MINERAL EXPLORATION REPORT
GEOPHYSICAL AND GEOCHEMICAL PROGRAM
JUNE 1990

LOG NO: 10-10	RD.
ACTION:	
FILE NO:	

CAZADOR EXPLORATIONS LIMITED
ARLINGTON SILVER PROJECT
SLOCAN MINING DIVISION
SLOCAN, BRITISH COLUMBIA
NTS: 82F/14W

49° 48'
117° 21'

LOG NO: Feb 05/91	RD.
ACTION: Date received back from amendment	
FILE NO:	

PREPARED BY: JOHN A. CHAPMAN, P.ENG.
ASSISTANT: BRETT SVEINSON
RE: "ASSESSMENT REPORT" TO BRITISH COLUMBIA MINISTRY OF ENERGY, MINES AND PETROLEUM RESOURCES

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INTRODUCTION

Cazador Explorations Limited's Arlington Silver project, consisting of several located mineral claims, crown granted mineral claims and mining leases, is located 12km east of Slocan City, B.C. The Property is within the Slocan Mining Division, on mapsheet 82F/14W.

Cazador obtained full title to the property's mineral tenure in 1990.

The Property area has produced approximately 1,000,000 ounces of silver, 1,900,000 pounds of lead and 250,000 pounds of zinc during a period of time from the late 1800's to the early 1960's. The two producing mines on the Property were the Arlington and the Speculator. Mineralization is shear controlled, and extends along several kilometres to former producing mines to the north of the Arlington and Speculator.

Annual work approval #NEL 90-0500333-401 was issued by the District Inspector of Mines, June 26, 1990. Notice of 1990 project completion will be filed in October 1990.

SUMMARY

The geophysical and geochemical survey conducted in June 1990 consisted of 2,775 line meters, with 118 sample stations established. Soil samples were taken from the "B" horizon, at 25 meter intervals along each line, and VLF-EM readings were taken at these same stations.

Small but significant metals-in-soils anomalies and a small VLF-EM anomaly were identified. The survey results indicate justification for further exploration work.

PROPERTY INFORMATION, DESCRIPTION:

The Arlington Silver property is located in the Slocan Mining Division on NTS map sheet 82F/14W at latitude 49 degrees, 48 minutes and at longitude 117 degrees 21 minutes. The property lies 12 kilometres east of Slocan City near the junction of Springer Creek and Speculator Creek.

At the Property, Cazador Explorations Limited is the recorded owner of the Spectwo (6074) modified grid claim, New Silver 1 through 4 (4576, 4577, 4578, 4579) two post claims as well as the Silver Leaf #2 (5763), Arlington #1 & #2 (2356, 2416), Burlington (2417) crown granted mineral claims, and the Eda Fraction (2363), Nancy (5259), Speculator (2361) crown granted mineral claims that have been converted to mineral leases M79 & M80.

The property encompasses the Arlington and Speculator which were former silver producing mines. The Enterprise silver mine, another former silver producer lies to the immediate north of the Property.

The property was extensively clear-cut logged during the mid 1980's.

Reference figure 1 for information on the project area location.

PROPERTY INFORMATION, PHYSIOGRAPHY:

Topography is steep but not overly rugged. Elevations range from 1430 to 2070 meters above sea level. Vegetation comprises alders and jackpine in the lower elevations to semi-alpine above 1900 meters. The Property is drained by Springer Creek flowing southwest and Speculator Creek flowing south. Along Springer Creek vegetation is thick, with fir and alders. The climate is typical of the Southern interior; snow conditions allow property work from late May to mid October.

PROPERTY INFORMATION, ACCESS:

Access to the Property is by way of a logging road, from Slocan City, that parallels Springer Creek for 12 kilometres. Old mine buildings and dumps from underground workings are visible at the roadside upon reaching Speculator Creek, a tributary to Springer Creek. The road then continues along Speculator Creek, within the Property, to the alpine elevations.

EXPLORATION HISTORY:

The Arlington Property was originally staked in the late 1800's and has been intermittently underground mined, since that period, for silver. The Arlington and Speculator mines have produced significant quantities of silver, zinc and lead, mainly during the turn of the Century.

The last period of extensive work was in 1981 by Sveinson Way Mineral Services when they opened the old Arlington workings and conducted underground drifting and development drilling.

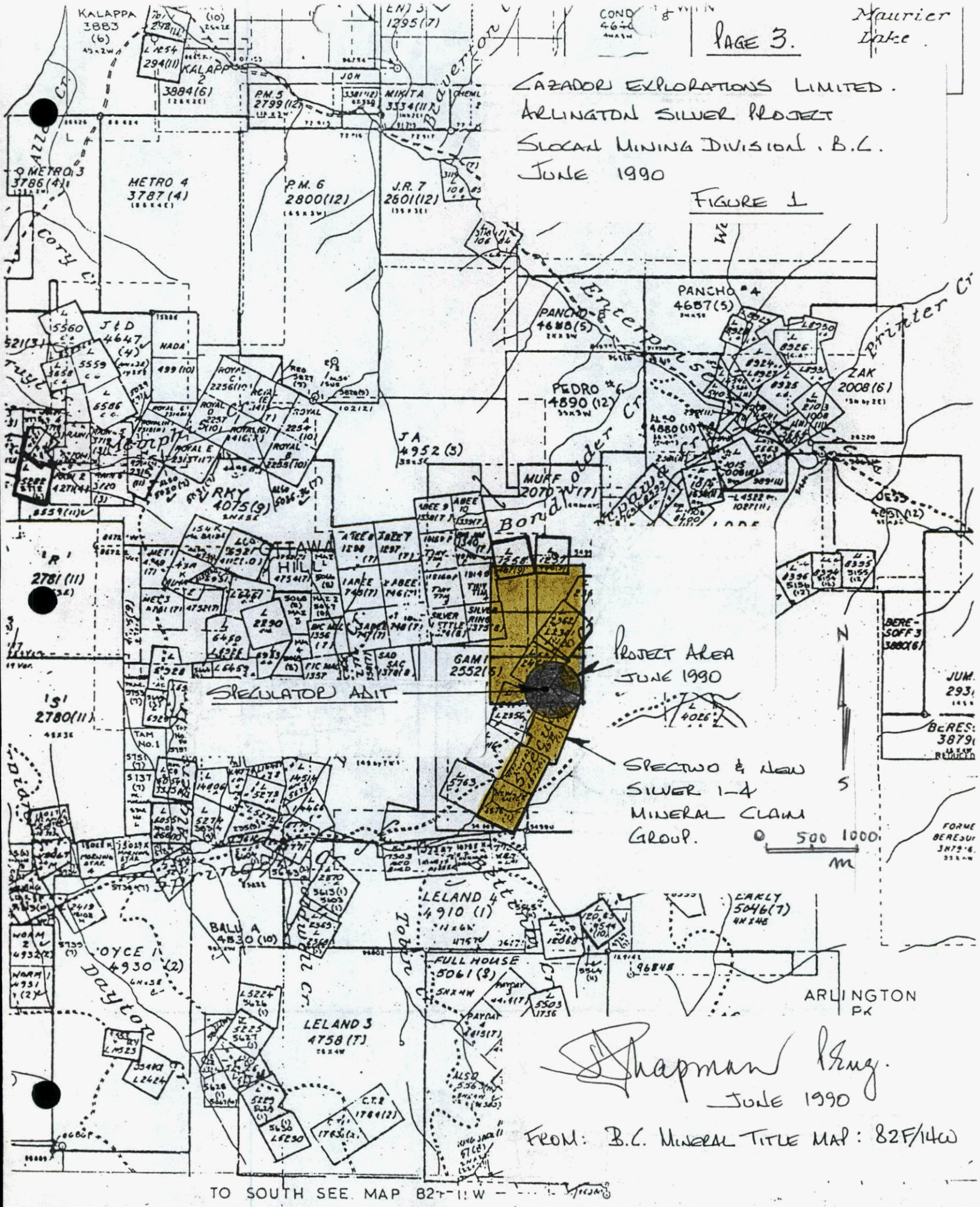
CURRENT EXPLORATION PROGRAM, OBJECTIVE:

The objective of the current exploration program was to explore, using surface methods, for possible mineralization in the hanging wall of the Arlington shear. The area near the Speculator adit was chosen and VLF-EM plus soil geochemistry were the exploration methods selected.

Maurier Lake

CAZADOR EXPLORATIONS LIMITED.
ARLINGTON SILVER PROJECT
SLOCAN MINING DIVISION, B.C.
JUNE 1990

FIGURE 1



TO SOUTH SEE MAP 82F-11W

S. Chapman P.Eng.
JUNE 1990

FROM: B.C. MINERAL TITLE MAP: 82F/14W

CURRENT EXPLORATION PROGRAM, THEORY:

In studying the large Arlington shear the model of the Comstock lode was considered appropriate. At the Comstock, bonanza semi-massive sulfide deposits occur in the hanging wall of a dipping shear between the 500 and 1500 foot levels, and leakage anomalies of arsenic, antimony and mercury are pathfinders to these bonanzas in the upper levels of the mineralized system. The current exploration program was designed to identify "leakage" metal-in-soils anomalies and buried near-surface, semi-massive sulfides in the hanging wall of the Arlington shear.

This theory was supported by zones of red mineral soils, east of the Speculator adit, in a recently logged area.

CURRENT EXPLORATION PROGRAM, EQUIPMENT:

Survey lines and stations were established using compass and hip-chain. A Phoenix VLF-2 instrument was used for the VLF-EM survey.

CURRENT EXPLORATION PROGRAM, PROCEDURES:

There were seven lines established at 50 meter intervals, they were located at an azimuth of 35 degrees to conform to an earlier grid established by Sveinson Way Mineral Services in 1981. A compass declination of 22 degrees and 29 minutes was utilized. Stations were established along each line at 25 meter intervals, and marked with ribbon and an aluminum tag.

The old Speculator adit near Speculator Creek was used as the starting reference point for the 1990 survey. This station was field marked as 2270N/550E and has been plotted in this report as 2280N/610E. This adjustment was necessary as an error was made in the field in selecting the proper coordinates to match the 1981 grid. All field stations require adding 10 meters north and 60 meters east to conform to the plotted coordinates in this report.

Soil samples were taken from the "B" soil horizon at each of the 118 stations. Sample analyses (30 element ICP) was done by Acme Analytical Laboratories Ltd. in Vancouver, B.C. Reference Appendix A for details of analysis technique. The geochemical analyses of each metal considered of interest has been plotted and presented as maps in Appendix D.

VLF-EM readings were taken at each of the 118 stations. The Hawaii transmitter was utilized on June 28th and the Seattle transmitter was used thereafter. It is not a normal procedure to change transmitters, however Seattle was not transmitting on June 28th. The VLF-EM readings were Fraser Filtered and then plotted and are presented in Appendix C of this report.

CURRENT EXPLORATION PROGRAM, RESULTS:

There were two main metals-in soils anomalies: (1) silver, lead, cadmium were anomalous over the known shear near the Speculator adit, and (2) all elements, except for gold, showed some elevation near 850 east and 950 east.

