

ATTNOOD GOLD CORPORATION

REPORT ON A SOIL GEOCHEMICAL<br>SURVEY ON THE WINNIPEG-GOLDEN CROWN-HARTFORD AREA OF THE<br>GOLDEN CROWN PROJECT<br>Greenwood Mining Division<br>B.C.



NTS:
LATITUDE:
82E/2E
LONGITUDE:
AUTHOR:
DATE OF WORK:
DATE OF REPORT: October 1990

## TABLE OF CONTENTS

Page
INTRODUCTION ..... 1
PROPERTY ..... 1
Table I (Description of Properties) ..... 2
PREVIOUS WORK ..... 4
LOCATION \& ACCESS ..... 6
GEOLOGY \& MINERALIZATION ..... 6
SOIL GEOCHEMICAL SURVEY
Sample Collection. ..... 7
Analysis. ..... 7
Plotting. ..... 7
DISCUSSION OF RESULTS
Geology \& Soil Contamination. ..... 8
Gold Geochemistry. ..... 8
Copper Geochemistry. ..... 10
Arsenic Geochemistry ..... 11
CONCLUSIONS \& RECOMMENDATIONS ..... 12
CERTIFICATE ..... 13
APPENDIX A (Geochemical Analysis Certificates)
APPENDIX B (Cost Statement)
IN POCKET (Figures 3 to 9 inc\}.)

## INTRODUCTION

The Golden Crown Project, located 5 km East of Greenwood B.C., incorporates the historic Winnipeg and Golden Crown gold-copper mines. The Winnipeg is reported to have been the largest gold mine in the Phoenix-Greenwood Camp.

Following the closure of the smelters at Greenwood and Grand Forks in 1919, other than limited production in the early 1930's and late 1940's, little recorded work was done on the Winnipeg-Golden Crown area until the mid 1970's.

Since that time, various geochemical and geophysical surveys have been conducted over portions of the 4.3 km long zone of gold bearing sulphide veins, a 782 meter adit was driven to provide underground access to the Winnipeg-Golden Crown area, extensive trenching and some 220 surface and underground diamond drill holes have been completed.

In the North Western portion of the gold vein zone, the Crown II area, Noranda Exploration Company Limited carried out a comprehensive exploration program in 1986 and 1987. This work consisted of line cutting, soil geochemistry, geologic mapping, magnetic, VLF-EM and IP geophysical surveys, trenching and Diamond and Reverse Circulation drilling. A number of attractive gold sulphide veins were discovered but Noranda returned the property without pattern drilling to define reserves.

In the South Eastern portion of the property, the Winnipeg-Golden Crown-Hartford area, similar work was intermittently carried out on small flagged chain and compass grids which have since been obliterated by time and logging activity.

In May 1990, White Geophysical Inc. extended the Noranda grid to the SE over the Winnipeg-Golden Crown-Hartford area and carried out magnetic and VLF-EM geophysical surveys. A geochemical survey, the subject of this report, was carried out under the direction of the Author as part of the program to develop a consistant, comprehensive geologic data base for the known area of gold-sulphide veins.

## PROPERTY

The property consists of two Crown Grants, twelve Reverted Crown Grants, of which two have private surface ownership, forty four two-post claims and fractions, and two four-post mineral claims totalling 18 units.

These claims are listed on table I and their relative positions are shown on figure 1.

The Crown No. 3 claims appear to have overstaked the Wendy No. 3 claim.


TABLE I

## 0

## DESCRIPTION OF PROPERTIES

Name Lot No. Record No. Expiry Date

Crown Granted Mineral Claims

| Golden Crown | 600 | N/A | N/A |
| :--- | :--- | :--- | :--- |
| Winnipeg | 599 | N/A | N/A |

Reverted Crown Granted Mineral Claims and Fractions

| Hecla | 859 | 1772 | December 12, 1994 |
| :---: | :---: | :---: | :---: |
| War Cloud Fr. | 1316 | 1773 | December 12, 1994 |
| Hard Cash | 1062 | 1774 | December 12, 1994 |
| Nabob Fr. | 1063 | 1774 | December 12, 1994 |
| Joe Joe | 7595 | 1775 | December 12, 1994 |
| Sissy | 1068 | 1776 | December 12, 1994 |
| Calumet | 1314 | 1777 | December 12, 1994 |
| $J$ \& R | (L.1059) | 1865 | November 8, 1991 |
| Silver Star | (L. 1550 ) | 1926 | December 21, 1991 |
| Hartford | (L. 1057) | 1927 | December 21, 1990 |
| Hartford Fr. | (L. 1061 ) | 1928 | December 21, 1990 |
| Nellie Cotton | (L.7460) | 2173 | May 13, 1993 |

Mineral Claims

| Win Fr. |  |  |
| :--- | :--- | :--- |
| Attwood No. 1 Fraction | 1784 | September 24, 1994 |
| Add No. 2 (12 units) | 4243 | February 25, 1996 |
| Ike 1 | 4615 | June 23, 1995 |
| Ike 2 | 1972 | January 23, 1994 |
| Ike 3 | 1973 | January 23, 1994 |
| Ike 4 | 1974 | January 23, 1994 |
| Ike 5 | 1975 | January 23, 1994 |
| Ike 6 | 1976 | January 23, 1994 |
| Ike 7 | 1977 | January 23, 1994 |
| Ike 8 | 1978 | January 23, 1994 |
| Ike 9 | 1979 | January 23, 1994 |
| Ike 10 | 2023 | February 6, 1994 |
| Ike 11 | 2024 | February 6, 1994 |
| Ike 12 | 2025 | February 6, 1994 |
|  |  | 2026 |


| Crown 1 | 1986 |
| :--- | :--- |
| Crown 2 | 1987 |
| Crown 3 | 1988 |
| Crown 4 | 1989 |
| Crown 5 | 1990 |
| Crown 6 | 1991 |
| Crown 7 | 1992 |
| Crown 8 | 1993 |
| Crown 9 | 2015 |
| Crown 10 | 2016 |
| Crown 17 | 2017 |
| Crown 13 | 2018 |
| Crown 14 | 2019 |
| Crown 14 | 2020 |
| Crown 15 | 2021 |
| Crown 16 | 2022 |
| Crown 17 | 2202 |
| Crown 18 | 2203 |
| Crown 19 | 2204 |
| Hip Fr. | 2199 |
| Go1den Crown Fr. | 2200 |
| Star Fr. | 2201 |
| Crown Fr. | 2027 |
| Mikro (6 units) | 4426 |
| Knob 1 | 4435 |
| Knob 2 | 4436 |
| Knob 3 | 4437 |
| Knob 4 | 4438 |
| Knob 5 | 4439 |
| Knob 6 | 4440 |
| Knob 7 | 4441 |
| Knob 8 | 4536 |
| Mikro 2 | 4537 |
| Mikro 3 |  |

Being seventy-one mineral claims, in the Greenwood Mining Division, Province of British Columia.

PREVIOUS WORK

The history of the Golden Crown Project area dates back to 1891 when the low grade copper deposits at Phoenix, immediately north of the Golden Crown project property, were discovered and the Winnipeg and Golden Crown claims were staked.

Details on the original work in the project area are sketchy.
Considerable development work had been completed on the Winnipeg and Golden Crown properties by 1896 and three years later it is reported that the Winnipeg shaft had been sunk to 300 ft with 275 ft of development completed on the 100 ft level as well as the cutting of a station on the 200 ft level. On the adjacent Golden Crown claim, the shaft had also reached 300 ft and levels developed at $100 \mathrm{ft}, 150 \mathrm{ft}$ and 300 ft . By 1901, a 250 ft shaft had been sunk on the Hartford vein and 150 ft of cross cutting and drifting completed.

Work on the $J \& R$ claim between the Hartford claim and the Golden Crown claim consisting of " 75 ft of shafting and Cross Cutting" had been completed.

On the Winnipeg and Golden Crown, production was reported in the 1901-1903 period and again in 1910-1912.

In 1919 a strike by coal miners resulted in the closure of the smelters in Greenwood and Grand Forks and the large copper mines at Phoenix.

No activity is reported on the Golden Crown property between 1912 and 1938. During 1938 and the following three years, small tonnages of ore were shipped, probably from near surface stopes, on the McArthur Vein.

The property then lay idle until 1965 when Sabina Mines and Scurry Rainbow carried out geophysical surveys and diamond drilling over a four year period, mainly looking for nickel in serpentinites.

In 1970 Granby, which had reactivated the Phoenix mines as an open pit operation, carried out IP surveys and possibly some drilling on the Wendy Group which included much of the present property northwest of the Golden Crown claim.

Since 1976 activity on the project area has been more or less continuous, as tabulated below:

1976: Golden Crown Syndicate drilled four holes.
1977-1978: Con Am Resources optioned the property and drilied four holes.
1979: Consolidated Boundary Exploration drilled four holes.
1980: The Winnipeg Golden Crown area was optioned by Mundee Mines, which among other things dewatered the Golden Crown shaft to the 100 ft level and drilled 16 holes. Two holes were drilled on the J \& R claim by others.

1981: A further nine holes were drilled by Mundee Mines on the Winnipeg Golden Crown area, while Argenta Resources carried out geophysical surveys and drilled four holes on the J \& R fraction.

1982: No activity.
1983: Geophysical and geochemical surveys were completed on the Winnipeg Golden Crown area along with backhoe trenching and 18 diamond drill holes.

1984: Consolidated Boundary drilled four or more holes on the Winnipeg Golden Crown claims and 12 holes on the $J \& R$ fraction.

1985: Four holes were drifled on the Golden Crown and five on the Crown No. 6 claim in an area of old workings labled the northwest zone. These workings may be the Bald Eagle workings shown on the geological map accompanying G.S.C. paper $45-20$ by D.A. McNaughton.

1986: On the Winnipeg Golden Crown area, Consolidated Boundary/Grand Forks Mines drilled 17 holes, mainly on the south zone. The area west of Golden Crown claims was optioned to Noranda Exploration Ltd. Noranda established a large grid on the south flank of Knob Hill, carried out geological, geochemical and geophysical surveys, excavated 26 trenches and drilled five diamond drill holes. This work may have rediscovered the Red Rock showings that are located on McNaughton's map.

1987: Noranda completed three diamond drill holes and ten Reverse Circulation drill holes on their portion of the property while Consolidated Boundary/Grand Forks drilled a reported ten holes. In September 1987, a trackless adit was collared on the eastern boundary of the calumet CTaim. At year end the adit had advanced about 444 meters and one underground drillhole completed to locate the flooded Winnipeg workings.

1988: The trackless adit was completed at 782 meters from the portal. In early 1988 crosscuts were driven to the Golden Crown shaft, the King Vein, to drill stations and to the expected location of the Winnipeg shaft. A raise was also completed to the Golden Crown 100 ft level. During the year, 48 diamond drill holes were completed underground and 12 were completed from the surface. Attwood Gold Corp. became the sole owner of the project.

1989: The development program was completed early in the year with the drilling of an additional 14 holes from surface and five from underground.

In May, R.H. Seraphim, Ph.D., P.Eng. estimated the reserves in the Winnipeg Golden Crown area at 62,670 tons grading $0.445 \mathrm{oz} \mathrm{Au/ton}$, oz Ag/ton and $0.7 \% \mathrm{Cu}$.

## LOCATION \& ACCESS

The Goiden Crown Project area is located 5 km West of Greenwood, B.C. or 13 km North West of Grand Forks, B.C. Access to the property from Highway No. 3, the Southern Trans Provincial or Crowsnest Highway, is via the Phoenix Mine road to the site of the old town of Phoenix and thence South from the Phoenix Cenotaph along the Lone Star Haul road for 3 km to the property. (figures 2 and 9).

Access on the property is primarily via a network of old railroad grades, now used as roads, which radiate out from Hartford Junction, a major railroad junction complex from the 1900 's.

Secondary 4 wheel drive access is provided by more recent logging roads that branch off the old railroad grades.

## GEOLOGY \& MINERALIZATION

The property is dominantly underiain by Paleozoic sediments and volcanics of the Attwood and Knob Hill groups. However, there appears to be no concurrence between regional mappers on the division between the Attwood and Knob Hill. For the purpose of this discussion, the Knob Hill group consists of the predominantly sedimentary package (siltstones, charts, conglomerates and minor intercalated intermediate volcanics that outcrop on the SW flank of Knob Hill in the NW corner of the property. A thin strip of Brooklyn sharpstone conglomerate, which unconformably overlies the Knob Hill, occurs along the North East edge of the Crown claims.

The balance of the property is predominately underlain by the metavolcanics of the Attwood group. This unit appears to consist of a thick succession of intermediate to basic volcanics variously regionally altered to the green schist or amphibolite facies. Both flow and pyroclastic textures are observed in drill core and outcrop. No marker horizons have been identified.

Dioritic, gabbroic and ultramafic rocks intrude both the knob Hill and Attwood groups. Locally, the dioritic intrusives may be coeval with the Attwood volcanics.

Serpentinized ultramafics outcrop in the central and southestern portion of the property with drill hole intercepts and exposures in underground workings show these serpentinites to be present at shallow depths under the Winnipeg/Gold Crown portion of the property.

Mineralization on the property consists of a North West - South East swarm or network of steep dipping quartz sulphide or massive sulphide veins which range in thickness from centimeters to several meters. Pyrrhotite and pyrite are the dominate sulphides with chalcopyrite and arsenopyrite being subordinate. Gold and silver are present in significant quantities. While some assay data suggests there may be a direct relationship between gold and arsenopyrite, metallurgical test work has shown that this relationship is not intimate.


Sample Collection:
Soil samples were collected with a mattock at 25 meter intervals along the grid lines spaced at 100 meters intervals. The samples were typically collected from the B soil layer at a depth of 10 to 17 cm and placed in a kraft soil envelope marked with the sample location's grid co-ordinates.

The sample co-ordinates, color, sampling depth, soil layer sampled, moisture and composition were recorded in a field book along with explanatory notes for locations where samples were not collected and notes on cultural features.

The sampling was carried out by Sonny Yip, B.A. supervised by Warren Robb, B.Sc., the project geologist.

The samples were then packed in cardboard boxes and taken to Acme Analytical Laboratories Ltd. for analysis.

Analysis:
The samples were dried at Acme Analytical Laboratories Ltd. and sieved at 80 mesh.

From the minus 80 mesh material, a 0.5 gram sub-sample was taken. This sample was digested with $3 \mathrm{ml} 3-1-2 \mathrm{HCL}-\mathrm{HNO} 3-\mathrm{H} 20$ at $85^{\circ} \mathrm{C}$ for 1 hour, diluted with 10 ml of water and the disolved elements $\mathrm{Mo}, \mathrm{Cu}, \mathrm{Pb}, \mathrm{Zn}, \mathrm{Ag}$, $\mathrm{Ni}, \mathrm{Co}, \mathrm{Mn}, \mathrm{Fe}, \mathrm{As}, \mathrm{U}, \mathrm{Au}, \mathrm{Th}, \mathrm{Sr}, \mathrm{Cd}, \mathrm{Sb}, \mathrm{Bi}, \mathrm{V}, \mathrm{Ca}, \mathrm{P}, \mathrm{La}, \mathrm{Cr}, \mathrm{Mg}, \mathrm{Ba}$, $T i, B, A 1, N a, K$ and $W$ determined by ICP-atomic emission spectroscopy. Results, see Appendix I, were reported in parts per million except for Fe, $\mathrm{Ca}, \mathrm{P}, \mathrm{Mg}, \mathrm{Ti}, \mathrm{Al}, \mathrm{Na}$ and K which were reported in percent.

Also from the minus 80 mesh fraction a 10 grams sub-sample was taken, ignited at $600^{\circ} \mathrm{C}$ for four hours, digisted with aqua rega at $95^{\circ} \mathrm{C}$ for one hour. A 50 ml aliquot was then extracted into 10 ml of MIBK. The MIBK solution was then analyzed for gold by graphite furnace Atomic Absorption at a lower detection limit of 1 ppb Au.

## Plotting:

The geochemical results on disk, together with a plan of the grid supplied by White Geophysical Inc., were taken to Geo-Comp Systems at 603-510 West Hastings Street, Vancouver, BC, where the data was entered into a computer aided drafting system and plots of the Cu, Au and As values produced at a scale of $1: 2500$ (figures 3,4 \& 5). The location of this grid, with respect to surface features, is shown on figure 9.

## DISCUSSION OF RESULTS

Geology \& Soil Contamination:
The area of the geochemical survey is predominantly underlain by "Greenstones" of the Paleozoic Attwood group which has, in the Eastern portion of the grid, been intruded by "01d" Diorite. On the property the "Greenstones" exhibit flow, pillow breccia and pyroclastic textures. Both the "Greenstones" and the "old" Diorite have been regionally altered to the green schist facies.

Serpentinized ultrabasic rocks of Jurassic or Cretaceous age outcrop South East of the grid area. Within this grid area, Serpentinites are exposed in the adit that was driven NW from near the Eastern limit of this grid, in deeper drill holes and in a trench at $4474+00 \mathrm{E}, 464+50 \mathrm{~N}$.

Numerous structurally controlled gold bearing sulphide veins or quartz-sulphide veins trend NW across this grid area.

The veins range in composition from near massive pyrrhotite with minor chalcopyrite and arsenopyrite to quartz-pyrite-chalcopyrite veins.

Overburden in this grid area consists of gray glacial till and varies in thickness from nil in outcrop areas to several meters. Local swamps have resulted in overlays of black organic muck in depressions.

Abandoned railway grades, now maily used as roads, cross the property in several directions. Waste rock from the copper mines at Phoenix, to the North of this grid, was used as fill and ballast. Copper responses on or adjacent to the old rail lines are thus suspect.

Mine dumps surrounding the collars of the Winnipeg, McArthur, Golden Crown and Hartford shafts are other sources of soil contamination.

Gold Geochemistry:
Aqua Riga-MIBK extractible gold in the minus 80 mesh fraction of the soil samples range from 1 ppb (the detection limit) to $18,400 \mathrm{ppD} \mathrm{Au}$, the latter taken from mine waste. Contoured Au values as shown on Plan yield a pronounced NW (grid E-W) trend, which as the Western margin of the grid is approached swings to the WNW.

Specific Au responses marked on the contoured plan (figure 6) as A-1 to A-12 are discussed below.

Au-1, Au-2:
These single sample responses (with copper correlation) are open to the NW Au-2 and are believed to be due to a gold-copper quartz vein intersected in drill holes GC 83-4 and GS 83-5.

Au-3:
This response which peaks at $L 460+00 E, 465+50 \mathrm{~N}$ can be interpreted to extend from $L 456+00 \mathrm{E} 464+00 \mathrm{~N}$ to $\mathrm{L} 462+00 \mathrm{E}, 466+00 \mathrm{~N}$. The possibility that this response is a continuation of $\mathrm{Au}-2$ should be investigated.

## Au-4:

This response correlates with the $J \& R$ Zone, previously tested by drilling with favourable results.

Au-5:
This gold response correlates with a massive sulphide vein exposed in a trench near $1474+00 \mathrm{E}, 464+25 \mathrm{~N}$. The vein was apparently tested by a number of short drill holes between line $1474+00$ and $475+00$ with mediocre results.

Au-6:
Geologic mapping indicates the Eastern extension of this Au geochemistry response was trenched in the vicinity of Line L474+00E. Fill-in geochemistry on lines $L 474+50, L 472+50, L 473+50$ is recommended to confirm the continuity of this response which has no apparent correlating geochemical or geophysical response.

Au-7:
This response was tested by drill holes $\mathrm{JR}-80-1$ and $\mathrm{JR}-80-2$, both holes intersected narrow zones of low grade gold-copper mineralization.

Au-8:
The Western continuation of this response on the Noranda grid was tested by trench CR-87-26 and drill hole RC-CR-87-10 with mediocre results.

Au-9:
This spotty response is South of the "South Zone" that was drill tested in 1976 and returned values to 1.260 oz Au/ton over a 4.0 foot core length. Follow up soil sampling and prospecting is warranted.

Au-10:
An old drill collar just East of L466+00E suggests this response was previously known but the results of the drilling have not been found. This geochemical response correlated with a sharp, near surface magnetic response and is crossed at a shallow angle by a VLF-EM conductor. Drill testing is warranted.
$\mathrm{Au}-11:$
This response consists of two strongly anomolous gold in soil responses $1,290 \mathrm{ppb} \mathrm{Au}$ at $\mathrm{L470+00E}, 460+00 \mathrm{~N}$ and $1,020 \mathrm{ppb}$ Au L473+00E, $460+25 \mathrm{~N}$. In the absence of fill in sampling the correlation of these responses is speculative.

Prospecting in the area of the highs is warranted.

## Au-12:

This response appears to be a continuation of a trend of scattered responses that were identified on the Noranda survey to the NW. Geologic mapping indicates shallow overburden thus prospecting for the source of the gold in the soil is indicated.

Copper Geochemi stry:
Copper values in soil vary from a low of 11 ppm to a high of $1,587 \mathrm{ppm}$ although the latter is contaminated with mine waste. Contoured copper values indicate a general NW -SE trend, similar to the gold trend. The copper responses marked on figure 7 are discussed below.

Cu-1:
This Copper in soil response correlates with the Calumet vein system that has been explored with trenches and drill holes.

Cu-2:
This response, which is open to the NW, correlates with Au-1.
Cu-3:
This strong, but somewhat vague, NNW trend that extends from L467+00, $466+25 \mathrm{~N}$ to $2470,464+75 \mathrm{~N}$ is likely a combination of contamination from mine waste and local bedrock sources. At the NNW end of the response, the high copper values correlate with $\mathrm{Au}-2$ and the intercepts in drill holes 83-4 and 83-5.

Cu-4:
This response is possibly due to the concentration of Cu in organic soils as it correlates with a small swamp.

Cu-5 A \& B:
These responses are possibly largely due to contamination from copper bearing railroad balast. Drill holes $3 R-80-1$ and $J R-80-2$ in response Cu-5A did intersect low copper values.

Cu-6 A, B \& C:
Responses 6 A and 6 C appear to be continuations of 6 B , the spotty response from the $J$ \& $R$ Zone. Care must be taken in further action on this response due to the proximity of old railroad grades to samples having high copper.
$\mathrm{Cu}-7,7 \mathrm{~B}:$
This branching response appears related to the Hartford $\mathrm{Au}-\mathrm{Cu}$ mineralized structure. The correlation of high copper values with magnetic spikes suggests pyrrhotite is associated with the copper. The Hartford vein was explored in the early 1900's by a shaft and underground levels. The proximity to old rail lines suggest the deposit may have shipped ore.

Cu-8:
The SW segment of this copper response correlates with a weak VLF-EM conductor.

Cu-9:
The correlation of this copper response with a VLF-EM conductor gives it added weight as a drill target.

Magnetic responses on lines $459+00 E$ and $461+00 E$ suggests pyrrhotite may be present locally.

## Arsenic Geochemi stry:

Arsenic Values range from a low of 2 ppm to a high of $52,128 \mathrm{ppm}$ in a sample contaminated by mine waste. Contoured Arsenic (figure 8) values show an overall WNW trend with the higher values concentrated in the NE quarter of the grid. Mapping and drill results show this area is underlain at a shallow depth by serpentinite and thus the higher arsenic values may be a function of proximity to this rock type.

Three arsenic responses, as discussed below, are interpreted from the contoured data.

AS-1:
This response correlates with the Northwesten continuation of the Calumet zone.

AS-2:
This low order response correlates with a gold bearing vein discovered in drilling in 1986.

AS-3:
This arsenic response correlates with the gold response Au-5 on line $474+00 E$. Copper values are also elevated. A massive sulphide vein (pyrrhotite \& pyrite) is exposed in a nearby trench. The vein has also been tested by diamond drilling with mediocre assay results.

While the soil results serve to highlight the potential of previously known and possibly inadequately tested veins, the soil survey did identify new targets.

These targets include gold responses $A u-9, A u-11$ and copper response Cu-9.

## CONCLUSION \& RECOMMENDATIONS

The 1990 soil geochemical survey has provided a consistant soil geochemical data base over the Winnipeg-Golden Crown-Hartford portion of the Golden Crown Project area. The contoured values for Copper, Gold and Arsenic show trends consistant with the known sulphide and quartz sulphide veins on the property. In many cases, the stronger soil geochemical responses correlate in part with known mineralization and the extent of the geochemical response is usefull in directing exploration along strike.

Three responses $\mathrm{Au}-9, \mathrm{Au}-11$ and $\mathrm{Cu}-9$ can be considered new discoveries in that no evidence of historic physical work directed at the sources of the responses has been found.

Follow up on these responses is warranted.

## CERTIFICATE

I. Gordon Melville Ford, of the City of Port Moody, Province of British Columbia, do hereby certify as follows:

1. I am a consulting Geological Engineer and President of Fordex Management Inc. with an office at 575 Garrow Drive, Port Moody, British Columbia.
2. I am a registered Professional Engineer in the Province of British Columbia.
3. I graduated with a degree of Bachelor of Science, Geology and Geophysics from the University of British Columbia in 1964.
4. I have practiced my profession for twenty six years.
5. I have no direct or contingent interest in Attwood Gold Corporation or any of the properties which comprise the Golden Crown Project.
6. This report is based on numerous field trips to the property, thorough review of the historical data, and observation of the field work being carried out. I have also observed a number of claim posts in the field, sufficient to conclude the property boundaries shown on the maps are reasonably accurate.
7. Written permission is required from Fordex Management Inc. to publish this report in any prospectus or statement of mateteqticacts.


Fordex Management Inc.
October 11, 1990

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## APPENDIX A <br> (GEOCHEMICAL ANALYSIS CERTIFICATES)

## CONTRACT SERVICES：

Soil Sampling：Sonny Yip（12 days）\＄1，094．02
Field Supervision：WR Geological Ltd．（3 days at $\$ 150.00 / \mathrm{day})$
450.00

Geochemical Analysis：Acme Analytical Lab．Ltd．
（ 689 Samples－30 element ICP Analysis
689 Geochem Au Analysis by Acid／each 10 grams） $5,936.15$

Field Expense：
1，235，97
Drafting
（Geo－Comp Systems）
480.00

Report Preparation：Fordex Management Inc．
（ 3 days at $\$ 300.00 /$ day $)$
900.00
$\$ 10,096.14$
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\frac{\text { APPEND I X B }}{\text { (COST STATEMENT) }}
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Attwood Gold Corp．PROJECT GOLDEN CROWN
File \＃90－1366
sutmit ted by： W ．ROQB

| SAMPLE空 | $\begin{aligned} & 10 \\ & \text { ppon } \end{aligned}$ | $\underset{\mathrm{Cum}}{\mathrm{Cu}}$ | pon | $\begin{aligned} & \mathrm{Zn} \\ & \mathrm{ppm} \end{aligned}$ | $\mathrm{Ag}$ | $\underset{\text { ppon }}{n}$ | Co | $\begin{gathered} \mathrm{Mn} \\ \mathrm{pqm} \end{gathered}$ | $\begin{gathered} \mathrm{Fe} \\ \mathbf{x} \end{gathered}$ | $\mathrm{Me}$ | $\begin{array}{r} \mathrm{U} \\ \text { ppon } \end{array}$ | $\underset{\text { ppom }}{\substack{\text { un }}}$ | Th ppon | $\underset{\mathrm{ppm}}{\mathrm{Sr}}$ | cd <br> pon | $\begin{array}{r} \text { Sb } \\ \text { ppin } \end{array}$ | $\begin{aligned} & \text { Bi } \\ & \text { ppm } \end{aligned}$ | $\begin{array}{r} V \\ \text { porn } \end{array}$ | $\begin{gathered} \mathrm{CB} \\ \mathrm{y} \end{gathered}$ | $\begin{array}{r} \mathbf{p} \\ \mathbf{x} \end{array}$ | $\begin{array}{r} \mathrm{LB} \\ \hline \mathrm{pqm} \end{array}$ | $\begin{gathered} \mathrm{Er} \\ \text { ppm } \end{gathered}$ | $\mathbf{M g}$ | $\begin{gathered} \mathrm{Ba} \\ \mathrm{ppom} \end{gathered}$ | $\mathrm{T} 5$ | $8$ | $\begin{aligned} & \text { Al } \end{aligned}$ | $\begin{aligned} & \mathrm{M} \\ & \mathbf{z} \\ & \hline \end{aligned}$ | $\mathbf{x}$ | 鼻娚 | $\begin{aligned} & \text { pat } \\ & \text { pph } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L456E 468000m | 1 | 82 | 14 | 56 | 2 | 25 | 14 | 964 | 2.28 | 20 | 5 | M 0 | 3 | 36 | 2 | 2 | 2 | 32 | ． 44 | $\times 061$ | 8 | 18 | .31 | 193 | 4 |  | 2.54 | ． 03 | ． 09 | 1 |  |
| L456E 465475\％ | 1 | 74 | 19 | 58 | 3 | 22 | 15 | 1283 | 2.20 | 25 | 5 | 10 | 2 | 34 | 4 | 2 | 2 | 31 | ． 38 | ． 055 | 7 | 17 | ． 29 | 187 | ． 11 |  | \＄．61 | ． 02 | ． 08 | 1 | 5 |
| 1456E 465450\％ | 1 | 86 | 13 | 48 | ． 1 | 25 | 15 | 814 | 2.45 | 22 | 5 | Mo | 3 | 25 | .2 | 2 | 2 | 33 | ． 28 | ． 049 | 8 | 49 | ． 31 | 134 | ， 14 |  | 2.64 | ． 03 | ． 06 | 1 | 67 |
| L456E 465＋25H | 1 | 42 | 10 | 97 | 1 | 36 | 14 | 1429 | 2.33 | 25 | 5 | N0 | 2 | 22 | ．2 | 2 | 2 | 33 | ． 20 | 108 | 5 | 18 | ． 27 | 254 | ． 14 |  | 2.12 | ． 03 | ．06 | 1 | B |
| L456E 465＋00\％ | 1 | 72 | 10 | 45 | 1 | 27 | 14 | 1356 | 2.17 | 15 | 5 | ND | 2 | 29 | .2 | 2 | 2 | 31 | ＋34 | ． 647 | 6 | 49 | .30 | 209 | 10 | 18 | 1.68 | ． 03 | ． 07 | I | 15 |
| 1456 464＋751 | 1 | 61 | 10 | 42 | 2 | 27 | 13 | 861 | 2.24 | 23. | 5 | NO | 3 | 18 | 2 | 2 | 2 | 32 | ． 22 | ．043 | $B$ | 22 | ． 36 | 161 | 42 |  | 1.09 | ． 03 | ． 07 | 1 | 49 |
| L456E 406450N | 1 | $\dagger 45$ | 17 | 54 | ． 5 | 43 | 17 | 545 | 2.87 | 39 | 5 | W0 | 5 | 25 | \％ 2 | 2 | 2 | 40 | ． 24 | ． 056 | 12 | 29 | ． 40 | 125 | A7 | 5 | 3.28 | ． 05 | ． 09 | I | 30 |
| L456E 465＋251 | 1 | 76 | 22 | 46 | 2 | 34 | 13 | 683 | 2.68 | 19 | 5 | ND | 3 | 76 | ． 2 | 2 | 2 | 39 | ． 21 | ．050 | 昌 | 33 | ． 56 | 97 | －11 | 2 | 1.73 | ． 03 | ． 06 | 1 | 32 |
| L456E 464＋00m | 1 | 46 | 19 | 66 | 3 | 26 | 15 | 1130 | 2.80 | 27 | 5 | W0 | 2 | 17 | 2 | 2 | 2 | 40 | ． 20 | \％7t | 7 | 26 | ． 37 | 179 | 11 | 4 | 1.42 | ． 03 | ． 07 | － | 4 |
| L456E 463－7TM | 1 | 52 | 10 | 41 | ＋ | 16 | 9 | 912 | 1.93 | 12 | 5 | ND | 1 | 14 | 2 | 2 | 2 | 33 | ． 15 | $\mathrm{CH7}$ | 5 | 16 | ． 25 | 115 | 09 | 4 | 1.05 | ． 03 | ． 05 | 1 | 19 |
| L456E 463－50m | 2 | 77 | 11 | $5 \%$ | 4 | 32 | 45 | 621 | 2.65 | 13 | 5 | WD | 3 | 16 | －2 | 2 | 2 | 37 | .17 | 063 | 7 | 25 | ． 47 | 195 | 14： | 2 | 2.40 | ． 02 | ． 04 | 1 | 15 |
| L456E 463＋25M | 1 | 110 | 14 | 4 B | ． 4 | 37 | 17 | 684 | 3.23 | 14 | 5 | H0 | 4 | 14 | 2 | 2 | 2 | 4 | ． 15 | －052 | 9 | 30 | ． 46 | 173 | ． 16 |  | 3.01 | ． 22 | ． 06 | 1 | 31 |
| 6456E 463＋00\％ | 2 | 60 | 12 | 57 | 4 | 38 | 16 | 679 | 2.23 | 15 | 5 | ND | 3 | 16 | ＋2 | 2 | 2 | 31 | ＋15 | ．057 | 6 | 17 | ． 26 | 179 | 15 |  | 3.00 | ． 02 | ． 06 | 1 | 4 |
| 6456E 462＋75H | 1 | 24 | 3 | 27 | ． 2 | 5 | 5 | 1259 | 1.01 | 4 | 5 | ND | 1 | 15 | － 2 | 2 | 2 | 23 | ． 19 | 028 | 2 | 4 | ． 08 | 900 | ．07： | 3 | ． 63 | ． 153 | ．65 | I |  |
| 1456E 462＋50N | 2 | 88 | 43 | 53 | ． 7 | 41 | 14 | 697 | 2.55 | 4 | 5 | ND | 3 | 24 | $+2$ | 2 | 2 | 32 | ． 20 | ．844 | 7 | 15 | ． 28 | 187 | 18 |  | 3.21 | ． 03 | ． 07 | ， | 11 |
| 2456E 462＋25N | 11 | 760 | 13 | 54 | 4 | 40 | 40 | 675 | B． 70 | 15 | 5 | Mo | 3 | 20 | 35 | 2 | 2 | 54 | ． 21 | 645 | 5 | 28 | ． 47 | 127 | －14 |  | 3.46 | ． 02 | ． 06 | 1 | 29 |
| （456E 462＋00m | 3 | 109 | 13 | 53 | ． 3 | 58 | 17 | 919 | 3.04 | 17 | 5 | H0 | 4 | 17 | ． 2 | 2 | 2 | 39 | ． 18 | ． 053 | 8 | 28 | ． 45 | 229 | ． 45 | 2 | 2.77 | ． 02 | ． 07 | 1 | 19 |
| L656E 461＋TSN | 4 | 68 | 14 | 72 | － 2 | 51 | 14 | 673 | 2.63 | 14 | 5 | N0 | 2 | 45 | ． 3 | 2 | 2 | 35 | ． 16 | 113 | 5 | 21 | ． 26 | 179 | ． 15 | 4 | 1.98 | ． 03 | ． 07 | 1 | 5 |
| L456E 461＋50m | 4 | 94 | 13 | 84 | ． 3 | 81 | 17 | 267 | 2.94 | 21 | 5 | Mo | 3 | 20 | 2 | 2 | 2 | 42 | ． 28 | 068 | 7 | 32 | ． 69 | 122 | 15 |  | 2.65 | ． 03 | ． 06 | 1 | 210 |
| t658E 464＋25M | ＊ | 60 | 13 | 52 | 2 | 56 | 13 | 655 | 2.50 | 18 | 5 | ND | 3 | 18 | －2 | 2 | 2 | 36 | ． 21 | ．066 | 8 | 29 | ． 41 | 980 | 16 | 2 | 3.02 | ． 13 | ． 05 | 1 | 18 |
| L456E 461＋00m | 1 | 13 | 4 | 25 | 4 | 6 | 4 | 755 | ． 95 | 2 | 5 | N0 |  | 7 | 2 | 2 | 2 | 22 | ． 09 | 8037 | 2 | 6 | ． 08 | 37 | 07 | 4 | ． 47 | ． 03 | ． 03 | 1 | 9 |
| L456E 460＋75M | 2 | 51 | 10 | 48 | 2 | 42 | 11 | 939 | 2.19 | 15 | 5 | ND | 3 | 13 | 2 | 2 | 2 | 33 | ． 15 | 060 | 7 | 25 | ． 34 | 154 | 14 | 2 | 2.53 | ． 02 | ． 65 | 1 | 13 |
| L456E 460 5 50N | 1 | 32 | 10 | 57 | 2 | 23 | 9 | 738 | 1.90 | 10 | 5 | ND | 2 | 10 | 2 | 2 | 2 | 31 | ． 13 | ¢056 | 5 | 19 | ． 25 | 112 | 12 |  | 1.41 | ． 03 | ． 04 | $t$ | 1 |
| L456E 460＋25M | 1 | 67 | 11 | 44 | ． 3 | 49 | 12 | 218 | 2.21 | 19 | 5 | Ni | 3 | 12 | 2 | 2 | 2 | 34 | ． 15 | 94\％ | 7 | 25 | ． 34 | 93 | ． 14 | 2 | 2.42 | ． 03 | ． 05 | \％ | 30 |
| L456E 460＋60N | 1 | 15 | 4 | 20 | 2 | 5 | 2 | 205 | .77 | 3 | 5 | NJ | 1 | 7 | 2 | 2 | 2 | 19 | ． 09 | D23 | 2 | 6 | ． 08 | 28 | 06 | ， | ． 47 | ． 04 | ． 04 |  | 1 |
| L456E 659+75M | 2 | 47 | 10 | 46 | 3 | 34 | 11 | 1359 | 2.37 | 24 | 5 | ND | 2 | 13 | 2 | 2 | 2 | 35 | .17 | ＋64 | 6 | 27 | ． 40 | 134 | 13 |  | 2.25 | ． 02 | ． 05 |  | 4 |
| L456E 459＋50H | 3 | 41 | 13 | 58 | 2 | 41 | 12 | 1090 | 2.34 | 20 | 5 | W0 | 2 | 15 | －2 | 2 | 3 | 34 | ． 23 | 045 | 6 | 27 | ． 36 | 172 | 16 |  | 2.38 | ． 02 | ． 06 | $1$ | 24 |
| L656E 459＋25\％ | 1 | 48 | 11 | 60 | 4 | 41 | 10 | 452 | 2.08 | 15 | 5 | ND | 3 | 17 | 2 |  | 2 | 31 | ． 19 | \％ 075 | 8 | 27 | ． 33 | 153 | .13 | 2 | 2.20 | ． 03 | ． 05 | 1 | 4 |
| L656E 659＋00M | 1 | 25 | 12 | 41 | 2 | 23 | 8 | 305 | 1.76 | 15 | 5 | NO | 2 | 15 | 2 | 2 | 2 | 27 | ． 20 | ＋066 | 6 | 21 | ． 24 | 90 | D80 | 2 | 1．12 | ． 02 | ． 04 | I： | 6 |
| 1456E 458475N | 1 | 48 | 12 | 74 | ． 3 | 36 | 16 | 481 | 2.73 | 24 | 5 | NO | 3 | 12 | －2 | 2 | 2 | 36 | ． 20 | 130 | 7 | 35 | ． 66 | 100 | ＋69 | 2 | 1.65 | ． 02 | ． 06 | $1$ | 75 |
| L4560 450＋50m | 1 | 54 | 14 | 80 | 4 | 42 | 13 | 405 | 2.49 | 20 | 5 | 10 | 3 | 17 | 2 | 2 | 2 | 36 | ． 22 | 139 | － | 30 | ． 39 | 120 | 17 |  | 2.30 | ． 02 | ． 06 | t | 47 |
| L456E 453＋25M | 1 | 108 | 9 | 94 | ． 3 | 165 | 49 | 501 | 2.56 | 24 | 5 | No | 2 | 21 | 2 | 2 | 2 | 31 | ． 34 | ．059 | 9 | 30 | ． 31 | 92 | 12 | 3 | 2.05 | ． 03 | ． 05 | 1 | 76 |
| L456E 458400N | 1 | 196 | 13 | 30 | 2 | 167 | 5 | 233 | 1.41 | 14 | 5 | ND | 1 | 30 | ${ }^{+3}$ | 2 | 2 | 21 | ． 80 | d09 | 0 | 18 | ＋20 | 50 | ， 6 | 4 | 1.15 | ． 03 | ． 03 | $t$ | 36 |
| L657E 465＋75M | 1 | 43 | 9 | 67 | .1 | 23 | 13 | 788 | 1.59 | 20 | 5 | N0 | 1 | 25 | － 2 | 3 | 2 | 29 | ． 27 | －104\％ | 5 | 18 | －28 | \＄73 | 09 | 3 | 1.18 | ． 83 | ． 04 | t | 5 |
| L457E 465450m | 1 | 77 | $g$ | 36 | .4 | 28 | 7 | 680 | 4.51 | 15 | 5 | N0 | 2 | 18 | 2 | 2 | 2 | 24 | ． 42 | 8029 | 14 | 13 | ． 98 | 55 | 12 | 4 | 2.06 | ． 65 | ． 05 | $t$ | 1 |
| L457E 465＊25M | 1 | 49 | 9 | 52 | －2 | 22 | 10 | 822 | 2.06 | 19 | 5 | ND | 2 | 14 | ． 2 | 2 | 2 | 31 | ． 15 | 0097 | 6 | 18 | ． 27 | 132 | 14 | 2 | 2.37 | ． 03 | ． 04 | ］－ | 10 |
| STMNDAR C／Alu－s | 19 | 57 | 39 | 132 | 6.7 | 73 | 29 | 1049 | 4.11 | 43 | 22 | 7 | 39 | 50 | 19.3 | 16 | 22 | 58 | ． 52 | ， 0.57 | 39 | 59 | ． 93 | 1.83 | 09 | 39 | 1．98 | ． 06 | ． 14 | 11 | 54 |

