ARIS SUMMARY SHEET

District Geologist, Nelson Off Confidential: 90.12.18

ASSESSMENT REPORT 19822 MINING DIVISION: Fort Steele

PROPERTY: Gold Creek
LOCATION: LAT 49 07 00 LONG 115 19 00
UTM 11 5441570 622836
NTS 082G03W
CLAIM(S): Tan 3-4,Twin 2-3,Twin 5-11,Link 1
OPERATOR(S): South Kootenay Goldfields
AUTHOR(S): Klewchuck, P.;Ryley, J.
REPORT YEAR: 1990, 37 Pages
COMMODITIES
SEARCHED FOR: Gold,Copper
KEYWORDS: Helikian,Purcell Supergroup,Siltstones,Quartzites,Basalts
Dolomites,Quartzites
WORK
DONE: Geophysical,Geochemical,Drilling,Physical
DIAD 31.4 m 1 hole(s);BQ
Map(s) - 2; Scale(s) - 1:5000
HMIN 60 sample(s) ;ME
IPOL 9.0 km
Map(s) - 13; Scale(s) - 1:5000
LINE 9.0 km
ROCK 10 sample(s) ;ME
SOIL 252 sample(s) ;ME

ASSESSMENT REPORT

ON

STREAM AND SOIL GEOCHEMISTRY, IP GEOPHYSICS, DIAMOND DRILLING AND PROSPECTING

GOLD 1 AND GOLD 2 GROUPS

GOLD CREEK AREA

FORT STEELE MINING DIVISION

NTS 82 G/3W
LATITUDE 49° 07'N
LONGITUDE 115° 19'W

FOR

SOUTH KOOTENAY GOLDFIELDS INC.
305 - 675 W. HASTINGS ST.
VANCOUVER, B.C.
V6B 1N2

BY

PETER KLEWCHUK, GEOLOGIST
246 MOYIE ST.
KIMBERLEY, B.C.
V1A 2N8

AND

JAMES RYLEY, GEOLOGIST
524 - 4TH ST. N.W.
CRANBROOK, B.C.
V1C 4A1

MARCH 19, 1990

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INTRODUCTION

i. The Gold 1 & Gold 2 groups are part of the Gold Creek claim block which covers much of the gold Creek drainage between 25 km & 65 km SE of Cranbrook, B.C. The Gold 1 & Gold 2 groups are located approximately 60 km SE of Cranbrook on NTS Map Sheet 82 G/3 W and centered at approximately 49° 07' North Latitude and 115° 19' West Longitude (Figure 1).

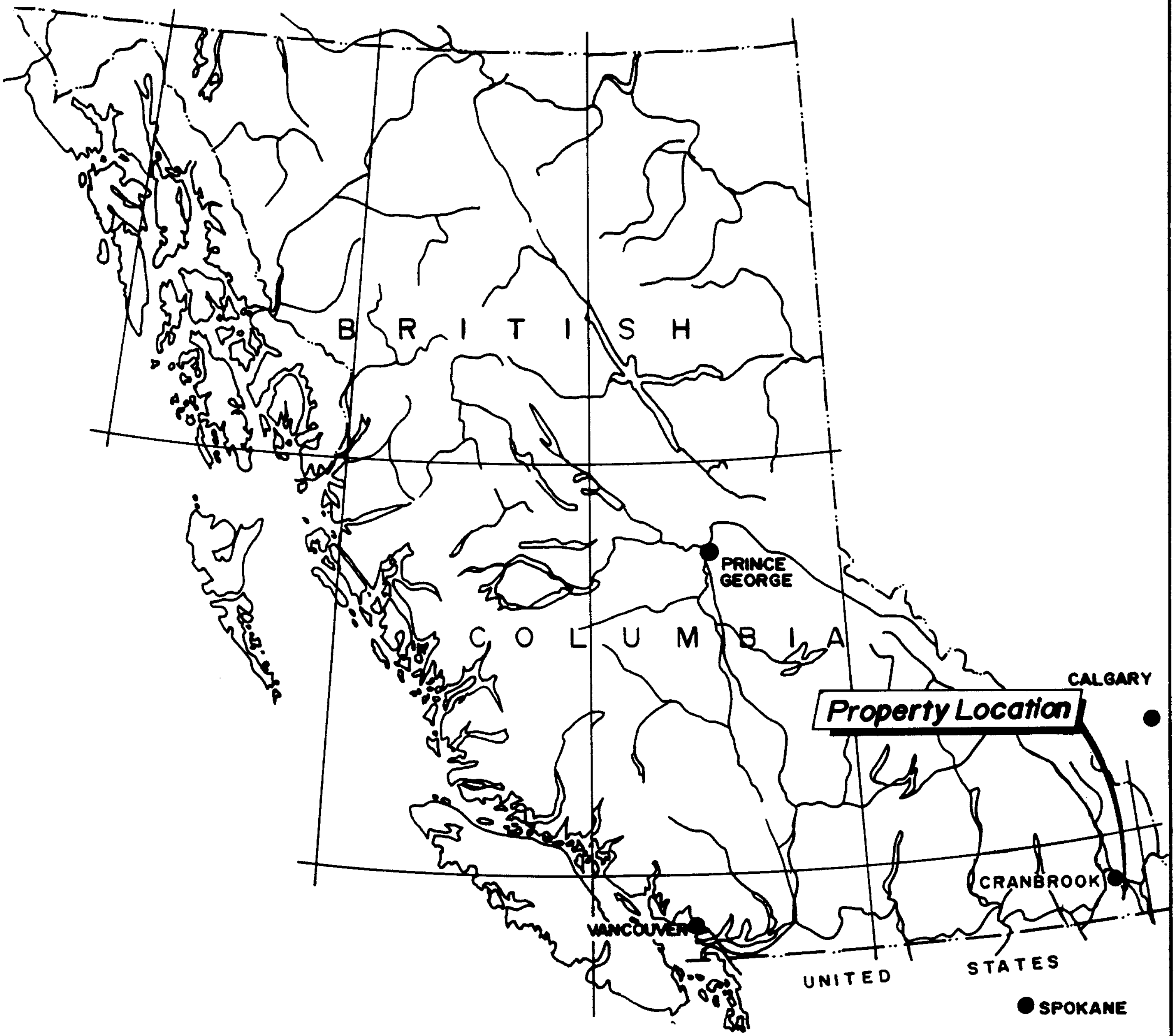
ii. The Gold 1 and Gold 2 claim groups were staked in 1988 and have no recorded previous mineral exploration history. South Kootenay Goldfields Inc. is the owner & operator. Placer gold in Gold Creek and surface mercury mineralization on the Gill claim, north of the Gold 1 and Gold 2 groups suggest the possibility of lode gold mineralization on the claim block. Disseminated copper mineralization has been located by prospecting on the Gold 2 group.

iii. Summary of work reported on:

- 30 Heavy mineral stream samples
- 30 Panned concentrate stream samples
- 252 Contour soil samples
- 9 km of linecutting
- 9 km of IP geophysics
- 31.4 m of Diamond Drilling in one hole
- 3 days of prospecting

iv. Work was performed on the following claims:

Tan 3
Tan 4
Twin 3
Twin 5
Twin 6
Twin 8
Twin 9
Twin 11
Link 1



Km 0 100 200 300 400 500

MILES 0 50 100 200 300

SOUTH KOOTENAY GOLDFIELDS INC.

Gold Creek Project

LOCATION MAP

BRITISH COLUMBIA

BAPTY RESEARCH LTD.

DRAWN J.K.R.	MINING DIV: FT. STL.	FIGURE
N.T.S. 82 K/4	SCALE: AS SHOWN	1
DATE FEB., 1990	REVISED:	

DETAILED TECHNICAL DATA AND INTERPRETATION

i. Heavy Mineral Stream Sampling

Thirty heavy mineral and thirty panned concentrate stream samples were collected on the Gold 1 and Gold 2 groups. Sample locations and sample numbers are shown on Figure 3. Stream sampling was done to evaluate the strength and distribution of placer gold in Gold Creek. Strong anomalous gold mineralization was detected in most of the samples.

ii. Rock Geochemistry

The rock samples were collected in 3 days of prospecting on the Tan 4, Twin 5, & Twin 6 Mineral Claims by prospector C. Kennedy. Location of the samples is shown on Figure 3; descriptions are provided in Table 1 with geochem data; complete geochem data is given in Appendix 2. Samples of quartzite, siltstone and breccia with minor pyrite and chalcopyrite mineralization were collected from the Tan 4, Twin 5 & Twin 6 claims. These are interpreted to be part of the Precambrian Gateway Formation. Many of the samples are anomalous in Ba and/or Cu and possibly Mn. All 3 of these elements could be indictors of gold mineralization but the gold values for samples collected is low.

Sample #	Claim	Description	Analysis Au	Ba	Cu	As	Mn
			\ ppb/			\ ppm	/
GR-89-16	Twin 6	Quartzite float with coarse dissem. pyrite	4	170	36	2	199
GR-89-17	Twin 6	Quartzite float with chalcopyrite and malachite staining	2	43	2823	12	565
GR-89-18	Tan 4	Bedrock; small chloritic quartz vein in quartzite	4	37	4	2	141
GR-89-19	Tan 4	Similar to above	3	40	5	2	149
GR-89-20	Tan 4	Similar to above	1	2058	3	2	357
GR-89-21	Twin 5	Cream colored silt-stone float, dissem. chalcopyrite	4	1818	257	2	486
GR-89-22	Twin 5	Breccia float, chalcopyrite and malachite	4	1723	1478	5	457
GR-89-23	Twin 5	Bedrock breccia, chalcopyrite, trace malachite	1	1754	43	7	603
GR-89-24	Twin 5	Bedrock breccia, small calcite veinlets chalcopyrite, trace malachite	1	1804	495	5	559
GR-89-25	Twin 5	Similar to above	1	1596	368	4	578

Table 1. Rock geochemistry; sample descriptions and partial analyses. For complete analysis see Appendix 1.

iii. Soil Geochemistry

Approximately 12,500 meters of roads and contour lines were soil sampled at 50 m spacings. B horizon soils wee collected and analyzed by Acme Analytical Laboratories Ltd. by standard analytical techniques for a 30 element ICP analysis and AA gold.

Soil sample lines and selected sample locations are shown in Figure 3; Figure 4 shows some of the analytical results for Au, Ba and Cu; complete results are shown in Appendix 2.

Gold values are generally low although there are anomalous values ranging up to 108 ppb. The eastern most line, on Twin 5, shows the strongest anomalous results with 3 samples in the 100 ppb Au range.

Barium values are normally in the 100 to 300 ppm range with anomalous values getting up to 1849 ppm. There is no obvious correlation between high Ba and high Au values.

Copper values are typically <10 ppm with anomalous values up to 143 ppm. There is no direct correlation with Cu and Au although higher Cu values tend to be located in the same general area as high Au and suggests a spatial relationship between Au and Cu.

Soils were collected late in the fall and no follow-up soil geochemistry has been completed on the anomalous results.

iv. Geophysics

The Induced Polarization geophysics is reported separately. (See Appendix 1). The geophysics was done to identify anomalous zones of sulphide mineralization which would then be drill tested.

v. Diamond Drilling

One NQ diamond drill hole, oriented -45^{o} from vertical and drilled at an azimuth of 225^{o} was drilled off a logging road which crosses the Twin 6 claim. Total depth of the hole is 31.4 meters of which 26.25 m is overburden and the remainder is bedrock. Considerable difficulty was experience in drilling through and casing the overburden. This hole was drilled to test an inferred IP anomaly. The bedrock encountered is quartzite and is interpreted to be part of the Precambrian Gateway Formation. No sulphides were noted in the core. (See Appendix 3 for the drill log).

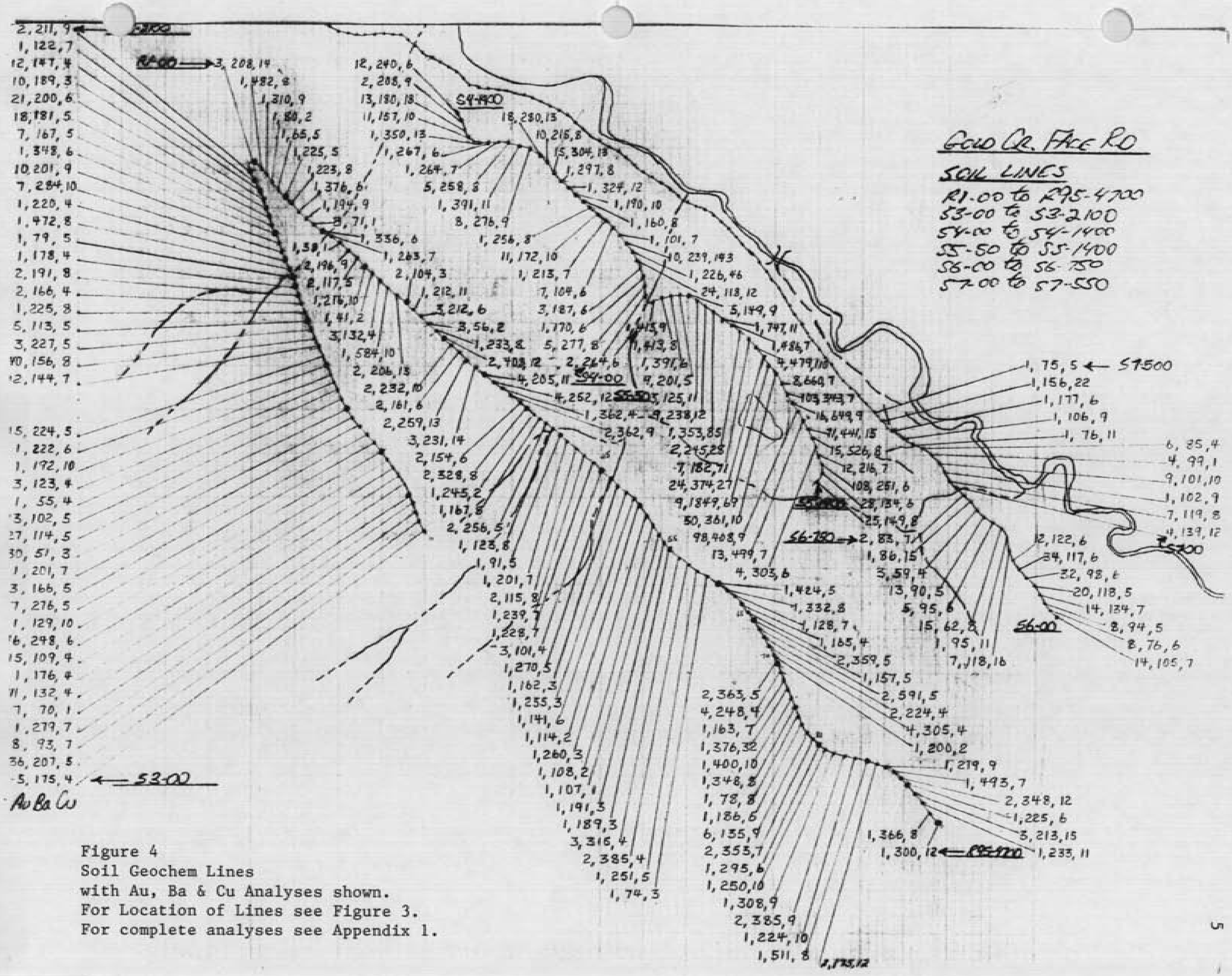


Figure 4
Soil Geochem Lines
with Au, Ba & Cu Analyses shown.
For Location of Lines see Figure 3.
For complete analyses see Appendix 1.

