ASSESSMENT REPORT ON GEOCHEMICAL WORK ON THE FOLLOWING CLAIMS

BEST BET 17 253569
BEST BET 18 253570

located

45 KM NORTH-NORTHWEST OF
STEWART, BRITISH COLUMBIA
SKEENA MINING DIVISION

56 degrees 22 minutes latitude
130 degrees 07 minutes longitude

N.T.S. 104B/8E

PROJECT PERIOD: Sept. 29 to October 11, 1991

ON BEHALF OF
TEUTON RESOURCES CORP.
VANCOUVER, B.C.

REPORT BY

D. Cremonese, P. Eng.
509-675 W. Hastings
Vancouver, B.C.

Date: April 19, 1992

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1. INTRODUCTION

A. Property, Location, Access and Physiography

The Best Bet claims are situated approximately 6 km north of the airstrip at Tide Lake Flats (just north of the old Granduc concentrator). Access from Stewart, 45 air-kilometers to the south, is by helicopter; alternative access is via the Granduc road to the aforementioned air strip and thence by helicopter. Access by foot is possible from the terminus of the Granduc Road system near the old East Gold mine, however this would entail a hazardous crossing over a highly crevassed glacier.

The claims are bisected by the west-east trending "Little Canoe" Glacier, the first valley glacier north of the giant Frankmackie Glacier, from which a small stream drains eastward into Toe Lake. An extensive icefield encroaches on the northern margins of the claims.

Terrain is steep throughout except on the topland bordering the icecap near the 1,600 m level, an area marked by gently sloping eskers, patches of glacially scoured rock and vegetation consisting of alpine grass, dwarf bushes and mountain flowers. From this upland, sharply incised creeks drain southward into the valley glacier. Intermittent patches of scrubby mountain balsam and hemlock thicken gradually downslope from treeline at the 1,300 m mark.

B. Status of Property

Relevant claim information is summarized below:

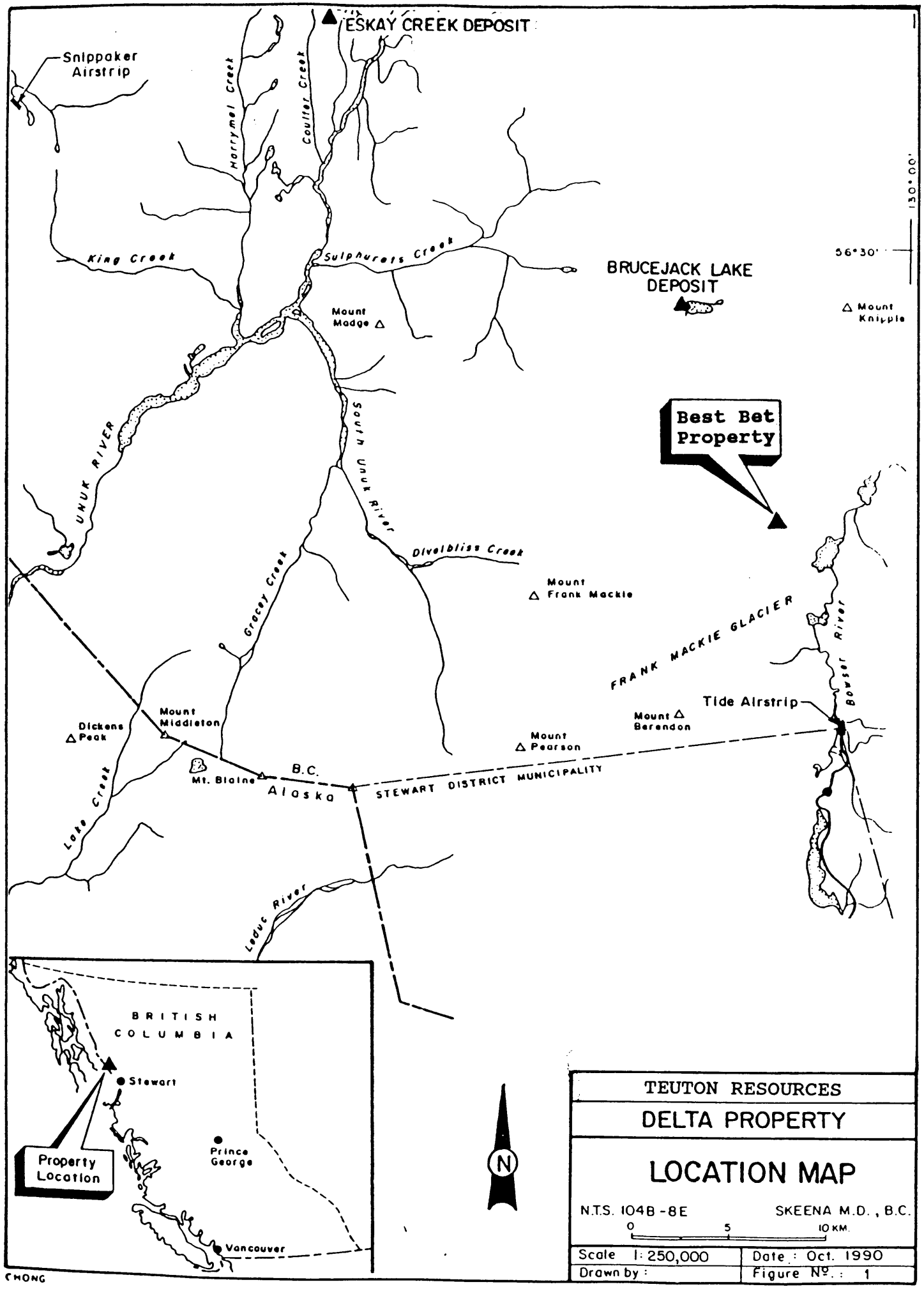
Name	Tenure No.	No. of Units	Record Date
Best Bet 17	253569	20	Jan. 22, 1990
Best Bet 18	253570	20	Jan. 22, 1990

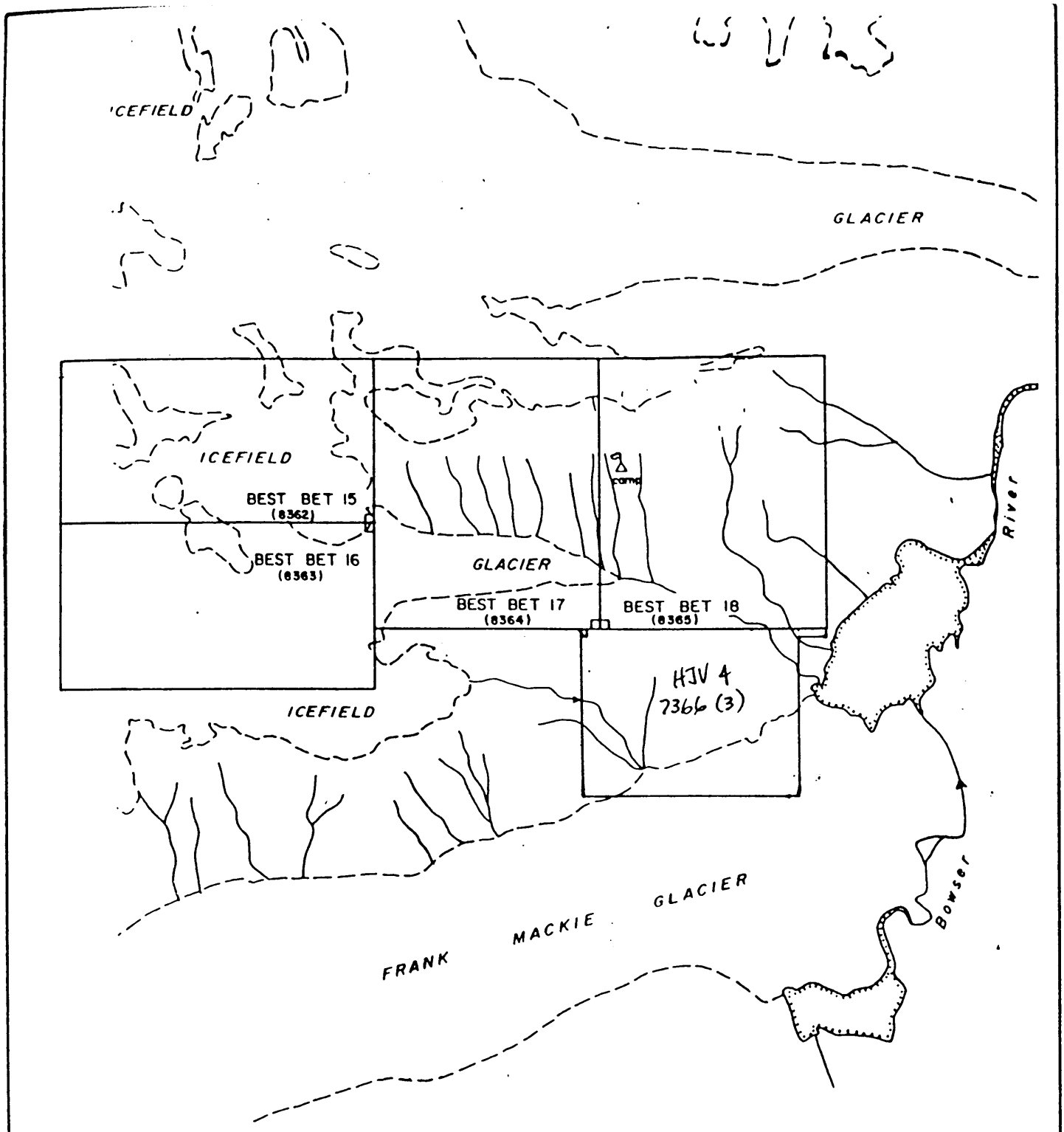
The claims are shown on Fig. 2 and are owned by Teuton Resources Corp. of Vancouver, British Columbia.

C. History

In 1966/67 the claim area formed part of a regional study by the B.C. Department of Mines under the direction of Ted Grove, P.Eng (Ref.3). A review of the standard geological and government references indicates there was no recorded work undertaken in the immediate vicinity of the property prior to this time.

The area remained dormant until the early 1980's when rising precious metal values prompted many exploration companies to


ESKAY CREEK DEPOSIT
Snippaker Airstrip
Harrymel Creek
Coulter Creek
King Creek
Sulphurets Creek
BRUCEJACK LAKE DEPOSIT
Mount Madge
Mount Knipple
130°00'
56°30'
Best Bet Property
UNUK RIVER
South Unuk River
Divalbliss Creek
Gracey Creek
Mount Frank Mackie
FRANK MACKIE GLACIER
Bowser River
Tide Airstrip
Mount Berendon
Mount Pearson
Dickens Peak
Mount Middleton
Mt. Blaine
B.C.
Alaska
STEWART DISTRICT MUNICIPALITY
Lake Creek
Ladue River
BRITISH COLUMBIA
Stewart
Property Location
Prince George
Vancouver
N
TEUTON RESOURCES
DELTA PROPERTY
LOCATION MAP
N.T.S. 104B-8E
SKEENA M.D., B.C.
0 5 10 KM.
Scale 1:250,000
Date: Oct. 1990
Drawn by:
Figure No.: 1
CHONG



N

TEUTON RESOURCES

DELTA PROPERTY

CLAIM MAP

N.T.S. 104B-8E

SKEENA M.D., B.C.

