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GEOLOGICAL, GEOCHEMICAL AND GEOPHYSICAL

ASSESSMENT REPORT

ON THE

WIN CLAIM GROUP

NORTHERN VANCOUVER ISLAND

BRITISH COLUMBIA, CANADA

NTS 92L/12

Latitude: 50°44'N

Longitude: 127°57'W

For

Essex Resource Corporation
1260 - 400 Burrard Street
Vancouver, B.C.
V6C 3A6

By

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and

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February 15, 1990

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SUMMARY

The Win property was evaluated by mapping, stream sediment and geochemical soil sampling and trenching in areas of previously noted sulphide mineralization in January 1990 by Daiwan Engineering Ltd.

During the program 640 soil samples, 72 rock samples, 4 pan concentrates and 1 silt sample were collected The property was mapped on a scale of 1:5000. Locally more detailed information was collected by trenching across mineralized zones.

The property is located on northern Vancouver Island, approximately 360 kilometres (225 miles) northwest of Vancouver, British Columbia, Canada. The claim group covers a 5 kilometre stretch of ground west of Nahwitti Lake on N.T.S. topographic map 92L/12W. All areas of the property can be reached by well maintained logging roads and forest tracks.

The Win claim group is underlain by volcanics and sediments of the Karmutsen, Quatsino, Parson Bay, and Bonanza formations. The rocks are intruded by at least four distinct phases of intrusives. The attitudes of the rocks are generally northwest striking, southwest dipping except where the bedding has been disrupted by the intrusives and the northwest and northeast trending late stage faults.

Four different styles of base and precious metal mineralization were observed on the property. They include auriferous zinc metasomatic replacement, semi-massive copper-zinc sulphide veins, auriferous quartz veins and copper bearing intrusive. Each of these styles of mineralization have been found on other properties in the surrounding district.

The exploration program conducted in 1990 was successful in defining numerous targets for follow-up work. The geochemical survey outlined new exploration targets and supported the information obtained from earlier surveys.

A two phase program, including infill geochemistry and drilling, is proposed for followup work on this property. Phase I is budgeted at $135,000, phase II, contingent upon the success of Phase I, is budgeted at $165,000.

INTRODUCTION

At the request of Mr. Michael Foley, President of Essex Resource Corporation, Daiwan Engineering Ltd. conducted an exploration program on the Win Group claims near Port Hardy B.C. The program consisted of geological mapping, stream sediment sampling and geochemical soil sampling in areas of previously noted sulphide mineralization.

During the program 640 soil samples, 72 rock samples, 4 pan concentrates and 1 silt sample were collected, and the property was mapped on a scale of 1:5000. Locally more detailed information was collected by trenching across mineralized zones.

This report is a description of work completed on the property between December 15, and February 15, 1990 and a compilation of previous reports of work in the area.

LOCATION AND ACCESS

The Win property is located on northern Vancouver Island, approximately 360 kilometres (225 miles) northwest of Vancouver, British Columbia, Canada (Figure 1). The claim group covers a 5 kilometre (2.5 mile) stretch of ground west of Nahwitti Lake on N.T.S. topographic map 92L/12W (see Figures 1 & 2). All areas of the property can be reached by well maintained logging roads and forest tracks.

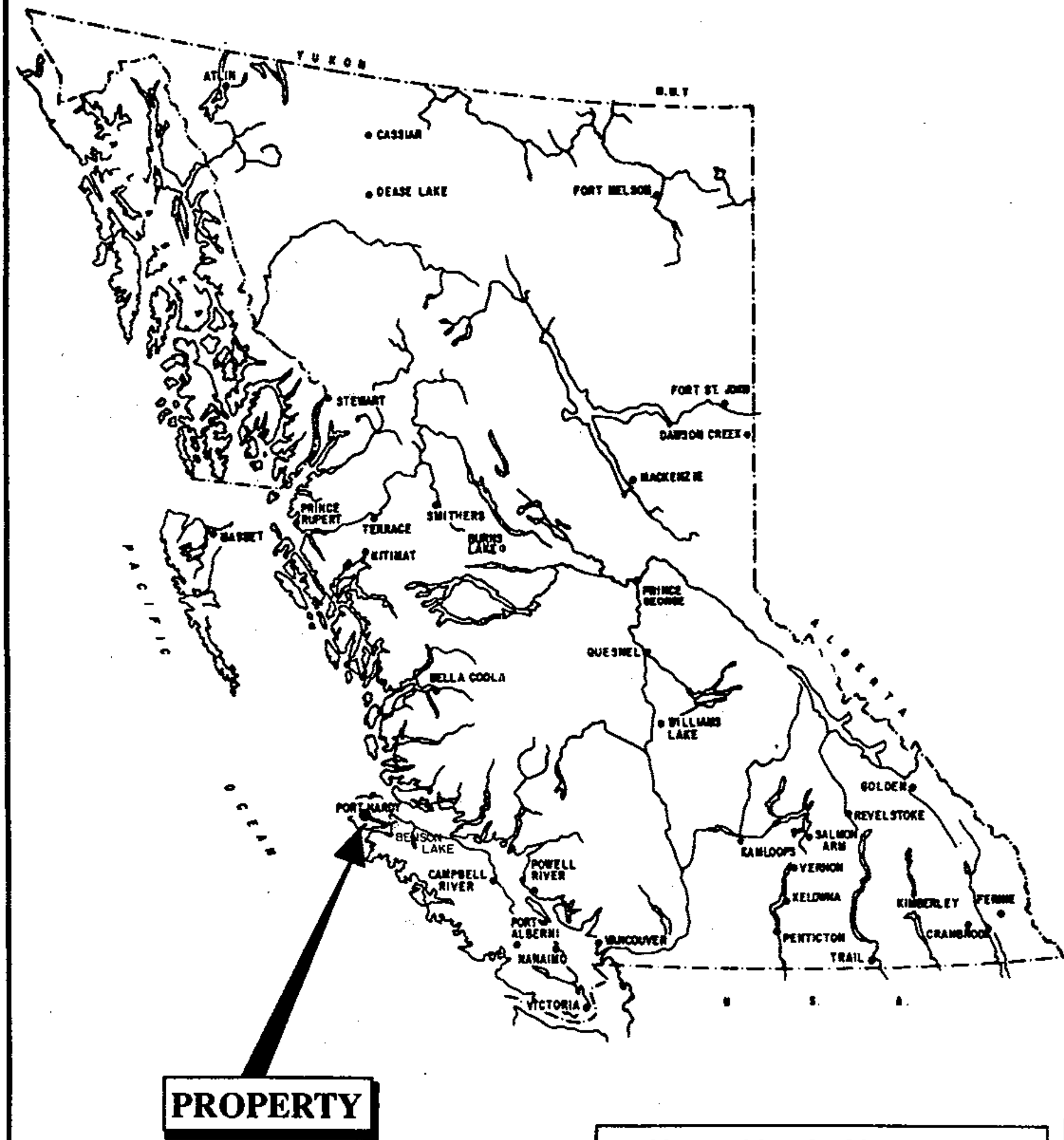
The main access to the claim block is by road "NE66" which leaves the Holberg-Port Hardy road at a point 13.5 road kilometres from Holberg. Access to the east end of the block is by the Nahwitti River logging road system (See Figure 2).

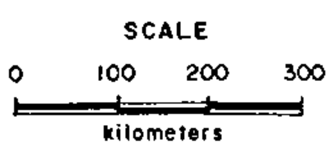
Regular Dash 7 air service is provided by both Canadian Airlines and Time Air from Vancouver to Port Hardy, each on a twice daily schedule. Alternately, there is good highway access, with travel from Vancouver taking 7 hours.

Port Hardy is the local commercial centre, but there are forestry and fishing centres at Coal Harbour and Holberg.

PHYSIOGRAPHY AND CLIMATE

The property is characterized by many low, northwest to westerly trending hills and ridges bounded by narrow deeply incised valleys and steep slopes. Elevations range from sea level to over 650 metres (2,000 ft). Within the claim block ridge tops are commonly about 300 metres (1,000 ft) above valley bottom. The property is within N.T.S. topographic map 92L/12W.





ESSEX RESOURCE CORPORATION		
WIN PROPERTY NANAIMO MINING DIVISION, B.C.		
LOCATION MAP		
DAIWAN ENGINEERING LTD.		
SCALE As Shown	DATE Jan., '90	FIG. 1

The claims are located within an active logging area, consequently forest cover varies from mature stands of fir, hemlock, spruce and cedar to dense second growth or to open clear-cut areas of recent logging. Low areas, especially along creeks are swampy and have thick brush and berry bushes.

Thick humus development on the forested slopes and scattered residual glacial gravels in the valley bottoms can restrict geological mapping in these areas. Rock exposure is limited to road cuts and well scoured creeks.

The area is characterized by warm summers and mild winters. Snowfall in winter is limited to the higher elevations and exploration can usually continue year round.

PROPERTY

The property consists of 11 contiguous mining claims totalling 41 units within the Nanaimo Mining Division. The claims were staked as "Win, Helper, and Helper 1, 2," claims. Additional claims LOD 1-7 were staked during course of the program. The claims are all recorded in the name of Daiwan Engineering, and are held in trust for Agilis Exploration who has optioned the property to Essex Resource Corporation. Particulars are as follows:

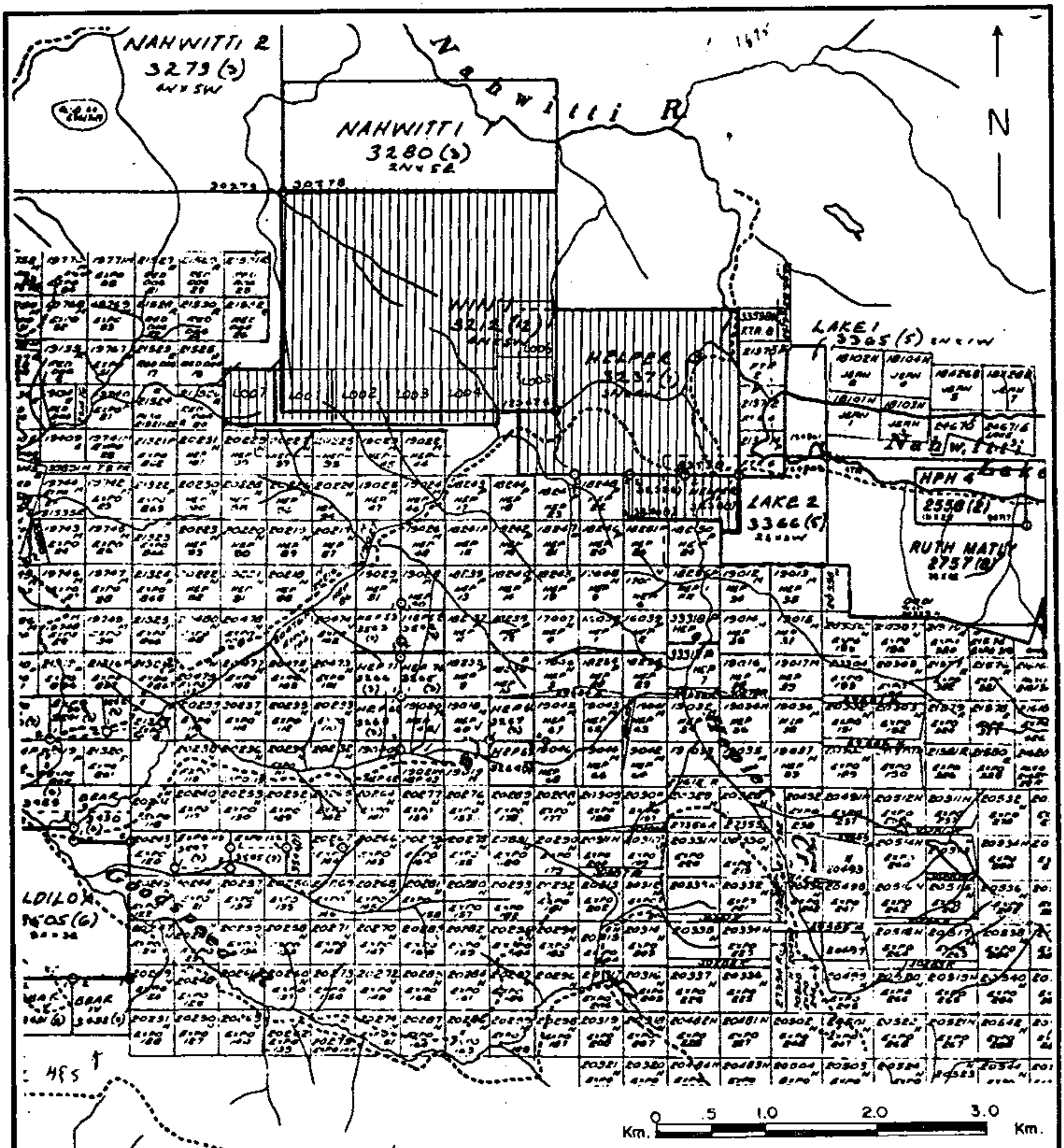
Claim	Rec. No.	Units	Expiry Date
LOD 1-7	3674-80	7	January 16, 1991
Win 1	3212	20	December 9, 1989
Helper	3237	12	January 31, 1991
Helper 1	3694	1	February 3, 1991
Helper 2	3695	1	February 3, 1991

The Win claim is slightly misplotted on the government claim map, Figure 2. The additional Lod claims were staked to cover any fractions which occurred as a result of the misplotting. The Helper 1&2 claims were restaked for assessment purposes.

HISTORY

Northern Vancouver Island has been intermittently explored since the early 1800s. Copper was discovered in 1911 at Benson Lake, 25 miles southeast of Port Hardy. This property, known as Coast Copper Mine, was acquired by Cominco in 1916. They carried out considerable underground development work, but closed in 1931, remaining idle until 1960. It was then actively mined from 1962-72 producing copper and iron concentrates which were shipped to Japan.

Magnetite occurrences were located in the Benson Lake area in 1897 but were considered of



ESSEX RESOURCE CORPORATION

WIN PROPERTY

NANAIMO MINING DIVISION, B.C.

CLAIM MAP

NTS 92L/12W

DAIWAN ENGINEERING LTD.

SCALE	DATE	FIG.
As Shown	Jan., '90	2

90-100-2-a

interest only for their copper content until the early 1950s. They were explored for their iron content between 1950-56, then mined until 1967, when the operation ceased. Iron concentrates were shipped to Japan.

In 1963, the B.C. Department of Mines published the results of a recently completed aeromagnetic survey covering the northern end of Vancouver Island.[2] Since magnetite deposits were of interest at this time, considerable exploration activity was generated in the area examining all magnetic anomalies of interest.

One magnetic anomaly of fairly large areal extent was recorded on the eastern end of Rupert Inlet. Diligent prospecting in this area located a number of poorly exposed copper occurrences. A large number of claims were located in 1966 and subsequently the property was acquired by Utah Construction and Mining Company, now BHP-Utah Mines Ltd. Over the years, they added to the claim block and conducted extensive geological-geochemical-geophysical surveys and diamond drilling throughout the property. This work resulted in locating the large copper-molybdenum deposit which was developed into the Island Copper Mine. The mine commenced production in October 1971. Production to 1987 has been in excess of 200 million tonnes milled, for concentrate sales of 753,000 tonnes of copper, 23.1 million grams gold, 168 million grams silver, and 15.3 tonnes molybdenum[14].

With the discovery of significant copper mineralization on the Utah property, a great deal of interest was generated in the area by individuals and companies searching for copper. Many copper occurrences were located but none were found to be economic at the time.

During the height of the exploration activity, Utah Mines Ltd. controlled most of the ground extending from the east end of Rupert Inlet to the west end of Holberg Inlet. The Win claims were at this stage located as the Ti, Bud, Mo, and Mon claims, immediately adjacent to the Utah Mines landholdings. The Utah Mines properties included the large block of claims covering the Island Copper deposit, as well as the Bonanza, Karmutsen, and Quatsino rocks to the northwest. Exploration on these claims in 1968-74 located a large area of low grade copper-molybdenum mineralization in the Bonanza volcanics (the Hushamu zone) estimated to contain 58,420,000 mineable tonnes grading 0.32% Cu, 0.008% Mo and 413 ppb gold. The drill indicated reserve for the deposit is over 100 million tonnes at the same grade. It is presently being evaluated for open pit mining by Moraga Resources Ltd.

A number of other alteration zones, similar to that at Island Copper Mine and the Hushamu zone, also exist adjacent to the Win claim. Among these are the Red Dog and the Hep deposits, located one kilometres west and one kilometre south of the Win property respectively.

Previous Work and Interpretations

Work on what is now the Win Group dates back to 1966 when Giant Explorations Ltd. examined a mineral occurrence (Aban showing) owned by G. Milbourne. The showing was reported as a skarn within the Quatsino limestone mineralized with sphalerite and galena. Three chip samples were taken and assays returned values of: 1.81% zinc, 0.97% lead and 0.06 oz/ton silver over 2.4 metres (8 feet); 2.78% zinc, 0.36% lead and 0.06 oz/ton silver over 3.05 metres (10 feet); and 1.71% zinc, 0.25% lead and 0.06 oz/ton silver over 1.83 metres (6 feet). No further work has been reported on this showing.

In 1968, Acheron Resources Ltd. began work on the TI, Mo, Mon, and Bud claims (now the Win 1, Nawhitti 1 and Lod 1-7 claims) located west of the Aban showing. Acheron explored the claims intermittently from 1968 through 1976 when the claims were abandoned. Work consisted of detailed geochemical and geophysical surveys and geological mapping. A compilation of work conducted by Acheron is shown on Figure 4. The geochemical survey produced several copper and zinc targets for additional work.

Copper anomalies with values in excess of 100 ppm occur along the, now recognized, contact between a large diorite intrusive body with the Karmutsen volcanics. A sample of diorite float collected from a creek in this area assayed 0.1% copper and 5.14 g/t silver. An additional soil copper anomaly was outlined in the southwest corner of the current claim group but no further work was completed. This anomaly occurs in an area where diorite is now known to intrude Bonanza volcanics.

A large zinc anomaly was outlined in the center of the current Win claim. Hand trenching in 1973 and 1974 exposed zinc skarn within the Quatsino limestone. Samples of this zone (trench 2) taken in 1975 showed zinc mineralization with values of 3.72% and 3.97% zinc over 4.9 and 2.5 metres (16 feet and 8 feet). Trench 3 produced 6.02% zinc over a 4.9 metre (16 feet) width. A grab sample from trench 4 assayed 5.40% zinc.

The magnetometer surveys conducted in 1968 and 1970 outlined a small magnetics high adjacent to the zinc anomaly. This magnetics high corresponds to a small diorite intrusive. Another well defined magnetics high, with adjacent sharp low, occurs in the area of the copper soil anomalies. Mapping now shows this to represent the contact zone between diorite and the Karmutsen volcanics.

Since 1975 no significant work has been completed on the claims although they have been staked periodically.

REGIONAL GEOLOGY

Vancouver Island, north of Holberg and Rupert Inlets, is underlain by rocks of the Vancouver Group. These rocks range in age from Upper Triassic to Lower Jurassic. They are intruded by rocks of Jurassic and Tertiary age and disconformably overlain by Cretaceous sedimentary rocks. Figure 3 shows the regional geological mapping of the northern part of the Island.

Faulting is prevalent in the area. Large-scale block faults with hundreds to thousands of metres of displacement are offset by younger strike-slip faults with displacements up to 750 metres (2,500 feet).

The Vancouver Group is described as follows:

(a) Basal Sediment - Sill Unit: Middle and Upper Triassic Age

The basal sediment-sill unit consists of laminated to graded-bedded black shales and siltstones, silicified and invaded by diabase sills. The entire unit is estimated as 750-900 metres (2,500-3,000 feet) with the sedimentary portion being about 180 metres (600 feet) thick.

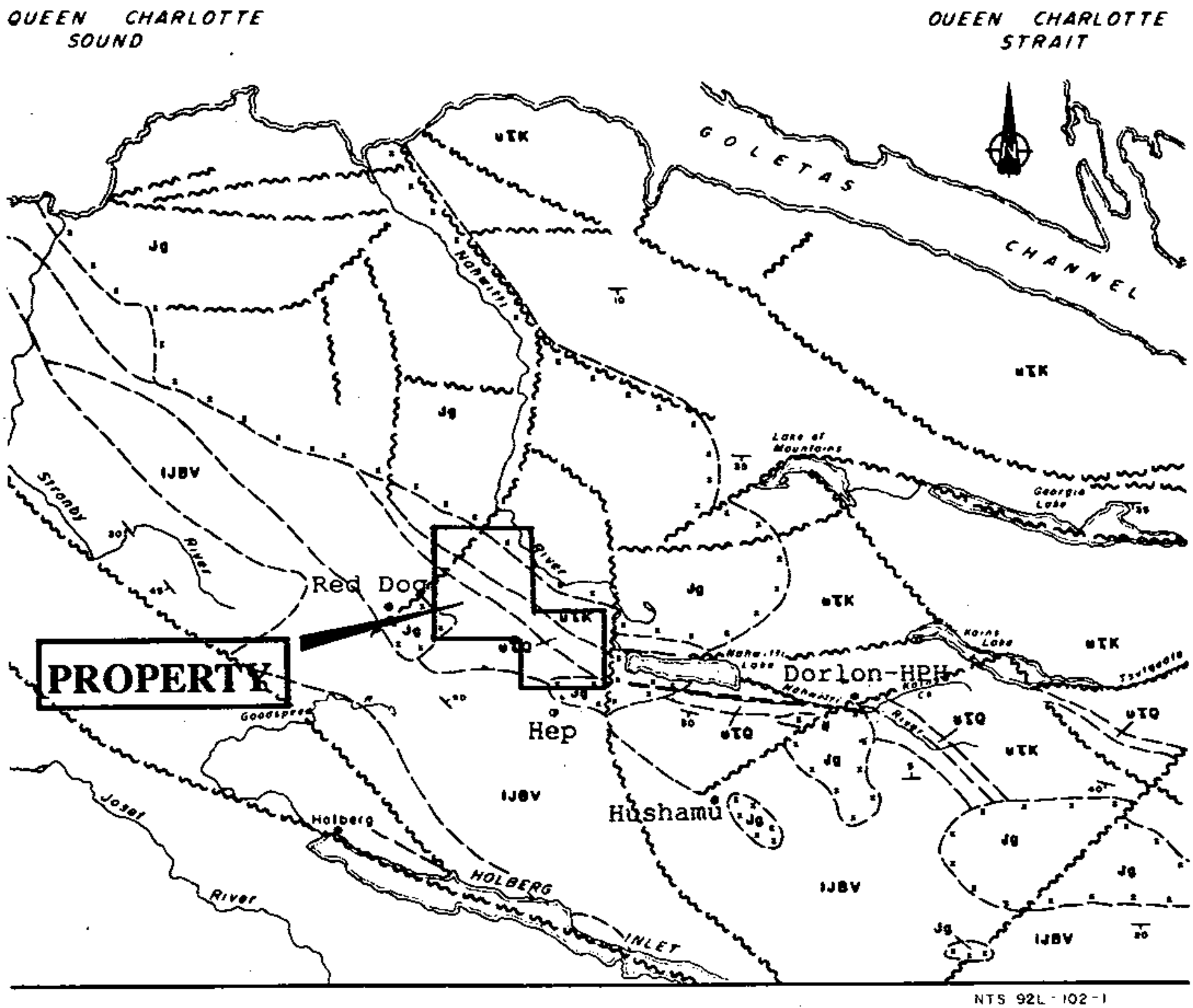
(b) Karmutsen Formation: Upper Triassic Age

Karmutsen Formation consists of 3,000-6,000 metres (10-20,000 feet) of volcanic flows, pyroclastics and minor sediments. It includes three distinct units: a lower pillow lava unit, a middle pillow breccia unit, and an upper lava flow unit. The latter consists of predominantly porphyritic and amygdaloidal basalt flows, individual flows of which range from 1-30 metres (to 100 feet) thick.

Two thin bands of limestone occur near the top of the Karmutsen Formation. The distribution of limestone outcrops is erratic and suggests a series of lenses at the same general stratigraphic horizon rather than one continuous bed.

The lower contact of the formation has not been observed on the northern part of Vancouver Island. The upper contact with limestone of the Quatsino Formation generally is sharp and easily recognized, although limestones and basalt locally are interbedded over a narrow stratigraphic interval at this contact.

Low-grade metamorphism of the Karmutsen Formation rocks has resulted in pervasive chloritization and amygdules filled with epidote, carbonate, zeolite, prehnite, chlorite, and quartz.



LEGEND

JURASSIC

Jg	ISLAND INTRUSIONS: quartz diorite, granodiorite, quartz monzonite, quartz feldspar porphyry.

LOWER JURASSIC (BONANZA GROUP)

IJBV	Andesitic to rhyodacitic lava, tuff, breccia.

TRIASSIC–UPPER TRIASSIC (VANCOUVER GROUP)

uTQ	QUATSINO FORMATION: limestone.
uTK	KARMUTSEN FORMATION: basaltic lava, pillow lava, breccia, aquagene tuff, greenstone; minor limestone.

SYMBOLS

— — Geological Boundary.

〰 〰 Fault, Lineament (approximate)

┴ Bedding.

SCALE

0 2 4 6 8 10

kilometers

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REGIONAL GEOLOGY		
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SCALE As Shown	DATE Jan.,'90	FIG. 4

90-100-4-a

Basaltic rocks along contacts with intrusive stocks are in many places converted to dark-coloured hornblende hornfels. Skarn zones occur sporadically along these contacts, both in the inter-lava limestones and in the basalts.

(c) Quatsino Formation: Upper Triassic Age

The Quatsino Formation ranges from 60-1,000 metres (200-3,500 feet) in thickness and consists almost entirely of limestone with a few thin andesite or basalt flows. It has conformable contacts with both the overlying Parson's Bay sediments and the underlying Karmutsen volcanics. The upper contact with the Parson's Bay Formation is gradational with limestone grading upward into carbonaceous argillites.

Within the contact metamorphic/metasomatic aureoles adjacent to intrusive stocks, skarn development and silicification of limestone, accompanied by chalcopyrite-magnetite or galena, sphalerite and silver mineralization has been noted.

(d) Parson's Bay Formation: Upper Triassic Age

The Parson's Bay Formation consists of between 60-360 metres (200-1,200 feet) of argillite, minor limestone, agglomeratic and tuffaceous limestone, tuff, quartzite and minor conglomerate. At both its base and top, the unit exhibits gradational contacts with the Quatsino and Harbledown Formations.

On a regional scale, the rocks are unmetamorphosed. Locally, adjacent to intrusive contacts, pyrite-magnetite replacement bands up to one-half inch thick in banded tuffs have been observed.

(e) Harbledown Formation: Lower Jurassic Age

The Harbledown Formation consists of 485 metres (1,600 feet), a non-volcanic argillite-greywacke sequence separating the Parson's Bay from the Bonanza Formation.

(f) Bonanza Formation: Lower Jurassic Age

The Bonanza Formation is approximately 1,500 metres (8,500 feet) thick. The lower portion consists of bedded and massive tuffs, formational breccias and rare amygdaloidal and porphyritic flows, in the compositional range andesite to basalt. Porphyritic dykes and sills intrude the lower part of the unit. In the upper part of the Bonanza, rhyodacite flows and breccias become more numerous and are interbedded with andesite and basalt flows, tuffs and tuff breccias.

Regional metamorphism within the Bonanza Volcanics is very low grade, possibly zeolite facies.

Plagioclase commonly is albitized and saussuritized. Chlorite, epidote and laumontite occur within the matrix of volcanic breccias, in veinlets, and in amygdules. Coarse intraformational breccias locally are hematized.

Biotite and amphibolite hornfelses occur adjacent to stocks which intrude the Bonanza Volcanics.

"Pyrobitumen", a black hydrocarbon erratically distributed within the Bonanza rocks, generally occurs as fracture fillings or in the centre of zeolite-carbonate veins. Its distribution is not related to the position of the intrusive stocks.

Cretaceous Sediments

The Vancouver Group is unconformably overlain by non-marine Cretaceous sediments of the Longarm Formation which are estimated to be about 300 metres (1,000 feet) thick in the Port Hardy area. These sediments, consisting of conglomerate, sandstone, greywacke, and siltstone and some carbonaceous and impure coal seams, occupy local basins. Early coal mining in the district was from several of these basins.

Intrusive Rocks

The Vancouver Group rocks are intruded by a number of Jurassic-aged stocks and batholiths. In the Holberg Inlet area a belt of northwest-trending stocks extend from the east end of Rupert Inlet to the mouth of Stranby River on the north coast of Vancouver Island[15].

Quartz-feldspar porphyry dikes and irregular bodies occur along the south edge of the belt of stocks. Dykes are characterized by coarse, subhedral quartz and plagioclase phenocrysts set in a pink, very fine grained, quartz and feldspar matrix. They are commonly extensively altered and pyritized. At Island Copper Mine, these porphyries are enveloped by altered, brecciated, mineralized Bonanza sequence wallrocks. The porphyries, too, are cut by siliceous veins, pyritized, extensively altered, and are mineralized with copper where they have been brecciated. The quartz-feldspar porphyries are thought to be differentiates of middle Jurassic, felsic, intrusive rocks.

Structure

The structure of the rocks north of Holberg and Rupert Inlets is that of shallow synclinal folding along a northwesterly fold axis. The steeper southwesterly limbs of the folds have apparently been truncated by faults roughly parallel to the fold axis. Failure of limestone during folding may have influenced the location of some of the faulting as indicated by the proximity of the Dawson and Stranby River Faults to the Quatsino horizon. Transverse faulting is pronounced and manifested by numerous north and northeasterly trending faults and topographic lineaments.

The northern part of Vancouver Island lies in a block faulted structural setting with post Lower Cretaceous northwesterly trending faults apparently being the major system (Figure 3). This system causes both repetition and loss of parts of the stratigraphic section, with aggregate movement in a vertical sense in the order of tens to hundreds of metres. The most significant of these fault systems trends west to northwest following Rupert and Holberg Inlets. Near the west end of the Holberg Inlet it splits with the main branch following the Holberg Inlet, the other branch passing through the west side of the Stranby Valley. Another northwesterly to westerly system passes through William Lake and still another smaller system passes through Nahwitti Lake.[6]

Northeasterly trending faults comprise a subordinate fault system. In some cases, apparent lateral displacement, in the order of a several hundred metres, can be measured on certain horizons. Movement, however, could be entirely vertical with the apparent offset resulting from the regional dip of the beds.

Recent computer modelling of the airborne magnetometer data has provided a very clear understanding of the relationship of secondary conjugate sets of northeast and northwesterly faults related to the major west-northwest trending breaks.[7] These conjugate fault sets appear to relate directly to the significant mineralization at the Island Copper, Hushamu, Hep and Red Dog copper/gold deposits.

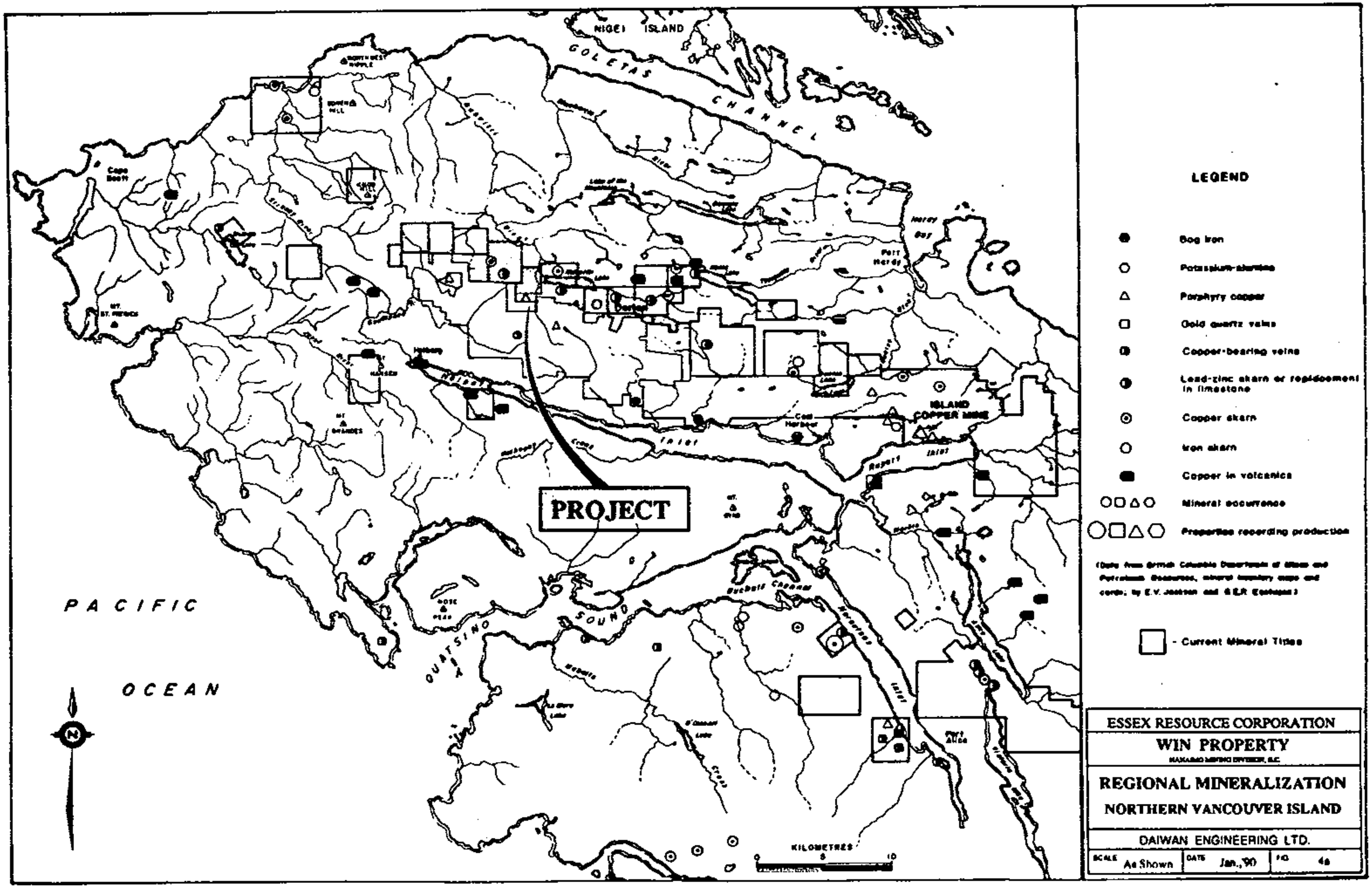
Generally, regional dip of the bedding is gentle to moderate southwesterly. Locally, in the area west of Holberg, dips are much steeper, but these are in close proximity to major faults. There is little folding or flexuring of bedding visible, except along loci of major faults where it is particularly conspicuous in thinly bedded sediments of Lower Bonanza. Bedding is generally inconspicuous in massive beds of Karmutsen, Quatsino and Bonanza rocks, particularly inland where outcrops are widely scattered.

REGIONAL MINERALIZATION

A number of types of mineral occurrences are known on Northern Vancouver Island. These include:

1. Skarn deposits: copper-iron and lead-zinc skarns

2. Copper in basic volcanic rocks (Karmutsen): in amygdules, fractures, small shears and quartz-carbonate veins, with no apparent relationship to intrusive activity


NIGEI ISLAND
GOLETAS CHANNEL
PACIFIC
OCEAN
PROJECT
ISLAND COPPER MINE
Port Hardy
Hardy Bay
Coal Harbour
Holberg
Rupert Inlet
Holberg Inlet
QUATSINO SOUND
Cape Scott
KILOMETRES
0
5
10
N
LEGEND
Bog iron
Porphyry copper
Gold quartz veins
Copper-bearing veins
Lead-zinc skarn or replacement in limestone
Copper skarn
Iron skarn
Copper in volcanics
Mineral occurrence
Properties recording production
- Current Mineral Titles
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DATE Jan.,'90
FIG. 4a

3. Veins: with gold and/or base metal sulphides, related to intrusive rocks

4. Porphyry copper deposits: largely in the country rock surrounding or enveloping granitic rocks and their porphyritic phases.

Two significant discoveries on ground adjacent to the Win property illustrate the copper mineralization in the area:

The Hep claims which border the Win property to the south hosts an estimated 43,350 tonnes grading 0.80% copper at the intersection of two shear zones. The Hep claims are underlain by andesites and tuffs of the Bonanza Group which is intruded by quartz monzonite. Propylitic alteration is most common, but argillic and silica alteration occurs along fractures and adjacent to the volcanic-intrusive contacts. Pyrite with chalcopyrite and lesser bornite occurs along fractures and as fine disseminations within the andesite.

The Red Dog deposit is located 2 kilometres west of the Win property. Tuffs and tuff breccia of the Bonanza Group are intruded by diorite, quartz diorite, and quartz-feldspar porphyry of the island intrusions. The tuffs have been altered to hornblende biotite hornfels in contact zones with silicification and hydrothermal alteration in shear zones. Chalcopyrite occurs as fine grained disseminations in the hornfels and in association with magnetite in siliceous breccia. Reserves are reported to be in excess of 45,359,000 tonnes grading 0.32% copper and 0.41 grams/tonne (.012 opt) gold.

Several showings around Nahwitti Lake, 3 kilometres east of the property, have been reported. These occurrences show significant zinc-gold mineralization near the transitional contact between Quatsino limestone and Bonanza group volcanics:

The Dorlon prospect includes three areas of mineralization within a 250 metre radius; the Zinc Vein, the Nose Showing, and the Shaft Showing.

The Zinc vein consists of sphalerite stringers up to 0.5 metres wide and 6.0 metres long striking north and dipping vertically. These stringers occur in silicified limestone adjacent to a felsic dyke. A 0.61 metre chip sample collected in 1966 assayed 19.2 grams/tonne (0.560 opt) gold, 24.0 g/t (0.701 opt) silver and 28.35% zinc. Channel samples of up to 0.30 metres returned values up to 18.49 g/t (0.54 opt) gold and 33.60% zinc.

The Nose showing consists of a 0.25 to 0.75 metre zone of massive sphalerite along a bedding plane in limestone. Trenching and drilling showed the mineralization to be gold bearing. A 2.0 metre chip sample assayed 4.18 g/t (0.122 opt) gold and 17.37% zinc, and grab samples of the massive sphalerite assayed up to 8.63 g/t (0.252 opt) gold and 32.19% zinc.

The Shaft showing consists of massive sphalerite within a breccia zone in limestone near a siliceous intrusive. A 1.6 metre channel sample assayed 10.31 g/t (0.301 opt) gold and 22.64% zinc, a 0.6 metre channel sample assayed 15.41 g/t (0.450 opt) gold and 29.63% zinc, grab samples assayed up to 14.79 g/t (0.432 opt) gold and 32.14% zinc.

The HPH is a further prospect which covers three showings of galena-sphalerite-silver mineralization. The first is a skarn within the Quatsino limestone adjacent to a felsic dyke. It is 3 metres wide and has been outlined along a strike length of 80 metres. Two shafts and one adit have been driven in the mineralization, which consists of galena and sphalerite with minor chalcopyrite, magnetite, pyrite and pyrrhotite. A 2.0 metre chip sample from the east wall of the east shaft assayed 3743.4 g/t (109.31 opt) silver, 38.1% lead and 10.6% zinc.

Galena and sphalerite stringers in silicified limestone near the contact with Karmutsen formation andesites assayed 267.4 g/t (7.81 opt) silver, 3.9% zinc, and 9.24% lead across 1.5 metres, and other areas of galena, sphalerite pyrite and sparse chalcopyrite mineralization in silicified Quatsino limestones occur near the contact with Bonanza Group volcanics.

The HPH and Dorlon prospects are managed by Hisway Resources Corp. and Silver Drake Resources Ltd.

PROPERTY GEOLOGY

The Win claim group is underlain by volcanics and sediments of the Karmutsen, Quatsino, Parson Bay, and Bonanza formations. The rocks are intruded by at least four distinct phases of intrusives. The attitudes of the rocks are generally northwest striking, southwest dipping except where the bedding has been disrupted by the intrusives and the northwest and northeast trending late stage faults.

A description of the various formations encountered on the property is as follows:

The Karmutsen volcanics consists of aphanitic to porphyritic, dark green to black basalts and andesites. This unit trends northwest and is intruded by a large diorite batholith from the northeast. Near the contact with the intrusive, the volcanics contain abudant finely disseminated magnetite. The Karmutsen basalts are conformably overlain by the Quatsino limestones in the southeast portion of the claims. A major northwest trending fault is the upper contact in the northwest portion of the property.

The Quatsino formation consists of medium bedded to massive dark grey to black limestone. The limestone has been recrystallized near the contact with a small diorite plug. The limestone has been altered to a epidote-garnet to actinolite-garnet skarn with abundant sphalerite and pyrite.

Interbedded with the limestone at various locations on the property is a feldspar crystal tuff. The crystal tuff is highly siliceous with up to 2% disseminated pyrite. Beds range in thickness from a few centimetres to tens of metres.

The Parson Bay formation overlays the limestone and consists of very siliceous argillites, shales, and tuffs. These sediments are generally thin bedded, with andesitic flows (crystal tuffs?) interbedded. These sediments and volcanics outcrop in the southwest portion of the property. The sediments display northwest strikes and moderate southwesterly dips. The bedding has been disturbed adjacent to faults. The argillites and tuffs contain disseminated pyrite and are highly rusted and enriched with pyrite adjacent to the late stage faults.

Overlaying the Parson Bay sediments and outcropping in the extreme southwest portion of the property are andesites of the Bonanza Formation. The andesites exhibit varying degrees of alteration, depending on their proximity to faults and the intrusive bodies. Adjacent to the diorite intrusions the volcanics are highly siliceous and have abundant quartz stringers and magnetite disseminated throughout. Adjacent to faults the andesites display argillic alteration and areas with potassium feldspar alteration of stringers.

Intruding the volcanics and sediments are at least four distinct phases of intrusions. A large diorite batholith extends onto the property from the northeast. This diorite is medium grained and relatively unaltered. Fracture density ranges from low to moderate near faults and is blocky with no significant alteration. Only trace pyrite was noted in this diorite. The diorite is in contact with the Karmutsen basalts and probably influences the disseminated-magnetite in the basalts along the northwest-southeast contact zone.

Three outcrops of diorite occur near the contact of the limestone with the Parson Bay sediments. These plugs are dioritic in composition and may be related to the large batholith in the northeast. The pluton in the center of the Win claim has introduced zinc, copper, lead and gold mineralization into the limestone.

