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### 1.0 INTRODUCTION

This report describes the 1990 Exploration Program on the Pelican Property, Iskut River Area of northwestern British Columbia. The field portion of the program was completed during the period August 14 -September 14, 1990. Aim of the program was to locate goldbearing mineralized structures through geophysical and geochemical surveys as well as geological mapping and prospecting. Previous work by Lonestar (1983), Western Canadian (1987), Cathedral Gold Corporation (1988) and Aerodat (1989) had outlined several target areas to focus exploration on. To prepare for the 1990 program a camp was constructed in the central portion of the property. Grids were laid out on several of the target areas. These grids consisted of lines spaced every 100 m and marked by wooden pickets every 25 m . The geophysical section of this report was written by Mr. Roger Caven, Consulting Geophysicist. Mr. Caven conducted or supervised all of the geophysical surveys.

## 20 LOCATION, ACCESS, TOPOGRAPHY

The Pelican Property is located in the Iskut River Area of northwestern British Columbia on NTS map sheet $104 \mathrm{~B} / 10 \mathrm{~W}$.

The property is located along branches of Snippaker Creek approximately 16 km southeast of the Bronson Airstrip currently servicing the Cominco/Prime Snip Project.

Access to the property is by aircraft from either Smithers ( 320 km ), Terrace ( 280 km ) or Wrangell, Alaska ( 80 km ) to one of three airstrips: Bronson, Johnny Mountain or Snippaker airstrip. The Snippaker airstrip is located along Snippaker Creek 1 km east of the Pelican Property. This strip is still in use but has not been maintained and can be used only by small aircraft. The Bronson airstrip has now been upgraded to enable large aircraft to land. Access to the property is by helicopter from either of the three airstrips. An alternative access route is by helicopter from the Bobquin airstrip - Highway Maintenance camp located along the Stewart-Cassiar Highway, 50 km to the east.

The property occurs within the Coast Range Mountains which are characterized by rugged, steep, glaciated terrain. Elevations on the property range from 600 m to 2300 m above sea level. The upper elevations are marked by ice caps and valley glaciers. The southwestern



PLATE 1 Pelican Camp looking NW towards Sericite Ridge and SJ Zone
portion of the property is marked by extremely rugged relief with many areas only accessible with mountain climbing gear. Movement about other portions of the property although time consuming is not overly difficult.

Vegetation ranges from thick alder growth along the valley bottoms to alpine grasses along the ridge tops. Stunted ( $1 \mathrm{~m}-3 \mathrm{~m}$ ) spruce trees cover the slopes to most ridges.

### 3.0 CLAIM INFORMATION

The Pelican Property is comprised of 11 claim blocks totalling 188 units. The claims are located on NTS map sheet $104 \mathrm{~B} / 10 \mathrm{~W}$ in the Liard Mining Division. The property has been divided into the following groups for assessment purposes:

TABLE 1
Claim Information - Pelican Property
GROUP 1

| Claim Name | Units | Record No. | Recording <br> Date | Year of Expiry |
| :---: | :---: | :---: | :---: | :---: |
| Gossan 1 | 20 | 2378 | August 12/82 | 1994 |
| Gossan 2 | 20 | 2379 | August 12/82 | 1993 |
| Gossan 3 | 20 | 2394 | August 12/82 | 1993 |
| Gossan 6 | 20 | 2397 | August 24/82 | 1999 |
| Gossan 7 | $\underline{20}$ | 2398 | August 24/82 | 1993 |
| 100 units |  |  |  |  |

GROUP 2

| Claim Name | Units | Record No. |  | Recording <br> Date | Year of <br> Expiry |
| :--- | :---: | :---: | :---: | :--- | :--- |
| Gossan 4 | 20 | 2395 |  | August $24 / 82$ | 1993 |
| Gossan 5 | 20 |  | 2396 |  | August $24 / 82$ |



The Pelican Property was staked by Mr. Chris Graf in 1982-83 as part of his Gossan Claim Group. In 1985, Western Canadian Mining Corporation signed an option agreement with Mr. Graf whereby Western Canadian could earn a $60 \%$ interest in the Gossan Property. In August 1988, Cathedral Gold Corporation signed an option agreement whereby Cathedral Gold Corporation could earn Western Canadian's $60 \%$ interest in two separate portions of the Gossan Property. One of these portions is now called the Pelican Property. In 1990 an agreement was signed with Cross Lake Minerals whereby Cross Lake Minerals could earn an interest in the Pelican Property.

### 4.0 EXPLORATION HISTORY

Mineral exploration in the area dates back to 1907 with the discovery of mineralization near Johnny Mountain. Since then the area has undergone sporadic episodes of mineral exploration for both precious metals and base metals. One such period was in the 1960-1970s when several of the prominent large gossans were examined as possible copper porphyry targets. One such gossan examined occurs on the ridge abounding the property to the north and east (Sericite Ridge Gossan). This large gossan was first explored by Great Plains Development in 1972. Subsequent work was done by Teck Corporation and Lonestar Resources Ltd. This work included geological mapping, soil geochemical surveys and silt geochemical surveys. Exploration in the area of the Pins Showing located in the southern portion of property was first recorded in 1972 by Cobre Explorations. This work consisted of prospecting, geological mapping, soil geochemical surveys, magnetometer surveys and ground electromagnetic surveys.

The present Pelican Property was staked in 1982-82 by Mr. Chris Graf as part of the larger Gossan Property which extended a further 10 km to the northwest. In 1983, Lonestar Resources Ltd. completed an extensive regional mapping, silt sampling and soil sampling program over the entire Gossan Property.

In 1987, Western Canadian completed a geological mapping, soil sampling and silt sampling program over portions of the Pelican Property.

In 1988, Cathedral Gold completed a rock chip sampling-prospecting program during which 237 rock chip and 383 soil samples were taken. The results returned from this program
include: 0.5 m wide quartz vein the area within the present Southeast Grid which returned a gold value of $6,205 \mathrm{ppb}$, a float sample from the Snow Grid area which returned $11,025 \mathrm{ppb}$ Au and mineralized float near the Pelican Grid samples of which returned gold values of up to $2,895 \mathrm{ppb}$ Au.

In 1989, Aerodat Ltd. was contracted to complete an airborne electromagnetic and magnetometer survey over the entire property. This survey outlined several electromagnetic and magnetic anomalies worthy of follow-up.

### 5.0 REGIONAL GEOLOGY

### 5.1 Introduction

Past geological mapping in the area by Kerr $(1948)$ and Grove $(1971,1986)$ is currently being revised and updated by both the Federal and Provincial governments (Anderson, 1989); (Britton et.al, 1990). Although this work is not yet finished there is now a clearer understanding of the geology of the area.

The Iskut map area is located near the boundary of the Intermontane Belt and the Coast Plutonic Complex. Anderson (1989) has proposed four tectonostratigraphic assemblages to define the geology of the area:

1. Tertiary Coast Plutonic Complex
2. Middle-Upper Jurassic Bowser Assemblage
3. Triassic-Jurassic volcanic-plutonic arc assemblage
4. Paleozoic Stikine Assemblage

The Pelican Property is underlain by rocks belonging to Triassic-Jurassic volcanic-plutonic arc assemblage within $5-10 \mathrm{~km}$ of the Coast Plutonic Complex.

### 5.2 Triassic-Jurassic Volcanic-Plutonic Arc Assemblage

The Triassic-Jurassic Volcanic-Plutonic Arc Assemblage has been divided into the following stratigraphic units:



a) Upper Triassic Stuhini Group
i) Eastern Facies
ii) Western Facies
b) Lower Jurassic Hazelton Group
i) Unuk River Formation
ii) Betty Creek Formation
iii) Mount Dilworth Formation
c) Lower and Middle Jurassic Salmon River Formation

A brief description of the above stratigraphic units follow:
a) Stuhini Group
i) Eastern Facies:

This facies grades to the northeast from a largely intermediate to mafic tuff sequence to a sequence containing abundant greywackes and siltstone. This facies lacks the thick limestone and felsic tuff units of the western facies.
ii) Western Facies:

This facies consists of a lower unit of limestone and conglomerate which changes towards the east to a largely feldspathic greywackesiltstone unit at Bronson Creek. This sedimentary unit is overlain by a bimodal volcanic suite consisting of volcanic breccia, limestone and felsic tuff. Overall the character of the sequence becomes more sedimentary towards the east.
b) Hazelton Group
i) Unuk River Formation:

This formation consists of andesitic breccias and lavas which grade into siltstones, conglomerates and greywackes west of the Bowser River.
ii) Betty Creek Formation:

This formation contains volcanic-siltstone, greywacke, conglomerate and breccia. A maroon colour characterizes this formation.
iii) Mount Dilworth Formation:

Consisting of felsic tuff, tuff breccia and dust tuff. This unit represents the final episode of Hazelton volcanism.
c) Salmon River Formation

The formation contains a basal calcareous sandstone unit overlain by one of three north trending facies:
i) East - Troy Ridge Facies:

Siltstone shale, tuff turbidite
ii) Central - Eskay Creek Facies:

Pillowed lava, limy to siliceous shale and siltstone
iii) West - Snippaker Mountain Facies:

Andesitic volcaniclastics

### 5.3 Intrusives

The northwestern area of British Columbia is characterized by four episodes of intrusive activity:

| Hyder Suite | (Tertiary) | $44-46 \mathrm{My}$ |
| :--- | :--- | :---: |
| Three Sisters Suite | (Middle Jurassic) | $175-180 \mathrm{My}$ |
| Texas Creek Suite | (Early Jurassic) | $189-196 \mathrm{My}$ |
| Stikine Suite | (Late Jurassic) | $213-226 \mathrm{My}$ |

These episodes appear to be coeval with volcanic rocks of the Stuhini Group, Hazelton Group and Salmon River Formation. The composition of plutons, associated with the various intrusive episodes are as follows:


After Anderson and Bevier (1990)

INSTRUSIVE SUITES ISKUT RIVER AREA

Hyder Suite (Tertiary) - monzogranite, quartz monzonite and granodiorite with minor monzodiorite and microdiorite dykes.

Three Sisters Suite (Middle Jurassic) - Plutons of this age have not yet been recognized in the Iskut River area.

Texas Creek Suite (Early Jurassic) - a) calc-alkaline quartz monzodiorite and granodiorite characterized by widespread chlorite-epidote alteration, b) alkaline syenite often associated with gold and porphyry copper-gold deposits.

Stikine Suite (Late Jurassic) - gabbro, diorite, and quartz monzonite.

### 5.4 Structure

Detailed structural studies within the Iskut area have not yet been done. Extensive deformation is essentially limited to the Paleozoic strata whereas Mesozoic units are for the most part flatlying. Faults fall into northwesterly, northeasterly and north-south sets. These faults are the most part steep-angled. Recent mapping in the area has also suggested that flatlying faults often occur between rock units of differing competency.

### 6.0 ECONOMIC GEOLOGY - REGIONAL

## 6.1 "Golden Triangle" - NW British Columbia

The mineral deposits of the area can be divided into four main classes: vein, porphyry/disseminated, stratabound massive sulphide and skarn. High-grade gold-quartz-base metals veins are by far most abundant type of deposit and have constituted the main exploration target until recently. Recent exploration programs on porphyry targets such as the Kerr property and several properties in the Galore Creek area as well as exploration programs for massive sulphide targets such as Eskay Creek have significantly widened the scope of exploration.


Figure 7. Distribution of ore deposits within a stratovotcano (modified from Branch, 1976).

TABLE 2
CHARACTERISTICS OF SELECTED DEPOSITS IN THE 'GOLDEN TRIANGLE'

| DEPOSTT | DEPOSTI TYPE | HOST <br> FORMATION | NEARBY INTRUSIVE | MINERALOGY | TRACE ELEMENTS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| SNIP | VEIN | STUHIN GP. | MONZODIORITE | PYRITE | AU |
|  | (SHEAR) | UPPER | -MONZONITE | PYRRHOTTTE | AG |
|  | 120/60SW | TRIASSIC |  | SPHALERITE | ZN |
|  |  | SILTSTONE- | TEXAS CK | ARSENOPY. | CU |
|  |  | WACKE | SUTTE | GALENA | PB |
|  |  |  |  | MOLYBDENITE | BI |
|  |  |  |  | CHALCOPY. | CD |
|  |  |  |  |  | AS |
|  |  |  |  |  | SB |
|  |  |  |  |  | HG |



| STONEHOUSE | VEIN | SIMILIAR | SIMILIAR | PYRITE | AU |
| :---: | :---: | :---: | :---: | :---: | :---: |
| -JOHNNY | 065 | TO INEL | TO INEL | CHALCOPY. | AG |
| MTN. |  |  |  | SPHALERITE | CU |
|  |  |  |  | GALENA | PB |
|  |  |  |  |  | ZN |
| SILBACK. | VEINS | UNUK RIVER | PORPH. | PYRITE | AU |
| PREMIER | STOCKWORK |  | DACITE | SPHALERITE | AG |
|  | BRECCIA |  | GRANODIORITE | CHALCOPY. | CU |
|  |  | andesite |  | TETRAHED. | PB |
|  | MAIN-050 | DACITE |  | Galena | ZN |
|  | WEST-290 | FLOWS,TUFFS, |  | ARSENOPY. | AS |
|  |  | BRECCIAS |  | PYRRHOTITE |  |


| DEPPOSTT | DEPOSTT TYPE | HOST FORMATION | NEARBY INTRUSIVE | MINERALOGY | TRACE ELEMENTS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| MCLYMONT | VEIN AND | MISS. OR | QUARTZ | PYRITE | AU |
| NORTHWEST | MANTOS | PERMIAN | SYENITE | SPHALERITE | AG |
|  | REPLACEMENT | SANDSTONE | AT DEPTH | GALENA | CU |
|  | $?$ | CHERT |  | CHALCOPY. | PB |
|  | SKARN ? | MARBLE |  | BARITE | ZN |
|  |  |  |  |  | AS |
|  |  |  |  |  | BA |
|  |  |  |  | GYPSUM | SB |
|  |  |  |  | MAGNETITE | SB |
|  |  |  |  | TETRAHED. | BI |
| ESKAY | STRATABOUND | MOUNT | FELDSPAR | PYRITE | AU |
| CREEK | MASSIVE | DILWORTH | PORPH. | SPHALERITE | AG |
|  | SULPHIDES | SALMON |  | GALENA | PB |
|  |  | RIVER |  | ARSENOPY. | ZN |
|  | VEINS | LOWER TO |  | STIBNITE | CU |
|  | STOCKWORK | MIDDLE |  | CINNABAR | AS |
|  |  | JURASSIC |  | TERAHED. | SB |
|  |  |  |  | ORPIMENT | HG |

The vein deposits occur at a variety of stratigraphic levels from the Permian/Mississippian (e.g. McLymont Creek) to the lower Middle Jurassic (e.g. Eskay Creek). With the exception of the Eskay Creek, which is now believed to be at least in part a massive sulphide deposit, the deposits do not appear related to specific stratigraphic horizons but several do appear to be related to Early Jurassic intrusions (Texas Creek Suite) (Premier, Kerr, Inel, Snip). In Table 2 some characteristics of several vein deposits are listed.

### 6.2 Bronson Trend

In the Iskut Gold Camp gold mineralization has been discovered within a NW-SE trending corridor approximately 2 km in width extending from Cominco/Prime's Snip deposit to Cathedral Gold's Pelican Property. Mineralized zones discovered to date include:
a) Snip (Twin Zone) - Cominco/Prime
b) Bronson Creek and Bonanza West - Placer Dome/Skyline
c) S and T Zones - Cathedral Gold Corporation/Ecstall Mining
d) AK Zone - Gulf International
e) Khyber - Vector Industries International/Graf
f) SJ - Cathedral Gold Corporation/Ecstall Mining

The above mineralized zones all trend NW-SE and appear to have similar mineralogy: gold, pyrite, pyrrhotite, sphalerite, chalcopyrite, galena, calcite and quartz.

THe information and data on this corridor obtained to date is insufficient as to why this corridor should be the focus of these mineralized zones. However it seems quite likely that additional exploration will uncover additional gold mineralization within the corridor.

A few kilometres southwest of the "Bronson Trend" workers in the area have mapped a major fault, the Sky Fault, which parallels the "Bronson Trend". The Sky Fault may have some economic significance in that no substantial mineralization has been found west of the Sky Fault.


PLATE 2 Bronson Trend - Looking NW from Pelican Property towards Brinco's Pyramid and Khyber Zones


### 7.0 PROPERTY GEOLOGY

### 7.1 Introduction

The volcanic and sedimentary rocks on the property were divided into the following lithological units by Lonestar Resources (1984):
a) Black Argillite Unit (BA)
b) Banded Siltstone Unit (BS)
c) Green Volcanic Unit (GB)

Alldrick et al (1990) in their recent geological mapping of the area have mapped most of the volcanic-sedimentary rocks on the property as belonging to the Jurassic Hazelton Group with the exception of the area south of the Sky Fault and west of "Southeast" Creek where they mapped the rocks as belonging to the Triassic Stuhini Group.

Lonestar Resources (1984) divided the intrusive rocks on the property into five suites:
a) Granodiorite-Diorite
b) Orthoclase Porphyry
c) Felsite Dykes
d) Coast Range Batholith
e) Alkali Basalt Dykes

Alldrick et al (1990) defined the following intrusive episodes in the immediate area of the property.
a) Triassic hornblende diorite dykes and plugs associated with adjacent Triassic volcanics.
b) Jurassic hypabyssal stocks and plutons. They include the Lehto Batholith, which underlies much of the northeastern portion of the property, within this intrusive category. Other stocks of this type have been mapped on the Johnny Mountain, Snip, Inel and Khyber properties and there is evidence that the significant mineralization occurring on these properties is directly related to these intrusives. The orthoclase porphyry plugs and dykes mapped on the Pelican property would be included in the above intrusive type.
c) Felsite, basaltic, andesitic sills and dykes.


### 7.2 Rock Types

### 7.2.1 Volcanic - Sedimentary

### 7.2.1.1 Black Argillite Unit (BA)

This unit is the lowermost litho-stratigraphic unit and is largely restricted to the area of the Pins Ridge in the southern part of the property. The unit consists of black, generally well bedded argillite.

### 7.2.1.2 Banded Siltstone Unit (BS)

This unit overlies the Black argillite unit and consists of thinly bedded siltstone with thin (1 to 3 cm ) alternating bands of finer and coarser material giving the unit a distinctly banded appearance. Occasional 1-3m horizons of greywacke occur.

### 7.2.1.3 $\quad$ Green Volcanic Unit (GB)

This unit overlies the Banded Siltstone Unit and consists of andesitic to basaltic pyroclastics and breccias. The unit characteristically has a green colour.

One should not that Alldrick et al (1990) have mapped some of volcanics in the Pins-SnowLake area of the property as "Premier" Porphyry. Such rocks have been mapped near several of the significant deposits of the "Golden Triangle".

### 7.2.2 Intrusive Rocks

### 7.221 Granodiorite-Diorite

These rocks occur as small stocks and dykes throughout the property. These rocks are generally fine to medium grained and occasionally magnetic.

### 7.2.22 Orthoclase Porphyry

The term "orthoclase porphyry" was first termed by J. Kerr (1948) to describe the distinctive porphyritic intrusive occurring throughout the Iskut area. This intrusive is characterized by very large orthoclase phenocrysts ( $1-3 \mathrm{~cm}$ ). Such intrusives are often associated with sericitization and pyritization both within the intrusive. Such alteration is most common with the smaller bodies.

### 7.2.23 Felsite and Alkali Basalt Dykes

Light coloured fine grained siliceous dykes have been mapped on Sericite Ridge but have not been mapped on the Pelican Property.

Very dark coloured basalt dykes up to 2 m thick have been mapped on the property, although few in number. The dykes are fine grained and magnetic.

### 7.3 Alteration

### 7.3.1 $\quad$ Sericite Alteration

Sericite-pyrite alteration largely occurs within the Banded Siltstone Unit associated with shears and over much larger areas along Sericite Ridge. The intensity of alteration and the amount of disseminated pyrite varies.

Such alteration is less commonly found within the Green Volcanic Unit although Western Canadian (1987) mapped an area of sericite-altered volcaniclastics in the North Sericite area of the property.

### 7.3.2 Silicification, Pyritization

Areas of intense quartz veining and silica flooding occurring throughout the property. Such zones also contain a variable amount of disseminated pyritic.

These zones are generally associated with small shears and faults. For the most part, they are quite narrow and not extensive.

Some of the more extensive zones of silicification occur in the Snow and Lake target areas. Such alteration is often intermixed within sericite-pyrite alteration especially near the SJ Zone.

### 7.4 Structure

The structural history of the area has not yet been determined. Regionally four sets of faults have been mapped:
a) Northwest-Southwest

Since all significant mineralization in the Iskut Camp is structurally controlled the presence of shears and faults is an important feature of any property. Within the "Bronson" Trend NW-SE structures appear to be especially significant as the larger mineralized zones all occur along such structures. On the Pelican property one of the larger of these structures is associated with the SJ Zone.

The "Sky" Fault is one of the most extensive of the faults and extends from Johnny Mountain through the Pelican property to the Pins Ridge.
b) North-South

Such faults are very prominent in the Pelican property especially within the Sericite, Lake, Pelican and Snow portions of the property.
c) Northeast-Southwest

These faults are generally younger than the other sets and often offset the other faults. Mineralization has also been found along such faults in the Iskut Region.

On the Pelican property at least three of these faults have been mapped. These faults occur along the three major drainages of the property.Geological, Geophysical and Geochemical Report PELICAN PROPERTY April 1991


PLATE 3 Strong Shear - Southeast Grid (Sample Site)

## d) Flat Faults

Flat faults have been mapped in the area largely near the contact between volcanic and sedimentary sequences. Examples of such include those occurring on the Inel and Johnny Mountain properties.

On the Pelican property such faults were noted on the Pelican Grid and SJ Zones.

### 7.5 Mineralization

### 7.5.1 SJ Zone

Talus fines samples in 1990 returned up to $3,090 \mathrm{ppb} \mathrm{Au}$ and defined a 200 m (+) area of greater than 500 ppb Au. In 1990 a prominent, 5 m wide NW-SE shear was mapped along the upper edge of this anomalous area. The shear dips moderately to the southwest.

The area is underlain by rocks of the Banded Siltstone unit which has been variably affected by sericite alteration and silica flooding. Disseminated pyrite occurs throughout and appears to increase with more intense alteration. Pyrite content varies between $2 \%-10 \%$ although the presence of numerous iron stained vugs suggests that much pyrite has been leached from surface exposures.

Rock samples from the shear and nearby sericite-silica-pyrite rock returned anomalous gold, copper and zinc including highs of $340 \mathrm{ppb} \mathrm{Au}, 478 \mathrm{ppm} \mathrm{Cu}$ and 351 ppm Zn .

A sample of a ( 8 cm thick) galena vein ( $\mathrm{J}-113$ ) returned $6,910 \mathrm{ppb} \mathrm{Au}$ and 39.4 ppm Ag . The underlying 10 cm of sericite-silica-pyrite rock with $70 \%$ disseminated pyrite returned 2,180 ppb Au.

### 7.5.2 Southeast Grid

In 1988 a sample ( $\mathrm{J}-88-82$ ) of a 0.5 m wide quartz-pyrite vein within the Southeast grid area returned $6,205 \mathrm{ppb} \mathrm{Au}$. The vein occurs along a NE-SW structure. Additional mapping in 1990 discovered similar but narrow quartz-pyrite veins (2-10\% pyrite) also trending NE-SW.


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SAMPLE NUMBER

PEL-90-J-65
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## 71

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PEL-90-G-62

## DESCPIPTION

FLOAT;QUARTX VEIN,2\% PYRITE FLOAT;GOSSAN BOXWORK
GRAB;SHEAR,FRACT.,SILICIFIED,50M WIDTH GRAB;4-4CM QTZ VEINS,CHLORITE CLOTS GRAB 4CM;QTZ VEIN,CHLORITE,160/20W GRAB;SILTSTONE,BLEACH.,SERICITIZED.3\% PY GRAB 3CM;QUARTZ VEIN;8\% PYRITE GRAB;SLICIFIED,3-5\% DISS. PYRITE GRAB;SLICIFIED,3-5\% DISS. PYRITE GRAB;SLICIFIED,3-5\% DISS. PYRITE GRAB:SILICFIED,FRACT.,5-10\% DISS. PYRITE GRAB:SILICFIED,FRACT.,5-10\% DISS. PYRITE GRAB 5M;SHEAR,SERICITE SCHIST, 1 MM PY SEA GRAB;GOSSAN
GRAB;GOUGE,SHEAR IN SAMPLE \#77
CHIP 2M;SHEAR
CHIP 2M;SHEAR
CHIP 2.5M;SHEAR AND ADJ PY-SILICA
GRAB;SILICIFIED,PYRITIZED
GRAB;QUARTZ VEIN,10\% PYRITE GRAG,VERY SILICIFIED,1\% PYRITE grab 30 cm ;silica rock,30-40\% pyrite grab;silicified,fractured, $2 \%$ diss. pyrite grab;gossan boxwork,estimate 40\% py grab;diorite,silicified, $10 \%$ diss. pyrite grab $18 \mathrm{~cm} ; 8 \mathrm{~cm}$ galena, 10 cm silicifed rock grab 1.5 m ;silicified rock adjacent to \#113 grab 40 cm;rusty qtz vein, 133/60w FLOAT;QUARTZ-PYRITE VEIN
$\underline{S A M P L E \#} \quad \mathrm{AU}(P P B) \quad \mathrm{CU}(P P M) \quad \mathrm{ZN}(P P M) \quad \mathrm{AG}(P P M) \quad \mathrm{AS}(P P M) \quad \mathrm{SB}(P P M) \quad \mathrm{BI}(P P M)$

|  |  |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| PEL-90-G-62R | 3 | 11 | 19 | 0.4 | 4 | 2 | 2 |
| PEL-90-G-62R | 8 | 156 | 48 | 1.3 | 19 | 3 | 2 |
| PEL-90-J-109R | 340 | 31 | 67 | 0.8 | 2 | 2 | 2 |
| PEL-90-J-110R | 30 | 211 | 24 | 0.2 | 14 | 2 | 2 |
| PEL-90-J-111R | 320 | 33 | 8 | 0.5 | 6 | 2 | 7 |
| PEL-90-J-112R | 164 | 10 | 64 | 0.5 | 4 | 2 | 2 |
| PEL-90-J-113R | 6910 | 106 | 281 | 39.4 | 367 | 32 | 29 |
| PEL-90-J-114R | 2180 | 98 | 805 | 5.5 | 306 | 8 | 2 |
| PEL-90-J-115R | 94 | 32 | 7 | 0.9 | 136 | 2 | 2 |
| PEL-90-J-65 | 18 | 32 | 49 | 0.1 | 2 | 2 | 2 |
| PEL-90-J-66 | 540 | 478 | 351 | 0.3 | 18 | 2 | 29 |
| PEL-90-J-67 | 300 | 348 | 104 | 1 | 20 | 2 | 2 |
| PEL-90-J-68 | 13 | 141 | 216 | 0.2 | 11 | 2 | 2 |
| PEL-90-J-69 | 32 | 163 | 251 | 0.8 | 6 | 2 | 2 |
| PEL-90-J-70 | 69 | 84 | 156 | 0.5 | 5 | 2 | 2 |
| PEL-90-J-71 | 28 | 277 | 177 | 5.4 | 10 | 2 | 2 |
| PEL-90-J-72 | 89 | 9 | 131 | 0.8 | 31 | 2 | 2 |
| PEL-90-J-73 | 31 | 11 | 58 | 0.1 | 15 | 2 | 2 |
| PEL-90-J-74 | 29 | 18 | 60 | 0.7 | 19 | 2 | 2 |
| PEL-90-J-75 | 27 | 12 | 28 | 0.2 | 22 | 2 | 6 |
| PEL-90-J-76 | 110 | 11 | 9 | 0.3 | 93 | 2 | 2 |
| PEL-90-J-77 | 61 | 42 | 26 | 1.7 | 6 | 2 | 2 |
| PEL-90-J-78 | 31 | 23 | 38 | 0.1 | 14 | 2 | 2 |
| PEL-90-J-79 | 82 | 320 | 192 | 2.2 | 26 | 2 | 2 |
| PEL-90-J-80 | 125 | 251 | 138 | 2.8 | 29 | 2 | 2 |
| PEL-90-J-81 | 9 | 39 | 15 | 0.1 | 3 | 2 | 2 |
| PEL-90-J-82 | 92 | 39 | 77 | 1.2 | 26 | 2 | 2 |
| PEL-90-J-83 | 200 | 25 | 48 | 2.8 | 85 | 2 | 2 |
| PEL-90-J-84 | 133 | 21 | 8 | 1.8 | 20 | 2 | 2 |
| PEL-90-J-85 | 73 | 15 | 86 | 0.8 | 35 | 2 | 2 |

SAMPLE NUMBER

## DESCRIPTION

GRAB;QUARTZ-PYRITE VEIN ALONG CREEK FLOAT;10 CM QTZ-PY,25\% PY,COARSE QTZ FLOAT;10 CM QTZ-PY,25\% PY,COARSE QTZ grab;qtz-py vein near site 87-521 grab;qtz-py vein near site 87-521 grab;qtz-py vein near site 87-521 grab;qtz-py vein near site 87-521 grab;qtz-py vein near site 87-521 grab;pyritized highly fractured float;quartz-pyrite vein 5\%-10\% py float;quartz-pyrite vein 5\%-10\% py float;quartz-pyrite vein 5\%-10\% py grab;ferricrete 3 m thick above shear grab;granodiorite;mod. fract.,5\% py grab; $1-2 \mathrm{~cm}$ qtz veins at 205/60N float;sercitized, pyritized granodiorite GRAB;FERRICRETE,4-5M THICK GRAB;SILIC.,BLEACH.GRANODIORITE,5\% PY GRAB;STRONG SHEAR,SERCITE SCHIST,5\%PY GRAB;ORTHO.PORPH.,INTENS.FRACT.,3\% PY GRAB;GRAB;ORTH.PORPH.SILIC..3\%PY GRAB;FRACT. SILTSTONE,SERIC.,3\%PY GRAB;SILTSTONE,BLEACH.,SERIC.,3\% PY QTZ.VEINS,1-10CM,VUGGY,COARSE,CHLORITE GRAB;SHEAR GOUGE,315/75E GRAB;SHEAR GRAB;QTZ.VEIN,5CM,GRANOD.,N-S/85W GRAB;SHEAR, $5 \%$, PY,BLEACHED INTRUS. GRAB;SHEAR,5\%,PY,BLEACHED INTRUS. GRAB;GOSSAN EXTREMELY FRACT. GRAB;GOSSAN EXTREMELY FRACT. GRAB;SHEAR,2M,170/60E GRAB;SILTSTONE,BLEACH.,3\%PY,SILIC. 5CM;RUSTY SHEAR,090/85N GRAB;GOSSAN,EXTREMELY WEATHERED GRAB;SILTSTONE,SERICITIZED,5\%PY GRAB 20CM;150/60W
GRAB;DIORITE,SHATTERED,MODER. FE STAIN GRAB;DIORITE,SHATTERED,MODER. FE STAIN GRAB 5CM;QUARTZ VEIN,150/70S GRAB;QTZ-CALCITE-CHLORITE VEIN,5CM

| 54 | GRAB;SHEAR,DIORITE,N-S/45E |
| ---: | :--- |
| 55 | GRAB;SHEAR,DIORITE,N-SI45E |
| 56 | GRAB;RUSTY SHEAR,DIORITE |
| 57 | FLOAT;QUARTZ VEIN,CHLORITE,FE-CARBONATE |
| 58 | FLOAT;QUARTZ VEIN,CHLORITE,FE-CARBONATE |
| 59 | GRAB;SHEAR,DIORITE,8\% DISS. PY |
| 60 | GRAB 40CM;SHEAR,DIORITE,SILICIFIED |
| 61 | GRAB;GOUGE AND INTERMIXED PYRITE |
| PEL-90-J-1R | GRAB;SILTSTONE,3\% DISS. PY,FE STAINED |
| 2 | GRAB 3M;SHEARED SERICITE SCHIST |
| 3 | GRAB 3M;SHEARED SERICITE SCHIST |
| 4 | GRAB 3M;SHEARED SERICITE SCHIST |
| 5 | CHIP 10CM;GOSSAN WITH FLAT SHEARING |
| 6 | GRAB 4CM;QUARTZ VEIN |
| 7 | GRAB;SHEARED DIORITE,2-3\% DISS. PY |
| 8 | GRAB;SHEAR,DIORITE,060/85W,3\% DISS. PY |
| 9 | GRAB;DIORITE,3\% DISS. PYRITE |
| 10 | FLOAT;4CM PYRITE BAND IN QUARTZ VEIN |
| 11 | FLOAT;SAME ROCK AS \#10 QUARTZ ONLY |
| 12 | FLOAT;QUARTZ,4\% PYRITE IN 5CM CLOTS |
| 13 | GRAB;SHEAR,CHLORITIC,3\% DISS. PYRITE |
| 14 | GRAB;SHATTERED DIORITE,2\% PY,3CM QTZ VEIN |
| 15 | GRAB 15CM;QUARTZ WITH 3-5\% COARSE PYRITE |
| 16 | GRAB 15CM;QUARTZ WITH 3-5\% COARSE PYRITE |
| 17 | GRAB;DIORITE,UNALTERED,WITIN 50 CM OF \#16 |
| 18 | GRAB 25CM;QUARTZ VEIN WITH 5\% PYRITE |
| 19 | CHIP 2M;SILICIFIED ROCK,PYRITIZED |
| 20 | CHIP 1M;SILICIFIED ROCK,PYRITIZED |
| 21 | GRAB 20 CM;QUARTZ VEIN ,10\% COARSE PYRITE |
| 22 | GRAB 20 CM;QUARTZ VEIN,8\% COARSE PYRITE |
| 23 | GRAB 20 CM;QUARTZ VEIN ,10\% COARSE PYRITE |
| 24 | GRAB;SILICIFIED,5-10\% DISS. PYRITE(88-J-81) |
| 25 | FLOAT;20 CM QUARTZ VEIN,10\% COARSE PYRITE |
| 35 | GRAB 3M;SHEAR,DIORITE,SILICIFIED,1-2\% PY |
| 36 | GRAB;SHATTERED CHERT,1-2\% DISS. PYRITE |
| 37 | GRAB;SHATTERED CHERT,1-2\% DISS. PYRITE |
| 38 | GRAB;SHATTERED CHERT,1-2\% DISS. PYRITE |
|  |  |

SAMPLE\# $\quad$ AU(PPB) CU(PPM) ZN(PPM) AG(PPM) AS(PPM) SB(PPM) Bl(PPM)

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| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| PEL-90-G-1 | 1121 | 39 | 9 | 0.4 | 2 | 2 | 2 |
| PEL-90-G-16 | 1796 | 15 | 39 | 0.2 | 2 | 2 | 3 |
| PEL-90-G-17 | 40 | 21 | 26 | 0.4 | 8 | 2 | 2 |
| PEL-90-G-18 | 15 | 12 | 15 | 0.1 | 3 | 2 | 2 |
| PEL-90-G-19 | 13 | 19 | 48 | 0.1 | 2 | 2 | 2 |
| PEL-90-G-2 | 25 | 76 | 8 | 0.4 | 15 | 2 | 7 |
| PEL-90-G-20 | 27 | 17 | 8 | 0.1 | 4 | 2 | 3 |
| PEL-90-G-21 | 9 | 34 | 77 | 0.3 | 3 | 2 | 2 |
| PEL-90-G-22 | 599 | 4 | 11 | 0.2 | 2 | 2 | 2 |
| PEL-90-G-23 | 33 | 79 | 9 | 4.5 | 2 | 3 | 2 |
| PEL-90-G-24 | 85 | 5 | 8 | 0.1 | 2 | 2 | 2 |
| PEL-90-G-25 | 12 | 12 | 57 | 0.3 | 2 | 2 | 2 |
| PEL-90-G-26 | 10 | 6 | 40 | 0.1 | 2 | 2 | 2 |
| PEL-90-G-27 | 5 | 5 | 35 | 0.3 | 2 | 2 | 2 |
| PEL-90-G-28 | 10 | 66 | 77 | 0.1 | 2 | 2 | 2 |
| PEL-90-G-29 | 15 | 10 | 30 | 0.2 | 3 | 2 | 2 |
| PEL-90-G-3 | 11 | 36 | 8 | 0.3 | 7 | 2 | 5 |
| PEL-90-G-30 | 4 | 10 | 10 | 0.2 | 6 | 2 | 2 |
| PEL-90-G-31 | 3 | 5 | 36 | 0.2 | 25 | 2 | 2 |
| PEL-90-G-32 | 1 | 1 | 31 | 0.1 | 2 | 2 | 2 |
| PEL-90-G-33 | 4 | 1 | 32 | 0.1 | 3 | 2 | 2 |
| PEL-90-G-34 | 1 | 2 | 64 | 0.2 | 2 | 2 | 2 |
| PEL-90-G-35 | 21 | 30 | 38 | 0.1 | 8 | 2 | 2 |
| PEL-90-G-36 | 2 | 1 | 35 | 0.1 | 2 | 2 | 2 |
| PEL-90-G-37 | 7 | 158 | 92 | 0.3 | 2 | 2 | 2 |
| PEL-90-G-38 | 10 | 51 | 89 | 0.3 | 9 | 2 | 2 |
| PEL-90-G-39 | 4 | 14 | 21 | 0.1 | 2 | 2 | 2 |
| PEL-90-G-40 | 26 | 21 | 11 | 0.3 | 4 | 2 | 2 |
| PEL-90-G-41 | 25 | 27 | 33 | 0.2 | 5 | 2 | 2 |
| PEL-90-G-42 | 10 | 1 | 46 | 0.2 | 5 | 2 | 2 |
| PEL-90-G-43 | 12 | 30 | 11 | 0.2 | 9 | 2 | 2 |
| PEL-90-G-44 | 51 | 18 | 482 | 0.2 | 20 | 2 | 2 |
| PEL-90-G-45 | 25 | 23 | 50 | 0.1 | 12 | 3 | 5 |
| PEL-90-G-46 | 220 | 62 | 20 | 0.9 | 23 | 2 | 7 |
| PEL-90-G-47 | 15 | 11 | 6 | 0.2 | 334 | 2 | 2 |
| PEL-90-G-48 | 59 | 728 | 1336 | 1.1 | 73 | 2 | 4 |
| PEL-90-G-49 | 12 | 10 | 246 | 0.3 | 5 | 2 | 2 |
| PEL-90-G-50 | 4 | 13 | 32 | 0.1 | 4 | 2 | 2 |
| PEL-90-G-51 | 4 | 11 | 25 | 0.1 | 9 | 2 | 2 |
| PEL-90-G-52 | 4 | 7 | 21 | 0.2 | 2 | 2 | 3 |
| PEL-90-G-53 | 1 | 8 | 122 | 0.1 | 2 | 2 | 2 |
|  |  |  |  |  |  | 2 | 2 |


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| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| PEL-90-G-54R | 55 | 197 | 108 | 0.7 | 6 | 11 | 2 |
| PEL-90-G-55R | 12 | 241 | 126 | 0.5 | 2 | 4 | 2 |
| PEL-90-G-56R | 7 | 9 | 78 | 0.3 | 5 | 2 | 2 |
| PEL-90-G-57R | 4 | 33 | 14 | 0.4 | 16 | 2 | 2 |
| PEL-90-G-58R | 5 | 39 | 30 | 0.1 | 3 | 2 | 2 |
| PEL-90-G-58R | 10 | 802 | 86 | 3.3 | 113 | 4 | 13 |
| PEL-90-G-60R | 7 | 87 | 42 | 1.1 | 23 | 2 | 2 |
| PEL-90-G-61R | 7 | 133 | 55 | 1.5 | 43 | 3 | 5 |
| PEL-90-J-1 | 63 | 76 | 120 | 1.8 | 251 | 8 | 2 |
| PEL-90-J-10 | 33400 | 29 | 6 | 5.2 | 33 | 25 | 275 |
| PEL-90-J-10RD | 46600 | 29 | 1 | 7.1 | 30 | 24 | 297 |
| PEL-90-J-11 | 970 | 11 | 5 | 0.1 | 7 | 3 | 9 |
| PEL-90-J-12 | 600 | 6 | 2 | 0.1 | 8 | 2 | 4 |
| PEL-90-J-13 | 74 | 588 | 247 | 3.6 | 29 | 2 | 3 |
| PEL-90-J-14 | 58 | 30 | 78 | 0.5 | 56 | 2 | 2 |
| PEL-90-J-15 | 1260 | 19 | 5 | 0.7 | 2 | 2 | 7 |
| PEL-90-J-16 | 470 | 30 | 1 | 0.3 | 8 | 2 | 8 |
| PEL-90-J-17 | 45 | 14 | 18 | 0.1 | 10 | 2 | 4 |
| PEL-90-J-18 | 3360 | 3 | 8 | 0.2 | 2 | 2 | 18 |
| PEL-90-J-19 | 370 | 7 | 13 | 0.1 | 2 | 2 | 2 |
| PEL-90-J-2 | 22 | 8 | 36 | 0.1 | 10 | 2 | 2 |
| PEL-90-J-20 | 980 | 1 | 7 | 0.2 | 2 | 2 | 8 |
| PEL-90-J-21 | 740 | 8 | 4 | 0.1 | 2 | 2 | 6 |
| PEL-90-J-22 | 1010 | 3 | 1 | 0.1 | 4 | 2 | 2 |
| PEL-90-J-23 | 140 | 7 | 3 | 0.1 | 2 | 2 | 2 |
| PEL-90-J-24 | 18 | 4 | 1 | 0.2 | 3 | 2 | 2 |
| PEL-90-J-25 | 610 | 5 | 1 | 0.1 | 7 | 2 | 2 |
| PEL-90-J-3 | 18 | 29 | 37 | 0.3 | 6 | 2 | 2 |
| PEL-90-J-35 | 4 | 1 | 2 | 0.1 | 2 | 2 | 2 |
| PEL-90-J-36 | 8 | 4 | 13 | 0.2 | 2 | 2 | 2 |
| PEL-90-J-37 | 24 | 22 | 11 | 0.3 | 2 | 2 | 2 |
| PEL-90-J-38 | 15 | 16 | 2 | 0.2 | 2 | 2 | 2 |
| PEL-90-J-4 | 32 | 12 | 32 | 0.2 | 7 | 2 | 2 |
| PEL-90-J-5 | 36 | 27 | 25 | 0.5 | 4 | 2 | 2 |
| PEL-90-J-6 | 21 | 18 | 17 | 0.3 | 2 | 2 | 2 |
| PEL-90-J-7 | 61 | 26 | 58 | 0.3 | 11 | 2 | 2 |
| PEL-90-J-8 | 83 | 87 | 63 | 1 | 16 | 2 | 2 |
| PEL-90-J-9 | 34 | 76 | 25 | 0.3 | 27 | 2 | 2 |
|  |  |  |  |  | 2 | 2 |  |

Samples of these veins returned up to $3,360 \mathrm{ppb}$ Au. Similar quartz-pyrite float, containing 4 cm seams of massive pyrite was discovered about 100 m north of J-88-82. Samples of this float returned up to $46,600 \mathrm{ppb} \mathrm{Au}, 25 \mathrm{ppm} \mathrm{Sb}$, and 297 ppb Bi .

The above mineralization suggests that similar mineralization will occur along the EM conductors outlined in this area.

### 7.5.3 Pelican

To date narrow discontinues sphalerite-galena-chalcopyrite-magnetite $\pm$ chlorite, quartz veins have been discovered on the Pelican Cliff. Samples taken to date have failed to return economic gold values although highly anomalous in gold, copper, zinc, silver and arsenic. Samples taken in 1990 include highs of $1,796 \mathrm{ppb} \mathrm{Au}, 4,152 \mathrm{ppm} \mathrm{Cu}, 23,124 \mathrm{ppm} \mathrm{Zn}, 30.8$ ppm Ag and 527 ppm As. This geochemistry compares to that of other mineralization within the Iskut Camp and suggests that there maybe other more substantial higher grade zones of mineralization within the Pelican area.

The veins occur in a variety of orientations including, E-W, N-S and flat-lying. It is unclear if one of the veins orientations is more significant than the others.

### 7.5.4 Lake - NG1 - NG2

To date narrow discontinuous quartz-sulphide veins have been discovered samples of which returned anomalous but uneconomic precious and base metal values.

More substantial showings NG1 and NG2 were discovered in 1988 along NW-SE shears in the vicinity of orthoclase porphyry plugs. The NG1 showing is 130 m long and 5 m wide and consists of $3-5 \%$ pyrite. Local pods of up to $30 \%$ pyrite also occur. The mineralization at the NG2 showing is similar but exposed over a shorter strike length. Samples taken in 1988 failed to return anomalous values.
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PLATE 8 Talus Slope below Pelican Cliff looking west towards SJ Zone

## SAMPLE

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PEL-90-J-86
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## DESCRIPTION

GRAB;PYRITIZED BOULDERS AT EDGE OF CLIFF GRAB;PYRITIZED BOULDERS AT EDGE OF CLIFF GRAB;PYRITIZED SILICIFIED SILTSTONE GRAB;PYRITIZED SILICIFIED SILTSTONE GRAB;PYRITIZED SILICIFIED SILTSTONE GRAB;MASSIVE E-W PY VEIN,DIP 80 S FLOAT;PYRITIZED,SILICIFIED BOULDERS FLOAT;PYRITIZED,SILICIFIED BOULDERS GRAB;1-4CM PYRITE VEINS, 20 DIP S GRAB;1-4CM PYRITE VEINS, 20 DIP S GRAB;HYDROZINCITE,DISS.PYRITE GRAB 20 CM;VERTICAL N-S QTZ-PY VEIN GRAB;GOSSAN ABOVE MAIN ZONE GRAB 40CM;SHEAR,N-S,VERTICAL GRAB;SHEAR,065/90 GRAB 5CM;QUARTZ VEIN 2-3\% PY,060/90 GRAB 50CM;QUARTZ VEIN,090/70S GRAB 15 CM;QUARTZ VEIN,2\% SPHALERITE GRAB 1.5M;FLAT SHEAR,FE STAINED GRAB 1.5M;FLAT SHEAR,FE STAINED GRAB;20 CM;TOP OF FLAT SHEAR,40\% PY

## SAMPLE\# AU(PPB) CU(PPM) ZN(PPM) AG(PPM) AS(PPM) SB(PPM) Bl(PPM)

| PEL-90-G-10 | 200 | 4152 | 1604 | 15.1 | 337 | 7 | 7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| PEL-90-G-10D | 140 | 272 | 1891 | 22.5 | 288 | 8 | 2 |
| PEL-90-G-11 | 333 | 1034 | 18217 | 14.2 | 319 | 9 | 2 |
| PEL-90-G-12 | 276 | 639 | 15981 | 5 | 375 | 6 | 2 |
| PEL-90-G-13 | 128 | 389 | 13020 | 6.7 | 499 | 8 | 2 |
| PEL-90-G-14 | 1796 | 177 | 734 | 30.8 | 527 | 5 | 10 |
| PEL-90-G-14D | 77 | 93 | 570 | 6.6 | 457 | 8 | 2 |
| PEL-90-G-15 | 98 | 316 | 3802 | 1.7 | 54 | 2 | 2 |
| PEL-90-G-4 | 827 | 2478 | 1081 | 7.2 | 401 | 4 | 2 |
| PEL-90-G-5 | 21 | 312 | 378 | 16 | 334 | 4 | 2 |
| PEL-90-G-6 | 27 | 446 | 242 | 2.1 | 45 | 2 | 2 |
| PEL-90-G-7 | 99 | 77 | 5693 | 1.1 | 162 | 2 | 3 |
| PEL-90-G-8 | 105 | 233 | 1312 | 5.9 | 304 | 5 | 3 |
| PEL-90-G-9 | 285 | 1124 | 21319 | 10.7 | 116 | 2 | 2 |
| PEL-90-J-86 | 105 | 99 | 630 | 4.7 | 139 | 3 | 2 |
| PEL-90-J-87 | 93 | 877 | 11726 | 4.2 | 109 | 2 | 2 |
| PEL-90-J-88 | 340 | 332 | 3874 | 5.3 | 31 | 2 | 2 |
| PEL-90-J-89 | 370 | 663 | 2197 | 11.3 | 319 | 4 | 2 |
| PEL-90-J-90 | 320 | 1923 | 2116 | 8.7 | 459 | 5 | 2 |
| PEL-90-J-91 | 860 | 1516 | 23124 | 7.7 | 151 | 2 | 2 |
| PEL-90-J-92 | 280 | 322 | 3125 | 6.2 | 373 | 5 | 2 |
| PEL-90-J-93 | 720 | 1053 | 12315 | 22.7 | 231 | 4 | 2 |
| PEL-90-J-94 | 210 | 89 | 566 | 4.3 | 496 | 5 | 2 |

TABLE 9 ROCK SAMPLE DESCRIPTIONS-SNOW GRID

SAMPLE NUMBER

PEL-90-G-63
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PEL-90-J-49
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54

## DESCRIPTION

FLOAT;QUARTZ VEIN MINOR PYRITE GRAB 5CM;QUARTZ-CARBONATE VEIN GRAB;QUARTZ VEIN 070/STEEPN FLOAT; QUARTZ VEIN
GRAB;RUSTY GOSSAN ABOVE STRONG SHEAR GRAB;SHEAR,BLEACH.QTZ VEINING,MALACHITE GRAB;SHEAR,BLEACH.QTZ VEINING,MALACHITE GRAB;SHEAR,BLEACH.QTZ VEINING,MALACHITE FLOAT?;RUBBLE WITHIN TRACE OF SHEAR 4CM;VUGGY QUARTZ-CHLORITE,N-S/62W FLOAT;EPIDOTE,BLEACH.,MALACHITE,PY FLOAT;EPIDOTE,BLEACH.,MALACHITE,PY FLOAT;SILTSTONE,MALACHITE GRAB 2CM;BLEACH.,PYRITIZATION ALONG SHEAR GRAB 2CM;BLEACH.,PYRITIZATION ALONG SHEAR FLOAT;RUSTY,COARSE QUARTZ GRAB 40 CM ;QUARTZ IN FLAT SHEAR,MINOR PY GRAB 40 CM;QUARTZ IN FLAT SHEAR,MINOR PY GRAB 40 CM ;QUARTZ IN FLAT SHEAR,MINOR PY GRAB 40 CM;QUARTZ IN FLAT SHEAR,MINOR PY GRAB;BRECCIATED VOLC.,IRREG.PY INFILLING GRAB;BRECCIATED VOLC.,IRREG.PY INFILLING FLOAT;SILTSONE,MALACHITE,DISS. PY FLOAT;SILTSONE,MALACHITE,DISS. PY 4 CM;QUARTZ IN SHEAR,120/68S GRAB 50 CM ;INTERMIXED PY \&BRECCIATED VOLC. GRAB 50 CM ;INTERMIXED PY \&BRECCIATED VOLC. FLOAT;QUARTZ-PYRITE ,30\% PYRITE FLOAT;QUARTZ-PYRITE ,30\% PYRITE FLOAT;QUARTZ-PYRITE ,30\% PYRITE FLOAT;QUARTZ-PYRITE ,30\% PYRITE FLOAT;VUGGY QUARTZ-PYRITE GRAB 5CM;QUARTZ VEIN @005/70W FLOAT;QUARTZ VEIN WITH 25\% PYRITE GRAB;WEAKLY PYRITIZED BASALT GRAB 10CM;QUARTZ VEIN 30\% PYRITE GRAB 20CM;IRREGULAR QUARTZ VEINS GRAB 3M;SILICIFIED,1M QTZ VEINS,1\% DISS. PY GRAB 5M;SILICIFIED
GRAB;QUARTZ VEIN ,5\% PYRITE

55
56

## 57

58
59
60
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62
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64
124
125
126
127
128
129
130

GRAB 20CM;QUARTZ VEIN IN BASALT?,DIORITE? GRAB:GOSSAN,4\% DISS. PYRITE GRAB:GOSSAN,4\% DISS. PYRITE GRAB:GOSSAN,4\% DISS. PYRITE GRAB:GOSSAN,4\% DISS. PYRITE GRAB;FRACT.,SILICIFIED SILTSTONE GRAB;BOXWORK GOSSAN GRAB;BOXWORK GOSSAN GRAB 10 CM;QUARTZ,25\% PYRITE GRAB;IRREGULAR QUARTX VEIN, $5 \%$ pyrite grab $30-60 \mathrm{~cm}$;irregular qtz vein, $8 \%$ py grab 25 cm;quartz vein,10-20\% pyrite grab;pyrite intermixed with quartz grab 1 m ;shear, $1-2 \mathrm{~cm}$ seams of pyrite float; $95 \%$ pyrite intermixed with quartz grab;irregular qtz-pyrite veins grab;silicified,1-2\% diss py,fractured


| PEL-90-G-63R | 7 | 20 | 8 | 3.6 | 96 | 2 | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL-90-G-64R | 45 | 1751 | 112 | 9.8 | 10 | 5 | 2 |
| PEL-90-G-65R | 22 | 96 | 141 | 3.2 | 36 | 6 | 6 |
| PEL-90-G-66R | 15 | 75 | 22 | 1.6 | 44 | 2 | 3 |
| PEL-90-G-67R | 27 | 29 | 111 | 2.3 | 27 | 6 | 2 |
| PEL-90-G-68R | 5 | 4835 | 98 | 14.3 | 4 | 2 | 2 |
| PEL-90-G-69R | 2 | 9866 | 53 | 9.9 | 3 | 2 | 3 |
| PEL-90-G-70R | 5 | 455 | 182 | 0.6 | 3 | 3 | 2 |
| PEL-90-G-71R | 45 | 121 | 118 | 1.6 | 152 | 11 | 2 |
| PEL-90-G-72R | 55 | 407 | 145 | 0.3 | 5 | 2 | 2 |
| PEL-90-G-73R | 5 | 2219 | 87 | 3 | 2 | 6 | 2 |
| PEL-90-G-74R | 11 | 4986 | 290 | 6.8 | 6 | 2 | 2 |
| PEL-90-G-75R | 9 | 4663 | 266 | 4.7 | 9 | 2 | 2 |
| PEL-90-G-76R | 21 | 151 | 257 | 0.8 | 36 | 7 | 2 |
| PEL-90-G-77R | 16 | 102 | 175 | 1.3 | 324 | 7 | 2 |
| PEL-90-G-78R | 270 | 47 | 33 | 4.8 | 231 | 2 | 3 |
| PEL-90-G-79R | 22 | 533 | 2181 | 0.6 | 21 | 2 | 2 |
| PEL-90-G-80R | 16 | 22 | 19 | 1.1 | 24 | 2 | 2 |
| PEL-90-G-80R | 32 | 292 | 508 | 1.2 | 37 | 2 | 2 |
| PEL-90-G-81R | 16 | 193 | 595 | 0.6 | 15 | 2 | 2 |
| PEL-90-G-82R | 72 | 200 | 2128 | 1.2 | 171 | 2 | 2 |
| PEL-90-G-83R | 62 | 27 | 165 | 2.6 | 26 | 7 | 2 |
| PEL-90-G-84R | 13 | 50 | 236 | 2 | 18 | 7 | 2 |
| PEL-90-G-85R | 13 | 3953 | 512 | 2.9 | 2 | 4 | 2 |
| PEL-90-G-86R | 6 | 6548 | 295 | 4.5 | 2 | 2 | 2 |
| PEL-90-G-87R | 42 | 1698 | 128 | 3 | 118 | 3 | 6 |
| PEL-90-G-88R | 168 | 209 | 366 | 2.1 | 163 | 2 | 3 |
| PEL-90-G-89R | 122 | 231 | 325 | 1.4 | 144 | 3 | 2 |
| PEL-90-G-90R | 48 | 4187 | 69 | 6.7 | 14 | 2 | 11 |
| PEL-90-G-91R | 37 | 5717 | 76 | 7.8 | 12 | 2 | 2 |
| PEL-90-G-92R | 46 | 2163 | 54 | 15.7 | 11 | 2 | 11 |
| PEL-90-G-93R | 42 | 3353 | 104 | 16.2 | 10 | 2 | 6 |
| PEL-90-G-94R | 207 | 86 | 85 | 3.9 | 41 | 2 | 5 |
| PEL-90-G-95R | 112 | 84 | 106 | 0.1 | 6 | 2 | 4 |
| PEL-90-G-96R | 27260 | 22 | 1 | 1.2 | 2 | 2 | 9 |
| PEL-90-J-49 | 1 | 18 | 58 | 0.1 | 4 | 2 | 2 |
| PEL-90-J-50 | 1 | 361 | 94 | 2.6 | 186 | 2 | 3 |
| PEL-90-J-51 | 280 | 127 | 175 | 5.9 | 285 | 2 | 5 |
| PEL-90-J-52 | 13 | 63 | 56 | 13.7 | 248 | 6 | 2 |
| PEL-90-J-53 | 151 | 49 | 64 | 5.9 | 203 | 4 | 2 |
| PEL-90-J-54 | 860 | 82 | 63 | 17.7 | 45 | 2 | 3 |


| PEL-90-J-55 | 290 | 153 | 1944 | 35 | 74 | 6 | 2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| PEL-90-J-56 | 184 | 21 | 20 | 1.8 | 20 | 2 | 3 |
| PEL-90-J-57 | 46 | 23 | 45 | 2.1 | 13 | 2 | 6 |
| PEL-90-J-58 | 8 | 144 | 76 | 2.5 | 17 | 2 | 6 |
| PEL-90-J-59 | 123 | 2160 | 111 | 6.1 | 81 | 2 | 2 |
| PEL-90-J-60 | 5 | 101 | 164 | 1 | 25 | 2 | 2 |
| PEL-90-J-61 | 88 | 23 | 18 | 3.3 | 13 | 2 | 10 |
| PEL-90-J-62 | 30 | 22 | 14 | 1.7 | 40 | 2 | 6 |
| PEL-90-J-63 | 980 | 87 | 197 | 18.8 | 1018 | 3 | 13 |
| PEL-90-J-64 | 206 | 47 | 25 | 2.4 | 74 | 2 | 4 |
| PEL-90-J-124R | 93 | 25 | 12 | 16.2 | 8 | 2 | 75 |
| PEL-90-J-125R | 87 | 432 | 52 | 0.4 | 87 | 2 | 2 |
| PEL-90-J-126R | 240 | 65 | 226 | 1.4 | 123 | 2 | 3 |
| PEL-90-J-127R | 37 | 33 | 35 | 1.4 | 77 | 2 | 2 |
| PEL-90-J-128R | 520 | 646 | 5 | 3.3 | 56 | 2 | 2 |
| PEL-90-J-128R | 730 | 876 | 10 | 3.4 | 58 | 2 | 2 |
| PEL-90-J-129R | 320 | 508 | 59 | 8 | 815 | 2 | 6 |
| PEL-90-J-130R | 89 | 8 | 2 | 0.9 | 10 | 2 | 7 |

### 7.5.5 Snow

Previous work has located narrow quartz-sulphide within silicified zones in the Snow Zone. Such altered zones generally contain several percent pyrite and weather gossanous.

Samples taken to date have returned anomalous values in gold, copper, zinc, silver and arsenic, including highs of $980 \mathrm{ppb} \mathrm{Au}, 9,866 \mathrm{ppm} \mathrm{cu}, 2,181 \mathrm{ppm} \mathrm{Zn}, 18.8 \mathrm{ppm} \mathrm{Ag}$, and 1,018 ppm As for samples taken in 1990.

In 1990 malachite was commonly found along fractures and along occasional small shears. Previous work by Great Plains Development (1973) reported chalcopyrite-malachite mineralization within granite porphyry which samples of which returned up to $7.07 \% \mathrm{Cu}$ and $0.08 \mathrm{oz} /$ ton Au .

### 7.5.6 Pins West

Numerous galena-sphalerite quartz veins occur within NW trending shears on the Pins Ridge. A $10-15 \mathrm{~cm}$ wide zone of sericite-carbonate alteration occurs alongside the mineralized shear.

Samples of this mineralized generally return several percent $\mathrm{Pb}+\mathrm{Zn}$ with anomalous silver and low gold values. One sample in 1988 returned $1.1 \% \mathrm{~Pb}, 4.8 \% \mathrm{Zn}$ and $3,605 \mathrm{ppb} \mathrm{Au}$.

### 7.5.7 Additional Targets

Additional targets examined in 1990 include:
a) Sericite North

Previous work by Western Canadian (1987) and Aerodat (1989) outlined soils anomalous in gold and airborne conductors respectively. A brief visit in 1990 indicated zones of sericite-silica-pyrite alteration and widespread ferricrete. One sample of sericite-silica-pyrite altered rock returned a value of 630 ppb Au .
b) West Sericite

Previous work by Western Canadian (1987) in the West Sericite area included a soil sample which returned $1,190 \mathrm{ppb}$ Au. In 1990 this area was briefly visited and additional soil samples taken to test significance of anomaly. Soil samples returned up to 390 ppb Au which enhances significance of the 1987 anomaly. A sample of a iron-stained silica boxwork in this area returned $1,290 \mathrm{ppb} \mathrm{Au}, 9.3 \mathrm{ppm} \mathrm{Ag}, 1.411 \mathrm{ppm}$ As and 52 ppm Bi . Further work will be required in this area to develop in exploration target.
c) Lake Ridge West

The Lake Ridge West Showing is listed in the B.C. Minfile as 104B-135, where it is described as consisting of narrow arsenopyrite-galena-quartz veins in a silicified shear.

The showing occurs along a steep face overlooking the Nee Glacier. In 1990 attempts were made to visit showing although actual showing could not be reached due to steep terrain. A quartz vein within a gossanous shear was sampled but returned only low values. This area is of interest due to the North Pins Glacier mineralized float which likely has a source within the Nee Glacier basin.
d) Lake - EM Airborne Conductor

The 1989 Aerodat airborne EM survey detected a strong, >30 moh, conductor in the Lake area of the Pelican property. Ground follow-up was carried out with the Apex double dipole EM systems and the airborne conductor was found to be caused by a 1 m wide graphitic pyritic basalt dyke trending $140^{\circ}$ intruding a host diorite.

The double dipole registered a $>1,000 \mathrm{ppm}$ positive response with a 1 m conductor width at the location of the airborne conductor. The strongest ground response corresponds to the outcrop of the basalt dyke but the conductor was only extended over a 60 m strike length under shallow overburden. Outcrops further along strike had no conductive response.

The basalt dyke contains $2-3 \%$ disseminated coarse pyrite and follows a strong narrow shear at $140^{\circ}$. Irregular 10 cm patches of the basalt dyke contain $20-30 \%$ white 4 mm feldspar laths in a black groundmass.


