LOG NO: /1 -07	RD.
ACTION	
and the second	

FTLE NO:

# GEOLOGICAL AND GEOCHEMICAL' REPORT

#### ON THE

# LARKSPUR PROPERTY

Record Numbers 5827, 5828, 6484 & 6485

GALORE CREEK AREA LIARD MINING DIVISION BRITISH COLUMBIA

N.T.S.: 104G/3W

LATITUDE: 57 DEGREES 14 MINUTES NORTH LONGITUDE: 131 DEGREES 19 MINUTES WEST

for

TICKER TAPE RESOURCES LTD.

GEOLOGICAL BRANCH ASSESSMENT REPORT

BY

ANDREW L. WILKINS B.Sc.

of

QUEST CANADA EXPLORATIONS LTD. COAST MOUNTAIN GEOLOGICAL LTD.

December, 1990

#### SUMMARY

Exploration on the Larkspur Property consisted of prospecting, silt sampling, contour soil sampling, grid soil sampling, VLF-EM geophysics, magnetometer geophysics and geological mapping.

The property is underlain by limestones of the Permian Stikine Assemblage. These are in fault contact with andesitic volcanics and sediments of the Upper Triassic Stuhini Group. The middle Triassic dioritic Hickman Batholith and early Jurassic granodiorite are the youngest rocks on the property.

One smithsonite-malachite showing has been found on the property. This showing assayed 43.9 grams per tonne (1.28 ounces per ton) silver, 34.95 percent zinc and 0.47 percent cadmium. Minor chalcopyrite in micro-quartz veins has also been found.

Soil geochemistry has resulted in numerous anomalies, the most significant being a north trending multi-element anomaly that is coincident with the one showing on the property.

Geophysics has outlined some VLF-EM anomalies that are improving to the northeast.

Further exploration should be focused on delineating the source for the strong geochemistry and weak geophysical anomalies.

# TABLE OF CONTENTS

ſ

1.	INTE	Page
	1.1	LOCATION & ACCESS 1
	1.2	CLIMATE, TOPOGRAPHY & VEGETATION 1
	1.3	CLAIM STATUS 1
	1.4	REGIONAL EXPLORATION HISTORY
	1.5	PROPERTY EXPLORATION HISTORY
	1.6	1990 WORK PROGRAM 5
2.	GEOL	OGY
	2.1	REGIONAL GEOLOGY 5
	2.2	PROPERTY GEOLOGY 7
		2.2.1 LITHOLOGY 7
		2.2.2 STRUCTURE 8
3.	GEOC	HEMISTRY
	3.1	INTRODUCTION 8
	3.2	SAMPLE PREPARATION & ANALYTICAL PROCEDURE 8
	3.3	MINERALIZATION & ROCK GEOCHEMISTRY
	3.4	STREAM SEDIMENT GEOCHEMISTRY
	3.5	SOIL GEOCHEMISTRY
		3.5.1 TREATMENT & PRESENTATION OF RESULTS 10
		3.5.2 SOIL GEOCHEMISTRY RESULTS 10
4.	GEOP	HYSICS
5.	DISC	USSION
б.	CONC	LUSIONS & RECOMMENDATIONS 12
7.	REFE	<b>RENCES</b> 14
8.	STAT	EMENT OF EXPENDITURES 15
a	ሮሞአሞነ	

# APPENDIXES

APPENDIX 1: ROCK SAMPLE DESCRIPTIONS

APPENDIX 2: ANALYTICAL RESULTS

APPENDIX 3: SUMMARY STATISTICS & HISTOGRAMS

# LIST OF FIGURES

FIG. 1	-	LOCATION MAP			2
FIG. 2	-	CLAIM MAP			4
FIG. 3	-	REGIONAL GEOLOGY MAP			6
FIG. 4	-	PROPERTY GEOLOGY & GEOCHEMISTRY	in	pocke	t
FIG. 5	-	GRID GEOLOGY	in	pocke	t
FIG. 6		GOLD SOIL GEOCHEMISTRY	in	pocke	t
FIG. 7	-	SILVER SOIL GEOCHEMISTRY	in	pocke	t
FIG. 8	-	MOLYBDENUM SOIL GEOCHEMISTRY	in	pocke	t
FIG. 9	-	COPPER SOIL GEOCHEMISTRY	in	pocke	:t
FIG.10	-	LEAD SOIL GEOCHEMISTRY	in	pocke	:t
FIG.11	-	ZINC SOIL GEOCHEMISTRY	in	pocke	۰t
FIG.12	-	TOTAL FIELD MAGNETOMETER PROFILE MAP	in	pocke	؛t
FIG.13	-	VLF-EM PROFILE MAP - HAWAII	in	pocke	۰t
FIG.14	-	VLF-EM PROFILE MAP - SEATTLE	in	pocke	ŧt

# TABLES

TABLE	1		CLAIM STATUS	1
TABLE	2	-	TABLE OF FORMATIONS	7
TABLE	3	-	95TH PERCENTILES FOR STREAM SEDIMENT SAMPLES	9
TABLE	4	_	STATISTICAL SUMMARY OF SOIL ANOMALIES 1	10

#### 1. INTRODUCTION

### 1.1 LOCATION & ACCESS

The Larkspur Property is located on the south fork of the Scud River approximately 80 kilometres south of Telegraph Creek in the Liard Mining Division of Northwestern British Columbia. The property is centred at 57 degrees 14 minutes North latitude and 131 degrees 19 minutes West longitude (N.T.S. 104G/3W). Access to the property is by helicopter only. Fixed wing airstrips exist within twenty kilometres of the claims (Galore Creek or Scud River) and are good locations for helicopter supported exploration camps.

## 1.2 CLIMATE, TOPOGRAPHY & VEGETATION

The climate in the vicinity of the Larkspur property is typical of the Coast Range Mountains. Temperatures are moderate due to the proximity of the Pacific ocean and range from a minimum of -20 degrees Celsius in the winter time to a maximum of 25 degrees in the summer. Precipitation is heavy (300 centimetres annually) with most of it falling as snow at the higher elevations and rain or wet snow at the lower elevations. The exploration season lasts from June to early October.

The topography of the property is rugged and steep with precipitous slopes leading away from the Scud River at an elevation of 390 metres, to mountain peaks, topping out at an elevation of 1,900 metres.

Vegetation below 900 metres consists of mature stands of spruce, hemlock and fir with alder, devils club and blueberry undergrowth. Above 900 metres, the forest gives way to sub-alpine spruce, heather, blueberries and alpine flowers. Sparse vegetation occurs above 1,300 metres.

### **1.3 CLAIM STATUS**

The Larkspur property is located within the Liard Mining Division and staked under the provisions of the British Columbian Mineral Tenure Act. The claims cover approximately 675 hectares and are listed in table 1 below.

## TABLE 1: - CLAIM STATUS

Claim	Record	Recording	Renewal	Total
Name	Number	Date	Period	Units
LARK 1	5827	19-FEB-89	19-FEB-93	8
LARK 2	5828	19-FEB-89	19-FEB-93	4
LARK 3	6484	06-OCT-89	06-OCT-92	20
LARK 4	6485	06-OCT-89	06-OCT-92	12
* pending	acceptan	ce of this rep	ort.	

- 1 -



The claims are owned by Joe Tarnowski of Vancouver and are under option to Ticker Tape Resources Ltd. of Vancouver, B.C.

## 1.4 REGIONAL EXPLORATION HISTORY

The first recorded mineral exploration in the area was undertaken in 1861 when placer gold was discovered on the Stikine River just downstream of the Telegraph Creek town site.

Exploration emphasis changed to the search for lode deposits during the 1920's, 30's and 40's. Exploration was confined to accessible areas along the Stikine River, with a number of small copper occurrences being discovered.

The first major exploration efforts occurred in the 1950's when Hudson Bay and Kenicott Copper were looking for large tonnage, porphyry copper deposits. This led to the discovery of the Galore Creek (137 MT grading 1.02% Cu, 0.014 OPT Au), Copper Canyon (27 MT grading 1.02% Cu, 0.02 OPT Au) and Shaft Creek (363 MT grading 0.40% Cu and 0.010 OPT Au) deposits.

Exploration since then has yielded more results including the Paydirt (0.2 MT grading 0.12 OPT Au), the Jack Wilson and Trophy deposits.

The Galore Creek Camp is currently undergoing a resurgence of exploration activity as mining companies look further north within the same "Stikine Arch" that has produced the successful Stewart and Iskut Gold Camps. Major exploration programs in the area for 1990 include drilling programs on the Galore Creek, Jack Wilson, Copper Canyon and Trophy prospects.

### **1.5 PROPERTY EXPLORATION HISTORY**

During the summer of 1987, the B.C. Geological Survey Branch conducted a regional stream sediment geochemistry survey in the area. Three creeks were sampled that drain the property. One sample was anomalous (>95th percentile) in antimony and weakly anomalous (>75th percentile) in lead, molybdenum and mercury, a second sample was weakly anomalous in gold, copper, nickel and antimony, and the final sample was weakly anomalous in copper, antimony and cobalt.

During the summers of 1988 and 1989, the B.C. Geological Survey Branch conducted a regional geological mapping program in the area. During this program, 4 rock samples were collected and assayed from the Larkspur property. Results from these assays were insignificant.

During October of 1989, one day was spent prospecting on the claims by Coast Mountain Geological Ltd. personnel. During this day, 9 rock samples and 2 stream sediment silt samples were collected.



One silt sample was strongly anomalous (>95th percentile) in silver, lead and zinc and weakly anomalous (>75th percentile) in gold, arsenic, molybdenum and nickel. The other silt sample was strongly anomalous in nickel and weakly anomalous in silver and zinc. No significant results were obtained from the rock samples.

#### 1.6 1990 WORK PROGRAM

Phase 1 exploration consisted of stream sediment silt sampling, prospecting and contour soil sampling. Phase 2 consisted of geological mapping, prospecting, grid soil sampling, VLF-EM geophysics and magnetometer geophysics. A total of 34 man days were spent on the claims. During this time, 1.0 kilometres of base line was cut and 10.9 kilometres of flagged grid lines were run while soil sampling. Soil samples were collected at 25 or 50 metre intervals. A total of 507 soil samples, 13 stream sediment silt samples and 36 rock samples were collected. A VLF-EM and Magnetometer Survey was conducted on three of the grid lines for a total of 2.175 kilometres using an IGS-2/MP4 instrument.

The 1990 work program was conducted by the following Quest Canada Exploration Ltd. and Coast Mountain Geological Ltd. personnel:

Andrew Wilkins B.Sc	Project Geologist
William Kushner B.Sc	Geologist
Todd Faragher	Geologist
David Ridley	Prospector
Catherine Ridley	Prospector
Jake Herrero	Prospector/Sampler
Jamie McClennan	Prospector/Sampler
Gerald McKee	Sampler
Andy Cooper Geog	hysical Technician

## 2. <u>GEOLOGY</u>

#### 2.1 REGIONAL GEOLOGY

The Regional Geology is presented in Figure 3 (Logan, Koyanagi and Rhys, 1989, and Brown and Gunning, 1989).

The Galore Creek Mining Camp lies on the western margin of the Intermontane Belt within the Stikine Arch in contact with the Coast Plutonic Complex. The Stikine Arch is a northeasterly trending belt of metamorphic rocks that formed a positive tectonic element throughout the Mesozoic (Souther and Armstrong, 1966). Sediments derived from rocks of the Stikine Arch were shed north and northeast in to the southern extension of the Whitehorse Trough during the Upper Triassic and Lower Jurassic.

The oldest rocks consist of highly deformed Permian and older metamorphic rocks and Permian crystalline limestones belonging to the Stikine Assemblage, and a thin succession of Middle Triassic siltstones. These are in fault contact or unconformably overlain



by the Upper Triassic Stuhini Group consisting of augite andesite and andesitic breccias, agglomerates, flows and tuff interspersed with locally derived sandstones and siltstones. These have been intruded by Upper Triassic to Lower Jurassic syenite stocks and dykes, quartz diorite and granodiorite stocks and plutons, belonging to or related to the Hickman Batholith, as well as Jurassic to Tertiary quartz monzonite, granodiorite, and quartz diorite belonging to the Coast Plutonic Complex to the west.

## 2.2 PROPERTY GEOLOGY

The property geology is presented in Figures 4 and 5 in the back of the report.

#### 2.2.1 LITHOLOGY

The Larkspur property is underlain by a succession of cliff forming Permian limestones belonging to the Stikine Assemblage. The limestones are light grey to buff, massive to thickly bedded, bioclastic calcarenite. Marcon to green coloured lapilli tuff and epiclastics are interbedded within the limestone.

#### TABLE 2: - TABLE OF FORMATIONS

QUATERNARY PLEISTOCENE AND RECENT Q ..... Glacial drift and alluvium.

#### Unconformity

EARLY JURASSIC <u>COAST PLUTONIC COMPLEX</u> eJm ..... Granodiorite.

MIDDLE TRIASSIC <u>HICKMAN BATHOLITH</u> mTd .... Diorite.

#### Intrusive contact

UPPER TRIASSIC

STUHINI GROUP

uTv ..... Andesitic flows, lapilli tuff, breccias and fragmentals.

#### Fault contact

#### PERMIAN STIKINE ASSEMBLAGE

Pl ..... Bioclastic calcarenite.

Plp ..... Lapilli tuff and epiclastics.

The limestones are in fault contact with volcanics and sediments of

the Upper Triassic Stuhini Group to the east. The volcanics consist of andesitic, light to dark green pyroxene-porphyry flows, lapilli tuff, breccias and fragmentals. The sediments consist of dark to medium grey, weakly gossanous argillite. A sliver of Stuhini volcanics and sediments also runs through the western portion of the property. Included in this sliver is an extremely siliceous light green siltstone or chert that forms a prominent 25 metre cliff band.

In the eastern portion of the claims, the Stuhini Group has been intruded by the middle Triassic Hickman Batholith, consisting of medium to coarse grained biotite, hornblende, augite diorite.

On the western boundary of the claims, the Stikine Assemblage has been intruded by early Jurassic medium grained hornblende, biotite granodiorite.

## 2.2.2 STRUCTURE

A major north trending, steeply dipping fault runs through the eastern portion of the claims and separates the Stikine Assemblage from the Stuhini Group. Associated with this fault is a major carbonate alteration zone up to 30 metres wide with minor chlorite and mariposite. No mineralization was found within this structure.

Other northwest and northeast trending, steeply dipping faults were observed on the claims.

## 3. <u>GEOCHEMISTRY</u>

### 3.1 INTRODUCTION

Stream sediment silt samples were collected from most creeks on the property. Soil samples were collected at 25 or 50 meter intervals on contour lines and grid lines in the southwest portion of the property. Grab rock samples were collected from interesting lithologies, alteration and mineralized showings. A total of 13 silt samples, 507 soil samples and 36 rock samples were collected.

Geochemical analysis are presented in Appendix 2.

## 3.2 SAMPLE PREPARATION AND ANALYTICAL PROCEDURE

Soil and silt samples were collected in KRAFT gusseted paper bags and sent to ACME ANALYTICAL LABS of Vancouver B.C.. At ACME, samples were oven dried at approximately 60 degrees Celsius and sieved to minus 80 mesh. Rock samples were collected in plastic bags and also sent to ACME. Samples were then crushed down to 3/16 of an inch, and then a 1/2 pound of the sample is pulverized to minus 100 mesh. A 0.5 gram sample of the minus 80 fraction of all samples was digested in hot, dilute aqua regia in a boiling water bath and then diluted to 10 millilitres. with distilled water. Samples were analyzed for a group of 30 elements using the Induced Coupled Plasma (ICP) technique. In addition, gold was analyzed from a 10 gram fraction by the conventional Atomic Absorption (AA) technique. One rock sample was assayed for silver, zinc and cadmium by conventional assay techniques.

## 3.3 MINERALIZATION & ROCK GEOCHEMISTRY

Rock sample descriptions are presented in Appendix 1.

Two mineralized showings were found on the property.

The first showing consists of a boulder 0.5 metres in diameter which assayed 43.9 grams per tonne (1.28 ounces per ton) silver, 34.95% zinc and 0.47% cadmium. The boulder consisted of predominately box worked weathered cellular Smithsonite (a secondary zinc carbonate) with minor malachite. Outcrop is limited and the showing is associated with a soil geochemistry anomaly. It is believed that the boulder is close to its outcrop source.

The second showing consists of minor chalcopyrite in quartz microveins within the Hickman diorite. This showing contained up to 774 ppm copper.

#### 3.4 STREAM SEDIMENT GEOCHEMISTRY

Stream sediment geochemistry results were compared with the results from the Regional Geochemistry Survey conducted in 1987 by the British Columbia Geological Survey. Samples greater than the 95th percentile were considered anomalous.

TABLE 3: - 95TH PERCENTILES FOR STREAM SEDIMENT SAMPLES

Cu	Pb	Zn	Ag	Au	Mo	Ni	Co	Sb
ppm	ppm	ppm	ppm	ppb	ppm	ppm	ppm	ppm
>125	>27	>152	>0.5	>72 >15*	>6	>92	>25	>5

\* 75th percentile for Au.

All but one sample were anomalous in at least one element. Numerous samples were anomalous in silver, zinc, antimony, nickel and cobalt. The southwest corner of the property is anomalous in the most elements and consists of a cluster of two samples which are anomalous in silver, molybdenum, zinc, antimony, nickel and cobalt. One of these samples is also anomalous in lead.

# 3.5 SOIL GEOCHEMISTRY

## 3.5.1 TREATMENT AND PRESENTATION OF RESULTS

The construction of histograms, probability plots and the calculation of means, medians and standard deviations were performed using the Association of Exploration Geochemists PROBPLOT program (Stanley, 1987).

The PROBPLOT program is an interactive software tool which allows a user to rapidly analyze cumulative frequency data. The program is capable of representing numerous forms of frequency distributions consisting of combinations of normal or log-normal populations. An appropriate frequency distribution model can be used to separate the multi-modal data distribution into its component populations. These, in turn, can be used to define thresholds which separate the data into groups corresponding to these component populations.

The data was treated as two populations. Gold, silver, copper, lead, zinc, and molybdenum were found to approximate a log-normal distribution. Threshold values and anomalous values were determined at the mean plus two standard deviations (x+2s) and the mean plus three standard deviations (x+3s) respectively. Anomalous sample divisions are summarized in Table 4 and summary statistics and histograms are presented in Appendix 3.

Mean (x)         Threshold           lognormal*         x+2s           Au*         8 ppb         76-235           Ag*         0.4 ppm         3.1-8.4           Mo*         3 ppm         10-20	Anomalous x+3s	Strongly Anomalous x+4s		
Au*	8 ppł	76-235 3.1-8.4 10-20 186-474 91-234 629-1529	236-732	733+
Ag*	0.4 ppn		8.5-22.9	23.0+
Mo*	3 ppn		21-39	40+
Cu*	28 ppn		475-1211	1212+
Pb*	14 ppn		235-603	604+
Zn*	107 ppn		1530-3717	3718+

TABLE 4: - STATISTICAL SUMMARY OF ANOMALIES

#### 3.5.2 SOIL GEOCHEMISTRY RESULTS

Soil geochemistry results are plotted in Figures 6 to 11.

The thresholds for anomalous silver, lead and zinc are very high for the Scud River and Galore Creek area making the anomalies pretty significant.

Geochemistry results outline a poorly defined discontinuous north trending lead, zinc, silver and gold soil anomaly with sporadic

copper. The anomaly runs through the west central part of the grid from approximately 101N/92E to 105N/98E and contains up to 2,240 ppb gold, 13.0 ppm silver, 3,709 ppm lead, 12,121 zinc and 2,522 ppm copper. Three hundred metres to the east and west are two less substantial anomalies in the same elements that parallel this same north trend.

In the eastern corner of the grid is a copper, lead, zinc, molybdenum, silver and gold anomaly of no definite orientation. Values of up to 16.7 ppm silver and 2,160 zinc have been returned from this anomaly.

A broad molybdenum anomaly occurs in the north central part of the claims centred at 102N/97E. The north trending multi-element anomalies run into this broad anomaly.

#### 4. <u>GEOPHYSICS</u>

A VLF-EM and Magnetometer Survey was conducted on three of the grid lines for a total of 2.175 kilometres using an IGS-2/MP4 instrument. A Total Field Magnetometer Profile Map is presented in Figure 12 and VLF-EM Profile Maps for Hawaii and Seattle are presented in Figures 13 and 14 in the back of the report.

The Magnetometer survey is fairly flat with values ranging from 56,930 nt. to 57,155 nt. The magnetometer highs seem to be coincident with the Stuhini Group volcanics.

The VLF-EM for Hawaii shows some weak anomalies that seem to improve to the northeast. Line 92E is fairly flat, with no response over the mineralized showing at 100+60N. Line 94E has one crossover centred at 97+75N. Two other weak anomalies occur at 100+75N and 104N. Line 96E contains the strongest anomaly centred at 99+80N. Another weaker anomaly occurs at 97+25N.

The anomalies at 94E/97+75N and 96E/99+80N have similar responses and are both coincident with a creek running through the property. Gold, copper and zinc soil anomalies are associated with this creek as well.

The VLF-EM for Seattle is fairly flat, however there is some noise around the same Hawaii anomaly at 94E/97+75N.

# 5. <u>DISCUSSION</u>

Numerous mineral deposit types have been recognized in the Galore Creek Camp and the Porcupine Creek Area. These include porphyry deposits, structurally controlled shears and veins, skarns, and breccias. Both a Lower Jurassic mineralizing event and a Tertiary mineralizing event are recognized.

Narrow, sporadic but strong soil geochemistry, topography and

geophysics suggest the presence of narrow, mineralized, north striking faults and shears in the southwest portion of the claims. The predominant limestone geology and the presence of granodiorite intrusions just west of the claims suggests that these structures are most probably skarns. The Smithsonite showing also looks skarn related.

## 6. <u>CONCLUSIONS AND RECOMMENDATIONS</u>

Exploration on the Larkspur Property consisted of prospecting, silt sampling, contour soil sampling, grid soil sampling, VLF-EM geophysics, magnetometer geophysics and geological mapping.

The property is underlain by the Permian Stikine Assemblage consisting of limestones with minor interbedded lapilli tuff and epiclastics. The Stikine Assemblage is in fault contact with andesitic volcanics and sediments of the Upper Triassic Stuhini Group. These have been intruded by the Middle Triassic Hickman Batholith to the east and by early Jurassic granodiorite to the west.

The most significant showing on the property consists of a boulder 0.5 metres in diameter which assayed 43.9 grams per tonne (1.28 ounces per ton) silver, 34.95% zinc and 0.47% cadmium. The boulder is made up of extremely weathered Smithsonite with minor malachite.

Numerous anomalous stream sediment silt samples occur on the property. These samples are anomalous in at least one of gold, silver, molybdenum, copper, lead, zinc, antimony, nickel and cobalt.

Soil geochemistry has resulted in numerous anomalies, the most significant being a north trending multi-element anomaly that is coincident with the one showing on the property.

Geophysics has outlined some weak VLF-EM anomalies that seem to improve to the northeast.

Further exploration should be focused on delineating the source for the geochemistry and geophysical anomalies.

Recommendations are as follows:

- 1) Genie EM geophysics over grid.
- 2) Kaboda trenching of coincident soil geochemistry and Genie EM geophysics anomalies as well as the Smithsonite showing at 92E/100+62N
- 3) Surface geological mapping of trenches.
- 4) Prospecting east of the Scud River in the vicinity of the

chalcopyrite showings.

If results warrant:

- 1) Diamond drilling of most promising zones.
- 2) Extension of grid to the north-northwest.
- 3) Soil geochemistry, Genie EM geophysics and geological mapping over the extended grid.

7. <u>REFERENCES</u>

- Allen, D.G., Panteleyev, A. and Armstrong, A.T., 1976: Galore Creek, Canadian Institute of Mining, Special Volume #15, pp. 402-414.
- Logan, J.M. and Koyanagi, V.M., 1989: Geology and Mineral Deposits of the Galore Creek Area, Northwestern B.C. (104G/3&4), British Columbia Ministry of Energy, Mines, and Petroleum Resources, Geological Fieldwork 1989, Paper 1989-1, pp. 269-284.
- Logan, J.M. and Koyanagi, V.M., 1989: Geology and Mineral Occurrences of the Galore Creek Area (104G/3&4), British Columbia Ministry of Energy, Mines, and Petroleum Resources, Geological Survey Branch Open File 1989-8.
- Panteleyev, A., 1976: Galore Creek Map Area, British Columbia, British Columbia Ministry of Energy, Mines, and Petroleum Resources, Geological Fieldwork 1975, Paper 1976-1, pp.79-81.
- Souther, J.G., 1971: Telegraph Creek Map Area, British Columbia, Geological Survey of Canada, Paper 71-44.
- Stanley, C.R., 1987: Probplot, An Interactive Computer Program to Fit Mixtures of Normal (or Log-Normal) Distributions with Maximum Likelihood Optimization Procedures, Version 1.00 H0, Association of Exploration Geochemists, Special Volume #14.

- 15 -

# 8. STATEMENT OF EXPENDITURES

Salaries:	
Project Geologist:	
17.69 man days @ \$370 per day	\$6,545.30
Geologists:	
11.11 man days @ \$285 per day	\$3,166.35
Prospector	
5.0 man days @ \$265 per day	\$1,325.00
Prospector/Samplers:	
10.0  man days  8255  per day	\$2,550.00
Samplers:	, -,
8 0 man dave & \$230 per dav	\$1,840,00
0.0 man days e \$200 per day	<i>ų170101000</i>
Helicoptert	
6 6 hours @ \$700 per hour	\$4,620,00
6.6 nours @ \$700 per nour	<i>Q47020100</i>
Geerherigel Analyzigt	
Geochemical Analysis:	
ROCK Samples:	¢ 265 40
36 samples @ \$10.15 per sample	\$ 305.40
Silt and Soil Samples:	AA 064 00
520 samples @ \$8.20 per sample	\$4,264.00
Freight	
489 lbs @ \$1.54 per lbs.	\$ 753.06
Room and Board in Scud Camp:	
39.50 man days @ \$155 per day	\$6,122.50
Pilot: (pro rata), 11 days	\$ 405.00
Miscellaneous:	
Field Gear	
45.75 days $&$ \$5 per day	\$ 228.75
Padiog	·
Kaulos AE dava A \$3 per dav	\$ 135.00
45 days 6 55 per day	ų 100 <b>1</b> 00
Chain saw	¢ 80.00
4 days @ \$20 per day	\$ 317 25
Consumables	\$ 317.23 ¢ 105.00
Expediting (pro rata)	\$ 102.00
Rock Cutting	<u> </u>
13 @ \$10 per rock	\$ 130.00
Project Preparation	\$ 93.98
Assessment Filing Fees	\$ 440.00
Other	\$ 9.00
Mob-Demob:	\$5 <b>,</b> 250.00
Management Fees: (15%)	\$5,811.84
Total Geological Costs:	\$
Project Geologist: 17.69 man days @ \$370 per day \$6,545.30 Geologists: 11.11 man days @ \$285 per day \$3,166.35 Prospector/Samplers: 10.0 man days @ \$255 per day \$1,325.00 Prospector/Samplers: 10.0 man days @ \$255 per day \$2,550.00 Samplers: 8.0 man days @ \$230 per day \$1,840.00 licopter: 6.6 hours @ \$700 per hour \$4,620.00 ochemical Analysis: Rock Samples: 36 samples @ \$10.15 per sample \$ 365.40 Silt and Soil Samples: 520 samples @ \$8.20 per sample \$4,264.00 Freight 489 lbs @ \$1.54 per lbs. \$753.06 om and Board in Scud Camp: 39.50 man days @ \$155 per day \$6,122.50 Filot: (pro rata), 11 days \$405.00 scellaneous: Field Gear 45.75 days @ \$5 per day \$228.75 Radios 45 days @ \$20 per day \$135.00 Chain saw \$317.25 Expediting (pro rata) \$105.00 Rock Cutting 13 @ \$10 per rock \$130.00 Project Preparation \$9.900 Other \$5,250.00 scellaneot: \$5,250.00 project Preparation \$9.900 Ab-Demob: \$5,250.00 magement Fees: (15%) \$5,811.84 stal Geological Costs:	

\$44,557.43

TOTAL EXPLORATION COSTS:			\$5	2,480.93
Total Report Costs:			\$	7,107.00
Management Fees: (15%)	\$	927.00	)	
Miscellaneous Costs:	\$	500.00	)	
Drafting Costs:	\$	500.00	)	
Salaries: Project Geologist: 14 days @ \$370 per day	\$5,	180.00	)	
Total Geophysical Costs:			\$	816.50
Management Fees: (15%)	\$	106.50	)	
1 day @ \$135 per day	\$	135.00	)	
VLF/Mag Survey: 2.3 km. @ \$250 per km.	Ş	575.00	)	

#### 9. STATEMENT OF QUALIFICATIONS

I, Andrew L. Wilkins, of P.O. Box 629, Pemberton, B.C., certify that:

- I am a graduate of the University of British Columbia with a B.Sc. degree in the geological sciences (1981).
- I have been engaged in the mining exploration industry in British Columbia and the Yukon since 1978.
- 3) I was the project geologist on the Larkspur project.
- 4) I was involved with the work performed on the LARK 1-4 Claims during the summer of 1990 and am author of this report.

