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MASS PROPERTY

Cariboo Lake, British Columbia

NTS: 93A/11W,14W

GEOLOGY, GEOCHEMISTRY, GEOPHYSICS AND TRENCHING, 1992

SUB-RECORDER	
NOV 0 5 1992	
M.R. # \$	
Claims:	Mass 1 to 6; Sel 1 to 4; Lad 1, 2, 10 - 15 Cariboo Mining Division 52° 44'N, 121° 22'W
Owners:	Formosa Resources Corporation
Operator:	Rio Algom Exploration In COLOGICAL BRANCH ASSESSMENT REPORT
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CC, D'

W S Donaldson

October 1992

SUMMARY

During the summer of 1992, at a cost of \$ 64,640, a programme of geological mapping, geophysical work, geochemical sampling and mechanical trenching was carried out over the Mass Property by Rio Algom Exploration Inc. The purpose of the program was to locate the source of the zinc, lead, silver and copper-bearing massive sulphide boulders found at the mouth of Frank Creek.

Geological mapping of the Palaeozoic Harveys Ridge succession identified most of the conductors detected in an airborne survey in 1991 as being due to graphitic schist. VLF-EM, GENIE HLEM and soil sampling surveys were conducted over the remaining four unexplained airborne conductors. The better targets were then mechanically trenched. All trenched conductors were found to be caused by of graphitic argillite and schist. It is concluded that the geochemical anomalies are due to either high background in the metasedimentary rocks, localized mineralized quartz veining, or faults and shears resulting in the remobilization of elements.

Massive sulphide mineralization of the type seen in the boulders and sought was not found through the work performed by Rio Algom Exploration Inc. The source therefore is up ice and off the property, or is very small and not detectable by the work done. It is recommended that the option be terminated.

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1 INTRODUCTION

1.1 General

This report describes the results of geological mapping, geophysical work, geochemical sampling and a mechanical trenching programme carried out by Rio Algom Exploration Inc during the 1992 field season on the Mass Property.

Rio Algom acquired an option on the Mass property from Formosa Resources Corporation and Annex Exploration Corp in the belief that the source of zinc, lead, silver and copper-bearing massive sulphide boulders, found at the mouth of Frank Creek, might lie somewhere on these claims.

The purpose of the 1992 work was to identify possible source areas of the massive sulphide boulders.

1.2 Location, Access and Physiography

The claims are situated on the south shore of Cariboo Lake, approximately 15 km northeast of the village of Likely, B.C. (Map 1). The claims are accessible by all weather logging roads from Likely. The 8400 Road, which begins just south of the Cariboo River, near the Weldwood logging camp, leads to spurs 8400C, 8400D and 8400E which give direct access to the property.

Elevations on the property range from 812 metres at Cariboo Lake to 1500 metres. The property is covered by a mixture of overgrown logging slash, fresh clearcuts and subeconomic timber. A tree farm licence covering the claims is held by Weldwood Canada.

1.3 **Property and Claim Status**

The Mass Property comprises the following claims:

Mass Option

Claim	Units	Record No.	Record Date	e
Mass 1	20		302116	May 17, 1991
Mass 2	20		205839	Sep 26, 1988
Mass 3	10		205840	Sep 27, 1988
Mass 4	12		205841	Sep 28, 1988
Mass 5	10		208563	Sep 29, 1988
Mass 6	12		305914	Oct 29, 1991
Sel 1	6		205618	Nov 18, 1987
Sel 2	18		205619	Nov 18, 1987
Sel 3	12		205620	Nov 18, 1987
Sel 4	12		205621	Nov 18, 1987

Lad 1 Lad 2	20 18	207367 207368	Apr 13, 1991 Apr 13, 1991
Lad 10	1	207376	Apr 11, 1991
Lad 11	1	207377	Apr 11, 1991
Lad 12	1	207378	Apr 11, 1991
Lad 13	1	207379	Apr 11, 1991
Lad 14	1	207380	Apr 11, 1991
Lad 15	1	207381	Apr 10, 1991

All claims are in good standing until 1995. The Mass 6 claim was staked by Rio Algom in 1991 and is not subject to the option agreement.

1.4 History

Frank Creek has seen sporadic placer mining activity since the early 1900's. The most recent placer work on the creek was undertaken by the Rasmussen brothers between 1984 and 1986. Boulders of massive sulphides were uncovered in the course of sinking a 14.6 metre shaft on the east side of the creek. A hard rock claim named the Home Run (9 units) was staked but little work was done and the property lapsed in 1987. Golden Eye Minerals restaked this area as the Mass claims in 1987 and incorporated them into the Mass group in February 1989.

In 1988, Formosa Resources Corporation optioned the Mass claims and carried out grid soil sampling, VLF-EM surveys and geological mapping over portions of the Mass 2, Mass 3, Mass 5 and Sel 1 claims. This work delineated a number of exploration targets consisting of coincident electromagnetic and coincident zinc-in-soil anomalies which Formosa geologists believed might be caused by massive sulphide mineralization.

The boulders were examined and sampled in 1991 by Rio Algom. The boulders are 30 to 60 cm across and consist solely of massive pyrite, with lesser pyrrhotite and minor sphalerite, galena, barite and chalcopyrite. White hydrozincite coats the surface. It was concluded that the sulphides in the boulders are the result of syngenetic mineralization, and that the boulders are from a local source.

The 1991 field programme of Rio Algom Exploration Inc. consisted of reconnaissance mapping, prospecting, silt sampling and an airborne EM survey, which was carried out over the entire potential boulder source area. Numerous EM conductors were identified by the airborne survey, leading to the more detailed exploration programme in 1992, reviewed in this report. Work in 1991 is described in a report by J.A. McClintock (1991).

2



2 REGIONAL GEOLOGY

The Mass Property lies in the Cariboo Gold Belt (Struik, 1988) in the Barkerville Terrane, one of four fault-bounded stratigraphic and tectonic terrains that were deposited in an ocean and consisting of continental shelf and slope clastics, carbonates and volcaniclastics.

Geology of the area consists of the Harveys Ridge succession, a member of the Palaeozoic Snowshoe Group and consists of quartzite, phyllite, schist, siltite, limestone, conglomerate and metatuff. Regional geology in the immediate area of the Mass property consists of undifferentiated Snowshoe Group rocks to the east and Harveys Ridge succession to the north. To the west, the rocks are the Hadrynian(?) Keithley succession, consisting of quartzite, phyllite and minor marble. An intrusion of Palaeozoic Quesnel Lake granite orthogneiss occurs in this succession, extending onto the Property.

Structurally, the area is dominated by a northwest-striking, moderately southwest-dipping foliation, as determined from abundant metasedimentary rocks in the area. The Lightning Creek anticlinorium (a northwest-trending structure) occurs five kilometres north of Frank Creek. Structural disturbance was accompanied by regional prograde and retrograde metamorphism to a chlorite-grade facies.

The NTS 93A/14 mapsheet was mapped by L.C. Struik in 1977-1982 and released as map 1638A which accompanies GSC Memoir 421.

3 RIO ALGOM WORK PROGRAMME

The 1992 field programme consisted of geological mapping, geophysical work, geochemical sampling and a mechanical trenching programme.

3.1 Geological Mapping

Using the geological map prepared by Formosa Resources Corporation in 1988, the 1992 geological mapping programme consisted of further subdivision of the metasedimentary units, the aim being to attribute EM geophysical conductors to either graphitic schists or possible massive sulphide horizons. Mapping was at 1:10,000 scale by Rio Algom personnel at various times between May 24 and September 10, 1992.

3.2 Geophysical Work

An airborne EM geophysical survey was done for Rio Algom Exploration Inc by Aerodat Limited of Mississauga, Ontario in 1991 (McClintock, 1991). The airborne geophysical anomalies not explained by outcropping graphitic schist were investigated further by VLF-EM and GENIE HLEM surveys in 1992.

Four grids (labelled A to D) were flagged for a total of 17.25 km by Durfeld Geological Management Limited of Williams Lake, B C from June 1 to 7, 1992, inclusive. The grid lines were 100 metres apart, with stations at 25 metre intervals.

The author ran a VLF-EM survey using a hand-held EM-16. The VLF transmitter station used for grid A and B was Cutler 'NAA' and grid C and D used Seattle 'NPG'. Results appear in the attached geophysical report (Appendix IV) by Dennis V. Woods.

Euro-Canadian Geological Services Inc of Vancouver, B C was contracted to run the horizontal loop EM (GENIE) survey. It was conducted from June 15 to 24, 1992, inclusive. The results and report appear in Appendix IV.

3.3 Geochemical Sampling

In conjunction with the geological mapping, prospecting and trenching, 35 silt, 308 soil and 87 rock samples were collected. The locations are plotted on Maps 9 and 11 and the results are plotted on Maps 10 and 11. The analytical data appears in Appendix II and rock descriptions in Appendix III.

Silt samples were collected from flowing streams encountered during prospecting and geological mapping. The silts were placed in kraft bags and sent to Acme Laboratory in Vancouver for analysis.

Soil samples were collected from grids A to C, over the VLF-EM conductors only. Grid D was sampled in its entirety. Soil grids were run on either side of Frank Creek, just above the massive sulphide boulder occurrence, and also in the southeast in an area where anomalous silts were obtained from two creeks. Anomalous soils at four sites on grids A-

C were resampled from the same hole and depth (sample designator 'RS') and from the same hole, but at a 60-80 cm depth (sample designator 'PB'). These results are not plotted on the zinc and lead map (Map 10), however the results may be found on the accompanying assay sheets in Appendix II. Soil samples were collected in kraft bags and sent to Acme Analytical Laboratories, Vancouver, B.C. for analysis.

Rocks sampled consisted of float, outcrop, and bedrock in the trenches on grids A-D. Approximately two kilograms of rock chips were collected for each sample, and the samples were sent to Chemex Laboratory of North Vancouver, B.C. for analysis.

3.4 Trenching Programme

The objective of the 1992 trenching was to assess the potential zinc/lead massive sulphide potential of several unexplained GENIE HLEM anomalies with or without coincident soil anomalies.

Guinet Management of Vancouver was contracted for 390 metres of trenching. A total of six trenches were excavated on grids A-D from September 1 to September 8, 1992.

Data on the six trenches is noted below:

Grid	Trench	Gric	Length (m)	
Α	A-1	13+00E	21+50N - 22+35N	85
В	B-1	11+00E	20+00N - 20+75N	75
	B-2	13+00E	19+65N - 20+00N	35
С	C-1	13+35N	17+25E - 17+80E	55
	C-2	11+00N	17+25E - 17+75E	50
D	D-1	10+00N	27+25E - 28+15E	90

The purpose of trenches A-1, B-1 and C-2 was to test coincident GENIE HLEM and soil anomalies. The other three trenches were excavated to test GENIE HLEM anomalies without coincident geochemical anomalies.

Six trenches were excavated and then mapped, with a 2 metre chip rock sample, approximately every 5 metres. Locations of the trenches are shown on Map 8 and the results are plotted on Maps 2 to 7. Analytical data appears in Appendix II. Detailed mapping of the trenches differentiated the various rock types, as described in 4.1 - Property Geology.

All trenches were backfilled and landscaped. Rio Algom personnel applied fertilizer and reseeded the trench sites in accordance with regulations of the Ministry of Energy, Mines and Petroleum Resources.

3.5 Laboratory Procedures

All samples were analyzed for gold (by FA/AA) and 30 or 32 elements by ICP (depending on the laboratory).

Soil samples were dried at 60° C, sieved to -80 mesh. A 0.5 gram sample was then digested with 3 ml 3-1-2 (HCl-HNO₃-H₂O) at 95°C for one hour and diluted to 10 ml with water. Analysis for 30 or 32 elements was by inductively coupled plasma (ICP). For gold analysis, a 10.0 gram sample was ignited at 600°C, digested with hot aqua regia, extracted with MIBK and analyzed by graphite furnace atomic absorption.

Rock samples were pulverized to -140 mesh and analyzed using the same procedure as described above. For gold however, the 10.0 gram sample was pre-concentrated using fire assay techniques and finished by atomic absorption analysis.

Silt samples were sieved to -80 mesh and a portion of the -80 mesh fraction was analyzed geochemically for gold and 30 additional elements by ICP.

4 **RESULTS OF WORK**

4.1 **Property Geology**

The purpose of the 1992 work programme was to assess the potential for zinc-lead massive sulphide mineralization on the Mass Property. To this end, prospecting, geological mapping (1:10,000 scale) and selective lithologic, silt and soil sampling was carried out.

Detailed mapping in 1992 has further subdivided the metasedimentary and sedimentary units mapped by Formosa Resources Corporation in 1988.

Property geology consists mainly of metasedimentary rocks of the Palaeozoic Harveys Ridge succession (a member of the Snowshoe Group), that have been intruded by Palaeozoic Quesnel Lake granite orthogneiss and minor Tertiary lamprophyre dykes. Descriptions of the units mapped, with the labels used on the accompanying maps, are as follows.

Metasedimentary Rocks

SAT: Sericite-Albite-Talc Schist

Localized along the east-central portion, this rock was originally a volcanic tuff(?). It is a light green, fine-grained, schistose rock composed of sericite, albite and talc. Minor quartz veins to 6 mm wide cut the unit and aggregates of pyrite (to 8 mm) average less than 0.5%. Scattered throughout are 1% ankerite porphyroblasts (to 2 mm).

SS: Sericite Schist

Silvery-yellow coloured, vitreous rock, fine-grained, with a good schistose fabric due to pervasive sericite. Minor ankerite porphyroblasts to 1 mm. There is also a trace of disseminated pyrite.

CS: Chlorite Schist

Dark olive-green to black coloured rock, very fine- grained, composed entirely of chlorite. A good foliation is present. There are 2% ankerite porphyroblasts to 3 mm. Minor quartz veins may cut the rock. Minor disseminated pyrite is present.

GS: Graphitic Schist

Dull silver-grey colour, very fine-grained, graphite-rich rock, that is conductive. A good foliation is developed in this rock.

PH: Phyllite

Dark grey to black coloured rock, very fine-grained, with a phyllitic texture. There are up to 2% ankerite porphyroblasts in the rock to 2 mm size. Minor disseminated pyrite may be present.

The following two schists are not abundant:

QCS: Quartz-Chlorite Schist

Grey-green colour, medium-grained rock composed of quartz and chlorite, with a weak schistose fabric. There are 2% - 1 mm ankerite porphyroblasts throughout.

QSS: Quartz-Sericite Schist

Grey-yellow colour, medium grain rock composed of quartz and sericite. It has a weak schistose fabric, and contains 2% - 1 mm ankerite porphyroblasts throughout.

Sedimentary Rocks

Sedimentary rocks without foliation comprise only 10% of all rocks on the Mass option.

AR: Argillite

Dark grey, fine-grained rock that is well-bedded. Minor carbonate veins to 1 mm wide cut the unit and some pyrite may be disseminated in the matrix. All fractures are rust-coloured. Argillite in some of the trenches was graphitic.

QA: Quartz Arenite

Light grey colour, with a medium grained, quartz-rich matrix. Minor chlorite is present as well as other sedimentary grains. There are 2% ankerite porphyroblasts in the matrix. The matrix has a weak schistose fabric with a trace of pyrite cubes to 8 mm.

AK: Arkose

Light tan colour, very fine-grained rock. Minor sericite has produced a weak schistose fabric in the rock. There is a trace of disseminated pyrite.

GT: Grit

Brown-grey colour, medium to coarse-grained rock composed of quartz grains to 3 mm, feldspars and other sedimentary minerals in a weakly chloritic and schistose matrix. There are 1% ankerite porphyroblasts in the matrix.

LC: Lithic Conglomerate

Tan-white colour, with lithic clasts (mainly quartz, minor lithic fragments) to 6 cm set in a medium to coarse-grained, channel-fill matrix. The matrix is quite siliceous and has a trace of carbonate. Clasts are elongated and flattened along the foliation plane, which parallels bedding. Quartz veins to 3 cm occur parallel to bedding. Minor disseminated pyrite was observed in some outcrops.

DOL: Dolomite

Two varieties of dolomite were observed:

1) Characteristic light-brown weathered surface, with a light grey-tan fresh surface. The rock is fine-grained with a weak crystalline appearance. Bedding is readily apparent. There is no visible mineralization.

2) Medium-grained crystalline rock with a grey-green coloured fresh surface. Bedding planes are not as apparent as in the first dolomite. The rock has minor disseminated pyrite.

LS: Limestone

Light grey colour, medium-grained, crystalline carbonate. Bedding is apparent (light versus dark layers). The crystallinity is due to metamorphic activity. There is no visible mineralization.

Intrusive Rocks

QLG: Quesnel Lake Granite Orthogneiss

Brown-grey-white colour, with phenocrysts of plagioclase to 6 cm set in a medium to coarse-grained matrix composed of quartz, plagioclase, potassic feldspar, chlorite and minor mafic minerals. Metamorphism has produced definite foliation planes, with most minerals being stretched along the planes. No visible mineralization.

LAM: Lamprophyre Dyke

A minor Tertiary dyke (1 metre wide) was noted in the southwest corner, crosscutting the Quesnel Lake granite orthogneiss.

The rock is dark green, fine-grained and chloritic. There is no visible mineralization.

4.2 Structure

A good structural picture is evident in this metasedimentary package. Most rocks on the property are variably slaty, foliated, laminated or schistose. The regional metamorphic grade is the chlorite zone of the green schist facies. Measurements of foliations and lineations in schistose rocks indicates that a northwest-plunging syncline occurs in the central portion. The syncline plunges 15° northwest and both walls dip on average, 50°.

Bedding measurements on the eastern portion indicate a fining-upward sequence, with the lithic conglomerate being the base of the sedimentary package, overlain by phyllite, argillite, quartz arenite, chlorite and sericite schist.

Quartz augen, lenses and bedding parallel and cross-cutting bull quartz veins occur everywhere, but are more prominent in the more deformed areas (McClintock, 1991).

Structural measurements in the trenches concur with those observed in outcrop. Intense structural deformation and faulting has formed several wide "clay-fault gouge" zones in which the country rock has been intensely sheared, resulting in its alteration to clay. This clay-fault gouge has been observed in some of the argiillites and graphitic schists, in intervals to 8 metres wide.

4.3 Mineralization

Disseminated pyrite to 1% was observed in some phyllites and argillites. Cubic pyrite (2 to 7 mm size) was observed in quartz arenites and the schistose rocks, to 1%. In trench B-1, beds of pyrite 1 to 5 mm thick were noted in the argillite and graphitic argillite at the north end of the trench.

The graphitic schists had low to abundant flake-graphite along bedding planes. There is no evidence of massive sulphide mineralization in any of the outcrops.

4.4 Silt Sampling

Silt sampling was conducted to delineate a source drainage for the massive sulphide boulders found at the base of Frank Creek.

A total of 35 silt samples were collected on the Property. The background used for zinc is 100 ppm and for lead 30 ppm.

All samples to the east of, and along Frank Creek are considered to be background.

Two creeks passing through grid E (in the southeast) show elevated zinc and lead content (up to 379 ppm zinc, 53 ppm lead). While anomalous, and no source was found, it is the author's opinion that these values are the result of high background in nearby argillites or due to possible manmade contamination (old logging activities at the western end of each creek).

4.5 Soil Sampling

Soil sampling was conducted over grids A to D to follow up VLF-EM anomalies. Two soil lines were also run on either side of Frank Creek to search for a possible source of the massive sulphide boulders. Soils were collected over the southeast corner (grid E) over and beside the two anomalous creeks noted above, to test for a possible source of the silt anomalies.

