. Galena from the Silver Crown had relatively high Cu-Zn as did samples from Silbak-Premier, Dunwell, and Indian mines. The significance of this comparison is that a polymetallic association of Pb-Zn-Cu is common to both the Silver Crown and the Silbak-Premier.

6. GENERAL GEOLOGY

The Stewart Complex includes a thick sequence of mainly late Triassic to late Middle Jurassic volcanic, sedimentary, and metamorphic rocks. These have been intruded and cut by a mainly granitic to syenitic suite of Lower Jurassic through Tertiary plutons which together form part of the Coast Plutonic Complex. Deformation, in part related to intrusive activity has produced complex fold structures along the main intrusive contacts with simple open folds and warps dominant along the east side of the Complex. Cataclasis marked by strong north-south structures are prominent structural features that cut all the pre Lower Middle Jurassic units. (Figure 2).

Country rocks in the general Stewart area comprise mainly Hazleton Group strata which include the Lower Jurassic Unuk River Formation and the Middle Jurassic Betty Creek and Salmon River Formation and the Upper Jurassic Nass Formation (Grove, 1971, 1986). In the general Stewart area the Unuk River strata include mainly fragmental andesitic volcanics, epiclastic volcanics and minor volcanic flows. Widespread Aalenian uplift and erosion was followed by deposition of the partly marine volcaniclastic Betty Creek Formation, the mixed Salmon River Formation, and the dominantly shallow marine Nass Formation.

Intrusive activity in the Stewart area has been marked by the Lower to Middle Jurassic Texas Creek granodiorite with which the Big Missouri, Silbak Premier and many small ore deposits are associated. Younger intrusions include the extensive Hyder Quartz Monzonite and the many Tertiary stocks and dike swarms which form a large part of the Coast Clutonic Complex. Mineral deposits such as the major B.C. Molybdenum mine at Alice Arm and a host of smaller deposists are localized in or related to these 48 to 52 m.y plutons which include dykes forming part of the regionally extensive Portland Canal Dike Swarm (Grove, 1986).

Stewart District Mineral Deposits

More than 700 mineral deposits and showings have now been discovered in a large variety of rocks and structural traps in the Stewart District. The famous Silbak Premier mine which has been reactivated as an open pit operation by Westmin Resources represents a telescoped epithermal gold-silver base metal deposit localized along a complex steep fracture system in Lower Jurassic volcaniclastics overlain by shallow dipping Middle Jurassic Salmon River Formation sedimentary rocks. In this example, the shallow lying younger rock units formed a dam, trapping bonanza type gold-silver mineralization at a relatively shallow depth. Mineralization at the Silbak Premier, Big Missouri and a number of other deposits in the area have been related to early Middle

Jurassic regional plutonic-volcanic event (Grove 1971, 1986). Younger high grade mineralization found localized in various members of the Portland Canal Dike Swarm particularly in the Stewart area have also been related to Cretaceous and Tertiary plutonic-volcanic events. Overall at least four major episodes of mineralization involving gold-silver, base metals, molybdenum and tungsten dating from early Lower Middle Jurassic through to the Tertiary have been recorded throughout the Stewart Complex.

7. 1989 FIELD PROGRAM

7.1 SCOPE AND PURPOSE

From September 7-13, 1989, a geologist and geotechnician carried out geological mapping, soil and talus fines sampling, and rock chip sampling of existing trenches.

From September 21-29, 1989, two geologist, three geotechnicians and a geophysicist carried out geological mapping, soil, talus fines, and stream sediment sampling, geophysics, and trenching.

The purpose of this program was:

a) to cover the property with detailed geochemical, geological, and geophysical surveys in order to define drill targets and additional follow-up exploration work,

b) to evaluate and extend the known showings, and

c) to find and systematically sample sulphide mineralization on the property.

7.2 METHODS AND PROCEDURES

Utilizing compass and hipchain, a flagged grid was laid over the southern portion of the Strike 2 claim. The grid covered an area 1.0 x 0.5 kilometres, with a line spacing of 100 metres. A total of 7.0 line kilometres were surveyed.

Geological mapping was carried out at a scale of 1:2,500.

A Swedish plugger was used to drill trench holes and 70% forcite was used to blast the trenching sites. A total of 102 rock chip samples, averaging 2.5 kilograms, were collected on the property and assayed for Cu, Pb, Zn, Ag, Au by Ecotech Lab, Stewart, B.C.

Using a grub hoe, soil samples were collected from talus fines. Sample depths averaged 25 cm. and a total of 236 soil and 10 stream sediment samples were collected and analyzed for gold and multi-element ICP by Acme Analytical Lab, Vancouver, B.C.

A VLF-EM and magnetometer geophysical survey was carried out over the grid area. Readings were taken at 12.5 metre spacing along a total of 7.0 kilometres grid line. Survey specifications and interpretation are included in Section 8.4 and Appendix A.

8. RESULTS

8.1 PROPERTY GEOLOGY AND MINERALIZATION (Map 1)

Geological mapping of the Strike 1, 2, and 3 Claims indicated Middle Jurassic, Betty creek Formation, banded, argillaceous siltstone, greywacke, chert pebble conglomerate, and minor limestone are overlain by Middle Jurassic, Salmon River Formation volcanic breccia, lithic tuff, and minor greywacke. (Figure 2). These Middle Jurassic formations overly Hazleton volcanic epiclastics which locally form the crest of the Bear River Ridge (along the Strike 3 claim). This entire sequence of sediments and volcanics is intruded by a dyke and high level stock complex. The older dyke swarm is mafic to intermediate in composition, some hornblende phenocrysts were noted, and the average width of dykes is 8.0 metres. These dykes were correlated to the Portland Canal Dyke Swarm that extends from Summit Lake to the headwaters of Bitter Creek. High level stocks forming feldspar porphyry have intruded the above sequence, and green-grey felsic dykes, average width of 6.0 metres, cut all the above. A relatively abundant amount of quartz-sulphide mineralization is spatially related to the felsic dykes. This zone is called the Silver Crown Showing, located in the southern portion of the Strike 2 Claim.

Detailed mapping of the Silver Crown reveals quartz and minor carbonate breccia are emplaced along shear zones and fractures in the folded, layered Betty Creek Formation sediments. Sulphide minerals in the quartz veins include medium to coarse-grained pyrite, galena, and honey coloured sphalerite and fine-grained chalcopyrite and tetrahedrite. Gangue minerals include granular white to pinkish quartz, calcite, and barite. 1-10 cm. angular clasts of slightly graphitic argillaceous siltstone form up to 50% of the vein material, but averages 10%. Sulphides form up to 50% of the vein materials, but average 5%. The total strike length of exposed quartz veins on surface is approximately 700 metres. The average width of the veins are 1.0 metre.

The veins are concentrated along the axial plane of a north plunging anticline. The Betty creek sediments are locally folded along this north trend with a shallow plunge angle. The dyke swarm generally trends northwest cutting the strike of the sediments and overlying volcanics. The preponderance of dykes (Plate 1) in various attitudes in the axial plane area of the folded sediments is an indication that this zone had ground conditions necessary for a physically favourable structural trap. Further evidence for this is the abundance of quartz-sulphide veins spatially related to the felsic dykes, which often grade into quartz-sulphide stringers, and 1-2 metre wide contact veins. This is also evident in the Salmon River volcanic breccia where the felsic dykes follow a linear trend (northwest), and are mineralized near their contacts. Veins that cut the argillaceous siltstone strike north (parallel to the strike of the sediments), and generally veins that are associated with the felsic dykes trend northwest (parallel to the strike of the dykes). This observation is verified by the geophysical compilation. The weak magnetic highs correspond to dykes and the EM conductor axes trend north and northwest corresponding to quartz-sulphide veins.

Crystalline quartz lined cavities in the veins suggesting a late stage fracture filling event, probably related to the felsic dykes, which caused remobilization of the quartz-sulphide veins. The fold axis of the north plunging anticline represents a favourable zone for mineral deposits at depth. A comparison of trace element geochemistry in various sulphides from different mineral deposits showed that the Silver Crown had a high Cu-Pb-Zn polymetallic association which compares favourably with the Premier Silbak. The Ag/Au ratios at the Premier Silbak varied from 112:1 near surface to 6:1 at depth (Grove, 1971). It is possible that conditions similar to the Premier Silbak exist at depth on the Silver Crown, and late stage fracture filling has remobilized silver rich minerals to the present surface exposure.

8.2 TRENCHING (Map 2)

The 1989 trenching program blasted an area of 20 square metres to a depth of 1 metre. This resulted in 69 rock chip samples. 33 rock chip samples were taken from existing trenches. (Figures 3 and 4).

Assays (Appendix A) show very high lead values in most of the quartz veins sampled. Medium to coarse grained galena is the most abundant sulphide in the quartz veins that are directly adjacent to the felsic dykes, which form approximately 80% of the exposed veins. These veins have medium grained sphalerite and average silver values are in the 30 to 60 gm/tonne range and average gold values are in the 1 to 2 gm/tonne range. The precious metal values are generally higher with an increase in base metals, however, in veins sampled in the argillaceous siltstone-greywacke host, the mineralogy is significantly different. Approximately 20% of the samples came from the sedimentary host rock where pyrite is the most abundant sulphide. In areas of galena-sphalerite enrichment within these veins, values up to 22.42 gm/tonne Au and 447.3 gm/tonne Ag were recorded accompanied by relatively low Pb-Zn. This suggests the sediment hosted quartz veins may be a different age, probably older than the felsic dyke related quartz veins.

8.3 GEOCHEMISTRY

At elevations above 1300 metres there is virtually no soil, however talus fines from overburden is abundant. Thus, the geochemical analysis certificates (Appendix C) can be considered C horizon or weathered parent material. (Figures 5-8).

Values for Pb-Zn-Ag are relatively high, especially in areas that corresponded to quartz-sulphide veins. Moderate to high Cu-Au values generally corresponded to the same zones. As-Sb-Bi values are low to moderate. This suggests that there is a polymetallic Cu-Pb-Zn-Ag-Au overall assemblage with a dominant Pb-Zn-Ag chemistry.

Sediment sampled from 10 streams at the west edge of the Strike 1 and 2 claims showed a significant increase in precious metals and Pb values in the area of the Silver Crown Showing. Cu and Zn values were moderate across the entire area. As, Sb and Bi values were low.

8.4 GEOPHYSICS

A detailed geophysical interpretation of the Silver Crown Showing is summarized in Appendix A and Maps 5-10. The geophysical survey located 6 VLF-EM conductors that roughly matched surface quartz-sulphide veins. Five magnetic anomalies were weak and roughly corresponded to dykes.

Several VLF-EM conductors were covered by overburden. This includes conductor C2 which is considered to be primary exploration target based on the strength of the VLF-EM anomaly.

9. CONCLUSION

The authors believe that the Strike 1, 2, and 3 Claim Group has potential for hosting an economic Cu-Pb-Zn-Ag-Au deposit for the following reasons:

1. Rock sampling from trenches returned potential economic precious metal and base metal values over significant widths and strike length.
2. Geological mapping has shown several cross-cutting episodes of mineralization indicating potential for a large system of mineralization at depth.
3. Soil sampling and VLF-EM geophysics indicate that there are additional target areas that are covered by overburden.
4. Mining infrastructure is relatively close and accessible to the showings.

For these reasons further exploration work is warranted.

10. RECOMMENDATIONS

PHASE II

a) Diamond drilling in a fence pattern is recommended to test depth extensions of surface trenching. Total diamond drilling to amount to 1525 metres (5,000 feet).

b) Trenching of geophysical and geochemical anomalies. At least two of the geophysical conductor axes were covered by overburden (including the one which gave the most favourable response). Several Au soil anomalies, should be followed up since there was no trenching done in the adjacent area.

c) UTEM or Pulse EM horizontal loop geophysics over a larger area than the present grid (increasing present area of coverage 100%).

d) Detailed geological mapping in the area of the drill program and regional mapping and prospecting of the unmapped areas of the claim.

REFERENCES

Grove, E.W. (1971), Geology and Mineral Deposits of the Stewart Area, BCDM Bulletin No. 58.

Grove E.W. (1986), Geology and Mineral Deposits of the Unuk River-Salmon-River-Anyox Area, Minister of Energy Mines and Petroleum Resources Bulletin No. 63.

Cremonese, D.M. (1984), Assessment Report on the Elk and Moose Claims, # 11800, for Teuton Res. Corp.

Lynberg, E. (1983), Geological Report on the Lois Claim, #12394, for Nor-Con Expl. Ltd.

STATEMENT OF QUALIFICATIONS

I, Andris, Kikauka, of Box 370, Brackendale B.C., V0N 1H0, do hereby declare that:

- I graduated from Brock University, Faculty of Geological Sciences, St. Catharines, Ontario, 1979, receiving Honours B.Sc., First Class.
- From 1976 - 79, have been performing geological field work for Uranium targets on the Canadian Shield.
- From 1979 to 1989, have been performing geological field work, for precious metal, base metal targets on the western cordillera in B.C. and the Yukon Territory.
- Maintain a professional affiliation with the G.A.C. and M.E.G.
- Personally participated in the field work of this report, reviewed and assessed the data.
- I am a principle of White Channel Resources Inc., and this assessment report is written to fulfill government regulations as specified by the current Mineral Act.

Sincerely:

Andris Kikauka

Andris Kikauka, B.Sc.(Hons.)
Geologist

CERTIFICATE

I, FAYZ F. Yacoub, of 13031 - 64th Avenue, Surrey, British Columbia, V3W 1X8, do hereby declare:

1. That I am a graduate in geology and chemistry from Assuit University, Egypt (B.Sc 1967), and Mining Exploration Geology of the International Institute for Aerial Survey and Earth Sciences (I.T.C.), Holland (Diploma 1978).

2. I am a fellow in good standing with the Geological Association of Canada.

3. I have actively pursued my career as a geologist for the past sixteen years.

4. The information, opinions, and recommendations in this report are based on fieldwork carried out by muyself, and on published and unpublished literature. I was present on the subject property on September 27, 1989 to October 3, 1989.

5. I have no interest, direct or indirect, in the subject claims or the securities of White Channel Resources Inc.

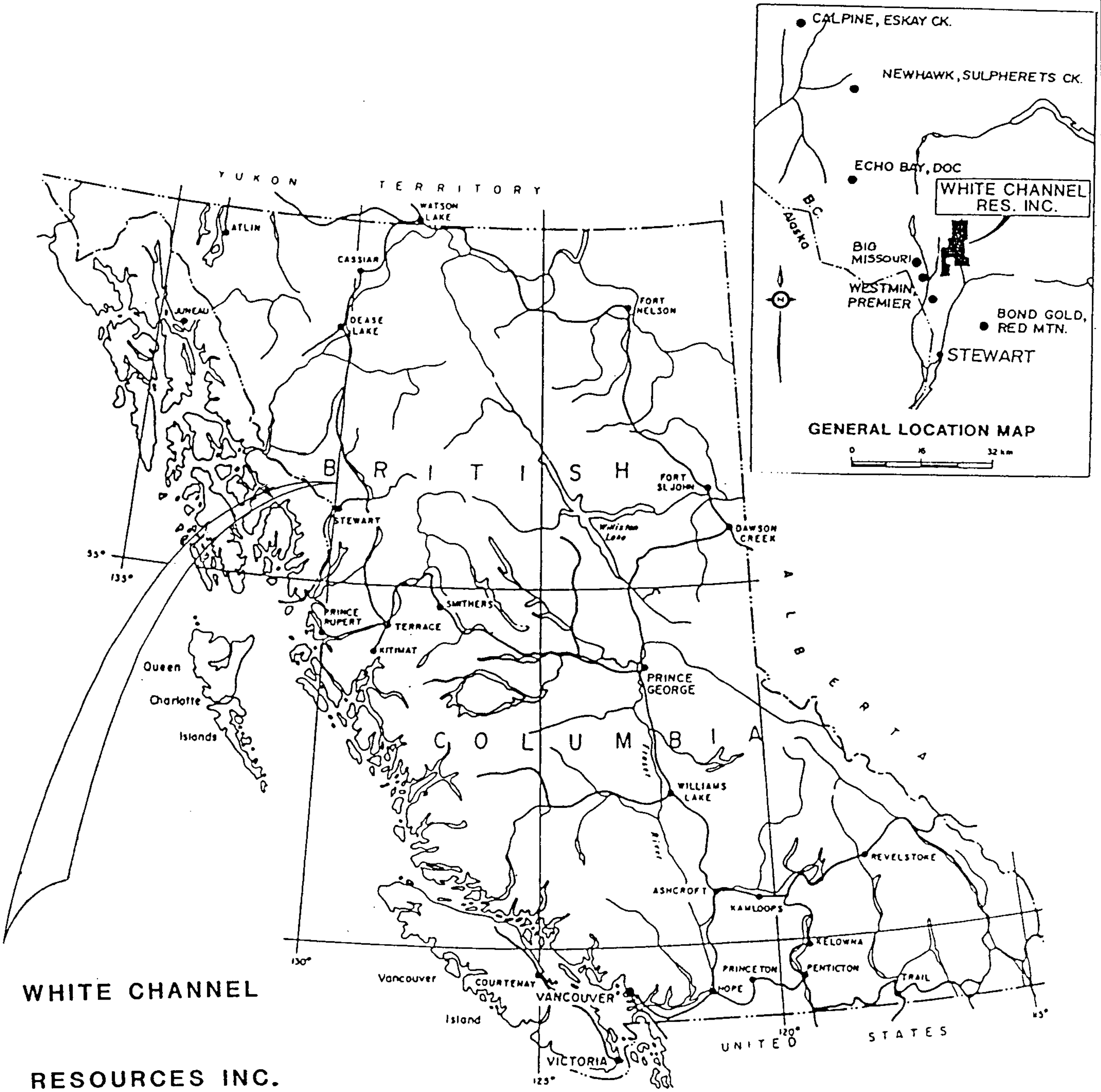
6. I consent to the use of this report in a Prospectus of Statement of Materials Facts for the purpose of private or public financing.

ASHWORTH EXPLORATIONS LIMITED

F. Yacoub

Fayz F. Yacoub, B.Sc., F.G.A.C.

Dated at Vancouver, November 1, 1989

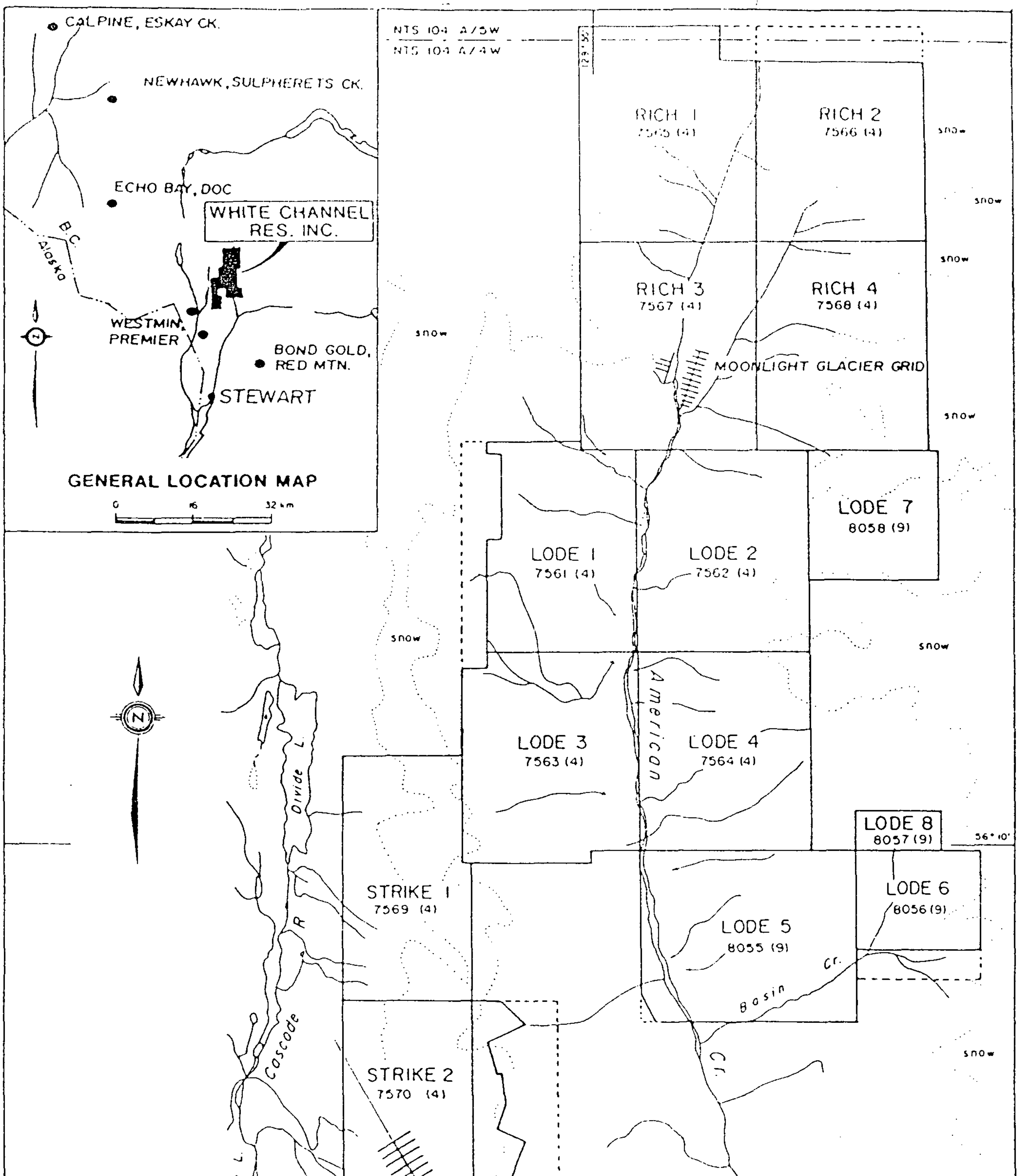


WHITE CHANNEL

RESOURCES INC.

