

GEOLOGICAL and GEOCHEMICAL
EXPLORATION REPORT

on the

JO 1-8 and CRO 1-5 MINERAL CLAIMS
NEW KC PROJECT

Omineca Mining Division, BC

Golden Rule Resources

2128

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NEW KC PROJECT
Omineca Mining Division, BC

February, 1991

for

GOLDEN RULE RESOURCES LTD.

by

Michael Fox
Consulting Geologist

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GEOLOGICAL and GEOCHEMICAL
EXPLORATION REPORT
JO 1-8 and CRO 1-5 MINERAL CLAIMS

Latitude 56 deg. 30'N
Longitude 126 deg. 05'W

NTS 94-D-8E/9E

Omineca Mining Division, British Columbia

for

GOLDEN RULE RESOURCES LTD.
#410, 1122 - 4TH STREET S.W.
CALGARY, AB T2R 1M1

by

Michael Fox, Consulting Geologist
Calgary, Alberta

February, 1991

G E O L O G I C A L B R A N C H
A S S E S S M E N T R E P O R T

21,502

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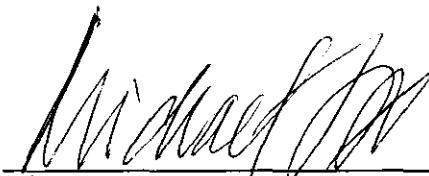
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| Map 1 | Compilation Map (Geology and Geochemical Analyses) |
|-------|--|

CERTIFICATE

I, Michael Fox, hereby certify that:

1. I reside at 5008 Varsity Dr., N.W., Calgary, Alberta.
2. I received a B.Sc. in geology from the University of British Columbia in 1974.
3. I have worked in the field of mineral exploration since 1965 and I have practiced my profession as a mineral exploration geologist continuously since 1974.
4. I am a member of the Association of Professional Engineers, Geologists, and Geophysicists of Alberta.
5. I am the author of the report entitled "Geological and Geochemical Exploration Report on the JO 1 to 8 and CRO 1 to 5 Mineral Claims", Omineca Mining Division, British Columbia.
6. This report is based on the references cited in the bibliography, and on field work carried out during parts of July, August and September, 1990.
7. I have no interest, direct or indirect, in the securities of Golden Rule Resources Ltd., nor any of its affiliated companies, nor do I expect to receive any.



Michael Fox, P.Geol.

February, 1991

SUMMARY

During parts of July, August, and September, 1990, a helicopter-supported program of reconnaissance geological mapping and stream silt geochemical sampling was carried out on the JO 1 to 8 and CRO 1 to 5 claims located in the Johanson Lake area (N.T.S 94-D-8E/9E) of north-central British Columbia.

The claims cover part of the Triassic - Jurassic island arc assemblage referred to as "Quesnellia" or Quesnel Terrane in an area of complex structure where several cupola or stock-like satellitic intrusions of the Hogem batholith intrude Takla Group (island arc) volcanic rocks.

The geological environment is considered favorable for hosting porphyry type Cu/Mo/Au mineralization as well as auriferous chalcopyrite-magnetite skarns.

Work to date has not identified any specific geological targets for more detailed evaluation, but numerous Au/Cu/Mo-in-stream silt anomalies have been identified that warrant follow-up work.

INTRODUCTION1.1 Location and Access

The JO 1 to 8 and CRO 1 to 5 claims are located in N.T.S. map-areas 94-D-8E and 94-D-9E approximately 360 km northwest of Prince George, B.C., astride the headwaters of Kliyul Creek, Darb Creek, and a tributary of Lay Creek (Figure 1) at 56 degrees 30' N latitude and 126 degrees 05' W longitude (Figure 2). The Omineca Mine Access Road passes 6 km north of the claims and a gravel airstrip is located 10 km to the northwest at Johanson Lake. Helicopter support for the reconnaissance geological mapping and geochemical sampling described in this report was provided in part by a Northern Mountain Helicopters Ltd. Bell 206-B helicopter based temporarily at Johanson Lake and in part by a Northern Mountain Bell 206-B helicopter working under contract to Golden Rule Resources Ltd. from a temporary base at Germansen Landing, B.C.

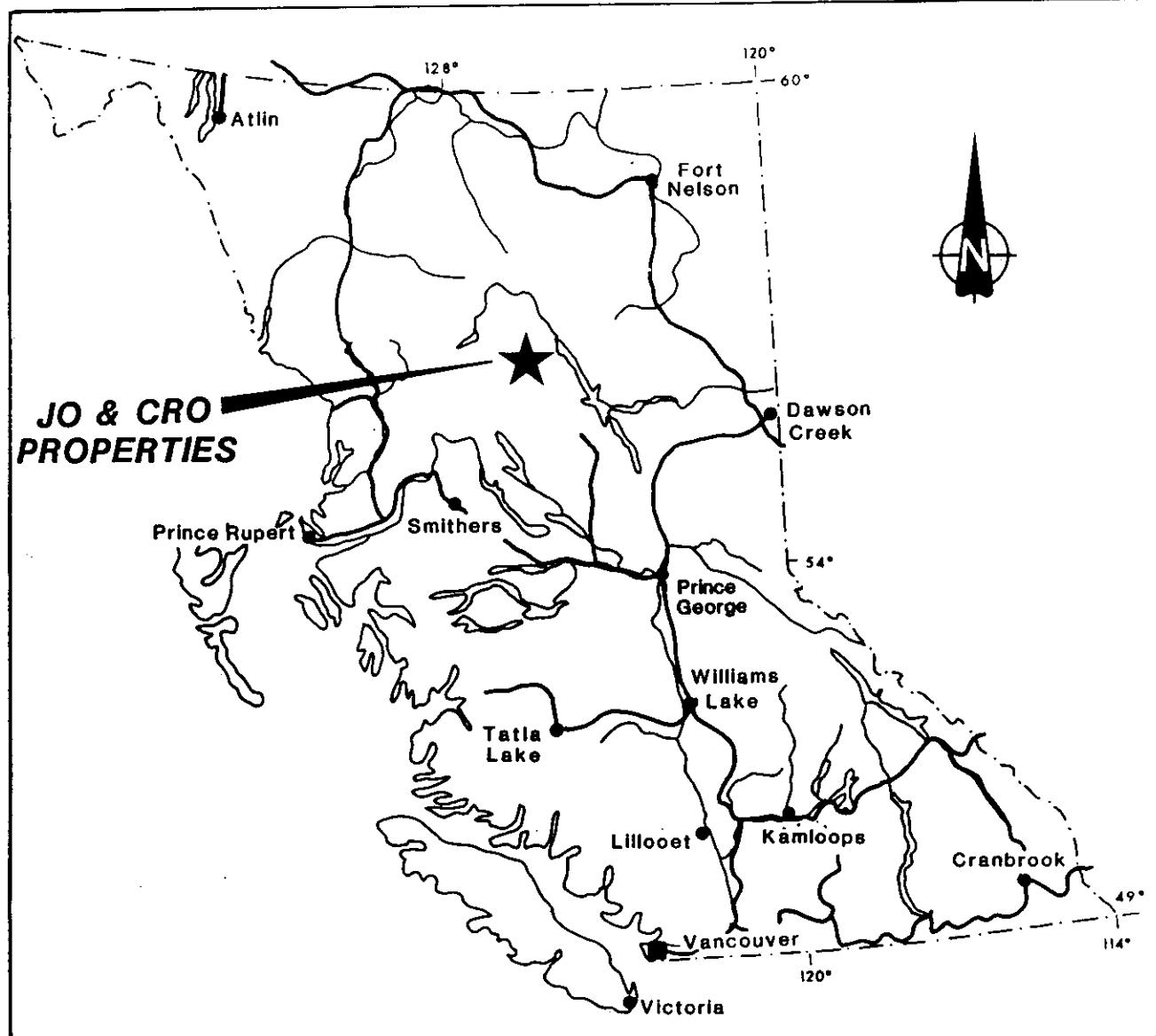
1.2 Claims and Ownership

The claims are situated in the Omineca Mining Division and are entirely owned by Golden Rule Resources Ltd. of Calgary, Alberta. Claims information is summarized below.

The claims are contiguous with the KC 1 and 2 claims, also owned by Golden Rule Resources Ltd., which are currently being explored by Ritz Resources Ltd. of Vancouver, B.C. under the terms of an option agreement between Ritz and Golden Rule.

TABLE 1
LIST OF CLAIMS

| CLAIM NAME | NO. OF UNITS | RECORD NO. | RECORD DATE | MAP NO. |
|------------|--------------|------------|-------------|-----------|
| CRO 1 | 18 | 12251 | JUL 14/90 | 94D/93/8E |
| CRO 2 | 20 | 12252 | JUL 11/90 | 94D/8E |
| CRO 3 | 20 | 12253 | JUL 11/90 | 94D/8E |
| CRO 4 | 20 | 12254 | JUL 11/90 | 94D/8E |
| CRO 5 | 6 | 12255 | JUL 14/90 | 94D/9E |
| JO 1 | 20 | 12243 | JUL 12/90 | 94D/9E |
| JO 2 | 20 | 12244 | JUL 12/90 | 94D/9E |
| JO 3 | 20 | 12245 | JUL 12/90 | 94D/9E |
| JO 4 | 20 | 12246 | JUL 13/90 | 94D/8E/9E |
| JO 5 | 20 | 12247 | JUL 13/90 | 94D/8E |
| JO 6 | 18 | 12248 | JUL 12/90 | 94D/8E |
| JO 7 | 15 | 12249 | JUL 12/90 | 94D/8E |
| JO 8 | 20 | 12250 | JUL 12/90 | 94D/8E |



0 100 200 300 400 500 Km

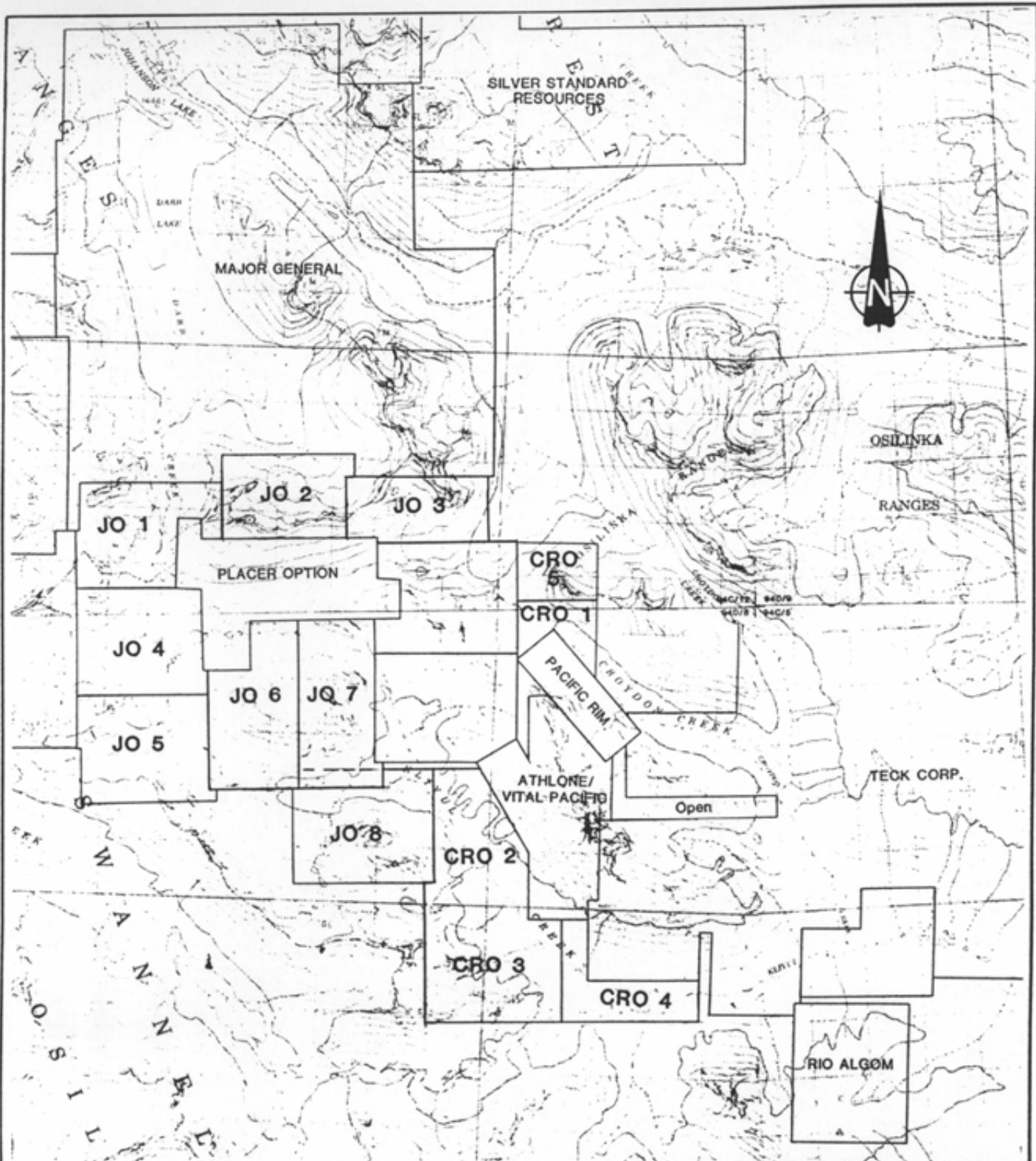
0 100 200 300 Miles

GOLDEN RULE RESOURCES LTD.

JO & CRO PROPERTIES

LOCATION MAP

| | |
|----------|-----------------|
| Date: | N.T.S.: |
| Revised: | FIGURE 1 |
| Scale: | |



GOLDEN RULE RESOURCES LTD.

JOHANSON LAKE AREA

JO AND CRO CLAIMS

CLAIMS LOCATION MAP

| | |
|------------------|----------|
| Date: APRIL 1991 | N.T.S.: |
| Revised: | FIGURE 2 |
| Scale: 1:100,000 | |

1.3 Physiography and Glaciation

The claims lie within the Omineca Mountains subdivision of the Interior Plateau. The region is entirely glaciated and is characterized by wide drift-filled major valleys. Numerous cirque basins, some occupied by tarns, and associated hanging valleys occur along both sides of Kliyul Creek, which was filled by a major valley glacier during Pleistocene time. One of these cirque basins contains a spectacular rock glacier, on the east boundary of the CRO 2 claim. The southwestern quadrant of the JO 8 claim covers part of a large composite cirque basin, almost 3 km wide, the floor of which is almost entirely devoid of overburden. Permanent icefields are present at the head of this basin as well as along the west boundary of the JO 1 claim. The terrain is rugged with steep cliff walls ringing most of the cirques. Narrow crested and razorback ridges, arêtes, and cols are common. Elevations at the claims range from approximately 1160 m to 2258 m ASL. Bedrock exposures comprise 5-10% of the total claims area. Most of the property is situated above treeline, which occurs at about 1500 m ASL. The valley of Kliyul Creek supports a fairly thick stand of timber below about 1400 m ASL, and dense patches of dwarf balsam occur at many locations above treeline.

1.4 Previous Work

Parts of the claim block currently held under disposition and described in this report have been previously staked at different times.

The claims adjoin the Kli Group of claims (Kennco Explorations Ltd.), the KC group (Golden Rule and Ritz Resources) and the SOUP, KLIYUL, and LADY DIANA claims (currently being explored by Teck Corp.). All of these groups, as well as the BAP claims, located internally within the KC 1 and 2 claims have seen considerable exploration in the past. The results of these exploration programs are described in numerous B.C. Assessment reports. Previous work has been directed towards evaluating the porphyry copper, gold-quartz vein, and copper-gold skarn potential of the area. Numerous gold bearing quartz veins have been discovered at the KC claims and gold-enriched magnetite-chalcopyrite skarns have been identified on the SOUP claims. Vancouver Stock Exchange news releases indicate that, on the Kli claims a drill-indicated tonnage of 1,000,000 tons grading 0.06 oz/t Au, 0.22 oz/t Ag, and 0.43% Cu is present.

1.5 1990 Program

Work carried out in 1990 at the JO and CRO claims consisted of helicopter supported reconnaissance geological mapping and stream silt sampling. A total of 76 rocks and 174 stream silt

samples were collected and analysed for Au and Ag by Fire Assay/AA methods, and a 30 element suite (including Au and Ag) by induction coupled plasma (ICP) analysis.

2

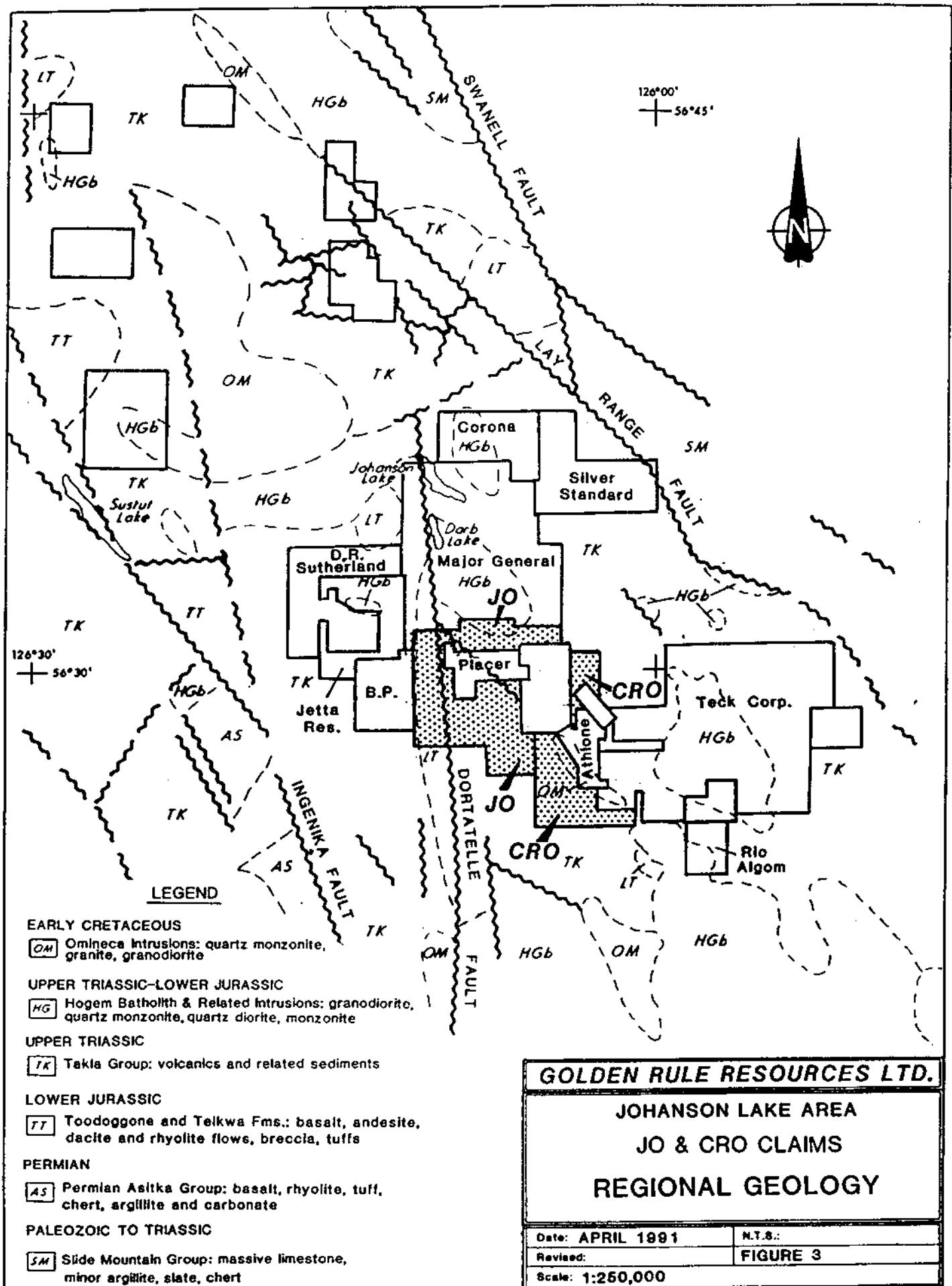
GEOLOGY

2.1 Regional Geology

The claims described in this report are underlain by an assemblage of Triassic to Jurassic basaltic to dacitic tuffs, breccias, and flows, and intercalated limestones, siltstones, sandstones, conglomerates and volcaniclastic rocks referred to as the "Takla Group". The Takla Group rocks, and a variety of plutonic rocks genetically related to Takla Group volcanic rocks comprise, in the Johanson Lake area, the northern extension of a 30 to 100 km wide and several hundred km long island arc assemblage referred to as the "Quesnel Trough", "Quesnel Terrane" and "Quesnellia" in the literature. The regional geology of the Johanson Lake area is illustrated in Figure 3 (Harper Ranch Subterrane ("Hr") is considered to be part of Quesnellia).

2.2 Property Geology

Reconnaissance mapping carried out in 1990 has outlined three major units which comprise the Takla Group in this area. The lower volcanic unit, outcropping extensively along Kliyul Creek consists of a thick succession of feldspar porphyritic andesitic flows and tuffs. Along the west side of Kliyul Creek the feldspar rich andesitic lavas are overlain by a southwestwards dipping sedimentary package of variable thickness consisting of interlayered thin bedded argillites, calcareous tuffs, silty to gritty limestone, and siltstone. The base of the sedimentary package is marked by a regionally continuous, gossanous, leucocratic exhalite (?) horizon composed of extremely fine grained quartz, sericite, feldspar, carbonate, and 2 - 15% extremely fine grained to coarse grained disseminated pyrrhotite. Minor pyrite and traces of chalcopyrite are also present. These sedimentary rocks correlate with a northeasterly dipping sequence of sedimentary rocks, including silty limestones, thinly bedded argillites, calcareous tuffs and a basal sulphidic chert or exhalite unit exposed along the east side of Kliyul Creek. Overlying the sedimentary succession (on both sides of Kliyul Creek) is a thick package of augite porphyritic basaltic flows and coarse breccias. The similar stratigraphic relationships, but opposing dips of the volcanic and sedimentary rocks on either side of Kliyul Creek suggests that the rocks form different limbs of a large anticlinal structure, the axis of which trends parallel to the northwesterly aligned section of Kliyul Creek. A number of small amplitude synclinal and anticlinal northeastward trending secondary folds



were noted in the sedimentary rocks exposed in the west limb of the "Kliyul Creek Anticline".

The "exhalite" unit referred to above has been described variously by previous workers as a "pyritic ash", a "rhyolitic tuff", and a "silicified volcanic", but its position at the interface of the lower feldspar rich andesitic lavas, and overlying sedimentary rocks strongly suggests an exhalative origin. Disseminated sulphides also occur as bands in the overlying massive to thinly bedded argillites.

2.3 Economic Geology

Some encouragement was gained from the mapping, prospecting and sampling carried out in 1990. A few quartz-chalcopyrite stringers were found and one sample of quartz float (sample number 86825) returned a gold assay in the order of 1 oz/t. Mapping of the large claim group is incomplete, however, and the economic potential of areas along Kliyul Creek, known to be underlain by intrusive rocks, has yet to be evaluated. Also, the geological significance of certain anomalous geochemical results, described below, has not yet been determined.

3

GEOCHEMISTRY

3.1 Sampling and Analytical Methods

A total of 174 stream silt samples and 76 rock samples were collected during the 1990 reconnaissance work described in this report. Rock samples consisted of "character" chip samples collected along traverses, and stream silt samples were collected at nominal 200 m to 250 m intervals. Stream silt sample material consisted of fine, "active" silts that samplers were able to obtain at sample sites. No pre-concentration of sample material was carried out, and moss mattes were not used as a sample medium.

Silt samples were dried and sieved and a -80 mesh fraction was analysed for Au and Ag by Fire Assay/AA techniques by Terramin Research Labs Ltd. of Calgary, Alberta. Sample pulps were shipped to Acme Analytical Laboratories Ltd. of Vancouver, B.C. and analysed for 30 elements including Mo, Cu, Pb, Zn, Ag, Ni, Co, Mn, %Fe, As, U, Au, Th, Sr, Cd, Sb, Bi, V, %Ca, %P, La, Cr, %Mg, Ba, %Ti, B, %Al, %Na, %K, and W by Induction Coupled Plasma (ICP) analysis. ICP analysis utilizes a .500 g sample digested with 3 ml of 3-1-2 HC₁-HNO₃-H₂O at 95 Degrees Celsius for 1 hour, followed by dilution to 10 ml with H₂O. This leach is only partial for Mn, Fe, Sn, Ca, P, La, Cr, Mg, Ba, Ti, B, and W, and the leach is limited for Na, K, and Al. Consequently, ICP

analyses for the above elements - particularly K - are not reliable indicators of alteration, particularly in volcanic rocks, where the effects of K alteration might be more subtle than in intrusive rocks.

3.2 Statistical Analysis of Data

Cumulative probability graphs for Au, Cu, and Mo-in-stream silts data are shown in Figures 4, 5, and 6 respectively.

The cumulative probability graph for Au-in-stream silt values (Figure 4) indicates that two extensively overlapping lognormal populations are present, with an anomalous threshold of 12 ppb Au, and definitely anomalous concentrations defined by values of 45 ppb Au or greater.

The cumulative probability graph for Cu-in-stream silt values (Figure 5) indicates that two overlapping lognormal populations are present, with an anomalous threshold of 90 ppm Cu and definitely anomalous concentrations defined by values of 250 ppm Cu or greater.

The cumulative probability graph for Mo-in-stream silt values (Figure 6) indicates that two lognormal populations are present, with an anomalous threshold of 8 ppm Mo, and definitely anomalous concentrations defined by values of 9 ppm Mo or greater.