## PINS GRID

SAMPLE NUMBER

## SAMPLE

## NUMBER

DESCRIPTION
grab 3.5m;shear,125/45sw grab;siltstone,silicified grab;sheared diorite dyke grab;sheared diorite dyke grab;gossan,silicified,2-3\% pyrite grab,float;quartz,5\% pyrite grab;silicified,2-3\% pyrite grab 60 cm ;vuggy quartz vein, no pyrite

## WEST SERICITE

## DESCPIPTION

GRAB;RUSTY SHEAR IN DIORITE GRAB;5\% PYRITE IN 1CM CLOTS GRAB;BOXWORK GOSSAN,3\% DISS. PYRITE FLOAT;SILICA ROCK,3\% diss. pyrite FLOAT;SILICA ROCK,3\% diss. pyrite grab 20 cm ;quartz vein grab;quartz vein unkown width grab;siltstone,rusty grab;silicified,trace pyrite

## SERICITE NORTH

## SAMPLE

DESCRIPTION
NUMBER
GRAB;SERICITE SCHIST,SILICA,3\% PY GRAB;SERICITE SCHIST,SILICA,3\% PY GRAB;SERICITE SCHIST,SILICA, < $1 \%$ PY CHIP 2M:SERICITE-SILICA ROCK,FE STAINED FLOAT;VERY SILICIFIED SERICIT ROCK,FE STAIN FLOAT;TALUS
GRAB;DIORITE?,HYROZINCITE? GRAB;SHATTERED,SICIFIED ROCK,1-2\% PY FLOAT;CHLORITIC,SILICA ROCK,GREEN STAIN

## LAKE AIRBORNE-EM

SAMPLE DESCRIPTION
NUMBER
PEL-90-J-2627
DIORITE,SILICIFIED,5\% DISS. PYRITE DIORITE,SILICIFIED,5\% DISS. PYRITE BASALT DYKE,BLACK,3-5\% DISS. PYRITE GRAB;GOSSAN,SILICIFIED,2\% DISS. PYRITE GRAB;GOSSAN,SILICIFIED,2\% DISS. PYRITE GRAB;GOSSAN,SILICIFIED,2\% DISS. PYRITE GRAB;BASALT DYKE,DK GREEN,2-3\% DISS. PY GRAB;DIORITE,SILICIFIED,FE STAINED, $2 \%$ PY GRAB;DIORITE,SILICIFIED,FE STAINED,2\% PY

## AIRBORNE ANOMALY-K

## SAMPLE <br> DESCRIPTION

NUMBER
PEL-90-J-95
ARGILLITE,SILTSTONE,BANDED,FE STAINED
96 ARGILLITE,SILTSTONE,BANDED,FE STAINED

## LAKE RIDGE WEST

## SAMPLE

DESCRIPTION
NUMBER

TABLE 12
ROCK GEOCHEMISTRY-ADDITIONAL TARGETS
PINS GRID

## SAMPLE \#

PEL-90-J-116R
PEL-90-J-117R
PEL-90-J-118R
PEL-90-J-119R
PEL-90-J-119R
PEL-90-J-120R
PEL-90-J-121R
PEL-90-J-122R
PEL-90-J-123R
PIN-J-B-1 SOIL
PIN-J-B-2 SOIL
PIN-J-B-3 SOIL

AU(PPB) CU(PPM) ZN(PPM) AG(PPM) AS(PPM) SB(PPM) Bl(PPM)

| 280 | 33 | 2 |
| ---: | ---: | ---: |
| 189 | 46 | 19 |
| 119 | 40 | 50 |
| 1 | 53 | 35 |
| 1 | 13 | 8 |
| 18 | 25 | 110 |
| 3 | 15 | 31 |
| 1 | 12 | 36 |
| 3 | 27 | 25 |
| 6 | 235 | 141 |
| 8 | 259 | 94 |
| 29 | 574 | 318 |
| 12 | 467 | 60 |


| 0.1 | 37 | 2 | 2 |
| ---: | ---: | ---: | ---: |
| 1 | 9 | 2 | 2 |
| 0.1 | 2 | 2 | 2 |
| 0.2 | 2 | 2 | 3 |
| 0.2 | 2 | 2 | 2 |
| 0.6 | 4 | 2 | 2 |
| 0.2 | 2 | 2 | 2 |
| 0.4 | 3 | 2 | 5 |
| 0.1 | 8 | 2 | 2 |
| 0.5 | 14 | 2 | 2 |
| 0.4 | 17 | 2 | 2 |
| 0.4 | 59 | 5 | 2 |
| 0.4 | 9 | 2 | 2 |

## WEST SERICITE

## SAMPLE \#

|  | 39 |
| :--- | ---: |
| PEL-90-J-100 | 39 |
| PEL-90-J-101 | 470 |
| PEL-90-J-102 | 1290 |
| PEL-90-J-103 | 27 |
| PEL-90-J-104 | 32 |
| PEL-90-J-105 | 4 |
| PEL-90-J-106 | 35 |
| PEL-90-J-107 | 27 |
| PEL-90-J-108 | 540 |
| WS-9081 SOIL | 123 |
| WS-90B2 SOIL | 200 |
| WS-90B3 SOIL | 49 |
| WS-90B4 SOIL | 45 |
| WS-90B5 SOIL | 24 |
| WS-90B6 SOIL | 66 |
| WS-90B7 SOIL | 330 |
| WS-90B8 SOIL | 155 |
| WS-90B9 SOIL | 65 |
| WS-90B10 SOIL | 79 |
| WS-90B11 SOIL | 40 |
| WS-90B12 SOIL | 390 |
| WS-90B13 SOIL | 51 |
| WS-90B14 SOIL | 103 |

## SERICITE NORTH

| SAMPLE \# | AU(PPB) | CU(PPM) | ZN(PPM) | AG(PPM) | AS(PPM) | SB(PPM) | Bl(PPM) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BR-90-J-1 | 4 | 3 | 4 | 0.2 | 7 | 2 | 2 |
| PEL-90-J-39 | 630 | 266 | 83 | 1.6 | 14 | 2 | 2 |
| PEL-90-J-40 | 1 | 56 | 8 | 0.2 | 2 | 2 | 2 |
| PEL-90-J-41 | 2 | 11 | 50 | 0.1 | 16 | 2 | 2 |
| PEL-90-J-42 | 1 | 104 | 42 | 1 | 16 | 2 | 2 |
| PEL-90-J-43 | 3 | 35 | 46 | 1 | 13 | 2 | 2 |
| PEL-90-J-44 | 1 | 64 | 99 | 0.4 | 9 | 2 | 2 |
| PEL-90-J-45 | 2 | 21 | 35 | 0.4 | 11 | 2 | 2 |
| PEL-90-J-46 | 1 | 154 | 71 | 0.3 | 2 | 2 | 2 |
| PEL-90-J-47 | 1 | 36 | 104 | 0.4 | 13 | 2 | 2 |
| PEL-90-J-48 | 5 | 27 | 89 | 1.6 | 4 | 2 | 2 |

## LAKE AIRBORNE-EM

SAMPLE\# $\quad$ AU(PPB) CU(PPM) ZN(PPM) AG(PPM) AS(PPM) SB(PPM) BI(PPM)
PEL-90-J-26

| 5 | 8 | 30 | 0.1 | 2 | 2 | 2 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 14 | 4 | 42 | 0.3 | 4 | 2 | 2 |
| 1990 | 83 | 277 | 0.9 | 10 | 2 | 2 |
| 2240 | 193 | 293 | 1 | 27 | 2 | 2 |
| 41 | 12 | 185 | 0.7 | 2 | 2 | 3 |
| 36 | 6 | 89 | 0.7 | 2 | 2 | 2 |
| 16 | 5 | 168 | 0.5 | 3 | 2 | 2 |
| 56 | 9 | 199 | 0.9 | 23 | 2 | 2 |
| 11 | 18 | 108 | 0.4 | 2 | 2 | 2 |
| 17 | 20 | 63 | 0.5 | 2 | 2 | 2 |

AIRBORNE ANOMALY K

| K-B-90-1 SOIL | 9 | 215 | 223 | 0.7 | 7 | 2 | 2 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| K-B-90-2 SOIL | 13 | 135 | 99 | 0.6 | 15 | 2 | 2 |
| K-B-90-3 SOIL | 6 | 212 | 243 | 0.8 | 24 | 2 | 2 |
| PEL-90-J-95 | 6 | 84 | 371 | 0.7 | 9 | 2 | 2 |
| PEL-90-J-95D | 780 | 28 | 56 | 1.1 | 130 | 3 | 2 |
| PEL-90-J-96 | 3 | 105 | 94 | 0.6 | 2 | 2 | 2 |

## LAKE RIDGE WEST

| PEL-90-J-97 | 10 | 198 | 45 | 3.5 | 11 | 6 | 4 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| PEL-90-J-98 | 4 | 71 | 168 | 0.6 | 20 | 3 | 2 |
| PEL-90-J-99 | 6 | 50 | 114 | 0.5 | 18 | 2 | 2 |



The 5 m of outcrop south of the basalt dyke is gossanous and strongly silicified with $2 \%$ disseminated pyrite. The gossanous area and the basalt dyke were sampled.

Results from the 1990 sampling included a high of $2,240 \mathrm{ppb} \mathrm{Au}$ (pyritic basalt).
e) Pins - Airborne EM Anomalies

The 1989 Aerodat airborne Em survey outlined several conductors on the central portion of the Pins Ridge. In 1990 several lines of reconnaissance soil samples and VLF-EM electromagnetic survey were completed as preliminary follow-up. This work outlined several EM anomalies one of which was associated with marginally anomalous gold ( $>15 \mathrm{ppb} \mathrm{Au}$ ).

Rock samples of pyritic shears returned up to 280 ppb Au .
f) Airborne Anomaly K

The 1989 Aerodat Airborne EM Survey outlined an EM anomaly on the southernmost portion of the property on the Gossan 25 mineral claim.

A brief visit was made to the area in 1990. Soil samples returned low gold values but up to 215 ppm Cu . A rock sample of rusty argillite returned 780 ppb Au .

Further work will be required in this area.

### 7.5.8 Skarn Mineralization - Iskut Region

The extensive exploration efforts in the Iskut region in the last few years has discovered skarn mineralization in addition to the more well known vein deposits such as the Snip mine.

There are two areas of skarn mineralization:
a) McLymont/Forrest-Kerr

- McLymont Northwest, Ken, Dirk, Kerr 1, Tic and Dundee Prospects
b) Snippaker Creek
- Stu, Shan, Kirk and Pyramid Hill Prospects

The McLymont Northwest Zone is the most significant and developed of the prospects. The mineralization consists of pyrite and magnetite, with lesser chalcopyrite, galena sphalerite and gold. The mineralization is hosted by a Mississippian sequence of tuffs, siltstones and marbles. A major NE-SW fault and marble members of the sequence appear to be the main ore controls.

As with many of the Iskut gold deposits diamond drilling has intersected some very high grade mineralization, such as DD87-29 which returned 11.2 m assaying $55.02 \mathrm{gr} /$ tonne $\mathrm{Au}, 1,362$ gr/tonne Ag and $0.97 \% \mathrm{Cu}$.

The Snippaker Creek skarns include:
a) Shan

The mineralization is located near the northern contact of the Lehto Batholith and is hosted by a sequence of interbedded andesitic tuffs, limestones and siltstones.

The mineralization consists of pods of sphalerite pyrite, magnetite, galena and tetrahedrite within epidote-actinolite-garnet-quartz altered rock. Samples taken to date indicate only low gold values.
b) Kirk

This prospect is also located near the northern margin of the Lehto Batholith within similar rocks to the Shan. The main zone is a $2-8 \mathrm{~m}$ thick massive magnetite horizon within a 150 m thick marble unit, nearby intrusive rocks are altered (chlorite, epidote, carbonate veins). The skarn contains some potassium feldspar.

Mineralogy consists of magnetite, pyrite and chalcopyrite. Some carbonate-barite veins occur.
c) Stu

Located south of the previous two prospects. This showing is hosted by a tremolite-actinolite-quartz-carbonate skarn within a 20 m thick marble unit of a tuff-sediment sequence similar to the above.

The mineralization occurs as irregular veins and pods over a 600 m strike length. Mineralogy consists of magnetite, pyrite an pyrrhotite with lesser chalcopyrite, galena and sphalerite. Crosscutting pyrite-quartz veins also occurs. Gold values reported to date have been low.

Western Canadian (1987) considered much of the mineralization on the Pelican property to be related to skarns and certainly the mineralogy within the Pelican, Snow and Lake target areas is similar to that of the skarns in the area. However the quartz-pyrite gold mineralization sampled in the southeast area and the information to date on the SJ Zone suggest that additional types of mineralization are also present. One should note the rocks underlying the Pelican property do not contain carbonate horizons such as those found on the described skarn prospects.

### 8.0 SOIL GEOCHEMISTRY

### 8.1 Introduction

Soil samples were taken on several flagged grids to keep locate mineralization. Since significant portions of the property are above treeline in alpine conditions, soil development in such areas differs from those areas at lower elevations. Of the grids soil sampled in 1990 only the SJ Grid would fall in the above category. The SJ grid is well above treeline in steep terrain in which there is little or no soil development. Samples ( $300 \mathrm{gr} \mathrm{)} \mathrm{taken} \mathrm{were} \mathrm{of} \mathrm{fine}$ grained highly weathered talus. These samples were taken at $5-10 \mathrm{~cm}$ depths using a soil mattock.

The other Pelican, Southeast and Pins Grids are all near treeline and are characterized by intermixed alpine meadows and small stands of stunted evergreens. The eastern half of the southeast grid would extend into forested terrain. On the above grids soil samples were taken at B-horizon at depths of $\mathbf{1 5 - 2 0} \mathrm{cm}$ using a soil mattock.

All samples were submitted to Acme Labs of Vancouver for 30 element ICP analysis and gold by atomic adsorption. A description of basic statistics and correlations can be found in Appendix V.

### 8.2 SJ Grid

Previous soil sampling by Western Canadian (1987) outlined a $400 \mathrm{~m} \times 400 \mathrm{~m}$ area which returned greater than 50 ppb Au including a high of 650 ppb Au . Results for $\mathrm{Cu}, \mathrm{Ag}$ and Zn also included anomalous values although more sporadic than that of gold.

Additional detailed sampling was completed by Cathedral Gold Corporation in 1990 within the above 1987 anomaly to more accurately delineate the source of anomalous gold.

Gold analyses returned indictate a sharp upper cutoff to the anomaly striking NW-SE. This cutoff is located near the strong NW-SE shear mapped in 1990 suggesting that the source of anomalous gold is located along the shear. Lead, arsenic and silver values indicate coincident although less pronounced anomalies. It is interesting to note that the above NW-SE trend
also marks the edge of a copper anomaly but instead of higher values occurring below the trend (towards the east) as with gold, copper values increase above the trend in the west.

### 8.3 Southeast Grid

### 8.3.1 Features Affecting Geochemical Interpretation

Line $8 W$ roughly defines the boundary between rocks containing several percent disseminated pyrite to the west from rocks with or minor disseminated pyrite. One should also note that elevations increase towards the southwest end of the grid with a corresponding increase in the amount outcrop and with a corresponding ever thinning layer of surface cover.

A third feature of the grid area is a seemingly quite widespread layer of ferricrete as much as 6 m thick. The ferricrete is observed mainly where streams have cut deeply into surface material forming small canyons. The ferricrete is found just above outcrop and is generally covered by gravel, soils, etc. The ferricrete consists of a iron stained fine cement with abundant talus, gravel, and boulders. The ferricrete appears limited to basin like depression in the northern portion of the grid between L4W and L9W. Two samples of the ferricrete (Pel-90-G25, 29R) were taken which returned only low values It seems quite likely that the presence of the ferricrete would affect geochemical patterns and could well suppress anomalies.

### 8.3.2 Conclusions

Gold Gold values from L8W to L12W are noticeably higher than those from L4W to L7W. The best values are from the southwestern portion grid (L11W, L12W) where eight samples returned greater than 100 ppb Au including a high of 250 ppb . Contouring of values suggest NE to NNE anomalies which broaden towards the southwest.

Copper The northern half of the grid contains several areas of moderately anomalous copper values ( $>60 \mathrm{ppm}$ ) including a high of 710 ppm).

Silver Occasional moderately anomalous but scattered values. No discernable patterns.

Zinc/Lead

Arsenic $\quad$ Occasional marginally anomalous values ( $>20 \mathrm{ppm}$ As) but no discernable pattern.

### 8.4 Pelican Grid

Gold Several marginally anomalous ( $>20 \quad \mathrm{ppb} \quad \mathrm{Au}$ ) roughly northtrending anomalies, including a high of 172 ppb Au .

One should note that much of the western and northwestern portion of the grid are not suitable for soil sampling due to thick talus cover.

Copper A few marginally anomalous values ( $>60 \mathrm{ppm}$ ) with some suggestion of north-south trends.

Silver $\quad$ Two sharply defined north-south anomalies ( $>1.0 \mathrm{ppm} \mathrm{Ag}$ ) including a high of 3.8 ppm Ag. Such values would be considered as marginally anomalous.

Zinc/Lead $\quad$ A few marginally anomalous zinc values ( $>100 \mathrm{ppm} \mathrm{Zn}$ ) several of which are also anomalous in lead ( $>100 \mathrm{ppm} \mathrm{Pb}$ ).

## 85 Pins Grid

The soil sampling done in 1990 returned a few marginally anomalous $\mathrm{Au}, \mathrm{Zn}, \mathrm{Ag}$ and As values. The most notable result is a northwest trending 15 ppb Au anomaly in the centre of the grid area.

### 9.0 GEOPHYSICS

### 9.1 Introduction

A. The 1990 geophysical exploration program on the Pelican Project had three aims, to locate structures, sulphide mineralization along structures, and also to determine suitability of various geophysical techniques for the property.
B. To fulfill the aims of the geophysical program Roger Caven, Consulting Geophysicist for Robert S Middleton Exploration Services Inc, brought five different instruments to the property. These instruments consisted of: Induced Polarization, Horizontal Loop EM, VLF-EM, Double Dipole EM, and Magnetometer.

The induced polarization equipment consisted of a Scintrex IPR-11 time domain receiver, a Scintrex TSQ-3 transmitter with motorgenerator and auxilliary items, such as wire, current and potential electrodes.

The horizontal loop electromagnetometer was an APEX MaxMin I unit with a 50 m cable to connect transmitter and receiver loops. The MaxMin I instrument has eight frequencies, of which five, $220,880,3520,7040$, and 14080 Hz , were used for this project.

In presenting the results, the inphase data were corrected by subtracting the 220 H readings from the four higher frequencies, thereby removing the effects of terrain induced differencies in coil separation.

The VLF-EM surveys were conducted with a Geonics EM-16 unit with receiver crystals for Cutler, Maine (NAA), and Jim Creek, Seattle (NLK), transmitter frequencies respectively. Both inphase equivalent and quadrature readings were recorded.

The Double Dipole EM instrument consists of a stable 1.5 m long wooden beam with transmitter and receiver coils mounted one at each end such that the primary signal from the transmitter coil is eliminated at the receiver coil, and thus only secondary signals are recorded, i.e. signals from the ground. The instrument operates at a frequency of 5000 Hz .

In mineral exploration it is usually helpful to know what the magnetic response of a potential target is. A Barringer GM122 portable proton precession magnetometer was included with the instruments. This magnetometer has a resolution of 1 nanoTesla (gamma).
C. On the Pelican project six target areas had been selected based upon earlier geological mapping work. These were: the Pelican Showing, the Southeast area, the Sericite - SJ target, the Pins area, the Snow Zone, and the Lake area, the latter was divided into two survey targets: an airborne EM anomaly, and a ground survey line, the Lake Line.
a. The Pelican Showing was closest to the camp and also the subject of immediate interest due to mineralized samples obtained from the talus on the north side of a cliff, and a gossan on the cliff face. Mapping had shown the possible existence of three intersecting faults or shears in the vicinity. Four east-west survey lines were available within the area of immediate interest: $P 1 N, P 2 N, P 3+25 N$, above the cliff, and P $4+75 \mathrm{~N}$ below the cliff.

The three first lines were surveyed with induced polarization and horizontal loop EM, and all four lines with VLF-EM, Double Dipole EM and magnetics.
b. The Southeast area grid was surveyed on 9 lines: 1 W to 9 W . The grid was cut by a creek, deeply incising overburden and rock. Two of the lines, 5 W and 6 W were covered by horizontal loop EM, 8 lines with VLF-EM, and lines 5 W to 9 W with Double Dipole EM and magnetics.
c. The Sericite - SJ gossan was surveyed by horizontal loop EM by Mr Michael Jones.
d. Further southeast was the Pins area, which was covered by VLF-EM on three lines.
e. Another large gossan area, the Snow Zone, to the east of the camp on or near the top of a mountain, was tested with induced polarization.
f. A helicopter borne EM survey had picked up a sharp, apparently near surface conductor high up on a mountain nearly due south of the camp. In order to locate, and if possible examine this anomaly, the area indicated on the airborne survey was traversed with the Double Dipole EM.
g. Approximately 500 m south of Pelican line P 1 N the Lake line was laid out east to west across the valley. This line was surveyed partly with horizontal loop EM, Double Dipole EM, and magnetics, and the easterly portion with VLF-EM.

The target areas are shown on the location map at a scale of $1: 50,000$, and the grids on the "Grid Locations (1990)" map at a scale of $1: 10,000$. The results of the surveys will be discussed below, and shown on accompanying pseudosections for the induced polarization and VLF-EM surveys. The Double Dipole, horizontal loop EM and magnetics are shown as profiles for each line.

The interpretations are compiled unto individual grid maps at a scale of $1: 2,500$, except for the Lake line for which there are only the profiles and pseudosection.

### 9.2 Pelican Target

A. The induced polarization survey was carried out with an array of six potential dipoles, each 25 m in length ( $a=25 \mathrm{~m}, \mathrm{n}=1-6$ ), where each increment in n increases the depth penetration to give the pseudosection. The locations of the resulting data points are by convention plotted as shown in the legend to the pseudosections.

The IP survey was done on the three lines above the cliff only since the line below the cliff was almost entirely on coarse talus, unsuitable for an electrical survey. The length of the lines which could in practice be covered was limited, and also the ground conditions in several places made it difficult, if not impossible, to inject sufficient current into the ground for synchronization of the receiver to the current pulses, and therefore no readings could be obtained. The area is heavily pyritized, hence the background is quite high. The line P 1 N presented another difficulty in that it passed through the camp, with ensuing interference which most likely caused the negative apparent resistivity values. The results as interpreted from the pseudosections show two or more relatively thin lenses plunging to the south and possibly dipping shallowly to the west. Depth to
significant mineralization is estimated at $20-25 \mathrm{~m}$ under line $\mathrm{P} 3+25 \mathrm{~N}$, although some may be present at shallower depth as it is difficult to separate background from desired response.
B. The horizontal loop EM survey results were influenced by the uneven terrain and the station spacing which had been chained to even distance along the surface. The resulting true coilseparation therefore varied with the topography, with even relatively small differences being amplified by the short, 50 m cable, and hence a noisy inphase response. The quadrature readings are much less affected and have been used in the interpretation. All anomalies are weak, visible only on the two highest frequencies, and especially the highest, 14080 Hz , which is in the VLF-EM range. The horizontal loop EM responds well to horizontal targets, and indeed there is some correspondence between IP and EM anomalies. No conventional "conductor" was found however. On line P 3+25N the EM and IP anomalies are in close proximity about the 100 W station, and also on line P 1 N at $210-215 \mathrm{E}$.
C. As mentioned with the horizontal loop method the responses were best at the highest frequency, in the VLF-EM range. It is then not surprising that the EM-16 VLF-EM instrument would produce better results in terms of outlining anomalies. On the Pelican target the EM-16 survey was done at a station spacing of 12.5 m , and the inphase readings filtered with a type of Hjelt filter to produce pseudosections. The original readings for inphase and quadrature are shown for each station, together with the pseudosection. All the anomalies are weak, but the best one corresponds with the horizontal loop EM and is adjacent to the interpreted IP anomaly at $75-100 \mathrm{~W}$, and flanking on a small magnetic anomaly situated to the west. A remnant of this anomaly on line P 2 N is also associated with the IP anomaly, but is not to be found on line P 1 N , as the depth penetration would be insufficient for a dipping body. Another anomaly is found on line $P 2 N$ at $75-100 \mathrm{E}$ and continues weaker at P 1 N ,but the association with the IP is uncertain due to the interference at the camp. A broader and deeper anomaly occurs further east at $200-225 \mathrm{E}$, also coincident with an IP response. The EM-16 responses on line $P 4+75 N$ were very weak.
D. The Double Dipole EM (DDEM) instrument is intended to locate near surface conductors or narrow conductive features. The responses on the Pelican target grid were very weak, confirming the absence of such features here.
E. The magnetic survey was mostly conducted parallel to the DDEM survey and the results are plotted together also as profiles. The magnetic profiles show some sharp peaks indicating narrow features, some crosscutting the interpreted IP and EM trends. The magnetic peaks are indicated with an M on the anomaly map.

## F. CONCLUSIONS

The VLF-EM survey appears to show structures, or mineralized structures, and the correspondence with the IP is encouraging. The weak anomalies indicate both depth and poor conductivity as seen also with the horizontal loop survey, and confirmed by the DDEM. The magnetic responses associated with the IP tend to indicate the presence of pyrrhotite, as magnetite would be expected to produce stronger peaks than is the case.

Several targets were located during the surveys as shown on the grid/ compilation map. The IP responses were very high, although this can be at least in part explained by the background disseminated pyritic mineralization seen in the rocks.

### 9.3 Southeast Target

A. Horizontal loop EM was used on two lines of the SE grid. In common with the results on the Pelican grid, the anomalies on the SE grid were also weak, although more distinct. The noisy inphase due to topography does not allow a quantitative conductivity thickness to be estimated, but qualitatively the conductivity is poor, as only the two highest frequencies clearly show the anomalies on the quadrature. The anomalies also coincide with VLF-EM anomalies. The anomaly widths are less than 10 m , and centred on L5W/6N and L6W/5N.
B. The EM-16 VLF survey was conducted at two separate frequencies, i.e. using two transmitter stations, NAA at Cutler, Maine, and NLK at Seattle, Washington. The anomalies are mostly different in strength, but also location. The NAA transmitter gave the better responses overall, but it is likely that two different structures were located, one (the NLK induced) being at an oblique angle to the grid. The NAA responses show good line to line correlation for two structures, one near baseline and the other to the south thereof, and on lines 5 W and 6 W also coincide with the horizontal loop anomalies, confirming that the anomalies are more than topographic expressions, and likely to be at least somewhat mineralized along structure. North of the baseline the line to line
correlation is of shorter length. The readings were taken at 25 m intervals so the anomaly resolution is not as high as would have been the case with shorter intervals, but the anomalies do show clearly. While some correlation with magnetics exists it is not consistent. The results are shown in pseudosection form and on the grid/compilation map.
C. The Double Dipole EM survey on the SE grid did not produce any clear anomalies except for an one station response at the baseline on line 7 W which also is coincident with a sharp magnetic peak. A narrow feature is indicated, but not seen in the VLF-EM data, although likely to be a continuation of the horizontal loop anomaly on line 6 W , and not extending to depth. This feature very likely continues to line 8 W where two magnetic peaks coincide with DDEM quadrature responses. However, the inphase response is negative, possibly caused by the magnetics, which also makes an interpretation uncertain. The VLF-EM response is stronger.
D. The magnetic survey shows larger anomalies to the west, and near the baseline magnetic peaks correlate with EM anomalies suggesting sulphide mineralization.

## E. CONCLUSIONS

The EM-16 VLF survey using the Cutler, Maine, transmitter produced the best and most consistent responses. The horizontal loop EM confirmed one of the anomalies, near the baseline, on the two lines surveyed, but this method was plagued by the topographic difficulties. From the results it would appear that the first priority on the SE grid should be placed on the anomaly along the baseline, unless geochemical or other data would favour other targets. The relatively deep overburden of a till-like material seen in the creek gorge has reduced the signal so that few anomalies can be determined with the DDEM.

Apart from the anomaly which closely follows the baseline, two other "conductors" merit attention. One is approximately 125 m south of the baseline, the other approximately 250 m north thereof. The results are shown on pseudosections and as profiles, and also plotted on the map.

### 9.4 Sericite - SJ Zone

A. The Sericite - SJ zone survey grid is situated on a steep slope near the top of a mountain approximately NW of the camp. Two lines of MaxMin I horizontal loop EM were read, lines L2S, and L2+50S. In common with other horizontal loop EM surveys there were difficulties with the inphase readings, and only the quadrature data could be used for interpretation. The two highest frequencies defined a weak anomaly on each line. On L2S the anomaly is very wide, estimated to be about 60 m , while on line L2+50S the anomaly is about 6 m wide. The anomalies are centred at 230 E and 233E, respectively.

### 9.5 Pins - Airborne EM

A. The PINS target area, situated in the southern part of the Pelican property was surveyed by VLF-EM on three lines, L1S, L1N, and L2N, using both the NAA and NLK transmitters. Both transmitter directions gave good anomalies but not usually in the same location. A true north trending set of structures appears most likely, but this cannot be established definitely from the data obtained in this survey. The results are shown in pseudosection form. The anomaly strengths suggest that relatively good conductors exist under this grid. The airborne EM anomalies also show good conductivities, but are not definite regarding anomaly axes. The flight lines are NNE - SSW which would be close to the expected N-S trend of the ground EM anomalies, and thus would not produce recognizable trends in the airborne data. Short but conductive targets trending approximately E-W cannot be ruled out.

### 9.6 Snow Zone

A. Several gossanous outcrops on top of the mountain were the targets of an attempted induced polarization survey. Only a limited amount of data could be obtained since the area is mainly outcrop or coarse talus, thus lacking places to inject sufficient current into the ground to obtain readings. Parts of the baseline and line $4 \mathrm{~N}(4+50 \mathrm{~N}$ ?) were read, and some good anomalies were found.

### 9.7 Lake Airborne EM

A. A very sharp airborne EM response was recorded high on the mountain due south of the Pelican target and the camp. It was an one line feature, but its conductivity thickness product was high with an indicated surface exposure, and of interest for exploration. In order to locate the anomaly the area was traversed with the Double Dipole EM instrument. A very thin graphitic conductor was found, giving DDEM readings of several parts per thousand. The lateral extent was found to be small, since it could only be traced $10-20 \mathrm{~m}$ in each direction from the strongest response. It is assumed that the helicopter traversed right over the best conductivity to produce the recorded response. Other anomalies were found towards the edge of the cliff, though not as strong as the first one, and all of short lateral extent. The rough topography precluded the determination of single or multiple trends. The anomalies were marked but no grid was established. No mineralization of interest could be located.

### 9.8 Lake Reconnaissance Line (Lake Line)

A. The western part of the Lake line was surveyed with horizontal loop EM, but no anomalies were found. Time did not permit continuation of this survey.
B. The eastern part $(0-1100 \mathrm{E})$ was read with EM-16 VLF-EM, at a station spacing of 12.5 m . Several weak to very weak anomalies are seen in the pseudosection.
C. Double Dipole EM and magnetic surveys were done from 275W to 612.5 E . Three very weak DDEM anomalies and three magnetic anomalies (not correlated) were found.

### 9.9 An Overview and Conclusions

Although the survey time was short for a large property such as the Pelican Project, the results were very encouraging, at least from the view of using geophysical techniques to locate targets. Without other corroborating data, however, the economic potential cannot be determined since only physical properties are measured, and in most cases little will be revealed about the actual minerals present.

For future exploration of the Pelican Project it is recommended that the SE and Pins grids be resurveyed with EM-16 at a shorter station interval, and the SE grid be explored further west. The anomaly quality tended to increase somewhat in this direction. The Pins grid also would benefit from fill-in lines and some line extensions to the west, with one or more lines added to the south, topography permitting.

The Snow Zone remains an interesting target, and is recommended for testing with EM-16, and also an SP survey using high impedance electrodes to overcome the ground conditions (except for coarse talus where no technique requiring ground contact would be likely to succeed).

The Pelican property would appear to be well suited to induced polarization surveys from a mineralization point of view, however, the ground conditions and topography would make such surveys generally unsuitable. The IP method requires a current of sufficient amplitude to be injected into the ground to synchronize the receiver, without which no readings are possible. Normally a moist soil is required to make sufficient contact with the current electrodes, thus in an area with outcrop or talus difficulties are encountered. On outcrop sometimes moist soil can be brought in and packed down to produce the contact, but this is a time consuming and cumbersome procedure. On thick talus it becomes impossible to provide the right conditions. The till-like material found $n$ many places also turned out to be too poorly conductive to be of use in for current injection.

The VLF-EM technique using the EM-16 and appropriate filtering to produce pseudosections appears to give the most consistent results. While many of the anomalies will be caused by faults and shears without economic potential they none the less aid in the mapping of an area. Other techniques need to be used to discriminate between responses. A station spacing of $10-15 \mathrm{~m}$ is recommended for the EM-16 surveys to give good definition of the anomalies.

The MaxMin I horizontal loop EM confirmed that the frequencies in the VLF-EM range (15 kHz and above) are generally the most useful in this area. The inphase readings of the HLEM method are critically dependent on a consistent and accurate coil separation. The degree of accuracy depends also on the nominal separation, with higher accuracy required for the shorter cables. On even slopes or in flat terrain it is sufficient to measure the grid along surface, but in uneven terrain chaining to the horizontal plane is most desirable. The horizontal distance together with recorded average slope angles ensures that the appropriate
corrections can be made to obtain smooth data and profiles. On the Pelican property the average slope angles were measured where line of sight existed, however no assurance existed that the station intervals were consistent or corrected for rough topography.

The Double Dipole EM is designed to quickly locate shallow conductive features, such as the Lake Airborne EM anomaly, and would possibly be useful on the PINS grid also to determine anomaly axes. The conditions on the other grids did not appear to favour this technique.

The magnetic surveys were a useful adjunct to the EM surveys.

Roger J. Caven, P. Eng. Consulting Geologist

January 29, 1991

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### 11.0 STATEMENT OF QUALIFICATIONS

I, DENNIS M. GORC, residing at 103-2083 Coquitlam Avenue, in Port Coquitlam, British Columba, V3B 1 J 4 state that:
(1) I graduated from Queen's University, Kingston, Ontario with a B.SC. (Eng.) degree in mineral exploration in May 1976.
(2) Since 1976, I have supervised mineral epxploration programs in British Columbia, N.W.T., Manitoba and Ontario.
(3) I am presently employed as a geologist with Cathedral Gold Corporation, Suite 800-601 West Hastings Street, Vancouver, B.C. V6B 5A6
(4) I supervised the 1990 exploration program on the Pelican property.

Dated this 22 day of $\qquad$ , 1991, in the City of Vancouver, Province of British Columbia.


## CATHEDRAL GOLD CORPORATION

Vancouver, B.C.

## APPENDIX I

## —n

 COST STATEMENT
## COST STATEMENT

## Geological-Geophysical-Geochemical Program August 25-September 15, 1990

## Wages

D. Gorc Aug. 25-27, 29-31, Sept. 2-15 ..... \$5,000
R. M. Jones Aug. 28-Sept. 13 ..... 4,000
N. Bertrand Aug. 25-31, Sept. 1-12, 14 ..... 2,500
B. Murphy Aug. 25-31, Sept. 1-3 ..... 1,200
A. Saltiel Aug. 25-29 ..... 500
D. Philip Aug. 25-29 ..... 500
D. Ross Sept. 7-12, 14 ..... 700
K. Palm Aug. 29-31, Sept. 1-12, 14 ..... 1,600
Travel = Transportation
Airline tickets: Vancouver-Smithers-Vancouver ..... 1,000
MJ, RC (Geophysicist)
Air freight - Air charter (Central Mountain Air) ..... 8,500
Smithers-Bronson Strip
Helicopter - Trans North; Northern Mountain ..... 24,000 ..... 33,500
Camp = Equipment
Food ..... 3,000
Field and camp equipment and supplies ..... 3,500
Radio rental ..... 5007,000
Geophysical
Consulting fees-Geophysics (Roger Caven) Aug. 28-Sept. 13 ..... 5,750

## Geochemical

494 soil samples analyzed for 30 element ICP + gold by Atomic adsorption240 rock samples analyzed for 30 element ICP + gold by atomic adsorption11 Hg analysis by flameless atomic adsorption6,900
Miscellaneous
Report (geologist, secretary, drafting, computer, reproductions) ..... 10,000
Shipping ..... 500
Miscellaneous (courier, telephone, truck rental) ..... $\underline{350}$
10,850
Cost Summary
Wages ..... $\$ 16,000$
Travel-Transportation ..... 33,500
Camp-Equipment ..... 7,000
Geophysical ..... 5,750
Geochemical ..... 6,900
Miscellaneous ..... 10,850
Pelican SW Group - Gossan 4, 5, 8, 9, 22, 25 ..... $\$ 30,000$
Pelican NE Group - Gossan 1, 2, 3, 6, 7 ..... 50,000$\$ 80,000$

## APPENDIX II

GEOPHYSICAL EQUIPMENT

## GEOPHYSICAL EQUIPMENT

The induced polarization equipment consisted of a Scintrex IPR-11 time domain receiver and the Scintrex TSQ-3 transmitter with a 3 kVA motorgenerator. The transmitter output is a squarewave current of 2 seconds on and 2 seconds off with every second on pulse alternating in polarity. The receiver reads the primary voltage during current on to determine resistivity, and the secondary decaying voltage during off intervals. The decaying secondary, or induced voltage is measured in 10 consecutive intervals, windows (or slices $0-9$ ), of which the slice number 7 is normally used for the interpretation of chargeability (IP effect). The IPR-11 is able to read the voltage between six pairs of potential electrodes simultaneously. The electrode pairs form an array with each pair probing to a depth determined by its order and the ground resistivity. The results are shown as a pseudosection.

The chargeability is interpreted relative to the background readings, and therefore the anomalies are not absolute, but apparent.

The MaxMin I horizontal loop EM system is the latest development by APEX Parametrics, and features eight frequencies from $220-14080 \mathrm{~Hz}$, five of which were used on the Pelican Project. The horizontal loop EM has two coils (or antennas) to be held co-planar, one transmitting the sine-wave signal and the other receiving a combination of primary and secondary voltage, out of phase with the transmitted signal. The connecting reference cable enables the receiver to determine the phase shift, and thus determine the inphase and quadrature components of the received signal. The inphase component includes the primary voltage, the strength of which is determined by the intercoil separation to the third power. When the received signal is of low amplitude, as was the case at the Pelican property any errors in the coil separation cause large variations in the inphase component overwhelming the desired signal. Accurate determination of true coilseparation and a coplanar alignment of the coils makes possible precise corrections. The quadrature component is but little affected. The anomaly width is the width of the conductor plus the coilseparation.

The Geonics (Ronka) EM-16 is a low frequency radiowave receiver in the $15-25 \mathrm{kHz}$ range. The radio transmitters are the Naval submarine communications transmitters located in the US and other parts of the world. The magnetic component of the long radio waves locally follow the topography unless a conductive feature cause them to tilt relative to the ground surface. This tilt angle is measured together with an out of phase component. The tilt angle is a measure of the inphase component, and because of the great distance to the transmitter the radiowaves behave as plane waves and provide an even "illumination" over a large area, unlike the very local behaviour of the primary signal in the horizontal loop configuration.

Since the tilt angle is measured in the VLF (Very Low Frequency) survey, the direction of measurement determines the sign of the tilt. In the direction of travel and reading the change of tilt from positive to negative, relative to ground slope, signals the presence of a "conductor". Since the measurement of ground slope for each station is cumbersome, a filter technique is employed to remove the ground slope from the data, and at the same time convert the change of tilt angle into a positive peak over the conductor. The present filter is sensitive to weak conductors and effectively removes topographic effects. In order to avoid undue noise created by less than exact readings a lowest contour of +1 is used throughout, and attention is usually paid to values above +2 . Values of filtered data less than $10 \%$ are classified as weak, although they may signify important mineralization or other ground condition to be investigated.

The Double Dipole EM by APEX Parametrics consists of a stable wooden beam with inclined parallel transmitter and receiver coils, one at each end. A sine wave at 5000 Hz is transmitted. The principle is similar to the horizontal loop EM except that the inclination of the coils combined with a precise separation makes it possible to eliminate the primary transmitted signal from the receiver coil, which then only records the secondary voltages emanating from the ground. Sensitivity is thus enhanced, and it is possible to read signals in ppm of primary voltage. The 1.5 m coil separation diminishes the depth penetration, especially in conductive terrains.

The DDEM has been useful in locating small conductive targets, and because it can be read while traversing precise locations can be obtained quickly without grids. Coincident positive inphase and quadrature peaks indicate conductors. Good conductors normally read 1000 $10,000 \mathrm{ppm}$, as did the graphite band at the airborne anomaly. The Pelican and SE grids had much smaller values.

## APPENDIX III

## SJ ZONE - GEOPHYSICAL PLOTS

## Max-Min Horizontal Loop EM

Sericite L2S, L2+50S


APPENDIX IV
SOUTHEAST GRID - GEOPHYSICAL PLOTS
EM-16 (Seattle, Washington)
L1W, L2W, L3W, L4W, L5W, L6W, L7W, L8W
EM-16 (Cather, Maine)L1W, L2W, L3W, L4w, L5W, L6W, L7W, L8W
Max-Min Horizontal Loop EM
L5W, L5W
Double Dipole EM and Magnetics
L5W, L6W, L7W, L8W, L9W

Project: Cathedral Gold Corp/ Pelican Line\#: SE 1 EM16 Seattle


Project: Cathedral Gold Corp/ Pelican Line\#: SE 2 EM16 Seattle


Project: Cathedral Gold Corp/ Pelican Line\#: SE 3 EM16 Seattle

- Str Inch Quad $n$ ni ni ni ni ns
$-250 \mathrm{~N} \quad 16.0 \quad 4.0$
$225 \mathrm{~N} \quad 13.0 \quad 6.0$ $200 \mathrm{~N} \quad 16.0 \quad 7.0$ $175 \mathrm{~N} \quad 14.0 \quad 6.0$ $150 \mathrm{~N} \quad 16.0 \quad 8.0$ $125 \mathrm{~N} \quad 19.08 .0$ LON $20.0 \quad 10.0$ $75 N \quad 19.0 \quad 8.0$ $50 \mathrm{~N} \quad 16.0 \quad 5.0$ $25 \mathrm{~N} \quad 16.0 \quad 2.0$ $000 \quad 15.0 \quad 3.0$ $25 \$ 17.0 \quad 3.0$ $505 \quad 17.0 \quad 3.0$ $755 \quad 17.0 \quad 3.0$ $1005 \quad 17.0 \quad 4.0$ 125522.02 .0 $1505 \quad 18.0 \quad 3.0$ $175521.0 \quad 4.0$ 2005 24.0
4.0
225524.0 .4 .0
$2505 \quad 22.0 \quad 6.0$

Project: Cathedral Gold Corp/ Pelican Line\#: SE 4 EM16 Seattle





Project: Cathedral Gold Corp/ Pelican Line\#: SE 7 EM16 Seattle

| Stn | Inph Quad | $n 1$ | $n 2$ | $n 3$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |

$[\quad 275 \mathrm{~N} \quad 5.0 \quad 0.0$
$250 \mathrm{~N} \quad 8.0 \quad 0.0$



| -2.1 | -5.3 | -2.4 |
| :--- | :--- | :--- |


| -3.9 | -6.1 | -4.2 |
| :--- | :--- | :--- |

$100 \mathrm{~N} \quad 11.0-5.0$
$75 \mathrm{~N} \quad 12.0 \quad 2.0$
$50 \mathrm{~N} \quad 13.0-4.0$
$25 \mathrm{~N} \quad 12.0-1.0$
$000 \quad 8.0-2.0$
$255 \quad 9.0-2.0$
$505 \quad 8.0-1.0$
$75 \$ \quad 7.0-2.0$

1005 5.0-2.0
$1255 \quad 0.0-2.0$
$-2.7 \quad-4.6$
$-0.1$
$-2.1$
$-1.5$
$-2.0$
$2005-7.0 \quad 2.0$
$2255 \quad 0.0 \quad 3.0$

Project: Cathedral Gold Corp/ Pelican Line\#: SE 8 EM16 Seattle


Project: Cathedral Gold Corp/ Pelican Line\#: SE 1 EM16 Cutler


T 300N 20.02 .0 $275 \mathrm{~N} \quad 22.0 \quad 3.0$ $250 \mathrm{~N} \quad 16.0 \quad 2.0$ $225 \mathrm{~N} \quad 15.0 \quad 2.0$ 200N $\quad 15.0 \quad 2.0$ $175 \mathrm{~N} \quad 12.0-1.0$
$150 \mathrm{~N} \quad 9.0 \quad 0.0$ $125 \mathrm{~N} \quad 13.0 \quad 2.0$

100N 20.0-2.0 $75 \mathrm{~N} \quad 14.0 \quad 0.0$ $50 \mathrm{~N} \quad 18.0 \quad 0.0$ $25 \mathrm{~N} \quad 22.0-2.0$
$000 \quad 22.0-2.0$ $255 \quad 20.0 \quad 0.0$ $505 \quad 15.0 \quad 2.0$ $755 \quad 17.0 \quad 2.0$
$1005 \quad 15.0 \quad 0.0$
$1255 \quad 15.0 \quad 1.0$
$1505 \quad 18.0 \quad 4.0$
$1255 \quad 18.0 \quad 4.0$
$2005 \quad 20.0 \quad 4.0$
$225515.0 \quad 6.0$
$2505 \quad 15.0 \quad 7.0$
$2755 \quad 17.0 \quad 10.0$
$300515.0 \quad 10.0$
$-3.5$
$-0.2$
$0.2-0.0$
$-1.6 \quad-1.4 \quad-3.5$


$\begin{array}{lll}-0.9 & -4.2 & -1.1\end{array}$
$\begin{array}{lll}-2.9 & -3.4 & -4.8\end{array}$


$\underbrace{1.3}_{1.4} \frac{1.3}{1.0}$
$-3.0$
$-3.0$
0.2

* 1.3

Project: Cathedral Gold Corp/ Pelican Line\#: SE 2 EM16 Cutler


Project: Cathedral Gold Corp/ Pelican Line\#: SE 3 EM16 Cutler


Project: Cathedral Gold Corp/ Pelican Line\#: SE 4 EM16 Cutler


Project: Cathedral Gold Corp/ Pelican Line\#: SE 5 EM16 Cutler

T $275 \mathrm{~N} \quad 22.0 \quad 0.0$

- 250N 20.0-3.0
$225 \mathrm{~N} \quad 25.0-3.0$

$-1.8$

$-3.5$
$200 \mathrm{~N} \quad 20.0-3.0$
$175 \mathrm{~N} \quad 25.0-2.0$
$150 \mathrm{~N} \quad 20.0-3.0$
$125 \mathrm{~N} \quad 21.0 \quad 0.0$
100N $\quad 14.0-4.0$
75N $14.0-4.0$
$50 \mathrm{~N} \quad 16.0-8.0$
$25 \mathrm{~N} \quad 5.0-8.0$
$000 \quad 20.0 \quad 8.0$
$25 \$ 14.0 \quad 2.0$
$505 \quad 15.0 \quad-3.0$
$755 \quad 15.0 \quad 4.0$
$1005 \quad 10.0 \quad 2.0$
$1255 \quad 19.0 \quad 5.0$
$1505 \quad 15.0 \quad 8.0$
$1755 \quad 13.0 \quad 7.0$
$2005 \quad 12.0 \quad 6.0$
$225511.0 \quad 5.0$
$250510.0 \quad 10.0$
27598.07 .0
$3005 \quad 9.0 \quad 9.0$

Project: Cathedral Gold Corp/ Pelican Line\#: SE 6 EM16 Cutler



Project: Cathedral Gold Corp/ Pelican Line\#: SE 8 EM16 Cutler




SE Gind L 5 K


Cathedral Cold Corponation - Pelican Project
se Girid 4 6H


Cathedral Gold Conponation - Pelican Project
sk Girid 4 in


Cattedral Cold Corporstion - Pelican Project

SI Grid L 8 \%


SE Grid L g g


## APPENDIX V

# PELICAN GRID - GEOPHYSICAL PLOTS 

EM-16 (Seattle, Washington)<br>L1N, L2N, L3+25N, L4+75N<br>Max-Min I Horizontal Loop EM<br>L1N, L2N, L3+25N<br>Double Dipole EM and Magnetics<br>L1N, L2N, L3+25N, L4+75N<br>Induced Polarization<br>L1N, L2N, L3+25N

Project: Cathedral Gold Corp/ Pelican Line\#: P $1 N$ EM16 Seattle


| Project: | Cathedral/ Pelican |  |  |  | Line: | IN Con | d. . . 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Stn | Inph | Quad | n1 | n2 | n3 | n4 | n5 |
| 25W | -2.0 | 6.0 |  | -1.0 |  | $-1.4$ |  |
|  |  |  | 0.1 |  | $-1.3$ |  | $-1.6$ |
| 37.5W | $-2.0$ | 6.0 |  | -0.1 |  | -1. 5 |  |
|  |  |  | -0.3 |  | -0.3 |  | -1.9 |
| 50W | -2.5 | 6.0 |  | -0.4 |  | -0. 5 |  |
|  |  |  | -0.2 |  | -0.6 |  | -1 |
| 62.5W | $-3.0$ | 6.0 |  | -0.5 |  | -0.9 |  |
|  |  |  | -0.2 |  | -0.6 |  | $-1.0$ |
| 75W | $-3.5$ | 5.0 |  | -0.4 |  | -0.7 |  |
|  |  |  | -0.3 |  | -0.4 |  | $-2.0$ |
| 87.5W | -4.0 | 6.0 |  | -0.1 |  | $-1.7$ |  |
|  |  |  | 0.1 |  | -1.5 |  | -1.7 |
| 100W | -4.0 | 6.0 |  | $-1.1$ |  | $-1.5$ |  |
|  |  |  | -1.2 |  | $-1.2$ |  | -1.4 |
| 112.5 W | -6.0 | 5.0 |  | -1.2 |  | -1.2 |  |
|  |  |  | 0.1 |  | $-1.3$ |  | 0.1 |
| 125W | $-6.0$ | 5.0 |  | -0.1 |  | 0.0 |  |
|  |  |  | -0.1 |  | 1.2 |  | 0.7 |
| $137.5 W$ | $-6.0$ | 5.0 | $\square$-1 | 1.2 |  | 2.0 |  |
|  | -4.0 | 6.0 | $\square 1.1$ | 1.7 | 1.8 | 1. | 2.0 |
| 150W |  |  | 0.5 |  | 1.9 |  | 2.0 |
| 162.5 W | $-3.0$ | 6.0 |  | 0.5 |  | 1.9 |  |
|  |  |  | -0.1 |  | 0.5 | $\bigcirc$ |  |
| 175W | -3.0 | 6.5 |  | -0.1 |  | 0.7 |  |
|  |  |  | -0.0 |  | -0.1 |  |  |
| 187.5W | $-3.0$ | 7.0 |  | 0.0 |  |  |  |
|  |  |  | 0.1 |  | $-0.7$ |  |  |
| 200W | $-3.0$ | 7.0 |  | -0.6 |  |  |  |
|  |  |  | -0.6 |  |  |  |  |
| 212.5W | -4.0 | 6.0 |  | -0.5 |  |  |  |
|  |  |  | 0.1 |  |  |  |  |
| 225W | -4.0 | 5.0 |  |  |  |  |  |
|  |  |  | 0.1 |  |  |  |  |
| $237.5 W$ | -4.0 | 6.0 |  |  |  |  |  |
| 250W | $-5.0$ | 5.0 |  |  |  |  |  |



Project: Cathedral/ Pelican Line: $P 2 N$ cont'd... 2

- stn Inph Quad $n$ 100W-10.0 9.0
n1 n2 n3 n4 n5 $112.5 \mathrm{~W}-10.0 \quad 8.5$ 125W-10.0 9.0 $137.5 \mathrm{~W}-10.0 \quad 11.0$ 150W -8.0 12.0 $162.5 \mathrm{~W}-8.0 \quad 11.0$ $175 \mathrm{~W}-6.0 \quad 12.0$ 187.5W -7.0 13.0 200W-8.0 12.0 $212.5 \mathrm{~W} \quad-8.0 \quad 11.0$ 225W-9.0 10.0 237.5W-10.0 9.0 250W-11.0 7.0

Project: Cathedral Gold Corp/ Pelican Line\#: P $3+25 N$ EM16 Seattle


| Stn | Inph | Quad | $n 1$ | n2 |
| :---: | :---: | :---: | :---: | :---: |
| 112.5W | -16.0 | 3.0 |  | 0.0 |
|  |  |  | -0.1 |  |
| 125W | -16.0 | 2.5 |  | $-0.3$ |
|  |  |  | -0.1 |  |
| 137.5W | -16.0 | 2.0 |  | 0.4 |
|  |  |  | 0.6 |  |
| 150W | -15.0 | 2.0 |  |  |
|  |  |  | -0.1 |  |
| 162.5W | -15.0 | 1.0 |  |  |
| $175 W$ | -14.0 | 0.5 |  |  |

Line: $P 3+25 N$ cont'd... 2
n3 n4 n5

Project: Cathedral Gold Corp/ Pelican Line\#: P 4+75N EM16 Seattle


$$
\begin{array}{lrr|cccccc}
\text { Project: Cathedral/ Pelican } & & \text { Line: P } 4+75 \mathrm{~N} & \text { cont'd...2 } \\
\text { Stn } & \text { Inph } & \text { Quad } & \mathrm{n} 1 & \mathrm{n} 2 & \mathrm{n} 3 & \mathrm{n} 4 & \mathrm{n} 5 \\
337.5 \mathrm{~W} & -16.5 & -1.5 & & -0.7 & & & \\
350 \mathrm{~W} & -17.0 & 0.0 & -0.3 & & -0.7 & & \\
362.5 \mathrm{~W} & -17.0 & -2.0 & 0.1 & -0.3 & & & \\
375 \mathrm{~W} & -18.0 & -2.5 & -0.6 & -0.6 & & & \\
387.5 \mathrm{~W} & -17.0 & -2.0 & 0.6 & & & & \\
400 \mathrm{~W} & -17.0 & -2.0 & & & & & \\
3
\end{array}
$$






Cathedral Gold Conponation - Pelican Pruject
rellican la 4


Cathedral Gold Corponation - Pelican Project







Logarithmic Contours 1.1.5.2.3.5.7.5.10....
Receiver: Seintrex IPR-11
Transmitter: Scintrex TSO-3
Operator: Roger J Caven
INTERPRETATION

- Strong increase in polarization acconpanied
by narked decrease in resistiving
- Well defined increase in polarization
without marked resistivity decrease.
- Poorly defined polarization increase
with no resistivily signature
- Low resistivity feature.


## RGBERT S. MIDDLETON

 EXPLORATION' SERVICES INC. CATHEDRAL GOLD CORPGRATIONNDUCED POLARIZATION SURVEY PELICAN PROJECT NW British Coluct

| NW British Columbia |  |
| :--- | :--- |
| Date: September 1990 | Scale $=1: 1250$ |
| Interp. by: R JC | M |

## APPENDIX VI

## PINS GRID - GEOPHYSICAL PLOTS

EM-16 (Seattle, Washington)
L1S, L1N, L2N

EM-16 (Cather, Maine)
(L1S, L1N, L2N)

Project: Cathedral Gold corp/ Pelican Line\#: PIN 15 EM16 Seattle


Project: Cathedral Gold Corp/ Pelican Line\#: PIN $1 N$ EM16 Seattle


Project: Cathedral Gold Corp/ Pelican Line\#: PIN $2 N$ EM16 Seattle


Project: Cathedral Gold Corp/ Pelican Line\#: PIN 15 EM16 Cutler


Project: Cathedral Gold Corp/ Pelican Line\#: PIN $1 N$ EM16 Cutler


Project: Cathedral Gold Corp/ Pelican Line\#: PIN 2N EM16 Cutler


# APPENDIX VII <br> <br> SNOW GRID - GEOPHYSICAL PLOTS 

 <br> <br> SNOW GRID - GEOPHYSICAL PLOTS}

## Induced Polarization

LB1, LAN



## APPENDIX VIII

## LAKE - GEOPHYSICAL PLOTS

EM-16 (Seattle, Washington)

Max-Min I - Horizontal Loop EM

Double Dipole EM and Magnetics



resican lake une


Cathedral Gold Corporation - Pelican Project


Project: Cathedral Gold Corp/ Pelican Line\#: Lake-line EM16 Seattle

- 1100E $38.0 \quad 9.0$
1087.5E $35.0 \quad 8.0$ $28.0 \quad 6.0$ $1062.5 E$ 1050E $\begin{array}{rrr}1037.5 \mathrm{E} & 32.0 & 8.0 \\ 1025 \mathrm{E} & 35.0 & 8.0\end{array}$ $\begin{array}{rrr}1012.5 E & 34.5 & 8.0 \\ 1000 E & 32.0 & 6.0 \\ 987.5 E & 28.0 & 6.0 \\ 975 E & 27.0 & 3.0\end{array}$ $962.5 \mathrm{E} \quad 27.0 \quad 2.0$

950 E 937.5
$925 E$ 912.5 E
$900 E$ 25.5
8.0 $887.5 \mathrm{E} \quad 25.0 \quad 7.0$ 875E $25.0 \quad 7.0$ $862.5 E \quad 23.0 \quad 6.0$

850 E $837.5 \mathrm{E} \quad 24.0 \quad 4.0$

825E 18.53 .0 812.5E $17.0 \quad 3.0$

800E 19.0 3.0
$787.5 \mathrm{E} \quad 15.0 \quad 3.0$
$.775 E 14.5 \quad 4.0$
762.5E $14.0 \quad 5.0$


APPENDIX IX

GEOCHEMICAL ANALYSES

Cathedral Gold Corp．PROJECT 8103
800－601 W．Hastings St．Vancouver BC V6B 5A6
File \＃90－4205
Submitted by：D．GORE
Page 1

| SAMPLE\＃ | $\begin{gathered} \text { Mo } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \text { Cu } \\ \text { ppm } \end{array}$ | Pb ppm | $\begin{array}{r} 2 n \\ \text { ppm } \end{array}$ | ing $\text { ppn } p$ | $\begin{array}{r} \text { Ni } \\ \text { ppon } \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { pppm } \end{array}$ | $\begin{array}{r} \mathrm{Mn} \\ \mathrm{ppm} \end{array}$ |  | $\begin{gathered} \text { Rs. } \\ \text { ppm. } \end{gathered}$ | $\begin{array}{r} U \\ \text { ppon } \end{array}$ | Au ppm | Th ppm | $\begin{array}{r} \mathrm{Sr} \\ \mathrm{ppm} \\ \hline \end{array}$ | $\stackrel{\mathrm{cd}}{\mathrm{ppm}}$ | Sb | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} v \\ \text { ppm } \end{array}$ | $\begin{gathered} \text { Ca } \\ \text { \% } \end{gathered}$ | $\%$ | $\begin{aligned} & \mathrm{La} \\ & \mathrm{pppm} \end{aligned}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \mathrm{Mg} \\ \% \end{array}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ |  |  | $\begin{gathered} \mathrm{Al} \\ \boldsymbol{X} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \boldsymbol{\%} \end{gathered}$ |  | ppint | $\begin{aligned} & A^{*} \\ & \mathrm{ppb} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PE | 4 | 39 | 37 | 9 | ，4 | 10 | 4 | 169 | 6.05 | 2 | 5 | ND | 1 | 4 | 2 | 2 | 2 | 3 | ． 08 | \％009 | 2 | 9 | ． 04 | 22 | \％ 01 | 2 | ． 09 | ． 01 | ． 04 | 1 | 1121 |
| PEL－90－ | 5 | 76 | 5 | 8 | \％ | 43 | 76 | 567 | 16.20 | 15 | 5 | ND | 1 | 18 | 8 | 2 | 7 | 5 | ． 45 | ． 005 | ． 2 | 7 | ． 39 | 6 | OS | 2 | ． 34 | ． 01 | ． 01 | 1 | 25 |
| PEL－90－G－3 | 6 | 36 | 2 | 8 | 3 | 32 | 57 | 445 | 14.19 | 7 | 5 | ND | 1 | 13 | ． 5 | 2 | 5 | 7 | ． 27 | ． 010 | 2 | 40 | ． 52 | 9 | 01 | 2 | ． 53 | ． 01 | ． 03 | \％ | 11 |
| PEL－90－G－4 | 8 | 2478 | 782 | 1081 | 1\％2 | 12 | 20 | 132 | 14.42 | 401 | 5 | ND | 1 | 3 | 6.7 | 4 | 2 | 12 | ． 03 | ，022 | 4 | 10 | ． 10 | 9 | \％18． | 3 | ． 21 | ． 01 | ． 04 | \％ | 827 |
| PEL－90－G－5 | 1 | 312 | 271 | 378 | 16.0 | 20 | 9 | 2879 | 8.12 | 334 | 5 | ND | 2 | 289 | 2．3 | 4 | 2 | 99 | 1.77 | 180 | 11 | 34 | 1.58 | 18 | 32 | 2 | 2.12 | ． 01 | ． 02 |  | 21 |
| PE | 4 | 446 | 47 | 242 | 2 | 7 | 14 | 1890 | 5.16 | 45 | 5 | ND | 1 | 65 | \＄9 | 2 | 2 | 12 | 1.56 | －025 | 2 | 31 | ． 16 | 6 | 08 |  | ． 20 | ． 01 | ． 01 | \％ 1 | 27 |
| PEL－90－6 | 8 | 77 | 48 | 5693 | 1.1 | 7 | 7 | 993 | 20.80 | 162 | 5 | ND | 2 | 4 | 32．8． | 2 | 3 | 7 | ． 12 | ，003． | ＋ 3 | 7 | ． 07 | 22 | 01 | 2 | ． 04 | ． 01 | ． 02 | 10. | 99 |
| PEL－90－6－8 | 31 | 233 | 210 | 1312 | 5．9 | 11 | 12 | 645 | 9.88 | 304 | 5 | ND | 1 | 129 | 8．9． | 5 | 3 | 42 | ． 98 | ． 61 | 3 | 14 | ． 10 | 9 | 34 | 2 | ． 44 | ． 01 | ． 01 | 2 | 105 |
| PEL－90－G－9 | 1 | 1124 | 171 | 21319 | 10．7 | 2 | 23 | 2823 | 25.08 | 116 | 5 | ND | 2 | 10 | 132.8 | 2 | 2 | 5 | ． 88 | ．003． | － 4 | 3 | ． 08 | 6 | 01 | 2 | ． 03 | ． 01 | ． 01 | 30. | 285 |
| PEL－90－G－10 | 12 | 4152 | 174 | 1604 | 15 | 21 | 39 | 1425 | 9.10 | 337 | 5 | ND | 1 | 207 | 12，6 | 7 | 7 | 40 | 1.92 | \％99\％ | 5 | 23 | ． 40 | 7 | 29 | 2 | ． 75 | ． 01 | ． 02 | ！ | 200 |
| PEL－90－G－10（ | 3 | 272 | 1895 |  | 22.5 | 25 | 18 | 1378 | 6.68 | 288 | 5 | ND | 1 | 175 | 10．2 | 8 | 2 | 64 | 1.35 | ＊64 | ＋ 5 | 61 | ． 55 | 22 | 32 |  | ． 86 | ． 01 | ． 05 | \％$\downarrow$ | 140 |
| PEL－90－G－11 | 2 | 1034 | 2064 | 18217 | 14.2 | 14 | 20 | 708 | 10.77 | 319 | 5 | ND | 1 | 34 | 105．8． | 9 | 2 | 23 | ． 26 | 8023 | ＋ 3 | 16 | ． 27 | 3 | ．04 | 2 | ． 36 | ． 01 | ． 01 | \％$\%$ | 333 |
| PEL－90－G－12 | 9 | 639 | 494 | 15981／ | 5．0 | 34 | 20 | 1526 | 7.87 | 375 | 5 | ND | 1 | 71 | 86．2 | 6 | 2 | 36 | ． 77 | \％104 | ＋ 3 | 66 | ． 52 | 7 | 18. | 2 | ． 69 | ． 01 | ． 02 | $\geqslant 7$ | 276 |
| PEL－90－G－13 | 5 | 389 | 762 | 13020／／ | 6．7． | 33 | 23 | 1495 | 8.26 | 499 | 5 | ND | 1 | 122 | 68.8 | 8 | 2 | 42 | ． 92 | ． 132 | 2 3 | 77 | ． 66 | 13 | 17. | 2 | ． 98 | ． 01 | ． 01 | 4 | 128 |
| PEL－90－G－14 | 3 | 177 | 193 | 734 | 30．8． | 2 | 6 | 695 | 21.09 | 527． | 5 | ND | 1 | 5 | 2.2 | 5 | 10 | 5 | ． 19 | 006 | 3 | 3 | ． 14 | 10 | O1． | 2 | ． 02 | ． 01 | ． 01 | 14. | 1796 |
| PEL－90－G－14（A） | 4 | 93 | 746 | 570 | 6．6． | 68 | 50 | 1948 | 12.57 | 457． | 5 | ND | 1 | 178 | 5.5 | 8 | 2 | 59 | 1.74 | ． 192 | 5 | 74 | ． 85 | 10 | ，30 |  | 1.29 | ． 01 | ． 02 | \％ | 77 |
| PEL－90－G－15 | 1 | 316 | 151 | 3802 | 17\％ | 7 | 40 | 2466 | 16.91 | 54 | 5 | ND | 1 | 36 | 12．5 | 2 | 2 | 8 | 4.07 | ．002 | 5 | 5 | ． 06 | 2 | ， 01 | 2 | ． 05 | ． 01 | ． 01 | 7. | 98 |
| PEL－90－G－16 | 5 | 15 | ， | 39 | $\stackrel{2}{2}$ | 8 | 7 | 478 | 7.99 | 2 | 5 | ND | 2 | 19 | $\cdots 3$ | 2 | 3 | 2 | ． 56 | ．030 | 2 | 35 | ． 19 | 22 | ． 01 | 2 | ． 19 | ． 01 | ． 10 | 4 | 1796 |
| PEL－90－G－17 | 2 | 21 | 4 | 26 | －4 | 6 | 11 | 508 | 5.28 | 8 | 5 | ND | 7 | 42 | ． 2 | 2 | 2 | 5 | 1.13 | ． 077 | 5 | 4 | ． 23 | 40 | 014 | 2 | ． 35 | ． 01 | ． 12 | 1 ， | 40 |
| PEL－90－G－18 | 6 | 12 | 4 | 15 |  | 7 | 10 | 804 | 2.83 | 3 | 5 | ND | 6 | 38 | ， 2 | 2 | 2 | 4 | 1.08 | ． 074 | 3 | 6 | ． 35 | 55 | ． 01 | 2 | ． 40 | ． 01 | ． 13 |  | 15 |
| PEL－90－G－19 | 4 | 19 | 2 | 48 | \％$<1$ | 6 | 9 | 511 | 4.33 | 2 | 5 | ND | 5 | 25 | ． 2 | 2 | 2 | 3 | ． 64 | ．050 | ， 3 | 6 | ． 25 | 36 | 01， |  | ． 33 | ． 01 | ． 10 | \％ | 3 |
| PEL－90－G－20 | 5 | 17 | 4 | 8 | \％1 | 7 | 12 | 447 | 4.98 | 4 | 5 | ND | 4 | 32 | －2 | 2 | 3 | 3 | ． 78 | ． 055 | 3 | 28 | ． 18 | 36 | 04 | 2 | ． 32 | ． 01 | ． 12 | 1 | 27 |
| PEL－90－G－21 | 1 | 34 | 5 | 77 | $\stackrel{+}{3}$ | 9 | 26 | 976 | 8.66 | 3 | 5 | ND | 3 | 55 | ¢， 2 | 2 | 2 | 81 | ． 33 | ， 098 | 4 | 30 | 2.29 | 40 | ． 28 | 2 | 1.97 | ． 02 | ． 06 | 1. | 9 |
| PEL－90－G－22 | 3 | 4 | 2 | 11 | $\bigcirc$ | 9 |  | 48 | 2.31 | 2 | 5 | ND | 1 | ， | $\stackrel{2}{2}$ | 2 | 2 | 1 | ． 01 | ． 004 | ＋ 2 | 8 | ． 01 | 22 | ．01 | 2 | ． 03 | ． 01 | ． 01 | 1 | 599 |
| PEL－90－G－23 | 6 | 79 | 3 | 9 | 4.5 | 13 | 3 | 42 | 1.46 | ？ | 5 | ND | 1 | 2 | $\stackrel{2}{2}$ | 3 | 2 | 1 | ． 01 | 0012 | 2 | 9 | ． 01 | 15 | O1， | 3 | ． 03 | ． 01 | ． 02 | ＊ | 33 |
| PEL－90－ | 8 | 5 | 2 | 8 | ¢ | 16 | 10 | 261 | 1.97 | \％ | 5 | ND | 1 | 2 | \％ 2 。 |  |  | 1 | ． 01 | －004 | 4 | 69 | ． 01 | 7 | ，01， | 2 | ． 02 | ． 01 | ． 01 | \％ | 85 |
| PEL－90－G－25 | 3 | 12 | 3 | 57 | $\bigcirc$ | 5 | 4 | 565 | 3.06 | \％ 2 | 5 | ND | 3 | 87 | \％$\nabla^{3}$ | 2 | 2 | 38 | ． 41 | \％44 | ＋ 5 | 6 | 1.24 | 33 | 13 | 2 | 1.64 | ． 03 | ． 09 | 1 | 12 |
| PEL－90－G－26 | 4 | 6 | 2 | 40 | \％ 1 | 6 | 7 | 238 | 3.27 | 2 | 5 | ND | 9 | 35 | \％$\% 2$ | 2 | 2 | 42 | ． 30 | 8095 | 5 | 7 | ． 96 | 40 | ．09． | 2 | 1.13 | ． 06 | ． 06 | － | 10 |
| PEL－90－6－27 | 4 | 5 | 2 | 35 | \％ 3 | 7 | 4 | 273 | 2.15 | 2 | 5 | ND | 5 | 48 | －3 | 2 | 2 | 35 | ． 37 | ．083 | 5 | 7 | ． 99 | 28 | 09 | 2 | 1.17 | ． 05 | ． 05 | 1 | 5 |
| PEL－90－G－28 | 2 | 66 | 3 | 77 | 相 | 18 | 12 | 494 | 4.12 | 2 | 5 | ND | 1 | 28 | ， | 2 | 2 | 64 | ． 33 | ．096 | ＊ 2 | 47 | 2.16 | 66 | 10 | 2 | 1.81 | ． 05 | ． 13 | \％ | 10 |
| PEL－90－G－29 | 2 | 10 | 7 | 30 | ＊ 2 | 3 | 2 | 265 | 2.31 | \％ | 5 | ND | 5 | 46 | 的 ${ }^{3}$ | 2 | 2 | 44 | ． 32 | \＄36 | 5 | 6 | ． 87 | 116 | 15． | 2 | 1.11 | ． 03 | ． 14 | \％ | 15 |
| PEL－90－G－30 | 10 | 10 | 4 | 10 | \％ 2 | 15 | 56 | 185 | 4.03 | \％ 6 | 5 | ND |  | 209 | \＃$\geqslant 2$ | 2 | 2 | 14 | ． 95 | －052 | ＋ | 12 | ． 19 | 47 | 06 |  | ． 97 | ． 01 | ． 10 | \％ | ＋ 4 |
| PEL－90－G－31 | 2 | 5 | 3 | 36 | ，2 | 32 | 13 | 413 | 5.49 | 25 | 5 | HD | 2 | 14 | 3 | 2 | 2 | 37 | ． 24 | 157． | 2 | 27 | 1.70 | 69 | 17 | 2 | 1.51 | ． 02 | ． 18 | \％ 1 | 3 |
| PEL－90－G－32 | 4 | 1 | 6 | 31 | $\stackrel{1}{1}$ | 5 | 5 | 580 | 2.66 | 2 | 5 | ND | 3 | 125 | 2 | 2 | 2 | 24 | ． 68 | 117 | 7 | 11 | 1.44 | 412 | 10 | 2 | 1.75 | ． 02 | ． 11 | \％ | 1 |
| PEL－90－G－33 | 3 | 1 | 4 | 32 | $\stackrel{1}{2}$ | 5 | 17 | 558 | 3.54 | 3 | 5 | ND | 2 | 189 | 2 | 2 | 2 | 24 | ． 86 | 120 | 6 | 4 | 1.13 | 81 | 09 | 2 | 1.64 | ． 01 | ． 11 | \％ | 4 |
| PEL－90－G－34 | 3 | 2 | 3 | 64 | 2 | 6 | 5 | 639 | 2.22 | 2 | 5 | ND | 1 | 123 | 3 | 2 | 2 | 19 | ． 61 | －074 | 4 | 6 | 1.12 | 392 | －07． | 2 | 1.39 | ． 01 | ． 08 | 1 | 1 |
| STANDARD C／AU－R | 19 | 58 | 40 | 133 | 7．1 | 73 | 31 | 1047 | 3.97 | 41 | 20 | 7 | 40 | 52 | 19．0 | 16 | 20 | 60 | ． 52 | ． 098 | 40 | 60 | ． 89 | 176 | 09. | 36 | 1.89 | ． 06 | ． 13 | 11 | 520 |