Dated this fifteenth day of December, 1990. Wilkins B.Sc. rew

# APPENDIX 1 ROCK SAMPLE DESCRIPTIONS

------

-----

ľ

. . .

\_\_\_\_

-------

COAS IOUNTAIN GEOLOGICAL LTD.

.....



QUEST CANADA RESOUL IS CORP.

Sompler <u>ANDREW WILKINS</u> Dote <u>JUN 19/21 Jul 2</u>

Property <u>LARK - R90-03-16</u>

NTS 1046/3

SAMPLE	lo	<u>ا</u>	DESCRIPT	ION	L Contraction of the second	1	A	SS	445	
NO.	Sample Width	Rock Type	Alteration	Minoralization	ADDITIONAL OBSERVATIONS	Cu	PB	Zn	Aa	Au
906-16-WI	G	ANDS	Vn= CA- QZ pv: 50-MS	, , , , , , , , , , , , , , , , , , ,	CA-QZ microverns in pervaissive SO-MS altered volcanics	37	3	18	./	3
90G-16-W2	G	ANDS	MF-CA-SO		Bright green fuchsite alter of fx, CA-SO alter as well.	25	10	<i>j4</i>	.1	,
90G-16-W3	G	ANOS	MS-MF		More intense servicite - fuchsite altin of volcanics	13	4	18	./	6
90F-16-WY	F	LMST	CB-MF		Carbonate and fuchsite alter of Permian LMST (skarny looking)	149	5	15	, j	2
90G-16-W5	G	LMST	Q7-14/F-50		Green QZ flooding in LMST with green mica. LMST is sheared with SD affin- 1040/6730	11	5	25	./	2
90 F - 16-W6	F	ANDS LPTF			Light green ANOS LAPILLI TUFF, well foliated with frage up to Icm - Gossanous	23	20	134	.4	1
90G-16-W7	G	ANDS TUFF	CL		Med green, chloritic ANOS TUFF, sheared in Places	8	5	13	.1	4
90F-16-W8	F		PY.		Sossanous cherty looking float 1% dis PY.	5	5	17	.1	1
90F-16-W9	Γ=	minor MS	52PY.		Felsic intrusive fine to med. grained with minor MS altin and 5% PY cubes - sossain	3	7	34	.2	1
706-16-WIO	G	ANOS			CB ver- enhedral CA, minor CL and dis PY Scinwide in CB altered ANDS	3	10	3/	3	38
90G-16-WII	G	BRXX	CB-MN		Hell rounded, CB altered trags in a gassanning HN stained matrix	14	31	80	.4	17
906-16-W12	G	ANDS	QZ-CB		22-CB microvening with PY - gossanous ANDS	529	2	30	.4	230
90G-16-W/3,	G	ANOS	CL	PR 2-5%	Theid to de green foliated ANDS Turk with 2-570 dis purite - Gossenous w stockwork of OZYM	22	4	.59	.1	10
90G-16-W13	G	ANDS	QZ	PY-PR	Essamons ANDS volcanics with Stie die PH and silica floodena alona shiar	1.7.4	9	35	7.3	47
906-16-W14	G	ANDS.	CL	MINOR CP	Shated ce- QZ schest (mylonite) - agglomerate shiceous veins a minor CP.	35	2	24		12:

C-CHIP G-GRAB F-FLOAT

SAMPLE DESCRIP				ION		_	A	SSA	YS	
NO.	Sample Width	Rock Type	Alteration	Mineralization	ADDITIONAL OBSERVATIONS	Cu	PЬ	70	Aa	A
90G - 16- WIS	G	QZ pod	QZ.	PY	Gossenous az pod with 5to dis PY- white-enhedral QZ w come large MS	22	3	22	·9 ·/	7
90G-16-W16	G	GRAN.	MN staining	570 PY(dis)	GZ rich, med grained granitic intrusion .	13	2	28	.1	
ÎOF-16-W17	F	LMST	CA.	dis PY	recrystallized CA.	5	3	19	.5	6
90F-16-W18	F	RHYL	-	<i>~</i> ~	Gossanous and ext. weathered at eye shuplite? - very broken up	103	7	70	•	3
906-16-620	G	LMST	CA-SD		whedral CA.SD Uning and DIXX in LOIST. SD DOIS an	7	5	i46	.1	1
90G-16-W21	G	ARGL		PV.	plack carbonaceous shale or argillite in 10% pu blebs	81	7	23	.5	1
90G-16-W22	G	MONZ	QZ-PY	PY.	Bleached matics and 10% dis PY, silicens I Manzaute	15	17	157	.5	4
90G-16-W53	G	ANDS	iz-cBuning CL	py	Juagy WZ-CA Uning in small shear in vilcanics	20	4.	9K	.2	5
70, F-16-6554	F	?	JCE	SL+ bexwork	Box work weathered QZ-CB reaccounted	2173	17	14 <sup>479</sup>	35.4	5
					boulder 30cm in diamater.					
			· · · · · · · · · · · · · · · · · · ·							

.

C-CHIP G-GRAB F-FLOAT

L LTD.	ROC	K SAMPLE SHEET	QUEST CAN	JA RES	OUR	RCES	S CO	RP.		QUEST CANAD	A RES	;OL.	.JES	3 CO	)RF
· · ·	Property	LARK (#16)		NTS _	10	46	/3	<u>}</u>			NTS .	102	<u>1</u> G	131	M
SCRIPT	ION				Å	55/	YS					Å	SS/	4YS	• • ₽ - \ ₽ - \
eration	Mineralization	ADDITIONAL OBSE	RVATIONS	w	61	Zn	Ag	Ph		ATIONS	in	94	Zn	Ra	A
icous	diss py (418)	limonitic, calcite venlets	160/82 E	346	9	$\gamma$	0.1	6		Ene.	38	2	27	3	1
uslade	trace CPY (LA)	ctz + K-spar Leins		774	g	с С	0.6	4		tered.	23	2	18	0.1	Ţ
1ceros	diss py (212)			189	rio	çq	0.6	4	· · ·	scordite	166	12	ç7	0.1	ŗ
డుంక	Juss A (218)			116	٩	28	0.3	4		J., scordit	e 271	10	53	0.3	ŗ
ans	no usible	limonitic share suffer	e 1005/82	w 478	18	77	0.%	JS							Ī
ians	CAI + Du (218)		1-	388	1ġ	ųΪ	0.2	6							T
						•									T
			- · · ·												Ī
		-			1						1.				T
															T
															T
															T
·			- <u></u>								-	T			T
															T
												1			Ţ

# APPENDIX 2 ANALYTICAL RESULTS

ł

[

ſ

DATE RECEIAEDI DEC IV 1330

DATE REPORT MAILED: Dec. 20/90

# **ASSAY CERTIFICATE**

Prime Exploration Ltd. FILE # 90-3011R2

SAMPLE#	Zn	Cd	Ag**
	%	%	oz/t
90F-16-W24	34.95	. 47	1.28

AG\*\* BY FIRE ASSAY FROM 1 A.T. - SAMPLE TYPE: ROCL PULP

SIGNED BY ..... D. TOYE, C.LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

ROCK GEOCHEMISTRY -	LARK	PROP	ERTY	- R900	3-16																										
	Mo	Cu	Pb	Zn	Åg	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cg	Sb	Bi	V	Ca	P	La	Cr	Ng	Ba	fi	B	Al	Na	ĸ	ĩ	ån*
Sample <b>#</b> JOP-16-W04	рр <b>в</b> 1	ppm 149	рра 5	ppm 18	ppm .1	ррв 276	₽₽ <b>m</b> 25	<b>ppn</b> 1222	\$ 3.40	pp <b>o</b> 2	ppm 7	рры 2	ppa 1	ррв 143	ppa .8	pp∎ 2	pp∎ 2	ppn 43	<b>\$</b> 14.09	\$ .047	рр <b>в</b> 2	ppm 146	\$ 5.77	ррв 72	<b>ዩ</b> በ1	ppn 2	*	۰۰۰ ۱۱	1	ppaa 1	ppb
108-16-W06	1	23	20	134	.4	11	38	2642	8.64	2	5	2	1	6	1.8	11	2	101	.18	.131	7	28	1.75	19	01	5	1 97	•01 05	.07	L C	4
00F-16-W08	4	5	5	17	.1	18	2	324	.61	4	5	2	1	2	.2	2	3	4	.11	. 0.04	2	10	1173	22	01	Â	102	•0J 01	101 01	0	1
JOF-16-W09	1	3	7	34	.2	8	4	654	2.35	19	5	2	1	20	.3	2	ž	10	1.35	.069	i	11	.18	87	101	15	75	*01 84	۱۷، ۱۲	1	1
JOF-16-W13	1	324	ģ	196	.3	18	14	486	3.82	14	5	2	1	12	1.2	2	2	169	1 07	085	1	56	50	1	17	10	2 71	404 10	•10 60	L t	1
30G-16-P01	1	346	g	31	.1	8	15	587	5.64	6	5	2	î	117	1.1	2	,	44	2.05	.101	3	11	1 00	127	17	6	2 01	104 24	102 00	1 1	91 2
30G-16-P02	1	774	8	60	.6	4	11	592	3.54	5	5	,	i	22	.8	1	2	16	2.07	170	12	10	1100	48	-11	12	1 60	*47	120	1	0 7
30G-16-P03	2	189	76	544	.6	15	11	426	2.44	141	5	,	i	35	4.8	ž	2	10	1.78	104	1	14	404 62	205	10	14	1 70	19	103 Ar	2	1
30G-16-P04	1	116	ĝ	28	.1	11	g	310	3.08	38	5	2	1	46	.5	2	2	57	1.74	.111	1	14	60	11	16	12	1 99	15	.vj ng	1	*
30G-16-F05	1	478	18	11	. 8	49	26	1058	5.73	172	5	2	1	45	1.1	12	3	85	4.72	.125	Å	61	1 64	90	10 00	11	3 36	•13	10	1	9 30
30G-16-P06	1	388	10	41	.2	14	12	389	2.96	7	5	2	ī	36	1.3	2	ž	97	2.28	.108	2	25	407	21	105 105		2.30	1.4	117	J J	20 6
90G-16-K01	1	38	2	27	.1	266	30	726	4.92	2	5	2	1	196	1.0	2	2	39	19.06	.021	2	Q2	1.77	103	01	7	1130	+1+ 01	01	1	U 1
30G-16-K02	1	73	2	18	.1	77	11	736	2.45	3	5	2	1	248	.2	2	2	12	24.62	.020	ì	44	4.55	173	01	12	17	101 01	05	1	1
90G-16-K03	16	166	12	87	.1	35	14	575	4.85	27	Š	2	1	24	1.4	2	2	138	1.67	.299	17	66	. 47	14	111	2	+1 ) 96	•VI 85	105	1 1	1
90G-16-K04	9	271	10	53	.3	44	14	487	12.07	10	5	2	1	27	.2	6	2	141	1.38	.106	7	124	.94	19	. 30	2	1 84	103 N7	85	1	1
90g-16-W01	1	37	3	18	.1	436	27	483	3.03	23	5	2	1	438	.)	2	2	25	18.28	.012	2	131	7.71	6	01	2	15	£01	04	1	2
90G-16-W02	1	25	10	14	.1	364	32	848	3.43	6	5	2	1	283	.2	2	2	35	11.92	.016	2	104	7.78	966	.01	7	.32	.01	.06	1	1
90g-16-w03	1	13	4	18	.1	126	17	676	3.85	4	5	2	1	119	.5	2	2	40	13.84	.035	2	113	5.48	33	.01	10	. 28	.01	.10	1	Ē
906-16-W05	1	11	Ę	25	.1	520	35	412	3,32	2	6	2	1	119	.7	2	2	12	10.93	.038	2	407	4.75	94	.01	5	1.08	.01	.06	1	ŷ
90G-16-W07	3	8	5	13	.1	9	5	435	1.42	2	5	2	1	216	.2	2	2	21	1.83	.092	2	10	. 30	24	.11	Ģ	1.31	.01	.02	1	Å
99G-16-W10	1	8	10	31	.3	1	4	4052	4.23	835	6	2	1	116	.7	4	2	4	27.05	.024	12	ç	.17	13	. 61	ź	. 22	.02	.07	1	१९
90G-16-W11	1	14	31	80	.4	2	7	971	2.40	140	8	2	1	27	.4	2	2	7	7.33	.095	14	4	.08	56	.01	1	54	.03		1	17
90G-16-W12	1	529	2	30	.4	21	6	1038	4.00	939	5	2	2	81	.4	3	2	25	8.89	.097	6	4	1.05	36	. 01	, ,	1.09	.01	.16	1	230
90F-16-W17	1	5	3	19	.5	1	1	4225	.59	7	9	2	2	137	.3	2	3	5	23.98	.005	2	1	4.49	5	.01	2	.02	.01	.01	1	6
90F-16-W18	1	103	7	70	.1	7	9	221	8,47	71	5	2	1	3	.2	2	2	67	.02	.014	6	5	.02	25	.01	2	.62	.01	.10	1	31
90G-16-W13	26	22	4	59	.1	35	9	546	4.24	5	5	2	1	4	.2	3	2	46	.16	.035	6	19	1.95	55	.01	2	2.18	.01	.07	1	10
90G-16-W14	1	35	2	24	.1	6	3	537	1.66	2	5	2	1	22	.2	2	2	6	1.38	.077	8	3	.41	63	.01	5	.42	.03	.19	1	128
90G-16-W15	1	22	3	22	.1	26	6	782	1.54	5	5	2	1	24	.2	3	2	12	1.79	.053	5	6	.70	37	.01	3	.22	.06	.04	1	7
90G-16-W16	2	18	2	28	.1	8	6	528	2.00	2	5	2	1	11	.3	2	2	6	.99	.077	7	4	.16	86	.01	6	.42	.04	.19	1	9
90S-16-Q12	2	789	46	222	9.4	24	8	14325	7.48	419	5	4	1	28	3.5	11	2	40	2.26	.107	32	31	.30	159	.02	3	1.59	.01	.04	1	3720
90F-16-W21	4	81	7	23	.5	14	7	307	4.47	15	5	2	2	4	.2	2	3	24	.10	.007	2	12	. 21	33	.02	2	.53	.01	.03	2	1
90E-16-W24	1	2173	17	99999	33.9	4	1	643	1.91	111	7	2	1	12	2188.1	60	2	4	3.40	.010	2	106	1.87	29	.01	2	.02	.01	.02	ĩ	53
90G-14-K01	1	93	21	1072	.3	22	23	165	7.49	3	5	2	3	36	17.6	3	2	29	.54	.042	12	13	1.92	92	.01	3	2.62	.01	.14	1	9
90G-14-W03	1	91	34	2476	.4	55	16	380	7.49	7	5	2	3	122	44.8	5	2	15	1.43	.057	22	15	1.47	55	.01	3	1.92	.01	.19	1	3
90G-16-K10	3	275	4	73	.2	7	6	951	2.35	2	5	2	2	24	1.0	2	2	10	2.02	.081	4	11	.49	96	.01	5	.38	.04	.18	1	15
90G-16-K11	1	36	8	358	.3	15	13	919	4.90	8	5	2	2	20	6.0	2	2	66	1.70	.101	6	23	1.28	47	.15	5	2.83	.07	.11	1	8
90G-16-W20	1	7	5	146	.1	1	1	1800	.42	9	ò	2	1	325	1.5	5	3	2	35.53	.001	16	16	.28	55	.01	2	.02	.01	.02	1	1
90G-16-W22	2	18	17	157	.5	5	13	609	4.95	9	5	2	3	47	2.9	2	2	58	.80	.090	9	6	.87	89	.15	3	1.97	.15	.12	1	4
90G-16-W23	I	20	4	976	.2	7	8	4110	3.09	37	5	2	1	35	15.9	2	2	20	3.23	.070	9	11	.68	177	.01	2	1.47	.01	.15	1	5

.

.

SILT GEOCHEMISTRY	- LARK	PROF	ERTY	- R900	3-16																										
	Mo	Cu	Pb	Zn	Ag	Ni	Co	Ħn	₽e	As	Ũ	Åu	Th	Sr	Co	Sb	Bi	V	Ca	P	La	Cr	Ng	Ba	Ti	В	Al	Na	K	W	Au*
Sample 🖡	ррш	ppn	ppa	ppm	ppm	ppm	ppm	₽₽₽	\$	ppm	ppm	ppn	ppn	ppm	ррг	ppm	ppm	ppm	ł	\$	ppm	ppm	\$	66p	\$	ppm	\$	2	\$	ppm	ppb
90L-16-Q01	2	74	7	213	.5	119	17	1942	4.17	21	5	2	1	61	1.3	2	2	55	2.84	.122	14	85	2.00	147	.05	4	2.12	.02	.05	1	21
90L-16-W01	1	179	3	87	•3	34	22	689	7.21	50	5	2	1	49	1.3	8	2	252	1.37	.135	10	60	1.40	75	.20	12	2.71	.03	.05	1	27
90L-16-W02	1	109	5	59	.2	17	13	436	6.39	27	5	2	2	29	•	2	2	284	1.31	.294	22	41	.82	30	.14	15	1.18	.02	.03	1	1
90L-16-W03	2	95	14	226	.8	104	20	982	4.78	33	5	2	1	52	1.3	. 5	5	58	2.84	.091	12	50	.92	103	.03	7	1.34	.01	.03	1	1
90L-16-W04	14	89	16	270	.8	289	29	1162	5.67	37	5	2	1	41	2.	1	2	104	1.48	.116	10	155	2.65	288	.06	- 14	2.09	.01	.05	1	5
90L-16-W05	21	94	30	269	.9	233	27	956	5.62	42	5	2	1	41	2.3	1 7	2	108	1.40	.116	11	132	1.92	275	.04	10	1.86	.01	.04	1	2
90L-16-W07	1	130	21	96	1.0	444	44	836	5.08	39	5	2	1	60	•	2	2	77	1.65	.062	4	230	5.46	139	.06	10	2.42	.03	.08	1	1
90L-16-W08	1	84	5	102	.5	38	13	759	3.56	22	5	2	1	53		3	2	99	1.66	.104	7	37	.97	50	.09	16	1.36	.02	.03	1	4
90L-16-W09	1	109	8	71	.9	22	18	535	6.94	14	5	2	1	65	1.	2 7	2	258	1.47	.126	9	39	1.25	37	.21	22	2.27	.03	.04	1	5
90L-16-W10	1	53	9	63	1.0	32	11	414	3.73	9	5	2	1	74		) 7	2	77	3.84	.084	7	34	1.33	37	.12	11	1.19	.03	.03	1	1
90L-16-W10A	1	110	15	582	.8	139	18	1641	4.69	32	5	2	1	32	4.	3	2	62	1.75	.123	11	118	1.66	221	.05	5	1.87	.02	.06	1	16
90L-16-W11	1	74	6	123	.3	754	56	716	5.07	16	5	2	1	56	1.	2 2	2	73	1.12	.043	3	208	10.40	70	.87	8	3.29	.01	.11	1	7
90L-16-W12	1	74	4	33	.1	670	46	531	5.83	8	5	2	1	120	1.	) 2	2	92	1.20	.043	2	376	9.05	168	.07	9	2.80	.03	.20	1	5

and side of a second second

,

· ·

	Ħo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Cr	Mq	Ba	Ti	B	Al	Na	K	W	Å12 <sup>±</sup>
Sample 🕯	ppm	ppm	ppm	ppm	ppm	ppm	ррш	ppm	2	рр∎	ppm	ррш	ppn	ppm	ppm	ррв	ppm	ppm	۶	1 p	DE	ppm	ş	ppm	۶	ppm	۶	ş	9	חסמ	pph
90S-16-K01	- 1	75	1	49	15	1051	67	570	8.82	2	5	2	1	141	.8	2	2	92	3.08.0	42	2	453	9.54	209	.01	12	4.84	.02	0.8	1	1
905-16-K02	1	170	11	23	.2	521	66	573	3.47	7	5	2	1	80	.7	5	2	51	4.17 .1	22	4	90	2.39	214	.01	2	1.05	.01	.10	1	1
90s-16-k03	4	162	13	42	.5	747	72	943	7.93	24	5	2	1	72	1.5	2	2	91	3.71 .0	81	4	315	6.42	156	.01	9	2.83	.01	.04	1	,
905-16-K04	1	80	2	42	.5	520	41	724	7.40	4	5	2	1	58	2.0	2	2	125	2.02.0	83	4	522	4.57	200	08	1	2.05	.02	.04	1	1
90S-16-K05	4	97	7	70	.7	519	42	697	8.16	23	5	2	1	46	1.5	7	2	111	1.82 .1	00	6	402	3.83	149	.06	5	1.75	.03	.04	Î	1
90S-16-W01	1	102	11	64	.4	772	65	883	8.29	4	5	2	1	113	1.2	5	2	93	2.81 .0	72	8	284	3.27	360	.02	11	2.01	.02	.05	Ĩ	ş
905-16-W02	5	1033	37	222	2.6	214	55	968	17.54	147	5	2	1	25	.9	27	2	159	1.78.0	78	9	131	1.80	55	.13	12	2.78	.02	.04	ī	10
90S-16-W03	3	260	23	156	.9	504	44	1094	9.60	181	5	2	1	40	2.2	11	2	106	1.10 .1	20	11	177	3.99	192	.14	14	3.33	.05	.15	1	32
90S-16-W04	1	66	2	34	4	1115	66	474	6.96	20	5	2	1	95	1.3	2	4	64	4.09 .0	39	2	279	6.90	139	.01	9	1.66	.01	.08	ī	1
90s-16-W05	1	89	5	42	.4	667	42	643	9.22	3	5	2	1	29	.3	2	2	126	.50 .0	60	4	628	4.99	106	.09	6	1.79	.04	.04	1	1
90S-16-W06	5	90	9	59	.3	682	54	763	8.05	16	5	2	1	33	1.9	8	2	74	1.86 .1	00	13	233	2.24	143	.03	ì	1.57	.02	.07	1	1
90S-16-W07	1	81	11	39	4	927	64	467	6.97	2	5	2	1	85	.8	2	4	68	2.21 .0	43	3	406	9.04	44	.08	10	5.26	.01	.07	1	i
90S-16-W08	1	62	49	307	1.2	22	52	2437	7.25	1479	5	2	2	22	17	4	2	76	1.83 .1	69	10	8	.23	154	.01	5	1.24	.03	20	ī	166
90S-16-W09	1	109	44	149	1.9	10	17	2758	7.30	5422	5	2	1	28	1.1	6	2	37	1.05 .0	73	11	8	.41	181	.01	4	1.23	.02	.13	1	1930
90S-16-W10	1	76	12	75	1.6	7	16	1945	4.53	237	5	2	1	22	.5	2	2	34	2.55 .1	45	1	4	.29	177	.01	7	1.30	.01	.13	1	90
001 88+60E 106+75N	6	13	31	133	.1	17	7	374	6.73	19	5	2	2	7	.6	2	2	74	.17 .0	131	10	36	.14	50	.02	4	5.59	.01	.01	Ī	Ģ
042 89+50E 106+55N	2	28	18	146	.2	20	7	534	5.92	23	5	2	1	1	.2	2	2	55	.12 .0	158	H	32	.42	45	.02	2	2.56	.02	.02	1	9
003 90+45E 106+10N	1	12	20	190	.3	15	6	1270	4.76	15	5	2	1	12	.8	2	2	81	.70 .(	46	20	30	.24	66	.04	2	2.22	.01	.02	1	10
004 91+25E 105+40N	2	55	21	210	1.4	10	5	4357	3.17	32	5	2	1	27	1.5	35	3	26	1.94 .(	169	25	18	.19	84	.09	11	2.07	.08	.04	1	5
005 91+85E 106+15N	4	46	20	104	.2	20	6	362	6.18	41	5	2	1	16	.5	2	3	106	1.02 .0	127	8	36	.36	51	.07	2	2.21	.02	.01	1	13
006 93+05N 105+70N	2	13	24	177	1.6	11	7	2270	5.43	12	5	2	1	13	.9	2	4	78	.87 .(	158	20	20	.10	70	.09	2	2.37	.01	.01	1	- 9
007 93+10E 104+80N	1	16	16	170	1.3	24	10	8151	7.44	27	5	2	1	6	3.6	2	2	55	.31 .(	91	43	26	.06	118	.02	2	2.77	.01	.03	1	8
008 92+80E 103+95N	15	27	35	279	.5	19	16	1848	10.40	82	5	2	1	4	.3	4	2	98	.02 .0	88	8	44	.04	32	.02	2	.99	.01	.02	1	14
009 92+30E 103+10N	1	2522	54	189	13.0	28	9	12303	8.93	560	5	2	1	29	3.6	11	2	32	1.93 .0	98	24	51	.14	129	.01	2	.73	.01	.05	1	2240
010 92+05E 102+10N	2	82	19	187	.4	13	5	1485	4.90	93	5	2	1	7	.8	4	2	50	.16 .0	)30	16	25	.18	254	.07	3	1.87	.05	.03	1	37
011 91+65E 101+25N	3	17	14	155	.4	9	5	445	4.84	16	5	2	1	10	.7	2	2	77	.21 .0	28	8	20	.13	49	.04	2	2.05	.01	.01	1	89
013 88+70E 105+60N	141	328	58	1819	4.6	180	36	1521	10.95	295	7	2	2	221	28.3	28	3	278	.82 .3	118	15	20	.03	366	.02	8	.71	.01	.14	1	16
014 92+30E 103+60N	1	12	24	118	.1	45	17	3929	7.43	36	5	2	1	11	1.6	2	2	29	.84 .0	)76	35	8	.04	122	.02	3	.98	.01	.06	1	13
Q15 92+30E 103+35N	1	38	21	140	1.0	42	12	2307	6.19	23	5	2	1	11	1.0	3	2	83	.26 .(	)84	17	58	.35	91	.06	3	2.47	.01	.03	1	10
016 92+30E 102+85N	2	77	15	100	1.0	101	15	1019	8.70	27	5	2	1	10	.5	2	4	83	.16 .0	93	7	116	1.36	52	.06	2	2.91	.01	.05	1	13
017 92+30E 102+60N	2	67	30	245	1.0	40	12	998	5.17	29	5	2	1	15	.6	2	3	68	.28 .1	)66	9	55	.73	66	.06	3	2.68	.02	.04	1	17
020 97+25E 97+55N	2	19	5	45	.1	9	5	117	1.76	7	5	2	1	13	.2	2	3	59	.17 .(	)24	6	15	.14	28	.04	3	.84	.01	.03	1	26
021 96+80E 98+50N	3	6	6	33	.2	4	2	129	1.69	2	8	2	2	8	.2	2	3	25	.09.1	)25	9	10	.08	50	.15	3	.54	.10	.08	2	12
Q24 96+25E 99+25N	3	52	14	81	.8	35	10	1203	5.31	10	5	2	1	9	.4	2	2	68	.14 .	166	10	82	.38	61	.05	4	2.14	.01	.03	1	19
025 95+70E 100N	4	26	11	85	.8	7	8	754	8.02	3	7	2	2	9	.6	2	2	48	.09 .1	507	9	15	.10	424	.02	3	2.38	.01	.02	1	4
026 99+55E 100+90N	18	26	14	80	.7	21	5	164	4.87	33	5	2	1	10	.2	2	2	86	.15 .0	175	9	41	.18	56	.07	2	1.18	.01	.02	1	6
027 95+05E 101+80N	4	36	22	87	1.6	49	7	508	7.54	50	6	2	2	7	.2	2	2	175	.10 .0	)91	10	91	.26	42	.03	2	2.23	.01	.04	1	25
428 95+15E 102+70N	22	43	32	188		64	14	2701	9.34	195	5	2	1	6	.2	2	2	147	.09 .1	597	7	110	.08	179	.02	3	1,22	.01	.03	1	12
020 95+40P 103+75N	 6	56	60	384	. 8	10	20	2876	8.62	70	Ę	2	1	4	1.3	2	2	38	.11	27	24	10	.85	101	.01	2	2.12	.01	.02	1	14

