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1990 GEOCHEMICAL AND GEOLOGICAL REPORT

on the

JOSH CLAIM GROUP

KUTCHO CREEK AREA, NORTHWESTERN B.C.

Liard Mining Division
NTS: 104I/1
Latitude: 58 12'N Longitude: 128 22'

Owned and Operated by :

Homestake Mining (Canada) Limited
1000-700 West Pender Street
Vancouver, B.C. V6C 1G8

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SUMMARY

The Josh claim group is located in the Liard Mining Division, approximately 100km east of Dease Lake. The claim group lies immediately to the south of, and is contiguous with, claims hosting the Kutcho Creek volcanogenic massive sulphide deposits.

Exploration work in the area of the claim group, was sporadic between 1968 and 1983. Since 1984 and 85, when geological mapping and a Questor airborne INPUT survey identified EM conductors within areas of favourable geology, exploration has been conducted on an annual basis. This report describes soil geochemical orientation surveys in two areas and geology and lithogeochemistry from one of these areas.

The orientation surveys determined that standard sampling methods are suitable in most areas but that extreme variations in the type and depth of overburden greatly influence the nature of the geochemical response and therefore a good understanding of the surficial geology at a local scale is necessary for geochemical interpretation. Multi-element analyses and careful statistical evaluation provide insights into the nature of the overburden and type of dispersion thereby increasing the productivity of the overall survey.

Four areas with clusters of base metal and related anomalies are thought to be indicative of mineralization and warrant further sampling.

1.0 INTRODUCTION

1.1 Location and Access

The Kutcho Creek property is located within the Liard Mining Division, NTS 104I/1, approximately 100 km east of Dease Lake, in northwest British Columbia (Figure 1.1). Geodetic coordinates are 58° 12' N and 128° 22' W.

Access to the property is by fixed-wing aircraft from Smithers, Dease Lake or Watson Lake to the 1100m gravel airstrip located beside Kutcho Creek. The property is connected to the airstrip by an 8km long road, however, the large size of the property requires helicopter access to the 88 claim groups.

1.2 Climate and Physiography

Located within the Cassiar Mountains, on the divide between Arctic and Pacific watersheds, the area is moderately rugged with elevations ranging from 1400m to 2200m. Most of the area is alpine, with treeline at approximately 1500m. Snow cover can persist for nine months of the year. Structural fabric and two periods of glaciation have produced an intersecting pattern of east-west and north-south ridges. Major valleys are often filled with a deep layer of till.

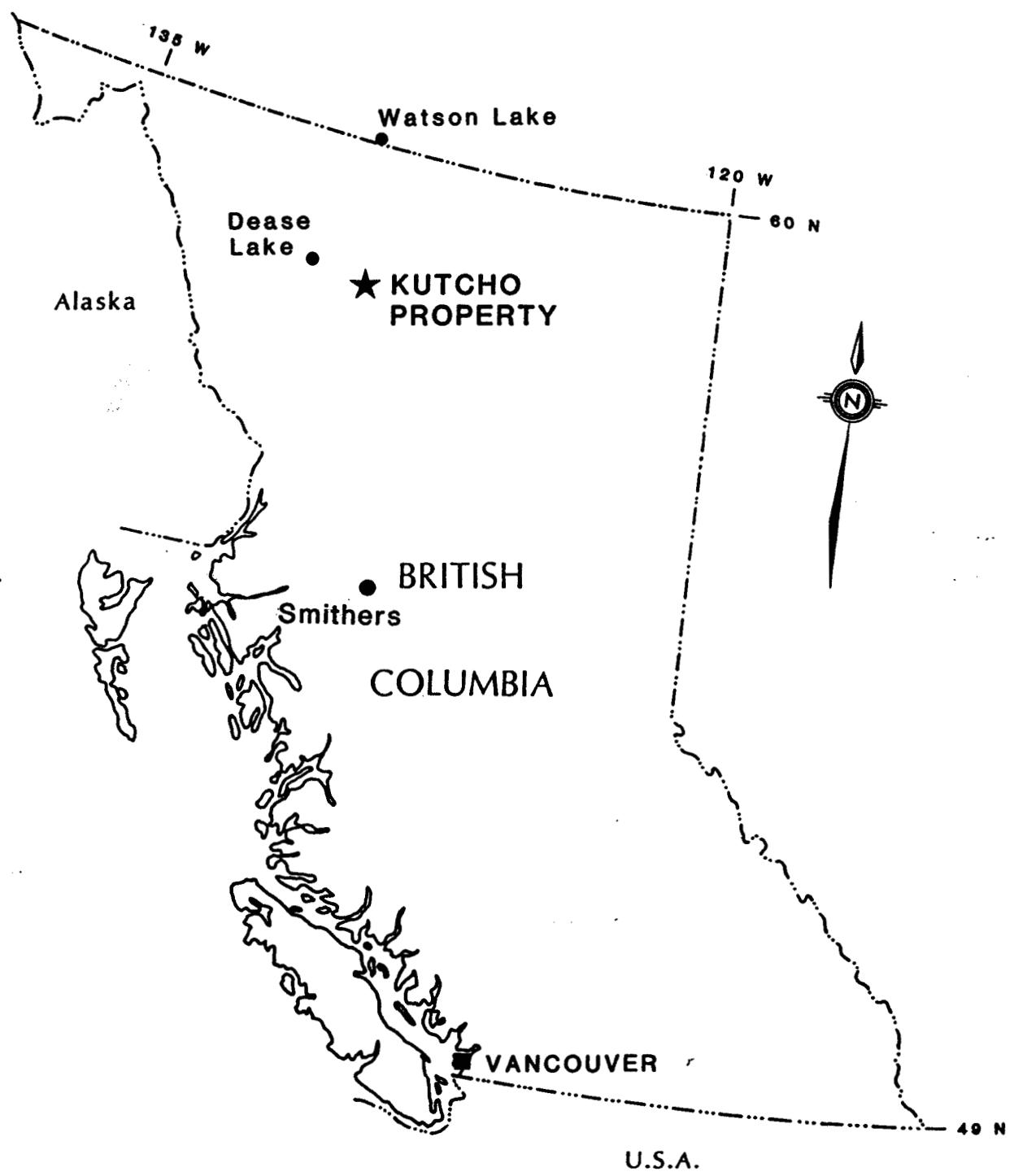


Figure 1.1 Property location map.

TABLE 1.1 - CLAIM STATUS

JOSH GROUP

| <u>CLAIM NAME</u> | <u>UNITS</u> | <u>EXPIRY DATE</u> | <u>RECORD NUMBER</u> |
|-----------------------|--------------|------------------------|--------------------------|
| PHIL 2 | 12 | Jul. 7/91 | 3565 |
| PHIL 3 | 4 | Jul. 7/91 | 3566 |
| JOSH 2 | 18 | Jul. 17/91 | 3359 |
| JOSH 5 | 20 | Aug. 19/91 | 3371 |
| JOSH 3 | 18 | Jul. 17/91 | 3360 |
| JOSH 4 | 18 | Jul. 17/91 | 3361 |

1.3 Property and History

The claim group lies to the south of, and is contiguous with, claims covering the Kutcho Creek polymetallic volcanogenic massive sulphide deposits. The claim group and location of the 1990 grid work is shown on Figure 1.2. Claim status is summarized in Table 1.1.

Various portions of the property have been held and worked by different companies in the past. The most significant exploration was carried out by Imperial Oil Ltd. (Esso Minerals Canada) who, in 1975, drilled four short holes to test airborne EM conductors located along the western and southern periphery of the property. Geological mapping in 1984 and 1985 suggested that altered felsic volcanics on the property were structurally related to rocks hosting the Kutcho deposits. A Questor airborne MKVII INPUT EM and Magnetic survey flown in November 1985 identified a number of conductors within areas of favourable geology on the property. Since then, evaluation of the airborne conductors, consisting of geological mapping, ground geophysics, and geochemical surveys, has been carried out on an annual basis.

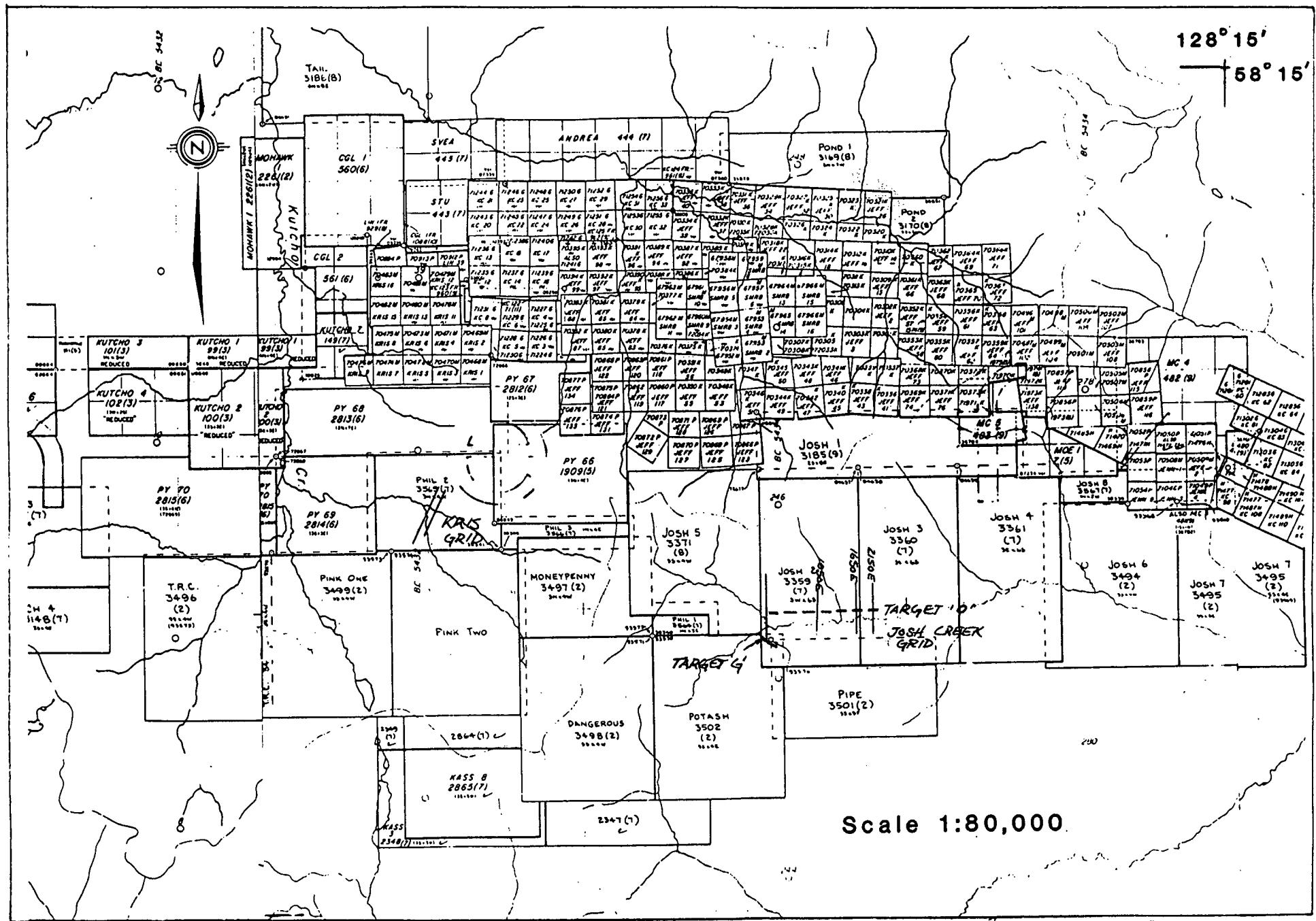


Figure 1.2 Claim Map

1.4 Current Work

The work discussed in this report was carried out between June 31 and July 6, 1990, and was part of a geochemical orientation survey conducted prior to a major exploration program. The orientation survey was designed to test which areas and sampling methods would be most amenable for follow-up surveys.

Approximately 6 line kilometers of grid and soil sampling were completed over three target areas (Kris, O and G). The soil grid consisted of 25m sample spacing on lines spaced at least 200m apart along the trend of the target area, usually an EM conductor. A total of 308 soil samples, 9 stream sediment samples and 9 lithogeochemical samples were collected.

The exploration crew was mobilized from Vancouver or Smithers and lodged at the Esso/Sumac camp located on the north side of the Kutcho deposit area. A Bell 47 helicopter with a turbine conversion was contracted from Northern Mountain Helicopters to transport the crew from the camp to the grid areas.

2.0 GEOLOGY

2.1 Regional Geology

The Kutcho property lies within the King Salmon Allochthon, a narrow belt of Triassic island arc volcanics and Jurassic sediments sandwiched between two northerly dipping thrust faults. Penetrative foliation and axial planes of the major folds are parallel to these bounding faults. The belt of volcanics is thickest in the area where it hosts volcanogenic massive sulphide deposits; due in part to primary

deposition, but also to stratigraphic repetition by folding and thrusting. Major folds are delineated by the Sinwa Limestone and the contact between Kutcho Formation volcanics and Inklin Formation argillites (Fig. 2.1).

Volcanogenic mineralization of the Kutcho deposits occurs at the contact between footwall lapilli tuffs and hanging wall quartz and quartz-feldspar crystal tuffs. The main sulphide bearing horizon is marked by extensive hydrothermal alteration and the presence of thinly bedded ash tuffs, the latter indicating a temporary hiatus in volcanic activity. This sulphide horizon is geochemically, and often visually, recognizable over a strike length of 8 km.

The coarsest grained pyroclastic rocks of the Kutcho Formation occur in the vicinity of the known sulphide deposits and become noticeably finer grained towards the south and east. The major center of volcanism is postulated to be northeast of the Kutcho sulphide lens, although subordinate centers may exist elsewhere on the property.

2.2 Property Geology

Rocks which underlie the Josh claim group are part of the Kutcho formation and consist of pyroclastic, flow and minor sedimentary units of mafic and felsic compositions. Lithological units tend to be thinly bedded and are finer grained than their compositional counterparts which host the Kutcho sulphide deposits. All rock units dip steeply to moderately to the north.

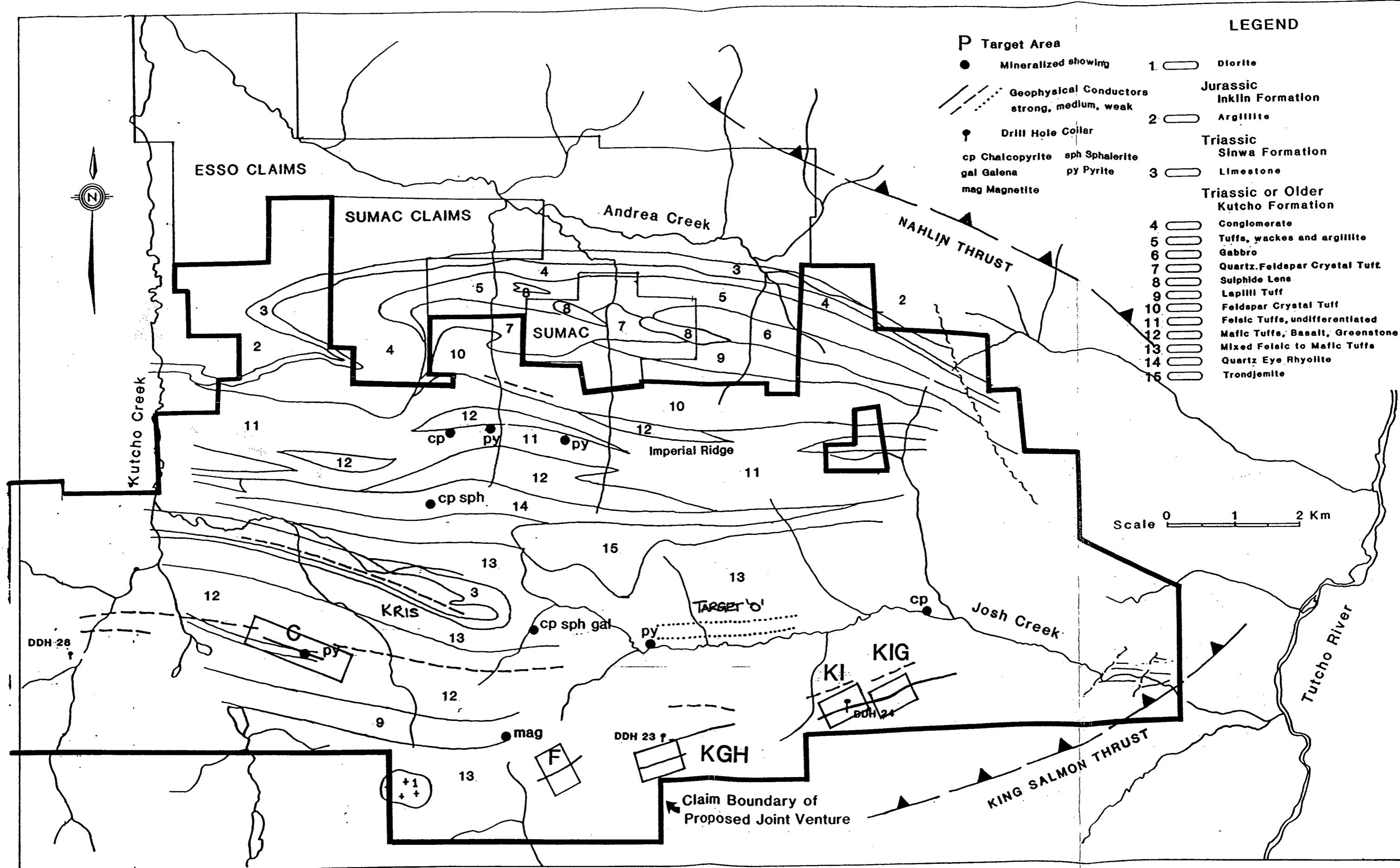


FIGURE 2.1 GENERALIZED GEOLOGY AND TARGET GRID LOCATIONS.

Geology of the Kris target (Fig. 3.2) is not well understood due to a paucity of outcrop. A synclinal keel of Sinwa limestone and Inklin Formation argillite is inferred to underlie the northern part of the Phil 2 claim based on better rock exposure to the east and west of the claim area, and on the surface trace of an airborne EM anomaly interpreted to correlate with the argillite. Approximately 200m to the south of the argillite, in the southern fork of Kris Creek, is an outcrop of altered felsic ash tuffs which may contain exhalative material (Fig. 3.2). In the vicinity of the Kutcho sulphide deposits the Sinwa limestone is separated from the mineralized stratigraphy by 400m of conglomerate and a unit consisting of interbedded sediments and mafic intrusive and extrusive rocks (tuff-argillite unit). The proximity of felsic tuffs to the Sinwa limestone in the Kris Creek area suggests that the conglomerate and tuff-argillite unit are thin or absent and that the felsic tuffs are probably stratigraphic equivalents of the Kutcho sulphide bearing sequence. A detailed geological description and lithogeochemical results for the Kris Creek outcrop are discussed in Section 3.

The O target parallels the central part of Josh Creek with the EM conductors located on the north side of the Creek in areas of deep and swampy overburden. Rocks exposed in the stream bed consist of siliceous and sericitic schists derived from felsic ash tuffs. Pyritic layers, up to 30cm wide and traceable over 100m along strike, occur on the cliffs along the stream gully in the geochemical grid area. Neither the EM conductors nor the gravity anomalies (Holbek, 1988) correlate well with the pyritic exposures.

2.3 Surficial Geology

Depth and type of overburden is extremely variable on the property. Thick till deposits, kame terraces and eskers are common in the valleys or at lower elevations. On the Kris grid bedrock exposure is restricted to stream beds and a small area near line 10+00W, 9+00N. The area between the north and south tributaries of Kris Creek is a remnant of a glacial outwash deposit consisting of a 5 to 30m thickness of coarse to fine bedded gravels.

In the Josh Creek area (targets 0 and G) outcrops are restricted to the Josh Creek canyon and the area south of line 4+50E and 9+00S. Soil development on the north side of Josh Creek is poor consisting of 10 to 40cm of organic-rich material overlying clay-rich boulder till. The water table is at or near surface in most areas. Diamond drilling subsequent to this survey revealed that thickness of the till ranges from 7 to 68m. The presence of outcrop south of the G target suggests that the cover is thinner in that direction.

3.0 GEOCHEMISTRY

3.1 Methods

Soil samples were collected at 25m stations along chained and flagged grid lines. Line spacing was variable depending upon target character and size. Samples were collected from the B horizon where possible, at depths between 20-40cm using mattocks. Where a good soil profile was present samples were collected from each soil horizon (denoted with subscript B or C following the sample number on the list of analytical results). Duplicate samples were collected with a soil auger from depths of 50 to 150cm along Line 10+00W on the Kris target area (denoted with subscript A following the sample number). Samples were placed in kraft paper bags and air dried before shipment.

Analyses were performed by Acme Analytical Ltd. of Vancouver using Induction Coupled Plasma methods for 30 elements. Gold was analyzed by aqua-regia digestion and atomic absorption techniques. Samples are sieved to -80 mesh and a 0.5g subsample is digested in 3ml of hot aqua regia for 1 hour and then diluted to 10ml with water prior to analysis.

Of the 31 elements analyzed 13 are deemed insignificant due to a combination of high detection limits, partial digestion and low background values. Analytical results for the remaining elements, which consist of Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, Ca, P, La, Cr, Mg, Ba, Al and Au, were statistically evaluated using Geomicro Systems' computer program GEOCHEM. Sample locations and copper and zinc values are plotted on 1:5,000 scale maps in Figures 3.1 and 3.2.

3.2 Description of Results

Previous geochemical surveys in the property area established that copper and zinc, being major components of the sulphide deposits, were the best geochemical indicators. Arsenic and silver, although very minor components of the sulphide lenses, were also found to be useful as they were less influenced by background lithological changes.

Similarly, lead and barium, trace components of the sulphide deposits, are useful geochemical indicators due to their different dispersion characteristics in the surficial environment, relative to copper and zinc. Rocks which underlie the grid area consist of interlayered basalt flows and tuffs and felsic ash tuffs. Sulphide deposits are

typically hosted by altered felsic rocks. It was thought that the altered felsic rocks would have a detectable difference in soil geochemical signature from the basaltic rocks, particularly for Ni, Co, Cr, Al, Mg and Ca, and therefore element plots would help with geological mapping in overburden areas. However, this does not appear to be the case, the distribution of these elements seems to be, at best, a function of type and depth overburden.

Table 3.1 is a summary of the basic statistics for the 18 elements investigated. Histograms and cumulative probability plots (Sinclair, 1974) were produced for each element and "threshold" values were chosen to separate different sample populations where appropriate. Extreme outliers in the sample data were culled prior to plotting histograms. In many cases, particularly for the major elements, sample populations were normally or log normally distributed and threshold values were of questionable significance. The elements associated with sulphide deposits typically have bimodal populations and threshold values are selected to separate background from anomalous (mineralized) populations. For those metals that did not have two (or more) distinct populations on the cumulative probability plots, thresholds were subjectively chosen between values at the mean plus one standard deviation and the 90th percentile.

