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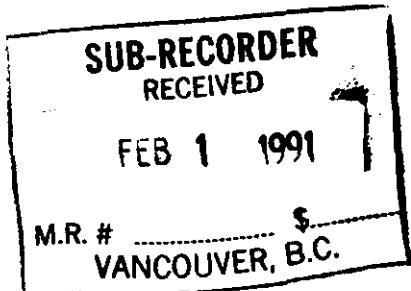
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NTS 92I / 3  
Lat 50°10'N  
Long 121°13'W

FILE NO:

GEOLOGICAL and GEOCHEMICAL  
REPORT  
on the  
MIME CLAIM GROUP  
Nicola Mining Division, B.C.

GEOLOGICAL BRANCH  
ASSESSMENT REPORT



for 20,912

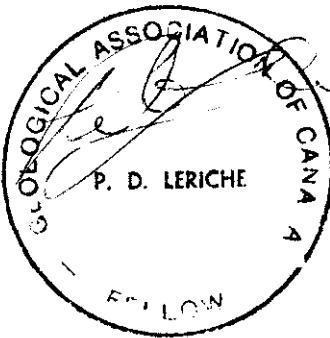
PACIFIC SENTINEL GOLD CORP.  
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by

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Date: 22 October 1990



## SUMMARY

During August and September 1990, Reliance Geological Services Inc carried out a Phase 1 geological-geochemical exploration program on the Mime property which consists of 4 contiguous mineral claims (80 units), located 35 kilometers west of Merritt, B.C.

Mining activity in the area has focused on the porphyry copper Highland Valley Camp camp which contained reserves of close to 2 billion tonnes grading approximately 0.45% copper equivalent in 1976. This camp remains a prolific copper producing area.

The Mime claims are underlain by Cretaceous Kingsvale Group amygdaloidal basalt flows and mid Tertiary feldspar porphyry. Mineralization is related to quartz-pyrite-chalcopyrite infilled shears and fractures within the feldspar porphyry unit. Alteration consists of silicification and pyritization of the porphyry adjacent to the mineralized shear zones.

The 1990 mapping, rock and soil sampling program outlined 3 target areas. Target Area #1 is a previous drilled area which includes: the Main Showing and intrusion breccia, a mineralized fracture system with results up to >10,000 ppm copper and 345 ppb gold, ten anomalous rock sample results up to 6392 ppm copper, two well defined areas of anomalous copper in soils, and a concentration of eleven gold anomalies in soils. Target Area #2 is a 3 point gold soil anomaly with results up to 990 ppb. Target Area #3 is the Barrie Creek drainage basin where a stream sediment sample assayed 540 ppb gold.

A Phase 2 exploration program has been recommended, consisting of gridding, geological mapping and sampling, soil sampling and backhoe trenching. The estimated cost is \$55,000.

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## 1.0 INTRODUCTION

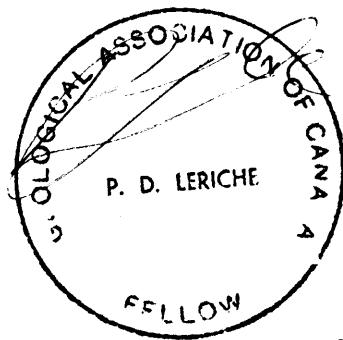
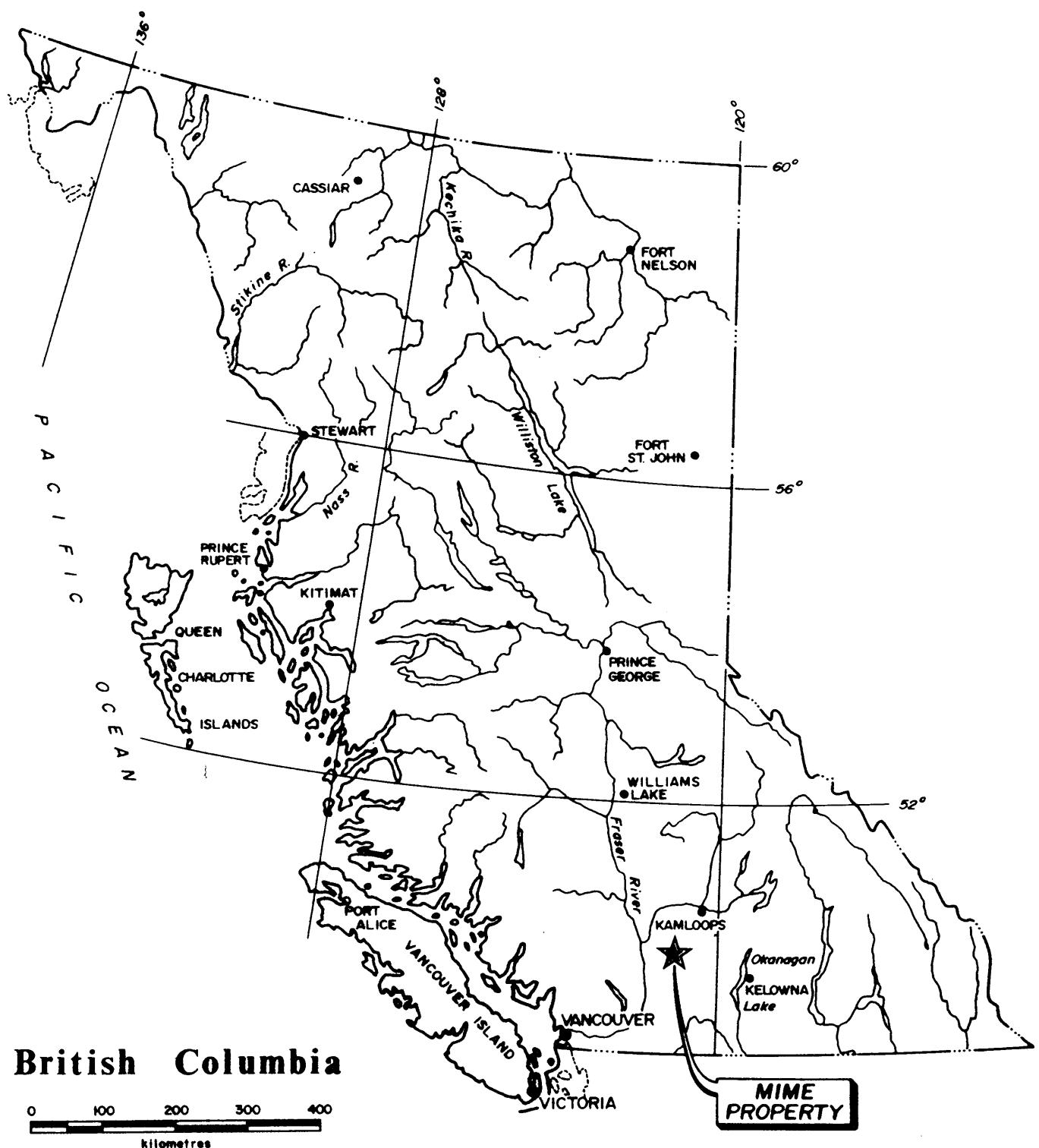
This report was prepared at the request of Pacific Sentinel Gold Corp to describe and evaluate the results of a geological-geochemical program carried out by Reliance Geological Services Inc on the Mime Property, Manning Creek area, B.C.

The field work was undertaken to evaluate the property for vein and/or shear hosted copper-gold potential. Field work was done by M. McLaren and B. Yorston (geologists) from August 1 to 8, 1990. Additional field work was carried out from August 20 to September 4, 1990, by Gordon Addie (geologist) and Andy Cooper (geotechnician), under the supervision of Peter Leriche, B.Sc., F.G.A.C., who was on the subject property on August 25 and 26.

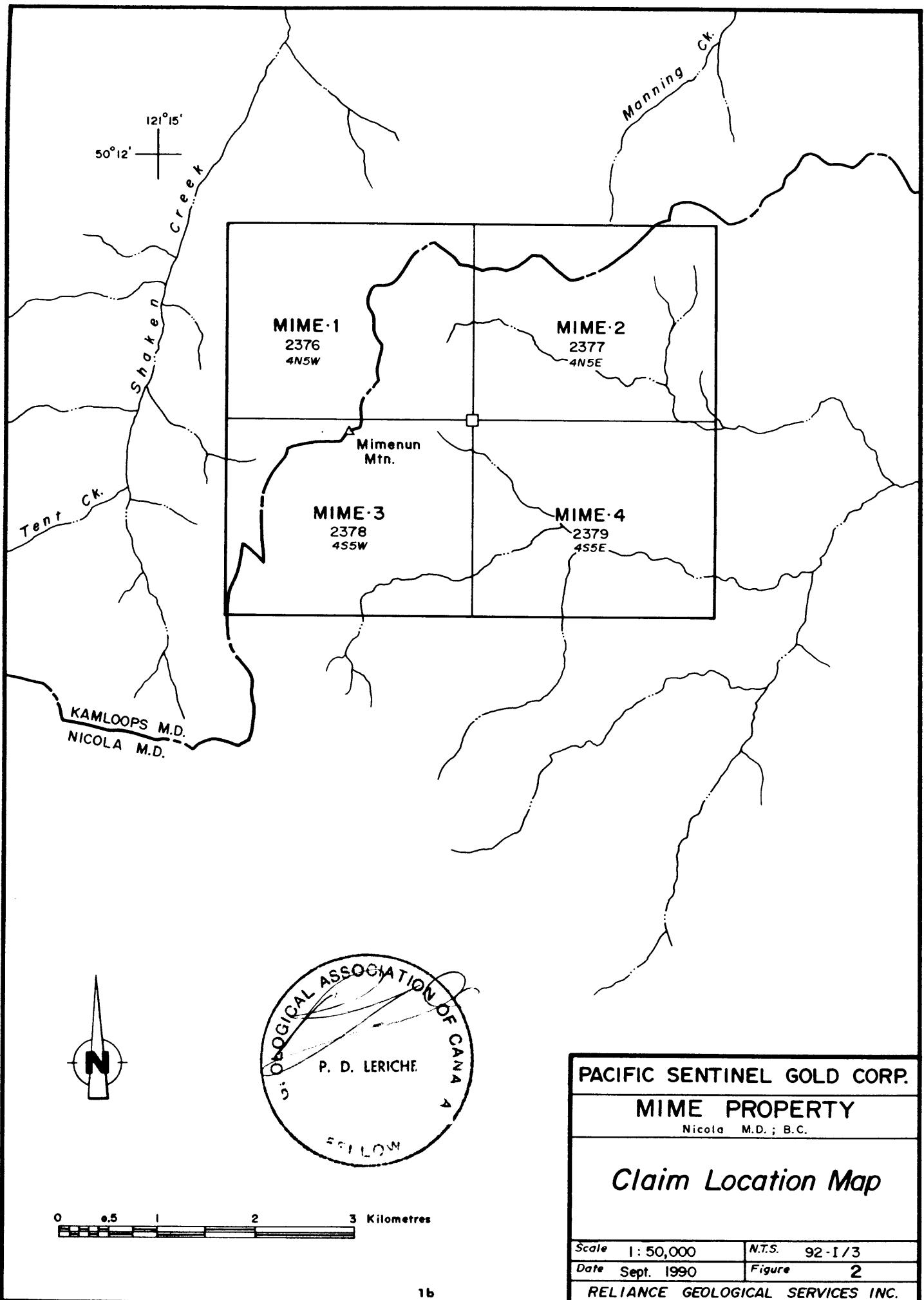
This report is based on the 1990 fieldwork, and on published and unpublished information supplied to the writer by Pacific Sentinel Gold Corp. The report also describes the area history, previous work, and regional geology, and makes recommendations for further work.

## 2.0 LOCATION, ACCESS AND PHYSIOGRAPHY

The Mime claims are situated in the Manning Creek area of south-central British Columbia, approximately 35 kilometers west of Merritt, B.C. (Figures 1 and 2). The claims lie within NTS Map Sheet 92I/3, at latitude 50°10' north, longitude 121°13' west, and between UTM 5557000 m and 5562000 m North and UTM 624000 m and 631000 m East.



|                                    |               |
|------------------------------------|---------------|
| <b>PACIFIC SENTINEL GOLD CORP.</b> |               |
| <b>MIME PROPERTY</b>               |               |
| Nicola M.D., B.C.                  |               |
| <b>General Location Map</b>        |               |
| Scale as shown                     | N.T.S. 92-1/3 |
| Date Sept. 1990                    | Figure 1      |
| RELIANCE GEOLOGICAL SERVICES INC.  |               |



Road access is via Highway 8 from Merritt, northwest 35 km to the village of Dot. From there, the Manning Creek logging road leads southwest for 18 km. The subject property is another 2 km south along a four-wheel drive road. A number of 4 x 4 roads cross the claims.

The property is on gentle to moderate terrain with slopes dipping in all directions from the peak of Mimenuh Mountain. Elevations vary from 6124 ft. (1867 m) at Mimenuh Mountain to 3400 ft (1036 m) on the eastern claim boundary for a total relief of 2724 ft (831 m). Drainage is to the east along Barrie, Shakan, Manning and Nuaitch Creeks to the Nicola River and into the Thompson-Fraser River system.

The area is relatively dry with vegetation consisting mainly of wide spaced lodge pole pine and Douglas fir.

The recommended field season is from mid-April to early November. Geophysical surveys and diamond drilling are feasible year-round.

### 3.0 PROPERTY STATUS

The property consists of four contiguous mineral claims (Figure 2) totalling 80 units in the Nicola Mining Division. The claims are registered in the name of United Mineral Services Ltd and are beneficially owned (100%) by Pacific Sentinel Gold Corp. Two placer claims, not owned by Pacific Sentinel Gold Corp, overlie Barrie Creek on the Mime 1 claim.

Details of the claim are as follows:

| <u>Claim</u> | <u>Record Number</u> | <u>Units</u> | <u>Record Date</u> | <u>Expiry Date</u> |
|--------------|----------------------|--------------|--------------------|--------------------|
| Mime 1       | 2376                 | 20           | 20 Apr 1990        | 20 Apr 1991        |
| Mime 2       | 2377                 | 20           | 20 Apr 1990        | 20 Apr 1991        |
| Mime 3       | 2378                 | 20           | 20 Apr 1990        | 20 Apr 1991        |
| Mime 4       | 2379                 | 20           | 20 Apr 1990        | 20 Apr 1991        |

The total area covered by the claims is 2000 hectares, or 4940 acres.

#### 4.0 AREA HISTORY

The mining history of the region has focused on the Highland Valley Camp (32 km NNE), a world-class copper producing area.

During the 1960's and early 1970's, 5 major porphyry copper deposits were developed within the Upper Triassic Guichon Creek Batholith. Reserves as of 1976 were as follows (McMillan, 1976):

| <u>Deposit</u> | <u>Tonnage<br/>(million tonnes)</u> | <u>Copper<br/>%</u> |
|----------------|-------------------------------------|---------------------|
| Bethlehem      | 55                                  | .47                 |
| Lornex         | 392                                 | .41                 |
| Valley         | 700                                 | .48                 |
| Hightmont      | 136                                 | .28                 |
| J.A.           | 260                                 | .43                 |
| Total          | 1,543                               | Avg. .41            |

McMillan (1976) reported aggregate ore reserves from the above and smaller deposits of almost 2 billion tonnes grading 0.45% copper equivalent.

The Craigmont Mine is located at the southern end of the Highland Valley camp, 19 km east of the subject property. The deposit is a copper-iron skarn hosted by Triassic Nicola Group volcanics and limestones. The Cretaceous Kingsvale Group unconformably overlies (200 m thick) the west end of the ore-body. The deposit was discovered in 1957-58, after drilling magnetic anomalies of extremely high intensity. Drill hole #15 (1958) intersected 195 meters grading 4.40% copper. The mine produced (underground and open pit) in excess of 36,400,000 tons grading approximately 1.29% copper until closure in 1982 (Briston, 1985).

#### 5.0 PREVIOUS WORK

The property (Copper Canyon Claims) was initially staked in the early 1960's by prospector L. Fournier of Merritt. The claims were optioned to Amalgamated Resources, then to Hurley River Gold Mines in 1962.

The target deposit in the early days of exploration was a Craigmont type orebody associated with high magnetics.

Nov. 1962 - May 1963: Hurley River Mines drilled 12 holes totalling approximately 5,000 ft., around Copper Canyon Creek.

Significant results include the following: (compiled from George Cross Newsletters, Hurley River News Releases, Drill Logs, Assay Sheets)

| Hole #            | Intersection |         | Interval<br>(ft) | Copper<br>(%) |
|-------------------|--------------|---------|------------------|---------------|
|                   | From (ft)    | To (ft) |                  |               |
| 1                 | 0            | 265     | 265              | 0.22          |
| 2<br>incl<br>incl | 245          | 415     | 170              | 0.55          |
|                   | 350          | 415     | 65               | 1.03          |
|                   | 350          | 370     | 20               | 2.21          |

| <u>Hole #</u>     | <u>Intersection</u> |                | <u>Interval</u> | <u>Copper</u> |
|-------------------|---------------------|----------------|-----------------|---------------|
|                   | <u>From (ft)</u>    | <u>To (ft)</u> | <u>(ft)</u>     | <u>(%)</u>    |
| 3                 | 20                  | 98             | 78              | 0.60          |
|                   | 184                 | 245            | 61              | 0.26          |
|                   | 245                 | 415            | 170             | 0.55          |
| 4<br>incl         | 28                  | 218            | 190             | 0.63          |
|                   | 58                  | 118            | 60              | 1.30          |
| 6<br>incl<br>incl | 60                  | 170            | 110             | 0.61          |
|                   | 60                  | 130            | 70              | 0.89          |
|                   | 80                  | 110            | 30              | 1.21          |

Little information is available for drill holes 7 to 12. Holes 7, 9, 10, were reported to intersect "low" copper values in quartz porphyry over significant lengths.

A sample taken across 10 ft. of outcrop returned values of 0.02 opt gold, 1.20 opt silver and 3.20 % copper.

July 1963 - Hurley River Mines Ltd. conducted geological mapping, soil sampling, magnetic and electromagnetic surveys. The magnetic survey proved useful in delineating lithologies which augmented mapping. Anomalous soil values (copper) were obtained along Copper Canyon Creek. Geologist B.R. Richards (from McIntyre Porcupine Mines) concluded that the quartz porphyry host and a fault structure along Copper Canyon Creek was "extremely favourable for sulphide deposition".

October 1964 - A Geomag geophysical survey was conducted by Hurley River Mines Ltd. The survey outlined a prominent structural anomaly along the east side of Copper Canyon Creek (Assessment Report 613).

1965 - A comprehensive review and diamond drill program allegedly took place in February 1965.

1969 - New Cinch Uranium Mines Ltd. conducted geochemical soil sampling (Assessment Report 2122) and a magnetometer survey (Assessment Report 2123) on the Copper Canyon Property. The soil sampling outlined numerous "spot" copper anomalies. The magnetic survey delineated 9 anomalies but no major magnetic zones. Backhoe trenching and stripping was recommended.

1979 - The property was re-staked as the Duke 1 mineral claim by Mr. T.D. Lewis, for its porphyry copper potential.

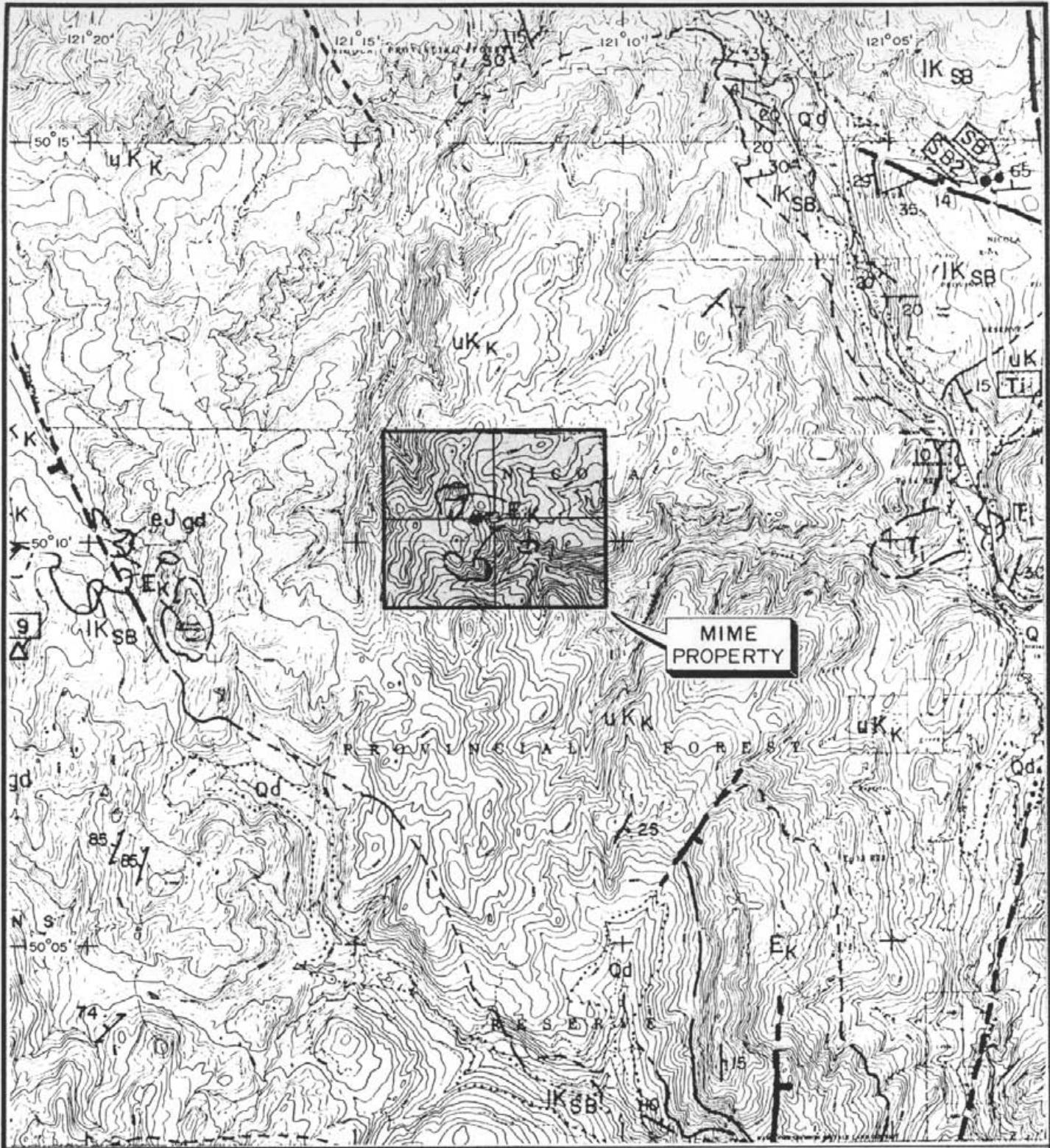
1980 - Noranda Exploration Company Limited performed geological mapping, soil geochemistry, VLF-EM and magnetometer geophysics (Assessment Report 8152). The results from soils and geophysics did not outline any significant anomalies. The writer (Mathieson) hypothesized that the scattered stockwork zones on the Duke property could represent the very top of a porphyry system, and that copper might be present in larger quantities at depth. He concluded that the only test of this hypothesis would be a deep drill hole.

April 1990 - Mine 1 to 4 claims staked for United Mineral Services Ltd.

#### 6.0 REGIONAL GEOLOGY (Figure 5)

The subject area is underlain by a succession of Palaeozoic to Tertiary volcanic and sedimentary rocks which have been intruded by Triassic-Jurassic granodiorite plutons.

The oldest rocks in the area belong to the Permian Cache Creek Group and consist of thick successions of chert, argillite, altered volcanic rocks and limestone.



- Limit of outcrop
- Limit of geological mapping
- Geological boundary (defined, approximate, assumed)
- - - Fault (defined, approximate, assumed, extension beneath drift)
- Fault; bar indicates down thrown side; arrow indicates relative movement
- Thrust fault; "layer parallel fault"; teeth on upper plate
- Diagnostic fossil locality. Refer to table 1, sheet 2
- Isotopic age (Ma). Refer to table 2, sheet 2
- △ K-Ar system:



G.S.C. Map Open File 980  
J.W. Monger 1982

0 1 2 3 4 5 Kilometres

PACIFIC SENTINEL GOLD CORP.

### MIME PROPERTY

Nicola M.D.; B.C.

## Regional Geology Map

|       |            |        |        |
|-------|------------|--------|--------|
| Scale | as shown   | N.T.S. | 92-1/3 |
| Date  | Sept. 1990 | Figure | 3      |

RELIANCE GEOLOGICAL SERVICES INC.

## GEOLOGIC LEGEND

### QUATERNARY

Qd      Glacial - fluvial alluvium, colluvium & till

### TERTIARY

Tj      Small intrusions of mainly intermediate compositions

EK      Kamloops Group: Basalt, andesite, dacite, rhyolite, breccia, tuff with minor interbedded sediments

### CRETACEOUS

UKK      Kingsvale Group: Basalt, local intercalated volcaniclastics

IKSB      Spences Bridge Group: Andesite, dacite, rhyolite, local volcaniclastics, sandstone & shale

### JURASSIC

eJgd      Granodiorite, quartz monzonite

### TRIASSIC & (?) JURASSIC

TJgd      Granodiorite

TJgd(qd)      Granodiorite, quartz diorite

UTNI      Nicola Group: Mafic to felsic volcaniclastics, interbedded argillite

The Upper Triassic Nicola Group (UTNI) consists of mafic to felsic volcaniclastics, mafic flows, argillite, chert, greywacke and limestone. The Group has been metamorphosed by the Guichon Creek batholith. This metamorphism is thought to be related to skarn mineralization at the Craigmont Mine.

The Cretaceous Spences Bridge Group (IKSB) consists of approximately 5000 ft. of multicoloured andesite, dacite, rhyolite flow rocks, local volcaniclastics and minor sandstone and shale.

The Cretaceous Kingsvale Group (UKK) underlies the subject property and unconformably overlies Spences Bridge Group and Nicola Group rocks. Basaltic and andesitic flows, commonly amygdaloidal, constitute the bulk of the group.

The Tertiary Kamloops Group consists of basalt, andesite, dacite, rhyolite flows with minor tuffs and sediments.

Batholithic rocks of Coast Intrusions range in age from Triassic to lower Cretaceous, and intrude Nicola and Cache Creek Group rocks. The Guichon Creek and Mt. Lytton batholiths range in composition from granite to diorite but average is granodiorite.

#### 7.0 1990 EXPLORATION PROGRAM

##### 7.1 Scope and Purpose

During August and September 1990, a field crew consisting of four geologists (M. McLaren, B. Yorston, G. Addie, P. Leriche) and one geotechnician (A. Cooper) completed a program of grid layout, geological mapping, rock sampling, contour and grid soil sampling, and stream sediment sampling.

The purpose of the program was to evaluate the entire property for vein/shear zone copper-gold potential using geological and geochemical techniques.

#### 7.2 Methods and Procedures

A survey grid was laid out over the drill road area and over copper geochemical anomalies outlined from 1969 work on the Mime 4 claim. The grid was initiated at the LCP, coordinates 10+000N, 10+000E. The baseline (11+550E) and cross-lines (100 m line spacings) were surveyed using compass and hipchain. Stations were marked at 50 m intervals with double flagging and embossed metal tags. Total line surveyed was 8.95 kilometers.

Geological mapping was performed over the entire property at a scale of 1:10000 (Figure 4). A total of 53 rocks were collected, with 30 analyzed for gold (fire assay) and multi-element ICP by Eco-Tech Laboratories (22) and Min-En Labs (8). The remaining twenty-three samples were analyzed for gold (fire assay and acid leach) by Acme Analytical Laboratories (9) and Chemex Labs (14). See Appendix A for rock sample descriptions and Appendix B for analytical techniques and results.

The 1990 grid was soil sampled at 50 meter station spacings, with 171 samples collected. A total of 112 contour soil samples were collected by Reliance (38) and McLaren/Yorston (74) along roads on the property (Figures 5, 6, 7, 8). All samples were taken with a grub hoe from the B horizon (approximate depth 30 cm), placed into marked Kraft paper bags and sent to Eco-Tech Laboratories Ltd. and Acme Analytical Laboratories Ltd. for analysis. The analytical results for 2 elements (Au, Cu) were computer-plotted on 1:5,000 scale maps (Figures 7 and 8).

To evaluate any existing geochemical anomalies, frequency distribution histograms based on laboratory data were prepared

for each of the aforementioned elements (Appendix C). Anomalous values were chosen using natural breaks in each histogram. 209 samples collected by Reliance were used for statistical purposes.

Correlation coefficients were calculated (Appendix C) and anomalous ranges for each element were plotted using symbol maps (Figures 7 and 8). All statistical and plotting work was performed by Tony Clark (Ph.D.) of Reliance Geological Services.

A total of 17 stream sediment samples were collected from the active part of the drainages, from the sand-silt fractions. Samples were packaged in Hubco Sand Bags and sent for analysis (Appendix B).

### 7.3 Property Geology (Figure 4)

Two lithologies were mapped on the Mime 1 to 4 claims.

The oldest and most widespread unit (90%) is massive fine grained basalt, amygdaloidal basalt flows and flow breccias (Unit 1) belonging to the Cretaceous Kingsvale Group. The volcanics are dark gray/black, fine grained and usually amygdaloidal. Amygdules are up to 1 cm in diameter, are infilled with chalcedony (agate), and are often rimmed with a bright green or orange mineral, thought to be celadonite. The groundmass locally contains feldspar phenocrysts, 1 mm wide. Flow lamination and elongation of amygdules trends at 140 degrees.

The feldspar porphyry (Unit 2) is exposed in four areas in the central part of the property. The porphyry is interpreted as sills and/or dykes which are part of a feeder system to the Eocene Kamloops Group volcanics. The unit is medium gray, fine to medium grained and contains phenocrysts of plagioclase (3 mm wide) and biotite (3 mm).

Structurally, a fault is inferred along Copper Canyon Creek. This fault and related fractures are conduits for quartz veins and mineralization.

Mineralization found to date is within fractures cutting Unit 2 in the Copper Canyon Creek (drill road) area. One mineralized outcrop (Main Showing) was located along Drill Road No. 2. A sheeted shear zone 3-4 meters wide contains blebs and dissemination of chalcopyrite, pyrite and magnetite. Mineralization occurs in the centre of the veins and is enveloped by fine grained quartz. The individual fractures are usually less than 20 cm wide.

An intrusion breccia was located 50 meters north of the Main Showing. Sub-rounded fragments of porphyry and volcanics are healed by a magnetite rich matrix.

Alteration consists of silicification and pyritization of the feldspar porphyry within 10 cm of the mineralized shear zones. The volcanics show local propylitic alteration of the groundmass. No contact relationships were observed between the volcanics and porphyry.

#### 7.4 Rock Geochemistry (Figures 5 and 6).

The following results are considered significant:

Sample

Number

Type

Results

Location

MYR-1 Select 1330 ppm Cu End of drill road No.4  
20 ppb Au

Description: Feldspar porphyry with weak quartz stockwork with disseminated pyrite and chalcopyrite.

MYR-5 Select 735 ppm Cu 45 m north of MYR-1

Description: Feldspar porphyry with hairline stringers infilled with chalcopyrite.

|   |              |  |  |
|---|--------------|--|--|
| MYR-7   | Select       | 360ppm Cu<br>30 m west of Copper Canyon Creek.   |  |
| Description: Silicified feldspar porphyry with narrow stringers infilled with chalcopyrite and magnetite.   |              |  |  |
| MYR-8   | Select       | 6392ppm Cu<br>2.3ppm Ag<br>27ppb Au<br>North of drill road No.2,<br>west of Copper Canyon Creek. |  |
| Description: Silicified feldspar porphyry with up to 10% chalcopyrite along fractures.  |              |  |  |
| MR-5  | Select       | >10000ppm Cu<br>345ppb Au<br>3.2ppm Ag<br>Main Showing   |  |
| MR-5B   | Select       | 5500ppm Cu<br>285ppb Au<br>6.9ppm Ag<br>Main Showing   |  |
| MIM90-A20R  | Chip<br>3.3m | 909ppm Cu<br>Main Showing  |  |
| MIM90-A21R  | Chip<br>3.8m | 730ppm Cu<br>Main Showing  |  |
| MIM90-A22R  | Chip<br>2.9m | 812ppm Cu<br>40ppb Au<br>Main Showing  |  |
| MIM90-A23R  | Chip<br>2.8m | 476ppm Cu<br>Main Showing  |  |
| MIM90-A24R  | Chip<br>3.4m | 530ppm Cu<br>Main Showing  |  |
| Description: Main Showing is a sheeted fracture system with shears infilled with chalcopyrite, pyrite and quartz. Samples A20R to A24R were continuous chips taken across the exposed road cut (16.3 meters). |              |  |  |
| MR-6  |              | 3100 ppm Cu<br>3.0 ppm Ag<br>30 meters south of Main Showing                                     |  |
| MR-7  |              | 4000 ppm Cu<br>End of drill road #1  |  |
| MR-8A   |              | 1200 ppm Cu<br>East bank of Copper Canyon Creek  |  |
| MR-8B   |              | 450 ppm Cu<br>East bank of Copper Canyon Creek   |  |

|       |   |                                 |
|-------|---|---------------------------------|
| MR-9  | 1000 ppm Cu<br>50.0 ppm Ag<br>85 ppb Au | 200 meters NE of Mimenuh Mtn.   |
| MR-18 | 410 ppm Cu                              | 30 meters north of Main Showing |
| MR-19 | 1000 ppm Cu                             | 50 meters NE of Main Showing    |

7.5 STREAM SEDIMENT GEOCHEMISTRY (Figures 5 and 6)

Sample MSS-9, collected from a tributary of Barrie Creek, assayed 540 ppb gold.