There was one low order VLF-EM anomaly within the shear at 2180N/660E, just southeast of the Speculator adit.

CURRENT EXPLORATION PROGRAM, DISCUSSION:

The metals-in-soils located in the southeast corner of the study area are significant. While there is no definite epithermal "finger print" the proximal silver, mercury, zinc and cadmium may represent a leakage halo from the Arlington shear hanging wall. The antimony data, normally a good epithermal precious metals pathfinder, was not plotted as no anomalous values were detected.

The VLF-EM technique is useful in defining the main Arlington shear zone. However, that was not the purpose of its application in this exploration program. No positive anomalies were located in the hanging wall area.

CONCLUSIONS:

The survey demonstrated that there is potential for discovery of mineralization in the hanging wall side of the Arlington shear. Whether the soil anomaly is transported or the result of hanging wall "leakage" or a parallel system will only be determined with further and more detailed exploration.

RECOMMENDATIONS:

The survey area should be extended to the east and south to fully cover the silver anomaly and cadmium anomaly detected near the southeast corner of the 1990 grid. Fill-in lines should be established between the existing grid lines and targets selected for deep drilling into the Arlington shear hanging wall. Pulse EM should be utilized in any future drilling as a follow-up to assist in the possible location of semi-massive sulfides, which do occur at the Arlington and Speculator. No major work should be undertaken until silver prices improve.

STATEMENT OF COSTS:

Mob/demob	$ 700
Personnel (note 1)	1,500
Meals & accommodation	250
Equipment rental	200
Field supplies	150
Geoanalysis	1,400
Report preparation	1,200
TOTAL EXPLORATION EXPENDITURES	$5,400

Note 1: The crew during the four day program included John A. Chapman B.Sc., P.Eng., Project Manager and Brett Sveinson, Field Assistant.

STATEMENT OF QUALIFICATION:

I John Arthur Chapman of the City of Surrey, British Columbia, Canada hereby certify as follows:

I am a mining engineer residing at #30 1725 Southmere Cr., Surrey, British Columbia and,

I graduated with honours in Mining Technology from the British Columbia Institute of Technology, June 1967 and,

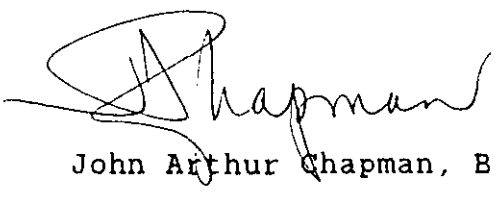
I graduated with honours in Mining Engineering (B.Sc.) from the Colorado School of Mines, January 1971 and,

I am a Professional Engineer registered in the Province of British Columbia since 1973 and,

I have practised my profession continuously since 1973 in Canada, United States and Philippines and,

I hold an indirect interest in the Arlington property, through my major shareholding in Cazador Explorations Limited, which is the subject of this report and,

I am the author of this report, which is based upon work on the Arlington project, which I personally supervised during 1990.



John Arthur Chapman, B.Sc., P.Eng.

APPENDIX A

ACME ANALYTICAL LABORATORIES LTD. 852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6 PHONE(604)253-3158 FAX(604)253-1716

GEOCHEMICAL ANALYSIS CERTIFICATE

Cazador Explorations Ltd. PROJECT ARLINGTON File # 90-2162 Page 1

902 - 626 W. Pender St., Vancouver BC V6B 1V9 Submitted by: JOHN A. CHAPMAN

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb	Hg ppb
AS #1	1	9	32	138	.4	6	7	410	4.52	10	5	ND	13	13	.2	3	2	48	.39	.422	19	15	.46	42	.09	4	5.01	.01	.08	1	3	80
AS #2	1	11	29	78	.4	6	5	276	4.02	9	5	ND	8	11	.2	2	2	55	.13	.127	14	14	.31	45	.15	4	2.90	.01	.09	1	4	90
AS #3	1	7	45	94	.2	5	5	275	4.02	6	5	ND	6	20	.2	2	2	49	.27	.116	17	16	.47	85	.12	6	2.21	.01	.12	2	3	60
AS #4	1	6	17	92	.3	3	6	374	3.08	5	5	ND	4	13	.2	3	2	35	.30	.209	16	10	.35	65	.07	5	2.22	.01	.06	1	2	40
AS #5	1	6	19	77	.3	5	6	286	3.60	3	5	ND	8	16	.2	2	2	41	.35	.187	18	12	.42	64	.08	3	2.29	.01	.09	1	1	50
AS #6	1	7	26	88	.4	8	7	321	3.25	2	5	ND	9	11	.2	2	2	41	.21	.134	20	16	.45	59	.09	6	2.91	.01	.09	2	4	40
AS #7	1	6	15	71	.3	4	5	285	3.24	2	5	ND	5	11	.2	2	2	46	.12	.119	14	14	.28	57	.10	10	1.67	.01	.06	1	1	40
AS #8	1	10	17	105	.6	12	9	764	3.67	8	5	ND	5	35	.2	2	2	46	.26	.069	17	21	.56	166	.12	6	3.11	.01	.09	2	1	30
AS #9	1	10	17	91	.5	8	6	303	3.95	6	5	ND	7	10	.2	2	2	47	.11	.114	12	19	.28	74	.13	4	3.77	.01	.06	1	2	80
AS #10	1	8	12	66	.2	5	5	192	3.54	8	5	ND	6	9	.2	3	2	52	.11	.095	11	16	.22	46	.13	2	2.47	.01	.06	1	1	50
AS #11	1	8	21	111	.3	9	9	355	4.25	6	5	ND	8	13	.2	2	3	48	.17	.192	16	19	.42	78	.12	9	3.51	.01	.08	1	4	60
AS #12	1	9	28	94	.4	8	5	177	3.75	12	5	ND	6	9	.2	2	2	43	.10	.252	8	17	.23	55	.13	2	4.96	.01	.05	1	1	80
AS #13	1	5	18	62	.1	3	4	448	2.12	2	5	ND	4	8	.2	2	2	32	.10	.080	9	9	.16	44	.10	5	1.80	.01	.04	1	2	50
AS #14	1	8	20	122	.2	7	8	710	3.21	6	5	ND	7	14	.2	2	2	39	.22	.140	17	15	.41	101	.12	4	2.75	.01	.08	1	1	50
AS #15	1	8	19	117	.2	6	7	764	3.06	6	5	ND	6	11	.2	2	2	40	.17	.145	15	14	.38	78	.12	4	2.37	.01	.09	1	1	30
AS #16	1	7	29	117	.3	7	6	510	3.53	4	5	ND	5	9	.2	3	2	45	.13	.151	11	14	.28	67	.13	3	2.52	.01	.07	1	1	60
AS #17	1	9	28	154	.7	7	8	364	4.26	3	5	ND	8	14	.2	2	2	49	.24	.149	27	17	.49	89	.14	7	3.68	.01	.11	2	1	70
AS #18	1	9	27	136	.1	8	7	717	3.67	8	5	ND	5	16	.2	2	2	44	.28	.191	16	17	.54	103	.12	6	2.79	.01	.11	1	2	60
AS #19	1	8	29	118	.3	7	7	517	3.15	4	5	ND	5	13	.2	2	2	40	.18	.162	12	16	.34	86	.13	5	2.56	.01	.07	2	1	50
AS #20	1	11	32	153	.6	11	15	634	4.74	7	5	ND	7	29	.8	2	3	56	.27	.104	17	24	.68	164	.17	4	3.67	.01	.13	1	1	40
AS #21	1	11	25	129	.6	11	10	733	4.26	4	5	ND	8	50	.2	2	2	46	.50	.077	31	40	.84	207	.10	2	3.32	.01	.19	1	2	30
AS #22	1	8	43	90	.4	7	6	545	2.70	5	5	ND	3	21	.5	3	2	38	.27	.094	12	15	.38	94	.10	4	1.66	.01	.08	1	4	40
AS #23	1	10	31	126	.5	13	9	825	4.15	7	7	ND	8	57	.7	2	2	53	.54	.049	33	31	.90	242	.12	6	3.34	.01	.16	1	2	30
AS #24	1	6	25	79	.5	5	8	480	3.02	4	5	ND	7	14	.2	2	2	40	.17	.121	18	16	.32	87	.12	5	3.24	.01	.06	1	1	70
AS #25	1	7	21	77	.8	5	4	325	4.05	3	5	ND	6	9	.2	2	2	50	.12	.152	10	17	.26	65	.14	4	4.39	.01	.05	1	1	90
AS #26	1	6	19	82	.4	6	6	431	3.38	9	5	ND	7	12	.2	3	2	43	.17	.119	15	18	.39	62	.11	3	2.87	.01	.07	1	1	60
AS #27	2	6	33	76	.8	7	5	233	3.46	5	5	ND	7	10	.2	2	2	37	.13	.079	14	13	.26	51	.11	3	3.67	.01	.05	7	1	100
AS #28	1	4	18	61	.2	4	4	141	3.21	4	5	ND	4	11	.2	2	2	52	.12	.041	12	10	.25	59	.12	3	1.37	.01	.07	1	1	40
AS #29	1	9	25	76	.7	5	7	798	3.20	3	5	ND	1	30	.3	2	2	37	.26	.083	37	13	.42	106	.05	3	2.28	.01	.10	1	1	70
AS #30	1	4	21	69	.5	3	4	340	2.78	2	5	ND	6	10	.2	2	2	38	.15	.104	16	9	.28	45	.09	2	1.48	.01	.07	1	1	40
AS #31	1	8	32	121	.6	4	7	337	3.82	8	5	ND	9	14	.2	2	2	44	.31	.201	22	13	.47	59	.10	6	3.28	.01	.10	1	2	60
AS #32	1	7	28	85	.6	5	5	423	3.24	8	5	ND	5	10	.2	2	2	41	.17	.135	17	10	.28	45	.10	4	2.65	.01	.07	1	1	90
AS #33	1	7	22	107	.6	2	6	372	3.66	5	5	ND	9	12	.2	2	2	42	.38	.208	24	10	.41	48	.10	8	2.45	.01	.09	1	1	80
AS #34	2	8	39	114	1.0	3	8	453	4.29	6	5	ND	11	13	.4	2	2	58	.15	.093	16	18	.57	73	.13	4	3.38	.01	.10	1	1	70
AS #35	2	5	33	106	.5	5	6	307	4.16	2	5	ND	5	17	.2	2	2	57	.21	.066	14	14	.48	80	.14	7	1.75	.01	.09	1	1	40
AS #36	2	4	108	214	1.3	2	7	409	4.13	2	5	ND	9	14	.2	2	2	49	.27	.096	24	12	.63	76	.07	2	2.59	.01	.15	1	2	60
STANDARD C/AU-S	18	57	36	131	7.2	67	30	1032	4.10	40	17	6	36	48	17.5	15	20	55	.53	.096	37	57	.91	172	.08	38	1.97	.06	.13	11	53	1500