To aid in the evaluation of multi-element data, element correlations were investigated (Table 3.2). Both expected and unexpected correlations were noted. Elements associated with mafic lithologies (Mg, Cr, Co, and Ni) display a high degree of intercorrelation with the exception of Fe which is weakly correlated with Zn and Al. Although Cu and Zn are strongly correlated the other elements associated with mineralization

Table 3.1

| Kutcho | Elementary Statistics | | | | Wed Sep 5, 1990 | | | | |
|-----------------------------------|-----------------------|---------|--------|----------|-----------------|---------|--------|------------|---------|
| Variable: | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Au ppb |
| Number of Samples Selected: | 311 | 311 | 311 | 311 | 311 | 311 | 311 | 311 | 311 |
| Number of Missing or Null Values: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Minimum: | 1.000 | 11.000 | 2.000 | 40.000 | 0.100 | 5.000 | 3.000 | 72.000 | 1.000 |
| Maximum: | 39.000 | 412.000 | 20.000 | 676.000 | 1.100 | 124.000 | 31.000 | 5816.000 | 272.000 |
| Range: | 38.000 | 401.000 | 18.000 | 636.000 | 1.000 | 119.000 | 28.000 | 5744.000 | 271.000 |
| Mean: | 1.296 | 36.672 | 9.341 | 108.768 | 0.154 | 58.650 | 13.492 | 702.608 | 5.064 |
| Median: | 1.000 | 33.000 | 9.000 | 103.000 | 0.100 | 57.000 | 13.000 | 611.000 | 3.000 |
| Variance: | 4.839 | 650.201 | 9.356 | 1977.136 | 0.016 | 350.498 | 12.494 | 218015.391 | 256.041 |
| Standard Deviation: | 2.200 | 25.499 | 3.059 | 44.465 | 0.127 | 18.722 | 3.535 | 466.921 | 16.001 |
| Standard Error: | 0.125 | 1.446 | 0.173 | 2.521 | 0.007 | 1.062 | 0.200 | 26.477 | 0.907 |
| Coefficient of Variation (%): | 169.751 | 69.533 | 32.747 | 40.880 | 82.263 | 31.921 | 26.199 | 66.455 | 315.962 |
| Coefficient of Skewness: | 16.224 | 10.547 | 0.062 | 6.976 | 3.794 | 0.293 | 1.045 | 6.601 | 15.127 |
| Coefficient of Kurtosis: | 277.601 | 151.850 | 3.348 | 86.357 | 21.127 | 3.250 | 7.085 | 62.436 | 249.653 |
| Log 10 Transformed Mean: | 0.051 | 1.525 | 0.941 | 2.015 | -0.884 | 1.743 | 1.115 | 2.802 | 0.491 |
| Log 10 Variance: | 0.178 | 0.238 | 0.248 | 0.197 | 0.000 | 0.240 | 0.166 | 0.243 | 0.506 |
| Log 10 Standard Deviation: | 0.422 | 0.488 | 0.498 | 0.444 | 0.000 | 0.490 | 0.408 | 0.493 | 0.711 |
| Variable: | Fe % | As ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Al % |
| Number of Samples Selected: | 311 | 311 | 311 | 311 | 311 | 311 | 311 | 311 | 311 |
| Number of Missing or Null Values: | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Minimum: | 0.960 | 2.000 | 0.070 | 0.026 | 5.000 | 10.000 | 0.280 | 52.000 | 1.050 |
| Maximum: | 8.020 | 26.000 | 1.560 | 0.208 | 71.000 | 128.000 | 1.660 | 565.000 | 5.760 |
| Range: | 7.060 | 24.000 | 1.490 | 0.182 | 66.000 | 118.000 | 1.380 | 513.000 | 4.710 |
| Mean: | 4.027 | 7.794 | 0.433 | 0.067 | 16.453 | 63.489 | 1.003 | 219.543 | 2.676 |
| Median: | 3.890 | 7.000 | 0.400 | 0.063 | 15.000 | 64.000 | 1.040 | 204.000 | 2.570 |
| Variance: | 0.645 | 15.758 | 0.049 | 0.001 | 55.701 | 174.481 | 0.052 | 8574.119 | 0.571 |
| Standard Deviation: | 0.803 | 3.970 | 0.221 | 0.026 | 7.463 | 13.209 | 0.229 | 92.597 | 0.756 |
| Standard Error: | 0.046 | 0.225 | 0.013 | 0.001 | 0.423 | 0.749 | 0.013 | 5.251 | 0.043 |
| Coefficient of Variation (%): | 19.937 | 50.931 | 51.063 | 38.824 | 45.360 | 20.805 | 22.822 | 42.177 | 28.245 |
| Coefficient of Skewness: | 0.884 | 0.841 | 1.355 | 2.208 | 2.716 | 0.043 | -0.531 | 0.746 | 1.000 |
| Coefficient of Kurtosis: | 5.662 | 4.472 | 6.463 | 10.676 | 15.987 | 5.353 | 3.499 | 3.632 | 4.713 |
| Log 10 Transformed Mean: | 0.596 | 0.828 | -0.419 | -1.200 | 1.182 | 1.792 | -0.013 | 2.301 | 0.411 |
| Log 10 Variance: | 0.126 | 0.396 | 0.000 | 0.000 | 0.255 | 0.144 | 0.000 | 0.302 | 0.188 |
| Log 10 Standard Deviation: | 0.355 | 0.629 | 0.000 | 0.000 | 0.505 | 0.380 | 0.000 | 0.550 | 0.433 |

Table 3.2

Kutcho Correlation Coefficients Wed Sep 5, 1990 Page 1 of 3
Kutcho

Table 3.2 con't

Kutcho Correlation Coefficients Wed Sep 5, 1990 Page 2 of 3
Kutcho

(Pb, Ag, As, and Ba) are not intercorrelated. P, La, Ba, Ca, Al and Mn are moderately to strongly intercorrelated and suggest a "felsic suite" of elements.

Calculated correlations can be somewhat misleading because they do not take into account spatial associations. Proportional symbol plots, or even scanning the data shows some interesting spatial associations. In general, areas with elevated Cu and Zn also have elevated values of Fe, Mn, La, Ba and Al. Ag, As and Mo are sometimes associated with areas of anomalous base metals.

Copper values have a skewed, slightly log normal distribution which could contain a small secondary population related to mineralization (Fig. 3.3). Threshold value was selected at 50ppm, at the break between the two populations. This threshold value is half of what has been used on past surveys on the property. There are four clusters of anomalous copper values approximately centered on the following grid points: 10+00W, 950N; 4+50E, 7+50N; 4+50E, 7+50S and 21+00E, 7+50N. The actual copper values at these points are not high and the areas are small (<200m), but clustering of anomalous values and their association with other element anomalies, particularly zinc, suggest that the values are related to mineralization. Other anomalous values do occur but lack of clustering or association with other element anomalies makes interpretation ambiguous.

The Zinc population is similar to copper but has improved range and contrast (Fig. 3.3). Threshold for zinc is 150ppm which is the same as for previous surveys. The most prominent zinc anomalies are associated with the copper anomalies described above. There are fewer isolated zinc highs than copper, likely due to the selection of higher (relatively) threshold value.

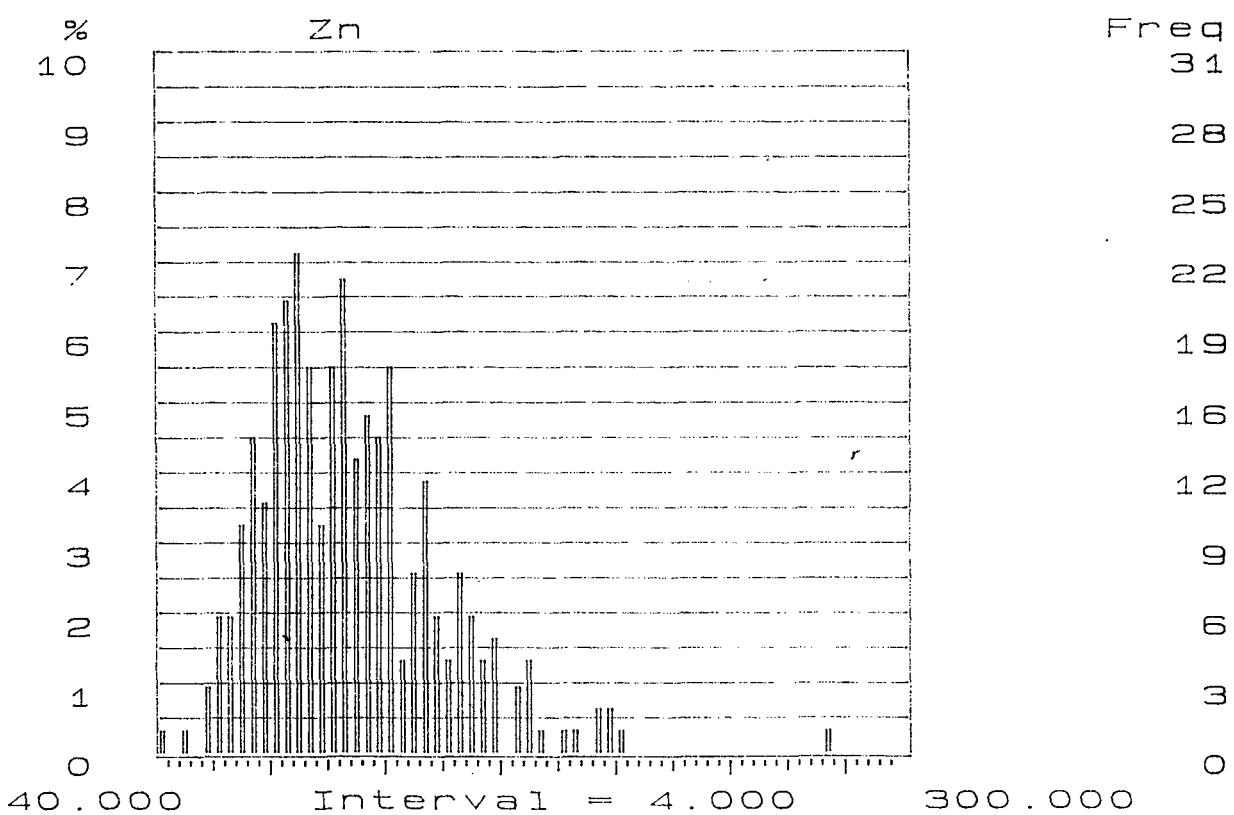
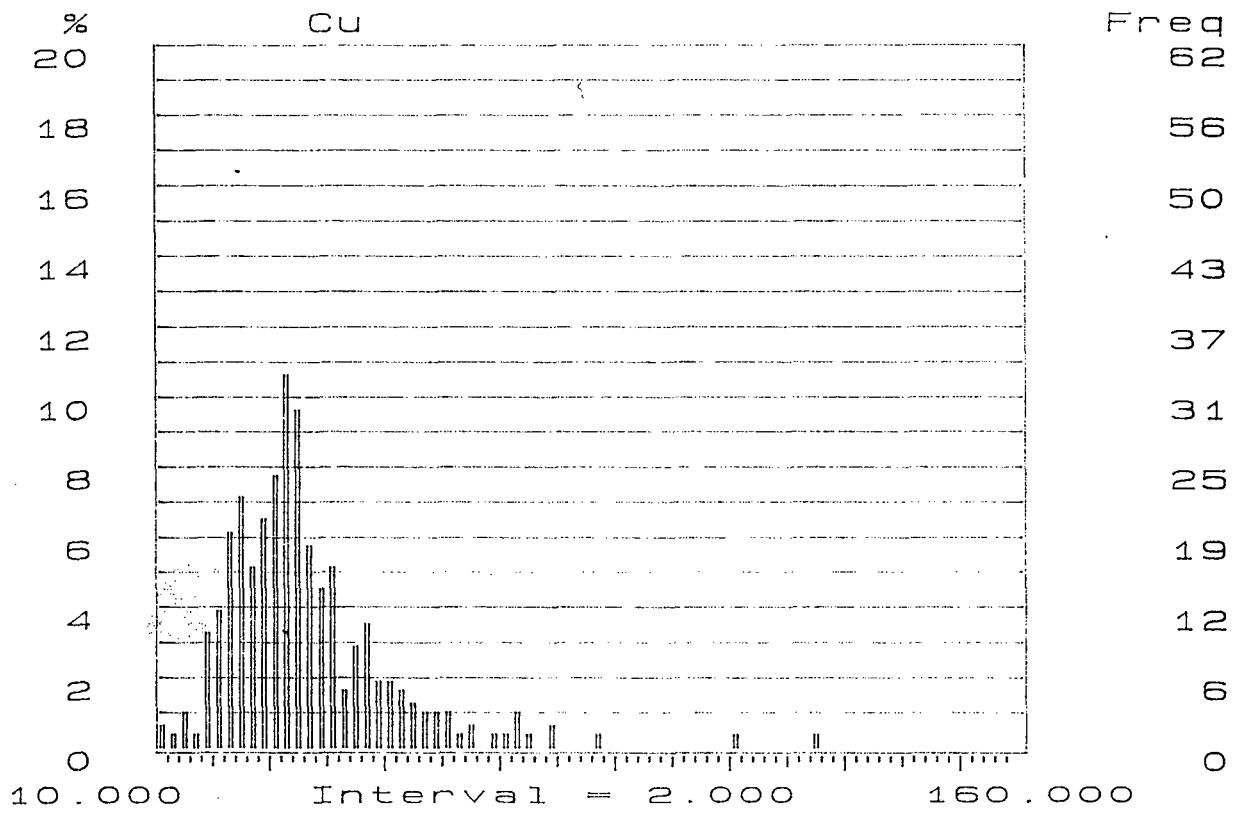


Figure 3.3

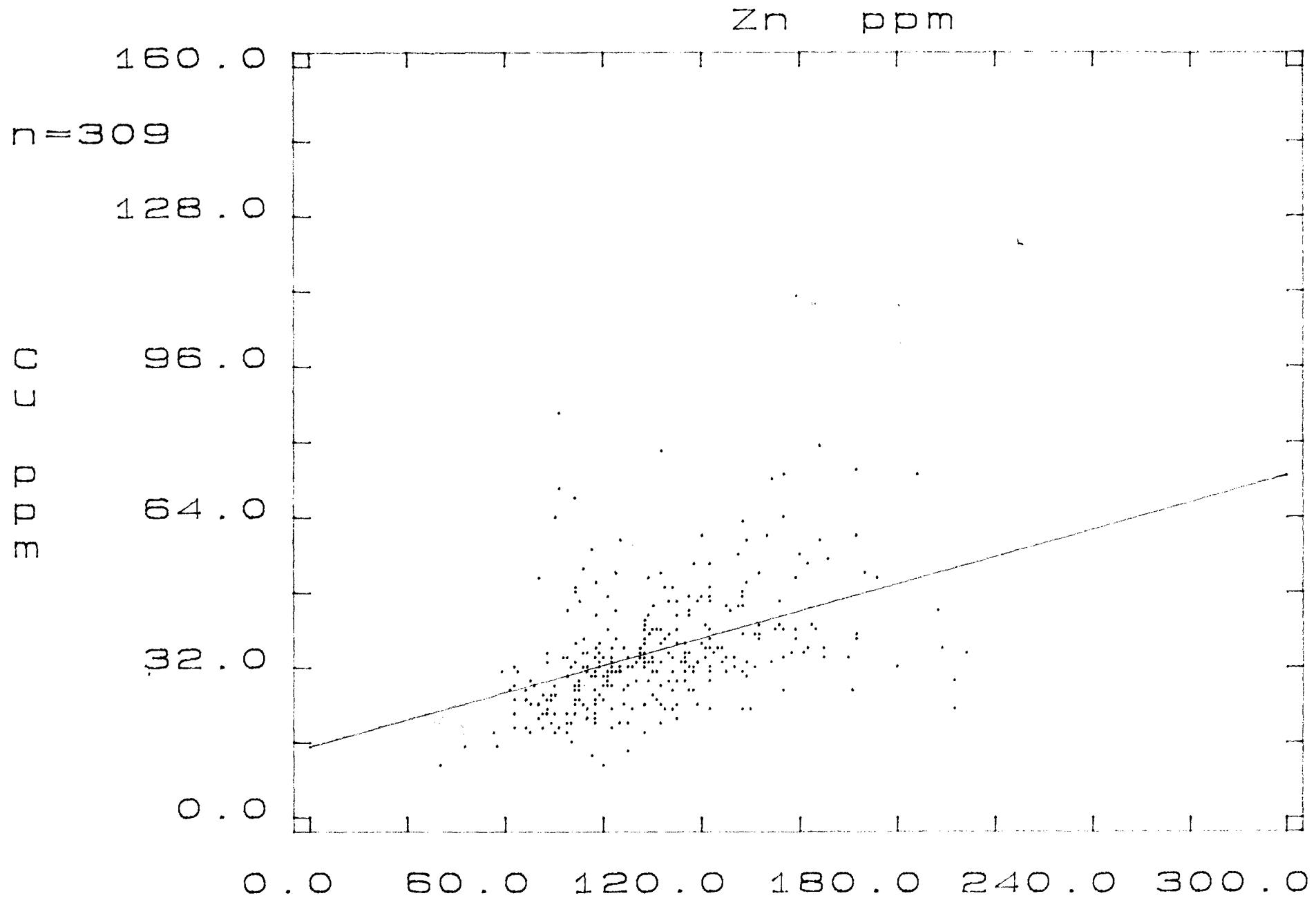


Figure 3.4

Lead values are low and have very low contrast. The distribution appears to be a single normal population. There is some association of high lead values with copper and zinc but it is inconsistent. The low lead values and weak association with copper and zinc suggest that hydromorphic dispersion is a significant factor.

Silver values are like those of lead. Apart from the anomaly at 10+00W, 9+50N, which is close to bedrock, there is little association of silver highs with those of copper and zinc. Molybdenum, commonly associated with exhalative rocks of the Kutcho Formation (Holbek and Heberlein, 1986), is virtually flat in this survey. A single anomalous value of 39ppm is associated with a high copper value at 20+50E, 2+50N, a sample taken from a rusty seep on the south bank of Josh Creek.

Manganese has a skewed population distribution that is bimodal (Fig. 3.5). The small anomalous population appears to be associated with mineralization. Manganese does not have a high correlation coefficient with either copper or zinc but does display a pronounced spatial association with base metal anomalies. Iron has a normal, bimodal distribution (Fig. 3.5). Anomalous iron values correlate well with other element anomalies. Barium has a skewed log-normal distribution that appears to be unimodal (Fig. 3.6). Anomalous values of barium are reasonably well correlated, both mathematically and spatially with copper and zinc.

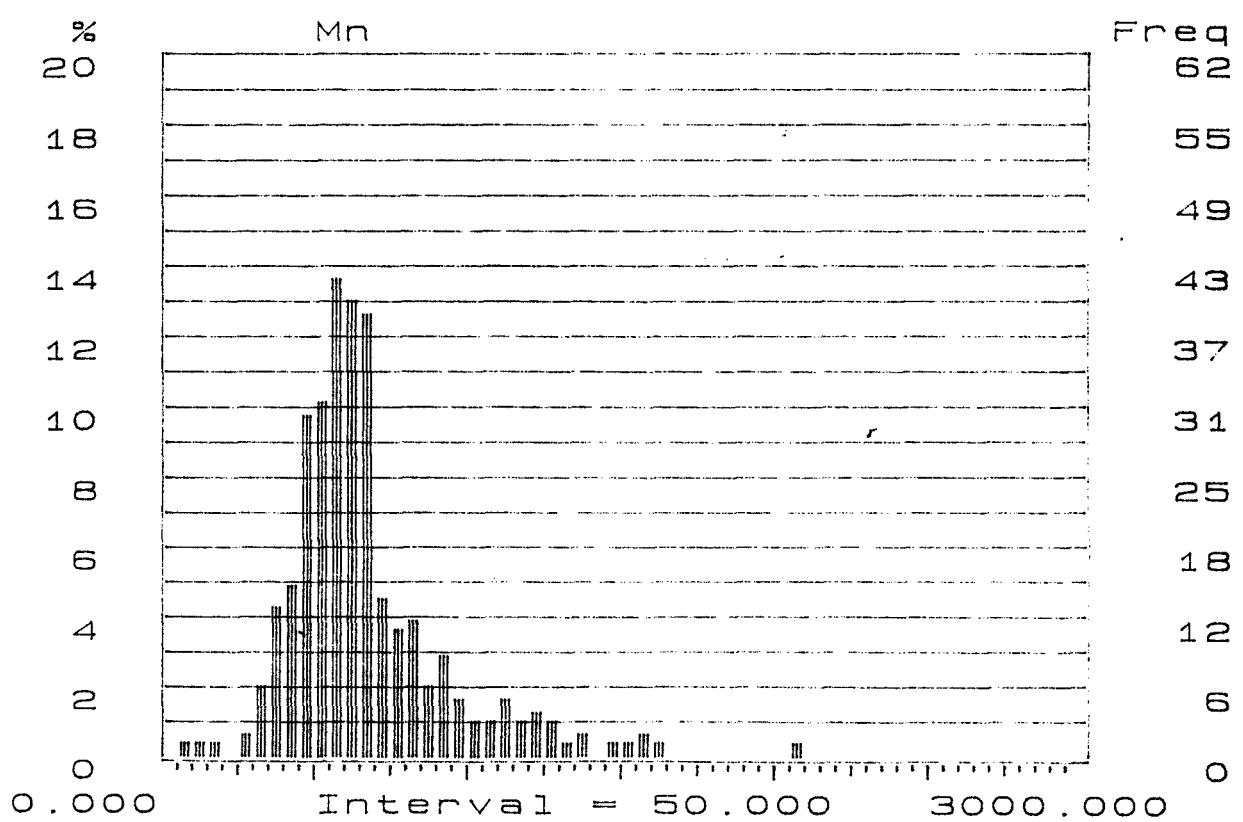
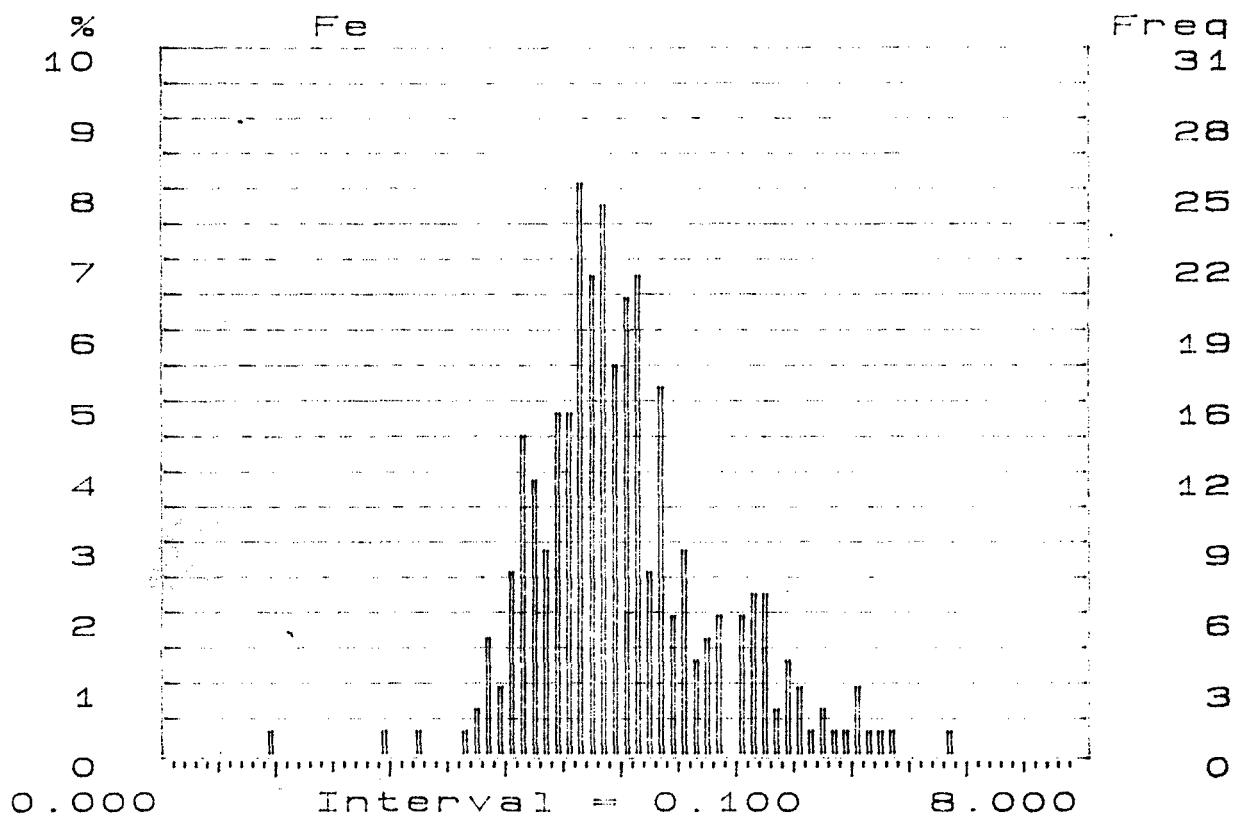