ICP－． 500 GRAM SAMPLE IS DIGESTED HITH 3ML 3－1－2 HCL－HNO3－h20 at 95 DEG．C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER．
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B 4 AND LIMITED FOR NA K AND AD AU DETECTION LIMIT BY ICP IS 3 PPM
－SAMPLE TYPE：P1－P3 ROCK P4 SOIL AU＊ANALYSIS BY ACID LEACH／AA FROM 10 GM SAYPLE．


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| SAMPLE\# | $\begin{array}{\|c} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathbf{Z n} \\ \text { ppm } \end{array}$ | $\begin{gathered} \text { Ag } \\ \text { pplit } \end{gathered}$ | $\begin{gathered} \mathrm{Ni} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{cc} \text { Mn } \\ n & p p m \\ \hline \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \% \end{gathered}$ | ppris | $\begin{array}{r} \mathrm{U} \\ \mathrm{ppm} \end{array}$ | Au ppm | Th <br> ppm | $\begin{gathered} \mathrm{Sr} \\ \mathrm{n} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \mathrm{cd} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathbf{S b} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} v \\ p p m \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \% \end{gathered}$ | $\%$ | $\begin{array}{r} \mathrm{La} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Cr} \\ \mathrm{ppm} \end{array}$ | $\mathrm{Mg}$ | $\begin{array}{r} \text { Ba } \\ \text { ppm } \end{array}$ | $\stackrel{1}{2}$ | $\begin{array}{r} B \\ \text { ppm } \end{array}$ | $\begin{gathered} \text { Al } \\ \mathbf{\%} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \% \end{gathered}$ | $\begin{aligned} & K \\ & \chi \end{aligned}$ | ${\underset{p p l}{1}}^{u_{1}}$ | $\mathbf{A u}^{\star}$ <br> ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL-90-G-35 | 2 | 30 | 2 | 38 | $\stackrel{1}{4}$ | 2 | 1 | 366 | 3.94 | 8 | 5 | ND | 2 | 6 | 2 | 2 | 2 | 19 | . 21 | 1333 | 3 | 4 | . 66 | 77 | 16 | 2 | . 94 | . 01 | . 19 | , | 21 |
| PEL-90-G-36 | 1 | 1 | 2 | 35 | $\stackrel{1}{4}$ | 1 | 2 | 522 | . 79 | 2 | 5 | ND | 3 | 28 | 2 | 2 | 2 | 5 | . 23 | <038 | 7 | 1 | . 20 | 405 | ,02 |  | . 45 | . 02 | . 16 | 2 | 2 |
| PEL-90-G-37 | 50 | 158 | 2 | 92 | $\stackrel{3}{3}$ | 20 | 42 | 1854 | 5.49 | 2 | 5 | ND | 1 | 12 | 7 | 2 | 2 | 50 | . 06 | \%111 | 7 | 47 | 1.37 | 44 | \% 05. | 2 | 2.56 | . 04 | . 10 | \% 1 | 7 |
| PEL-90-G-38 | 32 | 51 | 3 | 89 | \% | 19 | 14 | 969 | 6.51 | 0 | 5 | ND | 2 | 86 | . 7 | 2 | 2 | 73 | . 29 | -095. | 2 | 61 | 2.32 | 28 | *28 | 2 | 2.51 | . 04 | . 08 | 1 | 10 |
| PEL-90-G-39 | 4 | 14 | 2 | 21 | \&\% | 5 | 3 | 388 | 1.28 | 2 | 5 | ND | 4 | 19 | . 2 | 2 | 2 | 6 | . 18 | -041 | 6 | 5 | . 36 | 69 | 03. | 2 | . 65 | . 03 | . 09 | 2 | 4 |
| PEL-90-G-40 | 5 | 21 |  | 11 | -3. | 1 | 2 | 184 | 3.58 | 4 | 5 | ND | 5 | 25 | - 2 | 2 | 2 | 18 | . 14 | <092 | 2 | 3 | . 26 | 86 | 16 | + 4 | . 66 | . 01 | . 27 | ¢ | 26 |
| PEL-90-6-41 | 4 | 27 | 2 | 33 | 2 | 4 | 3 | 464 | 4.77 | 5. | 5 | ND |  | 17 | . 3 | 2 | 2 | 37 | . 21 | 181 | 3 | 12 | . 79 | 74 | 22 | 2 | 1.00 | . 01 | . 25 | 1 | 25 |
| PEL-90-G-42 | 1 | 1 | 4 | 46 | $\stackrel{2}{2}$ | 3 | 2 | 248 | 2.62 | \% 5 | 5 | ND | 2 | 16 | 4 | 2 | 2 | 44 | . 31 | 160 | 3 | 9 | . 91 | 74 | 16 | 2 | . 99 | . 03 | . 18 | 2 | 10 |
| PEL-90-G-43 | 1 | 30 | 2 | 11 | $\stackrel{2}{2}$ | 1 | 2 | 87 | 7.84 | $\stackrel{9}{1}$ | 5 | ND | 2 | 8 | -3 | 2 | 2 | 27 | . 03 | 014 | 3 | 5 | . 26 | 53 | 18. | 2 | . 73 | . 01 | . 19 | 2 | 12 |
| PEL-90-J-1 | 1 | 76 | 93 | 120 | 18. | 26 | 25 | 2156 | 6.81 | 251. | 5 | ND | 2 | 216 | 1. | 8 | 2 | 74 | 1.49 | 250 | 7 | 45 | 1.52 | 10 | 32 | 2 | 1.94 | . 01 | . 02 | 2 | 43 |
| PEL-90-J-2 | 4 | 8 | 2 | 36 | \% | , | 2 | 329 | 3.82 | 10 | 5 | ND | 4 | 32 | 2 | 2 | 2 | 30 | . 21 | +125 | 3 | 2 | . 80 | 77 | ,17 | 2 | . 96 | . 03 | . 17 | \% | 22 |
| PEL-90-J-3 | 4 | 29 | 8 | 37 | , 3 | 13 | 7 | 483 | 4.22 | 8 | \% 5 | ND | 4 | 17 | /2 | 2 | 2 | 52 | . 38 | 204 | 5 | 21 | 1.18 | 76 | 20 | 3 | 1.13 | . 04 | . 17 | § | 18 |
| PEL-90-J-4 | 3 | 12 | 9 | 32 | +2 | 7 | 4 | 261 | 4.28 | 7 | 5 | ND | 3 | 15 | 2 | 2 | 2 | 24 | . 27 | 221 | 5 | 8 | . 63 | 89 | 15 | 2 | . 77 | . 02 | . 18 | 1 | 32 |
| PEL-90-J-5 | 5 | 27 | 6 | 25 | 5 | 10 | 2 | 275 | 4.18 | \% 4 | 5 | ND | 3 | 17 | 3 | 2 | 2 | 46 | . 22 | 207 | 5 | 34 | . 78 | 106 | \$22 | 2 | . 86 | . 03 | . 21 | \% | 36 |
| PEL-90-J-6 | 18 | 18 | 2 | 17 | $\stackrel{3}{3}$ | 10 | 3 | 218 | 1.71 | 2 | 5 | ND | 1 | 8 | . 2 | 2 | 2 | 10 | . 18 | 1087 | 3 | 10 | . 30 | 84 | , 1 | 3 | . 44 | . 01 | . 13 |  | 21 |
| PEL-90-J-7 | 1 | 26 | 4 | 58 | +3. | 4 | 2 | 693 | 4.17 | 11 | 5 | ND | 3 | 45 | $\stackrel{3}{5}$ | ) 2 | 2 | 76 | . 46 | 262 | 6 | 14 | 1.33 | 62 | ¢8. | 2 | 1.20 | . 04 | . 12 | \% | 61 |
| PEL-90-J-8 | 1 | 87 | 5 | 63 | 1.0 | 15 | 20 | 1241 | 9.67 | 16 | 5 | ND | 5 | 74 | 1.5 | 2 | 2 | 74 | . 58 | +295 | 7 | 35 | 1.47 | 27 | 34. | 2 | 1.30 | . 01 | . 09 | , 1 | 83 |
| PEL-90-J-9 | 1 | 76 | 2 | 25 | $\stackrel{3}{3}$ | 46 | 27 | 453 | 5.56 | 27. | 5 | ND | 2 | 82 | . 6 | 2 | 2 | 49 | 1.04 | 278 | 14 | 68 | . 74 | 30 | 30. | 2 | . 85 | . 04 | . 11 | \% | 34 |
| PEL-90-J-10 | 4 | 29 | 9 | 6 | 5*2 | 10 | 20 | 49 | 17.02 | 33. | 5 | 15 | 1 | 7 | 6 | 25 | 275 | 2 | . 05 | -015 | 2 | 9 | . 01 | 5 | \%0\% | 2 | . 08 | . 01 | . 05 | * | 33400 |
| PEL-90-J-10 REF | 1 | 29 | 4 | 1 | 7, | 5 | 18 | 32 | 16.90 | 30. | 5 | 23 | 1 | 7 | , | 24 | 297 | 1 | . 05 | -013 | 2 | 5 | . 01 | 5 | 015 | 3 | . 03 | . 01 | . 03 | 1 | 46600 |
| PEL-90-J-11 | 6 | 11 | 3 | 5 | 1 | 17 | 5 | 78 | 2.65 | 寿 | 5 | ND | 1 | 3 | 2 | 3 | 9 | 2 | . 03 | -005 | . 2 | 13 | . 01 | 21 | 0\% | 2 | . 08 | . 01 | . 04 | \% | 970 |
| PEL-90-J-12 | 1 | 6 | 2 | 2 | \% \% | 7 | 16 | 64 | 3.63 | 8.8 | . 5 | ND | 1 | 1 | $\stackrel{2}{2}$ | 2 | 4 | 1 | . 01 | -003 | - 2 | 4 | . 01 | 5 | - 01 | 2 | . 04 | . 01 | . 01 | \%1 | 600 |
| PEL-90-J-13 | 5 | 588 | 10 | 247 | 3.6 | 34 | 29 | 1705 | 10.27 | 29 | 5 | ND | 2 | 31 | 1.6 | 2 | 3 | 121 | . 80 | \$305. | 5 | 86 | 4.09 | 30 | 18. | 2 | 3.72 | . 01 | . 06 | \%1 | 74 |
| PEL-90-J-14 | 1 | 30 | 20 | 78 | \% | 22 | 20 | 88 | 6.06 | 56 | 5 | ND | 1 | 18 | \% 4 | 2 | 2 | 19 | . 46 | 104 | 2 | 7 | . 35 | 14 | \% 01 | 2 | . 71 | . 03 | . 12 | \% 1 | 58 |
| PEL-90-J-15 | 6 | 19 | 2 | 5 | \% 7 | 10 | 12 | 101 | 5.63 | 2 | 5 | 3 | 5 | 7 | , 2 | 2 | 7 | 9 | . 16 | 073 | 3 | 8 | . 13 | 30 | \%1 | 2 | . 36 | . 01 | . 16 | 1 | 1260 |
| PEL-90-J-16 | 7 | 30 | 3 | 1 | $\stackrel{3}{ }$ | 4 | 26 | 18 | 7.54 | \% 8 | - 5 | ND | 6 | 6 | 2 | 2 | 8 | 5 | . 12 | -055 | 2 |  | . 02 | 19 | -01 | 3 | . 28 | . 01 | . 17 | 布 | 470 |
| PEL-90-J-17 | 6 | 14 | 2 | 18 | +1 | 7 | 26 | 448 | 4.11 | 10 | 5 | ND | 8 | 44 | , 2 | 2 | 4 | 12 | . 96 | ,082 | 11 | 3 | . 66 | 69 | -01 | 2 | 1.11 | . 01 | . 23 | 1 | 45 |
| PEL-90-J-18 | 1 | 3 | 2 | 8 | $\stackrel{2}{2}$ | 1 | 6 | 88 | 2.75 | 2 | 5 | 2 | 2 | 9 | \%2 | 2 | 18 | 8 | . 15 | \%068 | 7 | 1 | . 31 | 61 | -1\% | 3 | . 56 | . 02 | . 17 | \% 1 | 3360 |
| PEL-90-J-19 | 3 | 7 | 2 | 13 | \&1 | 5 | 6 | 368 | 3.62 | 2 | 5 | ND | 10 | 22 | $\geqslant 2$ | 2 | 2 | 13 | . 48 | 092 | 4 | 3 | . 46 | 60 | \% 01 | 3 | . 70 | . 03 | . 16 | 1 | 370 |
| PEL-90-J-20 | 2 | 1 | 2 | 7 | -2 | 1 | 2 | 72 | 3.63 | 2 | 5 | ND | 9 | 10 | \%2 | 2 | 8 | 8 | . 09 | 064 | 3 | 1 | . 28 | 60 | \% 0 | 2 | . 53 | . 02 | . 15 | 1 | 980 |
| PEL-90-J-21 | 13 | 8 | 3 | 1 | $\geqslant$ | 5 | 8 | 94 | 6.08 | 2 | 5 | ND | 7 | 9 | 2 | 2 | 6 | 5 | . 17 | -073 | 4 | 4 | . 22 | 28 | -04 | 5 | . 53 | . 02 | . 19 | \% | 740 |
| PEL-90-J-22 | 1 | 3 | 2 | 1 | $\stackrel{1}{1}$ | 2 | 4 | 96 | 3.31 | \% 4 | 5 | ND | 2 | 8 | $\stackrel{2}{2}$ | 2 | 2 | 2 | . 17 | -024 | 2 | 2 | . 05 | 28 | 0\% | 2 | . 17 | . 01 | . 07 | 1 | 1010 |
| PEL-90-J-23 | 13 | 7 | 2 | 3 | $\cdots$ | 7 | 2 | 875 | 2.86 | 2 | 5 | ND | 5 | 33 | $\stackrel{2}{2}$ | 2 | 2 | 3 | . 78 | 047 | 2 | 5 | . 24 | 53 | 01, | 2 | . 30 | . 01 | . 15 | \% | 140 |
| PEL-90-J-24 | 16 | 4 | 2 | 1 | $\stackrel{2}{2}$ | 4 | 32 | 53 | 6.16 | 3 | 5 | ND | 2 | 12 | \% 2 | 2 | 2 | 6 | . 07 | \% 019 | 2 | 1 | . 04 | 22 | ,03. | 2 | . 23 | . 01 | . 11 | 1 | 18 |
| PEL-90-J-25 | 5 | 5 | 2 | 1 | \% | 20 | 8 | 52 | 3.66 | 7 | 5 | ND | 1 | 1 | \%2 | 2 | 2 | 1 | . 01 | 00\% | 2 | 11 | . 01 | 22 | , 01 | 2 | . 04 | . 01 | . 01 | < | 610 |
| PEL-90-J-26 | 1 | 8 | 2 | 30 | $\stackrel{1}{ }$ | 12 | 29 | 214 | 3.18 | 2 | 5 | ND | 3 | 45 | 3 | 2 | 2 | 35 | . 56 | 1488 | 3 | 10 | 1.32 | 34 | 10 | 3 | 1.22 | . 05 | . 15 | 1 | 5 |
| STANDARD C/AU-R | 19 | 57 | 39 | 132 | 7.2 | 72 | 31 | 1048 | 3.97 | 40 | 20 | 7 | 40 | 52 | 19.2 | 16 | 19 | 60 | . 52 | . 094 | 40 | 60 | . 89 | 183 | .09. | 36 | 1.89 | . 06 | . 13 | 13 | 530 |

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| SAMPLE\# | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathbf{2 n} \\ \text { ppm } \end{array}$ | $\stackrel{\text { Ag }}{\text { ppm }}$ | $\begin{array}{r} \mathrm{Ni} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppm } \end{array}$ | $\begin{aligned} & \mathbf{e} \\ & \boldsymbol{z} \end{aligned}$ | $\begin{gathered} \text { As } \\ \text { Ppmit } \end{gathered}$ | $\begin{array}{r} \mathrm{U} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathbf{A u} \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Sr} \\ \mathrm{ppm} \end{array}$ | $\stackrel{\mathrm{cd}}{\mathrm{ppm}}$ | $\begin{array}{r} \text { Sb } \\ \text { ppon } \end{array}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} v \\ \text { pom } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{Z} \end{gathered}$ | \% | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Cr} \\ \text { ppm } \end{gathered}$ | $\begin{gathered} \mathrm{Mg} \\ \mathbf{X} \end{gathered}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | $\stackrel{1}{2}$ | $\begin{array}{r} \text { B } \\ \text { ppm } \end{array}$ | $\begin{gathered} \text { Al } \\ \mathbf{Z} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \% \end{gathered}$ | $\begin{aligned} & K \\ & \boldsymbol{Z} \end{aligned}$ | $\underset{\mathrm{PQ}}{\mathrm{~m}}$ | $\begin{aligned} & \mathrm{Au}^{*} \\ & \mathrm{ppb} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL-90-J-27 | 3 | 4 | 7 | 42 | -3 | 9 | 8 | 301 | 2.90 | 4 | 5 | ND | 7 | 17 | 2. | 2 | 2 | 31 | . 18 | 088 | 3 | 7 | . 67 | 40 | \% 06 | 2 | . 69 | . 08 | . 11 | 2 | 14 |
| PEL-90-J-28 | 1 | 83 | 6 | 277 | $\stackrel{9}{ }$ | 14 | 14 | 1086 | 18.72 | 10 | 6 | ND | 2 | 76 | \$19. | 2 | 2 | 64 | . 48 | 104 | 2 | 15 | 3.02 | 9 | \%13 | 2 | 3.28 | . 02 | . 03 | 3 | 1990 |
| PEL-90-J-28 REF | 1 | 193 | 7 | 293 | 1.0 | 4 | 20 | 1296 | 26.59 | 27 | 13 | ND | 2 | 17 | 1.6 | 2 | 2 | 60 | . 14 | -056 | 2 | 4 | 3.43 | 7 | \% 10 | 2 | 3.76 | . 01 | . 05 | , 1 | 2240 |
| PEL-90-J-29 | 4 | 12 | 44 | 185 | \% 7 | 11 | 19 | 970 | 7.76 | 2 | 5 | ND | 2 | 55 | 1, 4 | 2 | 3 | 79 | . 42 | 185 | 2 | 17 | 2.02 | 60 | \% 20 | 2 | 1.97 | . 15 | . 16 | 1 , | 41 |
| PEL-90-J-30 | 1 | 6 | 32 | 89 | $\stackrel{7}{2}$ | 4 | 5 | 347 | 5.38 | 2 | 5 | ND | 1 | 63 | $\stackrel{2}{2}$ | 2 | 2 | 41 | . 25 | 1085 | 4 | 7 | . 59 | 71 | ,17. | 2 | . 97 | . 07 | . 20 | , | 36 |
| PEL-90-J-31 | 2 | 5 | 6 | 168 | . 5 | 7 | 18 | 439 | 3.29 | 3. | 5 | ND | 1 | 81 | \% 8 | 2 | 2 | 24 | . 45 | 075 | 4 | 22 | . 54 | 25 | \%09 | 2 | . 90 | . 16 | . 08 | \% | 16 |
| PEL-90-J-32 | 2 | 9 | 55 | 199 | $\stackrel{ }{ } 9$ | 6 | 11 | 1073 | 10.73 | 23 | 5 | ND | 2 | 28 | \% $\%$ | 2 | 2 | 141 | . 16 | ,142 | 2 | 10 | 3.11 | 40 | \% 28 | 2 | 2.92 | . 10 | . 12 | 1 | 56 |
| PEL-90-J-33 | 4 | 18 | 23 | 108 | -4 | 11 | 14 | 477 | 5.85 | 2 | 5 | ND | 2 | 97 | , 5 | 2 | 2 | 84 | . 40 | .147 | 4 | 13 | 1.62 | 65 | \% 24 | 2 | 1.71 | . 17 | . 15 | 1 | 11 |
| PEL-90-J-34 | 2 | 20 | 17 | 63 | , 5 | 14 | 39 | 461 | 8.91 | 2 | 5 | ND | 2 | 49 | 4.0 | 2 | 2 | 82 | . 33 | 175 | 2 | 9 | 1.63 | 47 | \%22 | 2 | 1.64 | . 15 | . 13 | \% 1 | 17 |
| PEL-90-J-35 | 25 | , | 3 | 2 | \% 1 | 2 | 2 | 41 | 2.01 | 2 | 5 | ND | 8 | 6 | \%2 | 2 | 2 | 6 | . 07 | \$049 | 2 | 12 | . 05 | 110 | \$05 | 2 | . 52 | . 02 | . 33 | §, 1 | 4 |
| PEL-90-J-36 | 2 | 4 | 4 | 13 | 2 | 4 | 4 | 129 | 2.51 | 2 | 5 | ND | 3 | 38 | , 2 | 2 | 2 | 34 | . 43 | -200 | 3 | 5 | . 44 | 200 | 16: | 2 | . 82 | . 10 | . 24 | 1 | 8 |
| PEL-90-J-37 | 4 | 22 | 11 | 11 | 3 | 1 | 1 | 76 | 5.57 | 2 | 5 | ND | 3 | 14 | 2 | 2 | 2 | 42 | . 09 | . 049 | 2 | 5 | . 25 | 190 | 29 | 2 | . 82 | . 05 | . 35 | 2 | 24 |
| PEL-90-J-38 | 19 | 16 | 2 | 2 | 2 | 1 | 1 | 10 | 5.65 | 2 | 5 | ND | 2 | 2 | 2 | 2 | 2 | 13 | . 01 | . 0001 | 2 | 1 | . 04 | 230 | \% 17 | 2 | . 73 | . 01 | . 32 | 》1 | 15 |
| BR-90-J-1 | 5 | 3 | 3 | 4 | 2 | 10 | 3 | 288 | . 99 | 7 | 5 | ND | 1 | 24 | $\stackrel{2}{2}$ | 2 | 2 | 6 | . 91 | . 020 | 2 | 45 | . 03 | 31 | \% 0 | 2 | . 14 | . 01 | . 08 | , 1 , | 4 |
| STANDARD C/AU-R | 18 | 59 | 38 | 132 | 172 | 72 | 31 | 1049 | 3.97 | 42 | 20 | 7 | 39 | 55 | 19.5. | 15 | 18 | 58 | . 52 | ,097 | 39 | 59 | . 90 | 182 | . 09 | 35 | 1.90 | . 06 | . 13 | 13. | 520 |

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| SANPLE\＃ | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathbf{p P R} \mathbf{R}^{2} \end{array}$ | $\stackrel{\mathrm{A}_{\mathrm{p}},}{ }$ | $\underset{\substack{\mathrm{pi} \\ \hline}}{ }$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} M n \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \mathbf{\%} \end{gathered}$ | $\stackrel{\text { ppon }}{ }$ | $\begin{array}{r} \mathrm{U} \\ \text { ppm } \end{array}$ | Au ppm | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Sr} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{cd} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \text { Sb } \\ \text { ppin } \end{array}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathbf{p p m} \end{array}$ | $\begin{array}{r} v \\ p p m \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \% \end{gathered}$ | $\forall$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{pprin} \end{gathered}$ | $\begin{array}{r} \mathrm{Mg} \\ \mathbf{X} \end{array}$ | $\begin{array}{r} \text { Ba } \\ \text { ppm } \end{array}$ | $\%$ | $\begin{array}{r} \mathbf{B} \\ \mathbf{p p m} \end{array}$ | $\begin{gathered} \text { AI } \\ \mathbf{X} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ | $\begin{aligned} & k \\ & \mathbf{x} \end{aligned}$ |  | A $u^{*}$ <br> ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL－90－DS－1 | 12 | 91 | 18 | 71 | \％ | 2 | 7 | 825 | 7.75 | 11 | 9 | ND | 11 | 9 | \％ | 2 | 4 | 25 | ． 06 | \％048 | 30 | 8 | ． 15 | 30 | ¢18． | 2 | 3.71 | ． 06 | ． 07 | $\cdots$ | 9 |
| PEL－90－DS－2 | 5 | 31 | 39 | 104 | 8 | 12 | 3 | 850 | 3.69 | 16 | 5 | ND | 3 | 65 | 2 | 2 | 2 | 51 | ． 37 | 105． | 18 | 32 | 1.24 | 380 | ． 24 | 2 | 1.88 | ． 01 | ． 14 | ！ | 12 |
| PEL－90－DS－3 | 15 | 103 | 20 | 112 | 5． | 9 | 7 | 724 | 5.47 | 7 | 5 | ND | 6 | 50 | －3 | 2 | 2 | 50 | ． 25 | \％144． | 15 | 17 | ． 98 | 90 | 22 | 2 | 2.09 | ． 03 | ． 08 | 疗 | 40 |
| PEL－90－DS－4 | 7 | 43 | 41 | 91 | － 9 | 14 | 5 | 614 | 4.74 | 13 | 5 | ND | 4 | 66 | 3 | 2 | 3 | 52 | ． 24 | 168 | 13 | 35 | 1.02 | 304 | \％ 30 | 2 | 1.97 | ． 02 | ． 11 | \％ | 89 |
| PEL－90－DS－5 | 7 | 84 | 44 | 111 | $\geqslant .0$ | 12 | 16 | 776 | 5.16 | \％1\％ | 5 | ND | 4 | 60 | $\stackrel{5}{5}$ | 2 | 3 | 81 | ． 20 | \％086 | 11 | 45 | 1.12 | 104 | 4 47. | 3 | 2.86 | ． 02 | ． 06 | \％ | 190 |
| PEL－90－DS－6 | 9 | 14 | 18 | 96 | ，\％ | 2 | 5 | 1154 | 9.25 | \％ 15 | 7 | ND | 11 | 2 | ． 8 | 2 | 4 | 32 | ． 03 | \％039 | 35 | 13 | ． 08 | 9 | \％20 | 2 | 3.43 | ． 06 | ． 08 | 水 | 10 |
| PEL－90－DS－7 | 7 | 748 | 8 | 75 | 1．5． | 10 | 57 | 1059 | 1.02 | 30 | 5 | ND | 1 | 28 | \％ 8 | 2 | 2 | 7 | ． 31 | ， 127 | 39 | 3 | ． 04 | 26 | ， 02 | 2 | 10.10 | ． 01 | ． 01 | ィ | 29 |
| PEL－90－DS－8 | 7 | 28 | 51 | 70 | ， 7 | 7 | 3 | 360 | 4.58 | 6 | 5 | ND | 3 | 31 | 4 | 2 | 2 | 51 | ． 13 | ．087 | 19 | 19 | ． 51 | 109 | ，31， | 2 | 2.34 | ． 02 | ． 07 | 1 | 38 |
| PEL－90－DS－9 | 7 | 27 | 212 | 70 | 10 | 8 | 2 | 411 | 3.49 | 17 | 5 | ND |  | 49 | 2 | 2 | 2 | 46 | ． 20 | 101 | 10 | 22 | ． 87 | 170 | 24 | 2 | 1.68 | ． 01 | ． 06 | ， | 12 |
| PEL－90－DS－10 | 7 | 31 | 27 | 84 | ＊ 3 \％ | 16 | 7 | 888 | 5.68 | 14 | 5 | ND | 5 | 33 | \％ 2 | 2 | 2 | 43 | ． 15 | ＊ 122 | 20 | 23 | ． 80 | 137 | \％ 23. | 2 | 2.88 | ． 02 | ． 06 | ＊ | 32 |
| PEL－90－DS－11 | 14 | 112 | 150 | 292 | ， 7 \％ | 20 | 32 | 992 | 28.09 | 157 | 5 | ND | 2 | 42 | 1.3 | 2 | 2 | 15 | ． 04 | \％ 514 | 28 | 6 | ． 19 | 154 | \％8． | 2 | 3.26 | ． 01 | ． 04 | 9 | 99 |
| PEL－90－DS－12 | 7 | 35 | 44 | 80 | \％ | 6 | 4 | 361 | 6.16 | 13. | 5 | ND | 5 | 16 | 2 | 2 | 4 | 43 | ． 09 | 113． | 17 | 13 | ． 57 | 58 | \％ 36 | 2 | 2.36 | ． 03 | ． 05 | 行 | 85 |
| PEL－90－DS－13 | 22 | 44 | 46 | 67 | ． | 9 | 8 | 369 | 5.20 | 23． | 5 | ND | 4 | 54 | \％ 8 | 2 | 2 | 54 | ． 39 | ，081 | 11 | 15 | ． 81 | 67 | 445 | 2 | 1.83 | ． 13 | ． 11 | 迷 | 350 |
| PEL－90－DS－14 | 43 | 137 | 17 | 91 | \％ 6 | 16 | 20 | 797 | 14.53 | 15 | 9 | ND | 8 | 43 | 2， | 2 | 5 | 118 | ． 15 | $\stackrel{292}{ }$ | 5 | 44 | 1.40 | 92 | 40． | 2 | 2.50 | ． 04 | ． 06 | \} | 56 |
| PEL－90－DS－15 | 169 | 215 | 10 | 42 | \％ 4. | 7 | 28 | 802 | 15.59 | 5 | 7 | ND | 14 | 17 | 1，4 | 2 | 4 | 35 | ． 07 | 348 | 3 | 14 | ． 44 | 51 | ． 20 | 2 | 1.17 | ． 01 | ． 07 | ， | 69 |
| PEL－90－DS－16 | 10 | 35 | 19 | 59 | ， 3 | 6 | 6 | 452 | 4.03 | 9． | 5 | ND | 3 | 75 | 2 | 2 | 2 | 39 | ． 35 | \％168 | 7 | 10 | ． 86 | 228 | 24． | 2 | 1.27 | ． 05 | ． 10 | \％ | 21 |
| STANDARD C／AU－S | 18 | 57 | 40 | 131 | \％\％ | 72 | 31 | 1048 | 3.97 | 4 | 20 | 7 | 39 | 53 | 19．3 | 15 | 19 | 57 | ． 51 | \％093 | 39 | 58 | ． 90 | 181 | ． 09. | 35 | 1.90 | ． 06 | ． 14 | 11 | 48 |

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| SAMPLE\# | $\begin{array}{r} \text { Mo } \\ \text { ppp } \end{array}$ | $\begin{gathered} \mathrm{Cu} \\ \mathrm{pppm} \end{gathered}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{pp} \mathrm{~m} \end{array}$ | $\begin{array}{r} 2 n \\ p p m \end{array}$ | $\begin{gathered} \text { Ag } \\ \text { ppon } \end{gathered}$ | $\begin{array}{r} \text { Ni } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{rr} \mathrm{Mn} \\ \mathrm{n} & \mathrm{ppm} \\ \hline \end{array}$ | $\begin{array}{r} \mathrm{Fe} \\ \mathbf{\%} \end{array}$ | $\begin{gathered} \text { As } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} U \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Au } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | Sr | $\begin{gathered} \mathrm{cd} \\ \text { pen } \end{gathered}$ | $\begin{aligned} & \text { Sb } \\ & \text { ppm } \end{aligned}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} v \\ \mathrm{ppom} \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \boldsymbol{\%} \end{gathered}$ |  | La ppin | $\begin{array}{r} \mathrm{Cr} \\ \mathrm{Pp} \text { PII } \end{array}$ | $\begin{array}{rl} \mathrm{n} & \mathrm{Mg} \\ \boldsymbol{X} \end{array}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | T1, |  | $\begin{aligned} & \text { A! } \\ & \text { \% } \end{aligned}$ | $\begin{gathered} \mathrm{Na} \\ \boldsymbol{x} \end{gathered}$ |  |  | $A u^{*}$ ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL-90-G-44 | 3 | 18 | 38 | 482 | 2 | \% 7 | 4 | 414 | 3.92 | 20 | 2 | ND | 1 | 8 | 1.4 | 2 | 2 | 37 | . 16 | . 098 | + 2 | 16 | 1.32 | 98 | 17 |  | 1.15 | . 02 | . 15 | 3 | 51 |
| PEL-90-G-45 | 2 | 23 | 4 | 50 | 1 | - 7 | 5 | 359 | 2.52 | 12 | 2. 5 | ND | 1 | 20 | . 5 | 3 | 5 | 20 | . 33 | . 077 | 2 | 7 | 1.07 | 99 | 12 | 5 | 1.28 | . 03 | . 19 | 3 | 25 |
| PEL-90-G-46 | 16 | 62 | 5 | 20 | 9 | 6 | 10 | 37 | 13.33 | 23 | ) 5 | ND | 4 | 9 | . 4 | 2 | 7 | 35 | . 03 | . 055 | 3 | 25 | . 06 | 74 | 10 | 8 | . 40 | . 01 | . 13 | 2 | 220 |
| PEL-90-G-47 | 9 | 11 | 584 | 6 | 2 | 2 | 17 | 8 | 40.74 | 334 | 4 5 | ND | 6 | 6 | $\stackrel{\circ}{\circ}$ | 2 | 2 | 167 | . 01 | 4.484 | 2 | 44 | . 02 | 29 | -02 | 3 | . 68 | . 01 | . 02 | 3 | 15 |
| PEL-90-G-48 | 5 | 728 | 88 | 1336 | 1.1 | 460 | 52 | 2410 | 8.55 | 73 | 7 | ND | 2 | 57 | 72 | 2 | 4 | 79 | . 77 | 284 | 6 | 643 | 3.50 | 23 | 13. | 5 | 4.10 | . 01 | . 06 | 2 | 59 |
| PEL-90-6-49 | 16 | 10 | 2 | 246 | 3. | 22 | 45 | 4879 | 3.54 | 5 | 5 | NO | 9 | 29 | 1.4 | 2 | 2 | 19 | . 59 | 097 | \% 13 | 3 | 3.85 | 115 | - 04 |  | 1.76 | . 04 | . 12 | 1 | 12 |
| PEL-90-G-50 | 13 | 13 | 2 | 32 | $\stackrel{1}{1}$ | 5 | 18 | 625 | 2.11 | 4 | 5 | ND | 7 | 73 | $\stackrel{7}{ } 8$ | 2 | 2 | 45 | . 55 | 104 | 8 | 10 | 1.16 | 177 | 08 | 3 | 1.43 | . 05 | . 08 | 2 | 4 |
| PEL-90-G-51 | 15 | 11 | 16 | 25 | 1 | 4 | 6 | 404 | 2.71 | 9 | 2 5 | ND | 6 | 63 | -4 | 2 | 2 | 46 | . 49 | 164 | 8 | 5 | 1.00 | 140 | . 06 | 2 | 1.19 | . 05 | . 07 | 1. | 4 |
| PEL-90-G-52 | 3 | 7 | 2 | 21 | 2 | 13 | 1 | 504 | . 79 | 2 | 2 5 | ND | 1 | 20 | . 4 | 2 | 3 | 8 | . 75 | . 024 | 8 | 14 | . 27 | 23 | -01. | 3 | . 40 | . 01 | . 04 | 1 | 4 |
| PEL-90-G-53 | 2 | 8 | 3 | 122 | 11 | 7 | 9 | 4170 | 4.72 | 2 | 2 5 | ND | 6 | 3306 | $\stackrel{9}{ }$ | 2 | 2 | 61 | 12.64 | . 019 | 6 | 3 | 31.25 | 182 | -01. | 5 | 2.05 | . 01 | . 05 | 1 | 1 |
| PEL-90-J-65 | 8 | 32 | 8 | 49 | 3 | 19 | 13 | 417 | 2.44 | 2 | 2. 5 | ND | 1 | 17 | $\stackrel{2}{ }$ | 2 | 2 | 15 | . 20 | . 095 | 3 | 46 | . 50 | 126 | 02 | 3 | . 76 | . 01 | . 13 | 2 | 18 |
| PEL-90-J-66 | 15 | 478 | 24 | 351 | $\stackrel{3}{3}$ | 5 | 13 | 208 | 22.28 | 18 | 2. 5 | ND | 2 | 87 | 2 | 2 | 29 | 147 | . 33 | .282 | 5 | 10 | . 10 | 25 | 114 | 5 | . 85 | . 01 | . 01 | 1 | 540 |
| PEL-90-J-67 | 39 | 348 | 23 | 104 | 1.0 | 23 | 20 | 344 | 18.02 | 20 | . 5 | ND | 1 | 172 | 1.1. | 2 | 2 | 80 | . 44 | .201 | 8 | 31 | . 15 | 92 | 13 | 2 | 1.01 | . 01 | . 08 | 2 | 300 |
| PEL-90-J-68 | 6 | 141 | 3 | 216 | 2 | 13 | 7 | 1610 | 7.63 | 11 | 5 | ND | 1 | 78 | 17 | 2 | 2 | 66 | . 22 | 178 | . 13 | 8 | 1.75 | 76 | 13 | 4 | 1.96 | . 01 | . 03 | 1 | 13 |
| PEL-90-J-69 | 7 | 163 | 23 | 251 | . 8 | 16 | 9 | 927 | 8.22 | 6 | 5 | ND | 3 | 36 | $\stackrel{4}{4}$ | 2 | 2 | 63 | . 03 | . 192 | 17 | 44 | 1.65 | 161 | 06 | 4 | 2.43 | . 03 | . 15 | 1 | 32 |
| PEL-90-J-70 | 4 | 84 | 23 | 156 | 5 | 28 | 31 | 873 | 12.37 | 5 | 5 | ND | , | 24 | 1.4 | 2 | 2 | 51 | . 04 | . 069 | 4 | 45 | 1.18 | 59 | 25 | 2 | 1.54 | . 01 | . 11 | 1 | 69 |
| PEL-90-J-71 | 7 | 277 | 93 | 177 | 5.4 |  | 10 | 772 | 6.07 | 10 | ) 5 | ND | 1 | 171 | $\stackrel{9}{9}$ |  | 2 | 60 | . 43 | . 098 | 10 | 31 | 1.38 | 143 | +28 | 2 | 1.79 | . 03 | . 10 | 1 | 28 |
| PEL-90-J-72 | 3 | 9 | 16 | 131 | -8 | 8 | 7 | 769 | 5.82 | 31 | 5 | ND | 1 | 200 | ¢ 9 | 2 | 2 | 85 | . 85 | . 104 | 6 | 27 | 1.18 | 25 | . 35 | 6 | 1.49 | . 01 | . 10 | 2 | 89 |
| PEL-90-J-73 | 3 | 11 | 21 | 58 | 1 | 6 | 16 | 814 | 6.45 | 15 | 5 | ND | 1 | 204 | 1.0 | 2 |  | 72 | 1.02 | . 085 | 5 | 19 | 1.49 | 21 | 33. | 3 | 1.66 | . 02 | . 03 | 1 | 31 |
| PEL-90-J-74 | 2 | 18 | 4 | 60 | 7 | 7 | 28 | 1260 | 9.79 | 19. | 5 | ND | 2 | 39 | 7 | 2 | 6 | 69 | . 50 | 178 | 4 | 12 | 2.37 | 61 | 17. | 5 | 2.20 | . 05 | . 29 | 3 | 29 |
| PEL-90-J-75 | 3 | 12 | 7 | 28 | 2 | 4 | 22 | 353 | 4.16 | 22 | 5 | ND | , | 63 | $\stackrel{2}{2}$ | 2 | 2 | 37 | . 34 | . 056 | 4 | 6 | . 63 | 52 | 15 | 4 | . 78 | . 06 | . 13 | 1 | 27 |
| PEL-90-J-76 | 5 | 11 | 16 | 9 | 3 | 17 | 16 | 113 | 8.23 | 93. | 5 | ND | 1 | 106 | 1.1 | 2 | 2 | 114 | . 33 | . 095 | 4 | 42 | . 15 | 32 | 43 | 2 | . 51 | . 04 | . 09 | 1 | 110 |
| PEL-90-J-77 | 1 | 42 | 2 | 26 | 1.7 | 6 | 3 | 62 | 1.12 | 6 | 5 | ND | 1 | 11 | 2 | 2 | 2 | 8 | . 22 | . 099 | 4 | 5 | . 08 | 55 | . 05. | 2 | . 68 | . 01 | . 19 | 1 | 61 |
| PEL-90-J-78 | 1 | 23 | 12 | 38 | $\cdots$ | 40 | 9 | 439 | 5.61 | 14 | 5 | ND | 1 | 26 | $\stackrel{5}{5}$ | 2 | 2 | 85 | . 25 | 122 | 5 | 67 | 1.54 | 74 | 24. | 6 | 1.36 | . 05 | . 06 | 2 | 31 |
| PEL-90-J-79 | 4 | 320 | 13 | 192 | 2.2 | 59 | 71 | 3542 | 5.42 | 26 | 5 | ND | 1 | 11 | $\stackrel{0}{ }$ | 2 | 2 | 17 | . 17 | 200 | 6 | 6 | . 46 | 132 | 01. | 2 | 2.39 | . 01 | . 12 | 1 | 82 |
| PEL-90-J-80 |  | 251 | 16 | 138 | 2.8 | 43 | 116 | 5385 | 4.93 | 29 | 5 | ND |  | 7 | -6. | 2 |  | 15 | . 12 | 137 | 5 | 6 | . 41 | 91 | 05 | 3 | 1.39 | . 01 | . 15 |  | 125 |
| PEL-90-J-81 | 2 | 39 | 2 | 15 | $\stackrel{1}{1}$ | 8 | 11 | 708 | . 44 | 3 | 5 | ND | 14 | 7 | -2 | 2 | 2 | 2 | . 11 | 033 | 5 | 11 | . 05 | 114 | 01 | 2 | . 43 | . 01 | . 17 | 1 | 9 |
| PEL-90-J-82 | 5 | 39 | 10 | 77 | 1.2 | 12 | 8 | 260 | 3.57 | 26. | 5 | ND | 1 | 15 | $\stackrel{6}{6}$ | 2 | 2 | 16 | . 35 | 183 | 5 | 5 | . 66 | 85 | 14 | 2 | . 98 | . 01 | . 19 | 1 | 92 |
| PEL-90-J-83 | 4 | 25 | 37 | 48 | 2.8 | 14 | 8 | 206 | 4.70 | 85 | 5 | ND | 1 | 98 | -6 | 2 | 2 | 53 | . 60 | 101 | 4 | 25 | . 32 | 54 | 29 | 6 | . 70 | . 04 | . 07 | 1 | 200 |
| PEL-90-J-84 | 4 | 21 | 21 | 8 | 1.8 | 14 | 13 | 112 | 7.31 | 20 | 5 | ND | 1 | 49 | $\stackrel{2}{2}$ | 2 | 2 | 20 | . 23 | . 044 | 2 | 11 | . 03 | 29 | 10 | 2 | . 29 | . 02 | . 06 | 1 | 133 |
| $\begin{aligned} & \text { PEL-90-J-85 } \\ & \text { STANDARD C/AU-R } \end{aligned}$ | 20 | $\begin{aligned} & 15 \\ & 62 \end{aligned}$ | 14 42 | 86 130 | 7\% | 10 73 | 3 32 | $\begin{array}{r} 761 \\ 1053 \end{array}$ | 4.21 3.97 | 35 | 5 18 | ND 7 | 1 39 | 21 | 19.2 | 2 | 20 | 53 57 | .36 .52 | 163 .095 | 6 40 | $\begin{aligned} & 15 \\ & 59 \end{aligned}$ | 2.19 .90 | 76 183 | -29. | 3 | $\begin{aligned} & 2.01 \\ & 1.89 \end{aligned}$ | . 04 | .16 .13 | 11 | 73 510 |

> ICP - . 500 GRAM SAMPLE IS DIGESTED WITH $3 M L 3-1-2$ HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
> THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: P1 ROCK P2 SOIL AU* ANALYSIS BY ACID LEACH/AA FROM 10 GM SAMPLE.


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| SAMPLE\# | $\begin{aligned} & \text { Mo } \\ & \text { ppm } \end{aligned}$ | $\underset{\text { ppm }}{\mathbf{C u}}$ | Pb ppm | $\begin{array}{r} \mathbf{Z n} \\ \mathrm{ppm} \end{array}$ | $\begin{aligned} & \text { ng } \\ & \text { ppm } \end{aligned}$ | $\begin{array}{r} \mathrm{Ni} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Mn} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Fe} \\ \mathbf{X} \\ \hline \end{array}$ | $\begin{gathered} \text { As } \\ \text { ppin } \end{gathered}$ | $\begin{array}{r} \mathbf{U} \\ \mathbf{p p m} \end{array}$ | $\begin{array}{r} \text { Au } \\ \text { ppmin } \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Sr} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{cd} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \text { Sb } \\ \mathbf{p p m} \end{array}$ | $\begin{array}{r} \mathbf{B i} \\ \mathbf{p p m} \end{array}$ | $\begin{array}{r} V \\ p p i n \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{x} \end{gathered}$ | $\boldsymbol{*}$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cr} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Mg} \\ \mathrm{~K} \end{gathered}$ | $\begin{array}{r} \text { Ba } \\ \text { ppm } \end{array}$ | $7$ | $\begin{array}{r} B \\ p p n_{n} \end{array}$ | $\begin{gathered} \text { Al } \\ \boldsymbol{x} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{x} \end{gathered}$ | $\begin{aligned} & \mathbf{K} \\ & \mathbf{x} \end{aligned}$ | ppin | $A u^{*}$ ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL-90-DS-18 | 7 | 18 | 53 | 80 | 6 | 9 | 6 | 433 | 4.44 | 15 | 5 | ND | 5 | 53 | . 2 | 2 | 3 | 56 | . 43 | -064 | 17 | 18 | . 82 | 85 | $\stackrel{43}{ }$ | 2 | 2.54 | . 13 | . 11 | 1. | 46 |
| PEL-90-DS-19 | 31 | 99 | 229 | 138 | $\stackrel{.}{ }$ | 15 | 45 | 1182 | 6.77 | 29 | 6 | ND | 5 | 52 | 3 | 3 | 3 | 52 | . 44 | +118 | 15 | 18 | . 79 | 175 | . 33 | 2 | 4.37 | . 15 | . 13 | 1 | 66 |
| PEL-90-DS-20 | 10 | 48 | 34 | 84 | ¢ 4 | 6 | 12 | 599 | 6.65 | 12. | 5 | ND | 8 | 48 | 2 | 2 | 2 | 43 | . 21 | -086 | 14 | 16 | . 60 | 34 | . 26 | 3 | 2.09 | . 01 | . 05 | 2 | 19 |
| SER-90-B-1 | 6 | 208 | 36 | 189 | 7. | 24 | 14 | 1284 | 10.72 | 17. | 5 | ND | 5 | 75 | 1.4 | 2 | 3 | 88 | . 22 | . 363 | 16 | 33 | 1.63 | 170 | $\stackrel{30}{ }$ | 2 | 2.83 | . 07 | . 10 | 1 | 104 |
| SER-90-B-2 | 4 | 231 | 39 | 218 | 6 | 24 | 23 | 1916 | 10.37 | 13. | 5 | ND | 4 | 72 | 1.4 | 2 | 2 | 109 | . 35 | +330 | 13 | 27 | 1.77 | 139 | $\stackrel{36}{ }$ | 2 | 2.92 | . 11 | . 13 | 1. | 65 |
| SER-90-B-3 | 5 | 160 | 23 | 190 | ${ }^{6}$ | 22 | 18 | 1566 | 9.67 | 18 | 5 | ND | 7 | 54 | 1.2 | 2 | 2 | 87 | . 21 | +307 | 21 | 23 | 1.41 | 145 | +39 | 2 | 3.13 | . 08 | . 11 | 1. | 67 |
| SER-90-B-4 | 4 | 222 | 23 | 179 | . 6 | 31 | 26 | 1719 | 9.19 | 19 | 5 | ND | 4 | 68 | 1.4 | 2 | 2 | 114 | . 42 | , 316 | 14 | 28 | 1.91 | 170 | -39 | 2 | 3.22 | . 14 | . 13 | 1 | 52 |
| SER-90-B-6 | 5 | 190 | 26 | 250 | . 7 | 44 | 38 | 3573 | 8.79 | 10 | 5 | ND | 5 | 64 | 1.7 |  | 2 | 72 | . 50 | -205 | 19 | 23 | 1.52 | 286 | . 37 | 2 | 3.14 | . 18 | . 12 | 1 | 65 |
| SER-90-B-7 | 5 | 118 | 26 | 172 | 1.0 | 25 | 21 | 1701 | 8.87 | 26. | 5 | ND | 5 | 66 | $\stackrel{\square}{9}$ | 2 | 3 | 77 | . 28 | $\stackrel{263}{ }$ | 16 | 33 | 1.44 | 188 | 34 | 2 | 3.25 | . 09 | . 10 | 1. | 280 |
| SER-90-B-8 | 4 | 78 | 75 | 160 | 2.0 | 21 | 9 | 976 | 8.58 | 33 | 5 | ND | 4 | 67 | $\stackrel{\bigcirc}{\circ}$ | 3 | 2 | 99 | . 20 | 217 | 23 | 48 | 1.48 | 278 | 41 | 2 | 2.86 | . 07 | . 10 | $\stackrel{1}{*}$ | 134 |
| SER-90-B-9 | 5 | 117 | 50 | 153 | 1.3 | 27 | 18 | 1192 | 7.73 | 26 | 5 | ND | 4 | 62 | . 6 | 2 | 2 | 77 | . 33 | ,228 | 16 | 34 | 1.29 | 197 | $\stackrel{35}{ }$ | 3 | 3.07 | . 11 | . 10 | $\stackrel{1}{ }$ | 90 |
| SER-90-B-10 | 6 | 174 | 26 | 220 | $\stackrel{6}{6}$ | 35 | 29 | 3015 | 8.94 | 13 | 5 | ND | 7 | 35 | 1.4 | 2 | 2 | 57 | . 11 | .227 | 22 | 24 | 1.09 | 189 | ,24 | 2 | 3.25 | . 04 | . 08 | 1 | 57 |
| SER-90-B-12 | 4 | 231 | 25 | 178 | ${ }^{6}$ | 31 | 27 | 1840 | 9.12 | 17. | 5 | ND | 4 | 62 | 1.3 |  | 2 | 109 | . 33 | 324 | 14 | 27 | 1.80 | 151 | . 34 | 2 | 3.11 | . 11 | . 11 | 1 | 52 |
| SER-90-8-13 | 4 | 200 | 32 | 204 | 8 | 24 | 21 | 1738 | 9.66 | 15 | 5 | ND | 4 | 67 | 1.3 | 2 | 2 | 98 | . 29 | , 322 | 14 | 26 | 1.67 | 130 | $\bigcirc 35$ | 2 | 2.75 | . 09 | . 13 | 1 | 760 |
| SER-90-B-14 | 5 | 213 | 34 | 179 | $\stackrel{7}{7}$ | 22 | 15 | 1237 | 10.09 | 20 | 5 | ND | 5 | 73 | 1.3 | 2 | 2 | 85 | . 23 | ,337 | 15 | 27 | 1.44 | 184 | -33. | 2 | 2.63 | . 07 | . 10 | , | 141 |
| SER-90-B-15 | 4 | 47 | 27 | 139 | 1.2 | 11 | 8 | 532 | 7.32 | 32 | 5 | ND | 3 | 55 | 3 | 2 | 3 | 81 | . 37 | , 158 | 17 | 27 | . 99 | 109 | .36 | 2 | 2.73 | . 13 | . 09 | 1 | 140 |
| SER-90-B-16 |  | 54 | 18 | 108 | $\stackrel{\circ}{6}$ | 39 | 12 | 568 | 9.93 | 40 | 5 | ND | 3 | 55 | 1.2 | 2 | 2 | 116 | . 41 | ¢201 | 9 | 31 | 1.55 | 74 | $\stackrel{45}{ }$ | 2 | 2.21 | . 14 | . 09 | 1 | 79 |
| SER-90-8-17 | 5 | 105 | 29 | 115 | 1.0 | 22 | 11 | 810 | 8.96 | 46 | 5 | ND | 5 | 70 | 1,1 | 2 | 4 | 79 | . 27 | -254 | 15 | 26 | 1.21 | 188 | $\stackrel{38}{ }$ | 2 | 2.70 | . 08 | . 78 | 1 | 145 |
| SER-90-8-18 | 6 | 219 | 43 | 155 | 1,1 | 25 | 15 | 1106 | 12.58 | 51 | 5 | ND | 11 | 73 | 1.5 | 2 | 4 | 74 | . 17 | +364 | 20 | 26 | 1.34 | 337 | . 29 |  | 2.98 | . 05 | . 11 | 1 | 110 |
| SER-90-8-19 | 5 | 223 | 55 | 183 | 1.4 | 30 | 23 | 1527 | 10.01 | 59 | 5 | ND | 5 | 51 | 1.7. | 2 | 4 | 68 | . 12 | . 309 | 17 | 24 | 1.38 | 210 | -39 | 2 | 2.80 | . 04 | . 08 | 1 | 320 |
| STANDARD C/AU-S | 18 | 57 | 38 | 131 | 6.8 | 70 | 32 | 1049 | 3.97 | 38 | 21 | 7 | 38 | 53 | 18,4 | 15 | 20 | 55 | . 52 | .094 | 37 | 57 | . 90 | 180 | .09 | 35 | 1.90 | . 06 | . 14 | 11 | 45 |

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| SAMPLE\＃ | $\begin{array}{r} \text { Mo } \\ \text { pppa } \end{array}$ |  | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{pp} \mathrm{~m} \end{array}$ | $\text { b } \quad 2 n$ |  | $\begin{gathered} \mathrm{Ni} \\ \hline \mathrm{pp} \end{gathered}$ | $\begin{aligned} & \text { Co } \\ & \text { ppin } \end{aligned}$ | $\begin{aligned} & \text { Mn } \\ & \\ & \hline \end{aligned}$ | $\begin{array}{r} \mathrm{Fe} \\ \mathbf{x} \end{array}$ | $\begin{array}{\|c\|} \text { nsp } \\ \text { pp } \end{array}$ | $\begin{array}{r} \text { U } \\ \text { Ppm } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{aligned} & \text { Th } \\ & \text { ppin } \end{aligned}$ | $\begin{gathered} \mathrm{Sr} \\ \mathrm{ppp} \end{gathered}$ |  | $\begin{aligned} & \text { Sb } \\ & \text { ppm } \end{aligned}$ | $\begin{array}{r} \mathbf{8 i} \\ \text { ppin } \end{array}$ | $\begin{array}{r} V \\ \text { ppim } \end{array}$ | $\begin{gathered} \mathbf{C a} \\ \boldsymbol{\chi} \end{gathered}$ |  | La | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppm} \end{gathered}$ | $\begin{gathered} \mathrm{Hg} \\ \mathbf{Z} \end{gathered}$ | $\mathrm{g} \text { Ba }$ |  |  | $\begin{gathered} \mathbf{A !} \\ \mathbf{X} \end{gathered}$ | $\begin{array}{r} \mathrm{Na} \\ \mathbf{Z} \end{array}$ | $\ddot{\%}$ |  | lub |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| －12＋004 | 6 | 48 | 10 | 63 | 外2 | 8 | 16 | 1542 | 5.89 | $\stackrel{2}{2}$ | 5 | ND | 1 | 48 | ＊${ }^{2}$ | 2 | 2 | 72 | ． 37 | 098 | 16 | 17 | ． 58 | 97 | 3 S | 5 | 3.35 | 11 | ． 08 |  | 7 |
| 8 11＋7 | 4 | 26 | 5 | 579 | ＊ 1 | 15 | 7 | 777 | 5.26 | \％ | 5 | ND | 1 | 127 | \＄ 4 | 2 | 2 | 65 | ． 73 | ，098 | 4 | 26 | 1.00 | 107 | 和 3 | 6 | 1.86 | ． 07 | ． 10 | \％ | 7 |
| 8 $11+25 \mathrm{~W}$ | 6 | 27 | 18 | 65 | \％2 | 3 | 2 | 285 | 7.02 | \％ 3 | 5 | ND | 6 | 10 | 2 | 2 | 2 | 57 | ． 06 | ， 059 | 39 | 20 | ． 11 | 16 | \％27 | 7 | 4.42 | ． 04 | ． 05 | $\stackrel{1}{ }$ | 2 |
| B 10＋254 | 7 | 34 | 21 | 90 | \＆ 2 | 6 | 3 | 299 | 3.56 | \％ | 5 | ND | 1 | 58 | 4 | 2 | 2 | 58 | ． 25 | 07\％ | 16 | 17 | ． 70 | 172 | 交2 | 5 | 2.46 | ． 01 | ． 04 | ＊人去 | 32 |
| 8 10＋00N | 3 | 33 | 16 | 71 | \％ 2 | 9 | 5 | 471 | 3.35 | 12 | 5 | ND | 2 | 84 | \% | 3 | 2 | 49 | ． 41 | $103$ | 8 | 20 | 1.06 | 282 | $82$ | 4 | 1.77 | ． 05 | ． 19 |  | 148 |
| B 9＋75W | 5 | 20 | 19 | 49 | 的 | 3 | 2 | 132 | 6.99 | 6 | 5 | ND | 2 | 12 | 紬 | 2 | 2 | 106 | ． 08 | \％062 | 16 | 17 | ． 13 | 25 |  | 7 | 1.43 | ． 02 | ． 05 | 納 | 7 |
| B 9＋504 | 9 | 20 | 13 | 90 | \％ 3 | 4 | 3 | 439 | 9.30 | 85 | 5 | ND | 6 | 6 | 者 | 2 | 2 | 35 | ． 09 | \％05\％ | 57 | 14 | ． 01 | 18 |  | 5 | 3.76 | ． 05 | ．06 | 納 | 3 |
| B 9＋25W | 9 | 23 | 19 | 67 | \％2 | 5 | 4 | 477 | 8.77 | 8 | 5 | ND | 4 | 12 | \％ | 2 | 2 | 94 | ． 11 | 133 | 15 | 17 | ． 25 | 25 | \％ 6 | 6 | 1.99 | ． 02 | ． 04 | \％ | 8 |
| B 9＋00N | 3 | 19 | 49 | 32 | 3 | 2 | 1 | 147 | 5.42 | 16 | 5 | NO | 6 | 13 | 2 | 2 | 4 | 36 | ． 04 | ，047 | 2 | 5 | ． 22 | 51 | 苼 5 | 6 | ． 50 | ． 01 | ． 06 | 2 | 68 |
| B 8＋75W | 5 | 27 | 45 | 85 | \％ | 10 | 4 | 440 | 6.38 | 24 | 5 | ND | 1 | 59 | \％ | 2 | 2 | 75 | ． 31 | \％06\％ | 7 | 29 | ． 78 | 264 | \％ | 5 | 2.42 | ． 01 | ． 10 |  | 40 |
| B 8＋50W | 10 | 41 | 13 | 72 | 就 | 6 | 3 | 118 | 1.35 | \％ 4 | 5 | ND |  | 20 | \％＊ |  | 2 | 49 | ． 26 | \％ $0^{0}$ | 42 | 20 | .41 | 35 | 年 ${ }^{\text {\％}}$ | 2 | 4.97 | ． 03 | ． 03 | 納 | 8 |
| B 8＋25W | 1 | 65 | 33 | 68 | 寺 | 6 | 4 | 87 | 15.34 | 6 | 5 | No | 4 | 14 | ＊ 8 \％ | 3 | 2 | 118 | ． 12 | \％063 | 17 | 22 | ． 20 | 18 ： | \％ 0 | 3 | 2.87 | ． 04.02 | ． 02 | ＊＊ | 1 |
| B 8＋004 | 31 | 17 | 2 | 34 | \％ 2 | 3 | 2 | 35 | 7.39 | 2 | 5 | ND | 2 | 62 | ＊ 5 | 2 | 2 | 23 | ． 48 | \％ 067 | 16 | 3 | ． 03 | 10 | \％等皿 | 2 | 10.17 | ． 02 | ． 01 | 4 | 3 |
| BLI 10＋00N 3＋00N | 8 | 45 | 19 | 86 | \％ 2 | 11 | 10 | 571 | 5.24 | 11 | 5 | NO | 5 | 74 | \％ 2 | 3 | 2 | 61 | ． 43 | 148 | 21 | 16 | ． 90 | 214 | 的 | 7 | 2.19 | ． 10 | ． 11 |  | 22 |
| BLI 10＋00N 2＋75N | 8 | 48 | 14 | 60 | \％ 1 | 8 | 5 | 277 | 6.65 | \％$\%$ | 5 | ND | 4 | 39 | 郎䜌 | 2 | 4 | 81 | ． 28 | ， 12 | 20 | 20 | ． 60 | 53 | 率納 | 9 | 3.05 | ． 07. | ． 06 |  | 33 |
| BLI 1 10＋00W 2＋50 | 7 | 41 | 11 | 85 | \％ | 13 | 11 | 614 | 5.38 | \％ | 5 | ND | 5 | 75 | \％的 4 | 2 | 2 | 69 | ． 55 | 寺 $2 \%$ | 15 | 18 | 1.01 | 156 | 洨 0 | 7 | 2.52 | ． 18 | ． 12 | ＊ | 54 |
| BLI 10＋00N $2+25 \mathrm{~N}$ | 11 | 51 | 14 | 66 | 4 | 11 | 27 | 974 | 6.67 | － | 5 | ND | 7 | 59 | 就2 | 5 | 2 | 64 | ． 33 | 88\％ | 11 | 16 | ． 90 | 220 | シ， 3 | 6 | 1.90 | ． 07. | ． 08 | 䊽 | 56 |
| BLI 10＋00N 2＋00N | 7 | 49 | 13 | 128 | \％ | 14 | 10 | 857 | 5.58 | 7 | 5 | ND | 4 | 85 | 先 | 2 | 2 | 69 | ． 54 | 155 | 22 | 26 | 1.16 | 448 | ＊ 3 | 6 | 2.38 | ． 10 | ． 14 | ＊＊ | 84 |
| BLI 10＋00N 1＋75N | 5 | 63 | 12 | 320 | ＋ | 16 | 30 | 3784 | 6.99 | 5 | 5 | ND | 1 | 59 | \％ | 3 | 2 | 81 | ． 53 | \％ 215 | 14 | 29 | 1.62 | 358 ； | 蒳 | 6 | 3.44 | ． 08 | ． 08 | ＊㸚 | 26 |
| BLI 10＋00N 1＋50N | 1 | 23 | 6 | 83 | \％ 2 | 18 | 17 | 538 | 4.66 | ？ | 5 | ND | 1 | 109 | 行 | 2 | 2 | 94 | 1.06 | \％98 | 4 | 18 | 1.20 | 76 | \％为䅋 | 6 | 1.80 | ． 36. | ． 14 |  | 14 |
| BLI 10＋00W 1＋25 | 48 | 53 | 14 | 75 | \％ | 8 | 16 | 608 | 4.33 | \％ 3 | 5 | ND | 1 | 50 | \％ | 2 | 2 | 72 | ． 29 | －094 | 21 | 24 | ． 64 | 144 | 侍 | 7 | 2.81 | ． 02. | ． 05 | 緢 | 41 |
| BLI 10＋00N 0＋50N | 10 | 71 | 12 | 66 | \％ | 5 | 6 | 410 | 6.63 | \％$\%$ | 5 | ND | 1 | 57 | \％${ }^{\text {s }}$ | 2 | 2 | 52 | ． 19 | \％092 | 14 | 13 | ． 71 | 135 | \％ 16 | 5 | 2.56 | ． 01. | ． 05 |  | 23 |
| BLI 10＋004 0＋25N | 7 | 25 | 3 | 54 | \％ | 3 | 2 | 168 | 9.12 | 10 | 5 | ND | 6 | 5 | \％$\%$ | 2 | 2 | 37 | ． 05 | 052 | 43 | 20 | ． 01 | 14 | ＊ 22 | 7 | 5.23. | ． 03. | ． 04 |  | 4 |
| BLI 9＋00N 3＋00N | 9 | 46 | 13 | 78 | ＋ | 9 | 4 | 339 | 6.04 | 10 | 5 | ND | 5 | 28 | \％ | 2 | 2 | 55 | ． 14 | \％ 109 | 26 | 20 | ． 56 | 50 |  | 7 | 3.41. | ． 04. | ． 07 |  | 16 |
| BLI 9＋00W 2＋75N | 9 | 23 | 17 | 105 | ＊ | 7 | 5 | 533 | 7.16 | \％10 | 5 | ND | 15 | 9 | \％ 3 | 2 | 2 | 38 | ． 10 | \％ 058 | 22 | 11 | ． 21 | 25 |  | 7 | 3.94 ． | ． 13. | ． 09 |  | 3 |
| BLI 9＋00W $2+50 \mathrm{~N}$ | 7 | 32 | 11 | 75 | 令 | 4 | 2 | 214 | 7.39 | 15 | 5 | ND | 8 | 5 | \％$\%$ | 2 | 2 | 37 | ． 07 | \＄07\％ | 37 | 14 | ． 11 | 9 | \％ 22 | 6 | 4.21. | ． 06. | ． 08 |  | 11 |
| BLI 9＋00N $2+25 \mathrm{~N}$ | 8 | 38 | 16 | 73 | \％ 1 | 10 | 6 | 372 | 5.02 | ＊ | 5 | ND | 3 | 46 | \％ 2 | 2 | 2 | 61 | ． 29 | 097 | 18 | 19 | ． 74 | 63 | ＊$\%$ | 6 | 2.50. | ． 08. | ． 07 | ＊約 | 36 |
| BLI $9+00 \mathrm{~N} 2+00 \mathrm{~N}$ | 11 | 33 | 18 | 71 | ＊ | 9 | 5 | 342 | 4.91 | \％ | 5 | ND | 2 | 55 | \％ 4 | 2 | 2 | 60 | ． 29 | \％ 108 | 13 | 18 | ． 79 | 125 |  | 7 | 2.10 | ． 05 | ． 06 | 紬 | 38. |
| BLI $9+00 \mathrm{~N} 1+75 \mathrm{~N}$ | 31 | 64 | 11 | 68 | \＆ | 10 | 5 | 371 | 6.84 | 10 | 5 | ND | 1 | 42 | 行 | 2 | 2 | 56 | ． 19 | 3134 | 19 | 38 | ． 70 | 95 |  | 6 | 5.04 | ． 01. | ． 03 | \％isk | 31 |
| BLI $9+00 \mathrm{N1+50N}$ | 6 | 49 | 16 | 56 | \％ 2 | 6 | 4 | 137 | 4.78 | 4 | 5 | ND | 1 | 18 | \％ 2 | 2 | 2 | 87 | ． 20 | 080 | 22 | 29 | .33 | 28 | 多新 | 6 | 4.30 ． | ． 04. | ． 04 | 絞 | 6 |
| BLI $9+00 \mathrm{~W} 1+25 \mathrm{~N}$ | 10 | 24 | 13 | 63 | ＊ | 3 | 2 | 341 | 12.38 | \％${ }^{\text {a }}$ | 9 | Ho | 11 | 4 | \％ 1 \％ | 2 | 2 | 41 | ． 04 | \％093 | 26 | 17 | ． 01 | 13 |  | 4 | 3.49. | ． 03. | ． 03 | 紬 | 1 |
| BLI 9＋00N 1＋00N | 10 | 22 | 13 | 73 | 2 | 4 | 6 | 1039 | 8.79 | 13 | 5 | NO | 8 | 7 | 紷 6 | 3 | 2 | 63 | ． 06 | \％4\％ | 34 | 21 | ． 10 | 9 | 考尔 | 4 | 2.89. | ． 04. | ． 05 | ＊ | 1 |
| BLI 9＋00N 0＋75N | 8 | 20 | 15 | 69 | 戍 | 3 | 2 | 557 | 7.89 | 14 | 5 | ND | 8 | 4 | \％ 2 | 2 | 4 | 30 | ． 06 | \％ 050 | 36 | 15 | ． 01 | 6 | 多埰 | 6 | 4.66 .05 | ． 05. | ． 04 | ＊ | 1 |
| BLI 9＋00W 0＋50N | 7 | 14 | 12 | 87 | ，\％ | 4 | 3 | 442 | 6.09 | 14 | 8 | ND | 14 | 4 | \＆ 2 | 2 | 2 | 16 | ． 06 | 033 | 48 | 8 | ． 08 | 27 | 䋛寊 | 6 | 5.05. | ． 07. | ． 07 | ＊ | 34 |
| BLI 9＋00W $0+25 \mathrm{~N}$ | 24 | 115 | 26 | 116 | \％ 2 | 11 | 24 | 973 | 9.09 | 38 | 5 | ND | 3 | 52 | $10$ | 4 | 2 | 58 | ． 49 | V70 | 8 | 12 | ． 89 | 74 | 多 88 | 3 | 1.90. | ． 18. | ． 08 | $i_{i}$ | 59 |
| BLI 8＋00W 3＋00N | 9 | 27 | 7 | 74 | \％ | 6 | 4 | 357 | 4.45 | 5 | 5 | ND | 1 | 50 | 新 | 3 | 3 | 58 | ． 25 | 125 | 7 | 14 | ． 63 | 152 | －20 | 7 | 2.21. | ． 02. | ． 05 | 效 | 27 |
| STANDARD C／AU－S | 19 | 60 | 37 | 131 | 6．8． | 72 | 31 | 1048 | 3.97 | 39 | 19 | 6 | 39 | 52 | 18．6． | 15 | 18 | 59 | ． 52 | 09\％ | 38 | 57 | ． 90 | 182 | 80\％ | 40 | 1.89. | ． 06. | ． 14 | \％ | 45 |