PROPERTIES

FIGURE 1a			
PROPERTY LOCATION MAP			
0 — 100 — 200 MILES; 0 — 100 — 200 — 300 KILOMETRES			
DRAWN	PROJECT	DATE	



WHITE CHANNEL RESOURCES INC.

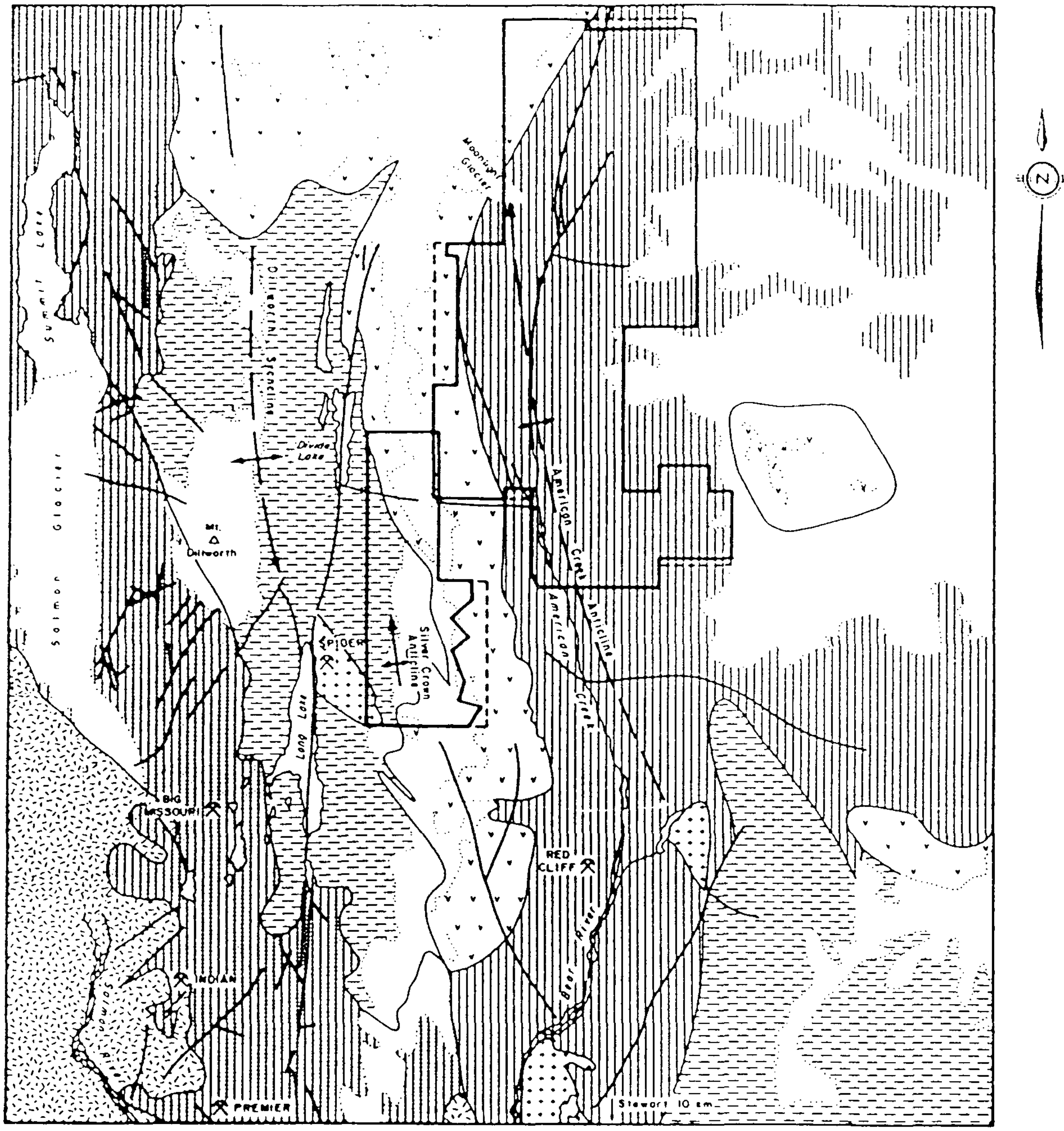
RICH 1-4, LODE 1-8, STRIKE 1-3 CLAIMS

Skeena Mining Division, B. C.

CLAIM LOCATION MAP

NTS 104 A/4W

DATE	Nov, 1989	FIGURE:	1b



SEDIMENTARY AND VOLCANIC ROCKS
MIDDLE JURASSIC
SALMON RIVER FORMATION
Siltstone, greywacke, sandstone, some calcarenite, minor limestone, argillite, conglomerate.
BETTY CREEK FORMATION
Volcanic breccia, conglomerate, sandstone, and siltstone, crystal and lithic tuff.
LOWER JURASSIC
UNUK RIVER FORMATION
Volcanic breccia, conglomerate, sandstone, and siltstone.
PLUTONIC ROCKS
EOCENE AND OLDER
Augite diorite
Granodiorite

Geologic contact
Fault
Fold axis
Snow boundary

METAMORPHIC ROCKS
JURASSIC
Cataclasite, mylonite

KILOMETRES
0 1 2 3 4 5

WHITE CHANNEL RESOURCES INC.

RICH 1-4, LODE 1-8, STRIKE 1-3 CLAIMS

Skeena Mining Division, B. C.

REGIONAL GEOLOGY MAP

NTS 104 A/4W after Grove, 1964-1970

DATE: Nov., 1989 FIGURE: 2

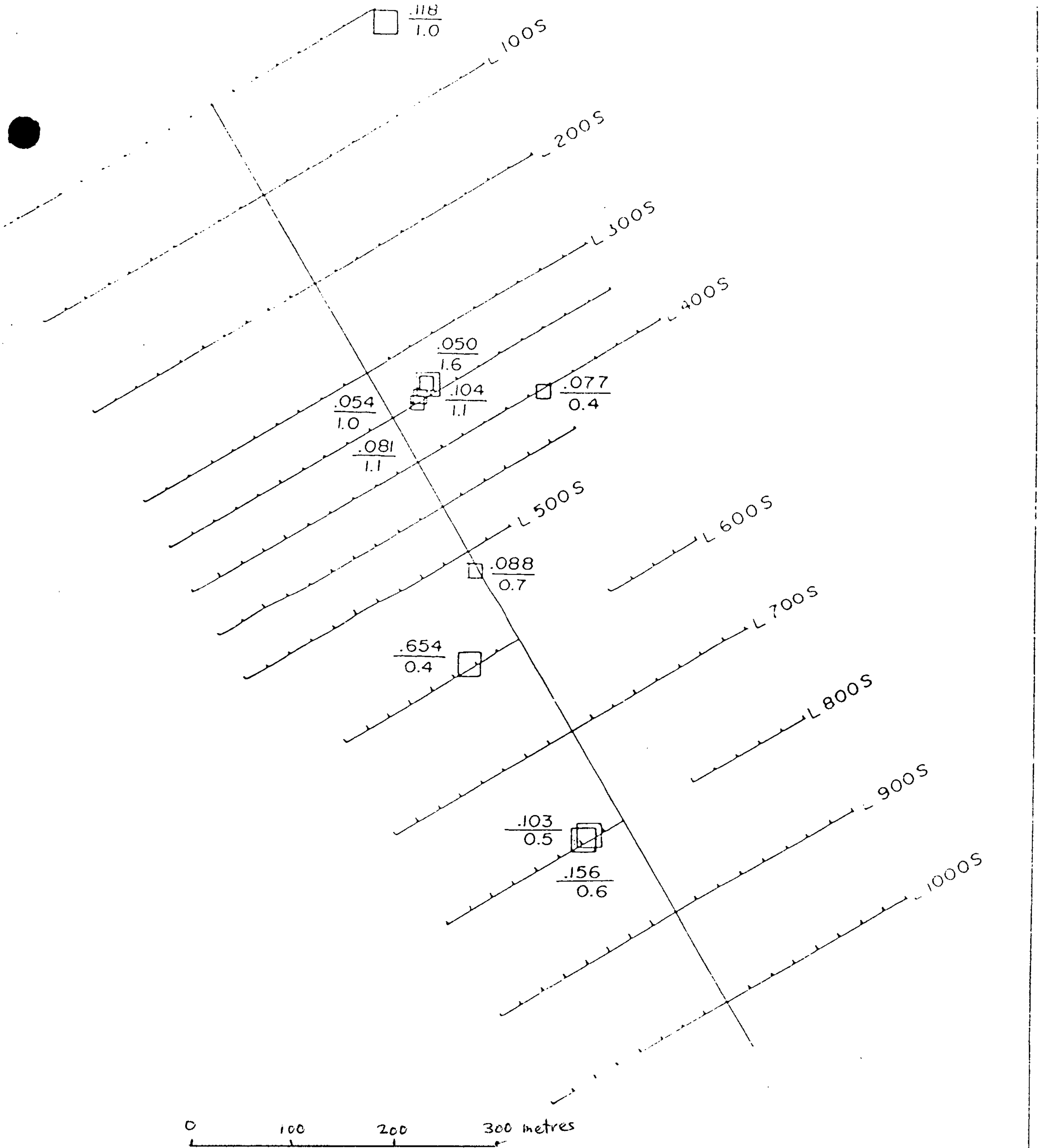


FIG. 3

WHITE CHANNEL RESOURCES INC. OCT 1989

SILVER CROWN SHOWING STRIKE 2 CLAIM - STEWART, B.C.

TRENCH SAMPLES Au

□ .050-.099 oz/t Au

□ ≥ .100 oz/t Au / 1.0 width metres

SCALE 1:5000

N

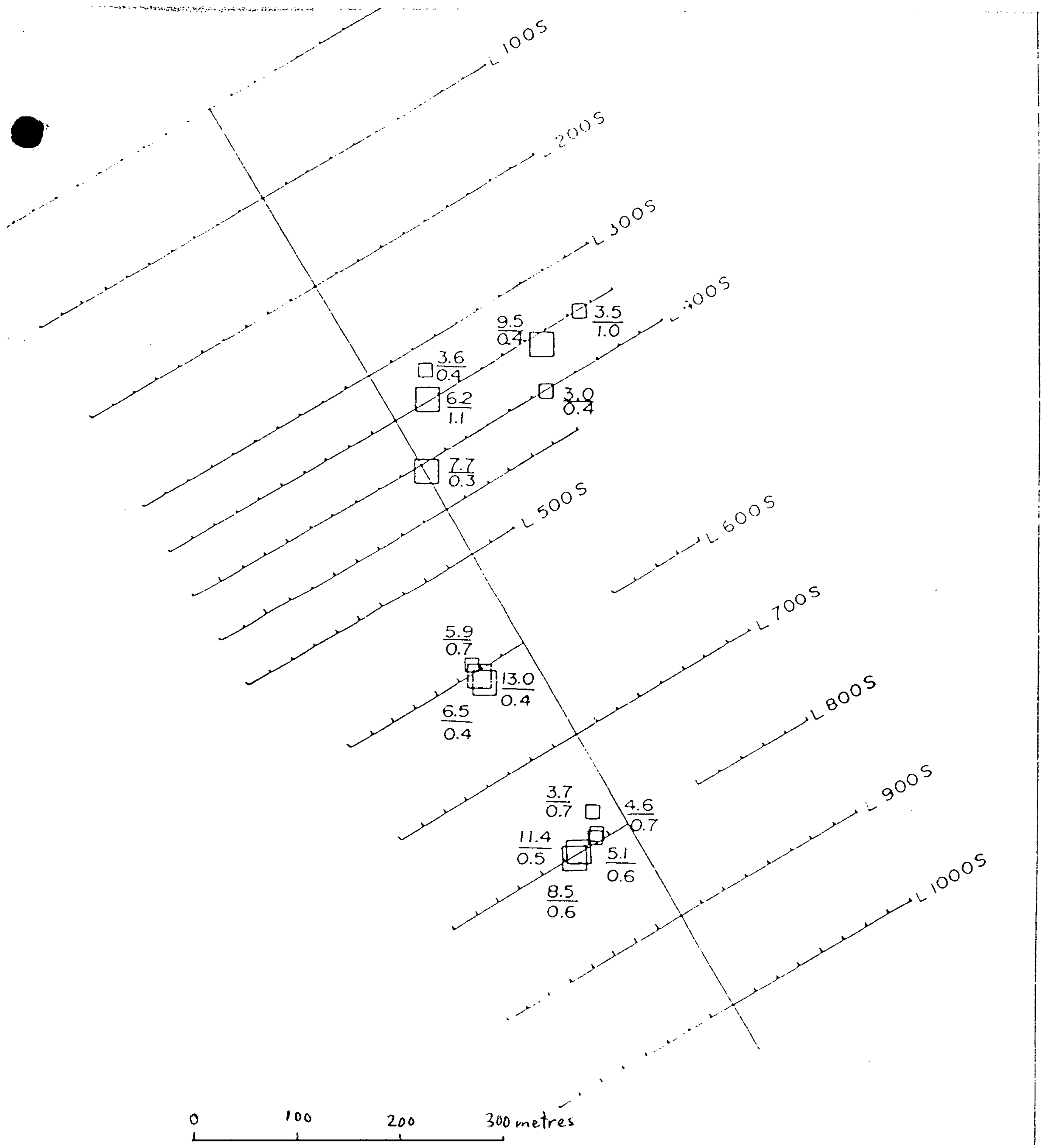


FIG. 4

WHITE CHANNEL RESOURCES INC OCT 1989

SILVER CROWN SHOWING STRIKE 2 CLAIM-STEWART, B.C

TRENCH SAMPLES Ag

□ 3.0-6.0 oz/t Ag

□ >6.0 oz/t Ag / 1.0 width metres

SCALE 1:5000

N

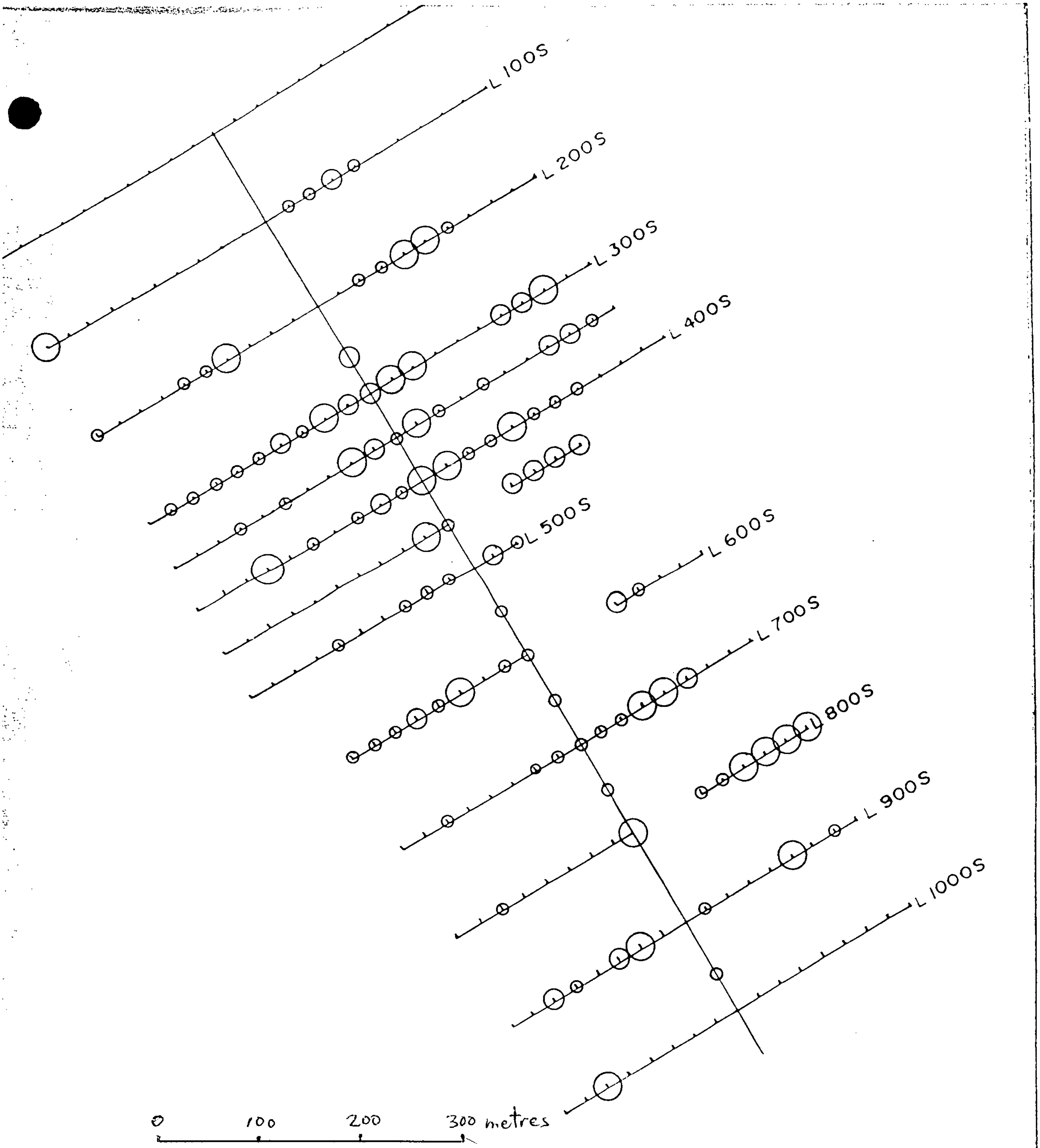


FIG. 5

WHITE CHANNEL RESOURCES INC. OCT. 1989

SILVER CROWN SHOWING STRIKE 2 CLAIM - STEWART, B.C.

SOIL GEOCHEM Pb

○ 300-499 ppm Pb
◯ 500-699 ppm Pb
◯ ≥700 ppm Pb

SCALE 1:5000

N

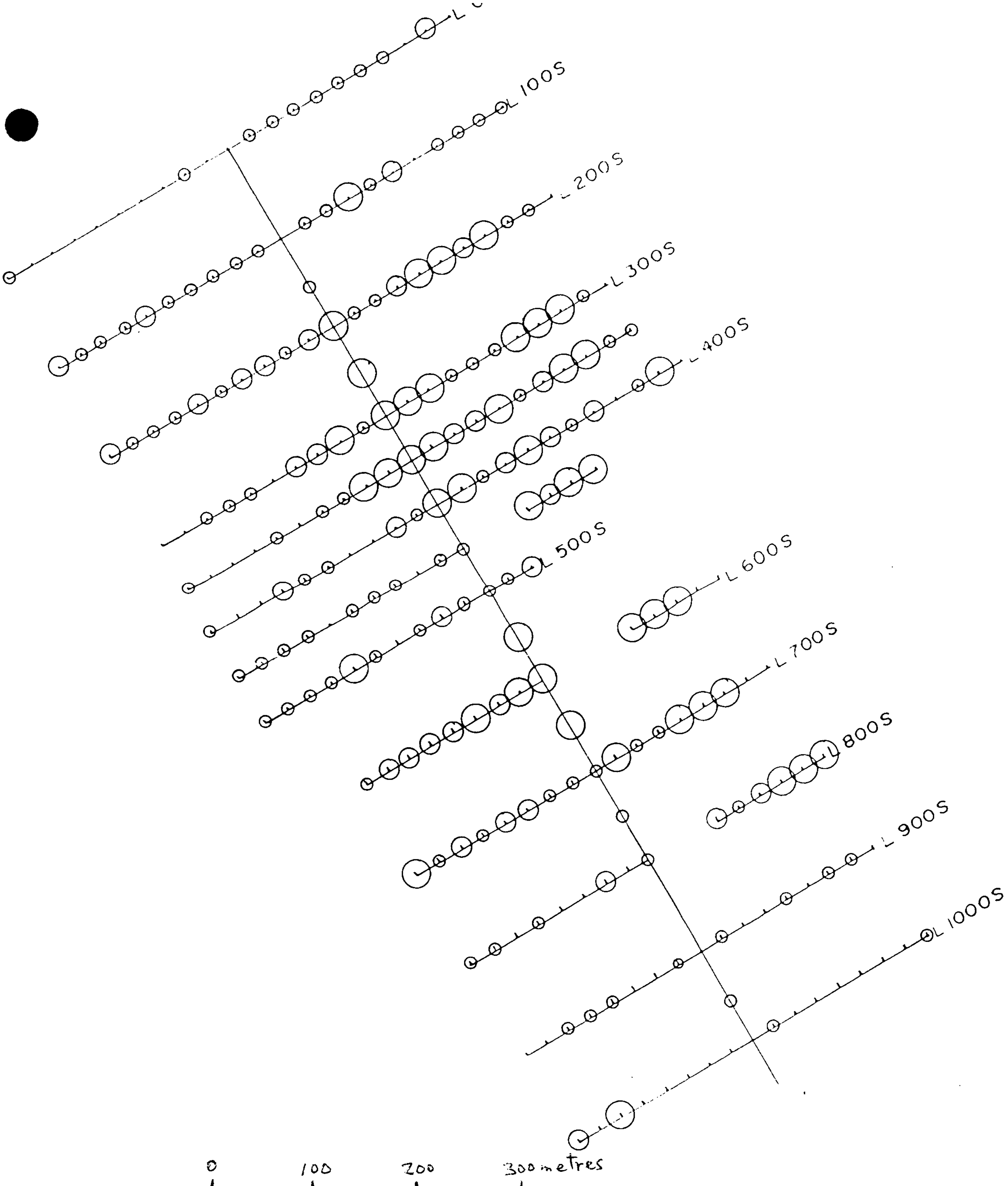


FIG. 6

WHITE CHANNEL RESOURCES INC. OCT. 1989

SILVER CROWN SHOWING STRIKE 2 CLAIM - STEWART, B.C.

