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**GEOLOGICAL, GEOCHEMICAL AND GEOPHYSICAL
ASSESSMENT REPORT
ON THE
MT. ALCOCK PROPERTY**

Recreation Area Mining Division
NTS 94F/11
Latitude 57°40'N Longitude 125°24'W

OWNER: Teck Corporation
#600-200 Burrard Street
Vancouver, B.C.
V6C 3L9

**GEOLOGICAL BRANCH
ASSESSMENT REPORT**

22,787

S. Jensen
January 1993
Kamloops, B.C.

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SUMMARY

The Mt. Alcock property consists of the Cu and Cv mineral claims totalling 432 units. The property, situated within the Kwadacha Recreation Area, is located within the Rocky Mountains of northern B.C., roughly 300 kilometres northwest of Mackenzie.

The Mt. Alcock barite-hosted sulphide occurrence was discovered in 1977. The property was staked in 1989 in response to the provincial government's decision to open the recreation area for mineral exploration.

Teck's 1992 program consisted of 1:5,000 scale mapping with concurrent rock sampling. In addition, two grids were established and soil sampled, with a gravity survey carried out over selected portions of one grid. The purpose of the program was to test for an economic barite-hosted Zn-Pb massive sulphide deposit hosted within Devonian black shales. Mapping and soil, rock and stream sampling was concentrated within the black shales. The program was carried out between July 15 and August 31, 1992.

Regionally, the property is underlain by Upper Devonian to Ordovician fine grained basinal clastics and carbonates. Middle to Upper Devonian lower Earn Group black shales, cherts, and siltstones of the Gunsteel Formation underlie a majority of the area worked in 1992.

Mapping on the Nod Grid delineated a structurally offset, 800m x 25m zone of nodular barite. In addition, two areas (up to 700 metres strike length) of favourable pregnant shale lithology were identified.

Rock samples from the nodular barite and pregnant shale as well as poker chip shale and cherts, returned subeconomic base metal (Zn-Pb) values. A soil survey conducted over the Nod Grid did not return significant base metal results, only weak anomalies were outlined, the most interesting being coincident zinc (up to 1119 ppm Zn), lead (up to 484 ppm Pb) and associated sedex indicator elements (cadmium, manganese and vanadium) in an area underlain by pregnant shales between L43N and L44N.

A limited gravity survey carried out over three lines on the Nod Grid returned weakly encouraging results. The survey along L50N indicates a 0.2 milligal anomaly centered at 46+75E (edge of nodular barite outcrop) that could be caused by a 25m x 100m x 100m mass of density contrast and holds hope of a larger down dip extension of the nodular barite horizon. However, geological interpretation suggests the body is faulted off. Weak gravity anomalies, most likely attributed to density contrasts between siliceous and non-siliceous black shales, were identified on lines 44N and 38N.

Mapping within the Seep Grid identified laminated pyrite exposures hosted by pregnant and poker chip shales. Rock sampling of the pyritic black shales returned subeconomic base metal values. Highly elevated zinc (up to 12967 ppm Zn) values were returned from stream and iron-seep sampling in the Seep Grid area. However, associated lead values are low, likely indicating a fault source for the seeps and anomalies.

Soils collected from the Seep Grid outlined several coincident anomalous base metal (Zn-Pb) zones. Values up to 4672 ppm Zn and 857 ppm Pb were obtained with locally anomalous, and usually coincident, sedex indicator elements including cadmium, manganese, vanadium and silver. However, a majority of the anomalies are likely related to fault zones. Several of the anomalous zones remain unexplained.

Mapping on the northwest side of Warneford River revealed numerous exposures of nodular barite hosted by poker chip, distinctly laminated and pregnant shales. One area of massive barite was identified with over 350 metres of strike length uncovered. Rock samples collected from both the nodular and massive barite returned subeconomic base metal and associated sedex indicator element values.

Laminated pyrite within pregnant shales was identified in the Longwok Creek area. Rock samples returned subanomalous base metal values.

RECOMMENDATIONS

Additional work on the Mt. Alcock property should consist of:

- 1) Close spaced soils on the west side of the Seep Grid to better define the coincident lead-zinc soil anomaly.
- 2) Hand trenching favourable results from 1).
- 3) Diamond drill testing the gravity anomaly on L50N within the Nod Grid.

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1. INTRODUCTION

During 1992, a program of 1:5,000 scale geological mapping and grid soil sampling with concurrent rock chip sampling was carried out on the Mt. Alcock property. In addition, a limited gravity survey and stream and iron seep sampling was completed. The property was staked in 1989 in response to the provincial government's decision to open the recreat area for mineral exploration. The 1992 program was designed to evaluate the potential for an economic sedex Zn-Pb massive sulphide deposit.

1992 surveys were concentrated on favourable black shale stratigraphy, as outlined by Triumph Resources previous 1989 and 1990 work on the claims. Work was concentrated on a Devonian thrust slice located northeast of the main Mt. Alcock barite-sulphide showing.

This report describes the 1992 program and results.

2. LOCATION AND ACCESS (Figure 1)

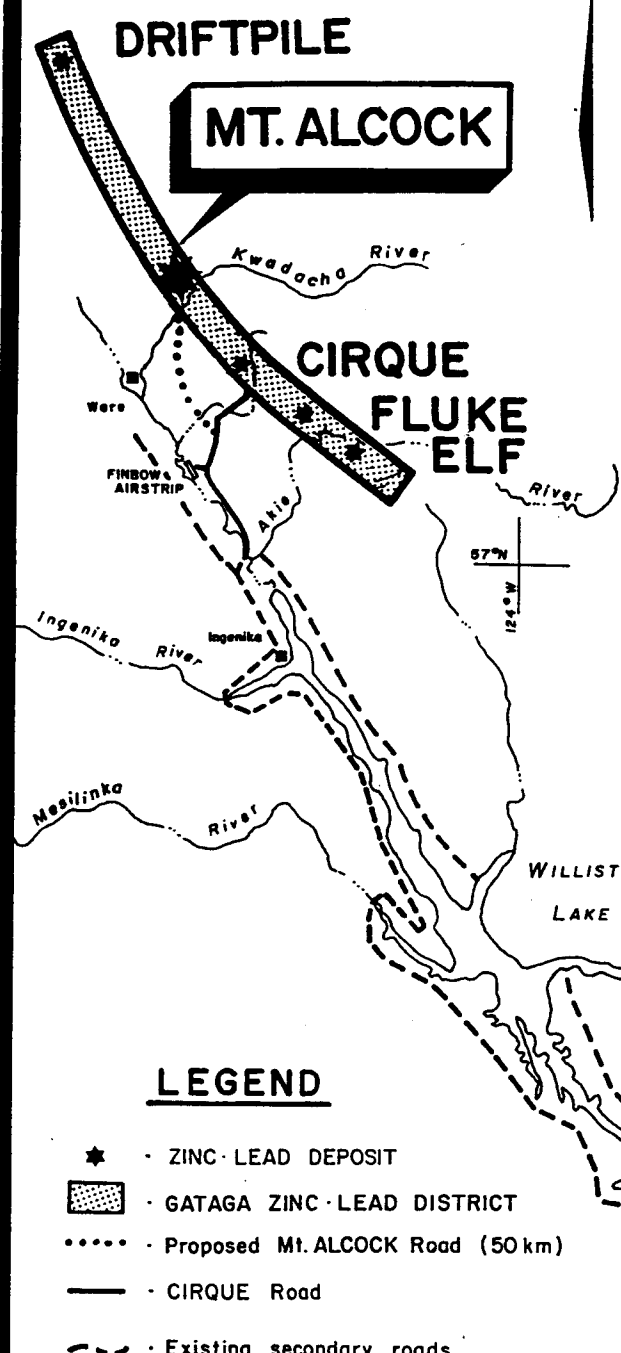
The Mt. Alcock property is located roughly 300 kilometres northwest of Mackenzie in northern British Columbia. The claims are situated within the western portion of the Kwadacha Recreation Area, approximately 25 kilometres northeast of Ft. Ware. The property is located on NTS map sheet 94F/11 with an approximate property centre latitude and longitude of 57° 40'N and 125° 24'W, respectively.

Access is via helicopter based locally at Finbow logging camp, located roughly 50 kilometres south of the property. Logistical support was provided by chartered fixed wing aircraft out of Mackenzie to the Finbow airstrip.

3. TOPOGRAPHY AND VEGETATION

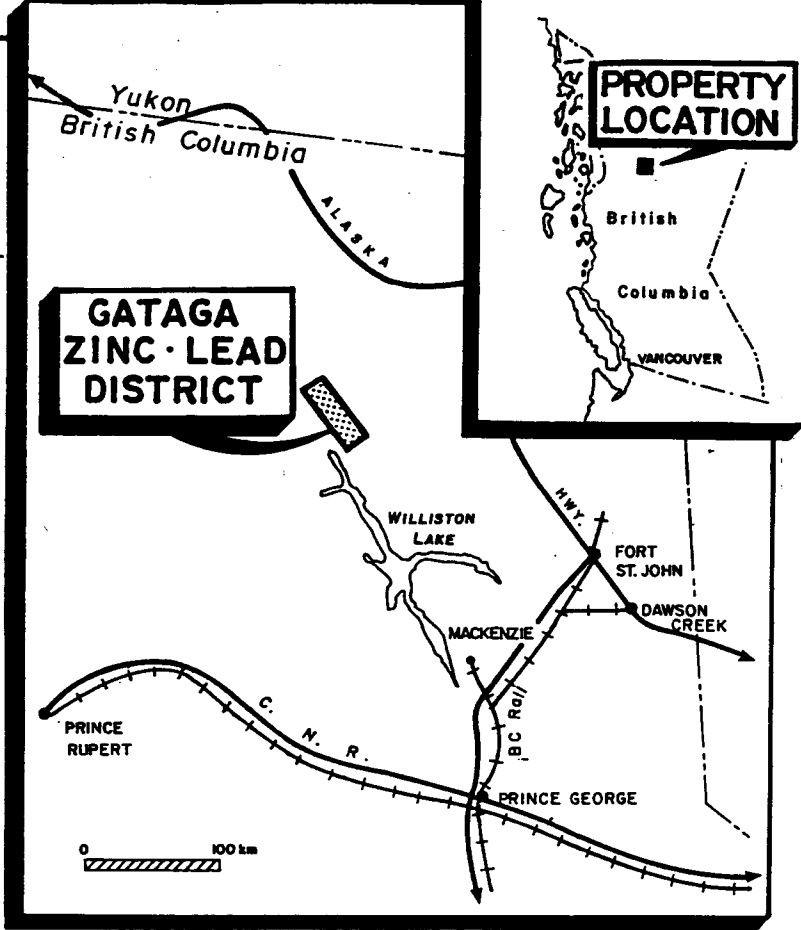
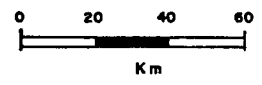
Topography is steep to moderate as the property is situated within the Muskwa Ranges of the Rocky Mountains. Elevations range from 2010 metres (6593 feet) on the slopes of Mt. Luke in the eastern claim area to 800 metres (2624 feet) at the confluence of the Kwadacha and Warneford Rivers located in the southwest corner of the property.

Vegetation is thick to open and consists predominantly of mature spruce and balsam. Underbrush is generally moderate and consists of alders, scrubbrush and burn. Moderate portions of the property area are covered by forest fire burns.



LEGEND

- ★ - ZINC-LEAD DEPOSIT
- - GATAGA ZINC-LEAD DISTRICT
- - Proposed Mt. ALCOCK Road (50 km)
- - CIRQUE Road
- - - - Existing secondary roads



PROPERTY LOCATION

TECK EXPLORATION LTD

LOCATION MAP

MT. ALCOCK PROPERTY

SCALE : 1 : 2,000,000 | FIGURE : 1

4. CLAIMS (Figure 2)

The property, located in the Recreation Area Mining Division, consists of the Cu and Cv mineral claims totalling 432 units ($\approx 10,800$ hectares). The claims are registered in the name of Teck Corporation and claims worked in 1992 were grouped into two, 96 unit groups as follows:

Nod Group: CV 5200 RAC, CV 5400 RAC, CU 5498 RAC, CU 5898 RAC, CU 5698 RAC, CU 5896

Seep Group: CV 5800 RAC, CV 5600 RAC, CU 6092 RAC, CU 6094 RAC, CU 6096 RAC, CU 6098 RAC

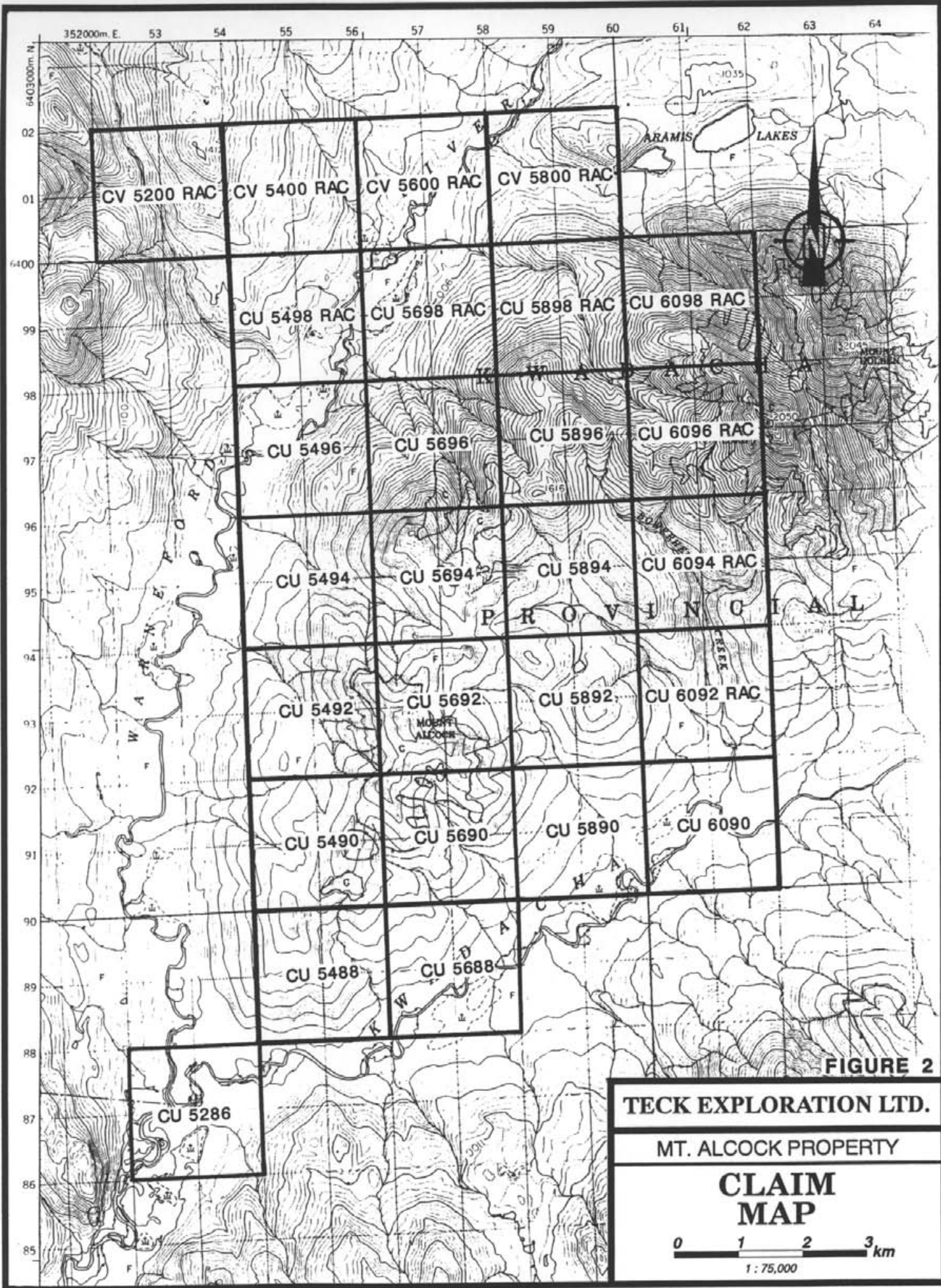
The following table lists all pertinent claim data.

TABLE 1
CLAIM RECORDS

Claim Name	Record No.	Units	Record Date	Expiry Date*
CU 5488	241394	16	June 27, 1989	June 27, 1996
CU 5490	241395	16	June 27, 1989	June 27, 1996
CU 5492	241396	16	June 27, 1989	June 27, 1996
CU 5494	241397	16	June 27, 1989	June 27, 1996
CU 5496	241398	16	June 27, 1989	June 27, 1996
CU 5688	241399	16	June 27, 1989	June 27, 1996
CU 5690	241400	16	June 27, 1989	June 27, 1996
CU 5692	241401	16	June 27, 1989	June 27, 1996
CU 5694	241402	16	June 27, 1989	June 27, 1996
CU 5896	241403	16	June 27, 1989	June 27, 1997*
CU 5890	241404	16	June 27, 1989	June 27, 1996
CU 5892	241405	16	June 27, 1989	June 27, 1996
CU 5894	241406	16	June 27, 1989	June 27, 1996
CU 5896	241407	16	June 27, 1989	June 27, 1996
CU 5286	241408	16	July 05, 1989	July 05, 1996
CU 6090	241416	16	Sept 28, 1989	Sept 28, 1996
CV 5200 RAC	307519	16	Feb 12, 1992	Feb 12, 1997*
CV 5400 RAC	307518	16	Feb 12, 1992	Feb 12, 1997*
CU 5498 RAC	307515	16	Feb 12, 1992	Feb 12, 1997*
CV 5600 RAC	307517	16	Feb 12, 1992	Feb 12, 1996*
CU 5698 RAC	307514	16	Feb 12, 1992	Feb 12, 1996*
CV 5800 RAC	307516	16	Feb 12, 1992	Feb 12, 1996*
CU 5898 RAC	307513	16	Feb 12, 1992	Feb 12, 1996*
CU 6092 RAC	307498	16	Feb 12, 1992	Feb 12, 1996*
CU 6094 RAC	307510	16	Feb 12, 1992	Feb 12, 1997*
CU 6096 RAC	307511	16	Feb 12, 1992	Feb 12, 1996*
CU 6098 RAC	307512	16	Feb 12, 1992	Feb 12, 1996*

Total = 432 Units

*Note= Expiry date based on acceptance of this report



5. PREVIOUS WORK and HISTORY

Regional exploration for sediment-hosted Pb-Zn in northeastern B.C. was generated in the late 1960's due to the recognition of clastic-hosted stratiform baritic sulphide deposits of the West German (Meggen and Rammelsberg) type in the Yukon (MacMillan Pass). The first major program in the Kechika Trough was conducted by Geophoto Consultants in 1970. Exploration was further intensified by the 1971 discovery of the carbonate-hosted Pb-Zn Robb Lake deposit. In 1974, Placer Development Ltd discovered several Devonian-aged barite-sulphide occurrences including Driftpile Creek (north of Mt. Alcock). The first major discovery, the Cirque (Stronsay) deposit, was made by Cyprus Anvil and Hudson's Bay Oil & Gas in 1977 and contains reserves in excess of 35 million tonnes averaging 10% (Pb + Zn) and 47 g/t Ag.

The Mt. Alcock barite-hosted sulphide occurrence was discovered in 1977 by Cyprus Anvil Mining Company. Grab samples from a 2-3m thick mineralized zone within the barite kill zone returned up to 14.8% combined Pb-Zn and 0.6 opt Ag.

In 1989, the Mt. Alcock area (part of the Kwadacha Recreation Area) was opened for mineral exploration with Triumph Resources, funded by Teck Exploration, becoming the successful bidder. During 1989, Triumph carried out a program consisting of mapping, prospecting, stream sampling; establishing and soil sampling a grid overlying the barite-sulphide showing; conducting 7 km of induced polarization survey over the same grid and testing the down-dip extension of the mineralized zone with nine diamond drill holes totalling 1111 metres. Drilling indicated the main showing area to be structurally complex with one of the best intersections containing 8.8 metres of 9.3% combined Zn-Pb (hole 89-3). Mapping and sampling within Devonian black shales northeast of the main showing revealed nodular barite zones as well as anomalous (Zn-Pb) drainages and soils.

In 1990, Triumph carried out a diamond drilling program totalling 1211.6 metres in six holes. The holes tested IP and geochemical targets (proximal to the main showing) and the down-dip extension of the main showing. No significant massive sulphide intercepts were obtained.

6. 1992 PROGRAM

In 1992, 87 mandays were spent on the Mt. Alcock property between July 15 and August 31. The program consisted of grid installation and soil sampling, a geophysical survey and 1:5,000 geological mapping with concurrent rock chip and stream sampling. Most of the work was carried out within Teck's newly staked claims.

A total of 741 soil samples on 21.5 km of grid line were collected on two grids; the Nod Grid and Seep Grid. Grid locations are shown on Figure 3. In addition, 57 rock chip, 29 moss mat, 5 silt and 6 iron seep samples were collected. A ground gravity survey was carried out over selected portions of the Nod Grid.

Mapping was done with topofil, compass and altimeter. Outcrop exposure on the property is variable, with most of the rock exposure provided along creek drainages.

7. GEOLOGY

A. Regional Geology (Figure 4)

The region (Gataga District) has been mapped on several occasions by the federal and provincial governments since the 1970's. The two most recent mapping projects are 'Geology of the Akie River Ba-Pb-Zn Mineral District' by D. MacIntyre of the B.C. MEMPR in 1981 (Preliminary Map 44) and 'Geologic Map of Ware (West 1/2) and Tooddoggone River Map-Areas' by H. Gabrielse of the Geological Survey of Canada in 1979 (Open File Report 483).

This work indicates the Mt. Alcock property area is underlain by Devonian to Ordovician clastic and carbonate rocks. Ordovician stratigraphy consists of black shales to siltstones of the Road River Group. These are unconformably overlain by Silurian Road River Group dolomitic siltstones and limestones. Lower to Middle Devonian limestones of the Road River Group unconformably overlie the Silurian strata. The youngest Devonian unit underlying the claims area is the Middle to Upper Devonian Gunsteel Formation black shales and cherts of the Earn Group. Cambrian sediments are fairly common proximal to the property area (Gataga district). The units (especially the Devonian and Silurian) outcrop in narrow

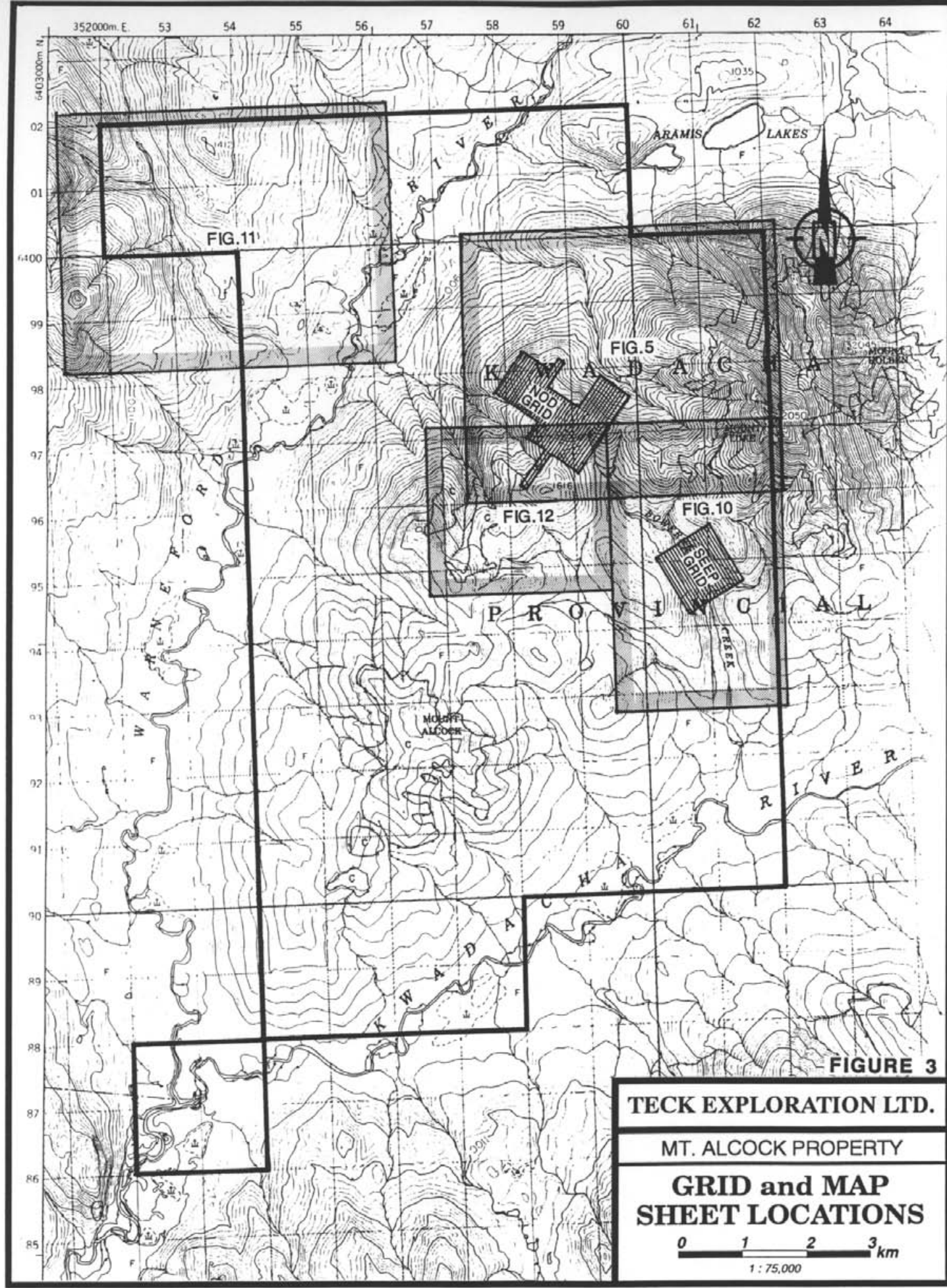


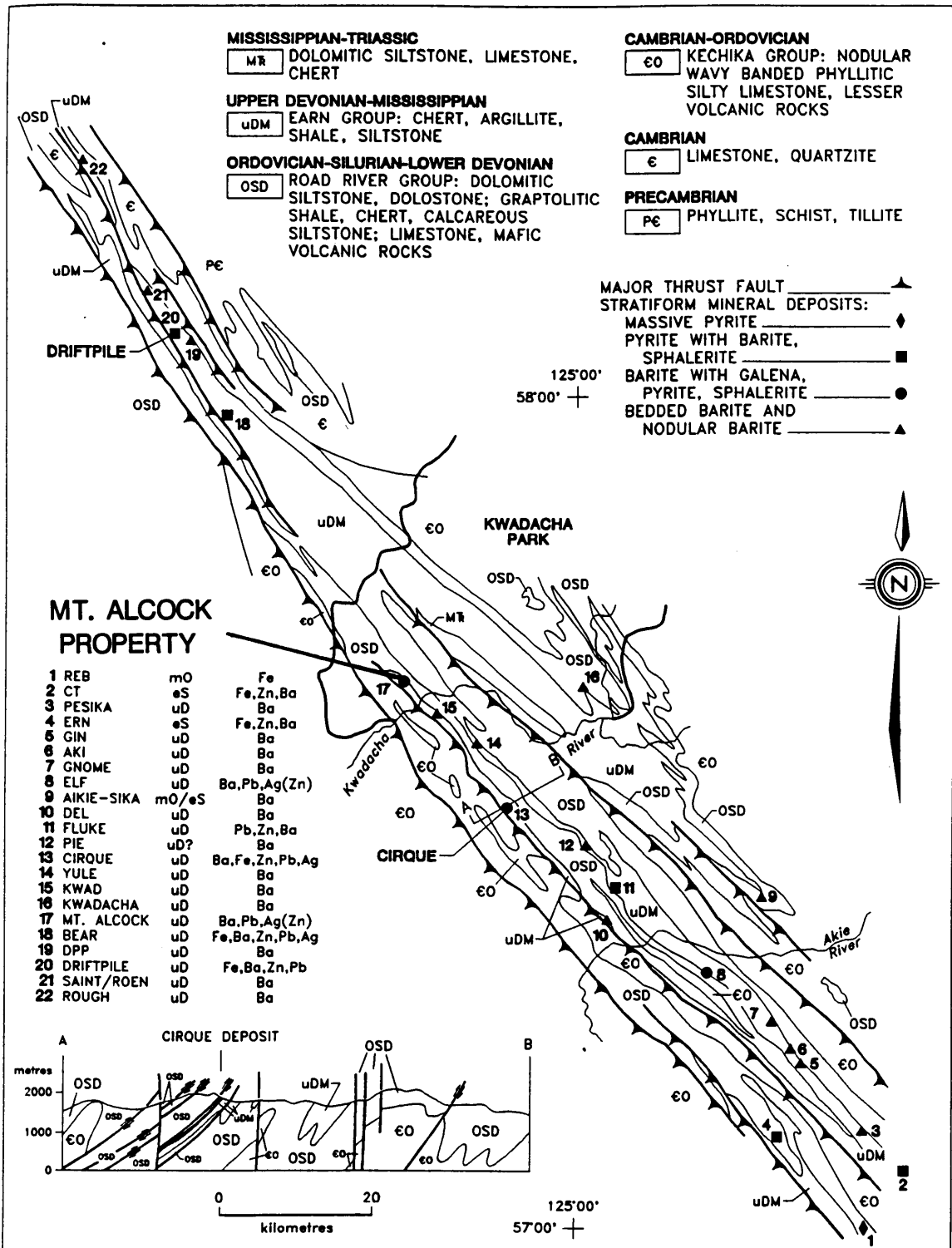
FIGURE 3

TECK EXPLORATION LTD.