7.6 SOIL GEOCHEMISTRY

7.6.1 Copper in Soils (Figures 5, 6, and 7)

|                    |   |              |
|--------------------|---|--------------|
| Range              | : | 9 to 757 ppm |
| Mean               | : | 46.32        |
| Standard deviation | : | 120.7        |
| Background         | : | 0 to 99 ppm  |
| Anomalous          | : | 100+ ppm     |

Statistics do not include 74 contour samples from the "MS" series. Anomalous thresholds based on statistics have been used for all samples.

The following anomalies were outlined from 1990 sampling. All anomalies are in the drill road area.

| Sample Number  | Copper (ppm) | Location                 | Comments             |
|----------------|--------------|--------------------------|----------------------|
| MS 8           | 231          | Main Showing &           | North-south trending |
| MS 9           | 309          | Intrusion Breccia        | anomaly approx. 100  |
| MS10           | 5547         | areas and south          | x 250m, including    |
| MS11           | 254          | to Copper Canyon         | 20 results over      |
| MS12           | 106          | Creek                    | 100 ppm              |
| MS17           | 826          |                          |                      |
| MS18           | 340          |                          |                      |
| MS19           | 131          |                          |                      |
| MS24           | 259          |                          |                      |
| MS25           | 116          |                          |                      |
| MS26           | 645          |                          |                      |
| MS27           | 400          |                          |                      |
| MS29           | 120          |                          |                      |
| MS30           | 100          |                          |                      |
| MS31A          | 333          |                          |                      |
| MS33           | 173          |                          |                      |
| MS34           | 434          |                          |                      |
| MS35           | 411          |                          |                      |
| 9+700N 10+250E | 111          |                          |                      |
| 9+800N 10+100E | 757          |                          |                      |
| MS41           | 393          | Drill Road               | Northwest-southeast  |
| MS42           | 310          | #4, southeast            | trending 11 point    |
| MS43           | 344          | area                     | anomaly approx.      |
| MS45           | 177          |                          | 100 x 180 m          |
| MS53           | 769          |                          |                      |
| MS54           | 919          |                          |                      |
| MS55           | 151          |                          |                      |
| MS56           | 185          |                          |                      |
| MS57           | 189          |                          |                      |
| MS58           | 309          |                          |                      |
| MS74           | 2157         |                          |                      |
| MS49           | 104          | Drill Road #4            | 1 point anomaly      |
| 9+900N 10+230E | 116          | Main Road @              | 2 point anomaly      |
| 9+900N 10+300E | 233          | Jct of Drill Roads 1 & 2 |                      |

7.6.2 Gold in Soils (Figures 5, 6, and 8)

|                    |   |               |
|--------------------|---|---------------|
| Range              | : | <5 to 990 ppb |
| Mean               | : | 8.83          |
| Standard Deviation | : | 70.28         |
| Background         | : | 0-15 ppb      |
| Anomalous          | : | 16+ ppb       |

Gold anomalies are spotty, possibly due to the "nugget effect" of gold in soils. The following anomalies were outlined:

| Sample Number   | Gold (ppb) | Location          | Comments   |
|-----------------|------------|-------------------|--|
| MS 5            | 23         | Main Showing area |  |
| MS 6            | 44         | to Copper Canyon  |  |
| MS 9            | 420        | Creek. Along      |  |
| MS10            | 100        | Drill roads 1 & 2 |  |
| MS19            | 18         |                   | A concentration of 11 anomalies along the east edge of the 20 point copper anomaly |
| MS24            | 49         |                   |  |
| MS28            | 24         |                   |  |
| MS29            | 27         |                   |  |
| MS35            | 21         |                   |  |
| 9+800N 10+050E  | 20         |                   |  |
| 9+800N 10+100E  | 15         |                   |  |
| MS46            | 16         | Drill Road #4     | Spot anomalies   |
| MS48            | 17         |                   |  |
| MS52            | 16         |                   |  |
| MS55            | 16         |                   |  |
| MS61            | 20         |                   |  |
| MS62            | 131        |                   |  |
| MS69            | 77         |                   |  |
| 9+900N 10+150E  | 20         |                   |  |
| 9+900N 10+050E  | 15         |                   |  |
| 9+800N 10+400E  | 990        | Grid Coordinates  | 3 point linear anomaly   |
| 9+900N 10+350E  | 25         |                   |  |
| 10+000N 10+400E | 40         |                   |  |
| 10+000N 10+650E | 15         | Grid Coordinates  | 2 point anomaly  |
| 10+000N 10+700E | 85         |                   |  |
| 9+700N 10+900E  | 25         | Grid Coordinates  | Spot anomaly   |
| 9+600N 11+100E  | 25         | Grid Coordinates  | Spot anomaly   |
| 9+600N 11+250E  | 15         | Grid Coordinates  | Spot anomaly   |
| 9+800N 11+200E  | 30         | Grid Coordinates  | Spot anomaly   |

### 7.7 Discussion of Results

Mineralization found on the Mime property is related to copper and associated gold in shear and fault zones within the Tertiary feldspar porphyry unit. Faulting and brecciation of the porphyry is likely associated with the regional Fraser River fault system. The age of mineralization (Eocene?) is approximately the same timing as the Blackdome epithermal gold deposit, 180 km northwest. The exploration potential lies in finding a high density of copper (and gold) bearing shears and faults in the Copper Canyon Creek area. Two broad copper soil anomalies and associated high copper results in rocks show that this potential does exist.

Exploration potential also exists in finding the source of placer gold in the Barrie Creek drainage.

The following target areas have been defined from previous and 1990 exploration work.

#### Target Area #1

This area encompasses Drill Roads 1 to 4 and the upper part of Copper Canyon Creek. No reliable data is available from the drilling which was done in the early 1960's.

The Main Showing is a sheeted fracture system infilled with quartz and chalcopyrite. Rock sample results at the Main Showing range from 476 to >10000 ppm copper and up to 345 ppb gold. Ten other select rock samples on Target Area #1 assayed up to 6392 ppm copper.

Soil sampling defined two zones (dimensions 100 x 250m and 100 x 180m) of anomalous copper (above 100 ppm). A concentration of 11 gold anomalies flanks the 100 meter x 250 meter copper anomaly.

Target Area #2 includes a 3 point gold anomaly in soils with a high result of 990 ppb.

Target Area #3 includes the Barrie Creek drainage basin. Two placer claims on the creek indicate that the gold source is within the drainage basin. One stream sediment sample assayed 540 ppb gold.

#### 8.0 CONCLUSIONS

The Mime property has good potential to host a vein and/or shear type copper/gold deposit for the following reasons:

- 1) The geological environment, Tertiary aged faulted and brecciated feldspar porphyry, is favourable; and
- 2) Previous work and the 1990 exploration program have outlined 3 target areas which warrant further work.

## 9.0 RECOMMENDATIONS

### Phase 2

1. Conduct a backhoe trenching program over target areas 1 and 2. Attention should focus on the Main Showing (extending the strike length) and the intrusion breccia.
2. Lay out one control grid over target areas 1 and 2, and map it in detail.
3. Lay out approximately 25 line kilometers of grid over target area #3 (Barrie Creek drainage basin). Suggested line spacing would be 100 meters with station spacings of 50 meters.
4. Collect approximately 500 soil samples at 50 meter intervals from the target area #3 grid.
5. Geologically map and sample the target area #3 grid.

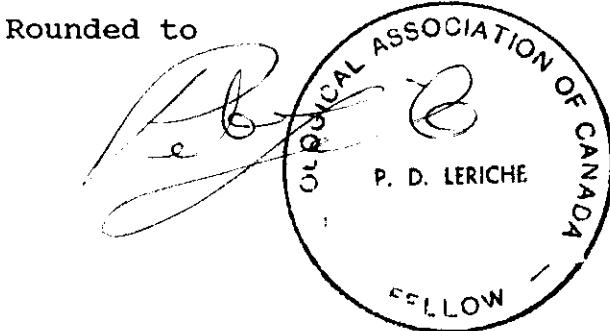
Contingent upon favourable results from Phase 2, Phase 3 would consist of further backhoe trenching and diamond drilling.

10.0

PROPOSED BUDGET

MIME PROPERTY  
PHASE 2

|  |                  |
|--|------------------|
| Project Preparation  | \$ 500           |
| Mobilization/Demobilization<br>(includes transportation, food & accommodation) | \$ 2,800         |
| Field Crew:  | \$14,280         |
| Field Costs:   | \$ 8,220         |
| Laboratory Analysis:   | \$ 8,190         |
| Sub-Contractors: Backhoe   | \$ 5,400         |
| Reclamation  | \$ 2,000         |
| Report:  | \$ <u>4,500</u>  |
| Sub-total  | \$45,890         |
| Administration, including Overhead and Profit                                  | \$ <u>4,589</u>  |
| Sub-total  | \$50,479         |
| <u>plus</u> Allowance for G.S.T. (7%)  | \$ <u>3,534.</u> |
| TOTAL  | \$54,013.        |
| Rounded to   | \$55,000         |



CERTIFICATE

I, PETER D. LERICHE, of 3125 West 12th Avenue, Vancouver, B.C., V6K 2R6, do hereby state that:

1. I am a graduate of McMaster University, Hamilton, Ontario, with a Bachelor of Science Degree in Geology, 1980.
2. I am a Fellow in good standing with the Geological Association of Canada.
3. I have actively pursued my career as a geologist for eleven years in British Columbia, Ontario, Yukon and Northwest Territories, Arizona, Nevada and California.
4. The information, opinions, and recommendations in this report are based on fieldwork carried out under my direction, and on published and unpublished literature. I was present on the subject property on August 25 and 26, 1990.
5. I have no interest, direct or indirect, in the subject claims or the securities of Pacific Sentinel Gold Corp.
6. I consent to the use of this report in a Prospectus or Statement of Material Facts for the purpose of private or public financing.

RELIANCE GEOLOGICAL SERVICES INC.

Peter D. Leriche, B.Sc., F.G.A.C.

Dated at North Vancouver, B.C., this 16th day of October, 1990.



ITEMIZED COST STATEMENT

UNITED MINERAL SERVICES LTD  
#1020 - 800 W. Pender St  
Vancouver, B.C. V6C 2V6

Re: Job 661 - MIME CLAIMS: RECONNAISSANCE

Project Preparation \$ 150.

Mobilization & demobilization  
(includes food & acc, transportation, wages) \$ 1,690.

Field Crew:

Geologists (2) \$ 325/day x 14 days \$ 4,550.  
(M McLaren & B Yorston, Aug 1 - 8, 1990)  
Geologist \$ 325/day x 14 days \$ 4,550.  
(G Addie, Aug 21 - Sep 4, 1990)  
Geologist \$ 325/day x 3 days \$ 975.  
(P Leriche, Aug 25 - 27, 1990)  
Prospector \$ 250/day x 14 days \$ 3,850. \$ 13,925.  
(A Cooper, Aug 21 - Sep 4, 1990)

Field Costs:

Camp rent & food \$ 60/day x 45 mandays \$ 2,700.  
Communications \$ 20/day x 14 days \$ 280.  
Supplies & fuel \$ 22/day x 45 mandays \$ 990.  
Vehicle \$ 110/day x 24 days \$ 2,640. \$ 6,610.

Lab Analysis:

17 silt and 283 soil samples @ \$14/sample \$4,200.  
(Geochem Au/AA and multi-element ICP)  
53 rock samples @ \$17/sample \$ 901. \$ 5,101.

Report:

Map preparation, drafting, plotting \$ 1,600.  
Report Writing & editing \$ 950.  
Word processing, copying, binding \$ 350. \$ 2,900.

Administration incl. Overheads & Profit \$ 3,037.

TOTAL \$ 33,413.

## REFERENCES

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**APPENDIX A**  
**ROCK SAMPLE DESCRIPTIONS**

| SAMPLE NO.                             | DESCRIPTION   | WIDTH (cm) |
|--|---|------------|
| MIM90-A1R                              | Chip sample 0.5 x 2.0 meters. Fine grained buff weathering volcanic with chlorite along fractures.          |            |
| MIM90-A2R                              | Select sample. Fine grained tan coloured volcanic, weakly magnetic with chlorite along fractures.           |            |
| MIM90-A3R                              | Select sample. Amygdaloidal basalt with amygdules infilled with chalcedony and rimmed with celadonite.      |            |
| MIM90-A4R)<br>MIM90-A5R)<br>MIM90-A6R) | Same as A3R   |            |
| MIM90-A7R                              | Select sample. Completely sausseterized feldspar porphyry(?) with 0.5% disseminate pyrite and chalcopyrite. |            |
| MIM90-A8R                              | Same as A7R.  |            |
| MIM90-A9R                              | Select sample. Crudely foliated basalt.   |            |
| MIM90-A10R                             | Select sample. Clay altered feldspar/quartz stringer, 10 cm wide, within fine grained basalt.               |            |
| MIM90-A11R                             | Select sample. Fine grained basalt with feldspar phenocrysts (51mm). Chalcedony along fractures.            |            |
| MIM90-A12R                             | Select sample. Amygdaloidal basalt.   |            |
| MIM90-A13R                             | Select sample. Limonitic volcanic breccia with chloritic rims.  |            |
| MIM90-A14R                             | Select sample. Volcanic breccia with feldspar phenocrysts.  |            |
| MIM90-A15R                             | Select sample. Fine grained massive basalt with limonitic fractures.  |            |
| MIM90-A16R                             | Same as A15R  |            |

| SAMPLE NO. | DESCRIPTION   | WIDTH (cm) |
|------------|---|------------|
| MIM90-A17R | Same as A15R  |            |
| MIM90-A18R | Select sample. Andesite/basalt flow breccia.  |            |
| MIM90-A19R | Select sample. Fine grained massive basalt with 1% diss. pyrite.  |            |
| MIM90-A20R | Chip sample, 3.3m. Sheared feldspar porphyry with quartz, chalcopyrite, magnetite and malachite in stringers. |            |
| MIM90-A21R | Chip sample, 3.8m. Sheared feldspar porphyry with quartz stringers. Minor pyrite and chalcopyrite.            |            |
| MIM90-A22R | Chip sample, 2.9m. Moderately sausseterized feldspar porphyry with magnetite stringers.                       |            |
| MIM90-A23R | Chip sample, 2.8m. Same as A22R.  |            |
| MIM90-A24R | Chip sample, 3.4m. Moderately sausseterized feldspar porphyry.  |            |

| <u>SAMPLE NO.</u> | <u>DESCRIPTION</u>   | <u>WIDTH (cm)</u> |
|-------------------|--|-------------------|
| MIM90-CR1         | Select sample. Pyritic rusty basalt.   |                   |
| MIM90-CR2         | Select sample. Tan weathered amygdaloidal basalt with clay infilled amygdules. |                   |
| MIM90-CR3         | Select sample. Basalt porphyry with fine grained feldspar phenocrysts.         |                   |
| MIM90-CR4         | Select sample. Volcanic breccia.   |                   |
| MIM90-CR5         | Select sample. Feldspar porphyry.  |                   |

| SAMPLE NO. | DESCRIPTION   | WIDTH (cm) |
|------------|---|------------|
| MYR-1      | Float. From hand trench at end of Drill Road #4. Feldspar porphyry with weak quartz stockwork. Quartz stringers <1cm wide contain pyrite and chalcopyrite.                                |            |
| MYR-2      | Select sample. Maroon coloured amygdaloidal flow.   |            |
| MYR-3      | Select sample. Maroon amygdaloidal flow with amygdules infilled with finely banded chalcedonic quartz.  |            |
| MYR-4      | Select sample. Tan coloured, limonitic, vuggy, extremely altered intrusive(?) adjacent to fresh basalt.   |            |
| MYR-5      | Select sample from trench. Feldspar porphyry with hairline stringers infilled with chalcopyrite.  |            |
| MYR-6      | Float. Hornfelsed andesite with 7-9% pyrite.  |            |
| MYR-7      | Select sample. Silicified feldspar porphyry with up to 1% chalcopyrite-magnetite along stringers and disseminated in the host.  |            |
| MYR-8      | Select sample in trench. Silicified feldspar porphyry with approximately 10% chalcopyrite along fractures and disseminated in host rock. Minor magnetite. Fracture attitude 045/vertical. |            |
| MYR-9      | Select sample. From gossan containing 10-15% fine pyrite along fractures. Fractures trend 045°.   |            |

**APPENDIX B**  
**ANALYTICAL RESULTS AND TECHNIQUES**

## ECO-TECH LABORATORIES LTD.

## RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-561

10041 EAST TRANS CANADA HWY.  
KAMLOOPS, B.C. V2C 2J3  
PHONE - 604-573-5700  
FAX - 604-573-4557

241 E. 1ST. ST.  
NORTH VANCOUVER, B.C.  
VIS 1J9

SEPTEMBER 18, 1990

VALUES IN PPM UNLESS OTHERWISE REPORTED

PROJECT: 661  
22 ROCK SAMPLES RECEIVED SEPTEMBER 13, 1990

| ET#      | DESCRIPTION   | AU(ppb) | AG | AL(%) | AS | B  | BA  | BI | CA(%) | CD | CO | CR  | CU  | FE(%) | K(%) | LA  | Mg(%) | MN   | MO | NA(%) | NI | P    | PB | SB | SN  | SR  | Ti(%) | U   | V   | W   | X  | Y   | Z% |
|----------|---------------|---------|----|-------|----|----|-----|----|-------|----|----|-----|-----|-------|------|-----|-------|------|----|-------|----|------|----|----|-----|-----|-------|-----|-----|-----|----|-----|----|
| 561 - 1  | MIM 90 CR-001 | 10      | <2 | 3.79  | <5 | <2 | 34  | 27 | .73   | 3  | 12 | 86  | 12  | 9.03  | .07  | <10 | 2.61  | 591  | <1 | .07   | 26 | 1357 | 94 | <5 | <20 | 132 | .13   | <10 | 120 | <10 | 10 | 96  |    |
| 561 - 2  | MIM 90 CR-002 | 5       | <2 | 4.82  | <5 | 4  | 47  | 19 | 2.47  | 2  | 15 | 111 | 17  | 8.20  | .18  | <10 | 2.83  | 736  | <1 | .02   | 33 | 753  | <2 | <5 | <20 | 259 | .38   | <10 | 120 | <10 | 24 | 51  |    |
| 561 - 3  | MIM 90 CR-003 | 5       | <2 | 2.67  | <5 | <2 | 23  | 35 | 1.61  | 3  | 29 | 75  | 30  | 13.72 | .14  | <10 | 2.25  | 1079 | 2  | .27   | 17 | 3308 | <2 | <5 | <20 | 138 | 1.11  | <10 | 166 | <10 | 54 | 71  |    |
| 561 - 4  | MIM 90 CR-004 | 25      | <2 | 3.28  | <5 | 8  | 97  | 18 | 2.33  | 2  | 18 | 58  | 27  | 6.58  | .19  | <10 | 2.08  | 640  | <1 | .10   | 51 | 1013 | <2 | <5 | <20 | 602 | .40   | <10 | 90  | <10 | 31 | 44  |    |
| 561 - 5  | MIM 90 CR-005 | 5       | <2 | 1.34  | <5 | 3  | 30  | 12 | .69   | 1  | 8  | 90  | 23  | 4.35  | .06  | <10 | .98   | 470  | 4  | .08   | 9  | 711  | <2 | <5 | <20 | 80  | .12   | <10 | 64  | <10 | 8  | 36  |    |
| 561 - 6  | MIM 90 A 7 R  | 5       | <2 | 1.33  | <5 | <2 | 358 | 10 | 2.59  | 1  | 6  | 50  | 21  | 3.86  | .22  | <10 | .87   | 599  | 2  | <.01  | 7  | 878  | <2 | <5 | <20 | 57  | <.01  | <10 | 28  | <10 | 5  | 54  |    |
| 561 - 7  | MIM 90 A 9 R  | 5       | <2 | 2.48  | <5 | <2 | 46  | 16 | 1.87  | 2  | 16 | 112 | 34  | 6.98  | .35  | <10 | 2.17  | 352  | 2  | .20   | 41 | 1226 | <2 | <5 | <20 | 91  | .27   | <10 | 112 | <10 | 22 | 16  |    |
| 561 - 8  | MIM 90 A 10 R | 10      | <2 | 1.35  | <5 | 3  | 135 | <5 | .81   | <1 | 4  | 103 | 9   | 1.65  | .09  | <10 | .44   | 156  | 5  | .06   | 8  | 219  | <2 | <5 | <20 | 125 | .09   | <10 | 49  | <10 | 5  | 7   |    |
| 561 - 9  | MIM 90 A 11 R | 5       | <2 | 2.30  | <5 | 4  | 12  | 17 | 1.10  | 2  | 18 | 84  | 11  | 7.40  | .05  | <10 | 2.65  | 1292 | <1 | .07   | 45 | 1335 | <2 | <5 | <20 | 43  | .33   | <10 | 89  | <10 | 24 | 42  |    |
| 561 - 10 | MIM 90 A 12 R | 5       | <2 | 3.31  | <5 | <2 | 92  | 21 | 3.62  | 2  | 18 | 76  | <1  | 7.50  | .13  | <14 | 2.52  | 1174 | <1 | <.01  | 30 | 1122 | <2 | <5 | <20 | 125 | <.01  | <10 | 67  | <10 | 12 | 67  |    |
| 561 - 11 | MIM 90 A 13 R | 5       | <2 | 2.56  | <5 | <2 | 98  | 23 | 1.63  | 2  | 16 | 105 | 7   | 7.23  | .30  | <11 | 1.61  | 782  | 3  | .02   | 28 | 1060 | <2 | <5 | <20 | 47  | .05   | <10 | 74  | <10 | 13 | 53  |    |
| 561 - 12 | MIM 90 A 14 R | 5       | <2 | 2.49  | <5 | <2 | 74  | 18 | 1.76  | 2  | 18 | 111 | 16  | 7.08  | .12  | <13 | 2.11  | 793  | 1  | .18   | 42 | 1285 | <2 | <5 | <20 | 110 | .17   | <10 | 107 | <10 | 22 | 40  |    |
| 561 - 13 | MIM 90 A 15 R | 5       | <2 | 2.78  | <5 | <2 | 66  | 19 | 1.74  | 2  | 19 | 130 | 26  | 7.55  | .10  | <13 | 2.43  | 764  | 2  | .21   | 42 | 1281 | <2 | <5 | <20 | 97  | .25   | <10 | 114 | <10 | 25 | 43  |    |
| 561 - 14 | MIM 90 A 16 R | 5       | <2 | 2.18  | <5 | <2 | 55  | 18 | 1.47  | 2  | 17 | 96  | 21  | 6.72  | .10  | <12 | 2.23  | 430  | 1  | .17   | 39 | 1098 | <2 | <5 | <20 | 74  | .24   | <10 | 95  | <10 | 23 | 38  |    |
| 561 - 15 | MIM 90 A 17 R | 5       | <2 | 2.03  | <5 | <2 | 52  | 20 | 1.45  | 2  | 16 | 89  | 22  | 6.42  | .10  | <13 | 1.96  | 367  | <1 | .17   | 38 | 1315 | <2 | <5 | <20 | 78  | .21   | <10 | 93  | <10 | 22 | 36  |    |
| 561 - 16 | MIM 90 A 18 R | 5       | <2 | 3.12  | <5 | <2 | 74  | 25 | .58   | 7  | 22 | 116 | 42  | 9.24  | .25  | <10 | 2.45  | 1227 | 10 | .02   | 43 | 1744 | 45 | <5 | <20 | 15  | <.01  | <10 | 62  | <10 | 16 | 229 |    |
| 561 - 17 | MIM 90 A 19 R | 5       | <2 | 0.54  | <5 | <2 | 68  | <5 | 1.78  | <1 | 17 | 68  | 56  | 4.66  | .07  | <12 | 2.38  | 621  | <1 | .20   | 48 | 1455 | <2 | <5 | <20 | 210 | .19   | <10 | 122 | <10 | 12 | 77  |    |
| 561 - 18 | MIM 90 A 20 R | 5       | <2 | 1.45  | <5 | <2 | 63  | <5 | .85   | <1 | 10 | 42  | 909 | 3.40  | .17  | <10 | 1.19  | 291  | 4  | .04   | 8  | 636  | <2 | <5 | <20 | 70  | .05   | <10 | 49  | <10 | 5  | 33  |    |
| 561 - 19 | MIM 90 A 21 R | 5       | <2 | 1.46  | <5 | 4  | 110 | <5 | .53   | <1 | 11 | 29  | 730 | 3.73  | .19  | <11 | 1.25  | 343  | 8  | .05   | 3  | 686  | <2 | <5 | <20 | 72  | .07   | <10 | 78  | <10 | 6  | 37  |    |
| 561 - 20 | MIM 90 A 22 R | 40      | <2 | 1.45  | <5 | 6  | 98  | <5 | .32   | <1 | 11 | 48  | 812 | 5.15  | .37  | <10 | 1.23  | 362  | 12 | .07   | 8  | 495  | <2 | <5 | <20 | 71  | .14   | <10 | 84  | <10 | 7  | 45  |    |
| 561 - 21 | MIM 90 A 23 R | 5       | <2 | 1.47  | <5 | 5  | 167 | <5 | .40   | <1 | 9  | 42  | 476 | 3.36  | .51  | <10 | 1.16  | 313  | 9  | .10   | 7  | 620  | <2 | <5 | <20 | 84  | .17   | <10 | 91  | <10 | 9  | 45  |    |
| 561 - 22 | MIM 90 A 24 R | 5       | <2 | 1.39  | <5 | 5  | 132 | <5 | .41   | <1 | 11 | 45  | 530 | 3.58  | .43  | <10 | 1.12  | 252  | 11 | .10   | 8  | 659  | <2 | <5 | <20 | 74  | .17   | <10 | 92  | <10 | 9  | 43  |    |

NOTE: &lt; = LESS THAN

*Jutta Jelouse*  
 ECO-TECH LABORATORIES LTD.  
 JUTTA JELOUSE  
 B.C. CERTIFIED ASSAYER

COMP: RELIANCE GEOLOGICAL SERVICE

PROJ: 661

ATTN: P. LERICHE

**MIN-EN LABS — ICP REPORT**

705 WEST 15TH ST., NORTH VANCOUVER, B.C. V7M 1T2

(604)980-5814 OR (604)988-4524

FILE NO: OV-1320-RJ1

DATE: 90/09/05

\* ROCK \* (ACT:F31)

| SAMPLE#    | Cu<br>ppm | Ag<br>ppm | Au*<br>ppb |
|------------|-----------|-----------|------------|
| MYR-1      | 1330      | .8        | 20         |
| MYR-2      | 34        | .1        | 1          |
| MYR-3      | 16        | .1        | 1          |
| MYR-4      | 9         | .1        | 2          |
| MYR-5      | 735       | .7        | 8          |
| MYR-6      | 205       | .3        | 7          |
| MYR-7      | 360       | .4        | 6          |
| MYR-8      | 6392      | 2.3       | 27         |
| MYR-9      | 158       | .3        | 10         |
| STANDARD C | 60        | 7.1       | -          |



# Chemex Labs Ltd.

Analytical Chemists • Geochemists • Registered Assayers  
 212 Brookbank Ave., North Vancouver  
 British Columbia, Canada V7J 2C1  
 PHONE: 604-984-0221

To: COVENANT RESOURCES LTD.

1000 - 800 W. PENDER ST.  
 VANCOUVER, BC  
 V6C 2V6

Page Number : 1  
 Total Pages : 1  
 Invoice Date: 15-AUG  
 Invoice No.: I-90202  
 P.O. Number : NONE

Project: MINE

Comments: ATTN: DOUG FORSTER CC: M. MCCLAREN

## CERTIFICATE OF ANALYSIS

A9020520

| SAMPLE DESCRIPTION | PREP CODE | Au ppb FA+AA | Cu ppm | Ag ppm Aqua R |           |  |  |  |  |  |  |  |  |
|--------------------|-----------|--------------|--------|---------------|-----------|--|--|--|--|--|--|--|--|
| MR-1               | 255 295   | 15           | 8      | < 0.2         |           |  |  |  |  |  |  |  |  |
| MR-1               | 255 295   | 15           | 370    | < 0.2         |           |  |  |  |  |  |  |  |  |
| MR-2               | 255 295   | < 5          | 160    | < 0.2         |           |  |  |  |  |  |  |  |  |
| MR-3               | 255 295   | 50           | 640    | < 0.2         |           |  |  |  |  |  |  |  |  |
| MR-4               | 255 295   | 30           | 66     | 0.2           |           |  |  |  |  |  |  |  |  |
| MR-5               | 255 295   | 345          | >10000 | 3.2           |           |  |  |  |  |  |  |  |  |
| MR-5B              | 255 295   | 285          | 5500   | 6.9           |           |  |  |  |  |  |  |  |  |
| MR-6               | 255 295   | 35           | 3100   | 3.0           |           |  |  |  |  |  |  |  |  |
| MR-7               | 255 295   | 60           | 4000   | 1.2           |           |  |  |  |  |  |  |  |  |
| MR-8A              | 255 295   | < 5          | 1200   | 0.4           |           |  |  |  |  |  |  |  |  |
| MR-8B              | 255 295   | 30           | 450    | < 0.2         |           |  |  |  |  |  |  |  |  |
| MR-8C              | 255 295   | < 5          | 46     | 0.3           |           |  |  |  |  |  |  |  |  |
| MR-9               | 255 295   | 85           | 1000   | 50.0          | MINE MTR. |  |  |  |  |  |  |  |  |
| MR-18              | 255 295   | 15           | 410    | 1.2           |           |  |  |  |  |  |  |  |  |
| MR-19              | 255 295   | 5            | 1000   | 0.9           |           |  |  |  |  |  |  |  |  |
| MS-17              | 255 295   | 15           | 940    | 1.0           |           |  |  |  |  |  |  |  |  |

988-GOLD

Hart Bichler

CERTIFICATION:

ECO-TECH LABORATORIES LTD.

RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-562

10041 EAST TRANS CANADA HWY.  
KAMLOOPS, B.C. V2C 2J3  
PHONE - 604-573-5700  
FAX - 604-573-4557

SEPTEMBER 24, 1990

241 E. 1ST. ST.  
NORTH VANCOUVER, B.C.  
VIS 1J9

VALUES IN PPM UNLESS OTHERWISE REPORTED

PROJECT: 661  
7 SILT SAMPLES RECEIVED SEPTEMBER 13, 1990

| ET#     | DESCRIPTION  | AU(ppb) | AG AL(%) | AS   | B  | BA | BI CA(%) | CO | CO   | CR | CU FE(%) | K(%) | LA MG(%) | MN   | MO NA(%) | NI | P    | PB  | SB | SN  | SR Ti(%) | U   | V  | W  | Y   | Zn  |     |     |     |     |    |    |
|---------|--------------|---------|----------|------|----|----|----------|----|------|----|----------|------|----------|------|----------|----|------|-----|----|-----|----------|-----|----|----|-----|-----|-----|-----|-----|-----|----|----|
| 562 - 1 | MIM 90 A 1 L | (5      | .2       | 3.01 | 54 | (2 | 135      | (5 | 1.00 | (1 | 15       | 38   | 18       | 3.08 | .03      | 43 | 1.23 | 608 | 1  | .02 | 20       | 749 | 18 | (5 | (20 | 95  | .18 | (10 | 75  | (10 | 7  | 68 |
| 562 - 2 | MIM 90 A 2 L | (5      | .2       | 2.01 | 33 | (2 | 100      | (5 | .95  | (1 | 18       | 40   | 22       | 3.01 | .09      | 44 | 1.23 | 641 | (1 | .03 | 28       | 950 | 13 | (5 | (20 | 98  | .20 | (10 | 85  | (10 | 7  | 42 |
| 562 - 3 | MIM 90 A 3 L | (5      | .2       | 2.10 | 30 | (2 | 65       | (5 | 1.11 | (1 | 14       | 41   | 21       | 2.71 | .03      | 39 | .97  | 444 | (1 | .04 | 26       | 786 | 11 | (5 | (20 | 128 | .29 | (10 | 83  | (10 | 12 | 32 |
| 562 - 4 | 90 CS 1      | (5      | .2       | 1.73 | 30 | (2 | 101      | (5 | 1.28 | (1 | 19       | 43   | 121      | 3.11 | .07      | 47 | 1.25 | 711 | 1  | .04 | 30       | 985 | 18 | (5 | (20 | 132 | .16 | (10 | 85  | (10 | 7  | 60 |
| 562 - 5 | MM CS 3      | (5      | .2       | 1.71 | 25 | (2 | 103      | (5 | 1.18 | (1 | 17       | 43   | 68       | 3.12 | .08      | 45 | 1.23 | 572 | 2  | .04 | 27       | 950 | 14 | (5 | (20 | 166 | .17 | (10 | 89  | (10 | 6  | 51 |
| 562 - 6 | MM CS 5      | (5      | .2       | 1.76 | 31 | 3  | 104      | (5 | 1.08 | (1 | 16       | 55   | 24       | 3.59 | .04      | 51 | 1.03 | 539 | 1  | .02 | 25       | 598 | 11 | (5 | (20 | 151 | .18 | (10 | 113 | (10 | 5  | 40 |
| 562 - 7 | MM CS 6      | (5      | .2       | 2.13 | 34 | (2 | 88       | (5 | .92  | (1 | 13       | 42   | 21       | 2.73 | .05      | 55 | .85  | 459 | (1 | .02 | 22       | 386 | 12 | (5 | (20 | 112 | .22 | (10 | 74  | (10 | 22 | 39 |

NOTE: ( = LESS THAN

SC90/RELIANCE

*Jutta Jealouse*  
ECO-TECH LABORATORIES LTD.  
JUTTA JEALOUSE  
B.C. CERTIFIED ASSAYER

| SAMPLE#         | Cu<br>ppm | Ag<br>ppm | Au*<br>ppb |
|-----------------|-----------|-----------|------------|
| MSS-1           | 47        | .3        | 1          |
| MSS-2           | 78        | .2        | 13         |
| MSS-3           | 46        | .7        | 4          |
| MSS-4           | 40        | .2        | 2          |
| MSS-5           | 29        | .3        | 4          |
| MSS-6           | 37        | .3        | 11         |
| MSS-7           | 32        | .1        | 1          |
| MSS-8           | 32        | .2        | 1          |
| MSS-9           | 40        | .2        | 540        |
| MSS-10          | 38        | .1        | 20         |
| STANDARD C/AU-S | 63        | 7.1       | 47         |

## ECO-TECH LABORATORIES LTD.

## RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-563

10041 EAST TRANS CANADA HWY.  
KAMLOOPS, B.C. V2C 2J3  
PHONE - 604-573-5700  
FAX - 604-573-4557

241 E. 1ST ST.  
NORTH VANCOUVER, B.C.  
V1S 1J9

SEPTEMBER 24, 1990

VALUES IN PPM UNLESS OTHERWISE REPORTED

PROJECT: 661  
209 SOIL SAMPLES RECEIVED SEPTEMBER 13, 1990

| ETR      | DESCRIPTION           | AU(ppb) | Al AL(%) | As   | B  | BA | Bi CA(%) | Co | Cr   | Cu FE(%) | K(%) | La MG(%) | Mn | Mo Na(%) | Ni  | P  | Pb   | SB  | Sn | SP Ti(%) | U  | V    | W  | Y | Zn  |     |     |    |     |    |    |     |
|----------|-----------------------|---------|----------|------|----|----|----------|----|------|----------|------|----------|----|----------|-----|----|------|-----|----|----------|----|------|----|---|-----|-----|-----|----|-----|----|----|-----|
| 563 - 1  | MIM 90 A 1            | 5       | .2       | 3.60 | (5 | 5  | 81       | (5 | .31  | (1       | 14   | 31       | 13 | 3.22     | .13 | 48 | .97  | 304 | 7  | .04      | 13 | 990  | 25 | 5 | 120 | 35  | .25 | 10 | 1   | 10 | 3  | .44 |
| 563 - 2  | MIM 90 A 2            | 5       | .2       | 4.58 | (5 | 2  | 134      | (5 | 1.10 | (1       | 20   | 53       | 16 | 3.88     | .21 | 57 | 2.03 | 510 | 2  | .08      | 19 | 577  | 23 | 5 | 20  | 182 | .27 | 10 | 43  | 10 | 2  | .44 |
| 563 - 3  | MIM 90 A 3            | 5       | .2       | 3.94 | (5 | 4  | 102      | (5 | 1.49 | (1       | 16   | 38       | 17 | 2.82     | .17 | 48 | 1.23 | 706 | 3  | .02      | 21 | 1471 | 19 | 5 | 20  | 112 | .21 | 10 | 73  | 10 | 11 | .46 |
| 563 - 4  | MIM 90 A 4            | 5       | .2       | 4.23 | (5 | 4  | 108      | (5 | .86  | (1       | 21   | 56       | 26 | 3.81     | .16 | 62 | 1.70 | 458 | 3  | .08      | 24 | 1041 | 19 | 5 | 20  | 131 | .24 | 10 | 106 | 10 | 3  | .42 |
| 563 - 5  | MIM 90 A 5            | 5       | .2       | 4.35 | (5 | 3  | 112      | (5 | .60  | (1       | 18   | 47       | 19 | 3.56     | .15 | 56 | 1.26 | 362 | 3  | .07      | 21 | 2097 | 20 | 5 | 20  | 98  | .27 | 10 | 97  | 10 | 3  | .46 |
| 563 - 6  | MIM 90 A 6            | 5       | .2       | 3.78 | (5 | 4  | 94       | (5 | .36  | (1       | 14   | 37       | 14 | 2.94     | .12 | 44 | .99  | 236 | 2  | .04      | 15 | 1836 | 22 | 5 | 20  | 53  | .19 | 10 | 65  | 10 | 1  | .44 |
| 563 - 7  | MIM 90 A 7            | 5       | .2       | 3.39 | (5 | 3  | 94       | (5 | .51  | (1       | 14   | 37       | 12 | 2.70     | .10 | 41 | .90  | 256 | 1  | .04      | 15 | 1170 | 20 | 5 | 20  | 56  | .19 | 10 | 65  | 10 | 1  | .49 |
| 563 - 8  | MIM 90 A 8            | 5       | .2       | 4.27 | (5 | 4  | 107      | (5 | .40  | (1       | 13   | 32       | 11 | 2.67     | .17 | 41 | .89  | 280 | 2  | .05      | 12 | 1902 | 25 | 5 | 20  | 57  | .27 | 10 | 53  | 10 | 2  | .36 |
| 563 - 9  | MIM 90 A 9            | 5       | .2       | 4.25 | (5 | 2  | 127      | (5 | .50  | (1       | 16   | 41       | 12 | 3.07     | .15 | 46 | 1.05 | 430 | 1  | .05      | 14 | 634  | 24 | 5 | 20  | 81  | .24 | 10 | 71  | 10 | 2  | .40 |
| 563 - 10 | MIM 90 A 10           | 5       | .2       | 5.17 | (5 | 3  | 131      | (5 | .38  | (1       | 18   | 49       | 14 | 3.27     | .16 | 50 | 1.31 | 402 | 2  | .05      | 18 | 657  | 28 | 5 | 20  | 88  | .26 | 10 | 89  | 10 | 3  | .42 |
| 563 - 11 | MIM 90 A 11           | 5       | .2       | 4.94 | (5 | 4  | 92       | (5 | .17  | (1       | 14   | 39       | 14 | 2.97     | .16 | 45 | .96  | 312 | 2  | .04      | 14 | 862  | 31 | 5 | 20  | 32  | .26 | 10 | 65  | 10 | 6  | .42 |
| 563 - 12 | MIM 90 A 12           | 5       | .2       | 3.71 | (5 | 3  | 117      | (5 | .37  | (1       | 13   | 37       | 14 | 2.62     | .20 | 39 | .95  | 841 | 2  | .04      | 13 | 1147 | 24 | 5 | 20  | 109 | .20 | 10 | 57  | 10 | 1  | .40 |
| 563 - 13 | MIM 90 A 13           | 5       | .2       | 5.13 | (5 | 4  | 105      | (5 | .24  | (1       | 15   | 31       | 16 | 2.59     | .11 | 39 | .82  | 207 | 1  | .04      | 23 | 987  | 29 | 5 | 20  | 36  | .15 | 10 | 41  | 10 | 3  | .31 |
| 563 - 14 | MIM 90 A 14           | 5       | .2       | 4.47 | (5 | 2  | 102      | (5 | .49  | (1       | 12   | 38       | 15 | 2.80     | .12 | 44 | 1.05 | 484 | 1  | .04      | 27 | 815  | 26 | 5 | 20  | 59  | .16 | 10 | 54  | 10 | 0  | .40 |
| 563 - 15 | MIM 90 A 15           | 5       | .2       | 4.12 | (5 | 3  | 117      | (5 | .27  | (1       | 17   | 31       | 17 | 2.76     | .11 | 42 | .86  | 651 | 7  | .03      | 22 | 1213 | 25 | 5 | 20  | 45  | .19 | 10 | 51  | 10 | 6  | .41 |
| 563 - 16 | MIM 90 A 16           | 5       | .2       | 2.90 | (5 | 2  | 98       | (5 | .67  | (1       | 13   | 33       | 28 | 2.73     | .10 | 58 | .82  | 388 | 1  | .03      | 18 | 395  | 21 | 5 | 20  | 66  | .15 | 10 | 66  | 10 | 9  | .32 |
| 563 - 17 | MIM 90 A 17           | 5       | .2       | 4.03 | (5 | 2  | 113      | (5 | .55  | (1       | 16   | 45       | 17 | 2.93     | .14 | 46 | .97  | 249 | 1  | .03      | 28 | 653  | 26 | 5 | 20  | 57  | .19 | 10 | 57  | 10 | 1  | .41 |
| 563 - 18 | MIM 90 A 18           | 5       | .2       | 2.85 | (5 | 2  | 102      | (5 | .64  | (1       | 14   | 51       | 28 | 2.77     | .09 | 48 | .94  | 482 | 2  | .03      | 24 | 397  | 21 | 5 | 20  | 56  | .17 | 10 | 71  | 10 | 3  | .40 |
| 563 - 19 | MIM 90 A 19           | 5       | .2       | 2.17 | (5 | 2  | 78       | (5 | .48  | (1       | 12   | 43       | 12 | 2.33     | .09 | 40 | .75  | 512 | 1  | .03      | 18 | 441  | 17 | 5 | 20  | 46  | .18 | 10 | 64  | 10 | 4  | .34 |
| 563 - 20 | MIM 90 A 20           | 5       | .2       | 2.68 | (5 | 2  | 81       | (5 | .55  | (1       | 15   | 56       | 16 | 2.99     | .11 | 50 | .98  | 343 | 2  | .03      | 24 | 441  | 21 | 5 | 20  | 46  | .20 | 10 | 81  | 10 | 3  | .49 |
| 563 - 21 | MIM 90 A 20 ROAD BD   | 5       | .2       | 2.89 | (5 | 2  | 91       | (5 | .64  | (1       | 14   | 45       | 15 | 2.73     | .10 | 43 | .71  | 402 | 1  | .04      | 19 | 623  | 19 | 5 | 20  | 81  | .28 | 10 | 75  | 10 | 9  | .44 |
| 563 - 22 | MIM 90 A 21           | 5       | .2       | 3.57 | (5 | 2  | 168      | (5 | .59  | (1       | 18   | 52       | 28 | 3.42     | .12 | 55 | 1.16 | 401 | 2  | .04      | 29 | 742  | 28 | 5 | 20  | 64  | .23 | 10 | 86  | 10 | 2  | .47 |
| 563 - 23 | MIM 90 A 21 ROAD 100  | 5       | .2       | 2.44 | (5 | 2  | 82       | (5 | .68  | (1       | 13   | 43       | 16 | 2.79     | .10 | 43 | .70  | 343 | 1  | .05      | 16 | 457  | 16 | 5 | 20  | 169 | .31 | 10 | 94  | 10 | 7  | .37 |
| 563 - 24 | MIM 90 A 22           | 5       | .2       | 2.99 | (5 | 2  | 129      | (5 | .38  | (1       | 12   | 32       | 13 | 2.41     | .16 | 39 | .65  | 412 | 2  | .02      | 15 | 1088 | 21 | 5 | 20  | 32  | .19 | 10 | 55  | 10 | 1  | .42 |
| 563 - 25 | MIM 90 A 22A ROAD 200 | 5       | .2       | 3.40 | (5 | 2  | 79       | (5 | .84  | (1       | 15   | 54       | 16 | 3.10     | .13 | 50 | 1.03 | 323 | 1  | .06      | 18 | 305  | 26 | 5 | 20  | 93  | .31 | 10 | 60  | 10 | 9  | .35 |
| 563 - 26 | MIM 90 A 23           | 5       | .2       | 2.64 | (5 | 2  | 80       | (5 | .63  | (1       | 11   | 30       | 12 | 2.29     | .10 | 36 | .53  | 326 | 1  | .04      | 19 | 382  | 17 | 5 | 20  | 69  | .24 | 10 | 58  | 10 | 5  | .43 |

## ECO-TECH LABORATORIES LTD.

## RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-563

PAGE 2

| ET#      | DESCRIPTION       | AU(ppb) | Ag AL(\$) | AS | B  | BA  | B1 CA(\$) | CD | CO | CR | CU FE(\$) | M(\$) | LA MG(\$) | MN   | MO NA(\$) | Ni      | P  | Pb     | SB  | SN  | SP  | Tl(\$) | U   | V | W  | X | Zn |
|----------|-------------------|---------|-----------|----|----|-----|-----------|----|----|----|-----------|-------|-----------|------|-----------|---------|----|--------|-----|-----|-----|--------|-----|---|----|---|----|
| 563 - 27 | MIM 90 A 24 S     | (5      | 1.2 3.36  | (5 | 3  | 85  | (5 .50    | (1 | 13 | 35 | 18 2.57   | .12   | 40 .71    | 291  | 2 .03     | 18 819  | 22 | (5 20  | 69  | .24 | 10  | .67    | 10  | 4 | 40 |   |    |
| 563 - 28 | MIM 90 A 25 S     | (5      | 1.2 4.02  | (5 | 2  | 103 | (5 .58    | (1 | 14 | 42 | 24 2.79   | .13   | 43 .91    | 248  | 2 .03     | 21 632  | 23 | (5 (20 | 75  | .22 | (10 | .64    | (10 | 1 | 35 |   |    |
| 563 - 29 | MIM 90 A 26 S     | (5      | 1.2 3.72  | (5 | 3  | 89  | (5 .63    | (1 | 13 | 38 | 16 2.64   | .23   | 41 .84    | 312  | 2 .03     | 23 1326 | 22 | (5 (20 | 72  | .21 | (10 | .60    | (10 | 2 | 45 |   |    |
| 563 - 30 | MIM 90 A 27 S     | (5      | 1.2 2.27  | (5 | 2  | 78  | (5 .97    | (1 | 14 | 39 | 20 2.88   | .16   | 49 .90    | 390  | 1 .07     | 19 573  | 13 | (5 (20 | 143 | .29 | (10 | .87    | (10 | 8 | 34 |   |    |
| 563 - 31 | MIM 90 A 28 S     | (5      | 1.2 2.44  | (5 | 2  | 85  | (5 .56    | (1 | 10 | 26 | 11 1.93   | .10   | 30 .41    | 590  | 1 .04     | 11 2241 | 18 | (5 (20 | 49  | .18 | (10 | .41    | (10 | 3 | 54 |   |    |
| 563 - 32 | MIM 90 A 29 S     | (5      | 1.2 3.50  | (5 | 2  | 92  | (5 .63    | (1 | 15 | 47 | 17 2.95   | .13   | 45 .84    | 328  | 1 .04     | 23 652  | 21 | (5 (20 | 95  | .25 | (10 | .73    | (10 | 2 | 34 |   |    |
| 563 - 33 | MIM 90 A 30 S     | (5      | 1.2 4.55  | (5 | 2  | 109 | (5 .92    | (1 | 16 | 47 | 21 3.13   | .24   | 52 1.09   | 301  | 1 .04     | 26 907  | 24 | (5 (20 | 151 | .21 | (10 | .78    | (10 | 1 | 30 |   |    |
| 563 - 34 | MIM 90 A 31 S     | (5      | 1.2 4.38  | (5 | 2  | 102 | (5 .73    | (1 | 16 | 47 | 19 3.20   | .19   | 52 1.00   | 295  | 2 .04     | 27 606  | 25 | (5 (20 | 131 | .24 | (10 | .74    | (10 | 1 | 37 |   |    |
| 563 - 35 | MIM 90 A 32 S     | (5      | 1.2 4.06  | (5 | 2  | 120 | (5 .75    | (1 | 16 | 46 | 21 3.26   | .12   | 53 1.02   | 410  | 1 .04     | 21 515  | 22 | (5 (20 | 140 | .30 | (10 | .87    | (10 | 5 | 37 |   |    |
| 563 - 36 | MIM 90 A 33 S     | (5      | 1.2 3.63  | (5 | 2  | 96  | (5 .47    | (1 | 13 | 33 | 13 2.44   | .13   | 38 .65    | 354  | 1 .03     | 18 766  | 22 | (5 20  | 57  | .23 | (10 | .54    | (10 | 3 | 36 |   |    |
| 563 - 37 | MIM 90 A 34 S     | (5      | 1.2 3.32  | (5 | 2  | 100 | (5 .54    | (1 | 13 | 36 | 15 2.57   | .12   | 40 .70    | 672  | 1 .03     | 18 948  | 20 | (5 20  | 1   | .24 | (10 | .63    | (10 | 2 | 41 |   |    |
| 563 - 38 | MIM 90 A 35 S     | (5      | 1.2 3.09  | (5 | 2  | 84  | (5 .89    | (1 | 16 | 45 | 21 3.09   | .12   | 55 1.11   | 391  | 1 .06     | 22 728  | 18 | (5 20  | 144 | .27 | (10 | .63    | (10 | 8 | 34 |   |    |
| 563 - 39 | L9+500N 9+ 350 E  | 5       | 1.2 2.08  | (5 | 2  | 96  | (5 1.09   | (1 | 17 | 44 | 36 3.08   | .12   | 56 1.14   | 565  | 2 .06     | 23 865  | 20 | (5 (20 | 123 | .22 | (10 | .39    | (10 | 1 | 36 |   |    |
| 563 - 40 | L9+500N 9+ 400 E  | (5      | 1.2 2.45  | (5 | 3  | 230 | (5 .87    | (1 | 15 | 45 | 25 2.94   | .23   | 52 .99    | 594  | 1 .02     | 17 1433 | 19 | (5 (20 | 55  | .10 | (10 | .59    | (10 | 1 | 46 |   |    |
| 563 - 41 | L9+500N 9+ 450 E  | (5      | 1.2 2.30  | (5 | 2  | 304 | (5 .72    | (1 | 13 | 33 | 20 2.32   | .16   | 44 .74    | 431  | 1 .03     | 15 1920 | 20 | (5 (20 | 51  | .11 | (10 | .48    | (10 | 3 | 34 |   |    |
| 563 - 42 | L9+500N 9+ 500 E  | (5      | 1.2 2.08  | (5 | 2  | 219 | (5 .83    | (1 | 15 | 43 | 15 2.60   | .21   | 44 .82    | 869  | 1 .02     | 17 986  | 18 | (5 (20 | 35  | .11 | (10 | .37    | (10 | 1 | 35 |   |    |
| 563 - 43 | L9+500N 9+ 550 E  | (5      | 1.2 2.22  | (5 | 2  | 136 | (5 .70    | (1 | 18 | 61 | 20 3.25   | .19   | 58 .76    | 784  | 2 .03     | 26 352  | 24 | (5 20  | 62  | .16 | (10 | .37    | (10 | 1 | 48 |   |    |
| 563 - 44 | L9+500N 9+ 600 E  | 5       | 1.2 1.25  | (5 | 2  | 124 | (5 .55    | (1 | 9  | 28 | 8 1.74    | .10   | 27 .45    | 1390 | 1 .03     | 8 513   | 11 | (5 20  | 39  | .11 | (10 | .45    | (10 | 1 | 36 |   |    |
| 563 - 45 | L9+500N 9+ 650 E  | (5      | 1.2 2.33  | (5 | 3  | 148 | (5 .72    | (1 | 15 | 62 | 18 2.56   | .20   | 42 .86    | 928  | 2 .03     | 22 942  | 17 | (5 20  | 79  | .11 | (10 | .57    | (10 | 1 | 56 |   |    |
| 563 - 46 | L9+500N 9+ 700 E  | (5      | 1.2 2.28  | (5 | 2  | 143 | (5 .60    | (1 | 15 | 79 | 18 2.87   | .19   | 48 .87    | 807  | 1 .03     | 23 637  | 19 | (5 20  | 51  | .18 | (10 | .72    | (10 | 1 | 51 |   |    |
| 563 - 47 | L9+500N 9+ 750 E  | 5       | 1.2 2.46  | (5 | 2  | 126 | (5 .92    | (1 | 14 | 47 | 17 3.41   | .24   | 45 .75    | 580  | 1 .03     | 29 716  | 13 | (5 20  | 87  | .20 | (10 | .73    | (10 | 3 | 46 |   |    |
| 563 - 48 | L9+500N 9+ 850 E  | (5      | 1.2 2.38  | (5 | 3  | 95  | (5 .97    | (1 | 11 | 45 | 18 3.44   | .16   | 48 .69    | 360  | 2 .05     | 16 286  | 12 | (5 (20 | 122 | .20 | (10 | .67    | (10 | 4 | 36 |   |    |
| 563 - 49 | L9+500N 9+ 900 E  | (5      | 1.2 2.19  | (5 | 2  | 86  | (5 .83    | (1 | 13 | 47 | 19 3.71   | .23   | 49 .81    | 508  | 2 .06     | 20 392  | 10 | (5 (20 | 109 | .22 | (10 | .60    | (10 | 4 | 44 |   |    |
| 563 - 50 | L9+500N 9+ 950 E  | (5      | 1.2 2.43  | (5 | 2  | 76  | (5 .83    | (1 | 13 | 49 | 21 3.87   | .18   | 51 .79    | 397  | 2 .07     | 20 279  | 9  | (5 (20 | 126 | .29 | (10 | .49    | (10 | 2 | 43 |   |    |
| 563 - 51 | L9+500N 11+ 000 E | (5      | 1.2 2.22  | (5 | 2  | 69  | (5 .72    | (1 | 11 | 47 | 13 3.37   | .14   | 41 .58    | 297  | 1 .06     | 17 335  | 9  | (5 (20 | 109 | .32 | (10 | .77    | (10 | 5 | 32 |   |    |
| 563 - 52 | L9+500N 11+ 050 E | (5      | 1.2 1.90  | (5 | 2  | 70  | (5 .69    | (1 | 10 | 42 | 13 3.22   | .11   | 39 .47    | 249  | 1 .05     | 12 293  | 9  | (5 (20 | 116 | .32 | (10 | .61    | (10 | 6 | 30 |   |    |
| 563 - 53 | L9+500N 11+ 100 E | (5      | 1.2 2.14  | (5 | 2  | 74  | (5 .55    | (1 | 9  | 38 | 10 2.90   | .11   | 36 .44    | 314  | 1 .04     | 12 198  | 11 | (5 20  | 78  | .29 | (10 | .65    | (10 | 5 | 30 |   |    |
| 563 - 54 | L9+500N 11+ 150 E | (5      | 1.2 2.47  | (5 | 3  | 76  | (5 .50    | (1 | 9  | 36 | 10 2.81   | .12   | 36 .46    | 392  | 2 .03     | 16 504  | 12 | (5 (20 | 58  | .24 | (10 | .69    | (10 | 3 | 42 |   |    |
| 563 - 55 | L9+500N 11+ 200 E | (5      | 1.2 5.57  | (5 | 2  | 141 | (5 .42    | (1 | 16 | 57 | 21 3.95   | .12   | 52 .92    | 671  | 2 .02     | 29 867  | 24 | (5 (20 | 57  | .22 | (10 | .65    | (10 | 1 | 39 |   |    |
| 563 - 56 | L9+500N 11+ 250 E | (5      | 1.2 2.86  | (5 | 2  | 74  | (5 .53    | (1 | 9  | 42 | 10 2.95   | .17   | 37 .62    | 345  | 2 .03     | 13 363  | 12 | (5 (20 | 65  | .22 | (10 | .60    | (10 | 1 | 41 |   |    |
| 563 - 57 | L9+500N 11+ 300 E | (5      | 1.2 2.70  | (5 | 3  | 85  | (5 .52    | (1 | 10 | 43 | 11 3.05   | .09   | 39 .60    | 298  | 2 .03     | 14 627  | 9  | (5 20  | 65  | .23 | (10 | .66    | (10 | 4 | 44 |   |    |
| 563 - 58 | L9+500N 11+ 350 E | (5      | 1.2 5.45  | (5 | 3  | 76  | (5 .52    | (1 | 19 | 66 | 21 4.44   | .11   | 62 .143   | 657  | 2 .05     | 13 495  | 13 | (5 (20 | 71  | .29 | (10 | .60    | (10 | 3 | 52 |   |    |
| 563 - 59 | L9+500N 11+ 400 E | (5      | 1.2 4.05  | (5 | 2  | 74  | (5 .87    | (1 | 14 | 63 | 14 3.58   | .15   | 51 1.19   | 397  | 1 .03     | 17 426  | 11 | (5 20  | 100 | .29 | (10 | .62    | (10 | 3 | 49 |   |    |
| 563 - 60 | L9+500N 11+ 450 E | (5      | 1.2 3.78  | (5 | 1  | 73  | (5 .69    | (1 | 11 | 46 | 11 3.09   | .13   | 39 .63    | 500  | 2 .04     | 15 435  | 14 | (5 20  | 76  | .24 | (10 | .64    | (10 | 1 | 41 |   |    |
| 563 - 61 | L9+500N 11+ 500 E | (5      | 1.2 4.20  | (5 | 2  | 66  | (5 .68    | (1 | 15 | 72 | 13 3.46   | .20   | 47 1.01   | 1627 | 2 .03     | 15 1495 | 19 | (5 20  | 96  | .27 | (10 | .67    | (10 | 2 | 54 |   |    |
| 563 - 62 | L9+500N 11+ 550 E | (5      | 1.2 2.96  | (5 | 17 | 71  | (5 .45    | (1 | 10 | 40 | 10 2.86   | .08   | 37 .61    | 380  | 2 .03     | 16 561  | 15 | (5 20  | 54  | .24 | (10 | 56     | (10 | 3 | 54 |   |    |
| 563 - 63 | L9+500N 10+ 350 E | (5      | 1.2 2.44  | (5 | 4  | 71  | (5 1.10   | (1 | 14 | 43 | 23 3.55   | .31   | 52 .91    | 651  | 1 .04     | 15 650  | 11 | (5 (20 | 148 | .24 | (10 | 30     | (10 | 3 | 44 |   |    |