SOIL GEOCHEM Zn

SCALE 1:5000

○ 300-499 ppm Zn
○ 500-699 ppm Zn
○ ≥700 ppm Zn

N

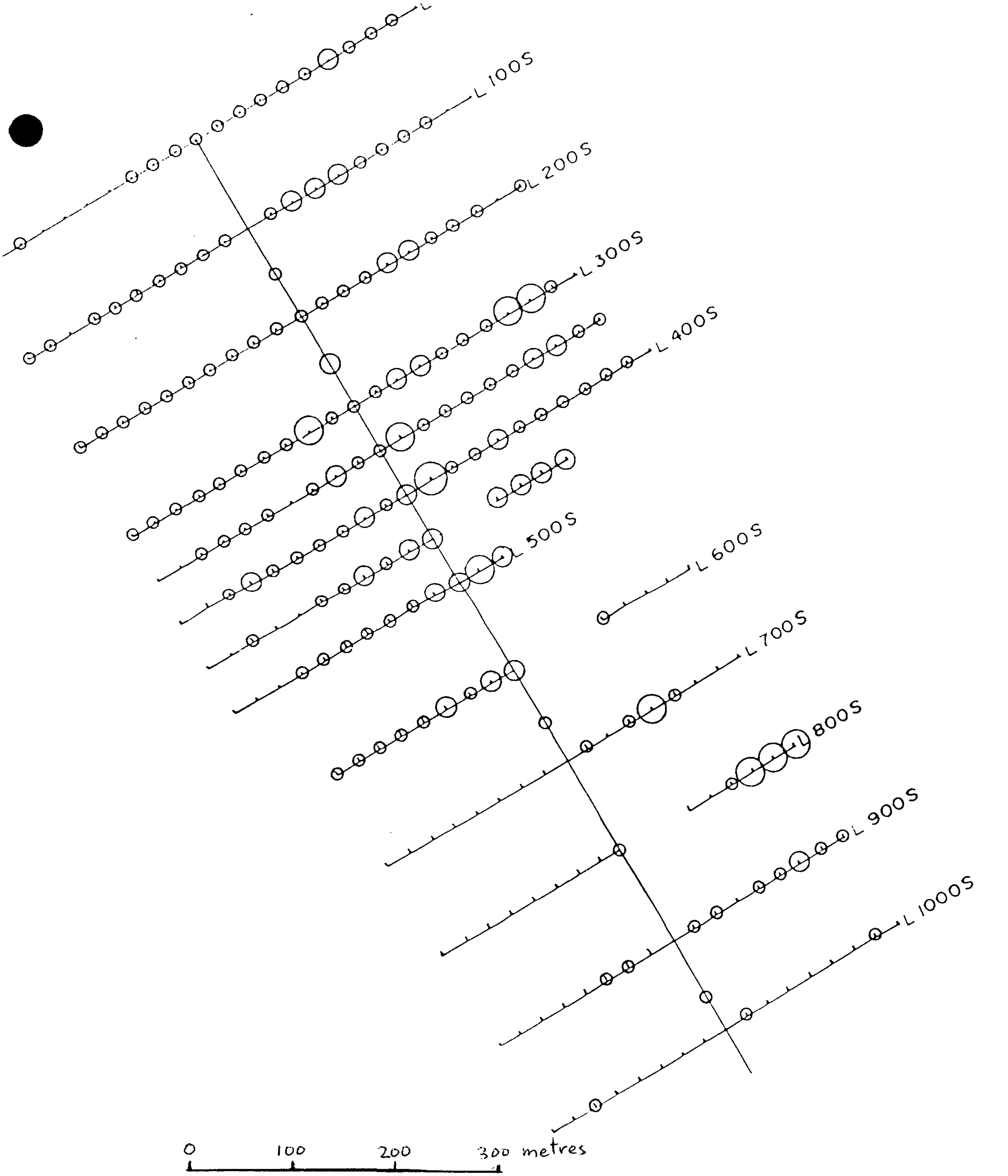


FIG. 7

WHITE CHANNEL RESOURCES INC. OCT. 1989

SILVER CROWN SHOWING STRIKE 2 CLAIM - STEWART, B.C.

SOIL GEOCHEM Ag

○ 2.0–3.9 ppm Ag
○ 4.0–6.0 ppm Ag
○ >6.0 ppm Ag

SCALE 1:5000

N

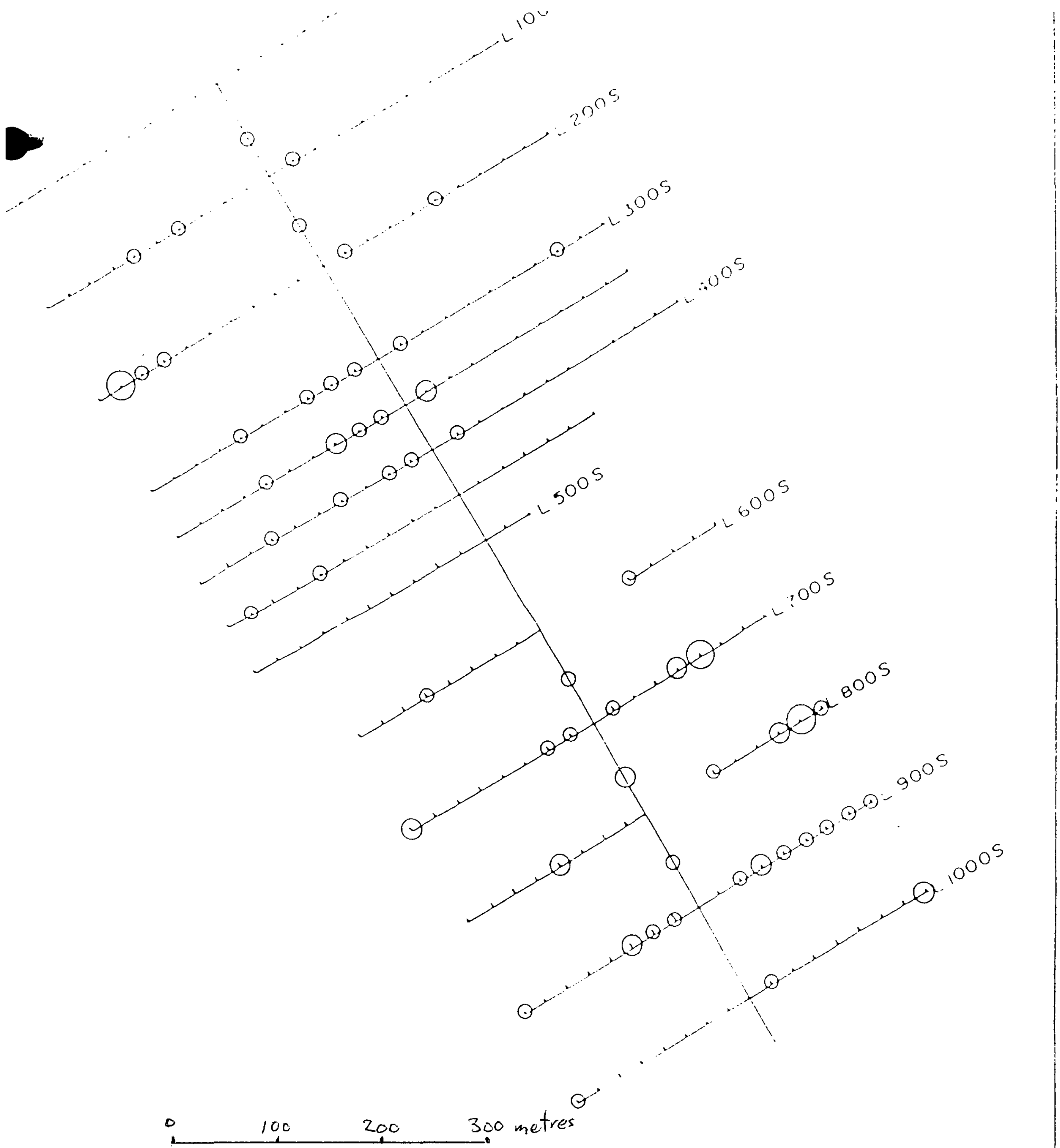


FIG. 8

WHITE CHANNEL RESOURCES INC OCT 1989

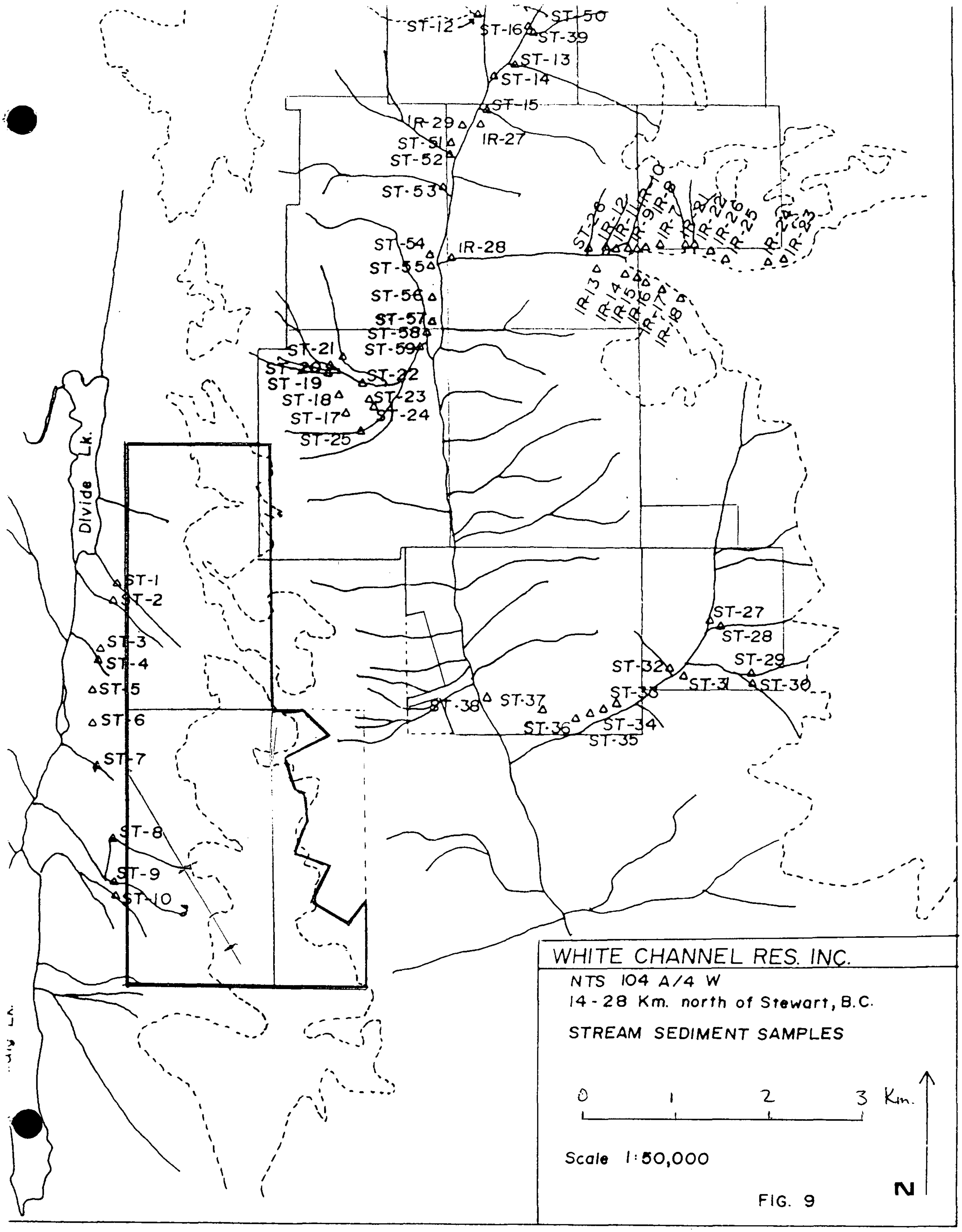
SILVER CROWN SHOWING STRIKE 2 CLAIM - STEWART, B C

SOIL GEOCHEM Au

○ 50-149 ppb Au
○ 150-500 ppb Au
○ >500 ppb Au

SCALE 1:5000

N



WHITE CHANNEL RES. INC.

NTS 104 A/4 W

14 - 28 Km. north of Stewart, B.C.

STREAM SEDIMENT SAMPLES

0 1 2 3 Km.

Scale 1:50,000

N

FIG. 9

APPENDIX A A1

1.0 INTRODUCTION

A geophysical program consisting of electromagnetic (VLF-EM) and magnetic surveys was carried over two showings on the Rich 1 - 4, Lode 1 - 4, and Strike 1 - 3 claims located near Stewart, B.C. in the Skeena Mining Division, B.C. The survey was carried out in October, 1989.

2.0 OBJECTIVES

- to establish a correlation between magnetic minerals and mineralized trends,
- to test the effectiveness of VLF-EM in following possible mineralized trends and to establish new unrecognized conductive trends,
- to establish geophysical areas of interest for future exploration.

3.0 SURVEY SPECIFICATIONS

Survey Parameters

- survey line separation - variable 50 m. to 100 m.
- survey station spacing - 12.5 m.
- VLF-EM and magnetic survey total 7.6 km.

Equipment Parameters

- VLF-EM and Magnetic Surveys
- Scintrex Omni Plus combined VLF-EM and magnetometer
- Dip Angle (in-phase) and Quadrature (out-of-phase) measured in percent at each station
- VLF-EM Field Strength measured at each station
- transmitting stations used - NPM (23.4 kHz) - Lualualei, Hi.
- NLK (24.8 kHz) - Seattle, Wa.
- earth's total magnetic field measured in gammas (nT)
- magnetic variations controlled by automatic magnetic base station recording every 30 seconds
- instrument accuracy +/- 0.1 nT.

Equipment Specifications - see Appendix I

4.0 DATA

Calculations

Total Field Magnetic Survey

Total field magnetic readings were individually corrected for variations in the earth's magnetic field using magnetic base station values. The formula used for magnetic corrections was;

$$CTFR = TFR + (DBL - BSR)$$

where: CTFR = Corrected Total Field Reading
TFR = Total Field Reading
DBL = Datum Base Level = 58400 gammas
BSR = Base Station Reading

Presentation

Silver Crown Survey Area

- Lualualei VLF-EM in-phase, out-of-phase and field strength readings are presented in profile form on Figure # G-1 at a scale of 1:2500
- Lualualei in-phase readings were Fraser filtered and are presented in contour form on Figure # G-2 at a scale of 1:2500
- Magnetic data were profiled and are presented on Figure # G-3 at a scale of 1:2500
- Magnetic data were contoured and are presented on Figure # G-4 at a scale of 1:2500
- The geophysical interpretation is presented on Figure # G-5 at a scale of 1:2500

5.0 INTERPRETATION

5.1 Silver Crown Showing

Discussion of Results

Total field magnetic data over the Silver Crown showing were noise free and no cultural sources were observed. Magnetic readings range from 57250 nT. to 57850 nT. within a stable background of approximately 57470 nT. The magnetic datum value for the total field magnetic profile map, Figure # G-3, was determined by statistical analysis to be 57470 nT. This datum value, which graphically shows if a magnetic reading is above or below the mean value for the grid, was also the threshold between dashed and solid contours on the total field magnetic contour map, Figure # G-4.

The magnetic environment was quiet over much of the Silver Crown showing. To obtain as much detail as possible the magnetic data have been processed at a 10 nT. contour interval. A number of magnetic lineaments were observed in present survey results. These lineaments were labeled "L1" to "L5" on Figure # G-4.

Magnetic lineament "L1" is the only magnetic low feature observed over the Silver Crown showing. "L1" trends northwest and exhibits weak lows

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approximately 50 nT. to 300 nT. below background. "L1" displays variable wavelengths ranging from 25 m. to 75 m.

Four weak magnetic high features were delineated over the survey area. All of these high features exhibit similar characteristics with wavelengths of 25 m. and magnitudes of approximately 100 nT. Lineaments "L2" and "L3" trend east-west and lineaments "L4" and "L5" trend north-south.

VLF-EM response over the Silver Crown showing was noise free and no cultural sources were observed. Although the direction to the transmitter was not optimum for conductor coupling, NPM, Lualualei VLF-EM data were chosen as the primary interpretation frequency because they constituted the only complete data set over the survey area.

Within the survey area, VLF-EM data display a response to major topographic features. The topographic signature characteristically exhibits long wavelength, large amplitude in-phase and quadrature responses as well as a broad field strength anomaly.

Three VLF-EM conductors were interpreted on the Silver Crown showing and were labeled "C1" to "C5" on Figures "G-1" and "G-2". Many conductors seen here tend to display short strike lengths, also numerous single line anomalies were observed in the area. Conductor "C1" trends northwest with a strike length of 100 m. and displays moderate response.

Conductor "C2" is a relatively long feature trending north and exhibiting short wavelengths with moderate in-phase and field strength response. Quadrature response for "C2" is unusually strong.

Conductor "C3" trends north-northwest displaying moderate response and relatively long wavelengths.

Conductor "C4" is a short feature trending in the same direction as "C2" and exhibiting weak response.

"C5" is a relatively long conductor also trending in the same direction as "C2" and exhibiting variable, weak to strong response.

Conclusions

The quiet magnetic environment over the Silver Crown showing indicates that there is little variation of magnetic susceptibilities in the survey area. The lack of variation in magnetic susceptibilities suggests that the Silver Crown showing is underlain by a homogeneous rock type or by rock types with similar magnetic suscepibilities. The quiet magnetic background allowed the delineation of weak magnetic features "L1" to "L5". From line 300N to line 450N on the western edge of the survey area, a high feature is observed but due to lack of continuation over this feature it is impossible to define the high as a lineament or a different magnetic unit.

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Magnetic lineament "L1" is interpreted to represent a fault and the lower magnetic field strength attributed to oxidization within the fault zone.

Magnetic high features observed over the survey area are believed to represent narrow, weakly magnetic dykes. Supporting this interpretation, the monopolar response displayed by all high features suggests that the magnetic sources have good depth extent and are not near surface occurrences of magnetite. "L2" and "L3" appear to be part of a single feature that was intersected and offset by "L1" which, would support the interpretation of "L1" as a fault.

VLF-EM results over the Silver Crown survey area show several conductors however there appears to be no correlation between magnetic features and VLF-EM conductivity. Conductor "C1" exhibits VLF-EM response indicative of a conductive structural feature, however the short strike length of this feature suggests that if "C1" is a structural feature, then it must be terminated north of line 700N by a cross-cutting structure. A change in magnetic profile character between line 700N and 800N suggests that a cross-cutting fault may be present, but a larger survey on lines perpendicular to the present orientation would be required to define this inferred feature.

Conductor "C2" is the strongest conductor discovered in the survey area. The strong quadrature response suggests that "C2" represents a highly conductive body, possibly massive sulphides or a very conductive structural feature. A stronger in-phase response is expected with such a strong quadrature response, however the conductive body may be so narrow that a smaller station spacing would be required to measure the in-phase response. "C2" stops abruptly at line 300N and may be terminated by lineament "L1".

"C3" is a moderate conductor exhibiting VLF-EM response similar to "C1" and also trending approximately in the same direction as "C1". "C3" is believed to be related to "C1" and is also thought to represent a structural feature such as a fault.

Conductor "C4" trends in the same direction as "C2" but exhibits weaker VLF-EM response and longer wavelengths than "C2". "C4" is interpreted to represent a minor structural feature such as a fracture or a narrow shear zone.

Conductor "C5" is thought to be related to "C2" and "C4" since these conductors all trend in the same direction. "C5" is interpreted to be a structural feature with the stronger anomalies within "C5" representing fault dilation, possibly containing sulphide mineralization.

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6.0 RECOMMENDATIONS

The VLF-EM and magnetic interpretation has delineated magnetic and conductive trends on the Silver Crown and Moonlight Glacier survey areas that warrant follow-up exploration. Surface geological investigations are recommended to determine the importance of the following targets discussed in order of priority.

Conductor "C2" on the Silver Crown survey area is considered to be a primary exploration target based on the strength of the VLF-EM anomalies. Detailed investigation is recommended for the following targets along "C2":

- 120W, Line 350S
- 130W, Line 400S
- 90W, Line 300S

A larger VLF-EM and magnetic survey is recommended to determine the extent of the conductors discussed above and to delineate magnetic features dicovered in the present survey.

A horizontal loop electromagnetic survey is recommended to more accurately define the location of strong VLF-EM conductors if fault controlled mineralization is suspected. If disseminated mineralization is believed to be present, an induced polarization/resistivity survey is recommended to determine chargeable and resistive zones. A deep electromagnetic survey, such as UTEM, is recommended to determine the depth extent of conductive bodies discovered in the present survey.

CERTIFICATE

I, Thomas Raymond Matich, Geophysicist of Surrey, British Columbia, Canada, hereby certify that:

1. I received a B.Sc. degree in Geophysics from the University of British Columbia in 1982.

2. I currently reside at 13914 116 Ave, in the Municpality of Surrey, in the Province of British Columbia.

3. I have been practising my profession since graduation.

4. I hold no direct or indirect interest in, nor expect to receive any benefits from, the mineral property or properties described in this report.