MT. ALCOCK PROPERTY

**GRID and MAP
SHEET LOCATIONS**

0 1 2 3 km
1 : 75,000



FROM : MACINTYRE, 1983

TECK EXPLORATION LTD

MT. ALCOCK PROPERTY

REGIONAL GEOLOGY

SCALE : 1 : 800,000

FIGURE : 4

northwest-trending panels bounded by southwest-dipping thrust faults. Precambrian sediments are found 60 kilometres northeast of the Mt. Alcock claims.

Ordovician to Devonian sediments were deposited in structurally controlled, epicratonic extensional basins (Kechika Trough) that formed along the western margin of the miogeocline of ancestral North America. These Paleozoic and older sediments are bounded to the east and west by limestones and shallow water clastics of the Mackenzie and Cassiar Platforms.

The Gataga district is located within the western half of the Rocky Mountain Tectonic Belt and is dominated by the characteristic structural style of this fold and thrust belt. The western margin of this belt is the Rocky Mountain Trench, a zone occupied by a major strike-slip fault zone along which over 450 km of dextral displacement has occurred in Cretaceous or Eocene time (Gabrielse, 1984).

McClay and Insley (1986) recognized three phases of deformation in the district. The dominant deformation is northwest-striking, southwest-dipping and northeast-verging thrust-bounded packages of gently northwest and southeast-plunging chevron to tightly folded and cleaved strata. This was preceded by an earlier pre-thrusting and pre-main cleavage phase of asymmetric folding on northeast-trending fold axes. These phase one fold hinges contain local cleavage development. All thrusts have been subsequently rotated and steepened during continued deformation by movement on underlying thrusts. The third phase of deformation is late, northeast to east-striking dextral reverse kink-folding. This results in minor folds, dilatant vein systems and minor reorientation of existing structures.

The area surrounding the Mt. Alcock property is host to numerous barite-sulphide mineral showings or occurrences, including Driftpile Creek, Bear, Cirque, Fluke, Pie, Elf, Kwadacha and Sika. The mineral district is over 180 kilometres long and occurs within Devonian basinal facies rocks of the northwest-trending Kechika Trough. The sedex deposits are interpreted to have formed in local, fault controlled, third order basins within the larger epicratonic to intracratonic marine basins (Large, 1983).

B. Property Geology (Figures 5-12)

The immediate area covering the Mt. Alcock property can be divided into 5 major mappable units (Figures 5-12). All references to 'the claims' refers to the claims worked on by Teck in 1992; predominately the newly staked claims that were added along the eastern and northern edge of the existing claims, north and east of the main Mt. Alcock showing. Coverage of the separate map sheets is shown on Figure 3.

The oldest rocks underlying the property are Ordovician black shales and siltstones and Silurian dolomitic siltstones. The predominately Silurian sediments are mainly exposed within the eastern portion of the property; just east of the Seep grid, and are traceable north/northwest for 5-6km to the Aramis Lakes area. The Silurian and Ordovician rocks are in thrust contact with younger Devonian sediments. Ordovician and/or Silurian sediments are also exposed one kilometre southwest of the Seep grid area. Silurian rocks have been identified on the north side of Warneford River, 800 metres southwest of the northwest corner of the claims. Possible Silurian sediments have been identified along Longwok Creek, located two kilometres southwest of the Nod Grid.

A majority of the claims are underlain by Devonian Gunsteel Formation black shales, cherts, siltstones and limestones. Poker chip shale and porcellanite (chert) are the most common rock type, with lesser siltstones and limestones. Limestones are found primarily at the base of the Devonian section on the property, proximal to the thrust contacts with the older Ordovician and Silurian sediments.

Units 1 to 4 (Figures 5 & 6) are described individually.

Unit 1 : Ordovician Black Shale and Siltstone

The oldest Road River Group lithology found on the property is Ordovician black shales and siltstones. Grey to black shales range from totally non-siliceous (soft) to strongly siliceous and cherty. The shales can contain appreciable quantities of silt, as there is a continuum between the shales and siltstone. Carbonaceous black shales can be calcareous and strongly cleaved. Ordovician shales often contain characteristically abundant graptolites, especially in the more silty and muddy layers.

Unit 2 : Silurian Dolomitic Siltstone and Limestone

The Silurian Road River Group contains siltstones and limestones. Unit 2a is grey to beige bedded limestone, grey weathering, locally silty and a prominent ridge former.

Unit 2b is a characteristically orange weathering dolomitic siltstone. This ridge forming, locally micaceous, well bedded and grey colored unit is often calcareous and contains local, but uncommon graptolites. A characteristic of the Middle to Late Silurian unit is abundant burrow and grazing trail trace fossils.

Unit 3 : Lower to Middle Devonian Limestone

Unit 3 is a medium grey fossiliferous limestone. It is locally black and silty; usually as thin beds within the thicker bedded limestone. The unit is locally a limestone breccia or conglomerate with predominantly limestone clasts in a limestone to calcareous mud matrix. The fragmental nature is possibly related to debris flows off adjacent limestone reefs.

Unit 4 : Gunsteel Formation

This Middle to Upper Devonian Earn Group unit is comprised of 5 subunits.

Subunit 4a is porcellanite; a grey to black strongly to totally siliceous rock (chert). *This competent rock is often phyllitic and can possess a cleavage and megascopic folds.* It is often ribbon-banded; 3-5 cm black chert bands with $\leq 5\text{mm}$ black shale partings and laminations. The porcellanite is also commonly interbedded with poker chip shale.

A moderate to strongly siliceous black shale; pregnant shale, makes up subunit 4b. It is a carbonaceous, non-calcareous, silvery blue-grey weathering shale. It is a thick bedded, with beds ranging from 2-8cm (mode 4-6cm). It locally contains weak laminated and disseminated pyrite and often contains a fine stockwork of quartz veins. This subunit is distinguished from the other black shales by its thick bedding and moderately to strongly siliceous nature. This is the favourable unit to host barite-sulphide mineralization in the Gataga district.

Subunit 4c, distinctly laminated shale, is grey to black, somewhat silty shale with

distinct rhythmic 0.5-3cm laminations. It is non-siliceous and locally weakly calcareous. This subunit most likely represents a distal turbidite and is often interbedded with the poker chip shale. It can locally host nodular to massive barite.

The poker chip shale, subunit 4d, is a strongly cleaved, often phyllitic and locally graphitic dark grey to black shale. It is non to weakly siliceous (very soft) and silvery grey weathering. This carbonaceous, often folded and contorted, locally silty and non-calcareous subunit is often rusty and locally contains laminated and disseminated pyrite. It can be interbedded with the distinctly laminated shales and can host nodular to massive barite.

Nodular to locally massive barite, laterally equivalent to the poker chip and distinctly laminated shales, comprises subunit 4e. The nodular barite is comprised of spherulitic barite nodules ranging from 0.1-5mm in diameter with a 1-3mm modal size. The nodules are circular to ellipsoid depending on the degree of deformation and flattening. Nodular barite constitutes 15-60% of the rock mass and may represent pulled apart laminae of barite. The nodules are often concentrated in discontinuous wavy bands (up to 5mm wide) along bedding. Barite is also locally found as massive beds up to 3m wide. The poker chip and distinctly laminated shales host the nodular and massive barite. The barite nodules may represent the distal equivalent to the stratiform barite-sulphide deposits.

I. Nod Grid Area (Figures 5,6,7,8,9)

The Nod Grid area is underlain by the five subunits of the Devonian Gunsteel Formation (Figure 5). Poker chip shale is the most abundant rock type with moderate porcellanite and lesser pregnant shale, nodular barite and distinctly laminated shale exposure.

The general bedding is strikes 120°-150° and dips 30°-50° southwest. A prominent penetrative cleavage found in the shales roughly strikes the same as, or close to bedding, with dips ranging from 60°-80° to the southwest or northeast. Local variations (often in close proximity) in the bedding and cleavage attitudes are due to numerous antiforms, synforms and minor folds. This variation is reflected in the steronet analysis of the structural data. The poles to bedding and cleavage plot into two very loosely scattered groups; the more prominent cluster reflecting the general attitudes listed above and the less populous cluster

reflecting the northeast dipping limbs of the minor folds. The bedding/cleavage intersection lineations and minor fold axes plot roughly 10° – 290° .

The Nod Grid was established to cover exposures of nodular barite. Nodular barite, up to 25m wide on surface, outcrops intermittently southwest of the baseline from line L38N to L52N. The northwest-trending horizon can be traced almost continuously from L44N to L52N except at L49N where it is apparently offset by a dextral normal-slip fault. A cross-section of L50N depicts this relationship (Figure 7).

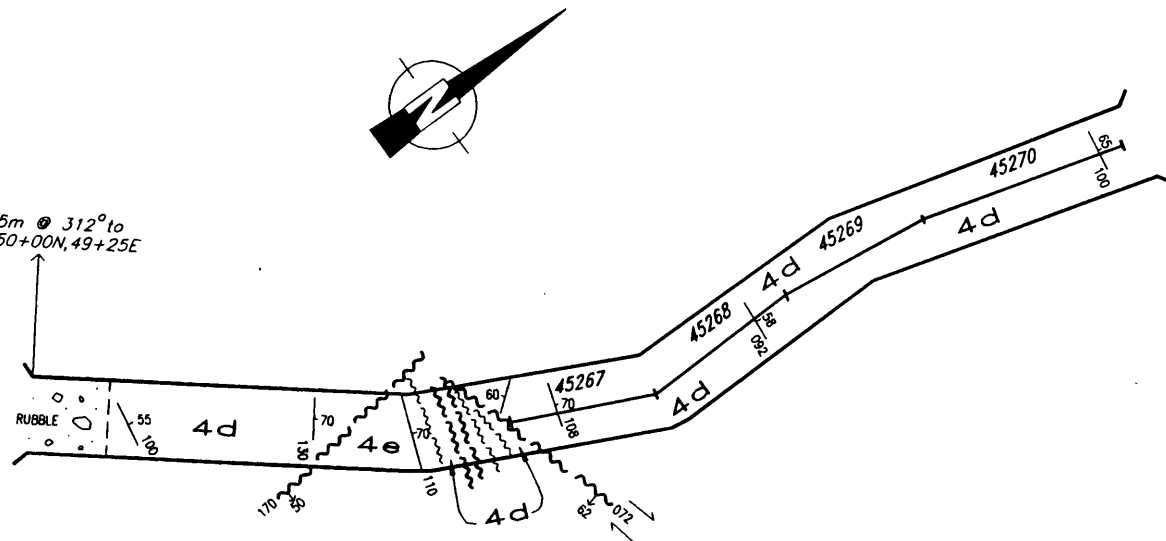
Approximately 100m northeast of the main nodular barite horizon lies a narrow and short exposure of nodular between L49N & L50N. Two small hand trenches seven metres apart, and totalling 25m in length, were constructed across the horizon (Figure 6). The barite is exposed up to 3m in width and appears to be fault controlled as the contacts of the barite with the poker chip shale in both trenches are fault zones and the horizon pinches out immediately along strike. This may be explained by the presence of a thrust fault as depicted in the cross-section along L50N (Figure 7). The rocks are consistently northeast-dipping and form the southern limb of a synform. A 600m exposure of barren pregnant shale occupies the axial trace of the synform.

A cross-section along L44N (600m southeast of L50N) further depicts the faulted and folded nature of the area (Figure 8). The favourable pregnant shale lithology is found along L44N from 43+00E to 44+50E and can be traced 700m northwest. It contains numerous small scale folds and faults. The pregnant shale horizon does not contain nodular or massive barite and appears to pinch out to the southeast. Nodular barite, up to 25 metres wide, is found within the poker chip shales and traceable northwesterly to L52N.

A small outcrop of nodular barite is located just off L38N, 46+00E. It is not traceable but appears to be the strike extension of the nodular barite horizon located to the northwest. A cross-section of L38N (Figure 9) indicates a uniformly dipping sequence of black shales and chert with no obvious folds and faults.

A long creek traverse carried out north of the Nod Grid revealed isolated outcrops of poker chip and pregnant shale and porcellanite. Approximately one kilometer north of the grid along a main drainage numerous outcrops of Lower Devonian grey, silty limestone were identified; usually adjacent to a major thrust fault.

25m @ 312° to
L50+00N, 49+25E



TRENCH A-NW

LEGEND

MIDDLE to UPPER DEVONIAN
LOWER EARN GROUP
GUNSTEEL FORMATION

4d POKER CHIP SHALE
4e NODULAR to MASSIVE BARITE

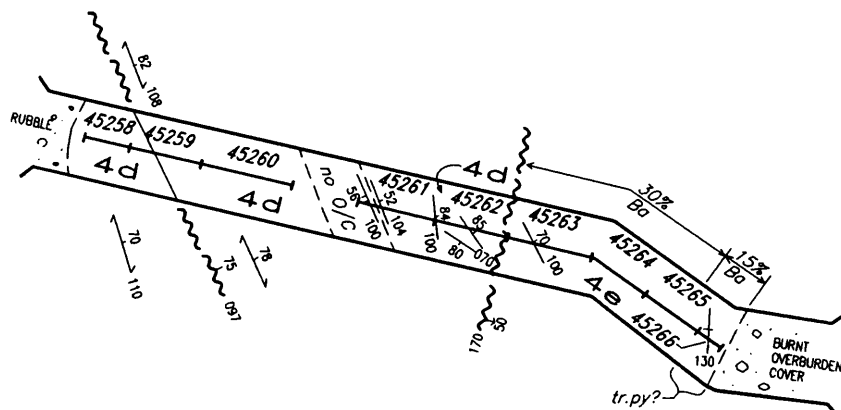
BEDDING
 FOLIATION

FAULT

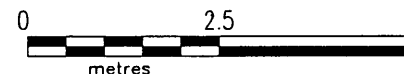
NOTE: TRENCH WIDTH EXAGGERATED

SAMPLE No	length(m)	Zn ppm	Pb ppm	Ag ppm	Fe %	Cd ppm	Ba ppm
45258	0.6	13	8	0.1	0.35	0.2	1707
45259	1.0	10	9	0.1	0.55	0.2	1830
45260	1.1	10	9	0.1	0.52	0.2	1337
45261	1.0	9	11	0.2	0.46	0.2	2124
45262	1.0	20	11	0.1	0.56	0.2	2734
45263	1.0	3	19	0.1	0.32	0.2	302714
45264	1.0	11	23	0.1	0.29	0.2	314099
45265	1.2	11	32	0.1	0.96	0.2	244827
45266	0.8	6	33	0.1	0.93	0.2	183598
45267	2.0	28	9	0.1	1.24	0.2	4026
45268	2.0	9	9	0.2	0.57	0.2	2008
45269	2.0	20	11	0.6	0.63	0.4	1923
45270	3.0	10	10	0.3	0.76	0.2	2959

FIGURE 6



TRENCH A-SE

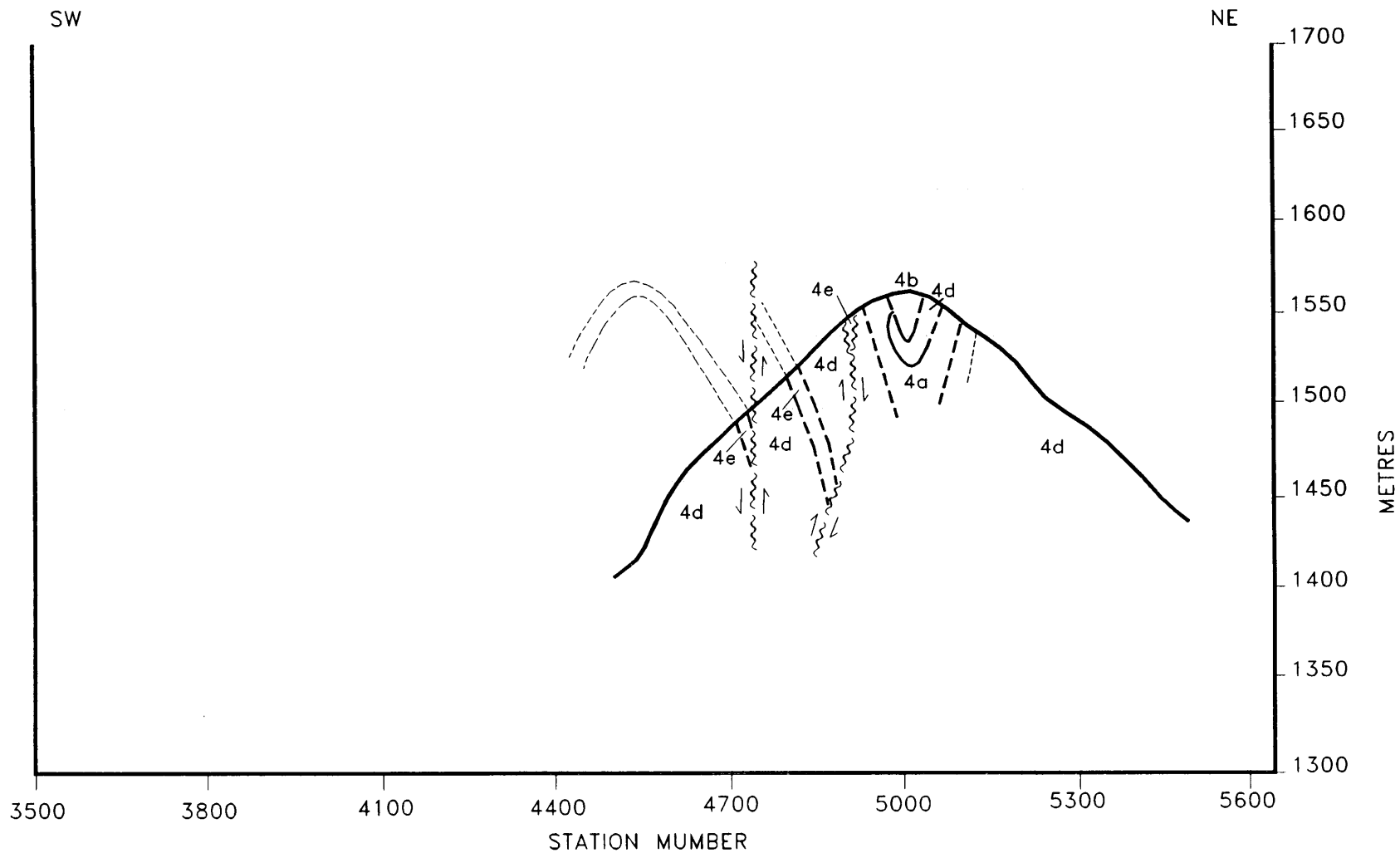


TECK EXPLORATION LTD.
KAMLOOPS, BRITISH COLUMBIA

MT. ALCOCK PROPERTY

NOD GRID
HAND TRENCHES
Geology & Geochemistry

DATE DRAWN: FEB. 2, 1993	SCALE: 1:100	DWG. NAME:
COMPILED BY: R.F.	JOB No: 1715	ALC-TR1
DRAWN BY: S.A.	NIS No: 94F/11	



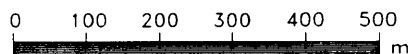
GEOLOGY

MIDDLE to UPPER DEVONIAN
LOWER EARN GROUP
GUNSTEEL FORMATION

- 4e** NODULAR to MASSIVE BARITE
- 4d** POKER CHIP SHALE
- 4c** DISTINCTLY LAMINATED SHALE
- 4b** PREGNANT SHALE
- 4a** PORCELLANITE (CHERT)

SYMBOLS

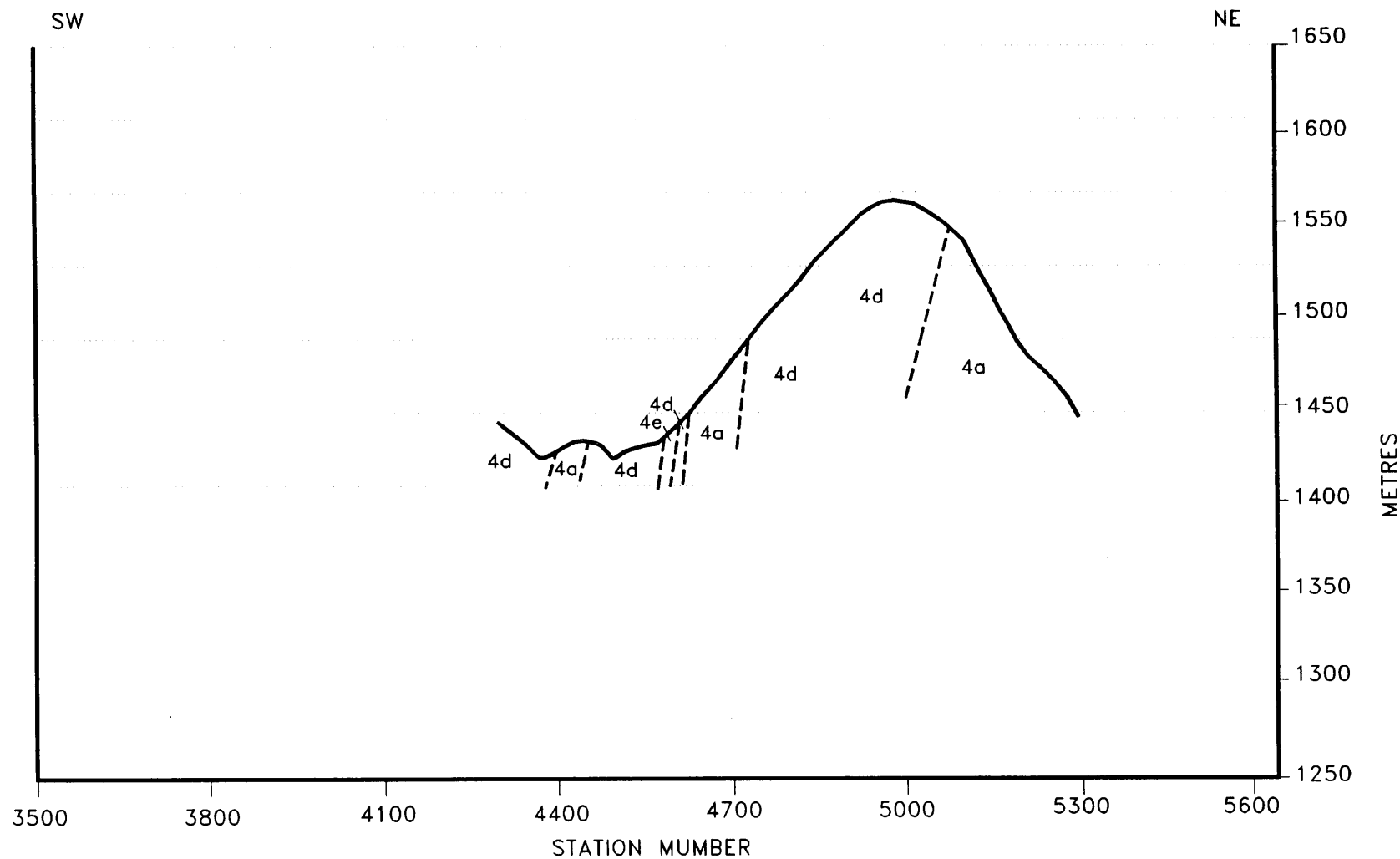
- GEOLOGIC CONTACT
- ~~~~~ FAULT



SCALE: 1:10,000 Vertical Exaggeration 3x

FIGURE 7

TECK EXPLORATION LTD. KAMLOOPS, BRITISH COLUMBIA		
MT. ALCOCK PROPERTY		
NOD GRID L 50+00 N CROSS-SECTION		
DATE DRAWN: FEB. 9, 1993	SCALE: 1:10,000	DWG. NAME:
COMPILED BY: R.F./S.J.	JOB No: 1715	ALC-L50
DRAWN BY: S.A.	NTS No: 94F/11	



GEOLOGY

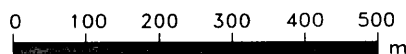
MIDDLE to UPPER DEVONIAN
LOWER EARN GROUP
GUNSTEEL FORMATION

- 4e NODULAR to MASSIVE BARITE
- 4d POKER CHIP SHALE
- 4c DISTINCTLY LAMINATED SHALE
- 4b PREGNANT SHALE
- 4a PORCELLANITE (CHERT)

SYMBOLS

--- GEOLOGIC CONTACT

~~~~~ FAULT



SCALE: 1:10,000 Vertical Exaggeration 3x

FIGURE 9

|                                                             |                 |            |
|-------------------------------------------------------------|-----------------|------------|
| <b>TECK EXPLORATION LTD.</b><br>KAMLOOPS, BRITISH COLUMBIA  |                 |            |
| MT. ALCOCK PROPERTY                                         |                 |            |
| <b>NOD GRID</b><br><b>L 38+00 N</b><br><b>CROSS-SECTION</b> |                 |            |
| DATE DRAWN: FEB. 9, 1993                                    | SCALE: 1:10,000 | DWG. NAME: |
| COMPILED BY: R.F./S.J.                                      | JOB No: 1715    | ALC-L38    |
| DRAWN BY: S.A.                                              | NTS No: 94F/11  |            |

## II. Seep Grid Area (Figure 10)

The Seep Grid covers part of a package of recently staked claims that cover the possible southeast strike extension of the nodular barite exposed within the Nod Grid area. Previous work by Triumph Resources outlined numerous zinc stream anomalies in an area just north of the Seep Grid. The Seep Grid area is underlain by Devonian shales, cherts and limestones. The most common lithology is poker chip shale with lesser porcellanite and pregnant shale. The main outcrop exposure is along Bowerheney Creek which roughly parallels the grid baseline. Rocks are quite folded and contorted as extreme strike and dip changes commonly occur over short distances. Stereonet analysis provided similar results as the Nod Grid area, with two scattered groups of pole plots to bedding and cleavages reflecting minor folding and contortion. The bedding/cleavage intersection lineation roughly plots at  $10^{\circ}$ - $300^{\circ}$ .

North of the grid along, Bowerheney Creek and a main tributary, poker chip shale and chert predominate with local beds of pregnant shale. Beds consistently strike northwest and dip southwest. Locally, the rocks are highly contorted possibly due to the presence of a major fault zone traceable two kilometres to the southeast.