A large granodiorite pluton outcrops on the property in the southeast. The granodiorite is pink, potassium feldspar rich and medium grained. Alteration consists of potassium feldspar alteration of the stringers throughout the intrusive. The granodiorite is in fault contact with the limestone in the southeast corner of the claims. The fault is marked by a sharp topographic break and the lack of alteration in the limestone.

The third intrusive observed on the property is on the western edge, it consists of a quartz diorite that intrudes the sediments. The quartz-diorite is fine grained with quartz and feldspar phenocrysts in a dark green ground mass.

The fourth intrusives are the mafic dykes that cut the property. These dark green dykes are generally very weathered and appear controlled by late stage northeast and northwest trending faults.

MINERALIZATION

Four different forms of potential base and precious metal mineralization were observed on the property. They include - metasomatic replacement, semi-massive sulphide veins, quartz veins and copper bearing intrusive.

In the centre of the Win claim, near the upper contact of the limestone adjacent to a diorite intrusive is a sulphide replacement zone. In previous surveys in 1968 & 1975 the "skarn" was described as being up to 30 metres wide and 210 metres long[18]. The mode of occurrence of the zinc rich replacement zone is similar to that reported on the Dorlon-HPH property. There zinc-silver and gold mineralization occurs in the limestone, with the siliceous Parson Bay sediments acting as a barrier to the solutions. On the Win claim samples of up to 8.59% zinc and 0.22% copper over 1.5 metres and 3.60% zinc, and 1.99 g/tonne (0.058 opt) gold over 1.0 metres were obtained from the zone. It is postulated that the zone of replacement will continue down dip along the contact. Grades and widths will vary down dip and should be tested with drilling. Figures 8 and 9 in the appendix show an interpreted cross-section.

Approximately 400 metres east of this skarn a large semi-massive sulphide vein occurs within the margin of a diorite plug. The vein strikes northeast (010°-050°) and dips southeast at 50°-60°. The vein is offset right laterally by 20 metres along a north west trending fault. The vein is up to 1.5 metres wide and varies in composition from footwall to hanging wall. Three adjacent samples across the various zones of the vein assayed 10.80% zinc, 0.93% copper, 0.36% lead, 15.60 g/tonne (0.455 opt) silver, and 0.137 g/tonne (0.004 opt) gold across 1.5 metres. Figure 10 in the Appendix is a sketch of the pit in which the vein was uncovered. Drill holes have been proposed to explore the extent of the vein and to check for parallel systems.

Locally derived quartz vein float was found in two areas of the claims. The first area was along logging road NE66 in the south of the Win claim, and consisted mainly of quartz with coarse crystal growth in small vugs. There was trace gold (62ppb) in the sample.

The second area of quartz veining was 500 metres south of the skarn zone, near line 4+50E at 3+00N. Here the vein material consisted of banded quartz-amethyst with trace disseminated pyrite cut by magnetite veining. It was found adjacent to a mafic dyke. Trenching removed the vein material, but indicated that the quartz and amethyst may form irregular pods and stringers alongside the dyke. The geochemical surveys conducted in 1968 and 1990 outlined a zinc anomaly in the area of the float. In the recent work soils showed anomalous zinc and weak gold (11 & 22 ppb Au). Samples of the vein material assayed up to 150 ppb Au, gold grades may increase at depth or along strike and additional work should be completed to trace the veining.

Two areas on the claims have geology favourable for "porphyry" copper-gold deposits similar to the Hushamu and Red Dog deposits. The first is along the eastern boundary of the Win claim where the Karmutsen volcanics have been intruded by a large diorite batholith. The geochemical survey conducted in this area in 1968 defined a large copper anomaly with values up to 184 ppm (see Figure 3). A sample of diorite float from one of the creeks assayed 0.1% copper and 5.14 g/tonne (0.15 opt) silver (no gold value was reported). Further work is necessary in the area to expose outcrop. Two drill holes have been proposed (see Figures 8 and 9 in Appendix 3).

At the second area, in the southwest corner of the claims, the Bonanza volcanics are intruded by diorite with disseminated pyrite, chalcopyrite and molybdenite. The andesites are highly siliceous with fine quartz stringers and disseminated pyrite and magnetite. Rock samples collected in this program showed elevated copper and molybdenum with values ranging up to 281 ppm copper and 44 ppm molybdenum. Follow up work in this area is recommended and should consists of grid extension and a geochemical survey.

SURVEY RESULTS 1990

GEOCHEMICAL SURVEY

A total of 640 soil samples were collected from the property. The samples were collected at 25 metre stations on lines spaced 150 metres apart. The soil samples were collected, from an average depth of 25 cm from the B horizon where possible, using a soil shovel and waterproof paper bags.

Five stream sediments were collected from four of the creeks that drain the claim group. The first sample was a silt collected from a creek that drains the area on the Helper claim near where the Aban showing is reported to occur. The remaining four stream samples were collected using a gold pan, the stream sediment was panned down to an approximate two tablespoon size and placed in a plastic bag. The process was repeated two to four times to ensure sufficient sample was collected.

The rock samples were representative chip samples, or float samples collected by R Husband or P Dasler. The rock samples were shipped to Acme Labs for crushing, grinding and analysis by 30 element I.C.P. and geochemical gold. Samples with highly anomalous values of zinc, copper, lead, silver, or gold were resubmitted for assay (gold by fire assay using 1/2 assay ton). Descriptions of all rock samples can be found in Appendix 1.

The samples were delivered to Acme Analytical Laboratories Ltd. in Vancouver where the silts and soils were dried and screened to -80 mesh and the rocks were crushed and powdered to -80 mesh. The samples were then analyzed for 30 elements by I.C.P. which involves the digestion of 0.5 grams of the sample with 3-1-2 HCl-HNO3-H2O acid at 95 degrees celsius for one hour. This sample is then diluted to 10 ml with water and analyzed. The samples were also analyzed for gold by acid leach and atomic absorbtion by Acme labs.

In 1968 an extensive regional geochemical survey was conducted by BHP Utah Mines Ltd. This survey resulted in 9592 soil samples being collected and analyzed. A detailed statistical analysis was conducted on the results and threshold values from Assessment report 2190[19] is included in Appendix 2. The calculated threshold values for the copper and zinc in each rock type in this area are as follows: Karmutsen - 68 ppm copper, 42 ppm zinc

Quatsino limestone - 109 ppm copper, 90 ppm zinc
Bonanza - 25 ppm copper, 44 ppm zinc
Intrusives - 31 ppm copper
Altered Rocks - 36 ppm copper 16.2 ppm zinc.

Results:

Stream Sediments

One silt sample and four pan samples were collected from various creeks that drain the claims. The sampling produced highly variable results, however anomalous values were found for varying elements in each sample.

The silt sample, (#109951), was collected from a small creek near where the Aban showing is reported. This silt assayed 14 ppb gold and 0.5 ppm silver. Values of copper, zinc and lead were background levels.

The two pan samples collected from the creek that drains the southwest comer of the claims showed variable results. Sample 109963 assayed 201 ppm zinc and 0.7 ppm silver with background levels of copper and lead. Sample 109966 contained 126 ppm copper and 88 ppm zinc with background levels of lead and silver.

Pan sample #109960 from the north-south flowing creek near line 21E contained 208 ppm zinc with background values in the remaining elements. Sample 109962 from the creek 100 metres southwest, near the diorite outcrop, contained 107 ppm copper.

Rocks

The locations and assay results for the 72 rock samples taken from the claims are shown of Figure 4. A total of 14 samples were resubmitted for assay of lead, zinc, copper, gold and silver. The sampling highlighted several areas of interest on the claims.

The first is the zone of zinc replacement near the upper contact of the limestone at 8+00N, 3+00E. The zone is adjacent to a small diorite intrusive. Zinc mineralization was first discovered in this area in 1973 when several hand trenches were dug on it. It was reported to extend 210 metres along an attitude of 280/45°S A 4.9 metre chip assayed 6.02% zinc, 0.04% lead and 4.8g/tonne (0.140 oz/t) silver. The current program uncovered epidote-actinolite skarn mineralization in the area of the previous trenching. Sampling of the mineralization here returned 2.29% zinc and 1.13g/tonne (0.033oz/ton) gold over 0.3 metres, collected immediately under a 2.0 metre wide magnetite bed. Other samples along this zone yielded values of 8.59% zinc and 0.22% copper and 3.60% zinc and 0.058 oz/ton gold over 1.5 and 1.0 metre widths respectively.

Three adjacent samples across the zone exposed 120 metres southeast (7+00N,4+50E) produced 1.66% zinc across 2.75 metres.

The semi massive sulphide vein located within the diorite at 7+50N, 8+50E assayed 10.80% zinc, 0.93% copper, 0.36% lead, 0.455 oz/t silver and 0.004 opt gold across 1.5 metres from three adjacent samples. A further sample assayed 13.33% zinc, 0.21% copper, 0.59% lead, 0.27 opt silver and 0.002 opt gold over 0.4 metres.

A 0.3 metre sample across the extension of this vein across a northwest trending fault assayed 20.85% zinc, 1.17% copper, 0.01% lead, 21.6 g/tonne (0.63 opt) silver, and 0.377 g/tonne (0.011 opt) gold. This vein occurs within the margin of a small diorite stock.

A 1.0 metre chip sample of highly siliceous, fractured sediments, taken at 3+00S 20+00E, (#109945), assayed 0.31% copper 30.17 g/tonne (0.88 opt) silver and 0.377 g/tonne (0.011 opt) gold. This mineralization would indicate that there has been significant replacement style mineralization along bedding planes and faults.

A full list of assays is attached to figure 5 and the assay certificates and sample descriptions are in appendices 1 & 2.

Soil geochemistry

The results for gold, silver, zinc, copper, lead and arsenic are plotted on Figures 6a-6f. A frequency distribution graph was plotted for each of the six elements and results are shown in Appendix 2. The values contoured for each element were guided by this data, and by the regional survey data (Appendix 2), in order that all trends would be shown.

The values for gold in the 640 soil samples ranged from 1 to 38 ppb and contours were drawn at 10, 15, 20, 25, 30 ppb., figure 6a. Anomalous gold in the soil generally occurs as single station anomalies throughout the grid. Areas of significant trends include:

> Line 4+50E at 3+00N centres an anomaly that extends to lines 150 metres away to the east and west. This anomaly occurs in the area of the quartz-amethyst vein float.
>
> In the vicinity of the skarn near the upper contact of the limestone, values of 26 and 37 ppb were obtained.
>
> On the eastern portion of the grid anomalies are spotty, but appear more frequently near the upper contact of the limestone.

Silver values are plotted on Figure 6b and values range from 0.1 to 5.8 ppm. Contours were drawn at 1.0 and 1.5 ppm and are considered anomalous. In the area of the quartz-amethyst vein float silver values range to 1.6 ppm and in apparent east-west trend is shown. Along the contact of the limestone with the overlying Parson Bay sediments, numerous anomalous values occur and detailed geochem may assist in defining exact trends and provide further drill targets. The eastern portion of the grid hosts numerous spot anomalies with the highest value of 5.8 ppm occurring here. This area is approximately where the Aban showing is reported to occur although it could not be located in 1990 due to recent logging and dense undergrowth.

The zinc values are plotted in Figure 6c, and values range from 13 to 3185 ppm. The majority of the samples were collected across the Quatsino limestone, and many of the values surpass the 90 ppm threshold, indicating that the whole area is anomalous in zinc. Values over 150 ppm were contoured and several areas of interest were defined. An approximate east-west trending anomaly occurs where the quartz-amethyst vein float was found with values to 638 ppm Zn. A very extensive anomaly extends over the skarn zone. It trends northwest over 450 meters and has values up to 2242 ppm Zn. It follows the assumed upper contact of the limestone. A further very prominent northwest trending anomaly occurs approximately 200 metres to the north. Here values range up to 3185 ppm Zn, and appear to represent a parallel zone of zinc mineralization within the limestone. The eastern portion of the grid has several isolated anomalous zones and one very large anomaly (1039 ppm Zn) in the vicinity of the Aban showing.

Copper values are shown on Figure 6d and contoured at 50 ppm intervals. Copper values range from 1 to 827 ppm but are generally less than 75 ppm. The 50 ppm contour shows many spot anomalies. Values over 100 ppm are highly significant. Areas of elevated copper occur in the vicinity of the skarn zone and extend northwest along the contact. The most significant copper values occur near the contact of the limestone with the older Karmutsen volcanics to the north. In the northwest portion of the grid this contact is a major fault. Here values range up to 827 ppm Cu. In the eastern portion of the grid the formational contact is thought to be conformable. In this area copper values range to 252 ppm. Around the Aban showing a significant northwest copper trend is shown with values up to 288 ppm.

Lead values from the survey range from 2 to 305 ppm and are shown on Figure 6e. Anomalous isolated lead values are occur throughout the grid. Significant trends occur near where the quartz-amethyst vein float was found with values up to 106 ppm Pb. Lead values around the Aban showing range up to 87 ppm.

Arsenic values are plotted on Figure 6f and range from 2 to 222 ppm. Contours at 25, 50, and 75 ppm were drawn to highlight any significant trends. Elevated arsenic occurs in the vicinity of the quartz-amethyst float. Arsenic does not appear to be related to other elements analysed.

The contouring of the geochemical plots is heavily biased by the sample line spacing (150 metre spaced lines, 25 metre sample spacing). Infill lines in areas of significant anomalies would assist in delineating the true orientation of the anomalies.

GEOPHYSICAL SURVEY

A total of 17.5 km of crossline was surveyed using a Scintrex MG-2 Proton Precession Magnetometer and a Sabre Electronics Model 27 VLF-EM. Readings were taken every 25 metres on lines spaced 150 metres apart.

Magnetometer

This instrument measures the earth's total magnetic field to within one gamma. A base station was used to check for diurnal variations but these were found to be insignificant (less than 50 gammas). There were no strong variations observed in the earth's magnetic field during the survey.

The plotted results from the magnetometer survey are shown on figure 7a. Contours were drawn at 500 gamma intervals and the background values were between 56,000 - 57,000 gammas.

Values above 57,000 gammas are considered as high and values below 56,000 gammas as lows. Several small magnetic highs occur scattered throughout the grid. These highs are represented by "A" on the plan, and likely represent small intrusive bodies.

Areas marked by "B" on the map are magnetic lows and represent areas of alteration or changes in lithology. In the northwest portion of the grid a narrow low trends east-west and cuts different lithologies and probably represents alteration adjacent to a fault zone. In the vicinity of "B'" sharp topographical features indicate faults.

The large magnetic highs illustrated by "C" on the map represent the large diorite batholith intruding the claims from the northeast.

VLF-EM

For this survey the transmitter located at Seattle, Washington (24.8khz) was used for all readings. The Sabre Electronics Model 27 VLF-EM acts as a receiver only. Powerful radio transmitters set up throughout the world for the purpose of military communication and navigation generate a primary field in the 15-25 khz range. When this primary field encounters a buried conductor (eg. massive sulphides, geological facies change, water filled faults, etc.) a secondary field is induced which distorts the primary field. The VLF-EM measures this distortion of the field. For maximum coupling, best results are obtained when the transmitting station is located in the direction of the geological strike of the conductor.

It should be noted that a limitation of the VLF-EM Method is its relatively high frequency. This causes such things as ridge tops, groundwater, swamps, and creeks to be recorded as conductors. Also the penetration is limited to about 20 metres of overburden or 60 metres of bedrock.

The VLF-EM data was fraser filtered using Scintrex's FRASER program. The results of the VLF-EM survey are plotted on figure 7b. Well defined northwest trends are evident. The most obvious is the linear that crosses the grid near the center, this axis corresponds to the upper contact of the limestone with the overlaying Parson Bay sediments. A parallel axis occurs north of this contact and about 100 metres south of the known lower contact of the limestone. This may represent the dip of the contact. Centred on line 4+50E at 4+25N is another significant east-west trending anomaly. This anomaly corresponds to the location of quartz-amethyst vein float and may indicate the attitude of the veining that was the source of the float.

DISCUSSION

The exploration on the Win group during January and February 1990 was hampered by excessive logging slash and underbrush developed following clearcut logging operations on the property in 1975. No evidence remained of the original survey grids, and there was no remnant of the (hand) trenching operations which had provided the original interest for this survey.

The area for the geochemical and geophysical survey was limited to the area of the Quatsino Formation and its contacts with the Karmutsen and Parsons Bay formations. This was because of the previously known mineralization on this property and on others in the district, and the budget constraints of the project.

A trenching programme was carried out using a Caterpillar 225 tracked excavator in an attempt to expose the skarn areas for sampling. This was not completely successful because of either the topography, overburden, or the very weathered nature of the sulphide zones. Further trenching is warranted. The current work was curtailed by a heavy snow fall.

The exploration program conducted in 1990 was successful in defining targets for follow-up work. The geochemical survey reinforced the information obtained from earlier surveys, and outlined new mineralized areas.

The zinc and silver plots outline the area of known zinc skarn near the upper contact of the limestone, as well as delineating probable extensions of it. The VLF-EM survey shows a strong anomaly that corresponds to this zone and the magnetometer survey defined three small highs along the zone that probably represent intrusives.

Rock samples taken from the exposed zinc mineralization assayed 8.59% zinc and 3.60% zinc 1.99 g/tonne and 0.058 oz/tonne gold over 1.5 and 1.0 metres respectively. Samples taken in 1968-75 and reported 50 metres northwest of this site, assayed 6.02% zinc 4.8 g/tonne (0.140oz/ton) silver across 4.9 metres. The zone should be drill tested to explore the zone along strike and down dip and to check for parallel systems.

Other showings in the region (HPH - Dorlon) report skarn development along both the upper and the lower contact of the limestone. It appears as if the formational contacts provide solution paths for fluids generated by the numerous intrusives in the area. The intense silicification of large areas of the Parsons Bay sediments above the limestones highlights the wide areal extent of the mineralizing events, and the potential for large scale replacement sulphide mineralization in the limestone. Although no skarn was mapped near the lower contact due to limited outcrop a drill hole is proposed to cross the limestone and check for skarn mineralization at the lower contact.

A second area for follow up work is in the vicinity of the quartz-amethyst vein found as float. Here the geochemical survey outlined an approximate east west trending anomaly in zinc, silver, gold and to a lesser extent lead and arsenic. This anomaly extends for a minimum of 300 metres for each element. A strong east-west anomaly is also shown by the VLF-EM survey and may represent a sulphide bearing vein system. Samples of the float did not return highly anomalous values in any of the 30 elements tested; however they did contain slightly elevated amounts of gold (81.89 and 150 ppb). Follow up work in this area should include infill detailed geochemistry and geophysics followed by trenching and/or drilling, to determine the potential for epithermal style gold mineralization.

The third area for follow-up work is in the area of the Karmutsen volcanics and the large diorite batholith to the northeast. The survey conducted in 1968 and 1969 defined a significant (80+ppm) copper anomaly (see figure 3). There is extensive soil and overburden cover in this area, so no rock chip sampling has been completed, however the sample of diorite float which was collected in the earlier survey assayed 0.1% copper and 5.14 g/tonne (0.15oz/ton) silver. The current mapping indicated intense felsic alteration in the diorite just east of the zone. A magnetometer survey conducted in 1969-1970 defines the contact zone between the volcanics and the diorite. Follow up work could consist of additional geochemistry followed by trenching/drilling to test the diorite. In this area the batholith may be mineralized with stringer copper mineralization, derived from the assimilation of the copper rich Karmutsen volcanics (see fig 4a).

In the southwest corner of the claims, diorite with disseminated pyrite, chalcopyrite, and molybdenite which was found to intrude Bonanza volcanics defines the fourth area of interest. The most intense clay alteration and pyrite mineralization in this area is bisected by the claim boundary. The area to the south is heavily forested, and the zone was not traced further. No anomalous samples were collected during this program but the 1968 geochemical survey outlined a copper anomaly on the Win claims in this region and additional work is warranted.

The fifth target area is the old Aban showing, where in 1968 Giant Explorations Ltd reported a skarn mineralized with sphalerite and galena. Samples of 1.81% zinc, 0.97% lead and 2.78% zinc and 0.36% lead were reportedly taken across 2.4 and 3.05 metres. No evidence of the showing was found during this program due to recent logging and road building, and the area is covered with new forest plantings (1976), and thick undergrowth. The geochemical and geophysical survey clearly define an area for follow up work. Highly anomalous values of zinc, silver, gold, copper and lead were obtained from soils in the area where the Aban showing is reported to be located. The magnetometer survey shows a strong high to the northeast that likely represents intrusive rock. Limestone outcrops in the area. Follow up work consisting of infill detailed geochemistry and geophysics followed by limited trenching (because of new tree planting) and possibly drilling is recommended in this area.

The sixth target area is the semi massive sulphide vein that occurs within the margin of a small diorite intrusive. The vein was uncovered in a pit on the side of the road between two of the survey lines and no definite geochemical or geophysical signature was established. The northeast striking, southeast dipping vein is offset 20 metres right laterally by a northwest trending fault. A series of three adjacent chip samples across the vein assayed 10.80% zinc, 0.93% copper, 0.36% lead, 15.60 g/tonnes (0.455 oz/t) silver and 0.137 g/tonne (0.004 oz/ton) gold over 1.5 metres. Another sample of the vein assayed 13.33% zinc 0.21% copper and 0.59% lead across 0.4 metres. A 0.3 metre chip across the extension of the vein across the fault assayed 20.85% zinc, 1.17% copper 21.60 g/tonne (0.63 oz/t) silver and 0.377g/tonne (0.011 oz/t) gold. Further similar veining is possible in this area, however outcrop is very sparse. This zone could easily be tested at depth and along strike by drilling.

CONCLUSIONS

1.0 The Win Claim Group is located in an area favourable for the occurrence of zinc-gold and copper-gold replacement style mineralization.

2.0 Zinc mineralization with gold can be traced on the claims near the upper limestone contact over a minimum of 170 metres. A strong geochemical anomaly, which parallels this skarn to the north may represent a second major zone of replacement.

3.0 The Aban mineral occurrence, which is over 1500 metres southeast of this area indicates that there has been significant replacement mineralization along the whole Quatsino limestone-Parsons Bay sediments contact.

4.0 Gold values of up to 1.00 g/tonne (0.058 opt) over 1.0 metres were obtained from areas of the zinc mineralization on the Win property. On the Dorlon - HPH properties, (zinc-gold replacement along the same formational contact), gold values up to 19.2 g/tonne (0.560 opt), over 0.61 metres are reported. Similar regional mineralizing processes are clearly evident.

6.0 Geochemical and geophysical surveys have delineated trenching and drill targets along the upper and lower limestone contacts.

7.0 Locally derived quartz-amethyst vein float containing elevated gold values was found within a zone of anomalous lead and gold soil geochemistry, and geophysical VLF-EM response.

8.0 A large sulphide vein with 10.8% zinc and 0.93% copper over 1.5 metres in width within the margin of a diorite intrusion may indicate a zone of remobilization and fracture replacement.

9.0 The previous geochemical surveys on the property outline a zone of copper mineralization within the diorite near the contact of the Karmutsen volcanics. A float sample of the diorite which assayed 0.1% copper indicates a significant target for copper mineralization.

11.0 Potential copper-gold mineralization, similar to the Red Dog deposit, may occur where diorite with disseminated pyrite and lesser chalcopyrite and molybdenite, was found intruding Bonanza Group Volcanics in the southwest of the claim group.

RECOMMENDATIONS

1.0 Drilling should be conducted along the areas of known zinc mineralization to explore grades and thicknesses at depth and along strike and also check for parallel zones of replacement.

2.0 Drilling should be conducted on the semi massive sulphide vein to explore the extent of the vein mineralization.

3.0 Infill geochemical soil sampling supported by VLF and magnetometer surveys should be carried out in the area of 3+00N, 21+00E to define the Aban showing. Limited trenching can be completed with possible drilling.

4.0 Detailed geochemistry, trenching, and prospecting is warranted in the area of the quartz-amethyst vein float followed by possible drilling.

5.0 Additional geochemical sampling should be carried out over the copper zone north of the of Karmutsen Formation-diorite contact with trenching to expose outcrop. Drilling may be necessary to achieve samples in this area, and to explore the diorite at depth.

6.0 Additional geochemical soil sampling supported by magnetometer and VLF surveys should be carried out in the southwest corner of the claims near the diorite-Bonanza Formation contact to explore for copper-gold mineralization.

STATEMENT OF COSTS

1.0 PERSONNEL			
	1 Senior Geologist 12.35 days @ $380/day	4,693.00	
	1 Project Geologist 48.4 days @ $260/day	12,584.00	
	2 Field Technicians 69 days @ $280/day	19,320.00	
	1 Draftsperson 9.4 days @ $220/day	2,013.00	
2.0 FOOD AND ACCOMMODATION			
	3 men 34 days @ $44.15/day ea.	4,503.08	
3.0 TRANSPORTATION			
	1 4x4 34 days @ $99.33/day (incl. gas)	3,377.26	
	1 4x4 4 days @ 101.10/day (incl. gas)	505.50	
	Airline	850.20	
4.0 FIELD SUPPLIES (flagging, topo etc.)		1,521.05	
5.0 EQUIPMENT RENTAL (mag, VLF, radios)		600.00	
6.0 ASSAYS			
	640 soil samples @ $9.06 ea.	5,799.25	
	72 rocks	968.75	
	5 stream sediments	20.50	
7.0 HEAVY EQUIPMENT (backhoe)		9,563.50	
8.0 MISCELLANEOUS (filing fees, contract labour, etc.)		1,221.00	
9.0 DRAFTING		1,053.96	
10.0 OFFICE COSTS (telephone, copying, etc.)		1,229.05	
11.0 DISBURSEMENTS		6,021.02	
	TOTAL PROJECT COSTS		**$75,844.62**

RECOMMENDED BUDGET

- infill geochem/geophysics and extend grid, trenching, roadbuilding and drilling

Geochemical Survey	
Grid Extension & Infill Lines	
say 20 cm flagged grid @ $90/cm	1,800
800 soil samples @ $4.50/each for collection	3,600
Geophysical Survey	
20 cm @ $150/cm - 20 man days	3,000
Assays	
800 soils @ $13.50	10,800
say 50 rocks @ $15	750
Transportation	
Geochemical and Geophysical	
30 days - 1 4x4 @ $950/month	1,900
Geologist	
1 4x4 @ $950/month	
gas and repairs	1,500
mileage	600
Food and Accommodation	
3 men - 30 days @ $65/day	5,850
Wages	
1 helper - 20 days @ $220/day	4,400
1 geologist - 30 days @ $260/day	7,800
Field Supplies	1,000
Office	750
Excavator	
Road Building (drill sites)	10,000
Trenching - 10 days @ $1,000/day	
Diamond Drilling	
Mobilization/Demobilization	3,000
3000' drilling @ $22/foot	66,000
Assay	
say 150 samples @ $15/sample	2,250
	117,200
Contingency 15%	17,800
TOTAL PHASE I say	**$135,000**

PHASE II (contingent on successful definition of Economic Grade Mineralization inPhase I)

Drilling	
Additional 5000' @ $22/foot	110,000
Mobilization/Demobilization	3,000
Wages	
1 helper - 30 days @ $220/day	6,600
1 geologist - 30 days @ $260/day	7,800
1 P. Eng. - 5 days @ $400/day	2,000
Assays	
say 300 samples @ $15	4,500
Excavator	
(build drill sites) - 5 days @ $1,000/day	5,000
Food and Accommodation	
35 man days @ $65/day	2,275
Transportation (4x4)	
30 days @ $950/month	950
gas and repairs	750
mileage	2,000
	143,175
Contingency 15%	21,825
Total Phase II	165,000
	135,000
TOTAL BOTH PHASES	**$300,000**

CERTIFICATE OF QUALIFICATIONS

I, Rod W. Husband, do hereby certify that:

1. I am a geologist for Daiwan Engineering Ltd. with offices at 1030 - 609 Granville Street, Vancouver, British Columbia.

2. I am a graduate from the University of British Columbia with a degree of B.Sc.,Geology.

3. I have practised my profession since completion of my degree in December 1986.

4. This report is based on personal field work completed on the Win property from January 3 - February 5, and information obtained from previous reports by Professional Engineers and others who have examined the property.

5. I have no interest in the property or shares of Essex Resource Corporation or in any of the companies with claims contiguous to the Win Claim Group, nor do I expect to receive any.

6. This report, when quoted in full may be used by Essex Resource Corporation for Stock Exchange approval or for the raising of funds.

Rod W. Husband, B.Sc.
February 15 1990

CERTIFICATE OF QUALIFICATIONS

I, Peter G. Dasler, do hereby certify that:

1. I am a geologist for Daiwan Engineering Ltd. with offices at 1030-609 Granville Street, Vancouver, British Columbia.

2. I am a graduate of the University of Canterbury, Christchurch, New Zealand with a degree of M.Sc., Geology.

3. I am a Fellow of the Geological Association Of Canada, a Member, in good standing, of the Australasian Institute of Mining and Metallurgy, and a Member of the Geological Society of New Zealand.

4. I have practised my profession continuously since 1975, and have held senior geological positions and managerial positions, including Mine Manager, with mining companies in Canada and New Zealand.

5. This report is based on a personal research and reports of Professional Engineers and others working in the area of Win claims, and by my supervision of fieldwork on the property in January 1990.

6. I have no interest in the Win property or shares of Essex Resource Corporation, nor do I expect to receive any. I have a part interest in shares of Moraga Resources Ltd, which controls the Expo property to the south of the Win property.

7. This report when quoted in full may be used by Essex Resource Corporation for stock exchange requirements and for the raising of funds.

Peter G. Dasler, M.Sc., FGAC
February 15, 1990

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APPENDIX 1

Sample Descriptions

Win-90-01	QZ vein with crystals in cavities strike 050°N no obvious sulfides
Win-90-02	35cm of diorite (amphibole porphyry) trends 275 dissem MO & PY
Win-90-03	grab of rubble at site of Win-90-02
Win-90-04	10cm QZ vein in road bed some MO greater than 1%
Win-90-05	1.0cm across diorite dyke in andesites mal stain, dissem PY & CP?
Win-90-06	highly altered - bleached, silicified andesite mod-high fractures abundant PY
Win-90-07	QZ vein with hematite/limonite and trace dissem PY
Win-90-08	locally derived QZ vein boulder with amethyst
Win-90-09	QZ veining - QZ supported breccia with host (andesitic) rock fragments
Win-90-10	QZ - carb vein float
109451	1M chip across light and dark banded recrystallized LST next to fault
109452	0.75 chip across fault gouge - rusty colour next to 451
109453	1.0m chip epidote - actinolite skarn highly silicified dissem. Py & SP next to '452
109454	75 cm chip across epidote - garnet skarn - highly altered v crumbly no obvious sulfides next to '453
109455	1.0m chip across epidote - actinolite skarn - highly siliceous dissem Py & SP? next to 109454
109456	diorite - siliceous mod. fractured dissem Py & Mo?
109457	30 cm of highly altered - gossanous with Mn staining siliceous seds
109458	highly siliceous sediments thin bedded dissem. Py.
109459	in trench 1 at lst-sed contact-highly fractured with rust and mn staining
109460	1.0m chip in highly fractured (350/90 & 040/90) thin bedded tuffs & sediments with epidote along fractures
109461	crystal tuff (felsite) with dissem PY adjacent to lst and epidote-garnet skarn
109462	2.5m wide epidote-actinolite skarn highly siliceous QZ stringers throughout dissem PY & SP. trench 1
109463	3.5m wide epidote-garnet skarn zone highly bleached
109464	float on road by 1st pit - epidote - actinolite skarn dissem py.cp sp with minor mal staining
109465	QZ vein float boulder - locally derived dissem up to 1%
109466	as 109466
109467	50cm wide epidote - actinolite skarn in trench 1 at upper contact of lst w/ Parson Bay seds dissem py, sp.
109468	highly altered contact zone of lst with Parson Bay - fault contact
109469	80cm across semi massive sulphide vein PY, SP cp? ga? abundant. 050/70 SE

109470	40cm chip of weathered rusty, mn stained portion of vein mal, cp PY adjacent to 109469
109471	30cm chip across upper section of vein galena? SP highly siliceous
109472	30cm epidote - garnet skarn on footwall of sulphide vein in diorite
109473	as 109471
109474	40 cm across semi massive sulphide vein 20 - 30% PY 010/52 E west wall offset from 109469
109475	45cm across semi massive sulphide portion of vein zone PY SP
109476	75cm chip in diorite with up to 1% dissem PY trace mo & cp
109477	old trench 4 - 30cm chip across epidote - actinolite skarn below mg PY SP ga highly siliceous
109478	1.4 m across massive magnetite bed above 109477 som PY & SP
109479	lower road 30 cm in karmutsen basalt andesite blocky fractures minor rust dissem PY to 1%
109480	35cm chip in highly fractured, kaolinized rusted volcanic?
109481	siliceous diorite med grained abundant dissem PY to 2%
109482	2.5m chip across dioritic sill in lst - fault contact on both hanging & footwall dissem PY to 1%
109483	70cm chip at footwall of sill highly fractured, rusty
109484	60cm chip at hanging wall of sill highly fractured rusty
109485	45cm chip in highly siliceous thin bedded seds w/ PY & SP dissem and on fracture surfaces
109486	1.0m chip of highly rusted - gossanous zone in siliceous seds abundant PY
109487	1.2m chip at footwall of fault (345/80 SW) dissem PY in seds
109488	1.0m chip in mod siliceous seds dissem PY & SP & on bedding planes
109489	1.0m across highly fractured/rusted & mn stained siliceous sediments near fault
109490	trench 2 1m wide epidote-garnet skarn bleached crumbly 060/45°NW
109491	trench 2 1.0m chip of 2.5m wide siliceous Mn-gossanous skarn PY & SP with yellow oxide
109492	trench 2 1.5m chip as above next to 109491
109493	trench 2 - 1.5m chip actinolite-garnet-epidote skarn abundant PY, SP with yellow oxide? highly siliceous
109494	as previous 4 meters along trench 1m chip

109495	pit on south road 1.0m chip across heavily rusted abundant PY to 20% adjacent to fault 055/80°NW
109496	LST pit on main road 1.0m chip of QZ - feld crystal tuff, dissem PY & PY on fractures (calcite) 0/8/70°-90°W
109497	LST pit on main road 2.0m chip across crystal tuff - rusted w/abundant Py
109498	line 19+50E 4+25N karmutsen andesite - basalt aphanitic dark green abundant magnetite disseminated minor ed along fractures
109499	1m chip in highly fractured (350/65°W) karmutsen basalt with abundant hairline stringers. No obvious sulfides
109500	40cm in bleached volcanic adjacent to fault 350/65°W K-spar alter of stringers
109952	75m chip in med grained pink granodiorite moderately fractured 044/90 minor PY k\spar alteration along fractures
109953	2m chip across dioritic dyke in granodiorite 275/52°N
109954	6m wide dark green dioritic dyke 260/75°SE gossanous QZ - feld phenos in parts in black groundmass
109955	40cm in karmutsen basalt - aphinitic mod. fractures - clay stringers magnetite dissem throughout
109956	20+90E 4185N andesite - basalt with abundant dissem magnetite
109957	diorite with mod. fractures minor clay alteration along fractures; disseminated Py
109958	highly siliceous volcanic andesite? at contact with diorite disseminated magnetite and pyrite quartz stringers
109959	highly siliceous volcanic; disseminated pyrite quartz stringers
109961	diorite - fresh - disseminated magnetite to 1%
109963	highly siliceous volcanic abundant pyrite (to 20%) disseminated and along fractures
109965	15 cm quartz pyrite stringer zone in siliceous volcanics
109966	highly siliceous volcanic abundant pyrite
109967	10 cm quartz-pyrite stringer zone 060/80°SE at base of cliff
109951	silt sample
109960	pan sample - sediment panned down to ~2 tablespoon size; very few heavies; total sample 4 pans
109962	pan sample - sediment panned down to ~2 tablespoon size; magnetite 2-3%
109963	pan sample - 3 pans taken down to ~2 tablespoon size; minor heavies

APPENDIX 2

Assay Certificates

and

Statistical Analysis

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: SILT/ROCK AU** ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.

DATE RECEIVED: JAN 8 1989 DATE REPORT MAILED: Jan 12/90 SIGNED BY.......... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN File # 90-0081

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM
C 109951	2	62	17	55	.5	10	11	972	4.85	5	5	ND	1	25	2
90-01	2	7	6	4	.1	6	1	58	.31	2	5	ND	2	15	1
90-02	3	228	14	12	.3	6	14	136	5.09	5	5	ND	2	59	1
90-03	12	116	9	29	.1	6	7	199	3.05	5	5	ND	2	30	1
90-04	32	24	7	3	.1	7	1	36	.31	2	5	ND	1	9	1
90-05	18	640	10	36	.1	6	7	140	1.74	2	5	ND	2	43	1
90-06	10	39	11	28	.1	11	6	244	4.97	4	5	ND	1	14	1
90-07	2	6	3	1	.1	6	1	67	.92	3	5	ND	1	1	1
90-08	2	3	4	1	.1	10	2	250	2.40	25	5	ND	1	1	1
90-09	1	2	3	7	.1	6	11	633	6.41	75	5	ND	1	1	1
STD C/AU-R	18	57	42	130	6.5	68	30	941	3.92	40	20	8	38	48	19

SAMPLE#	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	AU** PPB
C 109951	2	2	109	.77	.050	2	19	.26	37	.14	4	1.81	.01	.01	1	14
90-01	2	2	22	.38	.003	10	32	.02	236	.13	2	.23	.03	.01	1	62
90-02	2	2	69	.12	.034	2	11	.82	56	.08	3	1.11	.04	.05	1	7
90-03	2	2	60	.73	.034	4	11	.81	16	.09	2	2.06	.01	.04	2	6
90-04	2	2	4	.21	.014	5	8	.06	3	.01	2	.34	.01	.01	1	1
90-05	2	2	24	2.14	.030	5	7	.53	37	.03	3	2.09	.01	.03	1	17
90-06	3	2	86	.32	.056	2	64	1.37	24	.05	2	1.69	.01	.06	1	21
90-07	2	2	1	.15	.002	2	5	.01	1	.01	2	.03	.01	.01	1	89
90-08	2	2	3	1.61	.005	2	5	.02	1	.01	3	.07	.01	.01	1	81
90-09	2	2	8	3.19	.029	2	9	.06	1	.01	5	.32	.01	.01	1	150
STD C/AU-R	15	22	58	.43	.095	38	55	.81	175	.07	39	1.82	.06	.14	13	480