 THIS LEACH IS PARTLAL FDN MH FE SR CA P LA CR MG 日A TI B W MMO LIMITED FOR MAK AND AL．MU OETECTIOH LIMIT GY ICP IS 3 PPA． SHMPLE TYPE：PI－PT SOII PS ROCK NU ANMLYSIS EY ACID LEACH／AA FROM 10 GM SANPLE．


| SAMPLE* | $\begin{array}{r} \mathrm{Mo} \\ \mathrm{ppm} \end{array}$ | $\mathrm{Cu}$ | $\begin{gathered} \mathrm{Pb} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} 2 n \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { hg } \\ \text { ppon } \end{array}$ | $\begin{gathered} \mathrm{Hi} \\ \mathrm{prom} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { Ppom } \end{array}$ | $\underset{\mathrm{pom}}{\mathrm{Mn}}$ | $\begin{gathered} \mathrm{Fe} \\ \pi \end{gathered}$ | $\begin{aligned} & \mathrm{As} \\ & \mathrm{ppm} \end{aligned}$ | $\underset{\text { ppm }}{\text { U }}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{aligned} & \text { Th } \\ & \text { ppom } \end{aligned}$ | $\mathrm{Sr}_{\mathrm{prom}}^{\mathrm{pom}}$ | $\begin{array}{r} \text { Sb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{p} \mathrm{PO}^{\prime} \end{array}$ | $\begin{array}{r} V \\ \text { PPR } \end{array}$ | $\mathrm{C}_{\mathbf{x}}^{\mathrm{x}}$ |  | $\begin{gathered} \mathrm{La} \\ \text { ppon } \end{gathered}$ | $\underset{\mathrm{pr}}{\mathrm{Cr}}$ | Mg | $\begin{aligned} & \text { ge } \\ & \text { pporn } \end{aligned}$ | ${ }_{x}^{1}$ | $\begin{array}{r} \text { B } \\ \text { ppen } \end{array}$ | $\underset{y}{A!}$ | $\begin{gathered} \text { We } \\ \mathbf{x} \end{gathered}$ | $\begin{aligned} & \mathbf{K} \\ & \mathbf{X} \end{aligned}$ | M | $\begin{aligned} & \text { Aup } \\ & \text { ppot } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1457E 485400\% | 1 | 30 | 11 | 84 | .1 | 19 | 9 | 796 | 2.18 | 19 | 5 | M0 | 2 | $16: 82$ | 2 | 2 | 32 | . 16 | 0075 | 5 | 49 | . 26 | 151 | . 12 |  | 1.56 | .63 | . 04 | 1 | 43 |
| L457E 466+75M | 1 | 33 | 5 | 43 | 11 | 21 | 12 | 880 | 1.85 | 8 | 5 | NO | 1 | 15.2 | 2 | 2 | 29 | . 17 | 059. | 4 | 45 | . 24 | 121 | 10 | 2 | 1.36 | . 03 | . 03 | 2 | 8 |
| [457E 464+50W | 1 | 78 | 5 | 42 | . 2 | 26 | 14 | 447 | 2.12 | 40 | 5 | N0 | 3 | 16 . 2 | 2 | 2 | 34 | . 18 | . 1046 | 5 | 22 | .35 | 77 | 810 |  | 1.39 | . 63 | . 05 |  | 36 |
| L457E 464+25M | $i$ | 53 | 12 | 54 | $\pm$ | 35 | 13 | 673 | 2.91 | 25 | 5 | NO | 2 | $22 \because 2$ | 2 | 2 | 26 | . 27 | $\bigcirc 082$ | 5 | 15 | . 23 | 116 | . 15 | 5 | 3.07 | . 63 | . 04 | 1 | 26 |
| L657E 464+00N | 7 | 43 | 6 | 40 | $\pm$ | 14 | B | 413 | 1.34 | 10 | 5 | ND | 1 | 12.2 | 2 | 2 | 22 | . 11 | 2067 | 3 | 10 | . 16 | 75 | 108 | 2 | 1.14 | .03 | . 03 | 2 | 8 |
| [4575 633-75\% | 1 | 52 | 10 | 58 | 1 | 25 | 14 | 919 | 2.35 | 6 | 5 | N0' | 2 | 20.2 | 2 | 2 | 33 | . 19 | 061 | 5 | 17 | . 29 | 167 | . 83 |  | 1.86 | . 03 | . 06 | 1 | 11 |
| 1457E 463+50\% | 2 | 184 | 11 | 61 | . 3 | 34 | 49 | 548 | 3.01 | 19 | 5 | N0. | 3 | $21 \therefore 2$ | 2 | 2 | 39 | . 21 | -088 | 10 | 27 | . 46 | 146 | , 15 | 3 | 3.38 | . 03 | . 05 | ¢ | 65 |
| L457E 463+25M | 2 | 119 | 12 | 60 | 5 | 46 | 17 | 246 | 3.04 | 24 | 5 | ND | 4 | $17 \cdots \cdot 2$ | 2 | 2 | 40 | . 27 | .099 | 15 | 28 | .43 | 151 | 17 |  | 4.12 | . 05 | . 06 | d | 21 |
| 6457E 462+50m | 3 | 323 | 40 | 62 | 5 | 37 | 19 | 625 | 4.12 | 23 | 5 | NO | 4 | $34 \cdots 3$ | 2 | 2 | 47 | . 42 | D78 | 16 | 30 | . 52 | 452 | 16 |  | 2.61 | . 03 | . 12 | 1 | 46 |
| 6657E 462+25N | 3 | 462 | 55 | 67 | 4 | 36 | 18 | 570 | 4.20 | 22 | 5 | NO | 4 | 33 - 3 | 2 | 2 | 44 | . 39 | 088 | 14 | 29 | . 45 | 167 | 12 | 2 | 2.53 | . 02 | . 09 | 1 | 37 |
| L457E 462+00\% | 10 | 511 | 15 | 55 | . 3 | 56 | 37 | 784 | 5.69 | = 44 | 5 | ND | 3 | 19.4 | 2 | 2 | 55 | . 18 | .060 | 8 | 36 | . 72 | 114 | . 10 | 2 | 2.55 | . 02 | . 05 | 1 | 53 |
| 1657E 469+75M | 2 | 106 | 11 | 44 | 12 | 35 | 14 | 279 | 2.51 | 13 | 5 | WD | 4 | $22 \therefore 2$ | 2 | 2 | 35 | . 20 | . 059 | 9 | 22 | . 35 | 101 | 4.15 |  | 3.44 | . 03 | . 06 | 3 | 16 |
| L457E 461+50m | 1 | 63 | 14 | 55 | . 3 | 36 | 13 | 478 | 2.39 | + +5 | 5 | H0 | 3 | 19 Q 2 | 2 | 2 | 36 | . 18 | .046 | 0 | 25 | . 33 | 151 | 16 |  | 3.14 | . 02 | . 15 | 1 | 23 |
| 1457E 461+25N | 2 | 001 | 204 | 107 | 6 | 40 | 18 | 348 | 6.70 | 60 | 5 | WD | 4 | 76 - 0 | 7 | 2 | 52 | . 63 | 111: | 20 | 35 | . 55 | 287 | 809 |  | 1.40 | . 02 | . 12 | 1 | 9 |
| L457E 461+00w | 2 | 75 | 13 | 53 | .2 | 3* | 11 | 571 | 2.40 | 14 | 5 | ND | 3 | $15 \times 2$ | 2 | 2 | 34 | . 14 | 3090 | 5 | 20 | . 28 | 126 | + 86 |  | 3.27 | . 02 | . 05 | 1 | 17 |
| L657E 4604751 |  | 50 | 14 | 56 | 2 | 26 | 11 | 802 | 2.16 | 17 | 5 | MD | 3 | 15 -2 | 2 | 2 | 34 | . 14 | -807 | 6 | 21 | . 26 | 160 | 45 | 3 | 2.70 | . 02 | . 05 | 2 | 24 |
| L657E 460+50M | 1 | 15 | 4 | 26 | 1 | 4 | 6 | 610 | . 92 | 7 | 5 | NO | 1 | 8 - 2 | 2 | 2 | 21 | . 10 | 064 | 2 | 5 | .08 | 35 | 07 | 2 | . 54 | . 03 | . 03 | 1 | 3 |
| L657E 460-23\% | 1 | 51 | 8 | 48 | . 1 | 31 | 9 | 569 | t+73 | 7 | 5 | M0 | 2 | 49 2 | 2 | 2 | 28 | . 18 | 646 | 6 | 18 | . 26 | 103 | 80 | 2 | 1.58 | . 03 | . 04 | 2 | 171 |
| 1457E 460+00\% | 3 | 92 | 13 | 69 | 3 | 63 | 15 | 296 | 2.66 | 16 | 5 | ND | 6 | 20.2 | 2 | 2 | 37 | . 22 | -654 | 13 | 31 | . 43 | 116 | . 16 |  | 3.13 | . 03 | . 04 | 1 | 15 |
| L657E 459*75N | 4 | 77 | 10 | 47 | * | 37 | 12 | 915 | 2.46 | 13 | 5 | H0 | 3 | 19 :-2 | 2 | 2 | 35 | . 21 | 1050 | 9 | 30 | . 39 | 155 | 13 | 2 | 2.50 | . 02 | . 04 | 2 | 79 |
| L457E 459+50m | 2 | 66 | 11 | 50 | 5 | 34 | 12 | 35: | 2.54 | 47 | 5 | W0 | 3 | 15.2 | 2 | 2 | 38 | . 18 | 0084 | 14 | 31 | . 45 | 127 | 84 |  | 2.85 | . 02 | . 05 | t | 45 |
| 1457E 459+25 | 3 | 74 | 10 | 53 | 12 | 40 | 13 | 346 | 2.52 | 20 | 5 | ND | 4 | 15 \% | 2 | 2 | 37 | . 24 : | S059 | 11 | 30 | . 41 | 126 | 15 |  | 2.57 | . 02 | . 05 | 1 | 50 |
| L457E 459+00m | 1 | 55 | 12 | 56 | -2 | 27 | 13 | 549 | 2.26 | 11 | 5 | W0 | 4 | 14 <2 | 2 | 2 | 33 | . 15 | \%147 | 11 | 24 | . 31 | 154 | 4t4 | 4 | 2.94 | .02 | . 05 | 1 | 167 |
| L457E 459+75\% | 1 | 36 | 11 | 72 | .2 | 27 | 12 | 662 | 2.24 | 18 | 5 | 10 | 2 | 14 -2 | 2 | 2 | 32 | . 16 | \$36 | 6 | 26 | . 32 | 104 | $\ldots 1$ |  | 2.13 | . 02 | . 04 | 1 | 97 |
| L457E 450+50\% | 9 | 22 | 6 | 46 | . | 29 | 10 | 154 | 2.02 | 14 | 5 | N0 | 2 | 11 \%2 | 2 | 2 | 34 | . 16 | \$04 | 5 | 22 | . 27 | 53 | 09 | I | 1.42 | . 02 | . 05 | 2 | 14 |
| 1457E 458+25m | 1 | 96 | 12. | 31 | 3 | 73 | 7 | 224 | 1.38 | 9 | 5 | \% | , | 37 , 4 | 2 | 2 | 22 | . 91 | 4028 | 6 | 17 | . 23 | 49 | ¢07 | 4 | .99 | . 05 | . 05 | 1 | - |
| L657E 459+00N | 1 | 124 | 9 | 33 | 4 | 132 | 5 | 273 | . 81 | 9 | 5 | M | 1 | 731.0 | 2 | 2 | 11 | 2.08 | 056 | 6 | 9 | . 13 | 56 | 05 |  | 1.95 | . 03 | . 04 | 1 | 6 |
| L458E 465-75M | 1 | 192 | 10 | 75 | 2 | 55 | 14 | 1049 | 1.93 | 35 | 5 | HD | 2 | 311. | 2 | 2 | 27 | . 89 | 8049 | 12 | 24 | . 32 | 63 | 11 |  | 2.06 | . 04 | . 05 | $\stackrel{1}{1}$ | 11 |
| L459E 665+50m | 1 | 90 | d | 50 | 2 | 33 | 16 | 737 | 2.47 | 25 | 5 | MD | 3 | 20.2 | 2 | 2 | 35 | . 26 | +083 | 8 | 25 | . 36 | 143 | 12 |  | 2.25 | . 02 | .06 | , | 34 |
| L658E 465+25\% | 1 | 74 | 10 | 6. | 2 | 29 | 15 | 640 | 2.45 | 110 | 5 | N0 | 3 | 16.2 | 2 | 2 | 35 | . $\dagger 5$ | . 080 | 7 | 19 | .33 | 158 | 14 | 3 | 2.92 | .103 | . 05 |  | 19 |
| 44508 465+100 | 1 | 47 | 10 | 73 | 2 | 25 | 14 | 478 | 2.20 | 37 | 5 | N0 | 3 | 43 L 2 | 2 | 2 | 34 | . 13 | .127 | 5 | 19 | . 26 | 07 | 175 |  | 2.43 | . 02 | . 15 | 1 | 14 |
| (458e 484+75\% | 1 | 37 | 10 | 61 | 2 | 25 | 14 | 284 | 2.28 | 38 | 5 | W | 3 | $13 \times 2$ | 2 | 2 | 34 | . 15 | 102 | 5 | 19 | . 27 | 02 | +14 |  | 2.39 | . 02 | . 05 | 1 | 8 |
| L650E 464+50n | 1 | 29 | 12 | 71 | 2 | 22 | 10 | 310 | 2.18 | 24 | 5 | WD | 3 | 14 -2 | 2 | 2 | 33 | . 14 | ctes | 5 | 18 | . 22 | 12 | . 17 |  | 3.10 | . 03 | . 06 | 1 | 19 |
| LG5EE 464+25M | 2 | 164 | 13 | 46 | 2 | 58 | 16 | 304 | 2.03 | 25 | 5 | NO | 3 | 28 - 2 | 2 | 2 | 23 | . 30 | 6020 | 12 | 15 | . 23 | 69 | 16 |  | 3.00 | . 09 | . 04 | $z$ | 6 |
| L450E 664-00. | 1 | 156 | 12 | 57 | .6 | 58 | 15 | $10^{4} 2$ | 2.52 | 15 | 5 | NO | 4 | $21 \times 2$ | 2 | 2 | 37 | . 27 | 0.053 | 16 | 31 | . 40 | 95 | 20 | 2 | 4.37 | . 03 | . 04 | $1$ | 14 |
| L438E 463475 | 1 | 119 | 16 | 77 | , 4 | 104 | 23 | 402 | 2.36 | 20 | 5 | M | 5 | 16 \% 2 | 2 | 2 | 34 | . 24 | Y 046 | 0 | 20 | . 23 | 55 | 17 |  | 3.24 | . 12 | . 04 | 1 | 4 |
| STMENOM C/AU-S | 48 | 57 | 39 | 132 | 7.1 | 72 | 31 | 1036 | 4.04 | 43 | 21 | 6 | 39 | 5519.3 | 44 | 16 | 56. | . 51 | 8096 | 39 | 59 | .92 | 182 | 09 | 39 | 1.95 | . 06 | . 4 | 11 | 54 |


| $e_{\infty}^{\infty}$ | Attwood Gold |  |  |  |  |  |  |  |  | corp. |  | PROJE |  |  | GOLDEN CROWN |  |  |  | FILE |  | \# 90-1366 |  |  |  |  |  |  |  | Page 3 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SMMPLE\# | $\begin{array}{r} \text { mo } \\ \hline \end{array}$ | $\begin{gathered} \mathrm{Cu} \\ \mathrm{prom} \end{gathered}$ | $\begin{gathered} \text { Pb } \\ \text { ppon } \\ \hline \end{gathered}$ | $\begin{array}{r} \text { 2n } \\ \hline \text { pant } \end{array}$ | $\mathbf{M g}$ | $\begin{gathered} \mathrm{wi} \\ \text { pprn } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{Co} \\ \mathrm{ppom} \\ \hline \end{gathered}$ | $\begin{array}{r} \text { Mn } \\ \text { prom } \\ \hline \end{array}$ | $\begin{aligned} & \text { Fe } \\ & \mathbf{x} \end{aligned}$ | Aspm | $\begin{array}{r} \mathrm{D} \\ \mathrm{ppm} \\ \hline \end{array}$ | $\underset{\text { ppon }}{\mathrm{Al}}$ | $\begin{array}{r} \text { Th } \\ \text { pprin } \end{array}$ | $\begin{gathered} \mathrm{Sr} \\ \mathrm{ppm} \end{gathered}$ | $\mathrm{Ce}$ | $\begin{array}{r} \text { Sb } \\ \text { ppon } \end{array}$ | $\begin{gathered} \text { Bi } \\ \text { ppm } \end{gathered}$ | $\underset{\text { pom }}{\mathrm{V}}$ | $\begin{gathered} \mathrm{CB} \\ \mathbf{x} \end{gathered}$ | $8$ | Lit | $\mathrm{Cr}$ | $\begin{aligned} & \mathrm{mg} \\ & \mathbf{x} \end{aligned}$ | $\mathrm{Be}$ | $\frac{\mathbf{T}}{\mathbf{K}}$ | $\underset{~ B q}{8}$ | $\begin{aligned} & \text { Al } \\ & \mathbf{x} \end{aligned}$ | Me | $\underset{y}{x}$ | w | $\begin{aligned} & \text { Ms } \\ & \text { Mph } \end{aligned}$ |
| L450E 463+30N | 2 | 74 | 14 | 43 | . 4 | 133 | 21 | 134 | 2.28 | 15. | 5 | WD | 3 | 16 | 2 | 2 | 2 | 30 | .16 | 0044 | 4 | 13 | . 15 | 59 | +18 | 3 | 3.73 | . 03 | . 06 | 1 | 5 |
| 64585 463+251 | 1 | 56 | 10 | 67 | 2 | 42 | 95 | 761 | 2.33 | 20 | 5 | HD | 3 | 14 | 2 | 2 | 2 | 33 | .19 | [065 | 6 | 26 | . 26 | 112 | 8 |  | 3.24 | . 02 | . 05 | 1 | 19 |
| L458E 463+00m | 1 | 146 | 10 | 64 | 2 | 37 | 20 | 511 | 2.74 | 17 | 5 | ND | 3 | 14 | 2 | 2 | 2 | 39 | . 15 | 055 | 5 | 23 | . 24 | 113 | 14 |  | 2.44 | . 02 | . 04 | 1 | 8 |
| L458E 462+73M | 1 | 42 | 13 | 59 | 1 | 55 | 13 | 745 | 2.20 | 20 | 5 | ND | 3 | 14 | 2 | 2 | 2 | 35 | . 15 | $0{ }^{65}$ | 5 | 20 | . 26 | 133 | $+35$ |  | 2.48 | . 02 | . 04 | $t$ | 10 |
| L458E 462+50m | 4 | 74 | 10 | 72 | 4 | 64 | 27 | 362 | 2.55 | 21 | 5 | HD | 3 | 16 | 2 | 2 | 2 | 40 | .17 | ctis | 6 | 29 | . 35 | 114 | 13 | 3 | 2.54 | . 02 | . 04 | $t$ | 25 |
| 4458x 4-6235 | 1 | 87 | 15 | 48 | 2 | 147 | 22 | \% 68 | 2.33 | 8 | 5 | ND | 3 | 15 | 82 | 2 | 2 | 37 | . 19 | 047 | 8 | 25 | . 33 | 907 | 16 | 2 | 3.44 | . 02 | . 15 | 1 | 3 |
| 6458E 462+00m | 1 | 42 | 13 | 65 | 1 | 37 | 12 | 469 | 2.36 | 23 | 5 | ND | 3 | 11 | 2 | 2 | 2 | 36 | . 10 | 082 | 5 | 18 | . 21 | 111 | .17 | 2 | 3.82 | . 02 | . 04 | 1 | 9 |
| L658E 461+75N | 1 | 199 | 31 | 87 | . 3 | 30 | 12 | 459 | 2.33 | 18 | 5 | MD | 3 | 33 | 4 | 2 | 2 | 33 | . 51 | 110 | 9 | 20 | . 33 | 151 | $\cdots 4$ |  | 3.23 | . 05 | . 67 |  | 8 |
| 4454E 461+50m | 1 | 63 | 17 | 53 | 2 | 32 | 11 | 436 | 2.25 | 18 | 5 | ND | 3 | 19 | 2 | 2 | 2 | 35 | . 22 | 088 | 11 | 24 | +34 | 134 | 16 |  | 2.70 | . 03 | . 65 |  | 6 |
| 645.6E 461+25N | 1 | 102 | 14 | 47 | 2 | 35 | 14 | 247 | 2.74 | 17 | 5 | MD | 4 | 15 | 2 | 2 | 2 | 41 | . 15 | .0770 | 11 | 29 | . 43 | 125 | \$6 |  | 3.70 | . 02 | .65 |  | 7 |
| L695E 461400m | \% | 56 | 12 | 49 | 1 | 37 | 13 | 537 | 2.52 | 15 | 5 | M | 4 | 14 | 2 | 2 | 2 | 38 | . 14 | 0107 | B | 30 | . 41 | 149 | 14 |  | 2.90 | . 02 | . 05 |  | 23 |
| L45BE 460+75M | 1 | 59 | 11 | 58 | . 2 | 36 | 13 | 574 | 2.19 | 20 | 5 | MO | 5 | 19 | 2 | 2 | 2 | 32 | $+17$ | 078 | 7 | 23 | . 32 | 132 | . 14 | 3 | 2.59 | . 02 | . 05 | 1 | 3 |
| L4S*E 460 450 m | 1 | 86 | 11 | 57 | 1 | 44 | 15 | 504. | 2.42 | 29 | 5 | No | 3 | 16 | 2 | 2 | 2 | 38 | +18 | 058 | 7 | 33 | . 46 | 100 | 12 |  | 2.00 | . 02 | . 05 | + | 28 |
| L458E 460-25m | 2 | 288 | 11 | 52 | . 2 | 110 | 21 | 371 | 2.70 | -15 | 5 | W0 |  | 16 | $\square 2$ | 2 | 2 | 40 | . 31 | .032 | 10 | 36 | . 47 | 71 | ${ }_{44}$ |  | 2.58 | . 02 | .05 |  | 62 |
| L458E $460+00 \mathrm{~N}$ | $\dagger$ | 114 | 14 | 58 | 1 | 54 | 14 | 545 | 2.49 | 16 | 5 | HD | 3 | 17 | $\therefore 2$ | 2 | 2 | 36 | . 22 | .069 | 8 | 30 | . 38 | 122 | .43 | 5 | 2.61 | . 02 | . 05 |  | 0 |
| L6SEE 459475M | 1 | 165 | 14 | 73 | 2 | 44 | 32 | 323 | 2.02 | 6 | 5 | MO | 3 | 46 | 2 | 2 | 2 | 29 | . 30 | LS6 | 7 | 18 | . 22 | 65 | 35 |  | 3.26 | . 03 | . 05 |  | 13 |
| 1450x 459450m | 1 | 216 | \$2 | 73 | 34 | 56 | 44 | 374 | 2.00 | 12 | 5 | ND | 3 | 20 | . 2 | 2 | 2 | 27 | . 44 | coeo | 11 | 18 | . 22 | 48 | 16 |  | 3.50 | . 03 | -06 | 1 | 7 |
| 1456e 459400N | 2 | 85 | 10 | 31 | 3 | 50 | 11 | 337 | 1.44 | 10 | 5 | W0 | 2 | 20 | $+2$ | , | 2 | 21 | . 54 | . 024 | 8 | 15 | . 16 | 37 | 111 |  | 1.87 | . 06 | .03 |  | 7 |
| 4458x 458+75m | 1 | 24 | 4 | 38 | 2 | 21 | 8 | 101 | 1.64 | 12 | 5 | ND | 2 | 11 | $\bigcirc 2$ | 2 | 2 | 26 | . 17 | 002 | 5 | $1{ }^{1}$ | .17 | 46 | 10 |  | 1.70 | . 02 | . 03 |  | 8 |
| 4458x 458+50N | 2 | 121 | 12 | 42 | 3 | 88 | 42 | 241 | 2.05 | 9 | 5 | NO | 2 | 18 | $\times 2$ | 3 | 2 | 27 | . 4 | 025 | 8 | 26 | . 28 | 55 | 11. |  |  | . 03 | . 15 |  | 38 |
| L439E 466+00m | 4 | 40 | 14 | 42 | 1 | 25 | 12 | 480 | 2.07 | 29 | 5 | W0 | 3 | 18 | 2 |  | 2 | 26 | . 25 | 036 | - | 15 | . 20 | 57 | 16 | 4 | 3.37 | . 03 | .03 | 1 | 2 |
| 1459E 465+754 | 1 | 171 | 13 | 28 | 3 | 37 | 13 | 559 | 2.07 | 44 | 5 | W0 | 3 | 30 | 3 | 2 | 2 | 25 | . 69 | D21 | 14 | + ${ }^{\text {P }}$ | .21 | 51 | +16 | 5 | 3.43 | . 04 | . 03 |  | 3 |
| L459\% 465450m | 2 | 356 | 10 | 28 | 2 | 120 | 90 | 404 | 1.41 | 48 | 5 | H0 | 2 | 27 | 3 | 2 | 2 | 19 | . 63 | 020 | 9 | 12 | . 15 | 28 | 812 | 5 | 2.26 | . 04 | . 03 |  | 1 |
| L459E 465+25M | 2 | 75 | 14 | 57 | . 1 | 41 | 20 | 461 | 2.16 | 22 | 5 | H0 | 3 | 13 | 2 | 2 | 2 | 31 | . 15 | +17\% | 4 | 20 | . 25 | 84 | 18 | 3 | 2.96 | + 02 | . 04 | 2 | 8 |
| [459E 465400M | 1 | 33 | 12 | 59 | 1 | 22 | 8 | 777 | 1.80 | 17 | 5 | H0 | 2 | 15 | 2 | 2 | 2 | 29 | . 16 | 106 | 4 | 16 | . 17 | 103 | .12 | 3 | 2.40 | . 02 | . 04 |  | 5 |
| 1459E 460+75N | 1 | 66 | 14 | 63 | 1 | 36 | 19 | 251 | 2.38 | 12 | 5 | H0 | 4 | 16 | 2 | 2 | 2 | 32 | . 13 | 104 | 7 | 20 | . 25 | 432 | 16 |  | 4.14 | . 13 | . 04 |  | 27 |
| 1459E 44405 | 2 | 60 | 15 | 39 | 5 | 63 | 49 | 230 | 2.26 | 15 | 5 | 40 | 3 | 16 | 2 | 2 | 2 | 33 | . 19 | 035 | 6 | 19 | . 21 | 113 | 16 | 4 | 3.56 | . 63 | . 04 |  | 19 |
| 1459\% 464+25m | 1 | 51 | 12 | 45 | 3 | 32 | 44 | 213 | 2.22 | 15 | 5 | H0 | 3 | 15 | 2 | 2 | 2 | 32 | .17 | -652 | 4 | 20 | . 23 | 117 | +13 |  | 2.65 | . 02 | . 05 | 1 | 1 |
| L459E 444+00w | 1 | 66 | 19 | 45 | 3 | 38 | ${ }_{48}$ | 291 | 2.26 | 7 | 5 | H0 | 3 | 15 | 2 | 2 | 2 | 32 | . 14 | . 65.1 | 10 | 22 | . 25 | 120 | 13 | 5 | 2.94 | . 02 | . 04 |  | 9 |
| L459E 465-75N | 1 | 187 | 14 | 54 | 茥 | 61 | 25 | 175 | 2.87 | 19 | 5 | N0 | 4 | 17 | 2 | 2 | 2 | 41 | . 22 | ,635 | 10 | 36 | .47 | 19 | 14 |  | 00 | . 02 | . 0 |  | 15 |
| L4596 463+50m | 1 | 62 | 13 | 40 | 3 | 30 | 12 | 321 | 2.09 | 12 | 5 | N0 | 4 | 15 | 2 | 2 | 2 | 30 | . 13 | 005 | - | 19 | . 22 | 107 | 15 |  | 3.44 | 02 | + 05 |  | 24 |
| 6459E 463+2511 | 3 | 196 | 13 | 41 | 1 | 44 | 22 | 363 | 3.04 | 25 | 5 | ND | 4 | 15 | -2 | 2 | 2 | 41 | .12 | 0104 | 9 | 36 | . 49 | 840 | 12 | 2 | 2.38 | . 02 | . 04 |  | 32 |
| 14595 463+00m | 4 | 460 | 50 | 70 | 4 | 48 | 25 | 694 | 4.43 | 52 | 5 | NF | 5 | 29 | 2 | 3 | 2 | 50 | . 35 | 50,0 | \$8 | 47 | . 76 | 130 | 80 | ) | 1. 69 | . 02 | . 09 | 2 | 5 |
| L459E 462+75N | 1 | 93 | 15 | $\sqrt{3}$ | 1 | 36 | 14 | 600 | 2.32 | 9 | 5 | WD | 3 | 16 | 2 | 2 | 2 | 34 | . 15 | -059 | 5 | 20 | 19 | 99 | 84 | 6 | 3.11 | 02 | . 15 |  | 13 |
| L459E 462450m | 1 | 76 | 12 | 48 | 2 | 29 | 11 | 254 | 2.09 | 9 | 5 | WD | 3 | 14 | . 2 | 2 | 2 | 34 | . 11 | . 057 | 5 | 16 | . 19 | 119 | . 24 | 4 | \% | 2 | .15 |  | 7 |
| 16592 462+25\% | 1 | 48 | 6 | 39 | 1. | 20 | 10 | 189 | 1.05 | 10 | 5 | ND | 2 | 11 | 2 | 2 | 2 | 20 | . 10 | 0 | 2 | 7 | . 09 | 59 | . 10 | 3 | .97 | . 05 | . 04 |  | 5 |
| STAMOARD C/AN-S | 18 | 57 | 40 | 132 | 7.1 | 73 | 31 | 1048 | 4.08 | 44 | 23 | 7 | 39 | 55 | 19.7 | 45 | 48 | 57 | . 51 |  | 39 | 60 | . 93 | 183 |  | 39 | 1.98 | . 06 | . 1 | 14 | 54 |


