

GEOLOGICAL, GEOCHEMICAL, GEOPHYSICAL
AND DIAMOND DRILLING REPORT

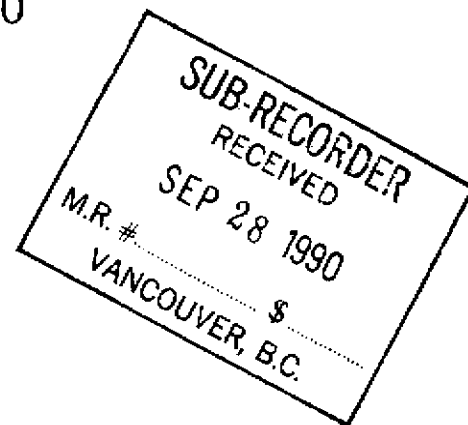
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on the

UNUK "C" CLAIM GROUP

UNUK RIVER AREA

SKEENA MINING DIVISION
NTS 104 B/9 AND 104 B/10



Held under option by:

GRANGES INC.
2300 - 885 WEST GEORGIA STREET
VANCOUVER, B.C.
V6C 3E8

GEOLOGICAL BRANCH
ASSESSMENT REPORT
SEPTEMBER 20, 1990

B.E. GABOURY
(E.J. Seagel)

20,390

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FIGURES

Figure 1. Location of Unuk Option Property

ENCLOSURES

Drill logs for diamond drill holes AP-6 to AP-12, inclusive

Figure 2. Claim Location Map

Figure 3. Geology and Sample Locations, Zone 1 Grid
(east half), Scale 1:2000

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(west half), Scale 1:2000, showing location of
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1 Grid, Scale 1:2000

INTRODUCTION

The area encompassed by this report entails a portion of the Unuk Claim Group "C" which includes Unuk 26 (6397), Unuk 14 (5242), and Unuk 15 (5243). Ashworth Explorations Ltd. and Malcolm Bell are the recorded owners of the claims. The claims are held by Granges Inc. of Vancouver, B.C. under option from Cove Resources Corporation and Springer Resources Ltd. The exploration program was completed under the supervision of B.E. Gaboury, geologist for Granges Inc.

LOCATION AND ACCESS

The claims are all located in the Skeena Mining Division, approximately 1000 km north of the city of Vancouver and 65 km north of Stewart, B.C. on NTS map sheets 104 B/9 and 104 B/10 (Figures 1 and 2).

Access to the area is gained by helicopter from Bell 2 on the Stewart-Cassiar highway approximately 50 km to the east.

The property is characterized by steep vegetation-covered slopes up to 1220 m (4000 ft) elevation and alpine conditions with ice fields and glaciers at higher elevations. Elevations on the property, vary from approximately 1069 m (3500 ft) to 1890 m (6200 ft).

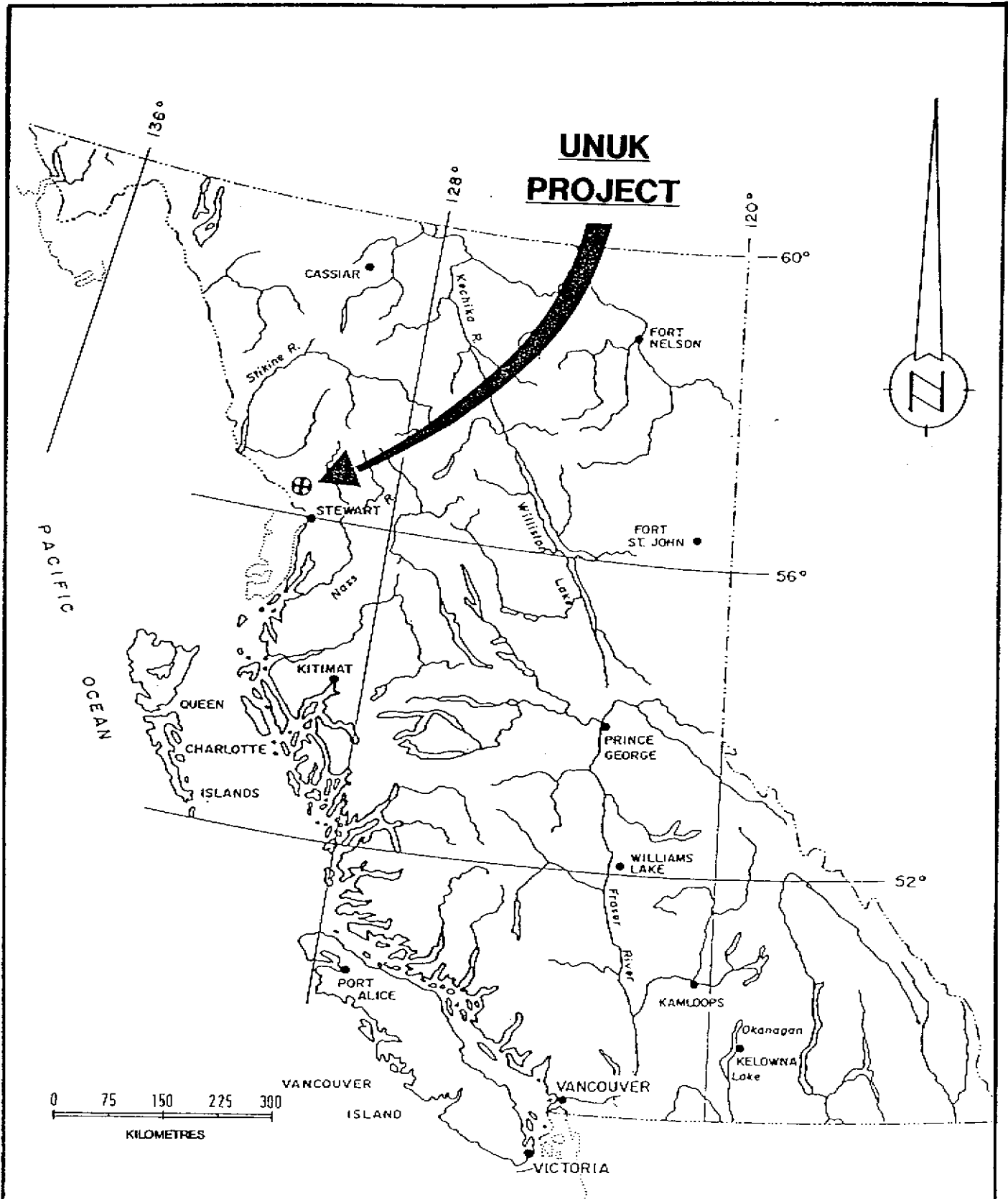
PREVIOUS WORK

The claims discussed in this report were staked in 1986 and 1987 on behalf of Malcolm Bell and Ashworth Explorations Ltd.

Initial work in 1986 involved an airborne VLF-Mag survey commissioned by Hi-Tec Resource Management Ltd., followed by a four day follow-up examination of the property geology by J.P. Sorbara and Associates. In September and October of 1987 Hi-Tec Resource Management Ltd. conducted a two-phase reconnaissance type exploration program (totalling 28 days) to find precious metal mineralization similar to that found in the Brucejack Lake area. Hi-Tec carried out a similar program in 1988 (28 days) to follow up the results of the previous year and to outline other areas of interest on which to focus future exploration efforts.

The net result of these preliminary reconnaissance-style investigations was the definition of six areas of interest. The area known as Zone 1/A.P. Zone is one area thus defined.

In June of 1989 Granges Inc. initiated its exploration program to examine further the six areas of interest outlined by the previous workers and to develop other new areas of interest.



**UNUK
PROJECT**

PROPERTY LOCATION MAP

UNUK OPTION
SKEENA MINING DIVISION, B. C.



FIGURE: 1

January and February 1989, followed by a ground exploration program. The summer ground-based exploration program involved establishing a surveyed control grid with 100 m line spacings, detailed (1:1000 scale) mapping, prospecting and collection of soil samples at 50 m intervals. The later discovery of a cross-cutting base metal-bearing, auriferous structure now known as the A.P. Structure led to the establishment of the A.P. grid located to the immediate south, and overlapping with the Zone 1 grid. The two grids were subjected to a ground-based VLF-Mag survey utilizing an EDA Instruments Inc. Omni-Plus VLF/Magnetometer carried out by SJ Geophysics of Delta, B.C. The result of the geological, geochemical and geophysical investigations was the discovery of gold mineralization associated with what appeared to be a zone of brecciation, hydrothermal alteration and sulfide mineralization known as the Zone 1 Trench Area; the delineation of the auriferous A.P. Structure; and the delineation and surface sampling of the Cliff Structure to the north along strike of the A.P. Structure. In addition, several other soil and rock geochemical anomalies were outlined in the 1989 field program. In the latter part of the field season the A.P. Structure was drill-tested with five holes. Although significant alteration and sulfide mineralization was encountered, assay results were discouraging. Gold values encountered in surface trenching (1989 field program) could not be repeated in drill core.

1990 FIELD SEASON PROGRAM

Surface geological work completed up to August 15, 1990 on the Zone 1/A.P. Zone included:

1. The re-establishment of pre-existing Zone 1 and A.P. Zone grids, location of anomalous soil sample sites from 1989 field program, and fill-in soil sampling where warranted.
2. The re-mapping of the Zone 1 grid plus more detailed prospecting and rock sampling in areas of interest outlined in 1989.
3. An IP survey over areas of interest (from 1989 field season).
4. Six diamond drill holes, AP-6 to AP-12 inclusive.

The camp utilized in 1989 was re-activated June 22, 1990 and work commenced in the Zone 1/A.P. Zone area two days later with field orientation and reconnaissance.

Re-establishment of the Zone 1 grid was accomplished primarily by Granges Inc. personnel, with some minor line-

cutting by Gordon Clark and Associates in preparation for IP survey. In conjunction with the Zone 1/A.P. Zone re-mapping program from June 24 to August 19, 1990, 139 rock samples were collected and submitted for analysis (Figures 3 and 4). In addition, 31 rock samples were collected and submitted for whole rock geochemical analysis.

Soil and rock samples collected were submitted to Acme Analytical Laboratories of Vancouver for 30-element ICP analysis, geochemical fire assay for gold and flameless atomic absorption for mercury. The rock samples collected for whole rock analysis were submitted to Chemex Laboratories of North Vancouver. Appendix A lists the rock samples (with descriptions) collected in conjunction with the mapping and prospecting activities, and includes certificates of analyses. Appendix B lists rocks collected for whole rock analysis plus descriptions and analyses.

IP surveying over areas of interest outlined in the 1989 field program was carried out by Peter Walcott and Associates utilizing a Hunttec 7.5 kw transmitter-generator and a BRGM Elrec 6 receiver in a pole-dipole array (Figure 5). A total of 8.69 km of IP pseudosections over the A.P. Zone and Zone 1 areas were completed.

Six diamond drill holes were completed by J.T. Thomas Diamond Drilling Limited of Smithers, B.C., during the period of August 15th to September 9, 1990. Assaying was performed by Acme Analytical Laboratories of Vancouver, B.C.

RESULTS OF 1990 MAPPING, PROSPECTING AND GEOPHYSICS

Remapping of the Zone 1 grid has produced a great deal of insight into the nature of the AP Structure and its relationship with other major regional structural features. The Zone 1 area is characterized by a series of rhyolitic to dacitic flowrocks and associated coarse fragmental volcanic rocks; variably welded dacitic ash flow tuffs; and a thick overlying crudely to nonbedded heterolithic pyroclastic breccia with occasional intercalations of fine-bedded tuff or debris flow (blackish argillaceous matrix as opposed to the more sericitic tuffaceous matrix of the pyroclastic breccia). The nature of these rocks suggest near-vent facies volcanism and this is further supported by "epithermal" geochemical signatures reported in numerous rock assays returned to date. The volcanic sequence is cross-cut by numerous "felsic" to andesitic dikes which are commonly vesicular and produce peripheral brecciation, hydrothermal alteration and sulfide mineralization (pyrite +/- sphalerite, +/- galena, +/- arsenopyrite) of the host rock. Larger diabase bodies are located in the northwest corner and the north central portion of the Zone 1 grid and in the AP Zone area itself (the AP Zone is noted for its

multitude of cross-cutting, anastomosing diabase dikes comprising 10-15% of the northwest area. The large diabase body in the Zone 1 area is characteristically black, aphanitic, and magnetic but occasionally contains brecciated, pyritic, greenish altered sections usually at the edges of the intrusive or along fractures. The altered sections have been found, through thin section analysis, to be a silicified, chloritized and carbonatized mafic rock. Similar alteration is observed in the AP diabase as well as the smaller sill-like diabase unit which occurs in the north central portion of the Zone 1 grid. An extreme case of this type of alteration is observed in the "felsic" dike swarm in the Zone 1 trench area. These dikes, as well as undergoing alteration themselves, have brecciated, silicified and introduced sulfide mineralization in the host pyroclastic breccias. Two north-south tie lines were IP surveyed (lines 800 W and 600 W) and although the sulfide mineralization is detected on 800 W as a moderately strong chargeability high it cannot be traced through to tie line 600 W. A soil anomaly of up to 145 ppb Au occurs on a west-facing slope above the Zone 1 trenches (which tested sulfide mineralization related to a swarm of east-west trending "felsic" dikes). The anomaly is located downslope to the west of the southeast contact of the large diabase body with the coarse pyroclastic breccia. IP over this area indicates several anomalous areas of high chargeability. One which occurs to the east of the previously-mentioned soil anomaly is visible as a strongly gossanous pyritic contact zone at least 5-10 m thick. A diamond drill hole is planned to test this contact and assays are currently pending for surface sampling carried out in this zone earlier.

Soil anomalies in the Zone 1 area are recognized as being spatially related to the sheared contact of the felsic volcanic sequence to the west (recognized as very likely being the Mt. Dilworth Formation) and a dominantly sedimentary sequence fitting the Department of Mine's description of portions of the Betty Creek Formation. Shearing at the felsic volcanic-sedimentary contact appears to be at very shallow angles (possibly a sheared bedding plane contact) and in many places a dominantly dip slip motion is indicated. The AP structure has been traced with IP from a Z-type flexure around 1350 N on the AP grid to the Cliff Zone at 700 N/275 W on the Zone 1 grid, a distance of approximately 500 m. The AP diabase (as traced by 1989 ground magnetic survey) appears to have deformed the AP structure (folded to the east as is indicated by IP data) and was likely instrumental in producing the gold-poor ankerite-galena-sphalerite veins such as "Don's Vein" in addition to the abundant near flat-lying tensional quartz veinlets which occur in trenches 1 and 10 on the AP Zone. The only apparent difference between the Cliff Zone and the AP Zone is that the AP Zone is observed to cross-cut stratigraphy while the Cliff Zone appears to follow a

lithologic contact. It is possible that the Cliff Zone is the major structure and that the AP Zone is a splay structure. Another such splay structure appears to originate from the main structure at 1200 N/250 W and extends southwestward at azimuth 225 towards "Red Knob", where gold levels in soil reach 420 ppb. It manifests itself only as a weak chargeability high and a minor inflection in the resistivity on the IP pseudosection for line 900 N.

Due to overburden cover below the cliffs of felsic volcanics a sporadic gold geochemical anomaly is detected in the soils there and sheared tuffs at 1225 N/170 W (near the felsic volcanic-sedimentary contact) were found to carry 15,381 ppb gold across a 1.5 m chip sample. The IP survey over the felsic volcanic-sedimentary contact has produced a continuously traceable zone of broad subtle chargeability highs which may have coincident resistivity lows or flanking resistivity highs.

Where exposed, the Cliff Zone (at the base of the cliffs between lines 700 N and 1100 N) has been found to carry consistently elevated gold values of up to 1400 ppb. Between lines 100 N and 1300 N the zone appears to be sinistrally drag-folded so as to produce an apparent displacement of about 200 m to the west. This appears to be supported by IP data. Smaller scale sinistral drag folds with steep northwesterly plunges are observed in ash flow tuffs around 1100 N/250 W. This sinistral drag-folding is also observed to overprint diabase dikes in this area. Slickenside evidence, as well as plunges of small-scale drag folds in this area, indicate an almost horizontal stress field. The sequence of structural events leading to what is today observed would then be as follows:

1. Development of a shear structure with dominantly dip-slip displacement (Cliff Zone = sheared felsic volcanic - sedimentary contact) + splay structures (AP structure and "Red Knob" structure).
2. Emplacement of diabase dikes and larger diabase intrusive bodies with resultant deformation of pre-existing AP Zone and development of ankeritic veins (eg. Don's Vein).
3. Re-activation of shear zones by a horizontal dextral stress field producing sinistral drag folding and northwestwardly trending siliceous auriferous veins such as those observed in the cliff between lines 1100 N and 1200 N.

Judging by the higher gold values observed in the northwest trending siliceous veins, it would appear that the later reactivation of the shear zone plays an important role in

the concentration of gold within the tensional regime created within the sinistrally drag-folded portions of the structures.

To date only approximately 300 m of strike length, of a total of 2000 m, has been drill-tested along the AP-Cliff Zone Structure. The area which has been drill-tested is one which is structurally complex with abundant cross-shears and cross-cutting diabase dikes. Better continuity is expected within the structure away from this area. These expectations are supported by the visual and geochemical evidence from the Cliff Zone between 700 N and 100 N and by IP data between 1200 N and 1600 N.

DIAMOND DRILLING

Drilling of the Zone 1 structure was undertaken to examine further the correlation of IP, geochemical and geological evidence. Six diamond drill holes, AP-6 to AP-12 were completed for a depth of 1,520.93 metres (Figure 4).

The following is a summary of results. For more information see appended drill logs and record sheets or contact Granges to view core.

Hole AP-6 1350 N 88.5 W -45° Az 302° Depth 300.84 m

Hole AP-6 encountered a series of greywackes, tuffaceous mudstones, argillites and minor dacitic tuffs. The target was an IP anomaly. Semi-massive pyrite and up to 15% disseminated pyrite were encountered in a siliceous tuff from 62.5 to 70.40 m downhole. No significant gold mineralization, however, was encountered. Similarly, an argillaceous tuff from 73.76 to 85.65 was found to carry up to 25% pyrite in short intervals (generally \leq 35 cm) but again these sections carried no significant gold mineralization.

Hole AP-7 738 N 195 W -45° Az 314° Depth 197.21 m

The target was a shear zone in tuffaceous mudstone, exposed in the "Cliff Zone". Sampling on surface in 1989 returned values of up to 1400 ppb gold. The drill hole was collared in a series of andesitic tuffs and tuffaceous wackes. These then grade into more tuffaceous argillites with dacitic lappilli-ash tuffs. Silicification, strong carbonate alteration and quartz-pyrite veining was encountered from 85.80 - 96.50 m downhole. No significant mineralization was encountered.

Hole AP-8 1175 N 321 W -55° Az 080° Depth 306.91 m

The target of this hole was an IP/geochemical anomaly and a test of continuity of high grade veins in a sinistrally drag-folded portion of a structural break between a thick felsic volcanic sequence to the west and a dominantly sedimentary sequence to the east. The drill hole encountered a coarse pyroclastic breccia, welded dacite tuff, flowbanded rhyolite and several fine-grained often pyritic "andesitic" dikes, plus black argillite and fossiliferous greywacke. The most significant sulfide mineralization was encountered within or peripheral to the "andesitic" dikes, but assaying returned negative results.

Hole AP-9 1117 N 258 W -55° Az 080° Depth 238.05 m

The target was an IP/geochemical anomaly and a test of the "high grade" cross-cutting veins which occur in the area of sinistral drag folding. The hole encountered a thick sequence of variably welded dacite tuff which grades downhole into tuffaceous mudstones and argillites. A silicified pyritic, sphalerite and arsenopyrite-bearing shear zone was encountered from 16.90 - 20.00 metres. Although it carried no significant gold, values were anomalous. Arsenopyrite and pyrite mineralization associated with brecciation, silicification and carbonate alteration in the argillites and siltstones was encountered from 219.05 - 220.05 metres. However, assaying returned negative results and, due to drilling difficulties, the hole was abandoned.

Hole AP-10 1600 N 075 W -45° Az 282° Depth 198.12 m

Target was an IP/geochemical anomaly. The hole intersected a series of tuffaceous mudstones and altered welded dacite tuff. Up to 7% pyrite was encountered in a brecciated and sheared interval of dacitic pyroclastic breccia from 95.84 - 102.41 m downhole. A wide zone of shearing in the graphitic black argillites was encountered near the bottom of the hole. No significant mineralization was encountered.

Hole AP-11 1600 N 003 W -45° Az 282° Depth 141.12 m

Target was an IP/geochemical anomaly. The hole encountered diabase with hydrothermal alteration, veining and pyrite-sphalerite-galena mineralization, at its contact with tuffaceous mudstones. The remainder of the hole encountered a series of tuffaceous mudstones, argillite and welded dacite tuff with no significant sulfide mineralization.

Hole AP-12 1240 N 094 W -45° Az 210° Depth 138.68 m

Purpose of the hole was to complete the drilling of the targets proposed for hole AP-9. The hole encountered a series of fossiliferous greywacke and argillite which grades into tuffaceous mudstone followed by welded dacite tuff. Brecciated carbonate veining, up to 5% pyrite and traces of brown resinous sphalerite was encountered in tuffaceous mudstone from 56.60 - 59.10 m downhole. This includes a 40 cm vein with 7-10% pyrite, trace chalcopyrite and tetrahedrite. Sheared tuffaceous mudstone near the welded tuff contact from 111.15 - 116.95 m is sericitized and carries up to 10% pyritic plus grey carbonate-pyrite veins. Assays yielded negative results.

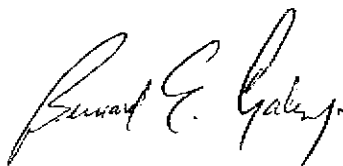
CORE STORED IN EXPLORATION CAMP ON THE COUL Z. CLAIM.

CERTIFICATE OF QUALIFICATIONS

I Bernard E. Gaboury of Nanaimo, British Columbia do hereby certify that;

- (1) I am a project geologist for Granges Inc. with office at 2300-885 West Georgia Street, Vancouver, B.C., V6C 3E8.
- (2) I am a graduate of University of Manitoba, Winnipeg, Manitoba with a BSc(Hons) degree in Physical Chemistry and an MSc degree in Geology.
- (3) That I have practised geology for twelve years.
- (4) I have been a member in good standing of the Association of Professional Engineers Province of Manitoba since 1983.

Dated at Vancouver, B.C. this 4th date of January 1990.



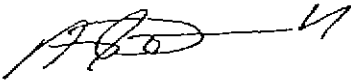
Bernard E. Gaboury, BSc Hons, MSc, P.Eng.

CERTIFICATE OF QUALIFICATIONS

I Arthur John O'Donnell, of Delta, British Columbia do hereby certify that:

- 1) I am Exploration Manager for Granges Inc. with office at 2300-885 West Georgia Street, Vancouver, B.C., V6C 3E8.
- 2) I am a graduate of Saint Francis Xavier University, Antigonish, N.S. with a BSc degree in geology. I also took an extra year of geology at Dalhousie University, Halifax, N.S.
- 3) That I have practised my profession for thirty years.
- 4) I have been a member in good standing of the Association of Professional Engineers of the Province of Ontario since 1970 and the Association of Professional Engineers Province of Manitoba since 1980.

Dated at Vancouver, B.C. this 24th day of May 1989.



A. J. O'Donnell, P.Eng.

STATEMENT OF EXPENDITURES

Claim 5242, Unuk 14

Geologists Wages:

| | |
|---|-----------|
| Prospecting and Mapping - 1.5 man days at \$235 | \$ 352.50 |
| 8 man days at \$200 | 1,600.00 |
| 7 man days at \$145 | 1,015.00 |
| 2 man days at \$130 | 260.00 |

Geochemical Survey Assays:

| | |
|-----------------------------------|------|
| 1 rock sample at \$6.25 | 6.25 |
|-----------------------------------|------|

Geophysical Survey:

| | |
|-----------------------------|----------|
| 1.17 km IP survey | 2,793.03 |
|-----------------------------|----------|

| | |
|---|--------|
| Report Preparation and Drafting | 100.00 |
|---|--------|

| | |
|---------------------------|---------------|
| Office Overhead | <u>612.68</u> |
|---------------------------|---------------|

| | |
|-------|------------|
| TOTAL | \$6,739.46 |
|-------|------------|

Claim 5243, Unuk 15

Geologists Wages:

| | |
|---|-----------|
| Prospecting and Mapping - 3 man days at \$235 | \$ 705.00 |
| 15 man days at \$200 | 3,000.00 |
| 5 man days at \$145 | 725.00 |

Geochemical Survey Assays:

| | |
|--|--------|
| 23 rock samples at \$6.25 | 143.75 |
| 6 whole rock samples at \$24 | 144.00 |

| | |
|---|--------|
| Report Preparation and Drafting | 100.00 |
|---|--------|

| | |
|---------------------------|---------------|
| Office Overhead | <u>481.77</u> |
|---------------------------|---------------|

| | |
|-------|------------|
| TOTAL | \$5,299.52 |
|-------|------------|

Claim 6397, Unuk 26

Geologists Wages:

| | |
|---|------------|
| Prospecting and Mapping - 9.5 man days at \$235 | \$2,232.50 |
| 25 man days at \$200 | 5,000.00 |
| 1 man day at \$130 | 130.00 |

| | |
|--|----------|
| Diamond Drilling - 7 days at \$200 | 1,400.00 |
| 12 days at \$175 | 2,100.00 |
| 5 days at \$145 | 725.00 |

Geochemical Survey Assays:

| | |
|---|--------|
| 115 rock samples at \$6.25 | 718.75 |
| 25 whole rock samples at \$24 | 600.00 |

Geophysical Survey:

| | |
|------------------------------|-----------|
| 6.898 km IP survey | 16,466.97 |
|------------------------------|-----------|

Diamond Drilling:

| | |
|----------------------|------------|
| 1,520.93 m | 112,467.09 |
|----------------------|------------|

Core Assaying:

| | |
|--|----------|
| 1,123 30-element ICP at \$6.25 | 7,018.75 |
|--|----------|

| | |
|---|----------|
| Report Preparation and Drafting | 2,000.00 |
|---|----------|

| | |
|---------------------------|------------------|
| Office Overhead | <u>15,085.90</u> |
|---------------------------|------------------|

| | |
|-------|--------------|
| TOTAL | \$165,944.96 |
|-------|--------------|

| | |
|-------------|--------------|
| GRAND TOTAL | \$177,983.94 |
|-------------|--------------|

APPENDIX A

Rock Samples Submitted for 30-Element ICP Analysis
Descriptions and Certificates of Analysis

Rock Sample Record Sheet

| Sample No. | Location | | Description | Geochem. | | | | | | | |
|------------|----------|-------|---|----------|-----|-----|-------|------|-------|------|--|
| | (ZONE 7) | | | Au | Ag | Cu | Zn | Pb | As | g/t | |
| 1 | 11+05N | 1+12W | 24cm wide ^{intensely sheared} vein ^{rich in sulf} - 15-25% diss. pyr, 10-35% sphal. | 2841 | 310 | 434 | 28811 | 2442 | 12257 | 1400 | |
| 2 | 11+45W | 1+45W | grab within sheared ^{intensely sheared} vein - 5-10% diss. pyr | 861 | 25 | 5 | 14 | 19 | 221 | 20 | |
| 3 | 11+70N | 1+45W | grab in int. sil fract. along shear zone 1-3% diss. pyr. | 2273 | 273 | 16 | 731 | 60 | 2851 | 27 | |
| 4 | 11+70N | 1+55W | grab in rusty weather, fract. along w 1-3% diss. pyr. | 1125 | 302 | 413 | 2227 | 785 | 2514 | 202 | |
| 5 | 11+00N | 0+75W | | 77 | 103 | 14 | 218 | 81 | 103 | 762 | |
| 6 Rock | 18+50N | 0+40E | SHEARED FLOW BAND RHYOLITE 5% - 10% DISSEM. Py | 211 | 11 | 14 | 128 | 14 | | | |
| 7 | 18+00N | 0+40E | " " " " " " " " | 15 | 1 | 4 | 25 | 16 | 28 | | |
| 8 | 8+90N | 3+30W | SHEARED RHYOLITE (Flow Band?) IN FAULT SHEAR 5% DISSEM. Py | 8 | 14 | 6 | 55 | 4 | 29 | | |
| 9 | 9+50N | 2+77W | ANDESITIC? DYKE 5% - 15% DISSEM. Py IN FAULT SHEAR | 13 | 5.3 | 11 | 512 | 41 | 123 | | |
| 10 | 9+60N | 2+75W | SHEARED RHYOLITE 3% - 5% Py IN SHEAR/FAULT, MINOR CHALCOPITE | 8 | 5.2 | 25 | 547 | 33 | 31 | | |
| 11 | 11+98N | 1+46E | GRAB FROM DYKE (ANDESITIC?) 10% - 15%+ DISSEM. Py | 11 | 1.5 | 16 | 370 | 105 | 19 | | |
| 12 | 13+00N | 0+10W | RHYO DYKE? w MINOR Py 1% - 2% | 3 | .1 | 9 | 24 | 3 | 17 | | |
| 13 | 16+50N | 0+40W | FLOW Banded RHYOLITE 2% - 4% DISSEM. Py | 4 | .1 | 5 | 31 | 2 | 5 | | |
| 14 | 16+85N | 0+30W | " " " 2% - 5% " " | 3 | .1 | 5 | 59 | 14 | 21 | | |
| 15 | 17+75N | 0+40E | " " " FRACTURED | 9 | .1 | 5 | 34 | 19 | 47 | | |
| 16 | 17+50N | 0+25E | FLOW Banded RHYOLITE? 3% - 5% DISSEM. Py | 3 | .1 | 4 | 21 | 2 | 2 | | |
| 17 | 15+75N | 2+50W | " " " ? - 2% DISSEM. Py | 6 | .4 | 6 | 116 | 10 | 12 | | |
| 18 | 14+00N | 5+25W | DYKE (? TYPE? OF DYKE) x-cutting PYROS. 5% - 8% DISSEM. Py | | | | | | | | |

Rock Sample Record Sheet

| Sample No. | Location | | Description | Geochem. | | | | | | |
|------------|----------|------------------|---|------------|-----|-----|-----|-----|-----|------|
| | (ZONE I) | | | Au | Ag | Cu | Zn | Pb | As | Hg |
| | | | | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| 19 | R | 1725N 880W | Heterolithic breccia, dacitic, + argillite | whole rock | | | | | | |
| 20 | R | 1630N 1010W | Qtz-chl-ankerite vein, along fault | 2 | 1.1 | 6 | 38 | 25 | 3 | |
| 21 | R | 1702N 970W | Qtz on, andesite | 8 | .1 | 4 | 69 | 6 | 4 | |
| 22 | R | 590N 560W | carbonate cemented brx, dacitic tuff, 3-5% diss py | 81 | .6 | 16 | 157 | 4 | 59 | 80 |
| 23 | R | 850N 475W | patchy diss. py, in massive rhyolite tuff | 17 | .6 | 8 | 46 | 12 | 30 | 90 |
| 24 | R | 875N 410W | rhyolite tuff, ash tuff, 1-2% diss. py | 11 | .2 | 6 | 106 | 2 | 7 | 80 |
| 25 | R | 910N 400W | sheared dacitic debris flow, 5-10% py blebs | 208 | 1.6 | 12 | 87 | 23 | 57 | 160 |
| 26 | R | 909N 400W | sheared dacitic debris flow, 10-20% py | 160 | .8 | 12 | 98 | 20 | 25 | 110 |
| 27 | R | 925N 370W | flow banded rhyol., Tr py | | | | | | | |
| 28 | R | 820N 385W | dacitic ash flow tuff, 2-3% py in blebs | 71 | .1 | 7 | 13 | 16 | 86 | 80 |
| 29 | R | 690N 335W | sheared ash flow tuff, 1-2% py, minor blebs | 2 | .1 | 13 | 76 | 14 | 8 | 60 |
| 30 | R | 700N 250W | 1-2 m shear zone, Fe-carb. brx, 10-20% py streaks | 370 | 1.8 | 14 | 492 | 124 | 65 | 190 |
| 31 | R | 885N 025E | andesitic, carbonate-alt'd dike rock | 4 | .1 | 12 | 141 | 2 | 14 | 330 |
| 32 | R | 885N 027E | less alt'd, grey-brown weathering andesitic dike | 1 | .1 | 13 | 14 | 2 | 17 | 50 |
| 33 | R | 815N 040E | fault zone, brx + carb. infilling, py blebs + veins | 31 | .2 | 15 | 30 | 2 | 69 | 2400 |
| 34 | R | 845N 050E | carb. (ankerite) brx vein, Tr-1% py, minor stain py | 3 | .1 | 8 | 149 | 2 | 2 | 100 |
| 35 | R | 620N 960E | basaltic andesite, bomb tuff, hbl-feld. porph. | whole rock | | | | | | |
| 36 L.S. | R | 9+30N 7+75W | RHYOLITE? to tr. Py | | | | | | | |
| 37 | R | 13+00N 7+00W | RHYOLITE Brx? 10% - 15% Py | 8 | .1 | 6 | 109 | 11 | 20 | 1500 |
| 38 | ✓R | 15+00N 8+50W | RHYOLITE? 2% Py | 4 | .2 | 5 | 191 | 5 | 2 | 180 |
| 39 | ✓R | 13+70N 7+00W | RHYOLITE 5% - 8% Dissem. Py | 7 | .1 | 6 | 200 | 2 | 5 | 620 |
| 40 | R | 13+80N 6+30W | RHYOLITE 10% Py MINOR CRYSTALLINE ALTERATION | 6 | .2 | 9 | 107 | 12 | 8 | 730 |
| 41 | ✓R | 15+90N 5+35W (B) | DIABASE? Rhy? | 21 | .1 | 6 | 126 | 2 | 2 | 30 |
| 42 | ✓R | 15+90N 5+35W (A) | RHYOLITE 2% - 3% Py | 7 | .1 | 6 | 164 | 2 | 3 | 180 |

Rock Sample Record Sheet

| Sample No. | Location | | Description | Geochem. | | | | | | |
|-------------------|----------|-------|---|----------|----|----|-----|----|-----|------|
| | | | | Au | Ag | Cu | Zn | Pb | As | Hg |
| 43 ✓ R | 15+85N | 4+15W | 3% disseminated to Pb shaly CHLORITIC Rhyolite | 2 | .1 | 6 | 133 | 3 | 5 | 330 |
| 44 R | 14+25N | 6+50W | Rhy. Bx. 1% - 3% Py. | 4 | .1 | 4 | 100 | 2 | 7 | 200 |
| 45 R | 15+30N | 5+50W | Rhy. 1% - 5% Py tr. Pb | 3 | .1 | 12 | 139 | 7 | 2 | 620 |
| 46 ✓ R | 15+00N | 6+00W | Rhy. 1% - 3% Py | 3 | .1 | 6 | 139 | 2 | 2 | 220 |
| 47 ✓ R | 16+70N | 4+20W | Rhyolite dyke? 3% Py | 4 | .1 | 9 | 147 | 11 | 2 | 330 |
| 48 ✓ R | 17+00N | 4+20W | Rhyolite dyke? to Pb - 3% Py in fractures | 6 | .1 | 11 | 140 | 2 | 7 | 180 |
| 49 R | 14+85N | 2+00W | TUFFS? Rhyolite w 3% disseminated Py | 4 | .2 | 6 | 83 | 6 | 4 | 130 |
| 50 R | 14+75N | 2+30W | Rhyolite tuff? to 5% Py | 1 | .4 | 10 | 96 | 20 | 5 | 270 |
| 51 R | 13+80N | 2+80W | Felsic dyke (Rhyolite) 1% - 5% Py | 8 | .1 | 9 | 176 | 11 | 8 | 780 |
| 52 R | 13+90N | 2+75W | Rhyolite 3% Py | 1 | .1 | 9 | 144 | 13 | 4 | 540 |
| 53 R | 13+60N | 2+35W | Flow Banded Rhyolite? 3% - 5% Py disseminated | 10 | .3 | 9 | 17 | 9 | 20 | 220 |
| 54 R | 13+70N | 2+60W | Rhyolite 3% Py tr. Sph. | 5 | .1 | 5 | 33 | 22 | 4 | 840 |
| 55 R | 11+10N | 8+60E | Dz Vein over 10cm wide sampled | 12 | .1 | 18 | 19 | 4 | 58 | 2000 |
| 56 R | 14+00N | 6+20E | Felsic Dyke w 15% disseminated Py | | | | | | | |
| 57 ✓ R | 14+00N | 6+50W | Rhyolite Bx | | | | | | | |
| 58 ✓ R | 15+30N | 4+75W | Rhyolite w slight chlorite alteration 3% Py | 3 | .1 | 4 | 108 | 2 | 3 | 130 |
| 59 ✓ R | 15+30N | 4+80W | Rhyolite w " " " " " " " " " " " " " " | | | | | | | |
| 60 ✓ R | 17+10N | 6+00W | Rhyolite | 20 | .1 | 6 | 159 | 2 | 4 | 400 |
| 61 ✓ R | 14+00N | 7+00E | Dz Veining w 5% Py (vein 2-7cm wide) | | | | | | | |
| 62 L.S. JULY 14 R | 17+00N | 5+70E | Shear in tuffaceous / and graphitic tuff beds | 15 | .1 | 23 | 41 | 9 | 2 | 50 |
| 63 L.S. R | 15+80N | 6+00E | Py + hydrothermal in shear zone in Dz | 15 | .1 | 35 | 142 | 25 | 85 | 740 |
| 64 L.S. R | 16+10N | 6+25E | Py + " " " " " " " " " " " " | 12 | .2 | 34 | 235 | 34 | 210 | 880 |
| 65 R | 11+90N | 5+80W | Pycroclastic breccia w inter. silicification < 2% diss pyrite | 4 | .3 | 10 | 348 | 9 | 11 | 3500 |
| 66 R | 11+90N | 6+18W | Pycroclastic bx, porv. tal, silic, mx alt. to Fe-oxide | 1 | .1 | 7 | 138 | 5 | 8 | 380 |
| 67 R | 11+60N | 5+50W | " " " " " " " " " " " " | 19 | .1 | 9 | 146 | 7 | 12 | 320 |
| 68 R | 18+00N | 0+30E | Flow banded rhyolite with 15-20% diss pyrite | 24 | .1 | 14 | 289 | 45 | 82 | 800 |

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Rock Sample Record Sheet

| Sample No. | Location | | Description | Geochem. | | | | | | | | |
|------------|----------|------|--|-----------|-----------|-----------|-----------|-----------|-----------|-----------|--|--|
| | | | | Au ppm | Ag ppm | Cu ppm | Zn ppm | Pb ppm | As ppm | Hg ppm | | |
| 69 R | 1226N | 171W | Bernie's fauna section of 12231 (40m) over width of 1 meter high | | | | | | | | | |
| 70 R | 1100N | 110W | 8 cm unal of Sh filled fracture in Assy, by sph. | 202 | 1.5 | 14 | 100 | 37 | 2.0 | 150 | | |
| U.S. 71 R | 1710N | 585W | altered basalt? diabase? w 5% py | 45 | 1.3 | 10 | 100 | 220 | 130 | 35 | | |
| U.S. 72 R | 1420N | 850W | " " " " ? in contact w gran: 5% py | 3 | .1 | 41 | 71 | 14 | 8 | 230 | | |
| 73 R | 1750N | 810W | altered diabase w 2-5% diss py | 1 | .1 | 9 | 84 | 24 | 8 | 220 | | |
| 74 R | 1550N | 220W | contact alt zone in rhy tuff-adj to diabase, 10% py | 1187 | | | | | | | | |
| 75 R | 1680N | 645W | brecciated rhy tuff, mottled diss py | 19 | 64 | 17 | 72 | 224 | 237 | | | |
| 76 R | 1690N | 775W | rhy lapilli tuff, 1-2% diss - blebs py | 2 | .1 | 6 | 228 | 26 | 6 | | | |
| 77 R | 1625N | 780W | fract filling & dispersed py (up to 10%) in felsic tuff | 4 | .1 | 7 | 36 | 12 | 8 | | | |
| 78 R | 1201N | 401W | qtz stringers in clay alt. rhyolite, <1% fine glass/txta | 3 | .1 | 10 | 60 | 16 | 7 | | | |
| 79 R | 1201N | 399W | clay alt rhy, to glass/txta, no qtz stringers | 192 | 202 | 35 | 514 | 547 | 1227 | 1100 | | |
| 80 R | 1801N | 100E | qtz stringers & repl. in f-gr seds, 10-15% fat diss py | 311 | 171 | 35 | 226 | 590 | 139 | 2600 | | |
| 81 R | 1500N | 175W | fract filling, 2% py in flow banded rhyolites | 1825 | | | | | | | | |
| 82 R | 1400N | 215W | grab pyritic/karitized? rhy w 2-4% diss py | 54 | .2 | 4 | 1 | 17 | 144 | | | |
| 83 R | 1390N | 140W | grab rhy w kaolinitization? - sericite-limonite 2-3% py | 15 | 1.0 | 5 | 4 | 13 | 63 | 90 | | |
| 84 R | 1450N | 160W | grab rhy tuff? sheared w 2-3% drusy-cubic py | 8 | .1 | 10 | 31 | 29 | 11 | | | |
| 85 R | 1475N | 020W | grab from gossanous rhy w sericitic/kaol. alt, 5-10% py | 1 | .2 | 7 | 207 | 35 | .2 | | | |
| 86 R | 1425N | 020W | grab from fract. 10m wide, 3-5% diss py | 14 | 1.0 | 6 | 68 | 26 | 3 | | | |
| 87 R | 1450N | 700W | grab select 6cm fracture % py? | 10 | 1.0 | 10 | 15 | 10 | 2 | | | |
| 88 R | 1500N | 650W | grab select across 6cm fract. 2-5% diss py | 2 | .1 | 9 | 59 | 15 | 2 | | | |
| 89 R | 1185N | 073W | grab select (10cm) in 4m fract, <5% to up to 25% diss py | 1 | .1 | 6 | 78 | 8 | 6 | | | |
| 90 R | 1200N | 075W | grab (250cm) in 5m wide shear w bleached gnd to 5% diss py | 41 | 2.1 | 10 | 16 | 20 | 166 | 1300 | | |
| 91 R | 1050N | 105W | grab in red fissil, rusty weath argill. | 4 | .3 | 28 | 31 | 10 | 21 | 70 | | |
| 92 R | 1075N | 115W | shear in lithic rhy andesite - grab over 1m - 5% diss py | 13 | 2.7 | 14 | 84 | 47 | 35 | 180 | | |

Zone 1

Rock Sample Record Sheet

| Sample No. | Location | | Description | Geochem. | | | | | | |
|-----------------------|----------|------------|---|-----------|-----------|-----|-----|-----|------|-------|
| | | | | Au ppb | Ag ppm | Cu | Zn | Pb | As | Hg |
| 93 | R | 1800N 525W | green brecciated diabase w blk mx cont diss py | 2 | .1 | 4 | 145 | 4 | 4 | 200 |
| 94 | | 1220N 264W | 2m chip across alter zone on N edge of green gray dacitic pyroclastic | 50 | 2.4 | 3 | 16 | 16 | 120 | 310 |
| 95 | | 1225N 240W | 1m composite grab from HW contact of 7-10m wide alter zone | 40 | 1.7 | 4 | 58 | 16 | 118 | 330 |
| 96 | | 1320N 507W | composite grab across 3-5m wide zone in Zg; up to 20% py | 4 | .5 | 8 | 140 | 14 | 23 | 2400 |
| 97 | | 1400N 533W | grab sample, bleached Zg w 3-5% py, possible felsic dike | 1 | .1 | 6 | 6 | 9 | 7 | 730 |
| 98 | | 1330N 573W | composite grab across ~3m wide zone in sericit Zg, up to 10% py | 1 | .1 | 4 | 12 | 4 | 6 | 2300 |
| 99 | | 1550N 500W | dacitic breccia in dark green matrix, 5-10% py | 44 | .1 | 8 | 143 | 9 | 9 | 320 |
| 100 | | 1705N 600W | strongly silicified dacite & diabase contact 3-5% py | 5 | .1 | 8 | 30 | 16 | 7 | 560 |
| 101 | | 1520N 810W | ankerite brx vein in diabase 3-5% py | 2 | .3 | 2 | 34 | 7 | 5 | 1800 |
| 102 | | 1420N 852W | strongly silic brx, concentric alteration rims | 6 | .2 | 10 | 78 | 57 | 224 | 1200 |
| 103 | | 1280N 760W | contact zone in diabase, brxd, silic, 10-15% py | 16 | .8 | 145 | 159 | 142 | 36 | 1500 |
| 104 | | 1000N 800W | qtz-carb brx in float, 1-2% py | 1 | .4 | 74 | 86 | 4 | 4 | 60 |
| 105 | | 1735N 750W | alt'd coarse and/dac tuff, near diabase 3-5% py | 1 | .1 | 5 | 40 | 10 | 9 | 620 |
| 106 | | 1150N 130W | py vn in strgly silic dac tuff brx 10-15% py | 138 | 9.4 | 6 | 13 | 178 | 208 | 430 |
| 107 | | 1125N 125W | strgly silic. dac tuff brx, qtz-carb vn, 10-20% py | 1976 | 71.8 | 30 | 325 | 124 | 205 | 760 |
| 108 | | 1550N 220W | chyalite in contact with diabase, 10% py | 1187 | 64.0 | 17 | 72 | 244 | 237 | 4300 |
| 109 | | 1680N 645W | brxd rhyolite tuff, mottled diss. py | 2 | .1 | 6 | 229 | 26 | 6 | 430 |
| 110 | | 1690N 775W | rhyolite tuff, 1-2% py | 4 | .1 | 7 | 36 | 12 | 8 | 700 |
| 111 | | 1625N 780W | fracture filling & diss. py in felsic tuff | 3 | .1 | 10 | 60 | 16 | 7 | 1200 |
| 112 | | 1201N 401W | qtz stringers in alt'd rhyolite, <1% py | 192 | 20.2 | 35 | 514 | 547 | 1227 | 7100 |
| 113 | | 1201W 399W | clay alt'd rhyolite, tr grab, tr tuff | 311 | 171.0 | 35 | 224 | 540 | 139 | 26000 |
| 114 | | 1801W 100W | qtz strgrs, in f. gr. sed, 10-15% py | | | | | | | |
| WEST OF BRUCE GLACIER | | | | | | | | | | |
| 116 | | R-DG-90-1 | strongly silic, seric, blocky tuff, 10-20% py | 7 | .3 | 4 | 7 | 21 | 30 | 920 |
| 117 | | R-KP-90-1 | pyrad. brx w pods py, diss py, tr arsenopy | 10 | .2 | 3 | 2 | 15 | 28 | 1700 |

ZONE 1

Rock Sample Record Sheet

| Sample No. | Location | | Description | Geochem. | | | | | | |
|------------|----------|------|---|----------|------|-----|------|-----|-----|------|
| | N | W | | Au | Ag | Cu | Zn | Pb | As | Hg |
| 118 R | 1210 | 150 | Composite grab across 4 m, ash flow tuff w 5% py (2e) | 64 | 1.0 | 36 | 33 | 11 | 107 | 180 |
| 119 | 1225 | 170 | composite grab across 6.5 m, andes ash tuff, sericitized, 10% py, tr sp | 1538 | 22.3 | 321 | 1706 | 238 | 962 | 860 |
| 120 | 1223 | 170 | sericitized andes tuff w abundant stz veins < 5% py (3d) | 114 | .4 | 19 | 210 | 27 | 115 | 360 |
| 121 | 1305 | 200 | silicified lapilli tuff w up to 10% fine py | | | | | | | |
| 122 | 1185 | 875 | graphitic shear with silicif/carbon host rock, abund stz veins, up to 10% py | 8 | 1.4 | 30 | 135 | 25 | 30 | 2000 |
| 123 | 1419 | 297 | sheared, carbonitized coarse pyroclastic w stz-carb-chl-py lenses/veins, 0-3% py | 2 | .3 | 14 | 334 | 2 | 23 | 1800 |
| 124 | 1415 | 300 | more sheared, carbon, sericit. coarse pyroclastic w up to 10% py (2g) | 6 | 2.1 | 15 | 27 | 27 | 75 | 1100 |
| 125 | 1405 | 330 | sheared, heavily carbonitized coarse pyroclastic, ank br vns up to 1m wide which appear to be concord. w shearing, 5-10% py, tr sp? | 3 | .2 | 8 | 102 | 8 | 30 | 710 |
| 126 | 1205 | 345 | 1m chip across sulfide-br vns on Fw of felsic dike. | 24 | 3.1 | 5 | 29 | 19 | 94 | 660 |
| 127 | 1195 | 342 | ankeritic sulfide-br, Hw of felsic dike, overall 3-5% py | 3 | .3 | 9 | 38 | 2 | 71 | 530 |
| 128 | 1216 | 325 | ~1m chip across sulfide rich zone in Fw of andesitic dike | 65 | 1.1 | 5 | 119 | 16 | 221 | 600 |
| 129 | 1225 | 312 | 5-10% py plus numerous stz veins in silicif, sulfide zone Fw to dike | 131 | 4.3 | 11 | 340 | 25 | 827 | 1600 |
| 130 | 1395 | 350 | carbonate, sericitized coarse pyroclastic (2g) along trace of dike, up to 10% py | 3 | .1 | 10 | 147 | 15 | 27 | 960 |
| 131 | 1399 | 381 | 1m chip (2g), sericitized, kaolinized, fine silic. stars, 5-10% py | 14 | .7 | 6 | 44 | 13 | 44 | 1200 |
| 132 | 1399 | 380 | 3 m chip stz-chl-py vns parallel to fol (Az 012/80E) | 103 | 2.2 | 7 | 5 | 15 | 70 | 300 |
| 133 | 1399 | 379 | 2 m chip in altered Fw to stz-chl-py vns (above), 5-3% py | 8 | .3 | 8 | 35 | 23 | 27 | 750 |
| 134 | 1365 | 432 | up to 20% py in carbonitized/sericitized (2g) adjacent to felsic dike | 40 | 2.3 | 10 | 25 | 14 | 109 | 830 |
| 135 | 1338 | 436 | brecciated dike w abundant stz-veins in med coarse (2g) weathered | 98 | 4.5 | 12 | 798 | 30 | 133 | 1000 |
| 136 R | 1226W | 171W | fol alt - qtz veins, 1-3% diss pyr | 243 | 1.5 | 14 | 144 | 39 | 359 | 150 |
| 137 R | 1230W | 170W | mineralized py pods along 0.75 fracture in alt | 1 | .1 | 8 | 73 | 12 | 17 | 180 |
| 138 R | 1095N | 110W | flow banded rhy w 5% py - arsenic along flow bands | 41 | .5 | 8 | 105 | 9 | 145 | 70 |
| 139 R | 1069N | 110W | lithic and - py arsenic along fractures | 24 | .3 | 6 | 128 | 8 | 22 | 150 |
| 140 R | 1280N | 790W | autobre, green alt, silic diabase - py encrusted frags | 5 | .2 | 8 | 334 | 24 | 13 | 2000 |
| 141 R | 1290W | 750W | br diabase - altered to white coral frags - py mx | 5 | .1 | 8 | 388 | 17 | 15 | 1700 |

Big Andesite like

ZONE I EAST GRID

Rock Sample Record Sheet

| Sample No. | Location | | Description | Geochem. | | | | | | |
|------------|----------|------------|--|----------|----|-----|----|----|-----|-----|
| | | | | Au | Ag | Cu | Zn | Pb | As | Hg |
| 142 | R | 1250N 815E | fault zone, graphitic actinolite, 3-5% py | 15 | .1 | 33 | 28 | 11 | 53 | 200 |
| 143 | R | 1275N 815E | fault, qtz-carb breccia veins, Tr cpy, 1-2% py | 15 | .1 | 182 | 76 | 3 | 115 | 100 |
| 144 | | 1270N 815E | | | | | | | | |
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GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT 134 File # 90-2564 Page 1
2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

Table with columns: SAMPLE#, and elements (Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K, Au**, Hg) with corresponding concentration values in various units (ppm, ppb, %).

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-P2 Rock P3 Soil AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUL 16 1990 DATE REPORT MAILED: July 27/90 SIGNED BY: D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au* | Hg |
|----------------|-----|-----|------|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|-----|-------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| R 13+90N 2+70W | 1 | 9 | 13 | 144 | .1 | 3 | 15 | 815 | 7.31 | 4 | 5 | ND | 1 | 69 | 1.7 | 5 | 2 | 87 | 1.37 | .255 | 12 | 4 | 1.20 | 74 | .01 | 4 | 2.30 | .05 | .15 | 1 | 1 | 540 |
| R 13+80N 6+30W | 2 | 9 | 12 | 107 | .2 | 4 | 12 | 961 | 6.68 | 8 | 5 | ND | 2 | 64 | 1.5 | 4 | 2 | 50 | 2.16 | .174 | 6 | 4 | 1.17 | 47 | .01 | 4 | .94 | .03 | .13 | 1 | 6 | 730 |
| R 13+80N 2+80W | 1 | 9 | 11 | 176 | .1 | 3 | 18 | 381 | 7.18 | 8 | 5 | ND | 1 | 29 | 1.6 | 7 | 2 | 102 | .73 | .169 | 9 | 4 | 1.17 | 68 | .01 | 6 | 2.92 | .04 | .21 | 1 | 8 | 780 |
| R 13+70W 7+00W | 2 | 6 | 2 | 200 | .1 | 2 | 14 | 1005 | 7.86 | 5 | 5 | ND | 1 | 55 | 2.7 | 3 | 2 | 116 | 1.99 | .221 | 12 | 4 | 1.28 | 60 | .01 | 9 | 2.76 | .06 | .10 | 1 | 7 | 620 |
| R 13+70W 2+60W | 1 | 5 | 22 | 336 | .1 | 4 | 15 | 1956 | 7.56 | 4 | 5 | ND | 1 | 99 | 3.5 | 2 | 2 | 71 | 3.15 | .222 | 10 | 2 | 1.37 | 79 | .01 | 2 | 2.23 | .05 | .14 | 1 | 5 | 840 |
| R 13+60N 2+35W | 2 | 9 | 9 | 17 | .3 | 2 | 2 | 797 | 2.41 | 20 | 5 | ND | 4 | 19 | .2 | 2 | 2 | 4 | 1.06 | .009 | 18 | 2 | .30 | 72 | .01 | 2 | .21 | .05 | .07 | 1 | 10 | 220 |
| R 13+00W 7+00W | 3 | 6 | 11 | 109 | .1 | 6 | 13 | 2212 | 5.93 | 20 | 5 | ND | 1 | 22 | .9 | 9 | 2 | 35 | .96 | .171 | 9 | 5 | .32 | 39 | .01 | 8 | .37 | .01 | .14 | 1 | 8 | 1500 |
| R 11+10N 8+60E | 1 | 18 | 4 | 19 | .1 | 12 | 4 | 123 | 1.99 | 58 | 5 | ND | 1 | 119 | .2 | 15 | 2 | 5 | .66 | .072 | 3 | 6 | .13 | 56 | .01 | 2 | .20 | .02 | .13 | 1 | 12 | 12000 |
| R 9+30N 8+50W | 4 | 5 | 2 | 108 | .1 | 7 | 2 | 311 | 2.30 | 2 | 5 | ND | 4 | 8 | .2 | 2 | 2 | 1 | .13 | .010 | 28 | 7 | .10 | 140 | .01 | 2 | .36 | .02 | .24 | 1 | 7 | 180 |
| UR 3225N 1700E | 1 | 96 | 2493 | 4262 | 8.4 | 5 | 10 | 257 | 6.19 | 84 | 5 | ND | 1 | 178 | 16.5 | 33 | 2 | 15 | 1.28 | .073 | 2 | 4 | .02 | 25 | .01 | 4 | .17 | .01 | .13 | 1 | 115 | 11000 |
| UR 3000N 1700E | 4 | 7 | 2 | 50 | .1 | 4 | 4 | 339 | 5.63 | 7 | 5 | ND | 1 | 26 | 1.0 | 2 | 2 | 2 | .72 | .004 | 2 | 3 | .42 | 2 | .01 | 2 | .03 | .01 | .01 | 1 | 66 | 400 |
| STANDARD C | 18 | 59 | 43 | 132 | 7.3 | 73 | 32 | 1041 | 4.21 | 38 | 21 | 8 | 36 | 52 | 18.1 | 15 | 17 | 55 | .54 | .096 | 37 | 59 | .95 | 178 | .07 | 36 | 2.03 | .06 | .14 | 12 | - | 1200 |

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|--------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| AP TRENCH #10 GRAB | 3 | 319 | 17046 | 3174 | 64.0 | 7 | 7 | 43 | 18.23 | 7842 | 5 | 20 | 2 | 3 | 11.1 | 130 | 8 | 1 | .02 | .001 | 2 | 5 | .01 | 3 | .01 | 2 | .09 | .01 | .03 | 2 | 38748 | 13400 |
| CR 030N 950W | 3 | 5 | 132 | 112 | .1 | 5 | 2 | 31 | 2.04 | 600 | 5 | ND | 2 | 62 | .2 | 10 | 2 | 6 | .11 | .103 | 13 | 16 | .01 | 188 | .01 | 3 | .34 | .01 | .25 | 1 | 71 | 260 |
| CR 025N 955W | 5 | 19 | 427 | 785 | 1.1 | 9 | 5 | 48 | 2.60 | 800 | 5 | ND | 1 | 15 | 4.8 | 27 | 2 | 4 | .13 | .058 | 5 | 8 | .01 | 35 | .01 | 4 | .25 | .01 | .15 | 1 | 197 | 560 |
| CR 00N 840W | 1 | 37 | 21 | 139 | .2 | 61 | 25 | 1309 | 6.00 | 39 | 6 | ND | 1 | 127 | 1.6 | 4 | 4 | 135 | 4.47 | .193 | 10 | 96 | 3.41 | 92 | .01 | 2 | 3.06 | .04 | .07 | 1 | 6 | 70 |
| CR 025S 1000W | 10 | 11 | 49 | 4 | .3 | 11 | 3 | 245 | 2.22 | 397 | 5 | ND | 1 | 7 | .2 | 17 | 2 | 2 | .03 | .038 | 2 | 10 | .01 | 166 | .01 | 5 | .17 | .01 | .11 | 1 | 40 | 380 |
| CR 174S 653W | 2 | 40 | 60 | 74 | 3.3 | 37 | 27 | 310 | 7.44 | 223 | 5 | ND | 1 | 37 | .2 | 4 | 2 | 45 | .67 | .236 | 8 | 30 | .28 | 21 | .01 | 3 | .49 | .04 | .11 | 1 | 68 | 40 |
| CR 180S 620W | 1 | 98 | 12 | 82 | .6 | 32 | 22 | 1183 | 7.07 | 50 | 8 | ND | 1 | 54 | .6 | 2 | 4 | 199 | 1.42 | .207 | 10 | 69 | 3.32 | 39 | .01 | 2 | 3.73 | .03 | .05 | 1 | 8 | 50 |
| CR 185S 640W | 1 | 19 | 14 | 123 | .5 | 35 | 24 | 1190 | 6.54 | 38 | 5 | ND | 1 | 96 | 1.5 | 2 | 2 | 188 | 2.46 | .178 | 9 | 82 | 2.64 | 39 | .01 | 2 | 2.90 | .06 | .03 | 1 | 10 | 40 |
| CR 185S 602W | 2 | 9 | 17 | 40 | .4 | 13 | 6 | 176 | 1.77 | 89 | 5 | ND | 1 | 21 | .2 | 2 | 2 | 5 | .30 | .055 | 11 | 4 | .11 | 89 | .01 | 4 | .39 | .02 | .18 | 1 | 15 | 70 |
| CR 185S 600W | 7 | 16 | 19 | 65 | 1.0 | 14 | 6 | 571 | 1.98 | 103 | 5 | ND | 2 | 40 | .2 | 2 | 4 | 4 | .63 | .041 | 12 | 7 | .18 | 96 | .01 | 3 | .38 | .01 | .19 | 1 | 13 | 120 |
| CR 190S 640W | 2 | 72 | 34 | 329 | 1.8 | 12 | 20 | 339 | 5.05 | 153 | 6 | ND | 1 | 57 | 2.1 | 17 | 2 | 14 | 1.34 | .223 | 8 | 2 | .23 | 31 | .01 | 3 | .48 | .04 | .22 | 1 | 29 | 100 |
| CR 230S 770W | 22 | 16 | 67 | 76 | 3.7 | 8 | 3 | 29 | 2.35 | 174 | 5 | ND | 1 | 11 | .2 | 10 | 2 | 8 | .05 | .023 | 4 | 17 | .01 | 123 | .01 | 5 | .22 | .02 | .17 | 1 | 304 | 90 |
| CR 245S 780W | 1 | 22 | 7 | 48 | .1 | 13 | 14 | 541 | 3.47 | 17 | 5 | ND | 1 | 171 | .2 | 3 | 2 | 11 | 3.70 | .081 | 13 | 2 | 1.21 | 104 | .01 | 4 | .54 | .03 | .22 | 1 | 2 | 20 |
| CR 250S 775W | 4 | 5 | 13 | 74 | 1.1 | 11 | 4 | 27 | 2.70 | 170 | 5 | ND | 1 | 47 | .2 | 3 | 3 | 11 | .13 | .115 | 6 | 29 | .02 | 142 | .01 | 6 | .17 | .01 | .28 | 1 | 81 | 90 |
| CR 260S 77W | 1 | 8 | 8 | 10 | .5 | 4 | 3 | 1578 | 2.40 | 44 | 5 | ND | 2 | 52 | .2 | 2 | 3 | 1 | 2.20 | .012 | 11 | 2 | .72 | 36 | .01 | 7 | .35 | .01 | .18 | 1 | 70 | 10 |
| CR 270S 760W | 4 | 12 | 13 | 26 | .4 | 44 | 23 | 404 | 7.45 | 84 | 5 | ND | 1 | 35 | .3 | 2 | 4 | 30 | .75 | .131 | 6 | 40 | .23 | 17 | .01 | 2 | .28 | .02 | .16 | 1 | 16 | 40 |
| CR 300S 860W | 1 | 20 | 9 | 61 | .1 | 14 | 12 | 632 | 3.22 | 15 | 5 | ND | 3 | 102 | .3 | 2 | 2 | 29 | 3.45 | .088 | 24 | 7 | 1.60 | 135 | .01 | 3 | .84 | .03 | .19 | 1 | 4 | 30 |
| CR 300S 775W | 9 | 12 | 32 | 24 | 1.9 | 13 | 3 | 193 | 3.12 | 133 | 5 | ND | 1 | 20 | .2 | 2 | 2 | 5 | .40 | .026 | 8 | 34 | .07 | 57 | .01 | 3 | .13 | .02 | .15 | 2 | 41 | 30 |
| CR 300S 610W | 6 | 9 | 25 | 5 | .1 | 6 | 3 | 330 | 1.53 | 19 | 5 | ND | 6 | 19 | .2 | 2 | 2 | 2 | .08 | .019 | 32 | 3 | .05 | 167 | .01 | 3 | .39 | .01 | .26 | 1 | 6 | 40 |
| CR 370S 595W | 3 | 2 | 9 | 5 | .1 | 3 | 1 | 25 | .40 | 54 | 5 | ND | 8 | 2 | .2 | 2 | 2 | 1 | .02 | .012 | 37 | 10 | .02 | 81 | .01 | 6 | .42 | .01 | .21 | 1 | 6 | 10 |
| CR 380S 820W | 3 | 48 | 470 | 238 | 3.1 | 31 | 20 | 37 | 7.05 | 389 | 5 | ND | 1 | 35 | .2 | 6 | 2 | 11 | .61 | .254 | 7 | 9 | .01 | 15 | .01 | 4 | .32 | .01 | .23 | 1 | 337 | 180 |
| CR 380S 575W | 1 | 20 | 5 | 129 | .1 | 2 | 21 | 1725 | 7.52 | 2 | 5 | ND | 1 | 76 | 1.3 | 2 | 2 | 72 | 2.90 | .100 | 10 | 4 | 2.09 | 102 | .01 | 3 | 3.00 | .04 | .15 | 1 | 1 | 20 |
| CR 405S 705W | 19 | 18 | 35 | 18 | 2.3 | 18 | 5 | 44 | 1.93 | 94 | 5 | ND | 1 | 12 | .2 | 2 | 2 | 4 | .05 | .045 | 8 | 8 | .02 | 100 | .01 | 6 | .26 | .02 | .17 | 1 | 25 | 120 |
| CR 450S 845W | 4 | 2 | 10 | 39 | .1 | 3 | 1 | 49 | 1.03 | 75 | 5 | ND | 1 | 4 | .2 | 2 | 2 | 1 | .04 | .009 | 16 | 18 | .02 | 90 | .01 | 5 | .29 | .01 | .18 | 2 | 5 | 5 |
| CR 495S 785W | 13 | 54 | 106 | 308 | 2.4 | 42 | 12 | 955 | 4.31 | 114 | 8 | ND | 1 | 124 | 2.2 | 5 | 3 | 22 | 2.01 | .084 | 5 | 7 | .69 | 55 | .01 | 2 | .35 | .01 | .18 | 1 | 77 | 100 |
| CR 510S 760W | 7 | 24 | 43 | 46 | 2.6 | 7 | 5 | 63 | 3.83 | 309 | 5 | ND | 1 | 37 | .2 | 5 | 2 | 27 | .33 | .208 | 8 | 13 | .07 | 72 | .01 | 4 | .34 | .05 | .12 | 2 | 180 | 80 |
| R 1800N 525W | 2 | 4 | 4 | 145 | .1 | 6 | 12 | 1236 | 6.52 | 4 | 7 | ND | 1 | 130 | 1.2 | 2 | 2 | 86 | 2.39 | .188 | 14 | 4 | 1.28 | 58 | .01 | 2 | 2.37 | .05 | .10 | 1 | 2 | 200 |
| R 1705N 600W | 6 | 8 | 16 | 30 | .1 | 6 | 3 | 219 | 3.82 | 7 | 5 | ND | 5 | 5 | .2 | 2 | 2 | 10 | .04 | .017 | 25 | 25 | .14 | 122 | .01 | 3 | .50 | .02 | .12 | 1 | 5 | 560 |
| R 1550N 500W | 2 | 8 | 9 | 143 | .1 | 3 | 13 | 2946 | 6.60 | 9 | 6 | ND | 1 | 134 | 1.4 | 2 | 3 | 103 | 5.13 | .183 | 11 | 3 | 2.33 | 78 | .01 | 4 | 1.75 | .05 | .04 | 1 | 44 | 320 |
| R 1520N 810W | 7 | 2 | 7 | 34 | .3 | 2 | 8 | 3999 | 5.75 | 5 | 8 | ND | 2 | 293 | 1.4 | 2 | 10 | 38 | 11.40 | .104 | 7 | 5 | 3.15 | 41 | .01 | 2 | .89 | .02 | .05 | 1 | 2 | 1800 |
| R 1420N 852W | 507 | 10 | 57 | 78 | .2 | 9 | 20 | 975 | 10.86 | 229 | 5 | ND | 1 | 47 | 1.6 | 11 | 3 | 17 | .96 | .156 | 6 | 3 | .32 | 8 | .01 | 2 | .39 | .04 | .18 | 1 | 6 | 1200 |
| R 1400N 533W | 5 | 6 | 9 | 6 | .1 | 6 | 10 | 120 | 4.00 | 7 | 5 | ND | 1 | 20 | .2 | 4 | 3 | 13 | .42 | .149 | 6 | 22 | .04 | 24 | .01 | 6 | .34 | .01 | .22 | 1 | 1 | 730 |
| R 1372N 516W | 6 | 5 | 5 | 78 | .1 | 7 | 5 | 611 | 5.53 | 10 | 7 | ND | 1 | 22 | .2 | 2 | 3 | 9 | 1.08 | .041 | 10 | 5 | .53 | 54 | .01 | 3 | 1.07 | .01 | .15 | 1 | 1 | 760 |
| R 1330N 573W | 10 | 4 | 9 | 12 | .1 | 6 | 2 | 31 | 2.53 | 6 | 5 | ND | 2 | 4 | .2 | 2 | 2 | 2 | .01 | .015 | 14 | 28 | .02 | 79 | .01 | 2 | .26 | .01 | .24 | 1 | 1 | 2300 |
| R 1320N 507W | 5 | 8 | 14 | 140 | .5 | 5 | 11 | 188 | 7.11 | 23 | 5 | ND | 2 | 10 | 1.1 | 9 | 2 | 12 | .20 | .119 | 8 | 3 | .05 | 18 | .01 | 3 | .46 | .01 | .26 | 1 | 4 | 2400 |
| R 1290N 750W | 9 | 8 | 17 | 388 | .1 | 8 | 10 | 158 | 5.26 | 15 | 5 | ND | 2 | 27 | 1.2 | 4 | 2 | 19 | .39 | .078 | 10 | 23 | .15 | 33 | .01 | 2 | .51 | .03 | .19 | 1 | 5 | 4900 |
| STANDARD C/AU-R | 18 | 58 | 41 | 131 | 6.9 | 68 | 31 | 1049 | 3.95 | 39 | 20 | 7 | 37 | 52 | 18.6 | 14 | 19 | 55 | .51 | .090 | 37 | 56 | .90 | 181 | .07 | 32 | 1.90 | .06 | .14 | 11 | 475 | 1200 |

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| R 1280W 790W | 4 | 8 | 24 | 330 | .2 | 4 | 10 | 1370 | 15.20 | 13 | 5 | ND | 1 | 29 | .2 | 3 | 2 | 72 | 1.66 | .166 | 8 | 12 | .63 | 14 | .01 | 8 | 1.20 | .03 | .08 | 1 | 5 | 2600 |
| R 1280W 760W | 25 | 145 | 142 | 159 | .8 | 1 | 7 | 92 | 18.73 | 36 | 5 | ND | 1 | 4 | .3 | 13 | 2 | 8 | .12 | .091 | 2 | 2 | .02 | 1 | .01 | 6 | .26 | .01 | .17 | 2 | 16 | 15000 |
| R 1230N 170W | 1 | 8 | 12 | 73 | .3 | 5 | 15 | 1241 | 7.14 | 17 | 5 | ND | 1 | 13 | 1.1 | 2 | 2 | 38 | .76 | .118 | 10 | 12 | .96 | 129 | .01 | 2 | 1.93 | .01 | .20 | 1 | 1 | 180 |
| R 1228N 240W | 5 | 4 | 16 | 58 | 1.7 | 5 | 2 | 356 | 3.03 | 118 | 5 | ND | 1 | 12 | .3 | 5 | 2 | 2 | .33 | .039 | 10 | 2 | .11 | 44 | .01 | 3 | .30 | .01 | .18 | 1 | 40 | 330 |
| R 1220W 264W | 4 | 3 | 16 | 16 | 2.4 | 4 | 2 | 218 | 1.92 | 120 | 8 | ND | 1 | 8 | .2 | 7 | 2 | 3 | .10 | .074 | 7 | 1 | .02 | 105 | .01 | 5 | .25 | .01 | .19 | 1 | 50 | 310 |
| R 1000W 800W | 2 | 74 | 4 | 86 | .4 | 27 | 11 | 715 | 3.55 | 4 | 5 | ND | 1 | 76 | .9 | 2 | 2 | 53 | 2.17 | .107 | 4 | 28 | 1.23 | 115 | .20 | 4 | 1.63 | .03 | .08 | 1 | 1 | 60 |
| R 1710N 585W | 4 | 41 | 14 | 71 | .1 | 9 | 10 | 444 | 4.58 | 8 | 5 | ND | 1 | 28 | .2 | 2 | 2 | 41 | .90 | .063 | 9 | 12 | .62 | 41 | .01 | 4 | .91 | .03 | .08 | 1 | 3 | 230 |
| R 1420N 850W | 3 | 9 | 24 | 84 | .1 | 2 | 13 | 1687 | 7.59 | 8 | 5 | ND | 1 | 117 | .2 | 5 | 2 | 66 | 3.80 | .198 | 8 | 10 | 1.32 | 53 | .01 | 2 | 1.24 | .04 | .09 | 1 | 1 | 220 |
| R 1226N 171W | 2 | 14 | 39 | 144 | 1.5 | 2 | 6 | 355 | 5.50 | 359 | 6 | ND | 1 | 13 | .2 | 7 | 2 | 7 | .10 | .097 | 8 | 1 | .03 | 132 | .01 | 5 | .28 | .01 | .29 | 1 | 243 | 150 |
| R 1100N 110W | 4 | 10 | 220 | 1276 | 11.7 | 5 | 10 | 580 | 7.38 | 16322 | 5 | 4 | 1 | 14 | 5.1 | 265 | 2 | 1 | 1.19 | .010 | 2 | 7 | .52 | 19 | .01 | 3 | .18 | .01 | .12 | 1 | 4123 | 350 |
| R 1096N 110W | 4 | 6 | 8 | 128 | .3 | 5 | 1 | 878 | 3.09 | 22 | 5 | ND | 1 | 14 | .9 | 2 | 4 | 1 | .39 | .017 | 6 | 3 | .33 | 79 | .01 | 5 | .57 | .01 | .16 | 1 | 24 | 150 |
| R 1095N 110W | 7 | 8 | 8 | 105 | .5 | 6 | 1 | 963 | 2.49 | 155 | 5 | ND | 1 | 19 | .3 | 2 | 2 | 1 | .67 | .011 | 5 | 3 | .22 | 43 | .01 | 2 | .24 | .01 | .14 | 1 | 61 | 70 |
| R 790N 190W | 2 | 15 | 266 | 257 | 3.4 | 9 | 11 | 1376 | 4.61 | 277 | 5 | ND | 1 | 38 | 1.1 | 13 | 2 | 6 | 2.83 | .059 | 2 | 7 | 1.16 | 27 | .01 | 2 | .25 | .01 | .14 | 1 | 219 | 110 |
| R 18+00N D+30E | 3 | 14 | 45 | 209 | 4.9 | 7 | 1 | 41 | 2.09 | 821 | 5 | 2 | 2 | 4 | 4 | 6 | 2 | 1 | .02 | .003 | 12 | 4 | .01 | 104 | .01 | 3 | .14 | .01 | .15 | 1 | 2491 | 840 |
| VR-1-L.S.-90 | 6 | 12 | 25 | 100 | 1.6 | 5 | 1 | 108 | 2.45 | 346 | 9 | ND | 2 | 3 | .6 | 6 | 2 | 1 | .01 | .009 | 13 | 1 | .01 | 57 | .01 | 8 | .19 | .01 | .17 | 1 | 108 | 240 |
| VR-2-L.S.-90 | 7 | 9 | 28 | 175 | 2.3 | 5 | 1 | 457 | 2.20 | 740 | 5 | ND | 2 | 10 | .7 | 11 | 2 | 1 | .36 | .012 | 15 | 5 | .12 | 60 | .01 | 2 | .16 | .01 | .14 | 1 | 101 | 200 |
| VR-3-L.S.-90 | 4 | 3 | 47 | 15 | .9 | 7 | 1 | 58 | 1.09 | 680 | 5 | ND | 4 | 3 | .2 | 6 | 2 | 1 | .01 | .003 | 20 | 5 | .01 | 176 | .01 | 2 | .12 | .01 | .20 | 1 | 193 | 160 |
| VR-4-L.S.-90 | 5 | 4 | 9 | 10 | 1.1 | 7 | 1 | 31 | .91 | 66 | 5 | ND | 5 | 3 | .2 | 4 | 2 | 1 | .01 | .004 | 21 | 6 | .01 | 200 | .01 | 4 | .15 | .01 | .22 | 1 | 58 | 130 |
| VR 2950N 2250E | 3 | 58 | 88 | 12 | .9 | 2 | 11 | 82 | 19.15 | 102 | 5 | ND | 1 | 22 | .3 | 36 | 3 | 27 | .18 | .035 | 2 | 1 | .04 | 7 | .01 | 6 | .29 | .01 | .19 | 1 | 31 | 820 |
| VR 2901N 2326E | 3 | 13 | 34 | 624 | 4.2 | 4 | 11 | 65 | 5.75 | 33 | 5 | ND | 1 | 11 | 2.7 | 16 | 2 | 18 | .52 | .177 | 7 | 1 | .07 | 15 | .01 | 4 | .42 | .02 | .22 | 1 | 29 | 710 |
| VR 2900N 2150E | 4 | 3 | 11 | 100 | .2 | 3 | 2 | 333 | 2.06 | 6 | 5 | ND | 1 | 74 | .2 | 2 | 2 | 5 | .86 | .016 | 16 | 5 | .33 | 68 | .01 | 3 | .93 | .03 | .11 | 1 | 1 | 210 |
| VR 2798N 1830E | 6 | 28 | 4 | 64 | .1 | 12 | 7 | 254 | 1.34 | 10 | 5 | ND | 1 | 401 | .7 | 8 | 2 | 8 | 2.65 | .046 | 3 | 6 | .15 | 62 | .01 | 7 | .25 | .03 | .12 | 1 | 42 | 600 |
| VR 2795N 1845E | 1 | 37 | 10 | 53 | .1 | 9 | 9 | 448 | 2.36 | 8 | 5 | ND | 1 | 538 | .2 | 7 | 2 | 12 | 3.09 | .060 | 3 | 9 | .59 | 56 | .01 | 7 | .26 | .03 | .13 | 1 | 45 | 500 |
| VR 2700N 1975E | 7 | 5 | 15 | 144 | .3 | 5 | 1 | 32 | .85 | 179 | 5 | ND | 2 | 9 | .2 | 3 | 2 | 1 | .04 | .001 | 19 | 5 | .02 | 48 | .01 | 5 | .22 | .01 | .16 | 1 | 40 | 240 |
| VR 2695N 2155E | 1 | 140 | 58 | 77 | .1 | 2 | 20 | 627 | 6.17 | 16 | 5 | ND | 1 | 228 | .5 | 2 | 2 | 137 | 4.18 | .143 | 5 | 11 | 1.16 | 29 | .18 | 6 | 1.70 | .04 | 1.14 | 1 | 2 | 30 |
| VR 2600N 1500E | 1 | 107 | 17 | 40 | .7 | 72 | 24 | 214 | 7.49 | 20 | 8 | ND | 1 | 4 | .2 | 2 | 2 | 33 | .03 | .057 | 2 | 36 | .57 | 46 | .01 | 5 | 1.31 | .02 | .13 | 1 | 8 | 280 |
| VR 2510N 2145E | 3 | 390 | 15873 | 99999 | 24.3 | 8 | 20 | 1138 | 2.88 | 165 | 5 | ND | 1 | 168 | 479.4 | 22 | 2 | 41 | 3.94 | .048 | 2 | 13 | 1.11 | 22 | .01 | 5 | .24 | .01 | .07 | 2 | 676 | 128000 |
| VR 2300N 2175E | 2 | 85 | 33 | 178 | .3 | 15 | 11 | 358 | 3.15 | 29 | 5 | ND | 1 | 38 | .7 | 6 | 3 | 39 | .58 | .103 | 9 | 10 | .26 | 58 | .01 | 10 | .60 | .02 | .30 | 1 | 37 | 1050 |
| VR 2145N 2240E | 7 | 72545 | 21449 | 40346 | 173.9 | 9 | 15 | 316 | 9.81 | 38 | 7 | 11 | 1 | 80 | 193.7 | 61 | 2 | 12 | .24 | .017 | 2 | 10 | .19 | 9 | .01 | 9 | .29 | .01 | .06 | 1 | 15798 | 162000 |
| VR 1900N 1525E | 1 | 246 | 139 | 234 | .6 | 4 | 16 | 742 | 7.28 | 5 | 5 | ND | 1 | 34 | 1.1 | 7 | 2 | 106 | .67 | .221 | 6 | 13 | 1.89 | 119 | .11 | 3 | 3.08 | .02 | .15 | 1 | 18 | 600 |
| STANDARD C/AU-R | 18 | 62 | 43 | 131 | 7.0 | 69 | 31 | 1051 | 3.96 | 42 | 18 | 7 | 36 | 53 | 18.5 | 14 | 20 | 56 | .51 | .090 | 37 | 60 | .87 | 180 | .07 | 36 | 1.86 | .06 | .13 | 11 | 461 | 1500 |

ASSAY RECOMMENDED for Cu, Pb, Zn As > 1%
Ag > 30 ppm

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT 134 File # 90-2376 Page 1
2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

Table with columns: SAMPLE#, Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K, W, Au**, Hg. Rows list various sample IDs and their corresponding element concentrations in ppm and ppb.

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: Rock AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: JUL 9 1990 DATE REPORT MAILED: July 14/90 SIGNED BY: D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| R 1680N 645W | 3 | 6 | 26 | 229 | .1 | 8 | 10 | 1069 | 5.31 | 6 | 5 | ND | 1 | 58 | .6 | 2 | 2 | 77 | 1.68 | .167 | 11 | 5 | 1.02 | 66 | .01 | 2 | 1.49 | .05 | .08 | 1 | 2 | 430 |
| R 1630N 1010W | 2 | 6 | 259 | 38 | 1.1 | 1 | 2 | 385 | 2.05 | 3 | 5 | ND | 1 | 126 | .2 | 2 | 2 | 7 | 1.32 | .050 | 3 | 5 | .19 | 48 | .01 | 2 | .58 | .01 | .04 | 1 | 2 | 40 |
| R 1625N 780W | 8 | 10 | 16 | 60 | .1 | 3 | 8 | 170 | 3.61 | 7 | 5 | ND | 2 | 16 | .2 | 2 | 3 | 14 | .44 | .111 | 10 | 6 | .11 | 48 | .01 | 4 | .40 | .03 | .13 | 1 | 3 | 1200 |
| R 1550N 220W | 2 | 17 | 244 | 72 | 64.0 | 1 | 13 | 21 | 7.19 | 2317 | 5 | ND | 1 | 2 | .2 | 84 | 2 | 13 | .01 | .019 | 2 | 2 | .01 | 15 | .01 | 3 | .23 | .01 | .17 | 1 | 1187 | 4300 |
| R 1419N 297W | 2 | 14 | 2 | 334 | .3 | 5 | 12 | 2306 | 7.34 | 23 | 5 | ND | 1 | 163 | 2.0 | 2 | 4 | 29 | 6.32 | .072 | 5 | 6 | 2.42 | 47 | .01 | 2 | .52 | .01 | .11 | 1 | 2 | 1800 |
| R 1415N 300W | 4 | 15 | 27 | 125 | 2.1 | 2 | 13 | 1537 | 6.31 | 75 | 5 | ND | 1 | 126 | .9 | 5 | 5 | 24 | 3.86 | .132 | 7 | 5 | 1.26 | 45 | .01 | 2 | .38 | .02 | .18 | 1 | 6 | 1100 |
| R 1405N 330W | 4 | 8 | 8 | 102 | .2 | 5 | 12 | 1184 | 6.33 | 30 | 5 | ND | 2 | 55 | .2 | 5 | 2 | 26 | 1.57 | .209 | 14 | 4 | .57 | 90 | .01 | 2 | .74 | .02 | .23 | 1 | 3 | 710 |
| R 13+10N 2+00W | 4 | 7 | 41 | 9 | 6.9 | 2 | 3 | 31 | 3.30 | 269 | 5 | ND | 1 | 6 | .2 | 9 | 2 | 3 | .02 | .012 | 9 | 3 | .01 | 37 | .01 | 2 | .23 | .01 | .23 | 1 | 131 | 730 |
| R 1228N 312W | 5 | 11 | 25 | 340 | 4.3 | 4 | 2 | 154 | 2.52 | 827 | 5 | ND | 2 | 7 | .2 | 21 | 3 | 1 | .08 | .056 | 14 | 5 | .02 | 146 | .01 | 2 | .24 | .01 | .17 | 1 | 131 | 1600 |
| R 12+25W 1+70W | 1 | 321 | 2348 | 1706 | 22.3 | 4 | 11 | 700 | 6.99 | 9602 | 5 | 15 | 1 | 17 | 2.0 | 131 | 8 | 5 | .84 | .092 | 5 | 3 | .30 | 33 | .01 | 2 | .31 | .01 | .23 | 2 | 15381 | 8600 |
| R 12+23N 1+70W | 2 | 19 | 27 | 210 | .4 | 8 | 14 | 1695 | 7.15 | 115 | 5 | ND | 1 | 18 | .7 | 2 | 4 | 37 | 1.56 | .102 | 7 | 9 | 1.23 | 69 | .01 | 2 | 1.85 | .01 | .14 | 1 | 114 | 360 |
| R 1216N 325W | 4 | 5 | 16 | 119 | 1.1 | 4 | 1 | 405 | 1.37 | 221 | 5 | ND | 5 | 4 | .2 | 7 | 2 | 1 | .08 | .008 | 21 | 5 | .02 | 103 | .01 | 2 | .21 | .01 | .14 | 1 | 65 | 600 |
| R 12+10N 1+50W | 6 | 36 | 11 | 33 | 1.0 | 6 | 2 | 560 | 2.38 | 107 | 5 | ND | 1 | 10 | .2 | 2 | 2 | 1 | .32 | .019 | 9 | 7 | .28 | 140 | .01 | 2 | .43 | .01 | .16 | 1 | 64 | 180 |
| R 1205N 345W | 4 | 5 | 19 | 29 | 3.1 | 1 | 2 | 56 | 2.47 | 94 | 5 | ND | 2 | 5 | .2 | 10 | 2 | 4 | .02 | .028 | 13 | 3 | .01 | 134 | .01 | 4 | .26 | .01 | .15 | 1 | 24 | 660 |
| R 1201N 401W | 4 | 35 | 547 | 514 | 20.2 | 8 | 3 | 143 | 1.58 | 1227 | 5 | ND | 1 | 13 | 1.0 | 21 | 2 | 17 | .26 | .132 | 7 | 9 | .02 | 101 | .01 | 5 | .24 | .01 | .16 | 1 | 192 | 7100 |
| R 1201N 399W | 3 | 35 | 590 | 226 | 171.0 | 1 | 13 | 303 | 5.17 | 139 | 5 | ND | 2 | 17 | .2 | 32 | 2 | 40 | .35 | .154 | 9 | 3 | .10 | 37 | .01 | 6 | .51 | .01 | .22 | 1 | 311 | 26000 |
| R 1195N 345W | 3 | 9 | 2 | 38 | .3 | 4 | 3 | 7400 | 6.45 | 71 | 5 | ND | 2 | 111 | 2.8 | 10 | 2 | 2 | 11.48 | .010 | 8 | 2 | 4.61 | 28 | .01 | 2 | .28 | .01 | .09 | 1 | 3 | 930 |
| R 11+90N 6+08W | 3 | 7 | 5 | 128 | .1 | 7 | 10 | 1085 | 5.62 | 8 | 5 | ND | 1 | 41 | .2 | 3 | 2 | 12 | .86 | .115 | 15 | 5 | .29 | 110 | .01 | 2 | .60 | .02 | .19 | 2 | 1 | 380 |
| R 11+90N 5+80W | 3 | 10 | 9 | 348 | .3 | 3 | 12 | 812 | 4.57 | 11 | 5 | ND | 2 | 23 | 1.3 | 2 | 5 | 33 | .39 | .134 | 18 | 6 | .42 | 86 | .01 | 5 | 1.34 | .03 | .19 | 1 | 4 | 2500 |
| R 1185N 875W | 6 | 30 | 25 | 135 | 1.4 | 3 | 7 | 921 | 3.09 | 30 | 5 | ND | 1 | 100 | .2 | 13 | 2 | 14 | 1.25 | .134 | 4 | 4 | .32 | 33 | .01 | 2 | .19 | .02 | .08 | 1 | 8 | 2000 |
| R 11+85N 0+73W | 3 | 10 | 20 | 16 | 2.1 | 5 | 24 | 347 | 9.73 | 166 | 5 | ND | 1 | 25 | .8 | 8 | 7 | 16 | 1.13 | .067 | 4 | 5 | .19 | 16 | .01 | 2 | .41 | .03 | .15 | 1 | 41 | 1300 |
| R 11+70N 1+55W | 7 | 243 | 1857 | 3897 | 308.8 | 1 | 4 | 65 | 9.56 | 25614 | 5 | 10 | 1 | 2 | 8.8 | 667 | 4 | 1 | .02 | .008 | 2 | 3 | .03 | 11 | .01 | 6 | .17 | .01 | .09 | 1 | 10738 | 6800 |
| R 11+70N 1+45W | 4 | 46 | 60 | 731 | 27.3 | 6 | 6 | 71 | 13.22 | 2851 | 5 | 2 | 1 | 3 | 2.1 | 65 | 6 | 1 | .07 | .005 | 2 | 7 | .02 | 5 | .01 | 5 | .19 | .01 | .10 | 1 | 3273 | 5500 |
| R 11+60N 5+50W | 2 | 9 | 7 | 146 | .1 | 5 | 16 | 1485 | 5.92 | 12 | 5 | ND | 1 | 70 | 1.2 | 2 | 3 | 74 | 2.83 | .248 | 12 | 4 | .55 | 77 | .01 | 2 | 1.26 | .04 | .09 | 2 | 19 | 320 |
| R 11+45N 1+45W | 1 | 5 | 19 | 14 | 2.5 | 2 | 4 | 84 | 3.07 | 1921 | 5 | ND | 1 | 5 | .2 | 39 | 2 | 1 | .12 | .011 | 7 | 4 | .02 | 38 | .01 | 3 | .24 | .02 | .15 | 1 | 861 | 60 |
| R 11+05N 1+12W | 4 | 434 | 2942 | 18891 | 390.4 | 6 | 5 | 263 | 6.27 | 12257 | 5 | 4 | 1 | 8 | 39.2 | 669 | 2 | 3 | .35 | .016 | 3 | 7 | .12 | 18 | .01 | 2 | .18 | .01 | .09 | 1 | 3841 | 17000 |
| R 11+00N 0+75W | 2 | 18 | 51 | 250 | 10.3 | 4 | 17 | 1599 | 8.76 | 153 | 5 | ND | 1 | 50 | 1.8 | 8 | 2 | 19 | 2.96 | .348 | 3 | 3 | 1.37 | 28 | .01 | 11 | .47 | .04 | .17 | 1 | 74 | 760 |
| R 10+75N 1+15W | 1 | 14 | 47 | 84 | 2.7 | 3 | 9 | 425 | 7.41 | 35 | 5 | ND | 1 | 7 | 1.4 | 9 | 5 | 39 | .24 | .104 | 5 | 6 | .85 | 35 | .01 | 3 | 2.00 | .01 | .18 | 1 | 13 | 180 |
| R 10+50N 10+05W | 1 | 28 | 10 | 31 | .3 | 16 | 13 | 241 | 3.76 | 21 | 5 | ND | 2 | 7 | .2 | 2 | 2 | 30 | .09 | .014 | 16 | 11 | .69 | 53 | .01 | 6 | 1.11 | .01 | .19 | 1 | 4 | 70 |
| 910N 400W | 3 | 12 | 23 | 87 | 1.6 | 4 | 12 | 177 | 5.27 | 657 | 5 | ND | 2 | 7 | .2 | 7 | 2 | 13 | .33 | .123 | 10 | 7 | .21 | 26 | .01 | 4 | .78 | .01 | .17 | 1 | 208 | 160 |
| R 909N 400W | 3 | 12 | 20 | 98 | .8 | 4 | 9 | 247 | 5.23 | 25 | 5 | ND | 2 | 7 | .2 | 5 | 2 | 14 | .27 | .118 | 9 | 6 | .24 | 34 | .01 | 2 | .89 | .01 | .18 | 1 | 160 | 110 |
| R 875N 410W | 8 | 6 | 2 | 106 | .2 | 7 | 2 | 367 | 2.56 | 7 | 5 | ND | 2 | 3 | .2 | 2 | 2 | 1 | .08 | .006 | 20 | 7 | .28 | 52 | .01 | 3 | .89 | .01 | .17 | 1 | 11 | 80 |
| R 850N 475W | 6 | 8 | 12 | 46 | .6 | 8 | 3 | 374 | 2.59 | 30 | 5 | ND | 2 | 3 | .2 | 2 | 2 | 4 | .04 | .020 | 19 | 9 | .14 | 84 | .01 | 2 | .68 | .01 | .14 | 1 | 17 | 90 |
| R 820N 385W | 4 | 7 | 16 | 13 | .1 | 8 | 2 | 397 | 3.20 | 86 | 5 | ND | 3 | 7 | .2 | 3 | 2 | 1 | .34 | .008 | 13 | 8 | .19 | 115 | .01 | 2 | .62 | .02 | .16 | 1 | 71 | 80 |
| R 700N 250W | 4 | 14 | 124 | 492 | 1.8 | 6 | 13 | 727 | 9.95 | 615 | 5 | ND | 1 | 38 | 3.3 | 6 | 12 | 2 | 1.44 | .017 | 2 | 5 | .33 | 15 | .01 | 2 | .22 | .01 | .14 | 1 | 322 | 190 |
| R 690N 335W | 5 | 13 | 14 | 76 | .1 | 9 | 4 | 1397 | 2.97 | 8 | 5 | ND | 1 | 16 | .6 | 2 | 2 | 1 | 1.40 | .011 | 8 | 5 | .55 | 67 | .01 | 2 | .46 | .01 | .20 | 1 | 2 | 60 |
| R 590N 560W | 6 | 16 | 4 | 157 | .6 | 1 | 2 | 8606 | 3.64 | 59 | 5 | ND | 2 | 138 | 1.1 | 3 | 2 | 2 | 7.81 | .010 | 11 | 3 | 2.09 | 34 | .01 | 2 | .68 | .01 | .11 | 1 | 81 | 80 |
| STANDARD C/AU-R | 19 | 57 | 37 | 133 | 7.2 | 71 | 30 | 1036 | 4.11 | 41 | 19 | 6 | 38 | 53 | 18.7 | 15 | 21 | 56 | .52 | .095 | 37 | 59 | .94 | 178 | .07 | 33 | 1.98 | .06 | .14 | 11 | 489 | 1500 |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|-------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| CR 5+20N 4+40W | 2 | 3 | 13 | 69 | .1 | 3 | 2 | 163 | 1.42 | 7 | 5 | ND | 4 | 4 | .2 | 2 | 2 | 1 | .03 | .005 | 33 | 4 | .03 | 95 | .01 | 5 | .31 | .02 | .12 | 1 | 5 | 20 |
| CR 5+20N 3+45W | 2 | 150 | 5 | 98 | .2 | 5 | 19 | 1040 | 5.93 | 12 | 5 | ND | 1 | 55 | .4 | 2 | 6 | 68 | 1.99 | .147 | 17 | 4 | 1.11 | 108 | .01 | 5 | 1.84 | .04 | .11 | 1 | 10 | 30 |
| CR 5+15N 2+90W | 6 | 4 | 26 | 39 | .6 | 5 | 1 | 21 | .91 | 175 | 5 | ND | 1 | 2 | .2 | 3 | 2 | 1 | .02 | .009 | 35 | 5 | .01 | 125 | .01 | 5 | .18 | .01 | .14 | 1 | 36 | 80 |
| CR 5+00N 10+65W | 1 | 10 | 12 | 119 | .1 | 1 | 10 | 1492 | 4.33 | 2 | 5 | ND | 1 | 56 | .8 | 2 | 2 | 47 | 2.76 | .126 | 14 | 4 | 1.17 | 148 | .01 | 4 | 1.87 | .04 | .11 | 2 | 4 | 20 |
| CR 5+00N 6+85W | 12 | 81 | 56 | 317 | 2.2 | 16 | 9 | 37 | 3.34 | 288 | 5 | ND | 1 | 9 | 1.9 | 23 | 2 | 6 | .06 | .030 | 8 | 8 | .01 | 36 | .01 | 4 | .16 | .04 | .11 | 1 | 74 | 320 |
| CR 5+00N 6+70W | 2 | 21 | 8 | 66 | .1 | 14 | 13 | 219 | 3.68 | 10 | 5 | ND | 4 | 18 | .2 | 4 | 4 | 37 | .25 | .086 | 24 | 12 | 1.54 | 371 | .01 | 6 | 2.01 | .01 | .16 | 1 | 6 | 20 |
| CR 5+00N 6+25W | 2 | 22 | 12 | 63 | .1 | 15 | 13 | 521 | 3.15 | 10 | 6 | ND | 2 | 71 | .2 | 2 | 2 | 32 | 2.40 | .090 | 20 | 11 | 1.72 | 134 | .01 | 4 | 1.71 | .02 | .16 | 1 | 10 | 20 |
| CR 5+00N 4+40W | 16 | 5 | 17 | 35 | .1 | 6 | 1 | 703 | 1.58 | 14 | 5 | ND | 1 | 100 | .2 | 2 | 4 | 1 | 1.29 | .005 | 17 | 7 | .04 | 59 | .01 | 5 | .19 | .03 | .07 | 1 | 8 | 10 |
| CR 4+80N 5+70W | 2 | 7 | 9 | 140 | .1 | 1 | 11 | 1071 | 5.22 | 3 | 5 | ND | 1 | 79 | 1.5 | 2 | 2 | 30 | 2.59 | .266 | 15 | 3 | 1.76 | 83 | .01 | 2 | 1.60 | .03 | .14 | 1 | 8 | 20 |
| CR 4+80N 5+45W | 6 | 5 | 8 | 29 | .1 | 5 | 1 | 15 | 1.28 | 88 | 5 | ND | 1 | 12 | .2 | 2 | 2 | 1 | .01 | .014 | 10 | 5 | .01 | 162 | .01 | 4 | .17 | .01 | .15 | 1 | 22 | 30 |
| CR 4+50N 5+20W | 5 | 5 | 27 | 55 | .3 | 5 | 2 | 50 | 2.08 | 255 | 5 | ND | 1 | 7 | .2 | 3 | 2 | 1 | .02 | .014 | 11 | 6 | .01 | 246 | .01 | 2 | .13 | .01 | .12 | 1 | 46 | 100 |
| CR 4+12N 4+40W | 16 | 8 | 6 | 232 | .1 | 10 | 2 | 71 | 2.06 | 22 | 5 | ND | 1 | 12 | .7 | 2 | 2 | 1 | .17 | .007 | 13 | 12 | .01 | 16 | .01 | 4 | .12 | .09 | .02 | 1 | 11 | 150 |
| CR 3+00N 12+75W | 2 | 8 | 7 | 105 | .1 | 1 | 13 | 1134 | 4.98 | 5 | 5 | ND | 1 | 42 | .4 | 2 | 2 | 56 | 2.43 | .140 | 11 | 4 | 1.31 | 213 | .01 | 8 | 1.87 | .03 | .11 | 2 | 9 | 20 |
| CR 0+85N 2+80W | 1 | 9 | 6 | 63 | .1 | 7 | 18 | 837 | 4.38 | 4 | 5 | ND | 2 | 111 | .2 | 2 | 2 | 28 | 2.85 | .126 | 23 | 4 | .78 | 66 | .01 | 10 | .56 | .03 | .22 | 1 | 16 | 30 |
| CR 0+20N 6+15W | 12 | 6 | 31 | 89 | .6 | 2 | 1 | 11 | 1.25 | 128 | 5 | ND | 1 | 3 | .2 | 5 | 2 | 1 | .01 | .002 | 19 | 4 | .01 | 230 | .01 | 3 | .14 | .01 | .12 | 1 | 32 | 150 |
| CR 0+05N 7+35W | 3 | 67 | 46 | 131 | 2.2 | 18 | 19 | 15 | 5.09 | 737 | 5 | ND | 1 | 7 | .2 | 13 | 2 | 7 | .10 | .054 | 4 | 5 | .01 | 14 | .01 | 7 | .33 | .01 | .18 | 1 | 41 | 100 |
| CR 0+20S 6+20W | 4 | 2 | 16 | 51 | .4 | 3 | 1 | 8 | 1.00 | 127 | 5 | ND | 1 | 2 | .2 | 2 | 2 | 1 | .01 | .002 | 28 | 4 | .01 | 169 | .01 | 4 | .14 | .01 | .15 | 2 | 30 | 50 |
| CR 0+40S 7+25W | 4 | 6 | 13 | 4 | .1 | 7 | 2 | 21 | 1.40 | 43 | 5 | ND | 1 | 4 | .2 | 2 | 2 | 1 | .01 | .001 | 7 | 9 | .01 | 106 | .01 | 4 | .13 | .01 | .15 | 1 | 16 | 40 |
| CR 1+00S 7+20W | 5 | 4 | 11 | 13 | .1 | 5 | 1 | 21 | 1.15 | 90 | 5 | ND | 2 | 3 | .2 | 2 | 2 | 1 | .01 | .008 | 28 | 6 | .01 | 51 | .01 | 4 | .15 | .05 | .07 | 1 | 16 | 50 |
| CR 1+00S 6+75W | 7 | 7 | 21 | 24 | .6 | 5 | 1 | 13 | 1.05 | 89 | 5 | ND | 1 | 10 | .2 | 3 | 2 | 1 | .01 | .010 | 29 | 5 | .01 | 207 | .01 | 4 | .14 | .01 | .14 | 1 | 45 | 40 |
| CR 1+50S 7+00W | 3 | 4 | 5 | 49 | .1 | 5 | 1 | 494 | .75 | 39 | 5 | ND | 1 | 14 | .2 | 2 | 2 | 1 | .77 | .007 | 10 | 6 | .37 | 83 | .01 | 3 | .11 | .01 | .12 | 1 | 184 | 20 |
| CR 1+50S 6+60W | 2 | 35 | 9 | 85 | .4 | 24 | 23 | 975 | 5.17 | 87 | 5 | ND | 1 | 104 | .2 | 2 | 2 | 41 | 2.67 | .221 | 11 | 15 | 1.06 | 60 | .01 | 3 | .50 | .03 | .17 | 2 | 13 | 80 |
| CR 1+57S 6+60W | 21 | 29 | 88 | 30 | 8.2 | 18 | 9 | 48 | 3.45 | 123 | 5 | ND | 1 | 3 | .2 | 8 | 2 | 7 | .01 | .039 | 5 | 4 | .01 | 68 | .01 | 4 | .25 | .01 | .18 | 2 | 108 | 160 |
| CR 1+60S 6+60W | 2 | 127 | 12 | 157 | 1.2 | 44 | 22 | 1307 | 5.24 | 126 | 5 | ND | 1 | 117 | 1.0 | 3 | 2 | 64 | 4.65 | .170 | 7 | 64 | 1.18 | 27 | .01 | 4 | .75 | .03 | .10 | 1 | 32 | 40 |
| CR 1+75S 6+50W | 18 | 33 | 65 | 43 | 3.5 | 33 | 11 | 343 | 3.98 | 76 | 5 | ND | 1 | 7 | .2 | 6 | 2 | 59 | .10 | .046 | 4 | 18 | .45 | 40 | .01 | 5 | .64 | .01 | .11 | 2 | 57 | 100 |
| R 18+60N 0+50E | 10 | 6 | 5 | 104 | 1.7 | 4 | 2 | 287 | 2.22 | 112 | 5 | ND | 1 | 4 | .2 | 3 | 2 | 1 | .22 | .005 | 16 | 5 | .11 | 72 | .01 | 3 | .30 | .01 | .19 | 2 | 48 | 60 |
| R 17+00N 5+70E | 3 | 23 | 9 | 41 | .1 | 4 | 33 | 815 | 7.96 | 2 | 5 | ND | 1 | 114 | .3 | 2 | 2 | 102 | 2.08 | .136 | 5 | 3 | 1.22 | 66 | .01 | 4 | .97 | .03 | .07 | 1 | 10 | 50 |
| R 16+90N 5+50E | 4 | 11 | 8 | 106 | .1 | 4 | 25 | 1298 | 7.41 | 13 | 5 | ND | 1 | 142 | 1.0 | 2 | 4 | 117 | 2.80 | .117 | 8 | 3 | 1.54 | 59 | .01 | 2 | .53 | .03 | .03 | 2 | 19 | 200 |
| R 16+10N 6+25E | 22 | 34 | 34 | 235 | .2 | 5 | 14 | 453 | 8.56 | 212 | 5 | ND | 1 | 115 | 1.9 | 4 | 6 | 25 | 1.87 | .022 | 2 | 5 | .53 | 23 | .01 | 2 | 1.46 | .02 | .07 | 1 | 12 | 880 |
| R 15+80N 6+00E | 13 | 35 | 25 | 142 | .1 | 3 | 14 | 263 | 7.36 | 85 | 5 | ND | 1 | 23 | .6 | 3 | 2 | 22 | .47 | .025 | 2 | 3 | .40 | 27 | .01 | 3 | 1.16 | .02 | .08 | 1 | 15 | 710 |
| R 12+75N 8+15E | 4 | 182 | 3 | 76 | .1 | 13 | 6 | 312 | 1.74 | 115 | 5 | ND | 1 | 323 | .2 | 2 | 2 | 5 | 2.14 | .085 | 3 | 9 | .47 | 68 | .01 | 6 | .27 | .01 | .18 | 1 | 15 | 80 |
| R 12+50N 8+15E | 3 | 33 | 11 | 28 | .1 | 16 | 8 | 152 | 6.67 | 53 | 5 | ND | 1 | 33 | .2 | 449 | 5 | 5 | .40 | .029 | 2 | 8 | .10 | 18 | .01 | 6 | .23 | .01 | .13 | 2 | 15 | 29000 |
| R-1-90-LS | 2 | 57 | 2 | 22 | .1 | 15 | 14 | 576 | 3.55 | 2 | 5 | ND | 1 | 28 | .3 | 2 | 2 | 107 | .69 | .164 | 10 | 30 | 1.22 | 30 | .26 | 6 | 1.42 | .06 | .03 | 2 | 12 | 20 |
| R-2-90-LS | 4 | 40 | 3 | 68 | .1 | 9 | 17 | 550 | 4.99 | 2 | 5 | ND | 1 | 12 | .8 | 6 | 4 | 165 | .60 | .141 | 7 | 8 | 1.29 | 43 | .26 | 2 | 1.52 | .03 | .05 | 1 | 3 | 180 |
| R-3-90-LS | 3 | 36 | 6 | 30 | .1 | 9 | 18 | 486 | 4.70 | 4 | 5 | ND | 1 | 5 | .3 | 2 | 2 | 181 | .51 | .131 | 6 | 6 | 1.50 | 22 | .26 | 5 | 1.54 | .03 | .03 | 2 | 11 | 10 |
| R-4-90-LS | 3 | 41 | 110 | 84 | .6 | 8 | 11 | 244 | 3.20 | 2 | 5 | ND | 1 | 5 | .2 | 2 | 2 | 88 | .34 | .068 | 3 | 8 | .67 | 24 | .18 | 4 | .74 | .02 | .02 | 1 | 8 | 20 |
| STANDARD C/AU-R | 19 | 59 | 41 | 132 | 7.3 | 71 | 32 | 1032 | 4.10 | 40 | 19 | 7 | 36 | 53 | 18.6 | 15 | 18 | 55 | .52 | .096 | 37 | 58 | .94 | 180 | .08 | 34 | 1.96 | .06 | .13 | 12 | 488 | 1600 |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | V | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| R-DG-90-1 | 5 | 4 | 21 | 7 | .3 | 6 | 2 | 36 | 2.05 | 30 | 5 | ND | 2 | 6 | .2 | 3 | 2 | 1 | .03 | .006 | 15 | 5 | .01 | 44 | .01 | 2 | .27 | .01 | .22 | 1 | 7 | 920 |
| R-KP-90-1 | 5 | 3 | 15 | 2 | .2 | 3 | 2 | 63 | 2.12 | 28 | 5 | ND | 2 | 3 | .2 | 2 | 2 | 1 | .05 | .002 | 12 | 3 | .02 | 60 | .01 | 3 | .18 | .02 | .15 | 1 | 10 | 1700 |
| * R 1750N 810W | 11 | 7 | 17 | 72 | .2 | 7 | 6 | 1118 | 3.59 | 19 | 5 | ND | 1 | 340 | .3 | 2 | 2 | 19 | 2.76 | .062 | 10 | 6 | .15 | 183 | .01 | 6 | .38 | .03 | .15 | 1 | 7 | 230 |
| * R 1735N 750W | 2 | 5 | 10 | 40 | .1 | 3 | 11 | 1007 | 6.47 | .9 | 5 | ND | 1 | 26 | .2 | 2 | 6 | 23 | 1.80 | .177 | 10 | 1 | .59 | 31 | .01 | 4 | .32 | .03 | .16 | 1 | 1 | 620 |
| CR 710N 440W | 6 | 13 | 21 | 56 | .1 | 3 | 13 | 537 | 5.95 | 28 | 5 | ND | 1 | 79 | .2 | 8 | 2 | 16 | .96 | .280 | 10 | 1 | .22 | 71 | .01 | 6 | .64 | .02 | .27 | 1 | 5 | 90 |
| CR 705N 710W | 1 | 23 | 15 | 33 | .2 | 2 | 5 | 100 | 3.93 | 554 | 5 | ND | 2 | 13 | .2 | 19 | 3 | 10 | .06 | .090 | 11 | 1 | .02 | 316 | .01 | 4 | .26 | .01 | .19 | 1 | 26 | 750 |
| CR 675N 475W | 4 | 2 | 10 | 19 | .5 | 3 | 1 | 32 | 1.35 | 172 | 5 | ND | 1 | 11 | .2 | 3 | 3 | 1 | .01 | .011 | 14 | 4 | .01 | 178 | .01 | 3 | .15 | .01 | .12 | 1 | 17 | 80 |
| CR 650N 475W | 2 | 3 | 10 | 10 | .2 | 2 | 1 | 18 | .76 | 116 | 5 | ND | 1 | 8 | .2 | 4 | 2 | 1 | .01 | .004 | 12 | 3 | .01 | 116 | .01 | 4 | .11 | .01 | .16 | 1 | 21 | 120 |
| CR 612N 487A W | 5 | 15 | 39 | 4 | 3.9 | 11 | 6 | 53 | 2.35 | 189 | 5 | ND | 1 | 2 | .2 | 3 | 5 | 5 | .01 | .002 | 2 | 5 | .01 | 46 | .01 | 2 | .17 | .01 | .15 | 1 | 99 | 190 |
| CR 610N 487B W | 3 | 21 | 69 | 9 | 2.5 | 5 | 3 | 19 | 2.01 | 423 | 5 | ND | 1 | 4 | .2 | 8 | 2 | 4 | .01 | .023 | 3 | 4 | .01 | 197 | .01 | 2 | .17 | .01 | .19 | 1 | 53 | 90 |
| CR 600N 487A W | 16 | 15 | 98 | 2 | 8.4 | 11 | 3 | 25 | 2.11 | 364 | 5 | ND | 1 | 2 | .2 | 12 | 3 | 4 | .01 | .001 | 3 | 6 | .01 | 99 | .01 | 2 | .15 | .01 | .20 | 1 | 159 | 500 |
| CR 600N 488A W | 3 | 7 | 83 | 4 | 1.6 | 5 | 2 | 26 | 1.55 | 318 | 5 | ND | 1 | 4 | .2 | 5 | 2 | 3 | .01 | .004 | 5 | 3 | .01 | 173 | .01 | 3 | .16 | .01 | .14 | 1 | 53 | 150 |
| CR 300N 885W | 2 | 10 | 17 | 39 | .1 | 3 | 6 | 147 | 3.00 | 549 | 5 | ND | 1 | 10 | .2 | 17 | 2 | 8 | .13 | .090 | 13 | 1 | .05 | 187 | .01 | 4 | .45 | .01 | .19 | 1 | 15 | 210 |
| UR 1609N 1619E | 1 | 101 | 5 | 62 | .1 | 2 | 11 | 738 | 3.73 | 52 | 5 | ND | 1 | 126 | .5 | 2 | 4 | 32 | 4.05 | .192 | 6 | 1 | .39 | 67 | .06 | 2 | 1.02 | .02 | .20 | 6 | 20 | 80 |
| UR 1608N 1621E | 2 | 70 | 12 | 55 | .1 | 4 | 27 | 556 | 5.69 | 47 | 5 | ND | 1 | 83 | .3 | 2 | 2 | 33 | 2.50 | .197 | 4 | 1 | .31 | 49 | .10 | 2 | .96 | .03 | .24 | 2 | 26 | 160 |
| STANDARD C/AU-R | 19 | 58 | 38 | 129 | 7.3 | 70 | 31 | 1052 | 3.97 | 40 | 19 | 7 | 38 | 53 | 18.6 | 15 | 21 | 55 | .52 | .097 | 38 | 56 | .89 | 182 | .07 | 33 | 1.89 | .06 | .14 | 11 | 500 | 1600 |

