#### ARIS SUMMARY SHEET

Off Confidential: 92.09.24 istrict Geologist, Smithers ASSESSMENT REPORT 22089 MINING DIVISION: Liard Iskut Joint Venture ROPERTY: LOCATION: LAT 56 42 00 LONG 131 05 00 09 6285718 372431 UTM 104B11E NTS Hemlo West 12-16, Aurum 3-4, Hemlo West 18, Ver 1, Isk 1 CLAIM(S): Prime Res. OPERATOR(S): UTHOR(S): Robertson, S. EPORT YEAR: 1992, 252 Pages COMMODITIES SEARCHED FOR: Gold, Silver, Copper, Lead, Zinc Triassic-Jurassic, Tuffs, Granodiorites, Diorites, Siltstones EYWORDS: Greywackes WORK Geological, Geochemical, Geophysical, Physical DONE: 1.6 km;VLF ,HLEM EMGR 4500.0 ha FOTO Map(s) - 1;  $Scale(s) - 1:10\ 000$ GEOL 4500.0 ha Map(s) - 2; Scale(s) - 1:10 000LINE 2.0 km 1.6 km MAGG 130 sample(s) ;ME ROCK Map(s) - 1;  $Scale(s) - 1:10\ 000$ 34 sample(s) ;MOSS;ME SILT SOIL 86 sample(s) ;ME RELATED **REPORTS:** 21041 104B 317,104B 356,104B 357 MINFILE:

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	ISKUT JOINT VENTURE PROP	ERTY

NTS 104B/11 Latitude 56°42'N Longitude 131°05'W Liard Mining Division

## for: THE ISKUT JOINT VENTURE

(Prime Resources Group Inc., American Ore Ltd., and Golden Band Resources Inc.)

Work performed by: **INTERNATIONAL CORONA CORPORATION** #1440 - 800 West Pender Street Vancouver, British Columbia V6C 2V6

GEOLOGICAL BRANCH

S. Robertson B.Sc. Geologist January 15, 1992

edited by: Don Lewis Exploration Manager

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## EXECUTIVE SUMMARY

The Iskut Joint Venture (IJV) property consists of ten contiguous mineral claims totalling 170 units (4250 hectares) centred on 56<sup>6</sup>42'N, 131<sup>6</sup>05'W (NTS 104B/11) approximately 100 kilometres north of Stewart in the Liard Mining Division. A two-claim internal block is held by Meridor Resources.

This report represents the summary of 1991 field and data compilation activities by International Corona Corporation, on behalf of Prime Resources and the Iskut Joint Venture, on the ISKUT property, situated immediately north of Cominco/Prime's Snip gold mine, along the Iskut River at the confluence with Bronson Creek. The intent of the 1991 program was to complete a comprehensive compilation of existing data, and to appraise the gold mineralization potential of the entire property.

Previous campaigns had concentrated primarily on delineating the limits of mineralization of the Hemlo West, Gregor, and Gorge/RPX showings on the West Grid. Between 1986 and 1990, exploration work included some 6019 soil samples, 204 stream silt sediment samples, 78 heavy mineral separates, over 1703 rock samples, and 3226 core samples selected from 6386 metres of diamond drilling in 42 DDH. A 325 line-kilometre airborne VLF-EM & Mag survey was flown in 1987 and an additional 12.5 line-kilometres of ground Mag, Max-Min and VLF-EM had been performed. Drill results include 3.96 g Au/t and 21.4 g Ag/t over 2 metres in DDH 87-05 (Hemlo West), and 14.6 g Au/t over 3.25 metres (RPX).

The regional geological setting is within the Stikine Terrane, on the western edge of the Intermontane tectonic belt, comprised of four tectonostratigraphic assemblages bounded by unconformities. The IJV property contains elements of three of these: the Palaeozoic Stikine assemblage comprised of thin-bedded metasediments with minor ash and crystal tuffs, Triassic-Jurassic volcanoplutonic arc complexes comprised of three kilometres of rapidly changing mixed volcanic and sedimentary rocks, basaltic to rhyodacitic volcanoclastic facies, comagmatic felsite stocks, and intrusive alkali feldspar syenite masses (such as the Bronson Stock), and the Coast granite-granodiorite batholith. Palaeozoic rocks exhibit the strongest deformation, while Mesozoic strata are generally sub-horizontal. High-angle faults are common and post-date flat faults. Some form well defined lineaments, traceable for kilometres on air photographs or satellite images.

Upper Triassic siltstone/wacke host the nearby Snip gold deposit's Twin Zone discordant shear-vein system which represents the primary exploration focus on the IJV property, which also, prior to 1991, was believed to have potential to host VMS polymetallic and alkaline porphyry style deposits.

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During 1991 Corona performed 80 man-days of field work, investigating 15 of 18 identified targets, primarily investigating the source of previously recognized gold +/- copper in soils anomalies on the Southwest and East Grids. 124 rock, 86 soil, 24 moss mat, 10 silt and 6 whole rock samples were collected. A 1.6 kilometre HLEM, VLF-EM, & Mag orientation survey was conducted over the Gregor showing.

Pre-1991 and 1991 exploration data was compiled in digital format and presented on TRIM-sourced base maps, utilizing orthophoto control. The geochemical database consists of 3156 soil, 2478 core, 1406 rock, 118 silt and 24 moss mat samples. Certain of the 1988 data could not be retrieved due to lost records.

The low-order, coincident gold-copper soil geochem anomalies on the **Southwest Grid** are explained by Bronson Stock-related quartz veins containing similar tenor mineralization (ie: 100-500 ppb Au, up to 1000 ppm Cu). The intrusive and invaded country rocks do not display the type or magnitude of alteration typical of alkaline porphyry systems.

The geophysical response over the **Gregor** area indicating discontinuous point source sulphidic mineralization is consistent with previous drilling results.

The structural-stratigraphic relations of the Hemlo West polymetallic mineralization were not sufficiently examined, and remain enigmatic. Future work would include detailed surface and trench mapping (plus trace and whole rock geochemistry), followed by additional trenching in advance of diamond drilling.

1991 follow-up of soil geochem anomalies on the East Grid isolated three areas warranting trenching, detailed sampling and geologic mapping:

- 1. At L 68-72E, BL 46N, follow-up of a Au-in-soil anomaly in the vicinity of the "Meridor Break" uncovered auriferous (up to 100 ppb) narrow semi-massive sulphide bands within volcanics.
- 2. Near L 81E, 42N six mossmat/silt samples returned anomalous gold values (ie: 67-553 ppb Au [Note: study indicates that mossmat sample values are generally comparable with silt sediment values]) in an area of subdued relief with no bedrock exposure.
- At L 70E, 40N selected quartz from sweats (generally 0.5 to 3 cm wide) from large angular talus blocks returned 769 ppb Au, 12.9 ppm Ag and 1.03% Cu; host rocks are barren of mineralization.

No other new gold-bearing mineral occurrences were discovered on the property during 1991, which completed the property-scale mineral potential assessment with the exceptions of the upper Verrett slopes and the lower slopes along the Iskut River.

The property remains prospective for Snip-style mesothermal vein gold mineralization, although traditional systematic geochemical and geophysical methodologies have been exhausted. The potential for Eskay-analog VMS deposits is considered low, due to the lack of widespread alteration and low magnitude trace element contents (particularly antimony and mercury). The IJV property is not prospective for alkaline or calc-alkalic porphyry deposits.

## 1.0 INTRODUCTION

Substantive field programs between 1987 and 1990, including some 6387 metres of diamond drilling, focused on three targets (Hemlo West, Gregor, Gorge/RPX zones) resulted in an imbalanced appraisal of the property's overall gold mineralization potential. The known showings did not display near-economic tenor, size and continuity and therefore do not warrant further investigation.

The Joint Venture's intent for 1991 was to achieve an overall mineral appraisal that would incorporate the following elements:

- 1. Preparation of an accurate topographic base map.
- 2. Compilation of all field data; preferably in digital format.
- 3. Follow-up on existing gold and/or copper in-soils geochemical anomalies, especially in the Southwest grid and west extension of the East grid areas.
- 4. Re-examine the polymetallic nature and controls in the Hemlo West area, particularly in light of the Eskay Creek deposit and Black Dog occurrence discoveries.
- 5. Prospect the balance of the property's stream drainages.

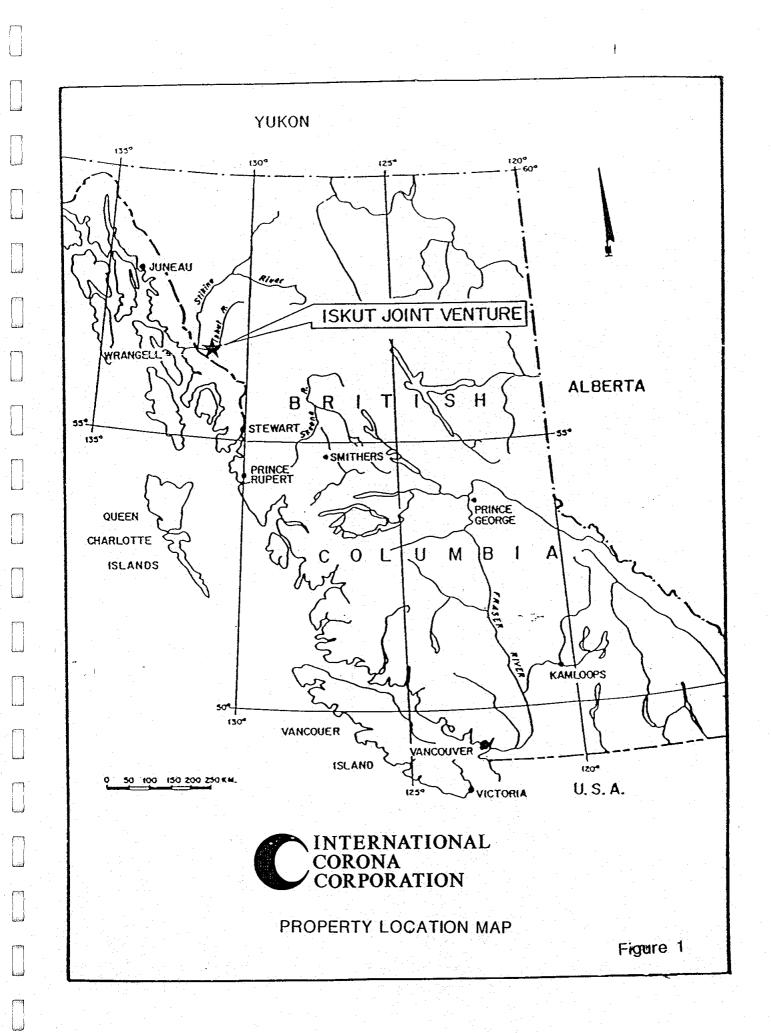
An original two-phased program with a budget of \$240,000 was proposed by Keewatin Engineering. International Corona Corporation, on behalf of Prime Resources (ie: the IJV operator), proposed an alternative \$120,000 program. The Joint Venture ultimately agreed to the Corona plan, which was subsequently modified to an approximate \$75,000 program, due to fiscal and merit considerations.

This report represents the summary of these activities.

#### 1.1 LOCATION AND ACCESS

The Iskut Joint Venture Property is centred on  $56^{\circ}42'$  north latitude and  $131^{\circ}05'$  west longitude on the 104B/11 NTS map sheet in northwestern BC (Figure #1).

Access is from Smithers (320 km southeast), Terrace (280 km southsoutheast) or Wrangell Alaska (80 km west) by fixed-wing to the Bronson Airstrip, situated on southeastern corner of the property. A proposed road link along the Iskut River with highway #37 was postponed indefinitely during 1991 following the decision by Cominco to not fund the Volcano Creek junction - Bronson strip portion. The Cominco/Prime Resources Snip gold mine and exploration properties in the area are supported from Bronson, which is 1600 metres long and can accommodate a Hercules aircraft.



Most of the IJV property requires helicopter shuttles from Bronson to a number of helicopter pads that have been built over the past five years.

#### **1.2 PROPERTY DESCRIPTION**

The Iskut Joint Venture property, located in the Liard mining division, is comprised of a contiguous claim block which completely surrounds a two mineral claim property owned by Meridor Resources (Figure #2). There are 10 located mineral claims totalling 170 units, covering approximately 4250 hectares. A complete list of the claims and their status is provided as Table 1.

The property is owned one third each by American Ore Ltd., Golden Band Resources Inc and Prime Resources Group Inc. Prime Resources is the operator, with International Corona Corporation performing the 1991 program on behalf of Prime.

### **1.3 PHYSIOGRAPHY AND CLIMATE**

Terrain in the area is rugged with steep slopes and deeply incised creeks. Maximum relief on the property is 1830 metres ranging from 70 metres elevation at the Bronson strip to 1900 metres on Mount Verrett. Vegetation consists of mixed conifers, slide alder, devil's club and a variety of undergrowth.

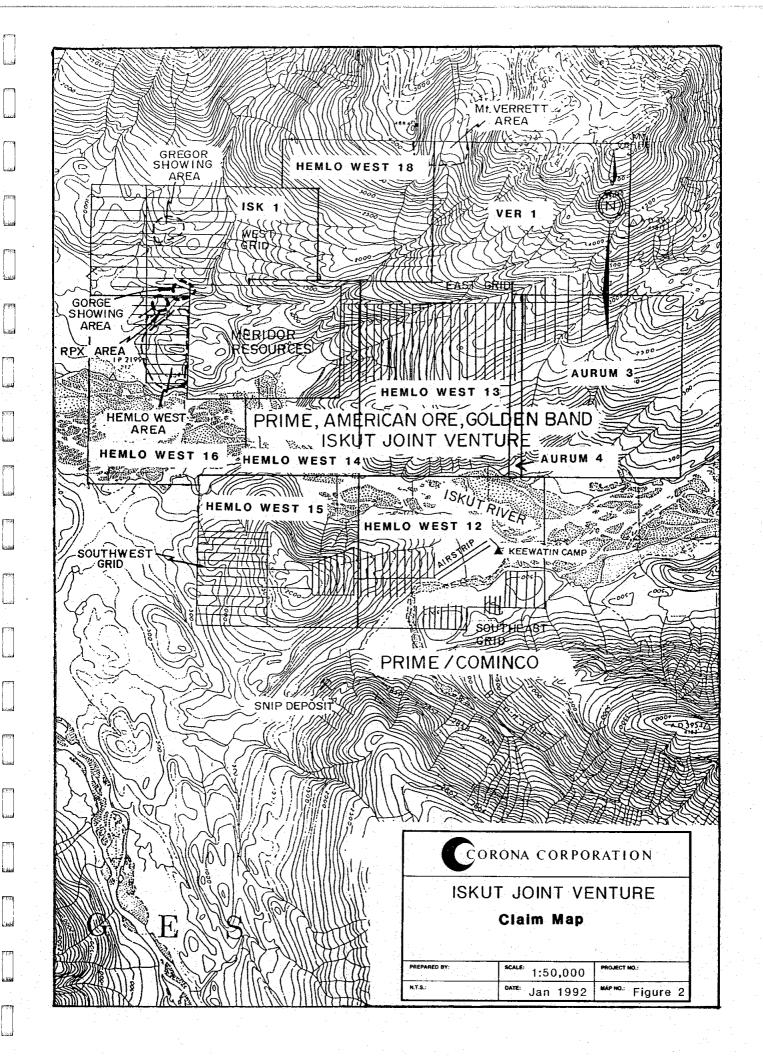
Annual precipitation is between 200 and 400 centimetres, and in the winters accumulations of snow are heavy, attaining a thickness of 3 metres at altitude. Temperatures are generally temperate. Prospecting can commence in May on southern slopes and little work can be done after the middle of October without considerable effort and expense.

#### **1.4 PROPERTY HISTORY**

The claims area now known as the Iskut Joint Venture (IJV) property (Figure #2) received minimal exploration activity prior to the mid 1980's. Since then, the discovery and development of several mineral deposits in the "Iskut Gold Camp", especially the adjoining Snip deposit, initiated considerable exploration activity on the property and in the district.

Following is the work history of the IJV property as described by Kerr (1948) and Pegg (1991):

The earliest claims "werestaked by the Iskut Mining Company in 1906, and some work was done on them almost every year until 1930. During 1929



## TABLE 1

## LIST OF CLAIMS

Province : B.C Mining Division: LIARD Land District : Lat./Long. : NTS : 1048/11 Location: BRONSON CREEK, BC Royalty i) . ii) iii)

	Operator : INTERNATIONAL CORONA CORP
	Owners 1) PRIME RESOURCES GROUP INC
	2) AMERICAN ORE LTD.
	3) GOLDEN BAND RESOURCES INC
.	J.V. Part. (%): PRIME RES 33.3%
	: AMER.ORE - 33.3%
<u> </u>	: GOLDEN BAND - 33.3%
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LOCATED MINERAL CLAIMS

CLAIN	UNITS	AREA (ha)	RECORD NO.	RECORD DATE	EXPIRY DATE	WORK REQUIRED
HENLO WEST 12	20	500.0	2518	1982.09.29	2000.09.29	4,000.00
HENLO WEST 13	20	500.0	2519	1982.09.29	2000.09.29	4,000.00
HENLO WEST 14	15	375.0	2520	1982.09.29	2000.09.29	3,000.00
HENLO WEST 15	16	400.0	2521	1982.09.29	2000.09.29	3,200.00
HEMLO WEST 16	20	500.0	2522	1982.09.29	2000.09.29	4,000.00
AURUM 3 #	20	500.0	2624	1982.11.24	1998.11.24	4,000.00
AURUM 4 #	5	125.0	2625	1982.11.24	1998.11.24	1,000.00
HEMLO WEST 18	16	400.0	2632	1982.12.16	2000.12.16	3,200.00
VER 1	20	500.0	3714	1986.12.04	2000.12.04	4,000.00
ISK 1	18	450.0	3715	1986.12.04	2000.12.04	3,600.00
Total: 10 Claims	170	4250.0			\$	34000.00

ISKUT JOINT VENTURE



# Note: Expiry Dates for Aurum 3 and Aurum 4 reflect work filed after 1991 field program.

claims were staked by the Consolidated Mining and Smelting Company in a belt practically surrounding those of the Iskut Mining Company. The property of the Iskut Mining Company has been mentioned in various reports of the Minister of Mines for British Columbia from 1911 to 1933." (Kerr)

In 1964, the project area was staked by Iskut Silver Mining Ltd during their search for porphyry copper deposits. This company undertook prospecting, trenching, geochemical and geophysical surveys and drilling (4 holes, 69 m) during 1965 and 1966. In 1970, the property was optioned to the Cerro Mining Company Ltd. who did prospecting, geological mapping and geochemical sampling. The option was then dropped and picked up by Amax Potash Limited the following year. Work included soil, silt and water sampling as well as geological mapping. These claims were eventually dropped.

In 1982, the present Iskut Joint Venture property was staked by the Alpha Syndicate. The Syndicate optioned the property to the Apex Energy Corp. who did 21.2km of line-cutting,geologicalmapping (1:10,000)and collected 475 soil, 36 rock and 44 silt samples for multi-element analysis. The option was subsequently dropped. In 1986 the property was acquired by Delaware Resources Corp who did geologicalmapping and collected 287 soil, 51 silt and 12 rock samples for gold and silver analysis. The following year, Prime Resources Corporation (nee Delaware Resources Corp) optioned the property to American Ore Ltd and Golden Band Resources Inc.

During 1987, Taiga Consultants Ltd performed geochemical surveys on four grids and reconnaissance-style contour soil sampling in selected areas of the property. Geological mapping and prospecting was carried out in conjunction with these surveys. A total of 3250 soils, 153 silts and 804 rock samples were collected and analyzed for gold and silver. In addition, 78 heavy mineral samples were collected and analyzed for gold, silver, copper, lead and zinc. The soil survey outlined a number of areas which were anomalous in gold and silver, especially on the Southwest Grid, the West grid and north of the East grid. Five trenches and eight drill holes (956 metres of BQ core) tested the gold-in-soil anomalies on the southern part of the West ("Hemlo West") grid, A total of 945 core samples were collected and analyzed for gold, silver, copper, lead and zinc. All of the drill holes reported elevated gold values with the best intercept being 3960 ppb Au and 21.40 ppm Ag over a 2.0m core length in DDH JV87-05.

During 1988, Prime engaged Keewatin Engineering Inc to perform geological, geochemical and geophysical surveys, concentrating on the Gorge and Gregor areas. A 325 line-km airborne Aerodat VLF-EM and Mag survey was flown over the property during the spring. A total of 1809 soil samples and 490 rock samples were collected and analyzed for gold, silver and copper. Geological mapping and prospecting were carried out during the coarse of the geochemical survey. The discovery of the auriferous Gorge and Gregor showings led to more detailed geochemical sampling and mapping. An eight line-km VLF-EM and MAG survey was completed over an east-west grid in the Gregor area and a trench was excavated on the

Gregor showing. Hydraulic sluicing was performed at the Gorge showing. Drilling, totalling 1759.5 metres in ten holes, was done in both showings' areas. 945 core samples were split and analyzed for gold and silver ( $\pm$ copper). During the fall of 1988 a legal survey of Meridor Resources' west boundary was completed and the common legal corner post of their Iskut 1 and 2 claims was located with respect to various bench marks on the Snip property.

Meridor has, apparently, completed 17.925 of line-cutting, 33 hand trenches, 14 blasted trenches and 97 drill holes (9565 m) in 1987 and 1988. This property has been inactive since January of 1989.

During 1989, Keewatin conducted geological and geochemical surveys on the western side of the property. The Gorge and Gregor showings' area was designated as the focus of the two phase program. Grid establishment, "infill" soil sampling, surveying, prospecting and geological mapping were completed in the targetarea. Previously obtained gold-in-soil anomalies and mineral occurrences were also investigated. Re-interpretations of the known showings led to further sampling, prospecting, geophysical surveys and trenching. Preliminary, follow-up prospecting and geological surveys were carried out in the "Hemlo West" and "Mount Verrett" areas during the latter part of the first phase of exploration. The 1989 work included 2.088 km of Max-Min and MAG, 2.423km of VLF-EM and MAG, 6.27km line cutting. 13.53 km grid establishment, 2.06 km of surveying and the investigation of more than 53 gold-in-soil anomalies. A total of 673 soil, 397 chip/grab and 1336 core samples were collected. Field personnel also blasted, mapped and sampled a trench in order to test a re-interpretation of the Gregor area mineralization. The trench excavated across the 480x 10 to 90 m wide, westsouthwest trending gold-in-soil anomaly in the Gregor area revealed an erraticallygold-bearing and esitic tuff breccia unit. Chip sample results from this unit averaged 0.133 oz/t gold over 7.0 metres, which included 0.376 oz/t gold across 1.0 metre.

During October and November, drilling of the Gorge/Gorge South area was completed. This program consisted of ten drill holes (1704.7 m) which tested several targets including geophysical and geochemical gold anomalies and possible on strike/down dip extensions of the Gorge mineralization. The drilling led to the discovery of gold mineralization, some 300 m westsouthwest of the Gorge showing, which was named the RPX zone. Drilling of the RPX zone indicated that the intercepts of up to 0.427oz/t gold over a core length of 3.25 metres are hosted by apparent east-west trending shear structures in altered metasediments.

The 1990 field program consisted of two phases of exploration and prior to the field work, a re-interpretation of the 1988 airborne VLF-EM and MAG surveys. During June and early July, Keewatin carried out drilling in the Gorge, RPX and Gregor areas, which consisted of ten diamond drill holes (1676.1 m). One of the holes attempted to test, at depth, drill hole 189-1's auriferous intercepts from the Gorge Showing area. Results confirmed the inconsistency of extent and grade of mineralization related to the Gorge showing. Four holes were drilled to test possible along strike/down dip

extensions of the RPX mineralization with similar results. Another two holes were drilled between the Gorge and RPX areas in order to probe for possible blind mineralization related to the Gorge Creek structure. The remaining three holes were drilled in the Gregor area to test the gold-bearing tuff encountered in the 1989 trench. Results indicate a thinning of the host tuff horizon to the west of hole 190-10. In October, Keewatin field personnel carried out geochemical, geological and prospecting surveys on the western portion of the southwest grid. A new baseline was cut and seven cross-lines and a tie-line were established for control as most of the previously established grids were found to be inaccurate. The crews also attempted to complete follow-up work on previously obtained gold/copper-in-soil anomalies, chasing alkaline porphyrycopper-goldmineralization. During late October and early November, a second phase of diamond drilling was carried out in the Gregor area consisting of four holes (289.25m) testing the gold-bearingtuff breccia encountered in hole 190-10, both along strike and down dip. All of the drill core was split/cut and sent for analysis. The remaining core has been stacked or stored in core racks at Keewatins' Bronson Creek camp site."

## 1.5 GEOLOGY

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#### **1.5.1 District & Local Geology**

[Adapted from Britton, Fletcher and Alldrick, 1990, (see Figures #3 & #4)]

The regional geological setting is within the Stikine Terrane, on the western edge of the Intermontane tectonic belt. Four tectonostratigraphic assemblages, bounded by unconformities are found in the 104B map area:

Tertiary Coast plutonic complex,

- Middle and Upper Jurassic Bowser overlap assemblage,
- Triassic-Jurassic volcanic-plutonic arc complexes, and
- O Palaeozoic Stikine assemblage.

Three of the assemblages (excluding Bowser sediments) are represented in the area shown in Figure #4. Most strata are Upper Triassic to Lower Jurassic volcanosedimentary arc-complex lithologies characterized by rapid facies changes. Strata have been cut by a variety of plutons representing at least four intrusive episodes spanning Late Triassic to Quaternary time. These included synvolcanic plugs, sills and stocks, minor dyke swarms, isolated dykes and sills, as well as the batholithic Coast plutonic complex. The stratigraphic sequence has been folded, faulted and metamorphosed mainly during Cretaceous time, but some Palaeozoic strata are polydeformed and probably record an earlier deformational event. Contacts between lithostratigraphic sequences within the area are not well exposed: commonly they are covered with moraine, disrupted by faults, or invaded by large intrusions such as the Lehto batholith and the Coast plutonic complex.

<u>Palaeozoic</u>: The Palaeozoic Stikine assemblage is observed in outcrop west of the Craig River and northeast of Mount Verrett. Rocks tentatively assigned include abundant fine-grained, thinly layered, biotite-rich quartzofeldspathic gneiss, phyllite,

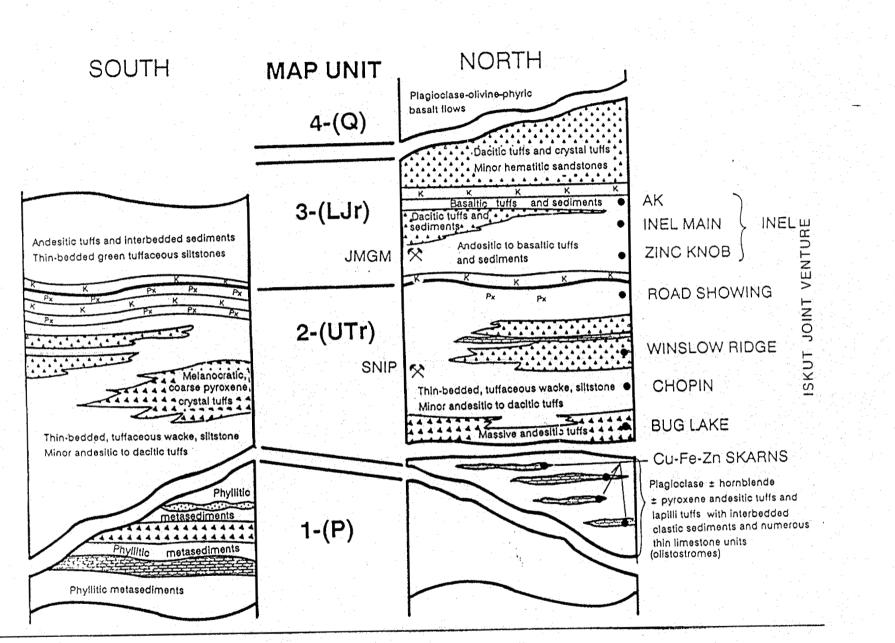
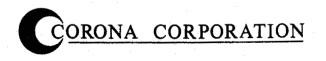
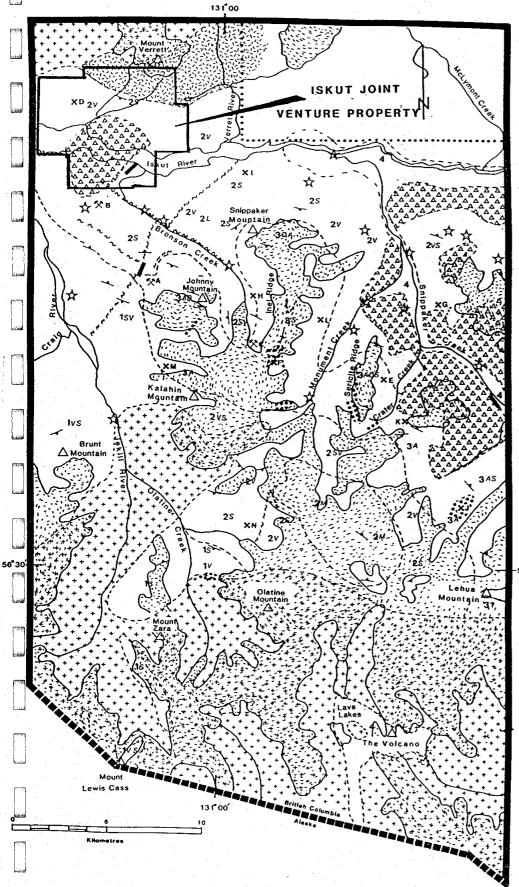


Figure 3

STRATIGRAPHIC COLUMN FOR THE SNIPPAKER MAP SHEET. Britton et al (1990).



## Figure 4



Geology of the Snippaker Map Sheet. Britton et al, 1990

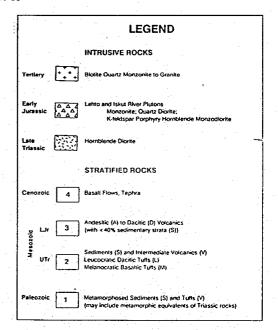
### SYMBOLS

Contact
Compositional layering (bedding, foliation) 🧡
Airstrip · · · · · · · · · · · · · · · · · · ·
RGS gold values > 90th percentile $\star$
Limit of mapping
Mine, developed prospect
Prospect
Gossan

#### PROSPECTS

NAME	COMMODITY
A Johnny Mountain	
в Snip	Au,Cu,Ag,Pb,Zn
c INEL	Au,Ag,Cu,Zn,Pb
D Gorge/Gregor	Au,Ag
E Sericite Ridge	
F Khyber Pass / Pyramid	Hill Au,Cu,Zn
G Josh	
H Cathedral Gold	Au
I Bug Lake	Au,Pb,Cu,Zn
J Pins	Au,Ag,Cu,Zn,Pb
ĸ Lake Area	Au
L Wolverine	Au,Cu,Pb,Zn
M Pez-Dan	Au,Ag,Cu,Pb,Zn
N Still	
o Mount Verrett · · ·	Au

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metawacke, metatuff and thin recrystallized limestone (marble). The gneisses were probably derived from tuffaceous siltstones and sandstones, with minor ash and crystal tuffs, and are the most structurally complex in the area: two phases of penetrative deformation have been observed. The contact between Palaeozoic rocks and overlying Mesozoic strata is probably an unconformity, based on relative states of deformation.

<u>Mesozoic</u>: Most of the stratified rocks in the area are Mesozoic. Strata form a thick (3 kilometres) sequence of mixed volcanic and sedimentary rocks. Facies changes, minor unconformities and the paucity of distinctive marker horizons make stratigraphiccorrelation difficult. Extrusive rocks are mostly volcaniclastic: pyroclastic units with derived epiclastic facies. Plagioclase, pyroxene and hornblende are common phenocrysts; distinctive coarse potassium feldspar is minor but important. Compositions range from basalt to rhyodacite, but most are andesite to dacite. Sedimentary rocks are volcanic-derived siltstone, wacke and conglomerate with minor amounts of limestone, either as relatively pure lenses or as calcareous mudstones. Limestone decreases upwards in the section and is rare in Hazelton strata.

<u>Upper Triassic</u>: Most of the volcanic rock in the Triassic succession is basaltic to andesitic with plagioclase and pyroxene as the principal phenocrysts, characteristic of the Stuhini Group. Pyroclastic units are more common than flows, but many outcrops are massive and difficult to classify. For example, a thick, monotonous sequence of fine-grained, medium to dark green, feldspar porphyry andesite <u>underlies the lower slopes of Mount</u> <u>Verrett</u> (ie: on the IJV property) and extends across the Iskut River to Bug Lake. These rocks are moderately to completely recrystallized north of the Iskut and could be either massive crystal tuffs or flows. There area some lapilli tuffs and tuff breccias around Bug Lake, but fragmental textures are generally absent.

Triassic sedimentary rocks are mostly siltstone with minor fine-grained wacke. Thin rhythmic bedding is common. In the north they are interbedded mudstone, lithic wacke, feldspathic wacke, minor conglomerate and limestone lenses, with locally abundant fine-grained volcaniclastic material-ash tuff or volcanic sandstone. <u>These rocks host the Snip deposit</u> and other prospects uphill from Bug Lake and on lower Bronson Creek. A sequence of light grey-green,waxy, dacitic pyroxene-plagioclase crystal and lapilli tuffs has been identified only on Winslow Ridge and appears to be conformable within the thick sedimentary sequence.

<u>Lower Jurassic</u>: Jurassic strata are mainly andesitic to dacitic fragmental volcanics with minor basaltic tuffs and lesser amounts of siltstone, wacke and conglomerate. Marked lateral facies changes, lithologic heterogeneity and variable rock colours (grey, green, maroon, and mottled combinations of these) are common.

On Johnny Mountain, the Jurassic strata consists of three main units. The lower unit is a plagioclase-phyric and esitic to dacitic crystal and ash tuff, lapilli tuff and agglomerate. In some of these rocks, the plagioclase phenocrysts are rounded, suggesting they have been reworked. The middle unit conformably overlies the lower unit and consists of grey and tan dacitic volcanic rocks. They include flow-banded and welded ash tuffs as well as well-bedded ash and lapilli tuffs with rhyodacite clasts. The upper unit comprises dark grey-green, flaggy, well-foliated basaltic andesite ash tuffs with minor siltstone and wacke interbeds.

On Snippaker Mountain and extending southward, the Jurassic sequence includes at least 300 metres of matrix supported, polymictic pebble to cobble conglomerate with minor siltstone and wacke interbeds. The unit grades laterallyand upwards into green volcanic conglomerate and lithic lapilli tuff. These conglomerates are locally overlain by thin-bedded, salt-and-pepper lithic arenite and siltstone with carbonized plant remains.

<u>Quaternary</u>: Pleistocene and Recent basaltic lava flows, cones and tephra occupy the valleys of the Iskut River, Snippaker Creek and Lava Lakes. These olivine and plagioclase phyric, often strongly vesicular flows are part of the north-trending Stikine volcanic belt of Miocene to Quaternary eruptive centres.

<u>INTRUSIVE ROCKS</u>: The oldest intrusives in the area are sills, dykes and plugs of hornblende diorite that are contemporaneous with Triassic host rock volcanics. <u>They</u> <u>are especially common in andesites located north of the Iskut River</u>. There is a large hornblende diorite stock of this type on the south slope of Mount Verrett (ie: on the UV property). The rock is texturally similar to the andesites it intrudes and consists of mesocratic medium to dark grey, fine-grained, anhedral granulardiorite with fine plagioclase phenocrysts. The diorite is largely recrystallized and pervasively propyliticallyaltered. Near its contact with the Coast batholith it has pegmatitic zones up to 50 centimetres wide by 6 metres long consisting of coarse bladed intergrowths of hornblende and plagioclase with minor biotite. Against the batholith it is migmatitic with a swirled foliated fabric in the diorite that is cut by leucogranite dykes. Contacts with andesite are indistinct and may be in part gradational.

Jurassic intrusions include synvolcanic hypabbysal stocks as well as phaneritic plutons of considerable size. Synvolcanic intrusions are thought to be comagmatic and coeval with extrusive rocks. Examples include felsite stocks on Johnny Flats and the Inel property. These are leucocratic to holofelsic, cream to tan, porphyritic rocks with fine feldspar and quartz phenocrysts set in an aphanitic groundmass. Contacts are altered and sheared but the stocks appear to form sheet-like bodies that are crudely conformable with enclosing strata.

Phaneritic intrusions of probable early Jurassic age include the Lehto batholith, the Iskut River stock (ie: <u>Bronson stock</u> on the IJV property) and smaller plugs and dykes such as the Red Bluff porphyry. A common feature of these intrusions is the presence of coarse (up to 5 centimetres) potassium feldspar phenocrysts. The Iskut River stock consists mainly of the coarse potassium feldspar phenocrysts set in a fine to medium-grained groundmass. [Kerr, 1948, noted that "sediments in contact with the porphyry are impregnated with much pyrite, but otherwise are not greatly altered, and contacts with the intrusion are generally sharp. The volcanic rocks northwest of the mass are rather completely metamorphosed, so much that at many contacts the country rock has been converted into material much like the intrusive rock, thus making it appear as if the two were gradational. The intrusion contains angular and rounded inclusions that resemble altered volcanic rocks, and many of them, at their edges, show evidences of assimilation."] The largest intrusive mass in the map area is the Coast Mountains batholith which occupies the southern quarter and northwestern corner of the map area consisting of medium-grained biotite and biotite = hornblende granite granodioriteand rarelyquartz diorite. Very little of it has been mapped. It is distinguished from Jurassic plutons by its fresh appearance, lack of foliation and shearing, minimal saussuritization and abundance of quartz. Biotite is either the sole mafic mineral or else is much more common than hornblende. There is little or no hydrothermal alteration of skarn developed along the intrusive contacts despite the presence of limestone units in the Palaeozoic country rocks. The age of these rocks is probably middle Eocene based on potassium-argon dating near Stewart.

Isolated dykes and minor dyke swarms occur locally in the area. In addition to local feeder dykes associated with the overlying volcanics, widespread biotite and hornblende lamprophyre dykes cut all other rock types including the Coast Mountains batholith [Note: The Twin zone is bisected and diluted by such a dyke]. They are typically isolated and narrow (up to 2 metres wide). The age of these dykes is probably Oligocene.

<u>STRUCTURE</u>: Palaeozoic rocks exhibit the strongest deformation. Folds rangefrom crenulations through upright chevrons to recumbent isoclines with fold amplitudes of 100 metres. The largestfolds plunge gently east-northeast. Crenulations and contorted open folds are also developed adjacent to faults in fine-grained sediments and tuffs of any age. These structures die out within a few metres of the fault zone.

At a regionalscale the Mesozoic lithostratigraphicsequences form flat-lyingpackages, but Triassic and Jurassic strata show mesoscopic folds. Some of these are primarily depositional features such as convolute layering in welded tuffs, flow banding and soft-sediment slumps.

Many rocks, but especially fine-grained sediments, mafic tuffs and limestones, show intense foliation, boudinage and transposition of primary layering. Rock composition, especially mica content, largely determines the amount of foliation developed.

There is a widespread sub-horizontal cleavage in most Triassic and some Jurassic rocks. Locally this is expressed in sub-horizontal faults between blocks of differing competence. An example of this is the contact between Jurassic volcaniclastic and Triassic sediments on Johnny Mountain. The underlying siltstone exhibits folding, shearing and recrystallization that decreases in intensity away from the fault. Overlying dacitic volcaniclastic rocks which act as a competent unit also show increased strain near the fault but deformation is much weaker, amounting to minor shearing and recrystallization.

High-angle faults are common in the area and appear to postdate flat faults. Some form well-defined lineaments, traceable for kilometres and visible in radar images and air photographs. Most have small displacements on mappable faults like those seen on Johnny and Snippaker Mountains is in the order of a few hundred metres. Most faults strike northeasterly or northwesterly.

<u>METAMORPHISM</u>: Rank is generally low (ie: lower greenschist), although recrystallizationis complete. Contact metamorphism occurs within 1 to 2 kilometres of the Coast Mountains batholith. The main effects are recrystallization with coarsening of grain size and replacement of mafic minerals by metamorphic biotite.

#### **1.5.2 Mineral Occurrences**

1.

Potentially economic gold +/- silver, copper, zinc, and lead mineralization in the Iskut region is genetically classified as:

1. Mesothermal/transitional quartz-sulphide veins (ex: Snip Twin zone, Johnny Mountain, Sulphurets West zone, Silbak-Premier),

2. Stratabound/form VMS (ex: Eskay 21B, Granduc, Big Missouri, Black Dog, SMC zones) [?],

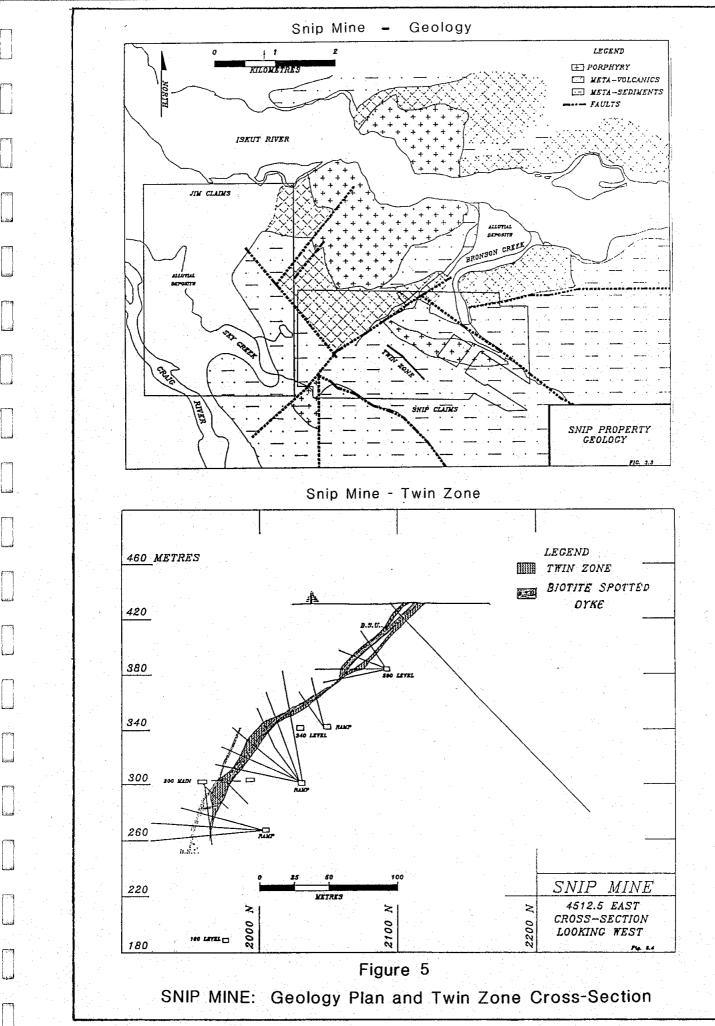
3. Alkaline Porphyry systems (ex: Galore Creek, Copper Canyon, Kerr, Sulphurets).

There is evidence that the IJV property is prospective for all three styles of gold mineralization, however the highest probability of success remains the Snip vein style, which has dominated exploration methodology since the realization of Snip's merits in 1986.

Mineral occurrences in the immediate vicinity of the Iskut Joint Venture property are:

The Snip Twin zone gold deposit: lies adjacent to the southern boundary of the Iskut JV property (see Figure #5). It is a one to ten metre thick (average 4.2 metres) discordant shear-vein system which cuts through a massively bedded feldspathic greywacke-siltstone sequence. The hosting grey to buff brown clastic sediments are regionally by extensive, pervasive, secondary altered biotite development and characterized by wide spread development of centimetre scale thick tension and gash veining filled with calcite-quartz-chlorite. These carbonate dominated unmineralized veins occur throughout the explored area of the Snip property extending several hundred metres into both the hanging wall and footwall of the Twin zone. The Twin zone strikes 120° and has dips ranging from 30° and 70° to the southwest. It has been traced by drilling over a strike length of 1000 metres and a vertical range from the 150 metre to 650 metre elevations. The undiluted ore reserves totalled 860,000 tons grading 1.05 oz Au/ton in 1989 (Snip personnel, 1990).

Gold mineralization occurs in centimetre to metre scale alternating bands of: massive streaky calcite, heavily disseminated to massive pyrite, crackled quartz, biotite-



annite, pyritic to non-pyritic fault gouge. Bands of sphalerite with locally massive arsenopyrite and minor disseminated chalcopyrite and galena also occur in the zone. Thicker sections (3 metres) show repetitive banding of all types. Twin zone contacts are sharp and well defined, with gold values in the immediate FW and HW generally less than 1 g Au/t.

[Important Note: Assuming minimal offset, the strike extension of the zone trends onto the IJV property, but no such extension has been identified to date.]

Johnny Mountain lies approximately 4 kilometres southeast of the Snip Mine and is also a mesothermal quartz-sulphide vein system. The several narrow northwest dipping (65<sup>°</sup>) quartz/sulphide veins are apparently associated with orthoclase porphyry dyke-metasediments contacts. Vein continuity is very poor, with numerous offsets caused by post-mineral SE-striking near vertical faults, as well as by gently rolling sub-horizontal faults. Mineable reserves totalled about 172,500 tons grading 0.6 oz Au/ton.

The <u>Black Dog</u> massive sulphide prospect, located on the Rock and Roll property, located 7 km west of the IJV property, is reported to be a stratigraphically controlled, disseminated to well laminated, semi-massive to massive sulphide horizon hosted within a sequence of volcanic and sedimentary rocks. The Black Dog Horizon has a thickness of approximately 25 metres, within which numerous semimassive to massive lenses occur over widths of up to 10 metres. The mineralization strikes northwest-southeast, dipping 20°-30° to the southwest and has been drill tested over a strike length of 250 metres. Preliminary geological resources are 640,000 tons grading 0.072 oz/ton AU, 9.8 oz/ton Ag, 0.79% Pb, 3.08% Zn and 0.64% Cu (Prime Explorations, Vancouver Stockwatch, Sept 30 1991).

#### **1.5.3 Property Geology** (see Map #2)

2.

3.

As indicated in the District Geology discussion, the property is essentially underlain by gently folded, flatly to moderately dipping, undifferentiated Upper Triassic/Lower Jurassic porphyritic andesitic tuffs and flows, and volcanically derived sediments that have been intruded by the Upper Triassic Verrett diorite stock, the

Lower Jurassic Iskut/Bronson alkali feldspar syenite mass, and the Eocene Coast plutonic complex. Numerous steep faults transect the property, as evident on Landsat images and airphotos. Overburden varies from a thin layer of developed soil to greater than five metres of glacial diamicton and glacial-fluvial sediments. Continuous exposure of bedrock is limited to areas above tree-line and in incised valleys.

Volcanics are dominated by flows with tuffaceous horizons throughout. The tuffs can vary from crystal tuff, containing 2 - 3 mm feldspar crystal, to polymictic lapilli tuffs which contain 5mm pyroxene phenocrysts. North of the Iskut the volcanics are moderately to completely recrystallized, blurring primary depositional and contact relations.

Sediments are dominantly siltstones and greywackes occurring as both thin lenses within thick volcanic units and as thick extensive packages of either well bedded or massive sediments. These rocks are regionally metamorphosed to greenschist facies. The northwest and western sections of the property are dominated by the later with occasional volcanic horizons [ie: Kerr inferred that these were Palaeozoic sediments, in ambiguous contact with Triassic volcanics to the east].

The main intrusive body, the Bronson Stock, is located south and north of the Iskut River and is covered to the south by the Southwest Grid (Figure #2, Map #1). It has been dated by Pb isotope means at  $205 \pm 4$  Ma (Macdonald et al, 1991). Smaller orthoclase porphyry intrusives with textural and chemical characteristics very similar to the Bronson Stock are found between the Gregor and Gorge areas (ie: the Gregor Stock) and in the northeast corner of the Meridor property. The northern boundary of the property crosses onto the southern edge of a large Tertiary diorite pluton, related to the Coast Plutonic Complex. The intrusive has caused some localized skarning in adjacent host rocks but the intrusive itself is generally unaltered. Lamprophyre dykes are found throughout the property in various orientations and sizes but are generally less than a few metres thick and cross-cut all other stratigraphy.

The property is transected by several prominent east-west lineaments and by fewer northeast-southwest features as plotted on Maps #1 & #2. The most prominent lineament is an east-west break extending from beyond the eastern property boundary, westward across the north end of the Meridor property, and disappears below the deep fluvial sediments in the Iskut River valley. The "Aurum" MinFile occurrence (#249: 0.2 oz Au/ton in a quartz vein) is associated.

The entire package has been regionally metamorphosed to lower greenschist facies. More intense alteration is found locally, associated with faults and intrusive contacts.

### 2.0 **1991 WORK DONE**

Pre-1991 work was compiled as presented in Map #1. 18 follow-up targets were identified.

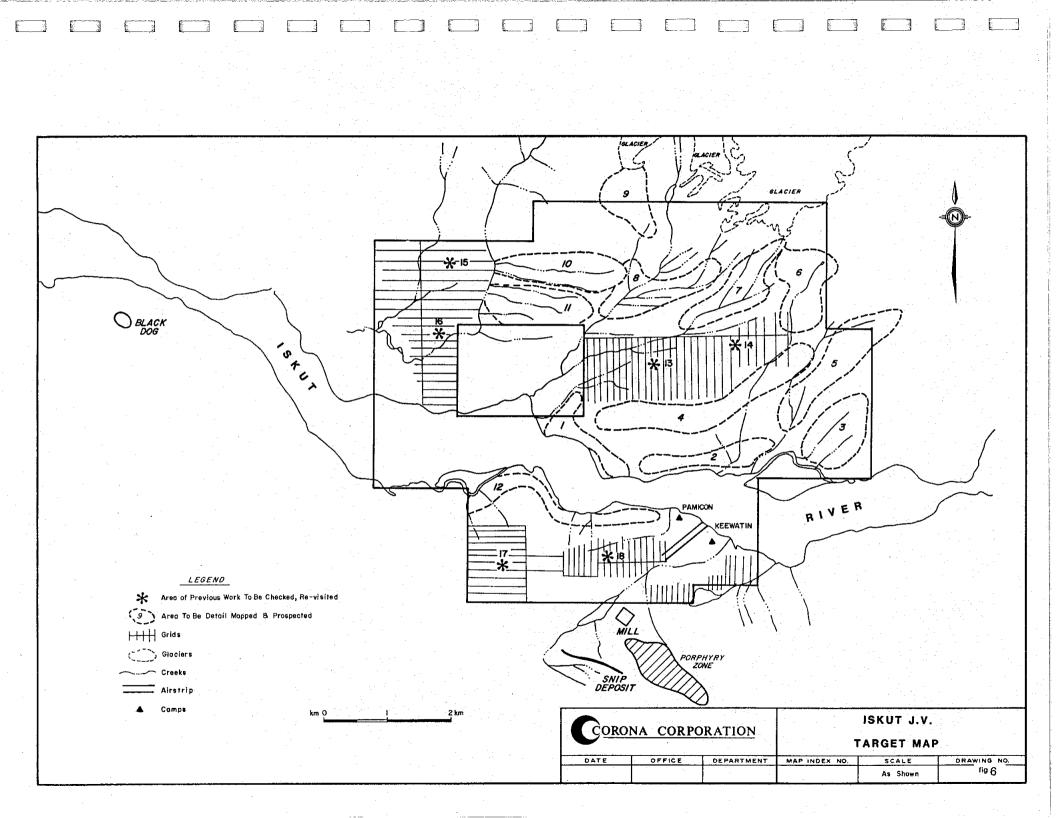
Corona's crew mobilized into Bronson on June 13 for 20 days. 15 of 18 target areas (Figure #6) were examined, and 124 rock, 86 soil, 24 moss mat, 10 silt, and 6 whole rock samples were collected. Four surviving targets were recommended for further examination on August 29. The Joint Venture elected to defer this and all other field activities pending the conclusion of the property data compilation, synthesis, and analysis.

An Orthophoto base map (Map #4) was created by combining airphotos flown by Cominco in July of 1982 and TRIM data, purchased from the government. [Note: The TRIM data for the area provides accurate topographic detail and includes various planimetric features so it can be used in isolation as a base map.]

Detailed follow-up soil sampling was done in the areas of geochemical anomalies from previous programs on the east grid, which could not be immediately explained by first pass inspection. A small slope corrected addition to the east grid (five lines, 200 to 250 metres long each) was installed, using hip chain and compass and soil sampled at 25 metre intervals (See Map #3).

The rock, soil, moss mat and silt samples were sent to Bondar-Clegg in North Vancouver for 29 element ICP analysis plus gold by Fire Assay AA. Complete assay certificates are provided as Appendix A. Rock descriptions are provided as Appendix B.

Geochemical results from rock, drill core, moss mat, silt and soil samples taken during the 1986 - 1991 field programs, were compiled into digital data files. The information was partitioned on the basis of sample type. Some of the 1988 data could not be retrieved from the lab due to Keewatin's loss of records containing the assay lab file numbers. Only rock



and drill core data from 1988 were manually transcribed from the 1988 property report. The resultant data is comprised of 3156 soil, 2478 drill core, 1406 rock, 118 silt and 24 moss mat samples [Note: certain elements and element groups were not consistently analyzed for].

Univariate and bivariate statistical calculations were completed. The results are provided as Appendices D & E.

## **3.0 1991 FIELD RESULTS**

#### **3.1 SOUTHWEST GRID**

The Southwest Grid covers a significant portion of the early Jurassic Bronson Stock and its western contact with Triassic volcanic and sedimentary rocks. 1987 soil geochem resulted in 7 Au-in-soil, 23 Au-insoil (unknown copper), 7 Au & Cu-in-soil, 14 Cu-in-soil, 4 Au-in-silt (unknown copper), and 1 Au & Cu in silt anomalies (Carter, 1991). Discrete gold values range up to 560 ppb, but are generally less than 100 ppb, and display poor lateral continuity. Copper values range up to 1000 ppm, and are not clearly correlated with gold content.

The discrete Au-in-soil geochemical anomalies within the grid are situated near discontinuous, contact related quartz veins with anomalous and comparable, but inconsistent gold values. The veins have not been properly trenched to fully expose their ultimate size potential, which is not considered to be extensive. As indicated by Kerr (1948) and 1991 Corona work, the intrusive appears fresh and does not exhibit the alteration assemblage characteristic of a mineralized porphyry system.

### **3.2 WEST GRID - GREGOR AREA**

Four 400 metre-long slope corrected lines were installed using a compass and tight chain, oriented at 155° and centred on the Gregor showing and DDH 90-10. A VLF-EM survey was completed to determine whether or not the mineralized tuff would generate a traceable response, and indicate down dip or along strike extent. Ground magnetics readings were also collected, but unfortunately the data was lost during retrieval due to equipment malfunction.

The geophysical results are provided as Appendix B. In summary, the survey demonstrated that the disseminated to podiform sulphides are discontinuous. The HLEM survey detected a point-source conductor,

coinciding with drill indicated gold-sulphide mineralization, indicating limited strike potential. The VLF survey did not detect the mineralized horizon, but did display a multi-line response tracing the volcanic - sediment contact south of the target horizon.

A sample (64074WR) of the relatively fresh pyroxene lapilli tuff which hosts the mineralized zone was selected from 1990 drill core, sent for whole rock analysis and indicates a basaltic composition (Figure #7).

#### 3.3 WEST GRID - GORGE & RPX AREA

The Gorge showing and the RPX area were inspected with Rex Pegg (Keewatin Engineering, Project Manager: 1988 - 1990 programs) for orientation. Corona concurs that drill testing has been complete, with the low tenor and discontinuity of results indicating that gold is erratically and uneconomically distributed.

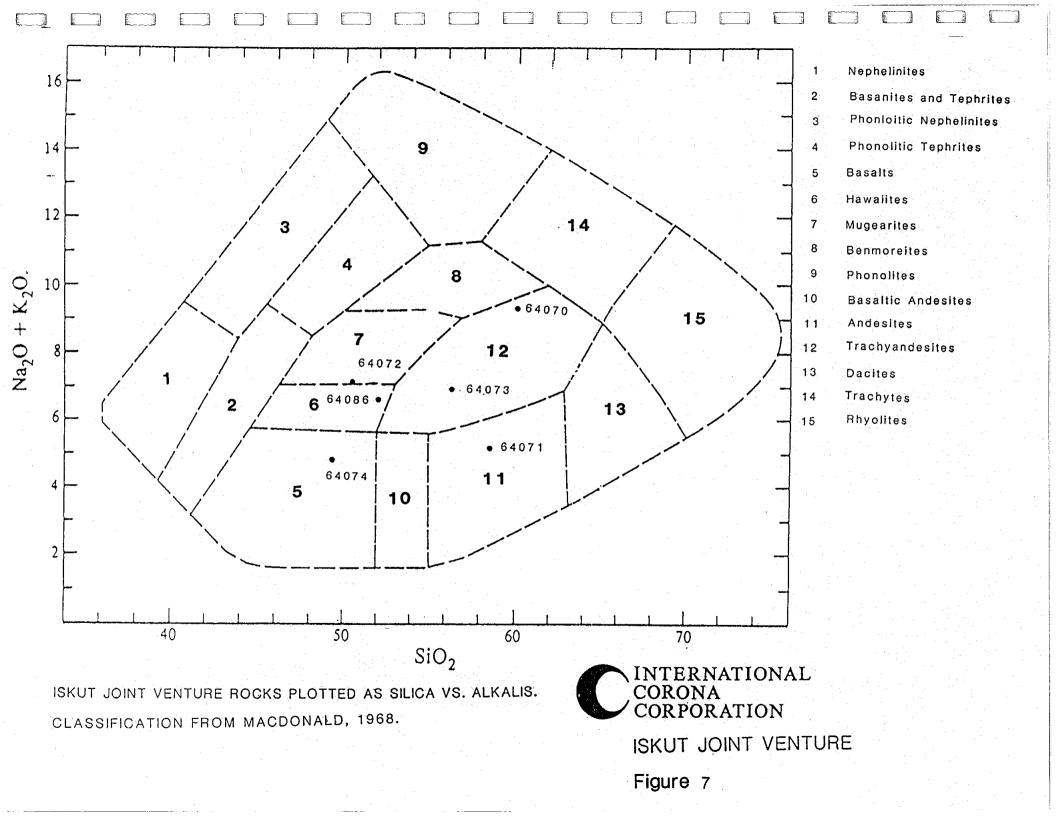
#### 3.4 WEST GRID - HEMLO WEST AREA

The drill core from the Hemlo West area was briefly re-examined and four samples (64070-73WR) were collected for whole rock analysis. Total alkalis in the andesitic - basaltic rocks (Ti/Al ratios range from 0.034 to 0.063; see also Figure #7) are elevated, likely indicating late Na and K introduction related to the Bronson and associated stocks. Unfortunately, the trench area was not remapped in sufficient detail to ascertain the structural-stratigraphic relations to the polymetallic mineralization.

#### 3.5 EAST GRID

Gold values up to 528 ppb had previously been identified in 13 soil anomalies (each greater than 100 ppb), along with 24 Cu-in-soil anomalies (>350 ppm), and four auriferous (840 ppb to 0.284 oz Au/ton) rock samples on the west extension of the East Grid. An additional 6 soils returned >50 ppb Au, up to 360 ppb, and 10 heavies returned >100 ppb Au, ranging between 130 and 12,000 ppb, in the East Grid area (Carter, 1991).

During 1991 these were located by grid number and ground checked by the Corona crew (Map #3). Many were interpreted as spurious results within glacial-fluvial material of indeterminable origin. Rock samples taken in the vicinity of anomalous soils at L 70+00E 40+00N of quartz sweats gave a result of 769ppb Au, 12.9ppm Ag and 1.03% Cu while the host volcanic returned no elevated Au, Ag or Cu values. Anomalies that



could not be immediately explained were detail soil sampled, ensuring sufficient penetration to avoid problems with overburden which could generate a false anomaly. Two of these areas were recommended for further investigation by trenching as of August 29, 1991:

1.

2.

A follow-up traverse to a previously identified Au & Cu-insoils anomaly along a small stream believed to be the extension of the "Meridor Break" just north of the east grid (L 68-72E, BL 46N) uncovered narrow semi-massive sulphide bands within host volcanics. The occurrence was partially exposed by redirection of the stream and hand trenching [3 chip rock samples later returned 30 to 100 ppb Au & 150 to 1050 ppm Cu, at two locations over a 50 metre strike extent]. In anticipation that this may be related to the source of the Au/Cu anomalies found to the south, five slope corrected lines were installed with a hip chain and compass These lines were soil sampled, prospected and mapped (although very little bedrock was exposed) to cover the new zone (see Map #3). Soil samples generally confirmed the presence of low magnitude Au and Cu-in-soil anomalies (ie: 10-146 ppb Au, and 30-300 ppm Cu), which may be related to the sulphidic-style mineralization located in the creek bed.

Follow-up of a previous silt sample (ie: L 81E, 42N) generated anomalous gold geochem in six mossmat samples [67-553 ppb Au, mean=215 ppb; 49-87 ppm Cu], in an area where no outcrop was seen and topography is subdued.

[Filenote regarding moss mat samples versus silt samples: Table 3 contains a comparison of moss mat and silt samples taken on the Iskut JV property. Comparison illustrates that the two sampling procedures provide similar results: Au values are slightly higher in silt samples than moss mats but the population distribution is very similar, with the silts having a small number of high values pulling up the mean and 90% <sup>tile</sup> (silt max=1700 vs moss mat max=225). Also, Ag is distinctly higher in the silts while Cu, Pb, Zn and Ni are distinctly higher in moss mats.]

		TABLE3: CO	MPARISO	N OF GEOCE	IEMICALTHRE	SHOLDS IN		
TABLE3: COMPARISON OF GEOCHEMICAL THRESHOLDS IN SILT ANDMOSS MATSAMPLES FOR ISKUT JV								
	MOSS MATS (n=24)					SILTS (n=1	18)	
	MEAN	MEDIAN	Q3	90%	MEAN	MEDIAN	Q3	90%
AU	30	4	26	79	53	4	23	120
AG	0.1	0.1	0.1	0.1	0.4	0.4	0.5	0.8
CU	66	59	69	82	29	5	44	77
PB	11	10	12	15	8	5	7	18
ZN	108	97	128	138	44	5	105	134
мо	2	1	2	3	13	5	13	38
SB	5	2	2	8	60	13	94	191
NI	110	122	152	196	65	16	94	191
со	14	15	16	19	8	9 .	14	16
CD	0.8	0.5	0.5	0.5	1.1	0.5	2.0	2.0
BI	3	2	2	5	24	5 .	44	63
AS	17	13	24	36	20	8	13	54
FE	3.39	3.46	3.63	4.10	3.37	3.48	3.72	4.06
TE	6	5	5	12	10	11	14	15
BA	209	198	258	291	249	249	320	328
CR	95	105	131	141	104	108	169	198
v	89	87	103	109	90	90	102	106
SN	10	10	10	10	10	10	10	10
w	10	10	10	10	10	10	10	10
LA	10	9	10	12	22	10	20	45
AL	1.98	2.03	2.38	2.49	2.29	2.31	2.74	2.83
MG	1.43	1.53	1.64	1.96	1.43	1.21	1.98	2.01
к	0.51	0.55	0.64	0.68	0.51	0.39	0.79	0.85
SR	47	43	52	62	56	51	62	79

## 3.6. EAST OF EAST GRID

The area near the eastern boundary of the property underlain by interbedded metasediments and porphyritic andesites was prospected and mapped with moss mat samples taken where large enough streams could be found. The vegetation in this part of the property is strongly dominated by tag alder, devil's club and miscellaneous bush, making prospecting and mapping difficult. Four moss mats returned gold values between 7 and 82 ppb, averaging 27 ppb Au.

### **3.7 MOUNT VERRETT**

The southern slopes of Mount Verrett was prospected and sampled. The exposure in the area is generally good, but the late snow cover prohibited a re-examination of the skarned contact zone which had been previously sampled. Farther down slope below the snow line, a few small rusty pods were found within the mafic volcanic flows. Three of seven samples returned gold values above detection limit, to a maximum of 42 ppb.

#### **3.8** NORTH OF MERIDOR GROUND

There is minimal bedrock exposure in this area. Creeks were moss mat sampled and float prospected. The metasediments showed no mineralization, but some of the moss mat samples were weakly anomalous in Au (ie: 4 of 11 samples contained 10-28 ppb Au, with another returning 121 ppb Au). A number of quartz veins were sampled in float, but none were found to be auriferous. [Note: 1987 flagging indicates that some stream sediment samples were misplotted, reinforcing the need for an orthophoto base for field orientation.]

4.0

## **1991 GEOCHEMICAL DATABASE & STATISTICS**

The database is comprised of 3156 soil, 2478 drill core, 1406 rock, 118 silt and 24 moss mat samples. Geochemical data is sorted by sample medium [it would have been very useful to separate rock and drill core data into lithotype populations, but this was not practically achievable]. Univariate (Appendix D) and bivariate statistics (Appendix E) were generated for each element and relevant element pairing (based on element associations and correlation coefficients).

Raw element data was plotted as histograms which are helpful in visualizing sample populations and for subjective estimation of anomalous thresholds. Many elements approach normal distributions (ex: Hg, Ba, Fe, Co, Cr K, Ca, Mg, Al, Sr, V, Y in rocks) reflecting minimal enrichment in purposefully biased samples, while others grossly approximate a natural lognormal distribution, even though several (Au, Ag, As, Sb, Zn, Pb, Cu) are severely skewed by extreme values during the same selection process. Rank order (ie: Spearman) correlation coefficients quantify positive and negative element associations.

Based on the genetic models described in section 1.5.2, we would predict the following metallic element associations:

Veins:	Au-Ag +/- Cu, Pb, Zn, As, Sb
VMS:	Zn-Pb-Cu-Au-Ag +/- As, Sb, Hg, Cd
Porphyry:	Cu-Mo +/- As, Sb, Ag, Au

Basic univariate statistics for the core study group of elements in rock samples are:

Element	n	Median	Mean	CV	Q3	95%
Gold	1406	45 ppb	1158	5.9	221	5211
Silver	1345	1.2 ppm	5.6	3.8	5.6	23.5
Copper	1345	172 ppm	713	4.0	528	2400
Lead	631	14 ppm	154	15.7	27	15.7
Zinc	548	60 ppm	504	6.7	100	1007
Arsenic	788	19 ppm	223	3.8	83	810
Antimony	387	2 ppm	5.5	8.4	3	11
Mercury	262	110 ppb	110	0.3	125	145
Molybdenum	387	2 ppm	8.3	2.2	7	34

Other than qualitative observations, very little can be inferred from the raw data as it is an exhaustive data set, including a significant number of purposefully biased samples (ie: grab samples of veins, gossanous material, etc). Very low concentrations of lead, antimony, mercury and molybdenum are noted. Zinc, gold, copper and arsenic are extremely skewed.

Examination of the rock, core and soil correlation matrices identified ranked positive associations [Note: (Spearman In-normal data) =: r > 0.6, : r > 0.4, +/-: r > 0.3]:

Rock:	Core:	Soils:
Au = Ag = Cu - As + /- Pb	Au - Pb	Au- 0 <u>0</u> .≁
Мо		
Ag = Au = Cu - Pb - As - Zn	Ag = Zn - Cu - Pb	Ag +/- Cu
Cu = Au = Ag = Co = Fe - V	Cu = Zn - Ag + / - Pb	Cu = Co =
$\mathbf{K} = \mathbf{V} - \mathbf{M}\mathbf{g} - \mathbf{A}\mathbf{u} - \mathbf{S}\mathbf{r}$		
Pb = Zn - As - Ag	Pb - Ag - Au +/- Cu	Pb - Zn - Cu
Zn = V = K = Fe = Mg = Pb - Co	Zn = Ag = Cu	Zn - Co +/-
Pb, Cu		
As - Pb - Au - Ag		As = Sb - Te
Sb = Te +/- Pb		Sb = Te = As
K = V - Mg - Au - Sr Pb = Zn - As - Ag Zn = V = K = Fe = Mg = Pb - Co Pb, Cu As - Pb - Au - Ag	Pb - Ag - Au +/- Cu	Pb - Zn - Cu $Zn - Co +/-$ $As = Sb - Te$

It may be possible that more subtle trace element haloes could be detected by utilizing factor analysis, although that methodology is perhaps more appropriate on the district scale, and the data set does not lend itself to ease of use.

## CONCLUSIONS AND RECOMMENDATIONS

Pre-1991 and 1991 exploration data has been compiled in digital format and is presented on TRIM-sourced base maps, utilizing orthophoto control. Certain plotting errors of pre-1991 work were discovered in the field this season, indicating both the need for an accurate base from the start of a field program, and the dangers associated with anomaly followup.

The few, small, low-order, coincident gold-copper soil geochem anomalies on the **Southwest Grid** are explained by Bronson Stock-related quartz veins containing similar tenor mineralization (ie: 100-500 ppb Au, up to 1000 ppm Cu). The intrusive and invaded country rocks do not display the type or magnitude of alteration typical of alkaline porphyry systems.

The geophysical response over the **Gregor** area indicating discontinuous point source sulphidic mineralization is consistent with previous drilling results.

The structural-stratigraphic relations of the Hemlo West polymetallic mineralization were not sufficiently examined, and remain enigmatic. Future work would include detailed surface and trench mapping, followed by additional trenching. Trace element and whole rock geochemistry in conjunction with mapping may detect subtle dispersion enrichments beyond the obvious alteration envelopes, and thereby isolate drill target vectors.

1991 follow-up of soil geochem anomalies on the East Grid isolated three areas warranting trenching, detailed sampling and geologic mapping:

- 1. At L 68-72E, BL 46N, a stream traverse in the vicinity of the "Meridor Break," uncovered auriferous (up to 100 ppb) narrow semi-massive sulphide bands within volcanics.
- 2. Near L 81E, 42N six mossmat samples returned anomalous gold values (ie: 67-553 ppb Au [Note: study indicates that mossmat sample values are generally comparable with silt sediment values]) in an area of subdued relief.
- 3. At L 70E, 40N selected quartz from sweats (generally 0.5 to 3 cm wide) from large angular talus blocks returned 769 ppb

Au, 12.9 ppm Ag and 1.03% Cu; host rocks are barren of mineralization.

No other new gold-bearing mineral occurrences were discovered on the property during 1991, which completed the property-scale mineral potential assessment with the exceptions of the upper Verrett slopes and the lower Iskut River slopes.

The property remains prospective for Snip-style mesothermal vein gold mineralization, although traditional systematic geochemical and geophysical methodologies have been exhausted. The potential for Eskayanalog VMS deposits is considered low, due to the lack of widespread alteration and low magnitude trace element contents (particularly antimony and mercury). The IJV property is not prospective for alkaline or calc-alkalic porphyry deposits.

Given the healthy assessment status of the Iskut Joint Venture property, and the generally low-order nature of the realized potential to date, reevaluation of the Hemlo West occurrence and trenching of the East Grid soil/rock anomalies can afford to await further industry-related mineral and logistical developments in the area.

Respectfully Submitted: INTERNATIONAL CORONA CORPORATION, on behalf of Prime Resources, IJV operator

Stephen Robertson Field Geologist Don Lewis Exploration Manager - W Canada

Copies to:

Prime Resources Group Inc American Ore Ltd Golden Band Resources Inc attn: Mr. A.H. Ransom attn: Mr. James Owen attn: Mr. Ken Carter

## INTERNATIONAL CORONA CORPORATION WESTERN EXPLORATION

## ISKUT JOINT VENTURE STATEMENT OF PROJECT EXPENDITURES FOR THE YEAR ENDED DECEMBER 31, 1991

	\$
LABOUR	48,370
FIELD EXPENSES	5,608
HELICOPTER	6,621
OTHER TRANSPORTATION	6,161
CAMP (FOOD & LODGING)	6,681
ANALYSIS	3,287
CONTRACT PAYMENTS	683
TOTAL	77,411

# LIST OF PERSONNEL

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<b>STEPHEN ROBERTSON - GEOLOGIST</b> (\$250/day) June 11 - July 1(21), August 28 - 29(2), October 8 - 31(17), November 1 - 22(16), December 4 - 31(14), January 2 - 10(7)	77 DAYS
PAUL JONES - PROSPECTOR/TEAM LEADER (\$27 June 11 - July 1(21), October 21 - 25(5), November 12 - 14(3)	/5/day) 29 DAYS
DAN BOYD - PROSPECTOR (\$200/day) June 11 - July 1(21)	21 DAYS
<b>RICHARD TAYLOR - STUDENT</b> (\$150/day) June 11 - July 1(21)	21 DAYS
JOHN BELLAMY - SENIOR GEOLOGIST (\$400/day) June 26(1)	1 DAY
KEN RYE - PROJECT GEOLOGIST (\$325/day) June 18(1)	1 DAY
MIKE KUSNEZOV - DRAFTSMAN (\$30/hr) October - December(157.5hrs)	157.5 HRS
<b>DAVE GAUNT - COMPUTING GEOLOGIST</b> (\$300/da August 16 - 30(2.5), October 8 - 10(2), November 14 - 15(1)	ay) 5.5 DAYS
DON LEWIS - PROJECT SUPERVISOR (\$425/day) August 26(1), January 9 - 10(2)	3 DAYS
ANDREW RANSOM - FIELD ASSISTANT (\$130/day) June 18(1)	1 DAY
<b>ELIZABETH CONESSA - FIELD ASSISTANT</b> (\$130/c July 18(0.5)	lay) 0.5 DAYS

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#### STATEMENT OF QUALIFICATIONS

I, Stephen Robertson, of 1969 Lower Road, Gibsons, B.C. VON 1V0 state that:

I am a 1989 graduate of the University of Alberta, Edmonton Alberta, with a B.Sc. in geology.