Figure 3.5

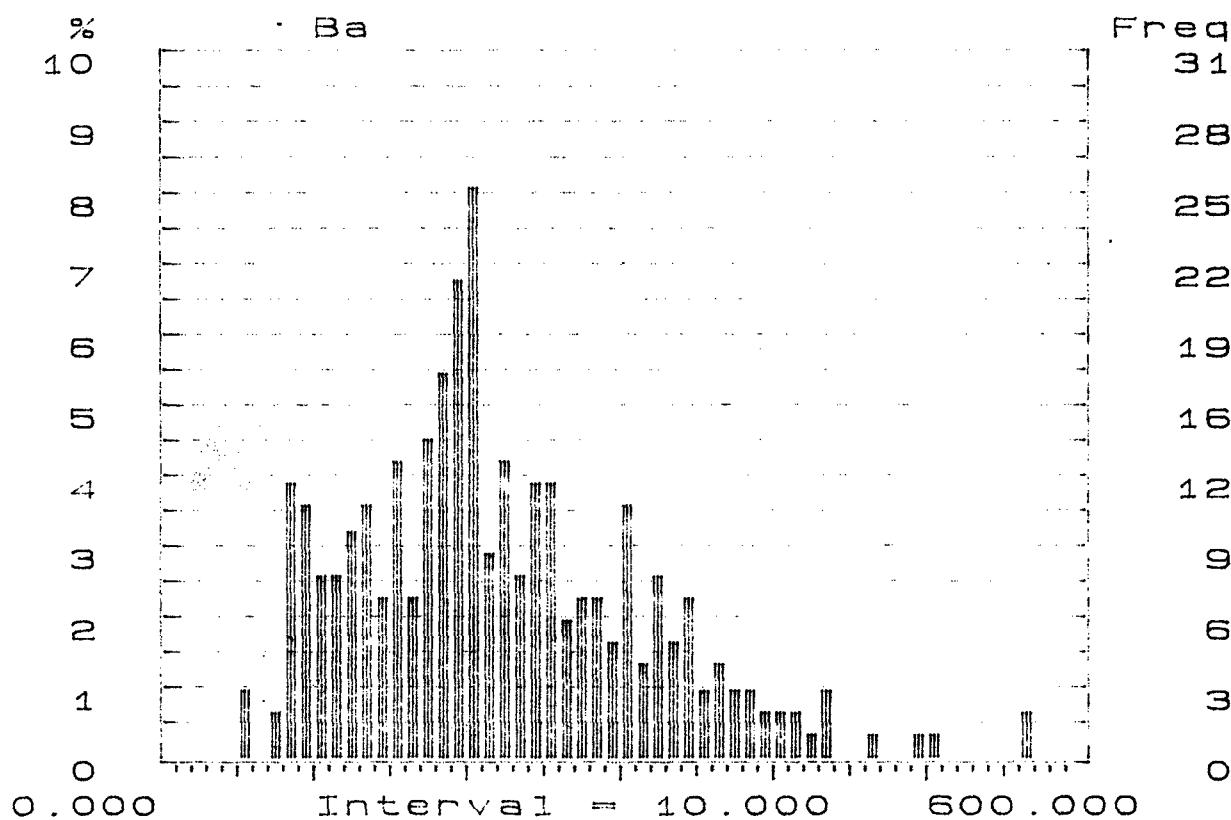


Figure 3.6

3.3 Comparison of Sampling Methods

For the most part, there is not a significant difference between analytical results from auger and mattock samples. A notable exception is sample 10+00W, 9+75N where the auger sample yielded a high copper and the highest zinc values while the corresponding mattock sample had values below threshold. This could be a random effect or one of the few cases on the property where sample depth is significant. The sample was taken near an outcrop containing anomalous base metals. For most of the survey area, where till cover is considerable, it would appear that element dispersion is hydromorphic and that sample depth is not a critical factor in concentration.

No anomalies were detected in the few locations where both B and C horizons were sampled and therefore the preference of one sample horizon over the other remains moot.

3.4 Lithogeochemistry

Approximately 100m of sub-continuous outcrop is exposed along the south bank of the south tributary of Kris Creek (Fig. 3.1). Rocks consist of fine-grained, siliceous, commonly pyritic sericite schists. The western end of the outcrop contains a 3m thickness of rusty weathering carbonate rich rock which resembles exhalative carbonate from the Kutcho deposit. The outcrop was chip sampled along its length (9 samples). Samples varied from 3 to 18m in length (Fig. 3.7) with sample length being determined by changes in lithology or alteration.

Sample Location
and Number

8

- Carbonate
Exhalite (?)

7

1

6

5

Rusty Paper (Sericite) Schist

4

Siliceous Sericite
Carbonate Schist,
locally pyritic

3

Aphanitic, Porcelanous,
white Rhyolite

9

2a

Pyritic Silica Exhalite

2b

2c

2d

2e

2f

2g

2h

2i

2j

2k

2l

2m

2n

2o

2p

2q

2r

2s

2t

2u

2v

2w

2x

2y

2z

2aa

2ab

2ac

2ad

2ae

2af

2ag

2ah

2ai

2aj

2ak

2al

2am

2an

2ao

2ap

2aq

2ar

2as

2at

2au

2av

2aw

2ax

2ay

2az

2ba

2ca

2da

2ea

2fa

2ga

2ha

2ia

2ja

2ka

2la

2ma

2na

2oa

2pa

2qa

2ra

2sa

2ta

2ua

2va

2wa

2xa

2ya

2za

HOMESTAKE
MINING (CANADA) LIMITED

LITHOGEOCHEMICAL SAMPLE
LOCATIONS FROM THE
KRIS CREEK EXPOSURE

| DRAWN NO | DATE | NTB | FIGURE |
|---------------|--------------|--------|--------|
| Revised _____ | OCTOBER 1990 | 104I/2 | 3.7 |

Samples were analyzed by International Plasma Labs. of Vancouver. Ag, Al, As, Ca, Co, Cu, Fe, K, Mg, Mn, Mo, Na, Pb, Sr and Zn are analyzed by ICP methods. Au is analyzed by fire assay with atomic absorption finish and F is analyzed by specific ion electrode. Ca, Fe, Mg, Mn and Sr are reanalyzed by ICP methods following a hot HCl selective extraction.

Apart from the carbonate rich sample, which was highly anomalous in copper and anomalous in zinc, iron and fluorine, samples did not display element enrichments or trends commonly observed in similar rocks near the Kutcho deposit. There does not appear to be any zonation of elements towards the anomalous carbonate rich unit.

4.0 CONCLUSIONS AND RECOMMENDATIONS

The 1990 exploration program on the Josh claim group was designed to test whether the Kris, G and O target areas were amenable to evaluation by soil geochemistry and if so, which sampling methods would be most useful. Approximately 6 line-km, totaling 308 samples were collected from the three target areas. All three targets contained anomalous areas although the best anomaly was obtained in an area of shallow overburden on a single line on the Kris target. The type and depth of overburden is highly variable over the property and even within individual target areas. Because the nature of the overburden can profoundly influence the distribution of elements within soils, an understanding of the surficial geology is a prerequisite for interpretation geochemical results. The type of overburden will also determine which sampling method will work best. In areas of relatively thin, dry overburden, the soil auger may give results with improved

contrast by collecting material closer to the bedrock surface. On the other hand, in areas of thick till cover where the water table is near surface, and elemental dispersion is by hydromorphic means the method of sample collection does not appear to be significant. The extreme variation in the nature of overburden on the property necessitates that each grid area have its own orientation survey, and its own set of threshold values.

The potential variation in threshold values due to overburden and other variations on the property makes interpretation of geochemical results difficult. The use of multi-element analyses and careful statistical evaluation can increase confidence in the interpretation and thereby increase the overall productivity of geochemical surveys at very little additional cost.

The O target, located along the north side of Josh Creek, corresponds to weak EM conductors near altered felsic volcanic rocks. The alteration zone within the Creek has a weak soil expression. Values over the entire grid are relatively low; quite reasonably due to excessive depths of glacial till (up to 68m). Poorly clustered, weakly anomalous results near 7+50N on all the O grid lines may correspond to a weak EM conductor. The best response is on line 4+50E and additional sampling is warranted in this area. Weakly anomalous samples near the south end of line 4+50E, target G, also warrant additional sampling.

Lines of the C grid should be extended to the north to cover the western extension of the Kris grid anomaly (10+00W, 9+50N). Additionally, because the Kris grid anomaly occurs on the south limb of a syncline the grid lines should be extended far enough to cover the north limb of the syncline. Weak zinc highs on the north ends of 10+00W and 8+00W may correspond to the north limb.

APPENDIX I
STATEMENT OF COSTS

LABOUR - June 31 to July 5, 1990

| | |
|---------------------------------|---------|
| P. Holbek - 5 days @ 250/day | 1250 |
| J. Smith - 5 days @ 180/day | 900 |
| G. Bickerton - 5 days @ 110/day | 550 |
| D. Holbek - 5 days @ 80/day | 400 |
| | ----- |
| | \$ 3100 |

FOOD AND ACCOMMODATION

| | |
|------------------------|---------|
| 25 man days @ \$50/day | \$ 1250 |
|------------------------|---------|

EQUIPMENT RENTAL

| | |
|------------------------------|-------|
| Computer Hardware & Software | 180 |
| | ----- |

GEOCHEMICAL ANALYSIS

| | |
|--|---------|
| 308 soil samples @ 11.00 (incl. prep.) | 3388 |
| 9 silt samples @ 11.00 | 99 |
| 9 Lithogeochem samples @ 24.00 | 216 |
| Freight | 75 |
| | ----- |
| | \$ 3778 |

TRANSPORTATION

| | |
|-------------------------------------|---------|
| Canadian Airlines | 920 |
| Central Mtn. Air - 206 | 640 |
| Northern Mountain Helicopters - B47 | |
| 5 hours @ 625 (incl. fuel) | 3125 |
| | ----- |
| | \$ 4685 |

| | |
|--------------------|--------|
| Report Preparation | \$ 400 |
| | ----- |

| | |
|--------------|-----------------|
| TOTAL | \$13,393 |
| | ----- |

STATEMENT OF QUALIFICATIONS

I, Peter Holbek, DO HEREBY CERTIFY THAT:

- 1) I am a project geologist presently employed by Homestake Mining (Canada) Limited, located at 1000-700 West Pender Street, Vancouver, BC V6C 1G8.
- 2) I graduated from the University of British Columbia with a B.Sc. (Hons.) in geology in 1980 and an M.Sc. in geology in 1988.
- 3) I have actively practiced my profession in North America since 1975.
- 4) The work described herein was done by me or under my direct supervision.

DATED THIS 9th DAY OF JANUARY, 1990 AT VANCOUVER, B.C.



Peter Holbek

APPENDIX III

GEOCHEMICAL DATA

GEOCHEMICAL ANALYSIS CERTIFICATE

104T-004

Homestake International Minerals PROJECT 3174 KUTCHO File # 90-2567 Page 1

1000 - 700 W. Pender St., Vancouver BC V6C 1G8

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | AS ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | Au** ppb | |
|------------------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|-------|--------|--------|--------|--------|--------|--------|-------|------|------|--------|--------|------|--------|------|-------|------|------|-----|----------|----|
| L10+10W 6+25N | 2 | 29 | 4 | 113 | .2 | 45 | 16 | 625 | 8.02 | 12 | 5 | ND | 1 | 16 | .18 | 2 | 2 | 82 | .18 | .056 | 9 | 95 | .71 | 156 | .18 | 2 | 2.98 | .01 | .05 | 1 | 3 |
| L10+05W 5+80N | 1 | 18 | 2 | 75 | .1 | 46 | 13 | 441 | 4.40 | 11 | 5 | ND | 1 | 18 | 1.1 | 2 | 2 | 73 | .21 | .030 | 7 | 76 | .97 | 128 | .12 | 2 | 2.41 | .01 | .05 | 1 | 2 |
| L10+00W 17+00N | 1 | 23 | 2 | 198 | .1 | 38 | 12 | 733 | 3.88 | 7 | 5 | ND | 1 | 35 | .2 | 2 | 2 | 53 | .48 | .058 | 7 | 54 | 1.05 | 191 | .06 | 4 | 2.39 | .01 | .09 | 1 | 1 |
| L10+00W 16+75N | 1 | 44 | 15 | 193 | .1 | 51 | 14 | 692 | 4.01 | 8 | 5 | ND | 1 | 51 | .8 | 2 | 2 | 55 | .93 | .069 | 15 | 58 | 1.25 | 233 | .07 | 5 | 2.68 | .02 | .10 | 1 | 3 |
| L10+00W 16+50N | 1 | 33 | 6 | 141 | .1 | 41 | 12 | 571 | 3.60 | 7 | 5 | ND | 1 | 52 | .9 | 2 | 3 | 51 | .94 | .063 | 13 | 54 | 1.17 | 208 | .08 | 2 | 2.21 | .02 | .08 | 1 | 4 |
| L10+00W 16+25N | 1 | 32 | 5 | 130 | .1 | 40 | 14 | 1034 | 3.79 | 6 | 5 | ND | 1 | 45 | 1.1 | 2 | 4 | 54 | .66 | .040 | 13 | 52 | 1.13 | 201 | .08 | 2 | 2.25 | .02 | .08 | 1 | 2 |
| L10+00W 16+00N | 1 | 31 | 3 | 106 | .1 | 38 | 12 | 639 | 3.80 | 6 | 5 | ND | 1 | 38 | .5 | 2 | 2 | 57 | .63 | .028 | 12 | 55 | 1.24 | 177 | .11 | 2 | 2.36 | .02 | .06 | 1 | 17 |
| L10+00W 15+75N | 1 | 37 | 10 | 115 | .1 | 45 | 13 | 695 | 3.70 | 5 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 58 | .68 | .047 | 13 | 60 | 1.19 | 265 | .06 | 2 | 2.89 | .02 | .08 | 1 | 6 |
| L10+00W 15+50N | 3 | 44 | 10 | 129 | .1 | 51 | 16 | 354 | 4.04 | 3 | 5 | ND | 1 | 40 | .9 | 2 | 2 | 70 | .58 | .059 | 15 | 58 | 1.06 | 219 | .09 | 3 | 2.64 | .02 | .08 | 1 | 10 |
| L10+00W 15+25N A | 1 | 31 | 2 | 91 | .1 | 50 | 14 | 637 | 3.99 | 8 | 5 | ND | 1 | 36 | .4 | 2 | 2 | 58 | .31 | .049 | 15 | 63 | 1.00 | 192 | .13 | 2 | 2.46 | .02 | .07 | 1 | 5 |
| L10+00W 15+00N | 1 | 28 | 4 | 69 | .1 | 48 | 12 | 546 | 3.08 | 7 | 5 | ND | 1 | 35 | .3 | 2 | 2 | 48 | .32 | .047 | 13 | 52 | .76 | 155 | .09 | 3 | 1.67 | .02 | .06 | 1 | 3 |
| L10+00W 14+75N | 1 | 28 | 5 | 63 | .1 | 51 | 11 | 557 | 3.18 | 9 | 5 | ND | 1 | 44 | .2 | 2 | 3 | 48 | .45 | .050 | 15 | 52 | .86 | 195 | .11 | 3 | 1.74 | .02 | .06 | 1 | 1 |
| L10+00W 14+50N | 1 | 32 | 3 | 84 | .1 | 57 | 13 | 554 | 4.04 | 4 | 5 | ND | 2 | 34 | .7 | 2 | 2 | 52 | .43 | .060 | 20 | 52 | .81 | 195 | .19 | 6 | 2.73 | .03 | .05 | 1 | 2 |
| L10+00W 14+25N A | 1 | 26 | 4 | 89 | .1 | 49 | 12 | 600 | 3.53 | 9 | 5 | ND | 1 | 47 | .2 | 2 | 2 | 53 | .52 | .058 | 13 | 60 | .95 | 179 | .11 | 5 | 1.93 | .02 | .07 | 1 | 5 |
| L10+00W 14+00N | 1 | 39 | 14 | 136 | .1 | 61 | 13 | 688 | 4.19 | 7 | 5 | ND | 1 | 60 | 1.0 | 2 | 2 | 56 | .73 | .078 | 20 | 64 | 1.00 | 383 | .09 | 2 | 3.06 | .02 | .09 | 1 | 3 |
| L10+00W 13+75N | 2 | 36 | 7 | 157 | .2 | 61 | 17 | 982 | 4.58 | 16 | 5 | ND | 1 | 48 | .2 | 3 | 2 | 64 | .43 | .080 | 11 | 66 | 1.04 | 268 | .05 | 3 | 2.61 | .01 | .11 | 1 | 1 |
| L10+00W 13+75N A | 1 | 36 | 6 | 125 | .1 | 52 | 15 | 822 | 4.43 | 7 | 5 | ND | 1 | 43 | .2 | 2 | 2 | 61 | .45 | .069 | 13 | 61 | .99 | 252 | .05 | 3 | 2.97 | .01 | .11 | 1 | 3 |
| L10+00W 13+50N | 1 | 28 | 2 | 98 | .1 | 43 | 11 | 579 | 3.69 | 9 | 5 | ND | 1 | 39 | .2 | 2 | 2 | 55 | .34 | .063 | 11 | 55 | .93 | 202 | .07 | 2 | 2.30 | .01 | .09 | 1 | 4 |
| L10+00W 13+50N A | 1 | 25 | 7 | 74 | .1 | 36 | 13 | 660 | 3.15 | 6 | 5 | ND | 1 | 40 | .2 | 2 | 2 | 48 | .41 | .060 | 12 | 47 | .84 | 149 | .10 | 2 | 1.57 | .02 | .06 | 1 | 1 |
| L10+00W 13+25N | 1 | 29 | 6 | 110 | .1 | 49 | 14 | 611 | 4.39 | 6 | 5 | ND | 1 | 28 | .2 | 3 | 2 | 60 | .21 | .048 | 12 | 55 | .94 | 190 | .07 | 2 | 2.78 | .01 | .09 | 1 | 4 |
| L10+00W 13+25N A | 1 | 22 | 6 | 72 | .1 | 35 | 12 | 610 | 3.04 | 2 | 5 | ND | 1 | 44 | .2 | 2 | 2 | 46 | .34 | .056 | 13 | 40 | .73 | 192 | .07 | 4 | 1.86 | .01 | .07 | 1 | 2 |
| L10+00W 13+00N | 1 | 33 | 7 | 114 | .4 | 34 | 11 | 401 | 4.13 | 8 | 5 | ND | 1 | 31 | .2 | 2 | 2 | 66 | .20 | .109 | 12 | 53 | .65 | 209 | .02 | 2 | 3.57 | .01 | .13 | 1 | 2 |
| L10+00W 13+00N A | 1 | 34 | 6 | 92 | .1 | 43 | 15 | 689 | 3.79 | 7 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 54 | .46 | .065 | 13 | 53 | .96 | 184 | .06 | 2 | 2.31 | .01 | .09 | 1 | 2 |
| L10+00W 12+75N | 1 | 27 | 11 | 81 | .1 | 47 | 13 | 610 | 3.49 | 7 | 5 | ND | 2 | 36 | .2 | 2 | 2 | 48 | .26 | .038 | 14 | 42 | .78 | 183 | .05 | 5 | 2.54 | .01 | .09 | 1 | 1 |
| L10+00W 12+75N A | 1 | 27 | 12 | 88 | .2 | 42 | 12 | 537 | 3.68 | 11 | 5 | ND | 2 | 33 | .2 | 2 | 2 | 54 | .22 | .036 | 13 | 45 | .76 | 186 | .06 | 2 | 2.61 | .01 | .09 | 1 | 2 |
| L10+00W 12+50N | 1 | 30 | 16 | 87 | .1 | 45 | 13 | 662 | 3.77 | 8 | 5 | ND | 1 | 56 | .2 | 2 | 2 | 53 | .36 | .053 | 16 | 43 | .76 | 209 | .10 | 2 | 2.53 | .02 | .10 | 1 | 5 |
| L10+00W 12+50N A | 1 | 31 | 12 | 128 | .1 | 47 | 14 | 614 | 5.42 | 2 | 5 | ND | 2 | 23 | .8 | 2 | 2 | 63 | .29 | .076 | 17 | 51 | .90 | 153 | .24 | 2 | 4.12 | .03 | .08 | 1 | 1 |
| L10+00W 12+25N | 1 | 28 | 10 | 92 | .1 | 49 | 14 | 658 | 4.70 | 4 | 5 | ND | 3 | 48 | .2 | 2 | 2 | 60 | .45 | .058 | 20 | 47 | .96 | 186 | .24 | 2 | 2.94 | .04 | .08 | 1 | 1 |
| L10+00W 12+25N A | 1 | 30 | 8 | 91 | .1 | 48 | 15 | 693 | 3.99 | 8 | 5 | ND | 2 | 45 | .2 | 2 | 2 | 54 | .39 | .065 | 16 | 46 | .90 | 184 | .15 | 2 | 2.65 | .03 | .09 | 1 | 5 |
| L10+00W 12+00N | 1 | 23 | 8 | 85 | .1 | 44 | 13 | 620 | 3.82 | 2 | 5 | ND | 2 | 36 | .2 | 2 | 2 | 52 | .29 | .043 | 15 | 49 | .89 | 201 | .12 | 2 | 2.44 | .02 | .07 | 1 | 11 |
| L10+00W 12+00N A | 1 | 24 | 13 | 81 | .1 | 40 | 12 | 693 | 3.19 | 6 | 5 | ND | 1 | 40 | .2 | 2 | 2 | 46 | .30 | .046 | 15 | 40 | .69 | 206 | .08 | 2 | 2.11 | .02 | .08 | 1 | 3 |
| L10+00W 11+75N | 1 | 24 | 15 | 67 | .1 | 35 | 11 | 565 | 2.91 | 2 | 5 | ND | 2 | 34 | .2 | 2 | 2 | 40 | .26 | .037 | 15 | 37 | .63 | 171 | .06 | 2 | 1.93 | .01 | .08 | 1 | 2 |
| L10+00W 11+75N A | 1 | 25 | 16 | 87 | .1 | 39 | 12 | 617 | 3.85 | 6 | 5 | ND | 1 | 35 | .2 | 2 | 2 | 54 | .30 | .055 | 14 | 45 | .76 | 179 | .12 | 2 | 2.38 | .02 | .08 | 1 | 5 |
| L10+00W 11+50N | 1 | 32 | 3 | 103 | .1 | 48 | 13 | 600 | 3.97 | 5 | 5 | ND | 1 | 34 | .2 | 2 | 2 | 53 | .26 | .050 | 17 | 48 | .80 | 222 | .08 | 4 | 2.65 | .01 | .09 | 1 | 3 |
| L10+00W 11+50N A | 1 | 25 | 10 | 81 | .1 | 35 | 11 | 638 | 3.06 | 4 | 5 | ND | 1 | 50 | .2 | 2 | 2 | 44 | .36 | .056 | 16 | 37 | .65 | 208 | .07 | 2 | 1.86 | .02 | .08 | 1 | 2 |
| L10+00W 11+25N | 1 | 28 | 6 | 108 | .2 | 48 | 11 | 469 | 3.88 | 6 | 5 | ND | 1 | 26 | .2 | 2 | 2 | 56 | .25 | .052 | 11 | 56 | .88 | 204 | .05 | 2 | 2.72 | .01 | .08 | 1 | 3 |
| L10+00W 11+25N A | 1 | 36 | 11 | 121 | .1 | 48 | 14 | 632 | 4.67 | 2 | 5 | ND | 1 | 26 | .2 | 2 | 2 | 59 | .24 | .066 | 14 | 57 | .85 | 188 | .06 | 2 | 2.83 | .01 | .07 | 1 | 2 |
| STANDARD C/AU-S | 18 | 60 | 44 | 132 | 7.1 | 69 | 29 | 1040 | 4.20 | 39 | 20 | 7 | 36 | 52 | 18.8 | 16 | 18 | 55 | .54 | .098 | 36 | 60 | .94 | 179 | .07 | 36 | 2.00 | .06 | .14 | 11 | 51 |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.