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Soil -80 Mesh AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUL 3 1990 DATE REPORT MAILED: July 9/90 SIGNED BY..... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb	Hg ppb
AS #37	1	6	115	182	.7	7	8	637	3.90	2	5	ND	11	20	.2	2	4	47	.59	.179	36	10	.75	89	.10	2	1.99	.01	.18	1	3	40
AS #38	1	4	31	125	.1	6	7	483	4.01	2	5	ND	4	23	.2	2	3	54	.32	.110	13	8	.68	81	.15	2	1.85	.01	.12	1	1	20
AS #39	1	7	24	66	.3	5	4	482	3.54	2	5	ND	4	8	.2	2	3	54	.11	.111	10	9	.20	40	.15	2	1.77	.01	.05	2	5	50
AS #40	1	8	18	77	.9	4	5	363	3.49	5	5	ND	6	9	.2	2	2	46	.14	.170	12	10	.29	38	.13	4	2.51	.01	.06	1	6	60
AS #41	1	10	22	136	.4	9	7	466	3.73	4	5	ND	9	13	.2	2	2	47	.21	.175	19	13	.60	63	.13	2	3.67	.01	.12	1	3	50
AS #42	1	6	23	107	.2	6	7	607	3.52	3	5	ND	20	19	.8	2	4	42	.57	.236	37	10	.65	75	.11	5	2.13	.01	.16	1	3	30
AS #43	1	7	24	82	.2	6	5	515	3.88	2	5	ND	3	15	.2	2	2	54	.19	.099	11	9	.33	67	.13	2	1.50	.01	.07	2	2	50
AS #44	1	11	19	48	1.8	4	4	147	2.61	4	5	ND	3	8	.4	2	2	35	.07	.116	6	7	.15	38	.13	7	3.68	.01	.04	1	1	90
AS #45	1	7	25	63	.4	4	4	176	3.14	2	5	ND	7	8	.2	2	3	39	.08	.098	13	11	.26	40	.09	2	3.11	.01	.06	1	1	70
AS #46	1	6	29	90	.2	6	6	250	3.31	4	5	ND	15	12	.2	2	2	37	.23	.171	21	9	.42	47	.06	2	2.67	.01	.08	1	1	50
AS #47	1	7	23	66	.1	4	4	309	2.91	4	5	ND	4	10	.2	2	2	41	.12	.071	11	8	.24	44	.09	2	1.51	.01	.06	1	1	30
AS #48	1	6	16	81	.1	5	4	215	3.64	3	5	ND	5	13	.2	2	2	40	.21	.106	16	10	.41	69	.11	5	1.71	.01	.08	1	4	20
AS #49	1	9	41	95	.4	8	6	813	2.99	7	5	ND	1	21	.2	2	2	40	.19	.070	18	11	.37	172	.11	3	2.02	.01	.09	2	4	50
AS #50	1	8	23	80	.7	8	6	450	3.32	2	5	ND	3	28	.2	2	4	43	.21	.045	20	14	.40	186	.11	2	1.92	.01	.08	2	1	40
AS #51	1	7	18	102	.4	8	5	208	4.00	5	5	ND	6	10	.2	2	2	46	.11	.170	12	15	.29	68	.11	3	3.41	.01	.07	1	3	80
AS #52	1	8	18	72	.3	6	5	208	3.80	2	5	ND	8	10	.2	2	2	50	.11	.171	16	13	.28	52	.10	2	2.37	.01	.06	2	4	60
AS #53	1	5	16	43	.1	3	3	332	1.97	2	5	ND	5	9	.2	2	2	31	.07	.053	15	6	.13	37	.06	2	1.42	.01	.04	1	3	40
AS #54	1	9	32	109	.1	7	7	552	3.35	6	5	ND	8	12	.2	2	2	43	.14	.127	16	14	.44	77	.09	6	2.79	.01	.08	1	1	60
AS #55	1	9	22	107	.2	9	8	418	3.10	4	5	ND	8	10	.2	2	2	40	.11	.108	14	13	.33	89	.12	3	4.05	.01	.06	2	1	80
AS #56	2	5	21	61	.1	6	4	289	2.31	2	5	ND	6	9	.2	2	2	32	.13	.083	12	11	.30	61	.09	4	1.85	.01	.04	7	1	50
AS #57	1	3	14	44	.1	3	2	266	1.72	2	5	ND	3	6	.2	2	2	26	.08	.044	8	6	.15	39	.06	2	1.00	.01	.03	1	5	40
AS #58	1	5	13	44	.1	4	3	196	1.82	3	5	ND	3	7	.2	2	2	27	.07	.058	8	8	.16	42	.06	3	1.18	.01	.03	1	2	40
AS #59	1	4	10	52	.1	4	4	370	1.72	13	5	2	2	10	.7	7	2	27	.10	.064	7	9	.21	68	.07	7	.93	.01	.03	1	3	30
AS #60	3	6	38	131	.1	6	6	499	3.80	3	5	ND	7	12	.2	2	5	45	.16	.145	13	11	.42	82	.11	2	2.58	.01	.12	9	3	40
AS #61	2	12	46	114	2.2	13	10	1142	4.77	4	5	ND	6	63	.2	2	2	60	.44	.065	43	18	.57	215	.15	2	4.20	.02	.14	2	2	50
AS #62	1	8	24	114	.5	9	9	456	3.87	2	5	ND	8	26	.4	2	2	49	.46	.136	24	15	.84	130	.13	2	2.57	.01	.12	1	1	30
AS #63	2	10	16	97	.1	8	7	242	3.49	5	5	ND	5	13	.2	2	2	48	.14	.136	10	15	.41	96	.15	4	3.10	.01	.08	1	1	40
AS #64	1	9	15	128	.4	17	11	773	3.88	6	5	ND	4	58	.7	2	2	58	.67	.149	24	30	.99	147	.23	4	2.67	.02	.09	2	1	40
AS #65	1	9	26	102	.6	10	7	353	3.60	3	5	ND	5	32	.2	2	2	45	.39	.110	27	16	.58	143	.12	6	2.76	.01	.12	1	1	60
AS #66	1	6	20	64	.2	6	4	151	2.98	5	5	ND	4	15	.2	2	2	37	.15	.119	10	9	.23	64	.11	7	2.27	.01	.05	1	5	40
AS #67	1	10	30	56	.8	6	4	196	3.43	9	5	ND	9	19	.2	2	2	39	.21	.166	16	12	.24	82	.16	3	4.49	.01	.05	1	1	80
AS #68	1	10	28	127	1.1	16	9	1105	4.41	5	5	ND	9	43	.5	2	2	56	.32	.067	23	24	.74	218	.14	5	4.40	.01	.14	1	2	40
AS #69	1	7	24	68	.2	5	4	521	2.77	5	5	ND	5	13	.2	2	2	39	.15	.114	13	12	.29	67	.09	6	1.89	.01	.07	1	2	50
AS #70	1	6	18	62	.1	5	5	235	2.94	2	5	ND	7	11	.2	2	2	46	.13	.102	15	12	.32	50	.11	2	1.76	.01	.07	1	2	30
AS #71	1	9	17	33	.4	2	3	142	2.72	4	5	ND	5	6	.2	2	2	34	.05	.146	7	9	.10	16	.12	5	6.84	.01	.02	1	1	70
AS #72	1	5	45	112	.5	4	6	326	3.39	7	5	ND	9	29	.2	2	2	38	.32	.103	21	13	.53	83	.08	3	2.08	.01	.14	1	4	80
STANDARD C/AU-S	17	58	44	132	7.3	64	31	1024	4.11	42	18	8	36	47	17.8	16	19	57	.53	.098	36	56	.91	173	.07	38	1.92	.06	.13	12	51	1200