Due to high soil values found throughout, the sampled areas backgrounds are considered to be 200 ppm for zinc and 60 ppm for lead. Using these cutoffs, the following observations can be made:

Grid A has scattered zinc and lead values. The highest zinc is 409 ppm and the highest lead, 160 ppm. At A13+00E, 22+00N, a hand excavated test pit resampled the original sample (409 ppm zinc, 137 ppm lead), resulting in 1765 ppm zinc and 1210 ppm lead; and, 60 cm deeper, 1999 ppm zinc and 1566 ppm lead. Mechanical trenching revealed graphitic argillite at this grid co-ordinate. Rock sample #15403 gave 1880 ppm zinc and 1240 ppm lead and is probably the source of the soil anomaly. However it is localized and values were not comparable in rock and soil samples to either side.

Grid B had scattered zinc and lead, the highest being 664 ppm and 195 ppm, respectively. Several shears and faults were observed in two trenches on the B grid. These may have concentrated mineralization along them, resulting in the soil anomalies.

Grid C had numerous zinc and lead anomalies, the highest being 627 ppm zinc and 740 ppm lead. Trench C-2 was over this anomaly, and rock sample #15390 had 494 ppm zinc and 340 ppm lead. The rock was a quartz-chlorite schist with 2% pyrite.

Grid D had one lead anomaly of 92 ppm.

The two soil lines on either side of Frank Creek had three zinc anomalies (615, 331, 209 ppm) and two lead anomalies (126, 66 ppm) scattered throughout. As these anomalies are localized it is the author's opinion that they are possibly due to weakly mineralized float in the overburden.

Grid E in the southeast corner, beside and across the two creeks failed to indicate a possible source for the anomalous silts. A total of three soil anomalies are present: 264 and 243 ppm zinc and 66 ppm lead. All others are at background.

4.6 Rock Sampling

Values above 200 ppm zinc and 60 ppm lead are considered to be anomalous in rocks. Four of the surface rock samples are anomalous.

One of the massive sulphide boulders at the base of Frank Creek was sampled. Sample #15224 contained 2.83% zinc, 2.44% lead, 1355 ppm copper, 73 ppm silver and 150 ppb gold. These results are similar to those obtained from boulder sampling in previous years (McClintock, 1991).

On grid A, rock sample #15230 at A13+00E, 22+00N ran 506 ppm zinc and 344 ppm lead. It was a float sample of argillite cut by quartz stringers, with 6% limonite on all fracture surfaces. This grid co-ordinate corresponds to the soil anomaly noted earlier.

On grid B, rock sample #15223 at B11+00E, 20+50N ran 332 ppm zinc and 384 ppm lead. It was of quartzite(?) float with 2% disseminated pyrite.

Sample #A5232, on the spur road to the east of Wilby Creek, ran 128 ppm lead . The rock was a graphitic schist.

Assays of rock from the trenches were generally more anomalous than those in outcrop. In trench A-1, anomalous zinc ranged from 214 -436 ppm and anomalous lead 80 - 280 ppm. Sample #15403 ran 1880 ppm zinc and 1240 ppm lead in a graphitic argillite.

In trench B-1 anomalous zinc ranged from 304 - 4360 ppm and lead 64 - 880 ppm. The high zinc, lead (4360, 880 ppm, respectively) in sample #15371 was from a graphitic schist, beside clay fault gouge. This anomalous value is seen as the result of remobilization of minerals during faulting. Sample #15367 had 1485 ppm zinc, 234 ppm lead, > 10,000 ppm copper and 25.8 ppm silver. The sample is of a large chloritic schist boulder originally thought to be outcrop.

Trench B-2 had one anomalous zinc of 458 ppm in a graphitic argillite shear zone.

In trench C-1, anomalous zinc ranged from 222 - 802 ppm and lead 70 - 636 ppm. Two anomalous samples were of quartz veins. The remaining anomalous samples were from sericite schists, chlorite schists and graphitic argillite.

In trench C-2, anomalous zinc ranged from 208 - 518 ppm and lead 106 - 340 ppm. A sample of clay fault gouge (#15393) gave 2130 ppm zinc and 2220 ppm lead.

Trench D-1 had anomalous zinc (394 ppm) in a sample of graphitic argillite fault gouge (#15354).







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5 CONCLUSIONS AND RECOMMENDATIONS

Evaluation of the Mass Property as a possible source for the massive sulphide mineralization in float resulted in disappointing results.

All of the geophysical anomalies from the airborne Em in 1991 and GENIE HLEM in 1992 are the result of graphitic argillite and graphitic schist, and are not due to massive sulphide mineralization.

Though there were some high results, the source of the soil anomalies are considered by the author to be caused by either high background in the metasedimentary rocks, localized mineralized quartz veining, or faults and shears resulting in the remobilization of minerals.

Rock sampling on surface and in the trenches indicated anomalous zinc and lead. However, the values are quite variable, non-continuous and well below economic levels. The boulders have no host rock and thus cannot be matched to any setting seen on the property.

In conclusion, the geological environment is not inhospitable to the type of mineralization observed in the boulders, but the work performed by Rio Algom has failed to find a source for these. Thus either i) the source is up ice (and off the property), or ii) the source is very small and not detectable by the work done. If it is small, the target is not attractive to Rio Algom. All anomalous situations have been explored. It is most unlikely that the source of the boulders would not have been reflected as both geochemical and geophysical features.

As the results of the 1992 field programme on the Mass Property were not encouraging, it is recommended that Rio Algom terminate the option, and return the property to Formosa Resources Corporation and Annex Exploration Corp.

6 **REFERENCES**

- Martin, L S Geological, Geochemical and Geophysical Report on the Mass Property, 1989. BCDM Assessment Report
- McClintock, J A Mass and Annex Options. Geology, Geochemistry and Geophysics, 1991. BCDM Assessment Report
- Struik, L C Structural Geology of the Cariboo Gold Mining District, East-Central British Columbia. GSC Memoir 421, 1988

7 STATEMENT OF QUALIFICATIONS

I, William Stratton Donaldson, do hereby certify that:

- 1 I am a graduate of Carleton University in Ottawa, Ontario with an Honours Bachelor of Science degree (1985) in Geology.
- 2 I have practised my profession as a geologist continually since graduation.
- 3 I currently reside at 14-1609 Harwood Street, Vancouver, British Columbia.
- 4 I am temporarily employed as a geologist with Rio Algom Exploration Inc with an office at 1650-609 Granville Street, Vancouver, British Columbia.
- 5 I personally assisted in the supervision of the geological, geophysical, geochemical and mechanical trenching programmes conducted on the Mass option during the 1992 field season.

Willia Dovalston

William Stratton Donaldson October 1992

APPENDIX I

COST STATEMENT

APPENDIX I - COST STATEMENT

Salaries

W. Donaldson, Geologist May 24 - Jun. 7, Jul. 1 - 10, Aug. 12 - 16, 31, Sep. 1 - 10 41 days @ \$ 250/day	\$ 10250.00
J. McClintock, Geologist June 1, 2, 17, 18 4 days @ \$ 350/day	\$ 1400.00
S. Casselman, Geologist Sep. 7 - 10 4 days @ \$ 250/day	\$ 1000.00
M. Renning, Prospector July 1 - 10, Aug. 12 - 16, 31, Sep. 1 - 3 19 days @ \$ 215/day	\$ 4085.00
Subtotal	\$ 16,735.00
Other Expenses	
Meals Groceries Accommodation Field Supplies Freight and Shipping Airfare (J. McClintock, C. Spence, M. Renning)	\$ 1105.00 \$ 260.00 \$ 1845.00 \$ 2062.00 \$ 341.00 \$ 955.00
Subtotal	\$ 6,568.00
Transportation	
Truck Rental (Nicholson and Associates), Fuel Boat Rental (2 days from G. Biggs, Likely, B C)	\$ 3045.00 \$ 80.00
Subtotal	\$ 3,125.00
Reports	
Preparation, Drafting, Miscellaneous Geophysical Report and Maps - Dennis V. Woods	\$ 7500.00 \$ 2541.25
Subtotal	\$ 10,041.25

Contract Work

Grid Flagging - Durfeld Geological Management Ltd. GENIE HLEM Survey - Euro-Canadian Geological Mechanical Trenching - Guinet Management	\$ 2939.32 \$ 11342.00 \$ 8626.88
Subtotal	\$ 22,908.20
Geochemical	
Analysis, Acme Analytical Laboratory 308 soils, 35 silts @ \$ 10.81/sample Analysis, Chemex Laboratory	\$ 3707.83
87 rocks @ \$ 17.88/sample	\$ 1555.56
Subtotal	\$ 5263.39
TOTAL COSTS	\$ 64,640.84

COSTS APPORTIONED TO GROUPINGS:

GROUP	GEOLOGY/GEOCHEM	ISTRY PHYSICAL	TOTAL
l	\$ 14,505.40	\$ 7,472.48 \$ 21,977.88	
II	\$ 28,157.55	\$ 14,505.41 \$ 42,662.96	

TOTAL

\$ 64,640.84

APPENDIX II

ANALYTICAL DATA

ACM. 7		LI	υ	ATC	S	Ľ.			E	•	STI	l	ST.		າວບ	I	в.с	16	A			ON	E) 2	5	.58	\$(r		53-	
AA		· .			Ric	<u>5 A</u>	<u>lqor</u> P.0.	n Ex Box	G Kp1 10335	EOCI ora1 , 165	IEM t io 0 - 6	ICA n <u>I</u> 1 0, Va	L Al ncouv	NAL PR er BC	YSI: DJE(V7Y	5 CI <u>CT 9</u> 165	ERT: 0124 Subm	LFIC 4] Nitted	CATI	E 9 # W. DO	92- NALDS	-13: ON	21						A	
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	BAL ppm %	Na %	K %	W / ppm	Au** ppb
SSM-1 SSM-2 SSM-3 SSM-4 SSM-5	1 1 1 1	25 25 24 23 18	13 10 10 11 10	96 64 104 113 118	.2 .1 .2 .1 .3	52 26 36 34 32	20 13 16 14 14	564 644 638 556 654	3.45 2.90 3.31 3.26 3.21	6 10 7 6 9	5 5 5 5 5	ND ND ND ND ND	11 6 10 12 9	15 36 20 18 21	2.7 2.3 3.3 3.1 4.1	2 2 2 2 2	2 2 2 2 2	16 8 10 12 10	.27 .57 .34 .28 .37	.079 .088 .085 .073 .078	31 28 36 39 35	26 17 18 19 17	.65 .38 .41 .41 .50	29 29 34 33 38	.02 .01 .01 .01 .01	2 1.35 2 1.20 2 1.18 2 1.18 2 1.22	.01 .01 .01 .01 .01	.04 .03 .04 .03 .03	1 1 1 1	9 6 2 9 1
SSM-6 SSM-7 SSM-8 SSM-9 SSM-9	1 1 1 1	20 21 23 25 26	13 15 9 14 10	120 113 76 63 83	.1 .2 .1 .2 .1	34 33 27 26 34	14 15 13 12 16	712 671 528 695 456	3.11 3.68 3.12 2.74 3.26	9 10 7 7 5	5 5 7 5	ND ND ND ND ND	11 8 6 4 10	20 23 35 46 15	3.0 3.5 2.5 2.1 2.8	2 2 2 2 2	2 2 2 2 2	7 9 11 9 12	.35 .36 .51 .73 .26	.087 .080 .089 .093 .071	38 32 25 30 29	18 19 20 19 20	.38 .41 .56 .37 .44	38 39 38 33 28	.01 .01 .02 .01 .02	2 1.11 2 1.30 2 1.30 2 1.20 2 1.20	.01 .01 .01 .01 .01	.03 .03 .05 .04 .03	6 1 1 1 1	5 11 10 3 1
RE SS-M92-102 SSM-11 SSM-12 SS-M92-100 SS-M92-101	1 1 3 2 2	46 23 180 28 51	49 17 46 18 74	243 90 247 169 281	3.4 .2 .5 .2 3.5	90 35 75 43 122	22 13 16 18 37	3830 538 597 709 5916	4.52 3.28 3.80 3.68 5.23	19 2 55 10 24	5 5 5 5 5	ND ND ND ND	4 7 3 8 7	80 21 44 21 70	5.1 2.7 3.8 3.1 6.0	2 2 2 2 2	2 2 2 2 2	20 9 14 14 24	1.17 .38 .60 .42 .96	.225 .093 .123 .094 .257	67 36 18 28 75	19 17 21 21 22	.28 .41 .45 .75 .32	274 43 113 74 355	.01 .01 .02 .01 .01	2 2.38 2 1.40 2 .88 2 1.57 2 3.22	.01 .01 .01 .01 .01	.07 .03 .08 .03 .08	1 1 1 1 1 1 1	3 2 5 1 1
SS-M92-102 SS-M92-103 SS-M92-104 SS-M92-105 SS-M92-106	1 1 1 1	47 38 45 37 29	53 45 45 19 16	243 193 221 91 86	3.5 2.5 3.3 .1 .2	90 65 77 43 35	22 17 22 18 12	3871 2217 3201 539 219	4.54 3.37 3.66 3.66 3.31	18 14 19 5 4	5 5 5 5 5	ND ND ND ND	2 2 7 8	81 73 85 24 21	4.9 3.8 4.2 2.7 2.7	2 2 2 2 2	2 2 2 2 2	20 17 18 9 9	1.17 1.09 1.31 .40 .34	.222 .180 .206 .089 .084	68 61 69 41 37	20 18 19 17 17	.27 .30 .31 .65 .56	275 218 237 44 42	.01 .01 .01 .01 .01	2 2.38 2 2.00 3 2.17 2 1.50 2 1.46	.01 .01 .01 .01 .01	.07 .05 .06 .03 .04	1 1 1 1	5 5 11 7 7
SS-M92-107 SS-M92-108 SS-M92-109 SS-M92-110 STANDARD C/AU-S	2 2 3 2 19	54 63 58 36 59	23 32 30 19 41	133 379 319 309 132	.6 2.1 1.9 .6 7.1	66 109 89 56 71	17 32 31 24 31	873 7087 6836 6072 1044	3.93 5.53 6.20 4.81 3.98	5 23 27 17 41	5 5 5 5 17	ND ND ND ND 7	4 5 5 4 37	13 80 56 39 52	3.0 5.9 4.8 4.7 17.8	2 2 2 2 15	2 5 2 2 20	12 16 13 10 54	.23 1.85 1.20 .78 .48	.048 .179 .174 .098 .091	21 76 71 33 37	14 16 17 13 56	.28 .35 .32 .33 .88	92 227 206 188 178	.01 .01 .01 .01 .09	2 1.20 4 2.61 2 2.61 2 1.59 34 1.88	.01 .01 .01 .01 .07	.03 .06 .06 .05 .15	1 1 1 1 1 10	8 3 2 53

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. Samples beginning HRE' are duplicate samples. - SAMPLE TYPE: SILT

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	A5210 A5231 A5232 RE A5231	8 2 4 3	191 227 138 221	10 4 128 2	121 92 70 91	.1 .1 1.3 .1	19 8 28 9	12 9 33 9	985 688 446 696	9.00 6.89 12.35 7.05	4 3 63 2	- 5 5 5 5	ND ND ND ND	9 9 2 10	61 15 4 15	.5 .2 .2 .2	2 2 2 2	6 7 38 8	72 32 12 33	.86 .30 .03 .29	.301 .054 .023 .055	14 11 5 11	35 32 22 32	2.69 2.51 .43 2.52	231 139 81 137	.13 .14 .01 .14	2 2 6 2	3.35 3.05 .59 3.03	.01 .01 .01 .01	.18 .20 .08 .21	1 1 1	6 12 21 6

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB - SAMPLE TYPE: ROCK AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. <u>Samples beginning / RE' are duplicate samples.</u>

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10+00E A24+00N 10+00E A23+50N 11+00E A25+00N 11+00E A24+50N 11+00E A24+00N	1 1 1 1	30 15 34 21 40	36 32 27 25 70	128 89 102 149 141	.1 .4 .3 .3 .4	26 16 32 31 39	9 6 8 12 22	145 93 129 399 580	4.57 4.03 2.74 2.79 3.98	21 18 26 20 34	5 5 7 5 13	ND ND ND ND	7 5 1 2	6 7 9 19 17	.2 .2 .2 .3 .2	2 2 2 2 2 2	2 2 2 2 4	24 34 17 24 26	.04 .05 .08 .16 .20	.100 .064 .051 .042 .068	23 24 28 17 20	27 25 26 30 33	.44 .30 .31 .31 .64	95 .01 99 .02 125 .01 104 .02 163 .01	2 1.82 2 1.52 2 1.04 2 1.09 2 2.08	.01 .01 .01 .01 .01	.06 1 .05 1 .06 1 .05 1 .09 1	1 3 8 14 1
11+00E A23+50N 11+00E A23+00N 11+00E A22+50N 11+00E A22+00N 11+00E A21+50N	3 1 1 1 1	113 28 83 74 14	65 33 47 53 35	224 99 208 211 64	1.5 .7 2.4 .8 .5	56 25 62 44 11	16 8 19 18 4	240 140 771 1083 218	5.45 3.65 4.58 3.77 2.23	64 22 39 29 14	7 5 8 5	ND ND ND ND ND	5 8 3 1	13 11 40 34 10	.2 .2 1.1 1.3 .2	2 2 2 2 2	2 2 3 2	27 24 22 19 21	.09 .12 .76 .58 .08	.201 .086 .113 .121 .165	22 31 26 15 20	26 23 29 22 16	.30 .47 .57 .47 .14	105 .01 114 .01 177 .01 112 .01 104 .02	2 1.50 2 1.46 2 2.06 2 1.45 3 .94	.01 .01 .01 .01 .01	.06 1 .06 1 .13 2 .08 1 .05 1	4 4 1 6
12+00E A25+00N 12+00E A24+50N 12+00E A24+00N 12+00E A23+50N 12+00E A23+00N	1 1 2 1 1	41 57 30 21 37	32 44 20 20 34	136 227 105 120 192	.9 2.4 .2 .1 .2	50 77 27 25 36	10 15 7 7 11	138 289 130 134 190	3.77 3.97 3.22 2.80 4.86	42 43 31 22 30	5 5 5 5	ND ND ND ND	7 3 5 5 7	12 33 7 9 11	.2 .3 .2 .2 .2	2 2 2 2 2	2 2 2 2 2	22 26 24 20 27	.11 .39 .07 .09 .12	.070 .064 .034 .052 .067	25 20 22 27 25	41 42 20 19 28	.50 .63 .29 .31 .45	130 .01 138 .01 98 .01 120 .01 127 .01	2 1.33 2 1.68 2 1.27 2 1.10 2 1.78	.01 .01 .01 .01 .01	.06 1 .06 2 .04 1 .06 1 .06 1	12 1 51 45 5
12+00E A22+50N 12+00E A22+00N 12+00E A21+50N 13+00E A25+00N 13+00E A24+50N	1 1 1 1 1	98 44 31 21 52	74 34 40 30 79	346 139 100 191 159	2.0 .2 .6 .8 .1	68 31 21 41 39	30 10 7 14 12	3170 214 174 270 139	5.88 4.76 4.20 3.51 4.22	43 24 31 27 100	5 5 5 5 5	ND ND ND ND ND	5 6 3 7 6	43 11 10 25 5	2.6 .2 .3 .2 .2	2 2 2 2 2	2 2 2 2 2	30 24 22 35 24	.88 .11 .15 .25 .03	.148 .137 .156 .030 .039	18 24 18 22 29	31 27 18 43 18	.67 .49 .22 .83 .12	207 .07 91 .01 91 .07 120 .02 55 .01	2 2.44 2 1.53 2 1.36 2 1.94 2 1.03	.01 .01 .01 .01 .01	.13 2 .06 1 .06 1 .05 2 .03 1	5 1 1 6 1
13+00E A24+00N 13+00E A23+50N 13+00E A23+00N 13+00E A22+50N 13+00E A22+00N	1 1 1 1 2	21 107 77 31 91	62 34 166 36 127	62 193 260 138 404	.4 .3 .1 .5 2.8	15 49 59 28 42	5 20 14 8 11	88 169 232 155 473	1.80 5.29 5.34 3.94 4.01	41 86 44 33 42	5 5 5 5 5	nd Nd Nd Nd	5 5 7 6 4	5 14 6 11 9	.2 .2 .2 .2 .2	2 2 2 2 2	2 2 2 2 2 2	17 25 21 23 27	.05 .17 .05 .13 .09	.032 .065 .106 .079 .078	31 21 24 27 22	9 15 30 24 17	.06 .12 .46 .42 .10	35 .0° 89 .0° 101 .0° 91 .0° 118 .07	2 .67 2 .84 2 1.77 2 1.26 3 .93	.01 .01 .01 .01 .01	.02 1 .04 2 .05 1 .06 1 .04 1	29 21 8 1 13
RE 13+00E A23+50N 13+00E A21+50N 14+00E A25+00N 14+00E A24+50N 14+00E A24+00N	1 1 1 1 1	112 57 15 15 39	37 41 34 30 47	198 199 98 84 128	.4 2.0 .8 .2 1.2	48 46 20 19 32	20 15 7 6 10	169 637 143 206 188	5.32 3.89 2.34 3.82 6.21	89 28 35 65 100	5 5 9 5 5	nd Nd Nd Nd	6 6 8 4 6	14 22 10 9 6	.2 .9 .2 .2 .2	2 2 2 2 2	2 2 2 2 2	25 20 26 26 30	.17 .37 .10 .16 .04	.065 .062 .027 .036 .206	23 22 24 24 20	14 25 14 12 24	.12 .60 .07 .05 .28	93 .0' 115 .0' 128 .0' 81 .0' 73 .0'	2 .89 2 1.76 2 .68 3 .73 2 1.39	.01 .01 .01 .01 .01	.04 1 .08 1 .03 2 .02 2 .05 1	31 1 7 1 30
14+00E A23+50N STANDARD C/AU-S	3 17	72 56	75 38	169 133	1.0 6.9	37 66	11 31	187 1056	5.67 4.01	88 41	5 22	ND 7	4 39	10 53	.2 16.8	2 14	2 19	25 56	.09 .49	.163 .090	20 35	20 56	.25 .89	100 .0 182 .04	2 1.25 34 2.00	.01 .07	.05 1 .15 11	4 49
DATE RECI	EIVEI	ICP - THIS - SAM	.50 LEAC IPLE JUL 1	0 GRA H IS TYPE: 0 199	M SAMP PARTIA SOIL 2 DI	PLE IS	DIGE MN I U** / REP	STED E SR NALY	WITH CA P SIS B MAI	3ML 3 LA CR (FA/1 LED:	S-1-2 MG B CP FR	HCL-H BA TI ROM 10	INO3-H B W A) GM S 17/	20 AT ND LI AMPLE	T 95 D IMITED E. <u>Sa</u> SI (EG. C FOR mples	FOR NA K begi BY	ONE H AND A ming		AND IS AU DET ' are	DILU ECTIO dupli	TED T N LIM cate YE, C	O 10 IIT BY Sampl	ML WITH V ICP IS I es. G, J.WANG	ATER. 5 PPM. ; CERTIFIED) B.C.	ASSAYERS	
										(]	/	/							1								