| SAMPLE！ | Attwood Gold |  |  |  |  |  |  |  |  | Corp． |  |  |  |  |  |  | CROWN |  | FILE |  | \＃ | 90－1366 |  |  | $\infty$ |  |  |  | Page 4 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { Mo } \\ & \text { ppon } \end{aligned}$ | $\underset{\mathrm{cu}}{\mathrm{Cu}}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{poom} \end{array}$ | 2n | $\begin{array}{r} \mathrm{Ag} \\ \hline \mathrm{plon} \end{array}$ | $\underset{\mathrm{pq} \boldsymbol{\mathrm { M }}}{\mathrm{Mi}}$ | $\begin{array}{r} \text { co } \\ \text { potin } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppon } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \mathrm{X} \end{gathered}$ | As | $\begin{array}{r} \text { U } \\ \text { pon } \end{array}$ | $\underset{\text { ppon }}{\text { AU }}$ | $\begin{array}{r} \text { Th } \\ \text { ppp } \end{array}$ | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p} \boldsymbol{m} \end{array}$ | $\mathrm{Cd}$ | $\begin{array}{r} \text { sb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} 8 i \\ \text { ppm } \end{array}$ | $\begin{array}{r} v \\ \text { popn } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{z} \end{gathered}$ | $\begin{array}{r} \boldsymbol{p} \\ \boldsymbol{x} \end{array}$ | Lz | $\begin{gathered} \mathrm{Cr} \\ \mathrm{pom} \end{gathered}$ | $\begin{gathered} \text { Wg } \\ X \end{gathered}$ | $\begin{gathered} \text { Be } \\ \text { ppon } \end{gathered}$ | $\mathbf{T}$ | B | $\mathbf{A !}$ | 解 | \％ | $\boldsymbol{w}$ | $\begin{aligned} & \text { Av* } \\ & \text { pot } \end{aligned}$ |
| 1459E 462＋90\％ | 1 | 70 | 10 | 45 | 2 | 25 | 11 | 603 | 1.99 | 3 | 5 | NH | 3 | 18 | 2 | 2 | 2 | 29 | ． 75 | 077 | 7 | 15 | ． 20 | 100 | ． 16 |  | 3.35 | ． 02 | ． 05 | 2 | 9 |
| L459E 461＋75N | 1 | 18 | 3 | 33 | ． 1 | 11 | 4 | 457 | 1.15 | T 7 | 5 | NO | 1 | 14 | 2 | 2 | 2 | 22 | ． 15 | 039 | 3 | 9 | ． 12 | 61 | 09 |  | 1.17 | ． 03 | ． 04 | 1 | 3 |
| 659E 461＋50m | ！ | 135 | 34 | 58 | 4 | 26 | 11 |  | 2.34 | 15 | 5 | ND | 3 | 23 | 2 | 2 | 2 | 33 | ． 28 | \％082 | 10 | 23 | ． 33 | 127 | 4 |  | 2.98 | ． 03 | ． 05 | 1 | 12 |
| 1459F 461425M | 1 | 78 | 11 | 56 | － 1 | 34 | 12 | 324 | 2.61 | 20 | 5 | ND | 3 | 16 | 3 | 2 | 2 | 42 | ． 19 | 071 | 11 | 34 | ． 51 | 107 | $4{ }^{4}$ |  | 2.84 | ． 32 | 5 |  | 16 |
| L459E 461400\％ | 1 | 139 | 87 | 86 | 4 | 33 | 12 | 574 | 2.50 | 18 | 6 | W0 | 3 | 35 | 2 | 2 | 2 | 38 | .37 | ． 070 | 10 | 32 | 43 | 184 | 13 |  |  | ． 82 | ． 15 |  | 24 |
| 1459E 660＋50 | 1 | 37 | 12 | 69 | ． 1 | 28 | 12 | 718 | 2.64 | $\therefore 16$ | 5 | W | 2 | 45 | ． 2 | 2 | 2 | 44 | .15 | \％93 | 5 | 28 | ． 34 | 107 | 14 |  | 2.37 | ． 02 | ． 04 |  | 13 |
| L459E 460＋25M | 1 | 13 | 4 | 33 | 2 | 10 | 5 | 567 | 1.20 | 4 | 5 | NO | 1 | 13 | －2 | 2 | 2 | 23 | .12 | 676\％ | 3 | 13 | ． 13 | 64 | \％戈 | 6 | ． 89 | ． 03 | ． 04 | 1 | 1 |
| L659E 460＋00m | 1 | 41 | 9 | 45 | 12 | 31 | 11 | 767 | 2.49 | 24 | 5 | ND | 3 | 45 | $\stackrel{2}{2}$ | 2 | 2 | 39 | ． 19 | ． 063 | 7 | 28 | ． 37 | 116 | 13 |  | 2.82 | ． 02 | ． 65 |  | 41 |
| L459E 659＋75\％ | 1 | 35 | 7 | 44 | －3 | 27 | 9 | 325 | 2.13 | 18 ： | 5 | ND | 2 | 19 | $\bigcirc 2$ | 2 | 2 | 34 | ． 20 | ＋192 | 5 | 26 | ． 32 | 81 | 10 |  | 2.36 | ． 02 | ， 0 |  | 10 |
| 6659E 459＋50\％ | 1 | 22 | 8 | 59 | 3 | 19 | 7 | 530 | 1.82 | 14 | 5 | ND | 2 | 19 | ． 2 | 2 | 2 | 28 | ． 19 | 180 | 5 | 16 | ． 21 | 112 | $\bigcirc 2$ |  | 2.76 | ． 02 | ． 06 |  | 23 |
| L459E 4504250 | ， | 287 | 11 | 85 | 13 | 82 | 39 | 213 | 2.55 | 14 | 5 | ND | 4 | 21 | 2 | 2 | 2 | 34 | ． 27 | 0443 | 15 | 28 | ． 37 | 79 | $\checkmark 7$ |  | 3.49 | ． 03 | ． 06 | ？ | 71 |
| L459E 459＋00m | 1 | 97 | 12 | 60 | 4 | 117 | 157 | 402 | 2.31 | 13 | 5 | ND | 2 | 15 | 2 | 2 | 2 | 29 | ． 26 | －060 | 7 | 22 | ． 23 | 75 | ． 45 |  | 2.54 | ． 02 | ．06 | \％ | 7 |
| L459E 658＋73\％ | 1 | 81 | 12 | 65 | ． 3 | 89 | 93 | 304 | 2.12 | $\bigcirc$ | 5 | ND | 2 | 17 | ${ }^{2}$ | 2 | 2 | 25 | ． 27 | \％096 | 5 | 18 | ． 18 | 79 | 15 |  | 3.18 | ． 03 | ． 05 |  | 4 |
| 4459E 458＋50m | 3 | 580 | 12 | 45 | $\cdots 8$ | 222 | 61 | 497 | 2.96 | 14 | 5 | ND | 3 | 22 | 3 | 2 | 2 | 35 | ． 48 | －2088 | 19 | 39 | ． 39 | 76 | ． 16 |  | 3.42 | ． 03 | ． 04 |  | 1 |
| L459E 458＋25M | 1 | 79 | 9 | 43 | ． 5 | 208 | 15 | 391 | 2.04 | 14 | 5 | HO | 2 | 15 | 2 | 2 | 2 | 31 | ． 26 | ． 039 | 7 | 27 | ． 32 | 67 | \＄2 |  | 2.00 | ． 03 | ． 05 |  | 6 |
| 1459E 458000w | 2 | 238 | 15 | 57 | \％ 6 | 595 | 26 | 456 | 3.30 | 26 | 5 | NO | 3 | 22 | $\stackrel{3}{4}$ | 2 | 2 | 45 | ． 38 | \％42 | 11 | 53 | ． 57 | 112 | 13 |  | 3.60 | ． 05 | ．6 |  | 1 |
| $14606466+000$ | 1 | 593 | 61 | 71 | ． 6 | 53 | 22 | 709 | 5.66 | 45 | 5 | NO | 5 | 40 | 5 | 4 | 2 | 56 | ． 52 | 0025 | 20 | 47 | ． 81 | 169 | 41 |  | 1.67 | ． 02 | ． 12 |  | 5 |
| 1460E 465＋75） | 1 | 76 | 9 | 117 | ． 1 | 26 | 20 | 340 | 2.68 | 16 | 5 | NO | 1 | 16 | 4 | 2 | 2 | 31 | 1t | ． 028 | 3 | 19 | ．17 | 67 | .09 |  | 1.15 | ． 03 | ．09 |  | 12 |
| 1460F $465+50 \mathrm{~m}$ | 1 | 45 | 10 | 122 | ． 1 | 42 | 21 | 322 | 2.64 | 23 | 5 | ND | 2 | 15 | $\because 2$ | 2 | 2 | 40 | ． 14 | ，068 | 4 | 28 | ． 32 | 93 | 16 |  | 2.93 | ． 02 | ． 04 | 1 | 720 |
| L460E 465＋25\％ | 1 | 67 | 95 | 59 | .2 | 35 | 12 | 458 | 2.32 | 12 | 5 | ND | 4 | 18 | 82 | 2 | 2 | 32 | ． 16 | ［130 | 11 | 21 | ． 29 | 107 | ． 18 |  | 4.84 | ． 03 | O5 |  | 15 |
| L460E 465＋001 | 1 | 57 | 16 | 46 | ． 2 | 27 | 9 | 268 | 2.15 | 9 | 5 | ND | 4 | 17 | 3 | 2 | 2 | 29 | ． 14 | 118 | 12 | 16 | ． 23 | 90 | ，19 |  | 5.14 | ． 03 | ． 03 |  | 1. |
| L460E 463＋50E | 1 | 253 | 16 | 56 | －6 | 62 | 17 |  | 2.56 | 174 | 5 | NO | 3 | 16 | 2 | 2 | 2 | 35 | ． 29 |  | 8 | 23 | ． 25 | 63 | 118 |  | 3.00 | ． 02 | ． 04 |  | 7 9 |
| L460E 463＋2SE | 1 | 54 | 13 | 54 | 2 | 30 | 14 | 393 | 2.22 | 18 | 5 | ND | 3 | 13 | 2 | 2 | 2 | 33 | ． 12 | ． 067 | 5 | 18 | ． 20 | 98 | .16 |  | 3.76 | ． 02 | ． 04 |  | 9 |
| L460E 463＋00E | 1 | 91 | 43 | 57 | ． 3 | 29 | 15 | 568 | 2.20 | 18 | 5 | N0 | 3 | 12 | 2 | 2 | 2 | 32 | ． 11 | ．074 | 5 | 17 | ． 20 | 110 | 17 |  |  | ． 02 | ．04 |  | 82 |
| 1460E 462＋75E | 1 | 19 | 9 | 37 | ¢ 1 | 17 | 7 | 301 | 1.69 | 13 | 5 | W0 | 2 | 11 | 2 | 2 | 2 | 28 | ． 12 | D8\％ | 4 | 17 | .15 | 96 | $\pm 12$ | 2 | 1.99 | ． 02 | ． 04 |  | 74 |
| 1460t 462＋50E | 1 | 46 | 11 | 47 | ． 3 | 26 | 9 | 358 | 2.13 | 14 | 5 | ND | 4 | 13 | $\stackrel{2}{ }$ | 2 | 2 | 32 | .15 | ． 051 | 7 | 18 | ． 23 | 106 | \％17 |  | 3.97 | .02 | ． 65 |  | 2 |
| 1460E 462＋25E | 1 | 33 | 14 | 42 | 2 | 22 | 9 |  | 2.14 | 14 | 5 | ND | 3 | 13 | 2 | 2 | 2 | 32 | ． 12 | 007 | 8 | 19 | ． 22 | 100 | ＊6 |  | 3.60 | ． 02 | 04 |  | 45 |
| 1460E 46240CE | 1 | 67 | 13 | 52 | － 2 | 21 | 9 | 462 | 2.13 | 45 | 5 | ND | 3 | 12 | 2 | 2 | 2 | 31 | ． 12 | 649 | 5 | 17 | ． 21 | 81 | 車 |  |  | 2 | ． 15 |  | 6 |
| 1460E 461450E | 1 | 154 | 12 | 50 | \％ 4 | 25 | 13 | 593 | 2.61 | 14 | 5 | NO | 4 | 12 | $\square 2$ | 2 | 2 | 34 | ． 10 | \％ 73 | \％ | 86 | ． 23 | 160 | 18 |  | 4.12 | ． 02 | ．04 |  | ${ }^{6}$ |
| L460E 461＋25E | 1 | 39 | 10 | 53 | ＋2 | 26 | 10 | 536 | 2.26 | 16 | 5 | ND | 3 | 12 | ． 2 | 2 | 2 | 36 | ． 13 | 075 | 6 | 21 | ． 28 | 141 | 4 \％ |  | 2.65 | ． 02 | ． 0 | $\%$ | 10 |
| L460E 46！＋00t | 1 | 53 | 15 | 69 | 3 | 38 | 12 | 598 | 2.39 | 21 | 5 | WD | 3 | 16 | －2 | 2 | 2 | 37 | ． 96 | 8033 | 7 | 32 | ． 35 | 197 | \％3 |  | 2.24 | ． 02 | ． 65 | ＋ | 29 |
| 1460E 460＋75E | 1 | 37 | 11 | 56 | 3 | 30 | 10 | 569 | 2.09 | 19 | 5 | ND | 3 | 14 | ＋2 | 2 |  | 30 | ． 13 | －091 | 6 | 20 | ． 24 | 122 | 13 |  | 3.36 | ． 02 | ． 04 | ＋ 9 | 7 |
| L．460E 460＋505 | 1 | 54 | 11 | 43 | ． 3 | 49 | 13 |  | 2.56 | 18 | 5 | ND | 3 | 18 | 2 | 2 |  | 39 | ． 20 | \％357 | 8 | 35 | ． 44 | 146 | ${ }^{13}$ |  | 2.70 | ． 02 | ． 05 |  | 18 |
| 1460E 460＋25E |  | 24 | 12 | 76 | 2 | 22 | 10 | 664 | 2.34 | 17 | 5 | N0 | 2 | 15 | 2 | 2 | 2 | 33 | ． 16 | ＋150 | 5 | 22 | ． 20 | 117 | 45 |  | 2.77 2.80 | ． 02 | ． 05 | \％ | 12 |
| L460E 460＋00E | 1 | 80 | 14 | 50 | 1 | 64 | 15 | 251 | 2.47 | 25 | 5 | N0 | 2 | 17 | ． 2 | 3 | 2 | 38 | ． 39 | ．05s | 6 | 34 | .44 | 75 | ． 14 |  | 2.80 | ． 02 | ． 06 |  | 12 |
| 1460E 459＋73E | 1 | 67 | 13 | 44 | ，3 | 40 | 13 | 248 | 2.38 | 19 | 5 | 10 | 3 | 14 | ＋2\％ | ${ }_{15}^{2}$ | 2 | 36 | ． 18 | $\mathrm{cos7}^{2}$ | 39 | 28 | .37 .93 | 84 | ＋69 | 23 | $\begin{aligned} & 3.54 \\ & 1.99 \end{aligned}$ | ． 02 | ． 05 | 11 | 4 |
| STAMDANO C／AU－S | 18 | 62 | 61 | 131 | 7.1 | 72 | 31 | 1036 | 4.08 | 39 | 23 | 7 | 39 | 53 | 39.7 | 15 | 19 | 56 | ． 52 | ， 892 | 39 | 59 | ． 93 | 102 | －69． | 39 | 1.99 | ． | ． 13 |  |  |

Attwood Gold corp. PROJE GOLDEN CROWN FILE \# 90-1366

| SAMPLE無 | $\begin{gathered} \text { Mo } \\ \text { ppon } \end{gathered}$ | $\begin{gathered} \mathrm{Cu} \\ \mathrm{pH} \end{gathered}$ | $\begin{gathered} \mathrm{Pb} \\ \mathrm{Pq} \end{gathered}$ | $\underset{p p n}{2 n}$ | Ag | $\begin{gathered} \mathrm{Ni} \\ \mathrm{pq} \% \end{gathered}$ | $\mathrm{Co}$ | $\begin{gathered} M n \\ p o r n \end{gathered}$ | fe | $\begin{array}{r} A s \\ p \neq m \end{array}$ | $\begin{array}{r} u \\ p p n \end{array}$ | $\begin{array}{r} \text { Au } \\ \text { pxan } \end{array}$ | fh ppm | $\begin{array}{r} \text { Sr } \\ \text { pom } \end{array}$ | pon: | $\begin{array}{r} \text { Sb } \\ \text { ppon } \end{array}$ | $\begin{gathered} \mathrm{Bi} \\ \mathrm{pq} \end{gathered}$ | $\begin{array}{r} v \\ \mathrm{ppm} \end{array}$ | $\underset{X}{C}$ | $\mathbf{\%}$ | L8 | $\begin{array}{r} \mathrm{Cr} \\ \text { pom } \end{array}$ | $\begin{aligned} & \mathrm{Hg} \\ & \mathrm{X} \end{aligned}$ | $\begin{array}{r} 88 \\ \text { ppon } \end{array}$ | $\begin{array}{r} 77 \\ \mathbf{x} \end{array}$ | $\begin{array}{r} 8 \\ \hline \text { pppn } \end{array}$ | $\begin{aligned} & \mathrm{A} \\ & \mathrm{~K} \end{aligned}$ | $\begin{gathered} \text { Na } \\ X \end{gathered}$ |  |  | $\begin{aligned} & \mathrm{Al} \\ & \mathrm{p} \boldsymbol{+}+\mathrm{b} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1460E 459450m | 1 | 74 | 10 | 48 | 3 | 40 | 19 | 959 | 2.52 | 17 | 5 | ND | 3 | 16 | . 2 | 2 | 2 | 36 | . 15 | 460 | 6 | 23 | . 29 | 155 | 15 |  | 3.74 | . 02 | . 05 | 2 |  |
| (460E 459425\% | 1 | 38 | 10 | 51 | :1 | 39 | 16 | 443 | 2.39 | 18 | 5 | ND | 3 | 13 | \% 2 | 2 | 2 | 35 | . 14 | +13 | 4 | 24 | . 28 | 105 | . 35 |  | 3.79 | . 02 | . 04 |  |  |
| [1660E 459+00m | , | 37 | 11 | 46 | 3 | 37 | 16 | 270 | 2.27 | 15 | 5 | ND | 3 | 16 | +2 | 2 | 2 | 33 | . 25 | 883 | 6 | 24 | . 26 | 117 | - 45 |  | 3.68 | . 02 | . 05 | 3 |  |
| 1460E 458+73M | 1 | 37 | 10 | 46 | 3 | 43 | 13 | 331 | 2.09 | 14 | 5 | ND | 3 | 22 | \% | 2 | 2 | 31 | . 25 | \% 65 | 7 | 25 | . 29 | 100 | 44 |  | 3.07 | . 02 | . 05 | 1 |  |
| 1460E 458+50m | 2 | 379 | 13 | 54 | 1.0 | 112 | 13 | 629 | 3.17 | 26 | 5 | NO | 2 | 26 | -2 | 2 | 2 | 42 | . 80 | . 035 | 30 | 52 | . 49 | 118 | 109 |  | 3.53 | . 63 | . 07 |  | 14 |
| 14608 458+250 | 1 | 24 | 10 | 45 | 2 | 49 | 19 | 319 | 2.03 | 15 | 5 | MD | 2 | 14 | 2 | 2 | 2 | 31 | . 16 | W102 | 4 | 20 | . 23 | 84 | . 15 |  | 2.81 | . 02 | . 35 | 1 | 15 |
| L660E 458000N | 1 | 278 | 15 | 63 | 1.2 | 119 | 17 | 532 | 3.54 | 23 | 5 | N0 | 3 | 30 | 2 | 2 | 2 | 50 | . 62 | . 036 | 18 | 67 | . 82 | 140 | . $10^{\circ}$ |  | 4.13 | . 03 | . 10 | E | 16 |
| 1461E 466+00m | 1 | 225 | 12 | 50 | 4 | 54 | 28 | 211 | 2.18 | 11 | 5 | WD | 2 | 18 | 2 | 2 | 3 | 29 | . 28 | .027 | 13 | 17 | . 20 | 58 | 18 |  | 2.70 | . 03 | . 04 | 1 | 10 |
| 1669E 465+75\% |  | 47 | 12 | 57 | 4 | 19 | 11 | 127 | 2.13 | 21 | 5 | ND | 2 | 15 | 12 | 2 | 2 | 33 | . 13 | *38 | 4 | 13 | . 12 | 70 | . 17 |  | 2.8 | . 02 | . 04 | $1$ | 20 |
| 2461E 465+50m | 1 | 133 | 11 | 59 | .3 | 54 | 24 | 334 | 3.57 | 25 | 5 | NO | 5 | 19 | 2 | 2 | 2 | 53 | . 24 | .066 | 16 | 47 | . 70 | 133 | 33 | 2 | 2.82 | . 01 | . 07 | 1 | 29 |
| L661E 465+25M | 9 | 82 | 12 | 61 | 1.1 | 42 | 17 | 336 | 2.63 | 20 | 5 | ND | 4 | 16 | 2 | 2 | 2 | 38 | . 17 | 085 | 13 | 29 | . 36 | 106 | 16 |  | 3.54 | . 03 | . 05 | 1 | 7 |
| L46IE 465000M | 1 | 21 | 9 | 44 | . 2 | 11 | 5 | 182 | 1.59 | 14 | 5 | ND | 2 | 8 | 2 | 2 | 2 | 30 | . 09 | -039 | 5 | 11 | . 13 | 57 | +17 | 2 | 1.12 | . 02 | . 04 | 1 | 8 |
| L467E 464-75\% | 1 | 31 | 8 | 67 | 1. | 23 | 13 | 493 | 2.22 | 17 | 5 | ND | 2 | 11 | 4 | 2 |  | 37 | . 11 | 8047 | 5 | 21 | . 20 | 97 | cts |  | 1.86 | . 02 | . 03 | $t$ | 9 |
| L464E 464450w | 1 | 41 | 11 | 84 | . 1 | 19 | 11 | 398 | 2.74 | 17 | 5 | ND | 3 | 9 | -2 | 2 | 2 | 40 | . 08 | 1344: | 5 | 21 | . 18 | 87 | 16 |  | 3.34 | . 02 | . 04 | 1 | 18 |
| L46tE 464+25M | 1 | 72 | 14 | 53 | 2 | 35 | 13 | 399 | 2.57 | 16 | 5 | ND | 4 | 12 | , 2 | 2 | 3 | 37 | . 11 | . 695 | 7 | 26 | . 35 | 107 | .97 | 2 | 4.59 | . 02 | . 04 | 1 | 66 |
| L689E 46400m | 1 | 64 | 19 | 41 | L | 30 | 16 | 190 | 2.06 | 10 | 5 | N0 | 3 | 14 | \%2 | 2 | 2 | 31 | . 14 | \%67 | \% | 20 | . 23 | 92 | / 1 | 3 | 3.20 | . 02 | . 04 | 4 |  |
| L467E 463-25m | 1 | 32 | 9 | 43 | - 2 | 24 | 10 | 878 | 1.77 | 16 | 5 | ND | 2 | 15 | 2 | 2 | 2 | 28 | . 13 | 8073 | 5 | 18 | . 16 | 105 | . 3 |  | 2.35 | . 02 | . 04 | 2 | 5 |
| L661E 463-00w | , | 64 | 12 | 53 | . 2 | 27 | 14 | 782 | 2.34 | 13 | 5 | N0 | 3 | 16 | 2 | 2 | 2 | 35 | . 16 | .103 | 6 | 24 | . 29 | 105 | 114 |  | 2.69 | . 02 | . 04 | 1 | 14 |
| 1461E 462+75\% | , | 70 | 10 | 43 | 4 | 24 | 12 | 330 | 2.17 | 15 | 5 | NO | 3 | 17 | -2 | 2 | 2 | 32 | . 16 | .078 | 11 | 21 | . 31 | 99 | 15 | 2 | 3.31 | . 02 | . 04 | - | 1 |
| L661E 462+50w | 9 | 284 | 15 | 40 | 2 | 39 | 19 | 349 | 3.48 | 25 | 5 | ND | 3 | 16 | $\square 2$ | 3 | 2 | 47 | . 20 | .060 | 12 | 63 | . 76 | 76 | . 10 | 2 | 1.76 | . 01 | . 65 | \% | 20 |
| L461E 462+25\% | 1 | 48 | 11 | 41 | . 2 | 32 | 12 | 597 | 2.16 | 18 | 5 | ND | 3 | 17 | . 2 | 2 | 2 | 33 | . 16 | O50 | 6 | 24 | . 29 | 125 | .15 |  | 3.23 | . 02 | . 03 | 2 | 48 |
| L461E 462+00N | 1 | 121 | 13 | 51 | . 3 | 38 | 29 | 361 | 2.26 | 9 | 5 | HD | 4 | 15 | 2 | 2 | 2 | 34 | . 15 | .071 | 8 | 25 | . 32 | 99 | 13 |  | 2.87 | . 02 | . 05 | 1 | 32 |
| L469E 461+75N | * | 96 | 11 | 40 | 4 | 58 | 33 | 228 | 2.44 | 35 | 5 | NO | 2 | 13 | . 2 | 2 | 2 | 41 | . 18 | 6022 | 8 | 34 | . 41 | 71 | 14 |  | 1.94 | . 02 | . 05 | 4 | 11 |
| L461E 469+50N | 1 | 35 | 10 | 42 | 3 | 26 | 9 | 415 | 1.98 | 6 | 5 | $N$ | 3 | 19 | $\checkmark 2$ | 2 | 2 | 31 | . 16 | 8083 | 8 | 18 | . 25 | 136 | $\bigcirc 15$ |  | 3.21 | . 02 | . 04 | 1 | 9 |
| L681E 46\% $+25 \%$ | 1 | 39 | 10 | 54 | 2 | 21 | 9 | 57 | 2.01 |  | 5 | ND | 3 | 10 | S2 | 2 | 2 | 32 | . 11 | ,108 | 5 | 17 | . 23 | 96 | 14 | 5 | 3.21 | . 02 | . 06 |  | 7 |
| L469E 469400\% | 1 | 152 | 17 | 58 | 4 | 47 | 25 | 455 | 2.08 | 12 | 5 | ND | . | 19 | 82 | 2 | 2 | 32 | . 49 | 805 | 8 | 27 | .37 | 93 | \% | 2 | 1.84 | . 02 | . 03 |  | 2 |
| L461E 460+75\% | 1 | 59 | 11 | 47 | .5 | 32 | 13 | 203 | 2.29 | 13 | 5 | ND | 3 | 17 | +2 | 2 |  | 35 | . 18 | -089 | 7 | 24 | . 31 | 130 | 14 |  | 3.01 | . 02 | . 66 | 1 | 1 |
| L461E 460+50m | 1 | 46 | 11 | 52 | 4 | 33 | 14 | 663 | 2.29 | 13 | 5 | ND | 3 | 15 | 2 | 3 | 2 | 34 | . 16 | -084 | 6 | 23 | . 29 | 131 | 44 | 2 | 3.95 | . 02 | . 05 | T | 4 |
| L461E 460425\% | 1 | 35 | 13 | 45 | 3 | 24 | 12 | 529 | 2.05 | 10 | 5 | ND | 3 | 16 | 2 | 2 | 2 | 30 | . 14 | ¢ 078 | 5 | 15 | . 18 | 102 | 816 |  | 3.76 | . 02 | . 05 | 1 | 4 |
| L461E 460400M | 1 | 66 | 13 | 51 | -3 | 44 | 16 | 244 | 2.53 | 16 | 5 | ND | 2 | 18 | 2 | 2 | 2 | 37 | . 26 | O588 | 7 | 29 | . 33 | 102 | ¢5 | 3 | 2.93 | . 02 | . 65 |  | 1 |
| 14695 459+75M | 1 | 65 | 12 | 4 | 5 | 42 | 12 | 633 | 2.28 | 14 | 5 | ND | 3 | 45 | - | 3 | 2 | 31 | . 21 | . 055 | 8 | 24 | . 29 | 126 | 814 |  | 3.36 | . 02 | . 0.6 |  | 2 |
| L461E 459+50W | 1 | 37 | 12 | 48 | .2 | 34 | 13 | 299 | 2.14 | 12 | 5 | NO | 2 | 45 | 2 | 2 | 2 | 33 | . 22 | . 074 | 4 | 26 | . 29 | 108 | 動3 | 2 | 2.75 | . 02 | . 11 | - |  |
| $14615459+25 \%$ | 1 | 118 | 16 | 91 | 180 | 85 | 18 | 460 | 3.70 | 11 | 5 | NO | 4 | 28 | 2 | 2 | 2 | 44 | . 64 | 8032 | 12 | 48 | . 56 | 138 | 15 | 4 | 4.42 | . 03 | .to | - | 7 |
| (467E 459400\% | 1 | 63 | 12 | 54 | 4 | 36 | 12 | 298 | 2.64 | 8 | 5 | ND | 3 | 17 | 2 | 3 | 2 | 35 | . 25 | $\underset{\sim}{126}$ | 9 | 28 | . 36 | 136 | - 14 |  | 3.56 | . 02 | . 06 | $\underline{3}$ | 49 |
| L4615 458475w | 1 | 61 | 13 | 73 | 3 | 44 | 14 | 388 | 2.58 | 16 | 5 | ND | 3 | 18 | 2 | 2 | 2 | 35 | . 26 | ${ }_{6} 43$ | 8 | 34 | . 42 | 144 | - 4 | 4 | 3.42 | . 02 | . 65 |  | 19 |
| 26615 430+50m | 1 | 201 | 12 | 67 | 1.0 | 67 | 17 | 576 | 3.12 | 21 : | 5 | ND | 3 | 24 |  | 2 | 3 | 48 | . 44 | 81852 | 31 | 57 | . 77 | 129 | . 4 | 2 | 3.17 | . 03 | . 6 | 1 | 2 |
| STAMDARD C/My-S | 18 | 58 | 39 | 132 | 7.1 | 72 | 319 | 1038 | 4.00 | 39 | 21 | 7 | 38 | 53 | 9,4 | 14 | 23 | 56 | . 51 | \% 042 | 39 | 59 | . 91 | 182 | 69 | 59 | 1.93 | . 06 | 16 | 14 | 49 |


