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SUB-RECORDER
RECEIVED
AUG 25 1992
M.R. # \$
VANCOUVER, B.C.

GEOLOGICAL BRANCH
ASSESSMENT REPORT

22,468

POCAHONTAS GROUP

Texada Island, British Columbia

Owner: D. Cukor

1. INTRODUCTION

The geophysical survey program outlined in this Report was conducted by D. Cukor, Geologist, the registered owner of the claim. The survey consisted of ground VLF-EM and resistivity, utilizing a Scintrex IGS-2 system.

This work is to be applied as assessment work on the property.

2. PROPERTY

The claims are located on the north portion of Texada Island, approximately 11 km southeast of Vananda, B.C., covering the top and southwestern slope of Mt. Pocahontas. See Figures 1 and 2. The property is shown on NTS sheet 92-F/9W, in the Nanaimo Mining Division. It is centered at about north latitude 49 42' and west longitude 124 26'.

Access to the property from Vananda is provided via the all weather road, which transects the property's southwest corner and by the dirt road which leads to Pocahontas Bay and then loops back toward the claims.

The nearest accomodation is in Vananda, and the nearest supply centre is Powell River. Texada Island is serviced by a regularly scheduled B.C. Ferry route from Powell River; access to Powell River is by a combination of road and B.C. Ferry up the Sunshine Coast or up Vancouver Island to Comox, then over to the mainland. Texada Island is also serviced by regularly scheduled air service.

The property consists of the following claims:

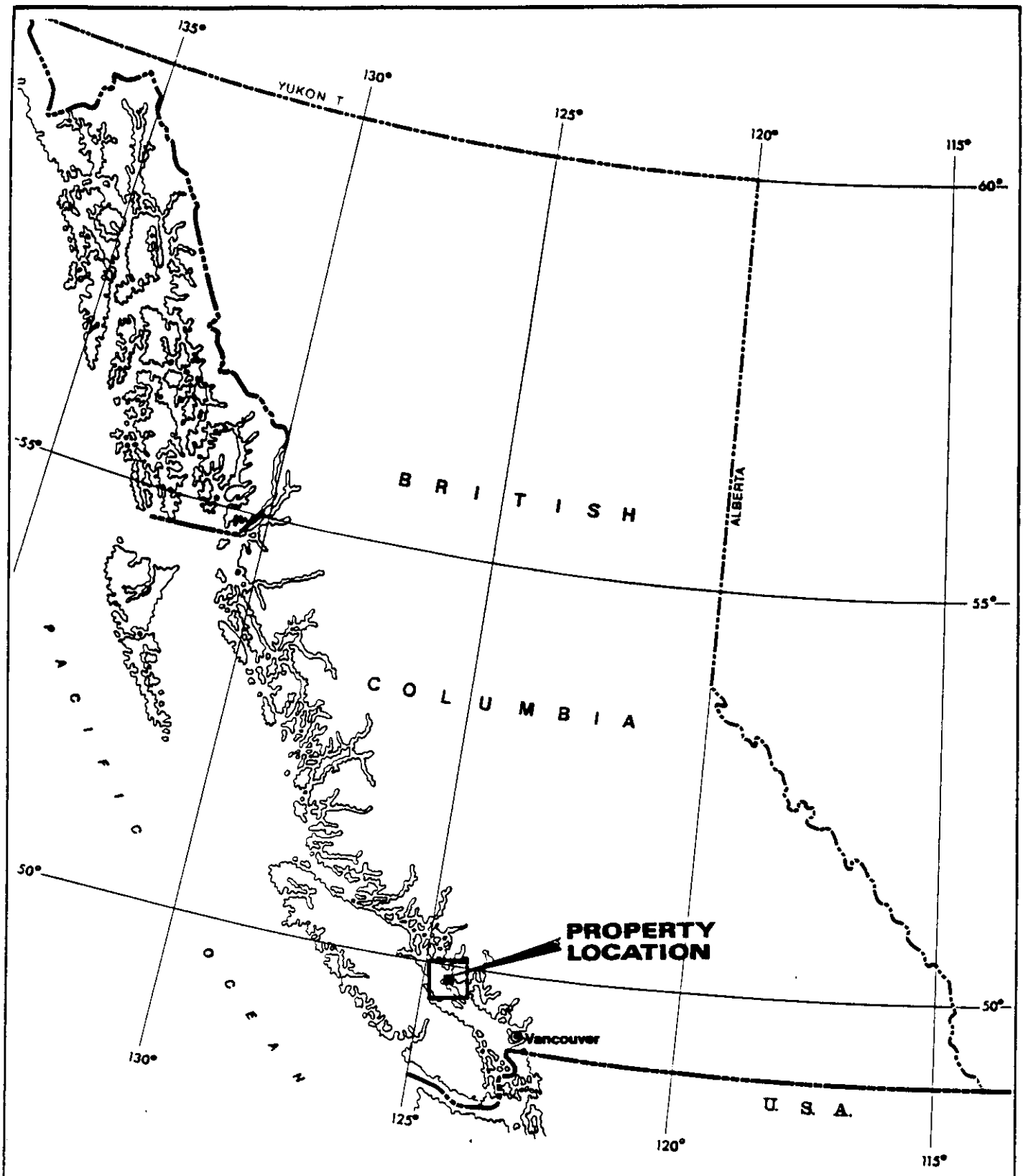
<u>Name</u>	<u>Record no.</u>	<u>no. of units</u>	<u>Anniversary date</u>
Grad	229847	16	May 28
Pocahontas 1	230266	1	May 26
Pocahontas 2	230267	1	May 26
Pocahontas 3	230268	1	May 26
Pocahontas 4	230269	1	May 26
Pocahontas 5	230270	1	May 26
Pocahontas 6	230271	1	May 26
Pocahontas 7	230272	1	May 26
Pocahontas 8	230273	1	May 26

See fig. 2 for claim locations.