ITEMIZED COST STATEMENT

GOLD 1 GROUP   Tan 3, 4   Twin 2, 3, 6   Link 1   Mineral claims

12 Heavy Mineral Stream samples		@ $75/sample	900.00
12 Panned Concentrate Stream Samples		@ $75/sample	900.00
252 Soil Samples		@ $19.50/sample	4,914.00
Line Cutting	3 km	@ $ 500/km	1,500.00
IP Geophysics	3 km	@ $2,000/km	6,000.00
Diamond Drilling DDH G-89-1	31.4m	@ $318.47/m	10,000.00
			$24,214.00

GOLD 2 GROUP   Twin 5, 7, 8, 9, 10, 11 Mineral Claims

18 Heavy Mineral Stream samples		@ $75/sample	1,350.00
18 Panned Concentrate Stream Samples		@ $75/sample	1,350.00
Line Cutting	6 km	@ $ 500/km	3,000.00
IP Geophysics	6 km	@ $2,000/km	12,000.00
Prospecting & Rock Geochem	3 days	@ $275/day	835.00
	10 analyses	@ $15/sample	150.00
			$18,685.00

Geophysics by:
S.J. Geophysics Ltd.
8081 - 112 St.
Delta, B.C.
V4C 4W4

Geochemical Analyses by:
Acme Analytical Laboratories Ltd.
852 East Hastings St.
Vancouver, B.C., Canada
V6A 1R6

Diamond Drilling by:
Connors Drilling Ltd.
2007 W. Trans. Cda. Hwy.
Kamloops, B.C.
V1S 1A7

AUTHOR'S QUALIFICATIONS

As author of this report I, Peter Klewchuk, certify that:

1. I am an independent consulting geologist with offices at 246 Moyie Street, Kimberley, British Columbia.
2. I am a graduate geologist with a BSc degree (1969) from the University of British Columbia and an MSc degree (1972) from the University of Calgary.
3. I am a Fellow in good standing of the Geological Association of Canada.
4. I have been actively involved in mining and exploration geology, primarily in the province of British Columbia, for the past 17 years.
5. I have been employed by major mining companies and provincial government geological departments.

Dated at Kimberley, British Columbia, this 19th day of March, 1990.

Peter Klewchuk
Geologist

AUTHOR'S QUALIFICATIONS

1. I, James K. Ryley, am a Contract Geologist, resident at 524 - 4th St. N.W., Cranbrook, British Columbia.

2. I am a graduate of the Southern Alberta Institute of Technology and am certified as a Geological Technologist.

3. I am a graduate of the University of Montana with a B.A. in Geology.

4. I have been involved in my profession in the provinces of British Columbia and Alberta since 1980.

5. I have been actively involved in oil and gas, coal and precious and base metal exploration.

Dated at Cranbrook, British Columbia, this 19th day of March, 1990.

James K. Ryley
Geologist

APPENDIX 1

STREAM, ROCK & SOIL GEOCHEM RESULTS

ACME ANAL[illegible]AL LABORATORIES LTD. 852 E. HASTINGS ST. [illegible]VER B.C. V6A 1R6 PHONE(604)253-3158 FA[illegible]53-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: H.M. AU* ANALYSIS BY ACID LEACH/AA FROM TOTAL SAMPLE.

DATE RECEIVED: NOV 20 1989 **DATE REPORT MAILED:** [illegible] **SIGNED BY**............D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Bapty Research Limited File # 89-4814 Page 1

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM
P1-PC	2	45	651	79	.5	40	28	360	16.16	36	5	ND	13	33	1	5	2	93
P2-PC	1	13	7	30	.3	12	13	503	7.66	11	5	ND	24	32	1	2	2	100
P3-PC	1	10	72	28	.1	11	11	520	7.28	8	5	ND	25	30	1	2	2	92
P4-PC	1	11	10	30	.3	11	11	487	6.70	9	5	ND	22	33	1	2	2	90
P5-PC	1	17	34	41	.4	17	14	587	8.87	16	5	ND	19	41	1	2	2	96
P6-PC	1	27	10	55	.3	20	14	884	8.26	13	5	ND	25	68	2	2	2	121
P7-PC	1	11	17	30	.2	12	11	524	7.25	7	5	ND	20	30	1	2	2	93
P8-PC	1	13	17	30	.3	14	13	471	8.90	12	5	ND	21	27	1	2	2	101
T24-PC	1	45	19	31	.1	27	63	457	15.70	20	5	ND	7	12	1	2	2	115
G30-PC	1	20	17	32	.3	16	26	258	13.43	13	5	ND	10	16	1	2	2	111
G32-PC	1	17	9	27	.4	14	18	264	12.32	13	5	ND	10	15	1	2	2	113
G33-PC	1	16	14	29	.3	16	22	267	12.60	11	5	ND	12	16	1	2	2	108
G34-PC	1	17	14	23	.6	19	28	344	13.08	16	5	3	13	20	1	2	2	102
G35-PC	1	32	18	32	.1	31	44	370	14.66	25	5	ND	14	31	2	2	2	104
G36-PC	1	24	20	35	.3	28	34	414	13.55	18	5	ND	15	36	1	2	2	111
G37-PC	1	40	24	34	.2	35	60	495	15.70	29	5	ND	14	37	1	2	2	104
G38-PC	1	30	22	34	1.3	29	39	370	13.85	20	5	13	13	29	2	2	2	103
G39-PC	1	22	261	28	1.4	29	36	346	13.85	21	5	4	15	20	1	2	2	101
G40-PC	1	31	19	38	.4	42	44	368	14.45	26	5	3	14	26	1	2	2	98
G41-PC	1	31	46	33	.2	30	35	369	13.16	17	5	ND	12	28	1	2	2	104
G42-PC	1	22	17	29	.4	27	37	361	14.22	18	5	7	12	22	1	2	2	108
G43-PC	1	18	19	31	.2	20	26	354	11.80	11	5	ND	13	25	1	2	2	105
G44-PC	1	26	15	34	.3	22	23	350	11.55	13	5	ND	12	28	1	2	2	104
G45-PC	1	23	19	33	.3	24	27	379	13.32	19	5	ND	15	29	2	2	2	114
G46-PC	1	24	16	30	1.8	22	28	367	13.88	16	5	30	13	22	2	2	2	113
G47-PC	1	35	13	29	.3	16	15	292	10.35	13	5	ND	11	24	2	2	2	109
G48-PC	1	24	18	27	4.3	28	33	359	13.72	18	5	101	12	33	1	2	2	104
G49-PC	1	23	16	30	6.7	27	31	324	13.59	18	5	198	12	21	1	2	2	106
G50-PC	1	23	14	31	.5	22	26	336	12.18	13	5	ND	12	23	1	2	2	105
G51-PC	1	27	18	34	.5	29	38	357	14.20	23	5	7	12	22	2	2	2	110
G52-PC	1	20	15	31	.2	27	30	376	13.40	15	5	ND	10	22	1	2	2	110
G53-PC	1	17	25	30	.1	23	27	322	12.42	18	5	ND	10	21	1	2	2	107
G54-PC	1	50	16	32	.2	28	33	388	13.47	19	5	ND	11	24	1	2	2	109
G55-PC	1	14	11	21	.2	16	18	275	11.55	12	5	ND	13	14	1	2	2	98
G56-PC	1	23	12	28	.1	29	36	311	13.64	18	5	ND	12	22	1	2	2	103
G57-PC	1	21	17	25	.3	29	33	308	13.81	15	5	ND	11	17	1	2	2	101
STD C/AU-R	18	58	38	132	7.2	68	30	1033	4.09	39	17	6	37	48	18	15	19	58

SAMPLE#	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	H.M. %	H.M. GM	SAMPLE WT GM	MAG. WT GM
P1-PC	1.24	.088	47	35	.90	1073	.27	24	1.47	.02	.15	1	896	2.70	2.70	100	.2
P2-PC	1.19	.113	123	42	1.07	79	.40	16	1.66	.02	.11	1	392	4.13	6.60	160	.1
P3-PC	1.10	.110	121	40	1.01	99	.39	18	1.51	.02	.08	2	88	6.00	9.60	160	.1
P4-PC	1.29	.119	114	37	1.01	43	.36	14	1.60	.02	.09	1	2153	4.92	9.60	195	.1
P5-PC	2.21	.109	97	39	.93	90	.35	14	1.81	.03	.13	2	105	2.28	3.30	145	.1
P6-PC	3.79	.099	140	54	1.19	98	.54	22	2.66	.06	.27	1	36	1.00	1.00	100	.1
P7-PC	1.27	.114	102	38	1.01	50	.35	13	1.60	.02	.08	1	263	6.71	9.40	140	.1
P8-PC	1.18	.088	104	41	1.02	44	.36	17	1.52	.02	.09	1	8	5.18	8.80	170	.6
T24-PC	.38	.092	33	53	1.49	109	.19	8	1.74	.01	.10	1	3160	11.43	20.00	175	2.3
G30-PC	.59	.081	43	44	1.12	54	.33	19	1.43	.01	.10	1	3	10.07	14.60	145	.9
G32-PC	.56	.079	43	47	1.18	51	.34	15	1.46	.01	.10	1	4370	13.77	17.90	130	.7
G33-PC	.57	.087	39	44	1.23	56	.32	20	1.52	.01	.10	1	2240	9.27	13.90	150	.8
G34-PC	.53	.065	60	42	.82	485	.31	11	1.08	.01	.06	1	2230	14.19	22.00	155	4.7
G35-PC	.87	.097	57	41	1.15	481	.30	21	1.68	.02	.15	1	2255	3.93	5.70	145	.4
G36-PC	.91	.099	67	44	1.17	737	.35	24	1.71	.02	.15	1	1392	3.42	5.30	155	.5
G37-PC	.76	.095	56	42	1.05	920	.31	24	1.52	.01	.14	1	429	5.15	6.70	130	1.8
G38-PC	.86	.103	50	38	1.16	353	.29	21	1.63	.02	.14	1	13873	3.45	5.00	145	.4
G39-PC	.63	.075	66	40	.87	351	.31	17	1.20	.01	.09	1	8119	8.30	11.20	135	1.6
G40-PC	.83	.102	52	38	1.08	409	.29	26	1.53	.02	.12	1	2424	4.41	6.40	145	.5
G41-PC	.91	.105	58	40	1.23	374	.32	17	1.73	.02	.15	1	15	3.88	6.20	160	.3
G42-PC	.77	.092	60	42	1.06	231	.30	20	1.49	.01	.11	1	14674	5.10	7.90	155	.7
G43-PC	.84	.100	60	42	1.21	182	.31	18	1.65	.01	.13	1	32	4.64	6.50	140	.5
G44-PC	.92	.114	57	42	1.26	153	.32	21	1.77	.02	.15	1	1153	3.41	4.60	135	.3
G45-PC	.87	.096	69	45	1.10	392	.35	20	1.60	.01	.14	1	1236	5.20	5.20	100	.5
G46-PC	.74	.083	65	44	1.02	245	.33	24	1.47	.01	.12	1	30407	5.58	6.70	120	.7
G47-PC	.83	.056	55	45	1.30	160	.37	22	1.82	.02	.15	1	178	3.50	4.90	140	.1
G48-PC	.67	.081	55	41	.98	864	.30	16	1.32	.01	.09	1	62102	6.89	9.30	135	.8
G49-PC	.72	.087	56	39	1.06	178	.30	16	1.46	.01	.11	1	249308	6.14	8.90	145	.5
G50-PC	.77	.098	56	43	1.21	200	.32	19	1.61	.01	.12	1	1	6.72	8.40	125	.5
G51-PC	.78	.090	57	42	1.06	215	.31	19	1.53	.01	.12	1	5950	4.92	6.40	130	.4
G52-PC	.77	.094	50	43	1.23	180	.31	21	1.66	.01	.13	1	173	4.55	6.60	145	.3
G53-PC	.73	.090	57	43	1.18	153	.32	17	1.58	.01	.12	1	643	5.24	7.60	145	.5
G54-PC	.78	.093	52	44	1.17	400	.33	17	1.62	.01	.14	2	80	5.05	5.30	105	.3
G55-PC	.54	.068	59	40	.84	133	.30	12	1.07	.01	.06	1	5610	12.56	15.70	125	1.7
G56-PC	.67	.087	56	41	1.12	360	.30	20	1.46	.01	.11	1	19974	6.37	8.60	135	.5
G57-PC	.52	.070	49	41	.92	243	.30	19	1.16	.01	.08	4	13590	11.06	18.80	170	1.6
STD C/AU-R	.49	.093	38	56	.90	175	.06	38	1.96	.06	.13	13	490	-	-	-	-

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	H.M. %	H.M. Gm	SAMPLE WT GM	MAG. WT GM
G58-PC	1	26	85	34	.3	25	31	296	14.56	19	5	ND	13	26	1	2	2	113	.70	.078	53	45	1.08	493	.35	14	1.49	.01	.12	1	613	5.25	6.30	120	.3
G59-PC	1	31	114	39	.3	33	40	295	15.56	22	5	ND	12	30	1	2	2	108	.63	.081	44	43	1.02	1003	.31	12	1.36	.01	.11	1	657	5.06	8.10	160	.5
G60-PC	1	16	24	28	.3	19	25	250	12.68	12	5	13	14	41	1	2	4	101	.50	.063	55	43	.83	1244	.32	16	1.10	.01	.08	1	13900	10.59	14.30	135	1.2
G60A-PC	1	21	27	41	.2	23	28	336	12.52	16	5	ND	10	28	2	2	2	105	.79	.095	48	42	1.29	414	.32	17	1.76	.02	.15	1	1101	3.46	4.50	130	.2
G61-PC	1	14	21	27	.2	15	21	257	12.52	10	5	ND	14	22	1	2	2	107	.61	.076	62	44	.99	293	.34	10	1.33	.01	.10	1	2961	5.87	8.80	150	.6
G62-PC	1	17	75	31	.4	15	18	300	12.62	12	5	ND	13	21	2	2	2	109	.70	.081	56	48	1.10	128	.36	13	1.51	.01	.12	1	225	4.81	6.50	135	.4
G63-PC	1	15	12	29	.2	16	21	254	11.83	7	5	ND	10	20	1	2	2	104	.63	.080	50	44	1.15	198	.33	11	1.48	.01	.11	1	324	5.29	7.40	140	.3
G64-PC	1	10	10	20	.2	11	15	185	9.12	7	5	ND	10	11	1	2	2	79	.41	.054	41	35	.85	128	.26	7	.99	.01	.07	1	3000	15.26	29.00	190	1.4
G65-PC	1	13	16	27	.3	15	24	264	13.03	13	5	ND	12	19	2	2	2	111	.62	.072	55	46	.99	132	.34	11	1.36	.01	.12	1	2119	6.16	7.70	125	.4
G66-PC	1	26	170	35	1.0	16	21	289	13.42	16	5	ND	11	21	2	2	2	115	.64	.071	54	49	1.02	219	.38	10	1.39	.01	.11	1	2739	6.44	8.70	135	.5
G67-PC	1	18	229	47	.9	14	15	145	15.57	10	5	ND	12	14	1	2	2	86	.34	.043	60	38	.82	131	.30	8	1.47	.01	.27	1	68	2.32	4.40	190	.2
G68-PC	1	25	43	47	.3	15	20	252	11.08	9	5	ND	9	25	1	2	2	79	.91	.132	50	30	1.66	260	.26	3	2.12	.01	.19	1	771	4.44	6.00	135	.2
G69-PC	1	131	50	31	2.1	31	50	359	14.72	27	5	35	10	24	1	3	2	95	.67	.091	42	36	1.01	388	.27	9	1.40	.01	.13	1	28936	5.63	7.60	135	.8
G70-PC	1	12	11	77	.2	13	24	142	10.66	9	5	ND	5	15	1	2	2	56	.41	.123	34	23	1.87	52	.17	2	2.05	.01	.15	1	420	9.87	22.20	225	2.0
G71-PC	1	12	16	26	.1	14	23	146	11.47	10	5	ND	5	13	1	2	2	71	.39	.104	31	22	2.36	88	.19	2	2.53	.01	.16	1	910	10.11	18.20	180	.3
G72-PC	1	11	47	28	.3	14	22	119	11.59	11	5	ND	5	12	1	2	2	66	.35	.109	25	22	2.18	69	.17	2	2.29	.01	.18	1	3	13.38	19.40	145	.5
G73-PC	1	17	12	26	1.1	17	23	237	12.29	13	5	ND	9	19	2	2	2	103	.50	.077	34	44	1.11	412	.30	12	1.34	.01	.09	1	17	11.88	19.60	165	.8
G74-PC	1	18	19	26	.5	15	22	263	13.25	12	5	ND	12	21	1	2	2	109	.55	.072	56	45	.98	376	.33	11	1.29	.01	.10	1	6326	7.54	13.20	175	1.0
G75-PC	1	18	13	25	.5	16	26	244	13.00	15	5	ND	12	16	1	2	2	105	.53	.072	50	45	.99	204	.31	15	1.27	.01	.10	1	1060	8.45	13.10	155	.8
G76-PC	1	15	16	25	1.3	13	17	236	12.72	13	5	4	13	18	2	2	2	110	.61	.077	49	47	.99	153	.34	12	1.30	.01	.10	2	13581	8.00	12.40	155	.5
G77-PC	1	38	16	34	.4	19	27	278	12.90	13	5	ND	9	24	1	2	2	112	.78	.099	47	47	1.30	182	.33	16	1.78	.01	.17	2	644	3.88	6.20	160	.2
G78-PC	1	43	25	36	.3	19	23	289	12.94	14	5	ND	11	23	1	2	2	114	.77	.086	50	46	1.18	172	.37	20	1.69	.01	.18	1	212	2.88	4.90	170	.2
STD C/AU-R	18	60	38	132	6.5	68	30	944	4.12	41	17	6	36	48	18	14	21	58	.49	.093	38	56	.90	172	.06	37	1.99	.06	.13	12	480	-	-	-	-