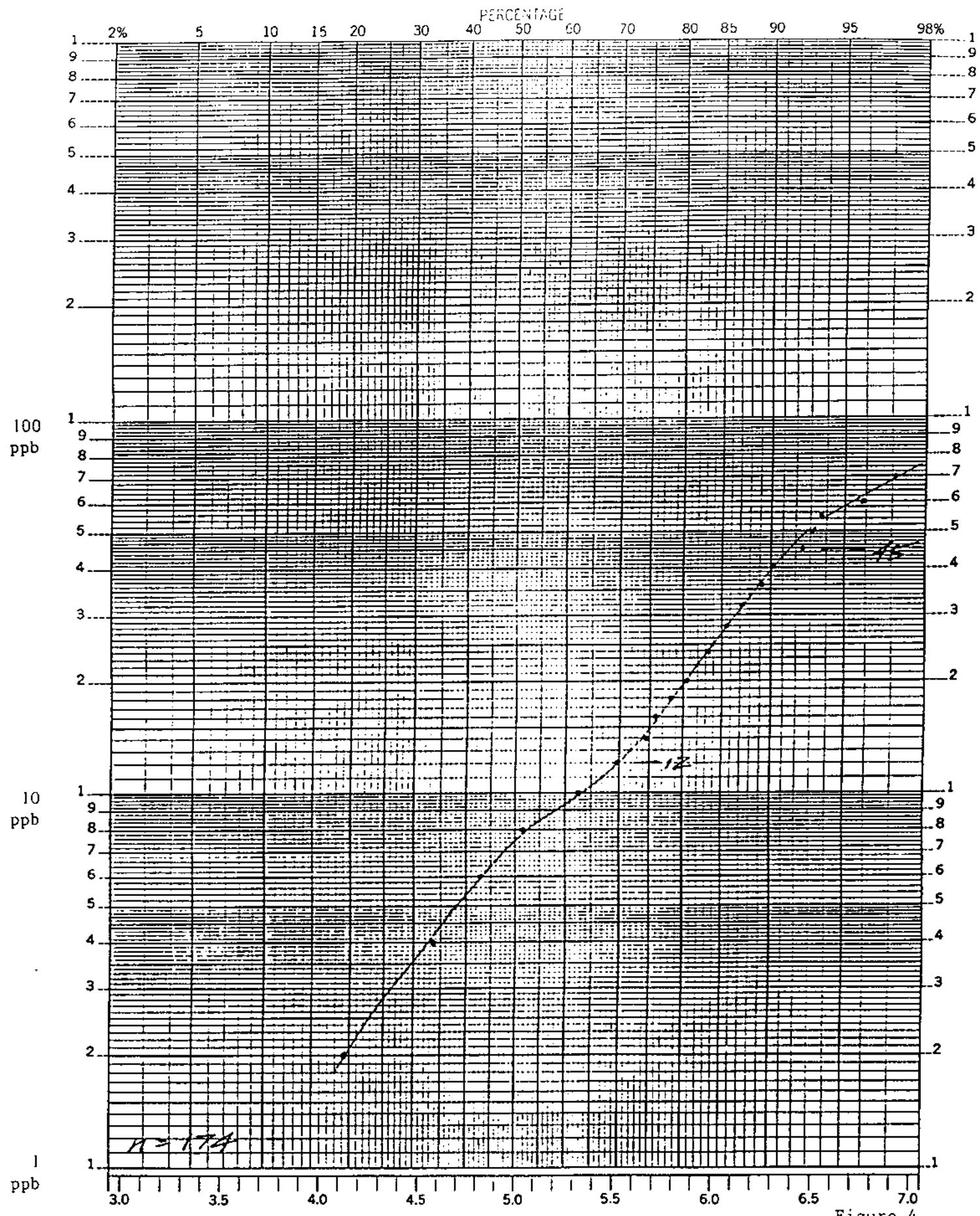
3.3 Results

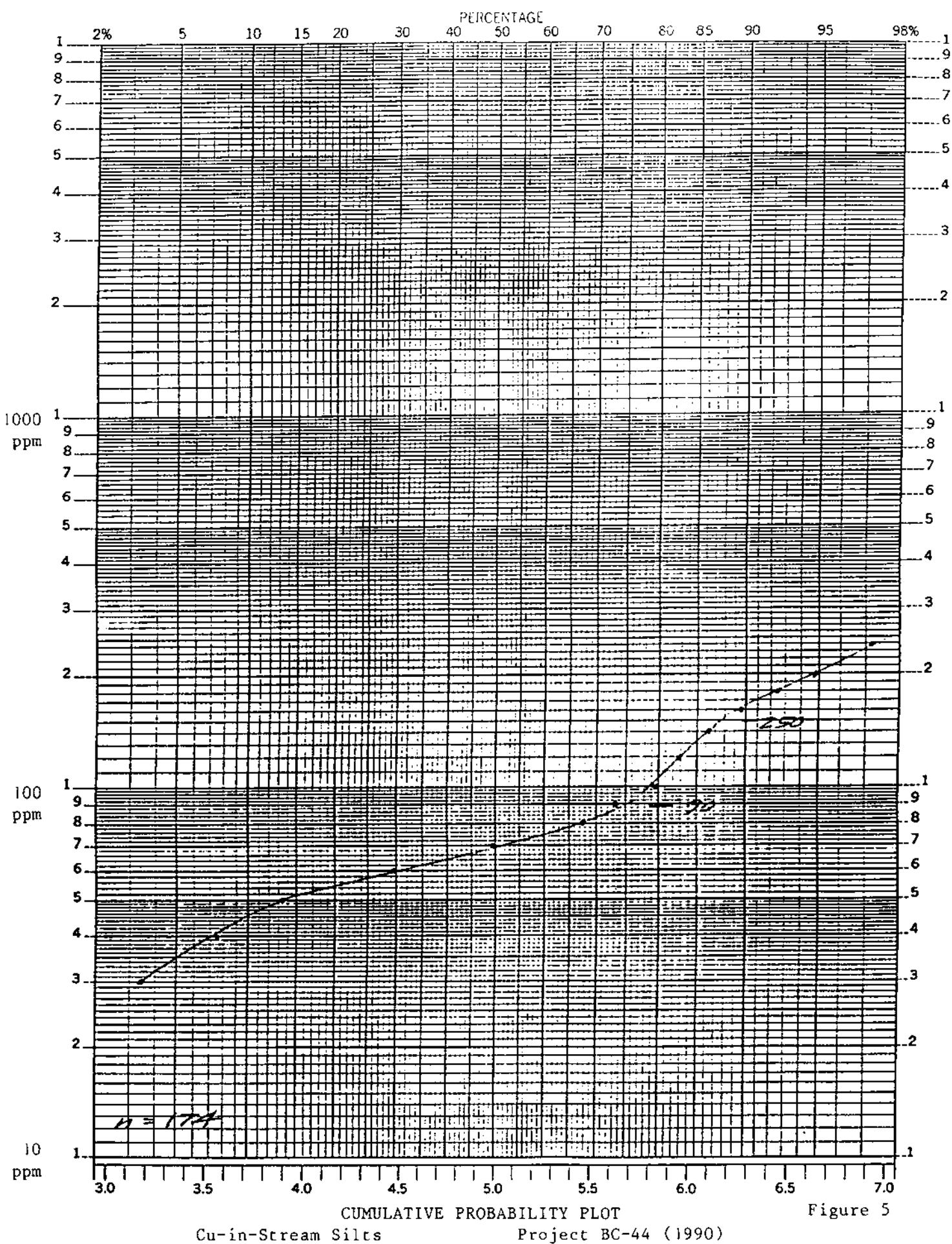
A) Kliyul Creek

Stream silt sampling was carried out along the main branch and the west fork of Kliyul Creek, which flows into the main branch near the northwest corner of the CRO 2 claim.

a) West Fork

The west fork of Kliyul Creek rises in the northern part of the JO 7 claim, in a wide upland basin above treeline. A low divide separates it from the headwaters of the north fork or main branch of Kliyul Creek. The west fork first flows westerly for about three kilometers, passing through a series of small, shallow lakes along the floor of the basin. It then flows southerly for about two kilometers, then easterly for approximately 5 kilometers, describing 3/4 of a circle before reaching its confluence with the north fork of Kliyul Creek, about 3 kilometers southeasterly from its origin, to form the main branch of Kliyul Creek.





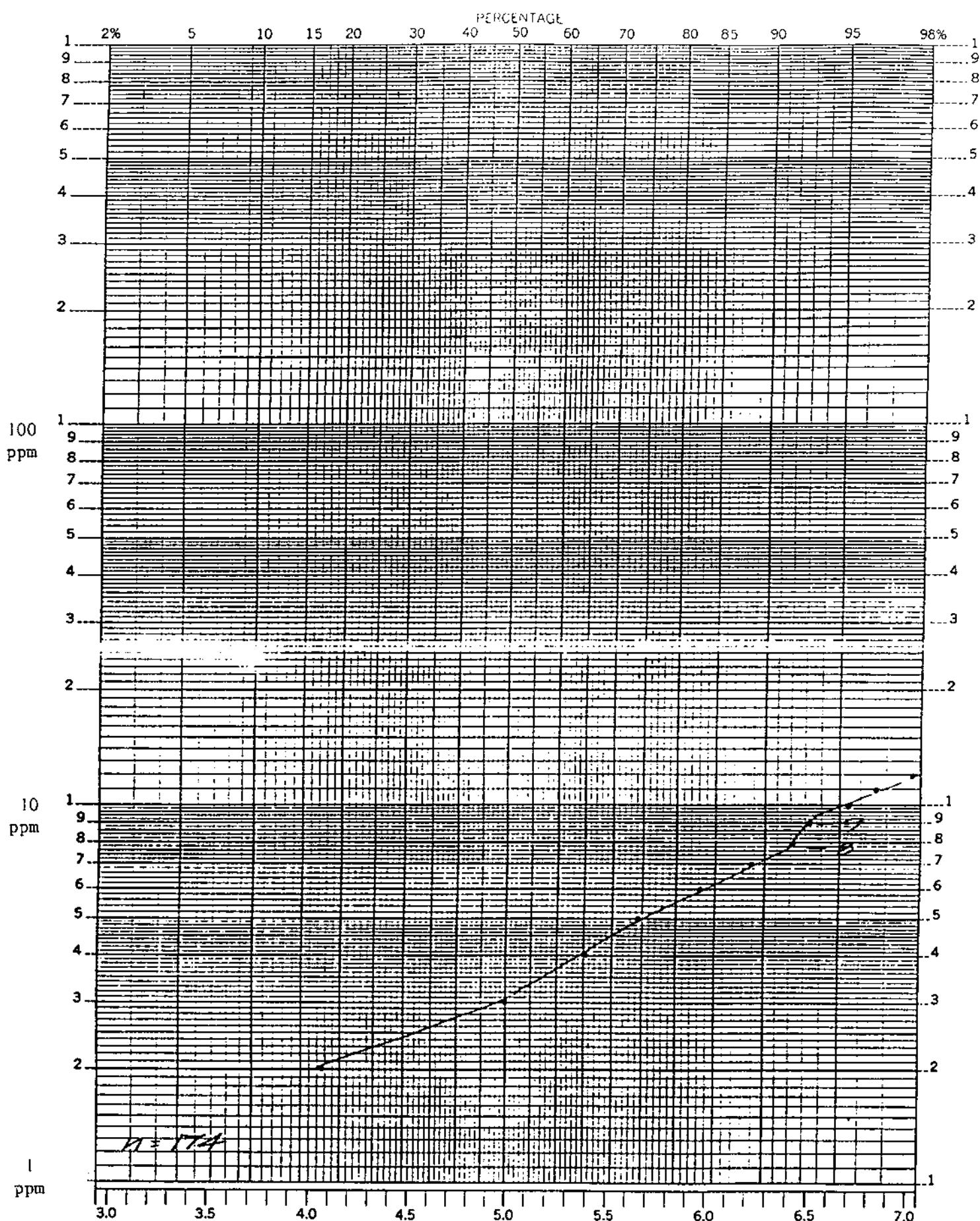


Figure 6

A 1 km long southerly flowing tributary enters the west fork of Kliyul Creek approximately 100 m upstream from the point where the west fork empties into the largest (800 m long) of the several shallow lakes along its course (two other larger lakes, each approximately 1 km in length occur along an easterly flowing tributary of the west fork, in the northwesterly and west-central sectors of the JO 5 claim). Anomalous Au-in-stream silt values of 44 ppb and 248 ppb occur along this drainage (sample numbers JRG 9 and 11), and a short distance to the west, an anomalous Au-in-stream silt value of 94 ppb (JRG 10) was returned from a small stream which flows into the north side of the lake. Both of these small tributaries of the west fork rise at a low divide separating Darb Creek, which flows northerly into Johanson Lake, and the west fork of Kliyul Creek. The area of the divide is transected by the Dortatelle Fault, a 40 km long structure, which is a major splay of the Pinchi-Ingenika fault system. Rocks within this deformation zone have been in places intensely sheared, chloritized, and silicified and host numerous small quartz/pyrite stringers. Quartz float assaying 0.76 oz/ton Au and 1.2 oz/ton Ag was found on the west side of this divide (rock sample number 86825).

Approximately 1 1/2 km southwest of this area, midway along the straight southerly flowing section of the west fork of Kliyul Creek (which here flows in a straight trench-like gully marking the trace of the Dortatelle Fault), two other anomalous Au-in-stream silt values of 28 ppb and 36 ppb (JRG 19 and 20) were returned. These values most likely are also related to gold mineralization associated with the Dortatelle Fault.

An isolated anomalous Au-in-stream silt value of 32 ppb Au (JRG 32) occurs further downstream, and one strongly anomalous Cu-in-stream silt value of 377 ppm Cu occurs at sample site JRG-49.

b) Main Branch of Kliyul Creek

A series of above threshold to anomalous Au-in-stream silt values occur along a 2 km length of the main branch of Kliyul Creek immediately downstream from the mouth of the west fork. The main branch or north fork of Kliyul Creek above the mouth of the west fork was not sampled as it lies within the KC 2 claim and has been previously sampled, with the result that a 2 km long trend of weakly anomalous Au-in-stream silt

values interspersed with occasional strongly anomalous Au-in-stream silt values has been detected. Associated strongly anomalous Cu-in-stream silt values are also present. The 2 km long downstream extension of this zone (below the mouth of the west fork) is defined by the Au values, as only 2 samples returned anomalous Cu-in-stream silt values.

For about 1 km above their confluence, the north and west forks of Kliyul Creek both occupy steep walled canyons out into bedrock. Along the north fork, the underlying volcanic rocks are cut by silicified, chloritized, and pyritized shear zones over a broad 50 m to 100 m (?) wide zone of deformation. Small quartz-pyrite veins are common throughout this zone. The creek is aligned along the inferred axis of the Kliyul Creek anticline as well as the trace of a major northwesterly striking splay of the Doretelle Fault, which appears to have controlled the emplacement of monzonitic and related intrusive rocks along the east side of Kliyul Creek. The anomalous gold values could be related to the quartz-pyrite stringers developed in the deformation zone, or could perhaps be related to auriferous chalcopyrite-magnetite skarns developed along the monzonite intrusive contacts, similar to skarns known on adjoining claim groups.

A few weakly anomalous Au-in-stream silt values occur along Kliyul Creek in the southern half of the CRO 4 claim. Above threshold Cu-in-stream silt values of 95 ppm and 123 ppm are associated with weakly anomalous gold values at two localities (DK 17 and 26). These anomalous results could be related to the southeastwards extensions of zones of shear or skarn type mineralization, as described above which may underlie the valley floor of Kliyul Creek (1 km wide at this point).

B) Darb Creek

A number of stream silt samples collected along the upper west fork of Darb Creek (JO 1 claim) returned weakly anomalous gold values at sporadic intervals as well as weakly anomalous to anomalous Cu-in-stream silt values along a several hundred meter long trend. Rocks underlying the drainage include zones of strongly sheared, silicified, and pyritized volcanics along the wide deformation zone associated with the Doretelle Fault (see description of results along the upper west fork of Kliyul Creek).

A more consistent anomalous Au-in-stream silt trend is defined by a sequence of samples collected at the upper end of the east fork of Darb Creek (JO 3 claim). Here, weakly anomalous Au values occur along a several hundred meter long zone and are accompanied by sporadic weakly anomalous to anomalous Cu-in-stream silt values. Several samples also returned anomalous Mo-in-stream silt samples at the head of this drainage, suggesting a source of porphyry type mineralization associated with the quartz diorite pluton that underlies most of the basin.

C) Lay Creek

Stream silt samples collected along a northerly flowing tributary of Lay Creek in the area of the CRO 5 claim returned an unusually long series of weakly to highly anomalous Au and Cu-in-stream silt values, ranging from 12 to 420 ppb Au and 131 to 290 ppm Cu (JRG 250 to 270). Prospecting carried out concurrently with sampling along this drainage identified a variety of different volcanic rock types including vuggy, leached and oxidized quartz vein material (limonite after coarse pyrite cubes up to 6 mm in diameter - sample number JRG 250), fine-grained, pyritized (1%) augite-feldspar porphyry of probable andesitic composition (JRG-251, 253, 255, 264, 268) quartz-chalcopyrite +/- malachite stringers cutting fine-grained andesitic silicified augite-feldspar porphyry (JRG 252), well pyritized recrystallized and silicified augite-feldspar porphyry (JRG 254, 256, 258, 262, 267) similar to wall rocks adjacent to quartz-chalcopyrite stringers at JRG-252, fresh quartz-pyrite vein material with coarse-grained pyrite cubes up to 6 mm in diameter (JRG 260), and feldspar porphyritic andesite (JRG 262). No alteration which would suggest proximity to a porphyry type hydrothermal centre was observed in any of these rocks. Anomalous Zn-in-stream silt values which occur along that branch of the stream that transects the north-central part of the KC 1 claim were not present in sample results reported in here.

4

CONCLUSIONS AND RECOMMENDATIONS

Reconnaissance geological mapping carried out at the JO 1 to 8 and CRO 1 to 5 claims during the 1990 field season has partly defined a stratigraphic sequence within the Takla Group rocks consisting of a lower feldspar rich succession of andesitic lavas and tuffs, overlain by a sedimentary package of variable thickness consisting of sulphide rich chert or exhalite, thinly laminated argillites and calcareous siltstones, and gritty to silty grey limestones. No thin section analyses have been done to

confirm this interpretation of the cherty sulphide rich unit as being an exhalite, and other workers have also referred to it as a pyritic ash bed sequence. Stratigraphically above the sedimentary package is a thick succession of augite porphyry flows, tuffs, breccias, and intercalated, discontinuous and chaotically bedded laharic units consisting of large volcanic clasts enclosed in thinly bedded, silty limestones and argillites.

None of the rock samples collected from the pyrrhotite rich exhalite unit returned metal values of any interest.

Anomalous Au-in-stream silt values along the upper part of the west fork of Kliyul Creek (JO 4 claim) appear to be related to zones of shearing, silicification, chloritization and quartz-sulphide stringers associated with a broad deformation zone along the trace of the Dortatelle Fault. The same inference would apply to anomalous Cu and Au-in-stream silt values returned from samples near the headwaters of the west fork of Darb Creek.

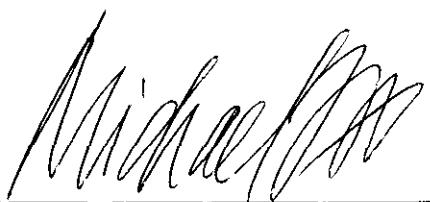
Anomalous Au-in-stream silt values and sporadically associated anomalous Cu-in-stream silt values returned from samples collected along Kliyul Creek below the confluence of the north and west forks (CRO 2 and 3 claims) appear to be related to similar alteration and mineralization associated with a wide deformation zone that strikes northwesterly parallel to Kliyul Creek. The possibility also exists that these anomalous values may be related to magnetite-chalcopyrite-gold skarns along the contact of a monzonitic intrusion underlying the slopes east of the creek. On the adjoining KC claims, the monzonite is in places strongly fractured and cut by numerous quartz +/- chalcopyrite stringers along the Kliyul Creek deformation zone, suggesting a potential for porphyry type Cu-Au mineralization at the CRO 2, 3, and 4 claims to the southeast.

Several coincident anomalous Cu, Mo, and Au-in-stream silt values occurring at the headwaters of the east fork of Darb Creek (JO 2 and 3 claims) suggest the possibility of porphyry type Cu-Mo-Au- mineralization associated with the quartz diorite pluton that underlies much of the basin.

A 3 km long trend of anomalous Cu and Au-in-stream silt values occurs along a north flowing tributary of Lay Creek (JO 3 and CRO 5 claims). Quartz-pyrite +/- chalcopyrite stringers and well pyritized fine-grained augite-feldspar porphyry andesitic volcanics outcrop at several locations along this stream. It seems unlikely that the few small veins so far recognized could completely explain the long, continuous anomalous Cu trend on this drainage, and the possibility of a large porphyry-type source of metallization needs to be further investigated.

The Kliyul Creek, Darb Creek, Lay Creek, and Croydon Creek area has significant potential for the discovery of porphyry type Cu-Au mineralization. Potentially economic tonnages and grades of skarn type Cu-Au mineralization may also be present in this geological environment. All of the above described stream silt anomalies warrant follow-up work. This work should consist of careful, detailed prospecting, geological mapping, and rock sampling, as well as grid-controlled soil sampling where the latter technique would be appropriate as a reconnaissance exploration tool or in delineating the extent of any mineralized zones found by prospecting and mapping.

Respectfully submitted,



Michael Fox, Consulting Geologist

February, 1991

STATEMENT OF COSTS

| | |
|----------------------------------|---------------------|
| Supervisory Geological Personnel | \$ 7,260.00 |
| Support Personnel | 1,350.00 |
| Camp Costs | 656.25 |
| Field Costs | 1,290.40 |
| Helicopter & Fixed Wing | 30,421.53 |
| Travel Expenses | 711.38 |
| Expediting | 25.00 |
| Geochemical Analyses | <u>3,687.71</u> |
| TOTAL: | \$ 45,402.27 |

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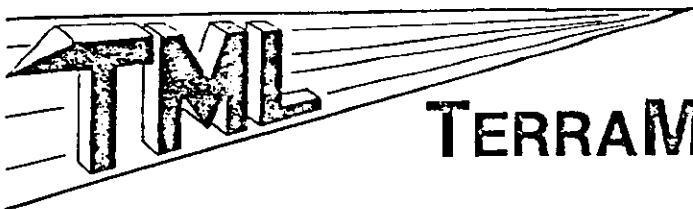
Report on a Trenching Programme on the KC-BAP Mineral Claims, for Ritz Resources Ltd.

Wilson, G. (1984):

Geological, Geochemical and Geophysical Report, Golden Rule Resources Ltd., Taiga Consultants Ltd.

APPENDIX I

ANALYTICAL METHODS



TERRAMIN RESEARCH LABS LTD.

14-2235 - 30th Avenue N.E. Calgary, Alberta T2E 7C7
(403) 276-8668

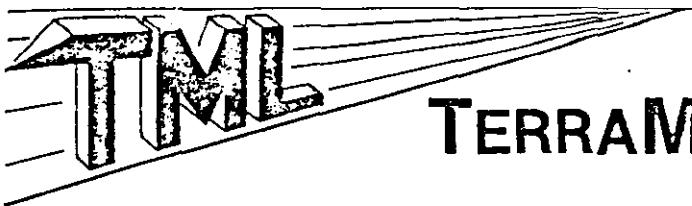
GOLDEN RULE RESOURCES

SAMPLE PREPARATION

Soil and sediment samples are dried and sieved to -80 mesh (approx. 200 micron).

Rock Samples:

The entire sample is crushed to approx. 1/8" maximum, and split divided to obtain a representative portion which is pulverized to -200 mesh (approx 90 micron).



TERRAMIN RESEARCH LABS LTD.

14-2235 - 30th Avenue N.E. Calgary, Alberta T2E 7C7
(403) 276-8668

GOLDEN RULE RESOURCES

ANALYTICAL METHOD FOR GOLD AND SILVER

Approximately 1 assay ton of prepared sample is fused with a litharge/flux charge to obtain a lead button. The lead button is cupelled to obtain a prill. The prill is dissolved in nitric/hydrochloric acids (aqua regia), and the resulting solution is analysed by atomic absorption spectroscopy.

APPENDIX II

GEOCHEMICAL DATA

GEOCHEMICAL ANALYSIS CERTIFICATE

Golden Rule Resources Ltd. File # 90-4927 Page 1
 410 - 1122 - 4th St. S.W., Calgary AB T2R 1M1

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P X | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm |
|------------|--------|--------|--------|--------|--------|--------|--------|--------|-------|--------|-------|--------|--------|--------|--------|--------|--------|-------|-------|------|--------|--------|------|--------|------|-------|------|------|------|-------|
| 74919 | 5 | 27 | 2 | 11 | .1 | 4 | 6 | 156 | 2.00 | 2 | 5 | ND | 1 | 99 | .2 | 2 | 2 | 34 | .72 | .077 | 3 | 80 | .35 | 29 | .08 | 3 | 1.04 | .11 | .05 | 2 |
| 74920 | 3 | 679 | 3 | 30 | .7 | 40 | 25 | 215 | 3.92 | 4 | 5 | ND | 1 | 69 | .3 | 2 | 3 | 60 | .97 | .052 | 2 | 57 | .98 | 38 | .14 | 4 | 1.70 | .13 | .04 | 1 |
| 74921 | 3 | 878 | 7 | 13 | .6 | 14 | 12 | 166 | 2.94 | 2 | 5 | ND | 1 | 117 | .5 | 2 | 2 | 40 | 1.62 | .048 | 3 | 37 | .36 | 103 | .13 | 3 | 2.05 | .17 | .05 | 2 |
| 74922 | 10 | 597 | 9 | 7 | .3 | 11 | 15 | 106 | 2.42 | 2 | 5 | ND | 1 | 79 | .2 | 2 | 2 | 31 | 1.34 | .062 | 3 | 56 | .23 | 33 | .13 | 3 | 1.45 | .14 | .06 | 1 |
| 74923 | 4 | 151 | 2 | 6 | .1 | 3 | 7 | 187 | 1.87 | 2 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 31 | .72 | .095 | 4 | 55 | .24 | 35 | .07 | 2 | .74 | .09 | .05 | 2 |
| 74924 | 11 | 259 | 4 | 13 | .1 | 3 | 8 | 178 | 1.83 | 3 | 5 | ND | 1 | 49 | .2 | 2 | 2 | 26 | .66 | .091 | 4 | 59 | .22 | 26 | .07 | 2 | .70 | .08 | .04 | 1 |
| 74925 | 1 | 15 | 11 | 66 | .4 | 31 | 15 | 1359 | 5.42 | 5 | 5 | ND | 1 | 90 | .2 | 2 | 2 | 48 | 12.64 | .043 | 4 | 44 | 1.11 | 217 | .01 | 4 | .51 | .01 | .15 | 1 |
| 74926 | 1 | 65 | 4 | 43 | .6 | 19 | 16 | 1024 | 4.42 | 9 | 8 | ND | 1 | 81 | .2 | 2 | 2 | 55 | 17.35 | .009 | 2 | 22 | 2.05 | 19 | .01 | 8 | .33 | .01 | .11 | 1 |
| 74927 | 4 | 280 | 8 | 28 | .2 | 13 | 18 | 318 | 3.90 | 2 | 5 | ND | 1 | 36 | .2 | 2 | 2 | 57 | 1.25 | .082 | 4 | 50 | .64 | 68 | .17 | 3 | 1.66 | .14 | .20 | 2 |
| 74928 | 15 | 163 | 6 | 37 | .4 | 36 | 16 | 232 | 4.32 | 24 | 5 | ND | 1 | 46 | .5 | 6 | 2 | 82 | .81 | .050 | 5 | 77 | 1.08 | 27 | .26 | 3 | 1.67 | .14 | .09 | 1 |
| 74929 | 3 | 102 | 6 | 49 | .6 | 27 | 16 | 502 | 5.06 | 4 | 5 | ND | 1 | 48 | 1.0 | 3 | 2 | 113 | 1.44 | .079 | 4 | 67 | 1.48 | 20 | .31 | 5 | 2.55 | .16 | .05 | 1 |
| 74930 | 1 | 38 | 11 | 63 | .4 | 35 | 13 | 834 | 3.30 | 181 | 8 | ND | 1 | 83 | .2 | 3 | 2 | 49 | 7.22 | .057 | 3 | 53 | 1.51 | 130 | .01 | 5 | .46 | .02 | .12 | 1 |
| 74931 | 8 | 103 | 5 | 46 | .4 | 27 | 17 | 502 | 4.58 | 3 | 5 | ND | 1 | 8 | .5 | 2 | 2 | 117 | 1.62 | .065 | 5 | 58 | .96 | 12 | .33 | 4 | 2.12 | .07 | .01 | 1 |
| 74932 | 1 | 38 | 5 | 47 | .4 | 50 | 18 | 793 | 3.47 | 15 | 12 | ND | 1 | 53 | .2 | 2 | 2 | 61 | 10.98 | .021 | 2 | 76 | 2.55 | 72 | .01 | 5 | .54 | .01 | .06 | 1 |
| 74933 | 5 | 95 | 8 | 81 | .6 | 36 | 19 | 837 | 5.95 | 7 | 5 | ND | 1 | 14 | .8 | 6 | 2 | 163 | 1.54 | .050 | 3 | 67 | 2.25 | 12 | .34 | 8 | 3.19 | .05 | .03 | 1 |
| 74934 | 1 | 13019 | 22 | 114 | 9.4 | 19 | 22 | 936 | 6.40 | 9 | 5 | 2 | 1 | 55 | 1.6 | 4 | 2 | 253 | 1.59 | .374 | 17 | 28 | 1.78 | 65 | .19 | 5 | 1.88 | .05 | .30 | 1 |
| 74935 | 1 | 5757 | 8 | 78 | 4.6 | 111 | 73 | 728 | 4.14 | 2 | 5 | ND | 1 | 27 | .8 | 2 | 2 | 146 | .76 | .072 | 6 | 164 | 2.35 | 167 | .24 | 2 | 2.06 | .14 | 1.49 | 1 |
| 74936 | 6 | 149 | 8 | 47 | .4 | 12 | 12 | 694 | 5.20 | 6 | 5 | ND | 1 | 43 | .2 | 2 | 2 | 106 | .86 | .118 | 4 | 46 | 1.03 | 43 | .17 | 2 | 1.82 | .15 | .72 | 2 |
| 74937 | 21 | 630 | 23 | 58 | 5.8 | 7 | 55 | 214 | 14.44 | 88 | 11 | ND | 1 | 26 | .2 | 4 | 4 | 108 | .13 | .112 | 2 | 82 | .38 | 81 | .12 | 4 | .74 | .02 | .20 | 1 |
| 74938 | 4 | 84 | 6 | 76 | .6 | 27 | 15 | 602 | 5.24 | 3 | 5 | ND | 1 | 57 | .2 | 3 | 2 | 56 | 3.53 | .069 | 3 | 31 | 1.42 | 40 | .14 | 2 | 1.98 | .03 | .08 | 1 |
| 74939 | 3 | 76 | 6 | 55 | .3 | 11 | 14 | 623 | 4.46 | 2 | 5 | ND | 1 | 27 | .2 | 2 | 2 | 20 | 2.80 | .054 | 2 | 18 | 1.04 | 61 | .20 | 2 | 1.62 | .03 | .12 | 1 |
| 74940 | 1 | 25 | 11 | 32 | .8 | 3 | 6 | 362 | 6.01 | 2 | 5 | ND | 1 | 23 | .3 | 3 | 2 | 40 | .36 | .047 | 2 | 29 | 1.47 | 49 | .40 | 2 | 1.47 | .02 | .10 | 1 |
| 74941 | 11 | 7451 | 4 | 94 | 10.3 | 19 | 16 | 795 | 5.40 | 7 | 12 | ND | 1 | 43 | 1.0 | 3 | 4 | 70 | 8.03 | .029 | 2 | 91 | 1.59 | 52 | .05 | 2 | 1.72 | .01 | .19 | 1 |
| 74942 | 12 | 115 | 9 | 20 | .4 | 25 | 14 | 274 | 4.36 | 10 | 5 | ND | 1 | 105 | .4 | 2 | 2 | 67 | 1.35 | .061 | 5 | 45 | .40 | 15 | .23 | 4 | 1.74 | .11 | .04 | 2 |
| 74943 | 2 | 1113 | 18 | 102 | .5 | 7 | 24 | 1769 | 10.71 | 5 | 5 | ND | 4 | 8 | .2 | 6 | 3 | 90 | .38 | .135 | 8 | 27 | 1.56 | 79 | .01 | 5 | 2.98 | .01 | .20 | 1 |
| 74944 | 3 | 235 | 3 | 18 | .3 | 19 | 20 | 326 | 3.73 | 3 | 5 | ND | 1 | 54 | .2 | 2 | 3 | 85 | .93 | .089 | 3 | 47 | 1.06 | 59 | .18 | 2 | 1.93 | .16 | .24 | 1 |
| 74945 | 3 | 99 | 2 | 10 | .2 | 16 | 12 | 127 | 1.94 | 5 | 5 | ND | 2 | 30 | .2 | 2 | 3 | 39 | .49 | .063 | 4 | 46 | .31 | 257 | .18 | 3 | .63 | .08 | .16 | 1 |
| 74946 | 1 | 83 | 14 | 77 | .5 | 39 | 23 | 1090 | 5.82 | 16 | 7 | ND | 1 | 78 | .2 | 4 | 2 | 97 | 6.15 | .048 | 2 | 81 | 2.70 | 21 | .10 | 3 | 3.24 | .02 | .05 | 1 |
| 74947 | 1 | 78 | 8 | 53 | .5 | 18 | 17 | 564 | 3.93 | 2 | 5 | ND | 1 | 70 | .5 | 3 | 2 | 94 | 1.71 | .051 | 2 | 42 | 1.42 | 233 | .27 | 2 | 2.46 | .21 | .97 | 1 |
| 74948 | 9 | 31 | 5 | 37 | .3 | 23 | 13 | 339 | 3.08 | 5 | 5 | ND | 1 | 51 | .6 | 2 | 2 | 70 | 1.12 | .059 | 2 | 64 | 1.03 | 43 | .19 | 2 | 2.21 | .26 | .59 | 2 |
| 74949 | 1 | 5 | 12 | 130 | .1 | 8 | 14 | 1804 | 4.62 | 2 | 5 | ND | 6 | 72 | .2 | 2 | 2 | 164 | .55 | .113 | 13 | 21 | .09 | 136 | .01 | 7 | .42 | .02 | .08 | 1 |
| 74950 | 7 | 159 | 7 | 29 | .3 | 38 | 21 | 230 | 3.53 | 3 | 5 | ND | 1 | 240 | .5 | 3 | 3 | 54 | 3.11 | .072 | 5 | 65 | .45 | 45 | .14 | 6 | 3.22 | .30 | .10 | 2 |
| 74951 | 7 | 219 | 9 | 16 | .3 | 37 | 16 | 90 | 2.83 | 3 | 5 | ND | 2 | 254 | .7 | 4 | 2 | 47 | 2.09 | .070 | 5 | 58 | .35 | 51 | .15 | 4 | 2.71 | .31 | .10 | 1 |
| 74952 | 1 | 80 | 11 | 32 | .6 | 5 | 22 | 223 | 4.84 | 6 | 5 | ND | 1 | 22 | .5 | 4 | 2 | 81 | .53 | .044 | 2 | 30 | 1.66 | 9 | .14 | 2 | 2.26 | .11 | .02 | 1 |
| 74953 | 2 | 193 | 7 | 39 | .7 | 12 | 20 | 263 | 4.38 | 5 | 5 | ND | 1 | 38 | .3 | 3 | 2 | 107 | .98 | .024 | 2 | 47 | 1.30 | 10 | .14 | 2 | 2.47 | .18 | .02 | 2 |
| 74954 | 3 | 186 | 9 | 55 | .5 | 9 | 15 | 359 | 4.65 | 4 | 5 | ND | 1 | 47 | .4 | 2 | 2 | 67 | .82 | .029 | 2 | 48 | 1.49 | 97 | .11 | 2 | 3.15 | .22 | .52 | 1 |
| STANDARD C | 18 | 61 | 37 | 131 | 7.0 | 68 | 32 | 1052 | 3.95 | 40 | 17 | 8 | 39 | 53 | 18.5 | 16 | 19 | 56 | .46 | .095 | 37 | 58 | .89 | 181 | .08 | 36 | 1.89 | .07 | .13 | 11 |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.
 THIS LEACH IS PARTIAL FOR Mn Fe Sr Ca P La Cr Mg Ba Ti B W AND LIMITED FOR Na K AND Al. Au DETECTION LIMIT BY ICP IS 3 PPM.
 - SAMPLE TYPE: PULP