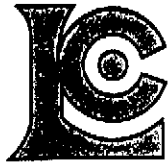
| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|----------------|-----|-----|-----|-----|------|-----|-----|------|------|------|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|-----|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| R 1150N 245W | 5 | 10 | 18 | 117 | 1.7 | 7 | 7 | 175 | 2.52 | 77 | 5 | ND | 1 | 10 | .4 | 6 | 4 | 7 | .33 | .137 | 11 | 5 | .07 | 39 | .01 | 6 | .45 | .01 | .22 | 1 | 21 | 320 |
| R 1150N 130W | 7 | 6 | 178 | 13 | 9.4 | 10 | 2 | 57 | 3.84 | 208 | 5 | ND | 1 | 3 | .5 | 13 | 4 | 1 | .01 | .006 | 6 | 17 | .01 | 19 | .01 | 2 | .19 | .01 | .17 | 1 | 138 | 430 |
| R 1125N 125W | 6 | 30 | 124 | 325 | 71.8 | 16 | 2 | 119 | 4.43 | 7855 | 5 | 3 | 1 | 3 | 1.5 | 148 | 3 | 1 | .04 | .013 | 5 | 3 | .07 | 27 | .01 | 2 | .21 | .01 | .11 | 1 | 1978 | 760 |
| R 940N 440W | 6 | 5 | 14 | 22 | .3 | 6 | 1 | 79 | .96 | 18 | 5 | ND | 2 | 5 | .2 | 2 | 5 | 1 | .01 | .009 | 19 | 30 | .01 | 88 | .01 | 2 | .20 | .04 | .10 | 1 | 8 | 60 |
| R 900N 390W | 8 | 6 | 13 | 34 | 1.0 | 9 | 1 | 119 | 1.34 | 68 | 5 | ND | 4 | 6 | .2 | 2 | 4 | 1 | .01 | .012 | 30 | 3 | .02 | 133 | .01 | 3 | .27 | .02 | .15 | 1 | 20 | 90 |
| R 900N 290W | 1 | 127 | 2 | 75 | .1 | 18 | 23 | 1012 | 7.14 | 2 | 5 | ND | 1 | 147 | 1.1 | 3 | 2 | 126 | 3.63 | .236 | 9 | 33 | 1.34 | 53 | .04 | 6 | 1.73 | .02 | .19 | 1 | 6 | 20 |
| R 895N 623W | 2 | 25 | 2 | 77 | .1 | 16 | 10 | 355 | 3.19 | 3 | 5 | ND | 3 | 36 | 1.1 | 2 | 4 | 29 | 1.09 | .092 | 26 | 20 | 1.50 | 103 | .01 | 2 | 1.83 | .03 | .18 | 1 | 5 | 40 |
| UR 2775N 1805E | 1 | 59 | 3 | 69 | .1 | 12 | 12 | 116 | 4.46 | 7 | 5 | ND | 1 | 79 | .2 | 2 | 4 | 12 | .62 | .118 | 3 | 9 | .04 | 18 | .01 | 8 | .40 | .02 | .19 | 1 | 11 | 570 |
| UR 2700N 2335E | 1 | 86 | 8 | 75 | 1.3 | 17 | 9 | 129 | 3.59 | 41 | 5 | ND | 1 | 31 | 1.2 | 6 | 2 | 53 | .31 | .129 | 10 | 20 | 1.33 | 92 | .01 | 2 | 1.68 | .01 | .20 | 1 | 23 | 110 |

✓ ASSAY RECOMMENDED

APPENDIX B

Rock Samples Submitted for Whole Rock Analysis
Descriptions and Certificates of Analysis

| Sample Number | Location | Description |
|---------------|-------------------------------------|-------------------------------------|
| WR 2 | 1390 N/200 W | Flowbanded rhyolite |
| WR 3 | 1380 N/330 W | Felsic dike |
| WR 4 | 1205 N/340 W | Felsic dike |
| WR 5 | 1420 N/230 W | Felsic dike |
| WR 6 | 1330 N/280 W | Welded ash flow tuff |
| WR 7 | 1419 N/297 W | Coarse pyroclastic flow |
| WR 8 | 1440 N/265 W | Coarse pyroclastic flow |
| WR 11 | 965 N/423 W Zone 1 grid | Dacite tuff, 5-10% pumice fragments |
| WR 12 | 975 N/135 W Zone 1 grid | Intermediate to felsic dike |
| WR 14 | 1725 N/880 W | Foliated coarse felsic pyroclastic |
| WR 15 | 925 N/370 W | "Andesitic" dike in sediments |
| WR 16 | 620 N/960 E | Basaltic andesite flow/flow breccia |
| WR 17 | DDH AP-1 at 75.5 m | Diabase dike |
| WR 18 | 1650 N/525 W | Diabase dike |
| WR 19 | 930 N/850 W | Rhyolite |
| WR 20 | 1770 N/600 W | Altered diabase |
| WR 21 | 1500 N/850 W | Altered diabase |
| WR 22 | 1500 N/800 W | Altered diabase |
| WR 23 | 1600 N/735 W | Altered diabase |
| WR 24 | 1685 N/645 W | Altered diabase |
| WR 25 | 1500 N/800 W | Diabase |
| WR 26 | 1710 N/600 W | Altered diabase |
| WR 27 | 1650 N/645 W | Diabase |
| WR 28 | 1200 N/285 W | Rhyolite autobreccia |
| WR 29 | 1000 N/200 W | Intermed <-> felsic dike |
| WR 30 | 1300 N/600 W | Mafic dike |
| WR 31 | 1380 N/540 W | Felsic dike |
| WR 34 | Unit 5e, ridge S.E. of A.P. zone | Granodiorite |
| WR 35 | 1680 N/570 E | Diabase dike |
| WR 36 | 1305 N/700 E | Andesitic dike |
| WR 37 | 1700 N/600 E | Diabase dike with epidote stringers |
| WR 40 | DDH AP-1 @ 53 m | Quartz-chlorite schist |
| WR 41 | DDH AP-1 @ 62 m | Andesite tuff breccia |
| WR 42 | DDH AP-1 @ 24 m | Dacitic ash tuff |
| WR 43 | DDH AP-4 @ 8.8 m | Ash flow (lenticular) tuff |
| WR 44 | DDH AP-4 @ 18.3 m | Debris flow (possibly "black tuff") |
| WR 45 | DDH AP-4 @ 26 m | Altered dacite |
| WR 55 | 990 N/295 W | Cherty, flowbanded rhyolite |
| WR 56 | 1452 N/206 W | Dacitic ash flow tuff |
| WR 57 | 975 N/135 E | Felsic dike |
| WR 59 | 1515 N/810 W | Diabase - green altered |
| WR 60 | 900 N/250 W | Diabase dike/stock |
| WR 61 | 1170 N/875 W | |
| WR 62 | 1250 N/850 W | |
| WR 63 | 1250 N/850 E | |
| WR 64 | 1250 N/875 W | |
| WR 65 | 1200 N/100 W | |
| WR 66 | 1250 N/700 W | |
| WR 67 | 1690 N/625 W | |



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To: GRANGES EXPLORATION LTD.

885 W. GEORGIA ST., 23RD FLOOR
VANCOUVER, BC
V6C 3E8

Page Number : 1
Total Pages : 2
Invoice Date : 2-AUG-90
Invoice No. : I-9019205
P.O. Number :

Project : UNUK R #134
Comments : ATTN: F. FELDER CC: B. GABOURY

CERTIFICATE OF ANALYSIS A9019205

| SAMPLE DESCRIPTION | PREP CODE | Al2O3 % | BaO % | CaO % | Fe2O3 % | K2O % | MgO % | MnO % | Na2O % | P2O5 % | SiO2 % | TiO2 % | LOI % | TOTAL % |
|--------------------|-----------|---------|-------|--------|---------|-------|-------|--------|--------|--------|--------|--------|-------|---------|
| WR-01 | 208 294 | 14.50 | 0.15 | 6.38 | 10.71 | 6.04 | 5.25 | 0.16 | 1.83 | 0.58 | 49.94 | 0.74 | 2.06 | 98.34 |
| WR-02 | 208 294 | 11.19 | 0.22 | 0.16 | 1.34 | 6.10 | 0.40 | 0.03 | 0.29 | < 0.01 | 78.85 | 0.16 | 1.54 | 100.30 |
| WR-03 | 208 294 | 14.26 | 0.02 | 6.53 | 10.33 | 2.25 | 4.60 | 0.23 | 2.48 | 0.33 | 43.87 | 1.40 | 11.90 | 98.20 |
| WR-04 | 208 294 | 14.05 | 0.09 | 3.28 | 11.15 | 3.86 | 3.45 | 0.13 | 2.04 | 0.40 | 52.94 | 1.44 | 6.40 | 99.23 |
| WR-05 | 208 294 | 8.77 | 0.01 | < 0.01 | 1.39 | 0.75 | 0.24 | 0.04 | 3.95 | < 0.01 | 84.61 | 0.14 | 0.93 | 100.85 |
| WR-06 | 208 294 | 13.62 | 0.14 | 0.43 | 4.40 | 4.87 | 0.47 | 0.12 | 3.86 | < 0.01 | 68.85 | 0.33 | 2.21 | 99.31 |
| WR-07 | 208 294 | 10.72 | 0.13 | 8.84 | 12.08 | 2.88 | 4.35 | 0.35 | 1.60 | 0.39 | 42.26 | 0.96 | 14.50 | 99.06 |
| WR-08 | 208 294 | 15.47 | 0.17 | 1.49 | 8.10 | 4.64 | 1.46 | 0.11 | 1.98 | 0.37 | 57.29 | 1.29 | 5.29 | 97.66 |
| WR-09 | 208 294 | 11.29 | 0.25 | < 0.01 | 0.79 | 7.91 | 0.16 | < 0.01 | 0.39 | 0.02 | 79.09 | 0.24 | 0.75 | 100.90 |
| WR-10 | 208 294 | 15.24 | 0.06 | 3.97 | 7.71 | 1.94 | 2.80 | 0.05 | 5.40 | 0.51 | 54.32 | 0.98 | 7.81 | 100.80 |
| WR-11 | 208 294 | 11.78 | 0.02 | 3.19 | 9.72 | 1.57 | 1.47 | 0.15 | 1.63 | 0.35 | 61.77 | 1.49 | 4.83 | 97.97 |
| WR-12 | 208 294 | 15.56 | 0.17 | 5.35 | 11.18 | 2.70 | 2.45 | 0.18 | 3.43 | 0.65 | 54.94 | 2.00 | 2.16 | 100.75 |
| WR-13 | 208 294 | 13.11 | 0.04 | 9.02 | 9.50 | 1.77 | 4.62 | 0.15 | 2.98 | 0.33 | 41.17 | 0.89 | 13.03 | 96.61 |
| WR-14 | 208 294 | 11.88 | 0.14 | 1.22 | 4.24 | 3.50 | 1.04 | 0.03 | 1.35 | 0.04 | 72.71 | 0.13 | 3.02 | 99.30 |
| WR-15 | 208 294 | 14.25 | 0.23 | < 0.01 | 5.66 | 7.77 | 0.91 | 0.06 | 0.87 | 0.06 | 67.62 | 0.55 | 1.52 | 99.51 |
| WR-16 | 208 294 | 13.56 | 0.11 | 8.41 | 8.82 | 5.08 | 6.72 | 0.01 | 2.03 | 0.61 | 49.19 | 0.91 | 2.10 | 97.56 |
| WR-17 | 208 294 | 14.44 | 0.16 | 5.81 | 11.22 | 3.06 | 3.06 | 0.21 | 2.92 | 0.65 | 54.71 | 2.00 | 2.13 | 100.35 |
| WR-18 | 208 294 | 14.31 | 0.18 | 4.43 | 10.68 | 2.90 | 2.15 | 0.20 | 3.04 | 0.63 | 55.52 | 1.82 | 2.42 | 98.28 |
| WR-19 | 208 294 | 14.34 | 0.16 | < 0.01 | 4.60 | 5.11 | 0.55 | 0.03 | 2.14 | 0.07 | 68.26 | 0.46 | 2.68 | 98.41 |
| WR-20 | 208 294 | 14.60 | 0.18 | 4.86 | 9.95 | 2.78 | 2.34 | 0.19 | 3.11 | 0.43 | 55.42 | 1.42 | 2.55 | 97.84 |
| WR-21 | 208 294 | 13.65 | 0.26 | 0.62 | 3.81 | 3.28 | 0.51 | 0.06 | 3.51 | < 0.01 | 70.66 | 0.34 | 2.84 | 99.55 |
| WR-22 | 208 294 | 14.73 | 0.12 | 2.83 | 9.12 | 1.70 | 2.38 | 0.12 | 4.82 | 0.56 | 57.58 | 1.39 | 3.76 | 99.13 |
| WR-23 | 208 294 | 14.63 | 0.18 | 4.07 | 10.17 | 2.83 | 2.56 | 0.16 | 3.30 | 0.48 | 56.54 | 1.27 | 3.48 | 99.67 |
| WR-24 | 208 294 | 13.52 | 0.17 | 4.77 | 8.04 | 3.35 | 2.38 | 0.17 | 3.02 | 0.40 | 56.59 | 1.02 | 5.65 | 99.07 |
| WR-25 | 208 294 | 14.20 | 0.20 | 5.15 | 10.72 | 2.81 | 2.22 | 0.20 | 3.17 | 0.50 | 54.86 | 1.36 | 4.29 | 99.67 |
| WR-26 | 208 294 | 16.68 | 0.15 | 3.86 | 7.21 | 1.99 | 3.02 | 0.13 | 6.02 | 0.64 | 53.81 | 1.58 | 4.66 | 99.74 |
| WR-27 | 208 294 | 15.48 | 0.23 | 2.97 | 10.06 | 3.05 | 1.58 | 0.19 | 4.24 | 0.58 | 57.17 | 1.50 | 2.14 | 99.20 |
| WR-28 | 208 294 | 14.44 | 0.28 | 2.61 | 8.16 | 4.50 | 1.82 | 0.14 | 1.97 | 0.42 | 60.26 | 1.06 | 3.94 | 99.59 |
| WR-29 | 208 294 | 11.90 | 0.12 | 0.29 | 1.86 | 6.82 | 0.41 | 0.03 | 1.34 | < 0.01 | 75.14 | 0.16 | 0.90 | 98.97 |
| WR-30 | 208 294 | 14.33 | 0.22 | 4.94 | 11.24 | 2.39 | 2.65 | 0.19 | 3.20 | 0.61 | 53.06 | 1.50 | 4.98 | 99.30 |
| WR-31 | 208 294 | 15.42 | 0.15 | 2.12 | 8.90 | 3.09 | 1.93 | 0.09 | 4.09 | 0.89 | 57.00 | 2.23 | 3.31 | 99.23 |
| WR-32 | 208 294 | 16.72 | 0.29 | 3.54 | 5.35 | 3.10 | 2.59 | 0.21 | 4.59 | 0.45 | 58.78 | 0.84 | 2.27 | 98.74 |
| WR-33 | 208 294 | 16.56 | 0.77 | 4.94 | 7.75 | 3.14 | 3.56 | 0.18 | 3.32 | 0.48 | 51.70 | 0.82 | 5.08 | 98.29 |
| WR-34 | 208 294 | 12.11 | 0.12 | 10.46 | 10.34 | 2.54 | 10.31 | 0.18 | 2.33 | 0.62 | 44.78 | 1.08 | 2.93 | 97.78 |
| WR-35 | 208 294 | 13.65 | 0.13 | 4.78 | 13.33 | 1.28 | 2.63 | 0.22 | 3.95 | 0.56 | 55.00 | 2.66 | 1.40 | 99.57 |
| WR-36 | 208 294 | 13.97 | 0.13 | 2.75 | 13.48 | 2.51 | 2.33 | 0.15 | 2.77 | 0.55 | 49.38 | 2.43 | 8.55 | 98.99 |
| WR-37 | 208 294 | 12.42 | 0.08 | 5.37 | 12.14 | 0.26 | 2.59 | 0.17 | 4.60 | 0.43 | 54.94 | 2.46 | 3.56 | 99.02 |
| WR-40 | 208 294 | 10.93 | 0.24 | 2.34 | 2.87 | 3.66 | 0.38 | 0.08 | 2.48 | 0.17 | 72.62 | 0.23 | 3.04 | 99.04 |
| WR-41 | 208 294 | 13.98 | 0.17 | 3.80 | 7.81 | 4.04 | 1.51 | 0.18 | 2.00 | 0.54 | 59.50 | 1.90 | 4.69 | 100.10 |
| WR-42 | 208 294 | 11.30 | 0.19 | 1.68 | 5.06 | 4.23 | 0.73 | 0.10 | 1.36 | 0.15 | 70.19 | 0.36 | 3.77 | 99.13 |

CERTIFICATION:

B. Gough



Chemex Labs Ltd.

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To: GRANGES EXPLORATION LTD.

885 W. GEORGIA ST., 23RD FLOOR
VANCOUVER, BC
V6C 3E8

Page Number : 2
Total Pages : 2
Invoice Date: 2-AUG-90
Invoice No. : I-9019205
P.O. Number :

Project : UNUK R #134

Comments: ATTN: F. FELDER CC: B. GABOURY

CERTIFICATE OF ANALYSIS

A9019205

| SAMPLE DESCRIPTION | PREP CODE | Al2O3 % | BaO % | CaO % | Fe2O3 % | K2O % | MgO % | MnO % | Na2O % | P2O5 % | SiO2 % | TiO2 % | LOI % | TOTAL % |
|--------------------|-----------|---------|-------|-------|---------|-------|-------|--------|--------|--------|--------|--------|-------|---------|
| WR-43 | 208 294 | 13.51 | 0.24 | 0.31 | 3.15 | 7.63 | 0.66 | 0.03 | 0.22 | 0.08 | 70.58 | 0.44 | 2.65 | 99.48 |
| WR-44 | 208 294 | 14.47 | 0.15 | 1.53 | 2.82 | 4.93 | 1.25 | 0.11 | 0.44 | 0.12 | 67.67 | 0.49 | 5.41 | 99.39 |
| WR-45 | 208 294 | 11.88 | 0.02 | 1.31 | 1.42 | 3.11 | 1.26 | 0.09 | 0.78 | 0.05 | 74.92 | 0.13 | 4.16 | 99.14 |
| WR-46 | 208 294 | 11.38 | 0.04 | 0.19 | 1.82 | 3.34 | 0.52 | < 0.01 | 0.03 | 0.02 | 76.79 | 0.23 | 3.23 | 97.59 |

CERTIFICATION:

B. Coghlin



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Page Number: 1
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Invoice Date: 15-AUG-90
Invoice No.: I-9020247
P.O. Number:

Project: UNUK R.PROJECT 134
Comments: ATTN:FRED FELDER CC:B.GABOURY

CERTIFICATE OF ANALYSIS A9020247

| SAMPLE DESCRIPTION | PREP CODE | Al2O3 % | BaO % | CaO % | Fe2O3 % | K2O % | MgO % | MnO % | Na2O % | P2O5 % | SiO2 % | TiO2 % | LOI % | TOTAL % |
|--------------------|-----------|---------|-------|-------|---------|-------|-------|-------|--------|--------|--------|--------|-------|---------|
| WR 38 | 205 294 | 18.07 | 0.17 | 5.14 | 8.85 | 1.05 | 4.41 | 0.30 | 5.77 | 0.47 | 50.75 | 1.17 | 3.38 | 99.53 |
| WR 39 | 205 294 | 10.13 | 0.26 | 0.53 | 3.29 | 5.86 | 0.28 | 0.01 | 0.20 | 0.17 | 74.96 | 0.38 | 2.32 | 98.38 |
| WR 59 | 205 294 | 16.40 | 0.18 | 2.29 | 10.06 | 2.27 | 3.68 | 0.10 | 4.73 | 0.69 | 53.86 | 1.53 | 3.63 | 99.44 |
| WR 60 | 205 294 | 12.91 | 0.08 | 5.58 | 12.74 | 1.90 | 3.12 | 0.15 | 1.82 | 0.35 | 51.10 | 1.71 | 6.78 | 98.23 |
| WR 61 | 205 294 | 15.03 | 0.21 | 4.48 | 10.67 | 2.92 | 2.49 | 0.21 | 3.38 | 0.63 | 54.82 | 1.45 | 3.17 | 99.47 |
| | | | | | | | | | | | | | | |

CERTIFICATION:



Chemex Labs Ltd.

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Page Number: 1
Total Pages: 1
Invoice Date: 11-JUL-90
Invoice No.: I-9018120
P.O. Number:

Project: UNUK (GS134)
Comments: ATTN: F. FELDER CC: J. HARDY

CERTIFICATE OF ANALYSIS A9018120

| SAMPLE DESCRIPTION | PREP CODE | Al2O3 % | BaO % | CaO % | Fe2O3 % | K2O % | MgO % | MnO % | Na2O % | P2O5 % | SiO2 % | TiO2 % | LOI % | TOTAL % |
|---|-----------|---------|-------|-------|---------|-------|-------|-------|--------|--------|--------|--------|-------|---------|
| WRG WRB WRB WRB WRB L11+70N 8+75W | 208 294 | 13.63 | 0.16 | 5.92 | 8.31 | 3.26 | 2.10 | 0.19 | 2.56 | 0.54 | 54.24 | 1.38 | 8.27 | 100.55 |
| WRB WRB WRB WRB WRB L12+50N 8+50W | 208 294 | 15.04 | 0.18 | 5.01 | 9.68 | 7.25 | 2.56 | 0.34 | 0.37 | 0.41 | 47.93 | 1.12 | 11.00 | 100.90 |
| WRB WRB WRB WRB WRB L12+50N 8+50N GR | 208 294 | 8.95 | 0.12 | 0.11 | 14.33 | 3.66 | 0.31 | 0.01 | 0.12 | 0.24 | 64.47 | 0.61 | 7.93 | 100.85 |
| WRB WRB WRB WRB WRB L12+50N 8+75W | 208 294 | 13.59 | 0.23 | 0.14 | 4.84 | 9.19 | 0.15 | 0.04 | 0.16 | 0.24 | 67.41 | 1.43 | 3.00 | 100.40 |
| WRB WRB WRB WRB WRB L12+00W 1+00W | 208 294 | 19.36 | 0.08 | 0.74 | 3.68 | 4.57 | 1.78 | 0.05 | 1.30 | 0.29 | 64.34 | 0.60 | 4.10 | 100.90 |
| WRB WRB WRB WRB WRB L1250N700WZ08K1 | 208 294 | 13.73 | 0.17 | 2.68 | 10.46 | 6.99 | 2.09 | 0.56 | 0.44 | 0.52 | 51.73 | 1.56 | 8.53 | 99.46 |
| WRB WRB WRB WRB WRB R1690N625W GRID1 | 208 294 | 14.86 | 0.24 | 5.66 | 9.86 | 2.73 | 1.39 | 0.20 | 3.69 | 0.76 | 56.14 | 1.54 | 3.92 | 100.95 |
| WRB WRB WRB WRB WRB R DYKE# GRID1 | 208 294 | 13.33 | 0.26 | 0.08 | 1.39 | 9.56 | 0.08 | 0.01 | 0.23 | 0.14 | 74.26 | 0.23 | 1.04 | 100.60 |
| WRB WRB WRB WRB WRB CR 580E 255W | 208 294 | 13.44 | 0.16 | 3.18 | 11.13 | 4.57 | 1.50 | 0.85 | 2.00 | 0.48 | 53.91 | 1.51 | 8.00 | 100.75 |

CERTIFICATION:

P. 02

GRANGES INC. UNUK

08:29

09/11/90

APPENDIX C

Core Sample Assay Certificates

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT 134 File # 90-3975 Page 1

2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

HP 6

Table with columns for SAMPLE#, Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K, Au**, Hg. Rows include sample IDs like 1087 G, 1088 G, etc., and a STANDARD C/AU-R row at the bottom.

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-11 CORE P12-13 ROCK P14-18 SOIL AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: AUG 28 1990 DATE REPORT MAILED: Sept 7/90. SIGNED BY: [Signature] D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. File # 90-3620
2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | V ppm | Au** ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|
| 1101-G | 1 | 19 | 34 | 99 | 3.2 | 10 | 20 | 1412 | 16.34 | 28 | 5 | ND | 1 | 78 | .9 | 2 | 2 | 11 | 3.04 | .101 | 6 | 4 | .23 | 29 | .01 | 2 | .79 | .01 | .23 | 1 | 8 |
| 1102-G | 1 | 21 | 60 | 108 | 1.4 | 18 | 25 | 1067 | 15.78 | 52 | 6 | ND | 2 | 81 | 1.1 | 7 | 2 | 17 | 3.50 | .071 | 3 | 6 | .41 | 29 | .01 | 2 | .99 | .01 | .19 | 1 | 11 |
| 1103-G | 1 | 26 | 24 | 161 | .7 | 20 | 17 | 706 | 7.87 | 19 | 5 | ND | 1 | 75 | .3 | 4 | 2 | 34 | 2.05 | .070 | 4 | 21 | .63 | 53 | .01 | 3 | 1.58 | .01 | .22 | 1 | 6 |
| 1104-G | 1 | 28 | 41 | 45 | 1.2 | 11 | 23 | 822 | 16.35 | 23 | 5 | ND | 1 | 67 | .6 | 2 | 2 | 20 | 2.33 | .079 | 3 | 5 | .44 | 28 | .01 | 2 | 1.12 | .01 | .20 | 1 | 9 |
| 1105-G | 4 | 32 | 27 | 127 | .3 | 21 | 11 | 706 | 6.20 | 5 | 5 | ND | 1 | 123 | .7 | 3 | 2 | 25 | 3.43 | .076 | 5 | 8 | .69 | 57 | .01 | 2 | 1.77 | .01 | .18 | 1 | 10 |
| 1106-G | 4 | 34 | 16 | 151 | .5 | 14 | 10 | 754 | 5.65 | 13 | 5 | ND | 2 | 116 | .6 | 2 | 2 | 21 | 3.25 | .059 | 5 | 9 | .73 | 64 | .01 | 2 | 1.81 | .01 | .17 | 1 | 8 |
| 1107-G | 5 | 32 | 54 | 171 | .4 | 17 | 14 | 630 | 8.75 | 112 | 5 | ND | 1 | 100 | 1.2 | 4 | 2 | 24 | 3.49 | .101 | 4 | 9 | .57 | 52 | .01 | 2 | 1.54 | .02 | .18 | 1 | 52 |
| 1108-G | 2 | 30 | 69 | 189 | .4 | 11 | 14 | 593 | 12.18 | 251 | 5 | ND | 1 | 89 | 1.7 | 6 | 2 | 17 | 2.99 | .123 | 4 | 5 | .44 | 31 | .01 | 2 | 1.22 | .01 | .17 | 1 | 94 |
| 1110-G | 1 | 16 | 69 | 171 | .4 | 59 | 26 | 1994 | 8.44 | 36 | 5 | ND | 1 | 89 | .7 | 2 | 2 | 144 | 3.76 | .075 | 5 | 123 | 2.03 | 47 | .01 | 2 | 3.89 | .02 | .12 | 1 | 2 |
| 1111-G | 1 | 25 | 47 | 141 | .6 | 65 | 38 | 1848 | 10.83 | 40 | 5 | ND | 1 | 106 | .9 | 2 | 2 | 162 | 4.20 | .093 | 5 | 130 | 2.09 | 43 | .01 | 2 | 3.86 | .02 | .11 | 1 | 3 |
| R 1235N 162W | 1 | 10 | 4 | 146 | .3 | 11 | 9 | 2636 | 3.81 | 478 | 5 | ND | 3 | 32 | .2 | 4 | 2 | 9 | 2.88 | .084 | 19 | 4 | 1.45 | 58 | .01 | 3 | .64 | .01 | .28 | 1 | 18 |
| R 1235N 152W | 1 | 7 | 11 | 53 | .4 | 4 | 2 | 2636 | 2.47 | 6 | 5 | ND | 3 | 76 | .2 | 4 | 2 | 6 | 5.36 | .010 | 13 | 3 | 2.54 | 59 | .01 | 2 | .26 | .01 | .10 | 1 | 1 |
| R 1235N 151W | 1 | 2 | 2 | 33 | .5 | 4 | 2 | 7263 | 4.45 | 5 | 5 | ND | 1 | 185 | .4 | 2 | 2 | 4 | 13.51 | .029 | 4 | 2 | 4.56 | 60 | .01 | 3 | .25 | .01 | .10 | 1 | 1 |
| R 1230N 150W | 7 | 3 | 80 | 247 | .7 | 3 | 1 | 729 | 2.44 | 132 | 5 | ND | 1 | 11 | .2 | 2 | 2 | 1 | .70 | .009 | 13 | 3 | .23 | 90 | .01 | 3 | .40 | .01 | .22 | 1 | 47 |
| STANDARD C/AU-R | 18 | 61 | 39 | 132 | 7.1 | 73 | 31 | 1045 | 3.95 | 42 | 15 | 7 | 38 | 53 | 18.6 | 15 | 17 | 57 | .51 | .094 | 39 | 60 | .89 | 182 | .09 | 35 | 1.89 | .06 | .14 | 13 | 512 |

FP6

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
- SAMPLE TYPE: Core/Rock AU** ANALYSIS BY FA/ICP FROM 30 GM SAMPLE.

DATE RECEIVED: AUG 18 1990 DATE REPORT MAILED: Aug 21/90. SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Tl | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| 1133 G | 2 | 19 | 3 | 152 | .6 | 9 | 17 | 2282 | 6.39 | 9 | 8 | ND | 1 | 97 | 1.0 | 2 | 2 | 31 | 5.33 | .117 | 10 | 7 | .92 | 61 | .01 | 2 | 2.51 | .01 | .25 | 2 | 4 | 30 |
| 1134 G | 1 | 14 | 5 | 142 | .3 | 7 | 16 | 2153 | 6.02 | 13 | 5 | ND | 1 | 77 | 1.2 | 2 | 2 | 29 | 4.46 | .123 | 9 | 4 | .86 | 74 | .01 | 6 | 2.40 | .01 | .26 | 1 | 12 | 20 |
| 1135 G | 5 | 15 | 15 | 149 | .7 | 7 | 16 | 2049 | 6.73 | 12 | 5 | ND | 1 | 71 | 1.2 | 2 | 7 | 29 | 4.13 | .136 | 10 | 5 | .88 | 84 | .01 | 6 | 2.45 | .01 | .28 | 1 | 6 | 20 |
| 1136 G | 2 | 18 | 12 | 163 | .8 | 8 | 17 | 1715 | 6.70 | 3 | 5 | ND | 1 | 77 | .8 | 2 | 2 | 27 | 4.07 | .127 | 10 | 6 | .79 | 60 | .01 | 2 | 2.19 | .01 | .22 | 1 | 4 | 20 |
| 1137 G | 1 | 17 | 23 | 139 | 1.0 | 10 | 20 | 2528 | 7.12 | 15 | 5 | ND | 1 | 132 | 1.0 | 2 | 4 | 29 | 5.96 | .134 | 9 | 7 | .83 | 53 | .01 | 3 | 2.27 | .01 | .23 | 1 | 6 | 30 |
| 1138 G | 1 | 18 | 12 | 145 | .7 | 9 | 19 | 1903 | 7.55 | 9 | 5 | ND | 1 | 80 | 1.1 | 2 | 9 | 31 | 4.09 | .138 | 8 | 6 | .91 | 54 | .01 | 6 | 2.37 | .01 | .24 | 1 | 8 | 20 |
| 1139 G | 1 | 16 | 8 | 143 | .8 | 8 | 19 | 1985 | 7.24 | 7 | 5 | ND | 1 | 88 | 1.2 | 2 | 6 | 29 | 4.28 | .135 | 8 | 6 | .92 | 48 | .01 | 4 | 2.26 | .01 | .22 | 1 | 5 | 20 |
| 1140 G | 1 | 16 | 2 | 139 | .4 | 7 | 15 | 2044 | 4.76 | 3 | 5 | ND | 1 | 95 | .5 | 2 | 2 | 27 | 4.37 | .139 | 10 | 5 | .88 | 51 | .01 | 7 | 2.13 | .01 | .26 | 1 | 6 | 30 |
| 1141 G | 1 | 15 | 8 | 65 | 1.4 | 6 | 16 | 1568 | 5.37 | 4 | 5 | ND | 1 | 106 | .6 | 2 | 3 | 21 | 4.88 | .125 | 7 | 6 | .51 | 56 | .01 | 5 | 1.45 | .01 | .26 | 1 | 4 | 40 |
| 1142 G | 1 | 20 | 12 | 142 | 1.4 | 3 | 23 | 1664 | 9.69 | 5 | 5 | ND | 1 | 87 | 1.6 | 2 | 6 | 76 | 3.81 | .138 | 6 | 2 | 1.38 | 37 | .01 | 2 | 3.19 | .01 | .14 | 2 | 9 | 50 |
| 1143 G | 2 | 17 | 11 | 127 | .9 | 10 | 17 | 1586 | 6.21 | 15 | 9 | ND | 1 | 107 | .6 | 4 | 3 | 30 | 4.87 | .125 | 8 | 7 | .85 | 52 | .01 | 2 | 2.33 | .01 | .21 | 1 | 5 | 20 |
| 1144 G | 2 | 16 | 8 | 152 | .3 | 6 | 16 | 1596 | 6.37 | 7 | 5 | ND | 1 | 93 | 1.2 | 2 | 2 | 38 | 4.30 | .136 | 10 | 8 | 1.08 | 49 | .01 | 2 | 2.90 | .01 | .20 | 1 | 1 | 30 |
| 1145 G | 1 | 20 | 17 | 159 | .7 | 8 | 25 | 1400 | 7.65 | 15 | 5 | ND | 1 | 79 | 1.6 | 2 | 2 | 39 | 3.69 | .153 | 9 | 9 | 1.11 | 75 | .01 | 7 | 3.08 | .01 | .23 | 1 | 9 | 20 |
| 1146 G | 1 | 21 | 2 | 151 | .5 | 9 | 17 | 1539 | 6.21 | 8 | 5 | ND | 1 | 108 | 1.3 | 2 | 2 | 36 | 4.79 | .137 | 10 | 8 | 1.01 | 51 | .01 | 2 | 2.81 | .01 | .21 | 1 | 1 | 20 |
| 1147 G | 1 | 18 | 32 | 134 | .7 | 8 | 18 | 1355 | 8.43 | 38 | 5 | ND | 1 | 103 | .9 | 2 | 2 | 37 | 4.30 | .137 | 8 | 8 | 1.01 | 52 | .01 | 2 | 2.83 | .01 | .20 | 1 | 2 | 10 |
| 1148 G | 1 | 21 | 17 | 143 | .6 | 7 | 21 | 1237 | 7.11 | 11 | 5 | ND | 1 | 93 | 1.8 | 3 | 2 | 41 | 3.77 | .137 | 9 | 8 | 1.08 | 51 | .01 | 3 | 3.01 | .01 | .19 | 1 | 8 | 10 |
| 1149 G | 1 | 21 | 2 | 158 | .4 | 8 | 17 | 1198 | 7.12 | 7 | 5 | ND | 1 | 101 | .8 | 2 | 2 | 43 | 3.92 | .137 | 10 | 9 | 1.12 | 52 | .01 | 4 | 3.17 | .01 | .19 | 1 | 12 | 20 |
| 1150 G | 1 | 25 | 2 | 155 | .4 | 9 | 18 | 1208 | 6.59 | 11 | 5 | ND | 1 | 107 | 1.1 | 2 | 2 | 42 | 4.05 | .150 | 12 | 10 | 1.06 | 52 | .01 | 3 | 3.06 | .01 | .19 | 1 | 38 | 30 |
| 1151 G | 1 | 24 | 17 | 138 | .7 | 9 | 18 | 1017 | 7.29 | 31 | 7 | ND | 1 | 99 | 1.0 | 3 | 2 | 34 | 3.83 | .148 | 8 | 8 | .85 | 52 | .01 | 4 | 2.45 | .01 | .19 | 2 | 109 | 30 |
| 1152 G | 2 | 11 | 9 | 142 | .3 | 9 | 18 | 1219 | 7.02 | 17 | 5 | ND | 1 | 100 | 1.4 | 2 | 6 | 53 | 4.13 | .132 | 12 | 10 | 1.18 | 53 | .01 | 3 | 3.37 | .02 | .19 | 2 | 2 | 20 |
| 1153 G | 1 | 20 | 2 | 154 | .5 | 8 | 17 | 1267 | 6.79 | 15 | 5 | ND | 1 | 114 | 1.2 | 2 | 5 | 51 | 4.61 | .126 | 12 | 10 | 1.15 | 51 | .01 | 4 | 3.19 | .02 | .17 | 1 | 1 | 30 |
| 1154 G | 1 | 17 | 18 | 141 | .3 | 9 | 20 | 1242 | 7.55 | 34 | 5 | ND | 1 | 114 | 1.0 | 2 | 2 | 50 | 4.59 | .133 | 7 | 10 | 1.13 | 52 | .01 | 2 | 3.17 | .02 | .17 | 1 | 1 | 20 |
| 1155 G | 1 | 18 | 2 | 144 | .3 | 9 | 16 | 1296 | 6.49 | 16 | 5 | ND | 1 | 129 | 1.2 | 2 | 2 | 51 | 4.98 | .121 | 10 | 10 | 1.10 | 50 | .01 | 3 | 3.04 | .02 | .15 | 1 | 2 | 30 |
| 1156 G | 1 | 16 | 37 | 127 | 1.0 | 11 | 24 | 1134 | 9.87 | 109 | 5 | ND | 1 | 109 | 1.8 | 2 | 2 | 41 | 4.54 | .115 | 7 | 8 | .88 | 55 | .01 | 2 | 2.48 | .02 | .17 | 1 | 3 | 30 |
| 1157 G | 2 | 20 | 28 | 141 | .8 | 11 | 25 | 1177 | 8.35 | 64 | 5 | ND | 1 | 95 | .9 | 3 | 2 | 49 | 4.08 | .125 | 7 | 9 | 1.07 | 45 | .01 | 2 | 2.94 | .02 | .15 | 1 | 3 | 20 |
| 1158 G | 2 | 24 | 23 | 152 | .5 | 11 | 22 | 1239 | 7.26 | 24 | 5 | ND | 1 | 87 | 1.3 | 2 | 2 | 55 | 3.87 | .128 | 9 | 11 | 1.20 | 55 | .01 | 3 | 3.27 | .02 | .16 | 2 | 3 | 30 |
| 1159 G | 1 | 22 | 13 | 145 | .2 | 10 | 19 | 1282 | 7.05 | 19 | 5 | ND | 1 | 103 | 1.2 | 2 | 2 | 55 | 4.32 | .126 | 10 | 10 | 1.19 | 46 | .01 | 4 | 3.25 | .02 | .14 | 2 | 8 | 20 |
| 1160 G | 2 | 20 | 5 | 141 | .4 | 12 | 18 | 1269 | 6.91 | 20 | 5 | ND | 1 | 105 | 1.4 | 2 | 2 | 57 | 4.33 | .123 | 11 | 13 | 1.16 | 68 | .01 | 2 | 3.28 | .02 | .17 | 2 | 3 | 30 |
| 1161 G | 1 | 18 | 4 | 143 | .4 | 8 | 18 | 1259 | 6.99 | 23 | 5 | ND | 1 | 103 | 1.5 | 2 | 2 | 56 | 4.21 | .131 | 11 | 11 | 1.18 | 53 | .01 | 2 | 3.31 | .02 | .17 | 1 | 2 | 20 |
| 1162 G | 2 | 31 | 10 | 129 | .2 | 12 | 19 | 1237 | 7.29 | 22 | 5 | ND | 1 | 91 | 1.0 | 2 | 2 | 59 | 3.91 | .127 | 13 | 11 | 1.26 | 59 | .01 | 2 | 3.48 | .02 | .18 | 1 | 1 | 10 |
| 1163 G | 2 | 23 | 20 | 118 | .6 | 17 | 22 | 1099 | 7.47 | 42 | 5 | ND | 1 | 100 | .7 | 3 | 2 | 49 | 4.23 | .105 | 6 | 18 | 1.05 | 66 | .01 | 3 | 2.89 | .02 | .19 | 3 | 5 | 20 |
| 1164 G | 2 | 24 | 2 | 116 | .3 | 19 | 20 | 1226 | 6.77 | 22 | 5 | ND | 1 | 100 | .9 | 2 | 2 | 60 | 4.36 | .107 | 9 | 22 | 1.27 | 66 | .01 | 2 | 3.37 | .02 | .19 | 1 | 15 | 20 |
| 1165 G | 1 | 15 | 2 | 68 | .1 | 14 | 14 | 868 | 4.51 | 13 | 5 | ND | 1 | 70 | .2 | 2 | 2 | 39 | 3.20 | .065 | 8 | 9 | .86 | 60 | .01 | 3 | 2.33 | .01 | .18 | 1 | 1 | 10 |
| 1166 G | 2 | 22 | 4 | 111 | .2 | 19 | 20 | 1174 | 6.46 | 18 | 5 | ND | 1 | 87 | .3 | 2 | 2 | 54 | 3.80 | .094 | 9 | 22 | 1.23 | 61 | .01 | 2 | 3.17 | .01 | .18 | 1 | 4 | 20 |
| 1167 G | 1 | 38 | 2 | 163 | .4 | 22 | 22 | 1337 | 6.43 | 18 | 5 | ND | 1 | 120 | 1.8 | 2 | 2 | 55 | 4.57 | .090 | 7 | 24 | 1.23 | 52 | .01 | 2 | 3.10 | .01 | .14 | 2 | 7 | 30 |
| 1168 G | 2 | 40 | 44 | 29 | .8 | 16 | 16 | 510 | 6.81 | 42 | 5 | ND | 1 | 68 | .4 | 7 | 2 | 17 | 2.18 | .059 | 3 | 6 | .43 | 58 | .01 | 3 | 1.29 | .01 | .21 | 2 | 4 | 40 |
| STANDARD C/AU-R | 19 | 60 | 39 | 132 | 6.8 | 73 | 32 | 1054 | 3.97 | 41 | 20 | 7 | 36 | 53 | 19.0 | 16 | 20 | 56 | .52 | .097 | 37 | 57 | .90 | 181 | .07 | 37 | 1.89 | .06 | .14 | 11 | 488 | 1600 |

RP 6

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| 1169 G | 1 | 14 | 5 | 74 | .3 | 8 | 9 | 569 | 3.20 | 7 | 5 | ND | 1 | 47 | .4 | 2 | 2 | 18 | 1.64 | .031 | 6 | 5 | .62 | 106 | .01 | 5 | 1.58 | .01 | .15 | 1 | 3 | 20 |
| 1170 G | 1 | 32 | 2 | 152 | .2 | 9 | 14 | 978 | 4.54 | 7 | 5 | ND | 1 | 76 | .9 | 2 | 2 | 39 | 2.47 | .033 | 5 | 9 | .93 | 248 | .01 | 7 | 2.33 | .01 | .23 | 1 | 1 | 40 |
| 1171 G | 1 | 8 | 21 | 68 | .2 | 6 | 9 | 874 | 3.55 | 21 | 5 | ND | 1 | 112 | .2 | 2 | 3 | 14 | 3.34 | .025 | 4 | 6 | .47 | 68 | .01 | 4 | 1.15 | .02 | .21 | 1 | 2 | 60 |
| 1172 G | 1 | 9 | 12 | 101 | .1 | 7 | 5 | 754 | 2.65 | 3 | 5 | ND | 1 | 67 | .2 | 2 | 3 | 22 | 2.26 | .025 | 4 | 6 | .60 | 61 | .01 | 6 | 1.37 | .01 | .16 | 1 | 1 | 20 |
| 1173 G | 2 | 44 | 26 | 237 | .6 | 11 | 21 | 997 | 6.57 | 7 | 5 | ND | 1 | 66 | 1.0 | 2 | 2 | 46 | 2.64 | .115 | 9 | 10 | .97 | 77 | .01 | 5 | 2.48 | .02 | .21 | 1 | 2 | 40 |
| 1174 G | 3 | 50 | 29 | 331 | .5 | 14 | 21 | 1158 | 7.09 | 2 | 5 | ND | 1 | 71 | 1.3 | 2 | 3 | 44 | 3.09 | .110 | 9 | 11 | 1.02 | 115 | .01 | 5 | 2.50 | .02 | .18 | 1 | 1 | 60 |
| 1175 G | 3 | 55 | 11 | 379 | .6 | 7 | 25 | 1032 | 7.22 | 5 | 5 | ND | 1 | 68 | 1.5 | 2 | 2 | 38 | 2.78 | .116 | 8 | 5 | .80 | 66 | .01 | 4 | 2.05 | .02 | .17 | 1 | 2 | 80 |
| 1176 G | 2 | 42 | 8 | 211 | .2 | 12 | 25 | 1426 | 4.93 | 7 | 5 | ND | 1 | 101 | 1.2 | 2 | 2 | 34 | 4.66 | .104 | 8 | 8 | .90 | 78 | .01 | 6 | 2.19 | .02 | .18 | 1 | 12 | 50 |
| 1177 G | 2 | 26 | 9 | 144 | .5 | 11 | 11 | 1130 | 3.38 | 5 | 5 | ND | 2 | 110 | .5 | 2 | 2 | 32 | 4.37 | .093 | 9 | 11 | .82 | 85 | .01 | 6 | 1.84 | .02 | .17 | 1 | 3 | 40 |
| 1178 G | 2 | 17 | 28 | 111 | .9 | 34 | 31 | 461 | 6.85 | 17 | 5 | ND | 1 | 71 | .2 | 5 | 2 | 16 | 2.25 | .064 | 3 | 8 | .29 | 46 | .01 | 5 | .86 | .01 | .21 | 1 | 8 | 50 |
| 1179 G | 3 | 25 | 7 | 188 | .3 | 13 | 12 | 1007 | 3.86 | 6 | 8 | ND | 1 | 89 | 1.1 | 2 | 2 | 38 | 3.40 | .108 | 7 | 14 | .98 | 73 | .01 | 6 | 2.07 | .02 | .20 | 1 | 7 | 40 |
| 1180 G | 2 | 9 | 16 | 22 | .4 | 6 | 11 | 762 | 3.16 | 14 | 5 | ND | 1 | 116 | .2 | 5 | 2 | 9 | 3.44 | .012 | 3 | 5 | .26 | 68 | .01 | 6 | .70 | .02 | .21 | 1 | 1 | 40 |
| 1181 G | 1 | 17 | 3 | 75 | .1 | 6 | 6 | 1133 | 3.06 | 2 | 5 | ND | 1 | 129 | .4 | 2 | 4 | 22 | 3.62 | .093 | 10 | 7 | .92 | 79 | .01 | 7 | 1.87 | .02 | .23 | 1 | 1 | 50 |
| 1182 G | 2 | 28 | 2 | 68 | .2 | 9 | 8 | 884 | 4.10 | 4 | 5 | ND | 1 | 78 | .6 | 2 | 2 | 25 | 1.95 | .018 | 7 | 9 | .98 | 74 | .01 | 6 | 2.18 | .02 | .21 | 1 | 1 | 50 |
| 1183 G | 1 | 24 | 2 | 166 | .2 | 10 | 12 | 636 | 4.22 | 8 | 5 | ND | 1 | 58 | .2 | 2 | 2 | 23 | 1.35 | .027 | 4 | 7 | .82 | 60 | .01 | 7 | 1.95 | .01 | .19 | 2 | 1 | 40 |
| 1184 G | 2 | 37 | 4 | 136 | .5 | 13 | 13 | 615 | 4.80 | 11 | 5 | ND | 1 | 54 | .4 | 2 | 4 | 24 | 1.04 | .048 | 4 | 7 | .88 | 60 | .01 | 6 | 2.00 | .01 | .20 | 1 | 3 | 30 |
| 1185 G | 2 | 25 | 2 | 97 | .3 | 12 | 14 | 716 | 4.47 | 8 | 5 | ND | 1 | 62 | .6 | 2 | 2 | 27 | 1.65 | .056 | 6 | 8 | .96 | 120 | .01 | 8 | 2.20 | .01 | .19 | 1 | 2 | 20 |
| 1186 G | 1 | 23 | 2 | 92 | .1 | 11 | 9 | 707 | 4.02 | 6 | 5 | ND | 1 | 64 | .3 | 2 | 2 | 32 | 1.74 | .073 | 10 | 9 | .92 | 177 | .01 | 3 | 2.13 | .01 | .18 | 1 | 1 | 10 |
| 1187 G | 2 | 19 | 2 | 110 | .1 | 10 | 6 | 642 | 2.70 | 5 | 5 | ND | 1 | 65 | .5 | 2 | 2 | 17 | 1.70 | .022 | 7 | 6 | .65 | 69 | .01 | 5 | 1.54 | .01 | .20 | 1 | 1 | 20 |
| 1188 G | 2 | 21 | 28 | 50 | .5 | 7 | 21 | 916 | 8.65 | 19 | 5 | ND | 1 | 81 | .5 | 3 | 5 | 26 | 3.57 | .098 | 5 | 7 | .68 | 56 | .01 | 4 | 1.51 | .01 | .18 | 2 | 4 | 10 |
| 1189 G | 1 | 4 | 2 | 40 | .1 | 8 | 13 | 867 | 3.85 | 7 | 5 | ND | 1 | 54 | .2 | 3 | 2 | 18 | 2.65 | .029 | 3 | 5 | .84 | 70 | .01 | 5 | 1.54 | .01 | .13 | 1 | 4 | 5 |
| 1190 G | 1 | 7 | 10 | 22 | .2 | 7 | 16 | 803 | 4.01 | 11 | 5 | ND | 1 | 44 | .2 | 2 | 2 | 18 | 2.42 | .051 | 3 | 4 | .73 | 56 | .01 | 3 | 1.32 | .01 | .11 | 1 | 1 | 10 |
| 1191 G | 2 | 32 | 14 | 59 | .4 | 21 | 25 | 1069 | 6.84 | 7 | 5 | ND | 1 | 77 | .2 | 3 | 2 | 30 | 3.93 | .091 | 4 | 11 | .90 | 38 | .01 | 3 | 1.62 | .01 | .17 | 1 | 7 | 10 |
| 1192 G | 2 | 31 | 11 | 80 | .5 | 18 | 19 | 834 | 7.28 | 13 | 5 | ND | 1 | 63 | .8 | 3 | 2 | 28 | 3.63 | .062 | 4 | 16 | .74 | 40 | .01 | 5 | 1.34 | .01 | .15 | 2 | 3 | 20 |
| 1193 G | 2 | 26 | 16 | 47 | .2 | 17 | 19 | 566 | 5.97 | 12 | 5 | ND | 1 | 35 | .3 | 2 | 2 | 15 | 1.58 | .042 | 2 | 8 | .75 | 34 | .01 | 7 | 1.25 | .01 | .13 | 1 | 1 | 10 |
| 1194 G | 1 | 19 | 5 | 13 | .1 | 7 | 8 | 478 | 2.06 | 3 | 5 | ND | 1 | 42 | .3 | 2 | 2 | 15 | 1.64 | .028 | 3 | 4 | .46 | 39 | .01 | 5 | .95 | .01 | .11 | 1 | 3 | 5 |
| 1195 G | 2 | 91 | 6 | 110 | .3 | 17 | 16 | 481 | 5.02 | 10 | 5 | ND | 1 | 66 | .6 | 2 | 2 | 28 | 1.36 | .059 | 6 | 10 | .89 | 51 | .01 | 5 | 2.19 | .01 | .16 | 1 | 1 | 40 |
| 1196 G | 2 | 25 | 27 | 68 | .1 | 14 | 13 | 718 | 5.49 | 9 | 5 | ND | 1 | 93 | .5 | 2 | 2 | 31 | 3.49 | .077 | 4 | 12 | .87 | 58 | .01 | 6 | 2.06 | .02 | .17 | 1 | 9 | 60 |
| 1197 G | 2 | 32 | 15 | 73 | .4 | 12 | 10 | 612 | 4.01 | 2 | 5 | ND | 1 | 99 | .6 | 2 | 2 | 20 | 3.20 | .114 | 7 | 9 | .85 | 43 | .01 | 5 | 1.80 | .01 | .14 | 1 | 12 | 30 |
| 1198 G | 1 | 26 | 11 | 97 | .1 | 9 | 9 | 510 | 3.88 | 2 | 5 | ND | 1 | 79 | .3 | 2 | 2 | 19 | 2.58 | .067 | 6 | 7 | .76 | 37 | .01 | 5 | 1.79 | .01 | .12 | 1 | 15 | 50 |
| 1199 G | 2 | 35 | 2 | 111 | .1 | 11 | 8 | 472 | 3.70 | 4 | 5 | ND | 1 | 81 | .7 | 2 | 2 | 19 | 2.28 | .048 | 8 | 8 | .76 | 45 | .01 | 10 | 1.82 | .01 | .15 | 1 | 7 | 40 |
| 1200 G | 2 | 27 | 8 | 89 | .1 | 9 | 10 | 366 | 3.15 | 5 | 5 | ND | 1 | 83 | .2 | 2 | 2 | 16 | 2.00 | .067 | 5 | 6 | .57 | 45 | .01 | 4 | 1.37 | .01 | .15 | 1 | 6 | 30 |
| 1201 G | 2 | 32 | 31 | 73 | .4 | 20 | 20 | 209 | 9.32 | 18 | 5 | ND | 1 | 67 | .4 | 8 | 2 | 8 | 1.58 | .064 | 3 | 5 | .22 | 24 | .01 | 4 | .72 | .01 | .17 | 1 | 12 | 40 |
| 1202 G | 2 | 40 | 6 | 115 | .1 | 11 | 13 | 373 | 3.40 | 3 | 5 | ND | 1 | 71 | .3 | 2 | 2 | 17 | 1.64 | .053 | 6 | 8 | .72 | 50 | .01 | 4 | 1.65 | .01 | .16 | 1 | 3 | 30 |
| 1203 G | 2 | 50 | 10 | 105 | .2 | 13 | 12 | 408 | 4.41 | 3 | 5 | ND | 1 | 73 | .2 | 2 | 5 | 18 | 2.06 | .065 | 4 | 7 | .77 | 42 | .01 | 4 | 1.68 | .01 | .14 | 1 | 3 | 30 |
| 1204 G | 2 | 34 | 8 | 100 | .1 | 10 | 11 | 431 | 3.98 | 3 | 5 | ND | 1 | 81 | .2 | 2 | 2 | 21 | 2.18 | .060 | 5 | 7 | .81 | 51 | .01 | 6 | 1.82 | .01 | .18 | 1 | 1 | 40 |
| STANDARD C/AU-R | 19 | 57 | 39 | 132 | 6.8 | 72 | 32 | 1051 | 3.96 | 39 | 19 | 7 | 38 | 53 | 19.1 | 15 | 22 | 56 | .52 | .097 | 38 | 57 | .89 | 182 | .07 | 36 | 1.88 | .06 | .13 | 11 | 495 | 1500 |

77p 6

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-------|-----|------|-----|-----|-------|------|------|-----|------|-----|-----|-----|------|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| 1205 G | 3 | 71 | 7 | 136 | .4 | 19 | 10 | 409 | 4.76 | 6 | 5 | ND | 1 106 | .6 | 2 | 8 | 32 | 1.84 | .064 | 9 | 12 | 1.02 | 117 | .01 | 8 | 2.36 | .01 | .18 | 3 | 1 | 30 | |
| 1206 G | 2 | 76 | 36 | 99 | .3 | 16 | 13 | 312 | 5.58 | 27 | 5 | ND | 1 91 | .2 | 3 | 7 | 25 | 1.38 | .057 | 5 | 9 | .75 | 70 | .01 | 6 | 1.82 | .02 | .22 | 1 | 30 | 40 | |
| 1207 G | 3 | 81 | 12 | 120 | .4 | 15 | 13 | 475 | 5.01 | 8 | 5 | ND | 1 104 | 1.0 | 4 | 2 | 32 | 2.15 | .058 | 8 | 11 | 1.07 | 97 | .01 | 8 | 2.47 | .02 | .18 | 1 | 3 | 50 | |
| 1208 G | 3 | 84 | 7 | 112 | .2 | 17 | 15 | 653 | 7.29 | 2 | 5 | ND | 1 102 | 1.2 | 2 | 9 | 50 | 2.22 | .126 | 8 | 15 | 1.53 | 59 | .01 | 3 | 3.57 | .01 | .15 | 1 | 4 | 30 | |
| 1209 G | 3 | 63 | 10 | 124 | .3 | 11 | 11 | 468 | 5.24 | 8 | 5 | ND | 1 103 | 1.2 | 2 | 3 | 35 | 1.98 | .066 | 5 | 11 | 1.04 | 62 | .01 | 3 | 2.42 | .01 | .21 | 1 | 9 | 40 | |
| 1210 G | 3 | 53 | 53 | 91 | .5 | 16 | 15 | 346 | 7.55 | 30 | 5 | ND | 1 86 | 1.2 | 6 | 2 | 27 | 1.37 | .066 | 4 | 10 | .81 | 59 | .01 | 4 | 1.94 | .01 | .18 | 1 | 10 | 30 | |
| 1211 G | 4 | 82 | 14 | 137 | .3 | 18 | 13 | 471 | 5.91 | 2 | 5 | ND | 1 79 | 1.0 | 2 | 8 | 40 | 1.04 | .081 | 7 | 13 | 1.24 | 57 | .01 | 6 | 2.93 | .01 | .18 | 1 | 1 | 30 | |
| 1212 G | 3 | 73 | 41 | 134 | .7 | 20 | 17 | 395 | 8.20 | 16 | 5 | ND | 1 91 | 1.6 | 2 | 2 | 24 | 1.84 | .064 | 4 | 8 | .66 | 60 | .01 | 3 | 1.76 | .01 | .21 | 1 | 14 | 50 | |
| 1213 G | 4 | 58 | 7 | 138 | .1 | 14 | 10 | 531 | 4.31 | 2 | 5 | ND | 1 114 | .9 | 2 | 4 | 33 | 2.19 | .079 | 10 | 12 | .94 | 63 | .01 | 3 | 2.23 | .02 | .18 | 2 | 2 | 40 | |
| 1214 G | 3 | 40 | 6 | 83 | .4 | 12 | 12 | 501 | 4.68 | 4 | 5 | ND | 1 125 | .5 | 2 | 3 | 28 | 2.39 | .076 | 6 | 10 | .78 | 59 | .01 | 9 | 1.82 | .02 | .18 | 1 | 2 | 40 | |
| 1215 G | 11 | 56 | 12 | 162 | .4 | 23 | 13 | 670 | 4.75 | 16 | 5 | ND | 1 165 | 1.5 | 2 | 2 | 32 | 3.19 | .071 | 6 | 11 | .85 | 114 | .01 | 7 | 2.05 | .02 | .17 | 1 | 11 | 50 | |
| 1216 G | 11 | 36 | 7 | 212 | .6 | 21 | 10 | 631 | 4.34 | 10 | 5 | ND | 1 152 | 1.3 | 2 | 2 | 35 | 2.71 | .076 | 8 | 13 | .98 | 95 | .01 | 2 | 2.16 | .01 | .15 | 1 | 4 | 50 | |
| 1217 G | 5 | 34 | 10 | 112 | .5 | 17 | 10 | 569 | 4.19 | 4 | 5 | ND | 1 121 | 1.0 | 2 | 2 | 17 | 2.96 | .066 | 5 | 8 | .66 | 61 | .01 | 2 | 1.62 | .01 | .16 | 1 | 7 | 40 | |
| 1218 G | 4 | 35 | 6 | 151 | .3 | 13 | 10 | 981 | 4.11 | 4 | 5 | ND | 2 168 | 1.2 | 2 | 5 | 25 | 4.34 | .064 | 7 | 9 | .86 | 55 | .01 | 5 | 2.05 | .02 | .15 | 2 | 4 | 60 | |
| 1219 G | 10 | 36 | 6 | 43 | .6 | 31 | 13 | 607 | 4.45 | 7 | 5 | ND | 3 127 | .3 | 3 | 2 | 33 | 3.15 | .075 | 7 | 12 | .93 | 97 | .01 | 8 | 2.22 | .02 | .20 | 1 | 14 | 30 | |
| 1220 G | 9 | 50 | 40 | 126 | .4 | 34 | 17 | 561 | 7.41 | 97 | 5 | ND | 1 124 | 1.5 | 4 | 3 | 30 | 3.50 | .070 | 4 | 10 | .84 | 69 | .01 | 3 | 2.06 | .01 | .18 | 1 | 49 | 40 | |
| 1221 G | 6 | 44 | 4 | 164 | .6 | 19 | 11 | 735 | 4.21 | 4 | 5 | ND | 2 147 | 1.3 | 2 | 3 | 29 | 4.05 | .066 | 7 | 11 | .83 | 61 | .01 | 3 | 2.09 | .01 | .16 | 1 | 4 | 60 | |
| 1222 G | 5 | 37 | 33 | 253 | .6 | 13 | 13 | 743 | 5.31 | 58 | 5 | ND | 1 134 | .9 | 2 | 5 | 19 | 4.97 | .083 | 5 | 8 | .53 | 59 | .01 | 4 | 1.29 | .01 | .15 | 2 | 34 | 50 | |
| 1223 G | 5 | 32 | 6 | 197 | .5 | 13 | 9 | 684 | 3.66 | 7 | 5 | ND | 1 103 | 1.4 | 3 | 2 | 30 | 2.96 | .084 | 8 | 10 | .85 | 53 | .01 | 5 | 1.93 | .02 | .17 | 1 | 3 | 40 | |
| 1224 G | 7 | 41 | 5 | 178 | .5 | 20 | 8 | 746 | 4.07 | 5 | 5 | ND | 2 118 | .7 | 2 | 3 | 31 | 3.77 | .066 | 8 | 13 | .87 | 58 | .01 | 6 | 2.05 | .01 | .16 | 1 | 1 | 30 | |
| 1225 G | 11 | 55 | 10 | 216 | .7 | 31 | 12 | 556 | 3.05 | 13 | 5 | ND | 2 118 | 1.4 | 2 | 2 | 29 | 4.03 | .066 | 7 | 11 | .66 | 73 | .01 | 3 | 1.56 | .01 | .17 | 1 | 18 | 50 | |
| 1226 G | 5 | 32 | 72 | 101 | 1.6 | 19 | 14 | 608 | 13.52 | 73 | 5 | ND | 3 112 | 1.5 | 11 | 8 | 8 | 3.21 | .044 | 5 | 8 | .32 | 32 | .01 | 5 | .89 | .02 | .18 | 3 | 41 | 70 | |
| 1227 G | 6 | 40 | 22 | 194 | .5 | 21 | 11 | 632 | 3.31 | 87 | 5 | ND | 1 132 | 1.2 | 2 | 3 | 15 | 3.65 | .065 | 5 | 8 | .57 | 60 | .01 | 4 | 1.28 | .02 | .19 | 2 | 44 | 50 | |
| 1228 G | 9 | 39 | 52 | 195 | 1.8 | 40 | 18 | 780 | 6.37 | 41 | 5 | ND | 3 170 | 1.2 | 7 | 3 | 26 | 5.66 | .083 | 4 | 11 | .84 | 46 | .01 | 2 | 1.51 | .01 | .16 | 1 | 23 | 80 | |
| 1229 G | 8 | 49 | 16 | 114 | 1.2 | 29 | 13 | 612 | 4.27 | 34 | 5 | ND | 1 117 | .5 | 3 | 2 | 24 | 3.82 | .079 | 5 | 9 | .84 | 59 | .01 | 4 | 1.76 | .01 | .17 | 2 | 40 | 60 | |
| 1230 G | 7 | 43 | 11 | 169 | 2.0 | 27 | 10 | 654 | 4.59 | 3 | 6 | ND | 1 115 | .7 | 2 | 2 | 23 | 3.35 | .063 | 4 | 9 | .89 | 78 | .01 | 4 | 1.90 | .01 | .16 | 1 | 4 | 90 | |
| 1231 G | 4 | 33 | 33 | 132 | 1.7 | 18 | 12 | 870 | 5.09 | 7 | 5 | ND | 2 162 | .7 | 2 | 4 | 15 | 5.24 | .051 | 5 | 5 | .90 | 61 | .01 | 4 | 1.77 | .01 | .17 | 1 | 23 | 130 | |
| 1232 G | 11 | 57 | 32 | 183 | 2.4 | 29 | 18 | 767 | 5.34 | 14 | 5 | ND | 2 136 | 1.1 | 2 | 2 | 32 | 4.15 | .081 | 6 | 8 | .80 | 61 | .01 | 5 | 1.79 | .01 | .18 | 2 | 10 | 110 | |
| 1233 G | 4 | 43 | 42 | 236 | 1.5 | 10 | 27 | 2136 | 10.70 | 50 | 8 | ND | 4 225 | 2.3 | 4 | 10 | 110 | 10.30 | .123 | 7 | 2 | 1.45 | 25 | .01 | 2 | 2.92 | .03 | .12 | 3 | 11 | 120 | |
| 1234 G | 6 | 22 | 20 | 166 | 1.3 | 19 | 26 | 1295 | 11.02 | 26 | 5 | ND | 2 143 | 1.0 | 5 | 7 | 58 | 5.95 | .104 | 4 | 6 | .95 | 30 | .01 | 2 | 1.96 | .02 | .13 | 1 | 5 | 80 | |
| 1235 G | 3 | 29 | 18 | 65 | 1.2 | 1 | 29 | 1477 | 9.95 | 85 | 5 | ND | 3 125 | 1.3 | 5 | 2 | 103 | 4.66 | .136 | 7 | 3 | 1.26 | 36 | .01 | 7 | 2.42 | .03 | .16 | 2 | 6 | 50 | |
| 1236 G | 4 | 24 | 7 | 48 | .5 | 3 | 25 | 1427 | 8.31 | 265 | 5 | ND | 1 125 | .9 | 2 | 10 | 117 | 4.30 | .146 | 7 | 3 | 1.49 | 54 | .01 | 7 | 2.79 | .03 | .19 | 2 | 11 | 40 | |
| 1237 G | 3 | 14 | 13 | 112 | .8 | 3 | 35 | 1421 | 10.93 | 28 | 5 | ND | 2 121 | 1.1 | 3 | 10 | 97 | 4.63 | .132 | 6 | 4 | 1.38 | 52 | .01 | 5 | 2.69 | .01 | .18 | 2 | 5 | 50 | |
| 1238 G | 3 | 9 | 7 | 124 | .7 | 1 | 30 | 1441 | 8.94 | 23 | 5 | ND | 3 123 | .6 | 2 | 9 | 105 | 4.25 | .137 | 8 | 2 | 1.50 | 50 | .01 | 2 | 2.99 | .02 | .16 | 1 | 4 | 30 | |
| 1239 G | 3 | 10 | 2 | 128 | .4 | 3 | 24 | 1431 | 8.32 | 17 | 5 | ND | 1 121 | .7 | 2 | 8 | 111 | 3.91 | .139 | 7 | 1 | 1.55 | 55 | .01 | 2 | 3.29 | .01 | .17 | 1 | 1 | 20 | |
| 1240 G | 2 | 29 | 6 | 114 | .5 | 3 | 25 | 1552 | 7.15 | 14 | 5 | ND | 2 145 | .7 | 2 | 2 | 96 | 5.46 | .123 | 7 | 2 | 1.09 | 34 | .01 | 2 | 2.40 | .03 | .13 | 1 | 6 | 40 | |
| STANDARD C/AU-R | 19 | 58 | 40 | 131 | 7.4 | 73 | 32 | 1050 | 3.92 | 41 | 20 | 7 | 39 | 53 | 18.8 | 16 | 22 | 56 | .52 | .097 | 38 | 57 | .89 | 182 | .08 | 36 | 1.89 | .06 | .13 | 11 | 471 | 1500 |

HP 6

Granges Inc. PROJECT 134 FILE # 90-3975

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Hg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | U ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1241 G | 9 | 44 | 27 | 117 | 1.5 | 31 | 21 | 713 | 6.24 | 17 | 5 | ND | 3 | 155 | 1.2 | 5 | 2 | 25 | 4.39 | .058 | 5 | 9 | .71 | 42 | .01 | 4 | 1.73 | .01 | .18 | 2 | 9 | 80 |
| 1242 G | 11 | 60 | 26 | 148 | 1.0 | 32 | 12 | 529 | 4.98 | 9 | 5 | ND | 1 | 106 | 1.0 | 2 | 3 | 32 | 2.34 | .059 | 5 | 11 | .85 | 82 | .01 | 2 | 2.11 | .01 | .19 | 1 | 17 | 40 |
| 1243 G | 4 | 39 | 15 | 137 | .6 | 19 | 18 | 974 | 5.82 | 25 | 5 | ND | 1 | 150 | 1.2 | 2 | 4 | 38 | 4.65 | .108 | 6 | 18 | 1.07 | 70 | .01 | 4 | 2.35 | .01 | .19 | 1 | 4 | 40 |
| 1244 G | 3 | 36 | 7 | 115 | .6 | 30 | 22 | 1065 | 4.92 | 25 | 5 | ND | 2 | 183 | .9 | 2 | 3 | 56 | 4.14 | .076 | 8 | 33 | 1.24 | 103 | .01 | 3 | 2.65 | .01 | .20 | 1 | 3 | 30 |
| 1245 G | 1 | 25 | 8 | 104 | .3 | 32 | 20 | 1446 | 5.27 | 28 | 5 | ND | 2 | 355 | 1.5 | 2 | 2 | 58 | 8.00 | .073 | 6 | 49 | 1.41 | 53 | .01 | 2 | 2.92 | .02 | .19 | 1 | 2 | 20 |
| 1246 G | 2 | 24 | 12 | 146 | .9 | 44 | 29 | 1498 | 9.36 | 44 | 5 | ND | 2 | 167 | 1.9 | 5 | 2 | 95 | 3.99 | .094 | 5 | 75 | 2.45 | 63 | .01 | 3 | 4.70 | .01 | .19 | 3 | 3 | 30 |
| 1247 G | 2 | 42 | 17 | 113 | .9 | 24 | 19 | 1171 | 6.52 | 36 | 5 | ND | 2 | 147 | 1.2 | 3 | 2 | 50 | 3.83 | .106 | 5 | 31 | 1.42 | 57 | .01 | 3 | 2.71 | .01 | .20 | 1 | 4 | 40 |
| 1248 G | 2 | 44 | 12 | 129 | 1.6 | 29 | 22 | 892 | 5.58 | 21 | 5 | ND | 1 | 112 | 1.1 | 2 | 3 | 49 | 2.54 | .093 | 5 | 29 | 1.25 | 64 | .01 | 3 | 2.48 | .01 | .20 | 1 | 1 | 30 |
| 1249 G | 2 | 49 | 11 | 131 | 1.7 | 47 | 31 | 1017 | 7.26 | 11 | 5 | ND | 1 | 105 | .7 | 2 | 2 | 78 | 2.15 | .090 | 4 | 54 | 1.66 | 93 | .01 | 5 | 3.41 | .01 | .20 | 1 | 1 | 40 |
| 1250 G | 4 | 36 | 18 | 122 | 2.0 | 16 | 12 | 637 | 3.92 | 3 | 5 | ND | 1 | 94 | .4 | 2 | 7 | 24 | 1.85 | .078 | 6 | 9 | .84 | 51 | .01 | 6 | 1.76 | .01 | .23 | 1 | 2 | 50 |
| 1251 G | 4 | 32 | 29 | 131 | 1.8 | 12 | 25 | 1597 | 8.15 | 58 | 5 | ND | 2 | 119 | 1.3 | 3 | 2 | 41 | 4.99 | .159 | 4 | 7 | 1.30 | 45 | .01 | 2 | 2.15 | .01 | .24 | 1 | 22 | 110 |
| 1252 G | 3 | 20 | 17 | 150 | 1.1 | 21 | 22 | 1328 | 7.07 | 88 | 5 | ND | 1 | 136 | 1.0 | 2 | 2 | 44 | 4.55 | .120 | 5 | 25 | 1.33 | 52 | .01 | 2 | 2.31 | .01 | .23 | 1 | 37 | 80 |
| 1253 G | 1 | 37 | 2 | 128 | 1.2 | 56 | 34 | 1503 | 7.30 | 22 | 5 | ND | 2 | 133 | 1.2 | 5 | 2 | 96 | 5.01 | .094 | 5 | 72 | 2.23 | 91 | .01 | 5 | 3.87 | .01 | .18 | 1 | 3 | 60 |
| 1254 G | 1 | 35 | 20 | 113 | 2.2 | 69 | 45 | 1537 | 10.17 | 123 | 5 | ND | 1 | 89 | .9 | 6 | 2 | 93 | 4.40 | .086 | 2 | 63 | 1.78 | 60 | .01 | 5 | 3.11 | .01 | .25 | 1 | 16 | 100 |
| 1255 G | 3 | 33 | 13 | 116 | 1.9 | 50 | 34 | 1671 | 8.83 | 96 | 5 | ND | 3 | 149 | 1.2 | 11 | 4 | 85 | 5.76 | .087 | 4 | 61 | 1.95 | 53 | .01 | 5 | 3.08 | .01 | .22 | 1 | 20 | 90 |
| 1256 G | 3 | 35 | 23 | 112 | 2.3 | 48 | 34 | 1599 | 8.92 | 147 | 5 | ND | 2 | 156 | 1.5 | 6 | 2 | 81 | 5.22 | .085 | 5 | 57 | 1.69 | 54 | .01 | 2 | 3.11 | .01 | .21 | 1 | 49 | 110 |
| 1257 G | 3 | 37 | 5 | 127 | 1.4 | 58 | 36 | 1472 | 7.45 | 48 | 5 | ND | 3 | 122 | 1.7 | 5 | 3 | 96 | 5.02 | .095 | 6 | 74 | 1.89 | 45 | .01 | 3 | 3.77 | .01 | .18 | 1 | 1 | 60 |
| 1258 G | 2 | 42 | 2 | 213 | .8 | 25 | 34 | 1582 | 5.65 | 54 | 5 | ND | 1 | 146 | .8 | 2 | 2 | 103 | 5.05 | .139 | 6 | 28 | 1.50 | 70 | .01 | 2 | 2.78 | .01 | .23 | 1 | 14 | 130 |
| 1259 G | 3 | 26 | 23 | 113 | 2.7 | 43 | 36 | 1324 | 10.36 | 103 | 5 | ND | 2 | 93 | 1.0 | 9 | 3 | 73 | 4.04 | .086 | 4 | 42 | 1.37 | 38 | .01 | 2 | 2.63 | .01 | .17 | 1 | 47 | 140 |
| 1260 G | 4 | 35 | 8 | 108 | .7 | 64 | 35 | 1614 | 7.36 | 41 | 5 | ND | 2 | 143 | .7 | 2 | 2 | 93 | 6.21 | .078 | 6 | 65 | 1.70 | 48 | .01 | 5 | 3.62 | .01 | .19 | 1 | 5 | 30 |
| 1261 G | 2 | 37 | 2 | 119 | .7 | 58 | 38 | 1734 | 8.84 | 62 | 5 | ND | 3 | 143 | 1.0 | 2 | 2 | 124 | 6.37 | .104 | 5 | 91 | 1.75 | 46 | .01 | 2 | 3.86 | .02 | .19 | 1 | 7 | 20 |
| 1262 G | 4 | 37 | 3 | 126 | .6 | 63 | 39 | 1959 | 9.72 | 49 | 5 | ND | 2 | 120 | 1.5 | 2 | 6 | 147 | 4.92 | .088 | 5 | 115 | 2.05 | 44 | .01 | 2 | 4.36 | .02 | .14 | 1 | 8 | 30 |
| 1263 G | 2 | 30 | 25 | 126 | 1.1 | 54 | 36 | 1743 | 9.22 | 38 | 5 | ND | 4 | 140 | .7 | 6 | 2 | 135 | 5.60 | .101 | 6 | 104 | 1.74 | 59 | .01 | 2 | 3.46 | .03 | .15 | 1 | 3 | 60 |
| 1264 G | 1 | 41 | 5 | 146 | .4 | 62 | 40 | 1727 | 7.65 | 43 | 5 | ND | 2 | 149 | .7 | 3 | 2 | 159 | 5.47 | .101 | 7 | 115 | 2.21 | 79 | .01 | 2 | 3.77 | .02 | .20 | 1 | 2 | 50 |
| 1265 G | 2 | 27 | 2 | 168 | .5 | 63 | 35 | 1672 | 7.93 | 34 | 5 | ND | 3 | 119 | 1.0 | 3 | 4 | 158 | 5.43 | .104 | 5 | 134 | 1.85 | 36 | .01 | 4 | 3.36 | .04 | .14 | 1 | 4 | 40 |
| 1266 G | 2 | 23 | 4 | 125 | .4 | 58 | 35 | 1861 | 8.13 | 31 | 5 | ND | 3 | 126 | 1.2 | 4 | 7 | 153 | 5.12 | .092 | 6 | 130 | 1.89 | 53 | .01 | 2 | 3.66 | .04 | .18 | 3 | 2 | 20 |
| 1267 G | 2 | 24 | 18 | 154 | .1 | 58 | 31 | 1937 | 7.79 | 34 | 5 | ND | 2 | 136 | 1.0 | 4 | 2 | 138 | 6.54 | .073 | 6 | 102 | 2.03 | 30 | .01 | 2 | 3.59 | .03 | .07 | 2 | 2 | 30 |
| 1268 G | 1 | 48 | 25 | 126 | .5 | 67 | 41 | 2356 | 8.56 | 49 | 5 | ND | 3 | 264 | 1.2 | 4 | 2 | 144 | 8.01 | .087 | 8 | 106 | 2.64 | 92 | .01 | 2 | 3.84 | .02 | .17 | 1 | 4 | 30 |
| 1269 G | 1 | 45 | 2 | 103 | .2 | 60 | 37 | 1291 | 7.77 | 29 | 5 | ND | 4 | 173 | 1.0 | 5 | 2 | 189 | 5.49 | .087 | 9 | 100 | 2.39 | 88 | .07 | 3 | 3.89 | .10 | .12 | 2 | 1 | 20 |
| 1270 G | 2 | 57 | 4 | 138 | .5 | 61 | 40 | 1551 | 8.02 | 38 | 5 | ND | 3 | 189 | 1.4 | 6 | 2 | 168 | 6.01 | .093 | 8 | 117 | 2.22 | 69 | .02 | 2 | 3.67 | .03 | .16 | 1 | 3 | 30 |
| 1271 G | 2 | 32 | 6 | 102 | .2 | 58 | 33 | 1902 | 7.83 | 38 | 5 | ND | 3 | 170 | .6 | 4 | 4 | 160 | 8.26 | .084 | 7 | 114 | 2.12 | 73 | .01 | 2 | 3.52 | .04 | .08 | 1 | 2 | 20 |
| 1272 G | 2 | 29 | 9 | 121 | .6 | 16 | 17 | 1115 | 4.81 | 14 | 5 | ND | 4 | 118 | .4 | 4 | 2 | 41 | 5.14 | .095 | 9 | 15 | .99 | 55 | .01 | 3 | 2.18 | .01 | .20 | 1 | 11 | 60 |
| 1273 G | 6 | 24 | 8 | 114 | .5 | 17 | 19 | 1126 | 5.17 | 18 | 5 | ND | 2 | 129 | .3 | 3 | 2 | 43 | 5.47 | .082 | 9 | 21 | 1.01 | 107 | .01 | 2 | 2.23 | .02 | .16 | 1 | 14 | 70 |
| 1274 G | 4 | 36 | 18 | 117 | .4 | 17 | 18 | 706 | 5.51 | 32 | 5 | ND | 3 | 107 | .4 | 8 | 6 | 40 | 3.44 | .092 | 8 | 15 | 1.01 | 63 | .01 | 2 | 2.20 | .02 | .17 | 2 | 10 | 110 |
| 1275 G | 3 | 34 | 14 | 86 | .1 | 14 | 10 | 1206 | 3.22 | 17 | 5 | ND | 3 | 254 | .2 | 2 | 4 | 25 | 10.92 | .054 | 11 | 11 | .59 | 171 | .01 | 2 | 1.41 | .01 | .15 | 13 | 7 | 90 |
| 1276 G | 3 | 32 | 7 | 100 | .1 | 15 | 16 | 662 | 4.28 | 12 | 5 | ND | 1 | 113 | .2 | 2 | 4 | 36 | 3.70 | .075 | 8 | 17 | .86 | 62 | .01 | 2 | 1.89 | .02 | .14 | 1 | 3 | 100 |
| STANDARD C/AU-R | 20 | 62 | 40 | 133 | 7.6 | 73 | 33 | 1054 | 3.97 | 40 | 21 | 8 | 40 | 54 | 19.6 | 15 | 23 | 64 | .52 | .097 | 40 | 60 | .90 | 194 | .08 | 38 | 1.89 | .07 | .14 | 13 | 498 | 1300 |

AP 6

HP 6

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | V ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1277 G | 4 | 33 | 2 | 136 | .1 | 20 | 15 | 788 | 5.90 | 24 | 5 | ND | 1 | 89 | 1.6 | 4 | 3 | 41 | 3.20 | .085 | 8 | 19 | 1.10 | 35 | .01 | 2 | 2.45 | .01 | .11 | 1 | 69 | 140 |
| 1278 G | 2 | 25 | 2 | 126 | .2 | 18 | 14 | 960 | 5.92 | 20 | 5 | ND | 2 | 105 | 1.0 | 4 | 2 | 42 | 4.12 | .081 | 8 | 18 | 1.15 | 68 | .01 | 2 | 2.54 | .02 | .10 | 1 | 4 | 100 |
| 1279 G | 2 | 34 | 3 | 165 | .1 | 31 | 22 | 1254 | 7.20 | 25 | 5 | ND | 2 | 116 | 1.9 | 2 | 5 | 92 | 4.91 | .093 | 8 | 49 | 1.35 | 59 | .01 | 2 | 3.12 | .03 | .11 | 1 | 17 | 80 |
| 1280 G | 7 | 37 | 12 | 143 | 1.0 | 27 | 14 | 1131 | 4.06 | 21 | 5 | ND | 1 | 340 | 1.0 | 8 | 7 | 21 | 7.30 | .058 | 5 | 11 | .60 | 89 | .01 | 3 | 1.48 | .01 | .15 | 1 | 13 | 150 |
| 1281 G | 8 | 51 | 20 | 183 | 1.1 | 27 | 12 | 926 | 4.80 | 23 | 5 | ND | 1 | 222 | .6 | 6 | 9 | 18 | 4.63 | .066 | 6 | 8 | .65 | 58 | .01 | 2 | 1.64 | .01 | .18 | 1 | 16 | 130 |
| 1282 G | 5 | 24 | 15 | 86 | .6 | 18 | 8 | 2176 | 2.92 | 19 | 5 | ND | 1 | 638 | .5 | 6 | 3 | 13 | 15.71 | .039 | 6 | 6 | .45 | 74 | .01 | 5 | 1.19 | .01 | .15 | 1 | 6 | 110 |
| 1283 G | 5 | 30 | 18 | 82 | .9 | 19 | 7 | 2227 | 2.39 | 13 | 5 | ND | 1 | 492 | .7 | 4 | 5 | 10 | 12.76 | .036 | 5 | 6 | .31 | 55 | .01 | 2 | .84 | .01 | .14 | 2 | 8 | 60 |
| 1284 G | 7 | 32 | 36 | 134 | 2.1 | 23 | 17 | 572 | 5.33 | 50 | 5 | ND | 1 | 95 | .9 | 9 | 2 | 15 | 1.74 | .067 | 5 | 8 | .48 | 52 | .01 | 4 | 1.20 | .01 | .19 | 1 | 17 | 70 |
| 1285 G | 8 | 25 | 38 | 134 | 1.7 | 32 | 21 | 501 | 4.95 | 49 | 5 | ND | 1 | 77 | .5 | 5 | 5 | 16 | 1.44 | .057 | 4 | 6 | .46 | 46 | .01 | 4 | 1.17 | .01 | .16 | 1 | 17 | 100 |
| 1286 G | 9 | 25 | 15 | 116 | 1.3 | 19 | 19 | 1045 | 6.11 | 30 | 5 | ND | 1 | 106 | .6 | 7 | 4 | 34 | 3.13 | .076 | 5 | 13 | .87 | 43 | .01 | 3 | 1.91 | .02 | .14 | 1 | 9 | 120 |
| 1287 G | 5 | 53 | 29 | 112 | 3.5 | 23 | 13 | 284 | 5.34 | 28 | 5 | ND | 2 | 81 | .2 | 11 | 3 | 19 | .26 | .057 | 5 | 10 | .77 | 58 | .01 | 5 | 1.66 | .01 | .19 | 1 | 26 | 190 |
| 1288 G | 4 | 56 | 26 | 102 | 2.7 | 27 | 30 | 790 | 5.56 | 28 | 5 | ND | 2 | 180 | .3 | 10 | 5 | 22 | 2.56 | .088 | 6 | 13 | 1.02 | 87 | .01 | 3 | 1.17 | .01 | .20 | 2 | 18 | 160 |
| 1289 G | 3 | 15 | 16 | 85 | 1.8 | 17 | 9 | 3436 | 3.99 | 27 | 5 | ND | 1 | 689 | 1.5 | 6 | 5 | 23 | 16.79 | .073 | 6 | 12 | .68 | 33 | .01 | 2 | 1.48 | .01 | .09 | 1 | 11 | 80 |
| 1290 G | 9 | 42 | 55 | 128 | 4.4 | 29 | 18 | 833 | 5.11 | 56 | 5 | ND | 1 | 132 | .2 | 10 | 3 | 19 | 2.41 | .079 | 5 | 8 | .67 | 68 | .01 | 2 | 1.22 | .01 | .19 | 1 | 27 | 180 |
| 1291 G | 2 | 25 | 2 | 132 | .8 | 15 | 12 | 1270 | 5.10 | 13 | 5 | ND | 2 | 110 | .6 | 6 | 3 | 28 | 3.66 | .059 | 10 | 15 | .96 | 116 | .01 | 2 | 2.08 | .02 | .13 | 1 | 5 | 130 |
| 1292 G | 4 | 82 | 16 | 150 | .1 | 26 | 15 | 417 | 5.36 | 28 | 5 | ND | 1 | 106 | .5 | 11 | 2 | 21 | 1.23 | .052 | 6 | 8 | .79 | 54 | .01 | 2 | 1.13 | .01 | .18 | 1 | 3 | 340 |
| 1293 G | 5 | 43 | 8 | 127 | .1 | 25 | 11 | 490 | 4.95 | 27 | 5 | ND | 1 | 118 | .5 | 10 | 4 | 16 | 2.11 | .082 | 4 | 6 | .77 | 54 | .01 | 3 | .68 | .01 | .17 | 1 | 5 | 420 |
| 1294 G | 9 | 50 | 24 | 163 | .4 | 29 | 11 | 569 | 4.74 | 39 | 5 | ND | 2 | 134 | 1.3 | 13 | 2 | 11 | 2.43 | .067 | 4 | 4 | .74 | 55 | .01 | 3 | .43 | .01 | .18 | 1 | 6 | 550 |
| 1295 G | 3 | 28 | 6 | 165 | .1 | 13 | 10 | 1413 | 5.08 | 19 | 5 | ND | 1 | 229 | .3 | 2 | 2 | 17 | 4.70 | .066 | 5 | 4 | .76 | 51 | .01 | 2 | .41 | .01 | .13 | 1 | 6 | 170 |
| 1296 G | 4 | 66 | 17 | 108 | .1 | 23 | 14 | 440 | 4.86 | 43 | 5 | ND | 1 | 115 | .2 | 14 | 2 | 11 | 1.24 | .053 | 5 | 3 | .69 | 50 | .01 | 3 | .43 | .01 | .18 | 1 | 6 | 590 |
| 1297 G | 3 | 62 | 16 | 95 | .3 | 21 | 13 | 462 | 5.60 | 33 | 5 | ND | 1 | 98 | .2 | 10 | 4 | 11 | 1.45 | .046 | 5 | 4 | .96 | 60 | .01 | 2 | .43 | .01 | .17 | 1 | 17 | 310 |
| 1298 G | 3 | 14 | 6 | 111 | .1 | 9 | 10 | 656 | 4.18 | 8 | 5 | ND | 1 | 88 | .2 | 4 | 2 | 14 | 1.89 | .046 | 14 | 12 | .54 | 51 | .01 | 4 | .59 | .01 | .15 | 1 | 1 | 140 |
| 1299 G | 5 | 6 | 2 | 144 | .1 | 5 | 2 | 580 | 1.15 | 3 | 5 | ND | 1 | 160 | .9 | 2 | 2 | 1 | 3.30 | .003 | 23 | 3 | .17 | 120 | .01 | 4 | .32 | .01 | .20 | 1 | 7 | 60 |
| 1300 G | 5 | 7 | 4 | 155 | .1 | 4 | 1 | 470 | .84 | 2 | 5 | ND | 1 | 181 | .7 | 2 | 2 | 1 | 3.17 | .002 | 17 | 3 | .14 | 59 | .01 | 5 | .29 | .01 | .22 | 2 | 21 | 70 |
| 1301 G | 4 | 6 | 2 | 129 | .1 | 5 | 1 | 879 | 1.29 | 2 | 5 | ND | 1 | 169 | .4 | 2 | 2 | 1 | 4.15 | .011 | 26 | 3 | .20 | 39 | .01 | 5 | .30 | .01 | .15 | 1 | 5 | 90 |
| 1302 G | 5 | 8 | 2 | 162 | .1 | 7 | 1 | 641 | 1.49 | 2 | 5 | ND | 1 | 80 | .5 | 2 | 2 | 1 | 2.66 | .004 | 23 | 18 | .17 | 33 | .01 | 4 | .30 | .02 | .13 | 1 | 2 | 180 |
| 1303 G | 3 | 14 | 8 | 92 | .1 | 7 | 5 | 647 | 2.61 | 3 | 5 | ND | 1 | 260 | .2 | 2 | 3 | 4 | 3.88 | .020 | 18 | 3 | .35 | 57 | .01 | 4 | .33 | .01 | .15 | 1 | 9 | 90 |
| 1304 G | 4 | 6 | 3 | 113 | .4 | 4 | 2 | 565 | 1.00 | 2 | 6 | ND | 2 | 124 | .4 | 4 | 2 | 1 | 2.91 | .002 | 24 | 3 | .14 | 45 | .01 | 4 | .26 | .01 | .16 | 1 | 1 | 80 |
| 1305 G | 4 | 5 | 3 | 144 | .1 | 3 | 1 | 526 | .98 | 2 | 5 | ND | 1 | 131 | .2 | 2 | 6 | 1 | 2.46 | .002 | 21 | 3 | .11 | 47 | .01 | 4 | .27 | .01 | .18 | 1 | 1 | 90 |
| 1306 G | 6 | 5 | 7 | 149 | .1 | 5 | 2 | 626 | 1.49 | 2 | 5 | ND | 2 | 122 | .2 | 2 | 4 | 2 | 2.81 | .019 | 21 | 15 | .17 | 47 | .01 | 5 | .38 | .02 | .18 | 1 | 1 | 100 |
| 1307 G | 5 | 8 | 6 | 206 | .2 | 5 | 1 | 481 | 1.74 | 4 | 5 | ND | 2 | 165 | .7 | 2 | 2 | 1 | 2.79 | .003 | 23 | 2 | .21 | 47 | .01 | 4 | .33 | .02 | .19 | 1 | 1 | 130 |
| 1308 G | 4 | 25 | 7 | 88 | .1 | 10 | 7 | 890 | 3.18 | 8 | 5 | ND | 1 | 126 | .2 | 2 | 6 | 9 | 3.02 | .037 | 17 | 5 | .40 | 62 | .01 | 4 | .61 | .01 | .18 | 1 | 2 | 80 |
| 1309 G | 5 | 7 | 7 | 120 | .3 | 6 | 5 | 533 | 3.05 | 6 | 5 | ND | 3 | 127 | .2 | 3 | 2 | 3 | 1.99 | .016 | 23 | 3 | .40 | 57 | .01 | 4 | .62 | .01 | .19 | 1 | 1 | 90 |
| 1310 G | 6 | 15 | 11 | 132 | .2 | 8 | 5 | 484 | 2.06 | 14 | 5 | ND | 1 | 114 | .7 | 3 | 2 | 4 | 1.68 | .023 | 18 | 2 | .29 | 53 | .01 | 4 | .36 | .01 | .18 | 1 | 6 | 80 |
| 1311 G | 5 | 6 | 5 | 151 | .1 | 4 | 1 | 463 | 1.09 | 6 | 5 | ND | 1 | 103 | .2 | 2 | 2 | 1 | 2.00 | .001 | 18 | 17 | .14 | 57 | .01 | 6 | .29 | .02 | .18 | 1 | 1 | 90 |
| 1312 G | 6 | 7 | 12 | 144 | .1 | 5 | 1 | 439 | .98 | 3 | 5 | ND | 1 | 82 | .2 | 2 | 2 | 1 | 1.65 | .001 | 17 | 4 | .12 | 41 | .01 | 3 | .25 | .02 | .14 | 1 | 1 | 110 |
| STANDARD C/AU-R | 19 | 58 | 40 | 132 | 6.9 | 73 | 32 | 1054 | 3.98 | 39 | 19 | 7 | 36 | 53 | 18.9 | 15 | 23 | 56 | .52 | .100 | 37 | 58 | .90 | 181 | .07 | 37 | 1.89 | .06 | .14 | 11 | 495 | 1500 |