## ECO-TECH LABORATORIES LTD.

## RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-563

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| ET#       | DESCRIPTION     | AU(ppb) | AS AL(%) | AS  | B    | BA | BI CA(%) | CD  | CO | CR   | CU FE(%) | X(%) | LA MG(%) | MN  | MO NA(%) | NI  | P  | PB   | SB   | SN | SP Ti(%) | U  | V    | W  | T  | Zn  |     |     |    |     |    |   |    |
|-----------|-----------------|---------|----------|-----|------|----|----------|-----|----|------|----------|------|----------|-----|----------|-----|----|------|------|----|----------|----|------|----|----|-----|-----|-----|----|-----|----|---|----|
| 563 - 64  | 9+600N 10+ 400  | E       | 15       | 1.2 | 2.07 | 15 | 2        | 122 | 15 | .69  | 0        | 11   | 44       | 14  | 3.54     | .18 | 47 | .72  | 420  | 2  | .04      | 16 | 499  | 13 | 15 | (20 | 88  | .21 | 10 | 76  | 10 | 1 | 50 |
| 563 - 65  | 9+600N 10+ 450  | E       | 15       | .3  | 3.74 | 15 | 2        | 170 | 15 | .80  | 0        | 21   | 37       | 38  | 4.39     | .26 | 62 | .84  | 900  | 2  | .02      | 21 | 608  | 19 | 15 | (20 | 238 | .16 | 10 | 68  | 10 | 1 | 37 |
| 563 - 66  | 9+600N 10+ 500  | E       | 5        | .5  | 2.75 | 15 | 3        | 175 | 15 | .57  | 0        | 14   | 50       | 29  | 4.04     | .19 | 61 | 1.01 | 391  | 0  | .03      | 18 | 480  | 17 | 15 | (20 | 68  | .10 | 10 | 75  | 10 | 1 | 56 |
| 563 - 67  | 9+600N 10+ 550  | E       | 15       | .6  | 2.44 | 15 | 2        | 159 | 15 | 1.11 | 0        | 12   | 49       | 28  | 3.34     | .14 | 57 | .98  | 579  | 1  | .02      | 16 | 985  | 12 | 15 | (20 | 84  | .10 | 10 | 62  | 10 | 2 | 45 |
| 563 - 68  | 9+600N 10+ 600  | E       | 10       | .3  | 2.70 | 15 | 2        | 164 | 15 | .62  | 0        | 13   | 51       | 29  | 3.73     | .21 | 53 | .97  | 555  | 2  | .04      | 17 | 514  | 15 | 15 | (20 | 126 | .12 | 10 | 73  | 10 | 1 | 46 |
| 563 - 69  | 9+600N 10+ 650  | E       | 10       | .7  | 2.89 | 15 | 2        | 165 | 15 | .77  | 0        | 15   | 55       | 29  | 3.93     | .25 | 57 | 1.07 | 939  | 3  | .02      | 27 | 989  | 27 | 15 | (20 | 64  | .13 | 10 | 67  | 10 | 1 | 52 |
| 563 - 70  | 9+600N 10+ 700  | E       | 15       | .8  | 2.57 | 15 | 2        | 348 | 15 | .99  | 0        | 14   | 52       | 23  | 3.15     | .19 | 47 | .80  | 1661 | 2  | .01      | 21 | 1682 | 19 | 15 | (20 | 81  | .10 | 10 | 53  | 10 | 1 | 80 |
| 563 - 71  | 9+600N 10+ 750  | E       | 15       | 1.2 | 2.66 | 15 | 2        | 155 | 15 | .77  | 0        | 14   | 61       | 18  | 3.69     | .19 | 51 | .88  | 843  | 3  | .03      | 24 | 619  | 15 | 15 | (20 | 70  | .18 | 10 | 71  | 10 | 1 | 57 |
| 563 - 72  | 9+600N 10+ 800  | E       | 15       | 1.2 | 2.53 | 15 | 2        | 117 | 15 | .79  | 0        | 12   | 44       | 17  | 3.29     | .17 | 46 | .89  | 656  | 2  | .03      | 20 | 987  | 12 | 15 | (20 | 103 | .14 | 10 | 66  | 10 | 1 | 41 |
| 563 - 73  | 9+600N 10+ 850  | E       | 5        | 1.2 | 2.39 | 15 | 2        | 91  | 15 | .81  | 0        | 10   | 41       | 13  | 3.00     | .09 | 42 | .58  | 332  | 1  | .03      | 15 | 266  | 12 | 15 | (20 | 87  | .12 | 10 | 61  | 10 | 1 | 38 |
| 563 - 74  | 9+600N 10+ 900  | E       | 15       | 1.2 | 2.19 | 15 | 2        | 63  | 15 | .79  | 0        | 12   | 47       | 17  | 3.26     | .15 | 45 | .76  | 414  | 1  | .05      | 18 | 362  | 12 | 15 | (20 | 122 | .15 | 10 | 77  | 10 | 1 | 51 |
| 563 - 75  | 9+600N 10+ 950  | I       | 10       | 1.2 | 1.81 | 15 | 2        | 75  | 6  | .68  | 0        | 10   | 40       | 12  | 2.96     | .11 | 38 | .52  | 432  | 1  | .05      | 14 | 786  | 3  | 15 | (20 | 97  | .13 | 10 | 63  | 10 | 1 | 58 |
| 563 - 76  | 19+600N 11+ 00  | E       | 5        | 1.2 | 2.61 | 15 | 2        | 71  | 15 | .81  | 0        | 14   | 52       | 21  | 3.74     | .17 | 55 | .81  | 351  | 2  | .04      | 24 | 509  | 12 | 15 | (20 | 102 | .19 | 10 | 83  | 10 | 3 | 36 |
| 563 - 77  | 19+600N 11+ 50  | E       | 10       | 1.2 | 2.11 | 15 | 2        | 65  | 6  | .57  | 0        | 9    | 38       | 12  | 2.88     | .09 | 39 | .49  | 243  | 1  | .05      | 13 | 318  | 11 | 15 | (20 | 66  | .19 | 10 | 65  | 10 | 5 | 32 |
| 563 - 78  | 19+600N 11+ 100 | E       | 25       | 1.2 | 2.76 | 15 | 3        | 75  | 15 | .57  | 0        | 11   | 43       | 13  | 3.23     | .08 | 43 | .58  | 346  | 2  | .04      | 19 | 435  | 13 | 15 | (20 | 63  | .17 | 10 | 75  | 10 | 4 | 45 |
| 563 - 79  | 19+600N 11+ 150 | E       | 10       | 1.2 | 2.77 | 15 | 2        | 70  | 0  | .44  | 0        | 10   | 36       | 11  | 2.73     | .07 | 36 | .51  | 339  | 2  | .03      | 15 | 349  | 15 | 15 | (20 | 50  | .24 | 10 | 56  | 10 | 4 | 59 |
| 563 - 80  | 19+600N 11+ 200 | E       | 10       | 1.2 | 3.60 | 15 | 2        | 99  | 15 | .38  | 0        | 11   | 37       | 12  | 2.91     | .11 | 38 | .59  | 729  | 2  | .02      | 20 | 575  | 17 | 15 | (20 | 40  | .18 | 10 | 52  | 10 | 1 | 68 |
| 563 - 81  | 19+600N 11+ 250 | E       | 15       | 1.2 | 5.84 | 15 | 2        | 103 | 7  | .34  | 0        | 17   | 69       | 20  | 4.38     | .12 | 62 | .97  | 1043 | 3  | .03      | 16 | 699  | 25 | 15 | (20 | 51  | .24 | 10 | 81  | 10 | 1 | 56 |
| 563 - 82  | 19+600N 11+ 300 | E       | 10       | 1.2 | 3.41 | 15 | 2        | 91  | 15 | .52  | 0        | 9    | 37       | 12  | 2.45     | .07 | 40 | .67  | 819  | 1  | .02      | 15 | 416  | 17 | 15 | (20 | 54  | .15 | 10 | 42  | 10 | 5 | 44 |
| 563 - 83  | 19+600N 11+ 350 | I       | 5        | 1.2 | 3.19 | 15 | 2        | 71  | 15 | .65  | 0        | 12   | 49       | 12  | 2.98     | .15 | 40 | .85  | 589  | 1  | .02      | 15 | 545  | 14 | 15 | (20 | 49  | .12 | 10 | 51  | 10 | 3 | 56 |
| 563 - 84  | 19+600N 11+ 400 | E       | 10       | 1.2 | 5.15 | 15 | 2        | 110 | 6  | .70  | 0        | 18   | 74       | 18  | 4.41     | .15 | 63 | 1.28 | 648  | 3  | .03      | 14 | 512  | 22 | 15 | (20 | 117 | .30 | 10 | 84  | 10 | 4 | 52 |
| 563 - 85  | 19+600N 11+ 450 | E       | 5        | 1.2 | 5.29 | 15 | 2        | 86  | 15 | .80  | 0        | 17   | 69       | 15  | 3.96     | .16 | 56 | 1.33 | 548  | 2  | .02      | 20 | 670  | 21 | 15 | (20 | 109 | .29 | 10 | 69  | 10 | 3 | 46 |
| 563 - 86  | 19+600N 11+ 500 | E       | 10       | 1.2 | 5.35 | 15 | 2        | 97  | 15 | .62  | 0        | 16   | 60       | 16  | 3.82     | .14 | 52 | .96  | 675  | 2  | .02      | 23 | 931  | 29 | 15 | (20 | 81  | .26 | 10 | 67  | 10 | 2 | 59 |
| 563 - 87  | 19+600N 11+ 550 | I       | 10       | 1.2 | 4.66 | 15 | 2        | 93  | 15 | .59  | 0        | 12   | 58       | 15  | 3.59     | .09 | 47 | .97  | 447  | 2  | .03      | 23 | 459  | 21 | 15 | (20 | 74  | .19 | 10 | 53  | 10 | 3 | 54 |
| 563 - 88  | 19+700N 10+ 200 | E       | 5        | 1.2 | 2.38 | 15 | 2        | 92  | 15 | 1.33 | 0        | 16   | 50       | 47  | 3.89     | .13 | 69 | 1.26 | 613  | 2  | .08      | 25 | 205  | 15 | 15 | (20 | 145 | .22 | 10 | 50  | 10 | 6 | 46 |
| 563 - 89  | 19+700N 10+ 250 | E       | 5        | 1.2 | 2.91 | 15 | 2        | 91  | 15 | 1.25 | 0        | 20   | 51       | 111 | 4.50     | .20 | 68 | 1.56 | 689  | 2  | .08      | 31 | 984  | 17 | 15 | (20 | 147 | .22 | 10 | 99  | 10 | 5 | 49 |
| 563 - 90  | 19+700N 10+ 300 | E       | 5        | .3  | 2.62 | 15 | 2        | 98  | 15 | 1.07 | 0        | 17   | 48       | 56  | 4.10     | .14 | 63 | 1.29 | 589  | 2  | .06      | 26 | 812  | 22 | 15 | (20 | 133 | .24 | 10 | 80  | 10 | 5 | 45 |
| 563 - 91  | 19+700N 10+ 350 | I       | 5        | .4  | 1.88 | 15 | 2        | 85  | 15 | .93  | 0        | 15   | 43       | 34  | 3.47     | .09 | 50 | .90  | 504  | 2  | .03      | 13 | 975  | 1  | 15 | (20 | 107 | .47 | 10 | 91  | 10 | 1 | 56 |
| 563 - 92  | 19+700N 10+ 400 | E       | 5        | 1.2 | 2.83 | 15 | 2        | 77  | 15 | .85  | 0        | 20   | 55       | 37  | 4.50     | .20 | 65 | 1.15 | 570  | 3  | .05      | 26 | 541  | 17 | 15 | (20 | 129 | .24 | 10 | 93  | 10 | 1 | 63 |
| 563 - 93  | 19+700N 10+ 450 | E       | 10       | .3  | 3.26 | 15 | 2        | 91  | 8  | .84  | 0        | 22   | 55       | 39  | 4.78     | .21 | 65 | 1.17 | 640  | 2  | .04      | 29 | 760  | 18 | 15 | (20 | 101 | .20 | 10 | 94  | 10 | 4 | 59 |
| 563 - 94  | 19+700N 10+ 500 | E       | 15       | .4  | 2.54 | 15 | 2        | 330 | 15 | 1.01 | 0        | 17   | 45       | 23  | 3.68     | .11 | 52 | 1.00 | 123  | 1  | .02      | 17 | 1313 | 17 | 15 | (20 | 54  | .37 | 10 | 57  | 10 | 3 | 62 |
| 563 - 95  | 19+700N 10+ 550 | I       | 15       | .6  | 3.70 | 15 | 2        | 324 | 15 | .80  | 0        | 19   | 67       | 51  | 6.98     | .26 | 97 | 1.71 | 959  | 2  | .01      | 25 | 782  | 36 | 15 | (20 | 23  | .22 | 10 | 113 | 10 | 3 | 51 |
| 563 - 96  | 19+700N 10+ 600 | E       | 15       | .4  | 3.53 | 15 | 2        | 124 | 15 | .41  | 0        | 18   | 48       | 32  | 4.18     | .16 | 79 | 1.95 | 597  | 1  | .01      | 25 | 878  | 14 | 15 | (20 | 20  | .20 | 10 | 75  | 10 | 4 | 47 |
| 563 - 97  | 19+700N 10+ 650 | E       | 15       | .7  | 4.78 | 15 | 2        | 123 | 15 | .49  | 0        | 20   | 61       | 30  | 5.63     | .18 | 75 | 1.79 | 644  | 1  | .02      | 29 | 1143 | 27 | 15 | (20 | 49  | .21 | 10 | 78  | 10 | 4 | 47 |
| 563 - 98  | 19+700N 10+ 700 | E       | 15       | .3  | 3.95 | 15 | 2        | 189 | 15 | .85  | 0        | 19   | 54       | 32  | 4.9      | .16 | 75 | 1.16 | 779  | 2  | .02      | 30 | 672  | 29 | 15 | (20 | 48  | .21 | 10 | 75  | 10 | 4 | 47 |
| 563 - 99  | 19+700N 10+ 750 | E       | 5        | .2  | 3.19 | 15 | 2        | 224 | 15 | .97  | 0        | 18   | 49       | 25  | 4.55     | .22 | 56 | 1.93 | 100  | 1  | .01      | 27 | 1013 | 37 | 15 | (20 | 31  | .21 | 10 | 72  | 10 | 3 | 47 |
| 563 - 100 | 19+700N 10+ 800 | E       | 5        | .6  | 2.77 | 15 | 2        | 148 | 15 | 1.65 | 0        | 11   | 32       | 39  | 3.22     | .12 | 70 | .69  | 746  | 3  | .01      | 26 | 518  | 17 | 15 | (20 | 31  | .21 | 10 | 49  | 10 | 3 | 46 |

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RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-563

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| ET#      | DESCRIPTION     | AU(ppb) | Ag AL(%) | AS  | B    | BA | Bl CA(%) | CD  | CO | CR   | Cu Fe(%) | X(%) | La Mg(%) | Mn  | Mo Na(%) | Ni  | P  | PB   | SB   | Sn | SR Ti(%) | U  | V    | W  | Y  | Zn  |     |     |     |    |     |    |    |
|----------|-----------------|---------|----------|-----|------|----|----------|-----|----|------|----------|------|----------|-----|----------|-----|----|------|------|----|----------|----|------|----|----|-----|-----|-----|-----|----|-----|----|----|
| 563 -101 | L9+700N 10+ 850 | E       | (5       | .3  | 3.13 | (5 | 2        | 123 | (5 | 1.48 | (1       | 12   | 41       | 27  | 3.67     | .10 | 58 | .70  | 507  | 2  | .03      | 18 | 283  | 13 | (5 | (20 | 97  | .17 | (10 | 52 | (10 | 8  | 33 |
| 563 -102 | L9+700N 10+ 900 | E       | 25       | 1.2 | 2.75 | (5 | 2        | 66  | (5 | .65  | (1       | 11   | 44       | 12  | 3.27     | .18 | 40 | .67  | 311  | (1 | .03      | 19 | 640  | 12 | (5 | (20 | 74  | .21 | (10 | 60 | (10 | 1  | 30 |
| 563 -103 | L9+700N 10+ 950 | E       | (5       | 1.2 | 3.40 | (5 | 2        | 85  | 6  | .50  | (1       | 11   | 45       | 11  | 3.54     | .11 | 42 | .66  | 355  | 2  | .03      | 22 | 743  | 17 | (5 | (20 | 64  | .23 | (10 | 62 | (10 | 1  | 40 |
| 563 -104 | L9+700N 11+ 00  | E       | (5       | 1.2 | 2.45 | (5 | 2        | 91  | (5 | .53  | (1       | 10   | 42       | 12  | 3.32     | .10 | 39 | .51  | 460  | 1  | .03      | 16 | 639  | 12 | (5 | (20 | 69  | .27 | (10 | 70 | (10 | 3  | 47 |
| 563 -105 | L9+700N 11+ 50  | E       | (5       | 1.2 | 3.09 | (5 | 2        | 72  | (5 | .54  | (1       | 12   | 47       | 14  | 3.61     | .07 | 45 | .69  | 305  | 1  | .03      | 20 | 300  | 15 | (5 | (20 | 65  | .27 | (10 | 73 | (10 | 4  | 47 |
| 563 -106 | L9+700N 11+ 100 | E       | (5       | 1.2 | 2.55 | (5 | 3        | 60  | (5 | .35  | (1       | 11   | 37       | 9   | 2.98     | .09 | 36 | .47  | 376  | (1 | .03      | 16 | 559  | 12 | (5 | (20 | 40  | .21 | (10 | 55 | (10 | 1  | 54 |
| 563 -107 | L9+700N 11+ 150 | E       | (5       | 1.2 | 3.03 | (5 | 3        | 84  | (5 | .60  | (1       | 12   | 49       | 16  | 4.00     | .08 | 48 | .77  | 341  | 2  | .04      | 21 | 462  | 14 | (5 | (20 | 80  | .29 | (10 | 83 | (10 | 3  | 52 |
| 563 -108 | L9+700N 11+ 200 | E       | 5        | 1.2 | 3.46 | (5 | 2        | 78  | (5 | .68  | (1       | 12   | 44       | 16  | 3.77     | .09 | 49 | .73  | 231  | 1  | .04      | 19 | 408  | 15 | (5 | (20 | 63  | .21 | (10 | 65 | (10 | 2  | 32 |
| 563 -109 | L9+700N 11+ 250 | E       | (5       | 1.2 | 4.02 | (5 | 2        | 127 | 5  | .57  | (1       | 13   | 54       | 15  | 4.09     | .13 | 49 | .92  | 213  | 2  | .02      | 22 | 550  | 17 | (5 | (20 | 62  | .22 | (10 | 70 | (10 | 3  | 53 |
| 563 -110 | L9+700N 11+ 300 | E       | (5       | 1.2 | 5.56 | (5 | 4        | 102 | (5 | .56  | (1       | 17   | 73       | 17  | 4.57     | .19 | 56 | 1.23 | 1079 | 2  | .02      | 27 | 845  | 21 | (5 | (20 | 78  | .28 | (10 | 77 | (10 | 41 | 69 |
| 563 -111 | L9+700N 11+ 350 | E       | (5       | 1.2 | 6.34 | (5 | 2        | 118 | 5  | .52  | (1       | 17   | 68       | 17  | 4.57     | .16 | 56 | 1.12 | 832  | 2  | .02      | 26 | 826  | 23 | (5 | (20 | 62  | .27 | (10 | 71 | (10 | 1  | 72 |
| 563 -112 | L9+700N 11+ 400 | E       | (5       | 1.2 | 5.90 | (5 | 2        | 120 | (5 | .60  | (1       | 18   | 69       | 21  | 4.93     | .13 | 62 | 1.11 | 538  | 2  | .03      | 31 | 648  | 10 | (5 | (20 | 85  | .29 | (10 | 83 | (10 | 1  | 49 |
| 563 -113 | L9+700N 11+ 450 | E       | (5       | 1.2 | 6.64 | (5 | 5        | 77  | (5 | .47  | (1       | 17   | 72       | 21  | 4.77     | .12 | 60 | 1.29 | 392  | 2  | .03      | 25 | 1085 | 23 | (5 | (20 | 69  | .30 | (10 | 75 | (10 | 4  | 52 |
| 563 -114 | L9+700N 11+ 500 | E       | 5        | 1.2 | 4.94 | (5 | 3        | 108 | (5 | .47  | (1       | 14   | 59       | 19  | 3.90     | .13 | 47 | .80  | 463  | 1  | .03      | 29 | 1151 | 19 | (5 | (20 | 75  | .22 | (10 | 65 | (10 | 41 | 53 |
| 563 -115 | L9+700N 11+ 550 | E       | 10       | 1.2 | 2.83 | (5 | 4        | 54  | (5 | .58  | (1       | 9    | 42       | 13  | 3.03     | .06 | 38 | .59  | 427  | (1 | .04      | 13 | 216  | 13 | (5 | (20 | 54  | .23 | (10 | 59 | (10 | 5  | 37 |
| 563 -116 | L9+800N 10+ 50  | E       | 20       | 1.2 | 3.22 | (5 | 3        | 74  | (5 | 1.39 | (1       | 20   | 59       | 37  | 4.85     | .27 | 66 | 1.74 | 679  | 1  | .09      | 37 | 946  | 11 | (5 | (20 | 162 | .27 | (10 | 92 | (10 | 9  | 45 |
| 563 -117 | L9+800N 10+ 100 | E       | (5       | .5  | 2.47 | (5 | 3        | 102 | (5 | .58  | (1       | 12   | 26       | 757 | 4.00     | .17 | 50 | .87  | 618  | 1  | .03      | 16 | 450  | 13 | (5 | (20 | 104 | .15 | (10 | 74 | (10 | 1  | 55 |
| 563 -118 | L9+800N 10+ 150 | E       | 5        | 1.2 | 2.49 | (5 | 3        | 92  | (5 | .76  | (1       | 17   | 53       | 74  | 4.37     | .25 | 58 | 1.02 | 607  | 1  | .06      | 23 | 345  | 16 | (5 | (20 | 111 | .24 | (10 | 86 | (10 | 4  | 41 |
| 563 -119 | L9+800N 10+ 200 | E       | 10       | 1.2 | 3.00 | (5 | 4        | 99  | (5 | .86  | (1       | 14   | 46       | 39  | 3.80     | .20 | 53 | .85  | 698  | 1  | .04      | 21 | 677  | 12 | (5 | (20 | 76  | .17 | (10 | 68 | (10 | 3  | 57 |
| 563 -120 | L9+800N 10+ 350 | E       | (5       | .3  | 2.75 | (5 | 4        | 89  | (5 | .73  | (1       | 18   | 26       | 18  | 3.23     | .13 | 36 | .55  | 835  | (1 | .03      | 16 | 2704 | 16 | (5 | (20 | 91  | .13 | (10 | 42 | (10 | 11 | 93 |
| 563 -121 | L9+800N 10+ 400 | E       | 990      | 4   | 4.49 | (5 | 2        | 86  | (5 | .91  | (1       | 26   | 48       | 44  | 5.82     | .15 | 73 | 1.44 | 689  | 2  | .03      | 24 | 760  | 13 | (5 | (20 | 232 | .14 | (10 | 81 | (10 | 41 | 77 |
| 563 -122 | L9+800N 10+ 450 | E       | (5       | .6  | 4.35 | (5 | 2        | 115 | (5 | .67  | (1       | 24   | 53       | 39  | 6.79     | .20 | 85 | 1.70 | 683  | 3  | .03      | 24 | 1030 | 25 | (5 | (20 | 203 | .09 | (10 | 89 | (10 | 41 | 68 |
| 563 -123 | L9+800N 10+ 500 | E       | (5       | .3  | 4.60 | (5 | 3        | 188 | (5 | .77  | (1       | 18   | 54       | 33  | 4.68     | .16 | 70 | 1.07 | 787  | 2  | .02      | 25 | 715  | 27 | (5 | (20 | 46  | .13 | (10 | 73 | (10 | 4  | 65 |
| 563 -124 | L9+800N 10+ 550 | E       | (5       | 1.2 | 4.62 | (5 | 3        | 298 | (5 | .60  | (1       | 16   | 55       | 25  | 4.60     | .15 | 56 | 1.09 | 2764 | 2  | .02      | 21 | 1835 | 29 | (5 | (20 | 45  | .10 | (10 | 75 | (10 | 41 | 92 |
| 563 -125 | L9+800N 10+ 600 | E       | (5       | 1.2 | 3.94 | (5 | 4        | 175 | (5 | .54  | (1       | 20   | 56       | 33  | 5.78     | .21 | 77 | 1.04 | 1285 | 2  | .02      | 27 | 1151 | 21 | (5 | (20 | 35  | .07 | (10 | 79 | (10 | 11 | 91 |
| 563 -126 | L9+800N 10+ 650 | E       | (5       | .3  | 3.86 | (5 | 5        | 205 | (5 | .58  | (1       | 21   | 65       | 38  | 5.74     | .21 | 82 | 1.16 | 1100 | 2  | .02      | 26 | 673  | 26 | (5 | (20 | 36  | .10 | (10 | 83 | (10 | 11 | 80 |
| 563 -127 | L9+800N 10+ 700 | E       | (5       | 1.2 | 4.38 | (5 | 4        | 354 | 6  | .86  | (1       | 24   | 66       | 41  | 5.23     | .20 | 86 | 1.28 | 1652 | 3  | .03      | 29 | 957  | 22 | (5 | (20 | 55  | .14 | (10 | 84 | (10 | 6  | 73 |
| 563 -128 | L9+800N 10+ 750 | E       | (5       | .4  | 3.31 | (5 | 3        | 213 | (5 | 1.34 | (1       | 18   | 36       | 39  | 4.07     | .20 | 77 | .93  | 1141 | 2  | .01      | 18 | 631  | 25 | (5 | (20 | 78  | .08 | (10 | 58 | (10 | 4  | 51 |
| 563 -129 | L9+800N 10+ 800 | E       | (5       | 1.2 | 2.93 | (5 | 3        | 117 | (5 | 1.01 | (1       | 12   | 34       | 23  | 3.34     | .16 | 57 | .66  | 404  | 2  | .03      | 16 | 341  | 13 | (5 | (20 | 65  | .15 | (10 | 62 | (10 | 8  | 36 |
| 563 -130 | L9+800N 10+ 850 | E       | (5       | 1.2 | 2.71 | (5 | 3        | 108 | 7  | .69  | (1       | 12   | 37       | 18  | 3.31     | .17 | 44 | .52  | 335  | 1  | .04      | 13 | 467  | 10 | (5 | (20 | 68  | .24 | (10 | 69 | (10 | 7  | 33 |
| 563 -131 | L9+800N 10+ 900 | E       | (5       | .3  | 3.67 | (5 | 5        | 85  | (5 | .81  | (1       | 12   | 46       | 15  | 3.82     | .18 | 47 | .77  | 465  | (1 | .04      | 24 | 1239 | 15 | (5 | (20 | 61  | .20 | (10 | 65 | (10 | 1  | 47 |
| 563 -132 | L9+800N 10+ 950 | E       | (5       | .7  | 5.62 | (5 | 2        | 130 | (5 | 1.54 | (1       | 15   | 41       | 43  | 4.31     | .14 | 86 | 1.23 | 639  | 1  | .03      | 33 | 671  | 19 | (5 | (20 | 55  | .22 | (10 | 57 | (10 | 7  | 32 |
| 563 -133 | L9+800N 11+ 000 | E       | (5       | 1.2 | 3.33 | (5 | 4        | 71  | (5 | .39  | (1       | 11   | 36       | 11  | 2.99     | .09 | 37 | .60  | 346  | (1 | .03      | 19 | 613  | 16 | (5 | (20 | 46  | .21 | (10 | 55 | (10 | 4  | 55 |
| 563 -134 | L9+800N 11+ 50  | E       | (5       | 1.2 | 3.58 | (5 | 1        | 80  | (5 | .49  | (1       | 11   | 43       | 14  | 3.23     | .08 | 40 | .73  | 385  | 1  | .04      | 22 | 361  | 17 | (5 | (20 | 56  | .22 | (10 | 56 | (10 | 3  | 51 |
| 563 -135 | L9+800N 11+ 100 | E       | (5       | 1.2 | 3.48 | (5 | 5        | 90  | (5 | .64  | (1       | 13   | 53       | 16  | 4.27     | .10 | 52 | .81  | 327  | 2  | .04      | 22 | 550  | 15 | (5 | (20 | 51  | .20 | (10 | 53 | (10 | 4  | 46 |
| 563 -136 | L9+800N 11+ 150 | E       | (5       | .3  | 2.96 | (5 | 2        | 40  | (5 | .45  | (1       | 10   | 39       | 11  | 2.92     | .03 | 34 | .59  | 341  | 1  | .04      | 19 | 344  | 13 | (5 | (20 | 55  | .25 | (10 | 56 | (10 | 5  | 45 |

## ECO-TECH LABORATORIES LTD.

## RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-563

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| ET#     | DESCRIPTION     | AU(ppb) | Ag AL(%) | As | B    | BA | Bi Ca(%) | Co  | Cd  | CR   | CU Fe(\$) | K(%) | LA Mo(\$) | Mn  | Mo Na(%) | Ni  | P  | PB   | Pb   | Sn | SP Fe(%) | V  | W    | X  | Y   | Zn  |      |     |     |      |     |    |      |
|---------|-----------------|---------|----------|----|------|----|----------|-----|-----|------|-----------|------|-----------|-----|----------|-----|----|------|------|----|----------|----|------|----|-----|-----|------|-----|-----|------|-----|----|------|
| 563-137 | L9+800N 11+ 200 | E       | 30       | .2 | 3.45 | .5 | 4        | 99  | .5  | .56  | 1         | 13   | 52        | 16  | 4.17     | .11 | 50 | .80  | 325  | 2  | .03      | 22 | 461  | 16 | .15 | .20 | .70  | .28 | .10 | .69  | .10 | .2 | .69  |
| 563-138 | L9+800N 11+ 250 | E       | 15       | .2 | 4.57 | .5 | 3        | 137 | .5  | .60  | 1         | 16   | 74        | 20  | 4.97     | .17 | 61 | 1.26 | 531  | 2  | .03      | 26 | 584  | 17 | .15 | .20 | .62  | .21 | .10 | .86  | .10 | .1 | .55  |
| 563-139 | L9+800N 11+ 300 | E       | 15       | .2 | 7.00 | .5 | 6        | 114 | .5  | .60  | 1         | 21   | 73        | 21  | 4.86     | .14 | 61 | 1.09 | 452  | 2  | .03      | 32 | 647  | 20 | .15 | .20 | .65  | .31 | .10 | .89  | .10 | .3 | .60  |
| 563-140 | L9+800N 11+ 350 | E       | 5        | .2 | 6.88 | .5 | 3        | 110 | .8  | .40  | 1         | 13   | 54        | 22  | 2.88     | .09 | 37 | .77  | 144  | 1  | .03      | 27 | 687  | 22 | .15 | .20 | .44  | .23 | .10 | .36  | .10 | .4 | .32  |
| 563-141 | L9+800N 11+ 400 | E       | 15       | .2 | 7.22 | .5 | 6        | 119 | .5  | .55  | 1         | 17   | 68        | 20  | 4.55     | .19 | 57 | 1.08 | 1093 | 2  | .02      | 30 | 1066 | 20 | .15 | .20 | .62  | .28 | .10 | .71  | .10 | .1 | .66  |
| 563-142 | L9+800N 11+ 450 | E       | 15       | .2 | 5.65 | .5 | 4        | 102 | .5  | .65  | 1         | 15   | 59        | 18  | 3.87     | .14 | 49 | .96  | 1044 | 2  | .02      | 24 | 893  | 18 | .15 | .20 | .56  | .25 | .10 | .65  | .10 | .1 | .62  |
| 563-143 | L9+800N 11+ 500 | E       | 15       | .2 | 3.76 | .5 | 5        | 71  | .10 | .50  | 1         | 12   | 44        | 13  | 3.19     | .11 | 39 | .73  | 509  | 1  | .03      | 18 | 461  | 14 | .15 | .20 | .51  | .22 | .10 | .58  | .10 | .3 | .49  |
| 563-144 | L9+800N 11+ 550 | E       | 5        | .2 | 5.01 | .5 | 5        | 80  | .7  | .75  | 1         | 13   | 42        | 13  | 3.19     | .19 | 40 | 1.07 | 580  | 1  | .03      | 15 | 1116 | 14 | .15 | .20 | .54  | .24 | .10 | .52  | .10 | .4 | .63  |
| 563-145 | L9+900N 10+ 00  | E       | 5        | .7 | 3.65 | .5 | 2        | 150 | .5  | 1.75 | 2         | 16   | 49        | 59  | 3.83     | .14 | 61 | .97  | 1697 | 3  | .03      | 27 | 996  | 36 | .5  | .20 | .113 | .12 | .10 | .71  | .10 | .7 | .32  |
| 563-146 | L9+900N 10+ 50  | E       | 15       | .2 | 3.27 | .5 | 5        | 157 | .5  | .66  | 1         | 17   | 51        | 56  | 4.31     | .27 | 58 | .30  | 291  | 1  | .04      | 22 | 537  | 19 | .15 | .20 | .45  | .29 | .10 | .55  | .10 | .1 | .99  |
| 563-147 | L9+900N 10+ 100 | E       | 5        | .2 | 3.07 | .5 | 5        | 137 | .5  | .57  | 1         | 15   | 49        | 20  | 4.15     | .26 | 54 | .70  | 643  | 2  | .03      | 27 | 318  | 24 | .15 | .20 | .54  | .23 | .10 | .72  | .10 | .3 | .37  |
| 563-148 | L9+900N 10+ 150 | E       | 20       | .2 | 3.94 | .5 | 4        | 121 | .5  | .76  | 1         | 18   | 52        | 40  | 4.94     | .23 | 68 | 1.16 | 733  | 2  | .03      | 27 | 987  | 39 | .5  | .20 | .18  | .76 | .10 | .82  | .10 | .1 | .79  |
| 563-149 | L9+900N 10+ 200 | E       | 5        | .2 | 3.73 | .5 | 4        | 113 | .5  | .84  | 1         | 19   | 52        | 62  | 4.46     | .25 | 62 | 1.07 | 827  | 3  | .03      | 26 | 634  | 31 | .5  | .20 | .28  | .26 | .10 | .81  | .10 | .3 | .81  |
| 563-150 | L9+900N 10+ 250 | E       | 15       | .2 | 3.58 | .5 | 3        | 102 | .5  | .65  | 1         | 17   | 53        | 53  | 4.63     | .23 | 61 | 1.15 | 618  | 4  | .03      | 25 | 487  | 15 | .15 | .20 | .129 | .15 | .10 | .83  | .10 | .4 | .52  |
| 563-151 | L9+900N 10+ 300 | E       | 15       | .2 | 4.47 | .5 | 2        | 107 | .5  | 1.11 | 1         | 21   | 52        | 235 | 5.89     | .23 | 85 | 1.57 | 482  | 4  | .04      | 28 | 1037 | 11 | .15 | .20 | .248 | .12 | .10 | .113 | .10 | .4 | .43  |
| 563-152 | L9+900N 10+ 350 | E       | 25       | .2 | 2.82 | .5 | 3        | 108 | .7  | .68  | 1         | 15   | 49        | 26  | 3.81     | .21 | 50 | .86  | 706  | 2  | .04      | 22 | 914  | 13 | .5  | .20 | .27  | .16 | .10 | .71  | .10 | .1 | .49  |
| 563-153 | L9+900N 10+ 400 | E       | 5        | .2 | 3.62 | .5 | 5        | 124 | .5  | .89  | 1         | 16   | 49        | 27  | 4.12     | .28 | 57 | 1.06 | 898  | 2  | .02      | 28 | 852  | 19 | .15 | .20 | .19  | .17 | .10 | .83  | .10 | .3 | .73  |
| 563-154 | L9+900N 10+ 450 | E       | 15       | .2 | 4.13 | .5 | 4        | 83  | .5  | .77  | 1         | 12   | 54        | 50  | 4.68     | .21 | 62 | 1.10 | 700  | 3  | .03      | 30 | 483  | 18 | .5  | .20 | .27  | .17 | .10 | .85  | .10 | .4 | .103 |
| 563-155 | L9+900N 10+ 500 | E       | 5        | .2 | 5.68 | .5 | 2        | 145 | .5  | .58  | 1         | 19   | 54        | 36  | 4.54     | .15 | 47 | 1.15 | 1139 | 2  | .02      | 32 | 578  | 16 | .5  | .20 | .36  | .18 | .10 | .71  | .10 | .3 | .73  |
| 563-156 | L9+900N 10+ 550 | E       | 30       | .5 | 2.38 | .5 | 3        | 194 | .5  | .59  | 1         | 12   | 47        | 15  | 2.34     | .10 | 43 | .92  | 500  | 41 | .02      | 17 | 391  | 16 | .15 | .20 | .37  | .07 | .10 | .71  | .10 | .4 | .35  |
| 563-157 | L9+900N 10+ 600 | E       | 5        | .2 | 5.19 | .5 | 2        | 231 | .5  | .63  | 0         | 16   | 59        | 27  | 4.73     | .18 | 42 | 1.19 | 1054 | 2  | .01      | 27 | 1168 | 24 | .5  | .20 | .34  | .12 | .10 | .74  | .10 | .4 | .78  |
| 563-158 | L9+900N 10+ 450 | E       | 5        | .2 | 4.64 | .5 | 3        | 162 | .5  | .60  | 1         | 19   | 61        | 9   | 4.89     | .11 | 43 | 1.98 | 899  | 2  | .01      | 24 | 407  | 14 | .5  | .20 | .27  | .14 | .10 | .75  | .10 | .3 | .76  |
| 563-159 | L9+900N 10+ 700 | E       | 5        | .3 | 5.01 | .5 | 6        | 216 | .5  | .72  | 1         | 17   | 55        | 21  | 4.43     | .24 | 51 | 1.08 | 1303 | 2  | .02      | 27 | 1179 | 17 | .5  | .20 | .46  | .15 | .10 | .71  | .10 | .4 | .65  |
| 563-160 | L9+900N 10+ 750 | E       | 5        | .2 | 4.70 | .5 | 4        | 264 | .5  | .79  | 1         | 18   | 57        | 26  | 4.69     | .23 | 46 | 1.09 | 1393 | 2  | .03      | 21 | 1146 | 16 | .5  | .20 | .53  | .16 | .10 | .70  | .10 | .4 | .65  |
| 563-161 | L9+900N 10+ 750 | EI      | 15       | .2 | 5.06 | .5 | 3        | 228 | .5  | .74  | 1         | 19   | 62        | 29  | 4.21     | .21 | 74 | 1.25 | 977  | 2  | .03      | 30 | 663  | 12 | .5  | .20 | .51  | .15 | .10 | .71  | .10 | .4 | .58  |
| 563-162 | L9+900N 10+ 800 | E       | 15       | .2 | 4.37 | .5 | 4        | 173 | .5  | .77  | 1         | 14   | 46        | 21  | 3.88     | .15 | 58 | .83  | 564  | 11 | .04      | 29 | 714  | 14 | .15 | .20 | .24  | .15 | .10 | .73  | .10 | .4 | .53  |
| 563-163 | L9+900N 10+ 850 | E       | 5        | .2 | 5.29 | .5 | 3        | 97  | 1   | 113  | 1         | 11   | 39        | 16  | 3.29     | .14 | 49 | .64  | 567  | 1  | .01      | 15 | 364  | 14 | .5  | .20 | .26  | .18 | .10 | .73  | .10 | .4 | .59  |
| 563-164 | L9+900N 10+ 900 | E       | 5        | .2 | 3.10 | .5 | 5        | 79  | .5  | .55  | 1         | 11   | 41        | 14  | 3.25     | .11 | 43 | .55  | 849  | 1  | .03      | 16 | 886  | 12 | .5  | .20 | .51  | .22 | .10 | .73  | .10 | .4 | .58  |
| 563-165 | L9+900N 10+ 950 | E       | 5        | .2 | 3.27 | .5 | 6        | 77  | .5  | .70  | 1         | 11   | 41        | 15  | 3.25     | .15 | 43 | .59  | 389  | 1  | .03      | 19 | 701  | 11 | .5  | .20 | .61  | .22 | .10 | .73  | .10 | .4 | .40  |
| 563-166 | L9+900N 11+ 000 | E       | 5        | .7 | 6.55 | .5 | 6        | 161 | .5  | 1.58 | 1         | 15   | 59        | 35  | 4.20     | .18 | 84 | 1.13 | 736  | 2  | .02      | 35 | 734  | 16 | .5  | .20 | .35  | .15 | .10 | .74  | .10 | .4 | .54  |
| 563-167 | L9+900N 11+ 50  | E       | 5        | .2 | 3.39 | .5 | 4        | 66  | .5  | .48  | 1         | 11   | 41        | 54  | 3.24     | .08 | 29 | .64  | 257  | 2  | .02      | 35 | 332  | 19 | .5  | .20 | .35  | .15 | .10 | .74  | .10 | .4 | .46  |
| 563-168 | L9+900N 11+ 100 | E       | 5        | .2 | 4.11 | .5 | 4        | 130 | .6  | .66  | 1         | 15   | 52        | 36  | 4.14     | .11 | 55 | .29  | 288  | 2  | .02      | 33 | 661  | 22 | .5  | .20 | .36  | .15 | .10 | .74  | .10 | .4 | .46  |
| 563-169 | L9+900N 11+ 150 | E       | 5        | .2 | 3.99 | .5 | 4        | 102 | .5  | .50  | 1         | 12   | 41        | 24  | 3.55     | .16 | 43 | .68  | 281  | 1  | .02      | 28 | 1152 | 21 | .5  | .20 | .35  | .15 | .10 | .74  | .10 | .4 | .46  |
| 563-170 | L9+900N 11+ 200 | E       | 5        | .2 | 3.73 | .5 | 5        | 94  | .4  | .57  | 1         | 10   | 39        | 25  | 3.55     | .07 | 41 | .70  | 152  | 1  | .02      | 24 | 340  | 17 | .5  | .20 | .35  | .15 | .10 | .74  | .10 | .4 | .46  |