The topography is fairly moderate over much of the property area, except for the southwest facing slope, which is fairly steep. Elevations on the property range from 300 to 1100 m above sea level. Occasionally, rock outcrops form bluffs. The claims are partially covered with timber, with several large blocks logged recently. Some areas have been subjected to juvenile thinning.

The property region has a modified coastal climate; Texada Island is located in Vancouver Island's rain shadow. Summers are generally warm to hot and dry and winters mild with a moderate amount of atmospheric precipitation. The property is generally snow-free all year round.

Water and timber for exploration purposes are available on the property.



POCAHONTAS CLAIM GROUP

LOCATION MAP

NANAIMO M.D., B.C.

NTS 92 F/9W

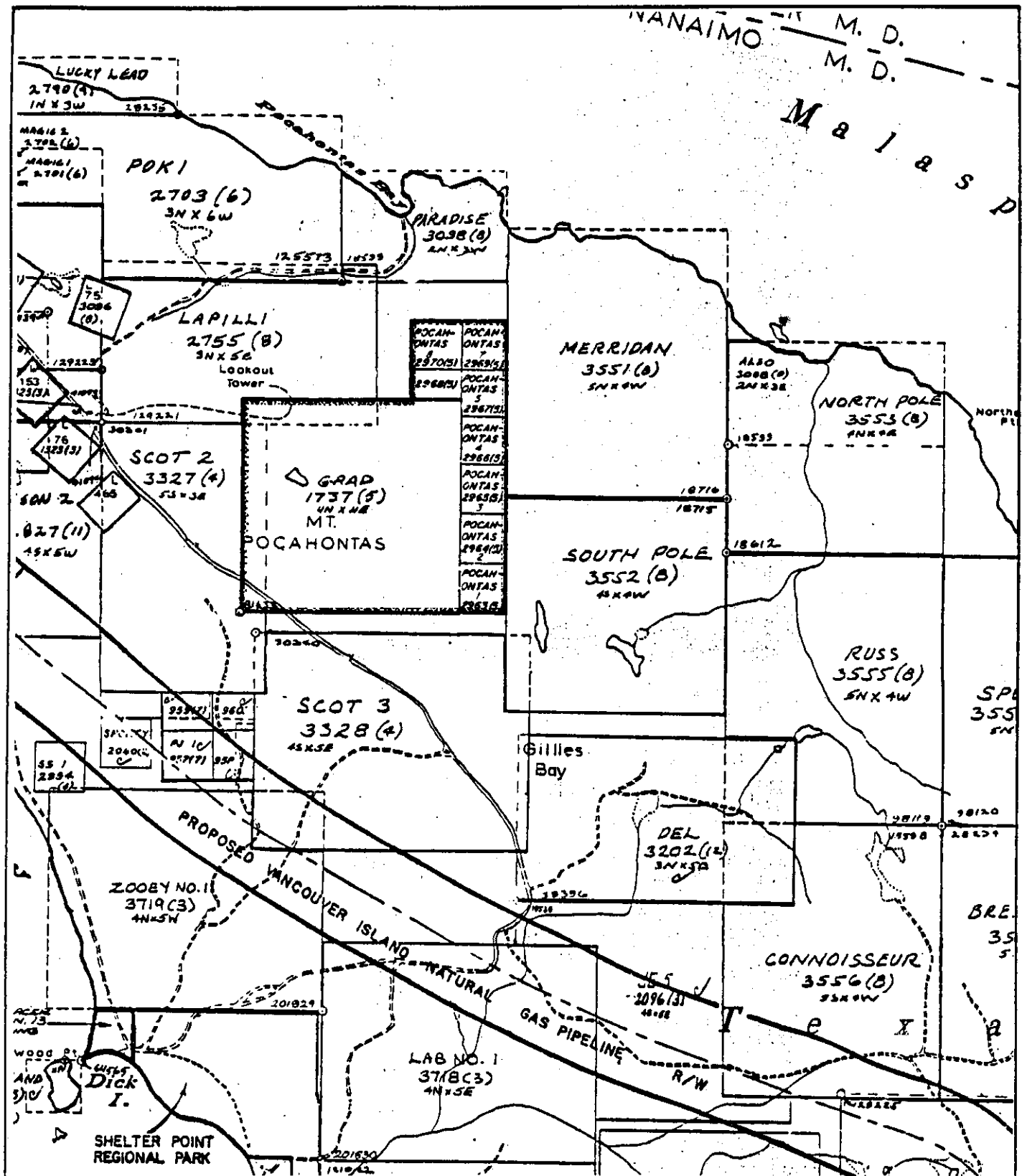
DAMIR CUKOR, geol.

VANCOUVER B.C.

DATE: Aug. 1992

SCALE: 0  100 Miles

FIG. 1



POCAHONTAS CLAIM GROUP

CLAIM MAP

NANAIMO M.D., B.C.

