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# **OF THE MGM PROPERTY**

Golden Mining Division NTS 83 D/1 & 82M/16 Lat: 52°02' Long: 118°14'

Owner: John Leask; White Knight Resource OLOGICAL BRANCH Suite 922 510 W. Hastings St. Vancouver, B.C. V6B 1L8

Operator: Teck Exploration Ltd. 960-175 Second Ave., Kamloops, B.C. V2C 5W1

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22.0 Craig Alford

Greg Thomson January, 1992

#### SUMMARY

A field exploration program was carried out by Teck Exploration Ltd. on the MGM property between June 14 to August 26 1991. The work consisted of property-wide mapping and sampling, grid establishment ( $\approx$ 11.0 kilometres) with accompanying grid mapping, soil sampling and an HLEM survey. The overall cost of the 1991 program was approximately \$200,000.

The MGM-TSAR property consists of 14 modified grid claims and one (1 unit) 2-post claim for a total of 152 units. The claims are located in the Cummins River area of the Golden Mining District of British Columbia.

Geological formations appear to be consistent throughout most of the property, generally striking northwest and dipping steeply southwest. The area north of the Cummins River appears to dip slightly shallower and is thrust over a sequence of strata similar to that observed south of the river.

Exploration work on the MGM property has located a similar geological sequence as that hosts the Cummins River massive sulphide occurrence (the Canyon showing). The Canyon showing is covered by Cominco's "Bend" claim group. Grades indicated by past drilling are subeconomic, however a 1991 drilling program by Cominco has extended the zone along strike to the southeast with improving grades in this direction, as well as down dip.

Grid work southeast of the Bend claims show a good correlation between soil geochemical values (Zn, Pb & Mn) and a persistent HLEM anomaly.

Geophysics, soil geochemistry and whole rock data indicate the sulphide horizon is continuous from the Cummins River south to Line 20+00S, a strike length of 3 kilometres.

The geology of the MGM property indicates good potential for hosting large tonnage 'sedex' style massive zinc, lead and silver mineralization within metasediments belonging to the Tsar Creek Formation of Mid to Lower Cambrian age.

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#### RECOMMENDATIONS

The next stage of exploration should involve a program of diamond drilling south of the Cummins River. Drill targets would test the mineralized zone on the MGM property immediatelye southeast of the Cominco (Bend) Claims property. Further drilling would test the depth and strike length of the sulphide zone.

Greater investigation of the region north of the Cummins River would be required before a drilling program can be recommended for the area.

Stream silt or moss mat sampling combined with reconnaissance examination of the area surrounding around the claims may serve to extend the known limit of mineralization within the Tsar Creek Formation.

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- Appendix B: Cost Statement
- Appendix C: Certificate of Analyses
- Appendix D: Analytical Procedures
- Appendix E: Rock Sample Descriptions

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## 1. INTRODUCTION

The MGM and TSAR claim groups surround The "Bend" SEDEX-style Zinc-Lead mineral prospect, currently owned and under exploration by Cominco Ltd.

This report encompasses geological mapping and sampling as well as grid related geochemical and geophysical surveys completed on the MGM and TSAR claim groups from June 14 to August 25, 1991.

The group of claims were optioned from John M. Leask - White Knight Resources Ltd. under the terms of an agreement dated April 12, 1991.

## 2. LOCATION AND ACCESS

The property lies on the east side of the Rocky Mountain Trench approximately 100km northwest of Golden, B.C. (Figure 1), located both north and south of the confluence of Cummins River and Columbia Reach (Kinbasket Lake). The property is located on NTS map sheet 83D1 and 82M/16, bounded by latitude's 51°59' to the south and 52°05' to the north and longitude's 118°04' to the east and 118°17' to the west.

The property may be reached by several modes. Large freight must be brought in by a barge service out of Bush Harbour, located approximately 50km southeast of the claim area. This is usually a 4 hour one-way trip. Alternately, the area can be reached via helicopter services out of Golden or Revelstoke. A float plane service from Golden is also available. Flight time from Golden or Revelstoke is approximately one hour.

The closest road access to the property is from the northwest, where a logging road at Redrock Harbour provides access south to Mica Creek and Revelstoke via Highway 23. To the southeast, the Sullivan Road provides access south to Golden via the old Big Bend Highway.

The property itself is well covered by recent clear cut logging areas and logging roads which are in good driveable condition. Several are present between Cummins River and Tsar creek.

Accommodation during the course of field work was provided through rental of the Tsar Creek (Evans Forest Products Ltd.) logging camp.

The portion of the property lying to the north of Cummins River is crossed by one main logging road; more are planned for 1992. Access to that area is via a 16 ft. motor boat.

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#### 3. PHYSIOGRAPHY AND VEGETATION

Geographically the property is within the southern extent of the Selwyn Range. These mountains have rugged peaks with gently to moderately inclined southwest facing slopes.

For the most part the property is covered by a veneer of alluvial sediments ranging in thickness from 1 to 20 metres. A portion of the MGM 8, TSAR 1, TSAR 3, TSAR 5, TSAR 7 and TSAR 8 claims occur below the Columbia Reach waterline which varies seasonally from approximately 730-765 metres ( $\approx$ 2400-2500 ft).

Climatologically the property lies within the Interior Wet Belt where precipitation can exceed 100 centimetres per year. Vegetation is thick and lush. Common evergreens are cedar, douglas fir and hemlock at lower elevations giving way to lodgepole pine and balsam fir above 1370 metres.

Elevations across the property range between lake level at approximately 762m, to the top of the property boundary at 1,800m. The entire property is below treeline which is approximately 1,970 metres.

Winters in the area are usually long and severe with snowfall often exceeding 9 metres.

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# 4. CLAIM STATUS

The property, located in the Golden mining division, consists of the MGM, MGM 2-5, MGM 8 TSAR 1-8 and ARM claims totalling 152 units (Figure 2). The claims are registered in the name of Teck Corporation held in trust for White Knight Resources Ltd. The following table lists all pertinent claim data.

| Claim Name       | Record No. | Units | Record Date | Expiry Date |  |  |  |  |
|------------------|------------|-------|-------------|-------------|--|--|--|--|
| MGM              | 373        | 9     | AUG/20/79   | AUG/20/95   |  |  |  |  |
| MGM 2            | 422        | 2     | SEPT/19/79  | SEPT/19/95  |  |  |  |  |
| MGM 3            | 423        | 6     | SEPT/19/79  | SEPT/19/95  |  |  |  |  |
| MGM 4            | 1004       | 20    | AUG/4/82    | AUG/4/93    |  |  |  |  |
| MGM 5            | 1130       | 5     | JAN/28/83   | JAN/28/92   |  |  |  |  |
| MGM 8            | 2156       | 6     | MAY/27/90   | MAY/27/95   |  |  |  |  |
| TSAR 1           | 2323       | 16    | FEB/17/91   | FEB/17/92   |  |  |  |  |
| TSAR 2           | 2324       | 20    | FEB/17/91   | FEB/17/92   |  |  |  |  |
| TSAR 3           | 2325       | 12    | FEB/18/91   | FEB/18/92   |  |  |  |  |
| TSAR 4           | 2326       | 12    | FEB/18/91   | FEB/18/92   |  |  |  |  |
| TSAR 5           | 2327       | 6     | FEB/16/91   | FEB/16/92   |  |  |  |  |
| TSAR 6           | 2328       | 12    | FEB/18/91   | FEB/18/92   |  |  |  |  |
| TSAR 7           | 2329       | 6     | FEB/16/91   | FEB/16/92   |  |  |  |  |
| TSAR 8           | 2330       | 18    | FEB/17/91   | FEB/17/92   |  |  |  |  |
| ARM              | 2331       | 1     | FEB/17/91   | FEB/17/92   |  |  |  |  |
| Total: 152 Units |            |       |             |             |  |  |  |  |

#### CLAIM RECORDS

Table 1

The MGM, MGM 2-5, MGM 8 and TSAR 1 (totalling 65 units) are grouped as the MGM Group. The TSAR 2-8 and ARM claims (totalling 87 units) are grouped as the TSAR Group.

# 5. **PREVIOUS WORK**

Table 2 chronicles the work and results of mineral exploration within the area.

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#### TABLE 2 PREVIOUS WORK

| YEAR      | COMPANY               | WORK   | RESULTS  |  |  |  |  |  |
|-----------|-----------------------|--|--|--|--|--|--|--|
| 1940<br>? |                       | Big Bend highway Construction  | Discovered Canyon zone on Cummins river.   |  |  |  |  |  |
| 1949      |                       | First claims staked  | Claims lapsed.   |  |  |  |  |  |
| 1966      | Cominco Ltd.          | Staked the Bend group of claims<br>(45 units)  |  |  |  |  |  |  |
| 1967      | Cominco Ltd.          | Geological mapping<br>240m of drilling (13 holes)<br>Trenched main showing on either side of Cummins river                           | Outlined the Canyon zone to be a stratiform body of massive sulphide<br>mineralization yielding an average width of 6.5m of 3% combined Zn-Pb &<br>0.25 oz/t Ag.<br>Considered occurrence to be of 'fissurevein' type.   |  |  |  |  |  |
| 1968-1974 | Cominco Ltd.          |  | Cominco gradually reduced claim group to the 12 now currently being held.  |  |  |  |  |  |
| 1970      | Laura Mines Ltd.      | Geological mapping<br>Soil sampling<br>≈490m of drilling (4 holes - canyon showing)  | A coincident Pb-Zn geochem anomaly was outlined in the area of the known mineralized structural trend. No other geochemical trend was outlined. Expanded known width of the canyon zone to 8.6m however as a result aggregate grades are lower than Cominco's. |  |  |  |  |  |
| 1979      | John Leask & Assoc.   | Staked the MGM and the MGM2-4 claims<br>Reconnaissance geological mapping  | Reinterpreted the Bend mineral occurrence to be of a shale hosted massive sulphide type similar to the Cirque and Howards Pass deposits.   |  |  |  |  |  |
| 1981      | E&B Explorations Inc. | Geological mapping   | Related the north road showing, the canyon showing and a pyrrhotite showing within the Tsar creek area to one conformable mineralized unit with a strike length of approximately 12 kilometres.  |  |  |  |  |  |
| 1983      | Riocanex              | Carried out Magnetic, VLF-EM and SE-88 Genie surveys over the MGM and the MGM 2,3 and 7 claims                                       | A banded mag anomaly striking ≈100 • most probably caused by magnetite<br>was observed.<br>No E.M. or magnetic response was observed over the known mineralization.  |  |  |  |  |  |
| 1985      | Esso Minerals Canada  | Geological mapping<br>Soil sampling<br>VLF-EM and large loop EM-37 over north showing<br>≉212m of drilling (2 holes - north showing) | Further outlined the north road showing (3km north of canyon zone).<br>Drill results neither confirmed nor denied the presence of the massive sulphide<br>extension to the North road area.<br>A picture of greater geological complexity was encountered.     |  |  |  |  |  |
| 1987      | Cominco Ltd.          | Geological mapping<br>Road access and drill site construction  | Enhanced access to mineralized area.<br>Observed the stratabound mineralization over a longer strike/dip distance than previously inferred.  |  |  |  |  |  |
| 1991      | Cominco Ltd.          | ≄1200m of drilling (3 holes)   | Traced mineralized dolomite unit to greater depth and southeasterly extent.  |  |  |  |  |  |

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## 6. 1991 PROGRAM

Table 3 summarises the work completed in 1991.

#### Table 3

| WORK   | DATES   |
|--|---|
| Project Preparation                          | June 3-11                                       |
| Mobilization                                 | June 12-14                                      |
| General Mapping, prospecting<br>and sampling | June 15-22<br>July 1-19<br>Aug 2-8<br>Aug 15-25 |
| Line cutting, grid mapping and soil sampling | July 20-Aug 1                                   |
| Geophysical survey (HLEM)                    | July 12-15<br>July 27-Aug 1                     |
| Blasting & Hand trenching                    | Aug 9-14  |
| Demobilization                               | Aug 26-28                                       |
| Drafting of maps & final report              | Aug 29-Sept 20                                  |

## MGM WORK SUMMARY & SCHEDULE - 1991

The primary focus of the exploration program was to show geologic continuity between the Cummins River - Bend massive sulphide prospect and possible mineralized zones both north and south of Cominco's Bend claims.

In 1991, 65 field days were spent on the MGM property between June 14 and August 25. The program consisted of geologic mapping, concurrent rock sampling, stream silt sampling, soil sampling and a HLEM survey. In addition drill core from previous workers was relogged.

General prospecting and mapping was carried out throughout the property. Logging roads and cuts were utilized to best advantage. The geologic investigation consisted of 1:10,000 scale property mapping as well as 1:5,000 scale mapping of the grid area near Cominco's Bend claims. A total of 28 rock and 49 stream silt samples were collected as part of the prospecting and mapping program.

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Minconsult Mineral Exploration Services of Vernon, B.C. were contracted to establish a 10.5 line kilometre cut grid adjacent to the southeast extent of the Cominco claims. Lines were cut to I.P. standard with picketed stations every 50m. Two additional lines were flagged in, one on Cominco's ground over a known showing and another extending the grid 100m to the southeast. All grid lines have been geologically mapped and the soil sampled every 50m or 25m in areas of suspected favourable geology. A total of 232 soil samples were collected.

A total of 7400 metres of ground HLEM were surveyed by Maple Services\MWH Geosurveys Ltd. on the MGM grid. In addition a 350 metre line was surveyed on Cominco's property in order to observe the geophysical signature concordant with the mineralized unit.

Blasting and hand trenching was conducted by Minconsult Mineral Exploration Services. Trenching was carried out on Line 20+00S between stations 3+90E and 5+10E.

Soil and rock geochemical samples were analyzed by Eco-Tech Labs of Kamloops, B.C.

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#### 7. GEOLOGY

#### A. Regional

The property lies just east of the Purcell Thrust Fault and is on the western limb of the Porcupine Creek Anticlinorium (Figure 3). The Purcell Thrust Fault zone closely follows the Rocky Mountain Trench and is delineated by the contrasting stratigraphic sequence on either side of the trench (Simony et al., 1980). The Hadrynian Windermere Group rocks of the Selkirk Mountains west of the trench have been thrust up against the Mid-Cambrian to Upper Proterozoic Chancellor, Gog and Miette Groups of the Rocky Mountains (Wheeler 1964).

The property is in an area of dominantly Lower to Mid Cambrian miogeosynclinal rocks. In the Cummins River area these sedimentary rocks form a thick, conformable stratigraphic succession.

The Cambrian section is represented by three main lithological elements: the Mid to Upper Cambrian Kinbasket Limestones and the Mid to Lower Cambrian Tsar Creek metapelites of the Chancellor Group and the Lower Cambrian Quartzites of the Gog Group. All lithologies have been metamorphosed to middle and upper greenschist assemblages.

#### **B. Property Geology**

The 1991 field mapping concentrated mainly in the area between Cummins River and Tsar Creek (Figure 4a & 4b). Outcrop exposure is very limited throughout most of the property. Logging roads and clear cuts have assisted greatly in providing sufficient exposure to allow distinction between major rock units.

Outcrop exposure is poor throughout the Tsar Creek Section, however the upper Gog quartzite-lower Tsar contact is evident as the quartzites provide a steeper erosionally resistant ridge. The upper Tsar Creek-lower Kinbasket contact is gradual and thus its placement is very much subjective.

Mapping south of Cummins River indicates a correlatable strike length of approximately 13.0 kilometres for the conformable Kinbasket Limestones, Tsar Creek metapelites and Gog Group Quartzite formations.

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FIGURE 3

Generalized geologic map of southern Canoe River area.

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## I) Lithology

Lithologies outcropping are those of the Gog and Chancellor groups;

## **Gog Group**

The Lower Cambrian Gog Group and consists of three formations, from youngest to oldest: Mahto, Mural and McNaughton. For the purpose of the 1991 investigation, Gog Group lithologies have not been subdivided by formational boundaries.

In the property area this sequence consists of milky to greyish white quartzite, light grey to pale pink micaceous quartzite, thinly laminated light grey to pink quartzofeldspathic (psammitic) schists, chert, interbedded biotite and garnet schists and a greyish white to light buff coloured marble. It is thought that the marble unit observed correlates with the Mural Formation.

The Gog Group quartzites conformably overlie Upper Proterozoic Miette Group metasediments which were not observed in outcrop on the property. The overall thickness of the Gog Group is estimated to be slightly greater than 1,000 metres.

## **Chancellor Group**

The Tsar Creek and Kinbasket Formations of the Chancellor Group are recognized to be Middle Cambrian. Due to structural thickening, stratigraphic thickness are hard to establish. Estimates for the thickness of the Tsar Creek Formation have ranged from 100 to 600 metres (Simony et. al. 1980) and thickness for the Kinbasket Formation have ranged from 150m (Meilliez 1972) to greater than 1,000 metres (Simony et. al. 1980).

## **Tsar Creek Formation**

The Tsar Creek Formation is dominantly a pelitic schist of variable metamorphic grade and argillaceous component. Lithological units recognized within this formation were muscovite and biotite schists, garnet-mica and garnet-staurolite-mica schists, greywacke turbidites, micaceous limestone and argillite.

Metamorphic grade throughout the property ranges from lower to upper greenschist facies up to amphibolite or garnet-staurolite-kyanite grade. Muscovite, biotite and almandine garnet are common metamorphic minerals. Kyanite and sillimanite were observed in a few localities.

The lithologies associated with the mineralization are a quartz sericite schist, mineralized dolomite, argillaceous garnet schist and a micaceous quartzite. Such lithologies may relate to metamorphosed shales, cherts and carbonates which are consistent with deposition within a 'starved basin' environment (Eckstrand 1984).

## **Kinbasket Formation**

The Kinbasket Formation is dominated by pale grey to grey, thinly laminated, sandy to silty limestones with interlaminated pelitic sediments. Interstratified beds of pelitic sediments from 2-30m in thickness occur within the limestones. Thinly bedded, grey micritic limestones with thin graphitic laminae are also recognized with the formation.

The limestones have been metamorphosed to impure marbles and pelitic material within the limestones have formed micaceous and garnetiferous horizons. Similarly, the interstratified pelitic layers have been metamorphosed to mica schists and garnet mica schists. Under the local metamorphic grade the Kinbasket limestones generally appear as a rusty to buff weathered, biotitic and locally garnet bearing grey unit.

# II) Structure

Regional structure in the area is dominated by the presence of the Columbia River-Purcell Fault systems and the Porcupine Creek Anticlinorium. Within the Cummins River area, the Purcell Thrust juxtaposes Hadrynian Windermere Group lithologies against Cambrian sequences east of the Rocky Mountain Trench. The Porcupine Creek Anticlinorium (PCA) exposes Chancellor Group rocks on the western flank and carbonate facies rocks to the east, with the Gog and Miette groups in the core (Lickorish and Simony 1991). The entire property exists on the westernmost extent of the PCA.

Three phases of deformation have been recognised within the region (Fyles 1960 and Simony et al., 1980). All phases of folding have been acknowledged to be essentially coaxial, thus, folding has not interrupted the stratigraphic sequence and linear extent of the rock units.

It has been noted (Meillez 1972) that the tight folding characterizing the Chancellor Group does not penetrate the Gog group and is presumed to be due to a detachment horizon in the basal Tsar Creek Formation.

The schistosity that pervades the area  $(S_2)$  is axial planar to the large scale  $(F_2)$  folds that make up the PCA (Lickorish and Simony 1991). The rocks of the Chancellor Group have an earlier bedding parallel cleavage  $(S_1)$  and many small refolded isoclines. First phase folds  $(F_1)$  are isoclinal and occur on single layer scale with the resultchistosity parallel to bedding  $(S_0)$ . Third phase fold structures were not recognised during the property examination.

Two structurally distinct areas exist within the property and for the most part occur on either side (north and south) of the Cummins River.

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## South Side

A virtually continuous stratigraphic sequence from the Kinbasket to the Gog Group quartzites is exposed on the property between Cummins River and Tsar Creek. The sequence is rightside up, with tops to the southwest (see Figure 6a).

Local bedding (Figure 7) and schistosity (Figure 8) orientations were observed to be essentially parallel. Units within the map area generally strike between 125° & 140° and dip southwest, between 50° & 65°. Mineral lineations, cleavage-bedding intersection lineations and minor fold axes plunge approximately 10°-20° to both the northwest and southeast (Figure 9a & 9b).

A compilation of bedding and schistosity contours and lineation maximums is displayed on Figure 10. The poles to bedding and schistosity fit two great circles with corresponding poles to the great circles approximately equal to the maximum linear fabric concentrations. The two great circles and linear fabric concentration indicates a curvilinear  $F_2$  fold axis, concordant with a sheath fold style, however, planar and linear data maximums indicate the predominant plunge is toward the northwest.

The dominant structures within the Kinbasket and Tsar Creek rocks are the second phase  $(F_2)$  asymmetric step-like folds with their axial planar cleavage  $(S_2)$  near parallel with the average long limb orientation of 131°-56°SW.

# North side

Two major structural elements define the area north of the Cummins River.

Outcrop within the Cummins canyon exposes, except for a quartzofeldspathic psammite unit, the same stratigraphically continuous section from Kinbasket limestones, through the Tsar creek metapelites to the Gog group quartzites as is observed throughout the south side of the property.

The character of the quartzofeldspathic psammites-Kinbasket limestones contact and the psammite unit infer a fault at this location, where the psammite unit is interpreted to belong to the Gog Group and has been thrust on top of the Kinbasket limestones. Previous investigations have interpreted a similar fault and geological sequence however, it now appears appropriate to project the fault south of the Cummins River to the Columbia reach and where it is thought to terminate against the Rocky Mountain Trench.

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| TECK EXPLORATION LTD.   |  |  |  |  |  |  |
|---|--|--|--|--|--|--|
| MGM PROJECT   |  |  |  |  |  |  |
| FIGURE 6a & 6b  |  |  |  |  |  |  |
| CROSS SECTIONS AT 27° (LOOKING NORTH WEST)  |  |  |  |  |  |  |
| DATE         DRAWN:         SEPT.         11,         1991         SCALE:         1:10,000         DWG.         NAME:           COMPILED         BY:         C.A.         JOB         No:         1703         MGM-SEC1           DRAWN         BY:         S.A.         NTS         No:         83D/1         MGM-SEC1 |  |  |  |  |  |  |



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Furthermore, the stratigraphy encompassed by the thrust fault boundary appears to be at a significantly different attitude than that presented on the south side. Structural measurements of schistosity indicate a maximum attitude of approximately 160°-25°SW (Figure 11). A second concentration of poles occurs at a similar location as that observed in the south side. This data relates to schistosity in an attitude similar to the pervasive  $S_2$  orientation. Linear data concentrations occur in the northwest and southeast (Figure 12), with a maximum in the northwest quadrant. This information, coupled with field observation, is interpreted to suggest a generally flat laying, more openly folded sequence of rocks plunging gently to the northwest and southeast, with the majority of folds plunging northwest.

Consequently, the stratigraphy encompassed by the thrust fault is close to its original horizontal attitude; which would mean if you were to walk from the waters edge of the Columbia Reach uphill you would be walking up stratigraphically (see Figure 6b). Beyond the thrust fault toward the north east and below the thrust fault the stratigraphic attitude is similar to the south side.

## III) Mineralization and Geochemistry

Due to the local lithologies, sulphide mineralogy and stratiform nature of the mineralization, the origin of this deposit is best interpreted to be a synsedimentary exhalative ('sedex') type.

The mineralized horizon is a crudely stratiform sulphide zone lying conformably in Tsar Creek metasediments. A thorough investigation of the Tsar Creek formation was conducted, including some work on the Cominco claims. Sample locations for the various geochemical surveys conducted accross the property are displayed on Figures 13a, 13b and 14.

Four main areas of mineralization, including the Cominco Canyon showing, were observed; the Canyon showing, the North Road showing, the Tsar Creek pyrrhotite and the 1991 grid trenches. Correlation with intersections from previous drilling will be examined.

## **Canyon Showing**

Both walls of the Cummins River canyon sulphide section were examined and sampled to determine the extent and nature of the pyrite-sphalerite-galena mineralization and geochemical relationships of hanging and foot wall lithologies. Three main mineralized zones are recognized on the basis of the sulphide and gangue relationships; siliceous sulphide, massive sulphide and manganiferous dolomite.

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Gangue minerals dominate the siliceous unit. Sulphide minerals comprise less than 40% of the unit. The sulphide assemblage is mainly pyrite with minor traces of galena and sphalerite. Petrographic analysis (Reddy 1986) indicate pyrrhotite both interstitial and in cracks of gangue, and chalcopyrite and tetrahedrite occurring as grains within galena.

The massive sulphide layer consists of 40-80% pyrite with sphalerite and galena occurring mostly interstitial to pyrite. Gangue minerals are dominantly quartz and dolomite. Chip sampling through the sulphide zone yielded assay values of 0.02% Zn, 0.76% Pb and 24.4 g/t Ag.

The manganiferous dolomite is grey-white and is characterized by a red-brown to chocolate brown weathered surface. Quartz composes approximately 10% of the unit. Sulphides occur mainly as layering parallel lenses and laminations up to 1cm thick.

Representative lithologies were obtained from the hanging wall, across the sulphide zone, to the foot wall on the north face of the canyon showing. Samples were analyzed to observe the bulk composition of the rocks across the zone. Figures 15a & 15b display the major oxides from the samples. A brief description of the units encountered with their geochemical features are described:

## Hanging wall

Garnet schist- Weakly to moderately foliated, light to dark grey garnet schist. Garnets are generally subhedral to euhedral, 0.5 to 4cm in diameter and red to red-brown in colour. Whole rock analyses reveals that the unit is CaO rich and MgO rich relative to the foot wall garnet schist.

Quartz sericite schist- Fine grained, light grey to waxy yellow, well foliated, highly siliceous schist with sericite defining foliation. Minor pyrite and graphite are observed on foliation surfaces.

Siliceous pyrite unit- Fine grained to aphanitic, light grey, siliceous pyrite horizon is also referred to as the siliceous sulphide unit. This unit may have originally been a chert. The high values of  $Fe_2O_3$  recorded for this unit correspond to the increased concentration of iron sulphides.

## Foot wall

Garnet schist- The foot wall garnet schist is fine grained, dark grey to black, garnet schist with a greater argillaceous component than the hanging wall garnet schist. Garnet size is generally 0.3-1.0cm. The unit is  $Al_2O_3$  and  $K_2O$  rich relative to the hanging wall garnet schist. Reddy (1980) has shown that the garnets of the footwall schist are primarily almandine while those of the hanging wall are spessartine.

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#### Tsar Creek showing

Approximately 700m up Tsar Creek, float boulders containing stockwork pyrrhotite were sampled. The rock is a massive, silicified fine grain metasediment containing stringer style pyrrhotite with no observable chalcopyrite. The actual source of the boulders, assumed to exist in the cliff above, was not located. An ICP analysis of the unit revealed 5% Fe, 25ppm Zn, 128ppm Pb, 1.2ppm Ag, 32ppm Cu and 2458ppm Mn.

The cliff along the southeast side of the creek exposed Kinbasket limestones, Tsar Creek argillites, fine grained turbidic wackes and quartz-sericite schists. Gog group quartzites were seen at the upper extent of the area of examination. This stratigraphy is comparable to much of the property, allowing for an assumed continuous section of strata from the Cummins river to Tsar Creek, a distance of approximately 12 kilometres.

#### North Road showing

Four bulldozed trenches (1966 - Cominco) are exposed along a section of road crossing the M.G.M., M.G.M.2 and M.G.M. 3 claims north of the Cummins River. A sulphide bearing chocolate brown weathering manganiferous dolomite layer is exposed in all of the trenches (Figure 16). Due to the strike and gentle dip of units within the area, the dolomite unit presents a broad outcrop exposure. The observed sequence of associated lithologies, (eg. garnet schists and quartz sericite schists) is similar to that observed within the Canyon Showing.

Two styles of mineralization occur within the dolomite:

1) 5-25cm wide bedding parallel bands of massive pyrite with minor galena and sphalerite, yielding 0.13% Zn, 0.12% Pb and 2.4 g/t Ag and 0.55% Zn, 0.1% Pb and 1.2 g/t Ag from Trench 3.