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb	Hg ppb
AS #73	1	7	21	60	.4	5	4	273	2.74	4	5	ND	4	8	.2	2	2	39	.12	.135	13	8	.20	44	.10	2	1.85	.01	.05	1	3	40
AS #74	1	4	25	86	.3	5	4	450	3.26	2	5	ND	7	17	.2	2	2	39	.35	.191	21	8	.42	53	.07	2	1.80	.01	.08	1	10	50
AS #75	1	6	34	95	.3	6	6	331	3.64	4	5	ND	7	10	.2	2	2	45	.13	.132	16	9	.34	44	.10	2	2.59	.01	.08	1	1	50
AS #76	1	7	35	100	.3	8	7	327	3.80	5	5	ND	7	10	.2	2	2	48	.11	.141	20	10	.31	55	.11	2	2.92	.01	.06	1	2	60
AS #77	1	7	25	64	.2	7	5	174	3.72	4	5	ND	7	9	.2	2	5	47	.13	.118	14	10	.30	39	.10	5	2.26	.01	.06	1	4	40
AS #78	1	5	20	58	.3	3	4	170	2.88	4	5	ND	5	10	.2	2	2	40	.11	.119	13	8	.22	45	.10	2	2.16	.01	.06	1	1	50
AS #79	1	7	29	98	.4	8	6	240	3.80	4	5	ND	11	12	.3	2	3	42	.20	.123	20	11	.34	63	.11	2	3.90	.01	.08	2	8	70
AS #80	1	7	36	98	.4	7	6	640	3.50	14	5	ND	6	12	.4	2	2	41	.19	.200	14	11	.31	65	.11	2	3.40	.01	.07	1	2	60
AS #81	1	7	26	133	1.1	7	6	265	3.26	2	5	ND	8	12	.2	2	2	38	.15	.204	15	12	.35	72	.11	2	3.85	.01	.06	1	2	80
AS #82	1	5	24	78	3.3	7	6	303	3.77	4	5	ND	7	14	.2	2	2	45	.17	.059	24	9	.50	63	.11	2	2.35	.01	.12	1	4	60
AS #83	1	4	17	105	.3	5	7	290	4.09	2	5	ND	8	26	.7	2	7	47	.31	.160	22	13	.56	63	.13	4	3.40	.01	.11	1	2	50
AS #84	1	7	17	68	.1	6	4	412	2.85	6	5	ND	5	9	.2	2	2	39	.11	.138	12	8	.25	46	.11	2	2.07	.01	.06	1	2	40
AS #85	1	6	16	57	.1	6	4	158	3.31	4	5	ND	5	12	.2	2	2	46	.12	.067	11	9	.24	52	.11	2	1.79	.01	.06	1	2	50
AS #86	1	6	33	81	.3	7	5	276	2.70	2	5	ND	6	13	.2	2	2	34	.25	.129	15	11	.34	54	.07	2	1.94	.01	.08	1	17	50
AS #87	1	8	28	111	.6	5	6	262	3.54	3	5	ND	8	14	.4	2	2	40	.26	.220	23	12	.40	61	.09	2	3.37	.01	.09	1	1	80
AS #88	1	6	9	99	.3	7	6	268	3.40	5	5	ND	11	12	.2	2	2	41	.27	.169	17	15	.44	63	.08	4	2.67	.01	.09	1	3	50
AS #89	1	6	26	85	.3	10	6	232	3.36	2	5	ND	9	13	.2	2	2	43	.14	.091	17	15	.35	79	.11	2	2.82	.01	.07	1	5	50
AS #90	1	6	23	96	.2	10	5	345	3.83	6	5	ND	10	11	.2	2	2	44	.17	.390	16	16	.30	71	.08	2	3.46	.01	.05	1	1	60
AS #91	2	8	24	86	.3	8	6	496	4.41	7	5	ND	7	9	.2	2	6	51	.11	.176	13	16	.26	65	.12	3	3.45	.01	.05	3	5	70
AS #92	1	7	18	79	.4	8	5	260	3.72	3	5	ND	7	11	.2	2	2	43	.13	.156	12	16	.28	64	.11	3	4.29	.01	.05	1	1	120
AS #93	1	4	19	47	.1	5	4	204	2.42	4	5	ND	5	9	.2	4	2	40	.10	.048	15	9	.18	38	.08	3	1.22	.01	.03	1	4	30
AS #94	1	9	23	98	.1	10	8	839	2.96	3	5	ND	6	12	.2	2	2	42	.14	.093	17	15	.34	86	.12	2	2.66	.01	.08	2	1	60
AS #95	1	6	23	79	.1	9	6	279	3.16	4	5	ND	6	11	.2	2	3	45	.13	.087	13	13	.30	65	.11	4	2.22	.01	.05	1	3	40
AS #96	1	6	17	98	.2	9	7	260	3.31	6	5	ND	7	12	.6	2	2	43	.15	.122	14	14	.35	73	.11	2	2.81	.01	.06	1	1	50
AS #97	1	8	14	77	.4	9	6	475	3.07	3	5	ND	5	11	.2	2	2	41	.12	.116	12	14	.22	66	.10	2	2.60	.01	.05	1	1	70
AS #98	1	8	20	75	.1	12	6	863	3.14	10	5	ND	5	11	.3	2	2	43	.13	.123	13	12	.25	53	.11	2	2.00	.01	.06	2	2	40
AS #99	1	7	15	48	.2	6	4	223	2.43	2	5	ND	5	9	.2	3	2	36	.12	.070	13	8	.23	33	.09	4	1.44	.01	.04	1	7	60
AS #100	1	10	22	68	.6	7	6	184	2.77	4	5	ND	6	9	.2	2	2	40	.09	.105	13	15	.27	48	.12	2	3.75	.01	.06	2	3	70
AS #101	1	7	13	48	.2	5	4	424	3.00	3	5	ND	4	9	.2	2	2	44	.09	.117	10	12	.19	57	.11	2	1.75	.01	.04	1	1	60
AS #102	1	9	26	79	.4	9	5	239	3.14	2	5	ND	8	10	.6	2	2	39	.13	.160	15	14	.32	58	.09	3	3.54	.01	.06	1	1	90
AS #103	1	9	26	87	.3	8	5	262	3.64	6	5	ND	8	11	.2	2	2	44	.17	.172	16	16	.38	66	.10	8	3.74	.01	.07	1	1	80
AS #104	1	9	23	80	.3	7	5	181	3.12	9	5	ND	6	9	.3	2	2	39	.12	.121	11	11	.33	53	.11	2	3.68	.01	.07	2	1	70
AS #105	1	4	35	99	.2	7	7	323	3.20	2	5	ND	12	13	.2	2	3	38	.32	.151	25	12	.53	74	.09	2	2.53	.01	.12	1	2	30
AS #106	1	4	25	37	.1	3	3	122	3.17	6	5	ND	3	9	.4	2	2	56	.08	.102	10	7	.11	36	.14	2	1.33	.01	.04	1	1	40
AS #107	1	9	22	77	.2	7	6	247	4.59	5	5	ND	7	14	.2	2	2	62	.17	.181	15	16	.38	63	.13	2	2.57	.01	.09	1	1	50
AS #108	1	7	20	54	.5	6	4	536	2.68	2	5	ND	3	9	.2	2	2	39	.12	.106	12	7	.21	37	.08	2	1.56	.01	.06	1	1	40
STANDARD C/AU-S	17	58	36	132	7.3	68	31	1021	4.18	42	16	7	36	48	18.4	16	21	56	.53	.098	35	57	.92	173	.07	35	1.93	.06	.14	12	52	1400

SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W ppm	Au* ppb	Hg ppb
AS #109	1	3	24	51	.3	2	3	106	2.56	3	5	ND	3	7	.6	2	2	39	.07	.077	13	8	.16	34	.08	3	1.34	.01	.04	1	4	50
AS #110	1	3	22	85	.2	3	5	257	2.78	2	5	ND	10	14	.4	2	3	32	.42	.183	26	9	.45	47	.06	2	1.78	.01	.08	1	3	40
AS #111	1	6	35	208	.4	8	9	864	3.76	2	5	ND	9	11	.8	2	5	46	.11	.078	23	13	.55	83	.10	2	2.89	.01	.13	1	1	50
AS #112	1	5	33	124	.3	2	7	504	3.82	2	5	ND	9	12	.2	2	2	44	.20	.136	23	10	.43	65	.08	2	2.65	.01	.13	1	2	60
AS #113	1	6	29	120	.8	4	7	284	3.93	2	5	ND	9	9	.2	2	5	45	.11	.128	19	12	.43	48	.10	2	3.45	.01	.09	1	3	80
AS #114	1	3	47	116	.1	3	6	511	3.17	3	5	ND	12	16	.2	2	2	36	.46	.167	39	8	.52	67	.08	2	1.58	.01	.15	1	2	20
AS #115	1	3	36	49	.2	1	4	333	2.84	4	5	ND	3	13	.4	2	2	45	.11	.040	11	8	.22	63	.16	3	1.33	.01	.08	1	1	40
AS #116	1	4	27	61	.2	2	5	589	2.54	5	5	ND	5	10	.2	2	2	33	.18	.095	18	7	.31	44	.07	2	1.29	.01	.08	1	2	30
AS #117	1	7	20	95	.2	4	7	297	3.21	4	5	ND	7	11	.2	2	5	38	.17	.137	18	14	.46	61	.08	5	3.00	.01	.07	2	2	50
AS #118	1	4	29	60	.3	1	4	201	3.41	3	5	ND	5	7	.2	2	2	47	.09	.126	10	11	.22	47	.11	4	2.13	.01	.05	1	1	60
STANDARD C	18	58	36	133	7.2	66	29	1027	4.08	38	18	7	36	48	17.6	15	23	55	.52	.096	37	57	.91	173	.07	35	1.97	.06	.14	11	-	1300

APPENDIX B

CAZADOR EXPLORATIONS LIMITED, ARLINGTON PROJECT, JULY 1990
BASE DATA FOR COMPUTER GENERATED PLOTS

SAMPLE NUMBER	FIELD COORDINATES NORTH	FIELD COORDINATES EAST	PROJECT COORDINATES NORTH	PROJECT COORDINATES EAST	VLF/EM (RAW)	VLF/EM (ADJ#1)	VLF/EM (ADJ#2)	LEAD (ppm)	ZINC (ppm)	SILVER (ppm)	ARSENIC (ppm)	CADMIUM (ppm)	GOLD (ppb)	MERCURY (ppb)
AS96	2420	850	2430	910	13	25		17	98	0.2	6	0.6	1	50
AS97	2420	825	2430	885	12	24	-3	14	77	0.4	3	0.2	1	70
AS98	2420	800	2430	860	12	22	-7	20	75	0.1	10	0.3	2	40
AS99	2420	775	2430	835	10	17	-7	15	48	0.2	2	0.2	7	60
AS100	2420	750	2430	810	7	15	-1	22	68	0.6	4	0.2	3	70
AS101	2420	725	2430	785	8	18	3	13	48	0.2	3	0.2	1	60
AS102	2420	700	2430	760	10	18	-4	26	79	0.4	2	0.6	1	90
AS103	2420	675	2430	735	8	14	-4	26	87	0.3	6	0.2	1	80
AS104	2420	650	2430	710	6	14	0	23	80	0.3	9	0.3	1	70
AS105	2420	625	2430	685	8	14	-5	35	99	0.2	2	0.2	2	30
AS106	2420	600	2430	660	6	9	-7	25	37	0.1	6	0.4	1	40
AS107	2420	575	2430	635	3	7	2	22	77	0.2	5	0.2	1	50
AS108	2420	550	2430	610	4	11	7	20	54	0.5	2	0.2	1	40
AS109	2420	525	2430	585	7	14		24	51	0.3	3	0.6	4	50
AS110	2420	500	2430	560	7			22	85	0.2	2	0.4	3	40
AS95	2370	850	2380	910	12	26		23	79	0.1	4	0.2	3	40
AS94	2370	825	2380	885	14	26	-4	13	98	0.1	3	0.2	1	60
AS93	2370	800	2380	860	12	22	-10	19	47	0.1	4	0.2	4	30
AS92	2370	775	2380	835	10	16	-9	18	79	0.4	3	0.2	1	120
AS91	2370	750	2380	810	6	13	2	24	86	0.3	7	0.2	5	70
AS90	2370	725	2380	785	7	18	3	23	96	0.2	6	0.2	1	60
AS89	2370	700	2380	760	11	16	-8	26	85	0.3	2	0.2	5	50
AS88	2370	675	2380	735	5	10	-4	9	99	0.3	5	0.2	3	50
AS87	2370	650	2380	710	5	12	5	28	111	0.6	3	0.4	1	80
AS86	2370	625	2380	685	7	15	4	33	81	0.3	2	0.2	17	50
AS85	2370	600	2380	660	8	16	2	16	57	0.1	4	0.2	2	50
AS84	2370	575	2380	635	8	17	2	17	68	0.1	6	0.2	2	40
AS77	2370	550	2380	610	9	18	2	25	64	0.2	4	0.2	4	40
AS78	2370	525	2380	585	9	19	-2	20	58	0.3	4	0.2	1	50
AS79	2370	500	2380	560	10	16	-8	29	98	0.4	4	0.3	8	70
AS80	2370	475	2380	535	6	11	-12	36	98	0.4	14	0.4	2	60
AS81	2370	450	2380	510	5	4	-10	26	133	1.1	2	0.2	2	80
AS82	2370	425	2380	485	-1	1		24	78	3.3	4	0.2	4	60
AS83	2370	400	2380	460	2			17	105	0.3	2	0.7	2	50
AS60	2320	925	2330	985	16	34		38	131	0.1	3	0.2	3	40
AS59	2320	900	2330	960	18	31	-5	10	52	0.1	13	0.7	3	30
AS58	2320	875	2330	935	13	29	-4	13	44	0.1	3	0.2	2	40
AS57	2320	850	2330	910	16	27	-8	14	44	0.1	2	0.2	5	40
AS56	2320	825	2330	885	11	21	-9	21	61	0.1	2	0.2	1	50
AS55	2320	800	2330	860	10	18	-5	22	107	0.2	4	0.2	1	80
AS54	2320	775	2330	835	8	16	-2	32	109	0.1	6	0.2	1	60
AS53	2320	750	2330	810	8	16	2	16	43	0.1	2	0.2	3	40
AS52	2320	725	2330	785	8	18	2	18	72	0.3	2	0.2	4	60
AS51	2320	700	2330	760	10	18	-3	18	102	0.4	5	0.2	3	80
AS50	2320	675	2330	735	8	15	-4	23	80	0.7	2	0.2	1	40
AS49	2320	650	2330	710	7	14	2	41	95	0.4	7	0.2	4	50
AS48	2320	625	2330	685	7	17	5	16	81	0.1	3	0.2	4	20
AS47	2320	600	2330	660	10	19	1	23	66	0.1	4	0.2	1	30
AS46	2320	575	2330	635	9	18	0	29	90	0.2	4	0.2	1	50