Bapty Research L..ited FILE # 89-4814

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	H.M. %	H.M. Gm	SAMPLE WT GM	MAG. WT GM
P1-H	3	131	1073	144	3.5	52	39	512	20.24	54	5	ND	17	34	1	38	2	102	1.16	.103	62	38	.73	1265	.24	18	1.33	.02	.13	1	1413	.28	6.50	2300	.8
P2-H	1	17	18	33	.1	14	12	430	6.72	6	5	ND	22	32	1	2	6	91	1.18	.117	108	40	1.00	75	.38	12	1.53	.02	.09	1	232	.20	7.40	3700	.1
P3-H	1	13	67	29	.1	12	13	377	6.78	6	5	ND	19	26	1	2	2	86	1.00	.119	91	38	1.09	95	.34	7	1.47	.01	.07	1	1416	.35	10.80	3050	.1
P4-H	1	13	12	27	.1	12	12	402	6.32	2	5	ND	17	27	1	2	2	85	1.13	.116	84	35	1.03	38	.32	14	1.50	.02	.07	1	77	.30	11.20	3750	.1
P5-H	1	25	27	40	.2	19	14	455	7.99	11	5	ND	16	39	1	2	2	88	2.42	.099	75	35	.88	113	.30	17	1.60	.03	.12	1	67	.23	5.00	2200	.2
P6-H	1	59	18	45	.1	17	13	705	6.74	10	5	ND	24	56	1	2	2	99	3.70	.099	132	41	.85	74	.44	15	1.94	.04	.16	1	1	.07	1.40	2050	.1
P7-H	1	12	12	27	.1	12	12	374	6.41	3	5	ND	14	25	1	2	2	84	1.12	.115	76	35	1.06	40	.30	12	1.48	.02	.07	1	5	.45	14.30	3150	.1
P8-H	1	12	17	26	.1	12	13	353	7.71	7	5	ND	17	23	1	2	2	87	1.06	.084	83	36	1.02	37	.30	10	1.37	.02	.07	1	670	.49	14.80	3050	.6
T24-H	1	35	26	26	.1	29	71	380	13.69	15	5	ND	6	11	1	2	2	98	.35	.098	27	45	1.48	106	.15	5	1.59	.01	.08	1	2	1.36	36.80	2700	3.9
G30-H	1	16	18	26	.1	17	24	215	11.82	5	5	ND	7	13	1	2	2	101	.53	.091	35	41	1.25	53	.28	13	1.45	.01	.08	1	1300	.97	26.80	2750	1.3
G32-H	1	13	13	23	.1	13	18	194	9.96	5	5	ND	7	11	1	2	2	92	.46	.083	34	38	1.23	40	.26	6	1.37	.01	.07	1	920	.98	34.30	3500	1.2
G33-H	1	18	12	28	.2	17	21	260	10.98	4	5	ND	9	14	1	2	2	97	.53	.089	37	40	1.33	56	.28	10	1.56	.01	.09	1	1030	.86	26.80	3100	1.2
G34-H	1	21	17	25	.1	21	27	283	11.44	8	5	ND	12	20	1	2	2	94	.59	.082	51	39	.97	379	.27	5	1.20	.01	.08	1	4940	.65	20.70	3200	3.0
G35-H	1	26	25	29	.2	29	39	329	13.06	18	5	3	10	27	1	2	2	97	.76	.092	46	38	1.06	538	.28	12	1.42	.01	.11	1	2486	.30	9.90	3350	.9
G36-H	1	29	16	30	.2	30	37	353	12.49	13	5	ND	13	32	1	2	2	98	.76	.091	52	39	1.06	784	.30	8	1.41	.01	.12	1	791	.36	8.50	2350	.7
G37-H	1	29	22	29	.1	30	38	336	12.75	17	5	ND	12	35	1	2	2	95	.74	.100	48	37	1.07	1038	.27	10	1.40	.01	.10	1	30	.53	12.70	2400	1.2
G38-H	1	34	35	33	6.1	33	45	344	13.29	17	5	93	11	24	1	2	2	98	.75	.106	50	37	1.17	280	.26	11	1.53	.01	.12	1	75462	.35	8.80	2500	.7
G39-H	1	25	202	28	.2	26	33	309	12.52	14	5	2	13	21	1	2	2	98	.65	.090	56	39	1.02	349	.29	9	1.29	.01	.09	1	5190	.57	15.30	2700	1.7
G40-H	1	39	19	32	.2	37	45	344	13.11	19	5	ND	11	24	1	2	2	92	.77	.104	44	37	1.10	406	.26	15	1.46	.02	.11	2	2502	.46	11.40	2500	.7
G41-H	1	31	24	33	.1	28	35	307	11.38	12	5	ND	11	23	1	2	2	92	.79	.103	45	36	1.24	308	.26	12	1.58	.01	.12	1	977	.29	9.70	3350	.4
G42-H	1	20	19	27	1.6	24	35	257	12.20	12	5	69	11	19	1	2	2	93	.60	.087	47	36	1.01	372	.24	10	1.25	.01	.08	2	27200	.48	17.90	3750	1.8
G43-H	1	21	19	28	.1	19	23	337	11.14	8	5	ND	12	23	1	3	2	104	.80	.092	58	43	1.14	163	.33	14	1.54	.01	.13	1	576	.21	7.80	3650	.5
G44-H	1	22	14	31	.1	22	29	314	11.86	10	5	ND	12	23	1	2	2	107	.81	.097	59	43	1.21	154	.32	13	1.63	.01	.13	1	696	.25	8.70	3450	.4
G45-H	1	21	12	30	.2	22	27	302	11.52	11	5	ND	13	21	1	2	2	101	.72	.093	53	41	1.13	303	.30	13	1.48	.01	.11	1	147	.37	9.60	2600	.6
G46-H	1	22	20	31	.1	19	24	280	11.58	6	5	ND	12	17	1	2	2	100	.61	.079	56	41	1.02	134	.30	12	1.32	.01	.09	1	11399	.35	13.00	3700	1.2
G47-H	1	21	12	28	.3	15	16	272	9.99	3	5	ND	11	21	1	2	2	109	.79	.049	55	47	1.23	145	.37	14	1.71	.02	.14	1	866	.16	4.60	2850	.1
G48-H	1	22	22	29	.1	23	29	318	12.30	11	5	ND	12	21	1	2	2	102	.67	.087	54	40	1.07	270	.30	10	1.42	.01	.10	1	1080	.35	11.80	3400	.8
G49-H	1	27	18	30	3.8	24	31	318	12.22	11	5	43	12	20	1	2	2	105	.74	.091	50	42	1.10	150	.31	16	1.49	.01	.12	1	25162	.27	8.80	3250	.5
G50-H	1	25	15	32	.1	25	29	330	12.77	10	5	ND	13	22	1	2	2	111	.79	.093	55	45	1.16	128	.33	16	1.59	.02	.13	1	225	.24	7.70	3200	.4
G51-H	1	26	23	30	.7	29	34	300	12.73	15	5	5	11	20	1	2	2	102	.71	.097	48	40	1.15	148	.28	13	1.51	.01	.11	1	24232	.39	12.30	3150	.7
G52-H	1	21	16	33	.2	23	27	325	11.41	9	5	2	11	24	1	2	2	107	.87	.104	49	43	1.33	110	.31	19	1.84	.02	.19	1	6217	.19	5.30	2850	.2
G53-H	1	161	16	66	2.1	22	27	304	11.76	10	5	3	11	22	1	2	2	106	.78	.096	50	42	1.25	114	.33	25	1.69	.02	.15	1	11827	.28	8.30	3000	.3
G54-H	1	20	15	29	.2	26	32	291	11.37	12	7	ND	11	20	1	2	2	96	.70	.101	41	38	1.27	298	.26	15	1.59	.01	.12	1	1757	.40	11.30	2800	.3
G55-H	1	21	17	26	.3	18	24	269	11.47	6	5	ND	12	17	1	2	2	102	.63	.085	52	42	1.14	116	.29	15	1.42	.01	.11	1	2530	.55	18.30	3300	1.2
G56-H	1	24	19	32	.6	32	38	322	12.72	12	6	13	11	22	1	2	2	103	.70	.096	43	42	1.21	432	.29	18	1.56	.01	.13	1	13485	.38	11.70	3050	.5
G57-H	1	20	21	27	.3	23	30	317	12.86	12	5	ND	13	18	1	2	2	104	.59	.080	49	42	1.09	190	.30	15	1.39	.01	.10	1	89	.45	14.20	3150	.8
STD C/AU-R	18	61	41	132	6.6	67	31	949	4.04	38	19	7	38	49	17	15	20	59	.48	.091	39	56	.88	176	.06	34	1.96	.06	.13	12	505	-	-	-	-

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB	H.M. %	H.M. Gm	SAMPLE WT GM	MAG. WT GM
G58-H	1	26	18	34	.3	26	31	262	12.00	16	9	ND	10	23	1	2	2	97	.65	.101	41	39	1.32	314	.27	17	1.73	.01	.14	2	11	.45	11.90	2650	.4
G59-H	1	25	27	27	.2	29	34	256	11.83	16	5	ND	8	21	1	2	3	86	.50	.084	36	35	1.15	778	.23	14	1.39	.01	.09	2	1480	.49	16.20	3300	.8
G60-H	1	16	14	25	.3	19	23	208	10.59	12	5	ND	13	23	1	2	2	90	.48	.078	43	37	1.08	572	.25	14	1.31	.01	.09	1	1970	.50	16.20	3250	1.2
G60A-H	1	15	16	31	.2	22	27	263	10.74	12	5	ND	9	24	1	2	2	91	.65	.093	40	37	1.32	416	.25	15	1.66	.01	.14	1	211	.29	7.60	2650	.2
G61-H	1	16	10	29	.1	18	22	241	10.14	9	5	ND	9	16	1	2	2	90	.57	.093	40	38	1.26	143	.24	8	1.51	.01	.10	1	510	.50	13.80	2750	.7
G62-H	1	13	12	29	.1	16	21	238	9.57	8	5	ND	9	18	1	2	2	85	.57	.090	39	36	1.30	154	.24	8	1.54	.01	.10	1	1050	.32	10.10	3150	.5
G63-H	1	14	15	29	.1	15	21	244	9.79	11	5	ND	9	18	1	2	4	89	.59	.089	39	37	1.29	159	.26	13	1.57	.01	.12	1	83	.24	8.70	3700	.3
G64-H	1	13	14	24	.1	14	18	223	10.38	9	5	ND	10	14	1	2	2	91	.44	.068	38	39	1.00	166	.26	7	1.18	.01	.08	1	2910	.59	21.70	3650	1.6
G65-H	1	11	13	25	.1	15	19	245	10.47	6	5	ND	11	14	1	2	2	92	.50	.077	41	38	1.13	94	.26	8	1.35	.01	.09	1	2470	.38	12.70	3300	.7
G66-H	1	10	15	28	.1	16	20	228	10.25	11	5	ND	9	16	1	2	3	90	.52	.083	39	39	1.23	169	.26	6	1.43	.01	.09	1	1020	.57	18.00	3150	.8
G67-H	1	13	67	31	.2	15	15	125	13.03	10	5	ND	10	10	1	3	5	67	.28	.042	43	30	.90	137	.23	5	1.48	.01	.28	1	46	.18	5.70	3100	.1
G68-H	1	11	9	33	.2	17	21	208	8.89	3	5	ND	7	26	1	2	3	61	.75	.135	35	22	1.94	645	.17	6	2.19	.01	.16	1	1732	.44	10.00	2250	.2
G69-H	1	26	30	35	.1	30	42	307	11.92	24	5	ND	9	20	1	2	4	83	.67	.099	35	32	1.14	280	.21	8	1.47	.01	.12	1	5	.35	8.80	2550	.7
G70-H	1	11	6	79	.1	13	23	141	9.57	7	5	ND	5	13	1	2	2	50	.36	.111	26	21	1.87	49	.14	2	1.92	.01	.13	1	5	.92	28.50	3100	2.8
G71-H	1	8	12	26	.1	16	25	141	9.27	6	5	ND	4	12	1	2	2	58	.38	.114	22	18	2.80	73	.13	2	2.78	.01	.13	1	1	.90	32.50	3600	.2
G72-H	1	8	9	22	.1	16	22	125	9.98	6	5	ND	4	12	1	2	2	57	.36	.117	21	18	2.42	70	.14	2	2.45	.01	.17	1	3	.89	29.80	3350	.6
G73-H	1	15	15	26	.1	16	24	214	11.03	8	5	ND	9	16	1	2	2	94	.48	.083	29	39	1.20	347	.24	8	1.38	.01	.09	1	7	.65	21.10	3250	.8
G74-H	1	11	13	27	.1	17	24	247	10.83	9	5	ND	13	17	1	2	2	92	.52	.088	37	38	1.29	230	.24	8	1.52	.01	.11	1	1670	.54	14.50	2700	.7
G75-H	1	14	14	25	.1	18	24	213	10.35	9	5	ND	9	15	1	2	5	86	.48	.086	38	37	1.19	175	.22	9	1.37	.01	.09	1	24	.82	22.60	2750	1.0
G76-H	1	14	13	24	.1	15	21	201	10.86	10	7	ND	10	14	1	2	2	91	.51	.089	39	37	1.24	88	.23	11	1.45	.01	.10	1	2680	.69	16.90	2450	.5
G77-H	1	14	16	30	.1	18	25	288	10.49	10	5	ND	8	19	1	2	2	91	.63	.101	35	38	1.37	182	.24	14	1.67	.01	.13	1	1344	.36	10.40	2900	.3
G78-H	1	17	15	32	.2	21	26	279	11.38	10	5	ND	9	19	1	2	2	97	.66	.100	36	39	1.34	215	.26	15	1.68	.01	.14	1	19	.43	9.90	2300	.3
STD C/AU-R	18	60	36	132	6.7	66	31	938	4.04	41	21	6	37	48	18	15	21	58	.49	.091	38	55	.90	172	.06	34	1.99	.06	.13	12	530	-	-	-	-

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(6 253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Soil -80 Mesh AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: NOV 30 1989 **DATE REPORT MAILED:** Dec 5/89 **SIGNED BY**..........D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