| SAMPLEF | $\begin{gathered} \text { Mo } \\ \hline \end{gathered}$ | $\begin{gathered} \mathrm{Cu} \\ \mathrm{PDPm} \end{gathered}$ | $\begin{aligned} & \mathrm{Pb} \\ & \mathrm{ppmm} \end{aligned}$ | $\begin{array}{r} 2 n \\ \text { ppm } \end{array}$ | $\mathrm{Ag}$ | $\begin{gathered} \mathrm{Ni} \\ \text { pom } \end{gathered}$ | $\begin{array}{r} \text { co } \\ \text { pom } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppm } \end{array}$ | $\begin{array}{lr} \text { n } & \text { Fe } \\ m & \mathbf{x} \end{array}$ | $\begin{aligned} & \text { As } \\ & \text { pon } \end{aligned}$ | $\begin{array}{r} \mathrm{U} \\ \mathrm{pram} \end{array}$ | $\begin{gathered} \mathrm{Au} \\ \mathrm{ppm} \end{gathered}$ | $\begin{gathered} \text { Th } \\ \text { ppom } \end{gathered}$ | $\begin{array}{r} \mathbf{S T} \\ \mathbf{p q} \boldsymbol{m} \end{array}$ | $\begin{gathered} \mathrm{cd} \\ \mathrm{ppm} \end{gathered}$ | $\begin{gathered} \mathbf{S b} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \text { Bi } \\ \text { Ppm } \end{array}$ | $\begin{array}{r} v \\ \text { pon } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ x \end{gathered}$ | $\%$ | Lem | $\underset{\mathrm{pram}}{\mathrm{Cr}}$ | $\begin{array}{\|c} \mathrm{Mg} \\ \mathrm{x} \end{array}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | $\mathrm{TI}$ | $\begin{array}{r} \text { B } \\ \hline \text { m } \end{array}$ | $\begin{gathered} \mathrm{Al} \\ \mathrm{X} \end{gathered}$ | Wa | $\begin{aligned} & x \\ & \mathbf{x} \end{aligned}$ | M | Avid |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2469E 458+25\% | 1 | 38 | 10 | 4 | 2 | 24 | 12 | 588 | 1.98 | 18 | 5 | ND | 2 | 21 | 2 | 2 | 2 | 32 | . 33 | \% 049 | 6 | 23 | . 33 | 124 | . 11 |  | 2.13 | . 02 | . 06 | 2 | 10 |
| L461E 450+00m | 1 | 30 | 9 | 55 | 2 | 19 | 9 | 579 | 1.62 | 15 | 5 | ND | 2 | 27 | ,2 | 2 | 2 | 24 | . 31 | . 167 | 5 | 20 | . 28 | 168 | \% 0 |  | 1.53 | . 02 | . 07 | 1 | 22 |
| $126628466+00 \mathrm{M}$ | 1 | 78 | 46 | 52 | 3 | 32 | 14 | 424 | 2.28 | 19. | 5 | ND | 2 | 21 | . 2 | 2 | 2 | 35 | . 21 | .052 | 7 | 28 | . 37 | 109 | to | 8 | 1.82 | . 02 | . 05 | 1 | 6 |
| (LUCZE 465+73M | 1 | 251 | 11 | 49 | 4 | 52 | 19 | 27 | 3.22 | 24 | 5 | ND | 4 | 15 | :2 | 2 | 2 | 45 | . 17 | 8055 | 13 | 45 | . 65 | 69 | .11 |  | 2.26 | . 02 | . 05 | 1 | 74 |
| 1462E 465+50m | 1 | 85 | 12 | 52 | 2 | 35 | 13 | 568 | 2.22 | 21 | 5 | N0 | 2 | 21 | 4 | 2 | 2 | 33 | . 29 | \%089 | 7 | 27 | . 38 | 105 | 11 |  | 2.32 | . 02 | . 07 | 1 | 6 |
| L462E 465+251 | $\dagger$ | 132 | 11 | 44 | 4 | 41 | 17 | 197 | 2.57 | 19 | 5 | no | 2 | 15 | 2 | 2 | 2 | 38 | . 28 | . 035 | 7 | 30 | . 38 | 72 | 13 |  | 2.66 | . 02 | . 05 | 1 | 7 |
| L46ZE 465+00M | 1 | 28 | d | 25 | 2 | 16 | 8 | 211 | 1.39 | 2 | 6 | ND | 3 | 6 | 2 | 2 | 2 | 21 | . 08 | .046 | 4 | 11 | . 13 | 51 | . 09 |  | 1.58 | . 02 | . 05 | 2 | 105 |
| C462E 464+751 | 1 | 23 | 6 | 42 | 1. | 12 | 7 | 192 | 1.64 | 22 | 5 | ND | 1 | 6 | 2 | 3 | 2 | 25 | . 06 | \$22 | 3 | 13 | . 12 | 50 | do9 |  | 1.71 | . 01 | . 02 | 1 | 18 |
| 1462E 464+50M | 1 | 33 | 7 | 49 | 2 | 17 | 8 | 347 | 2.33 | 13 | 6 | ND | 3 | 11 | 42 | 2 | 2 | 39 | . 12 | \%06\% | 6 | 21 | . 22 | 83 | $\underline{.13}$ |  | 1.64 | . 02 | . 05 | 1 | 19 |
| 1462E 464+25* | 1 | 38 | 11 | 57 | 4 | 30 | 13 | 576 | 2.23 | 16 | 5 | No | 3 | 16 | .2 | 2 | 2 | 32 | . 14 | 4093 | 5 | 18 | . 21 | 95 | 15 |  | 3.46 | . 02 | . 03 |  | 9 |
| L462E 464+00M | 1 | 41 | 19 | 61 | 33 | 23 | 10 | 790 | 1.99 | 22 | 5 | NO | 3 | 13 | L | 2 | 2 | 29 | . 14 | 144. | 5 | 18 | . 18 | 115 | 14 |  | 3.54 | . 02 | ,04 | 1 | 7 |
| L462E $663+75 \mathrm{H}$ | 1 | 11 | 5 | 15 | 1 | 7 | 2 | 41 | . 64 | 2 | 5 | ND | 1 | 8 | 2 | 2 | 2 | 17 | . 13 | 0014 | 2 | 9 | . 05 | 16 | . 0 |  | . 36 | . 02 | . 01 | 1 | 3 |
| L462E 463+00N | 1 | 42 | 9 | 85 | 2 | 33 | 20 | 502 | 2.11 | 15 | 5 | ND | 3 | 9 | , 2 | 2 | 2 | 32 | . 09 | .06t | 4 | 18 | . 21 | 66 | 13 |  | 2.61 | . 02 | .04 | 1 | 6 |
| 1462E 462+75M | 1 | 42 | 9 | 61 | 3 | 32 | 14 | 508 | 2.11 | 32 | 5 | ND | 3 | 15 | , 2 | 2 | 2 | 31 | . 14 | . 078 | 5 | 18 | . 20 | 116 | 14 |  | 3.39 | . 02 | . 06 | 1 | 90 |
| L462E 462+50N | 1 | 36 | 6 | 38 | 4 | 19 | 11 | 514 | 1.54 | 10 | 5 | HD | 2 | 8 | . 2 | 2 | 2 | 27 | . 09 | \$068 | 4 | 13 | . 15 | 89 | . 11 |  | 1.87 | . 03 | . 03 | 1 | 5 |
| L462E 462+25M | 1 | 37 | 9 | 48 | 2 | 19 | 10 | 314 | 1.80 | 16 | 5 | ND | 3 | 9 | 2 | 2 | 2 | 28 | . 09 | . 091 | 5 | 13 | . 16 | 61 | $\bigcirc 4$ |  | 2.99 | . 02 | .03 | 1 | 5 |
| L462E 462+000 | 1 | 36 | 11 | 54 | . 2 | 27 | 11 | 762 | 2.10 | 22 | 5 | wD | 2 | 13 | . 2 | 2 | 2 | 32 | . 14 | \%087 | 5 | 20 | . 24 | 137 | . 14 |  | 3.16 | . 02 | . 03 | * | 1 |
| 14625 461+75* | 1 | 67 | 8 | 54 | 2 | 37 | 16 | 176 | 2.37 | 13 | 5 | ND | 3 | 21 | ${ }^{2}$ | 2 | 2 | 35 | . 23 | . 063 | 7 | 26 | . 32 | 130 | 113 |  | 3.11 | . 02 | . 06 | 1 | 29 |
| L46ZE 461+501 | 1 | 462 | 16 | 70 | 7 | 128 | 17 | 302 | 2.50 | 23 | 5 | ND | 4 | 23 | 2 | 2 | 2 | 30 | . 42 | $\bigcirc 052$ | 12 | 21 | . 26 | 76 | .18 |  | 6.32 | . 06 | . 03 | 1 | 10 |
| 1462E 461425N | 1 | 79 | 5 | 52 | 3 | 34 | 14 | 213 | 2.50 | 25 | 5 | N0 | 3 | 16 | . 2 | 2 | 2 | 35 | . 18 | 119 | - | 27 | . 33 | 95 | . 12 |  | 2.92 | . 02 | . 04 |  | 16 |
| 1462E 461+00M | 1 | 42 | 90 | 61 | -2 | 25 | 13 | 436 | 2.35 | 19 | 5 | No | 3 | 11 | 2 | 2 | 2 | 34 | . 12 | .159 | 5 | 20 | . 22 | 92 | 14 |  | 3.67 | . 02 | . 05 | 1 | 6 |
| L462E 460+75M | 1 | 243 | 14 | 79 | 1.1 | 84 | 14 | 469 | 3.05 | 28 | 5 | ND | 4 | 26 | 14 | 2 | 2 | 42 | . 33 | . 059 | 15 | 39 | . 48 | 199 | 14 |  | 3.86 | . 02 | . 08 | 1 | 8 |
| 1462E 460+50W |  | 132 | 16 | 91 | . 8 | 72 | 13 | 447 | 2.78 | 23 | 5 | NO | 4 | 25 | 4 | 2 | 2 | 39 | . 23 | 069 | 11 | 31 | . 37 | 227 | 45 |  | 3.83 | . 03 | . 07 | 9 | 14 |
| 14625 460+25\% | , | 36 |  | 70 | . 4 | 40 | 10 |  | 2.28 | 21 | 5 | WD | 3 | 20 | 2 |  | 2 | 32 | . 22 | \%084 | 6 | 22 | . 28 | 153 | $\times 14$ |  | 3.12 | . 02 | . 06 | 1 | 5 |
| LU6ZE 660+00M | 1 | 40 | 5 | 69 | 4 | 31 | 8 | 307 | 1.87 | 18. | 5 | ND | 3 | 14 | 2 | 2 | 2 | 29 | . 14 | 144 | 5 | 21 | . 24 | 130 | \%11 |  | 2.07 | . 02 | . 05 |  | it |
| L462E 459+751 | 1 | 27 | 9 | 72 | 3 | 38 | 9 | 482 | 2.10 | 18 | 5 | ND | 3 | 17 | . 2 | 2 | 2 | 31 | . 16 | . 233 | 5 | 21 | . 26 | 179 | , 12 |  | 2.83 | . 02 | . 06 | 1 | 9 |
| LL6CE 459+50M | 1 | 49 | 11 | 59 | . 3 | 32 | 8 | 367 | 1.77 | 16 | 5 | No | 2 | 22 | . 2 | 2 | 2 | 28 | . 29 | 082 | 7 | 23 | . 30 | 130 | \%09 |  | 1.61 | . 02 | . 05 | 1 | 5 |
| 1462E 459+25\% | 1 | 129 | 9 | 39 | . 8 | 50 | 7 | 285 | 1.94 | 18 | 5 | ND | 2 | 16 | ${ }^{2}$ | 2 | 2 | 30 | . 46 | , 020 | 12 | 34 | . 34 | 74 | . 08 |  | 1.85 | . 04 | . 06 | 1 | 1 |
| t462E 459+00M | 1 | 39 | 8 | 66 | 3 | 25 | 8 | 607 | 1.65 | 16 | 5 | ND | 2 | 18 | 2 | 2 | 2 | 28 | . 30 | . 052 | 6 | 22 | . 27 | 86 | \% O |  | . 32 | . 02 | . 06 | 1 | 2 |
| 1462E 450+75M | 1 | 33 | 10 | 83 | 5 | 62 | 11 | 508 | 2.28 | 18 | 5 | WD | 3 | 19 | . 2 | 2 | 2 | 30 | . 18 | 190. | 6 | 27 | . 36 | 169 | $\pm 12$ |  | 2.87 | . 02 | . 06 |  | 1 |
| 1462E 450+50m | 1 | 29 | 10 | 87 | . 4 | 40 | 12 | 672 | 2.34 | 19 | 5 | NO | 3 | 25 | .2 | 2 | 2 | 32 | . 23 | 190 | 8 | 31 | . 37 | 224 | 10 |  | . 30 | . 02 | . 07 |  | 1 |
| 1462E 450+25M | 1 | 59 | 11 | 59 | ${ }^{4}$ | 41 | 9 | 496 | 1.71 | 16 | 5 | ND | 1 | 21 | 4 | 2 | 2 | 27 | . 21 | . 08 | 12 | 26 | . 35 | 103 | 07 |  | . 27 | . 02 | . 06 | 1 | 40 |
| 14622 650+00 | 1 | 46 | 9 | 81 | . 7 | 64 | 12 | 397 | 2.38 | 16 | 5 | ND | 3 | 23 | $\underline{2}$ | 2 | 2 | 33 | . 24 | 128 | 10 | 31 | . 43 | 178 | 41 |  | . 67 | . 02 | . 07 | 1 | 1 |
| (463E 462+50w | 1 | 197 | 4 | 27 | 4 | 46 | 5 | 166 | 1.11 | 6 | 5 | ND | 2 | 15 | $\stackrel{2}{2}$ | 2 | 2 | 19 | . 27 | 8020 | 9 | 18 | . 13 | 43 | $\stackrel{0}{0}$ |  | . 32 | . 04 | . 06 | 1 | 1 |
| L463E 462+25M | 1 | 58 | 6 | 52 | 6 | 30 | 12 | 331 | 2.28 | 24 | 5 | ND | 3 | 17 | 2 | 2 | 2 | 34 | . 22 | 0093 | 7 | 22 | . 28 | 117 | 4 |  | 3.4 | . 02 | . 06 | 1 | 20 |
| 1463E 462400m | 1 | 35 | 8 | 3 | 3 | 27 | 13 |  | 2.20 | 21 | 5 | ND | 3 | 13 | , 2 | 2 | 2 | 32 | . 14 | 038 | 4 | 16 | . 20 | 76 | 16 |  | . 88 | . 02 | . 03 | 1 | i. |
| Stampard c/au-s | 18 | 58 | 38 | 132 | 7.0 | 71 | 31 | 1032 | 3.94 | 43 | 21 | 6 | 38 | 53 | 19.1 | 15 | 19 | 55 | . 50 | .098 | 38 | 57 | . 90 | 180 | $\mathrm{COB}^{\text {c }}$ |  | . 89 | . 06 | . 13 | 11 | 34 |



| SHPPLE: | $\begin{aligned} & n_{0} \\ & \hline p o r \end{aligned}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{prm} \end{array}$ | $\begin{aligned} & \text { pb } \\ & p o p m \end{aligned}$ | $\begin{array}{r} 2 n \\ \text { PPN } \end{array}$ | Ag | $\begin{gathered} \mathrm{Mi} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { pom } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { pam } \end{array}$ | $\mathrm{Fe}$ | $\begin{aligned} & \text { AB } \\ & \text { pent } \end{aligned}$ | $\begin{array}{r} \mathrm{U} \\ \mathrm{ppom} \end{array}$ | $\begin{gathered} \mathrm{Au} \\ \mathrm{ppn} \end{gathered}$ | $\begin{array}{r} \text { Th } \\ \text { ppom } \end{array}$ | ${ }_{\text {ppr }}$ | $\begin{aligned} & \mathrm{cd} \\ & \mathrm{ppm} \end{aligned}$ | $\begin{array}{r} \text { sb } \\ \text { pom } \end{array}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{pem} \end{array}$ | $\begin{array}{r} \mathbf{y} \\ \text { pront } \end{array}$ | $\mathrm{Ca}$ | $\dot{P}$ | La | $\begin{gathered} \mathrm{Cr} \\ \mathrm{pon} \end{gathered}$ | $\begin{aligned} & \mathrm{Mg} \\ & \mathrm{x} \\ & \hline \end{aligned}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \\ \hline \end{array}$ | $\underset{1}{71}$ | $\begin{gathered} \mathrm{B} \\ \mathrm{pron} \end{gathered}$ | $41$ | $\mathrm{Mg}$ | $\begin{aligned} & x \\ & x \end{aligned}$ | Hive | $\begin{aligned} & \text { mp } \\ & \text { ppo } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Gck 90-? | , | 32 | 4 | 21 | 11 | 1351 | 25 | 35 | 3.23 | 26 | 5 | no | 1 | 74 | .5 | 2 | 2 | 13 | 1.6 | S005 | 2 | 334 | 11.55 | 57 | 01 | 2 | . 32 | . 01 | . 02 | 1 | 3 |
| $15 C R 190-2$ | 1 | 16 | 4 | 7 | ${ }^{2}$ | 1058 | 31 | 376 | 3.37 | 19 | 5 | No | 1 | 91 | 5 | 2 | 2 | 17 | . 81 | , 704 | 2 | 621 | 12.85 | 26 | 01 | 8 | . 51 | . 01 | . 02 | 1 | 4 |
| CCH 90-3 | 1 | 13 | 143 | 829 | 1 | 359 | 13 | 460 | 1.79 | 38 | 5 | ND | 1 | 590 | 31 | 2 | 2 | 13 | 5.64 | .003 | 2 | \$04 | 9.49 | 12 | $\cdots 01$ | 2 | . 42 | . 01 | . 09 | 1 | 1 |
| ach m-4 | 2 | 176 | 3 | $\bigcirc$ | 1 | 16 | 3 |  | 2.68 | 5 | 5 | no | 1 | 9 | 2 | 2 | 2 | 69 | . 33 | . 615 | 2 | 14 | . 61 | 22 | 14 | 2 | . 99 | . 13 | . 65 | 1. |  |
| OCI $90-5$ | 4 | 326 | 5 | 30 | 2 | 17 | 12 | 209 | 2.77 | 10 | 5 | no | 1 | 3 | $\checkmark 2$ | 2 | 3 | 76 | . 17 | ¢14 | 2 | 45 | 1.24 | 20 | $+\infty$ | 8 | 4.17 | . 05 | . 09 | 17 | 105 |
| 5tampare C/MU-a | 17 | 61 | 39 | 130 | 7.0 | 68 | 30 | 1022 | 3.93 | 39 | 22 | 7 | 38 | 53 | 18.4 | 15 | 19 | 55 | . 50 | 69\% | 37 | 56 | . 90 | 481 | 09 | 39 | 1.8 | . 06 | . 13 | 43 | 490 |


| SAMPLET | $\begin{gathered} \text { Ho } \\ \text { ppren } \end{gathered}$ | cu | $\begin{gathered} \text { Pb } \\ \text { ppm } \end{gathered}$ | 2n | hg | $\underset{\text { pprin }}{\text { Mi }}$ | $\begin{gathered} \mathrm{Co} \\ \mathrm{popm} \end{gathered}$ | $\begin{gathered} \mathrm{Mn} \\ \text { ppin } \end{gathered}$ | $\begin{gathered} \mathrm{Fe} \\ \mathrm{x} \end{gathered}$ | H8 | $\begin{array}{r} U \\ p p m i \end{array}$ | $\begin{array}{r} \text { Au } \\ \text { ppom } \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { ppon } \end{array}$ | $\begin{array}{r} \mathbf{5 r} \\ \text { pron } \end{array}$ | $\begin{aligned} & c d \\ & \text { ppman } \end{aligned}$ | $\begin{gathered} \text { sb } \\ \text { ppin } \end{gathered}$ | $\begin{gathered} \text { 日 } \\ \text { ppon } \end{gathered}$ | $\begin{array}{r} \mathrm{V} \\ \hline \end{array}$ | $\underset{\mathbf{X}}{\mathbf{C x}}$ |  | $\underset{\text { ppm }}{\text { L! }}$ | $\begin{gathered} \mathrm{Er} \\ \mathrm{ppm} \end{gathered}$ | Mg | Ben | $T$ | （8） | $\begin{gathered} \text { n! } \\ \mathbf{E} \end{gathered}$ | $\underset{~}{\text { We }}$ | $7$ | $\underset{y}{M}$ | $\begin{aligned} & \text { Aut } \\ & \text { RPb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 51 | 6 | 35 | 4 | 23 | 8 | 306 | $1 . \%$ | 10 | 5 | N0 | 2 | 45 | 4 | 2 | 2 | 29 | .17 | $\bigcirc 671$ | 5 | 12 | ． 15 | 09 | 24 |  | 4.42 | ． 02 | ． 63 | t： | 19 |
| 14635 460＋ | 1 | 57 | 9 | 42 | 3 | 29 | 12 | 399 | 2.25 | 16 | 5 | ND | 2 | ＊ 8 | 4 | 2 | 2 | 37 | ． 22 | 064 | 6 | 21 | ． 27 | 95 | 19 |  | 2.02 | ． 02 | ． 04 | 1 | 4 |
| L685E 465－50m | 1 | 129 | 12 | 46 | 3 | 31 | 14 | 464 | 2.56 | 17 | 5 | N0 | 3 | 15 | 6 | 3 | 2 | 39 | ． 45 | 8123 | 11 | 25 | ． 30 | 98 | 21 |  | 4.30 | ． 02 | ． 05 | 1 | 36 |
| L435E $465+25 \mathrm{M}$ | 1 | 73 | 12 | 50 | － | 31 | 13 | 610 | 2.28 | 18 | 5 | ND | 3 | 18 | 6 | 2 | 2 | 36 | ． 49 | ＋091 | 8 | 20 | ． 30 | 117 | 21 |  | 9 | ． 02 | ． 05 | 1 | 2 |
| L463E 465＋00N | 1 | 114 | 5 | 48 | 3 | 27 | 12 | 43． | 2.22 | 12 | 5 | ND | 2 | 14 | ＋7． | 2 | 3 | 37 | 17 | \％06： | 8 | 22 | ． 3 | 110 | 19 |  | 2.99 | ． 02 | ． 6 |  | 16 |
| LCGE 4 | 1 | 66 | 18 | 47 | 2 | 27 | 11 | 394 | 2.29 | \％ 4 | 5 | HD | 3 | 12 | 10 | 2 | 2 | 35 | ． 15 | D69． | 7 | 20 | ． 30 | 24 | 22 |  | ． 29 | ． 02 | ． 0 |  | 38 |
| L463E 46 | 1 | 222 | 10 | 56 | ． 5 | 37 | 14 | 17\％ | 2.57 | 1 | 5 | MD | 3 | 12 | 7 | 2 | 2 | 51 | ． 15 | 053 | 9 | 26 | ． 36 | 69 | ． 24 |  | 4.55 | ． 02 | ． 05 |  | 850 |
| L463E 46－25M | 1 | 116 | 5 | 56 | 1 | 26 | 12 | 319 | 2.48 | 12 | 5 | MD | 2 | 12 | 4 | 2 | 3 | 43 | ． 15 | \％070 | 7 | 24 | ． 31 | 6 | 19 |  | 2.61 | ． 02 | ．05 | 4 | 60 |
| 1463E 464001 | 9 | 80 | 12 | 49 | 1 | 20 | 7 | 210 | 2.54 | 14 | 5 | Mo | 2 | 8 | 2 | 2 | 2 | 43 |  | 0068 | 6 | 18 | －25 | 63 | 21. |  | 2.68 | ． 01 | ． 04 |  | 5 |
| L663E 463－75\％ | ＊ | 144 | 12 | 55 | 2 | 27 | 10 | 395 | 2.16 | 14 | 5 | N0 | 3 | 12 | 4 | 2 | 2 | 35 | ． 14 | 077． | B | 19 | ． 27 | 90 | co |  | 3.22 | ． 02 | ． 04 |  |  |
| 1648 433＋50m | 1 | 57 | 11 | 65 | 1 | 32 | 15 | 274 | 1.59 | 12 | 5 | W00 | 2 | 10 | 8 \％ | 2 | 2 | 27 | ． 10 | \％036 | 4 | 13 | ． 14 | 80 | 17 |  | 2.70 | ． 02 | － 010 |  | 1 |
| 1463E 463＋25 | 1 | 105 | 13 | 50 | 3 | 40 | 12 | 136 | 2.01 | 12 | 5 | MO | 2 | 21 | － 2 | 2 | 2 | 34 | ． 21 | \＄030 | 6 | 19 | ． 24 | 156 | t |  | 2.83 | 12 | 㐋 | 2 | 35 |
| L463E 463＋60\％ | 1 | 279 | 16 | 57 | 6 | 105 | 81 | 222 | 2．86 | 18 | 5 | MD | 3 | 23 | 2 | 3 | 2 | 35 | ． 56 | 4023 | 11 | 31 | ． 34 | 80 | 23 |  |  | ． 03 | ． 04 | 1 | 4 |
| L463E 462＋73N | 1 | 223 | 38 | 78 | 3 | 62 | 23 | 681 | 3.47 | 49 | 5 | 10 | － | 53 | 0 | 2 | 3 | 5 | ． 36 | 083． | 24 | 1 | 7 | 117 | 4． |  |  | 0 | －19 | ， | 2 |
| L464E 466＋00m | 1 | 45 | 9 | 56 | 11 | 22 | 9 | 247 | 2.09 | 14 | 5 | MD | 1 | 13 | 3 | 2 | 3 | 36 | ． 20 | 8455： | 5 | 18 | ． 24 | 7 | ＋6 |  | 9 | ． 02 | ． 04 |  | 2 |
| E | 1 | 168 | 11 | 78 | ． 5 | 33 | 11 | 220 | 2.31 | 13 | 5 | m | 2 | 12 | 3 | 2 | 2 | 35 | ． 13 | ＊erz | 6 | 19 | ． 25 | 101 | 21 |  | 3.76 | ． 02 | ． 08 |  | 1 |
| L44E 465＋50m | 1 | 87 | 10 | 85 | 3 | 34 | 15 | 463 | 2.55 | 13 | 5 | ND | 2 | 24 | 4 | 2 | 2 | 39 | ． 29 | O6\％ | 9 | 26 | ． 35 | 253 | d8 |  | ． 28 | ． 02 | －60 |  | 0 |
| L64E 465＋25in | 1 | 68 | 10 | 69 | 2 | 40 | 15 | 910 | 2.46 | 21 | 5 | MD | 2 | 22 | ．6 | 2 | 2 | 39 | ． 33 | C085： | 8 | 27 | ． 36 | 219 | 817 |  | 3.60 | ． 02 | ． 64 | \％ | 12 |
| L464E 465000 | 1 | 43 | 10 | 44 | 2 | 26 | 11 | 564 | 1.91 | 17 | 5 | ND | 2 | 15 | \％ | 2 | 3 | 30 | ． 15 | －063 | 5 | 14 | ． 22 | 153 | 21 |  | 3.39 | .02 | ． 05 |  | 10 |
| L464E 464＊751） | 1 | 69 | 14 | 64 | 2 | 36 | 12 | 436 | 2.59 | $12$ | 5 | ND | 2 | 12 | 2 | 2 | 2 | 43 | ． 17 | 10.7 | 7 | 26 | ． 35 | 153 | ． 2. |  | 3.3 | ＋ 02 | ． 05 |  |  |
| F 4 |  | 58 | 10 | 49 | 3 | 27 | 9 | 359 | 2.02 | 11 | 5 | HD | 3 | 11 | ， 2 | 2 | 2 | 34 | ． 12 | 006 | 7 | 18 | ． 28 | 129 | 20： |  | ．45 | ． 02 | ． 04 |  | 22 |
| L464E 464 | 1 | 75 | 40 | 56 | 3 | 29 | 11 | 491 | 2.21 | \％t1 | 5 | ND | 3 | 16 | － 3 | 2 | 2 | 36 | ． 16 | －064 | 9 | 22 | ． 30 | 127 | 2. |  | 3.59 | 02 | ． 04 |  | 1 |
| L484E 466000m | 1 | 156 | 7 | 70 | 4 | 36 | 13 | 308 | 3.18 | 20 | 5 | W0 | 2 | 13 | ． 2 | 2 | 2 | 51 | ＋16 | 07： | 7 | 27 | ． 38 | 9 | 21 |  |  | ． 01 | 0 |  | 4 |
| L664E 463 7 7 ${ }^{\text {\％}}$ | 1 | 172 | 10 | 43 | 3 | 24 | 12 | 346 | 5.84 | 15 | 5 | vo | 3 | 15 | ${ }_{5}$ | 3 | 3 | 26 | .15 | 074 | 5 | 13 |  | 61 |  |  |  | ． 02 | .05 |  | 4 |
| L64E 463＋50m | 1 | 165 | 44 | 72 | 1 | 27 | 25 | 164 | 1.74 |  | 5 | N0 | 2 | 11 | 4 | 2 | 2 | 26 |  |  | 5 |  |  |  |  |  |  | ． |  |  |  |
|  |  |  | 23 | 50 |  | 66 | 11 | 292 | 1.68 | 15 | 5 | MD | 1 | 34 | ， 5 | 2 | 2 | 24 |  | 065 | 7 | 49 | ． 20 | 137 | $8{ }_{4}^{20}$ |  | 2.85 | ． 13 | .10 | $\pm 1$ | 6 |
|  | 1 | 125 | 15 | 57 | 4 | 48 | ＊1 | 375 | 1.98 | 18： | 5 | ND | 1 | 26 | \％ | 2 | 2 | 33 | ． 48 | 068 | 10 | 24 | ． 33 | 123 | 17 |  | 2.64 | ． 02 | － 0 |  | 46 |
| 1464E 462＋751 | 1 | 280 | 8 | 53 | 2． 5 | 30 | 45 | 307 | 2．56 | 21 | 5 | NS | 2 | 20 | 4 | 2 | 3 | 38 | ． 24 | ．092 | 9 | 27 | ． 37 | 106 | 17 |  | 1 | ． 02 | ． 65 |  | 5 |
| LC64E 462＋50N | 1 | ＊ | 4 | 62 | 5 | 28 | 12 | 459 | 2.33 | 19. | 5 | ND | 2 | 16 | 2 | 2 | 2 | 55 | ． 20 | 8014 | 6 | 23 | ．32 | 115 | 4 |  | 3.21 3.76 | .02 | ． 05 | ＋1 | 2 |
| L464E 462＋25M | 1 | 167 | 16 | 81 | 2 | 76 | 16 | 611 | 2.50 | 20： | 5 | WD | 2 | 17 | 2 | 2 | 2 | 35 | ． 39 |  | 6 | 22 | ． 26 | 9 |  |  | 3.76 | ． 42 | － |  | 2 |
|  |  | 185 | 13 | 53 | 2 | 48 | 15 | 298 | 2.60 | $26:$ | 5 | ND | 2 | 16 | 42 | 4 | 2 | 4 | ． 37 | 01\％ | \％ | 50 | ． 55 | 101 | 13 |  | 2.13 | .02 | ． 04 | ＂ | 3 |
| LGGEE 6S1*TSM | 1 | 76 | 13 | 71 | 2 | 34 | 12 | 284 | 2.07 | 19 | 5 | ND | 2 | 10 | \％ 5 | 2 | 2 | 33 | ．13 | 0 Ot | 5 | 19 | ＋24 | 8t | 19 |  | 2. | ． 01 | ． 04 | 1 |  |
| LESGE 66t＋50m | 2 | 284 | 20 | 92 | $\pm$ | 59 | 19 | 302 | 3.60 | 35 | 5 | ND | 3 | 17 | ， 3 | 3 | 4 | 49 | ． 23 | D61 | 13 | 39 | ＋56 | 120 | f6 |  |  | ． 01 | 06 |  | 4 |
| L64E 46t＋25M |  | 102 | 7 | 95 | 3 | 52 | 16 | 482 | 2.55 | 23 | 5 | ND | 2 | 23 | $\pm 2$ | 2 | 3 | 39 | ． 61 | 087 | 9 | 29 | ． 40 | 132 |  |  |  | 2 | ． 05 |  | 15 |
| 1664E 467＋06m | 1 | 43 | 11 | 72 | 5 | 40 | 11 | 468 | 2.15 | 19. | 5 | ND | 2 | 18. | ． 8 | 2 | 3 | 31 | ． 19 | \％094 | 8 | 20 | ． 24 | 152 | －2： |  |  | 2 | ．お |  |  |
|  |  |  |  |  |  |  |  |  | 1.95 | 17 | 5 | \％ | 2 | 24 | S | 2 | 2 | 30 | ． 25 | 097\％ | 0 | 20 | ． 27 | 168 | \％16 |  | 2.46 | ． 02 | ． 05 | 1 | 17 |
|  | 18 | 50 | 39 | 129 | 4．31 | 67 | 31 | 1047 | 3.98 | 42 | 18 | 7 | 36 | 47 | $3 \mathrm{~B}, 5$ | 16 | 21 | 57 | ． 51 | ． 092 | 37 | 55 | ．89 | 174 | 8 | 36 | 1.98 | ． 06 | ． 13 | 11. | 52 |