ICP－． 500 GRAM SAMPLE IS DIGESTED WITH 3ML 3－1－2 HCL－HNO3－H2O AT 95 DEG．C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER．
THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI 8 H AND LIMITED FOR NA K AMP AlP AU DETECTION LIMIT BY ICP IS 3 PPM．
－SAMPLE TYPE：P1－6 SOIL P7 ROCK AU＊ANALYSIS BY ACID LEACH／AA FROM 10 GM SAMPLE．f


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| SAMPLE\＃ | $\begin{aligned} & \text { Mo } \\ & \text { Pppm } \end{aligned}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \\ \hline \end{array}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \text { ppm } \end{array}$ | ing | $\begin{gathered} \mathbf{N i} \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { pprn } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \% \end{gathered}$ | $\underset{\text { prus }}{\boldsymbol{n}}$ | $\begin{array}{r} \mathrm{U} \\ \text { ppm } \end{array}$ | $\begin{gathered} \text { Au } \\ \text { ppm } \end{gathered}$ | $\begin{aligned} & \text { Th } \\ & \text { ppprin } \end{aligned}$ | $\begin{array}{r} \mathbf{S r} \\ \mathrm{pppm} \end{array}$ |  | $\begin{array}{r} \text { Sb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} B i \\ \text { ppom } \end{array}$ | $\begin{array}{r} \mathrm{V} \\ \mathrm{ppn} \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{\%} \end{gathered}$ | $\stackrel{\otimes}{8}$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\underset{\mathrm{ppm}}{\mathrm{Cr}}$ | $\begin{aligned} & \hline \mathbf{M g} \\ & \boldsymbol{\%} \end{aligned}$ | $\begin{gathered} \mathrm{Ba} \\ \mathrm{pppm} \end{gathered}$ | $\begin{aligned} & \text { Kive } \\ & \text { kisisisis } \\ & \hline \end{aligned}$ | $\begin{array}{r} B \\ \text { ppin } \end{array}$ | $\underset{X}{A l}$ | $\begin{gathered} \mathrm{Na} \\ \boldsymbol{\%} \end{gathered}$ | $\mathbf{Z}$ |  | $\begin{aligned} & \text { Au } \\ & \text { Ppb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BLI $8+00 \mathrm{~W} 2+75 \mathrm{~N}$ | 8 | 33 | 19 | 99 | \＄3． | 15 | 7 | 811 | 6.70 | 16 | 5 | ND | 12 | 26 | \％ 8 | 2 | 2 | 44 | ． 13 | \％084 | 30 | 21 | ． 69 | 85 | 24 |  | 3.50 | ． 05 | ． 07 | \％s\％ | 31 |
| 8LI $8+00 \mathrm{~N} 2+50 \mathrm{~N}$ | 12 | 121 | 21 | 65 | 约 | 7 | 3 | 207 | 10.72 | 15． | 5 | HD | 9 | 16 | \％ | 2 | 2 | 63 | ． 08 | 8085 | 26 | 24 | ． 31 | 17 | \％\％ |  | 2.89 | ． 05 | ． 05 | \％ | 79 |
| BLI $8+00 \mathrm{~N} 2+25 \mathrm{~N}$ | 25 | 175 | 8 | 107 | \％2 | 4 | 13 | 812 | 5.77 | \％ | 5 | ND | 6 | 71 | \％$\%$ 。 | 2 | 2 | 51 | ． 25 | 16\％ | 9 | 8 | ． 96 | 57 | 六2． |  | 1.64 | ． 02 | ． 05 | 有 | 20 |
| 8L1 $8+00 \mathrm{~N} 2+00 \mathrm{~N}$ | 9 | 19 | 12 | 74 | ＊ | 3 | 3 | 217 | 6.44 | 18 18 | 5 | NO | 15 | 4 | \％为8． | 3 | 2 | 14 | ． 05 | \％ 040 | 40 | 10 | ． 04 | 10 | k 18 |  | 4.87 | ． 07 | ． 05 | 湤 | 6 |
| 6LI 8＋00N 1＋75N | 34 | 61 | 13 | 69 | 緃 | 5 | 8 | 448 | 5.62 | \％2 | 5 | ND | 6 | 7 | \％㳰 | 3 | 2 | 34 | ． 07 | \％ 040 | 37 | 15 | ． 16 | 11 維 | 的 2. |  | 3.97 | ． 07 | ． 06 |  | 3 |
| BLI $8+00 \mathrm{~N} 1+50 \mathrm{~N}$ | 13 | 31 | 24 | 48 | \％ | 4 | 4 | 290 | 3.79 | 17 | 5 | ND | 3 | 15 | s2 | 2 | 2 | 31 | ． 09 | \％ 05 | 4 | 8 | ． 42 | 54 |  | 4 | ． 89 | ． 02 | ． 06 | ＊ | 98 |
| BLI $8+00 \mathrm{~N} 1+25 \mathrm{~N}$ | 4 | 43 | 76 | 123 | 曻 | 14 | 4 | 709 | 3.19 | 21 | 5 | ND | 2 | 61 | 引細 | 3 | 2 | 56 | ． 20 | \％${ }^{\circ} 8$ | 8 | 29 | 1.12 | 404 | 渋的盎 |  | 1.62 | ． 01 | ． 13 | \％ | 55 |
| 8LI $8+00 \mathrm{~W} 1+00 \mathrm{~N}$ | 5 | 40 | 145 | 125 | 碞 | 51 | 4 | 905 | 4.14 | 外 | 5 | ND | 2 | 65 | \％ | 2 | 2 | 60 | ． 27 | \％08\％ | 11 | 96 | 1.42 | 281 | 26 |  | 2.12 | ． 01 | ． 08 | 跤 | 80 |
| BLI $8+00 \mathrm{~N} 0+75 \mathrm{~N}$ | 7 | 24 | 16 | 57 | \％ 2 | 5 | 4 | 280 | 7.29 | 10 | 5 | ND | 7 | 7 | 納为 | 3 | 2 | 65 | ． 07 | S048 | 29 | 22 | ． 22 | 15 |  |  | 2.97 | ． 04 | ． 06 | 行 | 4 |
| BLI $8+00 \mathrm{~N} 0+50 \mathrm{~N}$ | 1 | 91 | 6 | 30 | ＊ 2 | 3 | 4 | 36 | 41.65 | 2 | 5 | ND | 4 | 3 | $42$ | 7 | 2 | 52 | ． 02 | §4＊ | 5 | 6 | ． 01 | 6 | 令为 |  | 1.03 | ． 01 | ． 01 | \％为 | 2 |
| BLI $8+00 \mathrm{~N} \quad 0+25 \mathrm{~N}$ | 75 | 12 | 7 | 49 | \％ | 5 |  | 196 | ． 91 \％ | \％ 17 | 5 | ND | 1 | 383 | 认約 | 2 | 2 | 6 | 2.91 | \％\％ | 24 | 4 | ． 01 | 21 \％ | 紋0， | 2 | 1.88 | ． 02 | ． 01 | \％9 | 1 |
| BLI 7＋00W 3＋00N | 5 | 200 | 2 | 39 | \％2 | 4 | 3 | 66 | 7.29 | 20 | 5 | ND | 2 | 6 | 人考 | 5 | 2 | 27 | ． 04 | \％2 | 36 | 16 | ． 05 | 12 | ＊it |  | 7.10 | ． 01 | ． 01 | ＊納 | 8 |
| BLI 7＋00N $2+75 \mathrm{~N}$ | 13 | 97 | 70 | 146 | \％ 8 | 11 | 21 | 1117 | 9.02 | 48 | 5 | ND | 3 | 55 | \％ 5 | 6 | 2 | 70 | ． 25 | 323 | 12 | 29 | ． 97 | 150 | \％ 26 |  | 1.86 | ． 04 | ． 08 | ＊＊ | 102 |
| BLI $7+00 \mathrm{~N} 2+50 \mathrm{~N}$ | 6 | 22 | 9 | 70 | 的 | 4 | 4 | 450 | 6.90 | 14 | 5 | ND | 6 | 6 | \％$\%$ \％ | 2 | 2 | 41 | ． 06 | 8053 | 35 | 21 | ． 10 | 15 | \＄2\％ |  | 5.01 | ． 05 | ． 05 | 行 | 3 |
| BLI 7＋00W 2＋25N | 8 | 55 | 110 | 73 | \％ 8 | 7 | 3 | 432 | 4.08 | 29 | 5 | ND | 3 | 53 | \％${ }^{2}$ 。 | 2 | 2 | 51 | ． 20 | 180 | 6 | 20 | ． 81 | 80 | $2 \%$ |  | 1.58 | ． 01 | ． 05 | 㾧 | 53 |
| BLI 7＋001 2＋00N | 7 | 17 | 22 | 110 | \％${ }^{\text {\％}}$ | 4 | 5 | 832 | 7.41 | \％ 18 | 5 | ND | 8 | 5 | \％$\%$ | 3 | 2 | 33 | ． 06 | －038 | 38 | 16 | ． 11 | 14 | \％22 |  | 4.13 | ． 09 | ． 09 | \％ | 3 |
| BLI 7＋00N 1＋75N | 7 | 13 | 11 | 77 | \＆2 | 3 | 3 | 1089 | 6.27 | 14 | 5 | ND | 6 | 4 | \＃，\％ | 3 | 2 | 20 | ． 05 | \％ 05 | 45 | 11 | ． 06 | 14 | ＊ 3 |  | 5.16 | ． 06 | ． 06 | 行 | 2 |
| BLI 7＋00N 1＋50N | 6 | 28 | 26 | 51 | \％ | 5 | 2 | 266 | 7.61 | 17 | 5 | ND | 9 | 30 | \％$\%$ |  | 2 | 50 | ． 15 | 847 | 19 | 21 | ． 45 | 43 | ， 25 |  | 4.35 | ． 01 | ． 03 | \％ | 17 |
| BLI $7+00 \mathrm{~N} 1+00 \mathrm{~N}$ | 9 | 36 | 21 | 71 | ＊ 4 \％ | 5 | 2 | 311 | 8.28 | 15． | 5 | ND | 12 | 23 | K\％ | 2 | 5 | 58 | ． 10 | 878 | 16 | 22 | ． 30 | 41 | ＊ 2 \％ |  | 4.55 | ． 03 | ． 05 | 碞 | 25 |
| BLI $7+00 \mathrm{~N} \quad 0+75 \mathrm{~N}$ | 10 | 26 | 15 | 76 |  | 6 | 4 | 350 | 8.74 | 13 | 5 | ND | 6 | 16 | \％紬 | 2 | 2 | 58 | ． 09 | \％ 0.6 | 26 | 20 | ． 28 | 20 | 兗3＊ |  | 2.72 | ． 03 | ． 05 |  | 4 |
| BLI 7＋00H $0+50 \mathrm{~N}$ | 38 | 75 | 13 | 119 | 就 | 11 | 28 | 2196 | 4.22 | 8 | 5 | ND | 4 | 56 | \％ | 2 | 2 | 27 | ． 37 | － 5 | 21 | 10 | ． 64 | 132 |  |  | 2.39 | ． 01 | ． 03 | 行 | 8 |
| 8L： $7+00 \mathrm{~N} \quad 0+25 \mathrm{~N}$ | 14 | 46 | 19 | 84 | ＊ | 6 | 12 | 587 | 4.70 | 8 | 5 | MD | 2 | 45 | \％ | 2 | 2 | 62 | ． 28 | \％78 | 11 | 15 | ． 59 | 49 | ＊ |  | 2.60 | ． 03 | ． 04. | 納䊽 | 100 |
| BLI $6+00 \mathrm{~N} 3+00 \mathrm{~N}$ | 8 | 18 | 13 | 85 | 豹 | 3 | 5 | 1006 | 6.71 | \％ 88 | 5 | ND | 16 | 4 | \％ 6 | 2 | 2 | 20 | ． 06 | \％34 | 33 | 11 | ． 08 | 10 | 約 |  | 4.53 | ． 08 | ． 07 | 场 | ， |
| BLI $6+00 \mathrm{~N} \mathrm{2+75N}$ | 7 | 15 | 18 | 76 | ＊ | 3 | 3 | 634 | 6.07 | \％ 88 | 5 | ND | 11 | 3 | ， | 2 | 2 | 20 | ． 06 | 8044 | 38 | 10 | ． 05 | 9 | ＊ $1 \%$ |  | 4.86 | ． 06 | ． 06 | 晾 | 2 |
| BLI 6＋00N 2＋50N | 6 | 12 | 10 | 54 | $\%$ | 4 | 6 | 559 | 4.09 | 6 | 5 | ND | 1 | 43 | ＊${ }^{\text {\％}}$ | 2 | 2 | 46 | ． 21 | 3067 | 11 | 12 | ． 48 | 41 | 晈紷 | 4 | 2.00 | ． 02 | ． 04 |  | 87 |
| BLI 6＋00W 2＋25N | 6 | 18 | 15 | 78 | 的 | 4 | 5 | 1169 | 6.17 | 3 | 5 | ND | 7 | 4 | \％ 2 | 4 | 2 | 31 | ． 07 | \％048 | 34 | 15 | ． 09 | 13 | 洔20 |  | 3.82 | ． 06 | ． 07.05 | 葹 | 10 |
| BLI 6＋001 2＋00N | 5 | 39 | 13 | 73 | \％ 1 | 5 | 15 | 942 | 4.34 | \％ | 5 | ND | 7 | 84 | ＊ | 2 | 2 | 34 | ． 51 | 多68 | 10 | 10 | ． 86 | 160 | ＊ $0 \%$ |  | 1.86 | ． 01 | ． 05 | ＊${ }_{\text {\％}}$ | 10 |
| BLI $6+00 \mathrm{~W} 1+75 \mathrm{~N}$ | 16 | 41 | 19 | 68 | \％ | 7 | 12 | 747 | 5.31 | 12 | 5 | ND | 3 | 51 | \％$\%$ | 2 |  | 53 | ． 39 | \％2 | 29 | 12 | ． 72 | 51 | ＊納 |  | 2.39 | ． 08 | ． 06 |  | 120 |
| 8LI $6+00 \mathrm{~W} 1+50 \mathrm{~N}$ | 2 | 18 | 9 | 48 | \＆ | 4 | 10 | 739 | 2.46 | 2 | 5 | NO | 2 | 90 | \％ 2 | 2 | 2 | 26 | ． 67 | \％ 40 | 8 | 5 | ． 74 | 54 |  |  | 1.31 | ． 01 | ． 03 | 2 | 4 |
| BLI 6＋00N 1＋25N | 7 | 19 | 15 | 70 | ＊$\downarrow$ | 6 | 4 | 461 | 9.78 | ＋14 | 5 | NO | 6 | 19 | 的 | 2 | 3 | 49 | ． 15 | \＄052 | 25 | 17 | ． 15 | 19 | ＊ 8 \％ | 3 | 3.38 | ． 03 | ． 04 |  | 2 |
| BLI 6＋00W 1＋00N | 7 | 20 | 16 | 83 | 紷 | 4 | 4 | 846 | 7.49 | 18 | 5 | ND | 10 | 5 | \％的客 | 3 | 2 | 34 | ． 06 | － 04 | 37 | 17 | ． 08 | 12 | 8，${ }^{2}$ |  | 4.69 | ． 06 | ． 06 | \％ | 2 |
| BLI 6＋004 0＋75N | 2 | 10 | 10 | 49 | \％ | 2 | 5 | 916 | 2.03 | 2 | 5 | ND | 2 | 47 | 就 | 2 | 2 | 61 | ． 30 | － 85 | 7 | 6 | ． 45 | 34 | 30 |  | 1.00 | ． 03 | ． 03 | ¢ | 3 |
| BLI $6+00 \mathrm{~N} 0+50 \mathrm{~N}$ | 35 | 40 | 15 | 131 | \％ | 5 | 4 | 478 | 6.74 | 22 | 5 | ND | 18 | 22 | 效 | 2 | 2 | 19 | ． 22 | O4\％ | 39 | 12 | ． 23 | 63 | \％ 8 |  | 4.36 | ． 08 | ． 08 | 得 | 3 |
| BLI $6+00 \mathrm{~N} \quad 0+25 \mathrm{~N}$ | 6 | 32 | 12 | 58 | \％ | 5 | 15 | 2158 | 4.45 | 4 | 5 | ND | 4 | 43 | \％$\%$ \％ | 2 | 2 | 43 | ． 22 | \％92 | 15 | 13 | ． 57 | 23 | ＊ |  | 2.44 | ． 03 | ． 04 |  | 1 |
| BLI 5＋00W 3＋00N | 1 | 710 | 4 | 49 | $\$ .5$ | 10 | 7 | 200 | 3.23 | 2 | 5 | ND | 1 | 16 |  | 5 | 2 | 64 | ． 25 | \％ 16 | 37 | 18 | ． 61 | 27 | ＊ 48 | 3 | 6.58 | ． 04 | ． 05 |  |  |
| BLI 5＋00W 2＋50N | 3 | 401 | 9 | 61 | \％ | 12 | 14 | 311 | 3.38 | 2 | 5 | ND | 2 | 96 |  | 2 | 2 | 77 | 1.04 | \％94 | 32 | 14 | ． 85 | 47 | 50． |  | 3.20 | ． 39 | ． 16 | ， | 1 |
| STANDARD C／AU－S | 18 | 58 | 36 | 131 | \％．$\%$ | 71 | 32 | 1048 | 3.97 | 38 | 20 | 7 | 40 | 52 | 18．4＊ | 18 | 19 | 57 | ． 52 | －088 | 37 | 57 | ． 90 | 182 | ．09\％ | 37 | 1.90 | ． 06 | ． 14 | 䍃 | 46 |

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| SAMPLE＊ | $\begin{array}{r} \text { Mo } \\ \text { pppm } \end{array}$ | $\begin{array}{r} \mathrm{Cu} \\ \text { ppom } \end{array}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{pppm} \end{array}$ | $\begin{array}{r} \text { 2n } \\ \text { ppm } \end{array}$ |  | $\begin{array}{r} \mathbf{N i} \\ \text { ppom } \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} M n \\ \text { Mpm } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \mathrm{Z} \\ \hline \end{gathered}$ | ispre | $\begin{array}{r} \mathbf{U} \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Au } \\ \text { ppin } \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | $\underset{\text { prin }}{\mathbf{S r}}$ |  | $\begin{array}{r} \mathbf{S b} \\ \mathbf{p p m} \end{array}$ | $\begin{array}{r} \mathbf{B i} \\ \mathbf{p p m} \end{array}$ | $\begin{array}{r} v \\ \text { pprin } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{x} \end{gathered}$ | $\hat{N}_{\mathrm{k}}^{\mathrm{k}}$ | $\begin{array}{r} \text { La } \\ \text { pppa } \end{array}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppp} \\ \hline \end{gathered}$ | $\begin{aligned} & \mathrm{Hg} \\ & \mathbf{\%} \end{aligned}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ |  | $\begin{array}{r} \mathbf{8} \\ \text { ppan } \\ \hline \end{array}$ | $\begin{gathered} \text { A! } \\ \text { K } \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \boldsymbol{\%} \end{gathered}$ | $\mathbf{z}$ |  | $\begin{aligned} & \text { Au } \\ & \text { ppb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BLI 5＋00N 2＋25N | 10 | 40 | 16 | 58 | ， | 7 | 8 | 375 | 4.07 | 4 | 5 | ND | 4 | 54 | ， 2 | 3 | 3 | 73 | ． 45 | 057\％ | 15 | 21 | ． 73 | 30 | ＊ 40 |  | 2.40 | ． 08 | ． 05 | 絃 | 17 |
| BLI 5＋00N $2+00 \mathrm{~N}$ | 21 | 18 | 8 | 65 | 4 | 3 | 2 | 151 | 5.24 | 14 | 5 | ND | 20 | 5 | \＆ | 5 | 2 | 15 | ． 09 | 8，028 | 32 | 11 | ． 07 | 22 | 22\％ | 3 | 2.75 | ． 21 | ． 12 | 納㐫 |  |
| BLI 5＋00N 1＋75N | 13 | 18 | 12 | 92 | \％ | 4 | 3 | 465 | 7.18 | 20 | 9 | ND | 12 | 6 | \％\％ | 4 | 2 | 33 | ． 07 | 055 | 60 | 13 | ． 11 | 23 | 23． |  | 4.44 | ． 08 | ． 07 | 㐫 |  |
| BLI 5＋00N 1＋50N | 20 | 27 | 12 | 84 | S | 4 | 2 | 345 | 7.38 | 15 | 5 | ND | 11 | 4 | 率 2 | 2 | 2 | 28 | ． 07 | \＄086 | 49 | 14 | ． 10 | 17 | \％20 |  | 3.99 | ． 09 | ． 09 | 約 |  |
| BLI 5＋00N 1＋25N | 12 | 30 | 11 | 91 | \％ | 8 | 9 | 1987 | 6.83 | \％ 17 | 5 | ND | 7 | 6 | 納8 | 5 | 2 | 49 | ． 10 | 8076 | 41 | 21 | ． 26 | 22 | 湦2\％ | 8 | 4.33 | ． 09 | ． 08 |  |  |
| BLI 5＋00N 1＋00N | 9 | 14 | 15 | 80 | ＊ | 2 | 4 | 927 | 6.96 | 20 | 5 | ND | 17 | 3 | ＊is\％ | 3 | 2 | 17 | ． 07 | 4039 | 35 | 10 | ． 02 | 12 | 弾\％ |  | 4.24 | ． 08 | ． 07 |  |  |
| BLI 5＋00N 0＋75N | 7 | 18 | 9 | 67 | 2 | 3 | 5 | 703 | 6.69 | 13 | 5 | MD | 6 | 4 | 娄 | 5 | 2 | 29 | ． 05 | 8063 | 39 | 15 | ． 04 | 13 | 埧18 | 5 | 4.42 | ． 06 | ． 06 | 納 |  |
| BLI 5＋00N $0+50 \mathrm{~N}$ | 8 | 24 | 8 | 92 | 2 | 5 | 7 | 1745 | 6.65 | 14 | 5 | ND | 2 | 10 | 組娄 | 3 | 2 | 43 | ． 09 | 807\％ | 44 | 15 | ． 14 | 18 | 洨 1 | 5 | 3.79 | ． 05 | ． 05 |  |  |
| BL！5＋00N 0＋25N | 14 | 17 | 8 | 104 | 2 | 7 | 9 | 844 | 4.27 | 6 | 5 | ND | 3 | 55 | 餃娄 | 3 | 2 | 48 | ． 50 | 088 | 33 | 15 | ． 51 | 68 | 曻5 |  | 2.48 | ． 03 | ． 06 | 洨紋 |  |
| BLI 4＋00N 3＋00N | 4 | 61 | 13 | 71 | 2 0 | 9 | 8 | 461 | 4.53 | 星 | 5 | ND | 2 | 31 | 䏣务 | 2 | 2 | 61 | ． 33 | \％080 | 51 | 21 | ． 53 | 41 | \％ 26 | 2 | 3.16 | ． 08 | ． 07 |  |  |
| BLI 4＋00N $2+75 \mathrm{~N}$ | 12 | 94 | 18 | 67 | 3 | 8 | 18 | 888 | 3.83 | 14 | 5 | ND | 3 | 71 |  | 2 | 2 | 39 | ． 58 | \％ 0 \％ | 17 | 11 | ． 77 | 49 |  | 2 | 1.97 | ． 06 | ． 05 | 紷 | 34 |
| BLI 4＋00N 2＋50N | 8 | 20 | 10 | 58 | ， 2 | 6 | 5 | 311 | 3.44 | 5 | 5 | ND | 4 | 58 | 学 | 2 | 2 | 81 | ． 39 | 04\％ | 11 | 18 | ． 70 | 32 | 36 | 2 | 2.26 | ． 04 | ． 04 | \％繆顛 | 30 |
| $8 \mathrm{LI} 4+00 \mathrm{~N} 2+25 \mathrm{~N}$ | 10 | 23 | 8 | 67 | \％ | 8 | 4 | 381 | 6.96 | 10 | 5 | HD | 6 | 13 | 郎 2 | 2 | 2 | 72 | ． 12 | \％08\％ | 23 | 19 | ． 36 | 20 | 38 | 4 | 2.20 | ． 07 | ． 07 | 樃䊽 | 12 |
| BLI $4+00 \mathrm{~N} 2+00 \mathrm{~N}$ | 4 | 24 | 7 | 80 | ， 4 | 14 | 12 | 587 | 5.31 | 5 | 5 | ND | 3 | 60 | 晾 ${ }^{\text {S }}$ | 2 | 2 | 98 | ． 58 | ，062 | 8 | 21 | ． 84 | 50 | 脑4 | 2 | 2.35 | ． 19 | ． 09 | 納 |  |
| BLI 4＋00W 1＋75M | 8 | 16 | 14 | 106 | \＆ 1 | 4 | 4 | 736 | 6.66 | \％${ }^{\text {\％}}$ \％ | 5 | ND | 18 | 4 | $\psi_{i}$ | 2 | 2 | 22 | ． 07 | \％030 | 38 | 13 | ． 10 | 19 | ＊ 24 | 5 | 4.44 | ． 12 | ． 10 | \% \% |  |
| BLI 4＋00W 1＋50N | 11 | 20 | 2 | 82 | ， | 12 | 25 | 1051 | 7.01 | 10 | 5 | ND | 10 | 86 | 8 | 3 | 2 | 65 | ． 80 | 8123 | 15 | 16 | ． 97 | 45 | \＄ 6 |  | 2.61 | ． 26 | ． 11 | 紷 |  |
| 8LI $4+00 \mathrm{~N} \mathrm{1+25N}$ | 12 | 28 | 3 | 125 | ， 3 | 17 | 16 | 1389 | 5.26 | － | 6 | no | 7 | 72 | 3 | 2 | 2 | 68 | ． 64 | \％24 | 51 | 22 | ． 75 | 108 | 考3 | 3 | 4.15 | ． 11 | ． 09 | 行䊽 |  |
| 8LI $4+00 \mathrm{~N} 1+00 \mathrm{~N}$ | 4 | 41 | 4 | 92 | ，2 | 14 | 9 | 337 | 5.16 | 9 | 5 | ND | 6 | 46 | \％ | 2 | 2 | 95 | ． 50 | ， 102 | 20 | 23 | ． 73 | 53 | 60 |  | 3.86 | ． 14 | ． 08 |  |  |
| 8L！ $4+00 \mathrm{Na} 0+75 \mathrm{~N}$ | 9 | 19 | 12 | 69 | ， | 6 | 4 | 310 | 8.60 | 14 | 5 | ND | 9 | 10 | \％ 8 | 2 | 2 | 66 | ． 11 | \％048 | 24 | 20 | ． 23 | 16 | \％ 0 | 4 | 2.57 | ． 09 | ． 09 | \＃ |  |
| $81: 14+00 \mathrm{Na}$ | 8 | 24 | 9 | 73 | $\geqslant \%$ | 5 | 3 | 370 | 7.96 | 14 | 5 | NO | 6 | 8 | 就家 | 2 | 2 | 43 | ． 09 | $062$ | 38 | 20 | ． 14 | 15 |  | 4 | 3.79 | ． 07 | ． 07 | 者効 |  |
| 8LI $4+00 \mathrm{Na} 0+25 \mathrm{~N}$ | 10 | 16 | 21 | 84 | \％$\%$ | 3 | 3 | 713 | 8.92 | \％ 17 | 5 | ND | 14 | 4 | \％ | 3 | 2 | 32 | ． 06 | \％ 037 | 43 | 15 | ． 04 | 9 | \％ 28 | 3 | 3.55 | ． 06 | ． 07 | 行 |  |
| IL $4+000+255$ | 10 | 21 | 5 | 88 | \％ 2 | 5 | 3 | 181 | 6.02 | 16． | 5 | ND | 7 | 10 | \％$\%$ | 5 | 2 | 29 | ． 09 | \％072 | 32 | 18 | ． 11 | 22 |  |  | 5.33 | ． 05 | ． 05 | \％ |  |
| IL 4＋00 0＋505 | 4 | 25 | 6 | 93 | \％ 1 | 13 | 9 | 554 | 4.75 | 10 | 5 | NO | 7 | 42 | \％ 2 | 3 | 2 | 57 | ． 33 | 做103 | 25 | 19 | ． 66 | 39 | \％ 37 |  | 2.78 | ． 09 | ． 07 | 行 |  |
| IL． $4+000+755$ | 5 | 24 | 7 | 55 | \％ 4 | 5 | 4 | 568 | 5.75 | 8 | 5 | ND | 2 | 26 | \％ 3 | 2 | 2 | 44 | ． 16 | ，068 | 30 | 18 | ． 30 | 23 | 効 | 4 | 3.69 | ． 03 | ． 03 | 紬 |  |
| IL 4＋00 i＋00S | 8 | 8 | 9 | 82 |  | 4 | 2 | 372 | 9.09 | \％15 | 5 | ND | 9 | 5 |  | 2 | 2 | 37 | ． 05 | \％35 | 51 | 18 | ． 09 | 9 |  | 2 | 2.89 | ． 07 | ． 08 | $\boldsymbol{\psi}$ |  |
| IL． $4+00$ 1＋25s | 8 | 15 | 6 | 60 | \％$\%$ 2 | 4 | 5 | 494 | 8.45 | \％ $1 \%$ |  | ND | 4 | 11 | 紬 | 2 | 2 | 59 | ． 07 | \％054 | 26 | 18 | ． 10 | 14 | 交29 | 2 | 2.77 | ． 02 | ． 05 | 多 |  |
| IL． $4+001+505$ | 10 | 13 | 8 | 76 | \％ | 4 | 5 | 652 | 8.64 | \％ 10 | 5 | ND | 5 | 7 | 就 | 2 | 2 | 47 | ． 06 | \％ 066 | 35 | 17 | ． 09 | 15 | 做 |  | 3.25 | ． 03 | ． 05 | ＊ |  |
| IL 4＋00 1＋755 | 9 | 17 | 16 | 73 | \％$\%$ | 5 | 4 | 398 | 8.53 | \％ 10 | 5 | ND | 5 | 10 | 人\％ | 2 | 2 | 66 | ． 08 | \％ 06 | 25 | 20 | ． 17 | 13 | 食 3 |  | 3.15 | ． 03 | ． 04 | 䋛 |  |
| IL $4+002+005$ | 15 | 21 | 12 | 81 | ＊ | 7 | 13 | 1833 | 7.26 | 10 | 5 | ND | 2 | 11 | 的 6 | 3 | 2 | 80 | ． 11 | \％076 | 31 | 22 | ． 24 | 28 | \％${ }^{\text {3 }}$ |  | 3.35 | ． 04 | ． 04 |  |  |
| IL． $4+00$ 2＋25s | 5 | 21 | 13 | 50 | $\stackrel{*}{*}$ | 3 | 5 | 683 | 3.86 | $29$ | 13 | ND | 6 | 3 | $\xi_{i}$ | 19 | 2 | 33 | ． 04 | \％ $03 \%$ | 25 | 12 | ． 11 | 9 | 湤 | 6 | 2.52 | ． 03 | ． 04 |  |  |
| IL 4＋00 2＋505 | ， | 25 | 2 | 33 | ，\％\％ | 2 | 6 | 399 | 2.97 | 45 | 15 | ND | 7 | 8 | 8＊＊ | 34 | 2 | 30 | ． 03 | \％028 | 22 | 12 | ． 03 | 3 | 的只 |  | 1.89 | ． 03 | ． 05 | 多 |  |
| IL 4＋00 $2+75 \mathrm{~s}$ | 13 | 12 | 26 | 67 | \％ | 7 | 6 | 735 | 9.19 | 8 | 6 | NO | 7 | 8 | \％ 2 | 2 | 15 | 85 | ． 06 | 8042 | 18 | 23 | ． 22 | 19 | S2 | 2 | 3.16 | ． 03 | ． 03 | \％ | 8 |
| IL． $4+003+005$ | 9 | 23 | 12 | 88 | ， 1 | 5 | 5 | 907 | 7.14 | 18 | 5 | ND | 7 | 4 | \％ | 3 | 2 | 45 | ． 06 | \％047 | 35 | 22 | ． 14 | 16 | \％ 30 |  | 4.08 | ． 07 | ． 08 | \％ |  |
| IL． $5+000+25 s$ | 3 | 21 | 3 | 50 | 约 | 11 | 7 | 200 | 5.68 | 14 | 5 | ND | 4 | 17 | 量 | 3 | 2 | 113 | ． 24 | \％06\％ | 29 | 23 | ． 72 | 20 | \％ 88 |  | 2.40 | ． 05 | ． 05 | 行 | 7 |
| IL 5＋00 0＋50S | 8 | 18 | 14 | 52 | $\$ 2$ | 5 | 3 | 202 | 6.10 | 9 | 5 | NO | 1 | 17 | 紷 | 3 | 2 | 76 | ． 11 | 0.059 | 32 | 18 | ． 21 | 23 |  | 2 | 2.72 | ． 03 | ． 03 | §\#\# | 2 |
| IL 5＋00 0＋75S | 12 | 21 | 15 | 59 | 新 | 4 | 3 | 261 | 8.35 | 17 | 5 | ND | 4 | 19 | \％ | 3 | 3 | 76 | ． 24 | \％064 | 34 | 12 | ． 11 | 24 | ＊ 47 | 4 | 1.87 | ． 03 | ． 06 |  | 2 |
| SIANDARD C／AU－S | 19 | 58 | 37 | 131 | 8.9 | 70 | 32 | 1047 | 3.98 | 4！ | 21 | 7 | 39 | 52 | 38，4 | 14 | 20 | 56 | ． 52 | \％ 088 | 37 | 57 | ． 89 | 182 | \％ $0 \%$ | 33 | 1.89 | ． 06 | ． 14 | 3／ | 48 |

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| SAMPLE\＃ | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Cu} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} 2 n \\ \text { ppm } \end{array}$ |  | $\begin{gathered} \mathrm{Ni} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { ppon } \end{array}$ | $\begin{array}{r} M n \\ \text { ppn } \end{array}$ | Fe | $\stackrel{\boldsymbol{o}_{1}}{\text { Ppon }}$ | $\begin{array}{r} \mathrm{U} \\ \text { ppin } \end{array}$ | $\begin{gathered} \mathrm{Au} \\ \mathrm{pppa} \end{gathered}$ | $\begin{aligned} & \text { Th } \\ & \text { ppm } \end{aligned}$ | $\begin{array}{r} \mathrm{Sr} \\ \mathrm{pppm} \end{array}$ |  | $\begin{array}{r} \mathrm{Sb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} 8 i \\ \text { ppm } \end{array}$ | $\begin{array}{r} V \\ p p x^{\prime} \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{X} \end{gathered}$ | $\stackrel{\psi}{\psi}$ | $\begin{array}{r} \text { La } \\ \text { pppm } \end{array}$ | $\begin{gathered} \mathrm{Cr} \\ \text { ppinin } \end{gathered}$ | $\begin{gathered} \mathrm{Hg} \\ \boldsymbol{\%} \end{gathered}$ | $\begin{array}{r} 8 \mathbf{8 a} \\ \text { ppan } \\ \hline \end{array}$ | $\stackrel{1}{2}$ | $\begin{array}{r} \mathbf{B} \\ \text { ppin } \end{array}$ | $\begin{gathered} \text { A! } \\ X \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ | $\begin{aligned} & \mathrm{K} \\ & \mathrm{x} \end{aligned}$ |  | $\begin{aligned} & \mathbf{A} \mathbf{u}^{\boldsymbol{k}} \\ & \mathrm{pppb} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IL．5＋00 1＋00S | 7 | 14 | 10 | 65 | 㐫\％ | 5 | 4 | 458 | 6.95 | 12 | 5 | MD | 2 | 1 | \％ 8 | 3 | 2 | 63 | ． 08 | \％ 050 | 28 | 13 | .17 | 12 | 等98． | 8 | 2.54 | ． 03 | ． 04 | \％ |  |
| IL． $5+001+255$ | 6 | 14 | 7 | 55 | ＊ 3 ， | 5 | 4 | 275 | 4.84 | \％ | 5 | ND | 1 | 11 | $\stackrel{5}{5}$ | 3 | 2 | 45 | ． 12 | ， 052 | 37 | 15 | ． 26 | 10 | 28 | 8 | 3.02 | ． 05 | ． 05 | \％ |  |
| IL． $5+001+505$ | 6 | 16 | 11 | 59 | \％ | 5 | 5 | 442 | 6.21 | 8 | 5 | ND | 2 | 11 | ＊${ }^{5}$ | 2 |  | 62 | ． 07 | 058 | 28 | 17 | ． 19 | 8 | 318 | 8 | 2.57 | ． 03 | ． 04 | \％ | 2 |
| IL 5＋00 1＋75s | 8 | 15 | 7 | 65 | \％ | 5 | 8 | 1554 | 7.08 | \％ | 5 | NO | 2 | 11 | 行 | 2 | 2 | 67 | ． 06 | \％ 049 | 24 | 19 | ． 19 | 14 | \＄8． | 8 | 2.70 | ． 02 | ． 04 | 納 |  |
| IL 5＋00 $2+005$ | 10 | 18 | 14 | 59 |  | 5 | 2 | 281 | 6.36 | \％\％$\%$ | 5 | ND | 3 | 7 | 綡 | 3 | 4 | 80 | ． 06 | \％036 | 24 | 17 | .13 | 14 | \％ 60 | 9 | 1.50 | ． 03 | ． 06 | 令紬 |  |
| 11．5＋00 $2+25 s$ | 8 | 20 | 8 | 62 | 行 | 4 | 3 | 591 | 7.05 | 16 | 5 | ND | 3 | 6 | ＊9 | 4 | 2 | 56 | ． 05 | \％060 | 22 | 17 | ． 09 | 12 | 約2 | 10 | 3.39 | ． 04 | ． 04 | ， | 7 |
| IL 5＋00 2＋755 | 7 | 21 | 9 | 78 | \％ | 7 | 4 | 521 | 7.81 | 17 | 5 | MO | 5 | ， | 紬， | 4 | 2 | 57 | ． 05 | \％ 0 \％ | 28 | 21 | ． 19 | 12 | 法37 | 9 | 2.30 | ． 05 | ． 07 | \＆ | 2 |
| IL． $6+000+255$ | 11 | 11 | 10 | 58 | 好 | 4 | 3 | 279 | 8.33 | 8 | 5 | ND | 3 | 6 | 为\％ | 3 | 2 | 70 | ． 04 | \％ 058 | 19 | 17 | ． 04 | 10 | \％ | 7 | 2.23 | ． 03 | ． 05 | \＆ | 1 |
| IL $6+000+505$ | 6 | 14 | 4 | 66 | 就 | 5 | 7 | 674 | 5.43 | \％ | 5 | ND | 1 | 9 | ＊\％ | 4 | 2 | 62 | ． 09 | 05\％ | 16 | 14 | ． 16 | 12 | 年5 | 8 | 2.15 | ． 03 | ． 06 | \％ | 2 |
| IL $6+000+75 \mathrm{~s}$ | 27 | 14 | 10 | 80 | 行 | 2 | 2 | 746 | 5.88 |  | 7 | ND | 15 | 12 | 的 | 3 | 2 | 14 | ． 09 | 103\％ | 37 | 9 | ． 03 | 26 | \％ 8 | 7 | 3.95 | ． 10 | ． 08 | ¢ | 2 |
| IL． $6+001+005$ | 64 | 11 | 10 | 73 | \％ | 6 | 8 | 724 | 3.87 | 8 | 5 | ND | 1 | 59 | \％ | 3 | 2 | 94 | ． 34 | \％ 066 | 31 | 15 | ． 47 | 43 | 的88 | 7 | 1.77 | ． 03 | ． 05 | ¢ | 1 |
| IL $6+001+255$ | 9 | 12 | 13 | 64 | \％ 2 | 7 | 11 | 532 | 3.12 | \％ | 5 | no | 1 | 76 | \％ | 2 | 2 | 56 | ． 56 | 明6 | 10 | 9 | ． 83 | 40 | 令 4 | 6 | 1.46 | ． 12 | ． 08 | 浐 | 8 |
| IL 6＋00 1＋505 | 10 | 19 | 8 | 60 | 数 | 4 | 2 | 320 | 9.12 | 15 | 5 | ND | 5 | 19 | \％ | 5 | 2 | 101 | ． 08 | \％ 097 | 20 | 19 | ． 15 | 30 | \％s\％ | 7 | 2.27 | ． 01 | ．04 | 行 | 1 |
| IL $6+001+755$ | 10 | 27 | 15 | 66 | 䋛 | 4 | 3 | 369 | 9.13 | 18 | 5 | ND | 12 | 23 | 1，2\％ | 7 | 2 | 67 | ． 10 | \％ 188 | 24 | 17 | ． 27 | 28 | 新 |  | 3.19 | ． 02 | ． 04 | 行 | 1 |
| IL $6+002+005$ | 12 | 32 | 14 | 78 | 紬的。 | 6 | 5 | 436 | 9.57 | \％ 20 | 5 | ND | 22 | 13 |  | 3 | 2 | 46 | ． 07 | 做60 | 28 | 22 | ． 19 | 21 | 今部5 | 5 | 3.56 | ． 03 | ． 05 | 兗納 | 1 |
| IL． $6+002+255$ | 8 | 22 | 10 | 68 | \％ | 5 | 3 | 325 | 9.58 | 15 | 5 | ND | 4 | 12 | \＆o | 5 | 2 | 81 | ． 09 | \％06\％ | 23 | 23 | ． 10 | 15 |  | 6 | 2.96 | ． 02 | ． 04 | \％ | 5 |
| IL 6＋00 $2+505$ | 9 | 24 | 13 | 78 | \％ | 5 | 6 | 895 | 7.80 | 9 | 5 | ND | 5 | 14 | \％ | 2 | 2 | 84 | ． 08 | \％059 | 17 | 23 | ． 25 | 17 | \％为䅑 | 8 | 2.10 | ． 03 | ． 05 | 行 | 2 |
| IL 6＋00 2＋75s | 8 | 19 | 12 | 50 | \％ | 4 | 4 | 325 | 6.62 | 14 | 5 | ND | 2 | 11 | ， 3 | 3 | 2 | 85 | ． 07 | \％052 | 18 | 16 | ． 14 | 17 | \％\％ | 9 | 1.88 | ． 03 | ． 05 | ＊i | 2 |
| IL．7＋00 0＋25s | 6 | 22 | 10 | 65 | ， 2 | 8 | 4 | 255 | 6.53 | 14 | 5 | ND | 4 | 21 | ， 3 | 3 | 4 | 65 | ． 14 | \％ $04 \%$ | 19 | 32 | ． 45 | 31 | ＊ 33 | 8 | 3.74 | ． 03 | ． 03 | ＊＊ | 7 |
| IL 7＋000 $0+505$ | 5 | 21 | 16 | 54 | $\%$ | 6 | 5 | 353 | 4.82 | 11\％ | 5 | ND | 3 | 21 | \％$\%$ \％ | 2 | 2 | 57 | ． 14 | \％ 082 | 20 | 19 | ． 40 | 35 |  | 7 | 3.19 | ． 04 | ． 04 | 范 | 4 |
| IL． $7+000+755$ | 4 | 16 | 26 | 62 | 约 | 6 | 2 | 379 | 3.42 | 16 | 5 | MD | 2 | 40 | ＊ 2 | 2 | 2 | 42 | ． 18 | \％ 045 | 6 | 19 | ． 81 | 37 | ＊22 | 6 | 1.28 | ． 01 | ． 03 | \％ | 80 |
| IL 7＋00 1＋00s | 9 | 16 | 13 | 75 | 縣 | 4 | 6 | 1457 | 8.54 | 22 | 5 | no | 10 | 6 | \％ 8 | 3 | 2 | 49 | ． 05 | \％ 085 | 24 | 22 | ． 14 | 15 | 30． | 10 | 2.33 | ． 05 | ． 07 | \％ | 4 |
| IL 7＋00 1＋25s | 5 | 21 | 7 | 50 | \％ | 5 | 3 | 313 | 4.77 | 12 | 5 | no | 2 | 44 | \％ 2 | 4 | 2 | 48 | ． 21 | \％6\％ | 12 | 19 | ． 58 | 37 | 㐫 6 | 7 | 2.20 | ． 02 | ． 04 | 2 | 16 |
| IL． $7+001+505$ | 9 | 15 | 11 | 77 | 方 | 3 | 3 | 623 | 7.64 | 19． | 6 | ND | 15 | 7 | \％ 5 |  | 2 | 19 | ． 07 | \％ 038 | 28 | 15 | ． 09 | 12 |  | 9 | 3.47 | ． 06 | ． 06 | ＊s． | 3 |
| 11． $7+00$ 1＋75s | 7 | 14 | 12 | 71 | \％，\％ | 3 | 2 | 435 | 9.05 | \％ 19 | 6 | no | 6 | 5 | \％$\%$ | 3 | 2 | 44 | ． 05 | \％ 0 全 | 44 | 12 | ． 01 | 14 | 的里。 | 6 | 3.14 | ． 04 | ． 05 |  |  |
| IL 7＋00 2＋00S | 10 | 25 | 21 | 72 | \％s | 6 | 4 | 805 | 8.01 | 13 | 5 | ND | 5 | 14 | \％si | 4 | 3 | 74 | ． 08 | \％ 05 | 21 | 21 | ． 19 | 22 | \％$\% 3$ | 7 | 2.38 | ． 02 | ． 04 | 納 | 1 |
| 11． $7+002+255$ | 10 | 15 | 9 | 52 | 的多 | 4 | 2 | 223 | 9.94 | 23 | 5 | ND | 10 | 5 | \％ | 5 | 2 | 74 | ． 04 | \％ 83 | 20 | 16 | ． 01 | 18 | ＊站 | 7 | 1.85 | ． 05 | ${ }^{(7}$ | ＊玄 | 2 |
| IL． $8+000+255$ | 10 | 15 | 55 | 54 | \％$\%$ | 4 | 4 | 328 | 6.73 | 18 | 5 | ND | 1 | 21 | ＊$\%$ | 5 | 3 | 57 | ． 10 | 苓 036 | 22 | 21 | ． 27 | 26 | \％ | 8 | 2.11 | ． 01 | ． 03 | 晾 | 34 |
| IL．8＋0000 $0+505$ | 10 | 23 | 90 | 30 | \％ | 4 | 2 | 59 | 4.55 | 14 | 5 | ND | 1 | 14 | \％ | 2 | 2 | 44 | ． 08 | \％ 30 | 30 | 14 | ． 17 | 22 | 㖠 | 8 | 3.02 | ． 01 | ． 03 | ＊称 | 7 |
| IL 8＋00 0＋75S | 30 | 103 | 58 | 93 | $\%$ | 10 | 96 | 3149 | 14.93 | 43 | 5 | ND | 5 | 32 | 的 | 4 | 2 | 76 | ． 21 | \％3\％ | 8 | 22 | ． 44 | 47 | \％${ }^{\text {\％}}$ | 5 | 3.06 | ． 07 | ． 05 | $\psi_{8}$ | 110 |
| IL 8＋00 1＋25s | 7 | 31 | 2 | 81 | \＆ | 12 | 32 | 1720 | 3.45 | \％ | 5 | ND | 5 | 97 | 5 | 2 | 2 | 42 | ． 67 | \％10\％ | 8 | 14 | 1.07 | 116 | \％ 4 | 7 | 2.53 | ． 09 | ． 07 | ＊ | 8 |
| IL． $8+00$ 1＋505 | 18 | 49 | 2 | 126 | ＊ | 19 | 74 | 3692 | 6.17 | 15 | 5 | ND | 10 | 93 | ＜ | 4 | 2 | 53 | ． 72 | \％220 | 10 | 16 | 1.03 | 193 | 令22 | 9 | 4.20 | ． 14 | ． 07 | \％ | 9 |
| IL 8＋00 1＋75s | 10 | 88 | 12 | 145 | 约 | 12 | 65 | 4662 | 6.17 | 34 | 5 | ND | 4 | 19 | \％$\%$ \％ | 9 | 3 | 23 | ． 21 | \％106 | 12 | 15 | ． 34 | 90 | \％ 0 \％ | 9 | 10.01 | ． 04 | ． 01 | \％ | 6 |
| IL 8＋00 $2+005$ | 16 | 37 | 55 | 65 | ＊ | 7 | 19 | 1065 | 6.48 | 20 | 5 | ND | 3 | 36 | \％ | 4 | 2 | 49 | ． 19 | \％ 67 | 8 | 17 | ． 66 | 127 | \％8： | 6 | 3.24 | ． 01 | ． 03 | \％s | 48 |
| IL 8＋00 $2+25 \mathrm{~S}$ | 12 | 94 | 18 | 119 | $i_{i}$ | 7 | 11 | 657 | 4.73 | $6$ | 5 | ND | 3 | 68 | ${ }_{3}$ | 3 | 2 | 49 | ． 41 | \％24 | 9 | 13 | ． 86 | 66 |  | 10 | 1.37 | ． 03 | ． 04 |  | 57 |
| 1L．8＋00 2＋50s | 22 | 105 | 20 | 90 | ＊＊ | 6 | 12 | 737 | 5.40 | 13 | 5 | ND | 2 | 61 | \％ | 2 | 2 | 42 | ． 41 | \＄134 | 14 | 12 | ． 78 | 59 | \％ 10 | 10 | 1.78 | ． 01 | ． 04 | ， | 93 |
| STANDARD C／AU－S | 18 | 58 | 37 | 130 | \％ 6 | 70 | 321 | 1047 | 3.97 | 39 | 20 | 7 | 39 | 52 | $18 \leqslant 3$ | 16 | 20 | 56 | ． 52 | \％ 088 | 36 | 57 | ． 90 | 182 | \％09 | 38 | 1.89 | ． 06 | ． 14 | 令 | 46 |

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| SAMPLE＊＊ | $\begin{aligned} & \text { Mo } \\ & \text { pppa } \end{aligned}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppin} \\ \hline \end{array}$ | $\begin{array}{r} \mathbf{P b} \\ \mathbf{P p} \\ \hline \end{array}$ | $\begin{array}{r} 2 n \\ \mathrm{ppm} \end{array}$ |  | $\underset{\substack{\mathrm{Mi} \\ \hline \boldsymbol{p} \\ \hline}}{ }$ | $\begin{array}{r} \text { Co } \\ \text { ppa } \end{array}$ | $\begin{array}{r} \mathrm{Mn} \\ \mathrm{ppm} \end{array}$ | $\begin{aligned} & \mathrm{Fe} \\ & \mathrm{n} \\ & \mathrm{X} \\ & \hline \end{aligned}$ | prpm | $\begin{array}{r} \text { U } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p m} \end{array}$ |  | $\begin{array}{r} \text { Sb } \\ \text { ppin } \end{array}$ | $\begin{array}{r} 8 i \\ \text { ppm } \end{array}$ | $\begin{array}{r} v \\ \text { ppm } \end{array}$ | $\begin{aligned} & \mathrm{Ca} \\ & \mathbf{x} \end{aligned}$ | $\stackrel{\ominus}{\ell}$ | $\begin{array}{r} \text { La } \\ \text { ppom } \end{array}$ | $\begin{array}{r} \text { Cr } \\ \text { ppan } \end{array}$ | $\begin{gathered} \mathrm{Mg} \\ \mathbf{z} \end{gathered}$ | $\begin{array}{r} \text { Ba } \\ \text { ppm } \end{array}$ | 龄 | $\begin{array}{rr} 8 & A 1 \\ \operatorname{ppa} & \chi \end{array}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ |  |  | $\begin{aligned} & \text { Au* } \\ & \text { ppb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IL．8＋00 2＋75S | 15 | 108 | 20 | 94 | \％ 3 3 | 7 | 20 | 867 | 4.80 | \％ 13 | 5 | ND | 1 | 53 | ＊ 2 | 3 | 2 | 39 | ． 36 | ＊116 | 11 | 12 | ． 79 | 49 | \％ | 101.61 | ． 02 | ． 04 | \％ | 168 |
| IL． $8+003+005$ | 9 | 14 | 18 | 32 | \％${ }^{2}$ | 3 | 3 | 188 | 2.24 | 6 | 5 | ND | 1 | 37 | \％ 2 | 2 | 2 | 52 | ． 16 | －034 | 5 | 9 | ． 39 | 22 | 雬 | 51.31 | ． 01 | ． 02 | ＊ | 39 |
| IL 9＋00 0＋25s | 4 | 21 | 42 | 55 | 疎 4 | 9 | 4 | 320 | 5.34 | 14 | 5 | ND | 3 | 27 | \％ 2 | 4 | 2 | 80 | ． 19 | \％092 | 8 | 22 | ． 76 | 74 | 的0 | 112.08 | ． 02 | ． 08 | 率2 | 47 |
| IL 9＋00000505 | 8 | 25 | 58 | 153 | 的 | 25 | 5 | 1479 | 5.58 | 28． | 5 | ND | 5 | 61 | 率 6 | 3 | 2 | 65 | ． 23 | \％106 | 24 | 61 | 1.14 | 529 | \＄26 | 102.83 | ． 02 | ． 09 | 組 | 40 |
| IL 9＋000 $0+755$ | 7 | 24 | 14 | 44 | \％$\%$ \％ | 5 | 3 | 180 | 6.87 | 原 | 5 | ND | 2 | 15 | i 2 | 3 | 2 | 69 | ． 09 | \％062 | 24 | 23 | ． 18 | 50 | 泫 27 | 92.71 | ． 02 | ． 04 | 雱 | 26 |
| IL．9＋00 1＋00s | 1 | 12 | 9 | 41 | 2 | 5 | 3 | 76 | ． 6.69 | 3 | 6 | ND | 4 | 16 | 洨9 | 2 | 5 | 56 | ． 12 | 350 | 15 | 18 | ． 30 | 27 | 䫆9 | 31.94 | ． 05 | ． 03 | － | 2 |
| IL． $9+001+255$ | 5 | 32 | 15 | 61 | 交 | 9 | 5 | 297 | 5.01 | 嘌覀 | 5 | NO | 1 | 38 | 洨法2 | 3 | 2 | 75 | ． 20 | \％08 | 8 | 17 | ． 64 | 70 | 的配 | 101.79 | ． 04 | ． 06 | 瑯納 | 15 |
| IL 9＋00 1＋50S | 5 | 18 | 20 | 50 | 较 | 6 | 3 | 349 | 3.09 | \％ | 5 | MD | 1 | 46 |  | 2 | 2 | 49 | ． 25 | \％ 4 | 5 | 17 | ． 72 | 78 | 数 | 71.27 | ． 03 | ． 06 | ， | 44 |
| IL 9＋00 1＋75s | 4 | 34 | 23 | 56 | ＊ | 10 | 6 | 353 | 4.09 | － | 5 | MD | 1 | 55 | \％ | 2 | 2 | 61 | ． 36 | \％ 07 | 9 | 19 | ． 87 | 101 | 沴20 | 81.68 | ． 10 | ． 08 | ＊約 | 37 |
| IL 9＋00 2＋00S | 5 | 14 | 6 | 42 絧 | 约 | 5 | 2 | 153 | 3.83 | 17 | 5 | ND | 6 | 6 | 洤 | 6 | 2 | 49 | ． 07 | \％ 062 | 17 | 19 | ． 07 | 15 | $\text { 㢳 } 2$ | 93.52 | ． 05 | ． 06 |  | 3 |
| II．9＋00 $2+255$ | 8 | 12 | 8 | 52 | 号 | 4 | 2 | 193 | 9.43 | 10 | 5 | ND | 5 | 7 |  | 2 | 2 | 47 | ． 05 | \％052 | 23 | 18 | ． 02 | 17 | 泫30 | 83.22 | ． 02 | ． 03 | \％isk | 1 |
| IL．9＋00 $2+505$ | 6 | 17 | 7 | 50 |  | 8 | 6 | 354 | 6.68 | \％ | 5 | ND | 2 | 26 | 待 | 4 | 2 | 95 | ． 25 | \％06\％ | 9 | 16 | ． 51 | 26 | 約 5 | 121.85 | ． 09 | ． 06 | ＊ | 3 |
| IL 9＋00 $2+755$ | 5 | 17 | 7 | 49 | 的4 | 8 | 6 | 363 | 5.43 | 8． | 5 | ND | 1 | 28 | \％ 3 | 2 | 2 | 84 | ． 25 | \％06\％ | 12 | 17 | ． 43 | 22 | 50 | 122.17 | ． 09 | ． 06 | \％sisk | 1 |
| IL 9＋00 3＋005 | 1 | 22 | 2 | 71 | \％納 | 18 | 16 | 412 | 3.67 | ？ | 5 | ND | 1 | 120 | 有 | 2 | 2 | 71 | 1.20 | \％080 | 70 | 16 | 4.30 | 63 | 积6 | 103.05 | ． 46 | ． 16 | 組 | 1 |
| IL 10＋00 0＋25s | 6 | 31 | 17 | 69 | 动， | 7 | 4 | 338 | 3.66 | \％ | 5 | ND | 2 | 59 | 考 | 2 | 2 | 48 | ． 23 | \％ 338 | 15 | 13 | ． 78 | 256 | 全22 | 101.71 | ． 02 | ． 07 |  | 64 |
| IL 10＋00 0＋50s | 4 | 35 | 10 | 47 | ， | 6 | 3 | 166 | 5.10 | \％ | 5 | ND | 3 | 21 | K | 4 | 2 | 92 | ． 17 | \％068 | 12 | 20 | ． 38 | 49 | \％ 4. | 122.89 | ． 03 | ． 04 | ＊s＊ | 15 |
| IL 10＋00 0＋75s | 9 | 23 | 33 | 66 | 晾 | 7 | 5 | 897 | 8.33 | 2\％ | 5 | NO | 4 | 27 | 者8 | 3 | 2 | 71 | ． 12 | \％76 | 15 | 27 | ． 45 | 36 | 夜 | 102.05 | ． 03 | ． 06 | 納納 | 11 |
| IL 10＋00 1＋00s | 5 | 51 | 34 | 80 | \％ 6 | 10 | 6 | 498 | 4.46 | 14 | 5 | ND | 1 | 42 | \％ | 3 | 2 | 74 | ． 18 | \％08\％ | 15 | 26 | ． 75 | 88 | 食6 | 112.20 | ． 03 | ． 07 |  | 90 |
| IL 10＋00 1＋25s | 7 | 40 | 13 | 61 \％ | \＃ | 5 | 6 | 528 | 7.90 | 翰 | 5 | ND | 4 | 13 | 率\％ | 4 | 3 | 41 | ． 08 | \％058 | 27 | 17 | ． 19 | 23 | 成4 | 122.95 | ． 03 | ． 04 | ＊納 | 15 |
| IL 10＋00 1＋50S | 6 | 42 | 40 | 69 | \％ 5 | 5 | 1 | 116 | 5.01 | \％2． | 5 | No | 4 | 16 | \％ | 3 | 2 | 64 | ． 07 | \％064 | 24 | 30 | .16 | 23 | 教24 | 113.63 | ． 04 | ． 04 | \％＊＊ | 20 |
| IL 10＋00 1＋75S | 6 | 17 | 7 | 50 | 年4 | 3 | 2 | 133 | 6.57 | \％ 18 | 5 | ND | 3 | 6 | \％ 5 | 6 | 2 | 49 | ． 06 | ． 084 | 21 | 20 | ． 06 | 8 | 傢 0 | 94.88 | ． 04 | ． 04 |  | 5 |
| IL 10＋00 2＋25s | 1 | 12 | 3 | 59 | 娄 | 11 | 10 | 249 | 3.53 3 | 2 | 5 | ND | 1 | 65 | \％ | 2 |  | 93 | ． 64 | 07\％ | 3 | 15 | ． 79 | 56 | 納为 | 81.26 | ． 18 | ． 08 | 碞 | 3 |
| IL 10＋00 $2+505$ | 2 | 8 | 15 | 48 | \％ | 8 | 7 | 269 | 2.42 | ${ }^{6}$ | 5 | ND | 1 | 64 | 就 | 2 | 2 | 64 | ． 48 | \％074 | 9 | 16 | ． 78 | 64 | 沙＊ | 61.31 | ． 14 | ． 07 | 的 | 14 |
| IL 10＋00 3＋00s | 2 | 19 | 7 | 47 | \％\％ | 9 | 7 | 189 | 3.63 | 年， | 5 | ND | 1 | 38 | 繧 | 3 | 2 | 112 | ． 37 | 088， | 6 | 19 | .61 | 33 | 絲 | 81.70 | ． 13 | ． 08 |  | 65 |
| IL 11＋00 0＋25s | 5 | 35 | 25 | 86 | 泼晾 | 13 | 10 |  | 4.56 | ＊ 8 － | 5 | ND | 4 | 92 | 水 | 2 | 2 | 73 | ． 65 | 10\％ | 14 | 21 | 1.11 | 143 | 沙为颔 | 92.43 | ． 22 | ． 14 |  | 65 |
| IL 11＋00 0＋505 | 5 | 35 | 19 | 108 | \％ 2 | 12 |  | 536 | 5.82 | 2 | 5 | ND | 11 | 29 | \％ 2 |  | 2 | 64 | ． 20 | \％0\％ | 24 | 21 | ． 64 | 87 |  | 123.45 | ． 11 | ． 12 |  | 31 |
| IL 11＋00 0＋75s | 5 | 14 | 23 | 40 | \％ 3 | 5 | 1 | 116 | 4.18 | ¢ | 5 | ND | 1 | 23 | \％ | 2 | 2 | 90 | ． 09 | \％ 038 | 21 | 14 | ． 12 | 27 | \％ 3 | 81.33 | ． 01 | ． 04 |  | 14 |
| IL．11＋00 1＋00s | 2 | 43 | 36 | 53 | \％ | 6 | 4 | 216 | 6.59 3 | 28 | 5 | ND | 1 | 31 | 颠 | 4 | 2 | 131 | ． 11 | \％ 68 | 2 | 20 | ． 38 | 57 | 沙號 | 91.03 | ． 01 | ． 03 | 相 | 19 |
| IL 11＋00 1＋25s | 1 | 16 | 4 | 115 | 的 6 | 12 | 12 | 1264 | 2.52 ： | 6 | 5 | ND | 1 | 73 | 的 | 2 | 2 | 44 | ． 86 | \％\％\％ |  | 11 | ． 77 | 80 | \％${ }^{2}$ | 71.17 | ． 19 | ． 17 |  | 3 |
| IL 11＋00 1＋50S | 6 | 36 | 58 | 85 | \％ | 34 | 2 | 671 | 3.49 |  | 5 | ND | 2 | 133 | \＄ | 2 | 2 | 60 | ． 33 | \％ 078 | 8 | 60 | 1.17 | 339 | \％ 10 | 61.76 | ． 01 | ． 11 |  | 250 |
| IL 11＋00 1＋755 | 2 | 68 | 298 | 104 | 就 | 11 |  |  | 4.88 | 40 | 5 | ND |  | 241 | 縞 | 3 | 2 | 119 | ． 55 | \％ 20 | 17 | 45 | 1.07 | 145 | 約 | 92.38 | ． 04 | ． 05 | 童 | 139 |
| IL．11＋00 2＋00S | 6 | 16 | 35 | 45 |  | 7 | 3 | 277 | 4.91 | 28 | 5 | ND | 2 | 84 | 紷 | 3 | 2 | 147 | ． 35 | 洘 | 7 | 22 | ． 52 | 155 | 洮 | 81.34 | ． 03 | ． 05 | 2 | 73 |
| IL 11＋00 3＋00N | 6 | 35 | 14 | 78 | 效2 | 6 | 6 |  | 4.07 ： | 9 | 5 | ND | 4 | 83 | \％2 | 3 | 2 | 43 | ． 32 | \％85 | 20 | 11 | ． 90 | 274 |  | 91.80 | ． 03 | ． 11 | 洨 | 30 |
| IL 11＋00 $2+75 \mathrm{~N}$ | 8 | 27 | 7 | 122 | \％ | 9 | 9 | 959 | 6.10 | ＊1． | 5 | ND | 12 | 33 | 㐫 ， | 4 | 2 | 40 | ． 27 | \％ 0 \％ 6 | 26 | 12 | ． 57 | 57 | 22 | 103.03 | ． 14 | ． 11 | 納 |  |
| IL 11＋00 $2+50 \mathrm{~N}$ | 9 | 34 | 7 | 74 | $\stackrel{\psi}{\psi}$ | 11 | 6 | 351 | 7.72 | $\$$ | 5 | ND | 5 | 27 | $\%$ | 5 | 3 | 87 | ． 16 | \％0\％ | 20 | 22 | ． 62 | 39 | 家 | 102.74 | ． 03 | ． 04 |  | 16 |
| IL 11＋00 $2+25 \mathrm{~N}$ | 12 | 39 | 13 | 72 | ¢！ | 7 | 8 | 583 | 5.16 | \％ | 5 | ND | 1 | 40 | \％ | 4 | 2 | 59 | ． 18 | \％08 | 14 | 17 | ． 67 | 55 | \％ 2 \％ | 102.54 | ． 03 | ． 05 | 数 | 18 |
| STAMDARD C／AU－S | 18 | 57 | 38 | 130 | \％$\%$ | 71 | 32 | 1048 | 3.97 | 39． | 21 | 7 | 40 | 52 | 18， | 14 | 22 | 55 | ． 52 | \％089 | 37 | 56 | ． 89 | 187 | 洨0\％ | 391.89 | ． 06 | ． 14 |  | 49 |