5. This report may be used for the development of the property, provided that no portion will be used out of context in such a manner as to convey meanings different from that set out in the whole.

6. Consent is hereby given to the company for which this report was prepared to reproduce the report or any part of it for the purposes of development of the property, or facts relating to the raising of funds by way of a prospectus and/or statement of material facts.

Date: Oct 19, 1989

Surrey,
British Columbia

Signed: Tom Matich

Thomas Raymond Matich
B.Sc.

Appendix B B7

WHITE CHANNEL RESOURCES INC.

Silver Crown
(Strike Claims)

Sample Record

Sample Number	Showing Name	Survey Location	Width (Metres)	Description	Au g/t	Ag g/t	Cu %	Pb %	Zn %
47001	Baseline Vein	5+07S 1+27W	.75 m	30% qtz 2% ga. sp. vein swell in arg. slt.	.51	13.7	.01	.97	2.45
47002	"	BL 4+60S	1.20 m	40% qtz vuggy 2% ga tr. cp py	1.00	.1	.02	.26	.02
47003	"	BL 4+46S	1.15 m	40% qtz vuggy 2% ga tr. cp py	.01	25.4	.06	3.68	.02
47004	"	4+62S 0+65E	.65 m	25% qtz 15% py felsic dyke contact	.49	22.3	.30	.09	.03
47005	"	4+40S 0+62E	.65 m	30% qtz 5% sp. ga. cp felsic dyke contact	.03	10.1	.03	.16	21.60
47006	"	3+60S 0+30E	1.20 m	20% qtz 15% py 3% cp sp felsic dyke contact	1.11	33.2	.13	1.87	.57
47007	"	" "	1.80 m	30% qtz 3% ankerite tr. sp hanging wall bx	.63	12.1	.08	2.89	.57
47008	"	3+52S 0+38E	1.10 m	25% qtz 10% sp 1% ga tr. cp 5% py	1.04	29.5	.12	7.20	4.24
47009	"	" "	1.10 m	" " " " " " " " " "	3.55	63.5	.05	11.40	5.22
47010	"	3+47S 0+43E	1.55 m	25% qtz 10% ga 2% sp tr. cp	1.72	57.8	.01	16.50	.09
47011	"	3+42S 0+46E	.82 m	25% qtz 5% py 1% sp ga	.46	23.7	.02	2.45	.42
47012	"	3+40S 0+50E	1.20 m	" " " " " " "	.03	2.5	.01	.11	.04
47013	"	3+25S 0+55E	.40 m	25% qtz 10% ga 3% py tr. cp	.28	123.5	.01	12.90	.18
47014	"	3+06S 0+68E	.80 m	25% py 20% qtz 4% sp ga (stringer zone hanging wall)	.03	13.0	.01	3.67	.16
47015	"	3+10S 0+50E	.30 m	" " " " tr: sp ga	.03	2.0	.03	.17	.09
47016	"	2+70S 0+65E	.50 m	30% qtz 3% ga 1% sp pod stringers	.03	58.7	.02	12.20	14.60
47017	"	2+74S 0+62E	.30 m	" " " " " " " "	.95	41.3	.09	10.40	2.30

Silver Crown
(Strike Claims)

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WHITE CHANNEL RESOURCES INC.

Sample Record

Sample Number	Showing Name	Survey Location	Width (Metres)	Description	Au g/t	Ag g/t	Cu %	Pb %	Zn %
47018	Knob Vn	3+75S 2+12E	1.75 m	25% qtz 3% ga 2% py tr cp stringers	.37	1.2	.01	.24	.12
47019	"	3+71S 2+13E	1.60 m	" " " " " " " " "	.03	2.4	.01	.60	1.95
47020	"	3+63S 2+15E	1.00 m	" " " " " " " " "	.05	7.9	.02	.39	4.08
47021	"	3+63S 2+15E	1.20 m	25% qtz 3-5% ga 2% py tr. cp "Knob Vein"	.16	27.3	.05	4.95	2.52
47022	"	3+58S 2+17E	1.00 m	" " " " " " " " " "	.15	27.9	.01	4.83	1.73
47023	"	3+58S 2+17E	1.00 m	" " " " " " " " " "	.38	120.5	.01	11.20	.49
47024	"	3+55S 2+20E	1.70 m	" " " " " " " " " "	.43	10.8	.01	2.58	.01
47025	"	3+53S 2+22E	1.60 m	" " " " " " " " " "	.34	4.6	.01	.50	.20
47026	"	3+38S 2+20E	1.70 m	" " " " " " " " " "	.15	25.4	.01	.59	.13
47027	"	3+86S 1+70E	1.80 m.	" " " " " " " " " "	.37	26.8	.01	4.06	3.45
47028	Baseline Vn	7+25S 1+12W	.50 m	40% qtz. 3% py. sp cp ga	.30	42.3	.26	3.60	.01
47029	"	7+58S 1+24W	1.30 m	" " " " " "	.13	28.9	.29	1.68	.02
47030	"	7+74S 1+30W	1.60 m	" " " " " "	.03	8.7	.15	.16	.01
47031	"	7+90S 0+51W	.35 m	" " " " " "	.03	23.7	.16	1.98	.67
47032	"	8+00S 0+45W	.45 m	" " " " " "	.60	389.5	.01	4.16	.01
47033	"	9+10S 0+50W	.60 m	" " " " " "	.24	53.5	.15	9.10	.01
47058	"	5+21S 0+11W	.80 m	30% Qtz 8% py 1% sp. ga in arg	.22	17.5	.04	.04	.01

Silver Crown
(Strike Claims)

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WHITE CHANNEL RESOURCES INC.

Sample Record

Sample Number	Showing Name	Survey Location	Width (Metres)	Description	Au g/t	Ag g/t	Cu %	Pb %	Zn %
47059	Baseline	5+20S 0+13W	.75 m	30% qtz 8% py 1% sp ga in arg	.27	9.6	.04	.24	1.53
47060	"	5+20S 0+11W	.75 m	" " " " " " " " "	.12	3.6	.01	.07	.02
61	"	5+13S 0+03W	.75 m	30% qtz 3% py 1% sp ga in arg	.07	1.7	.01	.04	.01
62	"	5+12S 0+05W	.70 m	" " " " " " " " "	3.02	29.8	.01	6.63	.36
63	"	4+80S 0+01W	1.10 m	35%qtz 3% ga 3% py 1% sp tr. cp.	.83	17.2	.01	3.28	.08
64	"	4+78S 0+00W	.70 m	" " " " "	.20	39.6	.08	3.57	.56
65	"	4+73S 0+00W	.90 m	" " " " "	.50	94.3	.06	16.70	1.10
66	"	4+72S 0+01W	1.00 m	25% qtz 3% ga 1% sp 1% cp in f. dyke	.14	31.5	.13	4.20	.01
67	"	4+72S 0+02W	1.00 m	" " " " "	.28	97.6	.36	4.85	.02
68	"		.80 m	" " " " "	.16	15.1	.22	1.13	.77
69	"	4+58S 0+00W	.90 m	" " " " "	.13	52.8	.18	10.40	.09
70	"	4+49S 0+00W	.70 m	" " " " "	.31	64.3	.25	7.93	.06
71	"	4+08S 0+00W	.30 m	35% qtz 10% ga 3% sp in felsic dyke	.63	262.8	.04	13.30	.01
72	"	3+55S 0+36E	.90 m	30% qtz 8% ga 3% sp tr. cp in f. dyke	.60	68.6	.02	16.50	.02
73	"	3+55S 0+35E	1.00 m	" " " " " "	1.07	43.8	.01	11.40	.18
74	"	3+50S 0+38E	1.00 m	" " " " " "	1.84	79.5	.05	14.60	.26
75	"	3+50S 0+37E	1.10 m	" " " " " "	2.78	80.8	.03	4.13	1.13
76	"	3+48S 0+38E	1.10 m	" " " " " "	1.42	213.5	.01	12.70	.03
77	"	3+45S 0+41E	1.10	" " " " " "	.40	27.3	.01	4.68	.04

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WHITE CHANNEL RESOURCES INC.

Sample Record

Sample Number	Showing Name	Survey Location	Width (Metres)	Description	Au g/t	Ag g/t	Cu %	Pb %	Zn %
47078	Baseline	3+40S 0+44E	1.20 m	30% qtz 8% ga 3% sp tr. cp inf. dyke	.19	4.7	.01	.26	.03
47079	"	2+82S 0+60E	.50 m	25% qtz 6% ga 5% sp in arg slt.	.36	57.8	.02	9.61	9.23
47080	Knob vein	1+39E 4+03S	.30 m	30% qtz 5% ga 1% sp in felsic dyke	1.23	28.5	.14	4.59	1.25
81	"	4+04S 1+39E	.40 m	" " " "	2.65	103.8	.01	7.26	12.40
82	"	4+07S 1+40E	.60 m	" " " "	.59	21.2	.06	4.29	2.56
83	"	4+14S 1+42E	.40 m	" " " "	.40	19.5	.03	3.82	.62
84	"	4+17S 1+43E	.40 m	" " " " in arg. slt.	.31	15.2	.08	2.16	9.34
85	"	4+27S 1+43E	1.00 m	" " " " "	.50	12.8	.06	1.09	.06
86	"	4+24S 1+42E	.50 m	" " " " "	.46	9.9	.08	.82	.19
87	"	3+58S 1+75E	1.35 m	25% qtz 2% ga tr. sp in arg slt.	.12	3.0	.01	.20	.17
88	"	3+60S 1+75E	.80 m	" " " "	.08	1.8	.01	.11	.02
89	"	3+60S 1+68E	.40 m	" " " "	.35	324.3	.01	13.70	.03
90	"	3+48S 1+20E	.50 m	" " " "	.22	4.4	.01	.96	3.59
91	"	3+51S 1+20E	.50 m	" " " "	.05	0.6	.01	.15	.13
47101	BaselineVn	7+26S 1+25W	.90 m	30% qtz 3% ga tr. sp in felsic dyke	.10	33.3	.21	.08	.02
102	" "	7+27S 1+26W	.90 m	" " " " "	.13	18.4	.12	.05	.01
103	" "	7+28S 1+25W	.85 m	" " " " "	.20	22.4	.18	.04	.02

Silver Crown
(Strike Claims)

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WHITE CHANNEL RESOURCES INC.

Sample Record

Sample Number	Showing Name	Survey Location	Width (Metres)	Description	Au g/t	Ag g/t	Cu %	Pb %	Zn %
47104	Baseline	7+43S 1+30W	.75 m	30% qtz 3% ga tr. sp in felsic dyke	.07	33.0	.33	1.64	.02
105	"	7+45S 1+30W	.85 m	" " " " "	.11	13.6	.15	.32	.03
106	"	7+46S 1+30W	.75 m	" " " " "	.70	33.8	.15	3.18	.11
47092	"	0+25S 1+80E	1.00 m	30% qtz 3% ga 1% sp in arg. slt.	4.04	78.5	1.12	12.20	9.30
93	"	4+06S 0+05W	.65 m	" " " "	.61	61.8	.29	6.96	.02
94	"	5+92S 0+62W	.60 m	" " " "	.28	86.3	.07	11.80	1.35
95	"	5+95S 0+63W	.70 m	" " " "	1.50	203.6	.04	1.27	.08
96	"	6+00S 0+63W	.40 m	" " " "	22.42	447.3	.01	1.50	.96
97	"	6+01S 0+63W	.40 m	" " " "	.30	12.0	.01	2.03	5.36
98	"	6+07S 0+64W	.35 m	" " " "	.83	223.8	.04	13.50	10.06
99	"	6+08S 0+64W	.45 m	" " " "	1.10	84.4	.03	8.90	10.25
100	"	6+12S 0+64W	1.20 m	" " " "	.63	58.3	.62	6.28	.11
47107	BaselineVn	7+47S 1+30W	.80 m	30% qtz 3% ga tr. sp in fel. dyke	.13	16.9	.16	.61	.02
108	"	7+75S 0+48W	.60 m	" " " " " "	.24	17.7	.02	.33	.09
109	"	7+76S 0+48W	.50 m	" " " " " "	.49	6.7	.07	.37	.44
110	"	7+74S 0+27W	.70 m	" " " " " "	.16	127.7	1.59	1.71	.55

Silver Crown
(Strike Claims)

B12
WHITE CHANNEL RESOURCES INC.

Sample Record

Sample Number	Showing Name	Survey Location	Width (Metres)	Description	Au g/t	Ag g/t	Cu %	Pb %	Zn %
47111	Baseline	7+75S 0+27W	.60 m	30% qtz 3% ga tr. sp in fel dyke	.47	33.8	.09	4.93	.26
112	"	7+76S 0+27W	.60 m	" " " "	.80	75.6	.50	28.5	1.43
113	"	7+77S 0+27W	.65 m	" " " "	.28	93.3	.59	3.86	.53
114	"	7+78S 0+27W	.60 m	" " " "	.16	72.5	.18	11.20	.68
115	"	7+92S 0+42W	.60 m	" " " "	.35	28.7	.04	1.03	.10
116	"	7+93S 0+42W	.65 m	" " " "	1.14	83.5	.11	3.43	.08
117	"	7+94S 0+42W	.55 m	" " " "	.89	37.9	.04	.65	.12
118	"	7+96S 0+34W	.50 m	" " " "	3.54	156.0	.03	15.90	.66
119	"	7+97S 0+34W	.60 m	" " " "	.32	19.8	.02	.41	.03
120	"	7+93S 0+39W	.55 m	" " " "	5.35	174.8	.02	4.53	.16
121	"	7+94S 0+39W	.70 m	" " " "	.90	57.9	.04	1.11	.08
122	"	7+95S 0+39W	.70 m	" " " "	.81	98.3	.25	1.04	.03
123	"	7+96S 0+39W	.60 m	" " " "	1.14	58.7	.04	3.79	.06
124	"	7+97S 0+39W	.60 m	" " " "	.63	54.5	.05	2.09	.04
125	"	7+98S 0+39W	.80 m	" " " "	.61	65.3	.02	6.77	.06
126	"	7+99S 0+39W	.60 m	" " " "	.34	293.0	.03	24.40	.36
127	"	8+00S 0+39W	.55 m	" " " "	.36	98.6	.02	10.80	.02

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

APPENDIX C GEOCHEMICAL ANALYSIS CERTIFICATE

C13

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P7 SOIL P8 SILT AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: SEP 20 1989 DATE REPORT MAILED: Sept 26/89 SIGNED BY. C. Leong ..D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

White Channel Resources Inc. PROJECT SILVER CROWN File # 89-3779 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L0+00S 2+50W	2	58	127	354	1.6	36	17	947	4.44	27	5	ND	3	17	3	2	2	32	.22	.078	19	15	.75	150	.02	11	1.86	.01	.13	1	15
L0+00S 2+25W	2	54	120	267	1.5	35	16	873	4.26	24	5	ND	3	8	2	2	2	30	.11	.072	17	14	.77	100	.01	6	1.70	.01	.11	1	13
L0+00S 2+00W	4	54	132	270	2.0	34	16	807	4.39	25	5	ND	3	10	1	2	2	31	.13	.078	18	15	.78	95	.02	3	1.71	.01	.11	1	5
L0+00S 1+75W	3	51	122	277	1.6	35	16	922	4.16	22	5	ND	2	14	2	2	2	30	.20	.081	19	15	.75	92	.02	3	1.54	.01	.08	1	8
L0+00S 1+50W	3	74	57	195	.9	39	24	1408	5.25	28	5	ND	4	23	1	2	2	51	.25	.103	19	14	.97	179	.07	12	2.06	.01	.10	1	1
L0+00S 1+25W	3	55	122	259	1.5	27	15	717	4.28	21	5	ND	3	10	1	2	2	30	.15	.084	19	12	.71	91	.02	5	1.61	.01	.11	1	16
L0+00S 1+00W	3	55	123	255	1.7	33	17	637	4.45	18	5	ND	3	11	1	2	2	31	.17	.096	15	14	.76	95	.02	10	1.74	.01	.11	1	11
L0+00S 0+75W	3	48	95	231	2.1	34	12	471	4.94	26	5	ND	3	5	1	3	2	29	.05	.067	16	16	.81	52	.01	3	1.62	.01	.08	1	11
L0+00S 0+50W	4	76	115	471	3.0	64	27	1411	5.41	26	5	ND	3	11	2	3	2	28	.15	.076	15	13	.65	55	.01	5	1.47	.01	.05	1	7
L0+00S 0+25W	3	62	121	260	2.9	36	25	1047	4.60	24	5	ND	3	10	2	2	2	25	.16	.077	12	12	.73	57	.03	4	1.42	.01	.06	1	3
L0+00S 0+25E	4	59	204	441	2.4	35	17	1076	4.35	21	5	ND	2	17	4	2	2	28	.28	.084	16	12	.75	164	.02	11	1.55	.01	.12	1	14
L0+00S 0+50E	5	54	146	330	2.1	27	15	1090	4.26	21	5	ND	3	14	3	2	2	29	.26	.099	19	9	.79	129	.03	10	1.57	.01	.10	1	2
L0+00S 0+75E	4	59	133	384	2.2	32	15	1159	4.35	25	5	ND	4	20	3	2	2	34	.36	.099	18	10	.83	171	.03	2	1.73	.01	.12	1	1
L0+00S 1+00E	5	59	175	331	2.1	27	16	1140	4.42	26	5	ND	3	17	4	2	2	32	.31	.104	20	8	.75	135	.03	13	1.56	.01	.10	1	2
L0+00S 1+25E	7	67	176	433	2.4	30	14	1052	4.44	30	5	ND	3	29	5	2	2	31	.35	.095	18	8	.75	100	.03	3	1.38	.01	.07	1	7
L0+00S 1+50E	3	64	237	460	4.1	35	13	1093	5.06	30	5	ND	2	26	7	2	2	30	.38	.104	15	6	.70	79	.03	2	1.28	.01	.05	1	11
L0+00S 1+75E	7	50	114	458	1.1	34	11	1095	4.15	20	5	ND	2	20	5	2	1	31	.34	.086	14	5	.80	55	.03	7	1.42	.01	.07	1	1
L0+00S 2+00E	3	41	103	255	1.1	21	11	1026	3.91	20	5	ND	2	13	3	2	2	29	.26	.067	14	5	.78	74	.03	2	1.34	.01	.05	1	3
L0+00S 2+25E	13	56	126	507	3.0	29	12	1025	4.30	27	5	ND	2	18	5	2	2	29	.32	.084	13	8	.85	88	.03	11	1.45	.01	.07	1	3
L0+00S 2+50E	7	41	78	252	1.3	25	13	1002	4.10	19	5	ND	3	14	2	3	2	32	.31	.090	15	7	.34	55	.03	5	1.52	.01	.05	1	1
L1+00S 2+50W	3	61	590	534	2.6	27	16	1058	4.30	27	5	ND	2	15	5	2	2	29	.25	.085	17	13	.71	130	.03	2	1.53	.01	.12	1	11
L1+00S 2+25W	5	53	237	341	2.1	34	17	1013	4.51	27	5	ND	1	19	5	2	3	30	.30	.078	14	13	.79	72	.03	4	1.37	.01	.03	1	1
L1+00S 2+00W	3	42	148	218	1.6	27	13	770	3.96	13	5	ND	2	17	3	2	2	25	.27	.086	15	12	.70	80	.04	2	1.33	.01	.06	1	18
L1+00S 1+75W	2	55	174	337	1.2	40	19	965	4.50	27	5	ND	3	16	2	2	2	34	.22	.081	17	16	.84	130	.03	11	1.79	.01	.12	1	1
L1+00S 1+50W	3	73	224	545	2.9	42	21	1110	4.67	24	5	ND	3	22	5	2	2	30	.27	.086	20	15	.75	154	.02	5	1.73	.01	.11	1	70
L1+00S 1+25W	2	81	204	451	3.6	45	24	1287	5.31	49	5	ND	4	19	5	2	2	28	.31	.093	18	13	.76	120	.01	10	1.59	.01	.09	1	33
L1+00S 1+00W	2	74	169	370	2.7	43	22	1149	4.73	31	5	ND	3	12	3	2	2	29	.18	.088	18	13	.76	82	.03	5	1.58	.01	.08	1	57
L1+00S 0+75W	2	72	170	417	2.5	44	20	990	4.46	23	5	ND	2	17	4	2	2	25	.25	.085	17	12	.73	69	.01	2	1.39	.01	.06	1	20
L1+00S 0+50W	2	64	180	428	2.5	50	21	2062	4.62	23	5	ND	3	23	4	2	2	28	.29	.090	20	13	.73	121	.01	5	1.59	.01	.08	1	14
L1+00S 0+25W	5	191	270	370	3.5	125	45	1536	5.57	31	5	ND	2	24	4	2	2	26	.24	.084	20	13	.74	77	.02	5	1.82	.01	.07	1	51
L1+00S 0+25E	3	58	329	392	3.5	33	24	985	5.16	26	5	ND	4	12	2	2	2	27	.17	.091	16	12	.67	61	.03	2	1.45	.02	.08	1	24
L1+00S 0+50E	5	64	320	394	5.0	26	9	433	5.40	16	5	ND	2	3	1	3	2	24	.03	.074	14	14	.68	53	.02	2	1.45	.01	.05	1	33
L1+00S 0+75E	4	57	572	728	4.3	46	27	1288	4.57	35	5	ND	3	11	8	2	2	24	.19	.082	14	10	.62	116	.01	2	1.43	.01	.10	1	33
L1+00S 1+00E	7	84	385	337	4.4	24	13	628	5.17	23	5	ND	2	6	1	2	2	27	.06	.078	14	13	.63	105	.01	5	1.38	.01	.05	1	45
L1+00S 1+25E	7	67	229	542	3.1	39	15	1488	4.84	26	5	ND	3	17	6	2	2	29	.29	.095	18	9	.78	181	.02	2	1.66	.01	.12	1	45
L1+00S 1+50E	5	45	134	356	2.0	22	14	1325	4.37	20	5	ND	2	20	4	2	2	33	.40	.106	19	5	.80	179	.03	3	1.72	.01	.13	1	5
STD C/AU-S	18	62	39	132	6.6	67	31	961	4.01	41	21	7	38	48	18	15	22	58	.49	.089	39	56	.88	177	.07	34	1.97	.06	.14	13	45