NTS 92 F/9W

DAMIR CUKOR, geol.

VANCOUVER B.C.

DATE: Aug. 1992

SCALE: 0 1 km

FIG. 2

3. GEOPHYSICAL SURVEYS

The geophysical surveys comprised of VLF-EM and resistivity methods. Both methods were run simultaneously, utilizing the Scintrex IGS-2 system.

3.1 Field Method

A grid was prepared for these surveys; 6.2 km of lines was surveyed and flagged.

For the VLF surveys, the IGS unit was programmed to receive signals from two stations: NLK Seattle, Washington, 24.8 kHz and NPM Lualualei, Hawaii, 23.4 kHz, measuring the horizontal field strength and the inphase and out-of-phase or quadrature components of the vertical field. The instrument uses a three coil system, one horizontal and two vertical coils, all at 90 angles to each other. The system is set to automatically adjust for topographical shadowing of field strength.

Resistivity measurements were made using capacitive electrodes, and utilizing signals from NLK Seattle. For this method, the horizontal component of the electric field was measured.

3.2 VLF-EM Surveys

Data for both the Seattle and Hawaii VLF-EM surveys was plotted as stacked profiles on 1:2500 scale plans. Conductors were interpreted and are marked on both plans.

On the Seattle survey plan, fig.3, three structures have been interpreted. The strongest of the three is located at Line 1N, 200W. This conductor shows a strong response over a length of 250 meters, and closely coincides with a strong resistivity low. The north end of the structure is open. The second strongest structure is located approximately 100 meters to the east of the first; the two structures are sub-parallel to each other. This conductor, however is weak and is coincident with a resistivity high. The last structure occurs in the northwest corner of the grid. Although this conductor displays weak response, it coincides quite closely with a resistivity low. This structure is open to both the north and south.

The Hawaii survey identified only one structure at line 0, 300E, see fig 4. The conductor apparently ends to the north of line 0, and it weakens to the south. The coincidence of this structure with a resistivity high further lessens the potential of this target.

3.3 Resistivity Survey


The resistivity survey data is presented as fig.5, at the same scale as the stacked profile plans. The most striking feature on this map is a very strong resistive structure running north-south across the whole of the surveyed grid. Flanking this high are lows to the east and the west. These may be of significance; the eastern structure coincides with a strong Seattle conductor.

4. CONCLUSIONS AND RECOMMENDATIONS

The surveys carried out in this program were the first step in grass-roots exploration in this area of the claims. For this reason, the grid was fairly wide-spaced and irregular. The VLF conductors and resistivity lows identified should be traced along their lengths employing VLF-EM and resistivity, as well as prospecting, geological mapping, and ground magnetics._

Respectfully submitted,

D. Cukor
Geologist



NVC ENGINEERING LTD.

August 1992

COSTS OF THE WORK PROGRAM

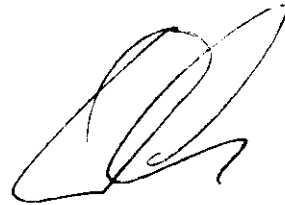
Field Work

3,000.00

Report

1,000.00

TOTAL Costs \$ 4,000.00




D. Cukor

CERTIFICATE

I, DAMIR CUKOR, of 6108 McKee Street, Burnaby, British Columbia, DO HEREBY CERTIFY that:

1. I graduated from the University of British Columbia in 1984 as a Bachelor of Science in Geology;
2. Since 1983 I have been employed as a geologist with NVC Engineering Ltd.;
3. I have worked in the field of exploration geology and geophysics for 16 seasons and have held positions of responsibility since 1982;
4. I have performed and/or supervised the work as documented in this Report.

August, 1992



D. Cukor, B. Sc.
NVC ENGINEERING LTD.

APPENDIX

INSTRUMENT SPECIFICATIONS

1. THE IGS-2 SYSTEM

1.1 General Information

The IGS-2 Integrated Geophysical System is a portable microprocessor-based instrument which allows more than one type of survey measurement to be performed by a single operator during a survey.

The IGS-2 is a modular system which can easily be configured to suit different and changing survey requirements. Reconfiguring the system is easy and offers both operational flexibility and minimal redundancy with a minimum number of spare consoles and/or modules.

When configured with any of the available sensor options, the IGS-2 System Control Console becomes a method-specific instrument according to the sensor option(s) utilized. In addition, the IGS-2 Console is an electronic notebook into which geophysical, geological or other data may be manually entered and digitally stored.

Data is stored in the IGS-2 in an expandable, solid state memory and can be output in the field by connecting the instrument to a printer, tape recorder, modem or microcomputer.

The 32 character digital display uses full words in most cases, ensuring clear communication. Both present and previous data are displayed simultaneously, allowing comparisons to be made at a glance during a survey.

The IGS-2 records header information, data values, station number, line number, grid number and the time of each observation in its internal memory. Data are first sorted by grid number, then in order of increasing line number and, within each line, by increasing station number. In this way, the data are organized logically regardless of the sequence in which they were taken. Ancillary data can also be manually entered and recorded at a given station, along with the survey parameters.