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P11 SOIL P12 ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JAN 23 1990 **DATE REPORT MAILED:** Jan 30/90 **SIGNED BY**.......... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN File # 90-0207 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L0+00E 15+00N	2	16	27	49	.1	17	4	262	2.26	2	5	ND	1	25	1	2	2	97	.65	.015	3	35	.58	19	.22	4	1.49	.01	.02	1	8
L0+00E 14+75N	3	5	32	36	.3	5	1	88	1.94	2	5	ND	1	18	1	2	5	81	.32	.025	3	18	.09	17	.19	3	.86	.01	.03	1	9
L0+00E 14+50N	2	11	18	56	.8	3	1	18	2.25	2	5	ND	1	7	1	2	2	45	.09	.072	3	17	.03	12	.06	2	.68	.01	.04	1	5
L0+00E 14+25N	3	5	30	32	.1	5	1	109	1.01	3	5	ND	1	17	1	2	7	113	.27	.013	3	23	.13	13	.23	4	.85	.01	.02	3	5
L0+00E 14+00N	2	9	11	85	.1	2	1	47	1.35	2	5	ND	1	13	1	2	4	20	.16	.069	2	7	.04	19	.04	2	.46	.01	.03	1	4
L0+00E 13+75N	5	10	28	46	.1	11	3	208	6.38	6	5	ND	1	20	1	2	2	221	.34	.009	3	28	.39	15	.28	2	1.67	.01	.02	1	4
L0+00E 13+50N	5	9	27	43	.1	6	2	218	3.94	6	5	ND	1	22	1	2	5	178	.39	.007	3	22	.27	18	.24	3	1.45	.01	.02	2	9
L0+00E 13+00N	3	6	27	35	.1	5	1	30	1.85	3	5	ND	1	17	1	2	2	43	.15	.026	3	19	.05	24	.06	3	.98	.01	.03	1	3
L0+00E 12+75N	11	11	47	67	.4	6	4	39	13.04	24	5	ND	1	10	3	2	10	149	.12	.085	4	16	.04	21	.03	6	1.27	.01	.04	1	1
L0+00E 12+50N	5	19	36	76	.1	14	4	235	6.25	12	5	ND	1	22	2	2	2	167	.50	.023	4	28	.44	15	.16	4	2.24	.01	.02	3	9
L0+00E 12+25N	2	9	17	89	.8	5	1	48	1.86	2	5	ND	1	17	1	2	2	56	.24	.039	2	8	.05	23	.08	3	.52	.01	.05	1	5
L0+00E 12+00N	3	37	32	80	.1	17	7	362	4.32	11	5	ND	1	27	1	2	2	138	.60	.013	3	31	.50	37	.23	3	2.58	.01	.02	1	6
L0+00E 11+75N	2	8	20	40	.1	5	3	143	3.30	2	5	ND	1	18	1	2	2	150	.31	.011	2	9	.10	14	.19	4	.56	.01	.03	1	6
L0+00E 11+50N	5	26	28	170	.1	24	9	697	3.90	13	5	ND	1	34	1	2	3	113	.76	.027	4	33	.93	49	.19	2	3.14	.01	.04	1	4
L0+00E 11+25N	3	68	44	168	.1	20	11	455	3.31	12	5	ND	1	45	1	3	2	85	1.08	.050	4	27	.72	83	.15	2	2.65	.03	.03	1	4
L0+00E 11+00N	19	25	30	328	.2	29	26	3454	4.59	21	6	ND	1	37	6	2	2	123	1.02	.072	6	40	.82	69	.09	7	3.36	.01	.03	1	1
L0+00E 10+75N	6	27	20	179	.1	23	8	477	3.42	17	5	ND	1	38	1	2	2	89	.95	.057	6	28	.75	47	.14	2	2.62	.02	.03	1	4
L0+00E 10+50N	2	14	9	72	.3	6	2	575	.54	2	5	ND	1	47	1	2	3	15	1.44	.082	2	5	.11	36	.01	5	.38	.01	.04	1	3
L0+00E 10+25N	4	61	45	192	.1	23	10	626	2.97	8	5	ND	1	58	3	2	6	82	1.70	.065	5	24	.56	62	.13	7	1.78	.04	.04	1	8
L0+00E 10+00N	3	40	23	109	.1	19	10	879	3.20	8	5	ND	1	50	1	2	8	73	1.13	.052	5	22	.65	54	.11	4	2.21	.02	.03	1	7
L0+00E 9+75N	8	56	29	886	.3	30	21	5296	3.75	63	5	ND	1	44	13	2	2	106	1.66	.083	6	39	.34	109	.05	11	3.53	.02	.04	1	3
L0+00E 9+50N	2	66	33	203	.1	25	10	583	3.41	14	5	ND	1	46	3	2	2	95	1.40	.065	5	29	.71	77	.15	4	2.47	.02	.03	2	7
L0+00E 9+25N	4	25	17	66	.1	11	6	264	6.91	10	5	ND	1	24	2	2	2	192	.57	.031	3	24	.35	25	.30	2	1.77	.01	.03	1	2
L0+00E 9+00N	4	33	21	105	.1	21	9	595	3.65	13	5	ND	1	54	2	2	2	90	1.25	.037	4	23	.68	48	.14	2	2.22	.02	.03	1	4
L0+00E 8+75N	3	41	15	99	.2	25	11	610	3.41	18	5	ND	1	56	1	4	3	85	1.16	.060	5	29	.94	46	.15	5	2.27	.03	.03	1	2
L0+00E 8+50N	17	18	17	123	.2	15	32	1728	7.64	53	5	ND	1	34	2	2	2	206	1.05	.041	4	35	.38	50	.14	4	2.47	.01	.03	2	2
L0+00E 8+25N	3	10	12	84	.1	19	5	350	2.06	6	5	ND	1	31	1	2	2	71	.69	.022	5	26	.68	38	.15	2	2.06	.01	.02	1	5
L0+00E 7+75N	2	9	9	66	.1	16	5	369	2.06	3	5	ND	1	29	1	2	2	62	.56	.025	4	23	.75	33	.15	2	1.63	.01	.02	1	3
L0+00E 7+50N	17	17	17	28	.1	6	2	80	4.49	98	5	ND	1	12	1	2	2	179	.16	.037	5	24	.05	19	.08	2	2.39	.01	.01	1	5
L0+00E 7+25N	2	8	6	71	.1	17	9	5137	2.54	10	5	ND	1	35	1	2	2	64	.62	.013	3	24	.72	61	.19	5	1.51	.02	.03	1	3
L0+00E 7+00N	4	8	17	37	.1	7	1	294	2.92	11	5	ND	1	33	1	4	4	140	.65	.010	4	16	.21	24	.27	2	1.08	.01	.02	2	4
L0+00E 6+75N	4	32	19	60	.3	11	6	340	5.68	34	5	ND	2	33	1	4	2	104	.35	.024	3	31	.57	37	.13	2	3.37	.01	.02	1	1
L0+00E 6+50N	2	31	14	117	.1	22	7	535	3.93	54	5	ND	1	44	1	2	2	81	.65	.036	6	28	.92	55	.10	2	2.36	.02	.03	1	1
L0+00E 6+25N	3	67	35	161	.1	30	7	380	2.77	19	5	ND	1	51	1	4	2	80	.82	.055	7	30	.88	92	.11	3	3.54	.02	.03	1	3
L0+00E 6+00N	5	34	25	84	.1	15	6	361	4.20	40	5	ND	1	29	1	2	2	105	.43	.031	4	20	.68	55	.14	2	2.54	.02	.04	1	2
L0+00E 5+75N	1	7	2	66	.2	3	1	88	.28	2	5	ND	1	46	1	2	2	8	.37	.033	2	3	.07	34	.01	5	.20	.01	.03	1	1
STD C/AU-S	18	60	37	132	7.1	67	30	1018	4.14	42	18	7	36	44	19	15	16	57	.51	.092	34	56	.91	172	.06	38	1.89	.06	.14	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L0+00E 5+50N	2	20	23	40	.1	6	5	222	2.34	4	5	ND	1	17	1	2	2	29	.26	.019	5	8	.37	30	.02	7	1.38	.01	.05	1	4
L0+00E 5+25N	4	21	17	46	.2	6	5	204	3.66	13	5	ND	1	24	1	3	2	69	.32	.020	5	14	.50	32	.07	2	1.94	.02	.04	1	3
L0+00E 5+00N	1	24	8	68	.5	1	3	68	4.55	2	5	ND	1	8	1	2	2	27	.15	.089	4	4	.03	19	.01	2	1.14	.02	.04	1	7
L0+00E 4+75N	2	33	19	161	.5	6	50	2613	8.12	9	7	ND	1	19	1	3	10	29	.81	.071	5	8	.05	53	.02	2	2.00	.02	.06	1	1
L0+00E 4+50N	2	51	16	76	.7	1	2	85	.68	2	6	ND	1	13	1	2	2	20	.31	.130	9	6	.06	19	.01	3	2.22	.01	.04	1	6
L0+00E 4+00N	4	49	19	72	.1	6	5	286	3.27	5	5	ND	1	28	1	2	8	58	.38	.032	7	12	.48	23	.08	3	2.82	.01	.04	1	3
L0+00E 3+75N	6	54	23	62	.1	13	7	306	5.66	7	5	ND	1	38	1	2	2	81	.46	.032	7	16	.54	33	.10	2	3.39	.02	.04	1	7
L0+00E 3+00N	7	51	31	78	.4	15	9	352	5.64	9	6	ND	1	30	1	4	2	94	.45	.065	6	22	.64	24	.13	3	4.11	.01	.04	1	4
L0+00E 2+75N	11	66	45	99	.5	13	6	420	3.37	14	5	ND	2	50	1	7	2	109	.67	.047	8	23	.87	22	.21	2	4.31	.02	.04	6	4
L0+00E 2+50N	7	42	21	74	.4	14	7	399	3.94	9	5	ND	1	47	1	2	2	107	.67	.045	6	20	.80	33	.20	5	2.20	.02	.04	1	1
L0+00E 2+00N	8	41	35	71	.5	16	8	490	4.84	17	5	ND	1	48	1	2	2	125	.62	.039	6	29	.85	19	.24	6	3.05	.02	.03	1	4
L0+00E 1+75N	5	32	25	92	.3	12	7	292	4.68	15	5	ND	1	50	1	6	2	116	.68	.067	6	14	.69	24	.20	7	3.64	.02	.03	1	11
L0+00E 1+15N	6	27	24	60	.2	11	6	233	6.06	14	5	ND	1	43	1	2	2	172	.51	.037	5	19	.53	21	.33	2	2.17	.02	.03	1	2
L0+00E 1+00N	7	58	34	87	.4	21	14	1395	5.54	20	5	ND	1	43	1	4	2	136	.53	.062	6	35	.86	27	.23	6	4.68	.02	.03	1	5
L0+00E 0+75N	4	54	23	90	.2	12	9	414	5.07	12	5	ND	1	54	1	2	2	112	.70	.065	6	23	1.01	24	.19	2	3.49	.02	.04	3	2
L0+00E 0+50N	6	38	25	75	.3	12	6	355	6.18	17	5	ND	1	39	1	6	2	151	.59	.048	8	30	.67	29	.26	2	3.88	.02	.02	1	6
L0+00E 0+25N	4	73	16	88	.1	16	11	488	4.34	19	5	ND	1	65	1	2	2	98	1.22	.082	6	22	1.03	33	.17	2	4.19	.02	.06	1	3
L0+00E 0+00N	5	76	23	94	.1	15	16	519	4.79	16	5	ND	1	84	1	4	2	96	1.76	.091	6	20	1.04	35	.16	4	5.05	.02	.08	1	3
L1+50E 15+00N	2	34	14	136	.2	11	7	438	3.38	10	5	ND	1	41	1	2	2	89	1.06	.023	5	23	.53	38	.16	5	2.23	.02	.04	1	2
L1+50E 14+75N	1	827	12	78	1.0	83	44	312	7.46	25	5	ND	1	141	3	2	2	114	2.73	.053	2	66	.96	28	.24	3	4.14	.02	.03	1	3
L1+50E 14+50N	3	39	67	110	.1	14	8	360	3.78	13	5	ND	1	41	1	3	2	153	1.63	.016	5	32	.41	19	.27	8	3.08	.01	.02	1	3
L1+50E 14+25N	1	23	20	52	.1	6	1	28	1.57	2	5	ND	1	12	1	2	2	35	.19	.091	2	17	.04	18	.04	5	1.04	.01	.03	1	3
L1+50E 14+00N	2	6	7	51	.1	1	1	121	2.29	5	5	ND	1	14	1	3	2	74	.29	.018	2	9	.05	13	.14	5	.64	.01	.02	1	3
L1+50E 13+75N	2	14	52	120	.5	3	1	107	1.67	2	5	ND	1	16	1	2	2	60	.23	.060	3	15	.16	24	.10	3	1.09	.01	.04	1	2
L1+50E 13+50N	3	13	7	92	.3	3	2	41	2.56	2	5	ND	1	13	1	2	2	48	.18	.057	2	14	.03	19	.01	4	.97	.01	.03	1	3
L1+50E 13+25N	20	30	49	137	.6	11	9	426	4.55	11	6	ND	1	30	1	6	2	169	.51	.041	6	37	.49	41	.12	9	3.23	.01	.03	4	5
L1+50E 13+00N	6	12	48	68	.4	5	3	82	3.72	28	5	ND	1	18	1	4	2	145	.21	.053	4	20	.07	30	.05	3	1.52	.02	.05	3	4
L1+50E 12+75N	1	7	9	109	.1	1	3	212	4.50	2	5	ND	1	23	1	2	2	26	.44	.091	2	6	.07	30	.01	2	.40	.02	.06	1	2
L1+50E 12+50N	3	14	36	74	.1	18	7	549	4.71	12	5	ND	1	39	1	2	2	160	1.29	.033	4	27	.60	25	.20	3	1.84	.02	.03	1	1
L1+50E 12+25N	1	13	25	153	.4	5	4	70	2.48	4	5	ND	1	12	1	2	2	100	.29	.087	4	13	.03	13	.01	6	.98	.01	.02	2	2
L1+50E 12+00N	4	49	43	134	.1	21	6	347	3.21	16	5	ND	1	37	1	3	2	149	.91	.023	4	48	.67	35	.23	5	4.57	.01	.02	3	2
L1+50E 11+75N	1	8	13	113	1.3	6	1	45	3.50	2	5	ND	1	14	1	2	4	41	.17	.066	2	7	.05	19	.05	9	.60	.01	.06	1	1
L1+50E 11+50N	1	12	31	152	.7	3	1	53	1.25	3	5	ND	1	17	1	3	4	30	.26	.056	3	9	.08	28	.05	8	.80	.01	.05	1	2
L1+50E 11+25N	2	9	12	101	.3	3	1	24	2.03	3	5	ND	1	8	1	2	2	33	.15	.099	3	8	.03	16	.03	5	.67	.01	.05	1	1
L1+50E 11+00N	1	6	3	123	.2	5	1	70	.08	2	5	ND	1	33	2	2	2	2	.38	.045	2	2	.16	35	.01	9	.07	.02	.05	1	1
L1+50E 10+75N	4	15	22	93	1.0	5	3	113	3.64	5	5	ND	1	24	1	2	2	85	1.05	.084	4	14	.06	43	.07	2	1.19	.01	.04	1	1
STD C/AU-S	18	63	41	131	7.2	68	29	962	4.31	41	18	7	36	44	19	14	17	57	.51	.094	34	56	.92	173	.06	38	1.91	.06	.14	13	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L1+50E 10+50N	4	64	17	170	.1	24	8	508	4.87	17	5	ND	1	40	2	4	6	130	1.62	.030	4	47	.89	62	.21	6	5.08	.01	.03	3	9
L1+50E 10+25N	4	38	14	85	1.4	9	5	200	4.62	2	5	ND	1	28	1	2	2	124	.56	.034	3	27	.32	27	.20	3	2.24	.01	.03	1	16
L1+50E 10+00N	3	51	11	107	.1	20	8	487	5.01	11	5	ND	1	34	1	3	2	137	.81	.025	4	45	.73	33	.24	2	3.98	.01	.02	1	6
L1+50E 9+75N	3	16	17	38	.1	5	3	206	4.28	8	5	ND	1	30	1	3	10	167	.71	.014	3	22	.16	17	.24	4	1.27	.01	.02	1	3
L1+50E 9+50N	4	54	26	110	.2	19	7	396	5.33	13	5	ND	1	30	1	5	2	135	.60	.022	3	49	.74	29	.26	2	4.84	.01	.02	1	2
L1+50E 9+25N	4	29	20	66	.2	15	8	338	6.17	9	5	ND	1	28	1	4	4	162	.54	.018	4	37	.67	17	.30	4	2.29	.01	.02	3	1
L1+50E 9+00N	3	39	18	101	.1	15	6	338	4.19	16	5	ND	1	33	1	4	2	124	.65	.018	4	41	.70	26	.22	2	4.00	.01	.02	1	1
L1+50E 8+75N	19	72	17	2242	.7	49	11	7660	4.57	222	5	ND	1	43	44	3	5	232	3.37	.102	9	64	.31	172	.03	10	3.35	.01	.03	1	4
L1+50E 8+50N	6	48	24	562	.1	17	7	456	3.86	26	5	ND	1	31	2	6	11	148	.72	.023	4	43	.60	34	.21	4	4.14	.02	.02	2	6
L1+50E 8+25N	10	29	21	117	.1	9	3	311	3.16	26	5	ND	1	36	2	3	2	141	.81	.010	5	31	.29	23	.22	2	3.31	.02	.02	3	4
L1+50E 8+00N	19	27	16	169	.7	17	8	420	2.22	18	5	ND	1	38	2	2	2	133	1.11	.077	6	38	.53	57	.07	6	2.76	.02	.04	1	3
L1+50E 7+75N	21	24	22	127	1.5	15	5	197	2.51	29	8	ND	1	24	2	6	4	103	.44	.072	7	51	.33	40	.07	4	3.17	.01	.03	2	1
L1+50E 7+50N	12	16	22	67	2.1	8	3	158	1.49	7	5	ND	1	23	3	2	4	96	.58	.091	7	28	.16	37	.03	4	2.40	.01	.04	2	1
L1+50E 7+25N	2	12	13	51	.3	7	1	94	1.31	2	5	ND	1	18	1	2	2	29	.28	.056	2	11	.13	16	.04	4	.88	.01	.03	1	1
L1+50E 7+00N	12	14	2	119	.3	4	6	291	3.48	2	5	ND	1	17	2	2	3	29	.42	.112	2	7	.05	29	.01	6	.45	.01	.10	1	1
L1+50E 6+75N	4	9	9	60	.5	4	2	89	1.19	2	5	ND	1	10	1	2	2	33	.27	.104	3	12	.04	10	.01	2	.70	.01	.04	1	1
L1+50E 6+50N	6	15	7	45	.7	2	2	29	.68	8	5	ND	1	10	1	2	2	69	.40	.071	4	12	.03	13	.01	3	1.05	.01	.01	2	1
L1+50E 6+25N	8	14	10	57	.4	2	3	228	1.67	3	5	ND	1	7	1	2	2	60	.18	.083	4	11	.02	11	.01	3	.95	.01	.02	1	1
L1+50E 6+00N	2	12	14	38	.3	3	1	255	.90	2	5	ND	1	11	1	2	2	21	.13	.056	4	13	.02	28	.03	3	1.00	.02	.02	2	4
L1+50E 5+75N	9	25	13	61	1.5	6	1	96	.71	2	5	ND	1	20	1	2	3	30	.33	.088	4	28	.08	23	.02	2	1.33	.01	.04	1	2
L1+50E 5+50N	15	40	37	237	.7	23	16	556	5.20	27	5	ND	1	34	1	7	4	125	.91	.034	6	60	.71	41	.21	5	4.22	.01	.03	1	4
L1+50E 5+25N	12	31	18	103	.9	7	5	97	.67	2	5	ND	1	39	3	2	3	30	1.40	.092	8	14	.13	35	.02	7	1.79	.01	.02	1	1
L1+50E 5+00N	5	44	59	148	.4	19	6	566	3.59	28	5	ND	1	30	2	4	9	86	1.14	.082	7	33	.47	45	.12	8	4.27	.01	.02	2	3
L1+50E 4+75N	9	42	18	140	.1	24	12	776	4.23	40	5	ND	1	54	1	2	2	108	2.00	.069	6	33	1.09	43	.18	2	2.76	.02	.03	2	1
L1+50E 4+50N	11	32	13	91	.1	25	9	504	3.42	10	5	ND	1	50	1	2	7	100	1.20	.042	5	32	1.20	49	.21	2	2.86	.02	.03	3	2
L1+50E 4+25N	12	26	14	56	.2	5	3	135	2.81	27	5	ND	1	52	1	2	2	69	.53	.037	2	9	.32	28	.13	3	.71	.02	.02	1	3
L1+50E 4+00N	4	43	16	98	.3	20	7	348	2.71	10	5	ND	1	43	1	4	2	80	1.03	.074	6	31	.79	40	.14	2	2.28	.02	.03	2	2
L1+50E 3+75N	3	14	8	67	.1	8	4	231	2.43	9	5	ND	1	30	1	2	2	67	.58	.075	5	19	.33	21	.10	2	1.29	.02	.03	1	1
L1+50E 3+50N	5	19	10	56	.1	17	6	336	3.40	12	5	ND	1	41	1	3	5	98	.76	.031	5	30	.76	24	.23	2	2.17	.02	.03	1	1
L1+50E 3+25N	6	31	12	71	.1	20	6	423	4.33	15	5	ND	1	41	1	2	2	153	.84	.039	5	31	.92	15	.26	2	2.56	.02	.02	1	1
L1+50E 3+00N	6	30	29	79	.2	29	8	465	3.45	12	5	ND	1	57	1	3	2	144	1.01	.035	6	41	.93	19	.23	2	2.46	.02	.03	1	1
L1+50E 2+75N	4	29	22	65	.1	17	6	450	2.62	8	5	ND	1	56	1	3	2	79	1.43	.045	6	25	.73	28	.13	2	2.84	.01	.03	1	1
L1+50E 2+50N	3	31	19	56	.1	15	5	363	4.74	4	5	ND	1	51	1	3	4	125	.67	.024	5	39	.79	20	.23	2	4.27	.01	.02	1	1
L1+50E 2+25N	3	58	17	69	.1	24	8	463	3.33	15	5	ND	1	45	1	4	3	118	.75	.034	6	45	.96	22	.21	2	4.24	.01	.02	1	8
L1+50E 2+00N	4	49	30	70	.1	26	10	544	5.12	14	5	ND	1	54	1	5	2	125	.75	.022	5	55	1.08	20	.25	2	4.52	.01	.02	5	3
L1+50E 1+75N	4	32	23	79	.2	21	7	742	3.20	14	5	ND	1	103	1	5	6	117	1.76	.028	5	40	.89	11	.27	2	3.63	.01	.01	1	2
STD C/AU-S	18	63	38	131	7.4	67	30	1017	4.23	44	17	8	36	45	19	15	23	57	.52	.093	34	52	.92	172	.07	39	1.96	.06	.14	11	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L1+50E 1+50N	1	39	14	100	.2	18	12	772	4.22	5	5	ND	1	67	1	3	6	119	.89	.088	7	25	1.99	19	.20	2	5.05	.01	.03	1	6
L1+50E 1+25N	5	18	17	75	.1	22	6	442	3.00	10	5	ND	1	43	1	2	7	93	.46	.041	4	39	.77	19	.20	2	1.80	.01	.02	1	1
L1+50E 1+00N	3	88	20	143	.3	17	19	1059	4.37	21	5	ND	1	128	2	2	2	109	2.19	.116	6	24	1.54	47	.20	2	4.60	.01	.05	2	2
L1+50E 0+75N	4	29	11	59	.1	22	7	445	2.82	11	5	ND	1	63	1	2	2	102	.62	.039	5	41	.88	22	.19	2	2.53	.01	.03	1	2
L1+50E 0+50N	3	30	2	73	.1	26	9	663	2.10	7	5	ND	1	85	1	2	2	61	1.13	.096	5	15	.59	19	.11	2	1.88	.01	.03	1	1
L1+50E 0+25N	1	52	15	185	.2	103	28	1876	5.48	5	5	ND	1	119	1	4	2	98	1.22	.041	3	189	3.18	23	.16	2	4.93	.01	.03	1	2
L3+00E 15+00N	1	69	50	419	.5	26	10	427	2.96	13	5	ND	1	36	4	2	2	80	.67	.033	6	38	.59	32	.15	2	2.52	.01	.02	1	6
L3+00E 14+75N	1	37	59	199	.2	25	19	2028	7.31	8	5	ND	1	30	1	2	2	141	.66	.020	3	40	.67	35	.25	2	2.07	.02	.03	1	4
L3+00E 14+50N	1	8	2	77	.5	3	1	64	.12	2	5	ND	1	30	1	3	2	4	.71	.037	2	5	.09	11	.01	9	.11	.02	.04	1	1
L3+00E 14+25N	1	60	39	48	.7	31	9	252	13.24	2	5	2	1	24	1	5	2	261	.25	.016	2	120	.53	13	.62	2	2.25	.02	.02	1	4
L3+00E 14+00N	1	69	45	760	.3	37	12	414	4.13	13	5	ND	1	39	2	2	2	103	.79	.036	4	55	.85	34	.21	4	2.49	.03	.03	1	5
L3+00E 13+75N	1	42	42	196	.1	32	9	309	5.22	13	5	ND	1	30	2	2	2	119	.50	.070	8	54	.62	45	.14	2	5.04	.02	.03	1	7
L3+00E 13+50N	1	70	30	115	.2	40	10	302	6.24	13	5	ND	1	26	1	4	2	158	.40	.025	3	95	.94	32	.28	2	5.17	.01	.02	1	6
L3+00E 13+25N	2	35	67	123	.2	15	6	429	6.51	16	5	ND	1	25	1	4	2	143	.43	.020	3	45	.52	24	.22	2	3.54	.01	.02	2	8
L3+00E 13+00N	2	25	81	127	.3	16	6	416	6.08	14	5	ND	1	28	1	2	6	177	.76	.015	2	39	.33	20	.27	2	1.62	.01	.02	1	3
L3+00E 12+75N	3	22	39	214	.4	6	28	1939	3.35	8	5	ND	1	21	2	2	3	67	.28	.106	4	23	.13	36	.09	6	1.76	.01	.07	1	2
L3+00E 12+50N	1	7	7	140	.2	2	1	128	.20	2	5	ND	1	27	1	2	2	8	.49	.043	2	5	.08	14	.02	5	.11	.01	.07	1	1
L3+00E 12+25N	1	19	30	95	.1	15	5	332	3.23	10	5	ND	1	33	1	2	3	115	.57	.023	4	30	.55	28	.19	2	2.02	.01	.03	1	3
L3+00E 12+00N	1	29	35	121	.1	18	7	356	4.51	16	5	ND	1	36	2	3	4	145	.75	.020	4	33	.52	31	.24	2	1.87	.01	.03	1	6
L3+00E 11+75N	1	6	5	157	.2	3	1	127	.16	2	5	ND	1	39	1	2	2	7	.23	.042	2	6	.17	20	.01	8	.14	.02	.03	1	1
L3+00E 11+25N	1	51	43	121	.1	18	6	321	3.62	14	5	ND	1	26	1	2	2	134	.50	.020	5	40	.53	28	.20	4	3.77	.02	.02	1	7
L3+00E 11+00N	1	27	26	159	.1	13	5	247	4.32	11	5	ND	1	26	1	2	2	141	.59	.017	4	29	.29	25	.23	2	2.64	.01	.02	1	4
L3+00E 10+50N	1	25	31	114	.1	13	7	234	4.72	29	5	ND	1	18	1	3	4	117	.35	.037	3	22	.29	24	.08	2	2.63	.01	.02	1	2
L3+00E 10+25N	1	58	71	474	.3	16	7	765	9.01	26	5	ND	1	25	1	3	2	159	.65	.020	3	46	.35	33	.25	2	3.18	.01	.02	1	4
L3+00E 10+00N	1	49	43	340	.1	12	6	548	7.07	26	5	ND	1	24	1	4	2	145	.66	.024	3	31	.26	22	.22	2	2.49	.01	.02	1	9
L3+00E 9+75N	1	66	31	155	.1	22	10	642	4.70	19	5	ND	1	32	1	4	2	126	.58	.028	5	43	.60	53	.19	2	3.71	.01	.02	1	6
L3+00E 9+50N	2	40	23	129	.2	19	6	462	4.82	20	5	ND	1	25	1	4	2	138	.44	.035	5	44	.48	33	.20	7	3.55	.01	.02	2	4
L3+00E 9+25N	2	45	24	101	.5	18	8	737	7.32	14	5	ND	1	39	1	4	2	152	.66	.027	5	51	.49	45	.26	2	3.69	.02	.03	2	3
L3+00E 9+00N	2	18	20	55	.2	12	3	253	1.71	8	5	ND	1	31	1	4	2	84	.48	.022	4	27	.40	34	.19	3	1.94	.01	.02	2	4
L3+00E 8+75N	2	38	25	114	.4	15	5	396	4.42	14	5	ND	1	27	1	2	5	137	.43	.029	4	36	.38	35	.21	2	2.92	.02	.02	1	6
L3+00E 8+50N	1	61	29	220	.1	23	9	516	5.22	12	5	ND	1	28	1	2	2	126	.46	.027	4	47	.60	40	.26	2	3.96	.02	.03	1	8
L3+00E 8+25N	1	41	24	294	.1	23	18	900	5.42	22	5	ND	2	26	1	5	2	125	.48	.029	4	38	.38	79	.18	2	4.44	.02	.02	1	6
L3+00E 8+00N	1	44	30	152	.1	17	7	494	5.14	22	5	ND	1	28	1	2	3	133	.55	.025	5	38	.41	40	.23	2	3.52	.02	.02	2	6
L3+00E 7+75N	1	43	17	141	.4	20	7	682	4.03	15	5	ND	1	28	1	2	2	134	.39	.045	5	33	.57	34	.18	2	2.94	.01	.02	1	4
L3+00E 7+50N	4	54	20	184	.2	36	6	346	4.55	53	5	ND	1	24	1	4	2	175	.51	.029	7	48	.48	37	.19	3	4.96	.02	.02	1	7
L3+00E 7+25N	2	48	28	219	.7	35	6	346	3.41	24	5	ND	1	20	1	8	2	197	.49	.041	5	52	.53	36	.16	5	5.45	.02	.03	1	5
STD C/AU-S	17	59	41	132	6.7	68	31	1013	4.21	42	18	8	37	48	19	14	23	59	.45	.099	38	56	.85	176	.07	39	1.92	.06	.13	11	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L3+00E 7+00N	4	49	19	123	.3	20	6	341	3.89	18	5	ND	1	24	1	3	2	122	.50	.038	5	46	.67	34	.17	3	4.36	.01	.02	4	7
L3+00E 6+75N	5	27	19	120	.4	14	4	266	4.35	19	5	ND	1	18	1	4	3	146	.35	.019	5	47	.44	31	.16	2	3.75	.01	.02	2	6
L3+00E 6+50N	6	30	22	74	.3	16	5	284	4.61	12	5	ND	1	26	1	2	3	146	.45	.021	5	40	.51	20	.22	2	3.36	.01	.02	1	5
L3+00E 6+25N	5	37	39	110	.6	23	7	398	4.70	20	5	ND	1	28	1	5	2	128	.57	.031	5	40	.64	31	.19	5	3.64	.01	.02	2	9
L3+00E 6+00N	4	21	19	57	.1	12	6	263	7.16	7	5	ND	1	29	1	2	2	174	.50	.014	4	36	.51	20	.32	2	1.82	.01	.02	1	3
L3+00E 5+75N	1	7	2	95	.7	2	1	34	.39	2	5	ND	1	43	1	2	2	9	.60	.054	2	6	.15	31	.02	6	.26	.01	.03	1	1
L3+00E 5+50N	5	12	21	70	1.4	7	1	50	3.56	4	5	ND	1	27	1	3	2	76	1.13	.049	4	14	.08	34	.13	5	1.29	.01	.03	1	5
L3+00E 5+25N	3	40	26	112	.2	23	7	474	4.01	17	5	ND	1	31	1	6	2	97	.72	.049	6	30	.79	39	.17	2	3.52	.01	.03	2	1
L3+00E 5+00N	3	12	13	59	.7	5	1	33	.90	2	5	ND	1	19	1	2	2	35	.52	.053	3	14	.05	37	.09	3	1.00	.01	.02	1	2
L3+00E 4+75N	5	37	33	200	.1	31	11	539	3.29	12	5	ND	1	40	1	2	2	107	.98	.051	6	36	.95	47	.18	3	2.96	.02	.02	1	2
L3+00E 4+50N	5	38	19	170	.3	27	9	409	2.72	11	5	ND	1	32	1	2	2	100	.76	.041	6	40	.73	40	.18	6	3.49	.01	.02	1	4
L3+00E 4+25N	4	46	15	310	.1	36	11	1399	3.67	17	5	ND	1	47	1	2	2	77	1.50	.079	7	29	.77	55	.13	2	2.76	.01	.02	1	7
L3+00E 4+00N	1	8	4	145	.3	4	1	59	.34	2	5	ND	1	47	1	2	2	11	.50	.043	2	7	.29	29	.02	7	.36	.01	.03	1	1
L3+00E 3+50N	3	18	20	61	.1	10	4	280	8.05	22	5	ND	1	18	2	2	2	137	.45	.027	4	20	.47	26	.17	2	1.88	.01	.03	1	1
L3+00E 3+25N	3	31	19	64	.1	23	6	373	2.83	15	5	ND	1	33	1	5	2	108	.57	.036	5	34	.89	30	.22	5	2.93	.01	.02	1	3
L3+00E 3+00N	2	26	20	58	.1	14	7	364	3.56	13	5	ND	1	35	1	3	2	103	.67	.025	5	26	.87	30	.24	2	2.89	.01	.02	1	1
L3+00E 2+75N	2	46	22	88	.1	20	8	428	3.49	12	5	ND	1	44	1	5	2	112	.68	.041	5	29	.99	89	.22	2	3.83	.03	.03	1	2
L3+00E 2+50N	2	19	11	79	1.6	3	2	79	1.92	4	5	ND	1	15	1	6	7	29	.17	.104	5	9	.13	24	.04	8	1.90	.01	.03	2	3
L3+00E 2+25N	3	29	11	52	.1	10	4	234	4.11	20	5	ND	1	17	1	2	3	112	.28	.026	4	29	.61	20	.20	3	2.91	.01	.02	1	11
L3+00E 1+75N	1	9	2	109	.1	4	2	40	.46	2	5	ND	1	66	1	2	2	9	.58	.037	2	5	.18	59	.02	7	.64	.01	.02	1	3
L3+00E 1+50N	5	22	23	77	.2	13	6	233	3.65	14	5	ND	1	33	1	4	2	94	.35	.043	5	32	.65	25	.16	2	2.18	.01	.03	1	7
L3+00E 1+25N	5	54	20	95	.1	17	15	648	4.35	30	5	ND	1	66	1	3	2	101	2.06	.103	8	19	.88	39	.16	2	3.59	.02	.04	1	2
L3+00E 1+00N	1	37	10	80	.1	7	1	23	.32	2	5	ND	1	9	1	2	3	13	.09	.168	5	10	.04	15	.01	7	2.50	.01	.01	1	8
L3+00E 0+75N	3	14	11	65	.1	6	2	159	1.65	14	5	ND	1	24	1	2	4	74	.48	.056	5	18	.25	22	.12	2	1.52	.01	.02	1	4
L3+00E 0+50N	2	37	12	101	.1	9	5	199	3.35	10	5	ND	1	23	1	2	8	84	.53	.102	5	11	.52	30	.10	2	2.02	.01	.03	1	1
L3+00E 0+25N	1	4	2	99	.1	1	1	17	.10	2	5	ND	1	32	1	2	6	3	.68	.052	2	2	.13	11	.01	9	.14	.02	.03	1	1
L3+00E 0+00N	3	20	10	39	.1	59	10	278	3.35	10	5	ND	1	30	1	2	5	108	.83	.024	3	103	1.34	25	.22	3	2.13	.03	.03	3	1
L4+50E 11+75N	3	32	22	76	.1	18	5	312	3.14	10	5	ND	1	27	1	3	2	113	.79	.027	3	37	.56	30	.20	2	2.84	.01	.02	1	1
L4+50E 11+50N	3	17	45	85	.1	13	5	295	2.66	8	5	ND	1	32	1	2	2	145	.80	.021	4	35	.54	39	.20	2	2.55	.01	.02	1	1
L4+50E 11+25N	2	11	21	88	.2	7	18	1940	3.18	5	5	ND	1	35	1	2	2	87	1.10	.033	4	20	.21	35	.11	2	1.44	.01	.03	1	2
L4+50E 11+00N	3	18	42	201	.1	17	7	442	4.77	10	5	ND	1	39	1	2	2	151	.94	.026	4	32	.56	33	.20	5	2.03	.01	.02	1	2
L4+50E 10+50N	1	12	2	248	.1	4	3	318	.79	2	5	ND	1	32	4	2	2	25	1.40	.034	2	8	.11	18	.03	2	.47	.01	.02	1	1
L4+50E 10+25N	2	36	10	3185	.8	7	1	1766	.48	4	5	ND	1	102	44	2	2	17	5.93	.073	2	7	.08	39	.01	11	.45	.01	.02	1	1
L4+50E 10+00N	1	10	2	1290	.4	4	1	71	.06	2	5	ND	1	85	13	2	2	2	4.52	.033	2	8	.05	17	.01	10	.07	.01	.01	1	1
L4+50E 9+75N	1	3	2	135	.3	1	1	186	.15	2	5	ND	1	21	1	2	2	3	.84	.045	2	3	.09	7	.01	3	.05	.01	.03	1	3
L4+50E 9+50N	3	16	17	69	.2	8	4	512	4.26	7	5	ND	1	31	1	2	2	123	1.38	.020	3	19	.18	18	.16	2	1.46	.01	.01	1	1
STD C/AU-S	20	58	40	132	7.6	73	31	1025	4.29	42	17	8	36	47	20	15	20	60	.51	.092	36	56	.94	173	.07	39	2.00	.06	.14	12	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L4+50E 9+25N	3	25	23	64	.6	13	5	361	3.81	6	5	ND	1	38	1	6	2	129	.72	.025	4	22	.40	21	.19	4	1.35	.02	.03	1	6
L4+50E 9+00N	3	29	37	238	1.4	12	10	17720	3.84	2	5	ND	1	33	4	6	2	98	.79	.080	5	27	.38	73	.09	2	2.50	.02	.05	1	8
L4+50E 8+75N	3	34	19	86	.5	13	8	1570	4.68	6	5	ND	1	35	2	7	2	119	.83	.036	4	29	.40	19	.20	5	2.99	.01	.03	1	6
L4+50E 8+50N	2	17	23	95	.5	11	7	2080	4.59	9	5	ND	1	70	1	7	2	82	1.74	.038	4	15	.46	19	.16	7	2.04	.01	.02	1	5
L4+50E 8+25N	1	8	7	90	.4	4	1	296	.97	2	5	ND	1	45	1	2	7	11	.61	.039	2	4	.19	15	.03	3	.35	.01	.02	1	5
L4+50E 8+00N	1	82	40	687	1.2	7	18	38234	16.21	167	5	ND	5	15	16	2	4	32	5.24	.040	4	6	.11	77	.03	2	1.30	.01	.01	3	37
L4+50E 7+75N	4	42	29	129	.8	20	8	1061	4.67	13	5	ND	2	31	1	7	7	135	.67	.026	5	32	.54	53	.14	8	2.62	.01	.05	1	5
L4+50E 7+50N	3	71	72	388	.4	17	8	1199	4.77	38	5	ND	1	45	2	9	8	140	.94	.062	8	22	.82	85	.16	7	4.36	.03	.05	1	6
L4+50E 7+25N	3	35	27	91	.4	16	5	428	3.33	13	5	ND	1	33	1	7	2	115	.72	.030	6	28	.54	30	.16	8	2.38	.01	.03	1	2
L4+50E 7+00N	1	30	29	133	.3	8	4	815	2.11	5	5	ND	2	44	1	4	2	36	1.30	.036	16	10	.32	55	.06	6	2.53	.02	.06	1	3
L4+50E 6+75N	1	5	9	64	.4	1	1	105	1.41	2	5	ND	1	7	1	5	4	22	.12	.018	8	6	.09	23	.02	4	1.87	.01	.05	1	3
L4+50E 6+50N	3	18	11	59	.3	6	4	314	3.79	8	5	ND	1	38	1	4	9	141	.70	.021	3	17	.25	20	.22	2	1.25	.02	.03	1	2
L4+50E 6+25N	2	12	9	43	.6	11	4	394	2.10	12	5	ND	1	60	1	5	2	120	.92	.025	3	18	.18	16	.19	7	.77	.01	.02	3	5
L4+50E 6+00N	3	45	21	100	.3	23	8	493	3.41	9	5	ND	1	42	1	7	6	93	.93	.069	7	28	.97	45	.18	3	3.70	.02	.04	2	4