0 1 2 KM

Scale 1:50,000	Date : Oct. 1990
Drawn by :	Figure No. : 2

CHONG

initiate new reconnaissance programs. Teuton Resources staked the ground in 1982 under the presumption that geology similar to that occurring at the Sulphurets property 15 km to the north may have been exposed by retreating ice. [Note: During this period the Best Bet 17 & 18 claims were covered by the Delta and Alpha claims: the latter were inadvertently allowed to lapse by an optionee in 1989]. The assumption was partially confirmed by a prospecting expedition in 1983 which uncovered a large alteration zone made up, among other units, of sericite schists and pyritized sediments.

Geochemical stream sediment and rock character sampling during a reconnaissance program carried out in 1985 by Teuton Resources Corp. (Ref. 7) resulted in the discovery of a number of samples highly anomalous in gold and silver.

The property was optioned to Territorial Petroleum a year later. Territorial drilled a few short holes to test for extensions of a native gold occurrence noted the previous year on the topland in the northeastern quadrant of the claim. This program failed to uncover any economic mineralization. Reconnaissance investigations carried out at the same time were more fruitful. A soil geochem survey along 30 m topographic contours, sample interval 25 meters, disclosed a number of distinct +400 ppb gold anomalies (with roughly coincident silver, lead, and zinc anomalies), located in the western half of the Delta claim [now covered by Best Bet 17 claim]. Rock sampling in the center of one of the anomalies provided samples of up to 0.2 ounces per ton in a silicified tuff.

The property was re-optioned to Canarc Resources Corp. in 1989. During 1989-1990 Canarc carried out a comprehensive exploration program consisting of prospecting, sampling, trenching, geological mapping, geochemical surveys and both airborne and ground geophysical surveys. Several targets were located as a result of this work including two prominent IP-resistivity anomalies (with coincident Mag/VLF trends) in the "M" and "J" zones. Canarc dropped the option in early 1991 and the property revereted to Teuton.

D. References

1. ALLDRICK, D.J.(1984); Geological Setting of the Precious Metals Deposits in the Stewart Area, Paper 84-1, Geological Fieldwork 1983, B.C.M.E.M.P.R.

2. GROVE, E.W. ET AL (1982); Unuk River-Salmon River-Anyox Area. Geological Mapping 1:1000000 B.C.M.E.M.P.R.

3. GROVE, E.W.(1982); The Frankmackie Glacier Property, A Summary Report Compiled for Teuton Resources Corp. (Private).

4. GROVE, E.W. (1971); Geology of Mineral Deposits of the Stewart Area. Bulletin 58, B.C.M.E.M.P.R.

5. CREMONESE, D. (1983); Assessment Report on Prospecting Work on the Following Claims, Alpha #3619(112) and Delta #3622(11). NTS 104B/8E.

6. GROVES, W.D. & SHELDRAKE, R.(1984); Assessment Report on Geophysical Work (Airborne EM and Mag) on the Bowser River Properties of Teuton Resources Corp. NTS 104B/8E

7. CREMONESE, D., P.ENG. (1985); Assessment Report on Geological and Geochemical Work on the Alpha and Delta Claims, NTS 104B/8E.

8. CREMONESE, D., P.ENG., (1987); Assessment Report on Diamond Drilling Work on the Delta Claim, NTS 104B/8E. On file with Dept. of Energy, Mines & Petroleum Resources.

9. WILSON, JOHN & MCCROSSAN, ED (1990); Geological, Geochemical and Geophysical Report on the Delta Property near Stewart, British Columbia. Private Report for Canarc Resources Corp.

10.STANLEY, CLIFFORD R. (1987): PROBPLOT--An Interactive Computer Program to Fit Mixtures of Normal (or Log Normal) Distributions with Maximum Likelihood Optimization Procedures; Instruction Manual -- Association of Exploration Geochemists, Special Volume 14.

E. Summary of Work Done

The 1991 geochemical program on the property was undertaken by contractor Terra Nova Explorations under the supervision of geologist Brian Hall. This program was part of a larger work program carried out in the Frankmackie Glacier area on several properties owned by Teuton Resources Corp. and spanning the period from Sept. 29 to Oct. 11, 1991.

A base camp was mobilized by helicopter to the Four J's property, located a few kilometers south of the Best Bet claims. Pickets for the grid were prepared at base camp, and, after a brief weather delay, Brian Hall and two assistants were flown to the Best Bet claims by helicopter on Oct. 3, 1991. A grid was established (conformable with the 1990 Canarc grid) and 203 soil samples were collected. The crew was demobilized to base camp by helicopter.

The soil geochemical samples were shipped to the Eco-Tech facility in Kamloops where they were analysed for gold content by standard AA techniques, as well as for 30 elements by I.C.P. (Inductively Coupled Argon Plasma).

2. TECHNICAL DATA AND INTERPRETATION

A. Regional Geology

The Best Bet claims lie in the Stewart area east of the Coast Crystalline Complex and within the western onlap boundary of the Bowser Basin. Rocks exposed in the area belong to the Mesozoic Hazelton Group and have been folded on regional NW-SE axes, cut by faults and selective tectonism, locally hydrothermalized and intruded by plugs of both Cenozoic and Mesozoic age.

Locally, within the Hazelton Group, Lower Jurassic volcanic and sedimentary rocks of the Unuk River Formation are unconformably overlain by the Middle Jurassic marine and non-marine volcanics and sediments of the Betty Creek Formation, the volcano-sedimentary Upper Jurassic Salmon River Formation, and the post-accretion fine clastic basinal Nass Formation.

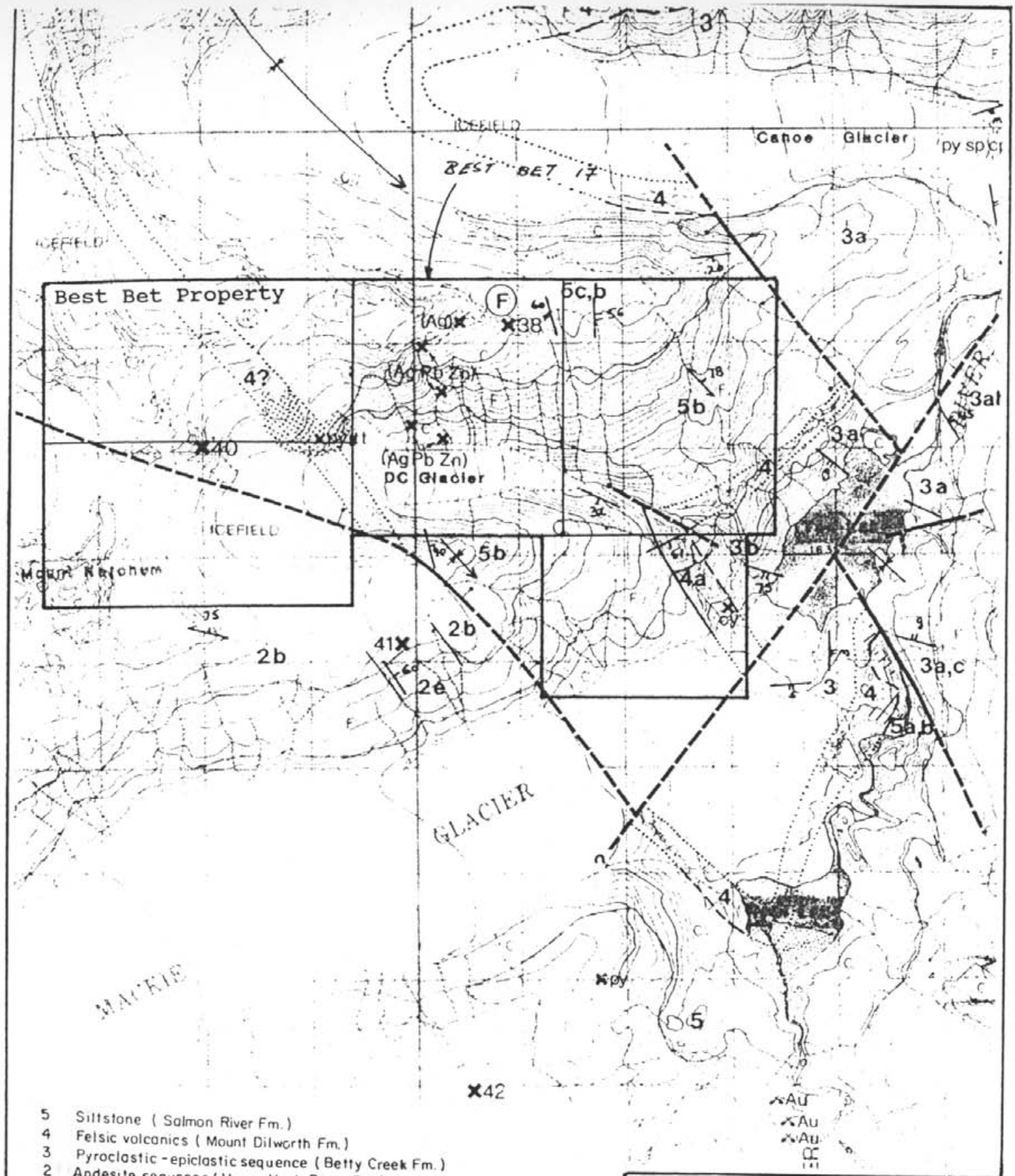
The oldest rocks in the area belong to the Lower Jurassic Unuk River Formation which forms a north-northwesterly trending belt extending from Alice Arm to the Iskut River. It consists of green, red and purple volcanic breccia, conglomerate, sandstone and siltstone with minor crystal and lithic tuff, limestone, chert and coal. Also included in the sequence are pillow lavas and volcanic flows.

In the study area the Unuk River Formation is overlain by Lower Middle and Middle Jurassic rocks from the Betty Creek and Salmon River Formations, respectively. A variable to high angle unconformity is in places traceable between the underlying (steeper) Unuk River cycle of volcanics and overlying (flatter) cycle of often similar-looking Betty Creek volcanics. Geometry of the interface between the Betty Creek and overlying Salmon River is, at most, somewhat disconformable: the Nass Formation overlies as a sedimentary quiet basin-filling onlap with only a relatively minor erosional component from the island-arc and/or accreted terrane.

The Betty Creek Formation consists of submarine pillow lavas, broken pillow breccias, andesitic and basaltic flows, plus (emergent) green, red and purple volcanic breccia, conglomerate, sandstone and siltstone with minor crystal and lithic tuff, limestone, chert and coal. Also included in the sequence are pillow lavas and volcanic flows.

According to Grove (Ref. 2 & 3), the majority of the rocks from the Hazelton Group were derived from the Hazelton age andesitic volcanoes subsequently rapidly eroding to form overlapping lenticular sedimentary wedges varying laterally in grain size from breccia to siltstone.

Intrusives in the region are dominated by the granodiorite of


Best Bet Property
BEST BET 17
Canoe Glacier
ICEFIELD
Mount Kerkham
(Ag Pb Zn)
DC Glacier
FRANK MACKIE GLACIER
5 Siltstone (Salmon River Fm.)
4 Felsic volcanics (Mount Dilworth Fm.)
3 Pyroclastic - epiclastic sequence (Betty Creek Fm.)
2 Andesite sequence (Upper Unuk River Fm.)
x Mineral occurrence
After Britton & Alldrick, 1988
N
TEUTON RESOURCES
BEST BET PROPERTY
GEOLOGY
FRANK MACKIE GLACIER AREA
N.T.S. 104B - 8E
SKEENA M.D., B.C.
0 1 2 KM.
Scale 1:50,000
Date : Oct. 1990
Drawn by :
Figure No. : 3

the Coast Plutonic Complex (to the west). Some of the smaller intrusive plugs in the study area range from quartz monzonite to granite and are likely related outlyer processes associated with the Coast Plutonic Complex.