I have been employed in mineral exploration prior to my graduation and that I have been practising my profession since 1989.

I am presently on contract as a geologist with International Corona Corporation, #1440 - 800 West Pender Street, Vancouver, British Columbia. V6E 2V6.

I am the author of this report which is based on public and property reports plus on site inspections.

I have no interest, direct or indirect, in the property discussed in this report.

This report may be used for development of the property, provided that no portion of it is used out of context or in such a manner as to convey meanings different from that set out in the whole.

Consent is hereby given to the Iskut Joint Venture to reproduce this report in part or whole for corporate purposes relating to the raising of funds by way of a prospectus or statement of material facts.

Signed and dated in Vancouver, British Columbia this <u>24</u> day of \_\_\_\_\_\_

Stephan Roberto

Stephen Robertson, B.Sc.

23

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# APPENDIX A

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# ASSAY CERTIFICATES

PROJECT: 8117



#### Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V91-DN764\_D ( COMPLETE )

REFERENCE INFO: P.O. 191-051

CLIFNT: CORONA CORPORATION

SUBNITTED BY: UNKNOWN

DATE PRINTED: 10-JUL-91

		ORDER	ELI	ENENT		NUMBER OF ANALYSES	LOWER DETECTION LIMIT	EXTRACTION	METH	OD	
. [يجو] .		1	Au 10g	Gold - Fire	Assay	82	5 PPB	Fire-Assay	Fire	Assay AA	
. التزميز با		2	Ag	Silver		82	0.2 PPN	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
स्रुपन		- 3	Cu	Copper		82	1 PP#	HN03-HC1 Hot Fa	xtr. Ind.	Coupled Plasma	
		4	Pb	Lead		82	2 PPN	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
الجستا .		5	Zn	Zinc		82	1 PPN	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
Patrony		6	No	Nolybdenum		82	1 PPN	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
		7	Ni	Nickel		82	1 PPM	HN03-HCI Hot Fx	ktr. Ind.	Coupled Plasma	
htidi		8	Со	Cobalt		82	1 PPN	HN03-HC1 Hot Ex	xtr. Ind.	Coupled Plasma	· · · · · · · · · · · · · · · · · · ·
لتعديا		9	Cd	Cadmium		82	1.0 PPN	HN03-HC1 Hot Ex	ktr. Ind.	Coupled Plasma	
		10	Bi	Bisauth		82	5 PPN	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
Lores .		11	As	Arsenic		82	5 PPH	HN03-HCI Hot Ex	ktr. Ind.	Coupled Plasma	
Ē		12	Sb	Antimony		82	5 PPM	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
		13	Fe	Iron		82	0.01 PCT	HN03-HCI Hot Ex	ctr. Ind.	Coupled Plasma	
		14	Mn	Nanganese		82	1 PPN	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
		15	Te	Tellurium		82	10 PPN	HN03-HC1 Hot Ex	ktr. Ind.	Coupled Plasma	
awy		16	Ba	Barium		82	2 PPN	HN03-HC1 Hot Ex	xtr. Ind.	Coupled Plasma	
		17	Cr	Chromium		82	1 PPH	HN03-HCI Hot Ex	ktr. Ind.	Coupled Plasma	
	<u> </u>	18	V	Vanadium		82	1 PPM	HN03-HC1 Hot Ex	xtr. Ind.	Coupled Plasma	
khai		19	Sn	Tin		82	28 PPH	HN03-HC1 Hot Fx		Coupled Plasma	
المنتقا		20	H	Tungsten		82	20 PPH	HN03-HC1 Hot Ex	xtr. Ind.	Coupled Plasma	
-		21	La	Lanthanua		82	1 PPN	HN03-HCI Hot Ex	ctr. Ind.	Coupled Plasma	
lumi.		22	AL	Aluminum		82	0.01 PCT	HN03-HC1 Hot Ex	xtr. Ind.	Coupled Plasma	
-1.000	<u></u>	23	lig	Hagnesiun		82	0.01 PCT	HN03-HC1 Hot Ex	xtr. Ind.	Coupled Plasma	
i ing		24	Ca	Calcium		82	0.01 PCT	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	
		25	Na	Sodium		82	0.01 PCT	HN03-HC1 Hot Ex	xtr. Ind.	Coupled Plasma	
البنيار.		26	K	Potassium		82	0.01 PCT	HN03-HC1 Hot Ex		Coupled Plasma	
interest of the second s		27	Sr	Strontium	e politica de la composición de la comp En contra composición de la composición	82	1 PPH	HN03-HC1 Hot Ex	ktr. Ind.	Coupled Plasma	
[etc.]		28	Y	Yttrium		82	1 PPN	HN03-HCI Hot Ex	xtr. Ind.	Coupled Plasma	



	REPORT: V91-	00713.0 ( COMF	PLETE )						ROJECT: 81	D: 2-JU 17		PAGE 1A	
	SAMPLE NUMBER	ELEMENT UNITS	Ag PPH	Au_10g PPB	Cu PPM	Pb PPM	Zn PPM	Ho PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM
	T1 64327		<0.2	<5	78	7	134	<1	87	16	<1.0	<5	5
	T1 64334		<0.2	8	44	7 .	317	<1	13	10	2.8	<5	66
	T1 64339		<0.2	6	64	15	152	<1	100	16	<1.0	<5	45
	R2 64042		<0.2	8 -	110	5	92	<1	119	19	<1.0	<5	<5
	R2 64044		<0.2	49	21	<2	5	<1	19	2	<1.0	<5	<5
<u></u>	R2 64045		<0.2	22	195	4	36	<1	97	14	<1.0	<5	9
	R2 64046		<0.2	<5	43	4	49	<1	79	13	<1.0	<5	<5
	R2 64048		<0.2	<5	32	31	28	<1	14	3	<1.0	<5	12
	R2 64049		<0.2	<5	6	<2	3	<1	11	1	<1.0	<5	<5
	R2 64050		<0.2	<5	56	3	29	<1	121	14	<1.0	<5	6
	R2 64051		<0.2	<5	144	5	40	5	32	15	<1.0	<5	<5
	R2 64052		<0.2	<5	37	4	.62	<1	105	15	<1.0	. <5	<5
	R2 64054		<0.2	41	101	21	308	<1	4	9	<1.0	<5	. <5
	R2 64055	1	<0.2	<5	27	4 -	88	<1	5	11	<1.0	<5 (5	
292	R2 64056	<u> </u>	<0.2	<5	86	6	77	4	115	19	<1.0	<5	. 0
J	R2 64057		0.5	42	40	14	69	<1	19	56	<1.0	<5 <sup>,</sup>	13
	R2 64058		<0.2	<5	117	4	79	<1	7	19	<1.0	÷. <5	6
	R2 64059		<0.2	<5	167	4	83	<1	8	20	<1.0	<5	1
	R2 64060		<0.2	<5	125	. 5	98	<1	5	17	<1.0	<5	6
	R2 64061		<0.2	<5	28	7	76	1	5	11	<1.0	<5	<5
	R2 64062		<0.2	<5	3	5	86	<1	9	22	<1.0	<5	<5
	R2 64063		<0.2	<5	5	<2	2	<1	-4	<1	<1.0	<5	<5
	R2 64064		<0.2	<5	. 6	3	17	<1	<1	2	<1.0	<5	<s< td=""></s<>
	R2 64106		<0.2	<5	40	5	23	<1 3	8	9 1	<1.0 <1.0	<5 <5	<5 <5
	R2 64109		<0.2	<5	11	3	4	3	9		×1.0	< 1	<u> </u>
	R2 64110		0.8	52	526	8	55	128	104	17	<1.0	<5	11
	R2,64111		2.4	101	1055	18	90	5	144	48	<1.0	<5	32
	R2 64112		0.7	30	290	27	67	8	84	16	<1.0	<5	12
	R2 64113 R2 64114		1.0 <0.2	73 36	1026 153	7 9	41 93	42	129 155	62 22	<1.0 <1.0	5 <5	40 6
<u> </u>			 	· · · · · · · · · · · · · · · · · · ·							· ·		
	R2 64115		<0.2	6	58	5	15	<1	80	8	<1.0	<5	6
	R2 64207		<0.2	<5 11.4	65	4	40	<1 /1	20	9	<1.0	<5 /5	<5 <5
	R2 64208 R2 64209		<0.2 0.3	114 100	16 17	12 20	33 34	<1 <1	13 8	5	<1.0 <1.0	<5 <5	<5 <5
	R2 64209 R2 64210		0.3 <0.2	100	24	20	53	<1 <1	8 10	. 9	<1.0 <1.0	<5	<5
	NZ U7210		10.2	100	<u></u>	14		<u> </u>			VI .U	\J .	
	R2 64211		<0.2	10	10	13	38	<1	10	7	<1.0	<5	<5
9	R2 64212		<0.2	<5	34	12	40	<1	13	8	<1.0	<5	6
	R2 64213		<0.2	6	14	17	29	<1	8	4	<1.0	<5 /5	б 10
	R2 64214 R2 64215		29.3 <0.2	<5 8	167 162	13 18	46 23	11 1	11 76	7 14	<1.0 <1.0	<5 14	10 24



A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

REPORT: V91-0	)0713.0 ( COM	PLETE )			APE INSPECT	ION & LEST	DA	TE PRINTE OJECT: 81	<u>D: 2-JUL</u> 17		PAGE 18	
SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Fe PCT	Mn Pct	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	₩ PPM	La PPM	A1 PCT
T1 64327 T1 64334 T1 64339 R2 64042 R2 64044		<5 <5 <5 <5 <5 <5	4.96 4.06 3.48 4.22 0.66	0.09 0.15 0.05 0.04 0.01	10 <10 <10 10 <10	407 187 210 164 14	108 15 143 197 292	151 78 106 113 7	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20 <20	4 27 4 3 <1	2.30 2.31 2.51 2.34 0.10
R2 64045 R2 64046 R2 64048 R2 64049 R2 64050		<5 <5 <5 <5 <5 <5	3.74 4.80 1.31 0.52 3.29	0.03 0.04 0.03 0.01 0.03	<10 10 <10 <10 10 10	176 652 120 14 298	177 291 141 306 274	71 141 18 5 109	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	5 4 2 <1 3	1.55 3.11 0.92 0.08 2.06
R2 64051 R2 64052 R2 64054 R2 64055 R2 64056		<5 <5 <5 <5 <5	4.79 3.72 5.75 4.90 5.21	0.06 0.03 0.14 0.11 0.04	12 12 11 12 12 15	153 672 87 98 83	103 201 33 25 233	165 95 180 143 169	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	7 3 6 3 2	2.01 2.34 5.04 1.51 3.23
R2 64057 R2 64058 R2 64059 R2 64060 R2 64061		<5 <5 <5 <5 <5 <5	5.55 5.73 5.62 5.44 5.30	0.12 0.06 0.10 0.08 0.13	13 12 11 11 <10	33 212 322 455 195	38 29 22 18 40	180 179 167 168 201	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	5 3 4 4 11	3.86 2.36 2.68 2.90 1.50
R2 64062 R2 64063 R2 64064 R2 64106 R2 64109		<5 <5 <5 <5 <5	4.81 0.42 1.31 3.74 0.55	0.10 0.01 0.08 0.03 0.01	<10 <10 <10 <10 <10 <10	326 6 118 106 40	31 361 49 68 276	207 4 23 83 8	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	11 <1 9 9 <1	2.62 <0.01 0.66 1.13 0.17
R2 64110 R2 64111 R2 64112 R2 64113 R2 64114		<5 <5 <5 <5 <5	4.13 6.90 3.57 7.32 5.57	0.05 0.04 0.06 0.05 0.04	<10 <10 <10 <10 <10 <10	81 22 127 16 142	209 178 187 248 407	138 92 102 138 142	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	5 7 9 12 3	3.25 2.83 2.34 3.30 3.19
R2 64115 R2 64207 R2 64208 R2 64209 R2 64210		<5 <5 <5 <5 <5	2.57 4.80 0.95 1.42 1.13	0.03 0.03 0.03 0.02 0.07	<10 <10 <10 <10 <10 <10	114 36 73 67 72	237 59 16 14 19	55 100 14 11 16	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	2 <1 4 4 4	1.39 1.69 0.74 0.65 0.68
R2 64211 R2 64212 R2 64213 R2 64214 R2 64215		<5 <5 <5 7 13	1.24 1.54 1.20 4.08 5.62	0.07 0.09 0.03 0.04 0.03	<10 <10 <10 <10 18	64 65 82 70 239	24 26 14 81 269	18 22 15 85 89	<20 <20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20 <20	6 7 7 4 3	0.70 0.84 0.70 2.60 2.24



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وطفيا	REPORT: V91-00	0713.0 ( COMP	LETE )						PROJECT: 8117 PAGE 1C
]	SAMPLE	ELEMENT	Mg	Ca	Na	K	Sr	Ŷ	
المتعنية	NUMBER	UNITS	PCT	PCT	PCT	PCT	PPH	PPM	
Lowood									
	T1 64327		1.90	0.89	0.04	0.85	40	7	
التعنيا	T1 64334		1.02	1.32	0.03	0.39	62	24	
(The second seco	T1 64339	الميني. مرجعة المرجع المرجع	2.01	0.95	0.13	0.53	57	7	
	R2 64042		2.07	0.68	0.16	1.72	30	8	and a first of the second state of the second state of the second state of the second state of the second state All second states are set of the second states and second states are set of the second states are set of the sec
استجها	R2 64044		0.10	0.04	0.01	0.02	3	<1	en an an an Anna an An Anna an Anna an
né-ili	R2 64045		1.65	0.92	0.14	1.03	32	9	
	R2 64046		3.01	0.59	0.16	2.17	38	9	
	R2 64048		0.56	0.60	0.08	0.23	19	3	
·	R2 64049		0.08	0.04	<0.01	0.03	2	<1	
	R2 64050		2.47	0.61	0.14	1.55	22	8	
					0.10				
	R2 64051	r en tr	2.13	1.20	0.16	1.46	27	- 8 E	
	R2 64052 R2 64054		2.41	0.67	0.19 0.21	1.55	. 34 70	. J 8	
Linth	R2 64054		1.20	2.53	0.18	0.57	77	. 8	
	R2 64056		3.30	0.71	0.10	2.15	48	8	
9	R2 64057		1.05	3.45	0.16	0.83	122	13	
<u>Γ</u>	R2 64058		1.94	1.23	0.15	1.64	66	9	
	R2 64059		2.26	2.88	0.11	2.01	86	8	
	R2 64060		2.15	1.36	0.12	2.13	84	8	
	R2 64061	<u></u>	1.23	0.76	0.10	1,55	97	. 8	
	R2 64062		2.24	2.49	0.06	2.03	133	6	and a second
	R2 64063		0.02	0.02	<0.01	0.02	- 1	<1	
۲	R2 64064		0.12	1.27	0.05	0.41	28	10	
lines	R2 64106		0.54	0.80	0.10	0.71	66	10	
	R2 64109		0.16	0.40	0.02	0.12	23	2	
	R2 64110	<u> </u>	2.24	4.20	0.24	1.57	151	9	
الم الم	R2 64111		1.83	1.56	0.16	1.79	74	. 7	
	R2 64112		1.70	4.57	0.12	1.58	86	10	
	R2 64113		2.70	1.94	0.12	2.21	57	10	
Line	R2 64114		2.73	0.80	0.11	2.25	23	8	
	DD (4115	· · · · · · · · · · · · · · · · · · ·	1 (1	1 00	0 07	0.36	010	r	
	R2 64115		1.65	4.88 1.08	0.07 0.08	0.36 0.02	213	5	
	R2 64207 R2 64208		0.26	0.52	<0.01	0.02	51 42	2	
	R2 64209		0.19	0.46	<0.01	0.09	34	2	
	R2 64210		0.33	0.69	<0.01	0.06	37	2	
i									
	R2 64211		0.33	0.40	<0.01	0.06	24	2	
	R2 64212		0.38	0.54	<0.01	0.06	29	2	
the state of the s	R2 64213		0.24	1.83	<0.01	0.05	54	3	
	R2 64214	1	1.08	0.73	0.06	0.12	56	6	
	R2 64215		1.61	0.74	0.15	1.25	63	6	

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Geochemical Lab Report

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	REPORT: V91-	00713.0 ( COM	PLETE )						OJECT: 81	D: 2-JUL 17		PAGE 2A	
	SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Au_10g PP8	Cu PPM	РЪ РРМ	Zn PPH	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM
· · ·	R2 64216	<u></u>	<0.2	<5	3	4	78	<1	2	4	<1.0	<5	<5
	R2 64217		<0.2	<5	36	5	47	<1	6	4	<1.0	<5	<5
	R2 64219		<0.2	8	15	3	17	<1	36	6	<1.0	<5	- 9
	R2 64221		<0.2	<5	82	10	99	<1	9	4	<1.0	<5	<5
	R2 64222		<0.2	<5	15	4	15	18	9	3	<1.0	<5	6
	R2 64223		<0.2	6	17	8	8	50	3	1	<1.0	<5	<5
	R2 64224		<0.2	<5	67	5	16	<1	169	14	<1.0	<5	25
	R2 64226		<0.2	· <5	160	7	68	<1	193	20	<1.0	<5	<5
	R2 64227		0.5	10	200	15	71	9	9	36	<1.0	<5	- 7
	R2 64228		<0.2	<5	73	11	65	11	161	20	<1.0	<5	11
<u>.</u>	R2 64229		<0.2	<5	91	10	44	<1	4	5	<1.0	<5	<5
	R2 64230		0.3	8	274	13	37	<1	10	10	<1.0	<5	<5
	R2 64231		1.3	66	466	. 7	31	3 .	7	41	<1.0	<5	6
	R2 64232		<0.2	<5	147	8	112	<1	6	21	<1.0	<5	<5
	R2 64233		0.4	44	1434	11	93	10	:	44	<1.0	. 7 .	<5
5—	R2 64234		(0.2	<5	16		42	11	3	4	<1.0	<5	<5
	R2 64235		<0.2 <0.2	<5 <5	44	4	42 55	11 <1		10	<1.0	<5	<5
	RZ 64255 R2 64311		<0.2	<5	81	- 11	85	1	90	16	<1.0	<5	7
	R2 64312		<0.2	<5	8	<2	2	<1	8	1	<1.0	<5	<5
	R2 64313		<0.2	<5	68	9	32	<1	33	10	<1.0	<5	9
	12 UNJIJ		NU+2				J2	<u> </u>	JJ	10		<b>`</b> J	,
	R2 64316		0.3	20	309	32	79	<1	57	21	<1.0	<5	785
	R2 64320		<0.2	28	119	29	635	2	132	19	2.4	<5	. 24
	R2 64323		<0.2	<5	. 77	10	77	<1	87	15	<1.0	`≺5	53
	R2 64324		<0.2	<5	22	7	14	<1	44	. 8	<1.0	<5	72
·	R2 64325		<0.2	<5	9	3	. 7	<1	16	3	<1.0	<5	<5
	R2 64328		<0.2	<5	32	<2	2	<1	29	4	<1.0	<5	<5
	R2+64329		1.7	95	146	867	793	<1	58	20	7.0	5	162
	R2 64330		<8.2	24	84	34	107	<1	33	24	<1.0	<5	40
	R2 64331		1.4	37	2434	12	50	<1	18	11	<1.0	6	5
	R2 64332		<0.2	<5	74	10	96	<1	21	24	<1.0	<5	11
	R2 64335		<0.2	<5	87	16	53	16	12	17	<1.0	35	<5
	R2 64336	· . · ·	<0.2	<5	98	9	50	<1	9	26	<1.0	<5	<5
	R2 64337		<0.2	<5	58	16	50	· <1 -	5	20	<1.0	<5	<5
	R2 64340		0.4	:<5	109	25	132	6	146	26	<1.0	5	12
	01 64041		<0.2	<5	58	8	112	<1	157	16	<1.0	<5	<5
	01 64043		<0.2	26	72	11	104	<1	164	16	<u>/1 0</u>		26
3	01 64043				178	11		7		16 12	<1.0	<5 <5	
9	01 64050		<0.2	<5 25		14	176		117	12	5.5	<5 75	10
	01 64053		<0.2 <0.2	<5	13	5	40	1	7 25	8	<1.0	<5 <5	<5 ~5
	UI 0410/		<u.z< td=""><td>&lt;5</td><td>42</td><td>6</td><td>47</td><td>&lt;1</td><td>73</td><td>11</td><td>&lt;1.0</td><td>50</td><td>&lt;5</td></u.z<>	<5	42	6	47	<1	73	11	<1.0	50	<5

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#### Geochemical Lab Report

	REPORT: V91-(	00713.0 ( COMF	PLETE )					PR	OJECT: 81	17		PAGE 28	
	SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Fe PCT	Mn PCT	Te PPM	Ba PPM	Cr PPM	V PPN	Sn PPM	W PPH	La PPM	A1 PCT
1	R2 64216		<5	2.64	0.08	<10	324	58	40	<20	<20	4	1.81
	R2 64217		<5	2.39	0.05	<10	94	65	45	<20	<20	4	1.33
	R2 64219		<5	1.23	0.03	<10	87	332	37	<20	<20	2	0.59
	R2 64221		<5	3.43	0.04	<10	148	75	158	<20	<20	4	2.28
	R2 64222		<5	1.91	0.02	<10	105	100	55	<20	<20	5	1.31
	R2 64223		<5	2.10	0.01	<10	324	158	16	<20	<20	<1	0.65
	R2 64224		<5	1.98	0.03	<10	137	187	56	<20	<20	4	1.70
	R2 64226		<5	4.26	0.04	<10	797	360	105	<20	<20	4	3.01
	R2 64227		<5	3.28	0.04	<10	56	100	218	<20	<20	6	3.80
	R2 64228		<5	4.53	0.03	<10	111	273	156	<20	<20	2	4.00
	R2 64229		<5	2.71	0.04	<10	245	167	62	<20	<20	9	2.03
	R2 64230		<5	3.56	0.03	<10	70	196	88	<20	<20	2	2.99
	R2 64231		<5	6.16	0.03	<10	233	209	85	<20	<20	<1	1.51
	R2 64232		<5	5.50	0.09	<10	575	26	207	<20	<20	2	3.50
	R2 64233		<5	6.87	0.08	<10	37	28	204	<20	<20	<1	3.11
)	R2 64234		<5	3.83	0.12	<10	118	95	37	<20	<20	11	1.22
	R2 64235		<5	5.04	0.08	<10	89	32	123	<20	<20	16	1.23
	R2 64311		<5	4.44	0.05	<10	543	148	140	<20	<20	4	4.72
	R2 64312		<5	0.46	0.00	<10	5	. 354	5	<20	<20	<1	0.02
· · · · · ·	R2 64313		<5	2.14	0.04	<10	302	119	50	<20	<20	3	3.57
	R2 64316		<5	3.12	0.08	<10	48	63	42	<20	<20	2	3.68
	R2 64320		<5	3.69	0.04	<10	351	213	110	<20	<20	3	2.72
÷	R2 64323		<5 .	3.16	0.04	<10	258	139	96	<20	<20	2	5.15
	R2 64324		<5	0.95	0.05	<10	40	69	28	<20	<20	3	2.76
	R2 64325		<5	0.59	0.01	<10	10	292	6	<20	<20	· · · · · · · · · · · · · · · · · · ·	0.21
<u> </u>	R2 64328		<5	0.62	0.00	<10	7	323	2	<20	<20	<1	0.03
	R2 64329		<5	6.41	0.14	<10	128	120	88	<20	<20	4	2.66
	R2 64330	•	<5	4.82	0.10	<10	66	70	56	<20	<20	5	1.50
	R2 64331		<5 	3.11	0.06	<10	333	249	83	<20	<20	4	1.40
	R2 64332		<5	5.96	0.09	<10	817	34	180	<20	<20	11	3.34
	· · · · · · · · · · · · · · · · · · ·			1						.00			2.00
	R2 64335		<5	4.85	0.06	<10	69	41	121	<20	<20	7	2.80
	R2 64336		<5	5.33	0.08	<10	134	24	229	<20	<20	7	3.18
	R2 64336 R2 64337		<5 <5	5.33 6.20	0.08 0.07	<10 <10	134 32	24 35	229 153	<20 <20	<20 <20	7	3.18 2.70
	R2 64336 R2 64337 R2 64340		<5 <5 <5	5.33 6.20 4.99	0.08 0.07 0.06	<10 <10 <10	134 32 75	24 35 210	229 153 154	<20 <20 <20	<20 <20 <20	7 3 1	3.18 2.70 6.45
	R2 64336 R2 64337		<5 <5	5.33 6.20	0.08 0.07	<10 <10	134 32	24 35	229 153	<20 <20	<20 <20	7	3.18 2.70
	R2 64336 R2 64337 R2 64340 01 64041		<5 <5 <5	5.33 6.20 4.99	0.08 0.07 0.06 0.08	<10 <10 <10	134 32 75	24 35 210	229 153 154	<20 <20 <20	<20 <20 <20	7 3 1	3.18 2.70 6.45
	R2 64336 R2 64337 R2 64340 01 64041 01 64043		<5 <5 <5 <5 <5	5.33 6.20 4.99 3.52 3.39	0.08 0.07 0.06 0.08 0.09	<10 <10 <10 <10	134 32 75 293	24 35 210 121	229 153 154 87	<20 <20 <20 <20	<20 <20 <20 <20	7 3 1 9	3.18 2.70 6.45 2.44
	R2 64336 R2 64337 R2 64340 01 64041		<5 <5 <5 <5	5.33 6.20 4.99 3.52	0.08 0.07 0.06 0.08	<10 <10 <10 <10 <10	134 32 75 293 213	24 35 210 121 	229 153 154 87 78	<20 <20 <20 <20 <20	<20 <20 <20 <20 <20	7 3 1 9 9	3.18 2.70 6.45 2.44 2.08

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# Geochemical Lab Report

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<b>W</b>			A DIVIS	ION OF INCHO	CAPE INSPEC	TION & TES	TING SERV		
	REPORT: V91	-00713.0 ( COMPLE	TE)	]				DATE PRINTED: 2-JUL-91 PROJECT: 8117	PAGE 2C
Tree I	SAMPLE NUMBER	ELEMENT UNITS	Mg Ca PCT PCT	Na PCT	K PCT	Sr PPM	Y PPM		
	R2 64216 R2 64217 R2 64219	0. 11.	0.62 0.35 0.55 0.39 0.33 1.40	0.15 0.13 0.06	1.00 0.58 0.25	40 21 26	5 7 5		
1793	R2 64221 R2 64222	0 0	0.45 0.45 0.44 0.21	0.16 0.05	1.29 0.67	71 23	7 5		
	R2 64223 R2 64224 R2 64226 R2 64227	0 2 0	0.18         0.16           0.95         1.82           0.88         0.90           0.71         3.47	0.03 0.19 0.19 0.12	0.49 0.41 1.86 0.74	76 85 50 257	2 10 7 12		
	R2 64228 R2 64229 R2 64230	0	1.38 1.68 0.67 1.66 1.79	0.41 0.18 0.22	0.72 0.62	118 70 240	8 8 6		
	R2 64231 R2 64232 R2 64233	2	.68 0.29 .23 4.14 .69 1.88	0.10 0.18 0.17	0.63 2.54 2.05	64 81 85	5 10 9		
	R2 64234 R2 64235 R2 64311 R2 64312 R2 64313	0 2 0	.42         0.57           .63         1.08           2.65         1.74           .05         0.04           .87         2.94	0.05 0.12 0.51 <0.01 0.30	0.81 0.79 2.26 0.01 0.41	28 64 160 2 278	9 15 12 <1 5		
	R2 64316 R2 64320 R2 64323 R2 64324 R2 64324 R2 64325	1 1 0	1.65 4.49 .59 1.06 .67 3.25 1.64 3.28 1.15 0.13	0.27 0.22 0.41 0.47 0.03	0.28 1.19 1.40 0.28 0.03	457 71 272 234 14	6 11 7 7 <1		
	R2 64328 R2 64329 R2 64330 R2 64331 R2 64332	1 0 1	.03         0.04           .87         2.92           .75         1.98           .08         1.65           2.60         2.61	0.05	0.01 1.19 0.72 0.95 2.59	5 62 40 100 183	<1 7 9 6 12		
	R2 64335 R2 64336 R2 64337 R2 64340 01 64041	2 1 3	.451.96.142.88.631.51.272.79.750.81	0.21 0.15 0.22 0.59 0.04	1.33 2.08 1.39 2.02 0.65	78 72 48 159 35	10 13 13 8 13		
	01 64043 01 64050 01 64053 01 64107 01 64108	1 0 0	.52 0.77 .20 1.61 .53 0.72 .88 0.76 .03 1.12	0.03 0.03 0.03 0.03 0.04 0.03	0.55 0.62 0.22 0.31 0.71	27 64 25 39 38	11 20 6 6 11		

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1 1. 	REPORT: V91-0	D0713.D ( COM	PLETE )		ł					DATE PR PROJECT				PAGE 3A	-
· · · ·	SAMPLE NUMBER	ELEMENT UNITS	Ag PPM	Au_10g PP8		Cu PPM	Pb PPM	Zn PP <del>M</del>	Mo PPN			Co PPM	Cd PPM	Bî PPM	As PPM
- <u>.</u> .	01 64218	<u>an in gorna</u> 1. Start - Start 2. Start - Start	<0.2	33	<u></u>	66	7	95	<1			20 17	<1.0	5	15
	01 64220 01 64225		<0.2 <0.2	121 6		69 75	9 8	94 90	<1 <1			16	<1.0 <1.0	<5 <5	40 <5
	01 64310 01 64314		<0.2 <0.2	<5 8		45 55	12 9	126 115	<1 <1			10 16	<1.0 <1.0	<5 <5	22 21
	UI 04314												<u>\1+0</u>		
	01 64315 01 64317		<0.2 <0.2	10 <5		56 58	14 8	86 90	4		6	15 15	<1.0 <1.0	8 <5	21 8
	01 64317		<0.2	<5		50	0 11	91	2		6	15	<1.0	<5	13
	01 64319		<0.2 0.4	<5 <5		59 65	9 16	88 85	<1 <1		6. 8.	16 14	<1.0 <1.0	<5 10	<5 31
	01 64321					00		<u> </u>				· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	J1
	01 64322 01 64326		<0.2 <0.2	<5 <5		40 89	9 12	128 138	<1 <1			14 20	<1.0 <1.0	<5 <5	. 9 8
	01 64333		<0.2	<5		31	10	208	<1	1	4	8	3.6	<5	36
	01 64338		<0.2	25		66	23	142	<1	12	б	19	<1.0	5	53
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\$\$ <b>9</b>	REPORT: V91-00	712 0 ( CON		A DIVISIO	N OF INCHC	APE INSPECT	FION & TESTI	ING SERVICES	E PRINTEC JECT: 811		)1	AGE 3B	
	KEPUKI: V91-00	/13.0 ( LUMP	([[[]]					PAU	JCC1: 011	• • • • • • • • • • • • • • • • • • •		NGC 30	· · · · · · · · · · · · · · · · · · ·
	SAMPLE NUMBER	ELEMENT UNITS	Sb PPM	Fe PCT	Hn PCT	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	W PPM	La PPM	A1 PCT
]	01 64218 01 64220 01 64225 01 64310 01 64314		ং ং ং ং ং ং	3.64 3.62 4.19 3.24 3.35	0.10 0.07 0.06 0.04 0.08	<10 <10 <10 <10 <10 <10	237 213 201 156 291	142 152 78 103 105	85 90 124 70 83	<20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	8 7 7 14 9	2.51 2.28 1.88 2.38 2.44
	01 64315 01 64317 01 64318 01 64319 01 64321		<5 <5 <5 <5 7	3.46 3.57 3.68 3.63 3.63	0.06 0.05 0.06 0.06 0.06	15 <10 <10 <10 <10 15	155 148 195 141 141	104 105 115 95 54	97 102 96 107 117	<20 <20 <20 <20 <20 <20 <20	<20 <20 <20 <20 <20 <20	9 9 10 9 9	1.90 2.02 2.11 2.04 1.79
	01 64322 01 64326 01 64333 01 64338		<5 <5 <5 <5	2.56 4.27 2.86 3.46	0.09 0.12 0.13 0.06	<10 <10 <10 <10	258 375 171 208	85 109 11 141	65 126 55 107	<20 <20 <20 <20 <20	<20 <20 <20 <20 <20	11 5 35 3	2.01 2.49 1.37 2.50
)												· · · · · ·	· · · · · · · · · · · · · · · · · · ·
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	REPORT: V91-0	0713.0 ( COM	PLETE )						F PRINTED: 2-JUL JECT: 8117	PAGE 3C
	SAMPLE NUMBER	ELEMENT UNITS	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM	Y PPM		
	01 64218 01 64220 01 64225 01 64310 01 64314		1.96 1.90 1.57 1.21 1.63	0.60 0.53 0.94 0.35 1.01	0.03 0.03 0.04 0.04 0.04	0.68 0.61 0.57 0.23 0.56	20 22 43 20 49	12 11 13 14 14		
	01 64315 01 64317 01 64318 01 64319 01 64321		1.54 1.64 1.61 1.57 1.28	0.83 0.89 0.76 0.90 0.89	0.03 0.03 0.03 0.03 0.03 0.04	0.49 0.52 0.60 0.52 0.52	43 42 41 44 40	13 14 15 14 13		
	01 64322 01 64326 01 64333 01 64338		1.10 2.02 0.65 2.11	1.24 1.44 2.59 1.26	0.04 0.03 0.03 0.10	0.41 0.74 0.33 0.69	57 52 103 62	15 9 24 9		
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## Geochemical Lab Report

	REPORT: V91-00713.0 ( CO	MPLETE )						ATE PRINT ROJECT: 8		91	PAGE 4A		
	STANDARD ELEMENT NAME UNITS	Ag PPM	Au_10g PPB	Cu PPM	РЪ РРМ	Zn PPM	Mo PPM	Ni PPM	Co PPM	Cd PPM	Bi PPM	As PPM	
	ANALYTICAL BLANK ANALYTICAL BLANK ANALYTICAL BLANK	<0.2 <0.2 <0.2	<5 <5 <5	<1 <1 <1	<2 <2 <2 <2	<1 <1 <1	<1 <1 <1	্ব ব ব	<1 <1 <1	<1.0 <1.0 <1.0	<5 <5 <5	<5 <5 <5	
	ANALYTICAL BLANK Number of Analyses	- 3	<5 4	- 3	3	- 3	- 3	- 3	- 3	3	-3	3	
	Mean Value Standard Deviation Accepted Value	0.10 0.000 -	2.5 0.00 5	0.5 0.00 -	1.0 0.00 -	0.5 0.00 -	0.5 0.00 -	0.5 0.00 -	0.5 0.00 -	0.50 0.000 -	2.5 0.00	2.5 0.00 -	· .
·						<u></u>			· · · · · ·			<u></u>	
	GEO TRACE STD 3 1989 Number of Analyses Mean Value Standard Deviation	0.3 1 0.31	-	256 1 255.5 -	29 1 28.8	241 1 241.3	<1 1 0.5	38 1 38.0	9 1 8.8 -	<1.0 1 0.50 -	<5 1 2.5	32 1 32.3	
· ·	Accepted Value	0.5	-	290	33	255	4	42	9	0.8	2	30	
)	HIGH GOLD STANDARD Number of Analyses Mean Value		1498 1 1498.0	-	-		-	-		-	-		
· ·	Standard Deviation Accepted Value		1500		-	-	· - · · · · · · · · · · · · · · · · · ·	- :	-	-	-	-	
	GEO TRACE STD-2 1989 Number of Analyses Mean Value Standard Deviation	3.8 1 3.84	-	740 1 740.2	240 1 240.1	451 1 450.6	465 1 465.8	533 1 532.8	42 1 41.6	<1.0 1 0.50	10 1 9.7	258 1 258.4	
	Accepted Value	5.0	_	820	250	500	600	600	40	2.0	4	320	
	GEO TRACE STD1 1989 Number of Analyses Mean Value	41.7 1 41.72		183 1 183.3	27 1 27.5	52 1 51.5	13 1 13.4	16 1 15.8	10 1 10.4	<1.0 1 0.50	9 1 8.8	16 1 16.3	
	Standard Deviation Accepted Value	36.0		190	- 15	62	17	14	7	0.2	1	8	
										· · · · ·			
									e Series Series Series Series				
<u> </u>					· · · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·						

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#### Geochemical Lab Report

A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES

								DATE PRIN	IED: 2-J	UL-91	PAGE 4		
	REPORT: V91-00713.0 ( CO	MPLCIC )						PROJECT:	0117	<u></u>	PAUC 4	D	
	STANDARD ELEMENT NAME UNITS	Sb PPM	Fe PCT	Mn PCT	Te PPM	Ba PPM	Cr PPM	V PPM	Sn PPM	₩ PPM	La PPM	A1 PCT	
	ANALYTICAL BLANK	<5	<0.01	<0.01	<10	<2	<1	<1	<20	<20	<1	<0.01	
	ANALYTICAL BLANK ANALYTICAL BLANK	<5 <5	<0.01 <0.01	<0.01 <0.01	<10 <10	<2 <2	<1 <1	<1 <1	<20 <20	<20 <20	<1 <1	<0.01 <0.01	
	ANALYTICAL BLANK	-	\U.UI -	×0.01	- 10	~~	~1 -		~20	×20 -			
	Number of Analyses	3	3	3	3	3	3	3	3	3	3	3	
	Mean Value	2.5	0.005	0.000	5.0	1.0	0.5	0.5	10.0	10.0	0.5	0.005	
	Standard Deviation Accepted Value	0.00	0.0000	0.0000	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0000	
	nucpicu faluc									a dhu t Ta			
									<u> </u>	<u></u>			
	GEO TRACE STD 3 1989	<5	· · · · · · · · · · · · · · · · · · ·	0.05	<10	62	76	9	<20	<20	3	0.78	
	Number of Analyses	1 2.5	2 000	1 0.051	1 5.0	1	1 75.6	1 8.7	1 10.0	1 10.0	1 3.0	1 0.783	
	Mean Value Standard Deviation	Z.9 -	2.989	0.001	5.0	62.0	12.0	0./·	10.0	10.0	<b>3.</b> 0	0.703	
	Accepted Value	5	2.40	0.06	-	64	75	9	5	1	4	0.77	
)	HIGH GOLD STANDARD			-	-		-	-	-	-			
	Number of Analyses	-		-	· · · - :		-	-	-	~		-	
	Mean Value	-	-	-	-	-	-	-	-	-	-	. –	
	Standard Deviation	-	-	-	ad ag 👘 s	-	<del>.</del> .			-	·		
·	Accepted Value			-	-			-		-			
	GEO TRACE STD-2 1989	37	4.33	0.07	<10	221	150	37	<20	<20	6	5.19	
	Number of Analyses	1	1	1	1 r 0	221 5	1 150.0	1 36.9	10.0	10.0	5.0	5 10¢	
	Mean Value Standard Deviation	36.7	4.325	0.069	5.0	221.5	120.0	30.9	10.0	10.0	5.9	5.194	
	Accepted Value	50	5.00	0.09	-	220	167	34	16	8	6	5.10	
	GEO TRACE STD1 1989	9	4.48	0.04	<10	71	91	94	<20	<20	4	2.96	
	Number of Analyses	1	1	1	1	1	1	1	1	1	1	- 1	
	Mean Value	8.6	4,476	0.044	5.0	71.5	91.2	93.9	10.0	10.0	3.8	2.958	
	Standard Deviation Accepted Value	- 7	4.50	0.05	_	- 74	89	90	-	2	- 4	2.75	

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			A DIVISI	ON OF INCH	ICAPE INSPE	CTION & TE	ESTING SERV	ACES DATE PRINTE	D: 2-JU	L-91		4
	REPORT: V91-00713.0 ( CC	)MPLETE )						PROJECT: 81	17		PAGE 4C	
	STANDARD ELEMENT NAME UNITS	Mg PCT	Ca PCT	Na PCT	K PCT	Sr PPM						
	ANALYTICAL BLANK ANALYTICAL BLANK ANALYTICAL BLANK ANALYTICAL BLANK	<0.01 <0.01 <0.01	<0.01 <0.01 <0.01	<0.01 <0.01 <0.01 -	<0.01 <0.01 <0.01	4 4 4	<1 -					· · · · · ·
	Number of Analyses	3	3	3	3	3	3					
	Mean Value Standard Deviation Accepted Value	0.005 0.0000	0.005 0.0000 -	0.005 0.0000	0.005 0.0000	0.5 0.00						
		en an					· · · · ·					
	GEO TRACE STD 3 1989 Number of Analyses Mean Value Standard Deviation	1.41 1 1.407	1.75 1 1.746	0.05 1 0.048	0.14 1 0.141	34 1 34.2	3 1 3.4		· · · · · · · · · · · · · · · · · · ·			
	Accepted Value	1.34	1.65	0.04	0.14	- 39	4				- 	· · · · · · · · · · · · · · · · · · ·
	HIGH GOLD STANDARD Number of Analyses Mean Value Standard Deviation Accepted Value						- - - -					
	GEO TRACE STD-2 1989 Number of Analyses Mean Value	4.57 1 4.569	5.98 1 5.981	0.31 1 0.315	0.21 1 0.208	80 1 79.7	6 1 6.0					
	Standard Deviation Accepted Value	4.90	5.13	0.30	- 0.20	78	- 6		·			
	GEO TRACE STD1 1989 Number of Analyses Mean Value	1.26 1 1.265	0.82 1 0.816	0.06 1 0.058	0.13 1 0.129	65 1 65.2	8 1 7.8					
P	Standard Deviation Accepted Value	1.21	0.76	0.06	0.12	63	-		· · ·			
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Geochemical Lab Report

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	REPORT: V91-00713.0 ( COM	PLETE )						ROJECT: 8			PAGE 5A	•
	SAMPLE ELEMENT NUMBER UNITS	Ag PPM	Au_10g PPB	Ĉu PPM	Pb PPM	Zn PPM	Mo PPM	Ni PPM	Со РРН	Cd PPM	Bi PPM	As PPM
	64042 Duplicate	<0.2	8 32	110	5	92	<1	119	19	<1.0	<5	<5
	64044 Prep Duplicate	<0.2	49 41	21	<2	5 <1	<1	10	2	<1.0	<5	<5
	64111 Duplicate	2.4	101 96	1055	18	90	5	144	48	<1.0	<5	32
	64215 Duplicate	<0.2 <0.2	8	162 171	18 7	23 25	1 <1	76 83	- 14 16	<1.0 <1.0	14 <5	24 <5
	64227 Duplicate	0.5	10 16	200	15	71	9	9	36	<1.0	<5	7
	64235 Duplicate	<0.2 <0.2	<5	44 42	4	55 54	<1 <1	4 3	10 10	<1.0 <1.0	<5 <5	<5 <5
	64312 Prep Duplicate	<0.2 <0.2	<5 <5	8 9	<2 <2	2 2	<1 <1	8 8	1 2	<1.0 <1.0	<5 <5	<5 <5
	64336 Duplicate	<0.2	<5 6	98	9	50	<1	9	26	<1.0	<5	`<5
	64050 Duplicate	<0.2 <0.2	<5	178 166	14 13	176 166	7 4	117 109	12 11	5.5 4.9	<5 <5	10 9
	64333 Duplicate	<0.2 <0.2	<5	31 31	10 11	208 207	4 4	14 13	8	3.6 3.8	<5 <5	36 37
	•											
										· · · · · · · · · · · · · · · · · · ·		
		· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·					· ·	· · · · · · · · · · · · · · · · · · ·
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# Geochemical Lab Report

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REPORT: V91-0	0713.0 C COM	PIFTE	1					TE PRINTE			PAGE 5B	
											nor JO	
SAMPLE	ELEMENT	Sb	Fe	Mn	Ĩe	Ва	Cr	Ŋ.	Sn	Ŵ	La	A1
NUMBER	UNITS	PPM	PCT	PCT	PPN	PPN	PPM	PPM	PPH	PPM	PPM	PCT
64042 Duplicate		<5	4.22	0.04	10	164	197	113	<20	<20	3	2.34
64044 Prep Duplicat	.e	<5	0.66	0.01	<10	14	292	7	<20	<20	<1	0.10
64111 Duplicate		<5	6.90	0.04	<10	22	178	92	<20	<20	7	2.83
64215 Duplicate		13 <5	5.62 6.41	0.03 0.03	18 <10	239 252	269 299	89 95	<20 <20	<20 <20	3 2	2.24 2.41
64227		<5	3.28	0.04	<10	56	100	218	<20	<20	6	3.80
Duplicate 64235 Duplicate		<5 <5	5.04 4.98	0.08 0.07	<10 <10	89 87	32 32	123 119	<20 <20	<20 <20	16 15	1.23 1.20
64312 Prep Duplicat	e	<5 <5	0.46 0.49	0.00 0.01	<10 <10	5 6	354 358	5 5	<20 <20	<20 <20	<1 <1	0.02 0.03
64336 Duplicate		<5	5.33	0.08	<10	134	24	229	<20	<20	7	3.18
64050 Duplicate		<5 <5	2.86 2.72	0.15 0.13	<10 <10	195 181	88 81	77 72	<20 <20	<20 <20	12 10	1.73 1.62
64333 Duplicate		<5 <5	2.86 2.73	0.13 0.13	<10 <10	171 170	11 11	55 52	<20 <20	<20 <20	35 33	1.37 1.30
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		lital Internet Nacional								· · ·		
	· · · · · · · · · · · · · · · · · · ·					1. * 1. 		· · · · · · · · · · · · · · · · · · ·			· · ·	
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Geochemical Lab Report

 REPORT: V91-007	13.0 ( COM	PLETE )						ATE PRINTED: ROJECT: 8117		PAGE	50	
 <u>.</u>			J									
SAMPLE	ELEMENT	Mg	Ca	Na	X	Sr	Y					
 NUMBER	UNITS	PCT	PCT	PCT	PCT	PPM	PPM					
 64042		2.07	0.68	0.16	1.72	30	8					
Duplicate									a tra			
64044	· .	0,10	0.04	0.01	0.02	3	<1				· ·	
Prep Duplicate	en e	0,10	0.04	0.01	0.02	<b>,</b>	<1					
64111 Dugliante		1.83	1.56	0.16	1.79	74	7					
Duplicate												
64215		1.61	0.74	0.15	1.25	63	6	•				
 Duplicate		1.87	0.81	0.16	1.32	65	7		· · · · · · · · · · · · · · · · · · ·		<u></u>	
64227		0.71	3.47	0.12	0.74	257	12					
Duplicate												
64235		0.63	1.08	0.12	0.79	64	15					
Duplicate	1. 1. 1. 1. 1.	0.62	1.00	0.12	0.76	63	14					
										· · · · · · · · · · · · · · · · · · ·		
64312 Prep Duplicate		0.05 0.06	0.04 0.04	<0.01 <0.01	0.01 0.02	2	<1 <1					
riep vupricate		0.00	V+V7	10+01	0.02	<b>,</b>	1					
64336		2.14	2.88	0.15	2.08	72	13					
 Duplicate										·		
64050	· · · · · · · · · · · · · · · · · · ·	1.20	1.61	0.03	0.62	64	20					
Duplicate		1.16	1.47	0.03	0.58	57	19					
64333		0.65	2.59	0.03	0.33	103	24					
Duplicate		0.63	2.57	0.03	0.31	98	23					
							n An the A					
e a Altar		· · ·										
 	<u> </u>	11. 								<u> </u>		

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ļ				A DIVISION	OF INCHC	APE INSPECT	TION & TESTI	NG SERVICES	te printi	ED: 10-JU	-91		
<u>l</u>	لتشل	REPORT: V91-00764.0 ( (	ONPLETE )					PR	OJECT: 8	117		PAGE 1A	
	rușe	SAMPLE FI FMFNI	Au_111g	Ag	Cu	РБ	Zn	No	Ni	Co	- Cd		As
	UHER O	NUMBER UNITS		PPN	PPN	PPN	PPH	PPM	PPN	PPN	PPN	PPH	PPII
7	with	S1 L68+00F 47+50N	10-	1.1	26	21	80	10	6	3	<1.0	<5	45
. [		S1 L68+00E 47+25N	<5	<0.2	97	15	105	22	10	15	<1.0	<s< th=""><th>28</th></s<>	28
		S1 L68+00F 47+00N	<5	1.9	9	31	48	7	. 3	<1	<1.0	<5	78
ſ	. المت	S1 L68+00E 46+75N	23	<0.2	89	18	163	7	27	10	<1.0	<5	24
	nad	S1 L68+00F 46+50N	128	0.9	99	19	122	11	22	5	<1.0	• <s< th=""><th>26</th></s<>	26
F		S1 L68+00E 46+25N	146	1.8	320	28	88	35	72	- 1	<1.0	<5	48
1		S1 L68+00E 46+00N	30	0.7	31	34	106	13	53	6	<1.0	<5	63
Ĺ		S1 L69+00E 48+25N	<5	0.7	10	26	137	7	7	3	<1.0	<s< th=""><th>42</th></s<>	42
		S1 L69+00E 48+00N	<5	0.7	49	19	93	5	14	6	<1.8	<5	46
		S1 L69+00E 47+75N	10	<0.2	74	6	106	3	9	15	<1.0	<b>\$</b>	<5
. 124	\$13	S1 L69+00E 47+50N	17	8.6	16			10	3	<u> </u>	<1.0	<১	
٢	المحث.	S1 L69+00E 47+25N	46	0.4	296	19	121	12	9	19	<1.0	<5	43
		S1 L69+00F 47+00N	18	<0.2	70	13	140	7	9	16	<1.8	<5	28
1	210 <b>1</b>	S1 L69+00E 46+75N	8	0.7	92	17	50	5	46	5	<1.0	<5	37
ſ		S1 L69+00F 46+50N	6	1.2	11	30	58		5	1	<1.0	<5	47
٦		S1 L69+UUE 46+25N	6	0.9	164	19	82	8	63	9	<1.0	<5	47
`	¥4:.	S1 L69+00E 46+00N	14	0.5	147	9	39	9	60	8	<1.0	<5	22
ſ	. است	S1 L70+00E 48+25N	13	<0.2	267	18	122	12	29	25	<1.0	<5	34
		S1 L70+00F 48+00N	3	0.6	14	17	49	7	6	2	<1.0	<5	27
<u>د</u> ت	- <b>-</b>	S1 L70+00E 47+75N	<5	0.4	126	19	109	6	32	17	<1.0	< <b>S</b> .	42
		S1 L70+00E 47+50N	16	1.0	182	25	126	12	39	12	<1.0	<5	
Ŀ	لسن	S1 L70+D0E 47+25N	13	<0.2	318	16	103	7	51	26	<1.6	<s< th=""><th>32</th></s<>	32
		S1 L70+00F 47+00N	12	0.3	111	13	111	5	11	14	<1.0	<5	22
ſ		S1 L70+00E 46+75N	<5	1.2	16	19	36	4	10	1	<1.0	<b>&lt;</b> S	39
Ļ	بر ۲۰	\$1 L70+00E 46+50N	17	0.7	57	19	73	6	26	3	<1.0	<5	60
F	seta	S1 L70+00E 46+25N	7	0.8	68	19	101	8		5 -	<1.0	<5	43
i		S1 L70+00F 46+110N	<5	0.4	89	13	34	9	43	6	<1.0	<s< th=""><th>25</th></s<>	25
۰.	الدينية.	S1 L71+00E 48+00N	<5	0.4	115	15	101	5	18	9	<1.0	<b>&lt;</b> 5	30
ŗ		S1 L71+00F 47+75N	6	2.1	44	28	85	4	29	7	<1.0	<5	31
		S1 L71+00E 47+50N	<5	1.6	22	33	145	9	6	1	<1.0	< <b>S</b>	77
		S1 L71+00E 47+25N	6	0.4	222	16	130	3	12	24	<1.0	<5	30
[		S1 L71+00E 47+00N	<b>&lt;</b> S	8.7	35	15	79	3	7	9	<1.0	<s< p=""></s<>	23
		S1 L71+00E 46+75N	20	<8.2	44	17	155	4	74	13	<1.0	<5	38
	·	S1 L71+00E 46+50N	<5	0.9	9	28	85	9	10	2	<1.0	<s s<="" th=""><th>59</th></s>	59
F		\$1 L71+00E 46+25N	<5	0.3	45	18	166	4	39	13	<1.0	<5	43
		S1 L71+00E 46+00N	8	0.4	92	15	59	12	52	8 -	<1.0	<5	28
l	eren eren eren eren eren eren eren eren	S1 L72+00E 48+25N	s s	0.3	52	18	100	7	79	11	<1.0	<b>&lt;</b> 5	46
1		S1 L72+DDE 48+DDN	11	0.6	128	15	76	4	72	18	<1.0	<5	38
, ka	i.as	S1 L72+00E 47+75N	<5	0.5	101	14	85	4	63	15	<1.0	<\$	30
	रह	S1 L72+00E 47+50N	<b>&lt;</b> 5	1.1	117	18	79	8	24	11	<1.0	<5	32

Bondar-Clegg & Company Ltd. Pop Pemberton Ave. rth Vancouver, B.C. P 2R5



# Geochemical Lab Report

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0 <b>4) 98</b> : 1	5-0681 Telex 04-352667	1	DIVISI	ON OF IN	CHCAPE	INSPECTIO	N & TESTIN		ROJECT:	8117		P	AGE 1B		
]	REPORT: 091-00764.0 ( COMPL	ETED		]	<b>v</b>	le	Ba	 Cr	V PPM	;	Sn PN	W PPM	La PPN	AT PCT	
1	SAMPLE ELEMENT	Sb PPN	Fe PCT		Mn PM	PPM	PP11	PPH			20	<20	12	3.47	
	NUMBER UNITS				226	- 15		13	151		<20	<20	11	7.72	
71	SI L68+UUE 47+50N	13	4.61		599	11	247	15	. 6		<20	<20	19 42	4.31	
	S1 L68+00E 47+25N	10	5.28		113	16	26	41	3	4	<20	<20	• 27	6.01	
ä	S1 168+00E 4/+11LIN	17	4.19		616	<10	84	.53	2		<20	<20	<i>c</i> ,		
	S1 168+10E 46+75N	<u>رج</u> ح	4.62		345	<10	46					<20		3.3	5
	S1 L68+00E 46+50N	0						153		1	<b>Z2IJ</b>	<20	34	4.1	
<b>.</b>		12	3.8	6	223	14	64	122		33	<20	<20	43	3.8	
	S1 L68+0UE 46+25N	18	4.2		296	20	84		1	9	<20 (20	<20	11	4.	
	S1 168+00E 46+000	11	4.1	17	648	<10 15	138	2		84	<20 <20	<20	6	2.	18
	S1 169+00E 48+ZON	13	4.2		300	<10	355	2	n 2	06	<b>\</b> <u></u>				 5 T
	S1 L69+00E 48+00N	<5	5.	34	609					(1)	<b>Z2U</b>	<20	13	1.	53 .14
1	S1 L69+DOE 47+75N	و د د 	<u></u>			<10	18			195	<20	<20	6	-	, 14 . 38
	S1 L69+00E 47+50N	<u> </u>		62	1179	19	19			173 184	<20	<20		_	. 68
	S1 L69+00E 47+25N	13		.11	1572	11	15		Fe .	61	<20	<20		· .	.69
1	C1 169+10F 4/+1111N	11		.62 .21	94	12	8		54 13	28	<20	<20	1		
 	C1 169+10E 46+15N	12		.71	141	13	1	9	70				1	3 3	3.6
	S1 L69+00F 46+50N	10	3	.05					.19	83	7211		· .		1.9
· }	and the second			3.87	192				109	88	<20				3.7
<b>(</b>	SI L69+00E 46+25N	15	. N	2.86	268	1	•	67	41	156	<20		u ,	6	2.5
N.	S1 169+00F 46+111N	8	· .	5.60	823			51	12	87	<21		, o	10	4.
	ST 170+80E 48+25N	8		4.28	179		U	28	49	193	<21	, ``	• • 		
l	C4 170+00E 48+00N	12		5.70	431	<b>1</b>	، ر.						23	11	3.
J.	S1 L70+00E 47+75N			<u></u>	- 43		14	146	68	134 190	<2	0 <	20	6	2.
<b></b>	SI L70+00F 47+50N	r		5.66	- 43	1 A A A A A A A A A A A A A A A A A A A	13	436	93	156	<2	0 <	20	9	. 4.
	S1 L70+00E 47+25N		4	5.34	87	<b>-</b>	10	218	21 71	40	<1	20 <	(20	13	3
(	S1 L70+00E 47+00N	<pre></pre>	5	4.86 4.11			(10	27	50	53	<	20 4	c20	18	و.
	S1 170+00E 46+15N		9	4.11 3.49	19		15	51	JU .					-11	-4
	S1 L70+00E 46+50N		13	3.4/						ST		24	<20	7	1
			n	3.87		91	12	<del>43</del> 103	104	.80		20	<20 <20	11	
 مرجع	S1 L70+00E 46+25N		11	2.83	1	29	11	322	42	123		(20 (20	<20	14	
	C4 170+00F 46+11UN		11	4.36		577	13 13	100	61	105		<20	<20	25	
	C1 171+00E 48+00M		9	4.64	· · · ·	893 474	17	57	13	20	]	160			
, <b> </b>	S1 L71+00E 47+75N		15	4.8	6	471					ç	<20	<20	9-	
	S1 L71+00E 47+50N				+	095	-14	-617				<20	<20	; 7 52	
Y	SI L71+00E 47+25N		-13	-5.1	•	393	15	176	16		8	<20	<20	53 · 36	
T	C1 171+00E 47+00N		8	3.5 3.8		619	13	204	151 9		10	<20	<20	36 35	
	C1 171+10E 46+12M		9	3.0		322	14	44	91		19	<20	<20	27	
	C1 171+111E 46+5UN		14	4		465	15	154	11						
	S1 L71+00E 46+25N		13	™ •	~×	 					99	<20	<20	12	
	la se a la seconda de la <u>seconda de la seconda de la s</u>				59	189		<u> </u>	138	1	12	<20	<20 <20	5	
	SI L71+00E 46+00N	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	<u>11</u> 14		.09	366	17	157 370	87	n 4 1	157	<20	<20	3	
	C1 172+00F 48+25N		14	1	.62	977	16	267	90	1 1	162	<20	<20	10	
1	1 72+00F 48+11UN	ų – – – – – – – – – – – – – – – – – – –	14	4	.60	362	15 12	240	3	1	174	<20	-64		• . •
I	S1 L72+00E 47+75N S1 L72+00E 47+50N S1 L72+00E 47+50N		10	-	.50	399	17								
		•			14 1 A 17 1 A				· · · ·						

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A DIVISION OF I	NCHCAPE	INSPECTION &	TESTING SE	RVICES		
				DAIF PRIN	1HD: 10-	JUL-91

است	REPORT: V91	-DN764.0 ( CO	NPLETE )						PRINTED: 10-JU ECT: 8117	PAGE	10
· -127	SAMPLE	FLFHENT	llg	Ca	Na	K	Sr	y			
	NUMBER	UNITS	PCT	PCT	PCT	PCT	PPN	PPN			
ijed	<u> </u>										
<u>اد.</u>	\$1 L68+00F	47+50N	0.37	0.10	0.02	0.10	- 37	6			
ł	S1 L68+DDE		1.03	D.24	0.03	D.47	35	7			· · ·
لنغنه	S1 L68+00F		0.02	0.01	0.02	0.02	<1	11			
	S1 L68+00E		0.53	0.05	0.05	0.19	10	31		-	
	S1 L68+DDE	46+50N	0.18	0.03	0.04	0.06	4	17		• • • • • • • •	
	S1 L68+00E	46+25N	1.32	0.15	0.02	0.41	22				
ما	S1 L68+00F	46+11NN	8.99	0.07	0.03	0.24	6	15			
	S1 L69+00E	48+25N	0.87	0.03	0.05	0.07	2	38			
للتؤيز	S1 L69+00E	48+110N	0.50	8.11	0.02	0.10	7	6			
<b>ا</b> لت:	S1 L69+00E	47+75N	1.52	0.38	0.02	0.62	23	4			
					<u>.</u>		· · · · · ·				· · · · · · · · · · · · · · · · · · ·
	S1 L69+00F	47+50N	0.06	0.04	0.02	0.03	6	4			· · · · · · · · · · · · · · · · · · ·
	S1 L69+00E	· · ·	1.52	0.54	0.03	0.40	55	5			
1	S1 L69+00F		1.49	0.58	0.02	1.01	23	7			
	S1 L69+DDE	and the second	0.97	0.07	0.03	0.16	5	8			
	S1 L69+00F	46+50N	0.03	0.02	0.02	0.04	2	8			
	S1 L69+DDE	46+25N	1.13	0.07	0.02	0.13	9	- 7			
ों •	S1 L69+00F	46+NNN	1.16	0.18	0.02	0.28	18	5			
	S1 L70+00E	48+25N	1.30	0.18	0.02	0.52	14	12			
	S1 L70+00E	48+00N	0.16	0.06	0.02	0.05	6	· · · 8 · · ·			
. 6	S1 L70+00E	47+75N	1.35	0.10	0.01	0.20	9	6			
	S1 L70+00E	47+50N	1.10	0.16	0.02	0.21	12	5			
	S1 L70+00E	47+25N	2.27	0.52	0.82	1.39	20	5			
	S1 L70+00E	47+00N	1.27	0.42	0.02	0.64	19	5			
لت.	S1 L70+00E	46+75N	0.23	0.04	0.02	0.05	5	7			
] .	\$1 L70+00E	46+50N	0.75	0.04	0.02	0.21	5	7			
	S1 L70+00E	46+25N	8.52	0.06	0.02	0.05	6	7			
)	\$1 L70+00E		8.71	0.13	0.02	0.15	14	5			
	S1 L71+00E		1.18	0.16	0.03	0.47	10	7			
	\$1 L71+00E		0.73	0.15	0.02	8.15	13	8			
	S1 L71+00E		0.11	0.03	0.04	0.07	1	27			
ual	S1 L71+00F	47+25N	1.64	0.36	0.02	0.89		5			i
	S1 L71+00E		0.73	0.38	0.02	0.34	25	5			
1	S1 L71+00E		1.56	0.11	0.02	0.50	12	32			
	S1 L71+00E		0.94	0.07	0.03	0.04	2	20			
	S1 L71+00F		1.68	0.22	0.03	0.39	22	14			
۹ <u>ـــــ</u>									en en en entre <del>La contracta da</del>		
 d	S1 L71+D0E	46+00N	1.02	0.07	0.03	9.17	8	6			
699	\$1 L72+00F		1.15	0.14	0.03	0.22	12	7			
4	S1 L72+0DE		1.91	0.28	0.04	0.87	16	5			
	S1 L72+00E		1.27	0.15	0.03	0.35	13	3			
25/	S1 L72+00E	47+50N	1.09	0.12	0.03	0.20	9	7			
3					· · · ·		<u> </u>	· · ·			



								NG SERVICES					
1. 14	REPORT: V9	1-011764.0 ( COP	PLETE )					PR	OJECT: 81	17		PAGE 2A	
	SAMPLE	FLEMENT	Au_10g	Âg	Cu	РЬ	Zn	flo	NT	Co	- Cd	Bi	As
	NUMBER	UNITS	PPB	PPM	PPN	PPN	PPN	PPN	PPN	PPN	PPN	PPM	PPM
	S1 L72+00F	47+25N	<5	0.9	36	33	102	8		7	<1.0	<5	88
	S1 L72+00E	47+00N	<5	0.3	129	18	207	4	57	19	<1.0	<5	35
•	S1 L72+00F	46+75N	<5	0.7	73	19	156	4	48	15	<1.0	<5	42
	S1 L72+00E	46+50N	<5	1.0	13	27	130	7	24	5	<1.0	<5	59
	S1 L72+00F	46+25N	<5	0.6	27	23	115	8	31	5	<1.0	• <5	43
	S1 L72+00E	46+1)11N	12	<0.2	269	14	72	5	93	14	<1.0	<\$	43
	<b>T1 64342</b>		7	<0.2	75	11	121	2	15	12	<1.0	<5	20
	T1 64344		12	0.4	92	18	172	3	14	12	<1.0	<5	38
	R2 64065		<5	<0.2	80	11	36	2	11	24	<1.0	<5	20
	R2 64066		<5	<0.2	38	14	55	2	19	16	<1.0	<5	19
	R2 64067		<5	<0.2		12	100	2	- 11	15	<1.0	<5	19
	R2 64068	an the second	<5	<0.2	64	11	35	12	8	16	<1.0	<	29
	R2 64069		<5	0.3	334	7	13	22	15	37	<1.0	< <u>s</u>	. 9
	R2 64116		<5	<0.2	33	3	10	26	2	4	<1.0	<5	7
	R2 64117		<5	<0.2	50	5.1	15	9	3	5	<1.0	<s s<="" td=""><td>18</td></s>	18
	R2 64118		<u>رج</u>	<0.2	82	<u> </u>	21		3	3	<1.0	<5	14
	R2 64119		14	<0.2	57	5	25	1	3	8	<1.0	<5	11
·* .	R2 64236		<5	<0.2	3	5	60	2	3	5	<1.0	<5	18
	R2 64237	and the second	19	0.5	244	23	439	4	88	25	<1.0	<5	30
	R2 64238		< <u>s</u>	<0.2	17	5	19	i	3	3	<1.0	<5	11
	R2 64239			<0.2			26	3		2	<1.0	<5	15
	R2 64240		<5	<0.2	30	5	18	<1	3	3	<1.0	<5	
	R2 64241		37	0.2	13	7	9	6	2	2	<1.0	<5	28
	R2 64242		<5	<0.2	8	7	3	2	3	2	<1.0	<5	11
	R2 64243		5	<0.2	9	8	48	3	3	3	<1.0	<5	14
 	R2 64244		<u>s</u>	<0.2	6		14	4		4	<1.0	<5	9
	R2 64245		6	0.2	62	7	30	3	3	4	<1.0	<5	15
	R2 64246		<s.< td=""><td>&lt;0.2</td><td>111</td><td>5</td><td>13</td><td>2</td><td>3</td><td>5</td><td>&lt;1.0</td><td>&lt;<b>Š</b></td><td>19</td></s.<>	<0.2	111	5	13	2	3	5	<1.0	< <b>Š</b>	19
	R2 64247		<5	0.5	61	8	34	3	3	6	<1.0	<5	19
	R2 64248		28	0.8	149	18	9	51	3	15	<1.0	<5	13
	R2 64249		211	0.4	12-	25	<u>5</u>	147	4	5	<1.0	<5	
	R2 64250		23	<0.2	55	5	11	22	2	2	<1.0	<5	8
	R2 64251		46	1.1	41	188	40	6	5	3	<1.0	<5	. 6
	R2 64345		<5	<8.2	2	12	72	<1	2	5	<1.0	<5	6
	R2 64346		553	8.7	715	43	28	73	6	3	<1.0	<5	29
			<u>(5</u>	<0.2			9				<1.0	<5	·9
	R2 64348		s	<0.2	10	6	42	11	4	. 6	<1.0	<5	13
	R2 64349		< <u>s</u>	<0.2	35	7	15	46	3	4	<1.0	<5	10
	R2 64350		<5	<0.2	33	4	15	10	3	3	<1.0	<5	ं रेड
	R2 64351		ा <b>८</b> ५	0.3		13	30	10		19	<1.0	<5	28



	REPORT: V91-00764.0 ( C	ORPLETE )		r N				OJECT: 81	D: 10-JUL 17		PAGE 28	
	SAMPLE ELEMENT	Sb	Fe	ňn.	Te	Ba	Cr		Sn	ų	la	A
	NUMBER UNITS		PCT	PPN	PPN	PPN	PPN	PPN	PPN	PPN	PPH	PC
	S1 L72+U0E 47+25N	19	4.39	424	211	68	14	46	<211	<211	-24	6,3
	S1 L72+00E 47+00N	13	4.26	1767	16	411	75	161	<20	<20	6	2.5
	S1 L72+80F 46+75N	15	4.47	1105	20	398	68	150	<28	<28	12	3.0
	S1 L72+00E 46+50N	15	4.08	340	15	47.	52	32	<20	<20	33	5.0
	S1 L72+D0F 46+25N	10	3.97	367	12	88	77	57	<20	<20	17	3.8
· · · ·	S1 L72+00E 46+00N	10	3.85	390	14	-313	171	121	<20	₹20	9	3.1
	T1 64342	7	2.89	1167	<10	122	18	67.	<20	<20	9	1.8
	T1 64344	8	3.24	1352	12	147	12	76	<28	<20	10	2.0
	R2 64065	8	3.13	538	13	216	33	115	<20	<20	7	1.6
	R2 64066	9	4.56	1033	13	354	46	168	<20	<20	6	2.2
	KZ 64067	8	5.01	1061	12	408	24	224	<20	₹20	9	2.3
	R2 64068	10	3.40	595	15	134	35	136	<20	<20	8	2.4
	R2 64069	6	3.46	848	<10	594	50	49	<20	<20	10	0.8
	R2 64116	<5	1.24	480	<10	265	71	21	<20	<20	12	0.5
	R2 64117	<5	1.72	443	<10	217	63	35	<20	37	10	0.7
	R2 64118	<5	1.41	450	<10	124	76		<20	<20	11	0.9
•	R2 64119	<5	1.76	601	<10	154	48	28	<20	<20	7	0.8
	R2 64236	6	2.47	596	<10	160	29	46	<20	<20	13	1.2
	R2 64237	11	5.58	934	15	231	100	171	<20	<20	12	2.2
	R2 64238	र्ड	1.21	425	<10	89	93	35	<20	<20	8	0.9
	R2 64239		1.65	242	<18	228	41	21	<28	<20	11	0.9
	R2 64240	<5	1.70	692	<18	176	70	29	<20	<20	14	0.8
	R2 64241	<5	1.88	94	<10	139	75	9	<20	<20	2	0.6
	R2 64242	<5	1.30	474	<10	39	123	31	<20	<20	8	0.8
	R2 64243	5	1.46	844	<10	238	86	20	<20	34	11	0.9
	R2 64244	6	0.95	248	<10	103	208	8	<20	<20	6	0.3
	R2 64245	8	1.72	637	<10	187	70	31	<20	<20	8	1.1
	R2 64246	<5	1.25	620	<10	164	78	17	<20	<20	17	0.6
	R2 64247	7	1.88	783	11	179	76	31	<20	<20	10	1.22
	R2 64248	6	7.15	201	<10	31	74	56	<20	69	3	0.8
	R2 64249	<5	2.68		<10	205	127	15	<20	<20	8	0.4
	R2 64250	<5	1.44	254	<10	625	112	15	<20	<20	7	0.4
	R2 64251	<5	1.69	68	<18	363	111	5	<20	<20	3	0.2
	R2 64345	<5	2.24	783	<10	193	52	41	<20	<20	6	1.2
	R2 64346	6	2.64	55	<10	48	185	48	<20	<20	đ	0.34
	R2 64347	<5	1.18	483	<10	211		- 22	<20	<20		0.6
	R2 64348	<5	3.07	637	<10	176	89	22	<20	<20	7	1.0
	R2 64349	6	1.39	842	<10	251	90	20	<20	<20	15	0.7
	R2 64350	s s	1.50	895	<10	212	72	23	<20	<20	11	0.70
	R2 64351	10	1.79	389	<10	537	296	44	<20	<20	4	1.00