L4+50E 5+75N	3	66	17	127	.1	31	11	618	4.22	8	5	ND	1	51	1	5	2	107	1.02	.063	6	38	1.17	49	.20	3	3.41	.02	.04	1	6
L4+50E 5+50N	3	40	22	120	.2	26	7	533	3.44	13	5	ND	1	37	1	3	6	97	.88	.061	6	32	1.06	50	.18	3	3.10	.02	.04	1	3
L4+50E 5+25N	4	47	30	315	.6	84	21	4605	4.92	140	5	ND	1	57	3	9	2	137	1.60	.079	10	133	1.42	59	.16	4	4.66	.02	.06	1	4
L4+50E 5+00N	3	66	26	390	.6	45	12	1773	4.12	38	5	ND	1	59	5	6	2	126	2.35	.124	10	55	.93	113	.14	6	3.40	.04	.06	1	3
L4+50E 4+75N	5	23	42	95	.4	25	7	918	3.59	12	5	ND	1	59	1	3	2	103	1.12	.033	5	37	.63	34	.19	3	1.75	.02	.03	1	1
L4+50E 4+50N	22	25	27	66	.6	22	9	793	4.98	2	5	ND	1	46	1	2	2	127	1.14	.030	6	61	.46	34	.22	6	2.50	.02	.02	1	3
L4+50E 4+25N	3	20	21	94	.1	13	7	1375	2.83	7	5	ND	1	43	1	2	2	61	.96	.046	9	16	.44	40	.09	4	1.97	.02	.06	1	3
L4+50E 4+00N	4	54	37	155	.7	26	15	1564	3.77	15	6	ND	1	51	1	7	2	88	1.16	.057	9	24	.75	50	.15	2	3.53	.02	.03	1	1
L4+50E 3+75N	5	22	88	137	.8	14	24	15263	6.41	10	5	ND	1	48	1	4	2	209	1.87	.145	6	27	.22	43	.14	6	2.38	.01	.04	1	3
L4+50E 3+50N	2	66	22	151	.3	25	16	1180	3.73	13	5	ND	1	79	1	6	2	89	2.13	.075	7	24	.97	74	.14	6	4.60	.05	.04	1	5
L4+50E 3+25N	2	72	12	129	.1	30	22	996	3.82	43	5	ND	1	94	1	6	2	77	2.95	.063	5	17	.95	76	.12	6	5.42	.04	.04	1	7
L4+50E 3+00N	1	33	50	218	.4	20	14	4081	7.61	47	6	ND	2	40	2	6	2	64	5.58	.066	5	20	.68	35	.12	2	3.26	.02	.03	3	22
L4+50E 2+75N	4	52	21	160	1.5	33	19	1979	6.59	27	6	ND	3	35	2	7	6	120	4.06	.082	6	40	.73	33	.19	2	3.88	.01	.02	3	4
L4+50E 2+50N	3	51	16	83	.3	17	6	690	3.36	18	5	ND	1	43	1	3	15	78	1.08	.066	7	17	.47	86	.17	5	2.34	.05	.03	1	1
L4+50E 2+25N	2	17	19	57	.2	7	2	178	.79	2	5	ND	1	23	1	3	2	42	.45	.080	4	13	.09	51	.08	2	1.39	.01	.03	1	1
L4+50E 2+00N	2	10	14	47	.4	4	1	86	.50	2	5	ND	1	24	1	2	4	32	.28	.059	4	13	.08	37	.10	2	1.04	.01	.03	2	1
L4+50E 1+75N	2	14	13	48	.1	7	4	304	3.76	2	5	ND	1	37	1	3	2	102	.58	.040	5	14	.84	32	.27	4	2.49	.02	.03	1	2
L4+50E 1+50N	3	20	15	42	.7	9	36	14947	16.06	52	5	ND	2	24	4	5	2	119	.41	.061	5	12	.45	53	.08	11	2.12	.02	.04	1	1
L4+50E 1+25N	3	36	15	35	.1	17	5	316	5.73	17	5	ND	1	35	1	2	2	178	.57	.026	6	25	.34	40	.36	4	2.10	.02	.02	1	1
L4+50E 1+00N	1	9	2	82	.5	3	4	451	2.35	2	5	ND	1	14	1	3	2	20	.15	.096	2	7	.07	28	.02	3	.91	.01	.03	1	1
L4+50E 0+75N	1	11	15	103	.2	1	1	81	.98	2	5	ND	1	18	1	2	2	18	.15	.093	2	5	.07	26	.03	2	.41	.01	.06	1	3
L4+50E 0+50N	1	6	5	83	.1	1	1	52	3.11	2	5	ND	1	6	1	2	2	23	.05	.099	2	4	.03	24	.01	2	.44	.01	.03	1	2
STD C/AU-S	18	62	44	131	7.6	68	30	1025	4.18	41	18	7	36	45	20	15	18	58	.51	.091	35	53	.94	172	.07	40	1.93	.06	.14	12	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L4+50E 0+25N	1	2	2	53	.1	2	1	35	1.31	2	5	ND	1	4	1	2	2	6	.05	.053	2	3	.02	10	.01	2	.20	.01	.02	1	1
L4+50E 0+00N	1	8	8	85	.1	1	1	51	.55	2	5	ND	1	14	1	2	2	15	.10	.057	2	3	.05	31	.06	2	.41	.02	.04	1	2
L6+00E 12+00N	2	18	16	65	.1	13	5	304	4.18	5	5	ND	1	27	1	2	4	76	1.12	.022	3	19	.56	22	.16	6	1.30	.02	.03	1	2
L6+00E 11+75N	2	19	13	35	.3	7	5	341	5.80	10	5	ND	1	16	1	2	8	114	2.37	.010	3	22	.24	15	.23	5	1.72	.01	.02	1	3
L6+00E 11+25N	4	47	36	548	.4	25	15	1715	4.94	28	5	ND	1	52	5	2	2	113	1.94	.042	7	29	.67	120	.11	2	3.21	.01	.05	1	4
L6+00E 11+00N	1	36	11	71	.1	11	5	213	5.94	11	5	ND	1	24	2	2	2	138	.77	.019	4	38	.40	24	.23	2	3.63	.02	.02	1	5
L6+00E 10+75N	2	50	34	96	.7	13	6	361	5.13	9	5	ND	1	37	2	2	2	128	.90	.015	4	46	.55	30	.26	2	4.37	.02	.03	3	4
L6+00E 10+50N	2	57	23	115	.2	17	7	396	4.28	15	5	ND	1	31	2	6	2	112	1.10	.056	4	45	.66	46	.19	3	5.03	.02	.02	1	3
L6+00E 10+25N	1	11	6	139	1.4	4	1	43	.35	2	5	ND	1	38	1	2	2	8	.27	.023	2	9	.21	15	.02	3	.30	.03	.02	1	4
L6+00E 9+75N	1	49	48	173	.1	15	4	259	1.60	5	5	ND	1	48	1	2	2	73	1.01	.027	4	26	.70	64	.20	2	2.58	.03	.04	1	6
L6+00E 9+50N	1	53	71	172	.5	1	2	29	.39	2	5	ND	1	23	4	2	3	19	.50	.041	3	7	.04	29	.02	3	.84	.02	.02	1	5
L6+00E 9+25N	2	17	81	205	.1	7	3	545	1.45	6	5	ND	1	50	1	2	2	48	1.07	.017	4	14	.56	35	.12	4	1.79	.01	.03	1	3
L6+00E 9+00N	6	31	82	104	1.2	7	2	80	3.16	10	5	ND	1	26	2	2	6	89	.46	.066	8	22	.10	52	.04	3	2.18	.01	.03	1	4
L6+00E 8+75N	1	17	18	116	.9	5	3	142	.46	2	5	ND	1	26	1	2	2	15	.43	.086	5	6	.08	41	.02	2	1.13	.02	.03	1	2
L6+00E 8+50N	8	54	29	139	.1	19	6	424	3.79	12	5	ND	1	41	1	3	2	142	1.31	.039	7	39	.68	39	.18	2	4.13	.01	.02	1	26
L6+00E 8+00N	5	32	24	87	1.1	12	16	876	4.47	7	5	ND	1	26	1	2	3	156	.69	.039	5	27	.34	20	.21	2	2.39	.01	.03	1	4
L6+00E 7+75N	9	63	14	62	.5	11	7	513	6.02	18	5	ND	1	49	2	6	7	188	1.70	.042	6	38	.29	41	.22	9	3.29	.02	.03	3	5
L6+00E 7+50N	3	53	20	100	.4	21	30	3442	3.93	12	5	ND	1	41	2	3	2	115	1.30	.049	5	33	.83	38	.19	6	2.58	.02	.03	1	5
L6+00E 7+25N	2	61	20	98	.1	16	8	470	4.51	15	5	ND	1	29	1	2	7	116	.75	.039	5	37	.75	39	.22	7	4.20	.03	.03	1	2
L6+00E 7+00N	2	78	14	136	.3	25	15	1154	4.76	17	5	ND	1	43	1	2	2	118	1.05	.045	5	35	.85	86	.22	6	3.54	.04	.04	1	5
L6+00E 6+75N	3	38	27	90	.3	13	16	1415	4.60	10	5	ND	1	49	1	2	2	125	.83	.039	5	21	.86	33	.20	2	2.33	.02	.03	1	3
L6+00E 6+50N	3	43	20	108	.1	18	12	1028	4.84	13	5	ND	1	26	1	3	2	118	.66	.028	7	35	.47	34	.17	7	3.11	.02	.03	1	3
L6+00E 6+25N	1	20	20	99	1.0	6	12	1433	1.98	8	5	ND	1	27	1	2	4	43	.36	.069	9	8	.19	35	.05	5	1.71	.01	.04	1	3
L6+00E 6+00N	5	61	75	256	.8	23	28	6413	7.68	29	5	ND	1	28	2	6	2	226	2.35	.107	5	43	.32	27	.12	11	3.30	.01	.03	2	15
L6+00E 5+75N	3	32	22	78	.3	9	9	656	4.86	15	5	ND	1	22	1	2	6	181	.45	.049	5	20	.34	25	.21	8	2.29	.01	.03	1	4
L6+00E 5+50N	8	71	29	381	.9	46	16	1877	5.70	31	5	ND	1	34	1	8	6	352	.92	.062	5	57	.44	43	.19	5	3.44	.01	.02	3	2
L6+00E 5+25N	3	42	19	110	.3	14	28	6253	5.93	20	5	ND	1	57	1	2	2	176	1.03	.050	7	26	.56	30	.24	3	3.18	.01	.02	1	5
L6+00E 5+00N	2	36	36	89	1.6	8	12	3798	3.91	13	5	ND	1	45	1	5	2	99	.77	.064	5	19	.41	35	.15	6	2.77	.01	.03	1	2
L6+00E 4+75N	5	53	21	67	.1	22	7	1278	5.48	30	5	ND	1	41	1	2	2	277	.70	.053	2	59	.69	25	.24	2	1.79	.02	.02	2	4
L6+00E 4+50N	4	38	32	86	.2	18	5	508	2.92	14	5	ND	1	36	1	3	2	108	.77	.079	6	76	.44	43	.17	2	4.93	.01	.02	1	6
L6+00E 4+25N	3	24	67	117	.6	12	76	17894	7.22	16	5	ND	1	27	1	2	2	115	.50	.129	5	68	.19	72	.09	7	2.60	.01	.04	2	6
L6+00E 4+00N	7	15	106	92	.8	19	7	760	2.31	19	5	ND	1	48	1	4	2	99	.80	.055	5	74	.32	50	.15	4	2.23	.01	.04	1	2
L6+00E 3+75N	14	48	71	638	.1	20	12	1722	6.50	28	5	ND	1	28	1	7	4	143	.79	.059	10	55	.83	55	.22	8	6.07	.01	.01	4	6
L6+00E 3+50N	3	22	25	61	.1	7	3	198	1.79	15	5	ND	1	28	1	7	4	81	.56	.025	6	25	.29	38	.19	6	3.03	.01	.02	1	4
L6+00E 3+25N	7	30	43	141	.1	15	8	1056	5.21	13	5	ND	1	29	1	2	2	154	.92	.062	6	34	.50	38	.21	5	3.26	.01	.02	1	5
L6+00E 3+00N	2	7	12	65	.7	5	2	426	1.65	6	5	ND	1	25	1	2	2	100	2.27	.020	6	13	.04	17	.09	2	.72	.01	.01	1	14
STD C/AU-S	18	63	38	132	7.5	67	31	1013	4.12	41	22	8	36	48	19	17	24	57	.48	.090	34	56	.94	173	.06	41	1.98	.06	.14	13	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L6+00E 2+75N	1	3	4	145	.1	2	1	61	.23	2	5	ND	1	33	1	2	2	6	.75	.058	2	5	.08	19	.01	8	.13	.03	.04	1	6
L6+00E 2+50N	1	8	6	101	.2	2	1	76	.54	2	5	ND	1	17	1	2	2	19	.21	.082	2	5	.04	20	.03	5	.48	.03	.05	1	5
L6+00E 2+25N	1	2	9	137	.1	4	1	272	.18	2	5	ND	1	19	1	2	2	3	.13	.076	2	2	.09	14	.01	8	.09	.02	.06	1	4
L6+00E 2+00N	1	4	8	98	.2	1	1	29	.26	2	5	ND	1	15	1	2	2	4	.11	.066	2	2	.04	17	.01	2	.20	.01	.02	1	2
L6+00E 1+75N	1	2	4	67	.7	2	1	11	.92	2	5	ND	1	4	1	2	2	24	.04	.064	2	6	.02	13	.04	3	.98	.01	.02	1	7
L6+00E 1+50N	1	15	14	75	.4	7	3	152	2.47	2	5	ND	1	19	1	2	2	62	.22	.038	2	9	.23	30	.14	6	.96	.01	.04	1	7
L6+00E 1+25N	1	6	9	158	.8	2	1	56	1.07	2	5	ND	1	13	1	2	7	32	.13	.053	3	6	.14	24	.06	4	.79	.01	.01	1	5
L6+00E 1+00N	2	52	21	71	.1	18	6	277	2.36	8	5	ND	1	34	1	2	3	105	.37	.018	5	35	.83	65	.20	2	3.57	.01	.01	1	10
L6+00E 0+75N	1	2	10	101	.3	3	1	20	.61	2	5	ND	1	18	1	2	2	3	.06	.056	2	2	.10	83	.01	4	.15	.02	.03	1	4
L6+00E 0+50N	1	4	11	155	.1	2	1	25	.22	2	5	ND	1	23	1	2	2	3	.11	.043	2	2	.09	29	.01	2	.11	.02	.02	1	4
L6+00E 0+25N	1	5	7	120	.1	4	1	37	.42	2	5	ND	1	11	1	2	2	9	.07	.029	2	4	.09	23	.02	2	.29	.01	.01	1	2
L6+00E 0+00N	1	1	5	150	.1	4	1	26	.42	2	5	ND	1	12	1	2	3	2	.10	.050	2	2	.06	12	.01	2	.19	.02	.02	1	4
L7+50E 5+25N	3	72	23	128	.8	25	15	1389	5.36	35	5	ND	1	22	1	5	2	153	.34	.081	5	39	.64	31	.15	5	3.55	.01	.03	1	10
L7+50E 5+00N	4	51	16	124	.9	17	13	989	5.14	40	5	ND	1	27	1	2	8	194	.37	.054	3	31	.47	30	.14	6	2.05	.01	.03	1	9
L7+50E 4+75N	4	90	28	130	.4	17	7	542	4.49	25	5	ND	1	26	2	2	5	137	.39	.078	4	29	.53	54	.14	2	3.30	.02	.03	1	3
L7+50E 4+50N	6	52	26	137	3.2	20	6	372	5.90	26	5	ND	1	22	2	2	2	189	.23	.126	5	38	.28	57	.10	7	2.40	.01	.05	2	5
L7+50E 4+25N	17	46	20	186	1.6	22	6	237	5.64	52	5	ND	1	14	2	3	7	393	.13	.055	3	43	.16	60	.26	5	1.99	.01	.03	1	5
L7+50E 4+00N	3	50	21	116	1.2	26	10	549	5.22	28	5	ND	1	23	1	2	2	123	.36	.041	4	46	.79	41	.17	6	2.62	.02	.03	1	7
L7+50E 3+75N	1	32	11	86	2.8	22	4	61	2.04	3	5	ND	1	19	1	3	2	17	.23	.142	7	11	.04	83	.02	2	2.06	.01	.04	1	1
L7+50E 3+50N	1	10	13	172	.5	3	1	51	.38	2	5	ND	1	29	1	2	2	7	.41	.066	2	4	.12	16	.01	6	.25	.02	.02	1	5
L7+50E 3+25N	3	59	20	145	.2	59	7	281	5.37	38	5	ND	1	19	1	2	2	155	.30	.038	4	98	1.00	43	.15	2	2.50	.02	.02	1	4
L7+50E 3+00N	3	22	16	108	.6	10	1	63	1.74	5	5	ND	1	9	1	2	2	36	.12	.147	3	15	.07	34	.02	2	.97	.02	.06	1	3
L7+50E 2+75N	2	16	7	91	1.0	7	1	21	1.35	3	5	ND	1	7	1	3	6	35	.06	.183	4	9	.06	28	.02	5	.99	.01	.04	1	6
L7+50E 2+50N	4	21	14	100	.9	5	2	47	2.65	8	7	ND	1	13	1	2	8	48	.17	.105	4	21	.08	21	.04	3	1.50	.01	.03	4	5
L7+50E 2+25N	4	29	23	71	.6	13	4	236	3.19	16	5	ND	1	18	1	2	2	124	.30	.027	3	24	.63	22	.19	2	2.20	.01	.02	1	5
L7+50E 2+00N	1	10	7	196	.2	3	2	108	.75	2	5	ND	1	41	1	2	5	16	.36	.064	2	4	.15	66	.02	2	.49	.02	.06	1	4
L7+50E 1+75N	1	5	10	133	.7	3	1	41	.67	3	6	2	1	13	1	3	2	12	.16	.060	2	5	.05	24	.02	8	.33	.01	.03	2	6
L7+50E 1+50N	1	2	5	146	.2	5	1	17	.44	2	5	ND	1	7	1	2	5	11	.05	.070	2	6	.05	20	.02	2	.34	.01	.02	1	4
L7+50E 1+25N	1	1	8	50	.1	4	1	4	.09	2	5	ND	1	10	1	2	6	3	.03	.047	2	4	.06	13	.01	4	.13	.01	.01	1	4
L7+50E 1+00N	1	3	2	118	.1	3	1	16	.05	2	5	ND	1	57	1	2	4	1	.64	.037	2	3	.17	3	.01	2	.06	.02	.03	1	1
L7+50E 0+75N	2	24	18	92	.3	14	4	183	2.18	6	5	ND	1	16	1	2	6	97	.42	.038	5	21	.46	20	.14	5	1.83	.01	.01	1	6
L7+50E 0+50N	1	57	20	167	.1	27	10	830	3.59	11	5	ND	1	31	1	4	3	80	.46	.033	3	35	.68	95	.18	2	3.16	.01	.02	1	4
L7+50E 0+25N	1	4	2	126	.4	3	1	20	.31	2	5	ND	1	10	1	3	6	3	.03	.044	2	3	.08	17	.01	2	.10	.01	.02	1	4
L7+50E 0+00N	1	27	5	181	.1	10	4	395	2.05	2	5	ND	1	21	1	2	6	42	.24	.032	2	16	.22	34	.08	3	.82	.01	.01	1	2
L9+00E 10+75N	2	49	22	71	.1	18	7	287	3.34	16	5	ND	2	19	1	2	2	102	.41	.021	4	29	.67	15	.18	2	2.32	.01	.03	1	5
L9+00E 10+50N	3	31	47	110	.3	8	143	4596	6.50	4	5	ND	1	19	1	4	10	72	.31	.038	3	25	.27	24	.09	10	1.77	.01	.03	1	8
STD C/AU-S	18	59	45	132	7.1	70	31	1021	4.27	42	17	8	36	45	19	16	20	58	.51	.098	35	56	.93	172	.07	37	2.04	.06	.14	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L9+00E 10+25N	1	4	9	107	.1	4	1	107	.19	2	5	ND	1	25	1	2	2	4	1.16	.041	2	3	.11	10	.01	7	.13	.01	.03	1	2
L9+00E 10+00N	2	11	13	75	.4	9	10	280	4.83	14	5	ND	1	36	1	2	8	94	1.61	.045	2	11	.17	25	.09	2	1.12	.01	.03	1	7
L9+00E 9+75N	2	35	27	67	.3	11	9	402	5.14	10	5	ND	1	32	1	6	7	77	.62	.045	6	15	.96	14	.16	5	4.09	.01	.02	1	4
L9+00E 9+50N	2	17	28	51	.3	6	5	210	6.31	2	5	ND	1	21	1	4	3	79	.53	.051	3	12	.20	24	.15	6	1.68	.01	.02	2	2
L9+00E 9+25N	3	57	46	118	.1	27	12	459	6.25	7	5	ND	1	27	2	6	2	160	1.15	.034	4	51	.85	39	.26	3	3.99	.01	.02	3	2
L9+00E 9+00N	1	8	5	120	.4	3	2	51	.29	2	5	ND	1	55	1	2	3	6	1.74	.086	2	3	.10	8	.01	11	.18	.01	.07	1	2
L9+00E 8+75N	3	42	47	107	.1	15	7	296	6.21	16	5	ND	1	27	1	4	13	115	.85	.086	3	37	.53	30	.18	5	4.08	.01	.02	1	5
L9+00E 8+50N	4	30	51	129	.7	14	11	593	5.41	19	5	ND	1	26	1	8	8	164	1.44	.051	4	33	.39	25	.22	10	3.88	.01	.02	8	2
L9+00E 8+25N	3	48	65	185	.2	21	10	481	4.43	9	5	ND	1	33	1	7	2	113	.97	.042	4	38	.67	38	.16	4	3.21	.01	.02	2	2
L9+00E 8+00N	1	7	2	111	.8	4	1	60	.30	2	5	ND	1	25	1	2	2	8	.77	.052	2	5	.13	7	.01	3	.22	.01	.03	1	1
L9+00E 7+75N	2	40	81	300	.7	41	14	1894	4.83	181	5	ND	1	41	3	9	5	119	3.04	.092	7	42	.89	50	.12	10	4.32	.01	.04	5	6
L9+00E 7+50N	2	19	25	120	2.8	10	3	257	2.35	8	5	ND	1	39	1	2	3	85	.81	.042	2	22	.41	32	.12	4	1.51	.01	.02	1	2
L9+00E 7+00N	4	60	41	168	.6	22	8	745	4.77	32	5	ND	1	29	2	5	2	145	.91	.082	4	40	.67	34	.15	5	3.17	.01	.03	2	8
L9+00E 6+75N	2	42	46	313	.9	24	14	8005	4.95	38	5	ND	1	33	3	6	2	112	1.38	.113	5	32	.34	49	.09	4	4.50	.01	.03	5	3
L9+00E 6+50N	1	9	10	116	.2	5	1	332	.25	2	5	ND	1	57	1	2	4	6	.30	.053	2	4	.23	16	.01	6	.27	.01	.02	1	2
L9+00E 6+25N	4	11	18	63	.1	10	1	352	2.03	6	5	ND	1	33	1	2	2	110	1.03	.035	3	25	.17	15	.16	2	1.19	.01	.02	3	1
L9+00E 6+00N	4	23	17	100	1.3	10	4	464	3.03	13	5	ND	1	34	1	4	7	149	.73	.069	3	22	.19	35	.14	9	1.24	.01	.04	1	10
L9+00E 5+75N	1	15	14	166	1.5	7	1	299	.52	2	5	ND	1	45	1	2	2	21	1.14	.129	2	7	.15	47	.02	7	.43	.01	.05	1	2
L9+00E 5+50N	5	41	34	322	.5	39	9	1772	4.51	21	5	ND	1	35	2	4	2	196	1.22	.079	4	31	.69	34	.15	2	3.23	.01	.03	2	8
L9+00E 5+25N	1	8	2	212	2.9	6	1	210	.37	2	5	ND	1	39	1	2	2	12	.46	.099	2	5	.15	17	.01	4	.35	.01	.04	1	2
L9+00E 5+00N	13	34	27	85	1.1	16	5	416	3.99	24	5	ND	1	30	1	2	6	195	1.12	.035	3	39	.12	22	.18	6	1.76	.01	.02	1	3
L9+00E 4+75N	17	55	12	465	2.4	41	66	10883	2.62	21	5	ND	1	26	9	2	2	88	.89	.190	9	88	.24	91	.07	11	9.23	.01	.02	2	1
L9+00E 4+50N	7	34	31	213	1.3	23	28	2676	4.21	19	5	ND	1	30	2	9	2	103	.67	.085	5	42	.61	36	.12	2	3.99	.01	.03	2	1
L9+00E 4+25N	3	66	32	412	.4	48	11	1311	3.29	14	5	ND	1	46	1	3	2	97	1.41	.088	5	53	.83	57	.12	3	2.69	.01	.02	1	1
L9+00E 4+00N	8	43	43	158	4.7	14	9	291	6.20	7	5	ND	1	20	2	8	2	78	.32	.124	6	31	.11	37	.04	9	3.00	.01	.06	3	2
L9+00E 3+75N	5	16	22	80	.7	8	4	232	3.22	13	5	ND	1	25	1	4	2	89	.42	.035	4	17	.32	22	.14	4	1.23	.01	.03	1	3
L9+00E 3+50N	5	39	19	102	.6	29	6	492	5.18	22	5	ND	1	37	1	4	2	149	.99	.030	4	58	.55	25	.13	9	2.10	.01	.03	3	3
L9+00E 3+25N	1	7	11	127	.4	3	1	105	.18	2	5	ND	1	28	1	2	5	5	.87	.060	2	3	.12	8	.01	9	.13	.01	.03	1	2
L9+00E 3+0DN	2	11	8	69	2.1	6	1	236	1.16	3	5	ND	1	33	1	2	5	33	.59	.043	3	8	.11	53	.05	7	.60	.01	.06	1	1
L9+00E 2+75N	3	48	31	168	.3	31	11	770	4.17	21	5	ND	1	33	1	2	2	91	.86	.074	6	46	.96	47	.15	8	3.52	.02	.04	2	3
L9+00E 2+50N	1	24	16	176	1.0	17	4	532	2.31	7	5	ND	1	37	1	3	4	56	.87	.077	3	28	.40	41	.09	11	1.07	.01	.05	1	1
L9+00E 2+25N	1	11	10	258	.1	6	2	786	.71	2	5	ND	1	28	1	2	2	15	.96	.085	2	9	.22	53	.03	13	.47	.01	.05	2	4
L9+00E 2+00N	2	19	15	89	.5	9	2	64	2.31	2	5	ND	1	21	1	2	4	35	.34	.120	3	19	.13	53	.03	7	1.41	.01	.05	1	1
L9+00E 1+75N	2	34	10	85	.2	7	7	329	8.39	10	5	ND	1	20	3	4	2	161	.42	.055	4	13	.79	31	.25	2	2.51	.02	.06	1	1
L9+00E 1+50N	3	20	8	117	.1	15	9	514	4.93	7	5	ND	1	31	1	2	2	128	.49	.038	4	18	1.12	24	.19	10	2.61	.01	.03	1	1
L9+00E 1+25N	2	11	14	98	.4	6	7	321	3.43	5	5	ND	1	30	1	2	2	86	.62	.108	5	13	.91	39	.13	6	1.96	.02	.05	1	1
STD C/AU-S	18	62	38	131	7.9	66	31	1023	4.33	41	22	7	35	44	19	16	22	59	.53	.095	35	55	.92	173	.07	38	1.97	.06	.14	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L9+00E 1+00N	1	22	10	99	.1	46	3	291	4.39	28	5	ND	1	52	2	2	4	336	2.36	.988	25	78	.67	25	.05	4	1.16	.01	.03	1	5
L9+00E 0+75N	1	7	10	141	.2	6	1	37	.51	2	5	ND	1	14	1	2	2	14	.13	.138	3	11	.06	31	.02	2	.66	.02	.05	1	5
L9+00E 0+50N	3	8	13	123	.4	6	1	44	.50	2	5	ND	1	50	1	2	2	43	.26	.079	3	19	.14	68	.07	3	.48	.02	.03	1	2
L9+00E 0+25N	2	23	19	116	1.0	13	4	164	2.45	12	5	ND	1	35	1	4	2	72	.23	.033	3	19	.39	42	.15	4	1.09	.02	.03	1	15
L9+00E 0+00N	1	6	2	221	.3	2	1	38	.36	2	5	ND	1	25	1	2	2	3	.08	.074	2	2	.13	90	.01	5	.19	.03	.05	1	4
L21+00E 0+00S	2	87	3	43	.1	23	7	146	5.58	8	5	ND	1	24	2	2	2	136	.46	.052	2	114	1.04	22	.24	2	1.87	.05	.05	1	10
L21+00E 0+25S	2	34	5	33	.2	14	8	123	6.90	6	5	ND	2	10	2	3	6	249	.26	.024	2	48	.25	9	.26	4	1.15	.01	.03	1	9
L21+00E 0+50S	1	7	8	57	.3	4	1	37	.34	2	5	ND	1	24	1	2	2	11	.74	.072	2	7	.11	8	.02	5	.12	.01	.04	1	3
L21+00E 0+75S	1	12	6	88	.4	7	1	75	.23	2	5	ND	1	26	1	2	3	8	.65	.106	2	8	.09	10	.01	3	.09	.02	.06	1	4
L21+00E 1+25S	2	11	12	47	.5	3	1	40	2.14	2	5	ND	1	17	1	2	2	98	.55	.042	2	18	.05	12	.07	3	.37	.01	.02	2	9
L21+00E 1+50S	1	11	5	74	.2	1	1	70	.45	2	5	ND	1	20	1	2	2	6	.49	.121	2	3	.06	16	.01	5	.29	.02	.05	1	2
L21+00E 1+75S	1	18	7	74	.2	3	1	11	.28	2	5	ND	1	30	1	2	2	11	1.22	.113	3	3	.05	16	.01	6	.54	.02	.05	1	3
L21+00E 2+00S	3	131	47	128	.8	11	1	99	.72	3	5	ND	1	32	1	2	5	43	1.22	.091	8	37	.35	32	.04	2	2.88	.01	.02	1	9
L21+00E 2+25S	1	26	18	68	.3	5	1	34	.38	2	5	ND	1	19	1	2	4	17	.43	.100	3	23	.06	21	.02	4	.85	.01	.03	1	7
L21+00E 2+50S	1	43	8	40	.6	4	1	6	.20	2	5	ND	1	6	1	2	2	3	.08	.096	4	8	.01	16	.01	2	1.71	.01	.01	1	4
L21+00E 2+75S	1	25	7	31	.1	7	7	158	5.02	4	5	ND	3	10	1	2	2	124	.18	.018	2	29	.38	15	.22	2	.94	.01	.03	1	4
L21+00E 3+00S	1	14	7	61	.9	2	1	29	.28	2	5	ND	1	23	1	2	2	7	.53	.100	2	6	.09	15	.01	2	.37	.02	.05	1	2
L21+00E 3+25S	4	53	20	28	.1	2	6	61	6.16	9	5	ND	1	11	1	2	2	195	.15	.024	2	27	.08	10	.24	2	.91	.01	.03	1	8
L21+00E 3+50S	1	7	6	46	.3	4	1	47	.26	2	5	ND	1	51	1	2	2	8	.45	.041	2	4	.13	45	.01	5	.11	.02	.03	1	1
L21+00E 4+00S	3	17	14	39	.9	4	3	40	5.02	3	5	ND	1	14	1	2	2	119	.17	.063	3	19	.07	21	.13	4	.79	.01	.05	1	9
L22+50E 0+00S	4	45	23	50	.1	12	6	213	5.48	12	5	ND	1	21	2	2	2	172	.45	.017	3	63	.62	16	.26	2	2.15	.01	.03	1	22
L22+50E 0+25S	1	9	2	91	.1	8	3	16	3.50	2	5	ND	1	13	1	2	2	24	.38	.077	2	7	.03	15	.02	2	.34	.01	.03	1	1
L22+50E 0+50S	1	9	2	106	.3	1	7	14	17.57	4	5	ND	2	6	2	2	2	86	.07	.051	2	11	.03	13	.02	2	.42	.01	.02	1	6
L22+50E 0+75S	1	13	8	108	.1	2	1	16	1.15	2	5	ND	1	11	1	2	2	41	.16	.048	2	39	.04	11	.12	2	.38	.01	.03	1	3
L22+50E 1+00S	1	8	2	188	.4	1	1	22	.97	2	5	ND	1	33	1	2	2	6	.57	.066	2	3	.09	22	.01	2	.09	.01	.06	1	1
L22+50E 1+25S	1	5	2	108	.2	3	1	10	.13	2	5	ND	1	47	1	2	2	3	.44	.053	2	6	.19	18	.01	2	.09	.02	.04	1	1
L22+50E 1+50S	1	5	2	147	.1	2	1	22	.19	2	5	ND	1	59	1	2	3	1	.45	.056	2	5	.21	26	.01	4	.06	.02	.04	1	2
L22+50E 1+75S	1	7	3	114	.5	2	2	109	.17	2	5	ND	1	30	1	2	2	3	.51	.091	2	3	.11	15	.01	5	.14	.02	.07	1	2
L22+50E 2+00S	1	5	2	137	.6	4	1	14	.10	2	5	ND	1	30	1	2	2	1	.57	.083	2	4	.09	9	.01	2	.08	.02	.05	1	4
L22+50E 2+25S	1	18	10	90	1.4	2	1	11	.52	2	5	ND	1	9	1	2	2	16	.12	.098	2	5	.04	16	.03	4	.56	.01	.03	1	2
L22+50E 2+50S	2	33	11	28	.1	7	4	81	4.65	8	5	ND	2	11	1	2	2	184	.17	.016	2	36	.17	16	.24	2	.80	.01	.01	1	38
L22+50E 2+75S	1	4	2	70	.1	1	1	15	1.35	2	5	ND	1	15	1	2	2	4	.23	.068	2	3	.05	11	.01	5	.12	.01	.03	1	3
L22+50E 3+25S	6	35	8	47	.3	9	5	297	4.90	6	5	ND	2	11	1	2	2	149	.24	.019	3	22	.52	19	.18	3	1.60	.01	.02	3	16
L22+50E 3+50S	1	32	9	81	.2	9	6	276	2.63	4	5	ND	1	29	1	2	2	46	.55	.056	3	19	.69	36	.11	7	1.13	.02	.02	1	2
L22+50E 3+75S	2	180	46	109	.2	27	17	295	6.14	31	5	ND	2	20	3	2	4	127	.36	.033	4	50	.54	29	.26	3	6.13	.01	.02	1	9
L22+50E 4+00S	1	9	2	135	.8	3	1	28	.37	2	5	ND	1	43	1	2	2	10	.12	.037	2	5	.23	26	.02	7	.21	.02	.03	1	1
STD C/AU-S	18	63	41	132	6.9	68	31	951	4.19	43	18	6	36	44	18	15	19	56	.51	.098	37	55	.90	173	.06	38	1.92	.06	.14	11	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L22+50E 4+25S	3	76	26	79	.7	12	7	166	5.19	4	5	ND	1	25	1	2	2	114	.47	.022	2	50	.45	17	.25	2	7.08	.01	.02	1	1
L22+50E 4+50S	1	17	9	112	.4	8	1	36	.96	2	5	ND	1	32	1	2	3	23	.79	.062	2	14	.14	14	.05	7	.65	.01	.05	1	5
L22+50E 4+75S	3	44	20	56	.5	15	10	226	8.47	9	5	ND	1	18	1	2	2	195	.37	.017	3	38	.37	24	.34	2	1.88	.01	.03	1	3
STD C/AU-S	18	58	42	132	7.0	67	31	953	4.31	36	18	7	36	45	19	16	19	57	.50	.089	35	52	.93	172	.06	40	2.07	.06	.13	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
C 109451	1	1	4	37	.1	2	1	224	.04	6	5	ND	1	674	1	2	2	2	56.53	.024	2	2	.16	2	.01	2	.06	.01	.01	1	44
C 109452	2	25	33	238	.1	11	5	1081	2.48	22	5	ND	2	51	1	3	2	93	.80	.081	7	20	.34	89	.12	2	1.97	.07	.04	1	11
C 109453	1	87	108	21523√	.3	1	10	18558	2.14	2	5	ND	1	27	154	2	2	1	1.85	.018	2	8	.11	23	.01	2	.05	.01	.01	1	48
C 109454	1	3	7	736	.1	4	1	3543	1.54	5	5	ND	2	207	7	2	2	14	2.32	.094	9	6	.36	10	.11	2	1.61	.01	.01	1	4
C 109455	1	45	44	18438√	.2	2	11	17952	3.41	9	5	ND	1	19	136	2	2	2	1.02	.032	2	7	.18	13	.01	2	.18	.01	.01	1	1
C 109456	1	61	13	53	.1	6	10	190	4.08	4	5	ND	1	164	1	2	2	144	2.06	.122	2	5	.57	84	.10	2	3.25	.22	.05	2	5
C 109457	1	1	2	726	.1	39	13	8148	4.77	11	5	ND	1	2	4	2	2	8	2.51	.019	9	6	.46	150	.01	2	.28	.01	.01	1	3
C 109458	6	106	9	47	.1	23	5	3488	2.83	9	5	ND	1	62	2	2	2	104	1.44	.028	2	22	.23	77	.07	2	.69	.01	.01	1	7
C 109459	1	7	16	479	.1	5	3	3241	4.23	20	5	ND	3	60	6	4	2	6	.55	.010	17	5	.18	77	.01	3	1.85	.01	.07	1	6
C 109460	1	1	2	16	.1	3	1	190	.19	2	5	ND	3	4	1	2	2	1	.08	.016	11	3	.03	42	.01	3	.35	.02	.07	1	1
C 109461	2	1	2	47	.1	7	1	326	.30	3	5	ND	3	40	1	2	2	1	.63	.014	8	7	.06	166	.02	2	.38	.03	.06	1	5
C 109462	1	6	4	194	.4	2	10	12796	4.09	41	5	ND	2	83	1	3	2	5	11.66	.014	2	1	.91	11	.01	2	1.04	.01	.01	1	5
C 109463	1	1	7	23	.1	3	1	1430	1.66	3	5	ND	1	269	1	2	2	5	2.34	.014	11	3	.07	13	.03	2	1.33	.01	.04	1	8
C 109464	1	1112	5	26	3.5	36	23	136	1.55	2	5	ND	1	148	1	2	2	53	4.73	.020	2	43	.39	7	.18	6	2.13	.03	.01	1	20
C 109465	2	3	4	18	.1	8	7	220	6.88	67	5	ND	1	1	1	2	2	5	1.21	.011	2	7	.02	2	.01	2	.14	.01	.01	1	23
C 109466	2	8	5	11	.1	12	6	155	5.26	38	5	ND	1	1	1	2	2	4	.62	.006	2	10	.02	1	.01	2	.08	.01	.01	1	20
C 109467	1	146	95	16015√	1.0	7	8	12236	3.73	14	5	ND	2	38	116	3	2	6	1.83	.013	2	12	.45	48	.01	2	.45	.01	.01	1	7
C 109468	4	23	239	32993√	5.6	1	20	65549	13.32	32	6	ND	5	118	290	2	17	2	3.34	.020	2	16	.33	118	.01	2	.08	.01	.01	1	6
C 109469	1	9595√	485	99999√	15.2	2	43	1011	14.39	29	5	ND	1	4	889	2	2	2	.51	.013	2	24	.13	2	.01	2	.23	.01	.01	1	27
C 109470	1	14174√	1597	67785√	26.0	2	33	9347	31.07	54	5	ND	2	8	581	9	4	5	.15	.035	2	1	.12	15	.01	2	.35	.01	.01	3	40
C 109471	1	209	11098√	16628√	4.1	2	15	15523	1.71	9	5	ND	1	12	116	3	7	7	2.22	.027	2	8	2.24	19	.01	2	.66	.01	.01	1	8
C 109472	1	1768	133	50235√	.8	7	49	752	1.87	10	5	ND	1	202	439	2	2	14	1.62	.063	2	1	.39	3	.07	2	1.34	.01	.01	2	8
C 109473	1	2012	4512	99999√	6.4	3	24	5632	14.40	35	5	ND	1	4	879	2	5	3	.73	.025	2	1	1.19	2	.01	2	.17	.01	.01	3	13
C 109474	1	11671√	103	99999√	21.0	6	116	432	14.13	28	5	ND	1	3	1460	2	3	1	.04	.006	2	72	.01	1	.01	2	.04	.01	.01	1	39
C 109475	1	105	192	1936	.4	8	12	2119	6.88	20	5	ND	1	116	14	2	2	12	4.08	.058	2	7	1.20	31	.04	2	1.53	.01	.04	1	9
C 109476	6	79	9	652	.1	9	14	395	4.49	7	5	ND	2	99	5	2	2	123	.82	.083	3	10	1.55	102	.20	2	2.44	.09	.07	1	4
C 109477	1	406	39	18273√	2.1	1	15	31130	16.22	336	6	ND	3	46	158	2	3	2	6.72	.017	2	6	.21	20	.01	2	.14	.01	.01	2	49
STD C/AU-R	18	57	36	137	7.0	66	30	1022	3.78	42	22	6	36	47	18	16	21	58	.44	.097	37	55	.87	171	.07	39	1.84	.06	.14	13	530