## ECO-TECH LABORATORIES LTD.

## RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-563

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| ST#     | DESCRIPTION     | Al(ppb) | Ag Al(%) | As  | B    | BA | Bi Ca(%) | CD  | CO | CR   | CU Fe(%) | K(%) | LA Mg(%) | Mn | Mo Na(%) | Ni  | P  | PB   | SB   | SN | SR Ti(%) | U  | V    | W  | X  | Zn  |    |    |    |     |    |    |     |
|---------|-----------------|---------|----------|-----|------|----|----------|-----|----|------|----------|------|----------|----|----------|-----|----|------|------|----|----------|----|------|----|----|-----|----|----|----|-----|----|----|-----|
| 563-171 | L9+900N 11+ 250 | E       | (5       | 1.2 | 6.76 | (5 | 4        | 170 | 5  | .52  | (1       | 16   | 71       | 18 | 4.28     | .18 | 54 | 1.10 | 191  | 2  | .02      | 30 | 194  | 21 | (5 | 120 | 24 | 10 | 62 | 10  | 1  | 89 |     |
| 563-172 | L9+900N 11+ 300 | E       | (5       | 1.2 | 5.20 | (5 | 3        | 83  | 7  | .76  | (1       | 16   | 66       | 22 | 4.65     | .14 | 61 | 1.23 | 468  | 2  | .03      | 28 | 543  | 16 | (5 | 120 | 28 | 10 | 89 | 10  | 5  | 52 |     |
| 563-173 | L9+900N 11+ 350 | E       | 10       | 1.2 | 5.40 | (5 | 4        | 89  | 8  | .73  | (1       | 17   | 67       | 22 | 4.70     | .13 | 62 | 1.26 | 422  | 2  | .03      | 31 | 462  | 16 | (5 | 120 | 26 | 10 | 66 | 10  | 4  | 57 |     |
| 563-174 | L9+900N 11+ 400 | E       | (5       | 1.2 | 5.38 | (5 | 6        | 53  | 6  | .65  | (1       | 14   | 65       | 14 | 3.66     | .14 | 48 | 1.08 | 794  | 2  | .02      | 21 | 745  | 17 | (5 | 120 | 27 | 10 | 59 | 10  | 4  | 58 |     |
| 563-175 | L9+900N 11+ 450 | E       | 5        | 1.2 | 4.43 | (5 | 5        | 111 | 7  | .59  | (1       | 14   | 51       | 15 | 3.82     | .14 | 47 | .78  | 478  | 2  | .02      | 20 | 690  | 15 | (5 | 120 | 26 | 10 | 71 | 10  | 2  | 51 |     |
| 563-176 | L9+900N 11+ 500 | E       | 10       | 1.2 | 4.36 | (5 | 7        | 75  | 8  | .59  | (1       | 11   | 44       | 13 | 3.35     | .11 | 42 | .68  | 301  | (1 | .03      | 19 | 612  | 15 | (5 | 120 | 57 | 8  | 12 | 56  | 10 | 3  | 49  |
| 563-177 | L9+900N 11+ 550 | E       | (5       | 1.2 | 3.44 | (5 | 4        | 84  | 8  | .54  | (1       | 13   | 46       | 15 | 3.78     | .11 | 45 | .62  | 251  | 1  | .03      | 21 | 494  | 12 | (5 | 120 | 61 | 28 | 10 | 77  | 10 | 3  | 46  |
| 563-178 | L1000N 10 000   | E       | 5        | 1.2 | 3.34 | (5 | 7        | 137 | (5 | .69  | (1       | 17   | 49       | 22 | 4.35     | .29 | 59 | .94  | 1086 | 2  | .03      | 23 | 799  | 40 | (5 | 120 | 80 | 22 | 10 | 74  | 10 | 1  | 21  |
| 563-179 | L1000N 10 050   | E       | (5       | 1.2 | 4.73 | (5 | 4        | 165 | 5  | .66  | (1       | 20   | 63       | 34 | 5.03     | .29 | 72 | 1.20 | 1024 | 2  | .02      | 31 | 1020 | 33 | (5 | 120 | 93 | 29 | 10 | 49  | 10 | 1  | 79  |
| 563-180 | L1000N 10 100   | E       | (5       | 1.2 | 4.80 | (5 | 5        | 129 | (5 | .81  | (1       | 20   | 60       | 46 | 4.76     | .33 | 65 | 1.19 | 919  | 2  | .02      | 31 | 691  | 18 | (5 | 120 | 96 | 30 | 10 | 52  | 10 | 1  | 74  |
| 563-181 | L1000N 10 150   | E       | (5       | 1.2 | 4.89 | (5 | 5        | 129 | (5 | .81  | (1       | 20   | 60       | 46 | 4.76     | .33 | 65 | 1.19 | 919  | 2  | .02      | 31 | 691  | 18 | (5 | 120 | 96 | 30 | 10 | 52  | 10 | 1  | 74  |
| 563-182 | L1000N 10 200   | E       | (5       | 1.2 | 3.53 | (5 | 3        | 130 | (5 | .66  | (1       | 14   | 44       | 38 | 3.65     | .14 | 51 | .79  | 714  | 2  | .02      | 20 | 429  | 16 | (5 | 120 | 77 | 21 | 10 | 62  | 10 | 1  | 49  |
| 563-183 | L1000N 10 250   | E       | (5       | 1.2 | 3.78 | (5 | 5        | 124 | (5 | .66  | (1       | 15   | 48       | 24 | 3.95     | .14 | 54 | .92  | 802  | 2  | .03      | 24 | 652  | 20 | (5 | 120 | 72 | 20 | 10 | 51  | 10 | 1  | 62  |
| 563-184 | L1000N 10 300   | E       | (5       | 1.2 | 5.18 | (5 | 5        | 135 | (5 | .91  | (1       | 21   | 62       | 40 | 4.95     | .27 | 71 | 1.31 | 986  | 3  | .03      | 33 | 978  | 20 | (5 | 120 | 90 | 23 | 10 | 82  | 10 | 4  | 75  |
| 563-185 | L1000N 10 350   | E       | 10       | 1.4 | 3.32 | 10 | 78       | 145 | (5 | 1.06 | (1       | 22   | 64       | 46 | 3.37     | .16 | 10 | 1.01 | 692  | 2  | .09      | 36 | 560  | 10 | 10 | 120 | 52 | 24 | 10 | 104 | 10 | 4  | 101 |
| 563-186 | L1000N 10 400   | E       | 40       | 1.6 | 3.26 | 10 | 44       | 155 | (5 | .98  | (1       | 19   | 56       | 38 | 2.94     | .11 | 10 | .92  | 657  | 2  | .09      | 31 | 570  | 14 | (5 | 120 | 65 | 18 | 10 | 77  | 10 | 4  | 94  |
| 563-187 | L1000N 10 450   | E       | (5       | 1.6 | 3.48 | 5  | 46       | 155 | (5 | .81  | (1       | 17   | 52       | 35 | 2.88     | .08 | 10 | .86  | 427  | 2  | .08      | 34 | 760  | 10 | (5 | 120 | 55 | 21 | 10 | 87  | 10 | 2  | 92  |
| 563-188 | L1000N 10 500   | E       | (5       | 1.4 | 3.64 | 10 | 24       | 220 | (5 | .71  | (1       | 18   | 49       | 35 | 2.72     | .09 | 10 | .77  | 653  | 2  | .05      | 31 | 860  | 8  | (5 | 120 | 41 | 10 | 10 | 82  | 10 | 1  | 67  |
| 563-189 | L1000N 10 550   | E       | (5       | 1.4 | 4.12 | 5  | 36       | 140 | (5 | .66  | (1       | 17   | 93       | 31 | 3.06     | .08 | 10 | 1.10 | 799  | 2  | .06      | 37 | 1090 | 8  | 10 | 120 | 30 | 21 | 10 | 82  | 10 | 2  | 90  |
| 563-190 | L1000N 10 600   | E       | (5       | 1.4 | 3.55 | 10 | 34       | 220 | (5 | .78  | (1       | 18   | 56       | 32 | 3.16     | .11 | 10 | 1.93 | 1100 | 2  | .06      | 29 | 1650 | 6  | (5 | 120 | 34 | 11 | 10 | 75  | 10 | 2  | 103 |
| 563-191 | L1000N 10 650   | E       | (5       | 1.4 | 3.55 | 5  | 16       | 235 | (5 | .72  | (1       | 15   | 53       | 28 | 2.77     | .09 | 10 | .80  | 1046 | (1 | .06      | 30 | 1400 | 12 | 10 | 120 | 37 | 20 | 10 | 75  | 10 | 1  | 93  |
| 563-192 | L1000N 10 700   | E       | 85       | 1.4 | 3.33 | 10 | 16       | 330 | (5 | .75  | (1       | 16   | 55       | 40 | 2.96     | .11 | 10 | .96  | 686  | 2  | .07      | 29 | 960  | 10 | (5 | 120 | 45 | 16 | 10 | 80  | 10 | 3  | 77  |
| 563-193 | L1000N 10 750   | E       | (5       | 1.2 | 3.11 | 5  | 12       | 200 | (5 | .75  | (1       | 16   | 49       | 28 | 2.71     | .07 | 10 | .81  | 380  | 1  | .07      | 31 | 570  | 6  | (5 | 120 | 54 | 18 | 10 | 76  | 10 | 2  | 57  |
| 563-194 | L1000N 10 800   | E       | (5       | 1.2 | 2.37 | (5 | 8        | 165 | (5 | .65  | (1       | 11   | 34       | 18 | 2.06     | .06 | 10 | .43  | 271  | (1 | .07      | 23 | 590  | 8  | (5 | 120 | 39 | 18 | 10 | 55  | 10 | 1  | 51  |
| 563-195 | L1000N 10 850   | E       | (5       | 1.2 | 2.91 | 5  | 14       | 125 | (5 | .47  | (1       | 14   | 37       | 21 | 2.22     | .08 | 10 | .46  | 263  | (1 | .06      | 25 | 2660 | 8  | (5 | 120 | 32 | 15 | 10 | 53  | 10 | 2  | 71  |
| 563-196 | L1000N 10 900   | E       | (5       | 1.2 | 2.22 | 5  | 4        | 70  | (5 | .6   | (1       | 14   | 42       | 24 | 2.34     | .06 | 10 | .66  | 244  | 1  | .04      | 24 | 466  | 4  | (5 | 120 | 55 | 15 | 10 | 52  | 10 | 2  | 46  |
| 563-197 | L1000N 10 950   | E       | (5       | 1.4 | 1.92 | 15 | 12       | 100 | (5 | .63  | (1       | 15   | 40       | 14 | 2.39     | .07 | 10 | .59  | 222  | 1  | .06      | 21 | 110  | 12 | (5 | 120 | 34 | 14 | 10 | 51  | 10 | 1  | 56  |
| 563-198 | L1000N 11 000   | E       | (5       | 1.2 | 2.06 | 5  | 12       | 80  | (5 | .46  | (1       | 14   | 37       | 17 | 2.07     | .06 | 10 | .49  | 292  | 1  | .07      | 19 | 550  | 8  | (5 | 120 | 34 | 18 | 10 | 52  | 10 | 1  | 60  |
| 563-199 | L1000N 11 050   | E       | (5       | 1.4 | 1.94 | 5  | 12       | 85  | (5 | .38  | (1       | 12   | 34       | 14 | 1.88     | .05 | 10 | .44  | 251  | 1  | .07      | 29 | 510  | 6  | (5 | 120 | 32 | 13 | 10 | 52  | 10 | 1  | 57  |
| 563-200 | L1000N 11 100   | E       | (5       | 1.2 | 2.00 | 5  | 10       | 110 | (5 | .47  | (1       | 12   | 40       | 14 | 2.03     | .04 | 10 | .49  | 768  | 1  | .06      | 18 | 465  | 4  | (5 | 120 | 32 | 10 | 10 | 52  | 10 | 1  | 59  |
| 563-201 | L1000N 11 150   | E       | (5       | 1.4 | 3.43 | 5  | 10       | 95  | (5 | .96  | (1       | 14   | 41       | 34 | 2.24     | .07 | 10 | .82  | 725  | 1  | .07      | 21 | 689  | 4  | (5 | 120 | 34 | 14 | 10 | 52  | 10 | 1  | 57  |
| 563-202 | L1000N 11 200   | E       | (5       | 1.2 | 2.34 | 5  | 12       | 95  | (5 | .50  | 1        | 13   | 39       | 22 | 2.01     | .06 | 10 | .57  | 994  | 2  | .08      | 17 | 450  | 2  | (5 | 120 | 44 | 15 | 10 | 57  | 10 | 1  | 62  |

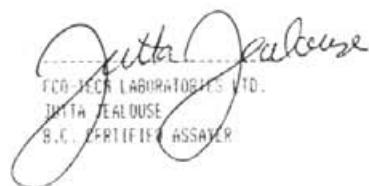
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## RELIANCE GEOLOGICAL SERVICES INC. - ETK 90-563

PAGE 7

| ET#      | DESCRIPTION   | AU(ppb) | AG AL(%)   | AS | B     | BA  | BI CA(%) | CD | CO | CP | CU FE(%) | K(%) | LA MG(%) | MN  | MO NA(%) | Ni | P    | PB | SB | SN  | SP Ti(%) | U   | V  | W   | X | Zn |
|----------|---------------|---------|------------|----|-------|-----|----------|----|----|----|----------|------|----------|-----|----------|----|------|----|----|-----|----------|-----|----|-----|---|----|
| 563 -203 | 10000N 11 250 | E       | (5 .2 4.03 | 5  | (2 95 | 5   | .60      | (1 | 17 | 55 | 30 3.05  | .08  | (10 .90  | 521 | 1 .07    | 38 | 580  | 6  | 15 | >20 | 51 .27   | 70  | 84 | >10 | 1 | 73 |
| 563 -204 | 10000N 11 300 | E       | (5 .4 4.11 | 10 | 40    | 80  | (5 .56   | (1 | 20 | 59 | 21 2.94  | .06  | (10 .97  | 295 | (1 .05   | 31 | 680  | 4  | 10 | >20 | 62 .19   | >10 | 86 | >10 | 1 | 64 |
| 563 -205 | 10000N 11 350 | E       | (5 .2 4.94 | 15 | 50    | 110 | (5 .57   | (1 | 21 | 68 | 23 3.41  | .07  | (10 .91  | 804 | 2 .07    | 38 | 680  | 5  | 10 | >20 | 77 .32   | 10  | 93 | >10 | 2 | 97 |
| 563 -206 | 10000N 11 400 | E       | (5 .2 3.17 | 10 | 34    | 65  | (5 .58   | (1 | 15 | 47 | 18 2.74  | .05  | (10 .57  | 255 | 2 .08    | 21 | 1660 | 4  | 5  | >20 | 65 .25   | 10  | 74 | >10 | 1 | 96 |
| 563 -207 | 10000N 11 450 | E       | (5 .4 4.85 | 5  | 46    | 75  | (5 .49   | (1 | 19 | 64 | 22 3.07  | .07  | (10 .98  | 779 | (1 .07   | 34 | 1530 | 3  | 10 | >20 | 58 .30   | >10 | 84 | >10 | 1 | 95 |
| 563 -208 | 10000N 11 500 | E       | (5 .2 2.74 | 5  | 28    | 70  | 5 .59    | (1 | 16 | 48 | 16 2.72  | .04  | (10 .65  | 381 | (1 .07   | 22 | 640  | 4  | 5  | >20 | 44 .28   | >10 | 82 | >10 | 1 | 57 |
| 563 -209 | 10000N 11 550 | E       | (5 .2 3.76 | 10 | 42    | 70  | 10 .82   | (1 | 17 | 55 | 18 2.56  | .06  | (10 .85  | 284 | (1 .10   | 29 | 520  | 4  | 10 | >20 | 61 .31   | >10 | 71 | >10 | 3 | 48 |

NOTE: &lt; = LESS THAN



JUDITH TEALOUSE  
ECO-TECH LABORATORIES LTD.  
JUDITH TEALOUSE  
B.C. CERTIFIED ASSAYER

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## GEOCHEMICAL ANALYSIS CERTIFICATE

Guinet Management FILE # 90-3202 Page 1  
305 - 850 W. Hastings St., Vancouver BC V6C 1E1

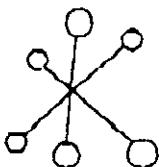
| SAMPLE #        | Cu<br>ppm | Ag<br>ppm | Au*<br>ppb |
|-----------------|-----------|-----------|------------|
| MS 1            | 86        | .5        | 10         |
| MS 2            | 85        | .3        | 5          |
| MS 3            | 64        | .2        | 12         |
| MS 4            | 56        | .2        | 6          |
| MS 5            | 55        | .3        | 23         |
| MS 6            | 42        | .2        | 44         |
| MS 7            | 38        | .1        | 15         |
| MS 8            | 231       | .3        | 9          |
| MS 9            | 309       | .5        | 420        |
| MS 10           | 5547      | 1.2       | 100        |
| MS 11           | 254       | .1        | 4          |
| MS 12           | 106       | .1        | 5          |
| MS 13           | 98        | .1        | 6          |
| MS 14           | 51        | .1        | 3          |
| MS 15           | 40        | .1        | 3          |
| MS 16           | 51        | .2        | 11         |
| MS 17           | 826       | .1        | 11         |
| MS 18           | 340       | .4        | 10         |
| MS 19           | 131       | .2        | 18         |
| MS 20           | 44        | .1        | 10         |
| MS 21           | 38        | .1        | 7          |
| MS 22           | 38        | .2        | 7          |
| MS 23           | 65        | .4        | 7          |
| MS 24           | 259       | .4        | 49         |
| MS 25           | 116       | .2        | 8          |
| MS 26           | 645       | .2        | 8          |
| MS 27           | 400       | .5        | 11         |
| MS 28           | 76        | .1        | 24         |
| MS 29           | 120       | .4        | 27         |
| MS 30           | 100       | .2        | 9          |
| MS 31           | 79        | .1        | 6          |
| MS 31 A         | 333       | .2        | 3          |
| MS 33           | 173       | .1        | 15         |
| MS 34           | 434       | .5        | 14         |
| MS 35           | 411       | .3        | 21         |
| MS 36           | 38        | .1        | 8          |
| STANDARD C/AU-S | 59        | 6.8       | 52         |

-- .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
THIS LEACH IS PARTIAL FOR Mn Fe Sr Ca P La Cr Mg Ba Ti B W AND LIMITED FOR Na K AND Al. AU DETECTION LIMIT BY ICP IS 3 PPM.  
- SAMPLE TYPE: P1-P3 Soil P4 Silt P5 Rock AU\* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.

SIGNED BY..... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

| SAMPLE#         | Cu<br>ppm | Ag<br>ppm | Au*<br>ppb |
|-----------------|-----------|-----------|------------|
| MS 37           | 87        | .1        | 8          |
| MS 38           | 73        | .1        | 4          |
| MS 39           | 97        | .2        | 5          |
| MS 40           | 89        | .5        | 1          |
| MS 41           | 393       | .5        | 6          |
| MS 42           | 310       | .8        | 2          |
| MS 43           | 344       | .6        | 3          |
| MS 44           | 97        | .4        | 10         |
| MS 45           | 177       | .1        | 2          |
| MS 46           | 30        | .3        | 16         |
| MS 47           | 49        | .2        | 3          |
| MS 48           | 39        | .3        | 17         |
| MS 49           | 104       | .1        | 3          |
| MS 50           | 53        | .3        | 5          |
| MS 51           | 74        | .3        | 5          |
| MS 52           | 61        | .1        | 16         |
| MS 53           | 769       | .7        | 6          |
| MS 54           | 919       | .2        | 2          |
| MS 55           | 151       | .7        | 16         |
| MS 56           | 185       | .4        | 7          |
| MS 57           | 189       | .4        | 3          |
| MS 58           | 309       | .5        | 6          |
| MS 59           | 44        | .2        | 5          |
| MS 60           | 38        | .3        | 2          |
| MS 61           | 35        | .1        | 20         |
| MS 62           | 27        | .5        | 131        |
| MS 63           | 32        | .1        | 7          |
| MS 64           | 27        | .3        | 1          |
| MS 65           | 31        | .3        | 12         |
| MS 66           | 43        | .5        | 8          |
| MS 67           | 42        | .2        | 8          |
| MS 68           | 49        | .2        | 9          |
| MS 69           | 43        | .3        | 77         |
| MS 70           | 14        | .3        | 1          |
| MS 71           | 38        | .3        | 15         |
| MS 72           | 31        | .2        | 14         |
| STANDARD C/AU-S | 57        | 6.8       | 48         |

| SAMPLE# | Cu<br>ppm | Ag<br>ppm | Au*<br>ppb |
|---------|-----------|-----------|------------|
| MS 73   | 41        | .3        | 13         |
| MS 74   | 2147      | .1        | 12         |



## ECO-TECH LABORATORIES LTD.

ASSAYING • ENVIRONMENTAL TESTING

10041 East Trans Canada Hwy., Kamloops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

### GEOCHEMICAL LABORATORY METHODS

#### SAMPLE PREPARATION (STANDARD)

1. Soil or Sediment: Samples are dried and then sieved through 80 mesh nylon sieves.
2. Rock, Core: Samples dried (if necessary), crushed, rifled to pulp size and pulverized to approximately -140 mesh.
3. Heavy Mineral Separation: Samples are screened to -20 mesh, washed and separated in Tetrabromothane. (SG 2.96)

#### METHODS OF ANALYSIS

All methods have either certified or in-house standards carried through entire procedure to ensure validity of results.

1. Multi-Element Cd, Cr, Co, Cu, Fe (acid soluble), Pb, Mn, Ni, Ag, Zn, Mo

##### Digestion

Hot aqua-regia

##### Finish

Atomic Absorption, background correction applied where appropriate

##### A) Multi-Element ICP

##### Digestion

Hot aqua-regia

##### Finish

ICP

##### 2. Antimony

##### Digestion

Hot aqua regia

##### Finish

Hydride generation - A.A.S.

##### 3. Arsenic

##### Digestion

Hot aqua regia

##### Finish

Hydride generation - A.A.S.

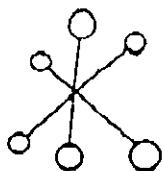
##### 4. Barium

##### Digestion

Lithium Metaborate Fusion

##### Finish

I.C.P.



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### 5. Beryllium

#### Digestion

Hot aqua regia

#### Finish

Atomic Absorption

### 6. Bismuth

#### Digestion

Hot aqua regia

#### Finish

Atomic Absorption

### 7. Chromium

#### Digestion

Sodium Peroxide Fusion

#### Finish

Atomic Absorption

### 8. Fluorine

#### Digestion

Lithium Metaborate Fusion

#### Finish

Ion Selective Electrode

### 9. Mercury

#### Digestion

Hot aqua regia

#### Finish

Cold vapor generation -  
A.A.S.

### 10. Phosphorus

#### Digestion

Lithium Metaborate Fusion

#### Finish

I.C.P. finish

### 11. Selenium

#### Digestion

Hot aqua regia

#### Finish

Hydride generation - A.A.S.

### 12. Tellurium

#### Digestion

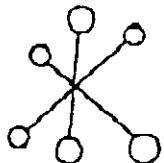
Hot aqua regia

#### Finish

Potassium Bisulphate Fusion

Hydride generation - A.A.S.

Colorimetric or I.C.P.



## ECO-TECH LABORATORIES LTD.

### ASSAYING - ENVIRONMENTAL TESTING

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#### 13. Tin

| <u>Digestion</u>       | <u>Finish</u>               |
|------------------------|-----------------------------|
| Ammonium Iodide Fusion | Hydride generation - A.A.S. |

#### 14. Tungsten

| <u>Digestion</u>            | <u>Finish</u>          |
|-----------------------------|------------------------|
| Potassium Bisulphate Fusion | Colorimetric or I.C.P. |

#### 15. Gold

- | <u>Digestion</u>  | <u>Finish</u>     |
|---|-------------------|
| a) Fire Assay Preconcentration followed by Aqua Regia   | Atomic Absorption |
| b) 10g sample is roasted at 600°C then digested with hot Aqua Regia. The gold is extracted by MIBK and determined by A.A. |                   |

#### 16. Platinum, Palladium, Rhodium

| <u>Digestion</u>                                   | <u>Finish</u>             |
|--|---------------------------|
| Fire Assay Preconcentration followed by Aqua Regia | Graphite Furnace - A.A.S. |

**APPENDIX C**  
**STATISTICAL ANALYSIS**

STATISTICAL EVALUATION  
OF SOIL SAMPLES COLLECTED FROM  
THE MINE PROPERTY  
NICOLA MINING DIVISION  
BRITISH COLUMBIA

FOR

PACIFIC SENTINEL GOLD CORP.  
1020-800 West Pender Street  
Vancouver, B.C. V6C 2V6

By

A.M.S.Clark, Ph.D., FGAC, P.Geol.(Alta.)  
RELIANCE GEOLOGICAL SERVICES INC.  
241 East First Street  
North Vancouver, B.C. V7L 1B4

4 October 1990

SUMMARY

Correlation coefficients, histograms , value maps and symbol maps have been prepared and used in the evaluation of the soil sample analyses from this property.

All assay values of economic elements are low to very low, and there are no significant correlations of elements that may assist exploration. Also, the elements that are usually of use in exploration show no spatial association on the grid with one another that could help or guide exploration.

This report is based on an evaluation of the geochemical analyses only, the author has not visited the property.

## 1. INTRODUCTION

The author of this report has not visited the sample area. This report is based on the assay results supplied by Eco-Tech Laboratories Limited, Kamloops, B.C., and discussions with the personnel who undertook the sampling. A complete interpretation of these results requires a thorough knowledge of the topography, geology and soil characteristics of the property.

The soil samples were collected from one grid (171 samples) on the property, and from road and stream traverses (29 samples). (Additional stream and rock samples collected are not included in this report).

Correlation coefficients have been determined for all the soil samples.

Histograms were plotted of gold, silver, arsenic, barium, bismuth, copper, molybdenum, lead, tungsten and zinc, to aid in determining which elements should be plotted as symbol maps, and also to help define useful groupings of the data values for the symbols on the maps.

The correlation coefficient table and histograms are attached at the end of the report.

## 2. DESCRIPTION OF STATISTICAL METHODS USED

(See Levinson, 1974, and Sinclair, 1987, for further discussion of statistical applications to soil sampling).

### 2.1 Correlation Coefficients

Correlation coefficients were calculated for all the elements analyzed. Correlations were considered to be significant for coefficient values equal to or above 0.25, with the following being the terminology used for both the positive and the negative correlations:

|               |                         |
|---------------|-------------------------|
| 0.25 to <0.30 | very weak correlation   |
| 0.30 to <0.40 | weak correlation        |
| 0.60 to <0.80 | strong correlation      |
| 0.80 to 1.00  | very strong correlation |

### 2.2 Histograms

Histograms were plotted of all elements considered of exploration significance. Where the samples show a few very high values, a second histogram has been plotted to show only the main body of samples, to allow interpretation of the type and shape of the histogram curve, and to determine ranges for plotting on the symbol maps. Ranges used for the symbols on the symbol maps were chosen to show any groupings that are indicated in the data by discordant changes in the shape of the curve at the higher values of the histogram. Where there is no obvious discordant change in the histogram, then grouping is chosen to give a visually useful distribution of symbols on the map. These groupings are usually into low and high anomalous categories. The values of the samples are not considered in this process as the pattern of distribution of the values, not the absolute values, is considered the main aid to exploration.

### 3. DISCUSSION OF CORRELATION COEFFICIENTS

The correlation coefficient table is in the appendix. Although the correlation matrix table shows the correlation coefficients of all the elements analyzed, only those elements considered of economic exploration significance are discussed below.

Gold: Gold shows no correlation with any element.

Silver: Silver has a weak correlation with boron, barium, antimony and titanium; and a very weak correlation with zinc.

Arsenic: Arsenic has a weak correlation with potassium and lead; and a very weak correlation with zinc.

Barium: Barium has a moderate correlation with manganese and titanium; a weak correlation with silver and zinc; and a very weak correlation with bismuth, potassium, sodium and yttrium.

Bismuth: Bismuth has a strong correlation with cadmium, iron and yttrium; a moderate correlation with calcium, chromium, magnesium and sodium; a weak correlation with lanthanum, phosphorous, titanium and vanadium; and a very weak correlation with barium and nickel.

Copper: Copper has a moderate correlation with molybdenum; a weak correlation with potassium; and a very weak correlation with nickel.

Molybdenum: Molybdenum shows a moderate correlation with copper and potassium.

Lead: Lead has a moderate correlation with lanthanum and zinc; and a weak correlation with aluminium and manganese.

Antimony: Antimony has a strong correlation with boron; a moderate correlation with lanthanum; a weak correlation with silver and potassium; and a very weak correlation with arsenic, iron, nickel, lead and zinc.

Tungsten: Tungsten shows no correlation with any element.

Zinc: Zinc shows a moderate correlation with cobalt, manganese, phosphorous and lead; a weak correlation with boron, barium, cadmium and nickel; and a very weak correlation with silver, aluminium and antimony.

### 4. INTERPRETATION OF HISTOGRAMS

Histograms and their associated tabular listings are appended to this evaluation.

Gold: Values form a log-normal histogram with most values below 20 ppb, but there is a slight secondary 'peak' at approximately 25 to 30 ppb and another at approximately 40 to 45 ppb which may be indicative of one or two secondary populations. These values are very low for soil samples in British Columbia. A symbol and value map was plotted (Figure 1) of gold greater than 15 ppb.

Silver: Values were all between 0 and 1 ppm. Usually anomalous silver is considered as greater than 1 ppm, so these

are very low values. Values above 0.5 ppm were plotted as symbols in Figure 3.

Arsenic: Values ranged up to 80 ppm, but the highest on the grid was 20 ppm. The histogram shows a lognormal curve with a possible weak secondary peak about 25 to 35 ppm. Arsenic was not plotted as a symbol map because of the low values.