DATE RECEIVED: SEP 27 1990 DATE REPORT MAILED: Oct 5/90. SIGNED BY: *C. L. Toye, C. Leong, J. Wang*; CERTIFIED B.C. ASSAYERS

Golden Rule Resources Ltd. FILE # 90-4927

Page 2

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| 74955 | 2 | 189 | 2 | 47 | .5 | 11 | 16 | 533 | 4.87 | 2 | 5 | ND | 2 | 41 | .2 | 2 | 2 | 72 | .82 | .030 | 2 | 52 | 1.58 | 124 | .09 | 2 | 3.18 | .19 | .27 | 1 |
| 74956 | 1 | 141 | 2 | 29 | .5 | 28 | 21 | 327 | 4.95 | 2 | 5 | ND | 1 | 33 | .2 | 2 | 3 | 78 | .88 | .018 | 2 | 128 | 2.21 | 6 | .08 | 2 | 3.70 | .18 | .02 | 1 |
| 74957 | 6 | 36 | 2 | 54 | .3 | 53 | 16 | 853 | 3.78 | 50 | 5 | ND | 2 | 37 | .2 | 2 | 2 | 72 | 2.48 | .029 | 2 | 295 | 2.30 | 12 | .01 | 3 | 1.98 | .02 | .03 | 1 |
| 74958 | 6 | 5 | 2 | 49 | .3 | 123 | 17 | 862 | 3.22 | 25 | 5 | ND | 1 | 30 | .2 | 2 | 2 | 44 | 6.03 | .041 | 2 | 228 | 1.49 | 16 | .01 | 2 | 1.40 | .01 | .04 | 1 |
| 74959 | 1 | 66 | 2 | 81 | .4 | 28 | 15 | 671 | 4.17 | 69 | 5 | ND | 1 | 26 | .2 | 2 | 2 | 69 | 1.67 | .048 | 6 | 28 | .39 | 44 | .01 | 5 | .61 | .01 | .07 | 1 |
| 74960 | 1 | 38 | 2 | 56 | .4 | 20 | 12 | 825 | 3.72 | 3 | 5 | ND | 2 | 158 | .2 | 2 | 2 | 69 | 16.22 | .023 | 2 | 37 | .83 | 21 | .01 | 3 | .48 | .01 | .03 | 1 |
| 74961 | 1 | 53 | 4 | 64 | .3 | 22 | 17 | 668 | 3.99 | 12 | 5 | ND | 2 | 32 | .2 | 2 | 2 | 82 | 1.42 | .108 | 7 | 43 | .53 | 111 | .01 | 3 | .93 | .02 | .10 | 1 |
| 74962 | 1 | 4 | 3 | 44 | .1 | 4 | 6 | 724 | 2.82 | 5 | 5 | ND | 2 | 7 | .2 | 2 | 2 | 41 | .26 | .087 | 13 | 21 | .07 | 60 | .01 | 5 | .75 | .01 | .10 | 1 |
| 74963 | 1 | 26 | 2 | 39 | .2 | 21 | 9 | 1185 | 3.66 | 14 | 5 | ND | 1 | 89 | .2 | 2 | 2 | 58 | 13.12 | .017 | 2 | 35 | 3.59 | 3 | .01 | 2 | .36 | .01 | .03 | 1 |
| 74964 | 1 | 33 | 2 | 41 | .2 | 24 | 11 | 1039 | 2.93 | 19 | 5 | ND | 2 | 57 | .2 | 2 | 2 | 57 | 8.77 | .021 | 2 | 45 | 1.78 | 3 | .01 | 2 | .31 | .01 | .02 | 1 |
| 74965 | 1 | 79 | 2 | 76 | .1 | 34 | 29 | 1215 | 7.00 | 15 | 5 | ND | 2 | 2 | .2 | 2 | 2 | 221 | .02 | .048 | 6 | 52 | .05 | 20 | .01 | 3 | .73 | .01 | .04 | 1 |
| 74966 | 1 | 11 | 2 | 29 | .3 | 29 | 6 | 1180 | 4.92 | 5 | 5 | ND | 2 | 151 | .2 | 2 | 2 | 14 | 16.67 | .005 | 2 | 32 | 3.07 | 6 | .01 | 2 | .16 | .01 | .05 | 1 |
| 74967 | 5 | 40 | 11 | 65 | .4 | 12 | 6 | 748 | 2.67 | 2 | 5 | ND | 3 | 16 | .2 | 2 | 2 | 17 | 3.58 | .016 | 3 | 60 | .16 | 16 | .01 | 3 | .30 | .04 | .06 | 1 |
| 74968 | 1 | 27 | 2 | 58 | .2 | 6 | 20 | 1943 | 7.79 | 2 | 5 | ND | 3 | 89 | .4 | 2 | 3 | 44 | 10.93 | .050 | 5 | 13 | 1.43 | 36 | .01 | 2 | .45 | .02 | .08 | 1 |
| 74969 | 4 | 77 | 654. | 2254 | .5 | 8 | 13 | 821 | 3.17 | 5 | 5 | ND | 3 | 30 | 8.2 | 2 | 2 | 48 | 11.86 | .036 | 5 | 38 | .55 | 13 | .01 | 2 | 1.01 | .04 | .04 | 1 |
| 74970 | 3 | 95 | 4 | 112 | .2 | 7 | 25 | 1479 | 6.28 | 3 | 5 | ND | 3 | 12 | .2 | 2 | 2 | 68 | 1.08 | .107 | 7 | 53 | .17 | 23 | .01 | 3 | .60 | .02 | .07 | 1 |
| 74971 | 1 | 73 | 3 | 96 | .3 | 20 | 23 | 1208 | 7.03 | 3 | 5 | ND | 3 | 12 | .2 | 2 | 2 | 214 | 2.25 | .047 | 5 | 61 | 2.48 | 15 | .38 | 2 | 2.42 | .04 | .04 | 1 |
| 74972 | 2 | 41 | 3 | 2 | .2 | 1 | 2 | 18 | 3.35 | 2 | 5 | ND | 2 | 9 | .2 | 2 | 2 | 21 | .02 | .020 | 2 | 21 | .01 | 12 | .01 | 2 | .26 | .06 | .03 | 1 |
| 74973 | 3 | 23 | 2 | 100 | .3 | 15 | 12 | 772 | 4.48 | 2 | 5 | ND | 4 | 20 | .2 | 2 | 2 | 64 | 1.64 | .051 | 12 | 35 | .91 | 36 | .33 | 2 | 1.47 | .06 | .04 | 1 |
| 74974 | 2 | 69 | 144 | 921 | .3 | 6 | 10 | 892 | 3.84 | 2 | 5 | ND | 3 | 15 | 3.2 | 2 | 2 | 40 | 2.74 | .054 | 6 | 21 | .23 | 12 | .01 | 2 | .84 | .06 | .04 | 1 |
| 74975 | 3 | 41 | 3 | 95 | .2 | 20 | 12 | 780 | 4.27 | 8 | 5 | ND | 3 | 70 | .4 | 2 | 2 | 116 | 7.98 | .052 | 6 | 31 | .96 | 12 | .29 | 4 | 1.31 | .05 | .02 | 1 |
| 74976 | 3 | 44 | 3 | 112 | .3 | 10 | 15 | 622 | 2.52 | 2 | 5 | ND | 2 | 45 | .2 | 2 | 2 | 68 | 8.53 | .032 | 4 | 32 | .37 | 4 | .20 | 2 | .77 | .05 | .02 | 1 |
| 74977 | 5 | 44 | 6 | 120 | .3 | 4 | 10 | 69 | 4.79 | 2 | 5 | ND | 2 | 1 | .2 | 2 | 2 | 15 | .01 | .006 | 2 | 78 | .07 | 2 | .03 | 2 | .23 | .05 | .02 | 1 |
| 74978 | 3 | 6030 | 7 | 42 | 3.0 | 4 | 24 | 553 | 4.15 | 8 | 5 | ND | 4 | 44 | .5 | 2 | 2 | 50 | 1.34 | .133 | 10 | 25 | .83 | 83 | .06 | 2 | 1.13 | .02 | .07 | 1 |
| 74979 | 3 | 165 | 2 | 3 | .1 | 1 | 2 | 1851 | .50 | 2 | 5 | ND | 1 | 265 | .2 | 2 | 2 | 4 | 22.72 | .006 | 9 | 37 | .10 | 1583 | .01 | 2 | .37 | .01 | .05 | 1 |
| 74980 | 3 | 212 | 5 | 50 | .3 | 3 | 11 | 438 | 4.35 | 3 | 5 | ND | 6 | 41 | .2 | 2 | 2 | 117 | 1.01 | .174 | 14 | 28 | .83 | 62 | .14 | 5 | 1.23 | .05 | .12 | 1 |
| 74981 | 78 | 283 | 5 | 28 | 1.6 | 5 | 101 | 415 | 19.31 | 61 | 5 | ND | 3 | 5 | .2 | 2 | 4 | 83 | .03 | .026 | 2 | 68 | .24 | 58 | .02 | 2 | .70 | .01 | .09 | 4 |
| 86226 | 7 | 482 | 694 | 1578 | 16.0 | 77 | 90 | 1223 | 16.89 | 859 | 5 | ND | 2 | 21 | 4.3 | 33 | 3 | 10 | 1.43 | .007 | 2 | 100 | .33 | 27 | .01 | 2 | .17 | .01 | .03 | 1 |
| 86228 | 1 | 43 | 26 | 200 | .7 | 27 | 16 | 1426 | 5.20 | 10 | 5 | ND | 2 | 150 | 1.0 | 3 | 2 | 46 | 10.19 | .096 | 4 | 23 | 2.29 | 440 | .01 | 7 | .46 | .01 | .16 | 1 |
| 86229 | 1 | 85 | 14 | 161 | .6 | 30 | 25 | 1310 | 6.42 | 2 | 5 | ND | 2 | 78 | .8 | 2 | 2 | 147 | 3.55 | .112 | 6 | 70 | 2.63 | 396 | .08 | 4 | 2.23 | .04 | .08 | 1 |
| 86230 | 3 | 132 | 4 | 20 | .2 | 20 | 21 | 288 | 3.42 | 2 | 5 | ND | 1 | 17 | .2 | 2 | 2 | 61 | .69 | .049 | 2 | 52 | .58 | 28 | .17 | 2 | .97 | .12 | .12 | 1 |
| 86231 | 5 | 120 | 3 | 14 | .3 | 25 | 19 | 84 | 2.25 | 3 | 5 | ND | 2 | 47 | .2 | 2 | 2 | 30 | .85 | .051 | 3 | 83 | .12 | 6 | .19 | 2 | .85 | .14 | .04 | 1 |
| 86235 | 5 | 168 | 4 | 20 | .2 | 17 | 12 | 238 | 2.69 | 8 | 5 | ND | 2 | 50 | .2 | 2 | 2 | 34 | 1.22 | .049 | 2 | 54 | .29 | 12 | .16 | 6 | 1.32 | .10 | .05 | 1 |
| 86236 | 6 | 187 | 2 | 18 | .3 | 20 | 23 | 649 | 7.81 | 41 | 5 | ND | 3 | 10 | .2 | 2 | 2 | 61 | 2.25 | .043 | 4 | 37 | .73 | 5 | .12 | 7 | 3.56 | .01 | .03 | 1 |
| 86237 | 6 | 127 | 3 | 16 | .4 | 36 | 19 | 187 | 4.20 | 13 | 5 | ND | 3 | 103 | .2 | 2 | 2 | 83 | 3.69 | .057 | 6 | 59 | .38 | 18 | .18 | 4 | 3.18 | .16 | .09 | 1 |
| 86239 | 18 | 171 | 3 | 11 | .3 | 15 | 22 | 162 | 3.29 | 17 | 5 | ND | 2 | 7 | .2 | 2 | 2 | 54 | 1.40 | .052 | 2 | 73 | .30 | 3 | .24 | 3 | 1.16 | .05 | .03 | 1 |
| STANDARD C | 19 | 61 | 39 | 130 | 7.0 | 73 | 31 | 1049 | 3.94 | 43 | 18 | 7 | 40 | 52 | 19.7 | 16 | 20 | 60 | .45 | .095 | 40 | 60 | .90 | 188 | .08 | 37 | 1.89 | .07 | .13 | 13 |

Golden Rule Resources Ltd. FILE # 90-4927

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| 86281 | 2 | 739 | 5 | 38 | .8 | 4 | 21 | 435 | 6.62 | 3 | 5 | ND | 3 | 131 | .2 | 2 | 2 | 282 | 3.08 | .487 | 6 | 21 | 1.18 | 131 | .15 | 4 | 2.56 | .12 | .19 | 1 |
| 86282 | 1 | 20 | 2 | 36 | .6 | 73 | 32 | 297 | 10.47 | 2 | 5 | ND | 2 | 165 | .2 | 2 | 2 | 443 | 1.89 | .040 | 2 | 146 | 1.42 | 151 | .22 | 2 | 2.95 | .15 | .35 | 1 |
| 86283 | 2 | 166 | 7 | 21 | .3 | 3 | 8 | 268 | 4.20 | 2 | 5 | ND | 3 | 46 | .2 | 2 | 2 | 127 | .88 | .173 | 11 | 36 | .47 | 89 | .16 | 5 | .78 | .08 | .22 | 1 |
| 86284 | 3 | 123 | 2 | 19 | .2 | 1 | 2 | 180 | 1.46 | 2 | 5 | ND | 4 | 89 | .2 | 2 | 2 | 97 | .19 | .034 | 6 | 45 | .10 | 61 | .07 | 2 | .27 | .05 | .15 | 1 |
| 86285 | 3 | 1544 | 2 | 57 | .4 | 2 | 5 | 353 | 2.32 | 3 | 5 | ND | 2 | 85 | .2 | 2 | 2 | 113 | .33 | .055 | 8 | 50 | .20 | 30 | .08 | 3 | .43 | .06 | .12 | 1 |
| 86286 | 1 | 7 | 7 | 96 | .6 | 8 | 6 | 1815 | 4.17 | 3 | 7 | ND | 1 | 303 | .3 | 2 | 2 | 27 | 22.23 | .002 | 2 | 15 | 4.99 | 8 | .01 | 2 | .04 | .01 | .02 | 1 |
| 86287 | 4 | 78 | 5 | 64 | .4 | 6 | 11 | 1111 | 3.98 | 6 | 5 | ND | 16 | 43 | .2 | 2 | 2 | 105 | 1.66 | .116 | 15 | 35 | .89 | 59 | .06 | 8 | 1.36 | .07 | .18 | 1 |
| 86801 | 1 | 16 | 2 | 69 | .2 | 3 | 17 | 929 | 4.91 | 2 | 5 | ND | 1 | 47 | .2 | 2 | 2 | 52 | .78 | .034 | 2 | 29 | 1.67 | 24 | .21 | 3 | 2.93 | .06 | .04 | 1 |
| 86802 | 1 | 39 | 2 | 69 | .1 | 2 | 12 | 662 | 4.78 | 2 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 60 | .60 | .067 | 2 | 22 | 1.42 | 20 | .29 | 2 | 2.63 | .08 | .03 | 1 |
| 86803 | 2 | 48 | 3 | 103 | .3 | 1 | 9 | 243 | 5.01 | 2 | 5 | ND | 1 | 40 | .2 | 2 | 2 | 60 | .94 | .077 | 2 | 30 | 1.85 | 198 | .25 | 2 | 2.37 | .11 | .63 | 1 |
| 86805 | 1 | 1212 | 2 | 112 | 1.0 | 15 | 20 | 1206 | 4.67 | 5 | 5 | ND | 1 | 76 | 1.2 | 2 | 2 | 39 | 2.56 | .039 | 2 | 53 | 2.15 | 9 | .16 | 2 | 3.10 | .03 | .05 | 1 |
| 86806 | 2 | 85 | 3 | 89 | .4 | 43 | 22 | 708 | 5.96 | 3 | 5 | ND | 1 | 18 | .2 | 2 | 2 | 46 | .50 | .049 | 2 | 77 | 2.09 | 22 | .23 | 2 | 2.12 | .06 | .05 | 1 |
| 86807 | 1 | 68 | 2 | 42 | .3 | 46 | 24 | 635 | 3.53 | 4 | 5 | ND | 1 | 21 | .2 | 2 | 2 | 57 | 1.27 | .012 | 2 | 94 | 2.77 | 2 | .17 | 3 | 3.06 | .01 | .01 | 1 |
| 86808 | 3 | 111 | 2 | 7 | .3 | 18 | 20 | 91 | 3.21 | 3 | 5 | ND | 1 | 46 | .2 | 2 | 2 | 21 | .91 | .039 | 2 | 25 | .12 | 8 | .22 | 3 | .71 | .07 | .01 | 1 |
| 86810 | 1 | 36 | 5 | 72 | .3 | 7 | 13 | 1193 | 4.36 | 2 | 5 | 2 | 2 | 460 | .2 | 2 | 2 | 102 | 16.19 | .035 | 6 | 17 | 3.67 | 108 | .01 | 2 | .37 | .01 | .02 | 1 |
| 86812 | 3 | 592 | 2 | 114 | .3 | 5 | 15 | 1850 | 7.60 | 4 | 5 | ND | 5 | 9 | .2 | 2 | 2 | 57 | .55 | .101 | 8 | 53 | 1.74 | 70 | .01 | 2 | 3.37 | .01 | .19 | 1 |
| 86813 | 4 | 18910 | 22 | 63 | 10.5 | 5 | 12 | 751 | 13.89 | 15 | 10 | ND | 2 | 4 | 3.6 | 2 | 2 | 57 | .19 | .027 | 3 | 56 | .64 | 18 | .01 | 2 | 1.26 | .01 | .10 | 12 |
| 86814 | 2 | 91 | 2 | 233 | .1 | 5 | 15 | 2866 | 10.15 | 2 | 5 | ND | 6 | 19 | .2 | 2 | 2 | 82 | .37 | .128 | 12 | 25 | 1.49 | 129 | .01 | 2 | 3.52 | .01 | .26 | 1 |
| 86815 | 6 | 13340 | 5 | 246 | 4.6 | 3 | 22 | 2509 | 19.29 | 49 | 14 | ND | 3 | 5 | 1.6 | 6 | 2 | 52 | .11 | .038 | 5 | 38 | .90 | 39 | .01 | 2 | 2.95 | .01 | .07 | 5 |
| 86816 | 1 | 113 | 4 | 52 | .1 | 9 | 14 | 532 | 2.48 | 2 | 5 | ND | 1 | 82 | .2 | 2 | 2 | 116 | 3.14 | .059 | 3 | 19 | 2.30 | 23 | .09 | 3 | 2.66 | .03 | .03 | 1 |
| 86817 | 5 | 167 | 3 | 21 | .5 | 6 | 14 | 358 | 3.42 | 2 | 5 | ND | 1 | 63 | .2 | 2 | 2 | 50 | .92 | .057 | 2 | 69 | .70 | 41 | .22 | 2 | 1.22 | .03 | .06 | 6 |
| 86818 | 7 | 155 | 4 | 38 | 1.3 | 12 | 31 | 424 | 5.30 | 2 | 5 | ND | 1 | 40 | .2 | 2 | 2 | 50 | .52 | .040 | 2 | 52 | 1.15 | 62 | .17 | 2 | 1.47 | .04 | .11 | 1 |
| 86819 | 1 | 42 | 3 | 49 | .2 | 11 | 26 | 510 | 3.90 | 2 | 5 | ND | 1 | 57 | .2 | 2 | 2 | 122 | .89 | .065 | 2 | 32 | 1.94 | 23 | .16 | 2 | 2.31 | .05 | .04 | 1 |
| 86820 | 14 | 2296 | 2 | 39 | 5.9 | 13 | 53 | 316 | 7.48 | 2 | 5 | ND | 1 | 31 | .2 | 2 | 2 | 101 | .31 | .037 | 2 | 78 | .92 | 20 | .12 | 2 | 1.21 | .08 | .02 | 31 |
| 86821 | 2 | 47 | 3 | 59 | .1 | 6 | 14 | 414 | 3.68 | 5 | 5 | ND | 1 | 26 | .2 | 3 | 2 | 94 | .80 | .031 | 2 | 38 | 1.69 | 232 | .13 | 4 | 2.29 | .07 | .35 | 1 |
| 86822 | 1 | 72 | 2 | 43 | .3 | 89 | 25 | 932 | 3.60 | 8 | 5 | ND | 2 | 87 | .2 | 2 | 2 | 109 | 16.48 | .045 | 2 | 143 | .21 | 14 | .01 | 3 | .77 | .03 | .04 | 1 |
| 86823 | 1 | 11 | 2 | 51 | .1 | 2 | 7 | 543 | 2.74 | 2 | 5 | ND | 1 | 35 | .2 | 2 | 2 | 31 | 1.14 | .019 | 2 | 34 | .81 | 121 | .12 | 2 | 2.39 | .20 | .79 | 1 |
| 86824 | 1 | 51 | 2 | 80 | .1 | 12 | 15 | 776 | 4.74 | 2 | 5 | ND | 1 | 34 | .2 | 2 | 2 | 105 | .97 | .070 | 2 | 21 | 2.63 | 12 | .31 | 3 | 3.19 | .03 | .01 | 1 |
| 86825 | 15 | 2 | 5 | 2 | 47.2 | 4 | 1 | 27 | .87 | 11 | 5 | 32 | 1 | 4 | .2 | 2 | 2 | 4 | .04 | .009 | 2 | 205 | .04 | 4 | .01 | 2 | .07 | .01 | .01 | 1 |
| 86826 | 1 | 40 | 2 | 107 | .5 | 36 | 16 | 3325 | 6.34 | 2 | 5 | ND | 1 | 77 | .5 | 2 | 2 | 172 | 8.85 | .017 | 2 | 116 | 2.49 | 205 | .07 | 2 | 3.29 | .23 | .47 | 1 |
| 86828 | 1 | 77 | 2 | 80 | .3 | 37 | 19 | 984 | 5.36 | 2 | 5 | ND | 1 | 34 | .2 | 2 | 2 | 168 | 1.54 | .044 | 2 | 106 | 2.68 | 54 | .06 | 2 | 2.66 | .06 | .12 | 1 |
| 86829 | 1 | 253 | 7 | 1253 | 1.4 | 12 | 23 | 604 | 6.27 | 10 | 5 | ND | 1 | 14 | 9.1 | 2 | 2 | 123 | .42 | .025 | 2 | 39 | 1.57 | 51 | .13 | 2 | 2.86 | .12 | .30 | 1 |
| 86830 | 1 | 30 | 2 | 93 | .2 | 31 | 15 | 454 | 5.48 | 2 | 5 | ND | 1 | 57 | .2 | 2 | 2 | 153 | .92 | .015 | 2 | 99 | 2.64 | 257 | .17 | 3 | 5.66 | .33 | 1.06 | 1 |
| 86831 | 2 | 68 | 2 | 91 | .1 | 46 | 25 | 387 | 6.45 | 2 | 5 | ND | 1 | 26 | .2 | 2 | 2 | 115 | .49 | .048 | 2 | 132 | 1.66 | 36 | .14 | 2 | 2.71 | .16 | .53 | 1 |
| 86832 | 3 | 60 | 3 | 64 | .1 | 47 | 32 | 428 | 6.59 | 2 | 5 | ND | 1 | 33 | .2 | 2 | 2 | 93 | .63 | .041 | 2 | 119 | 1.15 | 31 | .16 | 2 | 2.39 | .19 | .58 | 1 |
| 86833 | 3 | 86 | 2 | 62 | .4 | 16 | 22 | 702 | 6.97 | 2 | 5 | ND | 1 | 26 | .2 | 2 | 2 | 67 | 2.32 | .022 | 2 | 64 | 1.09 | 45 | .11 | 2 | 2.04 | .19 | .42 | 1 |
| 86834 | 5 | 18 | 2 | 14 | .1 | 3 | 6 | 226 | 1.35 | 2 | 5 | ND | 1 | 31 | .2 | 2 | 2 | 29 | .89 | .025 | 2 | 66 | .33 | 7 | .15 | 2 | 1.06 | .03 | .01 | 1 |
| STANDARD C | 18 | 63 | 40 | 131 | 7.0 | 73 | 31 | 1050 | 3.94 | 38 | 17 | 7 | 39 | 52 | 19.5 | 16 | 20 | 59 | .45 | .093 | 40 | 60 | .90 | 183 | .08 | 38 | 1.89 | .06 | .14 | 13 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | Li ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|-----------|
| 86835 | 2 | 27 | 2 | 58 | .4 | 6 | 13 | 455 | 3.72 | 5 | 5 | ND | 1 | 20 | .2 | 3 | 2 | 54 | .71 | .035 | 2 | 40 | 1.79 | 14 | .11 | 7 | 2.51 | .11 | .02 | 1 |
| 86836 | 3 | 66 | 2 | 49 | .4 | 4 | 11 | 285 | 3.18 | 3 | 5 | ND | 1 | 20 | .2 | 3 | 2 | 36 | .52 | .030 | 2 | 50 | 1.18 | 31 | .06 | 7 | 1.83 | .09 | .04 | 1 |
| 86837 | 6 | 19 | 4 | 4 | 19.7 | 7 | 34 | 289 | 14.41 | 2 | 5 | 12 | 1 | 19 | .2 | 2 | 2 | 35 | .38 | .037 | 2 | 68 | .26 | 8 | .06 | 2 | .72 | .03 | .16 | 5 |
| 86838 | 8 | 375 | 2 | 1 | 40.5 | 3 | 1 | 20 | 2.29 | 7 | 5 | 16 | 1 | 5 | .2 | 2 | 4 | 8 | .02 | .002 | 2 | 138 | .01 | 16 | .01 | 6 | .03 | .01 | .02 | 168 |
| 86839 | 7 | 10807 | 4 | 88 | 4.7 | 6 | 27 | 934 | 7.51 | 9 | 5 | 5 | 1 | 7 | .7 | 2 | 2 | 64 | .19 | .027 | 3 | 72 | .46 | 19 | .04 | 8 | 1.58 | .01 | .10 | 1 |
| 86840 | 4 | 1264 | 3 | 70 | .7 | 3 | 12 | 889 | 6.51 | 2 | 5 | ND | 2 | 14 | .2 | 2 | 2 | 95 | .76 | .069 | 7 | 43 | .54 | 55 | .11 | 11 | 1.14 | .03 | .15 | 1 |
| 86841 | 2 | 92 | 2 | 79 | .4 | 6 | 24 | 646 | 4.68 | 2 | 5 | ND | 1 | 28 | .2 | 3 | 2 | 58 | .56 | .077 | 2 | 35 | 2.35 | 56 | .24 | 8 | 2.41 | .04 | .27 | 1 |
| 86842 | 2 | 53 | 2 | 70 | .3 | 17 | 10 | 530 | 4.06 | 7 | 5 | ND | 1 | 36 | .2 | 4 | 2 | 42 | .66 | .039 | 2 | 62 | 1.33 | 114 | .21 | 8 | 1.92 | .03 | .30 | 1 |
| 86853 | 1 | 19 | 6 | 12 | .1 | 1 | 2 | 3548 | 1.06 | 7 | 9 | ND | 7 | 234 | .2 | 3 | 2 | 8 | 25.97 | .010 | 12 | 14 | .26 | 62 | .01 | 4 | .23 | .01 | .04 | 1 |
| 86856 | 1 | 208 | 4 | 35 | .8 | 4 | 20 | 1740 | 8.54 | 22 | 5 | ND | 3 | 39 | .5 | 2 | 2 | 214 | 2.62 | .102 | 11 | 16 | 1.04 | 23 | .01 | 17 | .69 | .03 | .03 | 1 |
| 86857 | 9 | 8 | 4 | 38 | .3 | 5 | 2 | 965 | 2.42 | 11 | 5 | ND | 1 | 30 | .2 | 3 | 3 | 17 | 5.48 | .022 | 2 | 49 | .62 | 8 | .01 | 10 | .23 | .04 | .03 | 1 |
| 86858 | 6 | 30 | 2 | 30 | .2 | 19 | 5 | 580 | 1.80 | 11 | 5 | ND | 1 | 20 | .2 | 2 | 3 | 12 | 1.25 | .021 | 2 | 80 | .53 | 17 | .01 | 6 | .19 | .06 | .01 | 1 |
| 86859 | 5 | 42 | 9 | 199 | .4 | 28 | 12 | 811 | 4.54 | 5 | 5 | ND | 3 | 26 | .8 | 2 | 2 | 103 | 3.56 | .050 | 10 | 38 | .94 | 11 | .10 | 10 | 1.39 | .06 | .01 | 1 |
| 86860 | 7 | 70 | 2 | 27 | .1 | 103 | 25 | 894 | 8.48 | 7 | 5 | ND | 2 | 4 | .2 | 2 | 2 | 245 | .61 | .055 | 4 | 180 | 3.07 | 10 | .51 | 4 | 3.12 | .07 | .02 | 1 |
| 86861 | 1 | 73 | 4 | 54 | .2 | 7 | 24 | 1669 | 8.60 | 10 | 6 | ND | 2 | 46 | .7 | 2 | 2 | 74 | 4.00 | .069 | 5 | 15 | 1.49 | 32 | .01 | 6 | .27 | .03 | .10 | 1 |
| 86862 | 1 | 82 | 5 | 141 | .2 | 14 | 23 | 1026 | 7.01 | 3 | 8 | ND | 2 | 16 | .8 | 2 | 2 | 191 | 2.32 | .043 | 5 | 25 | 1.26 | 21 | .40 | 10 | 1.67 | .09 | .04 | 1 |
| 86863 | 1 | 87 | 2 | 62 | .1 | 98 | 35 | 715 | 6.20 | 2 | 5 | ND | 1 | 14 | .2 | 2 | 2 | 169 | 3.19 | .076 | 3 | 197 | 2.40 | 11 | .34 | 25 | 4.89 | .03 | .02 | 1 |
| 86864 | 1 | 78 | 2 | 43 | .1 | 108 | 34 | 1077 | 7.61 | 2 | 5 | ND | 3 | 20 | .2 | 2 | 2 | 205 | 2.50 | .075 | 4 | 247 | 3.15 | 26 | .41 | 19 | 5.10 | .02 | .02 | 1 |
| 86865 | 5 | 90 | 7 | 75 | .2 | 18 | 17 | 652 | 6.48 | 11 | 7 | ND | 1 | 15 | .3 | 2 | 2 | 131 | 1.65 | .041 | 3 | 46 | 2.01 | 17 | .32 | 8 | 3.14 | .03 | .04 | 1 |
| 86866 | 1 | 11 | 2 | 30 | .3 | 44 | 25 | 1321 | 6.73 | 9 | 8 | ND | 2 | 13 | .5 | 2 | 2 | 42 | 8.41 | .059 | 6 | 37 | .25 | 34 | .01 | 9 | .42 | .02 | .12 | 1 |
| 86867 | 3 | 19 | 2 | 30 | .1 | 3 | 11 | 1035 | 3.38 | 2 | 5 | ND | 1 | 5 | .2 | 2 | 2 | 6 | .44 | .085 | 13 | 67 | .06 | 35 | .01 | 11 | .41 | .08 | .10 | 1 |
| 86868 | 6 | 15 | 2 | 1 | .1 | 3 | 4 | 916 | 1.47 | 5 | 5 | ND | 1 | 5 | .2 | 2 | 2 | 4 | 1.14 | .072 | 7 | 92 | .10 | 8 | .01 | 6 | .22 | .08 | .07 | 1 |
| 86869 | 9 | 25 | 22 | 9 | .3 | 3 | 4 | 149 | 9.43 | 4 | 5 | ND | 2 | 1 | .2 | 2 | 2 | 39 | .03 | .020 | 2 | 102 | .18 | 7 | .01 | 2 | .70 | .02 | .02 | 1 |
| 86870 | 1 | 40 | 7 | 56 | .2 | 14 | 10 | 432 | 4.25 | 3 | 5 | ND | 1 | 53 | .2 | 2 | 2 | 36 | 1.47 | .041 | 4 | 54 | .91 | 74 | .13 | 10 | 2.63 | .05 | .09 | 1 |
| 86871 | 6 | 59 | 10 | 54 | .1 | 9 | 17 | 471 | 9.46 | 8 | 5 | ND | 2 | 5 | .2 | 2 | 2 | 111 | .50 | .050 | 9 | 29 | 1.10 | 17 | .29 | 4 | 1.54 | .07 | .02 | 1 |
| 86872 | 5 | 1 | 6 | 43 | .1 | 2 | 1 | 129 | .49 | 2 | 7 | ND | 7 | 6 | .5 | 2 | 2 | 1 | .06 | .020 | 6 | 73 | .04 | 49 | .01 | 5 | .44 | .06 | .18 | 1 |
| 86873 | 8 | 16 | 13 | 69 | .1 | 6 | 4 | 248 | .66 | 2 | 5 | ND | 1 | 12 | .9 | 2 | 2 | 12 | .25 | .041 | 7 | 111 | .02 | 205 | .14 | 5 | .33 | .05 | .08 | 1 |
| 86874 | 7 | 4 | 6 | 17 | .2 | 6 | 2 | 206 | 1.28 | 2 | 5 | ND | 1 | 3 | .2 | 2 | 2 | 1 | .08 | .020 | 11 | 109 | .02 | 12 | .01 | 6 | .25 | .08 | .05 | 1 |
| 86875 | 1 | 8 | 3 | 27 | .1 | 2 | 4 | 309 | 3.76 | 3 | 5 | ND | 2 | 7 | .2 | 2 | 2 | 56 | .06 | .035 | 3 | 30 | .60 | 18 | .14 | 10 | .79 | .07 | .10 | 1 |
| 86876 | 4 | 229 | 28 | 126 | 1.1 | 4 | 12 | 1094 | 6.18 | 18 | 5 | ND | 3 | 27 | .6 | 3 | 2 | 157 | .89 | .189 | 9 | 17 | 2.00 | 17 | .43 | 8 | 2.52 | .06 | .05 | 1 |
| 86877 | 3 | 4815 | 4 | 89 | 1.2 | 3 | 13 | 1395 | 6.04 | 7 | 6 | 3 | 3 | 25 | .4 | 2 | 2 | 97 | .87 | .069 | 6 | 33 | .99 | 32 | .12 | 13 | 1.40 | .04 | .08 | 1 |
| 86878 | 2 | 510 | 4 | 126 | .2 | 4 | 11 | 1639 | 5.10 | 6 | 8 | ND | 3 | 28 | .2 | 2 | 2 | 88 | 1.12 | .070 | 6 | 34 | 1.39 | 41 | .14 | 11 | 1.67 | .06 | .10 | 1 |
| 86879 | 1 | 10 | 6 | 114 | .6 | 43 | 30 | 1683 | 8.39 | 13 | 5 | ND | 1 | 5 | .2 | 2 | 2 | 143 | .49 | .089 | 4 | 110 | 3.10 | 15 | .06 | 4 | 2.62 | .05 | .02 | 1 |
| 86880 | 2 | 462 | 3 | 137 | .3 | 3 | 11 | 1309 | 4.83 | 3 | 8 | ND | 3 | 20 | .4 | 2 | 2 | 107 | 1.12 | .079 | 9 | 34 | 1.25 | 45 | .13 | 11 | 1.62 | .05 | .09 | 1 |
| 86881 | 1 | 1 | 2 | 6 | .1 | 1258 | 63 | 335 | 3.78 | 137 | 5 | ND | 1 | 111 | .3 | 2 | 2 | 15 | 1.44 | .004 | 2 | 728 | 14.15 | 168 | .01 | 26 | .07 | .02 | .01 | 1 |
| 86882 | 1 | 8 | 23 | 74 | .1 | 24 | 9 | 223 | 3.73 | 6 | 12 | ND | 18 | 12 | .2 | 3 | 2 | 6 | .12 | .048 | 41 | 50 | .92 | 146 | .01 | 9 | 1.66 | .01 | .21 | 1 |
| 86883 | 13 | 15 | 27 | 78 | 1.2 | 10 | 1 | 210 | .44 | 2 | 5 | ND | 1 | 7 | .5 | 6 | 2 | 3 | .04 | .009 | 2 | 196 | .04 | 44 | .01 | 3 | .06 | .01 | .01 | 1 |
| STANDARD C | 17 | 59 | 37 | 130 | 7.0 | 73 | 32 | 1052 | 3.95 | 45 | 22 | 7 | 39 | 52 | 19.5 | 15 | 20 | 58 | .46 | .096 | 39 | 60 | .89 | 183 | .08 | 36 | 1.90 | .06 | .14 | 12 |

| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Be ppm | Tl ppm | B ppm | Al % | Na % | K % | Si ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|-----------|----------|---------|---------|--------|-----------|
| 86989 | 4 | 575 | 8 | 33 | 2 | 17 | 8 | 682 | 5.24 | 1178 | 5 | ND | 1 | 33 | .5 | 3 | 2 | 83 | 3.44 | .102 | 6 | 45 | 1.58 | 133 | .105 | 2 | 2.04 | .02 | .07 | 4 |
| 86990 | 2 | 328 | 8 | 32 | 1 | 56 | 14 | 863 | 5.12 | 162 | 5 | ND | 1 | 55 | 1.0 | 2 | 2 | 112 | 5.14 | .097 | 3 | 118 | 2.25 | 20 | .113 | 3 | 2.26 | .03 | .06 | 5 |
| 86991 | 1 | 1140 | 8 | 48 | 1 | 86 | 19 | 1054 | 6.01 | 626 | 5 | ND | 1 | 31 | 1.2 | 2 | 2 | 127 | 1.98 | .089 | 3 | 191 | 3.30 | 32 | .118 | 3 | 3.02 | .05 | .09 | 4 |
| 86992 | 1 | 314 | 7 | 30 | 1 | 32 | 16 | 899 | 4.94 | 168 | 5 | ND | 1 | 31 | 1.2 | 2 | 2 | 106 | .76 | .135 | 3 | 64 | 2.29 | 42 | .114 | 4 | 2.39 | .03 | .06 | 3 |
| 86993 | 1 | 365 | 6 | 36 | 1 | 73 | 18 | 1010 | 6.04 | 127 | 5 | ND | 1 | 23 | 1.8 | 2 | 2 | 128 | .52 | .094 | 4 | 170 | 2.64 | 44 | .116 | 2 | 2.86 | .04 | .07 | 3 |
| JRG 95 | 4 | 85 | 4 | 47 | 1 | 13 | 16 | 734 | 2.49 | 2 | 5 | ND | 2 | 69 | 1.1 | 2 | 2 | 47 | .54 | .058 | 4 | 60 | .80 | 169 | .07 | 3 | 1.34 | .03 | .10 | 1 |
| JRG 250 | 2 | 124 | 18 | 77 | 2 | 41 | 31 | 1714 | 6.00 | 2 | 5 | ND | 1 | 56 | 1.4 | 2 | 2 | 120 | .73 | .071 | 3 | 106 | 2.69 | 90 | .119 | 2 | 3.16 | .02 | .19 | 1 |
| JRG 251 | 2 | 169 | 6 | 111 | 2 | 59 | 31 | 2061 | 6.54 | 5 | 5 | ND | 1 | 70 | .9 | 2 | 2 | 124 | .76 | .073 | 2 | 147 | 3.06 | 104 | .114 | 2 | 3.78 | .03 | .15 | 1 |
| JRG 252 | 5 | 193 | 23 | 91 | 2 | 55 | 43 | 3833 | 6.61 | 6 | 5 | ND | 1 | 69 | 1.2 | 2 | 2 | 126 | .70 | .082 | 3 | 131 | 2.84 | 127 | .115 | 2 | 3.48 | .03 | .14 | 1 |
| JRG 253 | 4 | 266 | 19 | 101 | 3 | 60 | 37 | 2175 | 7.09 | 4 | 5 | ND | 1 | 83 | 1.0 | 2 | 2 | 126 | .78 | .081 | 4 | 148 | 2.98 | 97 | .113 | 2 | 3.75 | .03 | .12 | 1 |
| JRG 254 | 4 | 290 | 16 | 83 | 15 | 56 | 34 | 1661 | 6.38 | 2 | 5 | ND | 1 | 92 | 1.2 | 2 | 2 | 121 | .80 | .077 | 3 | 133 | 2.76 | 89 | .113 | 2 | 3.51 | .03 | .13 | 2 |
| JRG 255 | 3 | 198 | 4 | 97 | 15 | 40 | 28 | 1484 | 5.48 | 4 | 5 | ND | 1 | 99 | 1.4 | 2 | 2 | 100 | .88 | .083 | 3 | 101 | 2.47 | 95 | .112 | 2 | 3.21 | .03 | .11 | 1 |
| JRG 256 | 4 | 212 | 7 | 67 | 15 | 37 | 28 | 1251 | 5.68 | 2 | 5 | ND | 1 | 75 | 1.4 | 2 | 2 | 111 | .75 | .070 | 3 | 98 | 2.36 | 56 | .115 | 2 | 2.86 | .04 | .11 | 4 |
| JRG 257 | 2 | 239 | 14 | 73 | 13 | 44 | 30 | 1482 | 5.73 | 3 | 5 | ND | 1 | 74 | 1.3 | 2 | 2 | 112 | .67 | .073 | 2 | 97 | 2.55 | 61 | .113 | 2 | 3.07 | .02 | .09 | 1 |
| JRG 258 | 3 | 247 | 9 | 78 | 12 | 40 | 28 | 1440 | 5.39 | 2 | 5 | ND | 1 | 76 | 1.0 | 2 | 2 | 107 | .76 | .079 | 3 | 96 | 2.40 | 77 | .111 | 2 | 3.07 | .03 | .12 | 1 |
| JRG 259 | 3 | 178 | 7 | 61 | 12 | 32 | 24 | 1152 | 4.85 | 2 | 5 | ND | 1 | 64 | 1.2 | 2 | 2 | 101 | .67 | .071 | 2 | 84 | 2.22 | 58 | .112 | 4 | 2.62 | .03 | .10 | 7 |
| JRG 260 | 5 | 158 | 14 | 58 | 12 | 30 | 22 | 1023 | 4.39 | 2 | 5 | ND | 1 | 56 | 1.3 | 2 | 2 | 97 | .64 | .065 | 2 | 76 | 2.06 | 56 | .112 | 3 | 2.43 | .03 | .11 | 5 |
| JRG 261 | 3 | 193 | 11 | 58 | 12 | 34 | 24 | 1113 | 4.93 | 2 | 5 | ND | 1 | 62 | 1.2 | 2 | 2 | 105 | .66 | .068 | 2 | 85 | 2.26 | 59 | .113 | 2 | 2.68 | .04 | .12 | 1 |
| JRG 262 | 4 | 154 | 11 | 55 | 12 | 31 | 21 | 978 | 4.60 | 2 | 5 | ND | 1 | 63 | 1.2 | 2 | 2 | 103 | .75 | .064 | 3 | 97 | 2.11 | 62 | .115 | 2 | 2.53 | .05 | .15 | 2 |
| JRG 263 | 4 | 198 | 7 | 65 | 11 | 16 | 19 | 867 | 2.79 | 2 | 5 | ND | 1 | 60 | 1.3 | 2 | 2 | 70 | .59 | .065 | 2 | 55 | 1.40 | 79 | .111 | 2 | 1.66 | .03 | .15 | 1 |
| JRG 264 | 4 | 210 | 5 | 72 | 12 | 26 | 23 | 1047 | 4.16 | 2 | 5 | ND | 1 | 64 | 1.2 | 2 | 2 | 92 | .66 | .070 | 2 | 73 | 1.96 | 77 | .112 | 2 | 2.31 | .03 | .14 | 1 |
| JRG 265 | 5 | 161 | 12 | 58 | 12 | 26 | 21 | 932 | 3.92 | 4 | 5 | ND | 1 | 64 | 1.2 | 2 | 2 | 93 | .77 | .066 | 2 | 89 | 1.83 | 72 | .116 | 2 | 2.24 | .05 | .16 | 1 |
| JRG 266 | 11 | 131 | 9 | 50 | 12 | 28 | 28 | 1060 | 3.96 | 2 | 5 | ND | 1 | 80 | 1.6 | 2 | 2 | 96 | 1.06 | .060 | 3 | 107 | 1.64 | 75 | .118 | 2 | 2.11 | .08 | .23 | 2 |
| JRG 267 | 4 | 167 | 16 | 68 | 11 | 26 | 23 | 978 | 4.03 | 2 | 5 | ND | 1 | 56 | 1.2 | 2 | 2 | 92 | .65 | .067 | 2 | 72 | 1.89 | 69 | .113 | 2 | 2.20 | .03 | .15 | 1 |
| JRG 268 | 4 | 177 | 13 | 76 | 12 | 26 | 24 | 1017 | 4.19 | 2 | 5 | ND | 1 | 64 | 1.2 | 2 | 2 | 95 | .73 | .067 | 2 | 77 | 1.93 | 77 | .114 | 2 | 2.31 | .04 | .18 | 1 |
| JRG 269 | 5 | 148 | 13 | 68 | 12 | 35 | 23 | 1006 | 4.00 | 4 | 5 | ND | 1 | 71 | 1.2 | 2 | 2 | 92 | .83 | .066 | 2 | 95 | 1.86 | 84 | .114 | 2 | 2.28 | .05 | .19 | 2 |
| JRG 270 | 4 | 134 | 9 | 65 | 11 | 28 | 22 | 987 | 3.83 | 2 | 5 | ND | 1 | 67 | 1.2 | 2 | 2 | 90 | .74 | .067 | 2 | 80 | 1.82 | 74 | .114 | 2 | 2.17 | .04 | .17 | 1 |
| JRG 271 | 7 | 72 | 31 | 52 | 13 | 12 | 12 | 848 | 3.53 | 2 | 5 | ND | 3 | 89 | 1.2 | 2 | 2 | 80 | .73 | .079 | 9 | 59 | 1.01 | 118 | .110 | 2 | 2.05 | .05 | .13 | 2 |
| JRG 272 | 12 | 141 | 39 | 74 | 13 | 18 | 17 | 1063 | 3.85 | 2 | 5 | ND | 2 | 97 | 1.2 | 2 | 2 | 93 | .89 | .080 | 8 | 69 | 1.41 | 169 | .113 | 2 | 2.88 | .05 | .22 | 5 |
| JRG 273 | 12 | 31 | 19 | 39 | 14 | 9 | 10 | 964 | 2.38 | 3 | 5 | ND | 4 | 65 | 1.2 | 2 | 2 | 59 | .61 | .062 | 8 | 91 | .71 | 70 | .108 | 2 | 1.29 | .06 | .12 | 1 |
| JRG 274 | 7 | 47 | 6 | 38 | 12 | 13 | 12 | 653 | 3.47 | 5 | 5 | ND | 3 | 74 | 1.2 | 2 | 2 | 94 | .99 | .061 | 5 | 90 | .98 | 67 | .113 | 2 | 1.61 | .08 | .16 | 3 |
| JRG 275 | 6 | 56 | 4 | 42 | 13 | 13 | 13 | 651 | 2.75 | 3 | 5 | ND | 4 | 67 | 1.0 | 2 | 2 | 80 | .89 | .063 | 5 | 61 | 1.04 | 81 | .113 | 2 | 1.63 | .07 | .16 | 2 |
| JRG 276 | 8 | 57 | 26 | 39 | 11 | 14 | 13 | 602 | 2.92 | 2 | 5 | ND | 2 | 71 | 1.2 | 2 | 2 | 85 | 1.05 | .055 | 5 | 78 | 1.08 | 68 | .114 | 2 | 1.70 | .08 | .16 | 3 |
| JRG 277 | 6 | 65 | 12 | 38 | 12 | 15 | 15 | 607 | 3.10 | 2 | 5 | ND | 2 | 70 | 1.2 | 2 | 2 | 88 | 1.04 | .062 | 5 | 66 | 1.11 | 63 | .114 | 3 | 1.68 | .06 | .15 | 3 |
| JRG 278 | 8 | 65 | 12 | 46 | 12 | 14 | 13 | 603 | 2.62 | 2 | 5 | ND | 3 | 65 | 1.2 | 2 | 2 | 75 | .84 | .049 | 3 | 56 | .99 | 69 | .112 | 5 | 1.59 | .05 | .14 | 9 |
| JRG 279 | 7 | 69 | 15 | 41 | 11 | 12 | 13 | 601 | 2.82 | 2 | 5 | ND | 2 | 66 | 1.2 | 2 | 2 | 79 | .87 | .052 | 4 | 51 | 1.04 | 66 | .112 | 2 | 1.62 | .06 | .13 | 7 |
| STANDARD C | 17 | 63 | 40 | 132 | 7.5 | 73 | 31 | 1037 | 3.99 | 42 | 19 | 7 | 39 | 52 | 18.4 | 14 | 21 | 56 | .49 | .094 | 37 | 60 | .90 | 179 | .108 | 34 | 1.90 | .06 | .13 | 11 |