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| SAMPLE\＃ | $\begin{aligned} & \text { Mo } \\ & \text { pppm } \end{aligned}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Pb} \\ \mathrm{Pp} \text { 侣 } \end{gathered}$ | $\begin{array}{r} 2 n \\ p p m \end{array}$ |  | $\begin{gathered} \mathbf{M i} \\ \mathbf{p p r i n} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { ppim } \end{array}$ | $\begin{gathered} \text { Mn } \\ \text { ppan } \end{gathered}$ | $\begin{gathered} \mathrm{Fe} \\ \mathrm{y} \\ \hline \end{gathered}$ |  | $\begin{array}{r} \mathbf{U} \\ \text { ppin } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{pppin} \end{array}$ | $\begin{gathered} \text { Th } \\ \text { ppim } \end{gathered}$ | $\begin{array}{r} \mathbf{S r} \\ \text { pppm } \end{array}$ |  | $\begin{array}{r} \text { Sb } \\ \text { ppiu } \end{array}$ | $\begin{array}{r} \text { Bi } \\ \text { ppin } \end{array}$ | $\begin{array}{r} v \\ p p m \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{\%} \end{gathered}$ |  | $\begin{array}{r} \text { La } \\ \text { pppim } \end{array}$ | $\begin{array}{r} \mathrm{Cr} \\ \mathrm{ppm} \\ \hline \end{array}$ | $\begin{gathered} \mathrm{Mg} \\ \boldsymbol{Z} \end{gathered}$ | $\begin{gathered} \mathrm{Ba} \\ \text { ppm } \\ \hline \end{gathered}$ |  | $\begin{array}{r} \mathbf{B} \\ \text { ppman } \end{array}$ | $\begin{aligned} & \text { A! } \\ & \mathbf{Z} \end{aligned}$ | $\begin{gathered} \mathrm{Ka} \\ \mathbf{Z} \end{gathered}$ | $\begin{aligned} & K \\ & \chi \end{aligned}$ |  | $\begin{aligned} & \text { Au* } \\ & \text { Ppb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| IL 11＋00 $2+00 \mathrm{~N}$ | 12 | 79 | 14 | 105 | ＋ | 10 | 11 | 579 | 5.84 | \％ | 5 | ND | 5 | 41 | \％ | 2 | 2 | 66 | ． 24 | \＄106 | 15 | 17 | ． 79 | 64 | \％ 30 |  | 3.27 | ． 04 | ． 05 | 荥 | 20 |
| IL 11＋00 1＋75N | 24 | 218 | 18 | 169 | 等 | 21 | 56 | 2242 | 6.57 | 13 | 6 | ND | 8 | 74 | 4．9 | 3 | 2 | 59 | ． 55 | 212 | 24 | 19 | ． 96 | 163 | \％22 |  | 2.49 | ． 09 | ． 10 | 納令 | 35 |
| IL $11+001+50 \mathrm{~N}$ | 15 | 38 | 34 | 72 | \％ | 6 | 6 | 447 | 4.10 | 5 | 6 | ND | 3 | 95 | 洨 2 | 3 | 2 | 50 | ． 30 | \％4x | 11 | 12 | ． 95 | 549 | \％9 |  | 1.70 | ． 02 | ． 16 | 沙絡 | 50 |
| IL．11＋00 1＋25N | 1 | 26 | 8 | 75 | 就 | 24 | 24 | 706 | 5.59 | 7 | 7 | ND | 3 | 151 | 安， | 3 | 2 | 106 | 1.62 | \％7\％ | 6 | 23 | 1.86 | 90 | 离5 |  | 2.17 | ． 71 | ． 27 | 橀約 | 10 |
| IL．11＋00 0＋75M | 5 | 25 | 15 | 93 | ＊＊ | 8 | 22 | 534 | 5.50 | \％ 13. | 5 | ND | 3 | 99 | 納 2 | 3 | 2 | 47 | ． 48 | 109 | 6 | 8 | ． 71 | 1480 | 郎 3 |  | 1.57 | ． 07 | ． 07 |  | 31 |
| IL 11＋00 0＋50N | 8 | 62 | 20 | 95 | 积 | 9 | 11 | 534 | 4.71 | §納 4 | 5 | ND | 4 | 69 | 行 | 2 | 2 | 48 | ． 32 | 3 38 | 13 | 12 | ． 82 | 177 | \％${ }^{\text {\％}}$ |  | 1.71 | ． 06 | ． 09 | 多 | 25 |
| IL 11＋00 0＋25N | 6 | 66 | 22 | 75 | \％ | 10 | 16 | 603 | 4．48 | \％ | 7 | MD | 4 | 80 | \％ | 2 | 3 | 55 | ． 48 | 喲放 | 19 | 16 | ． 97 | 286 | 2\％ |  | 2.23 | ． 13 | ． 13 | ＊ | 44 |
| IL 12＋00 0＋25s | 7 | 56 | 24 | 81 | \％ | 7 | 5 | 502 | 3.58 | \％ | 5 | ND | 4 | 63 | 4 | 2 | 2 | 48 | ． 25 | \％ 05 | 25 | 19 | 1.04 | 392 | 洨娄采 |  | 2.04 | ． 01 | ． 16 | \％埧納 | 59 |
| IL．12＋00 0＋50s | 5 | 44 | 19 | 68 | 納 S | 9 | 5 | 409 | 3.77 | \％ | 5 | NO | 3 | 57 | 紋 2 | 2 | 2 | 57 | ． 21 | \％19\％ | 13 | 20 | ． 88 | 163 | 洛26\％ |  | 1.88 | ． 02 | ． 08 |  | 24 |
| IL 12＋00 0＋75s | 5 | 44 | 28 | 69 |  | 8 | 5 | 413 | 3.44 | 12 | 5 | NO | 4 | 80 |  | 3 | 2 | 60 | ． 26 | $4192$ | 10 | 21 | ． 96 | 168 |  |  | 1.61 | ． 04 | ． 08 |  | 180 |
| IL．12＋00 1＋00s | 6 | 47 | 36 | 73 | \％ | 9 | 3 | 455 | 3.76 | 12 | 5 | ND | 3 | 105 | 納\％ | 2 | 2 | 62 | ． 24 | \％ 288 | 13 | 23 | ． 94 | 274 | 沙数 |  | 1.73 | ． 02 | ． 09 | \％納 | 190 |
| IL 12＋00 1＋25s | 7 | 48 | 26 | 64 | 教 | 7 | 4 | 454 | 4.98 | 15 | 7 | ND | 5 | 60 | 尔多 | 2 | 2 | 51 | ． 22 | 等0\％ | 18 | 19 | ． 75 | 163 | 洨 1 |  | 1.99 | ． 01 | ． 08 | 絃 | 160 |
| IL 12＋00 1＋50s | 5 | 41 | 28 | 72 | \％2 | 9 | 6 | 417 | 3.76 | 8 | 5 | NO | 2 | 91 | \％ 2 | 2 | 2 | 63 | ． 40 | 行0\％ | 12 | 19 | ． 94 | 181 |  |  | 1.79 | ． 11 | ． 10 | 樃納 | 87 |
| IL 12＋00 1＋75s | 4 | 27 | 20 | 79 | 碞 | 7 | 4 | 410 | 2.96 | \％ | 5 | ND | 2 | 84 | \％ 22 | 2 | 2 | 58 | ． 43 | \％07\％ | 6 | 21 | 1.08 | 95 | 年\％ | 2 | 1.54 | ． 11 | ． 11 | 絡々 | 47 |
| IL 12＋00 2＋00s | 5 | 23 | 26 | 57 | 納絞 | 6 | 2 | 268 | 2.83 | \％ | 6 | ND | 2 | 63 | 紬 5 | 2 | 2 | 54 | ． 22 | ＜089 | 14 | 20 | ． 74 | 107 | 脑絡 |  | 1.98 | ． 02 | ． 06 | 洨洨絃 | 101 |
| IL 12＋00 2＋25s | 4 | 25 | 29 | 56 | ＜2 | 8 | 2 | 277 | 2.23 | 6 | 5 | ND | 1 | 66 | ，2 | 2 | 2 | 46 | ． 19 | \％09 | 13 | 22 | ． 74 | 100 | 爯 |  | 1.53 | ． 01 | ． 05 |  | 210 |
| IL 12＋00 2＋50s | 5 | 29 | 28 | 84 | 㨥 | 15 | 2 | 391 | 3.66 | 114 | 6 | ND | 2 | 56 | 的 ${ }^{\text {s }}$ | 2 | 2 | 51 | ． 22 | \％09\％ | 13 | 39 | ． 81 | 122 | 沙为 |  | 2.24 | ． 02 | ． 05 | 数 | 220 |
| IL 12＋00 2＋75s | 5 | 27 | 30 | 77 | \％ 3 | 9 | 3 | 343 | 3.67 | 安 | 5 | ND | 1 | 66 | ＊， 3 | 2 | 2 | 53 | ． 23 | 093 | 12 | 21 | ． 78 | 134 | 納 1 |  | 1.56 | ． 02 | ． 06 | 喲 | 96 |
| IL 12＋00 3＋00N | 9 | 98 | 12 | 98 | 水 | 17 | 20 | 876 | 6.15 | 5 | 5 | ND | 4 | 88 | \％ 0 | 2 | 2 | 90 | ． 79 | \％ 05 | 9 | 18 | 1.27 | 66 | 交8 |  | 2.29 | ． 29 | ． 13 | \％ | 25 |
| IL 12＋00 $2+50 \mathrm{~N}$ | 8 | 77 | 18 | 97 | 納 | 17 | 19 | 719 | 5.86 |  | 5 | ND | 6 | 88 | \％ision | 2 | 2 | 84 | ． 71 | $838$ | 11 | 20 | 1.17 | 71 | 絃縭 |  | 2.43 | ． 24 | ． 14 |  | 18 |
| IL 12＋00 $2+25 \mathrm{~N}$ | 9 | 96 | 13 | 117 | \＆ | 16 | 18 | 865 | 6.06 | 8 | 6 | MD | 8 | 61 | 倆 | 2 | 2 | 81 | ． 35 | \％ 72 | 16 | 21 | ． 96 | 116 | 紪如 |  | 2.92 | ． 07 | ． 10 |  | 22 |
| IL 12＋00 2＋00N | 12 | 130 | 19 | 122 | ， | 11 | 21 | 1183 | 6.48 | 9 | 5 | ND | 9 | 71 | 紬 | 2 | 2 | 65 | ． 26 |  | 12 | 15 | ． 95 | 229 | 多\％ |  | 1.86 | ． 04 | ． 09 |  | 20 |
| IL 12＋00 1＋25N | 7 | 40 | 18 | 66 | \％ 2 | 8 | 7 | 344 | 5.53 | 17 | 5 | ND | 3 | 43 | \％ | 2 | 2 | 58 | ． 22 | ＊ 87 | 11 | 15 | ． 64 | 76 |  |  | 2.07 | ． 03 | ． 07 | ＊s＊ | 33 |
| IL 12＋00 1＋00N | 3 | 25 | 19 | 61 | ， | 8 | 7 | 192 | 5.45 | 18 | 5 | ND | 1 | 42 | 給 | 3 | 2 | 72 | ． 33 | \％ $0 \%$ | 5 | 13 | ． 48 | 34 |  |  | 1.94 | ． 06 | ． 05 | 納䊽 | 34 |
| IL 12＋00 0＋75N | 2 | 13 | 8 | 45 |  | 5 | 5 | 131 | 2.47 |  | 5 | ND | 1 | 36 |  | 2 | 2 | 61 | ． 26 | \％ 068 | 3 | 10 | ． 35 | 52 |  | 2 | ． 90 | ． 05 | ． 05 | 苑 | 17 |
| STAMDARD C／AU－S | 19 | 60 | 38 | 131 | 6．7\％ | 73 | 31 | 1048 | 3.97 | 40 | 15 | 7 | 39 | 52 | 18．6 | 15 | 21 | 61 | ． 52 | 091 | 39 | 59 | ． 90 | 183 | 㿽埌 | 40 | 1.89 | ． 06 | ． 14 | 紋安交 | 45 |

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| SAMPLE\＃ | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Cu} \\ \mathrm{Pppm} \end{gathered}$ | $\begin{array}{r} \text { Pb } \\ \text { Ppm } \end{array}$ | $\underset{\text { Ppon }}{2 n}$ | $\begin{aligned} & \text { 品 } \\ & \text { ppr } \end{aligned}$ | $\underset{\mathrm{pppm}}{\mathrm{Mi}}$ | $\begin{array}{r} \text { Co } \\ \text { ppp } \end{array}$ | $\begin{gathered} \mathrm{Mn} \\ \mathrm{ppm} \end{gathered}$ | $\begin{gathered} \mathrm{Fe} \\ \boldsymbol{Z} \end{gathered}$ | As pprit | $\begin{array}{r} \mathrm{U} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppma} \end{array}$ | $\begin{gathered} \text { Th } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p m} \end{array}$ |  | $\begin{array}{r} \text { Sb } \\ \text { Pppm } \end{array}$ | $\begin{array}{r} 8 i \\ \text { ppm } \end{array}$ | $\begin{array}{r} V \\ p p m \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{x} \end{gathered}$ | $8$ | $\begin{aligned} & \text { Le } \\ & \text { ppen } \end{aligned}$ | $\begin{gathered} \text { Cr } \\ \text { ppma } \end{gathered}$ | $\begin{gathered} \mathbf{M g} \\ \boldsymbol{x} \end{gathered}$ | $\begin{array}{r} \text { Ba } \\ \text { ppan } \end{array}$ |  | $\begin{array}{r} \mathbf{B} \\ \text { ppn } \end{array}$ | $\begin{gathered} \mathrm{Al} \\ \mathbf{x} \end{gathered}$ | $\begin{gathered} \mathrm{Ma} \\ \boldsymbol{z} \end{gathered}$ | $\begin{aligned} & \boldsymbol{K}_{\boldsymbol{\chi}} \end{aligned}$ |  | $A u^{*}$ ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL－90－6－39 | 7 | 266 | 21 | 83 | 1.6 | 5 | 10 | 126 | 4.30 | 14. | 5 | ND | 3 | 24 | 2 | 2 | 2 | 10 | ． 14 | Or\％ | 5 | 3 | ． 18 | 45 | 0\％ | 3 | ． 68 | ． 01 | ． 25 | §納 | 630 |
| PEL－90－5－40 | 1 | 56 | 12 | a | 3 |  | 1 | 2 | 9.26 | §\％ | 5 | ND | 1 | 32 | S | 2 | 2 | 2 | ． 01 | \＄02， | 2 | 3 | ． 01 | 349 | 景賋 | 2 | ． 08 | ． 01 | ． 01 | ， | ${ }^{1}$ |
| PEL－90－5－41 | 1 | 11 | 20 | 50 | 4 | 3 | 4 | 442 | 3.76 | 16 | 5 | MD | 2 | 84 | \％ | 2 | 2 | 12 | ． 07 | 24\％ | 5 | 13 | 1.01 | 58 | \％ | 2 | 1.12 | ． 04 | ． 22 | ， | 2 |
| PEL－90－5－42 | 2 | 104 | 45 | 42 | 140 | 1 | 1 | 179 | 5.10 | 16 | 5 | no | 2 | 448 | 2． | 2 | 2 | 36 | ． 06 | \％ 22 | 20 | 10 | ． 29 | 249 | 先 | 2 | 1.01 | ． 01 | ． 32 |  | 1 |
| PEL－90－5－43 | 3 | 35 | 53 | 46 | \％ | 4 | 2 | 192 | 1.74 | 33 | 5 | No | 1 | 141 | ${ }^{2}$ | 2 | 2 | 25 | ． 11 | \％103 | 2 | 4 | ． 16 | 221 | 䜌 | 3 | 1.08 | ． 01 | ． 25 | 2 | 3 |
| PEL－90－5－44 | 4 | 64 | 23 | 99 | ＋ | 7 | 13 | 1021 | 4.86 | \％\％ | 5 | MO | 2 | 49 | \％ | 2 | 2 | 103 | ． 75 | \％182 | 4 |  | 2.56 | 67 | 交枵 |  | 2.15 | ． 04 | ． 14 |  | 1 |
| PEL－90－5－45 | 1 | 21 | 7 | 35 | \％ | 5 | 5 | 557 | 2.51 | 1 | 5 | no | 1 | 88 | \％ | 2 | 2 | 67 | ． 95 | 152 | 4 |  | 1.34 | 53 | 娄 |  | 1.33 | ． 12 | ． 09 | ！ | 2 |
| PEL－90－5－46 | 2 | 154 | 21 | 71 | S | 5 | 5 | 253 | 1.89 | §2 | 5 | N0 | 4 | 35 | \％ | 2 | 2 | 29 | ． 55 | \％0\％ | 5 | 4 | ． 55 | 41 | \％ | 3 | ． 90 | ． 13 | ． 11 | ， | 1 |
| PEL－90－5－47 | 1 | 36 | 26 | 104 | 䘨 | 3 | 1 | 1095 | 7.46 | 13 | 5 | no | 1 | 13 | \％ | 2 | 2 | 120 | ． 20 | 123 | 2 |  | 2.70 | 120 | \％ |  | 2.47 | ． 02 | ． 19 |  | 1 |
| PEL－90－5－48 | 6 | 27 | 25 | 89 | 令为 | 6 | 36 | 800 | 9.88 | \％ | 5 | No | 3 | 31 | \％ | 2 | 2 | 39 | 1.41 | 枟 | 5 |  | 1.35 | 73 | 9 ${ }^{\text {曷 }}$ | 2 | 1.87 | ． 05 | ． 34 | ， | 5 |
| PEL－90－5－49 | 1 | 36 | 12 | 58 | ＊ | 59 |  | 12 | 20 | §\％ | 5 | MD | 1 | 282 | \％ | 2 | 2 |  | 2.47 |  | 6 | 120 | ． 66 | 213 | 品碞 |  | 1.69 | ． 01 | ． 25 |  |  |
| PEL－90－5－50 | 2 | 361 | 31 | 94 | 2.6 | 25 | 27 | 1561 | 7.54 | 186 | 5 | no | 2 | 73 | \％ | 2 | 3 | 54 | 1.25 |  | 11 |  | 1.64 | 52 | 帾 |  | 1.97 | ． 01 | ． 13 | \＄ | 1 |
| PEL－90－5－51 | 1 | 127 | 647 | 175 | \＄\％$\%$ | 9 |  | 1175 | 7.91 | 285 | 5 | NO | 2 | 138 | 9． | 2 | 5 | 104 | ． 19 | 190 | 18 | 66 | 1.79 | 160 | （1） |  | 2.07 | ． 01 | ． 13 |  | 280 |
| PEL－90－5－52 | 3 | 63 | 321 | 56 | 13．7 | 10 | 2 | 247 | 3.37 | 248 | 5 | ND | 1 | 116 | ， | 6 | 2 | 38 | ． 45 | \％\％ | 6 | 26 | ． 12 | 35 | \％2） |  | ． 49 | ． 01 | ． 02 | ， | 13 |
| PEL－90－5－53 | 19 | 49 | 332 | 64 | \＄＊ | 13 | 11 | 317 | 5.52 | 203 | 5 | NO | 1 | 94 | 2 | 4 | 2 | 25 | ． 40 | \％04\％ | 3 | 36 | ． 27 | 27 | 的 | 2 | ． 58 | ． 01 | ． 09 | \％ | 151 |
| PEL－90－5－54 | 3 | 82 | 95 | 63 | 17\％ | 8 | － | 654 | 6.47 | 4． | 5 | ND | 1 | 49 | \％ | 2 | 3 | 23 | ． 22 | \％ 0,0 | 2 | 12 | ． 54 | 20 |  | 2 | ． 69 | ． 01 | ． 08 | ． | 860 |
| PEL－90－5－55 | 2 | 153 | 328 | 1944 | 34．0． | 10 | 3 | 699 | 5.51 | 74 | 5 | mo | 1 | 25 | 12\％ | 6 | 2 | 42 | ． 21 | \％70 | 15 | 19 | ． 84 | 41 | \＄p\％ | 2 | ． 99 | ． 01 | ． 06 | \＄ | 290 |
| PEL－90－5－56 | 2 | 21 | 13 | 20 | 1\％ | 10 | 6 | 197 | 6.80 | 20 | 5 | ND | 1 | 145 | 3 | 2 | 3 | 29 | ． 85 | \％07 | 3 | 17 | ． 16 | 64 | ＊ 6 | 3 | ． 69 | ． 01 | ． 12 | \＄ | 184 |
| PEL－90－5－57 | 3 | 23 | 19 | 45 | 2.1 | 15 | 14 | 802 | 8.34 | 13 | 5 | ND | 1 | 52 | 7 | 2 | 6 | 37 | ． 43 | ）090 | 3 |  | 1.47 | 36 | H2 |  | 1.89 | ． 01 | ． 13 | \％ | 46 |
| PEL－90－5－58 | 2 | 144 | 28 | 76 | 2 s． | 16 | 25 | 970 | 8.87 | 17 | 5 | MD | 1 | 59 | \％2 | 2 | 6 | 47 | ． 63 | 13／4 | 4 |  | 2.10 | 34 | \＄1积 | 2 | 2.25 | ． 01 | ． 09 | ， | 8 |
| PEL－90－5－59 |  | 2160 | 45 | 111 | 6．1） | 20 | 10 | 1537 | 6.74 | 81 | 5 | ND | 4 | 212 | \％ | 2 | 2 | 76 | 1.57 | \％260 | 18 |  | 2.25 | 37 | 立2 |  | 2.74 | ． 01 | ． 07 | \％ | 123 |
| PEL－90－5－60 | 2 | 101 | 179 | 164 | 10 | 4 | 2 | 64 | 9.51 | 25. | 5 | ND | 2 | 27 | \％ | 2 | 2 | 32 | ． 03 | 128 | 9 | 16 | ． 02 | 100 | 18 |  | ． 41 | ． 01 | ． 12 | ¢ | 5 |
| PEL－90－5－61 | 9 | 23 | 64 | 18 | 33 | 7 | 9 | 63 | 7.10 | 13. | 5 | No | 2 | 5 | \％ | 2 | 10 | 21 | ． 03 | \％06\％ | 2 | 36 | ． 03 | 56 | \％ | 3 | ． 22 | ． 01 | ． 12 | ． | 88 |
| PEL－90－5－62 | 30 | 22 | 31 | 14 | $\stackrel{1}{2}$ | 5 | 14 | 159 | 9.97 | 40 | 5 | No | 2 | 44 | \％ | 2 | 6 | 70 | ． 22 | 0084 |  | 19 | ． 21 | 46 | 4 | 4 | ． 45 | ． 01 | ． 05 | ， | 30 |
| PEL－90－5－63 | 2 | 87 | 183 | 197 | 88：8 | 42 | 44 | 222 | 11.29 | 1018 | 5 | ND | 1 | 48 | 23 | 3 | 13 | 13 | ． 24 | \％12 | 2 | 12 | ． 37 | 12 | \％ | 3 | ． 48 | ． 01 | ． 03 | \＄ | 980 |
| PEL－90－7－64 | 3 | 47 | 40 | 25 | 2\％ | 11 | 7 | 102 | 2.60 | 74. | 5 | ND | 1 | 2 | ，2 | 2 | 4 | 2 | ． 02 | \％00\％ | 2 | 9 | ． 01 | 14 | \％ 0 |  | ． 03 | ． 01 | ． 02 | 8 | 206 |
| Standard c／au－r | 18 | 59 | 40 | 130 | 8．9． | 71 | 31 | 1051 | 3.98 | 45 | 21 | 7 | 39 | 55 | 19．＊＊ | 15 | 19 | 57 | ． 52 | －19\％ | 39 | 59 | ． 91 | 182 | 唯\％ | 36 | 1.91 | ． 06 | ． 13 | 3 | 540 |

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| SAMPLE＊ | $\begin{gathered} \text { Mo } \\ \text { ppm } \end{gathered}$ | Cu ppm | $\begin{gathered} \text { Pb } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \mathbf{2 n} \\ \mathrm{ppm} \end{array}$ |  | $\begin{gathered} \mathrm{Ni} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { pprin } \end{array}$ | $\underset{\text { Mn }}{\mathrm{Mn}}$ | $\begin{gathered} \mathrm{Fe} \\ \mathbf{\%} \end{gathered}$ | As <br> ppro | $\begin{array}{r} U \\ \text { Ppm } \end{array}$ | $\begin{gathered} A u \\ p p m \end{gathered}$ | Th ppra | $\begin{array}{r} \mathrm{Sr} \\ \mathbf{p p m} \end{array}$ |  | $\begin{gathered} \text { Sb } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \text { Bì } \\ \text { ppm } \end{array}$ | $\begin{array}{r} V \\ \text { pppin } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \text { \% } \end{gathered}$ |  | La | $\begin{gathered} \mathrm{Cr} \\ \mathrm{pppm} \end{gathered}$ | $\begin{gathered} \mathrm{Mg} \\ \mathbf{Z} \end{gathered}$ | $\begin{gathered} \mathrm{Ba} \\ \mathrm{pp} \mathrm{~m} \end{gathered}$ | 維 | $\begin{array}{r} B \\ \text { Ppin } \end{array}$ | $\begin{gathered} \mathbf{A !} \\ \mathbf{Z} \end{gathered}$ | $\begin{gathered} \mathrm{Ha} \\ \text { \% } \end{gathered}$ | $\begin{aligned} & x \\ & x \end{aligned}$ |  | $\begin{aligned} & \mathrm{Acm} \\ & \text { ppb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL－90－DS－20 | 6 | 138 | 45 | 112 | 20\％ | 18 | 11 | 827 | 10.67 | 46 | 5 | ND | 4 | 121 | ，${ }^{\text {\％}}$ | 2 | 4 | 100 | ． 21 | 等225 | 16 | 23 | 1.13 | 305 | 2\％ |  | 2.20 | ． 10 | ． 12 | \％ | 1020 |
| PEL－90－DS－21 | 5 | 702 | 21 | 421 | ＊ 8 \％ | 79 | 74 | 2102 | 17.05 | 54 | 5 | ND | 5 | 8 | 界曻 | 2 | 2 | 51 | ． 03 | \％60\％ | 6 | 8 | ． 78 | 172 |  |  | 4.64 | ． 01 | ． 02 | \＆iov | 340 |
| SER－L2＋00S 0＋25E | 7 | 148 | 27 | 153 | 新 | 23 | 17 | 1246 | 7.06 | 21． | 5 | ND | 8 | 34 | \％ 3 | 3 | 2 | 56 | ． 20 | 16\％ | 20 | 28 | ． 83 | 106 | \％ 28 |  | 3.14 | ． 09 | ． 10 | 相 | 48 |
| SER－L2＋00S O＋50E | 5 | 171 | 44 | 171 | \％ | 20 | 14 | 1437 | 10.22 | 19 | 5 | ND | 6 | 92 | ＋＊＊ | 2 | 2 | 93 | ． 27 | 約数 | 26 | 30 | 1.54 | 338 | 迷 | 2 | 2.93 | ． 07 | ． 12 | \％sis | 68 |
| SER－L2＋COS 0＋75E | 4 | 172 | 25 | 153 | 晾 | 26 | 17 | 1143 | 11.39 | 16 | 5 | MD | 5 | 81 |  | 2 | 2 | 118 | ． 46 | \％ 20 | 13 | 33 | 1.49 | 157 | 約 | 2 | 2.80 | ． 18 | ． 12 | 行 | 51 |
| SER－L2＋00S 1＋00E | 3 | 171 | 44 | 173 | 䊉 | 24 | 15 | 1163 | 10.71 | 18 | 5 | ND | 5 | 80 | 令㐫 | 2 | 2 | 109 | ． 40 | 考78 | 13 | 34 | 1.59 | 209 |  |  | 2.75 | ． 16 | ． 12 | 紋 | 93 |
| SER－L2＋00S 1＋25E | 4 | 216 | 45 | 193 | \％乐 | 25 | 12 | 1126 | 11.86 | 2 | 5 | ND | 5 | 69 | 洨 9 | 3 | 2 | 105 | ． 15 | 等69 | 13 | 37 | 1.39 | 193 | 単効 |  | 2.68 | ． 05 | ． 07 | 勆納 | 184 |
| SER－L2＋00S 1＋50E | 4 | 207 | 46 | 198 | \％ | 25 | 12 | 1120 | 11.43 | 行 | 5 | ND | 5 | 65 | － 8 | 2 | 2 | 105 | ． 13 | \％\％62 | 14 | 36 | 1.46 | 181 | 2\％ |  | 2.87 | ． 05 | ． 09 |  | 97 |
| SER－L2＋00S 1＋75E | 4 | 212 | 31 | 173 | ＊${ }_{\text {\％}}$ | 30 | 19 | 1464 | 10.74 | 2\％ | 5 | ND | 5 | 55 | \％ | 2 | 2 | 102 | ． 13 | 玄里考安 | 13 | 31 | 1.47 | 159 | 年移 |  | 2.91 | ． 05 | ． 09 | \＄ | 65 |
| SER－L2＋00S 2＋00E | 3 | 164 | 31 | 179 |  | 28 | 18 | 1208 | 9.63 | \＄ 8 ． | 5 | ND | 4 | 72 | 汹納 | 2 | 2 | 104 | ． 42 | 苓52 | 12 | 32 | 1.60 | 129 | 令 |  | 2.83 | ． 15 | ． 14 | $\$$ | 65 |
| SER－L2＋00S 2＋25E | 4 | 190 | 28 | 203 | \％ | 37 | 24 | 1657 | 10.56 | 20 | 5 | ND | 5 | 72 | 䋛 | 2 | 2 | 86 | ． 53 |  | 14 | 26 | 1.71 | 126 | 薬＊ |  | 2.71 | ． 21 | ． 15 | 玄紬 | 122 |
| SER－L2＋00S 2＋50E | 3 | 111 | 39 | 179 | ，${ }^{\text {\％}}$ | 19 | 13 | 1074 | 9.63 | 12\％ | 5 | ND | 5 | 89 | 交 2 | 5 | 4 | 118 | ． 32 | 等6＊ | 15 | 17 | 1.18 | 177 | 亦＊＊ |  | 1.98 | ． 10 | ． 12 | 的 | 1480 |
| SER－L2＋00S 2＋75E | 2 | 50 | 185 | 89 | \％＊s | 8 | 7 | 792 | 8.74 | 248 | 5 | ND | 5 | 165 | \％ 0 | 6 | 2 | 142 | ． 30 | 漦3 | 22 | 16 | ． 87 | 322 | 玄40 |  | 1.60 | ． 10 | ． 19 | ＋ | 2270 |
| SER－L2＋00S 3＋00E | 4 | 51 | 185 | 128 | \％ | 12 | 8 | 818 | 9.87 | 8\％ | 5 | ND | 4 | 116 | 就 | 3 | 10 | 175 | ． 17 | 対22 | 33 | 24 | 1.29 | 327 | 的\％ | 2 | 2.30 | ． 10 | ． 19 |  | 2090 |
| SER－L2＋00S 3＋25E | 4 | 36 | 35 | 80 | \％${ }^{\text {\％}}$ | 12 | 6 | 602 | 7.60 | 50 | 5 | ND | 4 | 113 | \％$\%$ | 4 | 3 | 128 | ． 19 |  | 16 | 31 | 1.09 | 272 | 約䊽 | 2 | 1.95 | ． 09 | ． 13 |  | 450 |
| SER－L2＋00S 3＋50E | 4 | 50 | 25 | 83 | \％ | 13 | 6 | 653 | 8.60 | 54 | 5 | ND | 4 | 112 | \％ | 4 | 2 | 123 | ． 23 | \％ $180 \%$ | 16 | 27 | 1.14 | 236 |  |  | 2.98 | ． 06 | ． 10 |  | 280 |
| SER－L2＋50S O＋50E | 5 | 112 | 44 | 192 | \％ | 22 | 19 | 1556 | 7.97 | 2\％ | 5 | ND | 6 | 72 | \％ | 6 | 2 | 79 | ． 23 | 223 | 31 | 31 | 1.39 | 324 | ＋32 |  | 3.18 | ． 05 | ． 10 |  | 49 |
| SER－L2＋50S 0＋75E | 5 | 157 | 30 | 142 | ＊ 6 | 24 | 18 | 1123 | 7.93 | \％ | 5 | ND | 6 | 78 | \％ | 3 | 2 | 96 | ． 53 | 23） | 45 | 28 | 1.64 | 137 | 紬 | 2 | 2.63 | ． 17 | ． 13 | 納 | 140 |
| SER－L2＋50S 1＋00E | 4 | 184 | 27 | 155 | \％ | 26 | 30 | 1711 | 9.77 | ＊ 17 | 5 | ND | 5 | 89 | 㬉 | 3 | 2 | 103 | ． 58 |  | 14 | 27 | 1.78 | 156 |  |  | 2.81 | ． 21 | ． 16 |  | 65 |
| SER－L2＋50S 1＋25E | 5 | 207 | 30 | 192 | \％去 | 25 | 20 | 1452 | 11.51 |  | 5 | ND | 5 | 76 | 的 | 2 | 2 | 103 | ． 24 | 翏9\％ | 16 | 28 | 1.65 | 131 | ＊ 2 | 2 | 2.89 | ． 08 | ． 09 |  | 79 |
| SER－L2＋50S 1＋50E | 4 | 214 | 33 | 187 | \％ | 24 | 17 | 1293 | 11.19 | 25 | 5 | ND | 6 | 71 | \％ | 2 | 2 | 97 | ． 21 | \％ $7 \%$ | 14 | 26 | 1.49 | 114 |  |  | 2.71 | ． 06 | ． 09 | 行 | 107 |
| SER－L2＋50S 1＋75E | 3 | 218 | 20 | 186 | 的。 | 33 | 26 | 1707 | 9.32 | 13 | 5 | ND | 5 | 81 | ท\％ | 4 | 2 | 100 | ． 55 | 洤品 | 15 | 23 | 1.75 | 168 | 納納 |  | 3.10 | ． 19 | ． 14 |  | 53 |
| SER－L2＋50S 2＋00E | 3 | 232 | 23 | 195 | \％ 6 | 32 | 26 | 1793 | 9.61 | \＄12 | 5 | ND | 5 | 74 | \＄ | 3 | 2 | 97 | ． 42 | 3\％ | 15 | 22 | 1.70 | 147 |  |  | 3.07 | ． 14 | ． 12 | 行 | 93 |
| SER－L2＋50S 2＋25E | 5 | 220 | 30 | 194 | ＊ | 29 | 23 | 1715 | 10.08 | \％6 | 5 | ND | 6 | 55 | ＜ | 2 | 2 | 91 | ． 17 | 552 | 17 | 25 | 1.46 | 127 | 的 ${ }^{2}$ |  | 3.18 | ． 05 | ． 10 | \％ | 96 |
| SER－L2＋50S 2＋50E | 6 | 253 | 22 | 272 | ＊ | 37 | 26 | 1931 | 10.99 | 24 | 5 | ND | 6 | 54 | \％$\%$ \％ | 2 | 2 | 97 | ． 24 | 令80 | 14 | 24 | 1.63 | 137 | 水2 | 2 | 3.49 | ． 07 | ． 10 |  | 88 |
| SER－L2＋50S 2＋75E | 5 | 126 | 27 | 144 | \％ | 18 | 11 | 1161 | 8.64 | 21 | 5 | ND | 5 | 39 | \％ |  | 2 | 85 | ． 15 | 的92 | 18 | 24 | 1.08 | 118 | 全沓 |  | 3.75 | ． 04 | ． 07 | 行 | 75 |
| SER－L2＋50S 3＋00E | 3 | 33 | 33 | 60 | 令 | 5 | 4 | 479 | 8.08 | 37 |  | ND | 2 | 43 | \％ | 2 | 3 | 98 | ． 14 | 洔如 | 12 | 22 | ． 57 | 59 | ＊渋的 |  | 2.58 | ． 03 | ． 05 | 䊽 | 620 |
| SER－L2＋50S 3＋33E | 3 | 38 | 27 | 90 | \％${ }^{3}$ | 12 | 8 | 688 | 7.09 | 35 | 5 | ND | 3 | 106 | ＊ | 3 | 2 | 111 | ． 36 | 药85 | 15 | 25 | 1.23 | 192 | ＊ |  | 2.32 | ． 12 | ． 12 | 行 | 290 |
| SER－L2＋50S 3＋58E | 3 | 41 | 31 | 83 | \％$\%$ | 11 | 5 | 587 | 7.11 | 45． | 5 | ND | 3 | 70 | \％ | 3 | 2 | 109 | ． 25 |  | 16 | 27 | 1.04 | 161 |  | 2 | 2.78 3.97 | ． 06 | ． 08 |  | 310 |
| SER－L2＋50S 3＋83E | 3 | 68 | 33 | 113 | \％ | 15 | 8 | 1085 | 11.59 | 80 | 5 | ND | 4 | 73 | 組\％ | 2 | 2 | 179 | ． 11 | 薌5 | 23 | 39 | 1.07 | 201 | 令 ${ }^{\text {d }}$ | 2 | 3.97 | ． 04 | ． 09 |  | 480 |
| SER－L2＋505 4＋08E |  | 45 | 49 | 95 | 23 | 10 | 6 | 766 | 8.26 | 61 | 5 | ND | 3 | 88 | \％ | 4 | 3 | 136 | ． 22 | \％88 | 14 | 26 | 1.12 | 265 | \％ |  | 2.47 | ． 04 | ． 09 | 的㑊 | 570 |
| WS－90－8－1 | 13 | 55 | 35 | 124 | 方4 | 84 | 46 | 2613 | 9.22 | 40 | 5 | ND | 3 | 78 | 守 8 | 2 | 5 | 84 | ． 31 | 252 | 9 | 102 | 1.82 | 188 | \％ 28 |  | 3.08 | ． 10 | ． 12 | ，${ }^{1}$ | 123 |
| WS－90－8－2 | 7 | 57 | 27 | 129 | \％\％ | 32 | 18 | 972 | 8.19 | 4 | 5 | ND | 7 | 101 | ， 3 | 2 | 3 | 72 | ． 32 | \％89 | 8 | 28 | 1.44 | 134 | 22 |  | 3.15 | ． 09 | 14 | ， | 200 |
| WS－90－8－3 | 8 | 26 | 21 | 92 | ， | 17 | 7 | 515 | 4.82 | 50 | 5 | ND | 1 | 75 | \％ | 2 | 2 | 54 | ． 94 | 304． | 5 | 26 | 1.16 | 90 | \％ | 4 | 2.07 | ． 02 | ． 09 | \％ | 49 |
| WS－90－8－4 | 7 | 77 | 21 | 101 | \％\％ | 49 | 12 | 797 | 6.40 | 30 | 5 | ND | 2 | 69 | \％ 2 | 2 | 2 | 74 | ． 39 | \％088 | 6 | 105 | 1.53 | 68 | － | 2 | 2.84 | ． 03 | ． 08 |  | 45 |
| WS－90－8－5 | 9 | 47 | 23 | 83 | \％ | 24 | 19 | 1139 | 5.68 | 26 | 5 | ND | 88 | 65 | 2 | 2 | 2 | 72 | ． 34 | \％10 | 5 | 33 | ． 87 | 51 | ¢3 | 2 | 2.14 | ． 01 | ． 05 | ＜ | 24 |
| StANDARD C／AU－S | 18 | 57 | 36 | 131 | \％\％ | 71 | 31 | 1048 | 3.97 | \％ 38 | 20 | 7 | 38 | 53 | 19，0 | 16 | 18 | 56 | ． 52 |  | 37 | 59 | ． 90 | 181 | \％\％． | 36 | 1.90 | ． 06 | ． 14 | \％ | 49 |

ICP－． 500 GRAM SAMPLE IS DIGESTED WITH 3ML 3－1－2 HCL－HNO3－H2O AT 95 DEG．C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER． THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA II B W AND LIMITED FOR NA K AND AL．AU DETECTION LIMIT BY ICP IS 3 PPM． －SAMPLE TYPE：P1 TO P2 SOIL P3 ROCK AU＊ANALYSIS BY ACID LEACH／AA FROM 10 GM SAMPLE，


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| SAMPLE\＃ | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{cu} \\ \mathrm{ppm} \end{array}$ | Pb ppm | $\begin{array}{r} \text { 2n } \\ \text { ppm } \end{array}$ | $\sum_{\mathrm{pq}, \mathrm{mi}}^{\mathrm{A}}$ | $\begin{array}{r} \mathrm{Ni} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \mathrm{Z} \end{gathered}$ | $\stackrel{\text { As }}{\text { ppm. }}$ | $\begin{array}{r} \mathrm{U} \\ \mathrm{ppm} \end{array}$ | Au ppm | Th ppm | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p m} \end{array}$ | $\begin{gathered} \text { cod } \\ \text { ppme } \end{gathered}$ | $\begin{array}{r} \text { Sb } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathbf{B i} \\ \mathbf{p p m} \end{gathered}$ | $\begin{array}{r} v \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{\%} \end{gathered}$ | $\stackrel{\rightharpoonup}{*}$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cr} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathbf{M g} \\ \mathbf{Z} \end{array}$ | Ba <br> ppm | $\stackrel{1}{8}$ | $\begin{array}{r} \mathbf{B} \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Al} \\ \boldsymbol{X} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{Z} \end{gathered}$ | $\begin{aligned} & \mathbf{K} \\ & \mathbf{\%} \end{aligned}$ |  | $\begin{aligned} & \mathrm{A} \mathrm{u}^{*} \\ & \mathrm{ppp} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| WS－90－8－6 | 7 | 66 | 41 | 140 | ¢9 | 26 | 37 | 1491 | 5.69 | 18 | 5 | ND | 3 | 58 | 1，3． | 5 | 7 | 66 | ． 42 | ＊ 135 | 10 | 26 | 1.26 | 101 | ， 17 |  | 3.04 | ． 08 | ． 08 | 行 | 66 |
| WS－90－8－7 | 4 | 36 | 27 | 132 | 8.7 | 33 | 18 | 1121 | 6.39 | 17 | 5 | ND | 3 | 71 | 令 | 2 | 12 | 82 | ． 26 | \％179 | 7 | 36 | 1.67 | 271 | ＊ 8 | 2 | 5.34 | ． 02 | ． 50 | \％\％ | 330 |
| WS－90－B－8 | 10 | 35 | 55 | 128 | 8， | 52 | 19 | 1216 | 6.27 | 63 | 5 | ND | 1 | 57 | \％ 0 | 4 | 7 | 105 | ． 22 | 148 | 6 | 72 | 1.35 | 138 | ＊ 4 |  | 3.01 | ． 05 | ． 08 | \％ | 155 |
| WS－90－B－9 | 14 | 51 | 20 | 122 | \％ | 24 | 44 | 1464 | 7.18 | 12 | 5 | ND | 1 | 89 | 1 \％\％ | 4 | 8 | 65 | ． 19 | ＋15 | 7 | 31 | 1.15 | 133 | ＊$\leqslant$ |  | 4.18 | ． 02 | ． 13 S | 䋛 | 65 |
| WS－90－B－10 | 6 | 14 | 11 | 127 | \％ | 29 | 21 | 1164 | 11.56 | 25 | 5 | ND | 2 | 109 | 2 2 | 2 | 5 | 102 | ． 16 | $\stackrel{153}{ }$ | 7 | 64 | 2.60 | 283 | 叔䍃 |  | 4.44 | ． 04 | ． 99 䊽 | 坛就 | 79 |
| WS－90－8－11 | 18 | 90 | 37 | 183 | S． | 29 | 48 | 2012 | 6.21 | \％ 19 | 5 | ND | 1 | 69 | \％ | 2 | 6 | 70 | ． 31 | \％108 | 6 | 27 | 1.40 | 245 | ， 3 | 5 | 3.81 | ． 02 | ． 19 | 紬 | 40 |
| WS－90－8－12 | 10 | 86 | 146 | 230 | 1， 7 | 33 | 53 | 2915 | 7.02 | $\geqslant 17$ | 5 | ND | 1 | 64 | 1， 8 | 5 | 3 | 70 | ． 21 | $\stackrel{1}{33}$ | 14 | 25 | 1.36 | 671 | ＊ | 2 | 4.60 | ． 02 | ． 12 | \％$\chi^{*}$ \％ | 390 |
| ws－90－8－13 | 7 | 70 | 74 | 240 | 2．8 | 16 | 39 | 3733 | 5.91 | \％ 26 | 5 | ND | 2 | 36 | 1\％ | 3 | 7 | 52 | ． 15 | 102 | 16 | 21 | ． 71 | 100 | \％$\%$ | 3 | 4.06 | ． 01 | ． 06 | 約 | 51 |
| WS－90－8－14 | 9 | 89 | 68 | 215 | \％ | 26 | 37 | 2008 | 5.95 | 29 | 5 | ND | 1 | 77 | \％\％ | 2 | 10 | 67 | ． 32 | \％41 | 9 | 25 | 1.20 | 115 | 就 1 | 4 | 3.20 | ． 02 | ． 09 | 晾文 | 103 |
| STANDARD C | 20 | 59 | 36 | 133 | 7，6 | 73 | 32 | 1055 | 3.98 | 39. | 20 | 7 | 39 | 55 | 19， 3 | 15 | 20 | 57 | ． 52 | \％996 | 39 | 58 | ． 90 | 181 | ＊ 08 | 38 | 1.89 | ． 06 | ． 14 | 納 | － |

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| SAMPLE\＃ | $\begin{gathered} \text { Mo } \\ \text { Ppim } \end{gathered}$ | $\begin{gathered} \text { Cu } \\ \text { ppin } \end{gathered}$ | $\begin{gathered} \mathrm{Pb} \\ \mathrm{ppp} \end{gathered}$ | $\begin{array}{r} 2 n \\ \text { pprin } \end{array}$ |  | $\begin{array}{\|c} \mathrm{Ni} \\ \mathrm{Pp} \mathrm{~m}^{2} \end{array}$ | $\begin{array}{r} \text { Co } \\ \text { pprn } \end{array}$ | $\begin{array}{ll} \text { O } & \text { Mn } \\ 0 \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \mathbf{Z} \end{gathered}$ |  | $\begin{array}{r} U \\ \text { ppon } \end{array}$ | $\begin{array}{r} \mathbf{A u} \\ \text { ppran } \end{array}$ | $\begin{aligned} & \text { Th } \\ & \text { ppin } \end{aligned}$ | $\begin{aligned} & \mathbf{S r} \\ & \text { pppan } \end{aligned}$ |  | $\begin{aligned} & \text { Sb } \\ & \text { ppm } \end{aligned}$ | $\begin{array}{r} \mathbf{B i} \\ \text { ppm } \end{array}$ | $\begin{array}{r} v \\ \text { in ppm } \end{array}$ | $\begin{array}{cc} 1 & \mathrm{Ca} \\ \mathrm{n} & \end{array}$ | 粦 | $\begin{gathered} \text { La } \\ \text { ppm } \end{gathered}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{pppm} \end{gathered}$ | $\begin{array}{ll} \mathrm{r} & \mathrm{Mg} \\ \mathrm{~m} & \boldsymbol{K} \end{array}$ | $\begin{aligned} & 9 \mathrm{Ba} \\ & \mathrm{Bpm} \end{aligned}$ | 落 | $\text { 离 } \mathrm{Bp}$ | $\begin{array}{cc} \text { B } & \text { Al } \\ \text { pm } & X \end{array}$ | $\begin{gathered} \mathrm{Na} \\ \boldsymbol{Z} \end{gathered}$ |  |  | $\begin{aligned} & \text { Au* } \\ & \text { ppb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| K－ | 2 | 215 | 4 | 223 | 新 | 162 | 37 | 1336 | 6.88 | 7 | 5 | ND | 2 | 195 | 2 5 | 2 | 2 | 102 | 1.90 | 36\％ | 7 | 56 | 51.19 | 262 | \％30 |  | 24.81 | ． 28 | ． 78 | ＜ | 9 |
| K－B－90 | 1 | 35 | 7 | 99 | \％ | 60 | 19 | 974 | 3.51 | 15． | 5 | ND | 2 | 103 | \＄ 8 | 2 | 2 | 78 | 1.21 | 809\％ | ＋ 7 | 49 | 1.13 | 150 | 2\％ |  | 22.96 | ． 30 | ． 50 | ＊ | 13 |
| K－B－90－3 | 1 | 212 | 7 | 243 | \％ | 88 | 33 | 1134 | 6.21 | 24 | 5 | ND | 2 | 234 | \％\％$\%$ | 2 | 2 | 95 | 2.32 | \％2\％ | 6 | 37 | 1.24 | 127 | 50． |  | 25.16 | ． 57 | ． 46 | ¢ | 6 |
| PEL－90－J－86 | 1 | 99 | 60 | 630 | \％ | 18 | 13 | 598 | 8.26 | 139\％ | 5 | ND | 1 | 189 | 娄 | 3 | 2 | 44 | 1.45 | \％36 | 4 | 84 | ． 15 | 11 | \％ |  | 2.82 | ． 01 | ． 01 | ＊ | 105 |
| PEL－90－J－87 | 2 | 877 | 77 | 11726 | \％\％2 | 15 | 14 | 2090 | 9.57 | 109\％ | 5 | MD | 2 | 166 | 60\％ | 2 | 2 | 54 | 2.61 | \％198 | 4 | 22 | ． 55 | 22 | 30 |  | 21.06 | ． 01 | ． 02 | \％ 6 | 93 |
| PEL－90－J－88 | 1 | 332 | 20 | 3874 | \％${ }^{\text {\％}}$ | 1 | 4 | 894 | 14.64 | 3． | 5 | ND | 1 | 8 | 48＊ | 2 | 2 | 23 | ． 25 | ，00\％ | 4 | 2 | 2.17 | 12 | 8 |  | 2.14 | ． 01 | ． 01 | \％ | 340 |
| PEL－90－J－89 | 5 | 663 | 235 | 2197 | 徰采 | 6 | 5 | 5 404 | 11.18 | 319 | 5 | ND | 1 | 44 | － 0 | 4 | 2 | 33 | ． 30 | 304\％ | 2 | 16 | ． 16 | 4 | 約 |  | 2.39 | ． 01 | ． 01 | ， | 370 |
| PEL－90－J－90 | 4 | 1923 | 377 | 2116 | \％\％ | 11 | 22 | 408 | 6.68 | 849\％ | 5 | ND | 1 | 95 | ＊3 ${ }^{1}$ | 5 | 2 | 27 | ． 50 | 805\％ | 2 | 10 | ． 15 | 9 | 数賋 |  | 2.41 | ． 01 | ． 01 | \％ | 320 |
| PEL－90－J－91 | 15 | 1516 | 438 | 23124 | 效 | 13 | 7 | 1064 | 5.12 | \＄ $5 \%$ | 5 | 2 | 1 | 62 | 17\％ | 2 | 2 | 41 | ． 53 | 洖 | 2 | 43 | ． 65 | 5 | 淫\％ |  | 2.87 | ． 01 | ． 01 | 令5 | 860 |
| PEL－90－J－92 | 4 | 322 | 156 | 3125 | \％\％ | 17 | 26 | 1169 | 8.91 | 373． | 5 | ND | 2 | 262 | 翏＊＊䜌 | 5 | 2 | 47 | 1.99 | 等 5 | 4 | 22 | ． 25 | 11 | 維 |  | 2.96 | ． 01 | ． 01 | 的 | 280 |
| PEL－90－J－93 | 1 | 1053 | 249 | 12315 | 2\％） | 3 | 6 | 1092 | 20.93 | 23. | 5 | ND | 1 | 30 | \％ 4.8 | 4 | 2 | 22 | ． 29 | 时为吅 | 6 | 11 | ． 04 | 14 |  |  | 2.19 | ． 01 | ． 01 | \％ 8 | 720 |
| PEL－90－J－94 | 1 | 89 | 159 | 566 | \％\％＜ | 21 | 28 | 1305 | 8.20 | 49\％ | 5 | ND | 2 | 331 | 的紋 | 5 | 2 | 53 | 2.25 | \％ 28 | 7 | 22 | ． 67 | 4 | \％ |  | 31.48 | ． 01 | ． 01 | ， | 210 |
| PEL－90－J－95 | 1 | 84 | 5 | 371 | 㳽数 | 19 | 14 | 734 | 6.16 | ，${ }^{\circ}$ | 5 | ND | 2 | 23 | ＊等約 | 2 | 2 | 149 | ． 48 | \％\％\％ | 4 | 37 | 2.12 | 408 | 㜢 |  | 24.15 | ． 07 | 2.37 | \％ | 6 |
| PEL－90－J－95（0UP） | ， | 28 | 13 | 56 | 㐫納 | 14 | 16 | 11164 | 5.76 | 130． | 5 | ND | 2 | 114 | 喲2 | 3 | 2 | 65 | 1.18 | 26\％ | 5 | 16 | 1.26 | 26 | 缕年 |  | 21.31 | ． 01 | ． 08 | 2 | 780 |
| PEL－90－J－96 | 1 | 105 | 3 | 94 | 納 6 | 6 | 6 | 805 | 5.74 | \％ 2 ． | 5 | ND | 2 | 50 |  | 2 | 2 | 179 | ． 70 | \％32 | 4 | 34 | 2.00 | 99 | 洔 |  | 23.79 | ． 24 | 1.85 |  | 3 |
| PEL－90－J－97 | 1 | 198 | 123 | 45 | \％ 5 | 6 | 3 | 576 | 1.36 | ！ | 5 | ND | 1 | 9 | 行 | 6 | 4 | 2 | ． 01 | 8003 | － 2 | 4 | ． 01 | 10 | \％ 0 |  | 2.04 | ． 01 | ． 01 | \％${ }^{2}$ | 10 |
| PEL－90－J－98 | 1 | 71 | 20 | 168 |  | 7 | 11 | 2193 | 4.45 | 20 | 5 | ND |  | 544 | 響\％ | 3 | 2 | 28 | 5.30 | ＊ 20 | 9 | 3 | 1.20 | 60 | Sis |  | 4.61 | ． 02 | ． 21 | \％ | 4 |
| PEL－90－J－99 | 1 | 50 | 10 | 114 | \％ | 8 | 15 | 1850 | 5.01 | 18 | 5 | ND |  | 496 | 就 | 2 | 2 | 36 | 4.76 | 10\％ | 9 | 4 | 1.27 | 47 | 澵曾 |  | 3.91 | ． 02 | ． 18 |  | 6 |
| PEL－90－J－100 | 16 | 44 | 13 | 92 | 绊 | 59 | 135 | 9858 | 5.55 | 8 | 5 | ND | 3 | 36 | \％ | 2 | 2 | 17 | ． 14 | \％08\％ | 10 | 11 | ． 59 | 436 | 8is |  | 21.65 | ． 01 | ． 15 | \％ | 39 |
| PEL－90－J－101 | 10 | 10 | 23 | 122 | 35 | 59 | 25 | 1213 | 6.22 | 18． | 5 | ND |  | 144 | 行 | 2 | 20 | 90 | ． 89 | \％ 5 | 2 | 24 | 3.07 | 15 | 数全 |  | 22.70 | ． 01 | ． 03 | \％ | 470 |
| PEL－90－J－102 | 83 | 25 | 279 | 29 | 令 | 11 | 7 | 288 | 27.77 | 14\％ | 5 | ND | 3 | 92 | 者 | 2 | 52 | 111 | ． 05 | \％\％ | ＋ 4 | 11 | ． 47 | 52 | \％ |  | 2.95 | ． 07 | ． 06 | 䊽 | 1290 |
| PEL－90－J－103 | 1 | 6 | 6 | 76 | ， | 24 | 24 | 837 | 6.13 | 15 | 5 | ND | 1 | 61 | \％ | 2 | 2 | 53 | ． 52 | \％8\％ | 2 | 13 | 2.21 | 31 | 樃2 |  | 22.50 | ． 03 | ． 26 |  | 27 |
| PEL－90－J－104 | 35 | 7 | 12 | 6 | \％ 3 | 17 | 23 | 146 | 3.80 | 33 | 5 | ND | 1 | 200 | \％ | 2 | 2 | 31 | ． 94 | 8036 | 2 | 16 | ． 10 | 14 | \％ 20 |  | 2.78 | ． 01 | ． 02 | 涂 | 32 |
| PEL－90－J－105 | 3 | 10 | 3 | 6 | 就 | 4 | 4 | 111 | 1.60 | \％ | 5 | ND | 1 | 12 | 22 | 2 | 3 | 4 | ． 04 | 8008 | 2 | 4 | ． 05 | 11 | 很采 |  | 2.11 | ． 01 | ． 01 | \％ | 4 |
| PEL－90－J－106 | 25 | 18 | 7 | 18 | \％ | 3 | 18 | 112 | 24.92 | \％2 | 5 | ND | 9 | 52 |  | 2 | 7 | 61 | ． 18 | \％4\％ | 2 | 2 | ． 01 | 95 | 80 |  | 2.78 | ． 01 | ． 11 | ¢ | 35 |
| PEL－90－J－107 | 5 | 20 | 12 | 50 | \％ 2 | 9 | 3 | 366 | 4.33 | \％ 27 | 5 | ND | 1 | 187 | 的 | 2 | 2 | 79 | ． 81 | 80\％ | 2 | 25 | ． 96 | 13 | \％26 |  | 21.57 | ． 01 | ． 01 |  | 27 |
| PEL－90－J－108 | 47 | 63 | 22 | 51 | \％ | 14 | 10 | 480 | 2.31 | 2 2 | 5 | ND | 1 | 10 | \％ | 2 | 2 | 10 | ． 15 | 8030 | 2 | 8 | ． 09 | 54 | 84） |  | 2.45 | ． 01 | ． 06 | \％ | 540 |
| STANDARD C／AU－R | 19 | 61 | 37 | 131 | 6．8\％ | 72 | 32 | 1049 | 3.96 | 39\％ | 20 | 7 | 40 | 55 | \％ 2 S | 16 | 20 | 57 | ． 52 | 809\％ | 39 | 60 | ． 90 | 182 | 80 | 35 | 351.90 | ． 06 | ． 14 | \％ | 530 |