Rio Algom Exploration Inc. PROJECT 9124 FILE # 92-1858



SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	V	Ca	Pl % pr	La	Cr Om	Mg	Ba 1	i Y	B Al	Na %	K W Au**	* *
11+00E B21+00N 11+00E B20+50N 11+00E B20+00N 11+00E B19+50N 11+00E B19+00N	ррл 1 1 1 1	146 1020 54 52 70	75 195 33 40 64	240 664 111 168 295	5.1 5.9 .5 .6 1.4	75 86 51 53 63	15 33 16 18 33	2737 1319 586 566 777	3.75 7.03 3.53 4.35 5.88	44 214 22 36 52	7 8 5 5 5	ND ND ND ND ND	4 9 12 9 6	89 81 19 18 35	1.8 2.3 .2 .4 .7	2 6 2 2 2	2 2 2 2 2 2	17 24 18 21 26	7.90 .15 1.53 .13 .28 .08 .27 .07 .57 .08	0 2 1 3 7 3 1	25 37 32 27 19	25 28 35 34 38	.58 .68 .67 .60 .55	137 .0 109 .0 56 .0 71 .0 80 .0)1)2)2)2)2	5 1.65 4 2.62 2 1.18 3 1.39 2 1.90	.01 .01 .01 .01 .01	.07 2 13 .13 3 16 .06 1 6 .07 1 12 .06 1 12	3 6 6 2 2
11+00E B18+50N 11+00E B18+00N 12+00E B21+00N 12+00E B20+50N 12+00E B20+00N	1 1 1 1	47 31 59 49 31	46 28 47 33 47	158 127 224 142 113	.6 .7 1.2 1.8 .1	54 42 63 52 34	19 13 18 12 15	320 387 803 247 437	4.68 3.56 4.50 4.03 3.70	38 22 30 27 10	5 5 5 5 5	ND ND ND ND	8 6 7 10 13	15 19 31 14 10	.2 .2 .2 .2 .2	2 2 2 2 2 2 2	2 2 2 2 2 2 2	24 18 20 18 16	.20 .04 .30 .06 .52 .08 .22 .08 .07 .01	4 2 3 2 3 2 8 3	26 24 25 24 37	35 28 33 35 24	.55 .51 .57 .58 .49	78 .0 69 .0 94 .0 44 .0 64 .1)2)2)1)2)2	4 1.62 2 1.34 4 1.75 3 1.58 4 1.38	.01 .01 .01 .01 .01	.06 1 78 .08 1 8 .12 1 13 .04 1 6 .10 1 8	8 8 3 6 8
12+00E B19+00N 12+00E B18+50N 12+00E B18+00N 13+00E B20+00N 13+00E B19+50N	1 1 1 1	24 65 115 44 70	22 45 63 51 59	128 146 198 267 159	.5 .5 2.3 1.1 .5	34 67 96 39 68	12 22 32 16 22	403 678 921 810 642	3.35 4.65 6.53 4.89 5.36	20 34 69 39 48	5 5 5 5 5	ND ND ND ND	9 14 9 8 10	11 21 30 25 15	.2 .3 .2 1.4 .2	2 2 2 2 2	2 2 2 2 2	18 22 27 25 23	.11 .02 .30 .07 .48 .12 .33 .07 .19 .07	9	31 32 31 22 29	29 36 40 34 41	.46 .71 .96 .46 .66	66 .0 78 .0 68 .0 57 .0 71 .0)1)2)2)2)2	2 1.31 4 1.56 3 1.74 3 1.30 3 1.51	.01 .01 .01 .01 .01	.06 1 11 .14 1 9 .08 1 20 .05 1 5 .08 1 16	1 9 5 6
13+00E B18+50N 13+00E B18+00N 13+00E B17+50N 13+00N C18+00E 13+00N C18+50E	1 1 1 1	64 43 41 54 74	42 30 47 48 48	176 119 123 181 190	1.0 .3 .4 1.1 2.0	61 36 33 36 38	22 10 11 10 13	841 205 333 430 561	5.21 5.33 3.41 4.12 5.11	56 39 31 65 89	5 5 5 5 5	ND ND ND ND	4 5 4 3	23 15 14 6 10	.2 .2 .2 .2 .3	2 2 3 2	2 2 2 2 2 2	32 25 16 33 56	.35 .10 .18 .11 .22 .04 .05 .07 .15 .06	6 0 1 7 9	18 25 26 33 18	41 34 22 17 32	.66 .31 .29 .10 .59	106 .1 49 .1 46 .1 55 .1 68 .1)2)2)1)2)2)3	3 1.54 3 1.17 3 1.00 4 .57 4 1.13	.01 .01 .01 .01 .01	.07 1 11 .05 1 6 .06 1 12 .03 1 421 .03 1 16	1 6 2 1 6
13+00N C19+00E 13+00N C20+00E RE 13+00N C18+00E 13+00N C20+50E 13+00N C21+00E	1 1 1 1	317 101 54 84 44	70 65 46 49 30	260 223 193 236 108	8.1 .3 1.0 .7 2.3	85 36 38 81 28	25 10 11 21 7	1396 210 451 461 589	2.54 5.05 4.31 4.98 2.12	39 101 73 28 29	5 5 5 5 5	ND ND ND ND	3 8 3 10 3	125 8 6 18 38	2.6 .2 .2 .2 .2	2 2 2 2 2	2 2 2 2 2	8 21 34 19 15	2.79 .09 .06 .03 .05 .08 .24 .05 .71 .04	5 2 3 8 7	9 33 33 33 14	13 24 18 28 19	.56 .10 .11 .48 .14	87 . 27 . 56 . 61 . 102 .	01 01 02 02 01	6 .67 3 .60 4 .57 2 1.30 4 .68	.01 .01 .01 .01 .01	.02 1 7 .03 1 9 .03 1 44 .07 1 13 .02 1 5	7 9 7 3 5
12+00N C17+00E 12+00N C17+50E 12+00N C18+00E 12+00N C19+00E 12+00N C19+50E	1 1 1 1	47 43 52 138 77	49 48 176 119 42	166 183 261 268 155	.1 .1 1.1 1.3 .3	67 82 51 71 124	19 18 19 30 39	498 438 388 1138 844	4.57 4.82 6.08 6.43 4.77	39 47 65 69 53	5 5 5 5 5	ND ND ND ND	14 14 7 10 15	8 11 23 24 18	.2 .2 .4 .2 .2	2 2 2 2 2	2 2 2 2 2	16 19 17 17 15	.07 .03 .12 .04 .36 .06 .32 .07 .17 .07	3 4 1 4 1 7	45 42 28 27 32	45 50 33 35 41	.52 .66 .29 .46 .52	71 . 69 . 51 . 61 . 45 .	01 01 01 01 01	3 1.24 3 1.43 3 1.28 5 1.24 3 .93	.01 .01 .01 .01 .01	.06 1 8 .06 1 18 .02 1 19 .05 2 19 .03 1 1	8 5 15
12+00N C20+50E 12+00N C21+00E 11+00N C17+00E 11+00N C17+50E 11+00N C18+00E	2 1 1 1	100 56 33 78 53	134 65 55 740 66	365 186 170 627 175	.9 1.9 .1 1.0 .3	64 33 33 64 45	20 11 10 31 11	841 285 161 1306 197	5.24 5.74 4.76 7.91 5.25	103 73 50 269 41	5 5 5 5 5	ND ND ND ND ND	6 6 7 7 11	17 10 8 34 6	.3 .2 .2 .7 .2	2 2 2 2 2	3 2 2 16 2	17 26 32 19 14	.19 .05 .10 .15 .07 .03 .49 .09 .04 .02	7 6 3 2 9	27 29 34 22 41	32 32 38 34 50	.33 .33 .24 .37 .36	53 . 65 . 94 . 42 . 62 .	01 01 02 01 01	3 1.22 4 1.06 2 1.15 3 1.28 3 1.12	.01 .01 .01 .01 .01	.05 1 3 ⁻¹ .04 1 40 .02 1 4 .03 1 18 .03 1 18	11 10 4 18 18
11+00N C18+50E 11+00N C19+00E 11+00N C19+50E STANDARD C/AU-S	- 1 1 1 18	54 30 100 58	94 49 71 39	354 193 299 130	3.3 2.2 .8 6.9	61 25 45 67	23 9 19 29	737 678 631 1032	5.90 3.39 7.53 3.91	50 34 37 38	5 5 5 21	ND ND ND 7	6 8 7 38	43 13 13 53	.4 .2 .2 19.0	2 2 2 18	2 2 2 19	24 17 18 55	.58 .11 .16 .05 .09 .16 .47 .08	1 2 5 9	20 32 32 37	45 28 26 56	.18 .12 .22 .87	75 . 91 . 86 . 180 .	01 01 01 09	3 2.07 3 .83 3 1.08 33 1.89	.01 .01 .01 .07	.03 1 10 .04 1 4 .02 1 4 .15 10 44	6 4 4 9

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.


Rio Algom Exploration Inc. PROJECT 9124 FILE # 92-1858



	Ma	<u> </u>	Dh	70		Ni	<u></u>	Mo	Fo	Δc		Δ11	Th	Sr	Cd	Sb	Bi	v	Ca	P	La	Cr	Mg	Ba Ti	В	AL	Na	K W Au	**۱
SAMPLE#	0M IDCC	DU DOM	DOM	DDM	DDI	DDM	mqq	ppm	` %	Spm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	7	%	ppm	ppm	%	ppm %	ppm	%	%	% ppm p	opb
								···														77	45	01 01	. .	1 7/	01	05 1	25
11+00N C20+00E	14	104	379	293	4.8	67	14	352	8.36	99	6	ND	7	113	-8	2	2	23	.23	579	10	35	.15	71 .01	ے ح	1.74 64	.01	.05 1	32
11+00N C20+50E	2	120	67	251	-2	46	15	259	5.55	121	5	ND	8	21	• 4	2	2	19	.30 ÷	120	26	20	.11	72 01	2	1.76	.01	.04 1	15
11+00N C21+00E	2	82	92	5/8		90	51	510	1.20	04	7	NU	∡	14 () 7/ ()	- 4	2	5	21	.10	076	20	37	46	58 02	2	1.47	.01	.05 1	15
10+00N C17+50E	1	158	102	412	1.4	04 41	27	1202	2.90 / 70	47	5		6	22	1	2	5	32	30 0	053	22	60	.68	80 .02	2	1.56	.01	.05 1	6
10+00N C18+00E	1	22	42	220	1.3	01	17	955	4.30		,	лD	0			-	-					••							1
10+00N_C18+50E	1	87	60	188	.4	58	19	417	6.36	50	5	ND	9	9	.2	2	2	22	.06 .	041	29	39	.31	60 .01	2	1.27	.01	.03 1	6
10+00N C19+50E	7	33	165	369	.2	34	11	249	7.57	57	6	ND	24	17	.2	2	2	2	.15 🔮	120	26	5	.03	33 .01	2	.54	.01	.01 1	18
10+00N C20+00E	2	55	45	137	.1	31	7	114	3.68	42	5	ND	8	6	.2	2	2	19	.03	062	38	24	.07	62 .01	2	. 19	.01	.02 1	11
10+00N C20+50E	2	61	82	218	. 6	34	9	201	5.23	50	5	ND	9	8	-2	2	2	19	.06	091	30	36	.24	88 .01	2	1.14	.01	.03	0
10+00N C21+00E	1	27	31	131	.5	27	10	349	3.29	15	6	ND	8	26	-2	2	2	19	.29	U34	21	20	. 13	10. CO	2	1.20	.01	.03	0
40.000 074.505		07	70	201	1 0	17	11	17/	د م 🖇	42	5	ND	12	~ ~ ~	2	2	2	23	.02	033	37	36	.24	94 .01	2	1.38	.01	.03 1	22
10+00N C21+50E	1	122	20 77	201	1.0	43	18	278	4.92	72	5	ND	14	7	-5	3	2	19	.04	058	32	41	.39	81 .01	2	1.63	.01	.03 1	4
10+00N C22+00E	1	32	15	150	• •	20	10	196	4.91	25	5	ND	16	6	.2	2	2	18	.03	042	51	34	.26	45 .01	2	1.15	.01	.03 1	68
9+00N C17+JUE	1	84	67	351	1.8	113	33	1672	7.65	64	5	ND	9	25	.2	2	2	22	.28	070	25	48	.49	81 .02	2	1.83	.01	.06 1	6
9+00N C18+50E	1	29	22	89	.4	28	7	136	3.92	26	5	ND	10	7	.4	3	2	17	.08 .	046	43	31	.14	44 .01	2	.82	.01	.03 1	3
,																	-		. 8			· -	70		-	4 70	01	07 1	E
9+00N C19+00E	1	44	30	163	.6	100	22	339	5.99	44	5	ND	10	15	.2	2	2	15	.14	043	55	45	.30	46 -01	2	1.39	.01	.03 1	20
9+00N C19+50E	2	24	26	103	•1	27	9	486	3.13	24	6	ND	10	2	•2	2	2	20	.01 .	020	43	22	.14	59 .01 62 01	2 7	1.05	.01	.05 I	7
9+00N C20+00E	1	21	19	116	.9	30	10	607	5.82	25	2	ND	10	6	• 2	2	2	10	.04 .	025	37	16	27	97 02	2	1.43	.01	.05 1	7
10+00E E30+00N	1	26	11	42	1.4	24	7	1/7	2.83 / 13	4	2	NU	9	4	• 5	2	2	20	.00	083	19	19	.28	55 .01	2	1.53	.01	.03 1	2
UTUUE EZYTUUN		10		02	••	17	,	147	4. IJ 🔡		U	ND	,			-	-	2.0											
10+00E E28+50N	1	15	10	81	.1	22	10	265	3.24	3	5	ND	8	7	.2	2	2	18	.07 🖡	035	31	21	.50	87 .01	2	1.57	.01	.05 1	1
RE 9+00N C19+50E	1	25	23	105	.6	26	9	493	3.15	20	5	ND	12	5	.4	2	2	21	.01	036	44	35	.14	60 .01	2	1.05	.01	.02 1	15
10+00E E28+00N	1	22	26	80	.5	21	26	945	4.10	11	5	ND	4	17	.2	2	2	27	.23	860	29	23	.41	121 .01	5	1.60	.01	.08 1	5
10+00E E27+50N	1	7	8	52	.1	12	5	119	2.32	4	5	ND	8	6	•2	2	2	14	.07	018	51	13	.21	20 .01	2	. 90	.01	.03 1	ĩ
10+00E E27+00N	1	8	10	53	.5	10	5	118	5.76	4	2	ND	10	د	•-4	2	2	24	.02 .	054	21	19	. 50	+J +01	-	1.05			•
10+00E E26+50N	1	10	18	95	3	15	7	133	4.01	7	5	ND	9	5	.2	2	2	28	.04	039	32	20	.43	59 .02	2	1.74	.01	.02 1	1
10+00E E26+00N	1	18	22	87	.2	20	8	178	4.92	9	5	ND	9	6	.2	2	2	17	.07	056	26	25	.48	52 .01	2	1.82	.01	.04 1	1
10+00E E25+50N	1	38	37	264	.8	32	17	650	4.35	9	5	ND	5	14	.2	2	2	27	.22	052	37	25	.59	122 .02	2	1.83	.01	.03 1	5
10+00E E25+00N	1	24	37	125	1.1	25	15	490	4.45	67	6	ND	6	20	.2	2	2	19	.20	079	32	23	.55	78 .01	5	1.60	.01	.04 1	5
12+00E E29+50N	1	28	12	123	1.1	26	17	474	4.79	13	5	ND	3	27	-2	2	2	34	.33	059	24	18	. 14	170 .01	۲	1.04	.01	.02 1	,
12.005 530.000		40	77	100	c	47	70	1.61	7 07	17	5	ND	1/	11	•	2	2	38	08	100	34	28	.38	176 .02	2	2.53	.01	.06 1	3
12+005 529+504		00 70	23	1/5	- 7	0/ 77	20	404	5 17	12	2	ם א	11	0		2	2	28	.08	047	34	22	.48	98 .03	2	1.86	.01	.04 1	2
12+00E E20+30N	1	40	30	145	۰. ۶	34	18	1253	3.84	10	5	ND	11	18	.8	2	2	21	.21	052	37	24	.46	137 .02	2	1.84	.01	.04 1	4
12+00E E27+50N	1	11	14	60		11	5	212	4.52	5	5	ND	11	5	.6	2	2	17	.03	030	25	17	.24	36 .01	2	1.27	.01	.03 1	1
12+00E E27+00N	i	15	25	75	.3	15	9	286	7.29	9	5	ND	12	5	.2	2	2	31	.04 .	109	21	27	.32	36 .02	2	2.18	.01	.02 1	1
								·			_			_	_	-	-		⁰	0F.F	~/	77		40 04	7	2 00	01	02 4	1
12+00E E26+50N	• 1	22	27	171	.6	33	14	226	6.27	18	5	ND	12	5	.Z	2	2	18	.03	025	24	دد ۲.۲	.//	10 UO ۸۸ ח۱	2	2.90	.01	.02 1	4
12+00E E26+00N		46	19	95	.7	50	16	198	5./6	21	5	ND 7	15	57	14 7	د 13	10	20 54	.02	007	31	40 56	. 7.) 80	177 00	34	1.88	.07	.15 10	48
STANDARD C/AU-S	18	20	51	154	0.0	00	<u> </u>	1022	4.01 8	41	19				10.7		17	0	. 47 🧃	• 7 J	51		,						