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L1+00S 1+75E	6	54	128	308	2.2	26	16	1175	4.13	15	5	ND	2	20	3	2	2	34	.40	.106	19	9	.75	128	.02	6	1.58	.01	.09	2	13
L1+00S 2+00E	8	81	217	451	2.2	34	17	1229	4.39	20	5	ND	2	21	4	2	2	25	.36	.107	20	7	.76	117	.03	2	1.60	.01	.10	2	17
L1+00S 2+25E	6	44	105	384	1.5	18	13	1260	4.35	16	5	ND	2	50	3	2	2	37	1.00	.114	20	7	.85	254	.02	2	1.75	.01	.14	2	8
L1+00S 2+50E	7	50	150	445	1.9	24	12	1585	4.25	24	5	ND	2	23	6	2	2	37	.45	.112	18	8	.77	135	.05	3	1.37	.01	.07	2	21
L2+00S 2+50W	4	63	259	662	2.9	30	18	1240	4.65	27	5	ND	3	22	8	2	2	27	.35	.095	21	13	.73	151	.02	8	1.53	.01	.14	2	32
L2+00S 2+25W	5	53	205	433	2.1	23	13	1048	4.23	22	5	ND	2	18	6	2	2	27	.29	.086	15	13	.73	77	.02	4	1.38	.01	.09	1	560
L2+00S 2+00W	4	48	207	375	2.1	23	12	1034	3.95	17	5	ND	2	17	5	2	2	26	.27	.084	15	11	.68	67	.03	2	1.28	.01	.05	2	85
L2+00S 1+75W	5	52	244	428	2.4	21	13	1157	4.30	21	5	ND	3	17	5	2	2	27	.26	.075	15	13	.73	80	.02	5	1.37	.01	.06	2	57
L2+00S 1+50W	2	49	341	533	2.1	15	12	1025	3.98	13	5	ND	3	19	6	2	4	27	.35	.097	21	11	.64	156	.02	8	1.58	.01	.13	2	32
L2+00S 1+25W	5	64	337	373	3.4	25	13	1171	4.67	30	5	ND	2	12	5	2	2	26	.21	.090	14	13	.73	63	.02	2	1.38	.01	.06	1	32
L2+00S 1+00W	7	75	1218	674	3.9	31	17	1497	4.99	47	5	ND	2	14	5	2	2	34	.22	.081	17	16	.85	127	.03	2	1.72	.01	.11	1	28
L2+00S 0+75W	6	64	261	695	2.7	62	22	1556	4.90	27	5	ND	2	22	10	2	2	33	.29	.083	17	15	.81	115	.03	2	1.63	.01	.08	2	35
L2+00S 0+50W	3	72	278	398	2.8	41	19	947	4.97	17	5	ND	2	17	2	6	2	32	.19	.080	18	16	.81	104	.03	10	1.81	.01	.10	2	29
L2+00S 0+25W	2	65	268	602	3.5	30	18	1104	4.46	14	6	ND	2	33	6	2	2	28	.36	.096	21	10	.66	153	.02	4	1.57	.01	.11	1	61
L2+00S 0+25E	2	50	178	444	2.9	47	28	1337	4.70	14	5	ND	3	11	4	2	2	28	.20	.092	20	12	.70	120	.01	5	1.75	.01	.05	1	24
L2+00S 0+50E	3	75	329	497	3.2	43	26	1310	4.56	16	5	ND	3	11	3	5	2	28	.22	.100	20	10	.61	33	.01	22	1.60	.01	.05	2	21
L2+00S 0+75E	3	45	355	554	3.0	22	13	1112	3.78	12	5	ND	4	12	6	2	2	23	.30	.105	15	8	.53	118	.01	2	1.13	.01	.07	1	47
L2+00S 1+00E	6	152	735	875	4.8	37	23	1670	5.44	25	5	ND	2	16	11	2	2	22	.25	.101	17	9	.54	157	.01	2	1.35	.01	.11	2	35
L2+00S 1+25E	6	125	845	1455	4.6	49	25	1820	5.57	36	5	ND	2	27	16	4	2	24	.30	.102	15	11	.64	125	.01	2	1.53	.01	.11	2	57
L2+00S 1+50E	6	62	392	667	3.9	23	13	1027	4.70	26	6	ND	3	20	8	2	2	24	.35	.098	13	9	.60	135	.01	2	1.22	.01	.08	2	46
L2+00S 2+00E	7	95	213	781	2.6	44	28	1439	4.24	15	5	ND	3	18	10	2	2	27	.34	.097	17	8	.73	163	.02	2	1.67	.01	.09	2	10
L2+00S 2+25E	7	44	75	351	1.9	23	14	1310	4.37	22	5	ND	3	36	3	5	2	29	.69	.108	23	6	1.10	249	.03	7	2.12	.02	.15	2	11
L2+00S 2+50E	6	50	106	372	2.5	28	14	1556	4.57	22	7	ND	3	22	4	5	2	33	.47	.119	18	8	.61	125	.03	2	1.52	.01	.05	2	15
L3+00S 2+50W	3	57	286	241	2.1	21	13	798	4.52	17	5	ND	2	8	1	2	2	29	.11	.074	15	15	.77	64	.02	3	1.52	.01	.08	2	18
L3+00S 2+25W	6	53	340	256	3.1	24	15	937	5.79	25	5	ND	2	7	1	2	4	27	.10	.078	11	15	.74	48	.02	2	1.44	.01	.07	2	43
L3+00S 2+00W	7	109	254	302	2.9	31	23	1034	5.86	32	5	ND	1	3	2	2	2	27	.13	.077	11	15	.75	53	.02	16	1.47	.01	.07	2	46
L3+00S 1+75W	6	69	303	342	2.4	29	22	2111	5.55	30	5	ND	2	9	2	2	2	30	.12	.093	23	15	.77	103	.02	2	1.72	.01	.05	2	41
L3+00S 1+50W	6	115	394	312	3.4	29	22	1415	5.55	43	5	ND	3	8	2	2	2	25	.10	.089	16	13	.66	80	.01	13	1.30	.01	.08	2	63
L3+00S 1+25W	5	76	202	258	3.1	16	10	612	4.57	31	5	ND	2	6	1	3	2	25	.06	.076	18	14	.66	55	.02	2	1.15	.01	.08	2	34
L3+00S 1+00W	6	114	624	667	3.6	33	18	923	4.97	39	5	ND	2	13	6	3	2	27	.21	.076	11	16	.75	68	.02	7	1.48	.01	.10	2	34
L3+00S 0+75W	14	57	379	637	2.9	35	19	1668	5.40	37	5	ND	2	15	8	2	2	28	.20	.084	15	12	.75	111	.02	18	1.58	.01	.08	2	53
L3+00S 0+50W	25	203	1444	1003	6.9	31	18	1571	5.55	55	5	ND	3	20	13	6	2	24	.29	.088	14	5	.62	105	.01	2	1.24	.01	.07	2	73
L3+00S 0+25W	6	61	553	362	3.6	17	15	1029	4.48	20	5	ND	4	13	2	2	2	22	.25	.096	18	5	.60	101	.02	3	1.27	.01	.08	2	60
L3+00S 0+25E	5	125	766	761	5.6	43	38	1682	4.87	21	6	ND	3	11	5	2	2	21	.21	.088	15	9	.54	74	.01	3	1.47	.01	.08	2	126
L3+00S 0+50E	7	148	702	1384	4.2	118	52	2857	5.62	21	5	ND	2	13	19	5	2	24	.23	.084	15	12	.57	135	.01	2	1.70	.01	.08	4	35
L3+00S 0+75E	1	43	136	321	2.8	11	15	1036	4.02	15	5	ND	4	27	3	2	2	27	.13	.096	26	5	.55	220	.01	2	1.62	.01	.13	2	30
STD C/AU-S	18	57	38	132	6.7	68	31	942	3.95	39	21	7	37	47	18	15	15	57	.48	.088	38	58	.88	175	.07	33	1.95	.06	.13	13	45

C15 White Channel Resources Inc. PROJECT SILVER CROWN FILE # 89-3779

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
13+00S 1+00E	2	58	174	474	2.2	35	20	1376	3.93	14	5	ND	3	15	6	2	3	35	.23	.100	24	5	.65	124	.01	2	1.42	.01	.07	1	18
13+00S 1+50E	5	117	502	866	3.0	42	25	3251	4.43	13	5	ND	3	11	14	3	2	23	.28	.124	18	7	.58	80	.01	4	1.48	.01	.06	1	21
13+00S 1+75E	10	173	583	707	6.4	41	37	2118	6.11	26	5	ND	3	10	5	6	2	24	.16	.125	15	9	.49	82	.01	18	1.82	.01	.08	1	42
13+00S 2+00E	25	258	1725	1524	10.6	83	66	4935	7.62	35	5	ND	2	10	16	6	2	23	.11	.124	11	10	.46	82	.01	5	1.64	.01	.05	1	52
13+00S 2+25E	5	97	209	712	2.3	39	25	1734	4.45	23	5	ND	3	15	10	2	3	29	.33	.115	20	12	.75	168	.03	5	1.67	.01	.07	1	3
13+00S 2+50E	7	48	134	344	1.5	20	11	982	4.21	22	5	ND	3	18	4	2	2	28	.34	.098	21	10	.77	113	.02	5	1.43	.01	.07	1	2
13+50S 2+50W	6	67	148	392	1.6	35	17	1409	4.83	23	5	ND	1	10	3	2	2	29	.15	.081	15	17	.78	79	.02	6	1.54	.01	.08	1	14
13+50S 2+25W	6	92	208	270	1.7	32	19	1347	4.71	25	5	ND	1	10	2	6	2	30	.13	.071	14	17	.75	38	.02	3	1.58	.01	.07	1	24
13+50S 2+00W	5	180	220	225	2.1	26	15	1032	4.98	25	5	ND	1	5	1	3	4	28	.07	.082	12	18	.72	48	.01	5	1.45	.01	.07	1	27
13+50S 1+75W	5	69	231	246	3.0	24	12	672	4.90	22	5	ND	2	6	1	2	2	27	.08	.076	11	16	.74	52	.01	4	1.35	.01	.05	1	15
13+50S 1+50W	6	68	260	301	3.1	25	15	1156	5.27	28	5	ND	2	6	1	6	2	25	.07	.084	13	14	.67	58	.01	4	1.34	.01	.07	1	82
13+50S 1+25W	6	112	352	298	2.7	24	20	1130	5.12	29	5	ND	2	6	1	6	2	25	.05	.079	13	15	.69	105	.01	3	1.42	.01	.05	1	45
13+50S 0+75W	6	94	409	384	3.2	24	15	773	4.76	36	5	ND	2	9	3	6	3	25	.14	.074	11	16	.71	75	.02	4	1.30	.01	.08	1	162
13+50S 0+50W	18	172	904	860	5.2	60	21	1916	6.21	36	5	ND	1	19	13	6	2	28	.26	.081	11	17	.84	58	.02	3	1.50	.01	.05	1	57
13+50S 0+25W	6	83	505	590	3.9	27	15	1206	4.42	24	5	ND	1	16	14	3	2	19	.25	.081	10	9	.56	70	.01	4	1.07	.01	.04	1	57
13+50S 0+25E	12	428	5145	1332	23.7	38	27	2429	6.01	22	5	ND	3	12	10	9	2	23	.22	.096	11	10	.56	64	.01	5	1.50	.01	.07	1	210
13+50S 0+50E	3	64	378	550	3.2	16	15	1190	4.31	17	5	ND	4	22	6	3	2	25	.43	.113	20	10	.64	204	.02	5	1.52	.01	.13	1	32
13+50S 0+75E	3	52	242	618	3.3	20	13	947	3.91	14	5	ND	3	16	6	3	4	18	.30	.086	14	7	.50	51	.01	3	1.06	.01	.05	1	21
13+50S 1+00E	3	67	470	503	2.9	21	17	1323	4.39	19	5	ND	3	23	11	2	2	22	.38	.104	21	9	.58	255	.02	8	1.45	.01	.10	1	28
13+50S 1+25E	2	56	155	385	2.6	21	17	1503	3.76	17	5	ND	4	16	5	2	2	24	.37	.107	24	8	.50	148	.01	5	1.32	.01	.05	1	10
13+50S 1+50E	3	74	214	581	3.9	26	23	1909	3.93	15	5	ND	5	15	8	2	2	25	.38	.113	24	8	.54	175	.02	3	1.41	.01	.08	1	19
13+50S 1+75E	10	178	610	748	4.6	34	27	2020	4.33	24	5	ND	3	12	16	3	2	22	.32	.119	20	7	.52	135	.01	4	1.29	.01	.05	1	32
13+50S 2+00E	5	95	560	1684	4.0	78	31	2660	4.56	24	5	ND	5	14	24	2	2	25	.37	.137	23	7	.61	191	.01	3	1.47	.01	.07	1	14
13+50S 2+25E	11	144	437	472	2.5	27	26	1467	4.79	22	5	ND	3	11	5	2	2	22	.25	.114	14	8	.55	50	.01	11	1.33	.01	.05	1	12
13+50S 2+50E	4	54	185	485	2.2	27	18	1648	4.48	25	5	ND	3	24	6	3	2	30	.43	.109	21	13	.78	183	.03	7	1.60	.01	.05	1	9
14+00S 2+50W	5	73	162	335	1.2	42	20	1538	5.12	24	5	ND	3	11	3	7	3	35	.15	.088	18	22	.84	103	.03	3	1.95	.01	.07	1	17
14+00S 2+25W	5	85	135	249	1.7	37	24	1130	5.03	27	5	ND	1	7	1	2	2	25	.10	.074	12	15	.75	42	.01	2	1.45	.01	.04	1	22
14+00S 2+00W	5	58	180	195	3.2	27	15	722	4.34	24	5	ND	2	9	1	5	2	27	.16	.075	11	17	.76	53	.04	12	1.22	.01	.04	1	47
14+00S 1+75W	8	138	1118	554	4.6	58	29	1554	7.10	46	5	ND	2	19	6	6	2	27	.26	.098	13	15	.76	82	.02	4	1.50	.01	.05	1	55
14+00S 1+50W	6	93	235	376	2.3	35	24	1571	5.09	30	5	ND	2	11	4	3	2	25	.19	.093	18	13	.67	52	.02	12	1.38	.01	.05	1	43
14+00S 1+25W	10	138	477	365	3.3	30	25	1943	5.69	31	5	ND	2	9	2	6	2	26	.11	.090	15	13	.66	71	.02	2	1.40	.01	.05	1	75
14+00S 1+00W	7	91	272	254	3.2	23	18	906	5.41	27	5	ND	2	5	1	7	2	26	.06	.078	11	16	.70	49	.02	7	1.29	.01	.05	1	65
14+00S 0+75W	7	155	498	357	3.7	36	26	1127	5.75	38	5	ND	2	5	1	7	2	25	.12	.082	9	13	.67	70	.01	6	1.35	.01	.07	1	35
14+00S 0+50W	8	235	671	676	4.8	43	24	1514	5.00	32	5	ND	3	15	9	7	4	22	.21	.070	11	11	.56	127	.01	3	1.23	.01	.10	1	57
14+00S 0+25W	7	105	365	398	3.5	16	7	366	4.53	29	5	ND	1	7	3	3	2	20	.06	.067	9	12	.55	66	.01	4	.95	.01	.04	1	104
14+00S 0+25E	9	97	624	1740	8.2	40	19	1327	4.62	21	5	ND	2	30	26	6	2	15	.41	.076	8	8	.47	70	.01	23	.88	.01	.25	1	58
STD C/AU-S	19	61	39	132	6.6	67	31	1001	4.02	38	22	7	38	48	18	18	21	58	.49	.089	38	56	.65	175	.07	35	1.97	.06	.14	13	51

C16

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
14+00S 0+50E	4	45	345	478	3.0	13	14	1286	4.20	7	5	ND	2	17	6	2	2	22	.30	.088	18	6	.53	135	.02	3	1.12	.01	.05	1	8
14+00S 0+75E	4	57	409	639	3.5	16	14	1495	3.96	12	5	ND	3	23	8	2	2	21	.41	.115	22	7	.52	161	.02	2	1.14	.02	.07	1	13
14+00S 1+00E	6	73	716	1059	5.2	27	17	1426	4.63	14	5	ND	3	23	14	2	2	20	.37	.113	17	7	.50	142	.03	8	1.16	.01	.06	1	33
14+00S 1+25E	2	116	454	546	3.3	15	19	967	3.48	7	5	ND	4	15	6	2	2	19	.32	.103	17	6	.52	55	.02	10	1.16	.01	.05	1	5
14+00S 1+50E	4	76	415	474	3.6	11	13	1073	3.85	13	5	ND	4	19	6	2	2	22	.35	.096	15	8	.57	123	.03	2	1.20	.01	.06	1	14
14+00S 1+75E	2	45	320	595	2.8	11	15	1397	4.00	13	5	ND	4	43	7	2	2	23	1.00	.099	22	8	.52	190	.02	2	1.55	.01	.12	1	37
14+00S 2+00E	3	38	130	253	3.3	8	12	1137	3.60	13	5	ND	4	29	3	2	2	25	.80	.104	23	7	.63	180	.02	11	1.35	.01	.08	1	30
14+00S 2+25E	2	41	144	320	2.5	14	13	1446	3.86	19	5	ND	4	21	4	2	2	25	.48	.122	26	8	.54	144	.04	2	1.22	.01	.05	1	3
14+00S 2+50E	5	52	194	724	3.2	53	26	13735	6.65	66	5	ND	4	39	4	2	2	25	.60	.123	30	11	.62	369	.03	2	1.66	.02	.07	1	7
14+00S 2+75E	2	36	63	190	1.6	10	9	1036	3.27	11	5	ND	4	19	1	2	2	24	.60	.126	21	9	.53	117	.01	2	1.20	.01	.06	1	2
14+50S 2+50W	6	66	138	305	1.8	30	16	1108	4.58	24	5	ND	2	13	3	2	2	28	.19	.076	16	13	.74	76	.02	12	1.45	.01	.05	2	8
14+50S 2+25W	7	72	187	369	1.8	36	25	3120	5.18	26	5	ND	2	9	4	2	2	27	.15	.098	17	14	.68	73	.02	11	1.57	.01	.05	1	71
14+50S 2+00W	5	95	176	387	2.2	53	31	1854	6.03	35	5	ND	2	10	3	2	2	24	.15	.078	15	13	.73	78	.01	8	1.54	.01	.05	1	5
14+50S 1+75W	6	101	199	415	1.9	58	28	1773	5.48	31	5	ND	3	9	3	3	2	26	.13	.079	22	14	.75	104	.01	2	1.70	.01	.07	1	2
14+50S 1+50W	2	60	115	180	1.7	25	15	789	5.31	23	5	ND	2	4	1	2	4	28	.03	.074	14	16	.80	37	.01	12	1.53	.01	.06	2	54
14+50S 1+25W	4	95	284	352	2.6	37	23	1149	5.15	28	5	ND	3	12	3	2	2	25	.18	.077	14	17	.82	118	.02	2	1.55	.01	.08	1	15
14+50S 1+00W	5	154	196	457	3.0	50	24	1513	5.35	24	5	ND	2	19	4	2	2	25	.28	.082	16	17	.77	104	.04	2	1.47	.01	.06	1	13
14+50S 0+75W	3	209	255	351	4.0	45	39	1545	6.72	36	5	ND	3	11	2	6	2	24	.13	.085	13	14	.64	85	.02	2	1.45	.01	.08	1	5
14+50S 0+50W	7	122	258	265	3.3	25	12	512	5.40	24	5	ND	2	7	1	5	2	25	.07	.075	11	17	.65	82	.02	12	1.22	.01	.07	1	13
14+50S 0+25W	21	254	1078	479	5.2	65	53	3569	7.06	65	5	ND	3	12	4	6	2	37	.14	.103	14	15	.82	130	.03	2	2.19	.02	.09	1	13
14+50S 0+75E	6	102	568	1001	4.4	19	14	1307	4.15	18	5	ND	3	23	13	2	4	20	.37	.095	16	6	.48	125	.02	8	1.08	.01	.07	1	15
14+50S 1+00E	5	69	503	639	5.3	33	25	1241	4.24	11	5	ND	3	17	9	2	2	23	.31	.091	16	6	.57	112	.02	2	1.27	.01	.06	1	12
14+50S 1+25E	7	80	550	1115	4.5	22	13	1699	4.28	15	5	ND	4	26	18	6	2	22	.46	.122	22	7	.50	347	.02	9	1.10	.01	.08	1	23
14+50S 1+50E	5	56	565	1151	4.5	18	12	1212	4.07	16	5	ND	4	28	14	4	2	24	.49	.117	17	9	.57	204	.03	8	1.28	.01	.05	1	22
15+00S 2+50W	7	55	145	331	1.9	23	17	1025	4.66	24	5	ND	3	9	3	4	2	28	.11	.072	18	13	.75	102	.02	6	1.45	.01	.07	1	12
15+00S 2+25W	7	73	215	399	1.5	41	23	1420	5.30	27	5	ND	2	11	3	4	2	30	.11	.085	20	15	.75	122	.02	3	1.76	.02	.08	1	12
15+00S 2+00W	7	104	131	358	1.5	46	31	2691	6.81	21	5	ND	3	16	6	2	2	32	.25	.089	14	13	.70	65	.04	2	1.73	.01	.08	1	12
15+00S 1+75W	6	64	156	407	2.4	57	27	1431	5.48	34	5	ND	3	12	3	4	2	26	.18	.089	15	15	.82	94	.01	10	1.56	.01	.07	1	16
15+00S 1+50W	12	88	405	517	5.9	56	29	2470	5.63	52	5	ND	3	24	10	5	3	26	.29	.113	16	12	.67	95	.02	2	1.38	.01	.06	1	35
15+00S 1+25W	5	77	251	344	2.6	27	23	1261	5.89	33	5	ND	3	7	2	2	3	26	.09	.066	17	12	.70	52	.01	2	1.53	.01	.06	2	5
15+00S 1+00W	3	63	120	214	2.4	32	12	591	5.58	25	5	ND	3	5	1	4	2	29	.05	.070	12	17	.77	60	.01	12	1.53	.02	.07	1	3
15+00S 0+75W	4	151	384	401	2.5	52	25	1257	5.35	35	5	ND	3	10	3	2	2	25	.15	.074	13	14	.74	88	.01	2	1.50	.01	.07	1	10
15+00S 0+50W	3	130	357	607	3.7	50	22	1442	5.12	25	5	ND	2	15	7	4	2	28	.23	.078	17	14	.77	163	.01	2	1.50	.01	.03	1	8
15+00S 0+25W	6	147	334	406	4.1	35	22	1156	5.26	27	5	ND	3	12	2	4	2	28	.20	.082	13	17	.73	152	.03	4	1.43	.01	.05	1	[illegible]
15+00S 0+25E	16	259	683	495	7.5	15	8	429	6.78	37	5	ND	3	7	3	8	3	20	.05	.118	9	10	.32	54	.01	2	.57	.01	.08	1	45
15+00S 0+50E	11	180	424	597	5.1	16	9	327	4.66	24	5	ND	3	14	5	7	2	19	.15	.088	8	7	.39	145	.01	3	.52	.01	.08	1	27
STD C/AU-S	18	62	39	132	6.6	67	30	990	4.01	39	20	7	37	47	18	15	22	57	.49	.087	38	53	.88	175	.07	32	1.57	.06	.14	11	52