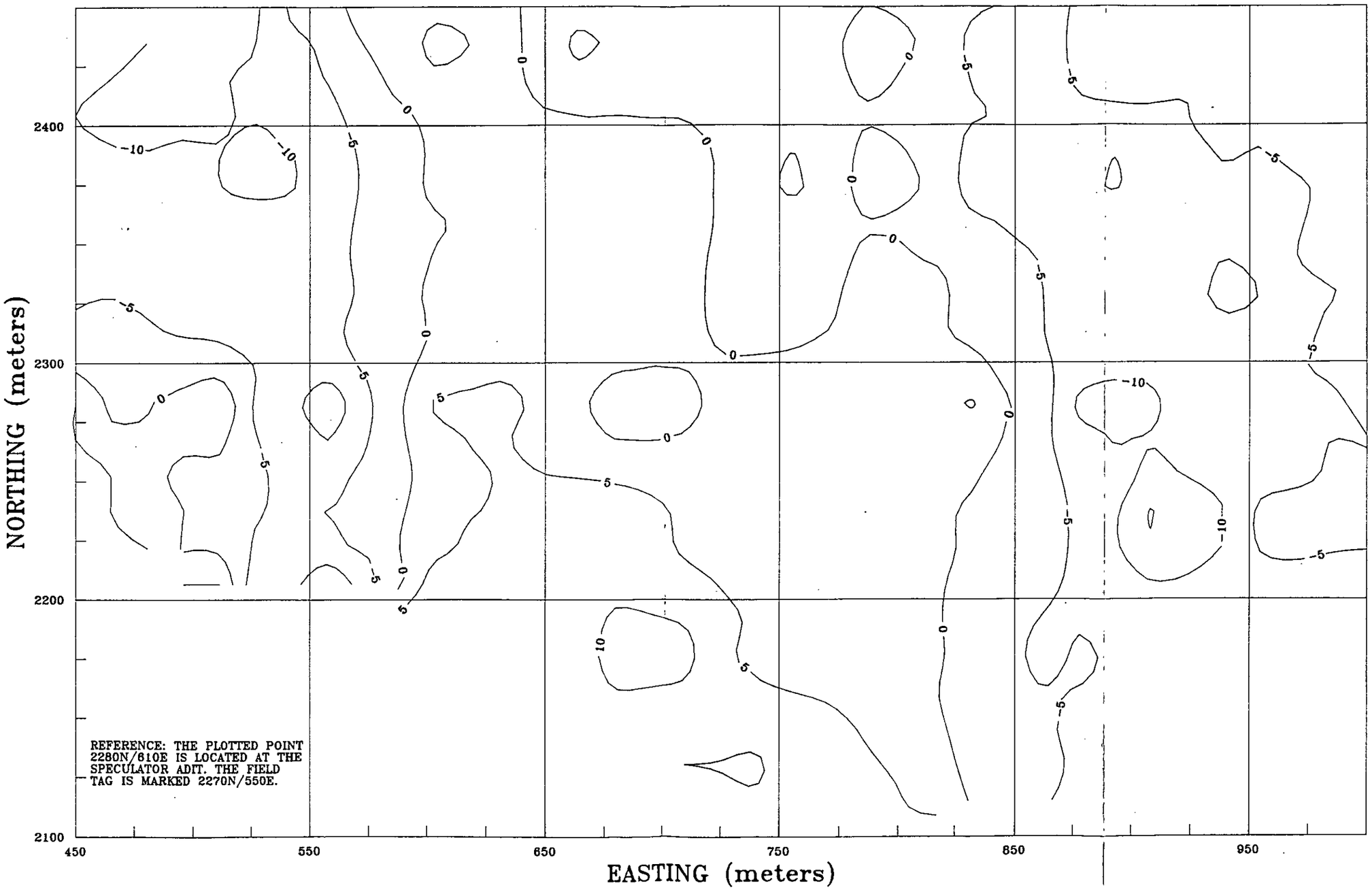
AS45	2320	550	2330	610	9	19	2	25	63	0.4	2	0.2	1	70
AS44	2320	525	2330	585	10	20	-2	19	48	1.8	4	0.4	1	90
AS43	2320	500	2330	560	10	17	-7	24	82	0.2	2	0.2	2	50
AS42	2320	475	2330	535	7	13	-7	23	107	0.2	3	0.8	3	30
AS41	2320	450	2330	510	6	10	-7	22	136	0.4	4	0.2	3	50
AS40	2320	425	2330	485	4	6		18	77	0.9	5	0.2	6	60
AS39	2320	400	2330	460	2			24	66	0.3	2	0.2	5	50
AS16	2270	925	2280	985	17	32		29	117	0.3	4	0.2	1	60
AS15	2270	900	2280	960	15	29	-5	19	117	0.2	6	0.2	1	30
AS14	2270	875	2280	935	14	27	-5	20	122	0.2	6	0.2	1	50
AS13	2270	850	2280	910	13	24	-11	18	62	0.1	2	0.2	2	50
AS12	2270	825	2280	885	11	16	-14	28	94	0.4	12	0.2	1	80
AS11	2270	800	2280	860	5	10	-3	21	111	0.3	6	0.2	4	60
AS10	2270	775	2280	835	5	13	6	12	66	0.2	8	0.2	1	50
AS9	2270	750	2280	810	8	16	4	17	91	0.5	6	0.2	2	80
AS8	2270	725	2280	785	8	17	2	17	105	0.6	8	0.2	1	30
AS7	2270	700	2280	760	9	18	2	15	71	0.3	2	0.2	1	40
AS6	2270	675	2280	735	9	19	2	26	88	0.4	2	0.2	4	40
AS5	2270	650	2280	710	10	20	-1	19	77	0.3	3	0.2	1	50
AS4	2270	625	2280	685	10	18	-4	17	92	0.3	5	0.2	2	40
AS3	2270	600	2280	660	8	16	1	45	94	0.2	6	0.2	3	60
AS2	2270	575	2280	635	8	19	7	29	78	0.4	9	0.2	4	90
AS1	2270	550	2280	610	11	23	8	32	138	0.4	10	0.2	3	80
AS33	2270	525	2280	585	12	27	-1	22	107	0.6	5	0.2	1	80
AS34	2270	500	2280	560	15	22	-15	39	114	1	6	0.4	1	70
AS35	2270	475	2280	535	7	12	-8	33	106	0.5	2	0.2	1	40
AS36	2270	450	2280	510	5	14	5	108	214	1.3	2	0.2	2	60
AS37	2270	425	2280	485	9	17		115	182	0.7	2	0.2	3	40
AS38	2270	400	2280	460	8			31	125	0.1	2	0.2	1	20
AS17	2220	925	2230	985	17	32		28	154	0.7	3	0.2	1	70
AS18	2220	900	2230	960	15	31	-2	27	136	0.1	8	0.2	2	60
AS19	2220	875	2230	935	16	30	-11	29	118	0.3	4	0.2	1	50
AS20	2220	850	2230	910	14	20	-18	32	153	0.6	7	0.8	1	40
AS21	2220	825	2230	885	6	12	-8	25	129	0.6	4	0.2	2	30
AS22	2220	800	2230	860	6	12	0	43	90	0.4	5	0.5	4	40
AS23	2220	775	2230	835	6	12	-1	31	126	0.5	7	0.7	2	30
AS24	2220	750	2230	810	6	11	1	25	79	0.5	4	0.2	1	70
AS25	2220	725	2230	785	5	13	6	21	77	0.8	3	0.2	1	90
AS26	2220	700	2230	760	8	17	3	19	82	0.4	9	0.2	1	60
AS27	2220	675	2230	735	9	16	0	33	76	0.8	5	0.2	1	100
AS28	2220	650	2230	710	7	17	4	18	61	0.2	4	0.2	1	40
AS29	2220	625	2230	685	10	20	9	25	76	0.7	3	0.3	1	70
AS30	2220	600	2230	660	10	26	9	21	69	0.5	2	0.2	1	40
AS31	2220	575	2230	635	16	29		32	121	0.6	8	0.2	2	60
AS32	2220	550	2230	610	13			28	85	0.6	8	0.2	1	90
AS61	2170	925	2180	985	16	30		46	114	2.2	4	0.2	2	50
AS62	2170	900	2180	960	14	28	-6	24	114	0.5	2	0.4	1	30
AS63	2170	875	2180	935	14	24	-10	16	97	0.1	5	0.2	1	40
AS64	2170	850	2180	910	10	18	-8	15	128	0.4	6	0.7	1	40
AS65	2170	825	2180	885	8	16	-4	26	102	0.6	3	0.2	1	60
AS66	2170	800	2180	860	8	14	-6	20	64	0.2	5	0.2	5	40
AS67	2170	775	2180	835	6	10	-4	30	56	0.8	9	0.2	1	80
AS68	2170	750	2180	810	4	10	2	28	127	1.1	5	0.5	2	40
AS69	2170	725	2180	785	6	12	4	24	68	0.2	5	0.2	2	50
AS70	2170	700	2180	760	6	14	2	18	62	0.1	2	0.2	2	30
AS71	2170	675	2180	735	8	14	3	17	33	0.4	4	0.2	1	70

AS72	2170	650	2180	710	6	17	12	45	112	0.5	7	0.2	4	80
AS73	2170	625	2180	685	11	26	14	21	60	0.4	4	0.2	3	40
AS74	2170	600	2180	660	15	31	6	25	86	0.3	2	0.2	10	50
AS75	2170	575	2180	635	16	32		34	95	0.3	4	0.2	1	50
AS76	2170	550	2180	610	16			35	100	0.3	5	0.2	2	60
AS118	2120	725	2130	785	5	11		29	60	0.3	3	0.2	1	60
AS117	2120	700	2130	760	6	14	8	20	95	0.2	4	0.2	2	50
AS116	2120	675	2130	735	8	19	11	27	61	0.2	5	0.2	2	30
AS115	2120	650	2130	710	11	25	10	36	49	0.2	4	0.4	1	40
AS114	2120	625	2130	685	14	29	7	47	116	0.1	3	0.2	2	20
AS113	2120	600	2130	660	15	32	5	29	120	0.8	2	0.2	3	80
AS112	2120	575	2130	635	17	34		33	124	0.3	2	0.2	2	60
AS111	2120	550	2130	610	17			35	208	0.4	2	0.8	1	50