2) Galena and sphalerite occur mainly as lenses and laminations associated with minor narrow quartz veinlets, yielding 6056ppm Zn, 1978ppm Pb and 7ppm Ag from Trench 1 and 1495ppm Zn, 190ppm Pb and 4.2ppm Ag from Trench 4.

Attempts have been made at drilling the North Road Showing, however, insufficient exposure, structural information and difficult drilling conditions led to poor results.

#### **Drill Core**

A total of metres of core from three 1991 Cominco holes (C-91-1, 2 & 3) was examined (see Figure for hole locations). Observation of mineralized zones within the core reveal apparent widths of 4-11 metres of weakly silicified dolomite with sections of massive to

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thinly laminated pyrite>sphalerite>galena. The "hanging wall-foot wall" sequence; from the carbonaceous garnet schist, quartz sericite schist and the sulphide horizon, to the argillaceous garnet schist was observed in all three Cominco drill holes.

A total of 211.85 metres of core was examined from two holes drilled north of the Cummins River by Esso Minerals in 1985 (see Figure for hole locations).

DDH-1 encountered broken, rubbly, iron carbonate altered micaceous quartzite and quartzofeldspathic schists. DDH-1 was terminated after 38.11 metres.

DDH-2 intersected a sequence of banded quartz-schists with minor bands of dolomite was encountered down to  $\approx$ 57.5m, below which a garnet-schist with increasing coarseness and staurolite content predominated. It is thought that the units encountered within DDH-2 are analogous to the sequence of quartz-sericite schists, dolomite and lower Tsar Creek Formation garnet-staurolite schists observed south of the Cummins River. DDH-2 was terminated within the garnet-staurolite schist at 173.7 metres.

The presence of trace amounts of galena within thin dolomitic horizons was identified in both holes.

## Grid trenches

Exposed on Line 20+00S is a sequence of hanging and foot wall lithologies which appears identical to surface exposures observed on Cominco's Bend property.

Between stations 3+90E and 4+80E, a 15 metre section of thinly bedded/laminated, cream coloured quartz-sericite schist was unearthed (Figure 17). More massive sections contain sparse foliation parallel blebs of galena and sphalerite. Trace fine grain pyrite has also been observed. ICP analysis of the unit reported 119ppm Zn, 322ppm Pb and 0.6ppm Ag.

Between stations 4+35E and 4+37E a chocolate brown weathering dolomitic (?) schist was exposed. Due to overburden depth, the full extent of dolomite horizon is not known.

From 4+95E to 5+10E a garnet-mica schist resembling the foot wall garnet schist was observed.

Whole rock analyses of the units uncovered on Line 20+00S are displayed along with analyses of the dolomite zone and selected hanging wall and foot wall lithologies from the Canyon Showing, the North Road trenches and the Cominco drill core (Table 4). The chemical similarities of the lithologies substantiate the continuity and extent of the sulphide associated units throughout the areas investigated.

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|        | LOCATION                              | SAMPLE NO. | ROCK TYPE           | SIO2  | Fe2O3 | A12O3 | BaO  | P2O5 | MnO  | MgO   | CaO   | 7102 | N#2O3 | к20               |
|--------|---------------------------------------|------------|---------------------|-------|-------|-------|------|------|------|-------|-------|------|-------|-------------------|
|        |                                       |            |                     |       |       |       |      |      |      |       |       |      |       |                   |
|        | DDH-C-91-2 @223m                      | 34089      | Lg. garnet schst    | 43.44 | 6.57  | 20.92 | 0.16 | 0.13 | 0.13 | 2.51  | 11.8  | 0.71 | 0.79  | 4.09              |
|        | Cummins R. north side                 | 34081      | Limy garnet schst   | 40.54 | 5.55  | 14.89 | 0.06 | 0.09 | 0.05 | 3.45  | 17.9  | 0.47 | 0.6   | 2.33              |
|        |                                       |            |                     |       |       |       |      |      |      |       |       |      |       |                   |
| - Guid | Line 20+005 4+10E                     | 34065      | Otz-ser schst       | 83.33 | 3.27  | 7.05  | 0.06 | 0.4  | 0.18 | 0.36  | 0.92  | 0.71 | 0.12  | 2.25              |
|        | DDH-C-91-2 @245m                      | 34071      | Qtz-ser schst       | 81.21 | 1.71  | 8.01  | 0.1  | 0.05 | 0.18 | 0.98  | 1.82  | 0.63 | 0.18  | 2.27              |
| _      | Cummins R. south side                 | 34073      | Qtz-ser schist      | 82.64 | 0.87  | 9.99  | 0.18 | 0.16 | 0.08 | 0.34  | 0.61  | 0.33 | 0.21  | 2.76              |
|        | Cummins R. north side                 | 34077      | Qtz-ser schist      | 88.21 | 1.67  | 5.3   | 0.08 | 0.21 | 0.04 | 0.25  | 0.72  | 0.41 | 0.12  | 1.44              |
| Zone   | North road showing                    | 34093      | Qtz-ser schist      | 83.49 | 2.08  | 7.71  | 0.09 | 0.19 | 0.26 | 0.55  | 0.63  | 0.61 | 0.23  | 2.23              |
|        | · · · · · · · · · · · · · · · · · · · |            |                     |       |       |       |      |      |      |       |       |      |       |                   |
|        | DDH-C-91-2 @260m                      | 34090      | Light grey dolomite | 11.31 | 9.15  | 1.65  | 0.03 | 0.28 | 2.08 | 13.02 | 26.76 | 0.09 | 0.12  | 0.64              |
|        | Cummins R. south side                 | 34075      | Pyritic dolomite    | 17.2  | 9.08  | 1.76  | 0.04 | 0.07 | 2.2  | 11.48 | 23.33 | 0.09 | 0.11  | 0.5               |
| e      | North Rd, trench 1                    | 34085      | Choc br. dolomite   | 11.94 | 12.24 | 1.3   | 0.02 | 0.2  | 5.32 | 12.24 | 29.26 | 0.08 | 0.13  | 0.15              |
| •      | North Rd. trench 4                    | 34092      | Choc br. dolomite   | 8.66  | 18.25 | 1.41  | 0.02 | 0.12 | 5.14 | 1.5   | 33.61 | 0.06 | 0.24  | <sup>-</sup> 0.81 |
|        |                                       |            |                     |       |       |       |      |      |      |       |       |      |       |                   |
| otwali | Line 20+005 5+6.5E                    | 34070      | Garnet schist       | 56.39 | 8.95  | 22.33 | 0.09 | 0.14 | 0.12 | 1.86  | 1.02  | 0.86 | 0.98  | 4.17              |
|        | DDH-C-91-2 @264m                      | 34091      | Garnet schist       | 55.91 | 9.19  | 20.58 | 0.1  | 0.14 | 0.12 | 2.1   | 0.8   | 0.79 | 0.45  | 5.86              |
| L R    | Cummins R. south side                 | 34076      | Garnet schist       | 53.6  | 10.47 | 22.18 | 0.16 | 0.07 | 0.06 | 2.25  | 0.35  | 0.82 | 0.45  | 6.42              |
|        | Cummins R. north side                 | 34080      | Garnet schist       | 54,43 | 7.98  | 24.43 | 0.2  | 0.14 | 0.05 | 1.64  | 0.04  | 0.87 | 0.45  | 6.54              |

#### TABLE 4 WHOLE ROCK ANALYSIS OF HANGING AND FOOTWALL FOOTWALL LITHOLOGIES

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## 8. **GEOPHYSICS**

The HLEM survey succeeded in locating the surface trace of a conductive unit which, according to geological interpretation, could correlate to either the sulphide zone or to a geologic contact within close proximity to the zone.

The anomaly meanders sinuously across the grid from line 12+00 S, 5+75E to line 32+00S, 0+25W (Figure 18). The depth to the top of the conductive zone is shallow, likely covered only by overburden to a depth of less than 10 meters. Dip is close to vertical, consistent with a 60-70 degree dip to the southwest.

The anomaly generally appears thin and weak, however, two areas of specific interest are:

a) Line 22+00S, 4+75E to 5+00E; the anomaly is quite strong, with in-phase values of about 30%. It is also quite clean, with little surface noise to degrade width interpretation of 25 metres.

b) Line 30+00S, 1+25E to 0+25W; there is an anomalous signature with two possible interpretations. One is of two thin, vertical conductors located at 0+25W and 1+12E. Another is to view this 150 meter wide response as a flat lying conductor (due to coil separation less that conductor width).

Lines 4+00S and 6+00S did not show an anomalous response. Possible explanations for this lack of anomaly may be due to the lack of access near the top of these lines, or a local lack of mineralization in the dolomite zone.

Lines 8+00S and 10+00S were shortened due to the presence of a steep gully, possibly representing a cross fault in this area. These lines were not geophysically tested as they fell short of the projected target area.

A test line was run over a known showing to correlate geophysical response with geology. Two anomalous zones were located. The first correlates with a schistose zone while the second correlates with the surface expression of the known showing. It was not possible to cover the east positive shoulder of the showing anomaly because of the extremely steep terrain to the east, dropping into the Cummins River.

Unfortunately there is a gap in the data set, from the original test line to line 12+00S on the grid. It is postulated that the zone is located on the east side of the ridge across this distance. The slope in this area is extremely steep and coverage was not attempted.

For instrumentation and field technique refer to Appendix F.

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## 9. SOIL AND SILT GEOCHEMISTRY

Mattock soil sampling was carried out over the grid area. Sample interval was generally 50m or 25m where warranted. A total of 234 samples were collected and examined by 30 element (Ag, Al, As, B, Ba, Bi, Ca, Cd, Co, Cr, Cu, Fe, K, La, Mg, Mn, Mo, Na, Ni, P, Pb, Sb, Sn, Sr, Ti, U, V, W, Y, Zn) ICP analysis. Samples were collected from the 'B' horizon which generally occurred at a depth of 15 to 20cm. All analyses were conducted by Eco-Tech Laboratories in Kamloops, B.C. For a complete list of results see Appendix C for certificate of analyses. Analytical procedures are included in Appendix D.

Sample locations are shown on Figure 15 and geochemical results for zinc, lead and manganese are displayed on Figures 19, 20 and 21 respectively.

High concentrations of Pb, Zn and Mn are essentially coincident, however Mn values are typically higher and more widely dispersed.

Two major trends are noted: a) High concentrations of Zn and Pb with significant Mn occur from line 4+00S and 6+00S near station 5+00E; b) Significant concentrations of the three elements trend from 4+50E on line 20+00S southeast toward 0+50W on line 32+00S.

No apparent trends are observed for base metals or trace elements within the soil geochemistry from line 8+00S to 18+00S; an increased depth to the sulphide bearing dolomite horizon may be the cause.

Silt samples were collected from all accessible drainages across the property (Figure 13a & 13b). Geochemical results from the creek silt samples do not exhibit any high level enrichment of Zn or Pb. However, elevated Mn values occur near the upper Gog - lower Tsar Creek contact.

Factors which may have effected the silt sample results include coarse particle size, depth to the mineralized horizon and sample technique (moss mat sampling may have been more effective).

For a complete list of soil and silt geochemical results see Appendix C.

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#### 10. DISCUSSIONS

The sulphide horizon and host lithologies are indicative of a platform-margin sedimentary exhalative deposit type. Such deposits occur in basins seaward of major platforms or cratonic shelves (Morganti 1981). A relatively simple sulphide mineralogy, low barite content and no copper zones are among the characteristics of the platformmargin 'sedex' deposits. Occurrences of this type (ie. Anvil, Howard Pass Deposit) within the Selwyn Basin vary in age from Cambrian to Mississippian, with Ba poor, Pb-Zn rich mineralization occurring within Cambrian to Silurian rocks (Maynard 1991).

Lithologies and lithogeochemistry indicate a depositional environment within a foreland basin or continental (half-graben) margin. The Tsar Creek Formation appears to be a product of an episodic (orogenic?) influx of pelitic material into a quiescent deep water calcareous-chert basin (Gog Group lithologies). Cessation of pelitic deposition gave way to a carbonate platform environment of thinly bedded turbidic limestones and interdepositional muds of the Kinbasket Formation.

Tsar Creek sediments associated with the sulphide horizon reflect a persistent low-energy environment or 'autochthonous' lithologies (after Large 1980). Autochthonous lithologies are usually comprised of fine grained clastics (shales and siltstones) and/or limestones and dolomites. The hanging wall siliceous pyrite and Quartz-sericite schist horizons are interpreted by the authors to have been originally chert horizons. Chert has been shown to be spatially associated with several 'sedex' deposits (Large 1980) and is considered a exhalative silica phase related to the ore forming hydrothermal activity. Graphite, observed on foliation planes within the MGM quartz-sericite schists may have derived from original organic carbon. The presence of carbon has been observed within several 'sedex' deposits and is interpreted to be indicative of a chemically reducing environment in which stratiform sulphides remain stable (Large 1983).

Analogies can be made between the sequence of lithologies observed bounding the MGM sulphide horizon and those of the Selwyn Basin deposits. In the Anvil district, ore is located at the transition from noncalcareous phyllite to overlying calcareous phyllite. Whole rock analysis of MGM rock types indicate hanging wall garnet schists possess a much greater carbonate content than foot wall garnet schists (see Figure 15a & Table 4). The local sequence of quartz-sericite schists above and argillaceous garnet schists below the MGM sulphide horizon correspond well with the chert horizons above and the pyritic shales below the Pb-Zn rich, Ba poor massive sulphides of the Howards Pass deposit.

Typically, the characteristic geologic features of "sedex" deposits include extensive length and breadth dimensions with relatively narrow widths. The economic sections of the Howard Pass deposits, for example, are limited to sub-basins within the platform-slope basin (Figures 22a & 22b), where metal bearing precipitates accumulated.



General model for the formation of the platform-marginal deposits showing the geometry of the platform-slope-base of slope and chert basin facies. Arrows show surface movement of ore fluids which migrate up to the sediment-water interface, down the basin slope and are trapped in the sub-basins at the base of the slope.

FIGURE 22a



Composite stratigraphic sections of the Howards Pass Formation across the base of slope facies. These sections show a general thickening of the Formation and the presence of the Zn-Pb containing active member in the sub-basins. Distance between sections A and E is approximately 8 km.

FIGURE 22b

Multiple phases of deformation within the MGM area have been essentially coaxial and have not interrupted the stratigraphic sequence. Chemical similarities observed from whole rock analyses of the dolomite zone and selected hanging wall and foot wall lithologies over several kilometres attest to the continuity of the stratigraphic succession. However, tight to isoclinal folding within the Chancellor Group has produced substantial structural thickening of the Kinbasket and Tsar Creek Formations (Meilliez 1972).

To date, thickness and grade of mineralization have been subeconomic. Locating tectonically thickened sections and/or sub-basins within the Tsar Creek Formation could produce economic widths and grades of sulphide mineralization.

The recognition of geochemical halos within host rocks of the sulphide horizon is of exploration significance. Manganese is enriched in carbonates that are at the same stratigraphic horizon as the stratiform sulphides at the Meggan (Germany), McArthur River (Australia) and Tynagh (Ireland) deposits (Large 1983). Similarily, the MGM dolomite horizon displays high Mn values (2.1%-5.3%) compared to Mn concentrations (0.05%-0.18%) within adjacent hanging and foot wall lithologies. Typically, over the dolomite horizon, the abundance of Mn within soils is much greater than that of Zn or Pb. It is this characteristic feature that would prove manganese a key 'tracer' element for defining the MGM sulphide-bearing dolomite horizon throughout the property.

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## 11. CONCLUSIONS

Regionally, the property lies on the west limb of a major anticlinorium and is bounded to the west by the Purcell Thrust Fault. Lithologies of the Kinbasket and Tsar Creek Formations generally strike northwest-southeast and dip 50°-60° southwest in the area between Cummins River and Tsar Creek. A thrust fault bounded sequence of similar lithologies occurs mainly north of the Cummins River, with a portion occurring south of the Cummins terminating at the Columbia Reach.

The dominant structures within the Kinbasket and Tsar Creek Formations are the second phase  $(F_2)$  tight to isoclinal asymmetric step-like folds with an associated axial planar cleavage  $(S_2)$  sub-parallel to the average long limb orientation.

The Tsar Creek Formation hosts a crudely stratabound sulphide horizon of variable width bounded by distinct hanging and foot wall lithologies. Sulphide mineralogy is predominantly pyrite, sphalerite and galena. Sediments hosting the sulphide layer were cherts, carbonates and argillites deposited within an unstable cratonic margin basin of early Paleozoic North America.

Whole rock geochemical analyses of hanging wall and foot wall lithologies have displayed the integrity and extent of the sulphide associated horizons across the property.

A distinct physical correlation exists between the enriched soil locations and the EM anomalies from line 20+00S to line 32+00S; the geophysical anomalies occur upslope of the higher concentrations of Zn, Pb and Mn.

Combined data from geophysical, soil geochemistry and whole rock surveys indicate that the sulphide-bearing dolomite horizon is continuous from the Cummins River south to at least Line 20+00S, a strike length of 3 kilometres.

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# APPENDIX A

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**Statement of Qualifications** 

I, Greg Thomson, do hereby certify that:

- 1. I am currently employed as a geologist by Teck Explorations Ltd. with offices at #960-175 Second Ave., Kamloops, B.C.
- 2. I graduated from the University of British Columbia in 1970 with a major in Geology.
- 3. I have worked continuously as a geologist in British Columbia.
- 4. The work described herein was done under my direct supervision.
- 5. I hold no personal interest, direct or indirect in the MGM Property which is the subject of this report.

J.K. Manion

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Greg Thomson Geologist November, 1991

I, Craig Alford, do hereby certify that:

- 1. I am a geologist and have practised my profession continuously since graduation.
- 2. I graduated in 1988 from Lakehead University with a M.Sc. in Geology.
- 3. I was actively involved in the mapping of the MGM Property and co-authored the report contained herein.
- 4. All data contained within this report and conclusions drawn from it are true and accurate to the best of my knowledge.
- 5. I hold no personal interest, direct or indirect in the MGM Property which is the subject of this report.

Craig (l)

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Craig Alford Geologist November, 1991

# APPENDIX B

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**Cost Statement** 

# MGM PROJECT EXPLORATION COSTS (June 1 - Sept 30/91)

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# A) SALARIES

B)

C)

D)

| G. Thomson (Project Geologist)<br>82 days @ \$271.92/day         | 24,200.80               |                     |
|--|-------------------------|---------------------|
| C. Alford (Geologist)<br>90 days @ \$232.00/day                  | 20,880.00               |                     |
| D. Nikirk (Field Technician)<br>42 days @ \$181.25/day           | 7,612.50                |                     |
| H. Stewart (Geological Assistant)<br>41 days @ \$181.25/day      | 7,431.25                |                     |
| B. Miller (Field Assistant)<br>53 days @ \$166.75/day            | 8,837.75                |                     |
|  | Subtotal                | \$68,962.30         |
| Supervision  | 1,073.23                |                     |
| Administration   | 119.25                  |                     |
| Miscellaneous  | 3,727.49                |                     |
|  | Total Salaries          | \$73,882.27         |
| LIVING EXPENSES  |                         |                     |
| -Camp rental (@ \$3000/month), and misc. motel and restaurant co | fuel, groceries<br>osts | <b>\$2</b> 1,864.91 |
| TRANSPORTATION   |                         |                     |
| -Rental of two 4x4 trucks, gasolin<br>Mica Marine Barge          | e and                   | \$13,839.37         |
| CHARTERED AIRCRAFT   |                         |                     |
| -Amiskwi Air & Canadian Helico                                   | pters                   | \$11,199.73         |

# E) CONTRACTORS

|    | <ol> <li>Geophysics - 11Km. HLEM Survey<br/>Maple Services Ltd.</li> <li>Linecutting - 10.5Km.<br/>Minconsult Mineral Exploration Services<br/>(Assessment fees allocated to MGM 8 claims)</li> <li>Trenching<br/>Minconsult Mineral Exploration Services</li> </ol>                            | \$12,444.70<br>21,892.11<br>-9,760.00<br>12,132.11<br>5,152.00 |             |
|----|---|--|-------------|
|    | Contractor tota   | Ì  | \$29,728.81 |
| F) | GEOCHEMICAL ASSAYS  |  |             |
|    | <ol> <li>Echo Tech Labs         <ol> <li>232 Soils (31 el. ICP) x \$6.19 ea.</li> <li>49 Silt (30 el. ICP) x \$6.19 ea.</li> <li>24 Rock (Whole rock analysis) x \$25.38 ea</li> <li>11 Rock (30 el. ICP) x \$8.80 ea.</li> <li>4 Rock (Pb, Zn &amp; Ag Assay) x \$20.47</li> </ol> </li> </ol> | \$1436.08<br>303.31<br>609.17<br>96.80<br>81.88                |             |
|    | Geochemical total   |  | \$2,527.24  |
| G) | FIELD EXPLORATION COSTS   |  | \$1,103.17  |
| H) | FREIGHT & SHIPPING  |  | \$685.07    |
| I) | MAPS & PRINTS   |  | \$627.06    |
| J) | DRAFTING  |  | \$2,124.67  |
| K) | TELEPHONE   |  | \$310.24    |
| L) | EQUIPMENT RENTAL  |  |             |
|    | -Camp Generator & Radio Telephone   |  | \$3,665.17  |

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Total

\$161,557.71

# APPENDIX C

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Certificate of Analysis

ROCK

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10041 EAST TRANS CANADA WWY. RANLOOPS, B.C. V2C 2J3 PHONE - 604-573-5700 PAX - 604-573-4557 TECK EXPLORATIONS LTD. - ETK 91-457

960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5V1

ATTENTION: PRED DALEY

AUGUST 1, 1991

VALUES IN PPM UNLESS OTHERWISE REPORTED

PROJECT NUMBER: 1703 2 ROCK SAMPLES RECEIVED JULY 16, 1991

| BTI        | DESCRIPTION | <b>A</b> G | AL(1) | 72     | 8      | 81 | DE C | C1(1) | CD | CO | CR  | CU    | <b>FR(</b> \) | K(%) | LA NG | 5( <b>1</b> ) | KW   | HO NA(\$)          | <b>HE</b> | 8      | <b>PB</b> | 88  | <b>S H</b> | SR TI(%)   | U    | T  | T   | T          | Z     |
|------------|-------------|------------|-------|--------|--------|----|------|-------|----|----|-----|-------|---------------|------|-------|---------------|------|--------------------|-----------|--------|-----------|-----|------------|------------|------|----|-----|------------|-------|
| 3232333222 |             |            |       | 373222 | 222222 |    |      |       |    |    |     | 28322 | 2222223       |      |       |               |      | ================== | *******   | ****** | 122222    |     |            | ********** |      |    |     |            | ***** |
| 1 -        | 33855       | .2         | .1#   | 55     | 6      | 10 | < 5  | . 22  | a  | 2  | 123 | 10    | 1.02          | .#5  | 20    | .03           | 524  | 8 < .01            | 5         | 500    | 14        | < 5 | < 20       | 7 < .01    | < 10 | <1 | 110 | 6          | 321   |
| 2 -        | 33856       | 7.0        | .#    | 65     | 2      | 88 | < 5  | ) 15  | 18 | 6  | 12  | 9     | 5.04          | .17  | I     | 1.43 > 1      | 0000 | (1(.01             | 2         | 330    | 1978      | 15  | < 28       | (1.02      | 30   | <1 | (1) | <b>d</b> ( | 6056  |

NOTE: < = LESS THAN > = GREATER THAN

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ECO-TECH LABORATORIES LTD. CLINTON AYERS LABORATORY NANAGER

SC91/TECK1



ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamioops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

JULY 30, 1991

CERTIFICATE OF ANALYSIS ETK 91-458

TECK EXPLORATION LTD. 960 - 175 2ND AVENUE KAMLOOPS, B.C. V2C 5W1

ATTENTION: FRED DALEY

SAMPLE IDENTIFICATION: 2 ROCK samples received JULY 16, 1991 PROJECT: 1703

| BT#        | Description    | BaO        | P205       | SiO2           | MnO | Fe203          | MgO          | A1203          | Ca0          | Ti02       | Na02       | K20 L | .0.I.        |
|------------|----------------|------------|------------|----------------|-----|----------------|--------------|----------------|--------------|------------|------------|-------|--------------|
| 1 -<br>2 - | TG -1<br>CG -1 | .02<br>.03 | .06<br>.12 | 41.25<br>38.51 | .42 | 30.21<br>31.32 | 2.34<br>2.05 | 18.61<br>19.08 | 5.51<br>7.90 | .44<br>.63 | .10<br>.07 | .08   | <.01<br><.01 |

NOTE: VALUES EXPRESSED IN PERCENT

SC91/TECK3

ECO-TECH LABORATORIES LTD. FRANK J. PEZZOTTI B.C. CERTIFIED ASSAYER

10041 EAST TRANS CANADA NUT. RANLOOPS, B.C. V2C 2J3 PHONE - 604-573-5706 PAX - 604-573-4557 TECK EXPLORATIONS LTD. - ETK 91-376

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968, 175 SECOUD AVENUE Kahloops, B.C. V2C SV1

JULY 3, 1991

VALUES IN PPH UNLESS OTHERWISE REPORTED

ATTENTION: FRED DALEY

PROJECT HUNBER: 1783 1 ROCK SAMPLE RECEIVED JUNE 24, 1991

| RT j      | DESCRIPTION | 1G  | AL(1)    | 15 | Ð | 81 | 81 CA(%) | CD     | CO | CR  | CU FE(1) | K(%) | LA NG(N) | KN   | HO NA(N) | ) HE    | Ł      | <b>PB</b> | SB     | SM     | SR TI(V) | U   | ۷           | ¥               | T           | 11         |
|-----------|-------------|-----|----------|----|---|----|----------|--------|----|-----|----------|------|----------|------|----------|---------|--------|-----------|--------|--------|----------|-----|-------------|-----------------|-------------|------------|
| ********* |             |     | ******** |    |   |    |          | ****** |    |     |          |      |          |      |          | ******* | S32223 |           | ****** | 322222 | 144 / 41 | /18 | 252222<br>9 | (\$32222<br>/14 | 222223<br>C | :===<br>36 |
| 1 -       | 34051       | 1.3 | 2 .03    | 5  | 2 | 5  | (5 1.73  | a      | 4  | 164 | 32 5.00  | .01  | (10 5.31 | 2458 | 6.07     | 19      | 11     | 124       | G      | (20    | 106 (.01 | CT. | 1           | CI.             | •           | 13         |

NOTE: < = LESS THAN

ECO-TECE LABORATORIES LTD. FRANK J. PRIIOTTI

B.C. CERTIFIED ASSATER

SCS/TECE2

10041 ELST TEAMS CLEADA SUT. EANLOOPS, B.C. V2C 233 PROME - 604-573-5780 PAX - 604-573-4557

## TECK EXPLORATIONS LTD. - BTK 91-447

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2

960, 175 SECOND AVENUE EANLOOPS, B.C. V2C 501

ATTENTION: FRED DALET

VALUES IN PPH UNLESS OTHERVISE REPORTED

PROJECT HUNBER: 1703 1 ROCK SAMPLE RECEIVED JULY 10, 1991

| ET F     | DESCRIPTION | 16 1L(1)    | 12     | 1     | 81    | BE CL(N)    | CĐ    | <b>C0</b> | (I | CU FE(N)   | <b>X(1)</b> | LA NG(N)    | 10      | MO H1(1)  | 11 | 2      | <b>?</b> # | 58    | <b>5 F</b> | SR TI(X)  | ŧ       | 1     | T      | T      | 11    |
|----------|-------------|-------------|--------|-------|-------|-------------|-------|-----------|----|------------|-------------|-------------|---------|-----------|----|--------|------------|-------|------------|-----------|---------|-------|--------|--------|-------|
| ******** |             | *********** | ****** | ***** | ***** | *********** | ***** |           |    | ********** | *******     | *********** | ******* | ********* |    | ****** | ******     | ***** | ******     |           | ******* | ***** | ****** | ****** | ***** |
| 1 -      | 34852       | (.2 1.88    | (5     | 4     | 25    | (5 12.53    | a     | 10        | 22 | 18 2.29    | .87         | 20 1.38     | 255     | <1 (0.01  | 15 | 250    | 1          | 5     | (28        | 166 (0.01 | (18     | 3     | (1)    | 4      | 61    |

SOTE: < = LESS THAN

JULY 20, 1991

RCO-TECH LINORATORIES LTD. PRINE J. PRINOTTI B.C. CRETIFIED ANNYER

TECE 3/SCS



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# ECO-TECH LABORATORIES LTD.

ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamloops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

AUGUST 21, 1991

CERTIFICATE OF ASSAY ETK 91-580

TECK EXPLORATION LTD. 960 - 175 2nd. AVE. KAMLOOPS, B.C. V2C 5W1

ATTENTION: FRED DALEY

| SAMPLE IDENTIFICATION:                   | 2 ROCK SAMPLES | RECEIVED | AUGUST 2 | , 1991 |
|--|----------------|----------|----------|--------|
| الله هي الله الله الله الله الله الله ال | PROJECT: 1709  |          |          |        |
|  |                |          |          |        |

|     |             | PB  | ZN    |
|-----|-------------|-----|-------|
| ET# | Description | (%) | (%)   |
|     |             |     | ===== |
| 1 - | 34062       | .04 | .02   |

ECO-TECH LABORATORIES LTD FRANK J. PEZZOTTI B.C. CERTIFIED ASSAYER

PHONE - 604-573-5700 V2C 5W1 FAX - 604-573-4557 SEPTEMBER 10 , 1991 ATTENTION: FRED DALEY VALUES IN PPN UNLESS OTHERWISE REPORTED PROJECT NUMBER: 1703 2 ROCK SAMPLES RECEIVED AUGUST 2, 1991 RT# DESCRIPTION AG AL(1) λS BR BI CA(1) CD CO CR CU PE(8) X(8) LA HG(1) 101 HO NA(\$) NI PB SB SR TI(A) U v ZN. ₽ SN 사 목록 부모는 것 같은 것 또 수 부장은 수 위장 중도 가 안 의 것 같은 것 것 같 것 이 것 1 - 34062 9 .94 .01 10 .07 94 18 <.01 11 1100 322 <5 <20 11 <.01 <10

TECK EXPLORATIONS LTD. - ETK 91-580

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960, 175 SECOND AVENUE

KANLOOPS, B.C.

NOTE: < - LESS TRAN

ECO-TECH LABORATORIES LTD.

KANLOOPS, B.C. V2C 2J3

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<5 . 29 <1

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10041 BAST TRANS CANADA HWY.

TECK3/8C5

BCO-TECH LABORATORIES LTD. Frank J. Persotti, A.Sc.T. B.C. Certified Assayer



ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamboops, B.C. V2C 2J3<sup>4</sup> (604) 573-5700 Fax 573-4557

AUGUST 19, 1991

CERTIFICATE OF ANALYSIS ETK 91-580

TECK EXPLORATION LTD. 960-175 2ND AVE. KAMLOOPS, B.C. V2C 5W1

SAMPLE IDENTIFICATION: 2 ROCK samples received AUGUST 2, 1991 PROJECT: 1703

| ET# | Description | BaO | P205   | SiO2   | MnO  | Fe203 | MgO    | A1203 | CaO   | Tio2  | NaO2 | K20  | L.O.I.  |
|-----|-------------|-----|--------|--------|------|-------|--------|-------|-------|-------|------|------|---------|
|     |             |     | 232222 | ****** | **** |       | 222222 |       | ===== | ***** |      |      | ******* |
| 2-  | 34063       | .04 | .13    | 50.20  | .22  | 18.35 | 3.03   | 22.14 | 2.73  | .69   | .46  | 2.16 | .3ť     |
|     |             |     |        |        |      |       |        |       |       |       |      |      |         |
|     |             |     |        |        |      |       |        |       |       |       |      |      |         |

NOTE: VALUES EXPRESSED IN PERCENT

SC91/TECK 4

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ECO-TECH LABORATORIES LTD. FRANK J. PEZZOTTI B.C. CERTIFIED ASSAYER ECO-TECH LABORATORIES LID. 10041 EAST TRANS CANADA HWY. KANLOOPS, B.C. V2C 2J3 PHONE - 573-5700 FAX - 573-4557

#### AUGUST 27, 1991

VALUES IN PPH UNLESS OTHERWISE REPORTED

TECK EXPLORATIONS LTD.- ETK 91-601 960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5W1

ATTENTION: FRED DALEY

PROJECT NUMBER: 1703 SAMPLE DESCRIPTION: 1 ROCK SAMPLES RECEIVED AUGUST 8 ,1991

| RT# | DESCRIPTION | AG        | AL(1) | λ <b>S</b> | в | BA                         | BI C            | CA(4) | œ  | <b>co</b> | CR  | CU | PE(\) | K(%) | LA NO | i(t) | KOL  | NO NA(\$)                       | WI  | P   | PB | 5B | 6 <b>X</b> | 6R | TI( <b>%</b> ) | U    | v  | W      | ¥     | <b>8</b> 36 |
|-----|-------------|-----------|-------|------------|---|----------------------------|-----------------|-------|----|-----------|-----|----|-------|------|-------|------|------|---------------------------------|-----|-----|----|----|------------|----|----------------|------|----|--------|-------|-------------|
|     |             | د د د ک ت |       | ******     |   | 1924-1925 in 1927 für 1920 | و م بو بو بو بو |       |    |           |     |    |       |      |       |      |      | 4 ه و و 4 ه و و و 5 او او او او |     |     |    |    | *****      |    |                | **** |    | ****** | ***** |             |
| 1-  | 34064       | .6        | .14   | 10         | 6 | 60                         | <5              | 3.21  | <1 | 6         | 100 | 2  | 4.50  | .04  | 10    | . 59 | 7249 | 5 <.01                          | 1 1 | 200 | <2 | <5 | <20        | 40 | <.01           | 10   | <1 | <10    | 10    | 63          |

ECO-TECH LABORATORIES LTD. CLINTON AVENS LABORATORY MANAGER



ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamioops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

SEPTEMBER 20,1991

## CERTIFICATE OF ASSAY ETK 91-723W

وجرعا بعانت بتدريدها فتاقات

TECK EXPLORATION LTD. 960 - 175 2nd. AVE. KAMLOOPS, B.C. V2C 5W1

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ATTENTION: FRED DALEY

SAMPLE IDENTIFICATION: 27 ROCK SAMPLES RECEIVED SEPTEMBER 4, 1991 ------PROJECT: 1703

| BT <b>\$</b> |   | Description | BaO | P205 | S102  | MnO  | Fe203 | MgO   | A1203 | СаО   | TiO2 | Na2O | <b>K</b> 20 | L.O.I. |
|--------------|---|-------------|-----|------|-------|------|-------|-------|-------|-------|------|------|-------------|--------|
| 1            | - | 34065       | .06 | .40  | 83.33 | .18  | 3.27  | .36   | 7.05  | .92   | .71  | .12  | 2.25        | 1.38   |
| 2            | - | 34066       | .06 | .64  | 89.81 | .01  | .72   | .12   | 5.02  | .75   | .45  | .06  | 1.43        | .83    |
| 3            | - | 34067       | .02 | . 47 | 85.82 | .82  | 4.13  | .10   | 1.96  | 2.82  | .32  | .05  | .29         | 3.22   |
| 4            | - | 34068       | .22 | .07  | 73.93 | .31  | 3.42  | .57   | 13.82 | .67   | .80  | .20  | 3.79        | 2.11   |
| 5            | - | 34069       | .06 | .34  | 90.19 | 09   | 2.86  | .10   | 3.15  | .55   | .35  | .12  | .99         | 1.21   |
| 6            | - | 34070       | .09 | .14  | 56.39 | .12  | 8.95  | 1.86  | 22.33 | 1.02  | .86  | .98  | 4.17        | 3.16   |
| 7            | - | 34071       | .10 | .05  | 81.21 | .18  | 1.71  | .98   | 8.01  | 1.82  | .63  | .18  | 2.27        | 2.74   |
| 8            | - | 34072       | .01 | .11  | 34.29 | 2.28 | 9.01  | 6.99  | 1.14  | 19.65 | .12  | .15  | .31         | 25.96  |
| 9            |   | 34073       | .18 | .16  | 82.64 | .08  | .87   | .34   | 9.99  | .61   | .33  | .21  | 2.76        | 1.94   |
| 10           | - | 34074       | .03 | .41  | 41.04 | 3.26 | 35.36 | 2.82  | 1.89  | 1.17  | .07  | .34  | .45         | 13.14  |
| 11           | - | 34075       | .04 | .07  | 17.20 | 2.20 | 9.08  | 11.48 | 1.76  | 23.33 | .09  | .11  | .50         | 34.18  |
| 12           | - | 34076       | .16 | .07  | 53.60 | .06  | 10.47 | 2.25  | 22.18 | .35   | .82  | .45  | 6.42        | 2.98   |
| 13           | - | 34077       | .08 | .21  | 88.21 | .04  | 1.67  | .25   | 5.30  | .72   | .41  | .12  | 1.44        | 1.43   |
| 14           | - | 34078       | .06 | .42  | 64.22 | .33  | 19.50 | .58   | 2.52  | 1.21  | .14  | .36  | .75         | 9.83   |
| 15           | - | 34079       | .09 | .14  | 71.83 | .25  | 9.80  | 1.21  | 8.52  | 1.41  | .49  | .27  | 2.07        | 3.89   |
| 16           | - | 34080       | .20 | .14  | 54.43 | .05  | 7.98  | 1.64  | 24.43 | .04   | .87  | .45  | 6.54        | 3.01   |
| 17           | - | 34081       | .06 | .09  | 40.54 | .05  | 5.55  | 3.45  | 14.89 | 17.90 | .47  | .60  | 2.33        | 14.20  |
| 18           | - | 34082       | .01 | .17  | 17.55 | 1.91 | 64.41 | 3.69  | 1.09  | .47   | .08  | .61  | .11         | 9.94   |
| 19           | - | 34083       | .02 | .17  | 88.36 | .17  | 3.66  | .22   | 3.84  | .38   | .40  | .07  | .97         | 1.67   |
| 20           | - | 34084       | .07 | .71  | 51.62 | .91  | 6.21  | .58   | 5.65  | 18.86 | .30  | .22  | 1.44        | 13.05  |
| 21           | - | 34085       | .02 | .20  | 11.94 | 5.32 | 12.24 | 7.07  | 1.30  | 29.26 | .08  | .13  | .15         | 32.25  |
| 25           | - | 34089       | .16 | .13  | 43.44 | .13  | 6.57  | 2.51  | 20.92 | 11.80 | .71  | .79  | 4.09        | 7.80   |
| 26           |   | 34090       | .03 | .28  | 11.31 | 2.08 | 9.15  | 13.02 | 1.65  | 26.76 | .09  | .12  | .64         | 34.78  |
| 27           | - | 34091       | .10 | .14  | 55.91 | .12  | 9.19  | 2.10  | 20.58 | .80   | .79  | .45  | 5.86        | 2.68   |

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PSC-TECH LABORATORIES LTD. FRANK J. PEZTOTTI, A.Sc.T. B.C. Certified Assayer



ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamioops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

SEPTEMBER 20, 1991

CERTIFICATE OF ASSAY ETK 91-723

TECK EXPLORATION LTD. 960 - 175 2nd. AVE. KAMLOOPS, B.C. V2C 5W1

ATTENTION: FRED DALEY

SAMPLE IDENTIFICATION: 27 ROCK SAMPLES RECEIVED SEPTEMBER 4, 1991

| ET#  | Description | AG<br>(g/t) | AG<br>(oz/t) | PB<br>(%) | 2N<br>(%) |  |
|------|-------------|-------------|--------------|-----------|-----------|--|
| 22 - | 34086       | 24.4        | .71          | .76       | .02       |  |
| 23 - | 34087       | 2.4         | .07          | .12       | .13       |  |
| 24 - | 34088       | 1.2         | .04          | .10       | .55       |  |

ECO-TECH LABORATORIES LTD. PGFRANK J. PEZZOTTI, A.Sc.T B.C. Cetified Assayer ВСО-ТЕСН LABORATORIKS LTD. 10041 EAST TRANS CANADA HWY. Камьоря, B.C. V2C 2J3 Phone — 604-573-5700 FAX — 604-573-4557 TECK EXPLORATIONS LTD.- ETK 91-723 960, 175 BECOND AVENUE KANLOOPS, B.C. V2C 5W1

ATTENTION: FRED DALEY

VALUES IN PPM UNLESS OTRERWISE REPORTED

PROJECT NUMBER: 1703 27 Rock Samples received September 3, 1991

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| et# | DESCRIPTION | ÀG ÀL(8 | )   | λ <b>8</b> | B | BA | BI CA(S | ) ( | CD | co | CR | CU 7 | Z(\$) | K(1) | LA  | HG(1) | KH   | NOI | HA(\) | NI | 7    | PB   | 88 | 8¥  | SR  | TI(\$) | U   | v  | W   | ¥   | 21:  |
|-----|-------------|---------|-----|------------|---|----|---------|-----|----|----|----|------|-------|------|-----|-------|------|-----|-------|----|------|------|----|-----|-----|--------|-----|----|-----|-----|------|
| 22~ | 34086       | 20.6 .0 | 5 4 | 84         | 4 | 5  | <5.2    | 7   | 1  | 3  | 78 | 1    | 5.44  | .05  | <10 | .03   | 459  | 3   | .04   | 8  | 200  | 7290 | 30 | <20 | 9   | <.01   | 10  | 6  | <10 | <1  | 233  |
| 23- | 34087       | 3.0 .0  | 3 3 | 47         | 4 | <5 | <5 8.4  | 5   | 2  | <1 | 23 | <1   | 5.56  | .03  | <10 | 3.56  | 1838 | 5   | .04   | 12 | 400  | 1016 | 15 | <20 | 63  | <.01   | 40  | ,  | 30  | 2 1 | 074  |
| 24- | 34068       | 2.4 .1  | 6   | 31         | 2 | 40 | <5 13.5 | 7   | 9  | 4  | 13 | 1 :  | 5.52  | .07  | <10 | 7.03  | 1871 | 7   | .04   | Э  | 1010 | 904  | 5  | <20 | 158 | .01    | <10 | 12 | 90  | 64  | 60 J |

NOTE: < = LESS TRAN

SEPTEMBER 20,1991

TECK3/BC5

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ECO-TECH LABOR TORIES LTD. PLC FRANK J. PERFOTTI B.C. CERTIFIED ASSAYER



ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamioops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

SEPTEMBER 25,1991

## CERTIFICATE OF ASSAY ETK 91-749

TECX EXPLORATION LTD. 960 - 175 2nd. AVE. KAMLOOPS, B.C. V2C 5W1

ATTENTION: FRED DALEY

SAMPLE IDENTIFICATION: 3 ROCK SAMPLES RECEIVED SEPTEMBER 13, 1991 ------ PROJECT: 1703

| BT <b>†</b> | Description | BaO | P205 | SiO2  | MnO  | Fe203 | MgO  | A1203 | CaO   | TiO2 | Na2O | <b>K2O</b> | L.O.I.  |
|-------------|-------------|-----|------|-------|------|-------|------|-------|-------|------|------|------------|---------|
| 1 -         | 34092       | .02 | .12  | 8.66  | 5.14 | 18.25 | 1.50 | 1.41  | 33.61 | .06  | .24  | . 8        | 1 29.92 |
| 2 -         | 34093       | .09 | .19  | 83.49 | .26  | 2.08  | .55  | 7.71  | .63   | .61  | .23  | 2.2        | 3 1.602 |
| 3 -         | 34094       | .07 | .15  | 54.70 | .10  | 7.66  | 1.87 | 23.09 | 1.91  | .81  | .96  | 4.7        | 9 3.065 |

NOTE: < = less than

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ECO-TECH LABORATORIES LTD. CLINTON S. AVERS LABORATORY MANAGER

ECO-TECH LABORATORIES LTD. 10041 EAST TRANS CANADA HWY. KANLOOPS, B.C. V2C 2J3 PHONE - 604-573-5700 FAX - 604-573-4557

SEPTEMBER 25 ,1991

VALUES IN PPM UNLESS OTHERWISE REPORTED

TECK EXPLORATIONS LTD.- KTK 91-749 960, 175 SECOND AVENUE KAMLOOPS, B.C. V2C 5W1

PROJECT NUMBER: 1703 3 ROCE SAMPLES RECEIVED SEPTEMBER 13 ,1991 ۲

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| et <b>i</b> | DESCRIPTION | лg  | AL(%) | λs | B | BA  | BIC | CA(8) | CD | со | CR | CU | P#(%) | X(%) | ТА Н | G(1) | HAR    | но | NA(\$) | NI | P   | PB  | 88 | sn  | SR T | I(\$) | U  | v  | W   | ¥    | 2 N |
|-------------|-------------|-----|-------|----|---|-----|-----|-------|----|----|----|----|-------|------|------|------|--------|----|--------|----|-----|-----|----|-----|------|-------|----|----|-----|------|-----|
| 1 -         | 34092       | 4.2 | . 32  | 50 | 4 | 110 | <5  | >15   | 1  | 5  | 7  | 13 | 7.27  | . 12 | 10   | .72  | >10000 | 3  | <.01   | 4  | 300 | 190 | 15 | <20 | <1   | .02   | 20 | <1 | <10 | <1 1 | 495 |

NOTE: < = LESS THAN

ECO-TECE LABORATORIES LTD. PRANK J. PETROTTI B.C. CERTIFIED ASSAYER

TECK3/SC5

SOIL

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10041 EAST TEAMS CANADA HVT. KANLOOPS, D.C. V2C 2J3 PNONE - 604-573-5780 PAX - 604-573-4557

## TECK EXPLORATIONS LTD. - ETK 91-448

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960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5V1

ATTENTION: PRED DALET

### VALUES IN PPN UNLESS OTNERVISE REPORTED

PROJECT NUMBER: 1783 8 SOIL SAMPLES RECEIVED JULY 9, 1991

| BT E      | DESCRIPTION                             | AG AL(N)          | 15     | l     | n   | BI CI       | 1(1)   | CD | CO     | CR     | CU    | FE(\} | K(\$)  | <b>N</b> 1 | IG{\}  | **     | 80    | II {\} | #1 | Ł    | 23     | 53    | 51     | SE 1   | 11(1) | U      | T  | T           | t      | 12     |
|-----------|---|-------------------|--------|-------|-----|-------------|--------|----|--------|--------|-------|-------|--------|------------|--------|--------|-------|--------|----|------|--------|-------|--------|--------|-------|--------|----|-------------|--------|--------|
| 222222222 | *************************************** | ***************   | ****** | ***** |     | ******      | ****** |    | ****** | ****** | ***** | ***** | ****** | ******     | ****** |        | 3482X |        |    |      | ****** | ***** | ****** | ****** |       | ****** |    |             | ****** | ****** |
| 1 - 61    | L 888 8+ 88                             | <.2 3.2 <b>8</b>  | <5     | 10    | 75  | (5          | .31    | a  | 11     | 15     | 1     | 2.31  | .17    | (11        | .61    | 495    | (1    | .12    | 12 | 1410 | 10     | (5    | <28    | 23     | .13   | (11    | 26 | (1)         | 4      | 110    |
| 2 - 61    | 1 882 8+ 58 E                           | <.2 1.3 <b>5</b>  | 10     | 1     | 38  | <b>(5</b>   | .11    | 4  | 1      | 15     | - 5   | 1.66  | .12    | (1)        | .24    | 153    | 4     | .#3    | 9  | 238  | 6      | <5    | (28    | 16     | .#3   | (10    | 39 | <10         | 2      | 42     |
| 3 - 61    | 00x 1+ 00 x                             | K.2 3.98          | (5     | 1     | 85  | (5          | . 40   | (1 | 15     | 32     | 1     | 2.58  | .11    | (11        | .11    | \$25   | 4     | .14    | 28 | 788  | 14     | (5    | (28    | 32     | .15   | (1)    | 32 | (1)         | 3      | 13     |
| 4 - 61    | 00x 1+ 50 x                             | K.2 4.34          | (5     | 14    | 170 | (5          | .24    | 4  | 16     | 36     | 15    | 3.83  | .13    | (1)        | .62    | 1414 - | - (1  | .02    | 19 | 1100 | 14     | <5    | (28    | 19     | .11   | (1)    | 31 | (1)         | 4      | - 11   |
| 5 - 11    | 000 2+ 00 B                             | <b>(.2 3.22</b>   | 21     | 1     | 55  | (5 ]        | 1.20   | a  | 21     | 3      | 11    | 1.12  | .#1    | 10         | .34    | 532    | (1    | .11    | 21 | 1100 | 28     | (5    | (21    | 121    | .11   | (1)    | 2  | (1 <b>1</b> | 6      | 101    |
| 6 - 61    | 008 2+ 50 K                             | <b>(.2 1.14</b>   | 15     | 6     | 58  | <b>(5</b>   | .16    | 4  | 10     | 12     | 5     | 1.11  | .13    | (1)        | .24    | 955    | 4     | . 82   | 14 | 670  | 1      | (5    | (21    | - 14   | .11   | (16    | 35 | (10         | 2      | 50     |
| 1 - 11    | 00# 3+ 00 B                             | <.2 <b>4.55</b>   | 10     | 1     | 68  | (5          | .15    | (1 | 14     | 11     | 1     | 3.77  | .02    | (11        | .27    | 293    | a     | .12    | 15 | 588  | 28     | 5     | <20    | 10     | .13   | (10    | 11 | (10         | 1      | - 16   |
| 1 - 11    | 800 3+ 50 B                             | <.2 5. <b>8</b> 8 | <5     | 1     | 48  | <b>(5</b> ] | 1.53   | (1 | 21     | 47     | 11    | 4.58  | .11    | 10         | 1.01   | 236    | đ     | .16    | 46 | 698  | 28     | 10    | <20    | 120    | .11   | (10    | 23 | <1 <b>8</b> | 2      | 136    |

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HOTE: < = LESS THAN

JULY 26, 1991

TECE 3/SC5

BCO-TECH LABORATORIES LTD. PRANE J. PEIIOTTI B.C. CERTIFIED ASSAYER

## TECK EXPLORATIONS LTD. - ETK 91-522

#### ECO-TECH LABORATORIES LTD.

960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5W1

ATTENTION: PRED DALEY

10041 EAST TRANS CANADA HWY. KAMLOOPS, B.C. V2C 2J3 PHOME - 604-573-5700 PAX - 604-573-4557

AUGUST 6, 1991

## VALUES IN PPH UNLESS OTHERWISE REPORTED

PAGE 1

## PROJECT NUMBER: 1703

30 SOIL SAMPLES RECEIVED JULY 25, 1991

| 871  |            | DESCRIPTION |               | ¥C. | AL(\$) | 15 | 3  | 82  | BI   | C1(1) | CD           | CÛ | Ch   | CU   | PI(1) | X(1) | L   | HC(1) | XI   | NO           | NA(3) | #1   | P    | PB     | 58 | ST  | SR 1   | r1(\$) | ۵      | V    | W               | T            | 23  |
|------|------------|-------------|---------------|-----|--------|----|----|-----|------|-------|--------------|----|------|------|-------|------|-----|-------|------|--------------|-------|------|------|--------|----|-----|--------|--------|--------|------|-----------------|--------------|-----|
|      | ====       | *********** | ************* |     |        |    |    |     | :::: |       |              |    |      |      |       |      |     |       |      |              |       |      |      | ****** |    |     | ****** |        | ****** |      | ******          |              |     |
| 1 -  | 1          | 4 + 005 0   | + 00          | <.2 | 3.05   | 5  | 6  | 105 | <5   | .19   | 4            | 27 | - 41 | 29   | 5.56  | .05  | <10 | .1)   | 374  | 1            | .01   | - 44 | 650  | 24     | <5 | <20 | 15     | .05    | <10    | 28   | <10             | $\mathbf{d}$ | 108 |
| 2 -  | L          | 4 + 008 0   | + 50E         | <.2 | 2.79   | 5  | 10 | 105 | <5   | .13   | 4            | 23 | 21   | 15   | 3.98  | .13  | 10  | . 64  | 286  | - 4          | .01   | 37   | 650  | 28     | <5 | <20 | 15     | .06    | (10    | 16   | <10             | - d          | 80  |
| 3 -  | Ŀ          | 4 + 00S 1   | + 00E         | <.2 | 2.19   | <5 | 10 | 65  | <5   | .16   | $\mathbf{q}$ | 18 | 19   | 11   | 3.76  | .08  | <10 | .47   | 552  | - 4          | .01   | - 26 | 530  | 20     | 5  | <20 | 15     | .01    | <10    | 22   | <10             | q            | 69  |
| 4 -  | - <b>L</b> | 4 + 005 1   | + 50B         | <.2 | 1.35   | 5  | 6  | 75  | <5   | .08   | 4            | 13 | 18   | 10   | 3.57  | .08  | 10  | .36   | 462  | - 4          | .01   | 15   | 1710 | 16     | <5 | <20 | 11     | .06    | <10    | 22   | <10             | - e          | 54  |
| 5 -  | 1          | 4 + 00S 2   | + 00E         | .2  | 1.54   | <5 |    | 65  | <5   | .09   | <b>d</b>     | 14 | 22   | 11   | 4.16  | .10  | 10  | .41   | 418  | - <1         | .01   | 19   | 1000 | 16     | <5 | <20 | 12     | .04    | <10    | 20   | <10             | 4            | 58  |
| 6 -  | 1          | 4 + 005 2   | + 50E         | <.2 | . 64   | (5 | 6  | 30  | <5   | .07   | d            | 1  | 10   | 1    | 2.12  | .04  | 10  | .17   | 156  | $\mathbf{q}$ | .01   | •    | 660  | 18     | <5 | <20 | 6      | .08    | <10    | 29   | <10             | $\mathbf{q}$ | 33  |
| 1 -  | L          | 4 + 005 3   | + 00E         | <.2 | 1.85   | <5 | 1  | 45  | <5   | .18   | a            | 11 | 18   | - 14 | 4.49  | .01  | <10 | .25   | 220  | - 4          | .02   | 10   | 1200 | 30     | <5 | <20 | 12     | .17    | <10    | - 44 | <10             | $\mathbf{q}$ | 48  |
| 8 -  | L          | 4 + 005 3   | + 50E         | ٢.2 | 4.15   | 5  | 10 | 55  | <5   | .31   | a            | 32 | 13   | 31   | 1.12  | <.01 | <10 | .54   | 575  | 1            | .03   | - 46 | 1430 | 38     | 5  | <20 | 25     | .06    | <10    | 5    | <10             | 2            | 117 |
| 9 -  | L          | 4 + 005 4   | + 00E         | ٢.2 | 4.25   | 5  | 12 | 65  | <5   | .16   | 4            | 16 | 29   | - 14 | 4.03  | .02  | <10 | .35   | 585  | <1           | .02   | 19   | 970  | 32     | <5 | <20 | 10     | .14    | <10    | 26   | <10             | 2            | 83  |
| 10 - | 6          | 4 + 005 4   | + 50E         | ٢.2 | 1.71   | 5  | 1  | 35  | <5   | .08   | 4            | 14 | 26   | 18   | 5.09  | .08  | 10  | .51   | 214  | <1           | .01   | 23   | 790  | 16     | <5 | <20 | 9      | .06    | (10    | 22   | <10             | 4            | 47  |
| 11 - | 1          | 4 + 005 5   | + 00E         | <.2 | 3.67   | <5 | 8  | 55  | <5   | . 53  | 4            | 33 | 16   | 46   | 1.36  | .02  | <10 | .42   | 1108 | - (1         | .04   | 39   | 1050 | 30     | (5 | <20 | 33     | .03    | <10    | 3    | <10             | 2            | 87  |
| 12 - | 1          | 4 + 005 5   | + 50E         | .4  | . 88   | 10 | 4  | 30  | <5   | .06   | 4            | 10 | 8    | 19   | 5.04  | .03  | 20  | . 20  | 154  | - <1         | .01   | 21   | 1510 | 490    | <5 | <20 | 11     | .02    | <10    | 14   | <10             | 4            | 753 |
| 13 - | L          | 4 + 005 6   | + 00E         | ٢.2 | . 38   | <5 | 6  | 15  | <5   | .05   | - d          | 4  | 5    | 3    | 1.42  | .02  | <10 | .07   | 51   | d            | .01   | 2    | 250  | 18     | (5 | <20 | 5      | .11    | <10    | 34   | <10             | 1            | 31  |
| 14 - | L          | 4 + 005 6   | + 50E         | .1  | 4.13   | 5  | 6  | 55  | <5   | .07   | d            | 12 | 9    | 11   | 2.77  | .01  | <10 | .11   | 419  | 4            | .02   | 6    | 1160 | 26     | <5 | <20 | 5      | .15    | <10    | 21   | <10             | 4            | 42  |
| 15 - |            | 4 + 005 7   | + 00E         | <.2 | 3.72   | 5  | 10 | 110 | <5   | .18   | 4            | 16 | 26   | 10   | 6.80  | .19  | <10 | .31   | 474  | (1           | .01   | 9    | 4380 | 30     | <5 | <20 | 11     | . 29   | <10    | 11   | <10             | 4            | 68  |
| 16 - | 1          | 6 + 005 0   | + 00          | ٢.2 | 3.15   | 5  | 10 | 140 | (5   | . 52  | a            | 18 | 32   | 9    | 3.59  | .11  | <10 | .56   | 2140 | 4            | .04   | 25   | 1420 | 18     | <5 | <20 | 43     | .09    | <10    | 26   | <10             | 4            | 130 |
| 17 - | 1          | 6 + 005 0   | + 50E         | (.2 | 4.64   | 5  | 12 | 110 | <5   | 1.67  | q            | 24 | 37   | 11   | 5.81  | .08  | <10 | .76   | 1551 | 4            | .18   | 37   | 2350 | 30     | <5 | <20 | 134    | .08    | <10    | 17   | <10             | d            | 189 |
| 18 - | 1          | 6 + 005 1   | + 00E         | (.2 | 3.98   | 5  | 1  | 60  | (5   | . 27  | 4            | 17 | 25   | 10   | 3.64  | .05  | <10 | . 45  | 477  | 4            | .02   | 22   | 940  | 24     | <5 | <20 | 21     | .15    | <10    | 26   | <1 <del>0</del> | 2            | 11  |
| 19 - | 1          | 6 + 005 1   | + 50E         | (.2 | 3.43   | (5 | 1  | 105 | <5   | . 30  | a            | 11 | 33   | 13   | 3.87  | .05  | <10 | .68   | 210  | d            | .02   | 30   | 790  | 24     | 5  | <20 | 21     | .10    | <10    | 26   | <10             | 4            | 84  |
| 20 - | L          | 6 + 005 2   | + 00E         | (.2 | 1.41   | (5 | 1  | 60  | (5   | .15   | d            | 10 | 25   | 1    | 2.68  | .03  | <10 | .21   | 207  | d            | .02   | 12   | 330  | 16     | <5 | <20 | 10     | .14    | (10    | 45   | <10             | 1            | 42  |
| 21 - | L          | 6 + 005 2   | + 50E         | (.2 | 3.79   | (5 | 10 | 85  | <5   | .28   | d            | 19 | 39   | ġ    | 3.45  | .07  | <10 | .59   | 301  | d            | .03   | 23   | 1210 | 26     | <5 | <20 | 22     | .17    | (10    | 40   | <10             | 1            | 98  |
| 22 - | L          | 6 + 005 3   | + 00E         | (.1 | 5.62   | 5  | 10 | 15  | (5   | . 95  | a            | 23 | 42   | 12   | 4.93  | .06  | <10 | . 94  | 709  | a            | .06   | 33   | 1080 | 36     | (5 | <20 | 69     | .14    | (10    | 24   | <10             | i            | 133 |
| 23 - | L          | 6 + 005 3   | + 508         | (.1 | 2.15   | Š  | 1  | 50  | Ġ    | .06   | d            | 15 | 21   | 20   | 4.53  | . 05 | 10  | .11   | 202  | ā            | .02   | 22   | 600  | 18     | <5 | <20 | ġ      | .06    | <10    | 22   | <10             | a            | 52  |
| 24 - | L          | 6 + 005 4   | + 008         | (.2 | .11    | Š  | 1  | 30  | Ś    | .10   | a            | 8  | 10   | 10   | 3.50  | . 02 | <10 | .21   | 121  | a            | .01   | 10   | 470  | 16     | <5 | <20 | 9      | .12    | (10    | 40   | (10             | a            | 27  |
| 25 - | L          | 6 + 005 4   | + 50R         | (.2 | 1.18   | 5  | 6  | 50  | (5   | .16   | a            | 1  | n    | 15   | 3.32  | .03  | <10 | .16   | 110  | i            | <.01  | 1    | 280  | 14     | (5 | <20 | 1      | .07    | <10    | 28   | <10             | - a          | 31  |
| 26 - | L          | 6 + 005 5   | + 00E         | <.2 | 4.43   | 5  | 10 | 50  | <5   | .44   | a            | 34 | 12   | 35   | 8.00  | <.01 | (10 | .31   | 1340 | ā            | .03   | 33   | 2200 | 44     | <5 | <20 | 33     | .07    | <10    | 3    | <10             | 3            | 131 |