1.2 Standard Console Specifications

Digital Display	32 character, 2 line LCD display
Keyboard Input	14 keys for entering all commands, coordinates, header and ancillary information
Languages	English plus French is standard
Standard Memory	16K RAM. More than sufficient for a day's data in most applications
Clock	Real time clock with day, month, year, hour, minute and second. One second resolution, ± 1 second stability over 12 hours. Needs keyboard initialization only after battery replacement
Digital Data Output	RS-232C serial interface for digital printer, modem, microcomputer or cassette tape recorder. Data outputs in 7 bit ASCII, no parity format. Baud rate is keyboard selectable at 110, 300, 600 and 1200 baud. Carriage return delay is keyboard selectable in increments of one from 0 through 999. Handshaking is done through X-ON/X-OFF protocol. Allows IGS-2 to act as a master for other instrumentation.

Analog Output	For a strip chart recorder. 0 to 999 mV full scale with keyboard selectable sensitivities of 10, 100 or 1000 units full scale.
Console Dimensions	240 x 90 x 240 mm includes mounted battery pack.
Weights	Console; 2.2 kg. Console with Non-rechargeable Battery Pack; 3.2 kg. Console with Rechargeable Battery Pack; 3.6 kg.
Operating Temperature Range	-40°C to +50°C provided optional Display Heater is used below -20°C.
Power Requirements	Can be powered by external 12 V DC or one of the Battery Pack Options listed below.

2. IGS-2/MP MAGNETOMETER

2.1 The Magnetic Method

The magnetic method consists of measuring the magnetic field of the earth as influenced by rock formations having different magnetic properties and configurations. The measured field is the vector sum of induced and remanent magnetic effects. Thus, there are three factors, excluding geometrical factors, which determine the magnetic field. These are the strength of the earth's magnetic field, the magnetic susceptibilities of the rocks present and their remanent magnetism.

The earth's magnetic field is similar in form to that of a bar magnet's. The flux lines of the geomagnetic field are vertical at the north and south magnetic poles where the strength is approximately 60,000 nT. In the equatorial region, the field is horizontal and its strength is approximately 30,000 nT.

The primary geomagnetic field is, for the purposes of normal mineral exploration surveys, constant in space and time. Magnetic field measurements may, however, vary considerably due to short term external magnetic influences. The magnitude of these variations is unpredictable. In the case of sudden magnetic storms, it may reach several hundred gammas over a few minutes. It may be necessary, therefore, to take continuous readings of the geomagnetic field with a base station magnetometer while the magnetic survey is being done. An alternative field procedure is to make periodic repeat measurements at convenient traverse points, although this is a very unreliable method during active magnetic storms when it is important to have proper reference data.

The intensity of magnetization induced in rocks by the geomagnetic field F is given by:

$$I = kF$$

where I is the induced magnetization

k is the volume magnetic susceptibility

F is the strength of the geomagnetic field

For most materials, k is very much less than 1. If k is negative, the body is said to be diamagnetic. Examples are quartz, marble, graphite and rock salt. If k is a small positive value, the body is said to be paramagnetic, examples of which are gneiss ($k =$

0.002), pegmatite, dolomite and syenite. If k is a large positive value, the body is strongly magnetic and it is said to be ferromagnetic, for example, magnetite ($k = 0.3$), ilmenite and pyrrhotite.

The susceptibilities of rocks are determined primarily by their magnetite content since this mineral is so strongly magnetic and so widely distributed in the various rock types. (Of considerable importance, as well, is the pyrrhotite content.)

The remanent magnetization of rocks depends both on their composition and their previous history. Whereas the induced magnetization is nearly always parallel to the direction of the geomagnetic field, the natural remanent magnetization may bear no relation to the present direction and intensity of the earth's field. The remanent magnetization is related to the direction of the earth's field at the time the rocks were last magnetized. Movement of the body through folding, etc., and the chemical history since the previous magnetization are additional factors which affect the magnitude and direction of the remanent magnetic vector.

Thus, the resultant magnetization M of a rock is given by:

$$M = M_n + kF$$

where M_n is the natural remanent magnetization, and F is a vector which can be completely specified by its horizontal (H) and vertical (Z) components and by the declination from true north. Similarly, M_n is specified when its magnitude and direction are known. Thus, considerable simplification results if $M_n = 0$, whereupon M simply reduces to kF . In the early days of magnetic prospecting, it was usually assumed that there was no remanent magnetization. However, it has now been established that both igneous and sedimentary rocks possess remanent magnetization, and that the phenomenon is a widespread one.

2.2 Magnetometer Specifications

Total Field Operating Range	20,000 to 100,000 nT (1 nT = 1 gamma)
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Gradient Tolerance	<u>+5000 nT/m</u>
Total F	

Total Field Absolute Accuracy	± 1 nT at 50,000 nT ± 2 nT over total field operating and temperature range.
Resolution	0.1 nT
Tuning	Fully solid-state. Manual or automatic mode is keyboard selectable.
Reading Time	2 seconds. For portable readings this is the time taken from the push of a button to the display of the measured value.
Continuous Cycle Times	Keyboard selectable in 1 second increments upwards from 2 seconds to 999 seconds.

3. IGS/VLF-4 ELECTROMAGNETIC RECEIVER

3.1 VLF Theory

VLF stations (total of 12 stations located around the world) radiate electromagnetic waves on the VLF band in the range between 15 to 29 kHz. The signals are transmitted for purposes of navigation and communication with submarines. The VLF Electromagnetic Receiver picks up the magnetic and electric fields of these signals to provide information about the electrical properties of the earth.