ł

÷

SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16

Mo Cu Pb Zn Ni Co Mn Fe As Th Sr Cđ Sb Bi Ca ₽ Cr Nσ Ba Ti B Al λq Au La ¥ Aut 1 \$ ٢ ٤ ł ŧ ł. Sample # ppm ppm ppm ppm ppm ppm ppp pp∎ ppm DDB ł ppa ppp ppm pp∎ ppa DDE ppa ppm ppm ppp ppa מממ ppb 54 248 .7 28 1077 11.32 291 5 2 3 .3 17 2 134 .03 .447 16 18 .05 113 .01 2 .92 .01 .02 030 95+75E 104+60N 98 276 142 8 ŝ 2 22 4.7 2 3 92 2.52 .186 24 48 .17 276 .03 .01 70 77 607 1.5 52 13 5.19 75 4 2.46 .05 031 96+10E 105+50N 5 3297 1 16 5 .9 23 .94 .122 19 .94 032 96+458 106+40N 2 17 13 122 .1 9 3 474 1.78 10 2 1 13 2 2 13 .11 68 .05 4 .03 .03 1 â 33 2 11 2 11 .5 2 85 .18 .036 13 62 .56 35 .11 2 3.55 .01 .02 40 12 52 .2 7 437 6.46 4 1 040 104+40E 102N 2 10 10 50 1.26 .01 2 .2 61 .08 .019 39 .16 .02 3 .04 041 104+20E 102+95N 2 11 26 .2 21 4 148 2.19 2 8 6 2 12 4 5 2 .2 2 45 .08 .021 6 16 .06 13 .11 .50 .02 .03 .1 .95 2 7 3 4 1 15 042 103+40g 103+30N 2 6 10 14 4 1 169 2 3 10 165 .61 95 .14 .01 .04 043 103E 104+35N 45 12 104 .4 71 11 482 6.93 ŝ 5 13 . 8 2 2 145 .14 .034 4 3.14 9 1 3 5 2 6 .2 2 2 29 .04 .012 9 18 .05 13 .05 4 .66 .02 .03 93 19 .2 5 1 82 1.04 1 044 103E 105+35N 1 5 8 5 1 .80 .01 2 7 .2 84 .04 .017 36 .06 25 .13 .01 045 103+208 106+30N 14 23 .1 11 2 88 1.75 3 2 2 4 11 9 13 2 1.72 .02 .03 17 75 5 2 8 1.2 134 .47 .021 28 .15 38 .12 1 44 16 L89E 105+00N Ę 30 49 374 .3 9 414 5.90 6 15 23 .21 1.09 .10 .06 16 L89E 104+75N 2 9 11 57 .1 6 3 210 2.16 9 8 2 2 11 .3 2 2 23 1.11 .019 11 .08 6 13 5 2 12 .2 2 133 .13 .011 9 50 .43 57 .09 2 2.42 .01 .03 1 11 37 32 229 5.50 3 2 24 100 .1 7 16 L89E 104+50N 26 26 1.56 .128 16 .06 55 4 1.23 .06 .06 17 5 2 .6 2 11 .11 16 L89E 104+25N 2 8 96 .2 5 4 1899 1.70 2 2 5 2 6 .2 2 2 21 .20 .028 12 10 .09 15 .23 3 .74 .11 .08 S 16 L89E 104+00N 2 8 12 57 .3 4 2 214 1.96 1 8 •2 2 2 90 .09 .034 19 54 .26 48 .11 2 4.99 .01 .03 16 L89E 103+75N 2 31 30 109 .1 23 8 513 7.80 13 2 4 .07 5 5 2 10 .5 2 2 31 1.02 .045 8 11 .05 35 .13 4 .64 .04 3 7 10 69 .3 3 367 1.54 10 16 L89E 103+50N 1 56 01 .04 ç 5 10 .2 2 2 .10 .033 8 41 .32 .08 2 2.35 30 23 67 .6 21 326 6.45 22 113 16 L89E 103+25N 2 6 13 .04 2 1.12 .01 .03 2 11 10 **.**2 g 3 69 1.83 16 ς 2 .2 4 2 47 .19 .024 6 33 .03 16 L89E 103+00N 2 40 5 .1 3 2 80 .68 .040 27 17 .07 31 .09 2 2.60 .01 .02 17 62 .1 ò 681 6.82 25 2 13 16 L89E 102+75N 2 147 4 .01 Ē, 2 10 2.5 6 2 110 .47 .081 25 40 .15 47 .04 2 3.19 .03 5 13 8 .1 3 604 21 2663 13.92 1€ L89E 102+50N 1 q 14 2 2.11 .01 .03 1 ĥ ŝ ) 13 .32 .034 15 .12 20 .14 16 L89E 102+25N 3 10 5-278 .2 8 8 1062 7.31 15 .4 . Ŭ ŝ 61 .: 24 5.78 17 £,  $\overline{27}$ 3.8 3 2 73 1.40 .093 29 23 .10 149 .08 7 3.12 .03 1 12 16 L89E 102+00N 26 421 11 6446 5 2 .28 .159 17 30 .15 <u>93</u> .13 3 2.63 <u>^</u> .03 79 2.4 112 7 27 ξ. 452 .1 27 9 8225 20.04 2 16 L89E 101+75N 2 3.35 .01 1.18 .05 55 5 48 6.1 8 2 102 3.30 .212 30 40 179 .03 1 £ 1 65 630 7664 10.45 104 16 L89E 101+50N 37 .1 9 2 3.50 .01 .06 8 2 68 .163 18 49 .15 145 .02 1 8 32 44 429 .3 28 15 6373 7.85 28 5 3.0 2 .12 16 L89E 101+25N 4 5 Ę .3 6 2 62 .03 .087 6 42 .08 120 .02 2 2.09 .61 .03 1 3 27 4617 10.71 64 16 L89E 101+00N 13 16 140 132 .4 Q. 2 2.27 .03 .05 1 5 10 3 84 .10 .091 11 46 .15 64 .02 14 206 25 9 3856 6.79 42 2 .4 19 53 .6 16 L89E 100+75N 11 3 1.89 .C: 26 5 17 35 2 40 .90 .096 20 55 .06 153 .02 .04 1 6.64 83 9.6 16 L89E 100+50N 22 38 160 1137 1.8 40 11 12091 .90 26 28 .10 158 4 2.57 .08 .06 1 6 15 47 402 1.5 16 4 5874 3.34 Q 5 16 4.1 5 2 32 .055 .14 16 L89E 100+25N 5 2 5 2 19 2 2 40 1.01 .060 43 24 .14 237 .11 5 2.69 \$0. .06 1 24 6.17 19 1.1 16 L89E 100+00N 6 13 28 244 .4 6 11907 26 .08 71 .02 2 2.02 .01 .02 3 17 6 2 88 .16 .031 7 5 2 7 1.0 41 40 137 .1 8 10 407 10.24 43 16 L90E 106+00N 2 .22 2 2.06 .01 .04 1 42 8 1.70 .069 15 25 121 .01 1719 6.84 81 5 2 16 4.2 2 77 16 L90B 105+75N 2 45 58 861 1.0 18 13 8 2 67 .08 10 33 .05 78 .01 2 3.44 .01 .02 1 50 16 L90E 105+50N 10 16 765 12.33 165 5 2 2 2.8 .034 46 216 1014 .1 1 2 3 f 2 2 131 .05 .016 6 48 .26 40 .03 2 2.87 .01 .02 1 10 12 234 11.71 43 5 1.9 22 .1 14 16 L90E 105+25N 3 46 146 5 2 1.1 13 48 2.55 .101 33 18 .32 116 .05 11 2.07 .05 .04 1 7 20 4 31 33 423 .8 20 9 6092 3.86 17 16 L90E 105+00N 2 .27 5 1.50 .13 .08 2 2 2 2 29 1.12 .032 21 11 44 .16 1 2 5 10 .4 2 8 18 127 .2 Q 6 1028 2.80 16 L90E 104+75N 01 2 10 9.85 27 2 3 Q 1.5 3 2 134 .11 .017 13 47 .45 72 .06 2 3.33 .02 28 20 89 .1 18 12 347 16 L90E 104+50N 3 2 18 .2 3 6 85 .76 .029 13 17 .07 37 .11 4 1.41 .02 .02 1 € ţ 162 2.74 2 Ę 1 18 62 .1 4 16 L90E 104+25N 2 q .66 .12 2 .2 3 2 24 .19 .021 12 9 .11 11 .17 3 .08 1 4 4 4 3 176 1.95 16 L90E 104+00N 2 3 ç 48 .1 7 2 .14 .044 11 42 .28 46 .13 2 1.74 .01 .02 i ς 15 2 10 .6 2 113 25 19 11 410 7.01 S, 2 16 L90E 103+75N 3 24 79 .1

	No	Cu	Pb	Zn	Åg	Ni	Co	Ma	Pe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	P	La	Ĉr	Ma	Ba	fti	R	A I	Na	K	ы	1 nt
Sample 🛔	ppn	ррв	ppm	ppm	ppm	ppn	ppm	ppm	ł	ppm	ppn	ppm	ppn	ppm	ppn	ngq	ppm	ppp	1	ş	200	מסמ	,	חממ	ł	้ออก	į	, tu	ş	л 5.016	-nnh
16 L90E 103+50N	4	51	34	127	1	59	17	137	9.64	32	5	2	- 2	10	1.6		<u></u> 2	96	.13	.025	10	85	. 88	76	.04	3	3.04	.01	.03	1	70 190
16 L90E 103+25N	2	18	52	422	.2	24	16	3250	7.71	17	5	2	1	21	3.5	2	2	95	1.48	.138	27	38	.11	124	.05	ŷ	3.70	. 01	.02	1	10
16 L90E 103+00N	16	31	86	150	.7	58	25	6163	16.17	47	5	2	1	8	6.8	5	2	73	.27	.116	44	38	.15	12	.01	2	4.06	.01	.02	2	37
16 L908 102+75N	1	8	21	155	.5	37	5	5301	3.96	26	5	2	1	32	4.2	4	2	41	14.55	.074	8	9	7.02	84	.01	2	.44	.01	.01	1	37
16 L908 102+50N	3	29	39	551	.4	32	17	12932	10.88	78	5	2	1	8	6.0	4	2	145	.81	.104	20	36	.60	106	.03	2	3.64	.01	.01	1	7
16 L90E 102+25N	4	17	28	130	.2	18	9	1488	6.48	25	5	2	1	11	.2	2	3	95	.19	.078	11	40	.24	52	.08	3	2.02	.01	.04	1	ů,
16 L908 102+00N	1	21	44	314	.8	46	6	10705	4.23	36	5	2	1	31	6.3	4	2	46	10.26	.282	33	21	4.51	165	.01	5	2.12	.01	.02	i	ś
16 L908 101+75N	2	20	55	340	.6	44	15	7553	6.93	34	5	2	1	17	3.7	2	2	82	1.35	.143	39	44	.60	135	.04	2	2.53	.01	.04	1	Q Q
16 L90B 101+50N	1	4	2	140	.3	19	1	2188	1.16	31	5	2	1	33	1.8	2	2	22	19.14	.060	5	1	8.99	63	.01	3	.22	.01	.01	1	ź
16 L90E 101+25N	2	19	32	124	.2	12	12	1206	9.18	35	5	2	1	12	3.4	2	2	94	3.22	.053	14	34	1.85	40	.07	2	2.90	.61	.02	1	11
16 L90E 101+00N	2	13	28	260	.2	17	8	2802	4.93	12	5	2	1	16	2.7	3	3	62	1.54	.135	39	25	.15	95	.04	3	2.39	.01	.03	i	
16 L90E 100+75N	2	8	23	118	.1	8	1	2956	2.30	3	5	2	1	10	1.7	3	2	30	.74	.058	14	15	.09	79	.10	4	1.00	.05	.04	i	7
16 L908 100+50N	74	37	39	179	.7	64	17	369	5.62	68	5	2	1	7	.2	8	2	48	.11	.045	2	11	.07	142	.01	6	1.27	.81	.03	1	Ś
16 L90E 100+25N	3	21	39	173	.1	17	15	1303	5.74	10	5	2	1	14	1.7	2	2	100	1.02	.042	23	27	.09	70	.11	2	2.08	.02	.02	2	6
16 L918 107+50N	1	29	32	423	.1	73	10	14925	10.07	34	5	2	1	28	5.2	2	2	52	2.72	.174	50	53	.66	512	.03	2	3.92	.01	.03	1	Å
16 L91E 107+25N	5	132	20	1297	.7	30	9	3935	6.03	88	5	2	3	8	9.1	93	2	41	.29	.035	21	33	.42	96	.17	5	1.64	.11	.08	1	16
16 L91B 107+00N	2	16	24	330	.1	15	6	5859	4.47	25	5	2	1	15	1.7	4	2	45	2.04	.054	28	23	.43	112	.10	2	1.71	.04	.04	1	2
16 L91E 106+758	2	13	11	72	•2	5	3	451	1.99	8	5	2	1	11	.2	2	2	24	1.07	.034	20	13	.07	26	.16	3	1.09	.05	.04	2	2
16 L918 106+50N	1	25	19	302	.2	15	7	7150	3.22	12	5	2	1	24	3.3	2	2	34	2.85	.125	24	17	.52	160	.06	4	1.67	.05	.06	1	2
16 L91E 106+25N	2	3	7	64	.3	4	2	339	1.86	3	5	2	1	5	.2	2	2	23	.23	.021	10	10	.05	11	.25	7	.43	.07	.07	2	2
16 L91E 106+00N	3	43	52	673	.1	31	11	9148	13.09	45	5	2	5	10	3.5	17	2	92	1.65	.062	37	41	.61	139	.12	2	3.45	.03	.03	1	2
16 L918 105+75N	2	38	59	571	. 4	15	6	1782	4.02	37	5	2	1	11	2.3	2	2	31	.45	.082	26	16	.14	40	.08	4	1.53	.07	.07	1	7
16 L91E 105+50N	1	10	17	120	.1	5	4	1083	2.60	9	5	2	1	13	.2	2	2	26	1.11	.043	22	10	.19	44	.19	7	1.61	.12	.08	1	3
16 L91E 105+25N	2	10	11	100	.2	5	3	294	1.64	8	5	2	1	11	.3	2	2	28	1.09	.037	12	12	.07	31	.18	3	.64	.05	.05	2	3
16 L91B 105+00N	2	23	40	289	.1	17	6	7404	5.85	23	5	2	1	24	1.6	2	2	49	1.95	.062	33	19	.44	136	.09	4	1.84	.04	.04	1	2
16 L91B 104+75N	1	15	21	379	.2	16	4	8782	3.97	27	5	2	1	26	2.9	2	2	32	7.03	.125	21	11	2.92	173	.03	7	1.19	.01	.03	1	3
16 L91B 104+50N	4	13	25	122	.3	9	5	734	3.50	11	5	2	1	19	.7	2	2	32	1.17	.052	26	21	.18	33	.12	3	2.02	.10	.07	1	.4
16 L91E 104+25N	5	17	36	159	.4	9	4	448	2.90	9	5	2	1	31	.7	2	2	47	1.83	.060	17	34	.07	85	.04	2	1.63	.04	.05	1	1
16 L91E 104+00N	2	9	27	208	.3	10	5	1464	2.80	12	5	2	1	16	1.6	2	2	30	1.89	.079	21	19	.46	34	.06	3	1.27	.04	.05	1	7
16 L918 103+50N	24	21	67	386	2.1	25	14	1853	8.08	55	5	2	1	29	2.6	13	2	35	1.55	.082	13	28	.11	66	.01	3	1.20	.01	.05	1	6
16 L91E 103+25N	20	16	48	301	1.3	28	14	1049	6.60	39	5	2	1	36	2.9	12	2	33	1.88	.056	14	24	.08	54	.01	6	1.08	.01	.04	1	13
16 L91E 103+00N	15	29	59	397	2.5	33	12	4074	6.65	22	5	2	1	19	6.2	5	2	45	3.00	.100	12	40	.92	106	.01	2	1.42	.01	.02	i	59
16 L91B 102+75N	12	15	36	207	.8	19	9	1235	5.45	11	5	2	1	10	.7	5	2	50	.29	.084	14	28	.12	58	.02	6	1.87	.01	.02	2	35
16 L91E 102+50N	8	19	80	366	1.3	16	9	277	7.39	14	5	2	1	25	1.5	3	2	57	.90	.062	14	34	.08	47	.01	2	2.48	.01	.02	1	30
16 L918 102+25N	2	61	15	108	.3	39	18	2432	5.20	18	5	2	2	8	2.7	2	2	55	.16	.062	12	58	.42	65	.03	6	5.80	.01	.01	1	13
16 L91B 102+00N	6	23	29	99	1.1	12	8	353	6.78	28	5	2	1	5	•3	7	2	95	.09	.039	5	32	.12	38	.01	2	1.56	.01	.01	1	9
16 L918 101+75N	15	17	98	432	.7	23	10	5494	9.01	27	5	2	1	4	2.0	18	2	127	.09	.073	7	32	.07	17	.02	2	1.27	01،	.01	1	· 9
16 L91E 101+50N	15	33	44	184	1.1	50	14	2316	6.47	52	ç	2	1	6	2.1	11	2	58	.42	.053	7	13	.07	75	.01	1	.56	.01	.03	1	15
16 L91E 101+25N	3	35	120	304	3.1	31	13	4382	6.47	14	5	2	1	24	3.6	7	2	64	1.74	.157	22	25	.32	119	.02	3	1.46	.01	.03	1	11
16 L91E 101+00N	2	32	19	134	1.7	27	12	805	6.80	18	5	2	1	26	1.0	2	4	95	1.23	.087	12	6i	.62	100	.06	3	2.91	.01	.03	1	9

j

.