C17 White Channel Resources Inc. PROJECT SILVER CROWN FILE # 89-3779

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
16+00S 2+00W	7	57	324	498	2.0	15	16	1553	3.94	18	5	ND	3	10	8	3	2	21	.21	.089	18	8	.48	60	.01	16	1.14	.01	.04	1	22
16+00S 1+75W	11	72	385	568	2.2	33	19	2804	4.73	35	5	ND	3	11	10	5	2	26	.15	.102	23	9	.62	114	.01	4	1.44	.01	.07	1	28
16+00S 1+50W	9	58	333	598	3.2	25	17	1625	4.41	27	12	ND	4	12	7	5	2	25	.20	.096	18	9	.55	130	.01	11	1.31	.01	.05	1	17
16+00S 1+25W	15	56	321	540	3.3	27	16	1802	4.74	39	5	ND	2	9	7	6	2	27	.14	.090	16	6	.60	77	.01	4	1.28	.01	.06	2	52
16+00S 1+00W	9	63	351	602	2.8	28	16	1553	4.56	18	5	ND	2	11	8	4	2	22	.19	.089	14	7	.54	85	.01	15	1.28	.01	.07	1	31
16+00S 0+75W	17	152	729	1335	5.3	75	38	3405	6.24	32	5	ND	2	14	24	6	4	22	.24	.104	13	9	.54	107	.01	10	1.15	.01	.06	1	31
16+00S 0+50W	13	54	192	585	3.8	25	13	1256	4.43	28	5	ND	1	19	8	5	2	19	.29	.097	13	6	.53	81	.02	2	.88	.01	.05	1	28
16+00S 0+25W	14	76	417	990	4.6	40	17	2190	5.17	30	9	ND	2	24	12	7	2	23	.38	.110	14	10	.51	203	.01	4	1.13	.01	.11	1	40
16+00S 1+00E	8	87	515	1044	3.4	15	22	1464	5.16	27	5	ND	5	22	12	3	2	32	.30	.110	23	10	.63	140	.03	7	1.65	.01	.09	1	61
16+00S 1+25E	3	62	328	1047	1.9	14	17	2727	4.19	15	5	ND	2	55	15	2	2	28	2.59	.099	15	10	.50	236	.02	15	1.66	.01	.08	1	30
16+00S 1+50E	4	155	260	1534	1.8	32	24	17858	5.96	28	5	ND	3	38	14	2	2	41	.83	.172	35	22	.96	385	.02	8	2.51	.01	.05	1	31
17+00S 2+00W	14	103	200	711	1.4	44	21	2984	5.95	70	5	ND	2	17	10	5	2	27	.20	.095	26	9	.67	154	.01	2	1.83	.01	.08	1	200
17+00S 1+75W	13	82	265	485	2.8	18	15	1778	4.86	52	5	ND	2	11	6	4	2	27	.19	.083	20	8	.64	110	.02	2	1.32	.01	.05	1	48
17+00S 1+50W	11	93	382	522	1.9	21	16	1790	4.91	97	5	ND	4	13	7	6	2	26	.23	.067	23	8	.62	135	.02	14	1.28	.01	.07	1	49
17+00S 1+25W	8	37	175	341	1.6	17	12	1162	4.28	59	5	ND	3	14	3	2	2	28	.23	.077	19	8	.84	102	.04	4	1.22	.01	.06	1	10
17+00S 1+00W	6	95	241	512	1.8	18	13	1771	4.76	44	5	ND	4	20	7	3	2	25	.30	.085	24	9	.67	147	.04	2	1.43	.01	.05	1	15
17+00S 0+75W	15	73	273	551	2.8	29	17	2068	5.58	38	11	ND	4	18	7	7	2	33	.19	.092	28	7	.78	154	.02	12	1.72	.01	.08	1	14
17+00S 0+50W	1	87	365	455	2.2	10	14	1001	4.87	2	5	ND	4	17	4	2	3	27	.23	.073	23	10	.72	108	.03	3	1.91	.01	.07	1	55
17+00S 0+25W	2	74	358	471	1.5	13	15	1324	5.25	18	5	ND	4	11	5	3	3	28	.23	.085	22	12	.64	75	.02	13	1.63	.01	.04	1	73
17+00S 0+25E	3	129	753	762	2.5	16	22	2062	5.93	17	5	ND	3	18	8	2	2	34	.25	.099	34	12	.74	145	.04	1	2.29	.01	.03	1	56
17+00S 0+50E	3	65	347	484	1.8	11	15	1367	5.03	11	5	ND	5	11	4	2	2	20	.16	.044	42	8	.74	53	.01	3	1.56	.01	.03	1	38
17+00S 0+75E	3	96	753	497	2.1	10	16	1439	5.01	13	5	ND	7	10	3	5	3	24	.15	.050	34	8	.74	87	.02	2	1.91	.01	.08	1	230
17+00S 1+00E	6	193	1532	2618	18.5	47	46	7689	7.37	51	5	ND	3	21	34	7	2	32	.33	.147	48	15	.55	247	.02	5	2.51	.01	.07	1	570
17+00S 1+25E	5	105	662	976	3.6	37	61	3357	5.97	39	5	ND	3	21	11	4	2	39	.32	.108	27	15	.79	161	.07	12	2.35	.02	.05	1	36
17+00S 1+50E	4	56	267	654	1.7	21	48	1918	4.63	38	5	ND	3	26	5	4	2	34	.73	.077	20	13	.72	118	.05	3	1.80	.01	.07	1	32
18+00S 2+00W	3	55	139	362	1.1	13	21	2475	4.43	24	5	ND	3	13	4	2	2	27	.29	.110	25	9	.48	124	.02	3	1.51	.01	.03	1	44
18+00S 1+75W	4	52	149	300	.8	21	15	1638	4.18	22	5	ND	3	9	2	2	2	20	.19	.117	25	18	.45	59	.01	2	1.34	.01	.05	1	12
18+00S 1+50W	5	53	362	291	1.6	17	21	1347	4.68	25	5	ND	3	8	2	4	2	23	.17	.112	19	12	.56	51	.02	15	1.43	.01	.05	1	20
18+00S 1+25W	8	111	265	431	1.3	38	37	2359	6.13	40	9	ND	4	10	2	5	2	32	.15	.134	24	18	.61	112	.03	4	2.63	.01	.05	1	14
18+00S 1+00W	2	65	181	243	1.3	6	23	845	4.02	13	5	ND	3	10	3	2	2	25	.23	.095	19	5	.53	83	.02	2	1.25	.01	.06	2	220
18+00S 0+75W	2	81	235	298	1.4	4	15	1052	4.09	10	5	ND	4	16	2	3	2	27	.31	.095	25	6	.57	128	.03	3	1.38	.01	.03	1	11
18+00S 0+50W	3	52	213	279	1.2	4	12	693	3.97	4	5	ND	3	12	2	2	2	27	.24	.085	21	5	.55	101	.03	18	1.29	.01	.05	1	13
18+00S 0+25W	1	50	179	238	1.0	13	12	646	4.05	9	5	ND	2	18	2	2	2	32	.28	.073	22	13	.77	85	.06	3	1.72	.01	.08	1	27
18+00S 0+75E	14	139	345	588	1.5	19	21	6947	6.04	35	11	ND	3	21	3	5	4	41	.22	.098	46	14	1.07	261	.04	5	2.84	.01	.11	1	61
18+00S 1+00E	2	85	320	432	1.5	6	17	1249	4.73	10	5	ND	2	13	4	2	2	25	.19	.057	25	7	.78	134	.03	2	1.54	.01	.07	1	25
18+00S 1+25E	5	176	812	596	2.8	13	18	2403	3.56	14	5	ND	3	19	5	6	2	30	.38	.061	27	11	.90	205	.04	6	2.13	.02	.07	1	38
STD C/AU-S	18	57	42	134	7.1	68	31	967	3.99	43	21	7	38	48	18	15	21	59	.48	.090	38	58	.88	177	.07	34	1.98	.06	.14	13	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L5+00S 1+50E	3	239	2747	1055	8.4	17	15	2362	7.37	22	6	ND	3	20	5	5	2	43	.38	.087	29	15	.94	201	.05	4	2.41	.03	.10	1	245
L5+00S 1+75E	20	1015	13436	6450	84.6	19	19	1969	6.94	36	5	ND	3	20	64	42	2	43	.27	.095	17	21	.75	96	.07	8	2.02	.04	.11	1	610
L5+00S 2+00E	4	132	2981	742	8.9	12	14	1356	5.14	10	5	ND	4	24	7	4	2	41	.42	.091	32	15	.84	157	.05	2	2.27	.03	.11	1	56
L5+00S 2+00W	1	60	263	299	1.1	8	13	1184	4.37	9	5	ND	2	18	3	2	2	32	.32	.126	23	14	.72	203	.02	2	1.57	.01	.12	1	16
L5+00S 1+75W	1	52	251	271	1.0	8	11	777	3.82	7	5	ND	1	14	3	2	2	29	.31	.110	21	14	.55	118	.03	14	1.39	.01	.08	1	14
L5+00S 1+50W	1	87	535	404	1.4	9	13	907	4.18	7	5	ND	3	15	3	2	2	30	.29	.112	23	13	.70	162	.03	3	1.60	.01	.12	1	13
L5+00S 1+25W	1	57	307	318	1.3	10	12	929	4.07	10	5	ND	3	14	3	2	2	31	.29	.103	23	13	.71	164	.04	15	1.57	.01	.10	1	71
L5+00S 1+00W	1	59	294	322	1.4	6	11	1090	3.84	6	5	ND	2	16	3	2	2	25	.35	.125	23	9	.63	202	.02	9	1.33	.01	.10	1	35
L5+00S 0+75W	2	94	601	438	2.1	10	15	1155	4.60	11	5	ND	2	16	2	2	2	33	.27	.104	27	14	.72	140	.03	8	1.80	.01	.11	1	250
L5+00S 0+50W	3	159	1458	520	2.3	7	18	1452	4.78	12	5	ND	1	17	9	2	2	26	.31	.123	22	8	.56	174	.02	11	1.30	.01	.09	1	85
L5+00S 0+25W	2	74	293	360	1.9	4	13	1849	4.68	5	5	ND	2	19	4	2	2	28	.36	.133	25	8	.71	283	.02	11	1.58	.01	.10	1	56
L5+00S 0+25E	7	61	350	498	2.9	3	14	1670	4.72	13	5	ND	1	14	4	2	2	26	.24	.114	25	5	.43	260	.01	11	1.35	.02	.12	1	33
L5+00S 0+50E	2	63	254	285	2.4	6	13	1630	4.23	11	5	ND	2	14	2	2	2	25	.24	.052	24	10	.67	212	.04	3	1.55	.02	.06	1	30
L5+00S 0+75E	1	49	134	271	1.4	8	12	1000	4.11	7	5	ND	2	15	3	2	2	39	.30	.092	23	10	.72	142	.05	7	1.59	.02	.08	1	220
L5+00S 1+00E	3	54	201	300	2.4	10	13	1377	4.33	12	5	ND	2	22	3	2	3	41	.38	.057	28	12	.74	249	.06	12	1.90	.02	.10	1	57
L5+00S 1+25E	5	62	1540	275	3.2	11	14	1163	4.25	13	5	ND	3	20	1	2	2	43	.31	.088	25	13	.77	144	.07	8	1.88	.03	.10	1	69
L5+00S 1+50E	1	58	254	317	4.5	13	18	1076	4.13	22	5	ND	3	25	3	2	3	41	.38	.090	29	15	.75	219	.07	12	1.81	.04	.10	1	50
L5+00S 1+75E	5	45	315	307	3.0	10	16	3328	5.34	15	5	ND	2	25	3	4	3	40	.31	.077	27	14	.61	429	.06	4	1.87	.03	.09	1	61
L5+00S 2+00E	1	51	169	274	3.5	12	14	679	3.83	8	5	ND	3	22	1	2	2	42	.36	.073	24	15	.83	154	.06	3	1.68	.04	.08	1	70
L10+00S 2+00W	1	122	526	507	1.8	4	13	1422	4.33	4	5	ND	3	22	6	2	2	33	.27	.135	15	16	1.00	153	.03	3	1.58	.01	.08	1	260
L10+00S 1+75W	1	78	296	375	1.5	4	13	1198	4.23	5	5	ND	3	22	4	2	2	33	.37	.122	19	5	1.07	364	.02	2	1.73	.01	.10	1	21
L10+00S 1+50W	4	191	545	787	2.9	5	12	1366	4.45	7	5	ND	3	32	10	2	2	34	.41	.121	20	13	1.00	248	.04	13	1.84	.02	.14	1	38
L10+00S 1+25W	1	63	158	242	.7	6	14	1896	4.09	7	5	ND	3	25	2	2	2	31	.31	.118	22	13	1.00	271	.03	2	1.70	.01	.13	1	20
L10+00S 1+00W	1	73	135	198	.5	7	14	2073	4.43	10	5	ND	3	16	2	2	2	34	.19	.099	20	14	.82	173	.04	4	1.65	.01	.05	1	15
L10+00S 0+75W	2	157	342	240	1.5	8	17	4723	6.27	8	5	ND	3	26	3	2	2	34	.26	.106	26	13	.72	382	.03	2	1.62	.01	.05	1	34
L10+00S 0+50W	1	56	87	186	1.0	5	12	5693	5.31	11	5	ND	1	28	3	3	2	25	.39	.144	36	11	.57	328	.02	2	1.97	.01	.10	1	17
L10+00S 0+25E	3	138	257	455	2.2	9	17	4156	5.98	11	5	ND	1	20	6	3	2	35	.30	.117	25	16	.70	517	.02	11	1.60	.01	.08	1	57
L10+00S 0+50E	1	35	71	130	.7	19	14	894	4.34	6	5	ND	3	15	1	2	3	47	.23	.075	25	33	1.12	152	.05	2	2.20	.02	.09	1	5
L10+00S 0+75E	1	45	64	150	.8	14	12	939	4.10	12	5	ND	3	17	1	2	2	45	.23	.052	24	20	.92	162	.06	3	2.07	.02	.09	1	11
L10+00S 1+00E	2	40	54	160	1.0	12	13	1110	3.48	7	5	ND	2	22	1	2	2	40	.32	.056	31	15	.73	163	.07	3	1.07	.23	.11	1	23
L10+00S 1+25E	2	46	344	223	1.6	11	15	1829	3.72	9	5	ND	1	19	2	2	2	43	.30	.102	39	14	.70	170	.05	4	2.64	.04	.12	1	12
L10+00S 1+50E	1	45	134	215	1.6	8	13	1725	4.68	10	5	ND	3	14	1	2	3	48	.25	.089	27	12	.98	128	.05	7	2.40	.01	.10	1	16
L10+00S 1+75E	1	51	133	280	2.7	12	13	1257	4.49	16	5	ND	4	19	1	2	2	55	.31	.054	34	16	.90	213	.05	3	2.70	.07	.13	1	33
L10+00S 2+00E	2	54	237	322	3.1	10	17	1405	4.70	10	5	ND	3	21	3	2	2	61	.23	.092	28	14	.87	275	.07	4	2.55	.04	.11	1	54
BL 0+00S	3	51	261	254	2.7	25	11	523	4.44	16	5	ND	2	9	1	2	2	28	.14	.081	12	16	.73	122	.01	4	1.42	.01	.10	1	32
BL 0+50S	1	46	116	226	1.9	38	11	462	5.16	20	5	ND	3	6	1	2	2	33	.05	.076	13	25	.56	68	.02	3	1.66	.01	.05	1	62
STD C/AU-S	18	53	40	132	6.7	68	31	954	4.10	42	23	8	36	46	18	15	21	58	.48	.095	38	57	.89	175	.07	35	1.90	.06	.14	11	510

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
BL 1+00S	4	59	161	233	1.2	35	22	1000	4.56	19	5	ND	3	4	1	2	2	25	.04	.073	15	16	.76	48	.01	11	1.45	.01	.08	1	27
BL 1+50S	3	65	161	431	2.8	48	22	1279	4.75	21	5	ND	3	14	5	2	2	25	.27	.093	16	13	.70	74	.01	13	1.52	.01	.08	1	60
BL 2+00S	3	93	250	738	3.5	50	35	1355	5.11	38	5	ND	4	35	6	3	8	27	.38	.098	23	11	.70	135	.01	18	1.55	.01	.09	1	15
BL 2+50S	5	115	555	860	4.5	65	33	2130	5.57	22	5	ND	4	18	10	6	2	24	.25	.101	20	11	.59	140	.01	2	1.65	.01	.08	1	45
BL 3+00S	3	69	522	765	3.2	31	15	1265	4.52	18	5	ND	2	28	8	2	2	24	.39	.100	18	11	.66	174	.02	7	1.58	.01	.11	1	25
BL 3+50S	2	75	392	789	2.8	33	15	1103	4.25	14	5	ND	1	32	8	2	2	23	.52	.075	13	13	.67	167	.01	4	1.53	.01	.10	1	25
BL 4+00S	7	138	906	1335	4.6	58	23	1293	4.94	24	5	ND	1	27	18	4	2	20	.28	.065	9	14	.64	125	.01	12	1.42	.01	.11	1	64
BL 4+50S	7	164	482	405	4.7	21	13	566	4.73	26	5	ND	2	5	2	6	2	19	.12	.062	10	10	.51	95	.01	5	1.20	.01	.10	1	45
BL 5+00S	7	133	230	339	4.6	24	13	648	5.69	27	5	ND	2	7	2	8	2	24	.09	.084	10	16	.68	55	.01	5	1.28	.01	.03	1	40
BL 5+50S	6	160	335	807	2.6	113	49	2156	6.56	58	5	ND	3	17	5	6	2	30	.23	.089	16	18	.78	177	.01	6	1.77	.01	.08	1	17
BL 6+00S	15	69	372	950	4.5	33	18	1782	4.83	32	5	ND	2	45	5	7	2	21	.98	.099	11	10	.55	123	.01	10	1.24	.01	.12	1	35
BL 6+50S	13	84	395	1060	3.3	23	18	2624	4.55	31	5	ND	2	30	15	2	2	18	.35	.094	17	8	.38	180	.01	3	1.04	.01	.11	1	74
BL 7+00S	3	103	414	432	1.8	13	15	1030	4.52	14	5	ND	3	13	3	2	2	25	.21	.061	21	14	.85	100	.03	12	2.07	.01	.05	1	55
BL 7+50S	1	70	358	391	1.3	12	15	998	4.61	6	5	ND	3	12	3	2	2	29	.19	.053	21	13	.99	85	.03	6	2.05	.01	.08	1	156
BL 8+00S	3	444	1221	383	2.8	9	25	1284	4.46	12	5	ND	5	11	3	2	2	27	.17	.071	22	7	.60	131	.03	4	2.09	.01	.10	1	21
BL 8+50S	2	121	166	251	1.7	3	11	1057	3.98	5	5	ND	3	12	1	2	2	26	.31	.104	21	3	.51	355	.02	11	1.33	.01	.08	1	58
BL 9+00S	4	58	135	223	1.2	8	12	1194	4.13	8	5	ND	2	13	1	2	2	32	.15	.061	22	7	.66	129	.03	3	1.63	.01	.07	1	32
BL 9+50S	6	95	358	475	2.3	10	24	4565	6.50	42	5	ND	3	37	5	3	2	37	.40	.103	25	11	.65	355	.08	6	1.75	.04	.11	1	42
BL 10+00S	2	53	195	265	1.1	8	16	3393	5.07	12	5	ND	2	18	2	2	2	35	.25	.107	24	13	.78	233	.02	3	1.78	.01	.03	1	32
BL 10+50S	2	79	45	148	.9	6	16	3572	4.71	14	5	ND	3	28	1	2	2	45	.35	.103	22	7	.77	374	.06	4	1.95	.01	.03	1	13
STD C/AU-S	18	60	43	132	7.2	68	30	995	3.97	43	19	7	38	47	18	15	20	57	.45	.087	38	56	.88	175	.07	33	2.00	.08	.14	12	45