ACM 💔	A	L :	R	AT	S	I		E Jack	2 E		STI		ST.		COL	E	3.1	Ve	5A _	- Kari		ION	F ,	1)2	•	158		x (^		53	
4 4				Ri	0 A.	lgoi	<u>m E</u> :	<u>xp1</u>	G <u>ora</u>	EOCI tion P.0.	HEMI n II Box	CA1	L A PR(, 165	NAL <u> OJE</u> 0 - 6	YSI <u>CT</u> 0, Va	5 CH 9124 ncouv	E RT : L] er BC	File V7Y	CAT ⊇ # 165	E 92-	-19()4	Pa	age	1					4 4	Ê
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	B ppm	Al %	Na %	K %	W A	lu** ppb
SO-M300 SO-M301 SO-M302 SO-M303 SO-M304	1 1 1 1	23 41 20 23 17	25 13 10 11 16	87 80 67 98 89	.1 .3 .2 .1 .1	33 30 19 24 19	10 13 8 10 9	312 181 206 310 374	3.73 4.92 3.61 4.33 4.50	2 4 2 2 2	5 5 5 5 5	ND ND ND ND ND	5 13 8 8 5	6 4 4 4 4	.2 .2 .2 .2 .2	2 2 2 2 2 2	2 2 2 2 2	17 17 16 16 18	.06 .03 .03 .03 .02	.037 .058 .052 .072 .105	18 27 24 23 22	25 18 16 19 18	.40 .35 .24 .30 .25	65 20 38 41 37	.02 .01 .01 .01 .02	5 7 6 4	1.39 1.07 1.28 1.25 1.05	.01 .01 .01 .01 .01	.02 .05 .02 .02 .01	1 1 1 1	5 1 2 5 7
SO-M305 RE SO-M310 SO-M306 SO-M307 SO-M308	1 1 1 1	18 26 22 18 59	14 17 25 36 66	107 130 163 331 198	.1 .2 .1 .1 .1	23 36 58 83 164	8 13 13 21 30	214 257 279 920 411	5.01 5.20 4.37 7.13 8.35	2 7 35 31 31	5 5 5 5	ND ND ND ND ND	6 11 4 1 8	5 7 9 15 10	.2 .2 .2 .2 .2	2 2 2 2 2	2 2 2 2 2 2	19 21 38 37 34	.03 .08 .11 .18 .10	.088 .169 .058 .197 .203	23 26 23 20 22	27 26 91 70 82	.39 .37 .71 .41 .55	55 50 97 144 455	.02 .01 .03 .03 .02	5 7 5 5 4	1.42 1.32 1.62 1.80 1.60	.01 .01 .01 .01 .01	.01 .04 .05 .01 .05	1	4 5 3 1 5
SO-M309 SO-M310 SO-M311 SO-M312 SO-M313	1 1 1 1	32 30 21 11 15	18 16 13 12 12	109 132 125 56 74	.1 .1 .8 .3 .2	38 37 28 11 16	14 14 13 6	306 284 468 587 257	4.92 5.28 3.65 2.76 3.15	3 6 4 2 2	5 5 5 5 5	ND ND ND ND	10 10 10 6 8	7 7 4 4	.2 .2 .2 .2	2 2 2 2 2	2 2 2 2 2 2	17 23 15 15 17	.08 .09 .03 .03 .02	.136 .176 .090 .148 .072	28 28 25 26 27	28 29 23 15 18	.48 .39 .34 .18 .21	53 <u>,</u> 57 54 40 54	.01 .01 .02 .02 .01	5 5 4 4	1.66 1.49 1.71 1.00 1.38	.01 .01 .01 .01 .01	.01 .01 .03 .01 .04	1 1 1 1	12 6 5 2 2
SO-M314 SO-M315 SO-M316 SO-M317 SO-M600	1 1 1 2	19 25 25 8 31	11 11 12 9 14	63 68 71 38 95	.1 .1 .2 .1 .1	17 21 60 12 23	6 8 10 4 9	166 264 181 116 172	4.40 4.33 4.04 1.46 5.04	2 2 7 2 2	5 5 5 5 5	ND ND ND ND	7 8 9 3 8	3 4 9 4	.2 .2 .2 .2 .2	2 2 2 2 2	2 2 3 2	30 17 22 13 16	.02 .02 .02 .10 .02	.094 .044 .029 .030 .080	25 26 22 22 24	17 18 48 11 20	.21 .31 .37 .16 .33	23 28 30 30 30	.02 .01 .01 .01 .01	4 4 2 4	1.07 1.18 1.23 .58 1.54	.01 .01 .01 .01 .01	.02 .03 .05 .02 .01	1 1 1 1 1 1	3 1 1 1 4
SO-M602 SO-M603 SO-M604 SO-M605 SO-M606	1 1 1 1	35 35 37 56 77	14 19 21 23 33	93 89 106 116 209	.1 .2 .1 .7 .9	30 26 29 27 31	12 12 13 14 10	268 303 475 604 312	4.85 6.71 5.07 4.11 3.39	2 3 2 11 16	5 5 5 5	ND ND ND ND	11 13 11 8 8	5 6 14 22	.2 .2 .2 .3 .8	2 2 3 2	2 2 2 2 2	14 26 15 15 22	.04 .06 .05 .22 .28	.083 .131 .082 .061 .036	24 25 26 21 22	20 22 22 18 25	.40 .31 .34 .35 .34	39 46 46 86 152	.01 .02 .01 .01 .01	5 5 4 5	1.35 1.14 1.62 1.05 1.39	.01 .01 .01 .01 .01	.02 .04 .01 .06 .08	1 1 1 1	8 3 1 4 4
SO-M607 SO-M608 SO-M609 SO-M610 SO-M611	1 1 1 1	56 64 46 22 54	24 37 126 29 50	170 143 158 121 615	.4 .1 .4 .3 1.2	38 60 45 31 44	11 15 15 11 19	249 535 464 336 663	3.41 3.96 4.90 3.50 4.24	6 7 45 7 36	5 5 5 5	ND ND ND ND	8 9 9 8 6	19 11 15 12 25	.3 1.1 .3 .2 .8	2 2 2 3	2 2 2 2 2	21 20 23 17 19	.22 .11 .16 .12 .34	.030 .027 .048 .044 .064	22 47 25 27 23	34 38 38 35 34	.58 .65 .51 .57 .49	80 101 117 74 78	.02 .02 .02 .01 .01	3 4 4 3 5	1.51 1.77 2.15 1.51 1.98	.01 .01 .01 .01 .01	.08 .05 .07 .05 .05	1 1 1 1	6 1 2 8 7
S0-M612 S0-M613 S0-M614 S0-M615 S0-M616	1 1 1 1	8 58 34 71 36	12 21 32 18 19	52 115 101 101 129	.2 .2 .4 .1 .1	11 41 35 74 32	6 15 10 22 15	285 315 211 1085 775	2.36 5.02 3.95 3.73 7.52	3 8 18 8 5	5 5 5 5	ND ND ND ND	8 15 11 6 6	5 7 8 29 13	.2 .2 .2 .6 .2	3 2 2 2 2	4 2 2 2 2	14 12 12 20 17	.04 .09 .07 .46 .18	.056 .076 .032 .059 .093	26 27 38 25 29	11 19 27 29 27	.19 .44 .56 .60 .56	29 34 40 68 32	.01 .01 .01 .02 .01	2 3 4 4 4	.76 1.15 1.43 1.48 1.80	.01 .01 .01 .01 .01	.03 .04 .05 .06 .01	1 1 1 1	5 3 5 2 7
SO-M617 SO-M618 STANDARD C/AU-S	1 1 17	8 27 57	6 13 39	60 106 130	.1 .1 7.4	16 31 72	6 15 30	183 301 1023	4.59 5.43 3.92	15 4 38	5 5 19	ND ND 7	9 9 36	4 23 52	.2 .2 17.8	2 2 13	2 2 19	18 16 56	.03 .25 .47	.066 .077 .089	33 58 36	23 28 56	.50 .65 .87	35 45 175	.01 .01 .09	3 4 34	1.52 1.96 1.86	.01 .01 .08	.04 .04 .14	1 1 11	1 4 48
		ICP	50	0 GRA	M SAM	PLE I	S DIG	ESTEI	WITH	3ML	3-1-2	HCL-	HN03-	H20 A	T 95 I	DEG. (C FOR	ONE	HOUR	AND I	S DIL	UTED	то 10	ML W	ITH W	ATER.					

THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND ALO AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: SOIL AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE. <u>Samples beginning 'RE' are duplicate samples.</u>

Inly 21/92

DATE RECEIVED: JUL 14 1992 DATE REPORT MAILED:



Rio Algom Exploration Inc. PROJECT 9124 FILE # 92-1904

Page 2

	T									Addugar N							_		1949-1949 1949-1949					janage					
SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	SP	Bi	v	Ca P	La	Cr	Mg	Ba	Ti	B Al	Na	ĸ	W Au*	r¥
	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	% %	ppm	ppm	%	ppm	%	ppm %	%	% pp	x pp	b,							
	1				관련																								
SO-M619	2	20	6	33	.1	36	9	137	2.89	2	5	ND	8	8	.2	2	2	18	.06 .029	32	24	.32	31	.01	5.92	.01	.02	1	6
SO-M620	1	8	28	118	.9	16	6	153	3.09	- 44	5	ND	15	9	.2	2	2	15	.11 .155	32	17	.40	45	.01	4 1.14	.01	.08	1	2
SO-M621	1	7	14	44	.9	9	3	70	3.27	14	7	ND	12	3	.2	4	2	20	.02 .084	30	10	.20	34	.01	4.99	.01	.07	2	2
SO-M622	1	2	7	22	.3	1	1	23	.27	2	5	ND	6	8	.2	2	2	3	.05 .016	30	3	.04	36	.01	2.69	.01	.04	2	1
SO-M623	1	9	10	30	.5	10	3	111	1.56	5	5	ND	9	6	.2	2	2	19	.05 .025	23	19	.26	46	.01	4 1.10	.01	.04	1	4
SO-M624	1	30	35	101	1.2	21	9	206	6.20	14	5	ND	11	5	.7	2	2	31	.03 .102	21	27	.44	45	.01	6 2.02	.01	.05	1	6
SO-M625	1	16	25	115	.9	17	6	168	6.86	2	5	ND	11	3	.2	2	2	22	.01 .089	24	31	.56	41	.01	5 2.32	.01	.05	1	4
SO-M626	1	10	26	81	.3	12	5	314	3.63	2	5	ND	8	4	.2	2	2	19	.04 .052	22	24	.43	51	.01	3 1.74	.01	.04	1	6
SO-M627	1	35	36	103	7	34	11	246	4.07	ō	5	ND	ō	10	2	2	Ā	26	17 060	38	26	55	108	01	3 2 30	01	07	ŝ	1
RF 50-M631	1	- 9	24	45	5	°,	Ĺ.	263	3 54	10	5	ND	Ŕ	i č		2	2	26	03 110	24	16	28	36	01	3 1 23	01	.0. A0	4	2
	· ·		- ·				-	205	5.54		-	NO	0	-	•	-	-	20	.05 .110	64	.0	.20	50		5 1.25				
SO-M628	1	6	19	41	1.7	9	4	93	2.51	2	35	ND	13	3	.2	3	3	21	.02 .031	27	14	.32	33	.01	4 1.32	.01	.11	2	1
SO-M629	1	8	15	53	1	11	5	151	2.73	5	5	ND	6	4	2	2	2	28	.03 .040	25	17	.37	42	-01	3 1.36	.01	.03	1	1
SO-M630	1	14	35	60	.4	13	5	163	3.32	9	5	ND	10	5	2	2	2	20	05 045	25	19	.44	61	01	4 1.76	.01	08	1	1
SO-M631	1	5	24	45	7	7	3	254	3.43	10	6	ND	9	3	2	2	2	26	02 107	23	15	.27	32	01	3 1 18	.01	07	1	1
SO-M632	1	25	24	83	4	26	ō	223	4.67	Š	5	ND	10	7	5	2	2	18	11 061	26	27	72	48	01	4 2 05	.01	06	1	Å
			-								-			•		-	-		••••••	20			40		4 2105				•
SO-M633	1	11	17	71	.1	19	7	147	6.41	2	5	ND	8	3	.2	2	2	21	.02 .046	20	27	.53	41	.01	2 2.09	.01	.03	1	4
SO-M634	1	17	14	72	.2	16	7	218	4.84	12	5	ND	6	5	.2	2	2	37	.05 .036	19	19	.28	57	.03	6 1.13	.01	.04	1	2
SO-M635	1	17	12	52	.5	15	6	134	2.64	16	5	ND	5	4	.2	3	2	40	.03 .044	22	13	.11	32	.03	5 .62	.01	.06	1	6
SO-M636	1	22	29	71	2.4	18	9	640	3.51	32	5	ND	2	6	2	2	2	42	02 054	16	22	06	33	03	4 63	.01	.06	1	2
SO-M637	1	59	30	106	.9	66	22	614	4.74	12	5	ND	12	32	2	3	2	41	.47 .072	29	86	1.05	92	05	6 1.60	.01	17	1	2
										17	-					-	-	••		- /			/ -		•				-
SO-M638	1	63	34	110	.4	105	34	781	5.33	4	5	ND	13	85	.2	2	2	67	1.31 .092	29	131	1.56	138	.10	4 2.06	.01	.30	1	4
12+00N C18+50E	1	29	24	141	.2	29	9	162	4.23	23	5	ND	9	9	2	2	2	22	.09 .021	32	33	.27	76	01	6 1.07	.01	.04	1	2
STANDARD C/AU-S	17	58	39	133	6.9	70	32	1074	3.99	38	19	7	37	54	19.0	13	19	59	.48 .090	39	58	-88	177	-09	35 1.93	.08	.17 1	0 4	÷6
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ACMLP	-	<i>1</i> T	r	_ RAI	Υ	_ S L	! •			E. GEC	S ОСНІ	TII.	s CAL	T. ANZ). Alys	50 518	. в. CEI	C. RTIF	J6A ICA	.TE			ONE		.)25	1	58	.k	(*	_ 53	Ξ λ λ	•
<u> </u>					1	Rio	Alc P.C	10m D. Box	Exp 1033	5, 16	at :	<u>ion</u> 60, V	Inc ancou	3.] Jver	PROJ	JEC: (165	<u>[' 91</u> Sub	<u>L24</u> mitte	Fi d by:	le WILI	# 9 .1am (92-1 DONALC	L993 Ison	3						4		
SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	В ррт	Al %	Na %	К %	V / ppm	Au** ppb	
SO-M-601	1	51	24	102	,1	38	15	300 5	5.06	8	5	ND	10	8	.2	2	2	18	.11	.107	27	17	.37	90	.01	2	1.00	.01	.04	1	4	

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER. THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM. - SAMPLE TYPE: SOIL AU** ANALYSIS BY FA/ICP FROM 10 GM SAMPLE.



Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 Fo: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5 Page per :1-A Total F_{2,2}-3s :1 Certificate Date: 16-JUL-92 Invoice No. :19217390 P.O. Number : Account :GZ

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Project : 9124 Comments: CC: WILLIAM DONALDSON

CERTIFICATE OF ANALYSIS

A9217390

	_				31 4	Ba ====	Be		Co. %	Cd	Co	Cm	C 11 TTTT	Po 4	7 4	No %
SAMPLE	P C	kep Ode	ац ррб Ганал	Ag ppm AAS	AL % (ICP)	Bappm (ICP)	Be ppm (ICP)	BI DDW (ICB)	Ca % (ICP)	(ICP)	(ICP)	(ICP)	(ICP)	re % (ICP)	к % (ICP)	ng % (ICP)
15162 15163 15164 15165 15166	205 205 205 205 205	274 274 274 274 274 274	15 < 5 < 5 80 < 5	2.4 0.4 < 0.2 < 0.2 0.2	8.62 5.75 11.30 6.81 7.02	3610 1730 1990 1210 1180	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5	4 4 8 2 2 2	0.04 0.18 0.58 7.19 0.41	< 0.5 1.0 < 0.5 0.5 < 0.5	2 8 17 26 4	155 131 121 88 129	139 27 34 28 2	4.87 1.47 3.78 5.82 1.31	3.51 2.10 4.25 1.73 1.94	0.76 0.76 0.96 2.69 0.28
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											CER		v: Yh	-ar f	t'rna	<u> </u>



Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 To: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5 Page er :1-B Total کریے :1 Certificate Date: 16-JUL-92 Invoice No. :19217390 P.O. Number : Account :GZ

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Project : 9124 Comments: CC: WILLIAM DONALDSON

CERTIFICATE OF ANALYSIS

A9217390

SAMPLE	P: Ci	rep Ode	Mn ppm (ICP)	Mo ppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)			
15162 15163 15164 15165 15166	205 205 205 205 205	274 274 274 274 274	35 55 165 1400 545	17 54 < 1 < 1 3	0.61 0.57 0.39 1.40 2.25	5 44 39 31 9	360 330 650 1560 840	34 14 12 4 32	98 81 133 247 103	0.30 0.21 0.46 0.73 0.08	835 481 95 198 8	< 10 < 10 < 10 < 10 < 10 < 10	64 104 96 94 38			
					:											ĺ
											CER	TIFICATIO	v: Yh	a E	Tha	~