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## TECK EXPLORATIONS LTD. - ETK 91-522

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| PAGE 2<br>BT | DESCRIPTION             | AG AL(%) | AS | 8  | BA | BI C | l(1) | CD | CO | CR | CU FE(%) | K(%) | <b>11</b> | NG( <b>\</b> ) |     | NO NA | (1) | NI     | P PI | SB  | 5 <b>N</b> | 8R 1 | 11(1) | ٥   | ¥<br> | ¥   | 1<br> | 11 |
|--------------|-------------------------|----------|----|----|----|------|------|----|----|----|----------|------|-----------|----------------|-----|-------|-----|--------|------|-----|------------|------|-------|-----|-------|-----|-------|----|
| 27 - 6       | 6 + 005 5 + 50x         | <.2.89   | <5 | 6  | 25 | <5   | .06  | a  | 9  | 11 | 11 2.87  | .04  | 10        | .25            | 147 | 4 4   | .01 | 13 42  | 0 14 | <5  | <20        | 8    | .11   | <10 | 32    | <10 | 2     | 33 |
| 28 - L       | 6 + 005 6 + 00 <u>e</u> | <.2 1.71 | 5  | 10 | 80 | <5   | .11  | -d | 18 | 21 | 18 4.88  | .13  | 10        | .54            | 431 | <1 .  | .01 | 40 110 | 0 16 | <5  | <20        | 9    | .06   | <10 | 12    | <10 | q     | 66 |
| 29 - L       | 6 + 005 6 + 50 <u>k</u> | <.2 2.84 | <5 | 6  | 55 | <5   | .05  | d  | 15 | 12 | 10 2.92  | .03  | <10       | .22            | 267 | 4     | .01 | 16 116 | 0 18 | < 5 | <20        | 5    | .09   | <10 | 18    | <10 | q     | 56 |
| 30 - L       | 5 + 005 7 + 00g         | <.2 1.02 | 4  | 8  | 30 | <5   | .03  | a  | 1  | 10 | 5 2.17   | .03  | <10       | .17            | 246 | - <1  | .01 | 1 41   | 0 12 | <5  | <20        | 5    | .10   | <10 | 33    | <10 | 1     | 35 |

ROTE: < = LESS TEAM > = GREATER THAN

ECO-TECH LABORATORIES LTD. CLINTON AYERS LABORATORY MANAGER

SC91/TECK1

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ECO-TECH LABORATORIES LTD. TECK EXPLORATIONS LTD.- FTK 91-582 10041 EAST TRANS CANADA EWY. KANLOOPS, B.C. V2C 2J3 PHONE - 604-573-5700 FAX - 604-573-4557

AUGUST 12 , 1991

#### VALUES IN PPN UNLESS OTHERWISE REPORTED

966, 175 SECOND AVENUE Kanloops, B.C. V2C 5W1

ATTENTION: FRED DALEY

PROJECT NUMBER: 1703 88 SOIL SAMPLES RECEIVED AUGUST 2, 1991 .

|    | DESCRIPTION |                | AG AL(%) | <b>AS</b> | <b>B</b> | 8 <b>a</b> | BI CA(%) | CD | <b>co</b> | CR | CU FE(1) | X(%) | LA  | HG(1) |      | моз | HA(%) | NI | P    | PB | 6B | sn<br> | SR 1 | CI(8) | U   | ۷  | ¥   | Y   | XN. |
|----|-------------|----------------|----------|-----------|----------|------------|----------|----|-----------|----|----------|------|-----|-------|------|-----|-------|----|------|----|----|--------|------|-------|-----|----|-----|-----|-----|
| 1  | - L 8+00 S  | 1+ 50E         | <.2 5.51 | <5        | 8        | 105        | <5 .53   | <1 | 23        | 47 | 13 4.20  | .20  | <10 | . 89  | 361  | <1  | .07   | 31 | 800  | 20 | 5  | <20    | 61   | .13   | <10 | 21 | <10 | 2   | 89  |
| 2  | - L 8+00 S  | 2+ 00%         | <.2 4.54 | <5        | 6        | 110        | <\$ .67  | <1 | 19        | 45 | 9 3.85   | .12  | <10 | .91   | 1488 | <1  | .04   | 24 | 890  | 16 | 5  | <20    | 43   | .12   | <10 | 29 | <10 | 1   | 72  |
| 3  | - L 8+00 S  | 2+ 50E         | <.2 3.39 | <5        |          | 120        | <5 .56   | <1 | 16        | 32 | 9 2.96   | .13  | <10 | .61   | 1177 | <1  | .03   | 19 | 670  | 12 | 5  | <20    | 37   | .13   | <10 | 27 | <10 | 2   | 62  |
| 4  | - L 8+00 S  | 3+ 00K         | <.2 4.76 | <5        | 6        | 55         | <5.20    | <1 | 11        | 19 | 8 3.43   | .03  | <10 | . 30  | 129  | 1   | .01   | 6  | 730  | 18 | <5 | <20    | 14   | .14   | <10 | 18 | <10 | 2   | 45  |
| 5  | - L 8+00 S  | 3+ 50E         | <.2 2.82 | . 5       | 6        | 90         | <5 .80   | <1 | 20        | 13 | 13 5.25  | .03  | <10 | .47   | 1335 | <1  | .03   | 29 | 730  | 16 | <5 | <20    | 40   | .07   | <10 | 14 | <10 | <1  | 113 |
| 6  | - L 8+00 S  | 4+ 008         | <.2 3.98 | <5        |          | 30         | <5 .06   | <1 | 13        | 12 | 13 2.92  | .01  | <10 | .24   | 186  | 1   | .01   | 10 | 690  | 14 | <5 | <20    | 6    | .09   | <10 | 15 | <10 | 1   | 36  |
| 7  | - L 8+00 S  | 4+ 50 <b>x</b> | <.2 1.67 | 5         | 6        | 45         | <5 .07   | <1 | 12        | 16 | 17 3.47  | .06  | 10  | .42   | 225  | <1  | .01   | 22 | 580  | 8  | <5 | <20    | 6    | .04   | <10 | 15 | <10 | <1  | 38  |
|    | - L 8+00 S  | 5+ 00E         | <.2 1.09 | 15        | 4        | 40         | <5.04    | <1 | 10        | 12 | 10 3.48  | .04  | 10  | . 29  | 143  | <1  | .01   | 12 | 320  | 10 | <5 | <20    | 5    | .08   | <10 | 25 | <10 | <1  | 29  |
| ,  | - L 8+00 B  | 5+ 358         | <.2 1.67 | 5         | 6        | 40         | <5 .07   | <1 | 11        | 12 | 9 3.19   | .03  | <10 | . 33  | 81   | <1  | .01   | 10 | 220  | 8  | <5 | <20    | 6    | .08   | <10 | 25 | <10 | <1  | 28  |
| 10 | - L 10+00 8 | 1+ 75B         | <.2 4.96 | <5        |          | 65         | <5 .60   | <1 | 24        | 40 | 20 3.98  | .19  | <10 | .91   | 339  | <1  | .04   | 30 | 710  | 16 | 5  | <20    | 40   | .14   | <10 | 24 | <10 | 3   | 79  |
| 11 | - L 10+00 S | 2+ 00E         | <.2 1.72 | <5        | 6        | 85         | <5 .22   | <1 | 11        | 15 | 6 1.96   | .05  | <10 | .28   | 994  | <1  | .02   | 7  | 500  | 10 | <5 | <20    | 15   | . 12  | <10 | 26 | <10 | 2   | 56  |
| 12 | - L 10+00 S | 2+ 50E         | <.2 3.64 | <5        |          | 55         | <5 .37   | <1 | 19        | 30 | 13 3.64  | .10  | <10 | . 69  | 321  | <1  | .03   | 24 | 580  | 16 | <5 | <20    | 25   | . 12  | <10 | 24 | <10 | <1  | 71  |
| 13 | - L 10+00 S | 3+ 00E         | <.2 2.73 | <5 -      |          | 50         | <5 .25   | <1 | 13        | 15 | 8 2.71   | .05  | <10 | . 34  | 527  | <1  | .01   | 12 | 1160 | 16 | <5 | <20    | ,    | . 12  | <10 | 20 | <10 | 1   | 65  |
| 14 | - 1 12+00 S | 1+ 50B         | <.2 1.84 | 5         | 6        | 50         | <5 .10   | <1 | 13        | 17 | 14 3.40  | .09  | 10  | . 52  | 312  | <1  | <.01  | 21 | 1110 | 10 | <5 | <20    | 7    | .03   | <10 | 10 | <10 | <1  | 41  |
| 15 | - L 12+00 B | 2+ 008         | <.2 1.20 | 10        |          | 55         | <5 .06   | <1 | 13        | 15 | 23 3.15  | .10  | 10  | .38   | 1690 | <1  | .01   | 16 | 1390 | 4  | <5 | <20    | 8    | . 02  | <10 | 14 | <10 | <1  | 63  |
| 16 | - L 12+00 B | 2+ 50E         | <.2 1.20 | 10        | 6        | 30         | <5 .06   | <1 | 10        | 12 | 16 3.13  | . 09 | 10  | . 34  | 298  | <1  | <.01  | 9  | 560  | 8  | <5 | <20    | 5    | .03   | <10 | 14 | <10 | <1  | 33  |
| 17 | - L 12+00 S | 3+ 00E         | <.2 1.21 | 10        | 6        | 30         | <5 .06   | <1 | 12        | 15 | 16 3.19  | .16  | 10  | .48   | 360  | <1  | .01   | 15 | 850  | 6  | <5 | <20    | 6    | .03   | <10 | 9  | <10 | _<1 | 35  |
| 18 | - L 12+00 S | 3+ 50E         | <.2 1.43 | 10        | 6        | 30         | <5 .05   | <1 | 14        | 18 | 15 3.66  | .14  | 10  | . 55  | 329  | <1  | <.01  | 17 | 600  | 8  | <5 | <20    | 7    | .02   | <10 | 10 | <10 | <1  | 37  |
| 19 | - L 12+00 S | 4+ 00X         | <.2 1.33 | 10        | 4        | 55         | <5 .04   | <1 | 10        | 13 | 9 3.42   | .08  | 10  | .41   | 224  | <1  | <.01  | 11 | 1420 | 8  | <5 | <20    | 5    | .03   | <10 | 14 | <10 | <1  | 35  |
| 20 | - L 12+00 S | 4+ 50E         | <.2 2.75 | 5         | 6        | 40         | <5 .12   | <1 | 16        | 17 | 21 3.53  | .05  | 10  | . 35  | 307  | <1  | <.01  | 17 | 770  | 12 | <5 | <20    | 8    | .05   | <10 | 13 | <10 | <1  | 41  |
| 21 | - L 12+00 S | 5+ 00E         | <.2 5.04 | <5        | 10       | 35         | <5 .68   | <1 | 23        | 33 | 16 4.86  | .05  | <10 | .71   | 545  | <1  | .06   | 31 | 1110 | 16 | <5 | <20    | 48   | .08   | <10 | 16 | <10 | <1  | 96  |
| 22 | - L 12+00 S | 5+ 50X         | <.2 .71  | 10        | 6        | 30         | <5 .13   | <1 | 10        | 7  | 8 2.21   | .03  | 10  | .10   | 463  | <1  | .01   | 10 | 760  | 10 | <5 | <20    | 7    | .07   | <10 | 26 | <10 | 3   | 39  |
| 23 | - L 12+00 S | 6+ 00E         | <.2 1.29 | 10        | 6        | 35         | <5 .04   | <1 | 12        | 11 | 8 3.25   | .04  | 10  | . 29  | 686  | <1  | .01   | 10 | 1030 | 8  | <5 | <20    | 4    | .07   | <10 | 15 | <10 | <1  | 38  |
| 24 | - L 12+00 S | 6+ 50B         | <.2 2.03 | 15        | 6        | 30         | <5 .07   | <1 | ,         | 13 | 11 4.71  | .03  | 10  | . 32  | 195  | 1   | .01   | 9  | 710  | 12 | <5 | <20    | 5    | .07   | <10 | 16 | <10 | <1  | 29  |
| 25 | - L 12+00 S | 7+ 00g         | .4 1.62  | <5        | 6        | 100        | <5.13    | <1 | 21        | 6  | 5 2.09   | .03  | <10 | .11   | 2440 | <1  | .01   | 10 | 1690 | 4  | <5 | <20    | 6    | .08   | <10 | 23 | <10 | 3   | 39  |
| 26 | - L 12+00 S | 7+ 50 <b>K</b> | <.2 .82  | 10        | 6        | 20         | <5 .06   | <1 | 5         | 5  | 3 1.96   | .02  | <10 | .11   | 133  | <1  | .01   | <1 | 780  | 8  | <5 | <20    | 4    | .10   | <10 | 31 | <10 | 1   | 19  |

TECK EXPLORATIONS LTD. - ETK 91-582

August 12, 1991

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| 57 <b>1</b> | DESCRIPTION |                | AG AL(%) | λ <b>s</b> | B  | BA  | BI CA(%) | œ  | 00 | CR | CU FR(%) | X(1) | LA  | NG(1) | жн<br> | MO | NA(%) | WI | P      | PB | 8B | 8 N | SR 1 | FI(%) | U   | v    | W   | ¥          | 8 M |
|-------------|-------------|----------------|----------|------------|----|-----|----------|----|----|----|----------|------|-----|-------|--------|----|-------|----|--------|----|----|-----|------|-------|-----|------|-----|------------|-----|
| 27          | - L 14+00 S | 1+ 00B         | <.2 3.20 | <5         |    | 75  | <5.26    | <1 | 18 | 19 | 13 3.58  | . 09 | 10  | . 52  | 442    | <1 | .01   | 23 | 700    | 14 | <5 | <20 | 18   | .06   | <10 | 12   | <10 | 2          | 59  |
| 28          | - L 14+00 S | 1+ 50M         | <.2 .95  | 15         | 6  | 30  | <5 .06   | <1 | 9  | 12 | 13 3.50  | .06  | 10  | . 32  | 166    | <1 | <.01  | 13 | 970    | 10 | <5 | <20 | 6    | .04   | <10 | 19   | <10 | <1         | 30  |
| 29          | - L 14+00 B | 2+ 00B         | <.2 1.32 | 15         | 6  | 40  | <5 .06   | <1 | 11 | 12 | 13 3.63  | .05  | 10  | . 36  | 273    | <1 | .01   | 12 | 570    | 8  | <5 | <20 | 7    | .04   | <10 | 14   | <10 | <1         | 36  |
| 30          | - L 14+00 S | 2+ 502         | <.2 2.38 | 15         | 8  | 50  | <5.32    | <1 | 20 | 15 | 27 4.93  | .05  | 10  | .48   | 654    | <1 | .01   | 34 | 920    | 14 | <5 | <20 | 15   | .03   | <10 | 9    | <10 | <1         | 42  |
| 31          | - L 14+00 S | 3+ COE         | <.2 2.80 | 5          | 6  | 60  | <5 .56   | <1 | 18 | 17 | 13 4.09  | .07  | <10 | . 49  | 1276   | <1 | .02   | 19 | 920    | 14 | 5  | <20 | 31   | .06   | <10 | 14   | <10 | 2          | 76  |
| 32          | - L 14+00 S | 3+ 50E         | <.2 2.96 | 5          | 8  | 85  | <5 .28   | <1 | 22 | 26 | 16 4.70  | .06  | <10 | .55   | 838    | <1 | .02   | 35 | 720    | 14 | <5 | <20 | 21   | .08   | <10 | 21   | <10 | <1         | 80  |
| 33          | - L 14+00 B | 4+ 002         | <.2 1.44 | 5          | 6  | 40  | <5.11    | <1 | 8  | 12 | 11 3.21  | .02  | <10 | .20   | 212    | <1 | .01   | 7  | 520    | 12 | <5 | <20 | 8    | .08   | <10 | 29   | <10 | . <1       | 31  |
| 34          | - L 14+00 S | 4+ 50E         | <.2 2.08 | <5         | 8  | 55  | <5 .09   | <1 | 14 | 15 | 16 3.25  | .06  | 10  | . 39  | 800    | <1 | <.01  | 19 | 750    |    | <5 | <20 | 6    | .03   | <10 | 12   | <10 | <1         | 48  |
| 35          | - L 14+00 S | 5+ 00E         | <.2 3.26 | 5          | 6  | 50  | <5 .19   | <1 | 18 | 15 | 17 4.53  | .04  | <10 | .35   | 857    | <1 | .02   | 23 | 830    | 22 | <5 | <20 | 15   | .04   | <10 | 8    | <10 | 1          | 81  |
| 36          | - L 14+00 S | 5+ 50B         | <.2 2.22 | 10         | 8  | 30  | <5 .06   | <1 | 10 | 15 | 20 3.81  | .03  | 10  | . 30  | 224    | <1 | .01   | 14 | 530    | 14 | <5 | <20 | 6    | .04   | <10 | 14   | <10 | <1         | 38  |
| 37          | - L 14+00 S | 6+ 00K         | <.2 4.09 | <5         |    | 35  | <5 .10   | <1 | 14 | 17 | 16 4.22  | .03  | <10 | .26   | 462    | <1 | .01   | 14 | 850    | 18 | <5 | <20 | 8    | .07   | <10 | 11   | <10 | 1          | 48  |
| 38          | - L 14+00 S | 6+ 50B         | <.2 1.21 | <5         | 6  | 40  | <5 .05   | <1 | 7  | 4  | 8 1.62   | .02  | <10 | .10   | 972    | <1 | .01   | <1 | 1350   | 6  | <5 | <20 | 4    | .06   | <10 | 16   | <10 | <1         | 24  |
| 39          | - L 14+00 S | 7+ 00E         | <.2 1.02 | <5         | 6  | 30  | <5 .09   | <1 | 6  | 4  | 7 1.50   | .02  | <10 | .07   | 310    | <1 | .01   | 1  | 480    | 12 | <5 | <20 | 5    | .06   | <10 | 21   | <10 | <1         | 18  |
| 40          | - L 14+00 S | 8+ 00E         | <.2 .91  | 10         | 6  | 55  | <5 .05   | <1 | 11 | 10 | 5 2.77   | .05  | <10 | . 19  | 663    | <1 | .01   | 4  | 360    | 10 | <5 | <20 | 4    | . 12  | <10 | 30   | <10 | 1          | 36  |
| 41          | - L 16+00 S | 1+ 50B         | <.2 4.42 | <5         | 12 | 90  | <5 .80   | <1 | 22 | 35 | 15 4.39  | .11  | <10 | .74   | 1805   | 1  | .03   | 29 | 1170   | 16 | <5 | <20 | 54   | .08   | <10 | 19   | <10 | <1         | 100 |
| 42          | - L 16+00 S | 2+ 00E         | <.2 4.82 | <5         |    | 50  | <5 .62   | <1 | 19 | 33 | 18 3.01  | .14  | <10 | .71   | 660    | <1 | .02   | 24 | 1190   | 18 | 5  | <20 | 29   | .08   | <10 | 14   | <10 | <1         | 69  |
| 43          | - L 16+00 S | 2+ 50B         | <.2 2.47 | <5         | 10 | 70  | <5 1.31  | <1 | 15 | 6  | 10 3.61  | .03  | <10 | .35   | 1151   | <1 | .01   | 19 | 830    | 14 | 5  | <20 | 42   | .05   | <10 | ,    | <10 | 1          | 62  |
| 44          | - L 16+00 S | 3+ 00B         | <.2 3.66 | <5         | 8  | 45  | <5 .57   | <1 | 21 | 17 | 16 4.87  | .04  | <10 | . 49  | 1169   | <1 | .04   | 25 | 1160   | 16 | <5 | <20 | 50   | .05   | <10 | 7    | <10 | <1         | 91  |
| 45          | - L 16+00 S | 3+ 50E         | <.2 2.97 | <5         | 10 | 40  | <5 .12   | <1 | 18 | 18 | 18 3.58  | .06  | <10 | . 52  | 235    | <1 | .01   | 28 | 710    | 10 | <5 | <20 | 9    | .04   | <10 | 9    | <10 | <1         | 48  |
| 46          | - L 16+00 B | 4+ 00B         | .2 1.93  | 5          | 6  | 100 | <5 1.01  | <1 | 18 | ,  | 18 3.85  | .02  | <10 | .26   | 3316   | 1  | .01   | 16 | 1070   | 8  | <5 | <20 | 28   | .03   | <10 | 9    | <10 | <1         | 113 |
| 47          | - L 16+00 B | 4+ 50X         | <.2 1.43 | 10         | 6  | 50  | <5.10    | <1 | 11 | 13 | 16 3.55  | .03  | <10 | . 30  | 252    | <1 | .01   | 12 | 530    | 12 | <5 | <20 | 6    | .04   | <10 | 20   | <10 | <1         | 49  |
| 48          | - L 16+00 S | 5+ 008         | <.2 1.14 | 15         |    | 30  | <5.11    | <1 | 10 | 14 | 16 3.84  | .02  | <10 | . 29  | 170    | <1 | .01   | 13 | 460    | 16 | <5 | <20 | 7    | .05   | <10 | 23   | <10 | <1         | 46  |
| 43          | - L 16+00 S | 5+ 50B         | <.2 1.78 | 15         | 6  | 50  | <5 .09   | <1 | 10 | 36 | 12 4.28  | .01  | <10 | .23   | 666    | 1  | .01   | 7  | 1020   | 18 | <5 | <20 | 5    | .09   | <10 | 33   | <10 | <1         | 42  |
| 50          | - L 16+00 S | 6+ 00E         | <.2 3.49 | <5         |    | 50  | <5.15    | <1 | 11 | 36 | 13 3.92  | .03  | <10 | . 30  | 144    | 1  | .01   | 12 | 940    | 16 | 5  | <20 |      | .07   | <10 | 17   | <10 | <1         | 43  |
| 51          | - L 16+00 S | 6+ 50 <b>8</b> | <.2 .67  | 10         | 6  | 35  | <5 .06   | <1 | 6  | 5  | 6 2.40   | .03  | <10 | .11   | 142    | <1 | <.01  | з  | 760    | 10 | <5 | <20 | 5    | .07   | <10 | 21   | <10 | <1         | 14  |
| 52          | - L 16+00 B | 7+ 00E         | <.2 1.38 | 20         | 6  | 35  | <5 .04   | <1 | 20 | 10 | 7 4.22   | .00  | 10  | . 32  | 533    | <1 | .01   | 15 | 750    | 18 | <5 | <20 | 5    | .10   | <10 | 23   | <10 | 4          | 42  |
| 53          | - 1 16+00 S | 7+ 50B         | <.2 2.06 | 5          | 8  | 65  | <5 .09   | <1 | 17 | 13 | 10 2.84  | . 09 | <10 | . 35  | 352    | <1 | .01   | 21 | 1340   | 18 | <5 | <20 | 5    | .09   | <10 | 16   | <10 | 1          | 61  |
| 54          | - L 16+00 S | 8+ 00E         | <.2 3.33 | <5         |    | 140 | <5 .31   | <1 | 20 | 5  | 6 3.21   | .06  | 10  | .19   | 1349   | <1 | .01   | 21 | 2540   | 10 | <5 | <20 | 10   | .12   | <10 | 13   | <10 | <b>~</b> 6 | 37  |
| 55          | - L 18+00 S | 1+ 758         | <.2 6.42 | <5         | 10 | 55  | <5 1.56  | 1  | 24 | 52 | 22 4.57  | .27  | <10 | 1.15  | 627    | <1 | .09   | 35 | 950    | 20 | <5 | <20 | 114  | .14   | <10 | 21   | <10 | 1          | 89  |
| 56          | - L 18+00 S | 2+ 008         | <.2 4.52 | <5         | 10 | 70  | <5 .58   | <1 | 22 | 36 | 17 3.75  | .11  | <10 | . 65  | 1750   | <1 | .03   | 25 | 2080   | 14 | 5  | <20 | 34   | . 10  | <10 | 20   | <10 | 2          | 164 |
| 57          | - L 18+00 S | 2+ 502         | .2 2.97  | 10         | <2 | 75  | <5.18    | <1 | 22 | 18 | 16 3.97  | .03  | <10 | .38   | 1105   | 3  | .04   | 29 | 1037   | 12 | 10 | <20 | 17   | .06   | 10  | 24   | <10 | 5          | 106 |
| 58          | - L 18+00 S | 3+ 00E         | <.2 3.61 | <5         |    | 60  | <5.19    | <1 | 19 | 23 | 14 3.92  | .06  | <10 | .53   | 879    | <1 | .02   | 21 | 1170 . | 16 | 5  | <20 | 15   | .09   | <10 | 18   | <10 | <u>د</u> ا | 114 |
| 59          | - L 18+00 S | 3+ 50X         | <.2 5.25 | <5         | 10 | 50  | <5 .53   | <1 | 23 | 37 | 15 4.85  | .16  | <10 | .74   | 472    | <1 | .04   | 32 | 1020   | 20 | 5  | <20 | 40   | .08   | <10 | 13   | <10 | 1          | 76  |
| 60          | - L 18+00 S | 4+ 008         | <.2 4.87 | <5         | 10 | 45  | <5.30    | <1 | 22 | 28 | 17 4.17  | .11  | <10 | .64   | 356    | <1 | .02   | 27 | 740    | 18 | <5 | <20 | 21   | .09   | <10 | 13   | <10 | 2          | 84  |
| 61          | - L 18+00 S | 4+ 508         | <.2 2.83 | <5         | 6  | 45  | <5.08    | 1  | 13 | 15 | 19 3.99  | .05  | 10  | . 36  | 242    | <1 | .01   | 19 | 790    | 12 | <5 | <20 | 7    | .03   | <10 |      | <10 | -<br><1    | 52  |
| 62          | - L 18+00 S | 5+ 00X         | <.2 2.60 | <5         | 8  | 35  | <5 .10   | <1 | 13 | 6  | 11 2.90  | .03  | <10 | .18   | 893    | <1 | .02   |    | 610    | 12 | <5 | <20 | 10   | .06   | <10 | . 13 | <10 | <1         | 59  |
| 63          | - L 18+00 S | 5+ 50E         | <.2 2.73 | 5          | 6  | 65  | <5 .14   | <1 | 17 | 21 | 19 4.30  | .05  | <10 | .50   | 185    | <1 | <.01  | 32 | 700    | 12 | <5 | <20 | ,    | .04   | <10 | 14   | <10 | <1         | 70  |
|             |             |                |          | -          | -  |     |          |    |    |    |          |      |     |       |        |    |       |    |        |    |    |     | -    |       |     |      |     |            |     |

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BCO-TECH LABORATORIES LTD.