Regional geology is presented in this report in Fig. 3.

B. Property Geology

In general, the western margin of the property is underlain by Lower Jurassic volcanics and sediments of the Unuk River Formation. These rocks are unconformably overlain to the east by Middle Jurassic sediments of the Salmon River Formation. The sediments have been folded into synclines and anticlines with northerly trending fold axes. Small Eocene feldspar porphyry intrusions, important as mineralizers in the region, outcrop in the northwest quadrant of the Best Bet 17 claim.

C. Geochemistry - Soil Samples

a. Introduction

Grid references were taken from the grid established during the 1989-90 surface exploration program operated by former optionee Canarc Resources Corp. Because of time constraints, the re-established grid was confined to a specific area of interest: between Lines 250S--900S and Stations 200W--1000W. This area coincided with the two IP-Resisitivity anomalies detected in the 1990 ground geophysical surveys. Object of the 1991 exploration program was to test this favourable zone for coincident soil geochem anomalies. Snow cover, steep terrain and rock outcrop precluded a complete investigation of the grid area selected. Nevertheless, 203 geochem soil samples were collected from 11 lines of varying length. Sampling was done at 25m intervals where possible.

Grid location relative to claim lines was fixed according to field altimeter readings and reference to airphotos.

b. Treatment of data

Values for gold, silver, arsenic, copper, lead, and zinc have been plotted in this report on Figs. 4 to 9, respectively. The data is presented on maps drawn at a scale of 1 to 5,000 and is shown in relation to stream courses and claim lines.

The numerical values for each of the sample sites have been contoured using the Probplot computer program (Ref. 10). Contour levels were chosen empirically for each element after reference to

results of several other soil geochem programs carried out in the region over the past ten years. This has been found to be a better method for delineating anomalous areas than the rigorous standard application of statistical methods.

c. Discussion

A strong gold anomaly is evident between Lines 300S--500S and Stations 475W--625W, coincident with the "M" zone IP-Resistivity anomaly discovered by Canarc crews in 1990. Nine sample sites within the core of this anomaly exceed 600 ppb gold, maximum value being 4850 ppb. The Fig. 4 gold computer contour plot shows a weaker anomaly, values between 150 ppb and 660 ppb, extending south from the western edge of the 600+ ppb core anomaly to the end of the grid on Line 900S. This may be either a typical downslope dispersion effect or evidence that the source continues in a southward direction.

A smaller, but intense, gold anomaly is centered on Line 850S, Stations 850 and 875W (gold values of 1,535 and 1,275 ppb, respectively). This geochem anomaly coincides well with the "J" IP-Resistivity anomaly discovered in 1990. Size of this anomaly is indeterminate at the present time due to its location near the southwestern edge of the grid. It may represent a faulted extension of the source of the "M" zone geochem anomaly, an interpretation that is supported by the mag data contours established by the 1990 ground geophysical surveys. For reference, a 1990 grab sample from an outcrop of tightly folded felsic tuffs taken within this area ran 1.767 oz/ton gold [Sample "DJ"]--it may well be related to the source of the geochem anomaly.

The silver plot on Fig. 5 shows a very good correlation with the gold plot. Two main anomalous areas are apparent, much like those on Fig. 4; the larger anomaly even has a downslope dispersion pattern similar to that in the gold plot. However, there is also a third silver anomaly evident in the northwest portion of the grid extending to the boundaries of the area tested. Anomalous silver values ranged up to a maximum value of 8.0 ppm at Line 350S, Station 600W.

The arsenic (Fig. 6), lead (Fig. 8) and zinc (Fig. 7) plots share a roughly similar pattern which is distinct from those for gold and silver. In general the most consistently anomalous values occur in the northwest portion of the grid between Stations 725 and 900W attentuating, with random highs in between, downslope in a SSE direction. The lead and zinc plots, and to a lesser extent the arsenic plot, also show anomalies coinciding with the two prime gold anomalies. Interestingly, the highest spot value for arsenic, lead and zinc occurs at Line 900S, Station 925W: 865 ppm As, 1374 ppm Pb and 2086 ppm Zn.

Copper contours, plotted on Fig. 7, show weaker anomalies clustered within the three silver anomalies more prominently expressed in Fig. 6. The copper-silver correlation may be due to tetrahedrite mineralization of the kind noted in small quartz veins throughout the property. Maximum value of 285 ppm copper occurs at Line 400S, Station 525W.

It should also be noted that metal values for all elements tested are at background levels in the easternmost portion of the grid between Stations 200W to 425W. This area is underlain by a sedimentary unit consisting of black argillites, wacke, siltstone and mudstone. By contrast, the more geochemically active area to the west is underlain by volcanic units, primarily crystal lithic tuffs (some lapilli tuff) and schist (quartz-sericite-pyrite).

D. Field Procedure and Laboratory Technique

Soil samples were taken in the field by digging with a mattock to the "C" soil horizon (poorly developed for the most part), with samples running approximately 300 to 500 grams of material. This was then placed into a standard Kraft Bag. The bags were then marked, allowed to dry, and shipped by bus to Vancouver for analysis at the Acme Analytical Laboratories facility on 852 East Hastings Street.

After standard sample preparation for soils, a .500 gram subsample was digested with 3ml of 3-1-2 HCl-HNO3-H20 at 95 degrees Centigrade for one hour, then diluted to 10 ml with water. The resulting solution was tested by Inductively Coupled Argon Plasma to yield quantatitive results for 30 elements. Gold was analysed by standard atomic absorption methods from a 10 gram subsample.

E. Conclusions

The 1991 geochemical soil survey located two distinct gold anomalies with overlapping Ag-Cu-(As)-Pb-Zn anomalies. A silver anomaly with coincident Pb-Zn-As-(Cu) highs is also present in the northwest corner of the grid area. The two gold geochem anomalies also correspond with two IP-Resistivity anomalies located during a ground geophysical survey conducted late in the field season the previous year (1990). The lower of the two gold anomalies overlaps the area where a 1990 grab sample returned values of 1.767 oz/ton Au.

More work is warranted to follow up the coincident geochemical and geophysical anomalies. This work should include further geochemical soil sampling and IP-Resistivity surveys both on untested portions of the 1991 grid as well as grid extensions along anomalous trends. This program should be supplemented by prospecting for the source of the anomalous responses, rock geochem

sampling, trenching and geological mapping. A favourable outcome would lead to a second phase of diamond drilling of selected targets.

Respectfully submitted,

D. Cremonese, P.Eng.
April 15, 1992

APPENDIX I -- WORK COST STATEMENT

Field Personnel--Period Sept. 29 to Oct. 11, 1991:	
B. Hall, Geologist	
2 days @ $321/day	$645
B. Sauer, Assistant	
2 days @ $187/day	374
M. Gray, Assistant	
2 days @ $187/day	374
Helicopter -- VIH/Stewart Base	
Crew drop-offs/pick-up	
1.4 hrs @ $771/hr.	1,079
Food -- 6 man-days @ $25/man-day	150
Personnel: mob/demob (home base to Stewart, return)	
(prorated with other projects where applicable)	900
Assays--Eco-Tech Labs, Kamloops, B.C.	
Geochem Au, I.C.P. and soil sample preparation	
203 @ $13.25 sample	2,690
Report Costs	
Report and map preparation, compilation and research	
D. Cremonese, P.Eng., 2.5 days @ $350/day	875
Draughting/Geochem Contouring -- RPM Computer	240
Word Processor - 4 hrs. @ $25/hr.	100
Copies, report, jackets, maps, etc.	40
TOTAL.....	**$ 7,467**

Amount Claimed Per Statement of Exploration: $7,200

APPENDIX II - CERTIFICATE

I, Dino M. Cremonese, do hereby certify that:

1. I am a mineral property consultant with an office at Suite 509-675 W. Hastings, Vancouver, B.C.

2. I am a graduate of the University of British Columbia (B.A.Sc. in metallurgical engineering, 1972, and L.L.B., 1979).

3. I am a Professional Engineer registered with the Association of Professional Engineers of the Province of British Columbia as a resident member, #13876.

4. I have practiced my profession since 1979.

5. This report is based upon work carried out on the Best Bet 17 & 18 claims, Skeena Mining Division in October of 1991. Reference to field notes and maps made by geologist Brian Hall is acknowledged. I have full confidence in the abilities of all samplers used in the 1991 geochemical program and am satisfied that all samples were taken properly and with care.

6. I am a principal of Teuton Resources Corp., owner of the Best Bet claims: this report was prepared solely for satisfying assessment work requirements in accordance with government regulations.

Dated at Vancouver, B.C. this 15th day of April, 1992.