* SAMPLE TYPE: P1-P9 Soil P10 Stream Sed. AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE.

DATE RECEIVED: JUL 17 1990 DATE REPORT MAILED: July 23/90 SIGNED BY D.TOEY, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

Homestake International Minerals PROJECT 3174 KUTCHO FILE # 90-2567

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb |
|------------------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|-------|--------|--------|--------|--------|--------|--------|-------|------|------|--------|--------|------|--------|------|-------|------|------|-----|-------|----------|
| L10+00W 11+00N | 2 | 27 | 10 | 166 | .1 | 51 | 10 | 556 | 4.28 | 7 | 5 | ND | 1 | 35 | 6 | 2 | 2 | 54 | .37 | .091 | 20 | 48 | .63 | 288 | .08 | 2 | 3.21 | .02 | .07 | 2 | 6 |
| L10+00W 10+75N | 1 | 27 | 5 | 117 | .1 | 41 | 15 | 1366 | 4.74 | 11 | 5 | ND | 1 | 20 | .8 | 3 | 2 | 73 | .13 | .073 | 18 | 71 | .64 | 184 | .11 | 2 | 2.54 | .01 | .05 | 1 | 4 |
| L10+00W 10+50N | 2 | 22 | 17 | 79 | .1 | 41 | 13 | 545 | 4.01 | 9 | 5 | ND | 2 | 13 | .8 | 2 | 2 | 52 | .15 | .041 | 8 | 53 | .77 | 92 | .11 | 5 | 2.65 | .01 | .04 | 1 | 5 |
| L10+00W 10+25N | 1 | 70 | 14 | 76 | .1 | 55 | 30 | 1273 | 5.22 | 18 | 5 | ND | 1 | 22 | 7 | 2 | 2 | 61 | .31 | .097 | 9 | 80 | 1.25 | 120 | .10 | 2 | 2.08 | .01 | .05 | 1 | 7 |
| L10+00W 10+00N | 2 | 52 | 7 | 107 | .1 | 55 | 17 | 600 | 3.97 | 9 | 5 | ND | 1 | 26 | .2 | 2 | 3 | 57 | .28 | .065 | 16 | 67 | 1.07 | 199 | .07 | 3 | 2.56 | .01 | .05 | 1 | 10 |
| L10+00W 10+00N A | 2 | 40 | 4 | 102 | .1 | 49 | 16 | 732 | 3.83 | 5 | 5 | ND | 1 | 29 | .3 | 2 | 3 | 56 | .33 | .056 | 13 | 65 | 1.07 | 193 | .07 | 2 | 2.35 | .02 | .06 | 1 | 5 |
| L10+00W 9+75N | 2 | 11 | 15 | 40 | .2 | 9 | 4 | 139 | 2.28 | 5 | 5 | ND | 1 | 11 | .2 | 2 | 3 | 78 | .09 | .034 | 7 | 34 | .29 | 57 | .22 | 2 | 1.31 | .01 | .03 | 1 | 6 |
| L10+00W 9+75N A | 3 | 124 | 6 | 676 | .1 | 15 | 14 | 1614 | 6.25 | 17 | 5 | ND | 1 | 12 | 3.1 | 2 | 2 | 59 | .07 | .055 | 7 | 33 | .28 | 52 | .12 | 5 | 1.05 | .01 | .03 | 1 | 9 |
| L10+00W 9+50N | 2 | 73 | 7 | 186 | .6 | 69 | 21 | 2083 | 5.67 | 9 | 5 | ND | 1 | 27 | 1.2 | 2 | 2 | 59 | .59 | .208 | 22 | 80 | 1.09 | 300 | .02 | 2 | 3.67 | .01 | .08 | 1 | 1 |
| L10+00W 9+50N A | 2 | 46 | 5 | 144 | .1 | 38 | 18 | 3531 | 5.12 | 2 | 5 | ND | 1 | 28 | 1.4 | 2 | 3 | 66 | .56 | .133 | 31 | 44 | .78 | 254 | .08 | 2 | 2.56 | .02 | .06 | 1 | 7 |
| L10+00W 9+25N | 4 | 73 | 20 | 145 | .8 | 58 | 29 | 4295 | 5.41 | 6 | 5 | ND | 1 | 30 | 1.3 | 2 | 4 | 53 | .61 | .201 | 53 | 59 | .85 | 376 | .02 | 2 | 3.73 | .01 | .08 | 1 | 5 |
| L10+00W 9+25N A | 3 | 60 | 14 | 140 | .8 | 53 | 31 | 5816 | 5.13 | 4 | 5 | ND | 1 | 28 | .8 | 2 | 2 | 48 | .56 | .196 | 47 | 51 | .82 | 360 | .02 | 2 | 3.46 | .01 | .08 | 1 | 11 |
| L10+00W 9+00N | 2 | 35 | 2 | 72 | .1 | 30 | 13 | 563 | 3.54 | 5 | 5 | ND | 1 | 14 | .3 | 2 | 5 | 53 | .19 | .045 | 8 | 51 | .84 | 87 | .08 | 4 | 1.97 | .01 | .04 | 1 | 9 |
| L10+00W 9+00N A | 1 | 53 | 4 | 84 | .2 | 37 | 16 | 559 | 4.13 | 7 | 5 | ND | 1 | 13 | .7 | 3 | 3 | 51 | .21 | .047 | 8 | 53 | 1.02 | 74 | .10 | 5 | 1.93 | .01 | .04 | 1 | 7 |
| L10+00W 8+75N | 3 | 19 | 18 | 66 | .1 | 25 | 10 | 459 | 3.89 | 10 | 5 | ND | 1 | 12 | .2 | 2 | 2 | 51 | .11 | .070 | 10 | 41 | .44 | 85 | .07 | 2 | 2.16 | .01 | .04 | 1 | 11 |
| L10+00W 8+75N A | 1 | 18 | 8 | 79 | .1 | 35 | 10 | 437 | 3.84 | 3 | 5 | ND | 1 | 15 | .3 | 2 | 2 | 51 | .19 | .050 | 9 | 48 | .76 | 88 | .09 | 2 | 2.07 | .01 | .04 | 1 | 2 |
| L10+00W 8+50N | 1 | 34 | 6 | 77 | .2 | 44 | 12 | 407 | 4.30 | 9 | 5 | ND | 1 | 15 | 1.1 | 3 | 2 | 54 | .20 | .057 | 7 | 62 | .94 | 101 | .07 | 2 | 2.92 | .01 | .04 | 1 | 1 |
| L10+00W 8+50N A | 1 | 37 | 9 | 81 | .3 | 26 | 8 | 379 | 3.74 | 4 | 5 | ND | 1 | 20 | .2 | 2 | 2 | 50 | .16 | .079 | 11 | 46 | .53 | 140 | .04 | 2 | 2.35 | .01 | .04 | 1 | 1 |
| L10+00W 8+25N | 1 | 31 | 6 | 59 | .1 | 52 | 15 | 645 | 3.40 | 6 | 5 | ND | 1 | 29 | .7 | 2 | 2 | 55 | .38 | .043 | 10 | 66 | 1.09 | 137 | .12 | 3 | 1.81 | .02 | .04 | 1 | 3 |
| L10+00W 8+25N A | 1 | 21 | 15 | 70 | .1 | 43 | 10 | 378 | 3.91 | 8 | 5 | ND | 1 | 17 | .2 | 2 | 2 | 61 | .18 | .054 | 7 | 64 | .90 | 99 | .07 | 5 | 2.17 | .01 | .04 | 1 | 1 |
| L10+00W 8+00N | 1 | 27 | 7 | 61 | .1 | 46 | 14 | 612 | 3.36 | 4 | 5 | ND | 1 | 28 | .2 | 2 | 2 | 55 | .39 | .045 | 10 | 65 | 1.08 | 120 | .13 | 2 | 1.70 | .02 | .04 | 1 | 2 |
| L10+00W 8+00N A | 1 | 25 | 2 | 66 | .1 | 55 | 14 | 592 | 3.65 | 8 | 5 | ND | 1 | 27 | .4 | 4 | 2 | 59 | .27 | .035 | 9 | 67 | 1.05 | 144 | .09 | 2 | 2.24 | .01 | .04 | 1 | 12 |
| L10+00W 7+75N | 2 | 18 | 10 | 68 | .1 | 30 | 11 | 483 | 5.04 | 7 | 5 | ND | 1 | 10 | .9 | 2 | 2 | 99 | .12 | .041 | 6 | 69 | .75 | 59 | .21 | 2 | 1.81 | .01 | .04 | 1 | 1 |
| L10+00W 7+75N A | 1 | 35 | 5 | 103 | .1 | 53 | 13 | 515 | 4.19 | 6 | 5 | ND | 1 | 18 | .4 | 2 | 2 | 51 | .17 | .047 | 9 | 60 | .84 | 112 | .08 | 3 | 2.21 | .01 | .05 | 1 | 4 |
| L10+00W 7+50N | 4 | 22 | 11 | 81 | .3 | 30 | 9 | 319 | 4.74 | 7 | 6 | ND | 1 | 19 | .6 | 2 | 2 | 66 | .20 | .050 | 10 | 63 | .58 | 110 | .14 | 3 | 1.60 | .01 | .04 | 1 | 6 |
| L10+00W 7+50N A | 2 | 22 | 5 | 75 | .1 | 29 | 10 | 406 | 3.87 | 2 | 5 | ND | 1 | 20 | .4 | 2 | 2 | 65 | .25 | .050 | 9 | 56 | .79 | 99 | .15 | 3 | 1.67 | .02 | .04 | 1 | 1 |
| L10+00W 7+25N | 4 | 19 | 5 | 92 | .1 | 34 | 12 | 941 | 4.34 | 2 | 5 | ND | 1 | 17 | .5 | 2 | 2 | 67 | .14 | .055 | 10 | 78 | .70 | 125 | .10 | 2 | 1.68 | .01 | .05 | 1 | 4 |
| L10+00W 7+25N A | 2 | 25 | 13 | 106 | .1 | 49 | 17 | 933 | 4.18 | 7 | 5 | ND | 1 | 21 | .2 | 2 | 2 | 52 | .27 | .052 | 8 | 73 | 1.07 | 133 | .07 | 2 | 1.89 | .01 | .06 | 1 | 1 |
| L10+00W 7+00N | 1 | 54 | 3 | 118 | .1 | 82 | 16 | 371 | 3.40 | 7 | 5 | ND | 1 | 43 | .6 | 2 | 2 | 59 | .66 | .066 | 14 | 74 | 1.36 | 289 | .10 | 4 | 2.17 | .02 | .06 | 1 | 4 |
| L10+00W 6+75N | 1 | 44 | 13 | 79 | .1 | 68 | 16 | 565 | 3.66 | 4 | 5 | ND | 1 | 24 | .7 | 2 | 2 | 58 | .26 | .031 | 10 | 74 | 1.08 | 151 | .07 | 2 | 2.36 | .01 | .05 | 1 | 1 |
| L10+00W 6+50N | 1 | 57 | 13 | 86 | .1 | 73 | 17 | 725 | 4.04 | 9 | 5 | ND | 1 | 27 | .7 | 2 | 2 | 56 | .40 | .026 | 10 | 74 | 1.34 | 172 | .10 | 2 | 2.38 | .02 | .05 | 1 | 3 |
| L10+00W 6+25N | 1 | 60 | 8 | 120 | .1 | 61 | 16 | 887 | 4.54 | 8 | 5 | ND | 1 | 30 | .8 | 3 | 2 | 55 | .76 | .064 | 15 | 68 | 1.30 | 277 | .10 | 2 | 2.68 | .02 | .08 | 1 | 2 |
| L10+00W 6+00N | 1 | 24 | 7 | 70 | .1 | 54 | 13 | 462 | 3.79 | 4 | 5 | ND | 1 | 19 | .5 | 3 | 2 | 57 | .23 | .041 | 8 | 72 | 1.04 | 115 | .08 | 4 | 2.29 | .01 | .04 | 1 | 2 |
| L10+00W 5+75N | 1 | 79 | 9 | 156 | .1 | 94 | 19 | 1387 | 5.78 | 9 | 5 | ND | 2 | 37 | 2.7 | 2 | 2 | 62 | 1.01 | .082 | 30 | 64 | 1.31 | 307 | .30 | 2 | 3.27 | .05 | .07 | 1 | 1 |
| L9+80W 7+00N | 3 | 20 | 5 | 107 | .1 | 25 | 10 | 526 | 4.31 | 2 | 5 | ND | 1 | 14 | .4 | 2 | 2 | 67 | .17 | .042 | 10 | 60 | .53 | 110 | .14 | 2 | 1.38 | .01 | .05 | 1 | 10 |
| STANDARD C/AU-S | 19 | 61 | 37 | 132 | 7.1 | 73 | 31 | 1052 | 4.06 | 40 | 22 | 7 | 37 | 52 | 18.6 | 16 | 22 | 56 | .55 | .096 | 38 | 60 | .96 | 180 | .07 | 39 | 2.05 | .06 | .14 | 11 | 54 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|
| L8+00W 18+00N | 1 | 21 | 9 | 112 | .1 | 37 | 14 | 1155 | 3.20 | 8 | 5 | ND | 1 | 40 | .4 | 2 | 2 | 58 | .48 | .039 | 9 | 52 | 1.03 | 132 | .16 | 3 | 1.91 | .02 | .07 | 1 | 1 |
| L8+00W 17+75N | 1 | 29 | 9 | 123 | .2 | 40 | 12 | 722 | 3.91 | 12 | 5 | ND | 3 | 51 | .4 | 2 | 2 | 68 | .69 | .057 | 15 | 56 | 1.12 | 228 | .11 | 7 | 2.45 | .02 | .12 | 1 | 6 |
| L8+00W 17+50N | 1 | 34 | 10 | 157 | .2 | 53 | 13 | 608 | 4.73 | 15 | 5 | ND | 2 | 44 | .4 | 2 | 2 | 78 | .54 | .045 | 18 | 62 | 1.15 | 267 | .12 | 6 | 3.40 | .02 | .12 | 2 | 3 |
| L8+00W 17+25N | 1 | 27 | 10 | 145 | .1 | 47 | 13 | 675 | 4.18 | 10 | 5 | ND | 2 | 41 | .2 | 2 | 2 | 70 | .50 | .061 | 13 | 61 | 1.12 | 215 | .11 | 7 | 2.83 | .02 | .12 | 1 | 4 |
| L8+00W 17+00N | 1 | 51 | 12 | 149 | .2 | 56 | 15 | 711 | 4.53 | 10 | 5 | ND | 2 | 37 | .4 | 2 | 2 | 74 | .41 | .060 | 18 | 64 | 1.25 | 246 | .09 | 3 | 3.39 | .01 | .14 | 2 | 1 |
| L8+00W 16+75N | 1 | 36 | 12 | 194 | .3 | 51 | 18 | 1117 | 4.39 | 5 | 5 | ND | 3 | 51 | .7 | 2 | 2 | 71 | .57 | .066 | 15 | 65 | 1.23 | 245 | .09 | 8 | 3.05 | .02 | .16 | 2 | 4 |
| L8+00W 16+50N | 1 | 23 | 8 | 111 | .1 | 41 | 13 | 602 | 3.37 | 7 | 5 | ND | 3 | 45 | .4 | 3 | 3 | 61 | .52 | .051 | 12 | 58 | 1.08 | 154 | .16 | 10 | 2.03 | .03 | .09 | 1 | 6 |
| L8+00W 16+25N | 1 | 29 | 10 | 198 | .1 | 45 | 13 | 674 | 3.84 | 9 | 5 | ND | 2 | 42 | .8 | 3 | 2 | 62 | .59 | .053 | 15 | 58 | 1.10 | 180 | .10 | 9 | 2.55 | .02 | .12 | 1 | 3 |
| L8+00W 16+00N | 1 | 29 | 9 | 100 | .2 | 42 | 13 | 769 | 3.60 | 14 | 5 | ND | 4 | 49 | .5 | 2 | 2 | 59 | .54 | .040 | 13 | 52 | .95 | 190 | .12 | 9 | 1.93 | .02 | .12 | 1 | 5 |
| L8+00W 15+75N | 1 | 50 | 8 | 134 | .1 | 44 | 12 | 627 | 3.47 | 11 | 5 | ND | 2 | 52 | .4 | 2 | 2 | 59 | .73 | .056 | 20 | 57 | 1.07 | 184 | .13 | 3 | 2.23 | .02 | .10 | 1 | 4 |
| L8+00W 15+50N | 1 | 41 | 10 | 154 | .2 | 48 | 14 | 595 | 4.39 | 8 | 5 | ND | 2 | 49 | .4 | 2 | 2 | 66 | .68 | .058 | 23 | 59 | 1.13 | 236 | .08 | 2 | 2.88 | .02 | .13 | 1 | 4 |
| L8+00W 15+00N | 1 | 41 | 11 | 102 | .2 | 51 | 10 | 375 | 4.01 | 10 | 5 | ND | 2 | 57 | .3 | 2 | 2 | 68 | .71 | .080 | 19 | 71 | 1.14 | 333 | .05 | 6 | 3.62 | .02 | .13 | 2 | 5 |
| L8+00W 14+75N | 1 | 25 | 8 | 66 | .1 | 40 | 9 | 465 | 2.98 | 8 | 5 | ND | 2 | 55 | .2 | 3 | 2 | 54 | .45 | .048 | 15 | 56 | .94 | 189 | .14 | 3 | 1.79 | .02 | .07 | 1 | 2 |
| L8+00W 14+50N | 1 | 15 | 7 | 57 | .3 | 25 | 7 | 383 | 3.06 | 8 | 5 | ND | 2 | 19 | .2 | 2 | 2 | 53 | .23 | .049 | 7 | 47 | .69 | 86 | .13 | 3 | 1.98 | .01 | .06 | 1 | 6 |
| L8+00W 14+25N | 1 | 32 | 10 | 95 | .1 | 63 | 14 | 672 | 3.56 | 14 | 5 | ND | 2 | 43 | .3 | 2 | 2 | 61 | .50 | .056 | 16 | 70 | 1.03 | 219 | .09 | 9 | 2.13 | .02 | .10 | 1 | 19 |
| L8+00W 14+00N | 1 | 11 | 8 | 90 | .1 | 40 | 11 | 432 | 3.21 | 8 | 5 | ND | 4 | 50 | .2 | 3 | 3 | 55 | .67 | .063 | 11 | 61 | 1.01 | 157 | .15 | 3 | 1.86 | .02 | .09 | 1 | 11 |
| L8+00W 13+75N | 1 | 28 | 9 | 81 | .1 | 46 | 10 | 469 | 3.49 | 8 | 5 | ND | 3 | 53 | .2 | 2 | 4 | 59 | .66 | .055 | 18 | 60 | .91 | 246 | .16 | 2 | 2.40 | .02 | .09 | 1 | 5 |
| L8+00W 13+50N | 1 | 72 | 13 | 141 | .1 | 94 | 19 | 1199 | 4.84 | 23 | 5 | ND | 3 | 30 | .8 | 2 | 2 | 65 | .36 | .080 | 11 | 69 | 1.20 | 185 | .12 | 4 | 2.84 | .02 | .12 | 1 | 1 |
| L8+00W 13+25N | 1 | 44 | 10 | 116 | .1 | 61 | 19 | 849 | 5.75 | 19 | 5 | ND | 2 | 20 | .4 | 2 | 2 | 73 | .20 | .076 | 13 | 68 | .93 | 135 | .10 | 6 | 3.31 | .01 | .08 | 1 | 3 |
| L8+00W 13+00N | 1 | 26 | 11 | 71 | .3 | 33 | 8 | 323 | 3.52 | 8 | 5 | ND | 1 | 26 | .2 | 2 | 2 | 67 | .18 | .066 | 11 | 59 | .78 | 162 | .07 | 6 | 2.57 | .01 | .09 | 1 | 2 |
| L8+00W 12+75N | 1 | 19 | 12 | 71 | .1 | 28 | 7 | 311 | 2.89 | 4 | 5 | ND | 1 | 27 | .2 | 2 | 2 | 58 | .16 | .053 | 11 | 41 | .58 | 138 | .07 | 3 | 2.12 | .01 | .09 | 1 | 2 |
| L8+00W 12+50N | 1 | 22 | 12 | 73 | .3 | 34 | 8 | 323 | 3.49 | 7 | 5 | ND | 2 | 19 | .2 | 2 | 2 | 68 | .20 | .063 | 10 | 55 | .85 | 106 | .09 | 2 | 2.35 | .01 | .10 | 1 | 4 |
| L8+00W 12+25N | 1 | 25 | 11 | 82 | .2 | 42 | 12 | 492 | 3.42 | 2 | 5 | ND | 2 | 29 | .2 | 2 | 2 | 65 | .29 | .047 | 10 | 56 | .90 | 141 | .13 | 2 | 2.34 | .01 | .10 | 1 | 4 |
| L8+00W 12+00N | 1 | 42 | 13 | 103 | .1 | 59 | 13 | 650 | 4.19 | 16 | 5 | ND | 3 | 36 | .3 | 2 | 2 | 68 | .27 | .051 | 13 | 67 | 1.19 | 199 | .09 | 6 | 3.01 | .01 | .13 | 1 | 3 |
| L8+00W 11+75N | 1 | 30 | 10 | 86 | .2 | 40 | 10 | 415 | 3.83 | 11 | 5 | ND | 1 | 25 | .2 | 3 | 2 | 74 | .20 | .028 | 10 | 62 | .98 | 152 | .11 | 6 | 2.80 | .01 | .10 | 1 | 62 |
| L8+00W 11+50N | 1 | 30 | 12 | 90 | .3 | 47 | 13 | 553 | 3.82 | 4 | 5 | ND | 3 | 31 | .2 | 2 | 3 | 64 | .30 | .045 | 13 | 59 | .95 | 186 | .14 | 6 | 2.78 | .01 | .11 | 1 | 5 |
| L8+00W 11+25N | 1 | 28 | 13 | 75 | .3 | 41 | 12 | 544 | 3.17 | 7 | 8 | ND | 4 | 47 | .3 | 2 | 3 | 59 | .38 | .042 | 16 | 48 | .82 | 199 | .12 | 2 | 2.09 | .02 | .11 | 1 | 3 |
| L8+00W 11+00N | 1 | 29 | 11 | 104 | .6 | 46 | 15 | 647 | 4.29 | 9 | 5 | ND | 1 | 34 | .2 | 3 | 2 | 74 | .17 | .100 | 12 | 61 | .86 | 294 | .03 | 6 | 4.28 | .01 | .15 | 2 | 3 |
| L8+00W 10+75N | 1 | 22 | 12 | 63 | 1.1 | 29 | 5 | 150 | 3.91 | 16 | 5 | ND | 2 | 23 | .2 | 2 | 2 | 55 | .11 | .092 | 15 | 47 | .46 | 181 | .04 | 2 | 2.71 | .01 | .10 | 1 | 10 |
| L8+00W 10+50N | 1 | 35 | 10 | 84 | .1 | 49 | 9 | 326 | 3.19 | 7 | 5 | ND | 2 | 27 | .2 | 2 | 2 | 51 | .23 | .059 | 18 | 53 | .73 | 153 | .12 | 8 | 2.71 | .02 | .07 | 1 | 2 |
| L8+00W 10+25N | 1 | 18 | 8 | 56 | .1 | 36 | 8 | 323 | 2.68 | 9 | 5 | ND | 2 | 27 | .2 | 2 | 2 | 48 | .27 | .053 | 11 | 47 | .71 | 95 | .12 | 3 | 1.76 | .01 | .06 | 1 | 3 |
| L8+00W 10+00N | 1 | 32 | 14 | 89 | .6 | 36 | 7 | 254 | 3.59 | 13 | 5 | ND | 2 | 22 | .2 | 2 | 2 | 59 | .12 | .075 | 18 | 52 | .59 | 162 | .08 | 7 | 3.21 | .01 | .10 | 1 | 3 |
| L8+00W 9+75N | 1 | 22 | 14 | 71 | .2 | 33 | 9 | 372 | 2.77 | 3 | 5 | ND | 2 | 27 | .2 | 2 | 3 | 46 | .15 | .033 | 15 | 36 | .55 | 165 | .06 | 2 | 2.45 | .01 | .10 | 1 | 1 |
| L8+00W 9+50N | 1 | 15 | 11 | 48 | .1 | 25 | 7 | 376 | 1.98 | 4 | 5 | ND | 4 | 55 | .2 | 2 | 2 | 37 | .38 | .034 | 17 | 31 | .51 | 183 | .12 | 2 | 1.28 | .02 | .07 | 1 | 3 |
| L8+00W 9+25N | 1 | 21 | 16 | 85 | .2 | 38 | 16 | 1325 | 6.10 | 16 | 5 | ND | 2 | 20 | .2 | 2 | 2 | 104 | .19 | .131 | 13 | 72 | .93 | 111 | .15 | 2 | 2.52 | .01 | .07 | 1 | 5 |
| L8+00W 9+00N | 1 | 37 | 14 | 107 | .3 | 64 | 14 | 527 | 3.86 | 13 | 5 | ND | 3 | 38 | .5 | 3 | 2 | 62 | .39 | .063 | 13 | 79 | .92 | 217 | .07 | 9 | 3.17 | .02 | .12 | 1 | 1 |
| STANDARD C/AU-S | 18 | 58 | 41 | 132 | 7.3 | 72 | 29 | 1000 | 3.90 | 40 | 25 | 8 | 39 | 52 | 18.6 | 16 | 21 | 58 | .50 | .092 | 39 | 61 | .91 | 182 | .09 | 34 | 1.95 | .06 | .16 | 11 | 58 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|
| L8+00W 8+75N | 1 | 35 | 11 | 101 | .2 | 60 | 19 | 980 | 4.36 | 16 | 5 | ND | 2 | 23 | .4 | 2 | 2 | 60 | .21 | .083 | 11 | 70 | .85 | 148 | .09 | 3 | 3.03 | .01 | .07 | 1 | 4 |
| L8+00W 8+50N | 1 | 27 | 9 | 66 | .1 | 51 | 11 | 443 | 2.85 | 14 | 5 | ND | 4 | 29 | .3 | 2 | 3 | 50 | .25 | .049 | 12 | 52 | .81 | 161 | .10 | 2 | 1.98 | .01 | .07 | 1 | 2 |
| L8+00W 8+25N | 1 | 47 | 8 | 122 | .1 | 64 | 15 | 549 | 3.74 | 12 | 5 | ND | 3 | 41 | .3 | 2 | 2 | 65 | .66 | .062 | 14 | 73 | 1.27 | 188 | .11 | 4 | 2.32 | .02 | .11 | 1 | 4 |
| L8+00W 8+00N | 1 | 28 | 9 | 83 | .1 | 48 | 15 | 686 | 3.67 | 11 | 5 | ND | 3 | 24 | .2 | 2 | 2 | 62 | .34 | .064 | 10 | 69 | 1.19 | 99 | .15 | 2 | 2.10 | .01 | .07 | 1 | 3 |
| L8+00W 7+75N | 1 | 24 | 14 | 88 | .3 | 38 | 9 | 457 | 3.36 | 10 | 5 | ND | 4 | 20 | .3 | 2 | 2 | 46 | .12 | .058 | 15 | 38 | .61 | 139 | .03 | 2 | 2.63 | .01 | .11 | 1 | 24 |
| L8+00W 7+50N | 1 | 36 | 13 | 96 | .1 | 47 | 9 | 440 | 3.44 | 13 | 5 | ND | 3 | 30 | .3 | 2 | 2 | 52 | .19 | .036 | 16 | 43 | .79 | 193 | .04 | 2 | 2.87 | .01 | .12 | 1 | 5 |
| L8+00W 7+25N | 1 | 31 | 14 | 95 | .5 | 42 | 7 | 296 | 3.21 | 15 | 5 | ND | 3 | 33 | .3 | 2 | 2 | 54 | .32 | .093 | 15 | 51 | .70 | 247 | .01 | 2 | 3.60 | .01 | .11 | 1 | 3 |
| L4+50E 9+00N | 1 | 35 | 10 | 124 | .4 | 53 | 12 | 628 | 4.36 | 7 | 5 | ND | 3 | 20 | .3 | 2 | 2 | 67 | .21 | .049 | 11 | 62 | .93 | 138 | .11 | 2 | 2.63 | .01 | .11 | 1 | 3 |
| L4+50E 8+75N | 1 | 40 | 14 | 112 | .4 | 43 | 8 | 376 | 3.97 | 10 | 5 | ND | 3 | 20 | .3 | 2 | 2 | 69 | .16 | .087 | 21 | 61 | .74 | 224 | .06 | 2 | 3.42 | .01 | .14 | 1 | 1 |
| L4+50E 8+50N | 1 | 55 | 11 | 159 | .1 | 69 | 12 | 562 | 5.23 | 15 | 5 | ND | 3 | 21 | .4 | 2 | 2 | 62 | .18 | .080 | 28 | 63 | .86 | 273 | .10 | 2 | 4.30 | .02 | .13 | 1 | 2 |
| L4+50E 8+25N | 1 | 60 | 9 | 168 | .6 | 77 | 18 | 1573 | 5.44 | 5 | 10 | ND | 5 | 38 | .3 | 2 | 2 | 78 | .33 | .141 | 24 | 78 | 1.14 | 565 | .03 | 2 | 5.23 | .01 | .18 | 1 | 3 |
| L4+50E 8+00N | 1 | 43 | 9 | 113 | .2 | 58 | 10 | 580 | 4.07 | 8 | 5 | ND | 3 | 29 | .3 | 2 | 2 | 66 | .25 | .063 | 19 | 63 | 1.02 | 298 | .04 | 2 | 3.59 | .01 | .13 | 1 | 1 |
| L4+50E 7+75N | 1 | 46 | 9 | 112 | .3 | 54 | 10 | 608 | 3.69 | 8 | 5 | ND | 2 | 34 | .2 | 2 | 2 | 59 | .34 | .077 | 22 | 60 | 1.02 | 288 | .04 | 2 | 2.97 | .01 | .11 | 1 | 3 |
| L4+50E 7+50N | 1 | 54 | 11 | 153 | .1 | 69 | 11 | 595 | 4.87 | 10 | 5 | ND | 2 | 29 | .2 | 2 | 2 | 68 | .27 | .071 | 27 | 66 | 1.01 | 325 | .07 | 2 | 4.15 | .01 | .13 | 1 | 3 |
| L4+50E 7+25N | 1 | 56 | 12 | 150 | .1 | 69 | 11 | 541 | 4.75 | 9 | 5 | ND | 2 | 34 | .3 | 2 | 2 | 67 | .36 | .087 | 30 | 66 | 1.03 | 364 | .07 | 2 | 4.34 | .01 | .13 | 1 | 2 |
| L4+50E 7+00N | 1 | 45 | 13 | 131 | .1 | 62 | 11 | 632 | 4.53 | 9 | 5 | ND | 4 | 44 | .3 | 2 | 2 | 69 | .41 | .055 | 24 | 58 | .98 | 320 | .11 | 2 | 3.39 | .02 | .12 | 1 | 3 |
| L4+50E 6+75N | 1 | 56 | 13 | 131 | .3 | 68 | 10 | 464 | 4.56 | 11 | 5 | ND | 1 | 36 | .3 | 2 | 2 | 66 | .36 | .099 | 28 | 64 | .99 | 326 | .05 | 2 | 4.47 | .01 | .13 | 1 | 4 |
| L4+50E 6+50N | 1 | 39 | 12 | 138 | .1 | 66 | 10 | 527 | 4.44 | 9 | 5 | ND | 3 | 38 | .3 | 2 | 2 | 67 | .38 | .066 | 25 | 64 | 1.05 | 342 | .08 | 2 | 3.66 | .02 | .11 | 1 | 3 |
| L4+50E 6+25N | 2 | 59 | 10 | 156 | .1 | 87 | 14 | 837 | 5.14 | 13 | 5 | ND | 5 | 45 | .4 | 2 | 2 | 71 | .49 | .072 | 29 | 78 | 1.19 | 430 | .06 | 2 | 4.55 | .01 | .18 | 1 | 3 |
| L4+50E 6+00N | 1 | 32 | 10 | 116 | .1 | 62 | 11 | 549 | 3.86 | 12 | 5 | ND | 3 | 41 | .3 | 2 | 2 | 61 | .46 | .060 | 21 | 67 | 1.12 | 322 | .08 | 2 | 3.01 | .01 | .10 | 1 | 2 |