√ ASSAY RECOMMENDED

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1-P8 SOIL P9-ROCK P - PULVERIZED AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: JAN 29 1990 DATE REPORT MAILED: Feb 2/90. SIGNED BY..........D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L4+50E 14+25N P	2	84	30	77	.8	12	51	640	8.70	4	5	ND	1	17	1	3	2	116	.22	.037	4	51	.26	24	.18	7	3.78	.01	.04	2	5
L4+50E 14+00N P	1	63	14	63	.5	25	106	3615	8.75	5	5	ND	1	19	1	2	2	137	.30	.025	3	54	.56	28	.22	4	2.54	.01	.02	1	2
L4+50E 13+75N P	1	289	17	112	.6	70	37	346	8.03	12	5	ND	1	44	2	3	2	152	.87	.032	2	82	.86	70	.30	4	6.26	.02	.04	1	3
L4+50E 13+50N P	1	89	18	80	.5	34	32	1101	7.20	4	5	ND	1	27	2	3	2	130	.41	.027	3	55	.76	29	.24	6	3.26	.02	.03	1	6
L4+50E 13+25N P	1	59	18	53	.4	20	8	224	7.20	9	5	ND	1	23	1	2	7	146	.37	.020	2	46	.45	20	.26	8	2.11	.01	.02	3	3
L4+50E 13+00N P	3	35	46	373	.7	18	25	1775	4.94	19	5	ND	1	45	3	5	2	97	1.31	.033	5	30	.53	77	.08	5	3.09	.01	.03	1	3
L4+50E 12+75N P	4	30	35	95	.5	9	5	249	8.84	11	5	ND	1	18	1	5	3	153	.36	.020	2	38	.20	25	.19	6	3.63	.01	.02	1	2
L4+50E 12+50N P	1	5	2	93	.1	4	1	57	.25	2	5	ND	1	27	1	2	2	8	1.45	.046	2	7	.06	9	.01	8	.15	.01	.03	1	7
L4+50E 12+25N P	1	44	40	95	.3	23	5	332	4.77	5	5	ND	1	26	1	2	6	124	.64	.025	3	61	.54	23	.21	3	3.78	.01	.02	2	6
L4+50E 12+00N P	1	100	21	100	.3	24	15	585	3.81	10	5	ND	1	43	2	3	2	89	.71	.051	5	34	.61	71	.14	2	2.61	.02	.03	1	7
L7+50E 11+00N P	2	52	25	62	.4	11	9	334	7.75	5	5	ND	1	20	1	4	2	109	.33	.018	4	32	.29	17	.11	2	2.37	.01	.02	1	5
L7+50E 10+75N P	3	31	27	101	.7	3	2	53	8.01	4	5	ND	1	9	1	2	2	86	.10	.056	4	17	.04	16	.04	5	1.12	.01	.03	1	3
L7+50E 10+50N P	1	5	11	29	.1	2	1	93	.71	2	5	ND	1	15	1	2	2	16	.15	.012	3	6	.09	21	.04	5	.60	.02	.06	1	8
L7+50E 10+25N P	2	18	13	57	.1	7	5	179	3.12	10	5	ND	2	21	1	2	2	77	.33	.025	4	15	.25	23	.11	3	1.91	.01	.04	1	1
L7+50E 10+00N P	1	25	30	56	.3	8	5	224	5.98	69	5	ND	1	16	1	2	2	123	.45	.025	2	19	.33	21	.15	4	1.84	.01	.01	1	1
L7+50E 9+75N P	1	27	16	110	.1	12	12	485	5.63	8	5	ND	1	19	1	2	2	96	.26	.028	4	23	1.05	18	.01	4	4.72	.01	.03	2	1
L7+50E 9+50N P	1	12	14	114	.3	6	3	205	2.24	98	5	ND	1	45	1	2	5	46	2.96	.040	2	8	.17	11	.06	7	1.11	.01	.03	1	2
L7+50E 9+25N P	1	23	39	118	.1	14	6	302	5.96	147	5	ND	1	21	2	6	4	113	.46	.019	2	17	.09	25	.12	3	1.35	.01	.02	1	2
L7+50E 9+00N P	1	37	43	114	.4	12	5	254	4.27	13	5	ND	1	20	2	4	2	121	.41	.021	4	25	.33	36	.16	2	3.70	.01	.02	1	9
L7+50E 8+75N P	1	26	22	142	.5	8	4	232	1.66	7	5	ND	1	28	1	2	2	57	.46	.044	2	13	.21	27	.09	6	1.45	.02	.03	1	1
L7+50E 8+50N P	1	8	30	157	.2	5	1	150	1.50	4	5	ND	1	20	1	2	2	40	.34	.020	4	10	.13	27	.04	2	1.26	.01	.03	2	3
L7+50E 8+25N P	1	50	127	244	.2	20	5	374	4.72	23	5	ND	3	24	2	4	2	102	.61	.035	6	37	.40	41	.12	5	6.56	.01	.02	1	7
L7+50E 8+00N P	1	22	46	224	.3	13	6	392	3.72	11	5	ND	1	46	2	3	2	120	.99	.026	4	29	.38	35	.13	2	3.38	.01	.02	1	6
L7+50E 7+75N P	7	22	35	255	1.2	6	21	6354	16.73	9	5	ND	1	72	3	4	2	82	1.63	.129	3	20	.15	133	.03	8	1.59	.01	.03	1	4
L7+50E 7+50N P	1	9	8	182	.3	4	1	931	.49	2	5	ND	1	27	1	2	2	17	.88	.071	2	5	.07	18	.03	7	.37	.01	.04	1	2
L7+50E 7+25N P	2	27	39	122	.6	16	4	548	3.64	10	5	ND	1	26	2	2	2	123	.52	.043	3	30	.37	26	.16	2	1.64	.01	.02	1	3
L7+50E 7+00N P	1	5	16	52	.3	4	1	107	.76	6	5	ND	1	22	1	3	2	59	.15	.034	3	5	.07	30	.09	5	1.17	.01	.02	1	3
L7+50E 6+75N P	1	10	12	137	1.0	4	1	512	.53	2	5	ND	1	31	1	2	2	29	.57	.088	2	5	.04	20	.03	5	.33	.01	.05	1	1
L7+50E 6+50N P	2	43	22	129	.7	20	7	629	4.05	18	5	ND	1	25	1	2	2	150	.48	.037	4	35	.49	27	.14	4	2.23	.01	.02	1	4
L7+50E 6+25N P	2	20	27	101	.8	10	4	356	4.49	14	5	ND	1	20	1	2	3	169	.42	.020	3	27	.24	15	.20	2	1.45	.01	.02	1	3
L7+50E 6+00N P	4	35	41	78	.5	9	6	801	8.26	29	5	ND	1	16	1	4	2	320	.50	.033	3	30	.06	12	.25	3	1.06	.01	.01	1	2
L7+50E 5+75N P	4	8	19	57	1.2	8	2	308	2.03	14	5	ND	1	20	1	3	2	177	.37	.046	3	15	.06	10	.12	3	.46	.01	.02	1	6
L7+50E 5+50N P	3	17	24	116	1.0	8	2	366	1.78	13	5	ND	1	27	1	2	4	97	.37	.070	3	12	.07	28	.10	3	.91	.01	.03	2	5
L13+50E 6+50N P	1	67	98	149	.1	18	6	293	5.01	13	5	ND	1	18	1	3	3	114	.27	.027	3	46	.48	27	.16	2	4.71	.01	.02	1	7
L13+50E 6+25N P	2	13	305	70	.2	4	1	52	.39	3	5	ND	1	18	1	2	4	50	.19	.020	4	29	.04	21	.14	2	1.25	.01	.02	1	3
L13+50E 6+00N P	1	9	17	117	.2	3	1	230	.37	2	5	ND	1	25	1	2	2	13	.08	.042	2	8	.20	17	.03	5	.43	.03	.05	1	2
STD C/AU-S	18	57	43	128	6.8	68	29	926	4.07	38	20	7	36	47	18	15	18	56	.44	.091	36	56	.80	174	.06	39	1.91	.06	.14	13	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L13+50E 5+75N P	1	20	13	63	.4	7	1	115	.59	2	5	ND	1	16	1	2	3	44	.31	.066	2	28	.13	27	.08	5	1.24	.01	.02	2	1
L13+50E 5+50N P	2	13	24	32	.1	5	2	115	2.05	7	5	ND	1	17	1	2	2	135	.32	.016	3	18	.15	16	.15	3	.92	.01	.02	2	6
L13+50E 5+25N P	1	24	19	110	.6	7	1	15	.29	2	5	ND	1	8	1	2	2	24	.07	.127	2	22	.02	24	.03	4	1.26	.01	.01	1	2
L13+50E 5+00N P	1	15	18	117	1.0	3	1	19	.60	2	5	ND	1	9	1	2	2	30	.10	.116	2	14	.03	21	.04	4	.79	.01	.02	1	5
L13+50E 4+75N P	1	13	16	71	.3	2	1	10	.42	2	5	ND	1	2	1	2	2	38	.03	.058	2	6	.01	9	.02	2	.47	.01	.01	1	1
L13+50E 4+50N P	2	14	23	50	.3	12	5	112	7.23	4	5	ND	1	10	1	4	5	231	.19	.012	2	32	.19	11	.32	3	.88	.01	.02	1	1
L13+50E 4+25N P	1	10	14	71	.5	3	1	13	.27	2	5	ND	1	9	1	2	2	44	.09	.066	2	16	.02	17	.08	4	.85	.01	.01	1	3
L13+50E 4+00N P	1	5	2	83	.1	3	1	25	2.89	2	5	ND	1	5	1	2	2	23	.06	.104	2	2	.02	13	.01	5	.40	.01	.04	1	4
L13+50E 3+75N P	1	10	8	145	.2	3	1	26	1.93	2	5	ND	1	13	1	2	3	32	.25	.082	2	4	.02	21	.01	7	.41	.01	.02	1	1
L13+50E 3+50N P	1	12	8	132	.3	2	1	40	.60	2	5	ND	1	20	1	2	2	37	.30	.076	2	2	.04	43	.01	4	.61	.02	.04	1	1
L13+50E 3+25N P	5	44	30	184	.8	16	8	478	1.50	4	5	ND	1	56	2	2	2	74	.84	.071	4	32	.88	83	.09	4	2.33	.01	.05	1	4
L13+50E 3+00N P	4	38	97	271	.3	29	8	436	1.64	8	5	ND	1	31	1	2	2	85	.78	.040	3	39	.65	152	.11	3	2.45	.01	.02	1	1
L13+50E 2+50N P	5	9	18	30	.1	6	1	119	2.49	3	5	ND	1	15	1	2	2	112	.19	.010	3	18	.19	35	.16	2	1.14	.01	.02	1	6
L13+50E 2+25N P	3	54	18	97	.2	21	5	310	3.38	8	5	ND	1	24	1	2	2	98	.39	.033	4	43	.68	32	.13	2	3.49	.01	.02	1	5
L13+50E 2+00N P	4	65	17	91	.5	19	6	277	4.06	10	5	ND	1	20	1	3	3	90	.27	.054	6	53	.55	33	.15	2	7.13	.01	.02	1	3
L13+50E 1+75N P	3	55	6	130	.2	20	13	617	3.32	15	5	ND	1	35	1	2	2	72	.56	.071	7	28	.76	47	.10	2	3.07	.01	.03	1	3
L13+50E 1+50N P	3	39	18	101	.3	11	5	293	3.70	10	5	ND	1	21	1	2	2	89	.27	.040	5	21	.47	33	.14	2	2.92	.01	.02	1	9
L13+50E 1+25N P	2	34	19	97	.4	10	6	334	5.06	9	5	ND	1	26	1	4	4	124	.32	.041	4	24	.44	33	.19	4	2.62	.01	.02	1	2
L13+50E 1+00N P	2	48	26	106	.5	11	7	524	3.88	7	5	ND	1	23	1	3	2	88	.30	.038	4	23	.48	30	.14	5	3.11	.01	.02	1	1
L13+50E 0+75N P	2	54	28	136	.4	19	6	345	4.43	16	5	ND	1	28	1	3	2	104	.41	.039	6	35	.63	33	.15	2	3.96	.01	.02	1	1
L13+50E 0+50N P	3	121	31	139	.6	69	17	384	4.92	11	5	ND	1	30	1	5	2	97	.29	.059	4	111	1.24	66	.12	3	5.41	.01	.02	1	1
L13+50E 0+25N P	5	91	13	85	.5	4	6	273	3.86	15	5	ND	1	31	1	2	2	63	.36	.078	7	10	.31	48	.10	2	3.52	.01	.02	1	3
L13+50E 0+00N P	5	85	22	108	2.8	9	7	254	5.94	5	5	ND	1	30	1	3	2	116	.22	.065	6	18	.34	48	.11	3	3.82	.01	.02	1	8
L15+00E 5+00N P	3	13	7	26	.3	6	4	79	2.28	4	5	ND	1	13	1	2	2	148	.19	.014	2	10	.06	14	.13	3	.53	.01	.01	1	1
L15+00E 4+75N P	2	12	15	77	.7	4	2	91	2.01	7	5	ND	1	21	1	2	2	126	.28	.024	2	12	.14	18	.16	4	.59	.01	.04	1	1
L15+00E 4+50N P	2	16	15	33	.2	5	4	131	3.20	5	5	ND	1	39	1	2	4	205	.29	.011	3	12	.28	15	.27	2	.91	.01	.01	1	4
L15+00E 4+25N P	1	10	8	97	.5	2	1	23	.21	2	5	ND	1	22	1	2	2	14	.30	.066	2	6	.04	44	.03	7	.44	.01	.03	1	2
L15+00E 4+00N P	1	4	8	91	.3	2	2	13	.34	2	5	ND	1	13	1	2	2	10	.23	.041	2	5	.02	26	.02	4	.34	.01	.01	1	2
L15+00E 3+75N P	1	3	6	130	.1	2	1	16	.16	2	5	ND	1	25	1	2	2	5	.27	.045	2	2	.04	48	.01	3	.16	.01	.01	1	2
L15+00E 3+50N P	1	4	5	69	.1	1	1	12	.04	2	5	ND	1	37	1	2	2	2	.45	.038	2	3	.11	23	.01	4	.06	.01	.03	1	2
L15+00E 3+25N P	1	6	4	125	.3	2	1	20	.14	2	5	ND	1	34	1	2	2	6	.67	.047	2	3	.07	47	.01	5	.37	.01	.02	1	2
L15+00E 3+00N P	3	18	8	115	.7	4	1	23	.41	2	5	ND	1	20	1	2	2	25	.59	.094	2	15	.03	32	.02	2	.79	.01	.02	1	1
L15+00E 2+75N P	1	10	13	54	.2	9	2	194	.79	2	5	ND	1	25	1	2	2	44	.44	.015	2	25	.39	24	.13	2	1.23	.01	.02	1	1
L15+00E 2+50N P	3	7	30	88	.3	5	1	54	.49	2	5	ND	1	19	1	2	3	35	.22	.045	3	17	.06	30	.07	4	1.12	.01	.02	1	5
L15+00E 2+25N P	1	7	7	83	.4	3	1	28	.53	2	5	ND	1	9	1	2	2	19	.14	.140	2	11	.03	20	.02	4	.89	.01	.03	1	4
L15+00E 2+00N P	4	7	28	77	.3	5	1	50	.44	2	5	ND	1	17	1	2	2	43	.18	.035	3	16	.05	30	.06	3	1.27	.01	.02	1	13
STD C/AU-S	18	57	37	127	6.8	68	29	933	3.94	44	19	8	36	47	18	16	18	56	.46	.098	36	55	.81	173	.06	38	1.86	.06	.14	12	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L15+00E 1+75N P	3	10	14	40	.1	5	1	97	.57	2	5	ND	1	23	1	2	2	41	.39	.012	3	12	.14	32	.08	2	1.00	.01	.02	2	9
L15+00E 1+50N P	5	13	16	64	.2	9	3	277	1.23	3	5	ND	1	28	1	2	2	68	.53	.015	3	21	.44	27	.13	2	1.35	.02	.02	1	11
L15+00E 1+25N P	1	7	6	109	.2	1	1	41	.07	2	5	ND	1	44	1	2	2	3	.44	.046	2	5	.10	28	.01	4	.11	.02	.04	1	4
L15+00E 1+00N P	4	31	30	65	.3	8	4	208	6.34	7	5	ND	1	21	2	2	2	153	.23	.023	3	31	.92	20	.21	2	2.11	.01	.01	1	2
L15+00E 0+75N P	7	11	19	79	.1	4	3	129	2.16	7	5	ND	1	18	1	2	2	123	.30	.012	3	14	.10	14	.12	3	.71	.01	.01	1	1
L15+00E 0+50N P	2	13	10	208	.4	5	2	135	.69	2	5	ND	1	68	2	2	2	18	3.08	.063	2	6	.16	78	.02	12	.59	.01	.05	1	2
L15+00E 0+25N P	1	40	24	330	.9	38	15	304	1.61	3	5	ND	1	47	1	3	2	52	1.76	.085	6	34	.76	62	.08	3	3.53	.01	.02	1	3
L15+00E 0+00N P	1	9	2	151	.6	2	1	1635	.19	2	5	ND	1	21	1	2	2	7	.83	.068	2	4	.06	26	.01	6	.14	.01	.04	1	1
L15+00E 0+25S P	5	10	12	89	.2	5	7	949	4.24	7	5	ND	1	56	1	2	2	134	.56	.029	3	11	.93	36	.14	2	1.76	.01	.02	1	2
L15+00E 0+50S P	4	12	15	76	.4	4	3	266	2.46	4	5	ND	1	46	2	3	2	95	.62	.027	3	11	.28	43	.14	3	1.18	.01	.03	1	1
L15+00E 0+75S P	2	9	5	88	.4	3	1	159	.34	2	5	ND	1	37	1	2	2	12	.71	.063	2	5	.15	48	.02	6	.26	.01	.05	1	1
L15+00E 1+25S P	9	24	10	109	.2	17	14	1356	4.14	7	5	ND	1	33	2	2	2	81	.79	.033	3	19	.56	36	.12	2	1.44	.02	.03	1	1
L15+00E 1+50S P	3	25	20	97	.4	9	4	245	4.00	6	5	ND	1	25	1	2	5	108	.45	.034	4	23	.43	31	.13	2	2.92	.01	.02	2	5
L15+00E 1+75S P	2	31	18	78	.4	9	7	271	3.85	5	5	ND	1	26	1	2	2	90	.23	.034	3	20	.39	55	.13	2	6.34	.01	.02	1	2
L15+00E 2+00S P	1	19	10	221	.3	5	3	901	1.86	5	5	ND	1	25	1	2	2	50	.81	.076	2	9	.34	35	.07	4	1.09	.02	.06	1	1
L15+00E 2+25S P	5	15	26	157	.4	7	15	1392	3.44	13	5	ND	1	33	2	2	3	87	1.25	.036	4	18	.22	45	.11	2	1.31	.01	.03	1	3
L15+00E 2+50S P	3	15	10	68	.3	4	2	100	2.03	5	5	ND	1	21	1	2	3	114	.40	.035	3	7	.10	26	.18	4	.65	.01	.03	1	1
L15+00E 2+75S P	3	10	10	130	.7	5	17	2507	1.23	6	5	ND	1	42	2	2	2	48	.81	.049	3	9	.13	76	.07	7	.65	.02	.05	1	1
L15+00E 3+00S P	12	19	31	315	1.3	18	12	1327	4.05	26	5	ND	1	35	3	2	3	145	1.00	.052	5	50	.30	55	.09	4	2.19	.01	.03	1	3
L15+00E 3+25S P	6	23	24	201	.4	14	11	1452	2.64	8	5	ND	1	37	3	2	2	87	.98	.044	4	28	.52	47	.09	3	1.83	.02	.03	1	1
L15+00E 3+50S P	11	21	23	256	1.1	12	9	1283	2.42	11	5	ND	1	39	4	2	2	105	1.26	.064	7	49	.24	54	.08	4	2.49	.01	.04	1	3
L15+00E 3+75S P	4	47	18	242	1.3	31	10	612	3.85	21	5	ND	1	49	1	2	2	104	1.19	.126	5	28	.27	94	.10	2	2.18	.02	.02	1	2
L15+50E 2+75N P	7	12	37	78	.3	13	2	180	.64	2	5	ND	1	27	1	2	3	75	.87	.021	3	29	.13	70	.13	2	1.31	.01	.02	1	2
L16+50E 5+00N P	2	15	23	64	.4	3	1	41	.89	2	5	ND	1	13	1	2	3	46	.15	.052	4	15	.04	24	.08	2	.94	.01	.03	1	8
L16+50E 4+75N P	2	32	26	98	.5	5	2	91	8.72	3	5	ND	1	18	1	2	6	99	.20	.048	3	24	.08	23	.13	4	1.09	.01	.04	1	4
L16+50E 4+50N P	1	37	16	144	.8	5	12	239	4.71	2	5	ND	1	26	1	2	2	38	.97	.117	7	11	.05	21	.02	6	1.38	.01	.03	1	2
L16+50E 4+25N P	1	52	12	106	.6	9	5	735	1.52	2	5	ND	1	75	2	3	2	17	4.24	.085	4	15	.09	27	.02	11	1.35	.01	.02	1	3
L16+50E 4+00N P	3	92	21	137	.8	21	12	3853	4.60	9	5	ND	1	54	2	3	2	77	2.12	.058	5	39	.35	53	.11	7	3.25	.01	.03	1	6
L16+50E 3+75N P	3	18	25	58	.2	3	3	250	1.28	4	5	ND	1	38	1	2	3	83	1.33	.022	5	19	.08	32	.12	2	1.02	.01	.02	1	13
L16+50E 3+50N P	3	55	22	99	.6	6	1	87	5.88	54	5	ND	1	12	1	2	2	109	.15	.105	4	15	.05	22	.02	2	1.45	.01	.03	1	3
L16+50E 3+00N P	3	24	20	61	.1	8	3	171	4.48	29	5	ND	1	24	1	2	2	128	.35	.020	3	23	.30	30	.13	2	1.42	.01	.02	1	5
L16+50E 2+75N P	4	5	19	80	.1	2	1	57	.44	2	5	ND	1	21	1	2	2	46	.26	.013	4	10	.05	19	.08	3	.61	.01	.03	1	13
L16+50E 2+25N P	1	53	18	166	.4	11	8	542	2.45	55	5	ND	1	138	2	4	2	43	18.74	.039	3	17	.26	25	.07	2	1.77	.01	.02	1	7
L16+50E 1+75N P	5	29	20	95	.3	11	6	253	5.41	7	5	ND	1	22	2	4	2	131	.52	.031	3	41	.48	26	.17	2	3.36	.01	.02	1	4
L16+50E 1+50N P	4	42	6	72	.4	23	6	312	4.05	7	5	ND	1	28	1	4	2	121	.67	.029	2	52	.84	32	.14	2	1.48	.02	.02	1	1
L16+50E 1+25N P	6	25	11	40	.2	7	5	126	4.12	8	5	ND	1	14	1	3	5	224	.39	.014	2	17	.08	12	.17	4	.63	.01	.01	1	4
STD C/AU-S	18	58	39	129	7.0	68	31	1009	4.05	42	17	8	36	48	19	16	19	58	.46	.092	37	55	.81	174	.07	38	1.93	.06	.14	12	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L16+50E 1+00N P	1	19	2	66	.3	4	1	30	1.58	2	5	ND	1	9	1	2	2	24	.10	.049	2	6	.03	14	.05	2	.70	.01	.02	1	1
L16+50E 0+75N P	2	30	18	80	.3	8	3	114	2.95	2	5	ND	1	22	1	3	3	93	.21	.035	3	17	.21	27	.16	5	1.34	.02	.05	1	2
L16+50E 0+50N P	1	32	10	133	.3	4	1	43	6.03	2	5	ND	1	9	1	2	3	56	.09	.057	2	10	.04	15	.05	6	.96	.01	.03	1	1
L16+50E 0+25N P	1	25	4	130	.2	5	2	66	4.95	2	5	ND	1	9	1	2	2	40	.08	.059	2	5	.04	14	.03	2	.71	.02	.04	1	1
L16+50E 0+00N P	5	15	7	28	.3	4	3	112	2.76	5	5	ND	1	19	1	2	5	145	.39	.016	2	9	.12	19	.17	2	.65	.01	.02	1	1
L16+50E 0+25S P	4	16	14	79	.4	7	2	140	1.53	2	5	ND	1	25	1	2	4	50	.39	.037	3	16	.27	25	.08	3	.99	.01	.02	2	32
L16+50E 0+50S P	2	21	9	110	.2	11	3	120	.39	5	5	ND	1	38	1	3	2	15	1.30	.073	4	15	.09	52	.02	8	2.92	.01	.02	1	1
L16+50E 0+75S P	8	28	13	171	.5	14	31	1394	3.00	9	5	ND	1	35	2	2	2	70	1.02	.061	7	19	.22	50	.05	4	3.15	.01	.03	1	2
L16+50E 1+00S P	10	36	15	107	.7	7	49	3043	2.93	5	5	ND	1	26	2	4	2	67	.51	.095	6	18	.39	49	.05	9	3.09	.02	.03	1	1
L16+50E 1+25S P	9	24	20	113	1.1	9	19	2385	5.09	6	5	ND	1	21	1	2	2	73	.36	.060	4	18	.22	34	.06	6	2.72	.01	.04	1	1
L16+50E 1+50S P	6	20	32	101	1.7	5	5	236	.81	2	5	ND	1	16	1	3	4	34	.19	.067	4	14	.10	35	.06	7	2.01	.01	.03	1	3
L16+50E 1+75S P	14	22	18	112	.5	9	5	310	.94	14	7	ND	1	34	1	2	2	38	.77	.076	6	16	.26	38	.03	7	1.97	.01	.02	1	2
L16+50E 2+00S P	14	14	16	38	.1	7	4	295	4.38	8	5	ND	1	20	1	2	2	122	.43	.013	3	15	.19	21	.14	2	1.41	.01	.02	1	5
L16+50E 2+25S P	14	29	20	103	.5	13	6	332	3.45	14	5	ND	1	28	1	2	2	105	.47	.037	4	28	.46	30	.12	3	1.96	.01	.03	1	2
L16+50E 2+50S P	5	17	25	52	.2	9	3	166	1.16	4	5	ND	1	20	1	2	2	77	.79	.018	3	25	.34	18	.11	5	1.37	.01	.02	2	1
L16+50E 2+75S P	5	12	8	32	.1	5	1	115	.92	2	5	ND	1	23	1	2	4	82	1.24	.018	2	24	.09	28	.13	4	.70	.01	.01	1	4
L16+50E 3+00S P	3	19	10	95	2.1	4	1	47	.98	2	5	ND	1	16	1	3	2	32	.24	.157	4	9	.05	31	.04	9	1.05	.01	.04	1	2
L16+50E 3+25S P	6	14	20	50	.4	4	1	53	1.61	2	5	ND	1	16	1	2	6	65	.23	.065	4	13	.05	24	.07	2	1.28	.01	.03	1	1
L16+50E 3+50S P	5	8	15	61	.5	13	3	365	1.87	2	5	ND	1	17	1	2	4	66	.36	.072	4	35	.31	24	.09	4	1.03	.02	.04	1	1
L16+50E 4+00S P	4	15	17	74	.3	7	2	80	.76	2	5	ND	1	23	1	2	5	37	.34	.080	4	22	.12	31	.05	2	1.22	.01	.03	1	1
L18+00E 5+00N P	4	8	10	52	.9	3	1	75	1.03	2	5	ND	1	23	1	2	3	41	.44	.029	3	7	.09	22	.07	3	.79	.01	.03	1	1
L18+00E 4+75N P	5	31	24	170	1.3	3	24	952	3.47	2	5	ND	1	20	2	3	2	37	.40	.122	5	19	.06	32	.03	8	2.07	.01	.05	1	1
L18+00E 4+50N P	12	17	43	49	1.2	2	58	3475	27.95	14	5	ND	1	11	1	2	5	136	.16	.036	2	25	.07	21	.06	4	1.69	.01	.03	1	1
L18+00E 4+25N P	5	22	17	181	.9	5	8	322	2.12	2	5	ND	1	27	2	2	2	36	.44	.084	4	10	.10	52	.04	4	1.24	.01	.05	1	1
L18+00E 4+00N P	2	30	12	142	.2	5	6	284	3.93	2	5	ND	1	10	1	2	2	44	.10	.068	3	8	.03	15	.02	2	.74	.01	.03	1	1
L18+00E 3+75N P	1	15	2	114	.1	2	1	40	.45	2	5	ND	1	11	1	2	2	10	.11	.061	2	4	.02	18	.01	2	.42	.01	.02	1	1
L18+00E 3+50N P	2	31	2	111	.5	4	1	74	4.04	2	5	ND	1	7	1	2	2	82	.07	.095	4	13	.03	13	.02	4	1.10	.01	.04	1	1
L18+00E 3+25N P	1	5	2	143	.1	1	1	24	.14	2	5	ND	1	34	1	3	2	3	.53	.042	2	4	.08	23	.01	3	.11	.01	.03	1	1
L18+00E 3+25N A P	1	36	8	72	.2	10	7	350	4.30	12	5	ND	1	18	1	2	2	93	.56	.049	4	18	.54	13	.20	5	1.50	.01	.02	1	1
L18+00E 3+00N P	1	19	4	50	.1	14	3	135	.98	2	5	ND	1	22	1	2	2	40	.50	.016	2	31	.35	18	.22	2	.81	.01	.03	1	2
L18+00E 2+50N P	1	12	9	103	.4	5	2	78	.93	4	5	ND	1	32	1	2	2	22	.91	.065	2	6	.12	11	.04	11	.45	.02	.03	1	1
L18+00E 2+25N P	2	38	11	56	.6	11	6	204	3.97	12	5	ND	1	23	1	2	2	123	.40	.019	3	34	.33	17	.18	5	1.47	.02	.02	1	2
L18+00E 2+00N P	1	4	2	131	.3	2	1	34	.10	2	5	ND	1	35	1	2	2	4	.53	.041	2	3	.11	10	.01	8	.13	.03	.03	1	1
L18+00E 1+75N P	2	16	27	104	.4	14	11	2263	3.37	138	5	ND	1	20	1	5	2	36	.82	.101	6	14	.10	13	.03	3	2.51	.01	.02	1	2
L18+00E 1+25N P	1	20	7	100	.7	5	3	273	2.06	8	5	ND	1	16	1	2	3	100	.48	.034	2	11	.12	14	.12	6	.70	.01	.03	1	2
L18+00E 1+00N P	1	65	17	97	.1	17	9	530	4.28	60	5	ND	1	21	1	2	2	73	.43	.038	4	43	.41	24	.11	2	5.62	.01	.02	1	4
STD C/AU-S	17	57	37	130	7.0	68	31	956	3.99	44	18	8	36	47	18	15	22	57	.47	.090	36	55	.82	174	.06	40	1.93	.06	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L18+00E 0+75N P	1	7	3	90	1.7	1	1	28	.14	2	5	ND	1	24	1	2	2	5	.54	.045	2	5	.08	6	.01	8	.13	.01	.03	1	1
L18+00E 0+50N P	1	8	5	108	.3	3	1	90	.30	2	5	ND	1	34	1	2	2	7	.55	.040	2	8	.16	22	.01	8	.46	.01	.02	1	1
L18+00E 0+25N P	1	4	2	97	.6	2	1	174	.06	2	5	ND	1	32	1	2	2	1	.80	.048	2	4	.06	24	.01	5	.11	.01	.03	1	1
L18+00E 0+00N P	48	22	111	109	1.5	4	82	81611	8.32	7	5	ND	1	22	4	2	14	140	.50	.071	2	21	.01	548	.03	2	1.24	.01	.03	1	1
L18+00E 0+25S P	7	16	36	100	.3	9	3	324	1.15	5	5	ND	1	24	1	2	2	67	.42	.014	3	29	.40	24	.12	4	1.39	.01	.02	1	1
L18+00E 0+50S P	10	6	37	47	.2	3	5	4524	1.02	2	5	ND	1	18	1	2	2	54	.30	.024	3	15	.06	53	.12	3	.85	.01	.02	2	8
L18+00E 0+75S P	9	9	9	125	.3	2	22	1672	6.34	2	5	ND	1	15	1	2	2	66	.27	.075	3	17	.12	28	.03	2	.99	.02	.04	1	4
L18+00E 1+00S P	4	6	7	96	.2	3	1	247	.44	2	5	ND	1	19	1	2	2	23	.21	.087	3	11	.05	23	.03	2	.71	.01	.03	1	2
L18+00E 1+25S P	1	4	4	143	.2	1	1	170	.09	2	5	ND	1	29	1	2	2	2	1.06	.047	2	3	.05	19	.01	7	.05	.01	.05	1	1
L18+00E 1+50S P	7	12	38	104	.7	9	8	502	2.85	2	5	ND	1	26	1	2	2	55	.39	.061	3	24	.22	26	.07	2	1.03	.01	.04	1	2
L18+00E 1+75S P	6	29	29	178	.6	33	18	5245	3.11	9	5	ND	1	41	3	2	2	72	.68	.050	5	55	1.04	72	.10	2	2.86	.01	.03	1	5
L18+00E 2+00S P	16	11	18	57	.2	3	3	211	3.37	11	5	ND	1	20	1	2	2	101	.26	.023	4	8	.13	28	.08	2	1.09	.01	.03	2	8
L18+00E 2+25S P	5	25	11	115	1.0	6	11	838	4.42	4	5	ND	1	14	2	2	2	73	.21	.068	4	18	.12	26	.05	5	1.57	.01	.04	1	3
L18+00E 2+50S P	2	17	8	110	.4	3	1	64	2.82	2	5	ND	1	8	1	2	2	26	.09	.103	3	3	.03	20	.01	2	.64	.01	.04	1	1
L18+00E 2+75S P	4	22	13	49	.2	5	3	178	1.97	4	5	ND	1	19	1	2	2	103	.26	.017	3	18	.12	18	.12	4	.82	.01	.02	3	1
L18+00E 3+00S P	5	16	6	92	.3	3	1	61	5.55	8	5	ND	1	13	1	2	2	35	.27	.063	2	5	.03	19	.02	3	.65	.01	.03	1	1
L18+00E 3+25S P	12	20	19	41	.4	3	3	184	2.92	9	5	ND	1	22	1	2	3	108	.29	.018	3	13	.19	25	.11	2	1.16	.01	.03	1	16
L18+00E 3+50S P	10	28	9	137	.5	12	20	3600	5.44	10	5	ND	1	28	2	2	4	86	.57	.039	4	21	.46	54	.08	3	2.10	.01	.03	1	1
L18+00E 3+75S P	2	9	5	147	.2	3	1	376	.30	2	5	ND	1	46	1	2	2	11	1.17	.048	2	4	.11	48	.02	9	.25	.01	.05	1	1
L18+00E 4+00S P	8	13	18	135	.6	3	2	297	1.10	2	5	ND	1	22	1	2	2	29	.28	.074	3	9	.08	34	.06	4	.91	.01	.05	1	2
L19+50E 5+00N P	1	7	8	175	.3	4	1	305	.79	2	5	ND	1	24	1	2	3	42	.76	.039	2	11	.12	13	.13	6	.21	.02	.05	1	3
L19+50E 4+75N P	1	20	7	214	.1	5	4	345	3.46	2	5	ND	1	25	1	2	3	35	.29	.079	2	7	.06	30	.04	4	.64	.02	.03	1	1
L19+50E 4+50N P	1	50	6	98	1.0	13	6	128	8.00	2	5	ND	1	21	1	2	3	231	.19	.040	2	48	.24	25	.38	3	1.64	.01	.03	1	5
L19+50E 4+25N P	1	243	8	82	.5	59	16	442	6.07	6	5	ND	1	43	1	3	2	128	.53	.055	3	82	1.54	21	.26	2	3.23	.02	.02	1	5
L19+50E 4+00N P	2	61	2	115	.4	34	8	278	6.86	3	5	ND	1	20	1	2	2	156	.35	.028	2	70	.77	13	.32	2	1.99	.02	.03	1	1
L19+50E 3+75N P	2	69	10	124	.4	14	9	569	6.36	7	5	ND	1	21	1	3	7	106	.29	.025	3	33	.53	26	.13	3	2.35	.01	.02	1	10
L19+50E 3+50N P	4	22	11	61	.3	10	5	223	5.05	5	5	ND	1	22	1	2	2	132	.23	.022	3	27	.55	21	.16	3	1.38	.01	.02	2	1
L19+50E 3+25N P	1	11	9	176	.4	4	3	434	1.07	2	5	ND	1	21	1	2	2	52	.47	.051	2	10	.25	15	.07	5	.36	.02	.05	1	2
L19+50E 3+00N P	3	20	2	78	.5	7	3	97	2.73	4	5	ND	1	22	1	2	3	152	.29	.016	2	54	.10	7	.20	6	.48	.01	.01	1	1
L19+50E 2+75N P	2	116	17	172	5.8	12	16	617	2.16	7	5	ND	1	86	2	2	2	56	2.30	.088	4	12	1.09	51	.06	6	2.17	.02	.05	3	1
L19+50E 2+50N P	1	6	3	123	.3	2	1	45	.09	2	5	ND	1	26	1	2	2	4	.58	.049	2	3	.03	7	.01	6	.09	.02	.02	1	1
L19+50E 2+25N P	4	43	5	63	.4	7	6	393	6.71	5	5	ND	1	19	1	2	2	158	.34	.025	2	26	.23	16	.20	2	1.23	.01	.02	1	1
L19+50E 2+00N P	2	18	11	117	.8	4	2	79	2.05	2	5	ND	1	25	1	2	5	83	.32	.065	3	9	.08	27	.08	9	.78	.01	.04	1	1
L19+50E 1+75N P	2	23	4	95	.9	7	3	210	2.59	2	5	ND	1	24	1	2	6	66	.26	.044	2	11	.22	24	.08	3	.80	.02	.02	1	4
L19+50E 1+25N P	1	15	41	246	1.4	4	2	3342	.56	4	5	ND	1	51	1	2	2	10	3.14	.100	2	5	.09	17	.01	14	.39	.02	.07	1	1
L19+50E 1+00N P	3	34	18	54	.7	6	4	103	5.60	15	5	ND	1	10	1	3	2	128	.14	.021	2	19	.05	11	.17	2	.87	.01	.01	1	4
STD C/AU-S	18	58	35	131	7.0	68	30	1023	4.02	42	21	8	36	47	19	15	20	58	.47	.091	37	55	.83	174	.07	40	1.92	.06	.14	13	47

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L19+50E 0+75N	5	44	28	53	.3	8	4	113	6.53	35	5	ND	1	12	1	2	7	149	.14	.019	2	29	.19	9	.13	3	1.13	.01	.01	1	8
L19+50E 0+50N	1	10	2	95	.2	3	1	29	.98	5	5	ND	1	16	1	2	2	32	.42	.031	2	6	.06	5	.03	2	.25	.01	.01	1	1
L19+50E 0+25N	2	7	4	118	.2	4	1	56	1.60	3	5	ND	1	26	1	2	2	48	.51	.035	2	4	.07	20	.04	4	.31	.01	.02	1	1
L19+50E 0+00S	3	15	14	39	.4	11	4	216	3.30	12	5	ND	1	18	1	2	2	126	.62	.020	2	21	.36	14	.17	2	.96	.01	.01	2	1
L19+50E 0+25S	1	4	2	105	.5	3	1	30	.27	2	5	ND	1	36	1	2	2	12	.40	.055	2	4	.16	11	.02	4	.14	.02	.04	1	1
L19+50E 0+50S	3	26	14	94	1.0	8	4	164	4.14	11	5	ND	1	18	1	2	4	116	.24	.089	2	25	.24	34	.12	2	1.70	.01	.01	1	4
L19+50E 0+50S A	4	16	6	50	.5	4	2	69	2.27	9	5	ND	1	16	1	3	2	137	.20	.019	2	11	.05	24	.14	2	.57	.01	.01	1	18
L19+50E 0+75S	3	60	19	168	.4	18	6	254	3.71	12	5	ND	1	21	1	2	2	94	.34	.030	3	34	.57	32	.13	2	2.93	.01	.02	1	4
L19+50E 1+00S	2	37	11	43	.3	10	4	108	4.17	10	5	ND	1	18	1	2	2	143	.21	.021	2	21	.25	18	.22	2	.86	.01	.02	2	9
L19+50E 1+25S	2	82	18	58	.2	19	8	239	5.24	9	5	ND	1	21	2	3	2	99	.25	.029	2	51	.58	17	.19	2	4.49	.01	.02	1	10
L19+50E 1+50S	3	38	12	53	.3	7	4	96	5.67	8	5	ND	1	14	1	2	4	199	.26	.031	2	24	.12	10	.21	2	.90	.01	.02	2	9
L19+50E 1+75S	4	24	2	69	.7	6	3	168	1.95	6	5	ND	1	25	1	2	3	93	.51	.041	2	16	.13	18	.08	4	.89	.01	.02	1	5
L19+50E 2+00S	2	91	13	68	.2	23	9	263	4.19	4	5	ND	1	22	2	2	2	107	.42	.031	2	36	.61	15	.21	2	2.93	.01	.02	1	5
L19+50E 2+25S	1	14	2	128	.7	5	2	83	1.18	2	5	ND	1	23	1	2	2	44	.58	.066	2	10	.11	15	.07	7	.42	.01	.03	1	3
L19+50E 2+50S	3	46	52	365	.3	14	11	1300	2.62	5	5	ND	1	44	4	2	2	60	1.41	.064	3	16	.38	61	.07	3	1.65	.01	.03	1	1
L19+50E 2+75S	1	58	13	88	.6	9	12	445	3.06	7	5	ND	1	91	1	2	2	76	1.87	.066	3	14	.70	349	.07	2	2.83	.02	.03	1	1
L19+50E 3+00S	1	35	22	242	1.5	12	11	1132	1.61	11	5	ND	1	78	2	2	2	39	2.00	.068	4	13	1.22	33	.08	2	1.72	.01	.01	1	1
L19+50E 3+25S	6	51	18	113	.6	12	8	396	3.34	11	5	ND	1	41	1	2	4	74	.76	.038	5	20	.63	46	.11	3	2.02	.01	.03	1	1
L19+50E 3+50S	5	70	15	115	.3	19	9	322	2.79	9	5	ND	1	40	2	2	2	75	.70	.044	4	31	.81	34	.11	2	2.18	.02	.04	1	5
L19+50E 3+75S	4	50	14	111	.3	13	6	227	5.39	7	5	ND	1	28	1	2	2	70	.42	.055	4	21	.45	29	.07	2	1.57	.02	.03	1	3
L19+50E 4+00S	3	22	13	78	.3	66	13	171	6.74	6	5	ND	1	7	1	5	2	121	.22	.038	2	90	1.64	11	.10	4	2.50	.03	.04	1	1
L21+00E 5+00N	1	252	11	131	.3	63	23	382	6.41	8	5	ND	1	58	2	6	2	140	.43	.026	2	100	1.50	40	.36	3	5.10	.01	.01	1	3
L21+00E 4+75N	1	26	15	53	.2	12	5	128	5.83	2	5	ND	1	16	1	2	2	201	.22	.025	2	26	.26	14	.30	2	1.17	.01	.02	1	6
L21+00E 4+50N	2	67	14	31	.3	14	7	160	9.68	3	5	ND	1	14	1	4	2	204	.24	.021	2	43	.41	6	.40	2	1.53	.01	.01	1	6
L21+00E 4+25N	1	64	5	39	.5	17	8	154	9.96	2	5	ND	1	15	2	4	2	218	.25	.020	2	71	.38	5	.50	2	3.71	.01	.01	2	5
L21+00E 4+00N	1	78	24	96	.4	34	12	410	5.73	5	5	ND	1	31	1	2	2	122	1.04	.021	2	71	1.12	6	.35	2	2.90	.01	.01	1	1
L21+00E 3+75N	4	37	15	26	.3	7	4	136	9.47	5	5	ND	1	13	1	2	2	189	.20	.022	2	37	.22	10	.26	2	1.17	.01	.01	1	18
L21+00E 3+50N	4	99	16	57	.2	21	8	328	5.87	10	5	ND	1	24	1	2	2	102	.40	.036	2	52	.79	19	.19	2	3.59	.02	.02	1	1
L21+00E 3+00N	1	10	4	68	.6	3	1	201	.90	2	5	ND	1	15	1	2	2	27	.70	.063	2	7	.08	6	.05	8	.22	.01	.03	1	4
L21+00E 2+50N	1	18	13	81	.3	4	2	694	.66	2	5	ND	1	25	1	2	2	17	.85	.078	2	9	.16	11	.04	7	.48	.01	.04	1	1
L21+00E 2+25N	1	64	15	73	.2	8	5	193	6.20	11	5	ND	1	18	1	2	2	114	.48	.018	2	32	.37	13	.13	2	3.17	.01	.01	1	9
L21+00E 2+00N	1	154	71	499	1.8	24	24	2357	5.08	19	6	ND	1	35	4	4	2	61	1.44	.341	8	48	.51	30	.09	4	6.69	.01	.02	1	4
L21+00E 1+75N	1	288	87	1039	2.8	48	43	10877	7.31	15	8	ND	1	36	8	2	2	67	1.47	.136	21	58	.52	68	.09	7	8.58	.01	.01	1	3
L21+00E 1+50N	1	160	35	374	1.8	28	31	11227	7.10	6	6	ND	1	39	5	2	2	88	1.70	.150	11	37	.24	73	.07	9	5.22	.01	.02	1	6
L21+00E 1+25N	1	35	19	83	1.1	12	9	4654	5.40	5	5	ND	1	33	2	2	2	173	1.00	.027	4	47	.10	50	.16	3	1.38	.01	.02	1	5
L21+00E 1+00N	1	37	14	31	.3	10	5	470	5.00	4	5	ND	1	91	2	2	2	145	.69	.021	2	30	.28	17	.32	2	1.64	.01	.01	2	10
STD C/AU-S	17	57	42	131	7.2	69	30	1019	4.18	43	20	8	36	48	20	15	21	59	.47	.094	37	57	.83	174	.07	38	1.96	.06	.14	13	49