The signal transmitted by the VLF station is recorded by the vertical coils as:

$$H_p = A \sin w ; H_s = B \cos (w - \phi) \quad (1.0)$$

where H_p = primary signal

A = amplitude of primary signal

H_s = secondary (phase laged) signal

B = amplitude of secondary signal

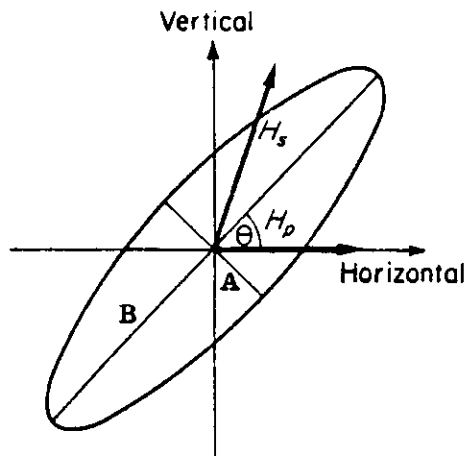
w = frequency

t = time

ϕ = phase lag

These two received signals combine giving an ellipse (see fig. A), which two axis correspond to the length and width of the ellipse.

$$\text{i.e. } \frac{H_p^2}{A^2} + \frac{H_s^2}{B^2} - \frac{2 H_p H_s \sin \phi}{AB} = \cos^2 \phi$$



By measuring the angle from the horizontal to the longaxis of the ellipse (θ), a conductor is located when this tilt angle is zero.

As its primary measurement, the IGS-2/VLF-4 employs two mutually orthogonal receive coils to determine three parameters of the VLF magnetic field. These are: 1) the horizontal amplitude vector in a direction perpendicular to a line joining the operator to the station; 2) the amplitude of the component of the vertical field vector which is in phase with the horizontal vector; and 3) the amplitude of the component of the vertical field vector which is 90° out of phase with the horizontal vector. These three parameters, for the given VLF transmitter, are recorded simultaneously. Since the vertical components are expressed as a percentage of the horizontal vector, they are automatically normalized for any changes in the amplitude of the transmitted primary field.

The primary field from a VLF station can, in fact, vary considerably. For the most part, the field fluctuates moderately during the course of the day due to changes in atmospheric conditions. There are, however, more dramatic changes. Towards evening there is a large upwards swing in the field strength, and at several points during the day, both partial and total drops in the field amplitude can be observed. In the light of these irregularities, the horizontal field data should always be considered with reservation as it is difficult to know whether changes are caused by conductors or by variations in the station's signal.

If the primary field strength is constant, changes in the amplitude of the horizontal magnetic field mainly reflect variations in the conductivity of the earth. Normally, there will be no vertical magnetic field. However, near a conductor, a vertical field will be observed. The relative amplitudes of the in-phase and quadrature components may be used to interpret the conductivity-size characteristics of the conductor.

3.2 IGS/VLF-4 Specifications

Frequency Tuning	Automatic digital tuning. Can be tuned to any frequency in the range 15.0 to 29.0 kHz with a bandwidth of 150 kHz.
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Up to three frequencies can be chosen by keyboard entry for sequential measurements.

Field Strength Range	Fields as low as 100 mA/m can be received. In practice, background noise may require fields up to 5-10 times this level. Maximum received field is 2 mA/metre. These values are specified for 20 kHz. For any other frequency, calculate the above limits by multiplying by the station frequency in kHz and dividing by 20.
Signal Filtering	Narrow bandpass, low pass and sharp cut-off high pass filters.
Measuring Time	0.5 seconds sample interval. As many as 216 samples can be stacked to improve measurement accuracy.
VLF-Magnetic Field Components Measured	1) Horizontal amplitude, 2) vertical in-phase component, and 3) vertical quadrature components. Vertical components are displayed as a percentage of horizontal component and are related in phase to the horizontal component. Their range is $\pm 120\%$; reading resolution 1%.
VLF-Magnetic Field Sensor	Two air-cored coils in a backpack mounted housing with an electronic level for automatic tilt compensation. The error in the vertical in-phase component is less than 1% for tilts up to $\pm 15^\circ$.

3.3 Fraser Filtering

This technique for filtering VLF-EM data was proposed by Dr. D. C. Fraser in 1969. The reason for applying this filter is that there is a dynamic range problem when presenting the data as profiles. In the same area that a 5° peak to peak anomaly may be significant, anomalies of 100° may also occur. This filtering operation transforms the zero cross-overs into peaks and noise is reduced by application of a low-pass filter. The data may be presented as profiles or the positive values may be contoured.

This filter was originally applied to dip angle data as collected by VLF receivers such as the Radem by Crone Geophysics. It is equally applicable to vertical in-phase and quadrature data.

The filter phase-shifts the data by 90° so that zero cross overs and inflections are transformed into peaks. It removes dc and attenuates long spatial wavelengths to increase resolution of local anomalies.

These requirements are met by the difference operator $(R(n+1)-R(n))$, where $R(n)$ and $R(n+1)$ are any two consecutive readings.

The filter does not exaggerate the random noise. This is achieved by applying a low-pass operator to the differences as follows:

$$0.25(R(n+1)-R(n)+0.50(R(n+2)-R(n+1))+0.25(R(n+3)-R(n+2))).$$

The filtered output is then $0.25(R(n+2)+R(n+3)-R(n)-R(n+1))$.