D. Cremonese, P.Eng.

Appendix III

Assay Certificates

ECO-TECH LABORATORIES LTD.
10041 EAST TRANS CANADA HWY.
KAMLOOPS, B.C. V2C 2J3
PHONE - 604-573-5700
FAX - 604-573-4557

OCTOBER 18,1991

TEUTON RESOURCES CORP. - ETK 91-811
602 - 675 WEST HASTINGS STREET
VANCOUVER, B.C.
V6B 1N2

VALUES IN PPM UNLESS OTHERWISE REPORTED

PROJECT: DELTA
203 SOIL SAMPLES RECEIVED OCTOBER 9, 1991

ET#	DESCRIPTION	AU(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1	- D L 250N- 575E	105	1.6	1.01	100	6	85	<5	.27	1	27	10	109	5.77	.02	<10	.49	883	3	<.01	28	1290	196	40	<20	14	.01	<10	31	<10	4	273
2	- D L 250N- 600E	145	1.4	1.14	135	6	75	<5	.20	<1	28	13	120	5.96	.01	<10	.54	749	4	<.01	33	1470	188	40	<20	12	.01	<10	37	<10	<1	289
3	- D L 250N- 625E	70	1.4	.22	285	6	90	<5	.20	<1	18	1	94	9.50	<.01	10	.18	1139	3	<.01	11	3990	722	65	<20	11	<.01	<10	12	<10	<1	237
4	- D L 250N- 650E	265	2.6	.69	310	8	105	<5	.26	2	38	5	268	8.99	<.01	10	.39	1776	15	<.01	41	1620	256	95	<20	24	<.01	<10	24	<10	3	392
5	- D L 250N- 675E	200	1.0	2.11	165	6	165	<5	.75	2	32	7	131	5.64	.03	10	1.05	1642	2	<.01	15	1610	194	20	<20	24	.02	<10	82	<10	7	371
6	- D L 250N- 700E	110	1.0	2.10	255	6	215	<5	.90	3	34	8	137	5.70	<.01	10	1.23	2261	1	<.01	14	1880	242	25	<20	30	.02	<10	80	<10	7	427
7	- D L 250N- 725E	85	1.0	2.07	340	8	280	<5	1.00	3	36	8	136	5.85	<.01	10	1.28	2345	1	<.01	15	2030	246	25	<20	30	.01	<10	80	<10	7	479
8	- D L 250N- 775E	95	1.0	2.14	375	8	250	<5	2.08	2	33	8	132	5.64	<.01	10	1.50	2095	1	<.01	14	1970	234	25	<20	47	.01	<10	83	<10	5	435
9	- D L 250N- 800E	120	1.2	1.94	345	8	230	<5	1.36	2	32	7	129	5.70	<.01	10	1.28	2042	1	<.01	13	1970	234	20	<20	36	.01	<10	76	<10	5	403
10	- D L 250N- 850E	55	1.8	2.22	515	8	315	<5	1.13	3	38	7	163	6.15	<.01	10	1.43	2830	1	<.01	15	2090	438	30	<20	35	.01	<10	93	<10	4	502
11	- D L 250N- 875E	160	3.4	2.08	715	6	350	<5	.93	6	41	6	172	6.35	<.01	10	1.33	3380	1	<.01	14	2080	1068	60	<20	33	.01	<10	80	<10	4	776
12	- D L 250N- 900E	70	1.8	1.76	310	6	380	<5	.94	3	37	7	147	5.61	<.01	10	1.22	2749	1	<.01	16	2150	376	20	<20	36	.01	<10	66	<10	4	635
13	- D L 300N- 525E	165	.6	1.15	80	4	65	<5	.19	<1	18	10	84	5.59	.03	10	.58	743	3	.01	17	1450	96	30	<20	11	.01	<10	31	<10	2	141
14	- D L 300N- 550E	120	3.0	.68	135	6	90	<5	.40	5	33	6	137	6.10	.01	<10	.37	1155	3	<.01	27	1720	582	125	<20	21	<.01	<10	26	<10	2	741
15	- D L 300N- 575E	130	2.0	.90	140	4	85	<5	.27	1	28	9	128	5.82	.01	10	.42	1244	6	<.01	28	1530	176	40	<20	12	<.01	<10	29	<10	1	277
16	- D L 300N- 625E	345	2.2	.53	265	6	140	<5	.26	2	28	<1	123	7.23	<.01	10	.28	2201	5	<.01	11	1410	208	40	<20	16	<.01	<10	18	<10	<1	357
17	- D L 300N- 650E	80	1.0	2.24	285	4	210	<5	1.13	2	32	8	122	5.75	<.01	10	1.33	1874	<1	<.01	12	1710	248	20	<20	31	.03	<10	88	<10	7	447
18	- D L 300N- 675E	100	1.0	2.09	360	4	235	<5	.66	3	37	8	143	6.06	<.01	10	1.32	2420	1	<.01	15	1980	282	25	<20	26	.02	<10	81	<10	7	538
19	- D L 300N- 700E	230	1.0	2.18	315	6	255	<5	.82	3	35	8	131	5.83	<.01	20	1.31	2006	1	.02	14	1800	246	20	<20	29	.03	<10	82	<10	8	468
20	- D L 300N- 725E	110	1.8	1.98	675	10	300	<5	.94	5	38	7	149	6.07	<.01	10	1.27	2636	1	<.01	16	1960	404	30	<20	39	.01	<10	75	<10	6	602
21	- D L 300N- 750E	75	1.4	2.08	670	4	290	<5	1.33	4	36	7	152	5.94	<.01	10	1.42	2220	1	<.01	15	2120	412	35	<20	39	.01	<10	79	<10	4	548
22	- D L 300N- 775E	100	1.8	1.97	340	4	270	<5	1.40	3	34	8	132	5.60	<.01	10	1.27	2164	1	<.01	15	1920	342	30	<20	35	.01	<10	76	<10	5	451
23	- D L 300N- 800E	110	2.2	2.01	510	4	290	<5	1.87	4	37	7	146	5.97	<.01	10	1.30	2579	1	<.01	16	1940	566	40	<20	50	.01	<10	76	<10	3	545
24	- D L 350N- 475E	405	1.0	.66	130	4	50	<5	.18	1	34	2	167	6.80	<.01	10	.43	1415	8	<.01	28	1480	76	15	<20	5	<.01	<10	10	<10	<1	134
25	- D L 350N- 500E	375	1.0	.67	105	6	40	<5	.17	1	28	2	148	6.18	<.01	10	.50	1052	7	<.01	22	1430	72	10	<20	5	<.01	<10	16	<10	<1	148
26	- D L 350N- 525E	135	.6	1.01	100	6	90	<5	.49	1	34	4	138	5.89	.02	10	.68	1797	3	<.01	16	1990	74	20	<20	16	<.01	<10	46	<10	9	168

ET#	DESCRIPTION	AU(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
27	D L 350N- 550E	60	2.0	.54	110	8	115	<5	.67	6	36	3	97	5.77	.01	10	.40	2087	1	<.01	15	2500	258	60	<20	23	<.01	<10	36	<10	5	602
28	D L 350N- 575E	70	1.6	.60	100	6	210	<5	.41	1	31	3	71	5.74	.03	10	.33	5230	6	<.01	15	1430	72	20	<20	27	<.01	<10	71	<10	3	179
29	D L 350N- 600E	635	8.0	.49	370	6	110	<5	.06	<1	22	3	150	7.68	<.01	10	.26	752	16	.01	16	1740	254	65	<20	20	<.01	<10	18	<10	<1	232
30	D L 350N- 625E	935	2.6	.58	355	6	120	<5	.13	1	46	<1	95	11.90	<.01	20	.33	4675	12	<.01	10	2100	178	20	<20	12	<.01	<10	12	<10	<1	207
31	D L 350N- 650E	65	1.0	2.55	225	8	180	<5	.88	2	38	12	143	5.71	.01	10	1.41	1855	1	<.01	19	1450	212	20	<20	19	.03	<10	96	<10	6	393
32	D L 350N- 675E	135	.8	1.92	295	6	220	<5	.65	2	32	8	124	5.43	<.01	10	1.21	1944	<1	.01	17	1960	208	25	<20	24	.02	<10	73	<10	7	402
33	D L 350N- 700E	90	1.2	1.77	395	8	270	<5	.68	3	33	6	128	5.52	<.01	20	1.05	2160	1	.03	14	2180	292	25	<20	27	.02	<10	66	<10	9	416
34	D L 350N- 725E	180	1.6	1.91	405	8	325	<5	.65	4	36	8	134	5.77	<.01	10	1.26	2330	1	<.01	16	2190	338	25	<20	24	.02	<10	77	<10	6	461
35	D L 350N- 750E	90	2.0	1.85	440	6	235	<5	.62	4	34	7	135	5.89	<.01	20	1.18	2310	1	<.01	14	2190	494	15	<20	24	.02	<10	76	<10	6	509
36	D L 350N- 775E	105	1.8	1.70	415	6	210	<5	.63	3	33	6	128	5.72	<.01	20	1.10	2136	1	<.01	13	2280	480	15	<20	24	.02	<10	72	<10	6	459
37	D L 350N- 800E	110	1.8	1.74	405	8	205	<5	.62	3	32	7	128	5.72	<.01	20	1.13	2085	1	<.01	14	2270	466	35	<20	23	.02	<10	73	<10	6	457
38	D L 350N- 825E	205	2.0	1.73	400	6	210	<5	.62	4	32	7	127	5.67	<.01	20	1.10	2100	1	<.01	14	2240	446	35	<20	24	.02	<10	73	<10	6	449
39	D L 350N- 850E	95	1.8	1.78	465	4	225	<5	.63	4	34	7	138	5.95	<.01	20	1.19	2238	1	<.01	15	2270	532	40	<20	26	.02	<10	75	<10	5	507
40	D 400N- 200E	5	<.2	1.83	30	4	75	<5	.28	<1	27	56	49	4.36	.03	10	.97	751	1	.01	92	1140	30	5	<20	36	<.01	<10	33	<10	<1	111
41	D 400N- 225E	20	.2	1.81	25	6	80	<5	.30	<1	29	57	58	4.71	.04	10	.92	957	1	<.01	92	1130	28	5	<20	34	<.01	<10	32	<10	2	131
42	D 400N- 250E	5	.2	1.53	25	4	60	<5	.28	<1	29	46	54	4.57	.03	10	.81	974	1	.01	90	1300	28	5	<20	34	<.01	<10	27	<10	1	123
43	D 400N- 275E	<5	<.2	1.84	25	8	60	<5	.25	<1	28	61	52	4.29	.02	10	1.04	747	1	<.01	94	1050	28	5	<20	30	<.01	<10	34	<10	<1	109
44	D 400N- 300E	<5	.2	1.92	30	6	85	<5	.24	<1	34	61	60	5.02	.04	10	.91	864	1	.01	104	1350	34	10	<20	34	<.01	<10	36	<10	<1	126
45	D 400N- 325E	<5	.2	1.48	55	6	85	<5	.32	<1	34	43	63	5.23	.03	10	.75	983	1	<.01	117	1420	34	10	<20	41	<.01	<10	27	<10	1	146
46	D 400N- 350E	<5	.4	1.55	35	6	120	<5	.28	<1	48	29	63	5.21	.04	10	.81	2409	2	<.01	98	1160	24	10	<20	35	<.01	<10	23	<10	1	156
47	D 400N- 375E	5	.4	1.63	40	6	110	<5	.25	1	47	37	77	5.41	.04	10	.79	2214	2	.01	118	1250	32	10	<20	32	<.01	<10	27	<10	2	168
48	D 400N- 400E	125	.4	1.67	40	6	110	<5	.26	1	46	38	78	5.49	.04	10	.81	2112	2	<.01	116	1260	30	10	<20	34	<.01	<10	28	<10	2	171
49	D 400N- 425E	10	.6	1.42	45	6	100	<5	.16	<1	49	38	86	6.32	.03	10	.61	2092	2	.01	121	1690	38	10	<20	24	<.01	<10	26	<10	<1	172
50	D 400N- 450E	85	.8	.68	90	6	30	<5	.06	<1	18	4	105	5.04	<.01	10	.50	692	7	.01	20	1380	62	15	<20	4	<.01	<10	13	<10	<1	112
51	D 400N- 475E	250	2.8	.49	145	6	50	<5	.12	<1	18	1	124	6.83	<.01	10	.37	734	9	<.01	18	1550	212	20	<20	6	<.01	<10	10	<10	<1	255
52	D 400N- 500E	800	2.4	1.47	145	8	115	<5	.39	4	28	6	262	6.07	.03	10	1.04	1891	6	<.01	18	1670	134	15	<20	18	<.01	<10	46	<10	5	278
53	D 400N- 525E	1170	2.2	1.49	155	8	120	<5	.39	4	30	7	285	6.43	.02	20	1.05	2006	7	<.01	18	1800	144	20	<20	18	<.01	<10	47	<10	6	283
54	D 400N- 550E	865	1.8	1.47	145	8	115	<5	.36	4	27	7	268	6.16	.02	10	1.06	1868	6	<.01	20	1680	136	20	<20	16	<.01	<10	46	<10	5	272
55	D 400N- 575E	4850	3.0	1.17	175	10	80	<5	.38	3	30	6	208	6.28	<.01	10	.89	1542	5	<.01	22	1600	114	25	<20	18	<.01	<10	39	<10	2	250
56	D 400N- 600E	2510	4.2	1.15	180	8	85	<5	.37	4	30	4	196	6.30	<.01	10	.87	1611	5	<.01	21	1650	124	25	<20	16	<.01	<10	39	<10	2	258
57	D 400N- 625E	380	4.8	.29	260	8	60	<5	.08	1	27	<1	205	6.98	<.01	10	.20	1002	15	<.01	16	1440	130	55	<20	11	<.01	<10	11	<10	<1	210
58	D 400N- 650E	275	1.8	.96	175	6	145	<5	.48	1	30	3	92	5.87	<.01	10	.60	1601	2	<.01	14	1510	86	20	<20	16	.01	<10	34	<10	1	197
59	D 400N- 675E	555	.8	2.26	340	6	185	<5	.81	2	39	7	164	6.04	<.01	10	1.34	1964	<1	<.01	18	1700	158	25	<20	23	.03	<10	94	<10	5	335
60	D 400N- 725E	205	1.0	2.06	430	8	320	<5	.65	3	36	9	150	5.94	<.01	20	1.30	1939	1	.01	19	1780	288	25	<20	26	.02	<10	79	<10	8	436
61	D 400N- 750E	105	1.4	2.02	345	8	225	<5	.63	3	33	7	123	5.93	<.01	20	1.22	1970	1	.01	15	1900	306	25	<20	28	.04	<10	81	<10	9	419
62	D 400N- 775E	85	1.4	1.83	525	6	235	<5	1.18	4	35	6	155	6.27	<.01	10	1.17	2740	1	<.01	15	1790	610	30	<20	32	.01	<10	92	<10	5	571
63	D 400N- 800E	35	1.0	2.01	265	8	185	<5	.84	2	30	9	185	5.63	<.01	10	1.29	1713	1	<.01	15	1830	266	20	<20	29	.02	<10	80	<10	5	339