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L21+00E 0+75N	2	53	10	26	.1	8	4	220	4.15	3	5	ND	1	22	1	2	7	141	.27	.024	3	38	.35	13	.21	2	2.70	.01	.01	1	14
L21+00E 0+50N	1	40	22	35	.2	12	7	228	7.90	2	5	ND	1	27	1	2	5	202	.28	.022	2	39	.40	8	.35	2	1.28	.01	.02	1	12
L21+00E 0+25N	1	60	23	58	.2	15	11	482	6.45	8	5	ND	1	21	1	2	2	142	.53	.038	3	42	.85	12	.26	2	3.27	.02	.02	1	13
L21+00E 1+00S	1	30	22	458	1.6	27	14	334	6.58	30	5	ND	1	18	4	2	5	741	3.80	.042	5	103	.28	5	.20	7	2.15	.01	.02	1	6
L22+50E 5+00N	1	39	16	94	.3	12	7	204	6.24	8	5	ND	1	15	2	2	4	217	.54	.038	3	41	.35	10	.24	2	1.65	.01	.02	1	7
L22+50E 4+75N	1	9	5	32	.1	5	3	103	3.32	2	5	ND	1	10	1	2	5	223	.28	.007	2	13	.09	5	.23	2	.60	.01	.01	1	11
L22+50E 4+50N	1	27	7	93	.1	7	3	114	3.00	6	5	ND	1	31	1	2	5	88	.24	.040	2	19	.25	19	.16	2	.86	.01	.03	1	10
L22+50E 4+25N	1	21	12	18	.1	3	1	59	1.65	2	5	ND	1	12	1	2	2	108	.14	.012	3	29	.09	12	.24	2	1.09	.01	.02	1	4
L22+50E 4+00N	1	52	2	20	.4	10	11	520	13.25	2	5	ND	1	16	1	2	5	203	.25	.016	2	30	.35	7	.35	2	1.36	.01	.02	1	8
L22+50E 3+75N	1	74	2	27	.1	22	9	162	6.30	2	5	ND	1	46	1	2	5	210	.44	.016	2	34	.63	4	.42	2	.93	.01	.01	1	9
L22+50E 3+50N	1	7	10	13	.1	4	2	83	1.35	2	5	ND	1	11	1	2	5	81	.17	.005	2	22	.15	8	.20	2	.56	.01	.01	1	3
L22+50E 3+25N	1	9	13	35	.3	3	1	55	1.13	2	5	ND	1	17	1	3	4	78	.15	.020	2	22	.10	11	.12	2	.60	.01	.02	1	5
L22+50E 3+00N	1	8	6	24	.1	3	2	68	2.04	2	5	ND	1	10	1	2	4	194	.18	.011	2	14	.06	7	.22	2	.59	.01	.01	1	8
L22+50E 2+75N	1	8	2	62	.1	3	2	16	1.11	2	5	ND	1	7	1	2	2	13	.11	.049	3	2	.02	14	.01	2	.44	.01	.01	1	3
L22+50E 2+50N	1	15	2	33	.1	10	4	126	3.02	3	5	ND	1	7	1	2	3	124	.17	.021	3	42	.38	10	.17	2	.75	.02	.02	1	3
L22+50E 2+25N	1	8	12	31	.1	1	1	22	1.87	5	5	ND	1	10	1	2	2	42	.06	.020	2	12	.02	20	.10	2	.58	.01	.02	2	10
L22+50E 2+00N	1	8	4	54	.2	4	2	62	1.04	2	5	ND	1	28	1	2	3	47	.41	.033	2	16	.17	17	.08	4	.32	.01	.03	1	5
L22+50E 1+75N	1	5	3	64	.2	1	1	14	.52	2	5	ND	1	26	1	2	4	16	.07	.029	2	8	.09	19	.05	4	.24	.01	.03	1	4
L22+50E 1+50N	2	11	23	33	.2	2	1	37	1.04	2	5	ND	1	13	1	2	6	43	.10	.029	3	15	.05	18	.12	2	.83	.01	.03	1	11
L22+50E 1+25N	5	69	20	117	.3	15	8	336	2.93	9	5	ND	1	41	1	2	3	77	.76	.042	5	24	.68	30	.12	2	2.33	.01	.03	2	7
L22+50E 1+00N	1	53	10	78	.2	10	6	252	3.44	2	5	ND	1	34	1	2	3	130	.69	.033	3	23	.46	52	.16	2	1.82	.01	.03	1	6
L22+50E 0+75N	1	31	14	116	.2	6	4	388	1.29	2	5	ND	1	21	1	2	4	47	.52	.062	4	9	.11	22	.03	2	1.00	.01	.02	1	1
L22+50E 0+50N	2	5	17	24	.1	2	1	78	3.09	3	5	ND	1	10	1	2	5	156	.12	.010	4	22	.06	11	.15	2	.83	.01	.02	1	9
L22+50E 0+25N	1	21	12	77	.2	6	2	50	.76	2	5	ND	1	13	1	3	4	58	.16	.043	3	36	.04	21	.09	2	.96	.01	.01	1	3
L24+00E 0+25S	1	22	4	65	.2	1	1	27	.84	2	5	ND	1	10	1	2	2	41	.09	.121	3	8	.03	20	.02	2	.69	.01	.03	1	3
L24+00E 0+50S	1	21	3	68	.2	3	1	14	.34	2	5	ND	1	11	1	2	3	31	.12	.117	3	11	.03	18	.03	4	.85	.01	.03	1	5
L24+00E 0+75S	1	14	10	27	.5	9	2	71	1.31	11	5	ND	1	21	1	2	2	55	.39	.019	2	30	.08	4	.10	2	.36	.01	.01	1	6
L24+00E 1+00S	1	53	12	132	.5	7	4	371	.47	2	5	ND	1	32	1	2	2	23	1.69	.076	4	11	.04	21	.01	3	1.05	.01	.01	1	1
L24+00E 1+25S	1	21	16	28	.4	12	6	119	3.77	5	5	ND	1	23	2	2	7	149	.30	.017	2	19	.26	22	.30	2	.71	.02	.02	2	5
L24+00E 1+50S	3	35	26	39	.1	9	5	173	5.03	4	5	ND	1	18	1	2	5	141	.22	.015	2	34	.31	15	.25	2	1.12	.01	.02	1	14
L24+00E 1+75S	1	8	2	115	.4	2	1	37	.51	2	5	ND	1	38	1	2	2	24	.49	.043	2	6	.12	20	.05	4	.16	.02	.04	1	3
L24+00E 2+00S	2	13	7	68	.2	3	3	65	1.21	2	5	ND	1	31	1	2	5	29	.42	.091	3	6	.07	33	.03	4	.49	.02	.04	1	4
L24+00E 2+25S	1	7	3	87	.1	1	1	30	.30	2	5	ND	1	22	1	2	3	12	.36	.035	2	4	.04	17	.01	2	.20	.01	.02	1	8
L24+00E 2+50S	1	3	3	58	.1	1	1	24	.07	2	5	ND	1	52	1	2	2	2	.17	.041	2	5	.18	14	.01	4	.05	.02	.05	1	2
L24+00E 2+75S	1	6	2	51	.4	2	1	14	.07	2	5	ND	1	41	1	2	2	1	.48	.045	2	4	.11	25	.01	7	.10	.01	.04	1	1
L24+00E 3+00S	1	4	8	93	1.0	1	1	94	.06	2	5	ND	1	43	1	2	5	2	.60	.063	2	4	.11	21	.01	8	.06	.01	.05	1	1
STD C/AU-S	18	58	37	129	6.9	68	30	1019	3.91	40	19	8	36	47	18	16	20	56	.47	.090	36	56	.82	173	.06	40	1.90	.06	.14	13	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
L24+00E 3+25S	1	31	10	69	1.7	5	1	89	.55	2	5	ND	1	13	1	2	2	16	.18	.159	2	10	.04	21	.02	8	.66	.01	.04	1	5
L24+00E 3+50S	2	18	6	20	.3	6	3	36	1.92	3	5	ND	1	7	1	2	2	86	.04	.017	2	15	.03	11	.06	3	.59	.01	.01	1	13
L24+00E 3+75S	1	84	15	52	.3	24	9	227	4.20	8	5	ND	1	19	1	2	3	101	.38	.054	3	47	.61	21	.16	2	3.10	.02	.02	1	2
L24+00E 4+00S	1	13	2	59	.3	4	1	33	.61	2	5	ND	1	16	1	2	2	26	.26	.101	2	9	.04	18	.02	8	.44	.01	.04	1	3
L24+00E 5+00S	1	22	5	66	.4	5	1	718	1.13	2	5	ND	1	32	1	2	2	41	.90	.080	2	10	.13	19	.05	9	.49	.01	.06	1	6
L24+00E 5+25S	1	15	9	89	1.2	3	1	281	.49	2	5	ND	1	26	1	2	2	19	.52	.097	2	7	.07	23	.03	7	.36	.02	.05	1	1
L24+00E 5+50S	2	103	23	116	.3	19	8	296	4.87	9	5	ND	1	34	1	2	2	94	.55	.046	4	31	.78	38	.11	3	2.20	.03	.03	1	10
L25+50E 0+00S	2	63	24	94	.3	29	8	281	4.99	9	5	ND	1	28	1	2	3	99	.46	.032	3	37	.76	22	.22	3	1.42	.02	.03	1	4
L25+50E 0+25S	1	40	18	111	.1	13	6	424	2.34	3	5	ND	1	41	2	2	2	68	.74	.070	3	19	.65	18	.13	3	1.13	.01	.02	1	11
L25+50E 0+50S	2	65	16	85	.3	14	8	353	5.84	4	5	ND	1	58	1	2	6	147	.82	.043	3	24	.47	31	.23	3	1.59	.03	.04	1	6
L25+50E 0+75S	2	28	11	104	.3	7	4	231	1.73	6	5	ND	1	38	1	2	3	50	.53	.042	4	14	.34	26	.11	2	.93	.01	.03	1	1
L25+50E 1+00S	2	26	9	39	.2	6	4	633	3.06	24	5	ND	1	15	1	2	3	91	.39	.035	3	13	.13	15	.07	2	.95	.01	.01	1	3
L25+50E 1+25S	1	107	6	55	.2	7	5	285	3.14	21	5	ND	1	47	1	2	2	60	2.69	.041	2	10	.15	14	.13	7	.64	.01	.02	1	4
L25+50E 1+50S	1	6	7	54	.2	3	1	204	.20	2	5	ND	1	24	1	2	2	7	1.00	.063	2	4	.05	11	.01	8	.10	.01	.04	1	5
L25+50E 1+75S	1	17	5	63	.7	5	5	4191	7.11	10	5	ND	1	46	1	2	3	9	3.47	.125	2	6	.02	93	.01	7	.42	.01	.01	1	4
L25+50E 2+25S	2	41	16	23	.1	5	3	213	6.65	5	5	ND	1	10	1	3	6	194	.25	.023	2	23	.07	11	.27	2	.89	.01	.02	1	1
L25+50E 2+50S	2	15	16	15	.1	2	1	292	2.08	2	5	ND	1	17	1	2	2	131	.65	.021	3	13	.07	24	.17	2	.81	.01	.02	1	15
L25+50E 2+75S	2	16	16	32	.3	5	5	1382	4.09	4	5	ND	1	16	1	2	2	106	.61	.034	3	18	.06	24	.11	2	1.25	.01	.03	2	1
L25+50E 3+00S	37	17	16	48	.4	3	5	480	17.01	59	6	ND	1	19	1	2	3	131	.39	.046	5	20	.11	36	.03	6	1.20	.01	.02	1	5
L25+50E 3+25S	4	37	18	48	.1	6	4	286	5.02	23	5	ND	1	16	1	2	2	139	.25	.024	2	20	.13	13	.12	2	.95	.01	.02	2	12
L25+50E 3+50S	14	38	17	80	.6	7	5	256	5.07	17	7	ND	1	24	1	2	2	84	.42	.041	4	17	.29	30	.06	2	1.45	.01	.03	1	9
L25+50E 3+75S	2	9	13	25	.1	8	2	176	1.62	2	5	ND	1	13	1	2	2	88	.20	.009	3	27	.34	11	.18	2	.75	.01	.02	1	10
L25+50E 4+00S	2	18	19	157	.2	63	15	466	6.36	2	5	ND	1	19	1	2	2	91	.34	.032	2	149	1.44	14	.13	2	1.84	.01	.02	1	2
L25+50E 4+50S	1	6	3	91	.1	4	1	37	.39	2	5	ND	1	53	1	2	2	11	.86	.027	2	8	.10	24	.02	2	.21	.01	.01	1	6
L25+50E 4+75S	1	20	8	103	.4	11	3	80	1.12	2	5	ND	1	39	1	2	3	20	.77	.071	2	23	.19	39	.02	4	.60	.01	.02	1	3
L25+50E 5+00S	1	5	4	63	.1	2	1	22	.13	2	5	ND	1	45	1	2	2	3	2.10	.028	2	6	.09	11	.01	2	.08	.01	.01	1	6
STD C/AU-S	18	57	44	128	6.7	68	31	947	4.01	42	20	8	36	47	19	15	22	57	.46	.091	36	55	.82	173	.06	37	1.88	.06	.14	13	48

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
C 109478	1	12	34	1691	.6	3	9	6810	36.51	64	5	ND	5	5	8	17	2	2	3.11	.013	3	5	.03	13	.01	4	.06	.01	.01	1	23
C 109479	1	166	9	40	.3	61	16	244	3.44	5	5	ND	1	125	1	7	4	76	1.51	.048	2	49	1.02	19	.20	4	2.55	.21	.02	1	8
C 109480	2	110	7	65	.2	31	6	245	3.54	17	5	ND	1	21	1	3	2	127	2.63	.049	2	117	.11	7	.46	2	2.38	.02	.01	1	4
C 109481	1	68	10	108	.1	21	21	710	4.80	4	5	ND	1	584	1	3	2	110	.88	.062	2	23	2.14	62	.12	2	2.65	.10	.05	1	11
C 109482	1	37	2	26	.1	8	8	269	2.35	6	5	ND	1	68	1	2	2	66	2.63	.079	6	8	.60	39	.16	6	2.22	.05	.03	1	1
C 109483	4	71	5	125	.1	5	12	225	2.80	10	5	ND	1	62	1	4	5	37	4.25	.092	5	3	.32	20	.11	6	3.18	.03	.01	1	3
C 109484	1	36	7	33	.1	10	13	315	1.89	6	5	ND	1	62	1	2	2	57	4.39	.086	4	6	.79	15	.13	7	3.16	.01	.01	1	5
C 109485	1	458	872	7318	8.9	9	18	4514	3.51	24	5	ND	1	8	68	2	18	11	1.48	.025	2	6	.22	13	.01	2	.12	.01	.01	1	10
C 109486	20	149	10	57	.6	38	12	569	7.34	35	5	ND	1	59	1	2	2	228	1.26	.083	5	24	.31	10	.07	5	1.44	.01	.01	1	9
C 109487	6	152	125	343	.5	41	10	1190	3.64	34	5	ND	1	42	3	2	2	86	3.41	.099	4	18	.08	9	.07	36	1.86	.01	.01	1	1
C 109488	8	92	63	637	.7	37	10	412	2.69	17	5	ND	1	17	8	4	4	104	2.63	.069	5	31	.11	54	.11	5	1.52	.03	.01	1	1
C 109489	2	69	13	38	.1	12	3	180	2.77	13	5	ND	1	14	1	3	3	71	.44	.055	6	22	.31	46	.22	2	.89	.04	.04	2	1
C 109490	1	5	3	615	.1	2	1	2285	1.72	4	5	ND	1	269	4	3	2	12	2.24	.109	8	3	.15	9	.14	3	1.63	.01	.01	1	4
C 109491	1	131	19	583	2.8	1	18	12875	31.64	90	5	ND	5	3	7	2	28	11	4.87	.029	2	2	.03	16	.04	2	.19	.01	.01	1	260
C 109492	2	88	18	464	.9	2	7	21026	26.07	80	6	ND	5	2	9	2	2	3	4.92	.013	2	2	.04	4	.01	2	.08	.01	.01	1	56
C 109493	1	2124	42	66476✓	8.1	3	49	12290	11.84	34	5	ND	2	3	812	2	8	2	1.86	.019	2	10	.14	3	.01	2	.13	.01	.01	3	27
C 109494	1	441	92	31254✓	1.6	2	16	7778	2.65	7	5	ND	1	33	295	2	2	8	1.17	.044	2	12	.16	2	.05	2	.24	.01	.01	1	13
C 109495	4	3056	29	534	25.7	74	228	1579	14.68	200	5	ND	1	20	4	2	30	59	5.38	.212	2	2	.70	4	.04	2	.98	.01	.01	2	280
C 109496	1	37	11	62	.2	8	12	367	2.16	20	5	ND	1	83	1	2	2	38	2.33	.069	5	2	.53	106	.11	4	2.07	.07	.05	1	6
C 109497	15	65	7	56	.4	6	9	376	3.31	26	5	ND	2	53	1	3	2	52	1.68	.073	6	5	.78	61	.13	3	1.91	.05	.05	1	14
C 109498	1	114	4	45	.1	64	17	332	4.23	3	5	ND	1	108	1	4	2	122	.97	.046	3	78	1.48	15	.40	2	1.92	.03	.01	2	2
C 109499	1	193	7	28	.1	21	9	254	2.23	10	5	ND	1	97	1	2	3	90	5.46	.030	2	42	.63	6	.22	4	6.07	.04	.04	1	7
C 109500	1	11	16	36	.1	1	1	347	.93	8	5	ND	5	237	1	2	2	5	6.29	.010	10	1	.25	21	.06	2	9.45	.01	.07	1	9
STD C/AU-R	17	60	38	133	7.1	66	30	944	3.67	42	19	7	39	48	18	18	20	60	.46	.096	39	56	.84	184	.07	39	1.73	.06	.13	12	520

✓ **ASSAY RECOMMENDED**

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: P1 SILT P2 ROCK

DATE RECEIVED: FEB 7 1990 **DATE REPORT MAILED:** Feb 9/90. **SIGNED BY** C. Leong ..D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN File # 90-0321 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
C 109960	2	37	18	208	.2	19	10	491	2.56	9	5	ND	1	59	2	2	2	90	2.24	.033	4	24	.66	27	.22	2	1.63	.02	.02	1
C 109962	6	107	18	88	.1	34	18	528	5.19	13	5	ND	1	94	1	2	2	98	.89	.053	4	49	1.54	45	.16	4	2.66	.03	.05	1
C 109963	3	38	28	201	.7	18	12	691	3.96	12	5	ND	1	75	2	2	3	100	2.65	.030	4	25	.65	25	.19	5	1.68	.02	.02	1
C 109966	7	126	12	88	.1	65	41	494	11.37	8	5	ND	1	73	1	2	2	130	.69	.052	4	46	1.26	33	.15	3	2.24	.02	.04	1
C 109969	7	37	9	263	.5	51	19	2270	4.24	15	5	ND	1	44	5	2	2	102	.92	.094	6	24	.45	172	.01	3	1.91	.01	.05	1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM
C 109952	2	29	7	28	.1	3	3	105	1.34	4	5	ND	3	91	1	2	2	27	2.73	.020	8	5	.27	24	.07	2	3.52	.02	.05	1
C 109953	1	17	52	89	.2	5	4	449	.80	3	5	ND	2	155	1	2	2	10	3.28	.011	3	4	.31	22	.05	2	4.31	.01	.05	1
C 109954	1	58	9	79	.1	11	14	650	3.03	3	5	ND	1	91	1	2	2	50	1.38	.033	4	6	1.46	24	.16	2	3.15	.01	.04	1
C 109955	1	62	9	21	.2	23	12	244	4.02	4	5	ND	1	108	1	2	2	125	2.51	.039	3	31	.65	14	.28	3	3.23	.40	.03	1
C 109956	1	638	13	47	.4	28	18	368	6.79	4	5	ND	1	43	1	2	2	162	2.27	.068	2	37	.73	22	.35	5	2.13	.15	.07	1
C 109957	43	277	7	47	.2	9	19	242	4.02	15	5	ND	3	34	1	2	2	46	.91	.037	6	5	.94	47	.08	2	2.02	.02	.06	1
C 109958	4	222	23	107	.4	58	14	545	4.69	4	5	ND	1	72	1	2	3	89	1.76	.068	6	210	1.89	51	.12	3	3.63	.08	.08	1
C 109959	44	281	11	26	.1	23	21	190	5.11	10	5	ND	1	27	1	2	2	217	.41	.023	3	189	2.11	42	.27	3	2.61	.02	.17	1
C 109961	1	60	6	33	.2	8	12	213	3.94	5	5	ND	1	136	1	2	2	139	2.08	.077	3	12	.70	134	.10	8	2.40	.14	.07	1
C 109964	1	20	24	38	.1	70	52	163	12.47	5	5	ND	1	114	1	2	2	23	2.33	.097	3	21	.31	15	.03	8	3.49	.41	.05	1
C 109965	1	29	226	187	.4	13	6	308	.86	2	5	ND	1	113	4	2	4	22	18.23	.010	2	25	.42	12	.04	2	5.64	.01	.03	1
C 109967	1	46	9	37	.1	47	23	323	4.65	3	5	ND	1	116	1	2	2	125	5.43	.070	4	87	2.35	27	.16	2	7.88	.02	.06	1
C 109968	5	42	10	15	.1	11	11	192	5.64	8	5	ND	2	78	1	2	2	78	1.47	.051	5	13	.89	87	.10	4	3.24	.03	.19	1
STD C	19	59	43	134	6.9	68	31	1013	3.90	42	22	7	38	48	19	16	17	59	.45	.099	38	53	.90	176	.07	40	1.92	.06	.13	12

ACME ANALYTICAL LABORATORIES LTD.
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PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: FEB 6 1990
DATE REPORT MAILED: Feb. 12/90.

ASSAY CERTIFICATE

AG** AND AU** BY FIRE ASSAY FROM 1/2 A.T.
- SAMPLE TYPE: ROCK PULP

SIGNED BY............ D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0207R

SAMPLE#	Cu %	Pb %	Zn %	Ag** OZ/T	Au** OZ/T
C 109453	.01	.01	2.37	.09	.001
C 109455	.01	.01	2.14	.02	.001
C 109467	.02	.01	1.87	.08	.001
C 109468	.01	.03	4.07	.17	.002
C 109469	.98	.06	14.31	.39	.002
C 109470	1.52	.26	10.44	.80	.010
C 109471	.02	1.31	1.94	.17	.006
C 109472	.20	.02	5.27	.06	.010
C 109473	.21	.59	13.33	.27	.002
C 109474	1.17	.01	20.85	.63	.011
C 109477	.05	.01	2.29	.10	.033

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: FEB 6 1990
DATE REPORT MAILED: Feb.12/90.

ASSAY CERTIFICATE

AG** AND AU** BY FIRE ASSAY FROM 1/2 A.T.
SAMPLE TYPE: ROCK PULP

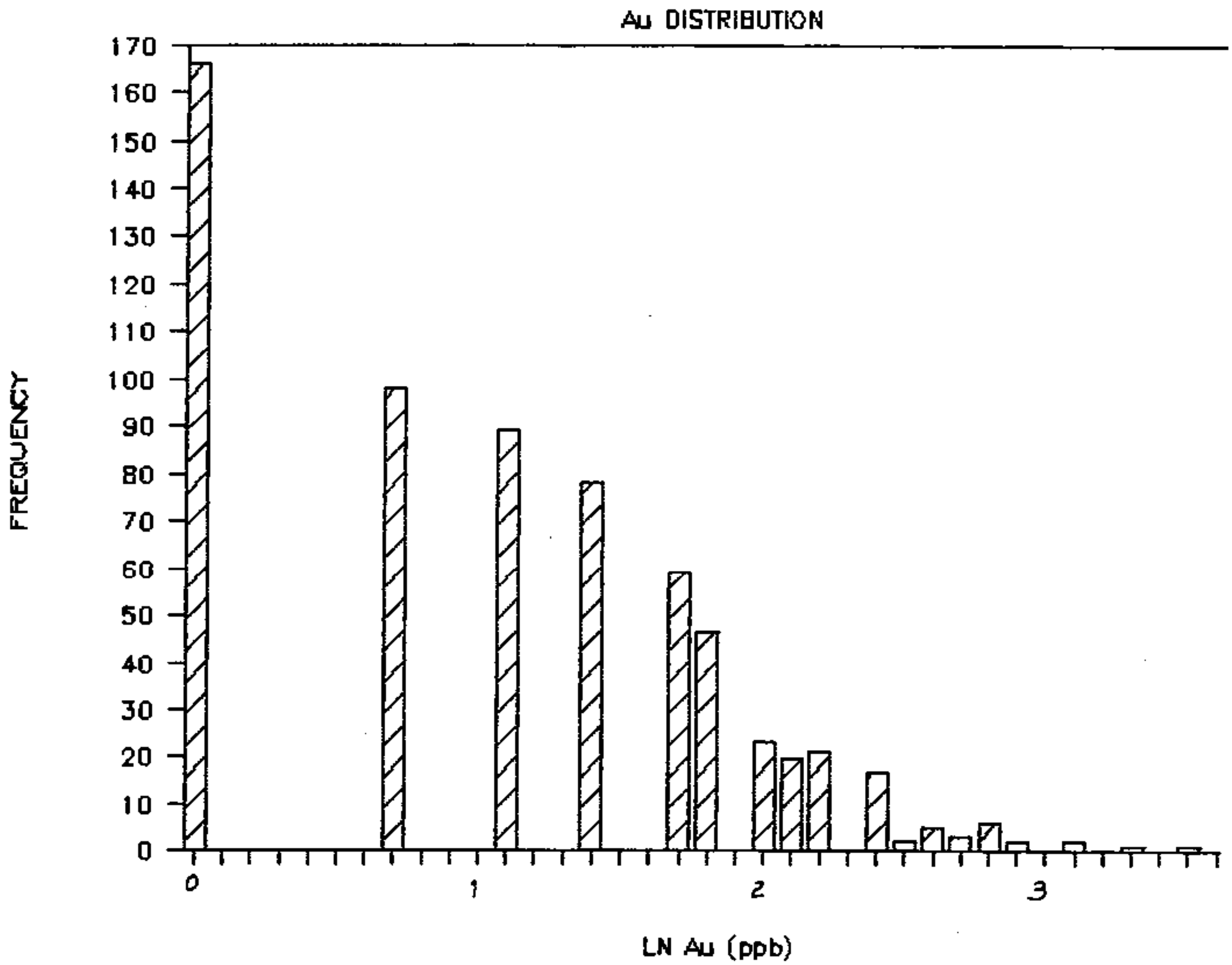
SIGNED BY. C. Leong . D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0245R

SAMPLE#	Cu %	Pb %	Zn %	Ag** OZ/T	Au** OZ/T
C 109493	.22	.01	8.59	.28	.003
C 109494	.04	.01	3.60	.08	.058 *
C 109495	.31	.01	.07	.88	.011

* Subject to reassay check

DAIWAN ENGINEERING LTD.



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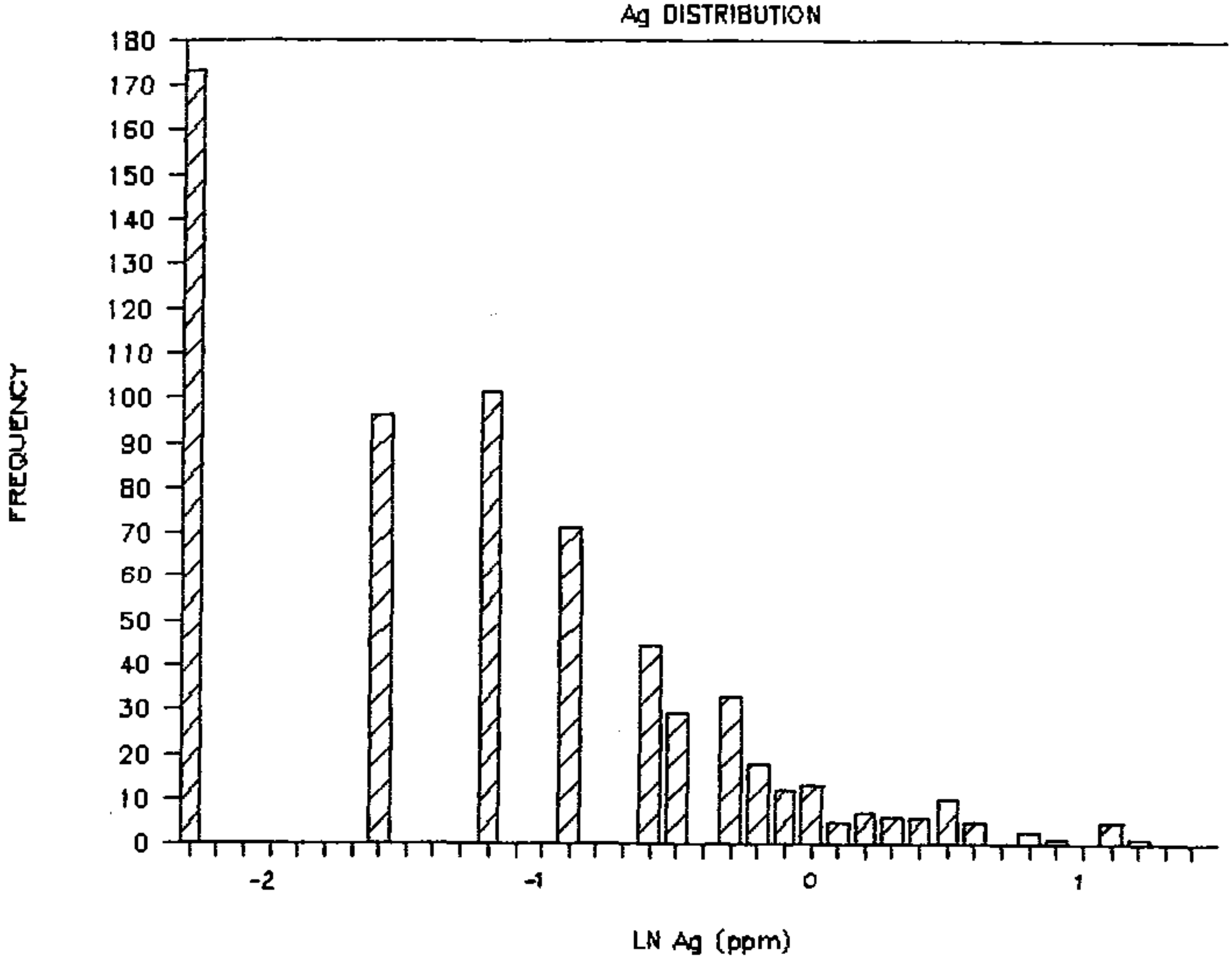

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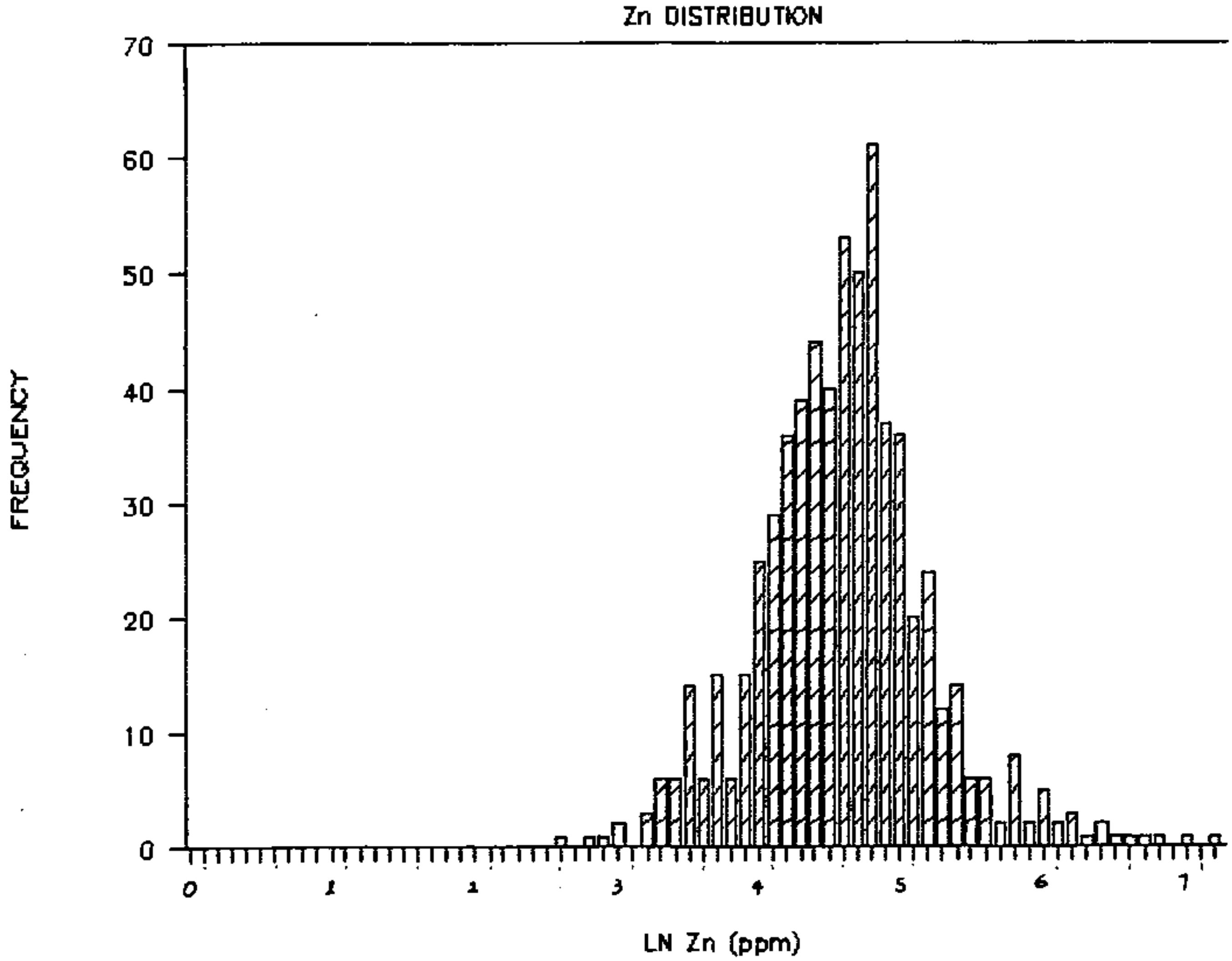
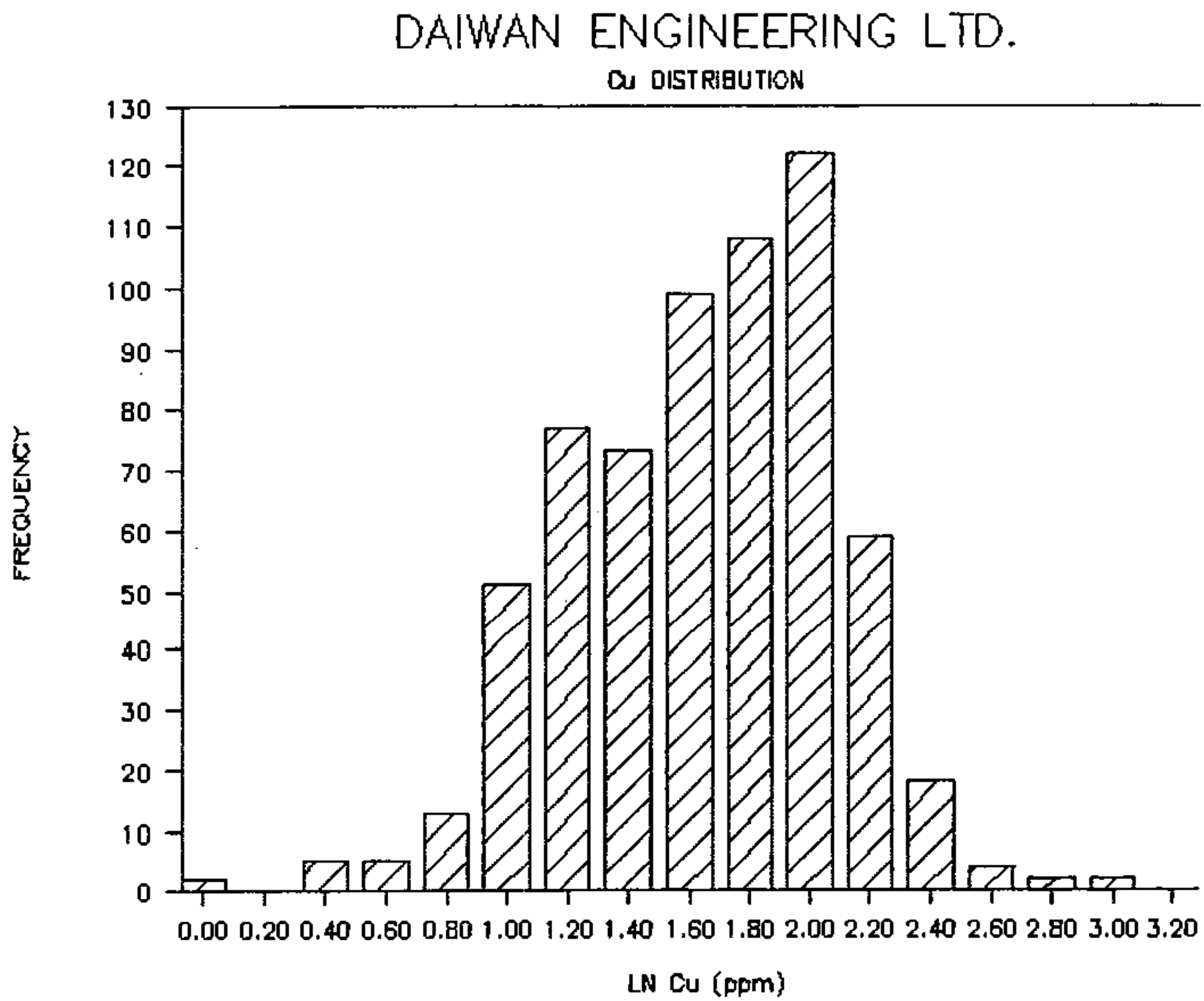
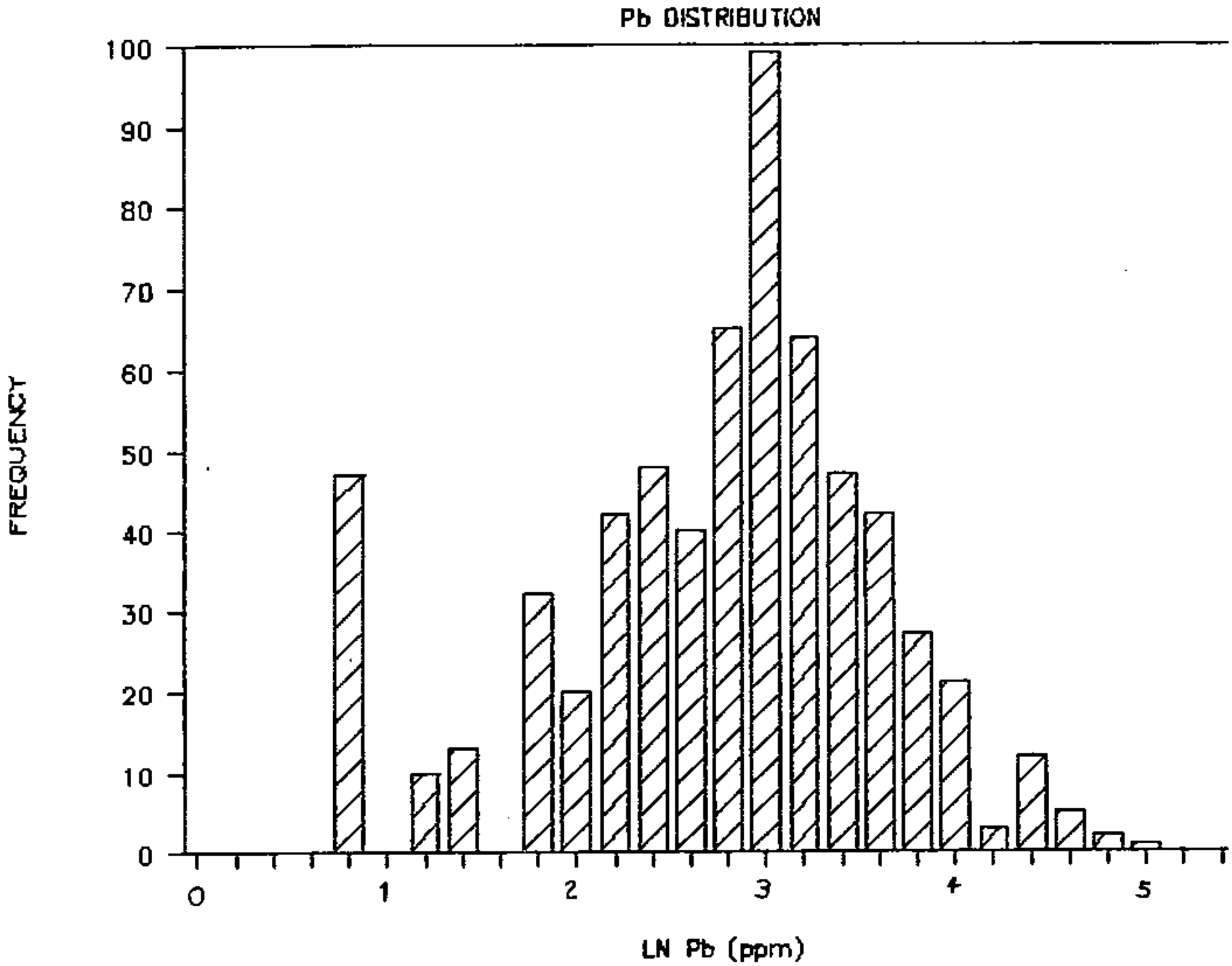
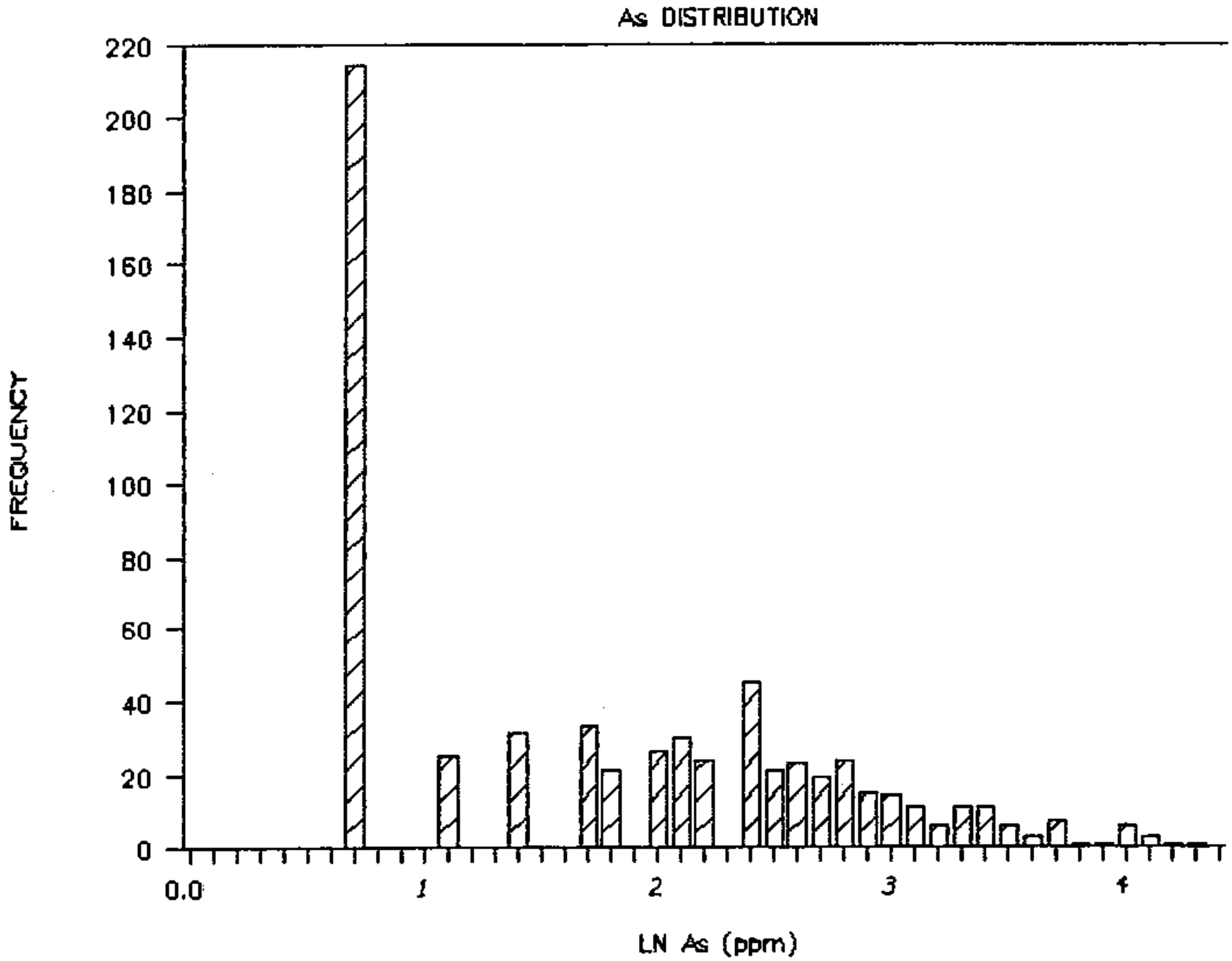



DAIWAN ENGINEERING LTD.
Cu DISTRIBUTION
FREQUENCY
130
120
110
100
90
80
70
60
50
40
30
20
10
0
0.00 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 1.80 2.00 2.20 2.40 2.60 2.80 3.00 3.20
LN Cu (ppm)

DAIWAN ENGINEERING LTD.



