| SUB-RECORDER<br>RECEIVED |                   | LOG NO: Jeb 13/91 RD. |
|--------------------------|-------------------|-----------------------|
| FEB - 5 1991             |                   | AUTION.               |
| .R. #\$                  | ASSESSMENT REPORT | FILE NO:              |

M ON DIAMOND DRILLING

ON THE BERESFORD LAKE CLAIM GROUP

| CLAIM NAME | RECORD No.   | UNITS       |
|------------|--------------|-------------|
| ADD #2     | <b>894</b> 8 | 1           |
| ADD #3     | 8949         | 1           |
| ADD #4     | <b>895</b> 0 | 1           |
| ADD #10    | <b>89</b> 56 | 12          |
| ADD #11    | 9026         | 4           |
| RICH       | 7896         | $\tilde{4}$ |
| [Notice    | to Group No. | ]           |

KAMLOOPS MINING DIVISION BERESFORD LAKE AREA, BRITISH COLUMBIA NTS 921/9

LOCATION: 11 Km SOUTH OF KAMLOOPS, BC

LATITUDE: 50 DEG. 33'N LONGITUDE: 120 DEG. 15'W

FIELD WORK PERIOD: MAY 11, 1990 TO JULY 22, 1990

CLAIM OWNERS: NAXOS RESOURCES LTD. 206-856 HOMER STREET VANCOUVER, BC. V6B 3W5 (604) 669-8078

> DAVID DECKER #6-1299 TRANQUILLE RD. KAMLOOPS, BC. V2B 1X6

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OPERATOR: NAXOS REBOURCES LTD. 206-856 HOMER STREET VANCOUVER, BC. V6B 3W5 (604) 669-8078

REPORT DATE: JANUARY 28, 1991.

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### MAP INDEX

MAP NAME SCALE

Location Map and Claims Map Showing Drill Hole Locations BAR

### APPENDIX

Diamond Drill Logs DDH# 90-1 and 90-2 by E. Lambert. Cross Section DDH 90-1 by E. Lambert. Cross Section DDH 90-2 by E. Lambert. Percussion Drill Logs IF-1 and IF-2 by W. Thompson. Metallurgical Test Data - Nesmont Precious Metals Corp. Certificate # 12140-1 & -2, Dated July 3 & 4, 1990. Total Gold Determination Tests & Results - Casmyn Research & Engineering, Dated October 2, 1990.

### DRILLING REPORT - 1000 FIELD SEASON on the BERESFORD LAKE (GAIM GROUP KAMLOOPS MINING DIVISION for NAXOS RESOURCES LTD.

### SUMMARY

The ADD #2, 3, 4, 10, 11 and RICH claims, 51% held by Naxos Resources Ltd. and 49% held by International Focus Resources Inc., consist of 20 units situated approximately 12 kilometres south of the City of Kamloops within the Kamloops Mining Division, south-central British Columbia.

The property is accessible by the gravelled Beresford Lake Road east from Highway No. 5 some four kilometres south of Knutsford.

The topography is gently undulating with elevations ranging from 670 metres to 914 metres above sea level.

Sufficient water is available for all phases of exploration and development.

Diesel electric power would be required for initial phases of development and hydro-electric power would be available if future requirements warrant.

Railroad and good daily trucking facilities are located in Kamloops where most supplies are obtainable.

The property appears to be underlain by volcanics of the Kamloops and Nicola Groups.

### LOCATION

The claims are located approximately 12 kilometres south of Kamloops within the Kamloops Mining Division in south-central British Columbia.

### ACCESS

The property is accessible by automobile southeasterly for three kilometres along the gravelled Beresford Lake Road some four kilometres south from Knutsford on Highway No. 5.

1

### TOPOGRAPHY AND CLIMATE

The main topographic features of the area are broad upland areas separated by deeply incised valleys. The property is located on the north east flank of the Nicola Plateau which forms part of the belt of Interior Plateaux. The elevations within the property boundaries varies between 670 metres and 914 metres, giving a relief of 245 metres.

The Kamloops area is semi-arid and experiences moderate to severe winters, and hot dry summers.

### WATER, POWER AND TIMBER

Sufficient water is available for all phases of exploration from streams, ponds and lakes which are located on or near the property. Diesel electric power will be required for initial phases of development and hydro-electric power would be available if future requirements warrant. Timber on the reachland area is sparse. Finished lumber is available from local sawmille.

### TRANSPORTATION AND SUPPLIES

Railroad and daily trucking facilities are available in Kamloops where most supplies are obtainable.

### PROPERTY

The property is comprised of six mineral claims consisting of 20 units. They are as follows:

| <u>Claim Name</u> | Record Number | <u>Units</u> |
|-------------------|---------------|--------------|
| ADD #2            | 8948          | 1            |
| ADD #3            | 8949          | 1            |
| ADD #4            | <b>895</b> 0  | 1            |
| ADD #10           | 8956          | 12           |
| ADD #11           | 9026          | 1            |
| RICH              | 7896          | 4            |

### <u>OWNERSHIP</u>

The claims are owned by Naxos Resources Ltd. (51%) of Vancouver, and David Decker (49%) of Kamloops, British Columbia.

### GENERAL GEOLOGY

The geology of the area is shown on Map 886A Nicola (East Half) of the Geological Survey of Canada. The area is underlain by the volcanic sequences of the Miocene Kamloops Group and the Upper Triassic Nicola Group which have been intruded by the elliptical-shaped Iron Mask Batholith. The rocks comprising the batholith are generally mediumgrained, grey, greenish grey to very dark, with ferromagnesium-rich phases and exhibit considerable alteration. They occur as microdiorite, micromonzonite, gabbro, diorite, pyroxenite, monzonite and syenite. The batholith appears to be intruded into the limb of a northwesterly trending syncline and is exposed some 19 kilometres long and four kilometres wide.

Two younger intrusives of post Iron Mask Batholith age occur in contact with the periphery if the Iron Mask intrusive to the north, west and south. They are the Cherry Creek and Sugarloaf intrusives. The Cherry Creek intrusives are comprised of porphyritic microdiorite, latite, trachyte porphyry, igneous breccia, minor porphyritic microquartz monzonite, and micro-granodiorite. The Sugarloaf intrusive consists of porphyritic microdiorite.

The Nicola rocks of Upper Triassic age are mainly a grey-green to bright green, fine-grained, nearly aphanitic to coarsely porphyritic basalt with lesser amounts of other coloured flows. Associated with the basalts are tuffs, breccias, and agg/omerates of various colours and appearance.

Alteration of the rocks is to chlorite, calcite, albite and epidote. Feldspars show advanced alteration with secondary calcite and deuteric quartz. Hornblende phenocrysts, probably derived from the uralization of augite, have been partially chloritized.

The rocks, sometimes referred to as Nicola Greenstones, are presumably the alteration product of hornblende and augite basalts.

There are also labradorite and augite porphyries and fine-grained to porphyritic amygdaloidal lavas containing amygdules of chlorite, calcite, guartz and chalcedony.

Mineralization in the Iron Mask Batholith area generally occurs as copper sulphides, oxides and carbonates in veins, as impregnations, in shear zones, stockworks and breccips. The principal minerals are chalcopyrite, bornite and native copper with lesser amounts of chalcocite, cuprite, azurite, malachite, and chrysocolla. There are also minor amounts of gold and silver present. Alteration products associated with the mineralized zones are pink potash feldspar, sercite, sausserite, carbonate, epidote, albite and hematite.

### PROPERTY GEOLOGY

The property is underlain by volcanic rocks of Kamloops and Nicola Groups. There is no known mineralization on the property except for very minor pyrite.

### 1990 FIELD PROGRAM

Between May 11 and July 22, 1990 two NQ diamond drill holes were drilled on the ADD #10 claim. The holes were drilled to test for the possible northern extension of the basaltic sill that has been the focus of extensive drilling by Naxos Resources Ltd. on the east side of Shumway Lake.

Hole DDH #90-1 was drilled approximately 500 metres east of the collar of DDH #90-2 on the ADD #10 claim. The hole was drilled at an angle of -45 degrees, at an azimuth of 094 degrees, and to a depth of 84 metres.

Hole #90-2 was drilled approximately 300 metres northeast of the southwest corner post of the ADD #10 claim. The hole was drilled at an angle of -45 degrees, at an azimuth of 061 degrees, and was terminated at a depth of 83.5 metres.

A total of 360 feet (109.7 m) of percussion drilling was drilled in two holes; IF-1 was drilled to a depth of 160 feet (48.8 m) and IF-2 to a depth of 200 feet (61 m).

No significant gold values were encountered.

Respectfully submitted,

Thomas R. Dough

Thomas R. Tough, P.Eng. Consulting Geologist.

### CERTIFICATE

I, Thomas R. Tough, of the City of Richmond, in the Province of British Columbia, do hereby certify:

That I am a Consulting Geologist and the principal of T. R. Tough & Associates Ltd., with offices located at 5580 Gibbons Drive, Richmond, British Columbia and at 110, 12761-16th Avenue, White Rock, British Columbia.

- I further certify:
- That I am a Graduate of the University of British Columbia (1965) and hold a B.Sc. degree in Geology.
- 2. That I have been practising my profession for the past 25 years.
- 3. That I am registered with the Association of Professional Engineers and Geoscientists of the Province of British Columbia.
- 4. That this report is based on information received from Naxos Resources Ltd. pertaining to drilling carried out by the Company on the property discussed in this report and from personal visits to the property during 1990 and from personal experience in, and knowledge of the area.
- 5. That I did examine the sites of DDH's #90-1 and #90-2 although I did not personally supervise the drill program nor did I log or sample the drill core.

Showar R. Do

Thomas R. Tough, P.Eng. Consulting Geologist.

White Rock, B.C. January 28, 1991.



### SUMMARY LOG FOR DRILL HOLE 90-1

94° Property: AD 10 Claim Azimuth: -45° Dates Drilled: May 11-14, 1990 Dip: 276 ft. May 15, 1990 Depth: Dates Logged: Ellen Lambert Core Size: NO Logged By:

### INTERVAL DESCRIPTION

(feet)

- 0 22 OVERBURDEN 20' of casing
- 22 68 GABBRO TUFF/ARGILLITE - Interbodded dark green to black argillite and dark green, fine to medium grained gabbroic tuff. Argillite is smooth textured on core surface, whereas tuff is slightly pitted. Gradational contacts are common. The two units are intimately mixed, probably a result of contemporaneous deposition. Tuff consists of chlorite, reddish mica and dark open amphibole crystals (after pyroxene). Argillite consists of dark green to medium green chloritized fine-grained material interbedded with ultrafine grained black material. Weakly to moderately developed bedding at 90° to core exis, coincident with a foliation development. Tuff and argillite are non-magnetic and are cut by guartz and calcite veinlets at all angles to the core axis. Calcite veinlets are commonly deformed whereas quartz and calcite stringers cut across deformation. Trace sulphides are visible and are very fine grained, consisting of pyrite and chalcopyrite (py>cpy).
- 68 69 FALLT ZONE core in intact both breccia texture is well developed, cemented with quartz and calcite. Fault cuts core at 15-25° to core points.
- 69 87 COARSE GRAINED GABBERO bluish-green gabbro consisting of euhedral augite crystals to 3 mm in width (65%), reddish mica? (25%), tiny white crystals of feldspar (2%) and a groundmass (8%). Rock is basically unfoliated. Rare calcite veinlets. Tiny specks of sulphides are disseminated throughout the gabbro (<1%) and appear to be chalcopyrite.

- 76-77 = strong fracturing recemented with calcite.

87-109 GABERO TUFF - interbedded fine grained and medium grained basic tuff. Disseminated pyrite locally to 1-2%. Minor chalcopyrite.

Summary Log DDH 90-1 Page 2

109-113 ARGILLITE - mainly black and medium green argillite

113-126.5 GABBRO TUFF/ARGILLITE - fine-grained tuff that grades into coarsegrained gabbro from 117-120'. Sharp contact with underlying argillite.

- 120-121.5 = mixed argillite and siltstone. Minor tuff

126.5-140 COARSE GRAINED GABBRO - rare py + cpy in tiny quartz + calcite veinlets.

140-140.5 **QUARTZ VEIN** - complex guartz vein that has been fractured and rehealed by guartz at least twice. Minor pyrite. Vein is enveloped by a carbonaceous siltstone.

- 140.5-171 GABBRO TUFF fine grained tuff with local pockets of coarse grained crystals. Minor siltstone-argillite lenses.
  - 147.5-148.7 = coarse-grained gabbro
  - 151-156 = coarse-grained gabbro
  - 158.5-165.5 = mixed fine grained and coarse grained gabbro (tuff) with local pale green to cream coloured cherty fragments; possibly a lithic tuff.
- 171-177 FAULT ZONE multiple fracturing and recementation with calcite. Local clay alteration of host rock. Core mainly intact.

177-276 GABERO TUFF locally mixed with ANVILLITE and COARSE GRAINED GABERO Variably thick "beds" of gabbro tuff in association with narrow lenses of argillite and local beds of coarse grained gabbro. Often see individual augite crystals within overlying argillite units above coarse grained gabbro. Coarse grained gabbro commonly has sharp lower contacts.

-180-183 = 10st core

- 185-196 = mixed argillite and tuff; strongly laminated at 75° to core axis.
- 202 = quartz + pyroxene + chlorite + sulphide vein (1-2 cm) cutting core axis at 35°; host rock is bleached for 5-10 mm on each side of vein. Sulphides are pyrrhotite and chalcopyrite (pyrr>>cpy).
- -200-202 = coarse grained gabbro

- 203-208 = " "

Summary Log DDH 90-1 Page 3

- 219-221 = " " " " - 224-227 = " " " " - 242-246 = " " " " - 244-246 = local guartz veins with pyrrhotite and chalcopyrite - 269 = 3 cm wide guartz vein with pyrite, pyrrhotite and chalcopyrite.