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	REPORT: V91-00764.0 ( C	UNPLENE )						PROJECT: 8117 PAGE 2C
a a a a a a a a a a a a a a a a a a a	SAMPLE FLEMENT	lig	Ca	Na	<u>к</u>	Sr	Y	
	NUMBER UNITS		PCT	PCT	PCT	PPN	PPN	
	· · · · · · · · · · · · · · · · · · ·							
(977 <b>0</b> )	S1 L72+00E 47+25N	0.34	0.06	0.03	0.08	/	14	
	S1 L72+00E 47+00N	1.44	0.48	0.04	0.61	32	5	
100.00	S1 L72+D0E 46+75N	1.59	0.49	0.03	0.86	30	10	
	S1 L72+00E 46+50N	0.37	0.04	0.04	0.06	3	17	
	S1 L72+00E 46+25N	0.61	0.07	0.04	0.17	7	10	
	S1 L72+00E 46+00N	1.97	0.19	0.03	0.82	24	7	
网络眼	T1 64342	1.02	1.39	0.02	0.30	79	10	
	T1 64344	1.00	1.05	0.03	0.32	51	12	
1364	R2 64065	1.17	1.53	0.07	1.12	246	7	
	R2 64066	1.16	2.47	0.07	1.63	315	. 6	
লি ব							·	a <u>na sa sa</u>
	R2 64067	1.42	1.13	0.08	1.81	71	8	
	R2 64068	1.45	1.40	0.07	1.49	169	8	
N 1.93	R2 64069	0.18	0.48	0.02	0.49	27	7	
	R2 64116	0.10	1.56	0.05	0.35	88	9	
	R2 64117	0.26	0.48	0.05	0.48	137	7	
<u> </u>								
	RZ 64118	0.23	1.39	0.06	0.34	413		
	R2 64119	0.29	1.30	0.05	0.55	93	6	
E	R2 64236	0.56	1.08	0.06	0.92	31	9	
	R2 64237	1.63	0.77	0.06	1.02	48	12	
أستنا	R2 64238	0.32	D.78	0.07	0.39	182	6	
[iffer]	R2 64239	0.31	0.43	0.04	8.65	46	9	
	R2 64240	0.23	1.01	0.06	0.46	228	10	
التنقط	R2 64241	0.11	0.05	0.02	0.43	12	1	
	R2 64242	0.05	1.19	0.07	0.10	691	6	
	R2 64243	0.33	1.60	0.04	0.62	178	9	
uizer	<u>er i se i de la si kate ser</u> Receber de la servici							
	R2 64244	0.07	0.41	0.03	0.24	34	3	
[]	R2 64245	0.46	0.66	0.05	0.51	217	7	
لس	R2 64246	0.05	1.96	0.04	0.37	90	10	
	R2 64247	0.38	0.99	0.06	0.65	291	<u>7</u>	
[]	R2 64248	0.14	0.52	0.04	0.52	93	5	
Jaines	R2-64249	0.04	0.08	0.06	0.26		2	
	R2 64251	0.07	0.17	0.04	D.27	183	4	
(FB)	R2 64251	0.03	0.05	0.06	0.19	25	2	
	R2 64345	0.64	0.83	0.08	0.98	46	5	
	R2 64346	0.04	0.03	0.02	0.24	8	<1	
- [TRA					· · · ·	<u> </u>		
	R2 64347	0.14	1.57	0.05	0.42	170	9	
6	R2 64348	0.32	0.18	0.02	0.70	26	5	
<u>المجا</u>	R2 64349	0.09	2.01	0.03	0.49	159	.11	
	R2 64350	0.08	8.95	0.04	0.41	82	9	
أخضنا	R2 64351	1.40	3.67	0.10	0.49	72	6	

ræð.	Bundar-Clegg & Co 130 Pemberton Ave. North Vancouver, B V7P 2R5 504) 985-0681 Telex	.C.				BO	BC NDAR-C						emical Report	
(	REPORT: 4			LETE )	A DIVISIO				NG SERVICES DA PR	TE PRINTE OJECT: 81	D: 10-JUL 17	-91	PAGE 3A	
	Sanple Number	F	IFMENT A UNITS	u_1Ug PPB	Ag PPN	Cu PPN	РЬ Ppn	Zn PPN	No PPN	Ni PPN	Co PPN	Cd PPN	Bi PPN	As PPN
ا الم	01 64341 01 64343			8 82	0.3 0.3	67 82	15 19	911 132	3 3	13 12	11 11	<1.0 <1.0	<del>ر</del> ج ح	24 41
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Geochemical Bondar-Clegg & Company Ltd. 130 Pemberton Ave. North Vancouver, B.C. Lab Report V7P 2R5 **BONDAR-CLEGG** '604) 985-0681 Telex 04-352667 A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES DATE PRINTED: 10-JUL-91 PROJECT: 8117 PAGE 38 REPORT: V91-D0764.0 ( COMPLETE ) FIFNENT Fe Tin Ba Cr U Sn ų ٤a. AT SAMPLE Sþ le PPM PPN PPN NUMBER PCT PPN PPN PPN PPN PPN PCT UNITS PPN 01 64341 <20 <20 10 8 2.57 1276 13 118 17 56 1.54 10 **<20** 1.79 01 64343 2.94 1360 12 132 10 67 <20 10

	Bondar-Clegg & Compa 130 Pemberton Ave. North Vancouver, B.C. V7P 2R5 '604) 985-0681 Telex 04-					BC IDAR-C					Lab	iemica Report	
	REPORT: V91-	-DN764.0 ( COM	PLETE )	A DIVISION	OF INCHCA	PE INSPECT	ION & TESTIN		ÅTF PRI ROJECT:	NTFD: 10-JU 8117		PAGE 3C	n de la composition de la comp
	SAMPLE NUMBER	ELEMENT UNITS	fig PCT	Ca PCT	Na PCT	K PCT	Sr PPM	<u>ү</u> РРИ					
	01 64341 01 64343		0.90 0.92	1.68 1.11	0.02 0.03	0.28 0.34	91 51	10 11					
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·			-			DSERVICES PROJECT: 8117			PAGE 4A			
	STANDARD FIFNENT NAME UNITS		Ag PPN	Cu PPH	P6 PPN	Zn PPN	No PPM	Ni PPN	Co PPH	Cd PPM	81 PPN	As PPI
	LOW AU STANDARD	51						-				
	Number of Analyses	t i t	-	<u>_</u>	-	-			-	-	· <u>-</u>	
	Nean Value	51.0	-		-	· · _ ·	<u>-</u>	-	<b>.</b>		-	
	Standard Deviation	-	-	_	· –	-	· · .	· <u> </u>	· · · ·	-	-	
	Accepted Value	50	-			-	<u>1</u> 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	-	-	<b>.</b>	• =	
	GEO IRACE STD-2 1989		6.9	677	187	411	4119	434	33	<1.0	<5	25
	Number of Analyses		1	1	1	1	1	1	1	1	. 1	:
	Mean Value	-	6.91	676.6	186.8	411.4	489.2	433.8	32.6	0.50	2.5	257.
	Standard Deviation	-	-	-	· [ -	_	-	· · · · - ·	1970 - <b>19</b> 70 - <b>19</b> 70 - 19700 - 19700 - 19700 - 19700 - 19700 - 19700 - 1970 - 1970 - 1970 - 1970 - 1970 - 1970 - 1970 -	-		
	Accepted Value	-	5.0	820	250	500	600	600	40	2.0	4	32
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	ANALYTICAL BLANK	<5	<0.2	4	<2	<1	. 1 .	<1	<1	<1.0	<\$	· <
	ANALYTICAL BLANK	<5	<0.2	<1	<2	<1	<1	· <1	<1	<1.8	<5	<
	Number of Analyses		3	3	3	3	3	3	3	3	3	
	Nean Value	2.5	0.10	0.5	1.0	8,5	0.7	0.5	0.5	0,50	2.5	2.
	Standard Deviation	<u> </u>	0.0M	0.00	0.00	0.00	0.35	0.00	0.00	0.000	0.00	0.0
	Accepted Value	5	1		-	-	-	-	-		-	
						e de la composición d La composición de la c						
	GEO TRACE STD1 1989		33.2	171	20	- 49	14	13	8	<1.0	~~<5	<u> </u>
	Number of Analyses		1	1	1	1	1	1	1	1	1	
	Nean Value	-	33.21	171.3	20.2	48.5	14.1	13.1	7.7	0.50	2.5	10.
	Standard Deviation	-	-	-	-	a su s <del>a</del> te	-	-	-	• •	- '	•
	Accepted Value	-	36.0	190	15	62	t7	14	7	0.2	1	·
	GEO TRACE STD 3 1989		0.5	280	39	248	4	47	10	<1.0	<5	4
	Number of Analyses		1	1	1	1 ( <b>t</b> )	1	1	1 -	1	1	
	Nean Value	-	0.51	279.7	39.3	247.7	3.5	47.3	9.7	0.50	2.5	45.4
	Standard Deviation	-	-			1	-			-		
: 	Accepted Value	- 	0.5	290	33	255	4	42	9	0.8	2	31
	······	<u> </u>		<u></u>		ala a si						



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A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES PRINTED: 10-JUL-91

i i ————	REPORT: 091-00764.0 ( CO	MPLETE )						ROJECT: 8			PAGE 4	3
T.S.	STANDARD ELEMENT NAME UNITS	Sb PPM	Fe PCT	No PPN	Te PPM	Ba PPN	Cr PPN	V PPN	Sn PPM	H PPN	La PPH	AI PCT
	LOH AU STANDARD					-			-			
ज़-रहे <b>स</b>	Number of Analyses	1. j. 1. <b>-</b> 1.	-		-	-	·-	· _		-	1. <u>1</u> .	
	Nean Value	-		. · · •		-		<del>.</del>	-	-	-	-
-17494 -	Standard Deviation	<del>-</del>	, - <u>-</u>	-	-	· -	·	· · · -	-	-	-	-
ومثل	Accepted Value	-	-	-	<del>-</del> .	- 19 <b>-</b> 1				-	• -	-
state	GEO TRACE STD-2 1989	- 44	3.46	598	14	210	128	32	<20	<20	5	4.19
	Number of Analyses	1	1	1	1	1	· 1	1	1	1	1	1
, 1979 -	Nean Value	44.3	3.465	597.9	14.2	210.0	127.9	32.3	10.0	10.0	5.5	4.190
ji si	Standard Deviation	· – .	1 . <del>-</del>	-	-	<del></del>	-	-	_	-		. –
	Accepted Value	50	5.00	850	·	220	167	34	16	8	6	5.10
T **	ANALYTICAL BLANK		0.01	<1	<10	<2	<1	<1	<20	<20	<1	<0.01
اللغنة. ·	ANALYTICAL BLANK	<5	0.01	<1	<10	<2	<1	<1	<20	<20	<1	<0.01
	ANALYTICAL BLANK	<5	<0.01	<1	<10	<2	<1	<1	<20	<20	<1	<0.01
	Number of Analyses	3	3	3	3	3	3	3	3	3.	3	3
	Nean Value	2.5	0.010	Ð.5	5.0	1.9	0.5	0.5	10.0	10.0	0.5	0.005
	Standard Deviation	0.00	0.0042	8.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.0000
143 1	Accepted Value	2 2 <b>1</b> 1	-	-	. <sup>.</sup> –	· · -	-	-	-	-		-
·····	GEO TRACE STD1 1989		3.54	407			85		<20	<20		2.33
	Number of Analyses	1	1	1	1	1	1	1	1	1	1	1
	Mean Value	11.1	3.536	407.5	11.3	70.2	85.1	86.9	10.0	10.0	3.8	2.333
1 I J I	Standard Deviation	_	1. <sup>198</sup> 2 <b>-</b> 1	- · · ·	-	_	· · · ·	-	-	-	<sup>-</sup>	· · · · •
ار	Accepted Value	7	4.50	500	-	74	89	90	- 	2	. 4	2.75
<u>منا</u> لی است	GEO TRACE STD 3 1989	6	2.53	546	- 11			10	<b>~2</b> 11	<20	4	0.74
ب	Number of Analyses	1	1	1	1	່ <b>t</b> ຸ	t	1	1	1	1	1
	Nean Value	6.1	2.527	546.1	11.2	69.3	79.1	10.2	10.0	10.0	4.0	0.743
1				1				1.1.1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		-
	Standard Deviation	-	· · · -	1	-			-	· · - ·			



# Geochemical Lab Report

REPORT: 091-00764.0 ( C	OMPLETE )		]			PRO	JECT: 8117	PAGE 4C
STANDARD FLEMENT	lig	Са	Na	K	Sr	Ŷ		
NAME UNITS	PCT	PCT	PCT	PCT	PPN	PPN		
LOW AU STANDARD	-	-						
Number of Analyses	-	-	-	-	-	-		
Nean Value Standard Deviation		<u>-</u>	-		·		n de la composición de	
Accepted Value			·	· -	-	<b>_</b>		•
		· · · · · · · · · · · · · · · · · · ·						
GEO TRACE STD-2 1989	3.32	3.36	0.26	0.16	70	4	<u> </u>	<u> </u>
Number of Analyses	1	1	1	1	1	1	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -	
Nean Value	3.321	3.356	0.262	0.163	70.3	4.1		
Standard Deviation Accepted Value	4.90	5.13	0.30	0.20	78	6	la de la companya de	
		5.15	0.00	0.20				
ANALYTICAL BLANK	<0.01	<0.01	<0.01	<0.01		<1		<u> </u>
ANALYTICAL BLANK	<0.01	<0.01	0.01	<0.01	<1	<1		
ANALYTICAL BLANK	0.01	<0.01	0.01	<0.01	<1	<1		
Number of Analyses Nean Value	3 0.007	3 0.005	3 0.008	3 0.005	3 0.5	3 0.5		:
		0.000	0.000	0.000	U•J		<u></u>	
Standard Deviation	0.0033	0.0000	0.0030	0.0000	0.00	0.00		
Accepted Value	. · · · ·	-	-	-	÷ -	-		
	<u> </u>	<u> </u>	<u>.</u>					
GEO TRACE STD1 1989	0.91	0.64	0.06	0.11	60	5		
Number of Analyses Nean Value	1 0.906	1 0.642	1 0.057	1 0.109	1 60.2	1 5.5		
Standard Deviation	0,700	U+0+2	-	0+1U/ -	UD 4 C 			
Accepted Value	1.21	0.76	0.06	0.12	63			
GEO TRACE STD 3 1989	1.12	4 ->0	0.06	0.15				
Number of Analyses	1.12	1.30	u.us 1	u.15 1	42	5 1		
Hean Value	1.117	1.376	0.057	0.147	41.6	3.3		
Standard Deviation	_		-	-	-	-		
Accepted Value	1.34	1.66	0.04	0.14	39	4	1.00	

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	REPORT: V91-00)	764.0 ( CO	NPLETE )						JECT: 81	10-301 117		PAGE 5A	·
	SAMPLE NUMBER	FIFMENT UNITS	Au_10g PPB	Ag PPN	Cu PPN	РБ РРМ	Zn PPN	No PPM	Ni PPM	Co PPN	Cd PPM	BT PPN	As Ppn
188	L68+00E 46+50N Duplicate		128 114	0.9 1.3	99 100	19 28	122 122	11 12	22 23	5 5	<1.0 <1.0	<5 <5	26 56
4	L70+00E 47+25N Duplicate		13	<0.2 <0.2	318 321	16 12	103 103	7 7	51 51	26 27	<1.0 <1.0	<5 • <5	32 30
) ]	L71+DOE 48+DON Duplicate		< <u>&lt;</u> <5	0.4	115	15	101	5	18	9	<1.0	<5	30
   	L72+00E 47+00N Duplicate		<5	0.3 0.4	129 131	18 16	207 210	4	57 60	19 19	<1.0 <1.0	<s <s< td=""><td>35 37</td></s<></s 	35 37
	64067 Duplicate		<u>ে</u> <5	<0.2	51	12	100	2	11	15	<1.0	<5	19
}	64237 Duplicate		19	0.5 <0.2	244 243	23 21	439 434	4 3	88 87	25 25	<1.0 <1.0	<5 <5	30 22
	64345 Duplicate		۲5 ۲5	<0.2	2	12	12	<1	2	5	<1.0	<5	6
	64350 Prep Duplicate		<5 <5	<0.2 <0.2	33 34	4 5	17 17	10 9	3 3	3 4	<1.0 <1.0	<5 د5	<5 11
7	Duplicate			<0.2	35	6	17	9	3	4	<1.0	<5	8



				A DIVISIO	N OF INCHC	APE INSPECT	ION & TESTI		TE PRINTE	ED: 10-JUL	-91		
	REPORT: 091-0076	64.U ( CUNH						Ph	ROJECT: 81	.17		PAGE 5B	
	SAMPLE	ELEMENT	Sb	Fe	ភិព	le	Ba	Cr	v	Sn	H	La	AI
	NUMBER	UNITS	PPM	PCT	PPM	PPN	PPM	PPN	PPM	PPM	PPM	PPN	PCT
	L68+00E 46+50N			4.62	345	<10	-46	53	26	<211	<20	21	6.01
	Duplicate		16	4.55	342	12	46	52	26	<20	<20	27	5.95
	L70+00E 47+25N		14	5.34	1292	13	436	93	190	<28	<20	6	2.77
	Duplicate		13	5.42	1299	16	438	93	193	<20	<20	• 6	2.81
-	L71+ODE 48+DDN Duplicate		11	4.36	5/7	13	322	42	123	<21)	<21)	11	3.12
	L72+00E 47+00N		13	4.26	1767	16	411	75	161	<20	<20	6	2.53
	Duplicate		12	4.38	1804	18	415	77	165	<20	<20	7	2.56
	64067		8	5.01	1061	12	408	24	224	<20	<20	9	2.34
	Duplicate												
	64237		11	5.58	934	15	231	100	171	<20	<20	12	2.23
	Duplicate		7	5.50	924	11	183	99	170	<20	<20	12	2.24
; <u> </u>	64345		<5	2.24	783	<10	193	52	41	<20	<20	6	1.26
	Duplicate				1								
	64350		<5	1.50	895	<10	212	72	23	<20	<20	11	0.70
	Prep Duplicate		5	1.51	909	<10	216	73	23	<20	<20	10	0.68
	Duplicate		<5	1.55	936	<10	224	74	24	<20	<20	11	0.71
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A DIVISION OF INCHCAPE INSPECTION & TESTING SERVICES TO PRINTED: 10-JUL-91

REPORT: V91-IIII/	54.U ( COM	PIFIF)					P	PROJECT: 8117	PAGE 5C
SAMPLE	ELEMENT	līg	Ca	Na	K	Sr	<u> </u>		
NUMBER	UNITS	PCT	PCT	PCT	PCT	PPM	PPM		
L68+00E 46+50N		0.18	0.03	0.04	0.06	4	17		
Duplicate		0.18	0.03	0.04	0.06	4	16		
L70+00E 47+25N		2.27	0.52	0.02	1.39	20	5		
Duplicate		2.30	0.54	0.02	1.41	21	6		•
L71+00E 48+00N		1.18	0.16	0.03	0.47	10	1		<u> </u>
Duplicate									
L72+00E 47+00N		1.44	0.48	0.04	0.61	32	5		
Duplicate	1	1.50	0.49	0.04	0.61	32	6		
64067		1.42	1.13	0.08	1.81	71	8		
Duplicate									
64237		1.63	0.77	0.06	1.02	48	12		
Duplicate		1.61	0.75	0.06	1.01	48	12		
64345	<u>.</u>	0.64	0.83	0.08	0.98	46	5		
Duplicate									
64350		0.08	0.95	0.04	0.41	82	9		
Prep Duplicate		0.08	0.93	0.04	0.42	80	8		
Duplicate		0.08	0.98	0.04	0.43	83	9		<u> </u>
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	REPORT: V91-	-00764.6 ( CO	IPLETE )					PROJECT:	8117	PAGE 1	
· · · · · · · · · · · · · · · · · · ·	SAMPLE NUMBER	ELEMENT UNITS	Au OPT								
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Peristered Accover Province of British Columbia

Bondar-Clegg & Company Ltd. 130 Pemberton Ave. North Vancouver, B.C. V7P 2R5 1604) 985-0681 Telex 04-352667



### Geochemical Lab Report

									DATE_PRINTE		-91		·
	REPORT: V91-UU770.Q ( COMPLETE )							3	ROJFCT: 81	17		PAGE 1A	
	SAMPLE	ELEMENT	Au_1flg	Âg	Cu	Pb	Zn	No	Ni	Co	Cd	Bi	Ás
	NUMBER	UNTTS	PPB	PPN	PPN	PPH	PPM	PPH	PPN	PPM	PPM	PPN	PPN
. *	S1 L70+D0E 4	2+25N	266	t.t	1120	37	151	17	26	17	<1.0	<5	51
	S1 L70+80F 4	and the second	132	0.3	88	54	106	8	10	11	<1.0	<5	51
	S1 L70+00E 4	1	94	1.0	89	18	127	13	13	u	<1.0	ँउ	40
	S1 L70+00F 4		57	1.6	85	78	234	27	. 7	6	<1.0	• <5	61
	S1 L70+00E 3		16	0.4	57	31	179	8	12	13	<1.0	<5	46
		р. <b>г</b> он		0.0	470	10	4.00			40			
	S1 L70+00F 3		77	2.2	162	48	122	63	5	12	<1.0	<5	48
	S1 L73+00E 4		<5	1.0	15	33	188	8	11	7	<1.0	<5	45
	S1 L73+00F 4		<5	0.8	40	21	60	5	29	8	<1.0	<5	21
	S1 L73+00E 4		tD	0.3	225	20	88	7	28	25	<1.0	<5	32
·	S1 L73+00E 4	1+37.5N	<5	<0.2	113	15	171	4	55	20	<1.0	<5	30
	S1 L73+00E 4	1+25N	<5	Ŋ.8	64	16	99	5	50	15	<1.0	<b>&lt;</b> 5	37
	S1 L75+00F 3	9+37.5N	<5	<0.2	95	17	112	5	27	24	<1.0	<5	36
	S1 L75+00E 3	9+25N	<5	0.5	107	24	112	5	31	18	<1.0	<5	43
	S1 L75+00F 3	9+12.5N	12	0.5	53	19	70	6	24	13	<1.0	<5	32
, e .	S1 L76+00E 3		<5	0.9	57	27	65	9	27	8	<1.8	<5	41
	S1 L76+00F 3	8+42 54	6	1.6	176	50	125	39	30	15	<1.0	<5	49
•	S1 L76+00E 3		32	1.9	78N	62	155	53	29	31	<1.0	3	51
	S1 L76+00F 3		- 37. <5	1.2	97	24	83	28	23	12	<1.0	دی دی	44
	S1 L80+87.5E		<u>رج</u> درج	0.3	59	19	87	4	62	12	<1.0	<u>۲</u> 5	40
:	S1 L80+87.5F	30+1101	<5	0.6	29	30	63	7	41	9	<1.0	<5	52
	S1 L81+DNE 3	1944 - A.	S	<0.2	8	33	46	6	3	<1	<1.0	<b>&lt;</b> 5	11
	S1 L81+00F 3		6	0.4	20	18	78	3	33	6	<1.0	<5	22
	S1 L81+00E 3	9+75N B	< <5	<0.2	47	24	91	6	75	12	<1.0	< <u>s</u>	27
	S1 L81+00F 3	7+62.5N	<5	0.2	30	24	72	6	98	10 ·	<1.0	<5	52
	S1 L81+00E 3	8+12.5N	6	<0.2	20	30	97.	9	t4	4	<1.0	<5	49
-	S1 L81+00F 3	B+UNN A	18	0.3	15	12	48	4	20	3	<1.0	<5	14
	S1 L81+DDE 3		321	<0.2	68	16	97	3	50	12	<1.0	<5	23
	S1 L81+00F 3		16	0.4	19	31	68	9	11	3	<1.0	<5	51
	S1 L81+12.5E	and a second	16	<0.2	81	20	71	5	114	16	<1.0	<5	45
	S1 L81+12.5F		<5	<0.2	12	23	103	5	4	2	<1.0	<5	41
	S1 L95+87.5E	45+50N	<5	1.2	17	35	94	8	15	2	<1.0	<5	59
	S1 L96+00F 4		Ś	<0.2	16	31	295	5	89	21	<1.0	<5	71
	S1 L96+DDE 4	4	11	0.5	24	41	161	4	41	6	<1.0	<5	39
	S1 L96+00E 4		7	<0.2	34	41	248	<1	66	21	<1.0	<5	21
	S1 L96+D0E45		<5	0.4	58	4J 28	240	. 3	89	16	<1.0	<5	45
<u></u>				••••T			·····				-1.0		
	S1 L96+00F 4		<5	0.4	34	27	352	. 4	143	25	<1.0	<5	78
	S1 L96+00E 4	3+DON A	14	0.9	14	17	52	11	7	2	<1.0	<b>(5</b> -	17
•	S1 L96+D0F 43	B+IION B	<5	8.6	19	36	112	11	6	2	<1.0	<5	.27
	S1 L96+00E43	+BON GRAVEL	<5	0.5	18	25	111	7	5	2	<1.0	<5	44
	S1 L96+12.5F	15.50.	6	0.2	47	72	1789	6	68	13	<1.0	<5	65

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Geochemical Lab Report

	REPORT: V91-00770.0 ( C					ROJECT: 81	0: 10-JUI 17		PAGE 1B			
	SAMPLE ELEMENT	Sb	Fe	Mo	Te	Ва	Cr	V	Sn	ų	la	Al
	NUMBER UNITS		PCT	PPN	PPN	PPN	PPN	PPN	PPN	PPH	PPH	PCT
•	S1 L70+00F 42+25N	15	8.26	437	11	73	54	107	<20	<20	7	3.20
	S1 L70+80E 40+50N	11	4.88	501	16	130	21	114	<20	<20	21	3.76
	S1 1.70+00F 48+25N	11	4.11	662	16	331	22	112	<20	<20	24	2.85
	S1 L70+00E 40+00N	12	4.18	324	11	64	15	82	<20	<20	• 16	3.22
	S1 L70+00E 39+75N	10	4.97	963	14	104	20	112	<20	<20	48	3.66
	S1 L70+D0E 39+50N	8	4.63	726	12	71	. 9	44	<20	<20	35	3.98
	S1 L73+00F 41+75N	10	4 81	489	<10	63	8	9	<20	<20	41	4.04
	S1 L73+00E 41+62.5N	10	4.06	210	12	151	60	137	<20	<20	7	2.03
	S1 L73+00F 41+50N	15	5.32	744	20	592	37	197	<20	<20	- 7	2.42
	S1 L73+00E 41+37.5N	11	4.73	776	15	399	82	165	<20	<20	5	2.57
	S1 L73+00F 41+25N	11	4.45	491	16	322	8(1	J4N	<28	<20	8	2.72
	S1 L75+80E 39+37.5N	12	5.38	667	18	579	51	191	<20	<20	5	2.91
	S1 L75+00F 39+25N	11	5.49	818	18	750	57	213	<20	<21	6	2.20
	S1 L75+00E 39+12.5N	13	5.20	351	20	248	54	183	<20	<28	5	2.15
	S1 L76+00F 38+75N	12	6.42	349	15	115	47	154	<20	<20	14	3.52
	S1 L76+00E 38+62.5N	11	4.99	1310	18	183	58	152	<20	<20	9	3.06
	S1 L76+00F 38+50N	11	6.83	1425	14	506	44	206	<20	<20	Э.	3.10
	S1 L76+00E 38+25N	12	6.57	442	19	169	47	195	<28	<20	5	2.98
	S1 L80+87.5F 39+75N	13	4.56	421	16	253	124	108	<20	<20	21	3.25
	S1 L80+87.5E 38+00N	16	6.13	301	18	113	74	97	<20	<20	2.2	3.66
1	S1 L81+00F 39+89.5N	<5	1.40	205	<10	24	9	28	<211	<28	26	0.50
	S1 L81+00E 39+75N A	6	1.48	1735	<10	174	43	35	<28	<20	7: 1	0.88
	S1 L81+DOF 39+75N B	12	4.14	1876	13	145	161	88	<20	<20	18	3.07
	S1 L81+DDE 39+62.5N	16	3.74	325	17	130	157	54	<20	<20	24	4.95
	S1 L81+DOF 38+12.5N	15	6.04	1797	1.3	32	65	63	<20	<20	38	3.69
• .	S1 L81+DDE 38+DON A	5	2.93	771	<10	58	47	86	<2()	<20	. 9	1.00
	S1 L81+00F 38+110N B	10	3.95	1108	10	133	102	122	<20	<20	12	3.22
	S1 L81+00E 37+89.5N	14	5.27	466	12	28	19	22	<21)	<20	41	4.80
	S1 L81+12.5F 39+75N	14	4.11	869	15	194	215	92	<20	<20	14	3.90
	S1 L81+12.5E 38+DAN	8	3.63	656	<10	36	7	8	<20	<20	45	4.27
	S1 L95+87.5F 45+50N	16	4.51	304	15	71	82	40	<20	<20	23	4.37
	S1 L96+DDE 45+62.5N	13	5.47	1472	15	33	240	111	<2D	<20	28	3.95
	S1 L96+00F 45+50N A	12	4.85	417	14	49	158	125	<20	<20	10	3.51
	S1 L96+0DE 45+50N B	<5	3.93	1187	<10	114	206	125	<20	<20	9	4.70
	S1 L96+D0F45+50N GRAVEL	<b>11</b>	4.19	1189	15	153	34	103	<20	<21	24	1.86
	S1 L96+00E 45+37.5N	23	5.10	895	24	165	366	157	<20	<28	14	4.50
	S1 L96+00F 43+110N A	<5	3.72	302	<10	17	18	42	23	<20	34	0.64
	S1 L96+DDE 43+DNN B	7	6.43	tont	<10	29	51	23	<20	<20	46	3.04
	S1 L96+00F43+IIIIN GRAVEL	9	3.66	952	01>	443	16	5	<28	<20	31	4.46
	S1 L96+12.5F 45+50N	12	6.25	1288	. 17	66	276	121	<28	<28	31	4.58

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### Geochemical Lab Report

	REPORT: V91-00770.0 ( C	OMPLETE )	ł				PROJECT: 8117 PAGE 1C	
	SAMPLE FI FMFNT NUMBER UNITS	. –	Ca PCT	Na PCT	K PCT	Sr PPN	Y PPN	
	S1 L70+80F 42+25N	N.61	0.08	0.02	0.23	10	8	
	S1 L70+00E 40+50N	8.47	<b>B.14</b>	0.03	0.16	16	16	
	S1 L70+00F 40+25N	0.74	0.36	0.04	0.17	44	<b>11</b>	
	S1 L70+00E 40+00N	0.37	0.16	0.03	0.89	21	10	•
	S1 L70+00F 39+75N	(1.82	0.20	0.03	0.39	19	28	
	S1 L70+00E 39+50N	Ŋ.18	<b>N.23</b>	0.04	0.10	9	25	
	S1 L73+00F 41+75N	0.07	0.03	0.66	0.09	2	30	
	S1 L73+DDE 41+62.5N	0.64	0.27	0.04	0.18	76	5	
	S1 L73+00F 41+50N	1.46	0.47	0.03	0.60	50	1940 <b>7</b> 1940 -	
	S1 L73+00E 41+37.5N	1.60	ก.48	0.03	0.80	55	4	
	S1 L73+00F 41+25N	1.22	N.46	0.03	0.53	64	5 al 1997 a	
	S1 L75+00E 39+37.5N	1.56	0.47	0.03	0.54	56	$[\mathbf{A}_{i}] = \mathbf{A}_{i}^{T}$ (1) and (	
	S1 L75+00F 39+25N	1.35	0.61	0.03	0.32	107	4	
	S1 L75+00E 39+12.5N	0.97	0.45	0.04	0.20	65	5 S	
	S1 L76+00F 38+75N	1.04	0.11	0.03	0.42	31	8	
	S1 L76+DDE 38+62.5N	1.47	0.34	0.03	0.73	41	8	
	S1 L76+00F 38+50N	1.88	0.46	0.02	1.10	32	5	
	S1 L76+00E 38+25N	0.77	0.10	0.02	0.23	13		
	S1 L80+87.5E 39+75N	1.49	0.11	0.03	0.49	13	19	
	S1 L80+87.5E 38+00N	0.89	0.22	0.04	0.31	12	12	
	S1 L81+00F 39+89.5N	8.05	0.05	0.02	0.06	8	5	
	S1 L81+00E 39+75N A	0.39	0.03 0.47	0.02	0.13	58		
	S1 L81+00E 39+75N B	1.26	0.47	0.06	0.30	20	<b>12</b>	
	S1 L81+00E 39+62.5N	1.23	0.13	0.05	0.45	7	12	
	S1 L81+00F 38+12.5N	0.34	0.13	0.03	0.45	5	16	
	S1 L81+00E 38+00N A	0.42	0.22	0.04	0.12	20		
	S1 L81+00F 38+00N B	1.30	0.31	0.03	0.39	22	10	
	S1 L81+DDE 37+89.5N	0.17	0.08	0.06	0.07	3	16 <b>16</b> - 17 - 18 - 18 - 18 - 18 - 18 - 18 - 18	
	S1 L81+12.5E 39+75N	1.75	0.20	0.04	0.52	13	1997) <b>14</b> Alexandra (1997) - Alexandra (19	
	S1 L81+12.5E 38+00N	0.09	0.05	0.06	0.11	2	17	
	S1 L95+87.5E 45+50N	0.26	0.04	0.07	0.87	2	12	
	S1 L96+DDE 45+62.5N	1.79	0.07	0.02	0.05	4	36	
	S1 L96+00F 45+50N A	1.73	0.08	0.03	0.04	9	<b>.</b>	
	S1 L96+DDE 45+50N B	2.70	N.15	N.N5	0.14	18	9	
	S1 L96+D0F45+5NN GRAVEL	0.91	0.25	8.02	8.15	18	25	
	S1 L96+00E 45+37.5N	3.15	0.21	0.02	0.13	13	13	
•	S1 L96+DDE 43+II(IN A	0.09	0.08	0.03	0.07	8	8	
1	S1 L96+00E 43+00N B	0.06	0.06	0.08	8.11	2	20	
	S1 L96+00E43+00N GRAVEL		0.07	0.16	0.15	6	18	
	S1 L96+12.5E 45+50N	1.83	0.13	0.03	0.07	10	10	

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## Geochemical Lab Report

		REPORT: 1	/91-00770.0 ( C	OMPLETE )		]				<del>te print</del> Oject: 8	FD: 10-JU 117	L-91	PAGE 2A	<u> </u>
		SAMPLE NUMBER	FI FINFNT UNITS	Au_1 Ng PPB	Ag PPN	Cu PPN	Pb PPN	Zn PPN	rio Ppn	Ni PPN	Co PPN	Cd PPH	Bi PPN	As PPit
إفديا		T1 64257		91	0.5	66	19	125	6	200	15	<1.0	<5	54
		T1 64259		254	0.4	72	18	105	5	191	17	<1.0	<5	63
- Halab		T1 64261		553	0.4	87	20	114	4	200	19	<1.8	<5	79
ألدينها		T1 64262		101	<8.2		19	128	4	157	24	<1.0	• <5	92
		T1 64263		6	1.8	295	24	134	4	277	7	3.4	<5	42
	· · · ·	R2 64075	<u> </u>	<5	<0.2	103	13	71	3	23	26	<1.0	<5	7
		R2 64076		<5	<0.2	112	15	96	5	40	26	<1.0	<5	31
		R2 64077		13	<8.2	301	5	43	2	18	13	<1.8	<5	12
		R2 64078		<5	<8.2	34	4	45	<1	2	4	<1.0	<5	7
	· · · · ·	R2 64079		19	<0.2	206	15	95	9	60	21	<1.0	<5	17
[limi]		R2 64080		<u>nt</u>	<0.2	279	15	62	23	75	17	<1.0	<5	36
l et a		R2 64081		118	0.7	1184	21)	93	3	40	27	<1.0	<5	18
		R2 64082		769	12.9	10290	7	50	··· 3	6	18	<1.0	<5	9
المتضا		R2 64083		43	<0.2	635	17	51	12	50	17	<1.0	<5	48
	.*.	R2 64084	· · · · · · · · · · · · · · · · · · · ·	<5	0.4	151	<2	3	<1	5	(1)	<1.0	<5	<5
		R2 64085		14	0.7	310	95	306	23	36	18	<1.0	ৎ	26
		R2 64252		<5	0.5	479	. 17	92	4	12	21	<1.0	<5	40
[		R2 64253		<5	<0.2	33	18	82	2	288	29	<1.0	<5	52
		R2 64254		<5	<8.2	9	. 4	6	1	9	1	<1.0	5	<5
لدفتنا		R2 64255		538	<0.2	14	22	138	3	141	17	<1.0	<5	41
1 (d) (d)		R2 64256		53	1.3	7	326	1176	3	5	4	8.1	<5	50
-		R2 64264	e de la constante de la constan La constante de la constante de	<u></u> <5	<0.2	138	13	52	6	168	20	<1.0	<5	19
		R2 64265		2178	2.8	143	17	15	1	14	7	0.1>	<5	25
		R2 64352		12	<0.2	51	11	45	6	127	15	<1.0	<5	27
luiste		R2 64353	ter an	<5	<0.2	92	17	82	9	184	24	<1.0	<5	36
التعديم 	t Sector	R2 64354		938	<0.2	91	8	46	<1	142	15	<1.0	<5	12
		R2 64355		28	<0.2	22	7	14	<b>11</b>	18	31	<1.0	<5	23
التغنيا	<sup>1</sup>	01 64258		225	<0.2	59	10	99	3	196	12	<1.8	<5	15
البيشا ا		01 64260		67	<0.2	49	nt	85	3	149	nt	<1.8	ৎ	37
					<u> </u>	<u> </u>	<u> </u>		<u> </u>					

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## Geochemical Lab Report

							TE-PRINTE	D: 10-JU	-91	· · · · · · · · · · · · · · · · · · ·		
	REPORT: V91-II	(1770.0 ( COMPLETE )					PR	OJFCT: 81	17	<u> </u>	PAGE 28	- '
	SAMPLE NUMBER	ELEMENT SD UNITS PPH	Fe PCT	iln PPH	Te PPN	Ba PPM	Cr PPN	V PPN	Sn PPN	H PPM	La PPN	AI PCT
<u>िल्लाम्</u>	T1 64257	13	3.68	1135	15	311	194	99	<20	<20	12	2.83
	<b>I1 64259</b>	13	3.65	1142	15	320	198	99	<20	<20	11	2.78
Cull	T1 64261	13	3.76	1970	16	328	228	105	<20	<20	9	2.87
ا سنا	T1 64262	9	3.26	1552	11	249	141	89	<28	<28	. 45	2.69
	T1 64263	99	1.06	2654	<1.0	320	67	48	<20	<20	104	1.09
	R2 64075	7	5.55	1555	<10	398	53	333	<20	<20	9	1.92
	R2 64076	t3	5.46	1364	19	1237	89	282	<20	<20	7	3.03
5.225	R2 64077	<5	2.01	549	<10	387	171	75	<20	<28	4	0.82
	R2 64078	<u>د</u>	1.04	743	<10	165	28	16	<20	<20	4	0.68
المن ا	R2 64079	6	5.21	1116	17	1762	123	270	<20	<20	6	3.05
	R2 64089	13	5.03	445	17	97	105	205	<20	<20	7	3.05
	R2 64081	8	6.50	239	<10	32	107	58	<20	<20	2	1.46
	R2 64082	6	3.80	299	<10	58	238	64	<20	<28	5	0.66
أهذف	R2 64083	13	4.26	968	19	498	172	255	<20	<20	13	3.62
চনৰ :	R2 64084	Ś	0.39	65	<10	Ĩ,	366	5	<20	<20	<1	0.04
	R2 64085	7	3.29	621	<10	189	114	144	<20	<20	13	1.37
Carrier -	R2 64252	13	4.41	933	19	613	43	160	<20	<20	7	2.56
- 47 J	R2 64253	13	4.70	663	13	153	496	169	<20	<20	4	3.96
	R2 64254	45 <5	0.38	81	<10	11	331	4	<20	<20	<1	0.05
	R2 64255	17	4.35	753	21	914	252	156	<20	<20	4	5.96
	R2 64256	t3	1.99	992	<10	194	66	16	<20	<20	9	1.03
ا لعب	R2 64264	8	2.89	291	12	399	230	91	<28	<20	5	2.07
	R2 64265	6	1.37	51	28	14	343	3	<20	<20	<1	0.02
<u></u>	R2 64352	6	3.90	458	11	550	257	1.70	<20	<20	5	3.39
and	R2 64353	18	3.96	398	19	4113	379	144	<20	<20	3	3.39
ر 	R2 64354	<\$.	2.96	1149	14	433	267	92	<20	<211	<1	3.45
	R2 64355	د5	2.54	373	<10	63	103	28	<20	<20	3	0.50
لفند	01 64258	Ś	3.02	1508	<10	338	157	86	<20	<20	12	2.51
	01 64260	<5	2.24	1660	<10	264	133	69	<20	<20	8	1.77

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	•		A DIVISIO	ON OF INCHC	CAPE INSPEC	CTION & TESI	TING SERVICES	Q=JUI -91
	REPORT: V91-	00770.0 ( COMPLETE )					PROJECT: 8117	PAGE 2C
	SAMPLE	ELEMENT Mg	Са	Na	K.	Sr	Y	
· .	NUMBER	UNITS PCT	PCT	PCT	PCT	PPN	PP1	
	T1 64257	1.95	1.02	0.05	0.74	43	13	
	T1 64259	2.01	1.03	0.05	0.83	42	11	
	T1 64261	2.16	0.97	0.04	0.86	41	<b>11</b>	
	T1 64262	1.21	0.95	0.04	0.38	36	40	
а • 1	T1 64263	0.40	2.85	8.03	0.14	95	144	
	R2 64075	1.39	4.39	0.09	1.50	143	8	
	R2 64076	2.03	2.93	0.08	2.44	335	8	
÷ .	R2 64077	0.51	1.27	0.09	0.60	68	4	
	R2 64078	0.15	0.60	0.06	0.43	19	5	
	R2 64079	1.81	2.23	0.10	2.38	88	8	
	R2 64080	1.75	0.57	8.15	2.13	52	8	
	R2 64081	0.47	0.14	0.08	0.87	14		
	R2 64082	0.35	0.18	0.05	0.54	19	3	
	R2 64083	2.46	0.75	0.16	2.52	67	8	
	R2 64084	N.(I)	0.02	t0.0	0.03	2	<1	
	R2 64085	1.01	1.19	0.08	0.52	41	11	
	R2 64252	1.74	2.47	0.09	1.77	162	8	
	R2 64253	4.83	2.50	0.03	0.31	109	8	
	R2 64254	0.(15	0.05	0.02	A.A3	4	<1	
	R2 64255	2.50	1.86	0.48	2.87	150	6	
	R2 64256		0.59	0.82	0.65	36	5	· · · · · · · · · · · · · · · · · · ·
	R2 64264	1.82	0.92	0.17	0.94	48	7	
	R2 64265	- 0.02	0.02	0.01	0.03	2	<1 €	
	R2 64352	2.86	0.44	0.11	2.41	40	9	
	R2 64353	2.75	0.60	<b>(1.23</b>	1.88	66	7	
	R2 64354	2.04	4.30	0.15	1.45	205	6	· · · · · · · · · · · · · · · · · · ·
	R2 64355	0.14	0.16	0.04	0.32	13	3	
	01 64258	1.52	1.55	0.04	0.65	58	12	
	01 64260	1.25	1.48	0.03	0.64	52	8	
							4	

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#### Geochemical Lab Report

ন্দ্	REPORT: V91-110770.0 ( CO	HPI FTF )			ant Standin Standard		1	DALE PRINI PROJECT: 8			PAGE 3A	l
	STANDARD ELEMENT NAME UNITS	Au_10g PPB	Ag PPM	Cu PPN	Pb PPM	Zn PPN	Ho PPN	Ni PPH	Co PPH	Cd PPff	Bi PPfi	As PPM
	HIGH GOLD STANDARD	1577	-			-		-	-			-
	Number of Analyses Nean Value	1 1577.0	-		-	-		-			-	
-ŋ	Standard Deviation			intentin La linita	_	- <u>-</u> -		2	_	- 		· _
	Accepted Value	ปรกก				-			-	-		
n 1	GEO TRACE STD 3 1989		0.6	269	39	252	4	72	10	<1.0	<5	37
a	Number of Analyses	-	1	1	1	1	1	1 72.0	1	• 1 0 50	1	1
	Nean Value Standard Deviation		0.58	269.2	39.1	251.5	3.6	72.u	10.1	0.50	2.5	36.8
	Accepted Value		0.5	290	33	255	4	42	9	().8	2	30
	ANALYTICAL BLANK	<5	<11.2	<1	.</td <td>ત</td> <td><t< td=""><td>4</td><td>4</td><td>&lt;1.0</td><td>&lt;5</td><td>&lt;</td></t<></td>	ત	<t< td=""><td>4</td><td>4</td><td>&lt;1.0</td><td>&lt;5</td><td>&lt;</td></t<>	4	4	<1.0	<5	<
1	ANALYTICAL BLANK	<5	<1.2	<1	<2	K)	<1	4	<1	<b>(1.</b> 0	<5	<5
	ANALYTICAL BLANK	<5	-	-		-	-	~	-	-	-	·
3	Number of Analyses Nean Value	3 2.5	2 በ.10	2 0.5	2 1.0	2 0.5	2 0.5	2 0,5	2 0.5	2 0.50	2 2.5	2 2.5
		<u></u>										0.00
	Standard Deviation Accepted Value	0.00 5	0.000	0.UA -	0.00	0.00	0.00	0.00	<b>0.</b> 00	0.000	0.00	0.00
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	GEO TRACE SID-2 1989		4.9	792	225	488	499	516	39	1.7	<5	333
, 	GEO TRACE SID-2 1989 Number of Analyses Nean Value		t	1	<b>t</b> -	1	1	516 1 515.6	1	t	1	333 1 333.4
	Number of Analyses						1. C.	1				1
	Number of Analyses Mean Value Standard Deviation		1 4.94 -	1 792.4 -	t 225.1 -	1 487.5 -	1 498.9 -	1 515.6 -	1 39.4 -	1 1.74 -	1 2.5 -	1 333.4 -
	Number of Analyses Mean Value Standard Deviation		1 4.94 -	1 792.4 -	t 225.1 -	1 487.5 -	1 498.9 -	1 515.6 -	1 39.4 -	1 1.74 -	1 2.5 -	1 333.4 -
	Number of Analyses Mean Value Standard Deviation		1 4.94 -	1 792.4 -	t 225.1 -	1 487.5 -	1 498.9 -	1 515.6 -	1 39.4 -	1 1.74 -	1 2.5 -	1 333.4 -
	Number of Analyses Mean Value Standard Deviation		1 4.94 -	1 792.4 -	t 225.1 -	1 487.5 -	1 498.9 -	1 515.6 -	1 39.4 -	1 1.74 -	1 2.5 -	1 333.4 -
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	Number of Analyses Mean Value Standard Deviation		1 4.94 -	1 792.4 -	t 225.1 -	1 487.5 -	1 498.9 -	1 515.6 -	1 39.4 -	1 1.74 -	1 2.5 -	1 333.4 -
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	Number of Analyses Mean Value Standard Deviation		1 4.94 -	1 792.4 -	t 225.1 -	1 487.5 -	1 498.9 -	1 515.6 -	1 39.4 -	1 1.74 -	1 2.5 -	1 333.4 -
	Number of Analyses Mean Value Standard Deviation		1 4.94 -	1 792.4 -	t 225.1 -	1 487.5 -	1 498.9 -	1 515.6 -	1 39.4 -	1 1.74 -	1 2.5 -	1 333.4 -
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### Geochemical Lab Report

	REPORT: V91-00770.0 ( CO	NPLETE )						NTE PRINTE ROJECT: 81			PAGE 3	3
	STANDARD ELEMENT NAME UNITS	S <del>d</del> PPM	Fe PCT	Mn PPN	Te PPN	Ba PPN	Cr PPN	V PP <b>n</b>	Sn PPN	H PPN	La PPN	AI PCT
<u> </u>	HIGH GOLD STANDARD Number of Analyses					-	-	-	-		-	
	flean Value	·	 _		-	_		-	-	-	-	
	Standard Deviation	_				-	-		-		• -	-
	Accepted Value	-						-			-	-
	GEO TRACE STD 3 1989	<\$	2.52	534	<10	67	89	10	<20	<29	4	0.73
	Number of Analyses	1	2 540	1	1 5.0	1 67.5	1 88,8	1 10.1	1 18.0	1 10.0	1 4.2	1 0.731
. N.	Nean Value Standard Deviation	2.5	2.518	534.1	5.0	- 10	00.0	10.1	-	-	4.2	<b>0.</b> /JI -
	Accepted Value	5	2.40	600	-	64	75	9	5	1	4	0.77
	ANALYTICAL BLANK	S	0.02	2	<18	<2	K)	(1	<20	<20 <20	<1 <1	<0.01 <0.01
	ANALYTICAL BLANK ANALYTICAL BLANK	<5	0.01	1	<10	<2	< <u>1</u>	<1	<21	<z8 -</z8 		- (0.01
	Number of Analyses	2	2	2	2	2	2	2	2	2	2	2
-	Mean Value	2.5	0.014	1.4	5.0	1.0	<b>0.5</b>	8.5	10.0	10.0	<b>a.</b> 5	0.005
	Standard Deviation	0.00	0.0019	0.50	0.00	0.00	0.00	0.00	0.01	0.00	0.00	0.0000
	Accepted Value	-	·	in a <b>⊆</b> in	- '	÷.,			·	<u> </u>	-	
									· . · ·			
· · ·	GEO TRACE STD-2 1989	52	3.90	698	18	248	155	38	<20	<20	6	4.64
	Number of Analyses	1	1	1	. 1	1	1	1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1	1	1
	Nean Value	51.9	3.905	697.6	17.7	247.9	155.1	37.9	10.0	10.0	6.4	4.643
	Standard Deviation Accepted Value	- 50	5.00	850		220	167	- 34	-16	- 8	. 6	5.10
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	REPORT: V91-00770.0 ( CO	MPLETE )						ATE PRINTED: 10-JUL-91 Roject: 8117	PAGE 3C
	STANDARD FI FMENT NAME UNITS	fig PCT	Ca PCT	Na PCT	K PCI	Sr PPN	Y PPH		
	HIGH GOLD STANDARD Number of Analyses				-		-		
	Nean Value Standard Deviation					in al s <del>e</del> n Sin <b>a</b> l	-		
	Accepted Value			-		-	_		
	GEO TRACE STD 3 1989	1.12	1.37	<b>N.</b> 05	0.14	41			
	Number of Analyses	1	1	1	1	1	1		
	Mean Value	1.120	1.366	0.054	0.142	40.2	3.6		· · · ·
	Standard Deviation	-		-	-	-	-		
	Accepted Value	1.34	1.66	0.04	0.14	39	4		
	ANALYTICAL BLANK	0.01	<0.81	0.01	<0.01	<1	<1		
	ANALYTICAL BLANK	0.01	<0.01	0.01	0.01	<1	<1		
	ANALYTICAL BLANK Number of Analyses	2	- 2	- 2	2	- 2	- 2		
÷.,	Nean Value	0.013	0.005	N.011	0.008	0.5	0.5		
м	0	0.004.0	0.0000	0 0000	0.00/2	0.00	0.00		· · · · · · · · · · · · · · · · · · ·
	Standard Deviation Accepted Value	0.0012	0.0000	0.0005	0.0043	0.00	0.00		•
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-	GEO TRACE STD-2 1989	3.81	3.28	8.30	0.19	81	5		
	Number of Analyses	1	1	1	1	1	1		
	Nean Value	3.807	3.281	0.296	0.188	81.2	5.2		
	Standard Deviation Accepted Value	4.90	5.13	0.30	0.20	78	- 6		· ·
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#### Geochemical Lab Report

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3	REPORT: V91-00770.0	( COMPLETE )	· · · · ·				PR	ROJECT: 811	.7		PAGE 4A	
		1FNT Au_1(lg NTTS PPB	Ag PPH	Cu PPN	Pb PPM	Zn PPH	tia PPN	Ni PPM	Co PPN	Cd PPN	Bi PPN	As PPN
	L70+00F 42+25N Duplicate	266 262	1.1 1.3	1120 1154	37 38	151 155	17 16	26 26	17 19	<1.0 <1.9	ব্য ব্য	51 48
]	L80+87.5E 39+75N Duplicate	<5	0.3 <0.2	59 59	19 14	87 89	4 3	62 62	12 12	<1.0 <1.0	• <5 <5	40 23
	L81+ODE 39+62.5N Duplicate	دی دع	0.2	30	24	72	6	98	10	(1.0	<5	. 52
1	L96+ODE 43+NNN B Duplicate	٢5	0.6 <0.2	19 18	36 32	112 118	11 9	6 5	2	<1.0 <1.0	<5 <5	27 15
	64076 Duplicate	دی دع	<0.2	112	15	96	5	40	26	<1.0	<5	31
1	64085 Duplicate	14	0.7 <0.2	31() 313	95 91	306 303	23 211	36 33	18 17	<1.0 <1.0	<5 <5	26 <5
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### Geochemical Lab Report

			A DIVIȘIC	ON OF INCHC	APE INSPECT	ION & TESTI			D:_10-JUL	01		
[]	REPORT: V91-00770.0 ( COM	PLETE )						OJECT: 81			AGE 48	
L					<u></u>		· · · · · · · · · · · · · · · · · · ·					
	SAMPLE FI FMENT	Sb	Fe	fin	Te	Ba	Cr	v t	Sn	H	La	A1
	NUMBER UNITS	PPN	PCT	PPN	PPH	PPN	PPM	PPM	PPN	PPM	PPH	PCT
Lesile .	L70+00E 42+25N	15	8.26	437	11	73	54	107	<20	<20	. 7	3.20
Sister Contract	Duplicate	12	8.66	451	13	74	56	110	<20	<20	7	3.31
۰ المتحيا	L80+87.5E 39+75N	13	4.56	421	16	253	124	108	<20	<20	. 21	3.25
	Duplicate	6	4.53	420	12	248	123	105	<20	<20	21	3.22
[	L81+00E 39+62.5N	16	3.74	325	17	130	157	54	<20	<20	24	4.95
(757)	Duplicate		3471	260		100	2.93	ЭТ	120	NEW .		1175
Caris			e e La sectoria						art. Arta arta			
असंहरण	L96+00E 43+11(IN B	7	6.43	1001	<10	29	51	23	<20	<20	46	3.04
	Duplicate	<5	6.40	1084	<10	33	52	23	<20	<20	51	3.27
L'isid	64076	13	5.46	1364	19	1237	89	282	<20	<20	7	3.03
(T.677)	Duplicate		5110	2.001		2207					•	0100
						- 1 - 19						
levaid	64085	7	3.29	621	<10	189	114	144	<20	<20	13	1.37
Lee	Duplicate	<5	3.18	647.	<10	203	112	149	<20	<20	13	1.40
Π	64255	17	4.35	753	21	914	252	156	<2(1	<2(1	4	5.96
Ndd-	Prep Duplicate	17	4.50	778	25	938	273	158	<20	<28	4	6.06
(15) M												
i initi	Prep Duplicate	17	4.50	778	25	938	273	158	<20	<28	4	6.06
L	Duplicate	<u></u>					<u> </u>					· · · · ·
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	REPORT: V91-00770.0	( COMP	LETE )						TE_PRINTED: 10-JUL- Oject: 8117	PAGE 4C
		MFNT INITS	Ng PCT	Ca PCT	Na PCT	K PCT	Sr PPH	Y PPN		
	L70+00E 42+25N Duplicate		(1.61 0.64	0.08 0.09	0.02 0.02	0.23 0.23	10 10	8 8		
1	L80+87.5E 39+75N Duplicate		1.49 1.48	0.11 0.11	0.03 0.03	0.49 0.49	13 13	19 19		
	L81+ODE 39+62.5N Duplicate		1.23	0.13	0.05	0.45	7	12		
• • •	L96+ODE 43+NNN B Duplicate		0.06 0.06	0.06 N.D6	0.08 0.08	0.11 0.12	2 2	20 22		
2 1	64076 Duplicate		2.(13	2.93	N_(18	2.44	335	8		
zi 	64085 Duplicate		1.01 0.95	1.19 1.22	0.(18 0.08	0.52 0.55	41 41	11 12		
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<b>1</b>	Prep Duplicate Duplicate	· · ·	2.56	1.89	0.48	2.96	150	6		
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		117711.6 ( COMPLETE )			PROJECT: 8117	PAGE 1
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	R2 64U82 R2 64255 R2 64265 R2 64354	0.030# 0.043# 0.037 0.137#				•
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	SAMPLE NUMBER	ELEMENT UNITS	A1203 PCT	Ca0 PCT	Fe203 PCT	K20 PCT	LOT PCT	Hg0 PCT	MnÖ PCT	Na20 PCT	P205 PCT	ST02 PCT	Tio2 PCT
177 177	R2 640864R D2 640704R D2 640714R D2 640714R D2 640724R D2 640734R		17.88 15.70 15.50 15.50 17.50	8.03 2.30 0.90 7.60 6.87	8.95 7.10 9.90 8.89 5.13	3.32 5.01 4.74 3.62 2.53	1.87 1.54 6.61 3.35 2.38	3.78 3.24 2.21 5.38 2.77	0.17 0.14 0.02 0.35 0.65	3.24 4.21 11.43 3.43 4.38	0.27 (1.22 0.21 (1.26 0.19	52.00 59.70 58.60 50.50 56.70	0.90 0.61 0.63 0.97 0.60
	D2 640744R		12.50	12.00	7.15	2.20	3.89	9.10	<b>0.24</b>	2.71	0.31	49.50	0.55
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	SAMPLE ELEMENT	Total Bad	) Cr203	S Tot	· .			
	NUMBER UNITS	PCT PCT	PCT	PCT				
E.KISS	R2 64086WR	99.33 0.097		0.02				
latie	D2 64070HR	99.77 0.164		1.45				
	D2 64071WR D2 64072WR	99.75 0.088 99.85 0.063		7.62 0.54				
- 7.P	D2 640724R	99.70 0.174		0.95				•
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	Sample Number	FLEMENT UNITS	A1203 PCT	Ca0 PCT	Fe203 PCT	K20 PCT	I OJ PCT	Ng0 PCT	Mn0 PCT	Na20 PCT	P205 PCT	SiO2 PCT	Ti02 PCT
	64071WR Duplicate		15.50	0.90	9.90	4.74	6.61	2.21	(1.(12	0.43	( <b>1.21</b>	58.60	0.63
	64074WR Duplicate		12.50	12.00	7.15	2.20	3.89	9.10	(1.24	2.71	(1.31	49.50	0.55
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R	EPORT: V91-00	789.N ( CO	MPLETE )					P	ROJECT: 811	1	PAGE	38	
	ample Iumber	FI FMENT UNITS	Total PCT	Ba0 PCT	Cr203 PCT	S Tot PCT							
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Bondar-Clegg & Company Ltd. 130 Pemberton Ave. North Vancouver, B.C. V7P 2R5 :'604) 985-0681 Telex 04-352667



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E IF	L70+00E 47+25N		2.27	0.52	0.02	1.39	20	5	
	Duplicate	<u>.</u>	2.30	0.54	0.02	1.41	21	6	
	L71+00E 48+00N	· · · · · · · · ·	1.18	0.16	0.03	0.47	10	7	
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	Duplicate		80.0	0.98	0.04	0.43	83	9	
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# APPENDIX B

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# **GEOPHYSICAL REPORT**

GEOPHYSICAL REPORT ISKUT JOINT VENTURE LIARD MINING DIVISION MAP SHEET 104 B 10

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PAUL W. JONES Prospector November 1991

#### SUMMARY

The geophysical assessment of the Gregor area on the Iskut Joint Venture Property, performed in June of 1991, showed that the volcanic Triassic hosted sulphides are discontinuous and disseminated to podiform. The HLEM survey detected a conductor that coincides with previous drill indicated mineralization. There were no continuous line conductors to indicate strike potential. The VLF survey did not detect the mineralized horizon but had a multi-line response that traced the volcanic\sediment contact south and below the Gregor stratigraphy. A previous magnetic survey, when correctly plotted to reflect actual position, shows a magnetic high corresponding to the outcropping of the mineralized tuff horizon. The geophysics outlined the known mineralization and did not indicate any subsurface extent to the zone.

#### INTRODUCTION

The Iskut Joint Venture Property was worked by a Corona exploration crew during June of 1991. Part of the property assessment included testing the Gregor Showing area with geophysical surveys to discovered in earlier determine whether the sulphide horizon, drilling could be detected and traced along strike. The drilled initially established principally by soil showings were mapping. After reviewing past geochemistry geological and geological, drilling, geochemical and geophysical data it was determined that the volcanic sulphide horizon had a NE\SW strike. All former grids were orientated in a north\south direction and to optimize the geophysical detection ability four grid lines were run at 155'azmuith. The work program was conducted from June 23rd-27th. The 12 mandays of work was performed by 4 people and included, grid installation (6 mandays), and the running of three geophysical surveys (6 mandays).

The three surveys included two electromagnetic and one magnetic survey. The electromagnetic surveys were a Horizontal Loop Electromagnetic (HLEM) Slingram Max-Min and a Very Low Frequency (VLF) survey. The magnetic survey data was lost during the dumping procedure, but a closely spaced magnetic survey had been completed over the Gregor area by S.J.V. Consultants for Delaware Resources in September 1988 and it covered a majority of the 1991 survey area.

The surveys were run on a 4 line reconnaissance grid. These lines were spaced 100 m apart with 25 m survey stations. The grid was centred on drill hole I90-10 with grid coordinates, Line 10+00 E, Station 10+00 N. The 4 lines were 9+00 E through 12+00 E, and extended from 8+50 N to 12+50 N. Extreme topography required that the grid be tight chained and slope corrected.

#### SURVEYS

The EM surveys produced 5 anomalies, of which one was a HLEM Maxmin response. The later occurred on line 10+00 E at 10+50 N and correlates with the drill detected sulphide stratigraphy. The remaining anomalies were VLF conductors and are located in 2 areas. The first zone includes 3 VLF anomalies which occur continuously from line 9 E through to 11 E, at 9+12.5 N, 9+25 N and 9+45 N respectively . This conductor axis parallels an interpreted volcanic\sediment contact. The final VLF conductor is situated at station 11+25 N on line 10+00 E, and as yet is unexplained.

The instrument used for the HLEM survey was an Apex Parametrics Ltd Maxmin II, 2 man portable horizontal loop system. The system is comprised of a transmitter(Tx) and receiver(Rx) connected by a reference cable. The instrument collects the vertical, in-phase and quadrature phase components of anomalous fields from electrically conductive zones. Interpretation of results is dependent on the Tx/Rx separation and frequency employed. Using various coil separations allows an interpretation of the depth and dip of the conductor, where optimal detection is 1/2 the coil separation. Knowing the approximate position of the mineralized horizon deemed the multi separation unnecessary. The effect of using various frequencies enables a measurement of the quality, ie conductivity of the anomaly and allows for the penetration through geologic noise when verifying anomalies. The HLEM Maxmin survey was run with a 100 m spacing and used three frequencies, 444 Hz, 1777 Hz and 3555 Hz.

The mineralized tuff layer was detected by drilling in 5 holes in the Gregor area.

The best mineralized intersect was in drill hole I90-10 at 20 metres depth. This intersect was 1 m of massive pyrrhotite/pyrite (ratio 4:1). The estimate of the conductivity of this mineralization is 4200 mhos.

The next best intersect was in drill hole I90-13 at 25 m depth. This included a narrow 5 cm, section of 35 % pyrrhotite/pyrite (ratio 8:1). The conductivity of this zone is estimated at 1750 mhos.

The other drill intersects are in:

190-12 at 17 m depth, 1 m of 10 % pyrrhotite/pyrite (ratio 2:1) conductivity estimate 400 mhos,

I90-11 at 53 m depth, 1/2 m of 10 % pyrrhotite/pyrite (ratio 3:1) conductivity estimate 400 mhos,

I90-14 at 15 m depth, 1/2 m of 20 % pyrrhotite/pyrite (ratio 2:1) conductivity estimate 733 mhos.

The horizontal volcanic horizon that hosts the mineralization is cut off to the south due to topography. The horizon is open geologically along the south-west\north-east strike direction and to the north-west. These are possible geologic exploration target areas. The Maxmin survey was set-up with a 100 m coil separation to detect conductors to a depth of 50 m. The reconnaissance grid was set up to explore the strike and geologic extent. The single response of the Maxmin survey in conjunction with the drill data implies that the mineralized horizon lacks continuity, is discontinuous and is disseminated to podiform. The horizon may continue along strike to the south-west as indicated by a weak, non-anomalous partial Maxmin response on line 9+00 E at 9+75 N. Topography in the south-west direction cuts off the stratigraphy.

The other EM survey incorporated a VLF method. The instrument used was a Geonics EM-16 VLF receiver. This receiver detects the primary (vertical) field component emitted from a designated source station. Conductors emanate their own electro-magnetic field which deflect the primary source field. The portable receiver detects the deviation of the primary field from the vertical which is measured as the dip-angle and indicates the presence of conductive bodies. The VLF method requires the use of a transmitting station along the direction of the strike of the conductor. Surface features, such as, conductive overburden and ground-water concentrations enhance the response of the high frequency source to conductors. This is an inherent weakness and can create false anomalies.

The VLF survey used Cutler, Maine, NAA 17.8 kHz, as a source. This station was chosen for its best fit for the determined east-northeast strike direction. The EM response detected by the VLF survey correlated with the volcanic/sedimentary contact south of the Gregor showing. The survey did not detect the mineralized horizon. A single station conductor on line 10+00 E at 11+25 N may be a structural feature that was detected in drill hole I90-11.

The detailed magnetic survey completed in 1988 is plotted as an orthogonal grid. This grid was resurveyed in 1990 and the extrapolated positions of the survey stations when re-plotted show a correlation between a continuous magnetic high and the outcropping of the mineralized tuff horizon. The presence of the feldspar porphyry stock to the south east also corresponds to a magnetic high.

#### CONCLUSIONS

The mineralization in the Gregor area was detected with the use of geophysical methods. These surveys confirm the disseminated to podiform and discontinuous nature of the volcanic hosted sulphides. No on strike or down dip conductors were found that would necessitate further exploration. No further geophysical work is recommended in the immediate Gregor showing area.