NOTE: VLF-EM (ADJ#2) represents Fraser Filtered Value

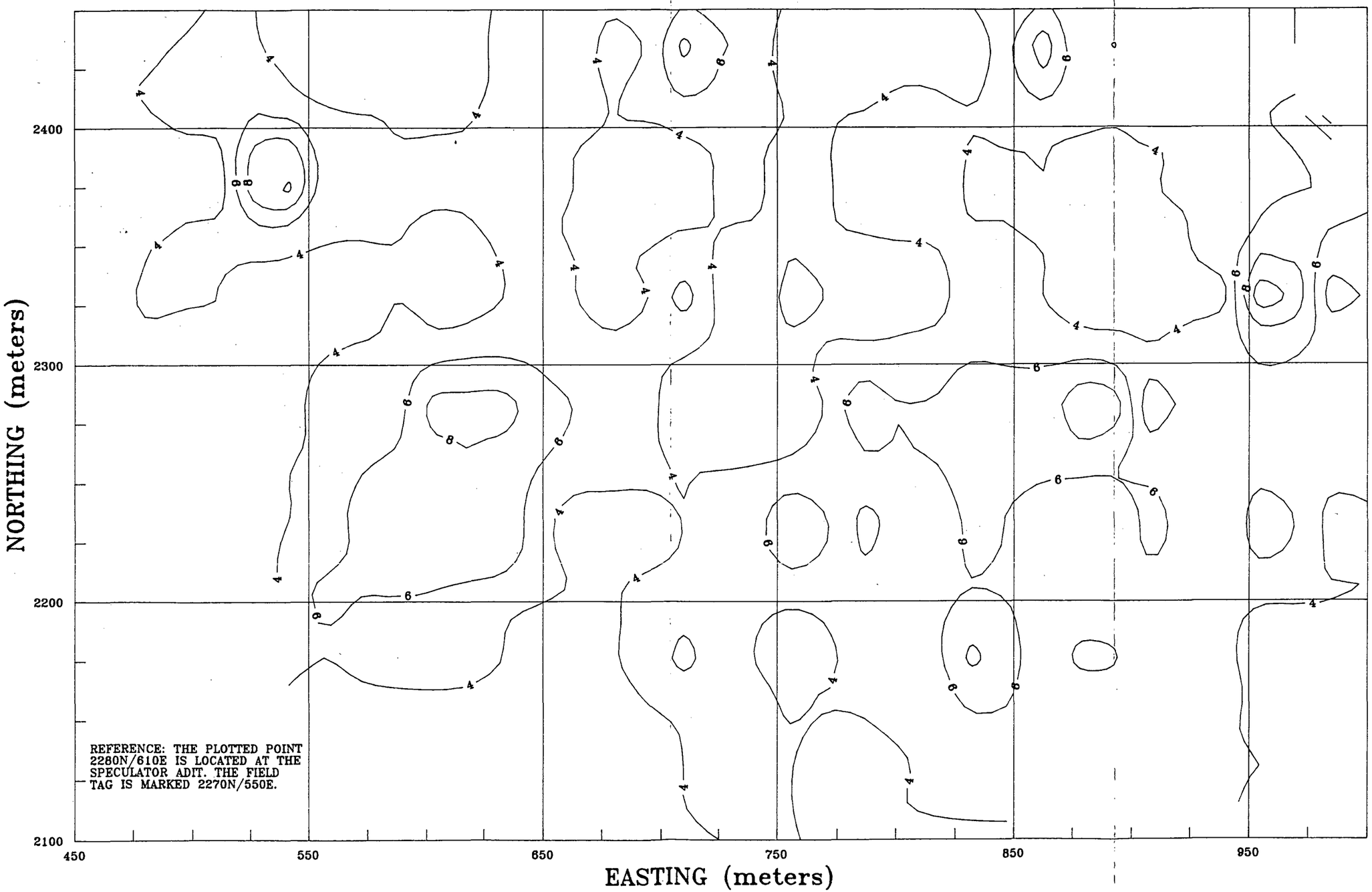
APPENDIX C

ARLINGTON SILVER PROJECT, FRASER FILTERED VLF-EM, JULY 1990
CAZADOR EXPLORATIONS LIMITED

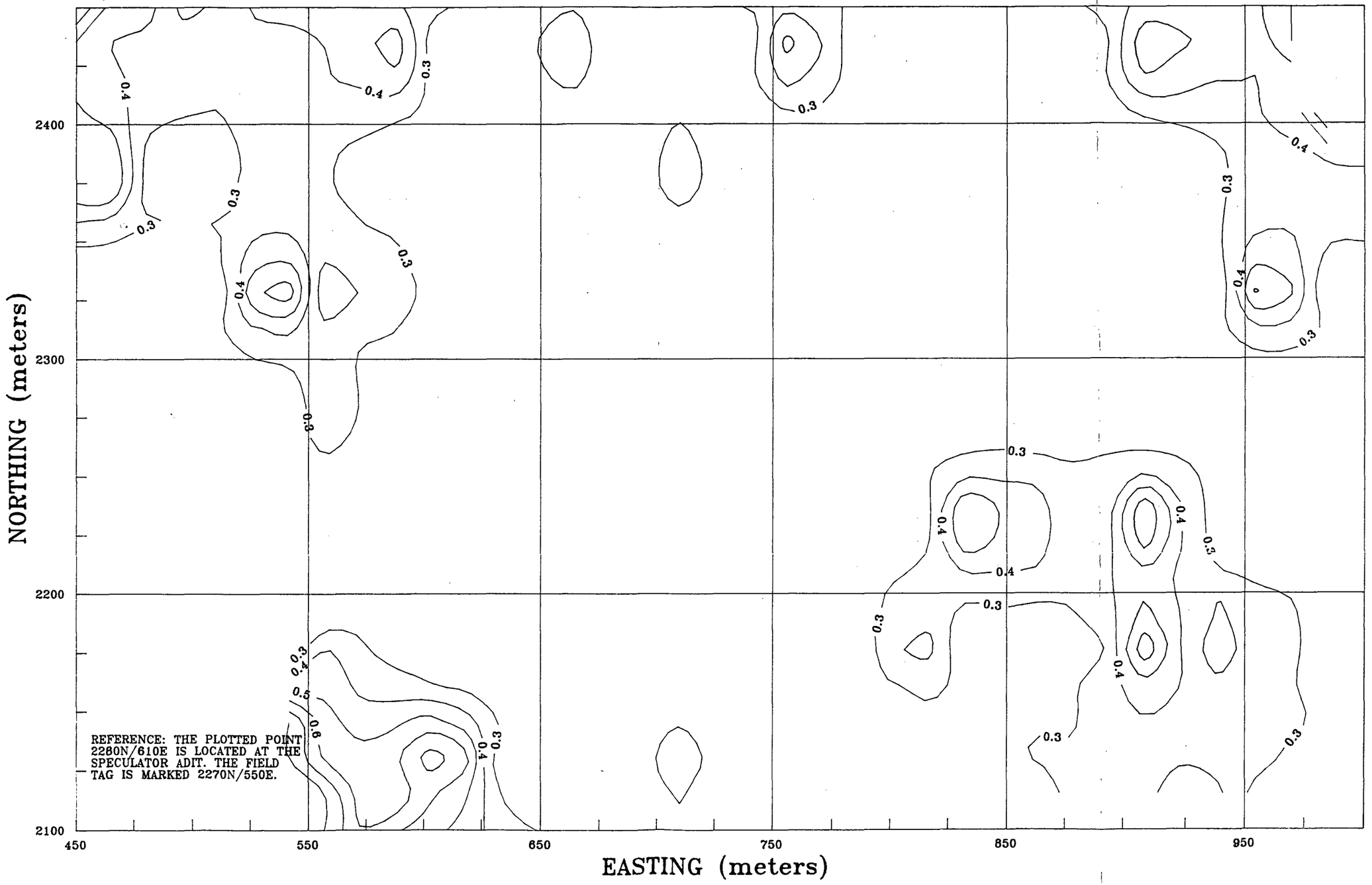


APPENDIX D

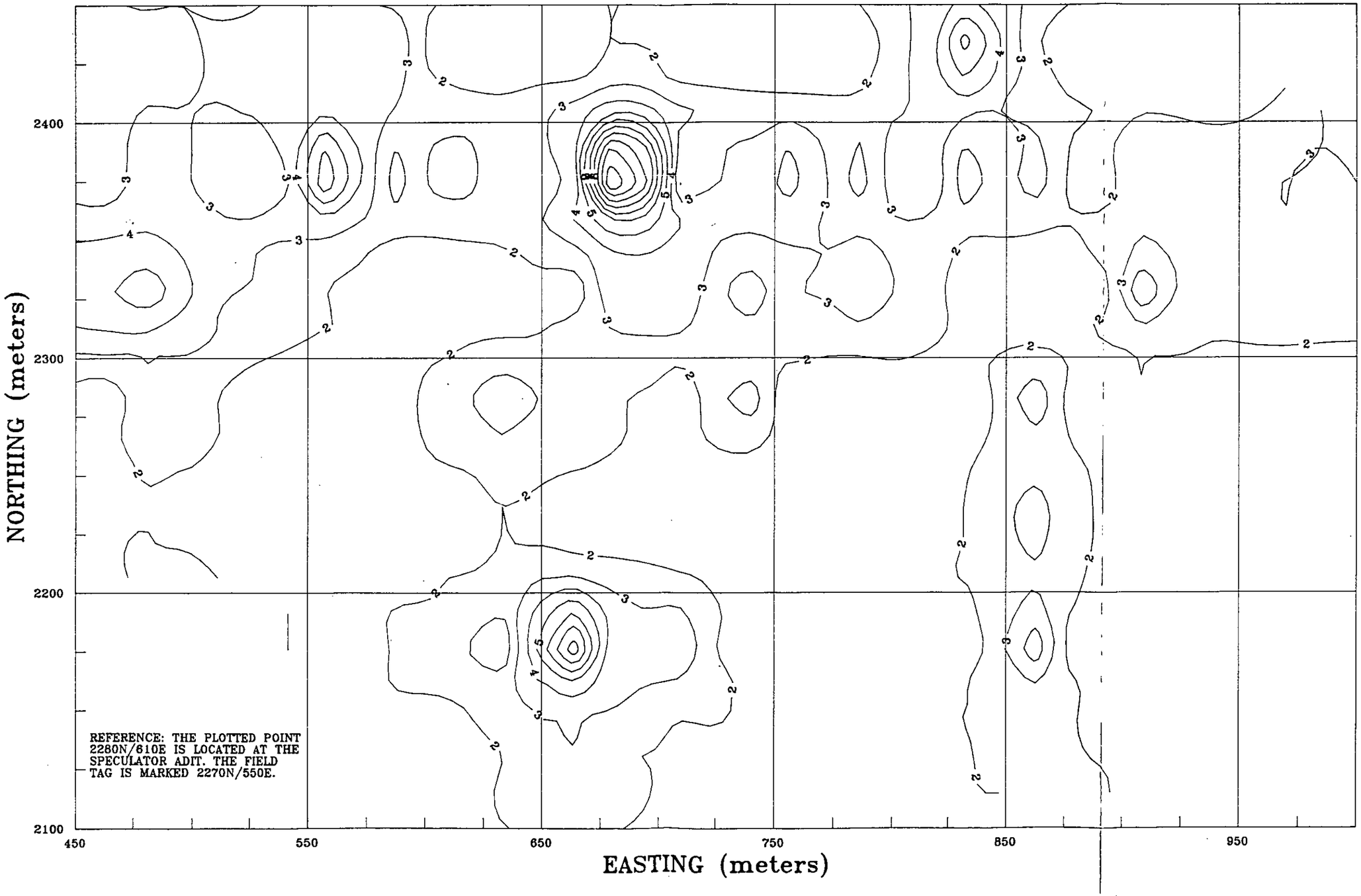
ARLINGTON SILVER PROJECT, ARSENIC IN SOILS (ppm), JULY 1990
CAZADOR EXPLORATIONS LIMITED