SAMPLE#	Mo	o Cu n ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Со ррт	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm (Bi opm	V ppm	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti %	В ррп	Al %	Na %	к %	W ppm	Au*
A 13+00E PB 22 A 13+00E RS 22 B 11+00E PB 20 B 11+00E RS 20 C 11+00E RS 20	2+00N 2 2+00N 2 0+50N 2 0+50N 2	2 284 1 237 1 386 1 1140	1210 1566 139 231	1765 1999 432 790	11.2 19.6 1.3 4.6	148 116 53 94	50 49 21 44	5334 6208 614 1942 775	11.03 16.01 5.44 9.34	82 73 109 211 75	5 5 5 5 5	ND ND ND ND	7 1 13 8	30 35 17 41	6.5 7.2 1.1 2.5 7	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9 11 5 3	27 36 21 27 13	1.03 1.32 .25 .78 20	.121 .286 .058 .113	17 14 35 32 42	23 29 32 34 40	.62 .64 .85 .90	221 281 68 99 46	.01 .01 .02 .02	2 2 2 2 3	1.54 1.93 1.93 3.05 1 03	.01 .01 .01 .01	.06 .05 .11 .13		3 1 1 1 2
C 11+00N PB 17 C 11+00N RS 17 C 11+00N PB 20 C 11+00N RS 20 12+00N D 23+50 12+00N D 24+00	7+50E 0+00E 19 0+00E 20 0E 20 0E 20	1 70 9 145 0 129 1 30 1 23	153 418 619 53 28	397 296 343 106 79	.5 2.1 4.9 .6	84 76 82 28 26	27 12 19 16 15	766 201 392 374 543	5.52 6.19 9.86 4.84 2.72	123 112 148 13 7	5 5 5 7 5	ND ND ND ND ND	10 6 8 10 6	17 113 163 20 16	.7 1.4 2.1 .2 .2	2 4 2 2 2	3 2 2 2 2 2	15 24 29 17 17	.25 .17 .30 .19 .17	.050 .313 .556 .045 .027	38 21 18 23 23	42 18 35 21 19	.50 .18 .23 .32 .29	36 128 144 61 64	.01 .01 .01 .01 .01	4 3 2 5 2	1.08 .79 1.84 1.35 1.23	.01 .01 .01 .01 .01	.04 .07 .07 .06 .06	1 1 1 1	2
12+00N D 24+50 12+00N D 25+00 12+00N D 25+50 12+00N D 25+50 12+00N D 26+50 12+00N D 26+50	DE DE DE DE	1 51 1 41 1 65 1 34 1 34	52 47 92 35 28	170 112 121 125 90	1.3 .9 1.6 .2 .3	60 38 55 35 34	26 23 17 16 17	1081 845 238 798 475	5.89 4.72 3.97 4.13 3.72	7 6 5 8 7	6 5 5 5 5	ND ND ND ND	10 4 13 7 7	42 37 27 33 25	.7 .5 .3 .5 .6	2 2 2 2 2	2 3 2 2 2	22 17 18 18 19	.52 .49 .34 .47 .31	.075 .082 .059 .051 .037	31 31 58 31 26	30 22 31 26 22	.49 .41 .48 .48 .37	108 69 97 90 63	.02 .02 .01 .02 .02	5 2 5 2 4	2.23 1.58 2.23 1.65 1.23	.01 .01 .01 .01 .01	.14 .08 .11 .08 .07	1 1 1 1	
12+00N D 27+00 12+00N D 27+50 12+00N D 28+00 12+00N D 28+50 12+00N D 29+00	DE D	1 28 1 23 1 41 1 44 1 23	21 21 22 31 21	90 86 113 106 100	.4 .1 .7 .3 .2	32 30 44 37 38	14 17 17 29 14	737 446 871 631 398	3.21 3.10 3.97 4.47 4.09	6 5 3 14 3	5 5 6 5	ND ND ND ND ND	3 6 5 15 7	30 15 30 10 13	.5 .3 .7 .2 .6	2 2 2 2 2	2 2 2 2 2 2	19 22 22 10 23	.39 .13 .32 .10 .12	.045 .031 .056 .046 .031	25 29 27 30 27	23 30 32 24 35	.41 .54 .58 .78 .67	90 103 125 42 90	.02 .02 .02 .01 .01	4 2 4 2 2	1.30 1.51 1.78 1.87 1.80	.01 .01 .01 .01 .01	.08 .10 .11 .05 .09	1 1 1 1 1	
12+00N D 30+00 12+00N D 30+50 12+00N D 31+00 12+00N D 31+50 12+00N D 32+00	DE D	1 25 1 12 1 23 1 24 1 12	19 14 29 25 13	103 63 95 82 88	.5 .1 .3 .5 .2	27 14 29 26 24	14 9 12 13 13	356 171 257 245 266	4.64 4.30 4.67 4.53 3.87	13 6 3 9 2	5 5 5 5 5	ND ND ND ND	8 11 10 10 11	26 6 7 7	.6 .2 .2 .2 .4	2 2 2 2 2	2 2 6 2 2	16 24 16 17 16	.27 .03 .05 .07 .05	.047 .052 .058 .025 .037	26 35 28 25 27	28 20 28 23 27	.61 .40 .49 .45 .53	83 36 54 48 69	.01 .01 .01 .01 .01	2 4 3 3 3	1.59 1.38 1.60 1.46 1.85	.01 .01 .01 .01 .01	.07 .04 .05 .04 .05	1 1 2 1 1	
11+00N D 23+50 11+00N D 24+00 11+00N D 24+50 11+00N D 25+00 11+00N D 25+50	0E	1 30 1 14 1 36 1 16 1 29	33 12 33 22 37	114 55 101 67 93	.1 .1 .7 .2 .4	31 11 31 17 30	15 7 19 10 15	1248 445 991 365 907	3.66 2.32 3.84 2.43 3.40	3 5 4 2 6	5 5 5 5 5	ND ND ND ND ND	8 4 5 5 4	18 10 47 19 31	.4 .2 .4 .2 .2	2 2 2 2 2 2	4 2 2 4 2	12 14 18 17 14	.19 .14 .49 .24 .45	.046 .044 .080 .030 .048	26 25 43 25 24	18 11 22 14 18	.38 .18 .30 .21 .35	73 23 109 54 65	.01 .02 .02 .01 .02	2 7 2 2 4	1.35 .57 1.71 .87 1.19	.01 .01 .01 .01 .01	.08 .05 .08 .05 .07	11111	1
11+00N D 26+00 11+00N D 26+50 11+00N D 27+00 RE 11+00N D 27 11+00N D 27+50	0E 0E 0E 5+00E 0E	1 28 1 24 1 31 1 17 1 9	48 30 19 24 9	98 89 98 69 35	.2 .1 .1 .1 .1 .2	28 30 26 18 8	19 14 15 12 5	773 342 295 352 99	3.75 3.95 4.78 2.59 1.53	4 7 16 5 10	5 5 5 5 5	ND ND ND ND	4 4 13 5 10	21 17 13 19 10	.4 .3 .2 .2 .2	2 2 2 2 2	2 2 5 2 7	18 20 14 17 14	.26 .17 .15 .24 .13	.042 .039 .039 .030 .030	28 24 41 25 39	20 23 19 15 8	.36 .34 .51 .23 .15	60 58 45 54 25	.02 .02 .01 .01 .01	3 2 2 4 4	1.20 1.28 1.30 .92 .55	.01 .01 .01 .01 .01	.07 .07 .05 .05 .04	1 1 1 1	3
11+00N D 28+00 11+00N D 28+50 STANDARD C/AU	0E 0E - S 1	1 17 1 8 9 58	19 13 39	77 51 133	.4 .1 7.3	20 11 70	12 6 32	490 191 1066	2.42 1.88 3.96	2 8 38	5 5 18	ND ND 7	4 9 39	26 8 52	.3 .2 19.4	2 2 15	2 2 19	17 13 58	.32 .08 .50	.038 .019 .088	21 34 39	17 11 61	.33 .25 .94	82 30 182	.01 .01 .08	3 3 34	1.03 .67 1.93	.01 .01 .06	.06 .06 .14	1 1 11	4



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SAMPLE#	Мо ррп	Cu	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm p	U Spm	Au ppm	Th ppm	Sr ppm	Cd ppm (Sb opm p	Bi xpm p	V mqc	Ca %	P %	La ppm	Cr ppm	Mg %	Ba ppm	Ti % p	B Spm	Al %	Na %	К %	W ppm	Au** ppb	
11+00N D 29+00E RE 11+00N D 32+00E 11+00N D 29+50E 11+00N D 30+50E 11+00N D 31+00E	1 1 1 1	25 21 29 20 23	21 27 29 14 14	88 78 103 78 109	.3 .4 .7 .6 .8	26 18 31 23 32	14 14 18 11 14	482 340 344 362 567	3.10 3.66 5.40 4.00 3.94	10 10 15 8 3	5 5 5 5 5	ND ND ND ND ND	16 11 11 11 8	15 6 5 8 14	.2 .2 .2 .2 .2	2 2 2 2 2	2 2 2 2 2 2 2	16 13 20 20 24	.14 .06 .04 .07 .12	.052 .030 .055 .049 .038	30 26 25 33 27	24 20 27 25 37	.49 .34 .49 .52 .70	56 39 48 55 100	.01 .01 .02 .01 .01	3 2 3 2 2	1.20 1.48 1.76 1.37 1.89	.01 .01 .01 .01 .01	.06 .04 .06 .07 .10	1 1 1 1 1 1	3 1 1 1	
11+00N D 31+50E 11+00N D 32+00E 11+00N D 32+50E 10+00N D 23+50E 10+00N D 24+00E	1 1 1 1	30 23 10 7 5	43 19 12 2 7	94 80 50 23 26	.3 .3 .5 .2 .1	27 20 11 8 5	13 15 7 4 3	303 330 140 206 231	5.56 3.72 3.21 .70 .69	10 10 4 8 3	6 5 5 5 5	ND ND ND ND ND	10 10 9 8 5	12 6 7 7 11	.2 .2 .2 .6 .2	2 2 2 2 2	2 2 2 2 2 2	21 14 24 6 9	.15 .06 .05 .09 .13	.031 .030 .020 .017 .014	22 28 31 33 24	31 21 19 4 4	.43 .34 .28 .05 .06	62 36 34 23 22	.01 .01 .01 .01 .01	2 2 2 2 2 2 2	1.89 1.48 1.12 .48 .26	.01 .01 .01 .01 .01	.06 .04 .04 .03 .03	1 1 1 1 1	7 1 3 1 1	
10+00N D 24+50E 10+00N D 25+00E 10+00N D 25+50E 10+00N D 26+50E 10+00N D 27+00E	1 1 1 1 1	24 20 33 42 36	12 22 35 27 30	53 97 93 93 84	.1 .3 .1 .1 .1	14 23 29 36 35	10 13 21 21 18	241 742 733 938 778	2.17 2.89 3.84 3.75 3.53	7 4 12 14 9	5 5 5 5 5	ND ND ND ND ND	7 7 9 8 10	9 28 16 17 12	.2 .2 .2 .2 .2	2 2 2 2 2	2 2 2 2 2 2	14 12 14 11 11	.10 .41 .22 .22 .14	.027 .042 .045 .043 .032	28 25 30 29 28	8 18 20 18 18	. 13 . 41 . 47 . 45 . 45	18 59 46 47 44	.02 .01 .02 .01 .01	2 3 2 2 2	.34 1.27 1.17 1.13 1.12	.01 .01 .01 .01 .01	.02 .05 .06 .07 .05	1111	1 1 3 1 5	
10+00N D 27+50E 10+00N D 28+00E 10+00N D 28+50E 10+00N D 29+00E 10+00N D 29+50E	1 1 1 1	17 25 22 12 30	16 17 20 17 33	64 76 96 77 93	.8 .1 .5 .2 .1	18 21 30 20 30	9 11 13 12 20	425 229 328 361 899	3.52 4.18 3.46 3.67 3.58	6 10 9 5 11	5 5 5 5 5	ND ND ND ND ND	6 8 10 7 10	6 6 8 7 10	.2 .3 .2 .2 .2	2 2 2 2 2	2 4 2 2 2	22 19 19 22 15	.05 .06 .09 .05 .11	.051 .038 .028 .030 .033	26 29 26 27 29	23 21 28 28 23	.35 .35 .47 .45 .50	35 28 57 68 60	.01 .01 .01 .01 .01	2 2 2 2 2 2	1.14 1.16 1.56 1.37 1.31	.01 .01 .01 .01 .01	.06 .05 .08 .07 .07	11111	1 1 1 3 1	
10+00N D 30+00E 10+00N D 30+50E 10+00N D 31+00E 10+00N D 31+50E 10+00N D 32+00E	1 1 1 1	28 20 16 17 21	25 37 25 11 15	98 102 81 66 65	.4 .8 .5 .1 .1	33 19 17 22 26	18 13 11 9 12	871 368 248 212 558	3.65 4.56 4.96 2.56 2.46	15 10 11 8 4	5 5 5 5 5	ND ND ND ND ND	9 8 7 7 7	13 12 8 7 20	.2 .2 .2 .2 .2	2 2 2 2 2	4 2 2 2 2 2	17 13 16 18 10	.18 .18 .08 .07 .93	.042 .094 .086 .015 .028	30 23 24 25 22	24 23 21 22 14	.52 .47 .35 .42 .32	65 49 33 37 38	.01 .01 .01 .02 .01	2 3 2 2 2	1.39 1.48 1.10 .92 .87	.01 .01 .01 .01 .01	.09 .06 .04 .07 .04	11111	3 6 3 4 1	
SO-M-PB 307 SO-M-RS 307 SO-M-PB 308 SO-M-RS 308 SO-M-PB 606	1 1 1 1	58 31 69 47 49	53 30 52 42 24	151 184 119 172 103	.3 .1 .1 .1 .1	125 98 137 141 35	32 24 35 33 15	641 325 650 337 471	6.22 5.89 6.16 6.46 2.97	38 35 35 37 18	5 5 5 5 6	ND ND ND ND ND	8 7 9 7 10	19 11 17 10 16	.3 .2 .3 .4 .3	3 2 2 2 2	2 3 4 3 2	48 38 44 31 18	.31 .12 .22 .12 .23	.093 .084 .074 .106 .045	33 27 43 24 29	114 82 107 73 30	1.17 .71 1.13 .54 .58	125 111 1302 488 101	.04 .02 .03 .02 .03	2 2 3 2	2.00 1.57 1.70 1.45 1.23	.01 .01 .01 .01 .01	.05 .04 .06 .04 .08	2 3 1 1 1	2 8 4 1	
SO-M-RS 606 SO-M-PB 609 SO-M-RS 609 SO-M-PB 611 SO-M-RS 611	1 1 1 1	99 27 59 36 58	36 23 245 50 50	184 80 137 227 594	.5 .1 .5 .7 .9	31 33 42 31 43	13 16 19 14 22	381 402 458 310 497	3.04 2.93 4.35 2.93 3.92	18 7 106 39 39	5 5 5 5 5	ND ND ND ND ND	6 9 8 5	22 12 15 14 22	.9 .2 .3 .3 .7	2 2 2 2 2	2 2 5 3	21 17 22 14 19	.33 .17 .17 .21 .32	.030 .051 .043 .057 .055	24 30 31 29 27	24 23 36 27 32	.34 .46 .49 .47 .51	159 62 125 64 79	.02 .02 .02 .01 .02	2 5 2 2 2	1.32 1.27 1.99 1.16 1.88	.01 .01 .01 .01 .01	.07 .07 .09 .06 .06	11111	1 6 167 4	
SO-M-639 SO-M-640 STANDARD C/AU-S	1 1 19	18 20 65	8 9 40	96 85 134	.1 .1 7.3	27 33 71	14 16 32	234 245 1072	5.43 4.67 3.96	3 6 41	5 5 18	ND ND 7	11 13 39	8 5 53	.2 .2 19.3	2 2 14	4 5 19	17 21 59	.06 .03 .50	.059 .060 .084	34 33 40	29 31 61	.67 .59 .94	69 52 183	.01 .01 .09	2 2 34	2.00 2.42 1.93	.01 .01 .07	.04 .05 .14	1 1 10	2 2 48	

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SAMPLE#	Mo ppm	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ni ppm	Co ppm	Mn ppm	Fe %	As ppm	U ppm	Au ppm	Th ppm	Sr ppm	Cd ppm	Sb ppm	Bi ppm	V ppm	Ca P % %	La ppm	Cr ppm	Mg %	Ba Ti ppm %	BAL ppm %	Na %	к (% рр	a Au** n ppb
SO-M-641 SO-M-642 SO-M-643 SO-M-644 SO-M-645	1 1 1 1 1	11 19 8 27 75	11 16 6 13 27	81 83 71 73 114	.1 .1 .1 .1 .1	23 30 14 19 83	13 14 11 15 28	235 233 269 263 323	4.58 4.40 5.41 6.57 10.01	2 3 2 2 2 2	5 5 5 5 5	ND ND ND ND	17 12 11 13 21	4 4 8 4 5	.2 .2 .2 .2 .2	2 2 2 2 2	2 2 2 2 3	21 18 20 22 15	.01 .028 .02 .042 .13 .086 .04 .106 .01 .069	28 30 49 41 3 0	29 30 34 30 31	.54 .67 .98 .81 .93	58 .01 81 .01 30 .01 20 .01 42 .01	3 1.98 2 2.28 2 2.24 2 2.13 4 3.47	.01 .01 .01 .01 .01	.04 .05 .03 .03 .03	1 1 1 4 1 7 1 4
SO-M-646 SO-M-647 SO-M-648 SO-M-649 SO-M-650	1 3 2 1	22 16 28 23 16	20 45 66 35 32	58 92 117 113 86	.9 .7 .5 .3 .1	14 21 35 25 32	9 13 16 13 15	286 205 353 508 254	4.02 7.13 5.66 3.49 3.41	2 36 18 9 11	5 5 5 5 5	ND ND ND ND	2 8 10 5 8	9 6 5 27 14	.2 .2 .3 .2 .2	2 2 2 2 2	2 3 2 2 2	23 33 17 23 26	.03 .164 .03 .211 .07 .087 .26 .058 .25 .056	27 21 22 29 28	23 30 35 27 28	.22 .37 .62 .62 .70	61 .01 68 .01 47 .01 188 .01 72 .01	2 1.21 4 1.67 2 2.43 2 1.81 2 2.05	.01 .01 .01 .01 .01	.04 .06 .04 .06 .07	1 3 1 5 1 3 1 1 1 3
SO-M-651 SO-M-652 SO-M-653 SO-M-654 RE SO-M-659	1 1 1 1	9 9 15 5 6	32 51 51 20 32	80 105 119 54 75	.1 .1 .4 .2 .2	17 19 25 9 16	10 12 14 6 9	168 211 479 205 349	5.05 5.89 4.18 2.24 3.68	9 15 14 10 11	5 5 5 5 5	ND ND ND ND	9 10 11 6 9	4 7 8 5 7	.2 .2 .5 .2 .3	2 2 2 2 2	2 2 2 2 2 2	22 32 19 22 25	.03 .043 .12 .150 .15 .088 .07 .030 .12 .155	24 25 26 30 24	29 31 29 15 25	.57 .61 .66 .30 .52	61 .01 74 .01 74 .01 81 .01 59 .01	3 2.15 2 2.37 2 2.33 2 1.27 2 2.65	.01 .01 .01 .01 .01	.05 .05 .06 .05 .07	1 6 1 4 1 2 1 3 1 2
S0-M-655 S0-M-656 S0-M-657 S0-M-658 S0-M-659	1 1 1 1 1	22 7 11 4 7	53 32 37 31 30	91 74 88 51 72	.9 .5 .2 1.2 .3	20 16 19 8 13	11 10 11 7 9	206 135 168 134 326	3.49 5.53 5.87 2.67 3.51	20 10 11 8 12	6 5 5 5 5	ND ND ND ND ND	6 10 12 5 9	22 4 5 7	.2 .2 .2 .5 .3	2 2 2 2 2	3 2 2 2 2	29 25 25 22 24	.37 .049 .05 .059 .03 .052 .05 .053 .11 .147	26 23 23 24 23	26 30 29 16 25	.56 .52 .56 .20 .49	169 .01 57 .01 53 .01 54 .01 52 .01	2 2.10 2 2.21 3 2.60 2 1.43 3 2.44	.01 .01 .01 .01 .01	.08 .05 .05 .04 .06	1 3 1 1 1 7 1 2 1 2
S0-M-660 S0-M-661 S0-M-662 S0-M-663 S0-M-664	1 1 1 1	6 8 5 10 13	28 20 26 22 27	77 87 50 63 92	.1 .1 .1 .1 .2	13 22 10 16 19	7 12 6 8 11	144 277 172 161 345	4.07 3.63 2.80 2.99 4.30	11 7 5 7 17	5 5 5 5 5	ND ND ND ND ND	9 8 6 9 8	5 7 4 5 6	.2 .3 .2 .3 .2	2 2 2 2 2	2 2 4 2	30 24 26 20 20	.05 .069 .11 .064 .06 .038 .07 .042 .10 .077	25 27 27 33 26	23 28 19 28 28	.39 .58 .35 .71 .64	73 .01 64 .01 74 .01 59 .01 48 .01	2 2.00 3 2.18 2 1.59 2 1.94 4 2.04	.01 .01 .01 .01 .01	.06 .06 .04 .07 .05	1 1 1 6 1 1 1 1 1 2
S0-M-665 S0-M-666 S0-M-667 S0-M-668 S0-M-669	1 1 1 2 1	12 8 3 80 23	25 14 15 41 21	56 65 31 174 93	.1 .3 .2 1.1 .3	14 15 56 21	8 10 5 25 13	254 927 197 1229 437	2.73 2.66 1.18 4.68 4.08	13 9 3 20 9	5 5 5 5 5	ND ND ND ND	8 3 6 4	4 8 5 35 6	.4 .4 .2 1.0 .4	2 2 2 2 2	2 2 5 2	23 27 14 22 20	.03 .048 .15 .063 .09 .031 .71 .089 .08 .051	31 23 29 55 27	17 21 10 30 31	.40 .54 .27 .80 .58	37.01104.0147.01135.0192.01	2 1.34 2 1.45 2 .97 4 1.99 2 2.03	.01 .01 .01 .01 .01	.06 .07 .05 .07 .04	1 6 1 7 1 1 1 1 1 2
S0-M-670 S0-M-671 S0-M-672 S0-M-673 S0-M-674	1 1 1 1	24 22 12 24 49	25 31 15 13 35	88 109 119 115 113	.6 1.3 .3 .4 .1	18 22 31 35 41	11 13 16 24 20	316 497 321 885 299	3.45 6.32 6.15 8.07 7.50	16 16 11 2 15	5 5 5 5 5	ND ND ND ND	3 6 10 8 15	6 5 6 34	.2 .2 .2 .3 .2	2 2 2 2 2	2 2 2 2 2	23 36 24 25 24	.05 .052 .04 .065 .05 .036 .06 .180 .03 .074	27 25 28 44 3 9	29 32 38 36 38	.62 .47 .95 .65 .86	83 .01 94 .01 40 .01 51 .01 119 .01	4 1.77 5 1.91 2 2.87 3 2.19 3 2.91	.01 .01 .01 .01 .01	.05 .04 .04 .03 .06	1 2 1 11 1 3 1 1 1 5
SO-M-675 SO-M-676 STANDARD C/AU-S	1 1 20	18 22 63	25 19 43	97 96 134	.1 .1 7.4	22 30 74	18 18 32	322 254 1078	7.85 6.52 3.96	8 20 42	5 5 22	ND ND 7	12 13 39	5 4 53	.2 .2 18.5	2 2 15	2 2 21	36 23 60	.04 .078 .02 .068 .50 .084	32 32 40	35 35 61	.73 .72 .95	58 .01 63 .01 183 .09	2 2.83 3 2.53 34 1.94	.01 .01 .07	.05 .05 .14 1	1 4 1 4 1 48