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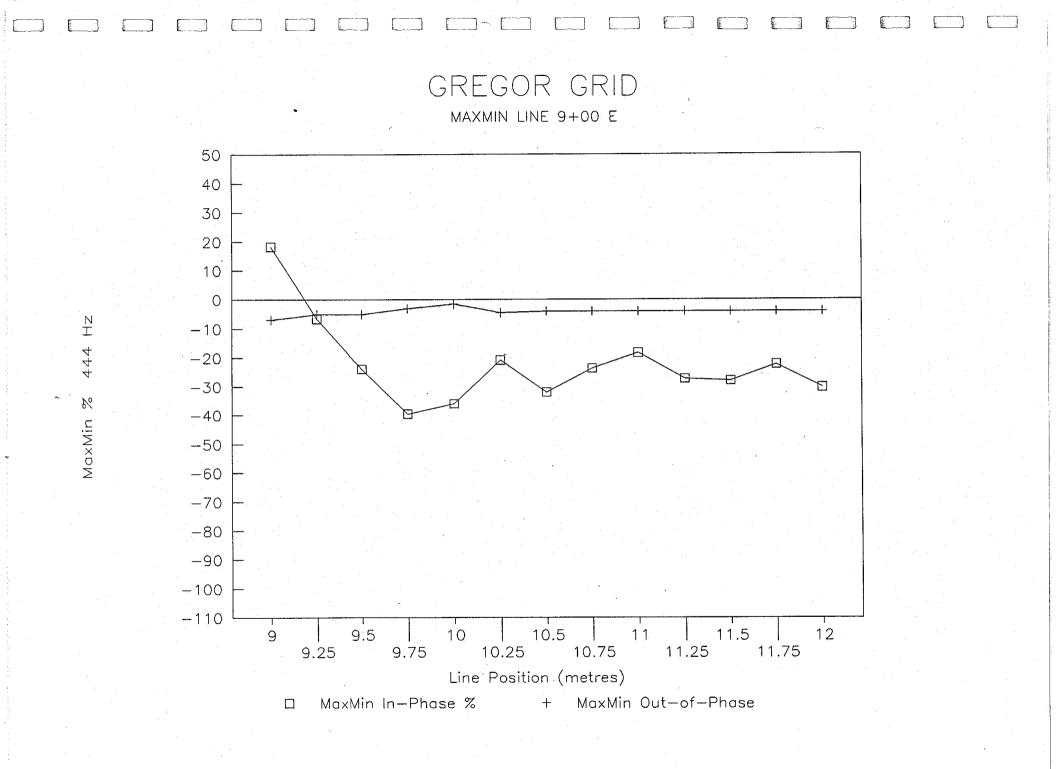
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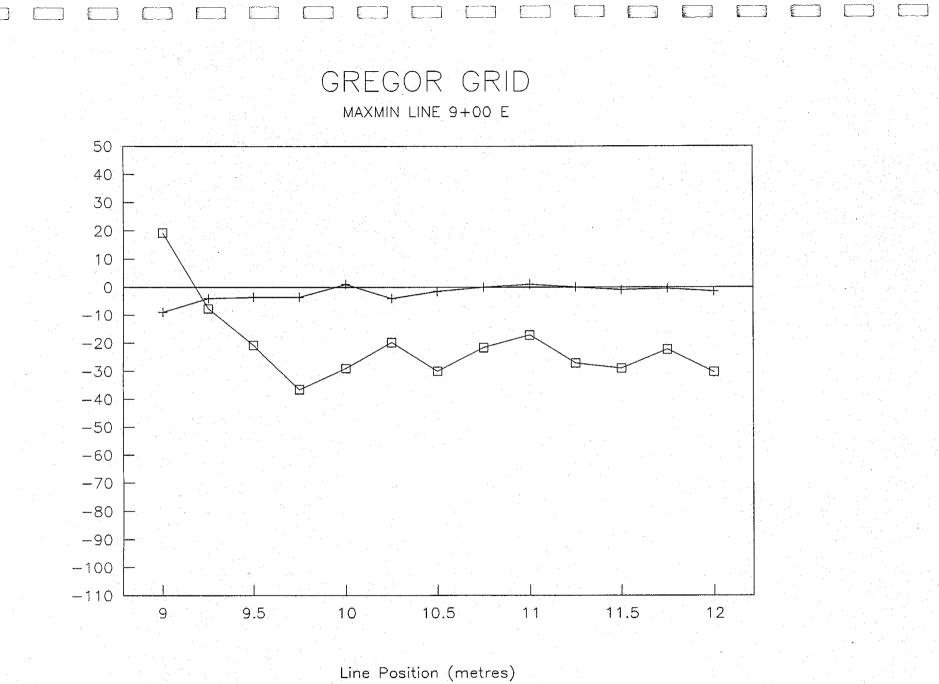
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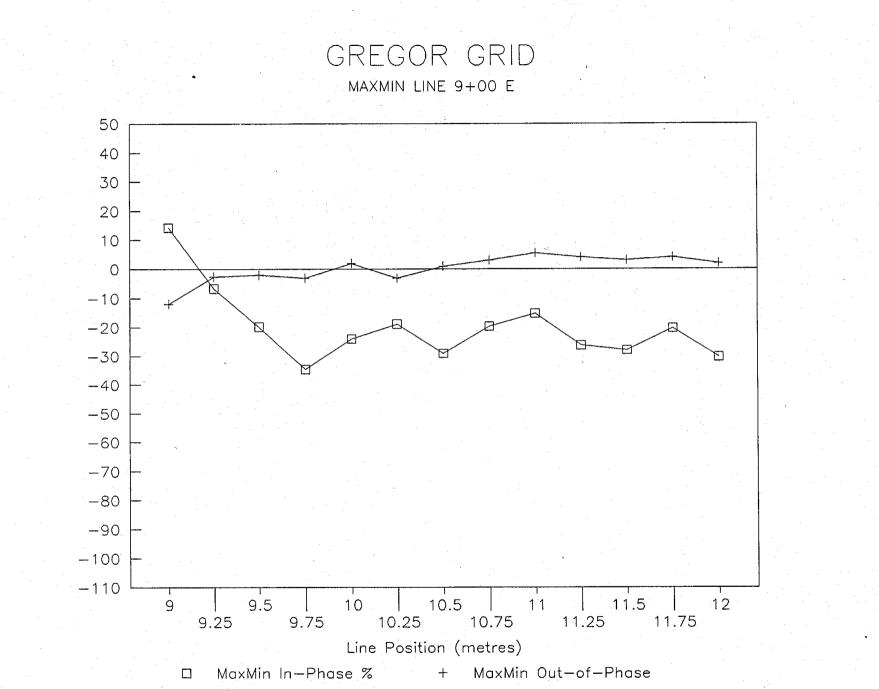
LINE POSITION NORTH		HORIZONTAL DISTANCE	CORRECTION FACTOR	MEASURED IN-PHASE 444 Hz	CORRECTED INPHASE 444 Hz	QUADRATURE	MEASURED INPHASE 1777 Hz	CORRECTED ( IN-PHASE 1777 Hz	DUADRATURE	MEASURED IN-PHASE 3555 Hz	CORRECTED ( IN-PHASE 3555 Hz	3555 Hz
LINE 9+00 E			÷.,									
					10010	-		19.240	9	-61	14.240	
9+00 N	52	112.7	75.240	-57	18.240	-7	-56 -69	(7.673)	-4	-68	(6.673)	-2
9+25 N	42	108.5	61.327	-68	(6.673)	-5				-50	(19.801)	· · · · ·
9+50 N	25	103.1	30,199	-54		-5	-51	(20.801)				
9+75 N	13	100.8	9.424	-49		-3	-46	(36.576)	-3.5	-44	(34.576)	
10+00 N	1	100	0.045	-36	(35.955)	-1.5	-29	(28.955)	1	-24	(23.955)	
10+25 N	6	100.2	2.190	-23	(20.810)	-4.5	-22	(19.810)	- <b>4</b> ,	-21	(18.810)	· -
10+50 N	4	100.1	1,013	-33	(31.987)	-4	-31	(29.967)	-1.5	-30	(28.987)	
10+75 N	. 5	100.1	1.413	-25	(23.587)	-4	-23	(21.587)	0	-21	(19.587)	
11+00 N	10	100.5	5.785	-24	(18.215)	-4	-23	(17.215)	1	21	(15.215)	· . E
11+25 N	10	100.5	5.785	-33		-4	-33	(27.215)	0	-32	(26.215)	
11+50 N	4	100.1	1.013	-29	(27.987)	-4	-30	(28.967)	-1	-29	(27,987)	
11+75N	. 9	100.4	4.704	-27	(22.296)	-4	27	(22.295)	-0.5	-25	(20.296)	
12+00 N	8	100.3	3.695	34		-4	-34	(30.305)	-1.5	-34	(30.305)	
LINE			CORRECTION	MEASURED	CORRECTED	QUADRATURE		CORRECTED	QUADRATURE		CORRECTED	UADRATU
POSITION N	DISTANCE	DISTANCE X	FACTOR	IN-PHASE 444 Hz	IN-PHASE 444 Hz	444 Hz	IN-PHASE 1777 Hz	IN-PHASE	1777 Hz	IN-PHASE 3555 Hz	IN-PHASE 3555 Hz	3555 Hz
NE 10+00 E	· · ·						andar dari Ari					
9+00 N	18	101.6	17.280	-55	(37.720)	-3.5	-53	(35.720)	0	-51 87	(33.720) (14.217)	. ·
9+25 N	- 50	111.8	72.783	-78		-7	-82		-8			. –
9+50 N	39	107.3	56.325	82		-15	-85		-10	-95	(38.675)	
9+75 N	37	106.6	52.848	62		7.5	-64	(11.152)	-14	-73	(20.152)	-
10+00 N	36	106.3	51.096	-56			-53		-11	-58	(6.904)	-
10+25 N	12	100.7	8.148	41	(32.852)	-11	-51	(42.852)	-25	-67	(58.852)	-
10+50 N	7	100.2	2.759	-62	(59.241)	-24	-74	(71.241)	-12	off scale	n/r	
10+75 N	13	100.8	9.424	~39	(29.576)	-6	-37	(27.576)	0	-34	(24.576)	
11+00 N	. 17	101.4	15.538	-36		-3	-34	(18.462)	. 1.5	-32	(16.462)	
11+25 N	2	100	0.180			6	-34		-1	-32	(31.820)	
11+50 N	8	100.3	3.695	-31	(27.305)	-5	29		-2	-28	(24.305)	
	1	100	0.045	36		- <b>4</b>	-36		-2	31	(30.955)	
11+75N									-3.	-44	(43.820)	· · · · · · · · · · · · · · · · · · ·
11+75N 12+00N	2	100	0.160	-43	(42.820)	-5	-43	(42.820)			(10.020)	
12+00N LINE POSITION	2 VERTICAL DISTANCE	HORIZONTAL DISTANCE	0.160 CORRECTION FACTOR	MEASURED IN-PHASE	CORRECTED	QUADRATURE	MEASURED IN-PHASE	CORRECTED	QUADRATURE	MEASURED IN-PHASE	CORRECTED ( IN-PHASE	QUADRATU
12+00 N LINE POSITION N	2 VERTICAL DISTANCE Z	HORIZONTAL	CORRECTION	MEASURED	CORRECTED		MEASURED	CORRECTED		MEASURED	CORRECTED	
12+00 N LINE POSITION N	2 VERTICAL DISTANCE Z	HORIZONTAL DISTANCE X	CORRECTION FACTOR	MEASURED IN-PHASE 444 Hz	CORRECTED IN-PHASE 444 Hz	QUADRATURE 444 Hz	MEASURED IN-PHASE 1777 Hz	CORRECTED N-PHASE 1777 Hz	QUADRATURE 1777 Hz	MEASURED IN-PHASE 3555 Hz	CORRECTED ( IN-PHASE 3555 Hz	QUADRATU 3555 Hz
12+00 N LINE POSITION N INE 11+00 E 9+00 N	2 VERTICAL DISTANCE Z	HORIZONTAL DISTANCE X 100.5	CORRECTION FACTOR	MEASURED IN-PHASE 444 Hz -49	CORRECTED N-PHASE 444 Hz (43.215)	QUADRATURE 444 Hz -4.5	MEASURED IN-PHASE 1777 Hz -48	CORRECTED N-PHASE 1777 Hz (42.215)	QUADRATURE 1777 Hz 2	MEASURED IN-PHASE 3555 Hz -47	CORRECTED ( IN-PHASE 3555 Hz (41.215)	QUADRATL 3555 Hz
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N	2 VERTICAL DISTANCE z 10 39	HORIZONTAL DISTANCE X 100.5 107.3	CORRECTION FACTOR 5,785 56.325	MEASURED N-PHASE 444 Hz -49 -64	CORRECTED N-PHASE 444 Hz (43.215) (7.675)	QUADRATURE 444 Hz -4.5 -4	MEASURED IN-PHASE 1777 Hz -48 -63	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.675)	QUADRATURE 1777 Hz 2 -1	MEASURED N-PHASE 3555 Hz -47 -63	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675)	QUADRATU 3555 Hz
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N	2 VERTICAL DISTANCE Z 10 39 49	HORIZONTAL DISTANCE X 100.5 107.3 111.4	CORRECTION FACTOR 5.785 56.325 71.502	MEASURED IN-PHASE 444 Hz -49 -64 -71	CORRECTED IN-PHASE 444 Hz (43.215) (7.675) 0.502	QUADRATURE 444 Hz -4.5 -4 -3	MEASURED IN-PHASE 1777 Hz -48 -63 -69	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502	QUADRATURE 1777 Hz 2 -1 2	MEASURED IN-PHASE 3555 Hz -47 -63 -71	CORRECTED ( IN-PHASE 3555 Hz (41.215) (6.675) 0.502	QUADRATU 3555 Hz
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N	2 VERTICAL DISTANCE z 10 39 49 34	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6	CORRECTION FACTOR 5.785 56.825 71.502 47.397	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48	CORRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603)	QUADRATURE 444 Hz -4.5 -4 -3 -4 -4	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397	QUADRATURE 1777 Hz -2 -1 2 0	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39	CORRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397	QUADRATU 3555 Hz
12+00 N LINE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N	2 VERTICAL DISTANCE Z 10 39 49 34 18	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48 -25	CORRECTED ( IN-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720)	QUADRATURE 444 Hz -4.5 -4 -3 -4 -3 -4 -3 -4 -3 -4 -6	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720)	QUADRATURE 1777 Hz 2 1 2 0 2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720)	QUADRATU 3555 Hz
12+00 N LINE POSITION N INE 11+00 E 9+00 N 9+25 N 9+55 N	2 VERTICAL DISTANCE z 10 39 49 34	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6	CORRECTION FACTOR 5.785 56.825 71.502 47.397	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48	CORRECTED ( IN-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720)	QUADRATURE 444 Hz -4.5 -4 -3 -4 -3 -4 -3 -4 -3 -4 -6	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720)	QUADRATURE 1777 Hz -2 -1 2 0	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610)	QUADRATI 3555 Hz
12+00 N LINE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+00 N	2 VERTICAL DISTANCE Z 10 39 49 34 18	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48 -25	CORRECTED ( IN-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720)	QUADRATURE 444 Hz -45 -4 -3 -4 -4 -6 -2 -4 -4 -4	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -4	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720)	QUADRATURE 1777 Hz 2 -1 2 0 2 1.5 2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -8 1	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190	3555 Hz
12+00 N POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+25 N	2 VERTICAL DISTANCE Z 10 39 49 34 18 6 6	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 101.6 100.2	CORRECTION FACTOR 5,785 56.325 71.502 47.397 17.280 2.190	MEASURED N-PHASE 444 Hz -49 -64 -71 -71 -48 -25 -15	CORRECTED ( N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.220) (12.810) (4.810)	QUADRATURE 444 Hz -45 -4 -3 -4 -4 -6 -2 -4 -4	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.510)	QUADRATURE 1777 Hz -2 -1 2 0 -2 15	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -8	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610)	QUADRATI 3555 Hz
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+50 N 9+50 N 10+25 N 10+25 N 10+75 N	2 VERTICAL DISTANCE Z 10 39 49 49 34 18 6 6	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 100.2 100.2	CORRECTION FACTOR 5.785 56.825 71.502 47.397 17.280 2.190 2.190	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -7	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.810) (4.241)	CUADRATURE 444 Hz -45 -4 -3 -4 -6 -2 -4 -6 -2 -4 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -4	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (1.810) (1.1241)	QUADRATURE 1777 Hz 2 -1 2 0 2 1.5 2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -8 1	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190	2UADRATL 3555 Hz
12+00 N POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+50 N 9+50 N 10+25 N 10+50 N 10+75 N 10+75 N 10+75 N	2 VERTICAL DISTANCE Z 10 39 49 34 16 6 6 6 7 7	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280 2.190 2.190 2.199 2.759 2.759	MEASURED IN-PHASE 444 Hz -49 -64 -71 -71 -48 -25 -15 -7 -15 -7 -15 -7 -19	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (12.241) (16.241)	QUADRATURE 444 Hz -4.5 -4 -3 -4 -3 -4 -6 -2 -4 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -69 -40 -22 -12 -12 -14 -14 -18.5	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.997 (4.720) (9.810) (1.810) (1.1241) (15.741)	QUADRATURE 1777 Hz 2 -1 2 0 -2 1.5 2 2 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -8 1 -12 -17	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241)	SUADRATL 3555 Hz
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N 9+75 N 10+00 N 10+75 N 10+75 N 10+75 N 10+75 N 11+00 N	2 VERTICAL DISTANCE Z 10 39 49 34 18 6 6 7 7 7 7 5	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280 2.190 2.190 2.759 1.413	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -15 -19 -24	CORRECTED ( N-PHASE 444 Hz (43.215) (7.675) 0.552 (0.603) (7.220) (12.810) (12.241) (16.241) (16.241) (22.587)	QUADRATURE 444 Hz -45 -4 -4 -4 -6 -2 -4 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -18 5 -22	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.875) 2.502 7.397 (4.720) (9.810) (1.541) (15.741) (20.587)	2 -7777 Hz 2 -1 2 0 -2 1,5 2 -2 -25 -2 -25 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -8 1 -12 -17 -12 -17 -20	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (15.557)	QUADRATI 3555 Hz
12+00 N LINE POSITION N NE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+00 N 10+25 N 10+50 N 10+75 N 11+50 N	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 6 7 7 7 5 5	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.1	CORRECTION FACTOR 5.765 56.325 71.502 47.397 17.280 2.190 2.190 2.759 2.759 1.413 1.413	MEASURED N-PHASE 444 Hz -49 -64 -71 -71 -48 -25 -15 -15 -15 -19 -24 -25	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (12.810) (12.241) (12.241) (16.241) (22.587) (23.597)	CUADRATURE 444 Hz -4.5 -4 -3 -4 -3 -4 -6 -2 -4 -5 -5 -5 -5 -5 -4	MEASURED N-PHASE 1777 Hz -48 -69 -40 -22 -12 -4 -14 -185 -22 -23	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.367 (4.720) (9.810) (1.1241) (1.541) (20.587) (21.587)	-2 -2 -1 2 0 -2 1.5 2 -2 -2 -2 -2 -2.5 -25 -25 -25 -3.5	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -8 1 -12 -17	CORRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (18.587) (19.587)	3555 H
12+00 N LINE POSITION N NE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+50 N 10+50 N 10+50 N 11+20 N	2 VERTICAL DISTANCE Z 10 39 49 34 18 6 6 7 7 7 7 5	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280 2.190 2.190 2.759 1.413	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -15 -19 -24	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.241) (16.241) (16.241) (16.241) (22.587) (20.562)	QUADRATURE 444 Hz -4.5 -3 -3 -4 -3 -3 -3 -4 -5 -5 -5 -5 -5 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -18 5 -22	CORRECTED N−PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (1.840) (1.1241) (1.5741) (21.587) (20.652)	2 -7777 Hz 2 -1 2 0 -2 1,5 2 -2 -25 -2 -25 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -6 1 1 -12 -17 -20 -21	CORRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (14.241) (19.567) (17.652)	2UADRATT 35555 Ha
12+00 N POSITION N INE 11+00 E 9+00 N 9+50 N 9+50 N 9+50 N 10+25 N 10+25 N 10+25 N 10+25 N 10+75 N 11+50 N 11+75 N	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 6 6 7 7 7 5 5 12 19	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.1 100.1 100.1	CORRECTION FACTOR 5,785 56,325 71,502 47,397 17,280 2,190 2,190 2,190 2,190 2,190 2,199 2,759 1,413 1,413 1,413 1,413 8,148	MEASURED N-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -15 -15 -15 -19 -24 -29 -29 -32 -29 -32	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (12.241) (16.241) (16.241) (16.241) (16.241) (22.567) (20.852) (12.950) CORRECTED	CUADRATURE 444 Hz -4.5 -4 -3 -4 -6 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -185 -22 -23 -29 -32 -29 -32 -29 -32	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.610) (11241) (11241) (20.587) (20.852) (12.950) CORRECTED		MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -71 -8 1 -12 -17 -20 -21 -26 -32 -32 MEASURED	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (15.857) (17.852) (12.650) CORRECTED (	2UADRATU 3555 Hz 
12+00 N LINE POSITION N NET1+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+50 N 10+50 N 10+50 N 11+25 N 11+25 N 11+25 N 11+25 N 11+25 N 11+20 N	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 6 6 7 7 5 5 12 19 19 VERTICAL	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.1 100.1 100.1	CORRECTION FACTOR 5.765 56.325 71.502 47.397 17.280 2.190 2.759 2.759 2.759 1.413 1.413 8.148 19.050	MEASURED IN-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -15 -15 -15 -19 -24 -25 -29 -32	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.810) (12.241) (12.241) (12.241) (12.241) (22.587) (23.557) (20.552) (12.950)	CUADRATURE 444 Hz -4.5 -4 -3 -4 -6 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -14 -185 -22 -23 -29 -32	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (11.241) (11.241) (20.587) (21.557) (21.557) (21.557) (21.550)		MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -6 1 1 -12 -17 -20 -21 -26 -32	CORRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (14.241) (14.2567) (17.652) (12.950)	2UADRATT 3555 Hz 
12+00 N LINE POSITION N 9+00 N 9+25 N 9+50 N 9+75 N 10+25 N 10+25 N 10+25 N 10+25 N 11+20 N 11+25 N 11+20 N 11+25	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 6 7 7 5 5 12 19 19 VERTICAL DISTANCE z	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.1 100.1 100.1 100.1 HORIZONTAL DISTANCE	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280 2.190 2.190 2.190 2.190 2.759 1.413 1.413 1.413 8.148 19.050	MEASURED IN-PHASE 444 Hz -49 -64 -49 -64 -71 -48 -25 -15 -17 -15 -7 -15 -7 -15 -7 -19 -24 -25 -29 -32 -32 MEASURED IN-PHASE	CONRECTED N-PHASE 444 Hz (43.215) (7.675) 0.562 (0.603) (7.720) (12.2410) (4.810) (12.2411) (16.2411) (16.2411) (22.587) (20.552) (12.950) (12.950)	QUADRATURE 444 Hz -4.5 -3 -4 -3 -3 -4 -6 -2 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -69 -40 -22 -12 -14 -14 -185 -22 -23 -23 -29 -32 -32 MEASURED IN-PHASE	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (1.840) (1.1241) (1.5741) (20.587) (20.652) (12.950) CORRECTED ( N-PHASE	QUADRATURE 1777 Hz 2 -1 -1 -2 -2 -1 5 -2 -2 -2 -2 -2 -2 -2 -3 -5 -3 -5 -3 -5 -3 -5 -3 -5 -3 -5 -3 -5 -3 -5 -3 -5 -3 -3 -3 -3 -3 -3 -3 -3 -3 -3	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -12 -17 -12 -17 -20 -21 -26 -32 -32 MEASURED IN-PHASE	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (14.241) (14.241) (17.652) (12.950) CORRECTED ( N-PHASE	2UADRATT 3655 Ha 
12+00 N LINE POSITION N 1400 E 9+00 N 9+25 N 9+25 N 9+25 N 9+75 N 10+25 N 10+25 N 10+25 N 10+25 N 10+25 N 11+20 N 11+25 N	2 VERTICAL DISTANCE Z 10 39 49 34 18 6 6 7 7 5 5 5 12 19 19 VERTICAL DISTANCE Z	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.1 100.1 100.1 100.7 101.8 HORIZONTAL DISTANCE X	CORRECTION FACTOR 5,785 56,325 71,502 47,397 1,7280 2,190 2,759 2,759 1,413 3,1413 6,148 19,050 2,663 2,675	MEASURED N-PHASE 444 Hz -49 -64 -49 -64 -49 -64 -71 -48 -25 -15 -15 -15 -19 -24 -25 -29 -32 MEASURED N-PHASE 444 Hz	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (12.241) (16.241) (16.241) (16.241) (22.567) (20.852) (12.950) (20.852) (12.950) N-PHASE 444 Hz	QUADRATURE 444 Hz -4.5 -3 -3 -3 -4 -6 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -69 -40 -22 -12 -14 -14 -14 -14 -14 -14 -14 -14 -14 -14	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.610) (11241) (15.741) (20.587) (20.852) (12.950) CORRECTED N-PHASE 1777 Hz (5.211)	QUADRATURE 1777 Hz -2 -1 2 -2 -1 2 -2 -2 -2 -2 -2 -3.5 -3.5 -3.5 QUADRATURE 1777 Hz	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -71 -8 1 -12 -71 -8 1 -12 -71 -8 -32 -21 -22 -21 -26 -32 -32 MEASURED IN-PHASE 3555 Hz -76	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (14.241) (15.67) (9.241) (14.241) (15.67) (17.652) (12.650) N-PHASE 3555 Hz (7.211)	2UADRATT 3555 Hz 
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+75 N 10+75 N 10+75 N 10+75 N 11+25 N 11+50 N 11+25 N 11+50 N 11+25 N I1+50 N I1+	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 7 7 5 5 5 12 19 19 VERTICAL DISTANCE z 47 55	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 107.3 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.4 HORIZONTAL DISTANCE x 110.5 114.1	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280 2.190 2.190 2.759 2.759 2.759 1.413 1.413 1.413 8.148 19.050 CORRECTION FACTOR	MEASURED N-PHASE 444 Hz -49 -64 -71 -64 -71 -52 -15 -15 -19 -24 -25 -29 -32 MEASURED N-PHASE 444 Hz	COHRECTED N-PHASE (43.215) (7.675) 0.502 (0.603) (7.20) (12.810) (4.610) (12.241) (16.241) (16.241) (16.241) (16.241) (22.587) (23.587) (20.652) (12.550) N-PHASE 444 Hz	CULADRATURE 444 Hz -45 -4 -4 -3 -4 -6 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -14 -18 5 -22 -23 -29 -32 -32 -32 -32 -32 -32 -32 -32 -32 -32	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (11.241) (11.241) (20.557) (21.587) (20.552) (12.950) N-PHASE 1777 Hz (5.211) 2.626	QUADRATURE 1777 Hz 2 -1 2 -2 -2 -2 -2 -2 -2 -2 -3.5 	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -6 -12 -12 -12 -17 -20 -21 -21 -26 -32 -32 N-PHASE 3555 Hz -766 -76 -76	CORRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (14.241) (14.257) (17.652) (12.650) N-PHASE 3555 Hz (7.211) 2.626	2UADRATL 3555 Hz 
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+50 N 10+50 N 10+50 N 11+25 N 11+50 N 11+75 N 11+75 N 11+75 N 11+75 N 11+75 N 11+75 N 11+75 N 11+25 N 11+20 N 11+25 N 11+	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 6 6 6 7 7 7 5 5 12 19 19 VERTICAL DISTANCE z 47 55 29	HORIZONTAL DISTANCE X 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.1 100.1 100.1 100.1 100.1 100.5 10	CORRECTION FACTOR 5.785 56.325 71.502 47.397 1.7280 2.190 2.190 2.190 2.759 2.759 1.413 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 3.7678	MEASURED N-PHASE 444 Hz -49 -64 -71 -71 -71 -75 -15 -15 -7 -15 -19 -24 -25 -29 -32 -38 MEASURED N-PHASE 444 Hz -27 -31 -38	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (12.810) (12.810) (12.810) (12.810) (12.810) (12.810) (12.810) (12.810) (12.810) (12.810) (12.857) (20.852) (12.950) (1	QUADRATURE 444 Hz -4.5 -4 -3 -4 -3 -4 -5 -5 -4 -5 -5 -4 -5 -5 -4 -5 -5 -4 -5 -5 -4 -5 -5 -4 -5 -4 -5 -4 -5 -4 -5 -4 -5 -4 -5 -4 -5 -4 -5 -4 -5 -5 -4 -5 -5 -5 -4 -5 -4 -5 -5 -5 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED N-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -4 -14 -185 -22 -23 -29 -32 -32 -29 -32 -29 -32 -4 -14 -14 -185 -22 -23 -29 -32 -32 -32 -4 -77 Hz	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) (6.675) 2.502 7.397 (4.720) (9.810) (1.810) (1.1241) (20.587) (20.552) (12.950) CORRECTED N-PHASE 1777 Hz (5.211) 2.626 (36.122)	QUADRATURE 1777 Hz -2 -1 2 0 -2 1.5 2 -2.5 -2.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -2.5 -2.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -2.5 -3.5 -2 -2 -2 -2 -2 -2 -2 -2 -3.5 -3.5 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -71 -8 1 -12 -17 -20 -21 -26 -32 -21 -26 -32 MEASURED IN-PHASE 3555 Hz -76 -76 -76 -76	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (14.241) (14.241) (15.657) (12.950) CORRECTED ( N-PHASE 3555 Hz (7.211) 2.626 (36.122)	2UADRATL 3555 Hz 
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12+00 N LINE POSITION N NE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+25 N 10+25 N 10+25 N 10+25 N 11+25 N 11+	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 7 7 7 5 5 5 12 19 19 VERTICAL DISTANCE z 47 55 29 23 13	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.5 100.2 100.5 100.5 100.5 100.5 110.5 114.1 102.6 100.6 100.6 100.5 110.5 114.1 102.6 100.5 10.5 10.5 10.5 10.5 10.5 10.5 10.	CORRECTION FACTOR 5.785 56.325 71.502 47.397 1.7280 2.190 2.759 2.759 2.759 2.759 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.678 26.325 9.424	MEASURED N-PHASE 444 Hz -49 -64 -64 -71 -48 -25 -15 -15 -19 -24 -25 -29 -32 MEASURED N-PHASE 444 Hz	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.810) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (23.567) (20.652) (12.550) N-PHASE 444 Hz 41.789 47.626 (0.122) (2.675) (14.576) (12.577) (12.	CUUDRATURE 444 Hz -45 -4 -5 -5 -5 -5 -5 -5 -5 -5 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -185 -22 -23 -29 -32 -32 -32 -74 N-PHASE 1777 Hz	CORRECTED ( N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (11.241) (11.241) (20.587) (21.587) (20.582) (12.950) N-PHASE 1777 Hz (5.211) 2.626 (36.122) (12.675) (28.576)	QUADRATURE 1777 Hz -2 -1 2 -2 -2 -2 -2 -2 -2 -2 -2 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -71 -8 1 -12 -17 -20 -21 -26 -32 -71 -28 -32 -76 -32 N-PHASE 3555 Hz -76 -76 -74 -39 -37	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (14.241) (14.241) (14.587) (17.652) (17.652) (12.650) N-PHASE 3555 Hz (7.211) 2.626 (36.122) (12.675) (27.576)	2UADRATT 3555 Hz 
12+00 N LINE POSITION N 9+00 N 9+25 N 9+25 N 9+75 N 10+25 N 10+25 N 10+25 N 11+25 N 11+25 N 11+25 N 11+25 N 11+25 N 12+00 N N N N N N N N 9+25 N 9+75 N 12+00 N 9+75 N 9+75 N 9+75 N 9+75 N 9+75 N 9+75 N 9+75 N 9+75 N 12+00 N 9+75 N 12+00 N 9+75 N 12+00 N 11+25 N 12+00 N 11+25 N 12+00 N 9+75 N 12+00 N 9+75 N 12+00 N 9+75 N 12+00 N 9+75 N 12+00 N 9+75 N 10+25 N 10	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 7 7 7 5 5 12 19 19 VERTICAL DISTANCE z 47 55 29 23 13	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.5 100.5 100.5 100.5 114.1 10	CORRECTION FACTOR 5.785 56.325 71.502 47.397 1.7280 2.190 2.190 2.190 2.759 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.878 26.325 9.424 12.390	MEASURED N-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -15 -15 -15 -19 -24 -29 -29 -32 -29 -32 -29 -32 -29 -32 -29 -32 -29 -32 -21 -31 -31 -31 -38 -29 -24 -44 -27 -31 -31 -38 -29 -24 -36 -29 -24 -24 -24 -27 -31 -36 -29 -24 -24 -24 -27 -31 -36 -29 -24 -24 -27 -27 -31 -27 -27 -31 -27 -27 -31 -27 -27 -27 -27 -27 -27 -27 -27 -27 -27	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.810) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.257) CORRECTED N-PHASE 444 Hz 41.789 47.626 (0.122) (2.675) (14.576) (12.577) (14.576) (15.576) (15.576) (15.576) (15	QUADRATURE 444 Hz -4.5 -4 -3 -4 -3 -4 -5 -5 -5 -5 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED N-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -4 -14 -185 -22 -23 -29 -32 MEASURED N-PHASE 1777 Hz -74 -74 -74 -74 -74 -74 -74 -74	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) (2.502 7.397 (4.720) (9.810) (1.810) (1.810) (1.241) (20.557) (20.552) (20.552) (12.557) (20.552) (12.557) (20.552) (12.557) (2.5211) 2.652 1777 Hz (5.211) 2.652 (3.612) (3.610) (3.610)	QUADRATURE 1777 Hz -2 -1 2 0 -2 1.5 2 -2.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -2.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -3.5 -2.5 -3.5 -4 -2 -2 -3.5 -4 -4 -4 -4 -4 -4 -4 -4 -4 -4	MEASURED IN -PHASE 3555 Hz -47 -63 -555 Hz -47 -63 -71 -39 -21 -71 -8 -12 -17 -20 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -26 -26 -26 -26 -26 -26 -26 -26 -26	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (14.241) (14.241) (15.87) (12.950) CORRECTED ( N-PHASE 3555 Hz (7.211) 2.626 (36.122) (12.675) (27.576) (32.610) (32.610) (32.610)	2UADRATT 3555 Hz 
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+75 N 10+50 N 10+75 N 11+25 N 11+20 N 11+25 N 11+25 N 11+20 N 11+25 N 11+25 N 11+20 N 11+25 N 11+20 N 11+25 N 11+20 N 11+25 N 11+20 N 11+25 N 11+20 N 11+25 N 11+25 N 11+20 N 11+25 N 11+20 N 11+25 N 11+	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 7 7 7 5 5 5 12 19 19 VERTICAL DISTANCE z 47 55 29 23 13	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.5 100.2 100.5 100.5 100.5 100.5 110.5 114.1 102.6 100.6 100.6 100.5 110.5 114.1 102.6 100.5 10.5 10.5 10.5 10.5 10.5 10.5 10.	CORRECTION FACTOR 5.785 56.325 71.502 47.397 1.7280 2.190 2.759 2.759 2.759 2.759 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.678 26.325 9.424	MEASURED N-PHASE 444 Hz -49 -64 -64 -71 -48 -25 -15 -15 -19 -24 -25 -29 -32 MEASURED N-PHASE 444 Hz	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.810) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.257) CORRECTED N-PHASE 444 Hz 41.789 47.626 (0.122) (2.675) (14.576) (12.577) (14.576) (15.576) (15.576) (15.576) (15	QUADRATURE 444 Hz -4.5 -4 -3 -4 -5 -5 -5 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -185 -22 -23 -29 -32 -32 -32 -74 N-PHASE 1777 Hz	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) (2.502 7.397 (4.720) (9.810) (1.810) (1.810) (1.241) (20.557) (20.552) (20.552) (12.557) (20.552) (12.557) (20.552) (12.557) (2.5211) 2.652 1777 Hz (5.211) 2.652 (3.612) (3.610) (3.610)	QUADRATURE 1777 Hz -2 -1 2 -2 -2 -2 -2 -2 -2 -2 -2 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -71 -8 1 -12 -17 -20 -21 -26 -32 -71 -28 -32 -76 -32 N-PHASE 3555 Hz -76 -76 -74 -39 -37	CORRECTED ( N-PHASE 3555 Hz (41:215) (6:675) 0:502 8:397 (3:720) (5:610) 3:190 (9:241) (14:241) (14:241) (15:557) (17:552) (12:950) CORRECTED ( N-PHASE 3555 Hz (7:211) 2:626 (36:122) (12:675) (27:576) (32:610) (	2UADRATT 3555 Hz 
12+00 N LINE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+50 N 10+50 N 11+25 N 11+50 N 11+25 N 11+50 N N N N N N E 12+00 N 9+25 N 9+50 N 9+55 N 9+50 N 9+55 N 9+50 N 9+55 N 9+50 N 9+55 N 9+50 N 9+55 N 10+00 N N N N N N N N N N N N N N	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 7 7 7 5 5 12 19 19 VERTICAL DISTANCE z 47 55 29 23 13	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.1 100.1 100.1 100.7 101.8 HORIZONTAL DISTANCE x 110.5 114.1 104.1 104.1 105.1 114.1 105.1 114.1 105.1 114.1 105.1 114.1 105.1 114.1 105.1 114.1 105.1 114.1 105.1 107.3 107.2 100.7 101.8 10.1 10.5 114.1 105.6 101.6 10.6 10.6 10.6 10.6 10.7 10.1 10.7 10.1 10.5 114.1 10.5 114.1 100.5 1000	CORRECTION FACTOR 5.785 56.325 71.502 47.397 1.7280 2.190 2.190 2.190 2.190 2.759 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.878 26.325 9.424 12.390 17.280	MEASURED N-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -15 -15 -15 -19 -24 -29 -29 -32 -29 -32 -29 -32 -29 -32 -29 -32 -29 -32 -21 -31 -31 -31 -38 -29 -24 -44 -27 -31 -31 -38 -29 -24 -36 -29 -24 -24 -24 -27 -31 -36 -29 -24 -24 -24 -27 -31 -36 -29 -24 -24 -27 -27 -31 -27 -27 -31 -27 -27 -31 -27 -27 -27 -27 -27 -27 -27 -27 -27 -27	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.241) (16.241) (12.241) (16.241) (23.597) (20.852) (12.550) N-PHASE 444 Hz 41.789 47.626 (0.122) (2.675) (14.576) (23.610) (2	QUADRATURE 444 Hz -4.5 -4 -3 -3 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED N-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -4 -14 -185 -22 -23 -29 -32 MEASURED N-PHASE 1777 Hz -74 -74 -74 -74 -74 -74 -74 -74	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (11.241) (15.741) (20.857) (20.852) (20.852) (12.950) N-PHASE 1777 Hz (5.211) 2.656 (36.122) (12.675) (28.576) (28.576) (31.610) (16.720) (16.720)	QUADRATURE 1777 Hz -2 -1 2 0 -2 1.5 2 -2.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -2.5 -3.5 -3.5 -2.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -2.5 -3.5 -3.5 -3.5 -3.5 -2.5 -3.5 -4 -2 -2 -3.5 -4 -4 -4 -4 -4 -4 -4 -4 -4 -4	MEASURED IN -PHASE 3555 Hz -47 -63 -555 Hz -47 -63 -71 -39 -21 -71 -8 -12 -17 -20 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -26 -26 -26 -26 -26 -26 -26 -26 -26	CORRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (14.241) (18.587) (17.652) (12.650) N-PHASE 3555 Hz (7.211) 2.656 (36.122) (12.675) (27.576) (32.610) (16.720) (17.720) (16.720) (16.720) (16.720) (16.720) (16.720) (16.720) (16.720) (16.720) (16.720) (16.720) (16.720) (16.720) (17.72	2UADRATT 3555 Hz 
12+00 N UNE POSITION N INE 11+00 E 9+00 N 9+25 N 9+55 N 9+55 N 9+75 N 10+50 N 10+50 N 10+50 N 11+25 N 11+50 N 11+25 N 11+50 N 11+25 N 11+50 N 11+25 N 11+25 N 11+25 N 11+25 N 11+25 N 11+25 N 11+25 N 11+25 N 11+25 N 11+20 N 11+25 N 9+00 N 10+25 N 1	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 7 7 7 5 5 5 12 19 19 19 19 19 19 19 19 20 31 5 5 29 23 31 15 18 8 29 23 31 5 5 8 8 29 23 31 25 29 23 31 25 29 23 31 25 29 23 31 25 29 23 31 25 29 23 31 25 29 23 31 25 29 22 31 20 20 39 49 34 20 39 49 34 34 49 34 49 34 49 34 34 34 34 34 34 34 34 34 34 34 34 34	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.5 100.2 100.5 100.2 100.5 100.2 100.5 10	CORRECTION FACTOR 5.785 56.325 71.502 47.397 1.7280 2.190 2.759 2.759 1.413 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.678 26.325 9.424 12.390 17.280 0.180	MEASURED N-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -15 -19 -24 -25 -29 -32 MEASURED N-PHASE 444 Hz -27 -31 -38 -29 -36 -36 -36 -36 -36 -36 -46 -46 -46 -46 -46 -46 -46 -4	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.810) (12.241) (12.241) (12.241) (12.241) (22.587) (23.557) (23.557) (23.557) (23.557) (23.557) (14.576) (12.577) (12.5	CUADRATURE 444 Hz -4.5 -4 -6 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -14 -14 -185 -22 -23 -29 -32 -32 -32 -32 -74 N-PHASE 1777 Hz	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (11.241) (20.587) (20.552) (12.950) CORRECTED N-PHASE 1777 Hz (5.211) 2.626 (36.122) (12.657) (28.576) (28.576) (31.610) (35.620) (35.620)	QUADRATURE 1777 Hz -2 -1 2 -2 -2 -2 -25 -25 -25 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -2.5 -3.5 -	MEASURED IN-PHASE 3555 Hz 3555 Hz 3555 Hz -47 -63 -71 -39 -21 -71 -20 -21 -21 -26 -32 -76 -32 IN-PHASE 3555 Hz -766 -76 -74 -39 -33	COHRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (14.241) (14.241) (14.567) (17.652) (17.652) (12.650) N-PHASE 3555 Hz (7.211) 2.626 (36.122) (12.7576) (32.610) (16.720) (32.620)	2UADRATT 3555 Hz 
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12+00 N LINE POSITION N INE 11+00 E 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+50 N 10+50 N 11+25 N 11+50 N 11+25 N 11+75 N 11+75 N 11+75 N 11+75 N 11+75 N N ILINE POSITION N INE 12+00 E 9+50 N 9+55 N 9+55 N 9+55 N 9+55 N 9+55 N 10+00 N 10+75 N 10+00 N 10+75 N 10+00 N 10+25 N	2 VERTICAL DISTANCE Z 10 39 49 34 18 6 6 7 7 5 5 5 5 12 19 VERTICAL DISTANCE Z 47 55 29 23 31 15 18 22 22 2 2 2 2 2 2 2	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 107.3 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.5 10	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280 2.190 2.190 2.759 2.759 2.759 2.759 1.413 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.878 26.325 9.424 12.390 17.280 0.180 0.180 0.180 0.180	MEASURED N-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -19 -24 -25 -29 -32 MEASURED M-PHASE 444 Hz -27 -31 -38 -28 -29 -32 -32 -44 -44 -45 -49 -25 -15 -15 -15 -15 -15 -15 -15 -29 -32 -29 -32 -32 -44 -44 -44 -25 -15 -15 -15 -15 -15 -29 -32 -32 -32 -44 -44 -44 -25 -25 -29 -32 -32 -44 -44 -45 -25 -29 -32 -32 -44 -44 -45 -25 -29 -32 -32 -44 -44 -45 -25 -29 -32 -44 -44 -45 -25 -29 -32 -32 -32 -34 -44 -44 -45 -44 -44 -25 -29 -32 -32 -44 -44 -44 -45 -44 -44 -45 -44 -44	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.610) (12.241) (16.241) (16.241) (16.241) (12.2507) (23.597) (23.597) (23.597) (23.597) (23.597) (23.597) (24.597) (14.576) (14.	CULADRATURE 444 Hz -45 -4 -4 -6 -5 -5 -5 -5 -5 -5 -5 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -69 -40 -22 -12 -4 -14 -14 -14 -185 -22 -23 -23 -29 -32 -29 -29 -29 -29 -29 -29 -29 -29 -29 -2	CORRECTED N−PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (11.241) (15.741) (20.587) (20.652) (12.950) N−PHASE 1777 Hz (5.211) 2.656 (36.122) (12.675) (28.576) (28.576) (28.576) (26.8276) (26.820) (20.820)	QUADRATURE 1777 Hz -2 -1 2 -2 -2 -5 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -71 -8 1 -12 -8 1 -12 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -27 -27 -27 -27 -27 -27 -27 -27 -27 -27	CONRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (14.241) (18.587) (17.652) (12.650) N-PHASE 3555 Hz (7.211) 2.656 (36.122) (12.675) (27.576) (32.610) (19.62	2UADRATI 3555 Hz 
12+00 N LINE POSITION N INE 11+00 E 9+00 N 9+25 N 9+55 N 9+55 N 9+75 N 10+50 N 10+50 N 10+50 N 11+25 N 11+25 N 11+25 N I1+25 N I1+25 N N E 12+00 E 9+00 N 9+50 N 9+50 N 9+50 N 9+50 N 9+50 N 9+50 N 10+75 N 10+25 N 11+20 N 10+25 N 10+25 N 10+25 N 11+20 N 11+20 N 10+25 N 10+25 N 10+25 N 11+20 N 10+25 N 11+20 N 11+20 N 10+25 N 10+20 N 10+25 N 11+20 N 11+20 N 10+25 N 11+20 N 11+25 N 11+20 N 11+25 N 10+25 N 10+25 N 10+25 N 10+25 N 10+25 N 10+25 N 10+25 N 10+25 N 11+25	2 VERTICAL DISTANCE z 10 39 49 34 18 6 6 6 7 7 7 5 5 5 12 19 19 VERTICAL DISTANCE z 47 55 5 12 19 19 23 3 15 18 8 2 2 12 19 23 19 10	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 101.6 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.5 100.2 100.2 100.5 100.2 100.5 100.5 100.5 100.5 100.2 100.2 100.2 100.5 10	CORRECTION FACTOR 5.765 56.325 71.502 47.397 1.7280 2.190 2.190 2.759 2.759 2.759 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.878 26.325 9.424 12.390 17.280 0.180 0.180 0.180 0.180 0.180 0.180 0.180	MEASURED N-PHASE 444 Hz -49 -64 -71 -71 -48 -25 -15 -15 -15 -19 -24 -25 -29 -32 -31 -31 -31 -31 -31 -31 -31 -33 -32 -31 -33 -31 -33 -31 -33 -39 -29 -24 -31 -31 -33 -39 -29 -24 -31 -31 -33 -39 -29 -24 -29 -29 -29 -29 -29 -29 -29 -29 -29 -29	COHRECTED N-PHASE 444 Hz (43.215) (7.675) 0.502 (0.603) (7.720) (12.810) (4.810) (12.241) (12.241) (12.241) (12.241) (22.567) (22.557) (23.557) (23.557) (23.557) (23.557) (14.576) (15.520) (15.5	QUADRATURE 444 Hz -4.5 -4 -6 -6 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED N-PHASE 1777 Hz -48 -63 -69 -40 -22 -12 -4 -14 -185 -22 -23 -29 -32 -32 -29 -32 	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (1.810) (1.1241) (20.587) (20.552) (12.950) N-PHASE 1777 Hz (5.211) 2.626 (36.122) (12.657) (20.5520) (20.552) (20.5520) (31.610) (31.610) (35.820) (20.8522) (11.550) (31.610) (35.820) (31.610) (35.820) (31.610) (35.820) (30.6522) (11.550) (31.610) (31.610) (31.610) (31.610) (31.610) (31.610) (31.610) (31.610) (31.610) (31.610) (31.620) (31.610)	QUADRATURE 1777 Hz -2 -1 2 0 -2 15 2 -2 -25 -25 -25 -25 -3.5 -3.5 -3.5 -3.5 -3.5 -3.5 -25 -25 -25 -25 -25 -25 -25 -2	MEASURED IN-PHASE 3555 Hz 3555 Hz -47 -63 -71 -39 -21 -71 -20 -21 -20 -21 -26 -32 -76 -76 -76 -76 -76 -76 -76 -76 -76 -76	CORRECTED N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.810) 3.190 (9.241) (14.241) (14.241) (14.241) (14.241) (14.247) (12.650) (12.650) N-PHASE 3555 Hz (7.211) 2.626 (36.122) (12.675) (27.576) (32.610) (32.620) (19.822) (19.852) (19.852) (19.852) (19.852) (19.852) (19.852) (19.852) (19.852)	2UADRATT 3555 Hz 
12+00 N LINE POSITION N 9+00 N 9+25 N 9+50 N 9+75 N 10+50 N 10+50 N 10+50 N 11+25 N 11+50 N 11+25 N 11+75 N 11+75 N 11+75 N 11+75 N N N N N N N N N N N N N N	2 VERTICAL DISTANCE Z 10 39 49 34 18 6 6 7 7 5 5 5 5 12 19 VERTICAL DISTANCE Z 47 55 29 23 31 15 18 22 22 2 2 2 2 2 2 2	HORIZONTAL DISTANCE x 100.5 107.3 111.4 105.6 107.3 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.2 100.5 10	CORRECTION FACTOR 5.785 56.325 71.502 47.397 17.280 2.190 2.190 2.759 2.759 2.759 2.759 1.413 1.413 1.413 8.148 19.050 CORRECTION FACTOR 68.789 78.626 37.878 26.325 9.424 12.390 17.280 0.180 0.180 0.180 0.180	MEASURED N-PHASE 444 Hz -49 -64 -71 -48 -25 -15 -19 -24 -25 -29 -32 MEASURED M-PHASE 444 Hz -27 -31 -38 -28 -29 -32 -32 -44 -44 -45 -49 -25 -15 -15 -15 -15 -15 -15 -15 -29 -32 -29 -32 -32 -44 -44 -44 -25 -15 -15 -15 -15 -15 -29 -32 -32 -32 -44 -44 -44 -25 -25 -29 -32 -32 -44 -44 -45 -25 -29 -32 -32 -44 -44 -45 -25 -29 -32 -32 -44 -44 -45 -25 -29 -32 -44 -44 -45 -25 -29 -32 -32 -32 -34 -44 -44 -45 -44 -44 -25 -29 -32 -32 -44 -44 -44 -45 -44 -44 -45 -44 -44	COHRECTED N-PHASE 444 Hz (43.215) 0.502 (0.603) (7.720) (12.810) (4.810) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (12.241) (22.557) (20.552) (12.557) (20.552) (23.610) (14.576) (23.610) (23.620) (32.652) (32.6520) (32.	QUADRATURE 444 Hz -4.5 -4 -4 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5	MEASURED IN-PHASE 1777 Hz -48 -69 -40 -22 -12 -4 -14 -14 -14 -185 -22 -23 -23 -29 -32 -29 -29 -29 -29 -29 -29 -29 -29 -29 -2	CORRECTED N-PHASE 1777 Hz (42.215) (6.675) 2.502 7.397 (4.720) (9.810) (1.810) (1.810) (1.241) (20.557) (20.522) (12.950) CORRECTED N-PHASE 1777 Hz (5.211) 2.652 (3.6122) (3.610) (3.620) (3.620) (3.620) (20.622) (20.622) (20.620) (20.620) (20.620) (20.620) (20.620) (20.620) (20.620) (3.620)	QUADRATURE 1777 Hz -2 -1 2 -2 -2 -5 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2	MEASURED IN-PHASE 3555 Hz -47 -63 -71 -39 -21 -71 -8 1 -12 -8 1 -12 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -26 -32 -21 -27 -27 -27 -27 -27 -27 -27 -27 -27 -27	CORRECTED ( N-PHASE 3555 Hz (41.215) (6.675) 0.502 8.397 (3.720) (5.610) 3.190 (9.241) (14.241) (15.557) (17.652) (12.950) CORRECTED ( N-PHASE 3555 Hz (7.211) 2.626 (36.122) (12.675) (27.576) (32.620) (19.622) (19.622) (19.622) (19.620) (28.596) (28.596)	2UADRATI 3555 Hz 





□ MaxMin In-Phase % + MaxMin Out-of-Phase

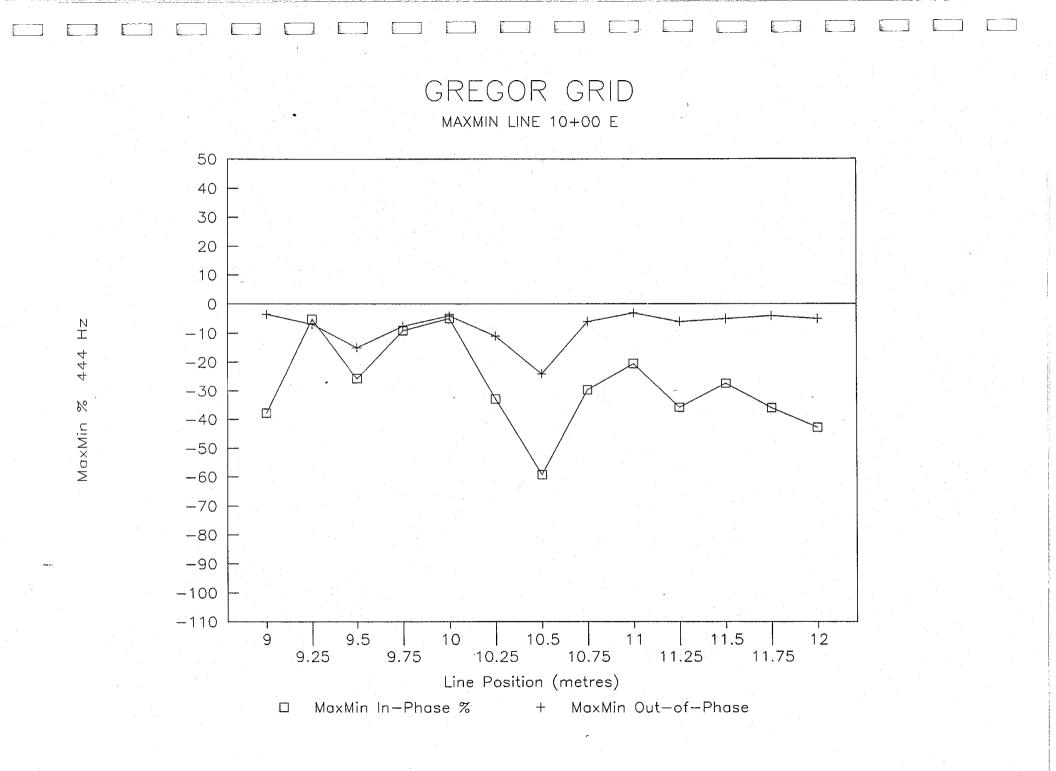
Ma×Min % 1777 Hz

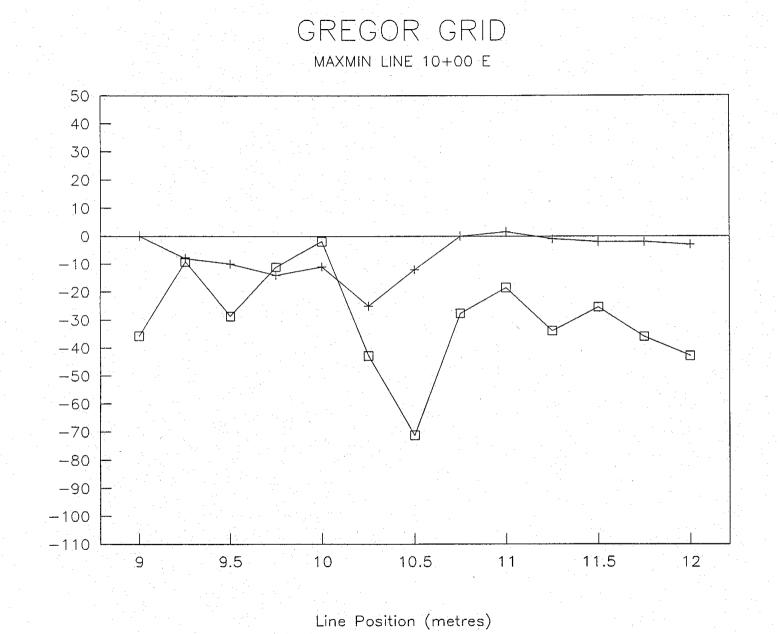


3555 %

N T

Ma×Min

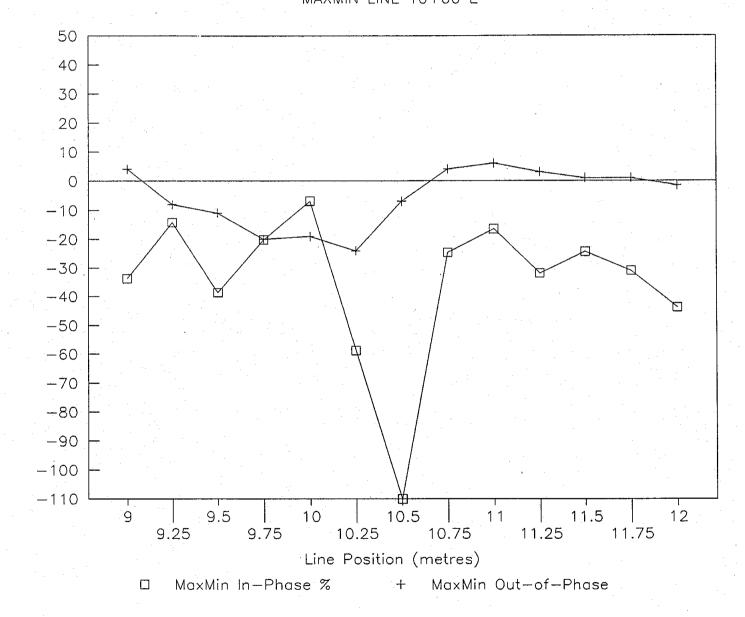




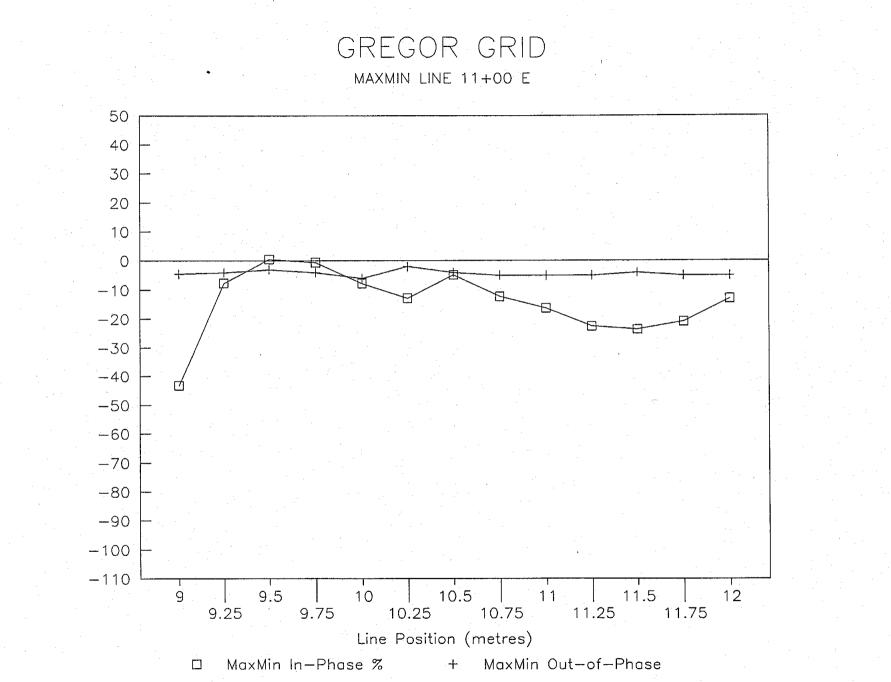
□ MaxMin In-Phase % + MaxMin Out-of-Phase

MaxMin % 1777 Hz

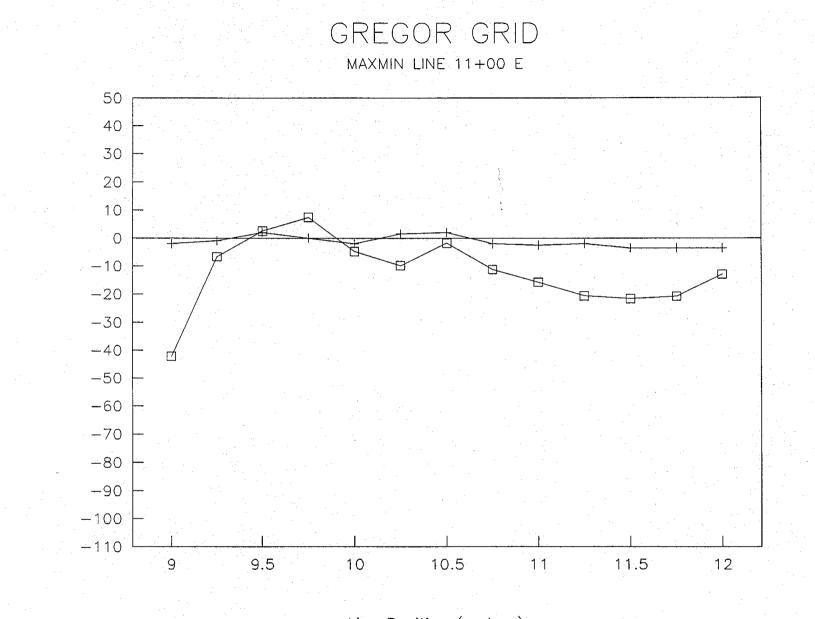
GREGOR GRID MAXMIN LINE 10+00 E



MaxMin % 3555 Hz



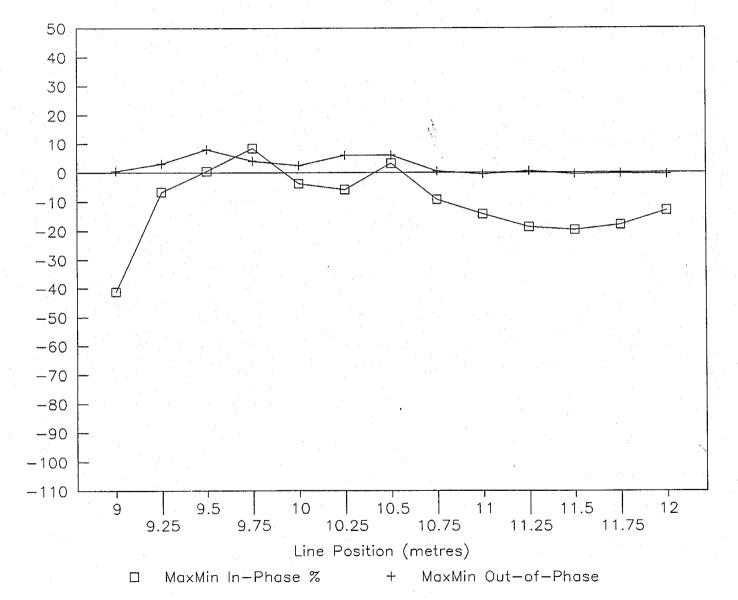
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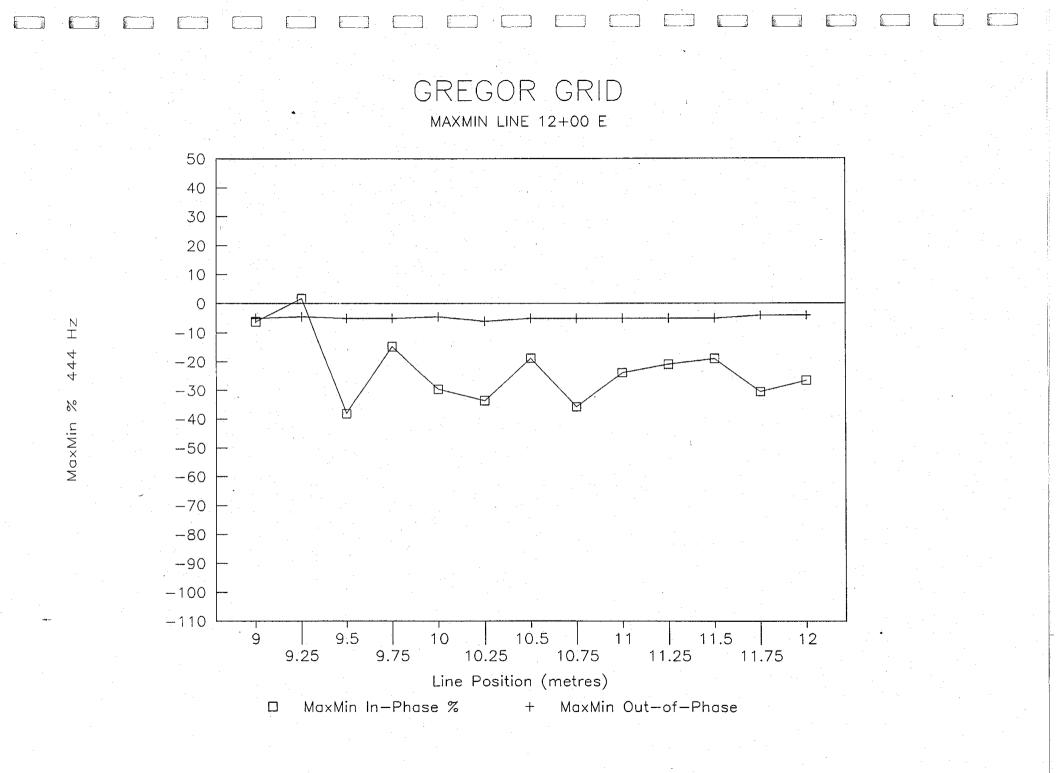
Line Position (metres)

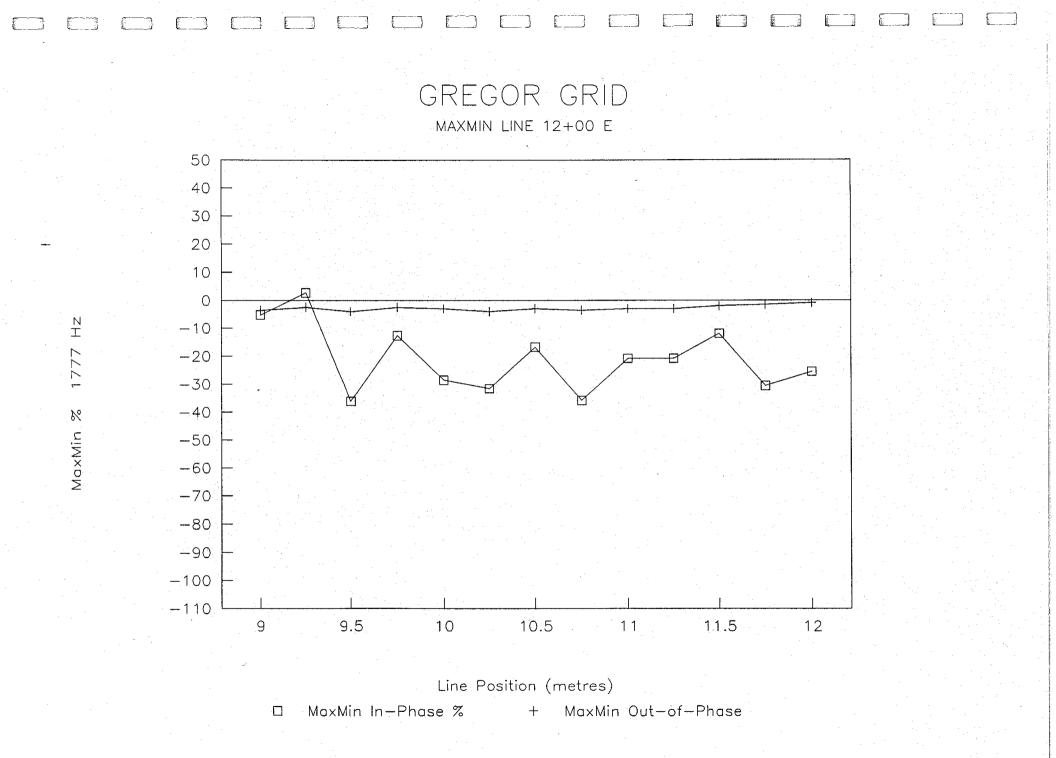
□ MaxMin In-Phase % + MaxMin Out-of-Phase

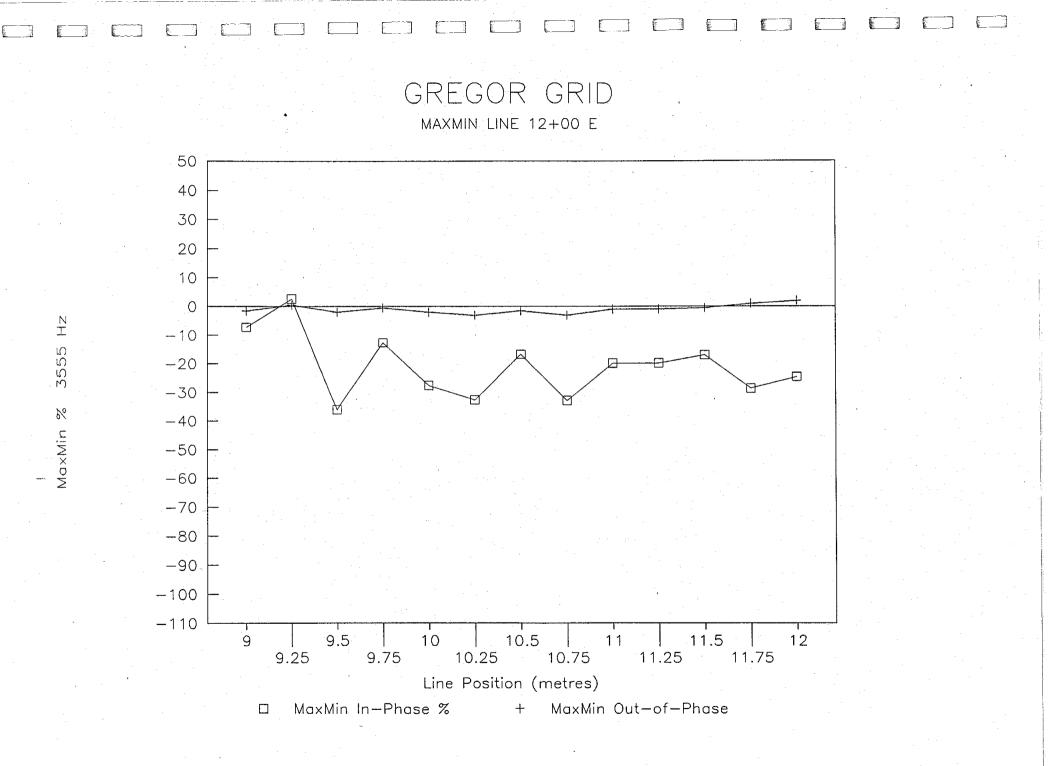
MaxMin % 1777 Hz

GREGOR GRID MAXMIN LINE 11+00 E 

MaxMin % 3555 Hz







#### GREGOR GRID ISKUTJV EM-VLF DATA, JUNE 1991

		LINE POSITION VLF DATA	VLF MEASURED	VLF FRASER FILTERED	LINE POSITION VLF FRASER FILTERED DATA	VLF FRASER FILTERED ANOMALLY DATA	VLF QUADRATURE	QUADRATURE FRASER FILTERED
	L9+00 E	8+50 N	53	-4	8+87.5 N		-4	12 *
		8+75 N 9+00 N	33 35	47 **	9+12.5 N 9+37.5 N		10 12	-4
		9+25 N	47	-85	9+62.5 N	n=55	6	-12
	· ·	9+50 N	68	-49	9+87.5 N	avg=9.4	12	-12
		9+75 N	12	-8	10+12.5 N	sd=13.7	6	6
		10+00 N	18	-21	10+37.5 N	sd*1=23.1 *	0	12 * 10
	н	10+25 N 10+50 N	13	-5	10+62.5 N 10+87.5 N	sd*2=36.8 ** sd*3=50.5 ***	6	0
		10+75 N	1	17	11+12.5 N	Ga 0-00.0	12	-10
		11+00 N	16	2	11+37.5 N		10	-4
		11+25 N	17	7	11+62.5 N		8	0
		11+50 N	17	12	11+87.5 N		4	-10
		11+75 N 12+00 N	18	-2	12+12.5 N		10 2	-3
		12+00 N	23				2	
		12+50 N	15	· .			7	
	L 10+00 E	8+50 N	35	2	8+87.5 N		0	14 *
		8+75 N	30	35 *	9+12.5 N		-4	10
		9+00 N	29.	31 *	9+37.5 N		5	-8
		9+25 N 9+50 N	38 56	-48 -104	9+62.5 N 9+87.5 N		5	-13 15 *
		9+50 N 9+75 N	50 42	-104 -66	9+87.5 N 10+12.5 N		-4	22 **
		10+00 N	.4	-7	10+37.5 N		2	-2
		10+25 N	-10	19	10+62.5 N		15	-2
		10+50 N	-10	27 *	10+87.5 N		5	8
		10+75 N	-3	30 *	11+12.5 N		10	. 7
		11+00 N	2	19	11+37.5 N		8 15	7 15
		11+25 N 11+50 N	12 17	2	11+62.5 N 11+87.5 N		10	-15
		11+75 N	16		12+12.5 N		6	-
		12+00 N	13				4	:
		12+25 N	22			si in	6	
		12+50 N	n/r					
	L 11+00 E	8+50 N	30	-10	8+87.5 N		0	4
	1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 - 1999 -	8+75 N 9+00 N	-6 0	46 **	01112.014		-7	16 * 15 *
	ан. Д	9+25 N	14	46 **	9+37.5 N 9+62.5 N		7	-7
		9+50 N	26	2	9+87.5 N		6	-18
	-	9+75 N	34	4	10+12.5 N		9	-8
		10+00 N	40	11	10+37.5 N		-3	5
	2	10+25 N	22	-49	10+62.5 N		· · · O	-4
		10+50 N	56	-49	10+87.5 N	. •	-2	8
		10+75 N 11+00 N	17 12	-13 -14	11+12.5 N	· · · [	-6	6
	1. A. A.	11+25 N	12	-14 -10	11+37.5 N 11+62.5 N	:	. 0	-3
		11+50 N	4	-5	11+87.5 N		0	3
		11+75 N	6	6	12+12.5 N	v	-3	3
		12+00 N	0		· · · · ·		0	. 1
		12+25 N	5 7				0	
	L 12:500 E	12+50 N 8+50 N	-2	24 *	8+87.5 N		0 10	1
		8+75 N	-2	24	9+12.5 N	· •	4	17 **
		9+00 N	7	8	9+37.5 N		6	22 **
		9+25 N	17	3	9+62.5 N		9	-7
	.	9+50 N	15	7	9+87.5 N		18	-31
		9+75 N	17	8	10+12.5 N		19	-11
		10+00 N	18	-11	10+37.5 N		1	0
		10+25 N 10+50 N	21 22	-32 -22	10+62.5 N 10+87.5 N		5	-7
	· · [	10+75 N	6	-7	10+87.5 N	· · [	4	
	· · · · · ·	11+00 N	5	-3	11+37.5 N		0	9
	· ·	11+25 N	1	-4	11+62.5 N		-2	13 *
		11+50 N	3	3	11+87.5 N	· · · · · [	-2	-4
		11+75 N	· 0	18	12+12.5 N		9	-3
		12+00 N	0				O	
•		12+25 N	6				3	
	1	12+50 N	12	. 1	1	- · · · · · ·	3	·

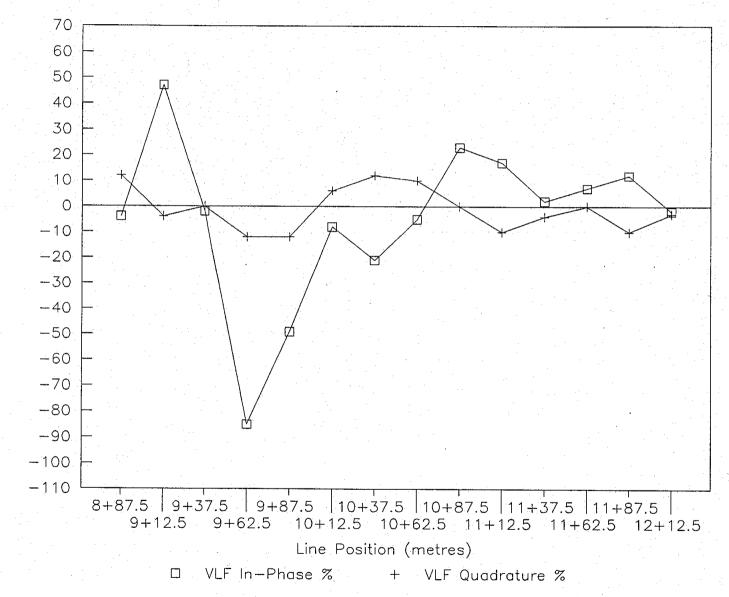
GREGOR GRID FRASER FILTERED VLF 9+00 E

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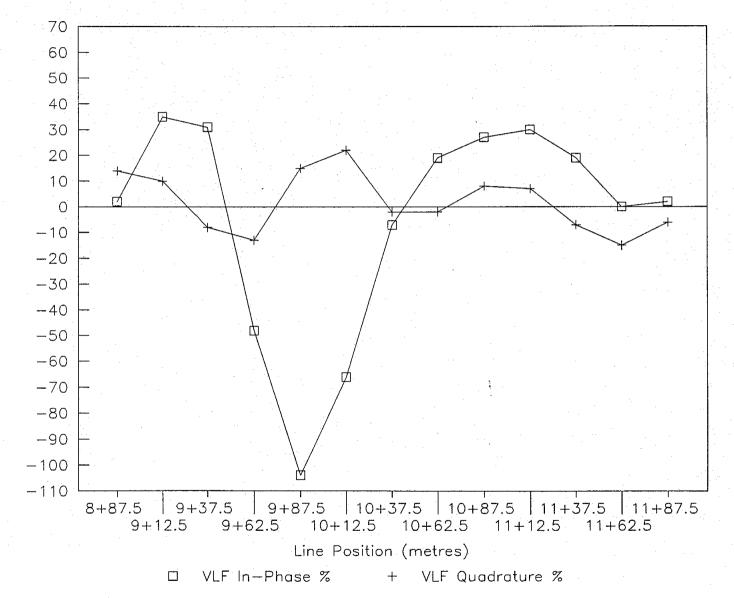
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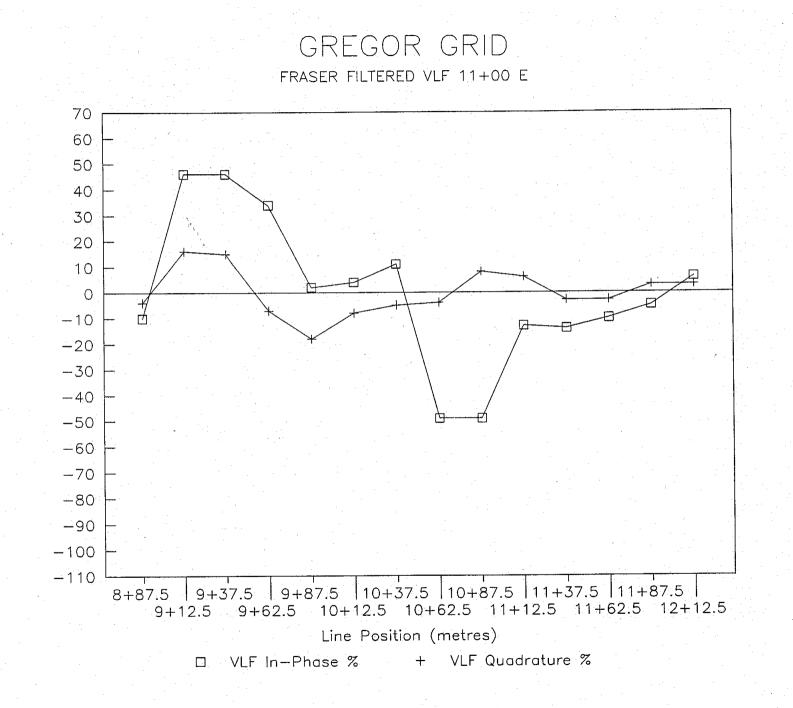
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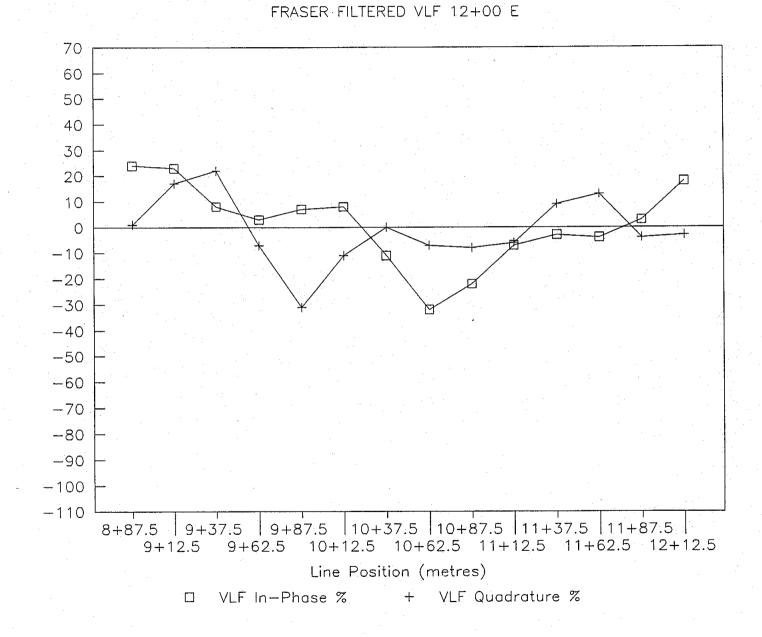


### GREGOR GRID FRASER FILTERED VLF 10+00 E



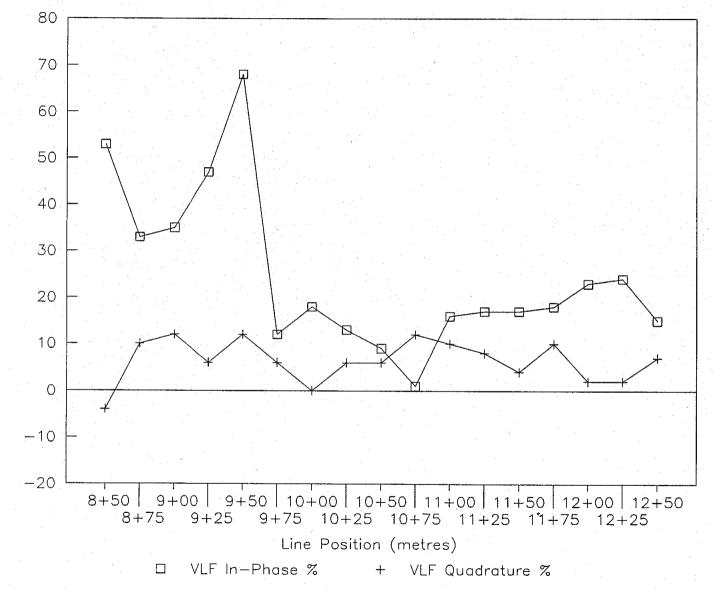


GREGOR GRID





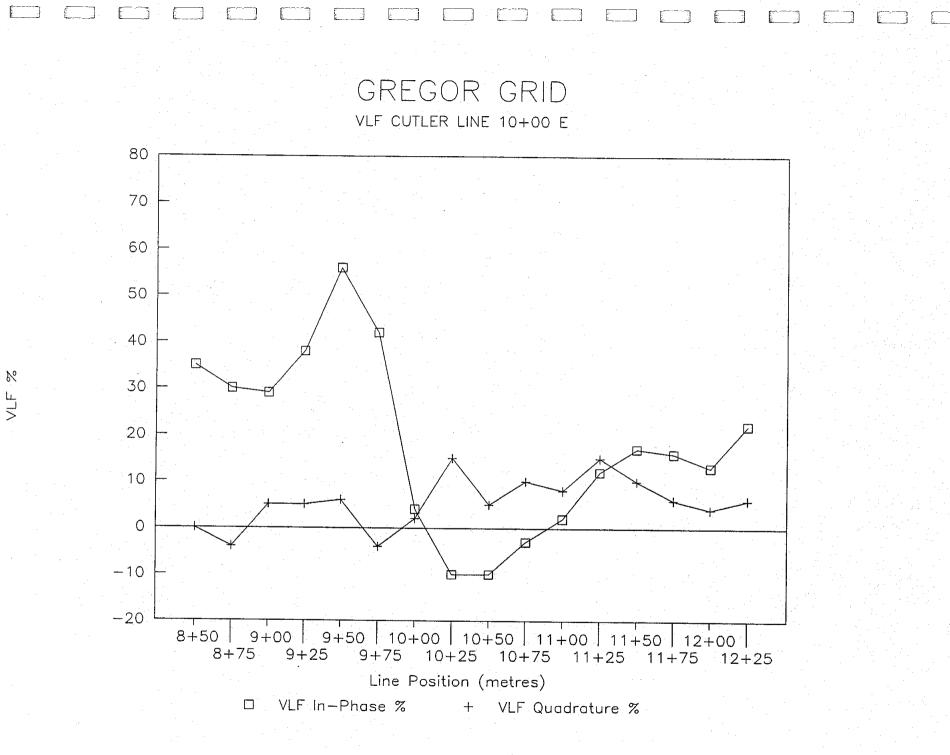
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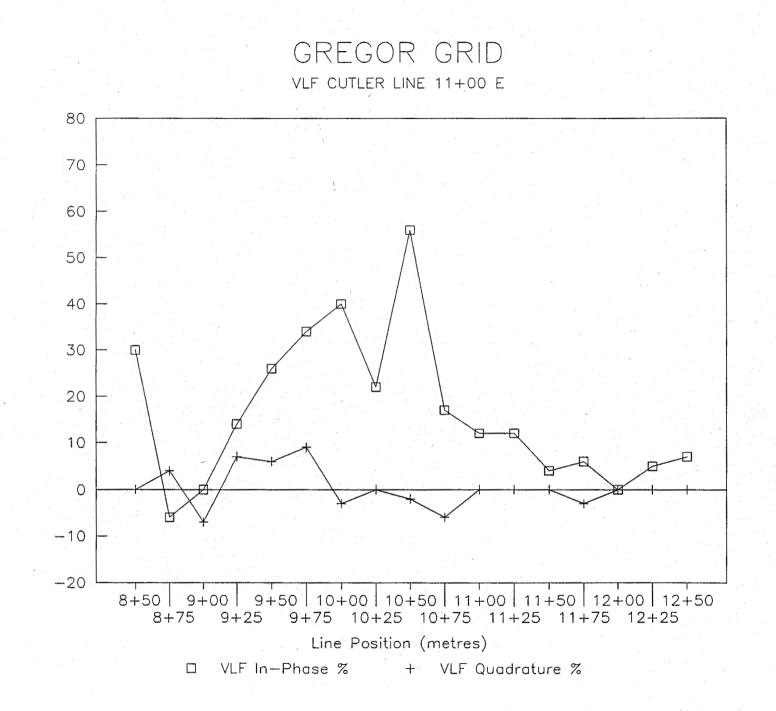


VLF %

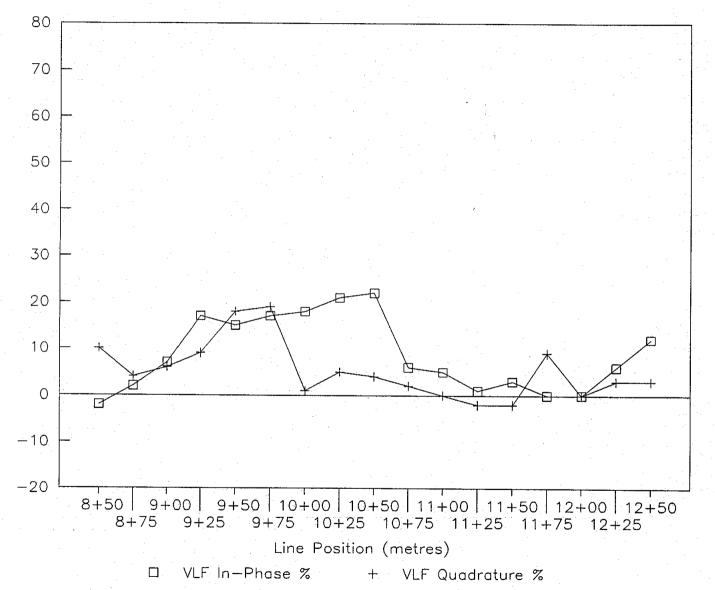
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GREGOR GRID VLF CUTLER LINE 12+00 E



## APPENDIX C

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### **ROCK DESCRIPTIONS**

#### **ROCK DESCRIPTIONS**

64042

<u>Grab</u>. Very proximal sub-crop found in the creek bed. Relatively fresh siltstone with some fine grained sulfides (probably pyrite with a trace of chalcopyrite).