•

~~~~ ]

and a second second

Mo Cu Pb 2n Ni Mn λq Co Fe. As Au Th Sr Cd Sb Bi Ca P V La Cr Мg Ba Ti B Al Na W Au\* Sample | ł ppm pp⊵ ppn pp∎ ppa ppm ppa ppn ppa ppo ppm ł ł ł ł ł ş ppa pp ppa ppa opn ppn ppp pp pp ppn ł ppa ppb 16 L91E 100+75N 3 86 36 38 140 .9 19 10 371 7.38 5 2 10 83 .22 2 1.7 4 97 .16 .031 1 44 76 .03 2.62 .01 4 .02 1 14 16 L91E 100+50N 3 20 5 51 .1 5 б 318 3.52 2 S 2 2 .2 3 2 33 12 .09 .040 11 .18 87 .09 1.33 3 .13 .08 2 8 16 L91E 100+25N 2 36 20 97 23 .1 34 14 680 5.75 2 17 1.3 2 61 4 .30 .032 10 54 .65 52 .07 4 3.35 .01 .02 4 15 16 L91E 99+75N 1 48 8 168 .7 69 21 8883 13.82 40 2 27 4.9 2 58 1.48 24 .091 45 .54 246 .02 2 2.56 .01 .02 2 20 16 L91E 99+50N 5 1 119 . 6 25 4297 8.94 76 26 14 10 5 2 6.1 2 2 17 10.14 .072 8 6 5.01 50 .01 .63 2 .01 .02 1 17 16 L91B 99+25N 1 16 6 170 . 8 26 10 10.90 148 5 2 38 8.9 2 8147 2 26 .115 17 10 57 9.15 4.30 .01 2 .61 .01 .02 1 81 16 L92E 106+50N 9 1 3 45 5 10 .1 4 673 4.45 14 5 2 1.0 2 2 95 .81 .021 10 21 .50 29 .09 2 1.60 .02 .02 1 14 16 L92E 106+25N 2 5 3 70 .1 ł 771 3.04 5 2 Ş .2 2 2 .19 .021 4 40 14 12 .06 25 .12 2 1.29 .05 .84 1 6 16 L92E 106+00N 3 6 23 60 .1 7 б 474 2.94 9 5 2 8 1.5 2 á 74 .13 .021 7 15 .05 14 .22 2 .80 .03 .02 1 4 16 L92E 105+75# 3 18 55 7.40 10 .1 10 8 211 16 5 2 8 2 2 131 .08 .015 6 36 24 . 4 .19 .10 2 2.04 .01 .02 1 1 16 L92B 105+50N 3 12 35 112 9 394 7.19 27 5 .1 11 2 1.4 2 2 74 .19 .040 9 5 33 22 .10 .03 2 3.48 .01 .02 2 4 5 16 L92E 105+25N 1 6 84 .2 3 3.24 2 .2 2 2 4 275 3 5 38 .15 .057 27 12 .04 15 .03 2 1.56 .01 .02 1 4 16 L928 105+00N 2 60 141 452 .4 26 19 1177 14.47 162 2.0 10 2 79 .07 .030 7 75 .34 59 .02 4 3.09 .01 .02 2 27 16 L92B 104+75N 3 37 28 11 121 35 30 2 3 .4 13 492 8.36 1.2 116 .15 .028 10 65 .52 44 .08 2.48 .01 2 .02 1 14 16 L92E 104+50N 32 27 315 7.66 10 2 3 87 .1 26 12 14 2 1.0 2 112 .10 .026 9 56 .36 47 .10 2 2.57 .01 .02 1 9 16 L92E 104+25N 3 38 16 86 .2 9.72 24 13 40 14 247 5 2 1.9 2 2 152 .13 .059 6 111 .49 62 .09 2 2.23 .01 .03 1 12 16 L92E 104+00N 22 18 66 17 10 238 4.26 19 12 .5 2 4 .1 3 160 .22 .019 1 34 .13 66 .10 3 1.57 .01 .03 8 t 16 L92E 103+75N 2 7.45 8 3 14 132 .1 1 7 1077 7 .8 2 2 .35 .048 10 14 .07 23 45 .06 2 .89 .02 .02 1 7 16 L92E 103+50N 10 13 84 8 5 3.11 20 .9 1 .1 2115 2 2 15 2.72 .095 19 1 .14 56 .06 8 1.27 .05 .03 1 8 27 16 L92E 103+25N 5.98 10 1 13 23 205 .2 11 7 4848 3.3 2 2 19 3.45 .112 29 8 .10 112 .04 7 1.39 .02 .02 2 1 16 L92E 103+00N 3 14 23 120 .5 8 12 817 5.52 27 .5 3 2 .17 .034 63 4 .07 18 .02 12 2 .97 .02 .02 1 Ą. 16 L92E 102+75N 3 12 Ę 61 . 8 2 24 .2 2 8 439 4.43 2 59 .06 .082 1 32 8 .16 .04 1.00 .03 .03 2 4 6 16 L92E 102+50N 27 7.12 3 18 445 .4 26 14 5096 -59 18 2.4 2 2 59 1.19 .113 18 69 .15 148 .01 2 2.64 .02 .03 2 18 16 L92E 102+25N 2 29 567 6 .5 121 .1 7 7 873 5.09 147 2 2 38 .10 .047 7 21 .07 .02 48 2 1.39 .02 .02 1 38 16 L92E 102+00N 145 26 4 3164 2.5 23 18 7189 14.17 121 21.0 58 2 77 .06 .094 15 34 684 .03 .01 39 .13 2 2.60 .01 4 16 L92E 101+75N 5 3 14 -5 89 .9 4 5 685 2.74 10 .9 2 2 40 .07 .055 8 15 5 .12 49 .07 .76 .06 .05 2 2 16 L92E 101+50N 3 10 9 692 2.67 .5 2 5 5 47 .4 2 4 -15 36 .04 .067 11 .04 21 .08 4 .41 .02 .02 ţ 9 16 L928 101+25N 11 86 38 297 3.2 28 18 4402 13.85 38 5.1 14 2 148 .02 .033 6 81 .05 71 .01 .52 .01 .01 23 2 1 16 L92E 101+00N 12 2 23 19 837 .6 35 66 10.0 2 2 .61 .060 36 14 4792 7.34 42 41 .25 1335 .01 2 3.00 .01 .03 1 18 16 L92E 100+75N 17 1 118 14 12121 3.9 28 12 6663 7.10 107 141.7 40 2 39 6.27 .098 10 16 3.30 247 .01 2 .81 .01 .01 5 22 16 L92E 100+62N 428 7969 5 3 13 7.2 19 6 2979 9.05 144 5 6 128.2 82 50 .24 .103 15 23 .14 129 .04 2 1.07 .02 .03 2 27 16 L92E 100+50N 206 8 5455 6.6 20 15 6457 16.23 95 11 59.0 76 2 3 2 46 .86 .173 17 17 .22 145 .02 2 1.46 .02 .03 4 6 16 L92E 100+25N 3 38 11 . 2 255 5.69 22 19 . 8 2 1 87 24 9 2 98 .24 .052 44 .51 45 2 2.34 .01 1 12 .06 .83 16 L92E 99+75N 87 7 333 6.12 22 2 .2 2 2 3 114 12 20 2 64 .07 .071 32 2 5 .07 .01 2 1.02 .01 .04 1 3 16 L92E 99+50N 4 161 21 244 1.3 21 13 9426 6.43 119 ς Q 2.9 -35 2 33 .55 .123 23 26 .05 98 .02 7 1.79 .01 .02 1 56 16 L92E 99+25N 3 26 30 76 20 2786 9.20 Ŷ 1.2 2 2 .18 .150 55 5 1.59 28 .2 32 41 62 7 49 .17 .02 .01 .03 1 26 10 16 L92E 99+00M 3 11 58 .5 391 .2 2 3 .094 10 43 .25 47 8 14 7 4.58 8 2 62 .14 .08 4 1.81 .05 .04 1 ŝ .17 .212 58 16 L92B 98+75N 76 15 62 .9 12 13 894 7.81 54 2 1 •2 5 2 66 5 22 .32 80 .01 .01 .06 1 4 3 2.82 16 L92E 98+50N 2 48 10 77 .6 23 678 7.49 28 5 Ģ .2 2 2 85 .13 .208 8 58 .38 59 .04 5 2.77 .01 1 13 11 .03 16 L93E 106+50N 3 13 30 213 .1 10 1728 5.13 8 2 ٦ 13 1.1 2 2 83 1.44 .028 27 21 .87 54 .19 2 2.82 .02 .03 2 6 14

|                 | Mo  | Cu  | Pb   | Zn  | Ag   | Ni  | Co  | Mn    | Fe    | As  | 0   | Au    | ፐስ  | Sr  | Cd   | Sb  | Bi         | V   | Ca   | р    | La  | Cr  | Ma   | Ba  | Ti  | B     | A)   | Na  | ĸ    | W         | ð:n‡   |
|-----------------|-----|-----|------|-----|------|-----|-----|-------|-------|-----|-----|-------|-----|-----|------|-----|------------|-----|------|------|-----|-----|------|-----|-----|-------|------|-----|------|-----------|--------|
| Sample 🛔        | ppn | թթա | ppn  | ppm | ppn  | ppn | ppm | ppm   | ş     | ppm | ppm | ppm   | þpm | ррв | рра  | ppm | ppm        | ppm | \$   | ş    | ppn | DDD | ,    | DDS | 5   | -     |      | 1   | 1    | "<br>החום | nnh    |
| 16 L938 106+25N | 6   | 12  | 92   | 336 | .4   | 10  | - 1 | 1652  | 4.19  | 32  | 5   | ··· 2 | 1   | 11  | .5   | 3   | <b>`</b> 4 | 117 | . 29 | .016 | 8   | 26  | .06  | 66  | .19 | · · · | 1.26 | .01 | .02  | 1         | 11     |
| 16 L93B 106+00N | 2   | 13  | 31   | 462 | .1   | 15  | 7   | 11355 | 3.44  | 18  | 5   | 2     | 1   | 21  | 4.1  | 2   | 2          | 38  | 3.02 | .131 | 32  | 14  | . 07 | 254 | .04 | Ā     | 1.87 | .01 | .01  | 1         | 17     |
| 16 L938 105+75N | 3   | 19  | 108  | 497 | .4   | 19  | 8   | 6962  | 5.37  | 61  | 5   | 2     | 1   | 17  | 3.1  | 2   | 2          | 44  | 1.69 | .103 | 27  | 19  | .12  | 162 | .05 | 2     | 2.22 | .03 | .03  | 2         | 12     |
| 16 L93E 105+50N | 2   | 8   | 16   | 116 | .1   | 7   | 6   | 3788  | 2.71  | 10  | 5   | 2     | 1   | 12  | 1.1  | 2   | 2          | 34  | 1.25 | .050 | 20  | 11  | .09  | 99  | .11 | Ā     | 1.32 | .07 | .05  | 1         | 11     |
| 16 L938 105+25N | 3   | 6   | 8    | 74  | •1   | 7   | 5   | 1153  | 3.49  | 9   | 5   | 2     | 2   | 7   | .2   | 2   | 2          | 42  | .28  | .031 | 13  | 14  | .13  | 33  | .14 | i     | 1.06 | .09 | .05  | 1         | τ<br>τ |
| 16 L93E 105+00N | 3   | 17  | 31   | 132 | .1   | 21  | 13  | 3195  | 7.92  | 18  | 5   | 2     | 1   | 6   | .2   | 2   | 2          | 50  | .35  | .047 | 22  | 16  | .05  | 66  | .02 | 2     | 2.42 | .01 | . 82 | 1         | 1      |
| 16 L938 104+75N | 3   | 9   | 9    | 96  | .7   | 10  | 6   | 2472  | 4.10  | 9   | 5   | 2     | 1   | 5   | .2   | 2   | 4          | 38  | .17  | .040 | 7   | 15  | .05  | 34  | .07 | 3     | 1.18 | .03 | .03  | 1         | 1      |
| 16 L938 104+50N | 4   | 11  | 9    | 48  | .2   | 13  | 6   | 346   | 3.69  | 11  | 5   | 2     | 1   | 8   | .2   | 2   | 2          | 90  | .10  | .025 | 6   | 19  | .09  | 14  | .09 | 2     | 1.10 | .02 | .02  | 1         | 1      |
| 16 G93E 104+25N | . 4 | 28  | 14   | 73  | .1   | 17  | 7   | 288   | 6.99  | 24  | 5   | 2     | 1   | 11  | .2   | 2   | 2          | 98  | .22  | .055 | 7   | 44  | .26  | 37  | .05 | 2     | 2.13 | .01 | .02  | 1         | 10     |
| 16 L93E 104+00N | 4   | 45  | 4    | 109 | .3   | 11  | 14  | 952   | 9.69  | 19  | 5   | 2     | 1   | 7   | .2   | 5   | 2          | 112 | .10  | .121 | 11  | 25  | .18  | 37  | .03 | 2     | 2.02 | .01 | .03  | i         | 8      |
| 16 L93E 103+75N | 6   | 23  | 16   | 222 | .7   | 37  | 23  | 1578  | 6.76  | 53  | 5   | 2     | 1   | 8   | .2   | 6   | 2          | 76  | .10  | .090 | 4   | 16  | .07  | 32  | .03 | 3     | .88  | .05 | .87  | 1         | q      |
| 16 L93E 103+50N | 3   | 18  | 41   | 258 | .3   | 33  | 12  | 6270  | 7,73  | 47  | 5   | 2     | 1   | 16  | 2.3  | 4   | 2          | 55  | 3.33 | .097 | 25  | 24  | .61  | 114 | .02 | 2     | 1.96 | .01 | .02  | 1         | 10     |
| 16 L93B 103+25N | 3   | 13  | 19   | 390 | .2   | 15  | 13  | 4380  | 6.45  | 117 | 5   | 2     | 1   | 6   | .3   | 2   | 2          | 45  | .44  | .106 | 36  | 49  | .12  | 68  | .01 | 3     | 1.84 | .01 | .03  | 1         | 22     |
| 16 193E 103+00N | 2   | 16  | 15   | 62  | .2   | 13  | 7   | 611   | 4.55  | 1   | 5   | 2     | 1   | 10  | .4   | 3   | 2          | 72  | .16  | .065 | 9   | 24  | .19  | 45  | .05 | 3     | 1.62 | .03 | .03  | 1         | 8      |
| 16 L93E 102+75N | 1   | 10  | 2    | 25  | .5   | 2   | 3   | 100   | 1.48  | 7   | 5   | 2     | 1   | 9   | .7   | 2   | 2          | 26  | .07  | .056 | 5   | 1   | .07  | 26  | .01 | 2     | 1.20 | .02 | .03  | 1         | 1      |
| 16 L93E 102+50N | 2   | 25  | 15   | 353 | .4   | 21  | 10  | 1776  | 5.78  | 35  | 5   | 2     | 1   | 16  | 1.6  | 5   | 2          | 63  | .69  | .070 | 15  | 59  | .30  | 104 | .03 | 2     | 2.73 | .02 | .03  | ī         | 17     |
| 16 L938 102+25N | 4   | 33  | 27   | 204 | .1   | 26  | 14  | 824   | 10.52 | 35  | 5   | 2     | 1   | 11  | 1.0  | 2   | 2          | 98  | .15  | .035 | 8   | 60  | .49  | 347 | .04 | 2     | 2.95 | .01 | .02  | 1         | 10     |
| 16 L93E 102+00N | 2   | 22  | 21   | 871 | .5   | 25  | 12  | 5788  | 7.20  | 30  | 5   | 2     | 1   | 13  | 11.3 | 6   | 2          | 57  | 2.37 | .108 | 38  | 25  | 1.20 | 269 | .03 | 2     | 3.93 | .01 | .02  | 1         | 4      |
| 16 L93E 101+75N | 5   | 11  | 35   | 149 | .1   | 8   | 13  | 1450  | 6.53  | 46  | 5   | 2     | 1   | 1   | .2   | 3   | 2          | 110 | .14  | .030 | 5   | 24  | .07  | 47  | .06 | 3     | 1.33 | .01 | .01  | 1         | 7      |
| 16 693E 101+50N | 1   | 24  | 33   | 746 | .6   | 12  | 7   | 6280  | 3.43  | 16  | 5   | 2     | 1   | 18  | 10.3 | 2   | 2          | 42  | 2.06 | .088 | 19  | 15  | .14  | 397 | .03 | 2     | 1.56 | .02 | .03  | 1         | 1      |
| 16 L93E 101+25N | 3   | 6   | 7    | 64  | .4   | 3   | 3   | 418   | 2.46  | 5   | 5   | 2     | 2   | 5   | 1.0  | 2   | 2          | 29  | .16  | .018 | 11  | 12  | .11  | 39  | .14 | 5     | .75  | .11 | .07  | 1         | 4      |
| 16 L93B 101+00N | 3   | 46  | 22   | 131 | 1.0  | 57  | 13  | 411   | 6.51  | 23  | 5   | 2     | 1   | 12  | 2.2  | 2   | 2          | 92  | .22  | .065 | 5   | 74  | .92  | 62  | .03 | 4     | 2.36 | .01 | .04  | 1         | 1      |
| 16 L93E 100+75N | 4   | 18  | 32   | 365 | .1   | 26  | 14  | 4190  | 7.21  | 26  | 1   | 2     | 1   | 5   | 1.8  | 4   | 2          | 101 | .18  | .512 | 10  | 30  | 1.76 | 97  | .03 | 2     | 3.63 | .01 | .06  | 1         | 1      |
| 16 L93E 100+50N | 3   | 12  | 11   | 43  | .6   | 23  | 3   | 231   | 1.59  | 4   | 6   | 2     | 1   | 13  | .6   | 2   | 2          | 42  | .15  | .062 | 7   | 29  | .22  | 37  | .08 | 3     | 1.26 | .04 | .04  | 1         | 12     |
| 16 L938 100+25N | 3   | 41  | 2    | 32  | .1   | 7   | 5   | 183   | 2.26  | 5   | 5   | 2     | 1   | 26  | .7   | 2   | 2          | 37  | .30  | .100 | 8   | 11  | .27  | 40  | .04 | 7     | 2.19 | .01 | .03  | 1         | 11     |
| 16 L938 99+75N  | 4   | 27  | 28   | 64  | .3   | 14  | 10  | 339   | 6.94  | 26  | 5   | 2     | 1   | 13  | .2   | 3   | 2          | 120 | •11  | .146 | 6   | 36  | .32  | 90  | .07 | 3     | 2.11 | .01 | .04  | 1         | 15     |
| 16 L93E 99+50N  | 3   | 34  | 2    | 39  | .6   | 6   | 6   | 415   | 4.78  | 11  | 5   | 2     | 1   | 22  | .6   | 2   | 2          | 73  | .20  | .171 | 10  | 16  | .20  | 50  | .02 | 3     | 2.76 | .02 | .05  | 1         | 1      |
| 16 L938 99+25N  | 3   | 19  | 2    | 33  | 1.0  | 4   | 5   | 723   | 3.02  | 8   | 5   | 2     | 1   | 6   | .2   | 2   | 2          | 37  | .07  | .110 | 8   | 14  | .14  | 56  | .04 | 2     | 1.44 | .05 | .06  | 1         | 5      |
| 16 L93E 99+00N  | 3   | 50  | 3    | 88  | 1.7  | 63  | 12  | 333   | 5.77  | 20  | 6   | 2     | 1   | 12  | . 2  | 4   | 2          | 82  | .20  | .099 | 7   | 97  | .81  | 76  | .05 | 8     | 2.70 | .02 | .05  | 1         | 12     |
| 16 L93B 98+75N  | 3   | 71  | 4    | 114 | 2.3  | 64  | 10  | 313   | 6.46  | 11  | S   | 2     | 1   | 12  | . 8  | 2   | 2          | 67  | .20  | .135 | 13  | 135 | .76  | 77  | .04 | 4     | 3.68 | .01 | .04  | 1         | 1      |
| 16 L938 98+50N  | 3   | 25  | 16   | 50  | 1.5  | 1   | 6   | 377   | 1.27  | 32  | 5   | 2     | 1   | 6   | .2   | 2   | 2          | 73  | .06  | .209 | 8   | 23  | .15  | 33  | .05 | 2     | 2.71 | .02 | .03  | 1         | 8      |
| 16 L94E 105+50N | 2   | 8   | 2    | 27  | .4   | 5   | 2   | 95    | 1.23  | 2   | 5   | 2     | 1   | 9   | .2   | 2   | 2          | 20  | .11  | .065 | 8   | 11  | .06  | 24  | .02 | 4     | .99  | .04 | .03  | 1         | 89     |
| 16 L948 105+25N | 3   | 11  | 12   | 46  | .3   | 1   | 9   | 2871  | 3.94  | 11  | 5   | 2     | 1   | 9   | .3   | 3   | 2          | 46  | .10  | .099 | 9   | 18  | .19  | 43  | .06 | 4     | 1.18 | .05 | .05  | 1         | 4      |
| 16 L948 105+00N | 4   | 64  | 25   | 222 | .6   | 37  | 16  | 1612  | 8.59  | 24  | 5   | 2     | 1   | 7   | .5   | 2   | 2          | 61  | .13  | .115 | 9   | 58  | .65  | 47  | .05 | 2     | 2.39 | .02 | .03  | 1         | 10     |
| 16 L94E 104+75N | 2   | 32  | 11   | 203 | 1.2  | 71  | 24  | 3742  | 9.48  | 18  | 5   | 2     | 2   | 4   | 4.0  | 3   | 2          | 82  | .26  | .068 | 20  | 192 | .22  | 55  | .04 | 3     | 7.53 | .01 | .01  | 1         | 5      |
| 16 L94B 104+50N | 5   | 60  | 30   | 246 | .5   | 112 | 27  | 6259  | 8.28  | 39  | 5   | 2     | 1   | 10  | 2.5  | 4   | 2          | 81  | .40  | .046 | 29  | 106 | .54  | 178 | .04 | 3     | 4.03 | .01 | .03  | 2         | 31     |
| 16 L94E 104+25N | 3   | 21  | . 20 | 392 | .4   | 33  | 14  | 1645  | 7.75  | 24  | 5   | 2     | 1   | 15  | 2.4  | 3   | 2          | 75  | 1.52 | .068 | 13  | 100 | .59  | 96  | .05 | 3     | 4.01 | .01 | .02  | 1         | 8      |
| 16 L94E 104+00N | 5   | 43  | 34   | 323 | .1.1 | 83  | 20  | 8367  | 10.47 | 57  | 5   | 2     | 1   | 18  | 5.8  | 4   | 2          | 70  | 1,87 | .089 | 23  | 137 | .99  | 177 | .02 | 3     | 2.33 | .01 | .03  | 1         | 9      |
| 16 L94E 103+75N | 4   | 29  | 94   | 185 | .4   | 11  | 10  | 2289  | 7.26  | 102 | 5   | 2     | 1   | 5   | .2   | 4   | 2          | 66  | .12  | .078 | 6   | 18  | ,11  | 44  | .03 | 2     | .90  | .01 | .03  | 1         | 44     |
| 16 L94E 103+50N | 3   | 45  | 43   | 128 | .7   | 15  | 14  | 906   | 9.92  | 119 | 5   | 2     | 1   | 5   | .8   | 4   | 2          | 105 | .08  | .049 | 1   | 48  | .23  | 117 | .02 | 5     | 2.96 | .01 | .02  | 1         | 27     |

A CONTRACTOR OF A CO

|                                  | Mo  | Cu       | Pb  | 2 n  | Ag  | Ni  | Co  | Mn    | Fe   | As   | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca     | P          | La  | Cr  | Ka   | Ba   | Ti           | B               | Al   | Na  | K   | W          | An* |
|----------------------------------|-----|----------|-----|------|-----|-----|-----|-------|------|------|-----|-----|-----|-----|------|-----|-----|-----|--------|------------|-----|-----|------|------|--------------|-----------------|------|-----|-----|------------|-----|
| Sample 🛊                         | ppm | ₽₽₽      | ppm | ppm  | pp∎ | ppm | ppm | ppn   | ş    | ppn  | ppn | ppm | ppn | ppm | ppm  | ppn | ppm | ppm | ş      | ۶          | ppm | ppm | į    | ррв  | ۶            | ppm             | ł    | ł   | 1   |            | daa |
| 16 L94E 103+25N                  | 6   | 28       | 20  | 130  | 1.0 | 22  | 10  | 515   | 6.57 | 35   | 5   | 2   | 1   | 9   | ,9   | 2   | 2   | 83  | .14 .  | 076        | 8   | 44  | .39  | 50   | .08          | <sup>••</sup> 2 | 1.94 | .03 | .04 | 1          | 1   |
| 16 L94E 103+00N                  | 3   | 56       | 11  | 81   | 1.0 | 5   | 11  | 2151  | 5.15 | 38   | 5   | 2   | 1   | 22  | .2   | 2   | 2   | 49  | .30 .  | 188        | 4   | 8   | .48  | 75   | .01          | 3               | 1.72 | .01 | .08 | 1          | 39  |
| 16 L948 102+75N                  | 4   | 16       | 14  | 51   | • 6 | 7   | 4   | 180   | 2.61 | 9    | 5   | 2   | 1   | 15  | .8   | 2   | 2   | 60  | .10 .  | 040        | 9   | 19  | .15  | 32   | .15          | 4               | 1.39 | .02 | .03 | 1          | 10  |
| 16 L94E 102+50N                  | 3   | 16       | 18  | 186  | .4  | 17  | 9   | 12699 | 5.35 | 11   | 5   | 2   | 1   | 16  | 3.8  | 2   | 2   | 81  | 1.20 . | 880        | 29  | 18  | .15  | 340  | .06          | 2               | 2.70 | .03 | .04 | ĩ          | 1   |
| 16 L948 102+25N                  | 1   | 251      | 11  | 308  | 1.9 | 13  | 9   | 10394 | 6.49 | - 74 | 5   | 2   | 1   | 24  | 2.6  | 16  | 2   | 21  | 2.05 . | 255        | 43  | 12  | .17  | 340  | .02          | 2               | 1.74 | .03 | .05 | 1          | 22  |
| 16 L94B 102+00N                  | 1   | 18       | 2   | 798  | 1.0 | 18  | 13  | 1420  | 6.90 | 19   | 5   | 2   | 1   | 13  | 9.4  | 2   | 2   | 39  | 1.39 . | 099        | 28  | 20  | .11  | 274  | .02          | 4               | 2.51 | .01 | .05 | 1          | 5   |
| 16 L94B 101+75N                  | 1   | 30       | 3   | 1462 | 4.3 | 34  | 11  | 7115  | 7.32 | 48   | 5   | 2   | 1   | 25  | 19.9 | 2   | 2   | 64  | 1.98 . | 154        | 65  | 24  | .26  | 1932 | .02          | 2               | 2.75 | .01 | .03 | 1          | 1   |
| 16 L94E 101+50N                  | 11  | 46       | 7   | 110  | 2.4 | 14  | 8   | 429   | 6.23 | 60   | 5   | 2   | 1   | 1   | 1.8  | 2   | 2   | 96  | .17 .  | 169        | 12  | 20  | .10  | 149  | .03          | 3               | .87  | .01 | .04 | 1          | 4   |
| 16 L94E 101+25N                  | 4   | 39       | 19  | 99   | .5  | 26  | 12  | 1119  | 9.96 | 24   | 9   | 2   | 3   | 6   | 3.2  | 2   | 2   | 105 | .10 .  | 109        | 12  | 59  | .31  | 63   | .05          | 3               | 3.07 | .01 | .03 | 1          | 10  |
| 16 L94E 101+00N                  | 11  | 40       | 22  | 270  | .8  | 29  | 16  | 3725  | 8.13 | 93   | 5   | 2   | 2   | 7   | 1.3  | 2   | 2   | 54  | .11 .  | 138        | 16  | 37  | .22  | 131  | .02          | 2               | 2.37 | .01 | .03 | 1          | 9   |
| 16 L94E 100+75N                  | 2   | 7        | 5   | 32   | .4  | 8   | 1   | 137   | 1.32 | 2    | 5   | 2   | 1   | 11  | .2   | 2   | 2   | 33  | .12 .  | 062        | 1   | 14  | .07  | 28   | .06          | 2               | .76  | .02 | .03 | 1          | 10  |
| 16 L94E 100+50N                  | 2   | 28       | 3   | 68   | .2  | 23  | 4   | 179   | 2.25 | 5    | 5   | 2   | 1   | 12  | .2   | 2   | 2   | 48  | .17 .  | 063        | 6   | 31  | .47  | 37   | .05          | 3               | 1.37 | .02 | .03 | 1          | 12  |
| 16 L948 100+25N                  | 3   | 42       | 9   | 69   | .1  | 31  | 8   | 214   | 6.42 | 24   | 5   | 2   | 2   | 10  | 1.5  | 2   | 2   | 105 | .16 .  | 047        | 11  | 75  | .46  | 36   | .08          | 2               | 2.28 | .01 | .02 | 1          | 9   |
| 16 L94E 99+75N                   | 3   | 39       | 2   | 62   | 1.4 | 29  | 5   | 495   | 2.94 | 8    | 5   | 2   | 1   | 11  | .6   | 2   | 3   | 48  | .59 .  | 101        | 12  | 75  | .47  | 61   | .03          | 8               | 1.84 | .01 | .03 | 1          | 5   |
| 16 L94E 99+50N                   | 4   | 61       | 8   | 86   | .1  | 65  | 10  | 265   | 6.91 | 33   | 5   | 2   | 1   | 8   | .4   | 3   | 2   | 101 | .26 .  | 116        | 8   | 120 | .74  | 50   | .07          | 2               | 2.66 | .01 | .03 | 1          | 14  |
| 16 L94E 99+25N                   | 4   | 16       | 11  | 61   | .5  | 20  | 4   | 254   | 2.11 | 5    | 5   | 2   | 1   | 10  | .2   | 2   | 2   | 41  | .16 .  | 049        | 9   | 38  | .24  | 62   | .05          | 4               | 1.11 | .02 | .04 | ì          | 18  |
| 16 L948 99+00N                   | 4   | 64       | 18  | 60   | .8  | 124 | 13  | 186   | 8.42 | 14   | 5   | 2   | 3   | 6   | 2.0  | 2   | 3   | 210 | .23 .  | 096        | 11  | 333 | 1.44 | 38   | .25          | 4               | 2.87 | .01 | .07 | 2          | 5   |
| 16 L94E 98+75N                   | 3   | -102     | 7   | 187  | .9  | 168 | 19  | 666   | 6.45 | 19   | 8   | 2   | 2   | ŝ   | •2   | 3   | 4   | 85  | .19 .  | 071        | 8   | 152 | 1.84 | 77   | .06          | 3               | 2.79 | .01 | .06 | 1          | 23  |
| 16 L94E 98+50N                   | 3   | 49       | 14  | 161  | .8  | 75  | 11  | 513   | 6.14 | 26   | 6   | 2   | 1   | 9   | 1.6  | 2   | 2   | 78  | .12 .  | 064        | 9   | 83  | .83  | 60   | .02          | 2               | 2.34 | .01 | .04 | 1          | 12  |
| 16 L94E 98+25N                   | 3   | 29       | 11  | 79   | . 4 | 35  | 7   | 178   | 6.10 | 14   | 5   | 2   | 2   | 7   | .1   | 2   | 2   | 133 | .08 .  | 039        | 19  | 53  | .41  | 44   | .05          | 2               | 2.31 | .01 | .02 | 1          | 10  |
| 16 L948 98+DON                   | 2   | 100      | 4   | 380  | .6  | 145 | 18  | 1731  | 4.56 | 59   | 5   | 2   | 1   | 50  | 2.6  | 3   | 2   | 108 | 1.45 . | 102        | 10  | 99  | 1.42 | 167  | .02          | 5               | 2.15 | .01 | .06 | 1          | 14  |
| 16 L94E 97+75N                   | 3   | 27       | ì   | 101  | .6  | 26  | 7   | 578   | 3.45 | 18   | 5   | 2   | I   | 12  | • 2  | 2   | 2   | 55  | .17 .  | 986        | 7   | 58  | .22  | 96   | .05          | 4               | 1.28 | .01 | .04 | 1          | 14  |
| 15 L948 97+50N                   | 2   | 155      | 23  | 192  | 1.0 | 113 | 8   | 1781  | 3.47 | 12   | 5   | 2   | 1   | 26  | 3.4  | 2   | 4   | 46  | 1.66 . | 178        | 38  | 176 | .43  | 170  | .04          | 6               | 1.95 | .03 | .05 | 1          | 10  |
| 16 L94E 97+25N                   | 4   | 55       | 2   | 47   | 1.2 | 7   | 4   | 151   | 1.88 | 3    | 5   | 2   | 1   | 7   | .2   | 2   | 2   | 35  | .18 .  | 148        | 9   | 16  | .10  | 114  | .01          | 7               | .78  | .01 | .05 | 1          | 20  |
| 15 L94E 97+00N                   | 3   | 12       | 2   | 35   | 1.0 | 6   | 3   | 100   | 2.24 | 2    | 5   | 2   | 1   | 7   | .2   | 2   | 2   | 70  | .08 .  | 042        | 9   | 14  | .10  | 47   | .02          | 5               | 1.35 | .01 | .03 | 1          | 13  |
| 16 L95E 99+75N                   | 6   | 39       | 13  | 127  | 1.3 | 80  | 11  | 401   | 8.17 | 49   | 5   | 2   | 2   | 8   | .2   | 2   | 2   | 101 | .12 .  | 093        | 9   | 299 | .68  | 60   | .06          | 4               | 2.23 | .01 | .03 | 2          | 65  |
| 16 L958 99+50N                   | 3   | 18       | Щ   | 58   | .4  | 119 | 16  | 1950  | 3.00 | 13   | 5   | 2   | 1   | 19  | •2   | 2   | 2   | 60  | .28 .  | 080        | 7   | 179 | .73  | 76   | .05          | 2               | 1.07 | .03 | .04 | 1          | 1   |
| 16 L95E 99+25N                   | 2   | 23       | 6   | 61   | .5  | 316 | 38  | 3342  | 3.82 | 4    | 5   | 2   | 1   | 14  | •2   | 2   | 3   | 82  | .40 .  | 115        | 3   | 350 | 4.02 | 90   | .07          | 5               | 1.80 | .03 | .05 | 1          | 4   |
| 15 L95E 99+00N                   | 4   | 30       | 6   | 125  | •2  | 443 | 85  | 2536  | 7.12 | y    | 5   | 2   | 1   | 34  | .5   | 2   | 5   | 139 | 1.26 . | 142        | 4   | 354 | 4.50 | 73   | .05          | 7               | 2.34 | .02 | .02 | 1          | 22  |
| 16 L958 98+50N                   | 2   | 66       | 2   | 125  | .1  | 755 | 54  | 685   | 5.53 | b    | 5   | 2   | 1   | 34  | •2   | 2   | 2   | 86  | .67 .  | 067        | 4   | 259 | 8.63 | 54   | .06          | 4               | 3.90 | .02 | .04 | 1          | 4   |
| 15 L95E 98+25N                   | 2   |          | 6   | 52   | 1./ | 19  | 2   | 1/0   | 1,94 | 2    | 5   | 2   | 1   | 1   | - 7  | 2   | 2   | 22  | .19 .  | 036        | 16  | 15  | .24  | 68   | .12          | 4               | 1.22 | .15 | .10 | 2          | 2   |
| 16 L95E 98+00N                   | 3   | 45       | 5   | 47   | .4  | 15  | 1   | 285   | 2.92 | 4    | 5   | 2   | 1   | 1   | .2   | 2   | 2   | 63  | .12 .  | 063        | 10  | 16  | .63  | 66   | .01          | 6               | 1.70 | .04 | .12 | 1          | 17  |
| 16 L95E 97+75N                   | 5   | 31       | 15  | 16   | , b | 11  | b   | 290   | 7.62 | 28   | 5   | 2   | 2   | 9   | .2   | 2   | 2   | 128 | .10 .  | 050        | 18  | 28  | .39  | 64   | .08          | 2               | 2.13 | .01 | .05 | 1          | 13  |
| 16 L95E 97+50N                   | y   | 11       | 19  | 505  | 2.1 | 21  | 11  | 2296  | 5.88 | 26   | 6   | 1   | 1   | 81  | .2   | 2   | 2   | 81  | .46 .  | 154        | 24  | 57  | .33  | 106  | .06          | 3               | 3.32 | .01 | .04 | 1          | 14  |
| 16 L95K 9/+25N                   | 6   | 15       | 1/  | 670  | 2.0 | 37  | 10  | 3039  | 4.97 | 16   | 5   | 2   | 1   | 31  | 2.1  | 2   | 2   | 60  | 1.13 . | 104        | 19  | 51  | .43  | 247  | .04          | 3               | 3.01 | .02 | .04 | 1          | 15  |
| TO PADE 04-324                   | 4   | 53       | 31  | 287  | . 9 | 52  | 12  | /16   | 1.28 | 31   | 5   | 2   | 1   | 11  | .2   | 2   | 2   | 91  | .26 .  | 981<br>107 | 8   | 12  | .82  | 55   | .07          | 3               | 2.19 | .03 | .04 | 1          | 18  |