276 BOH



|               | -         |                | ۰، م                  | 2-12-1                   | DIAMOND DRI L RECORD                                     |       |                      |                           | ر<br>۱              | )-J                     |                   |
|---------------|-----------|----------------|-----------------------|--------------------------|----------------------------------------------------------|-------|----------------------|---------------------------|---------------------|-------------------------|-------------------|
| PROP          | RTY -     | ADI            | 0                     |                          | Length $\frac{2711}{}$ Bearing $\frac{61}{}$             |       |                      | Sheet                     | ;                   | of                      | 3                 |
| Locat<br>Core | ion Size. | 300 m at<br>NC | ۲ <u>۲</u> ۲ ۲ ۲<br>۲ | <u>from AD10</u> (<br>35 | OF V. Comp Logged By E Lambert                           |       | Date<br>Date<br>Date | e Begun<br>Ended<br>Logge | May<br>May<br>d may | 15,1°<br>17,19<br>17,19 | $\frac{17n}{176}$ |
| Foot          | age       | Mete           | rage                  | X                        | DESCRIPTION                                              |       | SAMI                 | PLE.                      |                     | ASS                     | AY                |
| From          | To        | From           | To                    | Recovery                 | JEJGKIFTION                                              | No.   | From                 | То                        | Width               | Cu                      | Au                |
| 0             | 18        |                | oxidation<br>]        | 20-30':<br>(10'(·        | overburden                                               | _     |                      |                           |                     |                         |                   |
| 18            | 59        |                | ¥35'                  | 30-40 =<br>100%          | Argillite / Norite Tuff = intercalated black graillife + |       | 1                    |                           |                     |                         |                   |
|               |           |                |                       | 40-50 =<br>100 %         | at arrich. fire to not grance por te toff. Strongly      |       |                      |                           |                     |                         |                   |
|               |           |                | 5                     | 50-60:<br>68%            | laminated at 45° to CA. Lots I anguillite fragments      |       |                      |                           |                     |                         |                   |
|               |           |                | Notes (               | 60 - 70 =<br>67%         | (Flattened) in slowe of fol = noache looks like a        |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 70-80:<br>100'l.         | deformed condemante. Pa is common along                  |       |                      |                           |                     |                         |                   |
| ļ             |           |                |                       | 80-90:                   | Fractures + as ting specks in the rock, about 1-4%.      | •     |                      |                           |                     |                         |                   |
| ļ             |           |                |                       | 90-100 :<br>100 1.       | Local Q+CC veisters. Tr cpy secre Core locally           |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 160 -118 :<br>987.       | Strengly firetured, but usually weakly fractured.        |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 10 -120 -                | Oridation why to about 35. This 20 is throughout         |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 100-130-                 | Thouse & - mayor . Probably throw pyrations is a well.   |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 107.                     | -23-24' = Cae strongly boken                             |       |                      |                           |                     |                         | L                 |
|               |           |                |                       | 100/                     | -41' - Silica Flooding over 1-2" with Pyppyre            | · cpy |                      |                           |                     |                         |                   |
|               |           |                |                       | 100%                     | disseminated in Silica.                                  |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 100 /.                   | - 50-77'= core moderately broken up = some lost          |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 100%                     | core betw 52-69 (4' total).                              |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 100'1.                   | -65-68'= strongly br ken core, brown coloning (altra     | ?)    |                      |                           |                     |                         |                   |
|               |           |                |                       | 100 -210:                | -Bi' = see blacks of a white mineral (up to Icm in       |       |                      |                           | 1                   |                         |                   |
|               |           |                |                       | 100 %                    | length) = barile (?)                                     |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 100%                     | - 80-85' = local zones of while y arom silica w/ minor   |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 100 1.<br>230 -240:      | sulphide.                                                |       |                      |                           |                     |                         | [                 |
|               |           |                |                       | 100%                     | Argillit becames dartes green instead of black.          |       |                      |                           |                     |                         |                   |
|               |           |                |                       | 101.<br>252 -260:        | Also se lord layers of O.g. norike                       |       |                      |                           |                     |                         |                   |
| L             | 1         |                |                       | 100%                     | 100 /.                                                   |       |                      |                           |                     |                         |                   |

gou

|             |         |                                               |                |          | diamodů úki je kesúků                                        |                 |                  |                |       | )-2 |         |
|-------------|---------|-----------------------------------------------|----------------|----------|--------------------------------------------------------------|-----------------|------------------|----------------|-------|-----|---------|
| PROPERTYAOO |         |                                               | Length Bearing |          | ł                                                            | IOLE No<br>Shee | o. —             |                | 3     |     |         |
| Locat       | : i o'n |                                               |                |          | H. Comp Dip                                                  |                 | Date             | Begur          |       |     |         |
| Core        | Size    |                                               |                |          | V. Comp Logged By                                            |                 | Date<br>Date     | Ended<br>Logge | d     |     |         |
| Foot        | age     | Meter                                         | rage           | %        | DESCRIPTION                                                  | 1               | SAMF             | LE             |       | ASS | AY      |
| From        | То      | From                                          | To             | Recovery | DESCRIPTION                                                  | No.             | From             | То             | Width | Cu  | Au      |
| 59          | 74      |                                               |                |          | Ultrafg angillik, black & brown laminated                    |                 |                  |                |       |     |         |
|             |         |                                               |                |          | minor tuff - flinty in nature. Ger noter on previous         | page fr         | + this           | Sect           | ion)  |     |         |
| 74          | 141     |                                               |                |          | Mainly fig tuff with some local segments of                  |                 |                  |                |       |     |         |
|             |         |                                               |                |          | aggillite. (See notes on previous by for 1st part of         | this 5          | ection)          |                |       |     |         |
|             |         |                                               |                | ļ        | Local cq sections as well-                                   |                 |                  |                |       |     |         |
|             | L       | ļļ                                            |                |          | -77-79': ultra fg engillite                                  | ļ               |                  |                |       |     |         |
| 141         | 157     |                                               |                |          | Black + med green any like with minor tuff.                  | .               |                  |                |       |     |         |
|             |         | <b> </b>                                      |                |          | -143-149' = Zone of mod Silica veining =                     |                 |                  |                |       |     |         |
|             |         | <b> </b>                                      |                |          | Swirly. Lord abrendant pyre + Cpy (pyre                      | >>> <<          | 5)               |                |       |     |         |
|             |         | ┠───┼                                         |                |          | in host rock.                                                |                 |                  |                |       |     |         |
|             |         |                                               |                |          | whereas there is an in the second of                         |                 |                  |                |       |     |         |
| •           |         | <u>                                      </u> |                |          | supplies in adjacent host out                                |                 |                  |                |       |     | <b></b> |
| 157         | 165     | ┝──┤                                          |                |          | Eq tuff - always see some py + tr cpy in all                 |                 |                  |                |       |     |         |
|             | <br>    | <b>├</b> ────┣                                |                |          | these rocks.                                                 |                 |                  |                |       |     |         |
| 165         | 176     | <u> </u>                                      |                |          | Blackish angillite with mittor full. Locally mg.             |                 |                  | <del></del>    |       |     |         |
| 176         | 202     | <b> </b>                                      |                |          | Fg to mg tuff.                                               |                 |                  |                |       |     |         |
|             |         |                                               |                |          | - 195' = Texture here resembles accretionery lapilli,        |                 |                  |                |       |     |         |
|             |         | ┟───┼                                         |                |          | zoned in coloration, round pollet-like shapes,               |                 |                  | <u></u>        |       |     |         |
|             |         |                                               |                |          | diffuse texture                                              |                 |                  |                |       |     |         |
|             |         |                                               |                |          | Becomes my in lower half at section, with a sharp            | ·····           |                  |                |       |     |         |
|             |         |                                               |                |          | Contact with underlying angillite. Contact @ 13. A           | o cA            |                  |                |       |     |         |
| 202         | 206.5   | <u> </u>                                      |                | ·        | Blackish angillite becoming mixed with to full near          |                 |                  |                |       |     |         |
| 701 -       | 2-11    | ┝───┼                                         |                |          | bottem d section                                             |                 | $\left  \right $ |                |       |     |         |
| 06.J        | 007     | L                                             |                | <u> </u> | ry rug variably miles with argillite. Local rug tull section | ه               | <u> </u>         |                |       |     |         |

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DIAMOND DRI L RECORD

24

| PROPERTY <u>AD 10</u><br>Location |     | AD         Length         Bearing           H. Comp         Dip           V. Comp         Logged By |       |        |                                                               | HOLE No. <u>90-2</u><br>Sheet <u>3</u> of<br>Date Begun<br>Date Ended<br>Date Logged |      |     |          |     |          |  |  |
|-----------------------------------|-----|-----------------------------------------------------------------------------------------------------|-------|--------|---------------------------------------------------------------|--------------------------------------------------------------------------------------|------|-----|----------|-----|----------|--|--|
| Foot                              | age | Meter                                                                                               | age   | %      |                                                               | 1                                                                                    | SAM  | PLE |          | ASS | AY       |  |  |
| From                              | To  | From                                                                                                | To Re | covery | DESCRIPTION                                                   |                                                                                      | From | То  | Width    | Cu  | Au       |  |  |
|                                   | T   |                                                                                                     |       |        | Med grained version is foliated with arean +                  |                                                                                      |      |     |          |     |          |  |  |
|                                   | 1   |                                                                                                     |       |        | " aray matter seconated from each other by firthened          |                                                                                      |      |     |          |     | <u> </u> |  |  |
|                                   |     |                                                                                                     |       |        | red inica () diamica or gray, hocal                           |                                                                                      |      | 1   |          |     | <u> </u> |  |  |
|                                   |     |                                                                                                     |       |        | Q + cc blacks with assoc pyrr + cpy                           |                                                                                      |      |     |          |     |          |  |  |
| 224                               | 234 |                                                                                                     |       |        | Predominantly ma full with weak for development,              |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | Malier area in cafer, no obvious red mica,                    |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | trav subhides (including cow). Most other                     |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | tull wants have the red thinge                                |                                                                                      |      |     |          |     |          |  |  |
| 234                               | 274 |                                                                                                     |       |        | mixed full + angellite                                        |                                                                                      |      |     |          |     |          |  |  |
|                                   | EoH |                                                                                                     |       |        | -234-239 = tult (mg)                                          |                                                                                      |      |     |          |     |          |  |  |
| ļ                                 |     |                                                                                                     |       |        | -239- Ener Engillie                                           |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -241-2425 = tuff (mg)                                         |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -242.5-245 = argillite grading in to had down hate.           |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -245-249 = mg huff                                            | L                                                                                    |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -249-253 = argillite grading in to till some hole             |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -253-254 = mg tull                                            |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -254 - 257: assilide                                          |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -257-262 = mg tuff ; nanow fault zone at bottom con           | tact                                                                                 |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -262-266.5 = blackish brown angillike                         |                                                                                      |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | * note: pytroy occurs in these "angillite" units              | <u>_</u>                                                                             |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | as tiny flattened flecks. Thereas Ilits could be real fig. to | q.                                                                                   |      |     |          |     |          |  |  |
|                                   |     |                                                                                                     |       |        | * note: py is common in cross-cutting conventets.             |                                                                                      |      |     | <u> </u> |     |          |  |  |
|                                   |     |                                                                                                     |       |        | - 266.5-271 = Fy to my tiff                                   |                                                                                      |      |     | ļ        |     |          |  |  |
|                                   |     |                                                                                                     |       |        | -271-274 = vSa toff to angillite.                             |                                                                                      |      |     |          |     |          |  |  |

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Resmont Frequous Retals Corp. Custoner: Goldbar Resources - Andy Eably 7333 River Ed. Rane: Ladner, B.C. V4G 1E1 Address: 1065 Singh St. Kamloops, B.C. Date: 6112,98 376-2792 113190 Completed: Phone: 014: Nesmont # 12140 Connents:Head Sample from Drilled Product P 12140-1 G 12140-2 Quantity:48.05kg. 48.7kg. Float Fan/FilteDry/Clean Assay Crush Grind Frocess: 35 35 160 35 35 25 2 0.5 2 ! €.25 4 \$768.75 Equipment Hours: DirectionWeigh total ore, Split 24-Save, Split 40kg, Grind to 100% -200 mesh, Ploat, Collect tails, Pan, Filter, Dry, Conc & Fails, Size on pan tails, Bag. Assay Head, Pan Fails, Flot and Fan Concs. Analysis: Au oz. Au 0.003124 Quantity: 0.044 Tons/Kg. 40 Head: 0.071 oz (T)/Top Ploat Con 0.438 oz [T]/Top 0.000772 0.001815 Tons/Kg. 1.65 0.000245 Tons/Kg. 0.22313 Pan Conc 0.659 oz (f)/Ton 0.000164 2.039765 Tons/Kc. 36.15 Tails: 0.07 oz [f]/fon 0.002783 \$ Recovery: Hass Distribution: ş Gold Plost Conc: 24.72 Conc Ratio 1: 24.24 Ploat Conc: 4.13 0.56 5.26 Conc Ratio 1: 7.39 Pan Conc: Pan Conc: Pan Tails: 89.10 Pan Tails: 90.38 113.82 Slimes/Water Soluble Component"" Total: 4.94 Yotal: 100.00 1 0 grams +30 resb 0.00 Grind: 0 grams -30+60 mesh 0.00 0 grams -60+100 mesh 0.00 0 grams -100+140mesh 0.00 0.9 grams -140+200mesh 1.03 98.97 87.2 Total Sample Weight (g) g/Ton Total FLOTATION: Conditioner Reagents: Areo 250 C As needed grams 6.60 to k5 L. Conditioner FAT - ceil 150 Ball Mill CuSO4 -BH 50 2.20 рĦ 1.10 to 35 L Conditioner 8.35 3418A -cell 25 1.32 to -5 L Ball Mill Areo 209 BN 30 Comments:Hill time 2 hrs., Condition time .5 hrs., Ploat time .33 hrs. 0.5 Metallurgy floatation reagents br Grind, size fract hrs. ŵ. 5