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| SAMPLE＊ | $\begin{gathered} \text { Mo } \\ \text { ppm } \end{gathered}$ | $\begin{gathered} \mathrm{Cu} \\ \mathrm{pppm} \end{gathered}$ | $\begin{array}{r} \text { Pb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{ppm} \end{array}$ | $\stackrel{\sim}{\text { ppon }}$ | $\begin{array}{r} \mathrm{Ni} \\ \mathbf{p p m} \end{array}$ | $\begin{aligned} & \text { Co } \\ & \text { ppon } \end{aligned}$ | $\begin{array}{r} \text { Mn } \\ \text { ppm } \end{array}$ | $\begin{array}{cc} \mathrm{Fe} \\ \mathrm{n} & \mathrm{Z} \end{array}$ |  | $\begin{array}{r} \text { U } \\ \text { ppin } \end{array}$ | $\begin{gathered} \mathrm{Au} \\ \mathrm{ppm} \end{gathered}$ | Th ppm | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p m} \end{array}$ | $\stackrel{\text { pd }}{\text { PPII }}$ | $\begin{array}{r} \text { Sb } \\ \text { ppm } \end{array}$ | $\underset{\text { Ppin }}{\mathbf{B i}}$ | $\begin{array}{r} v \\ p p i n \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{x} \end{gathered}$ | $\stackrel{\rightharpoonup}{\mathrm{F}}$ | $\begin{array}{r} \text { La } \\ \text { pppm } \end{array}$ | $\underset{\mathrm{ppm}}{\mathrm{Cr}}$ | $\begin{aligned} & \mathrm{Mg} \\ & \mathrm{X} \end{aligned}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | $\% \%$ | $\begin{array}{r} \text { B } \\ \text { ppm } \end{array}$ | $\begin{gathered} \text { Al } \\ \boldsymbol{X} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ | $\begin{aligned} & K \\ & \mathcal{Z} \end{aligned}$ |  | $\mathrm{Ac}^{*}$ <br> ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PL1－0＋75N | 3 | 36 | 36 | 68 | \％ 2 | 10 | 4 | 285 | 3.79 | 13 | 5 | ND | 1 | 23 | \％ | 3 | 4 | 50 | ． 15 | ，083 | 13 | 19 | ． 60 | 113 | \％19 | 2 | 1.81 | ． 04 | ． 07 | \％ | 10 |
| PL1－0＋50N | 6 | 22 | 39 | 45 | ＋ 4 | 5 | 5 | 147 | 5.18 | － | 5 | ND | 1 | 16 | \％ | 2 | 3 | 113 | ． 09 | \％，050 | 8 | 15 | ． 26 | 47 | \％35 | 2 | 1.34 | ． 01 | ． 04 | ＊ | 20 |
| PL1－0＋25N | 2 | 9 | 18 | 40 | ， 4 \％ | 2 | 1 | 104 | 1.68 | \％ | 5 | ND | 1 | 15 | 2． | 2 | 8 | 49 | ． 09 | －053 | 7 | 6 | ． 15 | 37 | \％22 | 3 | ． 74 | ． 01 | ． 04 | \％ | 45 |
| PL1－0＋00N | 7 | 30 | 11 | 66 | 星 6 | 1 | 5 | 331 | 6.05 | 13 | 10 | ND | 8 | 2 | 2 | 2 | 6 | 10 | ． 06 | 038 | 32 | 8 | ． 06 | 8 | \％ 5 | 5 | 4.55 | ． 07 | ． 06 | \％ | 18 |
| PL2－0＋75N | 5 | 29 | 26 | 69 | $\%$ | 10 | 6 | 309 | 6.72 | \％\％\％ | 5 | ND | 4 | 19 | 1．6． | 2 | 2 | 80 | ． 14 | \％080 | 16 | 26 | ． 67 | 155 | \％ 42 | 4 | 2.77 | ． 02 | ． 07 | \％$\%^{2}$ | 17 |
| PL2－0＋50N | 5 | 54 | 34 | 88 | \％ | 10 | 6 | 420 | 5.07 | \％12 | 5 | ND | 5 | 27 | \％ | 2 | 2 | 43 | ． 17 | \％18 | 22 | 18 | ． 70 | 168 | －23 | 3 | 2.36 | ． 06 | ． 09 | 的 | 66 |
| PL2－0＋25N | 5 | 62 | 46 | 112 | \％ 4 | 8 | 6 | 431 | 5.06 | श 17 | 5 | ND | 3 | 41 | － | 3 | 2 | 44 | ． 13 | \％ 38 | 15 | 17 | ． 79 | 468 | ＋18 | 2 | 1.87 | ． 02 | ． 10 | \％$\frac{1}{*}$ | 48 |
| PL2－0＋00N | 5 | 55 | 71 | 100 | － 6 | 9 | 5 | 371 | 4.90 | \％ 17 | 5 | ND | 2 | 24 | 2 | 5 | 4 | 47 | ． 15 | \％103 | 23 | 18 | ． 71 | 179 | $\underline{17}$ | 2 | 2.36 | ． 04 | ． 09 | \％\％ | 29 |
| PL3－0＋00N | 7 | 85 | 59 | 85 | \％ | 9 | 11 | 613 | 7.73 | \％16 | 5 | ND | 4 | 20 | 6． | 2 | 2 | 53 | ． 14 | \％ 147 | 19 | 21 | ． 63 | 72 | \％22 | 2 | 2.37 | ． 04 | ． 07 | \％${ }^{\text {d }}$ | 57 |
| PLI－2＋50N | 2 | 15 | 6 | 52 | 1，0 | 9 | 8 | 273 | 6.73 | $\geqslant, 82$ | 5 | ND | 3 | 17 | 1，\％ | 2 | 2 | 118 | ． 24 | \％19 | 6 | 20 | ． 45 | 31 | \％ 62 | 2 | 1.52 | ． 03 | ． 04 | \％$\geqslant$ | 4 |
| PL1－2＋25W | 6 | 34 | 27 | 75 | 为 | 8 | 8 | 741 | 6.95 | 17 | 5 | ND | 5 | 23 | ， 2 | 2 | 2 | 42 | ． 11 | \％20 | 19 | 18 | ． 55 | 130 | \％88 | 2 | 2.94 | ． 03 | ． 09 | \％ | 31 |
| PL1－2＋00N | 3 | 7 | 18 | 34 | \％ 2 | 6 | 4 | 230 | 2.75 | \％ | 5 | ND | 1 | 33 | 1＊ | 2 | 2 | 68 | ． 27 | \％56 | 6 | 9 | ． 28 | 44 | \％ 3 | 2 | ． 99 | ． 04 | ． 04 | \％ | 8 |
| PL1－1＋75 | 3 | 11 | 13 | 70 | \％2． | 7 | 6 | 731 | 4.53 | 12 | 5 | ND | 1 | 24 | ， 3 | 3 | 2 | 68 | ． 24 | 107 | 7 | 12 | ． 37 | 50 | 29． | 3 | 1.16 | ． 03 | ． 08 | \％ | 4 |
| PL1－1＋50N | 4 | 13 | 17 | 71 | \％$\%$ | 12 | 14 | 384 | 4.25 | 3 | 5 | ND | 1 | 70 | ＊ 4 | 2 | 2 | 70 | ． 80 | ，087\％ | 12 | 13 | 1.11 | 45 | \％${ }^{29}$ | 2 | 1.72 | ． 29 | ． 14 | \％ | 3 |
| PL1－1＋25W | 4 | 11 | 19 | 39 | \％$\psi^{4}$ | 3 | 4 | 144 | 4.62 | 3 | 5 | ND | 1 | 14 | \＄${ }^{\text {\％}}$ | 3 | 2 | 65 | ． 11 | \％074 | 9 | 15 | ． 16 | 40 | 2\％ | 2 | 1.68 | ． 01 | ． 03 | $\stackrel{1}{2}$ | 7 |
| PL1－1＋00N |  | 8 | 46 | 38 | \％ | 7 | 8 | 291 | 2.37 | \％$\%$ \％ | 5 | ND | 1 | 38 | 9 | 3 | 2 | 52 | ． 37 | \％054 | 4 | 8 | ． 47 | 39 | \％35 | 2 | ． 82 | ． 10 | ． 06 | \％ | 12 |
| PL1－0＋75 | 2 | 3 | 26 | 16 | \％ | 1 | 1 | 49 | ． 55 | \％ 4 | 5 | ND | 1 | 17 | \％${ }_{\text {\％}}$ | 2 | 4 | 37 | ． 09 | \％024 | 5 | 4 | ． 09 | 35 | \％ 17 | 3 | ． 75 | ． 01 | ． 03 | ง | 29 |
| PL1－0＋50N | 4 | 7 | 24 | 39 | ， 6 | 3 | 3 | 102 | 4.81 | \％ 6. | 5 | ND | 1 | 20 | －2 | 3 | 2 | 60 | ． 16 | 062 | 10 | 10 | ． 08 | 66 | \％ 16 | 2 | 1.15 | ． 01 | ． 03 | ！ | 3 |
| PL1－0＋25W | 12 | 15 | 25 | 56 | ， | 4 | 5 | 235 | 6.28 | ¢\％ | 5 | ND | 3 | 9 | 1，2 | 3 | 2 | 102 | ． 05 | \％030 | 23 | 11 | ． 11 | 18 | \％ |  | 1.44 | ． 01 | ． 03 | \％ | 4 |
| PL1－0＋50E | 5 | 13 | 20 | 43 | \％ 1.6 | 2 | 4 | 94 | 6.24 | \％ | 5 | ND | 2 | 6 | \％ 2 | 5 | 2 | 34 | ． 06 | 075 | 18 | 14 | ． 07 | 16 | \％ 12 | 2 | 3.62 | ． 02 | ． 03 | 1 | 4 |
| PL1－0＋75E | 5 | 75 | 30 | 85 | ， 5 | 10 | 9 | 694 | 5.37 | 24 | 5 | ND | 3 | 27 | ， 2 | 3 | 2 | 37 | ． 14 | \％25 | 15 | 16 | ． 74 | 158 | \％16 | 2 | 1.74 | ． 02 | ． 09 | \％ | 27 |
| PL1－1＋00E | 6 | 23 | 29 | 75 | ＊$\stackrel{5}{ }$ ， | 4 | 4 | 223 | 3.57 | \％，$\%$ | 5 | ND | 1 | 17 | 4． | 2 | 2 | 40 | ． 15 | ，082 | 27 | 13 | ． 34 | 41 | \％ 19 | 3 | 2.80 | ． 06 | ． 05 | \％ | 7 |
| PL1－1＋25E | 6 | 169 | 16 | 66 | 1， 3 | 7 | 6 | 298 | 4.94 | \％ 8 ， | 7 | ND | 3 | 14 | \％ | 2 | 2 | 55 | ． 20 | \％098 | 23 | 15 | ． 36 | 26 | \％33 | 2 | 4.58 | ． 06 | ． 05 | \％ | 3 |
| PL1－1＋50E | 9 | 75 | 10 | 69 | 1， 3 | 10 | 10 | 394 | 4.80 | \％$\%$ | 5 | ND | 1 | 41 | 100 | 2 | 4 | 58 | ． 48 | ． 0995 | 30 | 15 | ． 67 | 54 | \％28 |  | 3.29 | ． 17 | ． 09 | \％ | 5 |
| PL1－1＋75E | 5 | 50 | 23 | 88 | \％ | 12 | 13 | 619 | 5.64 | \％ 16 | 6 | ND | 7 | 32 | \％ 0 | 2 | 4 | 50 | ． 24 | \＄21 | 21 | 15 | ． 64 | 127 | \％33 | 2 | 2.78 | ． 08 | ． 10 | \％ 8 | 49 |
| PL1－2＋00E | 9 | 40 | 18 | 98 | $\stackrel{\square}{4}$ | 11 | 16 | 1039 | 6.31 | \％ 14 | 5 | ND | 8 | 42 | 1， 3 | 2 | 2 | 45 | ． 41 | ， 112 | 20 | 13 | ． 77 | 149 | 29 | 5 | 2.63 | ． 16 | ． 12 | \％$\%$ | 22 |
| PL1－2＋25E | 5 | 44 | 27 | 92 | \％ | 10 | 12 | 566 | 5.34 | \＆17 | 5 | ND | 6 | 35 | \％ 3 | 4 | 2 | 41 | ． 20 | 136 | 21 | 14 | ． 67 | 174 | 24． | 2 | 2.38 | ． 06 | ． 10 | \％${ }^{\text {\％}}$ | 51 |
| PL1－2＋50E | 4 | 28 | 16 | 80 | \＆ s | 11 | 9 | 450 | 4.62 | 13 | 5 | ND | 5 | 33 | \％ 2 | 2 | 3 | 45 | ． 22 | \％107 | 21 | 12 | ． 61 | 138 | \％28 | 2 | 2.40 | ． 05 | ． 07 | ¢ | 43 |
| PL2－2＋50W | 5 | 25 | 24 | 81 | \％$\%$ | 7 | 4 | 527 | 3.27 | 10． | 5 | ND | 2 | 67 | \＄3． | 3 | 2 | 44 | ． 30 | ，133 | 8 | 18 | ． 99 | 354 | ＋4． | 3 | 1.58 | ． 02 | ． 18 | 2 | 32 |
| PL2－2＋25 | 5 | 35 | 26 | 112 | $3$ | 10 | 5 | 456 | 3.25 | ， 14 | 5 | ND | 7 | 105 | \％ | 2 | 2 | 45 | ． 22 | \％122 | 7 | 19 | ． 96 | 376 | 21 | 2 | 1.70 | ． 01 | ． 18 | \％${ }^{\text {\％}}$ | 34 |
| PL2－2＋00H | 4 | 23 | 55 | 60 | ， 2 | 6 | 6 | 408 | 6.63 | \％ 13 | 5 | ND |  | 36 | 2 | 2 | 2 | 53 | ． 14 | \％09\％ | 8 | 25 | ． 60 | 164 | \＄4 | 2 | 2.29 | ． 01 | ． 08 | \％${ }^{\text {\％}}$ | 15 |
| PL2－1＋754 | 7 | 47 | 293 | 73 | 4，2 | 5 | 14 | 1036 | 8.49 | \％ 3 | 6 | ND | 3 | 15 | 18． | 3 | 4 | 55 | ． 07 | \％16 | 15 | 18 | ． 28 | 60 | \％ 8 | 2 | 2.49 | ． 01 | ． 06 | \％ | 7 |
| PL2－1＋50W | 6 | 22 | 20 | 52 | \％ 4 | 7 | 6 | 200 | 7.03 | \％$\%$ | 6 | ND | 1 | 14 | \％$\%$ | 2 | 2 | 57 | ． 12 | 089 | 18 | 19 | ． 24 | 40 | 20． |  | 1.93 | ． 03 | ． 05 | \％ | 10 |
| PL2－1＋25W | 5 | 44 | 25 | 85 | ＋4 | 10 | 6 | 519 | 4.55 | 13 | 5 | ND | 5 | 58 | \％$\%$ | 2 | 2 | 43 | ． 17 | 10\％ | 18 | 20 | ． 77 | 277 | 19． | 2 | 2.15 | ． 04 | ． 14 | \＆ | 15 |
| PL2－0＋754 | 6 | 50 | 34 | 87 | $4$ | 13 | 8 | 599 | 5.70 | 16 | 5 | ND | 5 | 30 | \％ 2 | 2 | 2 | 42 | ． 14 | 124． | 17 | 25 | ． 83 | 127 | \％${ }^{\text {\％}}$ ， | 2 | 1.95 | ． 02 | ． 08 | \＄ | 28 |
| PL2－0＋50W | 3 | 33 | 30 | 100 | 㟶 | 10 | 5 | 572 | 4.56 | 20 | 5 | ND | 2 | 36 | －8 | 2 | 2 | 35 | ． 14 | 139 | 17 | 21 | ． 93 | 296 | \％4 | 2 | 1.51 | ． 01 | ． 11 | \％ | 35 |
| STANDARD C／AU－S | 19 | 61 | 35 | 130 | 6．9． | 72 | 31 | 1054 | 3.98 | \％ 40 | 18 | 7 | 37 | 53 | 39\％ | 15 | 22 | 55 | ． 52 | \％098 | 38 | 56 | ． 90 | 181 | \％ 07 | 37 | 1.89 | ． 06 | ． 14 | \％ 12 | 50 |

ICP＝． 500 GRAM SAMPLE IS DIGESTED WITH 3ML 3－1－2 HCL－HNO3－H2O AT 95 DEG．C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B $\mathbf{H}$ AND LIMITED FOR NA K AND AL $\mathrm{C}_{\mathrm{A}}$ AU DETECTION LIMIT BY ICP IS 3 PPM． －SAMPLE TYPE：P1－P6 SOIL P7－P8 ROCK AU＊ANALYSIS BY ACID LEACH／AA FROM 10 GM SAMPLE．


Cathedral Gold Corp．PROJECT 8103 FILE \＃90－4553

| SAMPLE＊ | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \text { Pb } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \mathrm{Zn} \\ \text { ppm } \end{array}$ | $\sum_{\mathrm{pp}}^{\mathrm{m}} \mathrm{~g}$ | $\underset{\substack{\mathrm{Ni} \\ \mathrm{pp} \\ \hline \\ \hline}}{ }$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \boldsymbol{\chi} \end{gathered}$ | As ppra | $\begin{array}{r} U \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | Th ppm | $\begin{array}{r} \mathrm{Sr} \\ \mathrm{ppm} \end{array}$ | $\stackrel{6}{\mathrm{eq}} \mathrm{p}$ | $\begin{array}{r} \mathbf{S b} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \text { Bi } \\ \text { ppan } \end{gathered}$ | $\begin{array}{r} v \\ p p m \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{x} \end{gathered}$ | $\stackrel{\%}{*}$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppm} \end{gathered}$ | $\begin{array}{r} \mathrm{Mg} \\ \mathrm{x} \end{array}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppan} \\ \hline \end{array}$ | $\stackrel{1}{2}$ | $\begin{array}{r} B \\ \text { ppin } \end{array}$ | $\underset{X}{A l}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ | $\begin{aligned} & \mathbf{K} \\ & \mathbf{Z} \end{aligned}$ | ㅇㅏㅜㄹ | $\begin{aligned} & \mathrm{A} \mathrm{u}^{*} \\ & \mathrm{ppb} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PL2－0＋00W | 2 | 24 | 19 | 101 | ， 3 | 13 | 11 | 625 | 5.56 | 8 | 5 | ND | 5 | 21 | ， 2 | 2 | 4 | 58 | ． 28 | ， 102 | 19 | 19 | ． 54 | 50 | 37． |  | 3.20 | ． 10 | ． 09 | \％ | 14 |
| PL2－0＋25E | 6 | 22 | 41 | 83 | － | 4 | 12 | 1666 | 9.57 | 34 | 5 | MD | 4 | 8 | 2 | 2 | 6 | 20 | ． 10 | \＄36 | 15 | 12 | ． 23 | 18 | 16 |  | 2.68 | ． 05 | ． 05 | ¢ | 10 |
| PL2－0＋50E | 7 | 9 | 27 | 90 | \％ | 3 | 3 | 324 | 5.54 | 9 | 7 | ND | 10 | 3 | 2 | 2 | 7 | 13 | ． 05 | \％ 01 | 22 | 6 | ． 11 | 13 | ，15， |  | 3.52 | ． 09 | ． 08 | 1 | 4 |
| PL2－0＋75E | 9 | 18 | 40 | 94 | \＆ | 8 | 6 | 603 | 7.25 | 14 | 5 | ND | 6 | 13 | 2 | 2 | 4 | 50 | ． 07 | Y09\％ | 12 | 24 | ． 38 | 38 | \％ 30 | 2 | 1.73 | ． 02 | ． 05 | \％ | 13 |
| PL2－1＋00E | 11 | 143 | 179 | 59 | 1，3 | 2 | 12 | 891 | 13.40 | 126 | 5 | ND | 1 | 8 | \％ 2 | 7 | 6 | 12 | ． 09 | 24 | 2 | 8 | ． 33 | 26 | ．05 | 2 | 1.14 | ． 01 | 02 | 1 | 33 |
| PL2－1＋25E | 2 | 18 | 27 | 53 | 3，8． | 5 | 2 | 163 | 5.96 | 41． | 5 | ND | 1 | 19 | ， | 2 | 4 | 48 | ． 11 | 8076 | 8 | 16 | ． 19 | 56 | \％ 15 | 2 | 1.74 | ． 01 | ． 02 | 1 | 12 |
| PL2－1＋50E | 3 | 64 | 47 | 107 | 1，2 | 8 | 36 | 2274 | 3.94 | 12 | 5 | ND | 1 | 14 | 2 | 3 | 6 | 34 | ． 17 | 20\％ | 27 | 15 | ． 31 | 95 | ＋15 | 2 | 4.67 | ． 03 | ． 04 | ¢ | 22 |
| PL2－1＋75E | 4 | 6 | 16 | 44 | \％ 8 | 3 | 2 | 172 | 5.62 | 8 | 5 | MD | 1 | 15 | 2 | 2 | 5 | 42 | ． 10 | \％ 104 | 12 | 7 | ． 07 | 60 | \％19 | 2 | 2.03 | ． 01 | ． 03 | \％ $\mathrm{k}_{1}$ | 6 |
| PL2－2＋00E | 4 | 5 | 17 | 46 | \％ 8 | 3 | 2 | 116 | 5.27 | 4 | 5 | No | 1 | 7 | 2 | 2 | 5 | 78 | ． 05 | \％060 | 26 | 12 | ． 09 | 16 | \＄38 | 2 | 1.99 | ． 01 | ． 03 | 㤽 | 6 |
| PL2－2＋25E | 2 | 3 | 26 | 21 | \％ 4 | 1 | 1 | 333 | ． 60 | \％${ }^{3}$ | 5 | ND | 1 | 29 | \％ 6 | 3 | 5 | 27 | ． 10 | \％20． | 4 | 2 | ． 06 | 113 | 需 | 4 | ． 86 | ． 01 | ． 05 | 3 | 9 |
| PL2－2＋50E | 1 | 1 | 12 | 36 | 1．9 | 4 | 3 | 134 | 1.66 | \％ 2 | 5 | ND | 1 | 26 | 5 | 3 | 8 | 69 | ． 27 | 5057 | 5 | 9 | ． 22 | 60 | \％6． | 2 | ． 74 | ． 05 | ． 05 | 2 | 7 |
| PL3－1＋754 | 1 | 90 | 101 | 56 | 2．6 | 6 | 4 | 689 | 10.21 | \％\％ | 5 | ND | 1 | 27 | ．2 | 2 | 2 | 68 | ． 15 | \％80 | 2 | 40 | ． 52 | 103 | \％20 | 2 | 1.31 | ． 01 | ． 06 | \％ | 34 |
| PL3－1＋504 | 1 | 7 | 43 | 33 | ＊ 6 | 5 | 3 | 179 | 3.18 | \％ | 5 | ND | 1 | 24 | 2 | 2 | 5 | 101 | ． 18 | ＊062 | 3 | 11 | ． 22 | 49 納 | \％ 47 | 2 | 1.13 | ． 02 | ． 04 | 2 | 10 |
| PL3－1＋25W |  | 7 | 37 | 60 | 1，6 | 7 | 7 | 235 | 2.43 | 4 | 5 | ND | 1 | 45 | － 4 | 3 | 2 | 70 | ． 46 | \＄082 | 4 | 14 | ． 33 | 41 | \％ 25 | 2 | ． 96 | ． 13 | ． 07 | 2 | 7 |
| PL3－1＋00N | 3 | 25 | 144 | 70 | \％\％ | 5 | 2 | 334 | 6.27 | \％23 | 5 | ND | 1 | 35 | \％ 2 | 2 | 2 | 69 | ． 10 | ，515 | 6 | 22 | ． 55 | 327 | ， 12 | 2 | 1.57 | ． 01 | ． 10 | \％ | 18 |
| PL3－0＋754 | 3 | 21 | 43 | 56 | \％\％ | 4 | 2 | 281 | 6.04 | \％88 | 5 | MD | 1 | 24 | ， | 2 | 3 | 72 | ． 09 | \％1\％ | 9 | 16 | ． 35 | 162 | 19 | 2 | 1.66 | ． 01 | ． 06 | 1 | 11 |
| PL3－0＋50N | 5 | 28 | 27 | 53 | 20， | 3 | 3 | 415 | 6.32 | 8 | 5 | ND | 1 | 8 | 2 | 2 | 2 | 38 | ． 12 | \％2t | 16 | 11 | ． 13 | 26 | \％ 18 | 2 | 3.00 | ． 01 | ． 03 | 行 | 18 |
| PL3－0＋25H | 6 | 13 | 27 | 59 | ＊ 8 | 4 | 4 | 465 | 6.77 | 10 | 5 | ND | ， | 12 | \％ 2 | 2 | 2 | 67 | ． 08 | \％070 | 10 | 16 | ． 19 | 25 | \％ 33 | 2 | 1.46 | ． 02 | ． 05 | ไ | 12 |
| PL3－0＋25E | 3 | 16 | 20 | 47 \％ | \％ 5. | 2 | 1 | 140 | 3.99 | 2 | 5 | ND | 1 | 9 | \％ 2 | 2 | 2 | 47 | ． 08 | 064 | 14 | 11 | ． 15 | 27 | ＋26 |  | 2.40 | ． 03 | ． 03 | ¢ | 5 |
| PL3－0＋50E | 3 | 48 | 35 | 139 | \％${ }^{\text {\％}}$ | 12 | 9 | 753 | 4.42 | 15 | 5 | ND | 2 | 31 | 22 | 2 | 2 | 37 | ． 16 | \％00 | 19 | 20 | ． 68 | 179 | 19． | 2 | 2.07 | ． 04 | ． 10 |  | 172 |
| PL3－0＋75E | 4 | 24 | 31 | 47 3 | \％${ }^{6}$ |  | 6 | 952 | 5.06 | \％ 5 |  | ND | 1 | 11 | \％ 2 | 2 | 2 | 92 | ． 07 | \％26 | 5 | 11 | ． 14 | 54 | ＋26 | 2 | 1.02 | ． 01 | ． 03 | \＄ | 8 |
| PL3－1＋00E | 4 | 20 | 36 | 40 | \％ 4 | 4 | 3 | 665 | 6.21 | 221 | 5 | ND | 1 | 17 | $\geqslant 2$ | 2 | 5 | 89 | ． 07 | 116 | 8 | 14 | ． 23 | 36 | ， 27 | 2 | 1.76 | ． 01 | ． 02 | ＜1 | 79 |
| PL3－1＋25E | 5 | 40 | 23 | 70 | \％ | 7 | 13 | 1134 | 6.50 | \％ 13 | 5 | ND | 2 | 18 | \％2 | 2 | 3 | 41 | ． 16 | V48 | 26 | 17 | ． 46 | 33 | \％25 |  | 3.20 | ． 05 | ． 05 | ¢ | 22 |
| PL3－1＋50E | 7 | 9 | 27 | 49 | \＄1， | 4 | 3 | 218 | 4.47 | \％ 11 | 5 | ND | 1 | 23 | \％ 2 | 2 | 2 | 69 | ． 14 | \％1／ | 16 | 14 | ． 17 | 53 | ＋30 | 2 | 1.04 | ． 02 | ． 04 | 2 | 13 |
| PL3－2＋00E | 1 | 13 | 14 | 55 | 12\％ | 6 | 2 | 92 | 2.19 | 2 | 5 | ND | 1 | 13 | \％3． | 2 | 2 | 77 | ． 14 | \％88 | 6 | 16 | ． 19 | 39 ； | \％ 46 | 3 | 1.91 | ． 02 | ． 03 | 3 | 4 |
| PL3－2＋25E | 2 | 31 | 27 | 59 | ＋3 | 9 | 10 | 797 | 4.44 | 10 | 5 | ND | 1 | 33 | \％ 2 | 2 | 2 | 48 | ． 19 | $\bigcirc 135$ | 10 | 14 | ． 56 | 125 | 25 | 2 | 1.87 | ． 03 | ． 06 | 2 | 32 |
| PIN L1－0＋00E | 3 | 25 | 32 | 63 | \％ 6 | 10 | 9 | 338 | 5.23 | 2 | 5 | ND | 1 | 22 | \％2 | 2 | 3 | 88 | ． 18 | 083 | 12 | 21 | ． 39 | 31 ； | 40 | 4 | 3.08 | ． 03 | ． 04 | 2 | 8 |
| PIN L1－0＋25E | 7 | 39 | 28 | 79 | 4 | 8 | 7 | 516 | 8.75 | 6 | 5 | ND | 2 | 13 | \％ 2 | 2 | 2 | 66 | ． 07 | \％061 | 16 | 34 | ． 36 | 23 | \％28 |  | 2.79 | ． 04 | ． 06 | \＄1 | 4 |
| PIN L1－0＋50E | 9 | 34 | 29 | 74 | ，2 | 8 | 7 | 489 | 7.37 | 5 | 5 | ND | 1 | 17 | ＋2 | 2 | 2 | 95 | ． 08 | 054 | 13 | 31 | ． 28 | 27 | \％ 38 | 2 | 2.36 | ． 02 | ． 04 | \％ | 3 |
| PIN L1－0＋75E | 6 | 28 | 20 | 67 | －2 | 9 | 9 | 636 | 6.53 | t | 5 | ND | 1 | 15 | \％ 2 | 2 | 2 | 79 | ． 15 | \％070 | 12 | 21 | ． 29 | 24 | \％ 40 | 2 | 2.60 | ． 04 | ． 06 | \} | 4 |
| PIN L1－1＋00E | 5 | 40 | 30 | 74 | ， | 9 | 9 | 454 | 8.39 | 5 | 5 | ND | 2 | 12 | 2 | 2 | 2 | 73 | ． 07 | －049 | 15 | 35 | ． 37 | 23 | \％ 31 | 2 | 3.47 | ． 03 | ． 05 | \％ | 15 |
| PIN L1－1＋25E | 1 | 21 | 19 | 66 | ， | 11 | 9 | 231 | 5.44 | 2 | 5 | ND | 1 | 28 | \％2 | 3 | 2 | 102 | ． 41 | \％085 | 14 | 25 | ． 61 | 35 | \％ 63 | 2 | 4.29 | ． 09 | ． 05 | \％1 | 3 |
| PIN 11－1＋50E | 4 | 36 | 48 | 92 | \％$\%$ | 13 | 10 | 651 | 5.17 | 3 | 5 | ND | 1 | 64 | ， 2 | 2 | 2 | 75 | ． 61 | 182 | 13 | 31 | 1.04 | 65 | \％ 36 |  | 2.79 | ． 21 | ． 11 | \％ | 21 |
| PIN L1－1＋75E | 6 | 20 | 23 | 66 | \％ 7 | 7 | 14 | 838 | 5.82 | 3 | 5 | ND | 1 | 14 | 2 | 2 | 2 | 80 | ． 13 | 6\％2 | 14 | 22 | ． 28 | 22 | ＋40 | 2 | 2.61 | ． 04 | ． 05 | 2 | 8 |
| PIN L1－2＋00E | 3 | 17 | 25 | 63 | \％ | 11 | 6 | 267 | 6.80 | 2 | 5 | ND | 1 | 16 | 2 | 2 | 2 | 105 | ． 19 | 1074 | 9 | 27 | ． 58 | 26 | \％ 55 | 2 | 2.57 | ． 04 | ． 06 | \％ | 5 |
| PIN L1－2＋25E | ， | 19 | 12 | 70 | ，4 | 10 | 14 | 556 | 6.24 | 3 | 5 | ND | 1 | 21 | 2 | 2 | 2 | 100 | ． 30 | 2086． | 11 | 24 | ． 54 | 28 | 6\％ | 2 | 4.00 | ． 07 | ． 06 | 行 | 3 |
| STANDARD C／AU－S | 17 | 59 | 42 | 133 | \％\％2 | 72 | 31 | 1059 | 3.98 | 39 | 21 | 7 | 36 | 53 | 18，6． | 16 | 21 | 56 | ． 53 | －09\％ | 36 | 60 | ． 90 | 180 | ． 07 | 39 | 9.89 | ． 06 | ． 14 | 机 | 46 |

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| SAMPLE\＃ | Mo ppm | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{pppm} \end{array}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} 2 n \\ \text { ppm } \end{array}$ | $\mathrm{N}_{\mathrm{p}}^{\mathrm{g}} \mathrm{~g}$ | $\underset{\mathrm{ppm}}{\mathrm{Ni}}$ | $\begin{array}{r} \text { Co } \\ \text { ppom } \end{array}$ | $\begin{array}{r} \text { Mn } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \mathbf{\%} \end{gathered}$ | $\sum_{\mathrm{p} \boldsymbol{p} \boldsymbol{p}}^{\mathrm{H}}$ | $\begin{array}{r} \text { U } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{aligned} & \text { Th } \\ & \text { ppm } \end{aligned}$ | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p m} \end{array}$ | $\begin{gathered} \text { cd } \\ \text { pprig } \end{gathered}$ | $\begin{array}{r} \text { Sb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Bi } \\ \text { ppm } \end{array}$ | $\begin{array}{r} V \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \mathbf{\%} \end{gathered}$ | $\psi_{i}$ | $\begin{array}{r} \text { La } \\ \text { pppm } \end{array}$ |  | $\begin{array}{r} \mathrm{Mg} \\ \mathbf{Z} \end{array}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | $\geqslant \% \text {, }$ | $\begin{array}{r} \text { B } \\ \text { ppin } \end{array}$ | $\begin{gathered} \text { Al } \\ \text { R } \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ | $\begin{aligned} & K \\ & \% \end{aligned}$ | ppon | Au＊ ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PIN L1－2＋50E | 6 | 23 | 21 | 82 | \％ 9 | 6 | 20 | 870 | 6.91 | 8. | 5 | ND | 1 | 11 | ． 2 | 2 | 4 | 72 | ． 13 | \＄059 | 26 | 24 | ． 22 | 21 | \％ 3 | 5 | 3.27 | ． 05 | ． 05 | \％ |  |
| PIN L1－2＋75E | 9 | 13 | 27 | 62 | \％ 4 | 2 | 3 | 183 | 6.50 | 5 | 5 | ND | 2 | 7 | ， 3 | 2 | 2 | 82 | ． 05 | ， 036 | 19 | 21 | ． 11 | 14 | 36 | 2 | 2.09 | ． 05 | ． 06 | \％ |  |
| PIN L1－3＋00E | 3 | 25 | 19 | 74 | \％ 5 | 9 | 9 | 330 | 7.84 | 5 | 5 | ND | 3 | 31 | \％ | 6 | 2 | 105 | ． 43 | \＄10 | 14 | 29 | ． 57 | 34 | 63 | 3 | 4.33 | ． 12 | ． 07 | ¢ |  |
| PIN L1－3＋25E | 4 | 41 | 33 | 131 | ， | 19 | 14 | 560 | 5.43 | 13． | 5 | ND | 5 | 24 | 相 | 2 | 2 | 69 | ． 28 | 186 | 25 | 28 | ． 64 | 43 | \％ 4 | 5 | 3.79 | ． 12 | ． 09 | \％ |  |
| PIN 11－3＋50E | 4 | 17 | 24 | 80 | 鲳 | 12 | 8 | 309 | 4.59 | \％，$\%$ | 5 | ND | 2 | 42 | 2 | 3 | 5 | 91 | ． 46 | \％070 | 12 | 24 | ． 68 | 33 | \％ 5 \％ | 4 | 2.54 | ． 17 | ． 10 | \％ |  |
| PIN L1－4＋00E | 1 | 13 | 13 | 84 | \％ | 19 | 32 | 1822 | 5.66 | 5． | 5 | ND | 1 | 112 | 1， 8 | 5 | 2 | 96 | 1.65 | ，097 | 10 | 23 | 1.27 | 70 | ，44． | 3 | 2.45 | ． 40 | ． 16 | \％ |  |
| PIN 11－4＋25E | 2 | 19 | 21 | 137 | \％ 7 | 14 | 12 | 419 | 5.91 | 8. | 5 | ND | 1 | 49 | 3．4 | 3 | 2 | 107 | ． 64 | \％09\％ | 14 | 22 | ． 60 | 43 | \％88 | 2 | 2.84 | ． 16 | ． 09 | \} |  |
| PIN L1－4＋50E | 3 | 15 | 27 | 69 | \％$\%$ | 9 | 8 | 307 | 4.92 | \＄10 | 5 | ND | 2 | 23 | \％ 6 | 4 | 2 | 80 | ． 30 | ，08\％ | 12 | 22 | ． 48 | 25 | ＋ 15 | 2 | 2.96 | ． 07 | ． 06 | \} |  |
| PIM L1－4＋75E | 3 | 42 | 22 | 121 | \％ 5 | 25 | 23 | 835 | 6.09 | \％ 14 | 5 | ND | 1 | 96 | \％2 | 5 | 2 | 81 | 1.14 | 103 | 13 | 30 | 1.46 | 64 | 42 | 2 | 2.97 | ． 44 | ． 18 | 2 |  |
| PIN L1－5＋00E | 2 | 57 | 21 | 139 | $\stackrel{\theta}{2}$ | 35 | 27 | 1316 | 7.37 | $83$ | 5 | ND | 1 | 81 | \％ 6 | 6 | 2 | 76 | ． 99 | \％ 5 50： | 13 | 31 | 1.46 | 58 | \％88 | 2 | 2.96 | ． 38 | ． 16 | \％ | 6 |
| PIN L1－5＋25E | 2 | 81 | 22 | 211 | \％$\%$ | 55 | 45 | 1967 | 9.92 | 208 | 5 | ND | 1 | 55 | \％ 6 | 9 | 2 | 64 | ． 66 | 203． | 21 | 33 | 1.05 | 51 | 28． | 2 | 3.05 | ． 23 | ． 11 | ， |  |
| PIM L\}-5+50E | 3 | 13 | 13 | 74 | \％ | 11 | 11 | 518 | 5.84 | 10． | 5 | ND | 1 | 31 | 88 | 5 | 2 | 95 | ． 40 | 8075 | 18 | 21 | ． 54 | 32 | 48 | 4 | 2.94 | ． 10 | ． 06 | 多 |  |
| PIN L2－0＋00E | 8 | 30 | 24 | 72 | \％ 8 | 7 | 6 | 532 | 6.80 | 5． | 5 | ND | 2 | 13 | ， 2 | 2 | 4 | 84 | ． 14 | －058 | 13 | 26 | ． 32 | 22 | 4 | 5 | 2.86 | ． 05 | ． 06 | \％ |  |
| PIN L2－0＋25E | 8 | 27 | 17 | 80 | 4 | 4 | 11 | 1303 | 7.82 | 8 | 5 | ND | 2 | 6 | 2 | 2 | 3 | 42 | ． 05 | 046 | 27 | 23 | ． 16 | 14 | 23 | 2 | 2.87 | ． 04 | ． 07 | ¢ |  |
| PIN L2－0＋50E | 8 | 27 | 23 | 61 | \％ | 4 | 15 | 851 | 7.71 | 5． | 5 | ND | 2 | 8 | ＋2 | 2 | 3 | 69 | ． 06 | \％04\％ | 22 | 20 | ． 16 | 19 | 835 | 2 | 2.49 | ． 03 | ． 06 | \％ |  |
| PIN L2－0＋75E | 6 | 20 | 21 | 58 | 水3． | 4 | 15 | 680 | 5.53 |  | 5 | ND | 1 | 13 | 5． | 2 | 5 | 73 | ． 10 | 8046 | 25 | 17 | ． 15 | 26 | ， 37 | 2 | 2.55 | ． 03 | ． 04 | 娄 | 11 |
| PIN L2－1＋00E | 6 | 25 | 20 | 85 | \％ 4 | 5 | 26 | 1224 | 8.25 | 6． | 5 | ND | 1 | 8 | 2 |  | 2 | 56 | ． 09 | 049 | 31 | 28 | ． 16 | 19 | ，27 | 2 | 3.01 | ． 05 | ． 05 | \＄ |  |
| PIN L2－1＋25E | 9 | 27 | 27 | 92 | \％ 6 | 12 | 29 | 1157 | 9.00 | \％ 13 | 5 | ND | 4 | 14 | ， 4 | 5 | 3 | 112 | ． 11 | ． 054 | 21 | 46 | ． 34 | 36 | 48． | 3 | 2.81 | ． 04 | ． 07 | \＄ | 15 |
| PIN L2－1＋50E | 6 | 53 | 57 | 111 | 粦 0 | 16 | 8 | 561 | 4.62 | 5 | 5 | ND | 3 | 31 | \％7 | 2 | 3 | 73 | ． 19 | \％28 | 20 | 35 | ． 93 | 90 | 35 | 2 | 3.10 | ． 04 | ． 06 | ＊ | 25 |
| PIN L2－1＋75E | 6 | 28 | 26 | 78 | \％\％ | 7 | 12 | 615 | 6.94 | 9 | 5 | ND | 3 | 8 | ＊ 4 | 2 | 2 | 50 | ． 08 |  | 21 | 27 | ． 20 | 18 | 2\％ | 2 | 3.54 | ． 05 | ． 06 | 永 |  |
| PIN L2－2＋00E | 3 | 41 | 33 | 135 | \％\％ | 13 | 10 | 378 | 6.39 |  | 5 | ND | 3 | 30 | \＆2 |  | 2 | 109 | ． 33 | \％13 | 15 | 30 | ． 59 | 41 | \％ 68 | 2 | 4.76 | ． 10 | ． 07 | 行 |  |
| PIN L2－2＋25E | 9 | 30 | 34 | 101 | \％ 2 | 8 | 16 | 1974 | 8.03 | 13． | 5 | ND | 3 | 7 | \％${ }^{\text {a }}$ | 2 | 2 | 54 | ． 05 | \％057 | 17 | 31 | ． 35 | 16 | 25 | 2 | 2.59 | ． 04 | ． 06 | \＄ |  |
| PIN L2－2＋50E | 10 | 21 | 23 | 56 | ＋3 | 7 | 6 | 480 | 5.30 | 2 | 5 | ND | 2 | 11 | \％ 3. | 2 | 3 | 71 | ． 12 | 1052 | 17 | 17 | ． 23 | 19 | \％44 | 2 | 2.38 | ． 04 | ． 05 | \＄ |  |
| PIN L2－2＋75E | 8 | 15 | 20 | 75 | $\geqslant 2 \%$ | 2 | 2 | 570 | 7.51 | ， 14 | 5 | ND | 8 | 2 | 2 | 2 | 2 | 15 | ． 05 | \％043 | 28 | 12 | ． 05 | 8 | 15． | 2 | 4.01 | ． 06 | ． 06 | 㐫 |  |
| PIN L2－3＋00E | 2 | 1 | 7 | 62 | \％ 4 | 11 | 6 | 210 | 4.85 | \％ 2 | 5 | ND | 3 | 25 | 4． | 2 | 2 | 130 | ． 30 | \％080 | 6 | 17 | ． 42 | 23 | \％7\％ | 2 | 1.68 | ． 09 | ． 06 |  |  |
| PIN L2－3＋25E | 3 | 40 | 23 | 145 | \％ 5 | 20 | 22 | 1431 | 6.60 | \％ | 5 | ND | 1 | 19 | ． 9 | 3 | 2 | 63 | ． 26 | \％23 | 13 | 25 | ． 73 | 57 | \％ 4 4 | 2 | 3.11 | ． 04 | ． 05 | \＆ |  |
| PIN L3－2＋00E | 3 | 33 | 43 | 108 | \％ 5 | 17 | 10 | 357 | 4.29 | \％ 8 \％ | 5 | ND | 2 | 39 | \％ 5 | 3 | 2 | 105 | ． 43 | 009\％ | 16 | 34 | ． 74 | 47 | ， 57 | 3 | 4.10 | ． 14 | ． 08 | \％ |  |
| PIN L3－2＋25E | 3 | 32 | 15 | 93 | \％ 5 | 13 | 8 | 286 | 6.74 | \％11 | 5 | ND | 3 | 25 | \％ 4 | 4 | 4 | 98 | ． 35 | ， 092 | 15 | 26 | ． 55 | 32 | \％ 61 | 2 | 4.47 | ． 09 | ． 06 | \％ |  |
| PIN L3－2＋50E | 3 | 17 | 22 | 77 | \％ 2 | 14 | 12 | 457 | 5.26 | 2 | 5 | ND | 1 | 55 | \％ 7 | 2 | 2 | 85 | ． 63 | －07\％ | 11 | 22 | ． 85 | 38 | \％ 47 |  | 2.62 | ． 23 | ． 11 | \％ |  |
| PIN L3－2＋75E | 1 | 6 | 10 | 71 | \％ | 17 | 15 | 410 | 4.77 | 2 | 5 | ND | 1 | 102 | \％$\%$ | 2 | 2 | 93 | 1.16 | \％078 | 7 | 20 | 1.23 | 54 | 56． | 2 | 2.17 | ． 42 | ． 17 | $\%$ |  |
| PIN L3－3＋00E | 2 | 26 | 15 | 62 | \％ 2 | 13 | 9 | 282 | 4.94 | 2 | 5 | ND | 2 | 36 | ， 3 | 2 | 3 | 98 | ． 51 | －099 | 10 | 25 | ． 66 | 30 | \％ 67. | 2 | 3.98 | ． 13 | ． 06 | \％ |  |
| PIN L3－3＋25E | 1 | 11 | 12 | 100 | \％$\%$ | 15 | 11 | 705 | 4.62 | 2 | 5 | ND | 1 | 40 | \％ 4 | 2 | 2 | 89 | ． 50 | \％13 | 7 | 19 | ． 48 | 53 | －38 | 2 | 2.83 | ． 12 | ． 06 | \％ |  |
| PIN L3－3＋50E |  | 4 | 2 | 100 | \％ 4 | 23 | 24 | 1116 | 5.64 | 2 | 5 | ND | 1 | 165 | 4． | 5 | 2 | 96 | 2.26 | \＄12 | 9 | 24 | 1.96 | 91 | \％62 | 2 | 2.51 | ． 77 | ． 28 | \％ |  |
| PIN－90 1 | 2 | 10 | 14 | 51 | \％$\%$ | 10 | 5 | 218 | 4.55 | 2 | 5 | ND | 2 | 21 | ， 2 ． | 4 | 2 | 86 | ． 26 | 5093． | 8 | 18 | ． 38 | 25 | \＄48 | 2 | 2.53 | ． 06 | ． 05 | \％ |  |
| PIN－90 2 | 2 | 17 | 14 | 57 | \％${ }^{\text {\％}}$ \％ | 9 | 5 | 171 | 4.08 | $5$ | 5 | ND | 3 | 19 | \％ 6. | 2 | 3 | 85 | ． 25 | \％080 | 13 | 25 | ． 37 | 26 | 488 | 2 | 3.82 | ． 05 | ． 04 | $\$$ |  |
| PIN－90 3 | 3 | 21 | 16 | 72 | ， | 12 | 8 | 303 | 5.38 | S． | 5 | ND | 2 | 37 | 3 | 4 | 3 | 87 | ． 44 | \％88． | 14 | 24 | ． 57 | 34 | 50 | 2 | 3.73 | ． 14 | ． 08 | ， | 2 |
| STANDARD C／AU－S | 19 | 60 | 39 | 135 | 172 | 72 | 31 | 1058 | 3.98 | 39． | 16 | 7 | 37 | 53 | 18，4 | 16 | 22 | 55 | ． 53 | \％094． | 37 | 60 | ． 90 | 181 | 07. | 40 | 1.90 | ． 06 | ． 14 | 12 | 55 |

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| SAMPLE＊ | $\begin{gathered} \text { Mo } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{pppm} \end{array}$ | Pb ppa | $\begin{array}{r} \mathbf{2 n} \\ \text { pprn } \end{array}$ |  | $\begin{gathered} \mathrm{Ni} \\ \mathrm{pppm} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { pppm } \end{array}$ | Mn <br> ppm | $\begin{gathered} \mathrm{Fe} \\ \boldsymbol{\%} \end{gathered}$ |  | $\begin{array}{r} u \\ \text { pprn } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | Th ppin | $\begin{array}{r} \mathrm{Sr} \\ \mathrm{ppm} \end{array}$ | $\mathrm{F}_{\mathrm{c}}^{\mathrm{cd}}$ | $\begin{array}{r} \mathbf{S b} \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathbf{B i} \\ \mathbf{p p m} \end{array}$ | $\begin{array}{r} V \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \% \end{gathered}$ | $\stackrel{\vartheta}{*}$ | La ppm | $\begin{gathered} \mathrm{Cr} \\ \text { ppm } \end{gathered}$ | $\begin{gathered} \mathrm{Mg} \\ \mathbf{\%} \end{gathered}$ | $\begin{array}{r} \mathbf{B a} \\ \text { ppm } \end{array}$ | $\stackrel{\%}{2}$ | $\begin{array}{r} B \\ \text { ppm } \\ \hline \end{array}$ | $\begin{gathered} A l \\ \chi \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ | $\begin{aligned} & \mathbf{K} \\ & \mathbf{Z} \end{aligned}$ | pront | $\begin{aligned} & A u^{*} \\ & \text { Ppob } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PIN－90 4 | 1 | 25 | 12 | 57 | 2 | 13 | 12 | 390 | 3.84 | 5 | 5 | ND | 1 | 88 | 22 | 2 | 2 | 71 | ． 95 | 064 | 7 | 15 | 1.04 | 49 | $\stackrel{1}{0}$ |  | 1.87 | ． 35 | ． 13 | \％ | 11 |
| PIN－90 5 | 5 | 51 | 24 | 87 | 2． | 12 | 6 | 434 | 6.12 | 4 | 5 | ND | 3 | 23 | 2 | 2 | 2 | 72 | ． 21 | 072 | 17 | 29 | ． 71 | 31 | 37． |  | 3.87 | ． 05 | ． 05 | 寿 | 7 |
| PIN－90 6 | 3 | 45 | 17 | 83 | ， 3 | 13 | 17 | 1277 | 5.90 | 3 | 5 | ND | 3 | 52 | 2 | 2 | 2 | 86 | ． 55 | －087 | 11 | 29 | ． 92 | 42 | 478 |  | 3.51 | ． 18 | ． 09 | ข | 15 |
| PIN－90 7 | 5 | 41 | 16 | 82 | ， 3 ． | 7 | 11 | 2019 | 5.39 | 行 | 5 | ND | 2 | 13 | ， 2 | 2 | 2 | 57 | ． 13 | 080 | 20 | 22 | ． 36 | 25 | 29． |  | 3.21 | ． 05 | ． 06 | \％ | 2 |
| PIN－90 8 | 3 | 47 | 27 | 85 | 数 | 16 | 15 | 630 | 5.40 | 4 | 5 | ND | 2 | 124 | ＊ 4 | 3 | 2 | 92 | 1.28 | 1092． | 12 | 22 | 1.19 | 77 | 6\％ |  | 3.16 | ． 53 | ． 21 | 1 | 1 |
| PIN－90 9 | 2 | 32 | 16 | 54 | 的 | 8 | 6 | 139 | 3.39 | 5 | 5 | ND | 1 | 39 | ． 2 | 2 | 2 | 99 | ． 37 | 060 | 4 | 17 | ． 58 | 35 | 84． |  | 1.76 | ． 09 | ． 05 | 寿 | 7 |
| PIN－90 10 | 3 | 32 | 9 | 75 | ， | 16 | 18 | 632 | 5.15 | 2 | 5 | ND | 1 | 141 | 3 | 2 | 2 | 92 | 1.48 | \＄081 | 6 | 16 | 1.27 | 68 | 68． |  | 2.51 | ． 62 | ． 23 | 1 | 2 |
| PIN－90 11 | 4 | 34 | 17 | 64 | \＆ | 10 | 12 | 523 | 4.76 | \％ | 5 | ND | 1 | 55 | －2 | 2 | 2 | 82 | ． 55 | 1080 | 7 | 15 | ． 75 | 40 | 52． |  | 1.79 | ． 20 | ． 09 | \＆ | 3 |
| PIN－90 12 | 2 | 39 | 6 | 47 | \％ | 9 | 6 | 202 | 5.82 | 2 | 7 | ND | 2 | 23 | 2 | 2 | 2 | 96 | ． 29 | －07\％ | 6 | 20 | ． 61 | 29 | 59\％ |  | 3.15 | ． 04 | ． 03 | 2 | 2 |
| PIN－90 13 | 4 | 43 | 16 | 78 | \％$\%$ | 11 | 7 | 239 | 5.06 | S | 5 | ND | 1 | 31 | ．2 | 2 | 2 | 93 | ． 26 | \％7\％ | 7 | 20 | ． 56 | 34 | 42． | 5 | 1.75 | ． 08 | ． 07 | \＆$\%$ ， | 2 |
| PIN－90 14 | 4 | 41 | 14 | 71 | \％ 1 | 14 | 13 | 583 | 5.74 | 4 | 5 | ND | 2 | 82 | －2 | 2 |  | 104 | ． 82 | －078： | 8 | 23 | ． 97 | 47 | ＊ 67 |  | 2.39 | ． 33 | ． 14 | \％ | 8 |
| PIN－90 15 | 2 | 47 | 6 | 54 | $\geqslant{ }^{\text {\％}}$ | 12 | 9 | 247 | 6.54 | 2 | 7 | ND | 3 | 30 | 4 | 2 | 2 | 110 | ． 33 | 1093． | 6 | 22 | ． 78 | 40 | 83， |  | 3.32 | ． 05 | ． 04 | \％ | 3 |
| SER L．150S 0＋25E | 4 | 131 | 23 | 182 | 44 | 33 | 35 | 1657 | 7.42 | \％ | 5 | ND | 6 | 82 | 1.2 | 2 | 2 | 76 | ． 82 | ， 151 | 19 | 26 | 1.14 | 135 | 4 4 ． |  | 2.80 | ． 32 | ． 18 | 1 | 28 |
| SER L150S 0＋50E | 6 | 201 | 31 | 306 | \％ 2 | 47 | 119 | 7583 | 12.47 | 34 | 7 | ND | 7 | 39 | 2.0 | 2 | 4 | 71 | ． 14 | 5337\％ | 17 | 28 | ． 84 | 191 | 20， |  | 2.50 | ． 04 | ． 07 | 1 | 56 |
| SER L150S 0＋75E | 9 | 165 | 33 | 255 | \％ 4 | 42 | 45 | 3982 | 10.76 | \％ 14 | 5 | ND | 7 | 39 | 1.5 | 2 | 3 | 68 | ． 16 | \＄269 | 19 | 32 | ． 92 | 163 | 23． |  | 2.64 | ． 06 | ． 08 | \＄\％ | 53 |
| SER L1505 1＋00E | 4 | 119 | 31 | 176 | \％${ }^{\circ}$ | 19 | 14 | 1262 | 9.72 | \％ 6 | 5 | ND | 6 | 68 | 13.3 | 3 | 2 | 105 | ． 21 | 240 | 19 | 40 | 1.12 | 189 | ，36． |  | 2.57 | ． 07 | ． 09 | \％1 | 166 |
| SER L150S 1＋25E | 5 | 70 | 22 | 135 | \％ | 18 | 11 | 1041 | 8.10 | ＋10． | 5 | ND | 6 | 37 | \％ 8 | 3 | 2 | 82 | ． 15 | ，89． | 21 | 35 | ． 87 | 105 | 28 |  | 3.28 | ． 06 | ． 07 | \％ | 44 |
| SER LIS0S 1＋50E | 6 | 121 | 23 | 169 | \％ 4 | 24 | 18 | 1605 | 8.41 | 20 | 5 | ND | 7 | 60 | －6 | 2 | 2 | 74 | ． 23 | \＄235 | 17 | 30 | 1.04 | 179 | 30． |  | 3.21 | ． 08 | ． 09 | \％ | 41 |
| SER L1505 1＋75E | 8 | 128 | 25 | 185 | ＊$\%$ | 39 | 24 | 1526 | 7.32 | 15 | 5 | ND | 5 | 61 | \％ | 2 | 2 | 74 | ． 33 | 2336 | 15 | 33 | 1.03 | 193 | \％ 3. |  | 3.74 | ． 11 | ． 09 | \％ | 93 |
| SER L150S 2＋00E | 6 | 124 | 27 | 173 | ＊ 7 \％ | 35 | 23 | 1653 | 8.50 | 24． | 5 | ND | 6 | 60 | 1．0． | 3 | 2 | 85 | ． 25 | 272． | 16 | 37 | 1.05 | 231 | 334． |  | 3.23 | ． 08 | ． 09 |  | 185 |
| SER L150S 2＋25E | 5 | 84 | 44 | 115 | ＊${ }^{\text {\％}}$ | 21 | 13 | 961 | 8.21 | 29． | 5 | ND | 5 | 91 | － 8 | 3 | 5 | 87 | ． 29 | 260 | 12 | 30 | ． 96 | 169 | \％6． | 2 | 1.85 | ． 10 | ． 09 | 很 | 880 |
| SER L150S 2＋50E | 4 | 59 | 172 | 74 | 2， 0 | 11 | 8 | 668 | 7.72 | 40， | 5 | ND | 4 | 171 | ． 6 | 4 | 4 | 128 | ． 36 | 207\％ | 15 | 27 | ． 86 | 330 | 88． | 2 | 1.48 | ． 12 | ． 13 | \％ | 1040 |
| SER L150S 2＋75E | 5 | 49 | 99 | 37 | 1.1 | 5 | 4 | 356 | 6.70 | 24 | 5 | ND | 7 | 167 | \％2 | 2 | 5 | 87 | ． 21 | 2254 | 14 | 18 | ． 50 | 314 | 39． | 3 | ． 90 | ． 05 | ． 09 | 2 | 860 |
| SER L150S 3＋O0E | 6 | 38 | 55 | 63 | \％ 8 | 13 | 9 | 568 | 12.56 | 27 | 5 | ND | 4 | 83 | 1，4 | 2 | 2 | 105 | ． 42 | 4．65 | 6 | 35 | ． 90 | 190 | 09． | 2 | 1.24 | ． 13 | ． 11 | \％ | 690 |
| PEL 90－DS 22 | 42 | 344 | 3 | 97 | \％ 5 | 16 | 77 | 2014 | 13.29 紟 | \％ 4 | 6 | ND | 6 | 8 | 1．9 | 2 | 2 | 37 | ． 07 | ＊61 | 6 | 18 | ． 70 | 22 | 19． | 2 | 5.73 | ． 02 | ． 03 | $\pi_{1}$ | 89 |
| PEL 90－DS 23 | 18 | 300 | 19 | 132 | \％ 7 ， | 11 | 28 | 1067 | 16.64 | 寿 | 5 | ND | 9 | 5 | \％${ }^{2}$ | 3 | 7 | 69 | ． 05 | 4 48 | 13 | 20 | ． 78 | 21 | 22， |  | 2.45 | ． 01 | ． 03 | \％ | 81 |
| PEL 90－DS 24 | 14 | 155 | 11 | 114 | \％ 2 | 20 | 52 | 1830 | 11.10 | 8 | 5 | ND | 6 | 15 | \％ | 2 | 6 | 52 | ． 08 | 578 | 12 | 35 | ． 98 | 60 | 18 |  | 2.22 | ． 02 | ． 05 | \} | 69 |
| PEL 90－DS 25 | 20 | 132 | 10 | 140 | \％2 | 63 | 72 | 1971 | 11.31 | 2 | 5 | ND | 6 | 12 | 1．5 | 2 | 3 | 43 | ． 09 | 324 | 9 | 69 | 1.05 | 36 | 20． | 2 | 1.89 | ． 03 | ． 04 | \％ | 80 |
| PEL 90－DS 26 | 30 | 64 | 11 | 86 | \％${ }^{\text {\％}}$ | 7 | 23 | 1433 | 5.80 | $\underline{6}$ | 5 | ND | 1 | 56 | $\bigcirc 2$ | 2 | 2 | 50 | ． 23 | 170 | 13 | 11 | ． 78 | 41 | 12. |  | 2.48 | ． 02 | ． 06 | ！ | 11 |
| PEL 90－DS 27 | 31 | 87 | 9 | 93 | ， 1 | 6 | 47 | 1628 | 6.60 | 5 | 5 | ND | 2 | 71 | ， 3 | 2 | 2 | 43 | ． 33 | 259 | 8 | 9 | ． 76 | 59 | ，08． | 4 | 2.57 | ． 02 | ． 0 ． |  | 11 |
| PEL 90－DS 28 | 12 | 83 | 17 | 76 | ＋4 | 5 | 20 | 1027 | 6.03 | 7 | 5 | ND | 2 | 48 | ， 2 | 2 | 2 | 56 | ． 17 | 咼 | 17 | 11 | ． 56 | 32 | 18. |  | 3.33 | ． 02 | ． 06 | \％． | 10 |
| PEL 90－DS 29 | 46 | 703 | 55 | 117 | \％ 1.8 | 3 | 49 | 1142 | 11.17 | 62 | 5 | ND | 5 | 49 | \％$\%$ | 2 | 16 | 46 | ． 18 | ， 125 | 11 | 7 | ． 46 | 52 | ， 14 |  | 2.08 | ． 02 | ． 10 | \％ | 18 |
| PEL 90－DS 30 | 6 | 403 | 111 | 135 | ＊${ }^{5}$ | 16 | 13 | 951 | 11.79 | 28 | 5 | ND | 6 | 44 | \％．4 | 2 | 2 | 121 | ． 18 | 174 | 13 | 57 | 1.03 | 64 | 45． | 2 | 3.31 | ． 01 | ． 04 | \％ | 47 |
| PEL 90－DS 31 | 5 | 156 | 65 | 117 | \％ 8. | 12 | 20 | 1113 | 5.78 | $\stackrel{9}{8}$ | 5 | ND | 3 | 37 | ， 2 | 2 | 2 | 62 | ． 26 | 100 | 17 | 23 | ． 68 | 118 | 27， |  | 2.85 | ． 03 | ． 06 | 2 | 17 |
| PEL 90－DS 31 （ A$)$ | 86 | 903 | 96 | 116 | \％${ }^{8}$ | 26 | 157 | 4820 | 13.98 | 178． | 5 | ND | 3 | 35 | 2， | 4 | 8 | 98 | ． 19 | 283 | 4 | 33 | ． 90 | 169 | \％ 32 | 2 | 2.41 | ． 04 | ． 04 | 2 | 65 |
| PEL 90－DS 32 | 18 | 2861 | 276 | 428 | 2．8 | 38 | 65 | 4433 | 8.22 | 92． | 5 | ND | 3 | 39 | 3．9 | 3 | 3 | 81 | ． 36 | 181 | 19 | 29 | ． 89 | 335 | 12\％ |  | 3.04 | ． 04 | ． 08 | ， | 80 |
| STANDARD C／AU－S | 19 | 62 | 42 | 132 | 6．9． | 72 | 31 | 1049 | 3.98 | 39 | 20 | 7 | 40 | 52 | 18．4． | 15 | 19 | 56 | ． 52 | －093 | 38 | 56 | ． 90 | 182 | ．09． | 38 | 1.89 | ． 06 | ． 13 | 13. | 48 |