DAIWAN ENGINEERING LTD.



STATISTICALLY ANOMALOUS SOIL GEOCHEMISTRY VALUES

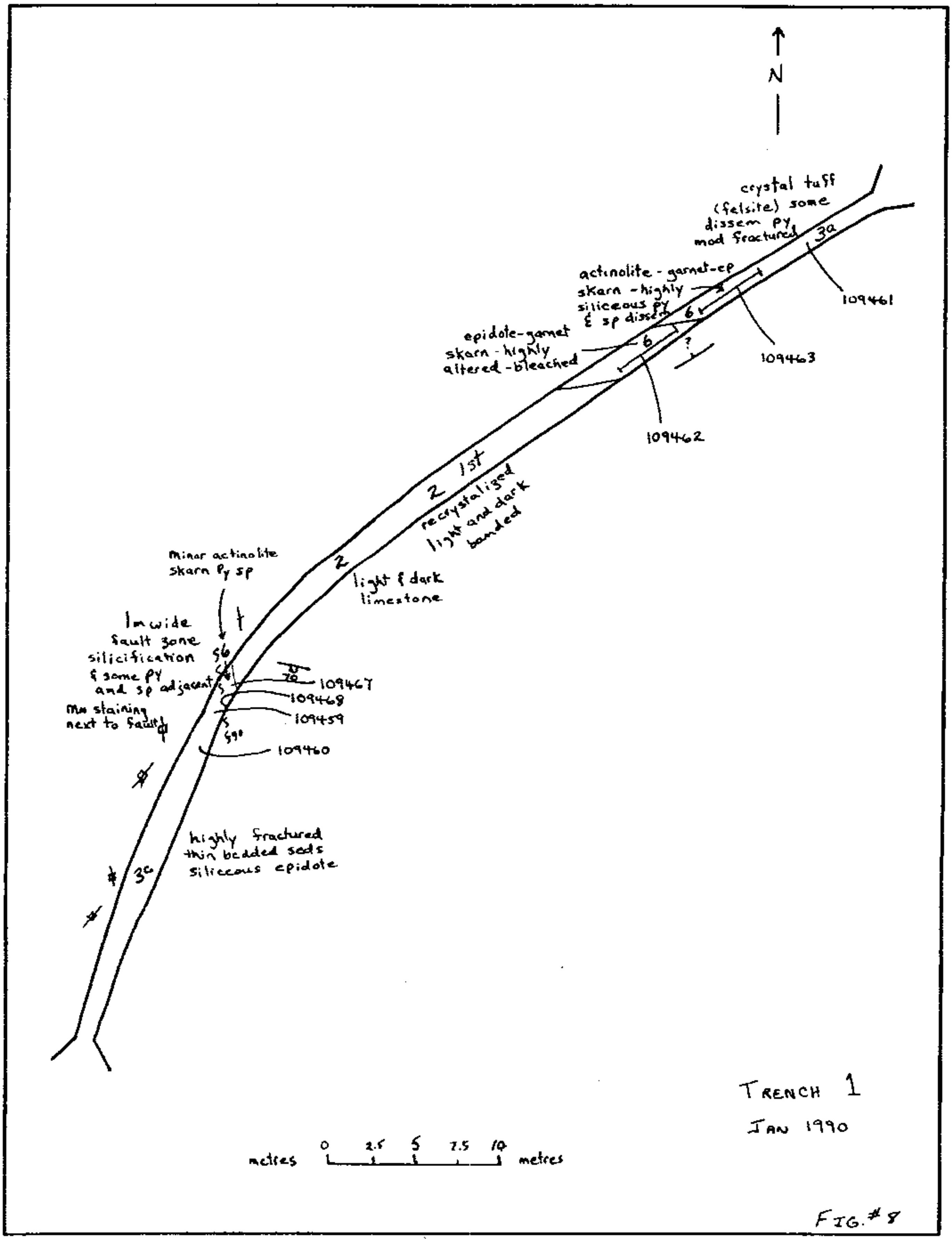
NORTHERN VANCOUVER ISLAND AREA

(ASSESSMENT REPORT #2190)

		Background			Anomalous		
		Population				Population	
Geology	Metal	x	x-2s	x-s	x	x+s	x+2s
Kalmutsen Volcanics	Cu	14.5	68	112	189	318	522
	Mo	-	-	-	.11	0.8	5.6
	Zn	15.1	42	74	136	250	450
Quatsino Limestone	Cu	18.5	109	155	220	315	445
	Mo	-	-	-	1.3	5.0	19.5
	Zn	24	90	140	220	345	535
Bonanza Volcanics	Cu	7.4	25	35	48	69	96
	Mo	0.23	3.3	4.8	7.15	10.5	15.5
	Zn	13.8	44	61	85.5	120	165
Altered Rocks	Cu	7.6	36	50	70	98	137
	Mo	0.22	3.35	5.9	10.4	18.7	33
	Zn	5.7	16.2	24.3	37	56	84
Intrusives	Cu	9.0	31	40	52	68	87
	Mo	0.24	3.7	6.2	10.5	17.8	30
	Zn	-	-	-	24	43	71

APPENDIX 3

GEOLOGIST'S SKETCHES



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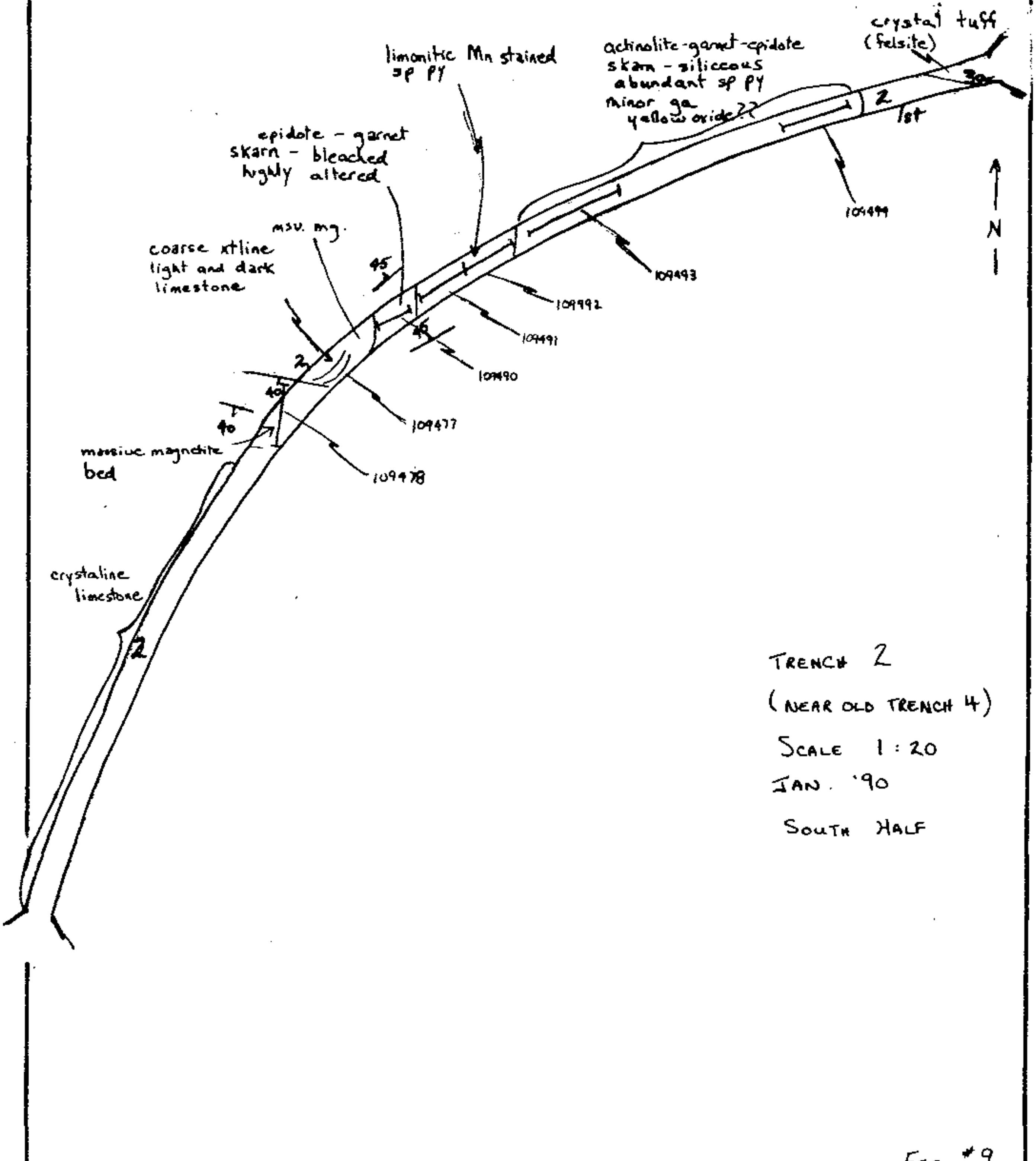
crystal tuff (felsite)
actinolite-garnet-epidote skarn - siliceous abundant sp py minor ga yellow oxide??
limonitic Mn stained sp py
epidote - garnet skarn - bleached highly altered
msv. mg.
coarse xtline light and dark limestone
massive magnetite bed
crystaline limestone
109494
109493
109492
109491
109490
109477
109478
TRENCH 2
(NEAR OLD TRENCH 4)
SCALE 1 : 20
JAN. '90
SOUTH HALF
N

FIG. #9

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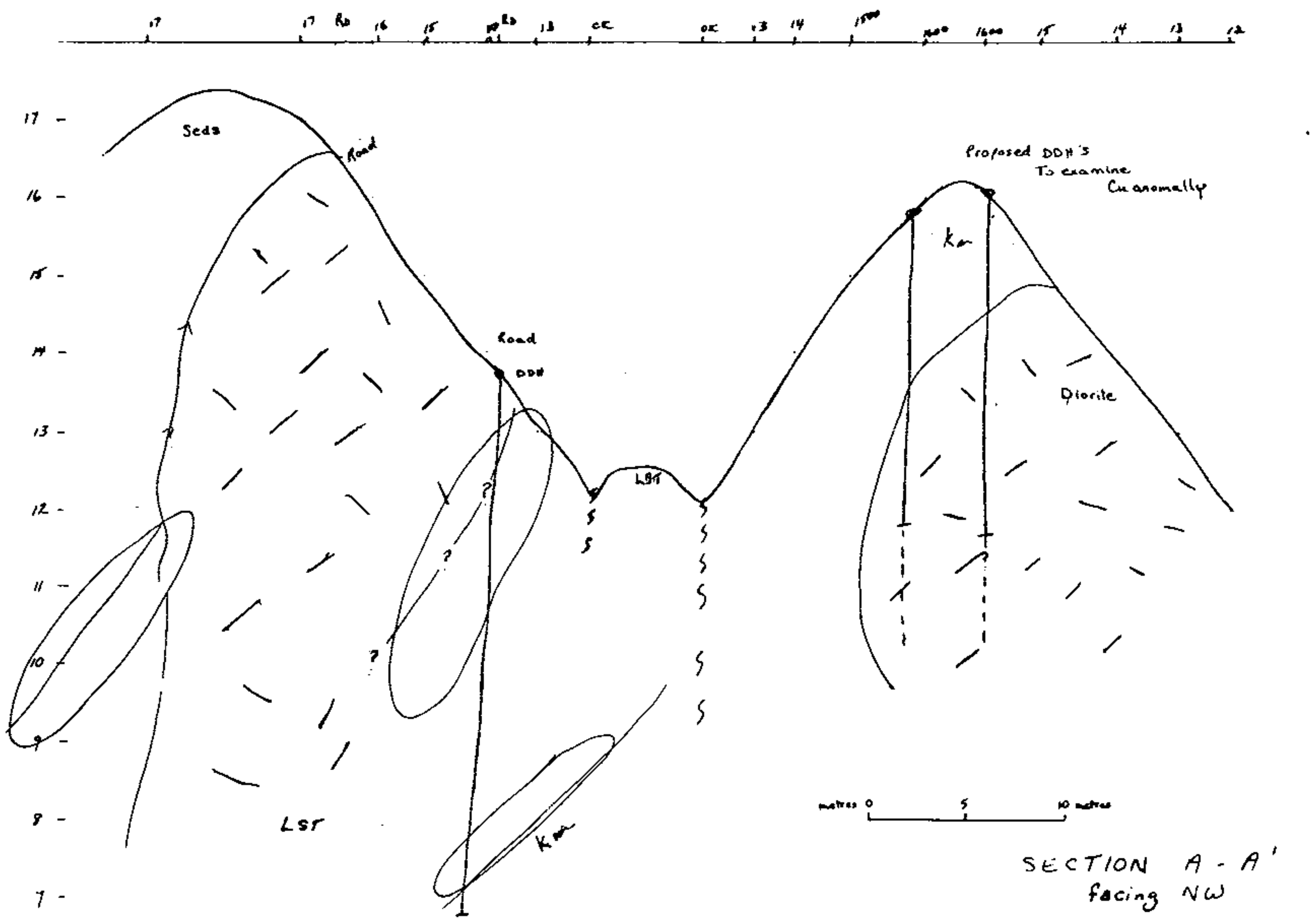

SECTION A - A'
facing NW

3.28 vert.
exag.

JAN. '90

Fig. #10

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1030 - 609 Granville Street, Vancouver, B.C.
(604) 688-1508

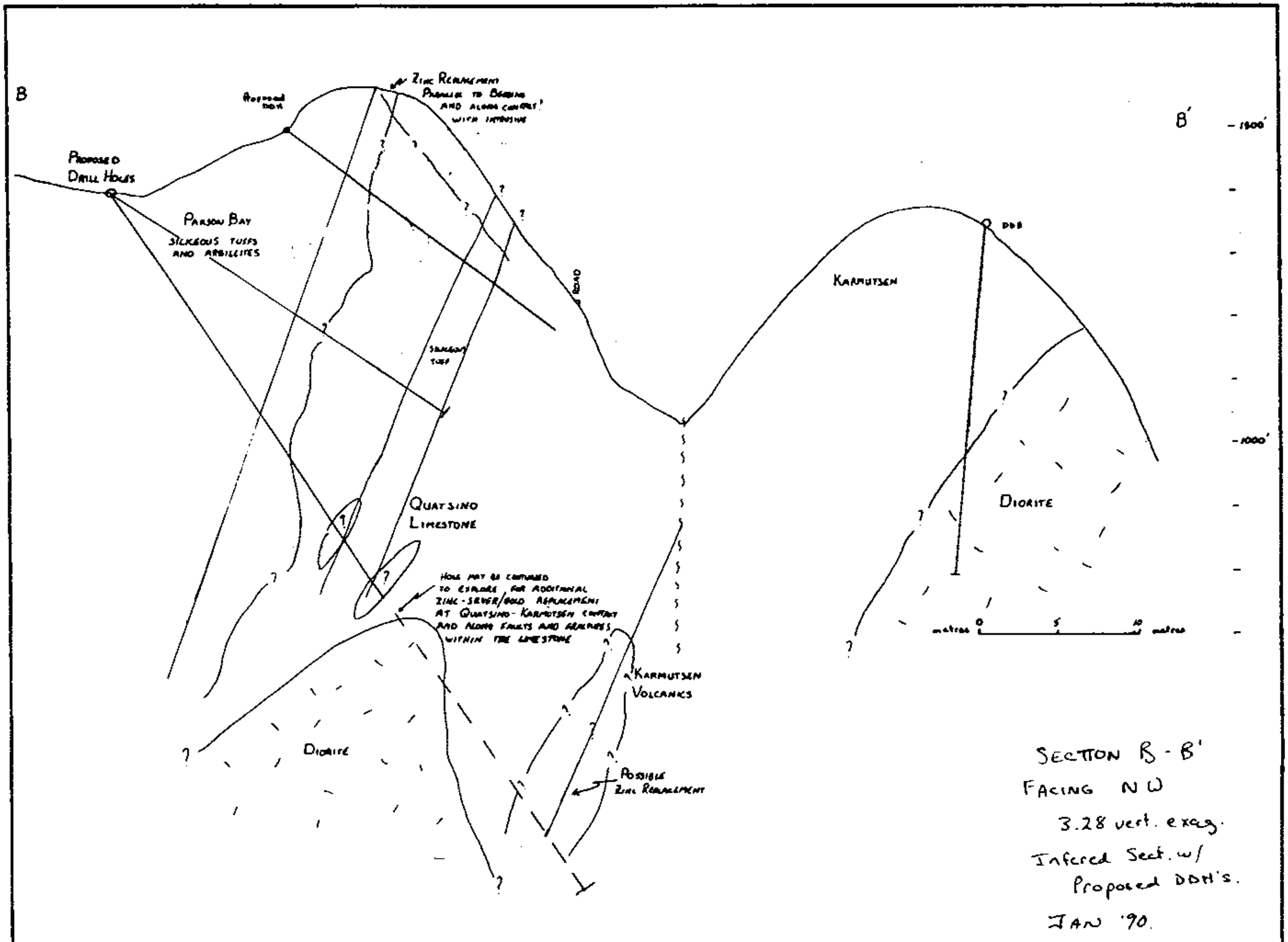
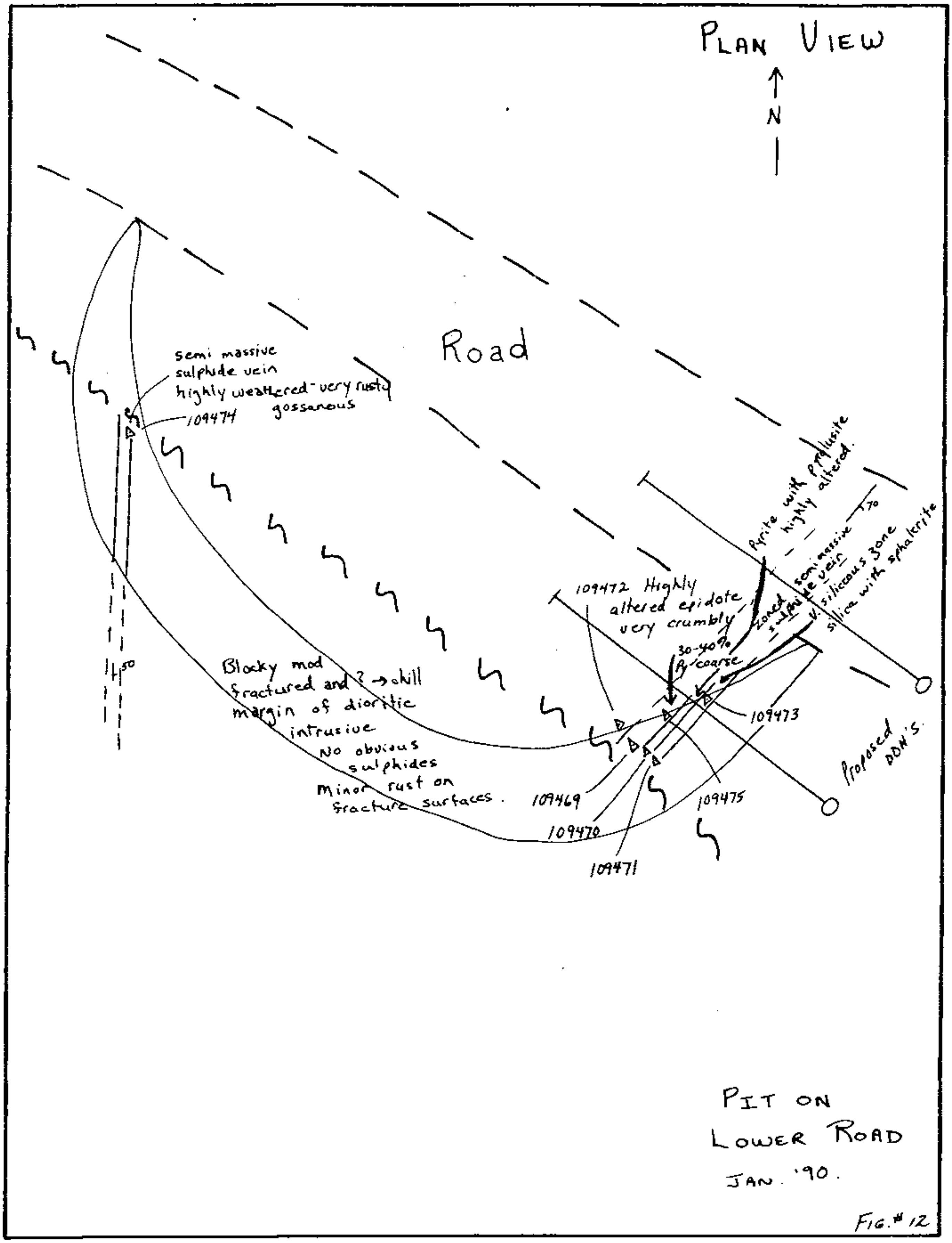


FIG. #11



Daiwan Engineering Ltd.
1030 - 609 Granville Street , Vancouver, B. C.
(604) 688-1508

ACME ANALYTICAL LABORATORIES LTD.
852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6
PHONE(604)253-3158 FAX(604)253-1716

DATE RECEIVED: FEB 14 1990
DATE REPORT MAILED: Feb. 16/90

GEOCHEMICAL ANALYSIS CERTIFICATE

- SAMPLE TYPE: P1 SILT PULP P2 ROCK PULP
AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

SIGNED BY. C. Leong D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Daiwan Engineering Ltd. PROJECT WIN FILE # 90-0321R Page 1

SAMPLE#	AU* ppb
C 109960	2
C 109962	3
C 109963	2
C 109966	8
C 109969	1

SAMPLE#	AU* ppb
C 109952	1
C 109953	1
C 109954	3
C 109955	5
C 109956	6
C 109957	7
C 109958	1
C 109959	3
C 109961	3
C 109964	2
C 109965	2
C 109967	8
C 109968	1

APPENDIX 4

VLF-EM RAW DATA

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
0	0	-24
0	25	-24
0	50	-23
0	75	-24
0	100	-21
0	125	-22
0	150	-18
0	175	-18
0	200	-12
0	225	-11
0	250	-6
0	275	-3
0	300	-3
0	325	-5
0	350	-7
0	375	-6
0	400	-4
0	425	-5
0	450	-6
0	475	-6
0	500	-7
0	525	-7
0	550	-5
0	575	-5
0	600	-3
0	625	-7
0	650	-3
0	675	-4
0	700	-5
0	725	-7
0	750	-6
0	775	-10
0	800	-9
0	825	-10
0	850	-11
0	875	-8
0	900	-3
0	925	-4
0	950	-6
0	975	-7
0	1000	-4
0	1025	-2
0	1050	-6
0	1075	-3
0	1100	-4
0	1125	-2
0	1150	0
0	1175	0
0	1200	-10
0	1225	-14
0	1250	-16
0	1275	-13
0	1300	-15
0	1325	-3
0	1350	0

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
0	1375	2
0	1400	-8
0	1425	-4
0	1450	-12
0	1475	-14
0	1500	-18
150	25	-20
150	50	-20
150	75	-18
150	100	-15
150	125	-15
150	150	-12
150	175	-12
150	200	-10
150	225	1
150	250	2
150	275	0
150	300	6
150	325	4
150	350	0
150	375	-1
150	400	-2
150	425	-2
150	450	-3
150	475	-2
150	500	-4
150	525	-3
150	550	-3
150	575	0
150	600	0
150	625	-1
150	650	0
150	675	-2
150	700	-1
150	725	-6
150	750	-6
150	775	-5
150	800	-6
150	825	-6
150	850	-2
150	875	0
150	900	0
150	925	-10
150	950	-12
150	975	-14
150	1000	-17
150	1025	-15
150	1050	-12
150	1075	-9
150	1100	-6
150	1125	-9
150	1150	-11
150	1175	-14
150	1200	-13
150	1225	-7

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
150	1250	-6
150	1275	-5
150	1300	-5
150	1325	-4
150	1350	-8
150	1375	-16
150	1400	-16
150	1425	-29
150	1450	-15
150	1475	-9
150	1500	-2
300	0	-10
300	25	-5
300	50	-7
300	75	-6
300	100	-7
300	125	-6
300	150	-7
300	175	-6
300	200	-6
300	225	-3
300	250	-3
300	275	-2
300	300	2
300	325	1
300	350	-3
300	375	-9
300	400	-3
300	425	0
300	450	2
300	475	4
300	500	5
300	525	2
300	550	4
300	575	2
300	600	3
300	625	1
300	650	-1
300	675	-2
300	700	0
300	725	4
300	750	1
300	775	6
300	800	-5
300	825	-7
300	850	-16
300	875	-20
300	900	-9
300	925	-7
300	950	-10
300	975	3
300	1000	0
300	1025	5
300	1050	10
300	1075	14

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
300	1100	11
300	1125	13
300	1150	18
300	1175	7
300	1200	7
300	1225	10
300	1250	6
300	1275	6
300	1300	14
300	1325	8
300	1350	23
300	1375	22
300	1400	20
300	1425	16
300	1450	19
300	1475	11
300	1500	9
450	0	-7
450	25	-8
450	50	-8
450	75	-8
450	100	-10
450	125	10
450	150	-8
450	175	-6
450	200	-7
450	225	-7
450	250	3
450	275	1
450	300	0
450	325	3
450	350	7
450	375	10
450	400	17
450	425	18
450	450	17
450	475	-3
450	500	-7
450	525	-3
450	550	3
450	575	3
450	600	-5
450	625	-6
450	650	-4
450	675	-6
450	700	0
450	725	-3
450	750	-6
450	775	-7
450	800	-6
450	825	-25
450	850	-23
450	875	-11
450	900	-6
450	925	-5

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
600	925	7
600	950	12
600	975	3
600	1000	7
600	1025	6
600	1050	5
600	1075	4
600	1100	4
600	1125	11
600	1150	12
600	1175	14
600	1200	7
750	0	11
750	25	11
750	50	7
750	75	3
750	100	0
750	125	-13
750	150	-11
750	175	-11
750	200	-5
750	225	-3
750	250	12
750	275	14
750	300	7
750	325	-3
750	350	-18
750	375	-7
750	400	-20
750	425	-24
750	450	-12
750	475	-5
750	500	-3
750	525	6
750	550	7
750	575	7
750	600	2
750	625	4
750	650	-15
750	675	-7
750	700	-5
750	725	8
750	750	5
750	775	6
750	800	12
750	825	8
750	850	10
750	875	2
750	900	2
750	925	4
750	950	6
750	975	7
750	1000	10
750	1025	20
750	1050	23

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
750	1075	29
750	1100	24
900	0	17
900	25	3
900	50	-23
900	75	-37
900	100	-32
900	125	-35
900	150	-20
900	175	-20
900	200	-14
900	225	-6
900	250	-4
900	275	-3
900	300	-13
900	325	-19
900	350	-20
900	375	-22
900	400	-23
900	425	-13
900	450	-4
900	475	0
900	500	-1
900	525	-4
900	550	-9
900	575	-7
900	600	-9
900	625	-10
900	650	-5
900	675	-2
900	700	5
900	725	25
900	750	20
900	775	20
900	800	17
900	825	20
900	850	10
900	875	11
900	900	14
900	925	13
900	950	19
900	975	21
900	1000	24
900	1025	24
900	1050	24
900	1075	25
1350	0	-10
1350	25	-10
1350	50	-9
1350	75	-7
1350	100	-4
1350	125	-5
1350	150	-3
1350	175	-3
1350	200	-4

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
1350	225	0
1350	250	2
1350	275	2
1350	300	3
1350	325	0
1350	350	2
1350	375	1
1350	400	0
1350	425	-2
1350	450	-4
1350	475	-6
1350	500	-8
1350	525	-7
1350	550	-5
1350	575	0
1350	600	5
1350	625	0
1350	650	-4
1500	-400	11
1500	-375	-14
1500	-350	-29
1500	-325	-18
1500	-300	-8
1500	-275	-8
1500	-250	0
1500	-225	4
1500	-200	8
1500	-175	2
1500	-150	2
1500	-125	-1
1500	-100	-1
1500	-75	-2
1500	-50	-1
1500	-25	0
1500	0	0
1500	25	0
1500	50	1
1500	75	0
1500	100	5
1500	125	12
1500	150	10
1500	175	10
1500	200	8
1500	225	4
1500	250	2
1500	275	1
1500	300	-3
1500	325	-2
1500	350	-5
1500	375	-4
1500	400	-10
1500	425	-5
1500	450	-10
1500	475	-1
1500	500	2

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
1650	-400	-22
1650	-375	-19
1650	-350	-6
1650	-325	-4
1650	-300	-2
1650	-275	0
1650	-250	3
1650	-225	2
1650	-200	3
1650	-175	4
1650	-150	4
1650	-125	7
1650	-100	10
1650	-75	5
1650	-50	1
1650	-25	2
1650	0	4
1650	25	0
1650	50	2
1650	75	5
1650	100	9
1650	125	9
1650	150	9
1650	175	-3
1650	200	-6
1650	225	-4
1650	250	-3
1650	275	2
1650	300	8
1650	325	10
1650	350	9
1650	375	8
1650	400	9
1650	425	8
1650	450	5
1650	475	5
1650	500	3
1800	-400	1
1800	-375	3
1800	-350	1
1800	-325	2
1800	-300	6
1800	-275	10
1800	-250	8
1800	-225	10
1800	-200	13
1800	-175	9
1800	-150	12
1800	-125	11
1800	-100	11
1800	-75	6
1800	-50	8
1800	-25	4
1800	0	3
1800	25	6

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
1800	50	2
1800	75	-13
1800	100	2
1800	125	2
1800	150	7
1800	175	7
1800	200	12
1800	225	11
1800	250	12
1800	275	17
1800	300	16
1800	325	20
1800	350	14
1800	375	13
1800	400	20
1800	425	13
1800	450	12
1800	475	14
1800	500	14
1950	-400	10
1950	-375	15
1950	-350	12
1950	-325	13
1950	-300	9
1950	-275	9
1950	-250	11
1950	-225	12
1950	-200	10
1950	-175	12
1950	-150	15
1950	-125	14
1950	-100	13
1950	-75	12
1950	-50	14
1950	-25	14
1950	0	0
1950	25	-5
1950	50	-11
1950	75	-6
1950	100	-6
1950	125	0
1950	150	-2
1950	175	-5
1950	200	-1
1950	225	2
1950	250	2
1950	275	2
1950	300	6
1950	325	7
1950	350	10
1950	375	12
1950	400	12
1950	425	14
1950	450	16
1950	475	2

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
1950	500	-5
2100	-425	4
2100	-400	7
2100	-375	15
2100	-350	13
2100	-325	9
2100	-300	6
2100	-275	3
2100	-250	5
2100	-225	0
2100	-200	-1
2100	-175	2
2100	-150	3
2100	-125	7
2100	-100	7
2100	-75	14
2100	-50	8
2100	-25	-1
2100	0	0
2100	25	-2
2100	50	-2
2100	75	1
2100	100	6
2100	125	8
2100	150	8
2100	175	6
2100	200	8
2100	225	5
2100	250	10
2100	275	10
2100	300	9
2100	325	12
2100	350	15
2100	375	15
2100	400	8
2100	425	2
2100	450	0
2100	475	-2
2100	500	-1
2250	-425	-1
2250	-400	1
2250	-375	4
2250	-350	-1
2250	-325	0
2250	-300	-3
2250	-275	0
2250	-250	1
2250	-225	4
2250	-200	5
2250	-175	5
2250	-150	8
2250	-125	5
2250	-100	10
2250	-75	15
2250	-50	7

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

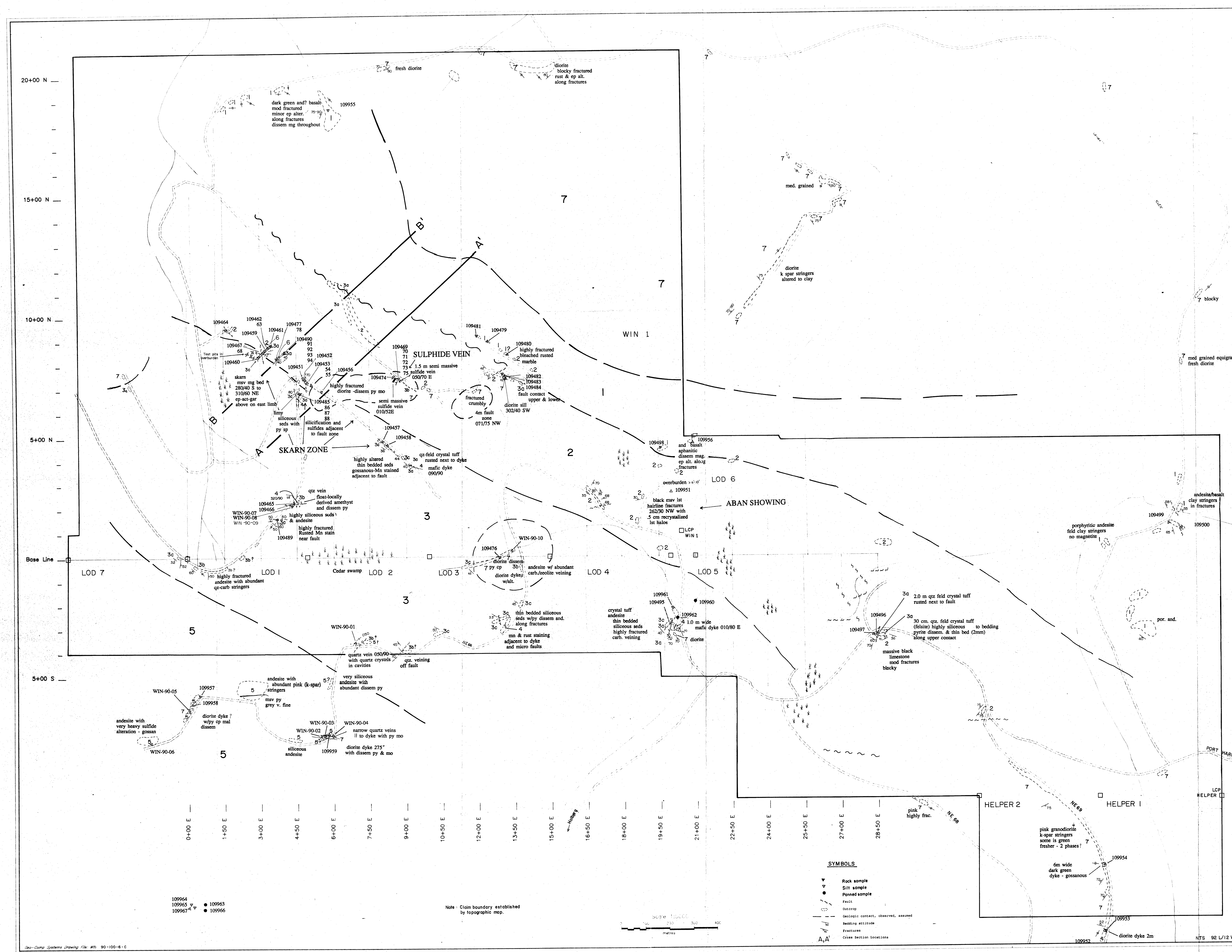
EASTING	N/S(-=S)	DIP
450	950	-1
450	975	1
450	1000	7
450	1025	9
450	1050	6
450	1075	8
450	1100	11
450	1125	2
450	1150	1
450	1175	6
450	1200	15
450	1225	18
450	1250	24
450	1275	23
450	1300	16
450	1325	14
450	1350	12
450	1375	17
600	0	1
600	25	-4
600	50	-9
600	75	-5
600	100	-1
600	125	3
600	150	4
600	175	4
600	200	2
600	225	2
600	250	3
600	275	8
600	300	8
600	325	12
600	350	15
600	375	8
600	400	-7
600	425	-5
600	450	-8
600	475	-16
600	500	-18
600	525	-13
600	550	-4
600	575	0
600	600	-2
600	625	-2
600	650	-5
600	675	-14
600	700	-20
600	725	-15
600	750	-16
600	775	-16
600	800	-15
600	825	-5
600	850	-1
600	875	9
600	900	5

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
2250	-25	-4
2250	0	-6
2250	25	0
2250	50	7
2250	75	10
2250	100	10
2250	125	12
2250	150	10
2250	175	10
2250	200	12
2250	225	11
2250	250	12
2250	275	6
2250	300	2
2250	325	-2
2250	350	1
2250	375	-1
2250	400	-2
2250	425	-4
2250	450	-1
2250	475	-1
2250	500	7
2400	-500	-6
2400	-475	-3
2400	-450	-1
2400	-425	-1
2400	-400	-8
2400	-375	-10
2400	-350	-8
2400	-325	2
2400	-300	1
2400	-275	-1
2400	-250	0
2400	-225	-9
2400	-200	-7
2400	-175	-10
2400	-150	0
2400	-125	3
2400	-100	7
2400	-75	-3
2400	-50	4
2400	-25	0
2400	0	-3
2400	25	-3
2400	50	-4
2400	75	-4
2400	100	4
2400	125	13
2400	150	4
2400	175	9
2400	200	2
2400	225	-4
2400	250	-2
2400	275	-7
2400	300	-7

DAIWAN ENGINEERING
WIN PROJECT
VLF-EM SURVEY DATA (RAW)

EASTING	N/S(-=S)	DIP
2400	325	-9
2400	350	-3
2400	375	0
2400	400	-5
2400	425	1
2400	450	2
2400	475	5
2400	500	-5
2550	-450	-5
2550	-425	-4
2550	-400	-7
2550	-375	-7
2550	-350	-7
2550	-325	-2
2550	-300	0
2550	-275	-3
2550	-250	-7
2550	-225	-6
2550	-200	-5
2550	-175	-5
2550	-150	-2
2550	-125	3
2550	-100	-1
2550	-75	-3
2550	-50	-4
2550	-25	-7
2550	0	-4
2550	25	8
2550	50	10
2550	75	16
2550	100	8
2550	125	8
2550	150	11
2550	175	6
2550	200	8
2550	225	4
2550	250	4
2550	275	0
2550	300	-14
2550	325	-3
2550	350	-3
2550	375	-2
2550	400	1
2550	425	1
2550	450	3
2550	475	3
2550	500	5



SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Au* PPB
C 109451	1	4	37	.1	44
C 109452	25	33	238	.1	11
C 109453	87	108	21523√	.3	48
C 109454	3	7	736	.1	4
C 109455	45	44	18438√	.2	1
C 109456	61	13	53	.1	5
C 109457	1	2	726	.1	3
C 109458	106	9	47	.1	7
C 109459	7	16	479	.1	6
C 109460	1	2	16	.1	1
C 109461	1	2	47	.1	5
C 109462	6	4	194	.4	5
C 109463	1	7	23	.1	8
C 109464	1112	5	26	3.5	20
C 109465	3	4	18	.1	23
C 109466	8	5	11	.1	20
C 109467	146	95	16015√	1.0	7
C 109468	23	239	32993√	5.6	6
C 109469	9595√	485	99999√	15.2	27
C 109470	14174√	1597	67785√	26.0	40
C 109471	209	11098√	16628√	4.1	8
C 109472	1768	133	50235√	.8	8
C 109473	2012	4512	99999√	6.4	13
C 109474	11671√	103	99999√	21.0	39
C 109475	105	192	1936	.4	9
C 109476	79	9	652	.1	4
C 109477	406	39	18273√	2.1	49
STD C/AU-R	57	36	137	7.0	530
C 109478	12	34	1691	.6	23
C 109479	166	9	40	.3	8
C 109480	110	7	65	.2	4
C 109481	68	10	108	.1	11
C 109482	37	2	26	.1	1
C 109483	71	5	125	.1	3
C 109484	36	7	33	.1	5
C 109485	458	872	7318	8.9	10
C 109486	149	10	57	.6	9
C 109487	152	125	343	.5	1
C 109488	92	63	637	.7	1
C 109489	69	13	38	.1	1
C 109490	5	3	615	.1	4
C 109491	131	19	583	2.8	260
C 109492	88	18	464	.9	56
C 109493	2124	42	66476√	8.1	27
C 109494	441	92	31254√	1.6	13
C 109495	3056	29	534	25.7	280
C 109496	37	11	62	.2	6
C 109497	65	7	56	.4	14
C 109498	114	4	45	.1	2
C 109499	193	7	28	.1	7
C 109500	11	16	36	.1	9

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM	AU** PPB
C 109951	62	17	55	.5	14
90-01	7	6	4	.1	62
90-02	228	14	12	.3	7
90-03	116	9	29	.1	6
90-04	24	7	3	.1	1
90-05	640	10	36	.1	17
90-06	39	11	28	.1	21
90-07	6	3	1	.1	89
90-08	3	4	1	.1	81
90-09	2	3	7	.1	150

SAMPLE#	Cu PPM	Pb PPM	Zn PPM	Ag PPM
C 109952	29	7	28	.1
C 109953	17	52	89	.2
C 109954	58	9	79	.1
C 109955	62	9	21	.2
C 109956	638	13	47	.4
C 109957	277	7	47	.2
C 109958	222	23	107	.4
C 109959	281	11	26	.1
C 109961	60	6	33	.2
C 109964	20	24	38	.1
C 109965	29	226	187	.4
C 109967	46	9	37	.1
C 109968	42	10	15	.1
STD C	59	43	134	6.9
C 109960	37	18	208	.2
C 109962	107	18	88	.1
C 109963	38	28	201	.7
C 109966	126	12	88	.1
C 109969	37	9	263	.5

* Submitted for re-assay

SAMPLE#	Cu %	Pb %	Zn %	Ag** OZ/T	Au** OZ/T	
C 109453	.01	.01	2.37	.09	.001	*
C 109455	.01	.01	2.14	.02	.001	*
C 109467	.02	.01	1.87	.08	.001	*
C 109468	.01	.03	4.07	.17	.002	*
C 109469	.98	.06	14.31	.39	.002	*
C 109470	1.52	.26	10.44	.80	.010	*
C 109471	.02	1.31	1.94	.17	.006	*
C 109472	.20	.02	5.27	.06	.010	*
C 109473	.21	.59	13.33	.27	.002	*
C 109474	1.17	.01	20.85	.63	.011	*
C 109477	.05	.01	2.29	.10	.033	*
C 109493	.22	.01	8.59	.28	.003	*
C 109494	.04	.01	3.60	.08	.058	*
C 109495	.31	.01	.07	.88	.011	*

LEGEND

7 ISLAND INTRUSIVES
Compositions range from diorite to qz diorite to granodiorite, sulfide content varies from 0 to 1% pyrite, chalcopyrite, molybdenum ± magnetite.

4 MAFIC DYKES
Generally dark green aphinitic with abundant alteration

6 SKARN
Epidote garnet, actinolite-garnet with abundant alteration (argillization and silicification) abundant sphalerite with lesser pyrite; galena, malachite. Abundant gossanous Mn weathering in parts.