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Pinal Report

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| Customer:                                                          |                                                                                                                                                             | Nesmont Precious Retals Corp.                                                                                                                                            |                   |
|--------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------|
| Name:                                                              | - Goldbar Resources - Andy Bab                                                                                                                              | iy 7333 River Rd.                                                                                                                                                        |                   |
| Address:                                                           | 1065 Singh St.                                                                                                                                              | Ladner, E.C. V4G 1E1                                                                                                                                                     |                   |
| - 1                                                                | Kamloops, B.C.                                                                                                                                              | Date: 6/12/90                                                                                                                                                            |                   |
| Phone:                                                             | 376-2792                                                                                                                                                    | Completed: 7/4/90                                                                                                                                                        |                   |
| Ore:                                                               | Nesmont # 12140                                                                                                                                             | 2                                                                                                                                                                        |                   |
| Comments:Head Samp<br>F 12140-1                                    | le from Drilled Product<br>G 12140-2                                                                                                                        |                                                                                                                                                                          |                   |
| Quantity:48.05kg.                                                  | 48.7kg.                                                                                                                                                     |                                                                                                                                                                          |                   |
| Frocess:                                                           | Crush Grind Float.                                                                                                                                          | Pan/FilteDry/Clean Assay                                                                                                                                                 |                   |
| Equipment Hours:                                                   | <b>0.5</b> 2                                                                                                                                                | i 6.25 3 4 (\$768.75                                                                                                                                                     | $\rightarrow$     |
| DirectionWeigh tot:<br>Collect t                                   | al ore, Split 2‡-Save, Split 4<br>ails, Pan, Filter, Dry, Conc &                                                                                            | )kg, Grind to 100% -200 mesh, Float,<br>Tails, Size on pan tails, Bag.                                                                                                   |                   |
| Assay nead                                                         | 1, Pan Tails, Flot and Pan Con-                                                                                                                             | 55.<br>An                                                                                                                                                                |                   |
| Head A 0 02                                                        | 02.<br>07 (T)/Top 0 6669                                                                                                                                    | AU<br>8 Guantity, 6 044 Fors/Ko 40                                                                                                                                       | CALC. HOAD 0.0322 |
| Ploat Con 0.13                                                     | a oz (T)/Ton 0.0003                                                                                                                                         | 5 0.002695 Tons/Kg. 2.45                                                                                                                                                 | Alex              |
| Fan Conc 0.2                                                       | loz (T)/Ton 0.0002                                                                                                                                          | 2 0.000825 Tons/Kg. 0.75                                                                                                                                                 |                   |
| fails: 0.02                                                        | 5 oz (T)/Ton 0.0008                                                                                                                                         | 3 0.034155 Tons/Kg. 31.05                                                                                                                                                |                   |
| Fectovery:<br>Gold Ploat Cond<br>Pan Conc:<br>Pan Tails:<br>Tctal: | <ul> <li>Kass Distribution:</li> <li>34.68 Conc Ratio 1: 16</li> <li>23.01 Conc Ratio 1: 3.1</li> <li>88.21</li> <li>122.89 Slimes/Water Science</li> </ul> | 3 Float Conc:       6.13         7 Pan Conc:       1.88         Pan Tails:       77.63         Puble Component***       14.38         Total:       100.00                |                   |
|                                                                    |                                                                                                                                                             | ٢                                                                                                                                                                        |                   |
|                                                                    | Grind:                                                                                                                                                      | 6 grams +30 mesh 0.00<br>0 grams -30+60 mesh 0.00<br>0 grams -60+100 mesh 0.00<br>0 grams -100+140mesh 0.00<br>0.3 grams -140+200mesh 0.33<br>91.8 grams -200 mesh 99.67 |                   |
|                                                                    |                                                                                                                                                             | 52.1 19681 Semple Weigut (g)                                                                                                                                             |                   |
| FLOTATION:                                                         | g/fon Tetal                                                                                                                                                 |                                                                                                                                                                          |                   |
| Enagents:Arec 250 C                                                | As needed press                                                                                                                                             | Conditioner                                                                                                                                                              |                   |
| FAX - ceil                                                         | . 150 6.60 to .5 1                                                                                                                                          | Conditioner                                                                                                                                                              |                   |
| ри СОБОД -ВМ<br>опроление                                          | 50 2.20<br>3 55 1.14 - 53                                                                                                                                   | Canditanaa                                                                                                                                                               |                   |
| 0.17 39185 -CE1                                                    | 1 20 1.10 to .5 1                                                                                                                                           | E CONVICIONET<br>Dall Will                                                                                                                                               |                   |
| Areo 200 E<br>Compents:Mill time                                   | A SO 1.32 to 15  <br>2 brs., Condition time .5 bis                                                                                                          | , Float time .33 hrs.                                                                                                                                                    | Bott Hours Juli   |
|                                                                    |                                                                                                                                                             |                                                                                                                                                                          | Arrive            |

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Hetallurgy floatation reagents hr = 0.5 Grind, size fract brs. = 0.5 Final Report = 5

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Drill Hole: IF - 1.

International Focus

Supervised and spotted by: Andy Babie

This drill was drilled using a 2" star type percussion drill. Essentially a large air-track. The drill hole intersected a sequence of volcanic ashes, tuffs, lapilli tuffs and possibly pillowed volcanics. The pillows are porphyritic and are logged as porphyritic volcanic. They contain phenocrysts of augite as large as 1 cm. long. The composition of the volcanic sequence ranges from intermediate to basic. Minor sulphides (pyrite, chalcopyrite) are mainly associated with hairline veins that occur throughout the hole. Minor sulphides are also found disseminated in the core.

Due to the powdered nature of the drill cuttings visual logging of the core is difficult at the least. The samples were idividually panned and a note of the sulphide content was made also the water table was evident as a result of wet samples. NOTE: W Thompson was not at the site during the drilling, but was asked to log the samples after the holes were drilled. (Which is not standard proceedure).

| 0-05 ft    | Casing                                   |
|------------|------------------------------------------|
| 5-60 ft    | Minor silvery sulphides (py-s)           |
| 60-70 ft   | Significant bronze sulphides (py-b). 2%. |
| 7ø-80 ft   | 1% py-s                                  |
| 80-90 ft   | 1/4% py-s                                |
| 90-100 ft  | 1 1/2% py-s                              |
| 100-110 ft | 2% ру-в                                  |
| 110-120 ft | 1 1/2% py-b. Samples wet to 160 ft.      |
| 120-150 ft | no samples recovered                     |
| 150-160 ft | 2% ру-Ь.                                 |
|            |                                          |

Minor chalcoprite was observed along with minor magnetite

Drill Hole: IF - 2.

International Focus

<u>Supervised and spotted by: Andy Babie</u> Logged By: W Thompson.

This drill was drilled using a 2" star type percussion drill. Essentially a large air-track. The drill hole intersected a sequence of volcanic ashes, tuffs, lapilli

tuffs and possibly pillowed volcanics. The pillows are porphyritic and are logged as porphyritic volcanic. They contain phenocrysts of augite as large as 1 cm. long. The composition of the volcanic sequence ranges from intermediate to basic. Minor sulphides (pyrite, chalcopyrite) are mainly associated with hairline veins that occur throughout the hole. Minor sulphides are also found disseminated in the core.

Due to the powdered nature of the drill cuttings visual logging of the samples is difficult. The samples were idividually panned and a note of the sulphide content was made also the water table was evident as a result of wet samples.

NOTE: W Thompson war not at the site during the drilling but was asked to log the samples after the holes were drilled. (Which i not standard proceedure).

Ø-10 ft Casing

10-100 ft Minor silvery pyrite (py-s).

80-100 ft The samples were oxidized with significant carbonate cuttings possibly indicating a fault zone. 90-100 ft The samples were wet indicating either that the fault zone affected sample recovery so water was added to assist in recovery or water was intersected in the dril hole. (All the samples to 200 ft were wet from 90 ft.) ft Significant bronze pyrite (py-b). Up to 2 1/2% py.

100-200 ft

110-120 ft....No sample. 150-160 ft....No sample.

minor magnetite and traces of cpy were observed in the samples throughout the lenght of the hole.

200 ft end of hole.

OCT 03 '90 10:03 CASMYN CORP. 416 847 0748



CASMYN Research & Engineering A division of Casmyn Corporation Mineral Processing & Environmental Specialists

October 2, 1990

Mr. Robert Fedun President International Focus Suite 910 Home Oil Tower 324 8<sup>th</sup> Avenue SouthWest Calgary, Alberta T2P 222

Dear Robert:

### Re: Total Gold Determination Tests - Shumway Lake

We are pleased to report that the total gold determination tests for the first two holes from Shumway Lake have been completed.

Each sample was tested in accordance with the following procedure:

- (a) crushing to 10 mesh
- (b) fine grinding to over 80% minus 200 mesh in a closed system ball mill, in the presence of a 10 g/lit NaCN solution, maintained at a pH of 10.5 to 11. The continuous grind-leach method represents the most severe from of cyanidation. All coarse, fine and physically refractory gold is readily dissolved in cyanide as a result of the continuous liberation by attrition. Kerosene is added to the process to suppress the "gold-robbing" carbonaceous species in the ore
- (c) filtration at the end of the 72 hour leach cycle
- (d) analysis of the gold content of the solution phase by atomic absorption and the solids phase by fire assay
- (e) computation of the total gold content of the sample via a metallurgical balance

Table 1 shows a summary of the results. Table 2 presents the detailed test parameters for each sample.

A total of 20 sample splits were taken for acid treatment prior to leaching. The results will be available shortly. OCT 03 '90 10:04 CASMYN CORP.416 847 0748

Mr. Robert Fedun October 2, 1990 Page 2

Table 1 shows that there is a sporadic gold occurrence in the holes. The are substantial sections in each hole which appear to be barren with respect to gold. This is confirmed by both the low solution and solid residue assays. The higher grade sections in the holes should help in the development of a comprehensive exploration strategy. This is an aspect that I would like to discuss with you in further detail. A meeting with your geologists at that time would be appropriate.

As you can see, Hole #1 shows an interesting uptick in assays in the 193 to 208 ft sections. There is another one in the 266 to 276 ft section. Hole #2 shows a value of 0.011 oz/t in the 28 to 38 ft section. The 88 to 98 ft section also shows values. This is indicative of gold occurance closer to surface in the area where Hole #2 was drilled. Hole #2 also shows higher values in the 163 to 173 ft, 232 to 238 ft and 258 to 261 ft sections. This data at depth could indicate a relationship with the Hole #1 data at similar depths.

The percussion drilling samples are currently in process. We should be getting some results in the near future. Our experience with the Shumway Lake deposit indicates that there is gold present. We have encountered some fairly high values from this deposit. However, correct spotting of the drill holes (or surface trenches) is most important. Our grind-leach technique successfully overcomes the nugget effect in the sample. But, that is only one half of the battle!

Please give me a call after you have reviewed the enclosed data.

Yours very truly,

Amyn 5. Dahya, P.Eng. President

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OCT 03 '90 10:04 CASMYN CORP. 416 847 0748

# TABLE 1 : SUMMARY OF RESULTS

CLIENT : INTERNATIONAL FOCUS

| 1               | CATC    | CATC    | 1 1             |
|-----------------|---------|---------|-----------------|
| SAMDLE NUMBER   | HEAD    | HEAD    | COMMENT         |
|                 | ACCAV   | ASSAV   |                 |
|                 |         | ADDAI   | 1 1             |
|                 | 1(9/2)  | ( 02/ ) | 1 . 1           |
|                 |         |         |                 |
|                 |         | 0 000   |                 |
| 1-022-034 SPT A | 0.027   | 0.001   |                 |
| 1-022-034 SPT B | 0.023   | 0.001   |                 |
| 1-022-034 SPT C | 0.030   | 0.001   | 1               |
| 1-034-039 SPT A | 0.034   | 0.001   |                 |
| 1-034-039 SPT B | 0.168   | 0.005   | 1               |
| 1-039-049 SPT A | 0.070   | 0.002   |                 |
| 1-039-049 SPT B | 0.045   | 0.001   | 1               |
| 1-039~049 SPT C | 0.041   | 0.001   | 1               |
| 1-039-049 SPT D | 0.040   | 0.001   |                 |
| 1~039-049 SPT E | 0.040   | 0.001   | · ·             |
| 1-046-060 SPT A | 0.036   | 0.001   |                 |
| 1-046-060 SPT B | 0.035   | 0.001   |                 |
| 1-046-060 SPT C | 0.035   | 0.001   |                 |
| 1-046-060 SPT D | 0.035   | 0.001   | 1               |
| 1-046-060 SPT E | 0.035   | 0.001   |                 |
| 1-060-070 SPT A | 0.036   | 0.001   | 1               |
| 1-060-070 SPT B | 0.050   | 0.001   |                 |
| 1-060-070 SPT C | 0.037   | 0.001   |                 |
| 1-070-087 SPT C | 0.026   | 0.001   |                 |
| 1-087-097 SPT A | 0.038   | 0.001   |                 |
| 1-087-097 SPT B | 0.033   | 0.001   |                 |
| 1-087-097 SPT C | 0.124   | 0.004   |                 |
| 1-087-097 SPT D | 0.045   | 0.001   |                 |
| 1-087-097 SPT E | 0.056   | 0.002   |                 |
| 1-097-112 SPT A | 0.029   | 0.001   |                 |
| 1-112-120 SPT A | 0.203   | 10.006  |                 |
| 1-112-120 SPT B | 0.236   | 0.007   |                 |
| 1-112-120 SPT C | 0.257   | 0.007   |                 |
| 1-120-127 SPT A | 0.028   | 0.001   | J i             |
| 1-120-127 SPT B | 0.000   | 0.000   | AWAITING ASSAYS |
| 1-127-140 SPT A | 0.027   | 0.001   |                 |
| 1-127-140 SPT B | 0.026   | 0.001   |                 |
| 1-127-140 SPT C | 0.027   | 0.001   | 1               |
| 1-140-147 SPT A | 0.036   | 0.001   |                 |
| 1-140-147 SPT B | 0-036   | 0.001   |                 |
| 1-140-147 RDT C | 0.036   | 0 001   |                 |
| 1-147-1KK CDM D | 0.030   | 0.001   | ł               |
| 1-147-186 800 C | 0.026   | 0.001   | 1               |
| 1-156-166 60T A | 0.025   | 0.001   |                 |
| 1-165-165 0F4 A | 0.037   | 0.001   |                 |
| 4-194-103 SLI D | 1 0.036 | 0.001   | 1               |

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OCT 03 '90 10:05 CASMYN CORP.416 847 0748