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1313 G | 5 | 3 | 10 | 140 | .1 | 5 | 1 | 466 | 1.20 | 4 | 5 | ND | 1 | 83 | .6 | 2 | 2 | 1 | 1.55 | .001 | 17 | 4 | .15 | 40 | .01 | 4 | .26 | .02 | .15 | 1 | 2 | 160 |
| 1314 G | 12 | 20 | 21 | 111 | 1.1 | 12 | 6 | 343 | 3.22 | 86 | 5 | ND | 1 | 104 | .6 | 4 | 8 | 2 | 1.13 | .014 | 11 | 3 | .34 | 59 | .01 | 2 | .36 | .01 | .21 | 1 | 53 | 130 |
| 1315 G | 7 | 30 | 35 | 29 | 2.6 | 17 | 14 | 820 | 8.77 | 267 | 5 | ND | 1 | 104 | .6 | 7 | 2 | 4 | 1.61 | .058 | 3 | 10 | .37 | 26 | .01 | 3 | .38 | .01 | .21 | 1 | 150 | 150 |
| 1316 G | 3 | 53 | 36 | 317 | 2.8 | 20 | 15 | 243 | 3.84 | 65 | 6 | ND | 1 | 100 | .8 | 10 | 4 | 8 | .61 | .076 | 6 | 3 | .33 | 50 | .01 | 4 | .46 | .01 | .25 | 1 | 39 | 460 |
| 1317 G | 3 | 56 | 56 | 180 | 6.7 | 19 | 12 | 270 | 4.52 | 86 | 5 | ND | 1 | 81 | .5 | 13 | 2 | 10 | .52 | .074 | 4 | 3 | .29 | 41 | .01 | 7 | .46 | .01 | .24 | 1 | 73 | 290 |
| 1318 G | 4 | 53 | 67 | 144 | 5.2 | 21 | 12 | 178 | 4.50 | 127 | 5 | ND | 1 | 85 | .4 | 11 | 3 | 6 | .65 | .069 | 4 | 3 | .15 | 46 | .01 | 3 | .43 | .01 | .24 | 1 | 78 | 250 |
| 1319 G | 4 | 42 | 56 | 156 | 5.4 | 19 | 11 | 121 | 3.86 | 120 | 5 | ND | 1 | 71 | .5 | 11 | 9 | 4 | .47 | .079 | 6 | 7 | .09 | 44 | .01 | 4 | .45 | .01 | .24 | 1 | 77 | 220 |
| 1320 G | 6 | 57 | 40 | 109 | 3.6 | 23 | 11 | 459 | 5.08 | 133 | 6 | ND | 1 | 231 | .6 | 9 | 2 | 5 | 2.74 | .054 | 3 | 5 | .41 | 44 | .01 | 4 | .33 | .01 | .19 | 1 | 90 | 180 |
| 1321 G | 6 | 42 | 18 | 104 | 1.6 | 15 | 10 | 878 | 4.18 | 36 | 5 | ND | 1 | 417 | .4 | 2 | 2 | 10 | 6.18 | .049 | 4 | 14 | 1.40 | 74 | .01 | 4 | .35 | .01 | .19 | 1 | 33 | 130 |
| 1322 G | 9 | 56 | 22 | 128 | 1.4 | 25 | 13 | 552 | 4.80 | 26 | 5 | ND | 1 | 158 | 1.1 | 2 | 5 | 9 | 2.23 | .060 | 3 | 7 | .66 | 74 | .01 | 2 | .38 | .01 | .21 | 1 | 11 | 120 |
| 1323 G | 8 | 53 | 21 | 115 | 1.7 | 26 | 11 | 450 | 4.06 | 28 | 5 | ND | 1 | 146 | .6 | 4 | 2 | 8 | 2.06 | .053 | 3 | 5 | .60 | 66 | .01 | 4 | .40 | .01 | .21 | 2 | 21 | 100 |
| 1324 G | 4 | 34 | 14 | 140 | .1 | 15 | 11 | 510 | 3.60 | 20 | 5 | ND | 1 | 144 | 1.1 | 7 | 2 | 11 | 2.64 | .055 | 4 | 3 | .61 | 66 | .01 | 7 | .36 | .01 | .17 | 1 | 1 | 190 |
| 1325 G | 5 | 29 | 18 | 113 | .1 | 14 | 10 | 381 | 3.64 | 18 | 5 | ND | 1 | 133 | .9 | 6 | 3 | 11 | 1.86 | .062 | 4 | 3 | .61 | 56 | .01 | 7 | .39 | .01 | .18 | 1 | 2 | 210 |
| 1326 G | 2 | 29 | 7 | 86 | .3 | 12 | 13 | 554 | 3.76 | 12 | 6 | ND | 2 | 138 | .3 | 5 | 6 | 15 | 2.56 | .060 | 6 | 4 | .71 | 128 | .01 | 5 | .40 | .02 | .18 | 2 | 2 | 160 |
| 1327 G | 5 | 30 | 14 | 125 | .1 | 16 | 12 | 631 | 3.93 | 17 | 5 | ND | 2 | 266 | 1.0 | 4 | 2 | 16 | 5.77 | .053 | 3 | 8 | .80 | 152 | .01 | 2 | .43 | .01 | .17 | 1 | 1 | 240 |
| 1328 G | 3 | 56 | 16 | 107 | .3 | 16 | 14 | 471 | 4.34 | 20 | 5 | ND | 1 | 145 | .4 | 6 | 2 | 14 | 1.84 | .039 | 3 | 4 | .70 | 76 | .01 | 5 | .40 | .02 | .20 | 1 | 4 | 440 |
| 1329 G | 2 | 20 | 6 | 104 | .1 | 11 | 16 | 1000 | 5.33 | 8 | 5 | ND | 2 | 179 | .3 | 2 | 2 | 30 | 3.69 | .085 | 10 | 5 | 1.05 | 101 | .01 | 3 | .52 | .02 | .15 | 1 | 1 | 240 |
| 1330 G | 2 | 29 | 7 | 104 | .1 | 12 | 15 | 557 | 4.61 | 8 | 5 | ND | 2 | 140 | .3 | 2 | 2 | 21 | 2.27 | .085 | 13 | 3 | .83 | 87 | .01 | 2 | .54 | .02 | .17 | 1 | 1 | 250 |
| 1331 G | 3 | 23 | 7 | 159 | .1 | 22 | 23 | 791 | 6.17 | 9 | 5 | ND | 2 | 128 | 1.2 | 3 | 2 | 43 | 3.10 | .105 | 9 | 21 | 1.14 | 63 | .01 | 2 | 2.08 | .02 | .14 | 1 | 3 | 220 |
| 1332 G | 3 | 12 | 2 | 128 | .1 | 7 | 16 | 1980 | 6.76 | 7 | 5 | ND | 3 | 277 | 1.7 | 2 | 2 | 26 | 7.95 | .087 | 14 | 5 | 2.24 | 43 | .01 | 2 | 1.69 | .02 | .12 | 1 | 1 | 100 |
| 1333 G | 3 | 17 | 2 | 131 | .1 | 9 | 21 | 1113 | 7.20 | 8 | 5 | ND | 3 | 121 | 1.5 | 2 | 5 | 35 | 3.38 | .118 | 17 | 5 | 1.64 | 49 | .01 | 2 | 2.54 | .02 | .16 | 1 | 5 | 90 |
| 1334 G | 3 | 14 | 5 | 187 | .2 | 7 | 18 | 1425 | 6.32 | 9 | 5 | ND | 3 | 120 | 1.0 | 3 | 2 | 30 | 4.05 | .121 | 16 | 5 | 1.62 | 63 | .01 | 2 | 2.10 | .02 | .14 | 1 | 2 | 160 |
| 1335 G | 3 | 22 | 14 | 151 | .1 | 15 | 23 | 993 | 6.66 | 5 | 5 | ND | 2 | 91 | .9 | 2 | 9 | 42 | 2.76 | .127 | 11 | 22 | 1.37 | 160 | .01 | 8 | 2.33 | .02 | .14 | 1 | 2 | 120 |
| 1336 G | 3 | 15 | 5 | 150 | .1 | 8 | 20 | 941 | 6.77 | 3 | 5 | ND | 2 | 87 | .6 | 3 | 3 | 33 | 2.65 | .126 | 14 | 6 | 1.34 | 82 | .01 | 2 | 2.37 | .02 | .12 | 1 | 1 | 100 |
| 1337 G | 4 | 13 | 5 | 126 | .1 | 6 | 16 | 1670 | 6.45 | 6 | 5 | ND | 3 | 124 | .7 | 2 | 2 | 29 | 4.92 | .116 | 16 | 6 | 1.45 | 89 | .01 | 2 | 2.10 | .02 | .13 | 1 | 1 | 80 |
| 1338 G | 2 | 24 | 8 | 104 | .1 | 7 | 20 | 1331 | 6.41 | 5 | 5 | ND | 3 | 127 | .7 | 2 | 4 | 29 | 4.49 | .111 | 13 | 7 | 1.41 | 41 | .01 | 2 | 2.08 | .02 | .15 | 1 | 13 | 70 |
| 1339 G | 2 | 17 | 2 | 148 | .1 | 5 | 16 | 823 | 6.82 | 2 | 5 | ND | 2 | 89 | .7 | 2 | 2 | 34 | 2.44 | .123 | 18 | 9 | 1.22 | 68 | .01 | 2 | 2.58 | .03 | .18 | 1 | 2 | 100 |
| 1340 G | 3 | 17 | 6 | 115 | .3 | 10 | 23 | 1182 | 5.94 | 15 | 5 | ND | 3 | 164 | .8 | 4 | 2 | 26 | 4.05 | .136 | 11 | 5 | 1.05 | 85 | .01 | 2 | 1.80 | .02 | .17 | 1 | 3 | 130 |
| 1341 G | 4 | 10 | 30 | 67 | .3 | 9 | 19 | 1877 | 5.87 | 42 | 5 | ND | 2 | 153 | .5 | 4 | 2 | 14 | 6.02 | .114 | 9 | 2 | 1.33 | 47 | .01 | 2 | .69 | .02 | .16 | 1 | 5 | 150 |
| 1342 G | 8 | 16 | 35 | 114 | .6 | 8 | 25 | 2211 | 7.03 | 41 | 5 | ND | 3 | 168 | 1.3 | 4 | 6 | 20 | 7.55 | .108 | 10 | 3 | 1.62 | 51 | .01 | 2 | .89 | .02 | .16 | 1 | 7 | 240 |
| 1343 G | 4 | 13 | 2 | 127 | .1 | 7 | 16 | 1237 | 5.69 | 5 | 5 | ND | 2 | 105 | .7 | 2 | 2 | 26 | 3.57 | .148 | 13 | 7 | 1.04 | 109 | .01 | 2 | 1.53 | .02 | .16 | 1 | 3 | 230 |
| 1344 G | 3 | 21 | 5 | 156 | .3 | 10 | 20 | 1204 | 5.89 | 11 | 5 | ND | 3 | 102 | .5 | 3 | 2 | 28 | 3.55 | .132 | 14 | 5 | 1.06 | 220 | .01 | 3 | 1.55 | .02 | .15 | 1 | 1 | 460 |
| 1345 G | 2 | 11 | 3 | 76 | .1 | 8 | 19 | 903 | 6.69 | 2 | 5 | ND | 2 | 78 | .3 | 2 | 2 | 31 | 2.24 | .125 | 18 | 4 | 1.04 | 60 | .01 | 7 | 2.01 | .02 | .16 | 1 | 1 | 420 |
| 1346 G | 5 | 7 | 2 | 54 | .1 | 11 | 24 | 1271 | 6.92 | 10 | 5 | ND | 2 | 93 | .4 | 2 | 3 | 31 | 3.13 | .120 | 13 | 4 | 1.09 | 112 | .01 | 3 | 1.66 | .02 | .16 | 1 | 1 | 310 |
| 1347 G | 2 | 13 | 2 | 63 | .2 | 10 | 22 | 1750 | 5.98 | 11 | 5 | ND | 3 | 105 | .5 | 4 | 2 | 24 | 3.87 | .139 | 15 | 9 | 1.12 | 61 | .01 | 2 | 1.22 | .03 | .13 | 1 | 1 | 190 |
| 1348 G | 8 | 51 | 33 | 215 | .6 | 13 | 33 | 2081 | 7.89 | 73 | 5 | ND | 3 | 145 | 1.0 | 4 | 9 | 27 | 7.22 | .134 | 11 | 2 | 1.83 | 63 | .01 | 2 | 1.16 | .02 | .16 | 1 | 13 | 400 |
| STANDARD C/AU-R | 20 | 60 | 39 | 133 | 7.1 | 73 | 33 | 1053 | 3.97 | 40 | 19 | 7 | 37 | 53 | 19.3 | 16 | 23 | 58 | .52 | .094 | 38 | 60 | .90 | 182 | .08 | 39 | 1.89 | .06 | .13 | 12 | 507 | 1600 |

776

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Tl | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | ppm | ppb | ppb | |
| 1349 G | 2 | 26 | 31 | 132 | .6 | 10 | 24 | 1850 | 7.27 | 36 | 5 | ND | 2 | 133 | 1.1 | 2 | 2 | 22 | 5.46 | .103 | 10 | 4 | 1.79 | 46 | .01 | 2 | 1.05 | .02 | .14 | 1 | 7 | 380 |
| 1350 G | 2 | 19 | 12 | 100 | .2 | 5 | 18 | 909 | 6.68 | 10 | 5 | ND | 2 | 78 | .3 | 2 | 2 | 29 | 1.79 | .132 | 17 | 3 | 1.09 | 112 | .01 | 3 | 1.58 | .02 | .21 | 1 | 17 | 200 |
| 1351 G | 3 | 21 | 9 | 180 | .3 | 10 | 23 | 857 | 6.95 | 32 | 5 | ND | 2 | 87 | 1.0 | 2 | 2 | 29 | 2.03 | .148 | 16 | 3 | 1.13 | 61 | .01 | 2 | 1.64 | .02 | .20 | 1 | 5 | 250 |
| 1352 G | 4 | 13 | 5 | 138 | .2 | 5 | 15 | 1561 | 6.26 | 9 | 5 | ND | 2 | 104 | .2 | 2 | 2 | 24 | 4.20 | .105 | 14 | 2 | 1.63 | 47 | .01 | 2 | .97 | .02 | .15 | 1 | 2 | 120 |
| 1353 G | 3 | 16 | 3 | 156 | .3 | 7 | 19 | 1164 | 6.66 | 13 | 5 | ND | 2 | 88 | .6 | 2 | 2 | 29 | 3.18 | .116 | 16 | 7 | 1.46 | 53 | .01 | 8 | 1.68 | .03 | .18 | 1 | 2 | 100 |
| 1354 G | 2 | 21 | 7 | 120 | .3 | 6 | 19 | 1056 | 5.64 | 9 | 5 | ND | 2 | 92 | .8 | 2 | 3 | 26 | 3.09 | .119 | 15 | 3 | 1.32 | 48 | .01 | 5 | 1.36 | .03 | .17 | 1 | 2 | 120 |
| 1355 G | 4 | 18 | 3 | 111 | .1 | 9 | 20 | 1057 | 6.15 | 12 | 5 | ND | 2 | 93 | .5 | 2 | 3 | 30 | 3.21 | .121 | 15 | 4 | 1.36 | 43 | .01 | 5 | 1.46 | .02 | .16 | 1 | 2 | 130 |
| 1356 G | 3 | 16 | 4 | 105 | .1 | 6 | 15 | 1029 | 5.40 | 6 | 5 | ND | 2 | 96 | .3 | 2 | 2 | 24 | 3.44 | .099 | 15 | 3 | 1.35 | 45 | .01 | 2 | 1.09 | .02 | .15 | 1 | 1 | 110 |
| 1357 G | 4 | 18 | 7 | 97 | .3 | 7 | 14 | 1194 | 5.20 | 7 | 5 | ND | 2 | 114 | .6 | 2 | 5 | 23 | 3.83 | .087 | 12 | 10 | 1.28 | 54 | .01 | 3 | .81 | .02 | .21 | 1 | 94 | 150 |
| 1358 G | 10 | 42 | 24 | 448 | .3 | 17 | 16 | 682 | 5.04 | 21 | 5 | ND | 1 | 168 | 3.0 | 4 | 2 | 17 | 2.78 | .080 | 5 | 3 | .96 | 74 | .01 | 5 | .66 | .01 | .25 | 23 | 5 | 710 |
| 1359 G | 2 | 19 | 16 | 48 | .5 | 11 | 14 | 1246 | 6.01 | 27 | 5 | ND | 2 | 158 | .5 | 4 | 2 | 14 | 4.33 | .049 | 4 | 3 | 1.27 | 54 | .01 | 3 | .37 | .01 | .17 | 2 | 2 | 250 |
| 1360 G | 4 | 30 | 9 | 80 | .1 | 9 | 11 | 1013 | 5.85 | 15 | 5 | ND | 1 | 148 | .4 | 2 | 4 | 22 | 3.59 | .053 | 3 | 4 | 1.16 | 75 | .01 | 8 | .42 | .02 | .16 | 1 | 4 | 240 |
| 1361 G | 4 | 27 | 12 | 80 | .3 | 9 | 10 | 853 | 4.20 | 13 | 5 | ND | 1 | 136 | .4 | 2 | 3 | 12 | 3.09 | .042 | 2 | 6 | 1.02 | 67 | .01 | 6 | .41 | .01 | .18 | 1 | 2 | 260 |
| 1362 G | 3 | 26 | 12 | 79 | .2 | 9 | 11 | 669 | 3.90 | 15 | 5 | ND | 1 | 116 | .5 | 3 | 4 | 12 | 2.46 | .059 | 3 | 3 | .80 | 66 | .01 | 5 | .43 | .02 | .19 | 2 | 2 | 210 |
| 1363 G | 3 | 21 | 7 | 102 | .2 | 7 | 7 | 778 | 3.44 | 8 | 5 | ND | 2 | 195 | .5 | 2 | 3 | 7 | 4.00 | .043 | 4 | 4 | .98 | 63 | .01 | 2 | .36 | .01 | .18 | 1 | 2 | 180 |
| 1364 G | 3 | 29 | 14 | 94 | .2 | 12 | 12 | 879 | 5.02 | 16 | 5 | ND | 1 | 117 | .4 | 2 | 3 | 19 | 2.30 | .083 | 8 | 5 | .79 | 72 | .01 | 2 | .47 | .02 | .19 | 1 | 5 | 150 |
| 1365 G | 8 | 35 | 24 | 144 | .6 | 8 | 10 | 913 | 3.93 | 10 | 5 | ND | 2 | 239 | .7 | 2 | 9 | 11 | 4.06 | .055 | 7 | 15 | .92 | 140 | .01 | 5 | .40 | .02 | .19 | 2 | 1 | 190 |
| 1366 G | 3 | 16 | 7 | 49 | .1 | 6 | 17 | 1443 | 6.49 | 13 | 5 | ND | 2 | 124 | .9 | 2 | 4 | 32 | 2.75 | .122 | 12 | 4 | 1.03 | 91 | .01 | 4 | .66 | .03 | .17 | 1 | 1 | 180 |
| 1367 G | 2 | 17 | 3 | 178 | .2 | 7 | 17 | 1785 | 7.73 | 8 | 5 | ND | 2 | 145 | 2.0 | 2 | 2 | 33 | 3.63 | .100 | 12 | 4 | 1.32 | 70 | .01 | 2 | .56 | .02 | .18 | 1 | 2 | 300 |
| 1368 G | 1 | 18 | 4 | 106 | .3 | 5 | 18 | 1570 | 6.98 | 10 | 5 | ND | 3 | 162 | 1.0 | 2 | 2 | 30 | 3.92 | .098 | 12 | 3 | 1.36 | 83 | .01 | 3 | .46 | .02 | .16 | 1 | 1 | 260 |
| 1369 G | 2 | 20 | 2 | 89 | .2 | 6 | 10 | 1035 | 3.83 | 3 | 5 | ND | 1 | 114 | .4 | 2 | 2 | 30 | 2.34 | .051 | 6 | 14 | .75 | 63 | .01 | 4 | 1.92 | .03 | .18 | 1 | 1 | 80 |
| 1370 G | 2 | 18 | 12 | 102 | .3 | 1 | 33 | 921 | 10.06 | 33 | 5 | ND | 1 | 200 | 1.6 | 2 | 2 | 147 | 3.63 | .123 | 3 | 1 | 1.35 | 32 | .02 | 2 | 3.10 | .05 | .08 | 1 | 7 | 500 |
| 1371 G | 1 | 15 | 2 | 103 | .1 | 1 | 22 | 1299 | 8.08 | 4 | 5 | ND | 1 | 193 | 1.5 | 2 | 2 | 172 | 5.07 | .113 | 3 | 1 | 1.40 | 22 | .03 | 3 | 3.37 | .05 | .04 | 1 | 1 | 380 |
| 1372 G | 1 | 16 | 2 | 60 | .1 | 7 | 12 | 539 | 3.44 | 6 | 5 | ND | 1 | 117 | .5 | 2 | 2 | 22 | 2.68 | .053 | 8 | 10 | .84 | 99 | .01 | 3 | 1.78 | .02 | .17 | 1 | 3 | 60 |
| 1373 G | 1 | 18 | 7 | 59 | .1 | 5 | 8 | 590 | 3.11 | 2 | 5 | ND | 1 | 122 | .5 | 2 | 2 | 19 | 2.89 | .045 | 7 | 14 | .87 | 121 | .01 | 2 | 1.77 | .02 | .19 | 1 | 1 | 50 |
| 1374 G | 1 | 15 | 2 | 56 | .1 | 4 | 8 | 505 | 2.97 | 2 | 5 | ND | 1 | 111 | .4 | 2 | 2 | 18 | 2.50 | .041 | 5 | 7 | .83 | 71 | .01 | 4 | 1.68 | .03 | .19 | 1 | 1 | 60 |
| 1375 G | 1 | 15 | 2 | 63 | .2 | 6 | 9 | 316 | 3.21 | 2 | 5 | ND | 1 | 73 | .4 | 2 | 2 | 20 | 1.40 | .047 | 6 | 8 | .82 | 63 | .01 | 4 | 1.65 | .02 | .16 | 1 | 1 | 70 |
| 1376 G | 2 | 31 | 11 | 76 | .3 | 15 | 17 | 192 | 3.76 | 11 | 5 | ND | 1 | 75 | .5 | 2 | 2 | 14 | .99 | .042 | 6 | 8 | .71 | 49 | .01 | 2 | 1.42 | .02 | .14 | 1 | 3 | 120 |
| 1377 G | 3 | 26 | 16 | 71 | .4 | 8 | 8 | 449 | 2.84 | 4 | 5 | ND | 1 | 298 | .2 | 2 | 2 | 16 | 4.90 | .094 | 5 | 23 | .74 | 50 | .01 | 3 | 1.39 | .02 | .16 | 2 | 7 | 140 |
| 1378 G | 1 | 12 | 11 | 71 | .3 | 8 | 9 | 650 | 3.61 | 6 | 5 | ND | 2 | 242 | .6 | 2 | 2 | 20 | 6.38 | .135 | 5 | 18 | 1.19 | 60 | .01 | 5 | 1.92 | .03 | .16 | 1 | 1 | 90 |
| 1379 G | 2 | 20 | 17 | 55 | .3 | 8 | 9 | 364 | 3.12 | 8 | 5 | ND | 1 | 224 | .2 | 4 | 3 | 13 | 4.48 | .110 | 5 | 10 | .70 | 57 | .01 | 2 | 1.32 | .02 | .16 | 1 | 1 | 130 |
| 1380 G | 2 | 13 | 11 | 41 | .1 | 4 | 6 | 271 | 2.46 | 2 | 5 | ND | 1 | 122 | .2 | 2 | 2 | 7 | 2.72 | .083 | 4 | 4 | .55 | 65 | .01 | 6 | 1.07 | .02 | .17 | 1 | 1 | 140 |
| 1381 G | 2 | 12 | 10 | 35 | .1 | 6 | 6 | 238 | 2.09 | 3 | 5 | ND | 1 | 151 | .3 | 2 | 4 | 6 | 2.94 | .078 | 4 | 13 | .51 | 59 | .01 | 3 | 1.01 | .02 | .18 | 2 | 6 | 110 |
| 1382 G | 1 | 21 | 17 | 58 | .1 | 7 | 8 | 528 | 3.12 | 6 | 5 | ND | 1 | 172 | .2 | 2 | 2 | 12 | 5.28 | .108 | 5 | 5 | .73 | 65 | .01 | 3 | 1.34 | .02 | .18 | 1 | 3 | 130 |
| 1383 G | 2 | 6 | 9 | 34 | .3 | 5 | 8 | 375 | 2.67 | 3 | 5 | ND | 2 | 165 | .2 | 2 | 2 | 8 | 4.29 | .069 | 4 | 7 | .66 | 62 | .01 | 4 | 1.13 | .02 | .18 | 1 | 21 | 120 |
| 1384 G | 2 | 11 | 2 | 37 | .1 | 8 | 9 | 530 | 2.80 | 2 | 5 | ND | 1 | 446 | .2 | 2 | 2 | 10 | 7.81 | .047 | 5 | 6 | .74 | 40 | .01 | 3 | 1.22 | .01 | .12 | 1 | 2 | 80 |
| STANDARD C/AU-R | 19 | 58 | 40 | 131 | 6.9 | 72 | 32 | 1054 | 3.97 | 39 | 20 | 6 | 37 | 53 | 19.1 | 15 | 21 | 56 | .52 | .095 | 38 | 56 | .90 | 181 | .07 | 36 | 1.89 | .06 | .14 | 11 | 493 | 1400 |

HPG

V

HPZ

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | V. Au** | Hg | |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-------|-----|------|-----|-----|-------|------|------|-----|------|-----|-----|-----|------|------|-----|-----|---------|-----|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| 1385 G | 2 | 16 | 13 | 51 | .1 | 9 | 8 | 566 | 2.96 | 3 | 5 | ND | 1 426 | .3 | 2 | 3 | 10 | 6.02 | .034 | 4 | 6 | .70 | 43 | .01 | 4 | 1.20 | .01 | .13 | 3 | 5 | 110 | |
| 1386 G | 2 | 12 | 15 | 47 | .1 | 11 | 8 | 433 | 2.93 | 2 | 5 | ND | 1 243 | .3 | 2 | 3 | 9 | 4.11 | .053 | 4 | 8 | .72 | 66 | .01 | 6 | 1.20 | .02 | .16 | 1 | 4 | 80 | |
| 1387 G | 1 | 31 | 30 | 71 | .3 | 13 | 14 | 168 | 4.77 | 8 | 5 | ND | 1 90 | .2 | 4 | 2 | 10 | 1.41 | .036 | 2 | 9 | .55 | 63 | .01 | 3 | 1.11 | .01 | .18 | 1 | 2 | 220 | |
| 1388 G | 2 | 23 | 19 | 55 | .4 | 12 | 11 | 340 | 3.64 | 5 | 5 | ND | 1 116 | .2 | 2 | 2 | 14 | 2.74 | .043 | 3 | 9 | .70 | 58 | .01 | 3 | 1.38 | .02 | .16 | 1 | 4 | 240 | |
| 1389 G | 2 | 26 | 28 | 71 | .2 | 12 | 12 | 372 | 3.72 | 7 | 5 | ND | 1 138 | .2 | 2 | 2 | 15 | 3.43 | .047 | 3 | 12 | .62 | 69 | .01 | 3 | 1.32 | .02 | .19 | 1 | 5 | 190 | |
| 1390 G | 1 | 16 | 10 | 59 | .2 | 11 | 10 | 331 | 2.32 | 4 | 5 | ND | 1 122 | .2 | 2 | 2 | 12 | 3.22 | .051 | 4 | 9 | .48 | 71 | .01 | 5 | 1.12 | .02 | .19 | 1 | 9 | 100 | |
| 1391 G | 2 | 12 | 25 | 16 | .4 | 9 | 8 | 1053 | 2.47 | 13 | 5 | ND | 1 279 | .5 | 2 | 2 | 7 | 7.48 | .048 | 5 | 11 | .44 | 73 | .01 | 4 | .83 | .02 | .15 | 1 | 1 | 90 | |
| 1392 G | 1 | 13 | 22 | 28 | .3 | 7 | 6 | 440 | 2.65 | 5 | 5 | ND | 1 167 | .2 | 3 | 2 | 8 | 4.11 | .069 | 3 | 6 | .52 | 57 | .01 | 7 | 1.03 | .02 | .15 | 1 | 5 | 80 | |
| 1393 G | 1 | 14 | 25 | 45 | .2 | 8 | 6 | 436 | 2.91 | 7 | 5 | ND | 1 163 | .2 | 2 | 2 | 8 | 3.89 | .065 | 3 | 7 | .57 | 75 | .01 | 6 | 1.12 | .02 | .14 | 1 | 7 | 100 | |
| 1394 G | 1 | 13 | 14 | 47 | .4 | 6 | 7 | 503 | 2.66 | 7 | 5 | ND | 2 238 | .2 | 4 | 2 | 7 | 5.69 | .059 | 4 | 5 | .59 | 55 | .01 | 5 | 1.06 | .02 | .15 | 1 | 6 | 140 | |
| 1395 G | 2 | 14 | 5 | 47 | .3 | 8 | 10 | 601 | 2.43 | 2 | 5 | ND | 1 247 | .2 | 2 | 4 | 5 | 6.17 | .046 | 3 | 10 | .52 | 65 | .01 | 2 | .91 | .02 | .15 | 2 | 4 | 330 | |
| 1396 G | 1 | 14 | 2 | 53 | .1 | 9 | 9 | 463 | 2.52 | 2 | 5 | ND | 1 203 | .3 | 2 | 2 | 9 | 4.61 | .063 | 4 | 11 | .69 | 57 | .01 | 7 | 1.19 | .02 | .15 | 1 | 4 | 180 | |
| 1397 G | 1 | 23 | 9 | 57 | .3 | 13 | 13 | 377 | 3.70 | 8 | 5 | ND | 1 239 | .6 | 2 | 2 | 12 | 4.29 | .057 | 3 | 10 | .66 | 61 | .01 | 5 | 1.22 | .02 | .16 | 1 | 3 | 170 | |
| 1398 G | 1 | 25 | 18 | 69 | .2 | 13 | 11 | 343 | 4.06 | 7 | 5 | ND | 1 148 | .2 | 2 | 2 | 16 | 3.23 | .056 | 3 | 11 | .75 | 61 | .01 | 3 | 1.41 | .02 | .16 | 1 | 28 | 120 | |
| 1399 G | 2 | 20 | 15 | 72 | .2 | 12 | 10 | 370 | 3.99 | 9 | 5 | ND | 1 155 | .2 | 2 | 2 | 14 | 3.41 | .055 | 3 | 16 | .78 | 71 | .01 | 5 | 1.44 | .02 | .17 | 1 | 3 | 100 | |
| 1400 G | 2 | 26 | 17 | 73 | .4 | 11 | 11 | 379 | 4.35 | 11 | 5 | ND | 1 161 | .4 | 5 | 2 | 15 | 3.50 | .050 | 3 | 10 | .81 | 61 | .01 | 5 | 1.47 | .02 | .15 | 1 | 7 | 130 | |
| 1401 G | 1 | 23 | 18 | 68 | .4 | 10 | 10 | 401 | 4.29 | 9 | 5 | ND | 1 159 | .5 | 3 | 3 | 17 | 3.47 | .049 | 3 | 9 | .88 | 66 | .01 | 6 | 1.62 | .02 | .17 | 1 | 3 | 110 | |
| 1402 G | 1 | 24 | 17 | 70 | .3 | 13 | 13 | 377 | 4.26 | 11 | 5 | ND | 1 144 | .2 | 2 | 2 | 18 | 3.14 | .045 | 3 | 10 | .86 | 71 | .01 | 5 | 1.68 | .02 | .18 | 1 | 6 | 130 | |
| 1403 G | 2 | 16 | 4 | 58 | .1 | 8 | 9 | 353 | 3.79 | 11 | 5 | ND | 1 189 | .6 | 4 | 2 | 14 | 3.31 | .121 | 5 | 15 | .85 | 70 | .01 | 7 | 1.59 | .02 | .17 | 1 | 7 | 60 | |
| 1404 G | 2 | 20 | 13 | 74 | .2 | 12 | 13 | 326 | 3.94 | 9 | 5 | ND | 1 163 | .3 | 2 | 2 | 13 | 2.96 | .086 | 4 | 9 | .75 | 86 | .01 | 2 | 1.51 | .02 | .19 | 1 | 9 | 100 | |
| 1405 G | 2 | 27 | 11 | 71 | .3 | 11 | 11 | 276 | 4.29 | 10 | 5 | ND | 1 138 | .6 | 2 | 2 | 15 | 2.33 | .050 | 3 | 10 | .81 | 71 | .01 | 5 | 1.58 | .01 | .19 | 1 | 5 | 120 | |
| 1406 G | 2 | 37 | 20 | 82 | .1 | 12 | 12 | 294 | 4.72 | 11 | 5 | ND | 1 139 | .3 | 2 | 5 | 17 | 2.33 | .046 | 3 | 9 | .89 | 77 | .01 | 7 | 1.75 | .02 | .21 | 1 | 9 | 110 | |
| 1407 G | 2 | 32 | 14 | 84 | .3 | 14 | 11 | 258 | 5.48 | 13 | 5 | ND | 1 118 | .3 | 2 | 2 | 17 | 1.83 | .060 | 3 | 13 | 1.10 | 72 | .01 | 3 | 1.88 | .02 | .18 | 1 | 5 | 100 | |
| 1408 G | 2 | 28 | 13 | 79 | .2 | 11 | 12 | 171 | 4.86 | 12 | 5 | ND | 1 98 | .5 | 2 | 3 | 14 | 1.20 | .060 | 3 | 10 | .96 | 39 | .01 | 3 | 1.63 | .01 | .16 | 1 | 8 | 90 | |
| 1409 G | 1 | 19 | 13 | 55 | .6 | 7 | 8 | 823 | 3.10 | 9 | 5 | ND | 2 828 | .5 | 2 | 2 | 9 | 12.42 | .035 | 3 | 6 | .61 | 56 | .01 | 3 | 1.04 | .01 | .14 | 1 | 11 | 70 | |
| 1410 G | 1 | 28 | 22 | 72 | .8 | 11 | 10 | 400 | 4.55 | 12 | 5 | ND | 1 309 | .9 | 2 | 2 | 12 | 4.35 | .073 | 3 | 7 | .80 | 63 | .01 | 5 | 1.42 | .01 | .18 | 1 | 14 | 90 | |
| 1411 G | 2 | 20 | 12 | 74 | .4 | 7 | 6 | 821 | 2.66 | 11 | 5 | ND | 1 870 | .4 | 2 | 2 | 8 | 11.89 | .056 | 3 | 12 | .58 | 121 | .01 | 6 | 1.00 | .01 | .14 | 1 | 11 | 60 | |
| 1412 G | 2 | 28 | 25 | 65 | 1.0 | 13 | 10 | 368 | 3.85 | 17 | 5 | ND | 1 163 | .2 | 3 | 2 | 11 | 2.50 | .080 | 4 | 7 | .75 | 51 | .01 | 3 | 1.26 | .01 | .18 | 1 | 15 | 40 | |
| 1413 G | 3 | 21 | 19 | 53 | 1.4 | 12 | 12 | 755 | 3.38 | 15 | 5 | ND | 2 479 | .2 | 4 | 2 | 9 | 7.32 | .082 | 3 | 10 | .64 | 68 | .01 | 2 | 1.02 | .02 | .19 | 4 | 16 | 60 | |
| 1414 G | 1 | 24 | 24 | 71 | .7 | 10 | 11 | 519 | 3.98 | 17 | 5 | ND | 1 421 | 1.2 | 3 | 2 | 15 | 5.59 | .047 | 3 | 9 | .82 | 87 | .01 | 3 | 1.48 | .02 | .18 | 1 | 15 | 40 | |
| 1415 G | 2 | 28 | 4 | 73 | .2 | 12 | 13 | 217 | 3.66 | 8 | 5 | ND | 1 86 | .2 | 2 | 3 | 16 | 1.37 | .052 | 5 | 17 | .79 | 77 | .01 | 6 | 1.53 | .02 | .20 | 1 | 7 | 50 | |
| 1416 G | 1 | 17 | 2 | 58 | .1 | 9 | 8 | 163 | 2.50 | 4 | 5 | ND | 1 85 | .3 | 2 | 2 | 15 | 1.24 | .081 | 8 | 10 | .64 | 88 | .01 | 4 | 1.29 | .02 | .18 | 1 | 2 | 30 | |
| 1417 G | 1 | 18 | 2 | 61 | .2 | 7 | 6 | 1040 | 2.68 | 3 | 5 | ND | 2 831 | .2 | 2 | 2 | 11 | 13.48 | .042 | 3 | 7 | .75 | 115 | .01 | 3 | 1.18 | .01 | .12 | 1 | 4 | 40 | |
| 1418 G | 2 | 37 | 6 | 81 | .2 | 13 | 14 | 199 | 4.65 | 13 | 5 | ND | 1 118 | 1.3 | 2 | 2 | 22 | 1.44 | .045 | 4 | 9 | 1.06 | 69 | .01 | 2 | 1.81 | .02 | .17 | 1 | 1 | 70 | |
| 1419 G | 2 | 38 | 12 | 84 | .2 | 12 | 12 | 164 | 4.47 | 10 | 5 | ND | 1 73 | .2 | 2 | 2 | 21 | .86 | .038 | 4 | 11 | 1.08 | 64 | .01 | 2 | 1.82 | .01 | .18 | 1 | 2 | 90 | |
| 1420 G | 2 | 40 | 8 | 90 | .1 | 12 | 12 | 245 | 5.04 | 13 | 5 | ND | 1 116 | .2 | 2 | 2 | 20 | 1.76 | .041 | 3 | 8 | 1.15 | 58 | .01 | 3 | 1.84 | .01 | .15 | 1 | 16 | 100 | |
| STANDARD C/AU-R | 19 | 58 | 39 | 132 | 6.9 | 72 | 32 | 1055 | 3.97 | 39 | 20 | 7 | 36 | 53 | 19.2 | 15 | 22 | 56 | .52 | .098 | 37 | 57 | .90 | 180 | .07 | 37 | 1.89 | .06 | .14 | 11 | 499 | 1500 |

FP 7

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | U | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| 1421 G | 2 | 41 | 19 | 90 | 2 | 11 | 10 | 227 | 5.31 | 11 | 5 | ND | 1 | 106 | 5 | 4 | 2 | 19 | 1.24 | .050 | 4 | 10 | 1.16 | 58 | .01 | 3 | 1.84 | .01 | .16 | 1 | 4 | 80 |
| 1422 G | 1 | 50 | 17 | 105 | 3 | 11 | 12 | 166 | 4.58 | 11 | 5 | ND | 1 | 86 | 2 | 2 | 2 | 19 | .85 | .034 | 4 | 10 | 1.13 | 58 | .01 | 2 | 1.80 | .01 | .16 | 1 | 4 | 90 |
| 1423 G | 1 | 43 | 13 | 95 | 3 | 12 | 10 | 202 | 4.56 | 10 | 5 | ND | 1 | 107 | 2 | 2 | 2 | 17 | 1.32 | .069 | 4 | 13 | 1.10 | 59 | .01 | 2 | 1.73 | .01 | .16 | 1 | 4 | 80 |
| 1424 G | 1 | 19 | 17 | 53 | 2 | 8 | 7 | 340 | 3.60 | 8 | 8 | ND | 1 | 227 | 2 | 2 | 2 | 9 | 3.68 | .078 | 4 | 10 | .87 | 55 | .01 | 2 | 1.16 | .01 | .14 | 1 | 6 | 70 |
| 1425 G | 1 | 14 | 15 | 52 | 2 | 10 | 8 | 427 | 3.16 | 7 | 5 | ND | 1 | 192 | 2 | 2 | 3 | 8 | 3.62 | .085 | 4 | 13 | .98 | 74 | .01 | 3 | 1.08 | .01 | .15 | 1 | 2 | 50 |
| 1426 G | 2 | 18 | 9 | 57 | 3 | 11 | 10 | 1088 | 4.13 | 10 | 5 | ND | 1 | 299 | 2 | 2 | 2 | 12 | 4.75 | .057 | 5 | 10 | 1.87 | 91 | .01 | 2 | .89 | .01 | .17 | 1 | 4 | 20 |
| 1427 G | 2 | 21 | 14 | 88 | 4 | 16 | 12 | 1786 | 5.19 | 14 | 5 | ND | 1 | 164 | 2 | 4 | 2 | 42 | 3.38 | .073 | 5 | 27 | 1.77 | 62 | .01 | 2 | 2.05 | .01 | .13 | 1 | 4 | 30 |
| 1428 G | 2 | 40 | 11 | 85 | 6 | 59 | 30 | 1960 | 7.50 | 41 | 5 | ND | 1 | 233 | 5 | 5 | 2 | 117 | 4.61 | .080 | 5 | 79 | 3.03 | 98 | .01 | 2 | 3.62 | .02 | .08 | 1 | 3 | 20 |
| 1429 G | 1 | 35 | 3 | 93 | 6 | 60 | 29 | 1573 | 8.13 | 34 | 5 | ND | 1 | 228 | 6 | 4 | 2 | 154 | 4.35 | .083 | 8 | 85 | 3.08 | 113 | .01 | 3 | 3.70 | .03 | .07 | 1 | 1 | 10 |
| 1430 G | 1 | 36 | 7 | 92 | 4 | 59 | 28 | 1343 | 8.13 | 29 | 5 | ND | 1 | 167 | 6 | 5 | 2 | 145 | 3.61 | .076 | 8 | 77 | 3.07 | 79 | .02 | 4 | 3.61 | .05 | .10 | 1 | 2 | 20 |
| 1431 G | 1 | 24 | 17 | 53 | 7 | 27 | 17 | 2707 | 6.57 | 31 | 5 | ND | 1 | 373 | 5 | 6 | 2 | 67 | 7.77 | .072 | 5 | 41 | 2.11 | 68 | .01 | 4 | 2.51 | .01 | .13 | 1 | 8 | 40 |
| 1432 G | 2 | 29 | 20 | 71 | 1.5 | 31 | 19 | 1763 | 6.95 | 64 | 5 | ND | 1 | 95 | 3 | 8 | 2 | 52 | 2.47 | .081 | 5 | 34 | 2.09 | 45 | .01 | 2 | 2.17 | .01 | .17 | 1 | 19 | 60 |
| 1433 G | 2 | 74 | 18 | 136 | 1.4 | 20 | 13 | 851 | 3.74 | 32 | 5 | ND | 2 | 69 | 2 | 3 | 3 | 13 | 1.18 | .068 | 5 | 9 | .78 | 49 | .01 | 3 | .98 | .01 | .22 | 2 | 17 | 70 |
| 1434 G | 7 | 27 | 29 | 113 | 1.2 | 27 | 11 | 723 | 5.06 | 89 | 5 | ND | 1 | 73 | 3 | 3 | 2 | 16 | .97 | .069 | 4 | 9 | .71 | 53 | .01 | 4 | 1.03 | .01 | .24 | 2 | 150 | 60 |
| 1435 G | 6 | 26 | 19 | 129 | 1.0 | 22 | 12 | 1445 | 4.56 | 66 | 5 | ND | 1 | 49 | 2 | 2 | 2 | 26 | 1.70 | .076 | 5 | 16 | 1.28 | 45 | .01 | 2 | 1.31 | .01 | .19 | 1 | 30 | 50 |
| 1436 G | 2 | 22 | 13 | 94 | .8 | 15 | 13 | 2569 | 5.40 | 36 | 5 | ND | 1 | 60 | 2 | 6 | 2 | 30 | 3.58 | .076 | 6 | 16 | 2.41 | 36 | .01 | 2 | 1.64 | .01 | .16 | 1 | 28 | 70 |
| 1437 G | 1 | 49 | 13 | 78 | 1.5 | 51 | 24 | 2492 | 7.51 | 45 | 5 | ND | 1 | 49 | 4 | 10 | 2 | 82 | 3.14 | .086 | 6 | 55 | 3.06 | 36 | .01 | 3 | 2.78 | .01 | .15 | 1 | 24 | 180 |
| 1438 G | 2 | 51 | 25 | 101 | 1.6 | 43 | 25 | 1930 | 7.05 | 49 | 5 | ND | 1 | 42 | 3 | 7 | 2 | 72 | 2.27 | .094 | 5 | 49 | 2.46 | 43 | .01 | 2 | 2.54 | .01 | .17 | 1 | 16 | 200 |
| 1439 G | 8 | 55 | 16 | 158 | 1.4 | 34 | 12 | 1067 | 5.43 | 27 | 5 | ND | 1 | 54 | 5 | 3 | 2 | 40 | 1.27 | .061 | 5 | 21 | 1.45 | 28 | .01 | 2 | 1.75 | .01 | .16 | 1 | 12 | 60 |
| 1440 G | 4 | 50 | 21 | 141 | 1.0 | 25 | 11 | 1233 | 5.37 | 54 | 5 | ND | 1 | 44 | 2 | 3 | 2 | 43 | 1.37 | .057 | 5 | 21 | 1.66 | 57 | .01 | 4 | 1.90 | .01 | .17 | 1 | 30 | 40 |
| 1441 G | 1 | 38 | 5 | 95 | 1.1 | 45 | 26 | 2182 | 7.49 | 38 | 5 | ND | 1 | 61 | 5 | 4 | 2 | 96 | 3.06 | .083 | 6 | 69 | 3.13 | 146 | .01 | 2 | 2.93 | .01 | .13 | 1 | 4 | 40 |
| 1442 G | 6 | 37 | 11 | 89 | 1.1 | 49 | 24 | 2272 | 7.71 | 50 | 5 | ND | 1 | 135 | 6 | 5 | 2 | 112 | 4.52 | .075 | 7 | 74 | 3.62 | 39 | .01 | 2 | 2.85 | .02 | .08 | 1 | 9 | 30 |
| 1443 G | 1 | 40 | 7 | 84 | .5 | 59 | 30 | 1262 | 7.46 | 18 | 5 | ND | 1 | 211 | .8 | 3 | 2 | 148 | 5.30 | .091 | 9 | 91 | 2.81 | 73 | .01 | 2 | 3.32 | .04 | .09 | 1 | 4 | 10 |
| 1444 G | 1 | 42 | 13 | 96 | .4 | 63 | 30 | 1159 | 8.14 | 2 | 5 | ND | 1 | 166 | .7 | 2 | 2 | 146 | 5.35 | .087 | 8 | 92 | 3.16 | 74 | .01 | 2 | 3.81 | .07 | .09 | 1 | 1 | 10 |
| 1445 G | 1 | 42 | 2 | 102 | .4 | 72 | 33 | 923 | 8.45 | 6 | 5 | ND | 1 | 156 | 1.0 | 3 | 2 | 173 | 4.10 | .095 | 10 | 98 | 2.82 | 150 | .09 | 4 | 3.95 | .19 | .09 | 1 | 1 | 10 |
| 1446 G | 1 | 43 | 14 | 97 | .5 | 69 | 33 | 888 | 8.12 | 5 | 7 | ND | 1 | 146 | 1.3 | 6 | 2 | 179 | 3.83 | .087 | 9 | 95 | 2.81 | 141 | .11 | 6 | 3.74 | .18 | .10 | 1 | 1 | 5 |
| 1447 G | 1 | 42 | 13 | 99 | .6 | 65 | 32 | 1161 | 8.22 | 11 | 5 | ND | 1 | 172 | .8 | 6 | 2 | 167 | 4.78 | .084 | 9 | 94 | 2.64 | 133 | .08 | 3 | 3.68 | .13 | .12 | 1 | 12 | 5 |
| 1448 G | 1 | 50 | 10 | 122 | .8 | 62 | 33 | 1394 | 8.18 | 43 | 5 | ND | 1 | 118 | .5 | 4 | 2 | 142 | 2.70 | .093 | 7 | 114 | 2.89 | 55 | .01 | 2 | 3.68 | .02 | .14 | 1 | 4 | 5 |
| 1449 G | 1 | 27 | 18 | 94 | 1.1 | 62 | 29 | 1932 | 8.72 | 34 | 5 | ND | 1 | 99 | .6 | 6 | 2 | 145 | 3.13 | .103 | 5 | 126 | 3.50 | 32 | .01 | 2 | 3.69 | .03 | .13 | 1 | 1 | 20 |
| 1450 G | 1 | 48 | 12 | 136 | 1.6 | 70 | 37 | 2264 | 7.63 | 51 | 5 | ND | 1 | 107 | .6 | 5 | 2 | 128 | 4.33 | .121 | 6 | 104 | 3.45 | 35 | .01 | 2 | 3.22 | .03 | .15 | 1 | 21 | 60 |
| 1451 G | 1 | 33 | 30 | 139 | 2.0 | 96 | 36 | 2260 | 8.19 | 156 | 5 | ND | 1 | 64 | .8 | 7 | 2 | 106 | 3.72 | .096 | 5 | 94 | 3.12 | 41 | .01 | 3 | 2.75 | .03 | .18 | 1 | 33 | 50 |
| 1452 G | 1 | 33 | 15 | 96 | 1.6 | 82 | 37 | 2125 | 8.71 | 69 | 5 | ND | 1 | 74 | .7 | 5 | 2 | 136 | 3.34 | .155 | 7 | 113 | 3.39 | 35 | .01 | 4 | 3.52 | .03 | .14 | 1 | 9 | 40 |
| 1453 G | 1 | 10 | 13 | 88 | .4 | 9 | 10 | 2621 | 4.98 | 16 | 5 | ND | 1 | 75 | .5 | 4 | 2 | 30 | 4.11 | .070 | 8 | 16 | 2.34 | 51 | .01 | 2 | 1.60 | .01 | .16 | 1 | 3 | 40 |
| 1454 G | 2 | 23 | 24 | 144 | .6 | 10 | 12 | 2569 | 5.89 | 12 | 5 | ND | 1 | 52 | .3 | 3 | 2 | 37 | 3.72 | .115 | 10 | 16 | 2.23 | 53 | .01 | 2 | 1.75 | .01 | .20 | 1 | 11 | 30 |
| 1455 G | 1 | 24 | 14 | 71 | .7 | 7 | 15 | 3855 | 8.12 | 13 | 5 | ND | 1 | 91 | .8 | 2 | 2 | 42 | 6.07 | .109 | 11 | 21 | 3.10 | 38 | .01 | 2 | 1.91 | .02 | .16 | 1 | 14 | 20 |
| 1456 G | 1 | 24 | 17 | 77 | .6 | 9 | 15 | 2493 | 8.78 | 9 | 5 | ND | 1 | 46 | 1.2 | 3 | 2 | 50 | 3.42 | .126 | 9 | 20 | 2.29 | 55 | .01 | 2 | 2.29 | .01 | .18 | 1 | 9 | 20 |
| STANDARD C/AU-R | 20 | 59 | 43 | 133 | 7.4 | 72 | 32 | 1054 | 3.97 | 40 | 15 | 7 | 39 | 52 | 18.6 | 15 | 21 | 58 | .51 | .099 | 39 | 61 | .92 | 187 | .08 | 36 | 1.92 | .06 | .14 | 12 | 505 | 1600 |

FP 7

777

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1457 G | 1 | 15 | 6 | 76 | .5 | 11 | 22 | 2138 | 6.71 | 21 | 5 | ND | 1 | 33 | .2 | 3 | 7 | 39 | 3.05 | .147 | 9 | 12 | 1.98 | 46 | .01 | 3 | 1.98 | .01 | .20 | 1 | 17 | 30 |
| 1458 G | 1 | 14 | 8 | 93 | .3 | 10 | 15 | 1966 | 5.35 | 8 | 5 | ND | 1 | 33 | .7 | 2 | 2 | 30 | 2.81 | .149 | 10 | 9 | 1.66 | 43 | .01 | 2 | 1.67 | .01 | .23 | 1 | 6 | 20 |
| 1459 G | 6 | 50 | 37 | 259 | 1.3 | 11 | 24 | 2330 | 13.14 | 22 | 5 | ND | 1 | 27 | 1.7 | 4 | 2 | 46 | 2.26 | .148 | 7 | 14 | 1.98 | 27 | .01 | 2 | 2.64 | .01 | .18 | 1 | 28 | 80 |
| 1460 G | 1 | 14 | 10 | 87 | .4 | 8 | 21 | 2205 | 5.41 | 22 | 5 | ND | 1 | 37 | .3 | 2 | 2 | 25 | 3.23 | .155 | 9 | 7 | 1.72 | 50 | .01 | 2 | 1.47 | .01 | .24 | 1 | 10 | 20 |
| 1461 G | 1 | 18 | 18 | 86 | .6 | 9 | 19 | 1842 | 6.32 | 18 | 5 | ND | 1 | 31 | .4 | 3 | 3 | 32 | 2.53 | .155 | 8 | 7 | 1.59 | 49 | .01 | 2 | 1.76 | .01 | .25 | 1 | 13 | 30 |
| 1462 G | 1 | 19 | 7 | 112 | .6 | 9 | 19 | 2093 | 6.68 | 11 | 5 | ND | 1 | 32 | 1.1 | 3 | 2 | 35 | 2.71 | .149 | 8 | 9 | 1.75 | 50 | .01 | 4 | 1.91 | .01 | .23 | 1 | 10 | 40 |
| 1463 G | 1 | 19 | 3 | 73 | .4 | 9 | 16 | 2135 | 6.76 | 5 | 5 | ND | 1 | 34 | .4 | 2 | 2 | 32 | 2.70 | .150 | 8 | 10 | 1.68 | 45 | .01 | 2 | 1.79 | .01 | .22 | 1 | 8 | 50 |
| 1464 G | 2 | 30 | 8 | 54 | .6 | 10 | 23 | 1679 | 6.84 | 12 | 5 | ND | 1 | 85 | .4 | 3 | 2 | 37 | 2.20 | .145 | 5 | 9 | 1.49 | 46 | .01 | 2 | 2.11 | .01 | .21 | 1 | 15 | 20 |
| 1465 G | 3 | 37 | 23 | 112 | 1.1 | 13 | 32 | 1404 | 11.30 | 22 | 5 | ND | 1 | 44 | 1.1 | 4 | 2 | 35 | 1.51 | .129 | 4 | 9 | 1.20 | 33 | .01 | 2 | 1.90 | .01 | .21 | 1 | 25 | 50 |
| 1466 G | 1 | 36 | 12 | 129 | 1.1 | 8 | 23 | 1888 | 8.83 | 9 | 5 | ND | 1 | 30 | 1.0 | 3 | 2 | 43 | 1.71 | .130 | 5 | 6 | 1.63 | 34 | .01 | 2 | 2.32 | .01 | .19 | 1 | 33 | 40 |
| 1467 G | 2 | 35 | 17 | 79 | .7 | 12 | 21 | 1552 | 9.06 | 12 | 5 | ND | 1 | 27 | .5 | 2 | 3 | 32 | 1.52 | .140 | 5 | 9 | 1.35 | 43 | .01 | 2 | 1.71 | .01 | .24 | 1 | 18 | 50 |
| 1468 G | 4 | 17 | 2 | 213 | .5 | 7 | 17 | 2250 | 7.10 | 10 | 7 | ND | 1 | 34 | 1.2 | 2 | 2 | 38 | 2.52 | .128 | 7 | 7 | 1.82 | 42 | .01 | 2 | 2.02 | .01 | .23 | 1 | 15 | 50 |
| 1469 G | 3 | 28 | 20 | 86 | 1.2 | 10 | 25 | 1803 | 9.80 | 16 | 5 | ND | 1 | 27 | .9 | 5 | 2 | 46 | 1.73 | .127 | 5 | 8 | 1.54 | 27 | .01 | 2 | 2.18 | .01 | .22 | 1 | 37 | 70 |
| STANDARD C/AU-R | 19 | 59 | 39 | 130 | 7.1 | 72 | 32 | 1052 | 3.96 | 40 | 19 | 7 | 37 | 53 | 19.0 | 15 | 22 | 55 | .52 | .096 | 37 | 57 | .89 | 180 | .07 | 37 | 1.86 | .06 | .14 | 11 | 498 | 1300 |

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT UNUK R, PROJECT 134 File # 90-3876

2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | V | Au** | Hg | |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|-------|------|-----|-----|-----|-----|------|-----|-----|-----|-------|------|-----|-----|------|-----|-----|----|------|-----|-----|----|------|------|-----|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | % | ppm | ppb | ppb |
| 1470 G | 1 | 21 | 14 | 27 | .3 | 12 | 23 | 1339 | 3.65 | 26 | 5 | ND | 1 | 42 | .4 | 2 | 2 | 10 | 2.26 | .139 | 7 | 10 | .86 | 44 | .01 | 3 | .57 | .01 | .27 | 1 | 7 | 50 | |
| 1471 G | 1 | 22 | 27 | 20 | .5 | 14 | 25 | 1415 | 3.65 | 32 | 5 | ND | 1 | 37 | .8 | 2 | 2 | 7 | 2.29 | .129 | 6 | 7 | .87 | 36 | .01 | 4 | .43 | .01 | .23 | 1 | 11 | 30 | |
| 1472 G | 2 | 16 | 13 | 338 | .4 | 9 | 15 | 1082 | 2.50 | 48 | 5 | ND | 1 | 37 | 2.0 | 3 | 4 | 8 | 1.86 | .130 | 6 | 7 | .69 | 43 | .01 | 3 | .51 | .01 | .26 | 1 | 11 | 130 | |
| 1473 G | 5 | 20 | 45 | 75 | 1.6 | 6 | 12 | 1860 | 9.49 | 3675 | 5 | ND | 1 | 141 | .2 | 44 | 2 | 9 | 3.66 | .068 | 2 | 11 | .89 | 21 | .01 | 2 | .50 | .01 | .19 | 1 | 806 | 140 | |
| 1474 G | 1 | 8 | 59 | 32 | 1.3 | 8 | 11 | 1682 | 8.41 | 4213 | 5 | ND | 1 | 108 | .5 | 41 | 2 | 5 | 3.49 | .083 | 3 | 9 | .88 | 27 | .01 | 2 | .32 | .01 | .15 | 1 | 767 | 100 | |
| 1475 G | 3 | 18 | 68 | 334 | 1.3 | 6 | 11 | 1239 | 7.85 | 996 | 5 | ND | 1 | 72 | 1.7 | 9 | 2 | 5 | 2.45 | .098 | 4 | 8 | .71 | 27 | .01 | 2 | .39 | .01 | .18 | 1 | 416 | 120 | |
| 1476 G | 1 | 19 | 209 | 45 | 3.8 | 6 | 12 | 1871 | 17.70 | 8159 | 5 | ND | 1 | 109 | .2 | 80 | 2 | 7 | 3.23 | .047 | 2 | 13 | .73 | 12 | .01 | 2 | .31 | .01 | .13 | 1 | 2399 | 150 | |
| 1477 G | 1 | 13 | 18 | 132 | .6 | 9 | 15 | 1233 | 5.57 | 549 | 5 | ND | 1 | 137 | .9 | 3 | 2 | 10 | 2.89 | .117 | 4 | 4 | .59 | 43 | .01 | 2 | .40 | .01 | .23 | 1 | 200 | 70 | |
| 1478 G | 1 | 26 | 13 | 120 | 1.4 | 12 | 22 | 851 | 5.81 | 74 | 5 | ND | 1 | 66 | .5 | 3 | 3 | 12 | 1.19 | .115 | 5 | 10 | .72 | 36 | .01 | 3 | .44 | .01 | .22 | 1 | 34 | 90 | |
| 1479 G | 1 | 20 | 5 | 120 | .3 | 9 | 19 | 1233 | 7.45 | 25 | 5 | ND | 1 | 37 | .2 | 6 | 2 | 31 | .90 | .122 | 6 | 11 | 1.13 | 34 | .01 | 2 | .59 | .01 | .21 | 1 | 6 | 80 | |
| 1480 G | 1 | 48 | 16 | 44 | 1.4 | 10 | 21 | 1458 | 10.81 | 38 | 5 | ND | 1 | 44 | .2 | 11 | 2 | 31 | 1.37 | .114 | 5 | 16 | 1.28 | 17 | .01 | 2 | .70 | .01 | .18 | 2 | 22 | 60 | |
| 1481 G | 1 | 17 | 10 | 71 | .6 | 8 | 19 | 974 | 5.28 | 24 | 5 | ND | 1 | 56 | .5 | 6 | 4 | 16 | 1.28 | .112 | 7 | 8 | 1.16 | 50 | .01 | 2 | .46 | .01 | .21 | 2 | 11 | 40 | |
| 1482 G | 1 | 8 | 5 | 38 | .4 | 10 | 19 | 1050 | 4.88 | 23 | 5 | ND | 1 | 148 | .3 | 5 | 4 | 11 | 2.86 | .124 | 6 | 10 | 1.20 | 53 | .01 | 2 | .40 | .01 | .20 | 1 | 12 | 50 | |
| 1483 G | 1 | 35 | 36 | 288 | 1.7 | 5 | 15 | 982 | 6.26 | 2003 | 5 | ND | 1 | 116 | 1.0 | 16 | 6 | 10 | 2.41 | .097 | 3 | 8 | 1.00 | 25 | .01 | 2 | .41 | .01 | .20 | 1 | 376 | 160 | |
| 1484 G | 1 | 10 | 38 | 134 | .9 | 8 | 8 | 2525 | 4.51 | 836 | 5 | ND | 1 | 177 | 1.0 | 16 | 2 | 5 | 5.19 | .051 | 4 | 5 | 3.04 | 55 | .01 | 2 | .33 | .01 | .19 | 1 | 161 | 110 | |
| 1485 G | 1 | 20 | 11 | 88 | .6 | 14 | 7 | 2012 | 3.72 | 59 | 5 | ND | 1 | 196 | 1.1 | 7 | 5 | 7 | 4.09 | .047 | 3 | 10 | 1.99 | 72 | .01 | 3 | .46 | .01 | .24 | 1 | 43 | 100 | |
| 1486 G | 1 | 18 | 7 | 80 | .5 | 6 | 17 | 2340 | 7.25 | 29 | 5 | ND | 1 | 138 | .2 | 7 | 2 | 67 | 2.73 | .093 | 5 | 11 | 2.32 | 54 | .01 | 2 | 1.26 | .01 | .18 | 1 | 13 | 90 | |
| 1487 G | 1 | 63 | 44 | 133 | 1.5 | 11 | 14 | 1163 | 7.43 | 117 | 5 | ND | 1 | 142 | .4 | 12 | 2 | 25 | 2.45 | .082 | 2 | 11 | 1.73 | 25 | .01 | 2 | .43 | .01 | .16 | 1 | 87 | 130 | |
| 1488 G | 1 | 11 | 18 | 78 | .3 | 6 | 10 | 2073 | 5.62 | 92 | 5 | ND | 1 | 265 | .7 | 7 | 2 | 34 | 3.88 | .054 | 3 | 9 | 2.16 | 63 | .01 | 2 | .29 | .01 | .07 | 1 | 31 | 110 | |
| 1489 G | 1 | 17 | 44 | 192 | 1.0 | 6 | 16 | 1255 | 6.69 | 413 | 5 | ND | 1 | 154 | 1.1 | 10 | 6 | 30 | 2.41 | .085 | 3 | 10 | 1.37 | 30 | .01 | 2 | .32 | .01 | .10 | 1 | 137 | 180 | |
| 1490 G | 2 | 38 | 21 | 521 | .9 | 11 | 7 | 4059 | 7.55 | 256 | 5 | ND | 1 | 420 | 1.9 | 27 | 2 | 16 | 8.62 | .035 | 4 | 11 | 1.84 | 51 | .01 | 2 | .21 | .01 | .08 | 1 | 83 | 1600 | |
| 1491 G | 1 | 6 | 37 | 148 | .9 | 4 | 9 | 1202 | 3.76 | 595 | 5 | ND | 1 | 109 | 1.8 | 5 | 2 | 9 | 2.43 | .045 | 2 | 7 | .65 | 31 | .01 | 4 | .16 | .01 | .04 | 1 | 523 | 120 | |
| 1492 G | 1 | 14 | 57 | 235 | 1.1 | 8 | 9 | 3775 | 7.81 | 587 | 5 | ND | 1 | 320 | .2 | 17 | 3 | 19 | 7.48 | .040 | 5 | 11 | 2.47 | 40 | .01 | 2 | .17 | .01 | .06 | 1 | 406 | 370 | |
| 1493 G | 1 | 38 | 12 | 128 | 1.1 | 7 | 4 | 6049 | 7.43 | 206 | 5 | ND | 1 | 432 | .6 | 16 | 2 | 9 | 12.30 | .020 | 6 | 8 | 3.91 | 77 | .01 | 2 | .18 | .01 | .06 | 1 | 107 | 600 | |
| 1494 G | 9 | 40 | 17 | 175 | .7 | 27 | 12 | 1029 | 4.15 | 41 | 5 | ND | 1 | 147 | 1.4 | 4 | 2 | 14 | 2.42 | .075 | 4 | 9 | .98 | 62 | .01 | 4 | .41 | .01 | .17 | 1 | 19 | 150 | |
| 1495 G | 4 | 35 | 21 | 154 | .8 | 20 | 11 | 1089 | 4.53 | 19 | 5 | ND | 1 | 170 | .9 | 4 | 2 | 16 | 2.53 | .068 | 4 | 10 | 1.01 | 78 | .01 | 6 | .38 | .01 | .17 | 1 | 8 | 140 | |
| 1496 G | 2 | 30 | 24 | 78 | .9 | 15 | 12 | 520 | 4.31 | 45 | 6 | ND | 1 | 75 | 1.1 | 4 | 2 | 14 | 1.27 | .064 | 5 | 10 | .79 | 50 | .01 | 7 | .60 | .01 | .29 | 2 | 19 | 110 | |
| 1497 G | 3 | 61 | 13 | 180 | .8 | 36 | 18 | 1162 | 6.49 | 38 | 5 | ND | 1 | 83 | 1.0 | 4 | 2 | 81 | 2.42 | .083 | 5 | 57 | 1.48 | 51 | .01 | 2 | 1.53 | .01 | .15 | 1 | 162 | 140 | |
| STANDARD C/AU-R | 18 | 60 | 36 | 134 | 7.0 | 72 | 32 | 1056 | 3.97 | 41 | 20 | 7 | 38 | 53 | 19.4 | 11 | 22 | 56 | .52 | .102 | 38 | 61 | .91 | 181 | .07 | 39 | 1.89 | .06 | .12 | 11 | 483 | 1500 | |

AP 7

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: CORE AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: AUG 27 1990 DATE REPORT MAILED: *Aug 31/90.* SIGNED BY: *[Signature]* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT UNUK R. 134 File # 90-4140 Page 1

2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| 1498 G | 2 | 36 | 12 | 76 | .6 | 18 | 14 | 1486 | 5.72 | 31 | 5 | ND | 1 | 80 | .8 | 2 | 2 | 62 | 3.16 | .074 | 7 | 26 | 1.68 | 37 | .01 | 2 | 1.96 | .02 | .10 | 1 | 66 | 30 |
| 1499 G | 2 | 31 | 8 | 101 | .7 | 19 | 16 | 1455 | 5.99 | 18 | 5 | ND | 1 | 60 | .6 | 5 | 2 | 66 | 2.77 | .094 | 8 | 28 | 1.82 | 44 | .01 | 4 | 1.99 | .02 | .11 | 1 | 29 | 20 |
| 1500 G | 3 | 25 | 17 | 89 | .9 | 20 | 16 | 1396 | 5.78 | 26 | 5 | ND | 1 | 59 | .9 | 4 | 2 | 57 | 2.67 | .085 | 8 | 24 | 1.60 | 40 | .01 | 4 | 1.75 | .02 | .12 | 1 | 19 | 80 |
| 1501 G | 4 | 29 | 16 | 102 | .7 | 15 | 19 | 1186 | 5.01 | 30 | 5 | ND | 1 | 62 | .3 | 4 | 2 | 47 | 2.18 | .075 | 7 | 16 | 1.32 | 45 | .01 | 3 | 1.46 | .02 | .13 | 1 | 31 | 60 |
| 1502 G | 2 | 13 | 5 | 96 | .4 | 12 | 12 | 1322 | 4.66 | 7 | 5 | ND | 1 | 49 | .7 | 2 | 2 | 48 | 2.30 | .076 | 10 | 16 | 1.47 | 36 | .01 | 2 | 1.78 | .02 | .12 | 1 | 16 | 50 |
| 1503 G | 4 | 30 | 10 | 118 | .6 | 7 | 17 | 1401 | 6.07 | 15 | 5 | ND | 1 | 67 | 1.1 | 2 | 2 | 68 | 2.86 | .143 | 7 | 8 | 1.37 | 58 | .01 | 6 | 1.97 | .02 | .09 | 1 | 37 | 70 |
| 1504 G | 1 | 29 | 13 | 95 | .6 | 11 | 14 | 1565 | 6.50 | 8 | 5 | ND | 1 | 79 | .8 | 2 | 2 | 65 | 3.11 | .162 | 9 | 5 | 1.53 | 45 | .01 | 2 | 2.19 | .02 | .13 | 1 | 51 | 50 |
| 1505 G | 1 | 19 | 7 | 188 | .3 | 7 | 12 | 1836 | 6.02 | 12 | 5 | ND | 1 | 110 | 1.1 | 2 | 5 | 93 | 4.19 | .167 | 8 | 6 | 1.40 | 22 | .01 | 2 | 2.47 | .03 | .05 | 1 | 49 | 70 |
| 1506 G | 5 | 19 | 8 | 169 | .1 | 11 | 13 | 1494 | 5.16 | 17 | 5 | ND | 1 | 71 | .9 | 2 | 2 | 62 | 2.98 | .155 | 11 | 10 | 1.55 | 48 | .01 | 2 | 2.30 | .01 | .14 | 1 | 9 | 60 |
| 1507 G | 1 | 10 | 5 | 86 | .2 | 25 | 16 | 1109 | 4.66 | 15 | 5 | ND | 1 | 54 | .8 | 2 | 2 | 74 | 2.65 | .033 | 5 | 26 | 1.36 | 29 | .01 | 4 | 2.11 | .01 | .10 | 1 | 7 | 40 |
| 1508 G | 28 | 66 | 8 | 113 | 2.5 | 55 | 30 | 2082 | 7.36 | 32 | 5 | ND | 1 | 71 | .4 | 3 | 4 | 64 | 3.44 | .044 | 4 | 32 | 1.74 | 42 | .01 | 2 | 2.42 | .01 | .11 | 1 | 178 | 120 |
| 1509 G | 1 | 9 | 8 | 170 | .3 | 16 | 10 | 1130 | 3.48 | 6 | 5 | ND | 1 | 57 | .4 | 3 | 4 | 32 | 2.55 | .031 | 7 | 19 | 1.03 | 32 | .01 | 2 | 1.46 | .02 | .12 | 1 | 10 | 90 |
| 1510 G | 3 | 23 | 15 | 76 | .8 | 13 | 15 | 2043 | 6.95 | 37 | 5 | ND | 1 | 69 | .9 | 5 | 2 | 58 | 3.92 | .074 | 9 | 14 | 2.00 | 32 | .01 | 2 | 2.64 | .02 | .11 | 1 | 27 | 40 |
| 1511 G | 12 | 14 | 14 | 104 | .6 | 20 | 11 | 1234 | 6.16 | 38 | 5 | ND | 1 | 48 | 1.1 | 3 | 2 | 53 | 2.09 | .069 | 5 | 17 | 1.42 | 37 | .01 | 2 | 2.18 | .01 | .10 | 1 | 18 | 30 |
| 1512 G | 3 | 36 | 7 | 87 | 1.2 | 27 | 24 | 1466 | 7.86 | 13 | 5 | ND | 1 | 39 | .3 | 2 | 2 | 103 | 1.63 | .051 | 4 | 31 | 1.78 | 35 | .01 | 2 | 2.87 | .02 | .10 | 1 | 10 | 40 |
| 1513 G | 4 | 33 | 5 | 106 | 1.0 | 26 | 22 | 1359 | 6.63 | 13 | 5 | ND | 1 | 29 | 1.1 | 3 | 2 | 91 | 1.11 | .056 | 5 | 28 | 1.92 | 31 | .01 | 2 | 2.72 | .01 | .11 | 1 | 5 | 50 |
| 1514 G | 6 | 23 | 26 | 99 | 1.0 | 18 | 24 | 1413 | 6.19 | 21 | 5 | ND | 1 | 49 | .8 | 4 | 2 | 67 | 1.41 | .081 | 6 | 24 | 1.61 | 34 | .01 | 2 | 2.45 | .02 | .13 | 1 | 23 | 40 |
| 1515 G | 4 | 19 | 17 | 104 | .7 | 13 | 14 | 1250 | 6.01 | 34 | 5 | ND | 1 | 50 | .5 | 3 | 2 | 40 | 1.66 | .066 | 6 | 12 | 1.36 | 38 | .01 | 2 | 1.94 | .02 | .14 | 1 | 13 | 60 |
| 1516 G | 1 | 136 | 12 | 52 | 2.1 | 9 | 20 | 3381 | 8.67 | 15 | 5 | ND | 1 | 65 | 1.4 | 2 | 2 | 57 | 4.21 | .156 | 12 | 10 | 2.68 | 20 | .01 | 3 | 2.83 | .03 | .06 | 1 | 27 | 80 |
| 1517 G | 3 | 42 | 16 | 136 | 1.3 | 22 | 24 | 1775 | 7.75 | 29 | 6 | ND | 1 | 46 | 1.3 | 4 | 2 | 62 | 2.04 | .112 | 9 | 15 | 1.69 | 48 | .01 | 5 | 2.69 | .01 | .14 | 2 | 30 | 60 |
| 1518 G | 1 | 30 | 2 | 55 | .6 | 8 | 17 | 2010 | 6.34 | 10 | 5 | ND | 1 | 59 | .2 | 2 | 2 | 56 | 2.54 | .130 | 12 | 12 | 1.53 | 59 | .01 | 2 | 2.44 | .02 | .15 | 1 | 1 | 40 |
| 1519 G | 1 | 17 | 5 | 167 | .2 | 8 | 18 | 1625 | 6.02 | 18 | 5 | ND | 1 | 51 | .9 | 2 | 2 | 51 | 2.82 | .134 | 11 | 11 | 1.15 | 45 | .01 | 3 | 2.34 | .02 | .16 | 1 | 3 | 40 |
| 1520 G | 3 | 18 | 2 | 126 | .2 | 7 | 17 | 1594 | 6.38 | 28 | 5 | ND | 1 | 49 | .9 | 2 | 2 | 50 | 2.92 | .137 | 11 | 12 | 1.13 | 38 | .01 | 2 | 2.48 | .02 | .19 | 1 | 1 | 50 |
| 1521 G | 10 | 21 | 13 | 182 | .4 | 9 | 18 | 1799 | 6.35 | 57 | 5 | ND | 1 | 68 | .7 | 2 | 2 | 53 | 3.53 | .136 | 11 | 11 | 1.15 | 66 | .01 | 2 | 2.52 | .02 | .18 | 1 | 11 | 60 |
| 1522 G | 1 | 12 | 10 | 171 | .3 | 6 | 15 | 1647 | 6.33 | 13 | 5 | ND | 1 | 58 | .9 | 2 | 2 | 52 | 3.50 | .122 | 10 | 9 | 1.16 | 37 | .01 | 2 | 2.41 | .01 | .14 | 1 | 3 | 50 |
| 1523 G | 2 | 13 | 42 | 225 | .3 | 10 | 23 | 1699 | 7.16 | 64 | 8 | ND | 2 | 68 | 1.6 | 2 | 2 | 55 | 3.35 | .126 | 10 | 11 | 1.15 | 45 | .01 | 3 | 2.51 | .02 | .15 | 1 | 13 | 100 |
| 1524 G | 1 | 24 | 9 | 129 | .4 | 8 | 16 | 1817 | 6.83 | 15 | 5 | ND | 1 | 33 | .8 | 2 | 2 | 50 | 2.54 | .118 | 8 | 8 | 1.78 | 36 | .01 | 2 | 2.20 | .02 | .15 | 2 | 3 | 40 |
| 1525 G | 1 | 20 | 2 | 49 | .4 | 4 | 11 | 2587 | 4.86 | 9 | 5 | ND | 1 | 177 | 1.0 | 2 | 2 | 35 | 5.59 | .109 | 7 | 7 | 1.78 | 49 | .01 | 2 | 1.64 | .01 | .14 | 1 | 3 | 30 |
| 1526 G | 1 | 25 | 6 | 34 | .6 | 7 | 17 | 2065 | 6.67 | 10 | 5 | ND | 1 | 36 | .6 | 2 | 2 | 46 | 3.31 | .119 | 9 | 10 | 2.10 | 30 | .01 | 2 | 2.13 | .01 | .14 | 1 | 1 | 20 |
| 1527 G | 3 | 19 | 11 | 99 | .6 | 11 | 18 | 1853 | 6.23 | 21 | 5 | ND | 1 | 72 | .9 | 3 | 2 | 49 | 3.30 | .096 | 8 | 9 | 1.76 | 42 | .01 | 2 | 2.04 | .02 | .14 | 2 | 2 | 30 |
| 1528 G | 7 | 14 | 14 | 65 | .5 | 14 | 15 | 1379 | 5.66 | 15 | 5 | ND | 1 | 34 | .2 | 4 | 2 | 51 | 2.12 | .088 | 7 | 13 | 1.53 | 42 | .01 | 2 | 2.02 | .02 | .17 | 1 | 2 | 20 |
| 1529 G | 1 | 27 | 5 | 69 | .4 | 6 | 17 | 2575 | 7.47 | 28 | 5 | ND | 1 | 55 | .8 | 2 | 2 | 48 | 4.20 | .101 | 8 | 7 | 2.25 | 31 | .01 | 2 | 2.13 | .02 | .12 | 1 | 1 | 90 |
| 1530 G | 2 | 16 | 2 | 210 | .3 | 7 | 12 | 1986 | 5.58 | 17 | 5 | ND | 1 | 59 | 1.2 | 2 | 3 | 48 | 3.47 | .109 | 10 | 9 | 1.99 | 51 | .01 | 2 | 2.09 | .02 | .14 | 1 | 2 | 40 |
| 1531 G | 1 | 18 | 8 | 157 | .6 | 5 | 14 | 1711 | 6.44 | 25 | 5 | ND | 1 | 53 | 1.1 | 3 | 2 | 53 | 3.13 | .108 | 8 | 8 | 1.92 | 31 | .01 | 2 | 2.24 | .02 | .13 | 1 | 1 | 80 |
| 1532 G | 1 | 21 | 2 | 68 | .5 | 4 | 14 | 1475 | 6.20 | 11 | 5 | ND | 1 | 29 | .6 | 2 | 2 | 48 | 2.76 | .111 | 9 | 8 | 1.88 | 38 | .01 | 3 | 2.10 | .02 | .13 | 1 | 1 | 20 |
| 1533 G | 3 | 14 | 3 | 117 | .5 | 12 | 14 | 1849 | 5.39 | 14 | 5 | ND | 1 | 55 | 1.1 | 2 | 2 | 44 | 3.43 | .093 | 9 | 10 | 1.81 | 33 | .01 | 2 | 2.03 | .02 | .15 | 1 | 2 | 40 |
| STANDARD C/AU-R | 19 | 59 | 40 | 130 | 6.9 | 69 | 31 | 1053 | 3.97 | 39 | 20 | 7 | 39 | 55 | 18.9 | 15 | 21 | 56 | .52 | .097 | 39 | 57 | .90 | 181 | .07 | 38 | 1.89 | .06 | .14 | 11 | 487 | 1500 |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AS. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-14 CORE P15 ROCK AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE HA ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: SEP 4 1990 DATE REPORT MAILED: *Sept 12/90* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT UNUK R. PROJECT 134 File # 90-4061 Page 1
 2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | % | ppm | ppb |
| 1537 G | 9 | 65 | 33 | 133 | 1.7 | 27 | 13 | 453 | 5.71 | 56 | 5 | ND | 1 | 23 | .2 | 4 | 2 | 23 | .43 | .050 | 3 | 9 | 1.01 | 39 | .01 | 2 | 1.80 | .01 | .22 | 1 | 13 | 40 |
| 1538 G | 12 | 56 | 24 | 133 | 1.8 | 26 | 11 | 1144 | 4.14 | 34 | 5 | ND | 1 | 35 | .6 | 5 | 2 | 24 | 1.68 | .056 | 6 | 9 | 1.50 | 55 | .01 | 2 | 1.82 | .01 | .19 | 1 | 10 | 80 |
| 1539 G | 12 | 58 | 26 | 137 | 2.2 | 29 | 12 | 529 | 4.98 | 44 | 5 | ND | 1 | 24 | .3 | 6 | 2 | 23 | .50 | .052 | 4 | 9 | 1.11 | 46 | .01 | 2 | 1.79 | .01 | .19 | 1 | 10 | 90 |
| 1540 G | 10 | 64 | 39 | 131 | 2.3 | 25 | 14 | 888 | 5.95 | 83 | 5 | ND | 1 | 36 | .3 | 8 | 2 | 29 | 1.17 | .093 | 5 | 7 | 1.25 | 26 | .01 | 5 | 1.81 | .01 | .18 | 1 | 18 | 80 |
| 1541 G | 2 | 31 | 6 | 84 | .4 | 8 | 17 | 2490 | 6.71 | 20 | 5 | ND | 4 | 41 | .6 | 3 | 3 | 51 | 3.41 | .124 | 9 | 10 | 2.24 | 58 | .01 | 2 | 2.33 | .02 | .13 | 2 | 5 | 70 |
| 1542 G | 3 | 28 | 18 | 196 | 1.3 | 14 | 14 | 1478 | 4.06 | 38 | 5 | ND | 1 | 37 | .8 | 4 | 2 | 24 | 2.16 | .067 | 5 | 8 | 1.37 | 53 | .01 | 2 | 1.51 | .01 | .19 | 1 | 7 | 80 |
| 1545 G | 5 | 19 | 15 | 146 | .7 | 16 | 9 | 1164 | 3.92 | 21 | 5 | ND | 5 | 26 | .4 | 2 | 2 | 20 | 1.77 | .045 | 10 | 9 | 1.50 | 64 | .01 | 2 | 1.66 | .01 | .16 | 2 | 9 | 110 |
| 1546 G | 15 | 57 | 17 | 170 | .6 | 30 | 11 | 712 | 4.55 | 31 | 5 | ND | 6 | 22 | .7 | 4 | 2 | 30 | .72 | .079 | 6 | 11 | 1.21 | 89 | .01 | 2 | 1.90 | .01 | .17 | 4 | 9 | 90 |
| 1547 G | 7 | 33 | 43 | 106 | 2.8 | 31 | 16 | 556 | 4.97 | 73 | 5 | ND | 1 | 27 | .4 | 6 | 2 | 20 | .74 | .049 | 4 | 9 | .71 | 35 | .01 | 5 | 1.30 | .01 | .21 | 1 | 23 | 120 |
| 1548 G | 3 | 40 | 20 | 121 | 1.8 | 16 | 15 | 942 | 4.67 | 33 | 5 | ND | 1 | 23 | .4 | 5 | 4 | 29 | 1.02 | .049 | 6 | 10 | 1.21 | 45 | .01 | 2 | 1.74 | .01 | .16 | 1 | 13 | 100 |
| 1549 G | 3 | 37 | 6 | 130 | 1.6 | 14 | 14 | 1300 | 3.93 | 19 | 5 | ND | 1 | 30 | .5 | 3 | 2 | 31 | 1.63 | .049 | 8 | 12 | 1.44 | 46 | .01 | 4 | 1.77 | .01 | .15 | 1 | 8 | 80 |
| 1550 G | 2 | 35 | 15 | 88 | .2 | 11 | 13 | 1383 | 5.70 | 17 | 5 | ND | 6 | 31 | .5 | 2 | 2 | 51 | 1.74 | .086 | 7 | 14 | 1.70 | 67 | .01 | 2 | 2.29 | .02 | .11 | 4 | 10 | 90 |
| 1551 G | 12 | 57 | 15 | 164 | .6 | 26 | 12 | 580 | 4.96 | 32 | 5 | ND | 5 | 28 | .4 | 4 | 2 | 31 | .63 | .065 | 4 | 12 | 1.17 | 77 | .01 | 5 | 2.00 | .01 | .16 | 3 | 9 | 100 |
| 1552 G | 8 | 42 | 16 | 137 | 1.1 | 19 | 9 | 1007 | 4.10 | 24 | 5 | ND | 1 | 101 | .2 | 4 | 2 | 29 | 2.41 | .059 | 4 | 10 | 1.11 | 40 | .01 | 2 | 1.76 | .02 | .14 | 1 | 10 | 80 |
| 1553 G | 5 | 57 | 17 | 137 | 1.0 | 24 | 12 | 481 | 5.02 | 33 | 5 | ND | 1 | 49 | .6 | 5 | 4 | 27 | 1.21 | .066 | 4 | 10 | .97 | 36 | .01 | 2 | 2.01 | .01 | .22 | 1 | 8 | 110 |
| 1554 G | 4 | 50 | 26 | 125 | .3 | 22 | 11 | 569 | 5.46 | 38 | 5 | ND | 5 | 58 | .3 | 4 | 2 | 26 | 1.83 | .114 | 5 | 11 | .94 | 76 | .01 | 3 | 1.90 | .01 | .18 | 2 | 8 | 90 |
| 1555 G | 4 | 38 | 15 | 114 | .9 | 25 | 10 | 654 | 4.77 | 39 | 5 | ND | 1 | 66 | .2 | 4 | 3 | 26 | 2.34 | .105 | 6 | 12 | .90 | 65 | .01 | 3 | 1.82 | .01 | .20 | 1 | 5 | 120 |
| 1556 G | 6 | 51 | 23 | 144 | 1.0 | 21 | 10 | 504 | 4.49 | 32 | 5 | ND | 1 | 54 | .5 | 4 | 2 | 23 | 1.57 | .069 | 4 | 8 | .90 | 70 | .01 | 2 | 1.77 | .01 | .19 | 1 | 5 | 100 |
| 1557 G | 6 | 32 | 15 | 90 | .7 | 20 | 9 | 588 | 3.75 | 27 | 5 | ND | 1 | 62 | .3 | 5 | 2 | 22 | 2.14 | .072 | 5 | 9 | .80 | 74 | .01 | 2 | 1.63 | .02 | .19 | 1 | 7 | 90 |
| 1558 G | 5 | 58 | 24 | 165 | .9 | 21 | 10 | 891 | 4.90 | 38 | 5 | ND | 1 | 74 | .4 | 3 | 5 | 23 | 2.54 | .064 | 5 | 8 | 1.09 | 51 | .01 | 3 | 1.82 | .01 | .21 | 1 | 7 | 120 |
| 1559 G | 5 | 43 | 22 | 110 | .8 | 21 | 11 | 538 | 4.70 | 31 | 5 | ND | 1 | 55 | .5 | 3 | 2 | 24 | 1.60 | .071 | 5 | 9 | .93 | 54 | .01 | 4 | 1.88 | .01 | .23 | 1 | 8 | 100 |
| 1560 G | 6 | 42 | 18 | 109 | .8 | 23 | 11 | 370 | 4.58 | 31 | 5 | ND | 1 | 42 | .2 | 4 | 3 | 22 | .77 | .070 | 4 | 9 | .88 | 65 | .01 | 3 | 1.76 | .01 | .19 | 1 | 4 | 80 |
| 1561 G | 8 | 54 | 22 | 145 | 1.0 | 25 | 12 | 332 | 5.13 | 34 | 5 | ND | 1 | 40 | .8 | 4 | 2 | 23 | .71 | .068 | 4 | 9 | .88 | 44 | .01 | 2 | 1.83 | .01 | .22 | 1 | 8 | 70 |
| 1562 G | 7 | 56 | 18 | 133 | 1.0 | 22 | 12 | 374 | 4.93 | 31 | 5 | ND | 1 | 43 | .4 | 4 | 3 | 26 | .96 | .065 | 4 | 10 | .83 | 56 | .01 | 4 | 1.71 | .01 | .16 | 1 | 7 | 50 |
| 1563 G | 7 | 59 | 26 | 89 | 1.2 | 25 | 11 | 671 | 5.15 | 38 | 5 | ND | 1 | 107 | .4 | 3 | 8 | 25 | 1.85 | .060 | 3 | 10 | .85 | 64 | .01 | 2 | 1.78 | .01 | .21 | 1 | 11 | 60 |
| 1564 G | 5 | 63 | 14 | 168 | 1.1 | 23 | 12 | 385 | 5.05 | 31 | 5 | ND | 1 | 60 | .2 | 3 | 2 | 24 | .81 | .064 | 4 | 9 | .85 | 61 | .01 | 6 | 1.85 | .01 | .21 | 1 | 4 | 80 |
| 1565 G | 9 | 43 | 14 | 228 | 1.0 | 28 | 14 | 611 | 5.46 | 28 | 5 | ND | 1 | 79 | 1.4 | 2 | 2 | 35 | 2.38 | .084 | 6 | 10 | .94 | 63 | .01 | 4 | 2.04 | .01 | .19 | 1 | 8 | 130 |
| 1566 G | 8 | 42 | 11 | 208 | .2 | 23 | 14 | 682 | 4.96 | 26 | 5 | ND | 6 | 85 | 1.0 | 5 | 2 | 32 | 2.91 | .069 | 7 | 7 | .89 | 75 | .01 | 7 | 1.81 | .01 | .14 | 2 | 9 | 120 |
| 2033 G | 7 | 11 | 29 | 345 | 2.3 | 10 | 8 | 1951 | 5.18 | 424 | 5 | ND | 1 | 142 | 1.4 | 12 | 2 | 19 | 3.17 | .106 | 8 | 6 | .74 | 46 | .01 | 2 | 1.17 | .01 | .12 | 1 | 43 | 510 |
| 2034 G | 4 | 4 | 11 | 125 | .8 | 1 | 9 | 1607 | 5.14 | 14 | 5 | ND | 1 | 40 | .2 | 3 | 2 | 31 | 1.30 | .136 | 13 | 2 | 1.02 | 62 | .01 | 5 | 1.90 | .02 | .12 | 1 | 6 | 220 |
| 2035 G | 4 | 4 | 11 | 110 | 2.1 | 6 | 8 | 4949 | 4.30 | 81 | 5 | ND | 1 | 30 | .2 | 8 | 2 | 13 | 1.68 | .126 | 11 | 4 | .66 | 55 | .01 | 2 | .92 | .01 | .19 | 1 | 32 | 350 |
| 2036 G | 4 | 12 | 43 | 115 | 4.8 | 4 | 9 | 1940 | 5.76 | 105 | 5 | ND | 4 | 57 | .5 | 14 | 2 | 10 | 1.68 | .120 | 9 | 2 | .47 | 44 | .01 | 5 | .66 | .01 | .14 | 2 | 79 | 620 |
| 2037 G | 6 | 12 | 49 | 148 | 7.3 | 6 | 10 | 978 | 7.47 | 207 | 5 | ND | 4 | 38 | .5 | 21 | 2 | 5 | 1.42 | .112 | 8 | 5 | .49 | 43 | .01 | 3 | .51 | .01 | .18 | 3 | 177 | 660 |
| 2038 G | 6 | 9 | 24 | 136 | 2.1 | 1 | 8 | 2721 | 3.31 | 280 | 5 | ND | 6 | 52 | .5 | 14 | 2 | 10 | 2.66 | .098 | 9 | 2 | 1.01 | 79 | .01 | 6 | .57 | .01 | .14 | 3 | 115 | 430 |
| STANDARD C/AU-R | 19 | 57 | 37 | 131 | 6.7 | 70 | 31 | 1049 | 3.95 | 41 | 23 | 7 | 38 | 52 | 19.6 | 15 | 21 | 55 | .51 | .092 | 37 | 55 | .91 | 180 | .07 | 37 | 1.89 | .06 | .14 | 13 | 484 | 1300 |

FP 7

FP 9

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1 CORE P2-4 ROCK AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: SEP 1 1990 DATE REPORT MAILED: Sept 5/90 SIGNED BY: *C. Leung* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| 1534 G | 1 | 22 | 12 | 89 | .6 | 5 | 11 | 1854 | 5.73 | 9 | 5 | ND | 1 | 42 | .2 | 5 | 2 | 42 | 2.77 | .088 | 9 | 15 | 1.71 | 28 | .01 | 3 | 1.90 | .02 | .13 | 1 | 3 | 80 |
| 1535 G | 5 | 44 | 15 | 155 | 1.4 | 14 | 11 | 1483 | 5.39 | 11 | 5 | ND | 1 | 42 | .2 | 5 | 2 | 37 | 2.21 | .076 | 7 | 12 | 1.54 | 56 | .01 | 4 | 1.94 | .01 | .16 | 1 | 6 | 70 |
| 1536 G | 6 | 73 | 18 | 152 | 2.1 | 22 | 12 | 726 | 5.04 | 37 | 5 | ND | 1 | 48 | .2 | 3 | 2 | 25 | .98 | .053 | 4 | 13 | 1.13 | 51 | .01 | 8 | 1.88 | .01 | .22 | 1 | 8 | 60 |
| 1543 G | 1 | 17 | 12 | 75 | 1.1 | 7 | 6 | 4106 | 4.12 | 33 | 5 | ND | 1 | 100 | .2 | 6 | 2 | 12 | 6.40 | .040 | 7 | 8 | 2.74 | 35 | .01 | 6 | 1.00 | .01 | .15 | 1 | 7 | 50 |
| 1544 G | 2 | 38 | 26 | 107 | 2.0 | 12 | 9 | 943 | 4.94 | 44 | 5 | ND | 1 | 24 | .2 | 4 | 2 | 25 | .90 | .070 | 5 | 14 | 1.27 | 54 | .01 | 6 | 1.90 | .01 | .20 | 3 | 17 | 100 |
| 1567 G | 10 | 35 | 15 | 120 | .7 | 23 | 10 | 509 | 4.22 | 22 | 5 | ND | 1 | 82 | .2 | 3 | 2 | 24 | 2.10 | .102 | 6 | 13 | .80 | 59 | .01 | 6 | 1.72 | .01 | .16 | 1 | 5 | 90 |
| 1568 G | 9 | 40 | 21 | 135 | .9 | 27 | 11 | 479 | 4.32 | 28 | 5 | ND | 1 | 88 | .2 | 6 | 2 | 21 | 1.87 | .099 | 5 | 13 | .75 | 64 | .01 | 6 | 1.66 | .01 | .18 | 1 | 7 | 100 |
| 1569 G | 9 | 35 | 17 | 114 | .7 | 24 | 8 | 438 | 4.68 | 34 | 5 | ND | 1 | 84 | .2 | 2 | 2 | 13 | 2.43 | .083 | 7 | 10 | .61 | 45 | .01 | 7 | 1.36 | .01 | .16 | 1 | 4 | 80 |
| 1570 G | 10 | 37 | 17 | 106 | .7 | 26 | 10 | 313 | 3.73 | 24 | 5 | ND | 1 | 56 | .2 | 4 | 2 | 20 | 1.19 | .113 | 5 | 13 | .70 | 65 | .01 | 7 | 1.58 | .01 | .19 | 1 | 14 | 90 |
| 1571 G | 3 | 12 | 9 | 180 | .3 | 5 | 8 | 1249 | 5.26 | 4 | 5 | ND | 1 | 101 | .2 | 2 | 2 | 72 | 4.62 | .160 | 8 | 9 | .74 | 22 | .01 | 3 | 1.98 | .03 | .07 | 1 | 2 | 80 |
| 1572 G | 1 | 15 | 8 | 107 | .2 | 7 | 11 | 1069 | 6.80 | 8 | 5 | ND | 1 | 80 | .2 | 3 | 2 | 83 | 3.34 | .154 | 8 | 15 | .97 | 25 | .01 | 5 | 2.54 | .03 | .06 | 1 | 1 | 40 |
| 1573 G | 2 | 37 | 4 | 155 | .4 | 7 | 9 | 1102 | 5.36 | 9 | 5 | ND | 1 | 75 | .2 | 3 | 2 | 49 | 3.75 | .100 | 7 | 12 | .79 | 30 | .01 | 3 | 2.07 | .02 | .09 | 1 | 1 | 50 |
| 1574 G | 3 | 9 | 9 | 119 | .5 | 5 | 9 | 549 | 4.13 | 18 | 5 | ND | 1 | 62 | .2 | 2 | 2 | 11 | 1.61 | .053 | 5 | 6 | .58 | 78 | .01 | 3 | 1.54 | .01 | .13 | 1 | 3 | 50 |
| 1575 G | 5 | 7 | 5 | 122 | .3 | 9 | 10 | 738 | 4.76 | 13 | 5 | ND | 1 | 54 | .2 | 2 | 2 | 26 | 2.50 | .112 | 7 | 10 | .78 | 156 | .01 | 5 | 1.89 | .02 | .12 | 1 | 3 | 40 |
| 1576 G | 3 | 44 | 18 | 174 | 1.4 | 17 | 14 | 1067 | 7.14 | 62 | 5 | ND | 1 | 100 | .2 | 2 | 2 | 54 | 2.93 | .082 | 5 | 31 | .76 | 32 | .01 | 5 | 1.90 | .02 | .11 | 1 | 7 | 110 |
| 1577 G | 4 | 20 | 8 | 144 | .7 | 9 | 7 | 521 | 2.86 | 12 | 5 | ND | 1 | 57 | .2 | 2 | 2 | 5 | 1.37 | .034 | 8 | 6 | .45 | 44 | .01 | 4 | 1.16 | .01 | .14 | 1 | 1 | 70 |
| 1578 G | 6 | 26 | 21 | 177 | 1.4 | 19 | 11 | 489 | 3.43 | 39 | 6 | ND | 1 | 50 | .4 | 2 | 3 | 14 | 1.28 | .059 | 6 | 8 | .49 | 55 | .01 | 4 | 1.27 | .01 | .16 | 1 | 13 | 90 |
| 1579 G | 22 | 27 | 24 | 142 | 2.0 | 19 | 13 | 1019 | 4.94 | 45 | 5 | ND | 1 | 62 | .4 | 5 | 4 | 26 | 2.55 | .065 | 6 | 14 | .86 | 45 | .01 | 8 | 1.64 | .02 | .14 | 1 | 6 | 100 |
| 1580 G | 5 | 26 | 12 | 177 | 1.1 | 20 | 13 | 1269 | 4.41 | 25 | 5 | ND | 1 | 212 | .6 | 3 | 5 | 27 | 4.90 | .065 | 5 | 17 | .70 | 132 | .01 | 6 | 1.68 | .02 | .16 | 1 | 3 | 110 |
| 1581 G | 12 | 33 | 5 | 114 | .8 | 16 | 13 | 1612 | 4.73 | 21 | 5 | ND | 1 | 93 | .2 | 2 | 2 | 33 | 4.41 | .049 | 9 | 14 | .61 | 30 | .01 | 4 | 1.78 | .02 | .08 | 1 | 3 | 80 |
| 1582 G | 20 | 37 | 7 | 97 | .8 | 26 | 18 | 1156 | 4.64 | 31 | 5 | ND | 1 | 71 | .2 | 3 | 2 | 31 | 2.99 | .046 | 9 | 16 | .62 | 122 | .01 | 3 | 1.80 | .02 | .12 | 1 | 2 | 70 |
| 1583 G | 15 | 30 | 5 | 234 | 1.0 | 22 | 14 | 1032 | 5.24 | 29 | 5 | ND | 1 | 106 | .2 | 3 | 2 | 28 | 2.71 | .061 | 8 | 15 | .75 | 205 | .01 | 3 | 1.68 | .02 | .10 | 1 | 3 | 80 |
| 1584 G | 6 | 30 | 18 | 179 | 1.3 | 18 | 11 | 773 | 5.28 | 52 | 5 | ND | 1 | 51 | .2 | 3 | 3 | 18 | 1.29 | .059 | 6 | 12 | .69 | 67 | .01 | 5 | 1.14 | .02 | .15 | 1 | 4 | 100 |
| 1585 G | 3 | 44 | 32 | 185 | 2.8 | 15 | 9 | 435 | 4.05 | 46 | 5 | ND | 1 | 63 | .2 | 4 | 5 | 10 | .50 | .059 | 4 | 6 | .58 | 65 | .01 | 4 | .44 | .01 | .20 | 1 | 8 | 120 |
| 1586 G | 3 | 56 | 45 | 125 | 4.2 | 19 | 11 | 651 | 4.50 | 53 | 5 | ND | 1 | 126 | .2 | 4 | 2 | 11 | 1.69 | .062 | 3 | 8 | .65 | 57 | .01 | 6 | .53 | .01 | .23 | 1 | 19 | 150 |
| 1587 G | 2 | 54 | 45 | 131 | 4.9 | 17 | 10 | 423 | 4.78 | 46 | 5 | ND | 1 | 77 | .2 | 4 | 2 | 12 | .56 | .062 | 4 | 8 | .69 | 56 | .01 | 6 | .47 | .01 | .22 | 1 | 23 | 160 |
| 1588 G | 4 | 56 | 39 | 151 | 4.4 | 20 | 11 | 517 | 4.90 | 80 | 5 | ND | 1 | 72 | .2 | 5 | 4 | 14 | .73 | .083 | 4 | 8 | .67 | 54 | .01 | 6 | .54 | .01 | .24 | 1 | 16 | 190 |
| 1589 G | 3 | 64 | 41 | 167 | 2.9 | 20 | 11 | 602 | 5.88 | 129 | 5 | ND | 1 | 90 | .3 | 4 | 2 | 13 | .79 | .087 | 4 | 9 | .71 | 50 | .01 | 6 | .58 | .01 | .25 | 1 | 21 | 150 |
| 1590 G | 4 | 52 | 30 | 262 | 2.5 | 22 | 10 | 384 | 3.52 | 75 | 6 | ND | 1 | 70 | .2 | 3 | 2 | 8 | .59 | .068 | 4 | 5 | .42 | 48 | .01 | 5 | .51 | .01 | .21 | 1 | 15 | 170 |
| 1591 G | 5 | 18 | 4 | 304 | .4 | 3 | 2 | 705 | 3.20 | 10 | 5 | ND | 1 | 143 | .6 | 2 | 2 | 5 | 2.37 | .028 | 10 | 2 | .33 | 75 | .01 | 5 | .32 | .02 | .14 | 1 | 4 | 130 |
| 1592 G | 5 | 12 | 8 | 108 | .8 | 10 | 2 | 293 | 2.37 | 40 | 7 | ND | 1 | 48 | .2 | 2 | 3 | 1 | .90 | .016 | 11 | 8 | .16 | 56 | .01 | 4 | .37 | .02 | .20 | 1 | 11 | 70 |
| 1593 G | 3 | 9 | 9 | 96 | .5 | 2 | 1 | 292 | 2.61 | 43 | 6 | ND | 1 | 44 | .5 | 2 | 2 | 1 | .88 | .014 | 9 | 1 | .14 | 49 | .01 | 5 | .27 | .02 | .17 | 1 | 31 | 50 |
| 1594 G | 4 | 8 | 5 | 97 | .3 | 5 | 1 | 563 | 2.94 | 4 | 5 | ND | 1 | 39 | .4 | 2 | 3 | 1 | 1.64 | .013 | 9 | 5 | .21 | 47 | .01 | 3 | .48 | .02 | .16 | 1 | 6 | 60 |
| 1595 G | 2 | 7 | 2 | 104 | .2 | 2 | 3 | 546 | 1.87 | 2 | 5 | ND | 2 | 60 | .3 | 2 | 3 | 1 | 1.69 | .008 | 17 | 3 | .16 | 46 | .01 | 2 | .58 | .02 | .13 | 1 | 2 | 40 |
| 1596 G | 3 | 24 | 14 | 111 | 1.0 | 12 | 13 | 1030 | 6.11 | 13 | 5 | ND | 1 | 66 | .2 | 3 | 3 | 39 | 2.18 | .079 | 7 | 16 | .70 | 42 | .01 | 5 | 1.72 | .02 | .14 | 1 | 9 | 60 |
| 1597 G | 5 | 21 | 19 | 247 | 1.0 | 9 | 10 | 1557 | 5.81 | 10 | 5 | ND | 1 | 156 | .5 | 2 | 2 | 30 | 4.13 | .090 | 7 | 11 | .70 | 36 | .01 | 5 | 1.52 | .01 | .15 | 1 | 9 | 120 |
| STANDARD C/AU-R | 19 | 61 | 41 | 131 | 7.0 | 72 | 31 | 1051 | 3.97 | 40 | 15 | 7 | 37 | 53 | 18.8 | 15 | 20 | 55 | .50 | .094 | 38 | 60 | .88 | 180 | .07 | 38 | 1.90 | .06 | .14 | 11 | 484 | 1500 |