NGE 3

TECK EXPLORATIONS LTD. - ETK 91-582

August 12, 1991

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| C# | DESCRIPTION  |                | AG AL(%) | <b>λ</b> 8 | B | BA  | BI CA( | ) CD        | <b>co</b> | CR | CU y | <b>Z(1)</b> | K(1) | LA  | HG(1) | NOF  | ю  | HA(\$) | NI | P    | PB  | <b>63</b> | 8N  | SR 1 | TI ( \ ) | U   | ▼  | W   | ¥  | 211 |
|----|--------------|----------------|----------|------------|---|-----|--------|-------------|-----------|----|------|-------------|------|-----|-------|------|----|--------|----|------|-----|-----------|-----|------|----------|-----|----|-----|----|-----|
| 64 | - L 18+00 S  | 6+ 00g         | <.2 3.81 | <5         |   | 40  | <5.1   | ∎ <1        | 21        | 12 | 11   | 4.72        | .03  | 20  | . 30  | 738  | <1 | .01    | 25 | 1010 | 24  | <5        | <20 | 12   | .03      | <10 | 2  | <10 | 7  | 63  |
| 65 | - L 18+00 S  | 6+ 50X         | <.2 1.71 | 10         | 6 | 45  | <5.0   | 5 <1        | 11        | 16 | 11   | 3.57        | .04  | <10 | . 42  | 160  | <1 | .01    | 17 | 800  | 10  | <5        | <20 | 5    | .03      | <10 | 13 | <10 | <1 | 40  |
| 66 | - L 18+00 S  | 6+ 75B         | <.2.71   | 10         | 6 | 35  | <5.0   | 4 <1        | 10        | 6  | 10   | 2.34        | .05  | 10  | . 19  | 363  | <1 | .01    | 11 | 500  | 6   | <5        | <20 | 5    | .04      | <10 | 18 | <10 | <1 | 42  |
| 67 | - L 20+00 S  | 3+ 00E         | <.2 2.33 | 10         | 6 | 110 | <5.2   | 8 <1        | 19        | 15 | 13   | 3.85        | .05  | <10 | . 37  | 2045 | <1 | . 02   | 20 | 1760 | 14  | <5        | <20 | 19   | .04      | <10 | 12 | <10 | <1 | 140 |
| 68 | - L 20+00 B  | 3+ 50E         | <.2 2.40 | <5         | 6 | 55  | <5 .0  | 7 <1        | 17        | 15 | 15   | 3.51        | . 05 | <10 | . 38  | 359  | <1 | .01    | 22 | 1230 | 16  | <5        | <20 | 7    | .05      | <10 | 13 | <10 | <1 | 103 |
| 69 | - L 20+00 S  | 4+ 00E         | <.2 1.74 | <5         | 6 | 50  | <5.0   | 8 <1        | 13        | 12 | 13   | 3.24        | .04  | <10 | . 30  | 227  | <1 | .01    | 17 | 520  | 18  | <5        | <20 | 7    | .04      | <10 | 15 | <10 | <1 | 96  |
| 70 | - L 20+00 S  | 4+ 25E         | <.2 .66  | 35         | 4 | 25  | <5.0   | 6 <1        | 7         | 5  | 7    | 2.78        | <.01 | <10 | .14   | 348  | <1 | .01    | 10 | 560  | 66  | <5        | <20 | 5    | .06      | <10 | 26 | <10 | <1 | 109 |
| 71 | - 1. 20+00 S | 4+ 50B         | .4 1.18  | 30         | 6 | 35  | <5.0   | 6 <1        | 16        | 7  | 26   | 5.10        | .01  | 10  | . 19  | 1126 | <1 | .01    | 26 | 1200 | 102 | <5        | <20 | 6    | .03      | <10 | 11 | <10 | <1 | 464 |
| 72 | - L 20+00 S  | 4+ 75 <b>X</b> | <.2 1.05 | 15         | 6 | 35  | <5.2   | 1 <1        | 9         | 10 | 13   | 3.48        | .02  | <10 | .21   | 363  | <1 | .01    | 9  | 750  | 16  | <5        | <20 | 7    | .06      | <10 | 26 | <10 | <1 | 39  |
| 73 | - 1 20+00 S  | 5+ 00X         | <.2 .72  | 10         | 6 | 25  | <5.1   | 2 <1        | 5         | 6  | 6    | 2.35        | .01  | <10 | .10   | 103  | <1 | .01    | 3  | 530  | 10  | <5        | <20 | 6    | .07      | <10 | 31 | <10 | <1 | 23  |
| 74 | - L 20+00 S  | 5+ 50E         | <.2 2.01 | 15         | 6 | 55  | <5 .0  | 4 <1        | ,         | 15 | 11   | 4.83        | .03  | 10  | .25   | 261  | 1  | .01    | 7  | 2250 | 16  | <5        | <20 | 6    | .08      | <10 | 21 | <10 | <1 | 36  |
| 75 | - L 20+00 S  | 6+ 00E         | 1.0 .51  | 5          | 6 | 135 | <5.1   | <b>9</b> <1 | 24        | ,  | 13   | 1.79        | .04  | <10 | .12   | 6855 | <1 | .01    | 4  | 650  | <2  | <5        | <20 | 6    | .04      | <10 | 20 | <10 | <1 | 56  |
| 76 | - L 20+00 S  | 6+ 25B         | <.2 2.49 | 5          | 8 | 45  | <5.0   | 7 <1        | 17        | 14 | 9    | 3.93        | .08  | 10  | . 42  | 363  | <1 | .01    | 19 | 970  | 14  | <5        | <20 | 6    | .12      | <10 | 21 | <10 | 4  | 57  |
| 77 | - L 22+00 S  | 2+ 75E         | .2 2.68  | <5         | 6 | 55  | <5.2   | 7 <1        | 14        | 13 | 21   | 3.12        | .05  | 10  | .26   | 921  | <1 | <.01   | 15 | 1140 | 12  | <5        | <20 | 11   | .04      | <10 | 10 | <10 | 5  | 48  |
| 78 | - L 22+00 S  | 3+ 008         | <.2 1.41 | 10         | 6 | 25  | <5.1   | 5 <1        | ,         | 9  | 19   | 3.13        | .03  | 10  | .17   | 351  | <1 | <.01   | ,  | 720  | 28  | <5        | <20 |      | .04      | <10 | 19 | <10 | 1  | 53  |
| 79 | - L 22+00 S  | 3+ 25B         | <.2 1.50 | 10         | 6 | 45  | <5 .0  | 7 <1        | 11        | 10 | 20   | 3.38        | .02  | <10 | .18   | 469  | <1 | .01    | ,  | 1250 | 18  | <5        | <20 | 7    | .06      | <10 | 20 | <10 | <1 | 50  |
| 80 | - L 22+00 S  | 3+ 50B         | <.2 1.14 | 15         | 6 | 35  | <5.0   | 4 <1        | 10        | 11 | 15   | 3.62        | .02  | <10 | .21   | 363  | <1 | .01    |    | 730  | 32  | <5        | <20 | 5    | .05      | <10 | 20 | <10 | <1 | 62  |
| 81 | - 1. 22+00 S | 3+ 758         | <.2 1.88 | 10         | 6 | 35  | <5.0   | 3 <1        | 10        | 14 | 18   | 3.87        | .03  | <10 | .24   | 211  | <1 | .01    | 11 | 580  | 30  | <5        | <20 | 4    | .05      | <10 | 15 | <10 | <1 | 61  |
| 82 | - L 22+00 S  | 4+ 00E         | <.2 .77  | 15         | 4 | 25  | <5 .0  | 6 <1        | 6         | 7  |      | 2.54        | . 02 | <10 | .14   | 188  | <1 | .01    | 4  | 700  | 16  | <5        | <20 | 5    | .05      | <10 | 23 | <10 | <1 | 28  |
| 83 | - L 22+00 S  | 4+ 25B         | <.2 1.27 | 20         | 6 | 60  | <5 .0  | 2 <1        | 11        | 11 | 8    | 4.23        | .03  | <10 | .24   | 447  | <1 | .01    | 6  | 1580 | 22  | <5        | <20 | 4    | .06      | <10 | 22 | <10 | <1 | 43  |
| 84 | - L 22+00 S  | 4+ 508         | <.2 1.68 | 5          | 4 | 35  | <5.0   | 3 <1        | ,         | 10 | 11   | 3.26        | .03  | <10 | .23   | 226  | <1 | <.01   | 8  | 910  | 18  | <5        | <20 | 5    | .05      | <10 | 18 | <10 | <1 | 38  |
| 85 | - L 22+00 S  | 5+ 00K         | <.2 .78  | 15         | 4 | 25  | <5.0   | 3 <1        | 7         |    | 6    | 3.13        | .02  | <10 | .18   | 271  | <1 | .01    | 4  | 1010 | 12  | <5        | <20 | 5    | .04      | <10 | 26 | <10 | <1 | 25  |
| 86 | - L 22+00 S  | 5+ 50K         | <.2 .63  | 15         | 6 | 25  | <5.0   | 3 <1        | 7         | 7  | 11   | 3.14        | .02  | <10 | .14   | 99   | <1 | .01    | 6  | 990  | 12  | <5        | <20 | 5    | .06      | <10 | 23 | <10 | <1 | 18  |
| 87 | - L 22+00 S  | 6+ 00E         | <.2 1.75 | 5          | 6 | 45  | <5 .0  | 8 <1        |           | 5  | 4    | 2.47        | .02  | <10 | .14   | 295  | <1 | .01    | 2  | 1900 | 10  | <5        | <20 | 4    | .07      | <10 | 18 | <10 | <1 | 30  |
| 88 | - L 22+00 S  | 6+ 50E         | <.2 .71  | 10         | 6 | 55  | <5.1   | 1 <1        | 12        | 3  | 5    | 2.70        | .01  | <10 | . 12  | 657  | <1 | .01    | ,  | 610  | 8   | <5        | <20 | 6    | .06      | <10 | 19 | <10 | 2  | 24  |

JES F \_\_\_\_

ECO-TECH LABORATORIES LTD. Person J. Persotti, A.Sc.T. B.C. Certified Assayer

ECO-TECH LABORATORIES LTD. 10041 EAST TRANS CANADA HWY. KAMLOOPS, B.C. V2C 2J3 PBONE - 604-573-5700 FAX - 604-573-4557

3UST 12 , 1991

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LUES IN PPN UNLESS OTHERWISE REPORTED

TECK EXPLORATIONS LTD.- ETK 91-581 960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5W1 \*

ATTENTION: FRED DALLEY

PROJECT NUMBER: 1703 70 Soil Samples Received August 2, 1991

| ŧ  | DESC | RIPTION                           |       |             | AG I | AL(%) | AS | B | BA | BI CA(1) | CD | co | CR         | CU FE(1) | X(%) | LA H | G(1) | 1CH    | HO NA(\$)  | NI P    | PB | 68  | 8N  | SR T | I(8)          | U                     | v  | W   | x  | X H |
|----|------|-----------------------------------|-------|-------------|------|-------|----|---|----|----------|----|----|------------|----------|------|------|------|--------|--|---------|----|-----|-----|------|---------------|-----------------------|----|-----|----|-----|
|    |      | و ها با با بر بر بر بر مر بر بر ب | ***** |             |      |       |    |   |    |          |    |    |            |          |      | **** |      | ****** |  |         |    |     |     |      | 1 8 H H H 4 4 | ي فا عام او جار اية : |    |     |    |     |
| 2  | - L  | 24+00 8                           | 2+    | 50 <b>E</b> | .2   | 1.72  | 5  | 4 | 60 | <5 .49   | <1 | 18 | 16         | 23 3.27  | .10  | 20   | .43  | 912    | <1 <.01  | 22 1020 | 18 | <5  | <20 | 15   | .02           | <10                   | 12 | <10 | 5  |     |
| 2  | - L  | 24+00 8                           | 2+    | 75 <b>K</b> | <.2  | 1.81  | 5  | 4 | 60 | <5.30    | <1 | 16 | 15         | 19 3.11  | .10  | 20   | . 42 | 829    | <1 .01   | 22 880  | 10 | <5  | <20 | 12   | .01           | <10                   | 11 | <10 | 7  | 53  |
| 3  | - L  | 24+00 8                           | 3+    | 002         | <.2  | 2.09  | 5  | 4 | 75 | <5 .23   | <1 | 17 | 17         | 19 3.52  | .11  | 20   | .48  | 792    | <1 .01   | 27 990  | 14 | <5  | <20 | 14   | .02           | <10                   | 12 | <10 | 4  | 66  |
| 4  | - L  | 24+00 8                           | 3+    | 258         | <.2  | 3.76  | <5 | 6 | 50 | <5 .60   | <1 | 21 | 33         | 21 3.80  | .07  | 20   | .63  | 1198   | <1 .06   | 29 1140 | 16 | <5  | <20 | 46   | .04           | <10                   | 15 | <10 |    | 108 |
| 5  | - L  | 24+00 8                           | 3+    | 50E         | <.2  | 1.07  | 5  | 4 | 30 | <5 .09   | <1 | 9  | 11         | 21 2.85  | .05  | 10   | . 31 | 301    | <1 .01   | 15 520  | 12 | <5  | <20 |      | .03           | <10                   | 19 | <10 | <1 | 36  |
| 6  | - L  | 24+00 8                           | 4+    | 75 <b>E</b> | .2   | 1.55  | 5  | 4 | 55 | <5 .18   | <1 | 13 | 16         | 18 3.14  | .07  | 20   | . 51 | 739    | <1 <.01  | 22 480  | 10 | 5   | <20 | 10   | .03           | <10                   | 16 | <10 | 5  | 54  |
| 7  | - L  | 24+00 8                           | 4+    | 002         | .2   | 1.35  | 5  | 4 | 35 | <5 .08   | <1 | 6  | 10         | 25 2.79  | .03  | 10   | .16  | 141    | 1 .01  | 10 690  | 12 | <5  | <20 | 7    | .04           | <10                   | 17 | <10 | <1 | 25  |
|    | - L  | 24+00 5                           | 4+    | 25 <b>H</b> | .2   | 1.03  | 10 | 6 | 35 | <5 .04   | <1 | 7  | 10         | 13 3.07  | .03  | 10   | .21  | 277    | <1 .01   | 10 1050 | 12 | <5  | <20 | 5    | .04           | <10                   | 20 | <10 | <1 | 23  |
| ,  | - L  | 24+00 5                           | 4+    | 508         | .2   | 1.67  | 10 | 6 | 45 | <5 .04   | <1 | 9  | 14         | 15 3.36  | .04  | 10   | . 32 | 278    | 1 <.01   | 14 660  | 12 | <5  | <20 | 5    | .04           | <10                   | 17 | <10 | <1 | 33  |
| 10 | - L  | 24+00 8                           | 4+    | 75E         | <.2  | .51   | 5  | 4 | 20 | <5 .04   | <1 | 4  | <b>,</b> 5 | 7 1.81   | .02  | 10   | .10  | 63     | <1 .01   | 7 250   |    | <5  | <20 | 4    | .03           | <10                   | 22 | <10 | <1 | 16  |
| 11 | - L  | 24+00 8                           | 5+    | 008         | <.2  | 1.62  | 10 | 4 | 45 | <5 .04   | <1 | ,  | 13         | 19 3.63  | .03  | 10   | .24  | 317    | 1 .01  | 11 830  | 12 | <5  | <20 | 6    | .06           | <10                   | 20 | <10 | <1 | 36  |
| 12 | - L  | 24+00 5                           | 5+    | 50B         | <.2  | 2.11  | 10 | 4 | 55 | <5 .04   | <1 | 10 | 16         | 13 3.79  | .06  | 10   | . 39 | 433    | <1 .01   | 14 910  | 12 | <5  | <20 | 6    | .04           | <10                   | 16 | <10 | <1 | 32  |
| 13 | - L  | 24+00 8                           | 6+    | 008         | <.2  | 1.31  | 20 | 6 | 45 | <5 .10   | <1 | 12 | 17         | 15 4.42  | .06  | 10   | .51  | 189    | 1 <.01   | 22 1100 |    | 5   | <20 |      | .03           | <10                   | 15 | <10 | <1 | 33  |
| 14 | - L  | 24+00 8                           | 6+    | 50E         | <.2  | .50   | 5  | 4 | 15 | <5 .04   | <1 | 4  | 3          | 5 1.72   | .01  | <10  | .06  | 53     | <1 .01   | 5 660   | 4  | <5  | <20 | 4    | .05           | <10                   | 29 | <10 | <1 | 12  |
| 15 | - L  | 26+00 8                           | 1+    | 75 <b>E</b> | .2   | 1.75  | 5  | 6 | 65 | <5 .09   | <1 | 11 | 17         | 13 3.16  | .09  | 10   | .31  | 401    | 1 .01  | 15 1771 | 30 | <\$ | <20 |      | .05           | <10                   | 19 | <10 | <1 | 75  |
| 16 | - L  | 26+00 8                           | 2+    | 008         | <.2  | 2.14  | <5 | 4 | 65 | <5 .01   | <1 | 15 | 14         | 14 3.14  | .07  | 10   | .33  | 565    | <1 .01   | 20 1117 | 32 | <5  | <20 | 18   | .04           | <10                   | 12 | <10 | <1 | 106 |
| 17 | - L  | 26+00 5                           | 2+    | 50 <b>x</b> | <.2  | 1.85  | 5  | 6 | 65 | <5 .14   | <1 | 14 | 16         | 16 3.23  | . 09 | 10   | .40  | 1202   | <1 .01   | 23 1260 | 16 | <5  | <20 | 10   | .04           | <10                   | 14 | <10 | <1 | 69  |
| 18 | - L  | 26+00 8                           | 3+    | 008         | .2   | 1.43  | 10 | 4 | 60 | <5 .15   | <1 | 12 | 12         | 18 3.19  | .06  | 10   | .28  | 875    | <1 <.01  | 15 780  | 12 | <5  | <20 | ,    | .04           | <10                   | 20 | <10 | <1 | 49  |
| 19 | - L  | 26+00 \$                          | 3+    | 50 <b>x</b> | <.2  | 1.72  | 10 | 6 | 45 | <5 .06   | <1 | 13 | 16         | 16 3.79  | .06  | 10   | . 36 | 495    | <l <.01<="" td=""><td>17 2450</td><td>16</td><td>&lt;5</td><td>&lt;20</td><td>5</td><td>.05</td><td>&lt;10</td><td>19</td><td>&lt;10</td><td>&lt;1</td><td>50</td></l> | 17 2450 | 16 | <5  | <20 | 5    | .05           | <10                   | 19 | <10 | <1 | 50  |
| 20 | - L  | 26+00 8                           | 4+    | 002         | .2   | .54   | 5  | 4 | 35 | <5 .11   | <1 | 5  | 6          | 11 1.84  | .03  | <10  | .12  | 348    | <1 <.01  | 10 670  | 16 | <5  | <20 |      | .02           | <10                   | 16 | <10 | <1 | 37  |
| 21 | - L  | 26+00 \$                          | 4+    | 50E         | <.2  | 1.43  | 15 | 6 | 85 | <5 .13   | <1 | 11 | 12         | 17 3.38  | .05  | 10   | .28  | 1116   | <1 .01   | 17 1800 | 22 | <5  | <20 | 10   | .04           | <10                   | 19 | <10 | <1 | 68  |
| 22 | - L  | 26+00 \$                          | 5+    | 008         | <.2  | .74   | 10 | 4 | 25 | <5 .04   | <1 | 5  | 6          | 6 2.05   | .02  | <10  | .12  | 158    | <1 .01   | 6 450   | 16 | <5  | <20 | 5    | .04           | <10                   | 22 | <10 | <1 | 25  |
| 23 | - L  | 26+00 8                           | 5+    | 50E         | <.2  | .41   | 10 | 6 | 15 | <5 .06   | <1 | 6  | 5          | 13 1.91  | .03  | 10   | .12  | 89     | <1 .01   | 12 420  | 8  | <5  | <20 | 5    | .04           | <10                   | 18 | <10 | <1 | 19  |
| 24 | - L  | 26+00 8                           | 6+    | 008         | <.2  | . 98  | 15 | 6 | 25 | <5 .19   | <1 | 22 | 12         | 16 4.08  | .06  | 60   | .25  | 802    | <1 <.01  | 30 1190 | 14 | <5  | <20 | 14   | .03           | <10                   | 13 | <10 | 34 | 29  |
| 25 | - L  | 28+00 8                           | B/L   |             | .2   | 1.31  | 10 |   | 45 | <5 .27   | <1 | 16 | 13         | 15 3.16  | .08  | 20   | .38  | 1240   | <1 <.01  | 25 570  | 58 | <5  | <20 | 13   | .02           | <10                   | 10 | <10 | 3  | 156 |
| 26 | - L  | 28+00 S                           | 0+    | 50 <b>2</b> | <.2  | 1.42  | 5  | 6 | 55 | <5 .20   | <1 | 19 | 15         | 14 2.07  | .11  | 20   | . 39 | 1190   | <1 <.01  | 28 750  | 20 | <5  | <20 | 13   | .02           | <10                   | 9  | <10 | 7  | 101 |