# TABLE 1 : BUMMARY OF RESULTS

CLIENT : INTERNATIONAL FOCUS

| SAMPLE NUMBER                                                                                                                                                                                                                                                                                                                                                                                                                                                        | CALC.<br>HEAD<br>ASSAY<br>(g/t)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | CALC.<br>HEAD<br>ASSAY<br>( oz/t )                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | COMMENT                                               |
|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------|
| 1-156-165 SPT C<br>1-165-175 SPT A<br>1-165-175 SPT B<br>1-165-175 SPT C<br>1-175-183 SPT A<br>1-175-183 SPT A<br>1-175-183 SPT C<br>1-183-193 SPT C<br>1-183-193 SPT B<br>1-183-193 SPT C<br>1-189-196 SPT A<br>1-189-196 SPT B<br>1-189-196 SPT B<br>1-193-203 SPT B<br>1-193-203 SPT A<br>1-193-203 SPT A<br>1-203-208 SPT A<br>1-203-208 SPT C<br>1-208-217 SPT C<br>1-208-217 SPT C<br>1-208-217 SPT D<br>1-217-227 SPT A<br>1-217-227 SPT B<br>1-227-236 SPT A | 0.030<br>0.026<br>0.028<br>0.028<br>0.053<br>0.053<br>0.053<br>0.046<br>0.035<br>0.035<br>0.039<br>0.020<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.030<br>0.030<br>0.043<br>1.083<br>1.033<br>0.043<br>1.083<br>1.033<br>0.043<br>1.033<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.043<br>0.045<br>0.045<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.035<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.035<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.020<br>0.035<br>0.039<br>0.020<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.0000<br>0.000<br>0.0000<br>0.0000<br>0.0000<br>0.000000 | 0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.000<br>0.000<br>0.000<br>0.000<br>0.001<br>0.019<br>0.001<br>0.001<br>0.025<br>0.003<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.001<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.0000<br>0.00000<br>0.00000<br>0.000000<br>0.00000<br>0.00000000 | AWAITING ASSAYS<br>AWAITING ASSAYS<br>AWAITING ASSAYS |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                | 0.028<br>0.026<br>0.028<br>0.046<br>0.027<br>0.040<br>0.183<br>0.065<br>0.039<br>0.000<br>0.032<br>0.030<br>0.435<br>0.397<br>0.477<br>0.047<br>0.045                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 0.001<br>0.001<br>0.001<br>0.001<br>0.005<br>0.002<br>0.001<br>0.001<br>0.001<br>0.013<br>0.012<br>0.014<br>0.001<br>0.001                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | AWAITING ASSAYS                                       |

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# TABLE 1 : SUMMARY OF RESULTS

CLIENT : INTERNATIONAL FOCUS

| 1                      | CALC.    | CALC.     |                 |
|------------------------|----------|-----------|-----------------|
|                        | HEAD     | HEAD      | COMMENT         |
| SAMPLE NUMBER          | ACCAV    | ASSAV     |                 |
|                        | ABOAL    | ( 07/+ )  |                 |
|                        | ( 3/ 5 ) | ( 02/ C ) |                 |
|                        |          | 0.001     |                 |
| 2-018-028 SPT C        | 0.043    | 0.001     |                 |
| 2-018-028 SPT D        | 0.051    | 0.001     |                 |
| 2-018-028 SPT E        | 0.046    | 0.001     |                 |
| 2-028-038 SPT A        | 0.121    | 0.004     |                 |
| 2-028-038 SPT B        | 0.365    | 0.011     |                 |
| 2-028-038 SPT C        | 0.042    | 0.001     |                 |
| 2-028-038 SPT D        | 0.042    | 0.001     |                 |
| 2-038-048 SPT A        | 0.038    | 0.001     |                 |
| 2-038-048 SPT B        | 0.037    | 0.001     |                 |
| 2-038-048 SPT C        | 0.037    | 0.001     |                 |
| 2-048-058 SPT A        | 0.043    | 0.001     |                 |
| 2-048-058 SPT B        | 0.031    | 0.001     |                 |
|                        | 0.035    | 0.001     |                 |
|                        | 0.047    | 0.001     |                 |
|                        | 0 049    | 0.001     |                 |
|                        | 0.023    | 0.001     | •               |
|                        | 0.023    | 0.006     |                 |
|                        | 0.135    | 0 007     |                 |
|                        | 0.649    | 0.007     |                 |
|                        | 0.020    | V 0 027   |                 |
| 2-088-098 8FT B        | 0.369    |           |                 |
| 2-088-098 SPT C        | 0.300    |           |                 |
| 2-098-108 SPI C        | 0.044    | 0.001     | 1               |
| 2-098-108 SPF D        | 0.053    | 0.002     |                 |
| 2-108-113 SFI A        | 0.039    | 0.001     | 1               |
| 2-108-113 SPT B        | 0.036    | 0.001     | }               |
| 2-113-117.5 SPT A      | 0.036    | 0.001     | 1               |
| 2-113-117.5 SPT B      | 0,048    | 0.001     |                 |
| 2-117.5-129 SPT A      | 0.022    | 0.001     |                 |
| 2-117.5-129 SPT B      | 0.025    | 0.001     |                 |
| <b>2-129-136</b> SPT A | 0.029    | 0.001     |                 |
| 2-129-136 SPT B        | 0.032    | 0.001     |                 |
| 2-136-143 SPT <b>A</b> | 0.043    | 0.001     |                 |
| 2-136-143 SPT B        | 0.039    | 0.001     | 1               |
| 2-136-143 SPT C        | 0.044    | 0.001     |                 |
| 2-136-143 SPT D        | 0.000    | 0.000     | AWAITING ASSAYS |
| 2-143-153 SPT A        | 0.030-   | 0.001     |                 |
| 2-143-153 SPT C        | 0.036    | 0.001     |                 |
| 2-153-163 SPT A        | 0.027    | 0.001     | 1               |
| 2-151-163 SDM 0        | 0.030    | 0.001     |                 |
| 2-167-162 COM N        | 0.028    | 0 001     |                 |
| 6-100-100 DEL U        | 0.086    | 0.002     |                 |
| 6-T02-T12 25. 4        | 1 4.463  | 1 0.002   | ŧ (             |

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# TABLE 1 : SUMMARY OF RESULTS

CLIENT : INTERNATIONAL FOCUS

| SAMPLE NUMBER                                                                                                                                                                                                                                       | CALC.<br>HEAD<br>ASSAY<br>(g/t)                                                                                            | CALC.<br>HEAD<br>ASSAY<br>( o2/t )                                                                       | COMMENT                                                                                               |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------|
| 2-163-173 SPT B<br>2-163-173 SPT C<br>2-163-173 SPT D<br>2-163-173 SPT D<br>2-163-173 SPT E<br>2-173-183 SPT A<br>2-173-183 SPT B<br>2-173-183 SPT C<br>2-183-189 SPT A<br>2-183-189 SPT A<br>2-196-208 SPT A<br>2-196-208 SPT C<br>2-208-216 SPT A | 0.439<br>0.116<br>0.039<br>0.085<br>0.109<br>0.132<br>0.000<br>0.035<br>0.035<br>0.037<br>0.054<br>0.037<br>0.085<br>0.022 | 0.013<br>0.003<br>0.001<br>0.003<br>0.004<br>0.000<br>0.001<br>0.001<br>0.001<br>0.002<br>0.001<br>0.002 | AWAITING ASSAYS                                                                                       |
| 2-208-216 SPT B<br>2-216-224 SPT A<br>2-216-224 SPT B<br>2-216-224 SPT C<br>2-224-232 SPT A<br>2-232-238 SPT B<br>2-232-238 SPT B<br>2-232-238 SPT C<br>2-238-248 SPT A<br>2-238-248 SPT B<br>2-238-248 SPT B                                       | 0.030<br>0.029<br>0.034<br>0.110<br>0.035<br>0.081<br>0.424<br>0.045<br>0.061<br>0.023<br>0.027<br>0.035                   | 0.001<br>0.001<br>0.003<br>0.001<br>0.002<br>0.001<br>0.002<br>0.001<br>0.002<br>0.001<br>0.001<br>0.001 |                                                                                                       |
| 2-248-258 SPT B<br>2-248-258 SPT C<br>2-248-258 SPT C<br>2-248-258 SPT D<br>2-258-261 SPT A<br>2-258-261 SPT B<br>2-261-274 SPT A<br>2-261-274 SPT B<br>2-261-274 SPT C<br>ACID TREATED                                                             | 0.038<br>0.038<br>0.042<br>0.478<br>0.321<br>0.035<br>0.046<br>0.024                                                       | 0.001<br>0.001<br>0.001<br>10.014<br>0.009<br>0.001<br>0.001<br>0.001                                    | AWAITING ASSAYS<br>AWAITING ASSAYS                                                                    |
| AW-1-060-070       SPT A1         AW-1-070-087       SPT A1         AW-1-070-087       SPT A2         AW-1-070-087       SPT B1         AW-1-070-087       SPT B1         AW-1-097-112       SPT A1         AW-1-097-112       SPT B1               | 0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000                                                                | 0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000<br>0.000                                              | IN PROGRESS<br>IN PROGRESS<br>IN PROGRESS<br>IN PROGRESS<br>IN PROGRESS<br>IN PROGRESS<br>IN PROGRESS |

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## TABLE 1 : SUMMARY OF RESULTS

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CLIENT : INTERNATIONAL FOCUS

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|-----------------|--------|-------|--------|----------------------------------------------------------------------------------------------------------------|
|                 |        | CALC. | CALC.  |                                                                                                                |
| SAMPLE NUMBE    | R      | HEAD  | HEAD   | COMMENT                                                                                                        |
|                 | -      | ASSAY | ASSAY  |                                                                                                                |
|                 |        | (a/t) | (oz/t) |                                                                                                                |
|                 |        |       |        |                                                                                                                |
| AW-1-097-112 S  | PT B2  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-127-140 8  | PT A1  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-147-156 S  | PT AL  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-147-156 S  | PT A2  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-156-165 S  | PT AL  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-165-175 S  | PT A1  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-208-217 S  | PT A1  | 0,000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-208-217 S  | PT A2  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-208-217 \$ | PT B1  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-208-217 S  | PT B2  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-227-236 S  | PT A1  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-1-236-246 5  | PT A1  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-038-048 5  | PT A1  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-068-078 S  | PT AL  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-068-078 S  | PT A2  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-078-088 S  | PT A1  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-078-088 5  | FT A2  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-098-108 S  | PT A1  | 0.000 | 0.000  | TN PROGRESS                                                                                                    |
| AW-2-098-108 S  | PT A2  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-098-108 S  | PT B1  | 0.090 | 0.000  | TN PROGRESS                                                                                                    |
| AW-2-098-108 S  | PT 82  | 0.000 | 0.000  | TN PROGRESS                                                                                                    |
| AW-2-108-113 S  | PT AI  | 0.000 | 0.000  | TN DROGRESS                                                                                                    |
| AW~2-117.5-129  | SPT C1 | 0.000 | 0.000  | TN DDOCDESS                                                                                                    |
| AW-2-117.5-129  | SPT C2 | 0.000 | 0.000  | TN PROGRESS                                                                                                    |
| AW-2-129-136 S  | PT C1  | 0.000 | 0.000  | IN PROCRESS                                                                                                    |
| AW-2-129-136 SI | PT C2  | 0.000 | 0.000  | TH PROGRESS                                                                                                    |
| AW-2-143-153 S  | DT BI  | 0.000 | 0.000  | TN DDOCREGG                                                                                                    |
| AW-2-143-163 g  | PT B2  | 0.000 | 0,000  | TH PROURESD                                                                                                    |
| AW~2~153-163 8  | PT R1  | 0.000 | 0.000  | TN DDOCDBCC                                                                                                    |
| AW-2-153-763 S  | DT R2  | 0.000 | 0.000  | TH PROGRESS                                                                                                    |
| AW-2-196-208 51 | PT AI  | 0.000 | 0.000  | IN PROGRESS                                                                                                    |
| AW-2-208-216 81 | וג דס  | 0.000 |        | IN PROGRESS                                                                                                    |
| AW-2-238-248 SI | DT A1  | 0.000 |        | IN PROGRESS                                                                                                    |
| AW-2-261-274 81 | DT 11  | 0.000 |        | IN PROGRESS                                                                                                    |
| CONTROL         |        | 0.000 |        | TH LKACKESS                                                                                                    |
| C-1-208-217 SI  | PTA    | 0.022 | 0,001  |                                                                                                                |
| C-1-208-217 S   | PTB    | 0.022 | 0.001  |                                                                                                                |
| C-2-078-082 SI  | PTÀ    | 0.073 | 0.001  | (                                                                                                              |
| C-2-098-108 SI  | PTA    | 0.025 | 0.001  | 1                                                                                                              |
| C-2~098-108 SI  | PT B   | 0.027 | 0.001  | ng in the second se |
|                 | /      |       |        |                                                                                                                |

TABLE 2 : TOTAL GOLD TEST RESULTS

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CLIENT : INTERNATIONAL FOCUS