As this filtering process was originally designed to be simple so it could be applied by field personnel with limited facilities, the constant is eliminated.

The plotted function then becomes $F(n+1,n+2)=(R(n+2)+R(n+3)-(R(n)+R(n+1)))$.

The interpretation of filter plots is qualitative. Since the filter retains relative amplitudes, large responses can be equated with large and/or highly conductive zones. Very sharp responses indicate shallow sources, and, conversely, broader anomalies indicate progressively deeper sources. The contouring connects responses from line to line and serves to delineate the trend of conductive zones.

An additional interpretive tool is a pseudo-section of the filter outputs. This is produced by processing a given data profile with filters of various lengths or spans. As the length of the filter increases, responses from increasing depths are successively emphasized. Therefore, if these outputs are arranged on a section such that greater depths correspond to longer filters, then the section should approximately resemble the current pattern in the ground. However, it must be emphasized that this is only an approximation to the section (i.e. pseudo-section). Construction of the section follows a number of steps.

3.4 Resistivity

To permit measurement of the VLF-electric field, a dipole consisting of two cylindrical electrodes and five metres of wire is used. When this dipole is correctly laid out, the IGS-2/VLF-4 measures the in-phase and quadrature components of the horizontal electric field in the direction of the line joining the operator and the transmitter station. The phase reference is the horizontal magnetic field.

The IGS-2/VLF-4 uses the magnetic and electric field measurements to automatically calculate the apparent resistivity of the earth as well as the phase angle between the magnetic and electric field components. If the earth is uniform (not layered) within the depth of the VLF measurement, the phase angle between the horizontal magnetic and electric VLF fields will be 45°. A non-uniform earth will give rise to other phase angles.

The following formulae are used for resistivity and phase calculations:

Apparent Resistivity Calculation:

$$\rho = \frac{1}{2\pi f \mu_0} \left| \frac{E_x}{H_y} \right|^2$$

where:

ρ = apparent resistivity on ohm metres

E_x = horizontal electric amplitude, calculated

$$E_x = (E_x(I)^2 + E_x(Q)^2)^{1/2}$$

H_y = horizontal magnetic amplitude, measured

f = VLF station frequency in Hertz

μ_0 = permeability of the ground in Henries/metre,
a constant

The resistivity calculation has a range of 1 to 100,000 ohm metres with a resolution of 1 ohm metre.

Phase Angle Calculation:

The phase angle ϕ is expressed as:

$$\phi = \text{arc tan } \frac{E_x(Q)}{E_x(I)}$$

where:

$E_x(Q)$ = horizontal quadrature VLF electric field

$E_x(I)$ = horizontal in-phase VLF electric field,
phase referenced to the horizontal
magnetic field, H_y .

The phase angle calculation has a range of -180° to $+180^\circ$ with a resolution of 1° . By definition, the angle is positive when the electrical field leads the magnetic field.



TYPE OF REPORT/SURVEY(S) GEOPHYSICAL	TOTAL COST \$ 4800.00
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AUTHOR(S) DAMIR CUKOR SIGNATURE(S) [Signature]

DATE STATEMENT OF EXPLORATION AND DEVELOPMENT FILED MAY 26 1992 YEAR OF WORK 92

PROPERTY NAME(S) GRAD, POCAHONTAS 1-8

COMMODITIES PRESENT COPPER, GOLD

B.C. MINERAL INVENTORY NUMBER(S), IF KNOWN

MINING DIVISION NANAIMO NTS 92F/9W

LATITUDE LONGITUDE

NAMES and NUMBERS of all mineral tenures in good standing (when work was done) that form the property [Examples: TAX 1-4, FIRE 2 (12 units); PHOENIX (Lot 1706); Mineral Lease M 123; Mining or Certified Mining Lease ML 12 (claims involved)]:

GRAD 229847, POCAHONTAS 1-8 230266-230273

OWNER(S) (1) DAMIR CUKOR (2)

MAILING ADDRESS 6108 McKEE ST BURNABY, B.C.

OPERATOR(S) (that is, Company paying for the work) (1) (2)

MAILING ADDRESS

SUMMARY GEOLOGY (lithology, age, structure, alteration, mineralization, size, and attitude): Volcanics of Karmutsen Formation intruded by Island Intrusives. Copper and gold mineralization hosted by massive magnetite skarns and banded skarns.

REFERENCES TO PREVIOUS WORK

500W 400W 300W 200W 100W 0 100E 200E 300E 400E 500E 600E 700E

BASELINE

GRAD CLAIM

POKAHONTAS 5
POKAHONTAS 4



LINE 4N

LINE 3N

LINE 2N

LINE 1N

LINE 0

LINE 1S

LINE 2S

— In phase
- - - Quadrature
Interpreted VLF Conductors {
— Strong
- - - Moderate
- ? - Weak and very weak