| L4+50E 5+75N | 1 | 86 | 8 | 76 | .9 | 48 | 8 | 465 | 3.64 | 2 | 5 | ND | 4 | 62 | .8 | 2 | 2 | 43 | .81 | .162 | 71 | 49 | .59 | 389 | .02 | 2 | 4.51 | .01 | .08 | 1 | 6 |
| L4+50E 5+25N | 1 | 37 | 9 | 120 | .2 | 63 | 11 | 566 | 4.00 | 7 | 5 | ND | 3 | 33 | .3 | 2 | 2 | 61 | .33 | .072 | 23 | 68 | 1.10 | 259 | .07 | 2 | 3.36 | .01 | .10 | 1 | 3 |
| L4+50E 5+00N | 1 | 33 | 9 | 104 | .2 | 59 | 12 | 552 | 4.06 | 9 | 5 | ND | 4 | 38 | .3 | 2 | 2 | 64 | .37 | .063 | 18 | 75 | 1.18 | 254 | .10 | 2 | 2.80 | .01 | .10 | 1 | 2 |
| L4+50E 4+75N | 1 | 34 | 9 | 111 | .1 | 60 | 12 | 661 | 4.08 | 10 | 5 | ND | 2 | 40 | .2 | 2 | 2 | 64 | .43 | .078 | 17 | 69 | 1.19 | 302 | .07 | 2 | 3.04 | .01 | .09 | 1 | 3 |
| L4+50E 4+50N | 1 | 32 | 9 | 136 | .1 | 61 | 11 | 530 | 4.15 | 9 | 5 | ND | 2 | 33 | .2 | 2 | 2 | 57 | .31 | .053 | 20 | 71 | 1.15 | 229 | .08 | 2 | 2.95 | .01 | .09 | 1 | 3 |
| L4+50E 4+25N | 1 | 45 | 11 | 128 | .2 | 68 | 11 | 531 | 4.73 | 11 | 5 | ND | 2 | 34 | .2 | 2 | 2 | 66 | .33 | .080 | 27 | 72 | 1.03 | 301 | .08 | 2 | 3.92 | .01 | .11 | 1 | 6 |
| L4+50E 4+00N A | 1 | 34 | 10 | 105 | .3 | 55 | 11 | 507 | 3.72 | 10 | 5 | ND | 4 | 32 | .2 | 2 | 2 | 65 | .30 | .044 | 12 | 71 | 1.03 | 163 | .12 | 2 | 2.52 | .01 | .10 | 1 | 2 |
| L4+50E 3+75N | 1 | 31 | 9 | 85 | .5 | 56 | 12 | 587 | 3.55 | 6 | 7 | ND | 5 | 33 | .2 | 2 | 2 | 57 | .33 | .057 | 14 | 68 | 1.13 | 133 | .12 | 2 | 2.15 | .02 | .10 | 1 | 1 |
| L4+50E 3+50N | 1 | 27 | 10 | 116 | .1 | 58 | 12 | 738 | 3.58 | 8 | 5 | ND | 1 | 47 | .3 | 2 | 2 | 56 | .50 | .071 | 16 | 67 | 1.13 | 299 | .06 | 2 | 2.62 | .01 | .09 | 1 | 4 |
| L4+50E 3+00N | 1 | 33 | 10 | 103 | .2 | 72 | 12 | 629 | 3.34 | 8 | 5 | ND | 2 | 47 | .2 | 2 | 2 | 53 | .55 | .063 | 16 | 66 | 1.08 | 288 | .07 | 2 | 2.40 | .01 | .07 | 1 | 5 |
| L4+50E 2+75N | 1 | 33 | 12 | 119 | .2 | 62 | 12 | 682 | 3.85 | 9 | 5 | ND | 2 | 44 | .2 | 2 | 2 | 59 | .52 | .067 | 18 | 69 | 1.11 | 308 | .07 | 2 | 2.88 | .01 | .10 | 1 | 3 |
| L4+50E 2+50N | 1 | 33 | 10 | 115 | .3 | 68 | 12 | 633 | 3.88 | 4 | 5 | ND | 3 | 46 | .2 | 2 | 2 | 60 | .54 | .070 | 20 | 71 | 1.14 | 302 | .10 | 2 | 2.89 | .01 | .10 | 1 | 4 |
| L4+50E 2+25N | 1 | 33 | 10 | 92 | .2 | 56 | 12 | 587 | 3.39 | 8 | 5 | ND | 2 | 38 | .2 | 2 | 2 | 56 | .38 | .071 | 13 | 66 | 1.04 | 238 | .08 | 2 | 2.40 | .01 | .08 | 1 | 3 |
| L4+50E 2+00N | 1 | 30 | 8 | 79 | .1 | 45 | 12 | 620 | 3.18 | 10 | 5 | ND | 1 | 30 | .2 | 2 | 2 | 56 | .29 | .060 | 10 | 59 | .91 | 143 | .08 | 2 | 1.95 | .01 | .07 | 1 | 3 |
| L4+50E 1+75N | 2 | 38 | 9 | 168 | .3 | 62 | 15 | 857 | 4.57 | 11 | 8 | ND | 2 | 21 | .2 | 2 | 2 | 62 | .16 | .058 | 10 | 71 | 1.10 | 194 | .04 | 2 | 3.23 | .01 | .12 | 1 | 4 |
| L4+50E 1+25N A | 1 | 46 | 8 | 83 | .3 | 73 | 15 | 821 | 3.61 | 7 | 5 | ND | 4 | 52 | .2 | 2 | 2 | 58 | .58 | .063 | 13 | 70 | 1.24 | 214 | .10 | 2 | 2.08 | .02 | .12 | 1 | 4 |
| STANDARD C/AU-S | 18 | 59 | 41 | 137 | 7.3 | 72 | 28 | 1000 | 3.91 | 37 | 16 | 7 | 40 | 52 | 18.6 | 15 | 19 | 58 | .50 | .093 | 39 | 60 | .91 | 182 | .09 | 35 | 1.95 | .06 | .13 | 13 | 51 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb |
|------------------|--------|--------|--------|--------|--------|--------|--------|--------|------|--------|-------|--------|--------|--------|--------|--------|--------|-------|------|------|--------|--------|------|--------|------|-------|------|------|-----|-------|----------|
| L4+50E 1+00N A | 3 | 49 | 13 | 122 | .1 | 68 | 18 | 1555 | 4.38 | 10 | 5 | ND | 4 | 46 | .5 | 3 | 2 | 67 | .60 | .076 | 22 | 71 | 1.03 | 333 | .09 | 4 | 3.53 | .02 | .12 | 1 | 8 |
| L4+50E 0+75N | 2 | 38 | 12 | 94 | .1 | 76 | 13 | 598 | 4.17 | 3 | 5 | ND | 4 | 44 | .2 | 2 | 4 | 59 | .56 | .065 | 24 | 63 | .99 | 242 | .22 | 4 | 2.91 | .02 | .11 | 1 | 5 |
| L4+50E 0+50N | 1 | 36 | 8 | 87 | .1 | 67 | 14 | 876 | 3.70 | 5 | 5 | ND | 4 | 47 | .3 | 2 | 2 | 59 | .52 | .064 | 17 | 69 | 1.09 | 243 | .11 | 2 | 2.41 | .01 | .11 | 1 | 4 |
| L4+50E 0+25N A | 1 | 31 | 9 | 95 | .3 | 58 | 12 | 614 | 3.86 | 9 | 6 | ND | 4 | 43 | .3 | 3 | 2 | 61 | .51 | .060 | 17 | 70 | 1.05 | 253 | .12 | 6 | 2.49 | .01 | .12 | 1 | 4 |
| L4+50E 0+00S | 1 | 26 | 12 | 74 | .1 | 52 | 12 | 683 | 3.29 | 6 | 5 | ND | 5 | 55 | .4 | 2 | 4 | 56 | .50 | .052 | 16 | 58 | .93 | 244 | .13 | 3 | 2.06 | .02 | .11 | 1 | 5 |
| L4+50E 0+25S A | 1 | 43 | 13 | 116 | .1 | 72 | 13 | 728 | 4.31 | 9 | 5 | ND | 4 | 49 | .3 | 2 | 2 | 59 | .49 | .067 | 31 | 68 | 1.04 | 340 | .11 | 7 | 3.07 | .02 | .14 | 1 | 4 |
| L4+50E 0+50S | 1 | 24 | 7 | 84 | .2 | 52 | 13 | 573 | 3.68 | 5 | 6 | ND | 3 | 32 | .2 | 2 | 2 | 62 | .30 | .052 | 11 | 67 | 1.19 | 122 | .12 | 2 | 2.28 | .01 | .11 | 1 | 4 |
| L4+50E 0+75S | 1 | 33 | 9 | 119 | .4 | 55 | 13 | 626 | 3.58 | 4 | 6 | ND | 4 | 40 | .3 | 3 | 3 | 59 | .47 | .065 | 12 | 71 | 1.18 | 220 | .11 | 5 | 2.34 | .02 | .13 | 1 | 1 |
| L4+50E 1+00S | 1 | 45 | 10 | 105 | .1 | 77 | 18 | 1147 | 4.54 | 6 | 5 | ND | 1 | 45 | .4 | 2 | 2 | 74 | .45 | .063 | 19 | 87 | 1.24 | 349 | .10 | 5 | 3.30 | .01 | .12 | 1 | 2 |
| L4+50E 1+25S | 1 | 34 | 12 | 98 | .1 | 64 | 15 | 577 | 4.08 | 5 | 5 | ND | 4 | 33 | .3 | 2 | 4 | 65 | .30 | .065 | 19 | 76 | 1.08 | 212 | .17 | 5 | 2.91 | .01 | .09 | 1 | 4 |
| L4+50E 1+50S | 1 | 38 | 10 | 103 | .1 | 65 | 13 | 668 | 3.72 | 2 | 5 | ND | 2 | 31 | .3 | 2 | 2 | 61 | .31 | .074 | 21 | 74 | 1.05 | 247 | .10 | 7 | 3.24 | .01 | .11 | 1 | 1 |
| L4+50E 1+75S | 1 | 37 | 11 | 112 | .1 | 70 | 13 | 623 | 3.95 | 2 | 5 | ND | 2 | 39 | .2 | 2 | 2 | 63 | .39 | .068 | 16 | 76 | 1.07 | 340 | .10 | 4 | 3.20 | .01 | .12 | 1 | 1 |
| L4+50E 2+00S | 1 | 49 | 13 | 111 | .2 | 82 | 15 | 797 | 4.44 | 3 | 6 | ND | 5 | 42 | .3 | 2 | 6 | 65 | .40 | .052 | 19 | 79 | 1.13 | 321 | .16 | 2 | 3.08 | .01 | .14 | 1 | 5 |
| L4+50E 2+25S | 1 | 43 | 10 | 87 | .1 | 72 | 15 | 602 | 4.01 | 2 | 5 | ND | 6 | 39 | .3 | 2 | 3 | 63 | .40 | .058 | 19 | 82 | 1.14 | 184 | .20 | 5 | 2.55 | .01 | .12 | 1 | 5 |
| L4+50E 2+50S | 1 | 44 | 11 | 94 | .4 | 73 | 19 | 785 | 4.00 | 8 | 8 | ND | 5 | 29 | .3 | 2 | 3 | 66 | .34 | .070 | 12 | 80 | 1.26 | 126 | .14 | 2 | 2.84 | .01 | .14 | 1 | 4 |
| L4+50E 2+75S | 1 | 39 | 9 | 110 | .3 | 65 | 15 | 645 | 3.94 | 3 | 6 | ND | 4 | 29 | .2 | 2 | 3 | 62 | .29 | .058 | 19 | 74 | 1.00 | 221 | .13 | 3 | 2.86 | .01 | .11 | 1 | 3 |
| L4+50E 3+00S A | 1 | 43 | 12 | 104 | .1 | 71 | 14 | 477 | 3.61 | 5 | 5 | ND | 4 | 35 | .3 | 4 | 4 | 64 | .35 | .067 | 32 | 76 | 1.03 | 308 | .12 | 3 | 3.04 | .01 | .11 | 1 | 7 |
| L4+50E 3+25S | 1 | 34 | 9 | 90 | .1 | 56 | 12 | 509 | 3.46 | 5 | 5 | ND | 2 | 41 | .2 | 2 | 3 | 58 | .42 | .058 | 15 | 68 | 1.11 | 202 | .11 | 3 | 2.44 | .01 | .10 | 1 | 1 |
| L4+50E 3+25S A | 1 | 49 | 9 | 109 | .2 | 82 | 14 | 664 | 4.13 | 7 | 5 | ND | 3 | 45 | .3 | 2 | 2 | 62 | .49 | .083 | 23 | 77 | 1.08 | 301 | .14 | 4 | 3.02 | .02 | .12 | 1 | 2 |
| L4+50E 3+50S | 1 | 48 | 9 | 81 | .1 | 83 | 17 | 672 | 3.64 | 12 | 5 | ND | 2 | 32 | .2 | 2 | 2 | 60 | .35 | .066 | 16 | 82 | 1.14 | 179 | .12 | 4 | 2.33 | .01 | .09 | 1 | 5 |
| L4+50E 3+75S | 1 | 51 | 8 | 70 | .2 | 86 | 16 | 664 | 3.54 | 11 | 5 | ND | 4 | 41 | .3 | 2 | 3 | 60 | .43 | .055 | 15 | 87 | 1.29 | 200 | .12 | 7 | 2.21 | .01 | .10 | 1 | 8 |
| L4+50E 4+00S | 1 | 39 | 9 | 104 | .2 | 77 | 14 | 700 | 3.72 | 2 | 5 | ND | 2 | 38 | .3 | 3 | 4 | 62 | .39 | .100 | 14 | 97 | 1.29 | 258 | .07 | 2 | 2.90 | .01 | .11 | 1 | 1 |
| L4+50E 4+25S | 1 | 64 | 10 | 145 | .1 | 119 | 18 | 847 | 5.02 | 5 | 5 | ND | 3 | 32 | .4 | 2 | 2 | 83 | .23 | .150 | 19 | 128 | 1.66 | 501 | .05 | 4 | 4.42 | .01 | .17 | 1 | 4 |
| L4+50E 4+50S | 1 | 64 | 10 | 75 | .1 | 106 | 16 | 605 | 4.14 | 5 | 5 | ND | 4 | 30 | .2 | 2 | 4 | 61 | .35 | .053 | 19 | 101 | 1.31 | 197 | .18 | 3 | 3.00 | .01 | .11 | 1 | 3 |
| L4+50E 4+75S | 1 | 32 | 11 | 80 | .4 | 72 | 26 | 1268 | 5.23 | 14 | 6 | ND | 4 | 22 | .3 | 4 | 5 | 75 | .27 | .082 | 10 | 87 | 1.17 | 103 | .18 | 5 | 2.29 | .01 | .08 | 1 | 5 |
| L4+50E 5+00S B | 1 | 31 | 9 | 64 | .2 | 62 | 13 | 603 | 3.51 | 7 | 5 | ND | 3 | 21 | .2 | 2 | 3 | 55 | .28 | .063 | 11 | 66 | 1.01 | 77 | .19 | 11 | 1.98 | .01 | .07 | 1 | 6 |
| L4+50E 5+00S C | 1 | 49 | 10 | 81 | .3 | 88 | 20 | 1069 | 3.67 | 12 | 7 | ND | 5 | 26 | .2 | 3 | 4 | 57 | .34 | .069 | 12 | 83 | 1.31 | 98 | .14 | 4 | 2.24 | .01 | .10 | 1 | 1 |
| L4+50E 5+25S | 1 | 32 | 11 | 63 | .1 | 62 | 19 | 1206 | 5.04 | 26 | 5 | ND | 3 | 19 | .2 | 2 | 2 | 77 | .24 | .074 | 9 | 78 | 1.10 | 89 | .19 | 2 | 1.87 | .01 | .05 | 1 | 1 |
| L4+50E 5+50S | 1 | 54 | 8 | 123 | .1 | 84 | 18 | 778 | 6.89 | 2 | 5 | ND | 4 | 13 | .2 | 2 | 2 | 80 | .28 | .063 | 23 | 80 | 1.32 | 102 | .42 | 5 | 4.98 | .03 | .08 | 1 | 1 |
| L4+50E 5+75S 'B' | 2 | 23 | 12 | 93 | .1 | 36 | 9 | 412 | 6.03 | 2 | 5 | ND | 5 | 11 | .2 | 2 | 7 | 81 | .13 | .058 | 21 | 62 | .55 | 87 | .50 | 4 | 3.53 | .02 | .06 | 1 | 3 |
| L4+50E 5+75S 'C' | 1 | 31 | 9 | 88 | .2 | 78 | 19 | 719 | 4.38 | 4 | 5 | ND | 4 | 23 | .2 | 2 | 2 | 63 | .28 | .052 | 16 | 86 | 1.46 | 99 | .24 | 6 | 3.00 | .01 | .06 | 1 | 4 |
| L4+50E 6+00S | 2 | 24 | 15 | 119 | .1 | 41 | 12 | 662 | 5.88 | 2 | 5 | ND | 6 | 9 | .2 | 6 | 3 | 56 | .24 | .076 | 34 | 45 | .73 | 80 | .36 | 2 | 5.76 | .04 | .07 | 1 | 1 |
| L4+50E 6+25S | 1 | 50 | 11 | 88 | .1 | 86 | 20 | 847 | 5.15 | 11 | 5 | ND | 5 | 21 | .2 | 2 | 2 | 67 | .31 | .055 | 22 | 79 | 1.53 | 112 | .35 | 6 | 3.61 | .03 | .08 | 1 | 2 |
| L4+50E 6+50S | 1 | 78 | 10 | 107 | .2 | 110 | 18 | 805 | 5.56 | 4 | 5 | ND | 6 | 31 | .3 | 4 | 6 | 65 | .38 | .066 | 38 | 78 | 1.25 | 230 | .28 | 3 | 4.74 | .02 | .11 | 1 | 2 |
| L4+50E 6+75S | 2 | 34 | 13 | 101 | .2 | 48 | 14 | 950 | 4.81 | 9 | 5 | ND | 2 | 15 | .2 | 2 | 4 | 56 | .16 | .083 | 20 | 55 | .61 | 90 | .26 | 2 | 3.07 | .01 | .05 | 1 | 4 |
| L4+50E 7+00S | 2 | 74 | 12 | 167 | .1 | 63 | 10 | 1282 | 5.53 | 11 | 5 | ND | 3 | 93 | .3 | 2 | 2 | 56 | 1.07 | .135 | 56 | 68 | .61 | 327 | .18 | 5 | 3.85 | .02 | .08 | 1 | 3 |
| STANDARD C/AU-S | 18 | 58 | 41 | 137 | 7.3 | 73 | 30 | 1006 | 3.92 | 40 | 16 | 8 | 39 | 52 | 18.7 | 16 | 23 | 59 | .50 | .093 | 40 | 61 | .92 | 183 | .09 | 35 | 1.95 | .06 | .13 | 11 | 48 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|
| L4+50E 7+50S | 1 | 111 | 9 | 149 | .1 | 83 | 17 | 570 | 3.96 | 17 | 5 | ND | 4 | 72 | .6 | 2 | 2 | 55 | 1.07 | .074 | 31 | 66 | .87 | 370 | .24 | 3 | 3.47 | .03 | .08 | 2 | 18 |
| L9+50E 0+00N | 1 | 33 | 5 | 89 | .1 | 54 | 18 | 1452 | 5.43 | 9 | 5 | ND | 2 | 52 | .3 | 2 | 2 | 52 | .69 | .067 | 15 | 54 | .81 | 254 | .06 | 3 | 1.66 | .02 | .07 | 1 | 7 |
| L10+50E 10+00N | 1 | 32 | 6 | 93 | .1 | 55 | 13 | 507 | 3.89 | 9 | 5 | ND | 2 | 24 | .2 | 2 | 2 | 67 | .21 | .054 | 9 | 71 | 1.05 | 117 | .10 | 3 | 2.27 | .01 | .10 | 1 | 3 |
| L10+50E 9+75N | 1 | 59 | 10 | 95 | .1 | 68 | 18 | 930 | 3.65 | 8 | 5 | ND | 5 | 100 | .4 | 2 | 2 | 58 | .70 | .054 | 18 | 64 | 1.29 | 294 | .09 | 3 | 2.54 | .03 | .19 | 1 | 4 |
| L10+50E 9+50N | 1 | 35 | 9 | 85 | .1 | 51 | 17 | 811 | 3.22 | 7 | 5 | ND | 3 | 50 | .2 | 2 | 2 | 56 | .40 | .038 | 14 | 65 | 1.10 | 206 | .13 | 2 | 2.05 | .03 | .10 | 1 | 2 |
| L10+50E 9+25N | 1 | 47 | 9 | 91 | .1 | 67 | 14 | 603 | 3.69 | 5 | 5 | ND | 3 | 26 | .2 | 2 | 2 | 57 | .22 | .055 | 15 | 65 | .99 | 152 | .12 | 2 | 2.67 | .01 | .09 | 1 | 2 |
| L10+50E 9+00N | 1 | 33 | 5 | 73 | .1 | 56 | 15 | 629 | 3.29 | 10 | 5 | ND | 3 | 30 | .2 | 2 | 2 | 57 | .31 | .055 | 10 | 65 | 1.11 | 104 | .12 | 3 | 1.97 | .02 | .07 | 1 | 2 |
| L10+50E 8+75N | 1 | 51 | 9 | 104 | .1 | 84 | 15 | 494 | 3.78 | 6 | 5 | ND | 2 | 40 | .3 | 2 | 2 | 61 | .37 | .040 | 17 | 78 | 1.30 | 205 | .09 | 5 | 3.12 | .02 | .11 | 1 | 1 |
| L10+50E 8+50N | 1 | 36 | 10 | 92 | .2 | 54 | 10 | 481 | 4.64 | 10 | 8 | ND | 3 | 21 | .2 | 2 | 2 | 54 | .21 | .086 | 10 | 66 | .76 | 106 | .06 | 4 | 3.00 | .01 | .09 | 2 | 1 |
| L10+50E 8+25N | 1 | 40 | 6 | 106 | .1 | 62 | 18 | 748 | 4.23 | 6 | 5 | ND | 2 | 23 | .2 | 2 | 2 | 68 | .29 | .056 | 9 | 75 | 1.40 | 102 | .11 | 4 | 2.98 | .01 | .07 | 1 | 2 |
| L10+50E 8+00N | 1 | 27 | 7 | 96 | .1 | 49 | 11 | 550 | 3.78 | 6 | 5 | ND | 1 | 29 | .3 | 2 | 2 | 71 | .25 | .040 | 12 | 62 | 1.00 | 190 | .11 | 3 | 2.35 | .01 | .07 | 1 | 4 |
| L10+50E 7+75N | 1 | 20 | 11 | 98 | .1 | 44 | 12 | 585 | 4.10 | 6 | 5 | ND | 2 | 18 | .2 | 2 | 2 | 80 | .14 | .068 | 11 | 66 | .91 | 104 | .12 | 3 | 2.07 | .01 | .09 | 1 | 1 |
| L10+50E 7+50N | 1 | 20 | 8 | 74 | .1 | 31 | 8 | 434 | 2.82 | 2 | 5 | ND | 2 | 28 | .2 | 2 | 2 | 60 | .22 | .058 | 9 | 53 | .82 | 170 | .05 | 2 | 2.24 | .01 | .10 | 1 | 3 |
| L10+50E 7+25N | 1 | 34 | 7 | 165 | .1 | 76 | 12 | 595 | 3.84 | 4 | 5 | ND | 3 | 54 | .3 | 2 | 2 | 60 | .60 | .100 | 20 | 73 | 1.17 | 394 | .05 | 3 | 3.64 | .02 | .12 | 1 | 2 |
| L10+50E 7+00N | 1 | 21 | 7 | 85 | .1 | 46 | 12 | 459 | 3.04 | 6 | 5 | ND | 3 | 42 | .2 | 2 | 2 | 53 | .44 | .039 | 13 | 58 | 1.14 | 178 | .10 | 4 | 2.00 | .02 | .08 | 1 | 42 |
| L10+50E 6+75N | 1 | 31 | 9 | 105 | .1 | 60 | 17 | 927 | 3.70 | 7 | 5 | ND | 2 | 40 | .4 | 2 | 2 | 62 | .47 | .062 | 16 | 64 | 1.06 | 311 | .07 | 2 | 2.97 | .02 | .10 | 1 | 3 |
| L10+50E 6+50N | 1 | 47 | 10 | 116 | .1 | 97 | 15 | 653 | 4.53 | 7 | 5 | ND | 4 | 41 | .2 | 2 | 2 | 66 | .47 | .049 | 21 | 76 | 1.13 | 273 | .18 | 2 | 2.97 | .02 | .12 | 1 | 2 |
| L10+50E 6+25N | 1 | 33 | 9 | 100 | .1 | 81 | 14 | 551 | 4.15 | 2 | 5 | ND | 4 | 47 | .2 | 2 | 2 | 66 | .53 | .066 | 20 | 83 | 1.35 | 216 | .15 | 3 | 2.65 | .02 | .11 | 1 | 3 |
| L10+50E 6+00N | 1 | 34 | 8 | 103 | .1 | 82 | 13 | 447 | 3.85 | 2 | 5 | ND | 3 | 39 | .2 | 2 | 2 | 59 | .43 | .062 | 22 | 77 | 1.13 | 223 | .13 | 4 | 2.99 | .02 | .09 | 1 | 11 |
| L10+50E 5+75N | 1 | 33 | 11 | 105 | .1 | 75 | 12 | 499 | 4.14 | 2 | 5 | ND | 3 | 40 | .2 | 2 | 2 | 63 | .47 | .053 | 23 | 63 | 1.02 | 255 | .13 | 3 | 3.09 | .02 | .11 | 1 | 3 |
| L10+50E 5+50N | 1 | 29 | 9 | 83 | .1 | 74 | 14 | 554 | 3.52 | 2 | 5 | ND | 3 | 42 | .2 | 2 | 2 | 58 | .41 | .053 | 14 | 79 | 1.27 | 164 | .16 | 3 | 2.08 | .02 | .09 | 1 | 3 |
| L10+50E 5+25N A | 1 | 34 | 6 | 88 | .1 | 97 | 15 | 578 | 3.69 | 8 | 5 | ND | 4 | 49 | .2 | 2 | 2 | 60 | .48 | .054 | 18 | 90 | 1.34 | 242 | .13 | 4 | 2.46 | .02 | .09 | 1 | 21 |
| L10+50E 5+00N A | 1 | 33 | 10 | 126 | .1 | 124 | 15 | 426 | 4.07 | 3 | 5 | ND | 4 | 39 | .2 | 2 | 2 | 60 | .61 | .057 | 17 | 82 | 1.43 | 265 | .20 | 4 | 2.81 | .02 | .10 | 2 | 4 |
| L10+50E 4+75N | 1 | 32 | 8 | 99 | .1 | 78 | 14 | 589 | 3.77 | 6 | 5 | ND | 2 | 45 | .2 | 2 | 2 | 58 | .55 | .070 | 17 | 78 | 1.26 | 227 | .13 | 4 | 2.60 | .02 | .09 | 1 | 4 |
| L10+50E 4+50N | 1 | 32 | 8 | 85 | .1 | 73 | 13 | 440 | 3.60 | 4 | 5 | ND | 3 | 36 | .2 | 2 | 2 | 56 | .38 | .043 | 16 | 70 | 1.21 | 164 | .16 | 13 | 2.47 | .02 | .08 | 1 | 4 |
| L10+50E 4+25N | 1 | 37 | 9 | 102 | .1 | 79 | 13 | 566 | 4.14 | 4 | 5 | ND | 3 | 41 | .2 | 2 | 2 | 61 | .38 | .045 | 18 | 68 | 1.09 | 249 | .12 | 3 | 2.88 | .02 | .10 | 1 | 2 |
| L10+50E 4+00N | 1 | 20 | 7 | 79 | .1 | 69 | 14 | 563 | 3.29 | 2 | 5 | ND | 3 | 40 | .2 | 2 | 2 | 56 | .41 | .031 | 11 | 76 | 1.24 | 457 | .16 | 4 | 1.83 | .02 | .08 | 1 | 1 |
| L10+50E 3+75N | 1 | 18 | 8 | 102 | .1 | 67 | 12 | 484 | 3.46 | 6 | 5 | ND | 3 | 44 | .2 | 2 | 2 | 57 | .44 | .044 | 13 | 78 | 1.16 | 191 | .13 | 3 | 2.24 | .02 | .10 | 1 | 2 |
| L10+50E 3+50N | 1 | 22 | 7 | 81 | .1 | 61 | 12 | 467 | 3.06 | 5 | 5 | ND | 2 | 52 | .2 | 2 | 2 | 53 | .48 | .044 | 14 | 67 | 1.09 | 202 | .12 | 2 | 2.00 | .02 | .07 | 1 | 1 |
| L10+50E 3+25N | 1 | 27 | 8 | 111 | .1 | 74 | 14 | 467 | 3.56 | 4 | 5 | ND | 3 | 54 | .2 | 2 | 2 | 59 | .77 | .072 | 18 | 75 | 1.31 | 230 | .10 | 4 | 2.43 | .02 | .10 | 1 | 20 |
| L10+50E 3+00N | 1 | 33 | 9 | 115 | .1 | 76 | 12 | 567 | 3.82 | 5 | 5 | ND | 2 | 49 | .2 | 2 | 2 | 62 | .54 | .067 | 13 | 77 | 1.24 | 258 | .09 | 4 | 2.64 | .02 | .11 | 1 | 3 |
| L10+50E 2+75N | 1 | 34 | 8 | 145 | .1 | 91 | 14 | 511 | 3.68 | 2 | 5 | ND | 2 | 57 | .2 | 2 | 2 | 58 | .71 | .077 | 18 | 83 | 1.35 | 334 | .06 | 7 | 3.08 | .02 | .11 | 1 | 2 |
| L10+50E 2+50N | 1 | 24 | 8 | 96 | .1 | 75 | 15 | 801 | 3.70 | 2 | 5 | ND | 3 | 48 | .2 | 2 | 2 | 62 | .54 | .059 | 16 | 78 | 1.34 | 201 | .15 | 5 | 2.16 | .02 | .08 | 1 | 3 |
| L10+50E 2+25N | 1 | 29 | 7 | 68 | .1 | 72 | 16 | 675 | 3.14 | 3 | 5 | ND | 4 | 57 | .2 | 2 | 2 | 54 | .45 | .064 | 17 | 72 | 1.04 | 196 | .15 | 5 | 1.58 | .04 | .09 | 1 | 3 |
| L10+50E 2+00N | 1 | 38 | 8 | 84 | .2 | 77 | 22 | 934 | 4.08 | 3 | 5 | ND | 2 | 38 | .2 | 2 | 2 | 63 | .32 | .068 | 10 | 91 | 1.18 | 202 | .07 | 2 | 2.09 | .01 | .10 | 1 | 2 |
| L10+50E 1+75N | 1 | 34 | 10 | 130 | .1 | 70 | 15 | 698 | 4.33 | 8 | 5 | ND | 2 | 33 | .2 | 2 | 2 | 68 | .27 | .052 | 13 | 81 | 1.33 | 193 | .08 | 5 | 2.66 | .02 | .11 | 1 | 2 |
| STANDARD C/AU-S | 18 | 57 | 38 | 132 | 7.3 | 72 | 31 | 1010 | 3.95 | 39 | 20 | 7 | 40 | 52 | 18.4 | 16 | 20 | 57 | .50 | .091 | 39 | 59 | .92 | 182 | .09 | 34 | 1.95 | .06 | .13 | 11 | 50 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|
| L10+50E 1+50N | 1 | 23 | 7 | 72 | .1 | 60 | 16 | 706 | 3.10 | 9 | 5 | ND | 2 | 38 | .2 | 2 | 2 | 52 | .39 | .054 | 12 | 62 | 1.01 | 148 | .14 | 3 | 1.60 | .02 | .06 | 1 | 1 |
| L10+50E 1+25N | 1 | 19 | 7 | 63 | .1 | 45 | 12 | 679 | 2.74 | 9 | 5 | ND | 2 | 37 | .2 | 2 | 2 | 47 | .36 | .043 | 12 | 52 | .85 | 130 | .15 | 4 | 1.46 | .02 | .07 | 1 | 2 |
| L10+50E 1+00N | 1 | 25 | 7 | 73 | .1 | 48 | 14 | 664 | 3.11 | 14 | 5 | ND | 2 | 42 | .2 | 2 | 2 | 52 | .38 | .057 | 12 | 57 | .95 | 152 | .16 | 8 | 1.69 | .02 | .07 | 1 | 2 |