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SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
R1 0M	1	14	11	28	.3	12	5	338	1.37	2	5	ND	7	17	1	2	2	12	1.59	.113	19	9	.44	208	.03	4	1.49	.01	.09	1	3
R2 50M	1	8	9	47	.2	16	4	572	1.27	2	5	ND	4	15	1	2	2	12	.19	.270	9	8	.21	482	.06	4	2.08	.01	.10	2	1
R3 100M	1	9	6	40	.2	13	4	302	1.12	2	5	ND	2	19	1	2	3	13	.19	.193	8	6	.14	310	.07	5	1.97	.02	.10	1	1
R4 150M	1	2	6	16	.1	8	3	31	1.04	2	5	ND	9	4	1	2	2	7	.06	.029	29	8	.32	80	.02	3	.76	.01	.07	1	1
R5 200M	1	5	8	21	.1	10	6	104	1.35	2	5	ND	9	4	1	2	2	9	.08	.022	35	10	.41	65	.01	2	.78	.01	.09	1	1
R6 250M	1	5	8	22	.2	11	5	203	1.22	2	5	ND	4	12	1	2	2	12	.15	.095	18	9	.25	225	.03	2	1.27	.01	.07	1	1
R7 300M	1	8	8	26	.2	14	5	243	1.31	2	5	ND	3	15	1	2	6	16	.17	.140	10	7	.17	223	.07	3	1.93	.02	.08	1	1
R8 350M	1	6	13	45	.1	17	5	452	1.34	5	5	ND	3	15	1	2	3	16	.12	.187	10	9	.19	376	.06	3	1.86	.01	.06	1	1
R9 400M	1	9	11	36	.1	18	5	154	1.32	3	5	ND	3	14	1	2	2	17	.12	.151	10	7	.15	194	.08	4	2.38	.02	.06	1	1
R10 450M	1	1	6	17	.1	6	3	61	1.04	3	5	ND	8	4	1	2	2	7	.05	.024	35	7	.23	71	.02	3	.64	.01	.08	1	3
R11 500M	1	6	9	32	.2	15	5	84	1.34	2	5	ND	7	17	1	2	2	10	.23	.175	21	8	.23	336	.05	3	1.94	.01	.12	1	1
R12 550M	1	7	8	40	.1	10	4	248	1.00	2	5	ND	2	17	1	2	2	13	.19	.111	9	7	.14	263	.06	6	1.48	.02	.08	1	1
R13 600M	1	1	3	10	.1	4	2	22	.78	2	5	ND	11	3	1	2	2	5	.06	.023	34	5	.17	38	.01	6	.38	.01	.05	1	1
R14 650M	1	9	12	27	.3	13	5	228	1.20	2	5	ND	4	14	1	2	5	14	.18	.132	14	6	.16	196	.06	6	1.90	.01	.06	1	2
R15 700M	1	5	10	27	.1	11	4	85	.99	2	5	ND	5	8	1	2	8	9	.11	.028	18	7	.21	117	.03	2	.98	.01	.06	1	2
R16 750M	1	10	10	24	.1	15	5	98	1.47	4	5	ND	3	13	1	2	2	14	.15	.112	10	8	.18	216	.05	4	2.16	.02	.07	1	1
R17 800M	1	2	7	14	.1	5	3	49	.94	2	5	ND	6	4	1	2	2	7	.06	.016	25	6	.19	41	.02	8	.65	.01	.06	1	1
R18 850M	1	4	10	25	.1	9	4	40	1.24	2	5	ND	7	7	1	2	4	9	.08	.064	25	7	.22	132	.03	3	1.12	.01	.09	1	3
R19 900M	1	10	10	43	.1	16	6	112	1.62	2	5	ND	5	27	1	2	3	13	.33	.300	14	10	.26	584	.06	6	2.38	.02	.12	1	1
R20 950M	1	13	10	27	.3	15	4	243	1.57	2	5	ND	3	20	1	2	2	21	.18	.199	8	8	.11	206	.10	5	3.34	.03	.05	1	2
R21 1000M	1	3	9	20	.1	8	3	138	1.03	2	5	ND	8	5	1	2	2	8	.05	.054	30	7	.17	104	.02	2	.73	.01	.06	1	2
R22 1050M	1	11	10	47	.2	20	5	350	1.17	3	5	ND	3	16	1	2	7	15	.14	.042	13	7	.16	212	.07	4	2.04	.02	.06	1	1
R23 1100M	1	6	10	36	.1	23	5	125	1.16	2	5	ND	2	11	1	2	2	13	.12	.130	11	7	.14	212	.06	2	1.93	.01	.07	1	3
R24 1150M	1	2	8	21	.1	9	3	51	1.14	2	5	ND	6	5	1	2	3	10	.06	.015	28	9	.28	56	.02	3	.64	.01	.05	1	3
R25 1200M	1	8	7	46	.2	16	5	491	1.26	2	5	ND	2	17	1	2	2	16	.23	.204	8	8	.16	233	.07	4	1.93	.02	.10	1	1
R26 1250M	1	12	9	40	.1	25	5	394	1.46	3	5	ND	2	23	1	2	5	16	.18	.351	7	10	.18	408	.08	6	2.46	.02	.06	1	2
R27 1300M	1	10	11	52	.2	21	5	212	1.39	3	5	ND	2	18	1	2	6	18	.20	.193	8	8	.14	232	.09	5	2.78	.02	.06	1	2
R28 1350M	1	6	9	27	.1	10	5	209	1.24	3	5	ND	9	5	1	2	3	9	.16	.052	31	12	.39	161	.02	8	.98	.01	.09	1	2
R29 1400M	1	13	12	49	.3	22	5	323	1.63	4	5	ND	3	20	1	2	2	23	.20	.213	8	8	.17	259	.11	4	3.45	.02	.06	1	2
R30 1450M	1	14	10	30	.2	25	5	312	1.48	2	5	ND	4	15	1	2	3	18	.16	.126	12	9	.19	231	.08	10	2.68	.02	.08	2	3
R31 1500M	1	11	7	34	.1	17	4	109	1.26	2	5	ND	1	14	1	2	3	14	.20	.126	8	7	.16	205	.06	4	1.95	.02	.08	1	4
R32 1550M	1	12	12	49	.1	21	5	190	1.58	2	5	ND	3	16	1	2	2	18	.19	.185	10	9	.19	252	.08	7	2.62	.02	.08	1	4
R33 1600M	1	4	8	39	.1	7	4	255	.98	2	5	ND	4	11	1	2	2	11	.14	.144	12	6	.13	362	.05	4	1.05	.01	.08	1	1
R34 1650M	1	9	10	40	.1	11	4	412	1.30	2	5	ND	2	16	1	2	3	14	.23	.373	9	7	.16	362	.07	4	2.19	.02	.09	2	2
R35 1700M	1	6	7	31	.1	14	4	73	1.27	2	5	ND	4	8	1	2	2	13	.14	.032	19	9	.23	154	.04	3	1.36	.01	.07	1	2
R36 1750M	1	8	5	42	.1	17	4	363	1.27	2	5	ND	3	10	1	2	2	12	.11	.130	13	9	.19	328	.05	4	1.89	.01	.09	1	2
STD C/AU-S	18	57	36	132	7.0	67	30	992	4.06	37	21	7	38	49	18	15	22	58	.48	.095	39	56	.88	177	.06	34	1.96	.06	.13	12	50

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
R37 1800M	1	2	6	36	.1	12	4	277	1.12	2	5	ND	4	13	1	2	3	10	.13	.095	22	8	.24	245	.04	2	1.35	.01	.07	1	1
R38 1850M	1	8	6	33	.2	17	5	78	1.39	2	5	ND	4	13	1	2	2	16	.16	.079	14	7	.21	167	.06	2	1.95	.01	.06	1	1
R39 1900M	1	5	9	27	.1	8	4	174	1.07	2	5	ND	5	9	1	2	5	9	.10	.121	22	8	.24	256	.03	3	.88	.01	.06	1	2
R40 1950M	1	8	4	22	.1	14	4	109	1.21	3	5	ND	2	11	1	2	2	13	.14	.014	15	9	.25	123	.04	3	1.29	.01	.08	1	1
R41 2000M	1	5	2	16	.1	10	4	46	1.17	2	5	ND	5	4	1	2	3	10	.07	.027	28	8	.25	91	.02	2	.73	.01	.06	1	1
R42 2050M	1	7	3	18	.1	13	7	117	1.65	2	5	ND	4	5	1	2	2	12	.08	.084	29	11	.45	201	.02	3	1.03	.01	.09	1	1
R43 2100M	1	8	2	20	.1	9	4	47	1.04	2	5	ND	8	7	1	2	2	9	.08	.017	31	8	.34	115	.03	3	.85	.01	.06	1	2
R44 2150M	1	7	6	25	.1	27	6	184	1.51	3	5	ND	3	11	1	2	2	16	.11	.091	16	9	.26	239	.06	7	2.03	.01	.07	1	1
R45 2200M	1	7	7	33	.1	21	5	120	1.35	4	5	ND	3	11	1	2	2	12	.11	.188	16	9	.29	228	.05	3	1.81	.01	.08	1	1
R46 2250M	1	4	2	19	.1	8	3	74	.93	2	5	ND	5	6	1	2	2	7	.11	.019	24	8	.25	101	.02	8	.67	.01	.07	1	3
R47 2300M	1	5	4	32	.1	11	4	127	.92	2	5	ND	2	14	1	2	2	11	.24	.061	12	7	.16	270	.04	5	1.11	.01	.09	1	1
R48 2350M	1	3	7	27	.1	11	4	79	1.13	3	5	ND	4	8	1	2	3	10	.11	.032	21	10	.27	162	.03	4	1.13	.01	.09	1	1
R49 2400M	1	3	6	18	.1	10	5	146	1.27	2	5	ND	4	8	1	3	2	10	.12	.057	18	10	.29	255	.03	6	1.15	.01	.11	1	1
R50 2450M	1	6	6	26	.1	13	5	109	1.55	2	5	ND	6	9	1	2	2	11	.17	.046	22	10	.39	141	.04	6	1.45	.01	.13	1	1
R51 2500M	1	2	4	16	.1	11	4	56	1.01	4	5	ND	8	6	1	2	2	8	.08	.025	32	9	.28	114	.02	7	.81	.01	.09	1	1
R52 2550M	1	3	3	32	.1	17	4	105	1.10	2	5	ND	3	16	1	2	2	11	.16	.059	15	9	.23	260	.05	6	1.49	.01	.12	1	1
R53 2600M	1	2	3	14	.1	7	3	168	.87	2	5	ND	7	8	1	2	2	6	.10	.014	33	9	.20	108	.02	6	.62	.01	.08	1	1
R54 2650M	1	1	2	15	.1	9	3	75	.95	2	5	ND	6	6	1	2	2	7	.07	.021	25	8	.20	107	.03	5	.86	.01	.10	1	1
R55 2700M	1	3	2	20	.1	15	4	85	1.15	2	5	ND	5	11	1	2	5	9	.12	.057	20	9	.26	191	.03	4	1.20	.01	.11	1	1
R56 2750M	1	3	3	29	.1	12	4	124	1.14	2	5	ND	4	13	1	2	2	9	.17	.063	16	9	.27	189	.04	8	1.25	.01	.14	1	1
R57 2800M	1	4	4	39	.1	13	4	181	1.12	2	5	ND	3	14	1	3	2	11	.15	.074	16	8	.29	315	.04	9	1.26	.01	.10	1	3
R58 2850M	1	4	5	35	.1	14	3	215	1.08	2	5	ND	3	18	1	2	2	10	.13	.123	14	9	.25	385	.04	5	1.34	.01	.12	1	2
R59 2900M	1	5	5	39	.1	21	4	129	1.12	2	5	ND	3	19	1	2	2	12	.17	.086	13	9	.25	251	.05	4	1.47	.02	.10	1	1
R60 2950M	1	3	2	18	.2	9	5	41	1.16	2	5	ND	8	5	1	2	2	7	.10	.024	32	9	.46	74	.02	14	.74	.01	.08	1	1
R61 3000M	1	5	9	33	.1	15	5	132	1.27	3	5	ND	4	13	1	2	2	11	.14	.138	16	10	.31	424	.05	11	1.53	.01	.09	1	1
R62 3050M	1	8	6	34	.1	13	6	236	1.40	3	5	ND	3	18	1	2	2	12	.24	.065	15	10	.37	332	.05	6	1.72	.01	.14	1	1
R63 3100M	1	7	3	18	.2	11	6	148	1.32	2	5	ND	7	5	1	4	2	9	.25	.023	26	11	.53	128	.02	11	.89	.01	.09	1	1
R64 3150M	1	4	5	20	.1	10	5	162	1.35	2	5	ND	7	7	1	2	2	9	.09	.037	26	9	.39	165	.03	8	.83	.01	.08	1	1
R65 3200M	1	5	6	29	.2	12	3	178	.92	2	5	ND	1	24	1	2	2	12	.23	.147	4	6	.14	359	.05	3	1.30	.03	.08	1	2
R66 3250M	1	5	5	26	.1	13	5	93	1.55	2	5	ND	4	10	1	2	2	10	.10	.040	20	9	.34	157	.04	3	1.32	.01	.10	1	1
R67 3300M	1	5	6	40	.2	11	4	577	.93	2	5	ND	1	29	1	2	2	12	.23	.261	6	6	.11	591	.05	7	1.33	.02	.08	1	2
R68 3350M	1	4	6	31	.1	12	5	157	1.41	2	5	ND	3	16	1	3	2	10	.19	.040	14	8	.27	224	.04	6	1.54	.01	.10	1	2
R69 3400M	1	4	5	46	.2	11	4	335	1.28	2	5	ND	3	15	1	2	2	10	.21	.052	13	8	.23	305	.04	6	1.45	.01	.11	1	4
R70 3450M	1	2	4	37	.3	9	4	166	1.17	2	5	ND	4	8	1	2	2	11	.06	.044	17	8	.17	200	.04	6	1.23	.01	.09	1	1
R71 3500M	1	5	7	64	.2	18	6	919	1.31	5	5	ND	3	14	1	2	2	14	.17	.087	11	9	.18	363	.06	10	2.08	.02	.10	1	2
R72 3550M	1	4	10	34	.2	13	6	161	1.46	5	5	ND	3	12	1	3	2	12	.14	.026	17	11	.24	248	.05	7	1.65	.01	.11	1	4
STD C/AU-S	18	58	37	132	6.8	66	31	1032	4.00	41	22	7	37	48	17	16	21	57	.47	.092	38	56	.87	172	.06	33	1.93	.06	.13	13	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
R73 3600M	1	7	6	31	.2	12	4	256	1.29	5	7	ND	5	11	1	3	2	11	.16	.022	16	8	.19	163	.04	5	1.19	.01	.13	1	1
R74 3650M	1	32	8	35	.2	17	7	216	1.73	5	5	ND	4	18	1	2	2	15	.25	.024	12	11	.27	376	.06	4	2.39	.02	.14	1	1
R75 3700M	1	10	4	49	.2	10	5	183	1.64	2	6	ND	5	18	1	2	2	13	.26	.039	12	9	.28	400	.06	8	1.97	.02	.14	1	1
R76 3750M	1	8	7	43	.4	12	5	287	1.63	4	7	ND	4	18	1	2	2	14	.19	.031	12	10	.25	348	.06	9	2.02	.02	.17	1	1
R77 3800M	1	8	4	28	.2	11	5	71	1.80	4	6	ND	7	9	1	3	4	17	.11	.027	26	12	.37	78	.04	3	1.06	.01	.16	1	1
R78 3850M	1	6	5	31	.3	12	4	206	1.40	2	6	ND	5	13	1	2	3	11	.14	.029	17	10	.24	186	.04	5	1.31	.01	.16	1	1
R79 3900M	1	9	3	31	.2	14	5	73	1.69	2	5	ND	7	11	1	3	2	12	.14	.040	22	11	.35	135	.04	3	1.28	.01	.15	1	6
R80 3950M	1	7	5	40	.3	15	4	100	1.02	2	5	ND	2	40	1	2	2	14	.34	.279	5	6	.14	353	.07	4	1.61	.03	.08	1	2
R81 4000M	1	6	3	53	.1	10	4	399	1.18	2	5	ND	2	23	1	2	2	12	.20	.060	10	7	.21	295	.05	6	1.30	.02	.12	1	1
R82 4050M	1	10	4	40	.3	19	5	115	1.47	3	5	ND	4	20	1	2	2	13	.18	.129	13	9	.28	250	.05	4	1.63	.02	.11	1	1
R83 4100M	1	9	8	43	.1	15	4	328	1.35	2	5	ND	2	23	1	2	2	12	.21	.094	10	9	.22	308	.05	4	1.69	.02	.14	1	1
R84 4150M	1	9	3	44	.2	15	5	205	1.45	2	5	ND	4	24	1	2	2	13	.24	.115	13	8	.26	385	.05	4	1.50	.01	.11	1	2
R85 4200M	1	10	2	36	.1	12	5	265	1.40	4	5	ND	4	34	1	2	2	12	.37	.135	16	7	.31	224	.04	3	1.12	.02	.10	1	1
R86 4250M	1	8	6	41	.3	18	4	205	1.07	2	5	ND	3	27	1	2	2	12	.26	.230	7	7	.17	511	.05	5	1.48	.02	.09	1	1
R87 4300M	1	12	6	30	.2	19	6	90	1.92	2	5	ND	4	11	1	2	2	15	.14	.051	18	11	.37	175	.05	8	1.72	.01	.12	1	2
R88 4350M	1	9	4	31	.1	18	6	103	1.72	5	5	ND	4	15	1	2	2	15	.14	.133	15	9	.31	219	.05	7	1.69	.02	.11	1	1
R89 4400M	1	7	5	36	.2	14	6	404	1.38	2	5	ND	2	27	1	2	2	14	.27	.149	8	8	.24	493	.05	3	1.73	.02	.12	1	1
R90 4450M	1	12	8	30	.1	10	5	137	1.30	4	5	ND	2	23	1	2	2	14	.31	.033	7	7	.30	348	.06	4	1.77	.03	.11	1	2
R91 4500M	1	6	7	24	.1	11	6	163	1.63	3	5	ND	2	13	1	2	2	12	.26	.017	12	11	.41	225	.05	4	1.76	.02	.12	1	1
R92 4550M	1	15	9	30	.2	14	8	146	2.08	2	5	ND	5	13	1	2	2	13	.21	.039	20	11	.62	213	.04	4	2.00	.01	.14	1	3
R93 4600M	1	11	7	27	.2	12	6	207	1.81	2	5	ND	4	12	1	2	2	14	.13	.046	15	10	.31	233	.05	4	1.77	.01	.14		
R94 4650M	1	8	5	38	.2	11	7	679	1.75	2	5	ND	4	18	1	2	2	13	.41	.068	15	10	.36	366	.04	11	1.73	.01	.17	1	1
R95 4700M	1	12	7	48	.2	16	5	182	1.43	2	5	ND	2	19	1	2	2	15	.22	.107	7	8	.24	300	.07	7	2.11	.03	.13	1	1
S3 00	1	4	9	33	.1	12	6	528	1.35	2	5	ND	2	13	1	2	3	16	.14	.193	10	9	.19	175	.06	10	1.68	.01	.08	1	5
S3 50	1	5	7	25	.2	13	5	203	1.27	5	5	ND	5	13	1	2	5	14	.11	.257	15	8	.21	207	.06	2	1.69	.01	.06	1	36
S3 100	1	7	6	17	.1	12	5	87	1.23	2	5	ND	6	6	1	2	2	13	.06	.057	25	8	.27	93	.04	5	1.19	.01	.05	1	8
S3 150	1	7	6	26	.1	12	4	402	1.24	2	5	ND	3	18	1	2	2	13	.39	.161	16	12	.30	279	.04	3	1.69	.01	.14	1	1
S3 200	1	1	3	14	.1	8	4	145	1.00	2	5	ND	7	5	1	2	2	8	.07	.025	28	9	.35	70	.02	4	.79	.01	.08	1	7
S3 250	1	4	6	25	.1	16	5	125	1.25	2	5	ND	4	12	1	2	2	16	.10	.089	14	8	.20	132	.07	3	1.78	.02	.06	1	11
S3 300	1	4	3	26	.1	11	5	687	1.20	2	5	ND	7	12	1	2	2	9	.20	.088	26	12	.38	176	.02	3	.97	.01	.11	1	1
S3 350	1	4	4	23	.1	11	3	199	1.07	2	5	ND	5	8	1	2	2	9	.10	.026	23	9	.28	109	.03	6	1.18	.01	.08	1	15
S3 400	1	6	7	30	.1	15	5	621	1.22	2	5	ND	3	11	1	2	2	14	.13	.223	14	9	.17	248	.05	4	1.65	.01	.07	1	16
S3 450	1	10	8	28	.2	18	4	96	1.34	2	5	ND	6	12	1	2	2	17	.12	.069	17	9	.20	129	.07	2	2.09	.02	.08	1	1
S3 500	1	5	7	44	.1	14	5	805	1.31	2	5	ND	2	15	1	2	2	16	.11	.275	8	9	.15	276	.07	2	1.78	.01	.09	1	7
S3 550	1	5	9	42	.1	13	5	300	1.32	2	5	ND	2	12	1	2	2	16	.11	.141	15	9	.22	166	.05	2	1.36	.01	.06	1	3
S3 600	1	7	4	41	.1	17	6	236	1.43	3	5	ND	4	13	1	2	3	17	.11	.060	16	10	.26	201	.06	9	1.91	.01	.08	1	1
STD C/AU-S	18	57	37	132	6.8	70	30	1028	4.03	37	23	7	38	48	17	14	17	57	.47	.093	38	55	.88	172	.06	33	1.97	.06	.14	12	53