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| SAMPLE* | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{cu} \\ \text { ppom } \end{gathered}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{ppm} \end{array}$ | $\stackrel{q}{\text { qog }}$ | $\underset{\substack{\mathrm{Ni} \\ \text { ppm }}}{ }$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{array}{r} M n \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \% \end{gathered}$ | $\stackrel{\text { spris }}{\text { pen }}$ | $\begin{array}{r} U \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { pppm } \end{array}$ | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p m} \end{array}$ | $\begin{gathered} \text { col } \\ \text { ppm, } \end{gathered}$ | $\begin{array}{r} \text { Sb } \\ \text { pppm } \end{array}$ | $\begin{gathered} \text { Bi } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} V \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \boldsymbol{\%} \end{gathered}$ | $\stackrel{\otimes}{\mathrm{F}},$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppm} \end{gathered}$ | $\begin{aligned} & \text { Mg } \\ & \text { \% } \end{aligned}$ | $\begin{array}{r} \mathbf{B a} \\ \mathrm{ppm} \end{array}$ | $\sum_{8} \boldsymbol{q}_{1},$ | $\begin{array}{r} 8 \\ \text { ppom } \end{array}$ | A! | $\begin{gathered} \mathrm{Na} \\ \mathrm{Z} \end{gathered}$ | $\begin{aligned} & K \\ & \boldsymbol{z} \end{aligned}$ | $\sum_{i+1}$ | $\begin{aligned} & \mathrm{A} \mathbf{u}^{\star} \\ & \mathrm{ppb} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1460-1 | 6 | 178 | 45 | 125 | 2.4 | 20 | 12 | 977 | 10.01 | 39. | 5 | ND | 6 | 135 | 8 | 2 | 2 | 123 | . 32 | 432 | 22 | 25 | 1.05 | 322 | \$ 30 | 2 | 2.34 | . 16 | . 22 | , \% | 500 |
| 1460-2 | 9 | 406 | 28 | 154 | \% 1 | 39 | 70 | 3093 | 9.55 | 31 | 6 | ND | 12 | 71 | 12\% | 4 | 6 | 104 | . 21 | 383 | 26 | 31 | . 96 | 218 | 28 | 2 | 3.99 | . 09 | . 07 | 1 | 320 |
| 1460-3 | 5 | 93 | 29 | 91 | 1,8 | 12 | 7 | 658 | 7.53 | 40 | 5 | ND | 3 | 68 | \% 4 | 2 | 2 | 109 | . 11 | \%229 | 12 | 23 | . 88 | 299 | 27. | 2 | 2.24 | . 03 | . 06 | ¢ | 310 |
| 1460-4 | 3 | 103 | 83 | 107 | 2. 6 | 11 | 8 | 1048 | 9.08 | 185 | 5 | 2 | 8 | 133 | 8. | 3 | 2 | 178 | . 22 | \%24 | 20 | 20 | . 94 | 269 | 4.4. | 6 | 2.01 | . 09 | . 14 | \% 1 | 4540 |
| 1460-5 | 2 | 45 | 188 | 58 | 3, 1 | 6 | 5 | 476 | 6.20 | 218. | 5 | ND | 6 | 349 | ,2. | 5 | 2 | 152 | . 26 | , 185 | 47 | 13 | . 70 | 398 | , 54. | 21 | . 91 | . 09 | . 13 | < | 2260 |
| 1460-6 | 7 | 56 | 32 | 68 | 1 | 14 | 11 | 594 | 8.06 | 44 | 5 | ND | 9 | 223 | \% | 2 | 2 | 115 | . 35 | 432 | 26 | 22 | . 83 | 628 | \% 32 | 4 | 1.78 | . 17 | . 12 | 1 | 430 |
| 1460-7 | 6 | 48 | 436 | 28 | 3.0 | 3 | 7 | 356 | 4.09 | 77 | 5 | 2 | 7 | 431 | \% 2 | 3 | 4 | 98 | . 23 | , 7 | 41 | 10 | . 33 | 557 | \% 60 | 6 | . 65 | . 05 | . 07 | , \% | 3080 |
| 1460-8 | 5 | 51 | 85 | 59 | \%18 | 10 | 4 | 384 | 5.90 | 31 | 5 | NO | 7 | 198 | 2 | 2 | 2 | 83 | . 10 | 248 | 21 | 31 | . 75 | 415 | +35 | 7 | 1.26 | . 08 | . 10 | \% | 470 |
| 1460-9 | 6 | 64 | 108 | 61 | 24. | 8 | 4 | 418 | 5.16 | 30. | 5 | ND | 5 | 238 | 2 | 2 | 2 | 90 | . 21 | \$239 | 20 | 21 | . 64 | 401 | S 50 | 6 | 1.05 | . 07 | . 16 |  | 2110 |
| 1460-10 | 15 | 76 | 61 | 80 | 就, | 15 | 5 | 436 | 8.28 | 31. | 5 | ND | 5 | 122 | . 2 | 2 | 3 | 190 | . 19 | 226 | 12 | 39 | . 93 | 300 | . 53 | 2 | 2.57 | . 08 | . 11 | \% | 670 |
| 1460-11 | 8 | 81 | 34 | 122 | \% $\% 4$ | 22 | 9 | 1388 | 7.17 | 22 | 5 | ND | 4 | 88 | \% | 2 | 2 | 101 | . 10 | 2\% | 19 | 41 | . 88 | 425 | , 24 | 5 | 3.48 | . 04 | . 08 | 1 | 135 |
| 1460-12 | 4 | 106 | 53 | 84 | \% | 31 | 9 | 366 | 11.89 | 71 | 5 | ND | 4 | 113 | 8. | 2 | 2 | 127 | . 21 | 61\% | 13 | 61 | . 88 | 189 | 13. | 2 | 1.62 | . 13 | . 15 | \% | 270 |
| 1460-13 | 7 | 142 | 22 | 94 | \% 0 | 23 | 8 | 503 | 12.02 | 152 | 5 | ND | 5 | 109 | , 4 | 2 | 6 | 125 | . 15 | 503 | 13 | 71 | . 73 | 222 | 25. | 2 | 1.62 | . 09 | . 08 | \% | 102 |
| 1460-14 | 3 | 267 | 24 | 156 | \% 1 \% | 37 | 13 | 605 | 12.98 | 99 | 5 | ND | 4 | 106 | \% | 2 | 6 | 165 | . 17 | 542 | 10 | 71 | . 93 | 170 | *27 | 2 | 2.34 | . 04 | . 07 | , | 115 |
| 1460-15 | 7 | 270 | 46 | 116 | \%22 | 19 | 12 | 633 | 10.77 | 185. | 5 | ND | 4 | 306 | 1.3.3 | 3 | 2 | 153 | . 24 | 349. | 24 | 57 | . 79 | 224 | 27, | 2 | 1.72 | . 14 | . 13 | \% | 290 |
| 1460-16 | 3 | 272 | 27 | 148 | 12 | 30 | 18 | 1032 | 9.88 | 89\% | 5 | ND | 4 | 91 | \% + | 2 | 2 | 129 | . 26 | \$67 | 13 | 62 | 1.10 | 150 | \% 27. | 2 | 2.43 | . 07 | . 09 | \% $\%$ | 108 |
| 1460-17 | 3 | 187 | 36 | 166 | 1 1\% | 29 | 10 | 691 | 7.72 | 57 | 5 | ND | 3 | 66 | * 5 , | 3 | 2 | 112 | . 17 | 240 | 16 | 34 | . 95 | 124 | 23. | 4 | 2.47 | . 05 | . 06 | \% | 111 |
| 1460-18 | 3 | 117 | 44 | 111 | \% 10 | 14 | 9 | 1606 | 8.89 | 65. | 5 | ND | 2 | 78 | . 6 | 4 | 2 | 138 | . 15 | $\geqslant 220$ | 12 | 48 | . 81 | 209 | 19. | 3 | 2.07 | . 02 | . 10 | 1. | 65 |
| 1460-19 | 3 | 196 | 47 | 225 | \%\% | 31 | 16 | 1527 | 7.72 | 65. | 5 | ND | 4 | 90 | *3. | 3 | 2 | 92 | . 14 | +336 | 20 | 38 | 1.07 | 615 | - 26 | 4 | 2.65 | . 02 | . 09 | \% | 141 |
| 1460-20 | 5 | 403 | 66 | 264 | 12 | 38 | 43 | 2196 | 7.66 | 57. | 5 | ND | 7 | 76 | 1.2 | 2 | 2 | 104 | . 20 | \$329 | 24 | 41 | 1.20 | 327 | \$32. | 3 | 3.40 | . 04 | . 11 |  | 164 |
| 1460-21 | 3 | 533 | 83 | 233 | \% $\%$ | 34 | 34 | 2049 | 8.72 | 49. | 5 | ND | 6 | 114 | 1, 6 | 2 | 2 | 111 | . 24 | 319 | 21 | 56 | 1.21 | 303 | \% 30 | 2 | 2.75 | . 06 | . 11 | < | 109 |
| 1460-22 | 3 | 415 | 172 | 286 | 3 3 | 35 | 44 | 3134 | 10.41 | 94 | 5 | ND | 6 | 54 | 2.3. | 4 | 2 | 129 | . 19 | 44t | 11 | 58 | 1.55 | 199 | 24. | 2 | 3.37 | . 02 | . 15 | ¢ | 123 |
| 1460-23 | 4 | 237 | 49 | 170 | \% 10 | 27 | 38 | 2707 | 9.40 | 68 | 5 | ND | 8 | 56 | 1.0 | 2 | 3 | 112 | . 26 | 576 | 15 | 49 | 1.33 | 127 | 29. | 2 | 3.37 | . 08 | . 13 | 1 | 83 |
| 1460-24 | 6 | 92 | 74 | 107 | 1, 3 | 14 | 8 | 853 | 7.12 | 30 | 5 | ND | 7 | 45 | \% 2 | 2 | 2 | 76 | . 09 | 180 | 27 | 28 | . 86 | 248 | .24. | 4 | 2.81 | . 03 | . 06 | 1 | 94 |
| 1460-25 | 5 | 107 | 31 | 126 | \% + \% | 19 | 11 | 943 | 7.18 | 35. | 5 | ND | 8 | 72 | . 2 | 2 | 2 | 83 | . 20 | 220 | 22 | 27 | 1.00 | 283 | . 30 | 4 | 2.25 | . 08 | . 10 | \% | 101 |
| 1460-26 | 4 | 75 | 35 | 101 | 1.2 | 12 | 7 | 610 | 6.28 | 19 | 5 | ND | 7 | 88 | 2 | 2 | 2 | 66 | . 12 | $\stackrel{223}{ }$ | 25 | 18 | . 82 | 401 | 24. | 5 | 1.48 | . 06 | . 10 | 1 | 68 |
| 1460-27 | 8 | 55 | 25 | 88 | 1.5 | 13 | 12 | 570 | 6.58 | 24 | 5 | ND | 6 | 102 | .2. | 2 | 2 | 62 | . 37 | 228 | 18 | 12 | . 81 | 331 | , 26 | 5 | 1.28 | . 16 | . 15 | 碞 | 30 |
| 1460-28 | 7 | 59 | 25 | 89 | \% 1 4 | 12 | 11 | 589 | 6.38 | 23 | 5 | ND | 6 | 96 | $\stackrel{2}{ }$ | 2 | 2 | 56 | . 33 | -227 | 18 | 11 | . 75 | 290 | $\stackrel{26}{ }$ | 5 | 1.26 | . 14 | . 14 | \% | 26 |
| 1460-29 | 5 | 123 | 61 | 145 | 2,2 | 18 | 10 | 1001 | 7.28 | 40 | 5 | ND | 6 | 76 | 3 | 2 | 2 | 81 | . 11 | 8186 | 18 | 32 | 1.00 | 649 | +28 |  | 2.46 | . 03 | . 11 | , | 150 |
| 1460-30 | 4 | 41 | 47 | 54 | 2.2 | 5 | 3 | 328 | 4.79 | 2\% | 5 | ND | 6 | 106 | \% | 2 | 2 | 34 | . 04 | 2665 | 24 | 6 | . 41 | 466 | $\stackrel{18}{ }$ | 5 | . 85 | . 03 | . 10 | \% | 29 |
| 1500-1 | 6 | 164 | 20 | 111 | \% | 21 | 12 | 965 | 8.45 | 16 | 5 | ND | 7 | 90 | 1.0 | 2 | 2 | 111 | . 29 | 347 | 17 | 25 | 1.04 | 223 | < 32 | 2 | 2.38 | . 12 | . 13 | 2 | 97 |
| 1500-2 | 6 | 258 | 42 | 177 | §\% | 25 | 16 | 1260 | 9.77 | 16 | 5 | ND | 7 | 78 | < 0 | 2 | 2 | 105 | . 13 | 374 | 18 | 31 | 1.06 | 237 | 24. | 2 | 2.48 | . 05 | . 08 | \% | 200 |
| 1500-3 | 6 | 293 | 23 | 185 | \% ${ }^{5}$ | 35 | 29 | 1763 | 8.85 | 23. | 5 | ND | 8 | 54 | \$12. | 3 | 5 | 110 | . 12 | \% 86 | 19 | 25 | 1.05 | 170 | -28 | 2 | 2.80 | . 05 | . 07 | \% | 73 |
| 1500-4 | 6 | 254 | 34 | 169 | , | 32 | 25 | 1571 | 9.83 | \% 15 | 5 | ND | 8 | 57 | 12 | 3 | 2 | 123 | . 13 | \$449 | 17 | 34 | 1.06 | 199 | 26. |  | 2.97 | . 07 | . 09 | \% | 64 |
| 1500-5 | 6 | 255 | 31 | 220 | \& $\downarrow$ | 39 | 31 | 1572 | 12.70 | \%69 | 5 | ND | 8 | 48 | 43, | 5 | 2 | 84 | . 16 | \$498 | 17 | 21 | . 83 | 139 | +18. | 2 | 1.77 | . 08 | . 06 | \$ | 330 |
| 1500-6 | 6 | 117 | 43 | 139 | § 1 | 27 | 12 | 905 | 9.66 | 42 | 5 | ND | 8 | 63 | $\stackrel{9}{ }$ | 3 | 2 | 88 | . 12 | 4 45 | 19 | 27 | . 95 | 259 | 25. | 2 | 2.20 | . 06 | . 07 | 1. | 210 |
| STANDARD C/AU-S | 20 | 65 | 41 | 134 | 6.7. | 74 | 33 | 1050 | 3.98 | 42 | 20 | 7 | 40 | 54 | 18.6. | 15 | 21 | 57 | . 52 | \%097. | 49 | 59 | . 90 | 182 | -09. | 40 | 1.89 | . 07 | . 13 | 12 | 46 |

Cathedral Gold Corp．PROJECT 8103 FILE \＃90－4553
Page 6

| SAMPLE\＃ | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{pppm} \end{array}$ | $\begin{array}{r} \mathrm{Pb} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} 2 n \\ \text { ppm } \end{array}$ | $\stackrel{\pi}{\text { ipg }}$ | $\begin{gathered} \mathrm{Ni} \\ \mathrm{pppm} \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Mn} \\ \mathrm{ppm} \end{gathered}$ | $\begin{aligned} & \mathrm{Fe} \\ & \boldsymbol{X} \end{aligned}$ | $\begin{aligned} & \text { iss } \\ & \text { ip } \end{aligned}$ | $\begin{array}{r} \mathbf{u} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{aligned} & \text { Th } \\ & \text { ppm } \end{aligned}$ | $\begin{gathered} \mathbf{S r} \\ \mathbf{p p m} \end{gathered}$ | $\stackrel{\operatorname{cod}}{ }$ \#pomp | $\begin{array}{r} \text { sb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathbf{B i} \\ \text { ppin } \end{array}$ | $\begin{array}{r} v \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \boldsymbol{z} \end{gathered}$ | $\boldsymbol{*}$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cr} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Mg} \\ \% \end{gathered}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | $\text { } \gtrless_{i}, \frac{1}{2}$ | $\begin{array}{r} B \\ \text { ppm } \\ \hline \end{array}$ | $\begin{gathered} A! \\ \boldsymbol{x} \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \mathbf{\%} \end{gathered}$ | $\begin{aligned} & k \\ & \chi \end{aligned}$ |  | $\begin{aligned} & \mathbf{A \mathbf { u } ^ { \star }} \\ & \mathbf{p p b} \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1500－7 | 4 | 63 | 134 | 125 | 2.6 | 17 | 9 | 891 | 8.08 | $10 \%$ | 5 | ND | 1 | 82 | ．2 | 3 | 5 | 71 | ． 21 | 37\％ | 16 | 29 | 1.24 | 297 | \＄ 30 | 2 | 1.81 | ． 08 | ． 13 | 的 | 220 |
| 1500－8 | 3 | 70 | 60 | 78 | 7\％ | 16 | 7 | 486 | 11.03 | 130 | 5 | ND | 1 | 69 | ， | 2 | 4 | 95 | ． 29 | \％ 381 | 9 | 61 | ． 87 | 196 | \％ 26 | 2 | 1.51 | ． 11 | ． 10 | \％ | 153 |
| 1500－9 | 1 | 39 | 28 | 86 | 1＊1 | 12 | 7 | 1381 | 6.19 | 25 | 5 | ND | 1 | 77 | \％ 6 | 2 | 2 | 104 | ． 29 | 188 | 9 | 37 | ． 81 | 218 | \％ 25 | 4 | 1.34 | ． 05 | ． 09 | 行 | 32 |
| 1500－10 | 3 | 55 | 57 | 96 | 2 | 13 | 6 | 652 | 8.15 | 40 | 5 | MD | 2 | 88 | ， 2 | 4 | 2 | 98 | ． 15 | 278 | 17 | 33 | ． 74 | 188 | 27， | 3 | 2.26 | ． 06 | ． 09 | \％ | 50 |
| 1500－11 | 1 | 23 | 27 | 72 | ๗1 | 13 | 8 | 454 | 4.98 | 15 | 5 | ND | 1 | 48 | ，2 | 2 | 4 | 78 | ． 29 | \＄123 | 8 | 22 | ． 63 | 101 | \％2\％ | 6 | 1.76 | ． 07 | ． 06 | $\mathbb{\$}$ | 29 |
| 1500－12 | 1 | 75 | 47 | 147 | 1－2 | 26 | 13 | 730 | 7.59 | 28 | 5 | ND | 1 | 84 | ，2 | 2 | 2 | 94 | ． 39 | 230 | 14 | 37 | 1.18 | 216 | \＄30． |  | 2.26 | ． 14 | ． 12 | \％ | 28 |
| 1500－13 | 3 | 83 | 26 | 136 | 数 | 20 | 5 | 508 | 6.25 | 30 | 5 | ND | 1 | 44 | 家 | 2 | 2 | 59 | ． 10 | \％179 | 16 | 32 | ． 82 | 146 | 雱， |  | 2.58 | ． 02 | ． 05 | \％ 1 | 29 |
| 1500－14 | 3 | 433 | 25 | 493 | \％$\%$ | 53 | 49 | 2572 | 12.21 | 78 | 5 | MD | 1 | 53 | 4， | 2 | 2 | 41 | ． 22 | \％ 628 | 11 | 47 | 1.10 | 493 | ， 8 \％ | 2 | 5.55 | ． 08 | ． 09 | \％ 1 | 23 |
| 1500－15 | 1 | 188 | 57 | 272 | 1上 | 27 | 34 | 2466 | 10.78 | 93． | 5 | MD | ， | 46 | $\stackrel{2}{2}$ | 2 | 2 | 102 | ． 21 | 428 | 10 | 54 | 1.55 | 235 | 23． | 2 | 3.15 | ． 05 | ． 09 | ＊1 | 26 |
| 1500－16 | 3 | 33 | 32 | 76 | \％ | 10 | 3 | 374 | 4.61 | 17 | 5 | ND | 1 | 23 | \％ 2 | 2 | 2 | 57 | ． 09 | \＄092 | 14 | 27 | ． 52 | 87 | \％ 17 | 6 | 2.48 | ． 02 | ． 04 | \％ | 14 |
| 1500－17 | 3 | 64 | 36 | 111 | 1．5 | 15 | 10 | 873 | 6.94 | 32 | 5 | ND | 1 | 41 | \％2． | 2 | 2 | 62 | ． 19 | \％6\％ | 17 | 29 | ． 84 | 120 | 21． |  | 2.64 | ． 07 | ． 08 | 1 | 36 |
| 1500－18 | 1 | 212 | 134 | 342 | 12， | 30 | 44 | 2606 | 9.34 | 87 | 5 | ND | 1 | 47 | ． 5. | 3 | 2 | 85 | ． 39 | 3 303 | 12 | 43 | 1.89 | 74 | 24． |  | 3.08 | ． 03 | ． 08 | ＜ | 26 |
| 1500－19 | 1 | 194 | 44 | 125 | ＊ 8 | 12 | 9 | 865 | 10.23 | 32 | 5 | ND | 1 | 45 | \％ 2 | 2 | 2 | 72 | ． 09 | \％187 | 17 | 43 | ． 80 | 120 | 16． |  | 2.69 | ． 01 | ． 05 | \％ | 48 |
| 4500－20 | 1 | 118 | 25 | 122 | \％ | 18 | 14 | 1039 | 9.18 | 37 | 5 | ND | 2 | 70 | \＄ 2. | 2 | 2 | 77 | ． 15 | 27\％ | 15 | 40 | 1.10 | 145 | 29． |  | 2.43 | ． 04 | ． 0 | \％ | 24 |
| 1500－21 | 2 | 87 | 33 | 119 | $\ddot{10}$ | 19 | 14 | 930 | 7.73 | 36 | 5 | ND | 2 | 84 | \％ 2 | 2 | 2 | 70 | ． 24 | \％22 | 17 | 30 | 1.06 | 178 | \％28 | 3 | 2.05 | ． 08 | ． 10 | ＜ | 26 |
| 1500－22 | 2 | 137 | 27 | 121 | \％ | 24 | 20 | 1228 | 8.79 | 48 | 5 | ND | 1 | 88 | 3 | 2 | 2 | 70 | ． 25 | \＄69 | 11 | 40 | 1.21 | 213 | \％24． |  | 2.06 | ． 06 | ． 08 | \％ | 48 |
| 1500－23 | 2 | 57 | 27 | 95 | 令 | 18 | 12 | 708 | 7.86 | 23 | 5 | ND | 2 | 80 | \％ 2 | 2 | 2 | 75 | ． 42 | 205 | 14 | 30 | 1.24 | 188 | 3 3 \％ |  | 2.01 | ． 16 | ． 13 | \％ | 66 |
| 1500－24 | 2 | 98 | 25 | 129 | \％$\%$ | 17 | 11 | 1075 | 7.91 | 30 | 5 | ND | 2 | 64 | 2 | 3 | 2 | 65 | ． 17 | 241 | 16 | 27 | 1.08 | 251 | 23． | 3 | 2.21 | ． 05 | ． 10 | \％ | 128 |
| 1500－25 | 2 | 90 | 34 | 132 | \％${ }^{\text {\％}}$ | 19 | 12 | 934 | 8.28 | 31 | 5 | ND | 2 | 74 | \％ | 2 | 2 | 69 | ． 31 | 216 | 19 | 30 | 1.24 | 186 | －29． |  | 2.23 | ． 11 | ． 11 | \％ | 33 |
| 1500－26 | 1 | 35 | 24 | 83 | 紂 | 10 | 7 | 505 | 6.06 | 2\％ | 5 | ND | 3 | 82 | 相 | 2 | 2 | 46 | ． 22 | 194 | 17 | 15 | ． 73 | 274 | 20． | 4 | 1.33 | ． 08 | ． 11 | 行 | 10 |
| 1500－27 | 8 | 30 | 28 | 69 | ＋4． | 5 | 5 | 372 | 6.59 | 30 | 7 | ND | 2 | 97 | ， | 2 | 3 | 29 | ． 13 | ¢259 | 15 | 5 | ． 34 | 267 | 15． | 3 | ． 82 | ． 03 | ． 11 | ไ | 10 |
| 1500－28 | 4 | 67 | 29 | 114 | \％ 1 | 5 | 12 | 1153 | 7.20 | 28 | 5 | ND | 2 | 65 | \％ | 2 | 3 | 30 | ． 11 | 227 | 13 | 9 | ． 49 | 250 | \％ 16 | 3 | 1.08 | ． 04 | ． 09 | ィ | 15 |
| 1500－29 | 2 | 49 | 39 | 109 | 2， | 6 | 7 | 502 | 6.32 | 28 | 5 | ND | 3 | 67 | \％ 2 | 2 | 2 | 26 | ． 08 | 230 | 15 | 6 | ． 37 | 288 | 18. | 3 | ． 81 | ． 03 | ． 09 | \％ | 14 |
| 1500－30 | 2 | 32 | 43 | 64 | シ， 5 | 4 | 4 | 494 | 5.30 | 23 | 5 | ND | 3 | 101 | \％ 3 | 2 | 2 | 30 | ． 05 | 221 | 17 | 6 | ． 40 | 377 | \％18 | 4 | ． 81 | ． 03 | ． 10 | 2 | 23 |
| PIN－J－8－1 | 12 | 235 | 35 | 141 | $\%$ | 67 | 66 | 1588 | 8.82 | 14 | 5 | ND | 5 | 94 | \％ 3 ， | 2 | 2 | 57 | ． 11 | 5337 | 23 | 76 | 1.18 | 679 | 109 | 2 | 3.98 | ． 03 | ． 12 |  | 6 |
| PIN－J－B－2 | 34 | 259 | 34 | 94 | \％ 4 | 32 | 68 | 1577 | 12.70 | 17 | 5 | ND | 5 | 28 | ， 2 |  | 2 | 47 | ． 04 | ＋401 | 18 | 50 | ． 96 | 699 | ， 0 \％ |  | 3.10 | ． 01 | ． 09 | \％ | 8 |
| PIN－J－B－3 | 18 | 574 | 456 | 318 | \％ 4 | 62 | 73 | 1969 | 8.89 | 59 | 5 | ND | 2 | 47 | ， 4 | 5 | 2 | 80 | ． 33 | 224 | 20 | 108 | 1.41 | 550 | \％ 08 | 2 | 3.51 | ． 01 | ． 09 | 1 | 29 |
| PIN－J－8－4 | 26 | 467 | 36 | 60 | ， 4 | 17 | 35 | 818 | 9.20 | 9. | 10 | ND | 12 | 34 | $\stackrel{3}{ }$ | 2 | 2 | 12 | ． 04 | 461 | 29 | 8 | ． 31 | 560 | \％ 01 | 3 | 2.71 | ． 01 | ． 04 | \＄ | 12 |
| STANDARD C／AU－S | 18 | 58 | 40 | 131 | 6．8． | 70 | 32 | 1055 | 3.98 | 39. | 18 | 7 | 36 | 52 | 18．4． | 15 | 21 | 55 | ． 52 | 1094． | 35 | 58 | ． 89 | 179 | ，07． | 41 | 1.89 | ． 06 | ． 14 | 12 | 45 |

Cathedral Gold Corp．PROJECT 8103 FILE \＃90－4553

| SAMPLE＊ | $\begin{array}{r} \text { Mo } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Pb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Zn} \\ \mathrm{ppm} \end{array}$ | $\sum_{\mathrm{r} \rho \mathrm{p}}^{\mathrm{g}} \mathrm{~g}$ |  | $\begin{gathered} \text { Co } \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \text { Mn } \\ \text { pppn } \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \boldsymbol{\alpha} \end{gathered}$ |  | $\begin{array}{r} \mathrm{U} \\ \text { ppin } \end{array}$ | $\begin{array}{r} \mathrm{Au} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} \text { Th } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathbf{S r} \\ \mathbf{p p m} \end{array}$ |  | $\begin{array}{r} \text { Sb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Bi } \\ \text { ppm } \end{array}$ | $\begin{array}{r} v \\ p p m \end{array}$ | $\begin{aligned} & \mathbf{e a} \\ & \mathbf{x} \end{aligned}$ | $\stackrel{\otimes}{\forall}$ | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{gathered} \mathrm{Cr} \\ \mathrm{ppm} \end{gathered}$ | $\begin{gathered} \mathrm{Mg} \\ \mathbf{\%} \end{gathered}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | $\hat{8}$ | $\begin{array}{r} \mathbf{B} \\ \text { ppm } \end{array}$ | $\begin{array}{r} \text { Al } \\ \mathbf{x} \end{array}$ | $\begin{gathered} \mathrm{Na} \\ \mathrm{Z} \end{gathered}$ | $\begin{aligned} & \mathrm{K} \\ & \mathbf{\chi} \end{aligned}$ | $\gtrless_{\mathrm{p}}^{\mathrm{n}} \mathrm{H}$ | $\begin{aligned} & \mathbf{A u ^ { * }} \\ & \text { ppb } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL－90－G－54R | 26 | 197 | 13 | 108 | \％ | 12 | 12 | 1205 | 7.90 | \％ | 5 | ND | 2 | 4 | 88 | 11 | 2 | 59 | ． 25 | \％93 | 6 | 32 | 1.95 | 53 | \％ 19 |  | 5.03 | ． 01 | ． 10 | 3 | 55 |
| PEL－90－G－5 | 21 | 241 | 14 | 126 | \％ | 20 | 60 | 2619 | 7.12 | 2 | 5 | ND | 1 | 9 | 4 |  | 2 | 57 | ． 64 | ¢198 | 8 | 27 | 2.12 | 77 | \％12 | 3 | 5.65 | ． 01 | ． 08 | 1 | 12 |
| PEL－90－G－56R | 3 | 9 | 6 | 78 | \％ | 5 | 3 | 719 | 4.89 | \％ | 5 | ND | 4 | 6 | ， 2 | 2 | 2 | 26 | ． 20 | 174 | 6 | 16 | 1.22 | 104 | \％05． | 3 | 1.36 | ． 01 | ． 16 | 4 | 7 |
| PEL－90－G－57R | 6 | 33 | 18 | 14 |  | 6 | 4 | 162 | 2.30 | 16 | 5 | ND | 3 | 7 | $\stackrel{*}{*}$ | 2 | 2 | 7 | ． 10 | 103\％ | 2 | 8 | ． 18 | 37 | \％0\％ | 5 | ． 55 | ． 01 | ． 14 | ¢ | 4 |
| PEL－90－G－58R | 3 | 39 | 9 | 30 |  | 5 | 7 | 217 | 2.00 | 3 | 5 | ND | 4 | 14 | \％$\%$ | 2 | 2 | 13 | ． 21 | \＄035 | 14 | 8 | ． 41 | 37 | \％ 0 \％ | 3 | ． 81 | ． 03 | ． 10 |  | 5 |
| PEL－90－G－58R（A） | 29 | 802 | 12 | 86 | 3， 3 | 1 | 61 | 258 | 28.35 | \％13 | 12 | ND | 4 | 35 | \％ 2 | 4 | 13 | 30 | ． 19 | \％ 052 | 2 |  | ． 38 | 24 | 09． | 5 | 1.45 | ． 01 | ． 08 | \％ | 10 |
| PEL－90－6－60R | 22 | 87 | 26 | 42 | 1， | 1 | 48 | 328 | 7.33 | \％ 23 | 5 | MD | 1 | 230 | ＊2 | 2 | 2 | 19 | 1.02 | 070 | 3 | 13 | ． 40 | 42 | \％ 07 | 2 | 1.37 | ． 01 | ． 14 | ＊ | 7 |
| PEL－90－6－61R | 86 | 133 | 57 | 55 | 1.5 | 3 | 72 | 689 | 9.26 | 43 | 5 | ND | 1 | 199 | ，${ }^{3}$ | 3 | 5 | 21 | ． 75 | \％67\％ | 2 | 12 | ． 44 | 60 | \％06 | 2 | 1.53 | ． 01 | ． 21 | \％ | 7 |
| PEL－90－G－62R | 5 | 11 | 10 | 19 | － | 11 | 2 | 221 | ． 90 | 4 | 12 | MD | 1 | 13 | 苼 | 2 | 2 | 2 | ． 03 | 019 | 2 | 10 | ． 11 | 16 | 时 | 4 | ． 29 | ． 01 | ． 03 | 行 | 3 |
| PEL－90－G－62R（A） | 9 | 156 | 7 | 48 | 1， | 2 | 18 | 839 | 8.02 | \％ 19 | 5 | ND | 1 | 153 | \％$\%$ | 3 | 2 | 32 | ． 61 | \％480 | 4 | 13 | 1.35 | 24 | \％ 10 | 3 | 2.37 | ． 01 | ． 09 |  | 8 |
| PEL－90－6－63R | 7 | 20 | 81 | 8 | 346 | 10 | 2 | 91 | 2.30 | 9 | 5 | ND | 1 | 57 | －2 | 2 | 4 | 14 | ． 16 | \％18 | 2 | 59 | ． 05 | 187 | 䊉 | 2 | ． 19 | ． 01 | ． 03 | ， | 7 |
| PEL－90－G－64R | 4 | 1751 | 24 | 112 | 98． | 24 | 28 | 1238 | 5.63 | 10 | 5 | ND | 1 | 112 | \％ 4 | 5 | 2 | 70 | ． 91 | 139 | 6 | 44 | 2.16 | 31 | 2\％ | 3 | 2.12 | ． 01 | ． 02 | \％ | 45 |
| PEL－90－G－65R | 1 | 96 | 264 | 141 | 3．2 | 27 | 20 | 1536 | 5.96 | 36 | 5 | ND | 1 | 288 | \％ 4 | 6 | 6 | 89 | ． 99 | 210 | 6 | 59 | 3.21 | 28 | \％ 24 | 2 | 2.90 | ． 01 | ． 01 | 2 | 22 |
| PEL－90－G－66R | 7 | 75 | 35 | 22 | 1，6． | 6 | 7 | 184 | 4.75 | 44 | 5 | ND | 1 | 69 | \％$\%$ | 2 | 3 | 39 | ． 24 | －050 | 2 | 24 | ． 28 | 294 | 19． | 5 | ． 53 | ． 01 | ． 02 | \％ | 15 |
| \|PEL-90-G-67R | 5 | 29 | 93 | 111 | 2\％ | 17 | 25 | 1481 | 10.12 | 27 | 5 | ND | 1 | 90 | \％ 2 | 6 | 2 | 112 | ． 97 | 275 | 13 | 73 | 2.72 | 88 | \％ 30 | 2 | 3.13 | ． 01 | ． 08 | 2． | 27 |
| PEL－90－6－68R | 5 | 4835 | 68 | 98 | 4．3． | 42 | 8 | 1233 | 4.05 | \％ 4 | 5 | ND | 1 | 86 | －5 | 2 | 2 | 30 | ． 78 | g101 | 11 | 28 | 1.56 | 1054 | O7． | 2 | 2.03 | ． 01 | ． 11 | 寿 | 5 |
| PEL－90－6－69R | 6 | 9866 | 88 | 53 | 9．9 | 26 | 5 | 1078 | 2.39 | \％ | 5 | MD | 1 | 112 | \％ 8 | 2 | 3 | 28 | 1.14 | 809\％ | 12 | 17 | ． 78 | 747 | 07 | 2 | 1.33 | ． 01 | ． 13 | 1 | 2 |
| PEL－90－G－70R | 1 | 455 | 11 | 182 | \％ | 34 | 12 | 1841 | 3.66 | 3 | 5 | ND | 1 | 99 |  | 3 | 2 | 28 | 1.88 | 123 | 15 | 31 | 1.79 | 280 | 05． | 2 | 2.39 | ． 01 | ． 14 | ＊ | 5 |
| PEL－90－G－71R | 4 | 121 | 59 | 118 | 1．6． | 24 | 24 | 1298 | 9.55 | 152 | 5 | ND | 2 | 112 | ，${ }_{\text {\％}}$ | 11 | 2 | 97 | 1.19 | \％ 305 | 11 | 86 | 2.28 | 64 | ， 34 | 3 | 2.80 | ． 01 | ． 05 | \％ 2 | 45 |
| PEL－90－6－72R | 4 | 407 | 4 | 145 | ，${ }^{3}$ | 11 | 10 | 981 | 1.72 | 5. | 5 | ND | 1 | 65 | \％ | 2 |  | 17 | ． 45 | 04\％ | 3 | 12 | ． 47 | 143 | 04． | 3 | ． 85 | ． 01 | ． 02 | 1 | 55 |
| PEL－90－G－ | 1 | 2219 | 40 | 87 | 3．0 | 17 | 16 | 1894 | 7.51 | 2 | 5 | ND | 1 | 92 | 6． | 6 | 2 | 79 | ． 98 | ， 158 | 6 | 24 | 3.32 | 192 | 10． | 2 | 3.89 | ． 01 | ． 06 | 1 | 5 |
| PEL－90－6－74R | 19 | 4986 | 112 | 290 | 6．8 | 7 | 15 | 627 | 2.04 | 6 | 5 | ND | － | 363 | 4．5 | 2 | 2 | 25 | 2.08 | 192 | 6 | 10 | ． 20 | 92 | 10 | 5 | 1.25 | ． 01 | ． 08 | 1 | 11 |
| PEL－90－G－75R | 1 | 4663 | 119 | 266 | 4．7， | 78 | 16 | 1813 | 5.08 | 3 | 5 | ND | ， | 51 | Y\％ | 2 | 2 | 26 | 2.25 | 128 | 8 | 52 | 1.05 | 242 | －07． | 2 | 2.36 | ． 01 | ． 28 | \％ | 9 |
| PEL－90－G－76R | 3 | 151 | 12 | 257 | ， 8 | 30 | 25 | 1760 | 8.99 | 36 | 5 | ND | 1 | 107 | ， | 7 | 2 | 69 | ． 71 | 140 | 3 | 44 | 2.23 | 16 | ，17． | 2 | 2.38 | ． 01 | ． 09 | $\stackrel{1}{1}$ | 21 |
| PEL－90－G－77R | 1 | 102 | 23 | 175 | 1ss． | 13 | 14 | 1144 | 9.30 | 324 | 5 | ND | 1 | 95 | \％ | 7 | 2 | 90 | ． 50 | \％+1 | 4 | 54 | 2.11 | 22 | 19 | 2 | 2.22 | ． 01 | ． 04 |  | 16 |
| PEL－90－G－78R | 2 | 47 | 177 | 33 | \％$\%$ \％ | 4 | 2 | 114 | 3.88 | 231 | 5 | ND | 1 | 96 | － | 2 | 3 | 36 | ． 32 | \％0，4\％ | 4 | 15 | ． 02 | 61 | ，13． | 2 | ． 36 | ． 01 | ． 08 | 2 | 270 |
| PEL－90－6－79R | 4 | 533 | 14 | 2181 | \％ 6 | 10 | 5 | 525 | 2.64 | 21 | 5 | ND | ， | 6 | 10．0 |  | 2 | 2 | ． 19 | \＄004 |  | 37 | ． 28 | 68 | 0 0 ， | 4 | ． 29 | ． 01 | ． 02 | \％ | 22 |
| PEL－90－6－80R | 2 | 22 | 19 | 19 | 1， 2 | 3 | 2 | 76 | 2.46 | 24 | 7 | ND | 1 | 165 | \％ 2 | 2 | 2 | 11 | ． 17 | 100\％ | 2 | 5 | ． 07 | 244 | 10． | 2 | ． 32 | ． 01 | ． 16 | ＊＊ | 16 |
| PEL－90－G－80R（A） | 2 | 292 | 19 | 508 | 1.2 | 5 | 5 | 383 | 3.92 | 37 | 5 | ND | 1 | 12 | \％．7． | 2 | 2 | 4 | ． 22 | \＄007 | 3 | 6 | ． 21 | 99 | －01． | 2 | ． 17 | ． 01 | ． 01 |  | 32 |
| PEL－90－G－81R | 2 | 193 | 25 | 595 | \％$\%$ | 7 | 4 | 409 | 2.89 | \＄15 | 5 | ND | 1 | 7 | 时 8 | 2 | 2 | 4 | ． 16 | \％00\％ |  | 7 | ． 22 | 108 | － | 3 | ． 25 | ． 01 | ． 01 |  | 16 |
| PEL－90－G－82R | 4 | 200 | 49 | 2128 | 1．2． | 10 | 7 | 306 | 3.87 | \％17 | 5 | MD | 1 | 34 | 10．6 | 2 | 2 | 7 | ． 28 | ＜13 | 2 | 37 | ． 12 | 38 | －04． |  | ． 14 | ． 01 | ． 01 | ＜ | 72 |
| PEL－90－G－83R | 2 | 27 | 61 | 165 | 2．6． | 25 | 53 | 988 | 12.52 | 26 | 5 | ND | ， | 88 | ，\％ | 7 | 2 | 65 | ． 92 | 19\％ | 4 | 54 | 2.17 | 6 | 24． | 2 | 2.29 | ． 01 | ． 09 | 4 | 62 |
| PEL－90－G－84R | 3 | 50 | 39 | 236 | 2.0 | 29 | 55 | 1750 | 12.13 | 18 | 5 | NO | 1 | 81 | ， 4 | 7 | 2 | 73 | 1.58 | 253 | 6 | 63 | 3.32 | 23 | \％19 |  | 3.33 | ． 01 | ． 08 | 2 | 13 |
| PEL－90－G－85R |  | 3953 | 2 | 512 | 2. | 38 | 31 | 2473 | 6.27 | 2 | 5 | ND | 1 | 121 | \％\％\％ | 4 | 2 | 89 | 1.82 | 313 | 6 | 76 | 3.87 | 86 | \％ 23. | 3 | 3.29 | ． 01 | ． 01 | ， | 13 |
| PEL－90－G－86R |  | 6548 | 2 | 295 | \％．5． | 43 | 38 | 2223 | 7.61 | 2 | 5 | ND | 1 | 116 | 2， 3 ， | 2 | 2 | 100 | 1.71 | 37\％ | 6 | 86 | 4.56 | 80 | \％25 | 4 | 3.79 | ． 01 | ． 01 | 1 | 6 |
| PEL－90－G－87R | 3 | 1698 | 29 | 128 | 3， 0 | 37 | 31 | 653 | 5.83 | 118 | 5 | ND | 1 | 122 | \％ | 3 | 6 | 41 | ． 96 | \％15 | 4 | 45 | ． 91 | 15 | ¢17 | 2 | 1.09 | ． 01 | ． 01 | ， | 42 |
| STANDARD C／AU－R | 18 | 59 | 39 | 133 | \％2 | 72 |  | 1058 | 3.98 | 40 | 18 | 7 | 36 | 53 | 18， 8 | 15 | 19 | 55 | ． 52 | 8099 | 38 | 59 | ． 90 | 180 | ， 07 | 38 | 1.90 | ． 06 | ． 14 | 13 | 540 |

Cathedral Gold Corp．PROJECT 8103 FILE \＃90－4553
Page 8

| SAMPLE＊ | $\begin{gathered} \text { Mo } \\ \text { pppm } \end{gathered}$ | $\begin{array}{r} \mathrm{Cu} \\ \mathrm{ppm} \end{array}$ | $\mathrm{Pb}$ ppm | $\mathbf{Z n}$ ppm |  | $\begin{gathered} \mathrm{Ni} \\ \text { ppm } \end{gathered}$ | $\begin{array}{r} \text { Co } \\ \text { ppon } \end{array}$ | $\begin{array}{r} \mathrm{Mn} \\ \mathrm{ppm} \end{array}$ | $\begin{gathered} \mathrm{Fe} \\ \mathrm{z} \end{gathered}$ | $\begin{aligned} & \text { \%pin } \\ & \text { ppon } \end{aligned}$ | $\$_{i} \mathrm{U}$ | $\begin{gathered} \text { AU } \\ \text { ppm } \end{gathered}$ | Th <br> ppm | $\begin{array}{r} \mathrm{Sr} \\ \text { ppm } \end{array}$ | $\hat{N}_{\mathrm{H}}^{\mathrm{g} 日 \mathrm{~m}}$ | $\begin{array}{r} \text { sb } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathrm{Bi} \\ \mathrm{ppm} \end{array}$ | $\begin{array}{r} v \\ \text { ppon } \end{array}$ | $\begin{gathered} \mathrm{Ca} \\ \boldsymbol{z} \end{gathered}$ |  | $\begin{array}{r} \text { La } \\ \text { ppm } \end{array}$ | $\begin{array}{r} \mathbf{C r} \\ \mathbf{p p r i n} \end{array}$ | $\begin{array}{r} \mathrm{Mg} \\ \% \end{array}$ | $\begin{array}{r} \mathrm{Ba} \\ \mathrm{ppm} \end{array}$ | 多 | $\begin{array}{r} B \\ \text { Ppm } \end{array}$ | $\begin{gathered} \text { AL } \\ \text { X } \end{gathered}$ | $\begin{gathered} \mathrm{Na} \\ \% \end{gathered}$ | $\begin{aligned} & k \\ & \% \end{aligned}$ |  | $A u^{*}$ ppb |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PEL－90－G－88R | 18 | 209 | 144 | 366 | 2\％ | 15 | 31 | 466 | 12.70 | 163 | 5 | MD | 1 | 20 | $\geqslant 2$ | － 2 | 3 | 24 | ． 11 | \％04\％ | 3 | 15 | ． 37 | 8 | $80 \%$ | 2 | ． 79 | ． 01 | ． 05 | 2 | 168 |
| PEL－90－G－89R | 10 | 234 | 71 | 325 | \＄ 4 \％ | 11 | 41 | 159 | 17.17 | 146 | 5 | ND | 1 | 13 | \％${ }^{2}$ | 3 | 2 | 22 | ． 08 | 8029 | 2 | 11 | ． 08 | 2 | S04 | 2 | ． 34 | ． 01 | ． 04 | 2 | 122 |
| PEL－90－G－90R | 2 | 4187 | 12 | 69 | 6\％\％ | 11 | 147 | 253 | 17.96 | 14． | 5 | ND | 2 | 129 | \％ 2 | 2 | 11 | 35 | ． 37 | 1047． | 3 | 15 | ． 56 | 11 | 220 | 7 | ． 81 | ． 01 | ． 05 | 3 | 48 |
| PEL－90－6－91R | 2 | 5717 | 9 | 76 | 7 ${ }^{2}$ | 13 | 177 | 268 | 19.89 | 82 | 5 | ND | 1 | 40 | \％ 2 | 2 | 2 | 31 | ． 07 | －054 | 2 | 11 | ． 61 | 8 | 809 | 4 | ． 72 | ． 01 | ． 01 | ， 3 | 37 |
| PEL－90－G－92R | 3 | 2163 | 9 | 54 | 15．\％ | 11 | 129 | 103 | 19.68 | \％1＊ | 5 | ND | 1 | 62 | 约 | 2 | 11 | 40 | ． 14 | 0533 | 2 | 13 | ． 20 | 9 | \％ 8 | 2 | ． 42 | ． 01 | ． 02 | 13． | 46 |
| PEL－90－G－93R | 3 | 3353 | 15 | 104 | 162 | 11 | 117 | 127 | 18.08 | 10 | 5 | ND | 2 | 51 | \％ 2 \％ | 2 | 6 | 41 | ． 12 | \％075． | 2 | 18 | ． 29 | 11 | \％\％ | 2 | ． 57 | ． 01 | ． 03 | \％ | 42 |
| PEL－90－G－94R | 1 | 86 | 333 | 85 | \％ | 1 | 5 | 59 | 3.17 | 4 | 5 | ND |  | 364 | ＊$\%$ | 2 | 5 | 14 | ． 11 | $\bigcirc 020$ | 2 | 1 | ． 04 | 25 | \％ | 6 | ． 33 | ． 01 | ． 19 | 䊽 | 207 |
| PEL－90－G－95R | 1 | 84 | 8 | 106 | \％ | 8 | 6 | 606 | 2.09 | \％ | 5 | ND | 1 | 108 | 2. | 2 | 4 | 32 | ． 67 | \％068 | 2 | 15 | ． 83 | 297 | \％3 | 5 | ． 89 | ． 01 | ． 01 | § | 112 |
| PEL－90－6－96R | 3 | 22 | 2 | 1 | \％$\geqslant 2$ | 11 | 60 | 25 | 14.45 | 2 | 5 | 24 | 1 | 3 | \％ 2 | 2 | 9 | 1 | ． 01 | \％002 | 2 | 5 | ． 01 | 4 | S61 | 6 | ． 05 | ． 01 | ． 01 | 永 | 27260 |
| PEL－90－J－109R | 8 | 31 | 18 | 67 | 疎 8 | 21 | 33 | 500 | 11.95 | ＊ 2 | 5 | ND | 1 | 70 | 就\％ | 2 | 2 | 33 | ． 38 | \＄048 | 2 | 10 | ． 91 | 10 | \＄20 | 2 | 1.02 | ． 01 | ． 10 | \％ | 340 |
| PEL－90－J－110R | 1 | 211 | 7 | 24 | \％ | 23 | 6 | 193 | 2.16 | \％${ }^{2}$ | 5 | ND | 1 | 33 | \％ 2 | 2 | 2 | 45 | ． 44 | \％061 | 2 | 15 | ． 52 | 34 | ＊24 | 6 | ． 79 | ． 04 | ． 20 | 食 | 30 |
| PEL－90－J－111R | 4 | 33 | 12 | 8 | 約 | 1 | 6 | 68 | 11.42 | 6 | 5 | ND | 2 | 17 | ， 2 | 2 | 7 | 52 | ． 04 | ， $0 \% 2$ | 2 | 12 | ． 06 | 115 | \％3 | 2 | ． 30 | ． 01 | ． 06 | ， | 320 |
| PEL－90－J－112R | 2 | 10 |  | 164 | ＊$\stackrel{3}{ }$ | 13 | 7 | 660 | 5.99 | 4 | 5 | MD | 3 | 82 | 22 | 2 | 2 | 76 | ． 20 | \％085 | 4 | 60 | 1.59 | 16 | \％19 | 4 | 1.37 | ． 05 | ． 13 | 2. | 164 |
| PEL－90－J－113R | 4 | 106 | 17723 | 281 | 3\％ 4 | 1 | 7 | 95 | 16.79 | 367 | 5 | 5 | 2 | 220 | 2．3． | 32 | 29 | 23 | ． 23 | \％ 860 | 44 | 22 | ． 05 | 40 | 35 | 2 | ． 60 | ． 01 | ． 09 | 納 | 6910 |
| PEL－90－J－114R | 2 | 98 | 956 | 805 | \％ 5 | 5 | 7 | 148 | 7.17 | 806 | 5 | 2 |  | 113 | \％\％ 2 | 8 | 2 | 29 | ． 16 | 10\％ | 23 | 9 | ． 06 | 27 | \％\％ | 5 | ． 33 | ． 01 | ． 09 | \％t | 2180 |
| PEL－90－J－115R | 9 | 32 | 187 | 7 | \＆\％ | ＋ 1 | 6 | 119 | 10.23 | 136 | 5 | ND | 3 | 122 | ＊ 2. | 2 | 2 | 62 | ． 03 | \％ 632 | 3 | 14 | ． 14 | 159 | 㮯3 | 7 | ． 33 | ． 02 | ． 17 | \％ | 94 |
| PEL－90－J－116R | 3 | 33 | 26 | 2 | 絞 | ＋ 3 | 4 | 24 | 8.91 | 878 | ＋ 5 | ND | 3 | 5 | ＊ 2 2 | 2 | 2 | 17 | ． 01 | 102 | 2 | 7 | ． 03 | 106 | 今80 | 6 | ． 28 | ． 01 | ． 13 | \％ | 280 |
| PEL－90－J－117R | 9 | 46 | 979 | 19 | \％ 1. | 1 | 5 | 32 | 3.24 | \％ | 5 | ND | 3 | 39 | \％ | 2 | 2 | 12 | ． 02 | \％078 | 19 | 2 | ． 03 | 1117 | 018 | 4 | ． 48 | ． 03 | ． 12 | \％ | 189 |
| PEL－90－J－118R | 12 | 40 | 17 | 50 | \％$\%$ \％ | 5 | 20 | 872 | 4.61 | \％ 2 | 5 | ND | 4 | 16 | 2 | 2 | 2 | 24 | ． 06 | \％165 | 14 | 1 | ． 44 | 95 | \％7 | 4 | ． 91 | ． 05 | ． 25 | § | 119 |
| PEL－90－J－119R | 6 | 53 | 12 | 35 | \％2 | 4 | 3 | 89 | 2.07 | \％2 | 5 | ND | 9 | 26 | \＄ 2 | 2 | 3 | 13 | ． 08 | \＄082 | 31 | 1 | ． 38 | 105 | \％01 | 2 | ． 85 | ． 02 | ． 14 |  | 1 |
| PEL－90－J－119R（A） | 15 | 13 | 2 | 8 | 就2 | 6 | 11 | 91 | 1.77 | 2 | 5 | ND | 1 | \％ | $\geqslant 2$ | 2 | 2 | 18 | ． 04 | \％018 | 5 | 4 | ． 30 | 87 | \％ 01 | 5 | ． 48 | ． 02 | ． 16 | 紬 | 1 |
| PEL－90－J－120R | 9 | 25 | 122 | 110 | \％$\%$ | 38 | 20 | 471 | 9.57 | 4 | 5 | ND | 2 | 16 | \％ 8 \％ | 2 | 2 | 82 | ． 73 | 262 | 7 | 50 | 1.45 | 19 | \％6 | 3 | 1.51 | ． 03 | ． 13 | 紬 | 18 |
| PEL－90－J－121R | 5 | 15 | 9 | 31 | $\pm$ | 4 | 11 | 400 | 4.96 | 2 | 5 | ND |  | 54 | $\geqslant 2$ | 2 | 2 | 55 | ． 71 | 158 | 7 | 1 | ． 97 | 28 | \％3 | 5 | 1.11 | ． 07 | ． 08 | \％ 1 | 3 |
| PEL－90－J－122R | 4 | 12 | 21 | 36 | 星 | 4 | 9 | 426 | 3.60 | 3 | 5 | ND | 5 | 43 | \％${ }^{2}$ | 2 | 5 | 26 | ． 50 | 102 | 8 | 1 | ． 91 | 44 | \％0 | 6 | 1.01 | ． 05 | ． 11 | \％ | 1 |
| PEL－90－J－123R | 4 | 27 | 10 | 25 | \% | 13 | 5 | 393 | 1.08 | 8 | 5 | ND | 1 | 2 | 22 | 2 | 2 | 14 | ． 02 | \％007． | 2 | 10 | ． 14 | 45 | \％018 | 3 | ． 37 | ． 01 | ． 06 | \％ | 3 |
| PEL－90－J－124R | 3 | 25 | 51 | 12 | 16．2 | ． 8 | 136 | 26 | 7.54 | 8 | 5 | ND | 1 | 10 | \％2 | 2 | 75 | 3 | ． 02 | 8003 | 2 | 7 | ． 02 | 2 | 301． | 3 | ． 05 | ． 01 | ． 02 | \％ | 93 |
| PEL－90－J－125R |  | 432 | 6 | 52 | ， 4 | 65 | 46 | 301 | 16.93 | 87 | 5 | ND |  | 59 | \％2 | 2 | 2 | 9 | ． 27 | 1004 | 2 | 11 | ． 37 | 5 | \％or | 2 | ． 48 | ． 01 | ． 01 | \％ | 87 |
| PEL－90－J－126R | 8 | 65 | 130 | 226 | \％\％ | 27 | 51 | 285 | 15.40 | 123 | 5 | ND | 1 | 86 | \＄4． | 2 | 3 | 13 | ． 42 | \％020 | 3 | 6 | ． 33 | 4 | 80\％ | 2 | ． 63 | ． 01 | ． 06 | 䊽 | 240 |
| PEL－90－J－127R | 109 | 33 | 49 | 35 | 14 4 | 12 | 37 | 471 | 7.22 | 77. | 5 | MD | 1 | 42 | \％ 2 | 2 | 2 | 15 | ． 93 | \％088 | 2 | 2 | ． 57 | 11 | 801 | 2 | ． 98 | ． 01 | ． 18 | \％ | 37 |
| PEL－90－J－128R | 5 | 646 | 20 | 5 | \％${ }^{3}$ | 58 | 53 | 39 | 17.68 | 56 | 5 | ND | 2 | 32 | \％2 | 2 | 2 | 3 | ． 11 | 100\％ | 2 | 6 | ． 01 | 6 | 6018 | 3 | ． 12 | ． 01 | ． 02 | \％ | 520 |
| PEL－90－J－128R（REF） | 3 | 876 | 9 | 10 | 3 3 | 55 | 34 | 73 | 18.45 | 58 | 5 | ND | 2 | 29 | \％ 2 | 2 | 2 | 4 | ． 11 | \％0014 | 2 | 2 | ． 01 | 11 | \％0\％ | 2 | ． 14 | ． 01 | ． 03 | 䜌 | 730 |
| PEL－90－J－129R | 18 | 508 | 73 | 59 | 8.0 | 52 | 36 | 200 | 16.96 | 815 | 5 | ND | 2 | 7 | \％ 2 | 2 | 6 | 29 | ． 09 | \％ $0 \$ 5$ | 4 | 21 | ． 29 | 4 | \％ 0 | 6 | ． 47 | ． 01 | ． 08 | \％ | 320 |
| PEL－90－J－130R | 10 | 8 | 17 | 2 | \％${ }^{\text {\％}}$ | 5 | 14 | 21 | 4.14 | 10， | 5 | ND | ， | 3 | \％ | 2 | 7 | 3 | ． 02 | \＄009 | 2 | 1 | ． 01 | 13 | \％ay | 4 | ． 26 | ． 01 | ． 16 | \％ | 89 |
| PIN L1 1＋05－1＋15E | 17 | 41 | 9 | 22 | \％${ }^{\text {\％}}$ | 4 | 4 | 103 | 4.49 | 56 | 5 | ND | 2 | 3 | \％ | 5 | 2 | 16 | ． 04 | \％085． | 10 | 5 | ． 47 | 42 | \％ 06 | 4 | 1.31 | ． 01 | ． 17 | \＄ | 14 |
| STANDARD C／AU－R | 18 | 59 | 38 | 131 | 8．\％ | 67 | 32 | 1052 | 3.97 | 38 | 19 | 7 | 37 | 53 | 18．\％ | 15 | 20 | 55 | ． 51 | \＄0\％\％ | 37 | 56 | ． 90 | 181 | 107 | 39 | 1.89 | ． 06 | ． 14 | 13 | 480 |

## GEOCHEMICAL ANALYSIS CERTIFICATE

Cathedral Gold Corp. FILE \# 90-4390R

| SAMPLE\# | Hg <br> ppb |
| :--- | ---: |
| SER L2+OOS 2+50E | 20 |
| SER L2+00S 2+75E | 10 |
| SER L2+00S 3+00E | 20 |
| PEL-90-J-91 | 680 |



## GEOCHEMICAL ANAI.YSIS CERTIFICATE

Cathedral Gold Corp. PROJECT 8103 FILE \# 90-4294R

| SAMPLE\# | Hg <br> ppb |  |
| :--- | :--- | ---: |
| 1 L | $12+00$ | $1+00 S$ |

- Sample type: soil pulp hg analysis by flameless an.

SIGNED BY. C.:. D. TOYE, c.leong, J. WANG; CERTIFIED b.c. ASSAYERS

# ACME ANALYTICAL LABORATORIES LTD. 

dAte received: Nov 271990
852 E. HAStings St. VANCOUVER B.C. V6A 1 R6 PHONE(604)253-3158 FAX(604)253-1716 date report mailed: oneç.3/90.

## GEOCHEMICAL ANALYSIS CERTIFICATE

## Cathedral Gold Corp. PROJECT 8103 FILE \# 90-4205R

| SAMPLE\# | Hg <br> ppb |
| :--- | ---: |
| PEL-90-G-11 | 230 |
| PEL-90-G-14 | 30 |
| PEL-90-J-10 | 20 |

- SAMPLE TYPE: ROCK PULP HG ANALYSIS by flameless an.

SIGNED BY... D.TOYE, C.LEONG, J.WANG; CERTIFIED B.C. ASSAYERS

## GEOCHEMICAL ANALYSIS CERTIFICATE

Cathedral Gold Corp. PROJECT 8103 FILE \# 90-4553R

| SAMPLE\# | Hg <br> pp |
| :--- | ---: |
| PEL-90-G-96R | 10 |
| PEL-90-J-113R | 20 |
| PEL-90-J-114R | 10 |



APPENDIX X

STATISTICAL REPORT - ROCK GEOCHEMICAL DATA

```
lon
```

Detail Report

Variable: CU

| Mean - Average | 375.8677 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 240.6831 | No. missing values | 0 |
| Upper 95\% c.i.limit | 511.0523 | Sum of frequencies | 257 |
| Adj sum of squares | 3.129907E+08 | Sum of observations | 96598 |
| Standard deviation | 1105.721 | Std.error of mean | 68.973 |
| Variance | 1222620 | T-value for mean=0 | 5.44949 |
| Coef. of variation | 2.941783 | T prob level | 0.0000 |
| Skewness | 5.008907 | Kurtosis | 29.83405 |
| Normality Test Value | 0.641 | Reject if > 1.021 (10\%) | 1.035 (5\%) |
| 100-\%tile (Maximum) | 9866 | 90-\%tile | 663 |
| 75-\%tile | 193 | 10-\%tile | 7 |
| 50-\%tile (Median) | 46 | Range | 9865 |
| 25-\%tile | 18 | 75th-25th \%tile | 175 |
| 0-\%tile (Minimum) | 1 |  |  |
|  | -Line P | t / Box Plot- |  |
| $\text { ZZL8652221 } 111121$ | 112 | 1111 |  |

## Distribution \& Histogram



| -ate/Time | $01-21-1991 \quad 13: 56: 24$ |
| :--- | :--- |
| Datel |  |
| Data Base Name $C: \backslash s t a t s \backslash n c s s \backslash d a t a \backslash p e l 90 r n c ~$ |  |
| Description | Imported from $A: p e l 90 r n c . p r n$ |

Detail Report
Variable: PB


## Distribution \& Histogram




| Date/Time | 01-21-1991 13:55:16 |
| :---: | :---: |
| Data Base Name | C: \stats $\backslash$ ncss $\backslash$ data $\backslash p e l 90 r n c$ |
| Description | Imported from A:pel90rnc.prn |

Detail Report
Variable: MO

| Mean - Average | 7.377432 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 5.889842 | No. missing values | 0 |
| Upper 95\% c.i.limit | 8.865023 | Sum of frequencies | 257 |
| Adj sum of squares | 37900.39 | Sum of observations | 1896 |
| Standard deviation | 12.16751 | Std.error of mean | . 7589887 |
| Variance | 148.0484 | T-value for mean=0 | 9.720081 |
| Coef. of variation | 1.649289 | T prob level | 0.0000 |
| Skewness | 4.917408 | Kurtosis | 31.14831 |
| Normality Test Value | 0.636 | Reject if > 1.021(10\%) | 1.035 (5\%) |
| 100-\%tile (Maximum) | 109 | 90-\%tile | 16 |
| 75-\%tile | 7 | 10-\%tile | 1 |
| 50-\%tile (Median) | 4 | Range | 108 |
| 25-\%tile | 2 | 75th-25th \%tile | 5 |
| 0-\%tile (Minimum) | 1 |  |  |
| $\begin{aligned} & \text { ZZWJM79735445211 } 22 \\ & \text {-[mX]a---- } \end{aligned}$ | 12111 | Box Plot----------1 |  |


|  |  |  |  | Distr | bution | n \& Hi | togra |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Variable: MO |  |  |  |  |  |  |  |  |
| Bin | Lower |  | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 |  | 2 | 53 | 20.6 | 53 | 20.6 | : ****************** |
| 2 | 2 |  | 4 | 67 | 26.1 | 120 | 46.7 | : ********************** |
| 3 | 4 |  | 6 | 51 | 19.8 | 171 | 66.5 | :***************** |
| 4 | 6 |  | 8 | 22 | 8.6 | 193 | 75.1 | : ******* |
| 5 | 8 |  | 10 | 16 | 6.2 | 209 | 81.3 | :***** |
| 6 | 10 |  | 12 | 7 | 2.7 | 216 | 84.0 | : ** |
| 7 | 12 |  | 14 | 7 | 2.7 | 223 | 86.8 | : ** |
| 8 | 14 |  | 16 | 5 | 1.9 | 228 | 88.7 | :** |
| 9 | 16 |  | 18 | 4 | 1.6 | 232 | 90.3 | : * |
| 10 | 18 |  | 20 | 7 | 2.7 | 239 | 93.0 | :** |
| 11 | 20 |  | 22 | 1 | 0.4 | 240 | 93.4 | : |
| 12 | 22 |  | 24 | 1 | 0.4 | 241 | 93.8 | : |
| 13 | 24 |  | 26 | 2 | 0.8 | 243 | 94.6 |  |
| 14 | 26 |  | 28 | 2 | 0.8 | 245 | 95.3 |  |
| 15 | 28 |  | 30 | 2 | 0.8 | 247 | 96.1 |  |
| 0 | Values | s out | of range | 10 | 3.9 |  |  | : |


| Date/Time | 01-21-1991 13:57:12 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss\data\pel90rnc |
| Description | Imported from A:pel90rnc.prn |

## Detail Report

Variable: AG


## Distribution \& Histogram



| Date/Time | 01-21-1991 13:57:56 |
| :---: | :---: |
| Data Base Name | C: \stats ${ }^{\text {a }}$ css $\backslash$ data $\backslash p e l 90 r n c$ |
| Description | Imported from A:pel90rnc.prn |

## Detail Report

Variable: NI

| Mean - Average | 18.18677 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 14.10662 | No. missing values | 0 |
| Upper 95\% c.i.limit | 22.26692 | Sum of frequencies | 257 |
| Adj sum of squares | 285121 | Sum of observations | 4674 |
| Standard deviation | 33.37296 | Std.error of mean | 2.081748 |
| Variance | 1113.754 | T-value for mean=0 | 8.7363 |
| Coef. of variation | 1.835013 | T prob level | 0.0000 |
| Skewness | 9.62718 | Kurtosis | 121.518 |
| Normality Test Value | 0.644 | Reject if > 1.021 (10\%) | 1.035 (5\%) |
| 100-\%tile (Maximum) | 460 | 90-\%tile | 40 |
| 75-\%tile | 21 | 10-\%tile | 3 |
| 50-\%tile (Median) | 10 | Range | 459 |
| 25-\%tile | 5 | 75th-25th \%tile | 16 |
| 0-\%tile (Minimum) | 1 |  |  |
| YZZPIC662373 111 | ```1 Line Plot / Box Plot------------------------------460``` |  |  |
| - [ma---- |  |  |  |

## Distribution \& Histogram

| Variable: NI |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower |  | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 |  | 3 | 25 | 9.7 | 25 | 9.7 | : ***** |
| 2 | 3 |  | 6 | 44 | 17.1 | 69 | 26.8 | : ********* |
| 3 | 6 |  | 9 | 43 | 16.7 | 112 | 43.6 | :********* |
| 4 | 9 |  | 12 | 31 | 12.1 | 143 | 55.6 | : ****** |
| 5 | 12 |  | 15 | 22 | 8.6 | 165 | 64.2 | :**** |
| 6 | 15 |  | 18 | 17 | 6.6 | 182 | 70.8 | :*** |
| 7 | 18 |  | 21 | 10 | 3.9 | 192 | 74.7 | :** |
| 8 | 21 |  | 24 | 7 | 2.7 | 199 | 77.4 | : * |
| 9 | 24 |  | 27 | 12 | 4.7 | 211 | 82.1 | :** |
| 10 | 27 |  | 30 | 6 | 2.3 | 217 | 84.4 | : * |
| 11 | 30 |  | 33 | 5 | 1.9 | 222 | 86.4 | : * |
| 12 | 33 |  | 36 | 6 | 2.3 | 228 | 88.7 | : * |
| 13 | 36 |  | 39 | 3 | 1.2 | 231 | 89.9 | : * |
| 14 | 39 |  | 42 | 1 | 0.4 | 232 | 90.3 | : |
| 15 | 42 |  | 45 | 5 | 1.9 | 237 | 92.2 | : * |
| 0 | Values | s out | of range | 20 | 7.8 |  |  | : |


| Date/Time | 01-21-1991 14:05:42 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss\data \pel90rnc |
| Description | Imported from A:pel90rnc.prn |

Detail Report

## Variable: FE\%

| Mean - Average | 7.364436 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 6.668376 | No. missing values | 0 |
| Upper 95\% c.i.limit | 8.060495 | Sum of frequencies | 257 |
| Adj sum of squares | 8297.931 | Sum of observations | 1892.66 |
| Standard deviation | 5.693311 | Std.error of mean | . 355139 |
| Variance | 32.41379 | T-value for mean=0 | 20.73677 |
| Coef. of variation | . 7730818 | T prob level | 0.0000 |
| Skewness | 2.040741 | Kurtosis | 5.936097 |
| Normality Test Value | 1.389 | Reject if > 1.021 (10\%) | 1.035 (5\%) |
| 100-\%tile (Maximum) | 40.74 | 90-\%tile | 16.2 |
| 75-\%tile | 8.91 | 10-\%tile | 2.2 |
| 50-\%tile (Median) | 5.91 | Range | 40.3 |
| 25-\%tile | 3.63 | 75th-25th \%tile | 5.28 |
| 0-\%tile (Minimum) | . 44 |  |  |
| .44-------- | --L | / Box Plot |  |
| 166EI9FJ9BKGB8CA87932 | 3242141 | 111211111 |  | ---[XXXXmXaXX]

Distribution \& Histogram

| Variable: FE\% |  |  |
| :---: | :--- | :--- |
| Bin Lower |  |  |
| 1 | 0 | Upper |
| 2 | 1 | 1 |
| 3 | 2 | 2 |
| 4 | 3 | 3 |
| 5 | 4 | 4 |
| 6 | 5 | 5 |
| 7 | 6 | 6 |
| 8 | 7 | 7 |
| 9 | 8 | 9 |
| 10 | 9 | 10 |
| 11 | 10 | 11 |
| 12 | 11 | 12 |
| 13 | 12 | 13 |
| 14 | 13 | 14 |
| 15 | 14 | 15 |
| 0 | Values out of range |  |


| Count | Prent | Total | Prant | Histogram |
| ---: | ---: | ---: | ---: | :--- |
| 5 | 1.9 | 5 | 1.9 | $: *$ |
| 12 | 4.7 | 17 | 6.6 | $: * *$ |
| 32 | 12.5 | 49 | 19.1 | $: * * * * * *$ |
| 27 | 10.5 | 76 | 29.6 | $: * * * * *$ |
| 26 | 10.1 | 102 | 39.7 | $: * * * * *$ |
| 30 | 11.7 | 132 | 51.4 | $: * * * * * *$ |
| 23 | 8.9 | 155 | 60.3 | $: * * * * *$ |
| 21 | 8.2 | 176 | 68.5 | $: * * * *$ |
| 18 | 7.0 | 194 | 75.5 | $: * * * *$ |
| 15 | 5.8 | 209 | 81.3 | $: * * *$ |
| 5 | 1.9 | 214 | 83.3 | $: *$ |
| 5 | 1.9 | 219 | 85.2 | $: *$ |
| 6 | 2.3 | 225 | 87.5 | $: *$ |
| 1 | 0.4 | 226 | 87.9 | $:$ |
| 4 | 1.6 | 230 | 89.5 | $: *$ |
| 27 | 10.5 |  |  | $:$ |


| Date/Time | 01-21-1991 14:06:09 |
| :---: | :---: |
| Data Base Name |  |
| Description | Imported from A:pel90rnc.prn |

Detail Report
Variable: AS

| Mean - Average | 67.65759 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 48.89713 | No. missing values | 0 |
| Upper 95\% c.i.limit | 86.41805 | Sum of frequencies | 257 |
| Adj sum of squares | 6027872 | Sum of observations | 17388 |
| Standard deviation | 153.4483 | Std.error of mean | 9.57184 |
| Variance | 23546.38 | $T$-value for mean=0 | 7.068399 |
| Coef. of variation | 2.268013 | T prob level | 0.0000 |
| Skewness | 4.733779 | Kurtosis | 30.33678 |
| Normality Test Value | 0.735 | Reject if > $1.021(10 \%)$ | 1.035 (5\%) |
| 100-\%tile (Maximum) | 1411 | 90-\%tile | 231 |
| 75-\%tile | 41 | 10-\%tile | 2 |
| 50-\%tile (Median) | 14 | Range | 1409 |
| 25-\%tile | 4 | 75th-25th \%tile | 37 |
| 0-\%tile (Minimum) | 2 |  |  |
|  | --L | / / Box Plot |  |
| 2ZJ754434321 2222511212111 <br> [m]-a--------- |  |  |  |

Distribution \& Histogram


```
\begin{tabular}{|c|c|}
\hline Date/Time & 01-21-1991 14:08:16 \\
\hline Data Base Name & C: \stats ncss \(\backslash\) data \(\backslash\) pel \(90 r n c ~_{\text {c }}\) \\
\hline Description & Imported from A:pel90rnc.prn \\
\hline
\end{tabular}
```

Detail Report
Variable: SB

| Mean - Average | 2.945525 | No. observations | 257 |
| :--- | :--- | :--- | :--- |
| Lower 95\% c.i.limit | 2.567673 | No. missing values | 0 |
| Upper 95\% c.i.limit | 3.323378 | Sum of frequencies | 257 |
| Adj sum of squares | 2445.237 |  | Sum of observations |


| 100-\%tile | (Maximum) | 32 | 90-\%tile | 5 |
| :---: | :---: | :---: | :---: | :---: |
| 75-\%tile |  | 2 | 10-\%tile | 2 |
| 50-\%tile | (Median) | 2 | Range | 30 |
| 25-\%tile |  | 2 | 75th-25th \%tile | 0 |
| 0-\%tile | (Minimum) | 2 |  |  |
| 2-------- | 7551 | 2 | / Box Plot |  |