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| 1 |               |           | 1  | SAMPLE | 50  | UTIC  | R.  | sour | TION | 150 | LUTION      | SOLDI       | ton        | SOLIDS | 6010      | GOLD   | TOTAL             |      | CALC.   | CAL   | Ċ.          | 1       |
|---|---------------|-----------|----|--------|-----|-------|-----|------|------|-----|-------------|-------------|------------|--------|-----------|--------|-------------------|------|---------|-------|-------------|---------|
| i | SAPPLE BUNKE  | R         | Ì  | NEIGHT | Į M | EJGHT | Ì   | MET  | GHT  | A   | SSAY        | ASSA        | Y          | ASSAY  | t N 🕴     | IN     | TOLD              | L I  | HEAD    | Her   | D           | COMMENT |
| I | :             |           | 1  |        | [PA | 55 #1 | p   | PASS | #2   | P.M | SS #1       | PASS        | #2         | 1      | SOLUT ION | SOLIDS | 1                 | 1    | ASSAY   | ASS   | AY          | 1       |
| 1 |               |           | ١  | (9)    | 15  | 9)    | ł   | ( 9  | 2    |     | (ppm)       | (pp         | m)         | (ppb)  | (2)       | 183    | (9)               |      | ( 1/2 ) | ( 02/ | 2)          | i       |
|   |               | ~ ~ ~ ~ ~ | -1 |        | · [ |       | - - | **** |      | 1   |             |             |            |        |           |        | -   + • • • • • • |      |         | }     |             |         |
| 1 |               |           | I  |        | 1   |       | 1   |      |      | ł   |             | 1           |            | 1      | 1         | [      | 1                 | 1    |         |       |             | l       |
| 1 | 1-022-034 SP  | t A       | I  | 3178.7 | 1   | 4000  | 1   |      |      | L   | 8.02        | 1           |            | 2      | 0.0001    | 0.0300 | 0.000             | 11   | 0.027   | 0.    | 001         | 1       |
| 1 | 1-022-034 SP  | ТВ        | 1  | 3792.1 | 1   | 4000  | 1   |      |      | 1   | 0.02        | 1           |            | 2      | 0.0001    | 0_0000 | 1 0.000           | n    | 0.023   | 0.    | 001         | ł       |
| 1 | 1-022-034 SP  | τc        | 1  | 2875.9 | I   | 4000  | ł   |      |      | 1   | 0.02        | 1           |            | 2      | 0.0001    | 6.0000 | 0.000             | n    | 0.030   | 0.    | 001         | Į.      |
| 1 | 1-034-039 SP  | T A       | 1  | 1849_4 | L   | 3000  | 1   |      |      | 1   | 0.02        | 1           |            | 2      | 0.0001    | 0.0000 | 0.000             | n j  | 0.034   | 0.    | 001         | l       |
| 1 | 1-034-039 SP  | ΥB        | 1  | 1566_8 | Ŧ   | 3000  | 1   | 1    | 000  | l   | 80.0        | 0.          | 02         | 2      | 0,0003    | 0.0000 | 1 0.000           | 13   | 0.168   | 0.    | 005         | 1       |
| ļ | 3-739-349 SP  | T A       | 1  | 2349.4 | 1   | 4000  | 1   | 1    | 000  | 1   | 0.02        | j 0.        | <b>3</b> 8 | 2      | 0.0002    | 0.0000 | 1 0.000           | 32   | 0.270   | 0.    | 200         | •       |
| 1 | 1-039-049 SP  | TB        | 1  | 2349.4 | 1   | 4000  | 1   | 1    | 000  | !   | <b>4.02</b> | <b>j</b> 0. | 92         | 2      | 0_0001    | 0.0000 | 0.000             | 1    | 0.045   | 0.    | 001         | 1       |
| 1 | 1-039-049 SP  | TC        | I  | 2583,4 | 1   | 4000  | 1   | 1    | 000  |     | 0.02        | 1 0.        | 02         | 2      | 0.0001    | 0.0000 | 1 0,000           | И    | 0.041   | Į D.  | 001         | 1       |
| 1 | 1-039-049 sp  | T D       | I  | 2399,4 | Ł   | 3500  | 1   | 1    | 000  | Ł   | 0.02        | [ 0.        | 02         | 2      | 0.0001    | 0.0000 | 0.000             | 11   | 0.040   | 0.    | 001         | 1       |
| 1 | 1-039-069 SP  | T E       | I  | 2387.4 | 1   | 3500  |     | 1    | 000  | 1   | 0.02        | į 0.        | 0Z         | 2      | 0.0001    | 0.0000 | 0.000             | 1    | 0.048   | 0.    | 001         | 1       |
| I | 1-046-060 SP  | ¥ A -     | ł  | 2409.4 | 1   | 3000  | 1   | T    | 000  | l   | 0.02        | 1 0.        | 02         | 3      | 0.0001    | 0.0000 | 1 0.000           | 1    | 0.036   | 0.    | 001         | 1       |
| 1 | 1-046-060 SP  | TB        | I  | 2349.4 | Ł   | 3000  | 1   | ļ    | 500  | I   | 0.0Z        | 0.          | 02         | 5      | 0.0001    | 0.0000 | 0.000             | n    | 0.035   | 0.    | 001         | 1       |
| ŀ | 1-046-060 SP  | T C       | 1  | 2399.4 | 1   | 3000  | 1   | 1    | 000  | 1   | 0.02        | 0.          | 02         | 2      | 0.0001    | 0.0000 | [ 0.000           | ומ   | 0.035   | 1 0.  | 001         | 1       |
| 1 | 1-046-060 57  | T D       | 1  | 2599,4 | I   | 3000  | Į   | 1    | 000  | 1   | 0.02        | 0.          | 02         | 2      | 0.0001    | 0.0000 | 0.00              | n    | 0.035   | 0.    | 001         | I       |
| Ļ | 1-046-060 SP  | T E       | 1  | 2399.4 | Ł   | 3000  | 1   | 1    | 000  | 1   | 0.02        | 0.          | 02         | 2      | 0.0001    | 0.0000 | 0.00              | n i  | 0,035   | 0.    | 001         | 1       |
| 1 | 1-060-070 SP  | T A       | }  | 1186.7 | 1   | 2000  |     |      |      | Ĺ   | 0.02        | ł           |            | 2      | 0.0000    | 6.0000 | 1 0.000           | 0    | 0.036   | 1 0.  | 001         |         |
| 1 | 1-960-070 57  | T B       | 1  | 1676.3 | 1   | 4000  | 1   |      |      | l   | 0.02        | t           |            | 2      | 0.0001    | 0.0000 | 1 0_000           | )1 - | 0.050   | [ 0.  | 001         | I       |
| 1 | 1-060-070 SP  | T C       |    | 2258.1 | I   | 4003  | 1   |      |      | I . | 0.02        | i           |            | 2      | 0_0001    | 0.0000 | 1 0.000           | И    | 0.037   | į 0.  | 001         | 1       |
| 1 | 1-070-087 SP  | T C       | 1  | 3466.0 | t – | 4000  | 1   |      |      | 1   | 0.02        | i i         |            | 3      | 0.0001    | 0.9000 | 0.000             | )1   | 0.026   | 0.    | 0 <b>D1</b> | 1       |
| 1 | 1-087-097 \$2 | Т.А.      | 1  | 2249.4 | 1   | 3000  | ł   | 10   | 000  | 1   | 0.02        | [ 0.        | .02        | 2      | 0.0001    | 0.0000 | 0.00              | 11   | 0.038   | 0.    | 001         | 1       |
| 1 | 1-087-097 SP  | T 8       | I  | 2249.4 | I   | 3000  | 1   |      | 500  |     | 0.02        | 0.          | .02        | 2      | 0.0001    | 0.0000 | 1 0.000           | n    | 0.033   | 0.    | 001         | i       |
| 1 | 1-087-097 SP  | TC        | Ī  | 2249.4 |     | 3000  | ł   | 1    | 000  | I   | 0.96        | 0.          | 02         | 1 8    | 0_0003    | 0.0000 | 1 0.000           | B    | 0.124   | 0.    | 004         | 1       |
| 1 | 1-087-097 SP  | t P       | 1  | 1849_4 | I.  | 3000  | 1   | 1    | 000  | l   | 0_02        | 1 0.        | <b>02</b>  | 2      | 0.0001    | 0.0000 | 1 0-000           | 1    | 0_045   | 0.    | 001         | 1       |
| ľ | 1-057-097 \$9 | T E       | 1  | 1487.6 | 1   | 3000  | 1   | 11   | 000  | 1   | 0.02        | 0.          | 92         | 2      | 0.0001    | 0.0000 | 0.000             | 1    | 0.056   | 0,    | 002         | 1       |
| ł | 1-097-112 SP  | T A       | ł  | 5922.8 | Į.  | 8006  | ł   |      |      | 1   | Ø_02        | l           |            | 2      | 0.0002    | 0.0000 | 0.00              | 12   | 0.029   | 0.    | 001         | 1       |

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TABLE 2 : TOTAL GOLD TEST RESULTS

CLIENT : INTERNATIONAL FOCUS

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| 1 |                    |          | SAMPLE | SOLUTION | SOLUTION     | SOLUTION | SOLUTION    | SOLIDS | 6010           | GOLD   | TOTAL    | CALC.   | CALC.    | s í             |
|---|--------------------|----------|--------|----------|--------------|----------|-------------|--------|----------------|--------|----------|---------|----------|-----------------|
| i | SANPLE             | HUMBER   | NEIGHT | HEIGHT   | WETGHT       | ASSAY    | ASSAY       | ASSAY  | IR             | IN     | GOLD     | HEAD    | HEAD     | COMMENT         |
| I |                    |          | 1      | PASS #1  | PASS #2      | PASS #1  | PASS #2     | 1      | SOLUTION       | SOLIDS | l        | ASSAT   | ASSAY    | I I             |
| 1 |                    |          | (e)    | [(0)     | (8)          | (ppm)    | (ppm)       | (ppb)  | (g)            | ( 2 )  | F ( @ )  | ( s/t ) | ( oz/t ) | E I             |
|   | - • • • • • • •    |          |        |          |              |          |             | {      |                |        | [        |         |          |                 |
| 1 | 1-112-1            | 20 SPT A | 3170.0 | 3000     | 1000         | 0_18     | 0_02        | 24     | 0.0006         | 0.0001 | 0.0006   | 0,201   | 0.006    |                 |
| l | 1-112-1            | 20 SPT B | 3170.0 | 3000     | 500          | 0.22     | 0_03        | 15     | 0.0007         | 0.0000 | 0.0007   | 0.236   | 0.007    | l I             |
| 1 | 1-112-1            | 20 SPT C | 3170.0 | 3000     | 500          | 0.21     | . 0.17      | 1 31   | 0.0007         | 0.0001 | 0.0005   | 0,27    | 0.007    |                 |
|   | 1-120-1            | 27 SPT A | 3116.8 | 4000     | I            | 0.02     |             | 2      | <b>D.00</b> 01 | 0.0000 | 0.0001   | 0.028   | 0,001    |                 |
| ł | 1-120-1            | 27 SPT B | 3511.4 | 4000     | 1            | I        | I           |        | 0.8000         | 0.0000 | 0.0000   | 0.000   | 0,000    | AMAITING ASSAYS |
|   | 1-127-1            | 40 SPT A | 1616.2 | 2000     | ]            | 1 0.02   | I           | 2      | 0.0000         | 0.0000 | 0.0000   | 0.027   | 0.001    |                 |
|   | <b>4 - 727</b> - 3 | 40 °P* 3 | 1205.7 | 4000     | -            | 1.32     | •           |        | 3,3001         | 9_0000 | 9.9001   | 9.926   | 0,001    |                 |
| i | 1-127-4            | au spi c | 3193.2 | 4000     | l.           | 0.82     | 1           | 2      | 0.0001         | 0.000  | 0.0001   | 0.027   | 0.001    |                 |
| I | 1-140-1            | 47 SPT A | 2349.4 | 3000     | 1000         | 0.02     | 0_32        | 2      | 0.0001         | 0.0000 | 0.0001   | 0.036   | 0.001    |                 |
| I | 1-140-1            | 47 SPT 8 | 2349.4 | 3000     | 1000         | 0.02     | 0_02        | 2      | 0.0001         | 0.0000 | 0.0001   | 0.036   | D.001    |                 |
| I | 1-140-1            | 47 SPI C | 2349.4 | 3000     | 1009         | 0.02     | 0_02        | 2      | 0.0001         | 0.0000 | 0.0001   | 0.036   | 0.001    |                 |
| [ | 1-147-1            | 56 SPT B | 2706.8 | 4000     | 1            | 0.02     | 1           | 2      | 0.0001         | 0.0000 | 0.0001   | 0.032   | 0.001    | 1               |
|   | 1-147-1            | 56 SPT C | 3333.7 | 4000     | 1            | 0.02     | 1           | 2      | 0.0001         | 0.0000 | 0.0001   | 0.026   | 0_001    | <b>I</b> [      |
| 1 | 1-156-1            | 65 SPT A | 1387.2 | 2000     | 1            | 0.02     |             | 2      | 0.0000         | 0.0000 | 0.0000   | 0.031   | 0,001    | <b>I</b>        |
| 1 | 1-156-1            | 65 SP18  | 2636.4 | 4000     | I            | 0.02     |             | Z      | 0.0001         | 0.0000 | 10.0001  | 1 0.032 | 0.001    | l .             |
| ł | 1-156-1            | 5 SPT C  | 2819.7 | 4000     | 1            | 0.02     | 1           | 2      | 0.0001         | 0.0000 | 0.0001   | 0.030   | 0.001    | <b>I</b>        |
| l | 1-165-1            | 75 SPT A | 1691.0 | 2000     | 1            | 0.02     | 1           | 2      | 0.0000         | 0.0000 | 0.0000   | 0.026   | 0.001    | 1               |
| 1 | 1-165-1            | 75 591 9 | 3122.0 | 4000     | 1            | 0.02     | 1           | 2      | 0.0001         | 0.0000 | 1 0.0001 | 0.028   | 0_001    | 1               |
| 1 | 1-165-1            | 75 SP1 C | 3060.6 | 4000     | 1            | 0.02     | 1           | 2      | 0.0001         | 0.0000 | 100010   | 0.025   | 0.001    | I I             |
| ł | 1-175-1            | 83 SP1 A | 1649.4 | 3000     | 1000         | 0.02     | 0.02        | 2      | 1000.0         | 0_0000 | 10001    | 0.051   | 0_001    | 1               |
| 1 | 1-175-1            | 83 591 8 | 1649.4 | 3000     | 1000         | 0.02     | <b>0.02</b> | ( 2    | 0.0001         | 0.0000 | 0.0001   | 0.051   | 0_001    | E i             |
| • | 1-175-1            | 83 SPT C | 1503.4 | 3000     | ( . 500      | 0.02     | [ 0.02      | 1 7    | 0.0001         | 0.0000 | [ 0.0001 | 0.066   | 0_001    |                 |
| 1 | 1-185-1            | 93 SP1 A | 3410.0 | 4009     | 1000         | 0.02     | 0.03        | 3      | 0.0001         | 0.0000 | 10.0001  | 0.035   | 0_001    | 1 1             |
| 1 | 1-183-1            | 93 SPT 8 | 3410.0 | 4000     | <b>10</b> 00 | 0.02     | J 0.04      | 4      | 0.0001         | 0.0000 | 100001   | 0.039   | 0,001    | 1 1             |
| ł | 1-183-1            | 93 SPT C | 3410.0 | 4000     | 1000         | 0.02     | 0.01        | 2      | 1 0.0001       | 0.0000 | 0.0001   | 0.025   | 0_001    | 1               |
| 1 | 1-189-1            | 96 SPT A | 3079.0 | 3000     | 1            | t        | 1           | 1      | 0.0000         | 0.0000 | 0_0000   | 0.000   | 0.000    | AWAITING ASSAYS |