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
S3 680	1	3	3	20	.1	10	4	83	1.15	3	5	ND	5	4	1	2	2	7	.06	.022	23	9	.46	51	.01	2	.82	.01	.05	1	30
S3 730	1	5	4	19	.1	5	3	370	.92	2	5	ND	3	9	1	2	2	9	.15	.048	19	6	.21	114	.02	3	.69	.01	.08	1	27
S3 800	1	5	4	18	.1	8	3	39	1.13	3	5	ND	7	6	1	2	2	9	.07	.024	31	7	.22	102	.03	2	.97	.01	.07	1	13
S3 850	1	4	5	15	.1	8	3	28	1.15	2	5	ND	7	5	1	2	2	9	.07	.014	33	7	.28	55	.02	4	.79	.01	.07	1	1
S3 900	1	4	6	25	.1	10	4	125	1.18	2	5	ND	6	7	1	2	2	10	.07	.046	23	7	.26	123	.04	4	1.42	.01	.08	1	3
S3 950	1	10	8	40	.1	21	6	240	1.56	2	5	ND	3	17	1	2	4	20	.14	.124	8	8	.21	192	.09	3	2.62	.02	.07	1	1
S3 1000	1	6	7	33	.1	14	5	167	1.35	2	5	ND	3	14	1	2	2	15	.14	.118	14	8	.22	222	.06	2	1.63	.01	.07	1	1
S3 1050	1	5	7	39	.1	10	5	285	1.22	2	5	ND	2	12	1	2	2	13	.14	.117	15	8	.22	224	.05	3	1.26	.01	.07	1	15
S3 1100	1	7	7	32	.2	17	5	231	1.33	2	6	ND	4	16	1	2	3	17	.13	.136	12	7	.19	144	.07	8	1.85	.02	.07	2	12
S3 1150	1	8	3	27	.1	9	5	481	1.23	3	5	ND	4	10	1	2	2	13	.20	.031	21	8	.28	156	.02	3	1.06	.01	.08	1	40
S3 1200	1	5	6	29	.1	10	3	358	1.02	2	5	ND	3	12	1	2	4	12	.18	.135	12	6	.15	227	.05	2	1.23	.01	.08	1	3
S3 1250	1	5	5	30	.1	11	4	46	1.22	2	5	ND	8	6	1	2	2	11	.07	.051	25	7	.21	113	.04	2	1.30	.01	.08	1	5
S3 1300	1	8	5	37	.1	16	4	187	1.28	2	5	ND	3	13	1	2	6	14	.17	.111	12	8	.18	225	.06	2	1.98	.02	.10	1	1
S3 1350	1	4	3	22	.1	11	3	136	.97	2	5	ND	5	9	1	2	2	10	.11	.057	20	5	.16	166	.04	4	1.07	.01	.07	1	2
S3 1400	1	8	8	33	.2	12	4	363	1.14	2	5	ND	4	9	1	2	5	12	.14	.068	17	7	.21	191	.04	5	1.39	.01	.08	1	2
S3 1450	1	4	6	32	.1	9	3	329	.95	2	5	ND	3	11	1	2	2	11	.13	.055	13	6	.16	178	.04	3	1.23	.01	.10	1	1
S3 1500	1	5	3	15	.1	7	4	200	1.12	3	6	ND	9	4	1	2	2	9	.05	.024	32	7	.26	79	.01	2	.73	.01	.08	1	1
S3 1550	1	8	8	29	.1	13	5	320	1.23	2	5	ND	1	15	1	2	2	14	.14	.290	7	6	.11	472	.06	3	1.93	.02	.06	1	1
S3 1600	1	4	7	26	.1	12	3	210	1.04	2	5	ND	4	9	1	2	2	11	.10	.099	14	6	.16	220	.05	2	1.41	.01	.06	1	1
S3 1650	1	10	12	37	.1	16	5	126	1.49	2	5	ND	3	17	1	2	2	16	.20	.115	9	7	.19	284	.09	4	2.85	.02	.07	1	7
S3 1700	1	9	7	44	.2	13	4	285	1.34	2	5	ND	2	24	1	2	2	18	.28	.284	5	6	.13	201	.09	5	2.64	.03	.06	1	10
S3 1750	1	6	8	39	.1	12	5	249	1.33	2	5	ND	3	19	1	2	2	13	.16	.362	12	7	.19	348	.06	3	1.82	.01	.08	1	1
S3 1800	1	5	4	21	.2	11	4	95	1.04	2	5	ND	6	7	1	3	3	10	.10	.030	20	8	.23	167	.03	4	1.23	.01	.06	1	7
S3 1850	1	5	6	25	.1	14	4	324	1.11	2	5	ND	5	8	1	2	2	12	.08	.163	16	6	.16	181	.05	9	1.54	.01	.06	1	18
S3 1900	1	6	8	29	.1	12	4	218	1.24	2	7	ND	6	10	1	2	2	12	.13	.081	19	8	.27	200	.05	2	1.72	.01	.10	1	21
S3 1950	1	3	6	27	.2	12	4	61	1.25	2	7	ND	5	8	1	2	2	10	.12	.045	23	10	.29	189	.04	2	1.51	.01	.09	1	10
S3 2000	1	4	9	28	.2	9	4	195	1.12	2	7	ND	5	11	1	2	2	11	.14	.054	20	8	.24	147	.04	4	1.45	.01	.09	1	12
S3 2050	1	7	7	16	.1	9	4	47	1.20	2	5	ND	5	6	1	2	2	9	.08	.041	21	8	.32	122	.03	2	1.31	.01	.07	1	1
S3 2100	1	9	7	31	.2	13	4	316	1.38	2	5	ND	3	13	1	2	2	16	.17	.137	9	6	.20	211	.07	5	2.15	.02	.07	1	2
S4 00	1	6	6	32	.1	8	3	265	1.13	2	5	ND	4	8	1	2	2	10	.18	.039	18	7	.25	264	.04	4	1.39	.01	.09	1	2
S4 50	1	8	9	45	.2	12	4	177	1.30	2	7	ND	3	11	1	2	2	13	.16	.109	11	7	.23	277	.05	7	1.88	.01	.08	1	5
S4 100	1	6	6	28	.2	9	4	100	1.26	2	7	ND	6	9	1	2	2	10	.15	.030	20	7	.28	170	.04	4	1.50	.01	.11	1	1
S4 150	1	6	4	24	.1	7	3	126	1.16	2	5	ND	5	8	1	2	2	9	.13	.021	19	7	.23	187	.04	6	1.31	.01	.12	1	3
S4 200	1	12	6	17	.2	9	5	72	1.45	2	6	ND	9	5	1	2	2	10	.13	.019	33	8	.36	118	.02	5	1.04	.01	.17	1	24
S4 250	1	46	9	23	.2	16	14	306	2.87	3	8	ND	10	8	1	2	2	14	.71	.044	32	10	.64	226	.02	9	1.75	.01	.27	1	1
S4 300	1	143	12	43	.1	17	7	339	2.96	2	5	ND	4	11	1	2	2	15	.52	.034	17	11	.43	239	.06	8	2.36	.01	.20	1	10
STD C/AU-S	18	59	40	132	6.8	68	31	949	4.10	38	22	6	38	48	18	14	17	58	.48	.091	39	55	.89	174	.06	33	1.98	.06	.13	12	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
S4 350	1	7	7	21	.2	8	4	107	1.18	2	5	ND	4	7	1	2	2	9	.14	.013	18	7	.23	101	.03	8	1.05	.01	.08	1	1
S4 400	1	6	4	23	.2	6	3	89	1.06	2	5	ND	4	7	1	2	2	8	.12	.017	18	6	.23	104	.03	4	.89	.01	.07	1	7
S4 450	1	7	9	42	.1	9	4	237	1.27	2	5	ND	2	10	1	2	2	10	.21	.038	15	7	.27	213	.04	7	1.46	.01	.09	1	1
S4 500	1	10	9	22	.1	11	6	240	1.29	2	5	ND	3	10	1	2	2	10	.38	.024	14	6	.23	172	.03	13	1.16	.01	.11	1	11
S4 550	1	8	8	40	.1	13	6	108	1.62	2	5	ND	3	11	1	2	2	12	.18	.039	11	9	.27	256	.05	6	2.06	.01	.09	1	1
S4 600	1	8	7	27	.1	9	6	262	1.35	3	5	ND	2	10	1	2	2	10	.19	.015	12	7	.22	160	.04	8	1.17	.01	.08	1	1
S4 650	1	10	8	23	.2	10	5	125	1.72	2	5	ND	3	11	1	2	2	14	.14	.022	14	8	.27	190	.05	7	1.55	.01	.06	1	1
S4 700	1	12	12	38	.1	12	5	182	1.41	2	5	ND	2	17	1	2	2	15	.19	.107	9	7	.19	324	.07	3	2.33	.02	.06	1	1
S4 750	1	8	8	39	.1	11	4	381	1.37	2	5	ND	2	14	1	2	2	13	.18	.068	10	8	.22	297	.05	7	1.90	.02	.08	1	1
S4 800	1	13	10	38	.2	13	5	227	1.45	2	5	ND	3	14	1	2	2	16	.16	.093	7	8	.18	304	.08	4	2.58	.02	.11	1	15
S4 850	1	8	8	40	.1	10	6	177	1.65	2	5	ND	2	14	1	2	3	11	.25	.033	9	8	.25	215	.06	8	2.06	.02	.14	1	10
S4 900	1	13	9	45	.2	13	10	285	1.42	2	5	ND	2	18	1	2	2	13	.38	.054	7	7	.26	280	.05	9	1.67	.02	.11	1	18
S4 950	1	9	8	48	.1	11	4	251	1.20	2	5	ND	2	15	1	2	2	13	.18	.129	8	7	.18	276	.06	8	1.88	.02	.08	1	8
S4 1000	1	11	9	42	.1	12	5	375	1.33	2	5	ND	2	15	1	2	2	11	.21	.214	10	7	.21	391	.05	9	1.89	.02	.10	1	1
S4 1050	1	8	9	39	.1	11	5	316	1.37	2	5	ND	3	11	1	2	2	12	.16	.053	14	9	.26	258	.05	9	1.79	.01	.07	1	5
S4 1100	1	7	7	38	.2	11	4	404	1.28	2	5	ND	2	11	1	2	2	14	.17	.105	8	7	.17	264	.06	3	1.90	.01	.06	1	1
S4 1150	1	6	6	39	.1	9	4	225	1.07	2	5	ND	3	8	1	2	2	11	.15	.120	14	9	.23	267	.04	8	1.32	.01	.07	1	1
S4 1200	1	13	9	38	.1	13	5	451	1.38	4	5	ND	1	18	1	2	5	14	.22	.184	8	8	.17	350	.06	7	2.04	.02	.07	1	1
S4 1250	1	10	5	26	.1	8	4	115	1.19	3	5	ND	4	8	1	3	2	9	.16	.018	14	8	.24	157	.03	6	1.07	.01	.07	1	1
S4 1300	1	18	6	29	.1	10	6	305	1.58	2	5	ND	4	9	1	3	2	12	.23	.017	16	9	.27	180	.04	17	1.34	.01	.14	1	13
S4 1350	1	9	5	25	.1	10	6	176	1.69	2	5	ND	3	9	1	2	2	11	.25	.015	13	8	.23	208	.05	6	1.51	.01	.10	1	2
S4 1400	1	6	5	23	.1	10	5	308	1.27	2	5	ND	2	12	1	3	2	11	.23	.019	10	7	.17	240	.05	9	1.60	.01	.11	1	12
S5 50	1	9	10	51	.1	14	5	512	1.45	3	5	ND	2	13	1	2	2	15	.18	.176	9	11	.23	413	.06	9	2.03	.02	.08	1	1
S5 100	1	8	9	39	.1	13	4	201	1.34	3	5	ND	2	11	1	2	2	13	.21	.138	10	8	.26	413	.06	7	1.83	.01	.07	1	1
S5 150	1	6	8	42	.2	12	3	189	1.25	2	5	ND	4	13	1	2	3	12	.17	.082	11	8	.27	391	.05	5	1.68	.01	.09	1	1
S5 200	1	5	6	34	.2	11	4	96	1.33	2	5	ND	6	8	1	2	2	10	.14	.060	19	8	.28	201	.04	6	1.70	.01	.10	1	9
S5 250	1	9	5	35	.1	12	4	138	1.41	2	5	ND	5	8	1	2	2	12	.19	.017	17	10	.31	149	.04	5	1.19	.01	.12	1	5
S5 300	1	11	7	27	.1	12	5	104	1.48	2	5	ND	5	7	1	2	2	10	.19	.031	17	9	.38	125	.03	10	1.08	.01	.09	1	3
S5 350	1	12	7	41	.2	9	4	212	1.18	3	5	ND	3	17	1	2	2	13	.24	.091	6	6	.18	238	.07	9	1.86	.02	.10	1	9
S5 400	1	85	10	43	.1	16	8	105	1.93	2	5	ND	4	15	1	2	2	16	.24	.028	14	9	.35	353	.07	6	2.56	.02	.09	1	1
S5 450	1	11	13	39	.3	19	16	239	2.04	2	6	ND	4	15	1	2	2	17	.26	.019	14	9	.32	747	.06	9	2.47	.02	.08	1	1
S5 500	1	7	8	68	.2	11	4	620	1.40	2	5	ND	3	24	1	2	3	14	.54	.094	9	7	.20	486	.07	12	2.08	.02	.15	1	1
S5 550	1	28	10	22	.2	25	11	100	3.42	2	5	ND	6	11	1	2	5	18	.25	.019	17	10	.29	245	.06	5	2.10	.01	.11	1	2
S5 600	1	71	8	40	.3	18	4	261	1.80	2	9	ND	4	16	1	2	4	16	.34	.050	10	8	.25	182	.06	9	1.75	.02	.12	1	7
S5 650	1	110	9	35	.1	25	10	302	2.92	2	5	ND	3	13	1	2	2	14	.91	.033	13	10	.68	479	.06	10	2.36	.01	.19	1	4
S5 700	1	27	10	23	.3	16	16	493	3.08	2	8	ND	5	14	1	2	2	17	1.83	.030	13	10	1.11	374	.06	8	2.26	.01	.12	1	24
STD C/AU-S	18	57	41	132	6.6	67	30	939	4.07	37	22	6	38	48	17	14	21	58	.48	.093	38	55	.89	173	.06	36	1.96	.06	.13	12	51