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ACHE ANALTIICAL																														
SAMPLE#	Mo	Cu	Pb	Zn	Ag	Ni	Co	Mn	Fe	As	U	Au	Th	Sr	Cd	Sb	Bi	v	Ca	P	La	Cr	Mg	Ba	Ti	B Al	Na	K	W	Au**
	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	*	ppm	ррп	ppm	ppm	ppm	ppm	ppm	ррп	ppm	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~ ~	ppm	ppm	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	ppm	76	ppm 7	~ ~~	76	ppm	ppo
50- M-677	1	11	1.	37	19 19 19 19 19 19 19 19	10	5	80	80 X	2	5	ND	8	5	15	7	2	27	02	030	18	26	.22	41	-01	11 1.42	.01	.01	4	1
SO M 677	-	17	12	48		15	2 8	285	5 50	ξ	ś	ND	10	6		रं	2	32	03	076	27	31	33	63	01	4 2.00	01	.06	2	1
50-M-670	1	5	14	42	<u></u>	6	~	121	1 07	5	ś		7	š	5	2	2	17	07	032	32	20	40	59	01	4 1.51	.01	.07	1	1
50-M-690	. 1	21	20	92		28	17	370	3 57	7	5	ND	11	11	- .	2	2	17	18	030	38	30	76	71	01	4 1.82	01	.08		2
SU-M-000	1	21	20	71	•	20	13	711	2.27	6	5	ND	7	5		2	2	19	.10	056	30	26		×1	01	3 1 70	01	.06		1
50-M-081	1	10	20	11	- 4	15	(211	5.33	3.8 M - 7	5	NU	'	J		٤	2	10	.07	-050	50	20		01		5 1.70				•
SO-M-682	1	2	9	16	.2	2	1	114	.46	- 4	5	ND	3	5	.2	2	2	9	.07	.016	29	6	.05	35	.01	3.74	.01	.05	1	1
SO-M-683	1	11	20	80	.2	15	7	241	4.67	8	5	ND	8	5	.2	2	2	24	.07	.076	24	31	.54	59	.01	2 2.19	.01	.06	1	228
SO-M-684	1	7	14	52	.2	10	5	411	2.25	6	5	NÐ	6	5	.2	2	2	19	.04	.027	31	16	.31	81	.01	3 1.19	.01	.05	<u></u> 1.	1
SO-M-685	1	13	26	79	.1	18	9	338	3.68	35	5	ND	7	7	.2	2	2	21	.09	.040	31	27	.63	105	101	3 1.89	.01	.06	- 1 1	1
SO-M-686	1	5	12	35	.3	7	5	574	2.03	4	5	ND	6	5	.2	2	2	17	.02	.053	30	15	.16	54	.01	3 1.04	01	.05	1	1
	·	-					-																							
SO-M-687	1	11	20	68	.2	14	7	303	4.44	9	5	ND	7	5	.3	2	2	27	.03	.035	27	30	.57	88	.01	3 1.82	.01	.06	1	1
SO-M-688	1	13	27	67	.6	14	8	577	3.73	10	5	ND	7	5	.2	2	2	28	.03	.058	28	27	.51	64	.01	2 1.63	.01	.07	1	1
SO-M-689	1	12	19	48	.5	11	5	375	3.32	11	5	ND	7	6	.3	2	2	31	.04	.042	27	20	.23	80	.01	2 1.33	.01	.05	1	1
SO-M-690	1	46	41	140	1.3	37	20	1225	4.02	10	8	ND	6	51	.5	2	3	26	.55	.096	52	30	.58	234	.01	2 2.15	.01	.07	1	1
SO-M-691	1	24	27	137	.4	35	11	439	3.74	11	5	ND	8	19	.4	2	2	23	.15	.061	38	32	.59	225	.01	3 2.10	.01	.05	1	1
	•																													
SO-M-800	1	55	40	172	.3	115	25	349	6.99	42	5	ND	9	19	.5	2	2	38	.28	.160	25	96	.84	184	.02	2 2.17	.01	.06	1	1
SO-M-801	1	26	19	95	.2	47	12	259	4.26	14	5	ND	9	10	.2	2	2	22	.11	.047	37	51	.52	103	.01	2 1.27	.01	.06	1	6
SO-M-802	1	35	24	164	1	59	18	312	5.70	23	5	ND	8	10	.4	2	3	27	.10	.062	31	59	.52	70	.01	3 1.40	.01	.06	1	1
SO-M-803	1	40	18	80	4	54	14	409	4.39	17	5	ND	5	9	.2	2	2	37	.09	.070	32	64	.48	74	.01	2 1.20	.01	.05	1	1
SO-M-804	1	7	14	77	.3	11	9	774	4.12	4	5	ND	8	6	.4	2	2	28	.05	.104	24	25	.27	51 🗄	.02	2 1.18	.01	.05	1	1
	•	•	•••								-		-																	
SO-M-805	1	16	14	98	.2	21	8	293	4.28	9	5	ND	9	11	.5	2	2	26	.13	.082	31	27	.51	92	.01	3 1.40	.01	.06	1	1
SO-M-806	1	20	14	87	.1	25	10	225	4.13	10	5	ND	9	13	.3	2	2	17	.14	.041	27	23	.38	39	-02	2 1.19	.01	.04	1	1
SO-M-807	1	21	15	70	.2	34	10	628	3.04	13	5	ND	7	9	.3	2	2	18	.12	.055	32	39	.31	60	.01	2 1.05	.01	.07	2	4
SO-M-808	1	21	38	116	.2	27	12	249	3.14	13	5	ND	8	17	.4	2	2	16	.26	.064	29	24	.39	31 👌	.02	2 1.12	.01	.05	1	1
SO-M-809	1	30	41	99	.2	31	10	941	2.93	23	5	ND	8	16	.5	2	2	12	.22	.051	28	19	.31	44	.02	2.83	.01	.05	1	2
						-																								
so-m-810	1	26	31	102	.2	27	13	317	3.16	14	5	ND	8	15	.5	2	2	20	.22	.034	24	26	.36	63	.02	2 1.33	.01	.06	1	2
SO-M-811	1	34	42	134	.4	34	13	697	3.13	20	5	ND	6	26	.6	2	2	17	.47	.055	22	28	.38	87	.01	3 1.20	.01	.08		3
SO-M-812	1	57	33	139	.1	42	16	554	4.05	16	5	ND	6	23	.4	2	2	24	.31	.043	29	41	.59	90	.02	3 1.88	.01	.09	1	2
SO-M-813	1	39	33	106	.3	36	13	391	3.40	12	5	ND	8	19	.7	2	2	19	.28	.048	25	32	.52	70	.02	3 1.45	.01	.07	1	1
SO-M-814	1	37	18	79	.1	43	11	321	3.47	8	5	ND	12	21	.2	2	2	23	.28	.056	29	43	.79	76	.03	2 1.60	.01	. 10	1	4
									- •				_																	_
RE SO-M-810	1	26	28	103	.2	28	13	310	3.14	15	5	ND	8	15	.2	2	2	20	.22	.034	23	26	.36	63	.01	2 1.33	.01	.06	1	3
SO-M-815	1	19	15	78	1	31	12	462	2.91	6	5	ND	6	14	.3	2	2	21	.19	.029	23	33	.53	79	.01	2 1.48	.01	.07	1	4
SS-M92-099	1	38	20	144	. 1	32	13	367	2.59	12	5	ND	8	12	.4	2	2	12	.29	.094	28	18	.37	69	.01	3.97	'.01	.03	1	1
STANDARD C/AU-S	19	60	37	130	6.9	71	31	1112	3.96	41	20	7	41	52	17.1	14	19	58	.51	.083	38	60	.93	183	.08	37 1.98	.07	. 15	10	52
SO-M-811 SO-M-812 SO-M-813 SO-M-814 RE SO-M-810 SO-M-815 SS-M92-099 STANDARD C/AU-S	1 1 1 1 1 1 19	34 57 39 37 26 19 38 60	42 33 33 18 28 15 20 37	134 139 106 79 103 78 144 130	.4 .1 .3 .1 .2 .1 .1 6.9	34 42 36 43 28 31 32 71	13 16 13 11 13 12 13 31	697 554 391 321 310 462 367 1112	5.13 4.05 3.40 3.47 3.14 2.91 2.59 3.96	20 16 12 8 15 6 12 41	5 5 5 5 5 5 5 20	ND ND ND ND ND ND ND 7	6 8 12 8 6 8 41	26 23 19 21 15 14 12 52	.6 .4 .7 .2 .2 .3 .4 17.1	2 2 2 2 2 2 2 2 2 14	2 2 2 2 2 2 2 2 2 19	17 24 19 23 20 21 12 58	.47 .31 .28 .28 .28 .22 .19 .29 .51	.055 .043 .048 .056 .034 .029 .094 .083	22 29 25 29 23 23 28 38	28 41 32 43 26 33 18 60	.38 .59 .52 .79 .36 .53 .37 .93	67 90 70 76 63 79 69 183	.01 .02 .03 .03 .01 .01 .01	3 1.26 3 1.88 3 1.45 2 1.66 2 1.33 2 1.48 3 .97 37 1.98	.01 .01 .01 .01 .01 .01 .01 .01	.08 .09 .07 .10 .06 .07 .03 .15	1 1 1 1 1 1 10	3 2 1 4 3 4 1 52



Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221

fo: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5

Project : 9124/9201 Comments: CC: W. DONALDSON

CERTIFICATE OF ANALVEIS

Page Number : 1-A Total Pages : 1 Certificate Date: 27-AUG-92 Invoice No. : 19219799 P.O. Number : Account :GZ

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									CERTI	FICATE	OF AN	ALYSIS		4921979	9 9	
SAMPLE	P) C	rep Ode	Au ppb FA+AA	Ag ppm AAS	Al % (ICP)	Bappm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Coppm (ICP)	Cr ppm (ICP)	Cuppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)
15195 15196 15214 15215	205 205 205 205	274 274 274 274 274	<pre>< 5 < 5 < 5 < 5 < 5 < 5</pre>	< 0.2 < 0.2 < 0.2 < 0.2 < 0.2	10.95 11.25 3.26 1.42	5500 1180 430 640	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5	10 12 < 2 < 2 < 2	0.20 0.09 0.06 0.19	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5	3 13 2 1	187 190 170 285	17 23 203 13	3.17 5.36 2.90 0.76	3.48 2.71 0.81 0.61	1.35 1.20 0.21 0.08
15216 15217 15218 15219 15220	205 205 205 205 205	274 274 274 274 274 274	<pre>< 5 < 5</pre>	< 0.2 < 0.2 < 0.2 < 0.2 < 0.2 < 0.2 < 0.2	0.06 4.02 5.14 13.70 9.83	20 550 550 1520 3230	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	< 2 < 2 < 2 < 2 < 2 < 2 8	12.75 0.61 1.07 0.10 3.95	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	4 10 8 9 13	155 181 233 127 102	3 21 16 21 26	11.15 2.16 3.56 3.30 3.96	0.01 1.16 1.74 4.73 2.18	0.90 0.29 0.25 0.44 2.76
15221 15222 15223 15225 15226	205 205 205 205 205	274 274 274 274 274 274	<pre>< 5 < 5</pre>	< 0.2 0.4 < 0.2 2.0 0.2	4.95 3.38 3.03 2.78 1.96	1200 680 630 40 690	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	< 2 8 < 2 10 < 2	9.13 0.24 0.07 0.04 0.19	0.5 < 0.5 < 0.5 0.5 < 0.5 < 0.5	35 9 3 21 < 1	266 367 210 138 302	31 396 15 423 11	7.11 3.52 1.61 6.65 0.86	1.67 1.01 1.07 0.15 0.87	4.19 0.59 0.20 1.50 0.11
15227 15228 15229 15230 15231	205 205 205 205 205	274 274 274 274 274 274	<pre>< 5 < 5</pre>	< 0.2 < 0.2 < 0.2 0.8 < 0.2 < 0.2 < 0.2	2.09 2.03 1.36 1.42 7.72	910 1050 1320 800 7280	< 0.5 < 0.5 < 0.5 < 0.5 < 0.5 < 0.5	< 2 < 2 < 2 < 2 < 2 < 2 8	0.08 0.44 0.02 7.69 4.99	< 0.5 1.5 < 0.5 < 0.5 < 0.5 < 0.5	2 1 < 1 5 10	145 264 256 199 196	141 61 9 67 128	0.54 0.95 0.40 2.94 3.61	1.05 0.74 0.65 0.50 2.05	0.27 0.13 0.11 4.46 2.03

CERTIFICATION:_



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212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 To: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5

Project : 9124/9201 Comments: CC: W. DONALDSON

CERTIFICATE OF ANALYSIS

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Certificate Date: 27-AUG-92 Invoice No. 19219799

Page Nu Total Pas

Account

P.O. Number

STAMOLE	PR	EP DE	Mn ppm (ICP)	Moppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)		
15195 15196 15214	205 205 205	274 274 274	150 315 660 20	15 < 1 1 12	0.74 0.80 0.21 0.03	3 15 22 18	140 580 130 1020	8 6 52 28	166 78 33 26	0.38 0.22 0.09 0.03	154 96 96 237	< 10 < 10 < 10 < 10	98 154 64		
15215 15216 15217 15218 15219	205 205 205 205 205	274 274 274 274 274	1080 345 455 210	1 <1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	< 0.01 0.89 0.75 0.60	14 38 24 29 28	60 310 100 370 430	4 4 12 12 8	104 62 41 52 486	< 0.01 0.10 0.11 0.30 0.37	10 39 39 92 83	< 10 < 10 < 10 < 10 < 10 < 10	188 54 72 82 78		
15220 15221 15222 15223 15223	205 205 205 205 205	274 274 274 274 274	535 2210 1245 1010 385	4 1 < 1 1	0.27 0.23 0.77 0.03	118 21 7 7	1400 390 100 80	6 40 18 384 168	355 26 21 4 27	0.36 0.10 0.04 0.02 0.06	135 30 10 13 278	< 10 < 10 < 10 < 10 < 10 < 10	116 74 34 332 52		
15226 15227 15228 15229	205 205 205 205 205	274 274 274 274 274	25 95 30 15 2040	4 < 1 22 13 1	0.08 0.03 0.04 0.02 0.02	11 19 11 6 21	230 2360 90 330	10 6 12 344	11 27 7 145	0.07 0.06 0.06 0.03 0.26	63 2350 1450 53 278	<pre>< 10 < 10</pre>	62 118 22 566 56		
15231	205	274	400	2	0.29	29	*120								
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CERTIFICATION:_



Analytical Chemists * Geochemists * Registered Assayers 212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221

fo: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5

Project : 9124 Comments: CC: W. DONALDSON

Page Nu Jer : 1-A Total Pages : 1 Certificate Date: 30-AUG-92 Invoice No. : 19219802 P.O. Number : Account :GZ

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								CERTIFICATE OF ANALYSIS A9219802								
SAMPLE	P C	REP ODE	Au ppb FA+AA	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Coppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)
15224	208	274	150	73.0	0.76	170	< 0.5	6	< 0.01	74.0	29	148	1355	>25.0	0.37	0.10
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Analytical Chemists * Geochemists * Registered Assayers 212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 fo: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5

Project : 9124 Comments: CC: W. DONALDSON Page Nu. Jer :1-B Total Pages :1 Certificate Date: 30-AUG-92 Invoice No. :19219802 P.O. Number : Account :GZ

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CERTIFICATE OF ANALYSIS A9219802 PREP Mn ppm Mo ppm Na 😵 Ni ppm P ppm Pb ppm Ti % V ppm W ppm Sr ppm Zn ppm Pb Zn SAMPLE CODE (ICP) (ICP) (ICP) (ICP) (ICP) AAS (ICP) (ICP) (ICP) (ICP) (ICP) € ÷ 15224 208 274 40 27 0.01 39 40 >10000 < 1 0.02 138 < 50 >10000 2.44 2.83

CERTIFICATION:

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Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221 5: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC . V7Y 1G5 Page er :1-A Total Pages :2 Certificate Date: 17-SEP-92 Invoice No. :19221145 P.O. Number : Account :GZ

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Project : 9124 Comments: ATTN: W.DONALASON