AP 7

3P7

FP 8

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | AU ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | AU** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1598 G | 3 | 11 | 15 | 184 | .6 | 3 | 5 | 458 | 4.60 | 25 | 5 | ND | 1 | 32 | .5 | 2 | 5 | 7 | .81 | .032 | 9 | 2 | .31 | 63 | .01 | 2 | .98 | .04 | .24 | 1 | 19 | 60 |
| 1599 G | 9 | 5 | 9 | 74 | .4 | 8 | 11 | 949 | 5.31 | 12 | 5 | ND | 1 | 38 | .7 | 2 | 4 | 31 | 1.54 | .137 | 13 | 4 | 1.00 | 22 | .01 | 2 | 1.64 | .03 | .18 | 1 | 3 | 110 |
| 1600 G | 1 | 8 | 6 | 48 | .1 | 4 | 7 | 466 | 3.44 | 6 | 5 | ND | 2 | 23 | .4 | 2 | 2 | 18 | .77 | .068 | 21 | 2 | .50 | 47 | .01 | 2 | 1.08 | .04 | .16 | 1 | 2 | 130 |
| 1601 G | 3 | 10 | 4 | 89 | .1 | 7 | 10 | 985 | 4.93 | 8 | 5 | ND | 1 | 36 | .2 | 2 | 2 | 29 | 1.60 | .133 | 16 | 5 | .97 | 52 | .01 | 5 | 1.54 | .03 | .20 | 1 | 3 | 180 |
| 1602 G | 2 | 5 | 12 | 121 | .1 | 4 | 10 | 1063 | 5.10 | 10 | 5 | ND | 1 | 35 | .3 | 2 | 2 | 30 | 1.65 | .133 | 14 | 2 | 1.02 | 43 | .01 | 2 | 1.55 | .03 | .20 | 1 | 1 | 430 |
| 1603 G | 2 | 6 | 6 | 77 | .3 | 5 | 10 | 975 | 4.89 | 6 | 5 | ND | 1 | 39 | .7 | 2 | 2 | 27 | 1.56 | .141 | 12 | 4 | .95 | 35 | .01 | 2 | 1.42 | .03 | .19 | 1 | 1 | 130 |
| 1604 G | 2 | 7 | 2 | 82 | .2 | 3 | 9 | 1072 | 5.17 | 6 | 5 | ND | 2 | 33 | .5 | 2 | 5 | 27 | 1.56 | .109 | 17 | 2 | 1.01 | 39 | .01 | 2 | 1.40 | .03 | .18 | 1 | 2 | 160 |
| 1605 G | 6 | 7 | 22 | 76 | .4 | 6 | 10 | 1631 | 4.86 | 8 | 5 | ND | 1 | 45 | .7 | 2 | 2 | 26 | 2.96 | .128 | 11 | 3 | 1.21 | 39 | .01 | 5 | 1.12 | .02 | .18 | 1 | 3 | 200 |
| 1606 G | 3 | 6 | 13 | 106 | .1 | 4 | 10 | 1093 | 5.02 | 11 | 5 | ND | 1 | 34 | .2 | 2 | 2 | 23 | 1.26 | .137 | 17 | 1 | .49 | 67 | .01 | 3 | .76 | .02 | .22 | 1 | 1 | 270 |
| 1607 G | 3 | 6 | 16 | 77 | .3 | 6 | 10 | 1133 | 5.43 | 10 | 5 | ND | 1 | 40 | .6 | 2 | 2 | 27 | 1.72 | .141 | 15 | 3 | .96 | 45 | .01 | 3 | 1.22 | .03 | .20 | 1 | 2 | 200 |
| 1608 G | 1 | 6 | 2 | 114 | .1 | 2 | 8 | 823 | 4.66 | 6 | 5 | ND | 1 | 33 | .5 | 2 | 2 | 23 | 1.32 | .134 | 16 | 2 | .73 | 42 | .01 | 2 | 1.29 | .03 | .20 | 1 | 1 | 240 |
| 1609 G | 3 | 12 | 7 | 88 | .1 | 6 | 7 | 702 | 4.25 | 10 | 5 | ND | 1 | 32 | .2 | 2 | 2 | 18 | 1.16 | .112 | 17 | 4 | .58 | 41 | .01 | 5 | 1.04 | .02 | .21 | 1 | 2 | 160 |
| 1610 G | 2 | 8 | 7 | 83 | .3 | 3 | 7 | 563 | 3.50 | 9 | 5 | ND | 2 | 23 | .2 | 2 | 3 | 9 | .95 | .071 | 21 | 2 | .27 | 62 | .01 | 2 | .72 | .01 | .22 | 1 | 2 | 190 |
| 1611 G | 4 | 6 | 9 | 74 | .2 | 5 | 5 | 527 | 3.12 | 8 | 5 | ND | 2 | 20 | .2 | 2 | 2 | 11 | .84 | .070 | 22 | 3 | .15 | 69 | .01 | 3 | .55 | .01 | .21 | 1 | 1 | 200 |
| 1612 G | 5 | 7 | 8 | 64 | .2 | 5 | 4 | 492 | 2.41 | 6 | 5 | ND | 3 | 8 | .2 | 2 | 2 | 3 | .34 | .021 | 31 | 1 | .08 | 84 | .01 | 2 | .61 | .02 | .29 | 1 | 1 | 180 |
| 1613 G | 6 | 9 | 10 | 102 | .2 | 6 | 6 | 444 | 2.88 | 3 | 5 | ND | 1 | 25 | .3 | 2 | 3 | 10 | .89 | .089 | 18 | 6 | .44 | 41 | .01 | 2 | .74 | .03 | .17 | 1 | 1 | 150 |
| 1614 G | 2 | 9 | 14 | 113 | .1 | 4 | 6 | 329 | 3.19 | 5 | 5 | ND | 2 | 22 | .3 | 2 | 2 | 10 | .60 | .079 | 20 | 2 | .39 | 52 | .01 | 2 | .97 | .04 | .25 | 1 | 2 | 160 |
| 1615 G | 8 | 13 | 8 | 101 | .1 | 9 | 5 | 366 | 2.37 | 4 | 5 | ND | 1 | 23 | .2 | 2 | 3 | 9 | .47 | .078 | 23 | 7 | .17 | 179 | .01 | 3 | .56 | .03 | .17 | 3 | 2 | 220 |
| 1616 G | 4 | 6 | 14 | 89 | .2 | 4 | 4 | 806 | 2.71 | 3 | 5 | ND | 1 | 23 | .4 | 2 | 2 | 4 | 1.59 | .032 | 32 | 2 | .72 | 47 | .01 | 4 | .54 | .02 | .22 | 1 | 2 | 150 |
| 1617 G | 5 | 5 | 10 | 162 | .1 | 9 | 4 | 488 | 2.76 | 3 | 5 | ND | 1 | 15 | .5 | 2 | 2 | 3 | .82 | .027 | 22 | 7 | .46 | 49 | .01 | 2 | .67 | .03 | .20 | 1 | 1 | 260 |
| 1618 G | 3 | 7 | 10 | 124 | .2 | 4 | 2 | 536 | 1.69 | 2 | 5 | ND | 2 | 14 | .2 | 2 | 2 | 2 | 1.01 | .030 | 25 | 2 | .30 | 53 | .01 | 2 | .34 | .03 | .16 | 1 | 39 | 250 |
| 1619 G | 6 | 6 | 8 | 70 | .2 | 10 | 2 | 247 | 1.09 | 4 | 5 | ND | 2 | 7 | .2 | 3 | 2 | 1 | .38 | .012 | 22 | 7 | .07 | 62 | .01 | 3 | .25 | .04 | .14 | 1 | 2 | 180 |
| 1620 G | 4 | 4 | 8 | 55 | .1 | 4 | 2 | 550 | 2.36 | 3 | 5 | ND | 1 | 14 | .4 | 2 | 2 | 1 | .97 | .003 | 17 | 2 | .45 | 47 | .01 | 2 | .37 | .03 | .16 | 1 | 5 | 210 |
| 1621 G | 5 | 5 | 13 | 62 | .1 | 10 | 1 | 348 | 1.28 | 3 | 5 | ND | 1 | 5 | .3 | 2 | 2 | 1 | .31 | .004 | 21 | 6 | .06 | 66 | .01 | 3 | .33 | .03 | .12 | 1 | 2 | 180 |
| 1622 G | 5 | 6 | 12 | 78 | .3 | 4 | 2 | 467 | 2.16 | 6 | 7 | ND | 1 | 14 | .2 | 2 | 2 | 1 | .76 | .013 | 19 | 2 | .35 | 58 | .01 | 3 | .35 | .03 | .14 | 1 | 2 | 220 |
| 1623 G | 7 | 4 | 21 | 68 | .1 | 13 | 1 | 258 | 1.58 | 4 | 5 | ND | 1 | 6 | .2 | 2 | 2 | 1 | .22 | .005 | 20 | 10 | .09 | 60 | .01 | 2 | .26 | .04 | .14 | 1 | 4 | 190 |
| 1624 G | 4 | 3 | 6 | 64 | .1 | 2 | 2 | 387 | 1.69 | 2 | 5 | ND | 1 | 8 | .2 | 2 | 2 | 1 | .52 | .004 | 22 | 3 | .18 | 100 | .01 | 2 | .22 | .03 | .15 | 1 | 3 | 180 |
| 1625 G | 6 | 5 | 10 | 74 | .1 | 12 | 1 | 249 | 1.34 | 3 | 5 | ND | 1 | 5 | .3 | 2 | 2 | 1 | .27 | .003 | 19 | 8 | .12 | 46 | .01 | 2 | .30 | .04 | .14 | 1 | 1 | 200 |
| 1626 G | 6 | 7 | 14 | 153 | .1 | 4 | 2 | 479 | 1.39 | 5 | 5 | ND | 2 | 10 | .5 | 3 | 2 | 1 | .85 | .002 | 24 | 3 | .26 | 52 | .01 | 6 | .26 | .01 | .19 | 1 | 1 | 380 |
| 1627 G | 5 | 8 | 10 | 69 | .1 | 11 | 2 | 210 | 1.27 | 5 | 5 | ND | 3 | 4 | .2 | 2 | 2 | 2 | .34 | .004 | 22 | 9 | .10 | 42 | .01 | 5 | .35 | .01 | .22 | 1 | 3 | 160 |
| 1628 G | 4 | 9 | 17 | 100 | .1 | 5 | 5 | 239 | 2.14 | 4 | 5 | ND | 5 | 6 | .4 | 2 | 4 | 5 | .11 | .026 | 32 | 2 | .05 | 48 | .01 | 3 | .42 | .01 | .19 | 1 | 3 | 230 |
| 1629 G | 4 | 9 | 11 | 107 | .1 | 10 | 3 | 238 | 1.50 | 7 | 5 | ND | 4 | 5 | .2 | 2 | 2 | 5 | .12 | .024 | 24 | 7 | .04 | 48 | .01 | 2 | .36 | .02 | .16 | 1 | 2 | 280 |
| 1630 G | 3 | 9 | 19 | 77 | .3 | 4 | 2 | 497 | 1.19 | 4 | 7 | ND | 4 | 9 | .2 | 2 | 2 | 1 | 1.02 | .004 | 25 | 2 | .15 | 51 | .01 | 2 | .26 | .01 | .15 | 1 | 6 | 220 |
| 1631 G | 4 | 4 | 18 | 50 | .2 | 8 | 2 | 436 | 1.09 | 2 | 5 | ND | 5 | 5 | .2 | 2 | 2 | 1 | .36 | .006 | 28 | 6 | .12 | 52 | .01 | 2 | .32 | .01 | .16 | 1 | 1 | 240 |
| 1632 G | 1 | 7 | 16 | 59 | .1 | 4 | 1 | 237 | .95 | 4 | 5 | ND | 5 | 4 | .3 | 2 | 2 | 1 | .20 | .005 | 29 | 2 | .04 | 51 | .01 | 2 | .22 | .02 | .13 | 1 | 1 | 270 |
| 1633 G | 3 | 4 | 17 | 47 | .1 | 10 | 2 | 280 | 1.09 | 4 | 5 | ND | 6 | 4 | .2 | 2 | 2 | 1 | .14 | .004 | 31 | 7 | .03 | 46 | .01 | 2 | .29 | .02 | .16 | 1 | 1 | 230 |
| STANDARD C/AU-R | 19 | 59 | 37 | 134 | 7.1 | 73 | 32 | 1054 | 3.97 | 40 | 21 | 7 | 39 | 52 | 19.1 | 15 | 20 | 58 | .52 | .096 | 39 | 59 | .90 | 183 | .08 | 38 | 1.89 | .06 | .14 | 11 | 483 | 1500 |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | AU** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | ppm | ppb | ppb | |
| 1634 G | 1 | 2 | 9 | 30 | .2 | 1 | 2 | 294 | .73 | 3 | 5 | ND | 6 | 2 | .2 | 2 | 3 | 1 | .15 | .003 | 26 | 1 | .03 | 43 | .01 | 3 | .24 | .02 | .14 | 1 | 6 | 130 |
| 1635 G | 3 | 4 | 18 | 60 | .1 | 1 | 2 | 267 | 1.19 | 3 | 5 | ND | 5 | 4 | .4 | 2 | 3 | 1 | .20 | .005 | 24 | 1 | .08 | 49 | .01 | 2 | .24 | .03 | .11 | 1 | 3 | 170 |
| 1636 G | 5 | 4 | 20 | 29 | .2 | 7 | 1 | 247 | .72 | 7 | 5 | ND | 4 | 3 | .2 | 2 | 4 | 1 | .26 | .004 | 25 | 6 | .07 | 49 | .01 | 2 | .18 | .02 | .11 | 1 | 4 | 100 |
| 1637 G | 4 | 4 | 23 | 19 | .2 | 5 | 2 | 119 | .88 | 6 | 5 | ND | 5 | 3 | .2 | 2 | 2 | 1 | .08 | .007 | 28 | 6 | .03 | 50 | .01 | 2 | .17 | .02 | .11 | 1 | 1 | 50 |
| 1638 G | 10 | 5 | 21 | 74 | .4 | 2 | 3 | 334 | 1.89 | 7 | 5 | ND | 5 | 4 | .4 | 2 | 2 | 3 | .13 | .007 | 25 | 2 | .09 | 59 | .01 | 2 | .37 | .02 | .12 | 1 | 2 | 120 |
| 1639 G | 3 | 3 | 11 | 74 | .2 | 5 | 3 | 535 | 1.42 | 7 | 5 | ND | 4 | 9 | .2 | 2 | 6 | 1 | .98 | .007 | 23 | 4 | .35 | 29 | .01 | 3 | .22 | .01 | .13 | 1 | 2 | 130 |
| 1640 G | 1 | 2 | 25 | 43 | .2 | 1 | 2 | 746 | 1.19 | 8 | 5 | ND | 4 | 32 | .2 | 2 | 2 | 1 | 1.69 | .006 | 21 | 2 | .46 | 84 | .01 | 2 | .19 | .02 | .12 | 1 | 1 | 100 |
| 1641 G | 13 | 18 | 27 | 180 | .7 | 4 | 7 | 133 | 3.06 | 8 | 5 | ND | 3 | 8 | .2 | 4 | 2 | 4 | .13 | .023 | 17 | 3 | .06 | 50 | .01 | 3 | .43 | .01 | .22 | 1 | 3 | 380 |
| 1642 G | 1 | 4 | 8 | 29 | .1 | 2 | 1 | 134 | 1.04 | 2 | 5 | ND | 5 | 5 | .3 | 2 | 2 | 1 | .23 | .003 | 25 | 2 | .07 | 43 | .01 | 2 | .21 | .02 | .15 | 1 | 5 | 160 |
| 1643 G | 4 | 2 | 2 | 17 | .1 | 6 | 2 | 122 | 1.37 | 7 | 5 | ND | 4 | 6 | .2 | 2 | 2 | 1 | .12 | .004 | 23 | 6 | .10 | 54 | .01 | 3 | .21 | .02 | .14 | 1 | 1 | 190 |
| 1644 G | 3 | 4 | 11 | 62 | .2 | 2 | 2 | 137 | 1.16 | 3 | 5 | ND | 4 | 5 | .4 | 2 | 2 | 1 | .07 | .005 | 24 | 2 | .04 | 49 | .01 | 3 | .29 | .02 | .16 | 1 | 6 | 250 |
| 1645 G | 6 | 9 | 21 | 20 | .2 | 3 | 2 | 183 | .98 | 4 | 5 | ND | 4 | 4 | .2 | 2 | 2 | 1 | .32 | .004 | 25 | 4 | .08 | 47 | .01 | 2 | .23 | .01 | .11 | 1 | 7 | 180 |
| 1646 G | 2 | 8 | 16 | 25 | .3 | 1 | 2 | 117 | 1.13 | 2 | 5 | ND | 5 | 8 | .2 | 2 | 2 | 1 | .10 | .003 | 24 | 1 | .06 | 52 | .01 | 3 | .24 | .02 | .15 | 1 | 1 | 160 |
| 1647 G | 5 | 2 | 15 | 22 | .3 | 5 | 2 | 865 | 1.56 | 2 | 5 | ND | 5 | 16 | .2 | 2 | 2 | 1 | 1.43 | .006 | 26 | 4 | .63 | 39 | .01 | 3 | .32 | .02 | .13 | 1 | 5 | 140 |
| 1648 G | 3 | 3 | 12 | 24 | .2 | 1 | 2 | 575 | 1.87 | 4 | 5 | ND | 6 | 12 | .2 | 2 | 2 | 1 | .92 | .004 | 28 | 1 | .50 | 35 | .01 | 3 | .34 | .02 | .15 | 1 | 22 | 80 |
| 1649 G | 4 | 2 | 12 | 18 | .2 | 6 | 1 | 236 | 1.65 | 3 | 5 | ND | 6 | 10 | .2 | 2 | 2 | 1 | .39 | .003 | 27 | 5 | .29 | 42 | .01 | 2 | .34 | .02 | .15 | 1 | 6 | 60 |
| 1650 G | 2 | 2 | 12 | 14 | .1 | 1 | 1 | 226 | 1.41 | 3 | 5 | ND | 5 | 7 | .2 | 2 | 2 | 1 | .35 | .004 | 26 | 2 | .25 | 49 | .01 | 3 | .32 | .03 | .13 | 1 | 2 | 80 |
| 1651 G | 5 | 1 | 8 | 12 | .1 | 5 | 2 | 179 | 1.25 | 2 | 5 | ND | 5 | 5 | .2 | 2 | 3 | 1 | .28 | .003 | 25 | 6 | .19 | 54 | .01 | 2 | .30 | .02 | .13 | 1 | 3 | 110 |
| 1652 G | 2 | 6 | 8 | 15 | .1 | 1 | 1 | 396 | .92 | 2 | 5 | ND | 6 | 4 | .3 | 2 | 3 | 1 | .05 | .005 | 35 | 2 | .03 | 83 | .01 | 2 | .35 | .01 | .14 | 1 | 6 | 120 |
| 1653 G | 4 | 4 | 8 | 12 | .1 | 11 | 1 | 228 | 1.19 | 2 | 5 | ND | 5 | 9 | .2 | 2 | 3 | 1 | .36 | .003 | 27 | 9 | .14 | 45 | .01 | 3 | .29 | .02 | .13 | 1 | 1 | 90 |
| 1654 G | 1 | 2 | 8 | 12 | .1 | 2 | 2 | 296 | 1.44 | 3 | 5 | ND | 5 | 8 | .2 | 2 | 2 | 1 | .44 | .004 | 29 | 2 | .25 | 49 | .01 | 2 | .39 | .02 | .15 | 1 | 3 | 70 |
| 1655 G | 5 | 4 | 16 | 10 | .1 | 11 | 1 | 263 | 1.16 | 2 | 5 | ND | 6 | 7 | .3 | 2 | 2 | 1 | .29 | .004 | 28 | 9 | .16 | 54 | .01 | 2 | .32 | .02 | .17 | 1 | 2 | 60 |
| 1656 G | 2 | 2 | 23 | 15 | .1 | 2 | 1 | 187 | 1.42 | 2 | 5 | ND | 6 | 6 | .2 | 2 | 6 | 1 | .23 | .004 | 30 | 2 | .18 | 57 | .01 | 2 | .38 | .02 | .15 | 1 | 12 | 60 |
| 1657 G | 4 | 3 | 20 | 21 | .1 | 11 | 1 | 200 | 1.35 | 2 | 5 | ND | 6 | 8 | .2 | 2 | 2 | 1 | .26 | .004 | 29 | 9 | .17 | 63 | .01 | 2 | .41 | .03 | .17 | 1 | 4 | 30 |
| 1658 G | 1 | 3 | 13 | 16 | .1 | 3 | 2 | 149 | 1.36 | 5 | 5 | ND | 7 | 5 | .2 | 2 | 4 | 1 | .09 | .004 | 29 | 3 | .12 | 42 | .01 | 2 | .38 | .02 | .15 | 1 | 8 | 40 |
| 1659 G | 5 | 5 | 17 | 18 | .2 | 10 | 2 | 164 | 1.63 | 7 | 5 | ND | 6 | 6 | .3 | 2 | 2 | 1 | .16 | .004 | 26 | 7 | .16 | 63 | .01 | 4 | .43 | .02 | .15 | 1 | 7 | 130 |
| 1660 G | 2 | 5 | 26 | 15 | .2 | 3 | 2 | 384 | 1.56 | 2 | 5 | ND | 6 | 12 | .4 | 2 | 2 | 1 | .54 | .004 | 26 | 2 | .26 | 59 | .01 | 2 | .38 | .02 | .14 | 1 | 5 | 120 |
| 1661 G | 5 | 3 | 11 | 21 | .1 | 10 | 2 | 231 | 1.68 | 2 | 5 | ND | 6 | 10 | .2 | 2 | 2 | 2 | .33 | .003 | 27 | 8 | .24 | 41 | .01 | 2 | .49 | .02 | .14 | 1 | 3 | 40 |
| 1662 G | 3 | 4 | 13 | 9 | .2 | 1 | 1 | 259 | 1.10 | 5 | 5 | ND | 5 | 20 | .2 | 2 | 2 | 1 | .51 | .004 | 28 | 3 | .20 | 51 | .01 | 2 | .31 | .02 | .12 | 1 | 1 | 50 |
| 1663 G | 6 | 4 | 32 | 32 | .1 | 10 | 2 | 363 | 1.47 | 2 | 5 | ND | 4 | 11 | .4 | 2 | 2 | 2 | .48 | .004 | 30 | 9 | .27 | 44 | .01 | 2 | .45 | .03 | .13 | 1 | 1 | 220 |
| 1664 G | 4 | 5 | 12 | 38 | .1 | 3 | 2 | 175 | 1.67 | 3 | 5 | ND | 6 | 6 | .4 | 2 | 2 | 2 | .19 | .004 | 27 | 3 | .22 | 37 | .01 | 2 | .53 | .02 | .14 | 1 | 3 | 110 |
| 1665 G | 6 | 3 | 15 | 30 | .1 | 10 | 2 | 158 | 1.27 | 2 | 5 | ND | 6 | 6 | .2 | 2 | 2 | 1 | .20 | .003 | 25 | 9 | .15 | 44 | .01 | 2 | .37 | .02 | .14 | 1 | 1 | 260 |
| 1666 G | 4 | 4 | 18 | 34 | .1 | 4 | 1 | 316 | 1.38 | 3 | 5 | ND | 5 | 18 | .6 | 2 | 3 | 1 | .63 | .004 | 25 | 2 | .30 | 34 | .01 | 2 | .43 | .02 | .13 | 1 | 13 | 240 |
| 1667 G | 6 | 1 | 12 | 33 | .1 | 7 | 1 | 307 | 1.67 | 2 | 5 | ND | 5 | 12 | .5 | 2 | 2 | 2 | .46 | .004 | 26 | 7 | .29 | 42 | .01 | 2 | .55 | .02 | .15 | 1 | 2 | 160 |
| 1668 G | 4 | 5 | 16 | 32 | .2 | 2 | 1 | 225 | 1.28 | 2 | 5 | ND | 5 | 8 | .2 | 2 | 2 | 1 | .32 | .004 | 25 | 2 | .19 | 44 | .01 | 2 | .38 | .02 | .12 | 1 | 1 | 260 |
| 1669 G | 6 | 3 | 18 | 48 | .2 | 7 | 1 | 171 | 1.48 | 4 | 5 | ND | 5 | 5 | .5 | 2 | 2 | 2 | .16 | .003 | 27 | 8 | .17 | 83 | .01 | 2 | .49 | .02 | .14 | 1 | 1 | 190 |
| STANDARD C/AU-R | 19 | 57 | 40 | 131 | 6.7 | 70 | 32 | 1050 | 3.97 | 41 | 20 | 7 | 37 | 53 | 19.0 | 14 | 17 | 55 | .51 | .094 | 37 | 57 | .89 | 180 | .07 | 34 | 1.89 | .06 | .14 | 11 | 488 | 1300 |

718

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe ppm | As % | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1670 G | 4 | 2 | 15 | 30 | .1 | 1 | 2 | 279 | 1.60 | 2 | 5 | ND | 5 | 6 | .2 | 2 | 2 | 2 | .34 | .004 | 30 | 1 | .23 | 74 | .01 | 3 | .47 | .02 | .14 | 1 | 5 | 100 |
| 1671 G | 6 | 4 | 15 | 27 | .1 | 6 | 1 | 208 | 1.35 | 4 | 5 | ND | 6 | 6 | .5 | 2 | 3 | 1 | .25 | .004 | 30 | 6 | .16 | 50 | .01 | 2 | .29 | .02 | .13 | 1 | 3 | 80 |
| 1672 G | 3 | 2 | 18 | 26 | .1 | 3 | 2 | 166 | 1.33 | 3 | 5 | ND | 5 | 9 | .2 | 2 | 2 | 1 | .17 | .003 | 28 | 1 | .12 | 75 | .01 | 4 | .19 | .02 | .14 | 1 | 7 | 90 |
| 1673 G | 6 | 5 | 23 | 72 | .1 | 9 | 2 | 147 | 1.40 | 4 | 5 | ND | 5 | 6 | .5 | 2 | 2 | 1 | .15 | .003 | 27 | 7 | .11 | 71 | .01 | 3 | .26 | .02 | .13 | 1 | 4 | 140 |
| 1674 G | 4 | 3 | 18 | 36 | .1 | 2 | 3 | 192 | 1.96 | 3 | 5 | ND | 6 | 5 | .9 | 2 | 2 | 1 | .17 | .004 | 34 | 1 | .17 | 63 | .01 | 2 | .40 | .02 | .15 | 1 | 6 | 90 |
| 1675 G | 7 | 5 | 14 | 29 | .1 | 7 | 2 | 159 | 1.40 | 5 | 5 | ND | 5 | 8 | .3 | 2 | 2 | 1 | .21 | .003 | 26 | 7 | .12 | 47 | .01 | 3 | .27 | .02 | .12 | 1 | 7 | 340 |
| 1676 G | 2 | 1 | 14 | 16 | .1 | 2 | 2 | 176 | 1.28 | 2 | 8 | ND | 5 | 11 | .8 | 2 | 2 | 1 | .31 | .004 | 26 | 1 | .16 | 51 | .01 | 2 | .28 | .02 | .13 | 1 | 1 | 60 |
| 1677 G | 4 | 4 | 14 | 19 | .1 | 7 | 2 | 167 | 1.32 | 2 | 5 | ND | 4 | 8 | .2 | 2 | 2 | 1 | .29 | .003 | 29 | 5 | .21 | 40 | .01 | 2 | .34 | .03 | .12 | 1 | 3 | 50 |
| 1678 G | 1 | 3 | 10 | 14 | .2 | 1 | 1 | 118 | 1.10 | 3 | 5 | ND | 6 | 6 | .3 | 2 | 6 | 1 | .15 | .004 | 26 | 1 | .12 | 54 | .01 | 2 | .26 | .02 | .12 | 1 | 9 | 60 |
| 1679 G | 4 | 1 | 16 | 24 | .1 | 8 | 1 | 138 | 1.30 | 2 | 5 | ND | 6 | 5 | .2 | 2 | 2 | 1 | .14 | .004 | 30 | 6 | .10 | 80 | .01 | 2 | .25 | .02 | .14 | 1 | 6 | 130 |
| 1680 G | 2 | 3 | 13 | 17 | .1 | 1 | 2 | 204 | 1.45 | 4 | 5 | ND | 4 | 12 | .2 | 2 | 2 | 1 | .26 | .004 | 26 | 2 | .11 | 58 | .01 | 2 | .26 | .03 | .14 | 1 | 7 | 120 |
| 1681 G | 5 | 2 | 17 | 9 | .1 | 7 | 1 | 180 | 1.55 | 3 | 5 | ND | 3 | 10 | .2 | 2 | 2 | 1 | .26 | .003 | 26 | 4 | .14 | 65 | .01 | 2 | .30 | .02 | .11 | 1 | 11 | 100 |
| 1682 G | 2 | 2 | 9 | 9 | .1 | 1 | 2 | 187 | 1.63 | 4 | 5 | ND | 4 | 13 | .2 | 2 | 2 | 1 | .35 | .003 | 26 | 1 | .16 | 52 | .01 | 2 | .29 | .03 | .13 | 1 | 9 | 110 |
| 1683 G | 6 | 4 | 15 | 10 | .2 | 9 | 2 | 158 | 1.26 | 5 | 5 | ND | 5 | 7 | .3 | 2 | 2 | 1 | .25 | .003 | 24 | 7 | .12 | 48 | .01 | 2 | .17 | .02 | .11 | 1 | 1 | 100 |
| 1684 G | 3 | 3 | 16 | 15 | .1 | 1 | 2 | 217 | 1.77 | 7 | 5 | ND | 5 | 7 | .2 | 2 | 2 | 1 | .23 | .003 | 31 | 1 | .15 | 48 | .01 | 3 | .24 | .02 | .16 | 1 | 6 | 130 |
| 1685 G | 4 | 3 | 15 | 8 | .1 | 6 | 1 | 102 | 1.12 | 6 | 5 | ND | 4 | 4 | .6 | 2 | 2 | 1 | .06 | .004 | 28 | 5 | .04 | 64 | .01 | 4 | .20 | .03 | .12 | 1 | 11 | 80 |
| 1686 G | 2 | 6 | 22 | 7 | .2 | 1 | 1 | 354 | 1.37 | 5 | 5 | ND | 4 | 13 | .2 | 4 | 2 | 1 | .72 | .004 | 24 | 1 | .29 | 44 | .01 | 2 | .19 | .02 | .12 | 1 | 5 | 60 |
| 1687 G | 3 | 4 | 21 | 11 | .2 | 6 | 2 | 179 | 1.54 | 3 | 5 | ND | 5 | 6 | .4 | 2 | 2 | 1 | .21 | .003 | 26 | 5 | .18 | 39 | .01 | 4 | .30 | .02 | .12 | 1 | 12 | 70 |
| 1688 G | 3 | 6 | 9 | 11 | .1 | 2 | 2 | 203 | 1.55 | 4 | 5 | ND | 6 | 5 | .2 | 2 | 2 | 1 | .16 | .003 | 34 | 3 | .11 | 71 | .01 | 2 | .36 | .04 | .18 | 2 | 8 | 80 |
| 1689 G | 4 | 1 | 20 | 11 | .1 | 11 | 2 | 187 | 1.63 | 2 | 5 | ND | 4 | 21 | .2 | 2 | 2 | 1 | .40 | .004 | 25 | 8 | .20 | 45 | .01 | 4 | .35 | .02 | .14 | 1 | 7 | 90 |
| 1690 G | 2 | 6 | 17 | 9 | .1 | 2 | 2 | 154 | 1.40 | 6 | 9 | ND | 4 | 6 | .3 | 2 | 2 | 1 | .17 | .003 | 27 | 2 | .10 | 46 | .01 | 4 | .22 | .02 | .13 | 1 | 3 | 60 |
| 1691 G | 5 | 4 | 27 | 8 | .1 | 11 | 2 | 163 | 1.29 | 4 | 5 | ND | 4 | 10 | .3 | 2 | 2 | 1 | .26 | .004 | 25 | 8 | .12 | 56 | .01 | 3 | .22 | .02 | .14 | 1 | 9 | 50 |
| 1692 G | 3 | 5 | 15 | 9 | .2 | 3 | 2 | 167 | 1.52 | 5 | 5 | ND | 5 | 8 | .3 | 3 | 2 | 1 | .20 | .005 | 24 | 2 | .17 | 73 | .01 | 3 | .31 | .03 | .14 | 1 | 2 | 80 |
| 1693 G | 6 | 6 | 12 | 7 | .1 | 13 | 2 | 183 | 1.37 | 9 | 5 | ND | 4 | 12 | .2 | 2 | 2 | 1 | .28 | .003 | 23 | 9 | .16 | 60 | .01 | 3 | .25 | .03 | .15 | 1 | 7 | 70 |
| 1694 G | 3 | 4 | 10 | 13 | .1 | 1 | 2 | 222 | 1.23 | 9 | 5 | ND | 4 | 13 | .2 | 2 | 2 | 1 | .40 | .002 | 23 | 2 | .17 | 77 | .01 | 3 | .21 | .02 | .14 | 1 | 6 | 90 |
| 1695 G | 7 | 3 | 15 | 16 | .1 | 11 | 2 | 325 | 1.58 | 5 | 5 | ND | 5 | 11 | .5 | 2 | 2 | 1 | .22 | .003 | 24 | 10 | .14 | 85 | .01 | 3 | .23 | .02 | .14 | 1 | 4 | 60 |
| 1696 G | 4 | 3 | 22 | 25 | .1 | 4 | 2 | 182 | 1.45 | 4 | 5 | ND | 4 | 10 | .4 | 2 | 2 | 1 | .23 | .003 | 24 | 5 | .14 | 53 | .01 | 2 | .21 | .02 | .14 | 1 | 6 | 80 |
| 1697 G | 6 | 3 | 16 | 17 | .2 | 13 | 2 | 182 | 1.41 | 3 | 5 | ND | 5 | 7 | .4 | 2 | 2 | 1 | .15 | .003 | 24 | 9 | .09 | 58 | .01 | 3 | .22 | .02 | .14 | 1 | 3 | 70 |
| 1698 G | 3 | 5 | 12 | 11 | .1 | 2 | 2 | 144 | 1.29 | 6 | 5 | ND | 4 | 11 | .2 | 2 | 4 | 1 | .16 | .004 | 23 | 2 | .12 | 68 | .01 | 3 | .21 | .02 | .14 | 1 | 2 | 80 |
| 1699 G | 6 | 4 | 14 | 16 | .1 | 12 | 2 | 160 | 1.47 | 4 | 5 | ND | 4 | 10 | .2 | 2 | 2 | 1 | .22 | .004 | 21 | 9 | .17 | 60 | .01 | 3 | .30 | .03 | .16 | 1 | 3 | 80 |
| 1700 G | 3 | 5 | 18 | 19 | .4 | 1 | 2 | 170 | 1.42 | 6 | 5 | ND | 6 | 8 | .5 | 2 | 2 | 1 | .25 | .004 | 21 | 2 | .17 | 52 | .01 | 2 | .24 | .02 | .13 | 1 | 4 | 70 |
| 1701 G | 6 | 12 | 25 | 21 | .3 | 12 | 2 | 300 | 1.42 | 5 | 5 | ND | 5 | 15 | .3 | 2 | 2 | 1 | .59 | .004 | 24 | 10 | .23 | 76 | .01 | 2 | .27 | .02 | .16 | 1 | 1 | 80 |
| 1702 G | 3 | 4 | 9 | 14 | .2 | 2 | 2 | 214 | 1.29 | 5 | 5 | ND | 4 | 12 | .2 | 2 | 5 | 1 | .45 | .004 | 18 | 3 | .21 | 55 | .01 | 2 | .21 | .03 | .13 | 1 | 2 | 100 |
| 1703 G | 6 | 3 | 12 | 16 | .3 | 11 | 2 | 371 | 1.21 | 4 | 5 | ND | 4 | 15 | .3 | 2 | 2 | 1 | .80 | .004 | 21 | 10 | .31 | 60 | .01 | 3 | .25 | .02 | .14 | 1 | 12 | 80 |
| 1704 G | 3 | 5 | 16 | 12 | .4 | 1 | 2 | 227 | 1.36 | 4 | 5 | ND | 5 | 6 | .2 | 2 | 2 | 1 | .25 | .003 | 24 | 2 | .12 | 73 | .01 | 3 | .26 | .02 | .13 | 1 | 1 | 60 |
| 1705 G | 6 | 4 | 14 | 15 | .2 | 11 | 2 | 543 | 1.47 | 5 | 6 | ND | 3 | 48 | .2 | 2 | 4 | 1 | 1.17 | .003 | 21 | 9 | .50 | 75 | .01 | 3 | .28 | .03 | .17 | 1 | 4 | 60 |
| STANDARD C/AU-R | 19 | 62 | 38 | 131 | 7.1 | 72 | 32 | 1047 | 3.94 | 37 | 20 | 7 | 39 | 55 | 20.0 | 14 | 19 | 56 | .50 | .095 | 38 | 55 | .87 | 182 | .07 | 33 | 1.91 | .06 | .14 | 11 | 504 | 1500 |

KTP B

FAP 8

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1706 G | 3 | 4 | 23 | 127 | .3 | 1 | 2 | 652 | 1.50 | 2 | 5 | ND | 5 | 6 | 1.5 | 2 | 2 | 1 | .15 | .003 | 24 | 2 | .08 | 91 | .01 | 6 | .29 | .03 | .17 | 1 | 5 | 140 |
| 1707 G | 4 | 7 | 21 | 146 | .3 | 4 | 1 | 1299 | .86 | 4 | 5 | ND | 6 | 7 | 2.1 | 2 | 2 | 1 | .30 | .004 | 32 | 5 | .14 | 109 | .01 | 5 | .37 | .01 | .22 | 1 | 3 | 290 |
| 1708 G | 3 | 5 | 31 | 58 | .2 | 2 | 1 | 244 | 1.10 | 3 | 5 | ND | 5 | 7 | .5 | 2 | 7 | 1 | .21 | .003 | 26 | 2 | .12 | 107 | .01 | 5 | .29 | .02 | .15 | 1 | 4 | 70 |
| 1709 G | 5 | 4 | 26 | 60 | .3 | 5 | 1 | 316 | 1.07 | 7 | 5 | ND | 4 | 26 | .6 | 2 | 2 | 1 | .67 | .004 | 23 | 6 | .29 | 52 | .01 | 4 | .22 | .03 | .14 | 1 | 5 | 80 |
| 1710 G | 3 | 5 | 29 | 87 | .5 | 1 | 2 | 453 | 1.32 | 7 | 5 | ND | 4 | 20 | .8 | 2 | 8 | 1 | .73 | .003 | 20 | 1 | .34 | 57 | .01 | 2 | .21 | .03 | .13 | 1 | 4 | 110 |
| 1711 G | 5 | 7 | 40 | 103 | .3 | 5 | 1 | 591 | 1.26 | 4 | 5 | ND | 2 | 22 | .9 | 3 | 2 | 1 | 1.15 | .002 | 18 | 6 | .51 | 53 | .01 | 4 | .19 | .03 | .11 | 1 | 4 | 160 |
| 1712 G | 3 | 3 | 22 | 235 | .2 | 1 | 1 | 455 | 1.07 | 6 | 5 | ND | 5 | 23 | 1.7 | 2 | 2 | 1 | .98 | .004 | 29 | 1 | .43 | 41 | .01 | 3 | .28 | .02 | .17 | 1 | 1 | 450 |
| 1713 G | 5 | 4 | 25 | 26 | .4 | 6 | 2 | 270 | 1.47 | 7 | 5 | ND | 3 | 12 | .3 | 2 | 5 | 1 | .46 | .002 | 15 | 7 | .31 | 60 | .01 | 2 | .30 | .03 | .09 | 1 | 4 | 70 |
| 1714 G | 3 | 1 | 16 | 24 | .1 | 1 | 1 | 1392 | 1.34 | 2 | 5 | ND | 3 | 39 | .6 | 2 | 2 | 1 | 3.24 | .002 | 25 | 1 | 1.42 | 269 | .01 | 5 | .41 | .01 | .18 | 1 | 4 | 50 |
| 1715 G | 2 | 1 | 10 | 19 | .1 | 1 | 1 | 3480 | 2.27 | 7 | 5 | ND | 1 | 76 | .3 | 2 | 2 | 1 | 6.50 | .002 | 15 | 3 | 2.92 | 34 | .01 | 2 | .26 | .01 | .11 | 1 | 4 | 60 |
| 1716 G | 1 | 1 | 4 | 21 | .1 | 1 | 1 | 3319 | 2.33 | 6 | 5 | ND | 1 | 74 | .8 | 2 | 2 | 1 | 6.65 | .002 | 11 | 1 | 2.94 | 48 | .01 | 4 | .25 | .01 | .11 | 1 | 1 | 90 |
| 1717 G | 4 | 3 | 2 | 26 | .3 | 3 | 2 | 2308 | 1.62 | 6 | 5 | ND | 4 | 17 | .6 | 3 | 3 | 2 | 2.88 | .003 | 25 | 3 | .16 | 213 | .01 | 3 | .52 | .01 | .26 | 1 | 1 | 80 |
| 1718 G | 3 | 2 | 8 | 22 | .3 | 3 | 2 | 924 | 1.08 | 2 | 5 | ND | 3 | 31 | .7 | 2 | 2 | 1 | 2.41 | .002 | 18 | 3 | .74 | 33 | .01 | 2 | .28 | .01 | .14 | 1 | 1 | 60 |
| 1719 G | 3 | 1 | 2 | 40 | .3 | 1 | 2 | 756 | 1.31 | 6 | 5 | ND | 4 | 19 | .5 | 3 | 2 | 1 | 1.64 | .004 | 23 | 1 | .40 | 59 | .01 | 6 | .33 | .02 | .18 | 1 | 3 | 320 |
| 1720 G | 4 | 3 | 5 | 27 | .1 | 4 | 1 | 570 | 1.07 | 6 | 5 | ND | 4 | 15 | .2 | 2 | 2 | 1 | .83 | .003 | 25 | 4 | .29 | 57 | .01 | 3 | .27 | .02 | .17 | 1 | 5 | 110 |
| 1721 G | 3 | 3 | 9 | 22 | .3 | 1 | 1 | 1660 | 1.58 | 3 | 5 | ND | 3 | 29 | .3 | 2 | 6 | 1 | 2.90 | .003 | 21 | 1 | 1.04 | 57 | .01 | 3 | .25 | .03 | .16 | 1 | 1 | 100 |
| 1722 G | 5 | 2 | 7 | 27 | .2 | 4 | 1 | 694 | 1.11 | 7 | 5 | ND | 3 | 26 | .2 | 2 | 2 | 1 | 1.37 | .003 | 18 | 5 | .53 | 49 | .01 | 5 | .18 | .04 | .11 | 1 | 4 | 240 |
| 1723 G | 2 | 1 | 11 | 26 | .1 | 3 | 1 | 2115 | 1.90 | 2 | 5 | ND | 2 | 41 | .4 | 2 | 4 | 1 | 4.38 | .003 | 20 | 6 | 1.39 | 56 | .01 | 3 | .31 | .03 | .18 | 1 | 4 | 320 |
| 1724 G | 3 | 3 | 10 | 51 | .1 | 5 | 1 | 2111 | 1.68 | 3 | 5 | ND | 1 | 69 | .6 | 2 | 4 | 1 | 4.35 | .004 | 16 | 3 | 1.93 | 41 | .01 | 2 | .17 | .02 | .13 | 1 | 4 | 190 |
| 1725 G | 2 | 1 | 9 | 31 | .4 | 2 | 3 | 4725 | 5.43 | 43 | 5 | ND | 1 | 129 | .7 | 2 | 2 | 1 | 7.31 | .003 | 4 | 1 | 2.91 | 32 | .01 | 2 | .15 | .01 | .08 | 1 | 5 | 280 |
| 1726 G | 3 | 1 | 2 | 37 | .4 | 4 | 2 | 5060 | 3.24 | 23 | 5 | ND | 1 | 126 | .7 | 3 | 5 | 1 | 8.22 | .005 | 9 | 4 | 2.81 | 39 | .01 | 3 | .20 | .02 | .11 | 1 | 13 | 220 |
| 1727 G | 3 | 3 | 8 | 193 | .4 | 3 | 2 | 4812 | 2.78 | 8 | 5 | ND | 3 | 112 | 1.1 | 2 | 2 | 1 | 9.71 | .005 | 16 | 3 | 3.15 | 65 | .01 | 2 | .27 | .01 | .17 | 1 | 2 | 400 |
| 1728 G | 6 | 4 | 17 | 139 | .3 | 12 | 2 | 1089 | 1.28 | 6 | 5 | ND | 2 | 29 | 1.0 | 2 | 3 | 1 | 2.25 | .003 | 20 | 9 | .68 | 110 | .01 | 3 | .27 | .02 | .17 | 1 | 1 | 380 |
| 1729 G | 4 | 7 | 18 | 119 | .2 | 2 | 3 | 799 | 1.37 | 5 | 5 | ND | 2 | 29 | .7 | 2 | 3 | 1 | 1.59 | .006 | 21 | 2 | .68 | 64 | .01 | 3 | .26 | .02 | .17 | 1 | 2 | 240 |
| 1730 G | 7 | 4 | 8 | 38 | .2 | 10 | 1 | 563 | 1.22 | 4 | 5 | ND | 3 | 16 | .2 | 2 | 4 | 1 | 1.08 | .003 | 24 | 8 | .48 | 50 | .01 | 4 | .25 | .03 | .18 | 1 | 3 | 120 |
| 1731 G | 3 | 11 | 28 | 44 | .3 | 5 | 5 | 339 | 1.19 | 5 | 5 | ND | 2 | 23 | .3 | 3 | 2 | 1 | .76 | .003 | 20 | 3 | .17 | 156 | .01 | 3 | .23 | .02 | .14 | 1 | 17 | 270 |
| 1732 G | 6 | 6 | 17 | 49 | .3 | 10 | 1 | 496 | 1.22 | 2 | 5 | ND | 3 | 16 | .2 | 3 | 2 | 1 | 1.20 | .003 | 25 | 9 | .29 | 242 | .01 | 2 | .27 | .01 | .22 | 1 | 4 | 180 |
| 1733 G | 4 | 6 | 10 | 64 | .3 | 2 | 2 | 711 | 1.28 | 8 | 5 | ND | 4 | 28 | .2 | 2 | 2 | 1 | 1.46 | .003 | 23 | 2 | .57 | 67 | .01 | 2 | .29 | .01 | .21 | 1 | 1 | 140 |
| 1734 G | 5 | 6 | 13 | 47 | .1 | 8 | 2 | 706 | 1.36 | 7 | 5 | ND | 2 | 34 | .2 | 2 | 4 | 1 | 1.42 | .003 | 21 | 7 | .61 | 56 | .01 | 5 | .30 | .01 | .18 | 1 | 2 | 120 |
| 1735 G | 1 | 4 | 11 | 166 | .6 | 2 | 22 | 1868 | 6.70 | 17 | 5 | ND | 1 | 67 | 1.1 | 5 | 2 | 90 | 3.58 | .095 | 9 | 6 | 2.57 | 52 | .01 | 2 | 2.06 | .02 | .13 | 1 | 1 | 230 |
| 1736 G | 1 | 4 | 2 | 125 | .2 | 3 | 21 | 1402 | 6.58 | 11 | 5 | ND | 1 | 142 | 1.2 | 3 | 2 | 131 | 3.70 | .106 | 9 | 8 | 2.19 | 78 | .01 | 2 | 1.78 | .03 | .15 | 1 | 1 | 180 |
| 1737 G | 1 | 6 | 6 | 133 | .2 | 2 | 20 | 1633 | 6.13 | 11 | 5 | ND | 1 | 415 | .7 | 2 | 2 | 110 | 7.07 | .098 | 9 | 6 | 2.28 | 81 | .01 | 2 | 1.37 | .02 | .13 | 1 | 1 | 200 |
| 1738 G | 1 | 4 | 2 | 119 | .3 | 2 | 21 | 1323 | 6.59 | 10 | 5 | ND | 1 | 136 | .9 | 2 | 2 | 155 | 3.50 | .106 | 10 | 8 | 2.42 | 75 | .01 | 2 | 1.95 | .03 | .14 | 1 | 1 | 150 |
| 1739 G | 1 | 5 | 8 | 97 | .2 | 2 | 20 | 1270 | 6.76 | 9 | 5 | ND | 1 | 152 | .8 | 2 | 2 | 149 | 3.27 | .110 | 9 | 7 | 2.24 | 80 | .01 | 2 | 2.14 | .03 | .12 | 1 | 1 | 90 |
| 1740 G | 1 | 6 | 8 | 110 | .2 | 4 | 20 | 1239 | 6.46 | 8 | 5 | ND | 1 | 170 | .8 | 4 | 3 | 127 | 3.41 | .106 | 9 | 9 | 2.05 | 88 | .01 | 2 | 1.95 | .03 | .13 | 1 | 32 | 120 |
| 1741 G | 1 | 6 | 3 | 77 | .5 | 2 | 21 | 1280 | 6.17 | 13 | 5 | ND | 1 | 189 | .5 | 3 | 2 | 93 | 3.69 | .101 | 10 | 7 | 1.85 | 104 | .01 | 6 | 1.19 | .03 | .18 | 1 | 12 | 100 |
| STANDARD C/AU-R | 19 | 61 | 41 | 129 | 7.0 | 73 | 32 | 1051 | 3.97 | 40 | 21 | 7 | 38 | 53 | 18.9 | 15 | 20 | 56 | .52 | .097 | 38 | 57 | .89 | 182 | .07 | 36 | 1.89 | .06 | .14 | 13 | 509 | 1400 |

FP 8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | ppm | ppb | ppb | |
| 1742 G | 1 | 1 | 2 | 87 | .1 | 3 | 19 | 2258 | 5.39 | 18 | 5 | ND | 1 | 166 | .4 | 2 | 2 | 57 | 4.92 | .080 | 9 | 3 | 2.01 | 65 | .01 | 3 | .84 | .02 | .17 | 1 | 10 | 270 |
| 1743 G | 5 | 3 | 9 | 52 | .2 | 10 | 2 | 402 | 1.47 | 22 | 5 | ND | 2 | 13 | .2 | 2 | 2 | 2 | .67 | .003 | 15 | 5 | .31 | 63 | .01 | 2 | .21 | .02 | .09 | 1 | 5 | 230 |
| 1744 G | 3 | 1 | 10 | 67 | .1 | 1 | 2 | 396 | 1.12 | 62 | 5 | ND | 4 | 14 | .2 | 2 | 4 | 1 | .72 | .003 | 28 | 1 | .31 | 58 | .01 | 4 | .31 | .01 | .20 | 1 | 5 | 200 |
| 1745 G | 4 | 3 | 10 | 72 | .2 | 8 | 1 | 966 | .93 | 21 | 5 | ND | 3 | 36 | .2 | 2 | 4 | 1 | 2.03 | .003 | 27 | 4 | .70 | 50 | .01 | 2 | .24 | .01 | .18 | 1 | 2 | 180 |
| 1746 G | 2 | 1 | 11 | 52 | .1 | 1 | 1 | 635 | .97 | 14 | 5 | ND | 4 | 13 | .2 | 2 | 4 | 1 | 1.31 | .004 | 29 | 1 | .42 | 50 | .01 | 5 | .30 | .01 | .21 | 1 | 2 | 150 |
| 1747 G | 4 | 1 | 14 | 50 | .1 | 7 | 1 | 353 | .93 | 10 | 5 | ND | 4 | 9 | .2 | 2 | 2 | 1 | .65 | .002 | 29 | 4 | .22 | 55 | .01 | 4 | .28 | .01 | .20 | 1 | 1 | 310 |
| 1748 G | 3 | 1 | 13 | 63 | .1 | 3 | 1 | 491 | .99 | 5 | 5 | ND | 3 | 14 | .2 | 2 | 2 | 1 | .97 | .002 | 28 | 1 | .29 | 48 | .01 | 3 | .29 | .01 | .20 | 1 | 2 | 370 |
| 1749 G | 4 | 1 | 20 | 76 | .3 | 5 | 1 | 522 | 1.03 | 7 | 5 | ND | 3 | 18 | .2 | 2 | 2 | 1 | .93 | .002 | 25 | 3 | .30 | 49 | .01 | 2 | .26 | .01 | .18 | 1 | 2 | 490 |
| 1750 G | 3 | 2 | 23 | 92 | .1 | 1 | 2 | 783 | 1.14 | 8 | 5 | ND | 2 | 22 | .3 | 2 | 2 | 1 | 1.45 | .002 | 24 | 1 | .53 | 60 | .01 | 4 | .33 | .01 | .21 | 1 | 5 | 450 |
| 1751 G | 4 | 1 | 14 | 47 | .1 | 7 | 1 | 560 | .80 | 2 | 5 | ND | 2 | 28 | .2 | 2 | 2 | 1 | 1.17 | .002 | 26 | 5 | .36 | 69 | .01 | 3 | .23 | .01 | .20 | 1 | 2 | 320 |
| 1752 G | 3 | 1 | 43 | 231 | .1 | 4 | 2 | 793 | 1.44 | 8 | 5 | ND | 2 | 30 | .9 | 2 | 2 | 1 | 1.49 | .004 | 24 | 2 | .56 | 65 | .01 | 3 | .27 | .01 | .22 | 1 | 2 | 560 |
| 1753 G | 3 | 1 | 13 | 56 | .1 | 4 | 1 | 447 | .77 | 4 | 5 | ND | 3 | 29 | .3 | 2 | 2 | 1 | 1.10 | .002 | 23 | 3 | .38 | 49 | .01 | 4 | .24 | .01 | .20 | 1 | 1 | 190 |
| 1754 G | 3 | 1 | 14 | 52 | .1 | 1 | 1 | 751 | .87 | 5 | 5 | ND | 2 | 28 | .2 | 2 | 2 | 1 | 1.61 | .001 | 24 | 1 | .62 | 34 | .01 | 3 | .30 | .01 | .24 | 1 | 1 | 140 |
| 1755 G | 3 | 1 | 13 | 51 | .1 | 4 | 1 | 697 | .70 | 7 | 5 | ND | 1 | 31 | .2 | 2 | 2 | 1 | 1.55 | .002 | 19 | 3 | .54 | 40 | .01 | 4 | .27 | .01 | .18 | 1 | 2 | 210 |
| 1756 G | 2 | 1 | 18 | 61 | .1 | 1 | 1 | 1658 | 1.10 | 17 | 5 | ND | 1 | 44 | .4 | 2 | 2 | 1 | 2.89 | .001 | 17 | 1 | 1.11 | 39 | .01 | 2 | .27 | .01 | .18 | 1 | 3 | 190 |
| 1757 G | 3 | 2 | 19 | 117 | .1 | 3 | 1 | 1266 | .88 | 7 | 5 | ND | 3 | 28 | .2 | 2 | 2 | 1 | 2.44 | .001 | 22 | 2 | .94 | 47 | .01 | 4 | .27 | .01 | .16 | 1 | 2 | 260 |
| 1758 G | 3 | 1 | 14 | 33 | .1 | 1 | 2 | 3220 | 1.95 | 34 | 5 | ND | 3 | 58 | .4 | 2 | 2 | 1 | 5.87 | .002 | 23 | 1 | 2.74 | 31 | .01 | 4 | .28 | .01 | .17 | 1 | 3 | 120 |
| 1759 G | 2 | 1 | 11 | 56 | .2 | 2 | 2 | 1333 | 1.61 | 9 | 5 | ND | 2 | 96 | .4 | 2 | 2 | 4 | 3.63 | .005 | 17 | 1 | 1.25 | 34 | .01 | 2 | .41 | .01 | .21 | 1 | 2 | 210 |
| 1760 G | 5 | 7 | 15 | 25 | .3 | 9 | 2 | 596 | 1.16 | 30 | 5 | ND | 1 | 35 | .2 | 2 | 2 | 1 | .99 | .001 | 16 | 7 | .32 | 24 | .01 | 4 | .31 | .01 | .15 | 1 | 2 | 270 |
| 1761 G | 4 | 5 | 12 | 26 | 1.0 | 2 | 2 | 610 | 1.34 | 32 | 5 | ND | 2 | 25 | .2 | 2 | 2 | 1 | .93 | .001 | 16 | 2 | .32 | 18 | .01 | 3 | .25 | .01 | .14 | 1 | 6 | 270 |
| 1762 G | 15 | 3 | 23 | 32 | .4 | 10 | 2 | 810 | 1.12 | 32 | 5 | ND | 2 | 44 | .2 | 3 | 2 | 1 | 1.33 | .003 | 20 | 7 | .46 | 32 | .01 | 6 | .33 | .01 | .19 | 1 | 9 | 190 |
| 1763 G | 4 | 6 | 17 | 38 | .1 | 3 | 3 | 936 | 1.36 | 27 | 5 | ND | 1 | 46 | .3 | 2 | 2 | 1 | 1.62 | .001 | 20 | 1 | .57 | 25 | .01 | 4 | .30 | .01 | .15 | 1 | 4 | 170 |
| 1764 G | 4 | 6 | 16 | 47 | .5 | 2 | 4 | 1216 | 2.48 | 23 | 5 | ND | 2 | 159 | .3 | 3 | 5 | 3 | 3.83 | .005 | 15 | 1 | 1.34 | 164 | .01 | 2 | .37 | .01 | .20 | 1 | 3 | 180 |
| 1765 G | 4 | 10 | 17 | 86 | .3 | 5 | 13 | 855 | 3.51 | 30 | 5 | ND | 1 | 153 | .3 | 2 | 4 | 19 | 3.06 | .045 | 8 | 1 | 1.25 | 117 | .01 | 2 | .49 | .01 | .21 | 1 | 2 | 270 |
| 1766 G | 4 | 42 | 8 | 109 | .4 | 15 | 10 | 1034 | 6.04 | 50 | 9 | ND | 1 | 177 | .7 | 15 | 2 | 19 | 3.68 | .105 | 4 | 3 | 1.36 | 56 | .01 | 9 | .69 | .01 | .31 | 1 | 6 | 510 |
| 1767 G | 4 | 71 | 11 | 116 | .1 | 21 | 16 | 718 | 5.05 | 43 | 5 | ND | 1 | 59 | .7 | 26 | 2 | 18 | 1.67 | .078 | 6 | 4 | 1.12 | 59 | .01 | 6 | .61 | .01 | .30 | 1 | 6 | 590 |
| 1768 G | 3 | 30 | 8 | 64 | .1 | 10 | 12 | 1129 | 4.26 | 21 | 5 | ND | 1 | 29 | .2 | 8 | 2 | 11 | 2.05 | .050 | 12 | 3 | 1.30 | 46 | .01 | 6 | .55 | .01 | .22 | 1 | 156 | 290 |
| 1769 G | 4 | 20 | 6 | 55 | .1 | 10 | 9 | 1191 | 4.32 | 14 | 5 | ND | 1 | 50 | .3 | 4 | 2 | 9 | 2.38 | .044 | 12 | 2 | 1.46 | 49 | .01 | 4 | .50 | .01 | .21 | 1 | 5 | 280 |
| 1770 G | 6 | 34 | 15 | 117 | .2 | 15 | 12 | 847 | 4.60 | 24 | 5 | ND | 1 | 24 | .7 | 15 | 2 | 14 | 1.64 | .063 | 9 | 4 | 1.19 | 69 | .01 | 4 | .64 | .01 | .21 | 1 | 5 | 480 |
| 1771 G | 5 | 48 | 13 | 152 | .4 | 13 | 14 | 1164 | 5.22 | 39 | 5 | ND | 1 | 118 | .8 | 18 | 2 | 14 | 3.01 | .055 | 5 | 4 | 1.42 | 59 | .01 | 6 | .49 | .01 | .24 | 1 | 3 | 470 |
| 1772 G | 5 | 55 | 19 | 148 | .6 | 16 | 15 | 1104 | 4.29 | 27 | 5 | ND | 1 | 85 | .7 | 18 | 2 | 11 | 2.38 | .045 | 8 | 11 | 1.15 | 97 | .01 | 2 | .42 | .01 | .20 | 9 | 4 | 510 |
| 1773 G | 4 | 51 | 23 | 213 | .1 | 18 | 13 | 883 | 5.61 | 63 | 5 | ND | 1 | 27 | 1.4 | 18 | 2 | 17 | 1.73 | .072 | 8 | 3 | 1.12 | 40 | .01 | 6 | .59 | .01 | .26 | 1 | 5 | 540 |
| 1774 G | 4 | 22 | 19 | 143 | .3 | 10 | 9 | 1399 | 4.71 | 28 | 5 | ND | 1 | 27 | 1.1 | 9 | 2 | 13 | 2.69 | .072 | 11 | 3 | 1.60 | 54 | .01 | 7 | .98 | .01 | .21 | 1 | 3 | 350 |
| 1775 G | 16 | 22 | 15 | 220 | .2 | 10 | 9 | 1052 | 3.81 | 19 | 8 | ND | 1 | 22 | .6 | 9 | 2 | 9 | 1.82 | .037 | 13 | 3 | 1.05 | 117 | .01 | 5 | .89 | .01 | .21 | 1 | 4 | 680 |
| 1776 G | 4 | 1 | 8 | 104 | .1 | 1 | 2 | 2495 | 2.57 | 3 | 5 | ND | 1 | 30 | .7 | 2 | 2 | 1 | 4.31 | .002 | 26 | 1 | 2.10 | 46 | .01 | 4 | .53 | .01 | .17 | 1 | 4 | 100 |
| 1777 G | 14 | 4 | 6 | 110 | .1 | 4 | 2 | 1333 | 2.52 | 5 | 5 | ND | 2 | 27 | .6 | 3 | 4 | 1 | 2.25 | .005 | 31 | 4 | 1.18 | 47 | .01 | 3 | .70 | .01 | .18 | 1 | 1 | 220 |
| STANDARD C/AU-R | 19 | 58 | 37 | 131 | 6.8 | 69 | 31 | 1049 | 3.95 | 40 | 21 | 7 | 37 | 53 | 18.9 | 15 | 21 | 55 | .51 | .094 | 38 | 56 | .91 | 179 | .08 | 34 | 1.89 | .06 | .14 | 12 | 495 | 1400 |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Tl | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| 1778 G | 30 | 13 | 14 | 125 | .2 | 9 | 5 | 800 | 3.78 | 13 | 5 | ND | 1 | 24 | .2 | 5 | 2 | 5 | 1.16 | .023 | 17 | 10 | .86 | 32 | .01 | 3 | .99 | .01 | .12 | 1 | 8 | 300 |
| 1779 G | 8 | 35 | 26 | 171 | .3 | 14 | 7 | 490 | 3.83 | 32 | 5 | ND | 2 | 17 | .6 | 13 | 2 | 7 | .69 | .049 | 13 | 7 | .63 | 42 | .01 | 2 | .64 | .01 | .19 | 1 | 10 | 620 |
| 1780 G | 3 | 40 | 24 | 120 | .3 | 16 | 11 | 386 | 3.78 | 39 | 5 | ND | 1 | 21 | .3 | 14 | 2 | 10 | .64 | .072 | 12 | 7 | .59 | 52 | .01 | 2 | .52 | .01 | .27 | 1 | 10 | 500 |
| 1781 G | 2 | 35 | 25 | 113 | .4 | 14 | 9 | 439 | 3.52 | 34 | 5 | ND | 2 | 21 | .2 | 15 | 2 | 8 | .70 | .069 | 12 | 5 | .55 | 48 | .01 | 5 | .49 | .01 | .24 | 1 | 10 | 540 |
| 1782 G | 3 | 74 | 17 | 106 | .4 | 25 | 17 | 714 | 3.69 | 24 | 5 | ND | 1 | 58 | .3 | 9 | 2 | 12 | 1.71 | .047 | 6 | 14 | .91 | 118 | .01 | 4 | .58 | .01 | .24 | 26 | 7 | 380 |
| 1783 G | 2 | 29 | 10 | 66 | .1 | 11 | 6 | 870 | 2.74 | 13 | 5 | ND | 1 | 55 | .2 | 6 | 2 | 9 | 1.72 | .022 | 14 | 10 | .95 | 104 | .01 | 3 | .42 | .01 | .20 | 13 | 6 | 260 |
| 1784 G | 4 | 41 | 18 | 144 | .3 | 16 | 10 | 718 | 4.53 | 32 | 5 | ND | 1 | 37 | .6 | 14 | 2 | 12 | 1.42 | .054 | 8 | 7 | 1.03 | 41 | .01 | 5 | .39 | .01 | .20 | 1 | 7 | 560 |
| 1785 G | 4 | 37 | 12 | 181 | .2 | 13 | 9 | 915 | 5.62 | 31 | 5 | ND | 2 | 33 | .6 | 14 | 4 | 13 | 1.76 | .070 | 16 | 7 | 1.12 | 47 | .01 | 6 | .44 | .01 | .21 | 1 | 4 | 480 |
| 1786 G | 3 | 19 | 8 | 68 | .1 | 8 | 7 | 763 | 4.50 | 17 | 5 | ND | 1 | 40 | .2 | 7 | 2 | 7 | 1.49 | .034 | 16 | 8 | 1.03 | 43 | .01 | 4 | .39 | .01 | .20 | 1 | 3 | 200 |
| 1787 G | 3 | 23 | 12 | 151 | .3 | 13 | 9 | 695 | 3.94 | 24 | 5 | ND | 2 | 28 | .6 | 9 | 2 | 10 | 1.36 | .049 | 15 | 6 | .94 | 46 | .01 | 7 | .42 | .01 | .21 | 1 | 8 | 300 |
| 1788 G | 4 | 42 | 31 | 123 | .6 | 21 | 10 | 455 | 3.43 | 39 | 5 | ND | 2 | 28 | .3 | 14 | 2 | 10 | .95 | .064 | 14 | 5 | .66 | 51 | .01 | 4 | .44 | .01 | .22 | 1 | 13 | 390 |
| 1789 G | 6 | 35 | 9 | 129 | .2 | 18 | 11 | 411 | 4.86 | 30 | 6 | ND | 2 | 29 | .3 | 7 | 3 | 20 | .80 | .068 | 15 | 7 | .81 | 49 | .01 | 3 | .52 | .01 | .24 | 1 | 1 | 210 |
| 1790 G | 3 | 42 | 2 | 40 | .1 | 13 | 7 | 295 | 4.67 | 19 | 5 | ND | 1 | 34 | .2 | 3 | 2 | 17 | .60 | .069 | 10 | 7 | .78 | 48 | .01 | 3 | .54 | .01 | .25 | 2 | 3 | 90 |
| 1791 G | 3 | 48 | 2 | 29 | .1 | 18 | 9 | 277 | 4.08 | 24 | 5 | ND | 1 | 31 | .2 | 5 | 2 | 13 | .57 | .053 | 5 | 5 | .82 | 45 | .01 | 5 | .49 | .01 | .25 | 1 | 5 | 80 |
| 1792 G | 3 | 48 | 6 | 22 | .2 | 18 | 9 | 324 | 4.47 | 30 | 5 | ND | 1 | 62 | .2 | 10 | 2 | 13 | .89 | .056 | 3 | 6 | .89 | 49 | .01 | 5 | .44 | .01 | .22 | 1 | 6 | 100 |
| 1793 G | 5 | 44 | 4 | 18 | .2 | 13 | 6 | 450 | 3.81 | 22 | 5 | ND | 1 | 153 | .2 | 11 | 2 | 13 | 2.01 | .060 | 4 | 8 | 1.22 | 55 | .01 | 5 | .46 | .01 | .24 | 1 | 7 | 80 |
| 1794 G | 2 | 23 | 2 | 14 | .1 | 10 | 5 | 483 | 4.39 | 13 | 5 | ND | 1 | 76 | .2 | 5 | 2 | 14 | 1.47 | .080 | 6 | 9 | 1.11 | 39 | .01 | 3 | .47 | .01 | .21 | 1 | 7 | 50 |
| 1795 G | 1 | 53 | 2 | 10 | .1 | 11 | 8 | 176 | 2.46 | 24 | 5 | ND | 1 | 43 | .2 | 11 | 2 | 8 | .51 | .048 | 3 | 4 | .58 | 45 | .01 | 3 | .47 | .01 | .25 | 1 | 7 | 70 |
| 1796 G | 2 | 40 | 2 | 21 | .1 | 11 | 7 | 335 | 4.24 | 18 | 5 | ND | 1 | 68 | .2 | 7 | 2 | 14 | .97 | .048 | 3 | 6 | .95 | 46 | .01 | 5 | .43 | .01 | .21 | 1 | 7 | 80 |
| 1797 G | 2 | 48 | 2 | 25 | .1 | 11 | 8 | 255 | 3.10 | 22 | 5 | ND | 1 | 66 | .2 | 10 | 2 | 11 | .73 | .056 | 3 | 6 | .76 | 52 | .01 | 6 | .47 | .01 | .23 | 1 | 4 | 100 |
| 1798 G | 2 | 25 | 2 | 22 | .1 | 6 | 7 | 335 | 2.63 | 14 | 5 | ND | 1 | 41 | .2 | 7 | 2 | 8 | .78 | .050 | 4 | 7 | .60 | 46 | .01 | 2 | .40 | .01 | .20 | 1 | 1 | 110 |
| 1799 G | 1 | 6 | 3 | 78 | .3 | 3 | 16 | 2233 | 7.35 | 15 | 5 | ND | 1 | 100 | .4 | 10 | 2 | 84 | 5.38 | .087 | 7 | 9 | 2.90 | 39 | .01 | 3 | .48 | .02 | .12 | 1 | 8 | 170 |
| 1800 G | 3 | 36 | 16 | 22 | .2 | 17 | 13 | 279 | 4.77 | 36 | 5 | ND | 1 | 27 | .2 | 12 | 2 | 9 | .58 | .043 | 5 | 6 | .76 | 39 | .01 | 4 | .40 | .01 | .19 | 1 | 9 | 250 |
| 1801 G | 2 | 29 | 4 | 21 | .1 | 12 | 8 | 345 | 4.80 | 15 | 5 | ND | 1 | 31 | .2 | 10 | 2 | 13 | .77 | .067 | 6 | 7 | .91 | 41 | .01 | 4 | .42 | .01 | .19 | 1 | 2 | 100 |
| 1802 G | 2 | 37 | 3 | 34 | .1 | 12 | 7 | 475 | 4.29 | 16 | 5 | ND | 1 | 56 | .2 | 11 | 2 | 11 | 1.20 | .064 | 11 | 11 | .96 | 45 | .01 | 5 | .45 | .01 | .21 | 10 | 3 | 120 |
| 1803 G | 2 | 44 | 37 | 25 | .5 | 20 | 10 | 435 | 4.94 | 35 | 5 | ND | 1 | 34 | .2 | 17 | 2 | 14 | .95 | .065 | 6 | 7 | .87 | 42 | .01 | 4 | .49 | .01 | .22 | 1 | 9 | 200 |
| 1804 G | 1 | 58 | 28 | 21 | .4 | 19 | 11 | 279 | 4.41 | 32 | 5 | ND | 1 | 30 | .2 | 20 | 2 | 12 | .61 | .063 | 5 | 6 | .73 | 45 | .01 | 6 | .45 | .01 | .24 | 1 | 10 | 130 |
| 1805 G | 3 | 54 | 18 | 29 | .3 | 21 | 12 | 273 | 4.67 | 31 | 7 | ND | 1 | 37 | .2 | 18 | 2 | 13 | .60 | .077 | 4 | 7 | .79 | 45 | .01 | 7 | .47 | .01 | .24 | 1 | 9 | 90 |
| 1806 G | 3 | 30 | 6 | 26 | .1 | 10 | 7 | 463 | 3.82 | 18 | 5 | ND | 1 | 67 | .2 | 12 | 2 | 10 | 1.54 | .035 | 3 | 9 | 1.01 | 128 | .01 | 7 | .39 | .01 | .20 | 1 | 6 | 100 |
| 1807 G | 1 | 37 | 7 | 27 | .2 | 13 | 12 | 446 | 4.46 | 27 | 5 | ND | 1 | 94 | .2 | 13 | 2 | 16 | 1.58 | .047 | 2 | 7 | 1.16 | 100 | .01 | 6 | .53 | .01 | .24 | 1 | 6 | 150 |
| 1808 G | 2 | 27 | 2 | 28 | .1 | 9 | 9 | 576 | 4.24 | 21 | 5 | ND | 1 | 71 | .2 | 12 | 2 | 10 | 1.54 | .054 | 3 | 8 | 1.14 | 64 | .01 | 7 | .40 | .01 | .20 | 1 | 5 | 130 |
| 1809 G | 2 | 31 | 5 | 43 | .1 | 11 | 9 | 342 | 3.98 | 19 | 5 | ND | 1 | 39 | .2 | 14 | 2 | 10 | .78 | .055 | 5 | 7 | .91 | 57 | .01 | 5 | .41 | .01 | .22 | 1 | 5 | 140 |
| 1810 G | 3 | 29 | 7 | 350 | .1 | 9 | 9 | 1144 | 4.96 | 20 | 5 | ND | 1 | 48 | .4 | 14 | 3 | 5 | 2.72 | .036 | 14 | 8 | 1.60 | 45 | .01 | 6 | .34 | .01 | .15 | 1 | 16 | 480 |
| 1811 G | 4 | 19 | 2 | 152 | .1 | 8 | 6 | 736 | 4.22 | 13 | 5 | ND | 2 | 47 | .7 | 9 | 2 | 6 | 1.76 | .032 | 19 | 13 | 1.22 | 67 | .01 | 2 | .37 | .01 | .18 | 1 | 1 | 300 |
| 1812 G | 3 | 27 | 2 | 25 | .1 | 10 | 8 | 534 | 4.09 | 21 | 5 | ND | 1 | 47 | .2 | 11 | 2 | 11 | 1.37 | .048 | 7 | 7 | 1.02 | 68 | .01 | 3 | .42 | .01 | .19 | 1 | 2 | 150 |
| 1813 G | 3 | 18 | 4 | 44 | .1 | 7 | 7 | 562 | 4.35 | 14 | 5 | ND | 1 | 31 | .2 | 9 | 2 | 7 | 1.27 | .035 | 16 | 7 | .95 | 44 | .01 | 3 | .37 | .01 | .14 | 1 | 1 | 180 |
| STANDARD C/AU-R | 19 | 60 | 36 | 131 | 6.9 | 72 | 31 | 1051 | 3.97 | 39 | 18 | 7 | 37 | 52 | 18.5 | 15 | 19 | 55 | .51 | .098 | 38 | 59 | .89 | 181 | .07 | 37 | 1.91 | .06 | .14 | 11 | 504 | 1600 |

HP 8

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT 134 File # 90-3988

2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

NP 3
 1
 NP 3
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| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|------|------|------|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|-------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| 1825 G | 8 | 33 | 42 | 61 | 1.8 | 6 | 12 | 2038 | 8.14 | 119 | 5 | ND | 1 | 62 | 2 | 20 | 7 | 9 | 1.54 | .179 | 6 | 12 | .58 | 42 | .03 | 11 | 1.05 | .01 | .48 | 2 | 16 | 620 |
| 1826 G | 6 | 9 | 23 | 236 | 1.2 | 3 | 9 | 1467 | 4.12 | 53 | 5 | ND | 1 | 58 | 4 | 11 | 4 | 8 | 1.65 | .169 | 7 | 6 | .49 | 56 | .02 | 9 | .74 | .01 | .38 | 1 | 10 | 750 |
| 1827 G | 6 | 6 | 22 | 137 | 1.0 | 5 | 8 | 1216 | 2.93 | 33 | 5 | ND | 1 | 66 | 3 | 10 | 2 | 7 | 1.56 | .181 | 9 | 9 | .58 | 100 | .01 | 11 | .74 | .01 | .38 | 1 | 8 | 650 |
| 1828 G | 6 | 9 | 36 | 133 | 2.0 | 1 | 10 | 930 | 3.89 | 95 | 5 | ND | 1 | 40 | 2 | 12 | 3 | 8 | 1.28 | .166 | 9 | 7 | .42 | 42 | .02 | 6 | .81 | .01 | .40 | 1 | 16 | 2800 |
| 1829 G | 6 | 16 | 80 | 1181 | 6.2 | 6 | 9 | 313 | 6.33 | 190 | 5 | ND | 1 | 24 | 2.5 | 18 | 2 | 6 | .75 | .150 | 9 | 6 | .19 | 26 | .01 | 7 | .67 | .01 | .32 | 1 | 41 | 3300 |
| 1830 G | 4 | 50 | 2870 | 987 | 14.7 | 1 | 5 | 3651 | 5.70 | 200 | 5 | ND | 1 | 47 | 2.7 | 44 | 2 | 3 | 3.14 | .080 | 3 | 8 | 2.25 | 30 | .01 | 3 | .41 | .01 | .22 | 1 | 39 | 3000 |
| 1831 G | 5 | 10 | 146 | 58 | 4.1 | 4 | 9 | 1887 | 6.24 | 208 | 5 | ND | 1 | 54 | 2 | 32 | 2 | 5 | 1.91 | .139 | 8 | 10 | .62 | 44 | .01 | 7 | .58 | .01 | .32 | 1 | 25 | 480 |
| 1832 G | 4 | 8 | 37 | 94 | 4.0 | 3 | 9 | 2394 | 4.71 | 109 | 5 | ND | 4 | 46 | 3 | 32 | 2 | 7 | 1.92 | .140 | 12 | 13 | .79 | 59 | .01 | 17 | .54 | .01 | .31 | 1 | 17 | 180 |
| 1846 G | 2 | 8 | 38 | 2240 | 4.6 | 3 | 5 | 4886 | 5.12 | 159 | 5 | ND | 1 | 104 | 5.0 | 15 | 2 | 4 | 6.77 | .080 | 4 | 6 | 3.45 | 48 | .01 | 2 | .38 | .01 | .20 | 1 | 225 | 4500 |
| 1847 G | 4 | 6 | 22 | 91 | 2.6 | 2 | 8 | 1109 | 4.61 | 69 | 5 | ND | 1 | 50 | 2 | 10 | 5 | 13 | 1.26 | .173 | 11 | 7 | .48 | 48 | .01 | 7 | .89 | .01 | .31 | 1 | 30 | 580 |
| 1848 G | 4 | 11 | 35 | 472 | 4.9 | 5 | 15 | 1679 | 6.86 | 350 | 5 | ND | 1 | 33 | 1.0 | 15 | 2 | 19 | 1.94 | .116 | 4 | 12 | 1.16 | 38 | .01 | 4 | .47 | .01 | .27 | 1 | 81 | 1200 |
| 1849 G | 2 | 14 | 35 | 17 | 6.1 | 1 | 18 | 1327 | 13.71 | 586 | 5 | ND | 1 | 28 | 4 | 16 | 2 | 20 | 1.45 | .123 | 5 | 14 | .71 | 28 | .01 | 2 | .42 | .01 | .25 | 1 | 136 | 1700 |
| 1850 G | 2 | 11 | 17 | 236 | 3.7 | 3 | 21 | 3099 | 5.23 | 141 | 5 | ND | 1 | 38 | 2 | 12 | 2 | 43 | 2.51 | .197 | 10 | 8 | 1.09 | 66 | .01 | 3 | .86 | .01 | .34 | 1 | 117 | 2100 |
| 1851 G | 1 | 18 | 36 | 6 | 7.7 | 2 | 18 | 1890 | 10.89 | 658 | 5 | ND | 1 | 25 | 7 | 18 | 2 | 23 | 1.44 | .129 | 2 | 13 | 1.14 | 26 | .01 | 2 | .69 | .01 | .29 | 1 | 139 | 2800 |
| 1852 G | 2 | 18 | 18 | 7 | 7.6 | 2 | 14 | 3251 | 8.52 | 447 | 5 | ND | 1 | 81 | 6 | 16 | 2 | 27 | 3.11 | .120 | 3 | 12 | 2.15 | 34 | .01 | 2 | .82 | .01 | .24 | 1 | 145 | 2400 |
| 1853 G | 2 | 13 | 38 | 256 | 8.7 | 5 | 13 | 2563 | 10.92 | 457 | 5 | ND | 1 | 26 | 1.2 | 23 | 2 | 20 | 1.77 | .093 | 2 | 16 | 1.68 | 37 | .01 | 2 | .88 | .01 | .27 | 1 | 185 | 3100 |
| 1854 G | 1 | 4 | 4 | 50 | 1.8 | 2 | 3 | 6371 | 5.55 | 305 | 5 | ND | 1 | 143 | 2 | 4 | 2 | 10 | 11.76 | .024 | 4 | 1 | 5.08 | 30 | .01 | 2 | .61 | .01 | .08 | 1 | 57 | 540 |
| 1855 G | 1 | 12 | 17 | 600 | 5.9 | 2 | 11 | 4243 | 7.30 | 823 | 5 | ND | 1 | 39 | 1.2 | 21 | 2 | 23 | 3.29 | .089 | 2 | 11 | 2.98 | 35 | .01 | 4 | .64 | .01 | .21 | 1 | 192 | 3600 |
| 1856 G | 1 | 9 | 16 | 17 | 5.0 | 3 | 9 | 4575 | 6.61 | 719 | 5 | ND | 1 | 52 | 2 | 27 | 2 | 19 | 4.83 | .076 | 2 | 7 | 3.44 | 32 | .01 | 2 | .60 | .01 | .18 | 1 | 137 | 2100 |
| 1857 G | 2 | 6 | 22 | 7 | 4.2 | 4 | 9 | 5749 | 7.44 | 289 | 5 | ND | 1 | 70 | 2 | 12 | 2 | 19 | 5.03 | .065 | 2 | 10 | 3.50 | 39 | .01 | 2 | .52 | .01 | .17 | 1 | 105 | 2400 |
| STANDARD C/AU-R | 19 | 62 | 37 | 133 | 7.2 | 73 | 32 | 1054 | 3.97 | 41 | 21 | 7 | 39 | 52 | 18.5 | 15 | 22 | 59 | .51 | .098 | 40 | 61 | .89 | 188 | .08 | 35 | 1.88 | .06 | .13 | 12 | 496 | 1600 |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: CORE AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: AUG 30 1990 DATE REPORT MAILED: *Sept 5/90* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1814 G | 3 | 15 | 2 | 97 | .1 | 6 | 6 | 592 | 4.17 | 11 | 5 | ND | 1 | 53 | .4 | 8 | 2 | 5 | 1.46 | .029 | 18 | 10 | 1.09 | 62 | .01 | 3 | .30 | .01 | .16 | 1 | 5 | 230 |
| 1815 G | 4 | 60 | 4 | 35 | .1 | 16 | 11 | 285 | 4.23 | 27 | 11 | ND | 1 | 35 | .2 | 31 | 3 | 12 | .51 | .049 | 7 | 8 | .81 | 53 | .01 | 4 | .40 | .01 | .22 | 1 | 2 | 220 |
| 1816 G | 1 | 40 | 2 | 24 | .1 | 10 | 8 | 340 | 3.80 | 16 | 9 | ND | 1 | 30 | .2 | 21 | 3 | 10 | .67 | .026 | 8 | 6 | .80 | 44 | .01 | 3 | .35 | .01 | .19 | 1 | 9 | 140 |
| 1817 G | 2 | 19 | 6 | 29 | .1 | 10 | 12 | 774 | 3.90 | 20 | 6 | ND | 1 | 58 | .2 | 11 | 2 | 8 | 1.69 | .035 | 7 | 9 | 1.07 | 41 | .01 | 4 | .31 | .01 | .16 | 1 | 4 | 130 |
| 1818 G | 1 | 29 | 9 | 69 | .2 | 10 | 11 | 795 | 4.30 | 22 | 5 | ND | 1 | 54 | .3 | 12 | 2 | 10 | 1.81 | .050 | 5 | 10 | 1.13 | 36 | .01 | 5 | .33 | .01 | .17 | 1 | 1 | 190 |
| 1819 G | 4 | 38 | 7 | 21 | .3 | 13 | 9 | 805 | 4.19 | 23 | 5 | ND | 1 | 78 | .2 | 20 | 2 | 8 | 1.29 | .055 | 6 | 9 | .95 | 33 | .01 | 2 | .36 | .01 | .20 | 1 | 4 | 180 |
| 1820 G | 2 | 28 | 3 | 33 | .4 | 6 | 6 | 1176 | 4.59 | 13 | 5 | ND | 2 | 67 | .2 | 13 | 2 | 8 | 1.40 | .036 | 15 | 7 | 1.08 | 37 | .01 | 3 | .34 | .01 | .19 | 1 | 4 | 150 |
| 1821 G | 2 | 32 | 5 | 37 | .3 | 7 | 6 | 1079 | 3.29 | 28 | 5 | ND | 1 | 57 | .2 | 16 | 2 | 5 | 1.40 | .028 | 13 | 7 | .86 | 34 | .01 | 3 | .27 | .01 | .15 | 1 | 7 | 160 |
| 1822 G | 3 | 13 | 4 | 36 | .3 | 7 | 6 | 1304 | 4.50 | 20 | 5 | ND | 1 | 76 | .2 | 7 | 3 | 6 | 1.60 | .039 | 15 | 9 | 1.09 | 47 | .01 | 5 | .29 | .01 | .16 | 1 | 3 | 140 |
| 1823 G | 4 | 22 | 17 | 61 | .6 | 9 | 6 | 1435 | 4.84 | 22 | 5 | ND | 1 | 127 | .2 | 15 | 2 | 7 | 1.81 | .044 | 14 | 15 | 1.09 | 39 | .01 | 5 | .34 | .01 | .19 | 1 | 9 | 210 |
| 1824 G | 5 | 23 | 16 | 197 | 1.2 | 7 | 7 | 722 | 2.99 | 18 | 6 | ND | 1 | 62 | .2 | 16 | 3 | 8 | 1.11 | .073 | 6 | 3 | .26 | 39 | .01 | 4 | .40 | .01 | .22 | 1 | 3 | 400 |
| 1833 G | 4 | 3 | 8 | 141 | .6 | 1 | 7 | 2159 | 4.09 | 10 | 5 | ND | 1 | 52 | .2 | 6 | 2 | 6 | 2.14 | .162 | 15 | 7 | 1.06 | 68 | .01 | 4 | .43 | .01 | .24 | 1 | 7 | 240 |
| 1834 G | 4 | 6 | 20 | 116 | .8 | 3 | 8 | 2080 | 5.09 | 14 | 5 | ND | 1 | 43 | .2 | 6 | 2 | 12 | 2.19 | .145 | 13 | 7 | 1.24 | 75 | .01 | 3 | 1.11 | .02 | .17 | 1 | 8 | 250 |
| 1835 G | 4 | 4 | 13 | 171 | .4 | 2 | 7 | 1840 | 4.50 | 18 | 5 | ND | 1 | 39 | .2 | 5 | 4 | 14 | 2.07 | .143 | 17 | 16 | 1.18 | 57 | .01 | 2 | 1.32 | .02 | .18 | 1 | 7 | 220 |
| 1836 G | 3 | 3 | 16 | 138 | .3 | 2 | 6 | 928 | 4.94 | 5 | 5 | ND | 1 | 65 | .2 | 3 | 2 | 18 | 1.39 | .122 | 14 | 8 | .85 | 129 | .01 | 4 | 1.44 | .02 | .13 | 1 | 1 | 150 |
| 1837 G | 4 | 4 | 5 | 111 | .3 | 2 | 4 | 838 | 4.28 | 4 | 5 | ND | 1 | 88 | .4 | 5 | 2 | 7 | 1.33 | .092 | 14 | 6 | .50 | 124 | .01 | 3 | .96 | .02 | .17 | 1 | 1 | 110 |
| 1838 G | 5 | 4 | 2 | 76 | .2 | 5 | 1 | 805 | 3.78 | 2 | 5 | ND | 1 | 33 | .2 | 2 | 2 | 1 | .52 | .020 | 12 | 5 | .38 | 73 | .01 | 5 | .37 | .03 | .12 | 1 | 1 | 100 |
| 1839 G | 8 | 5 | 4 | 96 | .2 | 11 | 2 | 859 | 3.80 | 2 | 5 | ND | 1 | 39 | .2 | 3 | 2 | 2 | .56 | .023 | 15 | 35 | .37 | 96 | .01 | 3 | .53 | .05 | .14 | 1 | 19 | 120 |
| 1840 G | 5 | 3 | 6 | 131 | .3 | 3 | 1 | 1051 | 3.83 | 2 | 6 | ND | 1 | 51 | .2 | 2 | 2 | 1 | .69 | .024 | 12 | 6 | .37 | 94 | .01 | 5 | .59 | .02 | .11 | 1 | 6 | 110 |
| 1841 G | 5 | 2 | 5 | 101 | .1 | 5 | 1 | 1038 | 3.28 | 3 | 5 | ND | 1 | 36 | .2 | 2 | 3 | 1 | .40 | .020 | 11 | 4 | .26 | 96 | .01 | 3 | .35 | .02 | .10 | 1 | 5 | 100 |
| 1842 G | 5 | 3 | 6 | 87 | .1 | 5 | 1 | 1258 | 3.44 | 2 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 1 | .55 | .020 | 12 | 3 | .25 | 63 | .01 | 2 | .13 | .03 | .09 | 1 | 1 | 90 |
| 1843 G | 6 | 3 | 9 | 117 | .3 | 4 | 1 | 1132 | 3.66 | 2 | 5 | ND | 1 | 54 | .2 | 2 | 2 | 1 | .90 | .019 | 13 | 21 | .31 | 61 | .01 | 3 | .26 | .04 | .11 | 1 | 5 | 130 |
| 1844 G | 5 | 3 | 3 | 85 | .1 | 4 | 1 | 1450 | 3.63 | 2 | 5 | ND | 1 | 187 | .2 | 2 | 2 | 1 | 2.93 | .017 | 10 | 8 | .45 | 48 | .01 | 2 | .16 | .03 | .11 | 1 | 14 | 140 |
| 1845 G | 5 | 4 | 10 | 97 | .1 | 6 | 2 | 1163 | 3.04 | 5 | 5 | ND | 1 | 125 | .2 | 3 | 4 | 1 | 2.64 | .025 | 9 | 8 | .44 | 70 | .01 | 2 | .17 | .03 | .10 | 1 | 1 | 190 |
| 1858 G | 3 | 15 | 11 | 52 | 1.8 | 7 | 4 | 1293 | 2.10 | 13 | 5 | ND | 1 | 19 | .2 | 6 | 3 | 2 | 1.18 | .020 | 10 | 7 | .42 | 50 | .01 | 3 | .36 | .01 | .20 | 1 | 16 | 170 |
| 1859 G | 6 | 3 | 8 | 108 | .2 | 6 | 2 | 971 | 3.57 | 2 | 5 | ND | 1 | 73 | .2 | 2 | 2 | 4 | 1.12 | .036 | 13 | 22 | .33 | 49 | .01 | 2 | .65 | .03 | .09 | 1 | 1 | 160 |
| 1860 G | 5 | 4 | 15 | 104 | .3 | 4 | 1 | 874 | 3.27 | 7 | 5 | ND | 1 | 59 | .2 | 3 | 2 | 1 | .94 | .019 | 10 | 5 | .28 | 70 | .01 | 2 | .28 | .03 | .10 | 1 | 1 | 210 |
| 1861 G | 6 | 3 | 59 | 94 | .3 | 5 | 1 | 1134 | 3.59 | 3 | 5 | ND | 1 | 47 | .2 | 2 | 2 | 1 | .92 | .020 | 11 | 8 | .34 | 208 | .01 | 2 | .33 | .04 | .09 | 1 | 2 | 200 |
| 1862 G | 6 | 5 | 8 | 77 | .2 | 8 | 1 | 1113 | 3.52 | 6 | 5 | ND | 1 | 96 | .2 | 2 | 2 | 1 | 1.71 | .018 | 10 | 9 | .39 | 71 | .01 | 4 | .24 | .04 | .09 | 1 | 2 | 230 |
| 1863 G | 8 | 5 | 12 | 152 | .4 | 7 | 2 | 1090 | 3.90 | 4 | 5 | ND | 1 | 36 | .5 | 2 | 3 | 1 | .73 | .022 | 13 | 26 | .39 | 59 | .01 | 5 | .42 | .04 | .08 | 1 | 4 | 410 |
| 1864 G | 4 | 8 | 14 | 120 | .3 | 4 | 4 | 955 | 4.15 | 2 | 5 | ND | 1 | 150 | .3 | 3 | 2 | 9 | 2.39 | .055 | 14 | 8 | .83 | 84 | .01 | 3 | .72 | .03 | .08 | 1 | 6 | 250 |
| 1865 G | 4 | 4 | 10 | 101 | .2 | 4 | 4 | 823 | 4.09 | 2 | 5 | ND | 1 | 77 | .2 | 2 | 2 | 16 | 1.21 | .049 | 16 | 8 | .61 | 55 | .01 | 2 | .80 | .03 | .07 | 1 | 1 | 300 |
| 1866 G | 3 | 7 | 8 | 104 | .4 | 3 | 6 | 1328 | 4.54 | 6 | 5 | ND | 1 | 245 | .4 | 4 | 2 | 16 | 3.39 | .112 | 11 | 8 | .76 | 65 | .01 | 4 | .50 | .03 | .11 | 1 | 9 | 270 |
| 1867 G | 4 | 4 | 8 | 96 | .2 | 4 | 7 | 1387 | 5.38 | 3 | 5 | ND | 1 | 86 | .3 | 3 | 2 | 26 | 1.38 | .128 | 14 | 21 | .72 | 109 | .02 | 3 | .89 | .05 | .11 | 1 | 10 | 260 |
| 1868 G | 3 | 4 | 10 | 126 | .4 | 2 | 4 | 1093 | 4.79 | 3 | 5 | ND | 1 | 193 | .2 | 4 | 2 | 24 | 2.80 | .103 | 15 | 9 | .71 | 92 | .07 | 2 | 1.57 | .04 | .06 | 1 | 4 | 200 |
| 1869 G | 3 | 3 | 4 | 122 | .4 | 1 | 7 | 1077 | 5.42 | 9 | 5 | ND | 1 | 181 | .2 | 3 | 2 | 41 | 2.34 | .141 | 13 | 8 | .91 | 121 | .05 | 2 | 1.82 | .03 | .05 | 1 | 1 | 120 |
| STANDARD C/AU-R | 19 | 60 | 40 | 132 | 7.1 | 70 | 31 | 1053 | 3.97 | 40 | 21 | 7 | 37 | 52 | 18.5 | 15 | 23 | 55 | .51 | .099 | 37 | 60 | .90 | 180 | .07 | 37 | 1.88 | .06 | .14 | 11 | 496 | 1500 |

7/18/8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | ppm | ppb | ppb | |
| 1870 G | 4 | 4 | 12 | 128 | .4 | 7 | 9 | 1208 | 5.10 | 14 | 5 | ND | 1 | 200 | .8 | 5 | 2 | 41 | 2.46 | .146 | 13 | 4 | .90 | 98 | .03 | 4 | 1.94 | .05 | .10 | 2 | 6 | 120 |
| 1871 G | 4 | 3 | 2 | 138 | .6 | 4 | 9 | 1579 | 5.47 | 17 | 5 | ND | 1 | 192 | .9 | 5 | 2 | 39 | 2.24 | .149 | 12 | 9 | 1.11 | 129 | .02 | 4 | 2.13 | .04 | .13 | 1 | 7 | 180 |
| 1872 G | 3 | 2 | 5 | 135 | .4 | 3 | 8 | 1314 | 5.59 | 6 | 5 | ND | 1 | 165 | .6 | 3 | 2 | 44 | 2.08 | .164 | 15 | 3 | 1.07 | 125 | .02 | 6 | 2.16 | .06 | .14 | 1 | 7 | 120 |
| 1873 G | 3 | 3 | 9 | 126 | .4 | 6 | 8 | 990 | 5.33 | 5 | 5 | ND | 1 | 96 | .2 | 2 | 2 | 35 | 1.25 | .158 | 16 | 4 | 1.01 | 131 | .01 | 3 | 1.84 | .05 | .16 | 1 | 7 | 150 |
| 1874 G | 3 | 2 | 2 | 129 | .5 | 6 | 9 | 859 | 5.53 | 8 | 7 | ND | 1 | 94 | .8 | 4 | 2 | 40 | 1.30 | .154 | 16 | 4 | 2.01 | 116 | .01 | 4 | 2.36 | .02 | .12 | 1 | 2 | 190 |
| 1875 G | 3 | 1 | 2 | 140 | .3 | 5 | 7 | 1431 | 5.32 | 15 | 5 | ND | 1 | 279 | .7 | 2 | 2 | 35 | 3.10 | .129 | 11 | 8 | 1.25 | 127 | .01 | 2 | 2.23 | .03 | .14 | 1 | 1 | 220 |
| 1876 G | 3 | 4 | 17 | 106 | 1.4 | 6 | 9 | 1491 | 6.12 | 40 | 5 | ND | 1 | 115 | .4 | 5 | 2 | 31 | 2.00 | .145 | 10 | 3 | .82 | 73 | .02 | 3 | 1.53 | .03 | .17 | 1 | 19 | 800 |
| 1877 G | 4 | 1 | 9 | 137 | .8 | 5 | 9 | 1809 | 5.79 | 28 | 5 | ND | 1 | 83 | 1.0 | 4 | 2 | 35 | 1.90 | .152 | 13 | 3 | 1.04 | 119 | .03 | 2 | 1.77 | .03 | .15 | 1 | 2 | 210 |
| 1878 G | 4 | 5 | 22 | 137 | 2.6 | 6 | 9 | 1989 | 5.31 | 101 | 5 | ND | 1 | 55 | .2 | 9 | 2 | 22 | 1.33 | .160 | 11 | 4 | .60 | 64 | .02 | 3 | 1.10 | .02 | .22 | 1 | 35 | 470 |
| 1879 G | 4 | 4 | 5 | 119 | .5 | 6 | 9 | 1791 | 5.36 | 7 | 5 | ND | 1 | 124 | .5 | 2 | 2 | 35 | 2.28 | .135 | 13 | 8 | .91 | 114 | .03 | 2 | 1.85 | .06 | .13 | 1 | 2 | 80 |
| 1880 G | 4 | 2 | 7 | 129 | .3 | 5 | 9 | 1479 | 5.58 | 6 | 5 | ND | 1 | 92 | .6 | 3 | 2 | 42 | 1.89 | .152 | 12 | 3 | .97 | 107 | .03 | 3 | 1.90 | .06 | .14 | 1 | 5 | 100 |
| 1881 G | 3 | 5 | 4 | 138 | .5 | 7 | 10 | 1574 | 5.67 | 10 | 5 | ND | 1 | 121 | .9 | 4 | 2 | 45 | 2.35 | .166 | 13 | 4 | .96 | 129 | .05 | 6 | 1.89 | .06 | .16 | 1 | 1 | 90 |
| 1882 G | 4 | 4 | 8 | 143 | .3 | 8 | 9 | 1452 | 5.57 | 7 | 5 | ND | 1 | 130 | 1.2 | 2 | 2 | 44 | 2.37 | .152 | 14 | 4 | .94 | 139 | .08 | 5 | 1.70 | .08 | .15 | 1 | 3 | 100 |
| 1883 G | 4 | 2 | 4 | 130 | .3 | 5 | 8 | 1449 | 5.44 | 9 | 5 | ND | 1 | 197 | .7 | 2 | 2 | 39 | 2.98 | .138 | 14 | 10 | .95 | 124 | .05 | 6 | 1.90 | .07 | .11 | 1 | 6 | 80 |
| 1884 G | 3 | 5 | 2 | 131 | .2 | 5 | 8 | 1469 | 5.61 | 9 | 5 | ND | 1 | 190 | .7 | 2 | 2 | 40 | 2.98 | .146 | 12 | 4 | .94 | 121 | .06 | 3 | 1.93 | .07 | .13 | 1 | 4 | 120 |
| 1885 G | 3 | 1 | 10 | 122 | .4 | 5 | 10 | 1511 | 5.97 | 9 | 5 | ND | 1 | 179 | .7 | 4 | 2 | 45 | 2.99 | .169 | 13 | 3 | .91 | 97 | .05 | 2 | 1.93 | .06 | .10 | 1 | 3 | 200 |
| 1886 G | 3 | 5 | 8 | 135 | .2 | 4 | 9 | 1581 | 5.60 | 5 | 5 | ND | 1 | 146 | 1.0 | 2 | 2 | 36 | 2.71 | .150 | 13 | 4 | .96 | 119 | .04 | 2 | 1.85 | .05 | .12 | 1 | 4 | 180 |
| 1887 G | 4 | 3 | 13 | 185 | .5 | 5 | 9 | 1379 | 5.51 | 13 | 5 | ND | 1 | 150 | .2 | 2 | 6 | 28 | 2.55 | .154 | 10 | 5 | .80 | 81 | .01 | 2 | 1.79 | .05 | .16 | 1 | 19 | 950 |
| 1888 G | 4 | 2 | 6 | 86 | .2 | 5 | 3 | 915 | 2.92 | 6 | 5 | ND | 1 | 39 | .4 | 2 | 2 | 6 | .96 | .043 | 16 | 5 | .58 | 90 | .01 | 6 | 1.11 | .01 | .18 | 1 | 7 | 160 |
| 1889 G | 5 | 3 | 17 | 88 | .4 | 6 | 3 | 760 | 2.30 | 7 | 5 | ND | 2 | 21 | .2 | 3 | 2 | 2 | .65 | .019 | 20 | 4 | .44 | 61 | .01 | 3 | .91 | .01 | .19 | 1 | 3 | 170 |
| 1890 G | 4 | 4 | 19 | 118 | .2 | 3 | 2 | 939 | 2.18 | 6 | 5 | ND | 2 | 13 | .2 | 2 | 2 | 1 | .78 | .007 | 22 | 4 | .52 | 44 | .01 | 4 | .86 | .01 | .23 | 1 | 10 | 220 |
| 1891 G | 7 | 5 | 22 | 64 | .4 | 7 | 3 | 1354 | 2.80 | 12 | 5 | ND | 1 | 27 | .2 | 2 | 2 | 1 | 1.23 | .045 | 13 | 21 | .65 | 97 | .01 | 3 | .93 | .01 | .20 | 1 | 2 | 300 |
| 1892 G | 4 | 15 | 15 | 55 | .7 | 9 | 6 | 977 | 3.12 | 8 | 5 | ND | 2 | 19 | .2 | 7 | 2 | 10 | .86 | .034 | 17 | 5 | .64 | 56 | .01 | 4 | 1.27 | .01 | .26 | 1 | 5 | 260 |
| 1893 G | 2 | 54 | 62 | 70 | 1.6 | 14 | 12 | 889 | 4.13 | 21 | 5 | ND | 5 | 10 | .2 | 21 | 2 | 11 | .75 | .049 | 23 | 6 | .67 | 32 | .01 | 7 | 1.46 | .01 | .26 | 1 | 7 | 210 |
| 1894 G | 7 | 6 | 11 | 68 | .6 | 8 | 5 | 888 | 4.04 | 10 | 5 | ND | 2 | 11 | .5 | 3 | 2 | 3 | .60 | .032 | 15 | 5 | .62 | 66 | .01 | 2 | 1.42 | .01 | .18 | 1 | 1 | 450 |
| 1895 G | 9 | 2 | 6 | 123 | .1 | 5 | 3 | 763 | 3.94 | 12 | 5 | ND | 1 | 11 | .2 | 2 | 2 | 1 | .41 | .028 | 14 | 13 | .53 | 96 | .01 | 3 | 1.38 | .01 | .21 | 1 | 4 | 130 |
| 1896 G | 8 | 3 | 13 | 79 | .6 | 3 | 3 | 1116 | 4.37 | 11 | 5 | ND | 1 | 14 | .2 | 2 | 2 | 1 | .82 | .032 | 10 | 3 | .71 | 97 | .01 | 5 | 1.47 | .01 | .20 | 1 | 3 | 160 |
| 1897 G | 6 | 8 | 12 | 92 | .8 | 4 | 3 | 1856 | 3.94 | 12 | 5 | ND | 1 | 29 | .4 | 4 | 2 | 2 | 1.28 | .031 | 8 | 4 | .77 | 94 | .01 | 2 | 1.22 | .01 | .17 | 1 | 5 | 410 |
| 1898 G | 7 | 3 | 4 | 96 | .3 | 9 | 5 | 1840 | 3.79 | 4 | 5 | ND | 1 | 26 | .2 | 2 | 2 | 8 | 1.42 | .032 | 16 | 6 | .86 | 63 | .01 | 4 | 1.47 | .01 | .23 | 1 | 1 | 250 |
| 1899 G | 6 | 9 | 11 | 167 | .9 | 10 | 9 | 2557 | 5.34 | 10 | 5 | ND | 2 | 20 | .7 | 2 | 2 | 7 | 1.60 | .038 | 18 | 11 | 1.18 | 278 | .01 | 2 | 1.98 | .01 | .31 | 1 | 8 | 580 |
| 1900 G | 4 | 25 | 10 | 73 | 1.4 | 14 | 16 | 2517 | 5.36 | 35 | 5 | ND | 3 | 20 | .6 | 7 | 2 | 20 | 1.68 | .074 | 17 | 6 | 1.16 | 141 | .01 | 7 | 1.99 | .01 | .30 | 1 | 7 | 500 |
| 1901 G | 3 | 31 | 24 | 26 | 2.8 | 13 | 15 | 3145 | 4.59 | 22 | 6 | ND | 2 | 21 | .2 | 15 | 2 | 14 | 2.40 | .101 | 10 | 5 | 1.08 | 42 | .01 | 4 | 1.10 | .01 | .31 | 1 | 18 | 560 |
| 1902 G | 3 | 20 | 13 | 76 | 1.4 | 10 | 13 | 3850 | 2.76 | 21 | 5 | ND | 1 | 25 | .2 | 10 | 2 | 13 | 2.88 | .118 | 11 | 4 | 1.13 | 71 | .01 | 3 | .82 | .01 | .31 | 1 | 8 | 300 |
| 1903 G | 3 | 18 | 24 | 141 | 1.9 | 12 | 10 | 2028 | 2.71 | 14 | 7 | ND | 3 | 15 | .3 | 7 | 3 | 7 | 1.02 | .064 | 17 | 11 | .42 | 43 | .01 | 6 | .67 | .01 | .30 | 1 | 16 | 350 |
| 1904 G | 3 | 21 | 20 | 86 | 2.2 | 9 | 8 | 917 | 1.99 | 187 | 5 | ND | 4 | 12 | .2 | 9 | 4 | 5 | .71 | .047 | 20 | 4 | .33 | 71 | .01 | 5 | .56 | .01 | .24 | 1 | 27 | 460 |
| 1905 G | 4 | 11 | 10 | 34 | 1.5 | 7 | 3 | 1409 | 1.15 | 18 | 5 | ND | 1 | 16 | .2 | 4 | 2 | 3 | 1.30 | .026 | 14 | 6 | .43 | 40 | .01 | 4 | .40 | .01 | .24 | 2 | 4 | 200 |
| STANDARD C/AU-R | 20 | 61 | 40 | 133 | 7.3 | 73 | 32 | 1053 | 3.97 | 41 | 19 | 7 | 40 | 53 | 19.4 | 15 | 22 | 59 | .51 | .098 | 39 | 61 | .90 | 182 | .08 | 36 | 1.89 | .07 | .13 | 12 | 495 | 1600 |