| 10 1958 964/5N                   | 3   | 145      | 1/  | 1254 | •1  | 60  | 17  | 5//5  | 5.55 | 31   | 5   | 2   | 1   | 22  | 0.3  | 2   | 2   | 65  | 1.40   | 194        | 24  | 80  | -54  | 385  | .04          | 3               | 2.25 | .02 | .05 | . 1        | 3   |
| 10 FADR ACTORN<br>10 FADR GCTORN | 2   | 35       | 21  | 550  | •4  | jl  | (   | 1000  | 3.43 | 10   | 5   | 2   | l   | 32  | 5.1  | 2   | 2   | 29  | 4.05 . | 131        | 21  | 26  | .73  | 144  | .93          | 4               | 1.82 | .02 | .04 | 1          | 3t  |
| 16 L908 96+20N                   | j   | 34<br>25 | 14  | 123  | 11  | 27  |     | 202   | 0.80 | 27   | 2   | 4   | 1   | 11  |      | 2   | 2   | 114 | .43 .  | 028        | 11  | 55  | • 41 | 55   | .05          | 2               | 2.65 | .01 | .02 | . <u>]</u> | 57  |
| 10 PADR AP+A6M                   | 5   | 25       | 31  | 404  | ډ.  | 15  | 12  | 928   | 1.27 | 19   | 5   | 1   | 2   | 14  | ••   | 7   | - 2 | 121 | .42 .  | U4U        | 10  | 51  | .20  | tž   | , J <i>T</i> | 4               | 3.20 | .01 | .03 | Ţ          | 25  |

:

**1 1 1** 

1

j

|                 | Mo  | Cu  | Pb  | Zn  | Ag  | Ni         | Co  | Mn   | Fe    | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | Гз  | Cr  | Mg   | Ba   | Ti  | В   | Al   | Na  | K   | W   | Au <sup>±</sup> |  |
|-----------------|-----|-----|-----|-----|-----|------------|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|------|-----|-----|------|-----|-----|-----|-----------------|--|
| Sample 🖡        | ppm | ppm | ppa | ppm | pp⊪ | ppm        | ppn | ppm  | ł     | ppm | pp∎ | ppn | pp∎ | ppm | ppm  | ppn | ppm | ppm | 2    | ş    | ppm | ppm | ł    | pp∎  | \$  | ppn | ş    | ş   | \$  | ppm | ppb .           |  |
| 16 L95E 95+75N  | 3   | 10  | 13  | 145 | .2  | 14         | 12  | 1321 | 7.56  | 9   | 5   | 2   | 2   | 4   | .9   | 2   | 2   | 46  | .23  | .051 | 13  | 13  | .33  | 172  | .02 | 3   | 2.85 | .01 | .02 | 1   | 3               |  |
| 16 L95E 95+50N  | 4   | 17  | 21  | 173 | .1  | 12         | 8   | 369  | 6.16  | 20  | 5   | 2   | 3   | 8   | . 2  | 2   | 2   | 121 | -19  | .024 | 16  | 39  | .29  | 52   | .11 | 2   | 3.34 | .01 | .02 | 1   | 13              |  |
| 16 L95E 95+25N  | 2   | 9   | 13  | 201 | .2  | 10         | 4   | 1138 | 2.87  | 8   | 5   | 2   | 1   | 15  | .5   | 2   | 2   | 32  | 1.21 | .098 | 20  | 16  | .18  | 82   | .11 | 3   | 1.80 | .10 | .07 | 1   | 4               |  |
| 16 L958 95+00N  | 4   | 17  | 15  | 121 | .2  | 12         | 6   | 285  | 7.28  | 16  | 5   | 2   | 2   | 9   | .3   | 2   | 3   | 86  | .16  | .063 | 13  | 40  | .18  | 83   | .06 | 2   | 2.34 | .01 | .02 | 1   | 11              |  |
| 16 L958 104+25N | 22  | 456 | 49  | 877 | .7  | 67         | 60  | 2666 | 14.79 | 84  | 5   | 2   | 1   | 19  | 13.7 | 2   | 2   | 76  | .70  | .103 | 48  | 10  | 1.56 | 515  | .04 | 33  | 2.04 | .01 | .07 | 1   | 280             |  |
| 16 L95E 104+00N | 19  | 138 | 37  | 205 | .9  | 34         | 24  | 2095 | 7.79  | 65  | 5   | 2   | 1   | 20  | 1.4  | 3   | 2   | 173 | .87  | .170 | 13  | 16  | .60  | 668  | .02 | 5   | 2.14 | .01 | .05 | 1   | 141             |  |
| 16 L95E 103+75N | 25  | 67  | 19  | 125 | .1  | 31         | 10  | 866  | 7.01  | 76  | 5   | 2   | 1   | 7   | .2   | 4   | 2   | 121 | .30  | .114 | 9   | 57  | .21  | 233  | .01 | 2   | 1.86 | .01 | .04 | 1   | 38              |  |
| 16 L95E 103+50N | 4   | 57  | 26  | 373 | .5  | 37         | 11  | 3139 | 5.00  | 42  | 5   | 2   | 1   | 28  | 4.2  | 2   | 2   | 83  | 4.01 | .183 | 33  | 25  | .21  | 283  | .03 | 3   | 1.52 | .01 | .06 | 1   | 15              |  |
| 16 L95B 103+25N | 12  | 58  | 12  | 121 | .9  | 65         | 8   | 616  | 2.82  | 27  | 5   | 2   | 1   | 18  | • 2  | 2   | 2   | 98  | .56  | .211 | 4   | 170 | .63  | 528  | .03 | 5   | .90  | .01 | .04 | 1   | 4               |  |
| 16 L95E 103+00N | 15  | 23  | 14  | 42  | 1.9 | 14         | 5   | 115  | 2.48  | 12  | 5   | 2   | · 1 | 8   | .2   | 2   | 2   | 77  | .19  | .139 | 14  | 21  | .05  | 210  | .07 | 2   | .87  | .02 | .04 | 1   | 34              |  |
| 16 L95B 102+75N | 3   | 13  | 11  | 25  | 2.5 | 5          | 2   | 79   | 1.69  | 14  | 7   | 2   | 1   | 10  | .2   | 2   | 2   | 25  | .15  | .142 | 1   | 10  | .06  | 50   | .03 | 2   | 1.13 | .03 | .05 | 1   | 13              |  |
| 16 L95E 102+50N | 2   | 15  | 16  | 23  | .8  | 3          | 1   | 34   | .75   | 2   | 5   | 2   | 1   | 14  | .2   | 2   | 2   | 19  | .11  | .065 | 7   | 9   | .04  | 29   | .02 | 3   | 1.28 | .01 | .03 | 2   | 30              |  |
| 16 L95E 102+25N | 3   | 32  | 12  | 39  | 2.1 | 5          | 4   | 199  | 4.24  | 10  | 5   | 2   | I   | 7   | .2   | 2   | 2   | 64  | .15  | .168 | 12  | 15  | .17  | 32   | .04 | 4   | 2.15 | .01 | .05 | 1   | 6               |  |
| 16 L95E 102+00N | 4   | 24  | 18  | 66  | .5  | 6          | 4   | 245  | 4.24  | 64  | 6   | 2   | 1   | 7   | .2   | 3   | 2   | 88  | .08  | .095 | 7   | 13  | .17  | 30   | .04 | 4   | 1.65 | .02 | .05 | 1   | 3               |  |
| 16 L95E 101+75N | 2   | 28  | 28  | 60  | 2.6 | 6          | 7   | 626  | 6.99  | 243 | 5   | 2   | 2   | 5   | .2   | 5   | 3   | 68  | .07  | .211 | 6   | 16  | .14  | 58   | .02 | 2   | 2.29 | .01 | .07 | 1   | 22              |  |
| 16 L95E 101+50N | 8   | 83  | 21  | 67  | .8  | 13         | 11  | 349  | 8.46  | 68  | 5   | 2   | 1   | £   | .2   | 3   | 2   | 81  | .15  | .276 | 9   | 79  | .08  | 73   | .02 | 4   | 1.87 | .01 | .04 | I   | 28              |  |
| 16 L95E 101+25N | 5   | 50  | 11  | 215 | .9  | 18         | 7   | 2212 | 3.25  | 11  | 5   | 2   | 1   | 32  | 3.4  | 2   | 2   | 35  | 1.67 | .143 | 21  | 28  | .21  | 274  | .05 | 7   | 2.01 | .06 | .06 | 1   | 12              |  |
| 16 L95E 101+00N | 2   | 79  | 13  | 121 | .5  | 22         | 14  | 824  | 8.91  | 57  | 5   | 2   | 2   | ŧ   | .2   | 2   | 2   | 89  | .12  | .149 | 3   | 13  | .09  | 52   | .01 | 2   | .88  | .01 | .07 | 1   | 13              |  |
| 16 L95E 100+75N | 5   | 43  | 34  | 100 | 1.7 | 32         | 10  | 859  | 6.87  | 47  | 5   | 2   | 1   | 6   | • 2  | 2   | 2   | 70  | .09  | .142 | 6   | 40  | .38  | 54   | .03 | 2   | 1.49 | .01 | .05 | 1   | 12              |  |
| 16 L95E 100+50N | 17  | 63  | 19  | 271 | .5  | 205        | 26  | 2128 | 6.82  | 172 | 5   | 2   | 1   | t - | .2   | 3   | 2   | 108 | .19  | .197 | 5   | 176 | .13  | 113  | .01 | 2   | 1.15 | .01 | .06 | 1   | 11              |  |
| 16 L95E 100+25N | 7   | 40  | 51  | 90  | 1.5 | 11         | 5   | 528  | 7.18  | 42  | 6   | 2   | t   | 5   | .2   | 2   | 2   | 65  | .04  | .144 | 13  | 35  | .23  | 65   | .05 | 2   | 1,43 | .02 | .05 | 1   | 9               |  |
| 16 L96E 104+00N | 82  | 238 | 37  | 233 | 3.1 | 7 <u>2</u> | 31  | 2102 | 20.91 | 205 | 11  | 2   | 2   | 21  | 5.0  | 2   | 2   | 226 | .93  | .084 | 14  | 7   | .12  | 205  | .01 | 2   | .38  | .01 | .05 | 1   | 81              |  |
| 16 L96E 103+75N | 30  | 80  | 2£  | 158 | .9  | 22         | 12  | 1823 | 4.41  | 41  | 5   | 2   | 1   | 35  | .2   | 2   | 2   | 64  | 1.09 | .229 | 6   | 8   | .28  | 620  | ,01 | 13  | .54  | .01 | .04 | 1   | 50              |  |
| 16 L96E 103+50N | 7   | 31  | ć   | 59  | .2  | 11         | 3   | 136  | 1.55  | 8   | 5   | 2   | i   | 15  | .2   | 2   | 2   | 30  | .57  | .076 | 4   | 7   | .05  | 585  | .05 | 4   | .49  | .01 | .02 | I   | 26              |  |
| 16 L96E 103+25N | 22  | 47  | 6   | 30  | 2.0 | 14         | 4   | 176  | 2.05  | 18  | 5   | 2   | 1   | 7   | • 2  | 2   | 2   | 44  | .36  | .141 | 7   | 7   | .05  | 158  | .02 | 5   | .44  | .01 | .03 | 1   | 11              |  |
| 16 L96E 103+00N | 3   | 36  | 8   | 53  | 5.5 | 13         | 2   | 157  | .66   | 2   | 5   | 2   | 1   | 9   | . 2  | 2   | 2   | 12  | .28  | .098 | 3   | 12  | .06  | 46   | .03 | 7   | .30  | .01 | .03 | 1   | 5               |  |
| 16 L96E 102+75N | 3   | 69  | 11  | 164 | .2  | 29         | 23  | 3865 | 5.04  | 19  | 5   | 2   | 1   | 19  | 1.0  | 2   | 2   | 55  | .84  | .394 | 8   | 25  | .71  | 229  | .01 | 2   | 3.68 | .01 | .11 | 1   | 12              |  |
| 16 L96E 102+50N | 5   | 80  | 17  | 73  | .9  | 21         | 9   | 623  | 6.18  | 46  | 5   | 2   | 1   | 14  | .4   | 2   | 2   | 62  | .16  | .175 | 6   | 26  | .32  | 62   | .01 | 2   | 2.71 | .01 | .04 | 1   | 44              |  |
| 16 L968 102+25N | 27  | 158 | 24  | 344 | 1.2 | 73         | 25  | 2741 | 7.96  | 94  | 5   | 2   | 1   | 21  | 2.8  | 2   | 2   | 96  | .64  | .170 | 20  | 62  | .57  | 383  | .01 | 2   | 1.46 | .01 | .05 | 1   | 10              |  |
| 16 L96E 102+00N | 3   | 22  | 18  | 56  | .3  | 6          | 5   | 556  | 2.45  | 11  | 5   | 2   | 1   | 14  | .2   | 2   | 2   | 43  | .39  | .138 | 5   | 10  | .17  | 86   | .01 | 4   | 1.25 | .02 | .06 | 1   | 6               |  |
| 16 L96E 101+75N | 2   | 63  | 14  | 87  | .1  | 8          | 11  | 1660 | 5.56  | 7   | 5   | 2   | 1   | 27  | .5   | 2   | 2   | 79  | .36  | .243 | 4   | 14  | .49  | 135  | .01 | 4   | 1,98 | .01 | .07 | 1   | 26              |  |
| 16 L968 101+50N | 5   | 41  | 8   | 263 | .7  | 24         | 10  | 769  | 5.31  | 40  | 5   | 2   | 1   | 7   | .3   | 2   | 2   | 48  | .09  | .196 | 6   | 47  | .34  | 60   | .01 | 4   | 1.99 | .01 | .05 | 1   | 14              |  |
| 16 L96E 101+25N | 30  | 40  | 13  | 99  | .9  | 22         | 19  | 947  | 11.36 | 181 | 5   | 2   | 1   | 8   | .4   | 3   | 2   | 34  | .37  | .210 | 6   | 7   | .06  | 89   | .01 | 2   | •23  | .01 | .04 | 2   | 35              |  |
| 16 L96B 101+00N | 69  | 216 | 46  | 229 | 1.7 | 64         | 23  | 1499 | 8.49  | 116 | 7   | 2   | 1   | 26  | 1.8  | 2   | 2   | 134 | .70  | .241 | 22  | 33  | .86  | 154  | .01 | 2   | 1.33 | .01 | .03 | 1   | 14              |  |
| 16 L96B 100+75N | 21  | 237 | 25  | 602 | •9  | 35         | 28  | 1004 | 12.33 | 91  | 5   | 2   | 1   | 5   | 2.9  | 2   | 2   | 40  | .09  | .109 | 14  | 8   | .48  | 132  | .01 | 3   | 1.29 | .01 | .02 | 1   | 21              |  |
| 16 L96E 100+50N | 81  | 119 | 19  | 502 | 1.3 | 68         | 20  | 1894 | 8.75  | 154 | 5   | 2   | 2   | 18  | 3.6  | 3   | 2   | 156 | .19  | .322 | 30  | 18  | 1.01 | 578  | .01 | 2   | 2.07 | .01 | .04 | 1   | 6               |  |
| 16 L96B 100+25N | 103 | 232 | 50  | 961 | 8.5 | 316        | 42  | 3656 | 7.16  | 155 | 14  | 2   | 2   | 147 | 12.5 | 9   | 2   | 310 | .85  | .308 | 17  | 20  | .31  | 1573 | .01 | 2   | .94  | .01 | .07 | 1   | 14              |  |
| 16 L96E 99+75N  | 3   | 715 | 19  | 78  | 1.0 | 20         | 57  | 2664 | 4.59  | 35  | 5   | 2   | 1   | 14  | .2   | 2   | 3   | 22  | .59  | .089 | 25  | 12  | .61  | 339  | .01 | 2   | 1.41 | .01 | .09 | 4   | 123             |  |
| 16 L96E 99+50N  | 3   | 75  | 10  | 48  | 1.0 | 16         | 14  | 465  | 5.37  | 15  | 5   | 2   | 1   | 6   | .2   | 3   | 2   | 93  | .16  | .057 | 6   | 60  | .23  | 41   | .07 | 2   | 1.65 | .01 | .02 | 3   | 44              |  |
| 16 L96B 99+25N  | i   | 6   | 2   | 21  | .3  | 1          | 2   | 76   | •93   | 2   | 5   | 2   | 1   | 3   | .2   | 2   | 2   | 18  | .04  | .038 | 6   | 11  | .03  | 11   | .05 | 3   | .33  | .04 | .04 | 1   | 35              |  |

1

ł

يصد وفكركم بري
|                 | Mo  | Cu   | Pb  | 2 n | Ag  | Ni  | Co  | Mn   | Fe    | As  | D   | Au  | Th  | Sr         | Cd    | Sb  | Bi    | V    | Ca       | ) La | Cr  | Mq   | Ba   | Ti  | B   | Al   | Na  | ĸ   | ¥   | An * |
|-----------------|-----|------|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|------------|-------|-----|-------|------|----------|------|-----|------|------|-----|-----|------|-----|-----|-----|------|
| Sample 🖡        | ppm | ppn  | ppm | ppm | ppn | ppn | ppm | ppn  | 2     | pp∎ | ppm | ppm | ppm | ppm        | ppn g | opp | ppm   | ppm  | ş        | ppm  | ppp | į    | DDB  | ł   | וממ | 2    | ş   | ş   | הממ | nnh  |
| 16 L96B 99+00N  | 4   | 40   | 32  | 46  | 1.7 | 5   | 3   | 58   | 4.18  | 14  | 5   | 2   | 2   | 6          | .2    | 2   | ··· 2 | 94   | .05 .04  | 12   | 34  | .04  | 39   | .08 | 5   | 1.69 | .01 | .02 | 1   | 11   |
| 16 L96B 98+75N  | 1   | 13   | 10  | 32  | 3.0 | 5   | 2   | 74   | .76   | 2   | 5   | 2   | 1   | 8          | .2    | 2   | 2     | 10   | .09 .04  | ) 11 | 7   | .02  | 46   | .05 | 6   | .62  | .04 | .03 | 1   | 13   |
| 16 L96E 98+50N  | 4   | 26   | 6   | 104 | 2.2 | 16  | 8   | 431  | 5.48  | 16  | 5   | 2   | 2   | 8          | .2    | 2   | 2     | 86   | .07 .08  | 9    | 30  | .28  | 51   | .04 | 2   | 1.68 | .01 | .03 | 1   | 63   |
| 16 L96E 98+25N  | 2   | 38   | 8   | 102 | .6  | 22  | 7   | 190  | 5.39  | 14  | 5   | 2   | 1   | 10         | .2    | 2   | 6     | 97   | .16 .04  | i 6  | 49  | .38  | 41   | .07 | 2   | 2.14 | .01 | .02 | 1   | 38   |
| 16 L96E 98+00N  | 4   | 36   | 14  | 78  | 1.9 | 14  | 6   | 167  | 3.74  | 10  | 5   | 2   | 1   | 10         | .2    | 2   | 3     | 75   | .15 .04  | 2 8  | 36  | .27  | 42   | .08 | 2   | 1.44 | .01 | .02 | 1   | 33   |
| 16 L968 97+75N  | 5   | 45   | 7   | 70  | .7  | 98  | 14  | 745  | 5.58  | 3   | 5   | 2   | 2   | 7          | .6    | 2   | 2     | 123  | .10 .05  | 13   | 126 | .53  | 81   | .06 | 2   | 1.58 | .02 | .02 | 1   | 11   |
| 16 L96E 97+50N  | 5   | 58   | 2   | 162 | .9  | 28  | 9   | 423  | 5.46  | 17  | 5   | 2   | 1   | 9          | .2    | 2   | 2     | 60   | .12 .22  | 58   | 44  | .33  | 47   | .02 | 2   | 1.66 | .01 | .02 | 1   | 21   |
| 16 L96E 97+25N  | 3   | 57   | 2   | 261 | .7  | 49  | 12  | 756  | 4.75  | 23  | 5   | 2   | 1   | 11         | 1.8   | 2   | 2     | 53   | .45 .08  | 5 8  | 48  | .71  | 50   | .03 | 2   | 2.51 | .01 | .02 | 1   | 21   |
| 16 L96B 97+00N  | 6   | 30   | 9   | 137 | .6  | 50  | 20  | 4635 | 8.38  | 159 | 5   | 2   | 1   | 36         | 3.1   | 2   | 2     | 36   | 2.93 .11 | 24   | 15  | .23  | 1370 | .01 | 2   | 1.42 | .01 | .03 | 1   | 9    |
| 16 L96B 96+75N  | 2   | 27   | 17  | 151 | .3  | 51  | 18  | 9181 | 5.31  | 39  | 5   | 2   | 1   | 35         | 3.7   | 2   | 2     | 35   | 3.33.10  | 27   | 21  | .30  | 252  | .02 | 4   | 1.57 | .01 | .03 | 1   | 3    |
| 16 L968 96+50N  | 2   | 17   | 18  | 91  | .1  | 13  | 4   | 521  | 2.57  | 22  | 5   | 2   | 1   | 15         | .2    | 2   | 3     | 49   | 1.57 .04 | 5 8  | 13  | .05  | 60   | .04 | 2   | .76  | .01 | .02 | 1   | 8    |
| 16 L96E 96+25N  | 2   | 11   | 14  | 69  | .1  | 11  | 3   | 288  | 1.62  | 7   | 5   | 2   | 1   | <u>1</u> 7 | .2    | 2   | 2     | 11   | 1.32 .08 | 10   | 4   | .04  | 110  | .01 | 2   | .43  | .01 | .05 | 1   | 2    |
| 16 L968 96+00N  | 1   | 10   | 2   | 64  | .1  | 2   | 1   | 20   | .28   | 2   | 5   | 2   | 1   | 24         | 1.1   | 2   | 2     | 5    | 4.23 .06 | 5 2  | 4   | .02  | 66   | .01 | 4   | .16  | .01 | .02 | 1   | 1    |
| 16 L97E 103+75N | 6   | 89   | 23  | 197 | .6  | 16  | 25  | 3861 | 5.29  | 71  | 5   | 2   | 1   | 54         | .8    | 3   | 2     | 21   | 3.13 .17 | 32   | 8   | .48  | 222  | .01 | 6   | 1.12 | .01 | .05 | 1   | 21   |
| 16 L97E 103+50N | 9   | 51   | 40  | 151 | 1.3 | 11  | 20  | 2895 | 8.73  | 200 | 5   | 2   | 1   | 12         | .5    | 4   | 2     | 22   | .58 .15  | ) 14 | 10  | .38  | 123  | .01 | 2   | 1.11 | .01 | .04 | 1   | 64   |
| 16 6978 103+25N | 6   | 37   | 105 | 154 | .6  | 11  | 11  | 2142 | 7.01  | 111 | 5   | 2   | 1   | 7          | .2    | 2   | 2     | 34   | .26 .15  | 3 11 | 14  | .43  | 91   | .01 | 2   | 1.80 | .01 | .04 | 1   | 22   |
| 16 L97E 103+00N | 3   | 28   | 17  | 52  | .5  | 72  | 9   | 371  | 3.58  | 6   | 5   | 2   | 1   | 11         | .2    | 2   | 2     | 59   | .22 .10  | ) 6  | 247 | .30  | 95   | .04 | 4   | 1.24 | .02 | .04 | 1   | 1    |
| 16 L97E 102+75N | 3   | 34   | 24  | 172 | .1  | 26  | 20  | 1998 | 9.53  | 48  | 5   | 2   | 1   | 21         | 1.7   | 2   | 2     | 25   | 1.07 .12 | 20   | 11  | .84  | 149  | .01 | 8   | 1.26 | .01 | .07 | 1   | 4    |
| 16 L97E 102+50N | 1   | 95   | 12  | 219 | .4  | 277 | 40  | 1620 | 7.03  | 41  | 5   | 2   | 1   | 21         | 1.2   | 2   | 2     | 128  | .31 .13  | 9 10 | 319 | 2.26 | 134  | .03 | 1   | 3.13 | .02 | .05 | 1   | 24   |
| 16 L97E 102+25N | 4   | 20   | 6   | 48  | .2  | 25  | 5   | 245  | 2.86  | 13  | 6   | 2   | 1   | 17         | .3    | 2   | 2     | 77   | .33 .05  | 6    | 72  | .21  | 81   | .14 | 7   | .84  | .03 | .0£ | 1   | 4    |
| 16 L97E 102+00N | 50  | 1098 | 46  | 538 | 1.9 | 58  | 31  | 4091 | 10.39 | 78  | 5   | 2   | 1   | 32         | 2.9   | 2   | 2     | 152  | .99 .27  | 3 23 | 34  | .58  | 216  | .01 | 5   | 1.90 | .01 | .07 | 1   | 45   |
| 16 6978 101-75N | 35  | 69   | 18  | 125 | 1.8 | 24  | 8   | 174  | 4.77  | 66  | 5   | 2   | 1   | 3          | .2    | 2   | 2     | 132  | .22 .19  | 23   | 2i  | .12  | 131  | .02 | 3   | 1.30 | .01 | .05 | 1   | 6    |
| 16 6978 101+50N | 14  | 44   | 18  | 104 | 1.3 | 11  | 6   | 354  | 6.33  | 107 | 5   | 2   | 1   | ŝ          | . 2   | 3   | 3     | 57   | .04 .13  | 11   | 13  | .03  | 122  | .03 | 5   | .66  | .01 | .04 | 1   | 10   |
| 16 L97E 101+25N | 9   | 17   | 8   | 43  | 1.0 | 6   | 2   | 194  | 2.54  | 8   | 5   | 2   | 1   | 7          | • 2   | 2   | 2     | 20   | .17 .15  | 14   | 13  | .07  | 57   | .09 | 2   | .90  | .07 | .06 | 1   | 1    |
| 16 L97E 101+00N | 8   | 135  | 38  | 137 | 1.9 | 151 | 38  | 2009 | 7.44  | 17  | 5   | 2   | 1   | 19         | .3    | 2   | 2     | 33   | .24 .54  | 3 27 | 11  | .28  | 270  | .01 | 5   | 2.05 | .02 | .08 | 1   | 1    |
| 16 L97B 10C+75N | 94  | 182  | 53  | 624 | 1.9 | 80  | 18  | 959  | 8.69  | 221 | 5   | 2   | 1   | 15         | 1.3   | 9   | 2     | 192  | .24 .36  | 2 16 | 33  | .37  | 269  | .01 | 7   | .83  | .01 | .04 | 1   | 11   |
| 16 6978 100+50N | 7   | 141  | 16  | 216 | .2  | 297 | 35  | 1011 | 4.26  | 37  | 5   | 2   | 1   | 32         | 1.4   | 2   | -2    | 87   | 1.75.09  | 9    | 135 | 3.24 | 274  | .07 | 3   | 2.13 | .02 | .09 | 2   | 70   |
| 16 L97E 100+25N | 3   | 284  | 22  | 81  | 1.0 | 40  | 25  | 727  | 7.42  | 22  | 5   | 2   | 2   | 10         | .5    | 2   | 2     | 93   | .18 .09  | 8 19 | 48  | .85  | 121  | .04 | 5   | 2.82 | .01 | .06 | 1   | 440  |
| 16 L97E 99+75N  | 2   | 5    | 2   | 53  | .7  | 4   | 1   | 40   | .63   | 2   | 5   | 2   | 1   | 18         | • 2   | 2   | 2     | - 14 | .37 .07  | 2 3  | 7   | .02  | 154  | .04 | 4   | .32  | .02 | .05 | 1   | - 34 |
| 16 L97E 99+50N  | I   | 14   | 2   | 29  | 1.1 | 5   | 1   | 59   | .77   | 2   | 5   | 2   | 1   | 9          | .2    | 2   | 2     | 11   | .19 .08  | 5    | 9   | .03  | 48   | .08 | 2   | .40  | .05 | .07 | 1   | 2    |
| 16 L97B 99+25N  | 2   | 15   | 4   | 37  | .9  | 6   | 3   | 114  | 1.50  | 3   | 5   | 2   | 1   | 7          | .2    | 2   | 2     | 23   | .12 .07  | 6    | 15  | .08  | 59   | .09 | 2   | .50  | .05 | .07 | 2   | 6    |
| 16 L97E 99+00N  | 4   | 21   | 3   | 43  | 1.2 | 8   | 6   | 77   | 1.90  | 11  | 5   | 2   | 1   | 8          | •2    | 2   | 2     | 47   | .16 .05  | 6    | 15  | .07  | 51   | .03 | 3   | .75  | .01 | .06 | 1   | 11   |
| 16 L97E 98+75N  | 1   | 9    | 4   | 49  | 1.4 | 14  | 4   | 174  | 1.31  | 10  | 5   | 2   | 1   | 8          | .2    | 2   | 2     | 21   | .23 .05  | 15   | 10  | .27  | 81   | .02 | 3   | .56  | .02 | .10 | 2   | 1    |
| 16 L97E 98+50N  | 1   | 8    | 5   | 50  | 1.2 | 4   | 1   | 93   | .71   | 4   | 5   | 2   | 1   | 11         | .3    | 2   | 2     | 12   | .53 .08  | ) 3  | 5   | .06  | 60   | .04 | 3   | .42  | .02 | .08 | 1   | 1    |
| 16 L97E 98+25N  | 3   | 18   | 6   | 37  | .2  | 6   | 6   | 432  | 2.56  | 7   | 5   | 2   | 1   | 11         | .2    | 2   | 2     | 63   | .38 .11  | 1    | 13  | .11  | 92   | .09 | 2   | .74  | .04 | .05 | 1   | - 5  |
| 16 L978 98+50NA | 1   | 4    | 10  | 33  | ,1  | 3   | 1   | 89   | .64   | 4   | 5   | 2   | 1   | 11         | .3    | 2   | 2     | 11   | .27 .04  | 1    | 6   | .03  | 71   | .09 | 3   | .33  | .12 | .09 | 1   | 13   |
| 16 L97E 98+00N  | 2   | 10   | 1   | 29  | .4  | 4   | 2   | 91   | 1.57  | 5   | 5   | 2   | 1   | 6          | .2    | 2   | 2     | 15   | .22 .06  | 3 10 | 10  | .03  | 52   | .10 | 2   | .13  | .08 | .07 | 2.  | 2    |
| 16 L97B 97+75N  | 3   | 54   | 10  | 67  | .6  | 32  | 12  | 2706 | 7.08  | 11  | 5   | 2   | 1   | 8          | .2    | 2   | 2     | 94   | .13 .26  | 5 11 | 82  | .30  | 113  | ,03 | 2   | 1.46 | .02 | .06 | 1   | 23   |
| 16 L97E 97+50N  | 4   | 28   | 12  | 128 | .9  | 32  | 5   | 406  | 4.35  | 19  | 5   | 2   | 1   | 11         | .2    | 2   | 2     | 61   | .17 .32  | 9    | 90  | .26  | 55   | .05 | 2   | 1.38 | .01 | .04 | 1   | 31   |
| 16 L97E 97+25N  | 2   | 9    | 6   | 43  | 1.1 | 7   | 2   | 93   | 1.09  | 2   | 5   | 2   | 1   | 7          | .3    | 2   | 2     | 19   | .11 .06  | 1    | 16  | .04  | 43   | .11 | 2   | .38  | .07 | .06 | 1   | 3    |

and the second of the second second

ţ

Mo Cu ₽b Zn Aq Ni Co Mn Fe As Àu Th Sr Cd Sb Bi Ca Lа Cr Μα Ba Ti R Al Na W An\* Sample | ppp ş ppm \$ ppm \$ ł ş ppm ppn Badd ррв pp∎ pp∎ ppn ppm pp ppm ppn ppm ppm ppm ppm ppm pps acc ppb .39 .02 16 L97E 97+00N 1.0 .8 1.64 .062 .01 .22 .02 .03 16 L97R 96+75N .5 .30 .7 2.17 .058 .01 .01 .16 .01 .03 .2 .28 .041 .03 .17 .06 16 L97E 96+50N .1 1.16 g q .44 .08 16 L978 96+25N 2.41 1.0 3.20 .056 .21 .02 2 1.18 .02 .05 .1 3.75 .40 .01 .01 3.48 2.8 .192 3 1.25 .05 16 L97E 96+00N 1.1 .70 1.3 2.57 .081 .05 .01 .26 .01 .04 16 L97E 95+75N .2 .25 Ę .6 1.24 .071 .05 .01 .01 16 L97E 95+50N .3 Ļ .11 .04 16 L97E 95+25N 3.66 11.1 4.88 .108 .30 .01 .70 .01 .05 6.6 4.72 8.9 4.42 .152 .37 .01 .74 .01 .06 16 L97E 95+00N 16.7 2.2 .01 .01 4.60 3.00 .116 .38 3 1.07 .06 16 L97E 94+75N 3.7 10.5 .90 .271 .08 .01 .85 .01 16 L97E 94+50N 3.2 6.62 .07 .93 .5 1.14 .052 .05 .05 .42 .02 .03 ţ 16 L98E 106+75N .4 .5 .83 .067 .02 .01 .11 .01 .03 .18 16 L98E 106+50N .3 ĥ .50 1.34 .2 .56 .034 .06 .09 .05 .04 16 L98E 106+25N .2 .3 2.19 2.9 7.35 .203 Q .14 .01 1.22 .01 .03 16 L98E 106+00N 3.27 .071 .05 .81 1.19 1.4 .07 .02 .01 16 L98E 105+75N .1 12.1 4.35 .087 .07 .01 5.42 .17 1.83 .01 16 L98E 105+50N 64 3799 5.1 5.34 .177 .15 .02 .78 .01 .02 16 L98E 105+25N 1.13 1.6 .4 1,30 1.5 6.29.139 .12 .02 .75 .01 .02 16 L98E 105+00N .3 2.41 1.8 2.39.151 .43 .03 .90 .01 .7 16 L98E 104+75N 3.31 .067 .15 .01 .31 .01 .03 .2 2.00 1.1 16 L98E 104+50N ĝ .2 1.82 .1 1.30 .148 .12 .01 .24 .01 .07 16 L98E 104+25N 4.2 1.50 .210 .91 .03 1.23 .01 .08 .8 4.41 16 L98E 104-00N 21 123 1.26 .170 4.59 .81 .02 2.0 1.05 .01 .10 .7 16 L98E 103+75N .03 .11 .2 .42 .055 .01 .01 .01 16 L98E 103+50N .2 .08 .2 Ł 1.47 .2 .32 .097 .01 .40 .01 .04 16 L98E 103+25N .7 .15 .115 .45 .01 1.15 .02 3.68 .08 16 L98E 103+00N .1 .72 .079 .04 .01 .16 .01 .02 .49 .2 .2 16 L98E 102+75N .2 .19 .116 .05 .02 .35 .01 .03 16 L988 102+50N .3 1.25 .92 .01 .07 4.88 .9 .84 .152 2 1.08 .01 16 L98E 102+25N .3 .2 .08 .118 .09 .02 .69 .01 .03 3.03 16 L98E 102+00N .9 .03 .152 .84 .02 2 1.05 .01 .02 • 2 4.5 2.83 q 16 L98E 101+75N .2 .15 .276 .14 .01 .68 .01 .84 16 L98E 101+50N 4.8 3.79 ł .6 .59 .113 1.87 .02 3 1.66 .01 .04 16 L98E 101+25N 15 118 . 6 33 1266 5.55 .2 .07 .097 .44 .01 .88 .01 .03 5.42 16 L98E 101+00N 1.0 .16 .053 2 1.16 .01 .03 162 3.00 .2 .16 .06 ξ 16 L988 100+75N 1.9 .02 2 4.08 .01 .01 Ļ 559 10.23 .3 .02 .052 .15 16 L98E 100+50N 1.0 • 2 .06 .038 .09 .03 .66 .02 .03 1.28 16 L98E 100+25N .4 2 1.31 .3 .16 .148 .14 .02 .02 .03 4.18 16 L99E 105+75N 4.5 .35 .167 .17 108 .04 3 1.42 .03 .07 .2 16 L99E 105+50N 2.8 568 4.74 

|                 | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Nn   | Fe    | As  | ប   | Au  | Th  | Sr   | Cd    | Sb | Bi  | ۷   | Ca P      | La  | Cr  | Mg   | Ba  | Ti  | В   | <u>81</u> | Na  | X   | W   | Ast |
|-----------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|------|-------|----|-----|-----|-----------|-----|-----|------|-----|-----|-----|-----------|-----|-----|-----|-----|
| Sample 🖡        | ppm | bbø | pp  | ppn | ppn | ppn | ppn | pp∎  | ۶     | ppn | ppn | ppn | ppn | ррв  | bbw i | pn | pp∎ | ppa | \$ \$     | рръ | ppn | 1    | ppm | ł   | pp∎ | ł         | \$  | \$  | ppn | aad |
| 16 L99E 104+75N | 2   | 8   | 9   | 25  | .5  | 5   | 1   | 71   | .47   | 6   | 5   | 2   | 1   | 4    | .2    | 2  | 2   | 5   | .38 .038  | 2   | 3   | .03  | 33  | .01 | 2   | .15       | .01 | .01 | 1   | 18  |
| 16 L998 104+50N | 3   | 56  | 12  | 140 | 2.2 | 26  | 4   | 407  | 2.20  | 11  | 5   | 2   | 2   | 31   | .7    | 2  | 2   | 35  | 3.06 .104 | 15  | 10  | .07  | 349 | .12 | 5   | .83       | .02 | .05 | 1   | 2   |
| 16 L99E 104+25N | 5   | 18  | 6   | 67  | .6  | 10  | 1   | 108  | .64   | 2   | 5   | 2   | 1   | 13   | • 2   | 2  | 2   | 11  | 1.88 .066 | 3   | 3   | .08  | 185 | .05 | 12  | . 42      | .01 | .02 | 1   | 1   |
| 16 L99E 104+00N | 10  | 40  | 1   | 81  | . 8 | 16  | 2   | 183  | .90   | 7   | 5   | 2   | 1   | 10   | .2    | 2  | 2   | 14  | .49 .088  | 3   | 5   | .05  | 134 | .01 | 2   | .16       | .01 | .04 | 1   | 6   |
| 16 L99B 103+75N | 34  | 64  | 21  | 112 | 1.9 | 35  | 7   | 318  | 5.29  | 11  | 5   | 2   | 2   | 18   | .2    | 2  | 2   | 108 | .23 .250  | 13  | 33  | .10  | 334 | .12 | 3   | .66       | .02 | .05 | 1   | 20  |
| 16 L99E 103+50N | 41  | 68  | 42  | 101 | .7  | 40  | 10  | 870  | 6.14  | 89  | 5   | 2   | 2   | 12   | .2    | 2  | 6   | 138 | .25 .466  | 11  | 36  | .11  | 261 | .05 | 2   | .99       | .02 | .06 | 3   | 12  |
| 16 L99E 103+25N | 18  | 44  | 13  | 66  | .5  | 19  | 3   | 155  | 2.91  | 25  | 5   | 2   | 2   | 9    | • 2   | 2  | 2   | 45  | .36 .156  | 13  | 10  | .04  | 102 | .13 | 2   | .75       | .02 | .05 | 1   | 9   |