At the north end of the grid baseline (L70N) and along Bowerheney Creek, a section of pregnant shale extends 400m southeastward along the creek to L66N. This area is host to a major iron seep. Extreme variations in bedding and cleavage are found within the shales. The contorted nature of the rocks is most likely due to the above mentioned major fault zone. Nodular barite was not discovered in the pregnant or poker chip shales in this area or in any area around the Seep Grid.

The southeast area of the grid contains locally abundant exposures of Devonian limestones and limestone fragmentals exposed in a 50m wide major reverse fault zone that trends  $125^{\circ}$ - $130^{\circ}$  and dips  $60^{\circ}$  to the southwest. Poker chip shales are exposed on either side of the limestones. The limestones are not traceable to the northwest and most likely pinch out against the fault. The fault zone is intermittently traceable two kilometres to the northwest and passes through the major iron seep. The fault zone probably continues to the southeast but no traverses were carried out in that area.

Silurian and/or Ordovician siltstones and silty limestones are found 300-500m east of

the Seep Grid and continue north 5-6 km's to the Aramis Lakes area (Figure 5). A thrust contact is assumed between the Devonian sediments of the Seep Grid and the Silurian and/or Ordovician sediments to the east. The assumed thrust contact between the Devonian and older sediments is intermittently traceable to the northern claim area, 5 kilometres to the northwest.

Approximately one kilometre southwest of the Seep Grid, a creek traverse identified Ordovician and/or Silurian silty black shales (Figure 10). The shales are different than any of the Devonian sediments identified within the property. Further downstream Devonian limy, silty black shales and limestones are exposed. A 100 metre exposure of pregnant shales are exposed just below the limestones and shales, along a main drainage.

### III. NW of Warneford River (Figure 11)

The northwest side of Warneford River covers the possible northeast strike extension of the nodular barite exposed on the Nod Grid. The area is underlain by all of the Devonian Gunsteel Formation subunits. Immediately west of the extreme western edge of the new claims lie two small outcrops of limy Silurian siltstone.

The area is similar to the Seep Grid area; a lot of outcrops are strongly contorted with major fluctuations in strikes and dips occurring over short distances, although the general attitude is again a northwest strike and southeast dip. This is again most likely the result of numerous minor folds and faults, common to the entire Mt. Alcock area.

The northern Warneford area is host to numerous exposures of nodular barite, usually occurring as narrow and local zones within the poker chip and distinctly laminated shale units. Unlike the Nod Grid area, nodular barite was found hosted by pregnant shales in two localities along a main creek drainage.

This area is also host to the only locality of massive barite found within the newly staked claims. The massive barite occurs over a strike length of 350m and is hosted within poker chip and distinctly laminated units. It grades, along strike, from massive barite 10+ metres in thickness at the north end to predominantly shale and silty shale at the southern end. The zone possibly continues to the northwest as massive barite float was found along a creek drainage 1.5km to the northwest. The area between the float and outcrops was not

prospected.

#### **IV. Longwok Creek and 1616 Peak Area (Figure 12)**

Traverses were carried out along Longwok Creek and creeks south of the 1616 Peak, roughly 1.5 kilometres southwest of the Nod Grid. These creeks contained previously outlined zinc stream anomalies. Upper Longwok Creek revealed abundant exposures of pregnant shale, often brecciated. Approximately one kilometre downstream, pregnant and poker chip shales are well exposed on the east side of the creek. A large outcrop along the west side of the creek, directly across from the pregnant shales, consisted of tan-weathering dark grey shale with local pyrite. It is not known whether the shale is part of the Devonian poker chip unit or the Silurian unit.

The area south of 1616 Peak is underlain predominately by poker chip shale. The overall strike and dip is consistent with the regional attitude; a northwest strike and a southwest dip. A minor synformal structure was identified within the poker chip shales along the southern part of the creek traverse. A 200 metre section of barren pregnant shale is exposed further upstream.

#### **V. Mineralization and Alteration**

*Fifty seven rock samples were collected during the 1992 Mt. Alcock program.* Samples were sent to Acme Analytical Laboratories Ltd. in Vancouver, B.C. and analysed for 29 elements by ICP (Ag,Al,As,B,Bi,Ca,Cd,Co,Cr,Cu,Fe,K,La,Mg,Mn,Mo,Na,Ni,P,Pb,Sb,Sr,Th,Ti,U,V,W,Zn) and Ba by whole rock ICP. In addition, 18 rock samples were analysed for whole rock geochem. A complete list of ICP, geochem Ba and selected geochem whole rock results are included in Appendix III, while rock sample descriptions are provided in Appendix V. Rock samples were 1m chips, where possible, and collected from black shales and cherts. Sample locations and selected results are shown on the respective geology and geochemistry maps; Figures 5,6,10,11,12.

Thirty-two rock samples were collected from the Nod Grid and immediate area. Sample locations and selected results are plotted on Figure 5. A majority of the samples were taken from nodular barite and associated footwall and hanging wall zones with whole rock analysis run on eighteen of the samples. The whole rock analysis shows the nodular

barite zones to be highly enriched in barium, highly anomalous in strontium and depleted in silica and aluminum. The nodular barite zones also contain very low zinc, lead and silver values. Two samples were collected from nodular barite exposed around L44N, 47+00E with sample 45206 returning the following results - 29.7% Ba, 1671 ppm Sr, 40.33% SiO<sub>2</sub>, 2.92% Al, 19 ppm Pb, 7 ppm Zn and 0.1 ppm Ag. The hanging wall and footwall results are nearly identical to each other with a typical result being 4671 ppm Ba, 62 ppm Sr, 77.14% SiO<sub>2</sub>, 11.19% Al, 19 ppm Pb, 34 ppm Zn and 0.3 ppm Ag (sample 45209; a footwall poker chip shale sample of the L44N nodular barite zone).

Similar results occur within the small nodular barite zone exposed by the two hand trenches (Figure 6). A chip through the nodular barite zone ran 31.4% Ba, 1251 ppm Sr, 38.45% SiO<sub>2</sub>, 2.44% Al, 23 ppm Pb, 5 ppm Zn and 0.1 ppm Ag (sample 45264) while a chip through the poker chip shale hanging wall returned 4026 ppm Ba, 51 ppm Sr, 85.43% SiO<sub>2</sub>, 5.19% Al, 9 ppm Pb, 28 ppm Zn and 0.1 ppm Ag (sample 45267).

Similar ICP results (whole rock analysis was not done) were obtained from poker chip shale footwall and hanging wall rock samples (#'s 45201, 45202, 45203, 45257) collected around the nodular barite exposed at 47+00E from L47N to L49N.

Three rock samples were collected from the favourable pregnant shale within the Nod Grid area. A sample from the pregnant shale exposed along the baseline returned weakly anomalous base metal and indicator element values. A sample (45254) collected from weakly pyritic pregnant shale exposed along L44N, 43+00E returned a weakly anomalous zinc value of 224 ppm Zn. A sample from the same pregnant shale zone located 650 metres to the northwest again returned a very weakly anomalous zinc value of 198 ppm Zn (sample 45202).

A chip sample (45205) through a poker chip shale with porcellanite bands, located 300m northwest of L48N-40+00E, returned one of the highest zinc values in 1992; 908 ppm Zn. The sample also returned anomalous sedex indicator element values of 13.1 ppm Cd and 235 ppm V. A rusty poker chip shale sample (45217) 200m northeast of baseline 50+00E and between L44N & L50N returned a weakly anomalous zinc value of 236 ppm Zn. Additional samples collected from poker chip shale and porcellanite within and proximal to the Nod Grid returned subanomalous base metal and sedex indicator element values.



The Seep Grid contained the most abundant pyrite found during the 1992 program. Sample locations and selected results are plotted on Figure 10. Laminated pyrite in bands up to 0.8cm wide were found in zones up to one metre wide within pregnant shales. No base metals were observed. The best exposures are along Bowerheney Creek within the Seep Grid and proximal to the major iron seep. Three samples were collected from the laminated pyrite zones and returned subeconomic base metal values.

A chip through rusty porcellanite located 500 metres south of the Seep Grid returned anomalous sedex indicator results of 10.3 ppm Cd and 174 ppm V (sample 45227). A chip across a rusty fault zone, 200 metres south of sample 45227, separating porcellanite and limestone returned the highest base metal values obtained during the 1992 program with sample 45275 returning 1787 ppm Pb, 2028 ppm Zn, 4.3 ppm Ag, 6.8 ppm Cd, and 164 ppm V.

A chip through a rusty chert with pregnant shale beds, located seven hundred metres north of the Seep Grid, returned anomalous values of 1051 ppm Zn, 7.3 ppm Cd and 143 ppm V. A similar sample (45229) 150 metres south returned subanomalous values from a weakly pyritic chert/pregnant shale.

Three rock samples collected from poker chip and pregnant shales located south of the 1616 Peak and one collected from a pyritic dark grey shale in upper Longwok Creek returned subeconomic base metal values. Sample locations and selected results are plotted on Figure 12.

A total of thirteen rock samples were collected from the northwest Warneford River area. Sample locations and selected results are plotted on Figure 11. The samples were collected predominantly from nodular barite zones within poker chip, distinctly laminated and pregnant shales. The nodular barite samples returned up to 26% barium (sample 45242) with no elevated base metal or sedex indicator element results returned from any of the samples. Two samples (45289 & 45290) were collected from massive barite; one from outcrop and one from float. Both returned very high barium (39% & 48% respectively) with subanomalous base metal results.

In summary, the sampled Devonian black shales ( $\pm$  barite) are not elevated in zinc, lead and silver and contain only local concentrations of stratiform pyrite. In addition, the shales were found to be silica-rich (averaging 75% to 85%  $\text{SiO}_2$ ), carbon-rich, iron-poor and enriched in barium (averaging 500-1000 ppm Ba) with respect to comparable pelagic sediments. This is consistent with the regional trend of the Gunsteel Formation rocks found in the Gataga district. Regionally, elevated base metal (Zn-Pb) values are found only very proximal to the barite-sulphide deposits in the Gataga district.

The abundance of nodular barite and local massive barite is a positive indicator of a favourable depositional environment for sedex deposits.

No significant alteration was noted within the black shales.

## 8. SOIL GEOCHEMISTRY (Figures 13-18)

Two soil grids were established and sampled during the 1992 program; the 'Nod Grid' and the 'Seep Grid'. Grid locations are shown on Figure 3. A total of 741 soils on 21.5 km of line were collected within the two grids. Samples were sent to Acme Analytical Laboratories Ltd. in Vancouver, B.C. and analysed for 29 elements by ICP (Ag,Al,As,B,Bi,Ca,Cd,Co,Cr,Cu,Fe,K,La,Mg,Mn,Mo,Na,Ni,P,Pb,Sb,Sr,Th,Ti,U,V,W,Zn) and Ba by whole rock ICP. Soil samples were collected using a shovel from the 'B' horizon, which generally occurred at a depth of 20-40 centimetres. All soils were collected in Kraft bags and allowed to air dry before shipment to the lab. Certificates of analyses are included in Appendix III and complete soil sample descriptions are provided in Appendix VI.

### A. Nod Grid

The Nod Grid covers nodular barite exposures within Devonian stratigraphy (Figure 5). Several anomalous zinc soil results from Triumph's previous work are located within the grid. Sixteen grid lines at  $045^\circ$  were established from L38+00N to L56+00N for a total distance (including the baseline) of 15.6 km. Eleven hundred metres of line were not soil sampled and established for use in the subsequent gravity survey. Lines are 100m apart, except for three 200m spaced lines, with samples collected every 25m (50m intervals on two lines) along the 500m to 1.5km long lines.

# I. Results (Figures 13-15)

Results from the Nod Grid geochemical survey including contour maps for zinc (ppm), lead (ppm) and barium (ppm) are shown on Figures 13,14 & 15, respectively. Contour intervals for zinc (750,1000 ppm) were determined by visual analysis of the data, the background value being roughly 200 ppm. The zinc geochemistry plot (Figure 13) reveals spotty anomalous zinc values. A six-point anomaly exists between L44N and L43N at 43+00E to 44+00E with values up to 1119 ppm Zn (L44N,43+50E). The anomalous zone corresponds to the location of favourable pregnant shale. Several one and two-point zinc anomalies exist along strike of the pregnant shale, 300 metres to the northwest along L47N, 42+75E to 44+25E. The maximum zinc soil value obtained during the survey was 6888 ppm Zn at 43+50E on L47N. Interestingly, the line between the anomalies (L46N) does not contain any elevated zinc soil values. Several one and two-point zinc soil anomalies are found north of the baseline between L40N and L43N. Spotty zinc values to 2312 ppm Zn are found within areas of little or no outcrop.

The soil geochemical plot for lead (Figure 14) is somewhat similar to zinc. Contour intervals (100,200,400 ppm) were again determined visually with a background of roughly 30-40 ppm lead. An anomalous zone (values up to 484 ppm Pb) exists between L44N and L47N at 43+00E to 44+00E. This correlates with the anomalous zinc zone and pregnant shales outlined above. The only other anomalous lead soil zone is found near the southern end of lines 45N to 47N. Values are only weakly anomalous and are located proximal to a stream with no outcrop located nearby.

Silver soil geochemical values are consistently low and contain local, weak anomalies usually associated with elevated zinc or lead values. As a result a silver soil profile map was not constructed.

Anomalous cadmium soil values and local clusters are associated with enhanced zinc values. Examples of this correlation include L47N , 43+50E - 36.9 ppm Cd and 6888 ppm Zn; L43N , 54+00E - 36.9 ppm Cd and 1740 ppm Zn; L56N , 49+50E - 52.9 ppm Cd and 759 ppm Zn. Due to the spotty nature of the anomalous cadmium soil values, a profile map was not constructed.

Manganese and vanadium soil values are similar to silver; there are local anomalies

throughout the grid, usually correlative with elevated zinc and/or lead values. Examples of this spotty association include L44N,43+00E - 822 ppm Mn & 125 ppm Pb; L44N,45+25E - 1591 ppm V & 936 ppm Zn; L47N, 43+50E - 649 Mn, 6888 ppm Zn & 455 ppm Pb; L46N,41+00E - 1052 ppm V & 1046 ppm Zn. Due to the spotty nature of manganese and vanadium values, profile maps were not constructed.

The barium geochemical plot is shown in Figure 15. Background barium values are consistently high (similar to high background barium found within the black shale rock samples) with a background value estimated at 1500 ppm Ba. Contour intervals were again estimated visually and determined to be 10,000 ppm and 100,000 ppm respectively. A main anomalous zone correlates quite well with the location of nodular barite outcrops. Barium soil values up to 14% Ba were returned. The anomalous zone extends from L44N to L50N around 43+00E and again from L49N to L54N centered around 48+00E. The offset in the anomaly corresponds to the assumed location of a dextral normal-slip fault. A three-point barium anomaly along L38N, 44+75E to 45+25E corresponds to outcropping nodular barite. Three one or two-point barium anomalies are found north of the baseline between lines 40N and 43N. They may be caused by local nodular barite zones (not found due to lack of outcrop) within black shales.

In summary, the most interesting base metal soil anomalies found within the Nod Grid are located between L43N and L44N. The coincident zinc and lead anomalous zone corresponds to favourable pregnant shale outcropping. In addition, sedex indicator elements including cadmium, manganese and vanadium are elevated within the same zone as the coincident zinc and lead. The strongly anomalous barium soil results are directly correlative with the exposures of nodular barite found within the grid.

#### **B. Seep Grid**

The Seep Grid covers the major iron-seep exposed along Bowerheney Creek and laminated pyrite found within pregnant black shales along the creek (Figure 10). In addition, zinc silt anomalies were identified upstream from the grid by previous workers. The grid is comprised of six, 1km long lines (L60+00N to L70+00N) for a total distance of 7.0km (including the baseline). A total of 245 soils were collected along the 060°-trending, 200m spaced lines.

# 1. Results (Figures 16-18)

Results from the soil survey conducted over the Seep Grid are encouraging. Zinc (Figure 16) and lead (Figure 17) anomalous thresholds were determined visually from the data. The background for zinc was roughly 300 ppm, thus contours of 500, 1000, 2000 and 4000 ppm were used. The background for lead was determined to be roughly 35 ppm and contours of 100, 200 and 300 ppm were utilized.

The zinc soil geochemical results outlined several anomalous zones (Figure 16). A large zinc anomaly exists from the east portion of L60N and trends northwest to L68N with values to 4716 ppm Zn. This anomaly may be explained by the large northwest-trending fault zone outlined by mapping (Figure 10). The zinc anomaly trends toward the eastern edge of L64N & L66N, 100-200 metres away from the main fault zone projection. This may be explained by the presence of secondary faults or splays. A three-point anomaly exists from L70N, 61+00E to L66N, 62+50E with a maximum value of 4586 ppm Zn at L68N, 61+25E. This zone is also most likely related to the above mentioned fault zone. A single point zinc anomaly exists at L60N, 62+25E (4672 ppm) and may be related to the fault zone. A weak zinc anomaly runs roughly parallel to B/L 60+00E from L60N to L66N. It overlies Devonian black shales, and more specifically, over pregnant shales containing stratiform pyrite from L68N to L70N.

Another anomalous zone in zinc is found from L60N at the B/L to L66N, 56+50E. Zinc values to 3377 ppm occur within this northwest-trending zone and may be related to a limestone - porcellanite contact zone. The contact is a fault zone 700 meters southeast of the grid with values of 1787 ppm Pb, 2028 ppm Zn, 4.3 ppm Ag, 6.8 ppm Cd, 164 ppm V and 3736 ppm Ba in a one metre rock chip (sample 45275). Although the fault zone was not identified within the Seep Grid, it may be the cause of the anomaly. Two additional zinc anomalies are outlined on the grid, a three-point anomaly between L60N, 57+75E to 58+00E and L60N, 55+75E and a three-point anomaly between L62N, 56+00E to 56+25E and L62N, 58+00E.

The lead soil geochemical profile identified several anomalous zones (Figure 17). The most prominent zone is coincident with the anomalous zinc zone from L60N at the B/L to L66N, 56+50E. Lead values to 349 ppm are outlined within the zone that may be related to a faulted limestone-chert contact zone. However, regionally, elevated lead values in the Gataga

area are favourable indicators of possible massive sulphide systems. Therefore, a possibility exists that the anomalous lead soil values could indicate a massive sulphide source intersected by a fault. The highest lead value (857 ppm) is a single-point anomaly coincident with the single-point zinc anomaly of 4672 ppm found along L60N at 62+25E. This coincident anomaly may be related to the main fault zone. Several other single-point weak lead soil anomalies were identified within the grid, two coincident with zinc anomalies. One anomalous lead sample was contained within the anomalous zinc zone trending along the baseline, the other at L62N, 58+00E.

The cadmium soil geochemical profile outlined several anomalous zones (Figure 18). Almost all of the anomalies are coincident with anomalous zinc zones. Other associated sedex indicator elements including manganese, vanadium and phosphorous are locally anomalous. The local highs of these elements (up to 0.634% P, 2950 ppm V, 2337 ppm Mn) as well as silver (up to 4.2 ppm) are almost directly correlative with elevated zinc and/or lead values. Therefore, individual soil profile maps of these elements are not constructed. The coincidence of anomalies is clearly demonstrated in the following soil locations; L60+00N, 62+25E - 857 ppm Pb, 4672 ppm Zn, 1.3 ppm Ag, 775 ppm Mn, 25.7 ppm Cd, 272 ppm V and 0.634% P; L62+00N, 56+25E - 30 ppm Pb, 2794 ppm Zn, 3.9 ppm Ag, 259 ppm Mn, 60.8 ppm Cd, 2455 ppm V and 0.185% P; and L62+00N, 63+75E - 42 ppm Pb, 4716 ppm Zn, 4.2 ppm Ag, 273 ppm Mn, 43.5 ppm Cd, 2950 ppm V and 0.151% P. In addition, locally elevated nickel (up to 934 ppm), strontium (up to 613 ppm) and iron (up to 10.62%) are associated with elevated zinc and/or lead. The barium soil values consistently range from 1000-4000 ppm Ba with a rough average of 1500 ppm. Local, sporadic anomalies (up to 47,669 ppm Ba) are found within the Seep Grid soil survey.

In summary, coincident zinc and lead anomalies are outlined within the Seep Grid. A majority of the anomalies are most likely related to northwest-trending fault zones. Several of the anomalies remain unexplained, including the coincident anomalous lead-zinc zone from L60N at the baseline to L66N, 56+50E. In addition, associated sedex indicator elements including cadmium, manganese, vanadium, phosphorous and silver are locally anomalous and almost always coincident with elevated zinc and/or lead values.

## 9. STREAM SAMPLES (Figures 5,10,11,12)

A total of 40 stream samples were collected, including 29 moss mat, 5 silt and 6 iron-seep. Samples were sent to Acme Analytical Laboratories Ltd. in Vancouver, B.C. and analysed for 29 elements by ICP (Ag,Al,As,B,Bi,Ca,Cd,Co,Cr,Cu,Fe,K,La,Mg,Mn,Mo,Na,Ni,P,Pb,Sb,Sr,Th,Ti,U,V,W,Zn) and Ba by whole rock ICP. Stream sample collection was concentrated in areas not previously sampled by Triumph Resources. Sample locations and Zn(ppm), Pb(ppm), Ag(ppm), Fe(%), Cd(ppm) and Ba(ppm) results are shown on Figures 5,10,11,12.

Only five stream samples were collected from the Nod Grid area as most of the drainages were previously sampled (Figure 5). One sample (M45251) was collected just east of L38+00N and returned low results. The remaining stream samples were collected northeast of the baseline between L42+00N and L50+00N. Values up to 1451 ppm Zn, 15.1 ppm Cd and 9380 ppm Ba were obtained indicating minor enrichment in barium and zinc.

Eight stream samples were collected in the immediate Seep Grid area with many more collected in the surrounding area (Figure 10). The Seep Grid is named for the major iron-seep that occurs along Bowerheney Creek between L68+00N and L70+00N. A sample from the spectacular iron seep (S45234) returned 12967 ppm Zn. Two minor iron-seeps located 200 metres upstream (S45230 & S45231) returned up to 4076 ppm Zn and 46.2 ppm Cd. However, associated lead and silver values for all three seeps are very low in addition to relatively low barium values (to 1928 ppm). Regional work carried out in the Gataga district since the 1970's has included numerous sampling of iron-seeps and concluded that unless there is associated elevated lead values the seeps are of little interest and probably related to fault zones. The iron-seeps that occur along Bowerheney Creek are most likely related to *faulting and the presence of a major fault zone through the area has been previously inferred.* Five additional moss mat stream samples collected in the grid and immediate area returned similar results (to 8923 ppm Zn, 92 ppm Pb, 39.2 ppm Cd and 5622 ppm Ba) and most likely are related to faulting. Sample M45249, collected from a tributary of Bowerheney Creek just upstream from the laminated pyrite exposures and draining the favourable coincident lead-zinc soil anomaly, returned the highest lead value, 92 ppm along with 1637 ppm Zn.

Four moss mats collected from streams draining Silurian to Ordovician stratigraphy east of the Seep Grid returned comparatively low zinc, lead, silver, cadmium and barium

results (Figure 10). A sample collected from an iron-seep (S45240) south of Aramis Lakes (4 kilometres north of the Seep grid and 3 kilometres northeast of the Nod grid) returned similar results (Figure 5).

Two moss mats were collected 700 metres south of the Seep Grid (Figure 10). Sample M45226, from Bowerheney Creek, returned 1055 ppm Zn, 30 ppm Pb, 6.4 ppm Cd and 16483 ppm Ba. A moss mat sample from a tributary of Bowerheney Creek (M45274) returned 2612 ppm Zn, 209 ppm Pb, 20.8 ppm Cd and 1958 ppm Ba. The sample was collected just downstream from a fault zone which returned strongly anomalous zinc and lead from a rock sample (45275). Thus the elevated lead in the moss sample is likely attributed to the upstream anomalous fault zone.

Four stream samples were collected south of the 1616 Peak area, 1.5 kilometres west of the Seep Grid and 2 kilometres south of the Nod Grid (Figure 12). A moss mat sample (M45219) collected from a tributary returned 13272 ppm Ba and likely reflects drainage from ground underlain by nodular barite, although not identified from mapping. Sample ST45221, a silt from another tributary returned a weakly anomalous 2072 ppm Zn and 18 ppm Pb. A sample from an iron-seep zone (3-4 total seeps) located just south of the 1616 peak returned 1021 ppm Zn but again very low lead, 2 ppm (S45225).

A silt and an iron seep sample were collected from upper Longwok Creek. The iron-seep (ST45273) returned high zinc (4283 ppm) but again returned a low lead (6 ppm) value (Figure 12).

Thirteen stream samples were collected from the northwest side Warneford River area; an area with no previous recorded sampling (Figure 11). Results of the stream sampling were mixed. Zinc values to 2712 ppm (M45237) were obtained, however associated lead, silver and sedex indicator elements were low, the maximum values obtained were 50 ppm Pb, 1.0 ppm Ag and 13.4 ppm Cd. Barium values are quite high as might be expected from the numerous nodular barite zones underlying the area. The maximum barium value obtained was 50763 ppm (M45248).

In summary, stream sampling conducted throughout the claims resulted in local anomalies in zinc and barium. The zinc anomalies, however, did not have corresponding elevated lead values except for moss mat M45249 collected from the Seep Grid and draining



the coincident anomalous lead-zinc soil zone. This was true of the iron-seeps, mosses and silts. In addition, the associated sedex indicator elements, including cadmium and manganese, were only locally and weakly anomalous.

#### 10. GRAVITY SURVEY - NOD GRID

A limited gravity survey (using a Lacoste & Romberg gravity meter) was carried out over selected portions of the Nod Grid. In total, 4.1 line-kilometres over three lines (L38+00N, L44+00N & L50+00N) were surveyed with readings taken every 25m. Appendix VII lists field procedures and specifications of the gravity and elevation surveys.

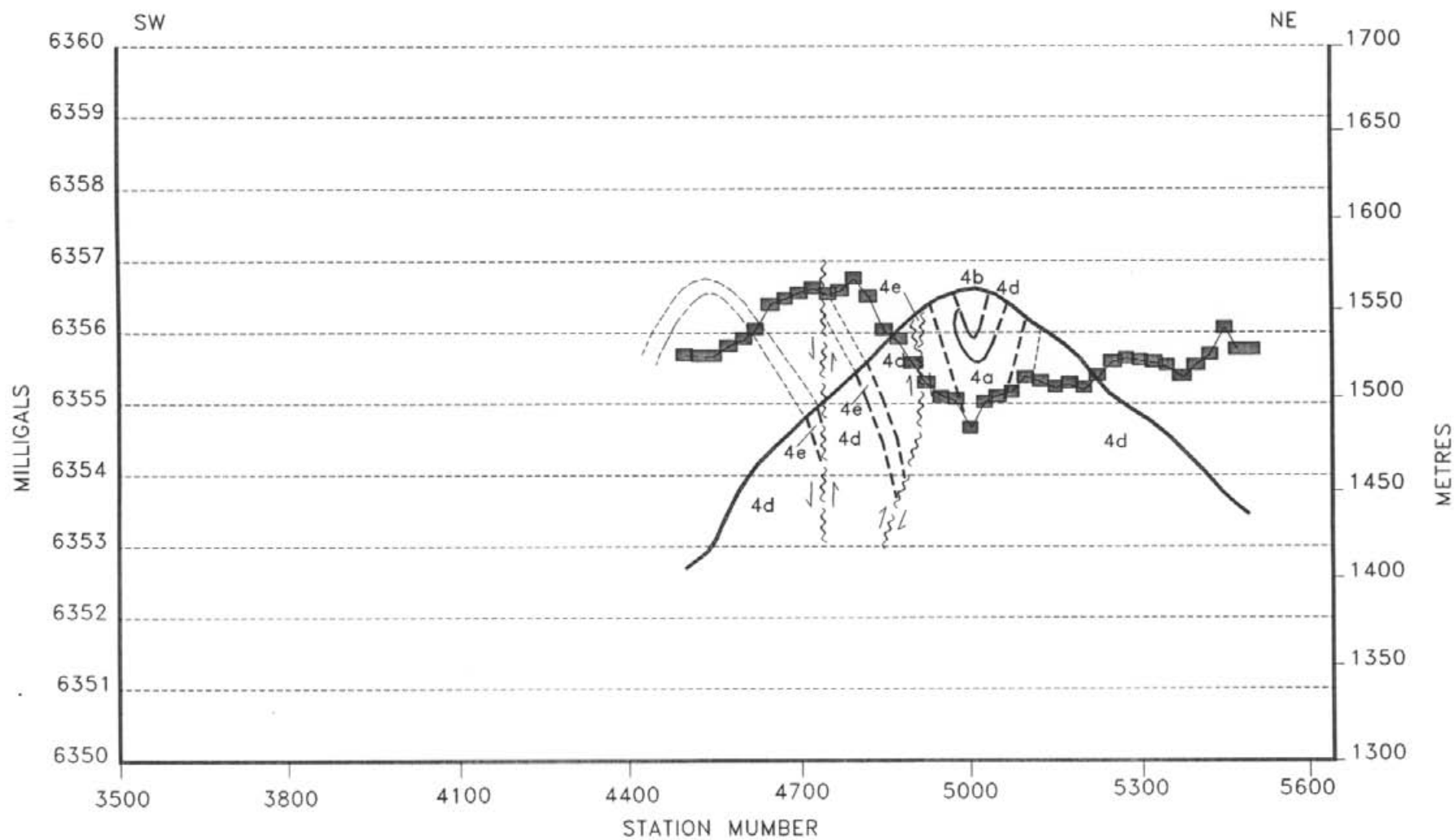
The following interpretations of the three lines were made by Al Wynne, geophysicist of Terra Surveys Ltd, who was contracted to interpret the gravity data. Assumed densities used were nodular barite 4.0 g/cc, pregnant shale 2.3 g/cc, black chert (porcellanite) 2.7 g/cc and poker chip shale 2.1 g/cc. Gravity line profiles along with accompanying geology are plotted on Figures 19, 20 and 21.