5 BONANZA FORMATION
Andesites and andesitic tuffs dark to light green argillic alteration with silicification near intrusives, quartz and clay stringers, variable disseminated sulfides.

3 PARSON BAY FORMATION
3c Thin bedded argillites and tuffs. Highly siliceous variable disseminated pyrite - more abundant near to faults.
3b Porphyritic andesites - dark green variable sulfides
3a Feldspar crystal tuff - highly siliceous up to 2% disseminated pyrite interbedded with underlaying limestones

2 QUATSINO FORMATION
Medium bedded to massive dark grey to black white recrystalized with banded appearance near intrusives. Altered to skarn in parts.

1 KARMUTSEN FORMATION
Basalts and andesites dark green to black aphanitic to porphyritic trace or no sulfides. Disseminated magnetite near intrusive contact.

SYMBOLS

- Rock sample
- Silt sample
- Panned sample
- Fault
- Outcrop
- Geologic contact, observed, assumed
- Bedding attitude
- Fractures
- A,A' Cross Section Locations

ESSEX RESOURCE CORPORATION

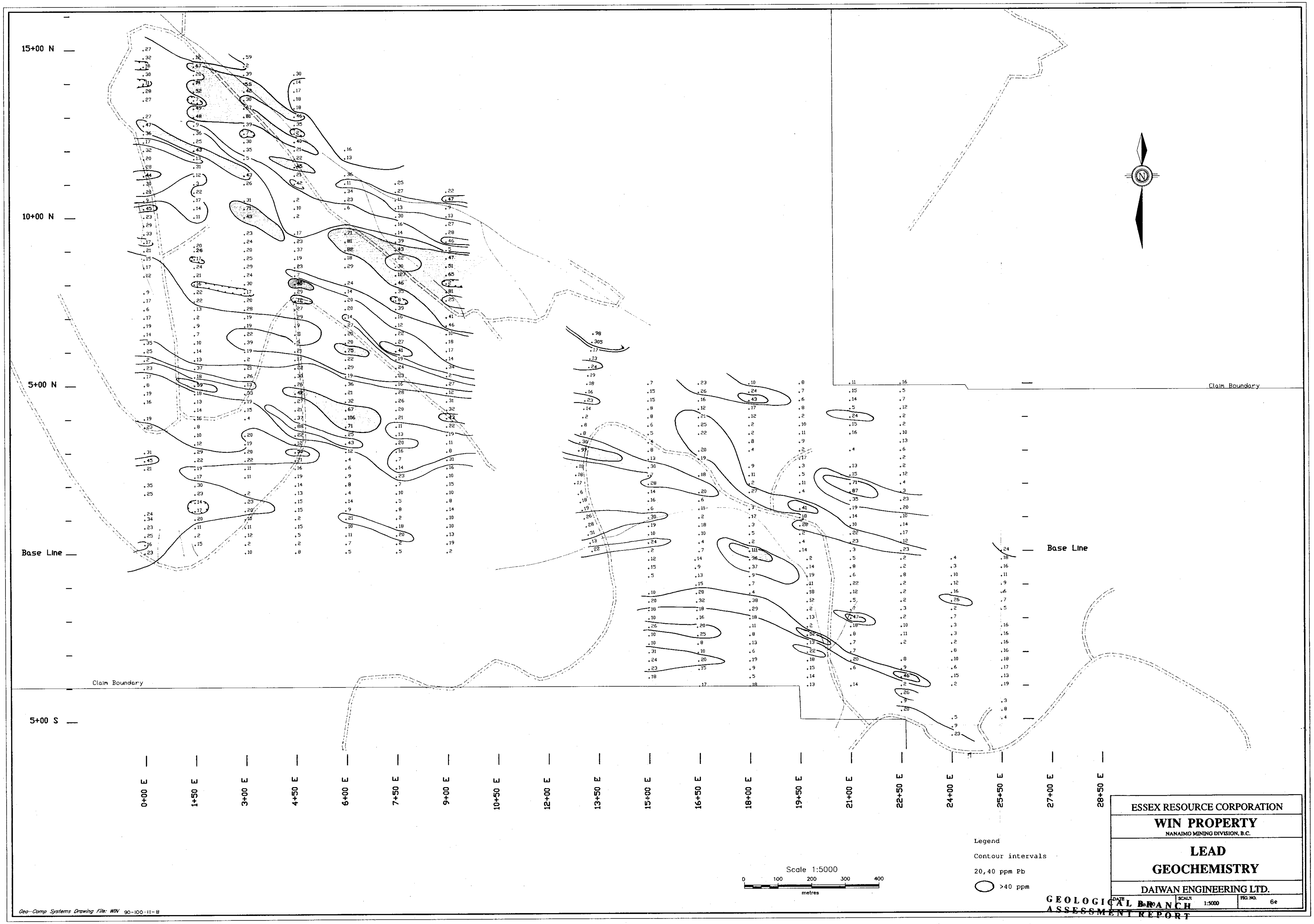
WIN PROPERTY

NANAIMO MINING DIVISION, B.C.

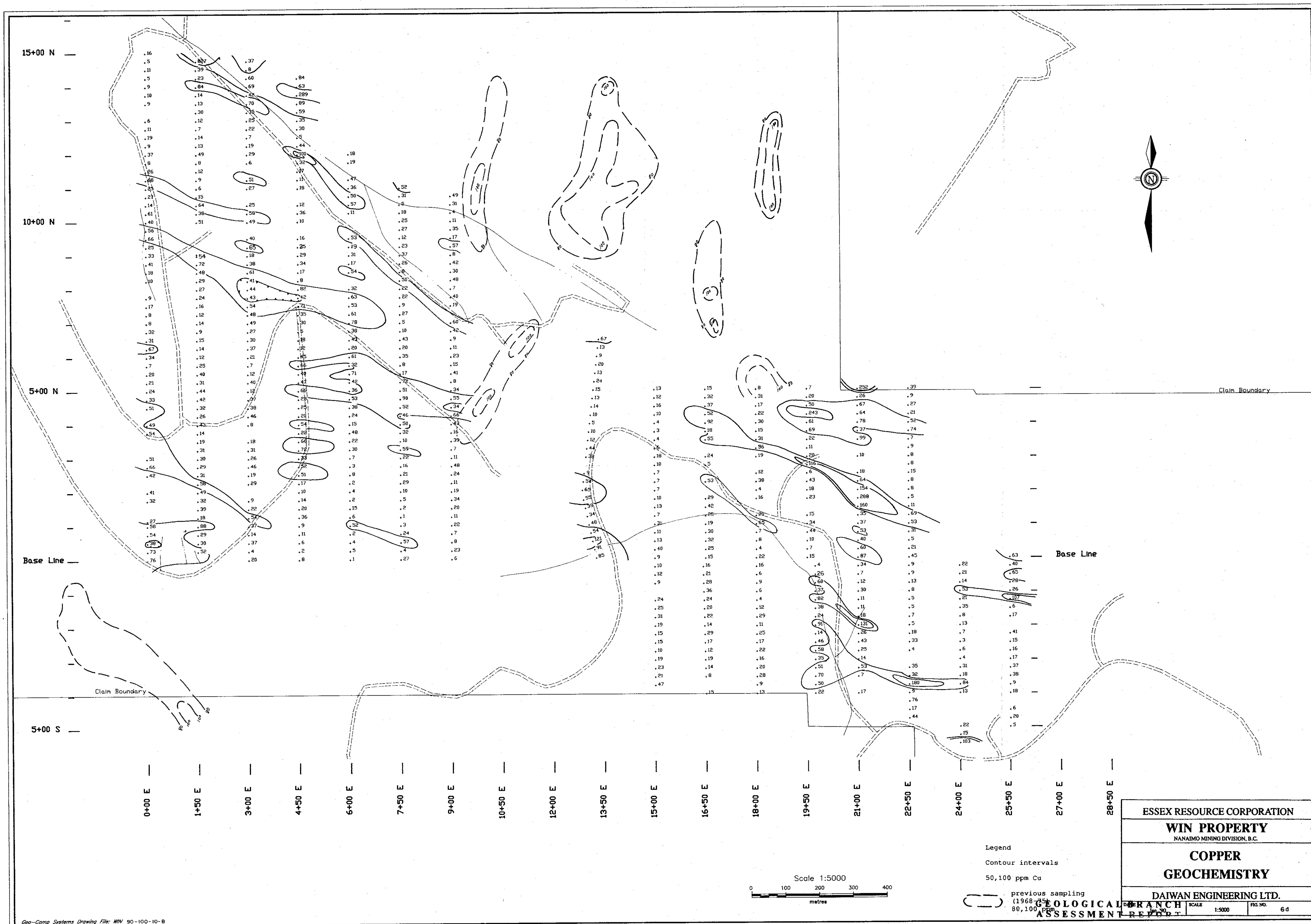
PROPERTY GEOLOGY & SAMPLE LOCATIONS

DAIWAN ENGINEERING LTD.

DATE	SCALE	FIG. NO.
Jan.,'90	1:5000	5

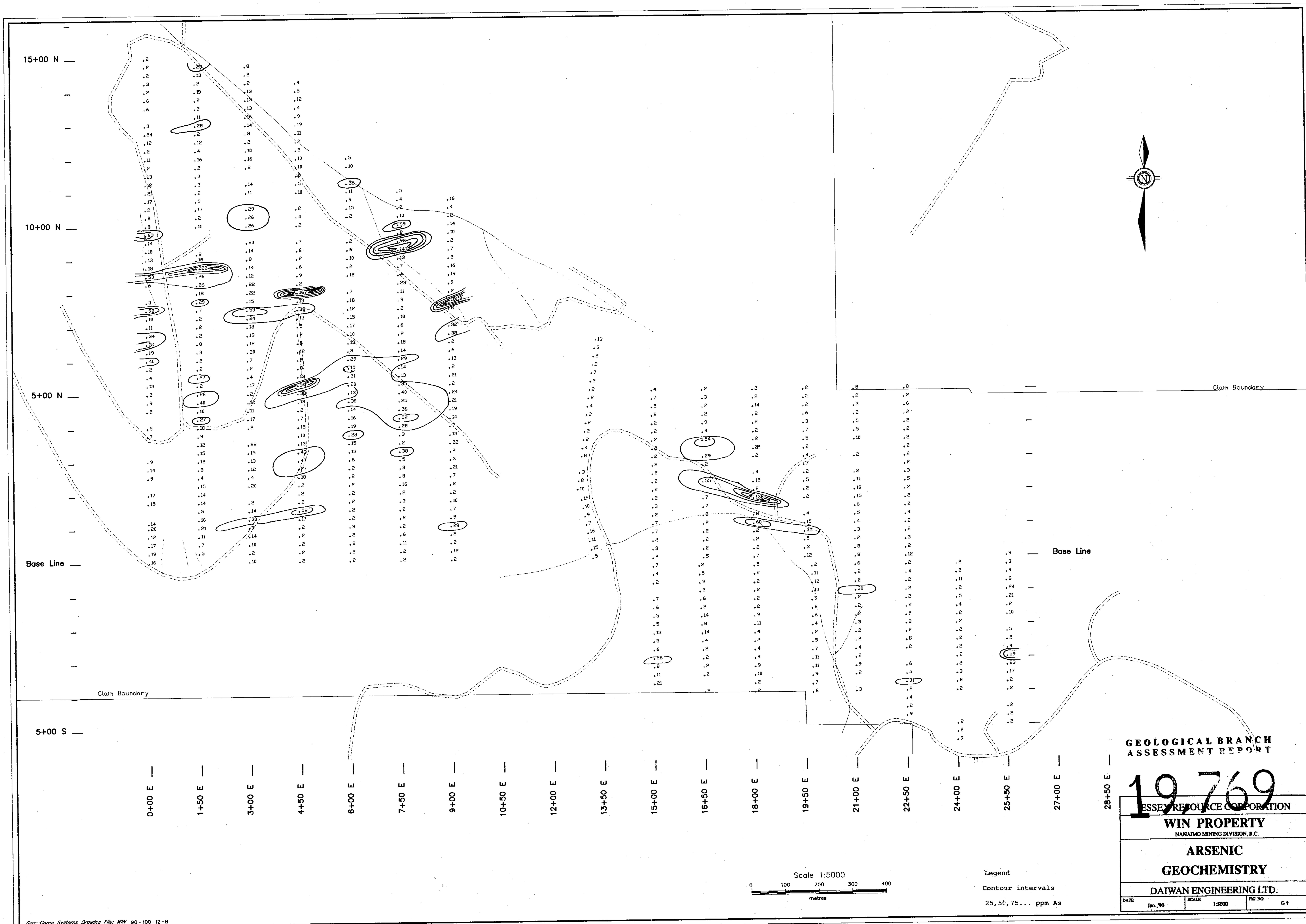

15+00 N
10+00 N
5+00 N
Base Line
5+00 S
Claim Boundary
Base Line
Claim Boundary
0+00 E
1+50 E
3+00 E
4+50 E
6+00 E
7+50 E
9+00 E
10+50 E
12+00 E
13+50 E
15+00 E
16+50 E
18+00 E
19+50 E
21+00 E
22+50 E
24+00 E
25+50 E
27+00 E
28+50 E
N
Scale 1:5000
0 100 200 300 400
metres
Legend
Contour intervals
20,40 ppm Pb
>40 ppm
ESSEX RESOURCE CORPORATION
WIN PROPERTY
NANAIMO MINING DIVISION, B.C.
LEAD
GEOCHEMISTRY
DAIWAN ENGINEERING LTD.
SCALE 1:5000
FIG. NO. 6e
GEOLOGICAL BRANCH
ASSESSMENT REPORT
Geo-Comp Systems Drawing File: WIN 90-100-11-B

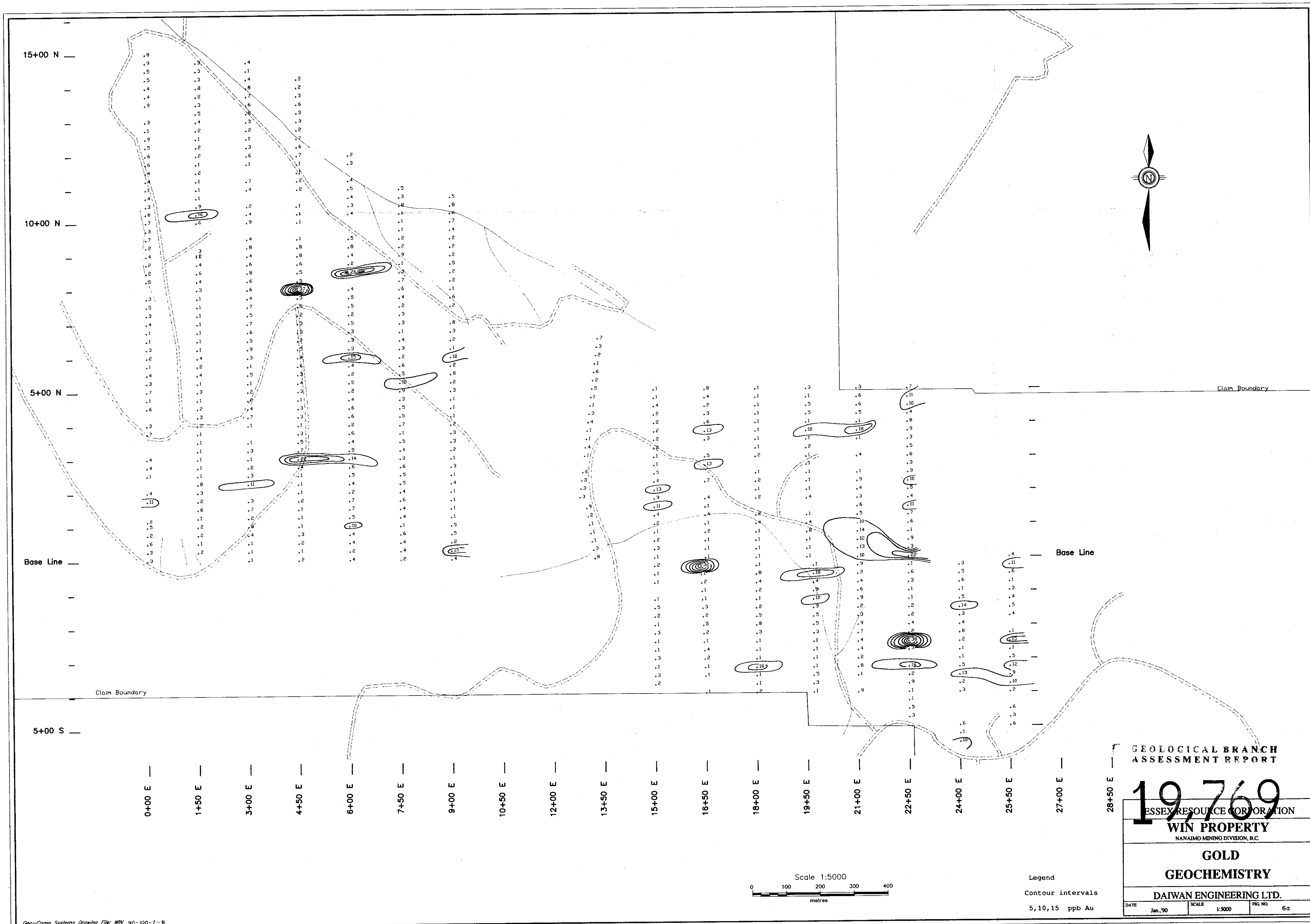
19,769



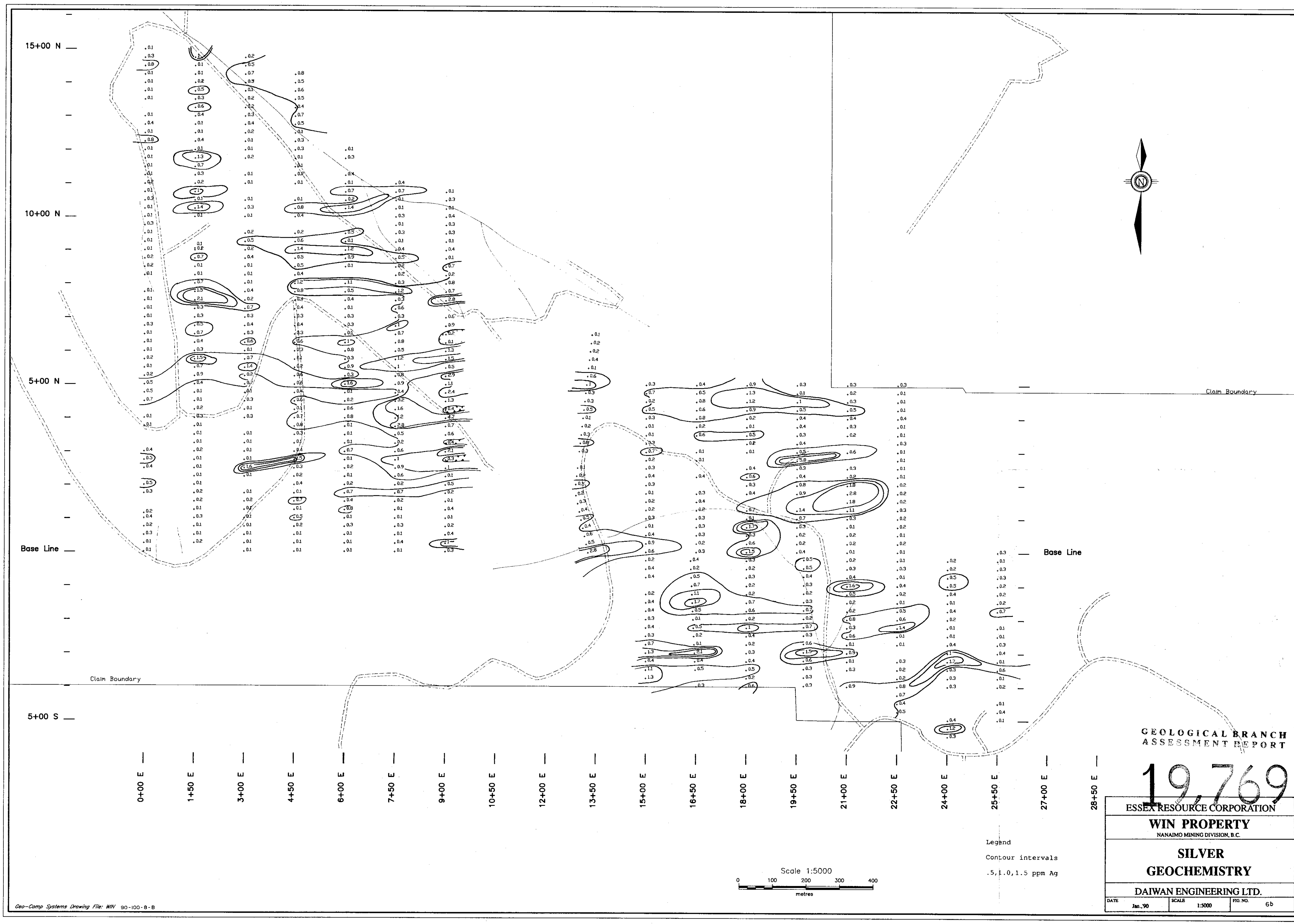
GEOLOGICAL BRANCH
ASSESSMENT REPORT

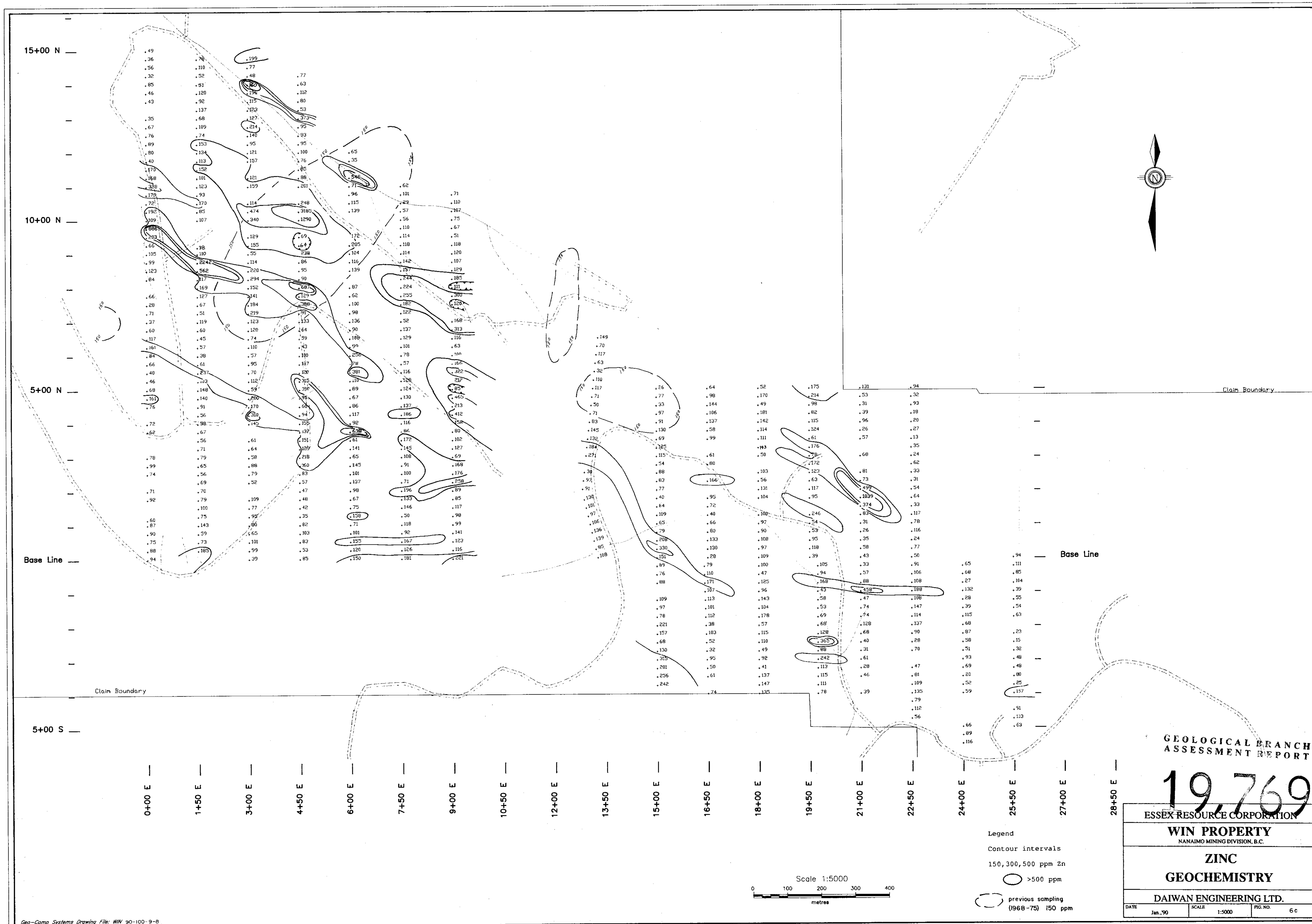
19,769

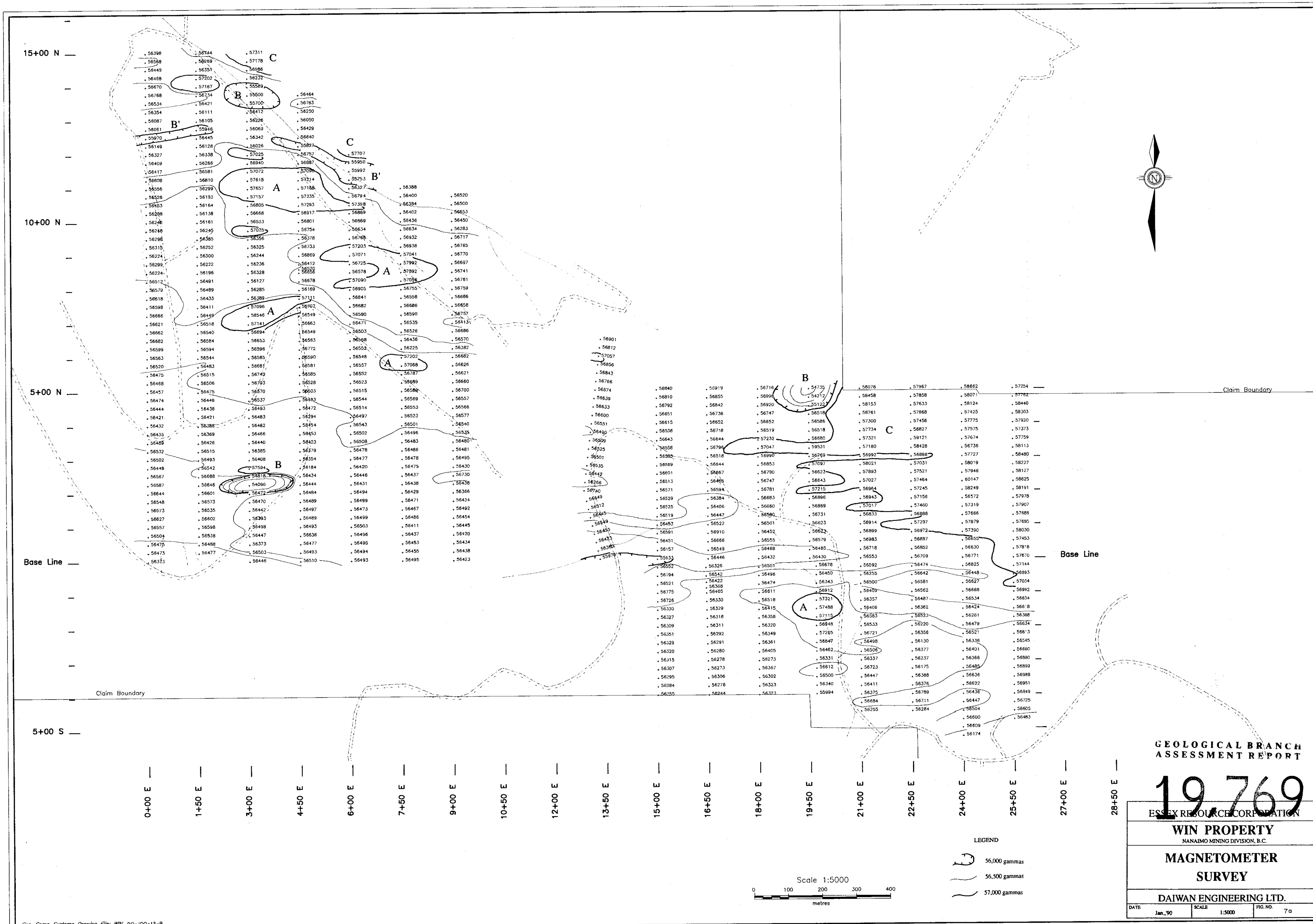

15+00 N
10+00 N
5+00 N
Base Line
5+00 S
Claim Boundary
Claim Boundary
Base Line
0+00 E
1+50 E
3+00 E
4+50 E
6+00 E
7+50 E
9+00 E
10+50 E
12+00 E
13+50 E
15+00 E
16+50 E
18+00 E
19+50 E
21+00 E
22+50 E
24+00 E
25+50 E
27+00 E
28+50 E
N
Scale 1:5000
0 100 200 300 400
metres
Legend
Contour intervals
25,50,75... ppm As
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,769
ESSEX RESOURCE CORPORATION
WIN PROPERTY
NANAIMO MINING DIVISION, B.C.
ARSENIC
GEOCHEMISTRY
DAIWAN ENGINEERING LTD.
DATE Jan.,'90
SCALE 1:5000
FIG. NO. 6f
Geo-Comp Systems Drawing File: WIN 90-100-12-B

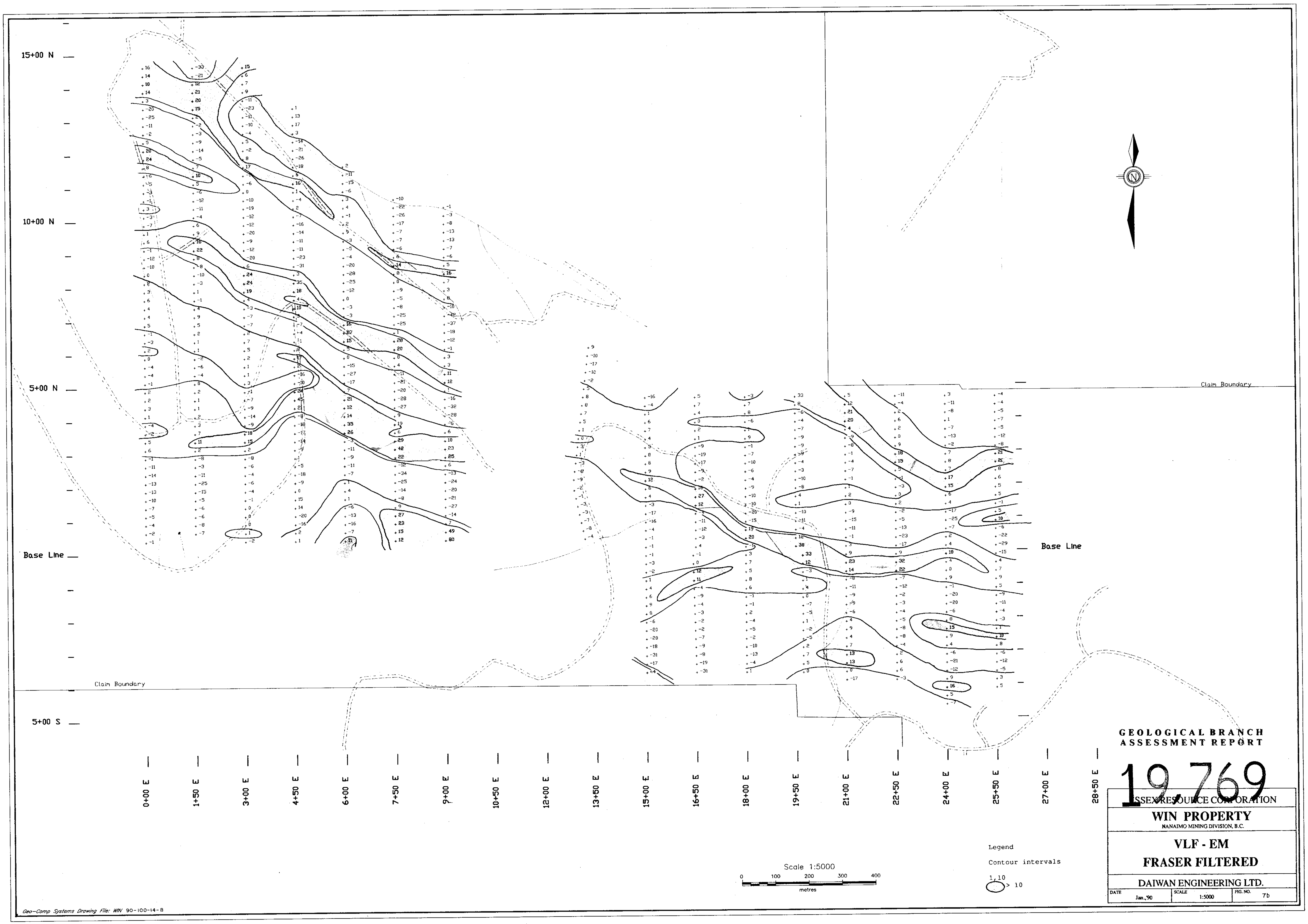


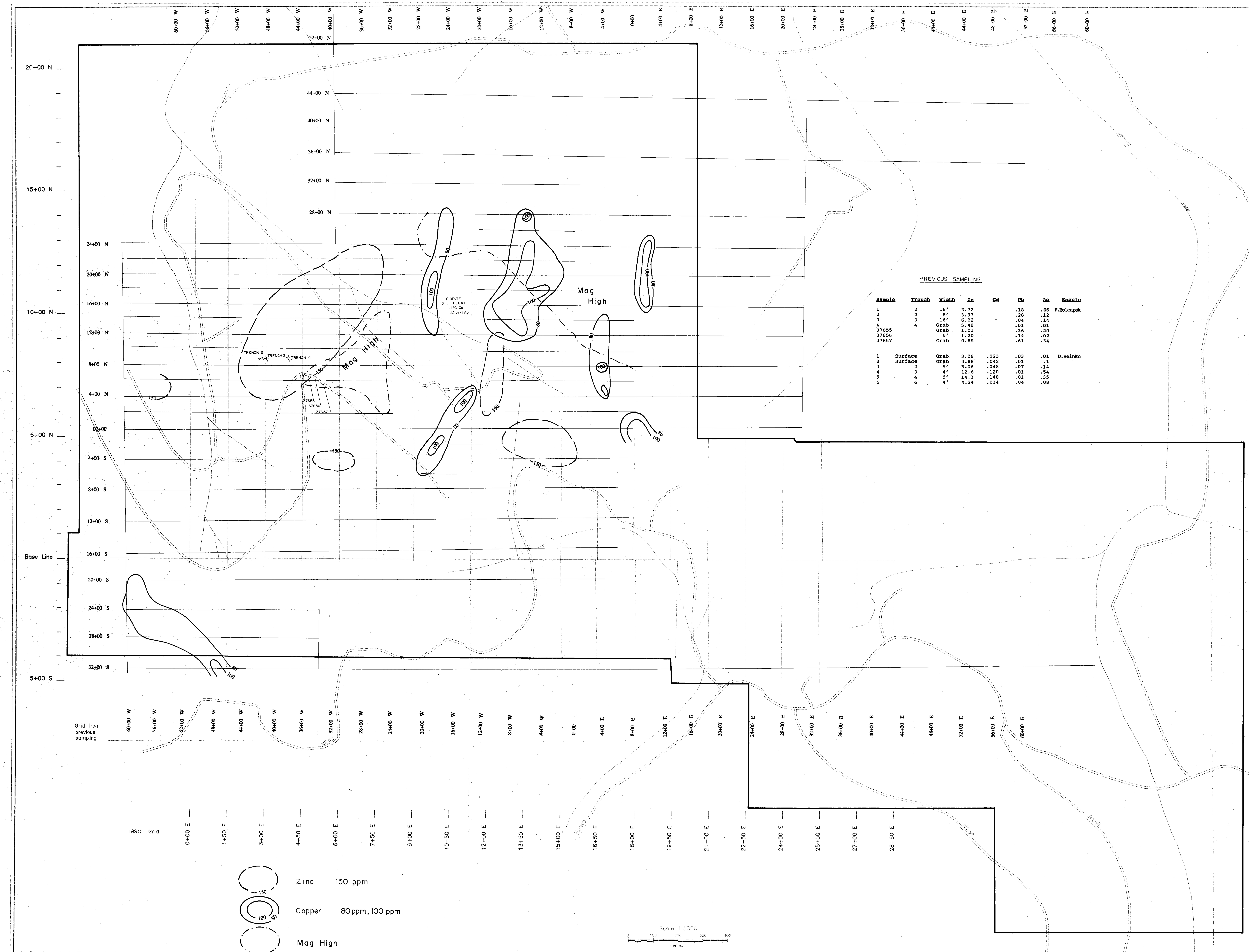
15+00 N
10+00 N
5+00 N
Base Line
5+00 S
Claim Boundary
Claim Boundary
Base Line
0+00 E
1+50 E
3+00 E
4+50 E
6+00 E
7+50 E
9+00 E
10+50 E
12+00 E
13+50 E
15+00 E
16+50 E
18+00 E
19+50 E
21+00 E
22+50 E
24+00 E
25+50 E
27+00 E
28+50 E
Scale 1:5000
0 100 200 300 400
metres
Legend
Contour intervals
5,10,15 ppb Au
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,769
ESSEX RESOURCE CORPORATION
WIN PROPERTY
NANAIMO MINING DIVISION, B.C.
GOLD
GEOCHEMISTRY
DAIWAN ENGINEERING LTD.
DATE Jan.,'90
SCALE 1:5000
FIG. NO. 6a
Geo-Comp Systems Drawing File: WIN 90-100-7-B


15+00 N
10+00 N
5+00 N
Base Line
Claim Boundary
5+00 S
Claim Boundary
Base Line
0+00 E
1+50 E
3+00 E
4+50 E
6+00 E
7+50 E
9+00 E
10+50 E
12+00 E
13+50 E
15+00 E
16+50 E
18+00 E
19+50 E
21+00 E
22+50 E
24+00 E
25+50 E
27+00 E
28+50 E
Legend
Contour intervals
.5,1.0,1.5 ppm Ag
Scale 1:5000
0 100 200 300 400
metres
Geo-Comp Systems Drawing File: WIN 90-100-8-B
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,769
ESSEX RESOURCE CORPORATION
WIN PROPERTY
NANAIMO MINING DIVISION, B.C.
SILVER
GEOCHEMISTRY
DAIWAN ENGINEERING LTD.
DATE Jan.,90
SCALE 1:5000
FIG. NO. 6b


15+00 N
10+00 N
5+00 N
Base Line
5+00 S
Claim Boundary
0+00 E
1+50 E
3+00 E
4+50 E
6+00 E
7+50 E
9+00 E
10+50 E
12+00 E
13+50 E
15+00 E
16+50 E
18+00 E
19+50 E
21+00 E
22+50 E
24+00 E
25+50 E
27+00 E
28+50 E
N
Legend
Contour intervals
150, 300, 500 ppm Zn
>500 ppm
previous sampling
(1968-75) 150 ppm
Scale 1:5000
0 100 200 300 400
metres
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,769
ESSEX RESOURCE CORPORATION
WIN PROPERTY
NANAIMO MINING DIVISION, B.C.
ZINC
GEOCHEMISTRY
DAIWAN ENGINEERING LTD.
DATE Jan.,90
SCALE 1:5000
FIG. NO. 6c
Geo-Comp Systems Drawing File: WIN 90-100-9-8


15+00 N
10+00 N
5+00 N
Base Line
5+00 S
Claim Boundary
Base Line
A
B
B'
C
0+00 E
1+50 E
3+00 E
4+50 E
6+00 E
7+50 E
9+00 E
10+50 E
12+00 E
13+50 E
15+00 E
16+50 E
18+00 E
19+50 E
21+00 E
22+50 E
24+00 E
25+50 E
27+00 E
28+50 E
N
LEGEND
56,000 gammas
56,500 gammas
57,000 gammas
Scale 1:5000
0 100 200 300 400
metres
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,769
ESSEX RESOURCE CORPORATION
WIN PROPERTY
NANAIMO MINING DIVISION, B.C.
MAGNETOMETER
SURVEY
DAIWAN ENGINEERING LTD.
DATE Jan.,'90
SCALE 1:5000
FIG. NO. 7a
Geo-Comp Systems Drawing File: WIN 90-100-13-8


15+00 N
10+00 N
5+00 N
Base Line
5+00 S
Claim Boundary
0+00 E
1+50 E
3+00 E
4+50 E
6+00 E
7+50 E
9+00 E
10+50 E
12+00 E
13+50 E
15+00 E
16+50 E
18+00 E
19+50 E
21+00 E
22+50 E
24+00 E
25+50 E
27+00 E
28+50 E
Scale 1:5000
0 100 200 300 400
metres
Legend
Contour intervals
1,10
> 10
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,769
ESSEX RESOURCE CORPORATION
WIN PROPERTY
NANAIMO MINING DIVISION, B.C.
VLF - EM
FRASER FILTERED
DAIWAN ENGINEERING LTD.
DATE Jan.,90
SCALE 1:5000
FIG. NO. 7b
Geo-Comp Systems Drawing File: WIN 90-100-14-8



PREVIOUS SAMPLING

Sample	Trench	Width	Zn	Cd	Pb	Ag	Sample
1	2	16′	3.72		.18	.06	F.Holcapek
2	2	8′	3.97		.28	.12	
3	3	16′	6.02		.04	.14	
4	4	Grab	5.40		.01	.01	
37655		Grab	1.03		.36	.20	
37656		5′	1.20		.14	.02	
37657		Grab	0.85		.61	.34	
1	Surface	Grab	3.06	.023	.03	.01	D.Reinke
2	Surface	Grab	3.88	.042	.01	.1	
3	2	5′	5.06	.048	.07	.14	
4	3	4′	12.6	.120	.01	.54	
5	4	5′	14.3	.148	.01	.35	
6	6	4′	4.24	.034	.04	.08	

ESSEX RESOURCE CORPORATION

WIN PROPERTY

NANAIMO MINING DIVISION, B.C.

COMPILATION MAP
of
Previous Work
(1968 - 1975)

DAIWAN ENGINEERING LTD.

DATE	SCALE	FIG. NO.
Jan.,'90	1:5000	3

Geo-Comp Systems Drawing File #N 90-100-3-C