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| ET#      | DES  | CRIPTION |          |             | AG I       | AL(%) | <b>X8</b> | 8 | BA       | BI CA(S | ) СД      | co  | CR                                      | CU FE(%) | K(8) | LA        | MG( ) | HOI  | ю         | MA(\$) | NI | 2    | PB | 63     | <b>s</b> N | 8R | TI( <b>\</b> ) | U   | ۷        | W    | ¥        | SN.      |
|----------|------|----------|----------|-------------|------------|-------|-----------|---|----------|---------|-----------|-----|---|----------|------|-----------|-------|------|-----------|--------|----|------|----|--------|------------|----|----------------|-----|----------|------|----------|----------|
| 27       | - L  | 28+00 5  | 1+       | 00E         | <.2        | 1.99  | <5        | 6 | 50       | <5 .2   | l <1      | 13  | 16                                      | 14 2.70  | .11  | 10        | .44   | 391  | <1        | .01    | 24 | 680  | 12 | <br><5 | <20        | 15 | .02            | <10 |          | <10  |          | 93       |
| 28       | - L  | 28+00 \$ | 1+       | 508         | <.2        | 1.56  | 10        | 6 | 45       | <5 .0   | s <1      | 20  | 20                                      | 25 3.56  | .12  | 20        | .66   | 281  | <1        | .01    | 49 | 580  |    | <5     | <20        | ,  | .03            | <10 | 12       | <10  | <1       | 41       |
| 29       | - L  | 28+00 \$ | 2+       | 008         | <.2        | 1.74  | 5         | 4 | 70       | <5 .13  | l <1      | 15  | 15                                      | 12 3.27  | .08  | 10        | . 39  | 720  | <1        | .01    | 24 | 590  | 22 | <5     | <20        | 11 | .03            | <10 | 15       | <10  | <1       | 77       |
| 30       | - L  | 28+00 8  | 2+       | 50E         | <.2        | .72   | 10        | 6 | 55       | <5 .50  | ) <1      | 11  | ,                                       | 15 2.29  | .07  | 10        | .27   | 720  | <1        | <.01   | 17 | 680  |    | <5     | <20        | 15 | .02            | <10 | 11       | <10  | <1       | 45       |
| 31       | - L  | 28+00 \$ | 3+       | 008         | <.2        | .93   | 15        | 4 | 25       | <5 .12  | · <1      | 12  | 12                                      | 14 2.91  | .08  | 10        | . 36  | 249  | <1        | <.01   | 22 | 530  | 10 | <5     | <20        | 7  | .02            | <10 | 13       | <10  | <1       | 47       |
| 32       | - L  | 28+00 B  | 3+       | 50 <b>2</b> | <.2        | .70   | 10        | 6 | 35       | <5 .13  | / <1      | 12  | 10                                      | 18 2.68  | .05  | 10        | .22   | 367  | <1        | <.01   | 19 | 610  | 8  | <5     | <20        | 10 | .02            | <10 | 13       | <10  | 1        | 31       |
| 33       | - L  | 28+00 8  | 4+       | 002         | <.2        | . 42  | 10        | 4 | 5        | <5 .05  | i <1      | 7   | 4                                       | 15 1.95  | .03  | 10        | .10   | 120  | <1        | <.01   | 12 | 290  | 6  | <5     | <20        | 4  | .04            | <10 | 19       | <10  | <1       | 17       |
| 34       | - L  | 28+00 8  | 4+       | 50 <b>B</b> | .2         | . 32  | 5         | 6 | 40       | <5 .57  | <1        | 4   | 3                                       | 19 1.41  | .01  | <10       | .06   | 95   | <1        | <.01   | 10 | 393  | 6  | <5     | <20        | 12 | .03            | <10 | 17       | <10  | 1        | 16       |
| 35       | - L  | 28+00 8  | 5+       | 00E         | <.2        | . 39  | 10        | 6 | 20       | <5 .23  | <1        | 6   | 7                                       | 14 2.00  | .05  | 10        | .14   | 145  | <1        | <.01   | 14 | 550  | 6  | <5     | <20        | 7  | .02            | <10 | 14       | <10  | <1       | 27       |
| 36       | - L  | 28+00 6  | 5+       | 50 <b>2</b> | <.2        | .89   | 10        | 6 | 40       | <5.12   | <1        | ,   | 10                                      | 13 2.73  | .07  | 10        | . 31  | 469  | <1        | <.01   | 14 | 890  | 8  | <5     | <20        | 7  | .01            | <10 | 13       | <10  | <1       | 31       |
| 37       | - L  | 28+00 8  | 6+       | 008         | <.2        | 1.01  | 10        | 6 | 30       | <5 .05  | i <1      | 9   | 11                                      | 17 3.10  | .06  | 10        | .27   | 323  | <1        | .01    | 13 | 1770 |    | <5     | <20        | 5  | .03            | <10 | 14       | <10  | <1       | 25       |
| 38       | - L  | 30+00 6  | B/L      | •           | <.2        | .88   | 10        | 4 | 40       | <5 .20  | <1        | 11  | 12                                      | 13 2.43  | .09  | 10        | . 29  | 311  | <1        | <.01   | 10 | 430  |    | <5     | <20        | ,  | .02            | <10 | 12       | <10  | <1       | 33       |
| 39       | - L  | 30+00 8  | 0+       | 50E         | <.2        | 1.05  | 5         | 6 | 30       | <5 .67  | <1        | 9   | 14                                      | 10 1.86  | .08  | 20        | .26   | 121  | <1        | <.01   | 38 | 650  | 6  | <5     | <20        | 13 | .01            | <10 | 7        | <10  | 7        | 27       |
| 40       | - L  | 30+00 B  | 1+       | 008         | <.2        | .94   | 10        | 6 | 35       | <5.25   | <1        | 10  | 13                                      | 13 2.74  | .08  | 10        | .27   | 219  | <1        | <.01   | 22 | 390  | 10 | <5     | <20        |    | .02            | <10 | 12       | <10  | <1       | 29       |
| 41       | - L  | 30+00 6  | 1+       | 50 <b>5</b> | <.2        | 1.27  | 5         | 4 | 45       | <5 .16  | <1        | 12  | 14                                      | 15 2.45  | .09  | 20        | .28   | 589  | <1        | .01    | 20 | 840  | 8  | <5     | <20        | •  | .01            | <10 | 9        | <10  | 6        | 45       |
| 42       | - L  | 30+00 B  | 2+       | 00E         | <.2        | .71   | 10        | 4 | 25       | <5 .43  | <1        | 7   | 10                                      | 11 2.46  | .07  | 10        | .23   | 268  | <1        | <.01   | 15 | 360  | 6  | <5     | <20        | ,  | .02            | <10 | 13       | <10  | <1       | 24       |
| 43       | - L  | 30+00 S  | 2+       | 50 <b>B</b> | <.2        | .92   | 5         | 6 | 35       | <5.30   | <1        | 9   | 12                                      | 11 2.37  | .10  | 10        | .27   | 278  | <1        | <.01   | 17 | 410  | 10 | <5     | <20        | 13 | .01            | <10 | 9        | <10  | <1       | 28       |
| 44       | - L  | 30+00 8  | 3+       | 002         | <.2        | .61   | 5         | 4 | 40       | <5 .42  | <1        | 9   | 8                                       | 20 2.08  | .05  | 10        | .19   | 738  | <1        | <.01   | 15 | 410  | 6  | <5     | <20        | 18 | .04            | <10 | 17       | <10  | 2        | 41       |
| 45       | - L  | 30+00 8  | 3+       | 50B         | <.2        | .80   | 10        | 6 | 25       | <5 .05  | <1        | 10  | 10                                      | 14 2.71  | .06  | 10        | .26   | 268  | <1        | .01    | 16 | 370  | 8  | <5     | <20        | 5  | .02            | <10 | 14       | <10  | <1       | 29       |
| 46       | - L  | 30+00 \$ | 4+       | 00E         | <.2        | 1.57  | 5         | 4 | 45       | <5 .19  | <1        | 18  | 19                                      | 16 3.31  | .13  | 20        | .58   | 597  | <1        | .01    | 26 | 560  | 10 | <5     | <20        | 13 | .02            | <10 | 9        | <10  | 6        | 44       |
| 47       | - L  | 30+00 8  | 4+       | 50 <b>x</b> | <.2        | 1.37  | 5         | 6 | 45       | <5 .26  | <1        | 15  | 16                                      | 17 3.17  | .13  | 30        | .52   | 712  | <1        | .01    | 26 | 570  | 10 | <5     | <20        | 12 | .02            | <10 | 9        | <10  | 6        | 46       |
| 48       | - L  | 30+00 8  | 5+       | OOE         | <.2        | 1.18  | 5         | 8 | 35       | <5 .85  | <1        | 16  | 12                                      | 16 2.48  | .14  | 30        | .46   | 787  | <1        | <.01   | 25 | 880  |    | <5     | <20        | 17 | .02            | <10 | 6        | <10  | 12       | 45       |
| 49       | - L  | 30+00 8  | 5+       | 508         | <.2        | .11   | <5        | 6 | 5        | <5 1.66 | <1        | 1   | 1                                       | 4 .46    | .01  | <10       | .06   | 97   | <1        | <.01   | 5  | 310  | <2 | <5     | <20        | 16 | <.01           | <10 | 4        | <10  | <1       | 12       |
| 50       | - L  | 30+00 8  | •+       | 008         | .2         | 1.48  | 5         |   | 55       | <5 .20  | <1        | 34  | 9                                       | 15 2.77  | .04  | 30        | .17   | 1806 | 1         | .01    | 17 | 550  | 10 | <5     | <20        | 9  | .08            | <10 | 21       | <10  | 10       | 41       |
| 51       | - 1  | 30+00 8  | 0+       | 50W         | <.2        | 1.31  | 5         | 4 | 50       | <5 .10  | <1        | 13  | 16                                      | 11 2.52  | .10  | 10        | .40   | 441  | <1        | .01    | 20 | 480  |    | <5     | <20        |    | .01            | <10 | 9        | <10  | <1       | 49       |
| 52       | - 1  | 30+00 8  | 1+       | UUW         | <.2        | 1.07  | -         |   | 30       |         | <1        |     | 14                                      | 10 1.94  |      | 20        | .27   | 342  | <1        | .01    | 34 | 610  |    | <5     | <20        | 15 | .01            | <10 | 1        | <10  | 6        | 27       |
|          | - 1  | 30+00 8  | 4+       | 30W         | <.2        | .81   | 3         | • | 30       | <5 .41  | <1        | ,,  | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 10 2.31  |      | 10        | .24   | 352  | <1        | <.01   | 16 | 320  |    | 0      | <20        | ,  | .03            | <10 | 15       | <10  | <1       | 32       |
| 24       | - 1  | 32+00 8  | 8/1      |             | <.2        | 1.40  | <5        |   | 43       | <> .43  | <1        | 15  | 13                                      | 16 2.40  | .11  | 20        | .37   | 233  | <1        | .01    | 27 | 700  |    | <5     | <20        | 15 | .02            | <10 | ,        | <10  | 10       | 43       |
| 33       | - 1  | 32+00 8  | 1.       | 30E         | <.2        | 1.00  | 3         |   | 30       | <5 .34  | <1<br>- 1 | 11  | •                                       | 18 2.39  | .05  | 10        | .1/   | 633  | <1        | <.01   | 13 | 490  | 10 | <      | <20        | 10 | .05            | <10 | 21       | < 10 | 2        | 31       |
| 20       |      | 32+00 B  | 1.       | UUB         | <.2        | 1.52  | 3         |   | 30       | <5 .10  | < 1<br>.1 | 13  | 13                                      | 10 2.73  | .10  | 20        | . 30  |      | <1<br>    | .01    | 17 | 800  | 12 | 3      | <20        | ., | .03            | <10 | 12       | <10  | •        | 47       |
| 57       |      | 32+00 B  | 1+       | 30 <b>5</b> |            | 1.85  | <3        |   | 8U<br>40 | <0.61   | <1        | 10  | 17                                      | 10 2.01  | .10  | 40        |       | 1195 | <1<br>- 1 | <.01   | 25 | 980  | 10 | <3     | <20        | 10 | .02            | <10 |          | <10  | 28       | ••       |
| 58       |      | 32+00 8  | 4T<br>24 | LOR         | <.2        | 1.55  | < 5       |   | 40       | <5 .53  |           | 1.6 | 11                                      | 10 2.37  | .07  | 30        | .21   | 1121 | <1<br>    | <.01   | 10 | 900  | 10 | <      | <20        | 11 | .02            | <10 | 10       | <10  | 14       | 43       |
| 59       |      | 32+00 8  | 3.       |             | <.2        | 1.01  | 2         | : | 30       | <5 .63  | <1<br>- 1 | 13  |   | 21 2.73  | .1/  | 10        |       | 1010 | <1        | <.01   | 30 | 880  | 14 | <      | <20        | 18 | .01            | <10 |          | <10  |          | 33       |
| 4U<br>41 | - 1  | 32+00 8  | 34       | 50#         | •4         | 1.49  | 2         | - | 30       | -5 .00  | <1<br>    |     | •                                       | 18 2 13  | .04  | 10        | .17   | 1930 | <1        | <.01   | 13 | 1090 | 10 | <      | <20        | 12 |                | <10 | 20       | <10  | 2        | 49       |
| 62       | - L  | 32+00 g  | 44       | 0.02        | .4         | . /0  | 3         | 2 | 20       | -3 .34  | ~1        |     |   | 22 2.64  | .07  | 20        |       | 26   | ~1        | < .01  | 10 | 4/U  | 10 |        | <20        | ,  | .03            | <10 | 21       | <10  | <b>4</b> | 4J<br>25 |
| 63       | - 1. | 32+00 8  | 4        | 508         | <.2<br>< 2 | .34   | -5        | - | 40       | -5 2 26 | ~1        | -1  | -1                                      | 4 4.34   | .02  | 2U<br>~10 |       | 785  | <1        | <.01   | 78 | 380  | 14 | <0     | <20        | •  | . UJ           | <10 | 41<br>~1 | <10  | -1       | 43       |
| ••       | ~ •  |          | 47       |             | <          | . 10  |           | • | 40       | -3 8.30 | -1        | ~*  | ~*                                      | 44       |      | ×10       |       | 193  | 54        | <.01   | 4  | 470  | •  | < 3    | <20        | 41 | <.01           | <10 | <1       | <10  | <.       | 33       |

| GE 3 |      |           |       |       |          |       |         |   |     |      |         |    |    |    |    |       |      |      |        |        |    |        |    |      |        |    |            |      |       |     |       |       |    |            |
|------|------|-----------|-------|-------|----------|-------|---------|---|-----|------|---------|----|----|----|----|-------|------|------|--------|--------|----|--------|----|------|--------|----|------------|------|-------|-----|-------|-------|----|------------|
| 1    | DESC | RIPTION   |       |       | AG       | AL(\) | 72      | B | BA  | BI C | =A(1)   | œ  | CO | CR | CU | PE(%) | K(%) | LA I | HG(\$) | Kar    | ю  | MA(1)  | NI | P    | PB     | 6B | 8 <b>N</b> | SR 1 | 21(1) | U   | v     | W     | ¥  | <b>5</b> M |
| ~~~~ |      | ********* | ***** | ***** | <br>**** |       | ******* |   |     |      | ******* |    |    |    |    |       |      |      |        | ****** |    | ****** |    |      | ****** |    | ****       |      |       |     | ***** | ***** |    |            |
| 64   | - L  | 32+00 B   | 5+    | 00E   | <.2      | 1.15  | 10      | • | 35  | <5   | . 48    | <1 | 12 | 13 | 17 | 3.32  | .08  | 20   | .38    | 396    | <1 | <.01   | 19 | 430  | 12     | <5 | <20        | 12   | .04   | <10 | 17    | <10   | 2  | 36         |
| 65   | - L  | 32+00 8   | 5+    | 50E   | <.2      | 1.17  | 10      | 4 | 95  | <5   | . 34    | <1 | 13 | 13 | 15 | 3.05  | .08  | 10   | .40    | 924    | <1 | <.01   | 19 | 660  | 10     | <5 | <20        | 11   | .02   | <10 | 16    | <10   | <1 | 73         |
| 66   | - L  | 32+00 8   | 6+    | 005   | <.2      | . 72  | 10      | 6 | 25  | <5   | .12     | <1 | 11 | ,  | 15 | 2.44  | .07  | 10   | .23    | 249    | <1 | .01    | 29 | 730  |        | <5 | <20        | 9    | .02   | <10 | 17    | <10   | 3  | 26         |
| 67   | - L  | 32+00 8   | 0+    | 50W   | <.2      | 1.73  | 10      | 6 | 95  | <5   | .17     | <1 | 20 | 12 | 12 | 3.94  | .05  | 10   | . 33   | 1324   | <1 | .02    | 24 | 650  | 14     | <5 | <20        | 16   | .06   | <10 | 18    | <10   | 1  | 103        |
| 68   | - L  | 32+00 S   | 1+    | 00W   | .2       | 1.41  | 15      |   | 120 | <5   | . 49    | <1 | 17 | 15 | 9  | 3.80  | .03  | <10  | .35    | 2857   | <1 | <.01   | 18 | 1200 | 10     | <5 | <20        | 17   | .08   | <10 | 28    | <10   | <1 | 130        |
| 69   | - L  | 32+00 8   | 1+    | 50W   | <.2      | . 58  | 10      | 4 | 30  | <5   | .05     | <1 |    |    | 9  | 2.64  | .02  | <10  | .14    | 203    | <1 | .01    | 9  | 320  | 12     | <5 | <20        | 5    | . 10  | <10 | 40    | <10   | 1  | 35         |
| 70   | - L  | 32+00 S   | 2+    | 100W  | <.2      | . 79  | 5       | 6 | 40  | <5   | .06     | <1 | 6  |    |    | 2.06  | .03  | <10  | .14    | 164    | <1 | .01    | 8  | 560  | 8      | <5 | <20        | 8    | .07   | <10 | 27    | <10   | <1 | 31         |
|      |      |           |       |       |          |       |         |   |     |      |         |    |    |    |    |       |      |      |        |        |    |        |    |      |        |    |            |      |       |     |       |       |    |            |

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BCO-TECH LABORATORIES LTD. Prank J. Pesnotti, A.Sc.T. B.C. Certified Assayer

ECO-TECH LABORATORIES LTD. 10041 EAST TRANS CAMADA HWY. KAMLOOPS, B.C. V2C 2J3 PHOME - 604-573-5700 FAX - 604-573-4557

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TECK EXPLORATIONS LTD.- ETK 91-600 960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5W1 5

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ATTENTION: FRED DALEY

VALUES IN PPN UNLESS OTHERWISE REPORTED

PROJECT NUMBER: 1703 2 Soil Samples Received August 6, 1991

| BT# | DESCRIPTION       | AU | AG  | AL(%) | λs<br> | B | BA | BIC | A(\$) | CD | <b>co</b> | CR | CU 78( | 1) X(1 | )   | LA NG | i(l) | KN<br>NOI | HO 3 | NA(\$) | NI | P   | P <b>B</b> | 8B | 8N  | 6R 1 | CI( <b>\</b> ) | V  | v  | ¥   | T  | IN. |
|-----|-------------------|----|-----|-------|--------|---|----|-----|-------|----|-----------|----|--------|--------|-----|-------|------|-----------|------|--------|----|-----|------------|----|-----|------|----------------|----|----|-----|----|-----|
|     |                   |    |     |       |        |   |    |     |       |    |           |    |        |        |     |       |      |           |      |        |    |     |            |    |     |      |                |    |    |     |    |     |
|     | 1-L 18+008 4+25 E | <5 | <.2 | 2.50  | <5     | 4 | 55 | <5  | .10   | <1 | 15        | <1 | 12 6.  | 80 .0  | 6 4 | <10   | . 30 | 320       | <1   | .02    | 15 | 730 | 20         | <5 | <20 | 8    | .04            | 10 | 15 | <10 | <1 | 57  |
| :   | 2-L 18+005 4+75 B | <5 | <.2 | 2.01  | <5     | 6 | 65 | <5  | .07   | <1 | 12        | 6  | 7 5.   | 94 .0  | 7 4 | <10   | . 33 | 219       | <1   | .01    | 11 | 580 | 16         | <5 | <20 | 6    | .06            | 10 | 30 | <10 | <1 | 64  |

NOTE: < = LESS THAN

AUGUST 27, 1991

ECO-TECH LABORATORIES LTD. CLINTON AVERS

ECO-TECH LABORATORIES LTD. 10041 EAST TRANS CANADA HWY. KAMLOOPS, B.C. V2C 2J3 PHONE - 604-573-5700 PAX - 604-573-4557

SEPTEMBER 11, 1991

VALUES IN PPH UNLESS OTBERWISE REPORTED

TECK EXPLORATIONS LTD.- ETK 91-709 960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5N1

ATTENTION: FRED DALEY / GREGG THOMPSON

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PROJECT NUMBER: 1703 27 Soil Samples Received August 29, 1991

| rt#   | DESCRIPTION       | DA  | AL(%) | <b>) (5</b> | B | BA  | BI | CA(1) | CD | c0 | CR | CU | PE(1) | X(1) | LA  | HG(%) | HN   | HO NA(&) | NI | P    | P8 - | 5B           | 8N  | 5R TI(\$) | U   | v  | W   | ¥  | IN  |
|-------|-------------------|-----|-------|-------------|---|-----|----|-------|----|----|----|----|-------|------|-----|-------|------|----------|----|------|------|--------------|-----|-----------|-----|----|-----|----|-----|
| 1- I  | . 16 + 008 4+ 25E | <.2 | 2.04  | 15          | 6 | 45  | <5 | .29   | <1 | 15 | 12 | 47 | 3.25  | .02  | <10 | .25   | 1242 | <1 .01   | 19 | 450  | 14   | <5           | <20 | 11 .05    | <10 | 16 | <10 | <1 | 62  |
| 2- I  | 16 + 008 4+ 75B   | <.2 | 1.72  | 15          | 6 | 40  | <5 | .16   | <1 | 12 | 11 | 23 | 3.14  | .02  | <10 | .23   | 532  | <1 <.01  | 15 | 470  | 14   | <5           | <20 | 7 .04     | <10 | 14 | <10 | <1 | 40  |
| 3- I  | 16 + 008 5+ 25E   | <.2 | .76   | 10          | 4 | 40  | <5 | .05   | <1 | 8  | 10 | 7  | 2.74  | .02  | <10 | .21   | 349  | <1 .01   | 12 | 1510 | 10   | <5           | <20 | 5 .08     | <10 | 29 | <10 | <1 | 41  |
| 4- I  | 16 + 008 5+ 75E   | <.2 | 2.31  | 25          | 6 | 35  | <5 | .10   | <1 | 9  | 9  | 9  | 4.48  | <.01 | <10 | .16   | 185  | <1 <.01  | 8  | 890  | 24   | <5           | <20 | 6.09      | <10 | 14 | <10 | <1 | 63  |
| 5- L  | 16 + 00S 6+ 25E   | <.2 | .40   | 5           | 4 | 30  | <5 | .02   | <1 | 4  | 2  | 8  | 1.35  | .01  | <10 | . 05  | 437  | <1 .01   | 6  | 240  | 6    | <5           | <20 | 2 .04     | <10 | 20 | <10 | 1  | 17  |
| 6- I  | 16 + 008 6+ 75K   | <.2 | . 34  | 10          | 6 | 20  | <5 | .03   | <1 | 5  | 3  | 4  | 1.30  | .02  | <10 | .07   | 148  | <1 <.01  | 8  | 200  | 12   | <5           | <20 | 3.03      | <10 | 21 | <10 | 1  | 28  |
| 7- L  | 18 + 008 5+ 258   | <.2 | 2.28  | 20          | 6 | 35  | <5 | .06   | <1 | 10 | 3  | 7  | 4.11  | <.01 | <10 | .16   | 229  | 1 <.01   | 8  | 500  | 22   | <5           | <20 | 5.12      | <10 | 29 | <10 | 1  | 54  |
| 8- L  | , 18 + 008 5+ 75E | <.2 | 2.05  | 20          | 4 | 30  | <5 | .14   | <1 | 11 | 7  | 11 | 3.83  | <.01 | <10 | .16   | 336  | 1 .01    | 12 | 550  | 22   | <5           | <20 | 7.06      | <10 | 15 | <10 | <1 | 57  |
| 9- L  | 21 + 948 3+ 768   | <.2 | 2.93  | 25          | 6 | 45  | <5 | .10   | <1 | 18 | 18 | 17 | 3.85  | .06  | 10  | . 45  | 400  | <1 <.01  | 33 | 1020 | 38   | <5           | <20 | 8.04      | <10 | 9  | <10 | 3  | 147 |
| 10- L | 22 + 008 3+ 458   | <.2 | 2.56  | 20          | 6 | 40  | <5 | .08   | <1 | 15 | 17 | 20 | 3.35  | .06  | 10  | . 42  | 338  | 1 .01    | 32 | 830  | 36   | <5           | <20 | 7 .03     | <10 | 9  | <10 | 3  | 117 |
| 11- L | 28 + 008 0+ 258   | .2  | 1.34  | 15          | 4 | 60  | <5 | .21   | <1 | 14 | 14 | 15 | 2.63  | .10  | 10  | . 33  | 1493 | <1 .01   | 27 | 380  | 18   | <5           | <20 | 10 .02    | <10 | 11 | <10 | 4  | 143 |
| 12- L | 28 + 005 0+ 758   | <.2 | 1.37  | 15          | 6 | 40  | <5 | .09   | <1 | 10 | 12 | 13 | 2.52  | .07  | <10 | .26   | 259  | <1 .01   | 16 | 340  | 16   | <5           | <20 | 7.02      | <10 | 13 | <10 | 1  | 56  |
| 13- L | 28 + 008 0+ 25W   | <.2 | .93   | 20          | 4 | 50  | <5 | .25   | <1 | 11 | 12 | 17 | 3.30  | .07  | <10 | .28   | 630  | <1 <.01  | 19 | 400  | 62   | <5           | <20 | 10 .02    | <10 | 13 | <10 | <1 | 123 |
| 14- L | 28 + 005 0+ 50W   | <.2 | 1.29  | 15          | 4 | 65  | <5 | .23   | <1 | 15 | 13 | 10 | 3.01  | .04  | <10 | . 31  | 1665 | <1 <.01  | 17 | 580  | 18   | <5           | <20 | 11 .04    | <10 | 16 | <10 | <1 | 108 |
| 15- L | 28 + 005 0+ 75W   | <.2 | 4.41  | 20          | 4 | 110 | <5 | 1.28  | <1 | 22 | 41 | 17 | 4.04  | .17  | <10 | .87   | 3043 | <1 .05   | 34 | 1660 | 16   | 5            | <20 | 60 .08    | <10 | 18 | <10 | <1 | 237 |
| 16- L | 28 + 008 1+ 00W   | <.2 | 1.73  | 15          | 6 | 140 | <5 | .24   | <1 | 16 | 16 | 14 | 3.01  | .04  | <10 | . 35  | 1268 | <1 .01   | 20 | 970  | 12   | <5           | <20 | 13 .05    | <10 | 19 | <10 | <1 | 135 |
| 17- L | 28 + 008 1+ 25W   | <.2 | 1.53  | 20          | 6 | 60  | <5 | .10   | <1 | 14 | 15 | 14 | 2.97  | .11  | 10  | . 42  | 687  | <1 <.01  | 27 | 790  | 40   | <5           | <20 | 8.02      | <10 | 7  | <10 | 2  | 187 |
| 18- L | 30 + 008 0+ 25E   | <.2 | 2.09  | 25          | 6 | 40  | <5 | .43   | <1 | 15 | 18 | 13 | 3.23  | .08  | 10  | .38   | 324  | <1 .02   | 24 | 510  | 14   | <5           | <20 | 32 .04    | <10 | 13 | <10 | 6  | 44  |
| 19- L | 32 + 008 0+ 75B   | <.2 | .79   | 15          | 4 | 25  | <5 | .17   | <1 |    | 10 | ,  | 2.85  | .04  | <10 | .27   | 128  | <1 <.01  | 14 | 270  | 10   | <b>&lt;5</b> | <20 | 8.02      | <10 | 10 | <10 | <1 | 29  |
| 20- L | 30 + 008 0+ 25W   | <.2 | .53   | 15          | 4 | 20  | <5 | .05   | <1 | 6  | 8  | 10 | 2.21  | .03  | <10 | .18   | 173  | <1 <.01  | 11 | 270  |      | <5           | <20 | 5 .02     | <10 | 14 | <10 | <1 | 30  |
| 21- L | 30 + 008 0+ 75W   | <.2 | . 89  | 15          | 4 | 35  | <5 | .08   | <1 | 10 | 12 | 12 | 2.51  | .07  | <10 | .28   | 232  | <1 <.01  | 17 | 280  | 10   | <5           | <20 | 7 .03     | <10 | 11 | <10 | <1 | 33  |
| 22- L | 30 + 006 1+ 25W   | <.2 | 1.52  | 15          | 4 | 35  | <5 | . 30  | <1 | 12 | 15 | 10 | 2.30  | .06  | 10  | . 32  | 445  | <1 .02   | 24 | 480  | 10   | <5           | <20 | 17 .02    | <10 | 8  | <10 | 5  | 37  |
| 23- L | 32 + 005 0+ 25E   | <.2 | .68   | 10          | 4 | 25  | <5 | . 59  | <1 | 10 |    | 17 | 2.00  | .04  | 10  | .18   | 258  | <1 <.01  | 21 | 350  | 8    | <5           | <20 | 13 .03    | <10 | 13 | <10 | 6  | 36  |
| 24- L | 32 + 005 0+ 25W   | <.2 | 1.24  | 15          | 4 | 45  | <5 | . 42  | <1 | 13 |    | 15 | 2.87  | .03  | <10 | .18   | 989  | <1 <.01  | 17 | 830  | 12   | <5           | <20 | 12 .04    | <10 | 13 | <10 | 1  | 85  |
| 25- L | 32 + 008 0+ 75W   | <.2 | 1.18  | 10          | 4 | 25  | <5 | .06   | <1 | 6  | 5  | 13 | 1.90  | .01  | <10 | .08   | 129  | <1 .01   | 8  | 330  | 10   | <5           | <20 | 4 .06     | <10 | 22 | <10 | 1  | 31  |
| 26- L | 32 + 008 1+ 25W   | .2  | .44   | 10          | 6 | 110 | <5 | .81   | <1 | 8  | 7  | 7  | 1.75  | .04  | <10 | .15   | 2181 | <1 <.01  | 10 | 480  | 6    | <5           | <20 | 20 .05    | <10 | 19 | <10 | <1 | 71  |
| 27- L | 32 + 008 1+ 75W   | <.2 | 1.73  | 15          | 4 | 40  | <5 | .08   | <1 | 11 | 12 | 13 | 2.50  | .02  | <10 | .19   | 445  | <1 .01   | 12 | 550  | 12   | <5           | <20 | 6.05      | <10 | 20 | <10 | <1 | 47  |

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ECO-TECH LABORATORIES LTD. PRANK J. PESSOTTI, B.C. Certified Assayer

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10041 BAST TRANS CAWADA HWY. Kamloops, B.C. V2C 2J3 PROME - 604-573-5700 PAX - 604-573-4557 TECK EXPLORATIONS LTD. - ETK 91-456

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960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5V1