in %
60
40
20
0
-20
-40
-60

Note:
Vertical scale applies
to all stacked profiles

0 25 50 75 100m

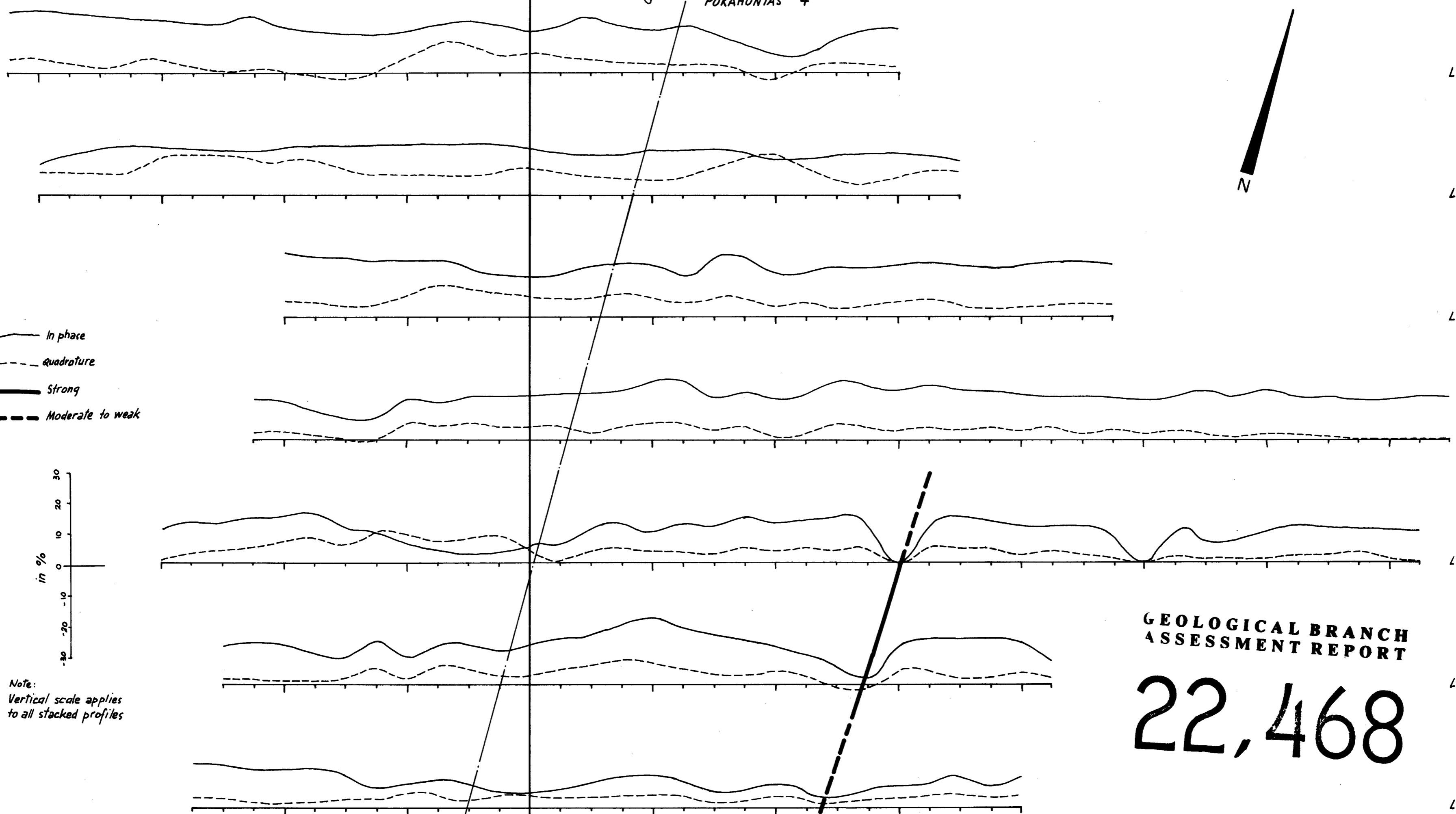
**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

22,468

NLK, SEATTLE, Wa. 24.8 kHz

POKAHONTAS CLAIM GROUP	
VLF-EM SURVEY - SEATTLE STACKED PROFILES	
NANAIMO M.D., B.C.	NTS 92F/9W
DAMIR CUKOR, geol.	VANCOUVER, B.C.
DATE: Aug. 1992	SCALE: 1:2,500
	FIG. 3

500 W 400 W 300 W 200 W 100 W 0 100 E 200 E 300 E 400 E 500 E 600 E 700 E



LINE 4N

LINE 3N

LINE 2N

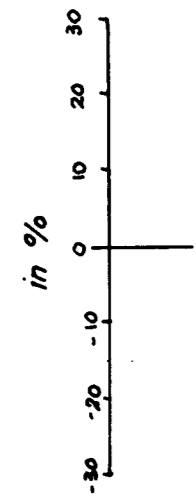
LINE 1N

LINE 0

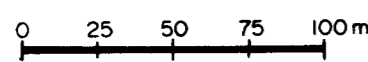
LINE 1S

LINE 2S

— In phase
 - - - quadrature
 Interpreted VLF Conductors { — Strong
 - - - Moderate to weak