TABLE 2 : TOTAL DOLD TEST RESULTS

CLIENT : INTERNATIONAL FOCUS

| 1  |          |                |          | I   | SHIPLE           | ţs  | OLUTION | ı įs | iolan Ion | SOLUTION | SOLUTION     | (SOLIDS | GOLD     | GOLD           | TOTAL    | I  | CALC_         | ŧ     | CM.C.  | <b>[</b>        | 1 |
|----|----------|----------------|----------|-----|------------------|-----|---------|------|-----------|----------|--------------|---------|----------|----------------|----------|----|---------------|-------|--------|-----------------|---|
| Ī  | SMPLE    | NUMBER         |          | Ì   | VELCHT           | 1   | WEIGHT  | Ì    | LEIGHT    | ASSAY    | ASSAY        | ASSAY   | 1 2N -   | 1 13           | COLD     | İ  | HEAD          | İ     | NEND   | COMNENT         | Ì |
| İ  |          | :              |          | I   |                  | 1P  | ASS #1  | 12   | ****      | PASS #1  | PASS #2      | I       | SOLUTION | SOLIDS         | i        | Ì  | ASSAY         | Ī     | ASSAY  | 1               | İ |
| İ  |          |                |          | ſ   | ( <del>a</del> ) | Ł   | (2)     | I    | ( a )     | (ppm)    | (ppm)        | (Cppb)  | ( )      | (2)            | (1)      | 10 | g/t 3         | ic    | oz/t > | 1               |   |
| Į  |          |                |          | -1- |                  | -1- |         | -    |           | Į        | <b>}</b>     | 1       | ]        | ]              | 1        | -  |               | - 1 - |        | ]               | l |
| I  | 1-189-19 | 76 SPT         | 8        | I   | 3079.0           | t   | 3009    | L    |           | ł        | {            | Į       | 0.0000   | 0.000          | 0.0000   | I  | 0_000         | ۱     | 0_000  | AVAITING ASSAYS | l |
| 1  | 1-189-15 | 76 SPT         | 3        | ł   | 3079_0           |     | 3000    | ł    |           | l        | 1            | 1       | 0.0000   | 0_2008         | 0.0000   | t  | 0.000         | ſ     | 0,000  | AWAITING ASSAYS | ł |
| 1  | 1-193-21 | <b>15 SPT</b>  | A        | 1   | 2749_4           | ł   | 4000    |      | 1000      | 0.02     | 1 0.02       | 3       | 0.0001   | 0.0000         | 0.0001   | 1  | 9.039         | ł     | 0.001  | 1               | I |
| 1  | 1-193-20 | 13 SPT         | B        | 1   | 2749.4           | l   | 4000    | ł    | 1000      | 0.40     | 0.02         | 50      | 0.0016   | 0.0001         | 0.0018   | ł  | 0.539         | 1     | 0.019  | 1               | l |
| i  | 1-195-20 | ns spi         | C .      | 1   | 2762.6           | 1   | 4000    | I    | 1000      | 0.02     | 0.04         | 1 2     | 1 0.0001 | 0.0000         | 0.0001   | 1  | 0.045         | I     | 0,001  | I               | Į |
| Ł  | 1-203-20 | 18 SP1         | A        | 1   | 2000.0           | 1   | 2500    |      | 1000      | 0.73     | <b>0.3</b> 3 | 7       | 0.0022   | 9.0000         | 0.0022   | I  | 1.085         | ļ     | 0.032  | [               | l |
| Ł  | 1-203-20 | DE SPT         | 8        | I   | 2000_3           | 1   | 2500    | I    | 2000      | 0.59     | 0.33         | 136     | 3. MAR   | 1.0703         | , 07965. | Ţ  | 1_0 <b>30</b> | ţ     | 3,370  | ŧ               | 2 |
| 1  | 1-203-21 | 98 SPT         | C        | i.  | 1909.5           | i   | 2500    | l    | 1000      | 0.51     | 1 0.25       | ] 55    | ] 0.0015 | 0.0001         | 0.0016   | 1  | J.J64         | ì     | 0.025  | 1               | 1 |
| 1  | 1-208-21 | 17 <b>SPT</b>  | C        | I   | 2249.6           | t   | 3000    | I    |           | 0_08     |              | 1 2     | 9,0092   | 0.0000         | 0,0002   | ſ  | 0.109         | i     | 9,903  | 1               | Ĩ |
| 1  | 1-208-21 | 1 <b>7 SPT</b> | D        | ł   | 2149_6           | I   | 3000    | ſ    | 1000      | 50.0     | 0.02         | 1 2     | 0.0001   | <b>0.00</b> 00 | 0.0001   | ŧ  | 0,039         | 1     | 0.001  | l .             | I |
| ł  | 1-217-22 | 17 <b>SPT</b>  | <b>A</b> | 1   | 2859.8           | l   | 4000    | I    |           | 0.02     | ł            | 1 5     | 0.0001   | 0.0000         | 0.0001   | 1  | 0.030         | I     | 0_001  | <b>!</b>        | 1 |
| 1  | 1-217-22 | 27 <b>SPT</b>  | B        | t   | 3890.0           | 1   | 4000    | I    |           | 0.02     | t            | 1 2     | 0.0001   | 0.0000         | 0.0001   | I  | 0.023         | ł     | 0.001  | 1               | ł |
| 1  | 1-227-23 | 56 <b>SPT</b>  | 8        | ł   | 1729.3           | ſ   | 2000    | 1    | :         | 0-05     | 1            | 2       | 0.0000   | 0.0300         | 0.0000   | Ì  | 0.025         | Î     | 0.001  | 1               | Ì |
| I  | 1-227-23 | 6 SPT          |          | [   | 3520.0           | E   | 4000    | ł    | !         | 0_02     | 1            | 1 5     | 0.0001   | 0.0000         | 0.0001   | İ. | 0.028         | Ì     | 0_001  | 1               | ł |
| 1  | 1-227-23 | 16 SPT         | C        | 1   | 3361.2           | ſ   | 4000    | ŧ    |           | 0.02     | 1            | 1 Z     | 0.0001   | 0.0000         | 0.0001   | Ĺ  | 0.026         | Ì     | 0.001  | 1               | ĺ |
| I  | 1-256-26 | 6 SPT          | A        | 1   | 1533.8           | 1   | 2000    | 1    |           | 0.02     | ſ            | { 2     | 0.0000   | 0.0000         | 0.0000   | Ì  | 0.028         | Ī     | 0.001  | 1               | ĺ |
| ĺ. | 1-236-24 | 6 SPT          | 8        | 1   | 3728.6           | l   | 4000    | Į.   | I         | 0.02     | ļ            | 25      | 0.0001   | 0.0001         | 3-000Z   | 1  | 0.046         | Ì     | 0_001  | }               | ł |
| 1  | 1-236-24 | 6 SPT          | C        | 1   | 3225.3           | I   | 4000    | i    |           | 0.02     | <b>j</b>     | 1 2     | 0.0001   | 0.0000         | 0.0001   | Ē  | 0.027         | t     | 0.001  | 1               | l |
| 1  | 1-266-25 | ið spt         | A        | 1   | 2369.4           | I   | 3500    | l    | 1000      | 0.02     | 0,02         | 1 2     | 0.0001   | 0.0000         | 0.0001   | l  | 0_040         | Ì     | 0.001  | 1               | ľ |
| 1  | 1-246-25 | <b>i6 SPT</b>  | 8        | 1   | 2369.4           | L   | 3500    | ţ    | 1003      | 0.10     | 0.08         | 2       | 0.0004   | 0.000          | 0.0004   | I  | 0.183         | I     | 0.005  | l .             | 1 |
| 1  | 1-246-25 | ig spt         | С        | F   | 2369.4           | I   | 3500    | Ł    | 1000      | 0.02     | 0.08         | 1 2     | 0.0002   | 0.0000         | 1 0.0002 | ŧ  | 0.065         | ł     | 0,002  | }               | İ |
| 2  | 1-246-25 | ig spt         | D        |     | 2407.2           | Ł   | 3500    | 1    | 1000      | 0.02     | 0.02         | 2       | 0.0001   | 0.0000         | 0,0001   | 1  | 0.039         | 1     | 0.901  | 1               | ł |
| 1  | 1-256-26 | ið spt         | A        | 1   | 3318.6           | ł   | 4000    | I    |           | 1        | 1            | 1       | 0.0000   | 0.0000         | 0.0000   | I  | 0.000         | ſ     | 0.000  | ANALTING ASSAYS | l |
| 1  | 1-256-26 | 6 SPT          | 8        | 1   | 3468.5           | Ł   | 4000    | L    |           | 50-05    | !            | 1 9     | 0.0001   | 0.0000         | 0.0001   | I  | 0.032         | ł     | 0.001  | 1               | I |
| ł  | 1-256-26 | ig spt         | C        | 1   | 2823.8           | I   | 4000    | ł    |           | 0.02     | 1            | 2       | 0.0001   | 60000          | 0.0001   | ł  | 0.039         | 4     | 0,001  | 1               | l |
| 1  | 1-266-27 | 76 <b>SP</b> T |          | 1   | 2500.0           | ì   | 2500    | ۱    | 1000      | 0.28     | 0.25         | 55      | 0.0010   | 0.0001         | 0,0011   | ł  | 0.435         | 1     | 0.013  | 3               | 1 |

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### : TOTAL GOLD TEST RESULTS TABLE 2

: INTERNATIONAL FOCUS **CLIENT** 

| 1 | ~                 | SAMPLE    | SOLUTION | 150LUTION | SOLUTION | SOLUTION | SOLIDS | 0100     | COLD                                      | TOTAL               | CALC.    | CALC.           | 1       |
|---|-------------------|-----------|----------|-----------|----------|----------|--------|----------|-------------------------------------------|---------------------|----------|-----------------|---------|
| 1 | SAMPLE MURBER     | MEIGHT    | L NETCHI | HEIGHT    | ASSAY    | ASSAY    | ASSAT  | f in i   | NI JR                                     | ເພນ                 | HEAD     | HEAD            | COMMENT |
| 1 |                   |           | PASE #1  | PASS #2   | PASS #1  | PASS #2  | t      | SOLUTION | SOLIDS                                    | ]                   | ASSAY    | ASSAY           | [       |
| 1 |                   |           | i(g)     | (g)       | (ppm)    | (ppm)    | (ppb)  | (9)      | (9)                                       | [(g)                | )( 9/t ) | ( oz/t )        | }       |
|   |                   | 1         | 1        |           |          | 1        | 1      |          |                                           |                     | 1        |                 |         |
| 1 | 1-266-276 SPT B   | 2500.0    | 2500     | 1000      | 0.24     | 0.25     | 57     | 0.0009   | 0.0001                                    | 1 0.0010            | 0_397    | 0,012           | 5       |
| ł | 1-266-276 SPT C   | 2559.4    | 2500     | 1000      | 0.41     | 0.17     | 10     | 0.0012   | 0.0000                                    | 0.0012              | 0.477    | 0_014           | l       |
| ł | 2-018-028 SPT A   | 2351.6    | 1 4000   | 1000      | 1 0.02   | ; 0.02   | 1 4    | 0.0001   | 0.0000                                    | 0.0001              | 0.047    | 0.001           | 1       |
| 1 | 2-018-028 SPT 8   | 2351.6    | 4000     | 1000      | 0.02     | 0.02     | 2      | 0.0001   | 0.0000                                    | 0.0001              | 0.045    | 0.001           |         |
| 1 | 2-018-028 SPT C   | 2449.6    | 4000     | 1 1000    | 1 0.02   | 0.02     | 2      | 0_0001   | 0_8000                                    | 0.8001              | 0.043    | 0_001           | 1       |
|   | 2-018-028 SPT D   | 1 1779.4  | 1 3009   | 1 1000    | 0.02     | 0.02     | 1 6    | 1 3.0001 | 0,3000                                    | 1 0.0001            | 0.051    | 2 0.001         |         |
|   | 2-010-028 SPT F   | 1 1854.2  | 3000     | 1000      | 56.1     | 9.02     | 1 2    | 1005.6   | م درمین می می از ا<br>م استفاد می می از ا | 1 10004<br>1 100055 | 1.040    | 9.401           | 1       |
|   | 2-0128-0138 SOT & | 1 2199.4  | i 3080   | 1000      | 1 0.08   | 0.02     | 3      | 0.0003   | 1 0.0000                                  | 0.0003              | 0.121    | 0.004           | 1       |
|   | 2-028-038 597 8   | 1 2199.4  | 1 3000   | 1000      | 1 0.17   | 0.27     | 1 10   | 8000_0   | 0.0000                                    | 1 0.0008            | 0.365    | 0_911           | 1       |
|   | 7-028-038 SPT C   | 1 2059.4  | 3000     | 1000      | 1 0.02   | 0.02     | 1 3    | 0.0001   | 0.0000                                    | 0.0001              | 1 0.042  | } 0.001         | l l     |
|   | 2-028-058 SPT D   | 2069.4    | 3000     | 1000      | 1 0.02   | 0.02     | 3      | 0.0001   | 1 0.0000                                  | 0.0001              | 0.042    | 0.001           | 1       |
|   | 2-020-008 SPT A   | 1123.2    | 2000     | i         | 0.02     | i        | 2      | 0.0000   | 0.0000                                    | 0.0000              | 0.038    | 0.001           | 1       |
| - | 2-038-048 SPE 8   | 2262.5    | 4000     | ;         | 0.02     | i        | 1 2    | 0.0001   | 1 0.0000                                  | 0.0001              | 0_037    | 0.001           | 1       |
|   | 2-030-040 JFT 6   | 2817 1    | 1 4000   | 1         | 0.02     | i        | 1 2    | 1 0.0001 | 0.0000                                    | 0.0001              | 0.037    | 0.001           | 1       |
| 1 | 2-030-040 SPL 6   | 1 3/40 4  | 1 3000   | 1 500     | 0.02     | 0.08     | 1 2    | 0.0001   | 0.0000                                    | 0.0001              | 1 0.043  | j 0 <b>.001</b> | 1       |
|   |                   | 1 2440 4  | 1 3000   | 1 500     | 1 0.02   | 1 0.02   | 1 2    | 0,0001   | 0.0000                                    | 0.0001              | 0.031    | 0.001           |         |
|   |                   | 1 2447 44 | 1 3000   | 1 2000    | 1 0.02   | 1 0.02   | 1 2    | 0.0001   | 0.0000                                    | 0.0001              | 0,035    | 0_001           | 1       |
|   | 2-068-038 571 6   | 1 7740 4  | 1 4000   | 1 9000    | 1 0.02   | 0.02     | 1 4    | 10.0001  | 0.0000                                    | 0.0001              | 1 0.047  | 0.001           | 1       |
|   | 2-035-068 591 8   | 1 2/02 8  | 1 4000   | 1 1000    | 1 0.02   | 1 0.02   | 1 6    | 0.0001   | 0.0000                                    | 0.0001              | 1 0.048  | 0.001           | 4       |
|   | 2-030-068 SPI 8   | 1 3735.3  | 1 4000   | 1 1000    | 0.02     | 1        | i 2    | 0.0001   | 0.0000                                    | 0.0001              | 0.023    | 0.001           | 1       |
|   | 2-000-070 5P1 9   | 1 4320 L  | 1 3000   | 1 1000    | 0.08     | 6.02     | 2      | 1 0.0003 | 0.0000                                    | 0.0003              | 0.195    | 0.006           | 5       |
|   | 2-010-000: 571 0  | 1 1144 5  | 1 3000   | 1 1000    | 1 0.05   | 1 0.02   | 2      | 0.0003   | 0.0000                                    | 9.0003              | 1 0.229  | 0.007           | 1       |
|   |                   | 1 2510 4  | 1 2500   | 1 1000    | 0.53     | 0.25     | 73     | 1 0.0016 | 0.0002                                    | 0.0018              | 0.698    | 1 0.020         | 1       |
| - |                   | 1 2400 A  | 1 2500   | 1 500     | 0.75     | 0.50     | 78     | 0.0021   | 0.0002                                    | 0.0023              | 1 0.928  | 0.027           | !       |
| 1 |                   | 1 2588 4  | 1 2500   | 1 1000    | 0,31     | 1 0.08   | 1 50   | 1 0.0009 | 1 0.0001                                  | 0.0010              | 0.380    | 0.011           | 1       |
|   | 2-000-095 371 0   | 1 1011 4  | 1 2000   | 1 1000    | 1 0.00   | 0.02     | 2      | 1 0.0001 | 1 0.0000                                  | 1 0.0001            | 0.044    | 0.001           | 1       |
|   | 2-970-108 SPT C   | 1 1711-4  | ູ້ລາກຄຸ  | 1 1000    | 1        | - 1      |        |          |                                           | •                   | •        | -               | -       |