ARLINGTON SILVER PROJECT, CADMIUM IN SOILS (ppm), JULY 1990
CAZADOR EXPLORATIONS LIMITED

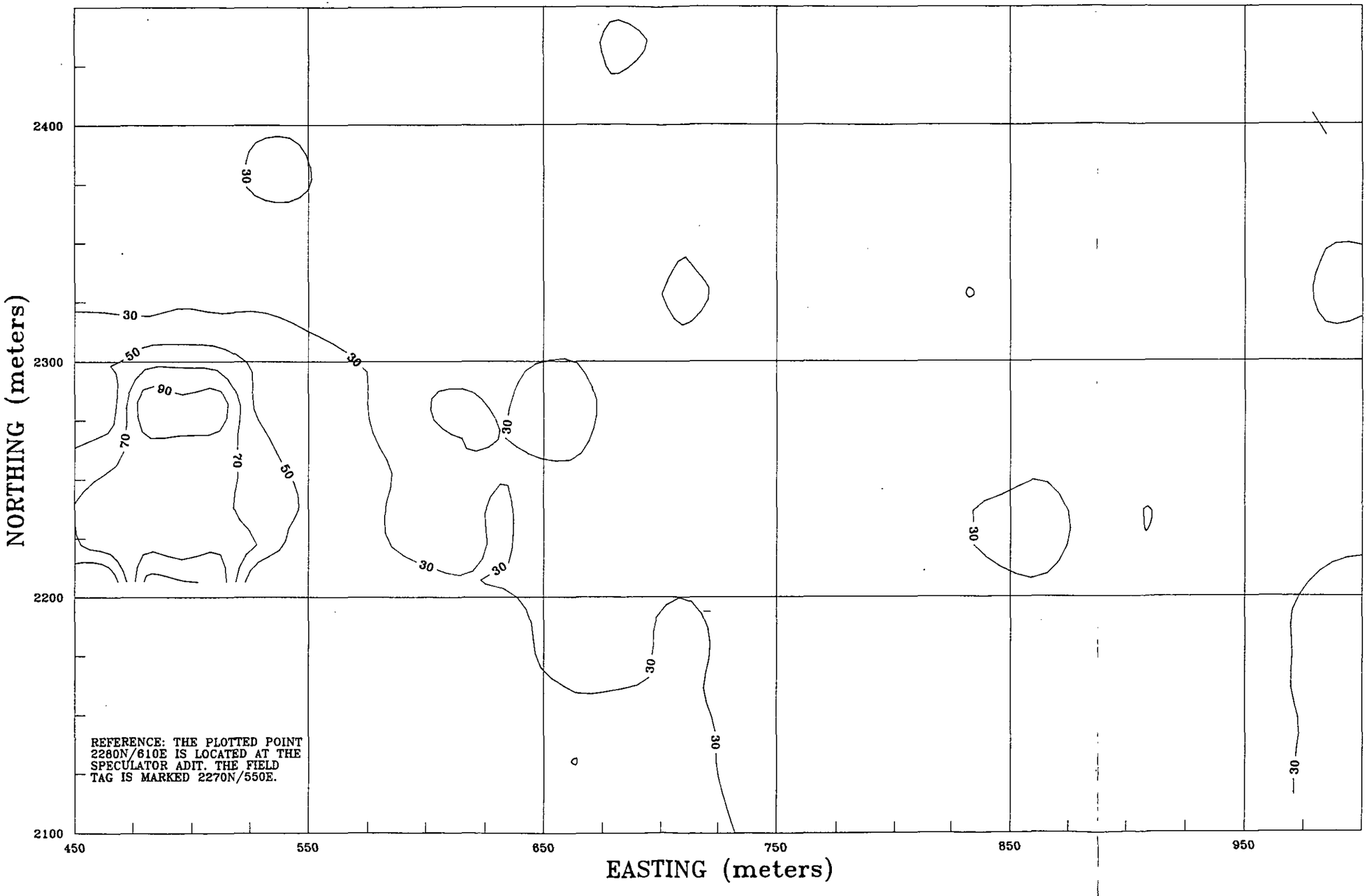


ARLINGTON SILVER PROJECT, GOLD IN SOILS (ppb), JULY 1990
CAZADOR EXPLORATIONS LIMITED

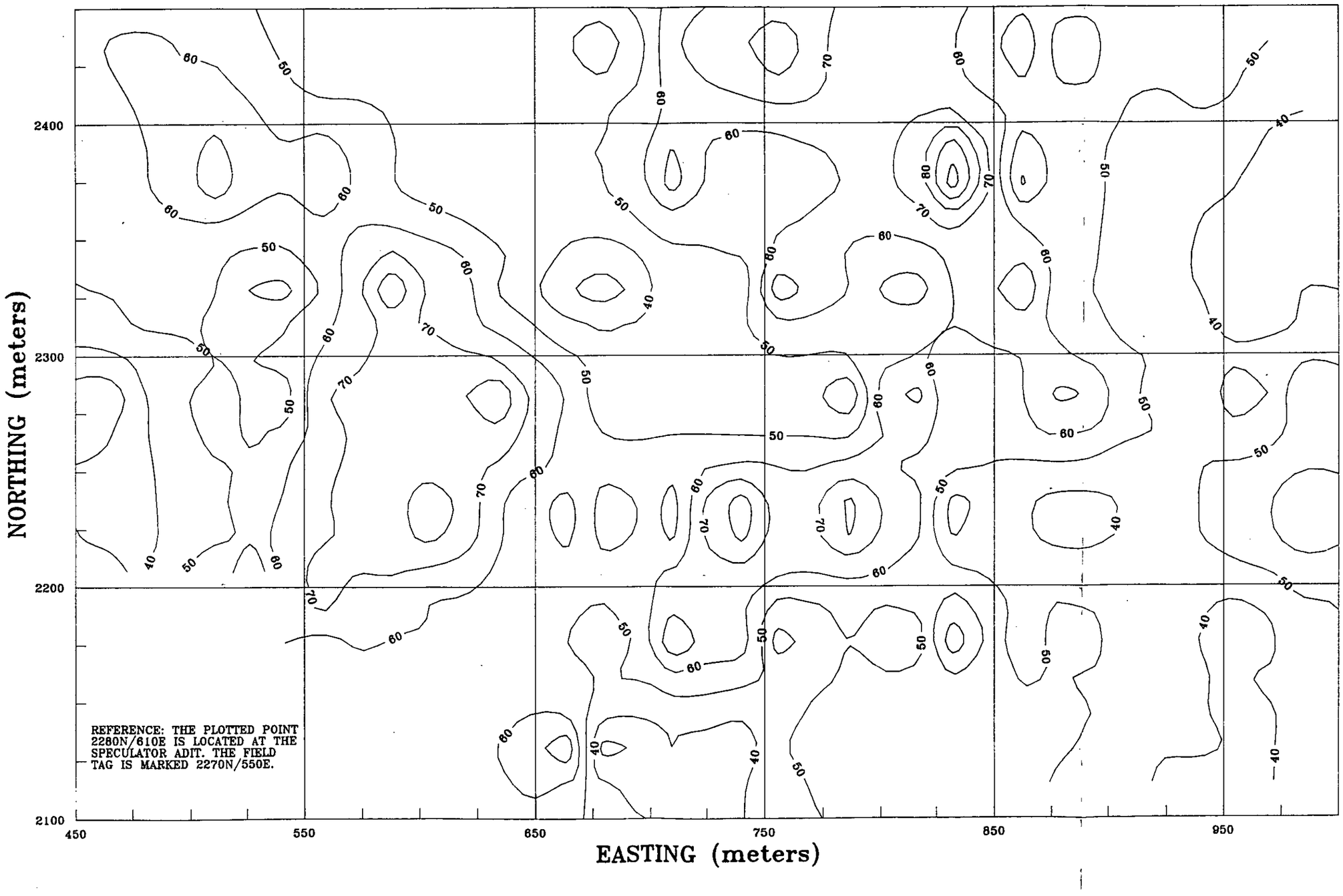


ARLINGTON SILVER PROJECT, LEAD IN SOILS (ppm), JULY 1990

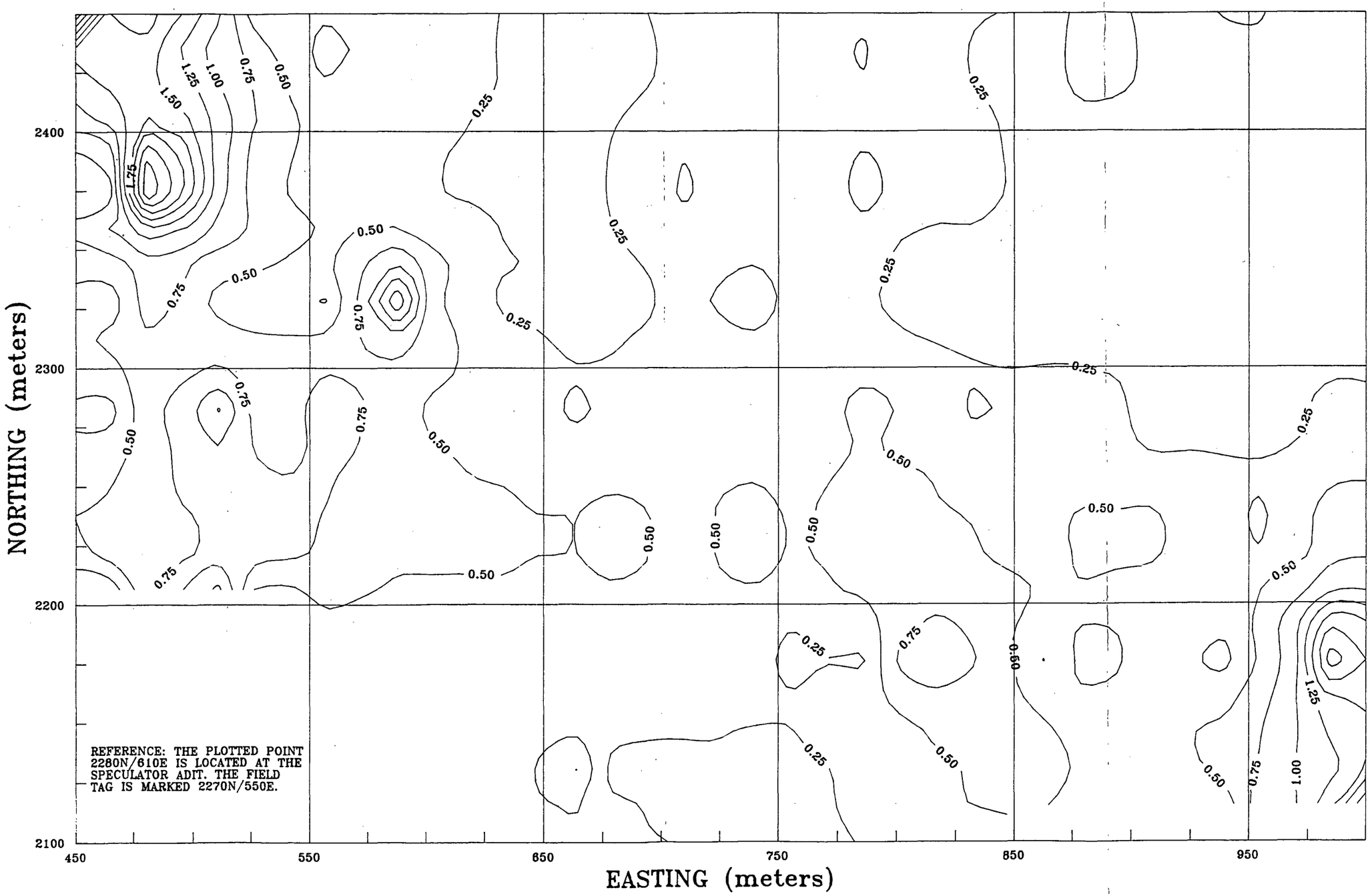
CAZADOR EXPLORATIONS LIMITED



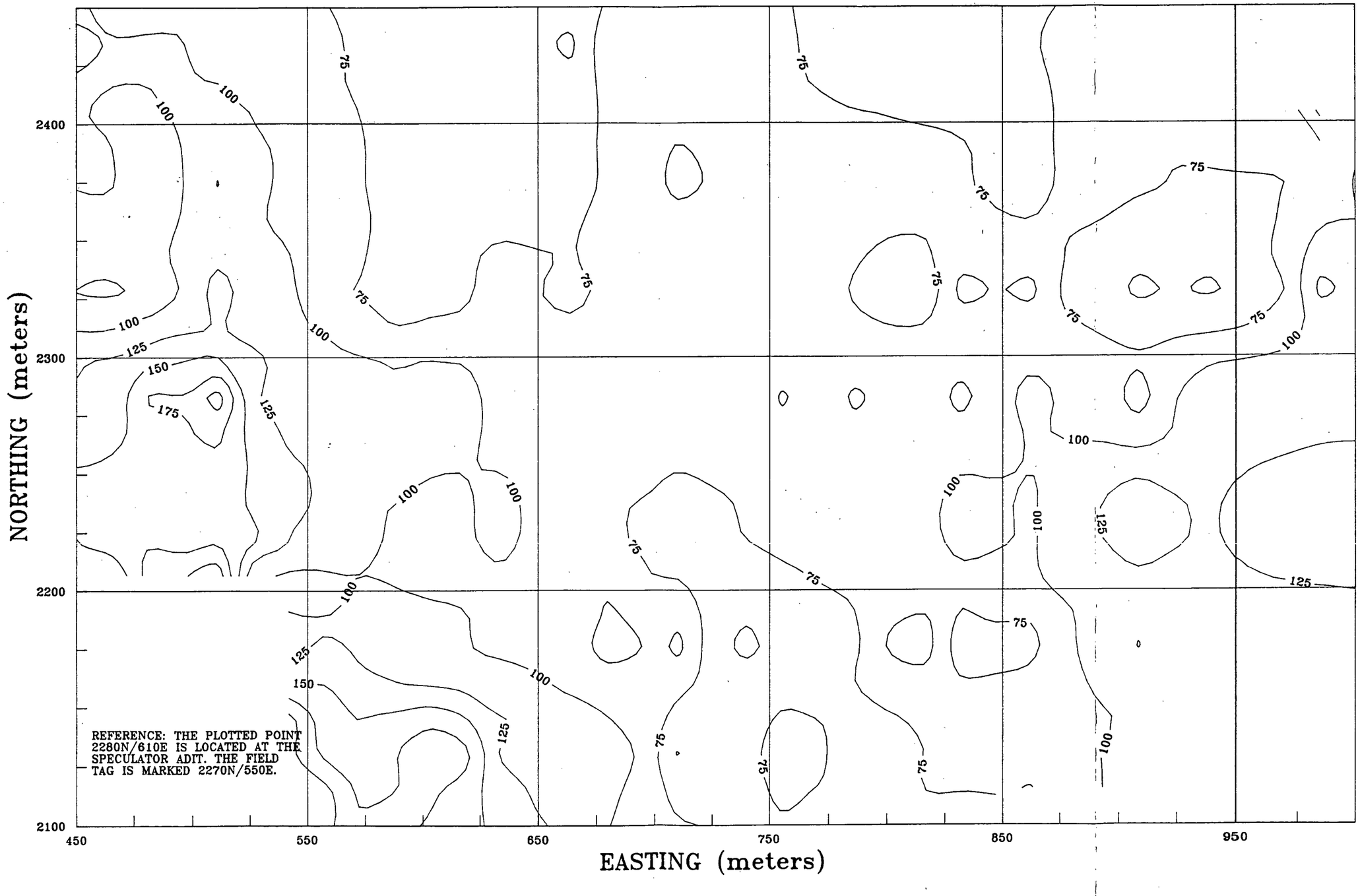
ARLINGTON SILVER PROJECT, MERCURY IN SOILS (ppb), JULY 1990
CAZADOR EXPLORATIONS LIMITED



ARLINGTON SILVER PROJECT, SILVER IN SOILS (ppm), JULY 1990
CAZADOR EXPLORATIONS LIMITED

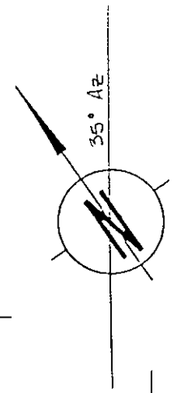


ARLINGTON SILVER PROJECT, ZINC IN SOILS (ppm), JULY 1990
CAZADOR EXPLORATIONS LIMITED



APPENDIX E

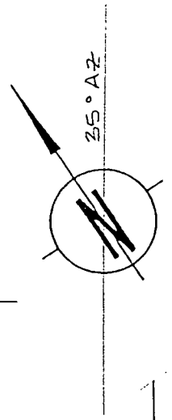
CAZADOR EXPLORATIONS LIMITED
ARLINGTON SILVER PROJECT, SILVER IN SOILS (ppm), JULY 1990



NORTHING (meters)	450	550	650	750	850	950
2400	0.30 3.30 1.10 0.40	0.40 0.30 0.20 0.10	0.10 0.30 0.60 0.30	0.30 0.20 0.30 0.40	0.10 0.10 0.10	
	0.30 0.90 0.40 0.20	0.20 1.80 0.40 0.20	0.10 0.10 0.40 0.70	0.40 0.30 0.10 0.10	0.20 0.10 0.10 0.10	0.10 0.10
2300	0.10 0.70 1.30 0.50	1.00 0.60 0.40 0.40	0.20 0.30 0.30 0.40	0.30 0.60 0.50 0.20	0.30 0.40 0.10 0.20	0.20 0.30
		0.80 0.60	0.50 0.70 0.20 0.80	0.40 0.80 0.50 0.50	0.40 0.60 0.60 0.30	0.10 0.70
2200		0.30 0.30	0.30 0.40 0.50 0.40	0.10 0.20 1.10 0.80	0.20 0.60 0.40 0.10	0.50 2.20
	REFERENCE: THE PLOTTED POINT 2280N/610E IS LOCATED AT THE SPECULATOR ADIT. THE FIELD TAG IS MARKED 2270N/550E.	0.40 0.30	0.80 0.10 0.20 0.20	0.20 0.30		