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| SAMPLE# | No | Cu | Pb | Zn | Ag | Wf | Co | Mn | Fe | As | U | Au | Tb | Sr | Yod | Sb | Bi | V | Ca | P | La | Cr | Mg | Ba | U | B | Al | Na | K | Si |
|------------|-----|-----|-----|-----|-----|-----|-----|-------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|------|-----|-----|-----|------|-----|-----|-----|
| | ppm | ppm | % | ppm | % | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm |
| JRG 280 | 7 | 70 | 11 | 41 | 12 | 15 | 15 | 608 | 2.91 | 2 | 5 | ND | 1 | 71 | 15 | 2 | 2 | 79 | .88 | 1054 | 4 | 50 | 1.17 | 72 | 13 | 2 | 1.75 | .06 | .14 | 3 |
| JRG 281 | 6 | 60 | 5 | 39 | 12 | 13 | 13 | 428 | 3.14 | 2 | 5 | ND | 1 | 71 | 12 | 2 | 2 | 88 | 1.08 | 1058 | 3 | 60 | 1.11 | 55 | 136 | 2 | 1.65 | .07 | .15 | 3 |
| JRG 282 | 6 | 63 | 7 | 47 | 12 | 15 | 14 | 447 | 2.87 | 2 | 5 | ND | 1 | 67 | 12 | 2 | 2 | 81 | .90 | 1056 | 4 | 60 | 1.14 | 59 | 134 | 2 | 1.62 | .07 | .14 | 2 |
| JRG 283 | 6 | 66 | 5 | 46 | 12 | 14 | 13 | 482 | 2.88 | 2 | 5 | ND | 1 | 67 | 12 | 2 | 2 | 78 | .82 | 1055 | 3 | 52 | 1.17 | 65 | 133 | 2 | 1.67 | .06 | .14 | 2 |
| JRG 284 | 4 | 61 | 3 | 47 | 12 | 14 | 13 | 419 | 2.80 | 2 | 5 | ND | 1 | 61 | 15 | 2 | 2 | 79 | .94 | 1054 | 3 | 55 | 1.12 | 48 | 135 | 2 | 1.54 | .07 | .14 | 2 |
| JRG 285 | 5 | 69 | 10 | 54 | 12 | 18 | 14 | 472 | 2.85 | 2 | 5 | ND | 1 | 68 | 19 | 2 | 2 | 76 | .90 | 1060 | 4 | 64 | 1.27 | 66 | 136 | 2 | 1.71 | .07 | .16 | 2 |
| JRG 286 | 6 | 81 | 6 | 51 | 12 | 18 | 14 | 475 | 2.98 | 2 | 5 | ND | 1 | 76 | 13 | 2 | 2 | 78 | .93 | 1056 | 4 | 72 | 1.25 | 74 | 133 | 2 | 1.77 | .08 | .17 | 1 |
| JRG 287 | 4 | 76 | 3 | 40 | 11 | 19 | 13 | 460 | 2.62 | 2 | 5 | ND | 1 | 72 | 12 | 2 | 2 | 69 | .76 | 1053 | 4 | 51 | 1.21 | 77 | 142 | 2 | 1.66 | .06 | .15 | 1 |
| JRG 288 | 3 | 54 | 6 | 41 | 11 | 17 | 12 | 408 | 2.35 | 3 | 5 | ND | 1 | 55 | 13 | 2 | 2 | 67 | .78 | 1053 | 3 | 52 | 1.14 | 54 | 132 | 2 | 1.44 | .06 | .14 | 1 |
| JRG 289 | 4 | 67 | 6 | 52 | 12 | 20 | 14 | 433 | 2.75 | 2 | 5 | ND | 1 | 64 | 15 | 2 | 2 | 75 | .89 | 1058 | 2 | 64 | 1.22 | 56 | 136 | 2 | 1.56 | .06 | .15 | 2 |
| TRG 1 | 6 | 75 | 10 | 91 | 11 | 2 | 9 | 905 | 3.25 | 7 | 5 | ND | 1 | 27 | 12 | 2 | 2 | 63 | .52 | 1099 | 7 | 45 | .57 | 55 | 105 | 3 | 1.12 | .04 | .09 | 1 |
| TRG 2 | 6 | 78 | 7 | 85 | 12 | 4 | 10 | 994 | 3.38 | 7 | 5 | ND | 1 | 42 | 12 | 2 | 2 | 85 | .70 | 100 | 7 | 56 | .65 | 58 | 107 | 2 | 1.33 | .06 | .11 | 1 |
| TRG 3 | 6 | 82 | 10 | 75 | 12 | 2 | 11 | 914 | 4.86 | 5 | 5 | ND | 1 | 35 | 12 | 2 | 2 | 155 | .71 | 119 | 8 | 57 | .70 | 46 | 110 | 5 | 1.23 | .06 | .10 | 1 |
| TRG 4 | 5 | 70 | 3 | 72 | 11 | 2 | 9 | 851 | 3.45 | 2 | 5 | ND | 1 | 35 | 12 | 2 | 2 | 97 | .67 | 105 | 8 | 49 | .63 | 51 | 108 | 3 | 1.14 | .05 | .10 | 2 |
| TRG 5 | 5 | 89 | 5 | 85 | 11 | 5 | 10 | 982 | 4.35 | 9 | 5 | ND | 1 | 33 | 14 | 2 | 2 | 140 | .67 | 113 | 9 | 38 | .62 | 63 | 108 | 4 | 1.18 | .04 | .08 | 1 |
| TRG 6 | 6 | 94 | 5 | 84 | 11 | 4 | 10 | 926 | 5.04 | 12 | 6 | ND | 2 | 23 | 12 | 2 | 2 | 169 | .53 | 1099 | 10 | 45 | .49 | 48 | 108 | 3 | .97 | .03 | .07 | 1 |
| TRG 7 | 6 | 85 | 2 | 80 | 12 | 9 | 11 | 938 | 3.66 | 9 | 5 | ND | 3 | 27 | 13 | 2 | 2 | 89 | .52 | 1082 | 10 | 46 | .53 | 60 | 106 | 3 | 1.05 | .04 | .08 | 1 |
| TRG 8 | 7 | 84 | 13 | 79 | 12 | 4 | 9 | 924 | 3.28 | 8 | 5 | ND | 2 | 25 | 12 | 2 | 2 | 79 | .57 | 1092 | 9 | 49 | .51 | 50 | 106 | 7 | 1.03 | .04 | .08 | 1 |
| TRG 9 | 6 | 77 | 10 | 91 | 11 | 5 | 10 | 955 | 4.40 | 5 | 5 | ND | 2 | 25 | 13 | 2 | 2 | 129 | .59 | 1096 | 8 | 60 | .55 | 49 | 107 | 6 | 1.03 | .04 | .08 | 1 |
| TRG 10 | 9 | 67 | 18 | 81 | 11 | 8 | 12 | 847 | 8.62 | 2 | 5 | ND | 1 | 25 | 16 | 2 | 2 | 331 | .65 | 1094 | 7 | 81 | .53 | 39 | 112 | 4 | .97 | .05 | .08 | 1 |
| TRG 11 | 6 | 75 | 6 | 74 | 11 | 10 | 12 | 919 | 5.52 | 9 | 5 | ND | 1 | 27 | 12 | 2 | 2 | 181 | .68 | 103 | 7 | 74 | .63 | 47 | 109 | 7 | 1.03 | .04 | .09 | 1 |
| TRG 12 | 5 | 73 | 14 | 75 | 11 | 14 | 12 | 807 | 5.88 | 6 | 5 | ND | 1 | 24 | 14 | 2 | 2 | 208 | .68 | 1093 | 7 | 75 | .63 | 39 | 109 | 6 | .95 | .04 | .07 | 1 |
| TRG 13 1/2 | 4 | 56 | 11 | 64 | 11 | 8 | 16 | 713 | 4.68 | 6 | 5 | ND | 1 | 26 | 12 | 2 | 2 | 158 | .74 | 1095 | 7 | 62 | .69 | 31 | 110 | 6 | 1.05 | .04 | .07 | 1 |
| TRG 13 2/2 | 3 | 64 | 7 | 69 | 11 | 10 | 10 | 743 | 3.00 | 7 | 5 | ND | 1 | 24 | 12 | 2 | 2 | 78 | .61 | 1079 | 6 | 61 | .59 | 39 | 106 | 3 | .90 | .04 | .07 | 1 |
| TRG 14 | 9 | 49 | 7 | 101 | 12 | 8 | 51 | 10873 | 5.65 | 16 | 5 | ND | 1 | 41 | 15 | 2 | 2 | 135 | .81 | 100 | 4 | 68 | .77 | 255 | 107 | 2 | 1.67 | .04 | .07 | 2 |
| TRG 15 | 1 | 63 | 2 | 65 | 11 | 20 | 16 | 1886 | 3.27 | 17 | 5 | ND | 1 | 20 | 12 | 2 | 2 | 79 | .60 | 1043 | 3 | 39 | .82 | 52 | 106 | 2 | 1.56 | .02 | .06 | 1 |
| TRG 16 | 1 | 83 | 7 | 61 | 11 | 28 | 19 | 685 | 4.01 | 10 | 5 | ND | 1 | 23 | 12 | 2 | 2 | 71 | .49 | 1032 | 2 | 48 | .98 | 35 | 103 | 3 | 1.58 | .03 | .04 | 1 |
| TRG 17 | 4 | 117 | 9 | 97 | 12 | 44 | 30 | 1244 | 6.75 | 65 | 5 | ND | 1 | 47 | 9 | 3 | 2 | 112 | .75 | 1053 | 3 | 80 | 1.31 | 72 | 105 | 5 | 2.53 | .05 | .07 | 1 |
| TRG 18 | 2 | 92 | 8 | 83 | 11 | 42 | 24 | 1034 | 5.66 | 45 | 5 | ND | 1 | 45 | 12 | 2 | 2 | 103 | .85 | 1068 | 3 | 65 | 1.48 | 73 | 107 | 5 | 2.30 | .04 | .05 | 1 |
| TRG 19 | 1 | 89 | 10 | 76 | 12 | 40 | 22 | 935 | 5.49 | 53 | 5 | ND | 1 | 37 | 12 | 2 | 2 | 105 | .91 | 1050 | 2 | 84 | 1.54 | 70 | 108 | 8 | 2.28 | .05 | .05 | 1 |
| TRG 20 | 1 | 107 | 6 | 80 | 11 | 40 | 24 | 1108 | 5.97 | 58 | 5 | ND | 1 | 46 | 12 | 2 | 2 | 111 | .81 | 1052 | 3 | 80 | 1.38 | 95 | 107 | 9 | 2.18 | .04 | .06 | 1 |
| TRG 21 | 2 | 102 | 3 | 79 | 11 | 38 | 21 | 826 | 6.48 | 39 | 5 | ND | 1 | 29 | 12 | 3 | 2 | 157 | .95 | 1055 | 3 | 100 | 1.50 | 59 | 111 | 5 | 2.24 | .05 | .07 | 1 |
| TRG 22 | 1 | 86 | 8 | 76 | 11 | 35 | 22 | 927 | 5.44 | 62 | 5 | ND | 1 | 34 | 12 | 2 | 2 | 112 | .79 | 1055 | 3 | 76 | 1.37 | 70 | 108 | 4 | 1.96 | .04 | .06 | 1 |
| TRG 23 | 1 | 75 | 10 | 67 | 11 | 31 | 20 | 855 | 5.89 | 32 | 5 | ND | 1 | 25 | 12 | 3 | 2 | 148 | .73 | 1058 | 3 | 80 | 1.27 | 58 | 109 | 5 | 1.74 | .04 | .06 | 1 |
| TRG 24 | 2 | 84 | 2 | 74 | 11 | 31 | 21 | 967 | 5.54 | 56 | 5 | ND | 1 | 31 | 12 | 2 | 2 | 127 | .74 | 1063 | 4 | 80 | 1.19 | 73 | 107 | 5 | 1.76 | .03 | .06 | 1 |
| TRG 25 | 2 | 185 | 11 | 76 | 11 | 27 | 19 | 851 | 4.65 | 240 | 5 | ND | 1 | 32 | 12 | 2 | 2 | 86 | .74 | 1068 | 4 | 69 | 1.26 | 144 | 104 | 4 | 1.72 | .02 | .08 | 1 |
| TRG 26 | 4 | 70 | 9 | 67 | 11 | 15 | 11 | 697 | 3.01 | 15 | 5 | ND | 1 | 28 | 12 | 2 | 2 | 76 | .65 | 1079 | 5 | 76 | .71 | 49 | 107 | 3 | 1.08 | .05 | .09 | 1 |
| STANDARD C | 18 | 62 | 43 | 132 | 7.5 | 69 | 31 | 1061 | 3.99 | 42 | 17 | 7 | 36 | 52 | 18 | 19 | 22 | 55 | .48 | 1094 | 36 | 60 | .90 | 180 | 107 | 33 | 1.90 | .06 | .13 | 11 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| DK-78 | 5 | 85 | 2 | 37 | .1 | 17 | 13 | 444 | 3.81 | 2 | 5 | ND | 1 | 124 | .2 | 2 | 2 | 97 | .74 | .132 | 6 | 90 | .63 | 121 | .08 | 2 | .62 | .04 | .15 | 1 |
| DK-79 | 5 | 160 | 4 | 62 | .1 | 29 | 20 | 698 | 3.81 | 3 | 5 | ND | 1 | 149 | .2 | 2 | 2 | 92 | .79 | .147 | 8 | 81 | 1.16 | 204 | .14 | 3 | 1.11 | .04 | .27 | 1 |
| DK-80 | 6 | 66 | 2 | 31 | .2 | 20 | 14 | 486 | 6.89 | 3 | 5 | ND | 1 | 118 | .2 | 2 | 2 | 177 | .64 | .112 | 6 | 145 | .38 | 113 | .07 | 5 | .54 | .05 | .13 | 1 |
| DK-81A | 5 | 105 | 2 | 45 | .2 | 24 | 16 | 505 | 5.59 | 2 | 5 | ND | 1 | 137 | .2 | 5 | 2 | 139 | .92 | .191 | 9 | 114 | .76 | 123 | .10 | 4 | .73 | .04 | .16 | 1 |
| DK-81B | 5 | 76 | 2 | 36 | .1 | 17 | 12 | 461 | 4.22 | 2 | 5 | ND | 1 | 120 | .2 | 2 | 2 | 109 | .70 | .139 | 7 | 91 | .49 | 106 | .07 | 3 | .56 | .04 | .13 | 1 |
| DK-82 | 5 | 101 | 2 | 44 | .1 | 21 | 15 | 541 | 4.30 | 2 | 5 | ND | 1 | 125 | .2 | 2 | 2 | 106 | .69 | .132 | 6 | 89 | .70 | 137 | .09 | 2 | .73 | .03 | .16 | 1 |
| DK-83 | 8 | 61 | 2 | 44 | .1 | 15 | 10 | 459 | 4.84 | 2 | 5 | ND | 1 | 124 | .2 | 2 | 2 | 128 | .60 | .094 | 5 | 131 | .33 | 118 | .06 | 4 | .54 | .06 | .15 | 1 |
| DK-84 | 4 | 96 | 2 | 47 | .1 | 17 | 12 | 501 | 3.90 | 3 | 5 | ND | 1 | 91 | .2 | 2 | 3 | 92 | .71 | .159 | 12 | 67 | .56 | 130 | .08 | 2 | .77 | .03 | .14 | 2 |
| DK-85 | 6 | 68 | 2 | 29 | .1 | 13 | 9 | 431 | 3.48 | 2 | 5 | ND | 1 | 112 | .2 | 2 | 2 | 91 | .56 | .095 | 5 | 96 | .38 | 112 | .06 | 2 | .56 | .05 | .14 | 1 |
| DK-86 | 5 | 85 | 2 | 34 | .1 | 14 | 10 | 442 | 2.53 | 2 | 5 | ND | 1 | 115 | .2 | 2 | 2 | 64 | .51 | .087 | 5 | 67 | .51 | 124 | .07 | 2 | .66 | .04 | .15 | 1 |
| DK-88 | 3 | 165 | 2 | 89 | .1 | 39 | 23 | 615 | 4.18 | 18 | 5 | ND | 1 | 125 | .4 | 3 | 2 | 122 | 1.24 | .081 | 2 | 65 | 1.37 | 67 | .18 | 5 | 3.54 | .04 | .06 | 1 |
| DK-89 | 2 | 114 | 30 | 144 | .3 | 51 | 18 | 512 | 4.01 | 10 | 5 | ND | 1 | 65 | .9 | 2 | 2 | 105 | .97 | .076 | 3 | 95 | 1.65 | 45 | .17 | 4 | 5.22 | .03 | .06 | 1 |
| DK-90 | 4 | 101 | 4 | 104 | .3 | 42 | 18 | 634 | 3.66 | 36 | 5 | ND | 1 | 91 | .8 | 2 | 2 | 105 | 1.60 | .061 | 2 | 83 | 1.40 | 46 | .16 | 5 | 2.85 | .08 | .07 | 1 |
| DK-91 | 4 | 96 | 5 | 101 | .3 | 40 | 20 | 725 | 3.76 | 37 | 5 | ND | 1 | 84 | .8 | 2 | 2 | 110 | 1.51 | .057 | 3 | 81 | 1.39 | 44 | .17 | 5 | 2.74 | .08 | .06 | 1 |
| DK-92 | 4 | 100 | 6 | 56 | .1 | 14 | 13 | 614 | 3.92 | 7 | 5 | ND | 1 | 86 | .3 | 2 | 2 | 110 | .97 | .108 | 6 | 40 | .79 | 75 | .10 | 5 | 1.80 | .04 | .06 | 1 |
| DK-93 | 6 | 75 | 4 | 58 | .1 | 13 | 12 | 685 | 3.31 | 7 | 5 | ND | 1 | 96 | .2 | 2 | 2 | 91 | 1.15 | .095 | 6 | 69 | .73 | 69 | .11 | 5 | 1.70 | .06 | .07 | 1 |
| DK-94 | 5 | 89 | 2 | 55 | .2 | 12 | 13 | 719 | 3.43 | 10 | 5 | ND | 1 | 92 | .2 | 2 | 2 | 96 | 1.07 | .095 | 5 | 62 | .70 | 70 | .11 | 5 | 1.67 | .05 | .07 | 1 |
| DK-95 | 5 | 90 | 2 | 58 | .1 | 11 | 11 | 646 | 3.11 | 7 | 5 | ND | 1 | 86 | .3 | 2 | 2 | 87 | .96 | .100 | 7 | 71 | .65 | 75 | .09 | 4 | 1.47 | .06 | .08 | 1 |
| DK-96 | 3 | 84 | 2 | 49 | .1 | 12 | 12 | 620 | 4.04 | 7 | 5 | ND | 1 | 76 | .2 | 2 | 2 | 122 | .85 | .092 | 6 | 51 | .60 | 60 | .10 | 5 | 1.35 | .04 | .06 | 1 |
| DK-97 | 4 | 74 | 2 | 44 | .1 | 11 | 10 | 532 | 3.01 | 3 | 5 | ND | 1 | 74 | .2 | 2 | 2 | 85 | .87 | .090 | 4 | 53 | .59 | 57 | .09 | 4 | 1.29 | .05 | .07 | 1 |
| DK-98 | 4 | 89 | 3 | 43 | .1 | 11 | 10 | 530 | 3.72 | 2 | 5 | ND | 1 | 70 | .2 | 2 | 2 | 113 | .78 | .105 | 6 | 53 | .56 | 59 | .09 | 3 | 1.17 | .04 | .07 | 1 |
| DK-99 | 4 | 82 | 2 | 42 | .1 | 11 | 10 | 495 | 3.49 | 5 | 5 | ND | 1 | 72 | .2 | 2 | 2 | 106 | .79 | .097 | 7 | 56 | .56 | 60 | .09 | 4 | 1.17 | .05 | .07 | 1 |
| DK-101 | 6 | 83 | 2 | 39 | .1 | 25 | 28 | 448 | 2.41 | 2 | 5 | ND | 1 | 76 | .2 | 2 | 2 | 76 | .62 | .048 | 3 | 93 | .50 | 38 | .07 | 3 | .92 | .05 | .11 | 2 |
| DK-102 | 5 | 91 | 3 | 41 | .1 | 29 | 31 | 619 | 2.71 | 2 | 5 | ND | 1 | 90 | .2 | 2 | 2 | 81 | .67 | .058 | 3 | 78 | .57 | 45 | .07 | 2 | .98 | .03 | .10 | 2 |
| DK-103 | 5 | 74 | 2 | 36 | .1 | 26 | 29 | 483 | 2.51 | 2 | 5 | ND | 1 | 95 | .2 | 2 | 2 | 73 | .73 | .059 | 2 | 104 | .63 | 46 | .08 | 2 | 1.01 | .04 | .11 | 2 |
| DK-105A | 3 | 73 | 2 | 41 | .1 | 30 | 22 | 419 | 2.42 | 4 | 5 | ND | 1 | 80 | .2 | 2 | 2 | 71 | .71 | .056 | 2 | 96 | .74 | 47 | .08 | 2 | 1.03 | .04 | .12 | 1 |
| DK-105B | 5 | 89 | 2 | 41 | .1 | 30 | 27 | 459 | 2.56 | 6 | 5 | ND | 1 | 92 | .2 | 2 | 2 | 75 | .80 | .057 | 2 | 109 | .78 | 52 | .09 | 3 | 1.16 | .05 | .13 | 1 |
| DK-106 | 5 | 84 | 2 | 43 | .1 | 31 | 23 | 497 | 2.50 | 2 | 5 | ND | 1 | 92 | .2 | 2 | 2 | 73 | .79 | .060 | 3 | 111 | .78 | 55 | .09 | 3 | 1.17 | .05 | .14 | 2 |
| DK-107 | 5 | 84 | 2 | 48 | .1 | 33 | 21 | 575 | 2.87 | 2 | 5 | ND | 1 | 92 | .2 | 2 | 2 | 81 | .82 | .060 | 3 | 129 | .80 | 55 | .09 | 3 | 1.18 | .05 | .14 | 2 |
| DK-108 | 6 | 78 | 4 | 46 | .1 | 32 | 18 | 508 | 2.92 | 2 | 5 | ND | 1 | 95 | .2 | 2 | 2 | 82 | .82 | .057 | 3 | 143 | .79 | 57 | .09 | 2 | 1.19 | .05 | .15 | 2 |
| DK-109 | 4 | 68 | 2 | 42 | .1 | 26 | 18 | 475 | 2.46 | 2 | 5 | ND | 1 | 85 | .2 | 2 | 2 | 72 | .70 | .054 | 3 | 89 | .64 | 48 | .08 | 2 | 1.02 | .04 | .11 | 1 |
| JDK-1 | 3 | 107 | 2 | 101 | .2 | 32 | 22 | 821 | 3.58 | 2 | 5 | ND | 1 | 75 | .2 | 2 | 2 | 67 | .68 | .068 | 2 | 73 | 1.77 | 76 | .10 | 2 | 2.21 | .03 | .08 | 1 |
| JDK-2 | 3 | 65 | 2 | 84 | .2 | 24 | 20 | 814 | 3.73 | 2 | 5 | ND | 1 | 53 | .3 | 2 | 2 | 70 | .61 | .059 | 2 | 63 | 1.92 | 51 | .12 | 2 | 2.37 | .03 | .06 | 1 |
| JDK-3 | 3 | 63 | 2 | 85 | .2 | 25 | 20 | 773 | 3.77 | 2 | 5 | ND | 1 | 54 | .3 | 2 | 2 | 71 | .64 | .057 | 2 | 73 | 1.86 | 53 | .12 | 2 | 2.29 | .03 | .06 | 1 |
| JDK-4 | 3 | 139 | 2 | 106 | .4 | 41 | 27 | 944 | 4.46 | 2 | 5 | ND | 1 | 86 | .3 | 2 | 3 | 79 | .76 | .073 | 2 | 98 | 2.01 | 88 | .12 | 2 | 2.75 | .03 | .09 | 2 |
| JDK-5 | 3 | 57 | 2 | 72 | .1 | 22 | 18 | 681 | 3.54 | 2 | 5 | ND | 1 | 43 | .2 | 2 | 2 | 68 | .65 | .055 | 2 | 61 | 1.76 | 37 | .13 | 2 | 2.12 | .02 | .05 | 2 |
| STANDARD C | 19 | 59 | 36 | 131 | 6.8 | 71 | 31 | 1052 | 3.98 | 37 | 17 | 7 | 38 | 53 | 18.4 | 15 | 22 | 56 | .47 | .093 | 38 | 56 | .92 | 181 | .07 | 34 | 1.89 | .06 | .14 | 11 |