### TABLE 2 : TOTAL GOLD TEST RESULTS

CLIENT : INTERNATIONAL FOCUS

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| t  |           |           | SANPLE |                | SOLUT ION | SOLUTION | SOLUTION | SOLIDS | { GOLD   | 60LD   | TOTAL          | CALC.           | CALC.        | <b>I</b>        |
|----|-----------|-----------|--------|----------------|-----------|----------|----------|--------|----------|--------|----------------|-----------------|--------------|-----------------|
| Ì  | STIPLE    | NUMBER    | VEIGHT | MEIGHT         | SEIGHT    | ASSAY    | ASSAY    | ASSAT  | ] ]]]    | 214    | GOLD           | READ            | HEND         | CONHENT         |
| Ì. |           |           | Ì      | PASS #1        | PASS #2   | ipass in | PASS #2  | 1      | SOLUTION | SOLIDS | 1              | ASSAT           | ASSAY        | 1 1             |
| 1  |           |           | (g)    | ( 8 )          | 1(g)      | (ppm)    | (ppm)    | (ppb)  | (3)      | (2)    | ( g )          | ( s/t )         | ( oz/t )     | 1 1             |
| 1  |           |           | *      | 1              |           |          |          |        |          |        | •••••          |                 |              | {               |
| 1  | 2-098-10  | B SPT D   | 1576.1 | 3000           | 1000      | j 0.02   | 0.02     | 2      | 1000.0   | 0.0000 | 102020         | 0.053           | 0.002        | 1 1             |
| l  | 2-108-11  | 3 SPT A   | 1087.1 | 2000           | 1         | I 0.02   | 1        | [ 2    | 0.0000   | 0.0000 | 0.0000         | 0_039           | 0.001        | 1 1             |
| ł  | 2-108-11  | 3 SPT 8   | 2352.6 | 4000           | 1         | 9,02     | 1        | 2      | 0.0001   | 0.0000 | 0.0001         | 0.036           | 0_001        | f i             |
| 1  | 2-113-117 | LS SPTA   | 2349.6 | 3000           | 1000      | 0.02     | 0.02     | [ 2    | 0.0001   | 0.0000 | 0_0001         | 0.036           | 0_001        | 1 1             |
| I  | 2-113-117 | 15 SPT #  | 1728.2 | 3000           | 1000      | 0.02     | 0.02     | 2      | 0_0001   | 0.0000 | 0.0001         | 0,048           | 8.001        | 1 1             |
| 1  | 2-117.5-1 | 29 SPT A  | 4048.7 | 4000           | 1         | 0.02     |          | 2      | § 0.0001 | 0_0003 | 0.0001         | 0.022           | 3.001        | 1<br>0          |
| 1  | 2-117.5-1 | 29 SPT a  | 3546.7 | 4000           | 1         | 0.02     | 1        | į 2    | 0.0001   | 9.0000 | 0.0001         | 0.025           | 1.301        | : 1             |
| I  | 2-129-13  | 6 SPT A   | 2934.8 | 4000           | 1         | 0.02     | 1        | 2      | 0.0001   | 0.0000 | <b>0.0</b> 001 | 0.029           | 0.001        | 1 1             |
| ł  | 2-129-13  | 6 SPT B   | 2684.0 | 4000           | 1000      | 0.02     | 1        | 2      | 0.0001   | 0.0000 | 0.0001         | 0.032           | 0.001        | 1 1             |
| ł  | 2-136-14  | 3 SPT A   | 1969.4 | 3000           | 1000      | 0.82     | 0.02     | 2      | 0.0001   | 0.0000 | 0.0001         | 0.063           | 0.001        | 1 1             |
| 1  | 2-136-14  | 3 SPT B   | 2149_4 | 3000           | 1000      | 0.02     | 0.02     | ] 2    | 0.0001   | 0.0000 | 1 0.0001       | 0.039           | 0.001        | 1               |
| 1  | 2-136-14  | 3 SPTC    | 1969.4 | 3000           | 1000      | 0.02     | 0.02     | 3      | 0,0001   | 9.0000 | 0.0001         | 1 0.044         | 0.001        | 1 1             |
| F  | 2-136-14  | 3 SPTD    | 1899.4 | 3000           | 1 1000    | 1        | 1        | ŧ –    | 0.0000   | 0.0000 | 0.0000         | 0.000           | <b>608.0</b> | AWAITING ASSAYS |
| 1  | 2-143-15  | 3 SPT A   | 3220.9 | 4000           | 1         | 0.02     | 1        | 1 5    | 0.0001   | 0.0000 | 1000.0         | <b>j 0.03</b> 0 | 0.001        | 1 1             |
| 1  | 2-143-15  | 3 SPTC    | 3678.7 | 4000           | 1         | 0.03     | l        | 2      | 0.0001   | 0.8000 | 0.0001         | 0.036           | 0.001        | I I             |
| 1  | 2-153-16  | 3 SPT A   | 3281.6 | 4000           | 1         | 0.02     | 1        | 3      | 0.0001   | 0_0000 | 0.0001         | 0.027           | 0.001        | 1 1             |
| 1  | 2-153-16  | 3 SPTC    | 3019.9 | 4000           | 1         | 0.02     | 1        | 4      | 0.0001   | 0_0000 | D.0001         | 0.030           | 6,001        | 1               |
| 1  | 2-153-16  | 3 SPT D   | 3172.2 | 4008           | 1         | 0.02     | ŧ        | 3      | 0.0001   | 0.0000 | 0.0001         | 0.028           | 0.001        | 1 1             |
| L  | 2-163-17  | 3 SPT A   | 2309.4 | 3008           | 1000      | 0.02     | 0.02     | [ 51   | 0.0001   | 0.0001 | 0.0002         | 0.086           | 0.002        | 1 1             |
| l  | 2-163-17  | 3 SPIB    | 2309.4 | <b>j 300</b> 0 | 1000      | 0.33     | 0.02     | 2      | 0.0010   | 0.0000 | 0.0010         | 0.439           | 0.013        | 1               |
| Ł  | 2-163-17  | 3 SP1 C   | 2309.4 | 3000           | 0001      | 0.05     | 0.02     | 3      | 0.0003   | 8.0000 | 2000.0         | 0.116           | 0.003        | 1 1             |
| 1  | 2-163-17  | 3 SPT 0   | 2149.4 | 3000           | 1008      | 50-0     | 9.02     | 2      | 0.0091   | 0.0000 | 0.0001         | 0.039           | 0.001        | 1               |
| 1  | 2-163-17  | 3 SPT E   | 952.1  | 3000           | 1000      | 50.0     | 0.02     | 2      | 0.0001   | 0.0000 | 10.0007        | 0.086           | 0.003        | 1               |
| t  | 2-175-18  | 5 SPT A 1 | 3369.2 | 4000           |           | 0.09     | t        | 2      | 0.0094   | 0.0000 | 0.0004         | 0.109           | 0.003        | 1 1             |
| L  | 2-175-18  | 3 SPT 8   | 3139.4 | 4000           | !         | 6_07     | ł        | 43     | 0,0003   | 0.0001 | 0.0004         | 1 0.132         | 0.004        | 1 1             |
| 1  | 2-173-18  | 3 ѕартс   | 3726.6 | 4000           | 1         | 1        | (        | 1      | 9.0000   | 0.0000 | 0.0000         | 0.000           | 0,000        | ANAITING ASSAYS |

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|   |                 |        |     |          |          |           |          |                  |          |          |                         |           |                 | **************** | -        |
|---|-----------------|--------|-----|----------|----------|-----------|----------|------------------|----------|----------|-------------------------|-----------|-----------------|------------------|----------|
|   |                 | SIN    | LE  | SOLUTION | SOLUTION | (SOLUTION | SOLUTION | <b>1501.10</b> 5 | 0010     | GOLD     | TOTAL                   | CALC.     | CALC.           | 1                | 1        |
| 1 | SANPLE NUMBER   | I VEIC | II. | WEIGHT   | NETCHT   | ASSAY     | ASSAY    | ASSAY            | i ini    | L KK     | SOLD                    | MEAD      | MEAD            | COMMENT          | 1        |
|   |                 | I      |     | PASS #1  | PASS #2  | PASS #1   | PASS #2  | Ī                | SOLUTION | SOLIDS   | }                       | ASSAT     | ASSAY           | 1                | 1        |
| } |                 | 1 ( 9  | >   | ( ( ) )  | (8)      | (ppm)     | (ppm)    | (ppb)            | (9)      | (2)      | (9)                     | ( =/1 )   | C oz/t )        | 1                | 1        |
|   |                 |        |     |          | <b>{</b> |           | <b>}</b> |                  |          |          |                         |           | i               |                  | ł        |
|   | 2-183-189 SPT A | 2399   | 2.4 | 3000     | 1000     | 0.02      | 0.02     | 2                | 0.0001   | 0.0000   | 0.0001                  | 9.035     | 0_001           | ł                | 1        |
|   | 2-183-189 SPT B | 2399   | -4  | 3000     | 1000     | 0.02      | 0.02     | 4                | 0.0001   | 0.0000   | 0.0001                  | 0.037     | 0.001           | 1                | 1        |
| ł | 2-196-208 BPT A | 1 1531 | .2  | 2000     | l        | 0.04      | 1        | 1 2              | 10.0001  | 0.0000   | 0.0001                  | 0.054     | 0.002           |                  | )        |
|   | 2-196-208 SPT B | 2637   | .9  | 4000     | 1        | 0.02      | I        | 7                | 0.0001   | 0.0000   | 0.0001                  | 0_037     | 0.001           | 1                | I        |
|   | 2-196-208 SPT C | 2901   | .5  | 4000     | 1        | 80.5      | 1        | 2                | 0.0002   | 0.0000   | 0.0002                  | 0.085     | 0.002           | 1                | [        |
|   | 2-208-216 SPT A | 202    | 8.1 | 2000     | 1        | 0.02      | 1        | 2                | 0.0000   | 1 0.0000 | 9.0000                  | 0.022     | 1 0_001         |                  | 1        |
| l | 2-208-216 SPT B | 3262   | .1  | 4000     | 1        | 1 0.02    | ]        | 5                | 1 0.0000 | 1.00     | <b>0.</b> 07 <b>0</b> * | ] ] 37320 | ] <b>3.</b> 357 | 1                | i        |
| 1 | 2-216-224 SPT A | 2800   | 10  | 3000     | 500      | 0.02      | 0.02     | 4                | 0.0001   | 0.000    | 0.0001                  | 0.029     | 0.001           | 1                | 1        |
| } | 2-216-224 SPT B | 2500   | .0  | 3000     | 1 1000   | 0.02      | 0.02     | 1 2              | 1 0.0001 | 0.0000   | 0.0001                  | 0.034     | 0.001           | 1                |          |
| ĺ | 2-216-224 SPT C | 287    | .5  | 3000     | 1 1000   | 0.02      | 0,20     | 20               | 0.0003   | 0_0001   | 0.0003                  | 0_110     | 0.003           | 1                | 1        |
|   | 2-224-232 SPT A | 2399   | 7,4 | 3000     | 1000     | 0_02      | 0.02     | 2                | 0.0001   | 0.0008   | 1000.0                  | 0.035     | 0.001           | 1                | 1        |
|   | 2-224-232 SPT 8 | 2399   | -4  | 3000     | 1000     | 0_02      | 0_08     | 23               | 0.0001   | D.0001   | 0.0002                  | 0.081     | 0.002           | 1                | 1        |
|   | 2-232-238 SPT A | 1849   | .4  | 3000     | 1000     | 0.02      | 0.02     | 381              | 0.0001   | 0.0007   | 0.0008                  | 0.424     | 0.012           |                  | 1        |
| ! | 2-232-238 SPT B | 1 1845 | .4  | 3000     | 1000     | 50.0      | 0.0Z     | 2                | 0.0001   | 0.0000   | 0.0001                  | 0.045     | 0.001           | 1                | I        |
|   | 2-232-238 SPT C | 1359   | 4   | 3000     | 1000     | 0.02      | 0.02     | 2                | 0.0001   | 0.0000   | 10.0001                 | 0.061     | 0.002           | 1                | I        |
|   | 2-238-248 SPT A | 1863   |     | 2000     | 1        | 0.02      | 1        | 2                | 0.0000   | 0.0000   | 0.0000                  | 0.023     | 0.001           | ŧ                | L        |
|   | 2-238-248 SPT B | 3223   | 3.  | 4000     | 1        | 0.02      | 1        | 1 2              | 0.0001   | 0.0000   | D.0001                  | 0.027     | 0.001           | 1                | Ł        |
|   | 2-248-258 SPT A | 2349   | -4  | 3000     | 1003     | 0.02      | 0.02     | 1 2              | 100010   | 0.0000   | 0.0001                  | 0.036     | 0.001           | 1                | 1        |
|   | 2-248-258 SPT 8 | 2345   | .4  | j 3000   | 1000     | 0.02      | 0.02     | [ 4              | 0_0001   | 0.000    | 1 0.0001                | 820.0     | 0.001           | 1                | l        |
|   | 2-248-258 SPT C | 2265   | 1.4 | 3000     | 1000     | 0.02      | 0.02     | 2                | 1 0,0001 | 0.0000   | 0.0001                  | 0.038     | 0_001           | 1                | 1        |
|   | 2-248-258 SPT D | 1995   | 4   | 3000     | 1000     | 0.02      | 0.02     | 1 2              | 0.0001   | 0.0000   | 0.0001                  | 0.042     | 0_001           | t                | Į        |
|   | 2-258-261 SPT A | 1284   | -0  | 1500     | 1000     | 0.35      | 0.02     | 54               | 0.0005   | 0.0001   | 0.0006                  | 0.478     | 0.014           | 1                | 1        |
|   | 2-258-261 SPT B | 1280   | .0  | 1 1500   | 1000     | 0.26      | 50.0     | 2                | 0.0004   | 0.0000   | 0.0004                  | 0.321     | 0.009           | Į                | <b>!</b> |
|   | 2-261-274 SPT A | 1465   | 1.5 | 2000     | 1        | 0.02      | I        | 9                | 0.0000   | 0.0000   | 0.0001                  | 0.036     | 0.031           | 1                | Į        |
|   | 2-261-274 SPT 8 | 3442   | L1  | 200A 5   | ł        | 0_04      | 1        | 1                | 0.0002   | 0.0000   | 2000.0                  | 0.046     | 0.001           | AUAITING ASSAYS  | 1        |
|   | 2-261-274 SPT C | 3265   | .9  | 4000     | \$       | 1 0,02    | 1        | 1                | 0.0001   | 0000.0   | 100001                  | 1 0.026   | 0.001           | AUAITING ASSAYS  | 1        |