ATTENTION: STRVE JENSEN

VALUES IN PPN UNLESS OTHERWISE REPORTED

AUGUST 1, 1991

PROJECT NUMBER: 1783 7 Soil Sinples received july 16, 1991

| 878<br> | DESCRIPTION          | AG AL(%) AS | 5 3 84 | BI CA(N) (  | D CO CE | CU FE(1) E(1) | LA HG(\$) HN HO | D HL(\$) HI P | PB SB SU    | SR TI(%) U  | 1 1 1     | 11 |
|---------|----------------------|-------------|--------|-------------|---------|---------------|-----------------|---------------|-------------|-------------|-----------|----|
| 1       | - L 34 +005 0 + 508  | < .2 .66 5  | 5 6 20 | < 5 .14 < 1 | 1 9     | 27 2.00 .02   | 20 .08 88 < 1   | < .01 19 270  | 10 < 5 < 20 | 7 .05 < 10  | 22 < 10 0 | 21 |
| 2       | - L 34 +005 1 + 00B* | (.2 .17 5   | 5 8 25 | (5 2.21 (1  | 6 1     | 13 1.23 .04   | 20 .19 362 < 1  | ( .81 16 548  | 10 < 5 < 20 | 20 .01 < 10 | 6 < 10 11 | 35 |
| 3       | - L 34 +005 1 + 50g  | (.2 2.52 5  | 5 6 95 | < 5 .55 ( 1 | 18 22   | 13 3.79 .20   | 20 .51 545 (1   | (.01 39 660)  | 16 < 5 < 20 | 17 .03 < 10 | 11 < 10 1 | 49 |
| 4       | - L 34 +005 0 + 000  | <.2.71 5    | 5 4 20 | < 5 .10 (1  | 6 1     | 16 2.11 .03   | 20 .10 106 < 1  | .01 13 390    | 8 < 5 < 20  | 6 .04 < 10  | 25 < 10 6 | 28 |
| 5       | - L 34 +005 0 + 500  | (.2 .56 15  | 5 4 30 | < 5 .11 (1  | 9 11    | 14 2.73 .04   | (10 .19 228 (1  | .01 13 530    | 12 < 5 < 20 | 7 .00 < 10  | 34 < 10 1 | 58 |
| 6       | - L 34 +005 1 + 00#  | (.2 1.31 10 | 0 6 30 | < 5 .11 (1  | 9 12    | 17 2.79 .05   | 10 .19 547 < 1  | <.01 13 620   | 10 < 5 < 20 | 7 .04 < 10  | 18 < 10 1 | 32 |
| 1       | - L 34 +005 1 + 50W  | < .2 2.42 5 | 5 6 60 | < 5 1.35 (1 | 19 22   | 18 3.03 .17   | 20 .75 564 < 1  | .01 35 760    | 12 5 < 20   | 38 .04 < 10 | 12 < 10 1 | 54 |

NOTE: ( = LESS THAN > = GREATER THAN

\* = -42 NESH

CC: STRVE JENSEN

P.O. BOX 207 GREENTOOD, B.C. VON 1JO C/O EVENING STAR MOTEL SC91/TRCK1

ECO-TECH LABORATORIES LTD. CLINTON AYERS LABORATORY HANAGER STREAM SILT

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10041 BAST TRANS CANADA NUT. KAMLOOPS, B.C. V2C 2J3 PNONE - 604-573-5700 PAX - 604-573-4557 TECK EXPLORATIONS LTD. - ETK 91-361

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960, 175 SECOND AVENUE KANLOOPS, B.C. V2C 5W1

ATTENTION: PRED DALLEY

JUNE 24, 1991

#### VALUES IN PPN UNLESS OTNERVISE REPORTED

PIGE 1

#### PROJECT NUMBER: 1783 38 SILT SIMPLES RECEIVED JUNE 19, 1991

| 6T)   |      | <b>D1</b>      | SCRIPT | 108 | 16  | )](\ | )             | 15 | 1 | N  | 11 | C1(1) | CD | CO | CE  | CU P | 1(\) | £(\) | 4   | NG(\) | XU  | NO N1(\) | 11 | P   | 23 | 53        | 51  | SE T | (1)   | U   | 1  | 1     | T  | 11 |
|-------|------|----------------|--------|-----|-----|------|---------------|----|---|----|----|-------|----|----|-----|------|------|------|-----|-------|-----|----------|----|-----|----|-----------|-----|------|-------|-----|----|-------|----|----|
| 361 - | - 1  | 1              | NGN S  | 1   | (.2 | 1.1  | 33            | 15 | 4 | 20 | (5 | 1.68  | (1 | 11 | 13  | 6    | 1.79 | .85  | (18 | .52   | 268 | (1 .02   | 15 | 540 | 10 | <5        | (28 | 82   | .03   | (10 | 10 | (1)   | 4  | 29 |
| 361 - | - 2  | 2              | NGN S  | 2   | <.2 | 1.1  | 13 .          | 15 | 4 | 35 | <5 | 4.32  | a  | 13 | 17  | 14   | 2.51 | .10  | (1) | .12   | 436 | (1 (0.01 | 19 | 548 | 14 | (5        | (21 | 112  | . 85  | (1) | 13 | (1)   | 5  | 43 |
| 361 - | • 3  | )              | NGN S  | 3   | <.2 | 1.1  | 15            | 15 | 4 | 25 | (5 | 1.17  | a  | 12 | 13  | 9    | 1.95 | .11  | (11 | .17   | 351 | (1 (0.01 | 11 | 558 | 18 | (5        | (28 | - 18 | .11   | (10 | ,  | (10   | 4  | 38 |
| 361 - | - 1  | 1              | NGN S  | 4   | <.2 | 2.2  | 20            | 15 | 4 | 40 | <5 | 4.53  | 4  | 11 | 21  | 18   | 2.07 | .11  | (18 | .91   | 417 | (1 (0.01 | 16 | 458 | 14 | (5        | (2) | 152  | .15   | (1) | 14 | (18   | 6  | 36 |
| 361 - | - 5  | 5              | NGN S  | 5   | ٢.2 | 2.4  | 17            | 15 | 1 | 10 | (5 | 3.56  | a  | 12 | 23  | 9    | 2.21 | .12  | (1) | .93   | 326 | (1 .44   | 17 | 788 | 16 | (5        | (2) | 166  | .16   | (10 | 15 | (1)   | 6  | 31 |
| 361 - | - 6  | 5              | NGN S  | 6   | <.2 | 1.1  | 15            | 15 | 4 | 20 | <5 | 2.07  | a  | 12 | 11  | 11   | 1.95 | .16  | (11 | .50   | 228 | (1 (0.01 | 28 | 630 | 18 | (5        | (2) | 58   | .83   | (18 | 1  | (1)   | 5  | 29 |
| 361 - | - 1  | Ι.             | NGN S  | 1   | <.2 | 2.1  | 13 1          | 28 | 4 | 65 | (5 | 3.49  | a  | 16 | 21  | 17   | 2.82 | .23  | 10  | 1.10  | 566 | (1 (0.01 | 25 | 650 | 18 | 5         | (20 | 110  | .11   | (18 | 17 | (10   | 12 | 52 |
| 361 - | - 1  | ) <sup>1</sup> | NGN S  | 1   | ٢.2 | 3.0  | 87            | 5  | 4 | 45 | (5 | 6.60  | a  | 11 | 25  | •    | 1.45 | .16  | (1) | 1.11  | 225 | (1 (0.01 | 14 | 578 | 16 | (5        | (28 | 191  | .07   | (10 | 16 | (1)   | 6  | 36 |
| 361 - | - 9  | )              | NGN S  | 9   | <.2 | 1.7  | 15            | 15 | 4 | 40 | (5 | 1.60  | a  | 11 | 11  | 10   | 1.94 | .14  | (10 | .70   | 288 | <1 <0.01 | 16 | 510 | 12 | (5        | (21 | 17   | . 85  | (10 | 12 | (1)   | 1  | 32 |
| 361 - | - 1  |                | NGN S  | 10  | (.2 | 1.9  | 6             | 20 | 4 | 48 | (5 | .96   | (1 | 14 | 11  | 11   | 2.51 | .11  | (1) | .52   | 318 | (1 .01   | 24 | 510 | 16 | (5        | (21 | 46   | .14   | (18 | 10 | (1)   | 5  | 51 |
| 361 - | - 1  | 1              | NGN S  | 11  | (.2 | 2.2  | 12 1          | 15 | 4 | 45 | (5 | 1.44  | (1 | 16 | 22  | 13   | 2.73 | .11  | 10  | .13   | 396 | (1 .14   | 26 | 558 | 16 | <5        | (21 | 92   | .16   | (10 | 14 | (10   | 3  | 38 |
| 361 - | - 1  | 2              | NGN S  | 12  | (.) | 1.6  | 54            | 10 | 4 | 30 | (5 | 5.88  | 0  | 11 | 17  | 3    | 1.82 | .11  | (1) | .15   | 262 | (1 (0.01 | 15 | 520 | 10 | (5        | (2) | 134  | .#    | (10 | 11 | (1)   | 5  | 32 |
| 361 - | - 1  | 3              | NGN S  | 13  | ٢.2 | .5   | 59            | 15 | 4 | 10 | (5 | 1.63  | (1 | 12 | 1   | 1    | 1.17 | .13  | 10  | . 95  | 214 | (1 (0.01 | 17 | 478 | 1  | (5        | (28 | 31   | .12   | (10 | 5  | (14   | 3  | 28 |
| 361 - | - 1  | 4              | NGN S  | 14  | <.2 | 1.5  | 58            | 15 | 4 | 30 | (5 | .91   | a  | 12 | 15  | 9    | 2.13 | .16  | (10 | .51   | 473 | 61 .B    | 11 | 578 | 12 | (5        | (28 | 78   | .11   | (10 | 10 | (1)   | 5  | 35 |
| 361 - | - 1  | 5              | NGN S  | 15  | <.2 | 1.2  | 11            | 15 | 4 | 30 | (5 | .65   | (1 | 13 | 12  | 9    | 2.01 | . 85 | 10  | .38   | 466 | (1 (0.01 | 19 | 558 | 10 | (5        | (28 | 31   | .83   | (18 | 1  | (1) " | 6  | 34 |
| 361 - | - 1  | 6              | NGN S  | 16  | (.2 | 1.7  | 12 :          | 15 | 4 | 40 | <5 | 1.62  | a  | 14 | 16  | 17   | 2.5  | .11  | 20  | .12   | 697 | (1 .02   | 33 | 611 | 16 | <b>(5</b> | (2) | 11   | .13   | (18 | •  | (18   | 12 | 40 |
| 361 - | - 1  | 1              | NGN S  | 17  | ٢.2 | . 6  | <b>13</b> – 1 | 15 | 4 | 28 | <5 | .20   | a  | 11 | l l | 1    | 1.56 | .14  | (11 | .24   | 258 | <1 <0.01 | 16 | 410 | 6  | (5        | <28 | 9    | .02   | (10 | 6  | (10   | 3  | 11 |
| 361 - | - 1  | 1              | KGN S  | 18  | <.2 | . 1  | 16            | 10 | 4 | 10 | (5 | .19   | (1 | 12 | 1   | 1    | 1.66 | .83  | 10  | .20   | 185 | (1 (0.01 | 19 | 510 | 4  | (5        | (21 | 1    | .02   | (18 | 6  | (1)   | 1  | 17 |
| 361 - | - 1  | 5              | NGN S  | 15  | <.2 | .1   | 16 1          | 15 | 4 | 28 | <5 | .26   | (1 | 12 | 10  | 9    | 1.88 | . 85 | 10  | . 29  | 211 | <1 <0.01 | 28 | 530 | 1  | (5        | <28 | 10   | .02   | <10 | 5  | (1)   | 5  | 26 |
| 361 - | - 2  |                | NGN S  | 20  | ٢.2 | 1.1  | 12            | 15 | 4 | 38 | (5 | .15   | (1 | 13 | 12  | 11   | 2.87 | .17  | 10  | . 44  | 521 | (1 (0.01 | 20 | 564 | 12 | (5        | (28 | 30   | .83   | (10 | 1  | (11   | 5  | 33 |
| 361 - | - 2  | 1              | NGN S  | 21  | <.2 | 1.3  | 37 :          | 24 | 6 | 30 | <5 | .94   | a  | 15 | 13  | 12   | 2.31 | .11  | 10  | .11   | 312 | (1 .01   | 24 | 598 | 14 | (5        | (20 | 41   | .13   | (1) | 6  | (1)   | 6  | 31 |
| 361 - | - 2  | 2              | NGN S  | 22  | (.2 | 1.1  | 11 1          | 15 | 6 | 25 | <5 | .58   | (1 | 13 | 12  | 14   | 2.13 | .16  | (1) | .36   | 361 | (1 (0.01 | 22 | 440 | 12 | (5        | <20 | 27   | .13   | (18 | 1  | (1)   | 1  | 37 |
| 361 - | - 2  | 3 1            | NGN S  | 23  | <.2 | 1.1  | 15 1          | 15 | 4 | 35 | (5 | .40   | (1 | 18 | 14  | B    | 2.28 | . 19 | 10  | . 42  | 365 | (1 (8.81 | 25 | 478 | 16 | (5        | <20 | 18   | . 82  | (10 | 6  | (10   | 5  | 31 |
| 361 - | • 2  | 4              | NGH S  | 24  | <.2 | 2.3  | 33 3          | 28 | 4 | 45 | (5 | .11   | 4  | 24 | 22  | 28   | 3.93 | .11  | 10  | .15   | 567 | (1 .84   | 40 | 788 | 20 | 5         | (2) | 78   |       | (18 | 10 | (1)   | 13 | 58 |
| 361 - | - 25 | 5 1            | NGN S  | 25  | (.2 | 1.5  | 59 3          | 28 | 4 | 45 | (5 | .41   | (1 | 25 | 15  | 23   | 2.41 | .11  | 28  | .51   | 625 | (1 (0.01 | 37 | 810 | 16 | <5        | <20 | 12   | .03   | (18 | 1  | (1)   | •  | 46 |
| 361 - | · 2( | 6 1            | IGN S  | 26  | (.2 | 1.3  | 30 3          | 20 | 4 | 48 | (5 | .21   | 4  | 15 | 14  | 15   | 2.41 | .11  | 20  | . 37  | 373 | <1 <0.01 | 48 | 588 | 12 | (5        | <28 | \$   | . \$2 | (18 | 6  | (10   | 21 | 30 |

#### TECK EXPLORATIONS LTD. - BTK 91-361

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PAGE 2 111 DESCRIPTION 1G  $M(\Lambda)$ 15 11 DI C1(1) CD CO CR CU PE(N) E(N) LA NG(N) HO HA(N) 1 NJ. 11 2 23 53 ŝĨ SE TI(1) U T T 1 28 361 - 27 NGM S 27 <.2 .65 25 <5 .25 (1 11 12 1.96 28 .26 15 , .11 592 (1 (0.01 24 750 <5 (21 1 . 01 (1) (1) 5 23 6 4 361 - 28 MGM 5 28 .13 15 25 (5 . 39 (1 16 10 14 2.19 20 .33 486 21 <.2 .11 (1 (1.11 141 (5 (20 .01 (1) 4 1 9 4 (11 13 22 361 - 29 MGH S 29 (.2 .41 15 1 18 <5 .21 (1 19 • 11 2.24 .14 10 .23 342 (1 (1.11 23 410 (5 (2) . 02 (10 6 1 1 (1) 5 19 (1 (0.01 361 - 30 NGH S 30 (.2 1.19 25 25 (5 .37 (1 23 16 27 3.39 .16 41 .51 (5 4 983 34 798 12 (28 11 . 12 (10 1 (14 1 39 58 (5 1.02 (1 21 16 24 2.60 .35 361 - 31 MGH S 31 (.2 2.68 28 4 . 16 41 1139 (1 (0.01 31 1040 16 **(5** (28 1 .83 (1) (1) 21 4 42 .51 361 - 32 MGM \$ 32 (.2 1.98 35 4 41 (5 (1 48 29 38 5.41 .14 " .54 132 (1 (0.01 100 151 14 (5 (28 16 .11 <10 • <10 55 53 361 - 33 HGH \$ 33 <.2 1.50 28 6 48 (5 .51 (1 16 17 15 2.63 .11 11 .42 331 (1 .12 26 540 14 (5 (2) 34 (10 .14 10 (1) 1 48 361 - 34 MGH S 34 (.2 1.72 15 38 (5 .94 (1 13 11 12 2.19 .# 10 .31 294 (1 .#2 25 628 28 65 4 (21 45 . 13 - (18 (1) 1 5 34 35 <5 361 - 35 MGM S 35 15 .53 (1 14 21 13 2.49 .11 11 .44 344 4. 1) 28 550 16 65 (.2 2.00 4 (2) 51 .11 (1) 12 (1) 5 41 361 - 36 NGH S 36 .92 15 25 **(5** .61 12 11 391 (5 (.2 4 <1 9 1.75 .16 11 .36 (1 (1.11 11 578 1 (20 21 . #2 (1) <18 6 26 4 361 - 37 MGH S 37 <.2 .50 15 4 15 <5 .21 (1 13 1 9 1.73 .14 10 .21 255 (1 (0.01 20 578 6 (5 (28 .41 (10 5 (18 1 5 16 361 - 38 MGH \$ 38 <.2 .4 15 4 15 ۲) .17 (1 13 9 1.72 .11 1 .21 239 (1 (0.01 28 -----4 (5 (28 5 .01 <10 5 (1) 21 1 4

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ECO-TECH LABORATORIES LTD. CLINTON ATERS LABORATORY MANAGER

NOTE: < = LESS THAN > = GREATER THAN

SC91/TECK2

10041 RAST TRANS CANADA HVY. KAMLOOPS, B.C. V2C 2J3 PHONE - 604-573-5700 PAX - 604-573-4557

JUNE 26, 1991

VALUES IN PPH UNLESS OTNERVISE REPORTED

TECK EXPLORATIONS LTD. - ETK 91-375

968, 175 SECOND AVENUE RAMLOOPS, B.C. V2C SV1

ATTENTION: FRED DALEY

PROJECT NUMBER: 1703 11 SILT SAMPLES RECEIVED JUNE 24, 1991

| RT         | DESCRIPTION             | AG AL(%)            | 15       | 1 | 11 | BI CL(1) | CD | CO | CR  | CU PE(N) | ) K(%)          | LA I | NG(\) | NN  | NO NA(N)             | <b>K</b> I     | P PB | 53       | SI         | SE TI(%)       | U   | 1 |     | 1 |          |
|------------|-------------------------|---------------------|----------|---|----|----------|----|----|-----|----------|-----------------|------|-------|-----|----------------------|----------------|------|----------|------------|----------------|-----|---|-----|---|----------|
| 1 -        | NGN 539                 | <.2 . <b>86</b>     | 15       | 6 | 25 | <5 1.55  | (1 | 16 | 11  | 14 2.5   | 2.11            | 20   | .47   | 641 | (1 (8.81             | 25 58          | 1 16 | <\$      | <20        | 13 .41         | (1) | 1 | (1) | 5 | 45       |
| 2 -        | NGN 540<br>NGN 541      | <.2.72<br><.7.78    | 18       | ł | 25 | (5.21    | 0  | 13 | 10  | 9 1.7    | 5. <b>8</b> 7   | 18   | .25   | 354 |                      | 19 41          |      | <5<br>/5 | <20<br>(20 | 7 .01<br>16 A2 |     | 6 | (18 | 4 | 17       |
| 1-         | NGN 542                 | (.2 .75             | 15       | 6 | 15 | (5.45    | ä  | 16 | ,10 | 12 2.4   |                 | 21   | .43   | 511 | (1 (0.01             | 22 56          | 12   | ćŚ       | <20        | 15 .02         | (1) | 6 | a   | i | 36       |
| 5 -        | NGN 543                 | <.2 . <b>8</b> 5    | 15       | ļ | 15 | (5.41    | 0  | 19 | 18  | 14 2.4   | i .ii           | 20   | .43   | 558 | (1 (0.01             | 21 11          | 10   | (5       | (28        | 8.83           | (1) | ļ |     | 5 | 23       |
| 1 -<br>7 - | NGN 546<br>NGN 545      | (.2 .13             | 15<br>15 | 6 | 20 | (5.19)   | 4  | 14 | 12  |          | 5.43            | 1    | .12   | 283 | <1 <0.01<br><1 <0.01 | 21 61<br>16 41 |      | ()<br>() | (28<br>(28 | 15 .02         |     |   |     | 1 | 58<br>22 |
| 1 -        | NGN 546                 | (.2 .76             | 10       | 6 | 15 | (5 .53   | ä  | 13 | n   | 11 2.1   | 5.11            | 20   | .37   | 475 | (1 (0.01             | 21 61          | ii   | (5       | (20        | 15 .82         | (1) | 1 | a   | 5 | 31       |
| 9 -        | TSAP 1                  | <.2 1.49            | 30       | ş | 10 | (5.64    | 0  | 22 | 24  | 44 3.9   | <b>5 (0.0</b> 1 | 1    | .90   | 496 |                      | 37 14          | 12   | (5       | <20        | 5 (0.01        |     | 5 | (18 | 0 | 1        |
| 10 -       | тэлк 2<br><b>Тэле</b> 3 | <.2 1.44<br><.2 .64 | 15       | 6 | 15 | (5.3)    | 4  | 16 | 11  | 20 2.3   |                 | 30   | .42   | 619 |                      | 25 11<br>25 71 |      | (5       | <20        | 5 .02          |     | 6 | (10 | 4 | 21       |

NOTE: < = LESS THAN

> = GREATER TEAM

ECO-TECH LABORATORIES LTD. CLIBTON AYERS LABORATORY MANAGER

# APPENDIX D

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Analytical Procedures



ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamioops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

#### GEOCHEMICAL LABORATORY METHODS

#### SAMPLE PREPARATION (STANDARD)

- Soil or Sediment: Samples are dried and then sieved through 80 mesh sieves.
  Rock, Core: Samples dried (if necessary), crushed, riffled to pulp size and pulverized to approximately -140 mesh.
- 3. Humus/Vegetation: The dry sample is ashed at 550 C. for 5 hours.

#### METHODS OF ANALYSIS

All methods have either cannet certified or in-house standards carried through entire procedure to ensure validity of results.

#### 1. MULTI ELEMENT ANALYSES

| l  | <b>a</b> ) | ) ICP | Package | es (6 | ,12 | , 30 | element) | ۱. |
|----|------------|-------|---------|-------|-----|------|----------|----|
| ۰. | _          |       |         |       | ,   |      |          |    |

Digestion Finish ------Hot Agua Regin ICP

(b) ICP - Total Digestion (24 element).

Digestion Finish

Hot HClO4/HNO3/HF

ICP

Atomic Absorption

\* = Background corrected

- (c) Atomic Absorption (Acid Soluble) Ag\*, Cd\*, Cr, Co\*, Cu, Fe, Pb\*, Mn, Mo, Ni\*, Zn.
  - Digestion Pinish

Hot Aqua Regia

(d) Whole Rock Analyses.

| Digestion                    | Finish |
|------------------------------|--------|
| Lithium Metaborate<br>fusion | ICP    |



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# ECO-TECH LABORATORIES LTD.

ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamioops, B.C. V2C 2J3 (604) 573-5700 Fax 573-4557

2. Antimony Digestion Finish \_\_\_\_\_ Hot agua regia ICP 3. Arsenic Digestion Finish Hot aqua regia Hydride generation - A.A.S. 4. Barium Digestion Finish -------------Lithium Metaborate ICP 5. Beryllium Digestion Finish ------\_\_\_\_\_ Hot aqua regia Atomic Absorption 6. Bismuth Digestion Finish -----Hot aqua regia Atomic Absorption (Background Corrected) 7. Chromium Digestion Finish \_\_\_\_\_ \_\_\_\_\_ Sodium Peroxide Atomic Absorption Fusion 8. Flourine Digestion Finish ----------------Lithium Metaborate Ion Selective Electrode Fusion



ASSAYING - ENVIRONMENTAL TESTING 10041 East Trans Canada Hwy., Kamioops, B.C. V2C 2J3 (604) 573-5709 Fax 573-4657

9. Gallium

Digestion

# Finish

Hot HC104/HN03/HF

Atomic Absorption

Atomic Absorption

#### 10. Germanium

Digestion

Finish

Hot HClO4/HNO3/HF

11. Mercury

| Digestion      | Finish                         |
|----------------|--------------------------------|
|                |                                |
| Hot aqua regia | Cold vapor generation - A.A.S. |

Finish

Finish

A.A.S.