Barium: Values ranged up to 400 ppm, with possible secondary population 'peak(s)' showing at about 200 to 240 ppm and 260 to 360 ppm. A symbol map was plotted of values above 200 ppm (Figure 3).

Bismuth: Bismuth values are low, up to 40 ppm, and show a possible secondary population 'peak' at about 15 to 30 ppm, but as the maximum value on the grid is only 15 ppm bismuth was not plotted as a symbol map.

Copper: Values ranged up to 1000 ppm. Copper greater than 100 ppm was plotted as a symbol map (Figure 2).

Molybdenum: Molybdenum shows only low values (less than 15 ppm) with a maximum of only 4 ppm on the grid, and so was not plotted as a symbol map.

Lead: Values are low (less than 100 ppm). Values greater than 30 ppm were plotted on a symbol map (Figure 3).

Tungsten: Tungsten values are all low with only one sample being greater than 1 ppm (it was 20 ppm). No symbol map was plotted.

Zinc: Values produce a slightly irregular log-normal curve up to about 110 ppm, with additional samples up to 250 ppm. These values are low, but values above 90 ppm were plotted on a symbol map (Figure 3).

## 5. DISCUSSION

A full interpretation of the distribution of values requires a knowledge of the geology, soil characteristics and topography of the property. All elements of exploration significance show only low to very low values. None of the elements plotted show any spatial relationship to one another, though the higher barium values tend to be clustered in the central part of the grid.

REFERENCES

Levinson, A.A., 1974. Introduction to Exploration Geochemistry. Applied Publishing Limited, Calgary. 612p. and 1980 Supplement.

A.J.Sinclair, 1987. Statistical Interpretation of Soil Geochemical Data. In: Reviews in Economic geology, Volume 3, Fletcher, W.K., Hoffman, S.J., Mehrtens, M.B., Sinclair, A.,J., and Thomson, I, Exploration Geochemistry: Design and Interpretation of Soil Surveys. Edited by: Robertson, J.M. Society of Economic Geologists.

CERTIFICATE

I, ANTHONY M.S. CLARK, of 2988 Fleet Street, Coquitlam, B.C., do hereby state that:

1. I am a graduate of the University of Cape Town, Cape Town, South Africa, with a Bachelor of Science Degree in Geology, 1963, and of Memorial University, St. John's, Newfoundland, with a Doctor of Philosophy Degree in Geology, 1974.
2. I am a Fellow in good standing with the Geological Association of Canada, and registered as a Professional Geologist with the Association of Professional Engineers, Geologists and Geophysicists of Alberta.
3. I actively pursued my career as an exploration geologist for twenty-three years from 1963 to 1986, since when I have undertaken consulting in the fields of mineral exploration and computer applications to exploration.
4. The information, opinions, and recommendations in this report are based on information obtained by other personnel who undertook the fieldwork on the property, and on published and unpublished literature. I have not visited the subject property.
5. I have no interest, direct or indirect, in the subject claims or the securities of Pacific Sentinel Gold Corp.
6. I consent to the use of this report in Prospectus or Statement of Material Facts for the purpose of private or public financing.

RELIANCE GEOLOGICAL SERVICES INC.

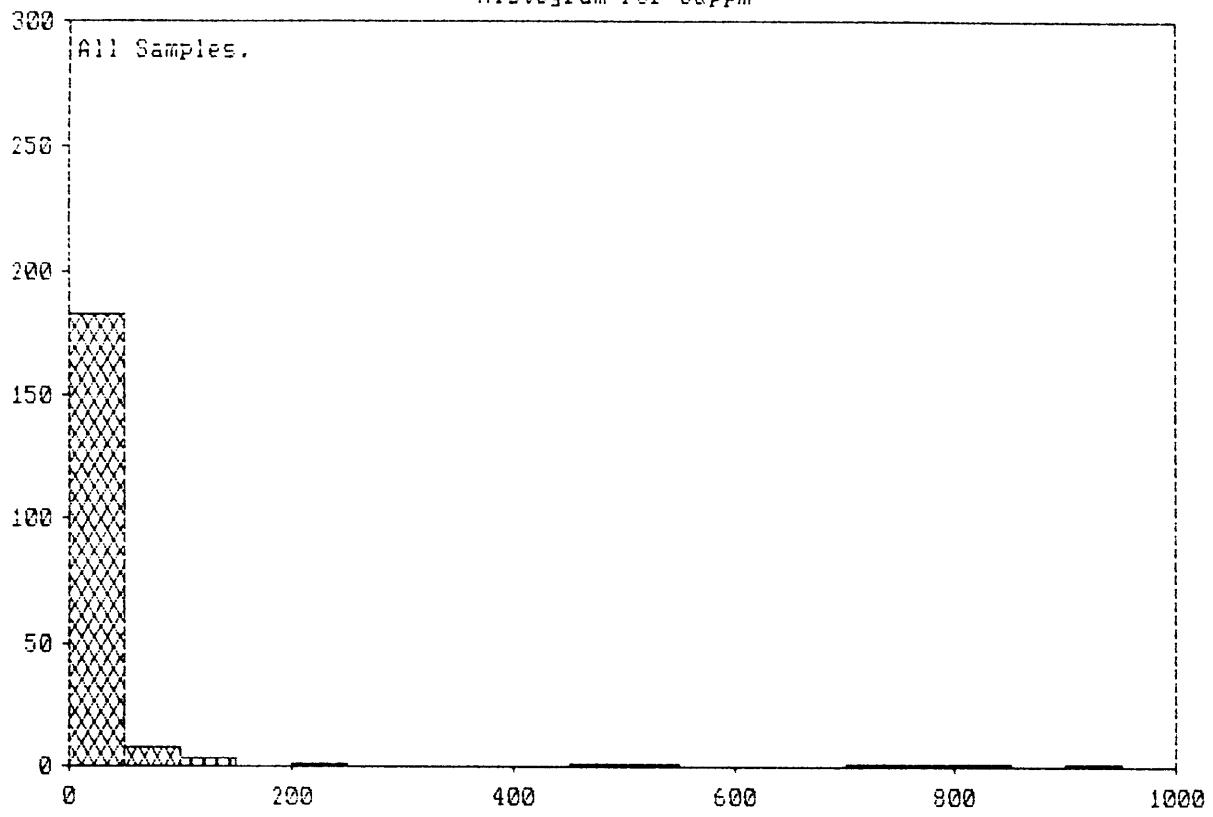
Anthony M.S. Clark, PhD., F.G.A.C., P.Geol (Alta)

Dated at North Vancouver, B.C., this        day of  
1990.

Mime Property. Soil Sample Correlation Coefficients: all samples

|       | aappb | agppm | alpct | asppm | .bppm | bappm | bippm | capct | cdppm | coppm | crppm | cuppm | feptc | .kpct | lappm | mpct | mppm | mppm | naptc | nippm | pppm | pbppm | sbppm | snppm | srppm | tipct | .uppm | .vppm | .vppm | .yppm | znppm |      |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|------|------|-------|-------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|------|
| aappb | 1.00  | 0.11  | 0.05  | 0.02  | 0.02  | 0.03  | 0.02  | 0.01  | 0.20  | 0.02  | 0.02  | 0.10  | 0.01  | 0.07  | 0.08  | 0.00 | 0.03 | 0.01 | 0.01  | 0.01  | 0.05 | 0.02  | 0.00  | 0.20  | 0.05  | 0.01  | 0.05  | 0.01  | 0.01  | 0.06  |       |      |
| agppm | 0.11  | 1.00  | 0.02  | 0.05  | 0.30  | 0.37  | 0.24  | 0.09  | 0.10  | 0.21  | 0.11  | 0.01  | 0.08  | 0.03  | 0.04  | 0.07 | 0.19 | 0.06 | 0.07  | 0.16  | 0.10 | 0.06  | 0.37  | 0.00  | 0.03  | 0.31  | 0.02  | 0.05  | 0.03  | 0.07  | 0.26  |      |
| alpct | 0.05  | 0.02  | 1.00  | 0.18  | 0.12  | 0.10  | 0.00  | 0.13  | 0.10  | 0.41  | 0.28  | 0.23  | 0.22  | 0.03  | 0.40  | 0.18 | 0.28 | 0.08 | 0.27  | 0.42  | 0.11 | 0.38  | 0.00  | 0.00  | 0.04  | 0.17  | 0.09  | 0.01  | 0.06  | 0.12  | 0.29  |      |
| asppm | 0.02  | 0.05  | 0.18  | 1.00  | 0.21  | 0.01  | 0.13  | 0.07  | 0.08  | 0.11  | 0.13  | 0.03  | 0.22  | 0.35  | 0.18  | 0.02 | 0.08 | 0.16 | 0.02  | 0.12  | 0.01 | 0.11  | 0.27  | 0.00  | 0.06  | 0.01  | 0.04  | 0.16  | 0.02  | 0.08  | 0.03  |      |
| .bppm | 0.02  | 0.30  | 0.12  | 0.21  | 0.00  | 0.07  | 0.09  | 0.09  | 0.10  | 0.22  | 0.07  | 0.02  | 0.19  | 0.17  | 0.40  | 0.09 | 0.02 | 0.06 | 0.15  | 0.28  | 0.08 | 0.20  | 0.79  | 0.00  | 0.12  | 0.11  | 0.03  | 0.16  | 0.02  | 0.11  | 0.31  |      |
| bappm | 0.03  | 0.37  | 0.10  | 0.01  | 0.07  | 1.00  | 0.28  | 0.04  | 0.19  | 0.19  | 0.08  | 0.01  | 0.08  | 0.26  | 0.23  | 0.07 | 0.49 | 0.09 | 0.29  | 0.01  | 0.20 | 0.18  | 0.07  | 0.00  | 0.19  | 0.45  | 0.08  | 0.14  | 0.05  | 0.28  | 0.30  |      |
| bippm | 0.03  | 0.24  | 0.06  | 0.13  | 0.09  | 0.28  | 1.00  | 0.44  | 0.77  | 0.15  | 0.57  | 0.11  | 0.66  | 0.02  | 0.36  | 0.56 | 0.02 | 0.03 | 0.40  | 0.29  | 0.30 | 0.06  | 0.11  | 0.00  | 0.19  | 0.34  | 0.03  | 0.64  | 0.03  |       |       |      |
| capct | 0.02  | 0.09  | 0.13  | 0.07  | 0.09  | 0.04  | 0.44  | 1.00  | 0.44  | 0.20  | 0.34  | 0.07  | 0.43  | 0.09  | 0.10  | 0.57 | 0.20 | 0.16 | 0.29  | 0.35  | 0.22 | 0.24  | 0.09  | 0.00  | 0.52  | 0.03  | 0.06  | 0.27  | 0.03  | 0.60  | 0.11  |      |
| cdppm | 0.01  | 0.10  | 0.16  | 0.08  | 0.16  | 0.19  | 0.77  | 0.44  | 1.00  | 0.20  | 0.60  | 0.04  | 0.66  | 0.06  | 0.36  | 0.65 | 0.19 | 0.17 | 0.34  | 0.37  | 0.38 | 0.08  | 0.09  | 0.00  | 0.15  | 0.08  | 0.04  | 0.30  | 0.02  | 0.61  | 0.32  |      |
| coppm | 0.20  | 0.21  | 0.41  | 0.11  | 0.22  | 0.19  | 0.15  | 0.20  | 0.20  | 1.00  | 0.39  | 0.11  | 0.56  | 0.22  | 0.26  | 0.56 | 0.48 | 0.03 | 0.16  | 0.67  | 0.44 | 0.24  | 0.15  | 0.00  | 0.19  | 0.14  | 0.10  | 0.58  | 0.07  | 0.15  | 0.51  |      |
| ctppm | 0.02  | 0.11  | 0.28  | 0.13  | 0.07  | 0.08  | 0.57  | 0.34  | 0.60  | 0.39  | 1.00  | 0.13  | 0.63  | 0.12  | 0.16  | 0.73 | 0.26 | 0.16 | 0.35  | 0.57  | 0.27 | 0.02  | 0.00  | 0.00  | 0.07  | 0.12  | 0.13  | 0.49  | 0.08  | 0.44  | 0.17  |      |
| cuppm | 0.02  | 0.01  | 0.23  | 0.03  | 0.02  | 0.01  | 0.11  | 0.07  | 0.04  | 0.11  | 0.13  | 1.00  | 0.03  | 0.34  | 0.17  | 0.09 | 0.11 | 0.59 | 0.08  | 0.26  | 0.06 | 0.19  | 0.06  | 0.00  | 0.05  | 0.18  | 0.04  | 0.16  | 0.02  | 0.03  | 0.09  |      |
| feptc | 0.10  | 0.08  | 0.22  | 0.22  | 0.19  | 0.08  | 0.66  | 0.43  | 0.66  | 0.56  | 0.63  | 0.03  | 1.00  | 0.31  | 0.11  | 0.83 | 0.33 | 0.17 | 0.31  | 0.43  | 0.42 | 0.19  | 0.29  | 0.00  | 0.27  | 0.25  | 0.07  | 0.65  | 0.09  | 0.57  | 0.23  |      |
| .kpct | 0.01  | 0.03  | 0.03  | 0.35  | 0.17  | 0.26  | 0.02  | 0.09  | 0.06  | 0.22  | 0.12  | 0.34  | 0.31  | 0.00  | 0.30  | 0.23 | 0.27 | 0.54 | 0.09  | 0.02  | 0.10 | 0.17  | 0.33  | 0.00  | 0.13  | 0.18  | 0.04  | 0.12  | 0.09  | 0.03  | 0.15  |      |
| lappm | 0.07  | 0.04  | 0.40  | 0.18  | 0.40  | 0.23  | 0.36  | 0.10  | 0.36  | 0.26  | 0.16  | 0.17  | 0.11  | 0.30  | 1.00  | 0.05 | 0.29 | 0.03 | 0.52  | 0.03  | 0.16 | 0.52  | 0.53  | 0.00  | 0.05  | 0.16  | 0.01  | 0.07  | 0.12  | 0.26  | 0.02  |      |
| mpct  | 0.08  | 0.07  | 0.18  | 0.02  | 0.09  | 0.07  | 0.58  | 0.57  | 0.65  | 0.56  | 0.73  | 0.09  | 0.83  | 0.23  | 0.05  | 1.00 | 0.33 | 0.14 | 0.39  | 0.60  | 0.39 | 0.10  | 0.16  | 0.00  | 0.36  | 0.08  | 0.14  | 0.66  | 0.09  | 0.59  | 0.20  |      |
| mppm  | 0.00  | 0.19  | 0.28  | 0.08  | 0.02  | 0.49  | 0.02  | 0.20  | 0.19  | 0.48  | 0.26  | 0.11  | 0.33  | 0.27  | 0.29  | 0.33 | 1.00 | 0.08 | 0.17  | 0.29  | 0.43 | 0.33  | 0.08  | 0.00  | 0.04  | 0.19  | 0.05  | 0.09  | 0.08  | 0.01  | 0.48  |      |
| mppm  | 0.03  | 0.06  | 0.08  | 0.16  | 0.06  | 0.09  | 0.03  | 0.16  | 0.17  | 0.03  | 0.16  | 0.59  | 0.17  | 0.54  | 0.03  | 0.14 | 0.08 | 1.00 | 0.01  | 0.18  | 0.04 | 0.01  | 0.16  | 0.00  | 0.05  | 0.19  | 0.09  | 0.09  | 0.08  | 0.01  | 0.17  |      |
| naptc | 0.01  | 0.07  | 0.27  | 0.02  | 0.15  | 0.29  | 0.40  | 0.29  | 0.34  | 0.16  | 0.35  | 0.08  | 0.31  | 0.09  | 0.52  | 0.39 | 0.17 | 0.01 | 1.00  | 0.31  | 0.30 | 0.42  | 0.22  | 0.00  | 0.21  | 0.42  | 0.02  | 0.56  | 0.05  | 0.57  | 0.11  |      |
| nippm | 0.01  | 0.16  | 0.42  | 0.12  | 0.28  | 0.01  | 0.29  | 0.35  | 0.37  | 0.67  | 0.57  | 0.26  | 0.43  | 0.02  | 0.03  | 0.60 | 0.29 | 0.18 | 0.31  | 1.00  | 0.31 | 0.08  | 0.25  | 0.00  | 0.22  | 0.10  | 0.11  | 0.47  | 0.00  | 0.31  | 0.35  |      |
| pppm  | 0.01  | 0.10  | 0.11  | 0.01  | 0.08  | 0.20  | 0.30  | 0.22  | 0.38  | 0.44  | 0.27  | 0.06  | 0.42  | 0.10  | 0.16  | 0.39 | 0.43 | 0.04 | 0.30  | 0.31  | 0.00 | 0.06  | 0.08  | 0.00  | 0.03  | 0.11  | 0.12  | 0.23  | 0.03  | 0.28  | 0.44  |      |
| pbppm | 0.05  | 0.06  | 0.38  | 0.11  | 0.20  | 0.18  | 0.06  | 0.24  | 0.08  | 0.24  | 0.02  | 0.19  | 0.19  | 0.17  | 0.52  | 0.10 | 0.33 | 0.01 | 0.42  | 0.08  | 0.06 | 1.00  | 0.27  | 0.00  | 0.08  | 0.19  | 0.03  | 0.01  | 0.06  | 0.28  | 0.43  |      |
| sbppm | 0.02  | 0.37  | 0.00  | 0.27  | 0.79  | 0.07  | 0.11  | 0.09  | 0.09  | 0.15  | 0.00  | 0.06  | 0.29  | 0.33  | 0.53  | 0.16 | 0.08 | 0.16 | 0.22  | 0.25  | 0.08 | 0.27  | 1.00  | 0.00  | 0.17  | 0.06  | 0.05  | 0.07  | 0.13  | 0.18  | 0.25  |      |
| sappm | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00 | 0.00 | 0.00 | 0.00  | 0.00  | 0.00 | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  | 0.00  |       |      |
| srppm | 0.20  | 0.03  | 0.64  | 0.06  | 0.12  | 0.19  | 0.19  | 0.52  | 0.15  | 0.19  | 0.07  | 0.05  | 0.27  | 0.13  | 0.05  | 0.36 | 0.04 | 0.05 | 0.21  | 0.22  | 0.03 | 0.08  | 0.17  | 0.08  | 1.00  | 0.20  | 0.02  | 0.32  | 0.06  | 0.40  | 0.15  |      |
| tipct | 0.05  | 0.31  | 0.17  | 0.01  | 0.11  | 0.45  | 0.34  | 0.03  | 0.08  | 0.14  | 0.12  | 0.18  | 0.25  | 0.18  | 0.16  | 0.08 | 0.19 | 0.19 | 0.42  | 0.10  | 0.11 | 0.19  | 0.06  | 0.00  | 0.20  | 1.00  | 0.02  | 0.41  | 0.02  | 0.43  | 0.18  |      |
| .appm | 0.01  | 0.02  | 0.09  | 0.04  | 0.03  | 0.08  | 0.03  | 0.06  | 0.04  | 0.10  | 0.13  | 0.04  | 0.07  | 0.04  | 0.01  | 0.14 | 0.05 | 0.09 | 0.02  | 0.11  | 0.12 | 0.03  | 0.05  | 0.00  | 0.02  | 0.02  | 0.00  | 0.09  | 0.01  | 0.05  | 0.02  |      |
| .vppm | 0.05  | 0.05  | 0.01  | 0.16  | 0.16  | 0.14  | 0.34  | 0.27  | 0.30  | 0.58  | 0.49  | 0.10  | 0.65  | 0.12  | 0.07  | 0.66 | 0.09 | 0.09 | 0.56  | 0.47  | 0.23 | 0.01  | 0.07  | 0.00  | 0.32  | 0.41  | 0.09  | 0.08  | 0.42  | 0.09  | 0.07  | 0.09 |
| .vppm | 0.01  | 0.03  | 0.06  | 0.02  | 0.02  | 0.05  | 0.03  | 0.03  | 0.02  | 0.07  | 0.08  | 0.62  | 0.09  | 0.09  | 0.12  | 0.09 | 0.08 | 0.08 | 0.05  | 0.00  | 0.03 | 0.06  | 0.13  | 0.00  | 0.06  | 0.02  | 0.01  | 0.08  | 0.00  | 0.04  | 0.02  |      |
| .yppm | 0.04  | 0.07  | 0.17  | 0.08  | 0.11  | 0.28  | 0.64  | 0.60  | 0.61  | 0.15  | 0.44  | 0.03  | 0.57  | 0.03  | 0.26  | 0.59 | 0.01 | 0.01 | 0.57  | 0.31  | 0.28 | 0.28  | 0.10  | 0.00  | 0.40  | 0.43  | 0.05  | 0.42  | 0.04  | 0.00  | 0.16  | 0.16 |
| zppm  | 0.06  | 0.26  | 0.29  | 0.03  | 0.31  | 0.30  | 0.03  | 0.11  | 0.32  | 0.51  | 0.17  | 0.09  | 0.23  | 0.15  | 0.02  | 0.20 | 0.48 | 0.17 | 0.11  | 0.35  | 0.44 | 0.43  | 0.25  | 0.00  | 0.15  | 0.18  | 0.02  | 0.09  | 0.02  | 0.16  | 0.00  | 1.00 |

Histogram for cuppm



Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

Histogram for cuppm

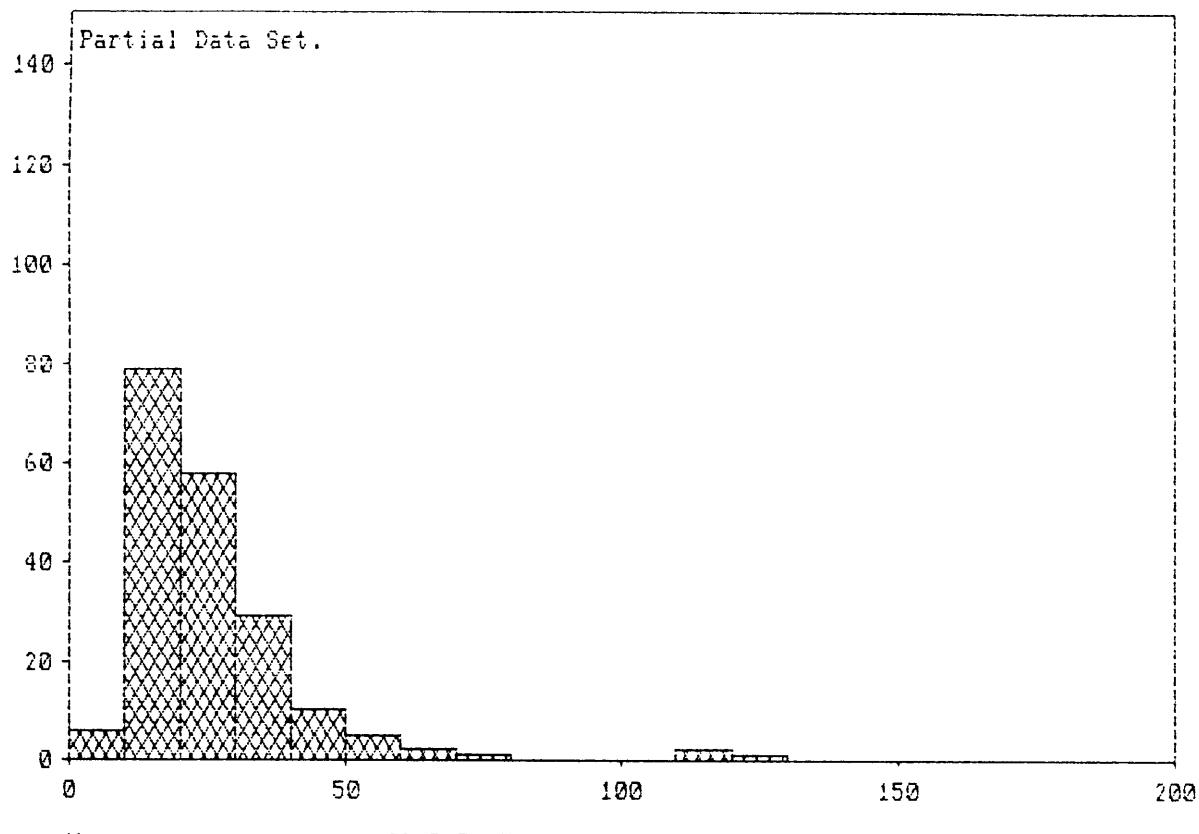
| Lower limit | Upper limit | Frequency | %  | Cumulative | %   | Mean |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 50          | 182       | 91 | 182        | 91  |      |
| 50          | 100         | 8         | 4  | 190        | 95  |      |
| 100         | 150         | 3         | 2  | 193        | 97  |      |
| 150         | 200         | 0         | 0  | 193        | 97  |      |
| 200         | 250         | 1         | 1  | 194        | 97  |      |
| 250         | 300         | 0         | 0  | 194        | 97  |      |
| 300         | 350         | 0         | 0  | 194        | 97  |      |
| 350         | 400         | 0         | 0  | 194        | 97  |      |
| 400         | 450         | 0         | 0  | 194        | 97  |      |
| 450         | 500         | 1         | 1  | 195        | 98  |      |
| 500         | 550         | 1         | 1  | 196        | 98  |      |
| 550         | 600         | 0         | 0  | 196        | 98  |      |
| 600         | 650         | 0         | 0  | 196        | 98  |      |
| 650         | 700         | 0         | 0  | 196        | 98  |      |
| 700         | 750         | 1         | 1  | 197        | 99  |      |
| 750         | 800         | 1         | 1  | 198        | 99  |      |
| 800         | 850         | 1         | 1  | 199        | 100 |      |
| 850         | 900         | 0         | 0  | 199        | 100 |      |
| 900         | 950         | 1         | 1  | 200        | 100 |      |
| 950         | 1000        | 0         | 0  | 200        | 100 |      |

Data elements inside histogram 200  
Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 46.315   |
| Variance           | 14559.57 |
| Standard Deviation | 120.6631 |
| Skewness           | 5.637034 |

Histogram for cuppm \*\*\* DATA OUTSIDE RANGE \*\*\*



ROUTINE: FRELIST FILE: ALL.NUM DATE: 10-05-1990  
Comment: Partial Data Set.

Page:

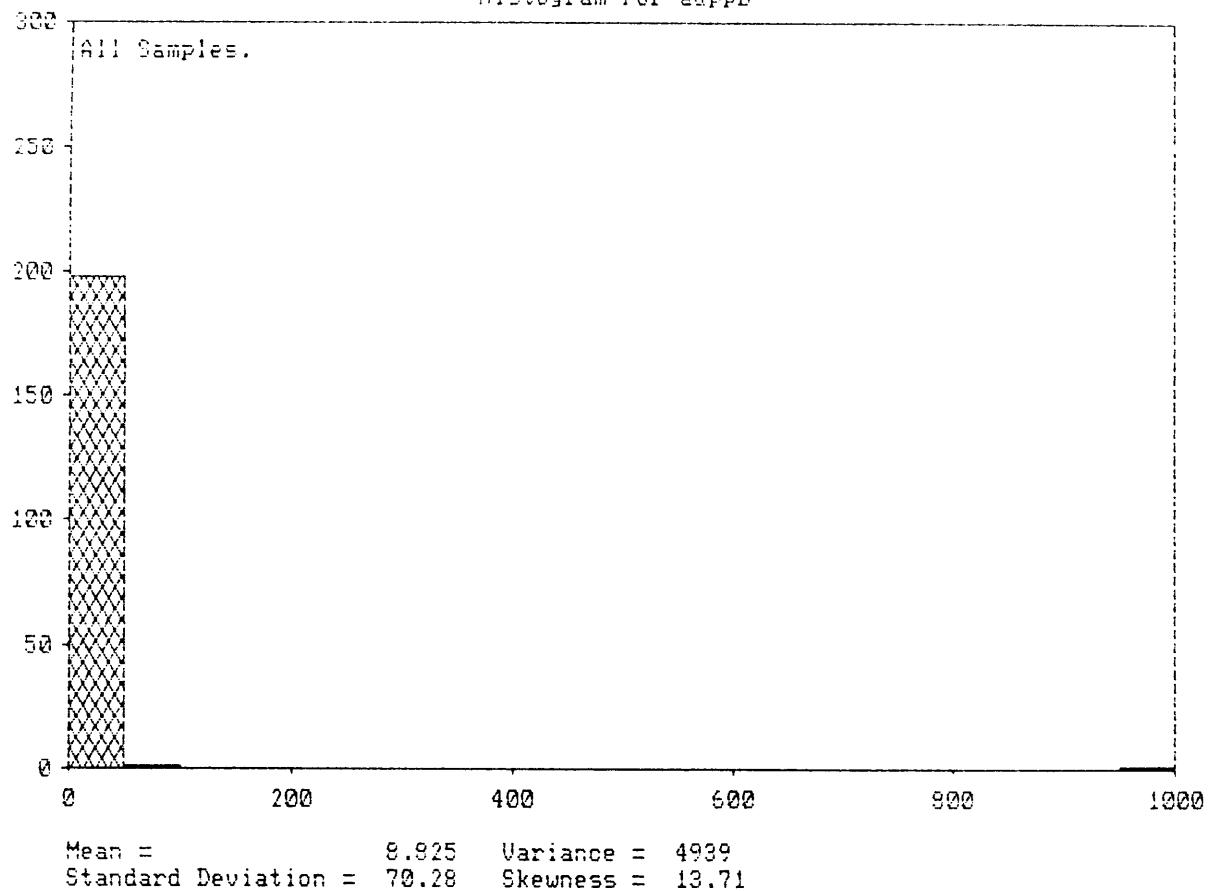
Histogram for cuppm \*\*\* DATA OUTSIDE RANGE \*\*\*

| Lower limit                     | Upper limit | Frequency | %  | Cumulative | %  |      |
|---------------------------------|-------------|-----------|----|------------|----|------|
| 0                               | 10          | 6         | 3  | 6          | 3  |      |
| 10                              | 20          | 79        | 40 | 85         | 43 |      |
| 20                              | 30          | 58        | 29 | 143        | 72 |      |
| 30                              | 40          | 29        | 15 | 172        | 86 |      |
| 40                              | 50          | 10        | 5  | 182        | 91 | Mean |
| 50                              | 60          | 5         | 3  | 187        | 94 |      |
| 60                              | 70          | 2         | 1  | 189        | 95 |      |
| 70                              | 80          | 1         | 1  | 190        | 95 |      |
| 80                              | 90          | 0         | 0  | 190        | 95 |      |
| 90                              | 100         | 0         | 0  | 190        | 95 |      |
| 100                             | 110         | 0         | 0  | 190        | 95 |      |
| 110                             | 120         | 2         | 1  | 192        | 96 |      |
| 120                             | 130         | 1         | 1  | 193        | 97 |      |
| 130                             | 140         | 0         | 0  | 193        | 97 |      |
| 140                             | 150         | 0         | 0  | 193        | 97 |      |
| 150                             | 160         | 0         | 0  | 193        | 97 |      |
| 160                             | 170         | 0         | 0  | 193        | 97 |      |
| 170                             | 180         | 0         | 0  | 193        | 97 |      |
| 180                             | 190         | 0         | 0  | 193        | 97 |      |
| 190                             | 200         | 0         | 0  | 193        | 97 |      |
| Data elements inside histogram  |             |           |    | 193        |    |      |
| Data elements outside histogram |             |           |    | 7          |    |      |

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 46.315   |
| Variance           | 14559.57 |
| Standard Deviation | 120.6631 |
| Skewness           | 5.637034 |

Histogram for *suppb*



Routine: FREMIST File: ALL.NUM Date: 10-05-1990  
Comment: All Samples.