| 16 L99E 103+00N | 61  | 95  | 43  | 162 | .4  | 39  | 13  | 1049 | 7.84  | 147 | 5   | 2   | 1   | 20   | .2    | 3  | 2   | 293 | .52 .227  | 11  | 31  | .30  | 385 | .03 | 4   | 1.11      | .01 | .04 | 1   | 43  |
| 16 L99E 102+75N | 2   | 16  | 5   | 46  | • 2 | 37  | 6   | 393  | 1.75  | 14  | 5   | 2   | 1   | 4    | .3    | 9  | 2   | 17  | .10 .100  | 5   | 63  | .24  | 39  | .08 | 2   | .42       | .01 | .01 | 1   | 4   |
| 16 L99E 102+50N | 2   | 15  | 2   | 54  | .2  | 39  | 11  | 740  | 1.53  | 19  | 5   | 2   | 1   | 4    | .2    | 2  | 2   | 24  | .08 .067  | 2   | 52  | .26  | 27  | .01 | 2   | .33       | .01 | .02 | 1   | 8   |
| 16 L99E 102+25N | 13  | 156 | 81  | 377 | •6  | 214 | 39  | 2847 | 8.63  | 122 | 5   | 2   | 2   | 24   | 2.3   | 2  | 2   | 91  | .48 .181  | 23  | 172 | 1.67 | 217 | .01 | 2   | 2.04      | .01 | .08 | 1   | 33  |
| 16 L99E 102+00N | 14  | 91  | 42  | 278 | .3  | 234 | 38  | 1847 | 6.00  | 72  | 5   | 2   | 1   | 29   | 1.1   | 2  | 2   | 94  | .64 .157  | 10  | 232 | 2.03 | 183 | .02 | 4   | 1.79      | .01 | .06 | 1   | 11  |
| 16 L99E 101+75N | 9   | 45  | 22  | 106 | 1.0 | 65  | 13  | 310  | 2.98  | 31  | 5   | 2   | 1   | 14   | .2    | 2  | 2   | 55  | .20 .084  | 13  | 54  | .46  | 243 | .07 | 3   | 1.04      | .06 | .07 | 1   | 13  |
| 16 L99B 101+50N | 2   | 29  | 12  | 55  | .5  | 46  | 8   | 412  | 9.42  | 20  | 5   | 2   | 2   | 11   | .3    | 2  | 2   | 137 | .10 .060  | 10  | 300 | .56  | 53  | .06 | 5   | 2.56      | .01 | .03 | 1   | 1   |
| 16 L99E 101+25N | 2   | 33  | 14  | 72  | 2.5 | 64  | 10  | 456  | 4.84  | 6   | 5   | 2   | 3   | 7    | .2    | 2  | 2   | 54  | .08 .074  | 13  | 105 | .89  | 48  | .04 | 4   | 3.05      | .02 | .07 | 1   | 11  |
| 16 L99E 101+00N | 4   | 34  | 10  | 68  | 1.2 | 35  | 6   | 299  | 3.82  | 18  | 5   | 2   | 2   | 18   | .2    | 2  | 2   | 73  | .08 .171  | 8   | 77  | .29  | 55  | .02 | 3   | 1.43      | .01 | .05 | i   | 9   |
| 16 L998 100+75N | 9   | 153 | 20  | 607 | 1.3 | 269 | 35  | 3368 | 7.78  | 30  | 5   | 2   | 1   | 92   | 4.2   | 3  | 2   | 92  | 1.74 .219 | 20  | 160 | 1.23 | 344 | .03 | 7   | 2.40      | .02 | .06 | 1   | 14  |
| 16 L99E 100+50N | 7   | 15  | 10  | 68  | .4  | 39  | 8   | 209  | 3.16  | 6   | 5   | 2   | 1   | 12   | .2    | 2  | 2   | 60  | .11 .061  | 9   | 45  | .14  | 77  | .03 | 2   | .92       | .02 | .04 | 1   | ĩ   |
| 16 L998 100+25N | 14  | 87  | Į û | 439 | 1.6 | 78  | 13  | 3012 | 5.00  | 23  | 5   | 2   | 1   | 49   | 2.3   | 2  | 2   | 67  | .86 .227  | 21  | 76  | . 49 | 294 | .03 | 3   | 2.19      | .03 | .06 | 1   | 10  |
| 16 L998 99+75N  | 2   | 14  | 6   | 58  | .6  | 7   | 2   | 139  | 1.16  | 2   | 5   | 2   | 1   | 17   | .2    | 2  | 2   | 27  | .32 .047  | 9   | 17  | .11  | 44  | .04 | 2   | .76       | .03 | .05 | 1   | 7   |
| 16 L99E 99+50N  | 2   | 2   | 10  | 32  | .5  | 12  | 3   | 110  | 1.31  | 7   | 5   | 2   | 2   | 8    | .2    | 2  | 2   | 45  | .08 .035  | 8   | 22  | .07  | 14  | .12 | 2   | . 47      | .05 | .07 | 1   | 4   |
| 16 L99E 99+25N  | 3   | 19  | 7   | 50  | 3.  | 44  | 6   | 157  | 4.11  | 2   | 5   | 2   | 1   | 9    | .2    | 2  | 2   | 121 | .05 .063  | 11  | 64  | .12  | 25  | .05 | 3   | 1.40      | .02 | .04 | 1   | 1   |
| 16 L99E 99+00N  | 2   | 21  | 7   | 35  | .1  | 11  | 7   | 220  | 3.01  | 4   | 5   | 2   | 2   | 16   | .2    | 2  | 2   | 93  | .11 .055  | 7   | 29  | .16  | 17  | .15 | 2   | .72       | .03 | .03 | 1   | 8   |
| 16 L99E 98+75N  | 1   | 5   | 19  | 23  | .1  | 26  | 6   | 740  | .94   | 2   | 5   | 2   | 1   | 11   | .2    | 2  | 2   | 25  | .09 .028  | 8   | 47  | .22  | 32  | .06 | 2   | .53       | .03 | .02 | 1   | 20  |
| 16 L99E 98+50N  | 2   | 11  | 12  | 36  | • 5 | 36  | 4   | 127  | 3.24  | 2   | 5   | 2   | 3   | 11   | .2    | 2  | 4   | 109 | .06 .034  | 9   | 63  | .21  | 35  | .09 | 2   | 1.06      | .02 | .05 | 1   | 15  |
| 16 G99B 98+25N  | 1   | 62  | lĵ  | 119 | .1  | 134 | 15  | 773  | 12.34 | 12  | 5   | ź   | 3   | Ę    | .5    | Ĵ  | 2   | 207 | .02 .059  | 6   | 384 | .76  | 61  | .03 | 9   | 2.65      | .01 | .02 | 1   | 8   |
| 16 L99E 98+00N  | 1   | 38  | 15  | 100 | .2  | 224 | 21  | 825  | 4.82  | 2   | 5   | 2   | 1   | . 10 | • 2   | 2  | 2   | 126 | .16 .064  | 8   | 342 | 2.39 | 120 | .14 | 3   | 2.15      | .05 | .05 | 1   | 15  |
| 16 L99E 97+75N  | 5   | 32  | 12  | 41  | .3  | 15  | 4   | 139  | 3.29  | 9   | 5   | 2   | 1   | 12   | .2    | 2  | 2   | 75  | .07 .063  | 11  | 39  | .16  | 39  | .06 | 2   | 1.38      | .02 | .94 | 1   | 38  |
| 16 L99B 97+50N  | 4   | 19  | 12  | 44  | .5  | 11  | 4   | 286  | 2.87  | 3   | 5   | 2   | 1   | 11   | .2    | 2  | 2   | 51  | .08 .096  | 9   | 35  | .17  | 29  | .05 | 2   | 1.15      | .03 | .05 | 1   | 29  |
| 16 L99E 97+25N  | 4   | 34  | 13  | 34  | 1.1 | 13  | 3   | 142  | 3.09  | 10  | 5   | 2   | 1   | 13   | .2    | 2  | 2   | 52  | .09 .090  | 10  | 31  | .14  | 40  | .06 | 2   | 1.36      | .03 | .04 | 1   | 33  |
| 16 L99E 97+00N  | 2   | 1   | 1   | 36  | 1.1 | 2   | 2   | 102  | 1.17  | 4   | 5   | 2   | 1   | 6    | .2    | 2  | 2   | 12  | .10 .043  | 8   | 8   | .03  | 17  | .14 | 2   | .43       | .07 | .06 | 1   | 3   |
| 16 L99E 96+75N  | 2   | 22  | 13  | 71  | 6.0 | 76  | 9   | 444  | 6.32  | 7   | 5   | 2   | 4   | 8    | • 2   | 2  | 2   | 159 | .05 .051  | 10  | 109 | .32  | 41  | .12 | 2   | 1.60      | .02 | .05 | 1   | 4   |
| 16 L99E 96+50N  | 2   | 18  | 16  | 39  | .5  | 22  | 5   | 190  | 5.46  | 18  | 5   | 2   | 3   | 15   | .2    | 2  | 2   | 192 | .07 .034  | 9   | 46  | .13  | 37  | .12 | 2   | 1.38      | .01 | .04 | 1   | 5   |
| 16 L99E 96+25N  | 3   | 1   | 7   | 31  | .2  | 10  | 2   | 138  | 2.11  | 3   | 5   | 2   | 1   | 7    | .2    | 2  | 2   | 23  | .07 .045  | 11  | 43  | .13  | 20  | .19 | 2   | .69       | .10 | .06 | 1   | 3   |
| 16 L99B 96+00N  | 1   | 5   | 2   | 30  | .3  | 106 | 12  | 269  | 1.82  | 14  | 5   | 2   | 1   | 3    | .3    | 11 | 2   | 28  | .04 .021  | 4   | 37  | 1.22 | 16  | .05 | 2   | .27       | .02 | .01 | 1   | 4   |
| 16 L99E 95+75N  | 1   | 38  | 9   | 94  | .5  | 202 | 17  | 509  | 5.54  | 9   | 5   | 2   | 1   | 17   | .2    | 2  | 2   | 88  | .16 .055  | 5   | 99  | .81  | 66  | .03 | 16  | 1.64      | .01 | .05 | 2   | 27  |
| 16 L99E 95+50N  | 5   | 33  | 12  | 99  | .3  | 154 | 14  | 399  | 6.82  | 8   | 5   | 2   | 1   | 7    | .2    | 2  | 2   | 111 | .04 .062  | 11  | 181 | .57  | 52  | .05 | 15  | 1.87      | .02 | .04 | 1   | 16  |
| 16 L99E 95+25N  | 2   | 851 | 14  | 898 | .4  | 150 | 14  | 1013 | 3.15  | 13  | 5   | 2   | 1   | 103  | 2.3   | 2  | 2   | 55  | 3.82 .108 | 12  | 88  | .58  | 226 | .03 | 10  | .98       | .02 | .04 | 1   | 6   |
| 16 L99B 94+75N  | 2   | 45  | 5   | 146 | .1  | 158 | 12  | 299  | 2.15  | 2   | 5   | 2   | 1   | 34   | .3    | 2  | 2   | 35  | .48 .082  | 2   | 78  | .88  | 99  | .02 | 8   | .49       | .01 | .05 | 1   | 2   |
| 16 L99E 94+50N  | 2   | 36  | 13  | 52  | .4  | 70  | 9   | 359  | 4.53  | 16  | 5   | 2   | 1   | 12   | .2    | 2  | 2   | 78  | .13 .052  | 10  | 100 | .50  | 46  | .11 | 10  | 1.79      | .02 | .03 | 1   | 8   |

No Cu ۶þ 2n Àg Ni Сo Mn Fe Ås Au Th Sr Cd Sb Bi Ca P La Cr Mg Ba Ti Al Na N Au\* Sample # ppm ł ł ł ppm ppa ррв ppa ppm ppm ppa ppa pp ppa ppm ppa ppm ppm ppp **DDB** pp∎ ł ppa \$ ł ł ppn ppm Ł ppn pob 16 E99E 94+25N 2 6 9 45 .1 19 3 124 1.05 2 5 2 8 2 1 .2 2 21 .13 .050 23 .09 8 40 .11 12 .45 .08 .08 1 4 40 12 57 79 16 L99E 94+00N 1 .1 8 232 21 .2 2 2 8.04 2 1 12 112 .22 .068 17 141 .48 32 .11 2.23 Ģ .01 .04 1 1 45 16 L99E 93+75N 51 121 532 1.8 59 20 2115 6.54 68 5 2 1 14 2.6 16 2 79 .32 .227 17 26 265 .20 .01 8 1.10 .01 .07 1 25 53 16 L99E 93+50N 3 18 9 .4 52 5 240 3.51 1 2 1 .2 2 93 .06 .094 1 44 .09 25 .18 7 .78 .02 .05 1 6 16 L99E 93+25N 15 54 39 3 8 .5 3.36 11 4 190 ĝ .2 2 2 7 .17 87 .13 .042 57 28 .08 5 .90 .02 .05 6 1 32 16 L99E 93+00N 14 75 2 .6 210 29 1082 8.54 ą 16 .6 2 3 114 .17 .080 8 .76 174 194 .06 4 1.74 .02 .04 1 22 16 L1008 99+75M 1 117 36 313 .2 79 39 4326 18.45 5 2 8 2.3 5 2 158 .17 .103 10 124 .27 144 .01 .01 6 4.64 .04 2 4 16 L100E 99+50% 64 2 13 50 58 .1 15 9.18 683 5 4 .7 3 2 125 .03 .050 12 105 .22 76 .82 2 1.87 .01 .04 1 1 16 L100B 99+25N 59 13 56 1 .1 517 37 2144 5.84 11 19 .1 3 2 111 .62 .057 10 259 5.21 161 .05 4 3.48 .03 .05 1 1 16 L100E 99+00N 1 9 3 28 1 44 5 252 1.60 2 6 .2 2 2 28 .09 .060 1 42 .30 28 .09 2 .47 .04 .05 1 1 16 L100E 98+75N 5 31 .2 2 1 4 152 1.06 2 10 .2 2 2 23 .16 .030 6 20 .07 25 .09 2 .32 .03 .05 1 6 16 L100B 98+50N 5 21 1 8 .1 6 2 81 1.48 2 6 •2 2 2 7 40 .05 .027 30 .06 23 .07 2 .61 .02 .03 1 10 16 L100E 98+25N 4 34 10 49 .2 7 3 203 1.95 .1 3 2 2 56 .16 .052 5 28 .16 58 .08 2 .46 .04 .05 2 15 28 16 L100E 98+00N 2 12 48 .2 99 19 596 7.74 5 Ş .06 .066 6 .7 2 7 176 8 27 427 .82 .08 2 1.72 .01 .03 2 4 16 L1008 97+50N 1 8 11 22 .1 7 2 90 .83 .1 2 2 19 .05 .022 9 21 .04 18 .08 2 .28 .06 .05 1 1 16 L100E 97+00N 3 15 12 27 .2 9 123 2.88 5 3 g 3 .6 2 2 34 .03 .061 12 34 .08 51 .07 5 1.22 .04 .05 2 1 23 16 L1008 96+50N 13 85 21 2 .1 124 17 607 4.46 5 1.4 3 2 95 .31 .077 8 202 .70 423 .07 2 1.38 .01 .03 1 1 16 L100E 96+00N 1 3 10 16 .1 6 1 72 .82 2 5 £ .3 2 3 20 .07 .031 6 14 .04 18 . 88 5 4 .32 .04 .05 1 16 L100E 95+50N 3 44 31 153 .2 167 5 11 34 849 8,18 16 2 .4 11 146 .16 .051 5 133 1.17 57 .05 2 1.91 .01 .03 1 11 21 10 16 LIOOR 95+00N 3 66 .3 117 21 684 5.70 10 5 9 .8 2 4 77 .11 .031 9 90 .49 54 .07 2 1.82 .02 .03 2 2 16 L100B 94+50N 57 22 30 1 147 .2 10 6 403 1.36 2 Ę 2.0 2 2 19 3.17 .080 28 21 .03 128 .04 4 1.59 .02 .03 2 ł 16 L100E 94+00N 9 4 39 .1 8 108 2.35 5 6 2 2 4 å .8 69 .22 .021 6 20 .04 18 .08 .52 2 2 .03 .03 2 16 L100B 93+50N 43 18 .3 45 4 117 11 567 5.48 23 5 4 1.5 2 .14 .070 50 4 92 10 58 .40 .07 2 4.05 .01 .02 ŧ 5 37 97 87 25 16 L100E 92+50N 7 940 1.3 68 2772 5.87 35 5 2 1 3 2 55 1.00 .088 4.4 14 55 .68 132 .02 3 1.79 .01 2 51 .04 11 16 L100E 92+00N 2 9 9 53 . 8 11 4 201 1.96 11 1 .9 2 2 60 .12 .024 22 7 .08 29 .07 .57 4 .02 .03 2 9 10 2 260 5 έ .07 .021 16 L100E 110+00N 4 .3 32 101 3.64 1 .2 2 2 105 6 79 .22 15 .10 2 .75 .02 .01 1 2 16 L100E 109+50N 2 56 11 129 .3 161 15 305 5.49 . 1 10 .3 2 2 80 .23 .046 12 Ł 240 1.49 55 .08 3 3.80 .01 .01 1 1 16 L100E 109+00N 3 45 2 78 25 2 32 . 91 18 2 .1 2 5 2 1 .1 2 13 .90 .074 6 30 .15 42 .02 .36 .01 g 6 .04 1 16 L100E 108+50N 5 21 7 68 1.0 48 5 68 3.93 1 .2 2 1 .09 .030 12 92 86 .41 38 .10 2 1.65 .01 5 .02 1 16 L100E 108+00N 8 11 2 25 31 61 2.69 8 .2 2 6 .1 4 1 72 .17 .023 12 98 .28 38 .09 4 1.11 .01 .01 2 2 16 G100E 107+50N 102 87 159 7 1.0 86 442 6.22 12 .2 2 2 4 14 88 .15 .209 1 162 .90 49 .07 2 5.50 .01 .01 2 1 2 16 L100E 107+00N 1 10 18 .3 6 2 54 .78 2 .2 2 2 q .19 .057 6 8 .05 41 .07 .40 .04 .04 1 1 4 16 L100E 106+75N 2 15 .2 2 50 .40 .2 2 1 ļ 2 q 2 6 .22 .055 Ę 4 .03 68 .04 2 .25 .04 .04 1 5 2 34 32 19 .5 16 L100B 106+50N 1 .2 .48 2 2 2 7 .46 .074 8 4 1 1 2 7 .04 185 .02 .20 .02 10 4 .04 1 16 G100E 106+25N 2 21 Ş 2 3 .1 1 78 .78 2 .2 2 2 12 .031 .14 6 8 .82 35 .10 .21 .05 .04 1 3 4 16 LIGOE 106+00N 1 4 4 if .1 2 1 145 .78 2 Ş .2 2 2 11 .12 .046 6 .05 21 6 .06 5 .26 .05 .05 1 5 16 L100E 105+75N 17 2 32 29 76 3 .1 45 .18 2 1.2 1 2 4 2.47 .085 2 5 .18 62 .01 13 .01 6 1 .12 .04 1 212 16 L100E 105+50N 1 68 8 68 .1 22 509 3.96 36 .5 2 2 112 1.83 .042 3.84 3 409 .22 7 124 2.89 .02 .17 1 1 16 16 L100E 105+25N 5 58 13 87 .2 238 21 442 5.00 5 5 .3 92 1.03 .275 2 3.36 2 2 3 138 4.20 67 .19 .02 .13 1 2 16 L100E 105+00N 8 37 82 .5 103 9 203 2.78 20 5 74 4 1 .2 2 2 84 1.89 .076 7 74 1.17 110 .10 7 1.19 .02 .05 1 1

Mo Ĉu-Pb 2nNi Ço Mn Fe Cd Sb Åq As n Au Th Sr Bi Ca P Cr Mq Ba Ti Al La Na ¥. Åu\* ž ş Sample 🛔 \$ ş ppm ppn ppm ppm ppm ppn ppm ppm ppm ppm ppm aqq \$ ppn ł 8 ş ppn ppn ppm ppm ppm ppm pp∎ aqq ppm dad 66 15 16 L100E 104+75N 3 61 .5 345 27 343 4.16 3 5 2 10 • 2 2 2 74 .68 .057 .19 3.42 4 141 4.16 49 9 .02 .09 1 1 •2 2 5 2 .2 2 2 16 L100E 104+50N 1 7 2 24 42 4 115 1.06 6 20 .32 .045 5 40 . 49 27 .37 .19 .03 .06 1 2 16 L100E 104+25N 13 .2 8 2 67 2.47 2 S 2 .2 2 2 3 46 12 18 .13 .171 16 23 .01 24 .05 2 1.47 .01 .01 1 5 16 L100E 104+00N 6 66 15 97 .7 158 14 387 4.81 16 5 2 17 .2 2 2 78 .32 .074 6 198 1.56 184 .04 1.81 .01 2 .02 1 25 16 L100E 103+75N 74 .1 138 28 2106 8.98 78 5 2 1.0 2 2 .36 .678 47 113 161 8 160 1.34 135 .07 2 2.48 .01 .04 1 2 16 L100E 103+50N 34 92 26 173 1.6 64 11 483 7.26 62 5 .2 4 2 91 .11 .371 12 89 2 1.28 .01 .44 104 .03 .03 1 32 .2 16 L100E 103+25N 99 206 2.2 92 15 1214 7.12 87 5 2 10 2 2 65 .26 .236 13 103 16 .71 115 . 64 2 1.74 .03 .05 1 6 37 12 16 L100E 103+00N 22 190 389 1.4 217 38 2462 8.87 99 5 2 3.0 2 2 97 .34 .176 17 179 1.92 184 .01 2 2.31 .01 .03 1 8 16 L100E 102+75N 35 29 87 5 2 13 3 2 19 142 377 1.4 175 2657 7.29 1.1 90 .38 .224 14 147 1.56 244 .01 2 1.96 .01 .04 1 10 17 -57 37 5 2 .2 2 2 16 L100E 102+50N 3 30 .9 g 666 6.35 20 8 152 .10 .101 8 79 .42 45 .10 2 1.38 .01 .02 1 1 16 LIODE 102+25N 9 145 15 282 .6 300 32 1387 5.19 5 2 32 1.1 2 2 85 1.21.142 Ģ 160 44 3.04 273 .03 2 2.06 .01 .06 1 1 26 10 16 L100E 102+00N 58 193 130 22 1040 5.17 53 5 2 .2 3 80 .25 .245 5 155 14 .4 1.37 110 .82 2 1.31 .01 .04 1 1 32 16 LIQOE 101+75N 4 106 16 198 .4 310 26 827 4.15 20 5 2 2.1 2 2 71 1.41 .087 6 163 3.54 252 .07 7 2.15 .01 .07 1 107 17 5 10 .2 16 L100E 101+50N 3 36 75 .5 47 10 871 6.99 16 2 103 .20 .309 7 54 1.88 .01 .02 15 141 .46 .07 6 1 16 L100E 101+25N 2 62 16 22 1081 7.65 13 5 2 1.6 76 .25 .085 10 162 1.94 140 .1 152 9 2 51 .08 3 3.46 .01 .02 1 29 .8 16 LIQOE 101+00N 2 38 Q 60 89 15 516 7.68 6 5 8 2 2 117 .09 .049 8 199 .92 72 .01 4 .97 3 2.59 .02 1 13 16 L1008 100+75N 3 20 52 ,2 60 1 249 4.15 2 1 1 .4 2 113 .11 .040 6 140 .56 31 .12 .91 .02 .03 2 6 4 6 6 3 51 .1 45 Ģ 5 •2 2 16 LIQUE 100+50N 24 11 421 5.47 3 8 2 94 .09 .039 10 100 .41 39 .09 6 1.54 .02 .03 18 1 16 L100E 100+25N 2 9 ς. 34 .1 7 3 153 2.13 2 5 2 7 • 2 2 2 51 .09 .028 7 16 .10 50 .02 .99 .01 .03 40 7 1 45 16 L101+75N 100+25E 12 26 S 345 2.35 11 188 .8 3 2 2916 .72 .036 12 1 .6 9 46 1.12 32 .06 3 1.14 .01 .04 1 2 16 BL100N 89E 23 27 ۲. 229 .1 47 10 8879 12.98 67 5 10 .8 17 92 .13 .082 18 56 .09 142 .93 2 2.22 .01 .03 ? 1 18 BL100N 89+25E î 31 373 5 ••• 3.5 73 19 .1 25 11 4167 18.84 31 2 1.36 .094 30 21 .59 . 13 2 3.97 .01 .02 ź 112 16 BL100N 89-50B 5 23 ŝ 11 .25 .041 22 17 281 .1 13 7 1609 12.53 37 4 1.1 103 26 .13 32 .11 3 2.59 .04 .04 ł Ę 22 16 BL100N 89+75E 2 28 314 30 9 3707 6.49 109 5 29 3.0 2 40 2.49.187 39 123 .1 4 14 .14 .62 4 1.31 .01 .06 1 2 5 3 229 11 6808 6.51 5 2 18 3.6 78 2.43 .134 30 25 .01 .03 16 BL100N 90E 19 .4 21 23 .13 136 .85 6 2.37 2 Ģ 32 5 2 26 16 BL100N 90+25E 4 23 146 .3 37 11 2460 5.66 29 1.4 4 2 67 1.87 .120 25 54 .29 84 .03 3 1.93 .01 .06 10 ŗ .6 .85 16 BL100N 90+50B 16 .7 8 1 2590 2 29 34 1.90.069 12 28 .06 156 2 .03 .05 2 2 18 141 2.44 3 .06 16 BL100N 90+75E 31 39 17 148 .7 21 9 356 6.12 25 5 2 13 .3 5 2 77 .24 .230 5 20 .08 58 .01 2 .92 .01 .03 7 5 30 61 17 45 .01 27 16 BL100N 91E 39 13 170 54 18 5966 9.78 48 4.0 1.72 .128 .50 141 .02 3 2.22 .03 2 1.2 .07 .268 965 5 2 9 • 2 2 80 g 79 .01 2 2.89 .01 05 27 16 BL100N 91+25E 3 104 0 49 . 8 6 9 7.23 17 3 16 .17 1 5 2 .2 2 82 .22 .196 4 10 .27 113 .01 2 2.09 .01 .08 1 64 16 BL100N 91+50E 3 43 12 52 .8 4 8 1045 4.94 15 18 11 17 1768 6.25 5 2 19 .5 2 2 67 .63 .121 14 22 .50 194 .01 2 3.24 .01 .06 1 19 16 BL100N 91+75E 2 1£ 110 .9 13 44 11 1.94 5 2 .5 2 43 .15 .056 9 13 .08 30 .04 4 1.32 .02 .03 1 13 16 BL100N 92E 3 13 33 .5 3 đ 97 4 17 3 358 5 2 2 161 .14 .139 9 48 .36 93 .11 2 1.97 .01 .04 1 12 16 BL100N 92+25E 28 20 71 18 9.95 29 1 14 .8 3 4 .2 ĥ 7 5 .40 54 2 .01 16 BL100N 92+50E 3 -39 17 140 .9 23 7 712 7.08 25 ) 1 16 .3 2 2 103 .15 .139 60 .11 2.01 .05 1 12 16 BL100N 92+75E 2 52 14 77 25 6 250 6.68 32 5 2 1 21 • 2 2 2 117 .23 .098 10 63 .36 44 .13 2 1.50 .01 .04 1 13 .4 5 5 .54 5 .5 2 ĝ .2 2 57 .08 .106 55 .01 5 .01 .06 13 16 BL100N 93E 2 54 6 11 848 6.05 16 14 3.02 1 47 5 2 15 3 .12 .126 6 25 .30 51 .82 2 11 16 BELOON 93+25E 26 10 48 1.0 8 6 278 5.51 23 1 .2 2 106 2.20 .01 .05 1 3 , 11 3 54 .68 2,35 .01 50 16 BL100N 93+50E 3 82 33 139 1.7 43 16 1380 8.04 80 5 2 1 11 .4 3 76 .18 .225 01 2 .06 1 60 .72 Ľ 2 : 5 2 193 15 092 29 83 69 18 16 BL100N 93+75E 2 -54 32 111 .1 47 Ģ 569 9.69 48 1 .6 3 2 2.67 .01 1

|                  | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe    | As  | 9   | Au  | Th  | Sr  | Cd  | Sb  | Bi        | V   | Ca       | P   | La     | Cr  | Ma   | Ba         | Ti  | B      | Al   | Na   | ĸ     | W        | ≛n‡        |
|------------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|-----|-----|-----------|-----|----------|-----|--------|-----|------|------------|-----|--------|------|------|-------|----------|------------|
| Sample 🛔         | ppm | ppn | pp∎ | ppn | ppm | ррв | ppm | ppm  | \$    | ppm | ppm | ppn | ppm | ppm | ppm | ppm | ppm       | ppm | ۶        | 2   | naa    | acc | ,    | DDm        | 2   |        | ş    | ş    | ş     | nne.     | nnh        |
| 16 BL100N 94E    | 1   | 58  | 11  | 149 | 3.1 | 44  | - 8 | 4115 | 3.68  | 36  | 5   | 2   | - 1 | 22  | .8  | 2   | <u></u> 3 | 38  | 2.44 .1  | 106 | 26     | 46  | .31  | 101        | .02 | 5      | 2.21 | .02  | .02   | 1<br>66m | 550<br>110 |
| 16 BL100N 94+258 | 5   | 42  | 36  | 68  | 2.2 | 25  | 6   | 589  | 11.07 | 37  | 5   | 2   | 3   | 11  | .5  | 3   | 2         | 159 | .25 .2   | 263 | 10     | 79  | .28  | 53         | .18 | ŷ      | 1.66 | .01  | .05   | 1        | 16         |
| 16 BL100N 94+50E | 4   | 45  | 15  | 58  | 1.2 | 12  | 5   | 441  | 6.53  | 22  | 5   | 2   | 1   | 13  | .2  | 2   | 2         | 97  | .15 .3   | 201 | 7      | 32  | .27  | 96         | .03 | ,      | 2.41 | . 01 | 100   | 1<br>1   | 11         |
| 16 BL100N 94+75E | 3   | 27  | 13  | 54  | .9  | 13  | 7   | 529  | 4.33  | 13  | 5   | 2   | 1   | 20  | .2  | 2   | 2         | 97  | . 21 . 1 | 108 | ,<br>6 | 25  | . 43 | 64         | .03 | 2      | 2.24 | 01   | 05    | 1        | 11         |
| 16 BL100N 95E    | 5   | 28  | 13  | 97  | 1.4 | 6   | 7   | 919  | 10.04 | 25  | 5   | 2   | 1   | 17  | .8  | 2   | 2         | 48  | .56 .3   | 238 | 11     | 19  | .13  | <b>9</b> 1 | .02 | ,      | 2 63 | . 01 | 13    | 1        | 17         |
| 16 BL100N 95+258 | 4   | 30  | 33  | 112 | .5  | 17  | 6   | 1087 | 7.15  | 111 | 5   | 2   | 1   | 3   | .2  | 4   | 2         | 63  | . 18 . ( | 085 | 14     | 12  | .21  | 211        | .02 | 5      | 1 72 | .01  | .03   | 1        | 17         |
| 16 BL100N 95+50B | 13  | 43  | 57  | 223 | 1.2 | 35  | 9   | 687  | 10.29 | 76  | 5   | 2   | 1   | 11  | .9  | 3   | 2         | 127 | .16 .1   | 153 | 16     | 83  | . 27 | 152        | .06 | 2      | 2.23 | .01  | .06   | t        | 1.0        |
| 16 BL100N 95+75B | 29  | 122 | 36  | 316 | .8  | 46  | 22  | 1727 | 7.13  | 45  | 5   | 2   | 1   | 22  | .9  | Å   | 2         | 104 | .08.1    | 126 | 15     | 31  | .24  | 165        | .01 | ż      | 2.33 | .01  | .04   | 1        | 10         |
| 16 BL100N 968    | 3   | 170 | - 2 | 80  | .3  | 848 | 135 | 4266 | 6.64  | 17  | 5   | - 2 | 1   | 21  | 3.0 | 2   | 2         | 184 | .23 .0   | 178 | . 1    | 141 | 7.65 | 141        | .01 | ,      | 2.66 | . 01 | .01   | 1<br>5   | 10         |
| 16 BL100N 96+25E | 4   | 65  | 12  | 252 | .4  | 233 | 23  | 1450 | 4.19  | 25  | 5   | 2   | 1   | 38  | 1.2 | 2   | 2         | 88  | 1.67.1   | 147 | 13     | 150 | 2.37 | 236        | .04 | ,<br>2 | 2.05 | .02  | .08   | 1        | 12         |
| 16 BL100N 96+50E | 1   | 113 | 7   | 141 | .1  | 400 | 46  | 1205 | 4.48  | 17  | 5   | 2   | 1   | 37  | 1.0 | 2   | 2         | 83  | 1.59 .0  | 072 | 7      | 199 | 4.53 | 221        | .07 | 5      | 2.77 | .01  | .08   | 1        | 11         |
| 16 BL100N 96+75E | 4   | 144 | 12  | 41  | .7  | 16  | 5   | 300  | 4.67  | 11  | 5   | 2   | 1   | ģ   | .2  | 2   | 2         | 82  | .12 .0   | 083 | 10     | 32  | .23  | 83         | .11 | 2      | 1.68 | .02  | .05   | i        | 11         |
| 16 BL100N 97E    | 2   | 12  | 3   | 40  | .6  | 7   | 2   | 86   | .58   | 5   | 6   | 2   | 2   | 11  | .4  | 2   | 2         | 11  | .35 .(   | 079 | 2      | 11  | .10  | 87         | .02 | 5      | .74  | .02  | .08   | 1        | 11         |
| 16 BL100N 97+25E | 1   | 12  | î   | 45  | .7  | 2   | 2   | 73   | .72   | 2   | 5   | 2   | 1   | 11  | .2  | 2   | 2         | 10  | .12 .0   | 056 | 9      | 8   | .03  | 71         | .06 | 2      | .58  | .06  | .06   | 1        | 1          |
| 16 BL100N 97+508 | 4   | 12  | 3   | 59  | 2.0 | 3   | 2   | 91   | .84   | 2   | 5   | 2   | 1   | 9   | . 2 | 2   | 2         | 33  | .12 .0   | 066 | 7      | 12  | .04  | 29         | .03 | 7      | .11  | .03  | .05   | Î        | 7          |
| 16 BL100N 97+75E | 4   | 24  | ţ   | 52  | .4  | 1   | 5   | 197  | 2.49  | 7   | 5   | 2   | 1   | 13  | ,3  | 2   | 2         | 95  | .27 .0   | 080 | 6      | 7   | .07  | 61         | .12 | 2      | .57  | .04  | .04   | 1        | 6          |
| 16 BLIOON 98+00E | 3   | 7   | 4   | 39  | .5  | 6   | 3   | 102  | .93   | 5   | 5   | 2   | 1   | £   | .2  | 2   | 2         | 31  | .08 .0   | 043 | 6      | 11  | .06  | 14         | .04 | ŝ      | .44  | .03  | .04   | 1        | Š          |
| 16 BL100N 98E    | Ę   | 33  | 19  | 55  | 1.0 | 65  | 11  | 330  | 9.90  | 10  | ţ   | 2   | 2   | 4   | .3  | 2   | 2         | 179 | .04 .1   | 139 | 7      | 183 | .75  | 34         | .09 | 2      | 14   | .01  | . 6 ! | 2        | 4          |
| 16 BL100N 98+258 | 1   | 5   | 2   | 28  | .5  | 2   | 1   | 73   | .52   | 2   | 5   | 2   | 1   | 10  | .2  | 2   | 2         | 17  | .14 .0   | 041 | 4      | 7   | .04  | 20         | .03 | 5      | .28  | .02  | .05   | 2        | į          |
| 16 BLIOON 98+50E | ç   | 11  | ç   | 42  | 2.0 | 6   | 2   | 87   | 1.16  | 7   | 5   | 2   | 1   | ŧ   | .2  | 2   | 2         | 56  | .04 .0   | 044 | 7      | 15  | .04  | 23         | .04 | 3      | 40   | .03  | .04   | 1        | 1          |
| 16 BL100N 98+755 | ::  | 18  | 11  | 64  | 1.9 | 9   | 5   | 312  | 2.97  | 14  | 5   | 2   | 1   | 7   | .4  | 2   | 2         | 49  | .12 .1   | 157 | 1      | 16  | .06  | 47         | .04 | 3      | .72  | .02  | .04   | Ī        | 5          |
| 16 BL100N 99E    | :   | 7   | 5   | 52  | .2  | ŝ   | :   | 61   | .52   | 2   | Ê   | 2   | 1   | 25  | , 2 | 2   | 2         | ò   | .20 .0   | 063 | 3      | 6   | .05  | 121        | .05 | 2      | 31   | .04  | .04   | 1        | 3          |
| 16 BLIOON 99+25E | !   | 10  | 2   | 36  | • 3 | 17  | 3   | 224  | 1.00  | 2   | 5   | 2   | 1   | - 6 | .3  | 2   | 2         | 20  | .11 .0   | 042 | 6      | 36  | .20  | 37         | .09 | 2      | . 14 | .05  | .05   | 1        | 3          |
| 16 BL100N 99+50E | 2   | 6   | 4   | 68  | .2  | 6   | 2   | 65   | .73   | 2   | 5   | 2   | 1   | 11  | .2  | 2   | 2         | 16  | .11 .0   | 035 | 5      | 11  | .04  | 52         | .06 | 3      | .29  | .04  | .03   | 1        | 6          |
| 16 BL100N 99+75E |     | 17  | 11  | 24  | .6  | 12  | 2   | 65   | .73   | 2   | 5   | 2   | 1   | 14  | .3  | 2   | 2         | 27  | .08 .0   | 019 | 8      | 29  | .11  | 24         | .04 | 2      | . 65 | .02  | .03   | 1        | I          |
| 16 BLICON 100B   | 2   | 7   | 2   | 48  | .6  | 4   | 2   | 96   | .80   | 2   | 5   | 2   | 1   | 7   | .2  | 2   | 2         | 16  | .10 .(   | 050 | 4      | 10  | .04  | 21         | .08 | 3      | .24  | .03  | .06   | 1        | . 1        |
| 16 BL100N 100E   | 1   | 7   | 2   | 19  | .1  | 1   | 1   | 31   | .54   | 2   | 5   | 2   | 1   | 1   | .2  | 2   | 3         | 17  | .04 .(   | 018 | 9      | 7   | .03  | 17         | .01 | 3      | .65  | .01  | .03   | 1        | 2          |

· 1

-

APPENDIX 3 SUMMARY STATISTICS AND HISTOGRAMS

Ē

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = 16-SOILS.DAT

| Variable =   | Au           | Unit = | ppb .       | N = 506<br>N CI = 28 |
|--------------|--------------|--------|-------------|----------------------|
| Transform    | = Logarithmi | .c     | Number of I | Populations = 2      |
| # of Missing | Observations | s = 0. |             |                      |

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1437.338

Parameterized Degrees of Freedom = 3

| Population | Mean    |   | Std Dev | Percentage |
|------------|---------|---|---------|------------|
|            |         | - |         |            |
| 1          | 7.879   | - | 2.537   | 98.98      |
|            |         | + | 24.465  |            |
| 2          | 177.373 | - | 59.601  | 1.02       |
|            |         | + | 527.861 |            |

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thre   | esholds |
|------|--------|---------|
|      |        |         |
| 1    | 0.817  | 75.97   |
| 2    | 20.027 | 1570.91 |

\*\*\*\*\*



<u>~``</u>

16:32:38 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/10/9

| Vari  | able =           | - Au              | Unit       | ; =         | ppb                   |                     | N =             | 506              |
|-------|------------------|-------------------|------------|-------------|-----------------------|---------------------|-----------------|------------------|
| std.  | Mean =<br>Dev. = | 0.9203            | Mir<br>Max | n =<br>( =  | 0.0000<br>3.3502      | lst Quart<br>Med    | ile =<br>lian = | 0.6021<br>0.9542 |
|       | CV % =           | 57.5325           | Skewness   | ; =         | 0.3839                | 3rd Quart           | ;ile =          | 1.204]           |