| L10+50E 0+75N | 1 | 24 | 6 | 70 | .1 | 50 | 12 | 518 | 3.11 | 9 | 5 | ND | 2 | 24 | .2 | 2 | 2 | 53 | .31 | .060 | 8 | 58 | .90 | 94 | .12 | 6 | 1.59 | .01 | .05 | 1 | 1 |
| L10+50E 0+50N | 1 | 40 | 11 | 105 | .1 | 88 | 12 | 533 | 4.19 | 10 | 5 | ND | 2 | 34 | .2 | 2 | 2 | 60 | .46 | .052 | 20 | 78 | 1.18 | 242 | .14 | 4 | 2.86 | .01 | .07 | 1 | 3 |
| L10+50E 0+25N | 1 | 41 | 11 | 137 | .1 | 97 | 15 | 809 | 4.43 | 9 | 7 | ND | 1 | 41 | .3 | 4 | 2 | 63 | .62 | .087 | 18 | 97 | 1.37 | 313 | .08 | 6 | 2.99 | .02 | .09 | 1 | 4 |
| L10+50E 0+00N | 2 | 23 | 10 | 135 | .1 | 78 | 13 | 555 | 4.06 | 7 | 5 | ND | 2 | 28 | .2 | 3 | 2 | 60 | .34 | .061 | 15 | 78 | 1.11 | 227 | .15 | 5 | 2.70 | .01 | .08 | 1 | 1 |
| L16+50E 9+00N | 1 | 40 | 14 | 142 | .1 | 85 | 12 | 540 | 4.31 | 6 | 5 | ND | 1 | 34 | .2 | 3 | 2 | 59 | .37 | .099 | 20 | 72 | 1.03 | 282 | .12 | 4 | 3.51 | .01 | .11 | 1 | 3 |
| L16+50E 8+75N | 1 | 31 | 8 | 115 | .1 | 72 | 15 | 483 | 3.73 | 17 | 5 | ND | 1 | 40 | .2 | 2 | 2 | 58 | .49 | .062 | 17 | 75 | 1.25 | 252 | .13 | 7 | 2.54 | .02 | .08 | 1 | 3 |
| L16+50E 8+50N | 1 | 34 | 8 | 115 | .1 | 69 | 12 | 492 | 3.62 | 12 | 5 | ND | 1 | 37 | .2 | 4 | 2 | 54 | .40 | .062 | 14 | 65 | 1.11 | 216 | .14 | 6 | 2.45 | .02 | .08 | 1 | 4 |
| L16+50E 8+25N | 1 | 40 | 12 | 155 | .2 | 92 | 13 | 575 | 4.26 | 8 | 6 | ND | 1 | 41 | .3 | 3 | 2 | 59 | .48 | .085 | 20 | 75 | 1.10 | 373 | .09 | 4 | 3.69 | .01 | .12 | 1 | 6 |
| L16+50E 8+00N | 1 | 31 | 9 | 123 | .1 | 72 | 12 | 622 | 3.97 | 14 | 5 | ND | 2 | 42 | .2 | 2 | 2 | 60 | .50 | .061 | 18 | 73 | 1.14 | 277 | .14 | 4 | 2.63 | .02 | .09 | 1 | 3 |
| L16+50E 7+75N | 2 | 39 | 15 | 168 | .1 | 84 | 17 | 909 | 5.28 | 10 | 7 | ND | 2 | 42 | .3 | 2 | 2 | 72 | .55 | .077 | 26 | 77 | 1.13 | 380 | .10 | 4 | 3.80 | .02 | .12 | 1 | 3 |
| L16+40E 7+50N | 1 | 68 | 5 | 81 | .3 | 32 | 3 | 72 | .96 | 2 | 9 | ND | 1 | 58 | 2.0 | 2 | 2 | 24 | 1.05 | .081 | 27 | 40 | .28 | 214 | .03 | 4 | 1.72 | .01 | .05 | 2 | 8 |
| L16+50E 7+25N | 3 | 23 | 7 | 122 | .1 | 54 | 14 | 393 | 6.06 | 9 | 5 | ND | 3 | 36 | .3 | 4 | 2 | 87 | .45 | .072 | 12 | 60 | 1.29 | 176 | .14 | 3 | 2.76 | .01 | .05 | 1 | 1 |
| L16+50E 7+00N | 1 | 29 | 10 | 115 | .1 | 80 | 14 | 537 | 4.26 | 10 | 5 | ND | 1 | 44 | .2 | 2 | 2 | 61 | .55 | .081 | 13 | 84 | 1.25 | 259 | .08 | 4 | 2.86 | .02 | .10 | 1 | 4 |
| L16+50E 6+75N | 2 | 35 | 15 | 147 | .1 | 88 | 14 | 696 | 5.25 | 20 | 5 | ND | 1 | 47 | .4 | 5 | 2 | 68 | .65 | .083 | 19 | 82 | 1.18 | 332 | .10 | 5 | 3.18 | .02 | .09 | 1 | 6 |
| L16+50E 6+50N | 1 | 30 | 9 | 134 | .1 | 83 | 11 | 531 | 4.28 | 12 | 5 | ND | 2 | 40 | .2 | 2 | 2 | 58 | .50 | .054 | 18 | 70 | 1.08 | 276 | .18 | 4 | 2.82 | .02 | .09 | 2 | 4 |
| L16+50E 6+25N | 1 | 23 | 10 | 99 | .1 | 72 | 11 | 465 | 3.48 | 11 | 5 | ND | 3 | 42 | .2 | 3 | 2 | 53 | .49 | .057 | 14 | 73 | 1.24 | 190 | .19 | 5 | 2.09 | .02 | .07 | 1 | 6 |
| L16+50E 6+00N | 1 | 20 | 5 | 80 | .1 | 68 | 11 | 354 | 2.89 | 10 | 5 | ND | 2 | 48 | .2 | 2 | 2 | 49 | .53 | .064 | 13 | 65 | 1.14 | 188 | .16 | 5 | 1.72 | .03 | .07 | 1 | 2 |
| L16+50E 5+75N | 1 | 33 | 7 | 134 | .1 | 84 | 12 | 516 | 4.18 | 11 | 5 | ND | 1 | 40 | .2 | 3 | 2 | 61 | .38 | .054 | 17 | 71 | 1.10 | 350 | .11 | 5 | 3.12 | .02 | .09 | 1 | 4 |
| L16+50E 5+50N | 1 | 26 | 8 | 75 | .1 | 56 | 11 | 467 | 3.04 | 9 | 5 | ND | 2 | 42 | .2 | 2 | 2 | 49 | .40 | .032 | 11 | 62 | 1.08 | 177 | .15 | 3 | 1.75 | .02 | .06 | 1 | 3 |
| L16+50E 5+25N | 1 | 23 | 8 | 109 | .1 | 67 | 11 | 517 | 3.79 | 7 | 5 | ND | 2 | 48 | .2 | 2 | 2 | 58 | .54 | .044 | 16 | 65 | 1.05 | 282 | .13 | 3 | 2.47 | .02 | .08 | 1 | 1 |
| L16+50E 5+00N | 1 | 24 | 9 | 102 | .1 | 54 | 11 | 468 | 3.65 | 5 | 5 | ND | 1 | 50 | .2 | 2 | 2 | 56 | .57 | .058 | 14 | 61 | 1.05 | 248 | .12 | 3 | 2.29 | .02 | .09 | 2 | 14 |
| L16+50E 4+75N | 1 | 28 | 7 | 90 | .1 | 52 | 11 | 499 | 3.61 | 6 | 5 | ND | 2 | 51 | .2 | 2 | 2 | 58 | .53 | .056 | 14 | 62 | 1.08 | 223 | .15 | 3 | 2.21 | .04 | .10 | 1 | 5 |
| L16+50E 4+50N | 1 | 27 | 11 | 82 | .1 | 51 | 12 | 545 | 3.38 | 9 | 5 | ND | 3 | 46 | .2 | 3 | 2 | 56 | .44 | .049 | 13 | 58 | 1.02 | 179 | .16 | 3 | 1.88 | .04 | .09 | 1 | 1 |
| L16+50E 4+25N | 1 | 20 | 10 | 87 | .1 | 49 | 11 | 491 | 3.36 | 7 | 5 | ND | 2 | 46 | .2 | 3 | 2 | 56 | .43 | .048 | 11 | 62 | 1.09 | 198 | .13 | 3 | 2.03 | .04 | .10 | 2 | 4 |
| L16+50E 4+00N | 1 | 28 | 4 | 91 | .1 | 67 | 14 | 582 | 3.47 | 13 | 5 | ND | 2 | 42 | .2 | 2 | 3 | 59 | .49 | .068 | 10 | 68 | 1.37 | 175 | .13 | 4 | 2.04 | .02 | .09 | 1 | 3 |
| L16+50E 3+75N | 1 | 33 | 8 | 107 | .1 | 62 | 20 | 588 | 5.32 | 7 | 5 | ND | 1 | 23 | .3 | 2 | 2 | 52 | .24 | .047 | 10 | 62 | 1.08 | 130 | .07 | 4 | 1.86 | .02 | .08 | 2 | 1 |
| L16+50E 3+00N | 1 | 13 | 2 | 86 | .1 | 5 | 6 | 690 | 3.94 | 2 | 5 | ND | 1 | 18 | .2 | 2 | 2 | 38 | .22 | .140 | 10 | 10 | .31 | 94 | .01 | 3 | 1.14 | .01 | .06 | 1 | 1 |
| L16+50E 2+75N | 1 | 35 | 6 | 110 | .1 | 49 | 15 | 625 | 4.08 | 8 | 5 | ND | 1 | 23 | .2 | 2 | 2 | 56 | .22 | .050 | 11 | 66 | 1.06 | 122 | .08 | 3 | 2.07 | .01 | .05 | 1 | 5 |
| L16+50E 2+50N | 1 | 30 | 9 | 79 | .1 | 43 | 9 | 370 | 3.23 | 9 | 5 | ND | 1 | 21 | .2 | 2 | 2 | 57 | .18 | .049 | 11 | 52 | .75 | 157 | .10 | 10 | 2.20 | .01 | .07 | 1 | 4 |
| L16+50E 2+25N | 1 | 25 | 3 | 63 | .1 | 48 | 12 | 528 | 2.81 | 9 | 5 | ND | 3 | 47 | .2 | 2 | 2 | 50 | .42 | .061 | 12 | 51 | .88 | 155 | .13 | 3 | 1.42 | .02 | .06 | 1 | 3 |
| L16+50E 2+00N | 2 | 16 | 12 | 80 | .1 | 26 | 8 | 533 | 4.69 | 9 | 5 | ND | 1 | 14 | .2 | 2 | 2 | 59 | .11 | .063 | 14 | 45 | .47 | 119 | .24 | 2 | 3.06 | .02 | .05 | 1 | 4 |
| L16+50E 1+75N | 3 | 14 | 17 | 98 | .1 | 24 | 8 | 640 | 5.17 | 7 | 6 | ND | 5 | 8 | .2 | 2 | 3 | 43 | .18 | .073 | 27 | 32 | .50 | 87 | .31 | 2 | 5.40 | .04 | .05 | 1 | 3 |
| L16+50E 1+50N | 1 | 19 | 12 | 76 | .1 | 38 | 14 | 1235 | 4.87 | 15 | 5 | ND | 2 | 17 | .2 | 2 | 2 | 78 | .15 | .082 | 9 | 55 | .74 | 82 | .20 | 4 | 1.99 | .01 | .05 | 1 | 3 |
| STANDARD C/AU-S | 17 | 58 | 39 | 132 | 7.2 | 69 | 31 | 1039 | 3.98 | 38 | 25 | 7 | 38 | 52 | 18.3 | 15 | 18 | 55 | .52 | .090 | 37 | 58 | .93 | 179 | .09 | 33 | 1.94 | .06 | .13 | 11 | 54 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | Hg ppm | Au** ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|-----------|-------------|
| L16+50E 1+25N | 1 | 22 | 10 | 88 | .1 | 38 | 12 | 1114 | 5.00 | 14 | 5 | ND | 1 | 17 | .2 | 2 | 2 | 63 | .16 | .183 | 9 | 63 | .58 | 83 | .08 | 3 | 2.78 | .01 | .04 | 1 | 1 |
| L16+50E 1+00N | 1 | 23 | 9 | 133 | .1 | 50 | 18 | 721 | 5.01 | 7 | 6 | ND | 5 | 15 | .2 | 2 | 2 | 58 | .37 | .068 | 20 | 41 | .93 | 130 | .43 | 2 | 4.57 | .03 | .06 | 1 | 1 |
| L16+50E 0+75N | 2 | 20 | 9 | 95 | .1 | 33 | 11 | 891 | 5.28 | 14 | 5 | ND | 2 | 14 | .2 | 2 | 2 | 74 | .14 | .065 | 13 | 51 | .59 | 85 | .24 | 4 | 2.57 | .02 | .04 | 1 | 1 |
| L16+50E 0+50N | 1 | 31 | 13 | 118 | .2 | 50 | 18 | 1047 | 4.49 | 7 | 6 | ND | 3 | 21 | .2 | 4 | 3 | 58 | .29 | .085 | 12 | 53 | .86 | 123 | .23 | 3 | 3.74 | .02 | .06 | 1 | 6 |
| L16+50E 0+25N | 1 | 31 | 11 | 111 | .2 | 43 | 13 | 721 | 5.31 | 10 | 5 | ND | 4 | 15 | .2 | 4 | 2 | 53 | .29 | .100 | 14 | 49 | .78 | 92 | .28 | 3 | 5.47 | .02 | .04 | 1 | 1 |
| L16+50E 0+00N | 1 | 24 | 8 | 102 | .1 | 34 | 12 | 790 | 5.13 | 4 | 5 | ND | 1 | 14 | .2 | 3 | 2 | 59 | .16 | .103 | 11 | 54 | .63 | 125 | .14 | 3 | 3.21 | .01 | .03 | 1 | 1 |
| L19+50E 4+00N | 1 | 46 | 10 | 119 | .1 | 95 | 20 | 1131 | 4.51 | 12 | 5 | ND | 2 | 53 | .3 | 2 | 2 | 66 | .66 | .083 | 18 | 79 | 1.35 | 285 | .11 | 4 | 2.90 | .02 | .10 | 1 | 272 |
| L19+50E 3+75N | 1 | 34 | 11 | 121 | .1 | 56 | 12 | 595 | 4.38 | 7 | 5 | ND | 1 | 42 | .2 | 2 | 2 | 71 | .44 | .134 | 16 | 68 | .90 | 313 | .08 | 3 | 2.93 | .01 | .07 | 1 | 4 |
| L19+50E 3+50N | 2 | 41 | 14 | 121 | .1 | 67 | 14 | 675 | 5.55 | 13 | 5 | ND | 2 | 31 | .2 | 2 | 2 | 64 | .36 | .069 | 21 | 57 | .82 | 206 | .30 | 4 | 3.65 | .02 | .06 | 1 | 1 |
| L19+50E 3+25N | 1 | 31 | 9 | 94 | .1 | 59 | 15 | 663 | 3.37 | 9 | 5 | ND | 2 | 51 | .2 | 2 | 3 | 59 | .53 | .067 | 12 | 64 | 1.19 | 205 | .14 | 3 | 1.96 | .02 | .09 | 1 | 3 |
| L19+50E 3+00N | 1 | 35 | 5 | 89 | .1 | 70 | 21 | 923 | 3.97 | 4 | 5 | ND | 2 | 37 | .2 | 2 | 2 | 64 | .40 | .057 | 9 | 71 | 1.43 | 178 | .11 | 5 | 2.09 | .02 | .08 | 1 | 2 |
| L19+50E 2+50N | 39 | 412 | 8 | 273 | .1 | 22 | 8 | 407 | 5.90 | 10 | 5 | ND | 2 | 12 | .5 | 2 | 2 | 59 | .20 | .114 | 5 | 19 | .77 | 86 | .03 | 3 | 1.56 | .03 | .05 | 1 | 10 |
| L19+50E 8+75N | 1 | 36 | 12 | 122 | .1 | 59 | 13 | 490 | 3.67 | 9 | 5 | ND | 2 | 51 | .2 | 2 | 3 | 62 | .55 | .064 | 16 | 62 | 1.10 | 271 | .13 | 4 | 2.31 | .03 | .10 | 2 | 7 |
| L21+00E 8+50N | 1 | 34 | 13 | 128 | .1 | 70 | 17 | 826 | 4.04 | 9 | 5 | ND | 2 | 50 | .4 | 3 | 2 | 65 | .56 | .070 | 20 | 69 | 1.19 | 344 | .11 | 4 | 2.74 | .02 | .10 | 1 | 2 |
| L21+00E 8+25N | 1 | 40 | 11 | 107 | .1 | 66 | 13 | 471 | 3.65 | 13 | 5 | ND | 4 | 55 | .2 | 3 | 2 | 59 | .56 | .067 | 21 | 60 | 1.02 | 269 | .22 | 4 | 2.27 | .04 | .10 | 2 | 3 |
| L21+00E 8+00N | 1 | 52 | 12 | 170 | .1 | 80 | 19 | 1155 | 5.26 | 14 | 5 | ND | 2 | 57 | .3 | 2 | 3 | 75 | .75 | .094 | 24 | 73 | 1.23 | 411 | .12 | 4 | 3.63 | .02 | .12 | 1 | 7 |
| L21+00E 7+75N | 1 | 35 | 10 | 116 | .1 | 68 | 13 | 616 | 4.10 | 13 | 5 | ND | 2 | 47 | .2 | 2 | 2 | 61 | .55 | .071 | 19 | 66 | 1.13 | 269 | .15 | 4 | 2.59 | .02 | .09 | 1 | 3 |
| L21+00E 7+50N | 1 | 51 | 9 | 174 | .1 | 73 | 14 | 1246 | 3.10 | 5 | 5 | ND | 1 | 95 | 1.5 | 2 | 2 | 42 | 1.56 | .132 | 31 | 48 | .87 | 562 | .03 | 4 | 3.12 | .01 | .13 | 1 | 3 |
| L21+00E 7+25N | 1 | 40 | 12 | 149 | .1 | 79 | 16 | 770 | 4.36 | 9 | 5 | ND | 2 | 50 | .2 | 2 | 3 | 67 | .62 | .076 | 17 | 64 | 1.07 | 430 | .08 | 3 | 3.51 | .02 | .12 | 1 | 5 |
| L21+00E 7+00N | 1 | 32 | 10 | 117 | .1 | 68 | 14 | 505 | 3.77 | 11 | 5 | ND | 1 | 53 | .2 | 2 | 2 | 62 | .63 | .086 | 17 | 62 | 1.04 | 333 | .09 | 3 | 2.92 | .02 | .09 | 1 | 3 |
| L21+00E 6+75N | 1 | 35 | 13 | 151 | .2 | 79 | 19 | 792 | 4.24 | 8 | 5 | ND | 2 | 59 | .6 | 2 | 2 | 72 | .77 | .107 | 15 | 69 | 1.08 | 430 | .05 | 3 | 3.63 | .02 | .13 | 1 | 1 |
| L21+00E 6+50N | 1 | 21 | 7 | 87 | .1 | 51 | 12 | 680 | 3.82 | 13 | 5 | ND | 2 | 48 | .2 | 2 | 2 | 58 | .54 | .070 | 14 | 56 | .97 | 208 | .14 | 4 | 1.93 | .03 | .07 | 1 | 11 |
| L21+00E 6+25N | 2 | 39 | 13 | 132 | .1 | 75 | 16 | 1106 | 5.10 | 13 | 5 | ND | 1 | 58 | .2 | 2 | 3 | 74 | .69 | .107 | 20 | 66 | 1.04 | 401 | .06 | 3 | 3.39 | .02 | .12 | 1 | 1 |
| L21+00E 6+00N | 1 | 38 | 11 | 149 | .1 | 86 | 14 | 880 | 4.85 | 15 | 5 | ND | 2 | 55 | .6 | 3 | 2 | 68 | .65 | .074 | 21 | 65 | .93 | 395 | .13 | 3 | 3.38 | .02 | .11 | 1 | 2 |
| L21+00E 5+75N | 2 | 59 | 13 | 134 | .1 | 108 | 15 | 650 | 6.08 | 10 | 5 | ND | 3 | 48 | .5 | 3 | 2 | 89 | .58 | .061 | 30 | 71 | .86 | 411 | .22 | 4 | 4.21 | .02 | .11 | 1 | 2 |
| L21+00E 5+50N | 1 | 36 | 12 | 153 | .1 | 85 | 12 | 573 | 4.24 | 9 | 5 | ND | 3 | 45 | .2 | 2 | 2 | 60 | .53 | .060 | 21 | 63 | .99 | 294 | .27 | 4 | 2.65 | .03 | .09 | 1 | 4 |
| L21+00E 5+25N | 1 | 52 | 12 | 137 | .1 | 83 | 13 | 651 | 5.08 | 5 | 5 | ND | 1 | 49 | .3 | 2 | 2 | 70 | .56 | .096 | 26 | 69 | 1.02 | 324 | .15 | 4 | 3.68 | .02 | .10 | 1 | 5 |
| L21+00E 5+00N | 1 | 32 | 9 | 97 | .1 | 62 | 12 | 551 | 3.70 | 10 | 5 | ND | 2 | 39 | .2 | 2 | 3 | 57 | .42 | .051 | 16 | 61 | .96 | 206 | .13 | 3 | 2.21 | .02 | .09 | 1 | 2 |
| L21+00E 4+75N | 1 | 47 | 9 | 133 | .5 | 91 | 12 | 463 | 3.93 | 3 | 6 | ND | 1 | 68 | .2 | 2 | 2 | 56 | .83 | .109 | 21 | 64 | 1.05 | 493 | .04 | 3 | 3.79 | .01 | .12 | 1 | 2 |
| L21+00E 4+50N | 1 | 36 | 9 | 126 | .1 | 79 | 12 | 506 | 4.15 | 10 | 5 | ND | 2 | 47 | .3 | 2 | 2 | 61 | .53 | .073 | 21 | 64 | .95 | 317 | .13 | 3 | 3.02 | .02 | .09 | 1 | 4 |
| L21+00E 4+25N | 1 | 45 | 7 | 132 | .1 | 85 | 11 | 473 | 3.47 | 9 | 5 | ND | 1 | 76 | .2 | 2 | 2 | 49 | .99 | .101 | 32 | 61 | .99 | 423 | .04 | 3 | 3.28 | .01 | .10 | 1 | 4 |
| L21+00E 4+00N | 1 | 31 | 6 | 93 | .1 | 66 | 11 | 480 | 3.43 | 5 | 5 | ND | 2 | 43 | .2 | 2 | 3 | 55 | .49 | .064 | 15 | 62 | 1.06 | 202 | .11 | 4 | 2.16 | .02 | .09 | 1 | 1 |
| L21+00E 3+75N | 1 | 47 | 9 | 120 | .1 | 77 | 16 | 916 | 4.15 | 7 | 5 | ND | 1 | 67 | .2 | 2 | 2 | 63 | .77 | .108 | 21 | 66 | 1.14 | 352 | .06 | 3 | 3.09 | .02 | .12 | 1 | 3 |
| L21+00E 3+50N | 1 | 46 | 8 | 123 | .1 | 82 | 12 | 586 | 4.33 | 5 | 5 | ND | 1 | 50 | .2 | 2 | 3 | 60 | .61 | .087 | 27 | 66 | .99 | 325 | .11 | 3 | 3.35 | .02 | .09 | 1 | 2 |
| L21+00E 3+25N | 1 | 26 | 8 | 105 | .1 | 59 | 15 | 755 | 3.59 | 9 | 5 | ND | 2 | 54 | .3 | 2 | 2 | 60 | .62 | .079 | 14 | 59 | 1.16 | 222 | .10 | 4 | 2.16 | .02 | .10 | 1 | 4 |
| L21+00E 3+00N | 1 | 24 | 7 | 107 | .1 | 51 | 12 | 651 | 3.34 | 5 | 5 | ND | 1 | 62 | .4 | 3 | 3 | 55 | .74 | .078 | 16 | 54 | 1.02 | 252 | .08 | 5 | 2.08 | .02 | .08 | 1 | 4 |
| STANDARD C/AU-S | 18 | 59 | 39 | 132 | 7.2 | 70 | 31 | 1025 | 3.93 | 38 | 21 | 7 | 37 | 53 | 18.4 | 15 | 22 | 55 | .51 | .092 | 37 | 58 | .93 | 179 | .09 | 34 | 1.91 | .06 | .14 | 11 | 52 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|
| L21+00E 2+75N | 1 | 38 | 8 | 109 | .1 | 71 | 17 | 911 | 4.18 | 3 | 5 | ND | 2 | 38 | .5 | 2 | 2 | 68 | .40 | .058 | 12 | 62 | 1.21 | 204 | .10 | 5 | 2.48 | .01 | .09 | 1 | 4 |
| L21+00E 2+50N | 1 | 40 | 7 | 122 | .1 | 69 | 19 | 973 | 3.99 | 2 | 5 | ND | 1 | 41 | .4 | 2 | 2 | 67 | .42 | .077 | 13 | 70 | 1.25 | 195 | .10 | 4 | 2.47 | .02 | .10 | 2 | 6 |
| L21+00E 2+25N | 1 | 52 | 5 | 94 | .1 | 76 | 20 | 1076 | 4.07 | 6 | 5 | ND | 4 | 65 | .2 | 2 | 2 | 72 | .67 | .071 | 15 | 66 | 1.44 | 239 | .14 | 4 | 2.35 | .02 | .13 | 1 | 12 |
| L21+00E 2+00N | 1 | 40 | 10 | 91 | .1 | 58 | 16 | 784 | 3.55 | 7 | 5 | ND | 2 | 55 | .4 | 2 | 2 | 64 | .50 | .075 | 14 | 55 | 1.11 | 209 | .13 | 6 | 2.06 | .02 | .10 | 1 | 11 |
| L21+00E 1+75N | 1 | 36 | 9 | 101 | .1 | 73 | 17 | 871 | 3.78 | 7 | 5 | ND | 1 | 50 | .4 | 3 | 2 | 62 | .59 | .079 | 15 | 72 | 1.24 | 223 | .12 | 5 | 2.17 | .02 | .09 | 1 | 6 |
| L21+00E 1+50N | 1 | 37 | 7 | 89 | .1 | 60 | 11 | 516 | 3.21 | 6 | 5 | ND | 2 | 47 | .2 | 3 | 2 | 56 | .52 | .065 | 18 | 57 | .89 | 237 | .13 | 4 | 1.96 | .02 | .08 | 1 | 5 |
| L21+00E 1+25N | 1 | 34 | 7 | 79 | .2 | 57 | 12 | 511 | 3.01 | 2 | 5 | ND | 2 | 40 | .3 | 2 | 2 | 53 | .43 | .054 | 14 | 56 | .88 | 204 | .11 | 4 | 1.91 | .01 | .07 | 1 | 6 |
| L21+00E 1+00N | 1 | 63 | 15 | 133 | .2 | 84 | 18 | 957 | 4.85 | 10 | 6 | ND | 3 | 61 | .6 | 5 | 2 | 68 | .80 | .086 | 37 | 67 | 1.08 | 463 | .09 | 5 | 3.81 | .02 | .14 | 1 | 3 |
| L21+00E 0+75N | 1 | 29 | 10 | 91 | .2 | 46 | 10 | 571 | 2.97 | 2 | 5 | ND | 2 | 59 | .3 | 2 | 2 | 50 | .79 | .073 | 15 | 45 | .82 | 231 | .10 | 3 | 1.88 | .01 | .11 | 1 | 4 |
| L21+00E 0+50N | 1 | 35 | 7 | 115 | .1 | 61 | 13 | 653 | 3.27 | 6 | 5 | ND | 2 | 53 | .3 | 3 | 2 | 57 | .73 | .078 | 20 | 59 | .99 | 302 | .09 | 4 | 2.56 | .01 | .10 | 1 | 2 |
| L21+00E 0+25N | 1 | 33 | 5 | 81 | .2 | 60 | 14 | 685 | 3.24 | 9 | 5 | ND | 3 | 52 | .2 | 3 | 2 | 59 | .58 | .083 | 15 | 59 | 1.04 | 171 | .14 | 5 | 1.75 | .02 | .08 | 1 | 1 |
| JE 0+00N | 1 | 46 | 10 | 110 | .1 | 69 | 13 | 610 | 3.88 | 9 | 5 | ND | 2 | 53 | .2 | 3 | 2 | 64 | .72 | .075 | 21 | 61 | 1.01 | 278 | .17 | 5 | 2.75 | .02 | .09 | 1 | 1 |
| STANDARD C/AU-S | 18 | 58 | 38 | 132 | 7.2 | 71 | 31 | 1003 | 3.83 | 38 | 22 | 7 | 38 | 53 | 18.4 | 15 | 19 | 56 | .50 | .092 | 38 | 59 | .90 | 180 | .09 | 34 | 1.88 | .06 | .13 | 11 | 54 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | U ppm | Au** ppb |
|-------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|
| L9+90W 15+50N 'S' | 2 | 48 | 11 | 132 | .1 | 46 | 15 | 1226 | 6.35 | 7 | 5 | ND | 2 | 64 | 1.3 | 2 | 2 | 58 | .88 | .073 | 19 | 49 | .86 | 405 | .06 | 3 | 2.47 | .02 | .09 | 1 | 7 |
| L4+35E 3+20S 'S' | 1 | 40 | 8 | 145 | .2 | 83 | 18 | 767 | 4.05 | 6 | 5 | ND | 2 | 34 | .2 | 4 | 2 | 62 | .37 | .076 | 19 | 76 | 1.12 | 344 | .11 | 3 | 3.30 | .01 | .10 | 1 | 5 |
| L4+50E 4+45N 'S' | 1 | 32 | 9 | 180 | .1 | 57 | 15 | 1511 | 3.16 | 7 | 5 | ND | 1 | 58 | .8 | 3 | 2 | 46 | .71 | .100 | 22 | 54 | .88 | 356 | .06 | 5 | 2.78 | .02 | .20 | 1 | 3 |
| L4+50E 0+60S 'S' | 1 | 32 | 7 | 122 | .1 | 51 | 17 | 846 | 3.95 | 6 | 5 | ND | 2 | 35 | .3 | 2 | 2 | 63 | .58 | .069 | 11 | 67 | 1.25 | 129 | .19 | 2 | 1.92 | .01 | .11 | 1 | 4 |
| L4+50E 3+90S 'S' | 1 | 38 | 8 | 123 | .1 | 88 | 19 | 1046 | 3.83 | 12 | 5 | ND | 1 | 45 | .6 | 3 | 2 | 59 | .67 | .082 | 14 | 89 | 1.50 | 203 | .14 | 6 | 2.32 | .01 | .10 | 1 | 4 |
| L4+50E 7+25S 'S' | 1 | 41 | 11 | 144 | .1 | 56 | 10 | 372 | 3.27 | 7 | 5 | ND | 3 | 78 | .2 | 3 | 3 | 45 | 1.23 | .097 | 37 | 50 | .60 | 349 | .28 | 5 | 3.11 | .04 | .06 | 1 | 5 |
| L4+60E 2+50N 'S' | 1 | 24 | 11 | 112 | .3 | 59 | 13 | 678 | 3.59 | 4 | 5 | ND | 2 | 44 | .2 | 2 | 2 | 58 | .55 | .067 | 17 | 64 | 1.04 | 306 | .11 | 3 | 2.76 | .01 | .10 | 1 | 1 |
| L4+60E 1+50S 'S' | 1 | 31 | 12 | 133 | .1 | 67 | 14 | 780 | 3.47 | 2 | 5 | ND | 1 | 48 | .4 | 2 | 2 | 55 | .52 | .070 | 15 | 71 | 1.08 | 361 | .12 | 2 | 2.54 | .02 | .13 | 1 | 4 |
| L20+40E 2+30N 'S' | 1 | 38 | 8 | 138 | .2 | 68 | 14 | 734 | 3.16 | 2 | 5 | ND | 2 | 66 | .8 | 2 | 2 | 49 | 1.33 | .101 | 19 | 64 | 1.17 | 300 | .06 | 14 | 2.42 | .02 | .14 | 1 | 5 |
| L20+50E 0+00N 'S' | 1 | 35 | 10 | 201 | .1 | 68 | 15 | 1072 | 3.64 | 6 | 5 | ND | 2 | 68 | 1.2 | 3 | 2 | 53 | 1.34 | .118 | 23 | 62 | 1.07 | 361 | .07 | 5 | 3.11 | .02 | .16 | 1 | 4 |
| L20... 4+27N 'S' | 1 | 25 | 7 | 90 | .1 | 67 | 13 | 655 | 3.16 | 4 | 5 | ND | 2 | 52 | .2 | 2 | 2 | 57 | .61 | .066 | 16 | 59 | .99 | 229 | .11 | 5 | 1.99 | .02 | .09 | 1 | 1 |