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
S5 750	1	69	9	54	.1	15	14	595	1.47	2	5	ND	1	19	1	2	2	12	.81	.259	10	8	.30	1869	.04	16	1.50	.02	.19	1	9
S5 800	1	10	8	56	.1	10	6	170	1.38	2	5	ND	2	17	1	2	2	12	.37	.050	6	7	.21	361	.06	14	1.98	.03	.12	1	50
S5 850	1	7	7	33	.1	9	8	271	2.13	2	5	ND	2	13	1	2	2	11	.52	.031	9	8	.34	660	.05	13	1.94	.02	.19	1	8
S5 900	1	7	9	35	.2	7	5	546	3.44	2	5	ND	4	12	1	2	2	15	.47	.036	11	10	.40	343	.06	11	2.16	.01	.27	1	103
S5 950	1	9	13	95	.1	8	4	541	1.81	2	5	ND	2	20	1	2	2	16	.37	.050	8	9	.29	649	.08	10	2.23	.02	.17	1	16
S5 1000	1	9	4	59	.1	7	4	254	1.63	2	5	ND	2	17	1	2	2	14	.33	.053	6	8	.29	408	.06	11	1.92	.02	.12	1	98
S5 1050	1	7	8	83	.2	6	3	542	1.20	4	5	ND	1	31	1	2	2	13	.44	.125	5	7	.20	499	.05	9	1.27	.02	.15	1	13
S5 1100	1	15	12	36	.3	11	6	544	2.56	2	5	ND	4	22	1	2	2	19	.41	.095	11	12	.42	441	.05	6	2.10	.04	.18	1	71
S5 1150	1	8	9	53	.2	12	5	315	1.56	2	5	ND	3	24	1	2	2	17	.38	.232	7	8	.22	526	.09	8	2.75	.03	.09	1	15
S5 1200	1	6	9	99	.1	6	4	474	2.08	2	5	ND	2	19	1	2	2	14	.47	.048	7	10	.32	303	.06	13	1.99	.02	.16	1	4
S5 1250	1	7	13	51	.1	8	6	504	3.40	2	5	ND	3	12	1	2	2	17	.43	.042	10	13	.42	216	.06	10	2.16	.01	.21	1	12
S5 1300	1	6	13	55	.2	8	6	560	4.32	2	5	ND	5	15	1	2	2	16	1.13	.064	14	15	.72	251	.06	15	2.22	.01	.32	1	108
S5 1350	1	6	8	29	.1	7	4	250	1.45	2	5	ND	5	8	1	2	5	12	.16	.013	20	9	.35	134	.04	6	1.10	.01	.12	1	28
S5 1400	1	8	4	25	.1	6	4	135	1.32	3	5	ND	4	7	1	2	2	10	.11	.014	21	8	.28	149	.04	3	1.02	.01	.11	1	25
S6 00	1	7	4	28	.2	11	4	138	1.75	2	5	ND	6	7	1	2	2	11	.19	.015	26	11	.55	105	.02	2	1.06	.01	.11	1	14
S6 50	1	6	8	25	.1	8	4	86	1.53	2	5	ND	5	8	1	2	2	11	.10	.014	24	9	.43	76	.03	4	1.10	.01	.10	1	8
S6 100	1	5	4	22	.1	9	5	96	1.54	2	5	ND	5	7	1	2	2	11	.09	.023	26	11	.43	94	.03	4	1.00	.01	.07	1	8
S6 150	1	7	7	32	.1	9	5	196	1.55	2	5	ND	4	10	1	2	2	12	.15	.024	19	9	.36	134	.04	2	1.47	.01	.11	1	14
S6 200	1	5	7	37	.1	6	3	112	1.42	2	5	ND	5	10	1	2	2	10	.19	.019	23	9	.33	118	.04	4	1.14	.01	.10	1	20
S6 250	1	6	5	32	.2	8	4	99	1.58	2	5	ND	5	10	1	2	2	12	.17	.017	22	9	.36	98	.04	3	1.27	.01	.12	1	32
S6 300	1	6	4	37	.1	8	3	108	1.32	3	5	ND	4	9	1	2	2	10	.14	.024	17	9	.31	117	.04	5	1.18	.01	.09	1	34
S6 350	1	6	5	40	.1	6	3	183	1.22	2	5	ND	4	10	1	2	2	9	.12	.020	20	8	.31	122	.04	3	1.12	.01	.10	1	12
S6 400	1	16	5	30	.1	11	7	236	1.78	2	5	ND	4	37	1	2	2	11	4.85	.090	20	10	.76	118	.02	8	1.24	.01	.14	1	7
S6 450	1	11	10	24	.2	11	8	91	2.20	2	5	ND	9	7	1	2	2	18	.17	.012	34	12	.63	95	.03	7	1.44	.01	.14	1	1
S6 500	1	8	8	26	.2	9	5	97	1.80	2	5	ND	7	7	1	2	2	12	.12	.020	30	11	.49	62	.03	3	1.17	.01	.16	1	15
S6 550	1	6	6	23	.1	7	4	88	1.50	2	5	ND	6	9	1	2	2	11	.09	.017	24	9	.38	95	.04	2	1.20	.01	.07	1	5
S6 600	1	5	7	21	.1	8	4	111	1.50	2	5	ND	5	7	1	2	2	11	.12	.011	25	9	.38	90	.03	2	1.21	.01	.07	1	13
S6 650	1	4	5	21	.1	6	3	76	1.46	2	5	ND	6	6	1	2	4	10	.10	.009	30	9	.41	59	.03	9	.93	.01	.09	1	3
S6 700	1	15	7	31	.1	13	7	219	2.13	2	5	ND	8	11	1	2	2	13	.91	.037	31	12	.64	86	.02	3	1.29	.01	.11	1	1
S6 750	1	7	6	24	.1	7	5	134	1.56	2	5	ND	6	7	1	2	2	11	.14	.013	28	10	.42	83	.03	4	1.02	.01	.09	1	2
S7 00	1	12	10	32	.1	13	8	350	2.18	2	5	ND	8	8	1	2	2	15	.50	.026	29	14	.70	139	.02	14	1.54	.01	.23	1	4
S7 50	1	8	7	37	.1	9	6	193	2.00	2	5	ND	7	9	1	2	2	12	.22	.019	30	12	.57	119	.03	5	1.45	.01	.13	1	7
S7 100	1	9	8	31	.3	12	6	128	2.05	2	6	ND	7	10	1	2	2	14	.23	.023	27	11	.55	102	.04	5	1.64	.01	.15	1	1
S7 150	1	10	7	29	.2	13	8	396	2.28	2	5	ND	9	8	1	2	3	14	.22	.031	31	12	.64	101	.03	5	1.40	.01	.17	1	9
S7 200	1	1	3	49	.1	5	3	88	.93	2	5	ND	5	6	1	2	3	8	.11	.024	23	7	.34	99	.02	2	.71	.01	.07	1	4
S7 250	1	4	7	34	.2	9	5	102	1.64	2	5	ND	8	7	1	2	2	10	.20	.057	27	12	.58	85	.02	5	1.03	.01	.14	1	6
STD C/AU-S	18	58	36	132	6.7	65	31	1021	4.01	42	17	7	37	47	18	15	22	57	.48	.092	38	55	.88	175	.06	32	1.95	.06	.14	12	52

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
S7 300	1	11	9	29	.1	11	5	228	1.45	3	5	ND	5	36	1	2	2	10	4.89	.045	18	8	1.08	76	.01	5	.96	.01	.10	1	1
S7 350	1	9	7	32	.1	10	5	124	1.43	3	5	ND	5	8	1	2	3	11	.26	.027	20	8	.40	106	.03	8	1.20	.01	.09	1	1
S7 400	1	6	8	49	.1	13	4	136	1.28	3	5	ND	2	12	1	2	2	11	.19	.101	12	7	.26	177	.05	6	1.65	.01	.08	1	1
S7 450	1	22	10	31	.2	16	8	211	2.22	7	5	ND	9	8	1	2	2	15	.62	.035	28	14	.85	156	.01	5	1.73	.01	.18	1	1
S7 500	1	5	4	21	.1	8	4	56	1.28	2	5	ND	5	5	1	2	4	9	.13	.019	23	8	.40	75	.02	4	.85	.01	.10	1	1
S7 550	1	1	2	34	.1	6	3	214	.96	2	5	ND	3	9	1	2	2	7	.15	.024	14	6	.24	140	.03	5	.90	.01	.11	1	1

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GEOCHEMICAL ANALYSIS CERTIFICATE

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: NOV 23 1989 **DATE REPORT MAILED:** Nov 24/89 **SIGNED BY.**.........D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Bapty Research Limited File # 89-4855

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
B 56253	1	898	2	8	.1	3	1	589	1.00	3	5	ND	2	47	1	2	2	5	15.59	.011	3	4	8.17	62	.01	5	.07	.01	.06	1	5
B 56254	1	11	2	8	.1	10	13	616	1.57	5	5	ND	2	51	1	2	2	4	15.38	.015	3	3	7.71	64	.01	4	.04	.01	.03	1	5
B 56255	1	6767	2	19	.6	5	1	528	1.47	6	5	ND	3	49	1	2	2	5	13.64	.015	3	4	7.17	769	.01	6	.10	.01	.07	1	8
B 56256	1	21	4	5	.1	6	6	634	1.21	2	5	ND	3	50	1	2	2	8	14.98	.016	4	5	7.24	48	.01	21	.13	.01	.08	1	4
B 56257	1	39	2	1	.1	3	1	52	.41	2	5	ND	2	27	1	2	2	5	1.81	.566	36	1	.28	60	.01	8	.80	.01	.42	1	2
B 56258	1	6	2	13	.1	21	11	748	4.67	4	5	ND	1	38	1	2	2	35	2.72	.199	7	11	1.95	73	.05	6	1.46	.01	.40	1	2
B 56259	1	20	2	11	.1	7	8	752	5.14	8	5	ND	2	27	1	2	2	11	2.96	.436	29	2	.99	209	.07	6	1.55	.01	.57	1	4
B 56260	3	11	10	12	.1	11	7	659	4.92	5	5	ND	1	163	1	2	2	45	1.33	.011	2	31	.61	2247	.01	2	.25	.01	.03	2	3
B 56261	1	6	2	4	.1	9	3	154	.98	2	5	ND	4	9	1	2	2	6	.69	.041	22	9	.62	396	.01	13	.65	.01	.22	1	5
B 56262	1	3	4	9	.1	6	5	1137	1.70	2	5	ND	1	94	1	2	2	7	11.60	.016	3	6	6.13	1937	.01	13	.35	.01	.05	1	4
B 56263	1	6	2	5	.1	9	4	206	1.51	2	5	ND	10	3	1	2	2	5	.23	.053	25	6	.24	105	.01	6	.62	.01	.29	1	1
B 56264	1	7	2	6	.1	28	13	592	2.83	4	5	ND	4	40	1	2	2	7	8.57	.048	8	7	4.41	241	.01	8	.29	.01	.19	1	2
B 56265	1	20	4	6	.1	3	1	923	3.01	5	5	ND	4	24	1	2	2	4	15.90	.013	6	3	6.64	79	.01	6	.09	.01	.05	1	2
GR89-16	2	36	2	7	.1	12	13	199	3.07	2	5	ND	1	8	1	2	2	4	1.00	.020	3	7	.66	170	.01	17	.32	.01	.13	1	4
GR89-17	1	2823	2	11	.5	18	6	565	1.64	12	5	ND	3	47	1	2	2	8	7.70	.018	3	5	4.04	43	.01	3	.38	.01	.09	1	2
STD C/AU-R	18	62	43	133	6.7	70	31	1043	4.07	42	20	8	37	47	18	14	20	58	.51	.097	38	56	.91	176	.06	32	1.94	.06	.13	13	530

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Bapty

GEOCHEMICAL ANALYSIS CERTIFICATE

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- SAMPLE TYPE: ROCK AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

DATE RECEIVED: NOV 30 1989 **DATE REPORT MAILED:** Dec 4/89. **SIGNED BY**..C.Leong......D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Bapty Research Limited File # 89-4916

SAMPLE#	Mo PPM	Cu PPM	Pb PPM	Zn PPM	Ag PPM	Ni PPM	Co PPM	Mn PPM	Fe %	As PPM	U PPM	Au PPM	Th PPM	Sr PPM	Cd PPM	Sb PPM	Bi PPM	V PPM	Ca %	P %	La PPM	Cr PPM	Mg %	Ba PPM	Ti %	B PPM	Al %	Na %	K %	W PPM	Au* PPB
GR89-18	2	4	2	1	.1	6	1	141	.27	2	5	ND	1	1	1	2	2	1	.50	.002	2	5	.07	37	.01	4	.05	.01	.01	1	4
GR89-19	2	5	4	2	.1	7	1	149	.68	2	5	ND	1	1	1	2	2	2	.32	.001	2	6	.40	40	.01	3	.39	.01	.01	1	3
GR89-20	2	3	5	3	.1	9	5	357	1.72	2	5	ND	1	20	1	2	2	6	.02	.007	2	10	.85	2058	.01	4	.87	.01	.01	1	1
GR89-21	1	257	3	7	.1	7	3	486	.99	2	5	ND	3	48	1	2	2	6	10.23	.027	5	5	5.07	1818	.01	8	.21	.01	.08	1	4
GR89-22	1	1478	2	8	.3	12	3	457	1.17	5	5	ND	5	41	1	2	2	7	8.04	.023	5	5	4.28	1723	.01	5	.35	.01	.08	1	4
GR89-23	1	43	2	3	.3	7	6	603	1.05	7	5	ND	3	50	1	2	2	7	12.86	.019	4	4	6.41	1754	.01	7	.15	.01	.06	1	1
GR89-24	1	495	4	3	.3	9	7	559	1.05	5	5	ND	4	48	1	2	2	8	12.49	.022	4	5	6.32	1804	.01	12	.21	.01	.08	1	1
GR89-25	1	368	2	2	.1	5	4	578	1.04	4	5	ND	3	53	1	2	2	9	14.50	.012	3	3	7.43	1596	.01	15	.17	.01	.05	1	1
GR89-26	1	932	5	4	.4	9	1	566	1.19	12	7	ND	4	46	1	2	2	5	13.76	.018	4	3	6.83	878	.01	9	.11	.01	.07	1	2
B 56401	1	10	4	5	.3	12	3	312	2.09	5	6	ND	8	26	1	2	2	4	2.40	.046	18	5	.50	713	.01	4	.38	.01	.17	1	1
B 56402	2	73	2	4	.4	13	29	865	2.83	6	5	ND	4	96	1	2	2	4	8.27	.016	3	3	3.74	1793	.01	7	.10	.01	.06	1	1
B 56403	1	34	2	3	.4	13	7	314	1.48	7	10	ND	7	47	1	2	2	6	8.05	.032	7	4	4.00	166	.01	26	.21	.01	.11	1	3
B 56404	1	171	4	5	.7	4	2	418	.91	38	5	ND	8	72	1	10	2	4	10.18	.031	16	2	4.92	392	.01	27	.17	.01	.08	1	3
B 56266	1	11	3	3	.2	9	15	726	1.73	4	5	ND	5	139	1	2	2	4	10.50	.032	5	3	4.80	1550	.01	22	.15	.01	.08	1	2
B 56267	1	10	10	2	.4	3	1	109	.40	12	5	ND	3	109	1	2	2	1	27.58	.014	12	1	.69	142	.01	15	.06	.01	.03	1	1
STD C/AU-R	18	58	39	132	7.1	67	30	990	4.05	41	19	8	38	48	18	15	18	58	.48	.090	38	55	.88	176	.06	32	1.97	.06	.13	13	520

APPENDIX 2

INDUCED POLARIZATION SURVEY

INDUCED POLARIZATION SURVEY

BY
SJ GEOPHYSICS LTD

AND

MAGNETOMETER SURVEY

BY
BAPTY RESEARCH LIMITED

ON THE

GILL PROPERTY

FOR

SOUTH KOOTENAY GOLDFIELD INC.