ET#	DESCRIPTION	AU(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
64 -	D 450N- 200E	50	.2	1.80	20	8	60	<5	.25	<1	34	57	56	4.30	.02	<10	.94	853	1	<.01	110	1150	22	5	<20	32	<.01	<10	31	<10	1	114
65 -	D 450N- 225E	45	.2	1.87	25	8	70	<5	.22	<1	32	60	56	4.41	.03	10	.98	904	1	<.01	97	1150	24	10	<20	29	<.01	<10	34	<10	<1	111
66 -	D 450N- 250E	20	<.2	1.83	20	8	65	<5	.24	<1	30	60	51	4.19	.03	10	1.00	773	1	<.01	95	1140	24	5	<20	31	<.01	<10	33	<10	<1	106
67 -	D 450N- 275E	35	.2	2.01	30	8	90	<5	.25	<1	36	64	63	4.99	.03	10	1.03	1046	1	<.01	109	1390	26	10	<20	35	<.01	<10	36	<10	<1	126
68 -	D 450N- 300E	30	.2	2.05	25	6	105	<5	.33	<1	36	62	62	5.09	.06	10	.98	1015	1	<.01	115	1320	30	10	<20	44	<.01	<10	36	<10	1	132
69 -	D 450N- 325E	20	.2	1.91	30	8	60	<5	.26	<1	28	65	68	4.87	.02	10	1.06	601	1	<.01	101	1170	34	5	<20	33	<.01	<10	38	<10	<1	125
70 -	D 450N- 350E	25	.2	1.55	50	6	105	<5	.31	<1	36	45	65	5.37	.04	10	.77	1036	1	<.01	127	1310	34	5	<20	42	<.01	<10	28	<10	1	154
71 -	D 450N- 375E	15	.2	1.80	40	6	105	<5	.35	<1	39	39	71	5.41	.06	10	.87	1360	1	.01	105	1250	24	10	<20	46	<.01	<10	27	<10	2	149
72 -	D 450N- 400E	10	.4	1.84	30	8	95	<5	.09	<1	50	42	71	5.33	.04	10	.91	1716	2	.01	104	1030	30	10	<20	19	<.01	<10	30	<10	<1	152
73 -	D 450N- 425E	20	.4	1.57	45	6	120	<5	.15	1	49	39	84	5.82	.05	10	.68	1648	2	.01	127	1390	36	15	<20	25	<.01	<10	27	<10	1	183
74 -	D 450N- 450E	20	.6	1.43	40	6	95	<5	.15	1	31	20	82	5.26	.04	10	.67	1387	6	.01	79	1130	38	10	<20	16	<.01	<10	22	<10	3	210
75 -	D 450N- 475E	10	1.4	.60	105	6	50	<5	.03	<1	19	3	67	5.69	<.01	10	.37	856	7	<.01	32	1280	112	25	<20	5	<.01	<10	13	<10	<1	185
76 -	D 450N- 500E	245	2.6	1.01	135	4	105	<5	.26	7	27	5	200	6.75	.02	10	.73	2799	13	<.01	37	1520	314	20	<20	12	<.01	<10	25	<10	6	782
77 -	D 450N- 525E	715	2.6	1.21	165	6	55	<5	.11	1	29	7	216	6.49	<.01	10	.90	1474	8	<.01	20	1710	120	20	<20	4	<.01	<10	34	<10	<1	219
78 -	D 450N- 550E	370	1.2	.86	140	6	100	<5	.26	2	31	4	140	6.18	.01	10	.58	1690	6	<.01	26	1560	102	20	<20	9	<.01	<10	23	<10	3	702
79 -	D 450N- 575E	325	3.0	.49	235	6	95	<5	.12	<1	30	1	186	6.93	<.01	10	.31	1320	14	.01	22	1660	120	40	<20	11	<.01	<10	17	<10	<1	233
80 -	D 450N- 600E	450	5.4	.43	250	6	100	<5	.19	2	33	2	164	6.96	<.01	10	.26	1663	10	.01	18	1330	134	70	<20	12	<.01	<10	14	<10	<1	297
81 -	D 450N- 625E	210	1.6	.60	170	6	95	<5	.33	1	29	<1	65	6.30	<.01	<10	.39	1458	3	<.01	9	1290	126	40	<20	12	<.01	<10	21	<10	<1	290
82 -	D 450N- 650E	430	.8	1.76	285	4	160	<5	.88	<1	38	6	121	6.06	<.01	10	1.08	1880	2	<.01	15	1670	110	25	<20	20	.01	<10	73	<10	3	242
83 -	D 500N- 200E	15	.2	1.62	25	8	75	<5	.20	<1	45	53	56	4.46	.02	<10	.84	1213	1	.01	100	1080	22	5	<20	23	<.01	<10	30	<10	1	134
84 -	D 500N- 225E	15	.2	1.85	20	6	65	<5	.14	<1	41	58	59	4.65	.03	<10	.92	1015	1	.01	102	1090	20	10	<20	21	<.01	<10	32	<10	<1	128
85 -	D 500N- 250E	5	<.2	1.70	15	6	55	<5	.24	<1	29	58	47	3.99	.02	<10	.95	743	1	.01	90	1080	18	5	<20	26	<.01	<10	32	<10	<1	107
86 -	D 500N- 275E	10	.2	1.99	20	6	80	<5	.16	<1	38	61	63	4.67	.04	10	.97	1058	1	<.01	107	1220	24	5	<20	25	<.01	<10	35	<10	2	142
87 -	D 500N- 300E	5	.2	1.90	20	8	85	<5	.23	<1	33	59	56	4.77	.04	10	.94	960	1	.01	101	1180	24	10	<20	30	<.01	<10	35	<10	<1	131
88 -	D 500N- 325E	5	.2	1.93	30	6	75	<5	.21	<1	41	60	66	5.09	.04	10	.94	1122	1	.01	111	1180	28	10	<20	28	<.01	<10	36	<10	<1	144
89 -	D 500N- 350E	5	.2	1.02	45	6	80	<5	.29	<1	35	34	51	4.57	.02	10	.53	1015	1	<.01	111	1210	24	10	<20	30	<.01	<10	21	<10	1	145
90 -	D 500N- 375E	5	.4	1.84	30	4	110	<5	.14	<1	54	38	71	5.77	.05	10	.87	2266	2	.01	109	1190	22	10	<20	23	<.01	<10	28	<10	<1	194
91 -	D 500N- 400E	5	.2	1.77	30	4	105	<5	.12	<1	48	41	72	5.63	.05	10	.80	1649	2	.01	113	1210	24	10	<20	21	<.01	<10	28	<10	<1	184
92 -	D 500N- 425E	5	.4	2.03	30	6	90	<5	.07	<1	35	54	79	5.82	.05	10	.90	795	3	.01	99	1390	32	10	<20	18	<.01	<10	34	<10	<1	173
93 -	D 500N- 450E	35	.6	.85	50	6	45	<5	.08	1	18	10	45	4.17	.01	<10	.48	823	4	<.01	34	900	82	10	<20	7	<.01	<10	14	<10	<1	270
94 -	D 500N- 475E	245	1.6	.75	110	4	60	<5	.16	2	27	6	131	6.07	<.01	10	.47	1408	12	<.01	35	1570	168	20	<20	9	<.01	<10	21	<10	<1	328
95 -	D 500N- 500E	260	1.6	1.15	125	6	75	<5	.14	3	25	8	159	5.41	.01	10	.80	1360	13	<.01	30	1350	132	20	<20	6	<.01	<10	34	<10	1	357
96 -	D 500N- 525E	1815	4.6	1.08	135	6	55	<5	.19	4	28	6	163	5.59	<.01	10	.79	1673	8	<.01	26	1320	800	20	<20	9	<.01	<10	30	<10	1	470
97 -	D 500N- 550E	245	2.2	.65	165	6	95	<5	.19	5	33	2	142	6.72	<.01	10	.42	2338	9	<.01	31	1480	156	30	<20	11	<.01	<10	18	<10	2	406
98 -	D 500N- 575E	35	.8	.49	90	4	85	<5	.12	4	21	<1	49	6.56	.02	10	.17	4087	8	<.01	59	1220	38	30	<20	10	<.01	<10	1	<10	13	385
99 -	D 500N- 600E	50	.8	.75	105	4	70	<5	.20	1	42	1	101	8.29	.02	10	.26	4108	7	.01	52	1570	38	30	<20	15	<.01	<10	7	<10	13	357
100-	D 550N- 200E	700	2.0	1.44	140	6	100	<5	.37	3	27	7	234	5.92	.03	10	1.01	1773	6	<.01	16	1610	122	20	<20	16	<.01	<10	45	<10	5	282