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| | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| ✓ 6 | 2 | 75 | 8 | 86 | .1 | 21 | 19 | 844 | 3.70 | 2 | 5 | ND | 1 | 56 | .2 | 2 | 2 | 73 | .81 | .055 | 2 | 83 | 1.83 | 59 | .13 | 3 | 2.67 | .03 | .06 | 1 |
| ✓ 7 | 3 | 68 | 7 | 86 | .1 | 29 | 25 | 911 | 4.15 | 2 | 5 | ND | 1 | 52 | .2 | 2 | 2 | 85 | .93 | .060 | 2 | 95 | 1.99 | 56 | .15 | 3 | 3.00 | .03 | .06 | 1 |
| JDK-8 | 2 | 48 | 2 | 95 | .1 | 37 | 20 | 922 | 4.33 | 4 | 5 | ND | 1 | 57 | .2 | 2 | 2 | 76 | .94 | .075 | 2 | 103 | 2.05 | 54 | .15 | 3 | 3.23 | .03 | .05 | 1 |
| JDK-9 | 2 | 68 | 9 | 88 | .1 | 33 | 21 | 980 | 4.18 | 7 | 5 | ND | 1 | 58 | .2 | 2 | 2 | 83 | .88 | .059 | 2 | 103 | 2.00 | 55 | .15 | 6 | 3.08 | .03 | .06 | 1 |
| JDK-11 | ✓ 3 | 66 | 15 | 87 | .1 | 32 | 24 | 914 | 4.34 | 2 | 5 | ND | 1 | 52 | .2 | 2 | 2 | 85 | .93 | .068 | 2 | 104 | 2.03 | 51 | .15 | 3 | 3.01 | .02 | .05 | 1 |
| JDK-12 | 2 | 77 | 8 | 72 | .1 | 40 | 19 | 735 | 3.60 | 3 | 5 | ND | 1 | 61 | .2 | 2 | 2 | 87 | 1.10 | .154 | 4 | 126 | 1.80 | 50 | .11 | 4 | 2.30 | .02 | .08 | 1 |
| JDK-13 | 3 | 74 | 2 | 90 | .1 | 31 | 24 | 1007 | 4.09 | 2 | 5 | ND | 1 | 67 | .2 | 2 | 2 | 81 | .89 | .063 | 2 | 108 | 1.97 | 77 | .14 | 2 | 3.10 | .03 | .07 | 2 |
| JDK-15 | 4 | 72 | 2 | 81 | .1 | 27 | 21 | 861 | 4.09 | 5 | 5 | ND | 1 | 59 | .2 | 2 | 2 | 82 | 1.05 | .070 | 3 | 127 | 1.91 | 62 | .16 | 6 | 2.96 | .04 | .08 | 1 |
| JDK-17 | 3 | 95 | 10 | 87 | .1 | 43 | 23 | 880 | 4.53 | 4 | 5 | ND | 1 | 57 | .2 | 2 | 2 | 91 | .96 | .083 | 3 | 136 | 2.05 | 71 | .14 | 2 | 3.03 | .03 | .07 | 1 |
| JDK-18 | ✓ 3 | 72 | 14 | 78 | .1 | 36 | 22 | 798 | 3.94 | 4 | 5 | ND | 1 | 52 | .2 | 2 | 2 | 78 | .84 | .068 | 3 | 103 | 1.89 | 58 | .14 | 5 | 2.64 | .03 | .07 | 1 |
| JDK-19 | 3 | 52 | 2 | 71 | .1 | 31 | 20 | 804 | 3.79 | 7 | 5 | ND | 1 | 49 | .2 | 3 | 2 | 76 | .86 | .066 | 3 | 96 | 1.84 | 53 | .14 | 4 | 2.52 | .03 | .06 | 1 |
| JDK-20 | 4 | 57 | 18 | 72 | .1 | 37 | 19 | 817 | 4.05 | 10 | 5 | ND | 1 | 50 | .2 | 4 | 2 | 81 | .89 | .072 | 3 | 110 | 1.93 | 57 | .14 | 3 | 2.69 | .02 | .05 | 2 |
| JDK-21 | 3 | 81 | 19 | 85 | .1 | 44 | 22 | 828 | 4.62 | 7 | 5 | ND | 1 | 58 | .2 | 2 | 2 | 93 | 1.01 | .093 | 3 | 157 | 2.01 | 57 | .13 | 4 | 2.92 | .03 | .07 | 2 |
| DK-23 | 4 | 58 | 4 | 52 | .1 | 81 | 23 | 624 | 4.12 | 2 | 5 | ND | 1 | 70 | .2 | 2 | 2 | 91 | 1.04 | .109 | 3 | 286 | 2.05 | 86 | .11 | 7 | 2.04 | .03 | .11 | 3 |
| DK-24 | ✓ 6 | 86 | 22 | 73 | .1 | 89 | 26 | 789 | 4.59 | 4 | 5 | ND | 1 | 71 | .2 | 2 | 2 | 98 | 1.20 | .105 | 4 | 285 | 2.24 | 84 | .13 | 6 | 2.70 | .04 | .11 | 4 |
| DK-25 | 6 | 66 | 17 | 75 | .3 | 63 | 23 | 754 | 4.18 | 9 | 5 | ND | 1 | 64 | .2 | 3 | 7 | 89 | 1.11 | .091 | 4 | 198 | 2.12 | 72 | .14 | 4 | 2.59 | .04 | .08 | 2 |
| DK-26 | 3 | 123 | 2 | 49 | .1 | 75 | 25 | 629 | 3.56 | 2 | 5 | ND | 1 | 51 | .2 | 2 | 8 | 74 | 1.17 | .055 | 3 | 203 | 2.05 | 76 | .12 | 5 | 2.20 | .05 | .12 | 2 |
| DK-27 | 3 | 67 | 3 | 74 | .1 | 55 | 24 | 728 | 4.57 | 6 | 5 | ND | 1 | 59 | .2 | 2 | 2 | 93 | 1.01 | .103 | 3 | 208 | 1.96 | 54 | .12 | 5 | 2.39 | .03 | .07 | 1 |
| DK-28 | 4 | 72 | 3 | 71 | .1 | 60 | 24 | 694 | 5.19 | 8 | 5 | ND | 1 | 73 | .2 | 2 | 2 | 107 | 1.05 | .105 | 4 | 314 | 1.89 | 64 | .12 | 6 | 2.43 | .04 | .08 | 9 |
| DK-29 | ✓ 7 | 78 | 2 | 71 | .1 | 94 | 24 | 585 | 5.77 | 8 | 5 | ND | 1 | 103 | .2 | 2 | 2 | 119 | 1.08 | .100 | 4 | 484 | 2.06 | 62 | .11 | 5 | 2.46 | .06 | .09 | 21 |
| DK-30 | 4 | 69 | 2 | 64 | .1 | 55 | 21 | 700 | 3.93 | 6 | 5 | ND | 1 | 58 | .2 | 2 | 2 | 80 | .93 | .085 | 3 | 167 | 2.00 | 65 | .12 | 6 | 2.27 | .03 | .09 | 1 |
| DK-31 | 3 | 71 | 3 | 69 | .1 | 60 | 23 | 739 | 4.21 | 6 | 5 | ND | 1 | 64 | .2 | 2 | 2 | 86 | 1.04 | .100 | 3 | 170 | 2.04 | 60 | .12 | 5 | 2.46 | .02 | .06 | 1 |
| DK-32 | 5 | 72 | 10 | 75 | .1 | 70 | 21 | 673 | 4.13 | 4 | 5 | ND | 1 | 67 | .2 | 2 | 6 | 84 | 1.00 | .095 | 4 | 208 | 2.12 | 70 | .12 | 2 | 2.55 | .03 | .08 | 1 |
| DK-33 | 3 | 93 | 9 | 70 | .1 | 75 | 26 | 680 | 4.39 | 3 | 5 | ND | 1 | 79 | .2 | 2 | 2 | 87 | 1.22 | .152 | 4 | 221 | 2.12 | 70 | .10 | 2 | 2.44 | .02 | .08 | 1 |
| DK-34 | ✓ 6 | 77 | 4 | 73 | .1 | 53 | 21 | 724 | 4.18 | 10 | 5 | ND | 1 | 57 | .2 | 2 | 2 | 81 | 1.06 | .082 | 4 | 171 | 1.85 | 73 | .13 | 2 | 2.30 | .02 | .08 | 3 |
| DK-35 | 8 | 62 | 4 | 58 | .1 | 42 | 20 | 643 | 3.86 | 2 | 5 | ND | 1 | 47 | .2 | 2 | 3 | 80 | 1.01 | .067 | 4 | 137 | 1.72 | 66 | .14 | 3 | 2.05 | .03 | .08 | 3 |
| DK-36 | 10 | 59 | 2 | 52 | .2 | 34 | 18 | 578 | 3.37 | 4 | 5 | ND | 1 | 44 | .2 | 2 | 6 | 70 | .80 | .065 | 5 | 113 | 1.55 | 70 | .12 | 4 | 1.76 | .03 | .08 | 1 |
| DK-37 | 9 | 96 | 6 | 66 | .1 | 53 | 21 | 693 | 4.21 | 2 | 5 | ND | 1 | 58 | .2 | 3 | 2 | 88 | 1.00 | .081 | 5 | 165 | 1.91 | 73 | .13 | 3 | 2.20 | .03 | .10 | 1 |
| DK-38 | 8 | 74 | 5 | 60 | .1 | 45 | 22 | 640 | 3.84 | 6 | 5 | ND | 1 | 57 | .2 | 2 | 5 | 83 | 1.07 | .079 | 5 | 133 | 1.71 | 59 | .14 | 4 | 2.02 | .03 | .08 | 1 |
| DK-39 | ✓ 9 | 153 | 2 | 74 | .3 | 76 | 28 | 800 | 4.61 | 8 | 5 | ND | 1 | 64 | .2 | 3 | 3 | 96 | 1.16 | .085 | 5 | 197 | 2.05 | 90 | .12 | 3 | 2.45 | .03 | .09 | 5 |
| DK-40 | ✓ 7 | 68 | 6 | 57 | .1 | 34 | 17 | 601 | 3.57 | 6 | 5 | ND | 1 | 48 | .2 | 2 | 4 | 76 | .90 | .068 | 5 | 116 | 1.60 | 68 | .13 | 2 | 1.88 | .03 | .09 | 1 |
| JO-1 | 4 | 60 | 11 | 75 | .1 | 54 | 18 | 547 | 3.06 | 7 | 5 | ND | 1 | 68 | .2 | 2 | 2 | 78 | 1.44 | .078 | 3 | 267 | 1.72 | 73 | .09 | 2 | 1.88 | .05 | .27 | 1 |
| JO-2 | 4 | 203 | 6 | 119 | .5 | 56 | 28 | 1083 | 3.96 | 11 | 5 | ND | 1 | 66 | .2 | 3 | 2 | 98 | 1.58 | .097 | 3 | 213 | 1.39 | 66 | .08 | 5 | 1.86 | .03 | .14 | 2 |
| JO-3 | 6 | 158 | 4 | 101 | .1 | 60 | 25 | 1077 | 3.84 | 8 | 7 | ND | 1 | 64 | .2 | 2 | 2 | 109 | 1.42 | .088 | 3 | 194 | 1.33 | 79 | .09 | 5 | 1.69 | .04 | .19 | 1 |
| JO-4 | 6 | 109 | 5 | 78 | .4 | 49 | 22 | 870 | 2.77 | 9 | 5 | ND | 1 | 53 | .2 | 2 | 8 | 124 | 1.38 | .118 | 4 | 205 | 1.33 | 72 | .06 | 5 | 1.86 | .02 | .07 | 1 |
| JO-5 | 3 | 68 | 2 | 38 | .1 | 22 | 10 | 541 | 2.48 | 10 | 5 | ND | 1 | 81 | .2 | 2 | 2 | 92 | 1.07 | .067 | 5 | 103 | .71 | 43 | .08 | 6 | 1.02 | .03 | .10 | 1 |
| STANDARD C | 18 | 62 | 37 | 132 | 7.7 | 73 | 31 | 1044 | 4.01 | 42 | 18 | 8 | 35 | 49 | 18.4 | 15 | 20 | 55 | .51 | .097 | 36 | 59 | .90 | 179 | .08 | 37 | 1.91 | .06 | .15 | 11 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Tl % | B ppm | Al % | Na % | K % | W ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| JO-185 | 5 | 91 | 3 | 37 | .1 | 3 | 7 | 422 | 2.43 | 3 | 5 | ND | 1 | 54 | .2 | 2 | 2 | 73 | .42 | .070 | 5 | 48 | .39 | 74 | .06 | 2 | .74 | .04 | .09 | 1 |
| JO-186 | 6 | 74 | 5 | 30 | .1 | 4 | 6 | 363 | 2.34 | 2 | 5 | ND | 1 | 64 | .2 | 2 | 2 | 74 | .48 | .072 | 6 | 60 | .35 | 71 | .07 | 2 | .75 | .05 | .11 | 1 |
| JO-187 | 8 | 101 | 3 | 43 | .1 | 5 | 8 | 436 | 2.94 | 2 | 5 | ND | 2 | 71 | .2 | 2 | 2 | 91 | .53 | .085 | 6 | 80 | .44 | 95 | .07 | 2 | .93 | .06 | .13 | 2 |
| JO-188 | 24 | 293 | 10 | 66 | .7 | 5 | 8 | 1049 | 2.36 | 12 | 35 | ND | 1 | 106 | .2 | 2 | 2 | 58 | 1.24 | .197 | 23 | 56 | .49 | 143 | .03 | 7 | 1.80 | .03 | .07 | 1 |
| JO-189 | 17 | 266 | 6 | 97 | .3 | 7 | 10 | 2809 | 2.87 | 10 | 75 | ND | 1 | 110 | .3 | 2 | 2 | 68 | 1.36 | .161 | 12 | 99 | .31 | 191 | .05 | 8 | 1.35 | .04 | .10 | 1 |
| JO-190 | 25 | 176 | 11 | 68 | .3 | 11 | 10 | 1716 | 3.30 | 7 | 28 | ND | 1 | 84 | .3 | 2 | 2 | 117 | .91 | .124 | 10 | 79 | .39 | 137 | .05 | 4 | 1.58 | .03 | .06 | 1 |
| JO-191 | 8 | 141 | 6 | 62 | .2 | 7 | 17 | 499 | 5.45 | 3 | 5 | ND | 3 | 155 | .2 | 2 | 2 | 169 | .96 | .189 | 11 | 87 | 1.23 | 152 | .25 | 2 | 1.65 | .07 | .17 | 1 |
| JO-192 | 7 | 166 | 6 | 89 | .3 | 14 | 12 | 778 | 5.41 | 5 | 5 | ND | 1 | 100 | .2 | 2 | 2 | 200 | 1.13 | .139 | 14 | 86 | .67 | 103 | .09 | 7 | 1.48 | .03 | .06 | 1 |
| JO-193 | 7 | 87 | 2 | 43 | .1 | 18 | 9 | 560 | 3.55 | 4 | 5 | ND | 1 | 37 | .2 | 2 | 2 | 131 | .56 | .124 | 10 | 90 | .63 | 53 | .07 | 3 | .86 | .04 | .05 | 2 |
| JO-194 | 7 | 102 | 2 | 45 | .1 | 21 | 10 | 607 | 4.69 | 2 | 5 | ND | 1 | 54 | .2 | 2 | 2 | 194 | .66 | .137 | 9 | 110 | .58 | 70 | .09 | 4 | 1.01 | .04 | .06 | 2 |
| JO-195 | 6 | 181 | 2 | 56 | .2 | 19 | 12 | 737 | 5.12 | 2 | 5 | ND | 1 | 74 | .5 | 2 | 2 | 195 | .91 | .159 | 14 | 96 | .68 | 110 | .08 | 4 | 1.39 | .03 | .06 | 1 |
| JO-196 | 7 | 207 | 4 | 64 | .2 | 21 | 11 | 640 | 4.89 | 4 | 5 | ND | 1 | 78 | .4 | 2 | 2 | 193 | .94 | .168 | 16 | 113 | .69 | 120 | .07 | 4 | 1.43 | .03 | .08 | 1 |
| JO-197 | 3 | 245 | 7 | 53 | .6 | 21 | 11 | 575 | 3.21 | 4 | 105 | ND | 1 | 64 | .2 | 2 | 2 | 108 | .72 | .139 | 27 | 80 | .77 | 104 | .08 | 2 | 1.36 | .03 | .07 | 1 |
| JO-198 | 7 | 106 | 2 | 44 | .1 | 24 | 10 | 544 | 4.46 | 2 | 5 | ND | 2 | 52 | .2 | 2 | 2 | 196 | .63 | .116 | 8 | 146 | .67 | 73 | .11 | 5 | 1.01 | .06 | .09 | 1 |
| JO-199 | 6 | 93 | 3 | 46 | .1 | 30 | 11 | 521 | 5.12 | 2 | 5 | ND | 2 | 42 | .2 | 2 | 2 | 245 | .57 | .113 | 7 | 148 | .68 | 58 | .11 | 5 | .91 | .04 | .06 | 2 |
| JO-200 | 6 | 107 | 2 | 45 | .1 | 25 | 10 | 505 | 4.41 | 2 | 5 | ND | 1 | 53 | .2 | 2 | 2 | 189 | .64 | .125 | 8 | 128 | .69 | 77 | .10 | 5 | 1.02 | .05 | .08 | 1 |
| JO-201 | 6 | 114 | 2 | 47 | .1 | 26 | 11 | 496 | 5.26 | 2 | 5 | ND | 1 | 51 | .2 | 2 | 2 | 234 | .65 | .132 | 9 | 136 | .67 | 71 | .10 | 5 | 1.02 | .05 | .07 | 1 |
| JO-203 | 7 | 78 | 2 | 31 | .1 | 16 | 8 | 352 | 2.96 | 2 | 5 | ND | 1 | 53 | .2 | 2 | 2 | 121 | .56 | .092 | 7 | 108 | .50 | 68 | .09 | 4 | .84 | .07 | .10 | 1 |
| JRG-1 | 4 | 61 | 7 | 98 | .3 | 33 | 20 | 941 | 4.14 | 19 | 5 | ND | 1 | 35 | .5 | 2 | 2 | 79 | .68 | .064 | 3 | 105 | 2.03 | 54 | .11 | 2 | 3.06 | .03 | .06 | 1 |
| JRG-2 | 5 | 45 | 2 | 89 | .1 | 36 | 22 | 1066 | 4.40 | 8 | 5 | ND | 1 | 38 | .3 | 2 | 2 | 86 | .71 | .044 | 2 | 115 | 2.36 | 41 | .21 | 2 | 3.03 | .04 | .06 | 1 |
| JRG-3 | 5 | 42 | 2 | 98 | .2 | 29 | 22 | 981 | 4.80 | 15 | 5 | ND | 1 | 59 | .6 | 2 | 2 | 87 | .75 | .048 | 2 | 102 | 2.42 | 40 | .23 | 2 | 3.24 | .05 | .06 | 1 |
| JRG-4 | 3 | 36 | 2 | 87 | .1 | 28 | 22 | 1050 | 4.52 | 11 | 5 | ND | 1 | 49 | .5 | 2 | 2 | 81 | .65 | .047 | 2 | 80 | 2.37 | 36 | .22 | 2 | 3.01 | .04 | .04 | 1 |
| JRG-5 | 4 | 42 | 2 | 88 | .1 | 27 | 21 | 1074 | 4.88 | 13 | 5 | ND | 1 | 40 | .3 | 2 | 2 | 78 | .49 | .049 | 2 | 85 | 2.39 | 38 | .18 | 2 | 3.07 | .03 | .05 | 1 |
| JRG-6 | 3 | 64 | 2 | 118 | .1 | 26 | 25 | 930 | 4.81 | 16 | 5 | ND | 1 | 39 | .4 | 2 | 2 | 77 | .44 | .052 | 2 | 70 | 2.25 | 39 | .16 | 2 | 2.88 | .02 | .04 | 1 |
| JRG-7 | 5 | 70 | 2 | 133 | .1 | 30 | 24 | 794 | 4.89 | 16 | 5 | ND | 1 | 49 | .4 | 2 | 2 | 79 | .50 | .052 | 2 | 99 | 2.31 | 45 | .15 | 2 | 3.09 | .03 | .05 | 1 |
| JRG-8 | 4 | 55 | 4 | 135 | .1 | 32 | 26 | 1021 | 4.75 | 13 | 5 | ND | 1 | 38 | .6 | 2 | 2 | 85 | .51 | .052 | 2 | 95 | 2.45 | 49 | .18 | 2 | 3.05 | .04 | .06 | 1 |
| JRG-9 | 3 | 79 | 2 | 113 | .1 | 33 | 22 | 801 | 4.59 | 5 | 5 | ND | 1 | 43 | .2 | 2 | 3 | 84 | .55 | .054 | 2 | 89 | 2.18 | 59 | .14 | 2 | 3.14 | .02 | .06 | 1 |
| JRG-10 | 5 | 74 | 6 | 100 | .1 | 14 | 19 | 772 | 3.74 | 2 | 5 | ND | 1 | 42 | .2 | 2 | 2 | 80 | .60 | .050 | 2 | 55 | 1.66 | 89 | .15 | 2 | 2.30 | .05 | .14 | 1 |
| JRG-11 | 5 | 77 | 2 | 98 | .1 | 27 | 21 | 981 | 4.73 | 6 | 5 | ND | 1 | 44 | .2 | 2 | 2 | 93 | .66 | .050 | 2 | 92 | 2.25 | 67 | .16 | 2 | 3.00 | .05 | .10 | 1 |
| JRG-12 | 4 | 61 | 2 | 84 | .3 | 30 | 20 | 956 | 4.68 | 5 | 5 | ND | 1 | 48 | .3 | 2 | 2 | 96 | .77 | .055 | 2 | 97 | 2.32 | 66 | .20 | 2 | 3.14 | .06 | .09 | 1 |
| JRG-13 | 4 | 58 | 2 | 84 | .2 | 30 | 22 | 939 | 4.82 | 6 | 5 | ND | 1 | 55 | .2 | 3 | 2 | 104 | .93 | .058 | 2 | 101 | 2.37 | 55 | .22 | 2 | 3.26 | .07 | .08 | 1 |
| JRG-14 | 3 | 81 | 2 | 96 | .2 | 31 | 23 | 1105 | 5.18 | 13 | 5 | ND | 1 | 56 | .4 | 3 | 3 | 109 | .83 | .056 | 2 | 92 | 2.34 | 89 | .18 | 2 | 3.42 | .06 | .13 | 1 |
| JRG-15 | 3 | 74 | 2 | 112 | .1 | 30 | 27 | 1485 | 4.97 | 22 | 5 | ND | 1 | 62 | .8 | 2 | 2 | 93 | .87 | .077 | 3 | 96 | 2.23 | 50 | .12 | 2 | 3.71 | .02 | .03 | 1 |
| JRG-16 | 7 | 99 | 4 | 176 | .1 | 31 | 28 | 910 | 4.34 | 9 | 5 | ND | 1 | 51 | .6 | 2 | 3 | 92 | .72 | .068 | 2 | 122 | 1.93 | 109 | .08 | 2 | 3.01 | .05 | .17 | 1 |
| JRG-17 | 7 | 64 | 2 | 120 | .1 | 35 | 34 | 1922 | 4.76 | 13 | 5 | ND | 1 | 40 | .6 | 2 | 3 | 101 | .59 | .058 | 2 | 131 | 2.09 | 93 | .11 | 2 | 2.90 | .05 | .08 | 1 |
| JRG-18 | 4 | 44 | 2 | 88 | .1 | 27 | 23 | 1139 | 4.08 | 7 | 5 | ND | 1 | 31 | .2 | 2 | 2 | 91 | .52 | .050 | 2 | 84 | 1.91 | 69 | .11 | 2 | 2.44 | .05 | .07 | 1 |
| STANDARD C | 19 | 59 | 39 | 132 | 7.1 | 72 | 31 | 1052 | 3.97 | 37 | 20 | 7 | 39 | 52 | 18.3 | 14 | 21 | 56 | .47 | .096 | 39 | 57 | .93 | 182 | .07 | 33 | 1.89 | .06 | .14 | 11 |

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| JRG-19 | 5 | 36 | 8 | 96 | .2 | 28 | 25 | 1457 | 4.20 | 4 | 5 | ND | 1 | 35 | .2 | 2 | 2 | 80 | .64 | .048 | 2 | 89 | 1.97 | 66 | .13 | 3 | 2.57 | .05 | .08 | 1 |
| JRG-20 | 3 | 70 | 2 | 102 | .2 | 26 | 25 | 1184 | 5.65 | 5 | 5 | ND | 1 | 34 | .4 | 2 | 2 | 96 | .63 | .050 | 2 | 83 | 2.45 | 59 | .09 | 4 | 3.54 | .04 | .07 | 1 |
| JRG-21 | 3 | 77 | 6 | 83 | .3 | 30 | 23 | 916 | 4.57 | 2 | 5 | ND | 1 | 53 | .2 | 2 | 2 | 91 | .89 | .060 | 2 | 96 | 2.42 | 44 | .16 | 3 | 2.95 | .04 | .06 | 1 |
| JRG-22 | 3 | 78 | 2 | 82 | .2 | 30 | 24 | 923 | 4.89 | 6 | 5 | ND | 1 | 47 | .4 | 2 | 2 | 96 | .86 | .062 | 2 | 92 | 2.52 | 43 | .15 | 4 | 3.17 | .04 | .06 | 2 |
| JRG-23 | ✓ 3 | 62 ✓ | 4 | 86 | .2 | 31 | 23 | 988 | 5.17 | 3 | 5 | ND | 1 | 39 | .2 | 2 | 2 | 96 | .66 | .056 | 2 | 93 | 2.62 | 42 | .12 | 3 | 3.40 | .04 | .06 | 1 |
| JRG-24 | 3 | 69 | 2 | 83 | .1 | 31 | 23 | 964 | 4.96 | 8 | 5 | ND | 1 | 48 | .3 | 3 | 2 | 103 | .82 | .063 | 2 | 96 | 2.58 | 52 | .14 | 4 | 3.30 | .04 | .07 | 1 |
| JRG-25 | 4 | 62 | 4 | 84 | .3 | 38 | 23 | 969 | 5.10 | 4 | 5 | ND | 1 | 53 | .2 | 2 | 2 | 102 | .76 | .060 | 2 | 119 | 2.75 | 54 | .14 | 3 | 3.43 | .05 | .09 | 1 |
| JRG-26 | 3 | 71 | 7 | 77 | .1 | 33 | 24 | 1105 | 5.07 | 6 | 5 | ND | 1 | 44 | .3 | 2 | 2 | 104 | .63 | .052 | 2 | 92 | 2.48 | 50 | .12 | 3 | 3.37 | .04 | .05 | 1 |
| JRG-27 | 4 | 51 | 6 | 86 | .1 | 34 | 24 | 1048 | 4.92 | 2 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 97 | .67 | .057 | 2 | 104 | 2.60 | 48 | .14 | 2 | 3.24 | .04 | .06 | 1 |
| JRG-28 | ✓ 2 | 72 ✓ | 2 | 88 | .1 | 38 | 24 | 865 | 5.07 | 8 | 5 | ND | 1 | 45 | .3 | 3 | 2 | 103 | .63 | .057 | 3 | 105 | 2.68 | 43 | .12 | 4 | 3.30 | .03 | .05 | 1 |
| JRG-29 | 2 | 55 | 2 | 83 | .1 | 36 | 24 | 935 | 4.85 | 6 | 5 | ND | 1 | 47 | .4 | 2 | 2 | 99 | .67 | .060 | 2 | 97 | 2.63 | 39 | .13 | 4 | 3.19 | .03 | .05 | 1 |
| JRG-30 | 2 | 58 | 5 | 85 | .3 | 36 | 23 | 971 | 4.93 | 3 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 92 | .66 | .056 | 2 | 101 | 2.60 | 41 | .13 | 2 | 3.23 | .03 | .05 | 1 |
| JRG-31 | 2 | 53 | 2 | 83 | .1 | 34 | 24 | 1001 | 4.88 | 5 | 5 | ND | 1 | 43 | .4 | 2 | 2 | 98 | .64 | .062 | 2 | 86 | 2.61 | 39 | .13 | 3 | 3.15 | .03 | .04 | 1 |
| JRG-32 | 2 | 51 | 2 | 82 | .1 | 34 | 23 | 960 | 4.86 | 2 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 93 | .66 | .059 | 2 | 89 | 2.59 | 40 | .13 | 2 | 3.13 | .03 | .05 | 1 |
| JRG-33 | ✓ 3 | 59 ✓ | 5 | 93 | .1 | 36 | 24 | 1022 | 5.03 | 9 | 5 | ND | 1 | 52 | .2 | 3 | 2 | 103 | .74 | .059 | 2 | 104 | 2.65 | 56 | .14 | 3 | 3.39 | .05 | .08 | 1 |
| JRG-34 | 2 | 60 | 4 | 86 | .1 | 36 | 24 | 993 | 5.00 | 5 | 5 | ND | 1 | 48 | .6 | 2 | 2 | 98 | .68 | .056 | 2 | 98 | 2.62 | 45 | .14 | 3 | 3.28 | .03 | .05 | 1 |
| JRG-35 | 2 | 59 | 2 | 88 | .1 | 36 | 24 | 999 | 5.06 | 5 | 5 | ND | 1 | 48 | .2 | 2 | 2 | 98 | .69 | .054 | 2 | 104 | 2.66 | 48 | .14 | 2 | 3.35 | .03 | .05 | 1 |
| JRG-36 | 3 | 44 | 6 | 69 | .3 | 27 | 21 | 801 | 4.64 | 3 | 5 | ND | 1 | 40 | .2 | 2 | 2 | 88 | .76 | .032 | 2 | 94 | 2.54 | 30 | .22 | 3 | 3.30 | .04 | .04 | 1 |
| JRG-37 | 3 | 58 | 2 | 74 | .1 | 27 | 22 | 819 | 4.72 | 11 | 5 | ND | 1 | 43 | .5 | 2 | 2 | 99 | .84 | .036 | 2 | 96 | 2.47 | 31 | .22 | 2 | 3.30 | .04 | .04 | 1 |
| JRG-38 | ✓ 3 | 39 ✓ | 4 | 73 | .2 | 27 | 21 | 812 | 4.56 | 2 | 5 | ND | 1 | 39 | .2 | 2 | 2 | 83 | .75 | .034 | 2 | 88 | 2.45 | 28 | .21 | 2 | 3.15 | .03 | .04 | 1 |
| JRG-39 | 2 | 48 | 4 | 69 | .2 | 29 | 21 | 812 | 4.71 | 2 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 94 | .65 | .028 | 2 | 92 | 2.56 | 35 | .18 | 2 | 3.27 | .03 | .03 | 1 |
| JRG-40 | 2 | 49 | 7 | 80 | .1 | 29 | 22 | 918 | 4.64 | 2 | 5 | ND | 1 | 43 | .4 | 2 | 2 | 89 | .68 | .049 | 2 | 84 | 2.43 | 36 | .16 | 2 | 3.04 | .03 | .04 | 1 |
| JRG-41 | 2 | 60 | 6 | 86 | .1 | 33 | 22 | 940 | 5.05 | 4 | 5 | ND | 1 | 44 | .3 | 2 | 2 | 94 | .57 | .050 | 2 | 91 | 2.62 | 43 | .14 | 2 | 3.30 | .02 | .04 | 1 |
| JRG-42 | 2 | 52 | 4 | 80 | .1 | 32 | 22 | 931 | 4.89 | 3 | 5 | ND | 1 | 43 | .5 | 2 | 2 | 96 | .61 | .050 | 2 | 98 | 2.58 | 43 | .15 | 2 | 3.25 | .03 | .05 | 1 |
| JRG-43 | ✓ 3 | 53 ✓ | 2 | 96 | .1 | 29 | 18 | 786 | 4.50 | 6 | 5 | ND | 1 | 154 | .5 | 2 | 2 | 63 | 2.68 | .047 | 2 | 80 | 1.92 | 54 | .16 | 2 | 2.81 | .03 | .04 | 1 |
| JRG-44 | 3 | 377 | 4 | 81 | 1.0 | 30 | 22 | 908 | 4.70 | 7 | 5 | ND | 1 | 45 | .4 | 2 | 2 | 94 | .75 | .056 | 2 | 94 | 2.48 | 38 | .17 | 2 | 3.13 | .04 | .05 | 1 |
| JRG-45 | 2 | 75 | 2 | 77 | .2 | 29 | 21 | 909 | 4.67 | 2 | 5 | ND | 1 | 41 | .2 | 2 | 2 | 89 | .64 | .050 | 2 | 86 | 2.46 | 36 | .16 | 2 | 3.07 | .03 | .04 | 1 |
| JRG-46 | 2 | 67 | 2 | 79 | .1 | 31 | 22 | 948 | 4.80 | 6 | 5 | ND | 1 | 46 | .6 | 3 | 2 | 97 | .71 | .054 | 2 | 94 | 2.53 | 41 | .17 | 3 | 3.20 | .04 | .05 | 1 |
| JRG-47 | 2 | 59 | 5 | 78 | .2 | 32 | 22 | 895 | 4.84 | 7 | 5 | ND | 1 | 44 | .3 | 2 | 2 | 90 | .62 | .050 | 2 | 93 | 2.52 | 39 | .16 | 2 | 3.14 | .03 | .04 | 1 |
| JRG-48 | ✓ 3 | 53 ✓ | 4 | 77 | .1 | 30 | 21 | 955 | 4.74 | 2 | 5 | ND | 1 | 49 | .3 | 2 | 2 | 91 | .66 | .052 | 2 | 93 | 2.48 | 43 | .16 | 3 | 3.17 | .04 | .05 | 1 |
| JRG-49 | 4 | 69 | 2 | 99 | .2 | 35 | 22 | 1361 | 5.26 | 16 | 5 | ND | 1 | 25 | .2 | 2 | 2 | 118 | .42 | .070 | 4 | 115 | 2.30 | 56 | .12 | 2 | 3.68 | .05 | .07 | 1 |
| JRG-50 | 6 | 56 | 2 | 127 | .1 | 26 | 26 | 2313 | 5.68 | 21 | 5 | ND | 1 | 41 | 1.1 | 2 | 2 | 109 | .70 | .049 | 2 | 92 | 2.48 | 33 | .17 | 3 | 3.72 | .05 | .02 | 1 |
| JRG-51 | 10 | 95 | 15 | 105 | .1 | 62 | 14 | 939 | 2.87 | 8 | 5 | ND | 2 | 27 | .2 | 2 | 2 | 46 | .38 | .057 | 8 | 200 | 1.40 | 88 | .04 | 3 | 2.05 | .06 | .14 | 1 |
| JRG-52 | 3 | 85 | 5 | 104 | .1 | 28 | 22 | 1009 | 5.68 | 11 | 5 | ND | 1 | 37 | .7 | 3 | 2 | 94 | .69 | .043 | 3 | 87 | 2.53 | 45 | .13 | 3 | 3.83 | .04 | .06 | 1 |
| JRG-53 | ✓ 3 | 76 ✓ | 4 | 99 | .1 | 27 | 20 | 949 | 5.51 | 7 | 5 | ND | 1 | 36 | .6 | 2 | 3 | 85 | .68 | .041 | 3 | 80 | 2.47 | 41 | .13 | 2 | 3.65 | .04 | .05 | 1 |
| JRG-54 | 3 | 77 | 2 | 94 | .1 | 30 | 21 | 991 | 5.46 | 11 | 5 | ND | 1 | 36 | .6 | 3 | 2 | 90 | .66 | .047 | 3 | 83 | 2.42 | 46 | .12 | 2 | 3.52 | .04 | .06 | 1 |
| STANDARD C | 18 | 58 | 37 | 131 | 6.7 | 70 | 31 | 1052 | 3.95 | 38 | 18 | 7 | 39 | 53 | 18.7 | 17 | 21 | 57 | .47 | .095 | 39 | 55 | .92 | 181 | .07 | 34 | 1.89 | .06 | .14 | 11 |

Golden Rule Resources Ltd.