##### I. L50+00N (Figure 19)

"This line is quite short, making regional trends difficult to account for. It is possible to visualize an anomaly of about 0.75 milligals centered at 47+50E. However, comparison with L44+00N and replotting of the data at a vertical scale of 0.1 milligal/cm indicates two anomalies, 0.2 milligals at 46+25E-47+00E and a one point anomaly of 0.1 milligals at 48+00E."

"Computer modelling of these anomalies indicate the 46+25E-47+00E anomaly can be caused by a unit of density contrast 1.0 g/cc with dimensions of width 25m length 100m depth 100m. The anomaly at 48+00E can be related to a unit of density contrast 1.0 g/cc with dimensions of width 10m, length 100m, depth 100m."

"These anomalies correspond to the known nodular barite showings, however put stronger emphasis on the 46+75E showing. Keeping in mind that a larger anomaly is possible the depth extent of this anomaly may be greater than interpreted."



GEOLOGY  
MIDDLE to UPPER DEVONIAN  
LOWER EARN GROUP  
GUNSTEEL FORMATION

- 4e NODULAR to MASSIVE BARITE
- 4d POKER CHIP SHALE
- 4c DISTINCTLY LAMINATED SHALE
- 4b PREGNANT SHALE
- 4a PORCELLANITE (CHERT)

SYMBOLS

- BOUG @2.1
- GEOLOGIC CONTACT
- FAULT



SCALE: 1:10,000 Vertical Exaggeration 3x

FIGURE 19

TECK EXPLORATION LTD.  
KAMLOOPS, BRITISH COLUMBIA

MT. ALCOCK PROPERTY

NOD GRID  
L 50+00 N  
GRAVITY SURVEY

|                          |                 |            |
|--------------------------|-----------------|------------|
| DATE DRAWN: FEB. 9, 1993 | SCALE: 1:10,000 | DWG. NAME: |
| COMPILED BY: R.F./S.J.   | JOB No: 1715    | ALC-50G    |
| DRAWN BY: S.A.           | NTS No: 94F/11  |            |

## II. L44+00N (Figure 20)

"This regional line (2.1 km) is dominated by terrain effects over the crest of the knob centered within the grid. This effect could be compensated for, however, any very small deviations off the trend and would be masked. It is better to look at the raw data, keeping in mind the terrain effects. Both topographic highs and topographic lows effect the data by lowering the Bouguer values. Any short wavelength positive anomalies can be related to surface geology (the result of topographic corrections is to emphasize deep seated structures, ie. oil exploration)."

"The geology of the section consists of poker chip black shale with one thin section of pregnant shale and one thin section of black chert."

"The sections of pregnant shale and black chert exhibit residual anomalies of about 0.75 milligals, indicating positive density differences from the poker chip shale of about 0.4 g/cc."

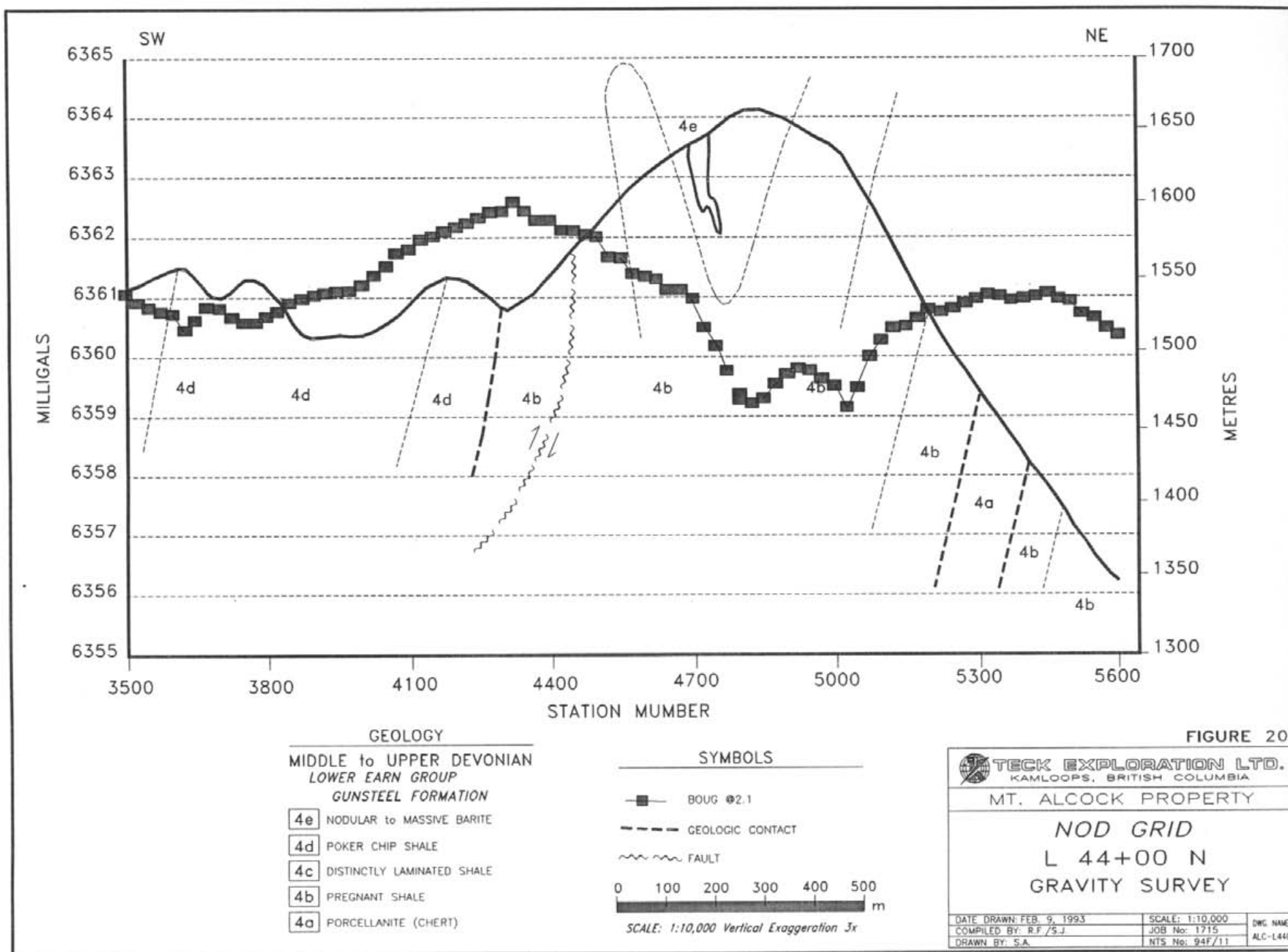
"The nodular barite showing has a signature of less than 0.1 milligals and would not be located without prior knowledge. This indicates very limited extent as the density contrast should be about 1 g/cc."

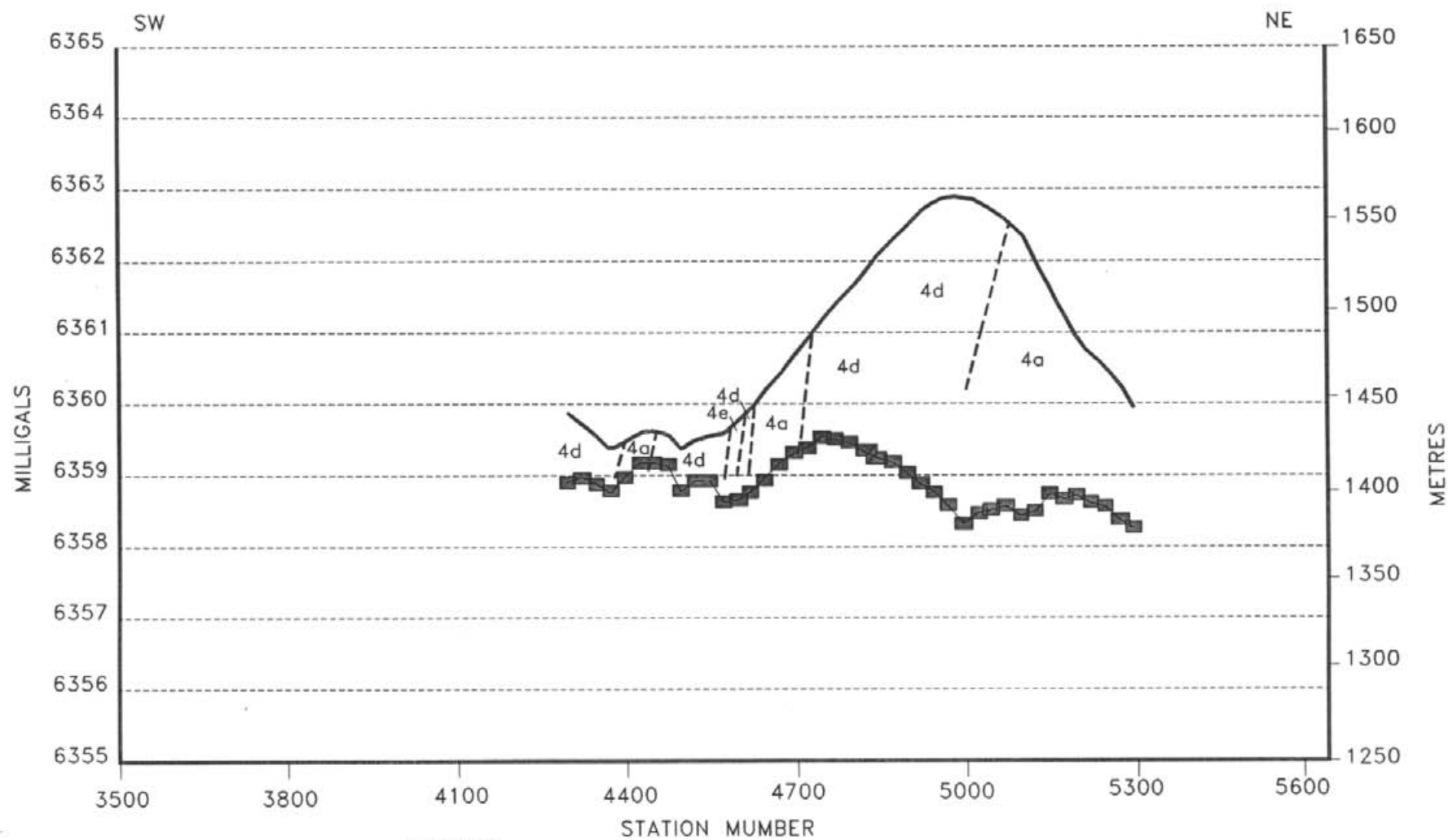
## III. L38+00N (Figure 21)

"On this line there are two positive anomalies centered at 47+50E and 44+50E, respectively. They appear to be related to geological contacts between poker chip black shale and black chert and indicate a contrast of about 0.4 g/cc. The nodular barite showing is not related to either of these anomalies."

## IV. Recommendations

"Of interest may be line 50+00N on the Nod Grid at 46+75E where the gravity corroborates a 25m x 100m x 100m showing and holds hope of a larger down dip extension."





GEOLOGY

MIDDLE to UPPER DEVONIAN  
LOWER EARN GROUP  
GUNSTEEL FORMATION

- 4e NODULAR to MASSIVE BARITE
- 4d POKER CHIP SHALE
- 4c DISTINCTLY LAMINATED SHALE
- 4b PREGNANT SHALE
- 4a PORCELLANITE (CHERT)

SYMBOLS

- BOUG 02.1
- GEOLOGIC CONTACT
- FAULT



SCALE: 1:10,000 Vertical Exaggeration 3x

FIGURE 21

|                                                              |                 |            |
|--------------------------------------------------------------|-----------------|------------|
| <b>TECK EXPLORATION LTD.</b><br>KAMLOOPS, BRITISH COLUMBIA   |                 |            |
| MT. ALCOCK PROPERTY                                          |                 |            |
| <b>NOD GRID</b><br><b>L 38+00 N</b><br><b>GRAVITY SURVEY</b> |                 |            |
| DATE DRAWN: FEB. 9, 1993                                     | SCALE: 1:10,000 | DWG. NAME: |
| COMPILED BY: R.F./S.J.                                       | JOB No: 1715    | ALC-L38G   |
| DRAWN BY: S.A.                                               | NTS No: 94F/11  |            |

## 11. CONCLUSION

Geological mapping has shown the property to be largely underlain by Lower Earn Group Middle to Upper Devonian black shales, cherts, silty shales, nodular barite and limestone of the Gunsteel Formation. Abundant exposures of Ordovician and Silurian dolomitic siltstones, black shales and siltstones are found in the eastern portion of the claims with local exposures found elsewhere.

Mapping and prospecting within the Nod Grid area has outlined a nodular barite zone 800 metres in strike length and up to 25 metres wide. Favourable pregnant shale lithology was identified in two zones up to 700 metres in strike length. Rock chip samples from both *the pregnant shale and nodular barite returned subeconomic base metal (Zn-Pb) values.*

Soils collected from the Nod Grid also failed to return significant base metal results, the most interesting anomaly located between L43N and L44N; a zone with coincident zinc (up to 1119 ppm Zn), lead (up to 484 ppm Pb) and associated sedex indicator element (cadmium, manganese and vanadium) values overlying pregnant shales. The highly anomalous barium soil values (up to 14% Ba) are correlative with the nodular barite outcrops.

The gravity survey carried out over portions of the Nod Grid provided mixed results. The survey over L50+00N indicates a 0.2 milligal anomaly centered at 46+75E that could be caused by a 25m x 100m x 100m mass of density contrast and holds hope of a larger down dip extension. However, the geological cross-section interpretation suggests this body is fault bounded. The two other lines surveyed, L44+00N and L38+00N, resulted in weak gravity anomalies associated with density contrasts between siliceous and non-siliceous black shales.

Mapping and prospecting within the Seep Grid identified several exposures of laminated pyrite hosted by Devonian pregnant and poker chip shales. Rock chip samples of pyritic black shales returned subeconomic base metal values. Stream and iron-seep sampling returned highly elevated zinc values (up to 12967 ppm Zn), however most associated lead values are low, thus likely indicating the iron-seeps are fault related.

The soil survey conducted over the Seep Grid delineated several coincident anomalous zinc and lead zones containing values up to 4672 ppm Zn and 857 ppm Pb.

Associated sedex indicator elements, including cadmium, manganese, vanadium and phosphorous and silver are locally anomalous and almost always correlative with elevated zinc and/or lead values. The majority of the anomalies are most likely attributed to northwest-trending fault zones. Several of the anomalous zones remain unexplained, including the anomalous lead stream value draining the lead-zinc soil zone from L60N at the baseline to L66N, 56+50E.

Mapping northwest of Warneford River identified numerous occurrences of nodular barite, usually hosted by poker chip shale. Two areas of nodular barite are hosted by favourable pregnant shale. One area of massive barite has over 350 metres of strike length. Samples collected from both nodular and massive barite returned subeconomic base metal and associated indicator element values.

Laminated pyrite within pregnant shales was identified in the Longwok Creek area. Rock chip samples returned no significant base metal values.

A significant Zn-Pb-Ag massive sulphide deposit is not outcropping in the areas covered by the 1992 surveys.

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**APPENDIX I**  
**Statement of Qualifications**

I, Steve Jensen, do hereby certify that:

- 1) I am a geologist and have practised my profession for the past five years.
- 2) I graduated from University of British Columbia, Vancouver, British Columbia with a Bachelor of Sciences degree in Geology (1987).
- 3) I was actively involved in the Mt. Alcock Property program and authored the report contained herein.
- 4) All data contained within this report and conclusions drawn from it are true and accurate to the best of my knowledge.
- 5) I hold no personal interest, direct or indirect in the Mt. Alcock Property which is the subject of this report.



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Steve Jensen  
Project Geologist  
November, 1992

**APPENDIX II**  
**Cost Statement**

**MT. ALCOCK PROPERTY**

**COST STATEMENT**

**1. Geology**

(Includes preparation, field plotting, travel days)

**NOD GROUP**

|    |                                                                                                         |                           |
|----|---------------------------------------------------------------------------------------------------------|---------------------------|
| A. | Randy Farmer (Geologist)<br>14 days @ \$256.65/day<br>July (15,17,22),29,30,31,Aug 1,2,3,4,(5),6,12,14  | \$3593.10                 |
| B. | Steve Jensen (Geologist)<br>14 days @ \$223.52/day<br>July (15,22),29,30,31, Aug 1,2,3,4,(5),6,12,14,16 | <u>\$3129.28</u>          |
|    |                                                                                                         | <b>Subtotal \$6722.38</b> |

**SEEP GROUP**

|    |                                                                                                      |                           |
|----|------------------------------------------------------------------------------------------------------|---------------------------|
| A. | Steve Jensen (Geologist)<br>9 days @ \$223.52/day<br>July (13,20,21), Aug 8,10,11,13,15,(20)         | \$2011.68                 |
| B. | Randy Farmer (Geologist)<br>11 days @ \$256.65/day<br>July (13,14,16,20,21), Aug 10,11,13,15,16,(20) | <u>\$2823.15</u>          |
|    |                                                                                                      | <b>Subtotal \$4834.83</b> |

**2. Hand Trenching**

**NOD GROUP**

|    |                                                           |                          |
|----|-----------------------------------------------------------|--------------------------|
| A. | Doug Nikirk (Technician)<br>1 day @ \$195.75/day<br>Aug 4 | \$195.75                 |
| B. | Gord May (Assisstant)<br>1 day @ \$253.75/day<br>Aug 4    | <u>\$162.00</u>          |
|    |                                                           | <b>Subtotal \$357.75</b> |

( ) Denotes non-field days

3. Soil Survey

NOD GROUP

|    |                                                                                      |                           |
|----|--------------------------------------------------------------------------------------|---------------------------|
| A. | Doug Nikirk (Technician)<br>8 days @ \$195.75/day<br>July (22),29,30,31, Aug 1,2,3,5 | \$1566.00                 |
| B. | Gord May (Assisstant)<br>8 days @ \$162.00/day<br>July (22),29,30,31, Aug 1,2,3,5    | <u>\$1296.00</u>          |
|    |                                                                                      | <b>Subtotal \$2862.00</b> |

SEEP GROUP

|    |                                                                                      |                           |
|----|--------------------------------------------------------------------------------------|---------------------------|
| A. | Doug Nikirk (Technician)<br>6 days @ \$195.75/day<br>July (21), Aug 10,11,12,13,(20) | \$1174.50                 |
| B. | Gord May (Assisstant)<br>6 days @ \$162.00/day<br>July (21), Aug 10,11,12,13,(20)    | <u>\$972.00</u>           |
|    |                                                                                      | <b>Subtotal \$2146.50</b> |

4. Gravity Survey

NOD GROUP

|    |                                                                                                                  |                           |
|----|------------------------------------------------------------------------------------------------------------------|---------------------------|
| A. | Kevin McNabb (Geophysicist) & Equipment Rental<br>5 days @ \$680.00/day<br>Aug (15),16,17,19,(20)                | \$3400.00                 |
| B. | Doug Nikirk (Technician)<br>3 days @ \$195.75/day<br>Aug 16,17,19                                                | \$587.25                  |
| C. | Gord May (Assisstant)<br>3 days @ \$162.00/day<br>Aug 16,17,19                                                   | \$486.00                  |
| D. | Gravity Survey - Report & Interpretation - Al Wynne (Geophysicist)<br>4 days @ \$400.00/day<br>Oct (27,28,29,30) | <u>\$1600.00</u>          |
|    |                                                                                                                  | <b>Subtotal \$6073.25</b> |

( ) Denotes non-field days

5. Analytical = Acme Analytical Labs, Vancouver, B.C.

NOD GROUP

|    |                                                                                                      |                           |
|----|------------------------------------------------------------------------------------------------------|---------------------------|
| A. | Rock samples<br>49 @ \$11.37 ea.<br>(29 el. ICP & Geochem Ba by whole rock ICP)                      | \$557.13                  |
| B. | Rock samples<br>18 @ \$9.00 ea.<br>(Geochem whole rock)                                              | \$162.00                  |
| C. | Soil samples<br>496 @ \$9.35 ea.<br>(29 el. ICP & Geochem Ba by whole rock ICP)                      | \$4637.60                 |
| D. | Moss Mat, silt and Fe-seep samples<br>25 @ \$9.35 ea.<br>(29 el. ICP & Geochem Ba by whole rock ICP) | <u>\$233.75</u>           |
|    |                                                                                                      | <b>Subtotal \$5590.48</b> |

SEEP GROUP

|    |                                                                                 |                           |
|----|---------------------------------------------------------------------------------|---------------------------|
| A. | Rock samples<br>8 @ \$11.37 ea.<br>(29 el. ICP & Geochem Ba by whole rock ICP)  | \$90.96                   |
| B. | Soil samples<br>245 @ \$9.35 ea.<br>(29 el. ICP & Geochem Ba by whole rock ICP) | \$2290.75                 |
| C. | Moss Mat and Fe-seep samples<br>15 @ \$9.35 ea.<br>(29 el. ICP & Au)            | <u>\$140.25</u>           |
|    |                                                                                 | <b>Subtotal \$2521.96</b> |

6. Helicopter = Northern Mountain Helicopters, Ft. Nelson, B.C.

NOD GROUP

| <u>Date</u>   | <u>Hours</u> | <u>Cost/Hour</u> | <u>Fuel &amp; Oil</u> | <u>Total</u>              |
|---------------|--------------|------------------|-----------------------|---------------------------|
| July 28       | 1.9          | \$660.00         | \$358.38              | \$1612.38                 |
| Aug 12        | 0.8          | \$660.00         | \$92.80               | \$620.80                  |
| Aug 14        | 2.1          | \$660.00         | \$243.60              | \$1629.60                 |
| Aug 16        | 0.7          | \$660.00         | \$81.20               | \$543.20                  |
| Aug 17        | <u>1.2</u>   | \$660.00         | \$139.20              | <u>\$931.20</u>           |
| Total 6.7 hrs |              |                  |                       | <b>Subtotal \$5337.18</b> |

SEEP GROUP

| <u>Date</u> | <u>Hours</u> | <u>Cost/Hour</u> | <u>Fuel &amp; Oil</u> | <u>Total</u>     |
|-------------|--------------|------------------|-----------------------|------------------|
| Aug 8       | 2.4          | \$660.00         | \$278.40              | \$1862.40        |
| Aug 10      | 2.1          | \$660.00         | \$243.60              | \$1629.60        |
| Aug 11      | 1.6          | \$660.00         | \$185.60              | \$1241.60        |
| Aug 12      | 1.0          | \$660.00         | \$116.00              | \$776.00         |
| Aug 13      | 2.0          | \$660.00         | \$232.00              | \$1552.00        |
| Aug 15      | 2.6          | \$660.00         | \$301.60              | \$2017.60        |
| Aug 16      | <u>2.0</u>   | \$660.00         | \$232.20              | <u>\$1552.00</u> |

Total 13.7 hrs

Subtotal \$10631.20

7. Fixed Wing Transportation = Williston Lake Air, Mackenzie, B.C.

| <u>Date</u> | <u>Cost</u>     | <u>Description</u>                                                                                                                          |
|-------------|-----------------|---------------------------------------------------------------------------------------------------------------------------------------------|
| July 22     | \$1845.00       | Twin Otter charter from Mackenzie to Ft. Ware - crew and field supplies mobilization to property                                            |
| Aug 10      | \$371.25        | Ceneca charter from Mackenzie to Finbow Camp - personnel, groceries and rock samples                                                        |
| Aug 13      | \$58.50         | Dangerous goods (naptha, propane) shipment from Mackenzie to Finbow                                                                         |
| Aug 15      | \$670.25        | Ceneca charter from Mackenzie to Finbow - personnel and groceries                                                                           |
| Aug 19      | \$315.00        | Ceneca charter from Finbow to Mackenzie - personnel & gear                                                                                  |
| Aug 20      | \$615.15        | Ceneca charter from Finbow to Mackenzie - personnel & gear                                                                                  |
| Aug 20      | \$271.73        | Canadian Airline flight from Prince George to Vancouver - personnel                                                                         |
| Aug 25      | \$168.30        | Part Ceneca charter from Finbow to Mackenzie - sample shipment                                                                              |
| Aug 31      | \$1122.43       | Northern Thunderbird Air charter (Beech 18) from Prince George to Finow and return - personnel & field supplies, camp gear - demobilization |
| Sept 1      | <u>\$371.25</u> | Ceneca charter from Finbow to Mackenzie - demobilization                                                                                    |

Subtotal \$5808.86

Subtotal \$5808.86



|     |                                                                                                      |                           |
|-----|------------------------------------------------------------------------------------------------------|---------------------------|
| 8.  | <u>Food and Accommodation</u>                                                                        |                           |
| A.  | Food - groceries<br>Shoppers Food Mart & Coop - Mackenzie<br>(July 22-Aug 20,1992)                   | \$1298.64                 |
| B.  | Expeditor Fees<br>Williston Lake Air - Mackenzie<br>(July 22-Aug 20,1992)                            | \$1250.00                 |
| C.  | Accommodation                                                                                        |                           |
|     | (i) Williston Lake Lodge<br>(July 20,21,Aug 5,14,24)                                                 | \$370.30                  |
|     | (ii) Finbow Logging Camp<br>(Aug 9,19)                                                               | <u>\$450.00</u>           |
|     | <b>Subtotal</b>                                                                                      | <b>\$3368.94</b>          |
| 9.  | <u>Truck Transportation</u>                                                                          |                           |
|     | 4x4 Toyota Pickup & Toyota Forerunner<br>33 days @ \$120.00/day<br>(includes fuel,insurance,repairs) | <b>Subtotal \$3960.00</b> |
| 10. | <u>Freight and Shipping</u>                                                                          |                           |
|     | Sample shipments, correspondance etc.                                                                | <b>Subtotal \$580.00</b>  |
| 11. | <u>Field Supplies</u>                                                                                |                           |
|     | Sample bags, flagging, topo thread, propane etc.                                                     | <b>Subtotal \$1529.22</b> |
| 12. | <u>Telephone</u>                                                                                     |                           |
|     | Radio telephone charges                                                                              | <b>Subtotal \$300.18</b>  |
| 13. | <u>Radio Rental</u>                                                                                  |                           |
| A.  | 4 - handheld IC-U16                                                                                  | \$360.00                  |
| B.  | 2 - SBX-11A high frequency radio phones                                                              | <u>\$240.00</u>           |
|     | <b>Subtotal</b>                                                                                      | <b>\$600.00</b>           |

14. Drafting

|    |                                                                |                    |
|----|----------------------------------------------------------------|--------------------|
| A. | Base maps preparation (Steve Archibald)<br>10 days @ \$200/day | \$2000.00          |
| B. | Drafting (Steve Archibald)<br>10 days @ \$200/day              | \$2000.00          |
| C. | Prints, Enlargments                                            | <u>\$500.00</u>    |
|    |                                                                | Subtotal \$4500.00 |

15. Report Writing and Typing

|    |                                                    |                    |
|----|----------------------------------------------------|--------------------|
| A. | Steve Jensen (Geologist)<br>15 days @ \$223.52/day | Subtotal \$3352.80 |
|----|----------------------------------------------------|--------------------|

**TOTAL COST MT ALCOCK 1992 PROGRAM    \$71,077.53**

COST ALLOCATION

Costs for the 1992 Mt. Alcock program will be split between two claim groups, the NOD and the SEEP. Each group contains the same number of units -96-, therefore the costs of sections 7 through 15 will be split evenly between the two groups.