- 64044 <u>Float</u>-Bull quartz vein found in the stream bed. Pieces of quartz in the area up to 8 cm. wide. Host is a metasediment. Float.
- 64045 <u>Float</u>-Gossanous siltstone found in the stream bed which is strongly silicified with very fine grained pyrite. Float.

64046 <u>Grab.</u> Very strongly silicified siltstone found on the face of an east-west trending prominent outcrop standing 2 to 4 metres high. Bedding measurement (dipdir, dip) (350,60). Grab.

- 64047 <u>Grab</u>. Metavolcanic found at the headwaters of a stream. Grab.
- 64048 <u>Grab.</u> Very strongly altered metasediment. Strongly silicified and bleached with quartz stringers and veinlets up to 1 cm. Gossanous but appears to be little sulfide. Grab.
- 64049 <u>Float</u>- Bull quartz veins found in the stream with pieces up to 25 cm. wide being common. Float.
- 64050 <u>Float</u>- Very pyritic metasediments. Very siliceous. Found in stream bed. Float.
- 64051 <u>Grab</u>. Metavolcanic with very fine grained disseminated pyrite and an unidentified white sulfide. Not silicified. Grab.
- 64052 <u>Float</u>-Metavolcanic float in the stream bed. Somewhat gossanous. Float.
- 64054 <u>Chip</u> Very gossanous pod found within a package of volcanic flows. (dipdir,Dip) (120,55) Pod is 4 m. long and 0.7m. thick. Contains some calcite, anhydride and some zeolite. Chip across 0.7 metres.
- 64055 <u>Grab</u> A small (1 2 metre wide) diorite dyke found at the contact of sediments and an andesite. Strongly foliated and silicified with up to 3% pyrite. Grab.
- 64056 <u>Grab</u> Well bedded, hornfelsed, metasiltstone with up to 5% pyrite. Grab.

64057 <u>Grab</u> Metavolcanic which is slightly gossanous. Quite mafic and dark. Grab.

64058 <u>Grab</u> Mafic metavolcanics. Slightly siliceous and pyritic. Contains plagioclase phenocrysts up to 4 mm. long. Grab.

64059 <u>Grab</u> Vesicular basalt with blebs of magnetite and chlorite with a trace of chalcopyrite. Flows of these volcanics sit at (dipdir, dip) (280, 87). Grab.

64060 <u>Grab</u> Sub-crop which has come from the cliffs above. Grab.

64061 <u>Chip</u> Metavolcanics very close to the contact of the Bronson Stock. Moderate amount of weak epidote and some quartz veins. Trace of very fine grained (pyrite?). Main foliation with quartz veinlets and sweats at (0, 65)(dipdir,dip). Chip across 1.0 metre.

64062 <u>Grab</u> Metavolcanics within metres of the Bronson Stock contact. Approximately 2% combined pyrite and magnetite. Mildly silicified. Grab.

64063 <u>Chip</u> Bull quartz vein at (dipdir, dip)(045, 25). 35 cm. wide hosted in relatively unaltered volcanics. Chip across 35 cm.

64064 <u>Grab</u> Fresh Orthoclase Porphyry with disseminated magnetite. Some epidote present. Grab.

64065 <u>Grab</u> Outcrop of metavolcanic found under an uprooted tree. Moderate to strongly and pervasively epidote altered, with small blebs of chlorite, pyrite, and hematite. Grab.

64066 <u>Grab</u> Carbonate flooded andesite lapilli tuff. Weak epidote with the carbonate. Very strongly magnetic. Grab.

64067 <u>Grab</u> Metasediments with large blebs (3cm.) of magnetite and hematite. Found in outcrop in a very steep stream. Weakly bedded at (dipdir,dip) (085, 70). Grab.

64068 <u>Grab</u> Strongly foliated orthoclase porphyry. Not very good outcrop but best estimate of the foliation is (strike, dip) (160, 90E). Strongly clay altered as well as blebs of pyrite and hematite. Grab.

64069 <u>Chip</u> Schist which was probably originally a volcanic. Very heavy sulfides (>10%) Contains pyrite, chalcopyrite, and abundant quartz/carbonate flooding. Foliation at (dipdir,dip) (230, 35). Chip across 1.0 metre.

64075 <u>Grab</u> Mafic volcanic flow found in outcrop next to the stream. Contains approximately 10% magnetite. Grab.

<u>Grab</u> Mafic flows with quartz veins up to 3 cm wide. Strongly magnetic. Minor amounts of pyrite and hematite. No quartz taken in this sample. Grab.

64076

64077 Grab Mafic volcanic flows. Same unit as 64076 but took the quartz as a sample this time. Trace of chalcopyrite. Grab. 64078 Grab Possibly a rhyolite. Very felsic with quartz and plagioclase crystals. See occasional guartz eyes. 1.5% of an unidentified black metallic mineral and 1 % pyrite. Grab. Grab Greywacke with fine disseminated Magnetite, pyrite and chalcopyrite. 64079 Slightly magnetic. Much of the surrounding rock is more magnetic and well bedded. Grab. Float - Hornfelsed siltstone/mudstone with up to 12% pyrite. and minor 64080 hematite. Sulfide found in stringers as well as blebs. Float. Float - Foliated diorite found in the roots of a tree. 10% total sulfide, mostly 64081 pyrite with some pyrrhotite, hematite and chalcopyrite. Quite angular. Float? Talus Talus blocks containing small quartz sweats and veinlets (up to 4 cm. 64082 wide). These metavolcanic talus blocks do not appear to be transported very far. Float. Grab Metasediments which are foliated but not strongly altered. Fractured 64083 with guartz/carbonate, manganese and minor sulfides along fractures. Grab. Chip Bull guartz vein, 30 cm. wide. Undulating with no true orientation but 64084 is generally flat lying. Chip over 30 cm. Grab Mafic lapilli tuff. Pyroxene is the main constituent. Minor sulfides 64086 (pyrite) but appears to be very fresh with tuffaceous texture very easily identified. Grab. 64106 Grab, coarse grained orthoclase porphyry with very fine grained disseminated pyrite. 64107 Moss Mat, EH #8 re sample. 64108 Moss Mat, EH #9 re sample. 64109 Float, angular bull white quartz vein with chlorite rim within black metavolcanic. 1m Grab/Chip, sheared/foliated dark green metavolcanic with blebs and 64110 bands of laminated pyrite/chalcopyrite. Grab, semi massive blebs/bands of laminated pyrite within dark volcanic. 64111

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	64112	3/4m Chip, massive bands of laminated pyrite within dark volcanic.
	64113	1m Chip, semi massive bands of laminated pyrite within dark volcanic.
	64114	Grab, metavolcanic, purple foliated garnet/feldspar/chlorite dark green andesite with 1-3% disseminated pyrite.
	64115	Grab, quartz veins with very fine grained pyrite.
	64116	Grab, weakly altered feldspar porphyry with disseminations and blebs pyrite.
	64117	Grab, feldspar porphyry with blebs of magnetite.
	64118	Grab, altered feldspar porphyry with blebs of pyrite.
•	64119	Grab, feldspar porphyry with blebs of pyrite.
	64208	<u>Grab</u> Metasediment with 1.5 cm quartz veinlets running parallel to each other. Grab.
	64209	Float- Silicified metasediment found 20 metres to the east of 64208. Float.
	64210	Float? Possible sub-crop or float- Strongly silicified metasediment with 2mm quartz veinlets with minor disseminated pyrite. Float?
•	64211	<u>Grab</u> Silicified metasediment found at a small outcrop just north of the stream. Some very fine grained disseminated unidentified sulfides. Grab.
	64212	<u>Grab</u> Silicified metasediment found in a dry creek bed. Up to 7 % sulfide. Grab.
	64213	Sub-crop or float- Metasediment with fine grained disseminated sulfides and blebs up to 4 mm. across. Float.
	64214	<u>Chip</u> Bull quartz vein- 7 cm wide with a trace of pyrite. Orientation (dipdir, dip (190, 86). Chip across 7 cm.
	64215	<u>Grab</u> Metasiltstone with up to 4% disseminated sulfide(pyrite + trace chalcopyrite). Mildly silicified. Grab.
	64216	<u>Grab</u> Metavolcanics with a trace of very fine grained disseminated pyrite. Grab
	64217	Float- Metavolcanics which appear to be flow banded. Float.

64219 Grab Bull quartz vein with an equal amount taken from each of four small veins. (1 - 2 cm. scale). Grab. Grab Metavolcanic with small stringers and blebs of fine grained sulfide. 64221 chlorite and magnetite. Foliation at (dipdir, dip) (80, 10). Grab. 64222 Grab Sample taken from an orthoclase porphyry dyke. Texturally very similar to the Bronson stock. Dyke is approximately 25 metres wide. Grab. 64223 Same as above (#64222). 64224 Grab Metavolcanic with many stringers of very fine grained sulfides (pyrite and minor pyrrhotite. Grab. 64226 Float Float found in creek bed - frothy appearance limonitic weathered out section of volcanic rock. Float. 64227 Grab Boulder in snowfield. Skarned sediment with chalcopyrite and pyrite present. Grab. 64228 Grab Basalt with disseminated 10% pyrite Heavy iron staining. Grab. 64229 Grab 1-3 cm bull quartz vein (230°, 50°N) (strike, dip) 25 m long. Grab. 64230 Grab 5 cm wide quartz vein (140, 10N). Traces of chalcopyrite and chalcopyrite present. Grab. 64231 Grab Start of second traverse going east. 4-5 cm quartz vein some sulphides weathered out with iron stain on rock. (190, 90N). Grab. 64232 Grab Basalt with blebs up to 1 cm. wide of magnetite + chlorite, pyrite and a trace of chalcopyrite. Possibility this is not outcrop. (Lots of snow cover). Grab? 64233 Grab Outcrop of metasediments above talus slope with small blebs of malachite 10% disseminated pyrite with lmm. pyrite stringers. Grab. 64234 <u>Grab</u> Orthoclase porphyry. Very near the intrusive margin but appears very fresh, with orthoclase phenocrysts up to 3 cm. long. Occasional blebs or stringers of magnetite. Grab. 64235 Grab Mafic volcanic rock with 2% very fine disseminated pyrite oriented at (30, 85W). Grab.

64236	Grab Metavolcanic found in outcrop (rare for this area). Quite unaltered. Grab.
64237	<u>Float</u> Float found under a fallen tree. Mildly altered with very little sulfide. Float.
64238 epidote	<u>Grab</u> Sample of the Orthoclase porphyry with an appreciable amount of alteration pervasive in the rock. Grab.
64239	<u>Grab</u> Large block of orthoclase porphyry found on $45^{\circ}$ talus slope. Orthoclase phenocrysts up to 1.3 cm long in apparent marginal phase with strong foliation. Grab.
64240	<u>Grab</u> Large outcrop of orthoclase porphyry 20 m long 10 m wide. Porphyry with 1-2 cm quartz veins - blebs with some disseminated pyrite. (240, 85S) foliation. Grab.
64241	<u>Float?</u> Float but more like sub-outcrop on a $40^{\circ}$ slope. Strongly foliated and metamorphosed rock with a high sericite contents. Up to 10% pyrite which is mainly disseminated as euhedral cubes up to 2mm across. Original rock type may be sedimentary. Float?
64242	<u>Grab</u> (105, 85S) foliation. 5 m from small drainage. Orthoclase porphyry. Grab.
64243	<u>Grab</u> Orthoclase porphyry. Quartz carbonate veins with an unidentified dark blueish green flaky mineral. Very fine disseminated pyrite seen in many rocks in the creek bed. Grab.
64244	Float Massive quartz boulder in creek bed. Found at the bottom of a talus slope The host orthoclase porphyry contains approximately 2% py. Float.
64245	Grab Orthoclase porphyry found on the north side of steep gully. Porphyry 3% disseminated pyrite with 1 mm blebs of pyrite. Grab.
64246	<u>Grab</u> Orthoclase porphyry with 1-2 mm. quartz stringers. 4% pyrite disseminated throughout 30 m long outcrop. Foliation has an orientation of (80, 85N). Grab.
64247	Float?. Fine grained orthoclase porphyry with 5% disseminated pyrite. Float.
64248	<u>Grab.</u> Completely silicified and silica flooded orthoclase porphyry. $5\% - 10\%$ epidote patches seen throughout the rock. Up to 7% disseminated pyrite with some blebs and stringers.

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Float. Quartz sweats up to 5 cm wide in orthoclase porphyry. Quartz is 64249 bullish with minor pyrite along the quartz host interface. Grab, rusty fractured biotite altered orthoclase porphyry with trace blebs 64250 pyrite. Grab, rusty quartz vein with blebs pyrite. 64251 Float, angular boulder 5m x 7m x 2m chlorite/epidote altered feldspar crystal 64252 lapilli tuff with fracture malachite and blebs chalcopyrite 1-2%. Grab, metasediment with quartz fragments, blebs pyrite and chalcopyrite. 64253 64254 Grab, granular white/orange quartz vein. 1m Chip/Grab, host "254" very fine grained siltstone. 64255 64256 Grab, 5cm shear previously sampled, pyrite, galena. 64310 Moss Mat, re sample SS#3, 1987 64311 1m Grab Chip, foliated black metasediment with 2-5% very fine grained silver disseminated pyrite. Grab, angular subcrop, white translucent bull quartz spec chalcopyrite with 64312 malachite, chlorite rim. 64313 Grab, subcrop, white metasandstone limy, weakly calcareous, 1-3% disseminated pyrite. Moss Mat, re sample SS#2, 1987 64314 64315 Moss Mat, re sample SS#1, 1987 64316 <u>Grab</u>, skarn pod, quartz/chlorite/garnet with minor epidote, trace pyrite/chalcopyrite, host metasediment. 64317 Moss Mat 64318 Moss Mat 64329 Moss\_Mat 64320 1m Chip/Grab, foliated black metasediment with milky white quartz filled gashes, trace disseminated pyrite.

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	64321	<u>Moss Mat</u>
	64322	Moss Mat
	64323	Grab, very find grained black metasediment with fracture pyrite and 1-2% disseminated pyrite, follow-up of "95701".
	64324	Grab, medium grained pale green metavolcanic feldspar porphyry with 3-5% disseminated pyrite.
	64325	Float, angular rusty quartz vein, chlorite rims with trace disseminated pyrite/chalcopyrite.
	64326	Moss Mat
	64327	<u>Silt</u>
	64328	<u>Float</u> , angular rusty milky white quartz, glassy with trace fracture and blebs of pyrite 25 cm x 20 cm.
	64329	Grab, rusty pyritic fractured, brecciated crystal lithic lapilli tuff.
	64330	Grab, quartz carbonate fracture zone within crystal lithic lapilli tuff, 5-10% disseminated pyrite.
	64331	Grab, 2-3 cm glassy rusty quartz filled fracture with blebs chalcopyrite.
	64332	Grab, host of "331" crystal lithic lapilli tuff.
	64333	<u>Moss Mat</u>
	64334	<u>Silt</u>
	64335	Grab/Chip, pyritic andesite flow
	64336	<u>1m vertical grab/chip</u> , very fine grained black volcanic at sediment contact, shear zone, 5-7% blebs and disseminations pyrite.
	64337	Grab, subcrop, sheared volcanic with Fe carbonate alteration, 5-12% fine grained disseminated pyrite.
	64338	Moss Mat
	64339	<u>Silt</u>

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64340Im vertical Chip, pyrite argillite at shear contact zone 2-5% disseminated pyrite.64341Moss Mat.64342Silt64343Moss Mat.64344Silt64345Im Chip/Grab., medium coarse grained feldspar porphyry with 1% blebs pyrite,? chalcopyrite?64346Float, angular quartz flooded feldspar porphyry with 1% blebs pyrite/chalcopyrite.643472m Grab, weakly prophylitic altered feldspar porphyry with 1% pyrite, trace chalcopyrite locally magnetic, quartz sweats, crystals locally.64349Grab, weakly altered feldspar porphyry with trace magnetite/pyrite and bull white quartz sweats.64350Grab, epidote/K-spar porphyry with 1-3% blebs and disseminated pyrite.64351Grab, pyritic metavolcanic, dark green64352Subcrop/Float., black/grey metasediment chips from within creek.64353Subcrop/Float., black siltstone porcelinite with disseminated pyrite.64353Subcrop, highly fractured pyritic felsic rock.		
64342Silt64343Moss Mat64344Silt64345Im Chip/Grab., medium coarse grained feldspar porphyry with 1% blebs pyrite,? chalcopyrite?64346Float, angular quartz flooded feldspar porphyry with trace disseminated pyrite/chalcopyrite.643472m Grab, weakly prophylitic altered feldspar porphyry with 1% pyrite, trace chalcopyrite locally magnetic, quartz sweats, crystals locally.64348Im vertical Grab/Chip., foliated feldspar porphyry with trace magnetite/pyrite and bull white quartz sweats.64349Girab, weakly altered feldspar porphyry with 1-3% blebs and disseminations pyrite.64350Grab, epidote/K-spar porphyry with magnetite and 1-2% disseminated pyrite64351Grab, pyritic metavolcanic, dark green64352Subcrop/Float., black/grey metasediment chips from within creek.64353Subcrop/Float., black siltstone porcelinite with disseminated pyrite, graphitic.64354Float, angular quartz float with disseminated pyrite.	64340	
<ul> <li>64343 Moss Mat</li> <li>64344 Silt</li> <li>64345 Im Chip/Grab, medium coarse grained feldspar porphyry with 1% blebs pyrite,? chalcopyrite?</li> <li>64346 Float, angular quartz flooded feldspar porphyry with trace disseminated pyrite/chalcopyrite.</li> <li>64347 2m Grab, weakly prophylitic altered feldspar porphyry with 1% pyrite, trace chalcopyrite locally magnetic, quartz sweats, crystals locally.</li> <li>64348 Im vertical Grab/Chip, foliated feldspar porphyry with trace magnetite/pyrite and bull white quartz sweats.</li> <li>64349 Grab, weakly altered feldspar porphyry with 1-3% blebs and disseminations pyrite.</li> <li>64350 Grab, epidote/K-spar porphyry with magnetite and 1-2% disseminated pyrite</li> <li>64351 Grab, pyritic metavolcanic, dark green</li> <li>64352 Subcrop/Float, black/grey metasediment chips from within creek.</li> <li>64353 Subcrop/Float, black siltstone porcelinite with disseminated pyrite, graphitic.</li> <li>64354 Float, angular quartz float with disseminated pyrite.</li> </ul>	64341	<u>Moss Mat</u>
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<ul> <li>and bull white quartz sweats.</li> <li>64349 Grab, weakly altered feldspar porphyry with 1-3% blebs and disseminations pyrite.</li> <li>64350 Grab, epidote/K-spar porphyry with magnetite and 1-2% disseminated pyrite</li> <li>64351 Grab, pyritic metavolcanic, dark green</li> <li>64352 Subcrop/Float, black/grey metasediment chips from within creek.</li> <li>64353 Subcrop/Float, black siltstone porcelinite with disseminated pyrite, graphitic.</li> <li>64354 Float, angular quartz float with disseminated pyrite.</li> </ul>	64347	
<ul> <li>pyrite.</li> <li>64350 Grab, epidote/K-spar porphyry with magnetite and 1-2% disseminated pyrite</li> <li>64351 Grab, pyritic metavolcanic, dark green</li> <li>64352 Subcrop/Float, black/grey metasediment chips from within creek.</li> <li>64353 Subcrop/Float, black siltstone porcelinite with disseminated pyrite, graphitic.</li> <li>64354 Float, angular quartz float with disseminated pyrite.</li> </ul>	64348	
<ul> <li>64351 <u>Grab., pyritic metavolcanic, dark green</u></li> <li>64352 <u>Subcrop/Float., black/grey metasediment chips from within creek.</u></li> <li>64353 <u>Subcrop/Float., black siltstone porcelinite with disseminated pyrite, graphitic.</u></li> <li>64354 <u>Float., angular quartz float with disseminated pyrite.</u></li> </ul>	64349	
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64353Subcrop/Float , black siltstone porcelinite with disseminated pyrite, graphitic.64354Float , angular quartz float with disseminated pyrite.	64351	Grab, pyritic metavolcanic, dark green
64354 <u>Float</u> , angular quartz float with disseminated pyrite.	64352	Subcrop/Float, black/grey metasediment chips from within creek.
	64353	Subcrop/Float, black siltstone porcelinite with disseminated pyrite, graphitic.
64355 <u>Subcrop</u> , highly fractured pyritic felsic rock.	64354	Float, angular quartz float with disseminated pyrite.
	64355	Subcrop, highly fractured pyritic felsic rock.

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#### WHOLE ROCKS

#### 64070WR Hemlo West drill core. Hole JV-87-01, 50.0 - 50.2 metres. Logged as:

"Fine-grained mafic tuff with intercalations of very fine grained dacitic tuff and greywacke."

The sampled core was comparatively light coloured (presumably dacite), appearing to have minimal alteration other than minor light brown alteration (oxidation of the mafic minerals).

<u>64071WR</u> JV-87-01, 105.5 - 105.9 metres. Logged as:

"Interbedded, fine-grained sandstone and pyrite-rich tuff."

Sampled core was fine grained tuff. Clasts are very small (2-4 mm.). Siliceous in part with strong, pervasive sericitization. Only a trace of pyrite in this particular section.

<u>64072WR</u> JV-87-01, 113.5 - 113.9 metres. Logged as:

"Dacite lapilli tuff."

Sampled core does not appear strongly altered. May have been more mafic than indicated by dacitic lable.

<u>64073WR</u> JV-87-01, 136.6 - 137.0 metres. Logged as:

"Interbedded dacite lapilli tuff and rhyolite."

Core is very light coloured indicating felsic composition. Clay alteration is present. Relict flow texture is visible in areas.

### <u>64074WR</u> I 90-11, 34.0 - 34.4 metres. Logged as:

"Locally weakly mineralized polylithic lapilli tuff."

Freshest intersection of andesite lapilli tuff in the hole. Fragments up to 3 cm across. Contains some pyroxene phenocrysts in some clasts. Moderate chloritization, which is found pervasively through all rocks in the area, is present. Fresh with two small (1mm) carbonate stringers.

<u>64086WR</u> Taken from the slope south of Mount Verrett, and just above tree line. Some of the freshest appearing rock seen on property. Fresh andesite flow. Approximately 18% feldspar phenocrysts (approximately 3 - 4 mm).

## APPENDIX D

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### UNIVARIATE STATISTICS

The data which was used for the stastical analysis in this report came from the following files:

### BONDAR-CLEGG

	V6042611 FTX	V6043611 FTX	V6045561 FTX	V6045566 FTX	V7042301 FTX	V1007130 FTX
	V7042311 FTX	V7046511 FTX	V7046671 FTX	V7046676 FTX	V7046861 FTX	V1007130 PRN
	V7046871 FTX	V7053881 FTX	V7054061 FTX	V7054066 FTX	V7054181 FTX	V1007640 FTX
	V7054186 FTX	V7070844 FTX	V9075840 FTX	V9075845 FTX	V9075846 FTX	V1007640 PRN
	V9075848 FTX	V9075980 FTX	V9075984 FTX	V9075985 FTX	V9075986 FTX	V1007646 FTX
	V9076080 FTX	V9076084 FTX	V9076085 FTX	V9076086 FTX	V9076088 FTX	V1007646 PRN
	V9076490 FTX	V9076495 FTX	V9076496 FTX	V9076498 FTX	V9076690 FTX	V1007700 FTX
	V9076700 FTX	V9076705 FTX	V9076706 FTX	V9076850 FTX	V9076856 FTX	V1007700 PRN
	V9076860 FTX	V9076990 FTX	V9076996 FTX	V9079480 FTX	V9079490 FTX	V1007706 FTX
•	V9079496 FTX	V9079500 FTX	V9079506 FTX	V9079510 FTX	V9079511 FTX	V1007706 PRN
	V9079514 FTX	V9079516 FTX	V9079930 FTX	V9079936 FTX		
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### T.S.L. LABS

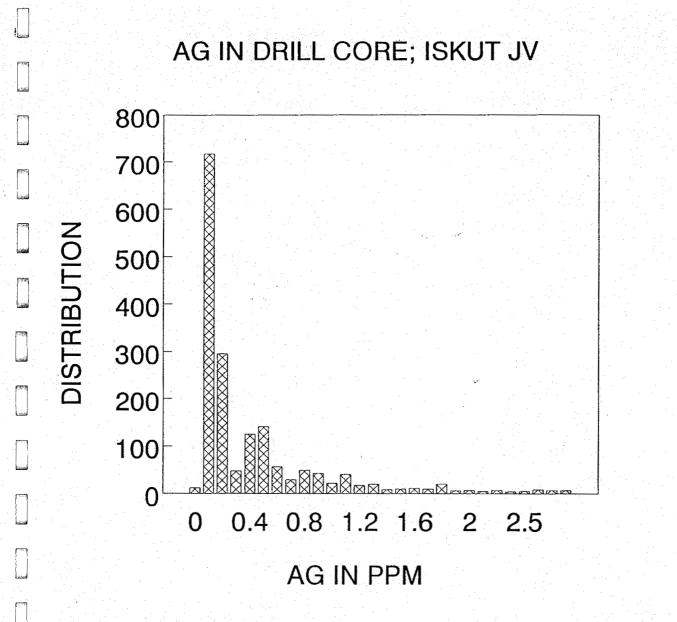
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S6935	DAT	\$6932	DAT	\$6933	DAT	\$6833	DAT	\$7331	DAT
\$7506	DAT	S7623	DAT	S7265	DAT	\$7233	DAT	\$7154	DAT
\$6979	DAT	\$6988	DAT	\$6934	DAT	\$6864	DAT	\$6899	DAT
\$9035	DAT	\$9038	DAT	\$9039	DAT	\$9040	DAT	S9041	DAT
\$9053	DAT	\$9054	DAT	\$9062	DAT	\$9063	DAT	<b>\$906</b> 4	DAT
\$9072	DAT	\$9096	DAT	\$9174	DAT	S9198	DAT	\$9200	DAT
\$9204	DAT								

### TERRAMIN LABS

	J08288A1	ASC	JO8288A2	ISC	J08288A3	ASC	J0828881	ASC	J0828882	ASC
	1082880		_108305A1		J08305A2		J08304A1	ASC	J08304A2	ASC
		ASC		ASC	108352		J08353A1	ASC	108353A2	ASC
• •	J08353A3	ASC	J08371A1	ASC	J06371A2	ASC	J08371A3	ASC	J08394A1	ASC :
	J08394A2	ASC	J08403A1	ASC	J08403A2	ASC	J08177	ASC		

#### MIN-EN LABS

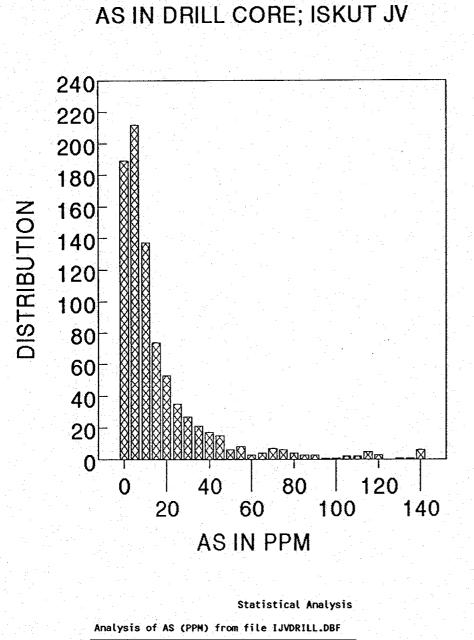
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0507425J A05	0S0742SJ A07	0\$0742SJ A08	0S0745RA A01	0S0745RJ A01
050749RJ A01	050749RJ A03	050749RJ A05	050749RA A01	OSO7SORJ A01

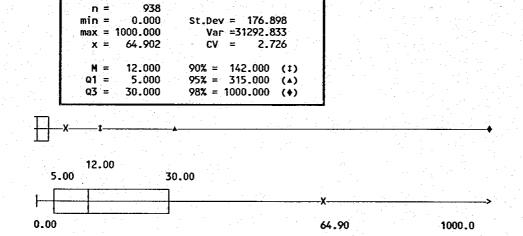


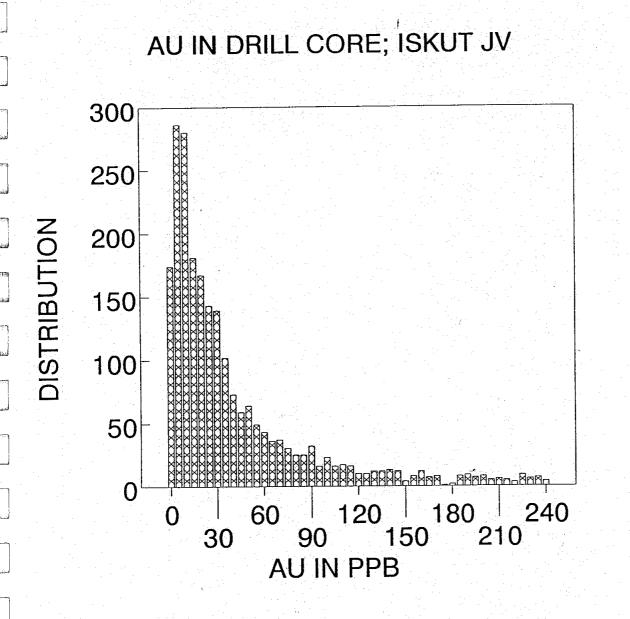
Statistical Analysis

Analysis of AG (PPM) from file IJVDRILL.DBF

n =	1841			
min =	0.010	St.Dev =	3.323	
max =	50.000	Var =	11.045	
x =	0.999	CV =	3.328	
M =	0.270	90% =	1.800 ()	
Q1 =	0.100	95% =	3.300 ()	
Q3 =	0.700	98% =	7.300 ()	





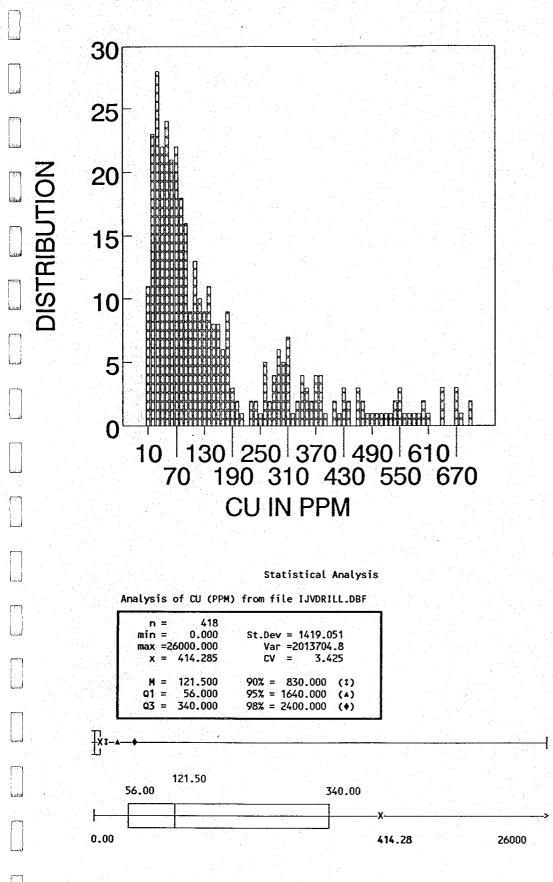


Statistical Analysis

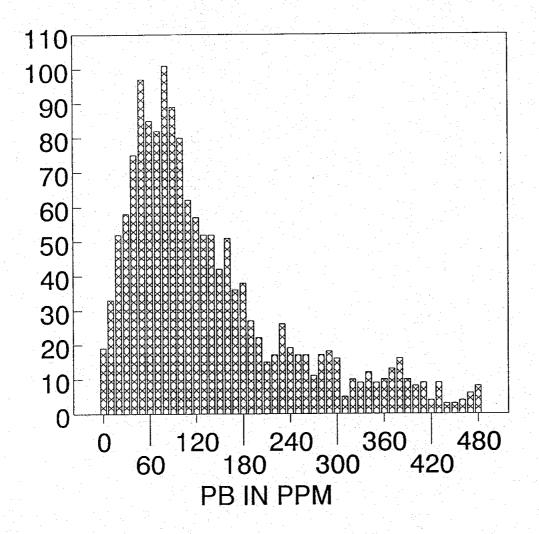
Analysis of AU (PPB) from file IJVDRILL.DBF

 		A State of the second		
n.	=	2466		
min	=	0.000	St.Dev = 1869.425	5
max	=6	6563.000	Var =3494751.2	
x	÷,	243.437	CV = 7.679	
M	= '	29.000	90% = 239.000 ()	
`Q1	=	12.000	95% = 543.000 ()	
Q3	=	76.000	98% = 1888.000 ()	

## CU IN DRILL CORE; ISKUT JV







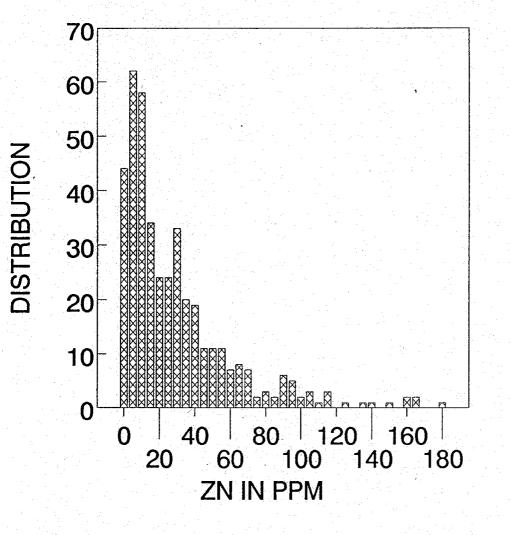
Statistical Analysis

Analysis of PB (PPM) from file IJVDRILL.DBF

DISTRIBUTION

. <u>18 1</u>	and the second second		1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	1. A.
			1665	n =
	= 603.117	St.Dev :	4.000	min =
	=363749.90	Var	6000.000	max =1
	= 2.509	CV	240.351	<b>x</b> =
	427.000 ()	90% =	119.000	M =
ar e	665.000 ()	95% = 0	69.000	· Q1 =
	1290.000 ()	98% = 1	231.000	Q3 =

# ZN IN DRILL CORE; ISKUT JV



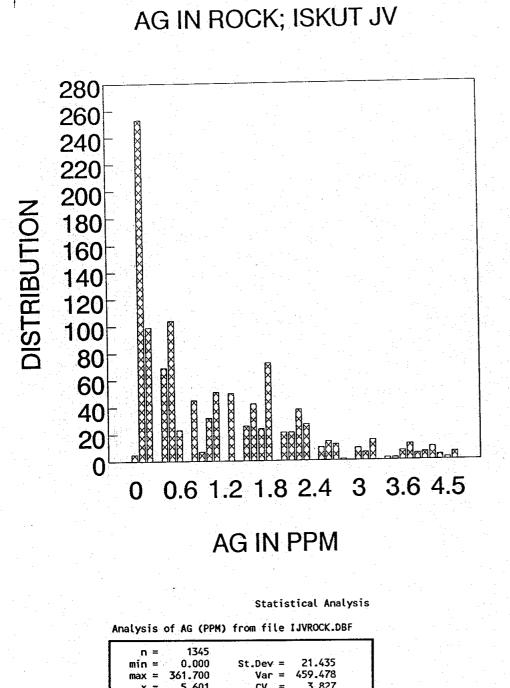
Statistical Analysis

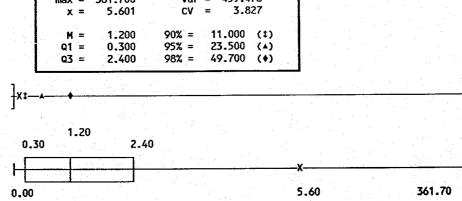
Analysis of ZN (PPM) from file IJVDRILL.DBF

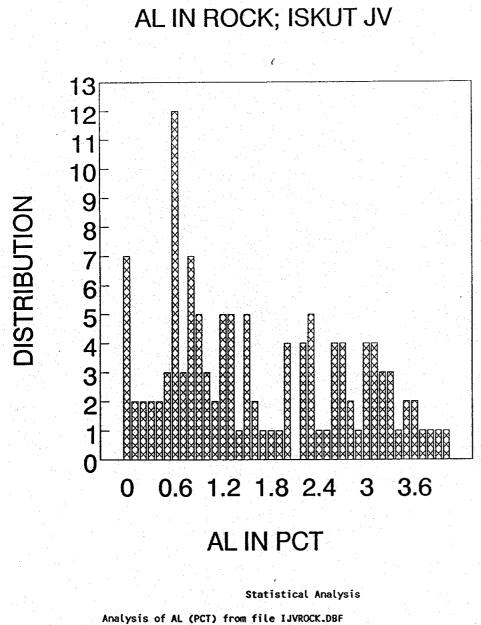
1.0	n	1	437	an tang ang	and the second second
1.5	ສາກ	=	0.000	St.Dev	= 189,995
1.	max	=	2400.000	Var	=36098.236
	X	Ξ	65.959	CV	= 2.881
	M	=	24.000	90% =	102.000 (1)
Ч., , Ч., ,	Q1	=	10.000	95% =	240.000 (*)
	03	=	48.750	98% =	500.000 (+)

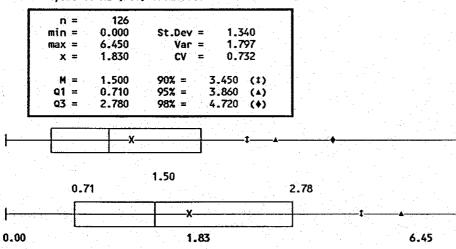
ريد معر اور سا 

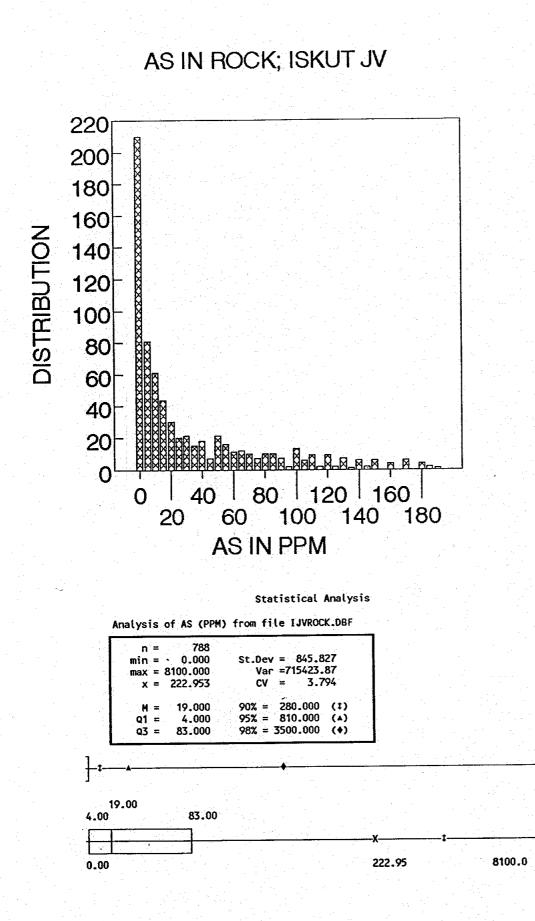
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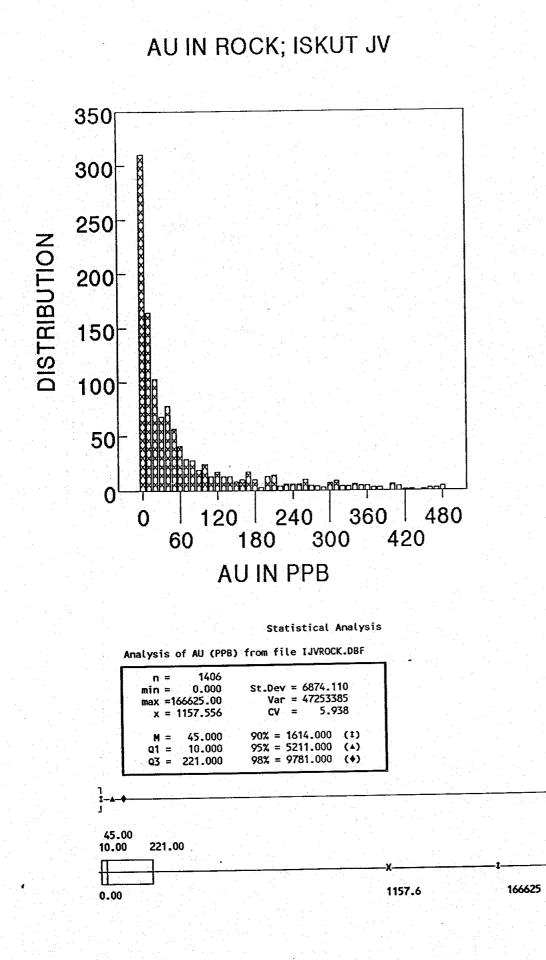


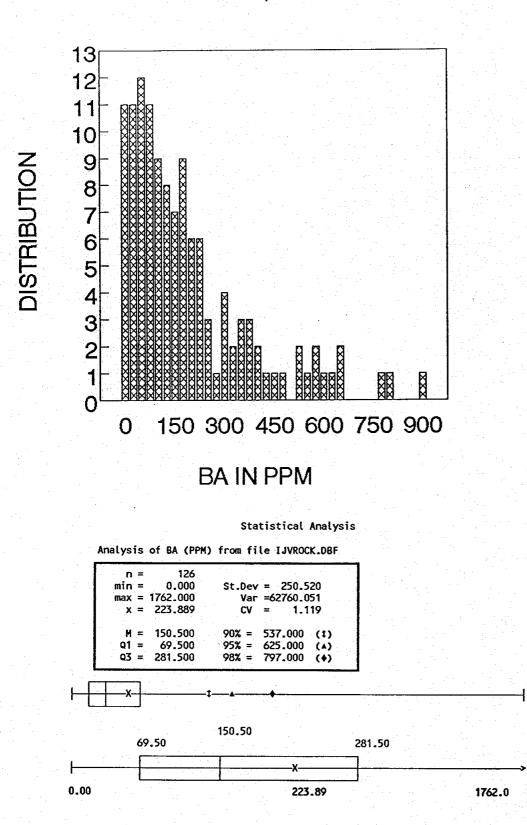




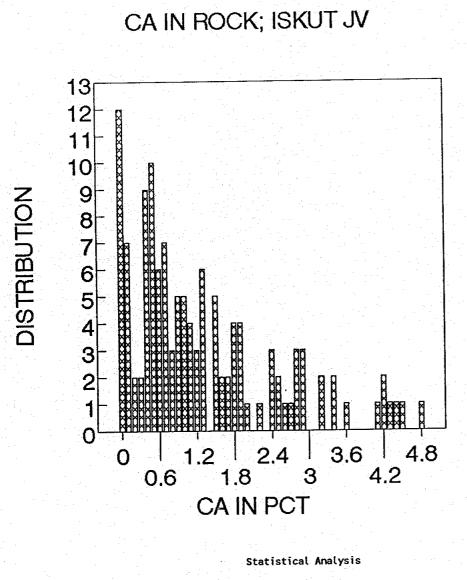




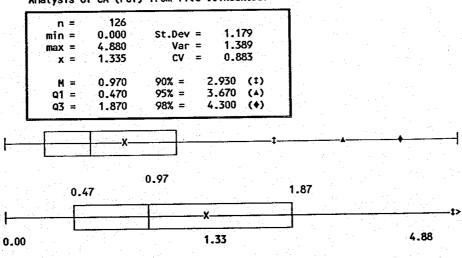


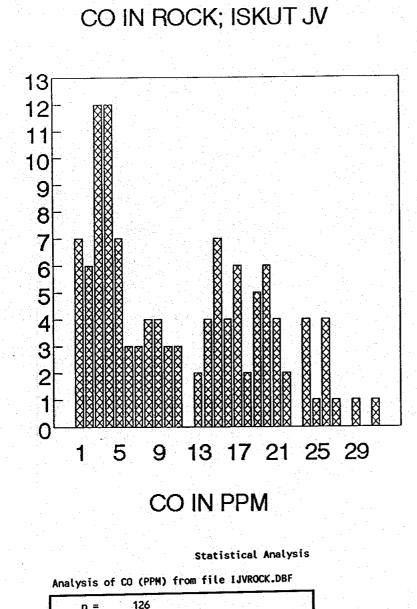


BA IN ROCK; ISKUT JV

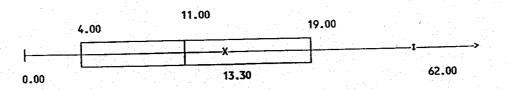


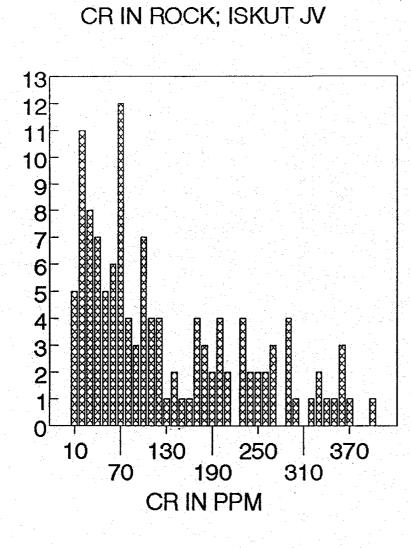
Analysis of CA (PCT) from file IJVROCK.DBF





126 0.000 n = 11.437 130.798 0.860 St.Dev = Var = min = max = 62.000 13.302 CV = x = 90% = 95% = 98% = 26.000 (1) 31.000 (4) 11.000 4.000 M = q1 = 41.000 (+) Q3 = 19.000

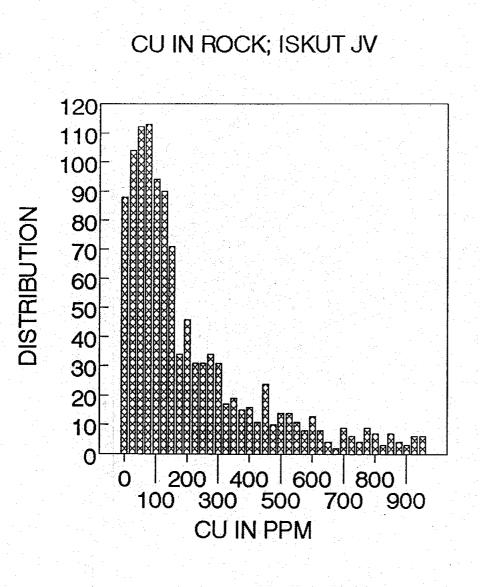




Statistical Analysis

Analysis of CR (PPM) from file IJVROCK.DBF

· ·	48.		00.00			2	209.0	0			
	L		<u></u>	<b>]</b>					· ·	star.	
	<u> </u>	x		]		•					
	M = Q1 = Q3 =	100.000 48.500 209.000		292.000 343.000 361.000	(1) (A) (+)						
		126 0.000 496.000 137.127		= 108.5 =11778.7 = 0.7	762						



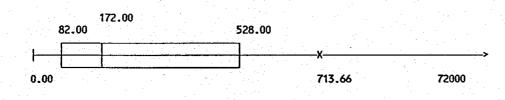
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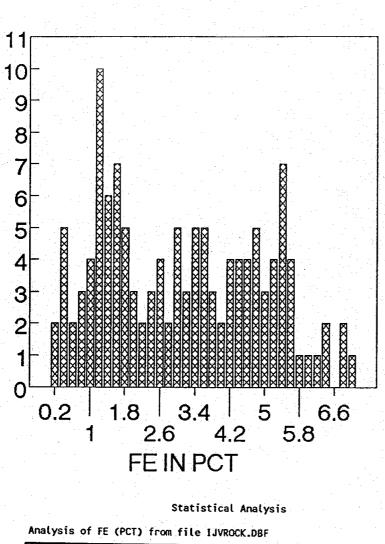
Statistical Analysis

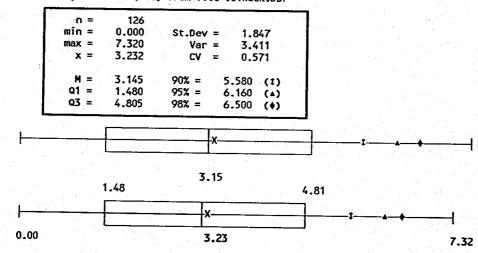
Analysis of CU (PPM) from file IJVROCK.DBF

n	= 1345	
៣រំព	= 0.000	St.Dev = 2871.470
max	=72000.000	Var =8245340.1
X	= 713.659	CV = 4.024
M	= 172.000	90% = 1500.000 (1)
Q1	= 82.000	95% = 2400.000 (*)
03	= 528.000	98% = 4600.000 (*)

XI

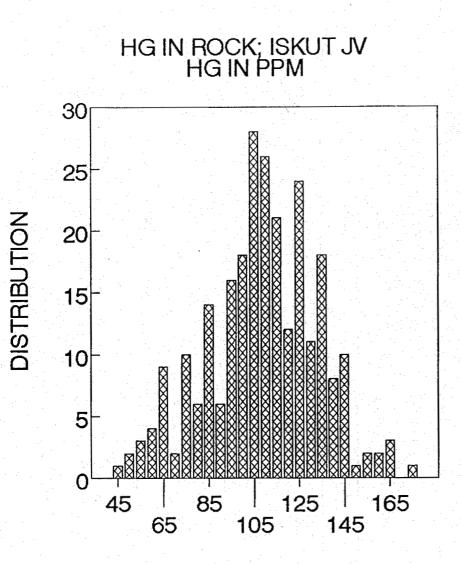


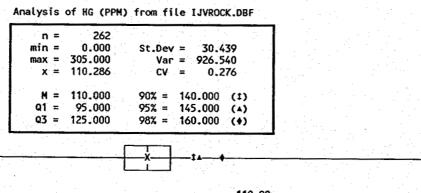


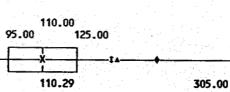


FE IN ROCK; ISKUT JV

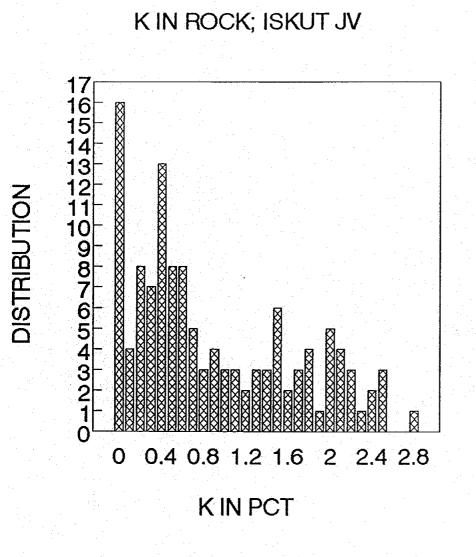
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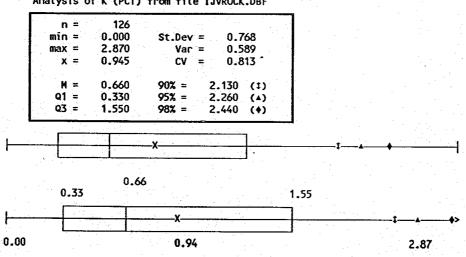


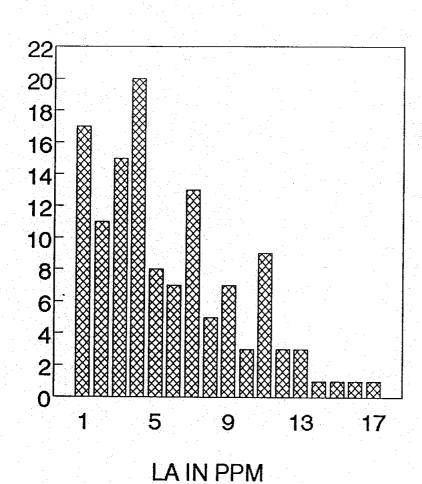
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Statistical Analysis

Analysis of K (PCT) from file IJVROCK.DBF



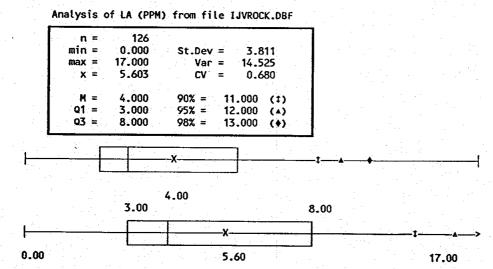


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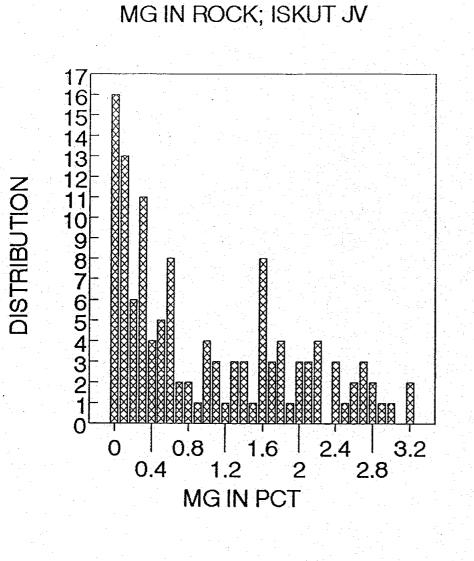
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Statistical Analysis



LA IN ROCK; ISKUT JV



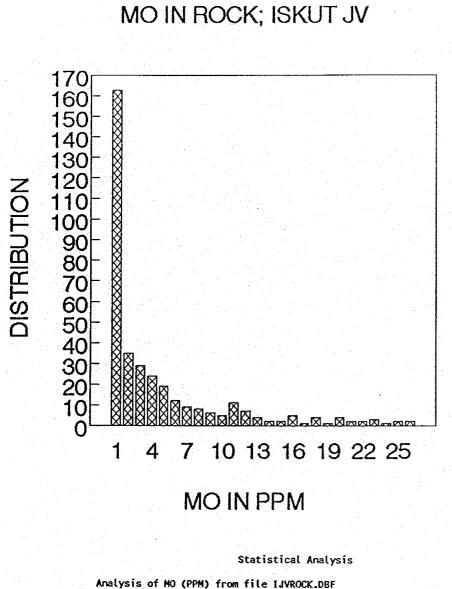
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Statistical Analysis

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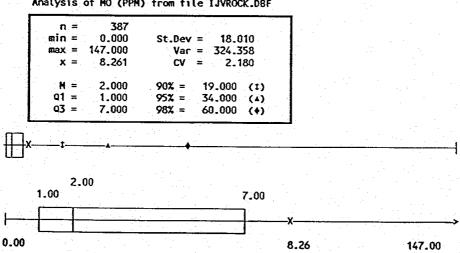
and the second

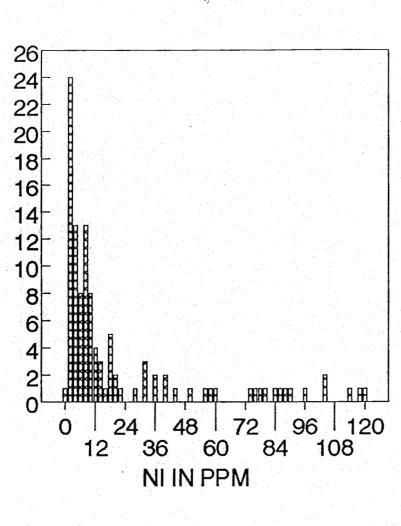
Analysis of MG (PPM) from file IJVROCK.DBF 126 0.000 n = 0.984 0.968 St.Dev = min = max = 4.830 Var = 0.909 1.082 CV Ξ x = 2.470 2.750 2.970 0.680 90% = 95% = (I) (A) M = Q1 = 1.745 03 = 98% = (+) 0.68 1.75 0.23 x 4.83 0.00 1.08



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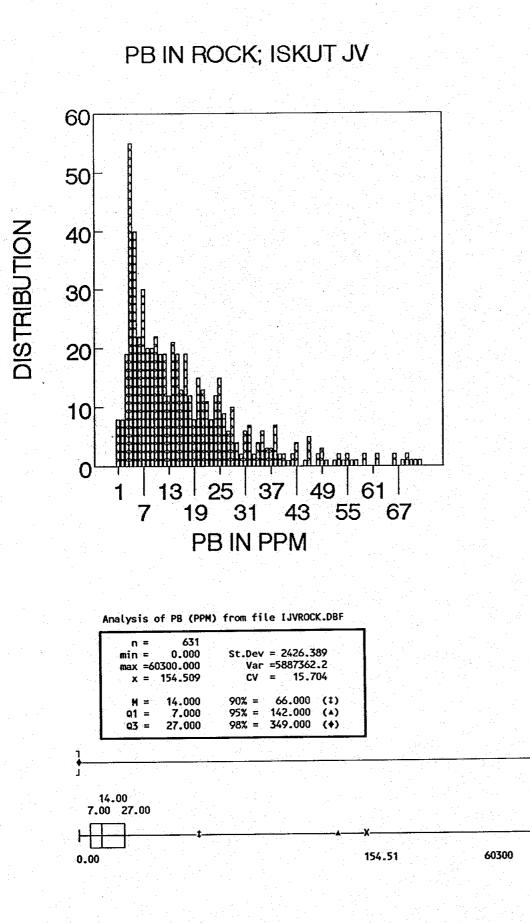


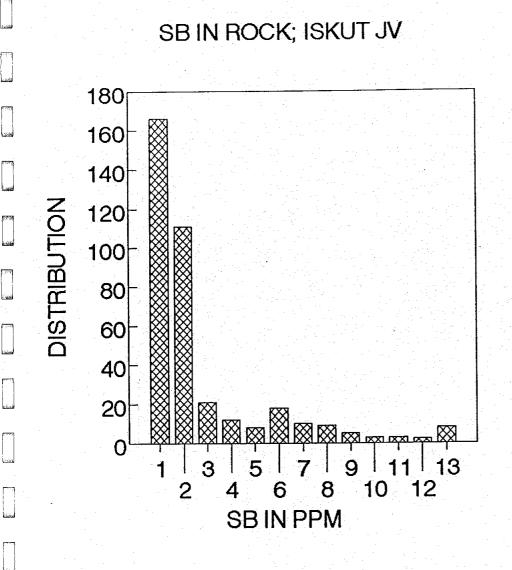
Statistical Analysis

Analysis of NI (PPM) from file IJVROCK.DBF

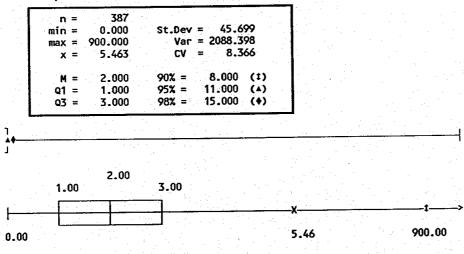
126 n = 0.000 56.383 min = St.Dev = 288.000 Var = 3179.066 max = 1.422 x = 39.659 CV = 90% = 129.000 (1) M = 10.000 95% = 155.000 (A) 98% = 169.000 (\*) 4.000 Q1 = 03 = 53.500 Н 10.00 4.00 53.50 ٠Xŀ 288.00 39.66 0.00

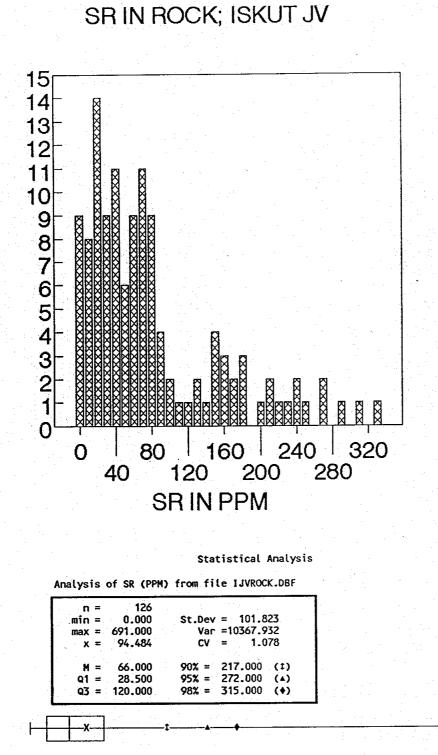
NI IN ROCK; ISKUT JV

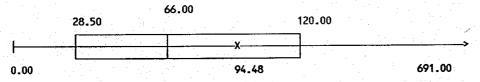




Analysis of SB (PPM) from file IJVROCK.DBF

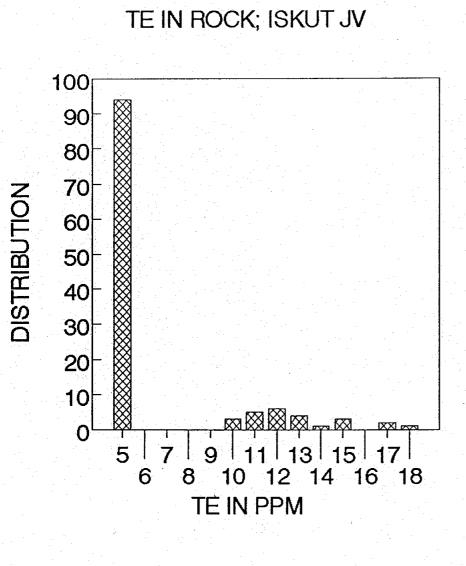


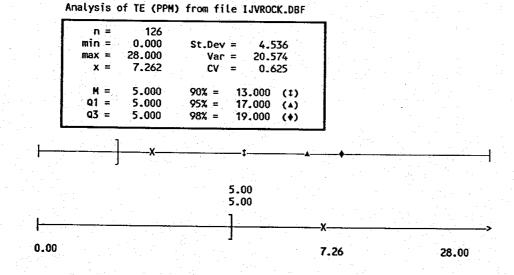


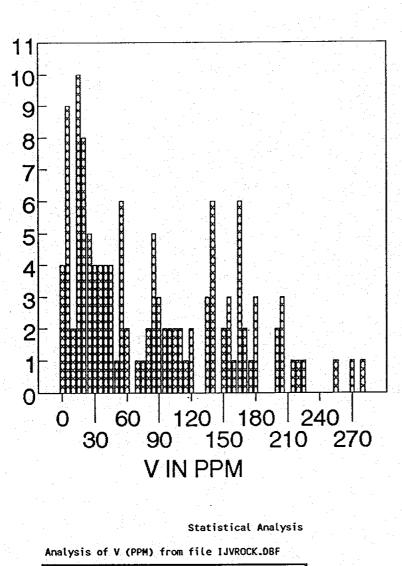


(\*\*\*\*) 1316-1

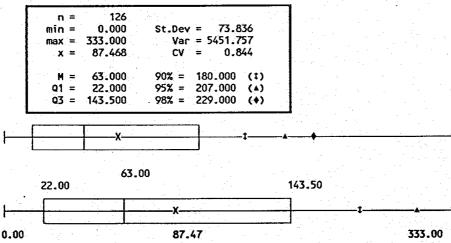
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V IN ROCK; ISKUT JV