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| SAMPLE# | Mo ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | U ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| JRG-55 | 3 | 67 | 2 | 90 | .2 | 29 | 19 | 944 | 5.28 | 2 | 5 | ND | 1 | 28 | .2 | 2 | 2 | 83 | .54 | .044 | 2 | 79 | 2.51 | 31 | .12 | 2 | 3.31 | .03 | .05 | 1 |
| JRG-56 | 3 | 216 | 8 | 118 | .4 | 37 | 25 | 1208 | 5.49 | 4 | 5 | ND | 1 | 85 | .2 | 2 | 4 | 70 | .65 | .060 | 2 | 68 | 2.25 | 55 | .14 | 2 | 3.15 | .02 | .06 | 1 |
| JRG-57 | 3 | 106 | 2 | 93 | .2 | 33 | 21 | 991 | 5.21 | .3 | 5 | ND | 1 | 46 | .2 | 2 | 2 | 77 | .54 | .051 | 2 | 72 | 2.38 | 38 | .13 | 2 | 3.13 | .02 | .05 | 1 |
| JRG-58 | 3 | 108 | 4 | 97 | .2 | 35 | 21 | 988 | 5.20 | .3 | 5 | ND | 1 | 52 | .2 | 2 | 3 | 76 | .55 | .054 | 2 | 82 | 2.33 | 46 | .14 | 2 | 3.10 | .02 | .05 | 1 |
| JRG-59 | 3 | 108✓ | 7 | 92 | .3 | 38 | 20 | 988 | 5.09 | 2 | 5 | ND | 1 | 51 | .2 | 2 | 2 | 75 | .54 | .055 | 2 | 81 | 2.30 | 45 | .13 | 2 | 3.06 | .02 | .05 | 1 |
| JRG-60 | 3 | 95 | 2 | 88 | .2 | 33 | 20 | 939 | 5.02 | 3 | 5 | ND | 1 | 47 | .2 | 2 | 3 | 79 | .66 | .054 | 2 | 78 | 2.29 | 52 | .14 | 3 | 3.07 | .03 | .05 | 1 |
| JRG-61 | 2 | 95 | 2 | 85 | .2 | 30 | 19 | 912 | 4.85 | 2 | 5 | ND | 1 | 50 | .2 | 2 | 2 | 77 | .67 | .056 | 2 | 66 | 2.20 | 49 | .12 | 2 | 2.89 | .02 | .04 | 1 |
| JRG-62 | 2 | 73 | 4 | 93 | .1 | 23 | 22 | 816 | 5.33 | 2 | 5 | ND | 1 | 30 | .2 | 2 | 2 | 87 | .56 | .067 | 2 | 55 | 2.40 | 32 | .11 | 2 | 3.17 | .02 | .04 | 1 |
| JRG-63 | 3 | 78 | 4 | 85 | .3 | 26 | 18 | 850 | 4.79 | 2 | 5 | ND | 1 | 41 | .2 | 2 | 2 | 77 | .65 | .056 | 2 | 63 | 2.21 | 44 | .13 | 2 | 2.87 | .03 | .05 | 1 |
| JRG-64 | 2 | 137✓ | 18 | 271 | .4 | 33 | 20 | 1084 | 4.34 | 2 | 5 | ND | 1 | 84 | .7 | 2 | 2 | 108 | .95 | .050 | 2 | 82 | 2.05 | 158 | .14 | 2 | 3.22 | .08 | .29 | 1 |
| JRG-65 | 2 | 87 | 2 | 92 | .2 | 26 | 19 | 877 | 4.86 | 2 | 5 | ND | 1 | 42 | .2 | 2 | 2 | 81 | .64 | .056 | 2 | 60 | 2.26 | 53 | .13 | 2 | 2.95 | .03 | .05 | 1 |
| JRG-66 | 3 | 76 | 2 | 92 | .3 | 24 | 18 | 846 | 4.84 | 2 | 5 | ND | 1 | 44 | .2 | 2 | 2 | 84 | .76 | .057 | 2 | 71 | 2.28 | 48 | .15 | 2 | 3.05 | .04 | .07 | 1 |
| JRG-67 | 2 | 100 | 5 | 91 | .3 | 28 | 20 | 902 | 4.97 | 2 | 5 | ND | 1 | 47 | .2 | 2 | 2 | 82 | .64 | .059 | 2 | 64 | 2.25 | 56 | .13 | 2 | 3.00 | .03 | .05 | 1 |
| JRG-68 | 3 | 74 | 2 | 84 | .3 | 24 | 19 | 816 | 4.86 | 2 | 5 | ND | 1 | 43 | .2 | 2 | 2 | 87 | .73 | .056 | 2 | 70 | 2.31 | 39 | .16 | 2 | 3.04 | .04 | .05 | 1 |
| JRG-69 | 3 | 86✓ | 2 | 46 | .3 | 15 | 18 | 445 | 3.51 | 2 | 5 | ND | 1 | 62 | .2 | 2 | 2 | 85 | 1.23 | .041 | 2 | 48 | 1.64 | 37 | .15 | 2 | 2.62 | .04 | .05 | 2 |
| JRG-70 | 3 | 71 | 2 | 81 | .1 | 23 | 18 | 764 | 4.68 | 2 | 5 | ND | 1 | 46 | .2 | 2 | 2 | 88 | .81 | .055 | 2 | 70 | 2.24 | 39 | .16 | 2 | 2.99 | .04 | .06 | 1 |
| JRG-71 | 2 | 75 | 2 | 82 | .2 | 23 | 19 | 775 | 4.69 | 2 | 5 | ND | 1 | 41 | .2 | 2 | 2 | 85 | .71 | .054 | 2 | 59 | 2.23 | 35 | .14 | 3 | 2.93 | .03 | .04 | 1 |
| JRG-72 | 3 | 93 | 2 | 82 | .2 | 26 | 20 | 802 | 4.69 | 2 | 5 | ND | 1 | 50 | .2 | 2 | 2 | 86 | .71 | .053 | 2 | 70 | 2.15 | 54 | .14 | 3 | 2.95 | .04 | .06 | 1 |
| JRG-73 | 2 | 81 | 2 | 78 | .2 | 24 | 18 | 775 | 4.58 | 2 | 5 | ND | 1 | 41 | .2 | 2 | 2 | 84 | .68 | .054 | 2 | 64 | 2.19 | 45 | .13 | 2 | 2.88 | .03 | .05 | 1 |
| JRG-74 | 2 | 69✓ | 4 | 80 | .2 | 23 | 18 | 746 | 4.59 | 2 | 5 | ND | 1 | 43 | .2 | 2 | 2 | 87 | .75 | .053 | 2 | 63 | 2.20 | 39 | .15 | 2 | 2.89 | .04 | .05 | 1 |
| JRG-75 | 3 | 81 | 7 | 80 | .3 | 28 | 19 | 772 | 4.66 | 2 | 5 | ND | 1 | 43 | .2 | 2 | 2 | 87 | .71 | .053 | 2 | 69 | 2.21 | 46 | .14 | 2 | 2.91 | .03 | .05 | 1 |
| JRG-76 | 2 | 63 | 2 | 70 | .1 | 21 | 17 | 678 | 4.28 | 2 | 5 | ND | 1 | 41 | .2 | 2 | 2 | 82 | .75 | .051 | 2 | 52 | 2.11 | 31 | .15 | 2 | 2.69 | .03 | .04 | 1 |
| JRG-77 | 3 | 77 | 4 | 81 | .2 | 25 | 18 | 771 | 4.52 | 2 | 5 | ND | 1 | 47 | .2 | 2 | 2 | 83 | .72 | .053 | 2 | 67 | 2.17 | 55 | .14 | 2 | 2.91 | .03 | .05 | 1 |
| JRG-78 | 3 | 94 | 4 | 84 | .2 | 26 | 21 | 799 | 4.65 | 2 | 5 | ND | 1 | 53 | .2 | 2 | 3 | 89 | .76 | .053 | 2 | 71 | 2.13 | 69 | .14 | 4 | 2.96 | .04 | .06 | 1 |
| JRG-79 | 2 | 73✓ | 4 | 75 | .1 | 23 | 18 | 721 | 4.41 | 2 | 5 | ND | 1 | 45 | .2 | 2 | 2 | 87 | .73 | .050 | 2 | 62 | 2.14 | 49 | .15 | 2 | 2.82 | .03 | .05 | 1 |
| JRG-80 | 3 | 67 | 7 | 78 | .2 | 21 | 17 | 736 | 4.39 | 2 | 5 | ND | 1 | 44 | .2 | 2 | 2 | 87 | .74 | .053 | 2 | 68 | 2.13 | 47 | .15 | 2 | 2.86 | .05 | .06 | 1 |
| JRG-81 | 5 | 32 | 2 | 46 | .2 | 12 | 9 | 381 | 2.24 | 2 | 5 | ND | 1 | 47 | .2 | 2 | 2 | 43 | .41 | .038 | 3 | 70 | .98 | 82 | .08 | 3 | 1.29 | .03 | .04 | 1 |
| JRG-82 | 11 | 22 | 2 | 55 | .1 | 9 | 7 | 379 | 1.97 | 2 | 5 | ND | 1 | 78 | .2 | 2 | 2 | 40 | .40 | .044 | 5 | 131 | .54 | 137 | .06 | 4 | 1.03 | .06 | .08 | 1 |
| JRG-83 | 17 | 24 | 2 | 60 | .1 | 10 | 7 | 414 | 2.04 | 2 | 5 | ND | 1 | 88 | .2 | 2 | 2 | 41 | .46 | .047 | 5 | 194 | .55 | 153 | .07 | 3 | 1.13 | .08 | .10 | 1 |
| JRG-84 | 19 | 20✓ | 2 | 58 | .1 | 10 | 6 | 351 | 2.02 | 2 | 5 | ND | 1 | 107 | .2 | 2 | 2 | 40 | .47 | .049 | 5 | 217 | .52 | 160 | .06 | 4 | 1.09 | .08 | .10 | 2 |
| JRG-85 | 5 | 16 | 3 | 45 | .1 | 8 | 6 | 399 | 2.22 | 2 | 5 | ND | 3 | 67 | .2 | 2 | 2 | 47 | .32 | .062 | 7 | 62 | .51 | 236 | .08 | 4 | .94 | .03 | .09 | 2 |
| JRG-86 | 19 | 20 | 2 | 50 | .1 | 10 | 7 | 398 | 1.98 | 2 | 5 | ND | 2 | 102 | .2 | 2 | 2 | 39 | .44 | .042 | 6 | 219 | .49 | 160 | .08 | 5 | 1.00 | .09 | .10 | 1 |
| JRG-87 | 13 | 287 | 2 | 62 | .4 | 9 | 6 | 812 | 1.94 | 4 | 5 | ND | 2 | 77 | .2 | 2 | 2 | 40 | .43 | .054 | 8 | 146 | .46 | 136 | .08 | 5 | .99 | .06 | .07 | 1 |
| JRG-88 | 7 | 56 | 2 | 45 | .1 | 7 | 7 | 389 | 1.73 | 2 | 5 | ND | 1 | 84 | .2 | 2 | 2 | 35 | .37 | .046 | 5 | 80 | .53 | 146 | .06 | 6 | .95 | .03 | .06 | 2 |
| JRG-89 | 8 | 70✓ | 2 | 43 | .2 | 11 | 13 | 522 | 2.04 | 2 | 5 | ND | 1 | 66 | .2 | 2 | 2 | 40 | .43 | .051 | 3 | 92 | .63 | 110 | .08 | 4 | 1.01 | .05 | .10 | 2 |
| JRG-90 | 6 | 43 | 2 | 40 | .1 | 8 | 9 | 407 | 1.85 | 2 | 5 | ND | 1 | 66 | .2 | 2 | 2 | 37 | .38 | .045 | 4 | 77 | .53 | 103 | .07 | 3 | .88 | .04 | .08 | 1 |
| STANDARD C | 18 | 60 | 40 | 131 | 6.8 | 69 | 31 | 1052 | 3.96 | 39 | 19 | 7 | 39 | 52 | 18.4 | 15 | 20 | 60 | .47 | .096 | 39 | 56 | .92 | 180 | .07 | 35 | 1.89 | .06 | .14 | 11 |

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| SAMPLE# | No ppm | Cu ppm | Pb ppm | Zn ppm | Ag ppm | Ni ppm | Co ppm | Mn ppm | Fe % | As ppm | U ppm | Au ppm | Th ppm | Sr ppm | Cd ppm | Sb ppm | Bi ppm | V ppm | Ca % | P % | La ppm | Cr ppm | Mg % | Ba ppm | Ti % | B ppm | Al % | Na % | K % | W ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| JRG-91 | 10 | 119 | 2 | 62 | .4 | 16 | 19 | 611 | 3.10 | 5 | 5 | ND | 2 | 89 | .2 | 2 | 2 | 59 | .70 | .068 | 4 | 121 | 1.01 | 182 | .09 | 2 | 1.73 | .06 | .14 | 1 |
| JRG-92 | 7 | 39 | 3 | 39 | .1 | 8 | 11 | 469 | 1.76 | 2 | 5 | ND | 1 | 70 | .2 | 2 | 2 | 34 | .38 | .045 | 3 | 80 | .53 | 107 | .06 | 2 | .89 | .04 | .07 | 2 |
| JRG-93 | 5 | 153 | 2 | 59 | .3 | 17 | 22 | 649 | 3.30 | .3 | 5 | ND | 1 | 88 | .2 | 2 | 2 | 62 | .67 | .075 | 4 | 66 | 1.11 | 181 | .09 | 2 | 1.77 | .04 | .13 | 1 |
| JRG-94 | 10 | 60 | 2 | 45 | .1 | 12 | 15 | 633 | 2.21 | 2 | 5 | ND | 1 | 81 | .2 | 2 | 2 | 42 | .47 | .047 | 4 | 123 | .71 | 150 | .07 | 2 | 1.22 | .05 | .09 | 2 |
| JRG-96 | ✓ 6 | 104 ✓ | 3 | 55 | .3 | 14 | 17 | 568 | 2.95 | 3 | 5 | ND | 1 | 90 | .2 | 2 | 2 | 55 | .59 | .068 | 4 | 77 | .98 | 194 | .08 | 2 | 1.59 | .04 | .10 | 1 |
| JRG-97 | 8 | 30 | 2 | 36 | .1 | 9 | 10 | 461 | 1.86 | 2 | 5 | ND | 1 | 66 | .2 | 2 | 2 | 35 | .37 | .038 | 3 | 96 | .66 | 103 | .06 | 2 | 1.02 | .04 | .06 | 1 |
| JRG-98 | ✓ 5 | 40 | 2 | 40 | .1 | 10 | 9 | 365 | 2.00 | 2 | 5 | ND | 1 | 62 | .2 | 2 | 2 | 38 | .40 | .043 | 3 | 66 | .72 | 117 | .06 | 2 | 1.05 | .03 | .06 | 1 |
| RG-1 | 12 | 218 | 19 | 150 | .4 | 9 | 10 | 706 | 3.15 | 4 | 5 | ND | 1 | 155 | 1.0 | 2 | 2 | 75 | .99 | .071 | 3 | 52 | .70 | 42 | .07 | 5 | 1.78 | .04 | .11 | 2 |
| RG-2 | 10 | 998 | 4 | 100 | 1.3 | 14 | 17 | 716 | 3.24 | 5 | 5 | ND | 1 | 149 | .2 | 2 | 2 | 77 | .94 | .092 | 3 | 77 | 1.00 | 36 | .10 | 4 | 1.79 | .05 | .13 | 1 |
| RG-3 | 11 | 354 ✓ | 28 | 130 | .5 | 9 | 15 | 789 | 3.20 | 4 | 5 | ND | 1 | 226 | .5 | 2 | 2 | 79 | 1.14 | .093 | 2 | 56 | .98 | 37 | .10 | 3 | 2.15 | .05 | .15 | 1 |
| RG-4 | 7 | 264 | 19 | 110 | .4 | 8 | 13 | 670 | 2.75 | 6 | 5 | ND | 1 | 251 | .4 | 2 | 2 | 67 | 1.35 | .082 | 2 | 43 | .85 | 40 | .08 | 2 | 2.46 | .06 | .13 | 1 |
| RG-5 | 8 | 227 | 12 | 112 | .3 | 9 | 12 | 660 | 3.09 | 5 | 5 | ND | 1 | 216 | .2 | 2 | 2 | 77 | 1.17 | .090 | 3 | 68 | .88 | 43 | .11 | 2 | 2.02 | .07 | .14 | 1 |
| RG-6 | 7 | 137 | 6 | 90 | .2 | 8 | 11 | 612 | 3.11 | 3 | 5 | ND | 1 | 177 | .2 | 2 | 2 | 81 | 1.01 | .088 | 3 | 65 | .78 | 42 | .11 | 3 | 1.60 | .06 | .13 | 1 |
| RG-7 | 6 | 154 | 3 | 87 | .2 | 8 | 10 | 590 | 2.79 | 3 | 5 | ND | 1 | 174 | .2 | 2 | 2 | 70 | .94 | .083 | 3 | 46 | .79 | 43 | .09 | 3 | 1.64 | .05 | .11 | 1 |
| RG-8 | 6 | 160 | 3 | 92 | .3 | 10 | 11 | 613 | 2.80 | 3 | 5 | ND | 1 | 173 | .2 | 2 | 2 | 69 | .97 | .084 | 3 | 51 | .85 | 48 | .09 | 3 | 1.73 | .05 | .12 | 1 |
| RG-9 | 6 | 111 | 4 | 73 | .3 | 11 | 10 | 550 | 3.08 | 4 | 5 | ND | 1 | 149 | .2 | 2 | 2 | 78 | .90 | .085 | 3 | 73 | .81 | 42 | .11 | 2 | 1.41 | .05 | .13 | 1 |
| RG-10 | 5 | 122 | 2 | 80 | .2 | 16 | 11 | 550 | 2.99 | 3 | 5 | ND | 1 | 138 | .2 | 2 | 2 | 70 | .87 | .087 | 2 | 74 | 1.02 | 49 | .10 | 2 | 1.51 | .04 | .12 | 1 |
| RG-11 | 5 | 97 | 3 | 75 | .1 | 13 | 10 | 548 | 2.83 | 2 | 5 | ND | 1 | 136 | .2 | 2 | 2 | 69 | .83 | .086 | 2 | 67 | .92 | 46 | .10 | 3 | 1.39 | .05 | .13 | 1 |
| RG-12 | 4 | 121 ✓ | 2 | 75 | .3 | 15 | 11 | 505 | 2.90 | 5 | 5 | ND | 1 | 125 | .2 | 2 | 2 | 68 | .78 | .083 | 3 | 62 | .92 | 46 | .08 | 3 | 1.33 | .03 | .11 | 1 |
| RG-13 | 5 | 109 ✓ | 3 | 68 | .1 | 12 | 10 | 535 | 2.68 | 2 | 5 | ND | 1 | 123 | .2 | 2 | 2 | 65 | .76 | .081 | 2 | 51 | .86 | 44 | .10 | 2 | 1.31 | .04 | .11 | 1 |
| RG-14 | 6 | 103 | 3 | 69 | .2 | 14 | 11 | 518 | 2.93 | 3 | 5 | ND | 1 | 121 | .2 | 2 | 2 | 71 | .77 | .081 | 2 | 68 | .87 | 45 | .10 | 2 | 1.27 | .04 | .12 | 1 |
| RG-15 | 5 | 102 | 3 | 67 | .1 | 13 | 11 | 538 | 2.84 | 3 | 5 | ND | 1 | 114 | .2 | 2 | 3 | 68 | .73 | .078 | 3 | 56 | .87 | 44 | .09 | 2 | 1.26 | .03 | .11 | 1 |
| RG-16 | 5 | 92 | 2 | 62 | .1 | 13 | 10 | 519 | 2.70 | 2 | 5 | ND | 1 | 111 | .2 | 2 | 2 | 67 | .74 | .080 | 3 | 62 | .85 | 46 | .10 | 2 | 1.20 | .04 | .12 | 1 |
| RG-17 | 6 | 89 | 3 | 68 | .1 | 12 | 10 | 534 | 2.71 | 2 | 5 | ND | 1 | 112 | .2 | 2 | 2 | 67 | .76 | .081 | 3 | 65 | .85 | 46 | .10 | 2 | 1.20 | .04 | .12 | 1 |
| RG-18 | 5 | 71 ✓ | 2 | 58 | .1 | 12 | 9 | 489 | 2.73 | 2 | 5 | ND | 1 | 105 | .2 | 2 | 2 | 68 | .73 | .079 | 3 | 72 | .83 | 44 | .11 | 3 | 1.09 | .05 | .13 | 1 |
| RG-19 | 5 | 71 | 3 | 58 | .1 | 12 | 9 | 493 | 2.83 | 2 | 5 | ND | 1 | 109 | .2 | 2 | 2 | 71 | .75 | .079 | 4 | 71 | .84 | 44 | .11 | 3 | 1.10 | .04 | .13 | 1 |
| RG-20 | 6 | 82 | 2 | 59 | .1 | 13 | 9 | 517 | 2.72 | 2 | 5 | ND | 1 | 107 | .2 | 2 | 2 | 69 | .74 | .082 | 4 | 66 | .86 | 49 | .11 | 2 | 1.22 | .05 | .13 | 1 |
| RG-21 | 4 | 76 | 2 | 34 | .1 | 17 | 8 | 354 | 4.72 | 2 | 5 | ND | 3 | 45 | .2 | 2 | 2 | 196 | .52 | .102 | 8 | 97 | .50 | 56 | .10 | 4 | .78 | .04 | .06 | 1 |
| RG-22 | 4 | 69 | 2 | 38 | .1 | 10 | 6 | 320 | 2.70 | 2 | 5 | ND | 3 | 50 | .2 | 2 | 3 | 79 | .59 | .106 | 7 | 63 | .55 | 53 | .07 | 5 | .83 | .05 | .07 | 2 |
| RG-23 | 4 | 62 ✓ | 2 | 36 | .1 | 10 | 6 | 289 | 2.73 | 2 | 5 | ND | 2 | 43 | .2 | 2 | 2 | 93 | .50 | .094 | 7 | 56 | .48 | 48 | .06 | 4 | .72 | .04 | .06 | 1 |
| RG-24 | 4 | 71 | 2 | 37 | .1 | 10 | 6 | 291 | 2.38 | 2 | 5 | ND | 2 | 50 | .2 | 2 | 2 | 72 | .51 | .092 | 6 | 55 | .53 | 60 | .07 | 4 | .82 | .04 | .07 | 1 |
| RG-25 | 4 | 102 | 2 | 38 | .1 | 5 | 7 | 328 | 2.82 | 2 | 5 | ND | 2 | 74 | .2 | 2 | 2 | 92 | .57 | .102 | 7 | 37 | .47 | 56 | .06 | 2 | .81 | .03 | .07 | 1 |
| RG-26 | 7 | 84 | 2 | 41 | .1 | 6 | 7 | 329 | 2.46 | 2 | 5 | ND | 2 | 89 | .2 | 2 | 3 | 74 | .59 | .082 | 7 | 74 | .50 | 73 | .06 | 4 | .92 | .06 | .11 | 2 |
| RG-27 | 5 | 65 | 2 | 33 | .1 | 8 | 6 | 319 | 2.79 | 2 | 5 | ND | 3 | 54 | .2 | 2 | 2 | 94 | .51 | .087 | 6 | 59 | .47 | 54 | .07 | 4 | .76 | .05 | .08 | 1 |
| RG-28 | 5 | 70 | 2 | 38 | .1 | 7 | 6 | 308 | 2.38 | 2 | 5 | ND | 2 | 61 | .2 | 2 | 2 | 72 | .52 | .082 | 6 | 65 | .49 | 67 | .06 | 4 | .85 | .05 | .09 | 1 |
| STANDARD C | 19 | 61 | 39 | 131 | 6.7 | 70 | 31 | 1054 | 3.97 | 36 | 19 | 7 | 40 | 53 | 18.4 | 15 | 21 | 60 | .48 | .099 | 39 | 58 | .95 | 182 | .08 | 38 | 1.90 | .06 | .14 | 13 |

Project:

| Sample Number | Au ppb | Ag ppm | Au oz/ton |
|-----------------|--------|--------|-----------|
| X-32 { | 74953 | 14 | 0.34 |
| | 74954 | 12 | 0.16 |
| | 74955 | 24 | 0.13 |
| | 74957 | 2 | 0.10 |
| | 74958 | 2 | 0.01 |
| X-31 { | 74960 | 4 | 0.04 |
| | 74962 | 2 | 0.03 |
| | 74963 | 2 | 0.02 |
| X-30 { | 74968 | 2 | 0.02 |
| | 74969 | 2 | 0.28 |
| BC-39 - BC-58 { | 86277 | 2 | 0.01 |
| | 86815 | 48 | 4.80 |
| | 86816 | 6 | 0.03 |
| | 86817 | 10 | 0.33 |
| | 86818 | 30 | 1.02 |
| BC-37 { | 86819 | 6 | 0.05 |
| | 86820 | 294 | 5.40 |
| | 86822 | 2 | 0.08 |
| | 86823 | 6 | 0.01 |
| | 86824 | 32 | 0.08 |
| BC-38 { | 86825 | 26200 | 0.764 |
| | 86826 | 124 | 0.29 |
| | 86828 | 24 | 0.19 |
| | 86829 | 44 | 1.27 |
| | 86830 | 10 | 0.05 |
| BC-39 { | 86831 | 12 | 0.13 |
| | 86832 | 10 | 0.12 |
| | 86833 | 10 | 0.16 |
| | 86834 | 2 | 0.05 |
| | 86835 | 2 | 0.04 |
| BC-36 { | 86836 | 32 | 0.10 |
| | 86837 | 12180 | 0.355 |
| | 86838 | 14640 | 0.427 |
| | 86839 | 6480 | 0.189 |
| | 86840 | 514 | 0.53 |
| BC-32 { | 86841 | 4 | 0.13 |
| | 86842 | 2 | 0.07 |
| BC-38 { | 86881 | 2 | 0.03 |
| | 86882 | 4 | 0.05 |
| | 86883 | 4 | 0.96 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-258

Project: BC-32

| Sample Number | Au ppb | Ag ppm |
|---------------|--------|--------|
| JRG 95 | 44 | 0.11 |
| 250 | 36 | 0.15 |
| 251 | 42 | 0.19 |
| 252 | 28 | 0.16 |
| 253 | 42 | 0.25 |
| 254 | 58 | 0.32 |
| 255 | 56 | 0.38 |
| 256 | 420 | 0.31 |
| 257 | 38 | 0.23 |
| 258 | 36 | 0.19 |
| 259 | 52 | 0.18 |
| 260 | 18 | 0.16 |
| 261 | 12 | 0.15 |
| 262 | 16 | 0.15 |
| 263 | 22 | 0.16 |
| 264 | 10 | 0.17 |
| 265 | 12 | 0.16 |
| 266 | 4 | 0.09 |
| 267 | 10 | 0.15 |
| 268 | 14 | 0.18 |
| 269 | 2 | 0.16 |
| 270 | 6 | 0.18 |
| 271 | 4 | 0.25 |
| 272 | 2 | 0.29 |
| 273 | 2 | 0.08 |
| 274 | 456 | 0.19 |
| 275 | 2 | 0.13 |
| 276 | 2 | 0.15 |
| 277 | 2 | 0.15 |
| 278 | 2 | 0.14 |
| 279 | 2 | 0.26 |
| 280 | 2 | 0.11 |
| 281 | 2 | 0.12 |
| 282 | 2 | 0.10 |
| 283 | 8 | 0.10 |
| 284 | 2 | 0.10 |
| 285 | 2 | 0.09 |
| 286 | 4 | 0.11 |
| 287 | 10 | 0.11 |
| 288 | 2 | 0.07 |
| 289 | 4 | 0.09 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-235

Project:

| Sample Number | Au ppb | Ag ppm |
|---------------|--------|--------|
| 74919 | 2 | 0.05 |
| 74920 | 2 | 0.45 |
| 74921 | 16 | 0.40 |
| 74922 | 28 | 0.18 |
| 74923 | 2 | 0.01 |
| 74924 | 2 | 0.04 |
| 74925 | 2 | 0.05 |
| 74926 | 4 | 0.13 |
| 74927 | 2 | 0.07 |
| 74928 | 2 | 0.04 |
| 74929 | 2 | 0.13 |
| 74930 | 4 | 0.16 |
| 74931 | 2 | 0.02 |
| 74932 | 2 | 0.04 |
| 74933 | 4 | 0.05 |
| 74934 | 506 | 8.90 |
| 74935 | 164 | 4.40 |
| 74936 | 8 | 0.08 |
| 74937 | 60 | 5.40 |
| 74938 | 2 | 0.17 |
| 74939 | 2 | 0.04 |
| 74940 | 2 | 0.32 |
| 74941 | 410 | 11.00 |
| 74942 | 6 | 0.17 |
| 74943 | 4 | 0.22 |
| 74944 | 2 | 0.14 |
| 74945 | 4 | 0.05 |
| 74946 | 2 | 0.15 |
| 74947 | 2 | 0.14 |
| 74948 | 2 | 0.06 |
| 74949 | 2 | 0.01 |
| 74950 | 2 | 0.14 |
| 74951 | 2 | 0.10 |
| 74952 | 14 | 0.24 |
| 74956 | 12 | 0.22 |
| 74959 | 2 | 0.25 |
| 74961 | 2 | 0.09 |
| 74964 | 2 | 0.06 |
| 74965 | 2 | 0.06 |
| (X-38) 74966 | 2 | 0.01 |

Job#: 90-235

Project:

| Sample Number | Au ppb | Ag ppm |
|---------------|-----------|-----------|
| 86263 | 4 | 0.09 |
| 86264 | 2 | 0.02 |
| 86265 | 10 | 0.12 |
| 86266 | 8 | 0.09 |
| 86267 | 2 | 0.15 |
| 86268 | 4 | 0.04 |
| 86269 | 4 | 0.07 |
| 86270 | 2 | 0.47 |
| 86271 | 338 | 3.80 |
| 86272 | 16 | 1.84 |
| 86273 | 2 | 0.02 |
| 86274 | 2 | 0.01 |
| 86275 | 2 | 0.02 |
| 86276 | 10 | 0.30 |
| 86278 | 118 | 3.10 |
| 86279 | 10 | 0.18 |
| 86280 | 16 | 0.23 |
| 86281 | 8 | 0.33 |
| 86282 | 2 | 0.01 |
| 86283 | 2 | 0.03 |
| 86284 | 2 | 0.08 |
| 86285 | 4 | 0.02 |
| 86286 | 2 | 0.20 |
| 86287 | 6 | 0.06 |
| 86801 | 2 | 0.02 |
| 86802 | 54 | 0.41 |
| 86803 | 2 | 0.16 |
| 86805 | 12 | 0.59 |
| 86806 | 2 | 0.08 |
| 86807 | 2 | 0.04 |
| 86808 | 2 | 0.14 |
| 86810 | 6 | 0.04 |
| 86812 | 4 | 0.14 |
| 86813 | 22 | 11.10 |
| 86814 | 2 | 0.06 |
| 86821 | 2 | 0.04 |
| 86853 | 2 | 0.02 |
| 86856 | 2 | 0.68 |
| 86857 | 2 | 0.06 |
| 86858 | 2 | 0.05 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-228

Project: BC-32

| Sample Number | Au ppb | Ag ppm |
|---------------|-----------|-----------|
|---------------|-----------|-----------|

↓
 BC-38
 81 B 10 0.07
 82 4 0.07
 83 6 0.08
 84 12 0.14
 85 6 0.09

86 34 0.08
 88 16 0.07
 89 12 0.12
 90 10 0.12
 91 8 0.09

92 16 0.04
 93 10 0.04
 94 28 0.06
 95 8 0.05
 96 8 0.04

97 8 0.03
 98 18 0.07
 99 6 0.05
 101 6 0.03
 102 6 0.02

BC-12
 103 4 0.04
 105 A 2 0.06
 105 B 8 0.08
 106 6 0.09
 107 8 0.10

108 8 0.08
 109 4 0.07
 JDK- 1 8 0.10
 2 12 0.08
 3 80 0.09

BC-32
 4 10 0.09
 5 14 0.08
 6 12 0.08
 7 12 0.08
 8 12 0.08
 9 12 0.07
 11 14 0.10
 12 2 0.12
 13 10 0.08
 15 4 0.07

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-228

Project: BC-32

| Sample Number | Au ppb | Ag ppm |
|---------------|--------|--------|
|---------------|--------|--------|