The sum of the costs of sections 7 thru 15 = \$24,000.00

Therefore \$12,000.00 (\$24,000.00/2) will be applied to each group.

The sum of costs of sections 1 thru 6 is \$26,943.04 for the Nod group and \$20,134.49 for the Seep group.

**TOTAL COSTS 1992 PROGRAM**

**Nod Group:**    \$26,943.04 (Sections 1-6)  
                  \$12,000.00 (Sections 7-15)  
                  **\$38,943.04**

**Seep Group:**    \$20,134.49 (Sections 1-6)  
                  \$12,000.00 (Sections 7-15)  
                  **\$32,134.49**

**APPENDIX III**  
**Certificates of Analysis**

# ROCKS



Teck Exploration (BC) PROJECT 1715 FILE # 92-2518

Page 2



| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*    |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|--------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm    |
| 45201              | 8   | 19  | 23  | 117 | .2  | 13  | 3   | 11   | 1.42 | 9   | 5   | ND  | 4   | 25  | .2   | 3   | 2   | 41  | .03 | .034 | 2   | 11  | .06 | 771  | .01 | 19  | .71  | .01 | .27 | 1   | 2685   |
| 45202              | 7   | 43  | 23  | 198 | .5  | 36  | 7   | 23   | 1.47 | 15  | 5   | ND  | 5   | 21  | 1.0  | 4   | 2   | 43  | .08 | .046 | 2   | 13  | .05 | 394  | .01 | 17  | .70  | .01 | .28 | 1   | 5848   |
| RE 45213           | 14  | 16  | 11  | 126 | .5  | 18  | 5   | 58   | .69  | 7   | 5   | ND  | 3   | 28  | 1.9  | 4   | 2   | 89  | .07 | .031 | 2   | 20  | .05 | 386  | .01 | 24  | .44  | .01 | .24 | 1   | 923    |
| 45203              | 14  | 11  | 10  | 62  | .1  | 17  | 2   | 13   | .83  | 4   | 5   | ND  | 1   | 14  | .2   | 2   | 2   | 102 | .05 | .006 | 2   | 8   | .04 | 883  | .01 | 20  | .37  | .01 | .17 | 1   | 2766   |
| 45204              | 6   | 42  | 20  | 74  | .4  | 44  | 6   | 19   | 1.49 | 13  | 5   | ND  | 5   | 27  | .6   | 3   | 2   | 51  | .23 | .065 | 2   | 14  | .11 | 138  | .01 | 19  | .77  | .01 | .32 | 1   | 2656   |
| 45205              | 40  | 25  | 52  | 908 | 1.3 | 39  | 2   | 25   | .96  | 24  | 5   | ND  | 1   | 12  | 13.1 | 18  | 2   | 235 | .11 | .016 | 2   | 17  | .04 | 302  | .01 | 15  | .31  | .01 | .13 | 1   | 1192   |
| 45213              | 15  | 14  | 10  | 140 | .6  | 20  | 5   | 60   | .72  | 7   | 5   | ND  | 3   | 29  | 2.0  | 3   | 2   | 94  | .07 | .032 | 2   | 21  | .05 | 398  | .01 | 24  | .46  | .01 | .25 | 1   | 913    |
| 45214              | 15  | 12  | 4   | 57  | .3  | 19  | 2   | 37   | .54  | 5   | 5   | ND  | 1   | 25  | 1.6  | 3   | 2   | 101 | .06 | .012 | 2   | 11  | .03 | 219  | .01 | 12  | .20  | .01 | .12 | 1   | 520    |
| 45217              | 10  | 37  | 34  | 236 | .6  | 45  | 8   | 47   | 2.46 | 22  | 5   | ND  | 5   | 43  | 1.1  | 3   | 2   | 37  | .08 | .036 | 2   | 12  | .05 | 1060 | .01 | 16  | .52  | .01 | .28 | 1   | 2629   |
| 45252              | 8   | 8   | 3   | 12  | .2  | 13  | 1   | 33   | .49  | 2   | 5   | ND  | 1   | 12  | .3   | 2   | 2   | 39  | .02 | .003 | 2   | 9   | .01 | 334  | .01 | 5   | .13  | .01 | .07 | 1   | 947    |
| 45253              | 3   | 5   | 10  | 9   | .1  | 7   | 1   | 13   | .14  | 2   | 5   | ND  | 1   | 82  | .3   | 2   | 2   | 79  | .02 | .002 | 2   | 11  | .03 | 1197 | .01 | 16  | .29  | .01 | .12 | 1   | 135160 |
| 45254              | 28  | 14  | 28  | 224 | .2  | 30  | 2   | 40   | .82  | 6   | 5   | ND  | 1   | 5   | .3   | 5   | 2   | 131 | .01 | .005 | 2   | 12  | .01 | 323  | .01 | 8   | .14  | .01 | .05 | 1   | 1124   |
| 45255              | 13  | 6   | 10  | 16  | .9  | 16  | 1   | 12   | .31  | 3   | 5   | ND  | 2   | 12  | .2   | 6   | 2   | 120 | .02 | .011 | 2   | 17  | .03 | 750  | .01 | 17  | .31  | .01 | .18 | 1   | 1426   |
| 45256              | 10  | 10  | 5   | 20  | .2  | 15  | 2   | 36   | .76  | 6   | 5   | ND  | 1   | 11  | .2   | 2   | 2   | 32  | .03 | .003 | 2   | 10  | .02 | 351  | .01 | 7   | .13  | .01 | .07 | 1   | 948    |
| 45257              | 11  | 14  | 10  | 29  | .2  | 10  | 2   | 12   | .53  | 2   | 5   | ND  | 1   | 30  | .7   | 2   | 2   | 77  | .02 | .007 | 2   | 15  | .03 | 1460 | .01 | 16  | .35  | .01 | .14 | 1   | 7848   |
| STANDARD C/CB-1200 | 19  | 57  | 38  | 132 | 7.2 | 70  | 31  | 1039 | 3.96 | 41  | 16  | 7   | 40  | 52  | 17.6 | 14  | 19  | 56  | .51 | .087 | 38  | 59  | .92 | 182  | .08 | 34  | 2.00 | .06 | .14 | 10  | 2133   |

Sample type: ROCK. Samples beginning 'RE' are duplicate samples.  
BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP.

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

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## GEOCHEMICAL ANALYSIS CERTIFICATE

Teck Exploration (BC) PROJECT 1715 File # 92-2518

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| SAMPLE#    | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|
| 45206      | 10        | 9         | 19        | 7         | .1        | 7         | 2         | 13        | .62     | 8         | 5        | ND        | 7         | 167       | .9        | 2         | 2         | 59       | .03     | .011   | 2         | 7         | .02     | 229       | .01     | 12       | .19     | .01     | .12    | 2        |
| 45207      | 11        | 3         | 15        | 3         | .1        | 7         | 1         | 7         | .18     | 2         | 5        | ND        | 1         | 76        | .2        | 2         | 2         | 82       | .02     | .003   | 2         | 7         | .03     | 926       | .01     | 16       | .27     | .01     | .12    | 1        |
| 45208      | 5         | 7         | 19        | 37        | .2        | 11        | 2         | 9         | .76     | 5         | 5        | ND        | 3         | 21        | .2        | 2         | 4         | 54       | .01     | .010   | 2         | 13        | .05     | 789       | .01     | 20       | .71     | .02     | .28    | 1        |
| 45209      | 6         | 12        | 19        | 34        | .3        | 12        | 2         | 9         | .90     | 8         | 5        | ND        | 3         | 24        | .2        | 2         | 2         | 71       | .01     | .023   | 2         | 16        | .05     | 948       | .01     | 21       | .77     | .01     | .31    | 1        |
| 45210      | 9         | 4         | 9         | 3         | .2        | 6         | 1         | 20        | .44     | 3         | 5        | ND        | 2         | 7         | .2        | 2         | 2         | 65       | .03     | .006   | 2         | 8         | .04     | 520       | .01     | 20       | .37     | .01     | .22    | 1        |
| 45258      | 10        | 3         | 8         | 13        | .1        | 8         | 1         | 7         | .35     | 3         | 5        | ND        | 1         | 16        | .2        | 2         | 2         | 67       | .01     | .006   | 2         | 16        | .04     | 628       | .01     | 18       | .38     | .01     | .19    | 1        |
| 45259      | 13        | 7         | 9         | 10        | .1        | 7         | 1         | 9         | .55     | 4         | 5        | ND        | 1         | 13        | .2        | 2         | 3         | 76       | .01     | .006   | 2         | 11        | .04     | 566       | .01     | 23       | .40     | .01     | .22    | 1        |
| 45260      | 12        | 4         | 9         | 10        | .1        | 8         | 1         | 5         | .52     | 3         | 5        | ND        | 2         | 11        | .2        | 2         | 2         | 82       | .01     | .006   | 2         | 16        | .05     | 338       | .01     | 23       | .45     | .01     | .24    | 1        |
| 45261      | 10        | 4         | 11        | 9         | .2        | 6         | 1         | 9         | .46     | 2         | 5        | ND        | 1         | 10        | .2        | 2         | 2         | 76       | .01     | .003   | 2         | 11        | .05     | 670       | .01     | 23       | .46     | .01     | .24    | 1        |
| 45262      | 12        | 8         | 11        | 20        | .1        | 8         | 1         | 6         | .56     | 3         | 5        | ND        | 1         | 12        | .2        | 2         | 2         | 114      | .01     | .007   | 2         | 15        | .05     | 576       | .01     | 21       | .46     | .01     | .24    | 1        |
| 45263      | 10        | 4         | 19        | 3         | .1        | 5         | 1         | 7         | .32     | 4         | 5        | ND        | 1         | 109       | .2        | 2         | 3         | 46       | .01     | .004   | 2         | 5         | .02     | 332       | .01     | 15       | .18     | .01     | .10    | 1        |
| 45264      | 7         | 4         | 23        | 5         | .1        | 5         | 1         | 4         | .29     | 3         | 5        | ND        | 1         | 105       | .2        | 2         | 2         | 51       | .01     | .003   | 2         | 7         | .02     | 383       | .01     | 12       | .18     | .01     | .10    | 1        |
| RE 45260   | 12        | 6         | 11        | 11        | .1        | 8         | 1         | 7         | .53     | 5         | 5        | ND        | 2         | 12        | .3        | 2         | 2         | 84       | .01     | .006   | 2         | 15        | .05     | 351       | .01     | 23       | .46     | .01     | .24    | 1        |
| 45265      | 14        | 7         | 32        | 11        | .1        | 6         | 1         | 7         | .96     | 10        | 5        | ND        | 1         | 89        | .2        | 2         | 3         | 64       | .01     | .013   | 2         | 7         | .02     | 93        | .01     | 12       | .22     | .01     | .19    | 1        |
| 45266      | 17        | 7         | 33        | 6         | .1        | 10        | 1         | 3         | .93     | 11        | 5        | ND        | 1         | 77        | .2        | 4         | 2         | 107      | .01     | .016   | 2         | 11        | .02     | 102       | .01     | 11       | .26     | .01     | .18    | 1        |
| 45267      | 18        | 16        | 9         | 28        | .1        | 12        | 2         | 18        | 1.24    | 12        | 5        | ND        | 1         | 15        | .2        | 2         | 2         | 98       | .01     | .015   | 2         | 11        | .03     | 310       | .01     | 15       | .34     | .01     | .23    | 1        |
| 45268      | 12        | 8         | 9         | 9         | .2        | 9         | 1         | 10        | .57     | 4         | 5        | ND        | 1         | 15        | .2        | 2         | 2         | 109      | .01     | .011   | 2         | 15        | .04     | 694       | .01     | 20       | .43     | .01     | .20    | 1        |
| 45269      | 10        | 12        | 11        | 20        | .6        | 11        | 2         | 29        | .63     | 5         | 5        | ND        | 3         | 14        | .4        | 3         | 2         | 135      | .03     | .019   | 2         | 12        | .07     | 463       | .01     | 24       | .54     | .01     | .24    | 1        |
| 45270      | 11        | 13        | 10        | 10        | .3        | 9         | 1         | 9         | .76     | 7         | 5        | ND        | 2         | 11        | .2        | 2         | 2         | 113      | .01     | .008   | 2         | 13        | .05     | 516       | .01     | 24       | .50     | .01     | .26    | 1        |
| STANDARD C | 19        | 57        | 38        | 132       | 7.2       | 70        | 31        | 1039      | 3.96    | 41        | 16       | 7         | 40        | 52        | 17.6      | 14        | 19        | 56       | .51     | .087   | 38        | 59        | .92     | 182       | .08     | 34       | 2.00    | .06     | .14    | 10       |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO<sub>3</sub>-H<sub>2</sub>O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB  
 - SAMPLE TYPE: P1 TO P2 ROCK P3 SILT P4 MOSS MAT Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 12 1992 DATE REPORT MAILED:

Aug 24/92

SIGNED BY: D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



## WHOLE ROCK ICP ANALYSIS



**Teck Exploration (BC) PROJECT 1715 File # 92-2518 Page 1**  
 350 - 272 Victoria St., Kamloops BC V2C 2A2

| SAMPLE#       | SiO2  | Al2O3 | Fe2O3 | MgO | CaO  | Na2O | K2O  | TiO2 | P2O5 | MnO | Cr2O3 | Ba     | Sr   | Zr  | Y   | Nb  | LOI  | SUM   |
|---------------|-------|-------|-------|-----|------|------|------|------|------|-----|-------|--------|------|-----|-----|-----|------|-------|
|               | %     | %     | %     | %   | %    | %    | %    | %    | %    | %   | %     | ppm    | ppm  | ppm | ppm | ppm | %    | %     |
| 45206         | 40.33 | 2.92  | .72   | .01 | .07  | .06  | .76  | .13  | .01  | .01 | .004  | 296658 | 1671 | 35  | 7   | 12  | 4.2  | 99.82 |
| 45207         | 55.72 | 3.85  | .28   | .01 | .06  | .07  | .84  | .17  | .01  | .01 | .004  | 194810 | 913  | 43  | 5   | 5   | 5.6  | 99.82 |
| 45208         | 76.93 | 11.24 | 1.08  | .45 | .02  | .09  | 2.70 | .55  | .02  | .01 | .008  | 4430   | 60   | 101 | 12  | 16  | 6.0  | 99.87 |
| 45209         | 77.14 | 11.19 | 1.21  | .42 | .01  | .07  | 2.60 | .53  | .05  | .01 | .006  | 4671   | 62   | 90  | 10  | 17  | 5.8  | 99.84 |
| 45210         | 84.45 | 6.84  | .64   | .22 | .05  | .07  | 1.76 | .32  | .01  | .01 | .003  | 1569   | 36   | 42  | 6   | 5   | 5.2  | 99.83 |
| 45258         | 85.76 | 6.52  | .49   | .23 | .02  | .07  | 1.57 | .27  | .01  | .01 | .002  | 1707   | 43   | 40  | 8   | 5   | 4.6  | 99.83 |
| 45259         | 85.12 | 6.54  | .66   | .22 | .05  | .09  | 1.66 | .29  | .01  | .01 | .002  | 1830   | 42   | 38  | 7   | 5   | 4.9  | 99.85 |
| 45260         | 84.10 | 7.14  | .69   | .29 | .02  | .08  | 1.55 | .33  | .01  | .01 | .003  | 1337   | 40   | 50  | 8   | 5   | 5.4  | 99.85 |
| 45261         | 83.06 | 7.36  | .61   | .32 | .25  | .09  | 1.97 | .32  | .01  | .01 | .003  | 2124   | 46   | 48  | 7   | 5   | 5.5  | 99.86 |
| 45262         | 83.28 | 7.16  | .69   | .30 | .04  | .07  | 1.70 | .31  | .01  | .01 | .003  | 2734   | 46   | 49  | 7   | 5   | 5.8  | 99.83 |
| 45263         | 40.28 | 2.68  | .36   | .01 | .05  | .05  | .71  | .12  | .01  | .01 | .006  | 302714 | 1449 | 27  | 5   | 5   | 4.0  | 99.87 |
| 45264         | 38.45 | 2.44  | .33   | .01 | .02  | .05  | .67  | .12  | .01  | .01 | .010  | 314099 | 1251 | 22  | 5   | 5   | 4.3  | 99.89 |
| RE 45260      | 83.55 | 7.30  | .71   | .31 | .02  | .08  | 1.83 | .33  | .01  | .01 | .002  | 1285   | 43   | 61  | 8   | 5   | 5.5  | 99.86 |
| 45265         | 46.94 | 3.10  | .92   | .01 | .02  | .05  | .81  | .17  | .02  | .01 | .002  | 244827 | 955  | 30  | 5   | 5   | 6.1  | 99.85 |
| 45266         | 54.48 | 3.88  | .92   | .01 | .03  | .06  | 1.05 | .20  | .01  | .01 | .005  | 183598 | 699  | 34  | 5   | 5   | 7.9  | 99.83 |
| 45267         | 85.43 | 5.19  | 1.24  | .09 | .03  | .09  | 1.31 | .24  | .02  | .01 | .002  | 4026   | 51   | 37  | 8   | 5   | 5.5  | 99.84 |
| 45268         | 84.87 | 6.26  | .65   | .20 | .02  | .07  | 1.35 | .27  | .01  | .01 | .004  | 2008   | 44   | 40  | 9   | 5   | 5.8  | 99.85 |
| 45269         | 81.49 | 7.91  | .74   | .36 | .58  | .10  | 2.02 | .36  | .03  | .01 | .002  | 1923   | 53   | 56  | 10  | 5   | 5.8  | 99.73 |
| 45270         | 79.76 | 8.78  | .92   | .43 | .02  | .11  | 2.19 | .38  | .01  | .01 | .004  | 2959   | 44   | 51  | 8   | 5   | 6.7  | 99.81 |
| STANDARD SO-4 | 69.15 | 10.16 | 3.44  | .89 | 1.53 | 1.29 | 2.04 | .56  | .20  | .08 | .008  | 800    | 197  | 308 | 23  | 14  | 10.4 | 99.95 |

.200 GRAM SAMPLES ARE FUSED WITH 1.2 GRAM OF LIBO2 AND ARE DISSOLVED IN 100 MLS 5% HNO3.

- SAMPLE TYPE: P1 TO P2 ROCK P3 SILT P4 MOSS MAT

Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 12 1992

DATE REPORT MAILED: Aug 24/92

SIGNED BY: C. Leong, D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



## GEOCHEMICAL ANALYSIS CERTIFICATE



Teck Exploration (BC) PROJECT 1715 File # 92-2641 Page 1

350 - 272 Victoria St., Kamloops BC V2C 2A2 Submitted by: RANDY FARMER

| SAMPLE#            | Mo  | Cu  | Pb   | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*    |
|--------------------|-----|-----|------|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|--------|
|                    | ppm | ppm | ppm  | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm    |
| 45220              | 13  | 16  | 14   | 37   | .2  | 16  | 2   | 11   | .86  | 9   | 5   | ND  | 3   | 16  | .5   | 5   | 2   | 22  | .07 | .007 | 2   | 9   | .05 | 558  | .01 | 21  | .61  | .01 | .31 | 1   | 2754   |
| 45223              | 21  | 8   | 5    | 86   | .3  | 17  | 1   | 35   | 1.11 | 9   | 5   | ND  | 2   | 15  | .2   | 5   | 2   | 59  | .05 | .031 | 3   | 11  | .03 | 344  | .01 | 13  | .32  | .01 | .15 | 1   | 1599   |
| 45224              | 10  | 20  | 12   | 125  | .1  | 32  | 5   | 31   | 1.34 | 8   | 5   | ND  | 3   | 22  | 1.1  | 4   | 2   | 48  | .04 | .014 | 2   | 10  | .09 | 779  | .01 | 16  | .80  | .02 | .30 | 1   | 3538   |
| 45227              | 68  | 37  | 106  | 330  | .9  | 41  | 1   | 44   | .81  | 13  | 5   | ND  | 1   | 9   | 10.3 | 10  | 2   | 174 | .07 | .020 | 2   | 17  | .02 | 182  | .01 | 11  | .23  | .01 | .11 | 1   | 546    |
| 45228              | 36  | 28  | 135  | 1051 | .2  | 42  | 2   | 68   | 1.28 | 14  | 5   | ND  | 1   | 17  | 7.3  | 8   | 2   | 143 | .06 | .007 | 2   | 12  | .02 | 149  | .01 | 11  | .18  | .01 | .08 | 1   | 999    |
| 45229              | 18  | 93  | 43   | 103  | .4  | 28  | 2   | 50   | .83  | 11  | 8   | ND  | 1   | 16  | .7   | 12  | 2   | 103 | .03 | .006 | 2   | 17  | .03 | 238  | .01 | 13  | .25  | .01 | .15 | 2   | 696    |
| 45232              | 23  | 38  | 11   | 46   | .1  | 71  | 6   | 54   | 4.10 | 25  | 5   | ND  | 2   | 23  | .4   | 3   | 2   | 23  | .34 | .031 | 2   | 9   | .14 | 21   | .01 | 15  | .33  | .01 | .18 | 1   | 972    |
| 45233              | 29  | 19  | 13   | 29   | .6  | 35  | 3   | 54   | 1.09 | 13  | 8   | ND  | 3   | 16  | .2   | 6   | 2   | 63  | .13 | .051 | 2   | 10  | .03 | 152  | .01 | 19  | .33  | .01 | .20 | 1   | 678    |
| 45235              | 25  | 46  | 28   | 57   | .7  | 43  | 5   | 36   | 2.35 | 15  | 5   | ND  | 1   | 8   | .6   | 5   | 3   | 32  | .05 | .015 | 2   | 11  | .03 | 44   | .01 | 20  | .34  | .01 | .20 | 1   | 847    |
| 45236              | 6   | 11  | 14   | 59   | .4  | 22  | 2   | 63   | .91  | 6   | 5   | ND  | 3   | 56  | .2   | 3   | 2   | 24  | .06 | .019 | 3   | 8   | .03 | 531  | .01 | 15  | .34  | .01 | .24 | 1   | 21155  |
| 45242              | 7   | 7   | 21   | 29   | .2  | 8   | 1   | 14   | .75  | 10  | 5   | ND  | 1   | 155 | .2   | 2   | 2   | 29  | .03 | .016 | 2   | 5   | .03 | 238  | .01 | 15  | .30  | .01 | .17 | 1   | 266159 |
| 45243              | 10  | 13  | 23   | 52   | .1  | 20  | 1   | 19   | .78  | 11  | 5   | ND  | 1   | 104 | .2   | 2   | 3   | 38  | .06 | .015 | 2   | 7   | .03 | 864  | .01 | 14  | .30  | .01 | .13 | 1   | 226420 |
| 45245              | 10  | 7   | 20   | 21   | .2  | 11  | 1   | 5    | .64  | 13  | 5   | ND  | 1   | 136 | .2   | 5   | 2   | 33  | .02 | .013 | 2   | 5   | .02 | 393  | .01 | 13  | .26  | .01 | .15 | 1   | 245042 |
| 45247              | 8   | 24  | 26   | 149  | .1  | 29  | 3   | 37   | 1.40 | 16  | 5   | ND  | 2   | 66  | .5   | 2   | 2   | 35  | .07 | .033 | 2   | 10  | .04 | 582  | .01 | 21  | .50  | .02 | .25 | 1   | 56999  |
| 45272              | 23  | 28  | 10   | 119  | .7  | 34  | 8   | 94   | 1.09 | 9   | 5   | ND  | 3   | 25  | .5   | 4   | 2   | 78  | .24 | .085 | 4   | 11  | .04 | 350  | .01 | 18  | .65  | .01 | .25 | 1   | 3303   |
| RE 45242           | 8   | 7   | 22   | 29   | .1  | 7   | 1   | 13   | .73  | 9   | 5   | ND  | 1   | 146 | .2   | 3   | 4   | 27  | .03 | .016 | 2   | 5   | .03 | 277  | .01 | 12  | .28  | .01 | .15 | 1   | 279618 |
| 45275              | 44  | 41  | 1787 | 2028 | 4.3 | 39  | 1   | 43   | 1.88 | 14  | 5   | ND  | 2   | 14  | 6.8  | 14  | 2   | 164 | .12 | .017 | 2   | 16  | .02 | 599  | .01 | 13  | .32  | .01 | .13 | 1   | 3736   |
| 45276              | 43  | 34  | 58   | 209  | .3  | 33  | 1   | 69   | 1.07 | 9   | 5   | ND  | 1   | 7   | 1.0  | 6   | 2   | 131 | .04 | .016 | 2   | 15  | .01 | 529  | .01 | 6   | .15  | .01 | .05 | 1   | 973    |
| 45283              | 12  | 44  | 23   | 126  | .3  | 43  | 2   | 17   | 1.49 | 12  | 5   | ND  | 1   | 106 | .2   | 2   | 2   | 28  | .09 | .063 | 2   | 14  | .02 | 488  | .01 | 13  | .67  | .01 | .16 | 1   | 111579 |
| 45284              | 9   | 15  | 22   | 54   | .5  | 18  | 2   | 30   | 1.35 | 14  | 5   | ND  | 3   | 51  | .3   | 5   | 3   | 30  | .09 | .064 | 2   | 12  | .04 | 179  | .01 | 16  | .46  | .01 | .23 | 1   | 19907  |
| 45286              | 7   | 13  | 9    | 26   | .5  | 16  | 1   | 18   | .99  | 11  | 5   | ND  | 3   | 43  | .2   | 4   | 2   | 41  | .11 | .058 | 2   | 11  | .03 | 402  | .01 | 17  | .55  | .01 | .21 | 1   | 48153  |
| 45288              | 7   | 15  | 13   | 52   | .3  | 22  | 2   | 18   | .88  | 10  | 5   | ND  | 1   | 31  | .2   | 2   | 2   | 29  | .01 | .038 | 2   | 13  | .02 | 104  | .01 | 15  | .34  | .01 | .18 | 1   | 19271  |
| 45289              | 1   | 3   | 2    | 20   | .1  | 6   | 1   | 7    | .45  | 2   | 5   | ND  | 1   | 111 | .2   | 2   | 2   | 8   | .01 | .003 | 2   | 1   | .01 | 285  | .01 | 3   | .08  | .01 | .01 | 1   | 484714 |
| 45290              | 1   | 3   | 5    | 8    | .1  | 6   | 1   | 15   | .29  | 2   | 5   | ND  | 1   | 404 | .2   | 2   | 2   | 5   | .03 | .016 | 2   | 4   | .01 | 1015 | .01 | 2   | .06  | .01 | .02 | 1   | 392204 |
| 45291              | 4   | 9   | 9    | 20   | .1  | 15  | 1   | 26   | .77  | 8   | 5   | ND  | 1   | 147 | .2   | 2   | 2   | 14  | .03 | .040 | 2   | 7   | .01 | 672  | .01 | 9   | .19  | .01 | .10 | 1   | 183547 |
| 45292              | 4   | 13  | 12   | 28   | .2  | 16  | 1   | 17   | .75  | 8   | 5   | ND  | 1   | 176 | .2   | 2   | 2   | 14  | .04 | .028 | 2   | 7   | .01 | 224  | .01 | 9   | .18  | .01 | .10 | 1   | 189699 |
| STANDARD C/CB-1200 | 18  | 60  | 39   | 133  | 7.3 | 79  | 31  | 1066 | 3.96 | 42  | 22  | 7   | 39  | 53  | 19.0 | 16  | 21  | 58  | .50 | .087 | 40  | 61  | .91 | 183  | .09 | 34  | 1.95 | .08 | .17 | 11  | 2240   |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 ASSAY RECOMMENDED FOR ROCK AND CORE SAMPLES IF CU PB ZN AS > 1%, AG > 30 PPM & AU > 1000 PPB  
 - SAMPLE TYPE: P1 ROCK P2 SILT P3 MOSS MAT BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP.  
 GEOCHEM BA ANALYSIS BY WHOLE ROCK ICP. Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 18 1992 DATE REPORT MAILED: *Aug 27/92* SIGNED BY: *C. Leong* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS

# STREAM- MOSS MATS



Teck Exploration (BC) PROJECT 1715 FILE # 92-2641

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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg   | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   | Hg   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|------|-----|----|------|-----|-----|-----|-------|------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %    | ppm  | %   | %  | %    | %   | %   | ppm | ppm   | ppb  |
| M45219             | 24  | 49  | 27  | 882  | .8  | 126 | 12  | 160  | 2.25 | 18  | 5   | ND  | 9   | 61  | 6.6  | 4   | 6   | 83  | .47  | .059 | 3   | 11  | .10  | 1134 | .01 | 11 | .56  | .01 | .13 | 3   | 13272 | 125  |
| RE M45239          | 28  | 40  | 28  | 1805 | .7  | 216 | 11  | 218  | 1.96 | 19  | 5   | ND  | 4   | 98  | 12.5 | 6   | 2   | 127 | 2.61 | .075 | 10  | 14  | .64  | 1098 | .01 | 11 | .60  | .01 | .12 | 1   | 13509 | 115  |
| M45222             | 40  | 57  | 22  | 630  | 1.0 | 141 | 24  | 393  | 3.46 | 27  | 5   | ND  | 4   | 90  | 7.8  | 6   | 6   | 76  | .42  | .092 | 4   | 11  | .11  | 662  | .01 | 7  | .68  | .01 | .16 | 1   | 2783  | 90   |
| M45226             | 31  | 35  | 30  | 1055 | .3  | 161 | 12  | 225  | 1.91 | 20  | 5   | ND  | 4   | 81  | 6.4  | 6   | 2   | 168 | 3.79 | .138 | 13  | 14  | 1.50 | 857  | .01 | 15 | .42  | .01 | .12 | 1   | 16483 | 100  |
| M45237             | 31  | 52  | 32  | 2712 | .7  | 360 | 12  | 282  | 2.56 | 20  | 5   | ND  | 1   | 91  | 13.4 | 6   | 6   | 95  | 1.62 | .098 | 13  | 12  | .42  | 896  | .01 | 9  | .55  | .01 | .12 | 1   | 5172  | 130  |
| M45238             | 22  | 44  | 26  | 1906 | .5  | 230 | 11  | 220  | 2.40 | 19  | 5   | ND  | 1   | 96  | 8.3  | 5   | 2   | 68  | 1.31 | .089 | 11  | 11  | .36  | 1314 | .01 | 7  | .53  | .01 | .11 | 1   | 22007 | 100  |
| M45239             | 27  | 44  | 26  | 1821 | .7  | 217 | 11  | 226  | 1.93 | 20  | 5   | ND  | 2   | 96  | 12.6 | 5   | 3   | 124 | 2.49 | .074 | 10  | 13  | .62  | 1185 | .01 | 12 | .57  | .01 | .12 | 1   | 12698 | 120  |
| M45244             | 15  | 45  | 45  | 1292 | .7  | 104 | 12  | 235  | 2.48 | 18  | 5   | ND  | 2   | 67  | 6.4  | 5   | 2   | 59  | .60  | .062 | 4   | 12  | .18  | 1612 | .01 | 7  | .68  | .01 | .12 | 1   | 21395 | 105  |
| M45244 DUP.        | 30  | 41  | 93  | 1528 | .7  | 104 | 11  | 294  | 2.47 | 16  | 5   | ND  | 2   | 68  | 8.4  | 4   | 4   | 60  | .62  | .069 | 3   | 11  | .15  | 1332 | .01 | 7  | .64  | .01 | .11 | 1   | 8096  | 100  |
| M45246             | 6   | 35  | 24  | 508  | 1.0 | 74  | 10  | 172  | 2.14 | 12  | 5   | ND  | 2   | 75  | 3.6  | 2   | 5   | 43  | .63  | .071 | 5   | 14  | .24  | 1171 | .01 | 9  | .81  | .01 | .12 | 1   | 7009  | 135  |
| M45248             | 13  | 34  | 29  | 648  | .7  | 68  | 10  | 183  | 2.18 | 15  | 5   | ND  | 4   | 67  | 3.7  | 2   | 2   | 44  | .46  | .068 | 7   | 12  | .21  | 1337 | .01 | 8  | .66  | .01 | .10 | 1   | 50763 | 90   |
| M45274             | 34  | 57  | 209 | 2612 | .8  | 499 | 12  | 308  | 2.38 | 19  | 5   | ND  | 1   | 97  | 20.8 | 7   | 2   | 116 | 2.29 | .138 | 5   | 12  | .32  | 538  | .01 | 29 | .48  | .01 | .17 | 1   | 1958  | 185  |
| M45277             | 22  | 29  | 14  | 660  | .1  | 161 | 6   | 194  | 1.45 | 10  | 5   | ND  | 1   | 36  | 4.5  | 3   | 2   | 113 | 2.25 | .095 | 14  | 13  | .82  | 165  | .01 | 11 | .39  | .01 | .10 | 1   | 965   | 80   |
| M45278             | 19  | 26  | 11  | 599  | .2  | 123 | 6   | 164  | 1.16 | 13  | 5   | ND  | 2   | 65  | 3.7  | 3   | 2   | 133 | 5.83 | .176 | 15  | 15  | 2.29 | 424  | .01 | 13 | .36  | .01 | .12 | 1   | 3052  | 85   |
| M45279             | 18  | 23  | 11  | 527  | .1  | 114 | 6   | 156  | 1.32 | 11  | 5   | ND  | 3   | 42  | 3.5  | 2   | 2   | 119 | 3.14 | .123 | 18  | 14  | 1.36 | 245  | .01 | 14 | .38  | .01 | .09 | 1   | 1096  | 80   |
| M45280             | 22  | 27  | 9   | 1036 | .3  | 179 | 6   | 160  | 1.29 | 13  | 5   | ND  | 1   | 57  | 6.1  | 3   | 2   | 145 | 4.55 | .127 | 13  | 15  | 1.38 | 263  | .01 | 14 | .37  | .01 | .10 | 1   | 1132  | 125  |
| M45281             | 59  | 59  | 27  | 1429 | .1  | 228 | 14  | 268  | 2.38 | 25  | 5   | ND  | 2   | 69  | 6.3  | 10  | 3   | 219 | 2.44 | .099 | 9   | 16  | .81  | 490  | .01 | 12 | .40  | .01 | .12 | 1   | 1931  | 155  |
| M45282             | 19  | 42  | 35  | 522  | .8  | 91  | 10  | 221  | 2.59 | 16  | 5   | ND  | 1   | 62  | 3.8  | 2   | 2   | 57  | .74  | .059 | 4   | 11  | .21  | 1090 | .01 | 9  | .59  | .01 | .12 | 1   | 3847  | 135  |
| M45285             | 17  | 49  | 30  | 537  | .6  | 92  | 11  | 286  | 2.77 | 22  | 5   | ND  | 1   | 95  | 5.0  | 4   | 3   | 56  | .71  | .064 | 4   | 11  | .14  | 1264 | .01 | 11 | .63  | .01 | .12 | 1   | 27693 | 140  |
| M45287             | 18  | 36  | 21  | 614  | .3  | 87  | 11  | 234  | 1.98 | 17  | 5   | ND  | 5   | 96  | 3.7  | 2   | 4   | 62  | 4.20 | .095 | 18  | 9   | 1.62 | 780  | .01 | 7  | .48  | .01 | .12 | 1   | 43491 | 80   |
| STANDARD C/CB-1200 | 20  | 59  | 41  | 133  | 7.3 | 71  | 32  | 1075 | 3.96 | 41  | 19  | 7   | 41  | 53  | 18.9 | 14  | 21  | 59  | .50  | .083 | 39  | 61  | .94  | 183  | .09 | 35 | 1.94 | .07 | .14 | 11  | 2075  | 1650 |

Sample type: MOSS MAT. Samples beginning 'RE' are duplicate samples.





## GEOCHEMICAL ANALYSIS CERTIFICATE



Teck Exploration (BC) PROJECT 1715

File # 92-2722

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350 - 272 Victoria St., Kamloops BC V2C 2A2 Submitted by: RANDY FARMER

| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm   |
| L48+00N 39+00E     | 45  | 32  | 46  | 206 | .6  | 38  | 8   | 136  | 2.23 | 99  | 5   | ND  | 2   | 20  | .8   | 7   | 2   | 165 | .15 | .034 | 5   | 11  | .06 | 545  | .01 | 8  | .46  | .01 | .05 | 1   | 1827  |
| L48+00N 39+25E     | 28  | 46  | 58  | 766 | 1.6 | 102 | 8   | 222  | 2.65 | 13  | 5   | ND  | 2   | 86  | 7.0  | 3   | 2   | 102 | .77 | .078 | 6   | 15  | .14 | 1410 | .01 | 7  | .91  | .01 | .13 | 1   | 3667  |
| L48+00N 39+50E     | 26  | 20  | 33  | 246 | .1  | 33  | 4   | 37   | 2.09 | 15  | 5   | ND  | 1   | 26  | .3   | 3   | 2   | 178 | .02 | .039 | 4   | 11  | .04 | 197  | .01 | 5  | .78  | .01 | .06 | 1   | 1344  |
| L48+00N 39+75E     | 47  | 25  | 42  | 730 | .5  | 105 | 6   | 42   | 2.08 | 20  | 5   | ND  | 3   | 10  | .4   | 18  | 2   | 279 | .01 | .026 | 4   | 15  | .04 | 112  | .01 | 6  | .58  | .01 | .06 | 1   | 808   |
| L48+00N 40+00E     | 16  | 11  | 22  | 204 | .3  | 28  | 2   | 29   | 1.08 | 8   | 5   | ND  | 2   | 11  | .4   | 5   | 2   | 108 | .03 | .020 | 8   | 10  | .05 | 234  | .01 | 6  | .62  | .01 | .07 | 1   | 1228  |
| L48+00N 40+25E     | 23  | 18  | 35  | 316 | .9  | 58  | 4   | 28   | 1.50 | 10  | 5   | ND  | 1   | 18  | .3   | 5   | 2   | 106 | .02 | .027 | 5   | 12  | .04 | 365  | .01 | 6  | .62  | .01 | .06 | 1   | 1669  |
| L48+00N 40+50E     | 27  | 34  | 29  | 429 | .1  | 65  | 5   | 38   | 2.53 | 12  | 5   | ND  | 2   | 26  | .5   | 2   | 2   | 149 | .01 | .038 | 4   | 12  | .05 | 397  | .01 | 11 | .77  | .01 | .06 | 1   | 1453  |
| L48+00N 40+75E     | 17  | 40  | 17  | 446 | .6  | 64  | 5   | 54   | 1.95 | 7   | 5   | ND  | 2   | 20  | 3.5  | 2   | 2   | 30  | .18 | .015 | 3   | 6   | .04 | 557  | .01 | 11 | .37  | .01 | .12 | 1   | 2244  |
| L48+00N 41+00E     | 32  | 35  | 39  | 262 | .6  | 47  | 5   | 43   | 2.28 | 13  | 6   | ND  | 2   | 27  | 2.4  | 4   | 2   | 98  | .04 | .054 | 5   | 12  | .04 | 934  | .01 | 11 | .63  | .01 | .13 | 1   | 3019  |
| L48+00N 41+25E     | 24  | 17  | 25  | 208 | .1  | 36  | 4   | 41   | 1.86 | 10  | 5   | ND  | 1   | 18  | .9   | 4   | 2   | 123 | .02 | .037 | 5   | 11  | .04 | 565  | .01 | 8  | .74  | .01 | .08 | 1   | 2230  |
| L48+00N 41+50E     | 29  | 22  | 47  | 317 | .3  | 50  | 3   | 29   | 1.81 | 15  | 5   | ND  | 2   | 30  | 1.5  | 6   | 2   | 181 | .10 | .041 | 4   | 11  | .04 | 835  | .01 | 9  | .55  | .01 | .12 | 1   | 5798  |
| L48+00N 41+75E     | 23  | 17  | 30  | 236 | .6  | 35  | 3   | 25   | 1.85 | 16  | 5   | ND  | 2   | 34  | .6   | 4   | 2   | 142 | .06 | .035 | 5   | 11  | .05 | 840  | .01 | 8  | .66  | .01 | .10 | 2   | 5604  |
| L48+00N 42+00E     | 58  | 41  | 53  | 499 | 1.5 | 69  | 9   | 43   | 3.29 | 18  | 5   | ND  | 2   | 17  | .9   | 5   | 2   | 185 | .08 | .041 | 3   | 14  | .04 | 980  | .01 | 10 | .61  | .01 | .10 | 1   | 3682  |
| L48+00N 42+25E     | 43  | 35  | 73  | 498 | 1.8 | 76  | 5   | 35   | 2.81 | 23  | 5   | ND  | 3   | 31  | 2.1  | 8   | 2   | 215 | .03 | .059 | 7   | 17  | .09 | 1089 | .01 | 8  | .98  | .01 | .12 | 1   | 6306  |
| L48+00N 42+50E     | 28  | 23  | 62  | 483 | .5  | 42  | 3   | 42   | 2.25 | 16  | 5   | ND  | 1   | 43  | 2.4  | 7   | 2   | 208 | .03 | .058 | 6   | 15  | .08 | 760  | .01 | 8  | .94  | .01 | .13 | 1   | 4546  |
| L48+00N 42+75E     | 34  | 23  | 70  | 441 | .3  | 61  | 3   | 24   | 1.97 | 17  | 5   | ND  | 1   | 29  | .8   | 12  | 3   | 221 | .02 | .037 | 7   | 13  | .03 | 437  | .01 | 6  | .46  | .01 | .08 | 1   | 1367  |
| L48+00N 43+00E     | 37  | 24  | 75  | 336 | .2  | 54  | 3   | 29   | 1.99 | 15  | 5   | ND  | 2   | 34  | 1.0  | 6   | 3   | 203 | .05 | .041 | 6   | 14  | .05 | 981  | .01 | 7  | .72  | .01 | .10 | 1   | 5069  |
| L48+00N 43+25E     | 29  | 21  | 32  | 273 | .1  | 46  | 3   | 28   | 1.96 | 19  | 5   | ND  | 1   | 35  | .5   | 7   | 2   | 191 | .02 | .032 | 5   | 10  | .03 | 723  | .01 | 7  | .49  | .01 | .11 | 1   | 8749  |
| L48+00N 43+50E     | 98  | 42  | 34  | 566 | .1  | 164 | 5   | 40   | 1.99 | 24  | 5   | ND  | 1   | 15  | 1.1  | 25  | 2   | 526 | .07 | .030 | 5   | 23  | .04 | 663  | .01 | 8  | .55  | .01 | .07 | 1   | 1471  |
| L48+00N 43+75E     | 78  | 33  | 33  | 494 | .7  | 135 | 5   | 45   | 2.19 | 19  | 5   | ND  | 1   | 20  | .7   | 11  | 2   | 446 | .03 | .036 | 8   | 26  | .05 | 1013 | .01 | 7  | .85  | .01 | .09 | 1   | 3477  |
| L48+00N 44+00E     | 61  | 27  | 15  | 405 | .1  | 99  | 4   | 38   | 1.68 | 14  | 5   | ND  | 1   | 15  | 1.0  | 8   | 2   | 350 | .04 | .043 | 7   | 23  | .04 | 1403 | .01 | 10 | .62  | .01 | .07 | 1   | 4836  |
| L48+00N 44+25E     | 112 | 59  | 32  | 697 | .7  | 150 | 3   | 30   | 2.33 | 43  | 5   | ND  | 1   | 16  | 1.1  | 37  | 2   | 722 | .03 | .038 | 12  | 40  | .04 | 1111 | .01 | 7  | .66  | .01 | .06 | 1   | 2256  |
| L48+00N 44+50E     | 22  | 25  | 26  | 261 | .5  | 42  | 4   | 35   | 2.28 | 16  | 5   | ND  | 3   | 46  | .6   | 7   | 2   | 172 | .02 | .047 | 6   | 13  | .06 | 683  | .01 | 8  | .84  | .01 | .14 | 1   | 3966  |
| L48+00N 44+75E     | 23  | 22  | 23  | 196 | .1  | 30  | 2   | 21   | 1.74 | 10  | 5   | ND  | 3   | 47  | .2   | 2   | 3   | 134 | .02 | .041 | 8   | 16  | .05 | 502  | .01 | 5  | .99  | .01 | .11 | 1   | 1623  |
| L48+00N 45+00E     | 48  | 68  | 45  | 489 | .6  | 102 | 5   | 32   | 2.94 | 26  | 6   | ND  | 2   | 85  | 3.1  | 9   | 2   | 265 | .18 | .073 | 8   | 18  | .10 | 804  | .01 | 6  | .80  | .03 | .17 | 1   | 3180  |
| L48+00N 45+25E     | 29  | 50  | 32  | 284 | .4  | 61  | 4   | 29   | 1.93 | 16  | 5   | ND  | 2   | 47  | 1.4  | 5   | 2   | 175 | .09 | .063 | 7   | 14  | .07 | 1063 | .01 | 7  | .75  | .01 | .14 | 1   | 5481  |
| L48+00N 45+50E     | 18  | 43  | 23  | 240 | .3  | 51  | 8   | 173  | 3.28 | 18  | 5   | ND  | 4   | 69  | 1.1  | 2   | 2   | 87  | .12 | .076 | 15  | 21  | .37 | 572  | .01 | 5  | 1.09 | .02 | .12 | 1   | 8555  |
| L48+00N 45+75E     | 16  | 45  | 23  | 180 | .5  | 29  | 3   | 41   | 2.45 | 15  | 5   | ND  | 1   | 64  | .7   | 2   | 2   | 108 | .04 | .080 | 7   | 14  | .09 | 726  | .01 | 7  | .98  | .01 | .15 | 1   | 3382  |
| L48+00N 46+00E     | 19  | 30  | 22  | 175 | .6  | 25  | 2   | 22   | 2.43 | 18  | 5   | ND  | 1   | 72  | .3   | 3   | 2   | 109 | .01 | .066 | 3   | 9   | .04 | 455  | .01 | 7  | .64  | .01 | .15 | 1   | 13916 |
| L48+00N 46+25E     | 13  | 18  | 14  | 134 | .4  | 17  | 2   | 27   | 1.61 | 7   | 5   | ND  | 1   | 21  | .3   | 2   | 2   | 126 | .03 | .034 | 6   | 11  | .05 | 812  | .01 | 6  | .71  | .01 | .09 | 1   | 1617  |
| L48+00N 46+50E     | 17  | 20  | 25  | 159 | .6  | 21  | 2   | 21   | 2.19 | 16  | 5   | ND  | 2   | 44  | .3   | 3   | 2   | 115 | .02 | .047 | 4   | 9   | .04 | 509  | .01 | 7  | .64  | .02 | .16 | 1   | 1795  |
| L48+00N 46+75E     | 21  | 42  | 24  | 257 | .7  | 41  | 4   | 68   | 3.52 | 21  | 5   | ND  | 3   | 89  | .7   | 3   | 2   | 89  | .07 | .088 | 8   | 17  | .19 | 245  | .01 | 6  | .93  | .02 | .16 | 1   | 13093 |
| L48+00N 47+00E     | 39  | 43  | 33  | 215 | .8  | 32  | 3   | 27   | 2.85 | 27  | 5   | ND  | 1   | 130 | 1.4  | 3   | 3   | 152 | .05 | .091 | 7   | 14  | .05 | 357  | .01 | 8  | .75  | .02 | .17 | 1   | 12207 |
| L48+00N 47+25E     | 24  | 39  | 26  | 184 | 1.3 | 26  | 2   | 28   | 3.33 | 25  | 5   | ND  | 1   | 65  | 1.4  | 7   | 2   | 125 | .04 | .096 | 5   | 12  | .06 | 389  | .01 | 7  | .75  | .02 | .21 | 1   | 4494  |
| L48+00N 47+50E     | 27  | 30  | 24  | 184 | .8  | 28  | 3   | 27   | 3.32 | 32  | 5   | ND  | 3   | 68  | .6   | 6   | 3   | 168 | .01 | .068 | 4   | 11  | .06 | 293  | .01 | 7  | .81  | .02 | .22 | 1   | 3138  |
| RE L48+00N 46+50E  | 19  | 21  | 26  | 157 | .2  | 21  | 2   | 18   | 2.16 | 15  | 5   | ND  | 1   | 45  | .4   | 2   | 2   | 117 | .02 | .047 | 3   | 9   | .04 | 510  | .01 | 8  | .64  | .02 | .15 | 1   | 1964  |
| L48+00N 47+75E     | 20  | 23  | 24  | 138 | .1  | 21  | 2   | 21   | 2.24 | 13  | 5   | ND  | 1   | 54  | .2   | 2   | 2   | 146 | .03 | .049 | 3   | 11  | .05 | 382  | .01 | 7  | .77  | .02 | .18 | 1   | 6440  |
| STANDARD C/CB-1200 | 17  | 61  | 38  | 135 | 6.9 | 77  | 31  | 1082 | 3.96 | 41  | 23  | 7   | 39  | 53  | 19.0 | 14  | 20  | 60  | .50 | .087 | 39  | 61  | .90 | 185  | .09 | 35 | 1.95 | .08 | .16 | 11  | 2204  |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: SOIL BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP  
 Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 22 1992

DATE REPORT MAILED:

Aug 28/92

SIGNED BY: .....