Distribution \& Histogram



Variable: BI


## Distribution \& Histogram




Distribution \& Histogram

| Variable: CA |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower |  | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 |  | . 1 | 47 | 18.3 | 47 | 18.3 | : **** |
| 2 | . 1 |  | . 2 | 40 | 15.6 | 87 | 33.9 | : **** |
| 3 | . 2 |  | . 3 | 35 | 13.6 | 122 | 47.5 | : *** |
| 4 | . 3 |  | . 4 | 25 | 9.7 | 147 | 57.2 | : ** |
| 5 | . 4 |  | . 5 | 21 | 8.2 | 168 | 65.4 | : ** |
| 6 | . 5 |  | . 6 | 12 | 4.7 | 180 | 70.0 | : * |
| 7 | . 6 |  | . 7 | 8 | 3.1 | 188 | 73.2 | :* |
| 8 | . 7 |  | . 8 | 12 | 4.7 | 200 | 77.8 | :* |
| 9 | . 8 |  | . 9 | 7 | 2.7 | 207 | 80.5 | :* |
| 10 | . 9 |  | 1 | 15 | 5.8 | 222 | 86.4 | :* |
| 11 | 1 |  | 1.1 | 4 | 1.6 | 226 | 87.9 | : |
| 12 | 1.1 |  | 1.2 | 4 | 1.6 | 230 | 89.5 | : |
| 13 | 1.2 |  | 1.3 | 2 | 0.8 | 232 | 90.3 | : |
| 14 | 1.3 |  | 1.4 | 1 | 0.4 | 233 | 90.7 | : |
| 15 | 1.4 |  | 1.5 | 3 | 1.2 | 236 | 91.8 | : |
| 0 | Values | s out | of range | 21 | 8.2 |  |  | : |


| Date/Time | 01-21-1991 14:15:07 |
| :---: | :---: |
| Data Base Name | c: \stats \ncss\data \pel90rnc |
| Description | Imported from A:pel90rnc.prn |

Detail Report

## Variable: NA\%

| Mean - Average | 2.750973E-02 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | $2.130102 \mathrm{E}-02$ | No. missing values | 0 |
| Upper 95\% c.i.limit | $3.371844 \mathrm{E}-02$ | Sum of frequencies | 257 |
| Adj sum of squares | . 6602062 | Sum of observations | 7.07 |
| Standard deviation | $5.078317 \mathrm{E}-02$ | Std.error of mean | 3.167767E-03 |
| Variance | $2.578931 \mathrm{E}-03$ | T-value for mean=0 | 8.684264 |
| Coef. of variation | 1.846008 | T prob level | 0.0000 |
| Skewness | 6.542815 | Kurtosis | 56.92672 |
| 100-\%tile (Maximum) | . 57 | 90-\%tile | . 05 |
| 75-\%tile | . 03 | 10-\%tile | . 01 |
| 50-\%tile (Median) | . 01 | Range | . 56 |
| 25-\%tile | . 01 | 75th-25th \%tile | . 02 |
| 0-\%tile (Minimum) | . 01 |  |  |
| .01------ | ------Line | / Box Plot---- |  |
| ZP HD D24 2131212 | 1111 |  |  |
| mXa]--- |  |  |  |

Distribution \& Histogram

| Variable: NA\% |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 | . 02 | 192 | 74.7 | 192 | 74.7 | : ***************** |
| 2 | . 02 | . 04 | 30 | 11.7 | 222 | 86.4 | :*** |
| 3 | . 04 | . 06 | 15 | 5.8 | 237 | 92.2 | :* |
| 4 | . 06 | 8.000E-02 | 6 | 2.3 | 243 | 94.6 | : * |
| 5 | 8.000E-02 | . 1 | 4 | 1.6 | 247 | 96.1 | : |
| 6 | . 1 | . 12 | 1 | 0.4 | 248 | 96.5 | : |
| 7 | . 12 | . 14 | 1 | 0.4 | 249 | 96.9 | : |
| 8 | . 14 | . 16 | 3 | 1.2 | 252 | 98.1 | : |
| 9 | . 16 | . 18 | 1 | 0.4 | 253 | 98.4 | : |
| 10 | . 18 | . 2 | 0 | 0.0 | 253 | 98.4 | : |
| 11 | . 2 | . 22 | 0 | 0.0 | 253 | 98.4 | : |
| 12 | . 22 | . 24 | 1 | 0.4 | 254 | 98.8 | : |
| 13 | . 24 | . 26 | 0 | 0.0 | 254 | 98.8 | : |
| 14 | . 26 | . 28 | 1 | 0.4 | 255 | 99.2 | : |
| 15 | . 28 | . 3 | 1 | 0.4 | 256 | 99.6 | : |
| 0 | Values out | of range | 1 | 0.4 |  |  | : |


| Date/Time | 01-21-1991 14:15:35 |
| :---: | :---: |
| Data Base Name | $\mathrm{C}: \backslash \mathrm{stats} \backslash$ ncss $\backslash$ data $\backslash$ pel90rnc |
| Description | Imported from A:pel90rnc.prn |

Detail Report
Variable: K\%

| Mean - Average | . 1244747 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 9.896116E-02 | No. missing values | 0 |
| Upper 95\% c.i.limit | . 1499882 | Sum of frequencies | 257 |
| Adj sum of squares | 11.14855 | Sum of observations | 31.99 |
| Standard deviation | . 2086841 | Std.error of mean | 1.301735E-02 |
| Variance | $4.354904 \mathrm{E}-02$ | T-value for mean=0 | 9.562212 |
| Coef. of variation | 1.676518 | T prob level | 0.0000 |
| Skewness | 7.586895 | Kurtosis | 71.00193 |
| Normality Test Value | 0.826 | Reject if > 1.021 (10\%) | 1.035 (5\%) |
| 100-\%tile (Maximum) | 2.37 | 90-\%tile | . 21 |
| 75-\%tile | . 15 | 10-\%tile | . 01 |
| 50-\%tile (Median) | . 09 | Range | 2.36 |
| 25-\%tile | . 03 | 75th-25th \%tile | . 12 |
| 0-\%tile (Minimum) | . 01 |  |  |
| . 01 | --Line | / Box Plot- | - |
| ZSZZZNG57323 12 | 11 |  |  |
| -[Xma] -- |  |  |  |

Distribution \& Histogram

| Var | able: K\% | Upper | Count | Prent | Total | Prent | Histogram |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | . 02 | 55 | 21.4 | 55 | 21.4 | :***** |
| 2 | . 02 | . 04 | 18 | 7.0 | 73 | 28.4 | :** |
| 3 | . 04 | . 06 | 24 | 9.3 | 97 | 37.7 | :** |
| 4 | . 06 | 8.000E-02 | 23 | 8.9 | 120 | 46.7 | :** |
| 5 | 8.000E-02 | . 1 | 25 | 9.7 | 145 | 56.4 | :** |
| 6 | . 1 | . 12 | 24 | 9.3 | 169 | 65.8 | :** |
| 7 | . 12 | . 14 | 22 | 8.6 | 191 | 74.3 | :** |
| 8 | . 14 | . 16 | 17 | 6.6 | 208 | 80.9 | :** |
| 9 | . 16 | . 18 | 6 | 2.3 | 214 | 83.3 | :* |
| 10 | . 18 | . 2 | 16 | 6.2 | 230 | 89.5 | :* |
| 11 | . 2 | . 22 | 4 | 1.6 | 234 | 91.1 | : |
| 12 | . 22 | . 24 | 2 | 0.8 | 236 | 91.8 | : |
| 13 | . 24 | . 26 | 6 | 2.3 | 242 | 94.2 | :* |
| 14 | . 26 | . 28 | 2 | 0.8 | 244 | 94.9 | : |
| 15 | . 28 | . 3 | 1 | 0.4 | 245 | 95.3 | : |
| 0 | Values out | of range | 12 | 4.7 |  |  | : |


| Date/Time | 01-21-1991 14:16:29 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss\data\pel90rnc |
| Description | Imported from A:pel90rnc.prn |

Detail Report
Variable: AUPPB

| Mean - Average | 624.4397 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 139.5043 | No. missing values | 0 |
| Upper 95\% c.i.limit | 1109.375 | Sum of frequencies | 257 |
| Adj sum of squares | $4.027585 \mathrm{E}+09$ | Sum of observations | 160481 |
| Standard deviation | 3966.454 | Std.error of mean | 247.4206 |
| Variance | $1.573276 \mathrm{E}+07$ | T-value for mean=0 | 2.523799 |
| Coef. of variation | 6.35202 | T prob level | 0.0116 |
| Skewness | 9.559584 | Kurtosis | 95.95003 |
| Normality Test Value | 0.640 | Reject if > 1.021(10\%) | 1.035 (5\%) |
| 100-\%tile (Maximum) | 46600 | 90-\%tile | 610 |
| 75-\%tile | 151 | 10-\%tile | 4 |
| 50-\%tile (Median) | 36 | Range | 46599 |
| 25-\%tile | 10 | 75th-25th \%tile | 141 |
| 0-\%tile (Minimum) | 1 |  |  |
| 1---------- | Line | / Box Plot-------1 |  |

ma

## Distribution \& Histogram

| Bin | Lower | Upper | Count | Prent | Total | Prent | Histogram |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | 5 | 34 | 13.2 | 34 | 13.2 | :*** |
| 2 | 5 | 10 | 26 | 10.1 | 60 | 23.3 | :** |
| 3 | 10 | 15 | 21 | 8.2 | 81 | 31.5 | : ** |
| 4 | 15 | 20 | 14 | 5.4 | 95 | 37.0 | :* |
| 5 | 20 | 25 | 9 | 3.5 | 104 | 40.5 | :* |
| 6 | 25 | 30 | 13 | 5.1 | 117 | 45.5 | :* |
| 7 | 30 | 35 | 10 | 3.9 | 127 | 49.4 | :* |
| 8 | 35 | 40 | 6 | 2.3 | 133 | 51.8 | : * |
| 9 | 40 | 45 | 5 | 1.9 | 138 | 53.7 | : |
| 10 | 45 | 50 | 8 | 3.1 | 146 | 56.8 | : * |
| 11 | 50 | 55 | 2 | 0.8 | 148 | 57.6 | : |
| 12 | 55 | 60 | 5 | 1.9 | 153 | 59.5 | : |
| 13 | 60 | 65 | 4 | 1.6 | 157 | 61.1 | : |
| 14 | 65 | 70 | 3 | 1.2 | 160 | 62.3 | : |
| 15 | 70 | 75 | 3 | 1.2 | 163 | 63.4 | : |
| 0 | Values | out of range | 94 | 36.6 |  |  | : |

Date/Time $\quad 01-21-1991 \quad$ 14:16:56
Data Base Name $C: \backslash s t a t s \backslash n c s s \backslash d a t a \backslash p e l 90 \mathrm{rnc}$
Description $\quad$ Imported from A:pel90rnc.prn

Detail Report
Variable: AUPPB

| Mean - Average | 624.4397 | No. observations | 257 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 139.5043 | No. missing values | 0 |
| Upper 95\% c.i.limit | 1109.375 | Sum of frequencies | 257 |
| Adj sum of squares | $4.027585 \mathrm{E}+09$ | Sum of observations | 160481 |
| Standard deviation | 3966.454 | Std.error of mean | 247.4206 |
| Variance | $1.573276 \mathrm{E}+07$ | T-value for mean=0 | 2.523799 |
| Coef. of variation | 6.35202 | T prob level | 0.0116 |
| Skewness | 9.559584 | Kurtosis | 95.95003 |
| Normality Test Value | 0.640 | Reject if > 1.021(10\%) | 1.035 (5\%) |
| 100-\%tile (Maximum) | 46600 | 90-\%tile | 610 |
| 75-\%tile | 151 | 10-\%tile | 4 |
| 50-\%tile (Median) | 36 | Range | 46599 |
| 25-\%tile | 10 | 75th-25th \%tile | 141 |
| 0-\%tile (Minimum) | 1 |  |  |
|  | ---Line | / Box Plot- |  |
| ZR732 1 1 |  | 11 |  |

Distribution \& Histogram


## Correlations -Rock.

| AS | SB | BI | PB | AG | FE\% |
| ---: | ---: | ---: | ---: | ---: | ---: |
| 1.0000 | 0.2395 | 0.0601 | 0.2045 | 0.4786 | 0.3799 |
| 0.2395 | 1.0000 | 0.6289 | 0.6251 | 0.4537 | 0.2106 |
| 0.0601 | 0.6289 | 1.0000 | 0.0489 | 0.1369 | 0.2083 |
| 0.2045 | 0.6251 | 0.0489 | 1.0000 | 0.4958 | 0.1312 |
| 0.4786 | 0.4537 | 0.1369 | 0.4958 | 1.0000 | 0.2924 |
| 0.3799 | 0.2106 | 0.2083 | 0.1312 | 0.2924 | 1.0000 |
| 0.0101 | 0.6021 | 0.8754 | 0.0930 | 0.1075 | 0.1996 |

## APPENDIX XI

## STATISTICAL REPORT - SOIL GEOCHEMICAL DATA

| Date/Time | $01-21-1991 \quad 13: 31: 11$ |
| :--- | :--- |
| Data Base Name $C: \backslash$ stats $\backslash$ ncss $\backslash$ data 1 pel 90 snc |  |
| Description | Imported from $A: p e l 90 s n c . p r n$ |

## Detail Report

Variable: MO

| Mean - Average | 7.754202 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 6.749097 | No. missing values | 0 |
| Upper 95\% c.i.limit | 8.759306 | Sum of frequencies | 476 |
| Adj sum of squares | 59460.24 | Sum of observations | 3691 |
| Standard deviation | 11.18836 | Std.error of mean | . 5128177 |
| Variance | 125.1795 | T-value for mean=0 | 15.12077 |
| Coef. of variation | 1.442877 | T prob level | 0.0000 |
| Skewness | 8.321219 | Kurtosis | 99.82639 |
| Normality Test Value | 0.691 | Reject if > 1.011(10\%) | 1.019 (5\%) |
| 100-\%tile (Maximum) | 169 | 90-\%tile | 12 |
| 75-\%tile | 8 | 10-\%tile | 2 |
| 50-\%tile (Median) | 6 | Range | 168 |
| 25-\%tile | 4 | 75th-25th \%tile | 4 |
| 0-\%tile (Minimum) | 1 |  |  |
|  | -----Li | / Box Plot |  |
| ZZZZZID23323124111 2 | 111 | 1 |  |

Distribution \& Histogram

| Variable: MO |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower |  | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 |  | 2 | 31 | 6.5 | 31 | 6.5 | :**** |
| 2 | 2 |  | 4 | 87 | 18.3 | 118 | 24.8 | :************ |
| 3 | 4 |  | 6 | 117 | 24.6 | 235 | 49.4 | :***************** |
| 4 | 6 |  | 8 | 97 | 20.4 | 332 | 69.7 | :************** |
| 5 | 8 |  | 10 | 61 | 12.8 | 393 | 82.6 | : ********* |
| 6 | 10 |  | 12 | 26 | 5.5 | 419 | 88.0 | :**** |
| 7 | 12 |  | 14 | 17 | 3.6 | 436 | 91.6 | : ** |
| 8 | 14 |  | 16 | 9 | 1.9 | 445 | 93.5 | : * |
| 9 | 16 |  | 18 | 2 | 0.4 | 447 | 93.9 | : |
| 10 | 18 |  | 20 | 3 | 0.6 | 450 | 94.5 | : |
| 11 | 20 |  | 22 | 3 | 0.6 | 453 | 95.2 | : |
| 12 | 22 |  | 24 | 2 | 0.4 | 455 | 95.6 | : |
| 13 | 24 |  | 26 | 3 | 0.6 | 458 | 96.2 | : |
| 14 | 26 |  | 28 | 1 | 0.2 | 459 | 96.4 | : |
| 15 | 28 |  | 30 | 2 | 0.4 | 461 | 96.8 | : |
| 0 | Values | s out | of range | 15 | 3.2 |  |  | : |


| Date/Time | 01-21-1991 13:32:17 |
| :---: | :---: |
| Data Base Name | C: \stats dncss $\backslash$ data $\backslash$ pel90snc $^{\text {a }}$ |
| Description | Imported from A:pel90snc.prn |

## Detail Report

Variable: CU

| Mean - Average | 79.40966 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 64.60574 | No. missing values | 0 |
| Upper 95\% c.i.limit | 94.21359 | Sum of frequencies | 476 |
| Adj sum of squares | 1.289905E+07 | Sum of observations | 37799 |
| Standard deviation | 164.7905 | Std.error of mean | 7.553159 |
| Variance | 27155.9 | $T$-value for mean $=0$ | 10.51344 |
| Coef. of variation | 2.075194 | T prob level | 0.0000 |
| Skewness | 11.11722 | Kurtosis | 173.7125 |
| Normality Test Value | 0.614 | Reject if > 1.011 (10\%) | 1.019 (5\%) |
| 100-\%tile (Maximum) | 2861 | 90-\%tile | 190 |
| 75-\%tile | 83 | 10-\%tile | 14 |
| 50-\%tile (Median) | 36 | Range | 2860 |
| 25-\%tile | 21 | 75th-25th \%tile | 62 |
| 0-\%tile (Minimum) | 1 |  |  |
| $\begin{aligned} & \text { ZZZWGHJ721 } 51 \quad 1 \quad 31 \\ & - \text { ma--- } \end{aligned}$ | $1{ }^{---L i n e}$ | / Box Plot |  |

## Distribution \& Histogram

| Variable: CU |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower |  | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 |  | 20 | 103 | 21.6 | 103 | 21.6 | : *************** |
| 2 | 20 |  | 40 | 147 | 30.9 | 250 | 52.5 | : ********************* |
| 3 | 40 |  | 60 | 76 | 16.0 | 326 | 68.5 | : *********** |
| 4 | 60 |  | 80 | 28 | 5.9 | 354 | 74.4 | : **** |
| 5 | 80 |  | 100 | 23 | 4.8 | 377 | 79.2 | :*** |
| 6 | 100 |  | 120 | 18 | 3.8 | 395 | 83.0 | : *** |
| 7 | 120 |  | 140 | 12 | 2.5 | 407 | 85.5 | :** |
| 8 | 140 |  | 160 | 6 | 1.3 | 413 | 86.8 | :* |
| 9 | 160 |  | 180 | 11 | 2.3 | 424 | 89.1 | :** |
| 10 | 180 |  | 200 | 7 | 1.5 | 431 | 90.5 | :* |
| 11 | 200 |  | 220 | 15 | 3.2 | 446 | 93.7 | :** |
| 12 | 220 |  | 240 | 7 | 1.5 | 453 | 95.2 | :* |
| 13 | 240 |  | 260 | 4 | 0.8 | 457 | 96.0 | :* |
| 14 | 260 |  | 280 | 3 | 0.6 | 460 | 96.6 | : |
| 15 | 280 |  | 300 | 2 | 0.4 | 462 | 97.1 | : |
| 0 | Values | out | of range | 14 | 2.9 |  |  | : |


| Date/Time | 01-21-1991 13:32:45 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss\data\pel90snc |
| Description | Imported from A:pel90snc.prn |

## Detail Report

Variable: PB

| Mean - Average | 31.63235 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 27.96047 | No. missing values | 0 |
| Upper 95\% c.i.limit | 35.30423 | Sum of frequencies | 476 |
| Adj sum of squares | 793562.7 | Sum of observations | 15057 |
| Standard deviation | 40.87369 | Std.error of mean | 1.873442 |
| Variance | 1670.658 | T-value for mean=0 | 16.88461 |
| Coef. of variation | 1.292148 | T prob level | 0.0000 |
| Skewness | 4.932584 | Kurtosis | 32.53784 |
| Normality Test Value | 0.749 | Reject if > $1.011(10 \%)$ | 1.019 (5\%) |
| 100-\%tile (Maximum) | 436 | 90-\%tile | 55 |
| 75-\%tile | 33 | 10-\%tile | 8 |
| 50-\%tile (Median) | 22 | Range | 434 |
| 25-\%tile | 13 | 75th-25th \%tile | 20 |
| 0-\%tile (Minimum) | 2 |  |  |
|  |  |  |  |
| HZZZZXVHP4E333 312121 <br> -[Xma]---- |  |  |  |

## Distribution \& Histogram



| Date/Time | 01-21-1991 13:33:17 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss\data\pel90snc |
| Description | Imported from A:pel90snc.prn |

Detail Report
Variable: ZN

| Mean - Average | 96.05462 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 90.96709 | No. missing values | 0 |
| Upper 95\% c.i.limit | 101.1422 | Sum of frequencies | 476 |
| Adj sum of squares | 1523415 | Sum of observations | 45722 |
| Standard deviation | 56.63205 | Std.error of mean | 2.595726 |
| Variance | 3207.189 | T-value for mean=0 | 37.00492 |
| Coef. of variation | . 5895817 | T prob level | 0.0000 |
| Skewness | 2.674068 | Kurtosis | 10.93403 |
| Normality Test Value | 0.848 | Reject if > $1.011(10 \%)$ | 1.019 (5\%) |
| 100-\%tile (Maximum) | 493 | 90-\%tile | 170 |
| 75-\%tile | 112 | 10-\%tile | 50 |
| 50-\%tile (Median) | 79 | Range | 477 |
| 25-\%tile | 63 | 75th-25th \%tile | 49 |
| 0-\%tile (Minimum) | 16 |  |  |
|  |  |  |  |
|  |  |  |  |

## Distribution \& Histogram

| Variable: ZN |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower |  | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 |  | 20 | 1 | 0.2 | 1 | 0.2 | Histogram |
| 2 | 20 |  | 40 | 16 | 3.4 | 17 | 3.6 | : ** |
| 3 | 40 |  | 60 | 81 | 17.0 | 98 | 20.6 | : ************ |
| 4 | 60 |  | 80 | 141 | 29.6 | 239 | 50.2 | : ******************** |
| 5 | 80 |  | 100 | 90 | 18.9 | 329 | 69.1 | : ************* |
| 6 | 100 |  | 120 | 46 | 9.7 | 375 | 78.8 | : ******* |
| 7 | 120 |  | 140 | 31 | 6.5 | 406 | 85.3 | : **** |
| 8 | 140 |  | 160 | 17 | 3.6 | 423 | 88.9 | :** |
| 9 | 160 |  | 180 | 18 | 3.8 | 441 | 92.6 | :*** |
| 10 | 180 |  | 200 | 14 | 2.9 | 455 | 95.6 | : ** |
| 11 | 200 |  | 220 | 4 | 0.8 | 459 | 96.4 | :* |
| 12 | 220 |  | 240 | 4 | 0.8 | 463 | 97.3 | :* |
| 13 | 240 |  | 260 | 2 | 0.4 | 465 | 97.7 | : |
| 14 | 260 |  | 280 | 3 | 0.6 | 468 | 98.3 | : |
| 15 | 280 |  | 300 | 2 | 0.4 | 470 | 98.7 | : |
| 0 | Values | out | of range | 6 | 1.3 |  |  | : |


| Date/Time | 01-21-1991 13:33:59 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss \data \pel90snc |
| Description | Imported from A:pel90snc.prn |

Detail Report
Variable: AG

| Mean - Average | . 6352941 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | . 5683304 | No. missing values | 0 |
| Upper 95\% c.i.limit | . 7022579 | Sum of frequencies | 476 |
| Adj sum of squares | 263.9271 | Sum of observations | 302.4 |
| Standard deviation | . 7454099 | Std.error of mean | 3.416581E-02 |
| Variance | . 5556359 | T-value for mean=0 | 18.59444 |
| Coef. of variation | 1.17333 | T prob level | 0.0000 |
| Skewness | 3.975503 | Kurtosis | 25.68104 |
| Normality Test Value | 0.990 | Reject if > 1.011(10\%) | 1.019 (5\%) |
| 100-\%tile (Maximum) | 7.2 | 90-\%tile | 1.4 |
| 75-\%tile | . 8 | 10-\%tile | . 1 |
| 50-\%tile (Median) | . 4 | Range | 7.1 |
| 25-\%tile | . 2 | 75th-25th \%tile | . 6 |
| 0-\%tile (Minimum) | . 1 |  |  |
| . 1 | --L | / Box Plot | - |
| ZZZZXZ MKEIA9B855 13 <br> - [XmXXaX]------ | 131213 | 11 |  |

## Distribution \& Histogram

| Variable: AG |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 | . 2 | 93 | 19.5 | 93 | 19.5 | : ************* |
| 2 | . 2 | . 4 | 116 | 24.4 | 209 | 43.9 | : ***************** |
| 3 | . 4 | . 6 | 79 | 16.6 | 288 | 60.5 | :*********** |
| 4 | . 6 | . 8 | 57 | 12.0 | 345 | 72.5 | : ******** |
| 5 | . 8 | 1 | 34 | 7.1 | 379 | 79.6 | : ***** |
| 6 | 1 | 1.2 | 28 | 5.9 | 407 | 85.5 | : **** |
| 7 | 1.2 | 1.4 | 20 | 4.2 | 427 | 89.7 | :*** |
| 8 | 1.4 | 1.6 | 13 | 2.7 | 440 | 92.4 | :** |
| 9 | 1.6 | 1.8 | 6 | 1.3 | 446 | 93.7 | :* |
| 10 | 1.8 | 2 | 6 | 1.3 | 452 | 95.0 | :* |
| 11 | 2 | 2.2 | 5 | 1.1 | 457 | 96.0 | :* |
| 12 | 2.2 | 2.4 | 4 | 0.8 | 461 | 96.8 | :* |
| 13 | 2.4 | 2.6 | 6 | 1.3 | 467 | 98.1 | :* |
| 14 | 2.6 | 2.8 | 0 | 0.0 | 467 | 98.1 | : |
| 15 | 2.8 | 3 | 3 | 0.6 | 470 | 98.7 | : |
| 0 | Values | out of range | 6 | 1.3 |  |  | : |



Variable: FE\%

| Mean - Average | 6.840715 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 6.551989 | No. missing values | 0 |
| Upper 95\% c.i.limit | 7.12944 | Sum of frequencies | 476 |
| Adj sum of squares | 4906.543 | Sum of observations | 3256.18 |
| Standard deviation | 3.213964 | Std.error of mean | . 1473118 |
| Variance | 10.32956 | T-value for mean=0 | 46.43698 |
| Coef. of variation | . 4698287 | T prob level | 0.0000 |
| Skewness | 3.590145 | Kurtosis | 32.1059 |
| Normality Test Value | 0.918 | Reject if > 1.011 (10\%) | 1.019 (5\%) |
| 100-\%tile (Maximum) | 41.65 | 90-\%tile | 10.08 |
| 75-\%tile | 8.305 | 10-\%tile | 3.69 |
| 50-\%tile (Median) | 6.49 | Range | 41.1 |
| 25-\%tile | 4.915 | 75th-25th \%tile | 3.39 |
| 0-\%tile (Minimum) | . 55 |  |  |
| . 55 | -L | / Box Plot- | ----- |
| $32357 \mathrm{FNQZZZZZSSNRJEB664431} 2112$ |  |  |  |

Distribution \& Histogram

Date/Time $\quad 01-21-1991 \quad 13: 37: 00$
Data Base Name $C: \backslash s t a t s \backslash n c s s \backslash d a t a \backslash p e l 90$ snc
Description $\quad$ Imported from A:pel90snc.prn

Detail Report
Variable: AS


Distribution \& Histogram

| Bin | Lower | Upper | Count | Prent | Total | Prent | Histogram |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | 4 | 43 | 9.0 | 43 | 9.0 | :****** |
| 2 | 4 | 8 | 88 | 18.5 | 131 | 27.5 | : ************* |
| 3 | 8 | 12 | 79 | 16.6 | 210 | 44.1 | :*********** |
| 4 | 12 | 16 | 79 | 16.6 | 289 | 60.7 | :*********** |
| 5 | 16 | 20 | 57 | 12.0 | 346 | 72.7 | : ******** |
| 6 | 20 | 24 | 32 | 6.7 | 378 | 79.4 | : ***** |
| 7 | 24 | 28 | 8 | 1.7 | 386 | 81.1 | :* |
| 8 | 28 | 32 | 22 | 4.6 | 408 | 85.7 | :*** |
| 9 | 32 | 36 | 9 | 1.9 | 417 | 87.6 | : * |
| 10 | 36 | 40 | 5 | 1.1 | 422 | 88.7 | :* |
| 11 | 40 | 44 | 9 | 1.9 | 431 | 90.5 | :* |
| 12 | 44 | 48 | 5 | 1.1 | 436 | 91.6 | : * |
| 13 | 48 | 52 | 6 | 1.3 | 442 | 92.9 | :* |
| 14 | 52 | 56 | 1 | 0.2 | 443 | 93.1 | : |
| 15 | 56 | 60 | 3 | 0.6 | 446 | 93.7 | : |
| 0 | Values out | of range | 30 | 6.3 |  |  | : |



Variable: SB

| Mean - Average | 2.714286 | No. observations | 476 |
| :--- | :--- | :--- | :--- |
| Lower 95\% c.i.limit | 2.540229 | No. missing values | 0 |
| Upper 95\% c.i.limit | 2.888342 | Sum of frequencies | 476 |
| Adj sum of squares | 1783.143 |  | Sum of observations |


| 100-\%tile | (Maximum) | 34 | 90-\%tile | 4 |
| :---: | :---: | :---: | :---: | :---: |
| 75-\%tile |  | 3 | 10-\%tile | 2 |
| 50-\%tile | (Median) | 2 | Range | 32 |
| 25-\%tile |  | 2 | 75th-25th \%tile | 1 |
| 0-\%tile | (Minimum) | 2 |  |  |
| Z Z Y L | 732 |  | $\begin{aligned} & \text { / Box Plot } \\ & 1 \end{aligned}$ |  |

Distribution \& Histogram


| Date/Time | 01-21-1991 13:40:11 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss $\backslash$ data $\backslash$ pel90snc |
| Description | Imported from A:pel90snc.prn |

Detail Report
Variable: BI

| Mean - Average | 2.510504 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 2.387057 | No. missing values | 0 |
| Upper 95\% c.i.limit | 2.633951 | Sum of frequencies | 476 |
| Adj sum of squares | 896.9475 | Sum of observations | 1195 |
| Standard deviation | 1.374158 | Std.error of mean | $6.298444 \mathrm{E}-02$ |
| Variance | 1.88831 | T -value for mean=0 | 39.85912 |
| Coef. of variation | . 5473634 | T prob level | 0.0000 |
| Skewness | 5.015595 | Kurtosis | 36.55122 |
| 100-\%tile (Maximum) | 16 | 90-\%tile | 4 |
| 75-\%tile | 2 | 10-\%tile | 2 |
| 50-\%tile (Median) | 2 | Range | 14 |
| 25-\%tile | 2 | 75th-25th \%tile | 0 |
| 0-\%tile (Minimum) | 2 |  |  |
| 2 | ---Li | / Box Plot | --- |
| Z Z V V E | 92 | 1 | 1 |

Distribution \& Histogram


```
-------------Descriptive Statistics-------------------------------------
Date/Time 01-21-1991 13:41:23
Data Base Name C:\stats\ncss\data\pel90snc
Description Imported from A:pel90snc.prn
```

Detail Report

Variable: CA\%

| Mean - Average | . 2611975 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | . 2368418 | No. missing values | 0 |
| Upper 95\% c.i.limit | . 2855532 | Sum of frequencies | 476 |
| Adj sum of squares | 34.91442 | Sum of observations | 124.33 |
| Standard deviation | . 2711163 | Std.error of mean | $1.242659 \mathrm{E}-02$ |
| Variance | $7.350404 \mathrm{E}-02$ | T-value for mean=0 | 21.01923 |
| Coef. of variation | 1.037974 | T prob level | 0.0000 |
| Skewness | 4.237563 | Kurtosis | 28.61817 |
| Normality Test Value | 0.911 | Reject if > 1.011(10\%) | 1.019 (5\%) |
| 100-\%tile (Maximum) | 2.91 | 90-\%tile | . 5 |
| 75-\%tile | . 325 | 10-\%tile | . 06 |
| 50-\%tile (Median) | . 2 | Range | 2.89 |
| 25-\%tile | . 1 | 75th-25th \%tile | . 225 |
| 0-\%tile (Minimum) | . 02 |  |  |
| . 02 | -----Line | t / Box Plot | ---2.91 |
| 4ZZZZZZLQK8I97A42523 | 321112111 | 111 | 1 |

Distribution \& Histogram


| Date/Time | $01-21-1991 \quad 13: 47: 07$ |
| :--- | :--- |
| Data Base | Name $C: \backslash s t a t s \backslash n c s s \backslash d a t a \backslash p e l 90 s n c$ |
| Description | Imported from A:pel |

Detail Report
Variable: NA\%

| Mean - Average | 7.313025E-02 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 6.527023E-02 | No. missing values | 0 |
| Upper 95\% c.i.limit | 8.099028E-02 | Sum of frequencies | 476 |
| Adj sum of squares | 3.636236 | Sum of observations | 34.81 |
| Standard deviation | . 0874942 | Std.error of mean | 4.01029E-03 |
| Variance | $7.655234 \mathrm{E}-03$ | T-value for mean=0 | 18.23565 |
| Coef. of variation | 1.196416 | T prob level | 0.0000 |
| Skewness | 3.880473 | Kurtosis | 20.75063 |
| Normality Test Value | 0.831 | Reject if > $1.011(10 \%)$ | 1.019 (5\%) |
| 100-\%tile (Maximum) | . 77 | 90-\%tile | . 14 |
| 75-\%tile | . 09 | 10-\%tile | . 01 |
| 50-\%tile (Median) | . 05 | Range | . 76 |
| 25-\%tile | . 03 | 75th-25th \%tile | . 06 |
| 0-\%tile (Minimum) | . 01 |  |  |
| .01------- | --Line | / Box Plot- |  |
| ZZZZZTRPMDB8AC26463 <br> --[XmXaX]----- | 41211211 | 111111 | 11 |

Distribution \& Histogram

| Bin | Lower | Upper | Count | Prent | Total | Prent | Histogram |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | . 02 | 112 | 23.5 | 112 | 23.5 | :****** |
| 2 | . 02 | . 04 | 115 | 24.2 | 227 | 47.7 | :****** |
| 3 | . 04 | . 06 | 74 | 15.5 | 301 | 63.2 | :**** |
| 4 | . 06 | 8.000E-02 | 52 | 10.9 | 353 | 74.2 | :*** |
| 5 | 8.000E-02 | . 1 | 35 | 7.4 | 388 | 81.5 | :** |
| 6 | . 1 | . 12 | 19 | 4.0 | 407 | 85.5 | : * |
| 7 | . 12 | . 14 | 22 | 4.6 | 429 | 90.1 | :* |
| 8 | . 14 | . 16 | 8 | 1.7 | 437 | 91.8 | : |
| 9 | . 16 | . 18 | 4 | 0.8 | 441 | 92.6 | : |
| 10 | . 18 | . 2 | 10 | 2.1 | 451 | 94.7 | : * |
| 11 | . 2 | . 22 | 5 | 1.1 | 456 | 95.8 | : |
| 12 | . 22 | . 24 | 3 | 0.6 | 459 | 96.4 | : |
| 13 | . 24 | . 26 | 1 | 0.2 | 460 | 96.6 | : |
| 14 | . 26 | . 28 | 0 | 0.0 | 460 | 96.6 | : |
| 15 | . 28 | . 3 | 2 | 0.4 | 462 | 97.1 | : |
| 0 | Values out | of range | 14 | 2.9 |  |  | : |

```
----------------------------Descriptive Statistics----------------------------------
Date/Time 01-21-1991 13:47:49
Data Base Name C:\stats\ncss\data\pel90snc
Description Imported from A:pel90snc.prn
```

Detail Report
Variable: K\%

| Mean - Average | $7.680672 \mathrm{E}-02$ | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | $7.330445 \mathrm{E}-02$ | No. missing values | 0 |
| Upper 95\% c.i.limit | . 080309 | Sum of frequencies | 476 |
| Adj sum of squares | . 7219462 | Sum of observations | 36.56 |
| Standard deviation | $3.898573 \mathrm{E}-02$ | Std.error of mean | $1.786908 \mathrm{E}-03$ |
| Variance | 1.519887E-03 | T-value for mean=0 | 42.98304 |
| Coef. of variation | . 5075822 | T prob level | 0.0000 |
| Skewness | 1.285731 | Kurtosis | 2.929319 |
| Normality Test Value | 1.032 | Reject if > $1.011(10 \%)$ | 1.019 (5\%) |
| 100-\%tile (Maximum) | . 28 | 90-\%tile | . 13 |
| 75-\%tile | . 1 | 10-\%tile | . 04 |
| 50-\%tile (Median) | . 07 | Range | . 27 |
| 25-\%tile | . 05 | 75th-25th \%tile | . 05 |
| 0-\%tile (Minimum) | . 01 |  |  |
| . 01 | --Line | t / Box Plot | . 28 |
|  | $\begin{array}{ccc} \mathrm{Z} & \mathrm{X} & \mathrm{O} \\ \mathrm{XXXXX} \end{array}$ | $\begin{array}{lllllll}\text { C } & 4 & 8 & 2 & 4 & 3 & 1\end{array}$ | 111 |

Distribution \& Histogram

| Bin | Lower | Upper | Count | Prent | Total | Prent | Histogram |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 0 | . 02 | 12 | 2.5 | 12 | 2.5 | :* |
| 2 | . 02 | . 04 | 83 | 17.4 | 95 | 20.0 | : **** |
| 3 | . 04 | . 06 | 125 | 26.3 | 220 | 46.2 | :******* |
| 4 | . 06 | 8.000E-02 | 86 | 18.1 | 306 | 64.3 | : ***** |
| 5 | 8.000E-02 | . 1 | 77 | 16.2 | 383 | 80.5 | :**** |
| 6 | . 1 | . 12 | 39 | 8.2 | 422 | 88.7 | :** |
| 7 | . 12 | . 14 | 29 | 6.1 | 451 | 94.7 | :** |
| 8 | . 14 | . 16 | 12 | 2.5 | 463 | 97.3 | :* |
| 9 | . 16 | . 18 | 2 | 0.4 | 465 | 97.7 | : |
| 10 | . 18 | . 2 | 7 | 1.5 | 472 | 99.2 | : |
| 11 | . 2 | . 22 | 1 | 0.2 | 473 | 99.4 | : |
| 12 | . 22 | . 24 | 1 | 0.2 | 474 | 99.6 | : |
| 13 | . 24 | . 26 | 0 | 0.0 | 474 | 99.6 | : |
| 14 | . 26 | . 28 | 2 | 0.4 | 476 | 100.0 | : |
| 15 | . 28 | . 3 | 0 | 0.0 | 476 | 100.0 |  |


| Date/Time | 01-21-1991 13:48:56 |
| :---: | :---: |
| Data Base Name | C: \stats ncss $\backslash$ data $\backslash$ pel 90 snc $^{\text {a }}$ |
| Description | Imported from A:pel90snc.prn |

Detail Report
Variable: AUPPB

| Mean - Average | 92.42017 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 66.78626 | No. missing values | 0 |
| Upper 95\% c.i.limit | 118.0541 | Sum of frequencies | 476 |
| Adj sum of squares | $3.867534 \mathrm{E}+07$ | Sum of observations | 43992 |
| Standard deviation | 285.345 | Std.error of mean | 13.07877 |
| Variance | 81421.77 | T-value for mean=0 | 7.066428 |
| Coef. of variation | 3.087476 | T prob level | 0.0000 |
| Skewness | 6.628696 | Kurtosis | 50.94736 |
| Normality Test Value | 0.590 | Reject if > 1.011 (10\%) | 1.019(5\%) |
| 100-\%tile (Maximum) | 3080 | 90-\%tile | 164 |
| 75-\%tile | 65.5 | 10-\%tile | 2 |
| 50-\%tile (Median) | 19.5 | Range | 3079 |
| 25-\%tile | 4 | 75th-25th \%tile | 61.5 |
| 0-\%tile (Minimum) | 1 |  |  |
|  | ------Line | / Box Plot- |  |
| $\mathrm{m}-\mathrm{a}--$ | 22 | 112 |  |

## Distribution \& Histogram

| Variable: AUPPB |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower | Upper | Count | Prent | Total | Prent | Histogram |
| 1 | 0 | 5 | 125 | 26.3 | 125 | 26.3 | :******* |
| 2 | 5 | 10 | 57 | 12.0 | 182 | 38.2 | : *** |
| 3 | 10 | 15 | 31 | 6.5 | 213 | 44.7 | :** |
| 4 | 15 | 20 | 25 | 5.3 | 238 | 50.0 | :* |
| 5 | 20 | 25 | 17 | 3.6 | 255 | 53.6 | : * |
| 6 | 25 | 30 | 21 | 4.4 | 276 | 58.0 | : * |
| 7 | 30 | 35 | 23 | 4.8 | 299 | 62.8 | :* |
| 8 | 35 | 40 | 8 | 1.7 | 307 | 64.5 | : |
| 9 | 40 | 45 | 9 | 1.9 | 316 | 66.4 | : |
| 10 | 45 | 50 | 12 | 2.5 | 328 | 68.9 | :* |
| 11 | 50 | 55 | 10 | 2.1 | 338 | 71.0 | :* |
| 12 | 55 | 60 | 9 | 1.9 | 347 | 72.9 | : |
| 13 | 60 | 65 | 2 | 0.4 | 349 | 73.3 | : |
| 14 | 65 | 70 | 17 | 3.6 | 366 | 76.9 | : * |
| 15 | 70 | 75 | 3 | 0.6 | 369 | 77.5 | : |
| 0 | Values | out of range | 107 | 22.5 |  |  | : |


| Date/Time | 01-21-1991 13:49:19 |
| :---: | :---: |
| Data Base Name | C: \stats\ncss\data \pel90snc |
| Description | Imported from A:pel90snc.prn |

Detail Report
Variable: AUPPB

| Mean - Average | 92.42017 | No. observations | 476 |
| :---: | :---: | :---: | :---: |
| Lower 95\% c.i.limit | 66.78626 | No. missing values | 0 |
| Upper 95\% c.i.limit | 118.0541 | Sum of frequencies | 476 |
| Adj sum of squares | $3.867534 \mathrm{E}+07$ | Sum of observations | 43992 |
| Standard deviation | 285.345 | Std.error of mean | 13.07877 |
| Variance | 81421.77 | T-value for mean=0 | 7.066428 |
| Coef. of variation | 3.087476 | T prob level | 0.0000 |
| Skewness | 6.628696 | Kurtosis | 50.94736 |
| Normality Test Value | 0.590 | Reject if > 1.011(10\%) | 1.019 (5\%) |
| 100-\%tile (Maximum) | 3080 | 90-\%tile | 164 |
| 75-\%tile | 65.5 | 10-\%tile | 2 |
| 50-\%tile (Median) | 19.5 | Range | 3079 |
| 25-\%tile | 4 | 75th-25th \%tile | 61.5 |
| 0-\%tile (Minimum) | 1 |  |  |
|  |  |  |  |
| ZZZKD83552 2211121 |  |  |  |
| m-a-- |  |  |  |

Distribution \& Histogram

| Variable: AUPPB |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Bin | Lower | Upper | Count | Prent | Total | Pront | Histogram |
| 1 | 0 | 100 | 399 | 83.8 | 399 | 83.8 | :********************* |
| 2 | 100 | 200 | 38 | 8.0 | 437 | 91.8 | : ** |
| 3 | 200 | 300 | 11 | 2.3 | 448 | 94.1 | :* |
| 4 | 300 | 400 | 7 | 1.5 | 455 | 95.6 | : |
| 5 | 400 | 500 | 4 | 0.8 | 459 | 96.4 | : |
| 6 | 500 | 600 | 2 | 0.4 | 461 | 96.8 | : |
| 7 | 600 | 700 | 3 | 0.6 | 464 | 97.5 | : |
| 8 | 700 | 800 | 1 | 0.2 | 465 | 97.7 | : |
| 9 | 800 | 900 | 2 | 0.4 | 467 | 98.1 | : |
| 10 | 900 | 1000 | 0 | 0.0 | 467 | 98.1 | : |
| 11 | 1000 | 1100 | 2 | 0.4 | 469 | 98.5 | : |
| 12 | 1100 | 1200 | 0 | 0.0 | 469 | 98.5 | : |
| 13 | 1200 | 1300 | 0 | 0.0 | 469 | 98.5 | : |
| 14 | 1300 | 1400 | 0 | 0.0 | 469 | 98.5 | : |
| 15 | 1400 | 1500 | 1 | 0.2 | 470 | 98.7 | : |
| 0 | values | out of range | 6 | 1.3 |  |  | : |

## Correlations - Soil

|  | AS | SB | BI | PB | AG | FE\% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\pm$ | 1.0000 | 0.1871 | 0.1541 | 0.4757 | 0.5902 | 0.3674 |
| 31 | 0.1871 | 1.0000 | -0.0273 | 0.0106 | 0.0380 | 0.0410 |
| 31 | 0.1541 | -0.0273 | 1.0000 | 0.1510 | 0.2196 | 0.1171 |
| ? B | 0.4757 | 0.0106 | 0.1510 | 1.0000 | 0.5182 | 0.1165 |
| 15 | 0.5902 | 0.0380 | 0.2196 | 0.5182 | 1.0000 | 0.1446 |
| $\cdots$ | 0.3674 | 0.0410 | 0.1171 | 0.1165 | 0.1446 | 1.0000 |
| $\pm$ IUPPB | 0.5197 | 0.0408 | 0.1336 | 0.5416 | 0.5551 | 0.0986 |

## APPENDIX XII

## ROCK SAMPLE DESCRIPTIONS - 1990

## ROCK SAMPLE DESCRIPTIONS-1990

ALL SAMPLES

| SAMPLE <br> NUMBER | TARGET AREA | DESCRIPTION |
| :---: | :---: | :---: |
| PEL-90-G-1R | SOUTHEAST | GRAB;QUARTZ-PYRITE VEIN ALONG CREEK |
| 2 | SOUTHEAST | FLOAT;10 CM QTZ-PY,25\% PY,COARSE QTZ |
| 3 | SOUTHEAST | FLOAT;10 CM QTZ-PY,25\% PY,COARSE QTZ |
| 4 | PELICAN | GRAB;PYRITIZED BOULDERS AT EDGE OF CLIFF |
| 5 | PELICAN | GRAB;PYRITIZED BOULDERS AT EDGE OF CLIFF |
| 6 | PELICAN | GRAB;PYRITIZED SILICIFIED SILTSTONE |
| 7 | PELICAN | GRAB;PYRITIZED SILICIFIED SILTSTONE |
| 8 | PELICAN | GRAB;PYRITIZED SILICIFIED SILTSTONE |
| 9 | PELICAN | GRAB;MASSIVE E-W PY VEIN,DIP 80 S |
| 10 | PELICAN | FLOAT;PYRITIZED,SILICIFIED BOULDERS |
| 11 | PELICAN | FLOAT;PYRITIZED,SILICIFIED BOULDERS |
| 12 | PELICAN | GRAB;1-4CM PYRITE VEINS, 20 DIP S |
| 13 | PELICAN | GRAB;1-4CM PYRITE VEINS, 20 DIP S |
| 14 | PELICAN | GRAB;HYDROZINCITE,DISS.PYRITE |
| 15 | PELICAN | GRAB 20 CM;VERTICAL N-S QTZ-PY VEIN |
| 16 | SOUTHEAST | grab;qtz-py vein near site 87-521 |
| 17 | SOUTHEAST | grab;qtz-py vein near site 87-521 |
| 18 | SOUTHEAST | grab;qtz-py vein near site 87-521 |
| 19 | SOUTHEAST | grab;qtz-py vein near site 87-521 |
| 20 | SOUTHEAST | grab;qtz-py vein near site 87-521 |
| 21 | SOUTHEAST | grab;pyritized highly fractured |
| 22 | SOUTHEAST | float;quartz-pyrite vein 5\%-10\% py |
| 23 | SOUTHEAST | float;quartz-pyrite vein 5\%-10\% py |
| 24 | SOUTHEAST | float;quartz-pyrite vein 5\%-10\% py |
| 25 | SOUTHEAST | grab;ferricrete 3m thick above shear |
| 26 | SOUTHEAST | grab;granodiorite;mod. fract.,5\% py |
| 27 | SOUTHEAST | grab;1-2cm qtz veins at 205/60N |
| 28 | SOUTHEAST | float;sercitized, pyritized granodiorite |
| 29 | SOUTHEAST | GRAB;FERRICRETE,4-5M THICK |
| 30 | SOUTHEAST | GRAB;SILIC.,BLEACH.GRANODIORITE,5\% PY |
| 31 | SOUTHEAST | GRAB;STRONG SHEAR,SERCITE SCHIST,5\%PY |
| 32 | SOUTHEAST | GRAB;ORTHO.PORPH.,INTENS.FRACT.,3\% PY |
| 33 | SOUTHEAST | GRAB;GRAB;ORTH.PORPH.SILIC..3\%PY |
| 34 | SOUTHEAST | GRAB;FRACT. SILTSTONE,SERIC.,3\%PY |
| 35 | SOUTHEAST | GRAB;SILTSTONE,BLEACH.,SERIC.,3\% PY |
| 36 | SOUTHEAST | QTZ.VEINS,1-10CM,VUGGY,COARSE,CHLORITE |
| 37 | SOUTHEAST | GRAB;SHEAR GOUGE,315/75E |
| 38 | SOUTHEAST | GRAB;SHEAR |
| 39 | SOUTHEAST | GRAB;QTZ.VEIN,5CM,GRANOD.,N-S/85W |
| 40 | SOUTHEAST | GRAB;SHEAR,5\%,PY,BLEACHED INTRUS. |
| 41 | SOUTHEAST | GRAB;SHEAR,5\%,PY,BLEACHED INTRUS. |

42 SOUTHEAST
43 SOUTHEAST
44 SOUTHEAST
45 SOUTHEAST
46 SOUTHEAST
47 SOUTHEAST
48 SOUTHEAST
49 SOUTHEAST
50 SOUTHEAST
51 SOUTHEAST
52 SOUTHEAST
53 SOUTHEAST
54 SOUTHEAST
55 SOUTHEAST
56 SOUTHEAST
57 SOUTHEAST
58 SOUTHEAST
59 SOUTHEAST
60 SOUTHEAST
61 SOUTHEAST
62 SJ ZONE
63 SNOW
64 SNOW
65 SNOW
66 SNOW
67 SNOW
68 SNOW
69 SNOW
70 SNOW
71 SNOW
72 SNOW
73 SNOW
74 SNOW
75 SNOW
76 SNOW
77 SNOW
78 SNOW
79 SNOW
80 SNOW
81 SNOW
82 SNOW
83 SNOW
84 SNOW
85 SNOW
86 SNOW
87 SNOW
88 SNOW
89 SNOW

GRAB;GOSSAN EXTREMELY FRACT.
GRAB;GOSSAN EXTREMELY FRACT.
GRAB;SHEAR,2M,170/60E
GRAB;SILTSTONE,BLEACH.,3\%PY,SILIC.
5CM;RUSTY SHEAR,090/85N
GRAB;GOSSAN,EXTREMELY WEATHERED
GRAB;SILTSTONE,SERICITIZED,5\%PY
GRAB 20CM;150/60W
GRAB;DIORITE,SHATTERED,MODER. FE STAIN
GRAB;DIORITE,SHATTERED,MODER. FE STAIN
GRAB 5CM;QUARTZ VEIN,150/70S
GRAB;QTZ-CALCITE-CHLORITE VEIN,5CM
GRAB;SHEAR,DIORITE,N-S/45E
GRAB;SHEAR,DIORITE,N-S/45E
GRAB;RUSTY SHEAR,DIORITE
FLOAT;QUARTZ VEIN,CHLORITE,FE-CARBONATE FLOAT;QUARTZ VEIN,CHLORITE,FE-CARBONATE GRAB;SHEAR,DIORITE,8\% DISS. PY
GRAB 40CM;SHEAR,DIORITE,SILICIFIED
GRAB;GOUGE AND INTERMIXED PYRITE
FLOAT;QUARTZ-PYRITE VEIN
FLOAT;QUARTZ VEIN MINOR PYRITE GRAB 5CM;QUARTZ-CARBONATE VEIN
GRAB;QUARTZ VEIN 070/STEEPN FLOAT; QUARTZ VEIN
GRAB;RUSTY GOSSAN ABOVE STRONG SHEAR GRAB;SHEAR,BLEACH.QTZ VEINING,MALACHITE
GRAB;SHEAR,BLEACH.QTZ VEINING,MALACHITE
GRAB;SHEAR,BLEACH.QTZ VEINING,MALACHITE FLOAT?;RUBBLE WITHIN TRACE OF SHEAR 4CM;VUGGY QUARTZ-CHLORITE,N-S/62W FLOAT;EPIDOTE,BLEACH.,MALACHITE,PY FLOAT;EPIDOTE,BLEACH.,MALACHITE,PY FLOAT;SILTSTONE,MALACHITE
GRAB 2CM;BLEACH.,PYRITIZATION ALONG SHEAR GRAB 2CM;BLEACH.,PYRITIZATION ALONG SHEAR FLOAT;RUSTY,COARSE QUARTZ
GRAB 40 CM;QUARTZ IN FLAT SHEAR,MINOR PY GRAB 40 CM; QUARTZ IN FLAT SHEAR,MINOR PY GRAB 40 CM;QUARTZ IN FLAT SHEAR,MINOR PY GRAB 40 CM;QUARTZ IN FLAT SHEAR,MINOR PY GRAB;BRECCIATED VOLC.,IRREG.PY INFILLING GRAB;BRECCIATED VOLC.,IRREG.PY INFILLING FLOAT;SILTSONE,MALACHITE,DISS. PY FLOAT;SILTSONE,MALACHITE,DISS. PY 4 CM;QUARTZ IN SHEAR,120/68S
GRAB 50 CM;INTERMIXED PY \&BRECCIATED VOLC. GRAB 50 CM ;INTERMIXED PY \&BRECCIATED VOLC.

| 90 | SNOW | FLOAT;QUARTZ-PYRITE ,30\% PYRITE |
| :---: | :---: | :---: |
| 91 | SNOW | FLOAT;QUARTZ-PYRITE ,30\% PYRITE |
| 92 | SNOW | FLOAT;QUARTZ-PYRITE ,30\% PYRITE |
| 93 | SNOW | FLOAT;QUARTZ-PYRITE ,30\% PYRITE |
| 94 | SNOW | FLOAT;VUGGY QUARTZ-PYRITE |
| 95 | SNOW | GRAB 5CM;QUARTZ VEIN @005/70W |
| 96 | SNOW | FLOAT;QUARTZ VEIN WITH 25\% PYRITE |
| PEL-90-J-1R | SOUTHEAST | GRAB;SILTSTONE,3\% DISS. PY,FE STAINED |
| 2 | SOUTHEAST | GRAB 3M;SHEARED SERICITE SCHIST |
| 3 | SOUTHEAST | GRAB 3M;SHEARED SERICITE SCHIST |
| 4 | SOUTHEAST | GRAB 3M;SHEARED SERICITE SCHIST |
| 5 | SOUTHEAST | CHIP 10CM;GOSSAN WITH FLAT SHEARING |
| 6 | SOUTHEAST | GRAB 4CM;QUARTZ VEIN |
| 7 | SOUTHEAST | GRAB;SHEARED DIORITE,2-3\% DISS. PY |
| 8 | SOUTHEAST | GRAB;SHEAR,DIORITE,060/85W,3\% DISS. PY |
| 9 | SOUTHEAST | GRAB;DIORITE,3\% DISS. PYRITE |
| 10 | SOUTHEAST | FLOAT;4CM PYRITE BAND IN QUARTZ VEIN |
| 11 | SOUTHEAST | FLOAT;SAME ROCK AS \#10 QUARTZ ONLY |
| 12 | SOUTHEAST | FLOAT;QUARTZ,4\% PYRITE IN 5CM CLOTS |
| 13 | SOUTHEAST | GRAB;SHEAR,CHLORITIC,3\% DISS. PYRITE |
| 14 | SOUTHEAST | GRAB;SHATTERED DIORITE,2\% PY,3CM QTZ VEIN |
| 15 | SOUTHEAST | GRAB 15CM; QUARTZ WITH 3-5\% COARSE PYRITE |
| 16 | SOUTHEAST | GRAB 15CM;QUARTZ WITH 3-5\% COARSE PYRITE |
| 17 | SOUTHEAST | GRAB;DIORITE,UNALTERED,WITIN 50 CM OF \#16 |
| 18 | SOUTHEAST | GRAB 25CM;QUARTZ VEIN WITH 5\% PYRITE |
| 19 | SOUTHEAST | CHIP 2M;SILICIFIED ROCK, PYRITIZED |
| 20 | SOUTHEAST | CHIP 1M;SILICIFIED ROCK,PYRITIZED |
| 21 | SOUTHEAST | GRAB 20 CM ;QUARTZ VEIN, 10\% COARSE PYRITE |
| 22 | SOUTHEAST | GRAB 20 CM;QUARTZ VEIN,8\% COARSE PYRITE |
| 23 | SOUTHEAST | GRAB 20 CM;QUARTZ VEIN, 10\% COARSE PYRITE |
| 24 | SOUTHEAST | GRAB;SILICIFIED,5-10\% DISS. PYRITE(88-J-81) |
| 25 | SOUTHEAST | FLOAT; 20 CM QUARTZ VEIN,10\% COARSE PYRITE |
| 26 | LAKE-AIRBORNE EM | DIORITE,SILICIFIED,5\% DISS. PYRITE |
| 27 | LAKE-AIRBORNE EM | DIORITE,SILICIFIED,5\% DISS. PYRITE |
| 28 | LAKE-AIRBORNE EM | BASALT DYKE,BLACK,3-5\% DISS. PYRITE |
| 29 | LAKE-AIRBORNE EM | GRAB;GOSSAN,SILICIFIED,2\% DISS. PYRITE |
| 30 | LAKE-AIRBORNE EM | GRAB;GOSSAN,SILICIFIED,2\% DISS. PYRITE |
| 31 | LAKE-AIRBORNE EM | GRAB;GOSSAN,SILICIFIED,2\% DISS. PYRITE |
| 32 | LAKE-AIRBORNE EM | GRAB;BASALT DYKE,DK GREEN,2-3\% DISS. PY |
| 33 | LAKE-AIRBORNE EM | GRAB;DIORITE,SILICIFIED,FE STAINED,2\% PY |
| 34 | LAKE-AIRBORNE EM | GRAB;DIORITE,SILICIFIED,FE STAINED,2\% PY |
| 35 | SOUTHEAST | GRAB 3M;SHEAR,DIORITE,SILICIFIED,1-2\% PY |
| 36 | SOUTHEAST | GRAB;SHATTERED CHERT,1-2\% DISS. PYRITE |
| 37 | SOUTHEAST | GRAB;SHATTERED CHERT,1-2\% DISS. PYRITE |
| 38 | SOUTHEAST | GRAB;SHATTERED CHERT,1-2\% DISS. PYRITE |
| 39 | SERICITE NORTH | GRAB;SERICITE SCHIST,SILICA,3\% PY |
| 40 | SERICITE NORTH | GRAB;SERICITE SCHIST,SILICA,3\% PY |
| 41 | SERICITE NORTH | GRAB;SERICITE SCHIST,SILICA,<1\% PY |


| 42 | SERICITE NORTH | CHIP 2M:SERICITE-SILICA ROCK,FE STAINED |
| :---: | :---: | :---: |
| 43 | SERICITE NORTH | FLOAT;VERY SILICIFIED SERICIT ROCK,FE STAIN |
| 44 | SERICITE NORTH | FLOAT;TALUS |
| 45 | SERICITE NORTH | GRAB;DIORITE?,HYROZINCITE? |
| 46 | SERICITE NORTH | GRAB;SHATTERED,SICIFIED ROCK,1-2\% PY |
| 47 | SERICITE NORTH | FLOAT;CHLORITIC,SILICA ROCK,GREEN STAIN |
| 48 | SERICITE NORTH | CHLORITIC ALTERED ROCK,NUMEROUS QTZ VEINS |
| 49 | SNOW | GRAB;WEAKLY PYRITIZED BASALT |
| 50 | SNOW | GRAB 10CM; QUARTZ VEIN 30\% PYRITE |
| 51 | SNOW | GRAB 20CM; IRREGULAR QUARTZ VEINS |
| 52 | SNOW | GRAB 3M;SILICIFIED,1M QTZ VEINS,1\% DISS. PY |
| 53 | SNOW | GRAB 5M;SILICIFIED |
| 54 | SNOW | GRAB;QUARTZ VEIN ,5\% PYRITE |
| 55 | SNOW | GRAB 20CM;QUARTZ VEIN IN BASALT?,DIORITE? |
| 56 | SNOW | GRAB:GOSSAN,4\% DISS. PYRITE |
| 57 | SNOW | GRAB:GOSSAN,4\% DISS. PYRITE |
| 58 | SNOW | GRAB:GOSSAN,4\% DISS. PYRITE |
| 59 | SNOW | GRAB:GOSSAN,4\% DISS. PYRITE |
| 60 | SNOW | GRAB;FRACT.,SILICIFIED SILTSTONE |
| 61 | SNOW | GRAB;BOXWORK GOSSAN |
| 62 | SNOW | GRAB;BOXWORK GOSSAN |
| 63 | SNOW | GRAB 10 CM;QUARTZ,25\% PYRITE |
| 64 | SNOW | GRAB;IRREGULAR QUARTX VEIN,5\% pyrite |
| 65 | SJ ZONE | FLOAT;QUARTX VEIN,2\% PYRITE |
| 66 | SJ ZONE | FLOAT;GOSSAN BOXWORK |
| 67 | SJ ZONE | GRAB;SHEAR,FRACT.,SILICIFIED,50M WIDTH |
| 68 | SJ ZONE | GRAB;4-4CM QTZ VEINS,CHLORITE CLOTS |
| 69 | SJ ZONE | GRAB 4CM;QTZ VEIN,CHLORITE,160/20W |
| 70 | SJ ZONE | GRAB;SILTSTONE,BLEACH.,SERICITIZED.3\% PY |
| 71 | SJ ZONE | GRAB 3CM;QUARTZ VEIN;8\% PYRITE |
| 72 | SJ ZONE | GRAB;SLICIFIED,3-5\% DISS. PYRITE |
| 73 | SJ ZONE | GRAB;SLICIFIED,3-5\% DISS. PYRITE |
| 74 | SJ ZONE | GRAB;SLICIFIED,3-5\% DISS. PYRITE |
| 75 | SJ ZONE | GRAB:SILICFIED,FRACT.,5-10\% DISS. PYRITE |
| 76 | SJ ZONE | GRAB:SILICFIED,FRACT.,5-10\% DISS. PYRITE |
| 77 | SJ ZONE | GRAB 5M;SHEAR,SERICITE SCHIST, 1 MM PY SEAMS |
| 78 | SJ ZONE | GRAB;GOSSAN |
| 79 | SJ ZONE | GRAB;GOUGE,SHEAR IN SAMPLE \#77 |
| 80 | SJ ZONE | CHIP 2M;SHEAR |
| 81 | SJ ZONE | CHIP 2M;SHEAR |
| 82 | SJ ZONE | CHIP 2.5M;SHEAR AND ADJ PY-SILICA |
| 83 | SJ ZONE | GRAB;SILICIFIED,PYRITIZED |
| 84 | SJ ZONE | GRAB;QUARTZ VEIN,10\% PYRITE |
| 85 | SJ ZONE | GRAG,VERY SILICIFIED, $1 \%$ PYRITE |
| 86 | PELICAN | GRAB;GOSSAN ABOVE MAIN ZONE |
| 87 | PELICAN | GRAB 40CM;SHEAR,N-S,VERTICAL |
| 88 | PELICAN | GRAB;SHEAR,065/90 |
| 89 | PELICAN | GRAB 5CM;QUARTZ VEIN 2-3\% PY,060/90 |

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GRAB 50CM;QUART $\angle$ VEIN,090/70S
GRAB 15 CM;QUARTZ VEIN,2\% SPHALERITE
GRAB 1.5M;FLAT SHEAR,FE STAINED
GRAB 1.5M;FLAT SHEAR,FE STAINED GRAB;20 CM;TOP OF FLAT SHEAR,40\% PY ARGILLITE,SILTSTONE,BANDED,FE STAINED ARGILLITE,SILTSTONE,BANDED,FE STAINED GRAB 3M;FLAT SHEAR WITH 1-5 CM QUARTZ VEINS GRAB 3M;FLAT SHEAR WITH 1-5 CM QUARTZ VEINS GRAB 3M;FLAT SHEAR WITH 1-5 CM QUARTZ VEINS GRAB;RUSTY SHEAR IN DIORITE GRAB;5\% PYRITE IN 1CM CLOTS GRAB;BOXWORK GOSSAN,3\% DISS. PYRITE FLOAT;SILICA ROCK,3\% diss. pyrite FLOAT;SILICA ROCK,3\% diss. pyrite grab 20 cm ;quartz vein grab;quartz vein unkown width grab;siltstone,rusty grab;silicified,trace pyrite grab 30 cm ;silica rock, $30-40 \%$ pyrite grab;silicified,fractured,2\% diss. pyrite grab;gossan boxwork,estimate 40\% py grab;diorite,silicified, $10 \%$ diss. pyrite grab $18 \mathrm{~cm} ; 8 \mathrm{~cm}$ galena, 10 cm silicifed rock grab 1.5 m ;silicified rock adjacent to \#113
grab 40 cm;rusty qtz vein,133/60w
grab 3.5 m ;shear, $125 / 45 \mathrm{sw}$
grab;siltstone,silicified
grab;sheared diorite dyke
grab;sheared diorite dyke
grab;gossan,silicified,2-3\% pyrite
grab,float;quartz,5\% pyrite
grab;silicified,2-3\% pyrite
grab 60 cm ;vuggy quartz vein, no pyrite
grab $30-60 \mathrm{~cm}$;irregular qtz vein, $8 \%$ py
grab 25 cm ;quartz vein, 10-20\% pyrite grab;pyrite intermixed with quartz grab 1m;shear, 1-2 cm seams of pyrite float;95\% pyrite intermixed with quartz grab;irregular qtz-pyrite veins grab;silicified, 1-2\% diss py,fractured