|       |                  |                   |            |             |                       |                     |                 | 0 454            |
|       | Ant              | i-Log Mean        | = 8.32     | 23          | Anti-Log              | Std. Dev.           | · · (-)         | 2+455            |
|       |                  |                   |            |             |                       |                     | (+)             | 20.10.           |
| ===== | ======           | ================= |            | =====       | =========             |                     |                 | ========         |
| %     | cum %            | antilog           | cls int    | (# of       | bins = 28             | 8 - bin             | size =          | 0.1241           |
|       |                  |                   |            |             |                       |                     |                 |                  |
| 0.00  | 0.10             | 0.867             | -0.0620    |             |                       |                     |                 |                  |
| 10.47 | 10.55            |                   | 0.0620     | *****       | ********              | * * * * * * * * *   |                 |                  |
| 0.00  | 10.55            | 1.535             | 0.1861     | *****       | * * * * * * * *       |                     |                 |                  |
| 0.32  | 10.00            | 2.043             | 0.3102     |             |                       |                     |                 |                  |
| 0.00  | 10.00<br>01 40   |                   | 0.4343     | * * * * * * | * * * *               |                     |                 |                  |
| 4.00  | 21.40            | 3+017             | 0.6925     | ****        | * * * * * * * * * * * | *                   |                 |                  |
| 11 07 | 20.70            | 6 4013            | 0.0025     | *****       | * * * * * * * * * *   | * * * * * * * * *   |                 |                  |
| 7 01  | 17 63            | 9 524             | 0.0306     | * * * * * * | * * * * * * * * * *   | * *                 |                 |                  |
| 1/ 23 | 61 83            | 11 342            | 1 0547     | ****        | * * * * * * * * * *   | ******              | *****           |                  |
| 12 65 | 74 46            | 15 094            | 1,1788     | * * * * * * | * * * * * * * * * *   | * * * * * * * * * * | * * *           |                  |
| 4.74  | 79.19            | 20.085            | 1.3029     | ****        | * * * * *             |                     |                 |                  |
| 5.14  | 84.32            | 26.727            | 1.4270     | ****        | * * * * * *           |                     |                 |                  |
| 5.14  | 89.45            | 35.566            | 1.5510     | * * * * *   | * * * * * *           |                     |                 |                  |
| 4.35  | 93.79            | 47.329            | 1.6751     | *****       | * * * *               |                     |                 |                  |
| 1.38  | 95.17            | 62.981            | 1.7992     | * * *       |                       |                     |                 |                  |
| 1.38  | 96.55            | 83.809            | 1.9233     | * * *       |                       |                     |                 |                  |
| 1.38  | 97.93            | 111.525           | 2.0474     | * * *       |                       |                     |                 |                  |
| 0.59  | 98.52            | 148.408           | 2.1715     | *           |                       |                     |                 |                  |
| 0.59  | 99.11            | 197.488           | 2.2955     | *           |                       |                     |                 |                  |
| 0.00  | 99.11            | 262.799           | 2.4196     |             |                       |                     |                 |                  |
| 0.20  | 99.31            | 349.709           | 2.5437     |             |                       |                     |                 |                  |
| 0.20  | 99.51            | 465.361           | 2.6678     |             |                       |                     |                 |                  |
| 0.00  | 99.51            | 619.260           | 2.7919     |             |                       |                     |                 |                  |
| 0.00  | 99.51            | 824.056           | 2.9160     |             |                       |                     |                 |                  |
| 0.00  | 99.51            | 1096.579          | 3.0400     |             |                       |                     |                 |                  |
| 0.00  | 99.51            | 1459.228          | 3.1641     |             |                       |                     |                 |                  |
| 0.20  | .99.70           | 1941.808          | 3.2882     |             |                       |                     |                 |                  |
| 0.20  | 99.90            | 2583.983          | 3.4123     |             |                       |                     |                 |                  |
|       |                  |                   |            |             | <br>1 <sup>-</sup>    |                     | - <b></b>       |                  |

Each "\*" represents approximately 2.4 observations

\*\*\*\*

09:38:59 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/16/91

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = 16-SOILS.DAT

Variable = Ag Unit = ppm N = 506 N CI = 28 Transform = Logarithmic Number of Populations = 2 # of Missing Observations = 0.

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1577.878

Parameterized Degrees of Freedom = 3

| Population | Mean  |   | Std Dev | Percentag |  |  |
|------------|-------|---|---------|-----------|--|--|
|            |       | - |         |           |  |  |
| 1          | 0.431 | - | 0.160   | 95.95     |  |  |
|            |       | ÷ | 1.165   |           |  |  |
| 2          | 2.430 | - | 1.476   | 4.05      |  |  |
|            |       | + | 4.000   |           |  |  |

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thres | holds |
|------|-------|-------|
|      |       | -~~   |
| 1    | 0.059 | 3.144 |
| 2    | 0.897 | 6.584 |

\*\*\*\*\*\*\*\*\*\*\*



.

09:08:09 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16

11/16/90

\*\*\*\* SUMMARY STATISTICS and HISTOGRAM LOGARITHMIC VALUES

| Vari  | able =           | Ag                | Uni      | t =        | ppm                 |                           | N =             | 506                |
|-------|------------------|-------------------|----------|------------|---------------------|---------------------------|-----------------|--------------------|
| Std.  | Mean =<br>Dev. = | -0.3274<br>0.4598 | Mi<br>Ma | n =<br>x = | -1.0000             | 1st Quart:<br>Med         | ile =<br>ian =  | -0.6990<br>-0.3010 |
|       | CV % =           | 140.4373          | Skewnes  | s =        | 0.2434              | 3rd Quart:                | ile =           | 0.0000             |
|       | Anti             | -Log Mean         | = 0.4    | 71         | Anti-Log            | Std. Dev.                 | : (-)           | 0.163              |
|       |                  |                   |          |            |                     |                           | (+)             | 1.356              |
|       |                  |                   |          |            |                     |                           |                 |                    |
| %     | cum %            | antilog           | cls int  | (# of      | bins = 20           | 8 - bin :                 | size =          | 0.0823)            |
|       |                  |                   |          |            |                     |                           |                 |                    |
| 0.00  | 0.10             | 0.091             | -1.0412  |            |                     |                           |                 |                    |
| 17.79 | 17.85            | 0.110             | -0.9588  | * * * * *  | ********            | * * * * * * * * * * * *   | * * * * * * * * | * * * * * *        |
| 0.00  | 17.85            | 0.133             | -0.8765  |            |                     |                           |                 |                    |
| 0.00  | 17.85            | 0.161             | -0.7942  |            |                     |                           |                 |                    |
| 0.00  | 17.85            | 0.194             | -0.7119  |            |                     |                           |                 |                    |
| 12.65 | 30.47            | 0.235             | -0.6295  | * * * * *  | ******              | * * * * * * * * * * * * * | * *             |                    |
| 0.00  | 30.47            | 0.284             | -0.5472  |            |                     |                           |                 | ·                  |
| 7.51  | 37.97            | 0.343             | -0.4649  | * * * * *  | ****                | * *                       |                 |                    |
| 9.09  | 47.04            | 0.414             | -0.3826  | * * * * *  | * * * * * * * * * * | * * * * *                 |                 |                    |
| 7.11  | 54.14            | 0.501             | -0.3003  | * * * * *  | *******             | *                         |                 |                    |
| 5.73  | 59.86            | 0.605             | -0.2179  | * * * * *  | * * * * * * *       |                           |                 |                    |
| 6.72  | 66.57            | 0.732             | -0.1356  | * * * * *  | * * * * * * * * *   |                           |                 |                    |
| 3.95  | 70.51            | 0.885             | -0.0533  | * * * * *  | * * *               |                           |                 |                    |
| 8.70  | 79.19            | 1.069             | 0.0290   | * * * * *  | * * * * * * * * * * | * * * *                   |                 |                    |
| 3.56  | 82.74            | 1.292             | 0.1114   | * * * * *  | * *                 |                           |                 |                    |
| 3.95  | 86.69            | 1.562             | 0.1937   | ****       | * * *               |                           |                 |                    |
| 2.96  | 89.64            | 1.888             | 0.2760   | * * * * *  | *                   |                           |                 |                    |
| 3.95  | 93.59            | 2.282             | 0,3583   | * * * * *  | * * *               |                           |                 |                    |
| 1.78  | 95.36            | 2.758             | 0.4406   | * * * *    |                     |                           |                 |                    |
| 1.38  | 96.75            | 3.334             | 0.5230   | * * *      |                     |                           |                 |                    |
| 0.40  | 97.14            | 4.030             | 0.6053   | *          |                     |                           |                 |                    |
| 0.99  | 98.13            | 4.871             | 0.6876   | * *        |                     |                           |                 |                    |
| 0.40  | 98.52            | 5.888             | 0.7699   | *          |                     |                           |                 |                    |
| 0.59  | 99.11            | 7.116             | 0.8523   | *          |                     |                           |                 |                    |
| 0.40  | 99.51            | 8.602             | 0.9346   | *          |                     |                           |                 |                    |
| 0.00  | 99.51            | 10.397            | 1.0169   |            |                     |                           |                 |                    |
| 0.00  | 99.51            | 12.567            | 1.0992   |            |                     |                           |                 |                    |
| 0.20  | 99.70            | 15,190            | 1.1816   |            |                     |                           |                 |                    |
| 0.20  | 99.90            | 18.360            | 1.2639   |            |                     |                           |                 |                    |
|       |                  |                   |          |            |                     |                           |                 |                    |
|       |                  |                   | t        | 0          | 1                   | 2                         | 3               | 4                  |

Each "\*" represents approximately 2.4 observations.

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = 16-SOILS.DAT

| Variable =   | Мо      | Unit =     | ppm         | N =            | 506 |
|--------------|---------|------------|-------------|----------------|-----|
|              |         |            |             | N CI =         | 28  |
| Transform    | = Logar | ithmic     | Number of P | opulations = 2 | 2   |
| # of Missing | Observa | tions = 0. |             |                |     |

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1506.892

Parameterized Degrees of Freedom = 3

| Population | Mean   |          | Std Dev | Percentage |  |  |
|------------|--------|----------|---------|------------|--|--|
|            |        | -        |         |            |  |  |
| 1          | 2.627  | <u> </u> | 1.334   | 87.76      |  |  |
|            |        | +        | 5.172   |            |  |  |
| 2          | 24.917 | -        | 13.167  | 12.24      |  |  |
|            |        | +        | 47.154  |            |  |  |

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Three | Thresholds |  |  |  |  |
|------|-------|------------|--|--|--|--|
|      |       |            |  |  |  |  |
| 1    | 0.678 | 10.184     |  |  |  |  |
| 2    | 6.957 | 89.236     |  |  |  |  |

\*\*\*\*



. I...

09:56:46 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/16/9

| Vari                          | able                             | = Mo                              | Uni                                   | .t =                                          | ppm                        |                               | N =                      | 506                        |
|-------------------------------|----------------------------------|-----------------------------------|---------------------------------------|-----------------------------------------------|----------------------------|-------------------------------|--------------------------|----------------------------|
| Std.                          | Mean<br>Dev. :<br>CV % :         | = 0.5317<br>= 0.4296<br>= 80.7964 | Mi<br>Ma<br>Skewnes                   | .n =<br>ax =<br>as =                          | 0.0000<br>2.1492<br>1.1675 | lst Quart<br>Med<br>3rd Quart | ile =<br>lian =<br>ile = | 0.3010<br>0.4771<br>0.6990 |
|                               | Ant                              | i-Log Mean                        | = 3.4                                 | 02                                            | Anti-Log                   | Std. Dev.                     | : (-)<br>(+)             | 1.265<br>9.146             |
| =====<br>%                    | cum %                            | antilog                           | cls int                               | (# of                                         | bins = 20                  | 8 - bin                       | size =                   | 0.0796                     |
| 0.00<br>17.39<br>0.00<br>0.00 | 0.10<br>17.46<br>17.46<br>17.46  | 0.912<br>1.096<br>1.316<br>1.581  | -0.0398<br>0.0398<br>0.1194<br>0.1990 | ****                                          | * * * * * * * * * *        | ****                          | ****                     |                            |
| 0.00                          | 17.46                            | 1.899<br>2.281                    | 0.2786                                | * * * * * :                                   | * * * * * * * * * *        | * * * * * * * * * *           | ******                   | > 4                        |
| 0.00<br>21.15<br>0.00         | 40.93<br>62.03<br>62.03<br>73.27 | 2.740<br>3.292<br>3.954<br>4.749  | 0.4378<br>0.5174<br>0.5970<br>0.6766  | * * * * * * * *                               | * * * * * * * * * * *      | * * * * * * * * * * *         | * * * * * * *            | > 4                        |
| 5.53<br>3.16<br>2.57          | 78.80<br>81.95<br>84.52          | 5.704<br>6.852<br>8.230           | 0.7562<br>0.8358<br>0.9154            | * * * * * * *<br>* * * * * * *<br>* * * * * * | * * * * *                  |                               |                          |                            |
| 1.58<br>1.19<br>1.98          | 86.09<br>87.28<br>89.25          | 9.886<br>11.874<br>14.263         | 0.9950<br>1.0746<br>1.1542            | * * *<br>* *<br>* * * *                       |                            |                               |                          |                            |
| 2.17<br>1.38<br>2.17          | 91.42<br>92.80<br>94.97          | 17.132<br>20.578<br>24.718        | 1.2338<br>1.3134<br>1.3930            | * * * *<br>* * *<br>* * * *                   |                            |                               |                          |                            |
| 0.79<br>1.19<br>0.40          | 95.76<br>96.94<br>97.34          | 29.690<br>35.663<br>42.837        | 1.4726<br>1.5522<br>1.6318            | * *<br>* *<br>*                               |                            |                               |                          |                            |
| 0.40<br>0.20<br>0.40          | 97.73<br>97.93<br>98.32          | 51.454<br>61.804<br>74.236        | 1.7114<br>1.7910<br>1.8706            | *                                             |                            |                               |                          |                            |
| 0.59<br>0.79<br>0.00<br>0.20  | 98.92<br>99.70<br>99.70<br>99.90 | 107.107<br>128.653<br>154.532     | 1.9502<br>2.0298<br>2.1094<br>2.1890  | ≍<br>★ ★                                      |                            |                               |                          |                            |
|                               |                                  |                                   |                                       | <b></b> -<br>0                                | 1                          | 2                             | 3                        | ·                          |

Each "\*" represents approximately 2.4 observations

\*\*\*\*\*\*\*\*\*\*\*\*

16:40:40 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/10/9

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = 16-SOILS.DAT

| Variable =   | Cu      | Unit =     | ppm          | N =<br>N CI =  | 506<br>28 |
|--------------|---------|------------|--------------|----------------|-----------|
| Transform    | = Logar | ithmic     | Number of Po | opulations = 2 |           |
| # of Missing | Observa | tions = 0. |              |                |           |

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1385.193

Parameterized Degrees of Freedom = 3

| Population | Mean    |   | Std Dev | Percentage |  |
|------------|---------|---|---------|------------|--|
| ~~~~~~~~~  |         | - |         |            |  |
| 1          | 28.411  | _ | 11.118  | 98.49      |  |
|            |         | + | 72.602  |            |  |
| 2          | 432.714 | - | 208.852 | 1.51       |  |
|            |         | + | 896.527 |            |  |

Default Thresholds.

Standard Deviation Multiplier = 2.0

Pop. Thresholds 1 4.351 185.526 2 100.804 1857.485

\*\*\*\*\*



t E

Land Kanal

. 1

. .

16:41:24 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/10/9

| Variable =                                                                                                                                                                                                                                                                                                                                                           | Cu                                                                                                                                                                                                                                                                               | Unit                                                                                                                                                                                                                                                                       | =                                       | ppm                                    |                                                                                       | N =                | 506                        |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------|----------------------------------------|---------------------------------------------------------------------------------------|--------------------|----------------------------|
| Mean =<br>Std. Dev. =<br>CV % =                                                                                                                                                                                                                                                                                                                                      | 1.4785<br>0.4429<br>29.9574                                                                                                                                                                                                                                                      | Min<br>Max<br>Skewness                                                                                                                                                                                                                                                     | =                                       | 0.3010<br>3.4017<br>0.4268             | lst Quartil<br>Media<br>3rd Quartil                                                   | e =<br>in =<br>e = | 1.176]<br>1.4771<br>1.7559 |
| Anti                                                                                                                                                                                                                                                                                                                                                                 | -Log Mean                                                                                                                                                                                                                                                                        | = 30.09                                                                                                                                                                                                                                                                    | 7                                       | Anti-Log                               | Std. Dev. :                                                                           | ( - )<br>( + )     | 10.854<br>83.454           |
| ======================================                                                                                                                                                                                                                                                                                                                               | antilog                                                                                                                                                                                                                                                                          | cls int                                                                                                                                                                                                                                                                    | =====<br>(# of                          | ====================================== | <br>3 - bin si                                                                        | ======<br>2e =     | ======<br>0.1148           |