MT#	DESCRIPTION	AU(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
101-	D 550N- 225E	55	2.2	.59	135	4	50	<5	.12	<1	27	2	131	6.82	<.01	10	.38	1150	10	<.01	19	1520	250	20	<20	6	<.01	<10	11	<10	<1	349
102-	D 550N- 250E	15	.2	1.82	20	6	70	<5	.26	<1	28	57	49	4.36	.03	<10	.96	758	1	<.01	91	1120	26	10	<20	33	<.01	<10	33	<10	<1	116
103-	D 550N- 275E	10	<.2	1.77	20	6	65	<5	.28	<1	26	56	47	4.27	.03	<10	.93	687	1	<.01	90	1150	22	5	<20	34	<.01	<10	33	<10	<1	113
104-	D 550N- 300E	15	<.2	1.90	15	8	70	<5	.26	<1	27	58	49	4.27	.04	<10	.97	994	1	<.01	85	1060	22	10	<20	32	.01	<10	35	<10	1	115
105-	D 550N- 325E	15	.2	1.73	20	6	75	<5	.29	<1	29	54	52	4.55	.04	10	.88	975	1	.01	89	1140	22	5	<20	33	<.01	<10	31	<10	1	127
106-	D 550N- 350E	10	.2	1.49	20	6	60	<5	.27	<1	27	46	51	4.46	.03	<10	.77	922	1	.01	85	1240	20	10	<20	32	<.01	<10	27	<10	1	126
107-	D 550N- 375E	5	<.2	2.04	20	6	85	<5	.32	<1	31	67	53	4.57	.04	<10	1.06	795	1	<.01	99	1230	24	10	<20	40	<.01	<10	36	<10	1	120
108-	D 550N- 400E	10	.2	1.78	25	6	90	<5	.25	<1	34	58	54	4.89	.04	10	.84	1043	1	<.01	108	1290	22	10	<20	33	<.01	<10	33	<10	1	134
109-	D 550N- 425E	5	.2	1.92	25	6	50	<5	.12	<1	41	56	85	5.26	.03	10	.96	718	2	<.01	102	1120	24	10	<20	23	<.01	<10	36	<10	<1	134
110-	D 550N- 450E	10	.2	1.42	45	4	80	<5	.30	<1	32	42	57	4.97	.04	10	.71	926	1	<.01	109	1300	26	10	<20	36	<.01	<10	26	<10	<1	144
111-	D 550N- 475E	5	.2	1.51	30	6	100	<5	.28	<1	43	29	57	5.07	.04	10	.79	2119	2	<.01	92	1070	18	10	<20	33	<.01	<10	22	<10	1	161
112-	D 550N- 500E	10	.2	1.61	30	4	105	<5	.27	<1	44	37	71	5.28	.04	10	.77	2105	2	<.01	111	1190	24	10	<20	33	<.01	<10	27	<10	2	177
113-	D 550N- 525E	15	.6	1.47	40	4	105	<5	.15	1	51	39	85	6.50	.04	10	.60	2103	2	.01	125	1710	30	10	<20	22	<.01	<10	26	<10	<1	196
114-	D 550N- 550E	105	1.0	.73	95	4	40	<5	.06	<1	22	6	96	5.66	<.01	10	.52	956	7	.01	24	1480	66	20	<20	5	<.01	<10	14	<10	<1	140
115-	D 550N- 575E	170	2.6	.52	145	4	50	<5	.13	<1	20	2	121	6.63	<.01	<10	.35	705	9	<.01	17	1570	212	25	<20	6	<.01	<10	11	<10	<1	267
116-	D 550N- 650E	395	.6	2.20	225	6	160	<5	1.17	1	34	6	132	5.51	.02	10	1.34	1915	<1	<.01	10	1850	110	20	<20	22	.02	<10	84	<10	3	230
117-	D 550N- 675E	425	.8	1.74	275	6	185	<5	.88	2	34	5	126	5.71	<.01	10	.99	1991	1	<.01	15	1700	188	30	<20	21	.01	<10	66	<10	2	440
118-	D 550N- 700E	660	.8	1.81	380	6	160	<5	1.33	2	34	6	143	5.49	<.01	10	1.05	1735	1	<.01	17	1840	174	25	<20	30	.01	<10	67	<10	3	342
119-	D 550N- 725E	330	1.0	1.83	225	6	160	<5	2.81	2	33	7	149	5.07	.02	10	1.09	1623	<1	<.01	17	1700	230	15	<20	54	.02	<10	66	<10	4	387
120-	D 550N- 750E	360	.8	1.90	270	6	155	<5	2.83	2	32	7	142	5.17	.02	10	1.13	1629	1	<.01	14	1570	206	15	<20	56	.01	<10	64	<10	3	367
121-	D 550N- 775E	90	.8	1.85	240	6	160	<5	2.26	1	32	7	126	5.02	.01	10	1.13	1718	1	<.01	15	1870	156	15	<20	37	.01	<10	58	<10	4	271
122-	D 550N- 800E	70	1.0	1.61	210	6	175	<5	2.31	3	27	4	95	4.84	.01	10	.98	1667	<1	<.01	9	1410	198	20	<20	29	.01	<10	59	<10	2	352
123-	D 650N- 600E	30	.4	.74	105	4	210	<5	.28	2	16	<1	39	4.56	.01	20	.26	1857	5	<.01	17	1400	84	15	<20	37	<.01	<10	13	<10	6	281
124-	D 650N- 625E	160	1.6	.77	165	6	130	<5	.36	1	30	1	72	6.07	<.01	10	.48	2467	3	<.01	12	1380	88	25	<20	16	.01	<10	28	<10	<1	204
125-	D 650N- 650E	280	.8	1.65	160	6	135	<5	.78	1	32	5	101	5.45	.02	10	1.01	1478	1	<.01	11	1830	72	20	<20	21	.02	<10	61	<10	3	167
126-	D 650N- 675E	275	.6	1.89	240	6	165	<5	1.07	1	34	5	123	5.32	.02	10	1.06	1865	<1	<.01	15	1560	140	20	<20	22	.01	<10	66	10	3	295
127-	D 650N- 700E	210	1.4	1.72	340	4	175	<5	1.12	4	38	6	172	5.80	<.01	10	.91	2016	1	<.01	25	1680	310	25	<20	34	.01	<10	59	<10	4	542
128-	D 650N- 725E	220	1.8	2.08	380	4	250	<5	.66	9	44	5	104	7.70	<.01	10	1.17	3708	1	<.01	13	1650	754	25	<20	26	.01	<10	103	10	7	884
129-	D 650N- 750E	125	1.0	1.77	325	4	170	<5	1.20	1	36	7	131	5.42	<.01	10	1.10	1932	1	<.01	16	1850	226	15	<20	30	.02	<10	59	<10	5	345
130-	D 650N- 775E	55	.6	1.99	150	6	150	<5	.65	1	31	8	115	4.97	.03	10	1.23	1581	<1	<.01	12	1600	102	10	<20	20	.02	<10	71	<10	4	210
131-	D 650N- 800E	85	1.0	1.92	270	6	165	<5	.57	2	35	9	124	5.56	<.01	10	1.28	1980	1	.01	16	1700	282	20	<20	21	.03	<10	72	<10	6	343
132-	D 650N- 725E	75	.8	1.84	300	4	175	<5	1.22	2	31	9	118	5.16	<.01	10	1.07	1785	<1	<.01	18	1740	174	15	<20	28	.01	<10	56	<10	4	351
133-	D 650N- 850E	25	.4	1.98	155	6	180	<5	.75	1	30	10	109	5.08	.03	10	1.25	1604	1	<.01	16	1820	122	15	<20	22	.01	<10	60	<10	4	252
134-	D 650N- 875E	40	.4	2.11	155	6	210	<5	.61	1	34	10	116	5.34	.04	10	1.32	1885	<1	<.01	17	1990	118	10	<20	20	.01	<10	64	<10	4	265
135-	D 650N- 900E	50	1.2	1.95	365	6	320	<5	1.08	2	32	7	115	5.61	<.01	10	1.19	2085	1	<.01	16	1720	264	20	<20	24	.01	<10	67	<10	3	469
136-	D 750N- 600E	275	.8	1.72	230	6	135	<5	.65	1	28	6	109	5.11	<.01	10	1.06	1411	<1	<.01	14	1950	138	20	<20	17	.03	<10	67	<10	4	247

#T#		DESCRIPTION	AU(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
137-	D	750N- 625E	490	1.0	1.81	330	4	215	<5	.62	2	38	7	154	5.53	<.01	10	1.01	1900	<1	<.01	19	1960	206	25	<20	21	.02	<10	65	<10	5	376
138-	D	750N- 650E	255	.8	1.89	200	6	145	<5	.55	1	29	8	116	5.29	.01	10	1.10	1496	1	<.01	14	1700	156	15	<20	19	.02	<10	72	<10	5	288
139-	D	750N- 675E	315	.8	1.89	250	6	135	<5	.59	2	31	6	123	5.35	<.01	10	1.12	1569	1	<.01	14	1910	186	20	<20	20	.02	<10	70	<10	4	332
140-	D	750N- 700E	70	.6	2.89	275	4	135	<5	.29	1	38	9	124	5.98	<.01	10	1.10	2029	1	<.01	15	1500	202	20	<20	13	.02	<10	81	<10	5	339
141-	D	750N- 725E	50	.8	1.93	180	6	175	<5	.58	2	30	6	103	5.32	.02	10	1.18	1824	1	<.01	11	1770	170	15	<20	18	.02	<10	74	<10	4	295
142-	D	750N- 750E	55	.6	2.06	215	6	150	<5	.42	1	30	9	102	5.28	<.01	10	1.20	1745	<1	.01	14	1700	136	15	<20	15	.02	<10	73	<10	4	261
143-	D	750N- 775E	30	.2	4.06	135	6	60	<5	.08	<1	15	8	67	4.92	.01	20	.56	677	3	.01	7	1200	88	10	<20	5	.02	<10	45	<10	6	173
144-	D	750N- 800E	45	.4	3.40	110	6	75	<5	.44	<1	12	10	57	4.47	.02	10	.56	552	1	.01	8	1360	82	10	<20	17	.02	<10	51	<10	3	137
145-	D	750N- 825E	75	.8	2.63	265	6	260	<5	.39	1	40	11	121	5.76	<.01	10	1.24	2726	<1	<.01	17	1390	176	20	<20	16	.01	<10	79	<10	6	327
146-	D	750N- 850E	65	1.0	1.84	270	6	235	<5	.65	2	33	8	117	5.51	<.01	10	1.18	2088	1	<.01	17	2090	236	20	<20	23	.01	<10	63	<10	5	391
147-	D	750N- 875E	85	.6	1.76	135	6	120	<5	.57	1	26	8	93	5.06	.01	10	1.25	1309	<1	.01	13	2000	124	20	<20	19	.03	<10	63	<10	5	237
148-	D	750N- 900E	80	.6	1.69	145	6	150	<5	.66	1	25	7	93	4.78	.01	10	1.17	1377	<1	<.01	12	2390	132	15	<20	20	.01	<10	60	<10	5	235
149-	D	800N- 600E	300	1.0	1.95	285	10	210	<5	.67	3	37	7	140	5.63	<.01	10	1.09	2051	<1	<.01	18	1760	232	30	<20	20	.02	<10	72	<10	4	394
150-	D	800N- 625E	310	.8	1.86	270	6	160	<5	.62	1	31	6	120	5.29	<.01	10	1.05	1589	1	<.01	14	1870	164	25	<20	19	.02	<10	69	<10	4	304
151-	D	800N- 650E	65	.4	3.53	135	4	70	<5	.26	<1	19	13	82	4.97	.02	10	.64	978	2	.01	9	1240	108	10	<20	12	.02	<10	69	<10	4	199
152-	D	800N- 675E	55	.2	3.67	95	4	60	<5	.08	<1	15	10	57	4.00	<.01	10	.42	911	2	<.01	7	1030	68	5	<20	6	.01	<10	64	<10	1	135
153-	D	800N- 700E	85	.8	3.10	200	8	100	<5	.19	<1	32	11	113	5.66	.03	20	.91	1645	2	.02	16	1670	152	20	<20	9	.04	<10	74	<10	10	291
154-	D	800N- 725E	55	.6	2.88	190	6	140	<5	.24	1	32	11	112	5.78	.04	20	1.09	1717	1	.01	16	1570	156	20	<20	10	.05	<10	82	<10	10	289
155-	D	800N- 750E	50	.6	2.76	215	8	140	<5	.22	<1	31	9	103	5.68	.04	20	1.08	1991	1	.02	15	1390	152	15	<20	10	.04	<10	73	<10	9	288
156-	D	800N- 775E	35	.2	2.80	155	6	75	<5	.12	<1	18	10	70	5.27	.03	20	.82	975	1	.02	7	1160	128	15	<20	7	.05	<10	74	<10	7	171
157-	D	800N- 800E	30	.2	3.65	130	8	45	<5	.07	<1	13	11	65	5.92	.01	20	.59	933	3	.02	7	1640	68	10	<20	5	.03	<10	62	<10	5	136
158-	D	800N- 825E	25	.4	1.93	320	4	75	<5	.06	<1	33	8	54	5.50	<.01	10	.66	3402	1	<.01	6	1870	236	15	<20	6	.01	<10	80	<10	<1	190
159-	D	800N- 850E	65	.8	2.60	290	6	240	<5	.36	1	39	10	117	5.94	.01	20	1.27	3190	1	<.01	16	1400	208	20	<20	15	.03	<10	81	<10	6	356
160-	D	800N- 875E	140	.8	3.06	155	4	150	<5	.31	1	32	14	104	5.52	.01	10	.76	3455	1	<.01	11	2120	132	15	<20	10	.02	<10	89	<10	2	243
161-	D	800N- 900E	185	2.6	3.36	345	4	70	<5	.14	<1	42	13	114	5.39	<.01	10	.82	3431	2	<.01	10	1680	542	35	<20	8	.01	<10	75	<10	<1	535
162-	D	800N- 925E	190	1.0	3.01	215	6	155	<5	.15	1	28	11	91	5.98	.02	20	.96	2769	2	<.01	14	1400	208	20	<20	9	.01	<10	62	10	6	351
163-	D	800N- 950E	65	.6	2.38	155	6	155	<5	.38	<1	15	12	67	4.54	.03	10	.78	1009	<1	<.01	10	2890	144	15	<20	13	.01	<10	74	<10	4	252
164-	D	800N- 975E	50	1.0	2.31	250	6	250	<5	.47	1	32	11	126	5.68	.04	20	1.31	2240	1	<.01	17	1660	222	25	<20	19	.01	<10	74	<10	5	357
165-	D	800N- 1000E	45	.8	2.04	190	6	150	<5	.36	1	30	10	93	5.07	.03	10	1.00	2259	<1	<.01	11	2320	180	20	<20	14	.01	<10	65	<10	6	267
166-	D	850N- 500E	50	.6	1.05	100	6	235	<5	.24	2	19	2	47	5.27	.05	20	.33	2296	5	<.01	22	1590	70	20	<20	39	<.01	<10	18	<10	6	252
167-	D	850N- 525E	95	.8	.80	100	4	125	<5	.30	1	20	2	48	5.00	.01	20	.41	2022	3	<.01	13	1310	46	20	<20	23	.01	<10	24	<10	2	149
168-	D	850N- 550E	170	1.0	1.30	145	4	120	<5	.54	<1	26	3	75	5.52	.01	10	.71	1530	2	<.01	14	1510	76	20	<20	21	.02	<10	44	<10	3	166
169-	D	850N- 575E	395	.4	2.19	195	4	170	<5	.83	1	31	6	102	5.34	.02	10	1.30	1524	<1	<.01	11	1800	100	20	<20	16	.04	<10	78	<10	5	202
170-	D	850N- 600E	360	.6	2.29	195	4	155	<5	.83	1	32	6	105	5.45	.04	10	1.29	1635	1	<.01	12	1720	100	25	<20	21	.04	<10	80	<10	5	227