7708

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|------|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | ppm | ppb | ppb | |
| 1906 G | 5 | 13 | 8 | 54 | 2.3 | 13 | 5 | 805 | 1.56 | 13 | 5 | ND | 3 | 16 | .2 | 5 | 2 | 6 | .62 | .026 | 13 | 3 | .34 | 55 | .01 | 3 | .64 | .01 | .25 | 2 | 41 | 200 |
| 1907 G | 4 | 32 | 41 | 143 | 5.8 | 12 | 24 | 659 | 7.77 | 143 | 5 | ND | 2 | 17 | .4 | 11 | 4 | 16 | .72 | .097 | 5 | 14 | .30 | 18 | .01 | 6 | .68 | .01 | .27 | 2 | 85 | 1200 |
| 1908 G | 2 | 17 | 32 | 35 | 4.2 | 6 | 23 | 1684 | 11.25 | 467 | 5 | ND | 1 | 54 | .2 | 38 | 4 | 13 | 2.47 | .125 | 4 | 3 | .91 | 13 | .01 | 3 | .39 | .01 | .21 | 1 | 77 | 1400 |
| 1909 G | 2 | 16 | 25 | 44 | 3.6 | 5 | 27 | 1168 | 7.41 | 181 | 5 | ND | 1 | 35 | .2 | 12 | 5 | 19 | 1.85 | .181 | 8 | 2 | .50 | 31 | .01 | 3 | .48 | .01 | .27 | 3 | 54 | 1900 |
| 1910 G | 2 | 16 | 27 | 120 | 3.6 | 6 | 27 | 2436 | 7.14 | 77 | 5 | ND | 1 | 59 | .3 | 8 | 2 | 58 | 2.78 | .196 | 12 | 1 | 1.28 | 35 | .01 | 2 | 1.21 | .01 | .24 | 1 | 30 | 1000 |
| 1911 G | 2 | 14 | 5 | 118 | .1 | 5 | 23 | 1398 | 7.43 | 25 | 5 | ND | 1 | 147 | .5 | 2 | 2 | 189 | 2.74 | .166 | 14 | 4 | 1.90 | 80 | .01 | 2 | 3.03 | .03 | .07 | 1 | 5 | 120 |
| 1912 G | 2 | 15 | 8 | 143 | .7 | 3 | 26 | 821 | 8.33 | 21 | 5 | ND | 1 | 84 | .9 | 2 | 3 | 207 | 1.89 | .180 | 13 | 2 | 2.40 | 66 | .01 | 2 | 3.37 | .03 | .09 | 1 | 8 | 340 |
| 1913 G | 2 | 11 | 12 | 117 | .4 | 4 | 24 | 526 | 8.52 | 18 | 5 | ND | 2 | 29 | 1.0 | 2 | 2 | 221 | .90 | .187 | 14 | 2 | 3.08 | 80 | .01 | 4 | 3.76 | .03 | .09 | 2 | 6 | 580 |
| 1914 G | 2 | 18 | 24 | 92 | 1.9 | 6 | 29 | 1710 | 8.03 | 23 | 5 | ND | 1 | 48 | 1.0 | 5 | 2 | 167 | 2.88 | .188 | 12 | 2 | 1.86 | 42 | .01 | 3 | 1.86 | .03 | .14 | 1 | 7 | 800 |
| 1915 G | 2 | 15 | 11 | 100 | .6 | 4 | 24 | 1384 | 7.49 | 14 | 5 | ND | 1 | 38 | .8 | 2 | 3 | 196 | 2.27 | .180 | 11 | 4 | 2.29 | 44 | .01 | 2 | 2.83 | .03 | .10 | 2 | 4 | 1400 |
| 1916 G | 1 | 15 | 3 | 99 | .8 | 3 | 23 | 1451 | 7.46 | 11 | 5 | ND | 1 | 41 | .9 | 2 | 2 | 202 | 2.32 | .173 | 11 | 4 | 2.02 | 54 | .01 | 2 | 2.67 | .03 | .08 | 1 | 5 | 2400 |
| 1917 G | 2 | 15 | 9 | 104 | .6 | 4 | 24 | 1091 | 8.22 | 21 | 5 | ND | 1 | 42 | .7 | 2 | 4 | 202 | 1.89 | .179 | 10 | 3 | 2.47 | 49 | .01 | 2 | 3.22 | .03 | .09 | 1 | 2 | 2000 |
| 1918 G | 3 | 16 | 19 | 80 | 1.4 | 2 | 25 | 884 | 8.18 | 35 | 5 | ND | 1 | 40 | .5 | 3 | 2 | 194 | 1.59 | .178 | 9 | 3 | 2.28 | 48 | .01 | 5 | 2.80 | .03 | .10 | 1 | 3 | 5000 |
| 1919 G | 3 | 13 | 10 | 137 | .7 | 4 | 21 | 1657 | 8.07 | 16 | 5 | ND | 1 | 87 | 1.3 | 2 | 4 | 194 | 3.24 | .145 | 9 | 5 | 2.55 | 70 | .01 | 2 | 2.95 | .03 | .08 | 1 | 2 | 1300 |
| 1920 G | 1 | 18 | 9 | 118 | .4 | 3 | 23 | 1362 | 8.53 | 18 | 5 | ND | 1 | 55 | 1.1 | 2 | 2 | 204 | 2.39 | .172 | 11 | 3 | 2.85 | 61 | .01 | 5 | 3.35 | .02 | .08 | 1 | 4 | 1400 |
| 1921 G | 2 | 10 | 5 | 141 | .6 | 1 | 22 | 2033 | 8.27 | 14 | 12 | ND | 1 | 112 | 1.3 | 2 | 2 | 213 | 3.40 | .163 | 8 | 2 | 2.70 | 48 | .01 | 2 | 3.17 | .03 | .07 | 1 | 3 | 2000 |
| 1922 G | 3 | 23 | 36 | 27 | 3.0 | 6 | 26 | 1358 | 8.78 | 39 | 5 | ND | 1 | 30 | .4 | 5 | 2 | 181 | 1.99 | .164 | 6 | 2 | 1.60 | 33 | .01 | 2 | 1.88 | .04 | .10 | 1 | 8 | 8800 |
| 1923 G | 3 | 48 | 21 | 87 | 2.8 | 4 | 26 | 1652 | 8.57 | 28 | 5 | ND | 1 | 47 | .5 | 2 | 6 | 179 | 2.75 | .166 | 11 | 4 | 2.40 | 53 | .01 | 2 | 2.58 | .03 | .10 | 1 | 10 | 950 |
| 1924 G | 5 | 36 | 20 | 153 | .9 | 17 | 10 | 1417 | 4.72 | 13 | 5 | ND | 2 | 33 | .6 | 2 | 2 | 35 | 2.43 | .068 | 11 | 6 | 1.97 | 55 | .01 | 3 | 1.94 | .01 | .24 | 1 | 6 | 280 |
| 1925 G | 5 | 19 | 105 | 506 | .2 | 17 | 9 | 1275 | 4.74 | 9 | 5 | ND | 2 | 22 | 1.6 | 2 | 4 | 27 | 2.21 | .061 | 13 | 7 | 1.93 | 51 | .01 | 3 | 2.14 | .01 | .27 | 1 | 1 | 330 |
| 1926 G | 5 | 51 | 7 | 79 | .3 | 16 | 9 | 526 | 4.51 | 18 | 5 | ND | 3 | 273 | .7 | 7 | 4 | 15 | 3.39 | .057 | 7 | 3 | 1.87 | 106 | .01 | 2 | .51 | .01 | .22 | 1 | 6 | 210 |
| 1927 G | 10 | 35 | 13 | 183 | .1 | 30 | 16 | 928 | 4.63 | 36 | 5 | ND | 2 | 42 | 1.2 | 14 | 5 | 28 | 2.80 | .086 | 7 | 5 | 1.87 | 54 | .01 | 4 | .98 | .01 | .22 | 1 | 7 | 1200 |
| 1928 G | 10 | 33 | 14 | 199 | .2 | 28 | 12 | 937 | 4.59 | 36 | 5 | ND | 3 | 32 | 1.4 | 18 | 6 | 26 | 2.79 | .078 | 11 | 5 | 2.00 | 50 | .01 | 3 | 1.19 | .01 | .21 | 1 | 9 | 1300 |
| 1929 G | 4 | 79 | 18 | 110 | .1 | 21 | 14 | 362 | 5.58 | 31 | 5 | ND | 3 | 96 | .6 | 9 | 2 | 13 | 1.05 | .059 | 11 | 2 | 1.15 | 64 | .01 | 3 | .55 | .01 | .26 | 2 | 7 | 760 |
| 1930 G | 3 | 74 | 12 | 103 | .1 | 18 | 12 | 619 | 4.97 | 34 | 5 | ND | 3 | 63 | .2 | 12 | 2 | 12 | 1.73 | .052 | 9 | 3 | 1.44 | 59 | .01 | 6 | .49 | .01 | .24 | 1 | 2 | 630 |
| 1931 G | 5 | 61 | 18 | 91 | .2 | 22 | 12 | 400 | 4.69 | 29 | 5 | ND | 3 | 31 | .2 | 12 | 2 | 11 | .97 | .064 | 10 | 4 | 1.06 | 57 | .01 | 4 | .52 | .01 | .25 | 1 | 9 | 1050 |
| 1932 G | 10 | 51 | 14 | 144 | .2 | 33 | 12 | 1072 | 4.74 | 46 | 5 | ND | 2 | 54 | 1.1 | 18 | 2 | 17 | 2.87 | .069 | 7 | 4 | 1.96 | 26 | .01 | 4 | .98 | .01 | .25 | 1 | 10 | 1300 |
| 1933 G | 7 | 21 | 11 | 192 | .8 | 10 | 3 | 3672 | 1.90 | 17 | 5 | ND | 1 | 65 | .7 | 3 | 2 | 6 | 5.77 | .044 | 8 | 2 | 2.95 | 39 | .01 | 4 | .41 | .01 | .22 | 1 | 12 | 180 |
| 1934 G | 6 | 37 | 59 | 169 | 3.7 | 21 | 12 | 3191 | 5.72 | 89 | 5 | ND | 1 | 56 | .8 | 12 | 4 | 8 | 4.98 | .061 | 6 | 2 | 2.85 | 30 | .01 | 3 | .40 | .01 | .18 | 1 | 30 | 1100 |
| 1935 G | 2 | 18 | 32 | 280 | 6.0 | 5 | 25 | 2873 | 7.63 | 178 | 9 | ND | 1 | 36 | .5 | 14 | 4 | 26 | 2.16 | .163 | 7 | 9 | .83 | 33 | .01 | 7 | .62 | .01 | .24 | 1 | 150 | 5400 |
| 1936 G | 2 | 25 | 38 | 2185 | 8.3 | 5 | 24 | 5325 | 10.33 | 398 | 5 | ND | 1 | 31 | 4.0 | 14 | 2 | 14 | 2.54 | .131 | 5 | 3 | 1.12 | 26 | .01 | 12 | .36 | .01 | .20 | 1 | 239 | 6800 |
| 1937 G | 2 | 10 | 15 | 130 | 1.8 | 4 | 22 | 4595 | 5.90 | 42 | 5 | ND | 1 | 61 | .4 | 5 | 8 | 29 | 4.62 | .177 | 8 | 2 | 2.16 | 42 | .01 | 4 | .71 | .01 | .24 | 1 | 18 | 750 |
| 1938 G | 2 | 8 | 10 | 90 | 1.1 | 5 | 25 | 3517 | 6.54 | 22 | 5 | ND | 1 | 47 | .5 | 2 | 5 | 63 | 3.48 | .176 | 8 | 2 | 1.96 | 43 | .01 | 6 | 1.30 | .01 | .22 | 1 | 19 | 330 |
| 1939 G | 2 | 9 | 18 | 151 | 2.1 | 5 | 24 | 2725 | 8.34 | 115 | 5 | ND | 1 | 36 | .5 | 4 | 2 | 108 | 2.56 | .180 | 9 | 7 | 2.23 | 37 | .01 | 3 | 2.24 | .01 | .17 | 1 | 61 | 2600 |
| 1940 G | 1 | 7 | 2 | 138 | .4 | 3 | 22 | 2777 | 7.26 | 36 | 5 | ND | 1 | 34 | .6 | 2 | 2 | 131 | 2.40 | .167 | 9 | 2 | 2.40 | 42 | .01 | 4 | 2.66 | .01 | .18 | 1 | 5 | 140 |
| 1941 G | 1 | 9 | 5 | 112 | 1.2 | 2 | 21 | 4412 | 5.55 | 19 | 5 | ND | 1 | 61 | .2 | 2 | 3 | 55 | 4.70 | .166 | 8 | 1 | 2.53 | 32 | .01 | 5 | .92 | .01 | .19 | 1 | 21 | 210 |
| STANDARD C/AU-R | 19 | 57 | 41 | 131 | 6.6 | 72 | 32 | 1049 | 3.95 | 40 | 19 | 7 | 39 | 53 | 19.5 | 15 | 18 | 55 | .51 | .094 | 38 | 56 | .92 | 182 | .07 | 37 | 1.92 | .06 | .14 | 11 | 483 | 1400 |

AP 8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|-------|------|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| 1942 G | 1 | 9 | 14 | 119 | 1.8 | 5 | 19 | 3978 | 6.15 | 60 | 5 | ND | 1 | 40 | .6 | 14 | 2 | 22 | 4.74 | .155 | 5 | 7 | 2.11 | 31 | .01 | 4 | .41 | .01 | .19 | 1 | 22 | 220 |
| 1943 G | 1 | 11 | 18 | 170 | 1.8 | 4 | 18 | 4460 | 6.82 | 22 | 5 | ND | 1 | 40 | .5 | 11 | 2 | 32 | 4.44 | .161 | 5 | 8 | 2.18 | 26 | .01 | 4 | .60 | .01 | .17 | 1 | 36 | 200 |
| 1944 G | 1 | 9 | 18 | 179 | 1.7 | 2 | 18 | 5150 | 7.38 | 20 | 8 | ND | 1 | 58 | .8 | 12 | 2 | 31 | 5.30 | .156 | 5 | 9 | 2.93 | 22 | .01 | 4 | .69 | .01 | .18 | 1 | 28 | 180 |
| 1945 G | 1 | 13 | 18 | 106 | 2.0 | 5 | 22 | 4180 | 7.71 | 31 | 5 | ND | 1 | 32 | .6 | 14 | 2 | 27 | 4.44 | .173 | 6 | 8 | 2.49 | 23 | .01 | 6 | .64 | .01 | .19 | 1 | 31 | 150 |
| 1946 G | 2 | 12 | 20 | 131 | 2.0 | 3 | 20 | 4706 | 7.25 | 23 | 5 | ND | 1 | 32 | .4 | 15 | 2 | 20 | 4.67 | .153 | 5 | 6 | 2.65 | 23 | .01 | 5 | .58 | .01 | .18 | 1 | 24 | 200 |
| 1947 G | 2 | 10 | 30 | 82 | 3.0 | 4 | 21 | 1655 | 6.93 | 405 | 5 | ND | 1 | 32 | .3 | 15 | 2 | 15 | 2.16 | .151 | 5 | 6 | .76 | 23 | .01 | 4 | .33 | .01 | .18 | 1 | 231 | 830 |
| 1948 G | 3 | 8 | 15 | 137 | 2.2 | 5 | 16 | 3707 | 7.57 | 752 | 5 | ND | 1 | 63 | .3 | 20 | 2 | 13 | 4.23 | .127 | 4 | 15 | 1.96 | 20 | .01 | 6 | .27 | .01 | .15 | 1 | 833 | 1900 |
| 1949 G | 2 | 12 | 27 | 70 | 2.7 | 5 | 20 | 2763 | 9.91 | 193 | 5 | ND | 1 | 55 | .2 | 19 | 2 | 30 | 2.90 | .151 | 3 | 9 | 1.59 | 16 | .01 | 11 | .57 | .01 | .17 | 1 | 174 | 2300 |
| 1950 G | 2 | 8 | 12 | 77 | .9 | 4 | 20 | 2266 | 6.23 | 17 | 5 | ND | 1 | 74 | .6 | 8 | 2 | 51 | 3.21 | .159 | 7 | 5 | 1.95 | 39 | .01 | 6 | 1.16 | .01 | .18 | 1 | 20 | 130 |
| 1951 G | 2 | 7 | 10 | 99 | .6 | 3 | 19 | 2728 | 8.21 | 17 | 5 | ND | 1 | 44 | .4 | 8 | 2 | 122 | 3.17 | .139 | 8 | 8 | 2.86 | 33 | .01 | 5 | 2.52 | .01 | .12 | 1 | 10 | 200 |
| 1952 G | 3 | 7 | 15 | 101 | 1.2 | 6 | 14 | 3156 | 6.33 | 1564 | 5 | ND | 1 | 256 | .2 | 11 | 2 | 52 | 6.75 | .108 | 6 | 17 | 2.71 | 60 | .01 | 3 | .55 | .01 | .10 | 1 | 114 | 650 |
| 1953 G | 2 | 10 | 36 | 22 | 3.6 | 4 | 12 | 3572 | 8.76 | 605 | 5 | ND | 1 | 94 | .2 | 20 | 2 | 13 | 4.35 | .090 | 2 | 7 | 2.60 | 17 | .01 | 10 | .27 | .01 | .14 | 1 | 97 | 1600 |
| 1954 G | 2 | 11 | 33 | 4 | 4.3 | 6 | 19 | 2309 | 9.74 | 217 | 5 | ND | 1 | 96 | .2 | 17 | 2 | 15 | 2.53 | .161 | 4 | 9 | 1.13 | 20 | .01 | 7 | .40 | .01 | .19 | 1 | 76 | 3700 |
| 1955 G | 2 | 9 | 32 | 12 | 3.8 | 4 | 14 | 4174 | 8.59 | 328 | 5 | ND | 1 | 27 | .2 | 14 | 2 | 18 | 3.66 | .119 | 2 | 7 | 2.70 | 16 | .01 | 6 | .52 | .01 | .14 | 1 | 85 | 1500 |
| 1956 G | 2 | 24 | 31 | 16 | 6.9 | 6 | 16 | 3812 | 11.18 | 503 | 5 | ND | 1 | 34 | .2 | 18 | 2 | 21 | 3.76 | .106 | 3 | 17 | 2.55 | 13 | .01 | 9 | .56 | .01 | .13 | 1 | 124 | 3200 |
| 1957 G | 6 | 3 | 15 | 15 | .8 | 6 | 2 | 2282 | 4.77 | 32 | 5 | ND | 1 | 24 | .3 | 4 | 2 | 2 | 1.70 | .017 | 6 | 3 | 1.19 | 37 | .01 | 3 | 1.34 | .01 | .09 | 1 | 21 | 280 |
| 1958 G | 6 | 2 | 11 | 26 | .4 | 4 | 1 | 1987 | 3.29 | 9 | 5 | ND | 1 | 50 | .9 | 2 | 3 | 1 | 3.21 | .020 | 7 | 5 | 1.53 | 49 | .01 | 5 | 1.17 | .01 | .09 | 1 | 11 | 180 |
| 1959 G | 5 | 3 | 7 | 46 | .4 | 7 | 1 | 1122 | 2.88 | 16 | 5 | ND | 1 | 33 | .6 | 2 | 2 | 2 | 1.78 | .019 | 8 | 7 | 1.15 | 51 | .01 | 7 | 1.14 | .01 | .10 | 2 | 11 | 140 |
| 1960 G | 8 | 3 | 12 | 28 | .3 | 7 | 1 | 497 | 2.98 | 5 | 6 | ND | 1 | 25 | .7 | 2 | 2 | 2 | .49 | .014 | 10 | 24 | .57 | 35 | .01 | 2 | 1.17 | .01 | .05 | 2 | 9 | 220 |
| 1961 G | 8 | 3 | 9 | 38 | .3 | 9 | 2 | 377 | 3.30 | 5 | 6 | ND | 2 | 8 | .6 | 2 | 3 | 5 | .10 | .014 | 11 | 5 | .70 | 56 | .01 | 3 | 1.44 | .02 | .07 | 2 | 3 | 140 |
| 1962 G | 9 | 3 | 14 | 45 | .3 | 9 | 2 | 505 | 2.80 | 8 | 6 | ND | 1 | 36 | .8 | 2 | 2 | 3 | .68 | .016 | 9 | 7 | .61 | 36 | .01 | 4 | 1.16 | .02 | .07 | 2 | 2 | 140 |
| 1963 G | 7 | 4 | 23 | 56 | .3 | 8 | 1 | 775 | 2.44 | 2 | 5 | ND | 1 | 103 | .9 | 2 | 2 | 2 | 1.89 | .019 | 9 | 7 | .51 | 45 | .01 | 5 | .98 | .02 | .05 | 1 | 1 | 90 |
| 1964 G | 11 | 3 | 23 | 61 | .3 | 11 | 2 | 440 | 2.37 | 6 | 6 | ND | 2 | 27 | .4 | 2 | 3 | 4 | .61 | .017 | 9 | 41 | .49 | 35 | .01 | 4 | .95 | .03 | .05 | 1 | 5 | 100 |
| 1965 G | 7 | 3 | 11 | 52 | .1 | 7 | 2 | 555 | 2.83 | 4 | 7 | ND | 2 | 39 | .2 | 2 | 2 | 2 | .83 | .015 | 12 | 4 | .41 | 35 | .01 | 3 | 1.10 | .03 | .05 | 2 | 9 | 80 |
| 1966 G | 7 | 3 | 11 | 68 | .1 | 8 | 2 | 813 | 2.99 | 2 | 5 | ND | 1 | 49 | .2 | 2 | 3 | 2 | 1.39 | .016 | 15 | 5 | .44 | 40 | .01 | 3 | 1.16 | .03 | .06 | 1 | 2 | 90 |
| 1967 G | 3 | 14 | 12 | 145 | .2 | 4 | 17 | 1783 | 7.13 | 2 | 5 | ND | 1 | 111 | .2 | 2 | 3 | 158 | 4.56 | .120 | 11 | 5 | 1.52 | 18 | .01 | 2 | 2.59 | .03 | .02 | 1 | 2 | 110 |
| 1968 G | 2 | 7 | 7 | 113 | .4 | 3 | 24 | 1634 | 7.90 | 19 | 5 | ND | 1 | 149 | .8 | 4 | 2 | 173 | 3.03 | .170 | 12 | 6 | 1.49 | 52 | .01 | 4 | 2.32 | .02 | .07 | 1 | 1 | 210 |
| 1969 G | 1 | 3 | 7 | 91 | .3 | 3 | 18 | 1855 | 6.77 | 10 | 5 | ND | 1 | 240 | .2 | 2 | 2 | 154 | 6.02 | .150 | 11 | 3 | 1.33 | 39 | .01 | 2 | 1.85 | .02 | .05 | 1 | 3 | 160 |
| 1970 G | 4 | 3 | 11 | 61 | .2 | 6 | 10 | 1533 | 4.97 | 10 | 5 | ND | 1 | 97 | .3 | 2 | 2 | 78 | 2.39 | .076 | 11 | 4 | 1.18 | 35 | .01 | 2 | 1.01 | .02 | .06 | 1 | 1 | 140 |
| 1971 G | 6 | 4 | 14 | 67 | .2 | 6 | 3 | 1069 | 3.33 | 13 | 5 | ND | 2 | 33 | .5 | 2 | 2 | 3 | .85 | .016 | 11 | 3 | .71 | 41 | .01 | 2 | .51 | .02 | .07 | 1 | 3 | 250 |
| 1972 G | 9 | 4 | 13 | 57 | .3 | 7 | 5 | 1021 | 3.85 | 10 | 5 | ND | 1 | 42 | .2 | 2 | 2 | 21 | .84 | .032 | 10 | 22 | .68 | 69 | .01 | 4 | .67 | .02 | .08 | 1 | 10 | 180 |
| 1973 G | 5 | 2 | 6 | 64 | .2 | 5 | 4 | 1090 | 3.33 | 9 | 5 | ND | 1 | 61 | .2 | 2 | 2 | 19 | 1.45 | .027 | 10 | 4 | .67 | 127 | .01 | 2 | .62 | .02 | .09 | 1 | 2 | 170 |
| 1974 G | 6 | 4 | 10 | 68 | .5 | 6 | 3 | 921 | 3.25 | 15 | 5 | ND | 2 | 33 | .3 | 2 | 2 | 13 | .86 | .022 | 9 | 4 | .64 | 93 | .01 | 3 | .49 | .02 | .08 | 1 | 6 | 560 |
| 1975 G | 6 | 4 | 11 | 67 | .4 | 4 | 2 | 776 | 2.64 | 11 | 5 | ND | 1 | 25 | .2 | 2 | 2 | 1 | .56 | .013 | 8 | 2 | .48 | 43 | .01 | 2 | .39 | .01 | .08 | 1 | 4 | 500 |
| 1976 G | 9 | 24 | 23 | 88 | 1.4 | 9 | 3 | 669 | 3.34 | 15 | 6 | ND | 1 | 24 | .4 | 9 | 2 | 1 | .49 | .029 | 8 | 25 | .47 | 40 | .01 | 4 | 1.01 | .03 | .05 | 1 | 5 | 680 |
| 1977 G | 7 | 19 | 20 | 51 | 1.2 | 7 | 3 | 735 | 3.62 | 19 | 8 | ND | 2 | 21 | .2 | 6 | 3 | 2 | .47 | .028 | 9 | 3 | .50 | 52 | .01 | 4 | .87 | .02 | .08 | 1 | 7 | 740 |
| STANDARD C/AU-R | 19 | 58 | 44 | 129 | 7.0 | 71 | 31 | 1047 | 3.99 | 39 | 21 | 7 | 38 | 53 | 18.7 | 15 | 19 | 56 | .52 | .097 | 38 | 60 | .88 | 180 | .07 | 33 | 1.89 | .06 | .14 | 13 | 498 | 1500 |

R108

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|-----------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 1978 G | 6 | 10 | 20 | 65 | .6 | 4 | 4 | 1809 | 4.75 | 10 | 9 | ND | 1 | 77 | .5 | 4 | 7 | 1 | 1.76 | .043 | 9 | 6 | .85 | 72 | .01 | 4 | .30 | .03 | .12 | 1 | 15 | 500 |
| 1979 G | 6 | 7 | 9 | 102 | .1 | 6 | 4 | 1067 | 4.44 | 2 | 5 | ND | 1 | 62 | .2 | 2 | 2 | 1 | .84 | .053 | 12 | 4 | .64 | 78 | .01 | 3 | .33 | .02 | .12 | 1 | 4 | 220 |
| 1980 G | 7 | 4 | 4 | 99 | .1 | 5 | 3 | 1489 | 3.84 | 2 | 5 | ND | 1 | 138 | .5 | 2 | 2 | 1 | 1.99 | .030 | 11 | 18 | .78 | 73 | .01 | 6 | .29 | .03 | .11 | 1 | 11 | 200 |
| 1981 G | 6 | 7 | 12 | 92 | .1 | 4 | 2 | 1383 | 3.47 | 7 | 5 | ND | 1 | 108 | .5 | 2 | 2 | 1 | 1.70 | .018 | 10 | 3 | .65 | 147 | .01 | 3 | .39 | .03 | .13 | 1 | 2 | 160 |
| 1982 G | 6 | 7 | 18 | 69 | .2 | 3 | 4 | 1002 | 3.88 | 7 | 5 | ND | 1 | 38 | .2 | 2 | 4 | 1 | .46 | .017 | 10 | 3 | .47 | 60 | .01 | 4 | .27 | .04 | .08 | 1 | 10 | 230 |
| 1983 G | 7 | 13 | 15 | 119 | .3 | 5 | 7 | 1156 | 5.43 | 13 | 5 | ND | 1 | 60 | .2 | 3 | 2 | 1 | .87 | .031 | 8 | 5 | .51 | 53 | .01 | 4 | .86 | .04 | .07 | 1 | 17 | 500 |
| 1984 G | 8 | 13 | 9 | 72 | .4 | 9 | 4 | 1075 | 3.82 | 64 | 5 | ND | 1 | 77 | .2 | 4 | 11 | 1 | .97 | .026 | 10 | 24 | .40 | 59 | .01 | 3 | .92 | .03 | .10 | 1 | 14 | 240 |
| 1985 G | 7 | 15 | 13 | 71 | .6 | 4 | 4 | 1015 | 3.59 | 3 | 7 | ND | 1 | 63 | .7 | 2 | 3 | 1 | .99 | .019 | 11 | 4 | .44 | 68 | .01 | 2 | 1.05 | .03 | .09 | 1 | 11 | 340 |
| 1986 G | 7 | 15 | 13 | 61 | .3 | 5 | 4 | 938 | 3.21 | 3 | 6 | ND | 1 | 47 | .3 | 3 | 2 | 1 | .80 | .010 | 12 | 4 | .38 | 60 | .01 | 9 | .91 | .02 | .10 | 1 | 6 | 310 |
| 1987 G | 6 | 65 | 20 | 63 | 1.7 | 5 | 4 | 2630 | 3.37 | 5 | 5 | ND | 1 | 239 | .5 | 4 | 2 | 1 | 3.30 | .009 | 7 | 4 | .43 | 37 | .01 | 2 | .97 | .02 | .09 | 1 | 6 | 820 |
| 1988 G | 10 | 12 | 21 | 75 | .4 | 7 | 3 | 764 | 3.31 | 6 | 5 | ND | 1 | 39 | .7 | 2 | 2 | 1 | .47 | .011 | 13 | 30 | .34 | 60 | .01 | 2 | 1.01 | .03 | .10 | 1 | 15 | 470 |
| 1989 G | 6 | 6 | 26 | 166 | .1 | 3 | 5 | 2016 | 4.71 | 2 | 5 | ND | 1 | 134 | 1.4 | 2 | 2 | 18 | 2.61 | .041 | 12 | 3 | 1.08 | 80 | .01 | 3 | 1.87 | .03 | .09 | 1 | 7 | 200 |
| 1990 G | 2 | 15 | 8 | 184 | .5 | 4 | 24 | 1743 | 8.15 | 9 | 8 | ND | 1 | 122 | 1.4 | 2 | 5 | 197 | 2.79 | .159 | 13 | 3 | 1.82 | 77 | .01 | 4 | 3.23 | .03 | .09 | 1 | 6 | 320 |
| 1991 G | 2 | 13 | 12 | 121 | .3 | 4 | 26 | 1396 | 7.83 | 33 | 5 | ND | 1 | 165 | .6 | 2 | 2 | 199 | 2.90 | .168 | 13 | 2 | 1.74 | 82 | .01 | 6 | 3.06 | .03 | .10 | 1 | 3 | 250 |
| 1992 G | 2 | 10 | 11 | 132 | .2 | 3 | 22 | 2114 | 6.97 | 9 | 7 | ND | 1 | 353 | 1.4 | 2 | 3 | 205 | 5.41 | .152 | 12 | 3 | 1.53 | 101 | .11 | 5 | 2.60 | .06 | .13 | 2 | 4 | 100 |
| 1993 G | 1 | 10 | 9 | 178 | .4 | 2 | 24 | 2149 | 7.24 | 21 | 5 | ND | 1 | 289 | 1.3 | 2 | 2 | 199 | 4.61 | .151 | 11 | 2 | 1.78 | 116 | .02 | 2 | 2.93 | .02 | .07 | 1 | 2 | 160 |
| 1994 G | 2 | 9 | 14 | 143 | .5 | 2 | 24 | 1658 | 8.00 | 26 | 5 | ND | 1 | 165 | .8 | 2 | 8 | 189 | 3.05 | .171 | 13 | 2 | 1.90 | 82 | .02 | 3 | 3.13 | .02 | .11 | 1 | 3 | 90 |
| 1995 G | 1 | 14 | 11 | 151 | .1 | 3 | 21 | 1843 | 7.21 | 14 | 5 | ND | 1 | 167 | .8 | 2 | 5 | 199 | 3.11 | .171 | 13 | 2 | 1.83 | 98 | .05 | 2 | 2.76 | .04 | .10 | 1 | 5 | 110 |
| 1996 G | 2 | 9 | 9 | 115 | .1 | 1 | 20 | 1493 | 7.18 | 4 | 5 | ND | 1 | 155 | .6 | 2 | 4 | 198 | 2.87 | .170 | 13 | 2 | 1.88 | 97 | .05 | 2 | 3.05 | .04 | .10 | 1 | 4 | 60 |
| 1997 G | 2 | 7 | 6 | 84 | .2 | 3 | 20 | 2830 | 8.24 | 9 | 7 | ND | 1 | 299 | 1.5 | 3 | 7 | 168 | 5.47 | .135 | 10 | 1 | 2.12 | 53 | .01 | 2 | 3.42 | .01 | .06 | 1 | 5 | 70 |
| 1998 G | 2 | 12 | 15 | 307 | .5 | 5 | 26 | 1560 | 8.77 | 10 | 7 | ND | 1 | 124 | 1.9 | 2 | 9 | 208 | 2.72 | .163 | 12 | 1 | 2.21 | 84 | .04 | 2 | 3.32 | .03 | .07 | 1 | 14 | 230 |
| 1999 G | 2 | 15 | 8 | 117 | .1 | 5 | 24 | 1692 | 7.42 | 10 | 5 | ND | 1 | 167 | 1.2 | 2 | 2 | 223 | 3.00 | .170 | 14 | 3 | 1.53 | 144 | .11 | 4 | 2.59 | .05 | .07 | 1 | 2 | 70 |
| 2000 G | 2 | 16 | 36 | 203 | .6 | 2 | 21 | 3466 | 7.40 | 16 | 5 | ND | 1 | 250 | 1.6 | 2 | 8 | 197 | 5.19 | .143 | 13 | 3 | 1.76 | 105 | .04 | 2 | 2.80 | .03 | .07 | 1 | 20 | 130 |
| 2001 G | 2 | 16 | 5 | 121 | .1 | 3 | 23 | 1450 | 7.92 | 2 | 5 | ND | 1 | 159 | .9 | 2 | 5 | 221 | 3.33 | .160 | 13 | 1 | 1.96 | 62 | .01 | 8 | 3.21 | .03 | .06 | 1 | 5 | 60 |
| 2002 G | 1 | 13 | 13 | 133 | .1 | 2 | 24 | 1359 | 7.80 | 2 | 5 | ND | 1 | 185 | 1.2 | 2 | 2 | 203 | 3.51 | .169 | 13 | 1 | 1.89 | 65 | .03 | 2 | 2.95 | .03 | .06 | 1 | 1 | 100 |
| 2003 G | 1 | 11 | 15 | 112 | .1 | 3 | 21 | 1438 | 7.34 | 19 | 5 | ND | 1 | 230 | .7 | 2 | 8 | 149 | 3.54 | .150 | 12 | 1 | 2.06 | 124 | .01 | 4 | 1.97 | .02 | .16 | 1 | 34 | 330 |
| 2004 G | 4 | 37 | 57 | 1308 | 1.6 | 9 | 17 | 1755 | 5.34 | 88 | 5 | ND | 1 | 244 | 5.2 | 4 | 2 | 26 | 2.79 | .096 | 8 | 3 | 1.42 | 90 | .01 | 8 | .70 | .01 | .31 | 1 | 23 | 2300 |
| 2005 G | 7 | 43 | 31 | 247 | 1.6 | 21 | 13 | 904 | 4.54 | 44 | 5 | ND | 1 | 164 | 1.3 | 6 | 2 | 27 | 2.45 | .081 | 7 | 3 | 1.17 | 39 | .01 | 2 | .75 | .01 | .21 | 1 | 18 | 500 |
| 2006 G | 16 | 38 | 44 | 185 | 2.8 | 32 | 10 | 787 | 4.20 | 45 | 5 | ND | 2 | 75 | 1.1 | 19 | 2 | 16 | 1.86 | .087 | 7 | 4 | 1.25 | 49 | .01 | 4 | 1.06 | .01 | .20 | 1 | 9 | 660 |
| 2007 G | 15 | 38 | 50 | 197 | 2.2 | 31 | 9 | 873 | 4.16 | 44 | 5 | ND | 1 | 62 | 1.2 | 18 | 4 | 14 | 1.90 | .095 | 8 | 4 | 1.38 | 21 | .01 | 2 | .88 | .01 | .19 | 1 | 8 | 760 |
| 2008 G | 13 | 35 | 34 | 156 | 1.4 | 25 | 10 | 875 | 4.79 | 36 | 5 | ND | 1 | 85 | 1.2 | 14 | 5 | 31 | 2.27 | .099 | 7 | 9 | 1.64 | 55 | .01 | 4 | 1.22 | .01 | .17 | 2 | 13 | 630 |
| 2009 G | 5 | 42 | 28 | 84 | .4 | 21 | 14 | 687 | 5.21 | 41 | 5 | ND | 1 | 135 | .2 | 7 | 2 | 30 | 2.06 | .076 | 5 | 6 | 1.38 | 27 | .01 | 2 | 1.43 | .01 | .17 | 1 | 4 | 400 |
| 2010 G | 5 | 51 | 18 | 109 | .1 | 18 | 13 | 697 | 4.90 | 33 | 5 | ND | 1 | 94 | .6 | 8 | 5 | 23 | 1.75 | .062 | 6 | 8 | 1.41 | 73 | .01 | 5 | 1.23 | .01 | .17 | 1 | 17 | 380 |
| 2011 G | 5 | 57 | 22 | 136 | .2 | 18 | 14 | 487 | 4.71 | 41 | 5 | ND | 1 | 78 | .2 | 10 | 6 | 16 | 1.08 | .074 | 6 | 5 | 1.10 | 59 | .01 | 3 | .82 | .01 | .20 | 1 | 5 | 630 |
| 2012 G | 4 | 54 | 15 | 103 | .3 | 19 | 12 | 398 | 5.14 | 48 | 5 | ND | 1 | 50 | .2 | 11 | 6 | 16 | .65 | .065 | 6 | 11 | 1.12 | 48 | .01 | 4 | 1.23 | .01 | .22 | 1 | 16 | 660 |
| 2013 G | 3 | 36 | 17 | 90 | .2 | 13 | 9 | 757 | 4.42 | 42 | 5 | ND | 1 | 133 | .2 | 6 | 2 | 18 | 2.58 | .061 | 5 | 9 | 1.52 | 52 | .01 | 3 | 1.63 | .01 | .17 | 1 | 11 | 410 |
| STANDARD C/AU-R | 19 | 59 | 38 | 129 | 6.7 | 69 | 32 | 1050 | 3.95 | 41 | 19 | 7 | 38 | 53 | 18.8 | 16 | 24 | 56 | .51 | .093 | 38 | 57 | .89 | 181 | .07 | 34 | 1.90 | .06 | .14 | 11 | 503 | 1400 |

APB

HPB
V
APP

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Hg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| 2014 G | 2 | 29 | 5 | 73 | .2 | 9 | 9 | 906 | 4.05 | 22 | 5 | ND | 1 | 77 | .2 | 4 | 2 | 16 | 2.62 | .059 | 7 | 10 | 2.17 | 83 | .01 | 6 | 1.69 | .01 | .14 | 1 | 7 | 210 |
| 2015 G | 4 | 22 | 8 | 55 | .1 | 10 | 8 | 790 | 4.15 | 34 | 5 | ND | 1 | 106 | .2 | 5 | 5 | 15 | 3.13 | .090 | 7 | 11 | 1.99 | 55 | .01 | 2 | 1.58 | .02 | .16 | 1 | 13 | 200 |
| 2016 G | 2 | 27 | 8 | 72 | .2 | 14 | 12 | 273 | 3.33 | 26 | 5 | ND | 1 | 53 | .3 | 7 | 3 | 13 | .73 | .063 | 6 | 14 | .84 | 63 | .01 | 2 | 1.10 | .02 | .18 | 1 | 11 | 270 |
| 2017 G | 2 | 36 | 22 | 88 | .1 | 10 | 14 | 287 | 3.86 | 24 | 5 | ND | 1 | 46 | .2 | 7 | 2 | 19 | .66 | .047 | 6 | 8 | .75 | 70 | .01 | 3 | 1.39 | .02 | .15 | 1 | 11 | 250 |
| 2018 G | 4 | 2 | 10 | 134 | .2 | 2 | 8 | 1509 | 5.63 | 10 | 5 | ND | 1 | 140 | .2 | 2 | 3 | 42 | 2.70 | .143 | 16 | 4 | .91 | 69 | .04 | 3 | 1.95 | .04 | .07 | 1 | 4 | 90 |
| 2019 G | 4 | 2 | 10 | 139 | .1 | 1 | 9 | 1261 | 5.78 | 4 | 5 | ND | 1 | 108 | .7 | 2 | 7 | 50 | 2.28 | .162 | 17 | 3 | .94 | 74 | .03 | 5 | 1.97 | .04 | .07 | 2 | 3 | 100 |
| 2020 G | 4 | 1 | 12 | 137 | .2 | 1 | 9 | 1278 | 5.74 | 11 | 5 | ND | 1 | 113 | .8 | 2 | 2 | 47 | 2.26 | .151 | 17 | 8 | .86 | 69 | .03 | 6 | 1.91 | .05 | .07 | 1 | 2 | 120 |
| 2021 G | 3 | 2 | 9 | 142 | .1 | 1 | 8 | 1128 | 5.67 | 9 | 5 | ND | 1 | 100 | .5 | 2 | 2 | 43 | 1.96 | .148 | 17 | 4 | .84 | 73 | .01 | 2 | 1.96 | .04 | .06 | 1 | 3 | 130 |
| 2022 G | 4 | 1 | 9 | 137 | .2 | 2 | 9 | 1496 | 5.66 | 6 | 5 | ND | 1 | 165 | .6 | 2 | 2 | 44 | 2.85 | .148 | 16 | 4 | .91 | 55 | .01 | 4 | 1.95 | .04 | .06 | 2 | 4 | 140 |
| 2023 G | 4 | 4 | 5 | 137 | .3 | 3 | 9 | 1247 | 6.03 | 9 | 5 | ND | 1 | 86 | .5 | 2 | 2 | 47 | 1.90 | .164 | 17 | 4 | 1.08 | 66 | .01 | 2 | 2.14 | .05 | .07 | 1 | 4 | 130 |
| 2024 G | 5 | 1 | 6 | 135 | .4 | 3 | 9 | 1229 | 5.47 | 10 | 5 | ND | 1 | 102 | .2 | 2 | 7 | 39 | 2.02 | .144 | 16 | 10 | .86 | 60 | .01 | 3 | 1.67 | .04 | .06 | 1 | 4 | 160 |
| 2025 G | 3 | 1 | 11 | 131 | .3 | 1 | 9 | 1080 | 5.33 | 10 | 5 | ND | 1 | 101 | .4 | 2 | 2 | 44 | 2.08 | .143 | 17 | 3 | .79 | 46 | .01 | 2 | 1.87 | .05 | .05 | 1 | 3 | 200 |
| 2026 G | 4 | 3 | 9 | 135 | .3 | 6 | 9 | 1285 | 5.48 | 11 | 5 | ND | 1 | 108 | .5 | 2 | 2 | 42 | 2.26 | .148 | 17 | 3 | .86 | 77 | .02 | 2 | 1.74 | .04 | .06 | 1 | 3 | 130 |
| 2027 G | 5 | 1 | 4 | 131 | .2 | 4 | 8 | 1233 | 5.13 | 11 | 5 | ND | 1 | 89 | .2 | 2 | 2 | 40 | 1.97 | .137 | 15 | 4 | .79 | 94 | .04 | 4 | 1.38 | .03 | .07 | 1 | 3 | 140 |
| 2028 G | 5 | 1 | 13 | 130 | .2 | 2 | 9 | 1268 | 5.47 | 8 | 5 | ND | 1 | 75 | .3 | 4 | 2 | 33 | 1.97 | .149 | 15 | 6 | .65 | 121 | .01 | 2 | 1.11 | .03 | .07 | 1 | 3 | 320 |
| 2029 G | 4 | 1 | 7 | 123 | .4 | 2 | 8 | 1143 | 5.20 | 8 | 5 | ND | 1 | 57 | .2 | 2 | 3 | 21 | 1.70 | .133 | 12 | 2 | .56 | 161 | .01 | 4 | .69 | .02 | .10 | 2 | 9 | 340 |
| 2030 G | 4 | 3 | 16 | 134 | .1 | 2 | 8 | 1418 | 5.44 | 11 | 5 | ND | 1 | 84 | .4 | 2 | 3 | 30 | 2.47 | .168 | 13 | 3 | .81 | 76 | .01 | 2 | .99 | .02 | .07 | 1 | 12 | 350 |
| 2031 G | 10 | 4 | 26 | 233 | 1.5 | 1 | 10 | 1254 | 6.50 | 91 | 5 | ND | 1 | 39 | .4 | 17 | 7 | 27 | 1.02 | .142 | 10 | 3 | .65 | 89 | .01 | 2 | .64 | .01 | .10 | 1 | 14 | 680 |
| 2032 G | 5 | 1 | 23 | 392 | 3.9 | 2 | 10 | 2205 | 9.17 | 244 | 6 | ND | 1 | 88 | 2.3 | 170 | 8 | 22 | 2.52 | .123 | 7 | 9 | .87 | 21 | .01 | 2 | .70 | .01 | .09 | 1 | 21 | 4300 |
| STANDARD C/AU-R | 19 | 58 | 37 | 131 | 6.9 | 70 | 32 | 1051 | 3.95 | 41 | 20 | 7 | 38 | 53 | 19.6 | 15 | 19 | 55 | .52 | .093 | 38 | 56 | .89 | 181 | .07 | 36 | 1.88 | .06 | .14 | 11 | 508 | 1600 |

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT 134 File # 90-4377 Page 1

2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

APP 9

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | ppm | % | % | % | ppm | ppb | ppb |
| 2039-G | 3 | 5 | 3 | 151 | .3 | 2 | 6 | 1230 | 4.98 | 16 | 5 | ND | 1 | 43 | .6 | 2 | 2 | 40 | 1.44 | .122 | 17 | 6 | .95 | 72 | .04 | 2 | 1.71 | .04 | .12 | 1 | 1 | 130 |
| 2040-G | 2 | 4 | 6 | 102 | .3 | 1 | 7 | 1165 | 5.41 | 8 | 5 | ND | 1 | 57 | .4 | 3 | 2 | 38 | 1.64 | .124 | 16 | 5 | .90 | 69 | .02 | 2 | 1.88 | .06 | .10 | 1 | 1 | 200 |
| 2041-G | 2 | 2 | 5 | 137 | .3 | 1 | 7 | 1229 | 5.02 | 6 | 5 | ND | 1 | 86 | .5 | 2 | 2 | 41 | 2.18 | .127 | 17 | 9 | .89 | 82 | .03 | 2 | 1.91 | .04 | .09 | 1 | 10 | 130 |
| 2042-G | 2 | 3 | 8 | 129 | .2 | 1 | 7 | 1231 | 5.32 | 6 | 5 | ND | 1 | 97 | .3 | 2 | 2 | 42 | 2.22 | .126 | 17 | 5 | .77 | 71 | .06 | 2 | 1.82 | .07 | .09 | 1 | 8 | 120 |
| 2043-G | 2 | 3 | 6 | 139 | .1 | 2 | 7 | 1085 | 5.64 | 6 | 5 | ND | 1 | 87 | .2 | 2 | 2 | 54 | 1.93 | .145 | 19 | 6 | .86 | 66 | .06 | 2 | 1.88 | .07 | .08 | 1 | 2 | 190 |
| 2044-G | 2 | 4 | 5 | 140 | .1 | 1 | 6 | 988 | 5.00 | 4 | 5 | ND | 1 | 85 | .5 | 2 | 2 | 45 | 1.87 | .125 | 18 | 8 | .80 | 106 | .12 | 2 | 1.69 | .07 | .17 | 1 | 16 | 110 |
| 2045-G | 3 | 3 | 6 | 128 | .1 | 2 | 6 | 1199 | 4.93 | 9 | 5 | ND | 1 | 152 | .4 | 2 | 2 | 43 | 2.77 | .121 | 17 | 7 | .75 | 71 | .07 | 2 | 1.68 | .06 | .08 | 1 | 8 | 120 |
| 2046-G | 1 | 4 | 2 | 92 | .2 | 1 | 5 | 2190 | 4.79 | 17 | 5 | ND | 1 | 212 | .3 | 3 | 3 | 37 | 4.72 | .103 | 13 | 6 | .75 | 53 | .04 | 2 | 1.70 | .07 | .08 | 1 | 36 | 150 |
| 2047-G | 4 | 4 | 8 | 177 | .2 | 1 | 7 | 1776 | 5.56 | 9 | 5 | ND | 1 | 264 | .4 | 2 | 2 | 42 | 4.09 | .121 | 15 | 7 | .78 | 51 | .05 | 2 | 1.87 | .07 | .07 | 1 | 16 | 200 |
| 2048-G | 2 | 3 | 8 | 138 | .2 | 1 | 7 | 1151 | 5.41 | 7 | 5 | ND | 1 | 99 | .4 | 2 | 3 | 47 | 2.18 | .130 | 17 | 8 | .75 | 77 | .08 | 2 | 1.84 | .09 | .09 | 1 | 3 | 130 |
| 2049-G | 3 | 3 | 7 | 140 | .1 | 2 | 7 | 1115 | 5.24 | 2 | 5 | ND | 1 | 98 | .5 | 2 | 2 | 46 | 2.18 | .122 | 20 | 6 | .72 | 58 | .04 | 4 | 1.65 | .07 | .07 | 1 | 7 | 160 |
| 2050-G | 2 | 3 | 2 | 139 | .1 | 1 | 7 | 1178 | 5.42 | 9 | 5 | ND | 1 | 102 | .5 | 2 | 3 | 47 | 2.14 | .129 | 21 | 6 | .79 | 79 | .05 | 6 | 1.62 | .08 | .10 | 1 | 1 | 130 |
| 2051-G | 3 | 4 | 5 | 289 | .1 | 1 | 7 | 1405 | 6.46 | 8 | 5 | ND | 1 | 150 | .9 | 2 | 2 | 46 | 3.00 | .130 | 18 | 7 | .94 | 39 | .02 | 2 | 2.06 | .06 | .05 | 1 | 10 | 300 |
| 2052-G | 4 | 5 | 8 | 160 | .2 | 1 | 7 | 1637 | 7.26 | 11 | 5 | ND | 1 | 140 | .2 | 3 | 2 | 52 | 3.46 | .133 | 17 | 8 | 1.22 | 51 | .02 | 2 | 2.05 | .11 | .06 | 1 | 13 | 310 |
| 2053-G | 3 | 4 | 6 | 140 | .1 | 2 | 7 | 1422 | 5.78 | 11 | 5 | ND | 1 | 101 | .3 | 2 | 3 | 48 | 2.15 | .143 | 19 | 7 | .74 | 82 | .05 | 2 | 1.58 | .08 | .11 | 1 | 12 | 160 |
| 2054-G | 2 | 3 | 3 | 135 | .1 | 1 | 7 | 1288 | 5.50 | 6 | 5 | ND | 1 | 83 | .3 | 2 | 2 | 46 | 1.93 | .133 | 18 | 5 | .75 | 88 | .05 | 2 | 1.43 | .09 | .13 | 1 | 2 | 150 |
| 2055-G | 2 | 3 | 6 | 126 | .1 | 1 | 7 | 1144 | 5.31 | 4 | 5 | ND | 1 | 98 | .2 | 2 | 2 | 45 | 2.12 | .129 | 20 | 6 | .78 | 58 | .02 | 5 | 1.74 | .06 | .07 | 1 | 3 | 170 |
| 2056-G | 3 | 4 | 6 | 128 | .1 | 2 | 7 | 1104 | 5.65 | 7 | 5 | ND | 1 | 89 | .2 | 3 | 2 | 49 | 2.05 | .141 | 19 | 8 | .82 | 59 | .02 | 2 | 1.91 | .08 | .08 | 1 | 4 | 160 |
| 2057-G | 2 | 3 | 4 | 112 | .2 | 1 | 7 | 1258 | 5.94 | 9 | 5 | ND | 1 | 104 | .3 | 4 | 2 | 51 | 2.61 | .144 | 18 | 8 | .83 | 64 | .05 | 2 | 2.05 | .08 | .09 | 1 | 12 | 220 |
| 2058-G | 3 | 4 | 6 | 131 | .1 | 1 | 8 | 1172 | 6.01 | 8 | 5 | ND | 1 | 85 | .4 | 2 | 2 | 54 | 2.03 | .149 | 17 | 9 | .84 | 93 | .07 | 4 | 2.03 | .08 | .14 | 1 | 3 | 120 |
| 2059-G | 2 | 4 | 5 | 131 | .1 | 1 | 8 | 1220 | 6.01 | 8 | 5 | ND | 1 | 99 | .2 | 2 | 2 | 57 | 2.21 | .158 | 17 | 9 | .92 | 98 | .07 | 2 | 1.96 | .10 | .14 | 1 | 10 | 110 |
| 2060-G | 2 | 3 | 18 | 141 | .1 | 1 | 8 | 1119 | 5.80 | 5 | 5 | ND | 1 | 102 | .3 | 3 | 2 | 56 | 2.13 | .158 | 17 | 8 | .92 | 74 | .05 | 2 | 2.05 | .07 | .10 | 1 | 6 | 120 |
| 2061-G | 2 | 4 | 7 | 151 | .1 | 1 | 7 | 1404 | 6.02 | 5 | 5 | ND | 1 | 181 | .5 | 2 | 3 | 46 | 3.00 | .140 | 17 | 7 | .85 | 83 | .03 | 2 | 2.06 | .07 | .10 | 1 | 7 | 170 |
| 2062-G | 2 | 4 | 9 | 138 | .1 | 1 | 8 | 1382 | 6.15 | 4 | 5 | ND | 1 | 104 | .2 | 2 | 2 | 52 | 2.52 | .146 | 17 | 8 | .94 | 64 | .03 | 2 | 1.98 | .07 | .09 | 1 | 6 | 150 |
| 2063-G | 2 | 5 | 8 | 133 | .2 | 1 | 7 | 1105 | 5.63 | 3 | 5 | ND | 1 | 85 | .2 | 2 | 2 | 47 | 2.20 | .143 | 19 | 5 | .79 | 72 | .02 | 2 | 1.96 | .08 | .10 | 1 | 9 | 140 |
| 2064-G | 3 | 3 | 2 | 141 | .1 | 3 | 7 | 1253 | 5.47 | 5 | 5 | ND | 1 | 98 | .2 | 2 | 2 | 46 | 2.16 | .134 | 18 | 7 | .80 | 96 | .09 | 2 | 1.53 | .09 | .15 | 1 | 6 | 100 |
| 2065-G | 2 | 7 | 5 | 93 | .4 | 1 | 8 | 2166 | 5.37 | 3 | 5 | ND | 1 | 136 | .2 | 3 | 2 | 42 | 3.50 | .129 | 15 | 8 | 1.33 | 49 | .02 | 2 | 1.80 | .07 | .07 | 1 | 1 | 240 |
| 2066-G | 3 | 3 | 45 | 141 | .6 | 4 | 7 | 784 | 4.98 | 3 | 5 | ND | 1 | 75 | .3 | 2 | 4 | 38 | 1.63 | .113 | 16 | 8 | .80 | 64 | .02 | 3 | 1.91 | .08 | .09 | 1 | 3236 | 260 |
| 2067-G | 1 | 2 | 58 | 105 | .1 | 1 | 4 | 3712 | 4.46 | 4 | 5 | ND | 1 | 648 | .2 | 2 | 2 | 31 | 11.17 | .076 | 14 | 6 | .64 | 38 | .01 | 2 | 1.52 | .04 | .05 | 1 | 29 | 130 |
| 2068-G | 3 | 3 | 19 | 101 | .3 | 4 | 8 | 659 | 4.58 | 6 | 7 | ND | 1 | 62 | .2 | 2 | 5 | 42 | 1.29 | .138 | 15 | 8 | .70 | 56 | .02 | 2 | 1.77 | .10 | .07 | 1 | 478 | 160 |
| 2069-G | 2 | 4 | 18 | 134 | .3 | 1 | 7 | 1030 | 5.47 | 4 | 5 | ND | 1 | 125 | .2 | 3 | 2 | 42 | 2.19 | .134 | 15 | 7 | .83 | 56 | .02 | 2 | 2.02 | .08 | .07 | 1 | 46 | 150 |
| 2070-G | 3 | 4 | 4 | 159 | .1 | 3 | 8 | 633 | 5.89 | 6 | 14 | ND | 1 | 39 | .2 | 2 | 2 | 47 | .79 | .149 | 19 | 8 | .93 | 74 | .02 | 2 | 2.20 | .06 | .09 | 1 | 12 | 110 |
| 2071-G | 2 | 6 | 5 | 133 | .1 | 1 | 7 | 1091 | 5.91 | 5 | 5 | ND | 1 | 85 | .3 | 3 | 2 | 51 | 2.21 | .154 | 17 | 8 | .85 | 77 | .08 | 3 | 2.00 | .08 | .11 | 1 | 40 | 120 |
| 2072-G | 4 | 4 | 2 | 152 | .1 | 5 | 7 | 1125 | 5.22 | 5 | 5 | ND | 1 | 79 | .2 | 2 | 2 | 50 | 1.73 | .134 | 18 | 8 | .85 | 91 | .14 | 3 | 1.31 | .09 | .22 | 1 | 15 | 90 |
| 2073-G | 2 | 4 | 4 | 130 | .2 | 1 | 7 | 1180 | 5.23 | 3 | 5 | ND | 1 | 88 | .2 | 2 | 3 | 41 | 2.42 | .133 | 17 | 5 | .77 | 62 | .02 | 2 | 1.76 | .08 | .08 | 1 | 11 | 140 |
| 2074-G | 2 | 5 | 11 | 136 | .3 | 1 | 6 | 1071 | 4.83 | 2 | 5 | ND | 1 | 75 | .2 | 2 | 2 | 41 | 2.29 | .125 | 13 | 7 | .78 | 55 | .02 | 2 | 1.79 | .07 | .09 | 1 | 36 | 130 |
| STANDARD C/AU-R | 18 | 57 | 36 | 130 | 6.7 | 69 | 32 | 1051 | 3.97 | 39 | 19 | 7 | 39 | 53 | 19.0 | 15 | 19 | 55 | .50 | .090 | 40 | 58 | .89 | 182 | .07 | 32 | 1.92 | .06 | .14 | 11 | 506 | 1500 |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1 TO P6 CORE P7 TO P9 ROCK AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: SEP 12 1990 DATE REPORT MAILED: *Sept 19/90* SIGNED BY: *[Signature]* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | AU** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | ppm | ppb | ppb | |
| 2075-G | 3 | 9 | 8 | 137 | .5 | 3 | 6 | 935 | 5.37 | 4 | 6 | ND | 1 | 60 | .2 | 2 | 3 | 36 | 1.80 | .128 | 16 | 8 | .77 | 58 | .04 | 3 | 1.69 | .05 | .09 | 1 | 37 | 100 |
| 2076-G | 2 | 4 | 9 | 113 | .5 | 2 | 7 | 1072 | 4.86 | 6 | 5 | ND | 1 | 87 | .2 | 2 | 2 | 44 | 2.52 | .126 | 16 | 7 | .78 | 50 | .02 | 4 | 1.65 | .06 | .08 | 1 | 1 | 150 |
| 2077-G | 2 | 4 | 9 | 120 | .5 | 3 | 7 | 1108 | 5.15 | 6 | 5 | ND | 1 | 85 | .2 | 2 | 2 | 48 | 2.30 | .136 | 15 | 9 | .94 | 46 | .02 | 2 | 1.91 | .08 | .07 | 1 | 21 | 160 |
| 2078-G | 2 | 5 | 5 | 139 | .4 | 1 | 6 | 1019 | 4.96 | 4 | 5 | ND | 1 | 76 | .2 | 2 | 2 | 45 | 2.10 | .126 | 17 | 6 | .80 | 53 | .02 | 2 | 1.72 | .07 | .08 | 1 | 2 | 110 |
| 2079-G | 5 | 5 | 4 | 173 | .6 | 2 | 3 | 1003 | 5.73 | 5 | 5 | ND | 1 | 39 | .2 | 2 | 4 | 2 | .58 | .050 | 14 | 4 | .68 | 65 | .01 | 2 | .57 | .02 | .14 | 1 | 3 | 390 |
| 2080-G | 5 | 5 | 4 | 114 | .3 | 2 | 3 | 1523 | 4.60 | 22 | 5 | ND | 1 | 172 | .2 | 2 | 2 | 5 | 2.62 | .042 | 7 | 4 | .49 | 107 | .01 | 2 | .59 | .01 | .11 | 1 | 4 | 400 |
| 2081-G | 3 | 11 | 4 | 118 | .3 | 5 | 4 | 707 | 4.88 | 9 | 10 | ND | 1 | 26 | .2 | 2 | 2 | 12 | .35 | .037 | 13 | 5 | .54 | 81 | .01 | 2 | .69 | .02 | .11 | 1 | 6 | 430 |
| 2082-G | 3 | 27 | 9 | 149 | .5 | 18 | 15 | 1280 | 6.18 | 40 | 5 | ND | 1 | 75 | .3 | 4 | 2 | 27 | 1.18 | .068 | 13 | 10 | .79 | 186 | .01 | 3 | .58 | .01 | .24 | 1 | 5 | 420 |
| 2083-G | 3 | 14 | 10 | 139 | .7 | 12 | 13 | 1609 | 5.97 | 23 | 9 | ND | 1 | 59 | .3 | 2 | 3 | 39 | 1.36 | .083 | 21 | 11 | .93 | 78 | .01 | 2 | 1.03 | .03 | .16 | 1 | 9 | 360 |
| 2084-G | 8 | 6 | 19 | 118 | .7 | 5 | 7 | 1221 | 4.43 | 13 | 5 | ND | 2 | 59 | .3 | 4 | 2 | 25 | 1.16 | .045 | 23 | 6 | .81 | 64 | .01 | 3 | 1.00 | .03 | .18 | 1 | 1 | 280 |
| 2085-G | 13 | 10 | 25 | 94 | .8 | 7 | 3 | 846 | 3.13 | 5 | 7 | ND | 1 | 34 | .5 | 2 | 2 | 1 | .72 | .017 | 17 | 7 | .58 | 41 | .01 | 2 | .80 | .04 | .09 | 1 | 1 | 230 |
| 2086-G | 9 | 64 | 9 | 101 | 1.0 | 3 | 3 | 1220 | 3.46 | 7 | 5 | ND | 1 | 32 | .2 | 3 | 3 | 2 | .99 | .016 | 15 | 3 | .65 | 70 | .01 | 2 | .74 | .06 | .06 | 1 | 3 | 210 |
| 2087-G | 6 | 10 | 6 | 87 | .2 | 7 | 1 | 425 | 2.86 | 6 | 17 | ND | 1 | 16 | .2 | 2 | 3 | 1 | .24 | .015 | 14 | 7 | .32 | 72 | .01 | 2 | .53 | .04 | .11 | 1 | 1 | 220 |
| 2088-G | 4 | 3 | 10 | 108 | .2 | 1 | 1 | 911 | 3.44 | 6 | 9 | ND | 1 | 23 | .2 | 2 | 2 | 1 | .58 | .012 | 13 | 3 | .39 | 117 | .01 | 3 | .75 | .04 | .14 | 1 | 2 | 160 |
| 2089-G | 6 | 4 | 9 | 138 | .2 | 7 | 1 | 555 | 2.63 | 5 | 8 | ND | 1 | 32 | .4 | 2 | 3 | 1 | .55 | .011 | 18 | 6 | .36 | 64 | .01 | 2 | .95 | .02 | .12 | 1 | 8 | 220 |
| 2090-G | 5 | 4 | 11 | 141 | .1 | 2 | 1 | 775 | 3.20 | 2 | 5 | ND | 1 | 51 | .5 | 2 | 2 | 1 | .73 | .011 | 18 | 3 | .35 | 56 | .01 | 2 | 1.02 | .06 | .10 | 1 | 1 | 150 |
| 2091-G | 8 | 5 | 12 | 142 | .1 | 6 | 2 | 945 | 3.35 | 2 | 6 | ND | 2 | 73 | .2 | 2 | 2 | 8 | 1.26 | .038 | 25 | 6 | .16 | 261 | .09 | 2 | .76 | .09 | .07 | 1 | 2 | 60 |
| 2092-G | 6 | 13 | 10 | 141 | .5 | 2 | 1 | 842 | 3.13 | 2 | 9 | ND | 2 | 49 | .3 | 2 | 2 | 3 | .89 | .013 | 17 | 2 | .13 | 53 | .06 | 2 | .61 | .05 | .07 | 1 | 172 | 80 |
| 2093-G | 8 | 5 | 15 | 140 | .2 | 6 | 1 | 1068 | 3.24 | 3 | 5 | ND | 2 | 73 | .4 | 2 | 4 | 3 | 1.13 | .014 | 24 | 4 | .15 | 112 | .08 | 2 | 1.03 | .07 | .10 | 1 | 7 | 70 |
| 2094-G | 7 | 5 | 16 | 157 | .2 | 3 | 1 | 702 | 3.19 | 10 | 9 | ND | 2 | 20 | .4 | 2 | 2 | 1 | .34 | .011 | 22 | 2 | .47 | 113 | .01 | 2 | .46 | .01 | .13 | 1 | 1 | 180 |
| 2098-G | 17 | 4 | 8 | 79 | .5 | 7 | 4 | 1677 | 2.85 | 13 | 7 | ND | 1 | 36 | .2 | 3 | 2 | 4 | 1.53 | .022 | 17 | 7 | .91 | 85 | .01 | 2 | .39 | .01 | .20 | 1 | 1 | 150 |
| 2099-G | 6 | 6 | 7 | 135 | .3 | 2 | 1 | 1171 | 2.90 | 51 | 5 | ND | 1 | 55 | .3 | 2 | 2 | 1 | 1.12 | .008 | 12 | 3 | .44 | 67 | .01 | 2 | .50 | .01 | .16 | 1 | 12 | 140 |
| 2100-G | 5 | 8 | 7 | 137 | .6 | 6 | 4 | 1817 | 2.67 | 25 | 5 | ND | 1 | 50 | .2 | 4 | 2 | 3 | 1.74 | .039 | 11 | 7 | .86 | 76 | .01 | 2 | .39 | .01 | .21 | 1 | 2 | 150 |
| 2107-G | 2 | 32 | 10 | 74 | 1.9 | 24 | 15 | 3607 | 4.03 | 50 | 5 | ND | 1 | 40 | .2 | 13 | 2 | 7 | 3.16 | .108 | 8 | 8 | 1.33 | 40 | .01 | 4 | .47 | .01 | .25 | 1 | 10 | 130 |
| 2108-G | 1 | 37 | 10 | 66 | 1.7 | 29 | 18 | 2935 | 4.69 | 50 | 5 | ND | 1 | 41 | .3 | 12 | 2 | 9 | 2.70 | .095 | 8 | 9 | 1.29 | 42 | .01 | 2 | .53 | .01 | .28 | 1 | 7 | 120 |
| 2109-G | 1 | 39 | 7 | 40 | 1.4 | 32 | 19 | 3116 | 5.04 | 47 | 5 | ND | 1 | 39 | .2 | 8 | 2 | 15 | 2.76 | .093 | 8 | 10 | 1.57 | 49 | .01 | 4 | .56 | .01 | .25 | 1 | 12 | 100 |
| 2110-G | 2 | 44 | 7 | 104 | 1.4 | 36 | 19 | 2434 | 5.19 | 38 | 5 | ND | 1 | 37 | .2 | 8 | 2 | 23 | 2.00 | .062 | 7 | 16 | 1.83 | 50 | .01 | 4 | .94 | .01 | .22 | 1 | 5 | 130 |
| 2111-G | 1 | 43 | 6 | 111 | 1.4 | 40 | 19 | 2583 | 6.39 | 33 | 5 | ND | 1 | 38 | .3 | 9 | 2 | 27 | 2.32 | .059 | 6 | 19 | 2.17 | 45 | .01 | 2 | 1.25 | .01 | .19 | 1 | 5 | 130 |
| 2112-G | 1 | 32 | 9 | 103 | 1.4 | 39 | 18 | 1703 | 6.34 | 49 | 6 | ND | 1 | 30 | .4 | 9 | 3 | 29 | 1.53 | .063 | 7 | 18 | 1.89 | 47 | .01 | 3 | 1.40 | .01 | .20 | 1 | 5 | 140 |
| 2113-G | 1 | 37 | 5 | 157 | 1.0 | 30 | 18 | 2150 | 5.28 | 28 | 5 | ND | 1 | 35 | .6 | 5 | 2 | 30 | 2.05 | .064 | 10 | 18 | 2.02 | 46 | .01 | 4 | 1.47 | .01 | .21 | 1 | 11 | 120 |
| 2114-G | 2 | 32 | 8 | 93 | 1.2 | 34 | 20 | 2090 | 5.90 | 29 | 5 | ND | 1 | 37 | .3 | 8 | 2 | 32 | 2.00 | .070 | 12 | 19 | 2.21 | 111 | .01 | 3 | 1.34 | .01 | .22 | 1 | 10 | 130 |
| 2115-G | 1 | 43 | 8 | 142 | 1.3 | 40 | 19 | 2457 | 5.64 | 51 | 5 | ND | 1 | 35 | .5 | 7 | 2 | 31 | 2.37 | .050 | 7 | 20 | 2.08 | 49 | .01 | 3 | 1.10 | .01 | .18 | 1 | 3 | 160 |
| 2116-G | 3 | 29 | 10 | 143 | 1.6 | 22 | 11 | 1719 | 3.58 | 55 | 5 | ND | 2 | 43 | .4 | 13 | 2 | 9 | 1.85 | .039 | 13 | 8 | 1.35 | 70 | .01 | 3 | .47 | .01 | .23 | 1 | 22 | 180 |
| 2117-G | 4 | 15 | 9 | 136 | .9 | 8 | 6 | 1528 | 1.56 | 23 | 5 | ND | 2 | 29 | .4 | 8 | 2 | 2 | 1.64 | .025 | 14 | 4 | .74 | 55 | .01 | 2 | .39 | .01 | .21 | 1 | 20 | 100 |
| 2118-G | 4 | 24 | 23 | 136 | 2.7 | 17 | 12 | 1469 | 4.20 | 262 | 6 | ND | 1 | 60 | .2 | 12 | 4 | 4 | 1.83 | .033 | 5 | 6 | .83 | 51 | .01 | 2 | .41 | .01 | .23 | 1 | 113 | 200 |
| 2124-G | 1 | 16 | 5 | 59 | .5 | 7 | 5 | 2663 | 4.14 | 12 | 5 | ND | 1 | 48 | .2 | 5 | 2 | 8 | 4.37 | .045 | 9 | 5 | 2.43 | 66 | .01 | 3 | .38 | .01 | .18 | 1 | 7 | 110 |
| STANDARD C/AU-R | 18 | 57 | 38 | 130 | 7.0 | 70 | 32 | 1051 | 3.98 | 40 | 19 | 7 | 39 | 53 | 18.6 | 15 | 20 | 55 | .50 | .090 | 39 | 60 | .89 | 182 | .07 | 34 | 1.88 | .06 | .14 | 11 | 487 | 1500 |

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT 134 File # 90-4231

2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|-----|-----|------|-------|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| LS-UR-90-99 | 1 | 50 | 16 | 42 | .1 | 7 | 10 | 817 | 2.98 | 146 | 5 | ND | 1 | 228 | .5 | 7321 | 2 | 15 | 3.82 | .104 | 3 | 8 | .72 | 21 | .01 | 7 | .21 | .01 | .13 | 1 | 161 | 110 |
| UR-90-BB-6 | 1 | 231 | 35 | 77 | .1 | 6 | 8 | 208 | 1.18 | 2 | 5 | ND | 1 | 44 | .5 | 57949 | 51 | 5 | .39 | .008 | 2 | 1 | .02 | 3 | .01 | 6 | .09 | .01 | .05 | 1 | 53 | 210 |
| LS-UR-100A-90 | 1 | 122 | 8 | 63 | .5 | 10 | 22 | 1233 | 6.96 | 11 | 5 | ND | 1 | 331 | .2 | 1755 | 2 | 137 | 6.94 | .158 | 7 | 19 | 1.60 | 45 | .01 | 7 | 1.34 | .03 | .13 | 1 | 5 | 120 |
| 2095 G | 6 | 7 | 13 | 126 | .6 | 2 | 2 | 944 | 2.89 | 31 | 5 | ND | 1 | 28 | .6 | 36 | 2 | 2 | .67 | .012 | 12 | 4 | .55 | 28 | .01 | 4 | .37 | .01 | .13 | 1 | 6 | 170 |
| 2096 G | 5 | 12 | 12 | 111 | 1.1 | 5 | 4 | 1938 | 4.21 | 30 | 5 | ND | 1 | 153 | .4 | 17 | 2 | 4 | 3.46 | .018 | 4 | 8 | 1.53 | 33 | .01 | 3 | .33 | .01 | .15 | 1 | 15 | 100 |
| 2097 G | 6 | 11 | 8 | 140 | 1.7 | 5 | 4 | 2222 | 2.61 | 9 | 5 | ND | 1 | 57 | .3 | 63 | 3 | 7 | 2.32 | .040 | 18 | 10 | 1.13 | 114 | .01 | 2 | .36 | .01 | .20 | 1 | 11 | 140 |
| 2101 G | 4 | 15 | 15 | 79 | 1.1 | 8 | 8 | 1579 | 3.19 | 16 | 5 | ND | 1 | 31 | .4 | 11 | 2 | 3 | 1.50 | .048 | 9 | 7 | .68 | 41 | .01 | 4 | .45 | .01 | .23 | 1 | 9 | 70 |
| 2102 G | 4 | 16 | 13 | 101 | 1.3 | 11 | 9 | 2470 | 4.09 | 21 | 5 | ND | 1 | 44 | .3 | 18 | 3 | 5 | 2.45 | .076 | 7 | 8 | 1.01 | 32 | .01 | 11 | .45 | .01 | .25 | 1 | 7 | 90 |
| 2103 G | 4 | 15 | 13 | 66 | 1.2 | 16 | 14 | 2720 | 3.70 | 44 | 5 | ND | 1 | 46 | .2 | 12 | 4 | 4 | 2.59 | .055 | 6 | 10 | 1.09 | 34 | .01 | 4 | .33 | .01 | .20 | 1 | 9 | 60 |
| 2104 G | 8 | 12 | 8 | 161 | .9 | 12 | 8 | 1876 | 1.63 | 57 | 5 | ND | 2 | 34 | .4 | 15 | 3 | 2 | 1.93 | .040 | 13 | 6 | .79 | 36 | .01 | 6 | .37 | .01 | .21 | 1 | 9 | 70 |
| 2105 G | 3 | 22 | 33 | 90 | 6.6 | 19 | 10 | 1581 | 4.95 | 1170 | 5 | ND | 1 | 48 | .2 | 23 | 2 | 3 | 1.67 | .035 | 6 | 8 | .70 | 36 | .01 | 4 | .39 | .01 | .22 | 1 | 787 | 180 |
| 2106 G | 3 | 12 | 60 | 179 | 8.2 | 11 | 7 | 1434 | 5.10 | 3708 | 5 | 3 | 1 | 73 | .2 | 43 | 2 | 2 | 2.48 | .023 | 5 | 8 | .98 | 33 | .01 | 3 | .31 | .01 | .18 | 1 | 3298 | 320 |
| 2119 G | 9 | 26 | 46 | 198 | 6.7 | 22 | 10 | 450 | 5.52 | 489 | 5 | ND | 1 | 49 | .4 | 18 | 2 | 5 | .97 | .058 | 3 | 7 | .39 | 39 | .01 | 3 | .38 | .01 | .21 | 1 | 211 | 250 |
| 2120 G | 2 | 7 | 21 | 79 | 2.3 | 4 | 5 | 1962 | 6.66 | 1831 | 5 | ND | 1 | 48 | .2 | 18 | 2 | 2 | 3.33 | .017 | 3 | 9 | 1.60 | 19 | .01 | 2 | .24 | .01 | .14 | 1 | 423 | 160 |
| 2121 G | 4 | 11 | 27 | 14 | 2.4 | 11 | 7 | 1462 | 3.89 | 781 | 5 | ND | 1 | 52 | .2 | 17 | 2 | 4 | 3.46 | .018 | 2 | 7 | 1.64 | 30 | .01 | 6 | .28 | .01 | .16 | 1 | 237 | 90 |
| 2122 G | 7 | 22 | 29 | 84 | 2.3 | 19 | 12 | 1024 | 3.90 | 199 | 5 | ND | 1 | 43 | .2 | 15 | 2 | 6 | 2.44 | .051 | 4 | 8 | .86 | 39 | .01 | 3 | .43 | .01 | .24 | 1 | 95 | 130 |
| 2123 G | 2 | 14 | 10 | 19 | 1.4 | 9 | 7 | 3197 | 4.31 | 28 | 5 | ND | 1 | 46 | .2 | 12 | 2 | 3 | 5.46 | .032 | 4 | 6 | 2.64 | 25 | .01 | 5 | .26 | .01 | .15 | 1 | 10 | 70 |
| 2130 G | 1 | 13 | 3 | 65 | .3 | 4 | 6 | 2593 | 4.04 | 7 | 5 | ND | 1 | 99 | .2 | 5 | 2 | 20 | 4.95 | .038 | 8 | 7 | 2.78 | 37 | .01 | 3 | .78 | .01 | .11 | 1 | 4 | 60 |
| STANDARD C/AU-R | 19 | 58 | 37 | 132 | 7.0 | 71 | 31 | 1052 | 3.94 | 40 | 20 | 7 | 38 | 53 | 18.5 | 15 | 22 | 55 | .51 | .099 | 38 | 60 | .90 | 181 | .07 | 38 | 1.88 | .06 | .14 | 13 | 495 | 1300 |

6/19

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR MH FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: ROCK/CORE AU** ANALYSIS BY FA\ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: SEP 8 1990

DATE REPORT MAILED: Sept 13/90

SIGNED BY: *C. Leong*, D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Tl | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| 2125-G | 2 | 13 | 2 | 116 | .5 | 7 | 6 | 2876 | 4.03 | 14 | 5 | ND | 1 | 48 | .4 | 4 | 2 | 9 | 4.85 | .052 | 7 | 7 | 2.75 | 69 | .01 | 2 | .36 | .01 | .17 | 1 | 16 | 100 |
| 2126-G | 2 | 18 | 2 | 90 | .4 | 12 | 9 | 1692 | 3.94 | 17 | 5 | ND | 1 | 37 | .4 | 4 | 2 | 15 | 2.61 | .038 | 12 | 12 | 1.96 | 68 | .01 | 2 | .75 | .02 | .17 | 1 | 3 | 60 |
| 2127-G | 1 | 20 | 5 | 60 | .7 | 28 | 23 | 1800 | 4.72 | 40 | 5 | ND | 1 | 45 | .2 | 5 | 2 | 41 | 2.95 | .075 | 6 | 21 | 2.30 | 84 | .01 | 4 | 1.09 | .01 | .18 | 1 | 9 | 50 |
| 2128-G | 3 | 21 | 6 | 77 | .7 | 22 | 18 | 2153 | 5.07 | 49 | 5 | ND | 1 | 48 | .2 | 6 | 2 | 35 | 3.52 | .075 | 6 | 19 | 2.48 | 95 | .01 | 2 | 1.14 | .01 | .20 | 1 | 11 | 70 |
| 2129-G | 1 | 11 | 2 | 95 | .2 | 7 | 5 | 1769 | 3.24 | 6 | 5 | ND | 1 | 37 | .3 | 3 | 2 | 6 | 2.96 | .025 | 12 | 7 | 2.04 | 44 | .01 | 2 | .53 | .01 | .15 | 1 | 6 | 50 |
| 2131-G | 4 | 3 | 4 | 83 | .1 | 1 | 1 | 1824 | 2.57 | 2 | 5 | ND | 1 | 165 | .4 | 2 | 2 | 1 | 4.20 | .012 | 13 | 6 | 1.61 | 72 | .01 | 2 | .41 | .01 | .18 | 1 | 5 | 180 |
| 2132-G | 3 | 9 | 3 | 126 | .1 | 3 | 4 | 1566 | 3.76 | 5 | 7 | ND | 1 | 46 | .5 | 2 | 2 | 11 | 2.77 | .037 | 14 | 8 | 1.90 | 53 | .01 | 2 | .70 | .01 | .16 | 1 | 2 | 70 |
| 2133-G | 3 | 60 | 38 | 120 | 2.1 | 19 | 12 | 519 | 5.36 | 55 | 5 | ND | 1 | 47 | .5 | 10 | 2 | 19 | .97 | .066 | 4 | 9 | 1.17 | 70 | .01 | 4 | .56 | .01 | .26 | 1 | 16 | 190 |
| 2134-G | 3 | 60 | 20 | 135 | 1.3 | 17 | 12 | 566 | 5.28 | 47 | 5 | ND | 1 | 42 | .4 | 11 | 2 | 21 | .83 | .048 | 4 | 9 | 1.16 | 69 | .01 | 7 | .47 | .01 | .20 | 1 | 14 | 170 |
| 2135-G | 2 | 69 | 10 | 112 | .6 | 14 | 12 | 764 | 5.00 | 37 | 5 | ND | 1 | 51 | .6 | 10 | 2 | 23 | 1.29 | .045 | 4 | 8 | 1.38 | 83 | .01 | 3 | .53 | .01 | .22 | 1 | 1 | 180 |
| 2136-G | 1 | 64 | 9 | 98 | .4 | 11 | 10 | 672 | 4.01 | 33 | 5 | ND | 1 | 48 | .3 | 9 | 3 | 16 | 1.28 | .050 | 4 | 9 | 1.18 | 70 | .01 | 4 | .47 | .01 | .22 | 1 | 3 | 170 |
| 2137-G | 2 | 61 | 13 | 82 | .5 | 15 | 11 | 728 | 5.10 | 36 | 5 | ND | 1 | 77 | .2 | 10 | 2 | 22 | 1.37 | .045 | 3 | 8 | 1.17 | 70 | .01 | 6 | .55 | .01 | .23 | 1 | 10 | 200 |
| 2138-G | 2 | 44 | 19 | 90 | 1.0 | 13 | 10 | 1291 | 4.56 | 37 | 5 | ND | 1 | 102 | .3 | 8 | 2 | 14 | 3.10 | .052 | 2 | 8 | 1.55 | 62 | .01 | 3 | .50 | .01 | .21 | 1 | 16 | 280 |
| 2139-G | 2 | 34 | 24 | 69 | .7 | 10 | 10 | 638 | 4.70 | 33 | 5 | ND | 1 | 43 | .3 | 7 | 2 | 16 | 1.04 | .073 | 4 | 8 | .80 | 69 | .01 | 4 | .58 | .02 | .23 | 1 | 8 | 350 |
| 2140-G | 2 | 37 | 27 | 89 | .6 | 13 | 9 | 835 | 6.44 | 41 | 5 | ND | 1 | 47 | .4 | 10 | 4 | 19 | 1.18 | .070 | 3 | 11 | .98 | 42 | .01 | 3 | .50 | .01 | .19 | 1 | 7 | 340 |
| 2141-G | 1 | 26 | 9 | 63 | .6 | 9 | 7 | 1806 | 3.87 | 24 | 5 | ND | 1 | 100 | .2 | 6 | 2 | 14 | 3.27 | .052 | 3 | 9 | 1.66 | 61 | .01 | 2 | .40 | .01 | .17 | 1 | 7 | 210 |
| 2142-G | 3 | 74 | 30 | 152 | 1.3 | 23 | 17 | 621 | 5.16 | 34 | 5 | ND | 1 | 57 | .6 | 6 | 2 | 29 | 1.31 | .062 | 5 | 17 | .94 | 70 | .01 | 2 | 1.90 | .01 | .22 | 2 | 8 | 310 |
| 2143-G | 3 | 58 | 19 | 155 | .8 | 18 | 14 | 1239 | 5.86 | 31 | 5 | ND | 1 | 99 | .4 | 8 | 2 | 27 | 2.78 | .056 | 4 | 19 | 1.29 | 76 | .01 | 2 | 2.13 | .01 | .22 | 1 | 9 | 360 |
| 2144-G | 3 | 17 | 7 | 9 | .3 | 6 | 2 | 1490 | 3.29 | 79 | 7 | ND | 1 | 61 | .4 | 3 | 2 | 3 | 2.64 | .012 | 7 | 9 | .85 | 56 | .01 | 2 | .46 | .01 | .17 | 1 | 67 | 120 |
| 2145-G | 2 | 13 | 5 | 1 | .4 | 2 | 2 | 977 | 3.57 | 145 | 5 | ND | 1 | 50 | .2 | 2 | 3 | 1 | 1.94 | .008 | 5 | 4 | .47 | 51 | .01 | 2 | .27 | .01 | .15 | 1 | 100 | 70 |
| 2146-G | 4 | 8 | 6 | 10 | .4 | 5 | 2 | 1053 | 3.81 | 85 | 5 | ND | 1 | 23 | .3 | 3 | 2 | 1 | 1.48 | .009 | 9 | 8 | .82 | 56 | .01 | 2 | .64 | .01 | .17 | 1 | 52 | 30 |
| 2147-G | 3 | 5 | 5 | 50 | .2 | 3 | 1 | 792 | 2.62 | 23 | 5 | ND | 2 | 20 | .3 | 2 | 2 | 1 | 1.05 | .010 | 14 | 4 | .53 | 61 | .01 | 3 | .56 | .01 | .18 | 1 | 10 | 20 |
| 2148-G | 4 | 3 | 4 | 29 | .3 | 5 | 2 | 488 | 2.53 | 16 | 5 | ND | 2 | 21 | .2 | 2 | 2 | 1 | .65 | .005 | 13 | 6 | .49 | 65 | .01 | 2 | .83 | .01 | .18 | 1 | 11 | 30 |
| 2149-G | 3 | 4 | 7 | 48 | .3 | 2 | 2 | 637 | 2.99 | 19 | 5 | ND | 2 | 24 | .3 | 2 | 2 | 1 | .86 | .007 | 12 | 5 | .56 | 56 | .01 | 2 | .84 | .01 | .17 | 1 | 12 | 50 |
| 2150-G | 3 | 2 | 6 | 33 | .1 | 6 | 2 | 668 | 2.22 | 9 | 5 | ND | 1 | 31 | .2 | 2 | 2 | 1 | 1.05 | .005 | 14 | 7 | .50 | 54 | .01 | 2 | .71 | .01 | .15 | 1 | 10 | 30 |
| 2151-G | 4 | 7 | 20 | 34 | .5 | 3 | 4 | 660 | 3.43 | 18 | 5 | ND | 1 | 21 | .3 | 4 | 2 | 1 | .94 | .004 | 11 | 4 | .54 | 44 | .01 | 2 | .71 | .01 | .14 | 1 | 29 | 70 |
| 2152-G | 4 | 5 | 12 | 92 | .3 | 5 | 2 | 823 | 3.85 | 9 | 5 | ND | 1 | 19 | .4 | 2 | 2 | 2 | 1.01 | .012 | 13 | 8 | .78 | 50 | .01 | 2 | 1.14 | .01 | .15 | 1 | 10 | 110 |
| 2153-G | 3 | 7 | 8 | 98 | .2 | 1 | 2 | 704 | 3.13 | 8 | 5 | ND | 3 | 27 | .6 | 2 | 2 | 2 | .99 | .012 | 20 | 5 | .62 | 61 | .01 | 5 | 1.11 | .02 | .14 | 1 | 3 | 120 |
| 2154-G | 5 | 19 | 8 | 47 | .4 | 8 | 2 | 861 | 3.95 | 14 | 5 | ND | 1 | 21 | .2 | 2 | 2 | 2 | 1.27 | .013 | 11 | 11 | .66 | 49 | .01 | 2 | .82 | .01 | .20 | 1 | 52 | 80 |
| 2155-G | 2 | 4 | 6 | 57 | .2 | 2 | 1 | 1872 | 3.43 | 3 | 5 | ND | 1 | 25 | .2 | 2 | 2 | 1 | 2.38 | .009 | 14 | 6 | 1.36 | 48 | .01 | 2 | .97 | .01 | .14 | 1 | 11 | 40 |
| 2156-G | 3 | 2 | 8 | 59 | .3 | 5 | 1 | 831 | 3.23 | 14 | 5 | ND | 1 | 12 | .2 | 2 | 2 | 1 | 1.16 | .010 | 11 | 8 | .84 | 48 | .01 | 2 | .90 | .01 | .17 | 1 | 6 | 120 |
| 2157-G | 3 | 3 | 8 | 82 | .4 | 2 | 1 | 927 | 3.24 | 29 | 5 | ND | 2 | 13 | .3 | 2 | 2 | 1 | 1.51 | .010 | 11 | 6 | .89 | 56 | .01 | 2 | .73 | .01 | .18 | 1 | 29 | 150 |
| 2158-G | 3 | 1 | 6 | 69 | .2 | 5 | 1 | 921 | 2.90 | 18 | 5 | ND | 3 | 15 | .2 | 2 | 2 | 1 | 1.20 | .010 | 18 | 8 | .81 | 46 | .01 | 4 | .97 | .01 | .18 | 1 | 6 | 60 |
| 2159-G | 1 | 3 | 6 | 59 | .3 | 1 | 1 | 720 | 2.35 | 21 | 5 | ND | 2 | 29 | .3 | 2 | 2 | 1 | 1.27 | .011 | 15 | 5 | .60 | 45 | .01 | 2 | .69 | .01 | .19 | 1 | 19 | 80 |
| 2160-G | 4 | 1 | 9 | 48 | .2 | 5 | 1 | 933 | 3.25 | 78 | 5 | ND | 1 | 19 | .3 | 2 | 2 | 1 | 1.78 | .012 | 12 | 8 | 1.02 | 39 | .01 | 2 | .75 | .01 | .18 | 1 | 10 | 110 |
| 2161-G | 1 | 1 | 3 | 95 | .2 | 1 | 1 | 1620 | 2.76 | 9 | 9 | ND | 2 | 26 | .2 | 2 | 2 | 1 | 2.66 | .010 | 15 | 6 | 1.54 | 37 | .01 | 2 | .83 | .01 | .15 | 1 | 4 | 350 |
| STANDARD C/AU-R | 18 | 57 | 39 | 130 | 7.0 | 67 | 31 | 1049 | 3.97 | 38 | 17 | 7 | 39 | 52 | 18.6 | 15 | 20 | 56 | .50 | .090 | 37 | 57 | .87 | 181 | .07 | 37 | 1.86 | .06 | .14 | 13 | 489 | 1300 |

HP 9

HP 10

AP-10

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | ppm | ppb | ppb | |
| 2162-G | 4 | 2 | 5 | 50 | .2 | 4 | 1 | 784 | 2.94 | 3 | 5 | ND | 2 | 34 | .3 | 2 | 2 | 1 | 1.45 | .010 | 16 | 8 | .90 | 52 | .01 | 4 | .51 | .01 | .17 | 1 | 5 | 290 |
| 2163-G | 2 | 2 | 4 | 56 | .4 | 1 | 1 | 1838 | 3.65 | 7 | 5 | ND | 1 | 62 | .2 | 3 | 4 | 1 | 4.11 | .009 | 6 | 6 | 1.78 | 47 | .01 | 2 | .63 | .01 | .19 | 1 | 19 | 300 |
| 2164-G | 5 | 3 | 12 | 51 | .4 | 6 | 1 | 508 | 3.91 | 11 | 5 | ND | 2 | 13 | .4 | 2 | 2 | 1 | .83 | .011 | 10 | 6 | .57 | 49 | .01 | 6 | .60 | .01 | .19 | 1 | 48 | 280 |
| 2165-G | 10 | 1 | 10 | 20 | .8 | 1 | 1 | 736 | 3.24 | 6 | 5 | ND | 2 | 28 | .5 | 2 | 4 | 1 | 1.27 | .011 | 11 | 5 | .72 | 53 | .01 | 5 | .78 | .01 | .23 | 1 | 12 | 50 |
| 2166-G | 4 | 2 | 14 | 18 | .3 | 5 | 1 | 471 | 2.95 | 5 | 5 | ND | 2 | 13 | .2 | 2 | 2 | 1 | .64 | .011 | 17 | 8 | .57 | 55 | .01 | 2 | .93 | .02 | .18 | 1 | 3 | 130 |
| 2167-G | 3 | 1 | 15 | 38 | .2 | 1 | 1 | 592 | 2.85 | 3 | 5 | ND | 2 | 15 | .2 | 2 | 3 | 1 | .78 | .011 | 14 | 6 | .55 | 60 | .01 | 2 | .84 | .02 | .20 | 1 | 4 | 140 |
| 2168-G | 4 | 2 | 5 | 31 | .2 | 4 | 1 | 560 | 2.27 | 2 | 5 | ND | 3 | 16 | .3 | 2 | 2 | 1 | .92 | .012 | 16 | 7 | .63 | 51 | .01 | 3 | .77 | .02 | .16 | 1 | 1 | 120 |
| 2169-G | 2 | 1 | 5 | 46 | .3 | 1 | 1 | 547 | 2.27 | 2 | 5 | ND | 3 | 14 | .4 | 2 | 3 | 1 | .87 | .011 | 15 | 5 | .58 | 60 | .01 | 4 | .75 | .02 | .20 | 1 | 1 | 180 |
| 2170-G | 3 | 1 | 9 | 26 | .1 | 6 | 1 | 452 | 2.55 | 4 | 5 | ND | 2 | 13 | .2 | 2 | 4 | 1 | .60 | .011 | 18 | 9 | .55 | 60 | .01 | 2 | .95 | .02 | .18 | 1 | 4 | 140 |
| 2171-G | 2 | 2 | 7 | 36 | .4 | 1 | 1 | 647 | 2.91 | 5 | 5 | ND | 3 | 23 | .3 | 2 | 2 | 1 | 1.09 | .013 | 14 | 5 | .70 | 58 | .01 | 5 | .90 | .02 | .21 | 1 | 5 | 150 |
| 2172-G | 3 | 1 | 6 | 25 | .1 | 5 | 1 | 685 | 2.23 | 14 | 5 | ND | 2 | 20 | .4 | 2 | 4 | 1 | 1.23 | .013 | 15 | 10 | .77 | 50 | .01 | 2 | .79 | .01 | .18 | 1 | 1 | 60 |
| 2173-G | 2 | 2 | 12 | 24 | .5 | 1 | 1 | 516 | 3.23 | 9 | 5 | ND | 2 | 17 | .4 | 2 | 2 | 1 | .97 | .012 | 12 | 5 | .59 | 61 | .01 | 4 | .73 | .01 | .27 | 1 | 2 | 70 |
| 2174-G | 25 | 1 | 11 | 24 | .7 | 2 | 1 | 1823 | 2.96 | 1005 | 5 | ND | 1 | 53 | .2 | 5 | 2 | 1 | 3.67 | .011 | 6 | 8 | 1.57 | 34 | .01 | 4 | .40 | .01 | .20 | 1 | 15 | 80 |
| 2175-G | 22 | 1 | 14 | 63 | .6 | 1 | 1 | 817 | 3.62 | 58 | 5 | ND | 2 | 25 | .3 | 2 | 2 | 1 | 1.22 | .012 | 11 | 5 | .72 | 55 | .01 | 3 | .77 | .01 | .25 | 1 | 3 | 130 |
| 2176-G | 18 | 3 | 18 | 44 | .5 | 5 | 1 | 644 | 3.59 | 88 | 5 | ND | 2 | 17 | .2 | 2 | 2 | 1 | .89 | .011 | 11 | 8 | .63 | 42 | .01 | 4 | .78 | .01 | .24 | 1 | 5 | 80 |
| 2177-G | 4 | 1 | 9 | 51 | .3 | 1 | 1 | 2373 | 3.82 | 20 | 5 | ND | 1 | 70 | .2 | 2 | 3 | 1 | 3.92 | .011 | 6 | 8 | 1.63 | 45 | .01 | 2 | .80 | .02 | .21 | 1 | 1 | 60 |
| 2178-G | 9 | 1 | 6 | 60 | .3 | 4 | 1 | 900 | 2.36 | 9 | 5 | ND | 2 | 21 | .3 | 2 | 4 | 1 | 1.19 | .012 | 13 | 8 | .67 | 51 | .01 | 2 | .64 | .02 | .20 | 1 | 1 | 40 |
| 2179-G | 3 | 1 | 11 | 35 | .4 | 1 | 1 | 666 | 3.17 | 9 | 5 | ND | 2 | 15 | .3 | 2 | 3 | 1 | .70 | .012 | 14 | 5 | .66 | 52 | .01 | 2 | .92 | .02 | .18 | 1 | 6 | 30 |
| 2180-G | 4 | 2 | 16 | 35 | .5 | 6 | 2 | 473 | 3.44 | 10 | 5 | ND | 2 | 14 | .2 | 2 | 2 | 1 | .45 | .011 | 13 | 9 | .48 | 57 | .01 | 4 | .87 | .02 | .21 | 1 | 6 | 40 |
| 2181-G | 3 | 3 | 12 | 33 | .2 | 3 | 1 | 558 | 3.28 | 7 | 5 | ND | 2 | 16 | .2 | 2 | 2 | 1 | .54 | .013 | 15 | 5 | .50 | 58 | .01 | 2 | .94 | .02 | .19 | 1 | 1 | 30 |
| 2182-G | 4 | 1 | 10 | 48 | .2 | 6 | 1 | 651 | 3.13 | 7 | 5 | ND | 2 | 16 | .3 | 2 | 2 | 1 | .61 | .011 | 16 | 8 | .53 | 58 | .01 | 2 | .94 | .02 | .21 | 1 | 6 | 20 |
| 2183-G | 3 | 3 | 6 | 49 | .1 | 2 | 1 | 495 | 2.24 | 8 | 5 | ND | 3 | 13 | .2 | 2 | 2 | 1 | .42 | .013 | 20 | 5 | .42 | 57 | .01 | 2 | .83 | .02 | .18 | 1 | 1 | 30 |
| 2184-G | 5 | 2 | 4 | 17 | .4 | 8 | 1 | 549 | 2.74 | 9 | 5 | ND | 3 | 16 | .2 | 2 | 2 | 1 | .53 | .013 | 21 | 9 | .51 | 76 | .01 | 5 | .91 | .03 | .20 | 1 | 5 | 20 |
| 2185-G | 3 | 3 | 13 | 29 | .4 | 2 | 2 | 1212 | 5.11 | 13 | 5 | ND | 1 | 23 | .2 | 2 | 2 | 1 | 1.28 | .011 | 9 | 8 | .91 | 54 | .01 | 2 | .98 | .02 | .16 | 1 | 13 | 40 |
| 2186-G | 5 | 1 | 7 | 45 | .3 | 5 | 1 | 520 | 2.54 | 9 | 5 | ND | 2 | 13 | .4 | 2 | 3 | 1 | .48 | .012 | 20 | 8 | .48 | 58 | .01 | 2 | .83 | .03 | .18 | 1 | 7 | 40 |
| 2187-G | 4 | 3 | 10 | 37 | .2 | 2 | 2 | 1158 | 4.56 | 10 | 5 | ND | 2 | 19 | .2 | 2 | 2 | 1 | 1.11 | .011 | 15 | 8 | 1.03 | 64 | .01 | 2 | 1.38 | .03 | .18 | 1 | 11 | 120 |
| 2188-G | 4 | 2 | 6 | 52 | .3 | 7 | 1 | 447 | 2.72 | 12 | 5 | ND | 4 | 10 | .5 | 2 | 2 | 2 | .35 | .013 | 22 | 9 | .50 | 65 | .01 | 7 | 1.00 | .03 | .17 | 1 | 12 | 200 |
| 2189-G | 3 | 4 | 9 | 56 | .5 | 2 | 2 | 475 | 3.00 | 9 | 5 | ND | 1 | 25 | .3 | 2 | 2 | 1 | .99 | .014 | 11 | 5 | .52 | 51 | .01 | 2 | .58 | .01 | .22 | 1 | 7 | 90 |
| 2190-G | 4 | 3 | 6 | 31 | .5 | 6 | 1 | 598 | 2.89 | 6 | 5 | ND | 1 | 24 | .2 | 3 | 2 | 1 | 1.27 | .014 | 11 | 8 | .69 | 53 | .01 | 5 | .46 | .01 | .23 | 1 | 16 | 110 |
| 2191-G | 3 | 5 | 9 | 27 | .9 | 2 | 1 | 709 | 2.91 | 8 | 5 | ND | 1 | 38 | .2 | 2 | 2 | 1 | 1.55 | .013 | 10 | 6 | .75 | 45 | .01 | 2 | .37 | .01 | .19 | 1 | 16 | 130 |
| 2192-G | 4 | 3 | 5 | 24 | .4 | 8 | 1 | 852 | 2.04 | 7 | 5 | ND | 1 | 43 | .3 | 2 | 2 | 1 | 2.15 | .012 | 11 | 12 | .93 | 48 | .01 | 4 | .28 | .01 | .20 | 1 | 4 | 140 |
| 2193-G | 2 | 5 | 10 | 48 | .3 | 3 | 2 | 622 | 3.21 | 10 | 5 | ND | 1 | 20 | .4 | 2 | 2 | 1 | .72 | .011 | 13 | 5 | .51 | 59 | .01 | 2 | .69 | .01 | .19 | 1 | 7 | 160 |
| 2194-G | 4 | 2 | 8 | 42 | .3 | 4 | 2 | 1240 | 2.78 | 12 | 5 | ND | 1 | 44 | .3 | 3 | 2 | 1 | 1.80 | .011 | 10 | 8 | .74 | 49 | .01 | 2 | .44 | .01 | .18 | 1 | 7 | 190 |
| 2195-G | 2 | 4 | 3 | 28 | .1 | 2 | 1 | 746 | 1.78 | 2 | 5 | ND | 1 | 33 | .5 | 2 | 2 | 1 | 1.10 | .011 | 16 | 5 | .43 | 55 | .01 | 2 | .36 | .01 | .19 | 1 | 4 | 150 |
| 2196-G | 6 | 3 | 14 | 56 | .7 | 4 | 1 | 717 | 3.82 | 12 | 5 | ND | 1 | 23 | .2 | 2 | 3 | 1 | .80 | .011 | 12 | 7 | .51 | 53 | .01 | 2 | .41 | .01 | .22 | 1 | 11 | 120 |
| 2197-G | 4 | 5 | 10 | 38 | .4 | 2 | 1 | 992 | 2.85 | 11 | 5 | ND | 1 | 36 | .2 | 3 | 2 | 1 | 1.51 | .011 | 10 | 6 | .67 | 64 | .01 | 2 | .38 | .01 | .18 | 1 | 5 | 140 |
| STANDARD C/AU-R | 18 | 58 | 38 | 131 | 6.8 | 70 | 32 | 1051 | 3.97 | 40 | 19 | 7 | 39 | 52 | 18.3 | 15 | 20 | 55 | .50 | .092 | 40 | 60 | .89 | 182 | .07 | 35 | 1.89 | .06 | .14 | 12 | 492 | 1500 |