| 0.00 $0.100.20$ $0.300.00$ $0.300.79$ $1.082.77$ $3.851.58$ $5.424.94$ $10.367.11$ $17.466.72$ $24.169.29$ $33.438.70$ $42.1111.66$ $53.7510.67$ $64.408.70$ $73.088.89$ $81.955.73$ $87.674.15$ $91.813.16$ $94.971.38$ $96.351.58$ $97.930.59$ $98.520.20$ $98.720.20$ $98.720.20$ $98.720.20$ $98.720.20$ $98.920.20$ $99.110.20$ $99.310.40$ $99.700.00$ $99.70$ | 1.752<br>2.283<br>2.974<br>3.874<br>5.046<br>6.574<br>8.564<br>11.156<br>14.532<br>18.931<br>24.662<br>32.127<br>41.851<br>54.519<br>71.021<br>92.519<br>120.523<br>157.004<br>204.528<br>266.437<br>347.085<br>452.144<br>589.004<br>767.289<br>999.541<br>1302.092<br>1696.224 | 0.2436<br>0.3585<br>0.4733<br>0.5881<br>0.7030<br>0.8178<br>0.9327<br>1.0475<br>1.1623<br>1.2772<br>1.3920<br>1.5069<br>1.6217<br>1.7365<br>1.8514<br>1.9662<br>2.0811<br>2.1959<br>2.3108<br>2.4256<br>2.5404<br>2.6553<br>2.7701<br>2.8850<br>2.9998<br>3.1146<br>3.2295 | * * * * * * * * * * * * * * * * * * * * | * * * * * * * * * * * * * * * * * * *  | * * * * *<br>* * * * * * * * * * * * *<br>* * * * * * * * * *<br>* * * * *<br>* * * * |                    |                            |
| 0.20 99.90                                                                                                                                                                                                                                                                                                                                                           | 2878.497                                                                                                                                                                                                                                                                         | 3.4592                                                                                                                                                                                                                                                                     |                                         |                                        | <b>-</b><br>7                                                                         | <br>2              |                            |

ή

Each "\*" represents approximately 2.4 observations

\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\*

11:46:52 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/12/9 PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS Data File Name = 16-SOILS.DAT 505 Variable = Pb Unit = N = ppmN CI =28 Number of Populations = 2 Transform = Logarithmic

# of Missing Observations = 0.

0 Observations Were Below the Minimum Value of 1.0000 1 Observations Were Above the Maximum Value of 500.0000

3

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1526.177

Parameterized Degrees of Freedom =

| Population | Mean    |   | Std Dev | Percentage |
|------------|---------|---|---------|------------|
|            |         | _ |         |            |
| 1          | 13.803  | _ | 5.367   | 99.47      |
|            |         | + | 35.499  |            |
| 2          | 124.319 | - | 85.053  | 0.53       |
|            |         | + | 181.715 |            |

Default Thresholds.

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds |         |  |  |  |
|------|------------|---------|--|--|--|
|      |            |         |  |  |  |
| 1    | 2.087      | 91.294  |  |  |  |
| 2    | 58.189     | 265.608 |  |  |  |

\*\*\*\*\*\*



. . ·

• .

11:38:00 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/12/

| Vari  | able =                     | e Pb                        | Uni                    | ; =               | ppm                         |                         | N =                              | 505                     |
|-------|----------------------------|-----------------------------|------------------------|-------------------|-----------------------------|-------------------------|----------------------------------|-------------------------|
| std.  | Mean =<br>Dev. =<br>CV % = | 1.1476<br>0.4317<br>37.6127 | Min<br>Max<br>Skewnes: | ) =<br>( =<br>3 = | 0.3010<br>2.5944<br>-0.0903 | 1st Qua<br>1<br>3rd Qua | artile =<br>Median =<br>artile = | 0.903<br>1.146<br>1.431 |
|       | Ant                        | i-Log Mean                  | = 14.04                | 19                | Anti-Log                    | Std. D                  | ev. : (-)<br>(+)                 | 5.20<br>37.95           |
| ===== | ======                     | ===============             |                        |                   |                             |                         |                                  |                         |
| %     | cum %                      | antilog                     | cls int                | (# of             | bins = 28                   | <b>3</b> – b:           | in size =                        | 0.084                   |
| 0 00  | 0 10                       | 1.814                       | 0.2586                 |                   |                             |                         |                                  |                         |
| 8 32  | 8 40                       | 2,205                       | 0.3435                 | ****              | ******                      | * * *                   |                                  |                         |
| 0.00  | 8.40                       | 2.682                       | 0.4284                 |                   |                             |                         |                                  |                         |
| 2.18  | 10.57                      | 3,261                       | 0.5134                 | * * * *           |                             |                         | •                                |                         |
| 0.00  | 10.57                      | 3,966                       | 0.5983                 |                   |                             |                         |                                  |                         |
| 2.97  | 13.54                      | 4,822                       | 0.6833                 | * * * * *         | *                           |                         |                                  | •                       |
| 3.76  | 17.29                      | 5.864                       | 0.7682                 | * * * * *         | * * *                       |                         |                                  |                         |
| 6.73  | 24.01                      | 7.131                       | 0.8531                 | * * * * *         | *****                       |                         |                                  |                         |
| 2.57  | 26.58                      | 8.671                       | 0.9381                 | ****              |                             |                         |                                  |                         |
| 6.34  | 32.91                      | 10.544                      | 1.0230                 | * * * * *         | * * * * * * * *             |                         |                                  |                         |
| 9.50  | 42.39                      | 12.822                      | 1.1080                 | * * * * *         | * * * * * * * * * *         | *****                   |                                  |                         |
| 10.89 | 53.26                      | 15.592                      | 1.1929                 | * * * * *         | * * * * * * * * * *         | ******                  | k                                |                         |
| 7.92  | 61.17                      | 18.960                      | 1.2778                 | * * * * *         | * * * * * * * * * *         | : <b>*</b>              |                                  |                         |
| 9.90  | 71.05                      | 23.055                      | 1.3628                 | * * * * *         | * * * * * * * * * *         | *****                   |                                  |                         |
| 5.54  | 76.58                      | 28.036                      | 1.4477                 | * * * * *         | * * * * * *                 |                         |                                  |                         |
| 5.94  | 82.51                      | 34.092                      | 1.5327                 | ****              | * * * * * * *               |                         |                                  |                         |
| 4.95  | 87.45                      | 41.456                      | 1.6176                 | * * * * *         | * * * * *                   |                         |                                  |                         |
| 3.56  | 91.01                      | 50.411                      | 1.7025                 | * * * * *         | * *                         |                         |                                  |                         |
| 3.56  | 94.57                      | 61.301                      | 1.7875                 | ****              | * *                         |                         |                                  |                         |
| 0.79  | 95.36                      | 74.543                      | 1.8724                 | * *               |                             |                         |                                  |                         |
| 1.78  | 97.13                      | 90.646                      | 1.9573                 | * * * *           |                             |                         |                                  |                         |
| 0.99  | 98.12                      | 110.227                     | 2.0423                 | * *               |                             |                         |                                  |                         |
| 0.40  | 98.52                      | 134.037                     | 2.1272                 | *                 |                             |                         |                                  |                         |
| 0.59  | 99.11                      | 162.992                     | 2.2122                 | *                 |                             |                         |                                  |                         |
| 0.40  | 99.51                      | 198.201                     | 2.2971                 | *                 |                             |                         |                                  |                         |
| 0.20  | 99.70                      | 241.015                     | 2.3820                 |                   |                             |                         |                                  |                         |
| 0.00  | 99.70                      | 293.078                     | 2.4670                 |                   |                             |                         |                                  |                         |
| 0.00  | 99.70                      | 356.388                     | 2.5519                 |                   |                             |                         |                                  |                         |
| 0.20  | 99.90                      | 433.373                     | 2.6369                 |                   |                             |                         |                                  |                         |
|       |                            |                             |                        |                   |                             | 2                       |                                  |                         |

h

ł

Each "\*" represents approximately 2.4 observation:

\*\*\*\*

09:29:25 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/16/5

PARAMETER SUMMARY STATISTICS FOR PROBABILITY PLOT ANALYSIS

Data File Name = 16-SOILS.DAT

Variable = Zn Unit = ppm N = 506 N CI = 28 Transform = Logarithmic Number of Populations = 2 # of Missing Observations = 0.

Class Interval Data Maximum Likelihood Parameter Estimates

Maximum LN Likelihood Value = -1389.340

Parameterized Degrees of Freedom = 3

| Population | Mean     |   | Std Dev  | Percentage |  |
|------------|----------|---|----------|------------|--|
|            |          | - |          |            |  |
| 1          | 106.517  | _ | 43.828   | 96.51      |  |
|            |          | + | 258.874  |            |  |
| 2          | 1282.004 | - | 574.068  | 3.49       |  |
|            |          | + | 2862.964 |            |  |

\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_

Default Thresholds.

ŧ

Standard Deviation Multiplier = 2.0

| Pop. | Thresholds |          |  |  |  |
|------|------------|----------|--|--|--|
|      |            |          |  |  |  |
| 1    | 18.033     | 629.156  |  |  |  |
| 2    | 257.061    | 6393.552 |  |  |  |

\*\*\*\*



09:27:26 SOIL GEOCHEMISTRY - LARK PROPERTY - R9003-16 11/16/9

1

| ·      | 'aria        | able =                       | Zn                                    | Un               | it =                 | ppm                        |                  |                                  | 506                        |
|--------|--------------|------------------------------|---------------------------------------|------------------|----------------------|----------------------------|------------------|----------------------------------|----------------------------|
| St     | il<br>d. 1   | Mean ;=<br>Dev. =<br>CV:% ;= | 3:::! 2.0615<br>0.4394<br>E:: 21.3159 | M<br>M<br>Skewne | in =<br>ax =<br>ss = | 1.0792<br>4.0835<br>0.8004 | 1st Qu<br>3rd Qu | artile =<br>Median =<br>artile = | 1.7404<br>2.0043<br>2.3253 |
| ٤      | :            | Ant                          | i⊢Log Mean                            | = 115.           | 212                  | Anti-Log                   | Std. D           | ev. : (-)<br>(+)                 | 41.886<br>316.904          |
| ==     | ====<br>%: ( | cum:%                        | antilog                               | cls int          | ======<br>(# of      | bins = 28                  |                  | =========<br>in size =           | 0.1113                     |
|        | •00          | 0.10                         | 10.557                                | 1.0235           | <br>,                |                            |                  | · · · · ·                        |                            |
| 0      | .20          | 0.30                         | 13.640                                | 1.1348           | ,                    |                            |                  | · · ·                            |                            |
| 0      | .79          | 1.08                         | 17.623                                | 1.2461           | * *                  |                            |                  | •                                |                            |
| 1      | .38          | 2.47                         | 22.770                                | 1.3574           | * * *                |                            | \$               | .: Ex.*                          |                            |
| 3      | .36          | 5.82                         | 29.419                                | 1.4686           | ****                 | * *                        |                  | tin tink ∰                       |                            |
| 4      | .74          | 10.55                        | 38.011                                | 1.5799           | ****                 | * * * * *                  |                  | . 1                              |                            |
| ģ      | .09          | 19.63                        | 49,111                                | 1.6912           | * * * * *            | *******                    | ****             |                                  |                            |
| 11     | .26          | 30.87                        | 63.453                                | 1.8025           | * * * * *            | ****                       | *****            | ** .                             |                            |
| 11     | .66          | 42.50                        | 81,983                                | 1,9137           | ****                 | ****                       | ******           | *** 1.                           |                            |
| - A    | 80           | 51 38                        | 105,925                               | 2 0250           | ****                 | * * * * * * * * * *        | ****             | 13 <sup>11</sup> 14              |                            |
| a      | 09           | 60 15                        | 136 858                               | 2.0200           | * * * * *            | * * * * * * * * * *        | ****             | 1                                |                            |
| 0      | + U 9<br>6 R | 70 12                        | 130+030                               | 2 2 2 3 0 5      | * * * * *            | * * * * * * * * * * *      | * * * * * *      |                                  |                            |
| ר<br>ה | +00<br>50    | 76 63                        | 228 162                               | 2 2 3 5 8 8      | * * * * *            | *******                    | ۰.               |                                  |                            |
| 6      | 12           | 0.0J                         | 220.402                               | 2.5500           | * * * * *            | * * * * * * * *            | · · ·            |                                  |                            |
| 5      | •1J          | 87 87                        | 293+100                               | 2.5911           | * * * * *            | * * * * * *                |                  |                                  |                            |
| 2      | •14          | 01 01                        | 402 756                               | 2.5014           | ****                 | ***                        |                  | ••                               |                            |
| ວ<br>າ | • 90<br>06   | $01 \cdot 01$                | 492.700                               | 2.0920           | *****                | *                          |                  |                                  |                            |
| 2      | • 90         | 74+//                        | 030.030                               | 2.0039           | **                   |                            | 1. A.            |                                  |                            |
| 1      | •19          | 90.90                        | 822.078                               | 2.9132           | * * *                |                            |                  |                                  |                            |
| 1      | . 38         | 97.03                        | 1002.790                              | 3.0264           | * *                  |                            |                  |                                  |                            |
| 0      | • / 9        | 98.32                        | 13/3+164                              | 3.13//           | ~ ~                  |                            |                  | •                                |                            |
| Ű      | • 20         | 98.52                        | 1//4.168                              | 3.2490           |                      |                            |                  | * F                              |                            |
| U      | •59          | 99.11                        | 2292.278                              | 3:3603           | × ,                  |                            |                  | . <b>.</b>                       |                            |
| 0      | •00          | 99.11                        | 2961.691                              | 3.4715           |                      |                            | •                | •                                |                            |
| 0      | •20          | 99.31                        | 3826.593                              | 3.5828           | ,                    |                            |                  | •                                |                            |
| 0      | •00          | 99.31                        | 4944.071                              | 3.6941           |                      |                            |                  |                                  |                            |
| 0      | .20          | 99.51                        | 6387.887                              | 3.8054           | •                    |                            |                  | -                                |                            |
| 0      | .20          | 99.70                        | 8253.340                              | 3.9166           |                      | · ·                        |                  | , <del>!</del> . !               |                            |
| 0      | .00          | 99.70                        | 10663.560                             | 4.0279           |                      |                            | i i'             | • · · · ·                        |                            |
| 0      | .20          | 99.90-                       | 13777.636                             | 4.1392           |                      | **                         | •                |                                  |                            |
|        |              |                              |                                       |                  |                      |                            | 2                | 3                                |                            |

, Frag

Each "\*" represents approximately 2.4 observations

6 44 FL

11

11.11.15





.

.

![](_page_63_Figure_0.jpeg)

![](_page_64_Picture_0.jpeg)

![](_page_65_Picture_0.jpeg)

•

![](_page_65_Picture_1.jpeg)

Ý, Ú,

![](_page_66_Picture_0.jpeg)

![](_page_67_Picture_0.jpeg)

![](_page_68_Picture_0.jpeg)

![](_page_68_Picture_1.jpeg)

![](_page_69_Picture_0.jpeg)

![](_page_69_Picture_1.jpeg)

![](_page_70_Picture_0.jpeg)

| <i>ž</i> y                                                         |                                       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |   |
|--------------------------------------------------------------------|---------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---|
|                                                                    | GEOLOGI<br>ASSESSM                    | CALBRANCH -                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | ( |
| 1060014                                                            | 20,                                   |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |   |
| 1050 10400 1                                                       |                                       | EARLY JURASSIC<br><u>COAST PLUIONIC COMPLEX</u><br>[eJgd] medium grained, hornblende, biotite granodiorite.<br>UPPER TRIASSIC<br><u>SIUHINI GROUP</u>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |   |
| * . * 10200 <sup>11</sup>                                          |                                       | uTv       Light to dark green, massive, andesitic pyroxene porphyry flows and tuffs.         uTs       dark to medium grey, weakly gossanous, occasionally carbonaceous argillite.         uTs       extremely siliceous light green siltstone or chert, with 3-5% pyrite.         PERMIAN       SILKINF ASSEMBLAGE                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |   |
| 10000 - 10000 - 001                                                | •                                     | Image: Structure Assembly definition         Image: Structure Assembly d |   |
|                                                                    | 970014                                | contact; defined, assumed<br>v v fault: defined, assumed<br>bedding attitude<br>foliation<br>vein attitude<br>%, fault attitude                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |   |
| * uTv<br>* * *                                                     | 9600 <sup>11</sup> 950 <sup>011</sup> | <pre>     rock sample location     soil sample location      ABBREVIATIONS     PY    pyrite    PR    pyrrhotite     SM    smithsonite    HA    malachite </pre>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |   |
|                                                                    | 3400 <sup>1</sup>                     | 930011                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |   |
| x x<br>x x<br>x x<br>x x<br>x x<br>x x<br>x x<br>x x<br>x x<br>x x |                                       | 9200 <sup>01</sup><br>SCALE 1:5000<br>0 100 200                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |   |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$               |                                       | TICKER TAPE RESOURCES LTD.<br>LARKSPUR PROJECT<br>GRID GEOLOGY                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |   |
| x x<br>x x                                                         |                                       | To accompany a report by Andrew WilkinsProject No:Report No:Mining Div:LiardN.T.S.:Mining Div:LiardN.T.S.:104G/3Date:Nov.1990Map No:QUEST CANADA EXPLORATION SERVICES INC                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |   |

.

.

![](_page_71_Figure_0.jpeg)