FORT STEELE M.D.   N.T.S. 82G

February 1990

Report By
Syd J. Visser
SJ GEOPHYSICS LTD.

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INTRODUCTION

A induced polarization survey was completed during the period of November 21 to December 19, 1989 and January 11, to January 12, 1990 on the Gill property by SJ Geophysics Ltd., at the request of Mr. Mike Bapty, Bapty Research Limited on behalf of South Kootenay Goldfields Inc. A magnetometer survey was completed on part of the survey area by Bapty Research Limited. The survey grid is located on the Gill property approximately 50 Km southeast of Cranbrook, on the west side of Gold Creek in the Fort Steele Mining mining district of B.C. (N.T.S. 82G).

The purpose of the survey was to search for sulphide concentrations or anomalous structures which may contain precious metals.

FIELD WORK AND DISCUSSION OF FIELD PARAMETERS

The induced polarization survey was completed during November 21, 1989 to December 19, 1989 and January 11 and 12, 1990. The field crew which consisted of one geophysicist and one technician and 3 helpers, commuted daily from accommodations in Cranbrook to the survey area. Nine lines were surveyed for a total of approximately 13 kilometers. A pole-dipole array with an "a" spacing of 50M and a "N" of 1 to 6 was used for the survey.

The equipment used was a Mk-2, 7.5 KW time domain transmitter, with a cycle time of 2 sec. on and 2 sec off, and a Mk-4 time domain receiver. The delay time of the receiver was set at 160 msec with 10 integrating windows with a width of 130 msec each, for a total chargeability window of 650 msec. The total chargeability was recorded and plotted by computer for interpretation purposes.

The mild weather conditions along with the snow and rain during the early part of the survey slowed the I.P. survey considerably .

The magnetic data collected by Bapty Research Limited personal was given to SJ Geophysics Ltd. for plotting and interpretation.

DATA PRESENTATION

The chargeability and the apparent resistivity were plotted as pseudosections. The average apparent resistivities and chargeabilities (triangular filter), calculated from averaging the values at 45 deg to the plotting point, as seen on the pseudosections, were plotted as profiles. The magnetic data and the relative topography calculated from the recorded slopes was also plotted as profiles. Attempts were made to contour the filtered I.P. data, magnetic data and topography, but it was not completed because of the wide line spacing in part of the grid and poor control over the relative line location. The following is a list of the enclosed plots (Appendix II):

Sections L1000N, L1500N, L2000N, L2200N, L2400N, L2600N, L2800N, L3400N, L4100N & Model L2200N	Induced Polarization Pseudosections (Lines 1000N, 1500N, 2000N, 2200N, 2400N, 2600N, 2800N, 3400N, 4100N & Model Line 2200N
Plate G1A	Magnetometer Survey Profiles & Compilation
Plate G2A	Relative Topography Profiles
Plate G3A	Induced Polarization Survey Filtered Chargeability
Plate G3B	Induced Polarization Survey Relative Resistivity
Plate G4	Induced Polarization Survey Compilation Map

INTERPRETATION

The interpretation of the I.P. data is shown on both the pseudosections of each line and the compilation map (Plate G4). The compilation of the magnetic data is shown with the magnetic profiles on Plate G2A. The I.P. data will be discussed separately for each line and then combined with the discussion of the magnetic data and the topography.

LINE 1000N

The I.P. data on line 1000N indicates a medium chargeability anomaly associated with a resistivity low centered at approximately 975E. This weak anomaly appears to be flanked by a stronger deep anomaly to the east at the contact of a resistivity high.

A weak chargeability anomaly at a resistivity contact is centered at approximately 1475N.

LINE 1500N

The deep long weak chargeability anomaly on the western end of line 1500N is likely lithological and appears to be due to a fairly flat lying chargeable layer at depth. The stronger shallow anomaly to the west of the above zone and centered at approximately 780W is associated with a resistivity low near a resistivity contact.

The remainder very weak anomalies located at approximately 1450W and 1750W are also centered on resistivity contact zones.

The last readings on the east end of this line indicates a possible anomaly. The line would have to be extended in this direction to confirm this anomaly.

LINE 2000N

Line 2000N has a strong shallow chargeability anomaly centered at approximately 1125E. This anomaly which is one of the best anomalies in the survey area, appears to be associated with the contact between a narrow low resistivity zone and a high resistivity zone. The weaker and possiblė deeper chargeability anomaly centered at approximately 1400N appears to correspond to a similar structure. The resistivity high between these two anomalies is also magnetic suggesting that these anomalies are separated by a magnetic possibly volcanic rock unit or a magnetic dyke.

The weak anomalies on the east end of the line and the anomaly centered at approximately 1750E correlate well with resistivity lows and may be lithological.

LINE 2200N

The chargeability anomalies on line 2200N are similar to line 2000N but appear to be weaker. The anomalies on the western end of the line are associated with resistivity lows. The medium chargeability anomalies on the eastern end of the line appears to be associated with a resistivity high. All of these anomalies may be lithological.

LINE 2400N

A computer generated model of line 2400N using vertical resistivity and changeability boundaries was used to aid interpretation and is plotted on a pseudosections model line 2400N.

The data indicates a good chargeability anomaly centered at approximately 1525E with a corresponding resistivity low. It is not certain if this anomaly is made up of two separate anomalies or is one wide anomaly. This anomaly correlates well with the eastern part of the magnetic zone and therefore could possible contain pyrrhotite or magnetite.

The weak I.P. anomaly centered at approximately 2000E is also associated with a low resistivity zone and a weak magnetic anomaly.

The remaining anomalies on this line are weak and probable lithological.

LINE 2600N

The anomaly centered at approximately 1500E is very similar to and is probably an extension of the anomaly at 1525E on line 2400N.

LINE 2800N

The very weak anomaly located at 1600E may also be an extension of the anomalies on line 2400E and 2600E but it is much weaker and is more likely due to the contact between the low resistivity magnetic zone and the higher resistivity rocks. The remaining weak anomalies on this line are likely lithological.

LINE 3400N

There is one weak anomaly on line 3400N centered at approximately 1300E. It is not clear if this anomaly is a single wide anomaly or two closely spaced anomalies (a 25M dipole would have to be used to separate these anomalies). This anomaly has a corresponding resistivity low.

There is also a weak magnetic anomaly located in this area suggesting a concentration of pyrrhotite or magnetite.

LINE 4100N

There are no well defined chargeability anomalies on this line. The chargeability does appear to increase towards the eastern end of this line but the line does not extend far enough east to confirm if it is an anomaly in this direction. The resistively also decreases in this region.

ANOMALIES CLASSIFIED IN ORDER OF PRIORITY

1) Line 2000N @ 1125E
2) Line 2400N @ 1525E
3) Line 1000N @ 1150E and 950E

4) Line 2000N @ 1400E
5) Line 3400N @ 1250E and 1350E
6) Line 1500N @ 1775E
7) Line 2000N @ 1800E
8) Line 2400N @ 1675E

MAGNETICS

The magnetic data indicates a wide highly variable magnetic zone, centered at approximately 1400E, striking across the length of the grid. This zone is likely a layered volcanic sequence or interbeded magnetic volcanics and nonmagnetic sedimentary layers which could also account for the variable resistivity and chargeability in this region. The eastern part of this anomaly appears to have a low resistivity and an associated chargeability anomaly which is most dominant on line 2400N.

The western side of the wide magnetic anomaly has a higher resistivity. The exception to this appears to be the eastern and western side of the magnetic highs located at approximately 1225E on lines 2000N and 2200N which have corresponding resistivity lows and chargeability highs.

The magnetic anomaly and I.P. anomalies on line 3400N may be the northerly extension of the eastern side of the above magnetic anomaly.

The weak narrow magnetic anomaly located on the eastern side of the grid is likely a magnetic dyke.

TOPOGRAPHY

It is interesting to note that the majority of the I.P. anomalies and the resistivity lows correlate with a low or relatively flat part of the topography and that the high resistivity zones correlate with peaks in the topography.

The change in topography does have an effect on the accuracy of the resistivity and chargeability. estimating the correcting for topography is a difficult process and was not attempted for this report.

RECOMMENDATIONS

It is recommended to do follow-up work on the I.P. anomalies on the eastern side of the wide magnetic zone especially on line 2400N and line 3400N.

It is also recommended to do follow-up work on the anomalies on the eastern side of the wide magnetic anomaly especially on line 2000N.

Additional lines should be surveyed between lines 1000N and 2000N and between 2800N and 4100N to locate the extension and end points of the anomalies.

CONCLUSION

A number of I.P. anomalies were located in the survey area mainly associated with resistivity lows or resistivity contact zones. The most interesting anomalies were associated with a magnetic anomaly and a topography low. These anomalies should be investigated further by detail geological work and drilling.

Syd Visser, B.Sc., F.G.A.C.

Geophysicist
SJ Geophysics Ltd.

STATEMENT OF QUALIFICATIONS

I, Syd J. Visser, of 8081-112th Street, Delta, British Columbia, hereby certify:

That I am a Consulting Geophysicist of S.J.V. Consultants Ltd., located at 8081-112th Street, Delta, B.C.

1) I am a graduate from the University of British Columbia, 1981, where I obtained a B.Sc. (Hon.) Degree in Geology and Geophysics.

2) I am a graduate from Haileybury School of Mines, 1971.

3) I have been engaged in mining exploration since 1968.

4) I am a Fellow of the Geological Association of Canada.

5) This report is compiled from data obtained from a Induced Polarization survey carried out by S.J.V. Consultants Ltd..

Syd J. Visser, B.Sc., F.G.A.C.
Geophysicist

APPENDIX 3

DDH G-89-1 DRILL LOGS

DRILL HOLE RECORD: Gold Creek HOLE NO.: G-89-1

COMMENCED: December 13, 1989	DISTRICT: Fort Steele	COLLAR DIP: -45°	TESTS @:
COMPLETED: December 15, 1989	PROPERTY: Gold Creek	BEARING: -225°	
LOGGED BY: Jim Ryley	LOCATION: Gold Mtn. Face Rd.	LENGTH: 31.40 m	
DATE LOGGED: December 15, 1989	CO-ORD.: 5442620N, 621760E	CORE SIZE: NQ	
	ELEV.: 1010 m	% RECOVERY:	ppm except Au ppb

FOOTAGE FROM TO	DESCRIPTION	ANALYSIS Au	Ba	Cu
0.0-10.67m	COLLAR No recovery in overburden.			
10.67-26.25m	OVERBURDEN Sub-rounded to rounded pebble to cobble sized fragments and localized sections of competent core 10-20 cm long. Lithology consists of dark-gray chert, light green to brown siltstones and quartzites. Localized 10-20 cm sections of core are chracteristically slightly to moderately altered, thinly bedded quartzites/siltstones occasionally with disseminated manganese and limonite.			
26.25-31.40m	QUARTZITE Light purple sub-well rounded, moderately sorted. Very fine-medium grained quartzite with 1-2% medium grained Jasper. Quartzite is moderately hard-hard. Trace pyrite. Occasionally interbedded with 2-3 cm bands light brown medium coarse grain quartzite, no visible sulphides.			
	Sampling: 39401 11.17-11.27 m 0.10 m	1	21	1
	39402 11.57-11.66 m 0.09 m	1	1659	384
	39403 11.83-11.93 m 0.10 m	1	68	1
	39404 12.39-12.51 m 0.12 m	3	1796	9
	39405 13.41-13.74 m 0.33 m	3	582	2
	39406 15.50-15.71 m 0.21 m	1	1076	16
	39407 17.64-18.00 m 0.36 m	1	596	4
	39408 18.90-19.21 m 0.31 m	1	280	3
	39409 19.21-19.25 m 0.04 m	1	30	3
	39410 22.65-22.82 m 0.17 m	2	508	6
	39411 28.85-29.08 m 0.23 m	1	6	3
	39412 29.08-29.53 m 0.45 m	1	68	1
	39413 29.53-31.40 m 0.87 m	1	46	12
31.40m	END OF HOLE			


TAN 3
TWIN 3
TWIN 2
TAN 4
TWIN 6
TWIN 7
LINK I
TWIN 5
TWIN 8
TWIN 9
TWIN 10
TWIN 11
G58
G57
G56
G55
G54
G53
G52
G51
G50
G49
G48
G46
G45
G44
G43
G47
G42
G41
G40
G39
G38
G37
G67
G68
GR89 18,19
GR89-20
GR89 16,17
GR89 21-25
IP RECON LINE 9
S7-1400
S4-1400
S3-2100
R1-00
S4-00
S5-50
S5-1400
S6-750
S7-00
S3-00
S6-00
R95-4700
IP GRID
L2800N
L2600N
L2400N
L2200N
L2000N
L1500N
L1000N
L1500E
Soil Geochemical Lines
McGILLIVRAY
RANGE
MOUNTAIN
TRENCH
LAKE
GOLD MOUNTAIN
TRAIL
Perce
LEGEND
Location Site Heavy Mineral and Panned Concentrate Samples
Soil Geochemistry Contour Line 50 m Sample Spacings
See Fig. 4 for Au, Ba & Cu Values; See Appendix 1 for Complete Analyses
Rock Geochem Sample Sites See Table 1 for Descriptions; Appendix for Analyses
SCALE 1:20 000
200 0 200 400 600 800 1000 1200 1400
METRES
T.N.
17° 39'
GRID NORTH
MAGNETIC NORTH
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,822
SOUTH KOOTENAY GOLDFIELDS INC.
Gold Creek Project
GOLD 1 & 2 GROUPS
1989 EXPLORATION
BAPTY RESEARCH LTD.
DRAWN: TW
MINING DIV.: FT. STL.
FIGURE 3
N.T.S. 82 G/3W
SCALE: 1:20,000
DATE: MAR. 90
REVISED:

GEOLOGICAL BRANCH
ASSESSMENT REPORT

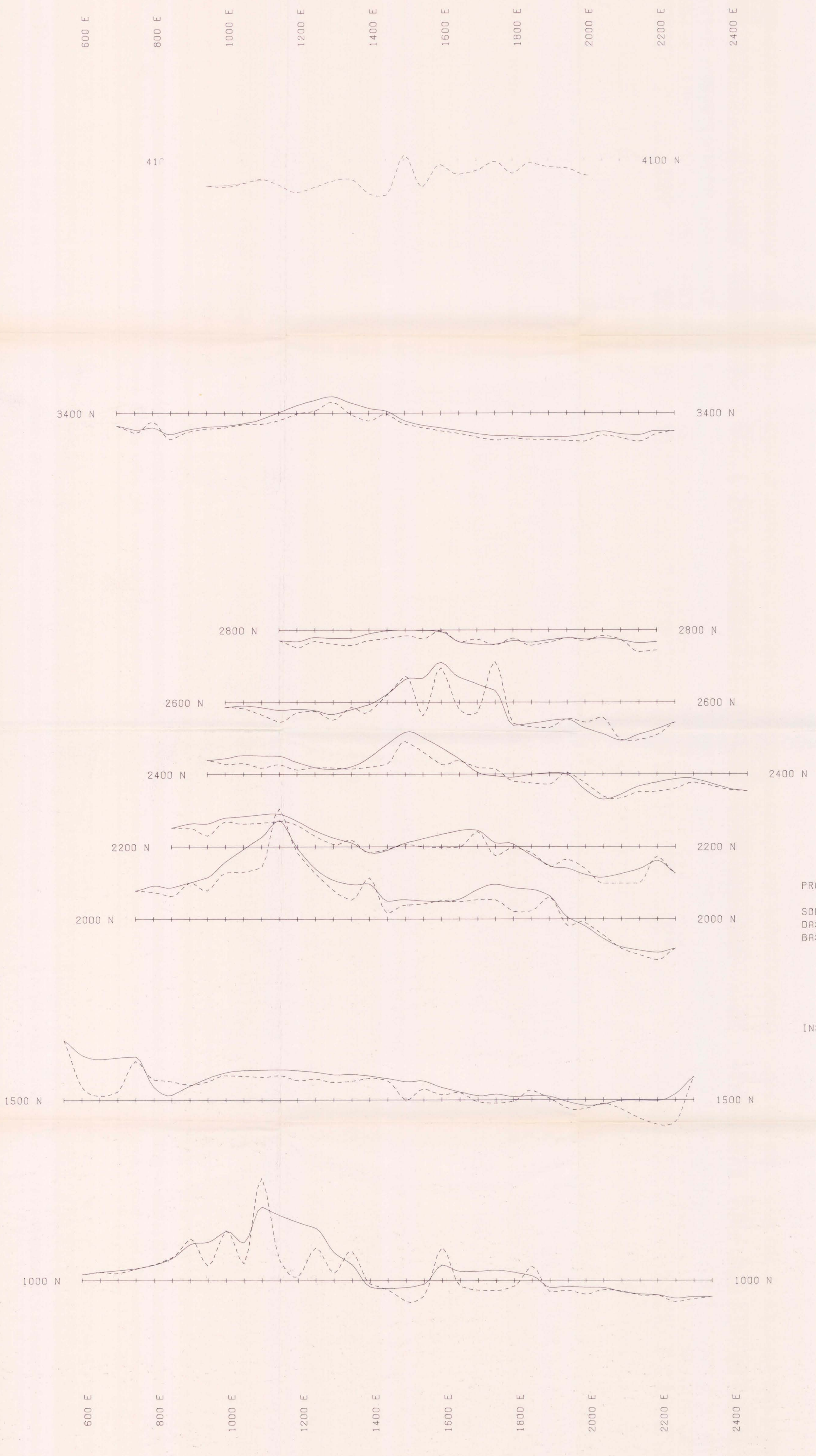
19,822

BAPTY RESEARCH LIMITED / SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY
CLAIM MAP

FIGURE 2

DRAWN BY:	PK/JMM	SCALE:	1:50,000	DATE:	APR. 7, 1989
LAYOUT BY:	JMM				



PROFILES POSITIVE UP

SOLID LINES : TOTAL TRIANGULAR FILTER 1.0 MSEC / CM
DASHED LINES: PARTIAL TRIANGULAR FILTER 1.0 MSEC / CM
BASE VALUE: 4 MSEC

INSTRUMENT USED: HUNTEC MK-2 TRANSMITTER
HUNTEC MK-4 RECIEVER

BAPTY RESEARCH LIMITED

SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY

INDUCED POLARIZATION SURVEY

FILTERED CHAGEABILITY

FORT STEELE M.D. N.T.S. 82G

SCALE 1:5000

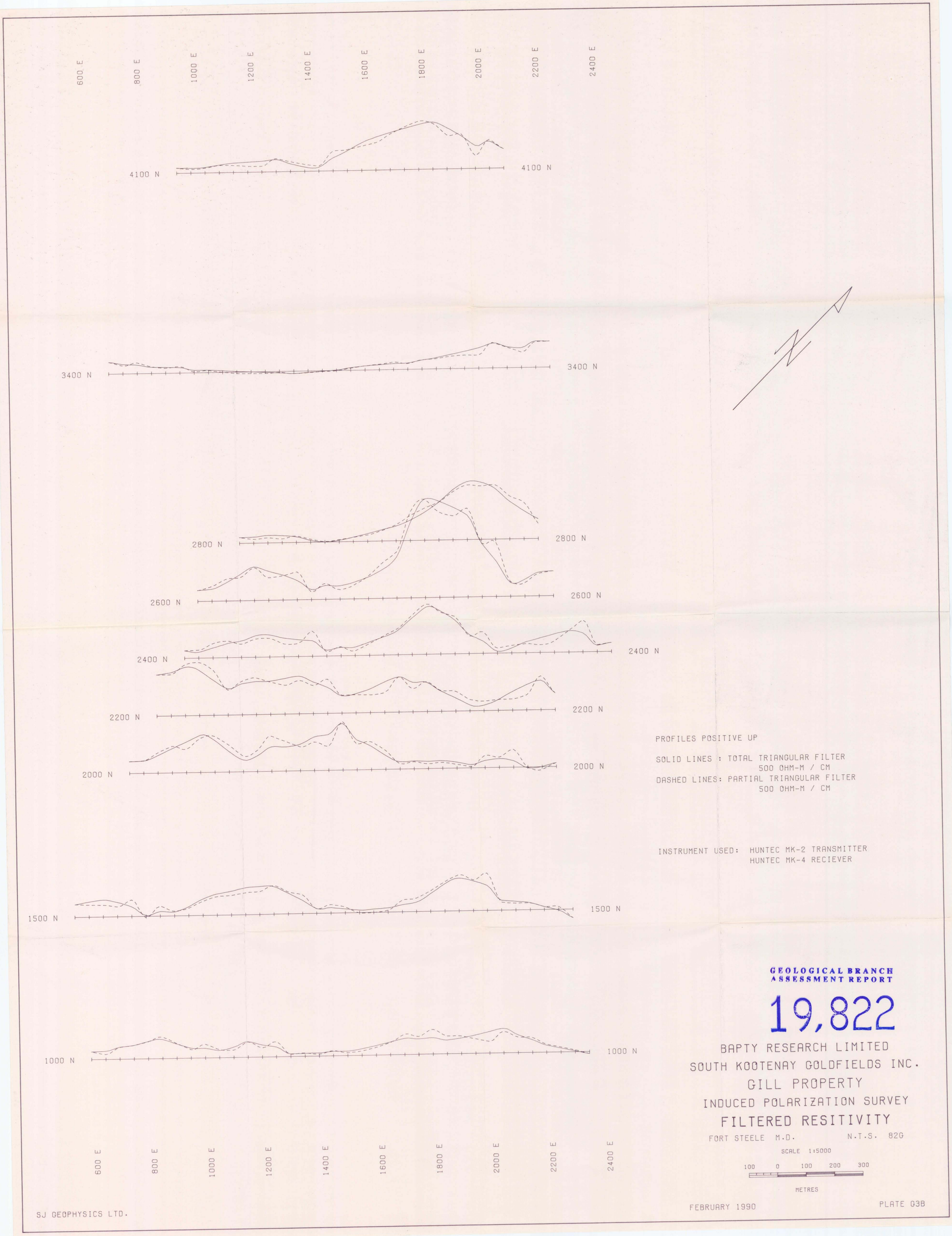
100 0 100 200 300

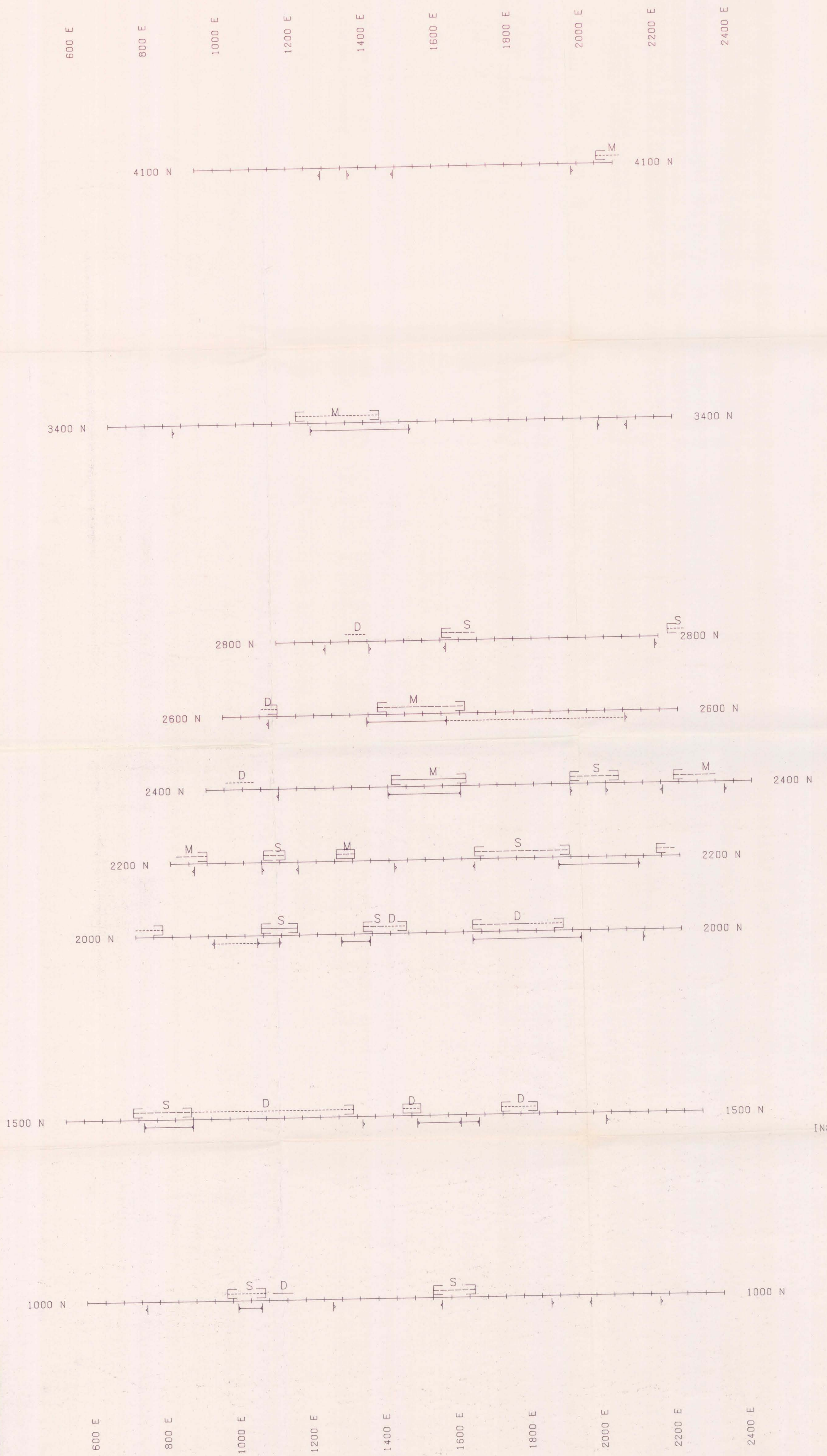
METRES

SJ GEOPHYSICS LTD.

FEBRUARY 1990

PLATE G3A


600 E
800 E
1000 E
1200 E
1400 E
1600 E
1800 E
2000 E
2200 E
2400 E
4100 N
3400 N
2800 N
2600 N
2400 N
2200 N
2000 N
1500 N
1000 N
PROFILES POSITIVE UP
SOLID LINES : TOTAL TRIANGULAR FILTER
500 OHM-M / CM
DASHED LINES: PARTIAL TRIANGULAR FILTER
500 OHM-M / CM
INSTRUMENT USED: HUNTEC MK-2 TRANSMITTER
HUNTEC MK-4 RECIEVER
GEOLOGICAL BRANCH
ASSESSMENT REPORT
19,822
BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.
GILL PROPERTY
INDUCED POLARIZATION SURVEY
FILTERED RESITIVITY
FORT STEELE M.D.
N.T.S. 82G
SCALE 1:5000
100 0 100 200 300
METRES
SJ GEOPHYSICS LTD.
FEBRUARY 1990
PLATE G3B



STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESISTIVITY
INTERMEDIATE RESISTIVITY
LOW APPARENT RESISTIVITY

RESITIVITY CONTACT
POINTING IN DIRECTION
OF INCREASING RESISTIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

INSTRUMENT USED: HUNTEC MK-2 TRANSMITTER
HUNTEC MK-4 RECIEVER

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY

INDUCED POLARIZATION SURVEY

COMPILATION MAP

FORT STEELE M.D. N.T.S. 82G

SCALE 1:5000

100 0 100 200 300

METRES

SJ GEOPHYSICS LTD.

FEBRUARY 1990

PLATE G4

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M
SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1,2,3,4,5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

SJ GEOPHYSICS LTD.

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,822

LINE 1000 N

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY
INDUCED POLARIZATION
PSEUDOSECTIONS

FORT STEELE M.D., B.C. N.T.S. 82 G
JANUARY, 1990 SECTION L 1000N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M
SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1,2,3,4,5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

SJ GEOPHYSICS LTD.

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,822

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.
GILL PROPERTY
INDUCED POLARIZATION
PSEUDOSECTIONS
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JANUARY, 1990 SECTION L 1500N

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ASSESSMENT REPORT

19,822

LINE 2000 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M

SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1.2.3.4.5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

SJ GEOPHYSICS LTD.

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY

INDUCED POLARIZATION

PSEUDOSECTIONS

FORT STEELE M.D., B.C. N.T.S. 82 G

JANUARY, 1990 SECTION L 2000N

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19,822

LINE 2200 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M

SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1,2,3,4,5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

SJ GEOPHYSICS LTD.

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY

INDUCED POLARIZATION

PSEUDOSECTIONS

FORT STEELE M.D., B.C. N.T.S. 82 G

JANUARY, 1990 SECTION L 2200N

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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LINE 2400 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M
SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1.2.3.4.5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

SJ GEOPHYSICS LTD.

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.
GILL PROPERTY
INDUCED POLARIZATION
PSEUDOSECTIONS
FORT STEELE M.D., B.C. N.T.S. 82 G
JANUARY, 1990 SECTION L 2400N

WEST

EAST

GEOLOGICAL BRANCH
ASSESSMENT REPORT

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MODEL LINE 2400 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M

SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1,2,3, & 4

CURRENT WEST OF POTENTIAL

COMPUTER GENERATED MODEL
ASSUMING VERTICAL CONTACTS
CHARGEABILITY AS INDICATED ON TOP OF CENTER LINE
RESISTIVITY AS INDICATED BELOW CENTER LINE

1 : 2500

50 0 50 100 150

METRES

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SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY

INDUCED POLARIZATION

PSEUDOSECTIONS

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JANUARY, 1990

MODEL L 2400N

GEOLOGICAL BRANCH
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LINE 2600 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M
SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1.2.3.4.5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

SJ GEOPHYSICS LTD.

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.
GILL PROPERTY
INDUCED POLARIZATION
PSEUDOSECTIONS
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GEOLOGICAL BRANCH
ASSESSMENT REPORT

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LINE 2800 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M
SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1.2.3.4.5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

SJ GEOPHYSICS LTD.

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

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SOUTH KOOTENAY GOLDFIELDS INC.
GILL PROPERTY
INDUCED POLARIZATION
PSEUDOSECTIONS
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JANUARY, 1990 SECTION L 2800N

GEOLOGICAL BRANCH
ASSESSMENT REPORT

19,822

LINE 3400 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M

SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1,2,3,4,5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

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STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S: SHALLOW DEPTH
M: MEDIUM DEPTH
D: DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.

GILL PROPERTY

INDUCED POLARIZATION

PSEUDOSECTIONS

FORT STEELE M.D., B.C. N.T.S. 82 G

JANUARY, 1990 SECTION L 3400N

LINE 4100 N

CONTOUR INTERVAL: CHARGEABILITY - 1.0 MSEC
RESISTIVITY - 100 OHM-M
SURVEY ARRAY: POLE-DIPOLE
A = 50 METRES N = 1.2.3.4.5 & 6
TD = 130 MS TW = 65 MS
CURRENT WEST OF POTENTIAL

INSTRUMENTATION: HUNTEC MARK 2 7.5 KW TRANSMITTER
HUNTEC MARK 4 RECEIVER

SJ GEOPHYSICS LTD.

STRONG CHARGEABILITY ANOMALY
MEDIUM CHARGEABILITY ANOMALY
WEAK CHARGEABILITY ANOMALY

HIGH APPARENT RESITIVITY
INTERMEDIATE APPARENT RESITIVITY
LOW APPARENT RESITIVITY

S SHALLOW DEPTH
M MEDIUM DEPTH
D DEEP DEPTH

RESITIVITY CONTACT - POINTING IN THE DIRECTION OF DECREASING RESITIVITY

1 : 2500
50 0 50 100 150
METRES

BAPTY RESEARCH LIMITED
SOUTH KOOTENAY GOLDFIELDS INC.
GILL PROPERTY
INDUCED POLARIZATION
PSEUDOSECTIONS
FORT STEELE M.D., B.C. N.T.S. 82 G
JANUARY, 1990 SECTION L 4100N