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|-----|-----|----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | ppm | ppb | ppb |
| 2198-G | 8 | 4 | 10 | 49 | .8 | 4 | 1 | 1488 | 3.37 | 40 | 5 | ND | 1 | 44 | .2 | 3 | 2 | 1 | 2.11 | .009 | 8 | 7 | .95 | 41 | .01 | 2 | .42 | .01 | .16 | 1 | 5 | 130 |
| 2199-G | 4 | 3 | 8 | 39 | .5 | 1 | 1 | 575 | 2.48 | 16 | 5 | ND | 2 | 18 | .2 | 2 | 4 | 1 | .63 | .009 | 14 | 2 | .43 | 45 | .01 | 2 | .44 | .01 | .17 | 1 | 9 | 120 |
| 2200-G | 5 | 3 | 12 | 52 | .6 | 4 | 1 | 498 | 2.52 | 12 | 5 | ND | 1 | 21 | .2 | 3 | 2 | 1 | .60 | .010 | 13 | 4 | .29 | 41 | .01 | 2 | .32 | .01 | .18 | 1 | 12 | 70 |
| 2202-G | 3 | 3 | 15 | 37 | .8 | 2 | 2 | 362 | 3.85 | 22 | 5 | ND | 2 | 32 | .2 | 3 | 2 | 1 | .46 | .010 | 14 | 3 | .18 | 37 | .01 | 2 | .38 | .01 | .22 | 1 | 10 | 130 |
| 2203-G | 5 | 3 | 4 | 52 | .3 | 6 | 1 | 804 | 1.21 | 7 | 5 | ND | 1 | 31 | .3 | 2 | 2 | 1 | 1.66 | .012 | 17 | 8 | .70 | 58 | .01 | 3 | .29 | .01 | .16 | 1 | 1 | 140 |
| 2204-G | 5 | 3 | 14 | 67 | .9 | 2 | 2 | 1692 | 3.48 | 19 | 5 | ND | 1 | 35 | .2 | 6 | 2 | 1 | 2.20 | .010 | 8 | 8 | .93 | 51 | .01 | 2 | .38 | .01 | .24 | 1 | 13 | 200 |
| 2205-G | 5 | 2 | 9 | 68 | .6 | 5 | 1 | 396 | 2.03 | 11 | 5 | ND | 1 | 25 | .2 | 2 | 2 | 1 | .55 | .009 | 13 | 3 | .23 | 47 | .01 | 2 | .22 | .01 | .15 | 1 | 6 | 150 |
| 2206-G | 7 | 2 | 15 | 73 | 1.0 | 2 | 2 | 1388 | 3.76 | 15 | 5 | ND | 1 | 51 | .2 | 3 | 2 | 1 | 2.04 | .009 | 7 | 5 | .87 | 43 | .01 | 2 | .31 | .01 | .20 | 1 | 12 | 160 |
| 2207-G | 4 | 3 | 8 | 57 | .4 | 5 | 1 | 337 | 1.71 | 6 | 5 | ND | 1 | 20 | .2 | 2 | 2 | 1 | .44 | .009 | 14 | 4 | .23 | 46 | .01 | 3 | .25 | .01 | .17 | 1 | 10 | 140 |
| 2208-G | 2 | 2 | 7 | 37 | .6 | 2 | 1 | 646 | 2.02 | 12 | 5 | ND | 2 | 78 | .2 | 3 | 2 | 1 | 1.09 | .008 | 12 | 4 | .45 | 37 | .01 | 4 | .33 | .01 | .19 | 1 | 6 | 180 |
| 2209-G | 3 | 2 | 7 | 76 | .6 | 4 | 1 | 512 | 2.03 | 9 | 5 | ND | 1 | 29 | .2 | 3 | 2 | 1 | .77 | .011 | 12 | 4 | .32 | 40 | .01 | 2 | .25 | .01 | .17 | 1 | 14 | 130 |
| 2210-G | 5 | 3 | 12 | 36 | .9 | 1 | 2 | 1232 | 3.99 | 12 | 5 | ND | 1 | 34 | .3 | 4 | 2 | 1 | 1.50 | .011 | 11 | 3 | .66 | 42 | .01 | 3 | .34 | .01 | .22 | 1 | 27 | 140 |
| 2211-G | 6 | 2 | 10 | 53 | .7 | 4 | 2 | 635 | 3.00 | 17 | 5 | ND | 1 | 30 | .2 | 3 | 2 | 1 | .93 | .012 | 10 | 4 | .40 | 41 | .01 | 2 | .26 | .01 | .17 | 1 | 6 | 130 |
| 2212-G | 3 | 2 | 7 | 81 | .3 | 1 | 1 | 835 | 1.72 | 8 | 5 | ND | 1 | 59 | .3 | 2 | 2 | 1 | 1.21 | .008 | 9 | 3 | .47 | 32 | .01 | 2 | .32 | .01 | .18 | 1 | 33 | 230 |
| 2213-G | 1 | 2 | 5 | 5 | .7 | 3 | 1 | 685 | 2.38 | 107 | 5 | ND | 1 | 29 | .2 | 4 | 2 | 1 | 1.06 | .011 | 9 | 4 | .42 | 39 | .01 | 2 | .24 | .01 | .16 | 1 | 1 | 80 |
| 2214-G | 2 | 3 | 22 | 2 | 1.4 | 2 | 2 | 328 | 3.76 | 239 | 7 | ND | 2 | 34 | .2 | 5 | 2 | 1 | .55 | .010 | 10 | 2 | .22 | 27 | .01 | 2 | .35 | .01 | .20 | 1 | 121 | 150 |
| 2215-G | 3 | 2 | 10 | 1 | .6 | 3 | 1 | 279 | 2.13 | 149 | 5 | ND | 2 | 45 | .2 | 3 | 2 | 1 | .48 | .006 | 11 | 3 | .19 | 20 | .01 | 2 | .30 | .01 | .17 | 1 | 63 | 100 |
| 2216-G | 3 | 3 | 15 | 76 | .9 | 6 | 2 | 880 | 2.78 | 5171 | 5 | ND | 1 | 50 | .3 | 20 | 2 | 1 | 1.35 | .011 | 5 | 7 | .56 | 22 | .01 | 4 | .30 | .01 | .16 | 1 | 499 | 240 |
| 2217-G | 2 | 5 | 14 | 39 | .8 | 2 | 1 | 295 | 2.71 | 1787 | 5 | ND | 2 | 30 | .3 | 12 | 4 | 1 | .46 | .009 | 11 | 2 | .19 | 45 | .01 | 4 | .29 | .01 | .16 | 1 | 244 | 180 |
| 2218-G | 5 | 3 | 10 | 3 | .6 | 7 | 1 | 137 | 1.87 | 180 | 11 | ND | 2 | 19 | .2 | 3 | 2 | 1 | .23 | .012 | 16 | 5 | .09 | 52 | .01 | 3 | .29 | .01 | .19 | 1 | 49 | 160 |
| 2219-G | 7 | 5 | 22 | 169 | 1.3 | 2 | 2 | 618 | 3.45 | 1563 | 5 | ND | 1 | 43 | .4 | 11 | 2 | 1 | 1.41 | .007 | 8 | 3 | .37 | 39 | .01 | 2 | .26 | .01 | .16 | 1 | 218 | 260 |
| 2220-G | 7 | 2 | 10 | 27 | .6 | 6 | 1 | 186 | 1.89 | 62 | 7 | ND | 1 | 27 | .2 | 2 | 3 | 1 | .29 | .009 | 17 | 4 | .11 | 49 | .01 | 2 | .30 | .01 | .19 | 1 | 21 | 70 |
| 2221-G | 6 | 6 | 10 | 21 | .7 | 3 | 1 | 450 | 2.45 | 111 | 5 | ND | 1 | 42 | .3 | 3 | 3 | 1 | 1.03 | .006 | 10 | 2 | .23 | 54 | .01 | 3 | .25 | .01 | .17 | 1 | 35 | 50 |
| 2222-G | 6 | 4 | 14 | 87 | 1.0 | 6 | 1 | 405 | 2.35 | 88 | 5 | ND | 1 | 25 | .3 | 3 | 2 | 1 | .59 | .009 | 13 | 5 | .23 | 51 | .01 | 4 | .31 | .01 | .20 | 1 | 18 | 100 |
| 2223-G | 5 | 5 | 10 | 43 | 1.0 | 2 | 1 | 1231 | 3.16 | 60 | 5 | ND | 1 | 54 | .2 | 4 | 3 | 1 | 1.91 | .009 | 7 | 3 | .59 | 45 | .01 | 2 | .22 | .01 | .16 | 1 | 53 | 80 |
| 2224-G | 5 | 3 | 8 | 41 | .5 | 5 | 1 | 399 | 1.64 | 22 | 5 | ND | 1 | 28 | .2 | 2 | 3 | 1 | .61 | .011 | 15 | 4 | .22 | 55 | .01 | 2 | .26 | .01 | .18 | 1 | 17 | 80 |
| 2225-G | 2 | 4 | 8 | 42 | .6 | 3 | 1 | 611 | 2.04 | 23 | 5 | ND | 1 | 29 | .2 | 3 | 2 | 1 | 1.00 | .011 | 11 | 4 | .36 | 43 | .01 | 2 | .26 | .01 | .17 | 1 | 12 | 70 |
| 2226-G | 4 | 3 | 13 | 30 | .8 | 6 | 3 | 666 | 2.30 | 31 | 5 | ND | 1 | 26 | .2 | 4 | 2 | 1 | 1.01 | .011 | 10 | 5 | .37 | 51 | .01 | 2 | .26 | .01 | .17 | 1 | 12 | 90 |
| 2227-G | 3 | 5 | 7 | 26 | 1.3 | 3 | 1 | 1192 | 2.68 | 39 | 5 | ND | 1 | 34 | .2 | 4 | 2 | 1 | 1.86 | .011 | 8 | 4 | .68 | 42 | .01 | 4 | .22 | .01 | .16 | 1 | 23 | 150 |
| 2228-G | 4 | 4 | 8 | 30 | .6 | 5 | 1 | 672 | 2.10 | 18 | 5 | ND | 1 | 33 | .3 | 2 | 2 | 1 | 1.09 | .012 | 11 | 6 | .42 | 44 | .01 | 5 | .27 | .01 | .18 | 1 | 10 | 60 |
| 2229-G | 2 | 4 | 8 | 26 | .4 | 3 | 1 | 364 | 1.87 | 57 | 8 | ND | 1 | 27 | .2 | 2 | 2 | 1 | .57 | .010 | 14 | 2 | .18 | 47 | .01 | 2 | .25 | .01 | .18 | 1 | 50 | 110 |
| 2230-G | 4 | 4 | 6 | 28 | .7 | 5 | 1 | 380 | 2.22 | 17 | 5 | ND | 1 | 31 | .2 | 2 | 2 | 1 | .60 | .010 | 15 | 5 | .22 | 54 | .01 | 2 | .29 | .01 | .20 | 1 | 41 | 70 |
| 2231-G | 2 | 6 | 5 | 74 | .7 | 2 | 1 | 479 | 1.81 | 17 | 5 | ND | 1 | 24 | .4 | 2 | 4 | 1 | .52 | .010 | 13 | 1 | .21 | 42 | .01 | 5 | .27 | .01 | .20 | 1 | 24 | 90 |
| 2232-G | 4 | 7 | 7 | 76 | .7 | 3 | 2 | 502 | 2.44 | 20 | 5 | ND | 1 | 25 | .2 | 2 | 6 | 1 | .49 | .011 | 12 | 3 | .19 | 34 | .01 | 2 | .33 | .01 | .22 | 1 | 20 | 150 |
| 2233-G | 2 | 6 | 2 | 120 | .3 | 1 | 2 | 1780 | 3.51 | 6 | 5 | ND | 1 | 69 | .2 | 2 | 2 | 1 | 1.66 | .023 | 13 | 4 | .92 | 55 | .01 | 3 | .37 | .01 | .19 | 1 | 4 | 120 |
| 2234-G | 2 | 29 | 20 | 70 | 2.1 | 14 | 15 | 2353 | 5.82 | 30 | 5 | ND | 1 | 59 | .2 | 10 | 2 | 12 | 2.27 | .089 | 8 | 9 | 1.29 | 45 | .01 | 3 | .48 | .01 | .24 | 1 | 28 | 210 |
| STANDARD C/AU-R | 18 | 57 | 38 | 131 | 6.9 | 68 | 31 | 1051 | 3.97 | 39 | 21 | 7 | 38 | 53 | 18.6 | 15 | 21 | 55 | .50 | .088 | 39 | 59 | .89 | 181 | .08 | 36 | 1.90 | .06 | .14 | 12 | 513 | 1600 |

APIC

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm | Au** ppb | Hg ppb |
|---------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|-------------|-----------|
| 2235-G | 3 | 32 | 19 | 206 | 2.0 | 18 | 18 | 1610 | 6.45 | 42 | 5 | ND | 1 | 48 | 1.1 | 11 | 8 | 18 | 2.02 | .102 | 8 | 5 | 1.39 | 40 | .01 | 2 | .70 | .01 | .23 | 1 | 18 | 220 |
| 2236-G | 5 | 22 | 24 | 107 | 3.5 | 13 | 9 | 1016 | 4.08 | 36 | 5 | ND | 1 | 170 | .5 | 7 | 3 | 10 | 3.13 | .052 | 6 | 3 | .61 | 72 | .01 | 3 | .40 | .01 | .19 | 1 | 42 | 130 |
| 2237-G | 5 | 53 | 20 | 162 | 1.9 | 14 | 11 | 921 | 3.91 | 33 | 12 | ND | 1 | 187 | .9 | 8 | 3 | 9 | 2.52 | .059 | 6 | 3 | 1.01 | 78 | .01 | 3 | .45 | .01 | .25 | 1 | 7 | 150 |
| 2238-G | 4 | 56 | 17 | 136 | 1.9 | 17 | 11 | 595 | 4.53 | 29 | 5 | ND | 1 | 93 | .4 | 9 | 3 | 10 | 1.72 | .052 | 2 | 3 | .81 | 71 | .01 | 3 | .45 | .01 | .25 | 1 | 15 | 170 |
| 2239-G | 6 | 45 | 16 | 121 | .8 | 17 | 11 | 594 | 4.37 | 25 | 5 | ND | 1 | 170 | .4 | 4 | 4 | 9 | 2.40 | .053 | 2 | 4 | .87 | 68 | .01 | 4 | .45 | .01 | .25 | 1 | 19 | 150 |
| 2240-G | 2 | 9 | 12 | 162 | .4 | 2 | 1 | 529 | 1.44 | 2 | 5 | ND | 2 | 123 | .6 | 2 | 13 | 1 | 2.89 | .001 | 28 | 2 | .22 | 83 | .01 | 2 | .31 | .01 | .19 | 1 | 1 | 110 |
| 2241-G | 2 | 7 | 14 | 143 | .6 | 1 | 1 | 503 | 1.06 | 3 | 5 | ND | 2 | 121 | .4 | 3 | 2 | 1 | 2.81 | .001 | 24 | 1 | .22 | 79 | .01 | 2 | .34 | .01 | .21 | 1 | 3 | 190 |
| 2242-G | 4 | 9 | 2 | 208 | .2 | 5 | 4 | 408 | 1.94 | 7 | 5 | ND | 2 | 82 | 1.0 | 2 | 8 | 3 | 1.42 | .015 | 17 | 2 | .37 | 55 | .01 | 2 | .34 | .01 | .19 | 2 | 9 | 180 |

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GEOCHEMICAL ANALYSIS CERTIFICATE

Grandes Inc. PROJECT 134 File # 90-4583 Page 1

2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | W | Au** | Hg | |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|-----|-----|----|------|-----|-----|----|------|------|-----|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | % | % | ppm | ppb | ppb |
| 2251 G | 4 | 30 | 50 | 119 | 4.5 | 18 | 10 | 641 | 3.56 | 88 | 5 | ND | 1 | 55 | 3 | 10 | 2 | 8 | 1.52 | 060 | 4 | 7 | .89 | 45 | 01 | 9 | .83 | .01 | .20 | 1 | 69 | 200 | |
| 2252 G | 8 | 10 | 9 | 130 | 6 | 2 | 1 | 745 | 2.78 | 18 | 5 | ND | 1 | 32 | 4 | 2 | 2 | 1 | .78 | 014 | 7 | 4 | .51 | 49 | 01 | 5 | .72 | .01 | .16 | 1 | 11 | 350 | |
| 2253 G | 5 | 14 | 18 | 104 | 1.0 | 1 | 2 | 1401 | 4.32 | 277 | 5 | ND | 1 | 57 | 2 | 4 | 2 | 1 | 2.42 | 015 | 3 | 6 | .85 | 33 | 01 | 4 | .42 | .01 | .19 | 1 | 135 | 140 | |
| 2254 G | 3 | 29 | 33 | 102 | 2.1 | 11 | 9 | 1224 | 4.24 | 135 | 5 | ND | 1 | 63 | 3 | 10 | 2 | 6 | 2.28 | 054 | 3 | 8 | 1.13 | 28 | 01 | 5 | .65 | .01 | .20 | 1 | 88 | 80 | |
| 2255 G | 5 | 40 | 52 | 175 | 5.4 | 18 | 10 | 808 | 4.18 | 188 | 5 | ND | 1 | 53 | 6 | 14 | 2 | 9 | 1.94 | 068 | 4 | 10 | 1.15 | 39 | 01 | 9 | .87 | .01 | .21 | 1 | 98 | 130 | |
| 2256 G | 6 | 16 | 12 | 124 | 2.5 | 5 | 1 | 667 | 2.39 | 9 | 5 | ND | 1 | 14 | 4 | 2 | 2 | 1 | .44 | 015 | 8 | 8 | .50 | 64 | 01 | 3 | .72 | .01 | .12 | 1 | 26 | 580 | |
| 2257 G | 5 | 8 | 13 | 131 | 1.5 | 1 | 1 | 648 | 3.21 | 10 | 5 | ND | 1 | 16 | 3 | 3 | 2 | 1 | .42 | 015 | 8 | 4 | .46 | 56 | 01 | 6 | .91 | .02 | .18 | 1 | 22 | 260 | |
| 2258 G | 6 | 7 | 3 | 88 | 4 | 2 | 1 | 1451 | 2.48 | 14 | 5 | ND | 1 | 61 | 2 | 2 | 2 | 1 | 2.14 | 008 | 8 | 8 | .84 | 51 | 01 | 5 | .29 | .01 | .17 | 1 | 47 | 120 | |
| 2259 G | 6 | 16 | 8 | 90 | 4.6 | 3 | 2 | 1189 | 3.06 | 12 | 5 | ND | 1 | 48 | 3 | 3 | 2 | 1 | 1.84 | 017 | 7 | 7 | .73 | 39 | 01 | 6 | .30 | .01 | .18 | 1 | 39 | 100 | |
| 2260 G | 5 | 4 | 8 | 125 | 4 | 4 | 1 | 787 | 1.15 | 10 | 5 | ND | 1 | 45 | 2 | 2 | 2 | 1 | 1.36 | 002 | 16 | 21 | .52 | 24 | 01 | 4 | .27 | .01 | .16 | 1 | 33 | 110 | |
| 2261 G | 6 | 8 | 8 | 122 | 4 | 3 | 2 | 788 | 1.89 | 9 | 5 | ND | 2 | 49 | 3 | 3 | 2 | 1 | 1.43 | 005 | 13 | 5 | .64 | 64 | 01 | 4 | .32 | .01 | .19 | 1 | 10 | 140 | |
| 2262 G | 8 | 11 | 15 | 100 | 5 | 8 | 2 | 484 | 1.61 | 8 | 7 | ND | 2 | 37 | 3 | 2 | 2 | 1 | .94 | 007 | 11 | 40 | .35 | 51 | 01 | 5 | .29 | .02 | .17 | 1 | 6 | 160 | |
| 2263 G | 5 | 9 | 12 | 77 | 3 | 7 | 1 | 861 | 1.33 | 8 | 5 | ND | 3 | 43 | 2 | 2 | 3 | 1 | 1.68 | 004 | 14 | 11 | .52 | 74 | 01 | 3 | .29 | .02 | .17 | 1 | 5 | 100 | |
| 2264 G | 7 | 5 | 14 | 38 | 2 | 10 | 2 | 563 | 1.47 | 4 | 5 | ND | 3 | 30 | 2 | 2 | 2 | 1 | 1.02 | 006 | 13 | 42 | .37 | 65 | 01 | 4 | .25 | .01 | .15 | 1 | 1 | 80 | |
| 2265 G | 3 | 6 | 13 | 63 | 2 | 6 | 1 | 962 | 1.59 | 5 | 5 | ND | 2 | 38 | 2 | 2 | 4 | 1 | 1.78 | 005 | 10 | 9 | .53 | 69 | 01 | 4 | .24 | .01 | .13 | 1 | 1 | 130 | |
| 2266 G | 7 | 8 | 9 | 74 | 1 | 11 | 1 | 458 | 1.08 | 2 | 7 | ND | 3 | 26 | 2 | 2 | 2 | 1 | .76 | 006 | 14 | 44 | .25 | 74 | 01 | 2 | .24 | .01 | .16 | 1 | 8 | 430 | |
| 2267 G | 4 | 9 | 10 | 104 | 3 | 6 | 6 | 979 | 3.08 | 13 | 5 | ND | 1 | 59 | 2 | 3 | 2 | 1 | 1.86 | 031 | 9 | 8 | .74 | 51 | 01 | 4 | .31 | .02 | .16 | 1 | 1 | 160 | |
| 2268 G | 3 | 7 | 10 | 91 | 4 | 4 | 6 | 1027 | 4.37 | 8 | 5 | ND | 1 | 43 | 2 | 3 | 2 | 3 | 1.78 | 050 | 7 | 17 | .98 | 49 | 01 | 6 | .56 | .01 | .20 | 1 | 1 | 110 | |
| 2279 G | 3 | 27 | 16 | 102 | 3 | 18 | 12 | 679 | 4.84 | 27 | 5 | ND | 1 | 37 | 3 | 8 | 2 | 16 | 1.63 | 063 | 5 | 9 | 1.35 | 54 | 01 | 6 | .42 | .01 | .17 | 1 | 4 | 190 | |
| 2280 G | 4 | 22 | 8 | 112 | 1 | 10 | 9 | 1395 | 5.94 | 14 | 5 | ND | 1 | 68 | 5 | 9 | 2 | 24 | 3.83 | 077 | 7 | 19 | 2.46 | 73 | 01 | 4 | .84 | .02 | .12 | 1 | 1 | 250 | |
| 2281 G | 14 | 42 | 14 | 279 | 4 | 33 | 11 | 613 | 4.82 | 34 | 5 | ND | 1 | 42 | 1.6 | 16 | 2 | 21 | 1.81 | 063 | 6 | 9 | 1.64 | 42 | 01 | 3 | .40 | .01 | .17 | 1 | 6 | 410 | |
| 2282 G | 17 | 40 | 20 | 258 | 5 | 35 | 10 | 813 | 5.04 | 37 | 5 | ND | 1 | 52 | 1.7 | 19 | 2 | 19 | 2.78 | 069 | 6 | 11 | 1.84 | 47 | 01 | 5 | .36 | .01 | .15 | 1 | 11 | 420 | |
| 2283 G | 12 | 41 | 20 | 317 | 4 | 32 | 7 | 867 | 3.85 | 34 | 5 | ND | 1 | 58 | 2.4 | 16 | 2 | 16 | 3.28 | 053 | 6 | 7 | 1.84 | 58 | 01 | 2 | .39 | .01 | .17 | 1 | 5 | 430 | |
| 2284 G | 13 | 44 | 21 | 300 | 6 | 35 | 9 | 750 | 3.89 | 36 | 5 | ND | 1 | 57 | 1.8 | 19 | 2 | 15 | 2.96 | 056 | 5 | 10 | 1.74 | 53 | 01 | 4 | .35 | .01 | .16 | 1 | 5 | 500 | |
| 2285 G | 9 | 37 | 15 | 258 | 2 | 23 | 6 | 1120 | 4.04 | 27 | 5 | ND | 1 | 348 | 2.2 | 13 | 2 | 12 | 6.00 | 093 | 5 | 9 | 2.52 | 56 | 01 | 3 | .26 | .01 | .12 | 1 | 1 | 350 | |
| 2286 G | 16 | 38 | 15 | 254 | 4 | 32 | 9 | 813 | 4.31 | 37 | 5 | ND | 1 | 59 | 2.0 | 18 | 2 | 17 | 2.90 | 065 | 7 | 14 | 1.76 | 59 | 01 | 2 | .39 | .01 | .18 | 1 | 1 | 490 | |
| 2287 G | 6 | 72 | 18 | 130 | 3 | 22 | 12 | 467 | 5.01 | 33 | 5 | ND | 1 | 58 | 1.6 | 12 | 2 | 18 | 1.23 | 066 | 5 | 9 | 1.13 | 45 | 01 | 5 | .45 | .01 | .20 | 1 | 3 | 300 | |
| 2288 G | 3 | 33 | 15 | 100 | 6 | 14 | 11 | 741 | 4.65 | 33 | 5 | ND | 1 | 54 | 1.5 | 9 | 2 | 18 | 1.50 | 013 | 3 | 10 | 1.25 | 88 | 01 | 3 | .30 | .01 | .13 | 1 | 9 | 210 | |
| 2289 G | 2 | 25 | 8 | 91 | 4 | 6 | 6 | 2531 | 4.74 | 22 | 5 | ND | 1 | 215 | 1.5 | 8 | 2 | 12 | 6.48 | 015 | 3 | 5 | 2.99 | 93 | 01 | 2 | .24 | .01 | .10 | 1 | 5 | 190 | |
| 2290 G | 1 | 25 | 8 | 107 | 4 | 8 | 7 | 927 | 3.83 | 19 | 5 | ND | 1 | 61 | 1.5 | 6 | 2 | 13 | 2.14 | 010 | 4 | 8 | 1.43 | 169 | 01 | 3 | .29 | .01 | .12 | 1 | 15 | 180 | |
| 2291 G | 1 | 16 | 2 | 112 | 6 | 7 | 8 | 941 | 4.14 | 14 | 5 | ND | 1 | 96 | 1.5 | 5 | 2 | 4 | 2.45 | 038 | 5 | 8 | 1.02 | 44 | 01 | 2 | .39 | .01 | .17 | 1 | 3 | 90 | |
| 2292 G | 2 | 22 | 15 | 199 | 8 | 7 | 15 | 392 | 5.36 | 187 | 6 | ND | 1 | 29 | 1.5 | 4 | 2 | 7 | .91 | 016 | 6 | 7 | .56 | 22 | 01 | 2 | .47 | .01 | .17 | 1 | 74 | 80 | |
| 2293 G | 1 | 19 | 6 | 24 | 1.0 | 7 | 18 | 505 | 7.31 | 36 | 7 | ND | 1 | 38 | 1.2 | 6 | 2 | 7 | 1.24 | 055 | 5 | 8 | .76 | 20 | 01 | 5 | .45 | .01 | .20 | 1 | 12 | 50 | |
| 2294 G | 1 | 15 | 8 | 41 | 8 | 9 | 21 | 1099 | 5.90 | 21 | 5 | ND | 1 | 45 | 1.2 | 8 | 2 | 5 | 2.48 | 025 | 5 | 8 | .91 | 22 | 01 | 2 | .33 | .01 | .19 | 1 | 10 | 70 | |
| 2295 G | 1 | 18 | 8 | 27 | 1.1 | 9 | 19 | 2460 | 9.38 | 23 | 5 | ND | 1 | 55 | 1.3 | 15 | 2 | 3 | 3.98 | 097 | 4 | 11 | 1.95 | 36 | 01 | 3 | .29 | .01 | .18 | 1 | 13 | 80 | |
| 2296 G | 4 | 9 | 25 | 213 | 8 | 13 | 9 | 977 | 3.38 | 86 | 5 | ND | 1 | 44 | 1.5 | 6 | 2 | 1 | 2.16 | 035 | 3 | 7 | .82 | 31 | 01 | 2 | .24 | .01 | .15 | 1 | 80 | 100 | |
| STANDARD C/AU-R | 18 | 60 | 40 | 131 | 7.0 | 71 | 31 | 1057 | 3.98 | 339 | 15 | 7 | 38 | 53 | 18.5 | 15 | 21 | 55 | .52 | 095 | 38 | 59 | .90 | 181 | 007 | 36 | 1.90 | .06 | .14 | 11 | 487 | 1500 | |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-N2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B V AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1-P3 CORE P4 ROCK AU** ANALYSIS BY FA/ICP FROM 10 GN SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: SEP 17 1990 DATE REPORT MAILED: Sept 25/90 SIGNED BY: [Signature] D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Pi | B | Al | Na | K | M | Au** | Hg |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|------|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % | ppm | ppm | % | ppm | % | % | % | % | ppm | ppm | ppm | ppm |
| 2297 G | 1 | 13 | 40 | 473 | 2.0 | 8 | 11 | 1446 | 5.20 | 291 | 5 | ND | 1 | 56 | 9 | 10 | 2 | 3 | 2.97 | .041 | 2 | 7 | 1.13 | 12 | .01 | 2 | .30 | .01 | .16 | 1 | 200 | 160 |
| 2298 G | 1 | 11 | 17 | 167 | .8 | 5 | 5 | 815 | 2.23 | 329 | 5 | ND | 1 | 54 | 8 | 6 | 2 | 4 | 2.27 | .048 | 3 | 7 | .88 | 50 | .01 | 5 | .36 | .01 | .20 | 2 | 108 | 100 |
| 2299 G | 1 | 14 | 19 | 30 | 1.4 | 4 | 10 | 1875 | 5.45 | 213 | 5 | ND | 1 | 51 | 8 | 9 | 2 | 3 | 3.46 | .055 | 2 | 6 | 1.44 | 22 | .01 | 2 | .29 | .01 | .16 | 1 | 224 | 60 |
| 2300 G | 2 | 20 | 7 | 84 | .7 | 8 | 9 | 1318 | 2.58 | 36 | 5 | ND | 1 | 51 | 12 | 7 | 2 | 5 | 2.69 | .052 | 5 | 8 | 1.08 | 52 | .01 | 2 | .38 | .01 | .21 | 1 | 36 | 100 |
| 2301 G | 2 | 23 | 12 | 92 | .5 | 8 | 6 | 1184 | 1.90 | 34 | 5 | ND | 1 | 35 | 12 | 5 | 3 | 2 | 2.70 | .045 | 7 | 17 | 1.12 | 39 | .01 | 2 | .36 | .01 | .20 | 1 | 34 | 60 |
| 2302 G | 1 | 22 | 11 | 98 | .6 | 8 | 6 | 1740 | 3.03 | 40 | 5 | ND | 1 | 42 | 2 | 5 | 2 | 5 | 3.78 | .044 | 7 | 10 | 1.84 | 38 | .01 | 2 | .72 | .01 | .21 | 1 | 7 | 50 |
| 2303 G | 1 | 20 | 12 | 84 | .5 | 10 | 7 | 1590 | 3.30 | 12 | 5 | ND | 1 | 62 | 2 | 3 | 2 | 8 | 3.68 | .045 | 7 | 20 | 1.78 | 43 | .01 | 2 | .99 | .01 | .21 | 1 | 9 | 40 |
| 2304 G | 1 | 15 | 18 | 92 | .8 | 8 | 6 | 2378 | 3.88 | 39 | 5 | ND | 1 | 214 | 3 | 5 | 2 | 8 | 6.80 | .037 | 5 | 12 | 1.92 | 48 | .01 | 2 | .96 | .01 | .17 | 1 | 5 | 70 |
| 2305 G | 3 | 18 | 16 | 184 | .4 | 9 | 7 | 1065 | 3.55 | 18 | 5 | ND | 1 | 38 | 8 | 3 | 2 | 10 | 2.24 | .051 | 8 | 19 | 1.39 | 43 | .01 | 2 | 1.16 | .01 | .19 | 1 | 5 | 70 |
| 2306 G | 2 | 5 | 8 | 115 | .5 | 4 | 14 | 1010 | 6.63 | 9 | 5 | ND | 1 | 49 | 2 | 5 | 2 | 105 | 1.96 | .178 | 10 | 11 | 1.33 | 105 | .02 | 2 | 2.48 | .04 | .11 | 1 | 5 | 80 |
| 2307 G | 1 | 11 | 29 | 148 | 1.5 | 2 | 18 | 1516 | 9.58 | 19 | 5 | ND | 1 | 117 | 2 | 5 | 2 | 153 | 3.58 | .243 | 11 | 13 | 1.35 | 57 | .02 | 2 | 2.94 | .07 | .05 | 1 | 36 | 60 |
| 2308 G | 1 | 25 | 14 | 69 | .6 | 2 | 3 | 970 | 3.36 | 74 | 5 | ND | 2 | 59 | 2 | 2 | 2 | 3 | 1.98 | .019 | 18 | 3 | .35 | 52 | .01 | 2 | .42 | .01 | .24 | 1 | 22 | 70 |
| 2309 G | 3 | 8 | 20 | 178 | .3 | 2 | 1 | 3057 | 3.00 | 2 | 5 | ND | 1 | 81 | 5 | 3 | 2 | 3 | 4.29 | .011 | 11 | 21 | 1.22 | 58 | .01 | 2 | .80 | .02 | .14 | 1 | 10 | 80 |
| 2310 G | 2 | 5 | 9 | 67 | .3 | 3 | 2 | 1953 | 3.14 | 3 | 5 | ND | 1 | 94 | 2 | 2 | 2 | 2 | 3.01 | .014 | 9 | 6 | .60 | 74 | .01 | 2 | .97 | .01 | .15 | 1 | 18 | 40 |
| 2311 G | 5 | 6 | 9 | 54 | .1 | 6 | 1 | 1254 | 1.60 | 2 | 5 | ND | 1 | 67 | 3 | 2 | 2 | 1 | 2.32 | .084 | 12 | 30 | .29 | 46 | .01 | 2 | .49 | .03 | .15 | 1 | 4 | 30 |
| 2312 G | 3 | 4 | 3 | 60 | 1.1 | 5 | 1 | 684 | 1.52 | 2 | 5 | ND | 1 | 36 | 3 | 2 | 2 | 1 | 1.49 | .082 | 13 | 5 | .15 | 63 | .01 | 2 | .45 | .02 | .17 | 2 | 6 | 40 |
| 2313 G | 9 | 6 | 9 | 146 | .1 | 7 | 1 | 709 | 1.57 | 2 | 5 | ND | 1 | 39 | 5 | 2 | 3 | 1 | 1.69 | .002 | 9 | 37 | .14 | 82 | .01 | 4 | .42 | .02 | .13 | 1 | 12 | 70 |
| 2314 G | 5 | 7 | 11 | 79 | .1 | 4 | 1 | 782 | 2.17 | 2 | 5 | ND | 1 | 51 | 4 | 2 | 2 | 1 | 1.63 | .007 | 10 | 6 | .24 | 60 | .01 | 3 | .73 | .02 | .15 | 1 | 22 | 30 |
| 2315 G | 7 | 6 | 4 | 56 | .1 | 7 | 1 | 614 | 1.84 | 2 | 5 | ND | 1 | 41 | 2 | 2 | 2 | 2 | 1.43 | .009 | 15 | 32 | .17 | 72 | .01 | 2 | .64 | .01 | .19 | 1 | 6 | 40 |
| 2316 G | 3 | 8 | 7 | 44 | .2 | 5 | 1 | 632 | 1.95 | 4 | 5 | ND | 2 | 50 | 2 | 2 | 4 | 1 | 1.54 | .007 | 16 | 5 | .16 | 52 | .01 | 2 | .59 | .04 | .18 | 1 | 3 | 30 |
| 2317 G | 7 | 13 | 7 | 23 | .2 | 4 | 2 | 943 | 2.10 | 10 | 5 | ND | 1 | 50 | 2 | 2 | 2 | 1 | 2.52 | .007 | 11 | 27 | .20 | 48 | .01 | 3 | .35 | .03 | .17 | 1 | 4 | 50 |
| 2318 G | 5 | 7 | 14 | 49 | .3 | 4 | 1 | 669 | 2.28 | 9 | 5 | ND | 2 | 37 | 6 | 2 | 2 | 1 | 1.76 | .008 | 14 | 5 | .23 | 72 | .01 | 2 | .38 | .02 | .18 | 1 | 9 | 60 |
| 2319 G | 10 | 23 | 7 | 87 | .2 | 15 | 1 | 1059 | 2.25 | 7 | 5 | ND | 1 | 39 | 4 | 2 | 2 | 1 | 1.73 | .008 | 10 | 42 | .48 | 33 | .01 | 2 | .22 | .04 | .11 | 1 | 8 | 80 |
| 2320 G | 3 | 9 | 4 | 70 | .2 | 5 | 1 | 774 | 2.13 | 3 | 5 | ND | 2 | 34 | 2 | 2 | 2 | 1 | 1.33 | .009 | 12 | 7 | .40 | 39 | .01 | 2 | .35 | .04 | .11 | 1 | 1 | 70 |
| 2321 G | 4 | 8 | 6 | 45 | .6 | 6 | 4 | 941 | 3.96 | 33 | 5 | ND | 1 | 39 | 2 | 2 | 2 | 5 | 1.49 | .020 | 3 | 29 | .55 | 65 | .01 | 3 | .41 | .01 | .07 | 1 | 13 | 130 |
| 2322 G | 2 | 8 | 4 | 68 | .5 | 2 | 3 | 2132 | 3.63 | 15 | 5 | ND | 1 | 40 | 2 | 3 | 5 | 4 | 2.21 | .038 | 6 | 8 | .76 | 74 | .01 | 2 | .61 | .01 | .03 | 1 | 7 | 110 |
| 2323 G | 4 | 6 | 6 | 79 | .4 | 1 | 3 | 1677 | 4.56 | 6 | 5 | ND | 1 | 64 | 12 | 4 | 3 | 5 | 1.75 | .060 | 8 | 16 | .71 | 119 | .01 | 2 | 1.16 | .02 | .12 | 1 | 4 | 60 |
| 2324 G | 4 | 9 | 5 | 139 | .2 | 4 | 3 | 853 | 2.95 | 6 | 5 | ND | 1 | 53 | 9 | 2 | 2 | 5 | 1.85 | .022 | 13 | 6 | .28 | 67 | .01 | 2 | .68 | .02 | .13 | 1 | 15 | 50 |
| 2325 G | 6 | 5 | 3 | 126 | .1 | 4 | 2 | 684 | 2.81 | 12 | 5 | ND | 1 | 34 | 6 | 2 | 2 | 1 | 1.09 | .013 | 10 | 24 | .15 | 73 | .01 | 2 | .92 | .03 | .18 | 1 | 7 | 40 |
| 2326 G | 7 | 3 | 4 | 196 | .1 | 5 | 2 | 811 | 2.14 | 16 | 5 | ND | 1 | 44 | 13 | 2 | 2 | 1 | 1.58 | .013 | 13 | 4 | .12 | 66 | .01 | 2 | .79 | .03 | .17 | 1 | 9 | 50 |
| 2327 G | 4 | 4 | 2 | 139 | .2 | 3 | 2 | 732 | 2.22 | 3 | 5 | ND | 1 | 34 | 8 | 2 | 2 | 1 | 1.35 | .012 | 9 | 4 | .14 | 55 | .01 | 2 | .74 | .02 | .16 | 1 | 10 | 40 |
| 2328 G | 4 | 8 | 3 | 382 | .1 | 2 | 2 | 1064 | 2.31 | 2 | 5 | ND | 1 | 49 | 2 | 4 | 2 | 1 | 1.80 | .010 | 9 | 2 | .13 | 65 | .01 | 4 | .70 | .03 | .16 | 1 | 18 | 80 |
| 2329 G | 5 | 9 | 5 | 549 | .1 | 4 | 2 | 891 | 2.24 | 2 | 5 | ND | 1 | 36 | 3 | 4 | 1 | 1.52 | .010 | 8 | 5 | .15 | 58 | .01 | 2 | .68 | .02 | .14 | 1 | 36 | 130 | |
| 2330 G | 4 | 7 | 8 | 195 | .2 | 2 | 2 | 974 | 2.54 | 2 | 5 | ND | 1 | 48 | 1 | 4 | 2 | 1 | 1.60 | .010 | 7 | 2 | .16 | 71 | .01 | 2 | .64 | .03 | .15 | 1 | 21 | 70 |
| 2331 G | 6 | 5 | 7 | 124 | .2 | 5 | 2 | 1169 | 2.67 | 3 | 5 | ND | 1 | 44 | 8 | 2 | 3 | 1 | 1.72 | .011 | 6 | 6 | .28 | 62 | .01 | 3 | .50 | .02 | .15 | 1 | 25 | 60 |
| 2332 G | 4 | 6 | 16 | 126 | .2 | 2 | 2 | 1137 | 2.44 | 3 | 5 | ND | 1 | 42 | 7 | 2 | 3 | 1 | 1.93 | .013 | 6 | 4 | .25 | 46 | .01 | 2 | .45 | .02 | .18 | 1 | 42 | 50 |
| STANDARD C/AU-R | 18 | 60 | 37 | 130 | 7.0 | 71 | 31 | 1056 | 3.99 | 30 | 15 | 7 | 37 | 53 | 18.6 | 15 | 18 | 55 | .52 | .097 | 37 | 60 | .89 | 182 | .07 | 32 | 1.89 | .06 | .13 | 13 | 474 | 1500 |

W/P 12

420 PWS

SEP 25 '90 11:56

| SAMPLE# | Mo | Cu | Pb | Zn | Ag | Ni | Co | Mn | Fe | As | U | Au | Th | Sr | Cd | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | Ti | B | Al | Na | K | U: Au** | ppb | ppb |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|-------|-----|-----|-------|-------|-------|-------|-------|-------|-------|---------|-----|------|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | % | % ppm | ppm | ppm | % ppm | % ppm | % ppm | % ppm | % ppm | % ppm | % ppm | % ppm | ppm | ppm |
| 2333 G | 6 | 4 | 6 | 132 | 3 | 6 | 1 | 1155 | 2.18 | 2 | 5 | ND | 1 | 34 | 3 | 2 | 2 | 1 | 1.67 | .013 | 6 | 6 | .27 | 48 | .01 | 5 | .73 | .02 | .15 | 1 | 20 | 30 |
| 2334 G | 5 | 5 | 3 | 139 | 3 | 4 | 2 | 1014 | 2.85 | 5 | 5 | ND | 1 | 32 | 5 | 2 | 2 | 1 | 1.36 | .011 | 5 | 3 | .23 | 59 | .01 | 2 | .74 | .02 | .15 | 1 | 14 | 50 |
| 2335 G | 4 | 4 | 11 | 137 | 6 | 5 | 2 | 949 | 2.42 | 22 | 5 | ND | 1 | 30 | 5 | 2 | 2 | 1 | 1.39 | .011 | 5 | 6 | .19 | 56 | .01 | 2 | .52 | .01 | .17 | 1 | 437 | 110 |
| 2336 G | 2 | 6 | 4 | 83 | 3 | 3 | 2 | 935 | 2.59 | 10 | 5 | ND | 1 | 48 | 2 | 2 | 2 | 1 | 1.36 | .011 | 5 | 2 | .18 | 46 | .01 | 2 | .57 | .01 | .16 | 1 | 137 | 70 |
| 2337 G | 3 | 4 | 7 | 130 | 3 | 6 | 1 | 1246 | 1.96 | 6 | 5 | ND | 1 | 64 | 5 | 2 | 2 | 1 | 1.98 | .011 | 7 | 4 | .17 | 42 | .01 | 2 | .62 | .01 | .17 | 1 | 15 | 60 |
| 2338 G | 2 | 5 | 6 | 115 | 3 | 2 | 1 | 945 | 2.23 | 3 | 5 | ND | 1 | 37 | 3 | 2 | 2 | 1 | 1.50 | .011 | 9 | 2 | .14 | 51 | .01 | 3 | .58 | .02 | .15 | 1 | 8 | 50 |
| 2339 G | 3 | 5 | 6 | 115 | 2 | 5 | 1 | 793 | 2.50 | 3 | 5 | ND | 1 | 29 | 7 | 2 | 2 | 1 | 1.09 | .010 | 10 | 5 | .18 | 113 | .01 | 2 | .76 | .02 | .13 | 1 | 126 | 30 |
| 2340 G | 7 | 7 | 3 | 163 | 3 | 5 | 4 | 914 | 2.55 | 6 | 5 | ND | 1 | 51 | 6 | 2 | 2 | 8 | 1.95 | .020 | 8 | 6 | .31 | 52 | .01 | 2 | .57 | .01 | .14 | 1 | 106 | 80 |
| 2341 G | 7 | 5 | 4 | 147 | 3 | 5 | 1 | 328 | 1.23 | 3 | 6 | ND | 1 | 22 | 6 | 2 | 2 | 1 | .52 | .001 | 13 | 4 | .12 | 66 | .01 | 3 | .32 | .02 | .15 | 1 | 24 | 90 |
| 2342 G | 6 | 4 | 6 | 104 | 2 | 1 | 1 | 640 | 1.41 | 4 | 5 | ND | 1 | 50 | 2 | 2 | 2 | 1 | 1.30 | .001 | 14 | 1 | .10 | 31 | .01 | 2 | .38 | .03 | .14 | 1 | 29 | 50 |
| 2343 G | 3 | 5 | 4 | 98 | 1 | 5 | 1 | 624 | 1.46 | 2 | 5 | ND | 1 | 48 | 2 | 2 | 2 | 1 | 1.44 | .001 | 17 | 5 | .13 | 53 | .01 | 2 | .47 | .01 | .14 | 1 | 10 | 60 |
| 2344 G | 4 | 5 | 3 | 136 | 1 | 2 | 1 | 615 | 1.19 | 2 | 5 | ND | 1 | 47 | 1 | 2 | 2 | 1 | 1.55 | .001 | 16 | 1 | .10 | 32 | .01 | 3 | .36 | .02 | .13 | 1 | 9 | 50 |
| 2345 G | 3 | 6 | 8 | 50 | 2 | 4 | 1 | 699 | 2.69 | 2 | 5 | ND | 3 | 27 | 2 | 2 | 2 | 1 | 1.26 | .008 | 12 | 5 | .24 | 47 | .01 | 2 | .69 | .03 | .07 | 1 | 18 | 60 |
| 2346 G | 1 | 7 | 2 | 76 | 3 | 4 | 3 | 735 | 3.23 | 2 | 5 | ND | 3 | 40 | 2 | 2 | 2 | 6 | 1.18 | .018 | 11 | 4 | .31 | 37 | .01 | 2 | .99 | .04 | .07 | 1 | 17 | 50 |
| 2347 G | 5 | 10 | 4 | 90 | 5 | 13 | 8 | 1006 | 4.19 | 8 | 5 | ND | 1 | 71 | 2 | 2 | 2 | 17 | 1.75 | .044 | 13 | 11 | .51 | 90 | .01 | 2 | 1.31 | .02 | .12 | 1 | 17 | 70 |
| STANDARD C/AU-R | 18 | 58 | 40 | 133 | 7.1 | 71 | 31 | 1057 | 3.99 | 41 | 15 | 7 | 37 | 53 | 18.5 | 15 | 20 | 55 | .52 | .096 | 37 | 60 | .90 | 180 | .07 | 36 | 1.89 | .06 | .14 | 11 | 492 | 1400 |

4.30 PM

SEP 25 '90 11:57

| SAMPLE# | Mo | | Cu | | Pb | | Zn | | Ag | | Ni | | Co | | Mn | | Fe | | As | | U | | Au | | Th | | Sr | | Cd | | Sb | | Bi | | V | | Ca | | P | | La | | Cr | | Mg | | Ba | | Ti | | B | | Al | | Na | | K | | V | | Ni | | Hg | |
|-------------------|-----|-----|-----|-----|-----|-----|-----|------|------|------|-----|-----|-----|-----|------|-------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|----|--|
| | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | | |
| 3179 G | 1 | 65 | 20 | 15 | 2.9 | 6 | 12 | 86 | 5.01 | 214 | 5 | ND | 1 | 71 | .2 | 10 | 2 | 36 | .28 | 207 | 6 | 2 | .07 | 77 | .01 | 5 | .47 | .02 | .21 | 1 | 81 | 140 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3180 G | 2 | 57 | 23 | 27 | 2.2 | 8 | 8 | 66 | 3.41 | 350 | 5 | ND | 1 | 73 | .2 | 8 | 5 | 31 | .24 | 169 | 5 | 4 | .08 | 88 | .01 | 5 | .47 | .02 | .14 | 2 | 180 | 110 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3181 G | 1 | 49 | 12 | 74 | 1.5 | 9 | 10 | 143 | 3.77 | 173 | 5 | ND | 1 | 79 | .2 | 4 | 2 | 67 | .37 | 166 | 7 | 6 | .48 | 81 | .01 | 4 | 1.06 | .03 | .12 | 1 | 71 | 40 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3182 G | 2 | 61 | 52 | 80 | 5.4 | 9 | 13 | 156 | 6.44 | 884 | 5 | ND | 1 | 67 | .2 | 18 | 3 | 102 | .22 | 122 | 5 | 11 | .47 | 53 | .01 | 4 | .94 | .04 | .09 | 2 | 1847 | 160 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3183 G | 1 | 111 | 7 | 88 | 1.7 | 10 | 19 | 1055 | 7.07 | 68 | 5 | ND | 1 | 61 | .2 | 7 | 2 | 189 | 1.88 | 233 | 8 | 13 | 1.85 | 61 | .01 | 4 | 2.18 | .04 | .09 | 1 | 30 | 110 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3184 G | 1 | 77 | 5 | 97 | 1.1 | 11 | 19 | 787 | 6.56 | 48 | 5 | ND | 1 | 55 | .2 | 6 | 3 | 223 | 1.62 | 215 | 7 | 15 | 1.99 | 50 | .01 | 2 | 2.32 | .04 | .04 | 1 | 28 | 70 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3185 G | 1 | 96 | 15 | 84 | .8 | 10 | 22 | 1494 | 7.06 | 26 | 5 | ND | 1 | 85 | .4 | 6 | 5 | 216 | 3.58 | 232 | 10 | 14 | 2.83 | 90 | .01 | 3 | 2.61 | .04 | .07 | 1 | 4 | 60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3186 G | 1 | 80 | 12 | 86 | .9 | 10 | 23 | 1391 | 6.84 | 19 | 5 | ND | 1 | 75 | .3 | 5 | 2 | 237 | 3.17 | 219 | 9 | 13 | 2.84 | 47 | .01 | 3 | 2.52 | .04 | .03 | 1 | 7 | 40 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3187 G | 1 | 67 | 12 | 96 | 1.1 | 10 | 23 | 1154 | 7.07 | 19 | 5 | ND | 1 | 68 | .2 | 10 | 3 | 226 | 2.94 | 221 | 9 | 14 | 2.57 | 58 | .01 | 4 | 2.53 | .04 | .04 | 1 | 15 | 60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3188 G | 1 | 62 | 13 | 61 | 1.4 | 7 | 13 | 1178 | 4.38 | 30 | 5 | ND | 1 | 72 | .3 | 5 | 5 | 155 | 3.21 | 225 | 7 | 14 | 1.43 | 57 | .01 | 4 | 1.23 | .05 | .08 | 1 | 18 | 50 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3189 G | 2 | 37 | 17 | 101 | 1.6 | 7 | 14 | 226 | 3.92 | 212 | 5 | ND | 1 | 37 | .2 | 5 | 2 | 95 | .57 | 210 | 10 | 7 | .54 | 106 | .01 | 2 | 1.03 | .04 | .10 | 1 | 65 | 110 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3190 G | 2 | 14 | 12 | 136 | .9 | 4 | 15 | 518 | 7.00 | 71 | 5 | ND | 1 | 38 | .2 | 5 | 2 | 125 | .86 | 201 | 12 | 9 | 2.05 | 129 | .01 | 5 | 2.72 | .02 | .08 | 1 | 24 | 50 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3191 G | 1 | 27 | 15 | 172 | 1.7 | 6 | 15 | 273 | 7.14 | 155 | 5 | ND | 1 | 61 | .4 | 9 | 3 | 156 | .58 | 207 | 8 | 9 | 1.91 | 126 | .01 | 5 | 2.59 | .03 | .06 | 1 | 66 | 180 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3192 G | 1 | 58 | 18 | 118 | 1.8 | 10 | 21 | 709 | 7.13 | 132 | 5 | ND | 1 | 53 | .5 | 10 | 4 | 188 | 1.25 | 227 | 8 | 14 | 1.93 | 124 | .01 | 8 | 2.68 | .03 | .06 | 1 | 36 | 60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3193 G | 1 | 17 | 20 | 129 | 1.8 | 4 | 14 | 172 | 7.80 | 139 | 5 | ND | 1 | 26 | .2 | 10 | 2 | 118 | .49 | 214 | 11 | 10 | 1.57 | 179 | .01 | 6 | 2.68 | .01 | .10 | 1 | 54 | 60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3194 G | 3 | 20 | 17 | 169 | 3.2 | 6 | 12 | 158 | 4.62 | 268 | 5 | ND | 1 | 23 | .6 | 8 | 2 | 45 | .24 | 130 | 7 | 6 | .44 | 246 | .01 | 4 | .95 | .01 | .10 | 1 | 74 | 330 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 3195 G | 2 | 11 | 17 | 166 | 1.1 | 3 | 16 | 362 | 6.88 | 58 | 5 | ND | 1 | 25 | .6 | 10 | 2 | 120 | .54 | 182 | 13 | 10 | 2.18 | 351 | .01 | 6 | 2.87 | .01 | .08 | 1 | 13 | 40 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| D-8-L.S.-U.R.-90 | 1 | 100 | 26 | 36 | 3.5 | 12 | 18 | 74 | 6.08 | 257 | 5 | ND | 1 | 32 | .2 | 13 | 2 | 61 | .38 | 164 | 5 | 12 | .36 | 32 | .01 | 8 | .69 | .03 | .14 | 1 | 116 | 80 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| D-9-L.S.-U.R.-90 | 3 | 15 | 12 | 43 | .8 | 5 | 14 | 114 | 3.78 | 55 | 5 | ND | 1 | 32 | .2 | 6 | 2 | 34 | .53 | 180 | 8 | 5 | .54 | 79 | .01 | 5 | .76 | .03 | .16 | 1 | 18 | 60 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| D-10-L.S.-U.R.-90 | 3 | 18 | 35 | 88 | 4.3 | 5 | 6 | 50 | 4.20 | 305 | 5 | ND | 1 | 142 | .2 | 10 | 2 | 17 | .02 | 088 | 5 | 2 | .02 | 112 | .01 | 2 | .26 | .02 | .30 | 1 | 145 | 250 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| L.S.-U.R.-102-90 | 2 | 124 | 31 | 10 | .8 | 15 | 20 | 676 | 4.67 | 35 | 5 | ND | 1 | 61 | .3 | 15 | 3 | 27 | 2.08 | 142 | 4 | 8 | .71 | 49 | .01 | 2 | .33 | .01 | .15 | 1 | 12 | 510 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| L.S.-U.R.-103-90 | 1 | 83 | 8 | 60 | .4 | 9 | 16 | 567 | 4.51 | 2578 | 5 | 2 | 1 | 442 | .2 | 67 | 2 | 33 | 3.55 | 080 | 3 | 11 | 1.71 | 107 | .01 | 5 | .24 | .01 | .15 | 1 | 1801 | 150 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| U.R.-90-88-1 | 1 | 80 | 15 | 57 | .3 | 8 | 14 | 850 | 3.50 | 118 | 5 | ND | 1 | 193 | .2 | 24205 | 2 | 14 | 4.01 | 060 | 2 | 6 | .68 | 22 | .01 | 6 | .20 | .01 | .11 | 1 | 483 | 190 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| U.R. 5050N 2300E | 6 | 7 | 22 | 20 | 2.3 | 5 | 1 | 64 | 2.20 | 60 | 5 | ND | 3 | 3 | .2 | 51 | 3 | 1 | .01 | 806 | 15 | 3 | .01 | 59 | .01 | 4 | .18 | .01 | .15 | 1 | 44 | 200 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| U.R. 3448N 2016E | 45 | 9 | 42 | 632 | 3.4 | 1 | 3 | 123 | 9.90 | 81 | 7 | ND | 1 | 3 | .8 | 161 | 2 | 5 | .03 | 007 | 8 | 11 | .78 | 11 | .01 | 6 | .82 | .02 | .10 | 1 | 6 | 1700 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| U.R. 3200N 1720E | 2 | 47 | 15 | 46 | .2 | 13 | 9 | 316 | 2.18 | 48 | 5 | ND | 1 | 146 | .2 | 10 | 2 | 5 | 2.24 | 043 | 6 | 7 | .21 | 105 | .01 | 5 | .48 | .02 | .18 | 1 | 7 | 210 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| U.R.-90-100 | 1 | 129 | 14 | 71 | .3 | 7 | 16 | 1311 | 5.74 | 7 | 5 | ND | 1 | 79 | .3 | 16 | 2 | 95 | 4.00 | 173 | 9 | 15 | 1.98 | 111 | .01 | 7 | 2.37 | .01 | .21 | 1 | 7 | 100 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| U.R.-90-101 | 4 | 17 | 12 | 107 | 2.3 | 5 | 4 | 150 | 3.17 | 54 | 5 | ND | 2 | 17 | .2 | 20 | 2 | 95 | .40 | 139 | 10 | 11 | .85 | 31 | .01 | 3 | 1.03 | .03 | .07 | 1 | 228 | 240 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| STANDARD C/AU-R | 18 | 60 | 43 | 132 | 7.1 | 70 | 31 | 1059 | 3.99 | 40 | 17 | 7 | 37 | 53 | 18.6 | 15 | 21 | 55 | .53 | 098 | 37 | 60 | .90 | 181 | .07 | 34 | 1.90 | .06 | .13 | 13 | 490 | 1400 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

436 P05

SEP 25 '90 11:58

GEOCHEMICAL ANALYSIS CERTIFICATE

Granges Inc. PROJECT 134 File # 90-4476 Page 1
2300 - 885 W. Georgia St., Vancouver BC V6C 3E8

HP 12

Table with columns for SAMPLE#, Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, Ca, P, La, Cr, Mg, Ba, Ti, B, Al, Na, K, W, Au**, Hg. Rows contain various sample IDs and their corresponding chemical analysis values in ppm and ppb.

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: CORE AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. HG ANALYSIS BY FLAMELESS AA.

DATE RECEIVED: SEP 16 1990 DATE REPORT MAILED: Sept 19/90 SIGNED BY: [Signature] ID. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Page 1 of 14

Property UNUK River Option Project No. 134 Depth 300.84 m. Date Began Aug. 15/1990
 Hole No. AP-6 Co. ord. 1350N/88.5W Horizontal Length 227 m. Date Completed Aug. 19/1990
 Claim No. UNUK 26 Core Size BG BDM Drilled By J.T. Thomas
 Grid No. Zone 1 Angle & Direction -45° az 302° Elevation 1268 m. Logged By D. Gaboury

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 0 - 4.10 | Casing | | | | | | | | |
| 4.10 - 44.50 | Greywacke - Fine to med. grained, silt to fine sand, muddy matrix, minor argillaceous interbeds. - Fossiliferous, with calcite replacement of bivalves, and minor pyrite replacement. - numerous small scale bedding disruptions (rehealed), moderately fractured, with thin limonite coatings, spaced 5-20 cm apart. - Overall 1-2% finely disseminated py., with minor small patches of 2-3% py. | | | | | | | | |
| 7.30 - 7.92 | close spaced, irregular fractures, 1-2 cm spacing, | | | | | | | | |
| 11.00 - 11.45 | broken core - shear zone, 50% recovery | | | | | | | | |
| 15.55 - 16.05 | rubbly broken core, 50% recovery | | | | | | | | |
| 18.30 - 20.10 | broken core, sharp irregular fractures abundant limonite coating. | | | | | | | | |
| 20.22 - 20.52 | rubbly, broken core, with talc and graphite coatings, .5cm of clayey/graphitic gouge. Irregular core angles, ~60° to CA. | | | | | | | | |
| 20.67 - 20.77 | rubbly, ground core. | | | | | | | | |
| 26.30 - 30.00 | well fractured, 1-2 cm spacing. Irregular core angles, limonite coating. | | | | | | | | |
| 30.00 - 37.70 | black argillaceous interbed, - muddy arenaceous, minor fine white calcite stringers, fossils | | | | | | | | |

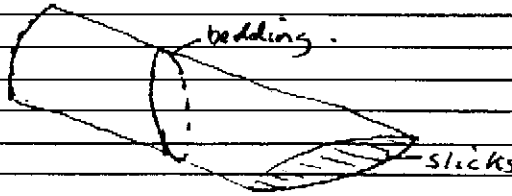
**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

20,390

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

20/ 14

Hole No. A.P. 6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. |
| - 33.86 - 37.5 | <p>Strongly fractured section with 2.5 - 2 cm spacing, limonite stain.</p> <p>- minor slickensides on graphitic slip surfaces, at 45° to CA. slicks rake 20° from horizontal.</p>  | | | | | | | |
| 37.70 - 37.86 | 3-5% diss. py in small pod, in med. grained grey wacke. | | | | | | | |
| 37.90 - 38.71 | broken, well fractured core, 1-2cm spacing. | | | | | | | |
| 40.23 - 41.15 | <p>Fault zone, graphite/talc gouge, tectonic brecciation + rehealing.</p> <p>- Fault at 30°-45° to C.A.</p> <p>- 10-15% tan to greenish grey sericitized breccia frags.</p> <p>10% QTZ + calcite + silts + strags.</p> | | | | | | | |
| 40.85 - 40.90 | 10-15% Qtz-carb stwk with 3-5% diss. py | | | | | | | |
| 41.15 - 41.45 | interbedded argillaceous dacitic debris flow 2-1.0 cm dacitic lithic fragments. | | | | | | | |
| 45.50 - 45.13 | <p>Transitional contact, from argillaceous greywacke to dacitic lapilli tuff.</p> <p>- weakly sericitized partially pyrite replaced angular fragments of dacite, 2-3.0 cm across, elongate parallel to bedding/foliation, in argillaceous matrix.</p> | | | | | | | |

3 of 14

Hole No. AP 6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | - Some fragments have zoned altin with silicified cores surrounded by pyrite, and sericitized rims. | | | | | | | | |
| | - minor (<2%) fine Qtz stringers and cross-cutting veinlets, 1-cm py stringer at lower contact. | | | | | | | | |
| | Core angles: | | | | | | | | |
| | (Bedding) 11.00 m. : 49° | | | | | | | | |
| | 32.00 : 48° | | | | | | | | |
| | 39.20 : 43° | | | | | | | | |
| | 43.00 : 35° | | | | | | | | |
| | 44.20 : 40° | | | | | | | | |
| | 44.90 : 65° | | | | | | | | |
| 45.13 - 48.20 | Dacitic lapilli-ash tuff | | | | | | | | |
| | - med. to coarse grained with .5 to 2.0cm long fragments, weakly chloritic | | | | | | | | |
| | - overall medium bluish-grey, (5B 5/1) to greenish grey. | | | | | | | | |
| | - minor limonite coated fractures at irregular angles | | | | | | | | |
| | - moderately well foliated | | | | | | | | |
| | - patchy pyrite replacement, minor stringers overall 5% py. | | | | | | | | |
| | 46.00 - 46.50 fine Qtz ladder veins at ~55° to core axis, in bleached zone parallel to bedding. | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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Hole No. AP6 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 48.20 - 57.90 | Argillaceous siltstone - massive, fine grained generally black to dark grey with minor sandy greywacke interbands. - strongly fractured, 1-3cm. spacing minor slickensides, with Qtz-chlor veining. | | | | | | | | |
| 48.20 - 51.30 | - weakly silicified zone, with ~2% fine Qtz veinlets, with chlorite & calcite, Tr-1% py. | | | | | | | | |
| 50.00 - 51.30 | - close spaced Qtz-chlorite tension joints, 1-2mm, parallel to core axis, with 1-2% fine diss. py. | | | | | | | | |
| 51.30 - 54.00 | - light greenish grey (5GY 6/1) altered, strongly silicified siltstone - 5% fine Qtz-carb. streak and 3-5% very fine black, diffuse hairline veinlets. - 10 to 30 cm. spaced fractures, - 3-5% py stringers + veinlets. | | | | | | | | |
| 53.85 - 54.0 | - 1-2 cm. wide Qtz vein subparallel to core axis, with patchy pink carbonate and arborescent dark brownish black mineral - sharp lower contact with 2cm. of 10% diss. py band. | | | | | | | | |
| Core angles (Bedding): | 45.20 m. : 45° 47.00 : 45° 55.00 : 45° 57.90 : 50° | | | | | | | | |

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 57.90 - 72.50 | Dacitic Lapilli - ash Tuff | | | | | | | | |
| | - medium bluish grey (SB 5/1) with dark greenish grey (SB 4/1) elongated fragments, up to 1x3cm matrix supported | | | | | | | | |
| | - <1% pyritic fragments, with Qtz-chlorite alteration | | | | | | | | |
| | - weakly pervasive sericite alt'n. | | | | | | | | |
| | 62.5 - 62.60 : 50-60% py in strongly silicified tuff section. | | | | | | | | |
| | 63.0 - 63.40 : fine grained tuff, weakly banded, 1cm. py band at top contact. | | | | | | | | |
| | 63.50 - 63.90 : 2-3% py blebs & nests, & fragments | | | | | | | | |
| | 63.90 - 63.97 : band of 10% diss. py. | | | | | | | | |
| | 69.05 - 69.10 : band of 10-15% diss. py, at ~ 25° to C.A. | | | | | | | | |
| | 69.70 - 70.40 : 5-8% diss. py, 1-2% blebs of fragments | | | | | | | | |
| | Core angles (bedding/foliation) | | | | | | | | |
| | 59.60 m. : 45° | | | | | | | | |
| | 62.20 : 55° | | | | | | | | |
| | 71.70 : 48° | | | | | | | | |

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Hole No. AP 6 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 72.50 - 82.75 | Argillaceous lapilli tuff - dark bluish grey (SB 3/1) - dacitic, locally silicified heterolithic tuff with 10-15% argillite fragments, 20% dacite fragments, in argillaceous/tuffaceous matrix, locally clast-supported. - fragments up to 1 x 4 cm. - overall Tr-1% py - minor interbedded siltstone/argillite. | | | | | | | | |
| 73.76 - 74.06 | : massive fine grained silicified section, poorly banded with minor sericite-altered fragments, Tr cpy py | | | | | | | | |
| 74.65 - 74.80 | : Tr-1% pyrochroite, cpy, in minor Qtz-carb. veinlets | | | | | | | | |
| 74.95 - 75.50 | : argillite/siltstone, thinly banded, with 2-3% diss. py | | | | | | | | |
| 78.10 - 78.55 | : 1-2% blebs + diss. py, 2cm. band at 78.30m. | | | | | | | | |
| 79.50 - 79.74 | : Black argillite with wispy py blebs and disseminations, 3-5% py | | | | | | | | |
| 79.74 - 79.94 | : 10-20% py blebs + bands, with Qtz-carb. veinlets strongly silicified tuff, & graphitic argillite 5cm. diss. py. band at 79.75m. | | | | | | | | |
| 79.94 - 80.85 | : 1-2% diss. py, minor blebs, in lapilli tuff. | | | | | | | | |
| * 80.85 - 81.20 | : 20-25% py, in blebs & bands, with a 10cm section of near massive py in silicified argillite | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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Hole No. AP 6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | 81.58 - 81.66 : 5-10% py in bands, weakly silicified tuff. | | | | | | | | |
| | 82.70 - 84.50 : banded argillaceous lapilli tuff, with 1-2% py blebs | | | | | | | | |
| | 84.95 - 85.40 : 3-5% py diss. & blebs in slightly argillaceous lapilli tuff | | | | | | | | |
| | 85.40 - 85.65 : 20% py, silicified tuff | | | | | | | | |
| | 85.65 - 87.75 : 3-5% py streaks & blebs in argillaceous tuff, with abundant Qtz - carb. vnlts. | | | | | | | | |
| | 87.30 - 87.40 : fault gouge, sandy / clayey, calcitic, brecciated argillaceous stuff. | | | | | | | | |
| | Core Angles (bedding/foliation): | | | | | | | | |
| | 73.00 m. : 45° | | | | | | | | |
| | 76.50 m. : 47° | | | | | | | | |
| | 85.00 : 48° | | | | | | | | |
| | 90.00 : 49° | | | | | | | | |
| 87.75 - 125.20 | Interbedded Argillite & Siltstone | | | | | | | | |
| | - Black, finely laminated to massive | | | | | | | | |
| | - 2-3% fine irregular cross cutting carbonate veinlets | | | | | | | | |
| | - Tr graphite on slip surfaces, and numerous small scale bedding disruptions. | | | | | | | | |
| | 89.65 - 90.00 : 2-3% py in irregular, <2mm thick | | | | | | | | |
| | 91.60 - 91.70 : 3-5% py blebs & streaks, minor coarse argillaceous breccia | | | | | | | | |
| | 93.80 - 94.10 : patchy py, 5-10% overall | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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 Hole No. AP 6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 97.75 - 97.95 | : 3-5% py blebs & stringers | | | | | | | | |
| 101.70 - 103.65 | : folded bedding, generally parallel to core axis, in interbedded siltstone/margillite with 3-5% py blebs & dissemination | | | | | | | | |
| 103.65 - 104.85 | : cobbly-angular broken core with graphitic fault gouge at 103.65 - 103.90 | | | | | | | | |
| 105.60 - 106.38 | : Broken sheared core, minor polished graphitic fault surfaces | | | | | | | | |
| 107.10 - 107.40 | : broken, graphitic section bedding = parallel faults | | | | | | | | |
| 107.70 - 109.00 | : 2-3% diss. + banded py | | | | | | | | |
| 109.31 - 109.37 | : silicified band, parallel to bedding; sericitic with perpendicular Qtz-carb. tension veins | | | | | | | | |
| 109.97 - 110.03 | : 2-3% disseminated & banded - py | | | | | | | | |
| 110.67 - 110.74 | : graphitic clay gouge, at 45° to core axis | | | | | | | | |
| 110.80 - 111.30 | : 3-5% disseminated and blebs py | | | | | | | | |
| 111.30 - 112.20 | : Slivery broken core with numerous graphitic + talcy slip surfaces at irregular core angles generally ~45° to C.A. with minor slickensides raking @ at ~80° down dip | | | | | | | | |
| 113.10 - 113.45 | : 5-10% py | | | | | | | | |

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Hole No. AP 6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 113.80 - 113.90 | : 15-20% diss. py in small lens, with surrounding 10cm of 3-5% py | | | | | | | | |
| 116.75 - 116.84 | : band of finely disseminated py. | | | | | | | | |
| 117.85 - 119.18 | : Fault gouge & broken core, graphitic clay gouge, at 118.05-118.25, 118.46-118.50, and 118.95-119.10, all parallel to bedding at ~40° to C.A. | | | | | | | | |
| 119.18 - 120.00 | : Folded bedding, parallel to core axis. | | | | | | | | |
| Core angles (bedding): | | | | | | | | | |
| | 99.90 m. : 25° | | | | | | | | |
| | 102.00 : 9° | | | | | | | | |
| | 105.00 : 25° | | | | | | | | |
| | 110.00 : 35° | | | | | | | | |
| | 116.90 : 45° | | | | | | | | |
| | 119.50 : 0° | | | | | | | | |
| | 121.10 : 50° | | | | | | | | |
| | 124.50 : 55° | | | | | | | | |
| 125.20 - 150.80 | Dacitic Ash-lapilli tuff | | | | | | | | |
| | - medium to dark bluish black matrix with lighter, greenish grey altered sections and sericitized fragments | | | | | | | | |
| | - minor argillite and argillaceous debris flow interbeds. | | | | | | | | |
| | - irregular upper contact at very low core angle, with band of diss. py, 3-5%, along contact from 125.20 - 126.00 m | | | | | | | | |
| | - Tr pycritic fragments with altered rims. | | | | | | | | |


**GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG**

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Hole No. A.P.-6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 125.20 - 129.20 | : strongly altered section, sericitized and bleached to greenish grey, mottled, with relic fragments, 3-5% py. | | | | | | | | |
| 129.20 - 131.15 | : graphitic argillite, Tr-1% py | | | | | | | | |
| 131.15 - 131.35 | : sericitized breccia fragments in argillaceous tuff, weakly silicified, 3-5% py stringers | | | | | | | | |
| 134.80 - 135.55 | : 2-3% py stringers and blebs in weakly silicified section, with 5-10% irregular, cross-cutting Qtz-carb. veinlets. | | | | | | | | |
| 143.20 - 148.40 | : re-silicified altered breccia, light greenish grey, weakly sericitized fine grained matrix with relic fragments, 146.40 - 146.50 : 5-10% diss. py | | | | | | | | |
| 148.40 - 150.80 | : Massive graphitic argillite, with minor x-cutting carb-veinlets. | | | | | | | | |
| Core Angles (Bedding): | | | | | | | | | |
| | 137.2 = : 45° | | | | | | | | |
| | 142.6 = : 45° | | | | | | | | |
| | 154.0 = : 47° | | | | | | | | |

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 150.80 - 280.30 | Argillaceous debris flow - overall greenish grey dacitic fragments, angular, 2-1.0 cm. in black or greenish black argillite matrix. - locally well bedded with ~ 1-3% diss. py, minor bands of 5-8% py, 1-2 cm. thick. - 1-2% x-cutting Qtz-carb veinlets, 1-2 cm. | | | | | | | | |
| 162.40 - 162.70 | : fault zone, brecciated, graphitic/clay gouge, minor Qtz-carb veinlets, parallel to bedding. | | | | | | | | |
| 166.60 - 166.90 | : broken core and graphitic gouge section | | | | | | | | |
| 179.50 - 181.00 | : broadly folded bedding, sub-parallel to core axis, with broken, faulted section, polished graphitic fault surfaces at irregular core angles. | | | | | | | | |
| 191.40 - 197.70 | : massive argillite section | | | | | | | | |
| 193.20 - 193.30 | : graphitic fault gouge. | | | | | | | | |
| 197.70 - 198.50 | : broken core 20cm. graphitic gouge 198.2 - 198.40 | | | | | | | | |
| 199.45 - 199.90 | : Qtz vein, 2cm wide at ±5° to C.A. | | | | | | | | |
| 200.25 - 200.35 | : Clay gouge seam in debris flow. | | | | | | | | |

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 208.00 - 214.40 | : graphitic argillite with close spaced fault cleavages at ~70° to core axes. with slickensides striking 45° from vertical. - numerous small graphitic gouge sections. | | | | | | | | |
| 218.00 - 218.50 | : slivery - broken core, graphitic slip surfaces and gouge. | | | | | | | | |
| 223.07 - 223.20 | : graphitic and sandy gouge. | | | | | | | | |
| 230.20 - 238.75 | : closely spaced fracturing with graphitic gouge sections 5-10 cm thick, - minor Qtz-carb veins parallel to bedding. | | | | | | | | |
| 239.20 - 239.80 | fault zone, broken core, 10-20 cm of graphitic gouge | | | | | | | | |
| 241.20 - 248.70 | : altered tuffaceous section - greyish to dusky yellowish green (5 GY 6/2) - sericitized, fine ground mass with 20-30% clay altered feldspar xls, Tr/py minor argillite debris flow interbeds | | | | | | | | |
| 245.36 - 247.00 | - Strongly brecciated tuffaceous debris flow, with numerous gouge sections + broken core. - talc coating fractures at bottom contact, at 40° to core axis | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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Hole No. AP. 6 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 250.76 - 253.15 | : fault zone in poorly laminated leucis (low / argillite) with numerous gouge sections | | | | | | | | |
| 255.00 - 256.00 | : rubble, broken core, with graphitic / clay gouge. | | | | | | | | |
| 261.80 - 262.86 | : Fault zone, broken core and graphitic gouge. | | | | | | | | |
| 264.30 - 264.85 | : fault zone graphitic gouge, minor talc. 1cm. Qtz-carb. vein, parallel to bedding at bottom of section | | | | | | | | |
| Core Angles (bedding): | | | | | | | | | |
| | 154.0 m | 47° | | | | | | | |
| | 159.0 m | 43° | | | | | | | |
| | 175.00 | 42° | | | | | | | |
| | 212.00 | 90° | | | | | | | |
| | 216.00 | 70° | | | | | | | |
| | 220.50 | 35° | | | | | | | |
| | 230.50 | 60° | | | | | | | |
| | 233.30 | 75° | | | | | | | |
| | 237.40 | 70° | | | | | | | |
| | 253.80 | 38° | | | | | | | |
| | 260.60 | 60° | | | | | | | |
| | 261.50 | 34° | | | | | | | |
| | 265.80 | 55° | | | | | | | |
| | 269.00 | 48° | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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Hole No. A.P. 6 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 280.30 - 300.84 | Dacitic Lapilli Tuff - bluish grey, partly welded tuff, with dacitic fragments up to 10 cm - matrix supported, and <5% argillite fragments. - weak, pervasive sericite alteration. | | | | | | | | |
| 285.00 - 285.60 | : 2-3% py stringers & blebs | | | | | | | | |
| 288.90 - 289.00 | : vuggy Qtz - carb. veinlets 2-3% py blebs. | | | | | | | | |
| 293.50 - 299.00 | : argillaceous debris flow with numerous fault gouge sections. | | | | | | | | |
| 294.50 - 295.20 | : 30% core recovery, 1-2% blebs & stringers py, | | | | | | | | |
| 299.30 - 300.84 | : bleached light bluish grey sericitized and clay-altered tuff. Tr-1% diss py. broken, rubbly core. | | | | | | | | |
| 300.84 | E.O.H - abandoned | | | | | | | | |
| | Acid tests | | | | | | | | |
| | 184.22 m ; 40° corrected | | | | | | | | |
| | 255.0 m ; 38° corrected. | | | | | | | | |



GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. ppb | Ag. ppm | Cu. | Zn. | As. ppm | WIDTH X ASSAY | | | | | AVERAGES | | | | | | | |
|---------------------------|--------|-------|------------|------------|-----|-----|------------|---------------|-----|-----|-----|-----|----------|-------|-----|-----|-----|-----|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | As. | WIDTH | Au. | Ag. | Cu. | Zn. | | |
| 0.00 - 4.00 | CASING | 4.00 | | | | | | | | | | | | | | | | | | |
| 4.00 - 8.03 | WASTE | 4.03 | | | | | | | | | | | | | | | | | | |
| 8.03 - 8.53 | 1087-G | 0.5 | 11 | .1 | | | 18 | | | | | | | | | | | | | |
| 8.53 - 8.83 | 1088-G | 0.3 | 14 | .3 | | | 27 | | | | | | | | | | | | | |
| 8.83 - 9.33 | 1089-G | 0.5 | 11 | .1 | | | 15 | | | | | | | | | | | | | |
| 9.33 - 9.83 | 1090-G | 0.5 | 8 | .2 | | | 13 | | | | | | | | | | | | | |
| 9.83 - 10.33 | 1091-G | 0.5 | 4 | .2 | | | 10 | | | | | | | | | | | | | |
| 10.33 - 10.63 | 1092-G | 0.3 | 7 | .1 | | | 7 | | | | | | | | | | | | | |
| 10.63 - 11.43 | 1093-G | 0.8 | 3 | .1 | | | 13 | | | | | | | | | | | | | |
| 11.43 - 11.73 | 1094-G | 0.3 | 16 | .1 | | | 16 | | | | | | | | | | | | | |
| 11.73 - 12.13 | 1095-G | 0.4 | 6 | .1 | | | 11 | | | | | | | | | | | | | |
| 12.13 - 12.43 | 1096-G | 0.3 | 6 | .2 | | | 23 | | | | | | | | | | | | | |
| 12.43 - 12.93 | 1097-G | 0.5 | 6 | .2 | | | 18 | | | | | | | | | | | | | |
| 12.93 - 13.07 | WASTE | 5.14 | | | | | | | | | | | | | | | | | | |
| 13.07 - 18.07 | 1098-G | 0.83 | 10 | .2 | | | 18 | | | | | | | | | | | | | |
| 18.07 - 18.90 | 1099-G | 0.5 | 6 | .1 | | | 11 | | | | | | | | | | | | | |
| 18.90 - 19.40 | 1100-G | 0.5 | 10 | .1 | | | 14 | | | | | | | | | | | | | |
| 19.40 - 19.90 | 1109-G | 0.6 | 4 | .1 | | | 15 | | | | | | | | | | | | | |
| 19.90 - 20.50 | 1112-G | 0.5 | 3 | .1 | | | 9 | | | | | | | | | | | | | |
| 20.50 - 21.00 | WASTE | 13.14 | | | | | | | | | | | | | | | | | | |
| 21.00 - 34.14 | WASTE | 13.14 | | | | | | | | | | | | | | | | | | |
| 34.14 - 34.64 | 1113-G | 0.5 | 5 | .1 | | | 23 | | | | | | | | | | | | | |
| 34.64 - 35.00 | WASTE | 0.36 | | | | | | | | | | | | | | | | | | |
| 35.00 - 35.50 | 1114-G | 0.5 | 4 | .2 | | | 23 | | | | | | | | | | | | | |
| 35.50 - 36.27 | WASTE | 0.77 | | | | | | | | | | | | | | | | | | |
| 36.27 - 36.77 | 1115-G | 0.5 | 6 | .1 | | | 18 | | | | | | | | | | | | | |
| 36.77 - 37.27 | WASTE | 0.5 | | | | | | | | | | | | | | | | | | |
| 37.27 - 37.57 | 1116-G | 0.3 | 5 | .2 | | | 19 | | | | | | | | | | | | | |
| 37.57 - 37.87 | 1117-G | 0.3 | 4 | .3 | | | 18 | | | | | | | | | | | | | |
| 37.87 - 38.37 | 1118-G | 0.5 | 8 | .1 | | | 11 | | | | | | | | | | | | | |
| 38.37 - 40.00 | WASTE | 1.63 | | | | | | | | | | | | | | | | | | |
| 40.00 - 40.40 | 1119-G | 0.4 | 5 | .2 | | | 32 | | | | | | | | | | | | | |
| 40.40 - 40.95 | 1120-G | 0.55 | 7 | .1 | | | 36 | | | | | | | | | | | | | |
| 40.95 - 41.50 | WASTE | 0.55 | | | | | | | | | | | | | | | | | | |
| 41.50 - 41.65 | 1121-G | 0.15 | 3 | .1 | | | 32 | | | | | | | | | | | | | |
| 41.65 - 45.30 | WASTE | 3.65 | | | | | | | | | | | | | | | | | | |
| 45.30 - 45.60 | 1122-G | 0.3 | 11 | .1 | | | 2 | | | | | | | | | | | | | |
| 45.60 - 45.90 | WASTE | 0.3 | | | | | | | | | | | | | | | | | | |
| 45.90 - 46.20 | 1123-G | 0.3 | 2 | .3 | | | 4 | | | | | | | | | | | | | |
| 46.20 - 47.10 | WASTE | 0.9 | | | | | | | | | | | | | | | | | | |
| 47.10 - 47.40 | 1124-G | 0.3 | 5 | .3 | | | 2 | | | | | | | | | | | | | |

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GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 6 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. ppb | Ag. ppm | Cu. | Zn. | As. ppm | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|------------|------------|-----|-----|------------|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | |
| 47.4 - 47.7 | 1125-G | 0.3 | 1 | .3 | | | 6 | | | | | | | | | | | | | |
| 47.7 - 50.7 | WASTE | 3.0 | | | | | | | | | | | | | | | | | | |
| 50.7 - 51.2 | 1126-G | 0.5 | 30 | .6 | | | 22 | | | | | | | | | | | | | |
| 51.2 - 51.5 | WASTE | 0.3 | | | | | | | | | | | | | | | | | | |
| 51.5 - 52.0 | 1127-G | 0.5 | 10 | 1.5 | | | 13 | | | | | | | | | | | | | |
| 52.0 - 53.5 | WASTE | 1.5 | | | | | | | | | | | | | | | | | | |
| 53.5 - 53.75 | 1128-G | 0.25 | 4 | .6 | | | 15 | | | | | | | | | | | | | |
| 53.75 - 54.05 | 1129-G | 0.3 | 104 | 1.2 | | | 227 | | | | | | | | | | | | | |
| 54.05 - 57.10 | WASTE | 3.05 | | | | | | | | | | | | | | | | | | |
| 57.10 - 57.60 | 1130-G | 0.5 | 6 | 1.7 | | | 7 | | | | | | | | | | | | | |
| 57.60 - 57.90 | 1131-G | 0.3 | 2 | 1.5 | | | 15 | | | | | | | | | | | | | |
| 57.90 - 58.40 | 1132-G | 0.5 | 1 | .3 | | | 4 | | | | | | | | | | | | | |
| 58.40 - 58.90 | 1133-G | 0.5 | 4 | .6 | | | 9 | | | | | | | | | | | | | |
| 58.90 - 59.50 | 1134-G | 0.6 | 12 | .3 | | | 13 | | | | | | | | | | | | | |
| 59.50 - 60.00 | 1135-G | 0.5 | 6 | .7 | | | 12 | | | | | | | | | | | | | |
| 60.00 - 60.50 | 1136-G | 0.5 | 4 | .8 | | | 3 | | | | | | | | | | | | | |
| 60.50 - 61.00 | 1137-G | 0.5 | 6 | .8 | | | 15 | | | | | | | | | | | | | |
| 61.00 - 61.50 | 1138-G | 0.5 | 8 | .7 | | | 9 | | | | | | | | | | | | | |
| 61.50 - 62.00 | 1139-G | 0.5 | 5 | .8 | | | 7 | | | | | | | | | | | | | |
| 62.00 - 62.40 | 1140-G | 0.4 | 6 | .4 | | | 3 | | | | | | | | | | | | | |
| 62.40 - 62.70 | 1101-G | 0.3 | 8 | 3.2 | | | 28 | | | | | | | | | | | | | |
| 62.70 - 63.00 | 1141-G | 0.3 | 4 | 1.4 | | | 4 | | | | | | | | | | | | | |
| 63.00 - 63.50 | 1142-G | 0.5 | 9 | 1.4 | | | 5 | | | | | | | | | | | | | |
| 63.50 - 64.00 | 1143-G | 0.5 | 1 | .9 | | | 15 | | | | | | | | | | | | | |
| 64.00 - 64.50 | 1144-G | 0.5 | 1 | .3 | | | 7 | | | | | | | | | | | | | |
| 64.50 - 65.00 | 1145-G | 0.5 | 9 | .7 | | | 15 | | | | | | | | | | | | | |
| 65.00 - 65.50 | 1146-G | 0.5 | 1 | .5 | | | 8 | | | | | | | | | | | | | |
| 65.50 - 66.00 | 1147-G | 0.5 | 2 | .7 | | | 38 | | | | | | | | | | | | | |
| 66.00 - 66.50 | 1148-G | 0.5 | 8 | .6 | | | 11 | | | | | | | | | | | | | |
| 66.50 - 67.00 | 1149-G | 0.5 | 12 | .4 | | | 7 | | | | | | | | | | | | | |
| 67.00 - 67.50 | 1150-G | 0.5 | 38 | .4 | | | 11 | | | | | | | | | | | | | |
| 67.50 - 68.00 | 1151-G | 0.5 | 109 | .7 | | | 31 | | | | | | | | | | | | | |
| 68.00 - 68.50 | 1152-G | 0.5 | 2 | .3 | | | 17 | | | | | | | | | | | | | |
| 68.50 - 69.00 | 1153-G | 0.5 | 1 | .5 | | | 15 | | | | | | | | | | | | | |
| 69.00 - 69.30 | 1154-G | 0.3 | 1 | .3 | | | 34 | | | | | | | | | | | | | |
| 69.30 - 69.70 | 1155-G | 0.4 | 2 | .3 | | | 16 | | | | | | | | | | | | | |
| 69.70 - 70.00 | 1156-G | 0.3 | 3 | 1.0 | | | 109 | | | | | | | | | | | | | |
| 70.00 - 70.40 | 1157-G | 0.4 | 3 | .8 | | | 64 | | | | | | | | | | | | | |
| 70.40 - 70.90 | 1158-G | 0.5 | 3 | .5 | | | 24 | | | | | | | | | | | | | |
| 70.90 - 71.40 | 1159-G | 0.5 | 8 | .2 | | | 19 | | | | | | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP6 Co ord. Horizontal Length Date Completed
Claim No. Core Size Drilled By
Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. | Ag | Cu | Zn. | As. | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|-----|-----|----|-----|-----|---------------|--|--|--|--|--|----------|--|--|--|-------|-----|-----|
| | | | | | | | | | | | | | | | | | | WIDTH | Au. | Ag. |
| 71.40 - 71.90 | 1160-G | 0.5 | 3 | .4 | | | 20 | | | | | | | | | | | | | |
| 71.90 - 72.20 | 1161-G | 0.3 | 2 | .4 | | | 23 | | | | | | | | | | | | | |
| 72.20 - 72.50 | 1162-G | 0.3 | 1 | .2 | | | 22 | | | | | | | | | | | | | |
| 72.50 - 73.00 | 1163-G | 0.5 | 5 | .6 | | | 42 | | | | | | | | | | | | | |
| 73.00 - 73.50 | 1164-G | 0.5 | 15 | .3 | | | 22 | | | | | | | | | | | | | |
| 73.50 - 74.00 | 1165-G | 0.5 | 1 | .1 | | | 13 | | | | | | | | | | | | | |
| 74.00 - 74.50 | 1166-G | 0.5 | 4 | .2 | | | 18 | | | | | | | | | | | | | |
| 74.50 - 75.00 | 1167-G | 0.5 | 7 | .4 | | | 18 | | | | | | | | | | | | | |
| 75.00 - 75.50 | 1168-G | 0.5 | 4 | .8 | | | 42 | | | | | | | | | | | | | |
| 75.50 - 76.00 | 1169-G | 0.5 | 3 | .3 | | | 7 | | | | | | | | | | | | | |
| 76.00 - 76.30 | 1170-G | 0.3 | 1 | .2 | | | 7 | | | | | | | | | | | | | |
| 76.30 - 76.60 | 1171-G | 0.3 | 2 | .2 | | | 21 | | | | | | | | | | | | | |
| 76.60 - 77.10 | 1172-G | 0.5 | 1 | .1 | | | 3 | | | | | | | | | | | | | |
| 77.10 - 77.50 | 1173-G | 0.4 | 2 | .6 | | | 7 | | | | | | | | | | | | | |
| 77.50 - 78.00 | 1174-G | 0.5 | 1 | .5 | | | 2 | | | | | | | | | | | | | |
| 78.00 - 78.50 | 1175-G | 0.5 | 2 | .6 | | | 5 | | | | | | | | | | | | | |
| 78.50 - 79.00 | 1176-G | 0.5 | 12 | .2 | | | 7 | | | | | | | | | | | | | |
| 79.00 - 79.50 | 1177-G | 0.5 | 3 | .5 | | | 5 | | | | | | | | | | | | | |
| 79.50 - 79.80 | 1178-G | 0.3 | 8 | .9 | | | 17 | | | | | | | | | | | | | |
| 79.80 - 80.10 | 1102-G | 0.3 | 11 | 1.4 | | | 28 | | | | | | | | | | | | | |
| 80.10 - 80.70 | 1179-G | 0.6 | 7 | .3 | | | 6 | | | | | | | | | | | | | |
| 80.70 - 81.38 | 1103-G | 0.68 | 6 | .7 | | | 19 | | | | | | | | | | | | | |
| 81.38 - 81.70 | 1180-G | 0.32 | 1 | .4 | | | 14 | | | | | | | | | | | | | |
| 81.70 - 82.20 | 1181-G | 0.5 | 1 | .1 | | | 2 | | | | | | | | | | | | | |
| 82.20 - 82.70 | 1182-G | 0.5 | 1 | .2 | | | 4 | | | | | | | | | | | | | |
| 82.70 - 83.20 | 1183-G | 0.5 | 1 | .2 | | | 8 | | | | | | | | | | | | | |
| 83.20 - 83.70 | 1184-G | 0.5 | 3 | .5 | | | 11 | | | | | | | | | | | | | |
| 83.70 - 84.20 | 1185-G | 0.5 | 2 | .3 | | | 8 | | | | | | | | | | | | | |
| 84.20 - 84.40 | 1186-G | 0.2 | 1 | .1 | | | 6 | | | | | | | | | | | | | |
| 84.40 - 84.70 | 1187-G | 0.3 | 1 | .1 | | | 5 | | | | | | | | | | | | | |
| 84.70 - 85.30 | 1188-G | 0.6 | 4 | .5 | | | 19 | | | | | | | | | | | | | |
| 85.30 - 85.80 | 1104-G | 0.5 | 9 | 1.2 | | | 23 | | | | | | | | | | | | | |
| 85.80 - 86.10 | 1189-G | 0.3 | 4 | .1 | | | 7 | | | | | | | | | | | | | |
| 86.10 - 86.40 | 1190-G | 0.3 | 1 | .2 | | | 11 | | | | | | | | | | | | | |
| 86.40 - 86.70 | 1191-G | 0.3 | 7 | .4 | | | 7 | | | | | | | | | | | | | |
| 86.70 - 87.10 | 1192-G | 0.4 | 3 | .5 | | | 13 | | | | | | | | | | | | | |
| 87.10 - 87.40 | 1193-G | 0.3 | 1 | .2 | | | 12 | | | | | | | | | | | | | |
| 87.40 - 87.75 | 1194-G | 0.35 | 3 | .1 | | | 3 | | | | | | | | | | | | | |
| 87.75 - 91.10 | WASTE | 3.35 | | | | | | | | | | | | | | | | | | |
| 91.10 - 91.60 | 1195-G | 0.5 | 1 | .3 | | | 10 | | | | | | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP6 Co ord. _____ Horizontal Length _____ Date Completed _____
Claim No. _____ Core Size _____ Drilled By _____
Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. | Ag. | Cu. | Zn. | As. | WIDTH X ASSAY | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|-----|-----|-----|-----|-----|---------------|--|--|--|--|----------|-----|-----|-----|-----|--|--|
| | | | | | | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | |
| 91.60 - 91.90 | 1196-G | 0.3 | 9 | .1 | | | 9 | | | | | | | | | | | | |
| 91.90 - 92.40 | 1197-G | 0.5 | 12 | .4 | | | 2 | | | | | | | | | | | | |
| 92.40 - 92.90 | 1198-G | 0.5 | 15 | .1 | | | 2 | | | | | | | | | | | | |
| 92.90 - 93.40 | 1199-G | 0.5 | 7 | .1 | | | 4 | | | | | | | | | | | | |
| 93.40 - 93.70 | 1200-G | 0.3 | 6 | .1 | | | 5 | | | | | | | | | | | | |
| 93.70 - 94.10 | 1201-G | 0.4 | 12 | .4 | | | 18 | | | | | | | | | | | | |
| 94.10 - 94.60 | 1202-G | 0.5 | 3 | .1 | | | 3 | | | | | | | | | | | | |
| 94.60 - 95.10 | 1203-G | 0.5 | 3 | .2 | | | 3 | | | | | | | | | | | | |
| 95.10 - 95.60 | 1204-G | 0.5 | 1 | .1 | | | 3 | | | | | | | | | | | | |
| 95.60 - 96.65 | WASTE | 1.05 | | | | | | | | | | | | | | | | | |
| 96.65 - 97.15 | 1205-G | 0.5 | 1 | .4 | | | 6 | | | | | | | | | | | | |
| 97.15 - 97.45 | 1206-G | 0.3 | 30 | .3 | | | 27 | | | | | | | | | | | | |
| 97.45 - 97.95 | 1207-G | 0.5 | 3 | .4 | | | 8 | | | | | | | | | | | | |
| 97.95 - 101.60 | WASTE | 3.65 | | | | | | | | | | | | | | | | | |
| 101.60 - 102.10 | 1208-G | 0.5 | 4 | .2 | | | 2 | | | | | | | | | | | | |
| 102.10 - 102.60 | 1209-G | 0.5 | 9 | .3 | | | 8 | | | | | | | | | | | | |
| 102.60 - 103.10 | 1210-G | 0.5 | 10 | .5 | | | 30 | | | | | | | | | | | | |
| 103.10 - 103.50 | 1211-G | 0.4 | 1 | .3 | | | 2 | | | | | | | | | | | | |
| 103.50 - 107.60 | WASTE | 4.1 | | | | | | | | | | | | | | | | | |
| 107.60 - 107.90 | 1212-G | 0.3 | 14 | .7 | | | 16 | | | | | | | | | | | | |
| 107.90 - 108.20 | 1213-G | 0.3 | 2 | .1 | | | 2 | | | | | | | | | | | | |
| 108.20 - 109.00 | 1214-G | 0.8 | 2 | .4 | | | 4 | | | | | | | | | | | | |
| 109.00 - 109.50 | 1215-G | 0.5 | 11 | .4 | | | 16 | | | | | | | | | | | | |
| 109.50 - 110.00 | 1216-G | 0.5 | 4 | .6 | | | 10 | | | | | | | | | | | | |
| 110.00 - 110.50 | 1217-G | 0.5 | 7 | .5 | | | 5 | | | | | | | | | | | | |
| 110.50 - 110.80 | 1218-G | 0.3 | 4 | .3 | | | 4 | | | | | | | | | | | | |
| 110.80 - 111.30 | 1106-G | 0.5 | 8 | .5 | | | 13 | | | | | | | | | | | | |
| 111.30 - 111.60 | 1219-G | 0.3 | 14 | .6 | | | 7 | | | | | | | | | | | | |
| 111.60 - 112.10 | 1220-G | 0.5 | 49 | .4 | | | 97 | | | | | | | | | | | | |
| 112.10 - 112.60 | 1221-G | 0.5 | 4 | .6 | | | 4 | | | | | | | | | | | | |
| 112.60 - 113.10 | 1222-G | 0.5 | 34 | .6 | | | 58 | | | | | | | | | | | | |
| 113.10 - 113.45 | 1107-G | 0.35 | 52 | .4 | | | 112 | | | | | | | | | | | | |
| 113.45 - 113.75 | 1223-G | 0.3 | 3 | .5 | | | 7 | | | | | | | | | | | | |
| 113.75 - 114.10 | 1108-G | 0.35 | 94 | .4 | | | 251 | | | | | | | | | | | | |
| 114.10 - 114.60 | 1224-G | 0.5 | 1 | .5 | | | 5 | | | | | | | | | | | | |
| 114.60 - 116.40 | WASTE | 1.8 | | | | | | | | | | | | | | | | | |
| 116.40 - 116.70 | 1225-G | 0.3 | 18 | .7 | | | 13 | | | | | | | | | | | | |
| 116.70 - 117.00 | 1226-G | 0.3 | 41 | 1.6 | | | 73 | | | | | | | | | | | | |
| 117.00 - 117.30 | 1227-G | 0.3 | 44 | .5 | | | 87 | | | | | | | | | | | | |
| 117.30 - 123.20 | WASTE | 5.9 | | | | | | | | | | | | | | | | | |