D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



## Teck Exploration (BC) PROJECT 1715 FILE # 92-2722

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| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*  |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm  |
| L48+00N 48+00E     | 9   | 16  | 19  | 97  | .3  | 15  | 4   | 40   | 1.29 | 6   | 5   | ND  | 8   | 19  | .4   | 2   | 2   | 96  | .08 | .035 | 7   | 13  | .07 | 247  | .01 | 3   | .87  | .01 | .12 | 2   | 1113 |
| L48+00N 48+25E     | 20  | 56  | 23  | 150 | .1  | 32  | 4   | 31   | 1.83 | 7   | 5   | ND  | 2   | 48  | 2.5  | 2   | 2   | 161 | .17 | .094 | 3   | 18  | .06 | 695  | .01 | 10  | .90  | .01 | .15 | 1   | 1694 |
| L48+00N 48+50E     | 27  | 21  | 23  | 192 | .4  | 16  | 4   | 34   | 2.58 | 20  | 5   | ND  | 1   | 53  | .8   | 7   | 2   | 123 | .16 | .065 | 3   | 10  | .09 | 555  | .01 | 4   | .61  | .01 | .17 | 1   | 1650 |
| L48+00N 48+75E     | 18  | 34  | 25  | 233 | .9  | 32  | 5   | 178  | 2.06 | 10  | 8   | ND  | 1   | 70  | 3.4  | 3   | 2   | 112 | .46 | .103 | 5   | 18  | .23 | 1160 | .01 | 2   | 1.20 | .01 | .18 | 1   | 2569 |
| L48+00N 49+00E     | 24  | 43  | 28  | 211 | .5  | 40  | 6   | 69   | 2.99 | 24  | 5   | ND  | 1   | 57  | 3.1  | 10  | 2   | 133 | .22 | .098 | 5   | 16  | .13 | 842  | .01 | 6   | 1.05 | .01 | .18 | 1   | 2859 |
| L48+00N 49+25E     | 20  | 35  | 21  | 175 | .6  | 28  | 5   | 46   | 2.95 | 19  | 5   | ND  | 2   | 49  | .5   | 2   | 2   | 87  | .04 | .071 | 6   | 12  | .10 | 693  | .01 | 2   | .92  | .01 | .12 | 1   | 6470 |
| L48+00N 49+50E     | 17  | 24  | 35  | 155 | 1.3 | 19  | 4   | 32   | 2.63 | 12  | 5   | ND  | 1   | 87  | .2   | 2   | 2   | 102 | .04 | .106 | 6   | 13  | .05 | 491  | .01 | 2   | .88  | .02 | .16 | 1   | 1463 |
| L48+00N 49+75E     | 17  | 15  | 21  | 111 | .4  | 17  | 4   | 32   | 2.03 | 13  | 5   | ND  | 1   | 35  | .3   | 2   | 3   | 139 | .03 | .048 | 8   | 16  | .10 | 467  | .01 | 6   | 1.18 | .01 | .11 | 1   | 1246 |
| L48+00N 50+00E     | 25  | 20  | 38  | 85  | .5  | 16  | 2   | 21   | 1.24 | 9   | 5   | ND  | 1   | 55  | .9   | 3   | 2   | 172 | .18 | .046 | 5   | 14  | .06 | 754  | .01 | 7   | .94  | .01 | .13 | 1   | 2083 |
| L44+00N 35+00E     | 14  | 42  | 20  | 254 | .4  | 34  | 10  | 61   | 5.31 | 10  | 5   | ND  | 2   | 21  | .4   | 2   | 5   | 91  | .02 | .076 | 2   | 20  | .11 | 303  | .01 | 6   | 1.62 | .01 | .11 | 1   | 2219 |
| L44+00N 35+25E     | 12  | 19  | 19  | 169 | .5  | 20  | 6   | 79   | 2.50 | 11  | 5   | ND  | 3   | 29  | .5   | 2   | 3   | 73  | .06 | .051 | 5   | 14  | .09 | 365  | .01 | 5   | 1.04 | .01 | .14 | 1   | 2398 |
| L44+00N 35+50E     | 10  | 12  | 15  | 168 | .2  | 16  | 6   | 44   | 2.34 | 5   | 5   | ND  | 1   | 13  | .2   | 2   | 2   | 76  | .03 | .036 | 4   | 13  | .06 | 319  | .01 | 2   | 1.15 | .01 | .12 | 1   | 2161 |
| L44+00N 35+75E     | 48  | 22  | 18  | 776 | .8  | 28  | 11  | 40   | 4.45 | 21  | 5   | ND  | 2   | 51  | .4   | 2   | 2   | 95  | .03 | .066 | 3   | 9   | .04 | 456  | .01 | 2   | .78  | .01 | .15 | 1   | 3014 |
| L44+00N 36+00E     | 22  | 17  | 17  | 127 | .6  | 14  | 4   | 27   | 2.62 | 15  | 5   | ND  | 2   | 45  | .2   | 2   | 5   | 108 | .01 | .056 | 5   | 15  | .07 | 362  | .01 | 3   | 1.16 | .01 | .12 | 1   | 2230 |
| L44+00N 36+25E     | 24  | 18  | 15  | 134 | .5  | 16  | 4   | 24   | 1.97 | 12  | 5   | ND  | 2   | 69  | .2   | 2   | 2   | 121 | .02 | .047 | 4   | 10  | .05 | 402  | .01 | 2   | .85  | .02 | .12 | 1   | 2084 |
| L44+00N 36+50E     | 23  | 15  | 16  | 151 | .4  | 15  | 5   | 26   | 1.77 | 9   | 5   | ND  | 1   | 28  | .2   | 2   | 3   | 143 | .01 | .040 | 7   | 12  | .05 | 213  | .01 | 7   | .89  | .01 | .07 | 1   | 2450 |
| L44+00N 36+75E     | 33  | 29  | 40  | 208 | .3  | 30  | 7   | 46   | 2.38 | 13  | 5   | ND  | 1   | 70  | .2   | 2   | 2   | 113 | .03 | .069 | 6   | 12  | .04 | 272  | .01 | 3   | .73  | .01 | .10 | 1   | 2163 |
| L44+00N 37+00E     | 24  | 29  | 54  | 151 | 1.4 | 26  | 5   | 24   | 2.18 | 13  | 5   | ND  | 2   | 157 | .2   | 2   | 2   | 67  | .06 | .070 | 2   | 13  | .04 | 403  | .01 | 8   | .69  | .03 | .16 | 1   | 2995 |
| L44+00N 37+25E     | 24  | 37  | 34  | 315 | .9  | 51  | 11  | 172  | 3.37 | 14  | 5   | ND  | 1   | 31  | .4   | 2   | 2   | 121 | .03 | .065 | 4   | 12  | .04 | 255  | .01 | 8   | .85  | .01 | .09 | 1   | 1355 |
| L44+00N 37+50E     | 26  | 28  | 37  | 259 | .5  | 40  | 7   | 59   | 2.36 | 15  | 5   | ND  | 1   | 41  | .2   | 2   | 2   | 109 | .02 | .041 | 6   | 13  | .04 | 349  | .01 | 3   | .69  | .01 | .09 | 1   | 1670 |
| L44+00N 37+75E     | 28  | 41  | 29  | 189 | .2  | 30  | 7   | 50   | 2.13 | 13  | 5   | ND  | 1   | 25  | .2   | 2   | 2   | 101 | .01 | .031 | 2   | 11  | .04 | 243  | .01 | 6   | .83  | .01 | .07 | 1   | 1413 |
| L44+00N 38+00E     | 30  | 29  | 41  | 309 | .4  | 47  | 8   | 59   | 2.49 | 14  | 5   | ND  | 2   | 20  | .2   | 3   | 2   | 180 | .01 | .030 | 6   | 15  | .05 | 189  | .01 | 4   | .92  | .01 | .08 | 1   | 1070 |
| L44+00N 38+25E     | 33  | 26  | 47  | 335 | .2  | 52  | 7   | 62   | 2.57 | 20  | 5   | ND  | 1   | 33  | .2   | 3   | 2   | 172 | .02 | .047 | 6   | 14  | .05 | 568  | .01 | 6   | .65  | .01 | .11 | 1   | 2036 |
| L44+00N 38+50E     | 35  | 30  | 62  | 373 | .4  | 56  | 7   | 50   | 2.47 | 17  | 6   | ND  | 2   | 28  | .4   | 5   | 2   | 172 | .02 | .053 | 6   | 15  | .04 | 523  | .01 | 4   | .75  | .01 | .10 | 1   | 1644 |
| L44+00N 38+75E     | 33  | 41  | 62  | 369 | .3  | 65  | 10  | 353  | 3.15 | 12  | 5   | ND  | 1   | 88  | 2.1  | 2   | 2   | 135 | .49 | .087 | 4   | 18  | .16 | 1243 | .01 | 6   | 1.02 | .01 | .16 | 1   | 3237 |
| L44+00N 39+00E     | 31  | 26  | 45  | 287 | .6  | 44  | 6   | 59   | 1.99 | 15  | 5   | ND  | 1   | 24  | .7   | 4   | 2   | 186 | .03 | .064 | 7   | 17  | .05 | 626  | .01 | 4   | .93  | .01 | .10 | 1   | 1974 |
| L44+00N 39+25E     | 37  | 34  | 54  | 428 | .6  | 69  | 8   | 120  | 2.94 | 21  | 5   | ND  | 2   | 38  | 1.0  | 4   | 2   | 197 | .05 | .089 | 7   | 18  | .11 | 617  | .01 | 10  | .88  | .01 | .11 | 1   | 2050 |
| L44+00N 39+50E     | 37  | 47  | 61  | 474 | .4  | 65  | 10  | 124  | 2.89 | 18  | 5   | ND  | 1   | 29  | 2.0  | 2   | 2   | 142 | .06 | .065 | 7   | 16  | .10 | 624  | .01 | 10  | .73  | .01 | .10 | 1   | 2350 |
| RE L44+00N 38+50E  | 34  | 29  | 58  | 366 | .4  | 56  | 7   | 50   | 2.43 | 15  | 5   | ND  | 1   | 28  | .2   | 2   | 2   | 170 | .02 | .052 | 5   | 15  | .04 | 515  | .01 | 7   | .77  | .01 | .09 | 1   | 1708 |
| L44+00N 39+75E     | 28  | 28  | 31  | 253 | .2  | 43  | 5   | 46   | 1.90 | 8   | 5   | ND  | 1   | 15  | .3   | 2   | 2   | 148 | .02 | .048 | 6   | 15  | .04 | 327  | .01 | 6   | .81  | .01 | .09 | 1   | 1582 |
| L44+00N 40+00E     | 22  | 25  | 29  | 202 | .1  | 31  | 5   | 43   | 1.66 | 6   | 5   | ND  | 1   | 14  | .5   | 2   | 2   | 128 | .02 | .046 | 8   | 16  | .05 | 430  | .01 | 7   | 1.02 | .01 | .07 | 1   | 1390 |
| L44+00N 40+25E     | 34  | 27  | 37  | 295 | .3  | 48  | 7   | 63   | 2.35 | 12  | 5   | ND  | 1   | 17  | .2   | 2   | 2   | 202 | .02 | .042 | 6   | 13  | .04 | 307  | .01 | 5   | .63  | .01 | .08 | 1   | 1366 |
| L44+00N 40+50E     | 38  | 32  | 53  | 301 | .6  | 48  | 7   | 56   | 2.47 | 14  | 5   | ND  | 1   | 21  | .2   | 3   | 2   | 190 | .02 | .047 | 5   | 15  | .05 | 327  | .01 | 7   | .83  | .01 | .09 | 1   | 1410 |
| L44+00N 40+75E     | 29  | 33  | 33  | 262 | .8  | 43  | 8   | 75   | 2.58 | 14  | 5   | ND  | 1   | 22  | .2   | 2   | 5   | 173 | .04 | .061 | 5   | 14  | .04 | 418  | .01 | 9   | .77  | .01 | .11 | 1   | 1705 |
| L44+00N 41+00E     | 32  | 25  | 42  | 286 | .7  | 48  | 7   | 51   | 2.25 | 14  | 5   | ND  | 1   | 17  | .2   | 2   | 2   | 175 | .01 | .042 | 4   | 13  | .05 | 469  | .01 | 7   | .82  | .01 | .09 | 1   | 1616 |
| L44+00N 41+25E     | 34  | 40  | 31  | 278 | .2  | 50  | 12  | 82   | 3.28 | 22  | 5   | ND  | 2   | 19  | .5   | 2   | 2   | 149 | .02 | .033 | 4   | 10  | .03 | 342  | .01 | 7   | .52  | .01 | .12 | 1   | 1593 |
| L44+00N 41+50E     | 28  | 29  | 38  | 204 | .2  | 35  | 7   | 50   | 2.45 | 20  | 5   | ND  | 1   | 19  | .4   | 2   | 2   | 125 | .02 | .032 | 5   | 11  | .05 | 294  | .01 | 3   | .66  | .01 | .10 | 1   | 1458 |
| STANDARD C/CB-1200 | 20  | 60  | 38  | 136 | 7.2 | 72  | 32  | 1081 | 3.96 | 41  | 22  | 7   | 40  | 53  | 18.6 | 13  | 19  | 60  | .49 | .084 | 39  | 61  | .94 | 183  | .09 | 35  | 2.02 | .07 | .14 | 10  | 2081 |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



## Teck Exploration (BC) PROJECT 1715 FILE # 92-2722

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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe    | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V    | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*    |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|------|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|--------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %     | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm  | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm    |
| L44+00N 41+75E     | 34  | 28  | 48  | 278  | .4  | 48  | 7   | 56   | 2.86  | 18  | 5   | ND  | 8   | 22  | .2   | 5   | 2   | 174  | .02 | .044 | 5   | 15  | .06 | 400  | .01 | 6   | .95  | .01 | .09 | 2   | 1552   |
| L44+00N 42+00E     | 29  | 23  | 41  | 241  | .1  | 45  | 6   | 44   | 2.02  | 13  | 5   | ND  | 2   | 20  | .4   | 4   | 2   | 188  | .02 | .029 | 4   | 13  | .05 | 369  | .01 | 4   | .89  | .01 | .08 | 1   | 1226   |
| L44+00N 42+25E     | 25  | 27  | 23  | 130  | .2  | 29  | 6   | 47   | 1.59  | 9   | 6   | ND  | 1   | 22  | .9   | 2   | 2   | 109  | .05 | .045 | 8   | 16  | .05 | 694  | .01 | 7   | .90  | .01 | .08 | 1   | 1793   |
| L44+00N 42+50E     | 24  | 29  | 22  | 145  | .1  | 31  | 7   | 53   | 2.01  | 4   | 5   | ND  | 1   | 72  | .6   | 2   | 2   | 110  | .02 | .043 | 7   | 13  | .05 | 401  | .01 | 8   | .90  | .01 | .07 | 1   | 1761   |
| L44+00N 42+75E     | 35  | 45  | 28  | 209  | .4  | 57  | 14  | 157  | 4.50  | 13  | 5   | ND  | 1   | 16  | .7   | 2   | 2   | 126  | .01 | .062 | 3   | 15  | .05 | 271  | .01 | 8   | .99  | .01 | .08 | 1   | 1777   |
| L44+00N 43+00E     | 32  | 58  | 125 | 369  | .6  | 76  | 27  | 822  | 10.53 | 2   | 5   | ND  | 1   | 17  | .3   | 2   | 3   | 80   | .08 | .098 | 3   | 17  | .05 | 672  | .01 | 8   | .76  | .01 | .09 | 1   | 3026   |
| L44+00N 43+25E     | 102 | 51  | 213 | 1068 | 3.0 | 92  | 11  | 157  | 5.56  | 34  | 5   | ND  | 1   | 13  | 1.3  | 19  | 5   | 629  | .04 | .118 | 3   | 24  | .04 | 510  | .01 | 10  | .84  | .01 | .07 | 1   | 1733   |
| L44+00N 43+50E     | 66  | 32  | 194 | 1119 | .2  | 104 | 5   | 48   | 2.86  | 39  | 6   | ND  | 1   | 13  | 1.3  | 16  | 3   | 743  | .05 | .055 | 2   | 33  | .06 | 1238 | .01 | 10  | 1.06 | .01 | .08 | 1   | 2592   |
| RE L44+00N 44+75E  | 71  | 42  | 60  | 406  | .4  | 103 | 6   | 42   | 2.13  | 27  | 6   | ND  | 1   | 37  | .9   | 19  | 2   | 577  | .02 | .084 | 4   | 30  | .05 | 756  | .01 | 7   | .85  | .01 | .11 | 1   | 3836   |
| L44+00N 43+75E     | 61  | 48  | 429 | 785  | .5  | 83  | 7   | 84   | 4.81  | 28  | 5   | ND  | 2   | 17  | 1.3  | 16  | 5   | 407  | .03 | .072 | 2   | 25  | .05 | 583  | .01 | 6   | .96  | .01 | .10 | 1   | 1900   |
| L44+00N 44+00E     | 123 | 51  | 197 | 442  | .1  | 92  | 7   | 52   | 3.64  | 34  | 5   | ND  | 1   | 43  | 1.1  | 16  | 2   | 647  | .05 | .087 | 5   | 30  | .06 | 666  | .01 | 9   | .94  | .01 | .12 | 1   | 2123   |
| L44+00N 44+25E     | 194 | 71  | 484 | 549  | .2  | 63  | 4   | 17   | 2.87  | 42  | 5   | ND  | 1   | 24  | 2.6  | 38  | 3   | 878  | .04 | .094 | 3   | 41  | .04 | 511  | .01 | 10  | .82  | .01 | .12 | 1   | 1456   |
| L44+00N 44+50E     | 110 | 53  | 70  | 548  | .2  | 145 | 6   | 40   | 2.08  | 25  | 7   | ND  | 1   | 16  | 3.7  | 23  | 2   | 621  | .07 | .114 | 4   | 40  | .05 | 963  | .01 | 8   | .89  | .01 | .09 | 1   | 1954   |
| L44+00N 44+75E     | 70  | 43  | 53  | 363  | .2  | 97  | 6   | 36   | 2.00  | 24  | 5   | ND  | 1   | 37  | .8   | 17  | 2   | 550  | .02 | .080 | 4   | 28  | .04 | 801  | .01 | 10  | .81  | .01 | .11 | 1   | 3740   |
| L44+00N 45+00E     | 50  | 39  | 88  | 304  | .3  | 68  | 7   | 34   | 2.93  | 24  | 5   | ND  | 1   | 78  | .4   | 6   | 2   | 313  | .01 | .078 | 3   | 20  | .05 | 440  | .01 | 11  | .87  | .02 | .18 | 1   | 2501   |
| L44+00N 45+25E     | 388 | 221 | 119 | 936  | .5  | 367 | 10  | 64   | 3.23  | 83  | 20  | ND  | 1   | 31  | 28.0 | 78  | 3   | 1591 | .07 | .086 | 11  | 82  | .05 | 766  | .01 | 9   | 1.04 | .01 | .16 | 1   | 2005   |
| L44+00N 45+50E     | 21  | 31  | 51  | 237  | .6  | 45  | 7   | 60   | 2.73  | 20  | 5   | ND  | 1   | 89  | .8   | 4   | 2   | 142  | .02 | .078 | 4   | 15  | .04 | 566  | .01 | 6   | .64  | .01 | .16 | 1   | 3345   |
| L44+00N 45+75E     | 17  | 31  | 52  | 245  | 1.6 | 46  | 9   | 37   | 3.90  | 27  | 8   | ND  | 3   | 84  | .3   | 6   | 5   | 116  | .01 | .080 | 4   | 15  | .04 | 399  | .01 | 7   | .82  | .03 | .21 | 1   | 3265   |
| L44+00N 46+00E     | 15  | 25  | 46  | 210  | .8  | 40  | 6   | 30   | 2.78  | 27  | 6   | ND  | 3   | 85  | .2   | 4   | 2   | 120  | .01 | .067 | 4   | 14  | .05 | 516  | .01 | 4   | .87  | .02 | .17 | 1   | 3290   |
| L44+00N 46+25E     | 11  | 22  | 31  | 142  | 1.1 | 29  | 6   | 62   | 2.38  | 16  | 5   | ND  | 1   | 50  | .2   | 2   | 2   | 91   | .01 | .051 | 6   | 15  | .04 | 505  | .02 | 4   | .58  | .01 | .14 | 1   | 13550  |
| L44+00N 46+50E     | 10  | 25  | 29  | 150  | .9  | 33  | 6   | 54   | 2.15  | 18  | 8   | ND  | 1   | 46  | .2   | 2   | 2   | 99   | .04 | .095 | 6   | 17  | .06 | 839  | .01 | 5   | .77  | .01 | .13 | 1   | 7563   |
| L44+00N 46+75E     | 8   | 20  | 35  | 99   | .7  | 23  | 3   | 17   | 1.85  | 8   | 5   | ND  | 1   | 73  | .2   | 2   | 2   | 77   | .02 | .082 | 3   | 15  | .05 | 584  | .01 | 6   | .90  | .03 | .17 | 1   | 6183   |
| L44+00N 47+00E     | 13  | 14  | 34  | 45   | .1  | 7   | 2   | 14   | 1.02  | 11  | 5   | ND  | 1   | 65  | .2   | 2   | 4   | 104  | .01 | .045 | 3   | 12  | .04 | 433  | .01 | 5   | .61  | .01 | .13 | 1   | 114414 |
| L44+00N 47+25E     | 10  | 18  | 12  | 34   | .1  | 11  | 1   | 11   | .57   | 6   | 5   | ND  | 1   | 21  | .2   | 2   | 2   | 102  | .01 | .032 | 2   | 10  | .03 | 1142 | .01 | 6   | .47  | .01 | .09 | 1   | 3217   |
| L44+00N 47+50E     | 14  | 15  | 20  | 117  | .2  | 25  | 5   | 61   | 1.67  | 6   | 5   | ND  | 1   | 26  | .2   | 2   | 2   | 142  | .04 | .050 | 6   | 17  | .07 | 714  | .01 | 4   | 1.16 | .01 | .09 | 1   | 1980   |
| L44+00N 47+75E     | 34  | 29  | 31  | 99   | .5  | 21  | 4   | 44   | 2.22  | 12  | 6   | ND  | 2   | 88  | .5   | 4   | 2   | 151  | .03 | .075 | 5   | 15  | .05 | 176  | .01 | 5   | .81  | .02 | .22 | 1   | 3256   |
| L44+00N 48+00E     | 22  | 20  | 17  | 138  | .3  | 30  | 5   | 45   | 1.44  | 9   | 7   | ND  | 1   | 18  | .2   | 2   | 2   | 151  | .04 | .061 | 11  | 17  | .05 | 278  | .01 | 5   | .84  | .01 | .08 | 1   | 1052   |
| L44+00N 48+25E     | 13  | 14  | 17  | 107  | .9  | 26  | 7   | 94   | 2.82  | 16  | 5   | ND  | 1   | 22  | .2   | 3   | 2   | 165  | .06 | .048 | 12  | 27  | .35 | 208  | .02 | 4   | 1.55 | .01 | .09 | 1   | 1179   |
| L44+00N 48+50E     | 22  | 19  | 23  | 112  | .2  | 26  | 5   | 50   | 1.83  | 18  | 5   | ND  | 1   | 33  | .2   | 2   | 2   | 80   | .03 | .047 | 8   | 14  | .07 | 306  | .01 | 6   | .79  | .01 | .13 | 1   | 1293   |
| L44+00N 48+75E     | 16  | 27  | 28  | 168  | .6  | 20  | 6   | 49   | 2.99  | 19  | 5   | ND  | 1   | 40  | .2   | 6   | 2   | 160  | .02 | .066 | 5   | 15  | .06 | 354  | .01 | 7   | 1.08 | .01 | .18 | 1   | 1308   |
| L44+00N 49+00E     | 17  | 27  | 17  | 248  | .4  | 22  | 6   | 61   | 3.56  | 16  | 5   | ND  | 1   | 28  | .4   | 8   | 2   | 157  | .02 | .064 | 5   | 16  | .07 | 307  | .01 | 6   | .94  | .03 | .19 | 1   | 1300   |
| L44+00N 49+25E     | 13  | 13  | 12  | 123  | .1  | 8   | 3   | 12   | 1.85  | 15  | 5   | ND  | 1   | 7   | .2   | 13  | 2   | 171  | .02 | .038 | 2   | 13  | .07 | 207  | .01 | 6   | 1.10 | .01 | .13 | 1   | 1317   |
| L44+00N 49+50E     | 16  | 33  | 24  | 245  | 1.1 | 18  | 5   | 37   | 3.33  | 21  | 5   | ND  | 1   | 30  | .7   | 15  | 2   | 164  | .02 | .069 | 3   | 14  | .06 | 385  | .01 | 5   | 1.07 | .02 | .19 | 1   | 1532   |
| L44+00N 49+75E     | 8   | 21  | 23  | 112  | .8  | 11  | 3   | 28   | 1.82  | 5   | 6   | ND  | 1   | 14  | .8   | 6   | 2   | 132  | .01 | .047 | 4   | 17  | .07 | 285  | .01 | 3   | 1.19 | .01 | .16 | 1   | 1225   |
| L44+00N 50+00E     | 8   | 20  | 33  | 122  | .8  | 15  | 4   | 42   | 2.26  | 12  | 5   | ND  | 1   | 35  | .3   | 2   | 2   | 117  | .02 | .059 | 5   | 17  | .07 | 370  | .01 | 2   | 1.18 | .02 | .17 | 1   | 1526   |
| STANDARD C/CB-1200 | 20  | 63  | 39  | 135  | 7.3 | 71  | 32  | 1068 | 3.96  | 42  | 21  | 7   | 39  | 53  | 18.6 | 15  | 21  | 59   | .50 | .085 | 39  | 60  | .95 | 183  | .09 | 34  | 1.99 | .07 | .14 | 10  | 2287   |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.

# NOD GRID SOILS

ACME ANALYTICAL LABORATORIES LTD.

852 E. HASTINGS ST. VANCOUVER B.C. V6A 1R6

PHONE (604) 253-3158

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## GEOCHEMICAL ANALYSIS CERTIFICATE

Teck Exploration (BC) PROJECT 1715 File # 92-2519

Page

350 - 272 Victoria St., Kamloops BC V2C 2A2



| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm   |
| L56+00N 45+00E     | 24  | 15  | 14  | 114 | .3  | 24  | 2   | 15   | 1.19 | 11  | 5   | ND  | 3   | 30  | 1.8  | 6   | 2   | 118 | .04  | .023 | 4   | 10  | .04 | 787  | .01 | 13 | .44  | .01 | .15 | 1   | 2539  |
| L56+00N 45+50E     | 20  | 18  | 16  | 113 | .1  | 19  | 1   | 6    | 1.26 | 10  | 5   | ND  | 1   | 41  | 2.1  | 2   | 2   | 71  | .04  | .031 | 3   | 7   | .02 | 594  | .01 | 10 | .33  | .01 | .14 | 1   | 2972  |
| L56+00N 46+00E     | 12  | 10  | 9   | 72  | .1  | 13  | 1   | 11   | .73  | 3   | 5   | ND  | 1   | 26  | 2.3  | 2   | 2   | 83  | .13  | .020 | 4   | 7   | .03 | 711  | .01 | 10 | .41  | .01 | .11 | 1   | 1647  |
| L56+00N 46+50E     | 24  | 31  | 21  | 145 | .3  | 26  | 2   | 12   | 1.63 | 13  | 5   | ND  | 1   | 51  | 2.3  | 3   | 2   | 106 | .05  | .044 | 4   | 9   | .03 | 658  | .01 | 11 | .48  | .02 | .15 | 1   | 5145  |
| L56+00N 47+00E     | 17  | 10  | 13  | 80  | .1  | 11  | 1   | 5    | .88  | 7   | 5   | ND  | 1   | 29  | .4   | 2   | 2   | 60  | .04  | .022 | 3   | 6   | .03 | 275  | .01 | 10 | .37  | .01 | .12 | 1   | 1079  |
| L56+00N 47+50E     | 5   | 10  | 13  | 27  | .3  | 5   | 1   | 2    | .25  | 2   | 5   | ND  | 1   | 10  | .4   | 2   | 2   | 59  | .02  | .009 | 2   | 7   | .03 | 394  | .01 | 9  | .40  | .01 | .09 | 1   | 2131  |
| L56+00N 48+00E     | 64  | 15  | 40  | 76  | .9  | 12  | 1   | 15   | 2.38 | 13  | 5   | ND  | 1   | 105 | 1.3  | 3   | 2   | 92  | .16  | .040 | 5   | 10  | .05 | 254  | .01 | 16 | .46  | .03 | .30 | 1   | 1623  |
| L56+00N 48+50E     | 56  | 13  | 19  | 80  | .2  | 17  | 2   | 21   | 1.98 | 22  | 5   | ND  | 1   | 59  | .2   | 5   | 2   | 194 | .05  | .032 | 6   | 9   | .04 | 719  | .01 | 7  | .43  | .02 | .15 | 1   | 2336  |
| L56+00N 49+00E     | 8   | 9   | 8   | 60  | .4  | 11  | 1   | 11   | .61  | 2   | 5   | ND  | 1   | 14  | .7   | 2   | 2   | 108 | .07  | .028 | 5   | 14  | .03 | 332  | .01 | 9  | .52  | .01 | .10 | 1   | 1264  |
| L56+00N 49+50E     | 9   | 140 | 13  | 759 | 1.6 | 116 | 10  | 143  | 1.90 | 10  | 5   | ND  | 1   | 96  | 52.9 | 6   | 2   | 82  | .90  | .082 | 8   | 12  | .18 | 460  | .01 | 6  | .87  | .01 | .14 | 1   | 1447  |
| L56+00N 50+00E     | 26  | 39  | 20  | 369 | .5  | 43  | 6   | 33   | 3.80 | 26  | 5   | ND  | 1   | 65  | 1.7  | 7   | 2   | 182 | .05  | .078 | 7   | 15  | .06 | 235  | .01 | 10 | .77  | .02 | .16 | 1   | 2509  |
| L56+00N 50+50E     | 51  | 26  | 29  | 163 | .9  | 20  | 1   | 8    | 3.69 | 22  | 5   | ND  | 1   | 128 | 3.2  | 5   | 2   | 127 | .16  | .079 | 5   | 11  | .04 | 118  | .01 | 10 | .48  | .04 | .44 | 1   | 1284  |
| L56+00N 51+00E     | 35  | 11  | 7   | 54  | .3  | 17  | 3   | 24   | 1.51 | 13  | 5   | ND  | 1   | 6   | .7   | 3   | 2   | 124 | .03  | .024 | 6   | 8   | .03 | 76   | .01 | 6  | .42  | .01 | .06 | 1   | 670   |
| L56+00N 51+50E     | 67  | 62  | 19  | 333 | 1.4 | 138 | 3   | 46   | 3.95 | 22  | 5   | ND  | 1   | 183 | 4.6  | 10  | 2   | 114 | 1.28 | .094 | 7   | 14  | .13 | 640  | .01 | 6  | .67  | .02 | .11 | 1   | 1387  |
| L56+00N 52+00E     | 63  | 35  | 35  | 313 | 1.3 | 109 | 6   | 76   | 2.55 | 30  | 5   | ND  | 2   | 156 | 4.4  | 7   | 2   | 175 | .58  | .068 | 5   | 13  | .07 | 513  | .01 | 10 | .57  | .02 | .26 | 1   | 1731  |
| L54+00N 45+00E     | 14  | 12  | 20  | 135 | 1.2 | 16  | 2   | 8    | 1.39 | 7   | 5   | ND  | 1   | 34  | 1.8  | 2   | 2   | 79  | .05  | .026 | 4   | 7   | .04 | 1030 | .01 | 10 | .46  | .01 | .18 | 1   | 7569  |
| L54+00N 45+50E     | 16  | 19  | 17  | 107 | .4  | 17  | 2   | 10   | 1.23 | 9   | 5   | ND  | 1   | 41  | 1.4  | 2   | 2   | 66  | .07  | .033 | 2   | 7   | .03 | 723  | .01 | 11 | .34  | .01 | .17 | 1   | 6184  |
| L54+00N 46+00E     | 20  | 37  | 18  | 138 | .4  | 28  | 2   | 10   | 1.89 | 15  | 5   | ND  | 2   | 57  | .8   | 6   | 2   | 82  | .06  | .029 | 3   | 9   | .04 | 379  | .01 | 9  | .48  | .02 | .20 | 1   | 12505 |
| L54+00N 46+50E     | 17  | 20  | 17  | 116 | .2  | 19  | 2   | 8    | 1.34 | 9   | 5   | ND  | 1   | 37  | .6   | 3   | 2   | 88  | .02  | .031 | 2   | 7   | .02 | 530  | .01 | 9  | .39  | .02 | .16 | 1   | 14678 |
| L54+00N 47+00E     | 14  | 12  | 16  | 105 | .4  | 15  | 2   | 19   | 1.39 | 8   | 5   | ND  | 1   | 30  | .3   | 3   | 2   | 92  | .02  | .026 | 5   | 8   | .03 | 488  | .01 | 6  | .48  | .01 | .13 | 1   | 1551  |
| L54+00N 47+50E     | 14  | 36  | 37  | 203 | .9  | 35  | 4   | 36   | 3.01 | 18  | 5   | ND  | 1   | 60  | .2   | 3   | 2   | 114 | .02  | .066 | 6   | 11  | .04 | 455  | .01 | 9  | .70  | .03 | .17 | 1   | 2637  |
| L54+00N 48+00E     | 81  | 41  | 60  | 118 | .5  | 16  | 2   | 20   | 6.22 | 45  | 5   | ND  | 1   | 130 | .7   | 3   | 2   | 190 | .03  | .107 | 4   | 12  | .03 | 43   | .02 | 8  | .44  | .06 | .63 | 1   | 51293 |
| L54+00N 48+50E     | 23  | 18  | 21  | 94  | .3  | 14  | 2   | 19   | 2.09 | 15  | 5   | ND  | 1   | 49  | 1.0  | 4   | 2   | 113 | .04  | .052 | 6   | 10  | .04 | 487  | .01 | 9  | .56  | .02 | .18 | 1   | 1509  |
| L54+00N 49+00E     | 59  | 30  | 35  | 59  | .8  | 9   | 1   | 18   | 4.28 | 26  | 5   | ND  | 4   | 149 | .2   | 6   | 2   | 177 | .03  | .081 | 5   | 12  | .04 | 97   | .01 | 6  | .70  | .07 | .47 | 1   | 2353  |
| L54+00N 49+50E     | 48  | 16  | 36  | 56  | .8  | 14  | 1   | 11   | 2.57 | 17  | 5   | ND  | 1   | 74  | .2   | 5   | 2   | 193 | .04  | .049 | 4   | 12  | .06 | 199  | .01 | 11 | .87  | .03 | .30 | 1   | 4376  |
| L54+00N 50+00E     | 72  | 28  | 26  | 180 | .7  | 51  | 6   | 39   | 3.46 | 47  | 5   | ND  | 2   | 16  | .2   | 5   | 2   | 99  | .02  | .047 | 3   | 13  | .05 | 202  | .01 | 14 | .77  | .01 | .18 | 1   | 1411  |
| L54+00N 50+50E     | 14  | 28  | 23  | 240 | 1.2 | 19  | 2   | 13   | 2.32 | 15  | 5   | ND  | 1   | 174 | .7   | 5   | 2   | 121 | .02  | .066 | 5   | 11  | .04 | 307  | .01 | 7  | .83  | .02 | .16 | 1   | 1229  |
| L54+00N 51+00E     | 49  | 8   | 19  | 27  | 1.1 | 7   | 1   | 2    | 1.44 | 11  | 5   | ND  | 1   | 55  | .2   | 4   | 2   | 180 | .01  | .018 | 2   | 10  | .03 | 418  | .01 | 8  | .47  | .02 | .19 | 1   | 1428  |
| L54+00N 51+50E     | 270 | 35  | 48  | 203 | 1.4 | 21  | 2   | 20   | 7.98 | 126 | 5   | ND  | 2   | 94  | .4   | 28  | 2   | 439 | .02  | .144 | 7   | 15  | .05 | 399  | .03 | 6  | .70  | .03 | .21 | 1   | 1443  |
| RE L54+00N 49+50E  | 48  | 15  | 38  | 55  | .6  | 13  | 1   | 9    | 2.55 | 17  | 5   | ND  | 1   | 72  | .2   | 3   | 2   | 187 | .04  | .048 | 4   | 13  | .05 | 217  | .01 | 9  | .84  | .03 | .28 | 1   | 4782  |
| L54+00N 52+00E     | 111 | 34  | 59  | 98  | .7  | 18  | 2   | 18   | 3.76 | 32  | 5   | ND  | 2   | 188 | .4   | 7   | 2   | 126 | .02  | .074 | 5   | 11  | .04 | 109  | .01 | 7  | .74  | .05 | .37 | 1   | 2859  |
| L52+00N 47+50E     | 17  | 15  | 21  | 136 | .3  | 18  | 2   | 21   | 1.75 | 10  | 5   | ND  | 1   | 50  | .2   | 3   | 2   | 111 | .01  | .031 | 5   | 9   | .04 | 793  | .01 | 7  | .68  | .01 | .13 | 1   | 8599  |
| L52+00N 47+75E     | 30  | 23  | 43  | 148 | .8  | 14  | 1   | 13   | 2.13 | 16  | 5   | ND  | 1   | 64  | .2   | 2   | 2   | 100 | .05  | .067 | 6   | 13  | .04 | 1070 | .01 | 8  | .75  | .01 | .13 | 1   | 3811  |
| L52+00N 48+00E     | 104 | 51  | 60  | 118 | 1.5 | 56  | 2   | 26   | 3.71 | 58  | 6   | ND  | 1   | 159 | .5   | 10  | 2   | 248 | .12  | .144 | 7   | 15  | .06 | 251  | .01 | 7  | 1.13 | .03 | .29 | 1   | 15557 |
| L52+00N 48+25E     | 46  | 26  | 17  | 119 | .8  | 22  | 2   | 32   | 1.56 | 15  | 5   | ND  | 1   | 63  | .5   | 3   | 2   | 102 | .16  | .048 | 8   | 13  | .04 | 1372 | .01 | 8  | .62  | .01 | .12 | 1   | 3428  |
| L52+00N 48+50E     | 48  | 90  | 51  | 158 | 1.7 | 89  | 3   | 31   | 3.48 | 56  | 13  | ND  | 1   | 189 | 5.2  | 10  | 2   | 197 | .71  | .152 | 7   | 16  | .17 | 388  | .01 | 6  | 1.36 | .03 | .28 | 1   | 4371  |
| L52+00N 48+75E     | 13  | 23  | 20  | 93  | .3  | 26  | 2   | 45   | 1.08 | 3   | 5   | ND  | 1   | 46  | 2.9  | 2   | 2   | 66  | .38  | .049 | 7   | 15  | .05 | 686  | .01 | 9  | .55  | .01 | .09 | 1   | 1535  |
| STANDARD C/CB-1200 | 17  | 59  | 38  | 131 | 7.6 | 73  | 31  | 1049 | 3.96 | 43  | 17  | 7   | 37  | 52  | 18.6 | 15  | 20  | 57  | .49  | .084 | 38  | 60  | .93 | 182  | .08 | 35 | 1.94 | .08 | .17 | 10  | 2277  |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: SOIL BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP.  
 Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 12 1992 DATE REPORT MAILED: Aug 25/92 SIGNED BY: C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