CLIENT : INTERRATIONAL FOCUS

THELE 2 : TOTAL GOLD TEST RESULTS

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TABLE 2 : TOTAL GOLD TEST RESULTS

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| ł |                    | ( SANPLE   | <b> SOLUTI</b> O  | N SOLUTION | SOUTION | SOLUTION | SOLIDS | GOLD          | GOLD   | TOTAL   | CALC.       | CALC.    |             | 1  |
|---|--------------------|------------|-------------------|------------|---------|----------|--------|---------------|--------|---------|-------------|----------|-------------|----|
| I | SAMPLE NUMBER      | [ WEIGHT   | WEIGHT            | WE I GHT   | ASSAY   | ASSAY    | ASSAY  | IN            | 3M     | GOLD    | HEAD        | KEAD     | COMMENT     | 1  |
| 1 |                    | ŧ          | PASS #1           | PASS #2    | PASS #1 | PASS #2  | 1      | SOLUTION      | SOLIDS | 1       | ASSAY       | ASSAY    |             | 1  |
| 1 |                    | [ ( g )    | (g)               | (2)        | (ppm)   | (ppm)    | (ppb)  | (9)           | (g)    | (9)     | ( g/t )     | ( oz/t ) | l           | 1  |
| ŀ |                    | [          | •   • - • • • • • | -          |         |          |        |               |        |         |             |          |             | -1 |
| I | ACID TREATED       | }          |                   |            | ł       | 1        | 1      | {             | ļ      | 9       |             |          | l           | 1  |
| ł | AU-1-060-070 SPT A | it         | 1                 |            | [       |          | I      | 0.0000        | 0.0000 | 0.0000  | I 1         | 0,000    | IN PROGRESS | ł  |
| ł | AW-1-070-087 SPT / | 1   2517.1 | 2000              | 1          | 1       | 1        | 1      | 0.0000        | 0.0000 | 0.00000 | 0.000       | 0.000    | IN PROGRESS | I  |
| l | AN-1-070-087 SPT A | 2   1996.2 | 2000              | 1          | 1       | l        | ł      | 0,0000        | 0.000  | 0.0000  | 0.000       | 0.000    | IN PROGRESS | I  |
| I | AN-1-070-087 SPT 8 | 1 2323.8   | 2000              | 1          | 1       | ŧ        | 1      | 0.0000        | 0.0000 | 0.0000  | 0.000       | 0.000    | IN PROGRESS | I  |
| 1 | AN-1-070-087 SPT E | 2   2518.5 | 2000              | 1          | 1       | [        |        | 0.0000        | 0.0000 | 0,0000  | 0.000       | 0.000    | IN PROGRESS | -  |
| I | AN-1-097-172 SPT # | 11         | 1                 | 1          | 1       | 1        | 1      | 0.0000 (      | 9,0000 | 0.0000  | 4           | 9,000    | IN PROGRESS | ľ  |
| ŧ | AN-1-097-112 SPT 8 | 1   1820.0 | 2000              | 1          | 1       | i        | )      | <b>0.0000</b> | 0.0000 | 0.0000  | 1 0.000     | J.000    | 14 PROGRESS | ł  |
| ł | AN-1-097-112 SPT 8 | 2   1353.6 | 2000              | 1          | 1       | 2        | 1      | 0_0000        | 8,0000 | 0.0000  | 0.000       | 0,000    | IN PRODRESS | 1  |
| ł | AW-1-127-140 SPT / | 1          | ]                 | 1          | 1       | 1        | 1      | 9.0000        | 0.0000 | 0.0000  | 1           | 0.000    | IN PROGRESS | 1  |
| ļ | AV-1-147-155 SPT / | 1 1768.2   | 2000              | 1          |         | 1        | l      | 0_0000        | 0.0000 | 0.0000  | 0.000       | 0.000    | IN PROGRESS | 1  |
| ŧ | AV-1-147-156 SPT / | 2   1064.6 | 2000              | 1          | 1       | 1        | !      | 0.0000        | 0.0000 | 0.0000  | 0.000       | 0.000    | IN PROGRESS | 1  |
| I | AV-1-156-165 SPT A | 1          | I                 | l          |         | 1        | ļ      | 0.0000        | 9.0000 | 0.0000  | 1           | 0_000    | IN PROGRESS | 1  |
| ł | AV-1-165-175 SPT A | 1          | I                 | 1          | 1       | 1        | 1      | 0.0000        | 0.0000 | 0.0000  | 1           | 0_000    | IN PROGRESS | ł  |
| ł | MI-1-208-217 SPT A | 1   455.6  | 1000              | ł          | 1       | 1        | ł      | 0.0000        | 0.0000 | 0.0000  | 0.000       | 0.000    | IN PROGRESS | 1  |
| Ł | M-1-208-217 SPT A  | 2   473.9  | 1000              | 1          | 1       | l        | Į      | 0.0000        | 0.0000 | 0.0000  | 0.000       | 0,600    | IN PROGRESS | ł  |
| 1 | AM-1-208-217 SPT 8 | 1 466.0    | 1000              | 1          | 1       | 1        | 1      | 0.0000        | 0.0000 | 0.0000  | <b>0.00</b> | 0.000    | IN PROGRESS | 1  |
| ł | AV-1-208-217 SPT 8 | 2   474.5  | 1000              | 1          | 1       | 1        | I      | 0.0000        | 0.0000 | 0.0000  | 0.000       | 0.000    | IN PROGRESS | ł  |
| I | AV-1-227-236 SPT A | 1          | 1                 | 1          | I       | 1        | 1      | 0.0000        | 0.0000 | 0.0000  | 1           | 0.000    | IN PROGRESS | 1  |
| 1 | AV-1-236-246 SPT A | 1          | 1                 | 1          | 1       | 1        | I      | 0.0000        | 9.0000 | 0.0000  | 1           | 0.000    | IN PROGRESS | 1  |
| 1 | AV-2-038-048 SPT # | s (        | 1                 | 1          | I .     | 1        | 1      | 0.0000        | 0.0000 | 0.0000  | 1           | 0.000    | IN PROGRESS | 1  |
| 1 | MI-2-068-078 SPT A | 1   1879_7 | 2000              | 1          | 1       | 1        | 1      | 0.0000        | 0.0000 | 0_0000  | 0.000       | 0.000    | IN PROGRESS | 1  |
| ł | MI-2-068-078 SPT A | 2   1968_2 | 2000              | 1          | 1       | 1        | t      | 0.0000        | 0.0000 | 0.0000  | 0.000       | 0_000    | IN PROGRESS | 1  |
| ł | AN-2-078-085 SPT A | 1   457.1  | 1000              | t          | I       | 1        | 1      | 0.0000        | 0.0000 | 0.0000  | 0,000       | 0.000    | IN PROGRESS | 1  |
| 1 | AV-2-078-088 SPT A | Z   465.3  | <b>100</b> 0      | E          | 1       | 1        | 1      | 0.0000        | 0,0000 | 0.0000  | 0.000       | 0.000    | IN PROGRESS | I  |
| Ł | AV-2-098-108 SPT A | 1 460_4    | 1000              | I I        | 1       | 1        | 1      | 0.0000        | 0.0000 | 0.0003  | 0.000       | 0.000    | IN PROGRESS | I  |

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TABLE 2 : TOTAL GOLD TEST RESULTS

CLIERT : INTERNATIONAL POCUS

|   | SAMPLE NUMBER         | SKOPLE<br>VENGRT | (SOLUTION<br>VEIGHT | Solution<br>Height<br>Mass #2 | (SOLUTION<br>  ASSAY<br> MASS #1 | (SOLUTION<br>  ASSAT<br> PASS #2 | SOL FDS<br> ASSAY<br> | ( 201.0  <br>  IN  <br>  SOLUTION | GOLD<br>IN<br>SOLIDS | TOTAL<br>GOLD   | CALC.  | CALC.<br>HEAD<br>ASSAY | i<br>Conhent | 1   |
|---|-----------------------|------------------|---------------------|-------------------------------|----------------------------------|----------------------------------|-----------------------|-----------------------------------|----------------------|-----------------|--------|------------------------|--------------|-----|
| Ī |                       |                  | (0)                 | (2)                           | (ppra)                           | (ppm)                            | (ppb)                 | ( 1 )                             | (9)                  | (8)             | (g/t)  | ( oz/t )               | 1            | 1   |
| 1 |                       |                  |                     |                               |                                  |                                  | Į                     |                                   |                      |                 |        |                        |              | - ] |
| 1 | AH-2-098-108 SPT A2   | 467.7            | 1000                | 1                             | 1                                | J                                | E .                   | 0.0000                            | 9.0000               | 0.0000          | 0.000  | 0.000                  | IN PROGRESS  | Ì   |
| 1 | AN-2-098-108 SPT 81   | 463.7            | 1000                | 1                             | 4                                | !                                | I                     | 0.0000                            | 0.0000               | 0.0000          | 10.000 | 0.000                  | IN PROGRESS  | ł   |
| l | AV-2-098-108 SPT 82   | 455.8            | 1 1008              | 1                             | 1                                | )                                | i                     | 0.0000                            | 0.0000               | 0.0000          | 0.000  | 0.000                  | IN PROGRESS  | 1   |
| l | AV-2-108-113 SPT A1   | 1                | 1                   | 1                             | ł                                | 1                                | l                     | 0.0000                            | 0.0000               | 0.0000          | 1      | 0.000                  | IR PROGRESS  | 1   |
| l | AN-2-117.5-129 SPT C1 | 1514.3           | 2000                | t                             | 1                                | 1                                | 1                     | 0.0000                            | 8_0000               | 0.0000          | 0.000  | 0.000                  | IN PROGRESS  | I   |
| ۱ | #1-2-117.5-129 SPT C2 | 1710.0           | 2000                | 1                             | 1                                |                                  | ł                     | 0.0000                            | 0.0000               | 0.0000          | 0.000  | 0.000                  | IN PROGRESS  | 1   |
| 1 | AN-2-129-136 SPT C1   | 1447.5           | 2000                | ļ                             |                                  | 1                                |                       | 0.0000                            | 9.0000               | 3 <b>3,9000</b> | 3,300  | ] <b>3.</b> 200        |              | i   |
| I | AN-2-129-136 SP1 C2   | 1883.0           | 2000                | 1                             | 1                                | 1                                | 1                     | 0.0000                            | 0_0000               | 0.0000          | 0.000  | 0.000                  | IN PROGRESS  | 1   |
| l | AH-2-143-153 SPT 81   | 1837.4           | 2000                | 1                             | 1                                | I                                | 1                     | 0.0000                            | 0.0000               | 1 0.0000        | 0.000  | 0.000                  | IN PROGRESS  | Į   |
| Į | AN-2-143-153 SPT 82   | 1 1527.6         | 1 2000              | 1                             | t i                              | I                                | 1                     | 0.0000                            | 6,0000               | 0.000           | 0.000  | D.000                  | IN PROGRESS  | I   |
| I | AV-2-153-163 SPT \$1  | 1693.4           | 2000                | ł                             | 1                                | I                                | 1                     | 0.0000                            | 0.0000               | 0.0000          | 0_800  | 0.000                  | IN PROGRESS  | l   |
| 1 | AH-2-153-163 SPT 82   | 1341.1           | 2000                | 1                             | l                                | 1                                | 1                     | 0.0000                            | 0.0000               | 0.0000          | 0.000  | 0,000                  | IN PROSNESS  | 1   |
| l | AH-2-196-208 SPT A1   | t                | 1                   |                               | I                                | 1                                | I                     | 0.0000                            | 0.0000               | 0.0000          | l      | 1                      | IN PROGRESS  | l   |
| 1 | AU-2-208-216 SPT A1   | 1                | 1                   | 1                             | 1                                | 1                                | }                     | 0.0000                            | 0.0090               | 0.0000          | Į      | !                      | IN PROGRESS  |     |
| 1 | AN-2-238-248 SPT A1   | 1                | l                   | [                             | 1                                | 1                                | 1                     | 0.0000                            | 0.0090               | 0_0000          | 1      | 1                      | IN PROGRESS  |     |
| I | AN-2-261-274 SPT A1   | 1                | 1                   | 1                             |                                  | 1                                | 1                     | 0.0000                            | 0.0000               | 0.0000          | 1      | l                      | IN PROGRESS  | 1   |
| 1 | C-1-208-217 SPT A     | 1000_8           | 1000                | 1                             | 0,02                             | 1                                | 2                     | 0.0000                            | 0.0000               | 0.0000          | 0-055  | 9,601                  | 1            | I   |
| 1 | C-1-208-217 SPT B     | 1008_8           | 1000                | 1                             | 0.02                             | 1                                | 1 2                   | 0.0000                            | 0.0000               | 0.0000          | 0_022  | 0.001                  | 1            | l   |
| l | C-2-078-082 SPT A     | 1000_0           | 1000                | 1                             | 0.07                             | 1                                | 3                     | 10.0001                           | 0.0000               | 0.0001          | 0.073  | 0.002                  | 1            | 1   |
|   | C-2-098-108 SPT A     | 862.6            | 1 1000              | 1                             | 0.02                             | 1                                | 2                     | a.2000 [                          | 4_0000               | 0.0000          | 0.025  | ( 0_001                | 1            | 1   |
| ł | C-2-098-108 SPT B     | 785.1            | 1000                | 1                             | 0.02                             | 1                                | 1 2                   | 0.0000                            | 0.0000               | 0.0000          | 0.027  | 0.001                  | 1            | 1   |