Use Black Pen Only


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 6 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. | Ag. | Cu. | Zn. | As. | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|-----|-----|-----|-----|-----|---------------|--|--|--|--|--|----------|-----|-----|-----|-----|--|--|
| | | | | | | | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | |
| 123.20 - 123.70 | 1228-G | 0.5 | 23 | 1.8 | | | 41 | | | | | | | | | | | | | |
| 123.70 - 124.10 | 1229-G | 0.4 | 40 | 1.2 | | | 34 | | | | | | | | | | | | | |
| 124.10 - 124.60 | 1230-G | 0.5 | 4 | 2.0 | | | 3 | | | | | | | | | | | | | |
| 124.60 - 124.90 | 1231-G | 0.3 | 23 | 1.7 | | | 7 | | | | | | | | | | | | | |
| 124.90 - 125.20 | 1232-G | 0.3 | 10 | 2.4 | | | 14 | | | | | | | | | | | | | |
| 125.20 - 125.70 | 1233-G | 0.5 | 11 | 1.5 | | | 50 | | | | | | | | | | | | | |
| 125.70 - 126.20 | 1234-G | 0.5 | 5 | 1.3 | | | 26 | | | | | | | | | | | | | |
| 126.20 - 126.70 | 1235-G | 0.5 | 6 | 1.2 | | | 85 | | | | | | | | | | | | | |
| 126.70 - 127.20 | 1236-G | 0.5 | 11 | .5 | | | 265 | | | | | | | | | | | | | |
| 127.20 - 127.70 | 1237-G | 0.5 | 5 | .8 | | | 28 | | | | | | | | | | | | | |
| 127.70 - 128.20 | 1238-G | 0.5 | 4 | .7 | | | 23 | | | | | | | | | | | | | |
| 128.20 - 128.70 | 1239-G | 0.5 | 1 | .4 | | | 17 | | | | | | | | | | | | | |
| 128.70 - 129.80 | 1240-G | 1.1 | 6 | .5 | | | 14 | | | | | | | | | | | | | |
| 129.80 - 130.30 | 1241-G | 0.5 | 9 | 1.5 | | | 17 | | | | | | | | | | | | | |
| 130.30 - 130.80 | 1242-G | 0.5 | 17 | 1.0 | | | 9 | | | | | | | | | | | | | |
| 130.80 - 131.30 | 1243-G | 0.5 | 4 | .6 | | | 25 | | | | | | | | | | | | | |
| 131.30 - 131.80 | 1244-G | 0.5 | 3 | .6 | | | 25 | | | | | | | | | | | | | |
| 131.80 - 132.30 | 1245-G | 0.5 | 2 | .3 | | | 28 | | | | | | | | | | | | | |
| 132.30 - 132.80 | 1246-G | 0.5 | 3 | .9 | | | 44 | | | | | | | | | | | | | |
| 132.80 - 133.30 | 1247-G | 0.5 | 4 | .9 | | | 36 | | | | | | | | | | | | | |
| 133.30 - 133.80 | 1248-G | 0.5 | 1 | 1.6 | | | 21 | | | | | | | | | | | | | |
| 133.80 - 134.30 | 1249-G | 0.5 | 1 | 1.7 | | | 11 | | | | | | | | | | | | | |
| 134.30 - 134.80 | 1250-G | 0.5 | 2 | 2.0 | | | 3 | | | | | | | | | | | | | |
| 134.80 - 135.30 | 1251-G | 0.5 | 22 | 1.8 | | | 58 | | | | | | | | | | | | | |
| 135.30 - 135.80 | 1252-G | 0.5 | 37 | 1.1 | | | 88 | | | | | | | | | | | | | |
| 135.80 - 136.30 | 1253-G | 0.5 | 3 | 1.2 | | | 22 | | | | | | | | | | | | | |
| 136.30 - 136.80 | 1254-G | 0.5 | 16 | 2.2 | | | 123 | | | | | | | | | | | | | |
| 136.80 - 137.30 | 1255-G | 0.5 | 20 | 1.9 | | | 96 | | | | | | | | | | | | | |
| 137.30 - 137.80 | 1256-G | 0.5 | 49 | 2.3 | | | 147 | | | | | | | | | | | | | |
| 137.80 - 138.30 | 1257-G | 0.5 | 1 | 1.4 | | | 48 | | | | | | | | | | | | | |
| 138.30 - 138.80 | 1258-G | 0.5 | 14 | .8 | | | 54 | | | | | | | | | | | | | |
| 138.80 - 139.30 | 1259-G | 0.5 | 47 | 2.7 | | | 103 | | | | | | | | | | | | | |
| 139.30 - 139.80 | 1260-G | 0.5 | 5 | .7 | | | 41 | | | | | | | | | | | | | |
| 139.80 - 140.30 | 1261-G | 0.5 | 7 | .7 | | | 62 | | | | | | | | | | | | | |
| 140.30 - 143.20 | WASTE | 2.9 | | | | | | | | | | | | | | | | | | |
| 143.20 - 143.70 | 1262-G | 0.5 | 8 | .6 | | | 49 | | | | | | | | | | | | | |
| 143.70 - 144.20 | 1263-G | 0.5 | 3 | 1.1 | | | 38 | | | | | | | | | | | | | |
| 144.20 - 144.70 | 1264-G | 0.5 | 2 | .4 | | | 43 | | | | | | | | | | | | | |
| 144.70 - 145.20 | 1265-G | 0.5 | 4 | .5 | | | 34 | | | | | | | | | | | | | |
| 145.20 - 145.70 | 1266-G | 0.5 | 2 | .4 | | | 31 | | | | | | | | | | | | | |



GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 6 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au | Ag | Cu | Zn | As | WIDTH X ASSAY | | | | | | | | AVERAGES | | | | | | | |
|---------------------------|--------|-------|----|-----|----|----|----|---------------|----|----|----|----|----|-------|----|----------|----|----|----|--|--|--|--|
| | | | | | | | | WIDTH | Au | Ag | Cu | Zn | As | WIDTH | Au | Ag | Cu | Zn | As | | | | |
| 145.70-145.90 | WASTE | 0.2 | | | | | | | | | | | | | | | | | | | | | |
| 145.90-146.40 | 1110-G | 0.5 | 2 | .4 | | | 36 | | | | | | | | | | | | | | | | |
| 146.40-146.90 | 1111-G | 0.5 | 3 | .6 | | | 40 | | | | | | | | | | | | | | | | |
| 146.90-147.40 | 1267-G | 0.5 | 2 | .1 | | | 34 | | | | | | | | | | | | | | | | |
| 147.40-147.90 | WASTE | 0.5 | | | | | | | | | | | | | | | | | | | | | |
| 147.90-148.40 | 1268-G | 0.5 | 4 | .5 | | | 49 | | | | | | | | | | | | | | | | |
| 148.40-150.50 | WASTE | 2.1 | | | | | | | | | | | | | | | | | | | | | |
| 150.50-151.00 | 1269-G | 0.5 | 1 | .2 | | | 29 | | | | | | | | | | | | | | | | |
| 151.00-151.50 | 1270-G | 0.5 | 3 | .5 | | | 38 | | | | | | | | | | | | | | | | |
| 151.50-152.00 | 1271-G | 0.5 | 2 | .2 | | | 38 | | | | | | | | | | | | | | | | |
| 152.00-156.40 | WASTE | 4.4 | | | | | | | | | | | | | | | | | | | | | |
| 156.40-156.90 | 1272-G | 0.5 | 11 | .6 | | | 14 | | | | | | | | | | | | | | | | |
| 156.90-157.40 | 1273-G | 0.5 | 14 | .5 | | | 18 | | | | | | | | | | | | | | | | |
| 157.40-161.90 | WASTE | 4.5 | | | | | | | | | | | | | | | | | | | | | |
| 161.90-162.40 | 1274-G | 0.5 | 10 | .4 | | | 32 | | | | | | | | | | | | | | | | |
| 162.40-162.90 | 1275-G | 0.5 | 7 | .1 | | | 17 | | | | | | | | | | | | | | | | |
| 162.90-163.40 | 1276-G | 0.5 | 3 | .1 | | | 12 | | | | | | | | | | | | | | | | |
| 163.40-166.10 | WASTE | 2.7 | | | | | | | | | | | | | | | | | | | | | |
| 166.10-166.60 | 1277-G | 0.5 | 69 | .1 | | | 24 | | | | | | | | | | | | | | | | |
| 166.60-167.10 | 1278-G | 0.5 | 4 | .2 | | | 20 | | | | | | | | | | | | | | | | |
| 167.10-173.90 | WASTE | 6.8 | | | | | | | | | | | | | | | | | | | | | |
| 173.90-174.40 | 1279-G | 0.5 | 17 | .1 | | | 25 | | | | | | | | | | | | | | | | |
| 174.40-179.25 | WASTE | 4.85 | | | | | | | | | | | | | | | | | | | | | |
| 179.25-179.75 | 1280-G | 0.5 | 13 | 1.0 | | | 21 | | | | | | | | | | | | | | | | |
| 179.75-180.25 | 1281-G | 0.5 | 16 | 1.1 | | | 23 | | | | | | | | | | | | | | | | |
| 180.25-180.75 | 1282-G | 0.5 | 6 | .6 | | | 19 | | | | | | | | | | | | | | | | |
| 180.75-181.25 | 1283-G | 0.5 | 8 | .9 | | | 13 | | | | | | | | | | | | | | | | |
| 181.25-186.85 | WASTE | 5.6 | | | | | | | | | | | | | | | | | | | | | |
| 186.85-187.35 | 1284-G | 0.5 | 17 | 2.1 | | | 50 | | | | | | | | | | | | | | | | |
| 187.35-187.85 | 1285-G | 0.5 | 17 | 1.7 | | | 49 | | | | | | | | | | | | | | | | |
| 187.85-190.70 | WASTE | 2.85 | | | | | | | | | | | | | | | | | | | | | |
| 190.70-191.20 | 1286-G | 0.5 | 9 | 1.3 | | | 30 | | | | | | | | | | | | | | | | |
| 191.20-197.50 | WASTE | 6.3 | | | | | | | | | | | | | | | | | | | | | |
| 197.50-198.10 | 1287-G | 0.6 | 26 | 3.5 | | | 28 | | | | | | | | | | | | | | | | |
| 198.10-199.00 | 1288-G | 0.9 | 18 | 2.7 | | | 28 | | | | | | | | | | | | | | | | |
| 199.00-199.45 | WASTE | 0.45 | | | | | | | | | | | | | | | | | | | | | |
| 199.45-199.95 | 1289-G | 0.5 | 11 | 1.8 | | | 27 | | | | | | | | | | | | | | | | |
| 199.95-200.45 | 1290-G | 0.5 | 27 | 4.4 | | | 56 | | | | | | | | | | | | | | | | |
| 200.45-207.10 | WASTE | 6.65 | | | | | | | | | | | | | | | | | | | | | |
| 207.10-207.60 | 1291-G | 0.5 | 5 | .8 | | | 13 | | | | | | | | | | | | | | | | |

Use Black Pen Only



GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP6 Coord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | NUMBER | WIDTH | Au. | Ag. | Cu. | Zn. | As. | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | | | | | | |
|---------------------------|--------|-------|-----|-----|-----|-----|-----|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|--|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | | | | | | |
| 207.60 - 222.90 | WASTE | 15.3 | | | | | | | | | | | | | | | | | | | | | | | |
| 222.90 - 223.40 | 1292-G | 0.5 | 3 | .1 | | | 28 | | | | | | | | | | | | | | | | | | |
| 223.40 - 227.50 | WASTE | 4.1 | | | | | | | | | | | | | | | | | | | | | | | |
| 227.50 - 228.00 | 1293-G | 0.5 | 5 | .1 | | | 27 | | | | | | | | | | | | | | | | | | |
| 228.00 - 234.60 | WASTE | 6.6 | | | | | | | | | | | | | | | | | | | | | | | |
| 234.60 - 235.10 | 1294-G | 0.5 | 6 | .4 | | | 39 | | | | | | | | | | | | | | | | | | |
| 235.10 - 235.60 | 1295-G | 0.5 | 6 | .1 | | | 19 | | | | | | | | | | | | | | | | | | |
| 235.60 - 236.80 | WASTE | 1.2 | | | | | | | | | | | | | | | | | | | | | | | |
| 236.80 - 237.30 | 1296-G | 0.5 | 6 | .1 | | | 43 | | | | | | | | | | | | | | | | | | |
| 237.30 - 237.80 | 1297-G | 0.5 | 17 | .3 | | | 33 | | | | | | | | | | | | | | | | | | |
| 237.80 - 240.60 | WASTE | 2.8 | | | | | | | | | | | | | | | | | | | | | | | |
| 240.60 - 241.10 | 1298-G | 0.5 | 1 | .1 | | | 8 | | | | | | | | | | | | | | | | | | |
| 241.10 - 241.60 | 1299-G | 0.5 | 7 | .1 | | | 33 | | | | | | | | | | | | | | | | | | |
| 241.60 - 242.10 | 1300-G | 0.5 | 21 | .1 | | | 22 | | | | | | | | | | | | | | | | | | |
| 242.10 - 242.60 | 1301-G | 0.5 | 5 | .1 | | | 2 | | | | | | | | | | | | | | | | | | |
| 242.60 - 242.90 | 1302-G | 0.3 | 2 | .1 | | | 2 | | | | | | | | | | | | | | | | | | |
| 242.90 - 243.40 | 1303-G | 0.5 | 9 | .1 | | | 3 | | | | | | | | | | | | | | | | | | |
| 243.40 - 243.90 | 1304-G | 0.5 | 1 | .4 | | | 2 | | | | | | | | | | | | | | | | | | |
| 243.90 - 244.40 | 1305-G | 0.5 | 1 | .1 | | | 2 | | | | | | | | | | | | | | | | | | |
| 244.40 - 244.90 | 1306-G | 0.5 | 1 | .1 | | | 2 | | | | | | | | | | | | | | | | | | |
| 244.90 - 245.40 | 1307-G | 0.5 | 1 | .2 | | | 5 | | | | | | | | | | | | | | | | | | |
| 245.40 - 245.90 | 1308-G | 0.5 | 2 | .1 | | | 8 | | | | | | | | | | | | | | | | | | |
| 245.90 - 246.40 | 1309-G | 0.5 | 1 | .3 | | | 6 | | | | | | | | | | | | | | | | | | |
| 246.40 - 246.90 | 1310-G | 0.5 | 6 | .2 | | | 14 | | | | | | | | | | | | | | | | | | |
| 246.90 - 247.40 | 1311-G | 0.5 | 1 | .1 | | | 6 | | | | | | | | | | | | | | | | | | |
| 247.40 - 247.90 | 1312-G | 0.5 | 1 | .1 | | | 3 | | | | | | | | | | | | | | | | | | |
| 247.90 - 248.40 | 1313-G | 0.5 | 2 | .1 | | | 4 | | | | | | | | | | | | | | | | | | |
| 248.40 - 248.70 | 1314-G | 0.3 | 53 | 1.1 | | | 86 | | | | | | | | | | | | | | | | | | |
| 248.70 - 249.20 | 1315-G | 0.5 | 150 | 2.6 | | | 267 | | | | | | | | | | | | | | | | | | |
| 249.20 - 249.70 | 1316-G | 0.5 | 39 | 2.8 | | | 65 | | | | | | | | | | | | | | | | | | |
| 249.70 - 250.20 | 1317-G | 0.5 | 73 | 6.7 | | | 86 | | | | | | | | | | | | | | | | | | |
| 250.20 - 250.70 | 1318-G | 0.5 | 78 | 5.2 | | | 127 | | | | | | | | | | | | | | | | | | |
| 250.70 - 251.20 | 1319-G | 0.5 | 77 | 5.4 | | | 120 | | | | | | | | | | | | | | | | | | |
| 251.20 - 251.70 | 1320-G | 0.5 | 90 | 3.6 | | | 133 | | | | | | | | | | | | | | | | | | |
| 251.70 - 252.20 | 1321-G | 0.5 | 33 | 1.6 | | | 36 | | | | | | | | | | | | | | | | | | |
| 252.20 - 252.70 | 1322-G | 0.5 | 11 | 1.4 | | | 26 | | | | | | | | | | | | | | | | | | |
| 252.70 - 253.20 | 1323-G | 0.5 | 21 | 1.7 | | | 28 | | | | | | | | | | | | | | | | | | |
| 253.20 - 258.50 | WASTE | 5.3 | | | | | | | | | | | | | | | | | | | | | | | |
| 258.50 - 259.00 | 1324-G | 0.5 | 1 | .1 | | | 20 | | | | | | | | | | | | | | | | | | |
| 259.00 - 259.50 | 1325-G | 0.5 | 2 | .1 | | | 18 | | | | | | | | | | | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

 Hole No. AP 6 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. | Ag. | Cu. | Zn. | As. | WIDTH X ASSAY | | | | | AVERAGES | | | | | | | |
|---------------------------|--------|-------|-----|-----|-----|-----|-----|---------------|-----|-----|-----|-----|----------|--|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | |
| 259.50 - 263.60 | WASTE | 4.1 | | | | | | | | | | | | | | | | | | |
| 263.60 - 264.10 | 1326-G | 0.5 | 2 | .3 | | | 12 | | | | | | | | | | | | | |
| 264.10 - 264.60 | 1327-G | 0.5 | 1 | .1 | | | 17 | | | | | | | | | | | | | |
| 264.60 - 265.10 | 1328-G | 0.5 | 4 | .3 | | | 20 | | | | | | | | | | | | | |
| 265.10 - 268.50 | WASTE | 3.4 | | | | | | | | | | | | | | | | | | |
| 268.50 - 269.00 | 1329-G | 0.5 | 1 | .1 | | | 8 | | | | | | | | | | | | | |
| 269.00 - 269.50 | 1330-G | 0.5 | 1 | .1 | | | 8 | | | | | | | | | | | | | |
| 269.50 - 280.00 | WASTE | 10.50 | | | | | | | | | | | | | | | | | | |
| 280.00 - 280.50 | 1331-G | 0.5 | 3 | .1 | | | 9 | | | | | | | | | | | | | |
| 280.50 - 281.00 | 1332-G | 0.5 | 1 | .1 | | | 7 | | | | | | | | | | | | | |
| 281.00 - 281.50 | 1333-G | 0.5 | 5 | .1 | | | 8 | | | | | | | | | | | | | |
| 281.50 - 282.00 | 1334-G | 0.5 | 2 | .2 | | | 9 | | | | | | | | | | | | | |
| 282.00 - 282.50 | 1335-G | 0.5 | 2 | .1 | | | 5 | | | | | | | | | | | | | |
| 282.50 - 283.00 | 1336-G | 0.5 | 1 | .1 | | | 3 | | | | | | | | | | | | | |
| 283.00 - 283.50 | 1337-G | 0.5 | 1 | .1 | | | 6 | | | | | | | | | | | | | |
| 283.50 - 284.00 | 1338-G | 0.5 | 13 | .1 | | | 5 | | | | | | | | | | | | | |
| 284.00 - 284.50 | 1339-G | 0.5 | 2 | .1 | | | 2 | | | | | | | | | | | | | |
| 284.50 - 285.00 | 1340-G | 0.5 | 3 | .3 | | | 15 | | | | | | | | | | | | | |
| 285.00 - 285.50 | 1341-G | 0.5 | 5 | .3 | | | 42 | | | | | | | | | | | | | |
| 285.50 - 286.00 | 1342-G | 0.5 | 7 | .6 | | | 41 | | | | | | | | | | | | | |
| 286.00 - 286.50 | 1343-G | 0.5 | 3 | .1 | | | 5 | | | | | | | | | | | | | |
| 286.50 - 287.00 | 1344-G | 0.5 | 1 | .3 | | | 11 | | | | | | | | | | | | | |
| 287.00 - 287.50 | 1345-G | 0.5 | 1 | .1 | | | 2 | | | | | | | | | | | | | |
| 287.50 - 288.00 | 1346-G | 0.5 | 1 | .1 | | | 10 | | | | | | | | | | | | | |
| 288.00 - 288.50 | 1347-G | 0.5 | 1 | .2 | | | 11 | | | | | | | | | | | | | |
| 288.50 - 289.00 | 1348-G | 0.5 | 13 | .6 | | | 73 | | | | | | | | | | | | | |
| 289.00 - 289.50 | 1349-G | 0.5 | 7 | .6 | | | 36 | | | | | | | | | | | | | |
| 289.50 - 290.00 | 1350-G | 0.5 | 17 | .2 | | | 10 | | | | | | | | | | | | | |
| 290.00 - 290.50 | 1351-G | 0.5 | 5 | .3 | | | 32 | | | | | | | | | | | | | |
| 290.50 - 291.00 | 1352-G | 0.5 | 2 | .2 | | | 9 | | | | | | | | | | | | | |
| 291.00 - 291.50 | 1353-G | 0.5 | 2 | .3 | | | 13 | | | | | | | | | | | | | |
| 291.50 - 292.00 | 1354-G | 0.5 | 2 | .3 | | | 9 | | | | | | | | | | | | | |
| 292.00 - 292.50 | 1355-G | 0.5 | 2 | .1 | | | 12 | | | | | | | | | | | | | |
| 292.50 - 293.00 | 1356-G | 0.5 | 1 | .1 | | | 6 | | | | | | | | | | | | | |
| 293.00 - 293.50 | 1357-G | 0.5 | 94 | .3 | | | 7 | | | | | | | | | | | | | |
| 293.50 - 294.50 | 1358-G | 1.0 | 5 | .3 | | | 21 | | | | | | | | | | | | | |
| 294.50 - 295.00 | 1359-G | 0.5 | 2 | .5 | | | 27 | | | | | | | | | | | | | |
| 295.00 - 295.50 | 1360-G | 0.5 | 4 | .1 | | | 15 | | | | | | | | | | | | | |
| 295.50 - 296.00 | 1361-G | 0.5 | 2 | .3 | | | 13 | | | | | | | | | | | | | |
| 296.00 - 296.50 | 1362-G | 0.5 | 2 | .2 | | | 15 | | | | | | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

1 of 8

Property Unuk River Option Project No. 134 Depth 197.21 m Date Began Aug. 20/90
 Hole No. A.P. 7 Co. ord. 738N/195W Horizontal Length 148 m Date Completed Aug. 22/90
 Claim No. UNUK 26 Core Size BG - BDM Drilled By J.T. Thomas
 Grid No. Zone 1 Angle & Direction 45° az 314 Elevation 1260 m Logged By D. Gaborury

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 0 - 7.62 | Casing | | | | | | | | |
| 7.62 - 61.10 | Fine Grained Andesitic Tuff / tuffaceous wacke - medium bluish grey (5B 5/1) - foliated, locally weakly banded - fine feldspar and mafic phenocrysts - minor limonite - weathered fracture down to 15.20 meters - Tr - 1% fine white carb. veinlets | | | | | | | | |
| 19.20 - 19.50 | : Sheared graphitic argillite section 1-2% py stringers, sub-parallel to C.A. | | | | | | | | |
| 20.42 - 21.95 | : very fine, weakly silicified altered tuff, greenish grey (5G 6/1) with weak laminations 1-3% py in stringers trending ~38° to C.A., with r-cutting, offsetting Qtz-carb. streak veins. | | | | | | | | |
| 23.78 - 24.38 | : Strongly fractured section thin calcite fracture coatings, 1-2 cm fracture spacing. | | | | | | | | |
| 24.38 - 27.40 | : 2-10 cm Qtz-carb.-chlorite veins at 80° to 90° to C.A., 5-10 cm apart. | | | | | | | | |
| 34.45 - 34.65 | : graphitic shear, with parallel Qtz-carb vein and perpendicular tension veinlets - shear at 30° to C.A. | | | | | | | | |
| 34.65 - 36.50 | : minor Qtz-carb. stringers, 2-3% py stringers & blebs | | | | | | | | |
| 43.15 - 43.35 | : sharply defined fine ash tuff bed, greenish grey, with weak sericite alteration. | | | | | | | | |

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

20,390

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

2 of 8

Hole No Co ord Horizontal Length Date Completed
 Claim No Core Size Drilled By
 Grid No Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 43.30 - 43.50 | : greenish grey fine ash tuff | | | | | | | | |
| 44.10 - 46.26 | : tuff becomes slightly argillaceous and graphitic, with rehealed brecciation, fracturing. | | | | | | | | |
| 46.70 - 46.80 | : shear zone, graphitic silvery core, 50% Qtz-carb. infilling of breccia, Tr-1% py | | | | | | | | |
| 47.40 - 49.60 | : Strongly fractured fault zone. Fractures at low core angles (5-10° to C.A.) with slickensides striking ~ 10° from horizontal. ~50% Qtz-carb stringers units, Tr-1% py. | | | | | | | | |
| 50.80 - 51.10 | : irregular Qtz-carb. stringers + veins, in brecciated shear zone, with minor chlorite and graphite. | | | | | | | | |
| 51.70 - 53.70 | : Argillaceous tuff section with irregular carb stringers at low core angles, 1-2% stringers of py. | | | | | | | | |
| 53.70 - 56.10 | : Shear zone, brecciated, re-silicified, numerous graphitic/talc gouge seams and silvery, broken core, minor Qtz-carb veining, locally strongly foliated friable 1-2% diss. py. | | | | | | | | |
| 56.10 - 60.90 | : moderately sericitized, fine grained andesitic tuff, with 40% med. grained chloritic clots, minor irregular Qtz-chlorite veins. | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

30f-8

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | - locally brecciated and Qtz-carb. healed, with 2-3% diss. py ~ 20% core Recovery | | | | | | | | |
| 61.10 - 66.10 | Argillaceous debris flow - tuffaceous with coarse feldspathic fragments, and argillite/siltstone interbeds - minor Qtz-carb-chlorite veinlets at varying core angles - numerous graphite slip surfaces, - overall 2-3% fine diss. py 61.10 - 61.60 : shear zone, highly fractured, graphitic argillite | | | | | | | | |
| 66.10 - 75.28 | Fine Andesitic Tuff - dark greenish grey weakly chloritic and sericitic with 3-5% Qtz-carb. veinlets and breccia in filling - weakly foliated, minor intercalated flows, 66.10 - 67.50 : brecciated, silicified, greenish grey sericite alt., 1-2% py blebs & stringers. * 70.00 - 72.00 : amygdaloidal andesite flow silicified, Qtz-carb. amygdules with 5-10% py stringers | | | | | | | | |

40/8

Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 75.28 - 78.40 | Interbedded Argillite / Argillaceous Andesite Tuff - fine ash to lapilli size fragments in tuffaceous interbeds - minor Qtz-carb. stringers at varying core angles - Tr-py stringers & bands, minor py fragments bedding at 60° to core axis at 63.80m. | | | | | | | | |
| 78.40 - 91.00 | Dacitic Lapilli - Ash tuff - matrix supported, angular fragments - medium bluish grey and greenish grey frags. in light bluish grey matrix - 45% pyritic fragments, with altered rims - gradational upper contact | | | | | | | | |
| * 85.80 - 86.50 | : Gradual increase in silicification and sericitization, 5-10% py blebs and stringers | | | | | | | | |
| * 86.50 - 88.00 | : Strong carb. & sericite alt'n, yellowish grey carb. matrix and a 1-2cm irregular carb.-py vein, sub-parallel to core axis, with 10-15% py, 1-2% arsenopyrite | | | | | | | | |
| * 88.00 - 91.00 | : Strongly sericite-altered fragments in siltified matrix - Qtz-carb. veinlets at 60°-90° to core axis - 5-8% py stringers and blebs | | | | | | | | |

5 of 8

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | | | | | | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|--|--|--|--|--|--|--|--|--|--|--|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. | | | | | | | | | | | |
| 91.00 - 96.50 | Argillite massive, locally brecciated, with cross-cutting carb. - Qtz stringers at varying core angles, largely $> 60^\circ$ | | | | | | | | | | | | | | | | | | | |
| | 91.50 - 92.30 : fault zone; broken core to gauge | | | | | | | | | | | | | | | | | | | |
| * | 92.30 - 94.40 : Qtz - carb - py vein strongly brecciated and reworked. - graphitic argillite frags, and cross-cutting Qtz stalk units. - 5-10% py blebs / stringers | | | | | | | | | | | | | | | | | | | |
| | 94.40 - 95.50 : Fault zone; sandy-graphitic gouge, brecciated, strong Qtz - carb. stalk, minor talc. | | | | | | | | | | | | | | | | | | | |
| | 96.20 - 96.50 : laminated tuffaceous argillite; fine grained, light greenish grey, weakly brecciated and sericitized | | | | | | | | | | | | | | | | | | | |
| | Core Angles: Foliation: 90.3 m. 45° | | | | | | | | | | | | | | | | | | | |
| 96.50 - 113.50 | Argillaceous volcanic debris flow - weak to non-foliated, argillaceous matrix with ~40% dacitic fragments, minor pyrites and argillite fragments - numerous tuffaceous interbeds, - overall 1-2% diss. py, and stringers | | | | | | | | | | | | | | | | | | | |
| | 98.50 - 101.00 : silicified tuff section, 3-5% py stringers | | | | | | | | | | | | | | | | | | | |

Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

608

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 113.50 - 127.25 | <p>Oacitic lapilli tuff</p> <ul style="list-style-type: none"> - Matrix supported, Dark bluish grey, with light grey to black fragments, up to 2 cm across. - minor cross-cutting carb. - Qtz veinlets at low core angles (30°-45°) - overall 1-2% py blebs & stringers <p>119.20 - 120.40 : Fine grained altered andesitic section, light greenish grey, weakly sericitized</p> <p>124.00 - 124.40 : Fault zone, strongly fractured, with slickensides raking at steep core angles</p> | | | | | | | | |
| 127.25 - 171.90 | <p>Argillite</p> <ul style="list-style-type: none"> - massive, with minor siltstone interbeds, minor cross-cutting carb. stringers and diffuse pyrite bands. - overall 1% py. - minor tuffaceous sections <p>133.50 - 135.00 : Fault zone, graphitic gouge seams at top and bottom of section</p> <p>136.25 - 136.60 : Carb.-in-filled breccia vein at ~20-30° to C.A.</p> <p>137.60 - 137.70 : Qtz - carb. breccia vein at ~40° to C.A.</p> <p>Core Angles: 136.80 - 72° - siltstone laminae 142.50 35° " "</p> | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

7 of 8

Hole No. Co ord. Horizontal Length Date Completed

Claim No. Core Size Drilled By

Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 171.40 - 184.70 | Oacitic Ash-lapilli tuff - slightly argillaceous matrix and minor argillite fragments - bluish grey matrix - minor chlorite alteration in fragments - weakly foliated - overall tr py 179.95 - 180.05 : graphitic/talc gouge 180.40 - 180.60 : minor talc coating in brecciated section 181.90 - 181.94 : Qtz vein with graphitic contacts at 42° to C.A. | | | | | | | | |
| 184.70 - 187.60 | Argillite - massive, with minor siltstone interbeds Tr = 1% py stringers, at ~ 50° to Core Axis 187.10 - 187.16 : graphitic gouge 187.48 - 187.58 : graphitic gouge and brecciated section Core angles : 185.00 - 45° 186.50 - 50° | | | | | | | | |
| 187.60 - 190.80 | Andesitic lapilli tuff Coarse, bluish grey, silicified and chlorite + sericite altered. 3-5% fine cross-cutting Qtz-carb. veinlets at 30° to 60° to Core Axis. 1-2% py stringers, minor py fragments | | | | | | | | |


**GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD**

Hole No. AP 7 Coord. Horizontal Length Date Completed

Claim No. Core Size Drilled By

Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | NUMBER | WIDTH | Au. | Ag | Cu. | Zn. | As. | WIDTH X ASSAY | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|-----|-----|-----|-----|-----|---------------|--|--|--|--|----------|-------|-----|-----|-----|-----|--|
| | | | | | | | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | |
| 0.00 - 7.62 | CASING | 7.62 | ppb | ppm | | | ppm | | | | | | | | | | | | |
| 7.62 - 20.40 | WASTE | 12.78 | | | | | | | | | | | | | | | | | |
| 20.40 - 20.95 | 1369-G | 0.55 | 1 | .2 | | | 3 | | | | | | | | | | | | |
| 20.95 - 21.45 | 1370-G | 0.5 | 7 | .3 | | | 33 | | | | | | | | | | | | |
| 21.45 - 21.95 | 1371-G | 0.5 | 1 | .1 | | | 4 | | | | | | | | | | | | |
| 21.95 - 22.45 | 1372-G | 0.5 | 3 | .1 | | | 6 | | | | | | | | | | | | |
| 22.45 - 22.95 | 1373-G | 0.5 | 1 | .1 | | | 2 | | | | | | | | | | | | |
| 22.95 - 23.45 | 1374-G | 0.5 | 1 | .1 | | | 2 | | | | | | | | | | | | |
| 23.45 - 23.95 | 1375-G | 0.5 | 1 | .2 | | | 2 | | | | | | | | | | | | |
| 23.95 - 24.35 | 1376-G | 0.4 | 3 | .3 | | | 11 | | | | | | | | | | | | |
| 24.35 - 24.85 | 1377-G | 0.5 | 7 | .4 | | | 4 | | | | | | | | | | | | |
| 24.85 - 25.35 | 1378-G | 0.5 | 1 | .3 | | | 6 | | | | | | | | | | | | |
| 25.35 - 25.85 | 1379-G | 0.5 | 1 | .3 | | | 8 | | | | | | | | | | | | |
| 25.85 - 26.35 | 1380-G | 0.5 | 1 | .1 | | | 2 | | | | | | | | | | | | |
| 26.35 - 26.85 | 1381-G | 0.5 | 6 | .1 | | | 3 | | | | | | | | | | | | |
| 26.85 - 27.35 | 1382-G | 0.5 | 3 | .1 | | | 6 | | | | | | | | | | | | |
| 27.35 - 27.85 | 1383-G | 0.5 | 21 | .3 | | | 3 | | | | | | | | | | | | |
| 27.85 - 28.35 | 1384-G | 0.5 | 2 | .1 | | | 2 | | | | | | | | | | | | |
| 28.35 - 28.85 | 1385-G | 0.5 | 5 | .1 | | | 3 | | | | | | | | | | | | |
| 28.85 - 29.35 | 1386-G | 0.5 | 4 | .1 | | | 2 | | | | | | | | | | | | |
| 29.35 - 29.85 | 1387-G | 0.5 | 2 | .3 | | | 8 | | | | | | | | | | | | |
| 29.85 - 30.35 | 1388-G | 0.5 | 4 | .4 | | | 5 | | | | | | | | | | | | |
| 30.35 - 30.85 | 1389-G | 0.5 | 5 | .2 | | | 7 | | | | | | | | | | | | |
| 30.85 - 31.35 | 1390-G | 0.5 | 9 | .2 | | | 4 | | | | | | | | | | | | |
| 31.35 - 31.85 | 1391-G | 0.5 | 1 | .4 | | | 3 | | | | | | | | | | | | |
| 31.85 - 32.35 | 1392-G | 0.5 | 5 | .3 | | | 5 | | | | | | | | | | | | |
| 32.35 - 32.85 | 1393-G | 0.5 | 7 | .2 | | | 4 | | | | | | | | | | | | |
| 32.85 - 33.35 | 1394-G | 0.5 | 6 | .4 | | | 7 | | | | | | | | | | | | |
| 33.35 - 33.85 | 1395-G | 0.5 | 4 | .3 | | | 2 | | | | | | | | | | | | |
| 33.85 - 34.35 | 1396-G | 0.5 | 4 | .1 | | | 2 | | | | | | | | | | | | |
| 34.35 - 34.85 | 1397-G | 0.5 | 3 | .3 | | | 8 | | | | | | | | | | | | |
| 34.85 - 35.35 | 1398-G | 0.5 | 28 | .2 | | | 7 | | | | | | | | | | | | |
| 35.35 - 35.85 | 1399-G | 0.5 | 3 | .2 | | | 9 | | | | | | | | | | | | |
| 35.85 - 36.35 | 1400-G | 0.5 | 7 | .4 | | | 11 | | | | | | | | | | | | |
| 36.35 - 36.85 | 1401-G | 0.5 | 3 | .4 | | | 9 | | | | | | | | | | | | |
| 36.85 - 37.35 | 1402-G | 0.5 | 6 | .3 | | | 11 | | | | | | | | | | | | |
| 37.35 - 44.00 | WASTE | 6.65 | - | - | | | - | | | | | | | | | | | | |
| 44.00 - 44.50 | 1403-G | 0.5 | 7 | .1 | | | 11 | | | | | | | | | | | | |
| 44.50 - 45.00 | 1404-G | 0.5 | 9 | .2 | | | 9 | | | | | | | | | | | | |
| 45.00 - 45.50 | 1405-G | 0.5 | 5 | .3 | | | 10 | | | | | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 7 Co ord Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | NUMBER | WIDTH | Au ppm | Ag ppm | Cu | Zn | As ppm | WIDTH X ASSAY | | | | | AVERAGES | | | | | |
|---------------------------|--------|-------|-----------|-----------|----|-----|-----------|---------------|-----------|-----------|----|----|----------|--|--|--|--|--|
| | | | | | | | | WIDTH | Au g/t | Ag g/t | Cu | Zn | As | | | | | |
| 68.00 - 68.50 | 1446-G | 0.5 | 1 | .5 | | | 5 | | | | | | | | | | | |
| 68.50 - 69.00 | 1447-G | 0.5 | 12 | .6 | | | 11 | | | | | | | | | | | |
| 69.00 - 69.50 | 1448-G | 0.5 | 4 | .8 | | | 43 | | | | | | | | | | | |
| 69.50 - 70.00 | 1449-G | 0.5 | 1 | 1.1 | | | 34 | | | | | | | | | | | |
| 70.00 - 70.50 | 1450-G | 0.5 | 21 | 1.6 | | | 51 | | | | | | | | | | | |
| 70.50 - 71.00 | 1451-G | 0.5 | 33 | 2.0 | | | 156 | | | | | | | | | | | |
| 71.00 - 71.50 | 1452-G | 0.5 | 9 | 1.6 | | | 69 | | | | | | | | | | | |
| 71.50 - 77.50 | WASTE | 6.0 | | | | | | | | | | | | | | | | |
| 77.50 - 78.00 | 1453-G | 0.5 | 3 | .4 | | | 16 | | | | | | | | | | | |
| 78.00 - 78.50 | 1454-G | 0.5 | 11 | .6 | | | 12 | | | | | | | | | | | |
| 78.50 - 79.00 | 1455-G | 0.5 | 14 | .7 | | | 13 | | | | | | | | | | | |
| 79.00 - 79.50 | 1456-G | 0.5 | 9 | .6 | | | 9 | | | | | | | | | | | |
| 79.50 - 80.00 | 1457-G | 0.5 | 17 | .5 | | | 21 | | | | | | | | | | | |
| 80.00 - 80.50 | 1458-G | 0.5 | 6 | .3 | | | 8 | | | | | | | | | | | |
| 80.50 - 81.00 | 1459-G | 0.5 | 28 | 1.3 | | | 22 | | | | | | | | | | | |
| 81.00 - 81.50 | 1460-G | 0.5 | 10 | .4 | | | 22 | | | | | | | | | | | |
| 81.50 - 82.00 | 1461-G | 0.5 | 13 | .6 | | | 18 | | | | | | | | | | | |
| 82.00 - 82.50 | 1462-G | 0.5 | 10 | .6 | | | 11 | | | | | | | | | | | |
| 82.50 - 83.00 | 1463-G | 0.5 | 8 | .4 | | | 5 | | | | | | | | | | | |
| 83.00 - 83.50 | 1464-G | 0.5 | 15 | .6 | | | 12 | | | | | | | | | | | |
| 83.50 - 84.00 | 1465-G | 0.5 | 25 | 1.1 | | | 22 | | | | | | | | | | | |
| 84.00 - 84.50 | 1466-G | 0.5 | 33 | 1.1 | | | 9 | | | | | | | | | | | |
| 84.50 - 85.00 | 1467-G | 0.5 | 18 | .7 | | | 12 | | | | | | | | | | | |
| 85.00 - 85.50 | 1468-G | 0.5 | 15 | .5 | | | 10 | | | | | | | | | | | |
| 85.50 - 85.80 | 1469-G | 0.3 | 37 | 1.2 | | | 16 | | | | | | | | | | | |
| 85.80 - 86.10 | 1470-G | 0.3 | 7 | .3 | 21 | 27 | 26 | | | | | | | | | | | |
| 86.10 - 86.40 | 1471-G | 0.3 | 11 | .5 | 22 | 20 | 132 | | | | | | | | | | | |
| 86.40 - 86.70 | 1472-G | 0.3 | 11 | .4 | 16 | 332 | 48 | | | | | | | | | | | |
| 86.70 - 87.00 | 1473-G | 0.3 | 806 | 1.6 | 20 | 75 | 3675 | | | | | | | | | | | |
| 87.00 - 87.30 | 1474-G | 0.3 | 767 | 1.3 | 8 | 32 | 4213 | | | | | | | | | | | |
| 87.30 - 87.60 | 1475-G | 0.3 | 411 | 1.3 | 18 | 334 | 996 | | | | | | | | | | | |
| 87.60 - 87.90 | 1476-G | 0.3 | 2399 | 3.8 | 19 | 45 | 8159 | | | | | | | | | | | |
| 87.90 - 88.20 | 1477-G | 0.3 | 200 | .6 | 13 | 132 | 549 | | | | | | | | | | | |
| 88.20 - 88.70 | 1478-G | 0.5 | 34 | 1.4 | 26 | 120 | 74 | | | | | | | | | | | |
| 88.70 - 89.20 | 1479-G | 0.5 | 6 | .3 | 20 | 120 | 25 | | | | | | | | | | | |
| 89.20 - 89.70 | 1480-G | 0.5 | 22 | 1.4 | 48 | 44 | 38 | | | | | | | | | | | |
| 89.70 - 90.20 | 1481-G | 0.5 | 11 | .6 | 17 | 71 | 24 | | | | | | | | | | | |
| 90.20 - 90.70 | 1482-G | 0.5 | 12 | .4 | 8 | 38 | 23 | | | | | | | | | | | |
| 90.70 - 91.00 | 1483-G | 0.3 | 376 | 1.7 | 35 | 298 | 2003 | | | | | | | | | | | |
| 91.00 - 91.30 | 1484-G | 0.3 | 161 | .9 | 10 | 134 | 836 | | | | | | | | | | | |

} 1.2m 1.097 2.0 ✓

GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. **AP 7** Co. ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au ppb | Ag | Cu | Zn | As | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | | | | | | |
|---------------------------|--------|-------|-----------|-----|----|-----|-----|---------------|----|----|----|----|----|----------|----|----|----|----|----|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au | Ag | Cu | Zn | As | WIDTH | Au | Ag | Cu | Zn | As | | | | | | |
| 91.30-91.80 | 1485-G | 0.5 | 43 | .6 | 20 | 88 | 59 | | | | | | | | | | | | | | | | | | |
| 91.80-92.30 | 1486-G | 0.5 | 13 | .5 | 18 | 80 | 29 | | | | | | | | | | | | | | | | | | |
| 92.30-92.60 | 1487-G | 0.3 | 87 | 1.5 | 63 | 133 | 117 | | | | | | | | | | | | | | | | | | |
| 92.60-92.90 | 1488-G | 0.3 | 31 | .3 | 11 | 78 | 92 | | | | | | | | | | | | | | | | | | |
| 92.90-93.30 | 1489-G | 0.3 | 137 | 1.0 | 17 | 192 | 413 | | | | | | | | | | | | | | | | | | |
| 93.30-93.50 | 1490-G | 0.3 | 83 | .9 | 38 | 521 | 256 | | | | | | | | | | | | | | | | | | |
| 93.50-93.80 | 1491-G | 0.3 | 523 | .7 | 6 | 148 | 595 | | | | | | | | | | | | | | | | | | |
| 93.80-94.10 | 1492-G | 0.3 | 406 | 1.1 | 14 | 235 | 587 | | | | | | | | | | | | | | | | | | |
| 94.10-94.50 | 1493-G | 0.4 | 107 | 1.1 | 38 | 128 | 206 | | | | | | | | | | | | | | | | | | |
| 94.50-95.00 | 1494-G | 0.5 | 19 | .7 | 40 | 175 | 41 | | | | | | | | | | | | | | | | | | |
| 95.00-95.50 | 1495-G | 0.5 | 8 | .8 | 35 | 154 | 19 | | | | | | | | | | | | | | | | | | |
| 95.50-96.00 | 1496-G | 0.5 | 19 | .9 | 30 | 78 | 45 | | | | | | | | | | | | | | | | | | |
| 96.00-96.50 | 1497-G | 0.5 | 162 | .8 | 61 | 180 | 38 | | | | | | | | | | | | | | | | | | |
| 96.50-97.00 | 1498-G | 0.5 | 66 | .6 | | | 31 | | | | | | | | | | | | | | | | | | |
| 97.00-97.50 | 1499-G | 0.5 | 29 | .7 | | | 18 | | | | | | | | | | | | | | | | | | |
| 97.50-98.00 | 1500-G | 0.5 | 19 | .9 | | | 26 | | | | | | | | | | | | | | | | | | |
| 98.00-98.50 | 1501-G | 0.5 | 31 | .7 | | | 30 | | | | | | | | | | | | | | | | | | |
| 98.50-99.00 | 1502-G | 0.5 | 16 | .4 | | | 7 | | | | | | | | | | | | | | | | | | |
| 99.00-99.50 | 1503-G | 0.5 | 37 | .6 | | | 15 | | | | | | | | | | | | | | | | | | |
| 99.50-100.00 | 1504-G | 0.5 | 51 | .6 | | | 8 | | | | | | | | | | | | | | | | | | |
| 100.00-100.50 | 1505-G | 0.5 | 49 | .3 | | | 12 | | | | | | | | | | | | | | | | | | |
| 100.50-101.00 | 1506-G | 0.5 | 9 | .1 | | | 17 | | | | | | | | | | | | | | | | | | |
| 101.00-101.50 | 1507-G | 0.5 | 7 | .2 | | | 15 | | | | | | | | | | | | | | | | | | |
| 101.50-102.00 | 1508-G | 0.5 | 178 | 2.5 | | | 32 | | | | | | | | | | | | | | | | | | |
| 102.00-102.50 | 1509-G | 0.5 | 10 | .3 | | | 6 | | | | | | | | | | | | | | | | | | |
| 102.50-103.00 | 1510-G | 0.5 | 27 | .8 | | | 37 | | | | | | | | | | | | | | | | | | |
| 103.00-103.50 | 1511-G | 0.5 | 19 | .6 | | | 38 | | | | | | | | | | | | | | | | | | |
| 103.50-104.00 | 1512-G | 0.5 | 10 | 1.2 | | | 13 | | | | | | | | | | | | | | | | | | |
| 104.00-104.50 | 1513-G | 0.5 | 5 | 1.0 | | | 13 | | | | | | | | | | | | | | | | | | |
| 104.50-105.00 | 1514-G | 0.5 | 23 | 1.0 | | | 21 | | | | | | | | | | | | | | | | | | |
| 105.00-113.00 | WASTE | 80 | | | | | | | | | | | | | | | | | | | | | | | |
| 113.00-113.50 | 1515-G | 0.5 | 13 | .7 | | | 34 | | | | | | | | | | | | | | | | | | |
| 113.50-114.00 | 1516-G | 0.5 | 27 | 2.1 | | | 15 | | | | | | | | | | | | | | | | | | |
| 114.00-114.50 | 1517-G | 0.5 | 30 | 1.3 | | | 29 | | | | | | | | | | | | | | | | | | |
| 114.50-115.00 | 1518-G | 0.5 | 1 | .6 | | | 10 | | | | | | | | | | | | | | | | | | |
| 115.00-116.50 | WASTE | 1.5 | | | | | | | | | | | | | | | | | | | | | | | |
| 116.50-117.00 | 1519-G | 0.5 | 3 | .2 | | | 18 | | | | | | | | | | | | | | | | | | |
| 117.00-117.50 | 1520-G | 0.5 | 1 | .2 | | | 28 | | | | | | | | | | | | | | | | | | |
| 117.50-118.00 | 1521-G | 0.5 | 11 | .4 | | | 57 | | | | | | | | | | | | | | | | | | |
| 118.00-118.50 | 1522-G | 0.5 | 3 | .3 | | | 13 | | | | | | | | | | | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 7 Co ord. _____ Horizontal Length _____ Date Completed _____
Claim No. _____ Core Size _____ Drilled By _____
Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET / METRES | NUMBER | WIDTH | Au | Ag | Cu. | Zn | As | WIDTH X ASSAY | | | | | AVERAGES | | | | | | | |
|---------------------------|--------|-------|----|-----|-----|----|----|---------------|--|--|--|--|----------|-----|-----|-----|-----|--|--|--|
| | | | | | | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | |
| 118.50 - 119.00 | 1523-G | 0.5 | 13 | .3 | | | 64 | | | | | | | | | | | | | |
| 119.00 - 121.50 | WASTE | 2.5 | — | — | | | — | | | | | | | | | | | | | |
| 121.50 - 122.00 | 1524-G | 0.5 | 3 | .4 | | | 15 | | | | | | | | | | | | | |
| 122.00 - 122.50 | 1525-G | 0.5 | 3 | .4 | | | 9 | | | | | | | | | | | | | |
| 122.50 - 123.00 | 1526-G | 0.5 | 1 | .6 | | | 10 | | | | | | | | | | | | | |
| 123.00 - 123.50 | 1527-G | 0.5 | 2 | .6 | | | 21 | | | | | | | | | | | | | |
| 123.50 - 124.00 | 1528-G | 0.5 | 2 | .5 | | | 15 | | | | | | | | | | | | | |
| 124.00 - 124.50 | 1529-G | 0.5 | 1 | .9 | | | 28 | | | | | | | | | | | | | |
| 124.50 - 125.00 | 1530-G | 0.5 | 2 | .3 | | | 17 | | | | | | | | | | | | | |
| 125.00 - 125.50 | 1531-G | 0.5 | 1 | .6 | | | 25 | | | | | | | | | | | | | |
| 125.50 - 126.00 | 1532-G | 0.5 | 1 | .5 | | | 11 | | | | | | | | | | | | | |
| 126.00 - 126.50 | 1533-G | 0.5 | 2 | .5 | | | 14 | | | | | | | | | | | | | |
| 126.50 - 127.00 | 1534-G | 0.5 | 3 | .6 | | | 9 | | | | | | | | | | | | | |
| 127.00 - 127.50 | 1535-G | 0.5 | 6 | 1.4 | | | 11 | | | | | | | | | | | | | |
| 127.50 - 128.00 | 1536-G | 0.5 | 8 | 2.1 | | | 37 | | | | | | | | | | | | | |
| 128.00 - 128.50 | 1537-G | 0.5 | 7 | 1.1 | | | 33 | | | | | | | | | | | | | |
| 128.50 - 133.40 | WASTE | 4.9 | — | — | | | — | | | | | | | | | | | | | |
| 133.40 - 133.90 | 1538-G | 0.5 | 17 | 2.0 | | | 44 | | | | | | | | | | | | | |
| 133.90 - 134.40 | 1539-G | 0.5 | 5 | .7 | | | 22 | | | | | | | | | | | | | |
| 134.40 - 134.90 | 1540-G | 0.5 | 7 | .9 | | | 28 | | | | | | | | | | | | | |
| 134.90 - 135.40 | 1541-G | 0.5 | 4 | .7 | | | 34 | | | | | | | | | | | | | |
| 135.40 - 136.20 | 1542-G | 0.8 | 14 | .7 | | | 24 | | | | | | | | | | | | | |
| 136.20 - 136.60 | 1543-G | 0.4 | 2 | .3 | | | 4 | | | | | | | | | | | | | |
| 136.60 - 137.10 | 1544-G | 0.5 | 1 | .2 | | | 8 | | | | | | | | | | | | | |
| 137.10 - 139.00 | WASTE | 1.9 | — | — | | | — | | | | | | | | | | | | | |
| 139.00 - 139.50 | 1545-G | 0.5 | 9 | .7 | | | 21 | | | | | | | | | | | | | |
| 139.50 - 140.00 | 1546-G | 0.5 | 9 | .6 | | | 31 | | | | | | | | | | | | | |
| 140.00 - 140.50 | 1547-G | 0.5 | 23 | 2.8 | | | 73 | | | | | | | | | | | | | |
| 140.50 - 141.00 | 1548-G | 0.5 | 13 | 1.8 | | | 33 | | | | | | | | | | | | | |
| 141.00 - 141.50 | 1549-G | 0.5 | 8 | 1.6 | | | 19 | | | | | | | | | | | | | |
| 141.50 - 142.00 | 1550-G | 0.5 | 10 | .2 | | | 17 | | | | | | | | | | | | | |
| 142.00 - 142.50 | 1551-G | 0.5 | 9 | .6 | | | 32 | | | | | | | | | | | | | |
| 142.50 - 143.00 | 1552-G | 0.5 | 10 | 1.1 | | | 24 | | | | | | | | | | | | | |
| 143.00 - 149.00 | WASTE | 6.0 | — | — | | | — | | | | | | | | | | | | | |
| 149.00 - 149.50 | 1553-G | 0.5 | 8 | 1.0 | | | 33 | | | | | | | | | | | | | |
| 149.50 - 150.00 | 1554-G | 0.5 | 8 | .3 | | | 38 | | | | | | | | | | | | | |
| 150.00 - 150.50 | 1555-G | 0.5 | 5 | .9 | | | 39 | | | | | | | | | | | | | |
| 150.50 - 151.00 | 1556-G | 0.5 | 5 | 1.0 | | | 32 | | | | | | | | | | | | | |
| 151.00 - 151.50 | 1557-G | 0.5 | 7 | .7 | | | 27 | | | | | | | | | | | | | |
| 151.50 - 152.00 | 1558-G | 0.5 | 7 | .9 | | | 38 | | | | | | | | | | | | | |



GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 7 Co. ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET/ <u>METRES</u> | NUMBER | WIDTH | Au. | Ag. | Cu. | Zn. | As | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | |
|---------------------------------|--------|-------|-----|-----|-----|-----|-----|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | |
| 152.00 - 152.50 | 1559-G | 0.5 | 8 | .8 | | | 31 | | | | | | | | | | | | | |
| 152.50 - 153.00 | 1560-G | 0.5 | 4 | .8 | | | 31 | | | | | | | | | | | | | |
| 153.00 - 153.50 | 1561-G | 0.5 | 8 | 1.0 | | | 34 | | | | | | | | | | | | | |
| 153.50 - 154.00 | 1562-G | 0.5 | 7 | 1.0 | | | 31 | | | | | | | | | | | | | |
| 154.00 - 154.50 | 1563-G | 0.5 | 11 | 1.2 | | | 38 | | | | | | | | | | | | | |
| 154.50 - 154.80 | 1564-G | 0.3 | 4 | 1.1 | | | 31 | | | | | | | | | | | | | |
| 154.80 - 168.35 | WASTE | 14.05 | — | — | | | — | | | | | | | | | | | | | |
| 168.35 - 169.35 | 1565-G | 0.5 | 8 | 1.0 | | | 28 | | | | | | | | | | | | | |
| 169.35 - 169.85 | 1566-G | 0.5 | 9 | .2 | | | 26 | | | | | | | | | | | | | |
| 169.85 - 170.35 | 1567-G | 0.5 | 5 | .7 | | | 22 | | | | | | | | | | | | | |
| 170.35 - 170.85 | 1568-G | 0.5 | 7 | .9 | | | 28 | | | | | | | | | | | | | |
| 170.85 - 171.35 | 1569-G | 0.5 | 4 | .7 | | | 34 | | | | | | | | | | | | | |
| 171.35 - 171.85 | 1570-G | 0.5 | 14 | .7 | | | 24 | | | | | | | | | | | | | |
| 171.85 - 172.35 | 1571-G | 0.5 | 2 | .3 | | | 4 | | | | | | | | | | | | | |
| 172.35 - 172.85 | 1572-G | 0.5 | 1 | .2 | | | 8 | | | | | | | | | | | | | |
| 172.85 - 173.35 | 1573-G | 0.5 | 1 | .4 | | | 9 | | | | | | | | | | | | | |
| 173.35 - 173.85 | 1574-G | 0.5 | 3 | .5 | | | 18 | | | | | | | | | | | | | |
| 173.85 - 174.20 | 1575-G | 0.35 | 3 | .3 | | | 13 | | | | | | | | | | | | | |
| 174.20 - 179.90 | WASTE | 5.7 | — | — | | | — | | | | | | | | | | | | | |
| 179.90 - 180.40 | 1576-G | 0.5 | 7 | 1.4 | | | 62 | | | | | | | | | | | | | |
| 180.40 - 180.90 | 1577-G | 0.5 | 1 | .7 | | | 12 | | | | | | | | | | | | | |
| 180.90 - 181.40 | 1578-G | 0.5 | 13 | 1.4 | | | 39 | | | | | | | | | | | | | |
| 181.40 - 181.90 | 1579-G | 0.5 | 6 | 2.0 | | | 45 | | | | | | | | | | | | | |
| 181.90 - 182.40 | 1580-G | 0.5 | 3 | 1.1 | | | 25 | | | | | | | | | | | | | |
| 182.40 - 182.90 | 1581-G | 0.5 | 3 | .8 | | | 21 | | | | | | | | | | | | | |
| 182.90 - 183.40 | 1582-G | 0.5 | 2 | .8 | | | 31 | | | | | | | | | | | | | |
| 183.40 - 183.90 | 1583-G | 0.5 | 3 | 1.0 | | | 29 | | | | | | | | | | | | | |
| 183.90 - 184.40 | 1584-G | 0.5 | 4 | 1.3 | | | 52 | | | | | | | | | | | | | |
| 184.40 - 184.90 | 1585-G | 0.5 | 9 | 2.8 | | | 46 | | | | | | | | | | | | | |
| 184.90 - 185.40 | 1586-G | 0.5 | 19 | 4.2 | | | 53 | | | | | | | | | | | | | |
| 185.40 - 185.90 | 1587-G | 0.5 | 23 | 4.9 | | | 46 | | | | | | | | | | | | | |
| 185.90 - 186.40 | 1588-G | 0.5 | 16 | 4.4 | | | 80 | | | | | | | | | | | | | |
| 186.40 - 186.90 | 1589-G | 0.5 | 21 | 2.9 | | | 129 | | | | | | | | | | | | | |
| 186.90 - 187.40 | 1590-G | 0.5 | 15 | 2.5 | | | 75 | | | | | | | | | | | | | |
| 187.40 - 187.90 | 1591-G | 0.5 | 4 | .4 | | | 10 | | | | | | | | | | | | | |
| 187.90 - 188.40 | 1592-G | 0.5 | 11 | .8 | | | 40 | | | | | | | | | | | | | |
| 188.40 - 188.90 | 1593-G | 0.5 | 31 | .5 | | | 93 | | | | | | | | | | | | | |
| 188.90 - 189.40 | 1594-G | 0.5 | 6 | .3 | | | 4 | | | | | | | | | | | | | |
| 189.40 - 189.90 | 1595-G | 0.5 | 2 | .2 | | | 2 | | | | | | | | | | | | | |
| 189.90 - 190.40 | 1596-G | 0.5 | 9 | 1.0 | | | 13 | | | | | | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

1 of 17

Property Unuk River Option Project No. 134 Depth 306.91 Date Began Aug. 23/90
 Hole No. A.P.8 Co ord. 1175 N Horizontal Length 186 m Date Completed Aug 29/90
 Claim No. Unuk 26 321 W Core Size BGBDM Drilled By J.T. Thomas
 Grid No. Zone 1 Angle & Direction -55° Az 080 Elevation 1408 m Logged By D & B Gabovny

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 0 - 3.05 | Casing | | | | | | | | |
| 3.05 - 21.50 | Pyroclastic breccia - very coarse, poorly sorted heterolithic breccia - greenish to bluish grey, matrix supported, with dacitic and rhyolitic (flow) and ash flow tuff fragments, minor argillite fragments - overall Tr. diss. py | | | | | | | | |
| 16.50 - 20.50 | Fault zone, highly fractured and limonite stained, uncectified altered, fractures 1-4cm apart. - 60% core recovery | | | | | | | | |
| 20.50 - 21.50 | Strongly silicified, weakly chloritized, partially re-brecciated, minor kaolinized fragments | | | | | | | | |
| | Core Angles: (of predominant fracture directions) | | | | | | | | |
| | | 11.5m | = | 45° | | | | | |
| | | 13.0m | = | 46° | | | | | |
| 21.50 - 26.15 | Ash Flow Tuff - Brecciated and strongly silicified dacitic welded tuff - relict flattened purplish fragments. - Strongly fractured and limonite-stained. | | | | | | | | |
| 21.50 - 22.20 | Very strongly fractured, fault zone kaolinized breccia fragments | | | | | | | | |
| 24.60 - 25.65 | Fault zone, strong brecciation, Fe-carb. and silica flooding. | | | | | | | | |
| 25.65 - 26.15 | minor argillite inter-flow breccia, silicified dacitic fragments in matrix | | | | | | | | |

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

20,390

20f 17

Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 26.15 - 27.40 | Argillaceous Debris Flow ~20% light greenish grey felsic fragments in black argillite matrix - strongly fractured broken core, with minor carb. stringers and limonite stain | | | | | | | | |
| 27.40 - 33.30 | Ash Flow tuff - strongly silicified & brecciated welded dacitic tuff - strongly fractured, with pervasive limonite/ ankerite alteration - abundant black arborescent and diffuse overgrowths along fine fracture veinlets - minor relict silicified/chloritized flattened pumice fragments 32.00 - 32.61 : irreg. carb. veinlets, sub-parallel to core axis 33.00 - 33.30 : fault gouge, rusty stained at bottom of section. | | | | | | | | |
| 33.30 - 63.80 | Dacitic Flow breccia - light greenish grey strongly silicified, locally flow banded fragments - fragment supported, matrix-deficient - chlorite and sericite alt'n in cores of fragments - fine black particulate rims around relict fragments - limonitic stain diffuses outward from numerous fractures - overall tr. py. 55.15 - 55.25 : fault gouge + limonitic breccia, at ~ 50° to C.A. | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. Co ord. Horizontal Length Date Completed
Claim No. Core Size Drilled By
Grid No. Angle & Direction Elevation Logged By

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| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 63.80 - 82.80 | Flow Banded/Brecciated Rhyolite - light bluish grey - gradational upper contact from silicified dacite to finely laminated rhyolite - minor very fine welded tuff sections with relict flattened pumice fragments | | | | | | | | |
| 68.00 - 69.50 | : Fault zone, strongly fractured & rubbly core | | | | | | | | |
| 73.90 - 74.50 | : Fault zone, strongly fractured, silicified + sericitized | | | | | | | | |
| 75.30 - 75.90 | : Fault zone, strongly fractured and broken, rubbly core ~50% core recovery | | | | | | | | |
| 78.00 | : 1cm wide band of massive pyrite, in irreg. Qtz vein, at ~55° to CIA. | | | | | | | | |
| 75.30 - 78.00 | : minor irreg. carb. veinlets, with grey outer margins and pale orange centers, .5-1cm. thick. | | | | | | | | |
| 81.40 - 82.80 | : light green sericite & chlorite alteration in breccia fragments. | | | | | | | | |
| 82.80 - 86.40 | Fine grained "Andesitic" Dike - massive, light grey, with 2-3% round chloritic patches, 1-2cm across, possible amygdules - moderately well fractured, 3-5cm. apart, with minor talc coatings | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. Coord. Horizontal Length Date Completed

Claim No. Core Size Drilled By

Grid No. Angle & Direction Elevation Logged By

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| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 84.50 - 86.40 | : strong fractures, fault zone, talc coatings, abundant gouge | | | | | | | | |
| 84.00 | : 1cm Qtz-carb. veinlet at $\pm 30^\circ$ to core axis | | | | | | | | |
| | upper contact at 33° to CA, with weak flow banding. | | | | | | | | |
| 86.40 - 99.00 | Brecciated / Banded rhyolite lapilli tuff | | | | | | | | |
| | - Strongly silicified breccia, with numerous welded tuff and flow banded fragments | | | | | | | | |
| | - Strong sericite alteration of fragments and in tuffaceous bands. | | | | | | | | |
| | - Tr very fine diss. py | | | | | | | | |
| 88.60 - 88.80 | = fault zone, strongly fractured, and limonitic gouge | | | | | | | | |
| 89.00 - 89.20 | : fault zone | | | | | | | | |
| 89.91 - 90.20 | : fault zone, rubbly limonitic core. | | | | | | | | |
| 90.20 - 93.60 | : Very strong silicification, with 1-2% fine Qtz stockwork veinlets, up to 1cm thick. | | | | | | | | |
| | - relict fragment outlines with strongly sericitized cores | | | | | | | | |
| -92.0 - 93.10 | : several short gouge seams, faults at low core angles. | | | | | | | | |
| 93.80 - 99.00 | : Strongly faulted, rubbly core - abundant gouge from 93.85 to 99.0. Tr-1% fine diss py | | | | | | | | |

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | - minor Qtz veinlets at 30-45° to core axis. 94.00-96.00 = 40% core recovery | | | | | | | | |
| 19.00 - 103.80 | Argillaceous Debris Flow - light greenish grey dacitic fragments supported in argillite matrix, with minor siltstone interbeds - Strongly faulted throughout section, with rubble broken core and graphitic/clay gouge to 103.00. - siltstone laminae at 100.00 = 55° to C.A. | | | | | | | | |
| 103.80 - 108.30 | Tuffaceous Wacke - medium grained, dark grey, finely laminated feldspathic grey wacke. - minor fractures with diffuse limonite stain, - weak chlorite alteration Core angles: upper contact 103.80 = 25° bedding 104.80 = 62° 105.30 = 52° 107.50 = 60° | | | | | | | | |
| 108.30 - 131.70 | Argillaceous Debris Flow - Interbedded debris flow and minor massive to poorly bedded argillite/siltstone - Strong to moderate incipient crackle breccia with very fine calcite veinlets - Tr diss py, and minor py in calcite veinlets | | | | | | | | |


**GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG**

Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

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| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 110.60 - 113.00 | : Strongly faulted with fractures at 0-20° to C.A. - Minor slickensides rake ~45° to C.A. - rubbly gouge from 110.6 to 111.6 | | | | | | | | |
| 114.91 - 116.40 | : Fault zone with gouge at 114.91 to 115.00, fault at low core angle, ~20° to C.A., slickensides rake ~30° from vertical - Tr = 1% py in calcite fracture veinlets | | | | | | | | |
| 118.80 - 119.20 | - very light grey, strongly silicified dike, with chloritic phenocrysts, and cross-cutting Qtz-carb. veinlets, | | | | | | | | |
| 122.90 - 123.45 | : Fault zone, gravelly-clay gouge and crackle breccia | | | | | | | | |
| 129.50 - 131.35 | : gradually increasing silicification - bleached sections, minor tuffaceous bands. | | | | | | | | |
| 131.35 - 131.70 | : Fault zone, graphitic/gravelly clay gouge. | | | | | | | | |
| 131.70 - 169.20 | Brecciated Dacite lapilli tuff - very strongly altered, + silicified, light bluish to light greenish grey. | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| * 131.70 - 134.00 | : very strongly silicified box work alteration pattern around relict fragments, - numerous Qtz stringers - 5-10% patch py blebs and stringers 133.20 - 133.25 : rusty, vuggy Qtz-carb. vein at 45° to C.A. with Tr-1% galena | | | | | | | | |
| 134.00 - 134.70 | : 1-2% py, in strongly silicified, box work - altered tuff-breccia weak to moderate sericitic alteration. | | | | | | | | |
| 134.70 - 145.70 | : Very strongly silicified, moderately to strongly sericitized, box work alteration around relict fragments, - cross cutting Qtz-carb. veinlets spaced ~ 1-2 cm apart, at ~ 35-45° to C.A. - minor chlorite alteration. | | | | | | | | |
| 143.00 - 143.50 | : Fault gouge | | | | | | | | |
| 146.00 - 154.30 | : very strong silicification, greenish black, chloritic, tuff-breccia, strong crackle brecciation and calcite stockwork veinlets. - Qtz-chlorite-carb. fracture veinlets with slickensides at varying core angles. In py | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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Hole No Co ord Horizontal Length Date Completed
 Claim No Core Size Drilled By
 Grid No Angle & Direction Elevation Logged By

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 153.90 - 156.90 | : Faulted, strongly brecciated and broken core, with Qtz-chlorite-carb infilling and veinlets. Tr-1% py in veinlets. | | | | | | | | |
| * 156.96 - 157.50 | : Strongly silicified section with ~50% Qtz-carb. veinlets, 5-10% py blebs and stringers. Tr sphalerite. Lower contact at ~35° to C.A. | | | | | | | | |
| 158.60 - 164.00 | : Fault zone, very strongly fractured, abundant slickensides at chaotic angles, and irregular Qtz-carb. tension veinlets. Minor greenish black, altered breccia fragments. Overall 3-5% py in stockwork veinlets. | | | | | | | | |
| 166.10 - 166.80 | : irregular Qtz-py vein sub-parallel to core axis, with diffuse alteration selvege. 2-3% py blebs and stringers. | | | | | | | | |
| 167.10 - 169.20 | : Strong boxwork-hydrothermal alteration in breccia, relict fragments abundant, strongly silicified and sericitized. | | | | | | | | |
| 174.2 | : minor fault surfaces at ~35° to C.A. with slickensides striking ~30° from vertical (C.A.) | | | | | | | | |

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | Core Angles : | | | | | | | | |
| | Faults / Fractures = 150.00 m : 60° 153.80 : " | | | | | | | | |
| 169.20 - 181.70 | Dacitic Ash-lapilli tuff - medium bluish grey matrix, with ~30% angular fragments of mostly sericitized dacite, and minor argillite, tr py fragments - minor irregular Qtz-carb. veinlets, tr diss py 169.20 - 169.70 : gradational upper contact, with decreasing brecciation and alteration 169.70 - 170.00 : fault zone, rubble, limonite stained 170.00 - 171.5 : weakly altered bleached section, light greenish grey, with minor limonite stained fractures at 40-50° to core axis. | | | | | | | | |
| 181.70 - 193.20 | Very fine "Andesitic" dike rock - light bluish grey, aphanitic, weakly silicified - pervasive stockwork fracture veinlets with diffuse pyrite/carb. infilling, - overall 2-3% py - upper contact at very low core angle, from 181.20 - 182.00, with a .5 cm wide py-Qtz-carb vein along contact - lower contact at ~60° to core axis | | | | | | | | |

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---------------------------|---|---------------|---------|-------|---------|-----|--------|-----|-----|-----|--------|-----|---|-----|--------|-----|---|-----|--------|-----|---|--|--|--|--|--|--|--|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. | | | | | | | | | | | | | | | | | | | |
| 193.20 - 209.20 | <p>Argillite</p> <ul style="list-style-type: none"> - massive to weakly foliated, with minor siltstone laminae - overall contains 2-3% qtz-carb veinlets & crackle breccia filling. - minor healed fault disrupted bedding. - 1-2% py as blebs & stringers <p>198.40 - 198.65 : graphitic gouge.</p> <p>206.50 - 209.20 : minor bands of dissem. py // to bedding.</p> <p>207.50 - 208.50 : fault zone; rubblely carb & graphitic gouge.</p> <table border="0" style="margin-left: 100px;"> <tr><td>CA.</td><td>196.00</td><td>36°</td><td>bedding</td></tr> <tr><td>CA.</td><td>198.50</td><td>64°</td><td>"</td></tr> <tr><td>CA.</td><td>203.20</td><td>30°</td><td>"</td></tr> <tr><td>CA.</td><td>206.00</td><td>37°</td><td>"</td></tr> <tr><td>CA.</td><td>207.90</td><td>60°</td><td>"</td></tr> </table> | CA. | 196.00 | 36° | bedding | CA. | 198.50 | 64° | " | CA. | 203.20 | 30° | " | CA. | 206.00 | 37° | " | CA. | 207.90 | 60° | " | | | | | | | |
| CA. | 196.00 | 36° | bedding | | | | | | | | | | | | | | | | | | | | | | | | | |
| CA. | 198.50 | 64° | " | | | | | | | | | | | | | | | | | | | | | | | | | |
| CA. | 203.20 | 30° | " | | | | | | | | | | | | | | | | | | | | | | | | | |
| CA. | 206.00 | 37° | " | | | | | | | | | | | | | | | | | | | | | | | | | |
| CA. | 207.90 | 60° | " | | | | | | | | | | | | | | | | | | | | | | | | | |
| 209.20 - 222.40 | <p>Massive Andesite / Dacite</p> <ul style="list-style-type: none"> - massive fine to medium fine grained, light olive to olive grey (5Y 5/2 ↔ 5Y 7/2) - brecciated upper contact with volcanic & argillite fragments - overall contains 5-6% py as fine grained disseminations, coarser blebs within quartz-carbonate veinlets, fracture fillings and as arborescent impregnations often peripheral to healed fractures - contains abundant very fine chalky white equant (epidote?) xtls, possible carbonate amygdalae with chloritic rims, occasional x-cutting carb. vnlts at CA's ≤ 25° (generally < 4mm dia and occasional qtz vnlts ≤ 1cm dia with pyritic | | | | | | | | | | | | | | | | | | | | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

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Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | selvages at CA's $\leq 25^\circ$ | | | | | | | | |
| 209.50 - 211.00 | brecciated, silica-flooded interval with ~10% py. | | | | | | | | |
| 211.00 - 212.50 | 5-7% py mainly as fracture fillings (fractures at shallow CA's) | | | | | | | | |
| 212.50 - 217.05 | ~2% py | | | | | | | | |
| 217.05 - 218.53 | mildly bxd interval with ~5% py as fracture fillings, disseminations & blebs within qtz-carb vnlts. Includes 217.45 - 217.70 a 1cm wide smokey qtz-carb-py vnlts at 15° core angle. | | | | | | | | |
| 218.53 - 219.75 | 1-3% py | | | | | | | | |
| 219.75 - 220.45 | fault zone in bxd bleached interval with qtz-py veining. Overall contains ~15% py & trasp. | | | | | | | | |
| 220.45 - 222.40 | bxd, mildly silicified interval with 10-15% py as impregnations, fracture fillings & coarser blebs in quartz fracture infilling. | | | | | | | | |
| 222.40 - 236.0 | Welded Dacite ash-lapilli Tuff - greenish grey (5-6% $\frac{1}{4}$) dacitic fragments composed of at least 20% lapilli-sized volcanic fragments of dacitic to andesitic composition in a fine ash groundmass. - fragments vary from angular to flattened, chloritic &/or sericitic wispy and aligned so as to give a foliated appearance probably indicative of bedding. | | | | | | | | |

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. |
| 223.4 - 224.6 | : medium grey (N5) to medium dark grey (N4) composed of angular fragments of massive andes/dacite (similar to 220.45 - 222.40) in a quartz-carb groundmass. - contains ~10% py in the quartz carb fracture filling. - chloritic rims around fragments - fracture set at ~45° to core axis & another set haphazardly oriented. | | | | | | | |
| 224.6 - 236.0 | : fractures with chloritic coating { 2-3% py, oriented ~30° to core axis. | | | | | | | |
| 224.6 - 226.4 | : "bedding" at ~40° to core axis. | | | | | | | |
| 236.4 - 230.73 | : increased chloritic micro fractures, randomly oriented, thin calcite veins (<1mm dia, oriented ≤ 25° to core axis) | | | | | | | |
| 236.00 - 244.68 | Massive Andesite (Dike?) - greenish black (SG 3/1) (236.0 → 240.30), greyish black (N2) (240.3 → 241.30), to dark greenish grey (SG 4/1) (241.30 - 244.68), massive fine grained with occasional inclusions of welded tuff. - contains two sets of thin calcite veins; one oriented 70° to core axis & the other at ≤ 25° to core axis. | | | | | | | |
| 236.00 - 240.30 | : carbonate alteration - lower contact is fault w rubble core & gouge. | | | | | | | |

13 of 17

Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 244.68 - 267.16 | Welded Dacite ash-lapilli Tuff | | | | | | | | |
| | - greenish grey (5GY 6/1) volcanic fragmental rock similar to 222.4 - 223.4 except lapilli fragments have decreased to ~10% | | | | | | | | |
| | - contains ≤ 2% py as fine fracture fillings & sparse disseminations | | | | | | | | |
| | - bedding indicated by tiamme is consistently around 50° to core axis. | | | | | | | | |
| | - minor interflow volcanic mudstone units varying from 2 to 6 m wide, composed of dacitic welded tuff fragments in an argillaceous matrix (fragments commonly angular). | | | | | | | | |
| | mudstone interbeds ; | | | | | | | | |
| | 244.68 - 245.80 | | | | | | | | |
| | 248.82 - 249.18 | | | | | | | | |
| | 249.60 - 250.00 bedding CA ~ 60° | | | | | | | | |
| | 250.17 - 250.60 bedding CA ~ 50° | | | | | | | | |
| | 250.74 - 250.87 | | | | | | | | |
| | 251.00 - 251.30 | | | | | | | | |
| 255.00 - 258.45 | FAULT ZONE | | | | | | | | |
| | 255.00 - 255.22 ; broken core | | | | | | | | |
| | 255.22 - 257.95 : brecciated bleached interval, light olive to pale yellowish grey (5Y 7/2 ↔ 5Y 7/1) | | | | | | | | |
| | 255.50 - 255.80 : 3-5% py as blebs & fine arborescent growths | | | | | | | | |
| | 255.80 - 256.80 : tr py, abundant fine discontinuous, haphazardly oriented qtz-carb vnlts generally < 3 mm dia | | | | | | | | |

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | 256.80 - 257.95 : broken core plus minor white gouge, minor thin pyritic vnlts | | | | | | | | |
| | 257.95 - 258.45 : fractured core, fracture set at ~ 60° to core axis. | | | | | | | | |
| | 259.95 - 260.29 : broken core, minor thin pyritic vnlts. | | | | | | | | |
| | C.A. 261.0 m : 50° bedding. | | | | | | | | |
| | C.A. 263.0 m : 43° bedding. | | | | | | | | |
| | CA. 267.0 m : 45° bedding. | | | | | | | | |
| 267.16 - 273.23 | Massive Andesite. - fine to medium fine, grayish black (N2) to olive grey (5Y 4/1), massive volcanic rock of andesitic to dacitic (finer grained portions) composition. - overall contains ≤ 1-2% py - upper contact cuts bedding at a core angle of ~ 45° across bedding so as to indicate that this unit is likely a dike, oriented vertically and trending across the drill section at ~ Az 035 to Az 045 - brecciated and contains abundant thin haphazardly oriented tensional qtz vnlts, with chloritic selvages, generally < 2 mm dia. 270.60 - 270.80 : qtz-chl-py vnlts ≤ 1cm dia @ 20° to core axis, contains abundant coarse py. 272.90 - 273.23 : bleached foliated lower contact : CA 34° (shearing) | | | | | | | | |

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Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 273.23 - 277.35 | Black Argillite - a generally fine grained black massive rock with occasional light grey tuffaceous laminae within 1.0 m of upper contact, laminae generally \leq 1 cm dia. - occasional tuffaceous mudstone intervals with sparse felsic volcanic fragments up to 20 mm dia in black argillite matrix. - Contains 1-3% py, overall as disseminations & stringers plus in minor submm sized qtz veinlets. | | | | | | | | |
| 273.63 - 277.35 | Fault Zone; broken rubble core plus gouge. | | | | | | | | |
| 275.73 - 276.00 | graphitic, clayey gouge plus fine qtz chips. | | | | | | | | |
| 276.00 - 277.35 | numerous thin qtz-py vugs, haphazardly oriented & ptigmatically folded, overall interval contains ~2-3% fine py. | | | | | | | | |
| | CA. 276.10 m : 23° shearing. | | | | | | | | |
| | 276.50 m : 45° shearing. | | | | | | | | |
| | 277.00 m : 45° shearing. | | | | | | | | |
| 277.35 - 279.49 | Fossiliferous Greywacke - a medium grained, dark grey arenite with white carbonate pebbled fossils and occasional argillite chips & interbeds. | | | | | | | | |

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Hole No. Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | 277.35 - 279.49 : Fault Zone ; broken , rubble core , chips & gouge. | | | | | | | | |
| | 277.35 - 279.20 : brecciated interval with discontinuous haphazardly oriented quartz units , overall ~ 3% py plys a dark colored sulfide in an intensely qtz-veined interval 278.4-279.2 | | | | | | | | |
| 279.49 - 285.20 | Interbedded Black Argillite & Siltstone - consists of massive black argillite (as in interval 273.23 - 277.35) interbedded with lighter grey siltstone beds up to ~ 4 cm wide ; contains minor pyritic horizons & thin concordant qtz veins up to 25 mm wide usually associated with small shears. | | | | | | | | |
| | 284.40 - 285.20 : fault zone ; broken core , chips & gouge toward bottom of interval. | | | | | | | | |
| | CA. 279.99 : 50° bedding. | | | | | | | | |
| | CA. 283.93 : 50° bedding. | | | | | | | | |
| 285.20 - 306.91 | Fossiliferous Greywacke a generally medium to medium dark grey arenite with fairly abundant light colored calcareous pelecypod plus other (?) fossils , argillitic rip-up clasts , gritty interbeds & rip-up clasts - gritty interbeds are generally ~ 60 cm or less in dia while argillaceous bands vary up to ~ 2 m wide. | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP8 Co ord Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. ppb | Ag. ppm | Cu. | Zn. | As ppm | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|------------|------------|-----|-----|-----------|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | |
| 162.50 - 163.00 | 1885-G | 0.5 | 3 | 1.4 | | | 9 | | | | | | | | | | | | | |
| 163.00 - 163.50 | 1886-G | 0.5 | 4 | .2 | | | 5 | | | | | | | | | | | | | |
| 163.50 - 164.00 | 1887-G | 0.5 | 19 | .5 | | | 13 | | | | | | | | | | | | | |
| 164.00 - 164.50 | 1888-G | 0.5 | 7 | .2 | | | 6 | | | | | | | | | | | | | |
| 164.50 - 165.00 | 1889-G | 0.5 | 3 | .4 | | | 7 | | | | | | | | | | | | | |
| 165.00 - 165.50 | 1890-G | 0.5 | 10 | .2 | | | 6 | | | | | | | | | | | | | |
| 165.50 - 166.00 | 1891-G | 0.5 | 2 | .4 | | | 12 | | | | | | | | | | | | | |
| 166.00 - 166.50 | 1892-G | 0.5 | 5 | .7 | | | 8 | | | | | | | | | | | | | |
| 166.50 - 167.00 | 1893-G | 0.5 | 7 | 1.6 | | | 21 | | | | | | | | | | | | | |
| 167.00 - 167.50 | 1894-G | 0.5 | 1 | .6 | | | 10 | | | | | | | | | | | | | |
| 167.50 - 168.00 | 1895-G | 0.5 | 4 | .1 | | | 12 | | | | | | | | | | | | | |
| 168.00 - 168.50 | 1896-G | 0.5 | 3 | .6 | | | 11 | | | | | | | | | | | | | |
| 168.50 - 169.00 | 1897-G | 0.5 | 5 | .8 | | | 12 | | | | | | | | | | | | | |
| 169.00 - 169.50 | 1898-G | 0.5 | 1 | .3 | | | 4 | | | | | | | | | | | | | |
| 169.50 - 170.00 | 1899-G | 0.5 | 8 | .9 | | | 10 | | | | | | | | | | | | | |
| 170.00 - 170.50 | 1900-G | 0.5 | 7 | 1.4 | | | 35 | | | | | | | | | | | | | |
| 170.50 - 171.00 | 1901-G | 0.5 | 18 | 2.8 | | | 22 | | | | | | | | | | | | | |
| 171.00 - 171.50 | 1902-G | 0.5 | 8 | 1.4 | | | 21 | | | | | | | | | | | | | |
| 171.50 - 172.00 | 1903-G | 0.5 | 16 | 1.9 | | | 14 | | | | | | | | | | | | | |
| 172.00 - 172.50 | 1904-G | 0.5 | 27 | 2.2 | | | 187 | | | | | | | | | | | | | |
| 172.50 - 173.00 | 1905-G | 0.5 | 4 | 1.5 | | | 18 | | | | | | | | | | | | | |
| 173.00 - 173.50 | 1858-G | 0.5 | 16 | 1.8 | | | 13 | | | | | | | | | | | | | |
| 173.50 - 181.00 | WASTE | 7.5 | — | — | | | — | | | | | | | | | | | | | |
| 181.00 - 181.50 | 1906-G | 0.5 | 41 | 2.3 | | | 13 | | | | | | | | | | | | | |
| 181.50 - 182.00 | 1907-G | 0.5 | 85 | 5.8 | | | 143 | | | | | | | | | | | | | |
| 182.00 - 182.50 | 1908-G | 0.5 | 77 | 4.2 | | | 467 | | | | | | | | | | | | | |
| 182.50 - 183.00 | 1909-G | 0.5 | 54 | 3.4 | | | 181 | | | | | | | | | | | | | |
| 183.00 - 183.50 | 1910-G | 0.5 | 30 | 3.6 | | | 77 | | | | | | | | | | | | | |
| 183.50 - 184.00 | 1911-G | 0.5 | 5 | .1 | | | 25 | | | | | | | | | | | | | |
| 184.00 - 184.50 | 1912-G | 0.5 | 8 | .7 | | | 22 | | | | | | | | | | | | | |
| 184.50 - 185.00 | 1913-G | 0.5 | 6 | .4 | | | 18 | | | | | | | | | | | | | |
| 185.00 - 185.50 | 1914-G | 0.5 | 7 | 1.9 | | | 23 | | | | | | | | | | | | | |
| 185.50 - 186.00 | 1915-G | 0.5 | 4 | .6 | | | 14 | | | | | | | | | | | | | |
| 186.00 - 186.50 | 1916-G | 0.5 | 5 | .8 | | | 11 | | | | | | | | | | | | | |
| 186.50 - 187.00 | 1917-G | 0.5 | 2 | .6 | | | 21 | | | | | | | | | | | | | |
| 187.00 - 187.50 | 1918-G | 0.5 | 3 | 1.4 | | | 35 | | | | | | | | | | | | | |
| 187.50 - 188.00 | 1919-G | 0.5 | 2 | .7 | | | 16 | | | | | | | | | | | | | |
| 188.00 - 188.50 | 1920-G | 0.5 | 4 | .4 | | | 18 | | | | | | | | | | | | | |
| 188.50 - 189.00 | 1921-G | 0.5 | 3 | .6 | | | 14 | | | | | | | | | | | | | |
| 189.00 - 189.50 | 1922-G | 0.5 | 8 | 3.0 | | | 39 | | | | | | | | | | | | | |


**GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD**

Hole No. AP8 Co. ord. Horizontal Length Date Completed

Claim No. Core Size Drilled By

Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au | Ag | Cu | Zn | As | WIDTH X ASSAY | | | | | | | | AVERAGES | | | | |
|---------------------------|--------|-------|-----|-----|----|----|-----|---------------|----|----|----|----|----|-----|-----|----------|-----|--|--|--|
| | | | | | | | | WIDTH | Au | Ag | Cu | Zn | As | ... | ... | ... | ... | | | |
| 220.90 - 221.20 | 1955-G | 0.3 | 85 | 3.8 | | | 328 | | | | | | | | | | | | | |
| 221.20 - 221.50 | 1956-G | 0.3 | 124 | 6.9 | | | 503 | | | | | | | | | | | | | |
| 221.50 - 221.80 | 1851-G | 0.3 | 134 | 7.7 | | | 658 | | | | | | | | | | | | | |
| 221.80 - 222.10 | 1852-G | 0.3 | 145 | 7.6 | | | 447 | | | | | | | | | | | | | |
| 222.10 - 222.40 | 1853-G | 0.3 | 185 | 8.7 | | | 457 | | | | | | | | | | | | | |
| 222.40 - 222.85 | 1957-G | 0.45 | 21 | .8 | | | 32 | | | | | | | | | | | | | |
| 222.85 - 223.40 | 1958-G | 0.55 | 11 | .4 | | | 9 | | | | | | | | | | | | | |
| 223.40 - 223.70 | 1854-G | 0.3 | 57 | 1.8 | | | 305 | | | | | | | | | | | | | |
| 223.70 - 224.00 | 1855-G | 0.3 | 192 | 5.9 | | | 823 | | | | | | | | | | | | | |
| 224.00 - 224.30 | 1856-G | 0.3 | 137 | 5.0 | | | 714 | | | | | | | | | | | | | |
| 224.30 - 224.60 | 1857-G | 0.3 | 105 | 4.2 | | | 289 | | | | | | | | | | | | | |
| 224.60 - 225.10 | 1959-G | 0.5 | 11 | .4 | | | 16 | | | | | | | | | | | | | |
| 225.10 - 226.50 | WASTE | 1.4 | | | | | | | | | | | | | | | | | | |
| 226.50 - 227.00 | 1960-G | 0.5 | 9 | .3 | | | 5 | | | | | | | | | | | | | |
| 227.00 - 227.50 | 1961-G | 0.5 | 3 | .3 | | | 5 | | | | | | | | | | | | | |
| 227.50 - 228.30 | WASTE | 0.8 | | | | | | | | | | | | | | | | | | |
| 228.30 - 228.80 | 1962-G | 0.5 | 2 | .3 | | | 8 | | | | | | | | | | | | | |
| 228.80 - 229.30 | 1963-G | 0.5 | 1 | .3 | | | 2 | | | | | | | | | | | | | |
| 229.30 - 229.80 | 1964-G | 0.5 | 5 | .3 | | | 6 | | | | | | | | | | | | | |
| 229.80 - 230.00 | WASTE | 5.2 | | | | | | | | | | | | | | | | | | |
| 230.00 - 230.50 | 1965-G | 0.5 | 9 | .1 | | | 6 | | | | | | | | | | | | | |
| 230.50 - 230.80 | 1966-G | 0.5 | 2 | .1 | | | 4 | | | | | | | | | | | | | |
| 230.80 - 231.00 | 1967-G | 0.5 | 2 | .2 | | | 2 | | | | | | | | | | | | | |
| 231.00 - 243.80 | WASTE | 7.3 | | | | | | | | | | | | | | | | | | |
| 243.80 - 244.30 | 1968-G | 0.5 | 1 | .4 | | | 19 | | | | | | | | | | | | | |
| 244.30 - 244.67 | 1969-G | 0.37 | 3 | .3 | | | 10 | | | | | | | | | | | | | |
| 244.67 - 244.96 | 1970-G | 0.29 | 1 | .2 | | | 10 | | | | | | | | | | | | | |
| 244.96 - 245.46 | 1971-G | 0.5 | 3 | .2 | | | 13 | | | | | | | | | | | | | |
| 245.46 - 245.96 | 1972-G | 0.5 | 10 | .3 | | | 10 | | | | | | | | | | | | | |
| 245.96 - 246.46 | 1973-G | 0.5 | 2 | .2 | | | 9 | | | | | | | | | | | | | |
| 246.46 - 246.96 | 1974-G | 0.5 | 6 | .5 | | | 15 | | | | | | | | | | | | | |
| 246.96 - 247.46 | 1975-G | 0.5 | 4 | .4 | | | 11 | | | | | | | | | | | | | |
| 247.46 - 254.50 | WASTE | 7.04 | | | | | | | | | | | | | | | | | | |
| 254.50 - 255.00 | 1976-G | 0.5 | 5 | 1.4 | | | 15 | | | | | | | | | | | | | |
| 255.00 - 255.50 | 1977-G | 0.5 | 7 | 1.2 | | | 19 | | | | | | | | | | | | | |
| 255.50 - 255.80 | 1978-G | 0.3 | 15 | .6 | | | 10 | | | | | | | | | | | | | |
| 255.80 - 256.30 | 1979-G | 0.5 | 4 | .1 | | | 2 | | | | | | | | | | | | | |
| 256.30 - 256.80 | 1980-G | 0.5 | 11 | .1 | | | 2 | | | | | | | | | | | | | |
| 256.80 - 257.45 | 1981-G | 0.65 | 2 | .1 | | | 7 | | | | | | | | | | | | | |
| 257.45 - 257.95 | 1982-G | 0.5 | 10 | .2 | | | 7 | | | | | | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP8 Co ord Horizontal Length Date Completed
Claim No Core Size Drilled By
Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. | Ag. | Cu. | Zn. | As | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|-----|-----|-----|-----|----|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | |
| 257.95 - 258.45 | 1983-G | 0.50 | 17 | .3 | | | 13 | | | | | | | | | | | | | |
| 258.45 - 258.95 | 1984-G | 0.50 | 19 | .4 | | | 64 | | | | | | | | | | | | | |
| 258.95 - 259.45 | 1985-G | 0.50 | 11 | .6 | | | 3 | | | | | | | | | | | | | |
| 259.45 - 259.95 | 1986-G | 0.50 | 6 | .3 | | | 3 | | | | | | | | | | | | | |
| 259.95 - 260.40 | 1987-G | 0.45 | 6 | 1.7 | | | 5 | | | | | | | | | | | | | |
| 260.40 - 260.90 | 1988-G | 0.50 | 15 | .4 | | | 6 | | | | | | | | | | | | | |
| 260.90 - 266.66 | WASTE | 5.76 | | | | | | | | | | | | | | | | | | |
| 266.66 - 267.16 | 1989-G | 0.50 | 7 | .1 | | | 2 | | | | | | | | | | | | | |
| 267.16 - 267.66 | 1990-G | 0.50 | 6 | .5 | | | 9 | | | | | | | | | | | | | |
| 267.66 - 268.10 | 1991-G | 0.44 | 3 | .3 | | | 33 | | | | | | | | | | | | | |
| 268.10 - 268.55 | 1992-G | 0.45 | 4 | .2 | | | 9 | | | | | | | | | | | | | |
| 268.55 - 269.45 | 1993-G | 0.90 | 2 | .4 | | | 21 | | | | | | | | | | | | | |
| 269.45 - 269.80 | 1994-G | 0.35 | 3 | .5 | | | 26 | | | | | | | | | | | | | |
| 269.80 - 270.20 | 1995-G | 0.40 | 5 | .1 | | | 14 | | | | | | | | | | | | | |
| 270.20 - 270.60 | 1996-G | 0.40 | 4 | .1 | | | 4 | | | | | | | | | | | | | |
| 270.60 - 270.80 | 1997-G | 0.20 | 5 | .2 | | | 9 | | | | | | | | | | | | | |
| 270.80 - 271.00 | 1998-G | 0.20 | 14 | .5 | | | 10 | | | | | | | | | | | | | |
| 271.00 - 271.50 | 1999-G | 0.50 | 2 | .1 | | | 10 | | | | | | | | | | | | | |
| 271.50 - 271.95 | 2000-G | 0.45 | 20 | .6 | | | 16 | | | | | | | | | | | | | |
| 271.95 - 272.40 | 2001-G | 0.45 | 5 | .1 | | | 2 | | | | | | | | | | | | | |
| 272.40 - 272.90 | 2002-G | 0.50 | 1 | .1 | | | 2 | | | | | | | | | | | | | |
| 272.90 - 273.23 | 2003-G | 0.33 | 24 | .1 | | | 19 | | | | | | | | | | | | | |
| 273.23 - 273.63 | 2004-G | 0.40 | 23 | 1.6 | | | 88 | | | | | | | | | | | | | |
| 273.63 - 274.00 | 2005-G | 0.37 | 18 | 1.6 | | | 44 | | | | | | | | | | | | | |
| 274.00 - 274.50 | 2006-G | 0.50 | 9 | 2.8 | | | 45 | | | | | | | | | | | | | |
| 274.50 - 275.00 | 2007-G | 0.50 | 8 | 2.2 | | | 44 | | | | | | | | | | | | | |
| 275.00 - 275.50 | 2008-G | 0.50 | 13 | 1.4 | | | 31 | | | | | | | | | | | | | |
| 275.50 - 276.10 | 2009-G | 0.60 | 4 | .4 | | | 41 | | | | | | | | | | | | | |
| 276.10 - 276.44 | 2010-G | 0.34 | 17 | .1 | | | 33 | | | | | | | | | | | | | |
| 276.44 - 276.80 | 2011-G | 0.36 | 5 | .2 | | | 41 | | | | | | | | | | | | | |
| 276.80 - 277.35 | 2012-G | 0.55 | 16 | .3 | | | 48 | | | | | | | | | | | | | |
| 277.35 - 277.80 | 2013-G | 0.45 | 11 | .2 | | | 42 | | | | | | | | | | | | | |
| 277.80 - 278.40 | 2014-G | 0.60 | 7 | .2 | | | 22 | | | | | | | | | | | | | |
| 278.40 - 279.20 | 2015-G | 0.80 | 13 | .1 | | | 34 | | | | | | | | | | | | | |
| 279.20 - 279.49 | 2016-G | 0.29 | 11 | .2 | | | 26 | | | | | | | | | | | | | |
| 279.49 - 279.99 | 2017-G | 0.50 | 11 | .1 | | | 24 | | | | | | | | | | | | | |
| 279.99 - 306.93 | ECH | 26.94 | | | | | | | | | | | | | | | | | | |

Hole No. AP-9 Co. ord. 1117 N Horizontal Length Date Completed Sept 3/90
 Claim No. UNUK 26 258 W Core Size BGBDM Drilled By J.T. THOMAS
 Grid No. ZONE 1 Angle & Direction -50/A2080 Elevation 1390m Logged By ROSS ZAWADA

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 0.0m → 6.10 | - CASING | | | | | | | | |
| 6.10 → 215.11 | : Welded Dacite Tuff - greenish grey (5 to 6%) to dark grey (M3) with a mottled appearance due to varying degrees of alteration. - 20-30% lapilli sized fragments that are obliterated to varying degrees due to alteration - moderate to highly silicified - chlorite filled tension gashes, 1-2mm wide and ≈ 55° to CORE AXIS (CA) - carbonate filled fractures, 4mm to 5mm wide, at ≈ 50° → 80° to CA. | | | | | | | | |
| 6.10 → 16.90 | - Shattered CORE - 10.66 → 11.27 - .45m extra CORE in shattered fragments due to material sloughing back down hole. - 11.27 → 14.33 - 45% Recovery - 14.33 → 16.90 - 22% Recovery | | | | | | | | |
| 16.90 → 20.0 | - high concentration of chl. filled fractures, 75/m - py 7-10% with Tr sph and Tr Aspy - silica flooding and brecciation (crackle breccia) - moderate → high sericitization - 16.90-17.37, 7-10% py, Tr -1% Aspy, Tr Sph. - 17.37-18.00, 1-2% py, Tr Aspy, Tr Sph - 18.0-20.0, 10% py, Tr Aspy, Tr Sph | | | | | | | | |

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

20,390


GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP 9 Co ord. _____ Horizontal Length _____ Date Completed Sept 3, 190
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By Ross Zawada

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 6.10-215.11 (cont'd) | 22.55 - 23.42 - black to greenish black dacite tuff - moderately silicified - carbonate filled fractures at 60°-80° to CA | | | | | | | | |
| | 24.30 - carbonate veinlet at 60° to CA | | | | | | | | |
| | 24.97 - carbonate veinlet, 7mm wide at 60° to CA | | | | | | | | |
| | 24.97-25.14 - zone of brecciation with quartz and carbonate flooding - weak hydrothermal alteration - Tc py | | | | | | | | |
| | 25.90-26.40 - lesser degree of alteration, resulting in a darker black color. - carbonate filled veinlets at 70° and 11 to CA. | | | | | | | | |
| | 28.55 - chlorite filled tension gashes at 70° to CA | | | | | | | | |
| | 33.64 - fracture at 55° to CA, slickensides at 50° S | | | | | | | | |
| | 37.36 - fracture at 45° to CA, slickensides at 10° to CA | | | | | | | | |
| | 39.59 - carbonate veinlet, 4mm wide at 50° to CA | | | | | | | | |
| | 40.72 - fracture at 45° to CA - py, chl, and carbonate on fracture surface. | | | | | | | | |
| | 41.76-42.26 - chl filled tension gashes at 70° to CA | | | | | | | | |
| | 41.30 - 47.85 - lesser degree of alteration expressed as a greenish black to black color. | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP9 Co. ord. Horizontal Length Date Completed Sept. 3/90
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By Ross ZAWADA

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 610-815.11 (cont'd) | 47.85-51.0 - greenish grey dacite with chlorite filled tension gashes at - 11 to CA - 4 to CA - 20 to CA | | | | | | | | |
| | 51.0-57.82 - black, less altered dacite - 54.05 - carbonate veinlet at 40 to CA - 54.23 - fracture at 35 to CA, chl + py on fracture surface - 54.89 - carbonate veinlet at 35 to CA | | | | | | | | |
| | 57.82-75.5 - greenish grey dacite - 59.4 - chl. filled tension gashes at 60 to CA - 60.3 - chl. filled tension gashes at 70 to CA - 60.8 - chl. filled tension gashes at 75 to CA - 64.8 - carbonate veinlet, 4mm wide at 20 to CA - 65.8 - chl. filled tension gashes at 75 to CA, displaced by carbonate veinlet at 15 to CA - 72.74 carbonate veinlet 30mm wide at 10 to CA | | | | | | | | |
| | 75.5-78.93 - back into dacite, less altered rock | | | | | | | | |
| | 78.93 - back into greenish grey color | | | | | | | | |
| | 84.11-84.4 - zone of hydrothermal alteration with leached reaction rims around fragments. - chl. filled tension gashes at 65 to CA | | | | | | | | |
| | 84.53 - carbonate veinlets 1mm-3mm // to CA | | | | | | | | |
| | 89.0-89.93 - chl. filled tension gashes sub // to CA, displaced on a mm scale by 1-2mm quartz veinlets at 50 to CA | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP 9 Co. ord. _____ Horizontal Length _____ Date Completed Sept. 3/90
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By Ross Zambora