JDK-
↓
17 24 0.08
18 14 0.09
19 4 0.08
BC-32 20 8 0.05
21 18 0.22

23 6 0.06
24 10 0.06
25 12 0.06
26 12 0.08
27 8 0.06

28 50 0.07
29 6 0.08
30 6 0.05
31 6 0.08
32 6 0.03

33 8 0.08
34 2 0.06
35 4 0.13
36 4 0.09
37 10 0.07

38 8 0.06
39 14 0.12
40 6 0.06
JO-
↓
1 6 0.15
2 10 0.15

42
3 20 0.09
4 14 0.28
5 2 0.07
6 2 0.10
7 2 0.18

8 2 0.05
9 6 0.08
10 2 0.03
11 10 0.05
12 .6 0.03

13 8 0.04
14 4 0.03
15 140 0.03
16 6 0.03
17 4 0.03

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-228

Project: BC-32

| Sample Number | Au ppb | Ag ppm |
|---------------|-----------|-----------|
| JO- 177 | 2 | 0.12 |
| 178 | 2 | 0.05 |
| 179 | 2 | 0.12 |
| 180 | 2 | 0.10 |
| 181 | 4 | 0.26 |
| 182 | 2 | 0.06 |
| 183 | 2 | 0.06 |
| 184 | 4 | 0.07 |
| 185 | 2 | 0.06 |
| 186 | 2 | 0.04 |
| 187 | 8 | 0.06 |
| 188 | 8 | 0.30 |
| 189 | 4 | 0.14 |
| 190 | 6 | 0.13 |
| 191 | 2 | 0.02 |
| 192 | 4 | 0.18 |
| 193 | 2 | 0.02 |
| 194 | 4 | 0.06 |
| 195 | 2 | 0.13 |
| 196 | 2 | 0.17 |
| 197 | 2 | 0.20 |
| 198 | 2 | 0.05 |
| 199 | 2 | 0.02 |
| 200 | 8 | 0.04 |
| 201 | 4 | 0.07 |
| 202 | 2 | 0.03 |
| JRG- 1 | 6 | 0.04 |
| 2 | 4 | 0.02 |
| 3 | 4 | 0.01 |
| 4 | 4 | 0.01 |
| 5 | 10 | 0.04 |
| 6 | 2 | 0.01 |
| 7 | 10 | 0.01 |
| 8 | 2 | 0.01 |
| 9 | 44 | 0.03 |
| 10 | 94 | 0.08 |
| 11 | 248 | 0.14 |
| 12 | 4 | 0.05 |
| 13 | 4 | 0.06 |
| 14 | 8 | 0.11 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-228

Project: BC-32

| Sample Number | Au ppb | Ag ppm |
|---------------|--------|--------|
| JRG- 15 | 2 | 0.07 |
| 16 | 8 | 0.14 |
| 17 | 2 | 0.04 |
| 18 | 10 | 0.07 |
| 19 | 28 | 0.05 |
| 20 | 36 | 0.06 |
| 21 | 6 | 0.07 |
| 22 | 10 | 0.07 |
| 23 | 2 | 0.04 |
| 24 | 4 | 0.05 |
| 25 | 4 | 0.03 |
| 26 | 2 | 0.02 |
| 27 | 6 | 0.04 |
| 28 | 6 | 0.05 |
| 29 | 4 | 0.04 |
| 30 | 2 | 0.03 |
| 31 | 6 | 0.03 |
| 32 | 32 | 0.04 |
| 33 | 2 | 0.02 |
| 34 | 14 | 0.04 |
| 35 | 4 | 0.04 |
| 36 | 2 | 0.01 |
| 37 | 6 | 0.01 |
| 38 | 4 | 0.01 |
| 39 | 2 | 0.01 |
| 40 | 8 | 0.03 |
| 41 | 18 | 0.03 |
| 42 | 4 | 0.02 |
| 43 | 6 | 0.08 |
| 44 | 2 | 0.10 |
| 45 | 4 | 0.10 |
| 46 | 2 | 0.07 |
| 47 | 2 | 0.05 |
| 48 | 2 | 0.04 |
| 49 | 6 | 0.06 |
| 50 | 2 | 0.04 |
| 51 | 8 | 0.18 |
| 52 | 4 | 0.11 |
| 53 | 10 | 0.10 |
| 54 | 10 | 0.09 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-228

Project: BC-32

| Sample Number | Au ppb | Ag ppm |
|---------------|-----------|-----------|
| JRG- 55 | 4 | 0.07 |
| 56 | 22 | 0.18 |
| 57 | 8 | 0.11 |
| 58 | 4 | 0.11 |
| 59 | 8 | 0.10 |
| 60 | 8 | 0.10 |
| 61 | 30 | 0.13 |
| 62 | 12 | 1.60 |
| 63 | 10 | 0.10 |
| 64 | 38 | 0.40 |
| 65 | 10 | 0.09 |
| 66 | 24 | 0.09 |
| 67 | 12 | 0.12 |
| 68 | 2 | 0.07 |
| 69 | 20 | 0.10 |
| 70 | 10 | 0.07 |
| 71 | 30 | 0.10 |
| 72 | 12 | 0.10 |
| 73 | 4 | 0.08 |
| 74 | 2 | 0.07 |
| 75 | 10 | 0.09 |
| 76 | 6 | 0.07 |
| 77 | 14 | 0.09 |
| 78 | 20 | 0.12 |
| 79 | 12 | 0.07 |
| 80 | 8 | 0.06 |
| 81 | 12 | 0.06 |
| 82 | 16 | 0.07 |
| 83 | 14 | 0.08 |
| 84 | 8 | 0.06 |
| 85 | 60 | 0.06 |
| 86 | 20 | 0.06 |
| 87 | 4 | 0.30 |
| 88 | 28 | 0.10 |
| 89 | 24 | 0.06 |
| 90 | 20 | 0.05 |
| 91 | 66 | 0.14 |
| 92 | 10 | 0.05 |
| 93 | 64 | 0.18 |
| 94 | 26 | 0.07 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-228

Project: BC-32

| Sample Number | Au ppb | Ag ppm |
|---------------|--------|--------|
| JRG- 96 | 60 | 0.11 |
| 97 | 10 | 0.05 |
| 98 | 18 | 0.05 |
| RG- 1 | 18 | 0.35 |
| 2 | 26 | 1.27 |
| 3 | 14 | 0.48 |
| 4 | 14 | 0.30 |
| 5 | 8 | 0.27 |
| 6 | 2 | 0.15 |
| 7 | 8 | 0.17 |
| 8 | 6 | 0.17 |
| 9 | 10 | 0.13 |
| 10 | 12 | 0.14 |
| 11 | 10 | 0.11 |
| 12 | 10 | 0.14 |
| 13 | 6 | 0.11 |
| 14 | 14 | 0.10 |
| 15 | 6 | 0.10 |
| 16 | 10 | 0.12 |
| 17 | 8 | 0.09 |
| 18 | 28 | 0.08 |
| 19 | 8 | 0.08 |
| 20 | 4 | 0.09 |
| 21 | 10 | 0.06 |
| 22 | 6 | 0.06 |
| 23 | 8 | 0.05 |
| 24 | 2 | 0.05 |
| 25 | 8 | 0.07 |
| 26 | 12 | 0.09 |
| 27 | 6 | 0.07 |
| 28 | 4 | 0.07 |
| 29 A | 8 | 0.06 |
| 29 B | 6 | 0.06 |
| 30 | 8 | 0.06 |
| 31 | 8 | 0.06 |
| 32 | 4 | 0.07 |
| 33 | 8 | 0.08 |
| 34 | 10 | 0.06 |
| 35 | 4 | 0.07 |
| 36 | 6 | 0.04 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-163

Project: BC-32

| Sample Number | Au ppb | Ag ppm | Cu ppm | Pb ppm | Zn ppm |
|---------------|-----------|-----------|-----------|-----------|-----------|
| 86162 | 90 | 0.46 | 16 | 4 | 45 |
| 86163 | 14 | 0.19 | 172 | 2 | 44 |
| 86164 | 2 | 0.04 | 19 | 6 | 60 |
| 86165 | 20 | 1.20 | 540 | 6 | 105 |
| 86166 | 8 | 0.12 | 17 | 3 | 57 |
| 86167 | 4 | 0.07 | 23 | 1 | 23 |
| 86168 | 4 | 0.28 | 133 | 1 | 83 |
| 86169 | 4 | 0.07 | 57 | 1 | 70 |
| 86170 | 2 | 0.07 | 36 | 1 | 62 |
| 86171 | 2 | 0.13 | 41 | 3 | 109 |
| 86172 | 6 | 0.09 | 51 | 1 | 71 |
| 86173 | 6 | 0.02 | 8 | 3 | 12 |
| 86174 | 2 | 0.11 | 108 | 5 | 8 |
| 86175 | 10 | 0.10 | 40 | 5 | 9 |
| 86176 | 38 | 0.69 | 12 | 50 | 6 |
| 86177 | 102 | 1.31 | 5 | 21 | 4 |
| 86178 | 2 | 0.23 | 144 | 1 | 19 |
| 86179 | 22 | 0.15 | 14 | 7 | 3 |
| 86180 | 28 | 0.19 | 20 | 8 | 23 |
| 86181 | 6 | 0.22 | 50 | 1 | 18 |
| 86182 | 4 | 0.43 | 27000 | 3 | 156 |
| 86183 | 142 | 54.0 | 18700 | 17 | 68 |
| 86184 | 2 | 0.48 | 23000 | 4 | 135 |
| 86185 | 2 | 0.13 | 340 | 3 | 10 |
| 86186 | 2 | 0.07 | 85 | 2 | 64 |
| 86187 | 6 | 0.16 | 19 | 4 | 31 |
| 86188 | 20 | 0.22 | 127 | 2 | 24 |
| 86189 | 4 | 0.11 | 130 | 2 | 21 |
| 86190 | 20 | 0.16 | 600 | 24 | 62 |
| 86191 | 8 | 0.10 | 37 | 10 | 75 |
| 86192 | 18 | 0.12 | 183 | 5 | 32 |
| 86193 | 48 | 0.28 | 154 | 1 | 28 |
| 86194 | 2 | 0.14 | 165 | 2 | 24 |
| 86195 | 14 | 0.16 | 88 | 3 | 74 |
| 86196 | 2 | 0.04 | 37 | 4 | 270 |
| 86197 | 84 | 0.24 | 12 | 2 | 31 |
| 86199 | 16 | 0.09 | 22 | 3 | 27 |
| 86200 | 8 | 0.06 | 24 | 4 | 45 |
| 86201 | 2 | 0.26 | 430 | 3 | 32 |
| 86202 | 8 | 0.12 | 145 | 3 | 37 |

TERRAMIN RESEARCH LABS Ltd.

Job#: 90-163

Project: BC-32

| Sample Number | Au ppb | Ag ppm | Cu ppm | Pb ppm | Zn ppm |
|---------------|--------|--------|--------|--------|--------|
| 86203 | 8 | 0.10 | 106 | 1 | 33 |
| 86204 | 10 | 0.21 | 430 | 4 | 62 |
| 86205 | 8 | 0.19 | 360 | 4 | 35 |
| 86206 | 8 | 0.02 | 12 | 1 | 63 |
| 86207 | 12 | 0.05 | 83 | 7 | 55 |
| 86208 | 2 | 0.03 | 20 | 3 | 44 |
| 86209 | 8 | 0.97 | 1320 | 39 | 79 |
| 86210 | 8 | 0.53 | 330 | 5 | 34 |
| 86211 | 2 | 0.01 | 21 | 5 | 19 |
| 86212 | 4 | 0.02 | 30 | 2 | 31 |
| 86213 | 8 | 0.13 | 146 | 4 | 75 |
| 86214 | 474 | 11.5 | 15700 | 12 | 51 |
| 86217 | 40 | 0.59 | 2200 | 2 | 26 |
| 86218 | 6 | 0.22 | 950 | 2 | 14 |
| 86219 | 4 | 0.14 | 530 | 2 | 9 |
| 86220 | 4 | 0.12 | 530 | 2 | 15 |

APPENDIX III

DESCRIPTIONS OF ROCK SAMPLES

JO/CRO CLAIMS

BC-44

| <u>Sample No.</u> | <u>Description</u> |
|-------------------|---|
| 86168 | Loc. JO 1 Claim, gossan on west side of headwaters of W fork of Darb Creek; fine-grained, fractured rusty weathering quartz diorite ?; 1 - 5 % variable pyrite content. |
| 86162 | Loc. CRO 4 Claim, near L.C.P.; very rusty, banded leucocratic recrystallized rhyolitic tuff (?) volcanic ash (?) or exhalite (?) bands of pyrite defining foliation in the rock; approximately 8% fine-grained to medium-grained euhedral pyrite in disseminated bands. |
| 86163 | Loc. CRO 4 Claim, near post OS1W; coarse-grained hornblende gabbro; > 50% coarse-grained dark green hornblende phenocrysts to 5 mm diameter in a light green felsic matrix - no sulphides; some epidote alteration. |
| 86164 | Loc. CRO 4 Claim, on ridge near post OS2W; silicified, recrystallized hornfelsed volcanic; probably originally an andesitic flow; strong epidote alteration on fractures; < 1% pyrite, both disseminated and on fracture planes. |
| 86165 | Loc. CRO 4 Claim, near post OS3W; dark green chloritized mafic volcanic cut by stringers of massive pyrite. |
| 86166 | Loc. CRO 4 Claim, near post OS3W; near 86165; leucocratic sheared, silicified, rusty weathering zone - mostly fine-grained quartz with 1 - 2% fine-grained pyrite, disseminated and on fracture planes. |
| 86167 | Loc. CRO 3 Claim, near post 4S3E; float; sulphide (pyrite) rich boulder from rusty formation outcropping in cliffs above; well-fractured, 4-5% fine-to coarse-grained disseminated pyrite, medium green siliceous matrix cut by pale green carbonate-epidote stringers. |
| 86168 | Loc. CRO 2 Claim, near post 2N0E; rusty weathering, fine-grained medium green volcanisediment; siliceous, recrystallized, hornfelsic texture; some disseminated blebs and fracture fillings of pyrite. |

- 86169 Loc. CRO 2 claim, near post 3N0E rusty weathering, fine-grained dark grey meta siltstone; cut by 2 cm wide quartz stringer, "hairline" stringers of massive pyrite cut rock perpendicular to quartz veinlet.
- 86170 Loc. CRO 2 Claim, near post 3N0E talus sample below cliffs; sandy, medium-grained volcanic arenite, or greywacke; 3% disseminated pyrite/pyrrhotite.
- 86171 Loc. same area as 86170, similar to 86179 but finer-grained; fine-grained, black calcareous siltstone 2 - 3% extremely fine-grained disseminated pyrite.
- 86172 Loc. same area as 86170, fine-grained, banded, dark grey siltstone similar to 86169, but with bands of disseminated pyrite and pyrite on fracture planes, probably up to 7% microscopic to very fine-grained sulphides, rock is heavy; leucocratic bands with pyrite might be barite.
- 86173 Loc. same area as 86170, thinly laminated dark grey mudstone, "heavy" - could contain microscopic sulphides.
- 86179 Loc. CRO 2 claim near post 5N2E leucocratic, recrystallized (?), highly limonitic zone with 5-8% fine-grained to medium-grained disseminated pyrrhotite, traces of malachite - rhyolitic tuff (?), or volcanic ash (?), or exhalite (?); rock is approximately 70% fine-grained quartz, 25% sericite, and 5% sulphides.
- 86180 Loc. same zone as 86179 similar to 86179, but a little less sericite, a little more pyrrhotite.
- 86181 Loc. on bedrock knob projected out into valley of NE flowing tributary of Kliyul Creek - 1 km S of post 4S1E of the CRO 3 claim; "gneissic" texture-bands of light grey siliceous fine-grained material alternating with fine-grained dark green chloritic bands; approximately 3% pyrrhotite/pyrite both disseminated and on fractures - most likely the "exhalite" unit here

-pyrite stringers, also pyrite on fracture planes, total approximately 4% extremely fine-grained to fine-grained pyrite.

- 86189 Loc. JO 2 Claim, same zone as 86188; sample similar to 86188; feldspar porphyry float noted in talus.
- 86193 Loc. CRO 1 Claim, near post 5S0W; narrow magnetite > epidote > chlorite skarn - no sulphides - in fine-grained mafic volcanic flow.
- 86194 Loc. CRO 1 Claim near post 3W3S at crest of divide; silica-pyrrhotite skarn, 4 - 5% disseminated pyrrhotite in extremely fine-grained siliceous matrix - probably near an intrusive contact.
- 86195 Loc. JO 7 Claim, near post 5S1E; fine-grained, black sulphidic metasediment; approximately 3% microscopic to extremely fine-grained disseminated pyrite, also pyrite in "hairline" stringers.
- 86196 Loc. JO 1 Claim, near post 5E2S; orange weathering quartz-carbonate stringers cutting greenish recrystallized quartz > carbonate rock - no sulphides.
- 86197 Loc. JO 2 Claim, near post 4S0E; rusty weathering, fine-grained, dark to medium green recrystallized metasediment cut by hairline quartz-pyrite stringers plus approximately 2% very fine-grained disseminated pyrite.
- 86198 Loc. JO 2 Claim, same area as 86197 but 50 - 75 m downhill; rusty, vuggy quartz float.
- 86199 Loc. JO 2 Claim, near post 4S2E; fine-grained, leucocratic, siliceous sulphide rich zone-exhalite ? ash tuff ?.
- 86200 Loc. JO 2 Claim, same location as 86199 sample similar to 86199.
- 86201 Loc. JO 3 Claim, near post 0N3E fine-grained quartz diorite; approximately 4 - 5% medium-grained disseminated euhedral pyrite.

- 86202 Loc. JO 3 Claim, near post 4N3E; sample similar to 86201 but finer-grained with pyrite on fracture planes.
- 86203 Loc. JO 3 Claim, near post 0N4E dark green siliceous, fine-grained to aphanitic intrusive-quartz diorite dike ? 2 - 3% disseminated fine- to medium-grained euhedral pyrite.
- 86801 Loc. 250 m SW of CRO3 L.C.P., aphanitic light green dacitic flow or sill - probably a sill injected into westerly dipping sedimentary sequence.
- 86802 Loc. 300 m W of CRO 2/3 L.C.P., sample similar to 86801 but carries approximately 1% pyrrhotite on fracture planes and as disseminated ragged blebs.
- 86803 Loc. approximately 100 m N of 86802, lahar ?, angular blocks of sulphide bearing dacite similar to 86802 embedded in thinly laminated black siltstone or silty limestone (see 86804); jointing in dacite N of siltstone zone is 033/62NW.
- 86804 Same location as 86803, thinly laminated black siltstone or silty limestone with variable attitude (324/75SW) with 0.5 cm to 30 cm fragments and angular blocks of dacite embedded in it.
- 86805 Loc. approximately 300 m NW of CRO 2/3 L.C.P., calcite vein float; veins, carbonate - filled rocks and carry blebs of chalcopyrite.
- 86806 Loc. CRO 2 Claim, approximately 250 m N of L.C.P.; sulphidic exhalite (?) or ash tuff (?); 1 - 15% disseminated extremely fine-grained pyrrhotite in aphanitic light green siliceous matrix-distinctive rusty weathering marker horizon.
- 86807 Loc. CRO 2 Claim, approximately 100 m E of 86806; andesite flow - feldspar - hornblende porphyry, approximately 5% 0.5 cm diameter hornblende phenocrysts and 10% 0.3 cm diameter, stubby, white, broken feldspar phenocrysts in a fine-grained to aphanitic medium green groundmass.
- 86808 Loc. approximately 950 S and 300 m E of CRO 2 post 4S0E on bedrock knob projecteingout into valley of NE flowing tributary of Kliyul Creek; sample is a

light green aphanitic banded felsic rock containing approximately 1% fine-grained disseminated pyrrhotite; position of outcrop near lower volcanic unit-sedimentary package interface suggests a transitional facies of the exhalite unit (see 86806).

- 86816 Loc. N Fork of Kliyul Creek approximately 200 m N of CRO 2 N boundary; "dioritized" andesite; altered, recrystallized silicified meta-andesite collected in Kliyul Creek deformation zone, andesite is cut by hairline, siliceous, light green stringers crosscutting in several directions - no sulphides; sample superficially resembles a diorite due to recrystallized mafic and felsic minerals in a granular texture.
- 86817 Loc. CRO 2 Claim, along west side of N Fork of Kliyul Creek, approximately 350 m S of 86816; well pyritized quartz veinlet from a zone or band of narrow shears and quartz stringers; andesitic wall rocks are impregnated with pyrite; shear zones trend subparallel to N Fork of Kliyul Creek, attitude of shearing 330/50 - 80SW.
- 86818 Same location as 86817, pyritized andesitic wall rock.
- 86819 Loc. CRO 2 Claim, 75 m SW of 86818 - another zone of recrystallized "dioritized" andesite; 1 - 2% fine-grained disseminated blebs of pyrite.
- 86820 Same location as 86819; quartz stringer cutting altered andesite.
- 86821 Loc. approximately 50 m SW of 86819; outcrop on west side of north fork of Kliyul Creek - fine-grained, non-porphyritic andesite.
- 86822 Loc. JO 5 Claim, approximately 100 m E of post 4S4E, intensely carbonatized orange-weathering zone along projected trace of Dourtatelle Fault.
- 86823 Loc. JO 1 Claim, near L.C.P.; hornblende porphyry dyke NW strike, dip?
- 86824 Loc. Jo 5 Claim, approximately 300 m N and 50 m E of post 4SOE; pyritized felsic dyke, northerly strike, steep W (?) dip approximately 2% euhedral disseminated fine-grained pyrite.

- 86825 Loc. JO 1 Claim, approximately 100 m E and 250 m N of post 4S2E; quartz float; contains disseminated coarse-grained pyrite euhedra (< 1%) plus finer-grained aggregates of pyrite along stringers.
- 86826 Loc. JO 1 Claim a few meters east of 86825, intensely sheared, recrystallized, "laminated" amphibolite derived from mafic volcanics near upper contact of "upper Triassic gabbro"; attitude of foliation variable but averages about 024/80W.
- 86827 Loc. JO 1 Claim just to west of 86828; meta-andesite - appears hornfelsed.
- 86828 Loc. JO 1 Claim 200 m E and 200 m N of post 4S2E; layered (024/80W) or foliated and compositionally banded "gneissic" amphibolitic zone; alternating dark green fine-grained chloritic bands and leucocratic fine-grained siliceous bands; occasional clasts or inclusions of leucocratic rock fragments carrying 1% disseminated pyrite plus 2 - 3% pyrite along fractures or shear-suggesting a pyroclastic origin.
- 86829 Loc. JO 1 Claim, same area as 86828 "gneissic" band of very fine-grained felsic material with 3-4% blebs of pyrite along foliation planes; foliation 002/80 - 85W.
- 86830 Loc. JO 1 Claim, approximately 150 m E of post 4S2E; series of sulphide rich horizons (022/74NW); first zone, 50 cm thick band of disseminated very fine-grained to fine-grained pyrite in leucocratic fine-grained siliceous matrix.
- 86831 Loc. JO 1 Claim, same area as 86830 approximately 10 m downslope; "second zone" 50 - 75 cm thick zone of > 5% disseminated sulphides similar to 86830; intervening rocks are alternating dark green and light grey bands (see 86828).
- 86832 Loc. JO 1 Claim approximately 6 m downslope from 86831; "third zone", 75 cm thick sulphide rich band similar to 86830, 86831.
- 86833 Loc. JO 1 claim, approximately 10 m downslope from 86832; "fourth zone", sulphide bands are now more closely spaced, semi-continuous, greater proportions of felsic rich bands - exhalite ?, strongly foliated, "gneissic" appearance; attitude 024/70 -80 NW, as above.

- 86834 Loc. JO 1 Claim, approximately 75 m NE of 86833; quartz vein (300/85SW) cutting "gabbroic gneiss" ("gneiss":322/50SW).
- 86835 Loc. JO 1 Claim, same area as 86834 "gabbroic gneiss" laminated alternating bands of felsic and mafic material, sulphides.
- 86836 Loc. JO 1 Claim, same area as 86835; good hand specimen of "gabbroic" unit showing elongated, flattened, felsic inclusions/lenses (pyroclastic origin ?); sulphides here are more euhedral, disseminated.
- 86841 Loc. JO 6 Claim, approximately 600 m W and 550 m N of post 690W; outcrop of pyrrhotite rich exhalite (?) unit exposed in bedrock knob on N side of W Fork of Kliyul Creek; 1 - 3% very fine-grained disseminated pyrrhotite in aphanitic leucocratic material.
- 86842 Loc. JO 6 Claim, same location as 86841; but about 50 m further south; thinly laminated silty dark grey limestone or limey siltstone beds overlying exhalite beds; strikes NNW, dips SW; bedding planes are disturbed.

LEGEND

Intrusive Rocks

JURASSIC TO CRETACEOUS

Hogen Batholith

mon Monzonite, quartz monzonite

qdi Quartz diorite

md Monsodiorite, local monzogabbro

Volcanic and Sedimentary Rocks

UPPER TRIASSIC

Takla Group

Undivided pillowd augite basalt flows and massive volcanic breccias and augite porphyry lavas, minor feldspar porphyritic flows.

Undivided volcanioclastic rocks and sedimentary rocks; includes tuff breccias, lahar, volcanic sandstones, tuffaceous argillite and black micritic carbonate beds.

Exhalite; leucocratic, thinly laminated to massively bedded fine grained quartz +/- sericitic +/- carbonate assemblage with 1% to 15% fine grained disseminated pyrrhotite, gradational upwards into dark grey to light grey thinly laminated tuffaceous argillite beds and gradational downwards into green laminated chlorite-carbonate tuffaceous beds.

Undifferentiated porphyritic feldspar rich tuffs, flows, and breccias of predominantly andesitic composition.

SYMBOLS

Geological contact, assumed

Fault

Strike and dip of bedding

Strike and dip of foliation, jointing

Legal corner post

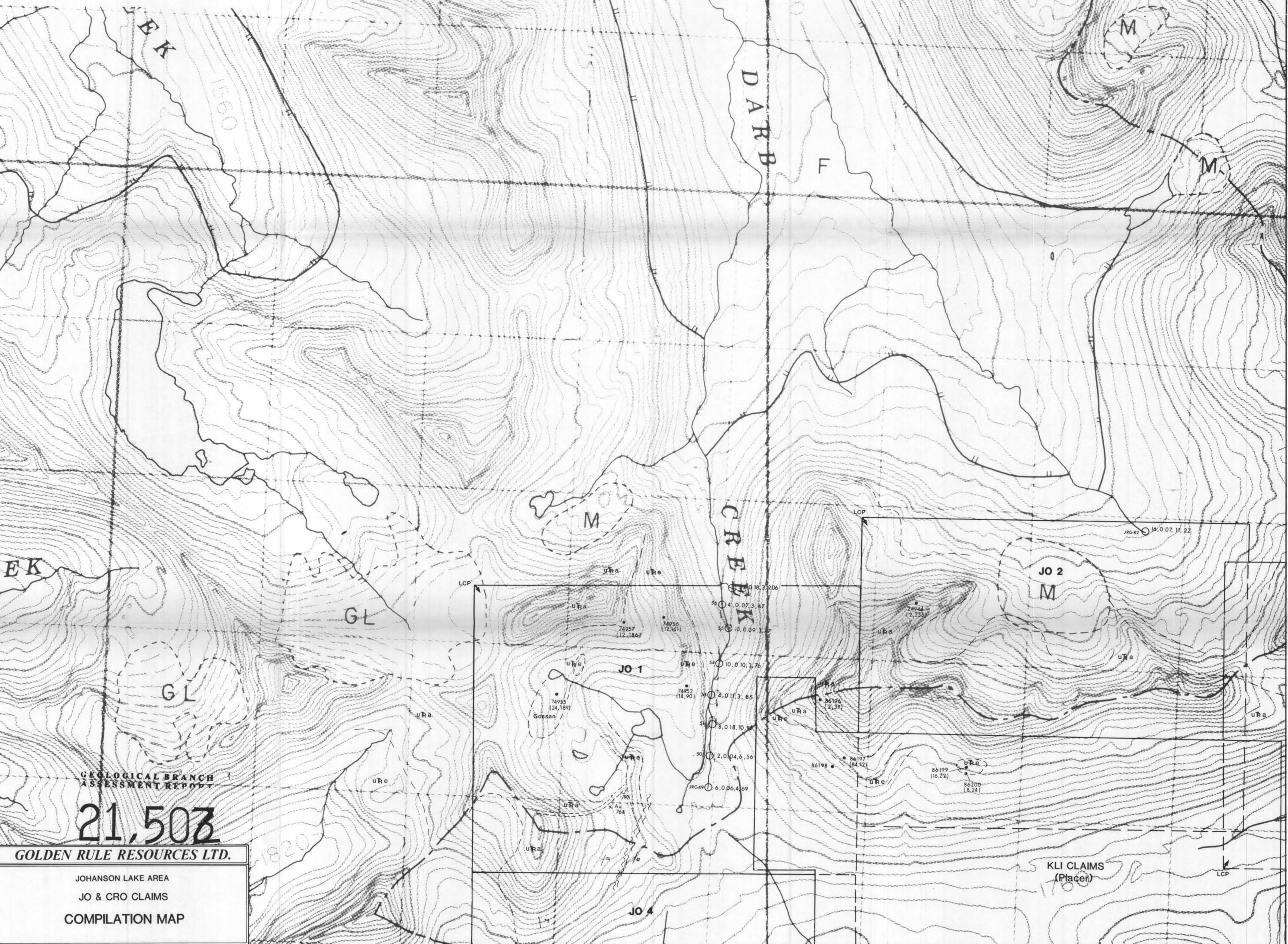
Claim boundary


Rock sample location and number

Au(ppm), Cu(ppm)


Silt sample location and number

Au(ppm), Ag(ppm), Mo(ppm), Cu(ppm), As(ppm)





| | |
|-----------------|-----------------|
| Date: MAY 1991 | N.T.S.: 94D/8,9 |
| Revised: | MAP NO.1 EAST |
| Scale: 1:10,000 | 0 500 1000m |



76

77

78

79

80

81

82

83

684000m. E.

6265000m. N.

64

63

62

61

60

59

58