Page:

Histogram for auppb

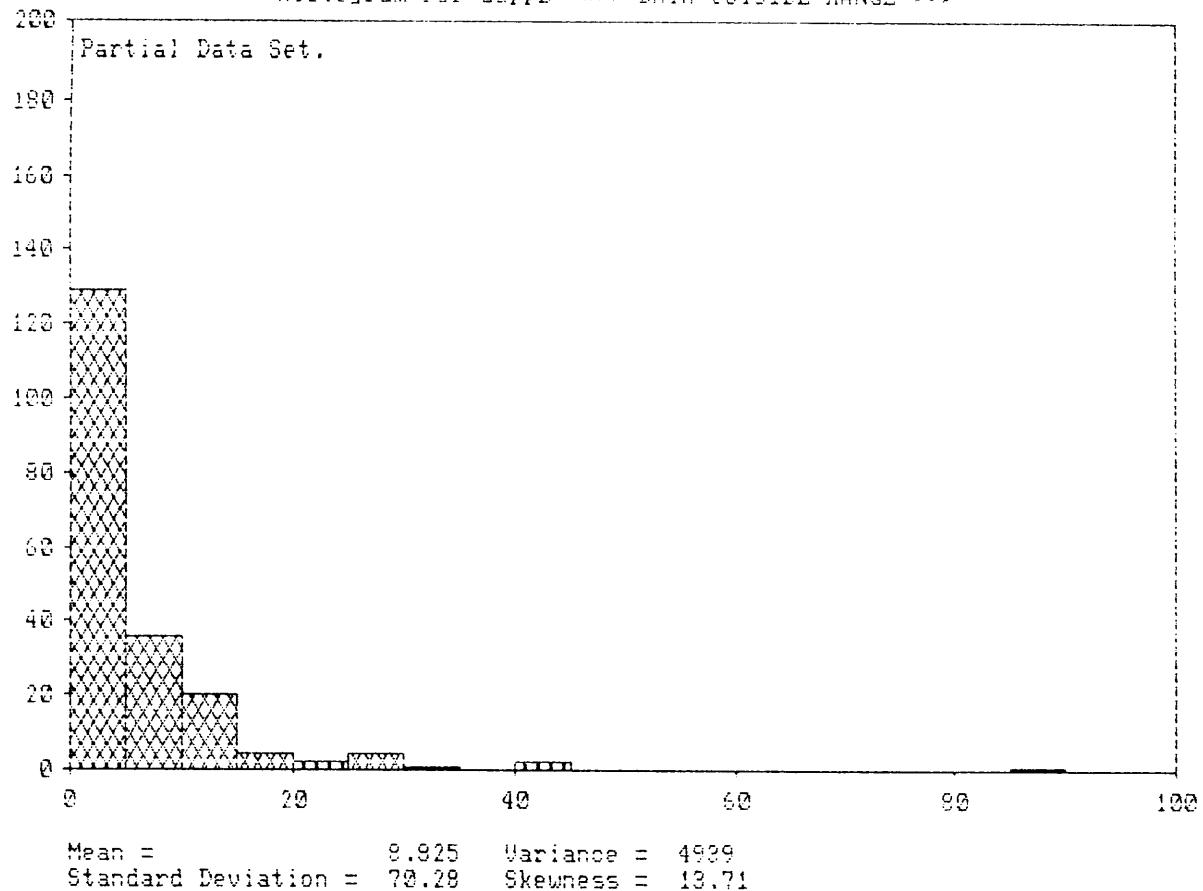
| Lower limit | Upper limit | Frequency | %  | Cumulative | %   | Mean |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 50          | 198       | 99 | 198        | 99  |      |
| 50          | 100         | 1         | 1  | 199        | 100 |      |
| 100         | 150         | 0         | 0  | 199        | 100 |      |
| 150         | 200         | 0         | 0  | 199        | 100 |      |
| 200         | 250         | 0         | 0  | 199        | 100 |      |
| 250         | 300         | 0         | 0  | 199        | 100 |      |
| 300         | 350         | 0         | 0  | 199        | 100 |      |
| 350         | 400         | 0         | 0  | 199        | 100 |      |
| 400         | 450         | 0         | 0  | 199        | 100 |      |
| 450         | 500         | 0         | 0  | 199        | 100 |      |
| 500         | 550         | 0         | 0  | 199        | 100 |      |
| 550         | 600         | 0         | 0  | 199        | 100 |      |
| 600         | 650         | 0         | 0  | 199        | 100 |      |
| 650         | 700         | 0         | 0  | 199        | 100 |      |
| 700         | 750         | 0         | 0  | 199        | 100 |      |
| 750         | 800         | 0         | 0  | 199        | 100 |      |
| 800         | 850         | 0         | 0  | 199        | 100 |      |
| 850         | 900         | 0         | 0  | 199        | 100 |      |
| 900         | 950         | 0         | 0  | 199        | 100 |      |
| 950         | 1000        | 1         | 1  | 200        | 100 |      |

Data elements inside histogram 200  
Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 8.825    |
| Variance           | 4939.44  |
| Standard Deviation | 70.28115 |
| Skewness           | 13.7139  |

Histogram for aupph \*\*\* DATA OUTSIDE RANGE \*\*\*



Routine: FRMHISI File: ALL.NUM Date: 10-05-1990  
Comment: Partial Data Set.

Page:

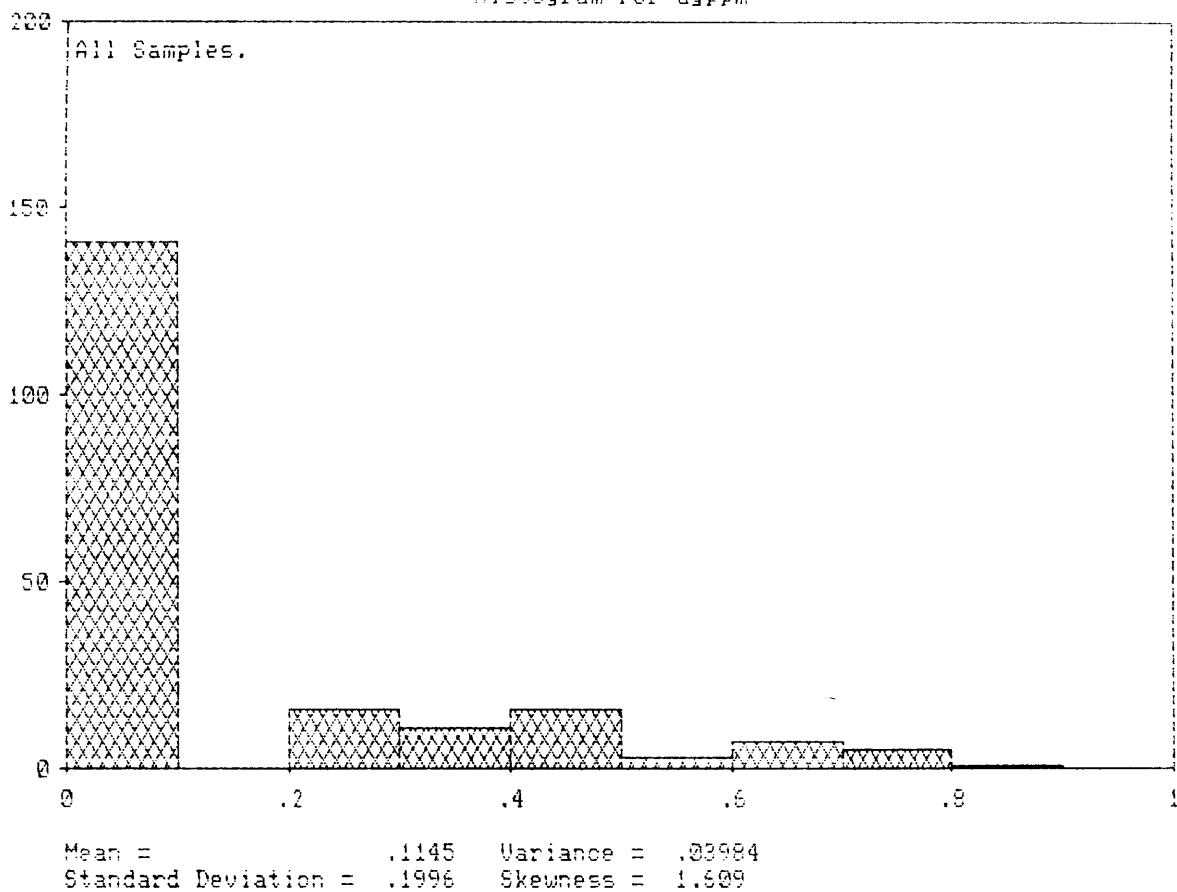
Histogram for auppb \*\*\* DATA OUTSIDE RANGE \*\*\*

| Lower limit                     | Upper limit | Frequency | %  | Cumulative | %   |      |
|---------------------------------|-------------|-----------|----|------------|-----|------|
| 0                               | 5           | 129       | 65 | 129        | 65  |      |
| 5                               | 10          | 36        | 18 | 165        | 83  | Mean |
| 10                              | 15          | 20        | 10 | 185        | 93  |      |
| 15                              | 20          | 4         | 2  | 189        | 95  |      |
| 20                              | 25          | 2         | 1  | 191        | 96  |      |
| 25                              | 30          | 4         | 2  | 195        | 98  |      |
| 30                              | 35          | 1         | 1  | 196        | 98  |      |
| 35                              | 40          | 0         | 0  | 196        | 98  |      |
| 40                              | 45          | 2         | 1  | 198        | 99  |      |
| 45                              | 50          | 0         | 0  | 198        | 99  |      |
| 50                              | 55          | 0         | 0  | 198        | 99  |      |
| 55                              | 60          | 0         | 0  | 198        | 99  |      |
| 60                              | 65          | 0         | 0  | 198        | 99  |      |
| 65                              | 70          | 0         | 0  | 198        | 99  |      |
| 70                              | 75          | 0         | 0  | 198        | 99  |      |
| 75                              | 80          | 0         | 0  | 198        | 99  |      |
| 80                              | 85          | 0         | 0  | 198        | 99  |      |
| 85                              | 90          | 1         | 1  | 199        | 100 |      |
| 90                              | 95          | 0         | 0  | 199        | 100 |      |
| 95                              | 100         | 0         | 0  | 199        | 100 |      |
| Data elements inside histogram  |             |           |    | 199        |     |      |
| Data elements outside histogram |             |           |    | 1          |     |      |

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 8.825    |
| Variance           | 4939.44  |
| Standard Deviation | 70.28115 |
| Skewness           | 13.7139  |

Histogram for agppm



Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

Histogram for agppm

| Lower limit | Upper limit | Frequency | %  | Cumulative | %   |      |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 0.1         | 141       | 71 | 141        | 71  |      |
| 0.1         | 0.2         | 0         | 0  | 141        | 71  | Mean |
| 0.2         | 0.3         | 16        | 8  | 157        | 79  |      |
| 0.3         | 0.4         | 11        | 6  | 168        | 84  |      |
| 0.4         | 0.5         | 16        | 8  | 184        | 92  |      |
| 0.5         | 0.6         | 3         | 2  | 187        | 94  |      |
| 0.6         | 0.7         | 7         | 4  | 194        | 97  |      |
| 0.7         | 0.8         | 5         | 3  | 199        | 100 |      |
| 0.8         | 0.9         | 1         | 1  | 200        | 100 |      |
| 0.9         | 1           | 0         | 0  | 200        | 100 |      |

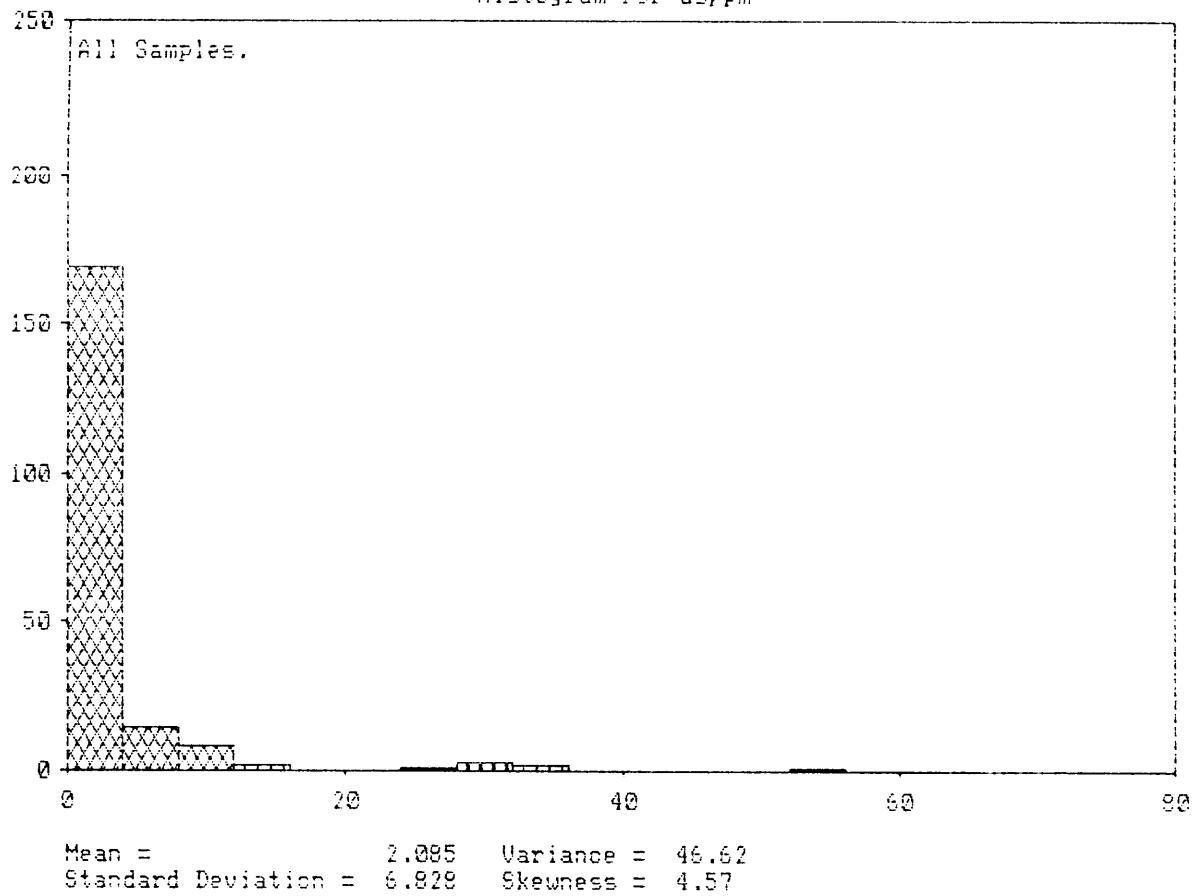
Data elements inside histogram 200

Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 0.11145  |
| Variance           | 0.039839 |
| Standard Deviation | 0.199597 |
| Skewness           | 1.608892 |

Histogram for asppm



Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

Histogram for asppm

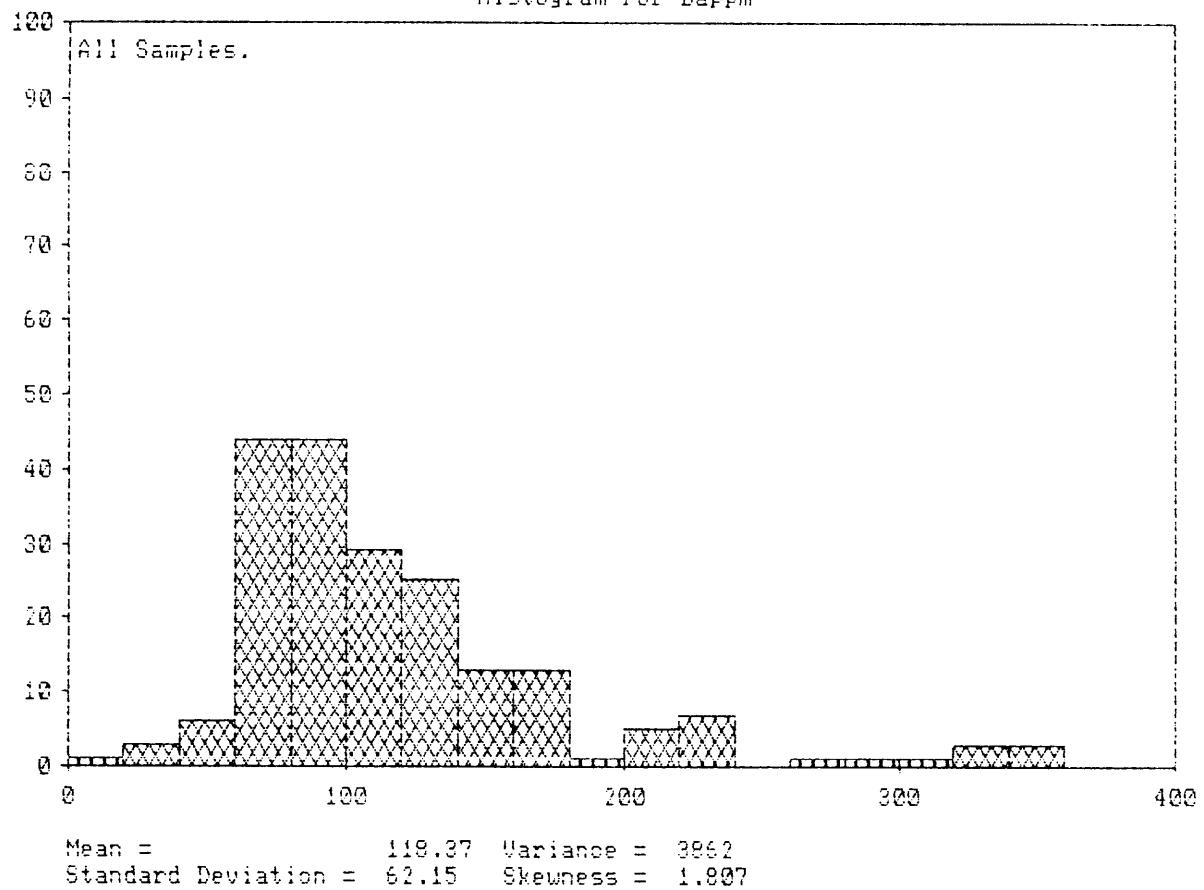
| Lower limit | Upper limit | Frequency | %  | Cumulative | %   | Mean |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 4           | 169       | 85 | 169        | 85  |      |
| 4           | 8           | 14        | 7  | 183        | 92  |      |
| 8           | 12          | 8         | 4  | 191        | 96  |      |
| 12          | 16          | 2         | 1  | 193        | 97  |      |
| 16          | 20          | 0         | 0  | 193        | 97  |      |
| 20          | 24          | 0         | 0  | 193        | 97  |      |
| 24          | 28          | 1         | 1  | 194        | 97  |      |
| 28          | 32          | 3         | 2  | 197        | 99  |      |
| 32          | 36          | 2         | 1  | 199        | 100 |      |
| 36          | 40          | 0         | 0  | 199        | 100 |      |
| 40          | 44          | 0         | 0  | 199        | 100 |      |
| 44          | 48          | 0         | 0  | 199        | 100 |      |
| 48          | 52          | 0         | 0  | 199        | 100 |      |
| 52          | 56          | 1         | 1  | 200        | 100 |      |
| 56          | 60          | 0         | 0  | 200        | 100 |      |
| 60          | 64          | 0         | 0  | 200        | 100 |      |
| 64          | 68          | 0         | 0  | 200        | 100 |      |
| 68          | 72          | 0         | 0  | 200        | 100 |      |
| 72          | 76          | 0         | 0  | 200        | 100 |      |
| 76          | 80          | 0         | 0  | 200        | 100 |      |

Data elements inside histogram 200  
Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 2.085    |
| Variance           | 46.62089 |
| Standard Deviation | 6.827949 |
| Skewness           | 4.570121 |

Histogram for bappm



Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

Histogram for bappm

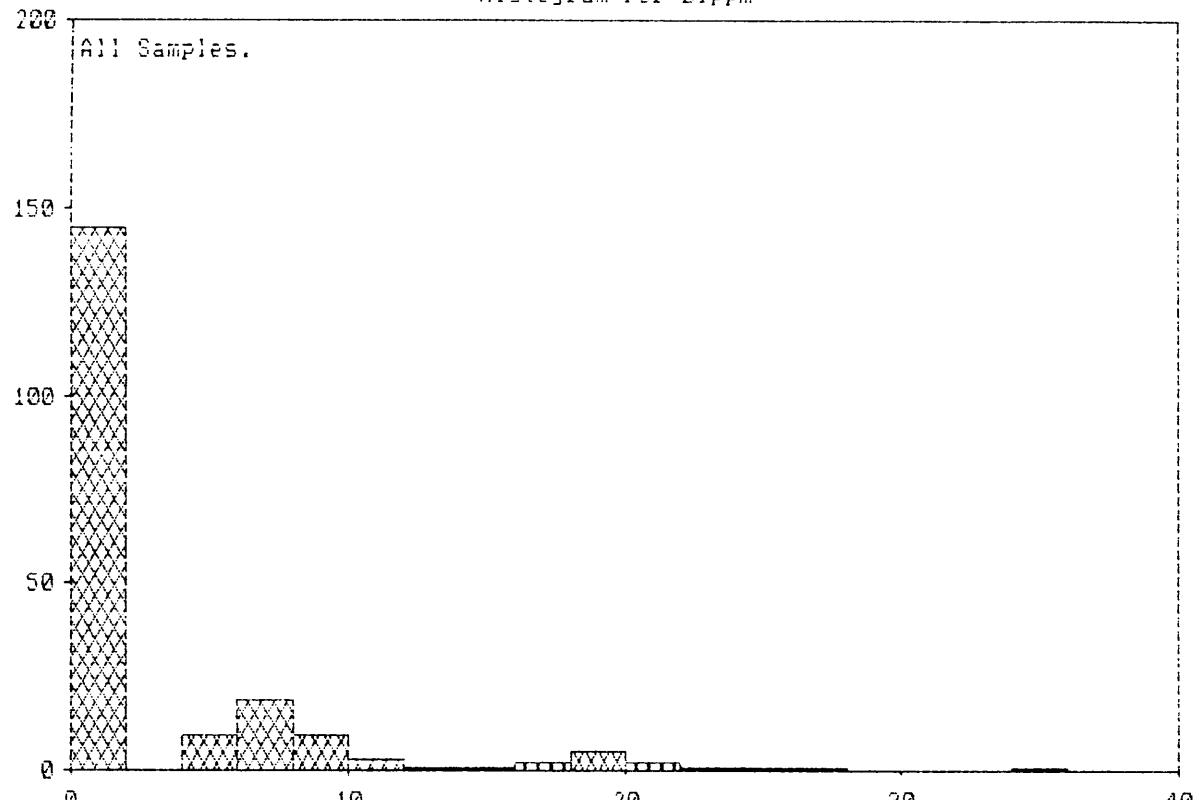
| Lower limit | Upper limit | Frequency | %  | Cumulative | %   |      |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 20          | 1         | 1  | 1          | 1   |      |
| 20          | 40          | 3         | 2  | 4          | 2   |      |
| 40          | 60          | 6         | 3  | 10         | 5   |      |
| 60          | 80          | 44        | 22 | 54         | 27  |      |
| 80          | 100         | 44        | 22 | 98         | 49  |      |
| 100         | 120         | 29        | 15 | 127        | 64  | Mean |
| 120         | 140         | 25        | 13 | 152        | 76  |      |
| 140         | 160         | 13        | 7  | 165        | 83  |      |
| 160         | 180         | 13        | 7  | 178        | 89  |      |
| 180         | 200         | 1         | 1  | 179        | 90  |      |
| 200         | 220         | 5         | 3  | 184        | 92  |      |
| 220         | 240         | 7         | 4  | 191        | 96  |      |
| 240         | 260         | 0         | 0  | 191        | 96  |      |
| 260         | 280         | 1         | 1  | 192        | 96  |      |
| 280         | 300         | 1         | 1  | 193        | 97  |      |
| 300         | 320         | 1         | 1  | 194        | 97  |      |
| 320         | 340         | 3         | 2  | 197        | 99  |      |
| 340         | 360         | 3         | 2  | 200        | 100 |      |
| 360         | 380         | 0         | 0  | 200        | 100 |      |
| 380         | 400         | 0         | 0  | 200        | 100 |      |

Data elements inside histogram 200  
Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 118.375  |
| Variance           | 3862.074 |
| Standard Deviation | 62.14558 |
| Skewness           | 1.806584 |

Histogram for bippm



Mean = 2.875 Variance = 34.35  
Standard Deviation = 5.861 Skewness = 2.591

Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

Histogram for bipm

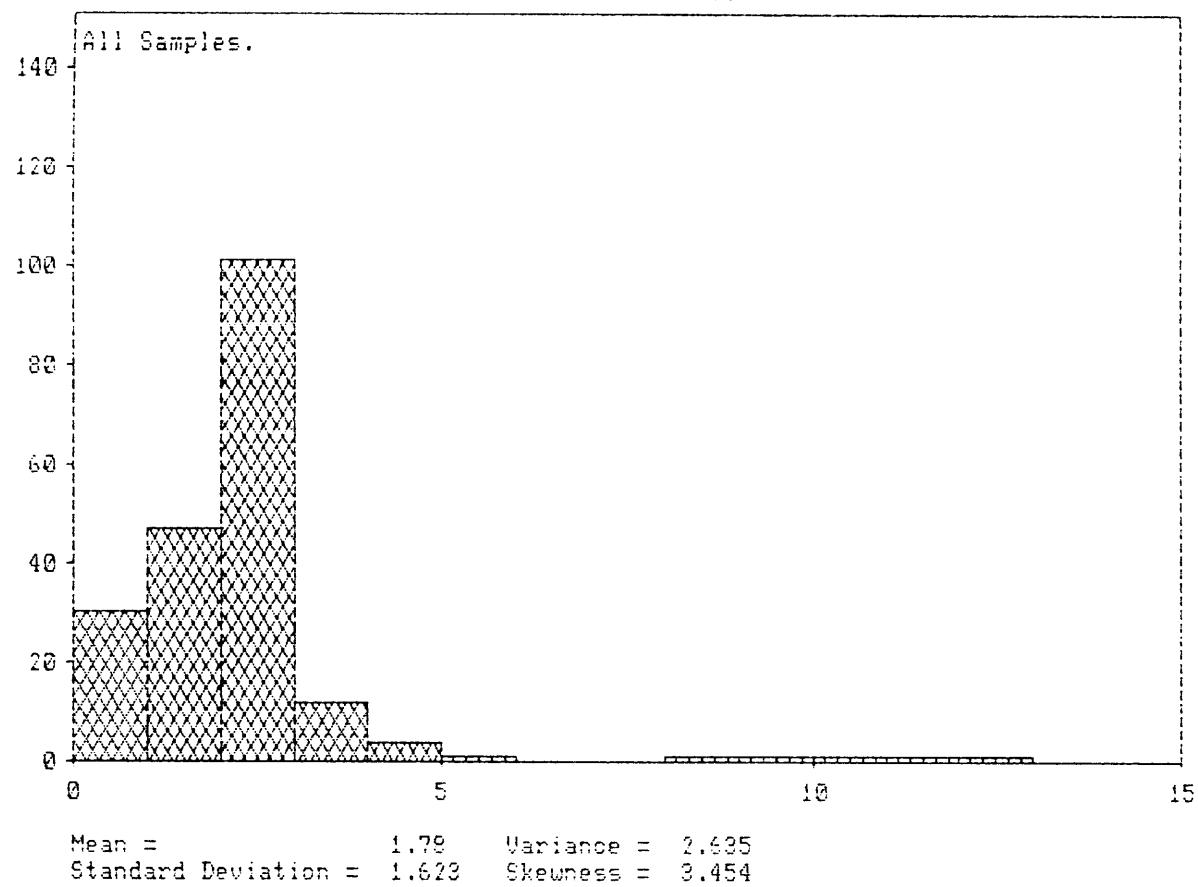
| Lower limit | Upper limit | Frequency | %  | Cumulative | %   |      |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 2           | 145       | 73 | 145        | 73  |      |
| 2           | 4           | 0         | 0  | 145        | 73  | Mean |
| 4           | 6           | 9         | 5  | 154        | 77  |      |
| 6           | 8           | 19        | 10 | 173        | 87  |      |
| 8           | 10          | 9         | 5  | 182        | 91  |      |
| 10          | 12          | 3         | 2  | 185        | 93  |      |
| 12          | 14          | 1         | 1  | 186        | 93  |      |
| 14          | 16          | 1         | 1  | 187        | 94  |      |
| 16          | 18          | 2         | 1  | 189        | 95  |      |
| 18          | 20          | 5         | 3  | 194        | 97  |      |
| 20          | 22          | 2         | 1  | 196        | 98  |      |
| 22          | 24          | 1         | 1  | 197        | 99  |      |
| 24          | 26          | 1         | 1  | 198        | 99  |      |
| 26          | 28          | 1         | 1  | 199        | 100 |      |
| 28          | 30          | 0         | 0  | 199        | 100 |      |
| 30          | 32          | 0         | 0  | 199        | 100 |      |
| 32          | 34          | 0         | 0  | 199        | 100 |      |
| 34          | 36          | 1         | 1  | 200        | 100 |      |
| 36          | 38          | 0         | 0  | 200        | 100 |      |
| 38          | 40          | 0         | 0  | 200        | 100 |      |

Data elements inside histogram 200  
Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 2.875    |
| Variance           | 34.35113 |
| Standard Deviation | 5.860983 |
| Skewness           | 2.591001 |

Histogram for moppm



Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

Histogram for moppm

| Lower limit | Upper limit | Frequency | %  | Cumulative | %   |      |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 1           | 30        | 15 | 30         | 15  |      |
| 1           | 2           | 47        | 24 | 77         | 39  | Mean |
| 2           | 3           | 101       | 51 | 178        | 89  |      |
| 3           | 4           | 12        | 6  | 190        | 95  |      |
| 4           | 5           | 4         | 2  | 194        | 97  |      |
| 5           | 6           | 1         | 1  | 195        | 98  |      |
| 6           | 7           | 0         | 0  | 195        | 98  |      |
| 7           | 8           | 0         | 0  | 195        | 98  |      |
| 8           | 9           | 1         | 1  | 196        | 98  |      |
| 9           | 10          | 1         | 1  | 197        | 99  |      |
| 10          | 11          | 1         | 1  | 198        | 99  |      |
| 11          | 12          | 1         | 1  | 199        | 100 |      |
| 12          | 13          | 1         | 1  | 200        | 100 |      |
| 13          | 14          | 0         | 0  | 200        | 100 |      |
| 14          | 15          | 0         | 0  | 200        | 100 |      |

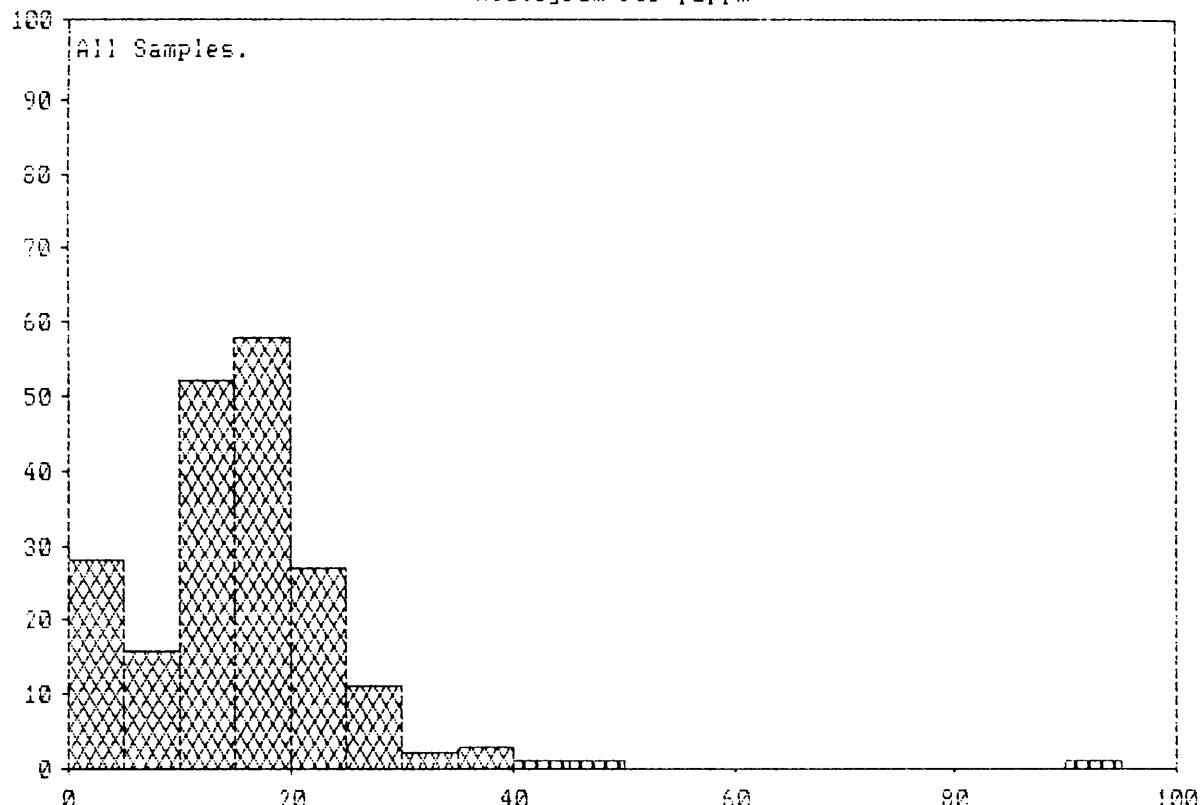
Data elements inside histogram 200

Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 1.78     |
| Variance           | 2.634774 |
| Standard Deviation | 1.623199 |
| Skewness           | 3.453922 |

Histogram for PbPPM



Mean = 14.895 Variance = 100.4  
Standard Deviation = 10.02 Skewness = 2.608

Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

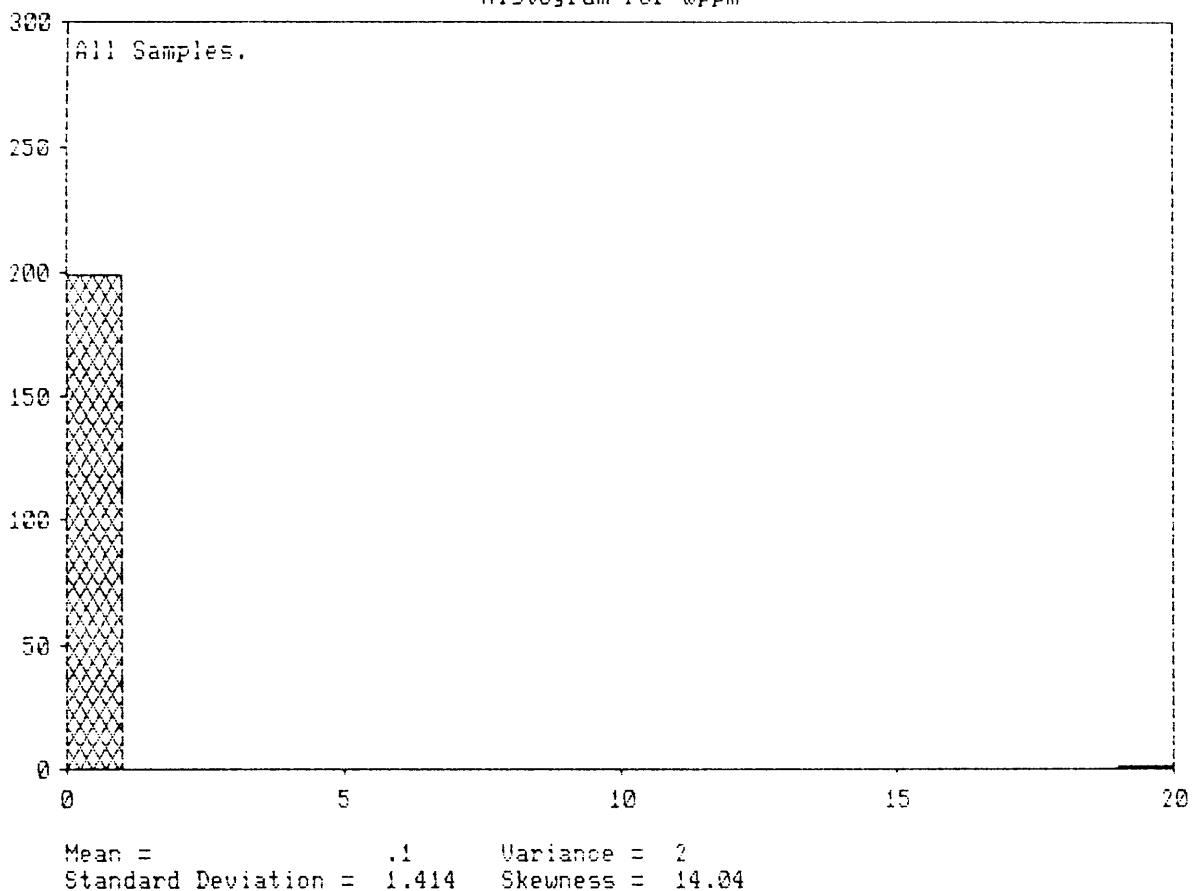
Histogram for pbppm

| Lower limit                     | Upper limit | Frequency | %  | Cumulative | %   |      |
|---------------------------------|-------------|-----------|----|------------|-----|------|
| 0                               | 5           | 28        | 14 | 28         | 14  |      |
| 5                               | 10          | 16        | 8  | 44         | 22  |      |
| 10                              | 15          | 52        | 26 | 96         | 48  | Mean |
| 15                              | 20          | 58        | 29 | 154        | 77  |      |
| 20                              | 25          | 27        | 14 | 181        | 91  |      |
| 25                              | 30          | 11        | 6  | 192        | 96  |      |
| 30                              | 35          | 2         | 1  | 194        | 97  |      |
| 35                              | 40          | 3         | 2  | 197        | 99  |      |
| 40                              | 45          | 1         | 1  | 198        | 99  |      |
| 45                              | 50          | 1         | 1  | 199        | 100 |      |
| 50                              | 55          | 0         | 0  | 199        | 100 |      |
| 55                              | 60          | 0         | 0  | 199        | 100 |      |
| 60                              | 65          | 0         | 0  | 199        | 100 |      |
| 65                              | 70          | 0         | 0  | 199        | 100 |      |
| 70                              | 75          | 0         | 0  | 199        | 100 |      |
| 75                              | 80          | 0         | 0  | 199        | 100 |      |
| 80                              | 85          | 0         | 0  | 199        | 100 |      |
| 85                              | 90          | 0         | 0  | 199        | 100 |      |
| 90                              | 95          | 1         | 1  | 200        | 100 |      |
| 95                              | 100         | 0         | 0  | 200        | 100 |      |
| Data elements inside histogram  |             |           |    | 200        |     |      |
| Data elements outside histogram |             |           |    | 0          |     |      |

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 14.895   |
| Variance           | 100.4261 |
| Standard Deviation | 10.02128 |
| Skewness           | 2.607715 |

Histogram for wppm



Routine: FREHIST File: ALL.NUM Date: 10-03-1990  
Comment: All Samples.