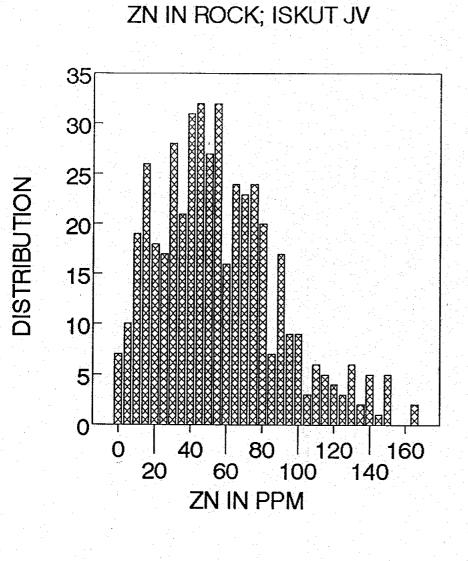
DISTRIBUTION

Statistical Analysis

Analysis of Y (PPM) from file IJVROCK.DBF

			_	x	<b>t</b>	•
			5.00	7.00	9.00	
			- <b></b>	<b></b> ]		
	·				t	
	M = Q1 = Q3 =	7.000 5.000 9.000	95% = 1	0.000 (1) 2.000 (A) 2.000 (A)		
n i n	n = nin = nax = x =	126 0.000 15.000 6.540	St.Dev = Var = CV =	3.251 10.566 0.497		

Y IN ROCK; ISKUT JV



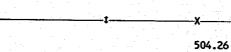
Analysis of ZN (PPM) from file IJVROCK.DBF

$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	$\begin{array}{rll} \min = & 0.000 & \text{St.Dev} = 3400.601 \\ \max = 62000.000 & \text{Var} = 11564089 \\ x = & 504.263 & \text{CV} = & 6.744 \\ \end{array}$ $\begin{array}{rll} \text{M} = & 60.000 & 90\% = & 344.000 & (1) \\ \text{Q1} = & & 37.000 & 95\% = & 1007.000 & (A) \end{array}$			and the second
$\begin{array}{rll} \max = 62000.000 & \text{Var} = 11564089 \\ x = 504.263 & \text{CV} = 6.744 \\ \text{M} = 60.000 & 90\% = 344.000 & (1) \\ \text{Q1} = 37.000 & 95\% = 1007.000 & (A) \end{array}$	$\begin{array}{rll} \max &= 62000.000 & \text{Var} &= 11564089 \\ x &= 504.263 & \text{CV} &= 6.744 \\ \text{M} &= 60.000 & 90\% &= 344.000 & (1) \\ \text{Q1} &= 37.000 & 95\% &= 1007.000 & (A) \end{array}$	n =	548	
	x = $504.263$ CV = $6.744$ M = $60.000$ 90% = $344.000$ (1) Q1 = $37.000$ 95% = $1007.000$ (A)	min =	0.000	St.Dev = 3400.601
M = 60.000 90% = 344.000 (1) Q1 = 37.000 95% = 1007.000 (A)	M = 60.000 90% = 344.000 (1) Q1 = 37.000 95% = 1007.000 (A)	max =6	2000.000	Var = 11564089
Q1 = 37.000 95% = 1007.000 (A)	Q1 = 37.000 95% = 1007.000 (A)	x =	504.263	CV = 6.744
Q1 = 37.000 95% = 1007.000 (A)	Q1 = 37.000 95% = 1007.000 (A)	M. =	60,000	90 <del>1</del> 7 - 3// 000 /+>
		••		
		Q1 =	37.000	95% = 1007.000 (A)

60.00 37.00 100.00

\$▲-

0.00



62000

Analysis of BI (PPM) from file IJVROCK.DBF

126		
0.000	St.Dev =	1.290
14.000	Var =	1.665
2.222	CV =	0.581
2.000	90% =	2,000 (t)
2.000	95% =	2.000 (4)
2.000	98% =	5.000 (+)
	0.000 14.000 2.222 2.000 2.000	0.000 St.Dev = 14.000 Var = 2.222 CV = 2.000 90% = 2.000 95% =

### Analysis of CD (PPM) from file IJVROCK.DBF

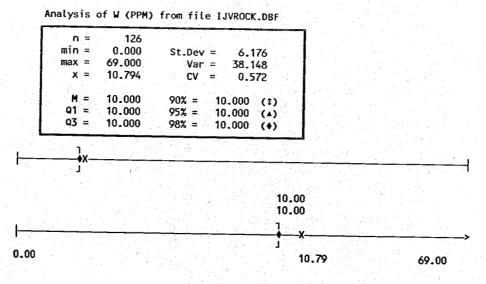
			L	0.62	8.10
· · · ·				<b>X</b>	>
			0.50 0.50		
1 		n an an se Shin			
1 ♦ X				· · · · · · · · · · · · · · · · · · ·	
Q1 = Q3 =	0.500	95% = 98% =	0.500 (A) 0.500 (+)		
M =	0.500	90% =	0.500 (‡)		
max = x =	8.100 0.623		12 2 2 2 NO 4		
min =	0.000				
	max = x = Q1 = Q3 =	min = 0.000 max = 8.100 x = 0.623 M = 0.500 q1 = 0.500 q3 = 0.500	min = 0.000 St.Dev = max = 8.100 Var = x = 0.623 CV = M = 0.500 90% = q1 = 0.500 95% = q3 = 0.500 98% =	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{rcl} \min = & 0.000 & \text{St.Dev} = & 0.900 \\ \max = & 8.100 & \text{Var} = & 0.809 \\ x = & 0.623 & \text{CV} = & 1.444 \\ \\ M = & 0.500 & 90\% = & 0.500 & (1) \\ q1 = & 0.500 & 95\% = & 0.500 & (A) \\ q3 = & 0.500 & 98\% = & 0.500 & (A) \\ \end{array}$

### Statistical Analysis

Analysis of SN (PPM) from file IJVROCK.DBF

n = :	126		
min =	0.000	St.Dev =	0.887
max =	10.000	Var =	0.787
<b>x</b> =.,	9.921	CV =	0.089
M =	10.000	90% = 1	0.000 (t)
Q1 =	10.000	95% = 1	0.000 (4)
Q3 =	10.000	98% = 1	0.000 (+)

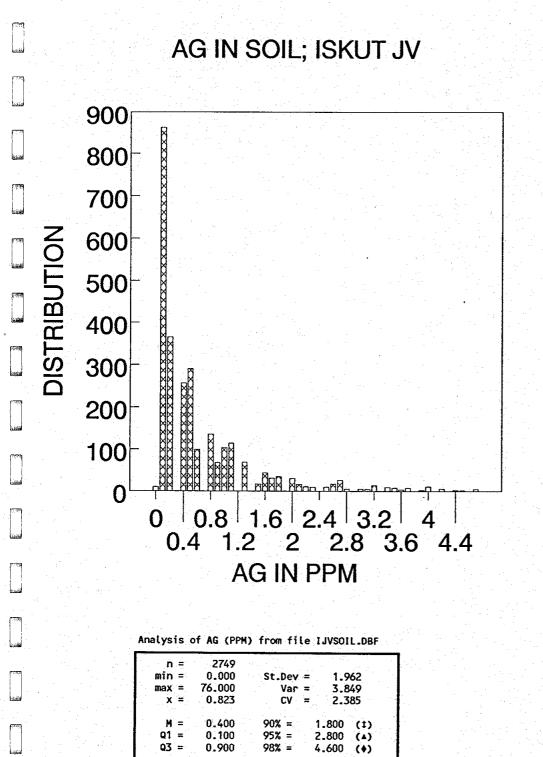
INSUFFICIENT SAMPLE POPULATION FOR MEANINGFUL PLOT



Statistical Analysis

Analysis of MN (PCT) from file IJVROCK.DBF

0.00			249.49		<b>1</b>	1555.0
			<b>X</b>		_	
0.00					466.00	-
<u>L</u>					-	
· · ·	X-			-1		
	M = Q1 = Q3 =	0.000 0.000 466.000	90% = 842.000 95% = 968.000 98% = 1061.000	(4)		againn a' stàiteachainn an stàiteachainn an stàiteachainn an stàiteachainn an stàiteachainn an stàiteachainn a Ar stàiteachainn an stàiteachainn an stàiteachainn an stàiteachainn an stàiteachainn an stàiteachainn an stàitea
		126 0.000 1555.000 249.492	St.Dev = 366. Var =134310 CV = 1.4			



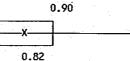
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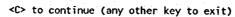
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0.00

0.10

0.40

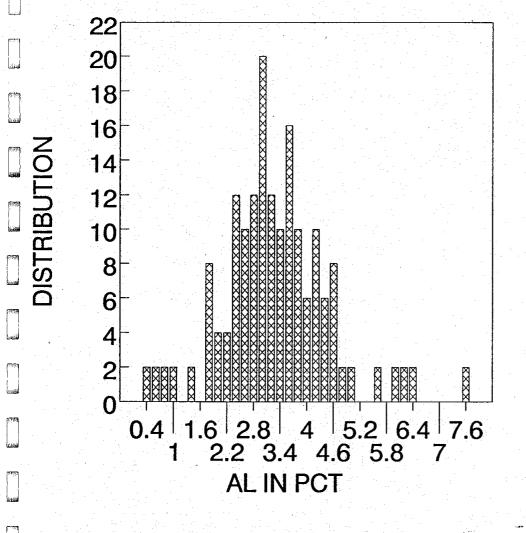




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76.00

### AL IN SOIL; ISKUT JV

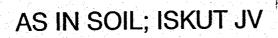


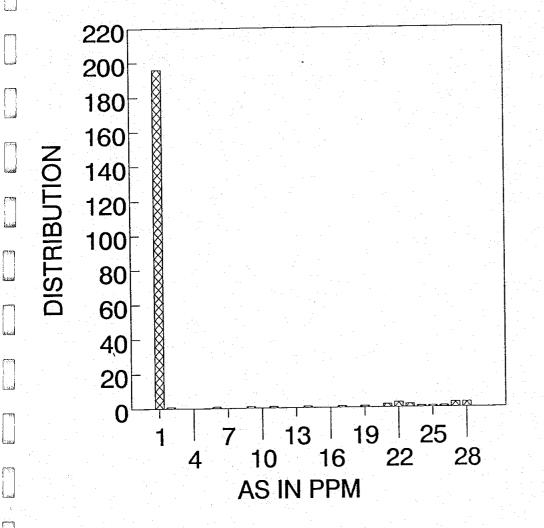
Statistical Analysis

Analysis of AL (PCT) from file IJVSOIL.DBF

0.50	en de la deserva. A la gradia			<b>۱</b>	3.40				7.72	•
					- x		t	▲	<u>.</u>	<b>}</b>
				2.75	3.24	4.00				
ľ.,					] •					1. <b>1</b> .
:					1 .	•				
	Q1 = Q3 =	2.745 3.995	95% = 98% =		.050 (A) .010 (+)					
	H =	3.235	90% =	= 4.	.700 (1)					
	max = x =	7.720 3.400		ar = / =	1.501 0.360	e de la consecue				
	n = ain =	86 0.500 7 700	St.D		1.225					

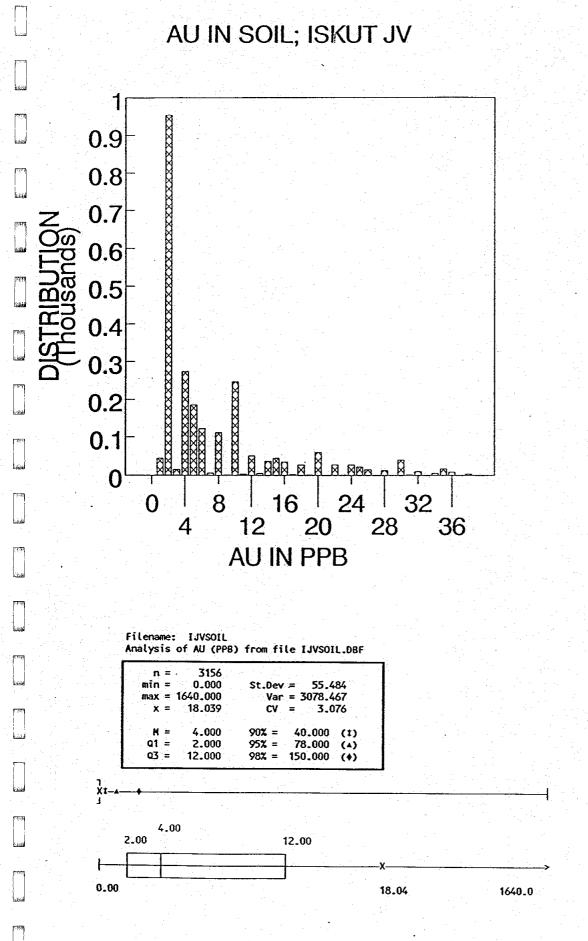
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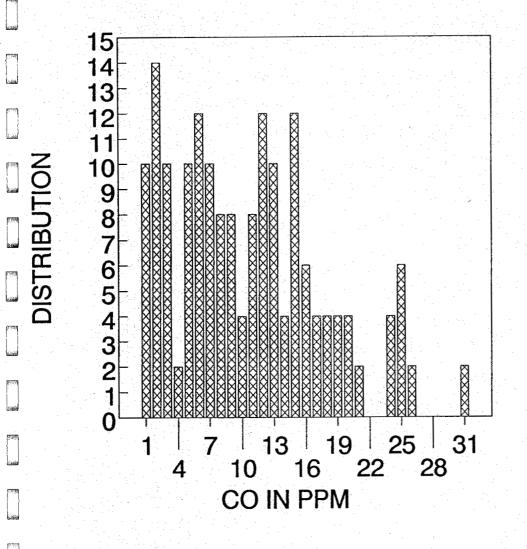


Analysis of AS (PPM) from file IJVSOIL.DBF

1.00	1	12.96	88.00
-		-X	
1.00			26.00
	~		
1	<b></b>	<b>t</b>	
	M = 1.000 Q1 = 1.000 Q3 = 26.000	90% = 45.000 (1) 95% = 51.000 (1) 98% = 61.000 (4)	
	n = 284 min = 1.000 max = 88.000 x = 12.965	St.Dev = 19.983 Var = 399.302 CV = 1.541	



# CO IN SOIL; ISKUT JV

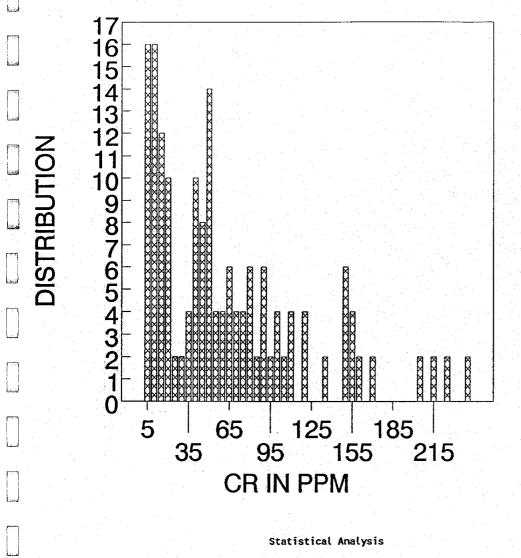


Analysis of CO (PPM) from file IJVSOIL.DBF

1.00	t de la composition de la comp		10	.67				31.00	
1	<u></u>		×-					 	_>
		5.00	10.0	0	15.	00			
	L		<u> </u>	]					
in de la composition La composition de la c	Γ		Y		t		- <u>_</u>		-1
	M Q1 Q3	= 5.000	95% = 2	0.000 (1) 4.000 (A) 5.000 (+)					
	n min max x	= 1.000 = 31.000	St.Dev = Var = CV =	7.002 49.034 0.656					

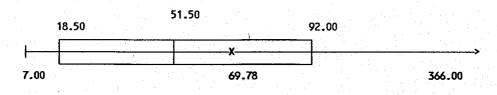
. . .

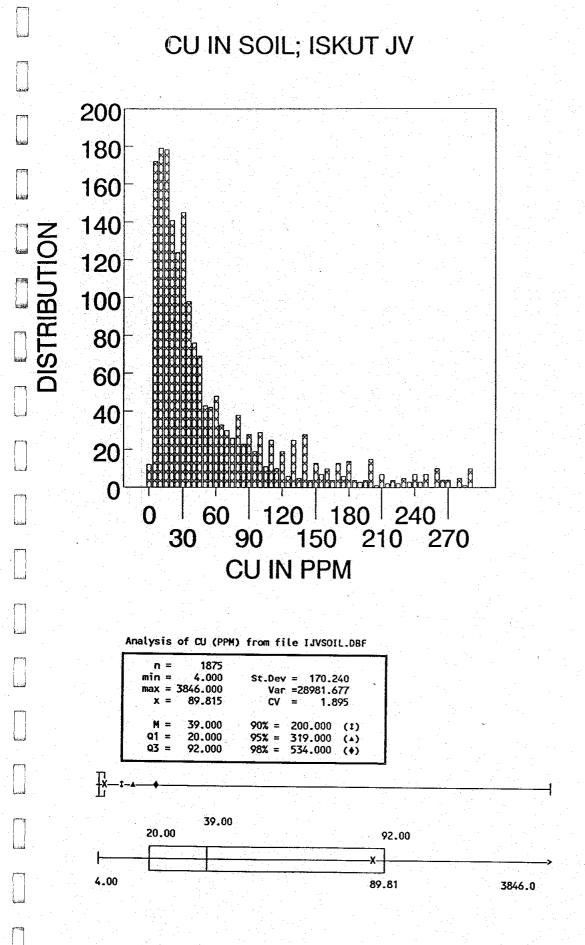
### CR IN SOIL; ISKUT JV

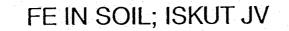


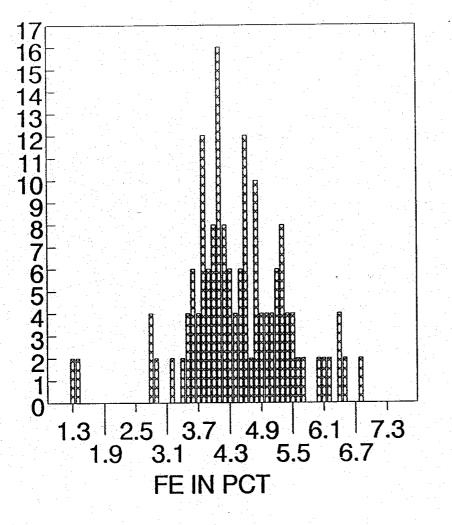
Analysis of CR (PPM) from file IJVSOIL.DBF

n = min =	86 7.000	St.Dev = 64.331
max =	366.000	Var = 4138.498
x =	69.779	CV = 0.922
M =	51.500	90% = 153.000 (1
Q1 =	18.500	95% = 171.000 (4
03 =	92.000	98% = 215.000 (4





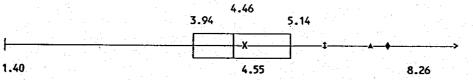


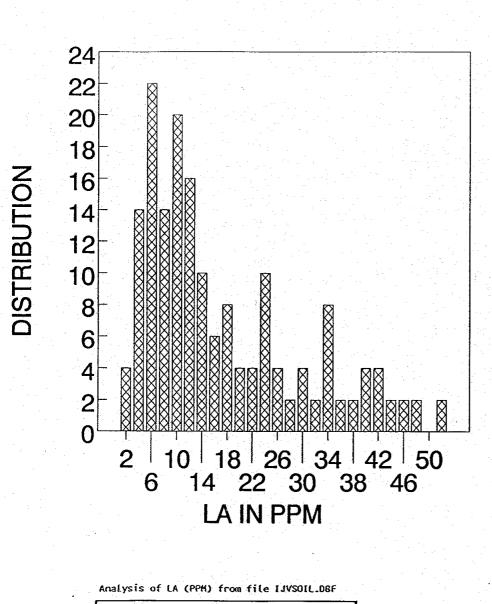


Analysis of FE (PCT) from file IJVSOIL.DBF

DISTRIBUTION

-					
	n	=	86		
	min	=	1.400	St.Dev	= 1.041
1	max	=	8.260	Var	= 1.083
	X	=	4.553	CV	= 0.229
	M	= .	4.460	90% =	5.660 (t)
1	Q1:	= '	3.940	95% =	6.250 (A)
	Q3	E	5.140	98% =	6.430 (+)
					ly t
					<b>^</b>





86

St\_Dev =

CV

90% =

95% =

98% =

Vac =

=

3.000

53.000

17.756

13.000

8.500

24.000

= n = nin

max =

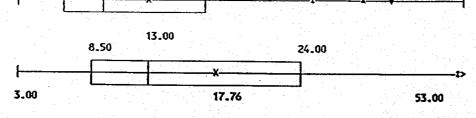
x =

H =

Q1 =

Q3; =

## LA IN SOIL; ISKUT JV



12.457

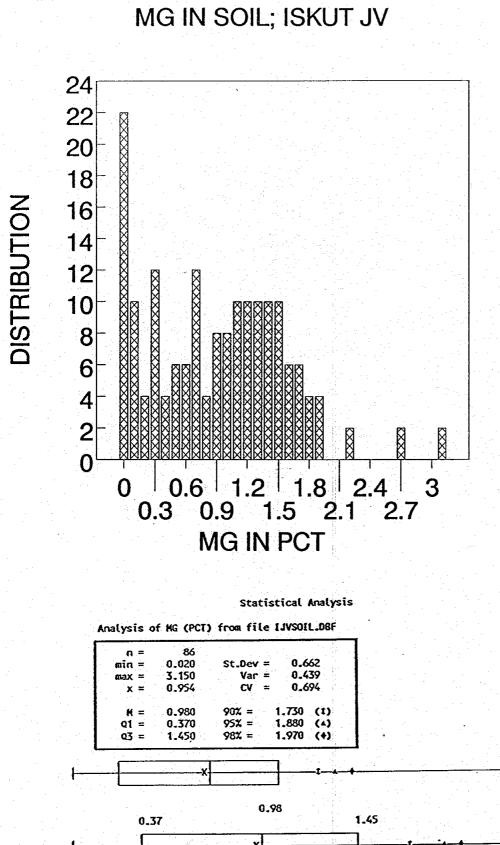
0.702

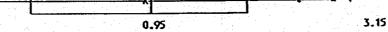
155.185

36.000 (1)

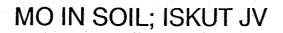
42.000 (4)

45.000 (+)

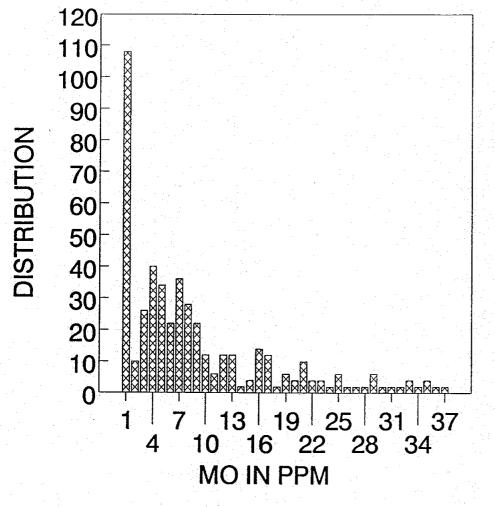




0.02



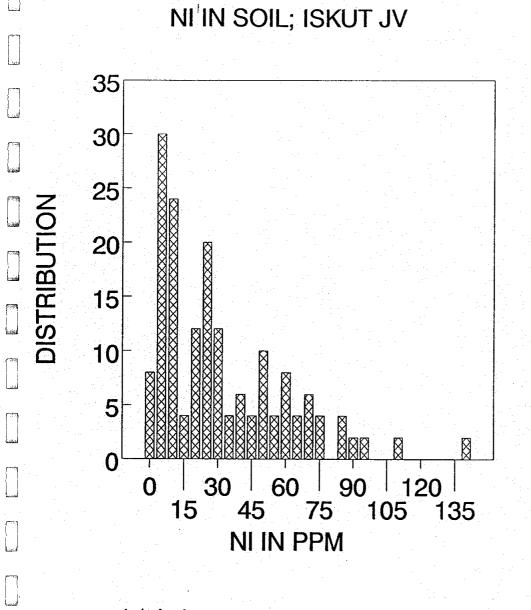
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Analysis of MO (PPM) from file IJVSOIL.DBF

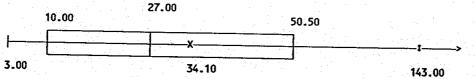
· · · ·					
1	n =	284	the state of the second		
1	min =	1.000	St.Dev = 39.0	001	
	max =	448.000	Var = 1521.0	071	
	x =	21.271	CV = 1.8	34	
1. J.					
1.1	M =	8.000	90% = 50.000	(1)	
. I.	Q1 =	3.000	95% = 80.000	(▲)	
	Q3 =	22.000	98% = 126.000	(+)	
	t	<b>^</b>			
َلْلَا			· · ·		
	·	8.00			
3.	.00			22.00	
· · · <b>г</b>					
		_		x	
Ľ	<u> </u>			]	
1.00				21.27	448.00

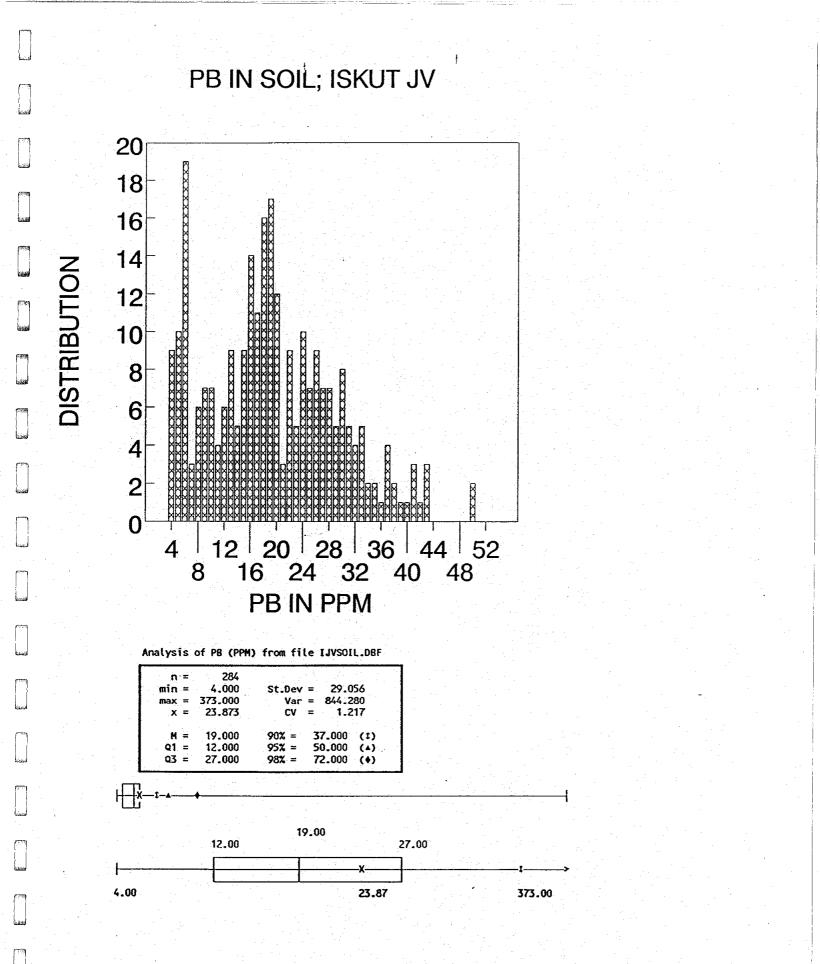


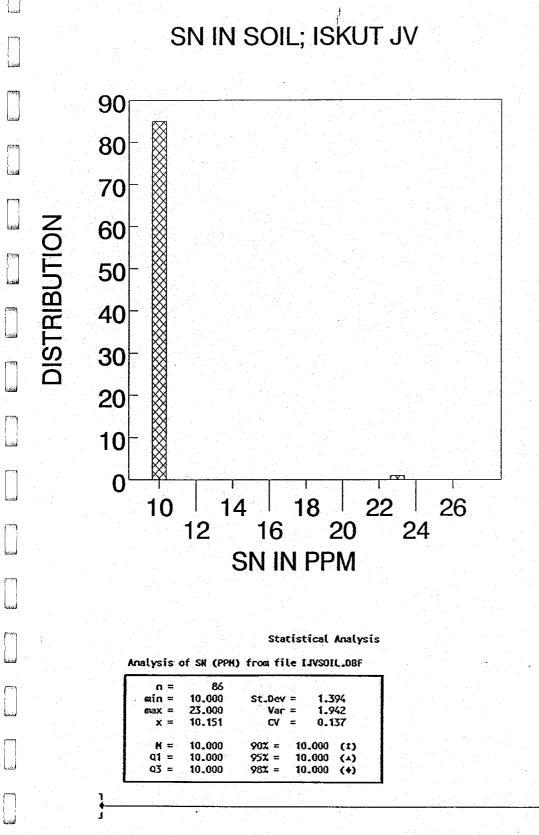


Analysis of NI (PPM) from file IJVSOIL.DBF

x = 34.105	CV = 0.845
M = 27.000 Q1 = 10.000 Q3 = 50.500	90% = 72.000 (t) 95% = 89.000 (A) 98% = 93.000 (A)







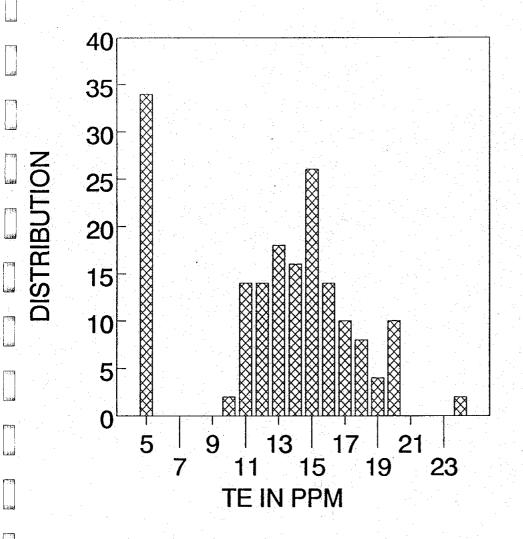
10.00 10.00

J 10.03

10.15

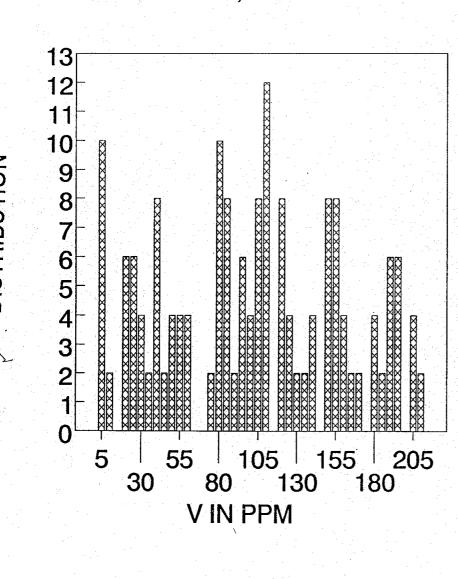
23.00

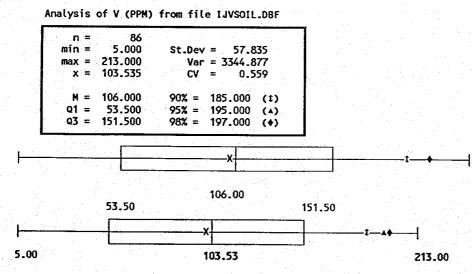
## TE IN SOIL; ISKUT JV



Statistical Analysis

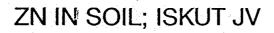
Analysis of TE (PPH) from file IJVSOIL.DBF n = 86 5.000 24.000 min = 4.666 St.Dev = max = Var = 21.772 x = 12.919 CV = 0.361 H = 14.000 90% = 18.000 (1) 95% = 98% = 20.000 (4) Q1 = 11.000 Q3 = 16.000 20.000 -(+) 14.00 11.00 16.00 5.00 12.92 24.00 1

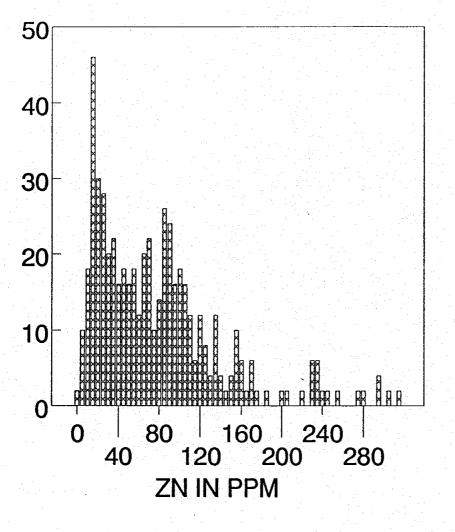




DISTRIBUTION

V IN SOIL; ISKUT JV



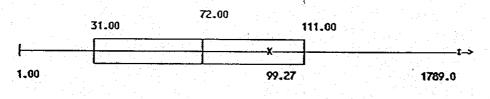


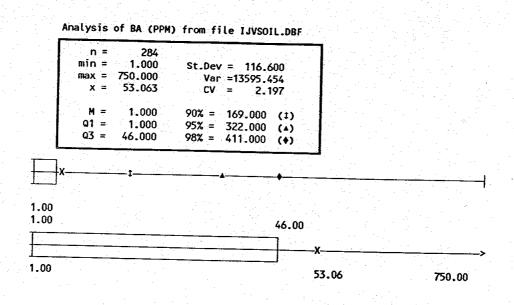
DISTRIBUTION

Statistical Analysis

Analysis of ZN (PPH) from file IJVSOIL.DBF

ณ์เก =	1.000	St.Dev = 143.187 Var =20502.643
	99.275	CV = 1.442
H =	72.000	90% = 172.000 (1)
Q1 =	31.000	95% = 256.000 (1)
- Q3 =	111.000	98% = 364.000 (+)





Analysis of BI (PPH) from file IJVSOIL.DBF

n =	86			
mîn =	5.000	St_Dev =	0.000	
max =	5.000	Var =	0.000	
x =	<b>5.0</b> 00	= V,3	0.000	
H =	5.000	90% =	5.000 (t)	
Q1 =	5.000	95% =	5.000 (4)	
Q3 =	5.000	98% =	5.000 (+)	
4	11 A.		a de la companya de l	1.1

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0.01

	n = min = max = x =	86 0.010 0.610 0.191	St_Dev Var ÇV	= 0.0	158 025 325			
	H = Q1 = Q3 =	0.140 0.070 0.245	90% = 95% = 98% =	0.470 0.480 0.520	(I) (A) (+)			
÷.,		×					 4	 
	0.07		0.14	X	•	0.25	*. •	

0.19

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0.61

Analysis of CD (PPM) from file IJVSOIL.DBF

n = min = max = x =	86 0.500 0.500 0.500	St.Dev = 0.000 Var = 0.000 CV = 0.000
M =	0.500	90% = 0.500 (1)
Q1 =	0.500	95% = 0.500 (A)
Q3 =	0.500	98% = 0.500 (A)

bises

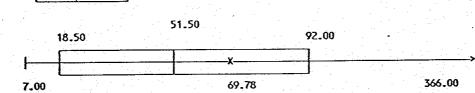
INSUFFICIENT SAMPLE POPULATION FOR MEANINGFUL PLOT

- - -

Analysis of CR (PPH) from file IJVSOIL.DBF

n =	86	
៣៣ =	7.000	$St_Dev = 64.331$
max =	366.000	Var = 4138.498
x =	69.779	CV = 0.922
K =	51.500	90% = 153.000 (1)
· 01 =	18.500	95% = 171.000 (*)
Q3 =	92.000	98% = 215.000 (+)

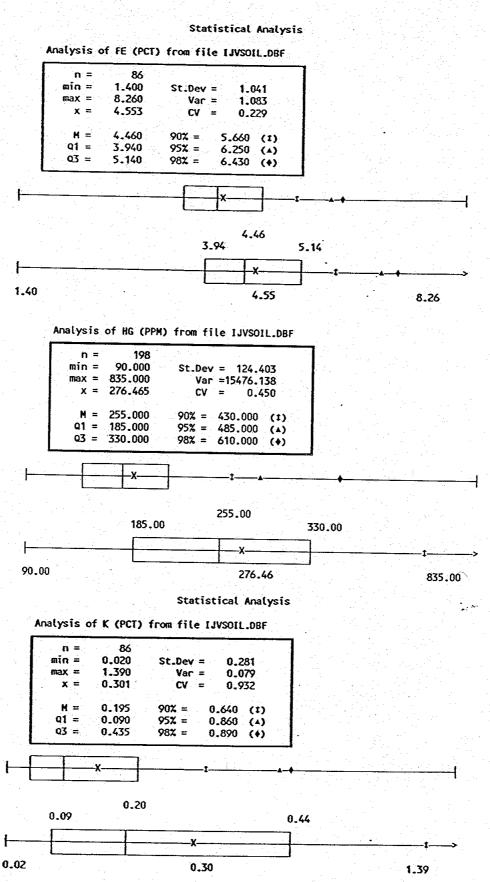
H



Analysis of CU (PPM) from file IJVSOIL.DBF

	n = 1875 min = 4.000 max = 3846.000 x = 89.815	Var =	= 170.240 =28981.677		
	x = 89.815 M = 39.000 Q1 = 20.000 Q3 = 92.000	95% = 3	= 1.895 200.000 (1) 319.000 (4) 34.000 (+)		
י קר עו					
Ľ.				92.00	

4.00 89.81 3846.0

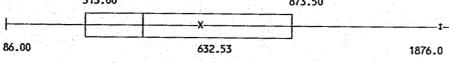


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	1 =	483.500 313.000 873.500	È.	95% = 1		(1) (A) (+)			
ma		86.000 1876.000 632.535 465.500		Var CV	= 442.0 =195408. = 0.6	.88 599			

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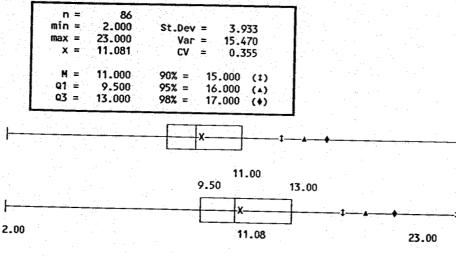
Statistical Analysis

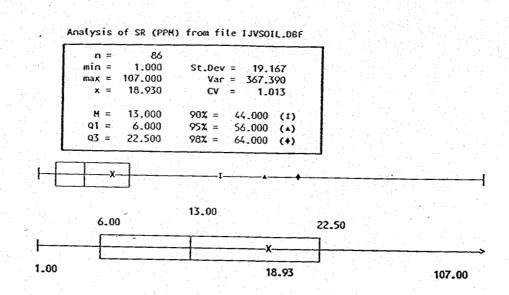
Analysis of NA (PCT) from file IJVSOIL.DBF 86 'n = 0.019 min = 0.010 St.Dev = 0.160 max = Var = CV = x = 0.033 0.568 0.030 90% = 0.050 (1) K = Q1 = 0.020 95% = 0.060 (4) Q3 = 0.040 98% = 0.060 (+) 0.03 0.02 0.04 ł X 0.01 0.03

0.16

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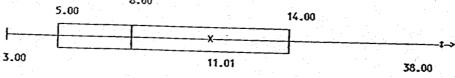
Analysis of SB (PPM) from file IJVSOIL.DBF





Analysis of W (PPH) from file IJVSOIL\_DBF n = 86 min = 10.000 St.Dev = 1.394 max = 23.000 Var = 1.942 x = 10.151 CV = 0.137 M = 10.000 10.000 (1) 10.000 (1) 90% = Q1 = 10.000 95% = Q3 = 10.000 10.000 (+) 98% = 10.00 10.00 10.00 10.15 23.00 Statistical Analysis

Analysis of Y (PPH) from file IJVSOIL.DBF n = 86 min = 3.000 St.Dev = 7.937 max = 38,000 Var = 62.988 x = 11-012 CV = 0.721 H = 8.000 90% = 20.000 (1) Q1 = 5.000 95% = 28.000 (1) Q3 = 14.000 98% = 31.000 (+) -¥. 8.00



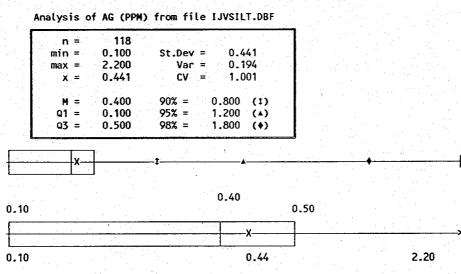
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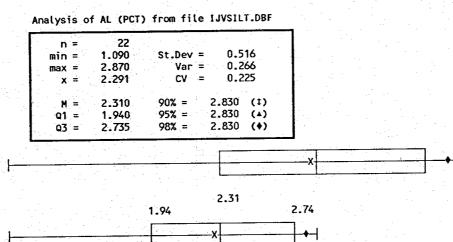
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Statistical Analysis



2.87

20.18

92.00

Statistical Analysis

2.29

Analysis of AS (PPM) from file IJVSILT.DBF

			1.001		
n = min = max = x =	92.000	St.Dev = 26.4 Var = 701.1 CV = 1.3	49		
M = Q1 = Q3 =	2.000	90% =       54.000         95% =       63.000         98% =       63.000			
	—x				
2.00	8.00	13.00		· · · · · · · · · · · · · · · · · · ·	· · ·
			x		 

2.00

1.09

Analysis of AU (PPB) from file IJVSILT.DBF

 nax =	118 2.000 1700.000 53.398	St.Dev = 178.673 Var =31923.952 CV = 3.346
м =	3.500	90% = 120.000 (t)
Q1 =	2.000	95% = 254.000 (A)
Q3 =	22.500	98% = 300.000 (+)

3.50 2.00 22.50 Γ 2.00 53.40 1700.0

Statistical Analysis

Analysis of BA (PPM) from file IJVSILT.DBF

Γ	n =	22				
	min =	122.000	St.Dev = 90	.601		
	max =	407.000	Var = 8208	.581		
- 14 - E	x =	248.682	CV = 0	.364		
	M =	249.000	90% = 328.000	0 (1)	•	
. · · ·	01 =	147.000	95% = 328.000			e e tra
	Q3 =	320.000	98% = 328.000			
L						
1 · · ·		in a sub- San ta ta ta sub-	<u>I</u>	<u> </u>	<b>-</b>	
			<u>X</u>			
			249.00			
	147.00			320	0.00	
1			<b>V</b>			
			~		, <u> </u>	
122.00		an a	248.68		n in the The annual second	407.0

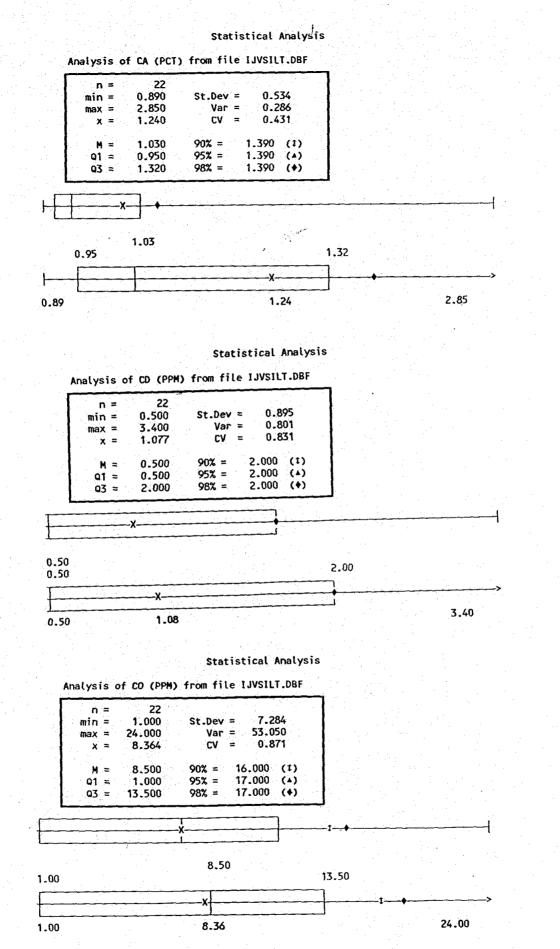
248.68

Statistical Analysis

407.00

Analysis of BI (PPM) from file IJVSILT.DBF n = 22 Dev = 29.180 Var = 851.471 min = 2.000 St.Dev = 92.000 max = 24.273 ·x = CV = 1.202 90% = 63.000 (1) M = 5.000 01 = 2.000 95% = 66.000 (1) Q3 = 43.500 66.000 (+) 98% = Х 5.00

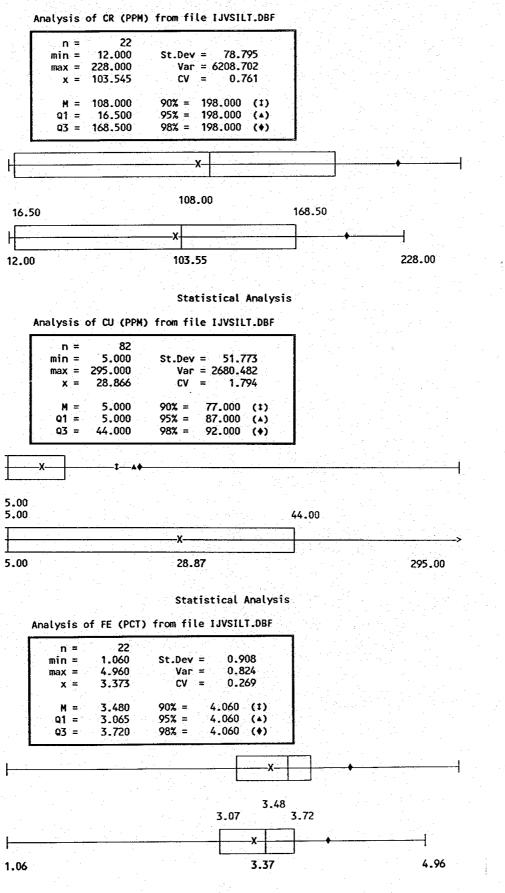


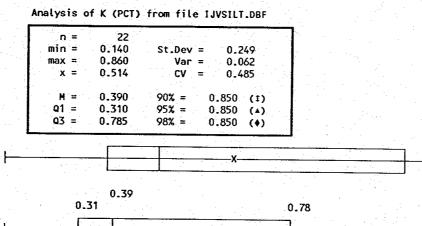


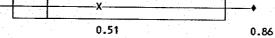
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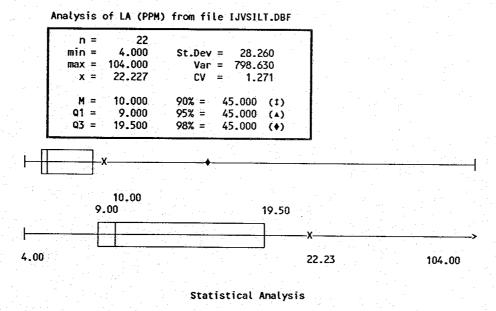




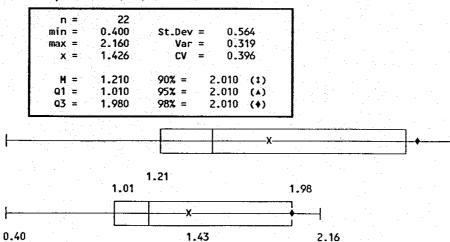
0.14

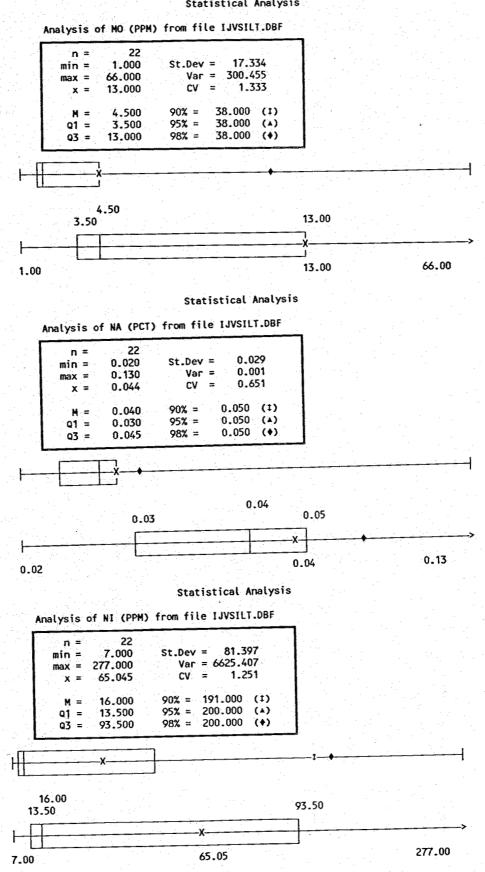
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Statistical Analysis



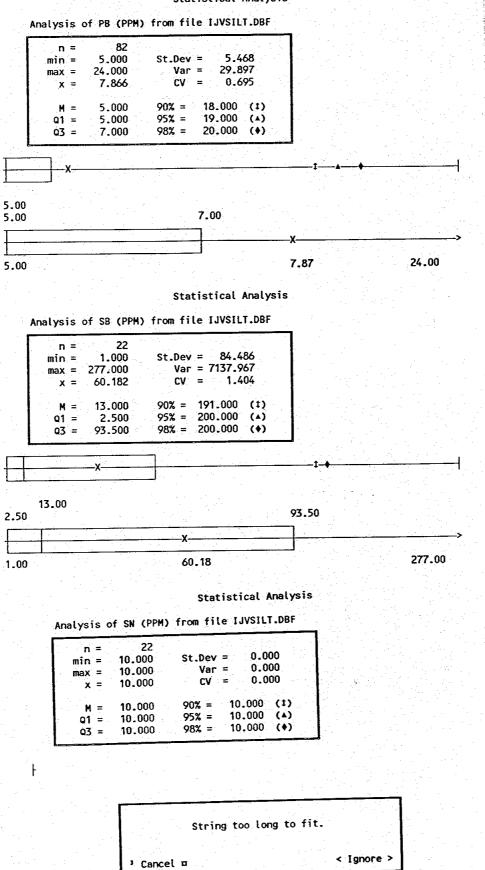
Analysis of MG (PCT) from file IJVSILT.DBF

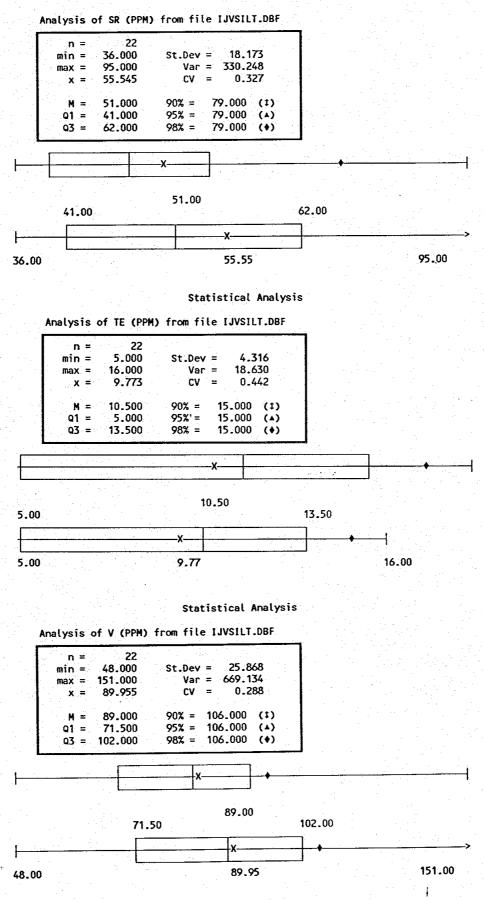


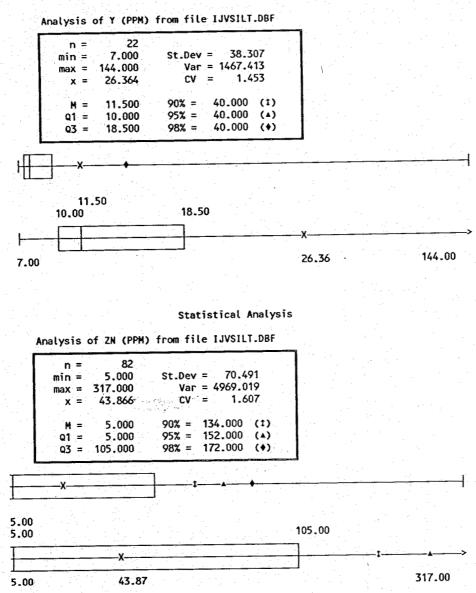


6.58

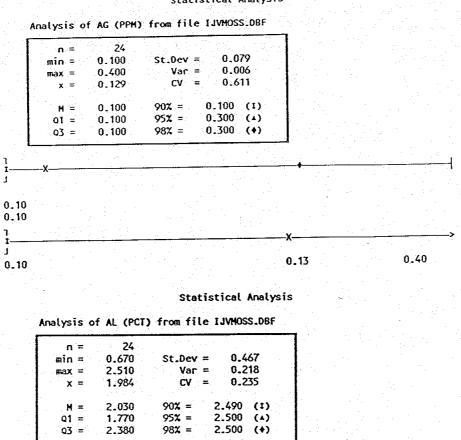
Line a



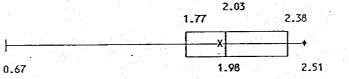




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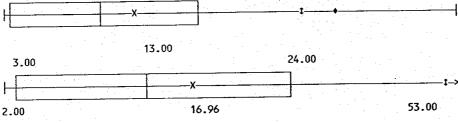


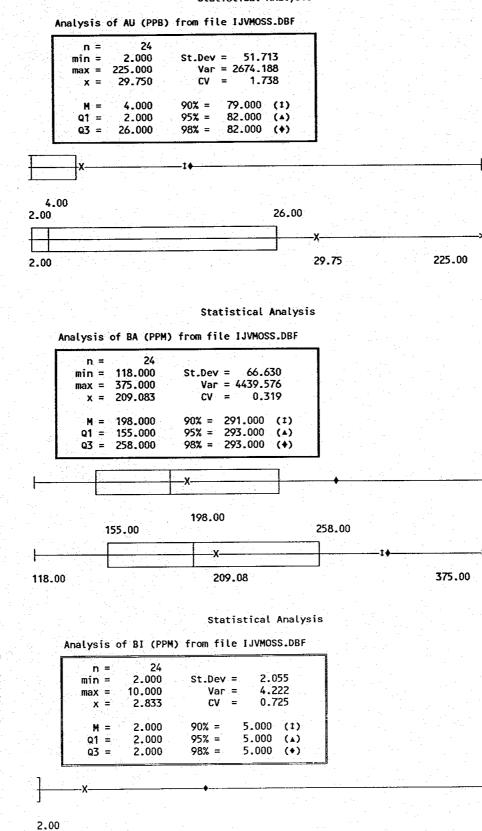




Analysis of AS (PPM) from file IJVMOSS.DBF

n =	24			
min =	2.000	St.Dev	= 14.3	95
max =	53.000	Var	= 207.2	
x =	16.958	ĊV	= 0.8	49
M =	13.000	90% =	36.000	(1)
01 =	3.000	95% =	40.000	(4):
03 =	24.000	98% =	40.000	(+)





2.00

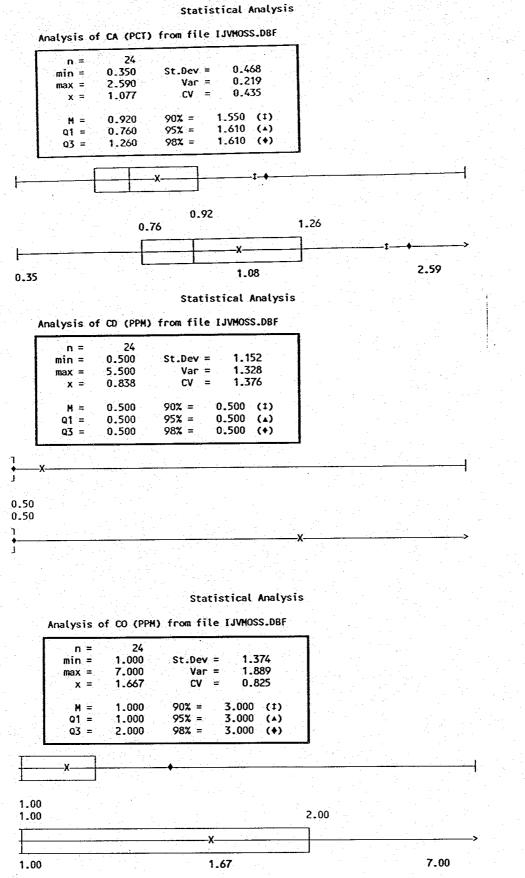
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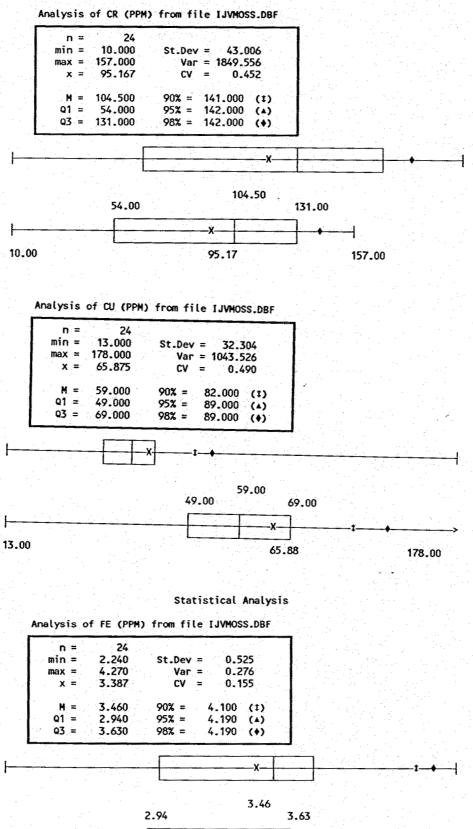
2.83

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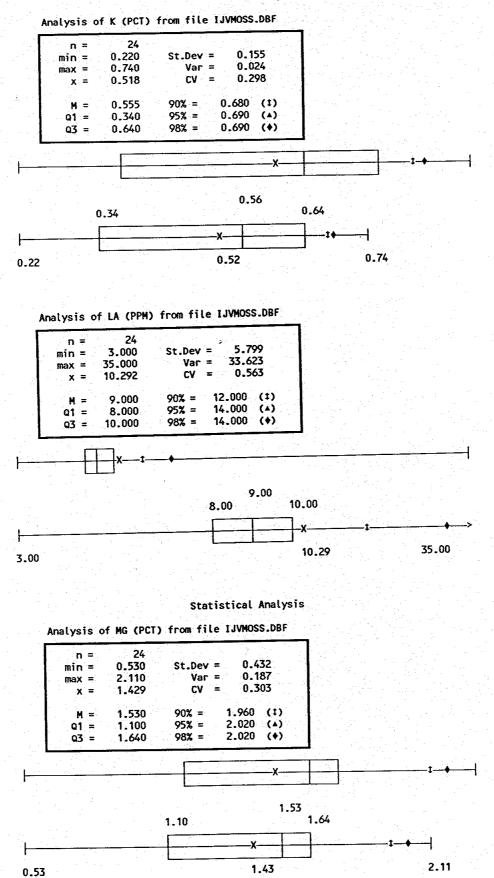
ł X-2.24 3.39 4.27

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ie iang

1.00

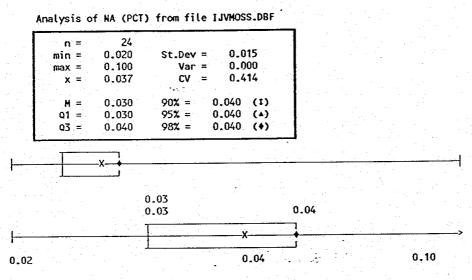
.



n =	24	Net al la second		
៣ាំភ =	1.000	St.Dev =		
max =	7.000	Var =	- 1.889	<b>)</b>
x =	1.667	CV. =	= 0.825	5
M =	1.000	90% =	3.000	(1)
Q1 =	1.000	95% =	3.000	(*)
Q3 =	2.000	98% =	3.000	(+)

1.00 1.00							2.00	F			
1	 · · · · · · · · · · · · · · · · · · ·	1	 ·	Y			1		1. 	 	
	 		 N			- 1 -	 				
1.00				1.0	67					7	.00

Statistical Analysis



Statistical Analysis

Analysis of NI (PPM) from file IJVMOSS.DBF 24 ηΞ St.Dev = 73.046 7.000 min = Var = 5335.667 max = 269.000 0.667 CÝ = x = 109.500 90% = 196.000 (1) M = 121.500 95% = 214.000 (A) 98% = 214.000 (\*) q1 = <u>38.000</u> Q3 = 152.000 ł 121.50 152.00 38.00 X-269.00 109.50 7.00

÷.,

	֥ .	= 0.3	64			· · · · ·
11.125 $CV = 0.364$ 10.000 90% = 15.000 (1) 8.000 95% = 16.000 (A) 12.000 98% = 16.000 (*) 10.00 8.00 12.00 11.13 23.00 Statistical Analysis						
1	<b>x</b>	10.00	_ <b>1</b> ∳	12.00		
$n = 24$ $min = 5.000  \text{St.Dev} = 4.045$ $max = 23.000  \text{Var} = 16.359$ $x = 11.125  \text{CV} = 0.364$ $M = 10.000  90\% = 15.000  (1)$ $q1 = 8.000  95\% = 16.000  (4)$ $q3 = 12.000  98\% = 16.000  (*)$ $10.00$ $8.00 \qquad 12.00$ $5.00 \qquad 11.13 \qquad 23.00$	-1+>					
		11.13	-		23.00	
	8.000 12.000	8.000 95% = 12.000 98% = X 8.00	8.000 95% = 16.000 12.000 98% = 16.000 	$\begin{array}{c} 8.000 \\ 95\% = 16.000 \\ (4) \\ 12.000 \\ 98\% = 16.000 \\ (+) \\ \hline \\ \hline \\ \\ \hline \\ \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ $	$\begin{array}{c} 8.000 & 95\% = & 16.000 & (A) \\ 12.000 & 98\% = & 16.000 & (*) \\ \hline \\ $	$\begin{array}{c} 8.000 & 95\% = & 16.000 & (\texttt{A}) \\ 12.000 & 98\% = & 16.000 & (\texttt{A}) \\ \hline \\ $

	n =	24			
	min =	2.000	St.Dev	= 7.4	50
	max =	37.000	Уаг	= 55.4	98
	x =	4.792	CV	= 1.5	55
	M =	2.000	90% =	8.000	(1)
Ł	Q1 =	2.000	95% =	10.000	(▲)
1	Q3 =	2.000	98% =	10.000	(+)

2.00 2.00

2.00

L.B.Ks

4.79

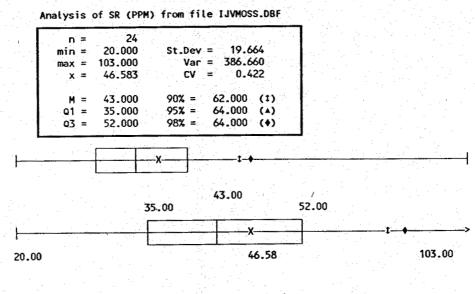
37.00

Statistical Analysis

Analysis of SN (PPM) from file IJVMOSS.DBF

n =	24			
min =	10.000	St.Dev	= 0.0	00
max =	10.000	Var	= 0.0	00
x =	10.000	CV	= 0.0	00
M =	10.000	90% =	10.000	(1)
Q1 =	10.000	95% =	10.000	:(A)
Q3 =	10.000	98% =	10.000	(+)

	String t	oo long	to fit.		
<sup>3</sup> Cancel ¤		•		< ignore	>



### Statistical Analysis

Analysis of TE (PPM) from file IJVMOSS.DBF 24 n '= 3.304 5.000 St.Dev = min = Var = 15.000 10.915 max = CV = 0.512 6.458 x = 90% = 12.000 (t) 95% = 13.000 (A) 98% = 13.000 (\*) 5.000 M = Q1 = 5.000 5.000 03 = ] 5.00 5.00 ] 15.00 6.46 5.00 Statistical Analysis Analysis of V (PPM) from file IJVMOSS.DBF

n = 24 St.Dev = 19.702 55.000 min = Var = 388.165 max = 126.000CV = 0.221 89.208 x = 90% = 109.000 (1) 86.500 M. = 95% = 117.000 (4) 70.000 Q1 = Q3 = 103.000 98% = 117.000 (\*) X 86.50 103.00 70.00 126.00 89.21 55.00

Analysis of W (PPM) from file IJVMOSS.DBF

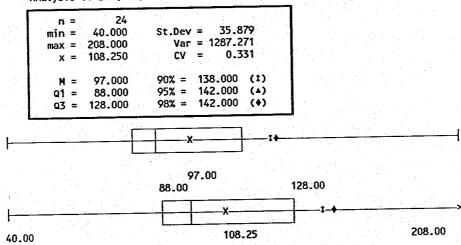
n =	24				
ุฒโก =	10.000	St.Dev =	0.0	00	
max =	10.000	Var =	0.0	00	
x =	10.000	CV =	0.0	00	
- ₩ == -	10.000	90% =	10.000	*(1)	
01 =	10.000	95% =	10.000	. (▲)	
Q3 =	10,000	98% =	10.000	(+)	

String too long to fit.	
<sup>3</sup> Cancel ¤	< Ignore >

### Statistical Analysis

Analysis of ZN (PPM) from file IJVMOSS.DBF

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## APPENDIX E

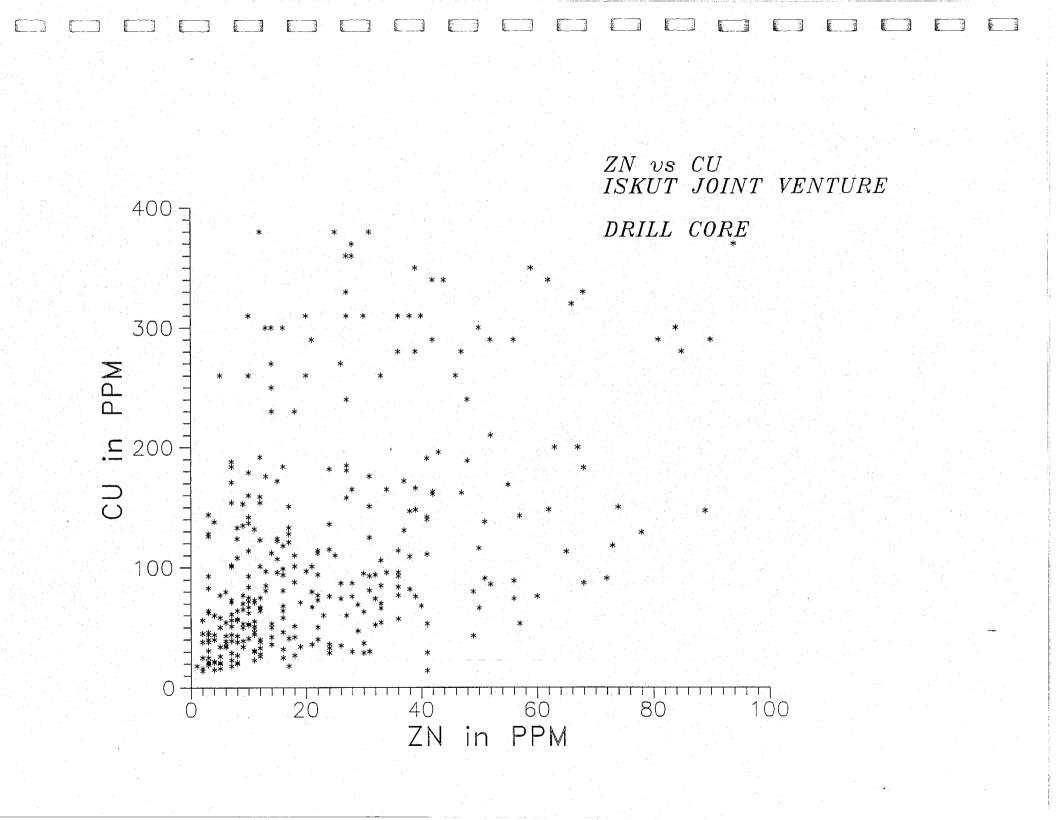
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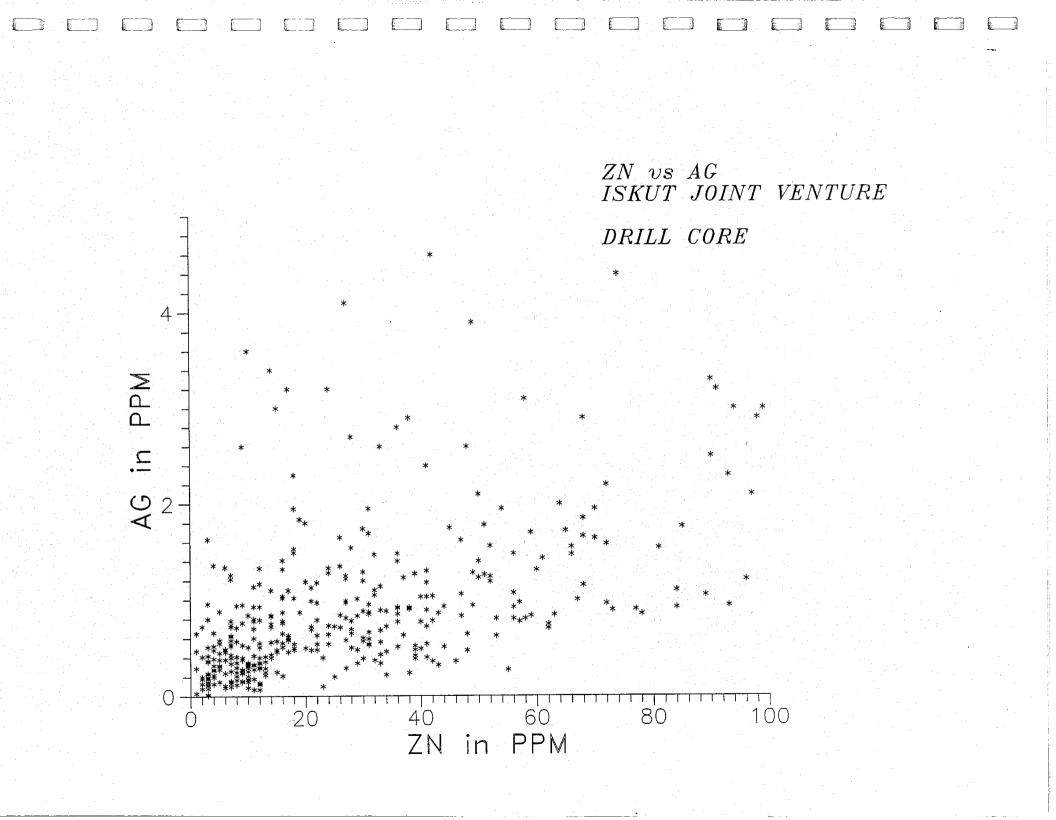
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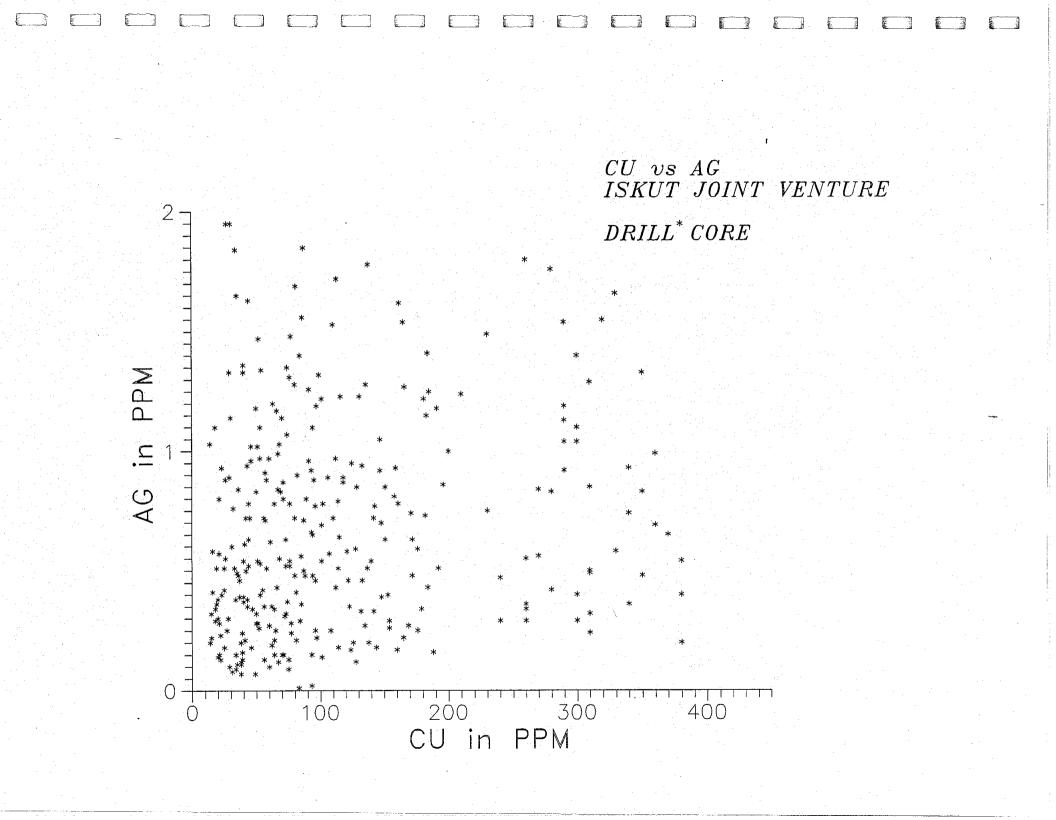
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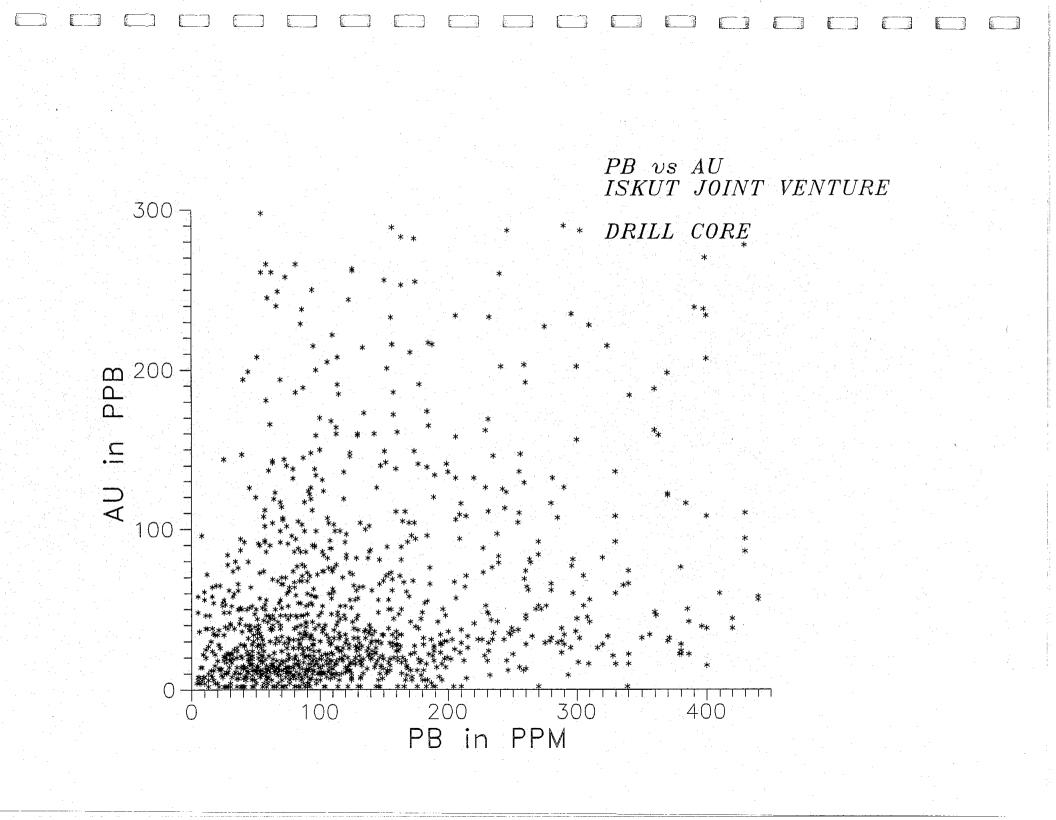
### **BIVARIATE STATISTICS**