 SAMPLE TYPE：Soil－BO Mesh RU＊AMALYSIS By AC1D LEACH／AM FROM 10 Gm sample．


Attwood Gold corp．PROJEb GOLDEN CROWN

| SAMPLE | $\begin{gathered} \text { Mo } \\ \text { ppp } \end{gathered}$ | Cu | $\begin{gathered} \text { Pb } \\ \hline \end{gathered}$ | $\begin{array}{r} \mathbf{2 n} \\ \hline \boldsymbol{p} \boldsymbol{n} \end{array}$ | $\begin{aligned} & \text { prn } \\ & \text { pron } \end{aligned}$ | $\underset{\text { Mi }}{\mathrm{Mi}}$ | $\mathrm{Co}$ | $\begin{array}{r} \text { Mn } \\ \text { ppon } \end{array}$ |  | $\begin{array}{r} \text { AO } \\ \mathbf{p p} \\ \hline \end{array}$ | epm | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \text { Th } \\ \text { ppon } \end{gathered}$ | $\begin{gathered} \mathrm{Sr} \\ \text { ppen } \end{gathered}$ | pod | $\begin{gathered} \mathrm{sb} \\ \mathrm{pppm} \end{gathered}$ | $\begin{array}{r} 8 i \\ \text { ppon } \end{array}$ | $\mathrm{y}$ | $\begin{gathered} \mathrm{Cs} \\ \mathrm{X} \end{gathered}$ | $\frac{8}{2}$ | $\begin{array}{r} \text { Ls } \\ \text { ppre } \end{array}$ | $\mathrm{cr}$ | $\begin{array}{r} \mathrm{Hg} \\ \mathbf{I} \end{array}$ | Bran | $1$ | Bron | $\begin{array}{r} \text { Xl } \\ \mathbf{X} \end{array}$ | $\begin{aligned} & n_{\mathbf{n}} \\ & X \end{aligned}$ | $\dot{z}$ | gon | $\begin{aligned} & \text { Af } \\ & \text { ppob } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1464E 460＋50\％ | 1 | 56 | 7 | 52 | ， 3 | 33 | 10 | 519 | 2.04 | 13 | 5 | WD | 2 | 23 | ． 3 | 2 | 2 | 29 | ． 18 | \％ 633 | 9 | 19 | ． 26 | 193 | ＋88 |  | 3.49 | ． 02 | ． 85 | ＋ | 36 |
|  | 1 | 56 | 11 | 60 | $\xrightarrow{+1}$ | 28 | 10 | 581 | 2.01 | 188 | 5 | ND | 2 | 13 | 4 | 2 | 2 | 31 | .12 | T88 | 6 | 23 | ． 31 | 155 | 45： |  | 2.86 | ． 81 | ． 04 | 1 | 28 |
| LG6ME $460+00 \mathrm{M}$ | 1 | 46 | 13 | 48 | $\checkmark$ | 21 | 8 | 539 | 1．56 | 111 | 5 | ND | 1 | 11 | $\bigcirc 4$ | 2 | 2 | 27 | ． 92 | ． 077 | 6 | 16 | ． 23 | 94 |  |  | 2.16 | ． 22 | ． 05 |  | 15 |
| LS64E 450＊75\％ | 9 | 26 | 8 | 64 | \％ 2 | 21 | 10 | 540 | 1.82 | 12 | 5 | ND | 1 | 17 | \＆ | 2 | 2 | 29 | .17 | －0\％ | 5 | 18 | ． 23 | 140 | 44 |  | 2.20 | ． 01 | ． 05 |  | 4 |
| L464E 459＋50\％ | 1 | 60 | 13 | 68 | －2 | 29 | 11 | 453 | 2.21 | 21： | 5 | W0 | 2 | 14 | \％ 2 | 2 | 2 | 35 | ． 13 | ， 16 | 7 | 24 | .36 | 144 | －15： |  | 2.89 | .01 | ． 0 |  | 8 |
| 1409545923 | 1 | 65 | 12 | 63 | ． 3 | 29 | 12 | 373 | 2.17 | 20 | 5 | W | 2 | 15 | \％ | 2 | 2 | 35 | ． 15 | 108 | 7 | 26 | ． 38 | 203 | － 14 |  | 2.45 | ． 01 | ． 05 | ＋ | 63 |
| L464E 45 | 1 | 65 | 4 | 6 | 3 | 39 | 13 | 446 | 2.47 | 2f | 5 | N0 | 2 | 22 | 2 | 2 | 2 | 40 | ． 23 | \％ 0 | 8 | 30 | ． 49 | 497 | ．14 |  | 2.34 | ． 01 | ． 06 |  | 69 |
| L464E 459＋75 | 4 | 65 | 20 | 64 | $\stackrel{3}{3}$ | 22 | 10 | 1142 | 1．78 | 18 | 5 | NO | 2 | 21 | ＋ | 2 | 2 | 29 | ． 22 | $\cdots 8$ | 8 | 17 | ． 26 | 188 | 16 |  | 2.56 | ． 01 | ． 06 |  | 43 |
| CH6tE 458＋50m | 1 | 34 | 10 | 52 | $\stackrel{1}{1}$ | 22 | 7 | 651 | 1.94 | 14 | 5 | ND | 1 | 11 | \％ | 2 | 3 | 34 | ． 14 | 313 | 6 | 21 | ． 32 | 117 | 15 |  | 1.95 | ． 02 | 65 | 2 | 21 |
| 1469E 458＋25\％ | 1 | 58 | 16 | 54 | － 2 | 26 | 10 | 789 | 2.06 | 16 | 5 | ND | 2 | 12 | ． 3 | 3 | 2 | 34 | ． 15 | 8692． | 7 | 24 | ． 37 | 129 | 5 |  | 2.35 | ． 01 | 4 |  | 2 |
| LCAE 4 | 1 | 50 | 10 | 68 | $\checkmark 1$ | 29 | 11 | 1092 | 2.27 | ． 18 | 5 | W0 | 2 | 14 | $\cdots$ | 2 | 2 | 34 | ． 15 | ＋23 | 6 | 21 | ． 31 | 235 | ． 36 |  | 2.64 | ． 01 | ． 05 |  | 25 |
| L665E 466400N | 1 | 47 | 10 | 102 | 3 | 26 | 8 | 709 | 1.87 | 184 | 5 | N8 | 2 | 20 | ＋5 | 2 | 2 | 28 | ． 17 | ，004 | 5 | 14 | ． 19 | 166 | .20 |  | 4.12 | ． 02 | ． 04 |  | 3 |
| L465E 465－75M | 1 | 26 | 8 | 52 | N | 12 | 7 | 324 | 1.43 | 13 | 5 | ND | 1 | 12 | $\stackrel{3}{3}$ | 2 | 2 | 23 | ． 12 | cos | 3 | 11 | ． 10 | 66 | ＋17 |  | 2.82 | ．01 | 3 |  | 14 |
| 1465E 465＊50m | 1 | 65 | 21 | 55 | \％t | 17 | 8 | 529 | 1.40 | 15. | 5 | W0 | 1 | 15 | $T$ | 2 | 2 | 25 | ． 15 | 0］\％ | 3 | 11 | － 38 | 119 | ${ }_{4}^{4}$ |  | 2.07 | ． 08 | ． 35 |  | 49 |
| 1465E 465＋25M | 1 | 276 | 12 | 52 | ． 3 | 27 | 14 | 458 | 2.44 | 21 | 5 | MD | 2 | 17 | ＊ 6 | 2 | 2 | 36 | ． 23 | \％0\％ | 9 | 25 | －38 | 11 | ．\％ |  | 2.07 | ． 01 | ． 05 |  |  |
| E | 1 | 88 | 9 | 56 | \％ 5 | 25 | 12 | 381 | 2.21 | 19 | 5 | WD | 2 | 13 | $\stackrel{8}{6}$ | 2 | 2 | 36 | ． 14 | 31303 | 7 | 19 | ． 27 | 127 | 17 |  | 3.24 | ． 01 | ． 65 |  | 9 |
| L465E 4 | 1 | 182 | 14 | 55 | － 4 | 39 | 13 | 252 | 2.90 | 29 | 5 | ND | 4 | 16 | 2 | 2 | 2 | 50 | ． 26 | 008 | 16 | 42 | ． 67 | 81 | 4 |  | 9 | ． 09 | ． 05 |  | 45 |
| L465E 464＋50 | 3 | 498 | 11 | 54 | 10 | 48 | 17 | 285 | 4.84 | 44 | 5 | ND | 3 | 19 | 2 | 3 | 2 | 62 | ． 47 | \％ 850 | 17 | 61 | ． 98 | 8 | ， 3 |  | 1.93 | －08 | ．06 |  | 290 |
| 1465E 466＋25w | 1 | 36 | 8 | 69 | ＋2 | 20 | 8 | 246 | 1.70 | 42 | 5 | WD | 1 | 14 | $\pm$ | 2 | 2 | 28 | ． 11 | ＊／3 | 5 | 11 | ． 15 | 110 | ${ }_{6} 8$ |  | 2.19 | －02 | ． 05 |  | 7 |
| 1465E 464000M | 1 | 18 | 7 | 72 | ， 2 | 16 | 7 | 383 | 1.51 |  | 5 | ND | 2 | 16 | ． 5 | 2 | 2 | 25 | ． 16 | ＊ $1 \times 9$ | 4 | 10 | ． 15 | 14 | ． 7 \％ |  | 2.35 | ． 01 | ． 5 |  |  |
| 1465843 | 1 | 129 | 19 | 53 | \％ 5 | 51 | 11 | 361 | 2.33 | 17 | 5 | WD | 3 | 20 | ，2 | 2 | 4 | 16 | ． 24 | 0 O3 | 13 | 28 | ． 37 | 169 | $\stackrel{17}{17}$ |  | 3.11 | ． 02 | ． 86 |  | 9 |
| L465E 463＋50w | 1 | 66 | 12 | 55 | 2 2 | 34 | 10 | 457 | i．93 | 建 | 5 | W | 2 | 15 | ， 4 | 2 | 2 | 32 | ． 17 | 660 | 6 | 19 | ． 27 | 164 | ${ }_{6} 17$ |  | 2.68 | ． 02 | ． 05 |  | 4 |
| L465E 463＋25x | 1 | 59 | 14 | 54 | －2 | 52 | 10 | 360 | 2.09 | 19 | 5 | WD | 2 | 12 | ． 3 | 2 | 2 | 32 | ．15 | 3349 | 12 | 21 | ． 27 | 206 | ． 19 |  | 2.02 | ． 02 | ． 06 |  | 4 |
| L485E 463＋00N | 1 | 80 | 22 | 71 | 8 | 31 | 11 | 592 | 1.95 | 37. | 5 | W0 | 2 | 24 | 3 | 2 | 2 | 43 | ． 29 | \％ 048 | 12 | 30 | ． 36 | 118 | ， 22 |  | 4.86 | ． 02 | ．86 |  | 5 |
| 1465E 462＋750 | 1 | 272 | 20 | 66 | $9$ | 81 | 13 | 572 | 3.01 | 35. | 5 | W ${ }^{\text {d }}$ | 3 | 18 |  | 2 | 2 | 4 | ． 26 | \％ | 18 | 30 | ． 36 | 118 | ＋22 |  | 4.0 | ． 02 | 0 |  |  |
| 1465E 462＋56m | 1 | 98 | 6 | 38 | \％ 3 | 42 | 12 | 355 | 2.14 | 53 | 5 | W0 | 2 | 13 | \％ 5 | 2 | 2 | 32 | ． 16 | 35 | 6 | 17 | ． 21 | 96 | －27 |  | 3.7 | ． 02 | ．04 |  | 1 |
| L465E 462＋25M | 1 | 64 | 8 | 38 | $\rightarrow 2$ | 25 | 10 | 252 | 2.02 | 24. | 5 | No | 3 | 16 | \％ 3 | 2 | 2 | 30 | ． 17 | 267 | 8 | 18 | ． 27 | 104 | 9 |  |  | 2 | ． 15 |  | 5 |
| $1465{ }^{\text {c }} 482+00 \mathrm{~cm}$ | 1 | 50 | 14 | 45 | \％ 6 | 23 | 11 | 326 | 1.89 | － 15 | 5 | ND | 2 | 12 | $\stackrel{5}{5}$ | 2 | 2 | 30 | ． 12 |  | 8 |  | ． 24 | 111 |  |  |  | 1 | 0 |  | 340 |
| 1465t 463＋75M | 1 | 35 | 6 | 64 | 2 | 23 | 9 | 477 | 1.95 | 14 | 5 | ND | ， | 0 | $\pm 2$ | ， |  | 33 | ＋ | 193 | 5 | 19 | 27 | 145 |  |  | 2.24 | ． 81 | ． 03 |  | 56 |
| L665E 461＋50m | 1 | 28 | 4 | 68 | － | 20 | 9 | 1043 | 1.89 | 22 | 5 | w | 1 | 10 | －s | 2 | 2 | 32 | ．${ }^{3}$ | 495 | 5 | 19 | ＋27 | 14 |  |  |  |  |  |  |  |
|  |  |  | 21 | 52 | \％ | 33 | 12 | 600 | 1.85 | 17 | 5 | no | 1 | 19 | ， 2 | 2 | 3 | 31 | ． 24 | ＜ 0 |  | 20 | ． 26 | 199 | ＋14： |  | 2.02 | ． 02 | 5 |  | 4 |
|  | 1 | 36 | 8 | 60 | ¢ 6 | 24 | 8 | 889 | 1.75 | 16 | 5 | WD | ， | 19 | ， 2 | 2 | 3 | 30 | ． 19 | TEA | 6 | 20 | ． 27 | 198 | ＋6： |  | 2.24 | ． 01 | ． 65 |  | 17 |
| （465E 460＋75\％ | 1 | 28 | 11 | 76 | 区 | 23 | 10 | 9484 | 1.83 | \％ 8 | 5 | ND | 1 | 14 | ，${ }^{3}$ | 2 | 2 | 28 | ． 15 |  | 6 | 19 | ． 28 | 277 | ． 4 |  | 2.19 | －01 | ） |  | 370 |
| 1465E 460450m | 1 | 52 | 2 | 23 | 84 | 11 | 27 | 511 | ． 69 | \％ | 5 | M0 | 1 | 11 | ＋2 | 2 | 2 | 21 | ． 14 | ＊ | 14 | 4 | 0 | 56 |  |  |  | 02 | \％ |  | 40 |
| 1465E 460－25M | 1 | 55 | 8 | 50 | $\pm$ | 31 | 10 | 424 | 1.97 |  | 5 | Hid | 2 | 10 | ＋ | 2 | 2 | 33 | ． 14 | \％ | 8 | 24 | ． 35 | 9 | \％ |  |  | ． 01 | ． |  |  |
| L45E 460400\％ |  | 28 | 18 | 68 | ， | 32 | 10 | 49 | 1.84 | 15 | 5 |  | 1 | 22 |  | 2 | 2 | 30 | ． 22 | ¢07． | 5 | 16 | ． 24 | 137 | 418 |  | 2.57 | ． 02 | ． 05 | 2 | 1 |
| Stampano C／Mj－S | 18 | 57 | 38 | 131 | \％ 0 | 67 | 30 | 1049 | 3.93 | ， 4 4 | 17 | 6 | 37 | 47 | 相， 6 | 15 | 22 | 58 | ． 51 | 860\％ | 37 | 55 | ． 89 | 174 | T0 | 36 | 1．90 | ． 0 | ． 13 | ${ }_{2}$ | 0 |


| SAMPIE | $\begin{gathered} \text { mo } \\ \text { ppm } \end{gathered}$ | Cu | $\begin{array}{r} \text { pb } \\ \text { ppon } \end{array}$ | In | ppon | $\begin{aligned} & \text { Non } \\ & \text { pron } \end{aligned}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppon } \end{array}$ | Fe | pppm | $\begin{array}{r} \mathrm{U} \\ \text { pprin } \\ \hline \end{array}$ | $\begin{array}{r} \text { hu } \\ \text { ppom } \end{array}$ | $\begin{gathered} \text { Th } \\ \text { pprf } \end{gathered}$ | $\begin{gathered} \mathbf{S r} \\ \text { prom } \end{gathered}$ | $\begin{gathered} \text { td } \\ \text { pomim } \end{gathered}$ | sb | $\begin{gathered} \quad \mathbf{B} \\ \text { Ppm } \end{gathered}$ | $\begin{array}{r} \mathrm{V} \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{8} \end{gathered}$ | $+\mathbf{P}$ | Lat | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppr} \end{gathered}$ | $\begin{gathered} \mathrm{Hg} \\ \mathrm{x} \end{gathered}$ | $\mathrm{Be}$ | 1 1 | P4\％ |  | $\underset{\mathbf{x}}{\mathrm{K}}$ | $\begin{aligned} & \mathbf{K} \\ & \mathbf{Z} \end{aligned}$ | $\underset{\mathbf{p o n}}{\mathbf{N}}$ | Apt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 2 | 301 | 2 | 66 | 2 | 65 | 49 | 238 | 3.13 | 22 | 5 | ND | 4 | 20 | ＊3 | 2 | 2 | 4 | .21 | ¢034 | 12 | 34 | ． 48 | 294 | 17 |  | 3.05 | ． 02 | ． 05 | 2 | 34 |
| L466E 465＋75M $14665465+504$ | 2 | 391 35 | 14 | 66 | 1 | 20 | 9 | 301 | 1．86 | 10 | 5 | W3 | 1 | 12 | ＋ 3 | 2 | 3 | 31 | .15 | 809 |  | 16 | ． 24 | 104 | 17 |  | 2.03 | ． 02 | ． 04 | ＋ | 18 |
| L466E 465＋50M cti6e $465+25 \%$ |  | 35 | 14 | 71 | $\xrightarrow{1}$ | 28 | 12 | 619 | 2.27 | 13 | 5 | W\％ | 1 | 15 | －2 | 2 | 2 | 36 | ． 18 | Stex | 6 | 22 | ． 27 | 184 | － 6 |  | 2.71 | ． 02 | ． 05 | ＋ | 19 |
| L6E0k 465 |  | 33 | 8 | 63 | 3 | 24 | 11 | 554 | 2.00 | 15 | 5 | 10 | 2 | 46 | ${ }^{2}$ | 2 | 2 | 31 | ． 27 | 458 | 6 | 16 | ． 24 | 115 | 4 |  | 3.00 | ． 02 | ． 05 |  | 13 |
|  | 4 | 43 | 5 | 57 | 4 | 32 | 11 | 271 | 2.25 | 19 | 5 | ND | 2 | 75 | $\checkmark 2$ | 2 | 2 | 36 | ． 2 | \％61： | 7 | 22 | ． 30 | 120 | 新： |  | 2.64 | 2 | ． 05 | － | 14 |
|  |  | 49 | 5 | 63 |  | 33 | 10 | 208 | 2.20 | 15 | 5 | N0 | 2 | 15 | 3 | 2 | 2 | 4 | ． 22 | 3060： | 7 | 48 | ． 27 | 111 | $\otimes 19$ |  | 3.27 | ． 02 | ． 65 |  | 34 |
| L46E 464＋50M | 1 | 6 | 7 | 51 | 3 | 47 | 12 | 231 | 2.71 | 22 | 5 | ND | 2 | 20 | $\pm 2$ | 2 | 2 | 39 | ． 35 | 5034 | 11 | 26 | ． 39 | 138 | －10 |  | 3.25 | ． 02 | ． 05 | $t$ | 42 |
| LCESE 464 LSAE 461 |  | 148 | 12 | 71 | 7 | 78 | 13 | 448 | 3.06 | 32 | 5 | N0 | 3 | 23 | －2 | 2 | 2 | 40 | ． 36 | 0065 | 12 | 29 | ． 39 | 180 | －22 |  | 4.47 | ． 03 | ． 06 |  | 35 |
| L46EE 463＋75N | ， | 65 | 6 | 61 | 5 | 45 | 11 | 183 | 2.46 | 17 | 5 | ND | 2 | 19 | $\stackrel{8}{6}$ | 2 | 3 | 36 | ． 36 | \％06 | 7 | 25 | ． 32 | 113 | 19 |  | 3.69 | .02 | ． 05 |  | 12 |
| L460E 463＋50N | 1 | ${ }_{*} 68$ | 15 | 65 | 5 | 76 | 12 | 374 | 2.97 | 29 | 5 | MD | 2 | 18 | ． 2 | 2 | 2 | 37 | ． 30 | 8046： | 12 | 30 | ． 33 | 149 | ． 41 |  | 7 | 2 | ．06 |  | 13 |
| Lest 4 | 1 | 3 | 16 | 75 | 6 | 42 | 10 | 513 | 2.02 | 16 | 5 | 10 | 2 | 18 | $\stackrel{2}{2}$ | 2 | 2 | 30 | ． 22 | tte | 13 | 17 | ． 22 | 152 | 边 |  | 3.67 | ． 03 | ． 06 |  | 11 |
| 1460t 463 | 1 | 59 | 12 | 74 | 4 | 41 | 12 | 909 | 2.22 | 17 | 5 | N0 | 2 | 19 | ． 4 | 2 | 3 | 37 | ． 31 | 859 | 8 | 27 | ． 40 | 180 | ．66 |  | 2.33 | ． 02 | ． 06 |  | 14 |
| L466E $462+75 M$ | 1 | 44 | 3 | 103 | 12 | 28 | 12 | 636 | 2.12 | 15 | 5 | H0 | 1 | 26 | 5 | 2 | 2 | 35 | ． 26 | ¢133 | 8 | 20 | ． 27 | 209 | 17 |  | 5 | .02 | 06 |  | 53 |
| L46SE 462＋50\％ | 1 | 44 | B | 62 | 3 | 43 | 11 | 439 | 2.99 | 17 | 5 | W0 | 2 | 24 | 3 | 2 | 2 | 35 | ． 27 | D71 | 8 | 4 | 3 | 1 | － |  | 8 | 2 | 0 |  | 22 |
| LG66E 462＋254 | 1 | 28 | 8 | 63 | 2 | 26 | 9 | 720 | \＄．81 | 21 | 5 | N0 | 2 | 27 | 3 ： | 2 | 2 | 29 | ＋ 18 | ， 23 | 6 | 4 | ． 20 |  |  |  |  |  |  |  |  |
|  |  |  | 0 | 57 | 2 | 25 | 9 | 732 | 1.84 | 12 | 5 | mo | 2 | 20 | ＋4 | 2 | 3 | 30 | ． 99 | ． 491 | 5 | 43 | ． 19 | 110 | ＋20 |  | ． 34 | ． 02 | ． 03 | \％ | 5 |
| SE 461 |  | 41 | 5 | 75 | 2 | 29 | 11 | 045 | 2.17 | 13 | 5 | N0 | 2 | 21 | ¢ 4 | 2 | 2 | 37 | ． 27 | 118 | 7 | 23 | ． 31 | 189 | 17 |  | 3.05 | ． 02 | ． 15 |  | 12 |
| L466E 481＋50m |  | 165 | 15 | 62 | $\cdots 7$ | 27 | 11 | 566 | 2.55 | 19 | 5 | mo | 3 | 14 | －5 | 2 | 2 | 30 | .16 | \％104 | 7 | 20 | ． 27 | 159 | 23 |  | 4.43 | ．02 | ＋65 |  | 20 |
| L466E 461＋25＊ | 1 | 96 | 4 | 55 | 2 | 35 | 15 | 492 | 2.35 | 19 | 5 | 10 | 3 | 21 | ＋2 | 2 | 2 | 37 | －21 | 4609 | 11 | 27 | ． 36 | 152 | 4 |  | 3.38 | ． 02 | .05 |  | 30 |
| LCB6E 461＋60\％ | 1 | 29 | 10 | 77 | 3 | 22 | 11 | 1526 | 1.70 | 12 | 5 | 10 | 1 | 24 | 2 | 2 | 2 | 28 | .22 | \％181 | 6 | 17 | 4 | 18 | ． 4 |  |  |  |  |  |  |
|  |  | 50 |  | 52 | 2 | 22 | 10 | 552 | 1.81 | 19 | 5 | W0 | 1 | 15 | $t$ | 2 | 5 | 30 | ． 16 | 120 | 7 | 16 | ． 23 | 441 | ＋16 |  | 2.99 | ． 02 | ． 04 |  | 30 |
| LSE6E 460＋50m |  | 64 | 17 | 56 | 3 | 33 | 13 | 737 | 2.14 | 14 | 5 | N0 | 2 | 17 | 2 | 2 | 2 | 36 | ． 16 | WF2 | 8 | 24 | －33 | 445 | 17 |  | 2．88 | 02 | 15 |  | 40 |
| Letice 460＋25 | 1 | 31 | 0 | 56 | ¢ | 31 | 12 | 626 | 2.16 | 14 | 5 | MD | 2 | 24 | 4 | 2 | 3 | 35 | ． 23 | 105. | 6 | 22 | 2 | 25 |  |  |  | 2 | ． 15 |  | 73 |
| LIE6E 460＋60\％ | 1 | 28 | 10 | 61 | 2 | 20 | 9 | 808 | 1.77 | 15 | 5 | Mip | 1 | 34 | － 3 | 2 | 3 | 27 | 7 | 219 | 3 | 16 |  | 88 |  |  | $2.0 \%$ | ． 02 | ． 04 |  | 3 |
| L467E 46\％＋50M | 1 | 15 | 15 | 71 |  | 12 | 8 | 1236 | 1.68 | 14 | 5 | MD | 2 | 14 | 3 | 2 | 2 | 20 | － 16 |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | 7 | 109 | ＊2 | 29 | 12 | 1032 | 2.40 | 26 | 5 | WD | 1 | 19 | \％ | 2 | 2 | 38 | ． 28 | 434 | 5 | 19 | ． 27 | 170 | ＊ |  | ． 30 | ． 82 | 0 |  | 2 |
| L6TR |  | 438 | 2 | 59 | 1．1 | 57 | 11 | 873 | 2.04 | 50） | 5 | ND | 2 | 23 | ＋ | 2 | 2 | 31 | ． 67 | ＋461 | 45 | 22 | ． 25 | 60 | 椪 |  | 3.00 | ． 13 | ． 015 |  | 6 |
| L467E 487475＊ | 1 | 42 | 12 | 69 | －2 | 18 | 8 | 385 | 1.71 | 12 | 5 | D | 2 | 13 | ＋ 4 | 2 | 2 | 25 | ． 25 | \％ 81 | 7 | 14 | ． 17 | 2 | 7. |  |  | －02 | ． 64 |  | 2 |
| L467E 6674S0m | 1 | 75 | 12 | 58 | $\stackrel{+}{3}$ | 25 | 12 | 411 | 2.33 | 22 | 5 | WD | 2 | 16 | 3 |  | 2 | 37 | ． 29 | 8077： | 8 | 22 | － 3 | 61 |  |  |  | ． 01 | ． 4 |  | 350 |
| L467E 467＋254 | 1 | 369 | 2 | 47 | ＋4 | 61 | 28 | 309 | 4．7！ | 52 | 5 | m | 3 | 16 | ${ }_{4}^{4}$ | 2 | 2 | 57 | ． 43 | 185 | 16 | 52 |  |  |  |  |  |  |  |  |  |
|  |  | 51 | 2 | 93 | 2 | 33 | 12 | 232 | 2.62 | 25 | 5 | mb | 2 | 15 | ， 4.4 | 2 | 4 | 4 | ． 18 | \％000 | 5 | 19 | ． 27 | 4 |  |  | ． 04 | ． 02 | ． 05 |  | 50 |
|  |  | 29 | 11 | 77 | 5 | 21 | 8 | 584 | 1．88 | 23 | 5 | mo |  | 21 | ， 2 | 2 | 2 | 50 | ． 18 | 00. | 5 | 10 | ． 15 | 127 57 | 02 |  | 4．00 | ． 02 | －04 | $\bigcirc$ | 60 |
| L467E 466＋50M |  | 149 |  | 44 | S | 40 | 11 | 201 | 2.14 | 19 | 5 | N0 | 2 | 24 | ， 8 |  | 4 | 27 | ． 55 | \％02\％ | 43 | 18 | ． 25 | 157 |  |  | 3.14 | ． 105 | ． 08 |  | 1010 |
| L46TE 466＋259 |  | 378 | 17 | 74 | 8 | 83 | 45 | 423 | 3.42 | 42 | 5 | 虽 | 3 | 26 |  | 2 | 4 | 43 | ． 8.8 | ＋184 | 1 | 9 | ． 15 | 99 | 4 |  | 4.75 | ． 03 | ．04 | \％． | 18 |
| L467E 465＋50m |  | 37 | 15 | 80 | .5 | 18 | 18 | 674 | 2.00 | 23 | 5 | 10 | 3 | 16 |  | 2 | 2 | 3 | － 17 |  | 5 | 7 | － | 9 |  |  |  |  |  | \％， |  |
|  |  | 43 |  | 74 | － 1 | 25 | 13 | 314 | 2.37 | 16 | 5 | 数 | 2 | 16 | \％ 6 | 2 | 2 | 57 | ． 15 | 10 | 6 | 19 | ． 24 | ¢ | 24 |  |  | ．02 | 5 |  | 10 |
| sTminep $t$ | 17 | 53 | 36 | 129 | 8.6 | 60 | 30 | 1041 | 3.92 | 6 | 19 | 6 | 37 | 47 | 783 | 16 | 27 | 57 | ． 51 | S | 30 | 53 | ． 90 | 17 | －10） | 3 | 1．＊ | ． 6 | － 13 |  | 52 |



Attwood Gold corp．PROJEET GOLDEN CROWN FILE \＃90－1341

| SAMPLES | No | tu | $\underset{p}{\text { Pb }}$ | $\begin{array}{r} \mathbf{Z n} \\ \text { ppm } \end{array}$ |  | $\underset{\mathrm{mi}}{\mathrm{Mi}}$ | Co | $\underset{p m n}{p m}$ | $\begin{gathered} \text { Fe } \\ X \end{gathered}$ | R | $\underset{\text { ppm }}{\mathrm{U}}$ | $\underset{\text { Mpm }}{\mathbf{H U N}}$ | $\begin{array}{r} \text { Ith } \\ \text { pppan } \end{array}$ | $\begin{array}{r} \mathbf{S r} \\ \text { ppm } \end{array}$ | $\mathrm{Cd}$ | $\begin{array}{r} \mathbf{S b} \\ \text { ppm } \end{array}$ | $\underset{\mathrm{Bi}}{\mathrm{Bi}}$ | $\begin{array}{r} \mathbf{Y} \\ \text { pram } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{x} \end{gathered}$ | $\frac{8}{2}$ | 18 | $\begin{gathered} \mathrm{Cr} \\ \mathrm{prpm} \end{gathered}$ | $\frac{\operatorname{mg}}{x}$ | $\begin{array}{r} 88 \\ \text { ppow } \end{array}$ | K1 | B | $\mathbf{A l}$ | $\begin{gathered} \text { Ms } \\ \mathbf{y} \end{gathered}$ | $2$ |  | $\begin{aligned} & \mathrm{Aln} \\ & \mathrm{pob} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L4808 465－23\％ | 1 | 35 | 12 | 82 | \％ | 21 | 9 | 527 | 1．9＊ | 13 | 5 | mo | 2 | 15 | 8 | 2 | 2 | 29 | ． 18 | －0\％3 | 4 | 14 | ． 19 | 93 | $\bigcirc 19$ |  | 3.2 | ． 02 | ． 0 |  | 5 |
| L468E 465＋00m | 1 | 43 | 13 | 58 | 3 | 29 | 12 | 400 | 1.96 | 46 | 5 | N0 | 7 | 26 | 2 | 2 | 2 | 30 | ． 31 | ¢ 152 | 5 | 18 | 25 | 170 | 16 |  | 2.49 | ． 02 | ．06 | 9 |  |
| L468E 464＊75 | 1 | 148 | 10 | 60 | 44 | 39 | 15 | 301 | 2.70 | 30 | 5 | M0 | 2 | 22 | 2 | 3 | 2 | 44 | ． 37 | －1040 | 10 | 38 | ． 62 | 96 | ， 13 | 2 | 1.88 | ． 01 | ．06 | 1 |  |
| L460e 464＋50 | 1 | 39 | 12 | 84 | 3 | 26 | 12 | 622 | 2.09 | 19 | 5 | N0 | ＊ | 13 | $\boldsymbol{\theta}$ | 2 | 2 | 33 | ． 17 | 122 | 5 | 21 | 27 | 113 | 16 |  | 2.50 | ． 01 | ． 05 | $\stackrel{1}{8}$ |  |
| L460E 464 +25 m | 1 | 28 | 11 | 55 | \％ | 27 | 10 | 590 | 2.08 | 16 | 5 | 10 | \＄ | 14 | 3 | 2 | 2 | 34 | ． 68 | 460 | 4 | 19 | ． 24 | 112 | t1： |  | 2.90 | ． 01 | ． 15 |  |  |
| L4605 44400．1 | 1 | 82 | 5 | 46 | 3 | 25 | 4 | 336 | 1.11 | 5 | 5 | 㠶 | ＋ | 10 | 2 | 2 | 3 | 23 | ． 45 | \％36 | 10 | 14 | ． 19 | 46 | 819 |  | 1.19 | ． 02 | ． 05 | 1 | 1 |
| L46tE 463＋75M | 1 | 434 | 8 | 53 | －2 | 79 | 30 | 551 | 4.76 | 32 | 5 | M0 | ＊ | 16 | 2 | 2 | 3 | 63 | ． 36 | \％036： | 12 | 111 | 1.61 | 79 | $\underline{2}$ | 2 | 2.38 | ． 01 | ． 13 | 1 | 2 |
| L460E 463－501 | 1 | 78 | 11 | 47 | 1 | 40 | 44 | 195 | 2.60 | 19 | 5 | ND | 2 | 15 | ＋2 | 2 | 2 | 46 | ． 27 | － 211 | 10 | 41 | ． 64 | 77 | \＄2 |  | 1．60 | .01 | ． 16 | \％ 1 | $t$ |
| （4602 463＋254 | 1 | 24 | 12 | 56 | $\times 3$ | 20 | 8 | 712 | 1.74 | 11 | 5 | W0 | 1 | 13 | 2 | 2 | 2 | 28 | ． 14 | \％hts | 4 | 16 | ． 18 | 119 | 17 |  | 3.23 | ． 01 | 13 | 1 | 1 |
| L468E 463＋00M | 1 | 42 | 9 | 58 | －1 | 20 | 11 | 616 | 2.06 | 20 | 5 | 10 | 1 | 17 | 2\％ | 2 | 2 | 34 | ． 21 | 179 | 5 | 25 | 33 | 139 | ${ }^{35}$ |  |  | .01 | ． 04 |  | 5 |
| L460x 463＋73N | 1 | 25 | 5 | 56 | $\checkmark 1$ | 16 | 9 | 275 | 1.74 | 8 | 5 | W0 | 1 | 7 | ．3 | 3 | 2 | $2{ }^{6}$ | ． 08 | 167 | 5 | 17 | ． 19 | 122 | ts |  | 2.24 | ． 01 | ． 13 | T | 13 |
| L460x 462＋50 | 1 | 32 | 9 | 39 | 2 | 22 | 9 | 475 | 1.67 | 11 | 5 | N0 | 1 | 10 | －2 | 2 | 3 | 29 | ． 11 | $-10$ | 4 | 20 | ． 26 | 107 | 14 | 2 | 1.95 | ． 01 | ． 05 | 1 | 21 |
| 1460E 462＋25M | 1 | 35 | 9 | 46 | 2 | 31 | 11 | 501 | 1.99 | 14 | 5 | N0 | 2 | 14 | 3 | 2 | 5 | 33 | ． 15 | fags | 5 | 21 | ． 27 | 164 | 17 | 2 | 2.75 | .01 | ． 04 |  | 37 |
| L460E 462＋00m | 1 | 4 | 5 | 30 | 2 | 26 | 10 | 575 | 1.86 | 15 |  | 40 | 2 | 17 | 2 | 2 |  | 31 | ． 15 | 00 | 7 | 19 | ． 23 | 190 |  |  | 3.07 | ．02 | ． 5 |  | 7 |
| L468E 461＋75M | 1 | 55 | 8 | 60 | －3 | 29 | 10 | 550 | 1.91 | $\mathbf{2 t}$ | 5 | H | 1 | 17 | 2 | 2 | 2 | 32 | ． 20 | \％990 | 8 | 24 | ． 35 | 145 | 3 |  | 2.15 | ． 01 | ． 65 |  | 1 |
| Li60E 461＋50m | 1 | 61 | 14 | 62 | ＋4． | 35 | 10 | 401 | 1.99 | 11 | 5 | H0 | 2 | 15 | 2 | 2 | 2 | 32 | ． 14 | 5068 | 8 | 25 | ． 33 | 163 | 15 |  | 2.37 | ． 01 | ． 65 |  | 22 |
| L46er 461＋25M | 1 | 41 | 9 | 50 | 1 | 29 | 10 | 465 | 1.86 | 17 | 5 | H0 | 2 | 13 | $\triangle$ |  |  | 31 | ． 14 | \％18 | 6 | 23 | ． 30 | $10 \dagger$ | 35 |  | 2.41 | ． 01 | ． 14 |  | 15 |
| 14608 461＋00N | 1 | 46 | ＊ | 58 | －3 | 31 | 10 | 576 | 2.15 | 17 | 5 | wo | 2 | 17 | $\checkmark$ | 2 | 2 | 34 | ． 18 | 099 | 8 | 26 | ． 35 | 475 | 16 | 2 | 2.55 | ． 01 | ． 05 |  | 6 |
| L468E 460＋751 | 1 | 50 | 18 | 52 | 2 | 31 | 17 | 617 | 1.94 | 18： | 5 | W0 | 1 | 18 | 2 | 2 | 2 | 53 | ． 20 | 60 | 7 | 27 | .35 | 147 | 3 |  |  | 01 | 0. |  |  |
| L468E 460－50m | 1 | 33 | 12 | 65 | .2 | 25 | 10 | 777 | 1.61 | 13 | 5 | N0 | 2 | 25 | － 4 | 2 | 2 | 26 | ． 24 | 2 OH | 6 | 16 | ． 19 | 967 |  |  |  | 2 |  |  |  |
| L46EE 460＋23M | 1 | 52 | 13 | 44 | 2 | 29 | 14 | 603 | 2.02 | 18 | 5 | N0 | 2 | 25 | 2 | 2 | 2 | 31 | ． 22 | 104 | 10 | 21 | ． 31 | 187 | T1 |  | 3.15 | ． 62 | ．06 | 2 | 9 |
| L460E 460＋00m | 1 | 71 | 12 | 50 | 4 | 28 | 12 | 307 | 2.08 | 13 | 5 | mp | 3 | 15 | $\bigcirc 3$ | 2 | 2 | 33 | ． 16 | 077 | 8 | 22 | ． 33 | 158 | 67 |  | 2.99 | ＋01 | 05 |  | 2 |
| 14654 459＋75M | 1 | 36 | 7 | 54 | ＋1 | 15 | 11 | 943 | 1.63 | \％ 6 | 5 | ND | 1 | 13 | －2 | 2 | 2 | 30 | ． 16 | 056 | 5 | 14 | ． 22 | 172 | 3 |  |  | ． 02 | 4 |  | 19 |
| L4ESE 499＋50m | 1 | 66 | 9 | 47 | 1 1． | 25 | 12 | 544 | 2.01 | ¢5 | 5 | m | 1 | 20 | ＋2 | 2 | 2 | 34 | ． 24 | 8107 | 6 | 23 | ． 35 | 435 | ＋14 |  | 2.31 | ． 01 | ． 04 |  | 11 |
| 4689 468＋50\％ | 1 | 48 | 11 | 47 | 1 | 18 | 9 | 507 | 1.75 | $14$ | 5 | ND | 1 | 17 | $\mathrm{i}$ | 2 | 2 | 32 | ． 21 | 104＊ | 6 | 20 | ． 26 | 121 | 2 |  | f．47 | ． 01 | ． 04 |  |  |
| Sit 46e－2in | 1 | 43 | 8 | 48 | 1 | 18 | 9 | 757 | 1.76 | 11. | 5 | N0 | 1 | 20 | ， 2 | 2 | 2 | 31 | ． 22 | ＜05 | 6 | 18 | 30 | 132 | －t5 |  | 2.44 | ． 02 | ． 06 |  | 12 |
|  | 1 | 30 | 11 | 64 | 3 | 22 | E | 492 | 1.81 | 16 | 5 | mo | 1 | 18 | $\bigcirc 3$ | 2 |  | 30 | ． 21 | 150 | 5 | 48 | ． 26 | 129 | ct |  |  | ． 01 | ． 15 |  | 15 |
| Li69E 467＋754 | 1 | 44 | 10 | 66 | 2 | 19 | 8 | 322 | 1.92 | 14 | 5 | 10 | 1 | 11 | －2 | 2 | 3 | 32 | .97 | 101 | 4 | 17 | ． 24 | 95 | \％6 |  | 2.42 | ． 01 | ． 04 |  | 16 |
| L469E 467＋25M | 1 | 72 | 13 | 72 | $\underline{2}$ | 27 | 10 | 350 | 2.15 | 15 | 5 | 0 | 2 | 16 | \％2 | 2 | 3 | 35 | ． 19 | 0／5 | 6 | 18 | ． 29 | ＋17 | － 18 |  | 3.42 | －02 | ． 04 |  | 5 |
| L460E 467＋05m | 1 | 111 | B | 71 | 6 | 30 | 14 | 522 | 2.23 | 22 | 5 | 0 | 1 | 21 | $2$ | 2 | 2 | 36 | ． 23 | 8070 | 6 | 20 | ． 33 | 130 | ＋17 |  | 2.94 | ． 02 | .05 | 业 |  |
| ＋e 4ictisim | 1 | 189 | 11 | 48 | 4 | 27 | 11 | 304 | 2.38 | 19 | 5 | 0 | 2 | 33 | ． 2 | 2 | 4 | 36 | ． 14 | \％060 | 5 | 19 | .28 | 104 | \％t\％ |  | ． 75 | ． 01 | ． 04 | 2 | 25 |
| 9e 466＋5911 | 4 | 133 | 8 | 49 | 1 | 39 | 14 | 413 | 2.02 | 16 | 5 | W0 | 2 | 12 | －2 | 2 | 2 | 46 | ． 18 | 069 | 7 | 29 | ． 47 | 134 | 86 |  | 2.60 | 01 | ． 05 | ＋ | 32 |
| L469E 466－25m | 1 | 106 | B | 65 | 1 | 28 | 14 | 767 | 2.30 | 16 | 5 | no | 1 | $\$ 2$ | ． 2 | 2 | 2 | 38 | ． 15 | 109 | 6 | 26 | ． 41 | 157 | 楼 |  | 2.12 | 0 | ． 04 |  | 33 |
| LISAE Lection | － | 0 | 17 | 53 | 2 | 24 | 12 | 613 | 2.11 | 19 | 5 | W | 2 | 45 | 2 | 2 | 2 | 32 | ． 15 | 101 | － | 18 | ． 26 | 115 | 17 |  |  | 02 | ． 04 |  | 1 |
| L469E 465＋75M | 1 | 109 | 14 | 7 | 4 | 32 | 14 | 240 | 2.58 | 19 | 5 | WD | 2 | 46 | －2 | 2 | 3 | 40 | ． 26 | \％031 | 0 | 25 | ． 37 | 115 |  |  |  | 1 | － |  |  |
| 14492 485＋50m | 1 | 276 | 47 | 72 | 4 | 40 | 17 | 436 | 2.79 | 49 | 5 | m | 1 | 49 | 2 | 2 | 3 | 39 | ． 32 | 8070 | 0 | 20 | ． 45 | 5 | $\stackrel{1}{4}$ |  | 2.20 | ． 01 | ． 05 |  | 30 |
| STAMPA的 C／mu－s | 18 | 57 | 40 | 120 | 7，2 | 70 | 30 | 1051 | 3.74 | 38 | 17 | 7 | 37 | 48 | 䨐1 | 15 | 22 | 56 | ． 50 | \％ 09 | 37 | 55 | ． 89 | 174 | 帾 | 32 | 1.05 | ． 0 | ． 13 | ＋1 | 51 |