Page:

Histogram for wppm

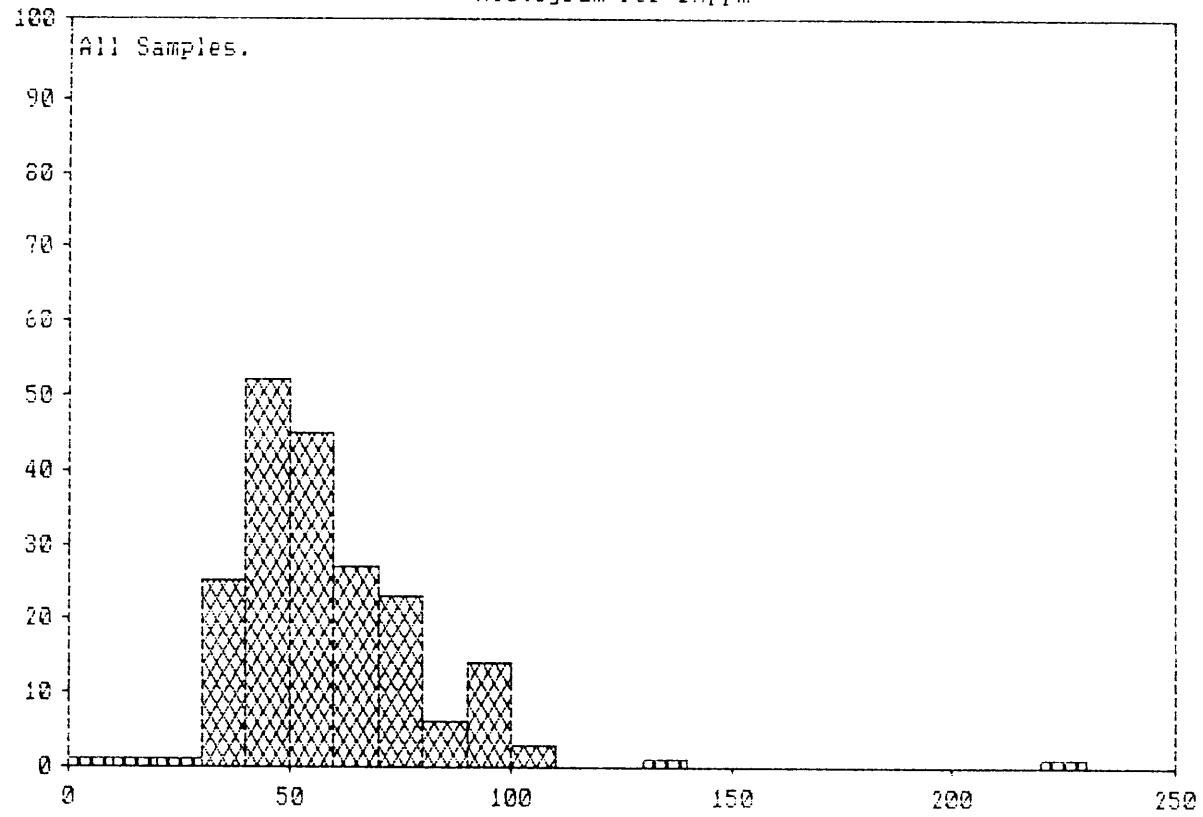
| Lower limit | Upper limit | Frequency | %   | Cumulative | %   | Mean |
|-------------|-------------|-----------|-----|------------|-----|------|
| 0           | 1           | 199       | 100 | 199        | 100 |      |
| 1           | 2           | 0         | 0   | 199        | 100 |      |
| 2           | 3           | 0         | 0   | 199        | 100 |      |
| 3           | 4           | 0         | 0   | 199        | 100 |      |
| 4           | 5           | 0         | 0   | 199        | 100 |      |
| 5           | 6           | 0         | 0   | 199        | 100 |      |
| 6           | 7           | 0         | 0   | 199        | 100 |      |
| 7           | 8           | 0         | 0   | 199        | 100 |      |
| 8           | 9           | 0         | 0   | 199        | 100 |      |
| 9           | 10          | 0         | 0   | 199        | 100 |      |
| 10          | 11          | 0         | 0   | 199        | 100 |      |
| 11          | 12          | 0         | 0   | 199        | 100 |      |
| 12          | 13          | 0         | 0   | 199        | 100 |      |
| 13          | 14          | 0         | 0   | 199        | 100 |      |
| 14          | 15          | 0         | 0   | 199        | 100 |      |
| 15          | 16          | 0         | 0   | 199        | 100 |      |
| 16          | 17          | 0         | 0   | 199        | 100 |      |
| 17          | 18          | 0         | 0   | 199        | 100 |      |
| 18          | 19          | 0         | 0   | 199        | 100 |      |
| 19          | 20          | 1         | 1   | 200        | 100 |      |

Data elements inside histogram 200  
Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 0.1      |
| Variance           | 2        |
| Standard Deviation | 1.414214 |
| Skewness           | 14.03584 |

Histogram for zNPPM



Mean = 58.105 Variance = 509.4  
Standard Deviation = 22.57 Skewness = 2.582

ROUTINE. FREQUENCIES. ALL. NUM DATE: 10-09-1990  
Comment: All Samples.

Page:

Histogram for znpmm

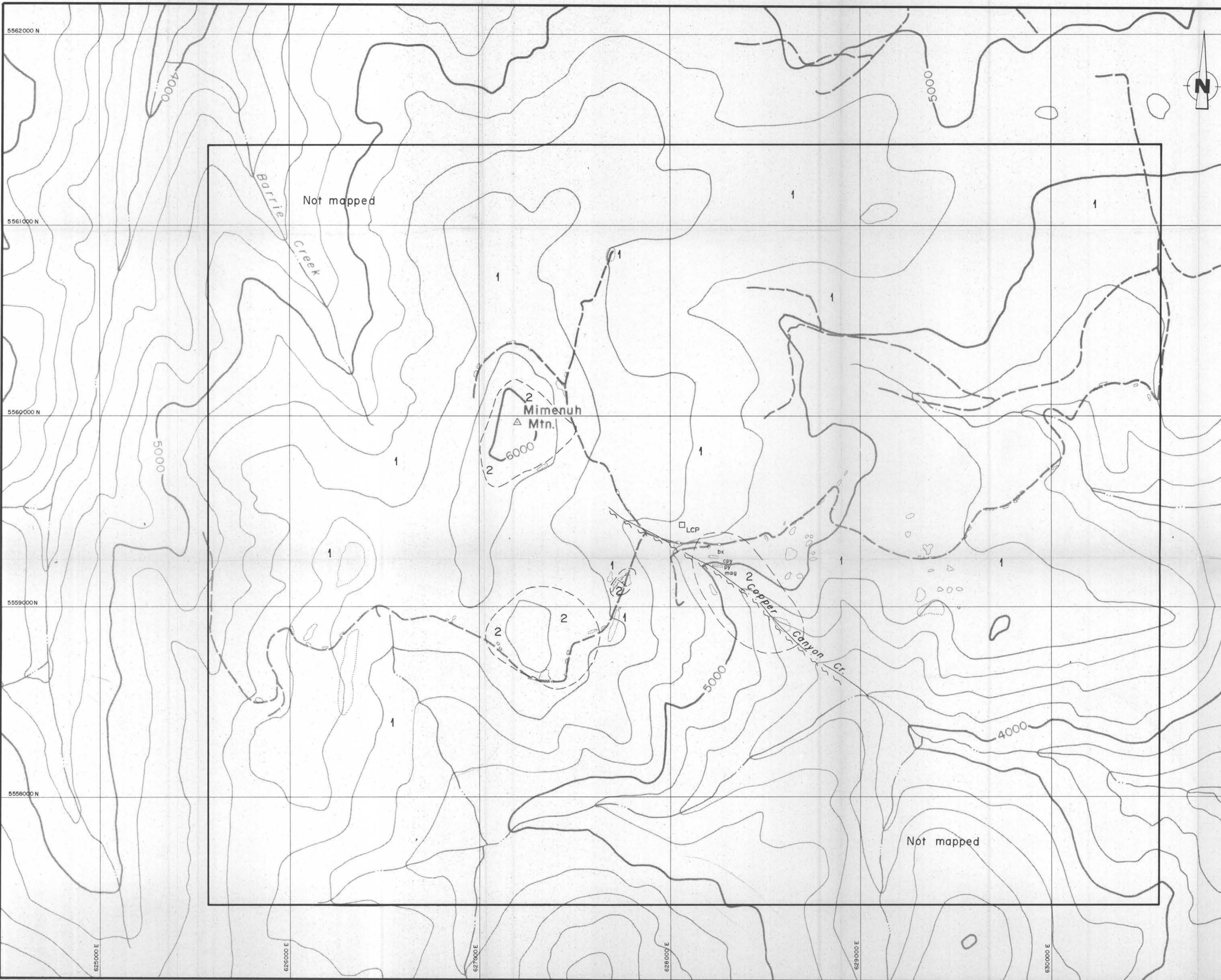
| Lower limit | Upper limit | Frequency | %  | Cumulative | %   |      |
|-------------|-------------|-----------|----|------------|-----|------|
| 0           | 10          | 1         | 1  | 1          | 1   |      |
| 10          | 20          | 1         | 1  | 2          | 1   |      |
| 20          | 30          | 1         | 1  | 3          | 2   |      |
| 30          | 40          | 25        | 13 | 28         | 14  |      |
| 40          | 50          | 52        | 26 | 80         | 40  |      |
| 50          | 60          | 45        | 23 | 125        | 63  | Mean |
| 60          | 70          | 27        | 14 | 152        | 76  |      |
| 70          | 80          | 23        | 12 | 175        | 88  |      |
| 80          | 90          | 6         | 3  | 181        | 91  |      |
| 90          | 100         | 14        | 7  | 195        | 98  |      |
| 100         | 110         | 3         | 2  | 198        | 99  |      |
| 110         | 120         | 0         | 0  | 198        | 99  |      |
| 120         | 130         | 0         | 0  | 198        | 99  |      |
| 130         | 140         | 1         | 1  | 199        | 100 |      |
| 140         | 150         | 0         | 0  | 199        | 100 |      |
| 150         | 160         | 0         | 0  | 199        | 100 |      |
| 160         | 170         | 0         | 0  | 199        | 100 |      |
| 170         | 180         | 0         | 0  | 199        | 100 |      |
| 180         | 190         | 0         | 0  | 199        | 100 |      |
| 190         | 200         | 0         | 0  | 199        | 100 |      |
| 200         | 210         | 0         | 0  | 199        | 100 |      |
| 210         | 220         | 0         | 0  | 199        | 100 |      |
| 220         | 230         | 1         | 1  | 200        | 100 |      |
| 230         | 240         | 0         | 0  | 200        | 100 |      |
| 240         | 250         | 0         | 0  | 200        | 100 |      |

Data elements inside histogram 200  
Data elements outside histogram 0

Descriptive Statistics

|                    |          |
|--------------------|----------|
| Mean               | 58.105   |
| Variance           | 509.4009 |
| Standard Deviation | 22.56991 |
| Skewness           | 2.582485 |

20,912



Topographic Contours  
(200' interval)

Stream

Road

2 Feldspar Porphyry.

1 Amygdaloidal Basalt Flows  
and Flow Breccias.

Area of Outcrop.

Contact.

Fault.

bx Breccia.

cpx Chalcopyrite.

py Pyrite.

mag Magnetite.



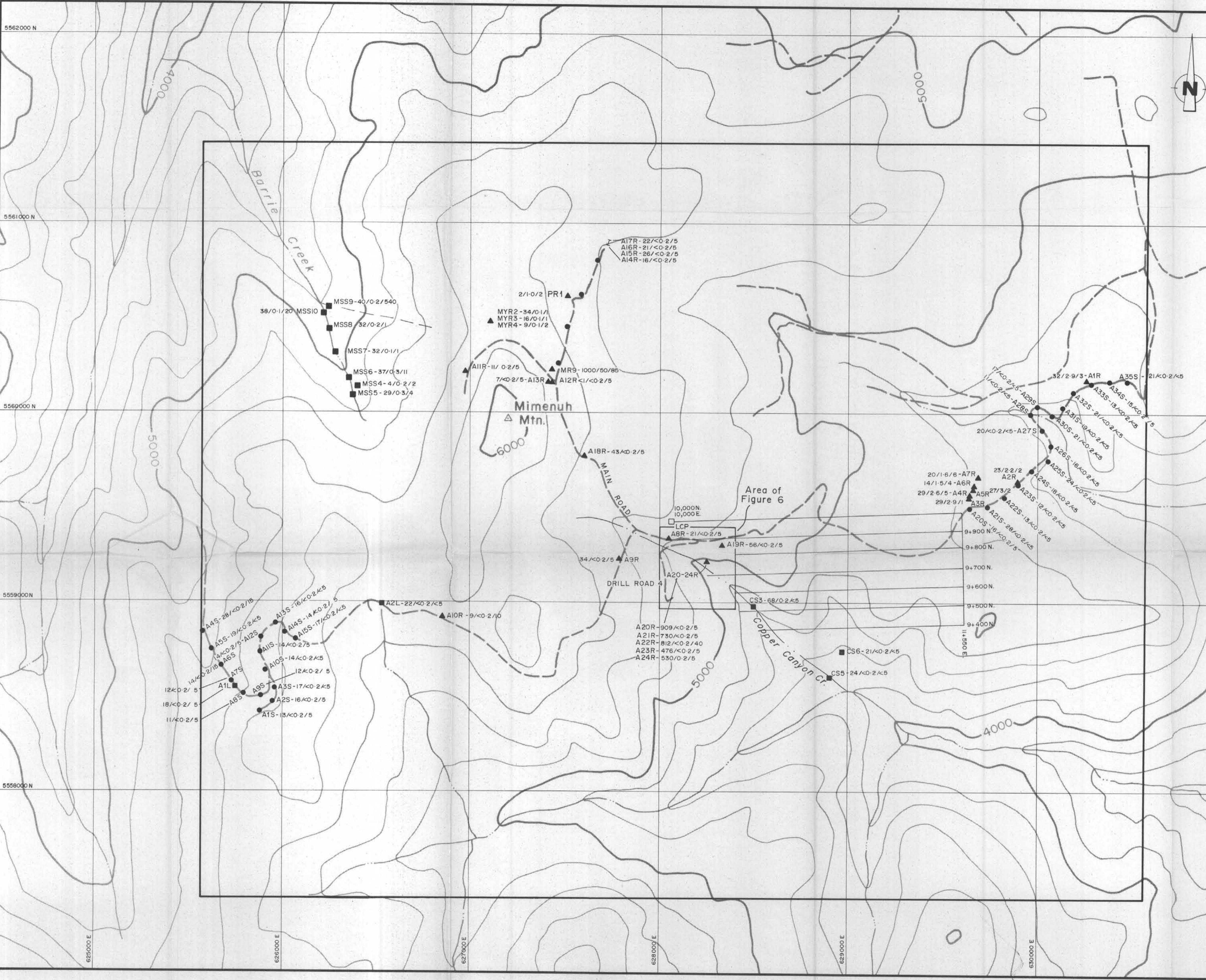
0 100 300 500 750 1000 Metres

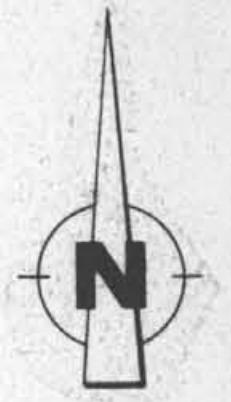
PACIFIC SENTINEL GOLD CORP.  
**MIME PROPERTY**  
NICOLA M.D., B.C.

## GEOLOGY

|                                   |               |                   |
|-----------------------------------|---------------|-------------------|
| Scale : 1:10,000                  | N.T.S. 92-1/3 | Drawn by : w.g.i. |
| Date : SEPT. 1990                 | Geologist :   | Figure : 4        |
| RELIANCE GEOLOGICAL SERVICES INC. |               |                   |

20,912

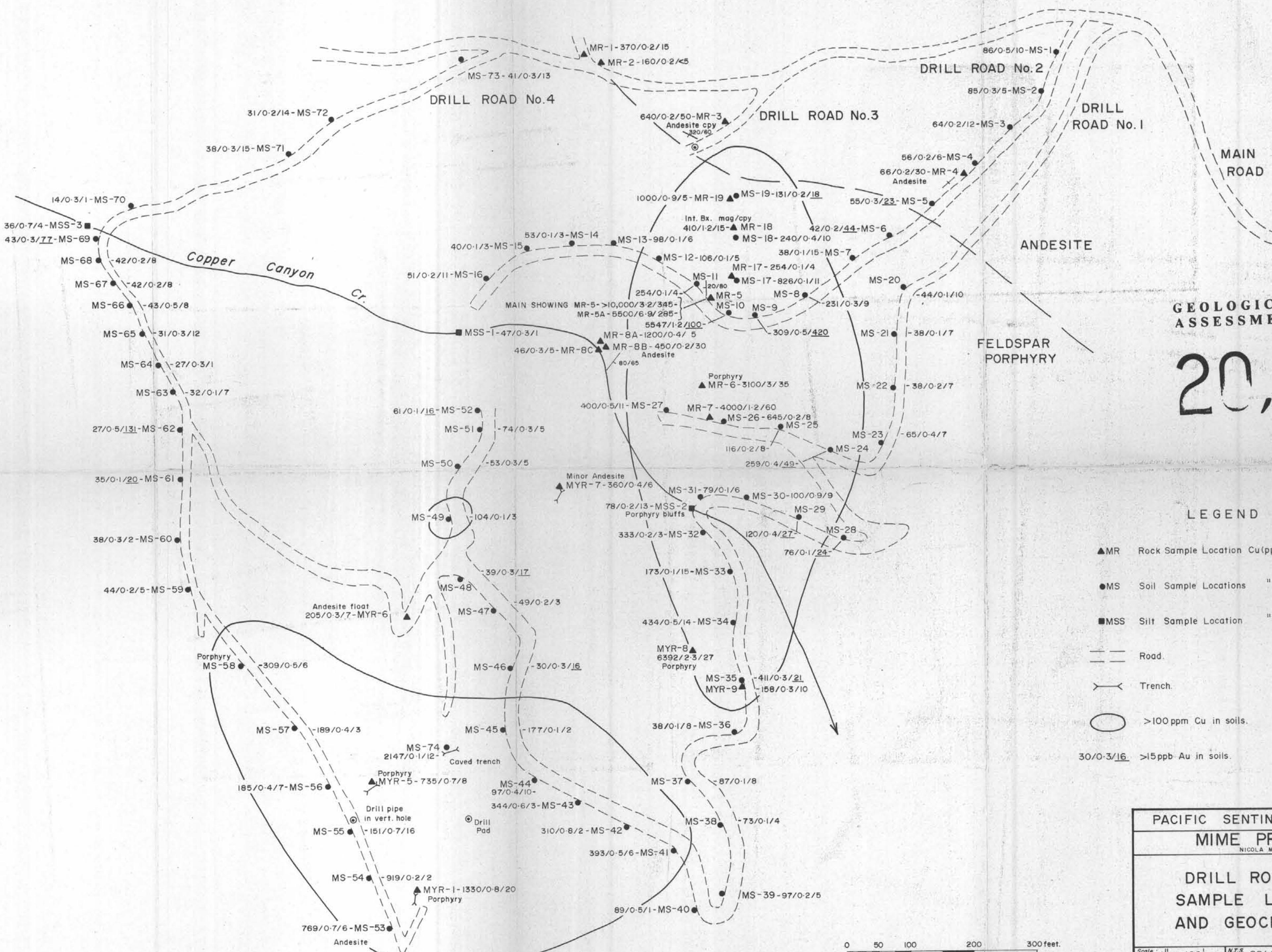




CAMP  
To Merritt

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

**20,012**



**LEGEND**

- ▲MR Rock Sample Location Cu(ppm), Ag(ppm), Au(ppb)
- MS Soil Sample Locations " " "
- MSS Silt Sample Location " " "
- Road.
- Trench.
- >100 ppm Cu in soils.
- 30/0.3/16 >15 ppb Au in soils.



PACIFIC SENTINEL GOLD CORP.

MIME PROPERTY

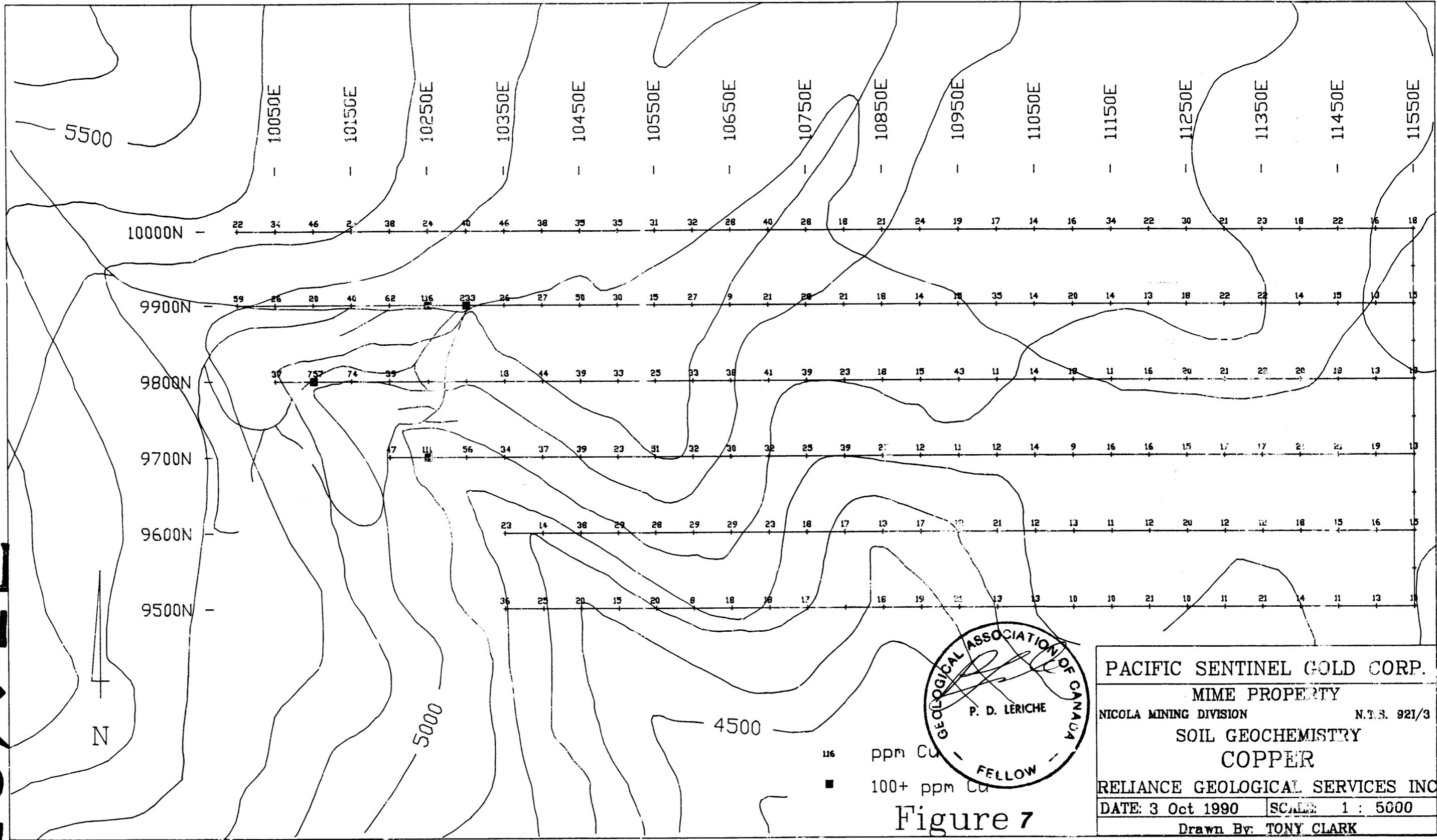
NICOLA M.D., B.C.

DRILL ROAD AREA  
SAMPLE LOCATIONS  
AND GEOCHEMISTRY

|                  |                  |           |
|------------------|------------------|-----------|
| Scale: 1" = 100' | N.T.S. 921/3     | Drawn by: |
| Date: SEPT. 1990 | Geologist: _____ | Figure: 6 |

RELIANCE GEOLOGICAL SERVICES INC.

20912



**GEOLOGICAL BRANCH  
AGENCEY OF THE FEDERAL  
GOVERNMENT**

2009-2

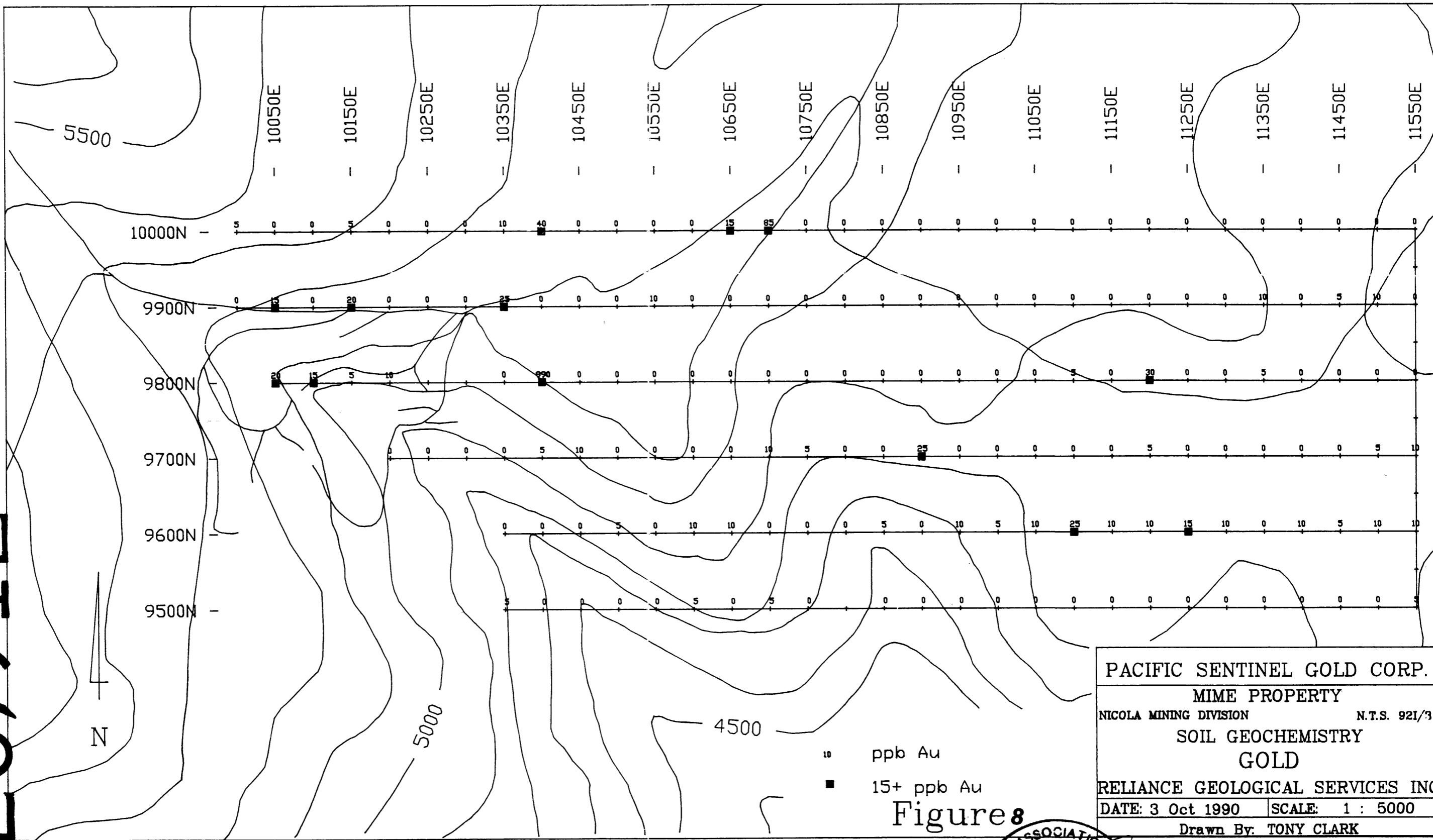


Figure 8