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| Sample Name | Type | Au ppb | F ppm | Ag ppm | Al % | As ppm | Ca % | Ca % | Co ppm | Cu ppm | Fe % | Fe % | K % | Mg % | Mg % | Mn ppm |
|-------------|------|-----------|----------|-----------|---------|-----------|---------|---------|-----------|-----------|---------|---------|--------|---------|---------|-----------|
| Blank | Pulp | <5 | <10 | 0.1 | <0.01 | <5 | <0.01 | <0.01 | <1 | <1 | <0.01 | <0.01 | <0.01 | <0.01 | <0.01 | 1 |
| R90KJ 1 | Rock | 5 | 186 | <0.1 | >5.00 | <5 | 0.12 | 0.03 | 2 | 21 | 1.64 | 0.55 | 0.78 | 0.55 | 0.45 | 113 |
| R90KJ 2 | Rock | <5 | 99 | <0.1 | >5.00 | <5 | 0.11 | 0.01 | 1 | 26 | 1.93 | 1.19 | 0.29 | 0.62 | 0.57 | 181 |
| R90KP 1 | Rock | <5 | 123 | <0.1 | >5.00 | <5 | 0.47 | 0.44 | 1 | 4 | 1.43 | 1.46 | 0.08 | 0.13 | 0.13 | 147 |
| R90KP 2A | Rock | <5 | 139 | <0.1 | >5.00 | <5 | 0.29 | 0.26 | 2 | 7 | 1.55 | 0.73 | 0.06 | 0.17 | 0.18 | 68 |
| R90KP 2B | Rock | <5 | 45 | <0.1 | >5.00 | 5 | 0.06 | 0.01 | 1 | 9 | 1.58 | 0.55 | 0.05 | 0.02 | 0.01 | 62 |
| R90KP 5 | Rock | <5 | 181 | <0.1 | >5.00 | <5 | 0.30 | 0.28 | 2 | 6 | 1.39 | 1.14 | 0.33 | 0.27 | 0.27 | 126 |
| R90KP 7 | Rock | <5 | 114 | <0.1 | >5.00 | <5 | 1.00 | 0.70 | 3 | 6 | 1.09 | 0.67 | 0.20 | 0.45 | 0.36 | 218 |
| R90KP 8 | Rock | 5 | 520 | <0.1 | >5.00 | <5 | 3.21 | 3.21 | 31 | 2686 | >5.00 | 4.45 | 0.19 | 3.06 | 3.12 | 1710 |
| R90KP 9 | Rock | <5 | 59 | <0.1 | >5.00 | <5 | 0.60 | 0.56 | 1 | 18 | 1.00 | 0.62 | 0.07 | 0.37 | 0.38 | 127 |
| R90KP 10 | Rock | 10 | 506 | <0.1 | >5.00 | <5 | 1.08 | 0.15 | 3 | 7 | 3.16 | 1.87 | 0.25 | 1.84 | 1.51 | 153 |
| R90KP 11 | Rock | 5 | 213 | <0.1 | >5.00 | <5 | 0.26 | 0.17 | 3 | 57 | 1.76 | 0.99 | 0.12 | 0.49 | 0.47 | 148 |
| R90PK 3 | Rock | 5 | 73 | <0.1 | >5.00 | <5 | 0.89 | 0.90 | 2 | 11 | 0.98 | 0.64 | 0.07 | 0.51 | 0.54 | 149 |
| R90PK 4 | Rock | 5 | 136 | <0.1 | >5.00 | 5 | 0.54 | 0.45 | 3 | 6 | 1.21 | 1.01 | 0.16 | 0.53 | 0.58 | 152 |
| R90PK 6 | Rock | 5 | 242 | <0.1 | >5.00 | <5 | 0.59 | 0.56 | 1 | 4 | 1.60 | 1.55 | 0.41 | 0.26 | 0.25 | 104 |
| Standard | Pulp | 190 | 300 | 1.6 | >5.00 | 25 | 0.29 | 0.21 | 16 | 354 | >5.00 | >5.00 | 3.85 | 1.07 | 0.64 | 207 |