MT#		DESCRIPTION	AU(ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
171-	D	850N- 625E	335	.8	2.00	235	4	160	<5	.62	1	30	7	119	5.38	.01	10	1.13	1623	1	<.01	14	1630	136	20	<20	18	.03	<10	74	<10	4	267
172-	D	850N- 650E	100	.6	2.85	160	4	70	<5	.14	<1	23	15	86	5.13	.03	10	.76	1182	3	<.01	17	1550	124	10	<20	7	.03	<10	70	10	3	218
173-	D	850N- 675E	80	.8	2.77	110	4	70	<5	.16	1	25	15	91	5.00	.01	10	1.18	1981	10	<.01	43	1340	88	15	<20	7	.03	<10	91	10	7	272
174-	D	850N- 700E	85	.4	3.14	145	4	90	<5	.13	<1	21	12	77	4.26	.04	10	.72	1771	2	<.01	11	1450	102	10	<20	8	.01	<10	83	<10	2	218
175-	D	850N- 725E	135	.4	3.17	120	4	60	<5	.19	<1	24	15	90	5.11	.03	10	.87	1160	2	.01	11	1530	98	15	<20	7	.04	<10	99	<10	4	191
176-	D	850N- 750E	50	.2	3.07	145	2	80	<5	.05	<1	14	11	65	4.85	.02	10	.62	921	1	.01	7	1550	82	10	<20	4	.01	<10	86	<10	<1	147
177-	D	850N- 775E	30	.6	2.80	270	4	185	<5	.16	<1	32	12	114	5.79	.05	10	1.16	2225	1	<.01	15	1180	186	15	<20	9	.01	<10	85	<10	4	330
178-	D	850N- 800E	50	.4	3.79	165	4	75	<5	.11	<1	30	11	83	5.55	.01	20	.80	2073	2	.02	10	950	130	10	<20	6	.03	<10	72	<10	6	222
179-	D	850N- 825E	370	.8	3.23	160	6	105	<5	.20	1	32	10	105	5.59	.03	20	1.08	2276	1	.01	13	1630	130	15	<20	7	.04	<10	76	<10	8	290
180-	D	850N- 850E	1535	.6	3.78	195	4	70	<5	.20	<1	22	13	117	5.40	<.01	10	.98	1201	1	<.01	13	1710	82	15	<20	7	.02	<10	78	<10	2	255
181-	D	850N- 875E	1275	1.4	3.94	195	4	85	<5	.23	<1	39	10	146	6.12	.03	20	1.05	3370	1	.01	13	2810	120	15	<20	6	.03	<10	115	<10	9	286
182-	D	850N- 900E	555	2.2	3.33	285	4	120	<5	.10	1	44	12	193	6.34	<.01	10	1.17	5065	2	<.01	18	2120	278	20	<20	8	.03	<10	88	<10	2	601
183-	D	850N- 925E	85	.6	1.93	160	4	150	<5	.44	1	27	9	101	5.12	.01	10	1.19	1792	<1	<.01	14	1980	178	20	<20	15	.02	<10	66	<10	5	297
184-	D	850N- 950E	70	.8	3.52	100	2	100	<5	.08	<1	24	18	71	4.01	.03	10	.56	1936	<1	<.01	6	1740	118	10	<20	6	.01	<10	75	<10	7	182
185-	D	850N- 975E	115	.6	3.04	140	2	95	<5	.14	<1	25	15	88	4.92	.04	10	1.12	1623	1	.01	13	1640	166	20	<20	8	.02	<10	87	<10	3	286
186-	D	850N- 1000E	85	1.0	3.17	115	4	110	<5	.19	<1	21	17	110	4.07	.05	10	.88	1368	1	<.01	12	1720	152	15	<20	9	.01	<10	75	<10	9	264
187-	D	900N- 600E	350	.6	2.00	160	4	110	<5	.75	1	26	7	87	5.05	<.01	10	1.22	1344	<1	<.01	12	1730	104	15	<20	17	.06	<10	73	<10	5	165
188-	D	900N- 625E	215	.8	2.08	230	4	140	<5	.54	1	30	8	112	5.31	.01	10	1.01	1498	1	<.01	15	1670	148	25	<20	15	.04	<10	71	<10	5	267
189-	D	900N- 650E	140	.4	3.32	90	6	40	<5	.17	<1	13	13	56	5.10	.03	20	.65	531	3	.02	9	1630	88	10	<20	7	.05	<10	60	<10	6	140
190-	D	900N- 675E	305	.2	3.60	80	4	45	<5	.23	<1	15	13	70	4.35	.01	10	.68	683	5	<.01	13	1480	68	10	<20	7	.03	<10	78	<10	2	163
191-	D	900N- 700E	135	.6	3.04	125	4	50	<5	.14	<1	19	13	77	4.78	.03	10	.79	1040	1	.01	11	1560	112	10	<20	7	.03	<10	90	<10	4	185
192-	D	900N- 725E	95	.4	3.48	130	6	60	<5	.27	<1	31	17	89	5.34	.03	10	.93	2046	2	.01	13	2730	116	15	<20	9	.05	<10	99	<10	6	187
193-	D	900N- 750E	50	.4	2.94	215	4	85	<5	.04	<1	26	12	76	5.62	.03	10	.92	2036	2	<.01	11	1250	122	15	<20	5	.01	<10	89	<10	<1	227
194-	D	900N- 775E	60	.6	2.79	165	4	100	<5	.10	<1	31	12	93	5.22	.05	10	1.02	2047	1	.01	11	1160	144	15	<20	7	.01	<10	82	<10	6	221
195-	D	900N- 800E	150	.6	2.80	175	4	145	<5	.29	2	19	12	100	4.82	.04	10	1.04	875	<1	<.01	13	1310	138	10	<20	12	.01	<10	83	10	4	238
196-	D	900N- 825E	85	.6	2.50	170	6	140	<5	.33	1	32	11	106	5.31	.05	10	1.20	2000	1	<.01	16	1520	132	15	<20	12	.02	<10	74	<10	6	264
197-	D	900N- 850E	160	.6	2.72	200	4	160	<5	.25	1	37	11	121	5.84	.04	10	1.29	2427	1	<.01	17	1430	162	15	<20	11	.02	<10	83	<10	5	330
198-	D	900N- 875E	155	1.0	2.78	245	4	90	<5	.19	<1	23	11	92	5.67	<.01	10	1.07	1466	1	<.01	12	2030	248	25	<20	9	.03	<10	87	<10	3	346
199-	D	900N- 900E	115	1.2	3.21	195	4	100	<5	.07	<1	38	13	98	5.04	.03	10	.80	3224	2	.01	8	1220	210	15	<20	6	.01	<10	74	<10	<1	273

ETÉ		DESCRIPTION		AU(ppb)		AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
200-	D	900N-	925E	705	•	3.0	1.57	865	4	650	<5	.28	21	54	3	192	9.61	<.01	30	.92	9632	3	<.01	39	1420	1374	70	<20	25	.01	<10	84	40	10	2086
201-	D	900N-	950E	75		1.0	2.39	190	4	155	<5	.19	<1	27	11	76	5.10	.01	10	.84	7424	1	.01	12	2200	198	15	<20	12	.01	<10	74	<10	<1	267
202-	D	900N-	975E	100		.8	2.75	190	4	90	<5	.15	<1	30	16	109	5.54	.03	10	1.19	2184	1	<.01	17	1930	216	20	<20	9	.02	<10	84	<10	1	320
203-	D	900N-	1000E	75		.8	2.94	125	4	110	<5	.09	<1	24	17	93	4.88	.05	10	.92	2946	<1	<.01	11	1780	140	15	<20	6	.01	<10	76	<10	3	222

NOTE: < = LESS THAN
• = TO -65

ECO-TECH LABORATORIES LTD.
Frank J. Pezzotti, A.Sc.T.
B.C. Certified Assayer

Corner Post 5N

Best Bet 17
8364

Best Bet 18
8365

N

Stn 200W ---
Stn 250W ---
Stn 300W ---
Stn 350W ---
Stn 400W ---
Stn 450W ---
Stn 500W ---
Stn 550W ---
Stn 600W ---
Stn 650W ---
Stn 700W ---
Stn 750W ---
Stn 800W ---
Stn 850W ---
Stn 900W ---
Stn 950W ---
Stn 1000W ---

Line 250S
Line 300S
Line 350S
Line 400S
Line 450S
Line 500S
Line 550S
Line 650S
Line 750S
Line 800S
Line 850S
Line 900S

DC GLACIER

SCALE 1:5000

100 0 100 200 300

METERS

Asterisks signify
Au < 5 ppb

Au Contours at
150, 250, 400, 600 ppb

GEOLOGICAL BRANCH
ASSESSMENT REPORT

22,261

LEGEND
Glacier
Creek
Claim Bdy

TEUTON RESOURCES CORP.