	_							CERTIFICATE OF ANALYSIS A9221145								
SAMPLE	I C	REP	Au ppb FA+AA	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Coppm (ICP)	Cr ppm (ICP)	Cuppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)
15305	205	274	< 5	6.4	6.01	900	< 0.5	< 2	4.80	14.0	41	269	1035	6.48	1.15	2.18
15306	205	274	< 5	< 0.2	8.43	3070	< 0.5	< 2	4.83	< 0.5	12	103	63	3.09	3.65	2.61
15307	205	274	< 5	< 0.2	2.57	1080	< 0.5	< 2	0.06	< 0.5	2	224	11	1.58	1.23	0.20
15308	205	274	< 5	< 0.2	9.04	1200	< 0.5	< 2	4.93	< 0.5	15	249	49	4.65	1.87	2.26
15351	205	274	< 5	< 0.2	3.64	350	< 0.5	< 2	0.69	< 0.5	6	245	26	1.90	1.17	0.36
15352	205	274	< 5	< 0.2	7.09	800	< 0.5	< 2	0.43	< 0.5	13	184	36	3.58	2.76	0.53
15353	205	274	< 5	< 0.2	7.29	1080	0.5	< 2	0.14	< 0.5	15	121	26	3.58	3.00	0.34
15354	205	274	< 5	0.8	3.80	4110	< 0.5	< 2	0.17	11.5	4	174	71	1.98	1.59	0.27
15355	205	274	< 5	< 0.2	8.57	2990	< 0.5	< 2	0.34	< 0.5	4	143	7	1.15	2.94	0.38
15356	205	274	< 5	< 0.2	4.39	1100	< 0.5	< 2	2.56	< 0.5	7	160	10	2.01	2.05	0.45
15357	205	274	< 5	< 0.2	5.49	740	< 0.5	< 2	0.60	< 0.5	11	184	17	2.34	2.13	0.39
15358	205	274	< 5	< 0.2	5.44	620	< 0.5	< 2	0.06	< 0.5	15	261	26	3.01	1.91	0.43
15359	205	274	< 5	< 0.2	9.93	1170	< 0.5	< 2	0.05	< 0.5	17	174	54	4.35	3.37	0.98
15360	205	274	< 5	< 0.2	7.77	730	< 0.5	< 2	0.41	< 0.5	16	220	33	4.03	2.58	0.86
15361	205	274	< 5	< 0.2	5.48	1060	< 0.5	2	2.00	< 0.5	8	119	42	2.41	2.30	1.45
15362	205	274	< 5	0.4	5.36	1200	< 0.5	2	1.24	< 0.5	12	160	17	2.84	2.12	0.79
15363	205	274	< 5	0.6	7.16	1600	< 0.5	< 2	1.30	2.0	16	208	22	3.55	2.85	0.89
15364	205	274	< 5	0.4	7.33	1850	< 0.5	< 2	0.13	< 0.5	11	131	26	2.55	3.17	0.35
15365	205	274	< 5	0.6	5.98	1380	< 0.5	< 2	0.10	< 0.5	14	176	94	2.92	2.45	0.31
15366	205	274	< 5	0.6	5.86	360	< 0.5	< 2	0.06	< 0.5	19	128	133	12.15	1.19	1.87
15367	205	274	50	25.8	6.74	190	< 0.5	< 2	0.16	4.0	44	123	>10000	19.40	0.63	2.83
15368	205	274	70	0.8	8.65	650	< 0.5	< 2	0.24	< 0.5	15	153	343	12.35	2.08	2.20
15369	205	274	< 5	0.3	8.54	780	< 0.5	< 2	0.24	< 0.5	22	90	415	10.60	2.39	2.36
15370	205	274	< 5	1.2	8.53	1470	< 0.5	< 2	0.07	< 0.5	10	142	70	4.19	3.63	0.63
15371	205	274	< 5	6.4	4.12	500	< 0.5	< 2	0.14	13.5	22	109	337	3.47	1.90	0.25
15372	205	274	< 5	0.4	6.82	1810	< 0.5	< 2	0.13	< 0.5	13	135	73	2.69	2.26	0.71
15373	205	274	< 5	0.2	8.13	2050	< 0.5	2	0.12	< 0.5	12	124	32	2.90	3.04	0.65
15374	205	274	< 5	< 0.2	6.40	1890	< 0.5	< 2	0.04	< 0.5	6	151	17	2.10	2.44	0.46
15375	205	274	30	0.4	7.54	3410	< 0.5	2	0.20	0.5	11	181	58	2.81	3.14	0.43
100/0	205	4/4	15	2.0	1.45	660	< 0.5	< 2	0.03	1.5	14	178	313	6.80	2.31	0.26
15377	205	274	35	2.0	1.72	180	< 0.5	< 2	0.03	1.0	4	293	130	2.85	0.69	0.08
15378	205	274	< 5	0.8	7.13	720	< 0.5	< 2	0.03	1.5	16	136	371	4.59	2.85	0.28
15379	205	274	< 5	0.8	6.59	660	< 0.5	< 2	0.03	< 0.5	8	215	156	4.04	2.74	0.25
15380	205	274	< 5	0.2	8.43	850	< 0.5	< 2	0.19	< 0.5	8	109	110	3.97	3.19	0.28
10001	205	2/4	< 5 	0.2	8.83	840	< 0.5	< 2	0.04	< 0.5	12	165	29	3.84	3.52	0.43
15382	205	274	< 5	0.4	9.01	740	< 0.5	4	0.18	< 0.5	14	170	45	6.13	2.81	1.54
15383	205	274	< 5	1.8	3.62	60	< 0.5	< 2	0.06	< 0.5	6	144	189	7.08	0.20	1.60
15305	205	274		0.2	0.77	80	< 0.5	< 2	0.01	< 0.5	1	327	16	1.30	0.32	0.05
15386	205	274		0.0	9.94	44∡U 0.⊆0	< U.5	< 2	0.08	< 0.5	10	357	26	4.21	1.74	0.72
2000		2/3		0.4	3.40	300	× 0.5	٢ ٢	0.14	< 0.5	18	192	80	4.0/	3.49	0.31
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CERTIFICATION



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Chemex Labs Ltd.

Analytical Chemists * Geochemists * Registered Assayers

212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221

o: RIO ALGOM EXPLORATION INC. P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5

Page Jer :1-B Total Pages :2 Certificate Date: 17-SEP-92 Invoice No. : 19221145 P.O. Number : Account :GZ

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Project : 9124 Comments: ATTN: W.DONALASON

CERTIFICATE OF ANALYSIS

A9221145

SAMPLE PREP (JCP) Mn ppm (ICP) Mo ppm (ICP) Na % (ICP) Ni ppm (ICP) P ppm (ICP) Pb ppm (ICP) Sr ppm (ICP) Ti % (ICP) V ppm (ICP) W ppm (ICP) Zn ppm (ICP) 15305 15306 15306 15307 15307 15308 205 274 274 440 830 41 < 1 2.01 88 1190 260 484 6 250 0.23 161 < 10 2760 15307 15308 205 274 205 274 180 1 0.07 21 340 4 10 0.06 68 < 10 90 15308 205 274 435 2 1.74 54 670 4 454 0.77 176 < 10 72 15351 205 274 620 < 1 0.77 14 100 12 73 0.06 25 < 10 28	
15305 205 274 830 < 1 2.01 88 1190 484 250 0.23 161 < 10 2760 15306 205 274 440 < 1 1.64 20 260 6 310 0.11 55 < 10 102 15307 205 274 180 1 0.07 21 340 4 10 0.06 68 < 10 90 15308 205 274 435 2 1.74 54 670 4 454 0.77 176 < 10 72 15351 205 274 620 < 1 0.77 14 100 12 73 0.06 25 < 10 28	
15306 205 274 440 < 1	
15307 205 274 180 1 0.07 21 340 4 10 0.06 68 < 10 90 15308 205 274 435 2 1.74 54 670 4 454 0.77 176 < 10	
15308 205 274 435 2 1.74 54 670 4 454 0.77 176 < 10 72 15351 205 274 620 < 1	
15351 205 274 620 < 1 0.77 14 100 12 73 0.06 25 < 10 28	
15352 205 274 570 1 0.80 31 190 38 82 0.10 51 < 10 78	
15353 205 274 630 1 0.79 32 120 12 70 0.09 51 < 10 68	
15354 205 274 150 47 0.09 50 1340 20 94 0.09 868 < 10 394	
15355 205 274 305 2 1.86 8 290 12 87 0.18 129 < 10 46	
15356 205 274 910 1 0.21 16 80 6 56 0.10 39 < 10 52	
15357 205 274 860 1 0.90 22 100 20 64 0.09 42 < 10 52 15357 205 274 1370 11 0.90 22 100 20 64 0.09 42 < 10	
15358 205 274 1270 < 1 0.76 37 110 14 38 0.09 34 < 10 68	
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15364 205 274 275 11 0.18 51 680 26 57 0.13 297 < 10 150	
15365 205 274 355 7 0.15 40 430 64 44 0.12 192 $<$ 10 304	
15366 205 274 1630 < 1 0.09 26 10 78 21 0.07 38 < 10 412	
15367 205 274 3160 1 0.30 31 830 234 36 0.12 147 < 10 1485	
15368 205 274 1750 2 0.19 40 910 40 46 0.15 106 < 10 472	
15369 205 274 2620 < 1 0.17 30 880 12 50 0.26 117 < 10 306	
15370 205 274 200 11 0.22 44 580 94 56 0.17 228 < 10 312	
15371 205 274 85 11 0.11 54 550 880 39 0.08 211 < 10 4360	
15372 205 274 365 9 0.53 69 600 20 72 0.16 218 < 10 190	
15373 205 274 390 8 0.29 58 550 16 73 0.25 295 < 10 154 154	
15374 205 274 55 12 0.20 31 280 16 51 0.19 347 < 10 88	
15375 205 274 210 6 0.19 56 1120 14 82 0.24 544 < 10 458	
15376 205 274 1395 < 1 0.45 29 360 280 67 0.05 76 < 10 790	
15377 205 274 465 1 0.09 12 140 636 14 0.02 22 < 10 436	
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15380 205 274 515 2 0.47 23 1080 92 61 0.08 118 < 10 222	
15381 205 274 790 1 0.54 30 190 86 57 0.09 62 < 10 260	
15382 205 274 1315 < 1 0.51 36 240 54 57 0.07 61 < 10 322	
15383 205 274 635 1 0.22 22 330 264 25 0.04 104 < 10 444	
15384 205 274 260 <1 0.03 8 70 26 4 0.01 7 < 10 78	
15385 $205 274$ 1365 1 0.29 45 330 148 33 0.06 36 < 10 314	
1000 200 200 21 0.58 54 510 32 82 0.12 72 < 10 144	
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CERTIFICATION:

RIO ALGOM EXPLORATION INC. J: P.O. BOX 10335, PACIFIC CENTRE 1650 - 609 GRANVILLE ST. VANCOUVER, BC V7Y 1G5

Page .er :2-A Total Fuyes :2 Certificate Date: 17-SEP-92 : 19221145 Invoice No. P.O. Number : Account :GZ

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Chemex Labs Ltd. 0

Analytical Chemists * Geochemists * Registered Assayers 212 Brooksbank Ave., North Vancouver British Columbia, Canada V7J 2C1 PHONE: 604-984-0221

Project : 9124 Comments: ATTN: W.DONALASON

CERTIFICATE OF ANALYSIS A9221145 PREP A1 % Au ppb Bi ppm Ca % Cd ppm K % Ag ppm Ba ppm Be ppm Co ppm Cr ppm Cu ppm Fe % Mar % SAMPLE CODE FA+AA AAS (ICP) 15387 205 274 < 5 1.2 9.10 2500 < 0.5 < 2 0.17 < 0.5 22 168 357 0.95 5.53 3.32 15388 205 274 45 1.2 6.31 170 < 0.5 < 2 0.15 < 0.5 13 199 133 3.73 2.51 0.43 15389 205 274 10 0.8 7.51 340 < 0.5 2 0.91 < 0.5 14 128 55 3.51 3.16 0.97 15390 205 274 15 3.8 7.01 210 < 0.5 < 2 0.10 0.5 14 140 206 4.23 2.85 0.32 15391 205 274 < 5 0.2 5.37 620 < 0.5 < 2 0.07 < 0.5 13 188 40 5.69 1.74 0.78 15392 205 274 < 5 < 0.2 8.22 1090 < 0.5 < 2 0.14 < 0.5 15 200 35 3.60 3.22 0.31 15393 205 274 30 12.8 6.04 350 < 0.5 8 0.14 7.0 28 176 1435 8.96 2.40 0.62 15394 205 274 1070 < 5 0.4 3.46 < 0.5 < 2 0.17 < 0.5 9 304 258 2.54 1.47 0.20 15395 205 274 < 5 < 0.2 0.56 160 < 0.5 < 2 0.03 < 0.5 2 389 50 1.72 0.22 0.03 15396 205 274 110 1.6 9.05 2010 < 0.5 < 2 0.49 < 0.5 32 210 525 7.23 3.48 0.58 15397 205 274 10 < 0.2 1.05 360 < 0.5 < 2 0.19 1 77 < 0.5 285 9.41 0.44 0.14 205 274 15398 < 5 < 0.2 3.58 1470 < 0.5 < 2 0.07 < 0.5 6 185 195 1.55 1.78 0.27 15399 205 274 < 5 0.6 2.89 970 < 0.5 < 2 0.14 < 0.5 3 227 161 2.09 1.31 0.20 15400 205 274 < 5 0.4 3.54 1290 < 0.5 2 0.02 < 0.5 3 236 102 1.45 1.74 0.28 15401 205 274 40 1.8 3.59 1330 < 0.5 < 2 0.01 < 0.5 3 172 257 2.28 1.72 0.27 15402 205 274 < 5 0.6 0.59 290 < 0.5 2 0.49 2 296 < 0.5 26 1.19 0.23 0.31 15403 205 274 < 5 3.8 3.99 2470 < 0.5 < 2 3.38 3.5 12 496 396 6.73 1.68 2.03 15404 205 274 < 5 1.4 0.90 350 < 0.5 < 2 0.06 < 0.5 3 463 28 1.17 0.27 0.04 15405 205 274 < 5 2010 0.4 4.22 < 0.5 < 2 0.09 < 0.5 8 364 223 2.53 2.08 0.30 15406 205 274 < 5 2.52 1280 0.6 < 0.5 < 2 0.03 < 0.5 3 203 271 1.97 1.26 0.19 15407 205 274 < 5 1.0 4.30 2260 < 0.5 < 2 0.46 0.5 8 251 262 3.18 2.23 0.32

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Project : 9124 Comments: ATTN: W.DONALASON

CERTIFICATE OF ANALYSIS

CERTIFICATION:

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SAMPLE	I	REP CODE	Mn ppm (ICP)	Moppm (ICP)	Na % (ICP)	Ni ppm (ICP)	P ppm (ICP)	Pb ppm AAS	Sr ppm (ICP)	Ti % (ICP)	V ppm (ICP)	W ppm (ICP)	Zn ppm (ICP)			
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Chemex Labs Ltd.

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SAMPLE	PREP CODE	Au ppb FA+AA	Ag ppm AAS	Al % (ICP)	Ba ppm (ICP)	Be ppm (ICP)	Bi ppm (ICP)	Ca % (ICP)	Cd ppm (ICP)	Coppm (ICP)	Cr ppm (ICP)	Cu ppm (ICP)	Fe % (ICP)	K % (ICP)	Mg % (ICP)
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APPENDIX III

ROCK SAMPLE DESCRIPTIONS

APPENDIX III - ROCK SAMPLE DESCRIPTIONS *** Trench sample descriptions on maps 2 to 7.

A5210	CHLORITE SCHIST 1% pyrite	Outcrop, grab
A5231	GRAPHITIC SCHIST trace disseminated pyrite	Outcrop, grab
A5232	GRAPHITIC SCHIST trace disseminated pyrite	Outcrop, grab
10056	CHLORITIC SCHIST 0.5% chalcopyrite, 1% pyrite	Outcrop, grab
10057	CHLORITIC SCHIST minor disseminated pyrite and ch	Outcrop, grab nalcopyrite
10058	SERICITE-ALBITE-TALC SCHIST 20 cm boulder, 10% disseminate	Float, grab d pyrite
15162	CHLORITIC SCHIST(?) limonitic rock with some quartz	Subcrop, grab
15163	GRAPHITIC PHYLLITE 0.5% disseminated and aggregat	Float, grab es of pyrite
15164	CHLORITE SCHIST 0.5% pyrite	Float, grab
15165	INTERMEDIATE VOLCANIC FLO angular rock, 1% pyrite	W Float, grab
15166	GRIT 0.5% disseminated pyrite, 2% chl	Float, grab orite
15195	CHLORITE SCHIST iron-stained weathered surfaces a	Outcrop, grab and fractures
15196	CHLORITIC SCHIST 1% disseminated pyrite, rust-colo	Outcrop, grab ured weathering
15214	GRAPHITIC SCHIST AND ARGIL	LITE Outcrop, grab

15215	GRAPHITIC PHYLLITE 0.5% thin quartz stringers, minor	Outcrop, grab diss. pyrite
15216	30 cm QUARTZ VEIN 50% limonitic-rich cavities	Outcrop, grab
15217	CHLORITE-SERICITE SCHIST 10% limonitic cavities, several qu	Outcrop, grab lartz veins
15218	CHLORITIC SCHIST limonite on several fractures	Outcrop, grab
15219	CHLORITIC SCHIST 0.2% pyrite cubes to 4 mm size	Outcrop, grab
15220	SERICITE-ALBITE-TALC SCHIST minor diss. pyrite, rust-coloured	⁻ Outcrop, grab laminations
15221	QUARTZ-SERICITE SCHIST 1 cm quartz vein, 1 cm thick lime	Float, grab onitic weathering
15222	QUARTZ VEIN 1% disseminated pyrite, 5% choo	Float, grab colate-brown weathering
15223	QUARTZ-ANKERITE SCHIST 4% ankerite porphyroblasts, 1 cr	Float, grab n quartz vein
15224	MASSIVE SULPHIDE BOULDER predominately pyrite, with hydro:	Float, grab zincite weathering
15225	QUARTZITE(?) 2% disseminated pyrite	Float, grab
15226	ARGILLITE graphitic, with rust-coloured frac	Outcrop, grab tures
15227	GRAPHITIC SCHIST limonite on fractures	Outcrop, grab
15228	GRAPHITIC SCHIST 0.5% remnant pyrite cavities to 4	Outcrop, grab mm width
15229	GRAPHITIC ARGILLITE 4% carbonate veins, 0.5% pyrite	Float, grab cubes to 3 mm size

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15230	QUARTZ AND ARGILLITE FLOAT 6% limonite on all fractures	Float, grab
15231	GRAPHITIC PHYLLITE 4% limonite on fractures, rock fee	Float, grab els heavy
15305	QUARTZ-SERICITE SCHIST 1% disseminated pyrite, 1 cm lim	Float, grab onitic weathering
15306	ALTERED VOLCANIC(?) abundant pyrite cubes to 3 mm s	Float, grab ize
15307	ARGILLITE extremely folded, with thin white I	Float, grab bands (non-calc)
15308	SILTSTONE 1% bedded disseminated pyrite	Float, grab

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GEOPHYSICAL REPORT

RIO ALGOM EXPLORATION INC.

GEOPHYSICAL REPORT ON A HORIZONTAL LOOP EM (GENIE) SURVEY

MASS PROPERTY LIKELY, B.C.

LATITUDE: 52°45'N LONGITUDE: 121°18'W CARIBOO M.D. NTS: 93A/11,14

AUTHOR: Dennis V. Woods, Ph.D., P.Eng. Consulting Geophysicist

> DATE OF WORK: 15-24 June 1992 DATE OF REPORT: 8 Aug 1992

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DENNIS V. WOODS, Ph.D., P.Eng. Consulting Geophysicist

2539 - 140th Street, White Rock, B.C. V4A 4H9 (604) 538-1445

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Мар	A1	VLF-EM Profiles - Grid A
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Мар	B1	VLF-EM Profiles - Grid B
Мар	B2	VLF-EM Contours - Grid B
Мар	B3	GENIE Profiles - Grid B
Мар	C1	VLF-EM Profiles - Grid C
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Мар	D1	VLF-EM Profiles - Grid D
Мар	D2	VLF-EM Contours - Grid D
Мар	D3	GENIE Profiles - Grid D

INTRODUCTION:

During the period 15-24 June 1992, a horizontal loop electromagnetic (HLEM) survey was carried out on the Mass Property in central British Columbia for Rio Algom Exploration Inc. The survey was conducted on four separate grid areas south of Cariboo Lake near Likely, B.C. using a Scintrex SE-88 GEometrically Normalized In-phase Electromagnetic (GENIE) system.