| 54mple | Mo | Cu | $\begin{gathered} \mathrm{Pb} \\ \mathrm{pp} \end{gathered}$ | $\begin{array}{r} 2 n \\ p p m \end{array}$ | $\begin{aligned} & \text { Ag } \\ & \text { pqun } \end{aligned}$ | $\begin{array}{r} \mathrm{Mi} \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { pppm } \end{array}$ | Mn Fe <br> Ppm  | $\mathrm{pm}$ | $\mathrm{J}$ | Au | $\begin{array}{r} \text { Th } \\ \text { perm } \end{array}$ | $\begin{gathered} \text { Sp } \\ \text { ppon } \end{gathered}$ | cred | $\begin{array}{r} \mathbf{5 b} \\ \mathbf{p p o n} \end{array}$ | $\begin{gathered} \text { 日í } \\ \text { Pom } \end{gathered}$ | $\begin{gathered} \mathrm{V} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Ca } \\ \mathbf{x} \end{gathered}$ | $\begin{array}{r} 8 \\ \$ 4 \end{array}$ | $\begin{gathered} \mathrm{Li} \\ \mathrm{pmom} \end{gathered}$ | $\mathrm{Cr}$ |  | $\begin{array}{r} \text { 8i } \\ \text { ppm } \end{array}$ | $\frac{11}{1}$ | $B$ A！ <br> 7  | $\mathbf{X a}$ |  | y |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14698 465＋25 | 1 | 676 | 17 | 53 | ＊ 6 | 49 | 23 | 4023.57 | 33 | 5 | 10 | 2 | 22 | 2 | 2 | 7 | 50 | ． 52 | 如 4 | 14 | 44 | ． 77 | 7 | 94 | 21.55 | ． 02 | ． 06 | 2 | 66 |
| L469\％464＋75 | 1 | 484 | 30 | 60 | 8 | 70 | 18 | 3733.10 | 33 | 5 | W | 2 | 15 | 2 | 2 | 2 | 46 | ． 23 | 6074 | 9 | 43 | ． 69 | 9 | tt | 32.05 | ． 02 | ． 05 | 1 | 2 |
| L469E 464＋50m | $t$ | 74 | 14 | 66 | 4 | 29 | 11 | 4142.16 | 19 | 5 | 10 | 2 | 95 | ＋4 | 2 | 3 | 35 | ． 17 | 4074 | 0 | 23 | ． 30 | 132 | 18 | 33.33 | ． 02 | ． 05 |  | 10 |
| 1469t 444－25N | 1 | 139 | 24 | 80 | E | 50 | 13 | 5772.51 | 50 | 5 | N0 | 2 | 21 | － 8 | 2 | 3 | 41 | ． 30 | 101 | 10 | 36 | 53 | 183 | 5 | 2.74 | d2 | 08 |  | 3 |
| L469E 404400m | 1 | 105 | ＋5 | 96 | \％ | 42 | 14 | 5982.34 | 18 | 5 | N0 | 2 | 21 | c | 2 | 2 | 38 | ． 24 | ＋145 | 0 | 20 | 38 | 178 | 16 | 3.10 | 2 | ． 07 |  | 20 |
| L465：463＋734 | 1 | 15 | 12 | 100 | 3 | 35 | 10 | 5032.02 | 16. | 5 | ND | 1 | 11 | 2 | 2 | 2 | 34 | ． 12 | 1\％\％ | 6 | 25 | ． 29 | 117 | ． 6 | 32.62 | ． 02 | ． 05 | $1$ | 5 |
| （460E 463＋50m | 1 | 67 | 45 | 106 | 3 | 44 | 12 | 4902.30 | 16. | 5 | ND | 1 | 20 | ＜2 | 2 | 2 | 37 | ． 23 | \％013 | 6 | 27 | ． 35 | 154 | 17 | 23.17 | 0.0 | ． 06 |  | 26 |
| L460E 463＋25N | 1 | 51 | 4 | 72 | 4 | 30 | 10 | 2972.00 | 26 | 5 | ND | 1 | 11 | 32 | 2 | 2 | 40 | ＋ 15 | 063 | 6 | 30 | ． 40 | 84 | 12 | 21.59 | ． 12 | ． 05 |  | 9 |
| L669E 463＋00m | 1 | 17 | ${ }^{\text {B }}$ | 75 | 1 | 13 | 7 | 6821.20 | 4 | 5 | ND | 7 | 22 | 5 | 2 | 2 | 20 | ． 15 | 194 | 6 | 41 | ． 11 | 230 | 48 | 41.43 | － 02 | ．03 |  | 5 |
| L469E 462＋751 | 1 | 29 | 9 | 74 | 6 | 29 | 9 | 5301.70 | 16 | 5 | ND | 2 | 17 | 4 | 2 | 2 | 29 | ． 13 | 33 | 6 | 16 | ． 19 | 155 | 96： | 42.62 | ． 62 | ．04 |  |  |
| 1640 462＋50m | 1 | 22 | 19 | 75 | 84 | 22 | 9 | 6911.60 | 12 | 5 | ND | 2 | 25 | 2 | 2 | 2 | 26 | ． 29 | 2210 | 5 | 13 | ． 16 | 158 | ＊ 7 | 52.73 | ． 02 | ． 15 |  | 2 |
| T469E 462＋25 | 1 | 19 | 9 | 78 | 1 | 16 | 9 | 007 1.55 | 10 | 5 | ND | 1 | 24 | 2 | 2 | 2 | 23 | ． 29 | 203 | 4 | 15 | .17 | 210 | 83 | 41.81 | 12 | ． 08 |  | 7 |
| 1469E 462＋00m | 1 | 2 | 2 | 92 | 2 | 28 | 12 | 7331.85 | 12 | 5 | ND | 1 | 18 | 3 | 2 | 2 | 30 | ．部 | 4159 | 6 | 21 | ． 25 | 158． | 14 |  | ． 02 | ． 05 |  |  |
| ［669E 461＋75 | 1 | 30 | 6 | 79 | 2 | 27 | 17 | 6479.93 | 9 | 5 | N0 | 2 | 19 | 2 | 2 | 2 | 32 | ． 20 | 8100 | 8 | 26 | ． 33 | 165 | 13 | 51.54 | ． 02 | ． 05 |  | 1 |
| L669E 461425＊ | 1 | 43 | 11 | 74 |  | 39 | 14 | 3381.91 | 15 | 5 | M | 2 | 14 |  | 2 | 2 | 30 | ． 13 | 156 | 6 | 17 | ． 22 | 130 | ¢18： | 3.30 | 2 | 15 |  |  |
| L685 460＋75 | 1 | 32 | 11 | 69 | 3 | 38 | 9 | 6151.8 | 13 | 5 | mo | 2 | 19 | $\underline{1}$ | 2 | 2 | 29 | ． 20 | $\stackrel{1}{4} 57$ | 6 | 20 | ． 27 | 168 | 15 | 22.69 | ． 0 | ． 05 | 1 | 47 |
| L649E 460＋50m | 1 | 34 | 9 | 66 | 1 | 25 | 9 | 7521.85 | 16 | 5 | ND | 2 | 24 | 6 | 2 | 2 | 29 | ． 18 | 5t29 | 7 | 18. | ． 26 | 192 | 16 | 33.04 | ． 02 | ． 05 | 1 | 70 |
| L669E 460＋25： | 1 | 46 | 9 | 68 | .2 | 32 | 11 | 11032.13 | 14 | 5 | W0 | 2 | 22 | 2 | 2 | 2 | 34 | ． 26 | 3122 | 10 | 26 | ． 37 | 254 | 15 | 52.80 | ．02 | ． 0. |  |  |
| L669E 460＋601 | 1 | 51 | 12 | 72 | 2 | 39 | 13 | 6162.20 | 75 | 5 | 40 | 3 | 16 | 3 |  | 2 | 35 | ． 17 | 117 | 10 | 24 | ． 35 | 19 | 17 | 3．17 | 2 | ．06 |  | 2 |
| L469E 459＋75M | 1 | 41 | 10 | 53 | 2 | 32 | 13 | 5722.12 | 15 | 5 | ND | 2 | 19 | －4 | 2 | 2 | 34 | ＋19 | －135 | 8 | 21 | ． 28 | 120 | 8： | 23.17 | ． 02 | ．06 |  |  |
| L469E 499040m | 1 | 62 | 9 | 62 |  | 38 | 15 | 6842.42 | 20 | 5 | ND | 2 | 20 | ． 2 | 2 | 2 | 39 | ． 23 | 006\％ | 10 | 32 | ． 46 | 257 | 15 | 42.00 | －02 | ．06 |  | 1 |
| L670E 460－50m | 1 | 50 | 14 | 59 | ． 5 | 22 | 9 | 4362.12 | 18 | 5 | WD | 3 | 25 | 12 | 2 | 2 | 34 | ． 23 | 140 | 12 | 21 | ． 53 | 152 | 18 | 23.5 | ． 02 | ．06 |  | 1 |
| L470E 460425M | ， | 43 | 11 | 59 | 4 | 21 | 10 | 6292.01 | 16 | 5 | ND | 2 | 24 | 86 | 2 | 3 | 31 | ． 25 | ．114 | 6 | 15 | ． 23 | 144 | 14 | 3.84 | ． 02 | ．064 |  | 7 |
| 1470E 460000 | 1 | 152 | 95 | 69 | 1.0 | 28 | 13 | 5782.40 | 29 | 5 | ND | 3 | 23 | 3 | 2 | 2 | 35 | ． 54 | 006 | 21 | 22 | ． 32 | 1 | 21 |  | 3 | ． 04 |  | 15 |
| 6470E 467＊75 | I | 71 | 9 | 65 | 5 | 17 | 10 | 3552.01 | 20 | 5 | ND | 3 | 14 | 3 | 2 | 2 | 32 | ． 13 | 15 | 8 | 13 | ． 1 | 1 | －21． |  | ． 62 |  | : |  |
| L470E 467＋501 | 1 | 58 | 9 | 68 | 6 | 23 | 14 | 10532.08 | 20 | 5 | NO | 2 | 14 | 4 | 2 | 2 | 34 | ． 16 | \％42 | 6 | 16 | ． 22 | 171 | 地 | 23.29 | ． $0^{2}$ | ． 04 |  | 16 |
| L4TOE 467420 | 4 | 104 | 11 | 48 | ． 3 | 23 | 13 | 4162.46 | 23 | 5 | ND | 3 | 18 | 4 | 3 | 2 | 38 | ． 20 | ．072 |  | 20 | ． 33 | 156 | 18 | 43.86 | ． 02 | 04 |  | 11 |
| L4TUE 467400w | － | 167 | 7 | 57 | 1 | 23 | 14 | 5022.61 | 21 | 5 | ND | 3 | 17 | 3 | 2 | 2 | 39 | ． 20 | 8078 | 12 | 21 | ． 35 | 140 | 16 |  | 12 | 04 |  | ， |
| L470e 466＋75H | \＄ | 319 | 11 | 47 | 2 | 29 | 16 | 3314.12 | 33 | 5 | 10 | 3 | 10 | 6 | 2 | 2 | 64 | ． 15 | \％065 | 9 | 35 | ． 66 | 403 | 44 | 5.3 | －01 | ＊ |  | 29 |
| 44TEE 460450m | $\dagger$ | 140 | 10 | 50 |  | 30 | 76 | $4 \% 32.71$ | 77 | 5 | N0 | 3 | 13 | 4 | 2 | 2 | 43 | ． 17 | 8045 | 11 | 31 | ． 42 | 103 | ／9 | 53.20 | － 82 | ． 0 |  | 2 |
| 160＋20 | 1 | 456 | 6 | 51 | － | 32 | 16 | 2963.14 | 19 | 5 | 0 | 4 | 14 | 2 | 2 | 2 | 48 | ． 19 | \％ 61 | 12 | 31 | ． 34 | 76 | 20： | 23.58 | 0 | 05 | \％ | 4 |
| C4TOE 46SNOM | 1 | 403 | 8 | 59 | 2 | 26 | 13 | 3803.43 | 79 | 5 | no | 2 | 12 | 3 | 2 | 2 | 55 | ． 15 | －0＊＊ | B | 30 | ． 50 | 78 | 16. | 22.17 | ． 017 | ． 05 |  | 14 |
| 4470e 465＋75M | 1 | 482 | 9 | 75 | 4 | 31 | 16 | 4872.63 | 34 | 5 | W0 | 2 | 17 | 4 | 2 | 2 | 43 | ． 21 | 108 | 8 | 27 | ． 42 | 111 | \％6 | 32.66 | ． 02 | ． 05 |  | 54 |
| L47ve 465＋50N | 1 | 104 | 13 | 74 | 2 | 40 | 18 | 4242.50 | 37 | 5 | WD | 2 | 16 | 3 | 2 | 2 | 39 | ． 23 | \％ 88 | 8 | 25 | ． 34 | 108 | 18 | 3.15 | ． 02 | 5 |  | 5 |
| L470E 465－28M | 1 | 53 | b | 60 | 5 | 17 | 10 | 5311.85 | 19 | 5 | N0 | 2 | 14 | ＊ | 2 | 2 | $2{ }^{\text {c }}$ | ． 14 | \％ | D | 13 | \％${ }^{\text {F }}$ | 114 |  | 33.09 | 12 | ． 04 | $\cdots$ |  |
| 1470 4694003 | 1 | 142 | 13 | 57 | 3 | 40 | 13 | 3992.35 | 29 | 5 | Mo | 2 | 47 | 3 | 2 | 2 | 37 | ． 20 | \％054 | 0 | 30 | ．38 | 100 | 14 | 22.32 | ．02 | .05 |  | 0 |
|  | 17 | 58 | 44 | 129 | 6S | 60 | 30 | 10453.77 | 40 | 18 | 7 | 37 | 45 | 18， 1 | 15 | 19 | 57 | ． 50 | \％99 | 37 | 57 | ． 87 | 174 | 80 | 331.73 | ． 06 | .13 | 冓 | 50 |



Attwood Gold corp．PROJEtri GOLDEN CROWN FILE \＃90－1341

| SAMPLE＊ | $\begin{gathered} \text { Mo } \\ \text { per } \end{gathered}$ | $\mathrm{Cu}$ | Pb PPRT | $\begin{array}{r} 2 n \\ p r m \end{array}$ | Ag | $\underset{\mathrm{ppm}}{\mathrm{Ni}}$ | co | $\begin{array}{r} \text { Mn } \\ \text { pem } \end{array}$ |  | A8 pan | $\begin{array}{r} \mathrm{V} \\ \text { ppm } \end{array}$ | su | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | $\begin{gathered} \text { Sr } \\ \text { ppm } \end{gathered}$ | Id | $\begin{array}{r} \text { Sb } \\ \text { ppRn } \end{array}$ | $\begin{array}{r} 8 i \\ p p i n \end{array}$ | $\begin{array}{r} V \\ \text { ppm } \end{array}$ | $\mathbf{x}$ |  | Le | $\underset{\text { prom }}{\mathrm{Cr}}$ | $48$ | $\begin{gathered} \mathbf{8 n} \\ \hline 10 n \end{gathered}$ |  | $8$ | $\mathrm{A!}$ | Ne |  | $\begin{aligned} & \text { Atiot } \\ & \text { ppob } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1674E 464060 | 1 | 46 | 47 | 68 | ． 3 | 28 | 9 | 637 | 1.94 | 35 | 5 | ND | 2 | 17 | \％ 6 | 2 | 2 | 30 | ． 22 | 143 | 4 | 17 | ． 25 | 106 | ST |  | 3.25 | ． 01 | ． 04 | 7 |
| 2471E 463＋75\％ | － | 32 | 8 | 78 | 2 | 24 | 11 | 1091 | 1.87 | 100 | 5 | ND | 1 | 23 | $\stackrel{2}{2}$ | 2 | 2 | 28 | ． 16 | 327 | 4 | 16 | ． 22 | 215 | 45 |  | 2.68 | ． 01 | ． $84 \%$ \％ | 5 |
| L471E 463＋50\％ | 1 | 18 | 12 | 51 | 1 | 16 | 7 | 457 | 1.40 | 30 | 5 | No | 1 | 24 | 8 | 2 | 2 | 22 | ． 23 | 203 | 3 | 11 | .17 | 149 | \％ 5 |  | 1.65 | ． 02 | ． 05 \％ | 15 |
| L47TE 463－25＊ | 1 | 37 | 8 | 53 | $\leqslant$ | 24 | 9 | 812 | 1.57 | 313 | 5 | HD | 1 | 23 | 3 | 2 | 3 | 28 | ． 19 | \％103 | 6 | 17 | ． 26 | 174 | ． 3 |  | 1.74 | ． 01 | ． 65 | 33 |
| L6T9E 463＋00w | 1 | 52 | 12 | 50 | ， 2 | 33 | 11 | 699 | 1.98 | 18 | 5 | ND | 1 | 19 | 3 | 2 | 2 | 33 | ． 19 | 120： | 8 | 22 | ． 36 | 148 | 14 |  | 2.37 | .01 | ． $04 \%$ | 16 |
| 1479E 462＋751 | 1 | 36 | 5 | 54 | 2 | 27 | 9 | 705 | 1.76 | 18： | 5 | 10 | 2 | 17 | ． 5 | 2 | 2 | 30 | ． 19 | 1t8： | 6 | 21 | ． 32 | 154 | 12 |  | 1．0\％ | ． 01 | ． 05 | 11 |
| 1471E 462＋50\％ | 1 | 37 | 99 | 58 | 3 | 27 | 9 | 858 | 1.64 | 15 | 5 | ND | 1 | 23 | \％2 | 2 | 2 | 28 | ． 26 | 18 | 6 | 20 | ． 31 | 185 | ． 42 |  | 1.89 | ． 01 | ． 04 | 10 |
| L471E 462＋25in | 1 | 35 | 9 | 66 | 6 | 36 | 9 | 520 | 1.92 | 18 | 5 | ND | 1 | 23 | 4 | 2 | 2 | 30 | ． 25 | －127 | 6 | 21 | ． 34 | 184 | ＋ 14 |  | 2.37 | ． 21 | ． 65 | 3 |
| LG77E 462＋00m | 1 | 38 | 10 | 64 | 1 | 22 | 8 | 757 | 1.73 | 75 | 5 | N0 | 2 | 13 | 2 | 2 | 2 | 26 | ． 12 | \％ 14 | 7 | 18 | ． 23 | 164 | .9 |  | 3.08 | ． 01 | ． 05 | 14 |
| 467E 461＋730 | 1 | 30 | 6 | 61 | $\stackrel{5}{8}$ | 26 | 8 | 698 | 1.67 |  | 5 | ND | 1 | 22 | $\bigcirc 2$ | 2 | 3 | 26 | ． 21 | \＄176 | 6 | 17 | ． 25 | 165 | .13 |  | 2.39 | .01 | ． 55 \％ 1 | 35 |
| 46 | 1 | 4 | 9 | 63 | －3 | 22 | 9 | 189 | 90 | 45 | 5 | N0 | 2 | 27 | 2 | 2 | 2 | 32 | ． 27 | 4ts | 8 | 18 | ． 30 | 203 | $\stackrel{15}{ }$ |  | ． 35 | ． 91 | ． 06 | 47 |
| LCTIE 461＊25M | 1 | 53 | 7 | 65 | 3 | 32 | 10 | 599 | 1.99 | 1 A | 5 | N0 |  | 23 | 2 |  | 2 | 32 | ． 24 | 003 | 8 | 25 | ． 38 | 162 | － 13 |  | ． 12 | ． 01 | ． 67 | 41 |
| L4T7E 461000m | 9 | 64 | 9 | 45 | $\checkmark$ | 35 | 12 | 444 | 2.29 | ＋17 | 5 | ND | 2 | 14 | －2 |  | 2 | 36 | ． 17 | 065 | 9 | 31 | ． 47 | 127 | －${ }^{+1}$ | 2 | 2.25 | ． 01 | ． 05 | 42 |
| L671E 660－75M | 1 | 62 | 28 | 63 | 2 | 35 | 12 | 1048 | 2.29 | $\bigcirc 18$ | 5 | ND | ， | 25 | \％ 4 | 2 | 2 | 36 | ． 30 | ． 159 | 8 | 30 | ． 46 | 170 | ＋14 |  | ． 85 | ． 09 | ． 65 | 143 |
| L479E 460－50m | \％ | 85 | 12 | 47 | $\stackrel{2}{2}$ | 46 | 17 | 603 | 2.63 | ¢ 23 | 5 | ND | 1 | 21 | ． 2 | 2 | 2 | 40 | ． 28 | 063 | 11 | 37 | ． 61 | 143 | ． 89 | 3 | 1.76 | ． 01 | ． 06 | 32 |
| L479 460－\％ | ！ | 54 | 12 | 45 | $\stackrel{1}{1}$ | 32 | 19 | 498 | 1.84 | \％ 8 | 5 | W | 1 | 24 |  | 2 | 2 | 29 | ． 29 | 63 | 8 | 23 | ． 36 | 152 | $\times 10$ |  | ． 61 | ． 01 | ． 68 | 59 |
| 1471E 460＋00m | 1 | 71 | 13 | 39 | 2 | 35 | 13 | 49 | 2.21 | 20 | 5 | NO | 1 | 24 | ， 2 | 2 | 2 | 34 | ． 31 | 18039 | 8 | 27 | ． 45 | 123 | 10 |  | ． 61 | ． 01 | ． 06 | 37 |
| L671E 459＋75\％ | 1 | 56 | 16 | 52 | 1 | 30 | 14 | 802 | 2.03 | \％25 | 5 | ND | 1 | 30 | －4 | 2 | 2 | 33 | ． 35 | 8050 | 7 | 25 | ． 40 | 136 | ． 89 | 3 | 1.32 | － 51 | ． 55 | 49 |
| L471E 459＋56m | 1 | 66 | 5 | 53 | d | 32 | 13 | 759 | 2.10 | 46 | 5 | ND | 1 | 23 | ． 2 | 2 | 2 | 34 | ． 30 | 076 | 8 | 25 | ． 38 | 450 | ＋11 |  | 1.72 | ． 01 | ． 06 \％ | 40 |
| C672E 468000\％ | 1 | 51 | 10 | 49 | 1 | 19 | 9 | 726 | 1.74 | 12 | 5 | ND | 2 | 25 | ， 2 | 2 | 2 | 30 | ． 28 | N09\％ | 8 | 18 | ． 29 | 151 | \＄4 |  | 2.24 | ． 01 | ． $06 \leqslant$ \％ | 50 |
| 1672E 467475\％ |  | 64 | 10 | 50 | －1 | 20 | 11 | 862 | 1.82 | 11 | 5 | HD | 1 | 24 | 2 | 2 | 2 | 33 | ． 25 | ＋078 | 7 | 20 | ． 36 | 150 | 40 |  | 53 | .01 | ．04 | 31 |
| L47EE 467450m | ， | 53 | 9 | 48 | 1 | 20 | 10 | 677 | 1.76 | 13 | 5 | N0 | 1 | 21 | ，2 | 2 | 2 | 31 | ． 21 | 078 | 6 | 17 | ． 29 | 131 | ． 63 |  | 01 | ． 02 | ． 55 \％ 2 | 18 |
| L472E 467＋25\％ | 1 | 46 | 7 | 50 | 4 | 20 | 10 | 556 | 2.05 | 13 | 5 | No | 1 | 12 | ＋2 | 2 |  | 38 | ． 17 | 8072 | 5 | 23 | ． 38 | 79 | 11 |  | ，4t | ． 01 | ． $04 \geqslant \%$ | 9 |
| L4TZE 467400， |  | 64 | 7 | 37 | \％ | 19 | 9 | 538 | 1.75 | $\bigcirc$ | 5 | ${ }^{10}$ | 1 | 26 | ， 2 | 2 | 2 | 30 | ． 22 | －062 | 6 | 16 | ． 30 | 130 | 43 |  | 1.95 | ． 08 | ． $05 \% 1$ | 37 |
| L472E 466＋75 | － | 52 | 7 | 70 |  | 18 | 10 | 11751 | 1.69 |  | 5 | ND | ， | 22 | \％ | 2 | 3 | 28 | ． 20 | 166 | 7 | 45 | ． 23 | 206 | ． 45 |  | 2.25 | ． 02 | ． 66 \％ 1 |  |
| 1672E 46 | 1 |  | 10 |  |  |  | 13 | 5 | 35 | 2 | 5 | W0 | 4 | 93 | － 2 | 2 | 4 | 3 | ． 19 | 139\％ | 7 | 25 | ． 42 | 105 | ＋3 |  | 2.30 | ． 01 | ．04 | 29 |
| L472E 464－75\％ | 1 | 21 | 2 | 41 | 1 | 15 | 6 | 2031 | 1.08 | \％ 1 | 5 | ND | 1 | 8 | $\stackrel{2}{2}$ | 2 | 2 | 23 | ． 12 | \％653 | 2 | 18 | ． 23 | 58 | \％19 |  | ． 75 | ． 02 | ． 63 | 4 |
| 1472E 464450m | ， | 55 | 7 | 52 | ， 1 | 35 | 11 | 593 | 4.79 | 26 | 5 | ND | ， | 19 | $\overbrace{3}^{3}$ | 2 | 2 | 29 | ． 25 | 924 | 6 | 21 | .31 | 136 | 613 |  | 2.13 | ． 02 | ． 04 | 25 |
| 4672x 464－25M |  | 65 | 8 | 46 | 1 | 25 | 11 | 689 | 1.97 | 16 | 5 | ND | ， | 14 | $\bigcirc 2$ | 2 | 2 | 35 | ． 16 | 8099 |  | 24 | ． 40 | 93 | $\cdots$ | 5 | ． 89 | ． 01 | ． 06 | 45 |
| L472E 463＋75M | 1 | 32 | 7 | 63 |  | 24 | 10 | 8881 | 1.81 |  | 5 | ND | 1 | 29 | － 2 | 2 | 2 | 29 | ． 28 | ， 412 | 5 | 18 | ． 30 | 197 | $\times 17$ | 3 | 1.69 | ． 61 | ． 06 | 17 |
| L472e 46 | 1 | 22 | 8 |  |  |  | － | 817 | 1.34 |  | 5 | WD | 1 |  | $\stackrel{+}{2}$ | 2 | 2 | 23 | ． 23 | 89\％ | 4 | 12 | ． 20 | 161 | ＋13 |  | 51 | ． 01 | －65 \％\％ | 4 |
|  | 1 | 36 | 10 | 70 | 5 | 42 | 11 | 7491 | 1.83 | 14 | 5 | ND | 1 | 26 | －2 | 2 | 3 | 28 | ． 27 | 30\％ | 7 | 15 | ． 25 | 198 | \％ 4 |  | 2.27 | ． 02 | ． 06 \％苑 | 16 |
| 16724 43300m | 1 | 48 | 7 | 73 | 4 | 36 | 12 | 7901 | 1.87 | \％ 16 | 5 | ND | 1 | 33 | \％ 2 | 2 | 2 | 28 | ． 34 | 號 | 7 | 22 | ． 33 | 229 | ¢0 |  | 1.69 | ． 08 | ． 07 | 15 |
| L47CE 462＋73M | 1 | 68 | 10 | 49 | －2 2 | 40 | 12 | 4532 | 2.04 | $\bigcirc 17$ | 5 | ND | 1 | 22 | ＋ 2 | 2 | 3 | 33 | ． 27 | 矢类 | 9 | 26 | ． 44 | 137 | ＋12 |  | 1.86 | ． 01 |  | 68 |
| 1477E 462＋30w | 9 | 37 | 2 | 42 |  | 26 | 11 | 11592 | 2.05 |  | 5 | ND | 1 | 24 | \％2 | 2 | 2 | 37 | ． 27 |  | 8 | 27 | ． 44 | 154 | 819． | 4 | 1.28 | ． 01 | ． 07 \％納 ${ }^{\text {a }}$ | 29 |
| 1472E 462＋259 | 1 | 62 | 9 | 54 | \％2 | 37 | 12 | 5222 | 2.02 ： |  | 5 | N0 | 1 | 29 | $\checkmark 2$ | 2 | 2 | 33 | ． 23 | 48 | 9 | 25 | ． 40 | 176 | ． 13 |  | 2.26 | ． 01 | ． 05 \％ | 90 |
| STAngund C／me | 18 | 57 | 38 | 129 | 1．1 | 69 | 30 | 10373 | 3.73 | 38 | 17 | 7 | 37 | 48 | 16.3 | 15 | 24 | 56 | ． 69 |  | 36 | 53 | ． 87 | 174 | 彻 | 36 | 1.85 | ．06 | $.14 \%$ | 30 |