2100						

EASTING (meters)

CAZADOR EXPLORATIONS LIMITED
ARLINGTON SILVER PROJECT, LEAD IN SOILS (ppm), JULY 1990



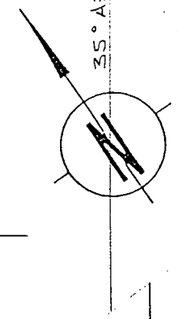
	450	550	650	750	850	950
2400		22 24 20 22	25 35 23 28	26 13 22 15	20 14 17	
	17 24 28 36	29 20 25 17	16 33 28 9	28 23 24 18	19 23 23	
	24 18 22 23	24 19 25 29	23 16 41 23	18 18 16 32	22 21 14 13	10 38
2300	31 115 108 33	39 22 32 29	45 17 19 26	15 17 17 12	21 28 18 20	19 29
		28 32	21 25 18 33	19 21 25 31	43 25 32 29	27 28
2200		35 34	25 21 45 17	18 24 28 30	20 28 15 16	24 46
		35 33	29 47 36 27	20 29		
2100						

REFERENCE: THE PLOTTED POINT 2280N/610E IS LOCATED AT THE SPECULATOR ADIT. THE FIELD TAG IS MARKED 2270N/550E.

NORTHING (meters)

EASTING (meters)

CAZADOR EXPLORATIONS LIMITED
ARLINGTON SILVER PROJECT, ZINC IN SOILS (ppm), JULY 1990



2400					85	51	54	77	37	99	80	87	79	48	68	48	75	77	98
	105	78	133	98	98	58	64	68	57	81	111	99	85	96	86	79	47	98	79
	66	77	136	107	82	48	63	90	66	81	95	80	102	72	43	109	107	61	44	44	52	131
2300	125	182	214	106	114	107	138	78	94	92	77	88	71	105	91	66	111	94	82	122	117	117
					85	121	69	76	61	76	82	77	79	126	90	129	153	118	136	154
2200					100	95	86	60	112	33	82	68	127	56	84	102	128	97	114	114
					208	124	120	116	49	61	95	80								
2100	450		550		650		750		850		950									

REFERENCE: THE PLOTTED POINT 2280N/610E IS LOCATED AT THE SPECULATOR ADIT. THE FIELD TAG IS MARKED 2270N/550E.

NORTHING (meters)

EASTING (meters)