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 8.10-215.11 (cont'd) | 91.65-95.70 - shear zone with quartz flooded brecciation - 91.85-91.95 - gouge - high degree of silicification across shear (except gouge) - hydrothermal alteration throughout, but most intense from 94.08-94.70 - foliation at 60° to CA - lithic mudstone unit at 92.56-93.36 with ≈ 30-40% dacite fragments - Tr pyrite | | | | | | | | |
| | 96.3-101.06 - greenish grey dacite rock with chl. filled tension gashes at 10-40° to CA 98.71-99.82 - shear with carbonate alteration - shattered core and gouge from 99.08-99.63 | | | | | | | | |
| | 101.76-102.51 - shattered core - fol. at 50° to CA, taken from larger fragments | | | | | | | | |
| | 102.51-120.71 - greenish grey dacite tuff with occasional carbonate veinlets at 50-70° to CA - high degree of silicification - flame giving a foliation at 40° to CA - mottled appearance - feldspar (Plagioclase) phenocrysts; euhedral-subhedral, 1-5mm across. | | | | | | | | |
| | 120.71-124.63 - shattered core - larger fragments show fol. // → sub // to CA | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP9 Co ord. Horizontal Length Date Completed Sept 31 90
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By ROSS ZANADA

| INTERNAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 6.10-215.11 (cont'd) | 129.63 - 135.45 - 2-4% feldspar phenocrysts - decrease in silicification - 129.30 - fiamme @ 11 to CA - 133.40 - fiamme at 20° to CA | | | | | | | | |
| | 135.45 - 154.98 - no feldspar phenocrysts - higher degree of welding - continues to be a lesser degree of silicification 138.10 - fiamme at 30° to CA 140.21 - 141.29 - shattered core 141.44 - fiamme at 20° to CA 142.77 - 143.24 - shattered core 147.19 - carbonate filled fractures \leq 1mm at 45° to CA - fiamme at 20° to CA 149.14 - 149.44 - py filled fractures at 70° to CA - fiamme at 20° to CA | | | | | | | | |
| | 154.98 - back into the feldspar phenocrysts | | | | | | | | |
| | 154.98 - 156.31 - lesser degree of welding | | | | | | | | |
| | 156.31 - 169.62 - intensely welded with fiamme giving foliation from 11 to 30° to CA - 163.4 carbonate filled fractures at 40° to CA - 163.97 - fiamme at 30° to CA - 164.10 - carbonate filled fractures at 70° to CA - 165.95 - 166.85 - shattered core - 167.44 - carb filled fractures at 70° to CA - 167.64 - fiamme at 11 to CA - 168.8 - carbonate filled fractures at 30° to CA | | | | | | | | |



GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP 9 Co ord. _____ Horizontal Length _____ Date Completed Sept 3/90
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By ROSS ZANADA

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 6.10 - 215.11 (cont'd) | 169.62 - 203.88 - lesser degree of welding - increase in chloritization - still in feldspar phenocrysts 171.89 - carbonate filled fracture at 25° to CA 172.85 - carbonate filled fracture at 70° to CA 173.23 - 173.59 - shattered core 173.97 - 174.12 - shattered core 177.10 - 179.11 - more intensely welded 178.6 - 178.78 - shattered core 179.68 - 180.13 - carbonate filled fractures at 80° to CA 181.87 - carbonate filled fracture at 25° to CA 186.67 - carbonate filled fractures at 50° to CA 187.54 - fracture at 45° to CA, py on fracture surfaces 191.0 - 191.59 - 1% py located in fractures and as fine ground disseminations throughout the rock. 192.27 - 193.08 - increase in density of carbonate filled fractures ≤ 15/100mm at 30° and 60° to CA 194.16 - 197.21 - mismatch resulting in 72% core recovery 198.0 - 198.18 - shattered core. 200.25 - calc filled fracture at 75° to CA 200.80 - carbonate filled fracture at 30° to CA 201.89 - 202.96 - shattered core. | | | | | | | | |
| | 203.88 - 213.44 - color change back to greenish grey - higher degree of welding 211.80 flame at 25° to CA | | | | | | | | |
| | 213.44 - 215.11 - sheared volcanics with a strong foliation at 40° to CA - some fragments highly chloritized - strongly sericitized throughout - Tr py locally - contact with 1.5" mudstone at ≈ 214.51 - 214.63 - 214.87, shattered core with gouge from 214.78 - 214.84 | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP9 Co ord. _____ Horizontal Length _____ Date Completed Sept 3 190
Claim No. _____ Core Size _____ Drilled By _____
Grid No. _____ Angle & Direction _____ Elevation _____ Logged By ROSS ZAWADA

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 215.11 → 238.05 | <ul style="list-style-type: none"> : Intercalated beds of dacite welded tuff and lithic mudstones and occasional argillite horizons - lithic mudstone is matrix supported with 10 → 70% angular to sub-angular fragments - fragments range in size from 1mm → 100mm and are moderately to highly sericitized - fragments have a moderate lineation of 40° to CA - py is found throughout the section in quantities ranging from 1r → 10% - 1r-1% Aspy and Tr Sph found locally | | | | | | | | |
| 215.23 - 215.48 | <ul style="list-style-type: none"> - dacite ash flow - highly sericitized - very weak carbonate alteration | | | | | | | | |
| 215.48 - 215.90 | <ul style="list-style-type: none"> - lithic mudstones with ≈ 30% fragments - upper contact at 70° to CA - lower contact at 55° to CA - ≈ 1-2% py replacing portions of or entire fragments | | | | | | | | |
| 215.90 - 216.92 | <ul style="list-style-type: none"> - dacite tuff - strong foliation at 40° to CA - high degree of sericitization from 215.90-216.06 - moderate sericitization through the rest of the interval - 215.83 quartz-carbonate vein, 14mm wide at 50° to CA vein contains fractures 1-3mm wide filled with a black mineral (Silicate?), fractures are ≈ 11 to CA and concentrated in the vein but do extend out into the host rock. - Tr py throughout the interval; somewhat more abundant in the "black" fractures | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP9 Co ord. Horizontal Length Date Completed Sept. 2/90
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By Ross F. MORA

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-----------------------------|---|---------------|--------|-------|--------|------------|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. ppm | Ag. | Cu. | Zn. |
| 215.11 - 238.05 (cont'd) | | | | | | | | | |
| | 216.92 - 227.19 | | | | | | | | |
| | - 216.92 - 219.55 - Lithic mudstone with ~20% fragments | | | | | | | | |
| | - 3-5% py, concentrated primarily in fragments | | | | | | | | |
| | - fragments moderately silicified | | | | | | | | |
| | - 218.50 - band of py 5mm wide at 30° to CA | 218.50 | 219.55 | .50 | | 787 | 6.6 | | |
| | | 219.55 | 220.05 | .50 | | 3298 | 8.2 | | |
| | - 219.55 - 220.10 - pegillite | | | | | | | | |
| | - moderately to highly silicified with small quartz veinlets throughout. Veining most intense at upper & lower contacts | | | | | | | | |
| | - upper contact - sulfide mineralisation and quartz veining. 5-6mm wide at 40° to CA | | | | | | | | |
| | - lower contact, quartz and carbonate veining 40mm wide at 35° to CA | | | | | | | | |
| | - py ranges from v.l.g. to euhedral stals 3mm across | | | | | | | | |
| | - Aspy, 3-5% in vein | | | | | | | | |
| | 220.10 - 224.38 | | | | | | | | |
| | - lithic mudstone, matrix supported with ~50% clasts. | | | | | | | | |
| | - clasts are angular to sub-angular, moderately silicified and uniform in size, ranging from 1mm to 5mm. | | | | | | | | |
| | 220.10 - 221.14 - 5% py, some fine grained disseminations but mostly fine grained agglomerations within fragments or as whole fragments | | | | | | | | |
| | 221.87 - py filled fractures @ 30° to CA 3mm wide | | | | | | | | |
| | 222.07 - py filled fractures at 40° to CA 3mm wide | | | | | | | | |
| | 222.51 - py filled fractures at 30° to CA 5mm wide | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Hole No. AP 9 Co ord. _____ Horizontal Length _____ Date Completed Sept 3/90
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By Pete Zamora

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-----------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 215.11 - 223.05 (cont'd) | | | | | | | | | |
| | 224.38 - 227.19 - argillite with ≈ 5% ghost fragments - high silicification - 2-3% py as blebs within fragments - quartz veining that contains Tr Sph and Tr Aspy | | | | | | | | |
| | 225.81 - quartz vein, 2-5 mm wide @ 60° to CA - Tr Sph, 10-15% py | | | | | | | | |
| | 226.15 - Quartz vein 30mm wide at 60° to CA - Tr-1% Aspy, 15-20% py | | | | | | | | |
| | 226.69 - Quartz vein 40mm wide at 50° to CA 15-20% py | | | | | | | | |
| | 226.75 - Quartz vein 35mm wide at 40° to CA = grey carb - Tr Aspy, 5-10% py | | | | | | | | |
| | 226.80 - 227.19 - weak brecciation with quartz filled fractures (+ carb) - 2-4% py concentrated in fractures - Tr sph. | | | | | | | | |
| | 227.19 - 238.05 - lithic mudstone with ≤ 20% fragments - 227.19 - 227.65 - 4-5% py + aspy in qtz-carb vein - 227.65 - 228.12 - weak to moderate brecciation with ≈ 5% py concentrated in quartz veinlets 228.12 - 231.25 - Tr py 228.36 - py concentrated on fracture plane? on bedding? 2-3mm wide at 40° to CA 230.97 - quartz vein 5mm wide at 30° to CA - Tr Sph, Tr py | | | | | | | | |
| | 231.25 - 231.79 - dacite tuff, highly silicified with complete silica replacement of some fragments - Random fracture with tr. py. | | | | | | | | |
| | 231.79 - 232.88 - Tr-1% py found as very fine grained dissemination but primarily concentrated in fractures | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 9 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. ppb | Ag. ppm | Cu. | Zn. | As ppm | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | |
|---------------------------|--------|-------|------------|------------|-----|-----|-----------|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | |
| 0.00 - 6.10 | CASING | 6.10 | | | | | | | | | | | | | | | | | | |
| 6.10 - 6.60 | 2018-G | 0.50 | 4 | .2 | | | 10 | | | | | | | | | | | | | |
| 6.60 - 7.10 | 2019-G | 0.50 | 3 | .1 | | | 4 | | | | | | | | | | | | | |
| 7.10 - 7.60 | 2020-G | 0.50 | 2 | .2 | | | 11 | | | | | | | | | | | | | |
| 7.60 - 8.20 | 2021-G | 0.60 | 3 | .1 | | | 9 | | | | | | | | | | | | | |
| 8.20 - 8.70 | 2022-G | 0.50 | 4 | .2 | | | 6 | | | | | | | | | | | | | |
| 8.70 - 9.20 | 2023-G | 0.50 | 4 | .3 | | | 9 | | | | | | | | | | | | | |
| 9.20 - 9.70 | 2024-G | 0.50 | 4 | .4 | | | 10 | | | | | | | | | | | | | |
| 9.70 - 10.20 | 2025-G | 0.50 | 3 | .3 | | | 10 | | | | | | | | | | | | | |
| 10.20 - 10.66 | 2026-G | 0.46 | 3 | .3 | | | 11 | | | | | | | | | | | | | |
| 10.66 - 10.96 | 2027-G | 0.30 | 3 | .2 | | | 11 | | | | | | | | | | | | | |
| 10.96 - 11.27 | 2028-G | 0.31 | 3 | .2 | | | 8 | | | | | | | | | | | | | |
| 11.27 - 12.20 | 2029-G | 1.53 | 9 | .4 | | | 8 | | | | | | | | | | | | | |
| 12.20 - 14.33 | 2030-G | 1.53 | 12 | .1 | | | 11 | | | | | | | | | | | | | |
| 14.33 - 15.60 | 2031-G | 1.27 | 14 | 1.5 | | | 91 | | | | | | | | | | | | | |
| 15.60 - 16.90 | 2032-G | 1.30 | 21 | 3.9 | | | 244 | | | | | | | | | | | | | |
| 16.90 - 17.50 | 2033-G | 0.60 | 43 | 2.3 | | | 424 | | | | | | | | | | | | | |
| 17.50 - 18.00 | 2034-G | 0.50 | 6 | .8 | | | 14 | | | | | | | | | | | | | |
| 18.00 - 18.50 | 2035-G | 0.50 | 32 | 2.1 | | | 81 | | | | | | | | | | | | | |
| 18.50 - 19.00 | 2036-G | 0.50 | 79 | 4.8 | | | 105 | | | | | | | | | | | | | |
| 19.00 - 19.50 | 2037-G | 0.50 | 177 | 7.3 | | | 207 | | | | | | | | | | | | | |
| 19.50 - 20.00 | 2038-G | 0.50 | 115 | 2.1 | | | 280 | | | | | | | | | | | | | |
| 20.00 - 20.50 | 2039-G | 0.50 | 1 | .3 | | | 16 | | | | | | | | | | | | | |
| 20.50 - 21.00 | 2040-G | 0.50 | 1 | .3 | | | 8 | | | | | | | | | | | | | |
| 21.00 - 21.50 | 2041-G | 0.50 | 10 | .3 | | | 6 | | | | | | | | | | | | | |
| 21.50 - 22.00 | 2042-G | 0.50 | 8 | .2 | | | 6 | | | | | | | | | | | | | |
| 22.00 - 22.50 | 2043-G | 0.50 | 2 | .1 | | | 6 | | | | | | | | | | | | | |
| 22.50 - 23.00 | 2044-G | 0.50 | 16 | .1 | | | 4 | | | | | | | | | | | | | |
| 23.00 - 23.50 | 2045-G | 0.50 | 3 | .1 | | | 9 | | | | | | | | | | | | | |
| 23.50 - 24.95 | WASTE | 1.45 | — | — | | | — | | | | | | | | | | | | | |
| 24.95 - 25.50 | 2046-G | 0.55 | 36 | .2 | | | 17 | | | | | | | | | | | | | |
| 25.50 - 26.00 | 2047-G | 0.50 | 16 | .2 | | | 9 | | | | | | | | | | | | | |
| 26.00 - 26.50 | WASTE | 0.50 | — | — | | | — | | | | | | | | | | | | | |
| 26.50 - 27.00 | 2048-G | 0.50 | 3 | .2 | | | 7 | | | | | | | | | | | | | |
| 27.00 - 27.50 | 2049-G | 0.50 | 7 | .1 | | | 2 | | | | | | | | | | | | | |
| 27.50 - 28.00 | 2050-G | 0.50 | 1 | .1 | | | 9 | | | | | | | | | | | | | |
| 28.00 - 28.50 | WASTE | 0.50 | — | — | | | — | | | | | | | | | | | | | |
| 28.50 - 29.00 | 2051-G | 0.50 | 10 | .1 | | | 8 | | | | | | | | | | | | | |
| 29.00 - 29.50 | 2052-G | 0.50 | 13 | .2 | | | 11 | | | | | | | | | | | | | |
| 29.50 - 30.00 | 2053-G | 0.50 | 12 | .1 | | | 11 | | | | | | | | | | | | | |

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GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 9 Co ord. _____ Horizontal Length _____ Date Completed _____
Claim No. _____ Core Size _____ Drilled By _____
Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au ppb | Ag. ppm | Cu. ppm | Zn ppm | As ppm | WIDTH X ASSAY | | | | | AVERAGES | | | | | | | |
|---------------------------|--------|-------|-----------|------------|------------|-----------|-----------|---------------|-----|-----|-----|----|----------|-----|-----|----|----|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn | As | Ag. | Cu. | Zn | As | | | |
| 95.80 - 96.30 | 2088-G | 0.50 | 2 | .2 | | | 6 | | | | | | | | | | | | | |
| 96.30 - 123.00 | WASTE | 26.70 | | | | | | | | | | | | | | | | | | |
| 123.00 - 123.50 | 2089-G | 0.50 | 8 | .2 | | | 5 | | | | | | | | | | | | | |
| 123.50 - 124.00 | 2090-G | 0.50 | 1 | .1 | | | 2 | | | | | | | | | | | | | |
| 124.00 - 190.50 | WASTE | 66.50 | | | | | | | | | | | | | | | | | | |
| 190.50 - 191.00 | 2091-G | 0.50 | 2 | .1 | | | 2 | | | | | | | | | | | | | |
| 191.00 - 191.55 | 2092-G | 0.55 | 172 | .5 | | | 2 | | | | | | | | | | | | | |
| 191.55 - 192.05 | 2093-G | 0.50 | 7 | .2 | | | 3 | | | | | | | | | | | | | |
| 192.05 - 213.60 | WASTE | 21.55 | | | | | | | | | | | | | | | | | | |
| 213.60 - 214.10 | 2094-G | 0.50 | 1 | .2 | | | 10 | | | | | | | | | | | | | |
| 214.10 - 214.60 | 2095-G | 0.50 | 6 | .8 | | | 31 | | | | | | | | | | | | | |
| 214.60 - 215.10 | 2096-G | 0.50 | 15 | 1.1 | | | 30 | | | | | | | | | | | | | |
| 215.10 - 215.60 | 2097-G | 0.50 | 11 | 1.7 | | | 9 | | | | | | | | | | | | | |
| 215.60 - 216.10 | 2098-G | 0.50 | 1 | .5 | | | 13 | | | | | | | | | | | | | |
| 216.10 - 216.60 | 2099-G | 0.50 | 12 | .3 | | | 51 | | | | | | | | | | | | | |
| 216.60 - 217.10 | 2100-G | 0.50 | 2 | .6 | | | 25 | | | | | | | | | | | | | |
| 217.10 - 217.60 | 2101-G | 0.50 | 9 | 1.1 | | | 16 | | | | | | | | | | | | | |
| 217.60 - 218.10 | 2102-G | 0.50 | 7 | 1.3 | | | 21 | | | | | | | | | | | | | |
| 218.10 - 218.60 | 2103-G | 0.50 | 9 | 1.2 | | | 44 | | | | | | | | | | | | | |
| 218.60 - 219.05 | 2104-G | 0.45 | 9 | .9 | | | 57 | | | | | | | | | | | | | |
| 219.05 - 219.55 | 2105-G | 0.50 | 787 | 6.6 | | | 1170 | | | | | | | | | | | | | |
| 219.55 - 220.05 | 2106-G | 0.50 | 3298 | 8.2 | | | 3708 | | | | | | | | | | | | | |
| 220.05 - 220.55 | 2107-G | 0.50 | 10 | 1.9 | | | 50 | | | | | | | | | | | | | |
| 220.55 - 221.00 | 2108-G | 0.45 | 7 | 1.7 | | | 50 | | | | | | | | | | | | | |
| 221.00 - 221.30 | 2109-G | 0.30 | 12 | 1.4 | | | 47 | | | | | | | | | | | | | |
| 221.30 - 221.80 | 2110-G | 0.50 | 5 | 1.4 | | | 38 | | | | | | | | | | | | | |
| 221.80 - 222.30 | 2111-G | 0.50 | 5 | 1.4 | | | 33 | | | | | | | | | | | | | |
| 222.30 - 222.80 | 2112-G | 0.50 | 5 | 1.4 | | | 49 | | | | | | | | | | | | | |
| 222.80 - 223.30 | 2113-G | 0.50 | 11 | 1.0 | | | 28 | | | | | | | | | | | | | |
| 223.30 - 223.80 | 2114-G | 0.50 | 10 | 1.2 | | | 29 | | | | | | | | | | | | | |
| 223.80 - 224.30 | 2115-G | 0.50 | 3 | 1.3 | | | 51 | | | | | | | | | | | | | |
| 224.30 - 224.70 | 2116-G | 0.40 | 22 | 1.6 | | | 55 | | | | | | | | | | | | | |
| 224.70 - 225.20 | 2117-G | 0.50 | 20 | .9 | | | 23 | | | | | | | | | | | | | |
| 225.20 - 225.70 | 2118-G | 0.50 | 113 | 2.7 | | | 262 | | | | | | | | | | | | | |
| 225.70 - 226.00 | 2119-G | 0.30 | 211 | 6.7 | | | 489 | | | | | | | | | | | | | |
| 226.00 - 226.50 | 2120-G | 0.50 | 423 | 3.3 | | | 1831 | | | | | | | | | | | | | |
| 226.50 - 226.90 | 2121-G | 0.40 | 297 | 2.4 | | | 781 | | | | | | | | | | | | | |
| 226.90 - 227.40 | 2122-G | 0.50 | 95 | 2.3 | | | 199 | | | | | | | | | | | | | |
| 227.40 - 227.90 | 2123-G | 0.50 | 10 | 1.4 | | | 29 | | | | | | | | | | | | | |
| 227.90 - 228.40 | 2124-G | 0.50 | .7 | .5 | | | 12 | | | | | | | | | | | | | |

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GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 9 Co ord. Horizontal Length Date Completed

Claim No. Core Size Drilled By

Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET/METRES | NUMBER | WIDTH | Au. ppb | Ag. ppm | Cu. ppm | Zn ppm | As ppm | WIDTH X ASSAY | | | | | AVERAGES | | | | | | | |
|-------------------------|--------|-------|------------|------------|------------|-----------|-----------|---------------|-----|-----|-----|-----|----------|--|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | |
| 228.40 - 228.90 | 2125-G | 0.50 | 16 | .5 | | | 14 | | | | | | | | | | | | | |
| 228.90 - 229.40 | 2126-G | 0.50 | 3 | .4 | | | 17 | | | | | | | | | | | | | |
| 229.40 - 229.90 | 2127-G | 0.50 | 9 | .7 | | | 40 | | | | | | | | | | | | | |
| 229.90 - 230.40 | 2128-G | 0.50 | 11 | .7 | | | 49 | | | | | | | | | | | | | |
| 230.40 - 230.70 | 2129-G | 0.30 | 6 | .2 | | | 6 | | | | | | | | | | | | | |
| 230.70 - 231.20 | 2130-G | 0.50 | 9 | .3 | | | 7 | | | | | | | | | | | | | |
| 231.20 - 231.50 | 2131-G | 0.30 | 5 | .1 | | | 2 | | | | | | | | | | | | | |
| 231.50 - 231.80 | 2132-G | 0.30 | 2 | .1 | | | 5 | | | | | | | | | | | | | |
| 231.80 - 232.30 | 2133-G | 0.50 | 16 | 2.1 | | | 55 | | | | | | | | | | | | | |
| 232.30 - 232.80 | 2134-G | 0.50 | 14 | 1.3 | | | 47 | | | | | | | | | | | | | |
| 232.80 - 233.30 | 2135-G | 0.50 | 1 | .6 | | | 37 | | | | | | | | | | | | | |
| 233.30 - 233.80 | 2136-G | 0.50 | 3 | .4 | | | 33 | | | | | | | | | | | | | |
| 233.80 - 234.10 | 2137-G | 0.30 | 10 | .5 | | | 36 | | | | | | | | | | | | | |
| 234.10 - 234.80 | 2138-G | 0.70 | 16 | 1.0 | | | 37 | | | | | | | | | | | | | |
| 234.80 - 235.50 | 2139-G | 0.70 | 8 | .7 | | | 33 | | | | | | | | | | | | | |
| 235.50 - 237.13 | 2140-G | 1.63 | 7 | .6 | | | 41 | | | | | | | | | | | | | |
| 237.13 - 238.05 | 2141-G | 0.92 | 7 | .6 | | | 24 | | | | | | | | | | | | | |
| HOLE ABANDONED | | | | | | | | | | | | | | | | | | | | |

Hole No. AP10 Co ord. 1600 N Horizontal Length 140 m Date Completed SEPT 3/90
 Claim No. UNUK 26 075 W Core Size BGBDM Drilled By J.T. THOMAS
 Grid No. ZONE 1 Angle & Direction -45° / Az 232° Elevation 1250m Logged By B. GABOURY

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 0 - 11.28 | Casing. | | | | | | | | |
| 11.28 - 13.60 | Volcanic Mudstone / Debris Flow ~ 20% angular, felsic to intermediate volcanic clasts up to 5mm dia in a dark argillaceous matrix. Entire section is a fault zone with ~ 30% core recovery C.A. 13.55 m : 75° weak foliation | | | | | | | | |
| 13.60 - 95.85 | Altered welded Dacite ash-lapilli Tuff. a mottled, medium grey (NS) to greenish grey (56Y 6/1) felsic to intermediate volcanic fragmental containing irregular bleached 3-5cm wide patches which appear to be ghost fragments. These became more pronounced downhole. Has a weak fabric by virtue of alignment of lenticular sericitic/chloritic schlieren (fiamme). In the upper portions of the unit are coarse carbonate clasts (& coarse py blebs) with chloritic selvages. Occasional feldspar-phryic sections with lath-like xtals up to 3mm long often semi-parallel to fabric. The rock is generally moderately well silicified & sericitized and contains an average of ~2% py. It contains brecciated intervals with abundant haphazardly oriented chloritic fractures occasionally with peripheral bleaching & pyrite mineralization. 13.60 - 15.10 : bleached & silicified interval with 2-4% py in chl/py units or as small blebs rimmed with chl. C.A. 1400m : 44° fabric (bedding?) | | | | | | | | |

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

20,390

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 18.74 - 20.88 | : brecciated interval with abundant haphazardly oriented rebedded chloritic fractures + 2-4% py qs, coarse blebs or stringers associated with chloritic fractures. | | | | | | | | |
| 21.38 - 22.30 | : Fault ; rubble core & clayey gouge. | | | | | | | | |
| 32.15 - 32.65 | : 2-3% coarse py, chloritic stringers. | | | | | | | | |
| 39.71 - 39.21 | : 2-3% py, chloritic stringers. | | | | | | | | |
| C.A. | 28.80 m : 45° fabric. | | | | | | | | |
| C.A. | 33.50 m : 50° weak fabric | | | | | | | | |
| C.A. | 43.00 m : 48° weak fabric | | | | | | | | |
| 56.70 - 57.30 | : minor fault ; crushed, broken core, minor bleaching & chloritic fractures. | | | | | | | | |
| C.A. | 57.30 : 60° fabric | | | | | | | | |
| C.A. | 62.30 : 55° fabric | | | | | | | | |
| 68.40 - 69.36 | : moderately intense brecciation ; irregular chloritic stringers at core angles generally ≥ 45° plus irregular carbonate blebs (fracture infillings), contains 3-5% py overall. | | | | | | | | |
| 69.36 - 72.24 | : very mildly bleached interval ; whitish envelopes around sericitic / chloritic ghost pumice fragments. | | | | | | | | |

Hole No. AY10 Co. ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 72.64 - 73.60 | : crushed & mildly sheared & sericitized interval with 3-5% fine dissemin py; core angles appear to be $\geq 55^\circ$. | | | | | | | | |
| 73.60 - 80.10 | : mildly brecciated interval with randomly oriented chl/py fractures; overall contains ~ 2-4% py mainly in or peripheral to chloritic stars or as coarse blebs in minor carbonate masses (fracture infillings). brecciation is most intense between 74.12 - 74.80 (5-7% py) | | | | | | | | |
| C.A. | 77.40 m : 45° fabric (bedding) | | | | | | | | |
| 87.36 - 89.20 | : brecciated interval with numerous randomly oriented chl-py stars, overall carries 3-5% py | | | | | | | | |
| | 87.89 - 89.20 : 30% core recovery | | | | | | | | |
| C.A. | 90.00 m : $\sim 65^\circ$ fabric (bedding) | | | | | | | | |
| C.A. | 93.00 m : 57° fabric (bedding) | | | | | | | | |
| 95.85 - 117.12 | Dacitic Pyroclastic Breccia / Lapilli Tuff. | | | | | | | | |
| | A medium light grey (N6) to light greenish grey (5GY 8/1) coarse dacitic fragmental volcanic rock composed of subrounded to angular fragments up to at least 5cm dia. in a finer grained lightly sericitic volcanic ash groundmass (generally always matrix supported). Rock is mildly to non-silicified, mildly sericitized, and contains 2-3% py, overall, as disseminations & as | | | | | | | | |

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | occasional stringers up to 5mm wide. Matrix color becomes pinkish grey (5YR 8/1) below 102.41). Lapilli content becomes notably depleted below ~110.0m. | | | | | | | | |
| 95.85 - 102.41 | : Brecciated Interval; a variably brecciated interval containing fairly abundant, haphazardly oriented chl-py stringers plus some occasional irregular gta-py veins up to ~1 cm wide. Rock is mildly to moderately silicified and the bleached (lighter colored) intervals are mildly to moderately sericitized. Overall contains 3-5% py as dissems in chl-py stars. | | | | | | | | |
| 96.32 - 98.00 | : Fault Zone; rubblely core — 20% core recovery | | | | | | | | |
| 98.80 - 100.50 | : Fault Zone; more intensely brecciated interval with ~5% py. includes a crushed interval from 99.30 - 99.57 with 5-7% py & rubblely interval with 60% core recovery from 99.67 - 100.50. | | | | | | | | |
| 101.17 - 101.50 | : 5% py mainly in chl-gta-py stars. | | | | | | | | |
| 102.00 - 102.41 | : 5% py as stars in bleached interval. | | | | | | | | |
| 108.91 - 109.10 | : C.A. 101.50 m; 58° very crude fabric. bed, pyritic healed shear w 5-7% py, tr sp, CA ~42° | | | | | | | | |
| 111.00 - 112.60 | : FAULT ZONE; rubblely, broken core plus clayey gouge, no visible alteration or change in sulfide content. | | | | | | | | |

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 114.42 - 114.75 | : brecciated interval with abundant randomly oriented chlorite-pyrite stringers ; overall ~5% py. | | | | | | | | |
| 114.75 - 115.50 | : Fault Zone ; bleached, rubble core plus white gouge, 3-5% py as disseminations ; in occasional stringers. | | | | | | | | |
| 115.50 - 116.12 | : numerous pyritic stringers & open py - qtz crystal lined fractures at ~45° to core axis, overall 3-5% py. | | | | | | | | |
| 116.12 - 117.12 | : brecciated interval with one 7cm wide qtz-py vein at ~40° to core axis (to fabric), abundant randomly oriented py & chl stars (although many are concordant with fabric); Overall 7-10% py plus tr-1% resinous brown sphalerite in qtz-py vein | | | | | | | | |
| | C.A. 117.12 m : 50° fabric | | | | | | | | |
| 117.12 - 163.07 | Welded Dacite Ash-Lapilli Tuff a generally more greenish to olive grey colored dacitic volcanoclastic rock demonstrating less silicification and more sericitization than that encountered in the interval 13.60 - 95.85. Otherwise fragment content, composition and general fabric is similar: | | | | | | | | |
| 117.56 - 117.96 | : mildly brecciated interval with ≤ 1cm wide qtz-py veinlet with tr sph, overall contains 4-6% py mainly in randomly oriented chl-py stringers. | | | | | | | | |
| | CA. 118.30 m : ~50° fabric | | | | | | | | |

page 6 of 9

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 119.1 - 123.0 | mildly brecciated & silicified with 3-5% py as disseminations & in randomly oriented stringers (± chl); | | | | | | | | |
| 119.1 - 120.1 | numerous carb-py (tan to dirty grey colored) vults, ~40° to 45° to core axis, up to 5 cm wide. | | | | | | | | |
| 121.85 - 123.0 | 5% py in a somewhat more brecciated interval. | | | | | | | | |
| 123.0 - 138.40 | FAULT ZONE; rubbly, broken core & gouge intervals, rock is locally mildly bleached & sericitized & contains 2-4% py; | | | | | | | | |
| 125.55 - 126.19 | interflow volcanic mudstone, dacitic fragments up to 1cm diameter in a somewhat argillaceous/sericitic matrix | | | | | | | | |
| 126.19 - 128.02 | broken core plus 22 cm of clayey gouge, ~60° core recovery | | | | | | | | |
| 128.02 - 134.60 | broken, rubbly core, contains 2-4% py mainly in randomly oriented py ± chl stringers. | | | | | | | | |
| 134.60 - 136.30 | broken, rubbly core with 3-5% py as stringers, blebs & disseminations (up to 6-8% py in somewhat more bleached and sericitized interval from 135.94 - 136.30 m) | | | | | | | | |
| CA. 134.80 m | 65° fabric | | | | | | | | |
| CA. 132.10 m | ~70° fabric | | | | | | | | |

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 138.40 - 156.20 | rock becomes more greenish to olive grey colored, with more sericitization & better fabric development, contains occasional brecciated intervals with fracture infilling by a dark colored chl/py (?) matrix. Brecciated intervals, although displaying random fracture orientation, possess one fracture set oriented // to fabric. | | | | | | | | |
| CA. 145.39 m | : 45° fabric | | | | | | | | |
| CA. 152.00 m | : 40° fabric. | | | | | | | | |
| 156.20 - 163.07 | sericitization increases from mild to moderately strong toward bottom contact. Pyrite content averages 1-3% py & occurs mainly as disseminations, blebs & schlieren: | | | | | | | | |
| | 162.05 - 163.07: intense sericitization & bleaching to a light olive color. | | | | | | | | |
| CA. 157.50 m | : 50° fabric | | | | | | | | |
| CA. 160.20 m | : 40° fabric | | | | | | | | |
| CA. 162.80 m | : 34° fabric / shearing. | | | | | | | | |
| 163.07 - 198.12 | Volcanic Mudstone (Debris Flow) with black argillite & siltstone interbeds | | | | | | | | |
| | A coarse volcanic fragmental composed of up to 35% subrounded to angular andesitic to dacitic fragments up to ~ 2cm diameter in a black argillite matrix. Fragments display minor to intense sericitization, | | | | | | | | |

Hole No. AP 10 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | depending on degree of shearing, overall 1-2% fine disseminated py & very minor concordant Qtz - carb vults. Interval containing black argillite or lighter colored coarser grained silty interbeds varying from ~3cm diameter to several metres. | | | | | | | | |
| CA | 165.00 m : 50° bedding / fol. | | | | | | | | |
| CA | 167.00 m : 47° " | | | | | | | | |
| CA | 171.80 m : 67° " | | | | | | | | |
| CA | 175.00 m : 65° " | | | | | | | | |
| 175.57 - 186.50 | : Fault; broken, splintery core plus several clayey/graphitic gouge intervals | | | | | | | | |
| 176.10 - 177.20 | : brecciated with 10-20% irregular, anastomosing Qtz stKuks (generally < 4mm wide), overall < 2% py, broken core & minor gouge | | | | | | | | |
| 177.20 - 177.55 | : mainly clayey gouge plus broken core | | | | | | | | |
| 177.55 - 178.82 | : sheared black argillite with ~10% fine concordant white Qtz-py vults (~2% py overall) | | | | | | | | |
| C.A. | 177.80 m : 52° fol / shearing. | | | | | | | | |
| 186.50 - 188.12 | : olive-colored, sheared tuffaceous interval, moderately sericitized, < 2% py overall. | | | | | | | | |
| C.A. | 187.70 m : 60° fabric. | | | | | | | | |
| 190.65 - 191.46 m | : olive colored, moderately well sericitized, tuffaceous interval, 10% irreg. Qtz vults up to 5mm dia at variable CA's, < 2% py. | | | | | | | | |
| CA. | 189.0 m : 85° bedding / fabric. | | | | | | | | |



GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

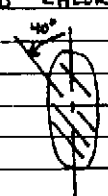
Hole No. AP 10 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET / METRES | NUMBER | WIDTH | Au. ppb | Ag. ppm | Cu | Zn | Tfs ppm | WIDTH X ASSAY | | | | | | AVERAGES | | | | | | | |
|---------------------------|--------|-------|------------|------------|----|----|------------|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | | | | |
| 73.60 - 74.12 | 2175-G | 0.52 | 3 | 1.6 | | | 58 | | | | | | | | | | | | | | |
| 74.12 - 74.47 | 2176-G | 0.35 | 5 | .5 | | | 28 | | | | | | | | | | | | | | |
| 74.47 - 74.80 | 2177-G | 0.33 | 1 | .3 | | | 20 | | | | | | | | | | | | | | |
| 74.80 - 75.20 | 2178-G | 0.40 | 1 | .3 | | | 9 | | | | | | | | | | | | | | |
| 75.20 - 75.50 | 2179-G | 0.30 | 6 | .4 | | | 4 | | | | | | | | | | | | | | |
| 75.50 - 76.00 | 2180-G | 0.50 | 6 | .5 | | | 10 | | | | | | | | | | | | | | |
| 76.00 - 76.50 | 2181-G | 0.50 | 1 | .2 | | | 7 | | | | | | | | | | | | | | |
| 76.50 - 77.00 | 2182-G | 0.50 | 6 | .2 | | | 7 | | | | | | | | | | | | | | |
| 77.00 - 77.50 | 2183-G | 0.50 | 1 | .1 | | | 8 | | | | | | | | | | | | | | |
| 77.50 - 78.00 | 2184-G | 0.50 | 5 | .4 | | | 9 | | | | | | | | | | | | | | |
| 78.00 - 78.60 | 2185-G | 0.60 | 13 | .4 | | | 13 | | | | | | | | | | | | | | |
| 78.60 - 79.10 | 2186-G | 0.50 | 7 | .3 | | | 9 | | | | | | | | | | | | | | |
| 79.10 - 79.60 | 2187-G | 0.50 | 11 | .2 | | | 10 | | | | | | | | | | | | | | |
| 79.60 - 80.10 | 2188-G | 0.50 | 12 | .3 | | | 12 | | | | | | | | | | | | | | |
| 80.10 - 86.86 | WASTE | 6.76 | — | — | — | — | — | | | | | | | | | | | | | | |
| 86.86 - 87.36 | 2189-G | 0.50 | 7 | .5 | | | 9 | | | | | | | | | | | | | | |
| 87.36 - 87.89 | 2190-G | 0.53 | 16 | .5 | | | 6 | | | | | | | | | | | | | | |
| 87.89 - 89.20 | 2191-G | 1.31 | 16 | .9 | | | 8 | | | | | | | | | | | | | | |
| 89.20 - 89.70 | 2192-G | 0.50 | 4 | .4 | | | 7 | | | | | | | | | | | | | | |
| 89.70 - 94.15 | WASTE | 4.45 | — | — | — | — | — | | | | | | | | | | | | | | |
| 94.15 - 94.85 | 2193-G | 0.70 | 7 | .3 | | | 10 | | | | | | | | | | | | | | |
| 94.85 - 95.35 | 2194-G | 0.50 | 7 | .3 | | | 12 | | | | | | | | | | | | | | |
| 95.35 - 95.85 | 2195-G | 0.50 | 4 | .1 | | | 2 | | | | | | | | | | | | | | |
| 95.85 - 96.32 | 2196-G | 0.47 | 11 | .7 | | | 12 | | | | | | | | | | | | | | |
| 96.32 - 98.00 | 2197-G | 1.68 | 5 | .4 | | | 11 | | | | | | | | | | | | | | |
| 98.00 - 98.35 | 2198-G | 0.35 | 5 | .8 | | | 40 | | | | | | | | | | | | | | |
| 98.35 - 98.80 | 2199-G | 0.45 | 9 | .5 | | | 16 | | | | | | | | | | | | | | |
| 98.80 - 99.30 | 2200-G | 0.50 | 12 | .6 | | | 12 | | | | | | | | | | | | | | |
| 99.30 - 99.57 | 2202-G | 0.27 | 10 | .8 | | | 22 | | | | | | | | | | | | | | |
| 99.57 - 100.10 | 2203-G | 0.53 | 1 | .3 | | | 7 | | | | | | | | | | | | | | |
| 100.10 - 100.55 | 2204-G | 0.45 | 13 | .9 | | | 19 | | | | | | | | | | | | | | |
| 100.55 - 101.17 | 2205-G | 0.62 | 6 | .6 | | | 11 | | | | | | | | | | | | | | |
| 101.17 - 101.50 | 2206-G | 0.33 | 12 | 1.0 | | | 15 | | | | | | | | | | | | | | |
| 101.50 - 102.00 | 2207-G | 0.50 | 10 | .4 | | | 6 | | | | | | | | | | | | | | |
| 102.00 - 102.41 | 2208-G | 0.41 | 6 | .6 | | | 12 | | | | | | | | | | | | | | |
| 102.41 - 108.31 | WASTE | 5.90 | — | — | — | — | — | | | | | | | | | | | | | | |
| 108.31 - 108.81 | 2209-G | 0.50 | 14 | .6 | | | 9 | | | | | | | | | | | | | | |
| 108.81 - 109.10 | 2210-G | 0.29 | 27 | .9 | | | 12 | | | | | | | | | | | | | | |
| 109.10 - 109.60 | 2211-G | 0.50 | 6 | .7 | | | 17 | | | | | | | | | | | | | | |
| 109.60 - 110.10 | 2212-G | 0.50 | 33 | .3 | | | 8 | | | | | | | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

1 OF 9

Hole No. AP-11 Co. ord. 1600N Horizontal Length 141.12m Date Completed SEPT 8/90
 Claim No. UNUK 26 Core Size 003W Drilled By J.T. THOMAS
 Grid No. ZONE 1 Angle & Direction -45°/Az 282 Elevation 1208 m Logged By B. BORNTRAEGER

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 0 - 9.75 | CASING | | | | | | | | |
| 9.75 - 42.90 | ALTERED AND ALTERED DIABASE DYKE WITH HYDROTHERMALLY BRECCIATED LOWER CONTACT - MASSIVE, VERY FINE GRAINED (vfg), GREENISH GREY (5 GY 6/1) TO GREENISH BLACK (5 GY 4/1), INTRUSIVE IGNEOUS ROCK, MILDLY BRECCIATED & FRACTURED WITH TENSIONAL QTZ-CARB VEINLETS UP TO 2cm WIDE AT VARIABLE CORE ANGLES (SOME FILLED WITH PINK MD-CALCITE), LARGER QTZ VEINLETS HAVE CHLORITE SELVAGES. - OVERALL COLOR BECOMES LIGHTER DOWN THE HOLE - < 1% DISS. py OVERALL + ISOLATED QTZ-CARB VEINLETS w py BLEBS 9.75-14.00 POOR CORE RECOVERY = 40-50% ; RUBBLY - SLIGHTLY MAGNETIC 18.53-18.90 MODERATE CHLORITE FOLIATION @ 80-90° TO C.A. 27.82-28.35 SHEAR ZONE INTENSE FOLIATION @ 60-75° TO C.A. @ 28.16-28.21 FAULT GOUGE FROM 28.25-28.35 31.14 SLICKENSIDES ON QTZ/CARB VEIN (2cm WIDE) - VEIN CONTACTS C.A. = 50° - WELL DEVELOPED CHLORITE MINERAL LINEATIONS  SLICKENSIDES TREND 40° FROM VERTICAL PLANE THROUGH CORE AXIS 39.11-39.11 SERICITIZED DIABASE DYKE - WALL ROCK OF HYDROTHERMALLY BRECCIATED LOWER CONTACT 39.11-40.04 INCREASE IN SILICIFICATION TOWARDS HYDROTHERMALLY BRECCIATED LOWER CONTACT | | | | | | | | |

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

20,390

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

2 OF 9

Hole No. AP-11 Coord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET/METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|-------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 40-04-40-16 | <p>HYDROTHERMALLY ^{ALTERED AND} BRECCIATED LOWER CONTACT OF DIABASE DYKE</p> <p>- PERVASIVE SERICITIZATION OF FRAGMENTS WITH A SURROUNDING BLEACHED RIND</p> <p>- 1-3% FINE GRAINED (f.g.) py ALONG FRACTURES</p> | | | | | | | | |
| 40-16-40-38 | <p>QTZ/CARB VEIN 10 cm WIDE WITH SILKIFIED BRECCIA FRAGMENTS ALONG BOTH CONTACTS OF THE VEIN</p> <p>- INCREASE IN SILICIFICATION AS YOU APPROACH THE VEIN</p> <p>- VEIN CONTACTS HAVE C.A.'s OF 55-60°</p> <p>SX'S</p> <p>- py (5-10%) OCCURS AS DISS. BLEBS AND ALONG FRACTURE SURFACES</p> <p>- TR OF gn, sl & asp</p> <p>- SX'S CONCENTRATED ALONG CONTACTS/SELVAGES OF QTZ/CARB VEIN.</p> | | | | | | | | |
| 40-38-40-82 | <p>HYDROTHERMALLY ALTERED BRECCIA WITH QTZ/CARB VEINETS UP TO 1cm WIDE. (S.A. 40-04-40-16)</p> <p>- C.A.'s RANGE FROM 50-70°</p> <p>SX'S</p> <p>- 1-5% py AS DISS. AND BLEBS ALONG FRACTURES SURROUNDING BRECCIA FRAGMENTS AND ALONG SELVAGES OF QTZ/CARB VEINETS</p> | | | | | | | | |
| | | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

3 OF 9

Hole No. AP.11 Co. ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

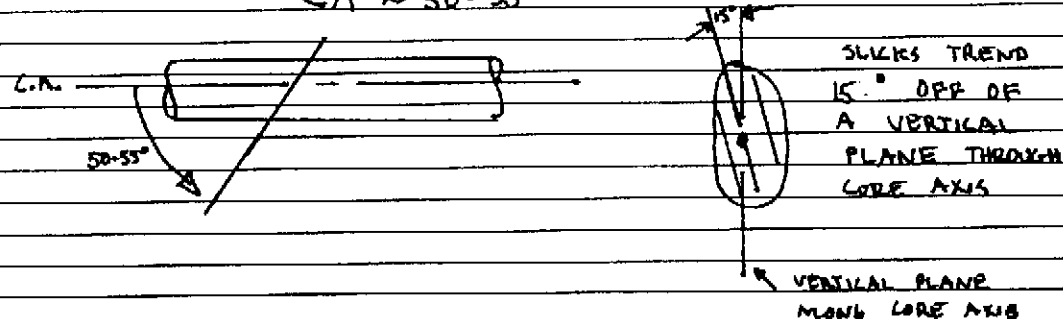
| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 40-82 - 41-29 | HYDROTHERMALLY ALTERED BRECCIATED LOWER CONTACT ↳ QTZ/CARB VEINLETS UP TO 0.3 cm WIDE (S.A. 40-04-40-16) - C.A.'s ≈ 80-90° - 1-5% py AS DISS AND BLEBS ALONG FRACTURE SURFACES | | | | | | | | |
| 41-29 - 42-12 | THIN HORIZON OF VOLCANOCLASTIC MUDSTONE GRADING INTO A "POKER CHIP CLEAVAGE" MUDSTONE - BOTH CONTACTS HAVE BEEN CARBONATE ALTERED - FRAGMENTS IN VOLCANOCLASTIC MUDSTONE ARE SUB-ANG - ANG UP TO 0.7cm ACROSS AND HAVE BEEN REPLACED BY CARBONATE - 1 py VEINLET 0.3 cm WIDE CONSISTING OF f.g. py. C.A. ≈ 55° - C.A.'s IN VOLC. MUDSTONE ≈ 50-60° - C.A.'s IN POKER CHIP CLEAVAGED MUDSTONE ≈ 80-90° | | | | | | | | |
| 42-12 - 42-90 | HYDROTHERMALLY ALTERED BRECCIATED LOWER CONTACT OF DIABASE DYKE (S.A. 40-04-40-16) - QTZ/CARB VEIN ≈ 3cm WIDE U. CONTACT C.A. ≈ 45° L. CONTACT C.A. ≈ 60° SX'S - 5-7% py AS DISS, BLEBS AND FRACTURE INFILLINGS - TR sl, ga, asp | | | | | | | | |
| 42-90 - 43-00 | SHEAR ZONE ALONG CONTACT BETWEEN ALTERED DIABASE DYKE AND MUDSTONE - MUDSTONE STRONGLY SHEARED & CARBONATE INFILLING | | | | | | | | |
| 43-00 - 46-82 | LOST CORE (MUDSTONE ↳ BLEBS OF v.f.g. DISS py.) | | | | | | | | |

Hole No. AP.11 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn |
| 46-82-67-93 | BLACK MUDSTONE WITH INTERCOLLATED ZONES/HORIZONS OF GREYWACKE AND VOLCANOCLASTIC MUDSTONE | | | | | | | | |
| | BLACK v.f.g. MUDSTONE w INTERBEDDED LAYERS OF GREYWACKE AND VOLCANOCLASTIC MUDSTONE UP TO 2m THICKNESS, BUT RARELY EXCEEDING 0-20cm THICKNESS. CARBONATE VEINLETS OCCUR IN THE MUDSTONE @ IRREGULAR C.A.'S AND CAN BE UP TO 0.5cm WIDE. OVERALL COLOR IS BLACK WITH THE GREYWACKE HORIZONS APPEARING AS BLACK AND WHITE SPECKLED LAYERS. OVERALL < 2% f.g. DISS PY HOWEVER THE CONCENTRATION OF PY INCREASES UP TO 2-5% IN THE GREYWACKE AND VOLC. MUDSTONE LAYERS. | | | | | | | | |
| 48-90-51-23 | BLACK MUDSTONE w "POKER CHIP CLEAVAGE" AND THIN BANDS (< 10cm WIDE) OF BLACK SHEARED, FAULT GOUGE | | | | | | | | |
| | CORE RECOVERY ~ 70-90% C.A.'s ~ 75-85° | | | | | | | | |
| 52-32 | 1.0cm WIDE CARB. BRECCIA w 1-2% py ALONG SELVAGES AS DISSEMINATIONS C.A. 80° | | | | | | | | |
| 53-08-59-13 | SHEAR ZONE IN MUDSTONE | | | | | | | | |
| | • FAULT GOUGE • POOR RECOVERY 20-80% | | | | | | | | |
| 59-60-59-80 | SHEAR ZONE w CARB VEINLETS UP TO 0.2cm WIDE C.A.'s ~ 70° | | | | | | | | |
| | • DEVELOPMENT OF FAULT GOUGE ON FRACTURE SURFACES • CORE HIGHLY FRACTURED | | | | | | | | |
| 62-65-62-80 | SHEAR ZONE w FAULT GOUGE | | | | | | | | |

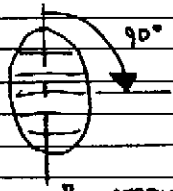
| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 62.95-64.84 | VOLCANO CLASTIC MUDSTONE • V.f.g. py IN BLESS UP TO 2cm ACROSS • FRAGMENTS SUB ANG. - ANG UP TO 2cm ACROSS - MODERATE TO INTENSE CARBONATE ALTERATION OF FRAGMENTS AS OPPOSED TO WEAK CARB ALTERATION IN MUDDY MATRIX • MATRIX SUPPORTED w MATRIX CONSISTING OF V. f.g. BLACK MUD | | | | | | | | |
| 67.93-69.22 | MODERATELY SILICIFIED/SERKITIZED FELSIK - INTERMEDIATE TUFF f.g. GREENISH GREY (SG 6/1) FELSIK - INT. TUFF • DEVELOPEMENT OF SERKITE THROUGHOUT • SILICIFICATION AND AN INCREASE IN SERKITE ALONG FRACTURED SURFACES • MINOR DEVELOPEMENT OF CHLORITE ON FRACTURE SURFACES • CA'S ARE VARIABLE 30-85° FOR FRACTURE SURFACES | | | | | | | | |
| 69.22-73.54 | BLACK MUDSTONE w INTERCOLLATED ZONES/HORIZONS OF GREY WACKE (S.A. 46-82-67-93) CA'S FOR CARB. VEINLET 0.5cm WIDE @ 71-75, 71-82 ≈ 80-85° - LACK OF POKER CHIP CLEAVAGE | | | | | | | | |
| 72.90 | SHEAR ZONE • FAULT GOUGE w f.g. DISS. py (1-2%) CA. ≈ 70-75° | | | | | | | | |

Hole No. AP 11 Co ord. _____ Horizontal Length _____ Date Completed _____
 Claim No. _____ Core Size _____ Drilled By _____
 Grid No. _____ Angle & Direction _____ Elevation _____ Logged By _____

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 73-54-105-81 | WELDED DACITIC ASH FLOW TUFF MASSIVE f.g. GREENISH GREY (56 6/1) TO DARK GREENISH GREY (56 4/1) ASH FLOW TUFF. WELDED PUMICE FRAGMENTS HAVE BEEN REPLACED BY CHLORITE. SOME ACCIDENTAL LAPILLI SIZE FRAGMENTALS UP TO 2 cm ACROSS. THESE FRAGMENTALS HAVE BEEN ALTERED TO CHLORITE OR HAVE BEEN BLEACHED. OVERALL < 2% py AS DISS THIN (< 0.25 cm) QTZ/LABR VEINLETS OCCUPY FRACTURES AND HAVE A THIN LAYER OF FAULT GOUGE COATING THE FRACTURE SURFACE. OVERALL THE CORE IS RUBBLY AND HIGHLY FRACTURED WITH FEW PIECES OF CORE OVER 10 cm IN LENGTH. L.A.'S OF FRACTURES ARE EXTREMELY VARIABLE THROUGHOUT THIS INTERVAL. | | | | | | | | |
| 73-54-73-92 | MOD. SERICITE ALTERATION TO SILICIFICATION AND MINOR CHLORITE DEVELOPEMENT ASSOCIATED WITH THE SILICA. - 1-2% f.g. DISS PY. | | | | | | | | |
| 90-83-91-00 | RUBBLY / GROUND CORE | | | | | | | | |
| 92-35-92-53 | FAULT GOUGE | | | | | | | | |
| 92-70-96-86 | RUBBLY CORE WHICH IS HIGHLY FRACTURED - CHLORITE AND FAULT GOUGE ON FRACTURE SURFACES | | | | | | | | |
| 100-18 | SLICKENSIDES ON FRACTURE SURFACE CA ≈ 50-55° | | | | | | | | |
| |  <p>SLICKS TREND 15° OFF OF A VERTICAL PLANE THROUGH CORE AXIS</p> <p>VERTICAL PLANE THROUGH CORE AXIS</p> | | | | | | | | |

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 100.19-100.40 | QZ / CHLORITE FILLED EXTENSION GASHES 0.3cm WIDE x 5cm LONG FOLLOW RE C.A. | | | | | | | | |
| 103.75-104.84 | SILICIFIED TUFF w QZ STRINGERS UP TO 0.3cm WIDE AND PORPHYRIC FELDSPAR CRYSTALS UP TO 0.2cm ACROSS - f.g. py AND CHLORITE REPLACING FLATTENED PUMICE FRAGMENTS - MODERATE SERICITE ALTERATION | | | | | | | | |
| 104.84-141.12 | MODERATELY SERICITIZED DACITIC ASH FLOW TUFF w INTER COLLATED ZONES OF VOLCANIC CLASTIC MUDSTONES. TUFF DACITIC ASH FLOW A HORIZONS VARYING IN THICKNESS FROM 1m → 6m WITH VARYING DEGREES OF SERICITE ALTERATION. OVERALL < 1% f.g. DISS PY. ACCIDENTAL MAFIC FRAGMENTS ARE SUB ANG - ANG (UP TO 0.7cm ACROSS) AND HAVE UNDERGONE CHLORITE ALTERATION. FELSIC FRAGMENTS; SUB ANG - ANG; UP TO 0.7cm ACROSS HAVE BEEN SERICITIZED. C.A.'S ARE VARIABLE VOLCANIC CLASTIC MUDSTONE CONTAINS SUB ANG - ANG FRAGMENTS UP TO 2cm ACROSS OF FELSIC COMPOSITION, SUPPORTED IN A BLACK MUDDY MATRIX. ALTERATION CONSISTS OF MODERATE SILICIFICATION. OVERALL < 1% f.g. PY. C.A.'S VARIABLE VOLC. MUDSTONE HAS TAKEN UP THE SHEARING. | | | | | | | | |
| 110.33-111.57 | SILICIFIED VOLC. MUDSTONE - SILICIFICATION OF MATRIX - 2-3% f.g. DISS PY. | | | | | | | | |
| 120.00 | 5cm WIDE SHEAR ZONE w FAULT GOUGE | | | | | | | | |
| 120.65-121.31 | SHEARED MUDSTONE w FAULT GOUGE SHEARING @ 90° TO C.A. | | | | | | | | |
| 121.66 | 5cm WIDE SHEAR ZONE w FAULT GOUGE | | | | | | | | |

Hole No. AP11 Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 121-66 - 126-99 | LAPILLI SIZED VOLC. MUDSTONE • BLACK MUDDY MATRIX SUPPORTED; CLAST SIZE UP TO 2cm ACROSS; SUB ANG-ANG. • SERICITIZED FELSIC FRAGMENTS | | | | | | | | |
| 126-99 - 131-79 | COARSE FRAGMENTAL VOLC. MUDSTONE • F.g. MUDDY MATRIX WITH AN INCREASE IN F.g. VOLCANIC ASH DOWN THE HOLE. • CLASTS ARE SERICITIZED AND FELSIC IN COMPOSITION SUB ANG-ANG; UP TO 8cm ACROSS • SERICITE ALTERATION INCREASES DOWN THE HOLE < 5cm WIDE FRACTURE SURFACES w/ PAULT GOUGE @ 129-39, 131-08, 131-11 CA'S ≈ 70-80° SLICKENSIDES @ 131-11 CA ≈ 75°  A VERTICAL PLANE | | | | | | | | |
| 131-79 - 141-12 | MODERATELY SERICITIZED LAPILLI DACITE TUFF GRADING INTO A MODERATELY SERICITIZED DACITE ASH FLOW TUFF • LAPILLI SIZED FRAGMENTS ARE MOD.-INT. SERICITIZED; REMNANT TEXTURES, GHOST FRAGMENTS • FRAGMENT SIZE DECREASES DOWN HOLE | | | | | | | | |


GRANGES EXPLORATION LTD.
DIAMOND DRILL RECORD

Hole No. AP 11 Co ord. Horizontal Length Date Completed

Claim No. Core Size Drilled By

Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | NUMBER | WIDTH | Au. PPb | Ag. PPm | Cu. PPm | Zn. PPm | Pb PPm | WIDTH X ASSAY | | | | | | AVERAGES | | | | |
|---------------------------|--------|-------|------------|------------|------------|------------|-----------|---------------|-----|-----|-----|-----|--|----------|--|--|--|--|
| | | | | | | | | WIDTH | Au. | Ag. | Cu. | Zn. | | | | | | |
| 0.00 - 9.75 | CASING | 9.75 | | | | | | | | | | | | | | | | |
| 9.75 - 38.11 | WASTE | 28.36 | — | — | — | — | — | | | | | | | | | | | |
| 38.11 - 39.11 | 2243-G | 1.00 | 18 | .1 | 7 | 126 | 17 | | | | | | | | | | | |
| 39.11 - 40.04 | 2244-G | 0.93 | 21 | .2 | 7 | 187 | 17 | | | | | | | | | | | |
| 40.04 - 40.16 | 2245-G | 0.12 | 13 | 1.4 | 19 | 240 | 21 | | | | | | | | | | | |
| 40.16 - 40.38 | 2246-G | 0.22 | 839 | 4.2 | 36 | 8123 | 765 | | | | | | | | | | | |
| 40.38 - 40.82 | 2247-G | 0.44 | 277 | 2.0 | 17 | 133 | 59 | | | | | | | | | | | |
| 40.82 - 41.29 | 2248-G | 0.47 | 53 | 2.8 | 31 | 223 | 45 | | | | | | | | | | | |
| 41.29 - 42.12 | 2249-G | 0.83 | 38 | 1.8 | 29 | 436 | 27 | | | | | | | | | | | |
| 42.12 - 42.90 | 2250-G | 0.78 | 72 | 2.7 | 77 | 447 | 509 | | | | | | | | | | | |
| 42.90 - 66.93 | WASTE | 24.03 | — | — | — | — | — | | | | | | | | | | | |
| 66.93 - 67.93 | 2251-G | 1.00 | 69 | 4.5 | 30 | 119 | 50 | | | | | | | | | | | |
| 67.93 - 68.65 | 2252-G | 0.72 | 11 | .6 | 10 | 130 | 9 | | | | | | | | | | | |
| 68.65 - 69.22 | 2253-G | 0.57 | 135 | 1.0 | 14 | 104 | 18 | | | | | | | | | | | |
| 69.22 - 70.22 | 2254-G | 1.00 | 88 | 2.1 | 29 | 102 | 33 | | | | | | | | | | | |
| 70.22 - 72.54 | WASTE | 2.32 | — | — | — | — | — | | | | | | | | | | | |
| 72.54 - 73.54 | 2255-G | 1.00 | 98 | 5.4 | 40 | 170 | 52 | | | | | | | | | | | |
| 73.54 - 73.92 | 2256-G | 0.38 | 26 | .5 | 16 | 124 | 12 | | | | | | | | | | | |
| 73.92 - 74.92 | 2257-G | 1.00 | 22 | .5 | 8 | 131 | 13 | | | | | | | | | | | |
| 74.92 - 104.82 | WASTE | 29.90 | — | — | — | — | — | | | | | | | | | | | |
| 104.82 - 105.90 | 2258-G | 1.08 | 47 | .4 | 7 | 88 | 3 | | | | | | | | | | | |
| 105.90 - 106.70 | 2259-G | 0.80 | 39 | .6 | 16 | 90 | 8 | | | | | | | | | | | |
| 106.70 - 107.30 | 2260-G | 0.60 | 33 | .4 | 4 | 125 | 8 | | | | | | | | | | | |
| 107.30 - 108.00 | 2261-G | 0.70 | 10 | .4 | 8 | 122 | 8 | | | | | | | | | | | |
| 108.00 - 108.51 | 2262-G | 0.51 | 6 | .3 | 11 | 100 | 15 | | | | | | | | | | | |
| 108.51 - 109.55 | 2263-G | 1.04 | 5 | .3 | 9 | 77 | 12 | | | | | | | | | | | |
| 109.55 - 110.33 | 2264-G | 0.78 | 1 | .2 | 5 | 38 | 14 | | | | | | | | | | | |
| 110.33 - 111.29 | 2265-G | 0.96 | 1 | .2 | 6 | 63 | 13 | | | | | | | | | | | |
| 111.29 - 111.73 | 2266-G | 0.44 | 8 | .1 | 8 | 74 | 9 | | | | | | | | | | | |
| 111.73 - 112.00 | 2267-G | 0.27 | 1 | .3 | 9 | 104 | 10 | | | | | | | | | | | |
| 112.00 - 113.00 | 2268-G | 1.00 | 1 | .4 | 7 | 91 | 10 | | | | | | | | | | | |
| 113.00 - 141.12 | EOH | 28.12 | | | | | | | | | | | | | | | | |

GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG

Page 1 of 8

Property: UNUK K Project No: 134 Depth: 138.68 m Date begun: 08/09/90
 Hole No: AP 12 Co. ord.: 1240 N Horizontal Length: Date Completed: SEPT 9/90
 Claim No: UNUK 26 094 W Core Size: B6BDM Drilled By: J.T. THOMAS
 Grid No: ZONE 1 Angle & Direction: -45°/Az 20 Elevation: 1244 m Logged By: B. GABOURY

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| 0 - 3.96 | Casing | | | | | | | | |
| 3.96 - 35.05 | Fossiliferous Greywacke | | | | | | | | |
| | A medium dark to dark grey (N4 - N3) siltstone/arenite with white carbonate pelecypod casts plus occasional intervals with darker colored wispy finer grained, subangular cherts (argillite or chloritized volcanic fragments) up to ~ 2cm diameter. The rock has a very weak fabric probably indicative of bedding. Overall it contains ≤ 1% pyrite plus minor blocky, rubbly intervals (faults). It generally becomes finer grained downhill: | | | | | | | | |
| | 8.05 - 14.33 : Fault ; rusty rubbly core & clayey gouge ; 30% core recovery. | | | | | | | | |
| | 23.00 - 29.57 : Fault ; broken core & gouge, 45-50% core recovery. | | | | | | | | |
| 35.05 - 37.00 | Andesite Dike | | | | | | | | |
| | A medium fine grained, massive, medium grey (N5) to greenish grey (5G 1) igneous rock with ≤ 1% pyrite as disseminations and as blebs in occasional quartz-carbonate veinlets up to ~ 3mm in diameter. The host rocks at both contacts is brecciated and contains minor accumulations of pyrite. There is a dominant fracture / carbonate veinlet set at ~ 45° to the core axis in the centre of the vein | | | | | | | | |
| | C.A. 17.80 m : 68° fabric (bedding) | | | | | | | | |
| | C.A. 20.80 m : 63° fabric (bedding) | | | | | | | | |
| | C.A. 32.40 m : 65° fabric | | | | | | | | |
| | C.A. 35.05 m : 15° contact. | | | | | | | | |

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

20,390


**GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG**

Page 4 of 8

 Property Project No. Depth Date Began
 Hole No. **AP 12** Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | impregnation. Contains 7-10% pyrite, trace chalcopyrite, trace dark metallic sulfide (tetrahedrite?) plus a reddish earthy mineral (cinnabar or hematite) | | | | | | | | |
| | CA. 59.10 m : 25° lower vein contact | | | | | | | | |
| 62.10 - 69.30 | Interval is composed of 75% tuffaceous mudstone & 25% of short intercalations of massive black argillite. | | | | | | | | |
| 69.30 - 69.66 | sheared tuffaceous horizon with 3-5% disseminated pyrite. | | | | | | | | |
| 69.66 - 74.90 | Black Argillite A generally massive fine grained sedimentary rock with 2-4% py as irregular patches of fine grained impregnation up to 3 cm across. | | | | | | | | |
| | CA 64.80 m : 23° fabric/shearing. | | | | | | | | |
| | CA 66.20 m : 37° fabric | | | | | | | | |
| | CA 69.30 m : 25° fabric/shearing | | | | | | | | |
| | CA 72.45 m : 20° pink carb - quartz vein | | | | | | | | |
| 74.90 - 118.93 | Interbedded Black Argillite/Siltstone & Tuffaceous Mudstone similar to interval 54.00 - 69.66 | | | | | | | | |
| 82.86 - 86.05 | massive black argillite interbed with irregular impregnation patches similar to those encountered in interval 69.66-74.90 | | | | | | | | |
| | CA 78.00 m : 33° fabric | | | | | | | | |
| | CA 79.95 m : 28° fabric | | | | | | | | |
| | CA 81.00 m : 30° fabric | | | | | | | | |


**GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG**

Page 5 of 8

 Property Project No. Depth Date began
 Hole No. **AP 12** Co ord. Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | CA 87.90 m : 25° fabric/shearing. | | | | | | | | |
| 93.00 - 93.80 | : sheared, carbonate-altered interval with crushed core & gouge (93.48-93.57). Peripheral to crushing is an envelope of brecciation and carbonate veining. Overall, interval contains 2-3% pyrite (top 20cm ~5% py) | | | | | | | | |
| | CA 93.57 m : 30° shearing | | | | | | | | |
| 96.62 - 111.15 | : The rock becomes more an interbedded tuffaceous mudstone and siltstone with minor black argillite interbeds. The siltstone intercalations are generally finely laminated, but laminations have been dismembered & distorted by brecciation & shearing. The siltstone appears to be greywacke (fairly high volcanic component) and locally becomes arenaceous. Overall, interval contains ~1% pyrite. | | | | | | | | |
| | CA 102.00 m : 33° fabric | | | | | | | | |
| | CA 106.00 m : 30° fabric | | | | | | | | |
| | CA 109.00 m : 30° fabric | | | | | | | | |
| 111.15 - 116.95 | : sheared interbedded andesite ash-lapilli tuff & argillite & siltstone. | | | | | | | | |
| | 111.15 - 111.60 : more sheared, sericitized & silicified, tuffaceous interval with 2-5% pyrite as disseminations, blebs & discontinuous stringers. Rock is composed of 35-40% sericitized lapilli in a light grey green ash matrix. | | | | | | | | |
| | 111.60 - 114.00 : a variably sheared, sericitized & silicified tuff similar to | | | | | | | | |

Property Project No Depth Date Began
 Hole No. **AP 12** Co ord Horizontal Length Date Completed
 Claim No Core Size Drilled By
 Grid No Angle & Direction Elevation Logged By

| INTERVAL FEET / METRES | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|---|---------------|----------|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | 111.15 - 111.60 with ~ 5% pyrite as blebs, impregnations, disseminations & occasional short irregular stringers. | | | | | | | | |
| | 114.00 - 114.75 : 7-10% py mainly as coarse blebs within roughly concordant grey carbonate-pyrite veinlets comprising > 30% of the interval. Possible trace fine arsenopyrite. Hostrock appears to be tuffaceous mudstone | | | | | | | | |
| | 114.75 - 115.95 : 3-5% pyrite as disseminations, blebs & irregular stringers often subparallel to the fabric. The interval includes narrow carbonate-pyrite breccia veins up to 2cm wide generally concordant with the fabric. | | | | | | | | |
| | 115.95 - 116.95 : a crushed & sheared interval with gouge. Shearing appears to follow core axis. The interval contains 4-6% pyrite as disseminations & blebs in quartz-carbonate stringers. Hostrock appears to be a siltstone exhibiting brecciation & numerous anastomosing grey carbonate vth. | | | | | | | | |
| CA. | 111.60 m | 28° | shearing | | | | | | |
| CA. | 113.50 m | 45° | fabric | | | | | | |
| CA. | 115.00 m | 45° | fabric | | | | | | |
| CA. | 116.90 m | 17° | fabric | | | | | | |


**GRANGES EXPLORATION LTD.
DIAMOND DRILL LOG**

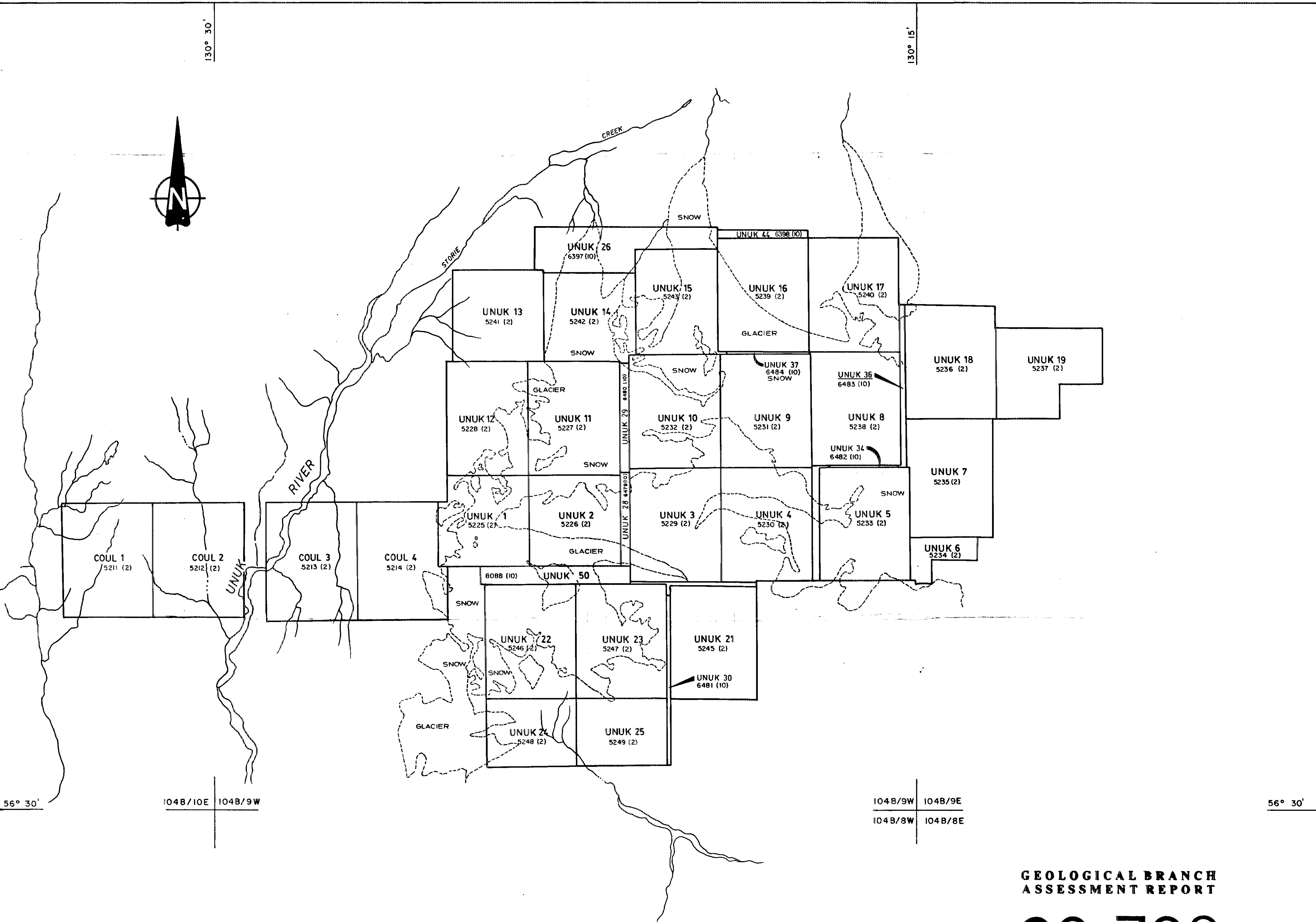
Page 8 of 8

Property Project No Depth Date Began
 Hole No. **AP 12** Co ord Horizontal Length Date Completed
 Claim No. Core Size Drilled By
 Grid No. Angle & Direction Elevation Logged By

| INTERVAL FEET (METRES) | DESCRIPTION | SAMPLE RECORD | | | | | | | |
|---------------------------|--|---------------|----|-------|--------|-----|-----|-----|-----|
| | | FROM | TO | WIDTH | SAMPLE | Au. | Ag. | Cu. | Zn. |
| | 121.73 - 122.20 : a relatively intensely brecciated interval with white/grey carb ± pyrite fracture infilling. | | | | | | | | |
| | 123.70 - 138.68 : mildly brecciated | | | | | | | | |
| | CA 119.70 m : ~ 85° fabric (fine) | | | | | | | | |
| | CA 122.80 m : 45° fabric " | | | | | | | | |
| | CA 123.10 m : 5° fabric " | | | | | | | | |
| | CA 132.00 m : 80° fabric " | | | | | | | | |
| 138.68 | End of Hole | | | | | | | | |
| | Acid tests : 61.0m : 42.5° corrected | | | | | | | | |
| | 123.0 m : 40° corrected. | | | | | | | | |

130° 30'

130° 15'



56° 30'

104B/10E 104B/9W

104B/9W 104B/9E
104B/8W 104B/8E

56° 30'

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

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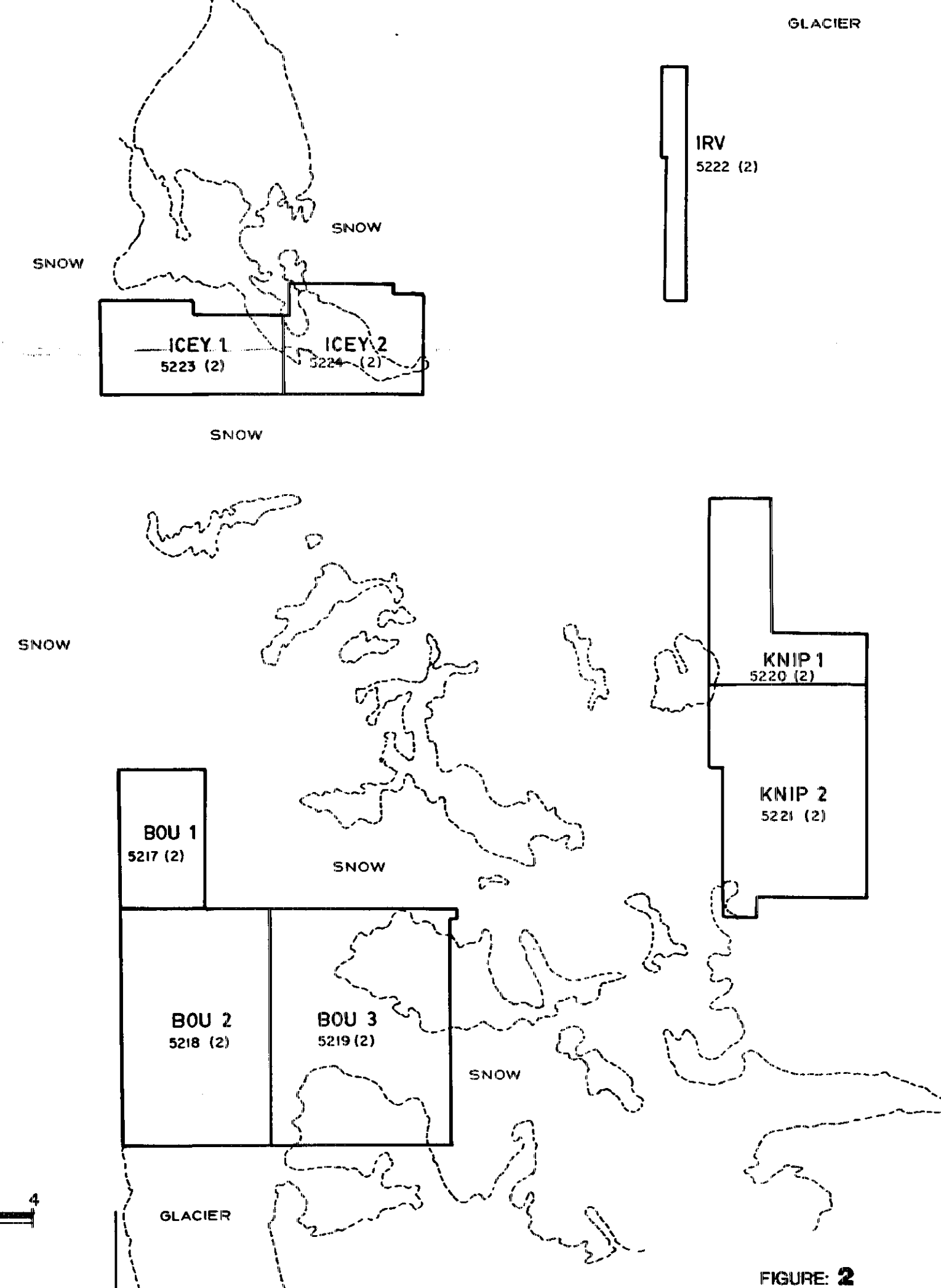


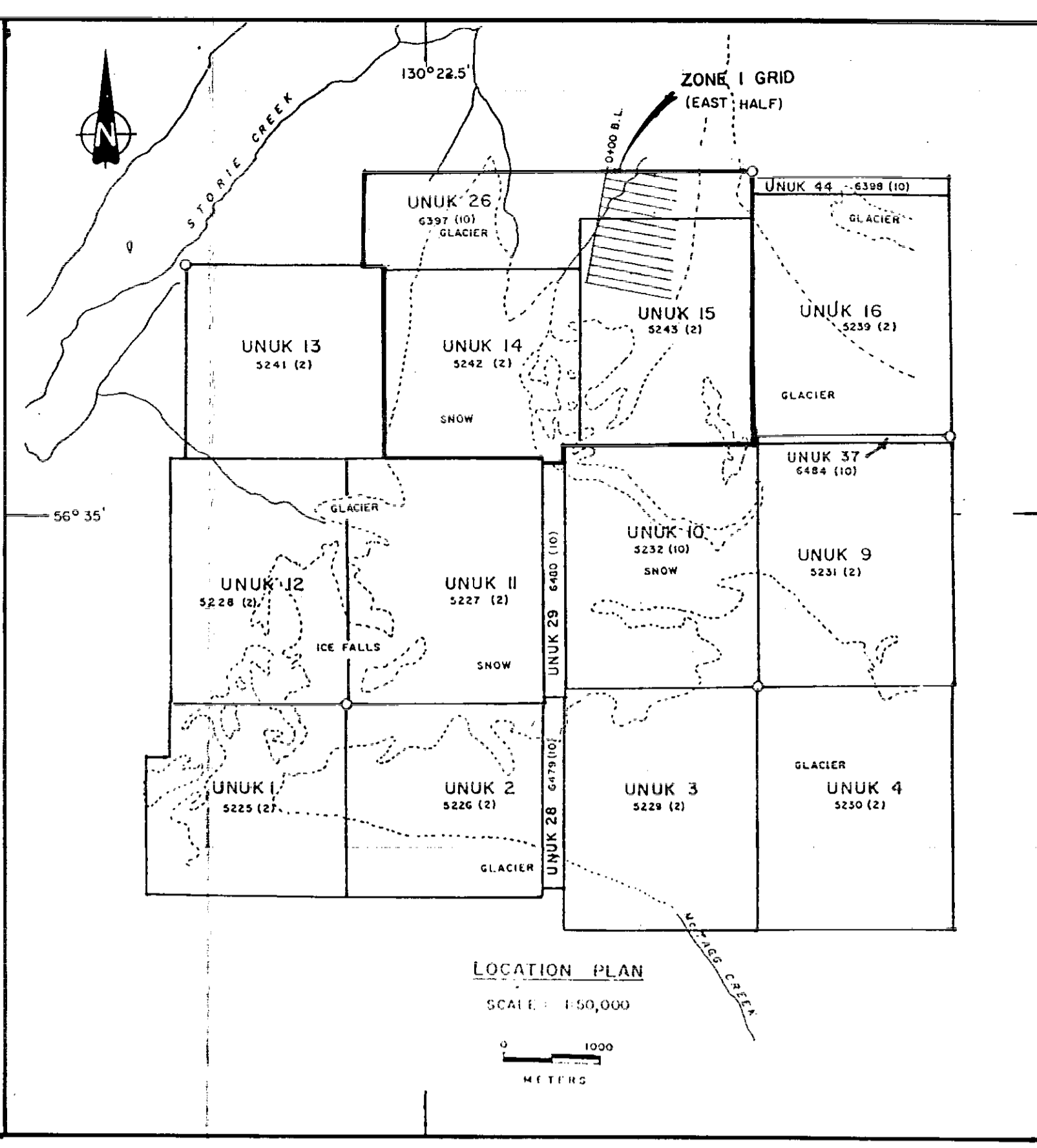
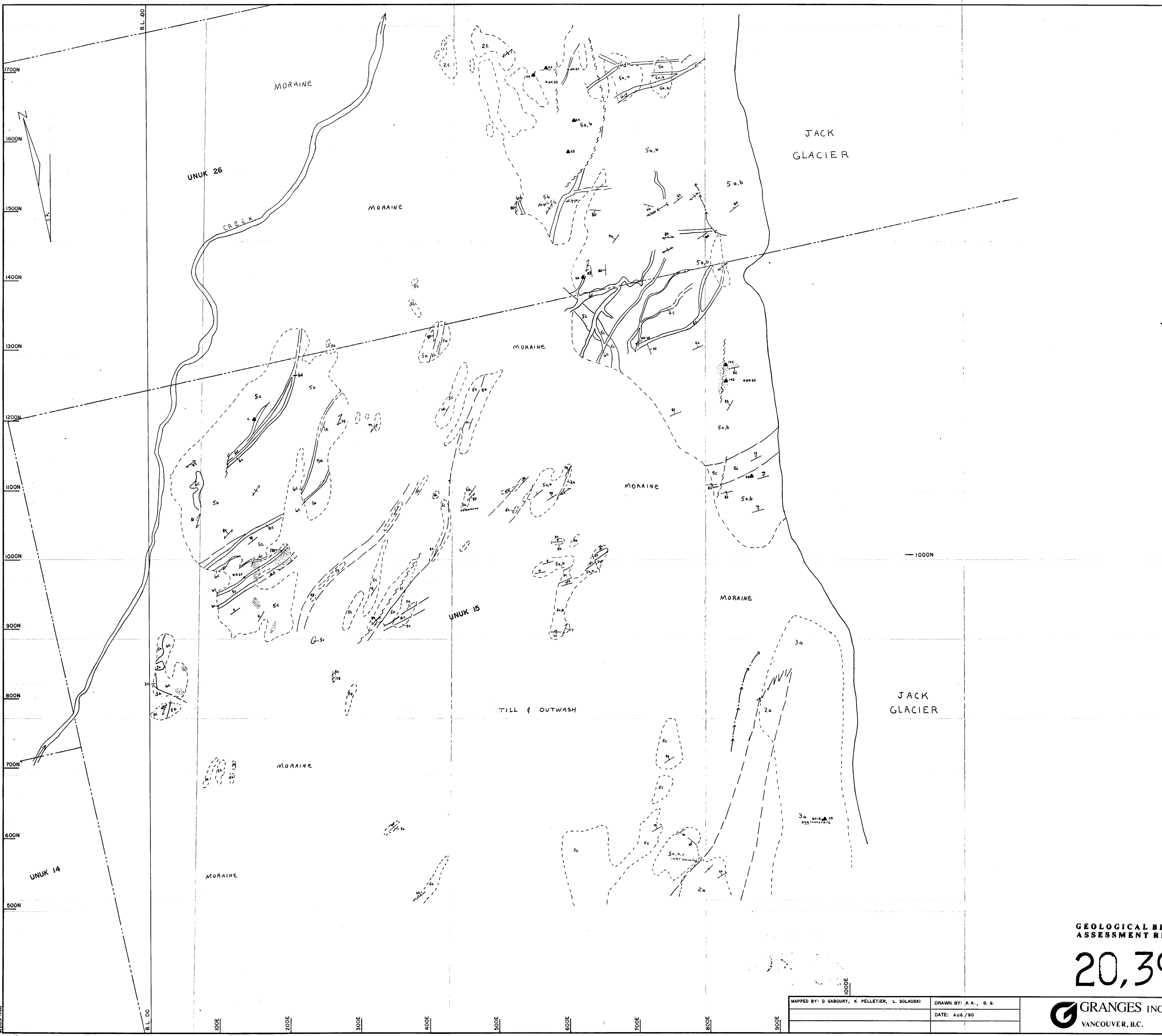
FIGURE: 2

DRAWN BY: PV/CU
DATE: JAN., 1990



CLAIM LOCATION MAP
UNUK OPTION
SKEENA MINING DIVISION, B.C.

SCALE: 1 : 50,000
PROJECT No.: 134
N.T.S.: 104B/9W



LEGEND

| | |
|---|--------------------|
| VOLCANIC ROCKS | |
| 1 Rhyolite | |
| 1a Rhyolite flow; massive, flow banded; spherulitic | 1b' lithic rich |
| 1b Rhyolite ash flow tuff; | 1c' lithic rich |
| 1c Rhyolite ash flow tuff; | |
| 1d Pyroclastic breccia, rhyolitic to rhyodacitic | |
| 1e Fine ash tuff, siliceous | |
| 2 Dacite | |
| 2a Dacite flow; massive, flow banded | 2b' lithic rich |
| 2b Dacite ash flow tuff; | |
| 2c Dacite lapilli tuff | |
| 2d Dacite pyroclastic breccia | |
| 2e Debris flow; argillaceous matrix | |
| 3 Andesitic | |
| 3a Andesite flow; massive, amygdaloidal; | 3a' porphyritic |
| 3b Andesite flow; pillowed; | 3b' pillow breccia |
| 3c Andesite lapilli tuff | |
| 3d Pyroclastic breccia, andesitic to dacitic | |
| 3e Fine ash tuff, andesitic to dacitic | |
| 4 Basaltic | |
| 4a Basalt flow; massive, amygdaloidal | |
| 4b Basalt flow; pillowed; | 4b' pillow breccia |
| SEDIMENTARY ROCKS | |
| 5 5a Mudstone, argillite | |
| 5b Siltstone, minor greywacke | |
| 5c Greywacke, minor arkose | |
| 5d Arkose, minor greywacke (and/or conglomerate) | |
| 5e Polymictic conglomerate | |
| 5f Epiclastic breccia | |
| 5g Debris flow breccia | |
| INTRUSIVE ROCKS | |
| 6 6a Feldspar porphyritic granodiorite | |
| 6b Augite porphyritic granodiorite | |
| 6c Diorite | |
| 6d Diabase | |

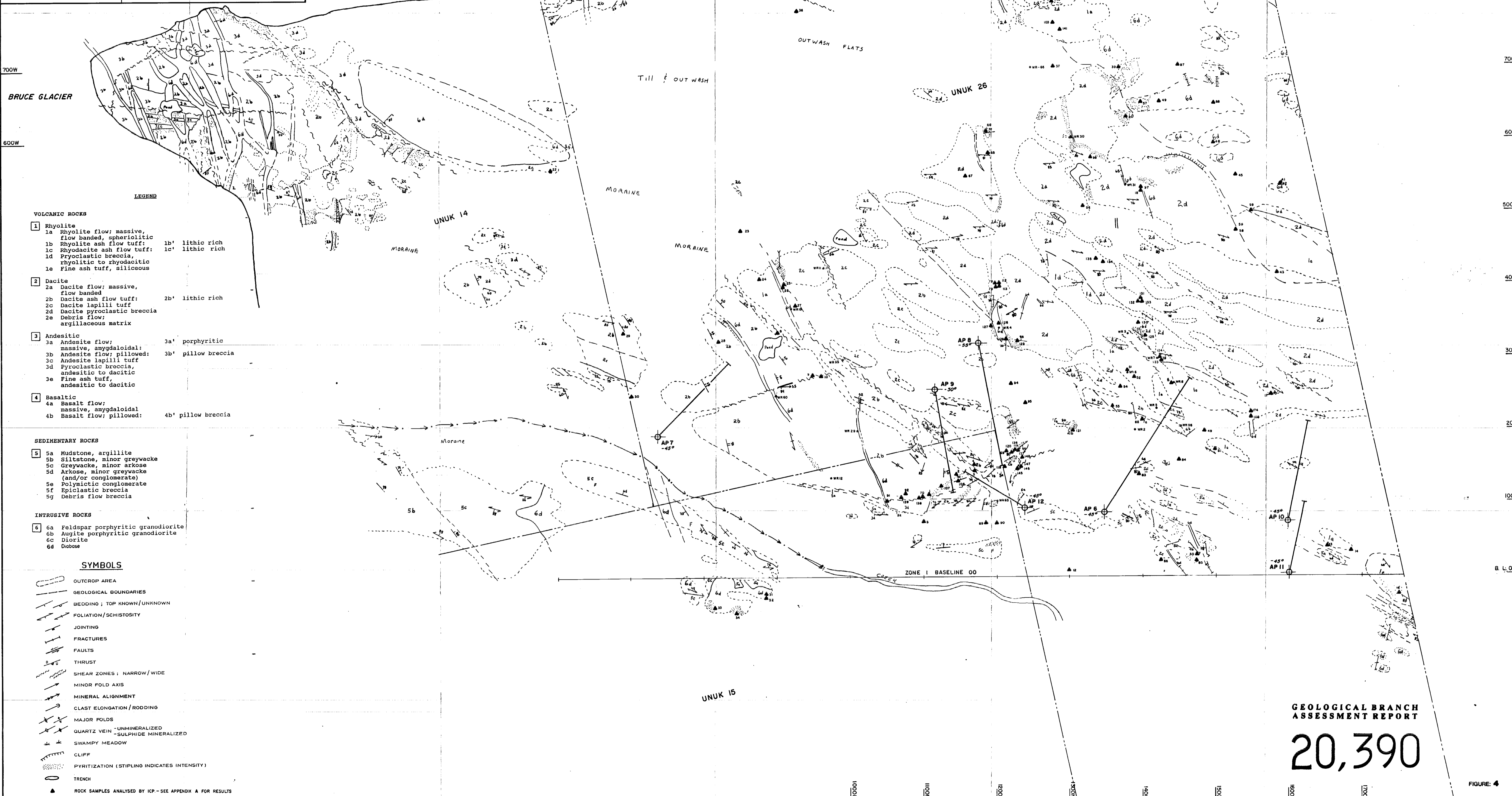
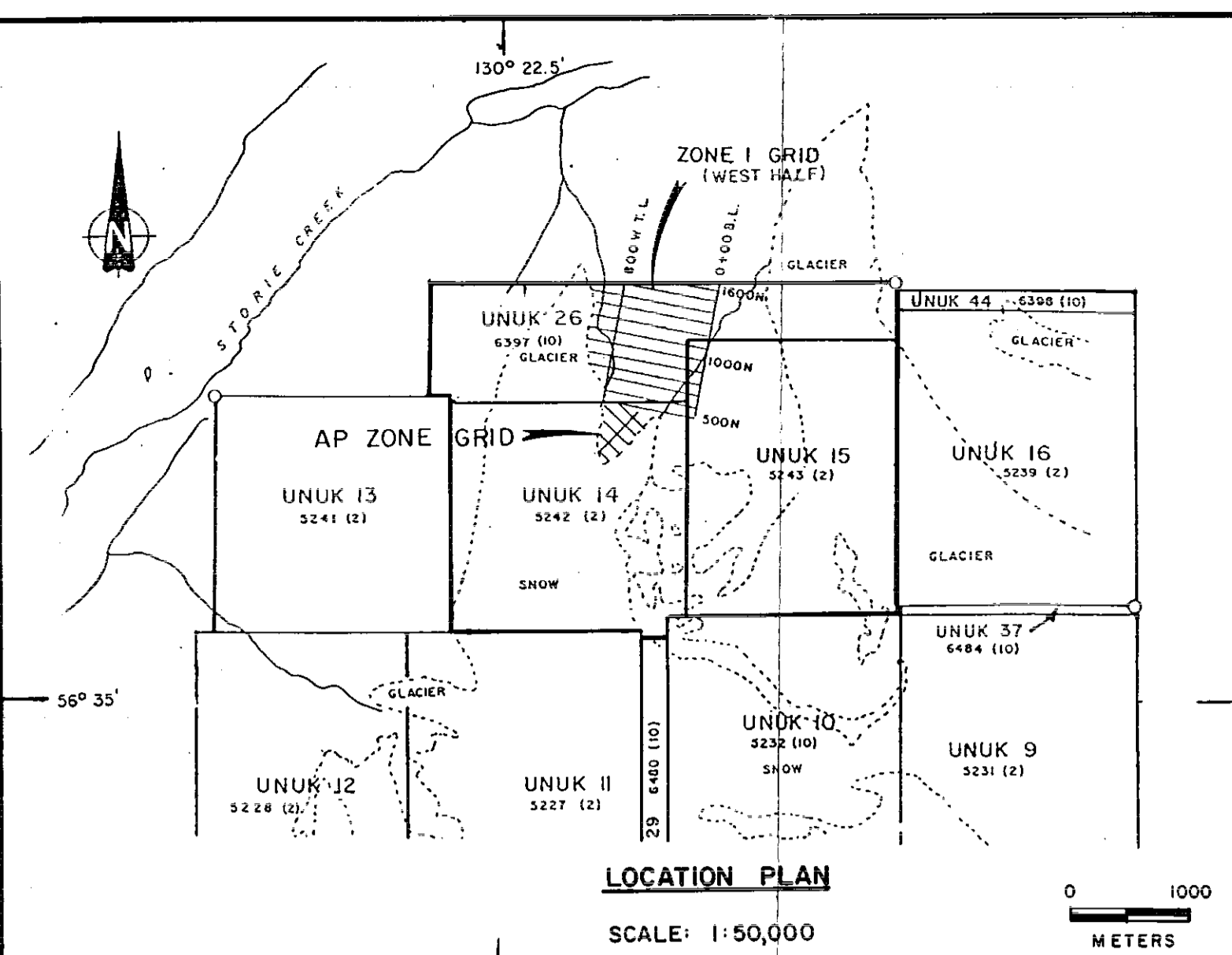
SYMBOLS

| | |
|--|--|
| | OUTCROP AREA |
| | GEOLOGICAL BOUNDARIES |
| | BEDDING; TOP KNOWN/UNKNOWN |
| | FOLIATION/SCHISTOSITY |
| | JOINTING |
| | FRACTURES |
| | FAULTS |
| | THRUST |
| | SHEAR ZONES: NARROW/WIDE |
| | MINOR FOLD AXIS |
| | MINERAL ALIGNMENT |
| | CLAST ELONGATION/RODDING |
| | MAJOR FOLDS |
| | QUARTZ VEIN - UNMINERALIZED |
| | QUARTZ VEIN - SULPHIDE MINERALIZED |
| | SWAMPY MEADOW |
| | CLIFF |
| | PYRITIZATION (STIPLING INDICATES INTENSITY) |
| | TRENCH |
| | ROCK SAMPLES ANALYSED BY ICP - SEE APPENDIX A FOR RESULTS |
| | WHOLE ROCK SAMPLES ANALYSED FOR COMPOSITION - SEE APPENDIX B FOR RESULTS |

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FIGURE 3



- VOLCANIC ROCKS**
- 1 Rhyolite
 - 1a Rhyolite flow: massive, flow banded, spherulitic
 - 1b Rhyolite ash flow tuff: lithic rich
 - 1c Rhyodacite ash flow tuff: lithic rich
 - 1d Pyroclastic breccia, rhyolitic to rhyodacitic
 - 1e Fine ash tuff, siliceous
 - 2 Dacite
 - 2a Dacite flow: massive, flow banded
 - 2b Dacite ash flow tuff: lithic rich
 - 2c Dacite lapilli tuff
 - 2d Dacite pyroclastic breccia
 - 2e Debris flow: argillaceous matrix
 - 3 Andesitic
 - 3a Andesite flow: massive, amygdaloidal: porphyritic
 - 3b Andesite flow: pillowed: pillow breccia
 - 3c Andesite lapilli tuff
 - 3d Pyroclastic breccia, andesitic to dacitic
 - 3e Fine ash tuff, andesitic to dacitic
 - 4 Basaltic
 - 4a Basalt flow: massive, amygdaloidal
 - 4b Basalt flow: pillowed: pillow breccia

- SEDIMENTARY ROCKS**
- 5 5a Mudstone, argillite
 - 5b Siltstone, minor greywacke
 - 5c Greywacke, minor arkose
 - 5d Arkose, minor greywacke (and/or conglomerate)
 - 5e Polymictic conglomerate
 - 5f Epiclastic breccia
 - 5g Debris flow breccia

- INTRUSIVE ROCKS**
- 6 6a Feldspar porphyritic granodiorite
 - 6b Augite porphyritic granodiorite
 - 6c Diorite
 - 6d Gabbro

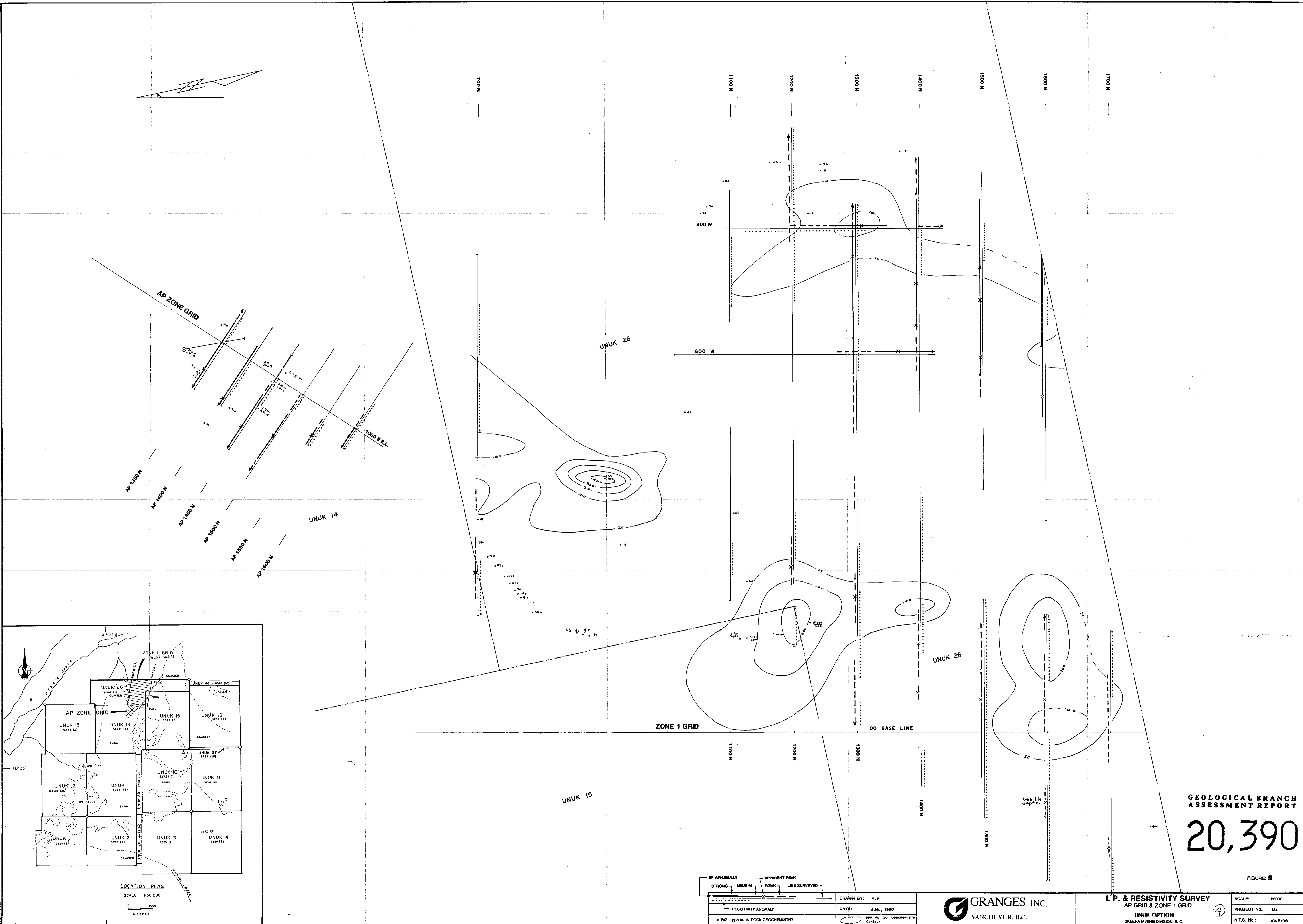
- SYMBOLS**
- OUTCROP AREA
 - GEOLOGICAL BOUNDARIES
 - BEDDING; TOP KNOWN/UNKNOWN
 - FOLIATION/SCHISTOSITY
 - JOINTING
 - FRACTURES
 - FAULTS
 - THRUST
 - SHEAR ZONES: NARROW/WIDE
 - MINOR FOLD AXIS
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 - CLAST ELONGATION/RODDING
 - MAJOR FOLDS
 - QUARTZ VEIN - UNMINERALIZED
 - QUARTZ VEIN - SULPHIDE MINERALIZED
 - SWAMPY MEADOW
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 - PYRITIZATION (STIPLING INDICATES INTENSITY)
 - TRENCH
 - ROCK SAMPLES ANALYSED BY ICP - SEE APPENDIX A FOR RESULTS
 - WHOLE ROCK SAMPLES ANALYSED FOR COMPOSITION - SEE APPENDIX B FOR RESULTS

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ASSESSMENT REPORT

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FIGURE 4

| | | | | |
|---|-----------------|--|--|------------------|
| MAPPED BY: D. GABOURY, B. GABOURY, K. PELLETHIER, L. SOLKOSKI | DRAWN BY: D. G. | | GEOLOGY & DIAMOND DRILLING ZONE 1 GRID (WEST HALF) & AP ZONE UNUK OPTION SKEENA MINING DIVISION, B.C. | SCALE: 1:2000 |
| | DATE: Aug./90 | | | PROJECT No.: 134 |



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FIGURE 5

IP ANOMALY
STRONG - MEDIUM - WEAK - LINE SURVEYED

RESISTIVITY ANOMALY
+ #10 ppb Au IN ROCK GEOCHEMISTRY

DATE: AUG., 1990

DRAWN BY: M.P.

20 ppb Au Soil Geochemistry Contour

GRANGES INC.
VANCOUVER, B.C.

I.P. & RESISTIVITY SURVEY
AP GRID & ZONE 1 GRID
UNUK OPTION
SKEENA MINING DIVISION, B.C.

SCALE: 1:2000
PROJECT No.: 134
N.T.S. No.: 104 B/9W

LOCATION PLAN
SCALE: 1:50,000

0 1000 METERS