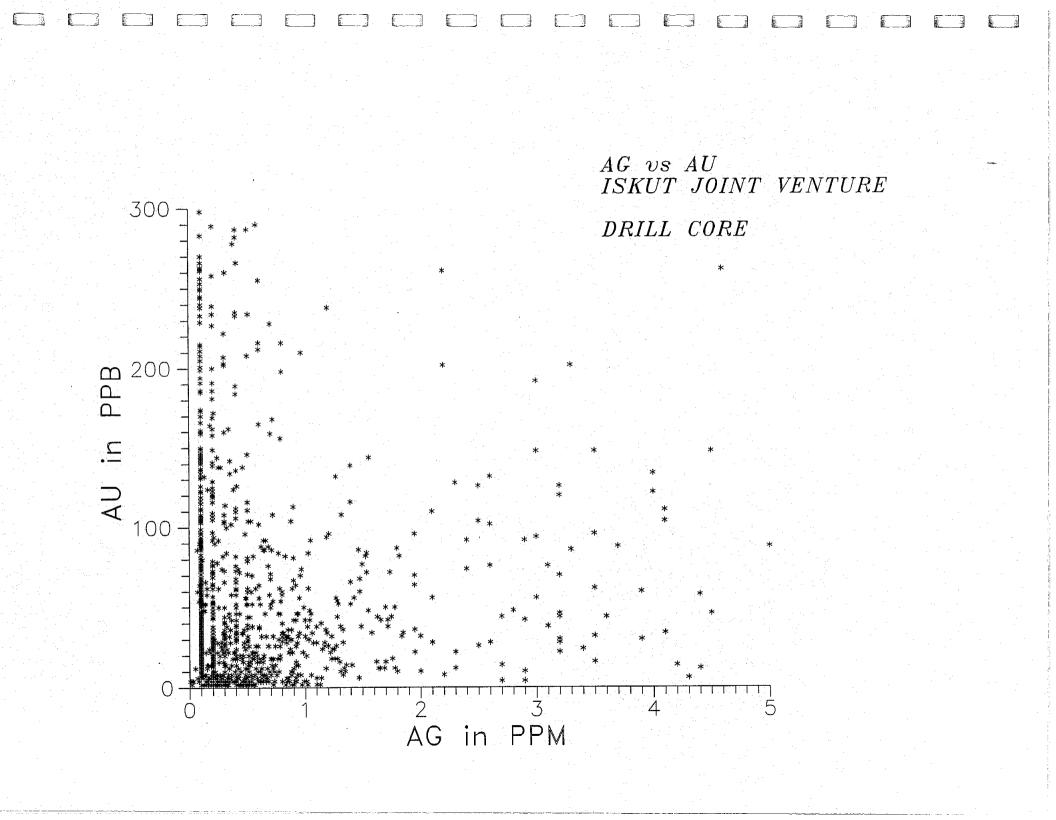
	И	ORMAL N	7S LN D	STRIBUTI	***************************************	EARSON PEARMAN	
		AU	AG	<u></u> CU	PB	ZN	AS
				NORMAL DI	STRIBUTION		
	AU		0.246 0.172	0.243 0.002	0.251 0.417	0.073 0.143	0.035 0.263
	AG	0.179 0.172		0.220 0.451	0.261 0.418	0.686 0.681	0.104 0.177
•	CU	0.077	0.457 0.448		0.158 0.318	0.338 0.681	****
	PB	0.406 0.416	0.379 0.417	0.315 0.314		0.148 0.244	0.022 -0.055
	ZN	0.153 0.140	0.684 0.680	0.707 0.679	0.272 0.241		**** ****
	AS	0.286 0.263	0.201 0.177	**** ****	-0.073 -0.057	**** ****	











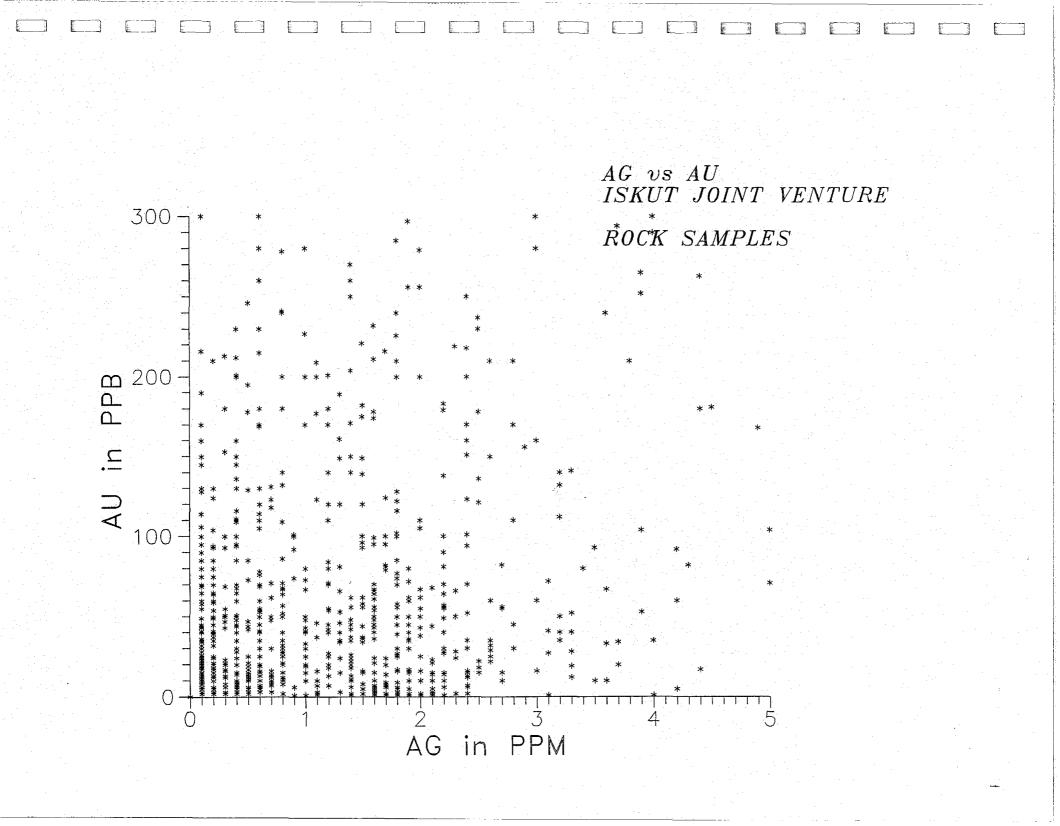
# CORRELATION COEFFICIENTS FOR ROCKS' ISKUT JOINT VENTURE PROPERTY

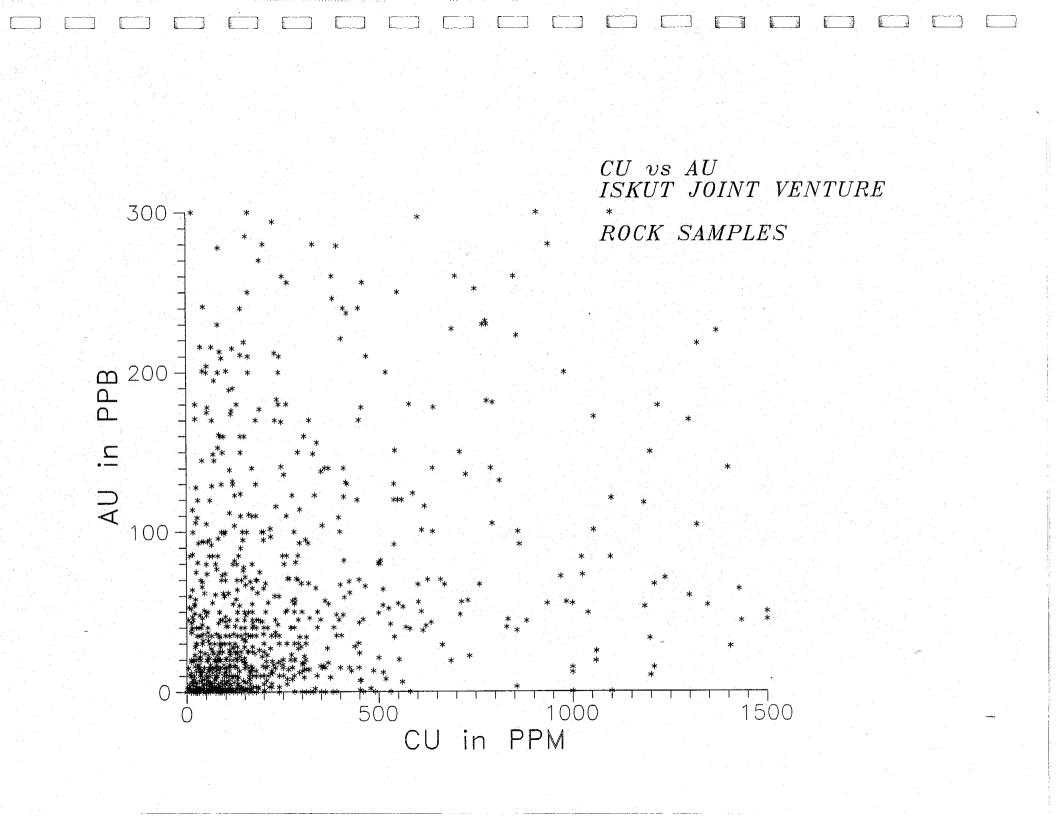
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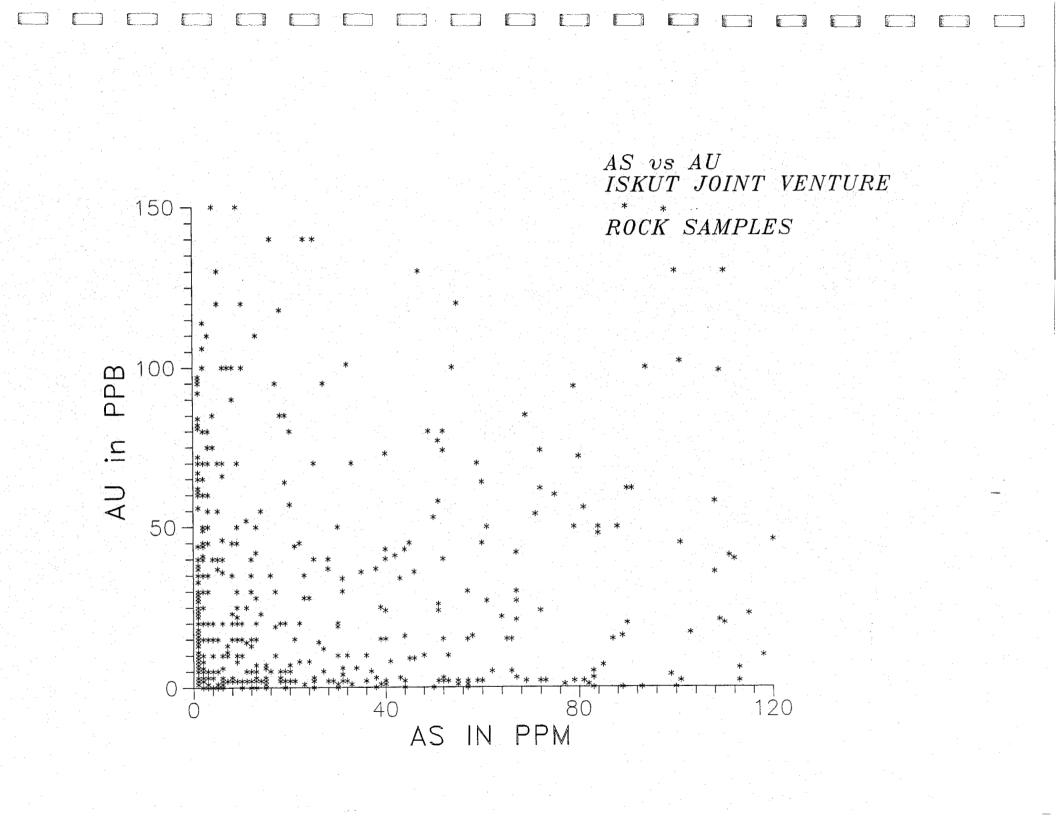
**R** 22

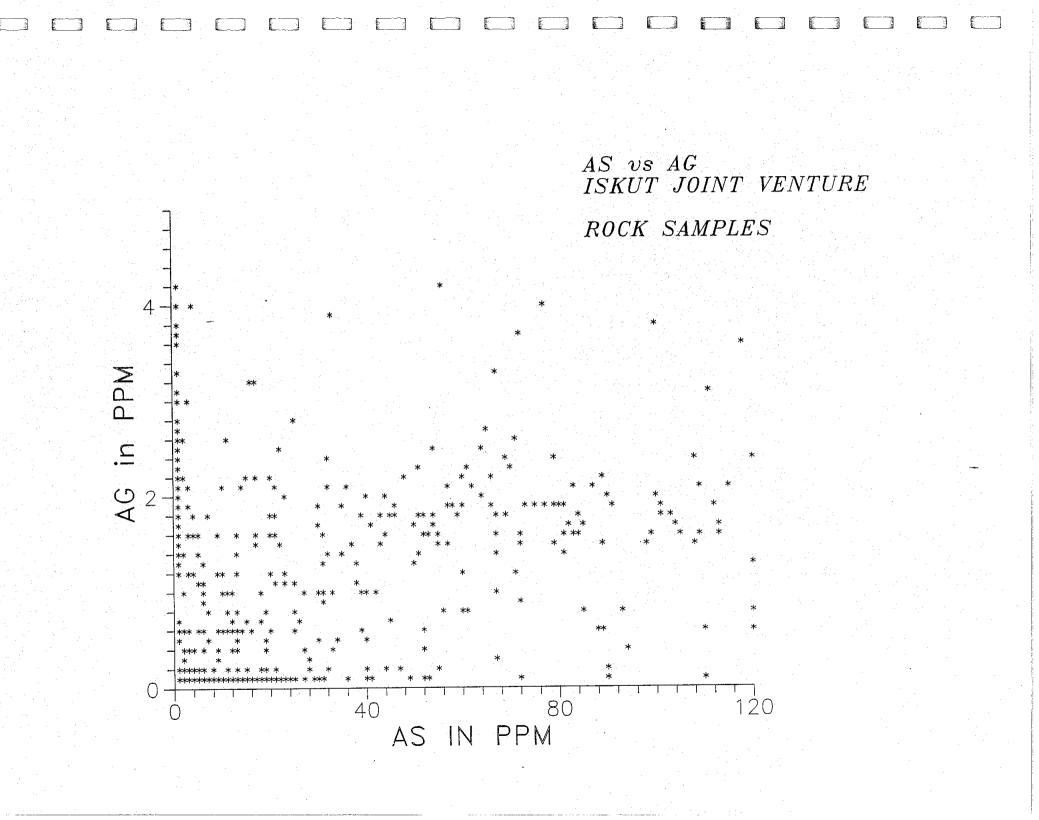
**1** 

	<u></u>	<del></del>							VS LN DIST			LRSON ARMAN							
		AU	AG	CU	PB	<u>ZN</u>	AS	мо	NI	CO	CD DISTRIBUTIO	SB	FE	TE	CR	v	MG	ĸ	S
AU		$\backslash$	0.399 0.696	0.290 0.655	0.041 0.329	0.192 0.144	0.283 0.451	0.020 0.093	0.036 0.133	-0.003 0.211	0.009 0.243	0.014 0.189	-0.045 0.141	0.415 0.133			-0.066 -0.022	-0.055 0.003	-
AG		0.639 0.694		0.658 0.645	0.550 0.529	0.307 0.425	0.277 0.515	0.073 0.066	-0.067 0.007	-0.007 0.193	0.033 0.286	0.033 0.081	0.069 0.189	-0.049 0.000	0.021 0.168	-0.034 -0.031	-0.053 -0.059	-0.127 -0.080	
CU		0.646 0.663	0.653 0.644		0.004 0.173	0.046 0.173	0.200 0.339	0.083 0.258	-0.023 0.360	0.169 0.624	-0.022 0.002	0.029 0.173	0.137 0.595	-0.041 0.240	0.106 0.153		0.017 0.448	0.023 0.442	
PB		0.324 0.328	0.554 0.528	0.207 0.172		0.336 0.663	0.131 0.533	-0.020 0.077	0.017 0.241	0.036 0.304	0.835 0.415	0.013 0.367	0.133 0.295	-0.048 0.223	-0.043 -0.026	-0.022 0.204	0.042 0.188	0.008 0.140	-
ZN		0.217 0.142	0.429 0.423	0.265 0.170	0.651 0.662		0.024 0.265	-0.049 -0.140	0.112 0.366	0.128 0.599	0.887 0.298	0.000 0.193	0.236 0.715	0.044 0.278	-0.080 -0.206	0.158 0.734	0.172 0.704	0.173 0.712	_
AS		0.448 0.525	0,415 0.515	0.299 0.362	0.519 0.532	0.228 0.262		-0.026 0.035	0.104 0.408	0.122 0.349	0.145 0.312	0.016 0.296	0.050 0.197	0.022 0.443	-0.042 0.125	-0.024 0.183	0.021 0.236	-0.035 0.196	
мо		0.118 0.091	0.122 0.063	0.234 0.256	0.203 0.075	-0.047 -0.144	0.203 0.033		-0.016 -0.048	0.011 0.061	-0.042 -0.043	-0.003 0.118	0.051 0.085	-0.087 0.011	0.009 0.055	-0.047 0.014	-0.071 -0.101	-0.029 0.031	-
NI		0.187 0.128	0.030 0.000	0.389 0.352	0.238 0.233	0.352 0.357	0.357 0.403	-0.060 -0.055		0.415 0.540	0.008 0.043	0.285 0.271	0.299 0.362	0.272 0.301	0.602 0.562	0.284 0.405	0.725 0.703	0.395 0.439	_
co		0.204 0.205	0.176 0.187	0.605 0.617	0.380 0.294	0.640 0.592	0.355 0.342	0.061 0.053	0.602 0.535		-0.007 0.023	0.176 0.256	0.742 0.780	0.236 0.292	0.029 0.003	0.610 0.731	0.562 0.684	0.538 0.630	
CD	LN_	0.203 0.235	0.218 0.280	-0.037 -0.036	0.527 0.402	0.424 0.272	0.274 0.301	-0,053 -0.066	0.061 0.018	0.024 0.011		0.138 0.180	0.065 0.082	-0.063 -0.045	0.036 0.027	-0.054 -0.024	0.012 0.050	0.003 0.056	-
SB		0.081 0.187	-0.106 0.079	0.088 0.170	0.287 0.366	0.158 0.190	0.365 0.294	0.204 0.117	0.199 0.266	0.235 0.249	0.082 0.165		0.205 0.232	0.646 0.712	0.132 0.108	0.313 0.311	0.258 0.256	0.267 0.263	
FE		0.151 0.133	0.189 0.181	0.541 0.586	0.430 0.283	0.716 0.708	0.225 0.187	0.154 0.075	0.389 0.353	0.830 0.776	0.064 0.042	0.217 0.222		0.311 0.304	-0.112 -0.126	0.778 0.849	0.685 0.754	0.740 0.784	
TE		0.111 0.129	-0.073 -0.005	0.188 0.232	0.124 0.216	0.269 0.270	0.285 0.439	-0.008 0.006	0.350 0.296	0.361 0.285	-0.084 -0.068	0.568 0.710	0.349 0.296		0.164 0.127	0.457 0.426	0.425 0.382	0.448 0.403	(
CR		0.155 0.126	0.150 0.160	0.159 0.136	-0.133 -0.044	-0.263 -0.232	0.122 0.114	0.107 0.045	0.509 0.557	-0.078 -0.016	0.017 -0.013	0.083 0.097	-0.170 -0.151	0.069 0.118		-0.102 -0.129	0.276 0.120	-0.007 -0.045	
v		-0.037 -0.060	0.000 -0.041	0.491 0.507	0.296 0.192	0.697 0.729	0.199 0.173	0.071 0.003	0.442 0.397	0.796 0.727	-0.016 -0.065	0.235 0.303	0.889 0.846	0.395 0.421	-0.162 -0.153		0.737 0.841	0.818 0.847	(
мg		-0.063 -0.030	-0.092 -0.069	0.377 0.438	0.281 0.176	0.725 0.699	0.205 0.227	-0.120 -0.112	0.631 0.700	0.759 0.679	0.059 0.015	0.175 0.248	0.784 0.749	0.384 0.376	-0.053 0.102	0.885 0.838		0.807 0.853	
К		-0.017 -0.005	-0.045 -0.090	0.380 0.432	0.325 0.127	0.670 0.707	0.268 0.187	0.182 0.022	0.309 0.432	0.657 0.624	0.062 0.021	0.217 0.256	3 0.807 0.780	0.343 0.397	0.118 0.065	0.836 0.844	0.763 0.851		(
SR		-0.151 -0.174	-0.108 -0.120	0.197 0.178	0.295 0.058	0.389 0.210	0.348 0.246	0.105 0.037	0.083 0.065	0.403	0.009 0.056	0.126 0.140	0.445 0.215	0.110 0.133	-0.299	0.561	0.484	0.556	









CU vs AG ISKUT JOINT VENTURE

\*\* ROCK SAMPLES

ानग

600

- 1 -

800

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400

CU in PPM

200

\*

4

3

PPM

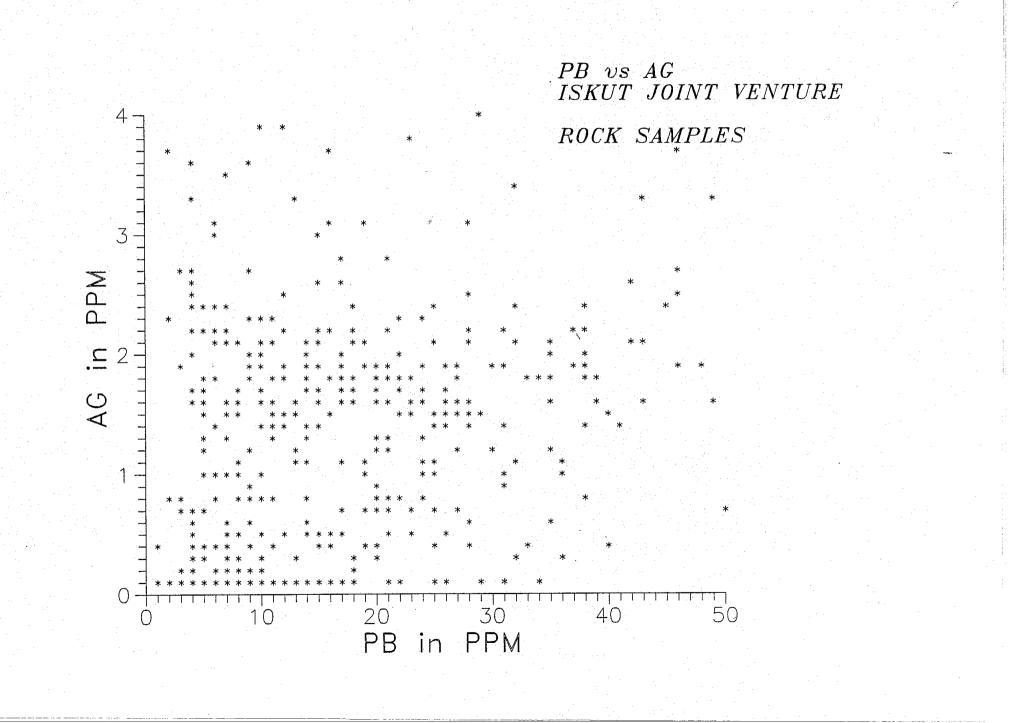
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AG

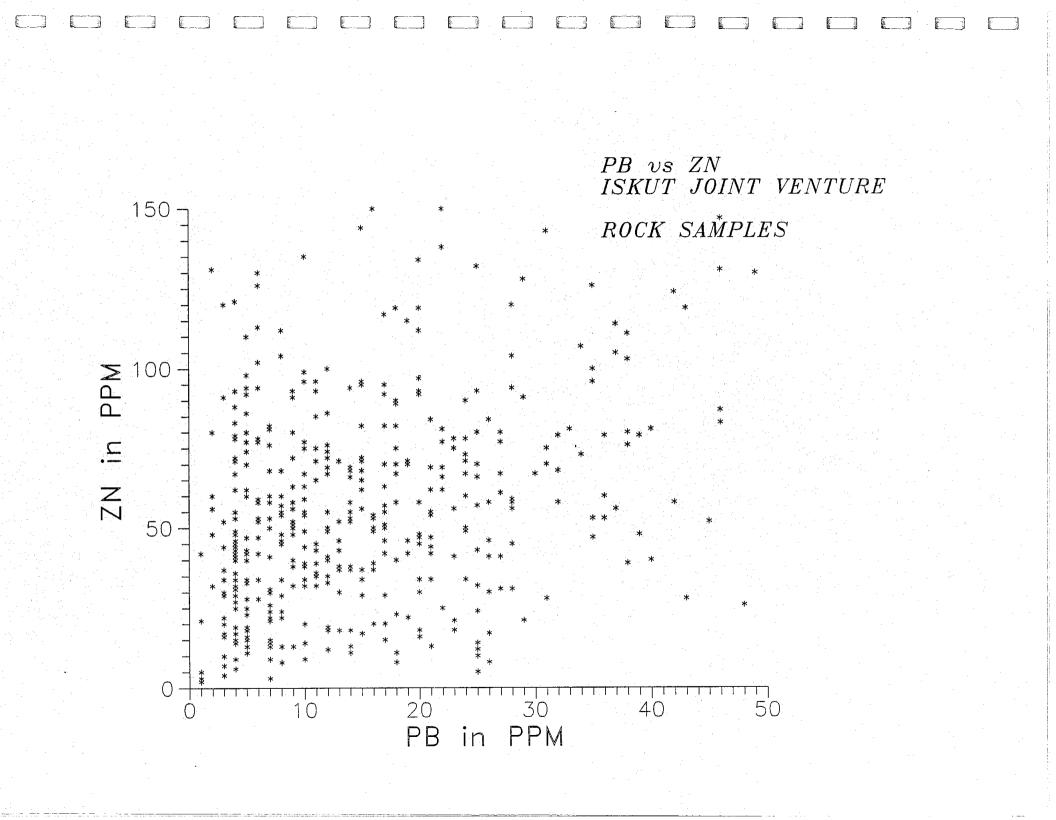
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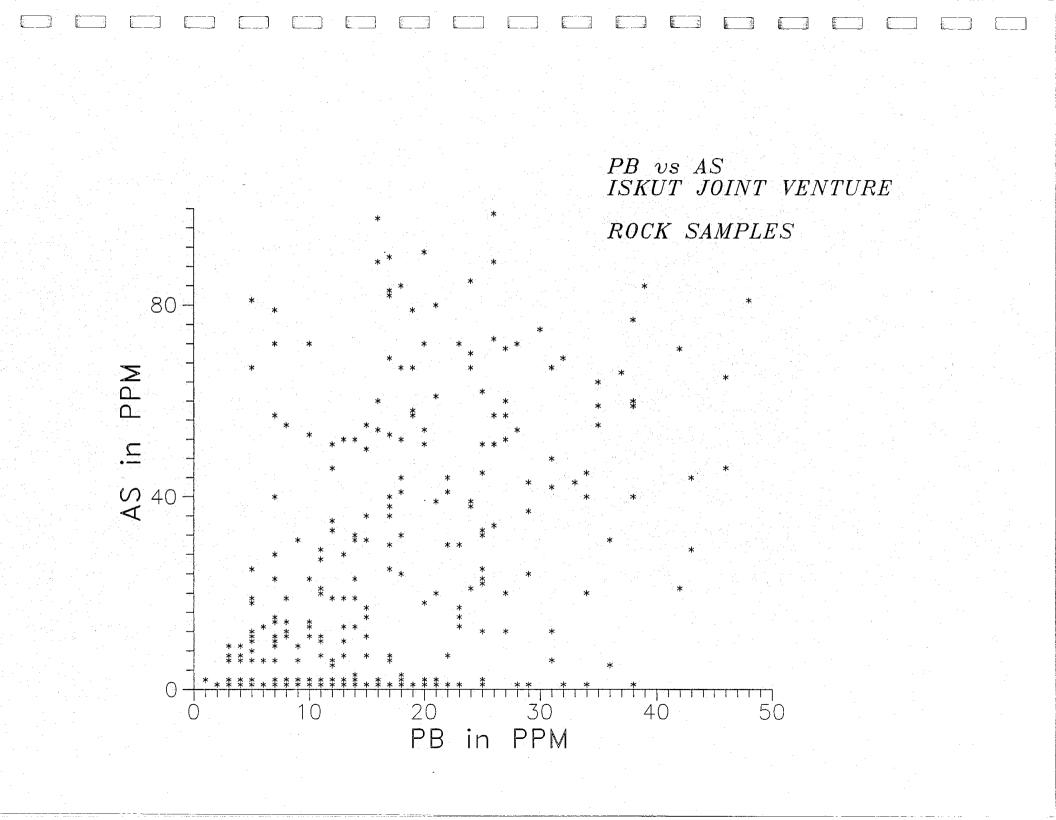
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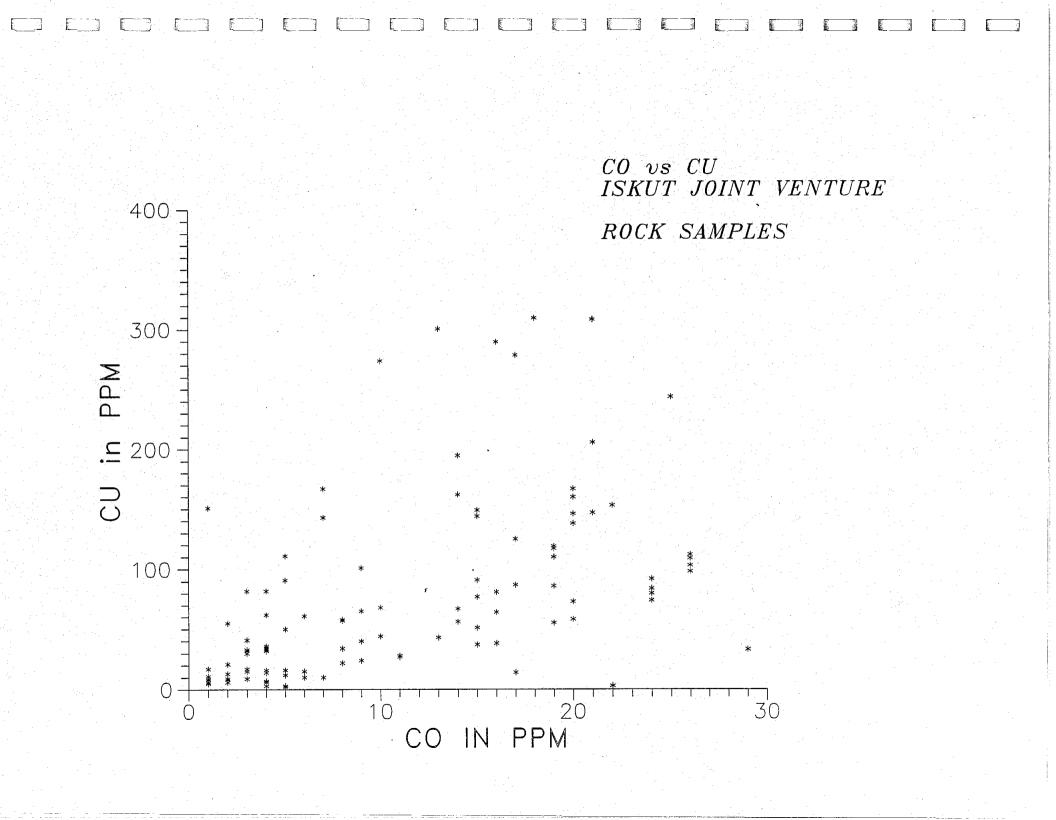
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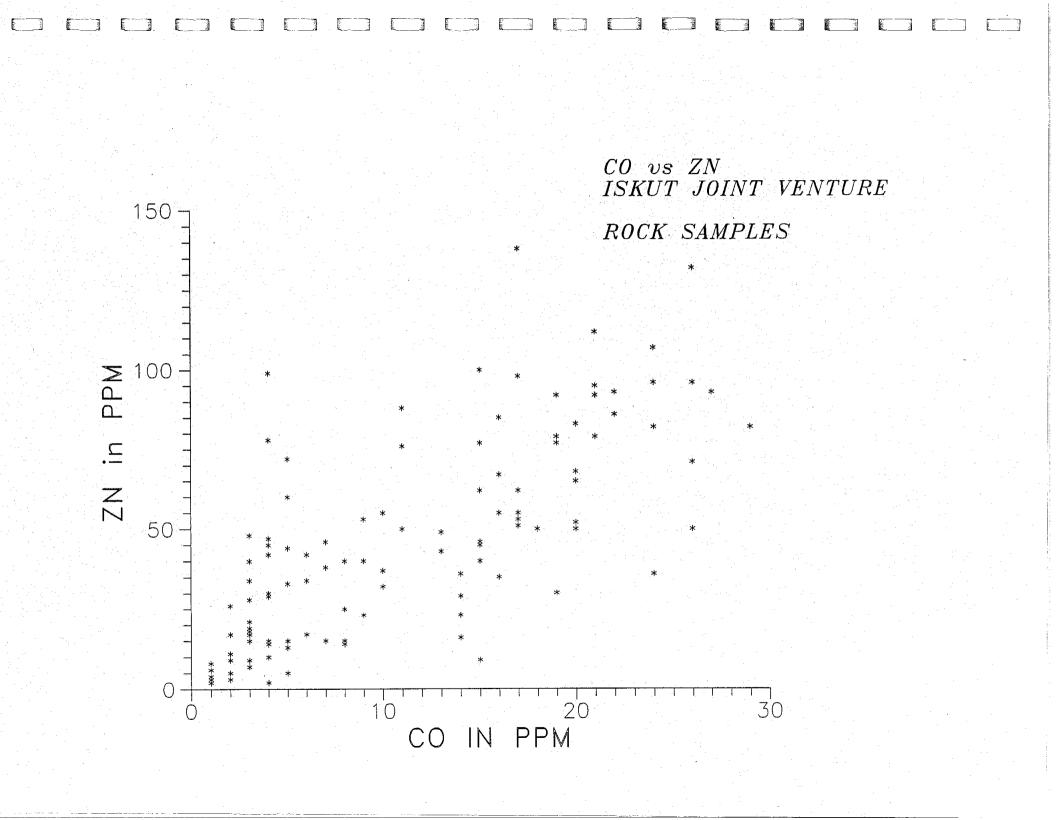


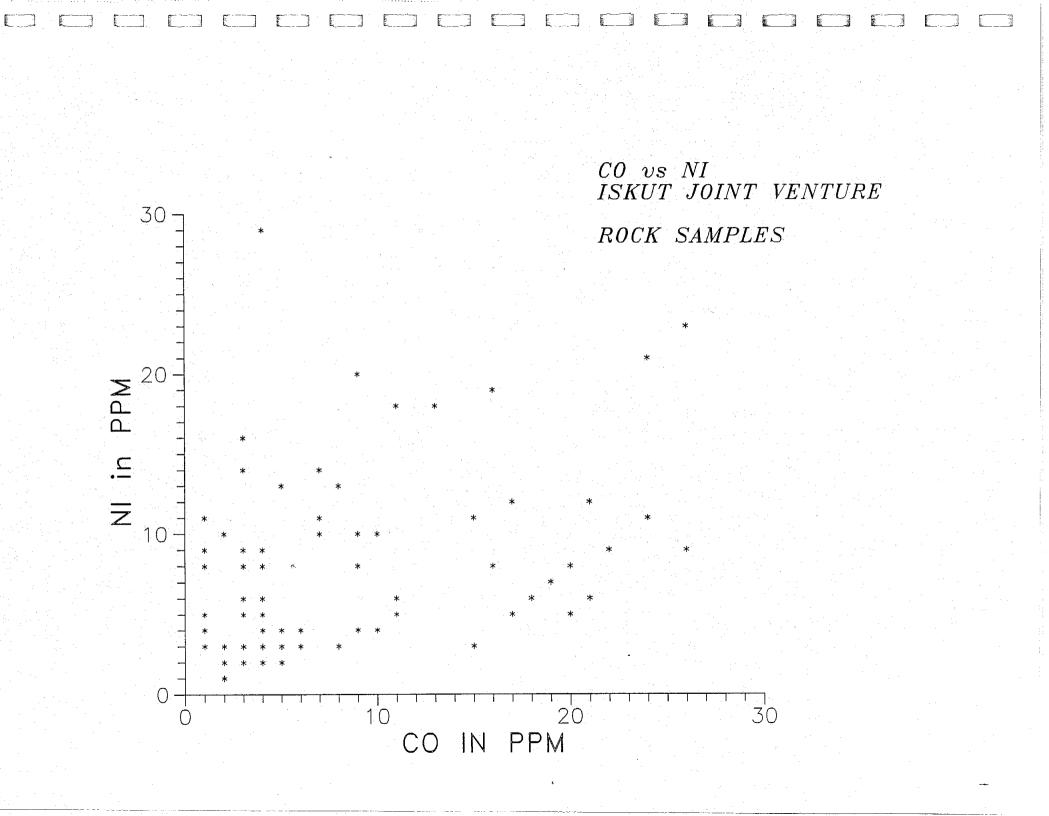
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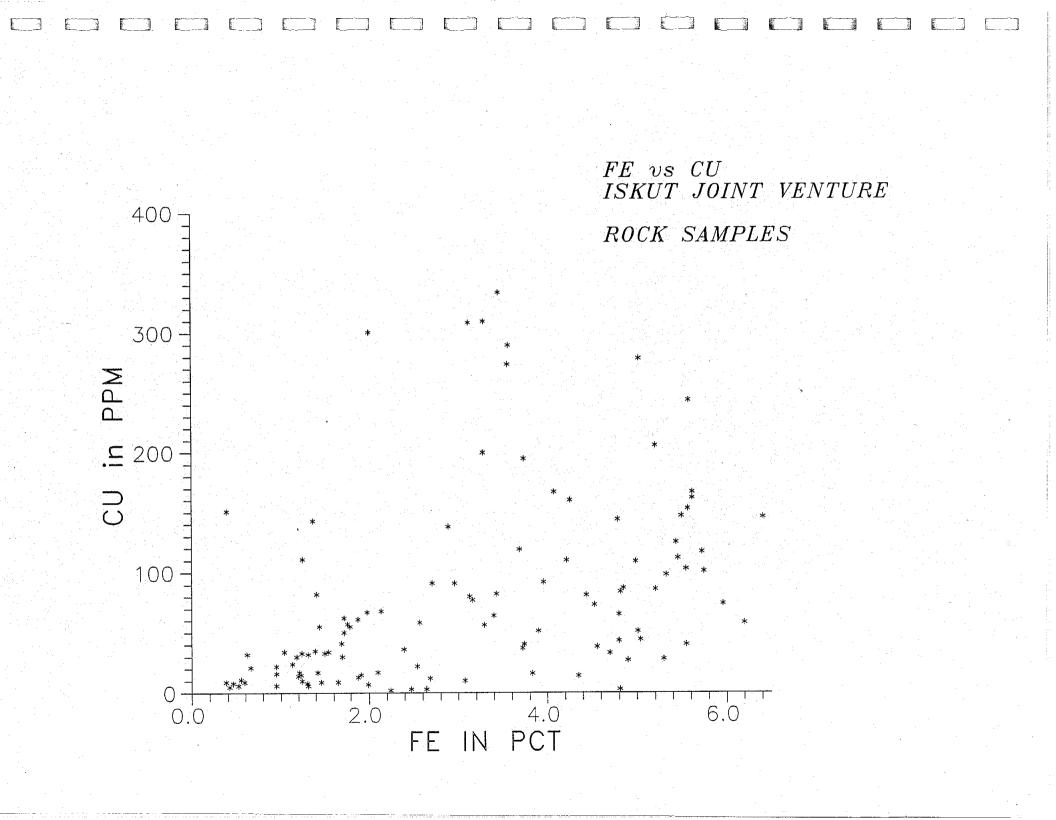