The purpose of the survey was to locate EM conductors which had previously been detected by a helicopter airborne EM survey (Aerodat, 1991). Poor navigational control of this survey, and hence the rather imprecise resolution of the detected conductors, necessitated a reconnaissance type ground EM follow-up. The GENIE system was selected because of its greater portability than fixed source, transient EM (e.g. PEM), and its immunity from topographic effects unlike conventional HLEM systems (e.g. MaxMin). Although GENIE survey data is not as fully interpretable as other more powerful systems, it was believed to be adequate to locate the airborne conductors for follow-up ground truth by trenching or shallow drilling.

The results of the survey are presented in this report along with a technical description of the GENIE method, survey procedures and data processing. The locations, depths, dips and conductivity-thickness products (conductances) of conductors have been interpreted from the survey data. The results of a VLF-EM survey carried out by personnel of Rio Algom in May 1992 have also been plotted and included in this report to aid in the discrimination of possible economic conductors.

SURVEY LOCATION AND ACCESS:

The Mass property is located on the north slopes of Browntop Mountain south of Cariboo Lake, about 20 kilometres northeast of Likely, B.C. (Figure 1). Access is via logging loads from Likely along the Cariboo River valley and up the slopes of Browntop Mountain. Each survey grid is easily accessible by logging road.

HORIZONTAL LOOP ELECTROMAGNETIC METHOD:

The horizontal loop electromagnetic (HLEM) method is a moving-source, frequency domain EM technique in which the transmitter and receiver coils are maintained in a horizontal (or at least parallel to mean terrain) coplanar alignment at a fixed separation. The vectorial sum of the secondary and primary fields are measured with the receiver coil and compared in amplitude and phase with a reference sample of pure primary field obtained by direct hard-wire connection to the transmitter. The measured response is usually resolved into a component which is perfectly in phase with the primary field (inphase or real component) and a component which is precisely 90° out of phase with the primary (quadrature or imaginary component).

Conductive structures in the ground will cause a marked change in the amplitude and phase (or in-phase and quadrature components) of the secondary field by electromagnetic induction. The character of an anomalous response depends on the geometry, size and conductivity of the conductive formation in the earth. Generally, a bedrock conductor will produce a negative response when straddled by the



Figure 1. Location Map - Mass Property Rio Algon Exploration Inc. transmitter and receiver, and a positive response when the system is removed from the conductor by a short distance. More complex anomaly profiles result from flat-lying to gently dipping conductors, and from multiple conductors separated by less than the transmitter to receiver coil separation.

The relative amplitude of the in-phase and quadrature components is a direct function of the conductivity and size of the conductor (along with coil separation and frequency of the system) and is used to interpret the conductance and depth of the conductor. The depth of detection of an HLEM system is nominally half the coil separation, however if noise is kept to a minimum, 2-3% anomalies due to conductors at twice that depth can sometimes be identified. Coil separation is limited by the size and power of the transmitter which can be efficiently carried through the bush. Maximum separation is usually of order 100-200 m, although some high powered systems can be operated at 400 m separation under ideal conditions.

GEOMETRICALLY NORMALIZED IN-PHASE ELECTROMAGNETIC SYSTEM:

The GENIE (GEometrically Normalized In-phase Electromagnetic) system is a frequency domain EM system which is essentially the same as conventional horizontal loop EM (HLEM) except that only the in-phase component is measured, and the secondary response is normalized to a low-frequency reference field rather than to a hard-wired sample of the primary field. This normalization method has two significant advantages: 1) the absence of a interconnection cable between the

receiver and the transmitter eases logistical use in rugged terrain, and 2) since the secondary field is normalized by a low-frequency reference field which will have nearly the same geometric distortion due to coil misalignment, the recorded response is almost completely unaffected by rugged topography.

There are some drawbacks however. Since only the in-phase response is measured there is less interpretive power than in-phase and quadrature HLEM systems, the ratio of high to low frequency secondary fields can potentially approach unity for extremely strong conductors thus rendering them undetectable, and the low-frequency reference field can be differentially effected by the geologic structure thus distorting an anomalous response which leads to misinterpretations.

These possible difficulties have been taken into account in the design of the instrument and the selection of the reference and signal frequencies. The system has been designed for use in the Canadian Shield and Cordilleran environments for massive sulphide exploration, where it has had considerable success (e.g. Doborzynski, et al., 1981). Further details of the theory of operation of the GENIE system are can be found in Johnson and Doborzynski (1986). Instrument specifications are included at the end of this report.

SURVEY PROCEDURES:

The GENIE survey at the Mass property was carried out on selected lines of four separate grids established by Rio Algom personnel after an initial ground follow-up investigation of the airborne EM survey

in May 1992. Reconnaissance VLF-EM using a Geonics EM16 VLF receiver was carried out at this time to approximately locate conductors and position the survey grids. A number of specific areas previously identified for follow-up work were eliminated from further consideration due to the presence of graphitic units in proximity to airborne EM anomalies. The four selected areas for the GENIE survey are designated "A" through "D" and are shown in Figures 2 to 5 respectively. Details of the survey are listed below in Table 1.

Table 1 GENIE Survey - Mass Property

Grid	Line	Stations	Length	
А	9+00E	19+00N to 25+00N	600 m	
	11+00E	19+25N to 25+00N	575 m	
	12+00E	19+00N to 25+00N	600 m	
	13+00E	19+00N to 25+00N	600 m	
	14+00E	19+00N to 25+00N	600 m	
	16+00E	19+00N to 25+00N	600 m	
В	10+00E	17+00N to 25+75N	875 m	
	11+00E	17+00N to 25+50N	850 m	
	12+00E	17+00N to 25+00N	800 m	
	13+00E	17+00N to 25+50N	850 m	
С	9+00N	16+50E to 22+00E	550 m	
	10+00N	16+50E to 22+00E	550 m	
	11+00N	16+50E to 22+75E	625 m	
	12+00N	16+25E to 22+75E	650 m	
	13+00N	16+50E to 21+75E	525 m	
	14+00N	16+50E to 21+25E	475 m	
D	10+00N	23+75E to 33+00E	925 m	
	11+00N	23+75E to 33+00E	925 m	
	12+00N	23+75E to 33+00E	925 m	
		total	13.1 km	

The GENIE survey was carried out using a 100 m transmitter to receiver coil separation. This separation limits the depth of investigation to about 50-75 m, however it provides finer resolution of multiple conductive horizons as expected from the airborne EM








data. The standard frequencies of 337.5, 1012.5 and 3037.5 Hz were recorded at a reference frequency of 112.5 Hz. The response ratio $(V_{sig}/V_{ref}-1) \times 100\%$ was manually recorded at each station and at the end of each survey day input to a computer. Repeat readings were taken at some stations to ensure low noise data quality. Stations were taken every 25 m along the grid lines.

The VLF-EM survey was presumable carried out using normal VLF survey procedures (Paterson and Ronka, 1971). Annapolis (21.4 kHz) was used for the surveys of grids A and B, Seattle (24.8 kHz) was used on grids C and D.

DATA PRESENTATION AND INTERPRETATION:

The VLF-EM data are plotted as line profiles on separate maps for each grid area (Maps A1, B1, C1 and D1). Both the in-phase and quadrature data are plotted on a common scale of 10%/cm, except for grid C where larger responses necessitated plotting at 20%/cm. The in-phase components have also been spatially filtered (Fraser, 1969) to transform cross-overs and inflections to peaks which can be contoured for visual presentation (Maps A2, B2, C2 and D2) and lineto-line correlation. The VLF-EM profile plots are interpreted by locating conductors at points of maximum inflection and then interpolating between lines with the aid of the Fraser filter contour plots. The interpreted conductors are the transferred onto the Fraser filter plots for comparison purposes.

The GENIE data are plotted relative to station location (defined as

the mid-point between the transmitter and receiver) to form response profiles on four separate maps of the grid areas (Maps A3, B3, C3 and D3). Each frequency is plotted as a separate profile combined on a common profile plot. All profiles are plotted at the same scale of 25%/cm.

Conductors are located at the centres of negative anomalies or half a coil separation from the positive to negative cross-overs. In some cases, where a wide negative response is observed, only a wide zone of multiple conductors or conductive overburden can be identified rather than interpreting individual conductors. Large positive responses can be caused by shallow flat-lying conductors, or by two conductors spaced about one to two coil separations apart, or by a strongly magnetic unit.

Where an anomaly from an individual conductor can be isolated, it is possible to determine the dip of the conductor from the relative amplitudes of the positive shoulders, the depth of the conductor from the amplitude of the negative peak, and the conductivity-thickness product (conductance) from the relative responses on the three frequencies (Johnson and Doborzynski, 1986). These estimates are subject to considerable error due to factors outlined in the previous section. Additional survey data are required at smaller coil separations in order to make an unequivocal interpretation.

DISCUSSION OF RESULTS:

Strong anomalous responses are observed on all grids with both the VLF-EM and the GENIE surveys. For the most part, the VLF-EM results duplicate the GENIE data indicating that most of the anomalies are due to relatively large conductive structures with significant strike length and depth extent. In some areas, broad anomalous responses are interpreted as wide zones of multiple conductors, however, attempts have been made to identify individual conductors within these zones.

<u>Grid A</u>

A 200-300 m wide zone of multiple conductors and/or conductive overburden is interpreted in the central portion of the survey grid from the large amplitude anomalous GENIE responses on all lines. (In places the response is so large that it has pegged off-scale on the highest frequency at about 100%). This anomalous GENIE response is most likely due to very shallow, closely spaced conductors within a broader, generally conductive formation.

There are surprising few strong VLF-EM anomalies in this area, however there does appear to be a broad response with both the inphase (dip angle) and quadrature VLF-EM components suggesting conductive overburden. Shallow, closely spaced multiple conductors might produce a similar VLF-EM response.

A large amplitude, coincident GENIE and VLF-EM anomaly in the

northern part of the grid is due to a large conductive sheet buried at shallow depth. The large size of this conductor, and it relatively high conductivity-thickness product of 10 to 30 mhos (Siemens), suggests a conductive stratigraphic horizon, possibly graphitic.

<u>Grid B</u>

Numerous individual conductors have been interpreted from the variety of anomalies observed in the GENIE survey data. The conductors are at various depths and have widely ranging conductances from less than 5 mhos to over 30 mhos. There is close correlation between the VLF-EM results and the GENIE data, indicating that the conductors are dominantly caused by large conductive formations.

The strongest response is due to a pair of very shallow conductors, which may be part of a wider, multiple conductive zone, at about 20+00N. These conductors also dominate the VLF-EM results and are most likely due to an extensive graphitic formation.

Most other GENIE anomalies, although not as strong as the dominant response, have coincident VLF-EM anomalies. The most notable exceptions are the GENIE conductors at about 22+25N on lines 12+00E and 13+00E, and at 18+00N on lines 10+00E and 11+00E. The first conductor has a coincident VLF-EM anomaly on line 13+00E but not on line 12+00E, possibly because it is much deeper beneath line 12+00E. The conductor at about 18+00N on lines 10+00 and 11+00E has a weak VLF-EM response however it is displaced about 25-50 m to the south. The apparent absence of a VLF-EM response from this GENIE conductor

may be related to the lower interpreted conductance and greater depth of this conductor.

<u>Grid C</u>

A wide zone of multiple conductors, similar to grid A, has been interpreted in the central portions of grid C from the broad, largeamplitude GENIE responses in this area. However, in this case, individual conductors can be definitively interpreted from the shape of the response profiles. These conductors are shallow, and have high conductances. Also, there is a very clear correlation between these conductors and anomalous VLF-EM responses. The interpretation is similar to grid A: the conductors are probably due to graphitic horizons of considerable strike length and depth extent, within a generally conductive formation.

Two conductors have been inferred in the western corner of the grid from weak GENIE responses. These possible conductors have no VLF-EM correlation and hence may be potentially better targets for follow-up investigation. However, the anomalous responses have only been partially recorded; additional data are required to the southwest to make a more definitive interpretation.

<u>Grid</u> D

Four separate conductors are interpreted from the GENIE data from grid D, however the two most easterly conductors at about 29+50E and

31+25E are so weak that they can only be classified as inferred. The strongest anomalous response is due to a conductor with a very high interpreted conductance of 20-60 mhos at about 27+75E. This conductor has only a weak in-phase VLF-EM correlation, which implies that it is more likely due to a conductor of limited depth extent and strike length. The quadrature VLF-EM is very large and negative, indicating that the conductor is partially buried beneath conductive overburden. All other GENIE conductors have closely coincident VFL-EM anomalies implying that they are more likely caused by large conductive horizons possibly graphitic.

CONCLUSION AND RECOMMENDATIONS:

The horizontal loop EM survey of four selected grid areas on the Mass property using the GENIE reconnaissance electromagnetic system has successfully located a variety conductors ranging in depth from near surface to over 50 m, and ranging in conductivity-thickness product (conductance) from less than 5 mhos (Siemens) to over 50 mhos. Many of these conductors occur within wide conductive zones which have been interpreted to be due to shallow, multiple conductive horizons within generally conductive formations. In some areas, particularly at grid A, individual conductors are not entirely resolvable from the current data set, which was collected using 100 m coil separation. A follow-up survey with 50 m coil separation is required to make a more definitive interpretation.

Most of the conductors which could be clearly identified from the

GENIE data have coincident VLF-EM anomalies. This implies that the conductors are large structures with considerable strike length and depth extent. The most likely causes of such conductors are graphitic stratigraphic horizons. A few GENIE conductors have poor or no VLF-EM correlation and hence should receive highest priority for follow-up ground truth by trenching or drilling. These conductors are (in order of priority):

- 1) grid D, lines 10+00N to 12+00N, 27+75E
- 2) grid B, lines 10+00E and 11+00E, 18+00N
- 3) grid C, lines 13+00N and 14+00N, 17+50E (may require additional GENIE data to the west to confirm)

Where the conductor is interpreted to be at a depth of 5 m or less, an attempt should be made to expose the conductor by trenching. Deeper conductors should be drill tested using dip information from the GENIE profiles where available, or inferred geologic dips if not available, to control the drill location and direction. All other shallow conductors should be investigated by trenching if practical.

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Paterson, N.R, and Ronka, V.: Five years of surveying with the very low frequency - electro magnetics method; Geoexploration, vol.9, pp. 7-26, 1971.

STATEMENT OF QUALIFICATIONS:

NAME: WOODS, Dennis V.

PROFESSION: Geophysical Engineer

- EDUCATION: B.Sc. Applied Geology, Queen's University, 1973
 - M.Sc. Applied Geophysics, Queen's University, 1975
 - Ph.D. Geophysics, Australian National University, 1979

PROFESSIONAL Registered Professional Engineer, #15745 ASSOCIATIONS: Province of British Columbia

> Active Member, Society of Exploration Geophysicist Canadian Society of Exploration Geophysicist Australian Society of Exploration Geophysicist

EXPERIENCE:

- 1971-79 Field geologist with St. Joe Mineral Corp. and Selco Mining Corp. (summers)
 - Research graduate student and teaching assistant at Queen's University and the Australian National University
- 1979-86 Assistant Professor of Applied Geophysics at Queen's University
 - Geophysical consultant with Paterson Grant & Watson Ltd., M.P.H. Consulting Ltd., James Neilson & Assoc. Ltd., and Foundex Geophysics Inc.
 - Visiting research scientist at Chervon Geosciences Ltd., Geological Survey of Canada, and the University of Washington
- 1986-89 Project Geophysicist with Inverse Theory & Applications (ITA) Inc.
 - Chief Geophysicist at White Geophysical Inc.
 - Chief Geophysicist at Premier Geophysics Inc
- 1990- President of Woods Geophysical Consulting

Transmitter	
Transmitting Element	Iron-cored coil for each frequency
Transmitting Frequency Pairs	Five pairs. 112.5 Hz reference with one of 337.5, 1012.5 or 3037.5 Hz; or 337.5 Hz reference with one of 1012.5 or 3037.5 Hz.
Transmitting Moments	150 Am^2 at 112.5 Hz, 100 Am^2 at 337.5 Hz, 50 Am^2 at 1012.5 Hz, 25 Am^2 at 3037.5 Hz.
Relative Amplitude Stability	Better than 0.1%
Power Supply	Rechargeable Nickel-Cadmium batteries; 2 options available, Light and Heavy Duty.
Power Supply Endurance	Light duty pack: 2 hours continuous at 20°C. Heavy duty pack: 3½ hours continuous at 20°C.
Operating Temperature Range	-30°C to +50°C
Storage Temperature Range	-40°C to +50°C
Total Weight with Batteries	Light duty configuration: 14 kg Heavy duty configuration: 16 kg
Dimensions	Height: 820 mm; Width: 380 mm; Depth: 180 mm
Receiver	
Receiving Element	Iron-cored coil
Receiving Frequency Pairs	Same as transmitter
Transmitter-Receiver Separation	Primary selector: 6.26 m, 12.5 m, 25 m, 50 m, 100 m, 200 m plus Multiplier: x 1, x 1.25, x 1.5, x 1.75

Maximum Transmitter-Receiver Separation	200 m under most conditions. Greater separations may be-possi- ble depending on atmospheric and power line noise.
Power Line Filtering	Internally switch selectable at 60 or 50 Hz and 3rd harmonic.
Signal Averaging Time	Switch selectable at 2, 4, 8 or 16 seconds.
Resolution of Ratio Display	0.1%
Power Supply	Rechargeable Nickel-Cadmium batteries
Power Supply Endurance	20 hours continuous at 20°C
Operating Temperature Range	-30°C to +50°C
Storage Temperature Range	-40°C to +50°C
Total Weight	6 kg
Console Dimensions	Length: 300 mm; Height: 230 mm; Depth: 160 mm
Coil Dimensions	Length: 500 mm; Diameter: 45 mm
Battery Charger	
Power Requirements	115 V or 230 V, 50 Hz or 60 Hz, 50 VA
Charging Time	7 hours for completely discharged batteries, subsequent automatic trickle charging. Transmitter and receiver batteries can be charged simultaneously.
Weight	4.5 kg
Dimensions	Length: 290 mm; Height: 150 mm; Depth: 130 mm

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EM16 SPECIFICATIONS

MEASURED QUANTITY	In-phase and quad-phase components of vertical magnetic field as a percentage of horizontal primary field. (i.e. tangent of the tilt angle and ellipticity).
SENSITIVITY	In-phase :±150%
	Quad-phase :± 40%
RESOLUTION	±1%
OUTPUT	Nulling by audio tone. In-phase indication from mechanical inclino- meter and quad-phase from a graduated dial.
OPERATING FREQUENCY	15-25 kHz VLF Radio Band. Station selection done by means of plug-in units.
OPERATOR CONTROLS	On/Off switch, battery test push button, station selector switch, audio volume control, quadrature dial, inclinometer.
POWER SUPPLY	6 disposable 'AA' cells.
DIMENSIONS	42 x 14 x 9cm
WEIGHT	Instrument: 1.6 kg Shipping : 4.5 kg











1200E 00E В 1001 2 2500N -2400N -2300N -2200N -2100N -7 ____ \subset 2000N -1900N - $\overline{}$, L 700E L 900E L 1100E L 1200E L 800E 1000E ÷ .

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WOODS GEOPHYSICAL CONSULTING





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GEOLOGICAL BRANCH ASSESSMENT REPORT Interpreted Conductor Inferred Conductor Conductive Zone (Multiple Conductors and/or Conductive Overburden) RIO ALGOM EXPLORATION INC. MASS PROPERTY - "A" GRID GENIE EM SURVEY - PROFILES L: 337 Hz, M: 1012 Hz, H: 3037 Hz (25%/cm) Scale 1: 2500.0 100 Date: Aug 1992 Survey: June 1992 WOODS GEOPHYSICAL CONSULTING















2500E 2600E 2800E 2400E 900E 27001 L 1200N L 1100N L 1000N 2400E 2700 290 ũõ