-----

Hydride generation -

-----

ICP finish

12. Phosphorus

Digestion

Lithium Metaborate Fusion

13. Selenium

Digestion

Hot aqua regia

#### 14. Tellurium

Digestion

Finish ------

Hot aqua regiaHydride generation - A.A.S.Potassium BisulphateColorimetric or I.C.P.FusionFusion

# APPENDIX E

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Rock Sample Descriptions

| PROJECT:      | IGM (1                  | 703)                    |             | DATE:  |   | TYPE: ICP GEOCHI                     | EM                          | NAME:   |  |  |
|---------------|-------------------------|-------------------------|-------------|--|---|--------------------------------------|-----------------------------|---|--|--|
| SAMPLE<br>NO. | РЬ                      | Zn                      | Ag          | LITHOLOGY &<br>SAMPLE TYPE                         | LOCATION                                      | MINERALIZATION                       | ALTERATION                  | VEINING &<br>TEXTURES                         | STRUCTURAL<br>ASPECTS  | COMMENTS   |
| 34051         | 128<br><sub>PP</sub> m  | 25<br>ppm               | 1.2<br>9/1  | Grab<br>Siliceous fine<br>grainged<br>metasediment | Slightly over 500m<br>up Tsar Creek           | Pyrrhotite                           | Silica<br>sericite          |   |  | From boulder on<br>Tsar Ck assumed to<br>have come from<br>above |
| 34052         | 8<br><sub>PPm</sub>     | 63<br><sub>PPM</sub>    | 7.2<br>g/t  | Grab - Rock<br>Micaceous<br>Limestone              | NW side<br>Tsar Creek inlet                   |                                      | Rusty, strongly<br>oxidized |   | Minor Folds,<br>moderately to<br>strongly schistose<br>@131-65 |  |
| 34062         | 0.4<br>%                | 0.2<br>•/o              | 0.6<br>g/t  | Grab<br>Quartz-sericite<br>schist                  | L 20+00S<br>4+10E                             | Minor Galena<br>Trace dissem. Pyrite | Silica                      | Waxy<br>appearance                            |  |  |
| 34064         | <2<br>ppm               | 63<br>ppm               | 0.6<br>g/t  | Grab<br>Choc. br. dolomite                         | L 20+05S<br>4+30E                             |                                      |                             | f.g.<br>unweathered<br>rock cream<br>coloured |  | Under uprooted<br>tree   |
| 34086         | 0.76<br>%               | 0.02<br>%               | 24.4<br>9/t | Chip<br>Massive sulphide<br>zone                   | North side<br>Cummins river<br>canyon showing | Pyrite, Galena, minor<br>Sphalerite  |                             |   | Zone at 140-53   |  |
| 34087         | 0.12<br>%               | 0.13<br>%               | 2.4<br>9/t  | Grab<br>Pyrite layer                               | North Rd. showing<br>Trench 2                 | Pyrite, minor Sphalerite             |                             |   | Rythmic py. bands<br>up to 15cm wide<br>@145-20                |  |
| 34088         | 0.10<br>%               | 0.55<br>%               | 1.2<br>g/t  | Grab<br>Choc. br. dolomite                         | North Rd. showing<br>Trench 3                 | Pyrite veinlets                      |                             |   | Py. veinlets are foliation parallel                            | -  |
| 33855         | 18<br><sub>Ppm</sub>    | 321<br><sub>PP</sub> m  | 0.2<br>g/t  | Grab<br>Micaceous quartzite                        | North Rd. showing<br>Trench 1                 | Minor pyrite                         |                             |   |  |  |
| 33856         | 1978<br><sub>PP</sub> m | 6056<br><sub>PP</sub> m | 7.0<br>g/t  | Grab<br>Rusty to Choc. br.<br>weathered dolomite   | North Rd. showing<br>Trench 1                 | Galena, Sphalerite,<br>Pyrite        |                             |   | Near antiformal<br>axis  |  |
| 34092         | 190<br>ppm              | 1495<br><sub>PP</sub> m | 4.2<br>9/t  | Choc, br,<br>weathering dolomite                   | North Rd. showing<br>Trench 4                 |                                      |                             |   | S @150-30  |  |

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| PROJECT: M    | GM (1703 | 3) | DATE:   |  | TYPE: WHOLE ROO                         | K ANALYSIS      | NAME:   |   |   |
|---------------|----------|----|---|--|---|-----------------|---|---|---|
| SAMPLE<br>NO. |          |    | LITHOLOGY   | LOCATION                                 | MINERALIZATION                          | ALTERATION      | VEINING &<br>TEXTURES                                     | STRUCTURAL<br>ASPECTS                     | COMMENTS                                  |
| 34065         |          |    | Thinly laminated,<br>siliceous Quartz-<br>sericite schist | L 20+00S<br>4+10E                        |   |                 | fine grained<br>waxy cream<br>coloured                    | Schistosity<br>@154-35                    | Hanging wall                              |
| 34066         |          |    | Thinty laminated,<br>siliceous Qtz-ser<br>schist          | L 20+00S<br>4+18.9E                      | Trace Galena,<br>Sphalerite             | Yellowish stain | Same as above<br>laminated to<br>more massively<br>bedded | S @133-55<br>Mineral lineation<br>@313-08 | Hanging wall                              |
| 34067         |          |    | Choc. br. weathered<br>siliceous Qtz-ser<br>schist        | L 20+00S<br>4+20.5E                      |   | Manganese       |   | S @129-48                                 | Possible dołomitic<br>portion             |
| 34068         |          |    | Gametiferous sericite<br>schist                           | L 20+00S<br>4+24E                        |   | Silica          | thinly laminated  |   | Pink subhedral 2-<br>10mm sized garnets   |
| 34069         |          |    | Qtz-ser schist  | L 20+00S<br>4+37E                        |   | Silica          | thinly laminated  |   | unit much like 34065                      |
| 34070         |          |    | Garnet schist   | L 20+00S<br>5+6.5E                       |   | Sericite        | very friable,<br>garnets easily<br>freed from matrix      |   | Footwall                                  |
| 34072         |          |    | Grab<br>Choc. br.<br>dolomitic breccia                    | N. Side<br>300m up from old<br>drill rd. | Minor Pyrite                            | Manganese       | calcite veinlets  | Bedding @35-40                            | drill rd. was for 1985<br>Esso DDH-2<br>- |
| 34073         |          |    | Qtz-ser schist  | South side<br>Cummins river              |   |                 |   | S @122-44<br>sericite defines fot.        | Hanging wall                              |
| 34075         |          |    | Pyritic dolomite  | South side<br>Cummins river              | Galena, pyrite bands<br>up to 10cm wide | Silica          |   | S @128-75                                 |   |
| 34076         |          |    | Gamet-musc schist   | South side<br>Cummins river              |   |                 |   | S @140-78                                 | Footwall                                  |
| 34077         |          |    | Qtz-ser schist  | North side<br>Cummins river              | Minor pyrite                            |                 | thinly laminated  | S @136-65                                 | Hanging wall                              |

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| PROJECT: M    | <b>GM (</b> 17 | 03) | DATE:                                       |                               | TYPE: WHOLE ROO   | K ANALYSIS             | NAME:   |   |   |
|---------------|----------------|-----|---|-------------------------------|---|------------------------|---|---|---|
| SAMPLE<br>NO. |                |     | LITHOLOGY                                   | LOCATION                      | MINERALIZATION  | ALTERATION             | VEINING &<br>TEXTURES   | STRUCTURAL<br>ASPECTS                     | COMMENTS  |
| 34078         |                |     | Silicified pyritic unit                     | North side<br>Cummins river   | 30% pyrite<br>minor galena,<br>sphalerite                     | Silica                 | very fine grained<br>difficult to distinguish<br>original lithology | S @140-53                                 | Hanging wall  |
| 34079         |                |     | Muscovite schist                            | North side<br>Cummins river   |   | Rusty oxidized<br>unit |   | S @131-69                                 | Footwall  |
| 34080         |                |     | Gamet-musc schist                           | North side<br>Cummins river   |   |                        |   | S @135-61                                 | Footwall  |
| 34081         |                |     | Limy Garnet schist                          | North side<br>Cummins river   |   |                        |   |   | Hanging wall<br>Intercalated<br>calcareous material<br>1-3cm reddish<br>brown garnets |
| 34082         |                |     | Strongly magnetic<br>oxide zone             | North Rd. showing<br>Trench 1 | Magnetite   | Manganese              |   |   |   |
| 34083         |                |     | Micaceous Quartzite                         | North Rd. showing<br>Trench 1 | Pyritic bands up to<br>1cm in width                           |                        | Laminated   |   | Fine grained white<br>to grey<br>Same location as<br>ICP sample 33855                 |
| 34084         |                |     | Fine grained<br>micaceous dolomite          | North Rd. showing<br>Trench 1 |   |                        |   | well foliated<br>S @150-30                | •-  |
| 34085         |                |     | Brecciated Choc. br.<br>weathering dolomite | North Rd. showing<br>Trench 1 | Pyrite, galena,<br>sphalerite associated<br>with Qtz veinlets | Sericite               |   | S @284-22                                 |   |
| 34092         |                |     | Choc. br. weathering<br>dolomite            | North Rd. showing<br>Trench 4 |   |                        |   | S @150-30                                 |   |
| 34093         |                |     | Quartz-sericite schist                      | North Rd. showing<br>Trench 4 |   |                        | Thinly laminated  | S @140-34<br>mineral lineation<br>@316-06 | Hanging wall  |

| PROJECT: M    | GM (1703) | ) | DATE:   |                               | TYPE: WHOLE ROO | K ANALYSIS | NAME:                           |                       |  |
|---------------|-----------|---|---|-------------------------------|-----------------|------------|---------------------------------|-----------------------|--|
| SAMPLE<br>NO. |           |   | LITHOLOGY   | LOCATION                      | MINERALIZATION  | ALTERATION | VEINING &<br>TEXTURES           | STRUCTURAL<br>ASPECTS | COMMENTS   |
| 34094         |           |   | Garnet schist   | North Rd. showing<br>Trench 4 |                 | Sericite   | 5-10mm garnets grey f.g. matrix | S @154-30             | Hanging wall   |
| PROJECT: M    | GM (1703) | ) |   |                               | TYPE: GARNET WH | IOLE ROCK  | NAME:                           |                       |  |
| SAMPLE<br>NO. |           |   | LITHOLOGY   | LOCATION                      | MINERALIZATION  | ALTERATION | VEINING &<br>TEXTURES           | STRUCTURAL<br>ASPECTS | COMMENTS   |
| TG-1          |           |   | 1-1.5cm, brownish<br>red euhedral<br>garnets                          | L 33+05S<br>1+50W             |                 |            |                                 |                       | Near Kinbasket-<br>Tsar Creek<br>formationat<br>boundary |
| CG- 1         |           |   | 1-3.0cm, black to<br>brownish red<br>subhedral to<br>euhedral garnets | L 3+30N<br>2+35E              |                 |            |                                 |                       | Hanging wall<br>garnets near<br>sulphide horizon         |
| 34063         |           |   | 0.5-1.0cm brownish<br>red subhedral to<br>euhedral garnets            | L 25+75S<br>0+20W             |                 |            |                                 |                       | Near Kinbasket-<br>Tsar Creek<br>formational<br>boundary |
|               |           |   |   |                               |                 |            |                                 |                       |  |
|               |           |   |   |                               |                 |            |                                 |                       |  |

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| PROJECT: M    | GM (170 | 3) | DATE:  |                                      |   |            | NAME:                 |                                |   |
|---------------|---------|----|--|--------------------------------------|---|------------|-----------------------|--------------------------------|---|
| SAMPLE<br>NO. |         |    | LITHOLOGY  | LOCATION                             | MINERALIZATION  | ALTERATION | VEINING &<br>TEXTURES | STRUCTURAL<br>ASPECTS          | COMMENTS  |
| 34071         |         |    | Waxy grey-white to<br>yellowish Quartz-<br>sericite schist | Cominco<br>DDH-C-91-2<br>@245m depth | minor pyrite and<br>graphite on foliation<br>surfaces |            |                       |                                | Hanging wall  |
| 34089         |         |    | Limy garnet schist   | Cominco<br>DDH-C-91-2<br>@223m depth |   |            |                       |                                | Hanging wall  |
| 34090         |         |    | Dolomite<br>Hosts sulphide<br>horizon                      | Cominco<br>DDH-91-2<br>@260m depth   | minor sphalerite,<br>galena and pyrite                | Silica     |                       |                                | Light grey medium<br>grained dolomite<br>with thinly laminated<br>sulphides |
| 34091         |         |    | Garnet schist  | Cominco<br>DDH-91-2<br>@264m depth   |   |            |                       | Bedded horizon,<br>1-4cm width | Footwall<br>Argilliceous<br>component                                       |
|               |         |    |  |                                      |   |            |                       |                                |   |
|               |         |    |  |                                      |   |            |                       |                                |   |
|               |         |    |  |                                      |   |            |                       |                                |   |
|               |         |    |  |                                      |   |            |                       |                                |   |

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# APPENDIX F

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Geophysical Instrumentation and Field Technique

## Instrumentation

The MaxMin II is a continously portable horizontal loop EM system which measures inphase and quadrature components of an induced electromagnetic field and compares them to a reference field provided by a fixed link. The Unit has frequencies of 222, 444, 888, 1777 and 3555 Hz and coil separations from 50 to 200 metres.

## **Field Technique**

The survey was performed at two frequencies, 444 and 1777 Hz. Coil separation was kept at 100 metres.

The coils were kept coplanar by using inclinometer chaining notes while horizontal separation was kept constant by the tight chain method. Any short cable effects were compensated for using the inclinometer data. Data was plotted daily and presented as field plots and as a DXF computer file.

Alan Wynne Consulting Geophysicist Maple Services/MWH Geo-Surveys Ltd. Sept. 11, 1991





![](_page_91_Figure_0.jpeg)

![](_page_92_Picture_0.jpeg)

![](_page_93_Picture_0.jpeg)

![](_page_94_Figure_0.jpeg)

**-** . • • m U • \$ 34063 ∕∕ sc 800 LEGEND

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- × Rock Assay or ICP
- D Whole Rock
- ♦ Garnet Analysis

500

• Soil Sample -sample numbers correspond with grid locations

![](_page_94_Picture_6.jpeg)

![](_page_95_Figure_0.jpeg)

![](_page_96_Picture_0.jpeg)

| 1600.0 E<br>1200.0 E                                 |  |  |                         |                            |          |                   |                                       |  |   | ·                                     |   |                                     |   |
|--|--|--|-------------------------|----------------------------|----------|-------------------|---------------------------------------|--|---|---------------------------------------|---|-------------------------------------|---|
| 200.0 E  |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     |   |
| DO.0 E   |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     |   |
| 20.0 E   |  |  |                         |                            |          |                   |                                       | -<br>-   |   |                                       | **  |                                     |   |
| <u>90,0 E</u>  |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     |   |
| 200.0 E  |  |  |                         |                            |          | . ·               |                                       | •  |   |                                       |   |                                     |   |
| 200.0 E  |  |  |                         |                            | •        |                   |                                       |  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          |                   |                                       | •  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          | ·                 |                                       | · .  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          |                   |                                       | 1  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          |                   |                                       |  | •   |                                       | •   |                                     |   |
| 800.0 E  |  |  |                         |                            |          |                   |                                       |  | •   |                                       |   |                                     | na sa |
|  | **************************************   |  |                         |                            | . + 19.0 | + <del>36.0</del> | + 37.0<br>+ 61.0                      |  |   | · · · · · · · · · · · · · · · · · · · |   |                                     |   |
|  |  | +68  | 8.0 +35.0               |                            | - 39.0   | +18.0             | - 42.0<br>- 28.0                      | +42.0  |   |                                       |   |                                     |   |
|  |  | +42  | 2.0 +56.0<br>1.0 +66.0  |                            | + 29.0   | +24.0<br>+48.0    | + 14.0<br>+ 17.0<br>+ 43.0            | + 40 . 0<br>+ 69 . 0   | +24.0<br>+57.0<br>+56.0 +30.0                   | +12.0<br>+33.0 +29.0                  | +25.0 +4  | 1.0 +26.0                           |   |
|  |  | - 75   | 53.0 +33.0              | - 28.0                     | • - 39.0 | +38.0             | +63.0<br>+42.0<br>+41.0               | +57.0<br>+70.0<br>+54.0  | -36.0 +18.0                                     | -32.0 +19.0                           | +31.0 +1  | 2.0 -73.0                           |   |
|  |  | +87  | 7.0 +131.0<br>7.0 +31.0 | -29.0                      | 96.0     | +81.0             | 46.0<br>40.0<br>49.0                  | +59.0<br>+64.0<br>+52.0  | +23.0 +25.0<br>+39.0<br>+464.0 +38.0            | +36.0 +25.0<br>+16.0<br>+33.0 +68.0   | +27.0 +4  | 5.0 -36.0                           |   |
| 400.0 E  |  | 83   | <del>3.0</del> +27.0    | 36.0                       |          | +31.0             | -62.0<br>-113.0                       | +57.0<br>+84.0   | 404.0 + 30.0<br>+ 109.0 + 43.0<br>+ 96.0 + 28.0 | +23.0<br>+25.0<br>+27.0               | 10.0 +4<br>17.0 +4                              | 4.0 25.0                            |   |
|  | + 136.0  | +11  | 17.0 +52.0              | -113.0                     | - 37.0   | +80.0             | 48.0                                  | +76.0  | +61.0<br>+103.0 +62.0<br>+50.0                  | +54.0<br>+36.0 +50.0<br>+108.0        | +31.0 +2  | 9.0 43.0                            | •   |
|  | +76.0<br>+50.0   | - 48   | 8.0 +133.0   3.0 +98.0  | +45.0 +65.0<br>+62.0 +71.0 | + 35.0   | + 76.0<br>+ 42.0  | +91.0<br>+82.0                        | +114.0<br>+106.0   | +140.0 +53.0 +48.0                              | +66.0 +49.0<br>+53.0<br>+88.0 +69.0   | +47.0 +4  | 1.0<br>9.0<br>+46.0<br>+55.0        |   |
|  | +101.0   | -58  | 8.0 +42.0               | +72.0 +56.0<br>+79.0       | +63.0    | +36.0             | 69.0                                  | +164.0<br>+89.0  |   | +106.0<br>+75.0                       | +77.0 +2  | 4.0 -43.0                           |   |
|  | +88.0<br>+83.0   | +54  | 4.0 +84.0<br>9.0 +77.0  | +89.0                      | + 41.0   | +30.0             | + 100.0                               |  |   |                                       | +41.0 +41.0 +41.0 +41.0 +41.0 +41.0 +41.0 +41.0 | 5.0 +64.0<br>9.0 +49.0              | +49.0<br>+35.0                            |
|  | +42.0  | -80  | 0.0 +189.0              |                            |          |                   |                                       |  |   | · · · · · · · · · · · · · · · · · · · | +56.0 +29<br>+101.0 +2<br>+143.0 +4             | 9.0<br>7.0 + 31.0<br>4.0 + 36.0     | +21.0                                     |
| 0.0 E  | <b>↓</b> + 150 . 0   | 10   | <del>08.0</del>         |                            |          |                   |                                       |  |   |                                       | +156.0 +3<br>+123.0 +30<br>+108.0 +40           | 3.0 43.0   0.0 +85.0   103.0 +103.0 | +28.0                                     |
|  |  |  |                         |                            |          | •                 |                                       |  |   |                                       | +237.0 +3<br>+135.0 +2<br>+187.0 +2             | 3.0 -31.0   7.0 -130.0   7.0 -71.0  | +32.0                                     |
|  |  |  |                         |                            |          |                   |                                       |  |   | •                                     | +3  | 2.0 +35.0<br>+47.0                  | +54.0                                     |
| •  |  |  |                         |                            |          |                   |                                       |  |   |                                       |   | +31.0                               |   |
|  |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     |   |
| -400.0 E   |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     | · · · · · · · · · · ·                     |
|  |  |  |                         |                            |          |                   |                                       |  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          |                   | :                                     | •  |   |                                       |   |                                     |   |
|  |  |  |                         |                            |          |                   |                                       |  | •   |                                       |   |                                     |   |
| 2  |  |  |                         |                            |          |                   |                                       | •  |   |                                       |   |                                     |   |
| -800.0 E   |  |  |                         |                            |          |                   |                                       |  |   | J                                     |   |                                     |   |
|  |  | 0.0 S  |                         | 800.0 S                    | 4200 0 S |                   | 1600.0 S                              | 2<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 |   | 2400.0 S                              | 2800 0 S  | S<br>0<br>000                       |   |
| NICK-PLOT<br>Encon Services Inc.<br>Horizontal Scale | DATE = 26-05-92     Teck Exp       TIME = 11: 43: 25     Kamloops       E =     1 : 5000     VERTICA | plorations Limited TECK EXPLORATION LTD<br>s Office SOIL SAMPLES Zn<br>TAL SCALE = 1: 5000 | ZINC<br>Soil Geochen    | nistry metres              | FIGURE 1 | 9                 | · · · · · · · · · · · · · · · · · · · |  |   |                                       |   |                                     |   |

| Market   A <th></th> <th></th> <th>1</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>   |   |   | 1                                  |  |                           |  |   |   |                            |   |  |
|---|---|---|------------------------------------|--|---------------------------|--|---|---|----------------------------|---|--|
|   | 1500 0 E  |   |                                    | an a fa an |                           |  |   |   |                            | i kana kan di kana dara kana ya |  |
| N   -   |   |   |                                    |  |                           |  | ,   |   |                            |   |  |
|   |   |   |                                    |  |                           |  |   |   |                            |   |  |
| 3   |   |   |                                    |  |                           |  |   |   |                            |   |  |
| 1     | E.  |   |                                    |  |                           |  |   |   |                            |   |  |
| M   -   |   |   |                                    |  |                           |  |   |   |                            |   |  |
| 1   01   0  | 1200.0 E  |   | r                                  |  |                           |  |   |   |                            |   |  |
| n     |   |   |                                    |  |                           | ч.<br>   |   |   |                            |   |  |
| MA  |   |   |                                    |  |                           |  |   |   |                            |   |  |
| Main A  |   |   |                                    |  |                           |  |   |   |                            |   |  |
|   | *   |   |                                    |  |                           |  |   |   |                            |   |  |
| Image: Problem in the second of the secon |   |   |                                    |  |                           |  |   |   |                            |   |  |
| 1   3   3   -   | 800.0 E   |   |                                    |  |                           | 10.0   |   |   |                            |   |  |
| 1     |   |   |                                    |  | -8.0                      | 18.0   |   |   |                            |   |  |
| AD   AD <td< th=""><th></th><th></th><th>- 30.0 + 12.0<br/>- 26.0 + 18.0</th><th>· ·</th><th>+4.0 +12.0<br/>+12.0 +6.0</th><th>+ 18.0<br/>+ 12.0<br/>+ 10.0<br/>+ 10.0</th><th></th><th>+8.0 +4.0</th><th></th><th></th><th></th></td<>   |   |   | - 30.0 + 12.0<br>- 26.0 + 18.0     | · ·  | +4.0 +12.0<br>+12.0 +6.0  | + 18.0<br>+ 12.0<br>+ 10.0<br>+ 10.0                               |   | +8.0 +4.0                                       |                            |   |  |
| Image: second               |   |   | 18.0 +16.0                         |  | 8.0 +18.0                 | +6.0<br>+16.0 +24.0<br>+24.0 +22.0                                 | + 14.0<br>+ 1.0   | +10.0 +8.0                                      | +14.0 +8.0                 | + 10.0  | 8.0                                      |
| 1     |   |   | 490.0 + 14.0                       | -8.0   | + 10.0 + 14.0             | +18.0 +12.0   +10.0 +22.0  | + 16.0  | +12.0 +12.0                                     | +8.0 -8.0                  | +.0   | - 10.0                                   |
| a.t.   b.t.  |   |   | + 30.0 + 44.0 -<br>+ 16.0 + 14.0 - | + 10 . 0<br>                                   | +16.0 +22.0<br>+12.0 +8.0 | $\begin{array}{c} +16.0 \\ +12.0 \\ +14.0 \\ +12.0 \\ \end{array}$ | + 10.0<br>+ 16.0<br>+ 102.0                                     | + 12.0<br>+ 8.0<br>+ 18.0<br>+ 12.0             | +16.0<br>+22.0 +6.0        | +8.0  | + 12.0<br>+ 4.0                          |
| 1.14   -0.5   0.7 <td< td=""><td>400.0 E</td><td></td><td>+32-0+16-0</td><td>·<br/>-14.0</td><td>+12.0</td><td>+14.0 +20.0<br/>+8.0 +18.0</td><td>+66.0</td><td>+22.0 +12.0<br/>+16:0 +12:0 +12:0 +12:0 +10.0</td><td>+16.0</td><td>+10:0</td><td></td></td<>   | 400.0 E   |   | +32-0+16-0                         | ·<br>-14.0                                     | +12.0                     | +14.0 +20.0<br>+8.0 +18.0  | +66.0   | +22.0 +12.0<br>+16:0 +12:0 +12:0 +12:0 +10.0    | +16.0                      | +10:0   |  |
|   | +28.0   |   | 38.0 +18.0                         | 16.0   | + 14.0                    | +10.0 +20.0  | + 16.0  | + 32.0 + 12.0<br>+ 18.0 + 16.0<br>+ 28.0 + 14.0 | + 16.0 + 8.0               | +8.0  | 10.0                                     |
| 42   43   43   43   43   44   45   45   47   1   48   30  | +20.0   |   | - 30.0 + 36.0 -<br>- 18.0 + 26.0 - | 12.0 + 16.0                                    | +8.0 +14.0                | +16.0<br>+14.0 +12.0   |   | +12.0 +14.0 +18.0                               | +16.0 +8.0                 | +10.0   | 12.0                                     |
| 41.0   43.0   62   62   62   63   | +20.0   |   | - 16.0 + 16.0                      | + 16.0 + 10.0<br>+ 16.0                        | 4.0 +8.0                  | + 18.0 + 14.0<br>+ 20.0  |   | •   | +32.0 +22.0                | +6.0  | 10.0                                     |
| A.A   A   | + 14.0  |   | 16.0 +24.0 -<br>-20.0 +24.0        | - 20 . 0                                       | + 10.0 + 10.0 + 14.0      | . + 16.0   |   |   | -8.0                       | +8.0  | +10.0 +16.0                              |
|   | +6.0  |   | 28.0 +30.0                         |  |                           |  | · .   |   | + 16.0<br>+ 20.0           | +10.0<br>+6.0   | 10.0 +10.0                               |
| 90.1  | 0.0 E + 18.0  |   | +24.0                              |  |                           |  | •   | ······  | + 18.0<br>+ 58.0<br>+ 62.0 | +14.0<br>+8.0<br>+8.0   | +8.0<br>+12.0                            |
|   |   |   |                                    |  |                           |  | ٦   |   | + 18.0<br>+ 16.0<br>+ 12.0 | +8.0<br>+10.0<br>+8.0   | + 14.0 + 12.0<br>+ 10.0<br>+ 10.0 + 10.0 |
| Mathematical state   Image: state   |   |   |                                    |  |                           |  |   |   | - 40 . 0                   | + 10.0<br>+ 8.0   | +6.0<br>+12.0 +12.0<br>+12.0             |
|   |   |   |                                    |  |                           |  |   |   |                            |   | 8.0                                      |
|   |   |   |                                    |  |                           |  | <b>,</b> .  |   |                            |   |  |
|   |   |   |                                    |  | ,                         |  |   |   |                            |   |  |
| 1000    | -400.0 E  |   |                                    |  |                           |  |   |   |                            |   |  |
| MULE  |   |   |                                    |  | · ·                       |  |   |   |                            |   |  |
| -#0.1.5   |   |   |                                    |  |                           |  |   |   |                            |   |  |
| -800, 0 E   |   |   |                                    |  |                           |  |   |   |                            |   |  |
| -B00.0 E  |   |   |                                    |  |                           |  |   |   |                            |   |  |
|   |   |   |                                    |  |                           |  |   |   |                            |   |  |
|   | -800.0 E  |   |                                    |  |                           |  |   |   |                            |   |  |
| 0     | - 400.0<br>S  | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 |                                    |  |                           |  | S<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>5000<br>50 | 2400 0 S  | 5800 0 0 C                 | 0<br>c  | 32000 0<br>32000 0<br>32000 0            |
| QUICk-PLOT<br>GENCOM Services Inc. DATE = 26-05-92<br>Kamloops Office Teck Explorations Limited<br>MGM PROPERTY<br>SOIL SAMPLES Pb LEAD   HORIZONTAL SCALE = 1: 5000 VERTICAL SCALE = 1: 5000 FIGURE 200  | QUICK-PLOTDATE = 26-05-92Feck ExGENCOM Services Inc.TIME = 11:50:30KamloopHORIZONTAL SCALE =1:5000VERTICE | xplorations Limited TECK EXPLORATION   ps Office MGM PROPERTY   ICAL SCALE = 1: 5000        | LEAD<br>Soil Geochemis             | stry metres                                    | FIGURE 20                 |  |   |   |                            | 1<br>   |  |

| 1600.0 E   |   |
|--|---|
|  |   |
|  |   |
|  |   |
|  |   |
| 1200.0 E   |   |
|  |   |
|  |   |
|  |   |
| +663.0 +1349.0   |   |
| +352.0<br>+474.0 +246.0<br>+310.0 +310.0 +363.0<br>+148.0 +363.0   | ્રા   |
| + 419.0   + 267.0     + 419.0   + 267.0     + 437.0   + 363.0     + 51.0   + 431.0     + 686.0   + 462.0     + 436.0   + 365.0     + 185.0   + 336.0   | 802.0 + 323.0 + 1806.0 + 249.0  |
| +147.0 +147.0 +81.0 +224.0 +666.0 +185.0 +261.0 +99.0 +433.0 +89.0 +349.0 +210.0 +103.0 +271.0 +317.0 +108.   | 89.0 +469.0 +97.0 +924.0   158.0 +145.0 +787.0 +396.0   |
| +312.0   +213.0   +307.0   +213.0   +303.0   +63.0     +214.0   +110.0   +225.0   +242.0   +1126.0   +226.0   +277.0     400.0 E   +285.0   +212.0   +212.0   +212.0   +336.0   +447.0   +277.0  | 1116.0 +95.0 +712.0 +795.0   348.0 +120.0 +597.0 +76.0  |
| +236.0<br>+237.0 +202.0 +1335.0<br>+293.0 +202.0 +109.0<br>+200 +709.0 +129.0 +201.0 +109.0<br>+200 +709.0 +129.0 +129.0 +100 +100 +100 +879.0 +2045.0 +351.0 +792.0 +875.0 +875.0 +875.0 +875.0 +100 +100 +100 +100 +100 +100 +100 +1   | 495.0   +367.0   +268.0   +680.0     875.0   +249.0   +738.0   +1830.0  |
| +955.0<br>+532.0<br>+532.0<br>+180.0<br>+207.0<br>+207.0<br>+207.0<br>+10<br>+207.0<br>+10<br>+207.0<br>+10<br>+207.0<br>+10<br>+207.0<br>+10<br>+207.0<br>+10<br>+20<br>+20<br>+20<br>+20<br>+20<br>+20<br>+20<br>+20<br>+20<br>+2  | 1202.0 +720.0 +278.0 +887.0   565.0 +720.0 +268.0 +1121.0   |
| $\begin{array}{c} +339.0 \\ +401 \\ +484.0 \\ +829.0 \\ +829.0 \\ +552.0 \\ +477.0 \\ +477.0 \\ +477.0 \\ +477.0 \\ +442.0 \\ +440.0 \\ +400.0 $ | 401.0<br>+281.0 +589.0 +1195.0 +545.0<br>-391.0 +219.0 +601.0 +362.0  |
| + 153.0<br>+ 286.0 + 1551.0<br>+ 405.0 + 2140.0  | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  |
|  | +630.0   +173.0   +989.0     +1665.0   +441.0   +1324.0   +228.0     +3043.0   +232.0   +129.0     +1269.0   +547.0 |
|  | 1200.0 1342.0 12037.0 1347.0   687.0 +445.0 +2181.0   +352.0 +203.0 +564.0   +445.0 +45.0                           |
|  |   |
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|  |   |
|  |   |
|  |   |
| Note and the second   | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  |