| SAMDEE | $\begin{array}{r} \text { Mo } \\ \mathrm{ppm} \end{array}$ | $\underset{\mathrm{prm}}{\mathrm{Cu}}$ | $\begin{array}{r} \text { Pb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} 2 n \\ p r m \end{array}$ | ng | $\underset{\text { pom }}{\mathrm{Mi}}$ | $\begin{aligned} & \text { Co } \\ & \text { pppin } \end{aligned}$ |  | $\begin{gathered} \mathrm{Fe} \\ \mathbf{y} \end{gathered}$ | 虭 ppon | $\frac{\mathrm{u}}{\mathrm{pan}}$ | Mu | Th ppm |  | Cd | $\begin{array}{r} \text { Sb } \\ \text { prom } \end{array}$ | $\begin{gathered} 8 i \\ \text { pern } \end{gathered}$ | $\begin{array}{r} \mathrm{V} \\ \hline \end{array}$ | $\begin{array}{r} \mathrm{C} \\ \mathbf{2} \end{array}$ | $\underset{X}{P}$ | $\begin{array}{r} \text { Le } \\ \text { ppm } \\ \hline \end{array}$ | $\begin{array}{r} \mathrm{Cr} \\ \mathrm{pem} \\ \hline \end{array}$ | $\begin{gathered} \mathrm{Hg} \\ \mathbf{x} \end{gathered}$ | $\begin{array}{r} \mathrm{Ee} \\ \mathrm{pprin} \\ \hline \end{array}$ | $\begin{aligned} \mathrm{F} \\ \hline \end{aligned}$ | $\begin{array}{r} \text { B } \\ \text { ppin } \\ \hline \end{array}$ | $\underset{\mathbf{X}}{\mathbf{A}}$ | $\begin{gathered} \text { Me } \\ \mathbf{y} \end{gathered}$ | $\mathbf{x}$ | pp | $\begin{aligned} & \text { ALP } \\ & \text { ppob } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1472E 462＋00m | 1 | 62 | 13 | 48 | 2 | 23 | 10 | 660 | 1．81 | 40 | 5 | ND | 2 | 20 | 5 | 2 | 2 | 31 | ． 24 | ． 070 | 11 | 19 | ＋31 | 137 | 16 | 2 | 2.65 | ． 02 | ． 05 | 1 | 16 |
| 1472E 461＋75N | 1 | 50 | 1 | 65 | 2 | 22 | 9 | 624 | 2.01 | 18 | 5 | $N 0$ | 2 | 16 | 5 | 2 | 2 | 35 | .17 | 162 | 8 | 21 | ． 33 | 167 | 16 | 3 | 2.50 | ． 02 | ． 06 | 1 | 15 |
| $14728461+50 \mathrm{~m}$ | 1 | 27 | 3 | 60 | 1 | 6 | 7 | 1467 | 1.02 | 7 | 5 | ND | 1 | 19 | ． 6 | 2 | 2 | 23 | .19 | － 048 | 3 | 7 | .11 | 194 | ． 98 | 2 | ． 67 | ． 02 | ． 04 | 1 | 5 |
| L472E 661＋25M | 1 | 49 | 10 | 67 | 2 | 29 | 11 | 1017 | 1.83 | 12 | 5 | W0 | 1 | 36 | 3 | 2 | 2 | 30 | ． 32 | 3骊 | 9 | 23 | ． 34 | 237 | t2 | 2 | 1.90 | ． 02 | ． 06 | 1 | 30 |
| L472E 461＋00m | 1 | 51 | 6 | 61 | 3 | 43 | 12 | 566 | 2.05 | 20 | 5 | ＊ 0 | 1 | 28 | 6 | 2 | 2 | 33 | ． 33 | 69 | 7 | 27 | ． 43 | 178 | ． 11 |  | 1.55 | ． 02 | ． 07 |  | H |
| 1472E $460+754$ | 1 | 7 | 9 | 50 | 3 | 47 | 16 | 391 | 2.57 | 29. | 5 | N0 | 2 | 22 | 5 | 2 | 2 | 40 | ． 32 | 3047 | 11 | 33 | ． 54 | \＄56 | 13 | 2 | 2.05 | ． 01 | ． 05 | 1 | 60 |
| L472E 460＋50m | 1 | 55 | 10 | 54 | ${ }^{2}$ | 49 | 15 | 593 | 2.39 | 18 | 5 | W0 | 2 | 22 | 4 | 2 | 2 | 37 | ． 30 | 644 | 11 | 28 | ． 44 | 175 | t3 | 4 | 2.00 | ． 02 | ． 06 | 2 | 71 |
| 4472E 460－25M | 1 | 64 | 12 | 51 | 2 | 47 | 16 | 743 | 2.30 | 16 | 5 | ND | 2 | 32 | 8 | 2 | 4 | 36 | ． 44 | －046 | 10 | 25 | ． 40 | 169 | $1{ }^{1} 4$ | 4 | 2.07 | ． 12 | ． 07 | 1 | 21 |
| $1472 E 460400 \mathrm{H}$ | 1 | 88 | 15 | 57 | 2 | 45 | 18 | 691 | 2.74 | 21 | 5 | H0 | 2 | 27 | － 6 | 2 | 3 | 44 | ． 39 | $\bigcirc 050$ | 12 | 34 | ． 54 | 145 | 16 | 3 | 2.17 | ． 01 | ． 06 | 1 | 59 |
| L472E 459475 | 1 | 105 | 12 | 54 | 1 | 55 | 16 | 464 | 2.64 | 16 | 5 | WD | 2 | 20 | 7 | 2 | 2 | 43 | ． 27 | \％601 | 13 | 28 | ． 48 | 85 | ．t7 |  | 3.04 | 1 | ． 06 | 1 | 4 |
| 14728459450 | 1 | 72 | 8 | 52 | 2 | 30 | 14 | 602 | 2.25 | 14 | 5 | W0 | 2 | 22 | 5 | 2 | 2 | 38 | ． 28 | D62 | 9 | 25 | ． 42 | 123 | ． 14 | 3 | 2.11 | ． 01 | ． 05 |  | 25 |
| L473E 468＋25M | 1 | 38 | 6 | 54 | 2 | 17 | 11 | 1043 | 1.73 | 13 | 5 | MD | 1 | 24 | 5 | 2 | 2 | 33 | ． 34 | 415 | 6 | 19 | ． 34 | 242 | 11 | 2 | 1.45 | ． 02 | ． 07 | 1 | 24 |
| L473E 488＋00w | 1 | 41 | 12 | 53 | 1 | 18 | 10 | 976 | 5．08 | 12 | 5 | ND | 2 | 24 | 7. | 2 | 3 | 33 | ． 37 | Y00 | 8 | 17 | ． 29 | 205 | TS | 4 | 2.25 | ． 02 | ． 07 | 2 | 8 |
| L473E 467＋75M | 1 | 90 | 11 | 65 | 2 | 25 | 14 | 556 | 2.48 | 17 | 5 | ND | 4 | 21 | 5 | 2 | 3 | 42 | ． 29 | ¢083 | 12 | 22 | ． 43 | 150 | t7 | 3 | 2.90 | 2 | 0 | 1 | 23 |
| L473E 467＋50N | 1 | 64 | 6 | 5 | －1 | 19 | 10 | 664 | 7.88 | $11:$ | 5 | HD | 1 | 17 | 5 | 2 | 3 | 36 | ． 25 | 046 | 7 | 18 | ． 33 | 148 | ＋4 |  | 1.85 | 2 | 6 |  | 6 |
| 1473E 667＋25M | 1 | 105 | 9 | 53 | 1 | 25 | 14 | 712 | 2.54 | 15 | 5 | MD | 1 | 17 | 5 | 2 | 2 | 44 | ． 23 | 1004 | 11 | 24 | ．48 | 107 | 15 | 2 | 2.66 | ． 01 | ． 05 |  | 24 |
| 1473E 467＋001 | 1 | 101 | 13 | 54 | 1 | 25 | 16 | 0.14 | 2.44 | 14 | 5 | WD | 1 | 27 | 5 | 2 | 2 | 42 | ． 40 | \＄045 | 10 | 26 | ． 46 | 130 | 15 | 2 | 2.48 | ． 01 | ． 07 |  | 1 |
| 1473E 466－25N | 1 | 128 | 9 | 67 | 3 | 31 | 20 | 581 | 3.06 | 26 | 5 | ND | 1 | 13 | ［5 | 2 | 2 | 48 | ． 22 | 177 | 12 | 33 | ． 5 | 58 | ． 10 |  | 3．6 | .01 | ． 05 |  | 5 |
| 1473E 460＋00m | 1 | 84 | 15 | 60 | 1 | 26 | 18 | 850 | 2.71 | 17 | 5 | ND | 1 | 22 | 5 | 2 | 5 | 46 | ． 32 | 015 | 10 | 25 | ． 46 | 0 | 7 |  | 2.61 | 01 | ．08 |  | 57 |
| L473E 465＋251 | 1 | 69 | 0 | 62 | ． 1 | 45 | 15 | 640 | 2.50 | 32 | 5 | N0 | 1 | 18 | 3 | 2 | 2 | 36 | ． 23 | －118 | 7 | 32 | ． 42 | 199 | 14． |  | 2.35 | ． 02 | ． 6 |  | 4 |
| L473E 464＊75： | 1 | 60 | 17 | 64 | 2 | 35 | 15 | 786 | 2.31 | 24 | 5 | 10 | 2 | 22 | 3 | 2 | 2 | 36 | ． 27 | 188 | 7 | 27 | ． 37 | 208 | 14 | 2 | 2.50 | ． 02 | ． 06 |  | 68 |
| L675E 464．50w | 1 | 64 | 1 | 57 | 1 | 25 | 13 | 650 | 2.04 | 17 | 5 | NO | 1 | 21 | 5 | 2 | 2 | 33 | ． 26 | \＄116 | 7 | 21 | ． 34 | 173 | 13 | 2 | 2.06 | ． 02 | ． 05 | 1 | 30 |
| 1473E 464＋2\％ | 1 | 98 | 8 | 54 | 2 | 34 | 17 | 734 | 2.60 | 23. | 5 | No | 2 | 28 | 2 | 2 | 3 | 40 | ． 33 | ＋695 | 1 | 28 | ． 46 | 187 | 17 | 3 | 2.85 | ． 02 | ． 07 |  | 300 |
| L473E 466＋00\％ | 1 | 76 | 8 | 62 | 1 | 26 | 14 | 828 | 2.11 | 24 | 5 | N0 | 2 | 26 | 7 | 2 | 2 | 53 | ． 31 | 125 | 10 | 23 | ． 39 | 201 | 13 |  | 2.37 | 2 | ． 07 |  | 30 |
| 1473E 464－73M | 1 | 55 | 10 | 78 | －1 | 27 | 12 | 776 | 1.91 | 19 | 5 | NO | 1 | 44 | 3 | 2 | 2 | 34 | ． 46 | 144 | 9 | 23 | ． 37 | 238 |  |  | 1.95 | ． 02 | ． 0 |  | 47 |
| L673E 4634．50m | I | 68 | 10 | 53 | .1 | 25 | 15 | 817 | 2.14 | 27 | 5 | No | 1 | 31 | 6．7 | 2 | 2 | $4 \%$ | ． 36 | ＋085 | 8 | 23 | ． 39 | 160 | 12 | 2 | 1.65 | 02 | ．06 |  | 22 |
| 1673E 463－75 | 1 | 67 | 27 | 75 | －1 | 26 | 15 | 1970 | 2.00 | 24 | 5 | ND | 1 | 24 | 1.0 | 2 | 3 | 40 | ． 28 | 111 |  | 25 | ． 41 | 148 | ， 10 | 3 | 1.55 | ． 02 | ． 05 | 3 | 22 |
| L473E 463＋00m | 1 | 52 | 14 | 69 | 2 | 31 | 14 | 976 | 1.99 | 17. | 5 | 10 | 1 | 32 | 6 | 2 | 2 | 34 | ． 41 | 15 | 6 | 27 | ． 40 | 15 | 10 | 2 | 1.53 | 2 | ．06 |  | 22 |
| 1673E 462＋751 | 1 | 58 | 9 | 53 | 1 | 38 | 12 | 801 | 1.86 | 22 | 5 | 10 | ， | 23 | \％ 6 | 2 | 2 | 33 | ． 29 | \％007 | 6 | 24 | ． 31 | 156 | 10 |  | 1.29 | 2 | ． 07 | 1 | 77 |
| L473E 462450m | 1 | 46 | 8 | 58 | 2 | 32 | 11 | 55 | 1.92 | 14. | 5 | 10 | 1 | 35 |  | 2 | 2 | 32 | ． 33 | \％DP2 | 9 | 21 | ． 31 | 185 | ． 14 |  | 2.14 | ． 42 | ． 07 |  | 20 |
| 1473 462＋23M | 1 | 58 | 9 | 56 | 2 | 32 | 11 | 776 | 1.95 | 20 | 5 | 10 | 1 | 26 | \％ | 3 | 3 | 32 | ． 30 | ＋130 | 10 | 21 | ． 34 | 169 | 14 |  | 2.45 | ． 02 | ． 07 |  | 16 |
| 447E 462＋00\％ | ， | 105 | 15 | 57 | ${ }_{-3}$ | 92 | 18 | 603 | 2.72 | 33 | 5 | Wo | 2 | 20 | 6 | 2 | 2 | 4 | ． 2 t | 8092 | 11 | 46 | ． 65 | 173 | 15 | 2 | 2.59 | ． 01 | ． 06 |  | 6 |
| 4473E 469＋75 | 1 | 57 | 31 | 83 | 2 | 35 | 12 | 831 | 2.02 | 22 | 5 | ND | 1 | 32 | 1.4 | 3 | 2 | 33 | ． 37 | 8109 | 8 | 26 | ． 40 | 202 | ＋11 | 3 | 1.82 | ． 02 | ． 0 |  | 5 |
| L673E 461＋50m | 1 | 54 | B | 65 | 2 | 30 | 12 | 757 | 1.92 | 15 | 5 | ND | 1 | 28 | 8 | 2 | 2 | 52 | ． 26 | 135 | 9 | 26 | ． 36 | 173 | ＋12 | 2 | $\%$ | 2 | 6 |  | 3 |
| 1473E 461＋00m | 1 | 55 | 12 | 49 | 1 | 33 | 12 | 688 | 2.14 | 23 | 5 | W | 1 | 16 | 6 | 2 | 2 | 36 | ． 25 | \％069 | 0 | 28 | ． 4 | 13 | 1 |  |  | 01 | ． 6 |  | 19 |
| L473E 460－754 |  | 64 | 7 | 63 | 2 | 33 | 14 | 631 | 2.26 | 22 | 5 | N0 | 1 | 20 | 0 | 2 | 2 | 39 | ． 30 | \％ 077 | 0 | 29 | ． 45 | 116 | 13 | 2 | 2.05 | ． 01 | ． 05 | 1 | 6 |
| STAmpate craj－s | 10 | 58 | 37 | 129 | 6.7 | 67 | 30 | 1046 | 3.81 | 31. | 17 | 7 | 37 | 48 | 18.3 | 16 | 23 | 57 | ． 51 | ， 0 戈 | 37 | 55 | ． 88 | 174 | $\bigcirc \mathrm{OC}$ | 34 | 1.91 | ． 06 | ． 13 | 2 | 50 |


| SAMPLE* | $\begin{gathered} \text { Ho } \\ \text { pron } \end{gathered}$ | cu | $\underset{\mathrm{pb}}{\mathrm{~Pb}}$ | $\begin{array}{r} \text { In } \\ 90 \cdot n \end{array}$ | pomg | $\underset{\text { pomi }}{\mathrm{Ni}}$ | $\begin{array}{r} \mathrm{CO} \\ \mathrm{PRP} \end{array}$ | $\underset{p p m}{\mathrm{mpm}}$ | $\begin{array}{r} \mathrm{Fe} \\ \mathbf{y} \end{array}$ | $\begin{gathered} \text { AB } \\ \text { ppon } \end{gathered}$ | $\begin{array}{r} \mathrm{U} \\ \text { pom } \end{array}$ | $\begin{array}{r} \mathbf{A d} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { porin } \end{array}$ | $\begin{gathered} \mathbf{5 r} \\ \mathbf{p p r i n} \end{gathered}$ | C <br> pp | $\begin{array}{r} \mathbf{S b} \\ \mathbf{p p r} \end{array}$ | $\begin{array}{r} \text { Bi } \\ \text { ppon } \end{array}$ | $\begin{array}{r} \mathrm{V} \\ \text { pan } \end{array}$ | $\mathrm{Cz}$ | $\frac{1}{2}$ | $\begin{gathered} \text { Ln } \\ \text { Pprin } \end{gathered}$ | $\underset{\mathrm{pr}}{\mathrm{Cr}}$ | $\begin{gathered} \mathrm{Mg} \\ \mathrm{x} \end{gathered}$ | Bep | $\frac{T}{1 / 4}$ | $\stackrel{8}{\mathrm{pg}}$ | $\stackrel{A!}{\mathbf{X}}$ | $\begin{gathered} \mathrm{Ma} \\ \mathrm{Z} \end{gathered}$ | $\mathbf{z}$ |  | $\begin{aligned} & \text { Al } \\ & \text { peb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1475 460450/ | 1 | 56 | 10 | 56 | 1 | 29 | 13 | 1052 | 2.18 | 1 | 5 | ND | 1 | 25 | +2 | 2 | 2 | 40 | . 32 | \%063 | 7 | 23 | . 40 | 132 | 4t | 3 | 1.90 | . 02 | . 07 | 1 | 410 |
| 1473E $460+59 \mathrm{~m}$ | 1 | 77 | 13 | 49 | 1 | 35 | 15 | 827 | 2.42 | 18 | 5 | ND | 2 | 18 | +2 | 2 | 5 | 42 | .25 | $\bigcirc 052$ | 8 | 31 | . 49 | 102 | . 14 | 2 | 1.98 | . 92 | . 05 | 2 | 020 |
| 1475 +66+50N | 9 | 99 | 14 | 67 | 2 | 31 | 16 | 1088 | 2.62 | 26 | 5 | MD | 1 | 28 | 5 | 2 | 5 | 44 | . 67 | 077 | 13 | 34 | . 57 | 139 | 12 |  | 2.26 | 1 | . 08 | d | 56 |
| 1474E 468+25N | 1 | 39 | 12 | 43 | -1. | 17 | 9 | 981 | 1.61 | 15 | 5 | WD | 1 | 21 | 2 | 2 | 2 | 29 | . 19 | \%082 | 8 | 17 | . 25 | 189 | 4 | 2 |  | .03 | - 01 |  | 6 |
| L474E 460+00M | 1 | 102 | 10 | 50 | 1 | 30 | 14 | 451 | 2.71 | 18 | 5 | N0 | 3 | 12 | 3 | 2 | 3 | 45 | .17 | \% 839 | 11 | 32 | . 50 | 9 | -17 |  |  | . 01 |  |  |  |
| 1474E 467*754 | \$ | 101 | B | 57 | 1 | 26 | 14 | 578 | 2.50 | 18 | 5 | M1 | 1 | 11 | 2: | 2 | 5 | 43 | . 18 | c74: | 12 | 27 | . 48 | 80 | 17 | 13 | 2.59 | . 01 | . 05 | 1 | 72 |
| L474E 46745 DM | \% | 105 | 7 | 53 | 1 | 25 | 14 | 702 | 2.30 | 25 | 5 | 嗗 | 1 | 23 | 5 | 2 | 4 | 40 | . 40 | 053 | 10 | 28 | . 51 | 102 | . 42 | 3 | 1.95 | . 02 | . 05 | 1 | 0 |
| L674E 467400\% | 9 | 76 | 11 | 70 | 1 | 22 | 16 | 1251 | 1.73 | 18: | 5 | *D | 1 | 23 | ¢ | 2 | 2 | 34 | . 43 | ,06 | 7 | 24 | .37 | 149 | dis. |  | 1.34 | . 02 | 06 | 1 | 3 |
| L474E 486+75M | 1 | 96 | 2 | 68 | 1 | 27 | 14 | 780 | 2.36 | 21 | 5 | N0 | 1 | 31 | 4 | 2 | 2 | 42 | -41 | H80 | 12 | 30 | . 50 | 165 | -15 |  | 2.11 | .02 | . 07 |  | 4 |
| 4474E 466+00M | 1 | 92 | 10 | 52 | 4 | 28 | 17 | 621 | 2.53 | 534 | 5 | WD | 2 | 22 | 3 | 2 | 4 | 40 | . 26 | CO42 | 9 | 28 | . 43 | 141 | -16. |  | 2.46 | . 02 | . 06 |  | 124 |
| 1474 40 | 1 | 38 | 11 | 63 |  | 14 | 9 | 952 | 1.58 | 25 | 5 | 的 | 1 | 25 | 4 | 2 | 2 | 31 | . 26 | O56 | 5 | 14 | . 23 | 175 | 12 | 2 | 1.48 | . 02 | . 04 |  | 5 |
| L47E 463+79 474E 46-50H | \% | 92 | 5 | 57 | $\times 2$ | 29 | 14 | 518 | 2.28 | 63 | 5 | MD | 2 | 45 | -2 | 2 | 3 | 36 | . 26 | \%63 | 14 | 25 | . 39 | 64 | 18 |  | 2.86 | . 02 | . 05 | 1 | 1 |
| L474E 465+25m | 9 | 97 | 12 | 54 | 1 | 51 | 14 | 427 | 2.64 | 41 | 5 | WD | 3 | 16 | \%.2 | 2 | 3 | 39 | . 17 | 070 | 9 | 32 | . 44 | 137 | >19 |  | 3.18 | . 02 | . 06 | 2 | 58 |
| L474E 465*00m | 1 | 48 | 5 | 51 | 2 | 26 | 11 | 806 | 1.78 | 13 | 5 | *D | 1 | 15 | +2 | 2 | 2 | 32 | . 19 | 60, | 5 | 26 | . 35 | 116 413 | +62 |  | 1.57 | . 08 | . 04 | 1. | 53 36 |
| L476E 464*75M | 1 | 105 | 11 | 50 | 2 | 36 | 16 | 466 | 2.73 | 21 | 5 | MD | 2 | 20 | 2 | 2 | 2 | 42 | . 26 | 068 | 10 | 35 | . 55 | 113 | - 86 |  | 2.6 | . 12 | . 05 |  | 6 |
| ( | * | 87 | 18 | 72 | 1 | 45 | 15 | 600 | 2.56 | 88 | 5 | N0 | 1 | 14 | 3 : | 2 | 3 | 37 | . 23 | tos | 6 | 36 | . 44 | 121 | 45 | 4 | 2.19 | . 02 | . 05 | 1 | 469 |
| 4E 484+25 | * | 221 | 5 | 46 | $\square 2$ | 70 | 24 | 383 | 3.96 | 102 | 5 | W0 | 2 | 18 | 2 | 2 | 3 | 57 | . 38 | 463 | 13 | 59 | . 97 | 79 | 12 | 2 | 1.8 | . 02 | . 06 | 2 | 122 |
| 1474E 466-09N | 4 | 53 | 7 | 68 | 2 | 23 | 12 | 740 | 1.98 | 22 | 5 | ND | 3 | 22 | +3 | 2 | 2 | 34 | . 30 | 124 | 7 | 21 | . 35 | 0 | +16 |  | 2.29 | 2 | . 10 |  | 6 |
| L474E 463+75M | \$ | 75 | 10 | 43 | 2 | 28 | 12 | 654 | 2.15 | 17 | 5 | W0 | 1 | 19 | 2 | 2 | 3 | 36 | - 25 | C5 | 9 | 26 | . 40 | 151 | $\stackrel{16}{*}$ |  |  | 02 | +06 |  | 3 |
| 1474E 463+25M | 1 | 65 | 9 | 75 | -2 | 28 | 9 | 700 | 1.70 | 15- | 5 | 10 | 1 | 22 | 2 | 2 | 4 | 28 | . 23 | 168 |  | 20 |  |  |  |  | 1.7 | . 0 | . 6 |  |  |
| - |  | 52 | 9 | 7 | 3 | 39 | 11 | 527 | 1.92 | 23 | 5 | N0 | 1 | 19 | \% 2 | 2 | 3 | 31 | . 23 | \%ov: | 9 | 24 | . 33 | 162 | \%14: | 2 | 1.97 | . 02 | . 06 |  | 19 |
|  | 1 | 44 | 6 | 45 | 1 | 36 | 10 | 565 | 1.89 | 16 | 5 | 410 | 2 | 22 | , | 3 |  | 31 | . 23 | $\mathrm{OH}^{\text {O }}$ | 8 | 25 | . 32 | 164 | . 44 | 2 | 2.03 | . 05 | . 07 |  | 43 |
| 1474E 462+50w | 1 | 38 | 8 | 56 | 2 | 24 | 10 | 935 | 1.60 | 15 | 5 | 40 | 1 | 21 | \% | 2 | T | 28. | . 25 | C58 | 5 | 21 | . 29 | 143 | 80 |  | 1.16 | .02 | .06 |  | 6 |
| 1474E 462+251 | 1 | 54 | 8 | 67 | -2 | 30 | 11 | 698 | 1.78 | 13 | 5 | N0 | 1 | 22 | 3 | 2 | 2 | 27 | . 20 | +115 | 7 | 19 | . 31 | 192 | +22 |  | 1.74 | . 05 | .06 |  | 14 |
| L474E 462+00w | 1 | 38 | 6 | 51 | 2 | 25 | 11 | 811 | 1.71 | 21: | 5 | NO | 1 | 24 | 3 5: | 2 | 3 | 27 | . 30 | -1 | 7 | 19 | . 26 | 192 | . 2 |  |  | . | . |  |  |
| 1476E 461+7 | 1 | 43 | 8 | 55 | $\cdots$ | 28 | 13 | 593 | 2.10 | 21 | 5 | NO | 2 | 27 | ,3 | 2 | 4 | 31 | . 26 | 140 | 9 | 23 | . 33 | 468 | -14 |  | 2.28 | . 02 | . 05 | 1 | 6 |
| L474 $461+50 \mathrm{~m}$ | 1 | 74 | 8 | 58 | 2 | 37 | 13 | 611 | 2.24 | 24. | 5 | H0 | 2 | 29 | \% | 2 | 2 | 35 | .30 | 114 | 11 | 27 | . 40 | 171 | 4 |  | 2.10 | . 02 | . 06 |  | 15 |
| L474E 461+25N | 1 | 37 | 6 | 62 | - 6 | 32 | 12 | 799 | 1.93 | 17 | 5 | mo | 1 | 32 | ${ }^{3}$ | 2 | 3 | 31 | . 31 | 6s5 | 8 | 22 | . 30 | 200 | 13 |  |  | . 12 | . 07 |  | 17 |
| L474E 461000 | 1 | 44 | 10 | 56 | \% 2 | 36 | 14 | 653 | 2.25 | 14 | 5 | mo | 1 | 26 | 2 | 3 | 3 | 37 | .30 | 072 |  | 7 | . 4 | 152 | 2 |  |  | 2 | 0 |  | 10 |
| L474E 460475M | 1 | 73 | 2 | 50 | +2 | 42 | 17 | 907 | 2.59 | 16 | 5 | W | 1 | 24 | +3 | 2 | 2 | 41 | . 30 | 3 | 9 | 32 | . 32 | 149 |  |  |  | 2 | . 07 |  |  |
|  |  |  |  | 8 |  | 91 | 14 | 795 | 2.15 | 13 | 5 |  | 2 | 20 | \% 8 | 2 | 3 | 39 | . 29 | 36 | 8 | 41 | . 35 | 134 | +15 |  | 1.00 | . 12 |  |  | 14 |
|  | 1 | 52 | 26 | 176 | $\stackrel{1}{2}$ | 59 | 12 | 607 | 1.91 | 14 | 5 | MD | 1 | 20 | - 8 | 2 | 3 | 40 | . 31 | 1054 | 4 | 36 | . 49 | ${ }^{6}$ | +2 | 3 | 1.57 | . 02 | . 07 |  |  |
| L474 460400m | 1 | 90 | 5 | 74 | $\pm$ | 40 | 13 | 874 | 2.41 | 9 | 5 | ND | , | 30 | -4 | 2 | 2 | 50 | . 36 | -659: | 7 | 27 | . 49 | 130 | +15 |  | 2.49 | . 02 | .97 |  | 6 |
| L474E 459075N | 1 | 24 | 7 | 52 | 4 | 107 | 11 | 657 | 1.88 | 27 | 5 | WD | 2 | 21 | 2 | I | 2 | 26 | . 16 |  | 4 | 25 | . 27 | 202 | , 17 |  | 3.10 | . 02 | ${ }^{-07}$ |  |  |
| L474E 459+50M | 4 | 28 | 7 | 67 | 2 | 82 | 12 | 274 | 2.22 | 24 | 5 | ND | 2 | 19 | 8 | 2 | 2 | 33 | . 19 | +153. | 6 | 30 | . 37 | 174 |  |  |  | . 02 | . 05 |  |  |
|  | 9 | 58 | 35. | 129 | 67 | 67 | 30 | 1059 | 3.01 | 35 : | 17 | 7 | 37 | 48 | 17\% | 16 | 23 | 50 | . 49 | 4994 | 39 | 55 | + 80 | 175 | 0 | 33 | 1.80 | . 06 | . 13 | 11 | 53 |