Minimum Detection

| | | | | | | | | | | | | | | | |
|-------|-------|-------|------|-------|-------|--------|-------|-------|------|------|-------|-------|-------|-------|-------|
| 5 | 10 | 0.1 | 0.01 | 5 | 0.01 | 0.01 | 1 | 1 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 1 |
| 10000 | 10000 | 100.0 | 5.00 | 10000 | 10.00 | 10.00 | 10000 | 20000 | 5.00 | 5.00 | 10.00 | 10.00 | 10.00 | 10.00 | 10000 |
| GeoSp | GeoSp | ICP | ICP | ICP | ICP | ICPHC1 | ICP | ICP | ICP | ICP | ICP | ICP | ICP | ICP | ICP |

Maximum Detection

Method

-- = Not Analysed unr = Not Requested ins = Insufficient Sample

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Report: 9000647 R Homestake Mining (Canada) Ltd.

Project: 3174

Page 1 of 1

Section 2 of 2

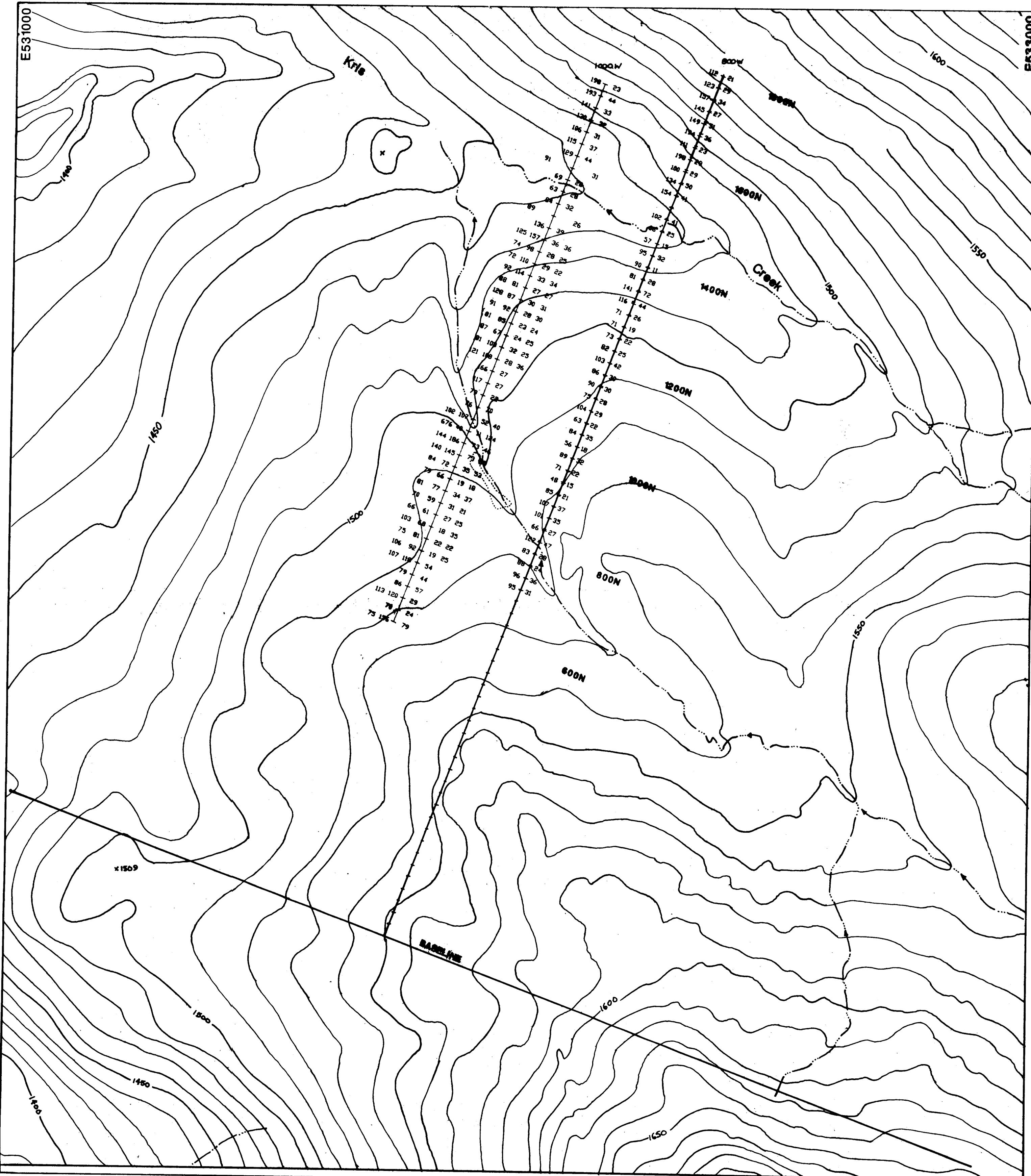
| Sample Name | Mn ppm | Mo ppm | Na % | Pb ppm | Sr ppm | Sr ppm | Zn ppm |
|-------------|-----------|-----------|---------|-----------|-----------|-----------|-----------|
| Blank | <1 | 1 | <0.01 | 2 | <1 | <1 | 1 |
| R90KJ 1 | 104 | 4 | 3.25 | <2 | 42 | 3 | 31 |
| R90KJ 2 | 173 | 1 | 3.81 | <2 | 30 | 1 | 34 |
| R90KP 1 | 152 | <1 | 4.06 | <2 | 27 | 3 | 13 |
| R90KP 2A | 75 | 5 | 4.03 | <2 | 19 | 2 | 16 |
| R90KP 2B | 33 | 2 | 3.98 | 2 | 17 | 1 | 7 |
| R90KP 5 | 135 | 2 | 3.27 | <2 | 25 | 5 | 12 |
| R90KP 7 | 180 | 3 | 4.04 | <2 | 66 | 9 | 24 |
| R90KP 8 | 1722 | 15 | 2.38 | <2 | 48 | 22 | 166 |
| R90KP 9 | 130 | 1 | 3.62 | <2 | 24 | 4 | 12 |
| R90KP 10 | 111 | 23 | >5.00 | 2 | 107 | 15 | 39 |
| R90KP 11 | 150 | 2 | 4.33 | <2 | 40 | 6 | 73 |
| R90PK 3 | 161 | 4 | 3.66 | <2 | 29 | 7 | 12 |
| R90PK 4 | 165 | 3 | 3.75 | <2 | 39 | 9 | 14 |
| R90PK 6 | 103 | 4 | 3.45 | <2 | 27 | 5 | 14 |
| Standard | 162 | 43 | 0.44 | 12 | 127 | 16 | 64 |

| | | | | | | | |
|-------------------|--------|------|------|-------|-------|--------|-------|
| Minimum Detection | 1 | 1 | 0.01 | 2 | 1 | 1 | 1 |
| Maximum Detection | 10000 | 1000 | 5.00 | 20000 | 10000 | 10000 | 20000 |
| Method | ICPHC1 | ICP | ICP | ICP | ICP | ICPHC1 | ICP |

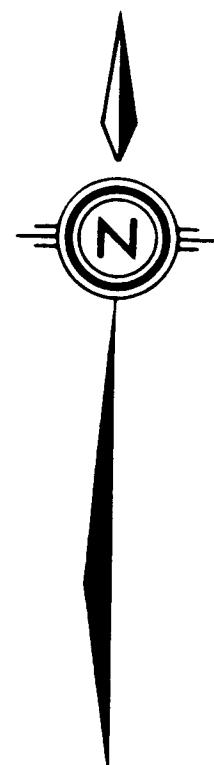
-- = Not Analysed unr = Not Requested ins = Insufficient Sample

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Fax (604) 879-7898

ippl
INTERNATIONAL PLASMA LABORATORY LTD.



N0449250



Zn assay value
(ppm)

Cu assay value
(ppm)

| | |
|-----|----|
| 79 | 22 |
| 76 | 70 |
| 102 | 52 |
| 107 | 40 |

soil sample location

outer Cu & Zn values
indicate duplicate sample
taken from site
sample collected by auger

creek

contour interval is 10 m

GEOLOGICAL BRANCH ASSESSMENT REPORT

20,337

scale 1:5mm

**HOMESTAKE
MINING (CANADA) LIMITED**

KUTCHO PROJECT

'C' GRID

GEOCHEMICAL ORIENTATION SURVEY

| | |
|----------------|----------------------|
| DRAWN PH/HO | DATE OCTOBER 1990 |
| Revised _____ | |

104 I/

Fig. 3.1

Fig. 3.1



LEGEND

Zn assay value
(ppm) Cu assay value
(ppm)

110 43 104 43
105 109 34 40 145 109 34 40

soil sample location
outer Cu + Zn values
indicate duplicate sample
taken from site

creek

contour interval is 10 m

GEOLOGICAL BRANCH
ASSESSMENT REPORT

20,337

Scale 1:5000

HOMESTAKE
MINING (CANADA) LIMITED

KUTCHO PROJECT

'O' TARGET, JOSH CREEK
SOIL GEOCHEMISTRY

| | | | |
|---------------|----------------------|---------------|----------|
| DRAWN HO | DATE OCTOBER 1990 | NTS 104I/1 | Fig. 3.2 |
| Revised _____ | | | |