Note: Vertical scale applies to all stacked profiles



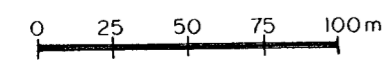
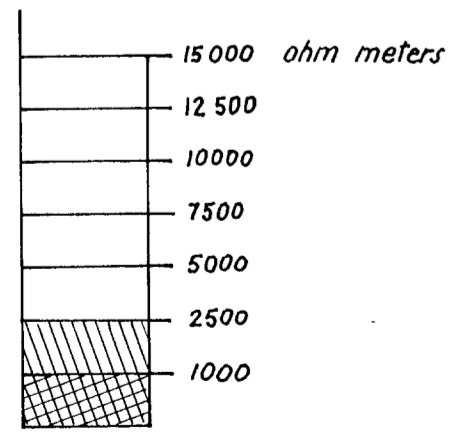
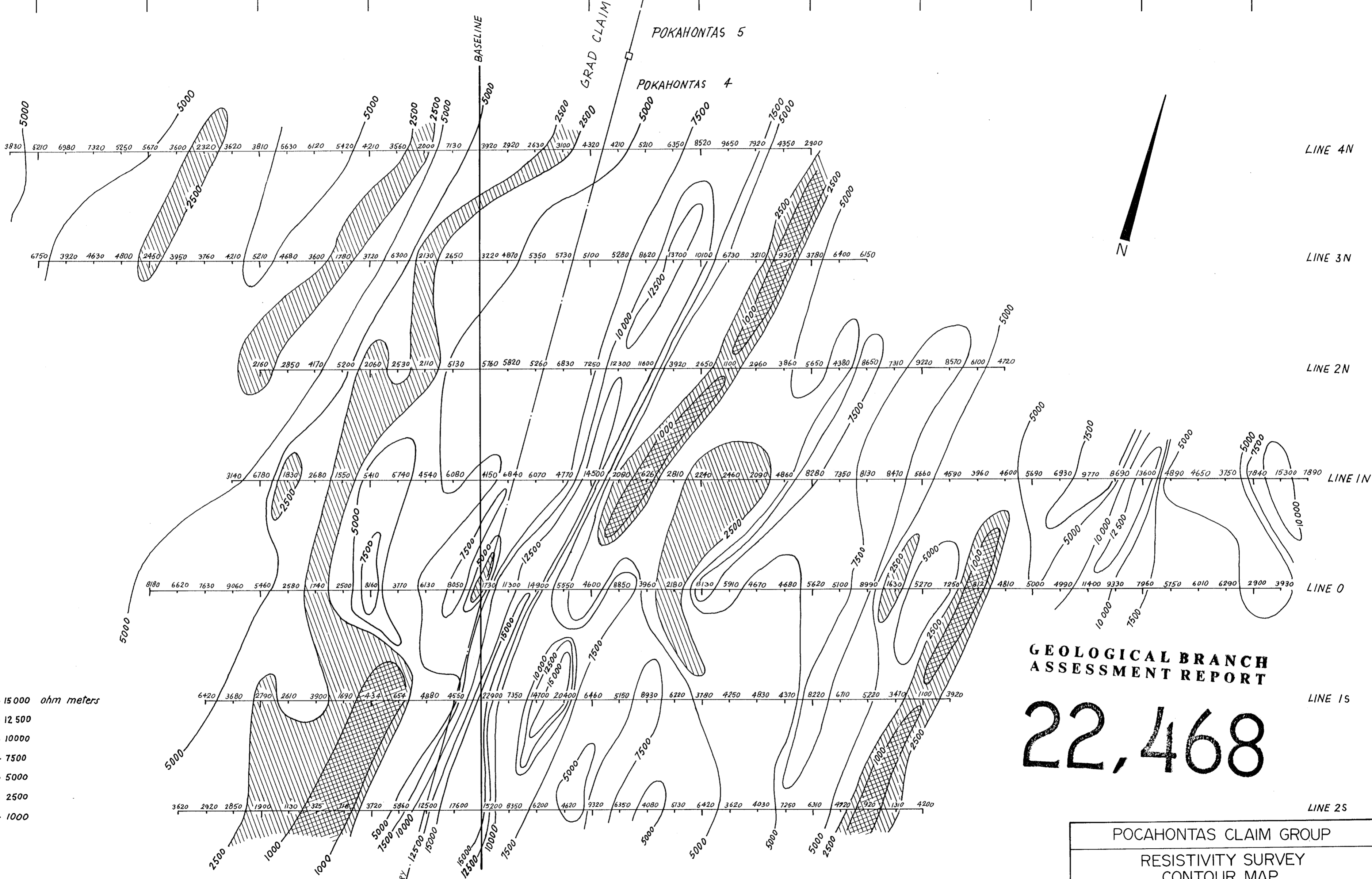
**GEOLOGICAL BRANCH
 ASSESSMENT REPORT**

22,468

NPM, LUALUALEI, HAWAII 23,4 kHz

POCAHONTAS CLAIM GROUP	
VLF-EM SURVEY - HAWAII STACKED PROFILES	
NANAIMO M.D., B.C.	NTS 92F/9W
DAMIR CUKOR, geol.	VANCOUVER, B.C.
DATE: Aug. 1992	SCALE: 1: 2,500
	FIG. 4

500 W 400 W 300 W 200 W 100 W 0 100 E 200 E 300 E 400 E 500 E 600 E 700 E



**GEOLOGICAL BRANCH
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POCAHONTAS CLAIM GROUP		
RESISTIVITY SURVEY CONTOUR MAP		
NANAIMO M.D. B.C.	NTS 92F/9W	
DAMIR CUKOR, geol.	VANCOUVER, B.C.	
DATE: Aug. 1992	SCALE: 1:2,500	FIG. 5

VLF STATION: SEATTLE 24.8 KHZ