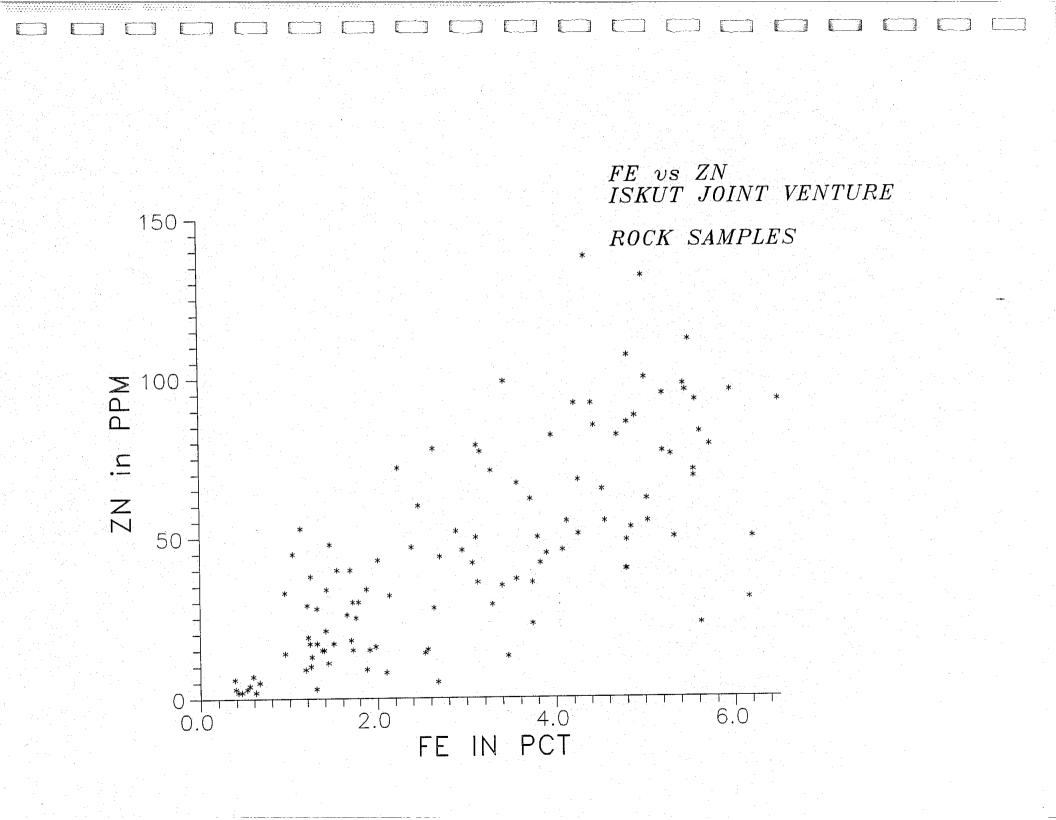


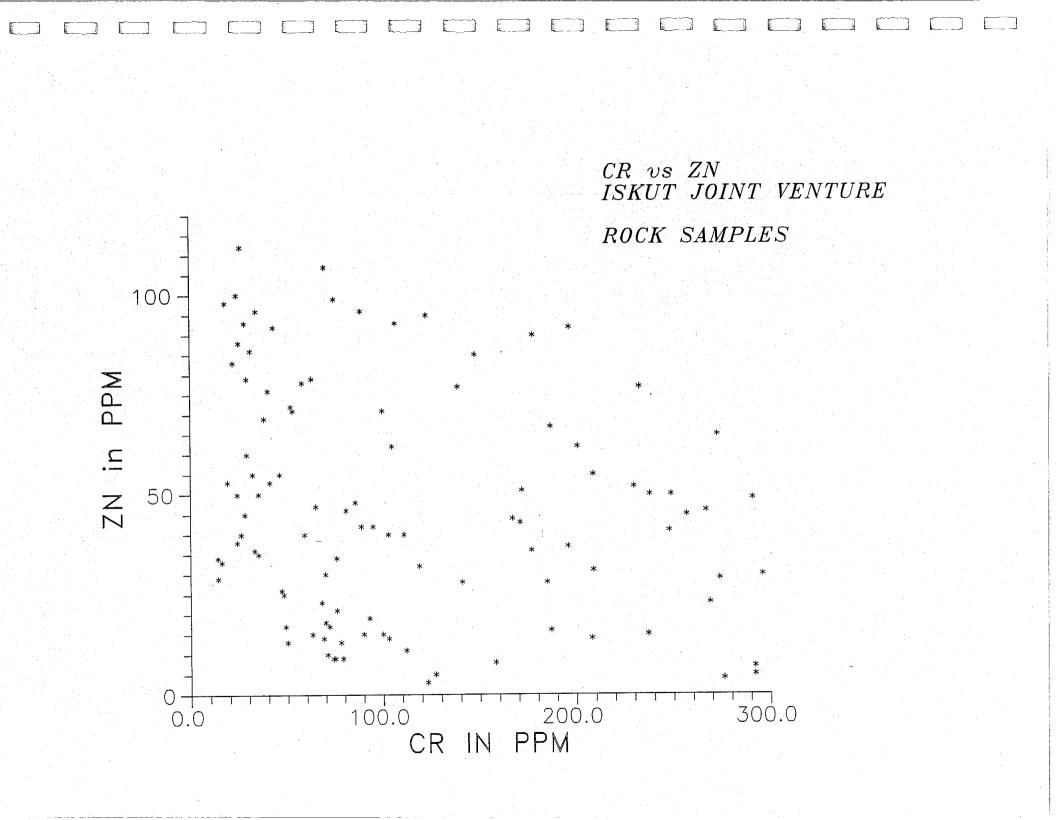


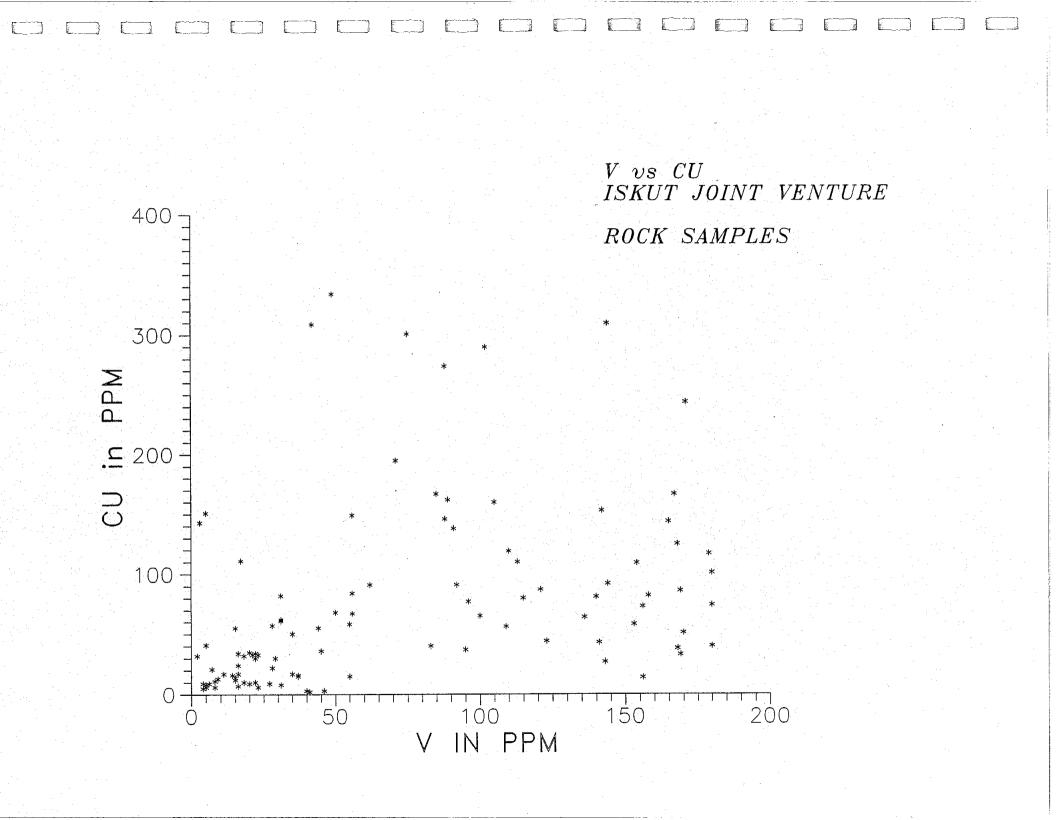


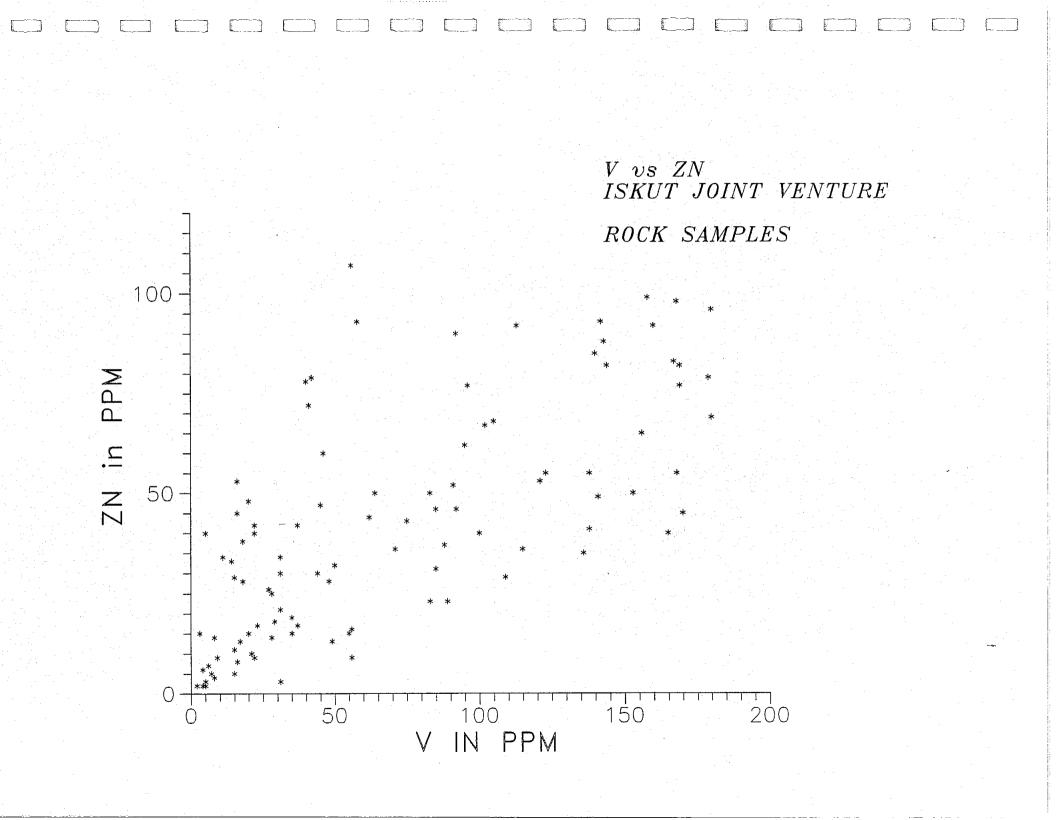


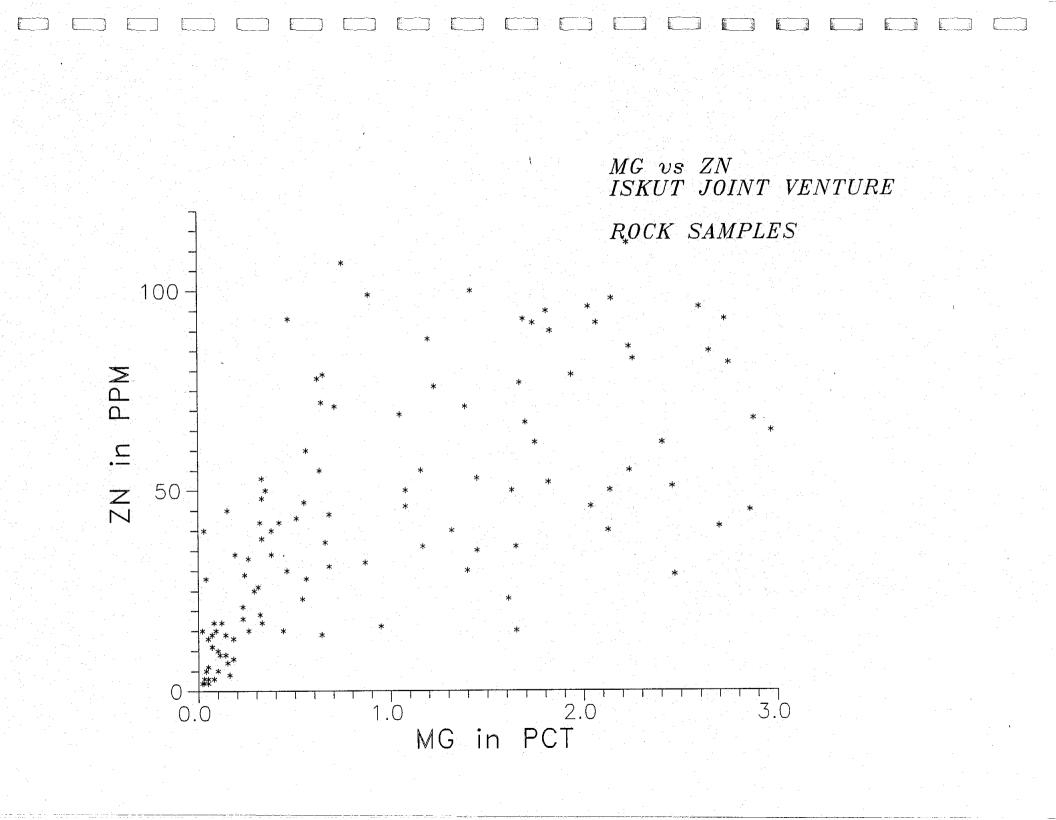


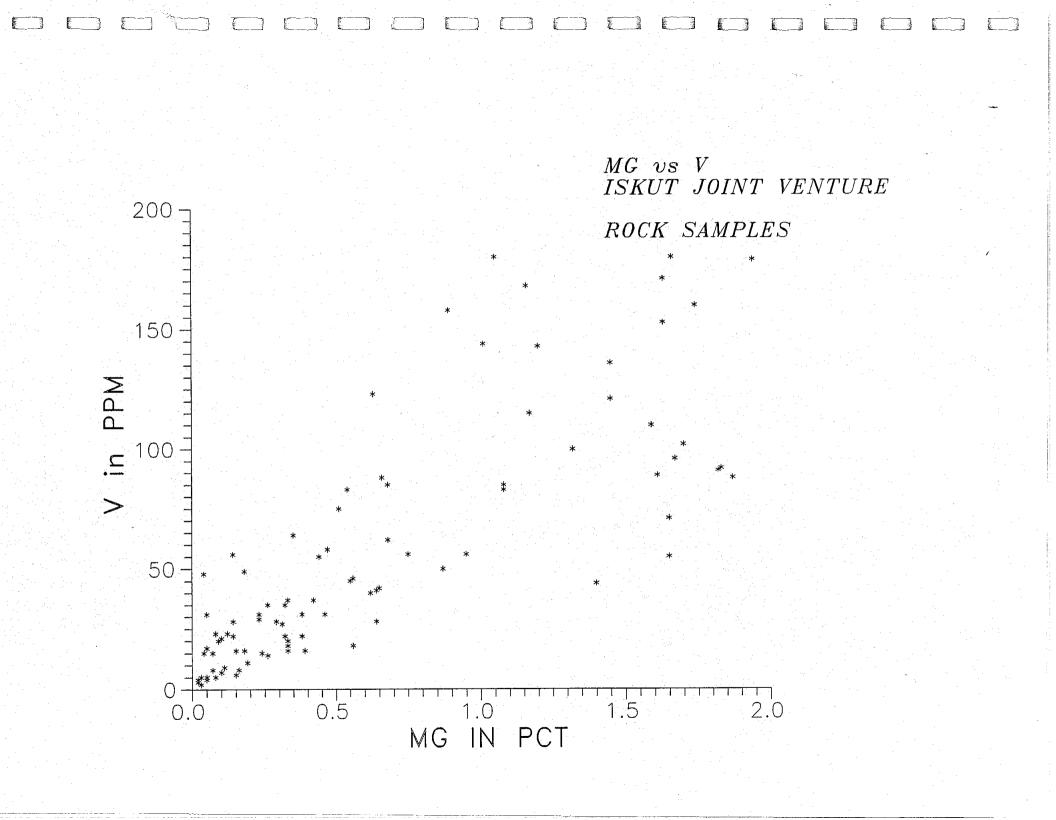


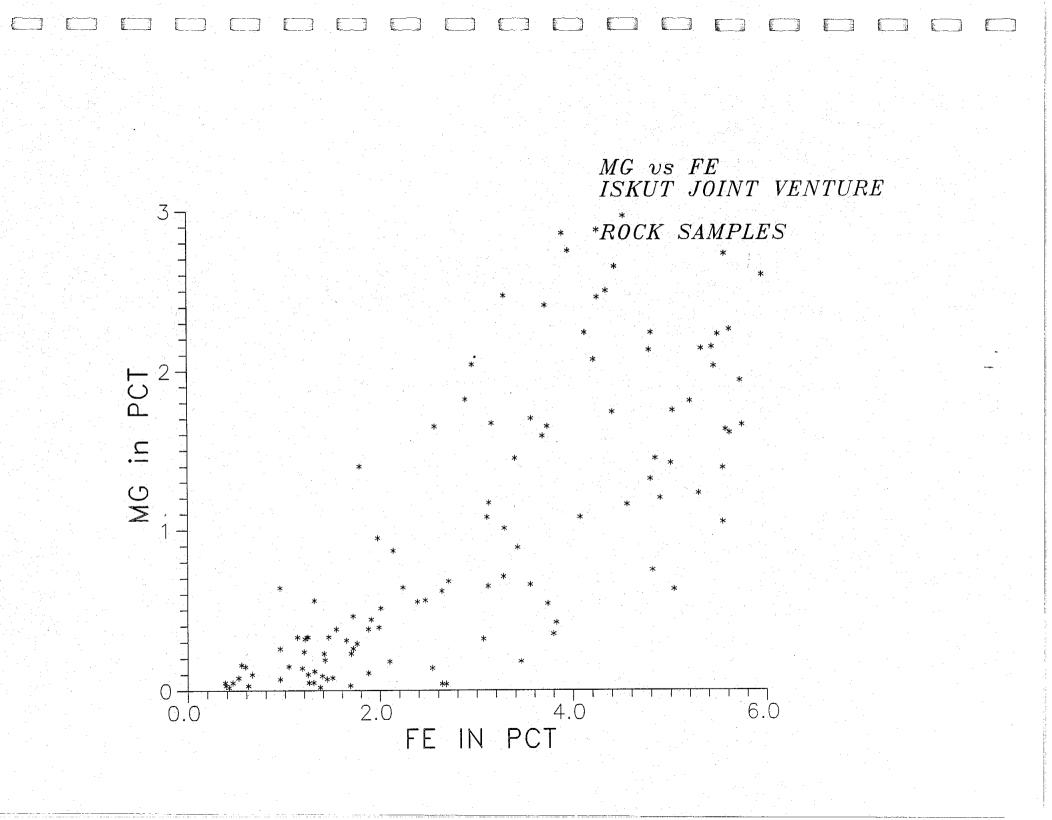


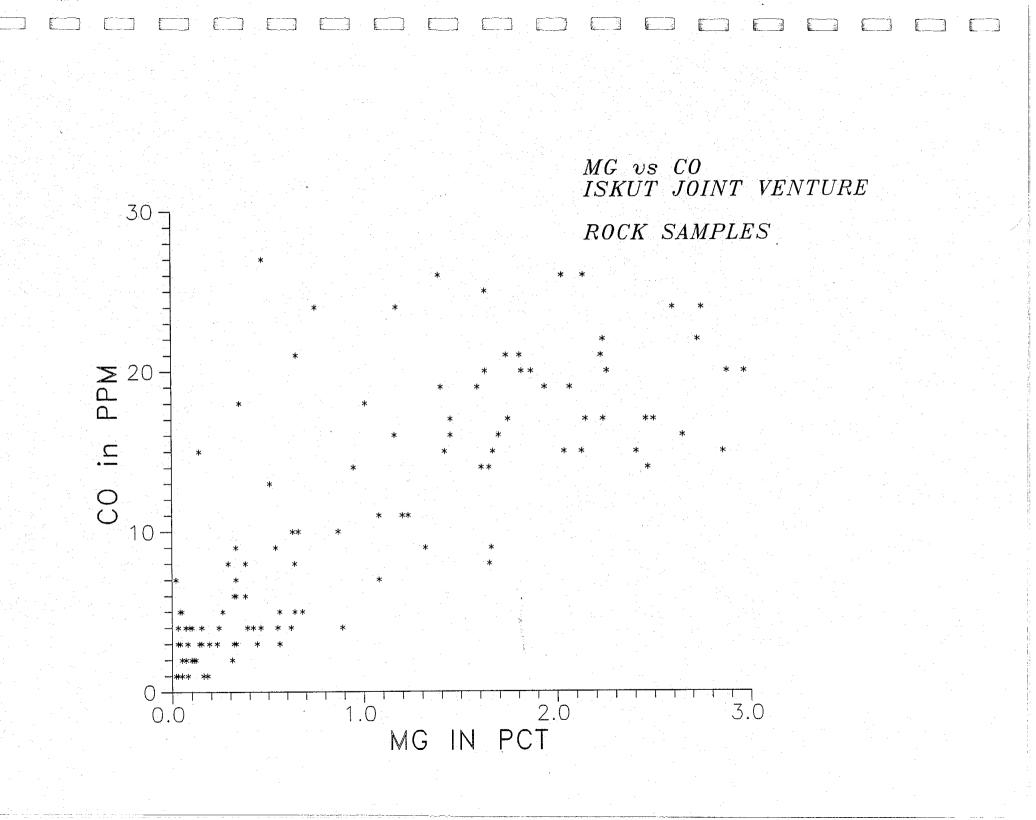


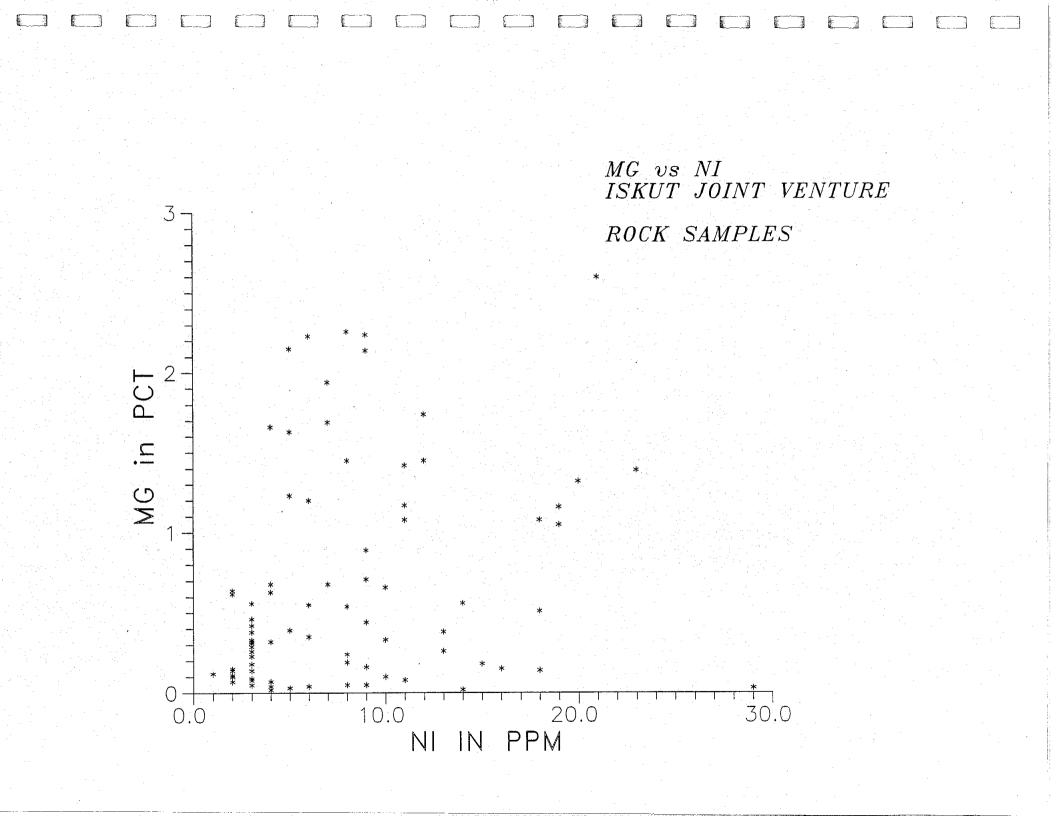


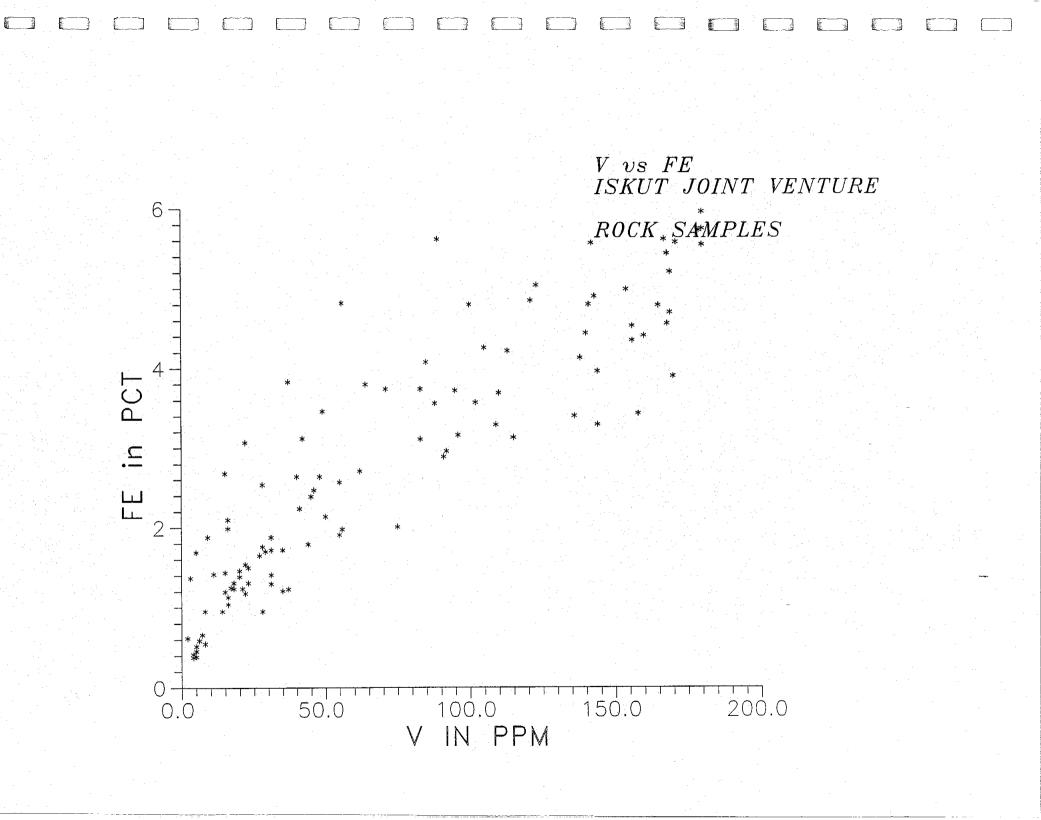


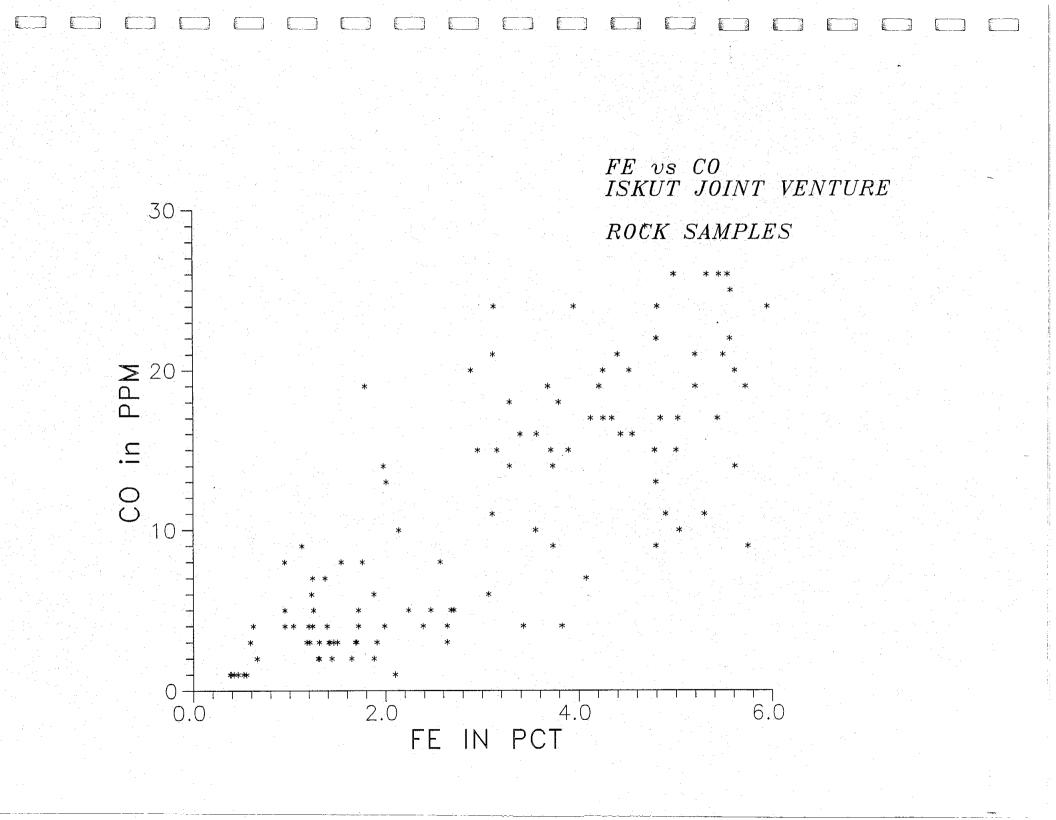


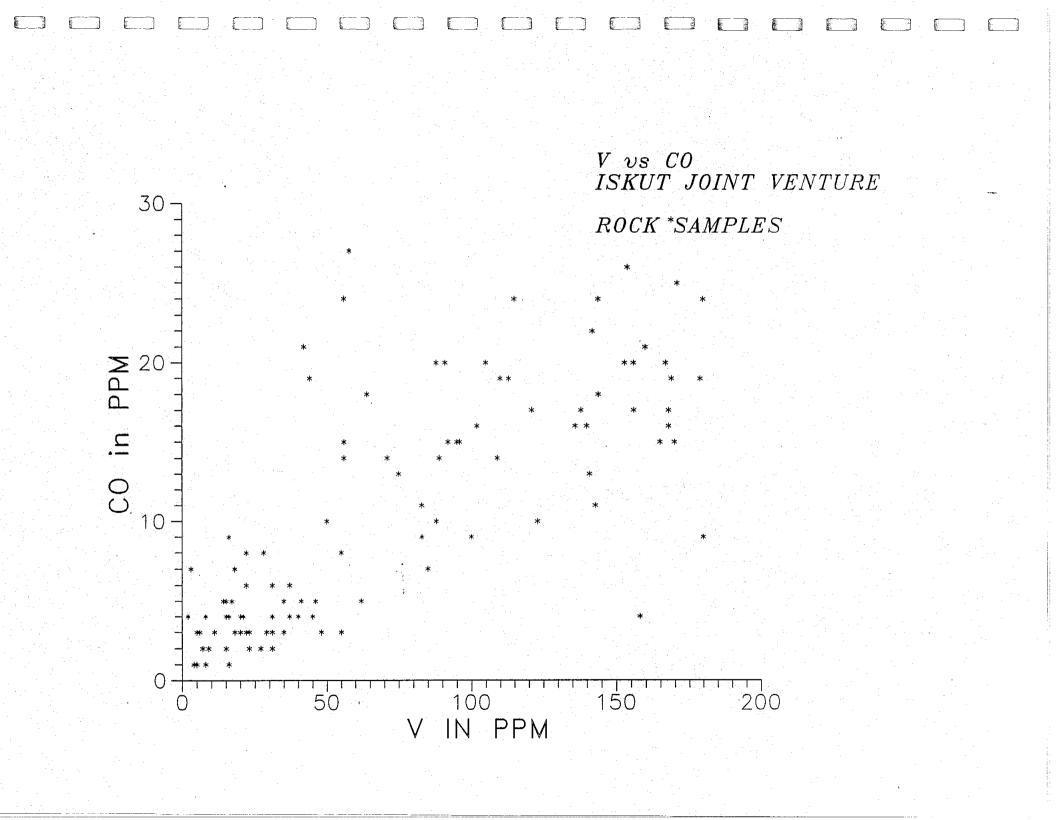








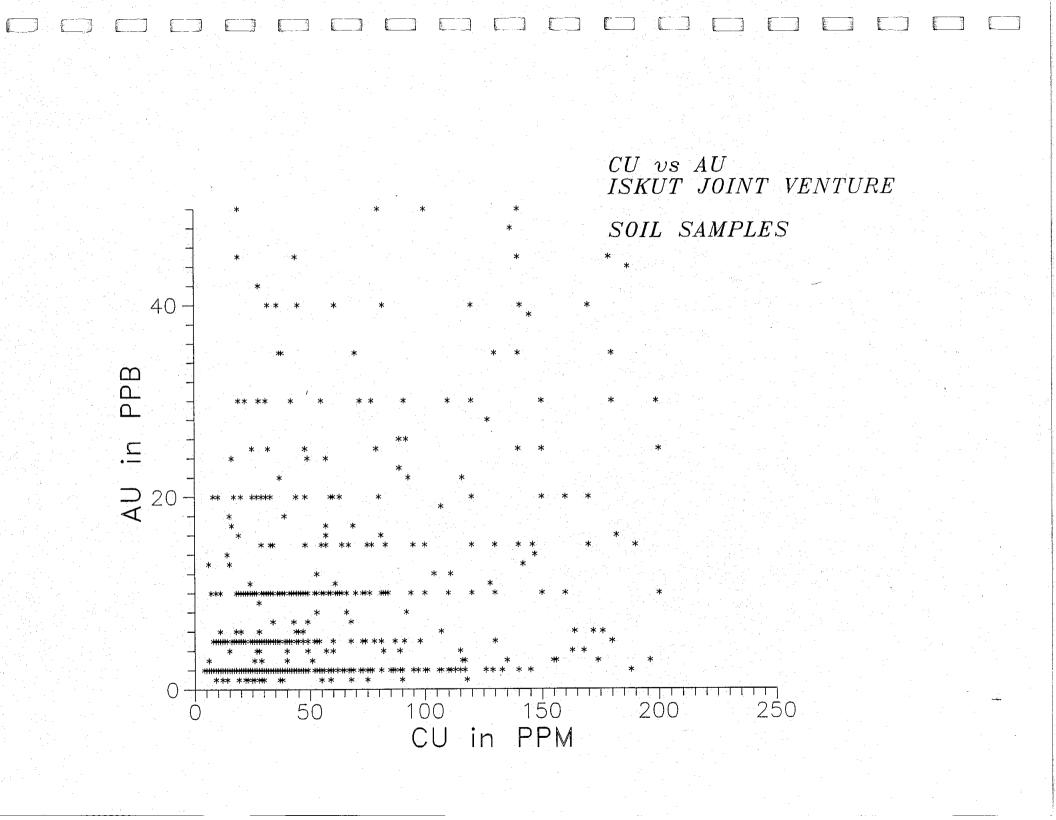


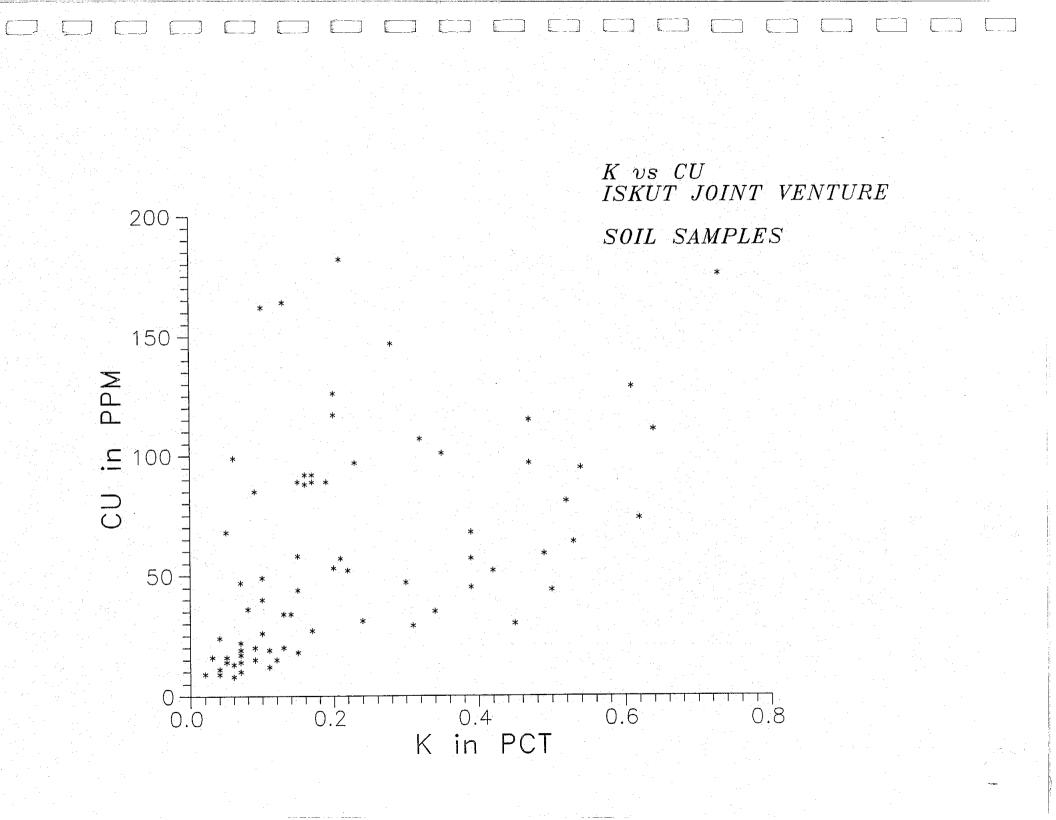


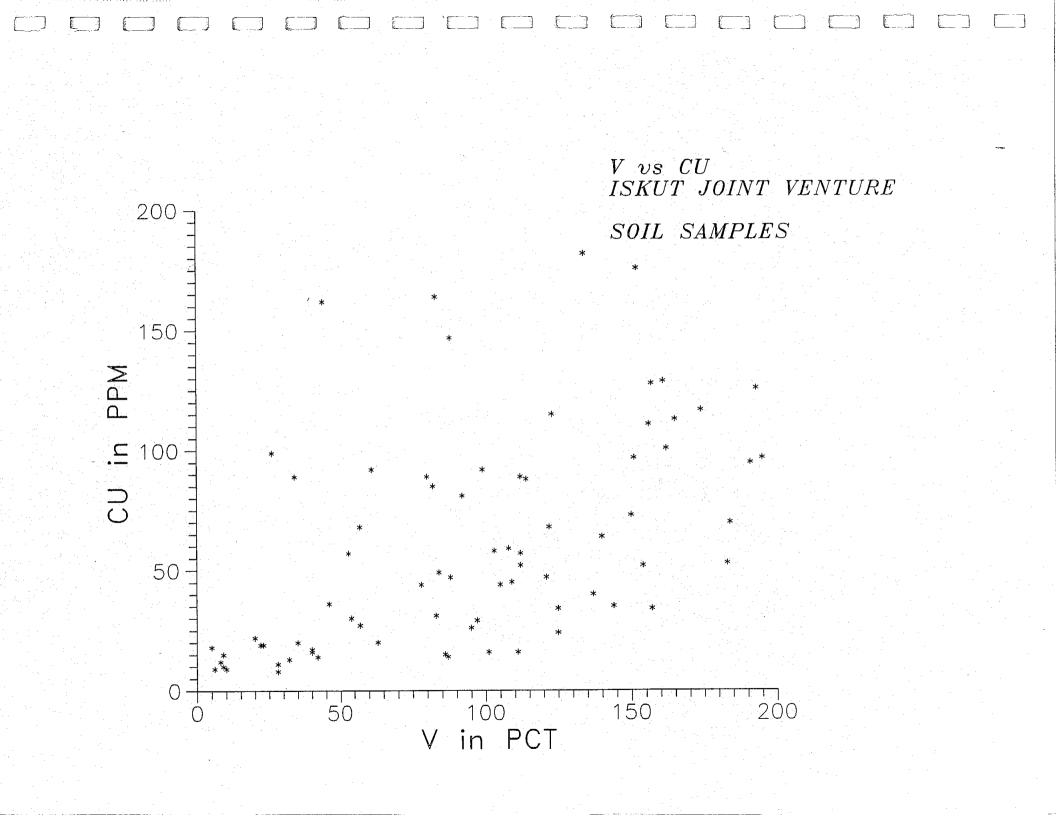
			CO	RREL	ATION	COEF	FICIE	NTS F	ORS	DILS:	ISKI	JT JOI	NT VE	NTUP	EPRC	PERI	Ŷ		
	<del></del> ,							NORMAL	VS LN DIST	RIBUTION		ARSON ARMAN			-				
		_AU	AG	CU	PB	ZN	AS	мо	NI	CO	CD DISTRIBUTI	SB	FE	TE	CR	v	MG	<u> </u>	s
AU			0.092 0.201	0.193 0.372	0.489 0.187	0.152 0.167	-0.055 -0.081	0.139 0.383	-0.016 -0.050	0.054 0.072	****	-0.048 -0.161	0.157 -0.008	-0.085 -0.134		0.007 0.025	-0.039 0.007	-0.013 0.069	2 - 1 - 1 - 1 - 1 - 1 - <del>-</del> - 1 - 1 - <del>-</del>
AG		0.180 0.200		0.285 0.384	0.112 0.086	0.049 0.083	-0.443 -0.481	-0.059 -0.028	-0.311 -0.331	-0.263 -0.341	****	0.141 0.156	0.134 0.072	0.108 0.094	-0.271 -0.266	-0.211 -0.237	-0.369 -0.427	-0.225 -0.323	
CU		0.524 0.485	0.325 0.384		0.068 0.071	0.232 0.409	-0.166 -0.237	0.225 0.242	0.058 0.309	0.483 0.674	****	0.096 0.038	0.481 0.313	0.095 0.222		0.348 0.652	0.248 0.589	0.397 0.662	
PB		0.170 0.187	-0.018 0.086	0.005 0.071		0.256 0.431	0.069 0.268	-0.031 0.060	-0.080 -0.120	0.018 0.106	****	0.166 0.234	0.304 0.298	0.124 0.149	0.064 0.046	-0.155 -0.245	-0.071 -0.196	-0.211 -0.371	
ZN	_	0.123 0.167	0.006 0.083	0.420 0.409	0.341 0.431		0.207 0.361	-0.111 -0.210	0.219 0.138	0.178 0.503	****	0.072 0.099	0.244 0.376	0.141 0.154		0.080 0.214	0.264 0.351	-0.063 0.179	-
AS		-0.067 -0.081	-0.631 -0.481	-0.249 -0.237	0.239 0.268	0.333 0.361		0.171 0.191	0.1 <i>5</i> 0 0.085	-0.024 -0.029	****	0.750 0.742	0.261 0.240	0.584 0.564	0.205 0.078	-0.250 -0.224	0.029 0.060	-0.211 -0.201	-
мо		0.321 0.383	-0.042 -0.028	0.238 0.242	0.148 0.060	-0.143 -0.210	0.043 0.191		-0.172 -0.256	0.116 0.053	****	-0.007 0.044	0.253 0.237	0.063 0.025	-0.166 -0.229	0.050 0.041	-0.090 -0.215	0.098 -0.051	
NI		0.002 0.050	-0.268 -0.331	0.407 0.309	-0.130 -0.120	0.254 0.138	0.133 0.085	-0.253 -0.256		0.429 0.463	****	0.321 0.266	-0.062 -0.094	0.392 0.339	1	0.225 0.285	0.703 0.694	0.230 0.336	
со		0.136 0.072	-0.320 -0.341	0.733 0.674	-0.121 -0.106	0.488 0.503	0.015 -0.029	-0.058 -0.053	0.615 0.463		****	0.166 0.156	0.450 0.488	0.415 0.396	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.786 0.800	0.807 0.829	0.702 0.718	
CD	LN	****	****	****	****	****	****	****	****	****	$\searrow$	****	****	***	****	****	****	****	**
SB		-0.198 -0.161	0.232 0.1 <i>5</i> 6	0.103 0.038	0.240 0.234	0.096 0.099	0.723 0.742	0.148 0.044	0.255 0.266	0.167 0.156	****	$\backslash$	0.286 0.238	0.795 0.754		0.088 0.074		0.050 0.044	-
FE		0.071 -0.008	0.110 0.072	0.366 0.313	0.252 0.298	0.390 0.376	0.292 0.240	0.265 0.237	0.065 0.094	0.412 0.488	****	0.318 0.238		0.312 0.319	1	0.444 0.505		0.228 0.249	
TE		-0.073 -0.134	0.143 0.094	0.350 0.222	0.167 0.149	0.199 0.154	0.576 0.564	0.122 0.025	0.434 0.339	0.477 0.396	****	0.766 0.754	0.362 0.319		0.309 0.249			0.228 0.261	
CR		-0.010 -0.039	0.233 0.266	0.258 0.183	-0.049 -0.046	0.175 0.048	0.114 0.078	-0.248 -0.229	0.901 0.887	0.396 0.268	****	0.200 0.252	0.053 0.102		$\searrow$	0.128 0.172		0.042 0.181	-
v		0.159 0.025	-0.210 -0.237	0.648 0.652	-0.246 -0.245	0.142 0.214	-0.207 -0.224	-0.060 -0.041	0.489 0.285	0.725 0.800	****	0.100 0.074	0.331 0.505	0.340 0.249			0.721 0.765	0.643 0.689	1 ·
MG		0.115 0.007	-0.348 -0.427	0.657 0.589	-0.236 -0.196	0.322 0.351	0.049 0.060	-0.195 -0.215	0.770 0.694	0.852 0.829	****	0.181 0.169	0.489 0.392	0.447 0.393	0.656	0.848		0.628 0.734	
ĸ		0.108 0.069	-0.356 -0.323	0.693 0.662	-0.367 -0.371	0.109 0.179	-0.185 -0.201	-0.047 -0.051	0.443 0.336	0.746 0.718	****	0.074 0.044	0.224	0.307	0.259	· · .	0.720		
SR		0.174 0.081	-0.220 -0.163	0.559	-0.269 -0.253	0.079	-0.294 -0.307	-0.072 -0.030	0.355	0.642	****	-0.035 -0.065	0.037	0.279	0.206	0.771	0.678		

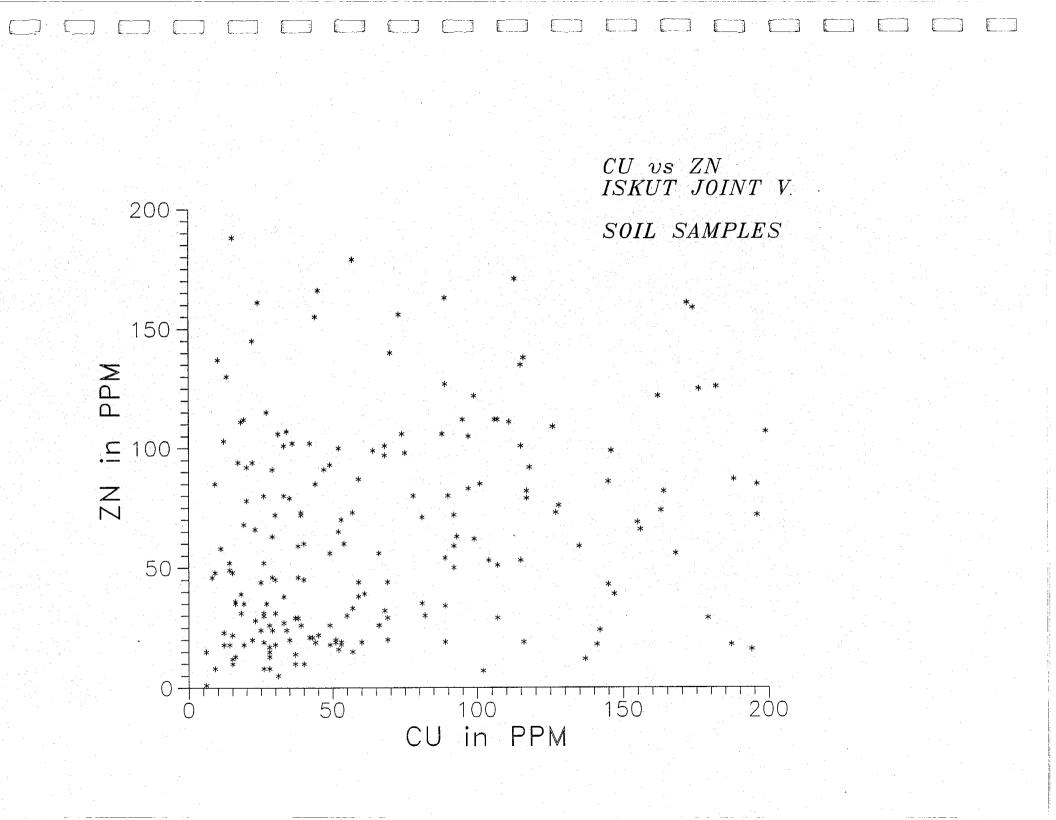
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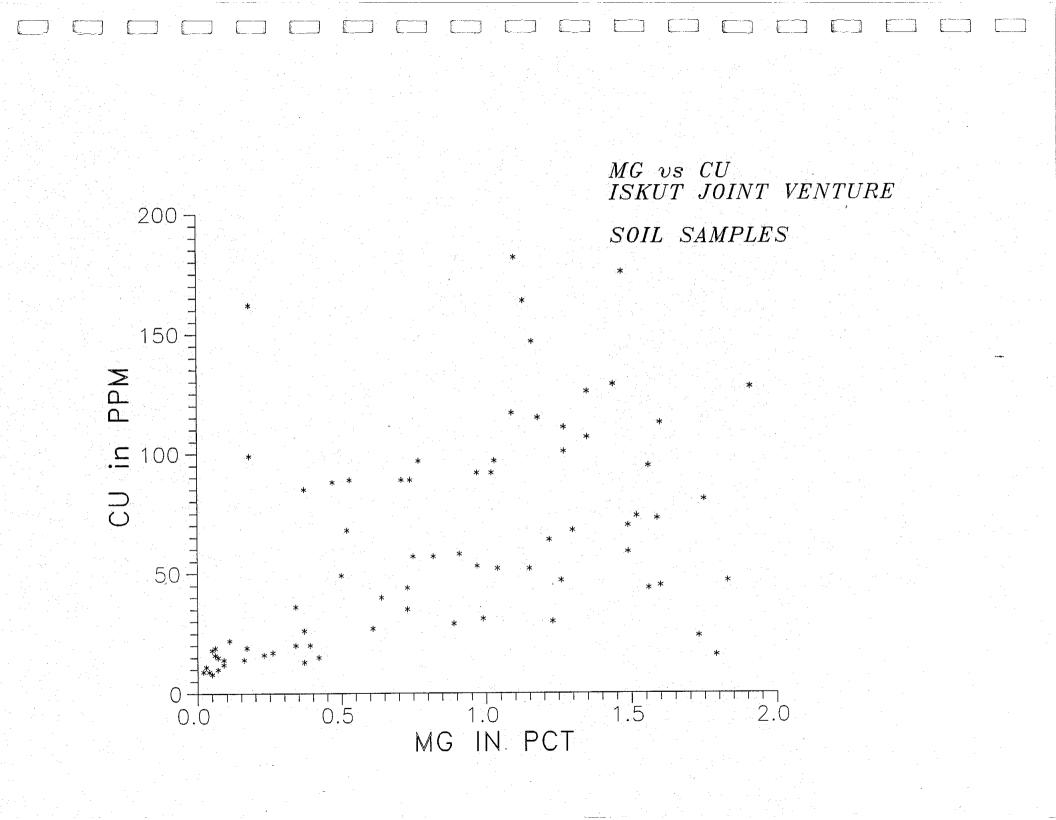
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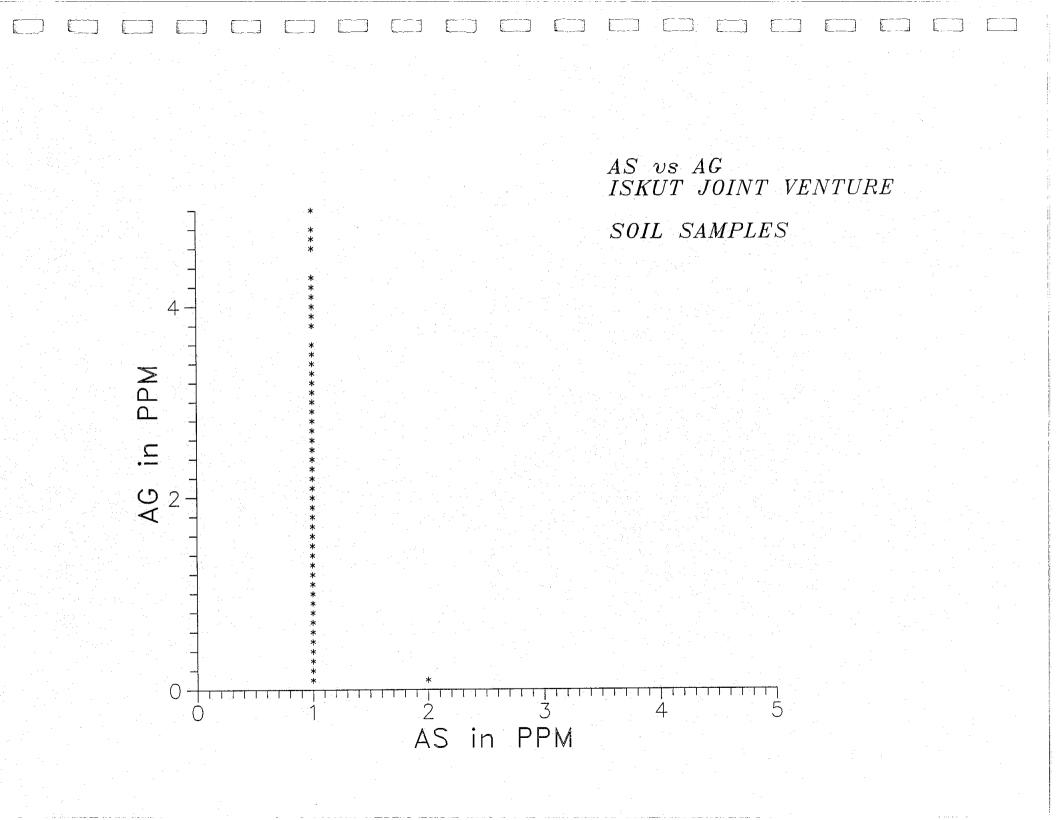


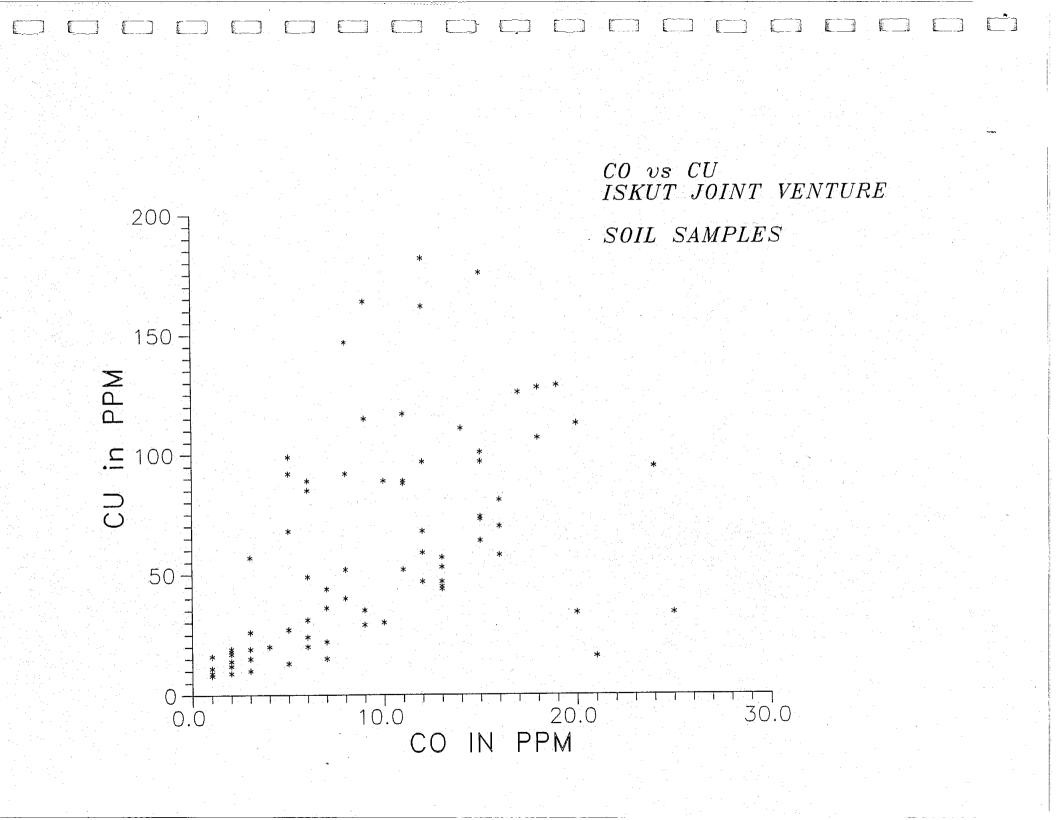


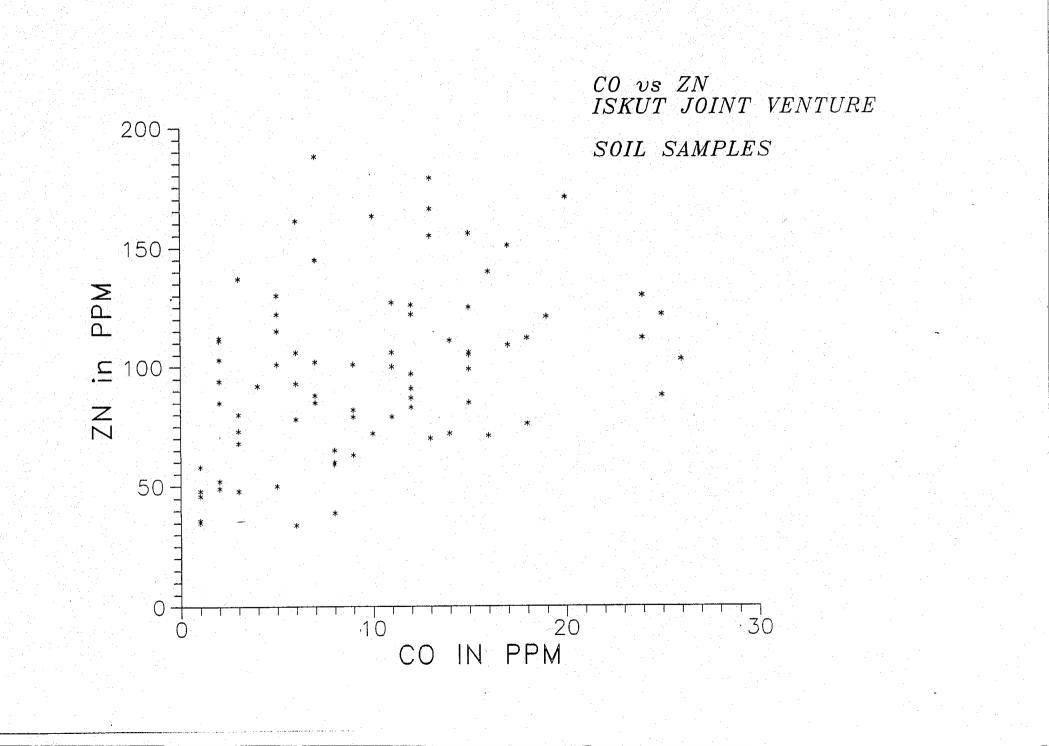












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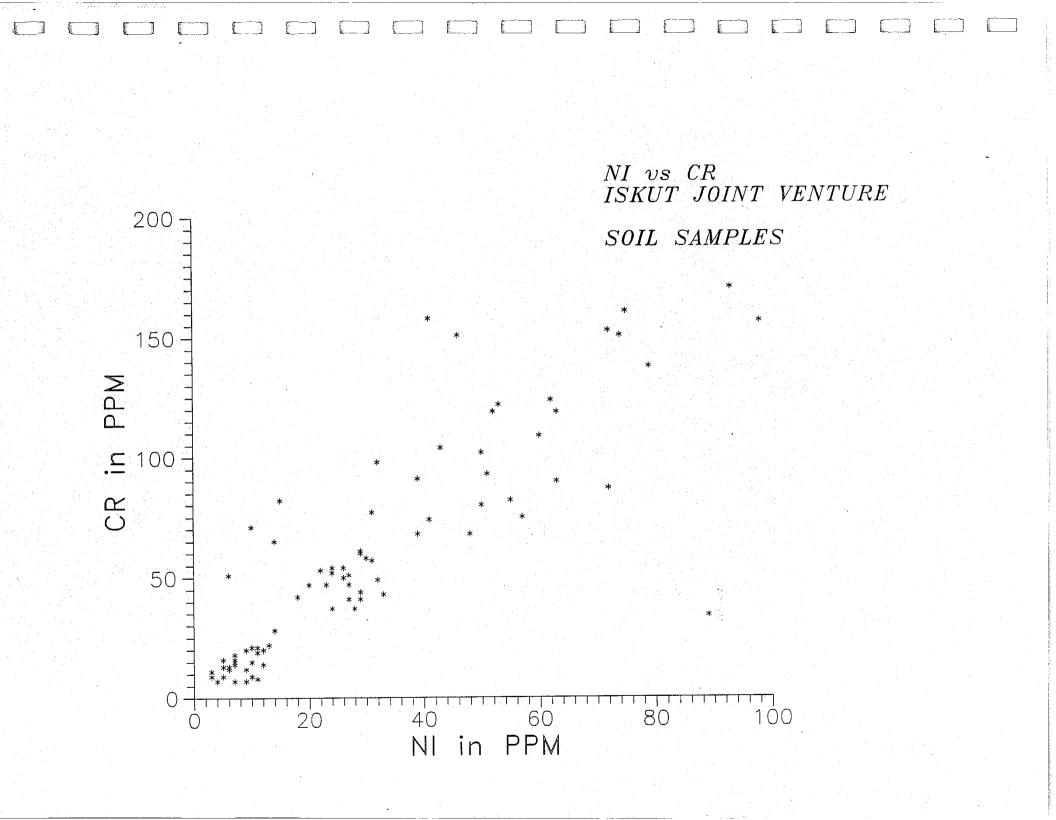
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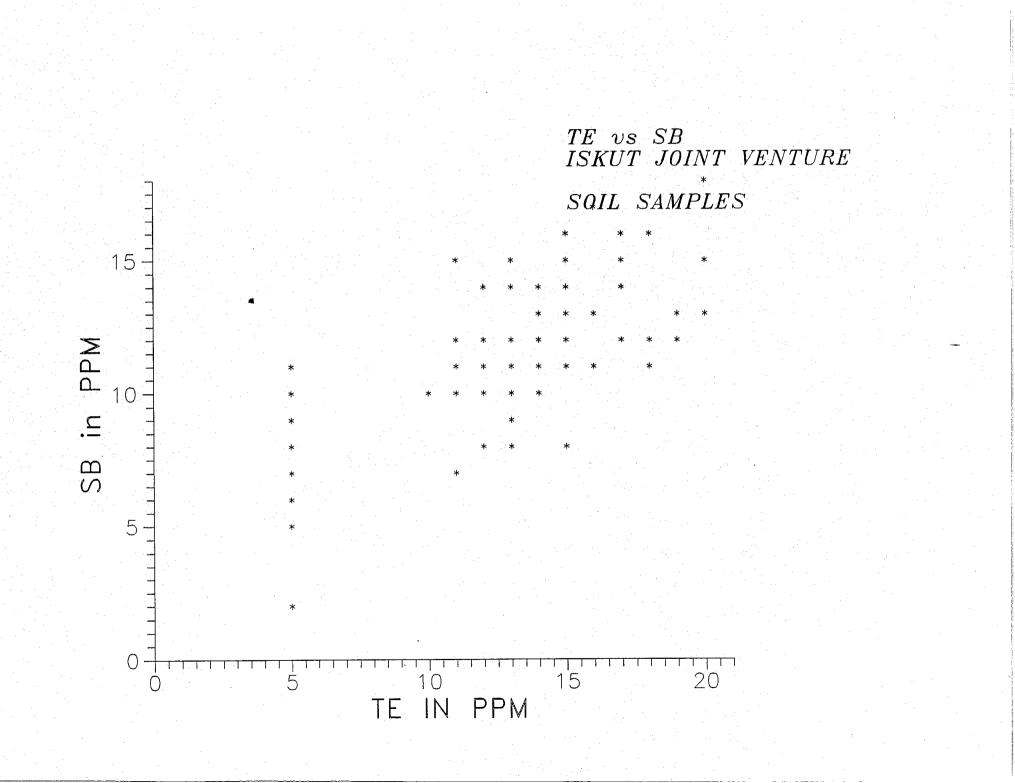
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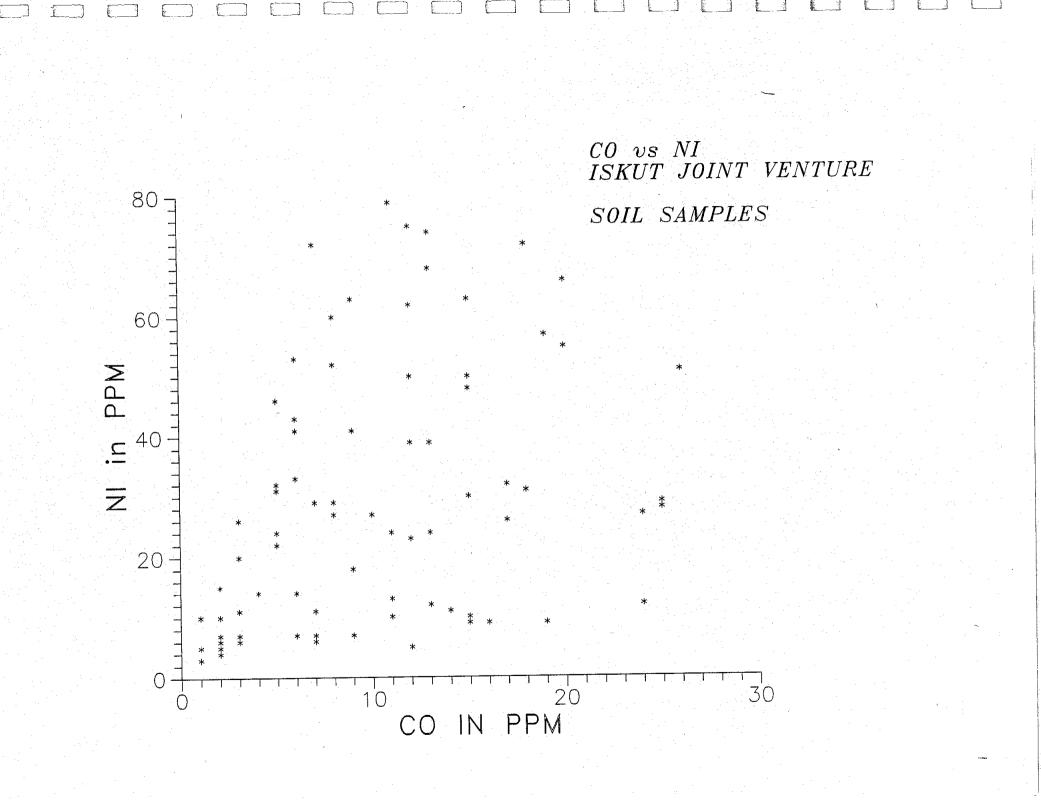
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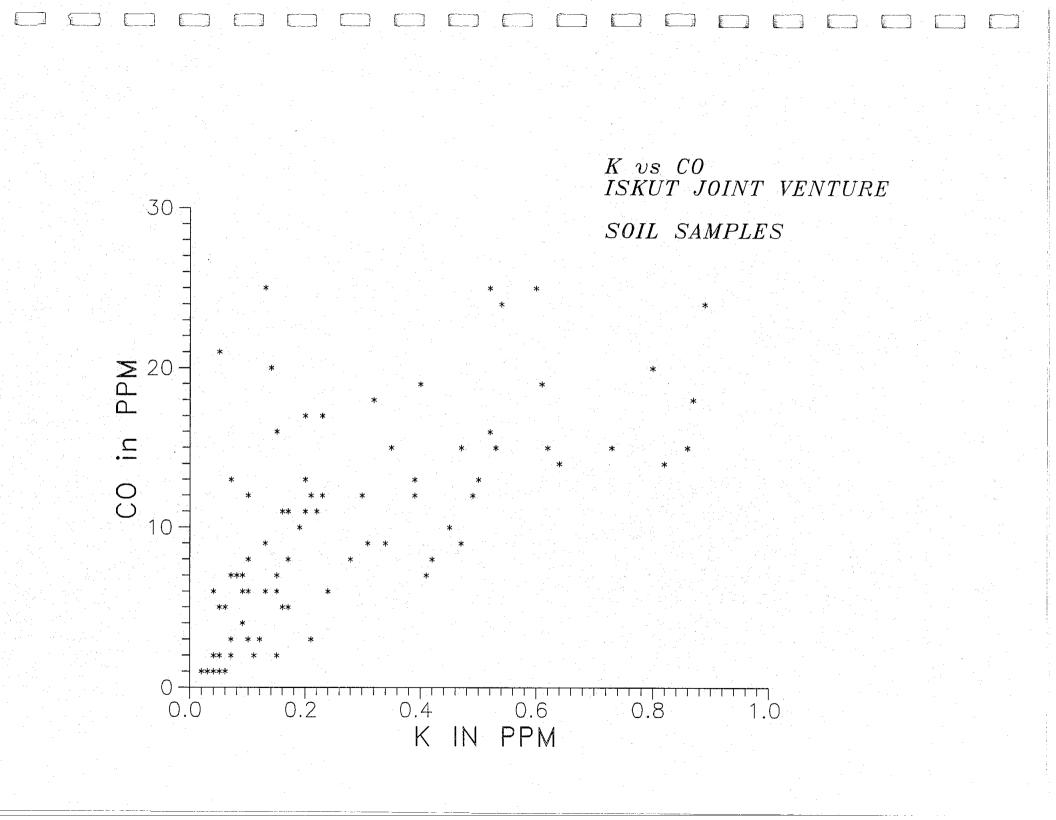


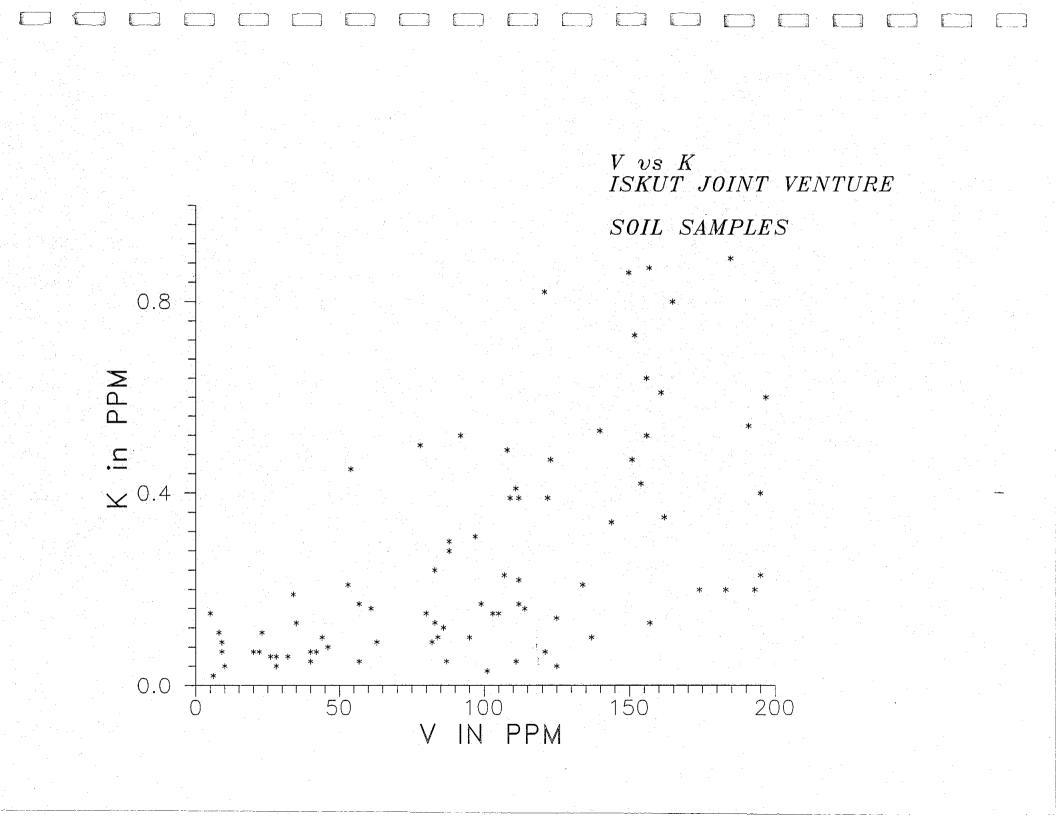


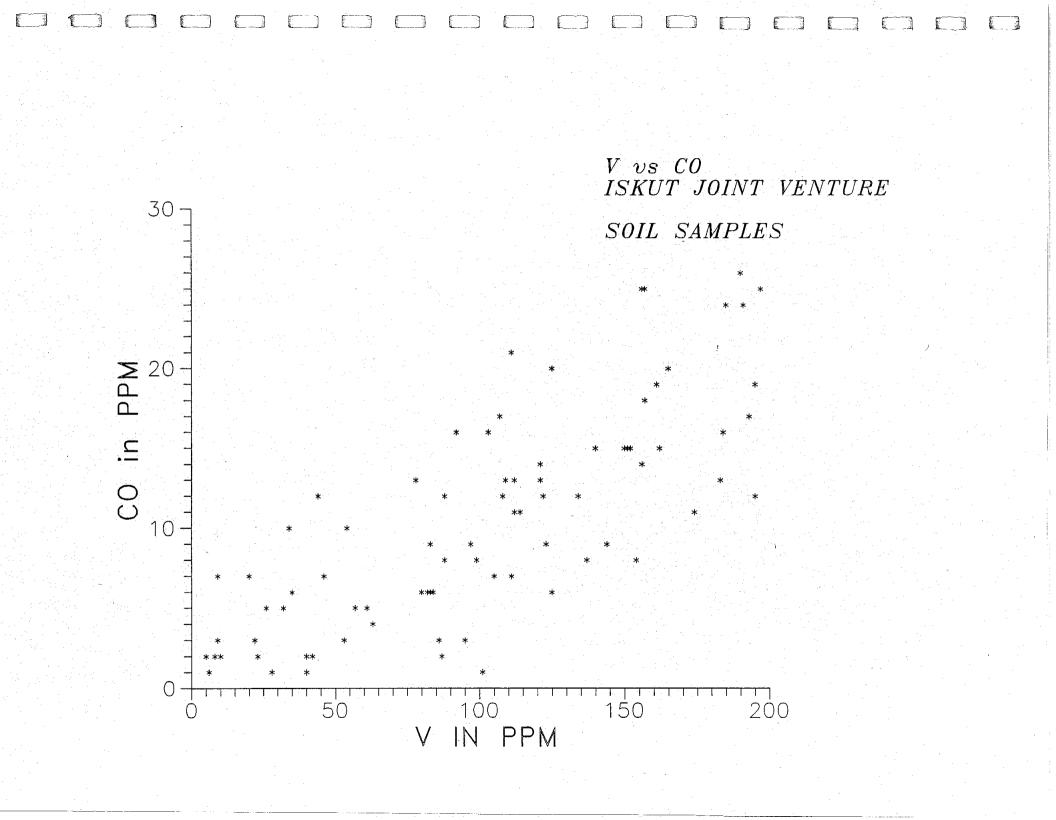
 $\left( \begin{array}{c} \end{array} \right)$ 

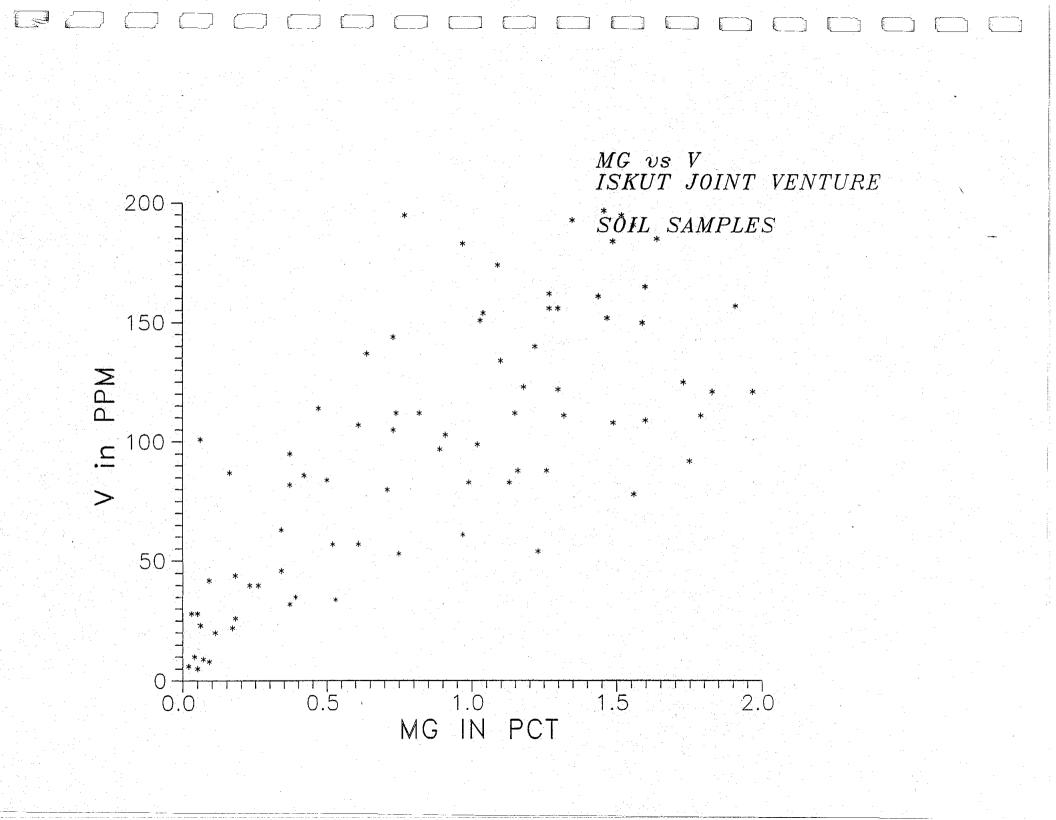
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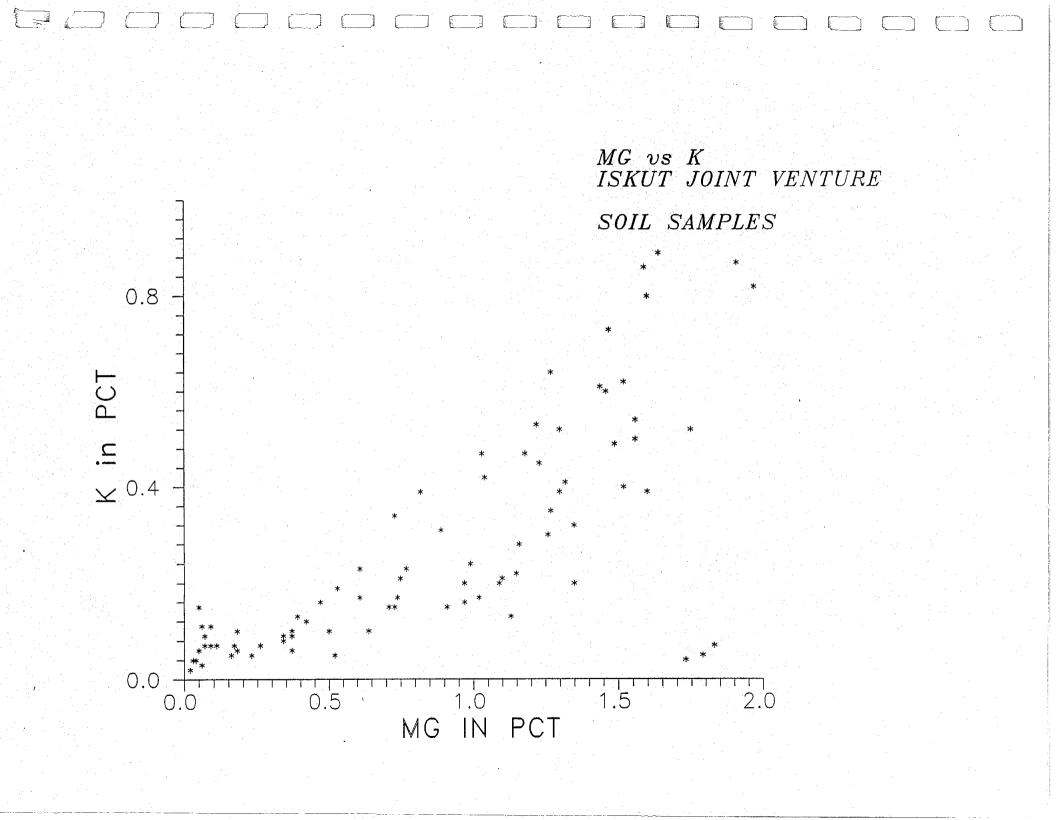


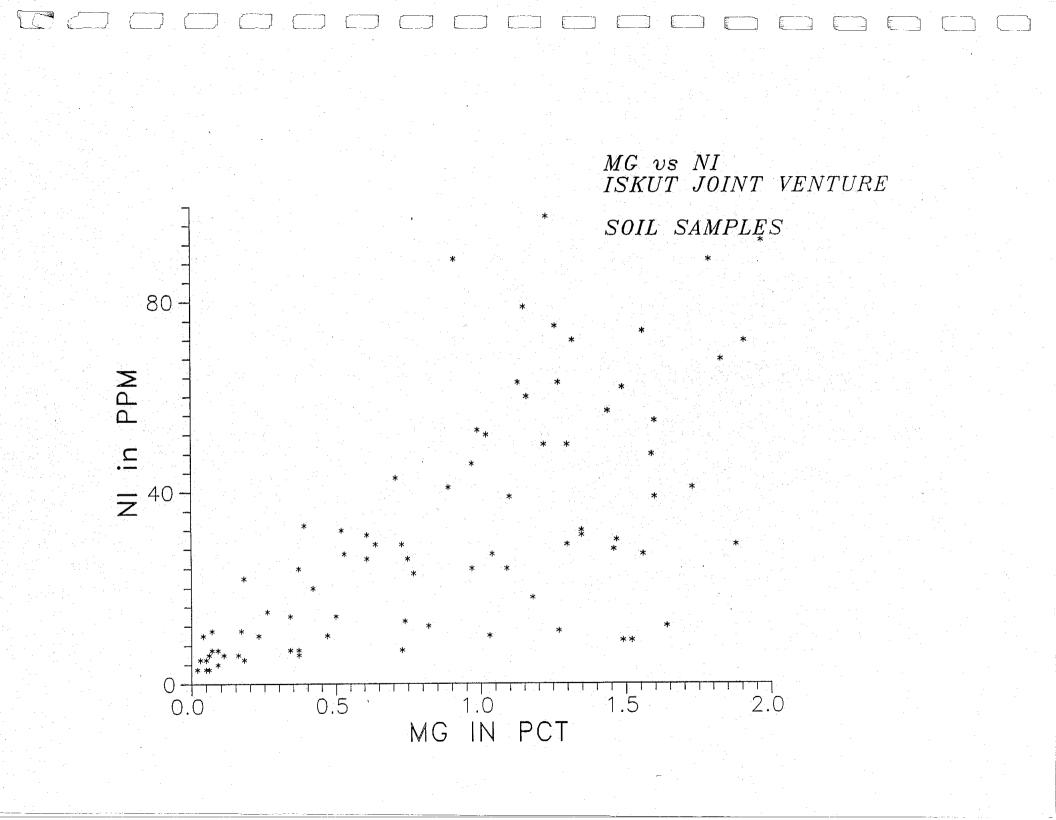


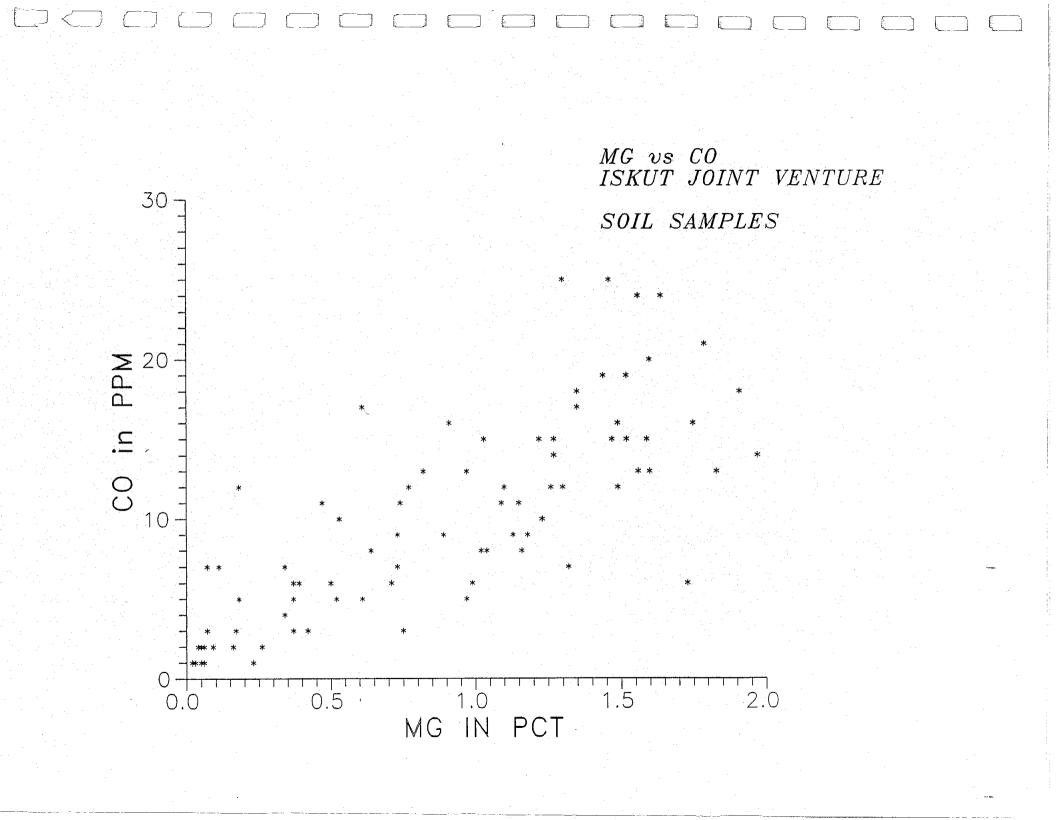


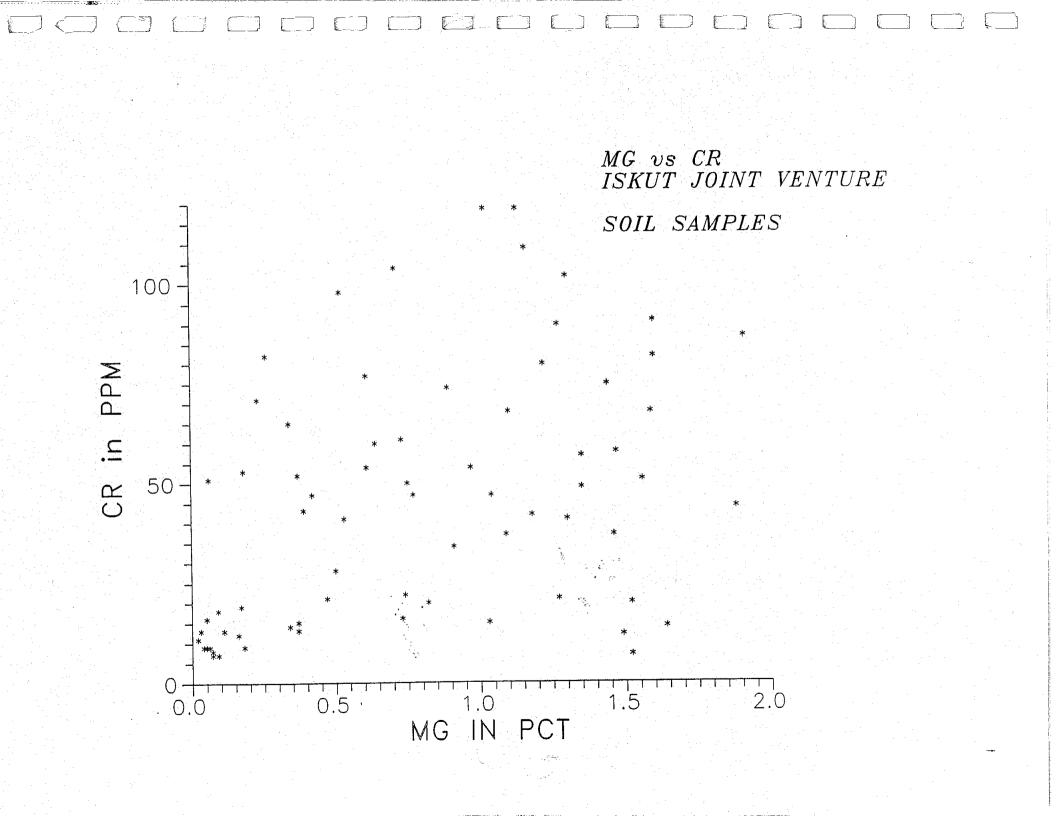


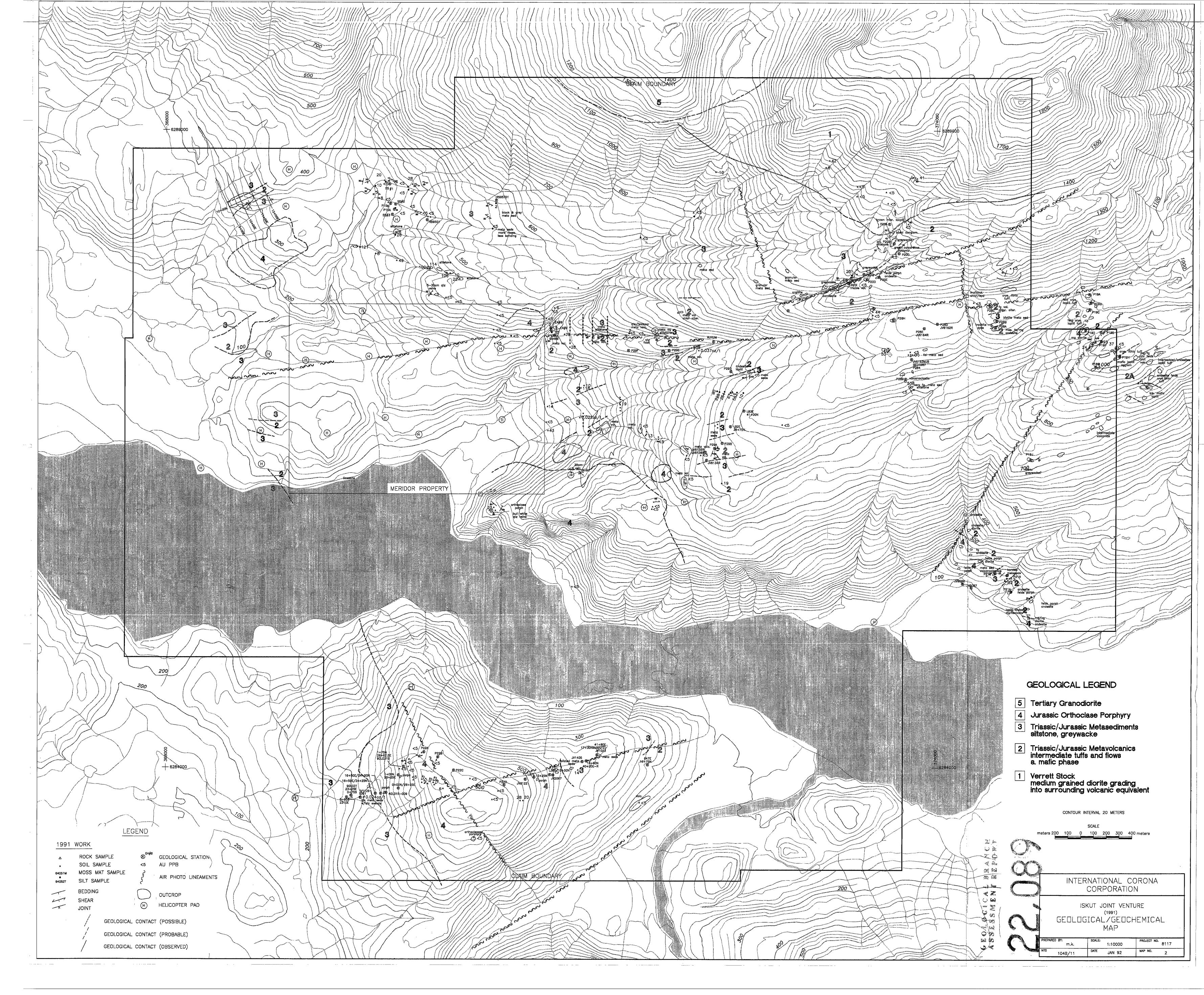


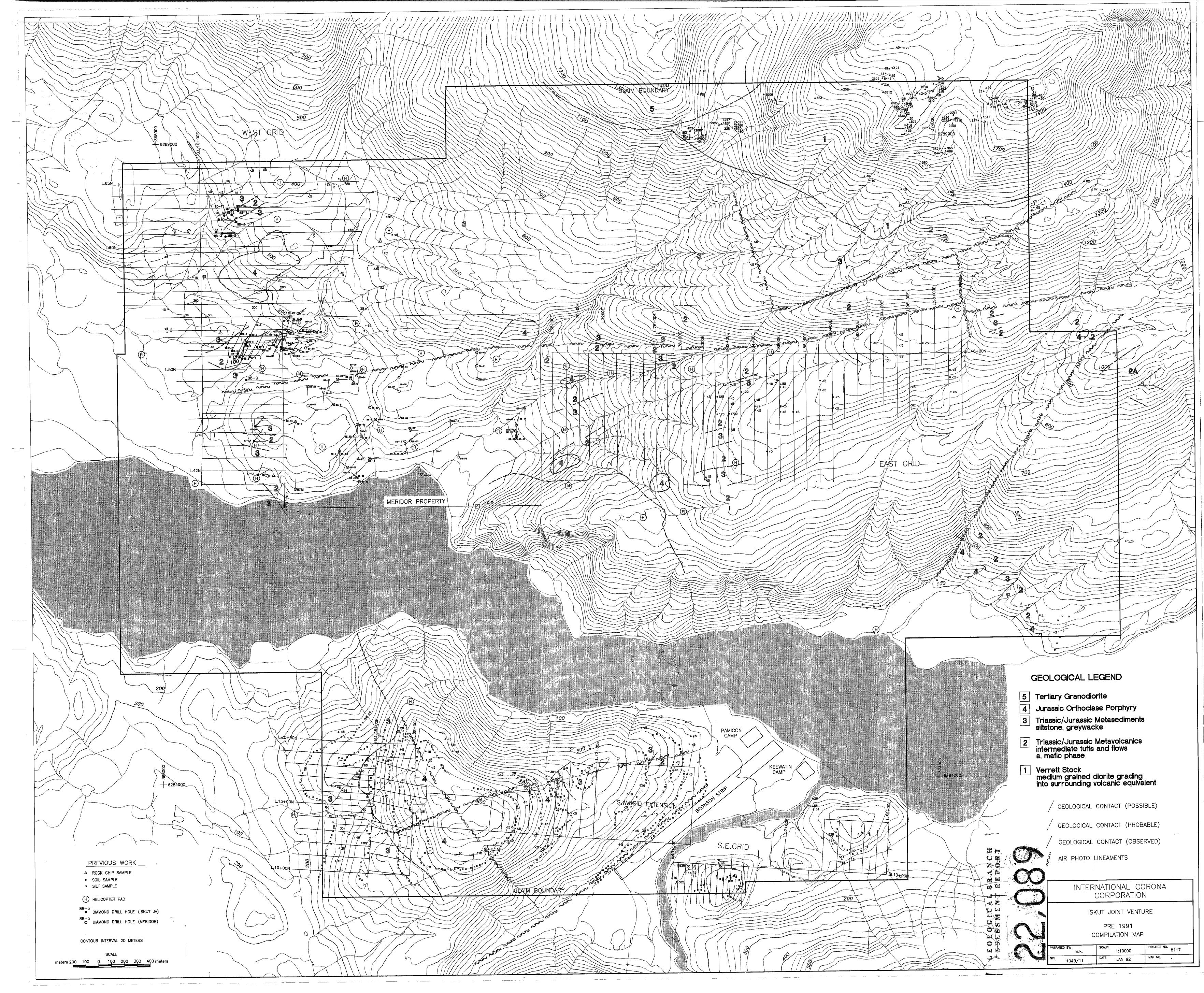


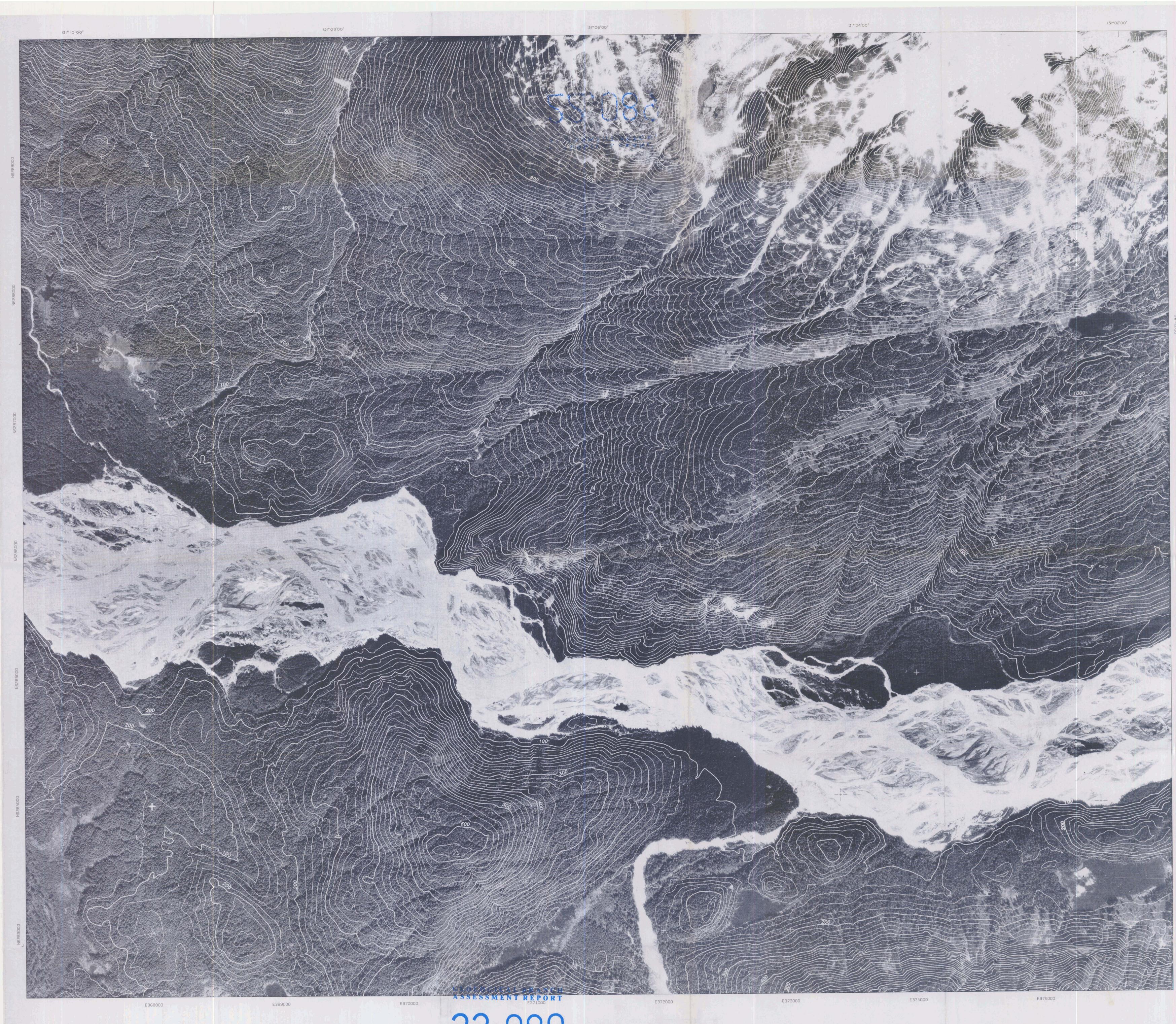












Date of photography: July 1982 Control taken from "TRIM" data base Contours supplied by Corona Corporation Area located on TRIM sheets 104B065, 104B075 Compiled by THE ORTHOSHOP W0#3467



Contour Interval 20 m
MAP 4

200 400 600 800 1000 m