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
ST-1	4	53	19	270	.5	101	33	1583	6.41	28	5	ND	1	20	1	2	2	51	.25	.113	14	38	1.13	90	.04	6	2.28	.01	.04	1	1
ST-2	2	80	19	243	.3	98	33	2227	5.67	28	5	ND	3	25	1	2	2	42	.25	.105	14	41	1.09	120	.02	20	2.08	.01	.05	1	1
ST-3	1	42	19	135	.3	65	17	822	4.07	15	5	ND	3	21	1	2	2	35	.24	.076	12	33	1.00	57	.03	9	1.62	.01	.04	1	1
ST-4	1	40	10	138	.3	76	16	726	4.13	14	5	ND	1	15	1	2	2	32	.22	.077	10	44	1.16	34	.02	8	1.76	.01	.03	1	1
ST-5	1	45	17	150	.4	80	19	907	4.73	12	5	ND	1	26	1	2	2	41	.21	.087	10	38	1.27	57	.04	6	1.57	.01	.04	1	1
ST-6	1	48	12	148	.4	83	17	985	4.94	17	5	ND	1	18	1	2	2	40	.24	.080	5	42	1.25	35	.02	5	1.98	.01	.02	1	2
ST-7	1	60	20	188	.7	88	25	1153	4.96	20	5	ND	1	19	1	2	2	34	.22	.082	13	34	1.13	60	.01	2	1.97	.01	.04	1	1
ST-8	2	21	52	186	4.8	14	6	516	2.91	27	5	ND	1	10	1	2	2	14	.20	.055	12	7	.51	58	.01	3	.93	.01	.02	1	1
ST-9	3	27	27	160	1.5	15	9	634	3.50	10	5	ND	1	15	1	2	2	32	.33	.084	12	21	.77	58	.04	2	1.32	.01	.03	1	4
ST-10	4	29	116	275	1.2	21	10	784	4.02	14	5	ND	1	15	3	2	2	30	.27	.085	12	15	.71	54	.03	2	1.29	.01	.04	1	310
STD C/AU-S	17	58	44	132	7.1	67	30	1017	4.15	40	19	7	36	47	16	15	22	57	.48	.092	37	53	.88	173	.07	36	1.95	.06	.14	11	50

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Assaying & Trace Analysis
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Telephone: 253-3158

Appendix D

Analytical Technique;

Gold & Silver by Fire Assay

1/2 A.T. samples is mix in dry reagent flux with 1 Ag inquart and fused for 45 - 60 mins. The resulting bead from cupellation is dissolved in aqua regia. Analysis by A.A/ICP.

- For Au > 1 oz/t, determination by gravimetric finished.
- Wet acid leached for Ag is also ran. (Procedure same as below).

Determination of Cu, Pb, Zn and Ag

In 100 ml volumetric flask, 1 g sample is digested in 50 ml 3-1-2 $HCl-HNO_3-H_2O$ at 95°C for one hour, dilute to 100 ml with demineralized water, analyze by ICP.

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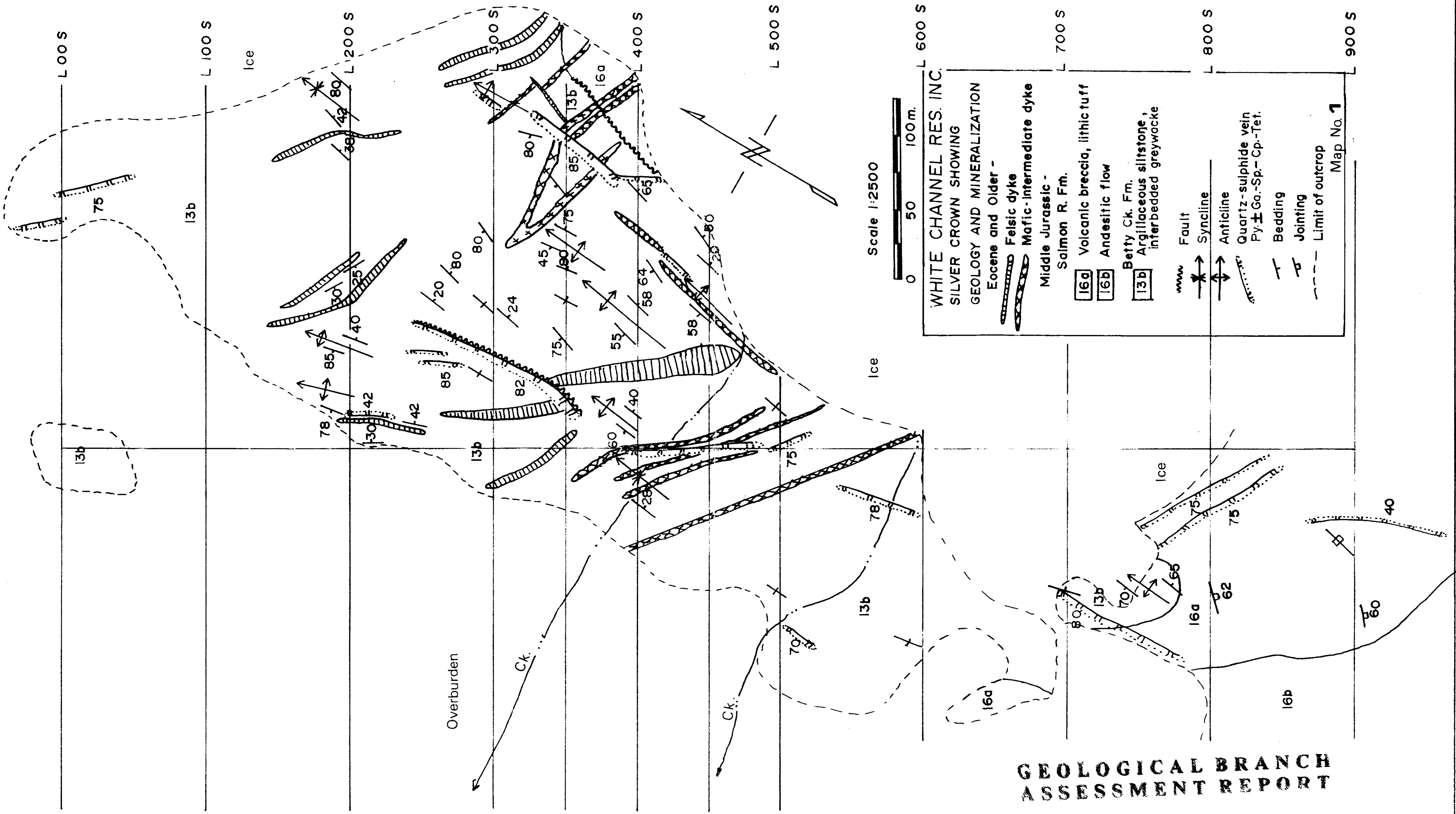
ICP - .5 gram sample is digested with 3 ml 3-1-2 HCl-HNO3-H2O at 95 deg.C for one hour and is diluted to 10 ml with water. This leach is Partial for Mn, Fe, Sr, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited for Na, K, Al.

Au* - 10 gram samples are ignited at 600 deg.C, digested with aqua regia at 95 deg.C for one hour, 50 ml aliquot is extracted into 10 ml MIBK, analysed by graphite furnace AA.

Soil prep - Dry 2lbs at 60°c Sieve approx 3g of -80 mesh.

Rock prep - Crush to approx -3/16" up to 10 lbs, split to approx 200-300g Pulverize to -100 mesh.



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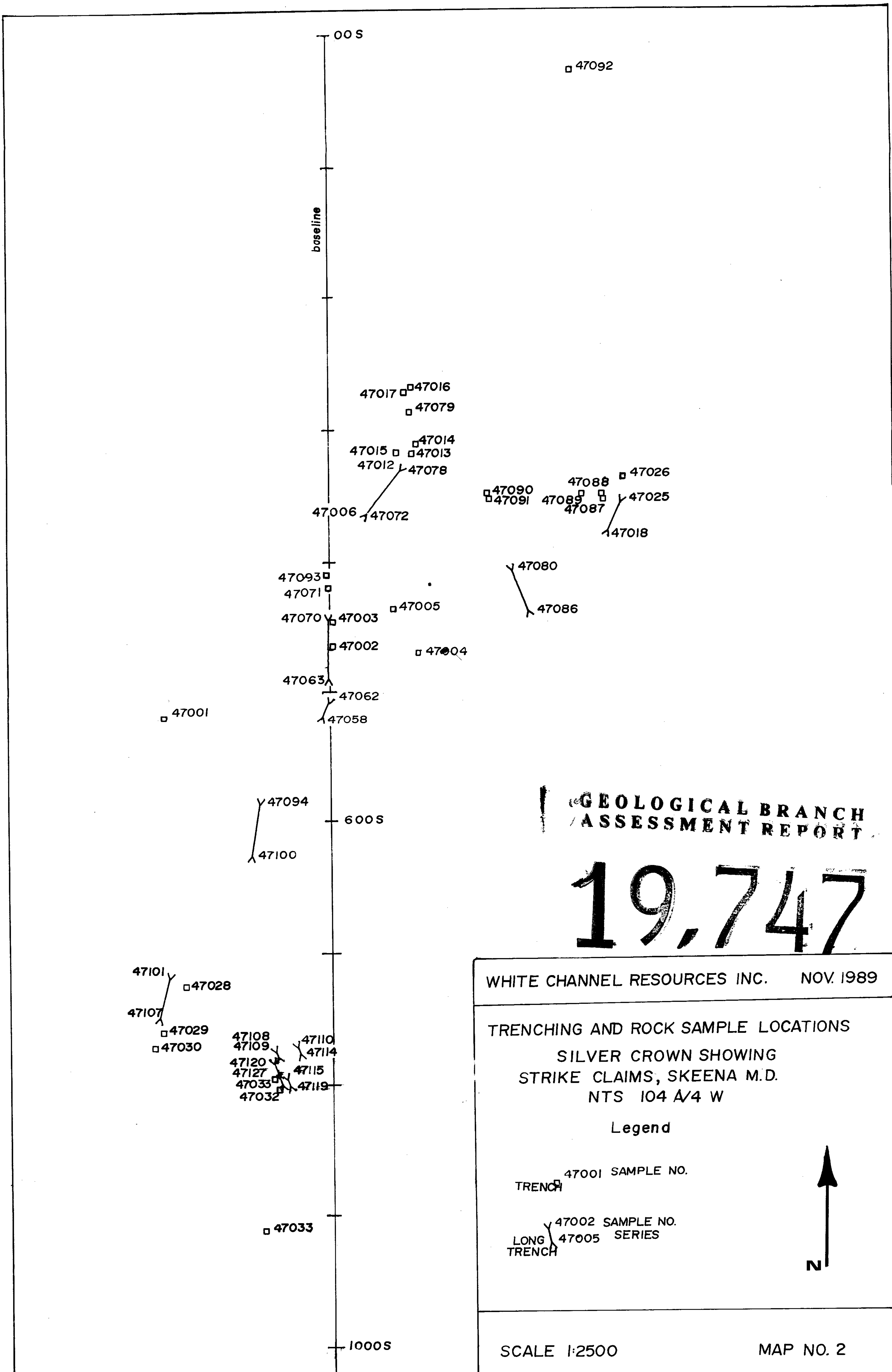

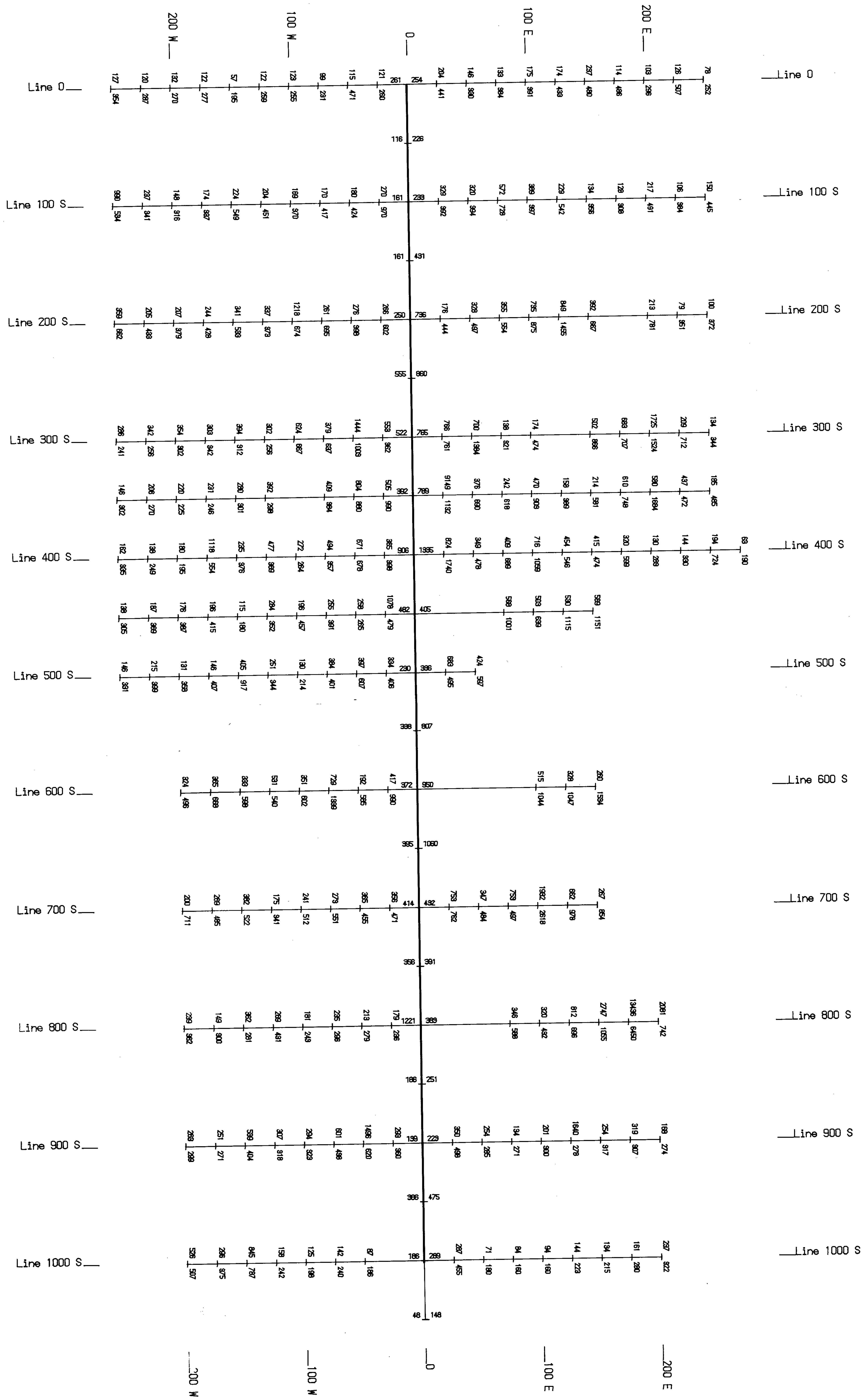

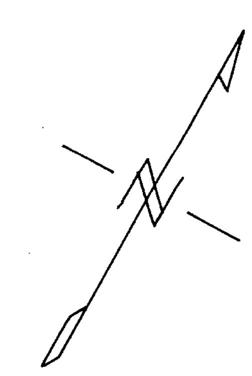

Scale 1:2500

25 0 25 50 75 100 125 (metres)

LEGEND

Lead (PPM)

Zinc (PPM)

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WHITE CHANNEL RESOURCES INC.

Soil Geochemistry

Zinc and Lead

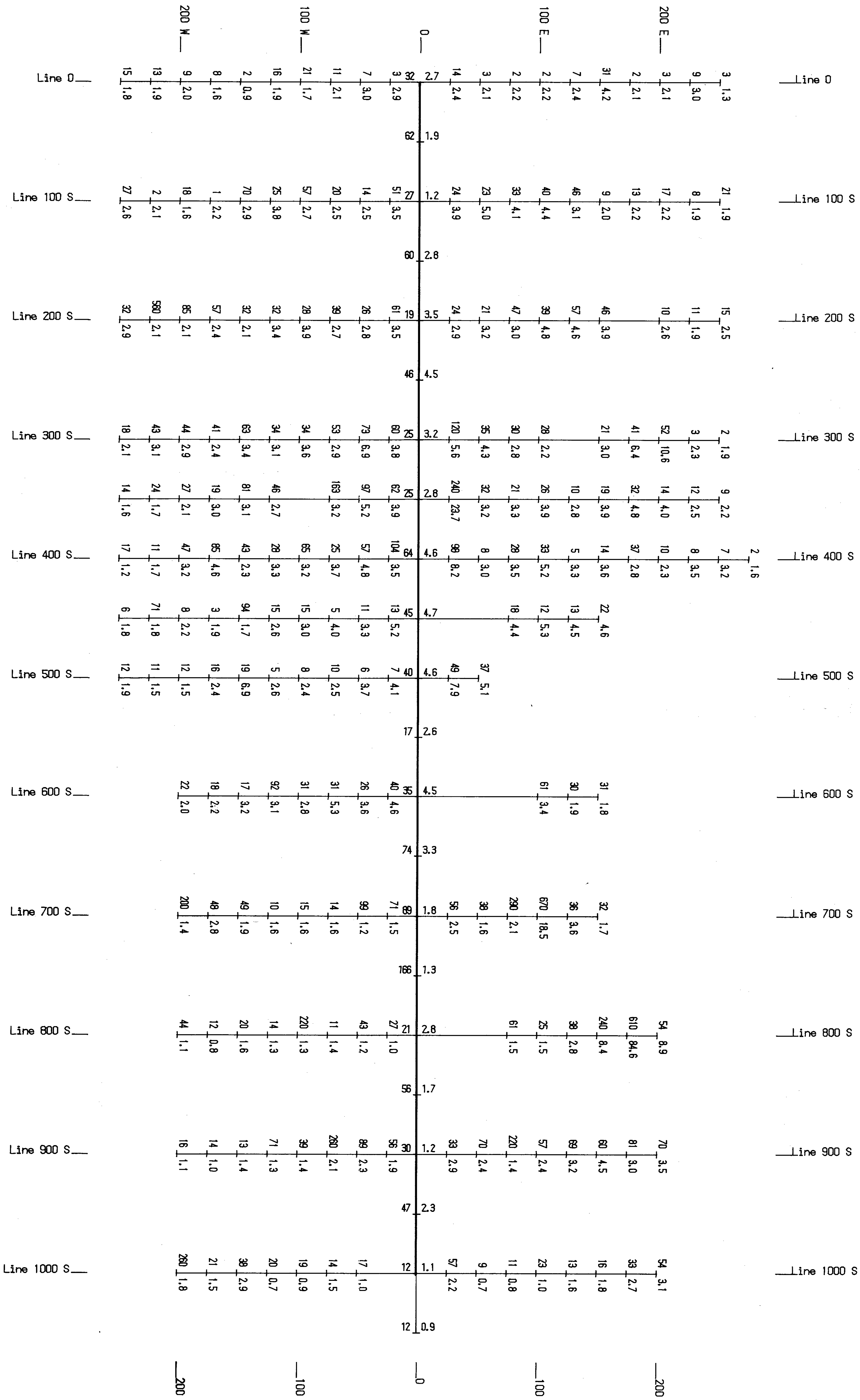
SILVER CROWN SHOWING - STRIKE 2 CLAIM

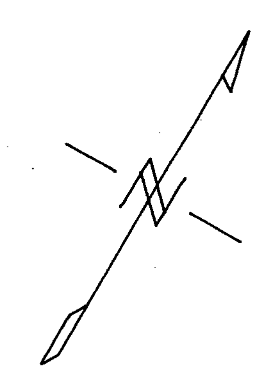
NTS: 104 A/4,5 Skeena Mining Division, B.C.

October, 1989

Figure # Map No. 3

Ashworth Explorations Limited





Scale 1:2500

25 0 25 50 75 100 125 (metres)

LEGEND

Gold (PPB)

Silver (PPM)

GEOLOGICAL BRANCH
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WHITE CHANNEL RESOURCES INC.

Soil Geochemistry

Gold and Silver

SILVER CROWN SHOWING - STRIKE 2 CLAIM

NTS: 104 A/4,5 Skeena Mining Division, B.C.