Attwood Gold corp. PROJECT GOLDEN CROWN FILE \# 90-1341

| SAMPLE: | No | $\underset{\mathrm{pram}}{\mathrm{Cu}}$ | $\begin{gathered} \text { 䧁 } \\ \text { pom } \end{gathered}$ | $\begin{array}{r} \mathbf{2 n} \\ p r o m \end{array}$ | Ag | Mi | $\begin{gathered} \mathrm{CO} \\ \text { pon } \end{gathered}$ | $\begin{array}{r} \text { Mn } \\ \text { ppin } \end{array}$ | $\begin{gathered} \text { Fe } \\ \mathbf{y} \end{gathered}$ | $\begin{gathered} \text { As } \\ \hline \text { pran } \end{gathered}$ | $\begin{array}{r} \text { U } \\ \text { pom } \end{array}$ | $\begin{array}{r} \text { AU } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { ith } \\ \text { ppom } \end{array}$ | $\underset{\text { prom }}{\mathbf{S r}}$ | cd Ppor | $\begin{array}{r} \text { Sb } \\ \text { pprm } \end{array}$ | $\begin{array}{r} 9 i \\ \text { ppm } \end{array}$ | $\begin{array}{r} v \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{\%} \end{gathered}$ | $\begin{array}{r} \mathrm{P} \\ \mathrm{I} \end{array}$ | $\begin{aligned} & \text { Lb } \\ & \text { ppon } \end{aligned}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppm} \\ \hline \end{gathered}$ | $\underset{\mathbf{x}}{\mathrm{Xg}}$ | $\begin{array}{r} \mathrm{Be} \\ \mathrm{ppm} \\ \hline \end{array}$ | $\boldsymbol{T}$ | $\begin{array}{r} \text { B } \end{array}$ | $\begin{gathered} \mathbf{A !} \\ \mathbf{X} \end{gathered}$ | $\begin{array}{r} \mathrm{Ma} \\ \mathbf{x} \end{array}$ | $\hbar$ |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1475E 460450m | 1 | 49 | 10 | 65 | 2 | 20 | 8 |  | 1.68 | 20 | 5 | ND | 2 | 27 | . 2 | 2 | 2 | 28 | . 32 | 147 | 6 | 99 | . 29 | 217 | 14 |  | 2.08 | . 02 | . 05 | 2 | 51 |
| L475E 468+25 | 1 | 47 | 10 | 49 | 2 | 20 | $\bigcirc$ | 750 | 2.04 | 15 | 5 | ND | 4 | 27 | -2 | 2 | 2 | 33 | . 30 | -019 | 10 | 21 | . 34 | 182 | 78 |  | 0 | 2 | . 05 | 1 | 45 |
| L475E 48-00w | 1 | 46 | 10 | 48 | . 2 | 22 | 11 | 983 | 2.19 | 14 | 5 | HD | 2 | 17 | 3 | 4 | 2 | 58 | . 25 | O6t | 8 | 27 | . 40 | 169 | 7. |  |  | 04 |  | 1 | 4 |
| L6TSE 467+754 | 1 | 66 | 7 | 40 | 2 | 19 | 10 |  | 2.04 | 13 | 5 | HD | 2 | 16 | -2 | 4 | 2 | 39 | . 23 | \% 850 | 8 | 23 | -35 | 124 | 17 |  |  | 01 |  |  | 17 |
| L6TSE 4674004 | 1 | 60 | 11 | 43 | 2 | 21 | 12 | 708 | 1.86 | 20 | 5 | ND | 1 | 20 | 2 | 2 | 2 | 33 | 31 | .068 |  | 20 | . 34 |  |  |  |  |  |  |  |  |
| L67E 466-75\% | 1 | 60 | 0 | 65 | 2 | 29 | 14 | 852 | 2.21 | 27 | 5 | N0 | 2 | 25 | + | 2 | 2 | 35 | . 44 | . 069 | \% | 29 | .43 | 205 | 13 | 3 | 1.85 | . 01 | . 09 | 1 | 21 |
| L6FE 460-750 | 1 | 119 | 5 | 66 | 1. | 29 | 12 |  | 2.18 | 22 | 5 | ND | 3 | 32 | 2 | 2 | 3 | 35 | . 41 | 1099 | 11 | 26 | . 43 | 165 | . 15 | 3 | 2.26 | . 02 | . 10 | 1 | 20 |
| L675E $466+25 \%$ | , | 8 | 45 | 51 | 2 | 21 | 12 | 649 | 2.14 | 4 | 5 | No | 2 | 21 | 2 | 2 | 5 | 34 | . 40 | .050: | 12 | 23 | . 34 | 123 | 19 | 5 | 2.93 | . 02 | . 05 | 3 | 14 |
| L6TSE 46\% 6001 | 8 | 74 | 43 | 37 | 2 | 19 | 19 | 520 | 1.85 | 49 | 5 | ND | 1 | 22 | 3 | 2 | 2 | 32 | . 45 | 0034 | 7 | 21 | . 32 | 119 | 13 |  | 1.89 | . 02 | . 05 | 2 | 24 |
| L4TSE 465*75\% | 9 | 08 | \$4 | 63 | 3 | 83 | 15 | 361 | 2.15 | 49 | 5 | NO | $\dagger$ | 28 | 4 | 2 | 2 | 33 | . 51 | .092 | 7 | 40 | . 57 | 96 | . 12 |  | 1.69 | 2 | . 05 |  | 175 |
| L675 465+50\% | * | 107 | 10 | 59 | 2 | 38 | 15 | 681 | 2.38 | 38 | 5 | ND | 2 | 18 | +3 | 2 | 2 | 36 | . 36 | 065 | 9 | 26 | . 40 | 95 | .14 | 4 | 2.17 | . 02 | . 04 | 2 | 54 |
| L6TSE 465-25\% | 1 | 86 | 11 | 49 | 2 | 40 | 15 | 539 | 2.48 | 21 | 5 | ND | 2 | 16 | +2 | 2 | 2 | 40 | . 23 | . 055 | 8 | 39 | . 55 | 123 | 17 | 2 | 2.71 | . 01 | . 05 |  | 8 |
| t 675 E 465-00M | 1 | 94 | 16 | 66 | 2 | 24 | 14 | 979 | 1.99 | 64 | 5 | ND | 1 | 24 | . 2 | 2 | 2 | 32 | . 37 | .083 | 8 | 22 | . 36 | 153 | 45 |  | 4 | . 01 | . 06 |  | 5 |
| 1675E 464+531 | 1 | 146 | B | 7 | 3 | 61 | 14 | 634 | 2.17 | 72 | 5 | WD | 2 | 22 | 2 | 3 | 2 | 32 | . 43 | .055 | 13 | 28 | . 40 | 90 | - 75 |  | 8 | 2 | 06 | 1 | 14 |
| L4TSE 464+50N | * | 188 | 10 | 41 | . 2 | 50 | 22 | 326 | 3.45 | 53 | 5 | N( | 3 | 14 |  | 2 | 2 | 53 | . 22 | -058 | 11 | 53 | 6 | 72 | 4 |  | 6 | 1 | . 04 |  |  |
| 35 464+25 | 4 | 50 | 19 | 54 | 2 | 20 | 11 | 924 | 2.03 | 18 | 5 | Mo | * | 17 | 4 | 2 | 2 | 37 | . 22 | Ors: | 5 | 24 | . 37 | 132 | . 13 | 2 | 7.61 | . 01 | . 04 | 4 | 167 |
| L4Tse 464*00m | * | 36 | 13 | 34 | . 1 | 11 | B | 740 | 1.30 | 12 | 5 | NT | \% | 18 | 2 | 2 | 2 | 27 | . 19 | 030 | 4 | 14 | . 20 | 82 | .10 | 2 | . 91 | . 02 | . 03 | 1 | 8 |
| 6675E 463-751 | 9 | 94 | 8 | 53 | 4 | 30 | 17 | 1039 | 2.43 | 22 | 5 | WO | * | 31 | 2 | 2 | 2 | 41 | . 3 | . 052 | 9 | 32 | . 48 | 177 | 6 |  | 2.37 | . 02 | . 0 | 3 | 63 |
| 1495E 463+50n | 1 | 107 | 11 | 57 | . 3 | 37 | 17 | 586 | 2.52 | 26 | 5 | MD | 2 | 23 | 2 | 2 | 3 | 40 | . 33 |  | 19 | 32 | .31 | 146 | 13 |  | 2.05 | 0 | . 06 | 1 | 14 |
| L675E 463-25M | 1 | 27 | 13 | 79 | . 2 | 47 | 13 | 834 | 2.17 | 20 | 5 | NO | $\ddagger$ | 23 | 2 | 2 | 2 | 32 | . 33 | $\cdots 379$ | 6 | 30 | . 34 | 262 | + 3 |  | 2.05 | . 02 | . 06 |  | 14 |
| L4TSE 463+00M | 1 | 33 | 10 | 89 | 3 | 37 | 12 | 676 | 2.11 | 19 | 5 | ND | * | 24 | . 2 | 2 | 2 | 31 | . 32 | 232 | 6 | 25 | . 34 | 191 | +15 | 3 | 1.90 | . 01 | . 05 |  | 45 |
| L4TSE 462-75M | 9 | 120 | 23 | 33 | 5 | 56 | 10 | 512 | 1.83 | 54 | 5 | No | 4 | 22 | $\cdots 2$ | 2 | 2 | 32 | . 70 | . 035 | 15 | 31 | . 34 | 78 | 14 |  | 2.01 | . 92 | . 05 |  | 22 |
| L675E 462+50m | 1 | 56 | 15 | 90 | .2 | 50 | 13 | 783 | 2.22 | 24 | 5 | No | 2 | 23 | -6 | 2 | 2 | 33 | . 33 | 65 | 10 | 31 | . 39 | 258 | -15 |  |  | . 02 | .06 |  | 41 |
| L675E 462+25M | * | 35 | 15 | 97 | 2 | 59 | 12 | 719 | 1.99 | 25 | 5 | NO | $t$ | 34 | 2 | 2 | 2 | 31 | . 28 |  | 6 | 24 | . 36 | 235 | 7 | 5 | 2.62 | . 02 | . 06 | 1 | 45 |
| L675E 462+001 | 9 | 33 | T3 | 72 | 2 | 41 | 12 | 731 | 1.95 | 24 | 5 | M ${ }^{\text {P }}$ | 2 | 20 | 2 | 2 | 3 | 30 | . 21 |  |  | 20 | . 26 | 160 | 7 | 5 | 2.8 | . 02 | . 06 | . |  |
|  | 1 | 73 | 12 | 61 | 3 | 37 | 12 | 734 | 1.96 | 22 | 5 | No | 1 | 28 | ,2 | 2 | 2 | 31 | . 31 | +122 |  | 25 | . 35 | 191 | 13 | 4 | . 80 | . 02 | . 05 |  | 45 |
| L675E 461+50 | 1 | 35 | 8 | 71 | 2 | 46 | 41 | 900 | 1.56 | 13 | 5 | NO | 1 | 31 | $\square 2$ | 2 | 3 | 25 | . 30 | . 144 | 7 | 21 | . 29 | 237 | 11 | 5 | 1.4* | . 02 | +07 |  | 10 |
| 6475E 461+25M | 1 | 45 | 9 | 61 | 2 | 72 | 15 | 397 | 2.23 | 20 | 5 | ND | 1 | 19 | -2 | 2 | 2 | 35 | . 28 | 666 | 9 | 37 | . 54 | 148 | 13 | 2 | 1.89 | . 01 | . 06 |  | 4 |
| LGTSE 461*00m | 1 | 35 | 12 | 61 | 2 | 成 | 16 | 423 | 2.43 | 15 | 5 | HD | 1 | 20 | +3 | 2 | 2 | 35 | . 28 | 007. | 6 | 48 | .63 <br> 71 | 164 | -12 | 2 | 1.75 | . 01 | . 06 |  | 78 |
| 1475E 460+754 | 1 | 48 | 11 | 69 | 2 | 97 | 17 | 634 | 2.42 | 14 | 5 | ND | 1 | 29 | 4 | 4 | 2 | 36 | . 38 | .062 | 9 | 56 | . 7 | 16 | . 11 | 2 | 1.62 | . 0 | . 06 |  |  |
| 4-3F $480+2$ W |  | 40 | 7 | 56 |  | 76 | 14 | 546 | 2.07 | 16 | 5 | ND |  | 21 | . 2 | 2 | 2 | 31 | . 27 | 068 | 7 | 37 | . 51 | 141 | 11 | 2 | 1.54 | . 02 | . 55 |  | 27 |
| L475 460+00m | 1 | 35 | 12 | 65 | . 2 | 76 | 13 | 788 | 2.00 | 23 | 5 | ND | 2 | 26 | 4 | 2 | 2 | 32 | . 34 | 065 | 7 | 38 | . 45 | 158 | , 4 | 2 | 1.81 | . 02 | .06 | 1 | 19 |
| L475E 459+75M | 1 | 37 | 16 | 66 | 3 | 122 | 15 | 670 | 1.90 | 33 | 5 | ND | 1 | 17 | 7 | 2 | 2 | 29 | . 25 | 813 | 6 | 49 | . 45 | 149 | . 13 |  | 7 | . 02 | . 07 |  | 29 |
| L475E 459\%50m | 1 | 20 | 20 | 100 | 2 | 256 | 21 | 628 | 2.41 | 47 | 5 | MD | 1 | 17 | 4 | $?$ | 3 | 36 | . 22 | -066 | , | 81 | . 61 | 178 | 42 |  | . 64 | . 02 | . 15 |  | 2 |
| 6476E 468+254 | 1 | 20 | 7 | 37 |  | 11 | 5 | 1427 | . 87 | 5 | 5 | MD | 1 | 18 | 4 | 2 | 2 | 20 | . 27 | \%061 | 3 | 9 | . 12 |  | . 07. | 3 | . 61 | . 02 | . 0 |  |  |
|  |  |  |  |  |  | 27 | 14 |  | 2.31 | 23 | 5 | ND | 1 | 26 | 2 | 2 | 2 | 45 | . 42 | \%00) | 11 | 31 | . 52 | 122 | ¢2 |  | 1.00 | . 01 | . 06 | 1 | 30 |
| 6476E 460+401 | 1 |  | 30 | 67 |  | 10 | 14 | 1255 | 1.45 | 19 | 5 | ND | 1 | 19 | 8 | 2 | 2 | 33 | . 28 | +12t | 7 | 13 | . 24 | 176 | $\cdots$ | 2 | 1.35 | . 01 | . 04 | 1 | 23 |
| 4676E 667+ 75 N | 17 | 5981 | 30 39 | 67 129 | 6.7 | 66 | 30 | 1053 | 3.85 | 36. | 16 | 7 | 37 | 48 | \%8.0 | 15 | 24 | 57 | . 49 | \%089 | 38 | 57 | . 88 | 175 | \% 3 | 32 | 1.81 | . 06 | .13 | 12 | 52 |


| SAmples: | $\begin{gathered} \text { Wo } \\ \text { ppon } \end{gathered}$ | $\underset{\mathrm{parm}}{\mathrm{Cu}}$ | $\begin{gathered} \text { Pb } \\ \text { ppom } \end{gathered}$ | in | Ag | $\underset{\text { pron }}{\text { N }}$ | $\begin{gathered} \text { Co } \\ \text { pprm } \end{gathered}$ | $\begin{array}{r} \mathrm{Mn} \\ \mathrm{ppom} \end{array}$ | $\begin{gathered} \text { Fe } \\ \boldsymbol{Z} \end{gathered}$ | ps: | $\begin{array}{r} \text { Uf } \\ \text { mpon } \end{array}$ | $\underset{\text { ppor }}{\text { Au }}$ | $\begin{aligned} & \text { Th } \\ & \text { ppom } \end{aligned}$ | $\begin{array}{r} \mathbf{S r} \\ \text { ppm } \end{array}$ | cd | $\begin{array}{r} \mathbf{S b} \\ \text { porin } \end{array}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{ppm} \\ \hline \end{array}$ | $\begin{array}{r} V \\ \text { ppoin } \\ \hline \end{array}$ | $\underset{y}{C a}$ | $\begin{gathered} 6 \\ \mathbf{x} \end{gathered}$ | $\begin{array}{r} \text { La } \\ \text { pprim } \\ \hline \end{array}$ | $\underset{\text { pron }}{\text { Cr }}$ | $\underset{X}{\operatorname{Xin}}$ | Pat | $\frac{11}{2}$ | Ppp | $\begin{aligned} & \mathrm{Al} \\ & X \end{aligned}$ | $\begin{gathered} \mathrm{N}: \\ \mathbf{t} \end{gathered}$ | $\begin{aligned} & \mathbf{K} \\ & \mathbf{Z} \end{aligned}$ | 苗 | $\begin{aligned} & \text { Am } \\ & \text { phom } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14765 467+25M | 1 | 102 | 9 | 49 | 1. | 27 | 45 | 818 | 2.48 | 25 | 5 | NO | 9 | 18 | .5 | 2 | 2 | 45 | . 31 | 0050 | 10 | 29 | . 55 | 113 | . 6 |  | 2.16 | . 01 | . 06 | 1 | 4 |
| L476E $467+00 \mathrm{~N}$ | 1 | 95 | 14 | 57 | 1 | 22 | 44 |  | 2.17 | 32 | 5 | HD | 1 | 27 | .7 | 2 | 2 | 38 | . 38 | \%009 | 12 | 23 | . 39 | 144 | . 84 |  | 2.26 | .01 | . 05 | 1 | 62 |
| L476E 466+751 | 1 | 108 | 11 | 55 | 2 | 24 | 14 | 760 | 2.25 | 23 | 5 | N0 | 1 | 21 | 84 | 2 | 2 | 40 | . 34 | .054 | 9 | 27 | .48 | 127 | -t |  | 1.80 | . 01 | . 05 | -1 | 39 |
| L476E 466+30m | 1 | 82 | 8 | 60 | 2 | 19 | 40 | 659 | 1.56 | 30 | 5 | H0 | 1 | 15 | 5 | 2 | 2 | 25 |  | 8067 | 0 | 16 | . 27 | 72 | 97 |  | 1.50 | . 02 | . 15 | 1 | 9 |
| L476E 466+25m | 1 | 86 | 6 | 47 | 1 | 10 | 10 | 975 | 1.33 | 17 | 5 | N0 | 1 | 20 | 5 | 2 | 2 | 27 | . 28 | 8053 | 4 | 11 | 19 | 120 | : |  |  | 2 | . 04 |  | 11 |
| 1476\% 468000 m | 1 | 50 | 22 | 92 | 2 | 11 | 17 | 1903 | 1.50 | 27 | 5 | WD | 1 | 41 | :4 | 2 | 2 | 29 |  | sh7t | 4 | 13 | . ${ }^{6} 8$ | 260 | 149 | 3 | 1.04 | . 02 | . 07 | 1 | 12 |
| L476E 465+75\% | 1 | 169 | 7 | 44 | . 3 | 32 | 18 | 531 | 2.76 | 65 | 5 | N0 | 2 | 23 | 4 | 2 | 2 | 41 | . 37 | -058 | 13 | 32 | +52 | 106 | 14 | 2 | 2.46 | . 02 | . 05 |  | 27 |
| L476E 465+50 | 1 | 37 | 10 | 62 | $\cdot 4$ | 18 | 7 | 800 | 1.45 | 21 : | 5 | N0 | 1 | 42 | $\stackrel{8}{6}$ | 2 | 2 | 21 |  | 462 | 6 | 13 | . 17 | 179 | 15 |  | 2.32 | .02 | .06 |  | 27 |
| 1476E 465+251 | 1 | 69 | 6 | 59 | 1 | 26 | 12 | 900 | 1.92 | 35 | 5 | Wid | 1 | 24 | 17 | 2 | 2 | 34 | . 32 | +114 | 5 | 25 | . 39 | 117 | 1. |  | 1.42 | . 02 | . 05 |  | 6 |
| L476E 465+00m | 1 | 128 | 15 | 51 | -2 | 45 | 18 | 418 | 3.07 | 26 | 5 | ND | 3 | 16 | 5 | 2 | 2 | 47 | . 22 | 8467 | 11 | 4 | 4 | 7 | O. |  | - | . 01 | . 05 |  | 2 |
| L476E | 1 | 87 | 11 | 53 | 2 | 34 | 17 | 770 | 2.26 | 17. | 5 | ND | 1 | 19 | 3 | 2 | 2 | 39 | . 28 | 2056 | 6 | 30 | . 49 | 95 | 10 | 5 | 1.65 | . 02 | . 05 |  | 41 |
| L476E 464450m | 1 | 67 | 10 | 48 | -2 | 35 | 13 | 531 | 2.04 | 32 | 5 | ND | 1 | 27 | 2 | 2 | 2 | 30 | . 29 | 0 | 6 | 30 | . 40 | 141 | 10: | 2 | 1.68 | . 02 | .06 | 2 | 2 |
| 6476E 464+25M | 1 | 50 | 4 | 35 | 1 | 23 | 10 | 482 | 1.64 | 31. | 5 | ND | 1 | 15 | 3 | 2 | 3 | 29 | . 15 | -148 | 5 | 21 | 34 | 100 | 11. |  |  | 02 | . 03 | 1 | 12 |
| L476E 464+00m | 1 | 65 | 11 | 46 | . 1 | 21 | 16 | 1006 | 1.92 | 22 | 5 | ND | 1 | 23 | -2 | 2 | 2 | 37 | 28 | 9 | 8 | 37 | . 50 | 109 | 413 |  | 2.04 | . 01 | . 05 | 1 | $\stackrel{\square}{4}$ |
| L676E 463+75 | 1 | 71 | 16 | 48 | .1 | 34 | 14 | 764 | 2.34 | 24 | 5 | ND | 1 | 23 |  | 2 | 2 | 40 | . 30 | - 342 | 8 | 32 | . 50 | 109 | - 13 |  |  | . 01 | - 6 |  | , |
|  |  | 92 | 2 | 59 |  | 43 | 16 | 528 | 2.72 | 25 | 5 | ND | 2 | 23 | 2 | 2 | 2 | 53 | . 30 | \%27 | 8 | 42 | . 75 | 107 | $\pm 4$ |  | 2.48 | . 02 | . 03 | 1 | 3 |
|  |  | +07 | 7 | 42 | $\checkmark 2$ | 51 | 17 | 303 | 2.93 | 34 | 5 | ND | 2 | 15 | 2 | 2 | 2 | 46 | . 41 | OSE | 12 | 46 | . 73 | 73 | . 12 | 3 | 1.39 | . 02 | . 08 |  | 8 |
| L476E 463-00N | 1 | 30 | 8 | 64 | . 1 | 36 | 11 | 385 | 2.03 | 25 | 5 | ND | 2 | 14 | - | 2 | 2 | 31 | . 25 | +183 | 5 | 25 | . 32 | 100 | 13 | 2 | 1.83 | . 02 | .05 |  | 29 |
| L676E 462+75N | 1 | 26 | 10 | 53 | \% 1 | 112 | 12 | 799 | 1.77 | 15 | 5 | ND | , | 21 | -2 | 2 | 2 | 28 | 28 | 8 | 6 | 20 | 38 | 161 | -13 | 2 | 1.91 | . 02 | . 04 | \% | 1 |
| L476E 462+50m | 1 | 36 | 6 | 41 | 1 | 39 | 9 | 406 | 1.63 | 17. | 5 | ND | * | 16 | 3 | 2 | 2 | 28 | . 22 | +70\% | 6 | 20 | .29 | 161 | . 13 |  |  | -02 | . 04 |  |  |
| 14785 462+23n |  |  | 7 |  |  | 50 | 12 | 504 | 2.09 | 16 | 5 | N0 | 2 | 20 | 6 | 2 | 2 | 33 | . 22 | .084 | 9 | 28 | . 41 | 159 | ts |  | 2.24 | . 01 | . 05 | 2 | 22 |
| $1476 E$ 462+8N $1476 E$ 46200N |  | 47 | 6 | 41 | -1 | 73 | 13 | 609 | 2.01 | 20 | 5 | HD | 2 | 22 | 4 | 2 | 3 | 3 | . 25 | 1776 | 8 | 37 | . 46 | 153 | .14 |  | 2.17 | . 02 | . 05 | 2 | 1 |
| 1476E 46E 461+75M | 1 | 50 | 4 | 45 | \%1. | 87 | 14 | 659 | 2.05 | 19 | 5 | W0 | 1 | 21 | \% 5 | 2 | 2 | 32 | . 27 | 8044 | 8 | 43 | . 56 | 144 | 13 | 2 | 1.95 | . 02 | .06 | 1 | 12 |
| L676E 461+50N | 1 | 40 | 16 | 57 | , 1 | 97 | 15 | 609 | 2.09 | 24: | 5 | N0 | 1 | 15 | 4 | 2 | 3 | 32 | . 22 | 8085 | 6 | 48 | . 61 | 141 | 10 | 4 | 1.63 | . 01 | . 05 |  | 82 |
| 1676E 461425M | 1 | 33 | 15 | 63 | 1 | 70 | 13 | 439 | 1.88 | 27: | 5 | MD | 1 | 15 | \% | 2 | 2 | 29 | . 20 | 168 | 5 | 37 | .46 | 116 | . 10 : |  | 7. 32 | . 02 | . 0 |  | 2 |
|  |  |  | 19 | 85 | 2 | 13 | 13 | 560 | 2.10 | 22 | 5 | ND | 2 | 25 | $\bigcirc$ | 2 | 2 | 31 | . 33 | $10 \%$ | 7 | 47 | . 52 | 163 | 13 | 13 | 2.90 | . 02 | . 08 | I | 11 |
| L676e $461+00 \mathrm{~m}$ |  | 56 | 109 | 192 | 8 | 255 | 21 | 420 | 2.98 | 34 | 5 | 10 | 2 | 21 | $1+1$ | 2 | 2 | 40 | . 21 | ypa | 11 | 79 | . 71 | 104 | 17 |  | 2.87 | . 02 | . 04 | 1 | 1 |
| $1476 E$ 460+75 $16762 \times 80+50$ |  | 42 | 14 | 192 | -2 | 344 | 28 | 800 | 2.93 | 39 | 5 | ND | 1 | 13 | -7 | 2 | 2 | 37 | . 13 | -1005 | 7 | 94 | . 64 | 167 | 13 |  | 2.10 | . 01 | . 04 |  | 10 |
| L676E 460 + 25N | 1 | 35 | 19 | 68 | 1 | 159 | 19 | 553 | 2.41 | 26 | 5 | 10 | 1 | 13 | 5 | 2 | 2 | 57 | . 14 | 0055 | 6 | 58 | . 62 | 153 | 13 | 2 | 2.02 | . 01 | . 04 |  | 2 |
| 1476E 450+75N | 1 | 56 | 8 | 77 | 1 | 386 | 20 | 273 | 2.73 | 79 | 5 | WD | 2 | 15 | 2 | 2 | 2 | 39 | . 18 | 8040 | 8 | 65 | . 81 | 100 | \$6 |  | 2.69 | . 01 | . 04 |  | 35 |
|  |  |  |  |  |  |  |  |  |  | 16 | 5 | 10 | 1 | 15 | 2 | 2 | 2 | 46 | . 21 | 1276 | 6 | 15 | . 28 | 59 | 13 |  | 1.74 | . 02 | . 05 | 1 | 1 |
| 1677t $480+50 \mathrm{~m}$ | 1 | 49 | 11 | 89 |  | 19 | 14 | 178 | 2.78 | 16 | 5 | ND | 1 | 19 | +2 | 2 | 2 | 56 | . 27 | . 690 | 10 | 19 | . 45 | 190 | 4 H | 2 | 3.00 | . 01 | . 07 | 1 | 4 |
| L47PE 468+254 | 1 | 74 | 14 | 89 |  | 19 | 14 | 868 | 2.78 1.15 | \% | 5 | W0 | 1 | 27 | + 4 | 2 | 2 | 30 | . 46 | +083 | 6 | 7 | . 9 | 109 | . 08 | 3 | . 90 | . 02 | . 05 | $\stackrel{1}{1}$ | 3 |
| L477E 468+00N |  |  |  | 42 |  | 24 | 10 | 938 | 1.72 | 25 | 5 | No | 1 | 31 | $\stackrel{+}{9}$ | 3 | 3 | 32 | . 46 | $\mathrm{Cl}^{2} 2$ | 9 | 22 | . 32 | 136 | 12 |  | 1.50 | . 02 | . 05 | 1 | 5 |
| L47TE 467473N |  | 70 | 43 | 8 | 1 | 24 | 14 | 974 | 2.59 | 26 | 5 | ND | 1 | 24 | 5 | 2 | 2 | 47 | . 42 | 06\% | 12 | 31 | . 54 | 128 | 12 |  | 2.86 | . 01 | . 07 | 1 | 2 |
| L47TE 467450m | 1 | 7 | 12 | $\boldsymbol{\pi}$ | -1 | 29 | 14 |  |  | 27 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  |  | 6 |  | 47 | 17 | 716 | 2.90 | 31 | 5 | ND | 3 | 28 |  | 2 | 2 | 48 | . 32 | \%057 | 15 | 40 | . 57 | 171 | . 16 |  | 2.54 | . 01 | . $0_{0}$ | 1 | 2 |
| 57 Modat craly-s | 18 | 57 | 39 | 129 | +1 | 68 | 29 | 1027 | 3.78 | 37 | 19 | 6 | 36 | 47 | 17.3 | 16 | 20 | 56 | . 49 | 687. | 37 | 56 | . 88 | 174 | ,080 | 34 | 1.87 | . 06 | . 14 | 3 | 51 |

Attwood Gold Corp. PROJECH GOLDEN CROWN FILE \# 90-1341
Page 13

| SAMDLE* | $\begin{array}{r} \text { mo } \\ \text { pon } \end{array}$ | $\mathrm{Cu}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{p} \times \mathrm{n} \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{pom} \end{array}$ | $\begin{aligned} & \text { Ag } \\ & \text { pomin } \end{aligned}$ | $\begin{gathered} \mathrm{Mi} \\ \mathrm{pOR} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { porn } \end{array}$ | $\begin{gathered} \text { Mn } \\ \hline p p s: 1 \end{gathered}$ | $\begin{gathered} F e \\ y \end{gathered}$ | $\begin{aligned} & A s \\ & p p \pi \end{aligned}$ | $\underset{\mathrm{p} p}{\mathrm{U}}$ | $\underset{\text { PPDB }}{A U}$ | $\begin{array}{r} \text { Th } \\ \text { pporf } \end{array}$ | $\underset{p p \times n}{S r}$ | Cd | $\underset{\text { pob }}{\text { Sb }}$ | $\begin{array}{r} 8 i \\ \text { ppon } \end{array}$ | $\frac{v}{p p m}$ | $\begin{gathered} C \\ X \end{gathered}$ | $\begin{array}{r} \boldsymbol{P} \\ \boldsymbol{\%} \end{array}$ | Le | $\begin{gathered} \mathrm{Cr} \\ \text { prom } \end{gathered}$ | $\begin{array}{r} \text { Mg } \\ \mathbf{X} \end{array}$ | $8 \mathrm{Ba}$ | $T$ | $\begin{array}{r} 8 \\ \text { ppon } \end{array}$ | $\mathbf{A l}$ | $\begin{gathered} \text { W8 } \\ \mathbf{X} \end{gathered}$ | $\boldsymbol{x}$ | $\begin{array}{r} \text { pam } \end{array}$ | $\begin{aligned} & \text { an } \\ & \text { pob } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1477E 467+00\% | 1 | 37 | 5 | 50 | 1 | 26 | $B$ | 416 | 1.65 | 20 | 5 | ND | 2 | 24 | 2 | 2 | 2 | 26 | . 32 | .057 | 8 | 17 | . 27 | 132 | 009 | 3 | 1.49 | . 02 | . 6 | 1 | 22 |
| L4T7E 466+75M | 9 | 30 | 3 | 55 | $i$ | 21 | 8 | 680 | 1.77 | 33 | 5 | ND | 1 | 22 | 2 | 2 | 2 | 27 | . 27 | 135 | 7 | 16 | . 24 | 126 | (1) | 2 | 1.99 | . 03 | . 05 | 1 | 29 |
| L477E 466-50M | 1 | 71 | 8 | 83 | . 2 | 30 | 14 | 828 | 2.66 | 62 | 5 | \$0 | 3 | 27 | . 2 | 2 | 2 | 36 | . 41 | . 174 | 11 | 27 | . 40 | 207 | , 13 | 5 | 2.64 | . 02 | . 07 | 1 | 92 |
| 167TE 460+25M | 1 | 109 | 9 | 70 | 3 | 25 | 13 | 603 | 2.35 | 56 | 5 | ND | 3 | 23 | 2 | 2 | 2 | 32 | . 51 | \%033 | 12 | 22 | . 34 | 106 | .13 | 5 | 2.75 | . 03 | . 07 | 3 | 36 |
| 1677E 466006m | 4 | 215 | 8 | 54 | - 5 | 333 | 53 | 614 | 3.94 | 182 | 5 | ND | 3 | 28 | 2 | 2 | 2 | 42 | . 74 | . 047 | 16 | 240 | . 83 | 59 | .11 | 5 | 2.34 | .03 | . 05 | 1 | 459 |
| L677E 465400\% | 1 | 8 | 16 | 65 | -2 | 48 | 19 | 717 | 3.01 | 34 | 5 | N0 | 3 | 20 | 2 | 2 | 2 | 45 | . 33 | 1303 | 7 | 47 | . 66 | 116 | (12 | 5 | 2.22 | . 02 | . 0 | 1 | 38 |
| 6477E 466475N | 1 | 148 | 7 | 48 | - 1 | 194 | 27 | 355 | 4.24 | 84 | 5 | ND | 4 | 19 | . 2 | 2 | 2 | 53 | . 36 | 8041 | 14 | 133 | 2.00 | 60 | 10 | 8 | 1.65 | . 01 | . 06 | 2 | 380 |
| [477E 464+50N | 9 | 81 | 7 | 69 | 3 | 55 | 19 | 447 | 2.93 | 61 | 5 | ND | 3 | 32 | 2 | 2 | 2 | 39 | . 37 | 141. | 12 | 35 | . 51 | 139 | . 12 | 4 | 2.40 | . 02 | . 06 | 1 | 57 |
| 1677E 464+25N | 9 | 65 | 7 | 63 | +1 | 43 | 15 | 602 | 2.43 | 34 | 5 | ND | 2 | 49 | 22 | 2 | 2 | 33 | . 43 | 107 | 9 | 30 | . 46 | 176 | $\pm 10$ | 4 | 1.73 | . 02 | . 07 | 2 | 82 |
| 1477E 484+00W | 1 | 47 | 6 | 44 | ! | 46 | 13 | 452 | 2.22 | 29 | 5 | ND | 2 | 24 | 2 | 2 | 2 | 31 | . 25 | 140: | 8 | 26 | . 39 | 128 | 415 | 3 | 2.15 | . 03 | . 6 | - | 123 |
| 4477E 463-75N | 1 | 57 | 7 | 58 | 3 | 127 | 16 | 401 | 2.31 | 17 | 5 | ND | 2 | 19 | -2 | 2 | 2 | 31 | . 30 | .038: | 8 | 60 | . 73 | 89 | T1 | 5 | 1.96 | . 02 | .06 | 1 | 78 |
| 2677E 463+50N | 1 | 22 | 7 | 69 | . 1 | 230 | 26 | 757 | 3.13 | 93. | 5 | No | 2 | 22 | . 2 | 2 | 2 | 39 | . 38 | +120. | 5 | 102 | . 53 | 142 | \% 1 | 4 | 1.86 | . 03 | .06 | 1 | 50 |
| 1677E 463+25M | 1 | 32 | 7 | 48 | , 1 | 130 | 17 | 486 | 2.19 | 23 | 5 | ND | 2 | 17 | 2 | 2 | 2 | 30 | . 24 | . 072 | 5 | 46 | . 55 | 139 | *09 | 6 | 1.46 | . 02 | . 05 | 1 | 67 |
| L4TTE 463+00N | 1 | 53 | 13 | 55 | .2 | 114 | 19 |  | 2.86 | 26 | 5 | ND | 4 | 20 | 2 | 3 | 2 | 42 | . 27 | 083 | 12 | 43 | . 60 | 102 | +18 | 5 | 3.45 | . 03 | . 06 | - | 41. |
| 6479E 467450N | 1 | 65 | 10 | 74 | -1 | 29 | 13 | 613 | 2.72 | 24 | 5 | ND | 3 | 22 | 2 | 2 | 2 | 40 | . 24 | \$19\% | 6 | 22 | . 38 | 130 | ¢5 | 4 | 3.52 | . 03 | . 05 | 1 | 21 |
| 449E 469+50m | 1 | 19 | 7 | 73 | 3 | 23 | 10 | 496 | 1.74 | 15 | 5 | ND | 2 | 24 | 2 | 2 | 2 | 24 | - 20 | 216 | 5 | 13 | . 15 | 172 | 44 | 4 | 2.88 | . 03 | . 05 | $\cdots$ | 9 |
| 1479E 469+00W | 1 | 33 | 10 | 70 | . 4 | 40 | 10 | 360 | 2.02 | 8 | 5 | NO | 3 | 23 | 2 | 2 | 2 | 30 | . 22 | . 747 | 7 | 18 | . 24 | 205 | . 5 | 2 | 3.27 | . 03 | . 05 | 1 | 12 |
| STAMDARO C/Au-S | 19 | 61 | 39 | 132 | 7,1 | 72 | 31 | 1048 | 4.13 | 43 | 20 | 7 | 39 | 53 | 18.0 | 15 | 19 | 57 | . 53 | . 094 | 39 | 60 | .95 | 182 | 0 | 38 | 2.03 | . 06 | . 14 | 13 | 54 |

## CONTRACT SERVICES：

Soil Sampling：Sonny Yip（12 days）May 7－May 18 \＄1，094．02
Field Supervision：WR Geological Ltd．（3 days at $\$ 150.00 /$ day $) 450.00$

Geochemical Analysis：Acme Analytical Lab．Ltd．
（698 Samples－30 element ICP Analysis
698 Geochem Au Analysis by Acid／each 10 grams） $6,004.95$

Field Expense：Room \＆Board
Room 11 days at $\$ 22.68 /$ day 249.48
Meals May 7 －May $18 \quad 286.51$
Supplies：soil bags，mattocks， and other stationaries 699.98

1，235．97
Drafting：Geo－Comp Systems
（12 hours at $\$ 40.00 /$ hour） 480.00
Report Preparation：Fordex Management Inc．
（ 3 days at $\$ 300.00 /$ day）
900.00
$\$ 70,164.94$
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