Delta Property
Stewart, B.C, – Skeena M.D.

M-J AREA
SOIL GEOCHEMISTRY
AU VALUES (ppb)

g.c.

RPM Mapping and Computer Services Ltd.

Date: Dec. 1991

NTS No.: 104B/8E

Figure: 4

Corner Post 5N

Best Bet 17
8364

Best Bet 18
8365

Stn 200W
Stn 250W
Stn 300W
Stn 350W
Stn 400W
Stn 450W
Stn 500W
Stn 550W
Stn 600W
Stn 650W
Stn 700W
Stn 750W
Stn 800W
Stn 850W
Stn 900W
Stn 950W
Stn 1000W

Line 250S
Line 300S
Line 350S
Line 400S
Line 450S
Line 500S
Line 550S
Line 650S
Line 750S
Line 800S
Line 850S
Line 900S

DC GLACIER

SCALE 1:5000

100 0 100 200 300

METERS

Asterisks signify
Ag < 0.2 ppm

Ag Contours at
0.8, 1.2, 2.0 & 3.5 ppm

LEGEND

Glacier

Creek

Claim Bdy

GEOLOGICAL BRANCH
ASSESSMENT REPORT

22,261

TEUTON RESOURCES CORP.

Delta Property
Stewart, B.C., - Skeena M.D.

M-J AREA
SOIL GEOCHEMISTRY
AG VALUES (ppm)

J.C.

RPM Mapping and Computer Services Ltd.	Date: Dec. 1991
	NTS No.: 104B/8E
	Figure: 5

Corner Post 5N

Best Bet 17
8364

Best Bet 18
8365

Stn 200W
Stn 250W
Stn 300W
Stn 350W
Stn 400W
Stn 450W
Stn 500W
Stn 550W
Stn 600W
Stn 650W
Stn 700W
Stn 750W
Stn 800W
Stn 850W
Stn 900W
Stn 950W
Stn 1000W

Line 250S
Line 300S
Line 350S
Line 400S
Line 450S
Line 500S
Line 550S
Line 650S
Line 750S
Line 800S
Line 850S
Line 900S

DC GLACIER

SCALE 1:5000

100 0 100 200 300

METERS

As Contours at
150, 250, 400, 600 ppm

GEOLOGICAL BRANCH
ASSESSMENT REPORT

22,261

LEGEND

Glacier

Creek

Claim Bdy

TEUTON RESOURCES CORP.

Delta Property
Stewart, B.C. – Skeena M.D.

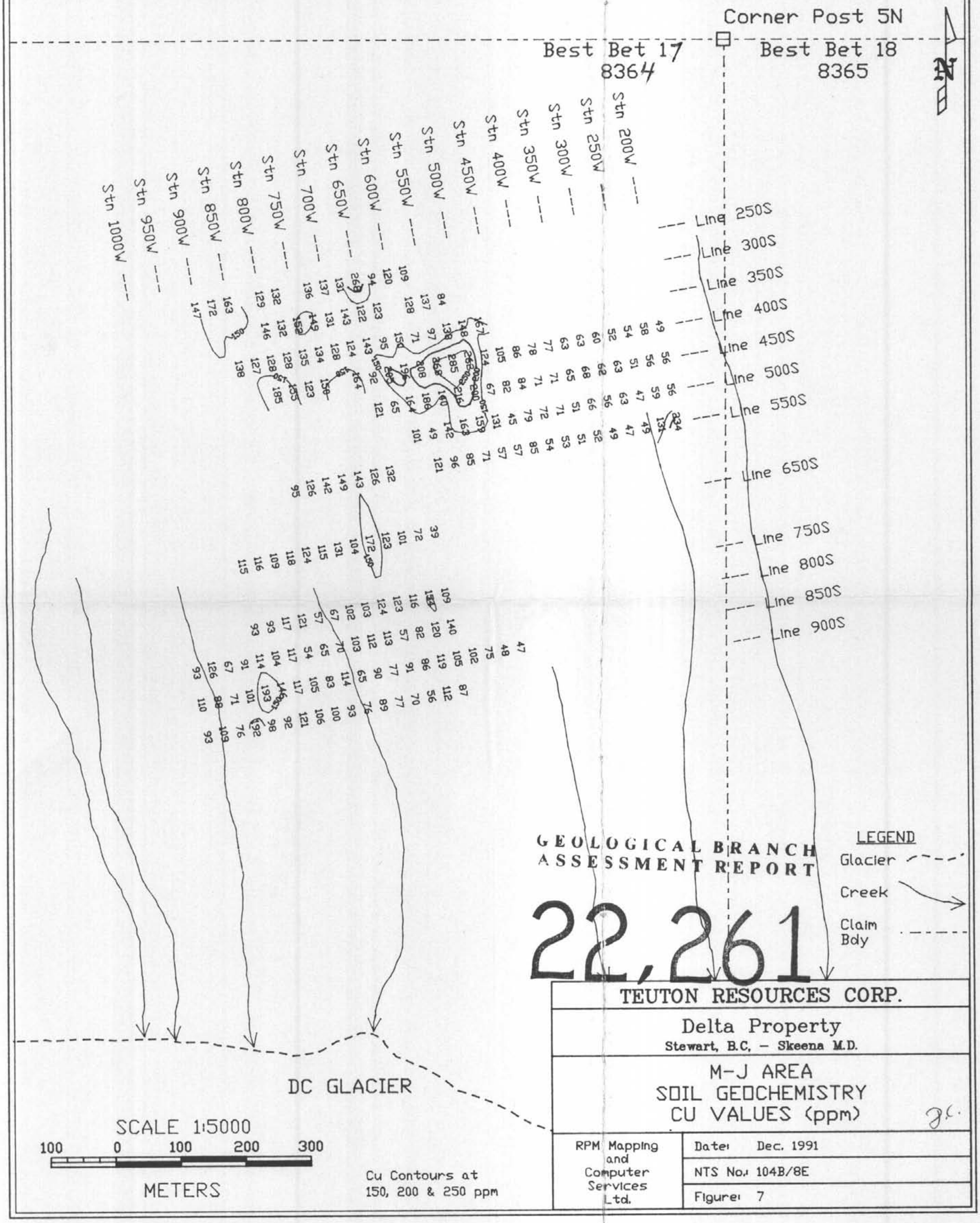
M-J AREA
SOIL GEOCHEMISTRY
AS VALUES (ppm)

RPM Mapping and Computer Services Ltd.

Date: Dec. 1991

NTS No.: 104B/8E

Figure: 6


Corner Post 5N
Best Bet 17
8364
Best Bet 18
8365
N
Stn 200W
Stn 250W
Stn 300W
Stn 350W
Stn 400W
Stn 450W
Stn 500W
Stn 550W
Stn 600W
Stn 650W
Stn 700W
Stn 750W
Stn 800W
Stn 850W
Stn 900W
Stn 950W
Stn 1000W
Line 250S
Line 300S
Line 350S
Line 400S
Line 450S
Line 500S
Line 550S
Line 650S
Line 750S
Line 800S
Line 850S
Line 900S
DC GLACIER
SCALE 1:5000
100 0 100 200 300
METERS
Cu Contours at
150, 200 & 250 ppm
GEOLOGICAL BRANCH
ASSESSMENT REPORT
22,261
LEGEND
Glacier
Creek
Claim Bdy
TEUTON RESOURCES CORP.
Delta Property
Stewart, B.C. – Skeena M.D.
M-J AREA
SOIL GEOCHEMISTRY
CU VALUES (ppm)
RPM Mapping and Computer Services Ltd.
Date: Dec. 1991
NTS No.: 104B/8E
Figure: 7

Corner Post 5N

Best Bet 17
8364

Best Bet 18
8365

N

Stn 200W ---
Stn 250W ---
Stn 300W ---
Stn 350W ---
Stn 400W ---
Stn 450W ---
Stn 500W ---
Stn 550W ---
Stn 600W ---
Stn 650W ---
Stn 700W ---
Stn 750W ---
Stn 800W ---
Stn 850W ---
Stn 900W ---
Stn 950W ---
Stn 1000W ---

Line 250S
Line 300S
Line 350S
Line 400S
Line 450S
Line 500S
Line 550S
Line 650S
Line 750S
Line 800S
Line 850S
Line 900S

DC GLACIER

SCALE 1:5000

100 0 100 200 300

METERS

Pb Contours at
100, 150, 250 & 400 ppm

GEOLOGICAL BRANCH
ASSESSMENT REPORT

22,261

LEGEND
Glacier
Creek
Claim Bdy

TEUTON RESOURCES CORP.

Delta Property
Stewart, B.C, – Skeena M.D.

M-J AREA
SOIL GEOCHEMISTRY
PB VALUES (ppm)

RPM Mapping and Computer Services Ltd.	Date: Dec. 1991
	NTS No.: 104B/8E
	Figure: 8

Corner Post 5N

Best Bet 17
8364

Best Bet 18
8365

N

Stn 200W ---
Stn 250W ---
Stn 300W ---
Stn 350W ---
Stn 400W ---
Stn 450W ---
Stn 500W ---
Stn 550W ---
Stn 600W ---
Stn 650W ---
Stn 700W ---
Stn 750W ---
Stn 800W ---
Stn 850W ---
Stn 900W ---
Stn 950W ---
Stn 1000W ---

Line 250S
Line 300S
Line 350S
Line 400S
Line 450S
Line 500S
Line 550S
Line 650S
Line 750S
Line 800S
Line 850S
Line 900S

DC GLACIER

SCALE 1:5000

100 0 100 200 300

METERS

Zn Contours at
200, 300, 450 & 600 ppm

GEOLOGICAL BRANCH
ASSESSMENT REPORT

22,261

LEGEND
Glacier
Creek
Claim Bdy

TEUTON RESOURCES CORP.

Delta Property
Stewart, B.C. – Skeena M.D.

M-J AREA
SOIL GEOCHEMISTRY
ZN VALUES (ppm)

B.C.

RPM Mapping and Computer Services Ltd.

Date: Dec. 1991
NTS No.: 104B/8E
Figure: 9