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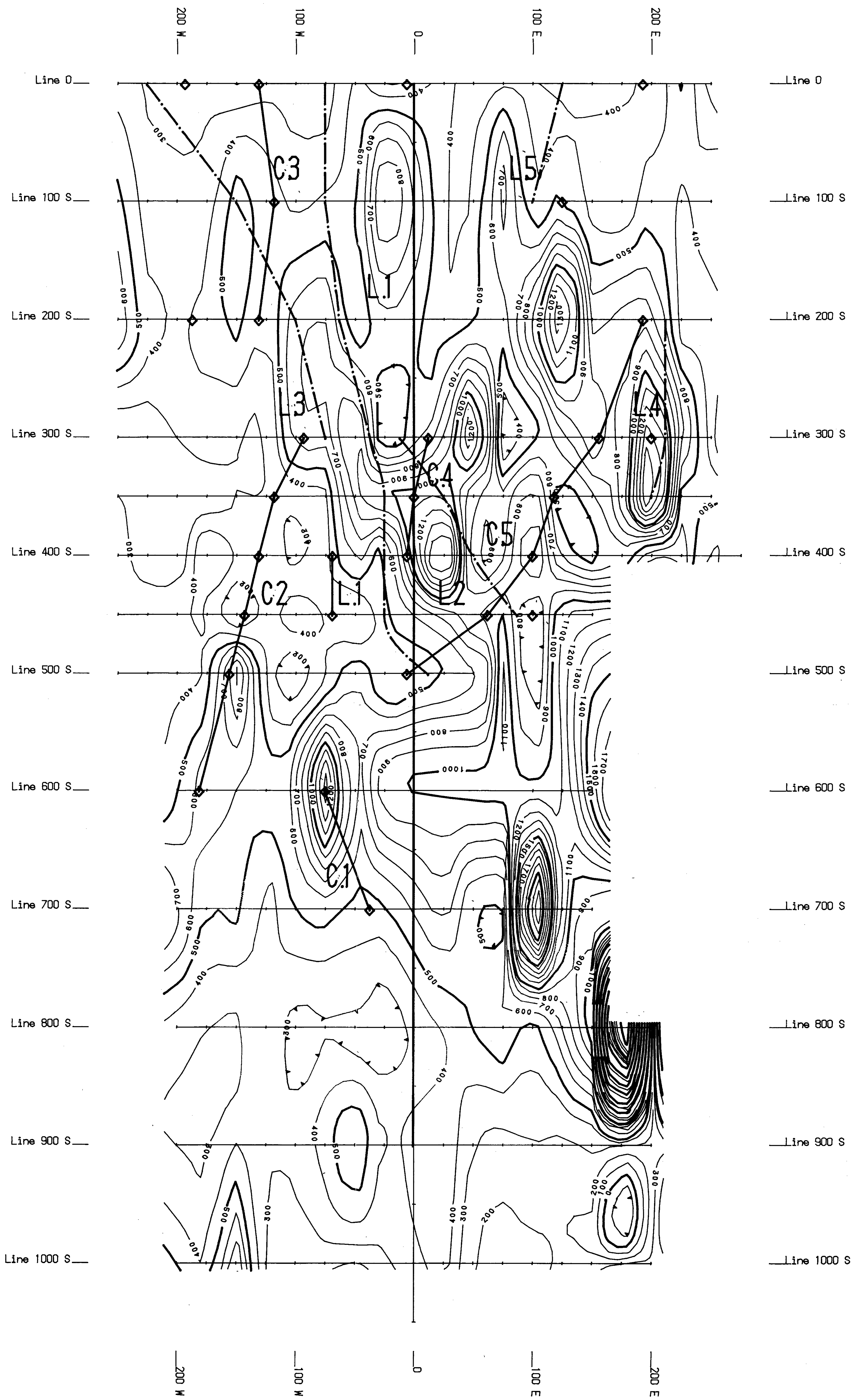
Figure # Map No. 4

Ashworth Explorations Limited



Scale 1:2500

25 0 25 50 75 100 125 (metres)

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LEGEND

Zinc Soil Geochemistry
Contour Interval

———— 100 PPM

———— 500 PPM

C2 —◇—◇—◇— VLF-EM Conductor

L3 —·—·— Magnetic Lineament

WHITE CHANNEL RESOURCES INC.

Compilation Map

SILVER CROWN SHOWING - STRIKE 2 CLAIM

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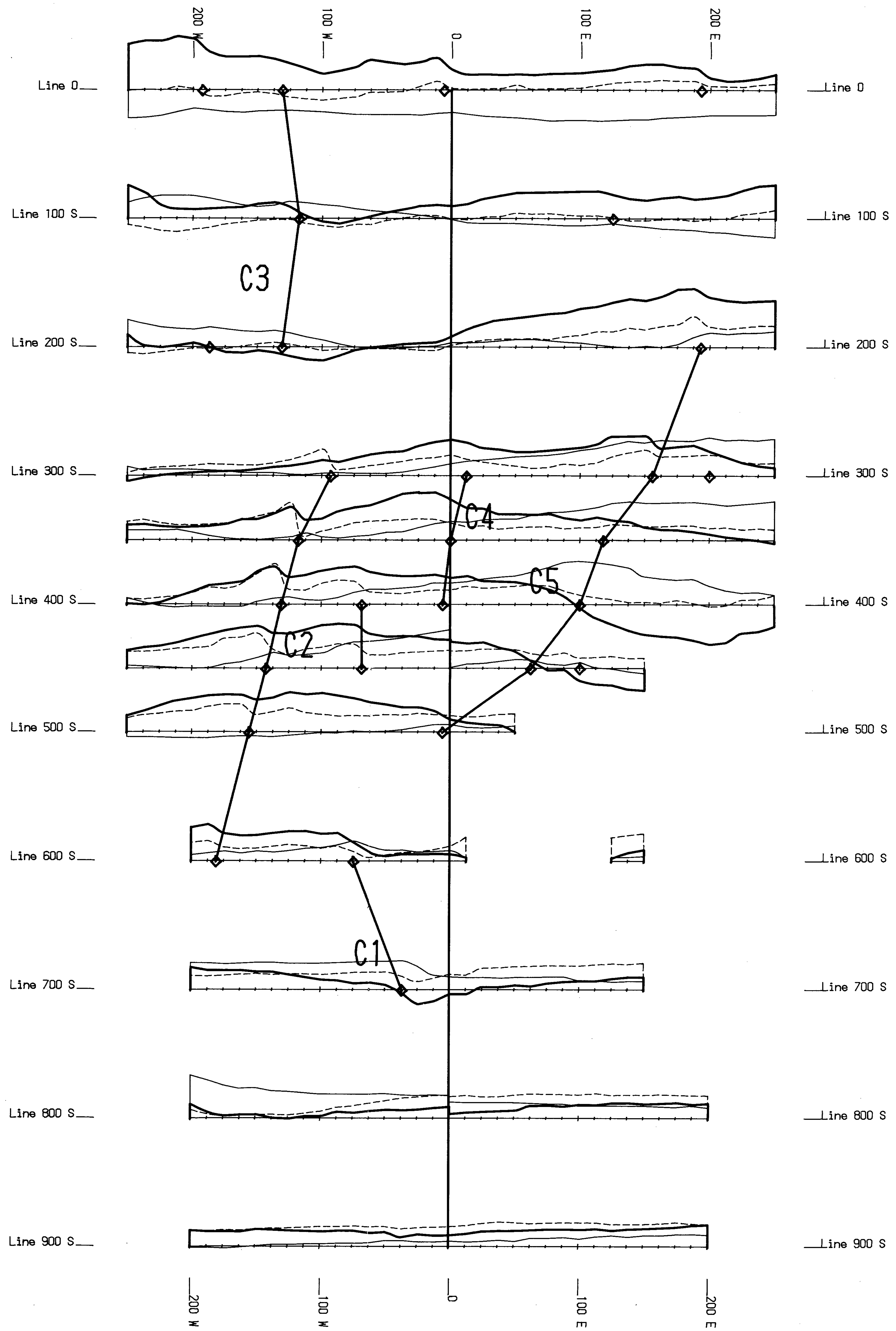
Figure # Map No. 5

Ashworth Explorations Limited



Scale 1:2500

25 0 25 50 75 100 125 (metres)

GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,747

LEGEND

Anomalous Inflection (In-Phase)

In-Phase

Quadrature

Field Strength 1 cm. = 5 units

VLF-EM Conductor

WHITE CHANNEL RESOURCES INC.

VLF-EM Profiles

NPM, Lualualei, Hawaii

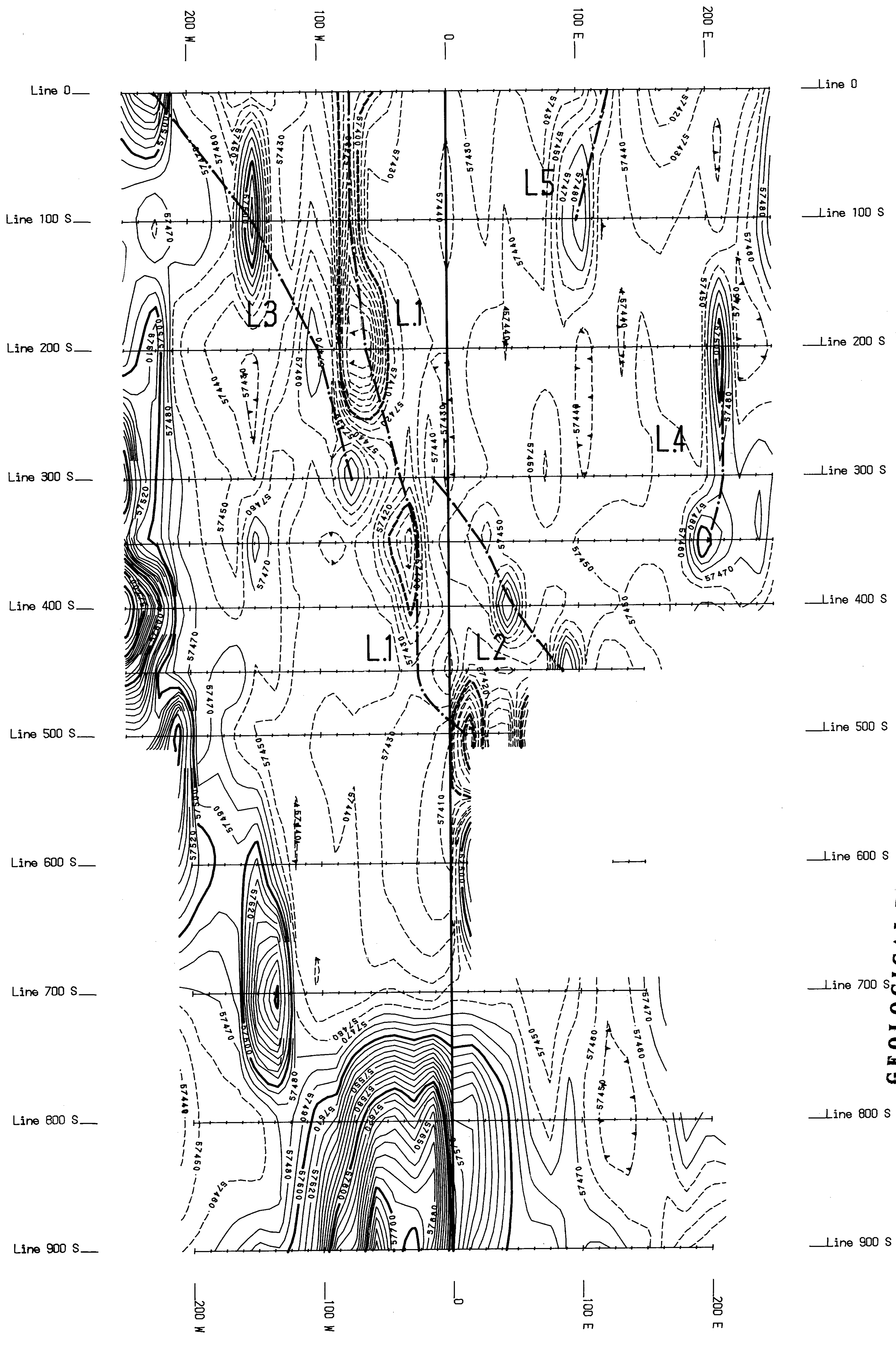
SILVER CROWN SHOWING - STRIKE 2 CLAIM

NTS: 104 A/4,5 Skeena Mining Division, B.C.

Figure # G-1 October, 1989

Surveyed by Ashworth Explorations Limited

Interpretex Resources Ltd. Map No. 6



GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,747

Scale 1:2500

25 0 25 50 75 100 125
(metres)

LEGEND

Contour Interval

< 57470 nT	> 57470 nT	
- - - .	——— .	10 nT
- - - .	———	100 nT
— · —		Magnetic Lineament

WHITE CHANNEL RESOURCES INC.

Total Field Magnetic Contours

SILVER CROWN SHOWING - STRIKE 2 CLAIM

NTS: 104 A/4,5 Skeena Mining Division, B.C.

Figure # G-4 October, 1989

Surveyed by Ashworth Explorations Limited

Interpretex Resources Ltd. Map No. 7

Scale 1:2500

25 0 25 50 75 100 125 (metres)

LEGEND

Contour Interval

5 Units

20 Units

VLF-EM Conductor

WHITE CHANNEL RESOURCES INC.

VLF-EM Fraser Filter Contours

NPM, Lualualei, Hawaii

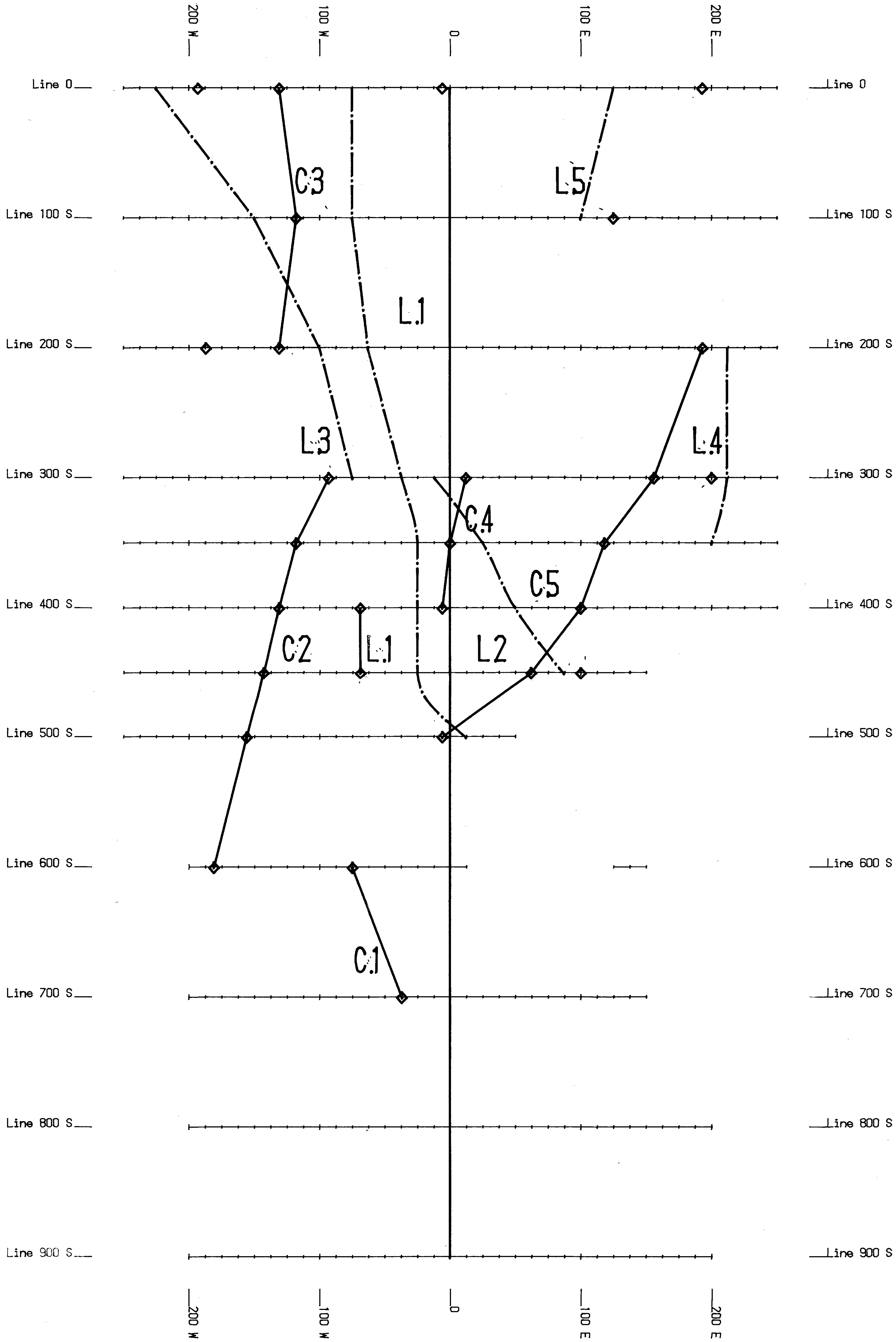
SILVER CROWN SHOWING - STRIKE 2 CLAIM

NTS: 104 A/4,5 Skeena Mining Division, B.C.

Figure # G-2 October, 1989

Surveyed by Ashworth Explorations Limited

Interpretex Resources Ltd. Map No. 8



Scale 1:2500

25 0 25 50 75 100 125 (metres)

GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,747

LEGEND

C2 VLF-EM Conductor

L3 Magnetic Lineament

WHITE CHANNEL RESOURCES INC.

Geophysical Interpretation Map

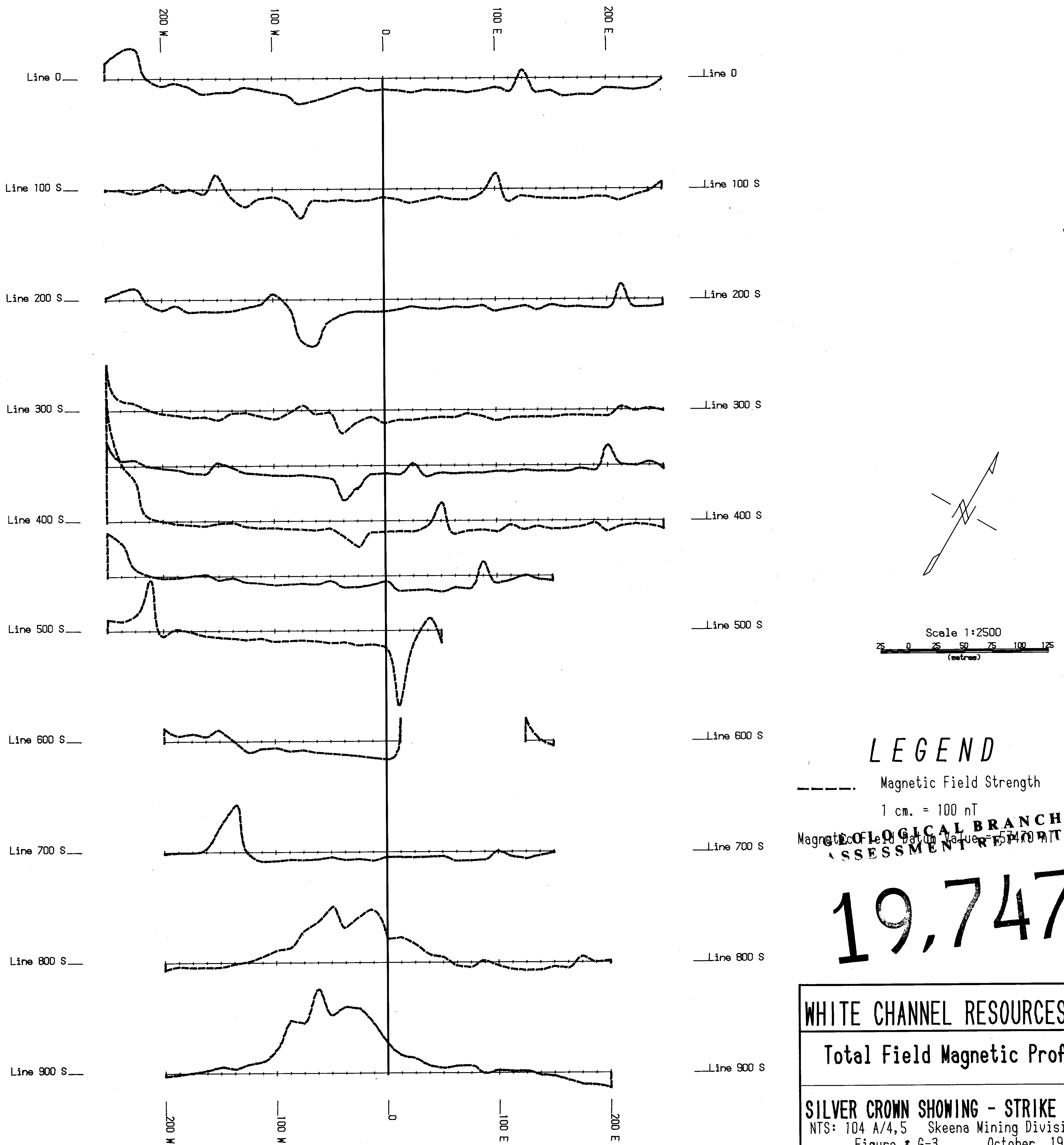
SILVER CROWN SHOWING - STRIKE 2 CLAIM

NTS: 104 A/4,5 Skeena Mining Division, B.C.

Figure # G-5 October, 1989

Surveyed by Ashworth Explorations Limited

Interpretex Resources Ltd Map No. 9



LEGEND

Magnetic Field Strength

1 cm. = 100 nT

Magnetic Field Datum Value = 57470 nT

GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,747

WHITE CHANNEL RESOURCES INC.

Total Field Magnetic Profiles

SILVER CROWN SHOWING - STRIKE 2 CLAIM

NTS: 104 A/4,5 Skeena Mining Division, B.C.
Figure # G-3 October, 1989
Surveyed by Ashworth Explorations Limited

Interpretex Resources Ltd. Map No. 10