## Teck Exploration (BC) PROJECT 1715 FILE # 92-2519

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| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe    | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*    |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|--------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %     | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm    |
| L52+00N 49+00E     | 13  | 9   | 12  | 77  | .6  | 11  | 2   | 23   | 1.16  | 5   | 5   | ND  | 4   | 16  | .2   | 2   | 3   | 145 | .05 | .040 | 5   | 16  | .08 | 569  | .01 | 11  | 1.16 | .01 | .14 | 2   | 1574   |
| RE L52+00N 50+25E  | 11  | 15  | 18  | 130 | .6  | 16  | 5   | 35   | 1.71  | 10  | 5   | ND  | 2   | 14  | .2   | 5   | 2   | 142 | .02 | .035 | 5   | 16  | .07 | 197  | .01 | 8   | 1.13 | .01 | .13 | 1   | 1015   |
| L52+00N 49+25E     | 22  | 22  | 19  | 189 | .4  | 34  | 6   | 34   | 1.92  | 21  | 5   | ND  | 2   | 28  | .2   | 3   | 2   | 166 | .03 | .035 | 4   | 15  | .08 | 308  | .01 | 8   | 1.22 | .01 | .12 | 1   | 1112   |
| L52+00N 49+50E     | 15  | 17  | 23  | 81  | .8  | 9   | 3   | 30   | 2.02  | 7   | 5   | ND  | 2   | 37  | .2   | 4   | 3   | 133 | .04 | .046 | 4   | 15  | .08 | 340  | .01 | 9   | 1.14 | .02 | .22 | 1   | 1389   |
| L52+00N 49+75E     | 15  | 28  | 12  | 91  | .8  | 19  | 4   | 26   | 1.68  | 7   | 5   | ND  | 1   | 29  | 1.1  | 4   | 2   | 117 | .19 | .044 | 6   | 16  | .11 | 486  | .01 | 6   | 1.17 | .01 | .14 | 1   | 1249   |
| L52+00N 50+00E     | 10  | 6   | 14  | 46  | 1.3 | 5   | 2   | 18   | .88   | 3   | 5   | ND  | 1   | 9   | .2   | 2   | 2   | 58  | .02 | .030 | 5   | 13  | .07 | 196  | .01 | 9   | 1.03 | .01 | .15 | 1   | 1263   |
| L52+00N 50+25E     | 11  | 15  | 20  | 128 | .6  | 19  | 5   | 35   | 1.70  | 8   | 5   | ND  | 1   | 14  | .2   | 4   | 2   | 139 | .02 | .033 | 5   | 15  | .07 | 186  | .01 | 8   | 1.12 | .01 | .13 | 1   | 1049   |
| L52+00N 50+50E     | 9   | 13  | 19  | 119 | .4  | 13  | 4   | 28   | 1.65  | 11  | 5   | ND  | 2   | 20  | .2   | 3   | 2   | 138 | .04 | .037 | 4   | 14  | .08 | 263  | .01 | 3   | 1.25 | .01 | .17 | 1   | 1076   |
| L52+00N 50+75E     | 10  | 33  | 22  | 249 | .8  | 23  | 7   | 103  | 4.88  | 12  | 5   | ND  | 2   | 36  | .9   | 5   | 2   | 166 | .02 | .078 | 3   | 14  | .09 | 325  | .01 | 2   | 1.15 | .01 | .20 | 1   | 1173   |
| L52+00N 51+00E     | 11  | 20  | 26  | 367 | 2.5 | 30  | 7   | 37   | 3.68  | 14  | 5   | ND  | 2   | 72  | .9   | 14  | 2   | 167 | .04 | .105 | 4   | 16  | .08 | 384  | .01 | 8   | 1.42 | .02 | .24 | 1   | 1164   |
| L52+00N 51+25E     | 29  | 9   | 37  | 101 | 1.9 | 14  | 4   | 28   | 1.96  | 9   | 5   | ND  | 1   | 70  | .4   | 5   | 2   | 169 | .02 | .051 | 6   | 16  | .06 | 407  | .01 | 6   | .84  | .01 | .19 | 1   | 1154   |
| L52+00N 51+50E     | 28  | 20  | 31  | 135 | 1.1 | 23  | 6   | 44   | 3.11  | 20  | 5   | ND  | 3   | 85  | .2   | 2   | 2   | 169 | .03 | .068 | 4   | 18  | .09 | 441  | .01 | 7   | 1.06 | .02 | .25 | 1   | 1384   |
| L52+00N 51+75E     | 165 | 36  | 20  | 69  | .1  | 6   | 8   | 6    | 10.40 | 306 | 5   | ND  | 1   | 18  | .2   | 4   | 2   | 535 | .04 | .144 | 2   | 20  | .06 | 157  | .01 | 3   | .83  | .01 | .05 | 1   | 822    |
| L52+00N 52+00E     | 16  | 38  | 48  | 286 | .9  | 49  | 9   | 28   | 3.45  | 25  | 5   | ND  | 4   | 167 | .2   | 3   | 2   | 131 | .02 | .066 | 3   | 14  | .07 | 277  | .01 | 6   | 1.04 | .03 | .24 | 1   | 1909   |
| L52+00N 52+25E     | 9   | 46  | 40  | 270 | 1.8 | 68  | 14  | 137  | 5.57  | 22  | 5   | ND  | 2   | 78  | .2   | 2   | 4   | 104 | .02 | .097 | 4   | 17  | .11 | 239  | .01 | 2   | 1.19 | .01 | .16 | 1   | 1608   |
| L52+00N 52+50E     | 9   | 23  | 16  | 153 | .7  | 26  | 7   | 119  | 3.18  | 14  | 5   | ND  | 1   | 15  | .2   | 2   | 3   | 100 | .02 | .051 | 5   | 15  | .09 | 197  | .01 | 6   | 1.06 | .01 | .13 | 1   | 1345   |
| L51+00N 47+50E     | 22  | 25  | 21  | 113 | .1  | 18  | 3   | 13   | 1.61  | 12  | 5   | ND  | 1   | 208 | .9   | 4   | 2   | 178 | .04 | .062 | 2   | 12  | .04 | 1221 | .01 | 10  | .53  | .01 | .10 | 1   | 4040   |
| L51+00N 47+75E     | 23  | 19  | 24  | 143 | .4  | 25  | 4   | 23   | 1.65  | 14  | 5   | ND  | 1   | 54  | .5   | 3   | 2   | 110 | .06 | .052 | 3   | 10  | .04 | 799  | .01 | 8   | .54  | .01 | .13 | 1   | 4301   |
| L51+00N 48+00E     | 37  | 38  | 34  | 172 | .6  | 36  | 5   | 62   | 2.67  | 24  | 5   | ND  | 1   | 103 | .8   | 3   | 3   | 200 | .22 | .080 | 8   | 17  | .07 | 497  | .01 | 7   | .97  | .01 | .17 | 1   | 14308  |
| L51+00N 48+25E     | 127 | 69  | 23  | 74  | .6  | 132 | 5   | 13   | 4.76  | 74  | 10  | ND  | 2   | 163 | .7   | 7   | 2   | 630 | .30 | .168 | 3   | 16  | .04 | 152  | .01 | 3   | .98  | .02 | .25 | 1   | 112415 |
| L51+00N 48+50E     | 45  | 14  | 43  | 54  | .2  | 12  | 3   | 19   | 1.56  | 16  | 5   | ND  | 1   | 62  | .2   | 2   | 2   | 112 | .10 | .055 | 4   | 15  | .05 | 675  | .01 | 11  | .53  | .01 | .20 | 1   | 3375   |
| L51+00N 48+75E     | 33  | 15  | 24  | 123 | .2  | 14  | 4   | 37   | 2.54  | 16  | 5   | ND  | 1   | 130 | .2   | 3   | 5   | 200 | .18 | .079 | 6   | 17  | .07 | 697  | .01 | 10  | .85  | .01 | .15 | 1   | 1471   |
| L51+00N 49+00E     | 26  | 13  | 21  | 130 | .3  | 17  | 4   | 42   | 1.83  | 12  | 5   | ND  | 1   | 47  | .2   | 2   | 2   | 177 | .03 | .046 | 4   | 16  | .09 | 755  | .01 | 11  | 1.19 | .01 | .15 | 1   | 3130   |
| L51+00N 49+25E     | 60  | 20  | 8   | 457 | .2  | 121 | 20  | 237  | 4.05  | 24  | 5   | ND  | 1   | 25  | .2   | 2   | 2   | 174 | .07 | .043 | 8   | 14  | .06 | 1445 | .01 | 2   | .71  | .01 | .07 | 1   | 141476 |
| L51+00N 49+50E     | 13  | 8   | 10  | 79  | .3  | 10  | 3   | 43   | .92   | 3   | 5   | ND  | 1   | 13  | .7   | 2   | 3   | 88  | .10 | .041 | 8   | 17  | .07 | 319  | .01 | 7   | .88  | .01 | .10 | 1   | 1291   |
| L51+00N 49+75E     | 16  | 14  | 15  | 129 | .7  | 12  | 4   | 27   | 1.67  | 8   | 5   | ND  | 1   | 23  | .2   | 5   | 2   | 105 | .09 | .042 | 4   | 14  | .08 | 489  | .01 | 9   | .97  | .01 | .14 | 1   | 1284   |
| L51+00N 50+00E     | 33  | 23  | 10  | 148 | .8  | 25  | 5   | 31   | 2.15  | 19  | 5   | ND  | 1   | 20  | .5   | 5   | 3   | 124 | .10 | .042 | 5   | 13  | .07 | 1076 | .01 | 5   | .89  | .01 | .11 | 1   | 2189   |
| L51+00N 50+25E     | 14  | 11  | 28  | 127 | .8  | 9   | 3   | 27   | 2.48  | 15  | 5   | ND  | 2   | 25  | .2   | 6   | 2   | 129 | .03 | .055 | 4   | 13  | .07 | 390  | .01 | 10  | 1.01 | .01 | .24 | 1   | 1352   |
| L51+00N 50+50E     | 15  | 12  | 20  | 122 | .5  | 10  | 4   | 22   | 2.35  | 13  | 5   | ND  | 2   | 31  | .2   | 4   | 2   | 153 | .02 | .039 | 4   | 14  | .08 | 303  | .01 | 5   | 1.13 | .01 | .20 | 1   | 1171   |
| L51+00N 50+75E     | 7   | 8   | 10  | 90  | .5  | 10  | 4   | 35   | 1.25  | 6   | 5   | ND  | 2   | 9   | .2   | 3   | 3   | 113 | .02 | .016 | 9   | 15  | .08 | 183  | .01 | 6   | 1.13 | .01 | .11 | 1   | 929    |
| L51+00N 51+00E     | 13  | 15  | 18  | 179 | .7  | 18  | 5   | 24   | 2.17  | 12  | 5   | ND  | 2   | 40  | .3   | 3   | 2   | 123 | .02 | .039 | 4   | 13  | .06 | 238  | .01 | 7   | .90  | .02 | .18 | 1   | 919    |
| L51+00N 51+25E     | 40  | 25  | 24  | 143 | 1.1 | 25  | 6   | 43   | 2.89  | 14  | 5   | ND  | 1   | 70  | 1.0  | 2   | 2   | 138 | .15 | .052 | 7   | 18  | .09 | 322  | .01 | 4   | 1.10 | .04 | .22 | 1   | 1287   |
| L51+00N 51+50E     | 42  | 30  | 33  | 154 | .6  | 42  | 6   | 27   | 2.32  | 13  | 5   | ND  | 2   | 59  | .2   | 2   | 2   | 149 | .04 | .050 | 3   | 17  | .07 | 296  | .01 | 5   | 1.13 | .03 | .18 | 1   | 1179   |
| L51+00N 51+75E     | 18  | 17  | 22  | 122 | .5  | 18  | 3   | 23   | 1.51  | 10  | 5   | ND  | 2   | 40  | .2   | 3   | 4   | 98  | .02 | .036 | 4   | 11  | .05 | 253  | .01 | 8   | .82  | .01 | .16 | 1   | 1010   |
| L51+00N 52+00E     | 10  | 42  | 38  | 255 | 1.1 | 102 | 19  | 116  | 4.38  | 14  | 5   | ND  | 3   | 95  | .2   | 2   | 2   | 112 | .03 | .098 | 5   | 20  | .14 | 305  | .01 | 2   | 1.60 | .01 | .17 | 1   | 1380   |
| L51+00N 52+25E     | 10  | 16  | 27  | 118 | .4  | 19  | 5   | 36   | 1.65  | 9   | 5   | ND  | 1   | 28  | .2   | 2   | 2   | 95  | .02 | .036 | 5   | 13  | .07 | 259  | .01 | 4   | .99  | .01 | .13 | 1   | 1161   |
| L51+00N 52+50E     | 6   | 22  | 15  | 162 | .6  | 30  | 6   | 59   | 1.61  | 7   | 5   | ND  | 1   | 10  | .2   | 2   | 3   | 96  | .02 | .029 | 5   | 14  | .07 | 218  | .01 | 8   | 1.04 | .01 | .12 | 1   | 1360   |
| STANDARD C/CB-1200 | 19  | 63  | 39  | 137 | 7.5 | 70  | 32  | 1056 | 3.96  | 43  | 18  | 7   | 41  | 53  | 18.9 | 14  | 21  | 59  | .49 | .087 | 39  | 61  | .94 | 183  | .08 | 35  | 1.93 | .07 | .14 | 10  | 2249   |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm   |
| L50+00N 45+00E     | 22  | 63  | 25  | 387 | .8  | 77  | 16  | 260  | 3.21 | 29  | 8   | ND  | 7   | 79  | 5.4  | 7   | 4   | 130 | .11 | .103 | 5   | 18  | .12 | 891  | .01 | 8   | 1.28 | .01 | .18 | 2   | 10942 |
| L50+00N 45+25E     | 19  | 31  | 22  | 155 | .4  | 31  | 5   | 39   | 2.13 | 18  | 5   | ND  | 2   | 57  | 1.5  | 3   | 2   | 99  | .07 | .057 | 4   | 13  | .06 | 1119 | .01 | 11  | .80  | .01 | .14 | 1   | 16252 |
| L50+00N 45+50E     | 20  | 21  | 27  | 185 | .6  | 34  | 5   | 31   | 2.19 | 21  | 5   | ND  | 3   | 55  | .8   | 5   | 2   | 115 | .02 | .046 | 5   | 11  | .04 | 685  | .01 | 10  | .51  | .01 | .15 | 1   | 13407 |
| L50+00N 45+75E     | 21  | 18  | 27  | 198 | .3  | 38  | 6   | 30   | 2.05 | 20  | 5   | ND  | 2   | 51  | .5   | 5   | 2   | 126 | .05 | .047 | 5   | 10  | .05 | 742  | .01 | 13  | .55  | .01 | .14 | 1   | 15927 |
| L50+00N 46+00E     | 20  | 20  | 26  | 228 | .2  | 47  | 6   | 31   | 3.04 | 28  | 5   | ND  | 2   | 73  | .2   | 5   | 2   | 119 | .01 | .066 | 4   | 11  | .04 | 465  | .01 | 7   | .49  | .01 | .16 | 1   | 23792 |
| L50+00N 46+25E     | 21  | 18  | 23  | 190 | .2  | 34  | 6   | 24   | 2.21 | 28  | 5   | ND  | 2   | 58  | .2   | 5   | 2   | 111 | .01 | .038 | 3   | 9   | .04 | 443  | .01 | 9   | .53  | .01 | .15 | 1   | 34768 |
| L50+00N 46+50E     | 5   | 3   | 8   | 54  | .1  | 9   | 3   | 17   | .60  | 4   | 5   | ND  | 1   | 19  | .2   | 2   | 2   | 68  | .03 | .018 | 8   | 12  | .06 | 1691 | .01 | 10  | .91  | .01 | .08 | 1   | 6242  |
| L50+00N 46+75E     | 17  | 13  | 21  | 140 | .1  | 23  | 4   | 31   | 1.64 | 14  | 5   | ND  | 1   | 62  | .2   | 2   | 2   | 124 | .02 | .036 | 6   | 13  | .05 | 1018 | .01 | 9   | .82  | .01 | .13 | 1   | 6005  |
| L50+00N 47+00E     | 19  | 14  | 29  | 177 | .5  | 29  | 5   | 30   | 2.07 | 17  | 7   | ND  | 1   | 60  | .2   | 2   | 2   | 134 | .03 | .040 | 5   | 13  | .05 | 944  | .01 | 9   | .87  | .01 | .15 | 1   | 10669 |
| L50+00N 47+25E     | 13  | 8   | 22  | 75  | .1  | 13  | 3   | 28   | 1.16 | 5   | 5   | ND  | 1   | 22  | .2   | 2   | 2   | 92  | .07 | .043 | 8   | 15  | .04 | 1694 | .01 | 13  | .70  | .01 | .12 | 1   | 15057 |
| L50+00N 47+50E     | 16  | 21  | 40  | 232 | 1.4 | 34  | 5   | 29   | 3.50 | 21  | 5   | ND  | 2   | 96  | .3   | 3   | 3   | 106 | .02 | .081 | 4   | 15  | .06 | 577  | .01 | 8   | 1.00 | .03 | .21 | 1   | 2295  |
| L50+00N 47+75E     | 18  | 25  | 63  | 222 | 1.4 | 32  | 6   | 39   | 3.81 | 27  | 5   | ND  | 2   | 138 | .6   | 3   | 2   | 105 | .02 | .094 | 5   | 15  | .05 | 545  | .01 | 6   | .94  | .01 | .23 | 1   | 2708  |
| L50+00N 48+00E     | 19  | 25  | 25  | 265 | .4  | 52  | 8   | 84   | 2.81 | 20  | 5   | ND  | 1   | 78  | .4   | 2   | 2   | 126 | .05 | .051 | 10  | 19  | .07 | 881  | .02 | 6   | .99  | .01 | .13 | 1   | 30596 |
| L50+00N 48+25E     | 17  | 17  | 38  | 90  | .4  | 22  | 4   | 59   | 1.54 | 10  | 5   | ND  | 1   | 52  | .4   | 2   | 2   | 123 | .11 | .071 | 10  | 23  | .05 | 2265 | .02 | 9   | .68  | .01 | .11 | 1   | 40992 |
| L50+00N 48+50E     | 44  | 21  | 23  | 337 | .5  | 36  | 7   | 104  | 2.81 | 23  | 5   | ND  | 1   | 30  | .2   | 3   | 2   | 170 | .03 | .045 | 9   | 15  | .05 | 545  | .02 | 8   | .77  | .01 | .12 | 1   | 1702  |
| RE L50+00N 49+75E  | 33  | 14  | 31  | 104 | .7  | 21  | 6   | 54   | 2.43 | 14  | 5   | ND  | 1   | 41  | .2   | 3   | 2   | 122 | .02 | .033 | 8   | 17  | .06 | 321  | .01 | 8   | .97  | .02 | .20 | 1   | 1487  |
| L50+00N 48+75E     | 28  | 22  | 10  | 113 | .1  | 16  | 3   | 38   | 1.27 | 8   | 5   | ND  | 1   | 17  | .2   | 2   | 2   | 127 | .03 | .030 | 6   | 14  | .07 | 460  | .01 | 10  | .89  | .01 | .09 | 1   | 1283  |
| L50+00N 49+00E     | 43  | 8   | 26  | 91  | .9  | 14  | 5   | 37   | 3.03 | 16  | 8   | ND  | 1   | 95  | .2   | 5   | 2   | 154 | .04 | .063 | 6   | 13  | .05 | 183  | .01 | 4   | .56  | .03 | .25 | 1   | 2297  |
| L50+00N 49+25E     | 16  | 9   | 17  | 75  | .6  | 10  | 3   | 40   | 1.27 | 9   | 5   | ND  | 1   | 20  | .3   | 2   | 2   | 115 | .04 | .022 | 6   | 13  | .05 | 411  | .01 | 9   | .56  | .01 | .15 | 1   | 1538  |
| L50+00N 49+50E     | 79  | 49  | 53  | 196 | 1.8 | 33  | 8   | 95   | 4.79 | 65  | 5   | ND  | 1   | 194 | .4   | 4   | 2   | 251 | .12 | .131 | 5   | 27  | .08 | 303  | .01 | 7   | 1.15 | .03 | .23 | 1   | 1595  |
| L50+00N 49+75E     | 33  | 13  | 38  | 98  | .6  | 20  | 5   | 53   | 2.44 | 15  | 5   | ND  | 1   | 44  | .2   | 3   | 5   | 120 | .02 | .035 | 7   | 16  | .06 | 309  | .01 | 6   | .93  | .02 | .19 | 1   | 1503  |
| L50+00N 50+00E     | 70  | 40  | 11  | 164 | 1.0 | 36  | 11  | 51   | 8.07 | 107 | 5   | ND  | 1   | 5   | .2   | 3   | 2   | 199 | .03 | .111 | 7   | 17  | .05 | 97   | .02 | 4   | .75  | .01 | .07 | 1   | 630   |
| L49+00N 45+00E     | 13  | 21  | 18  | 123 | .5  | 22  | 4   | 32   | 1.75 | 15  | 5   | ND  | 2   | 31  | .3   | 3   | 2   | 112 | .01 | .042 | 9   | 19  | .06 | 757  | .01 | 8   | .92  | .01 | .12 | 1   | 2343  |
| L49+00N 45+25E     | 20  | 25  | 26  | 201 | .3  | 36  | 6   | 50   | 2.67 | 22  | 5   | ND  | 1   | 60  | .3   | 6   | 2   | 113 | .02 | .065 | 5   | 14  | .09 | 566  | .01 | 10  | .77  | .01 | .16 | 1   | 12783 |
| L49+00N 45+50E     | 21  | 34  | 24  | 183 | .3  | 31  | 6   | 46   | 2.91 | 25  | 5   | ND  | 1   | 54  | 1.1  | 6   | 5   | 86  | .02 | .058 | 4   | 11  | .08 | 599  | .01 | 7   | .57  | .01 | .15 | 1   | 12481 |
| L49+00N 45+75E     | 20  | 27  | 24  | 158 | .4  | 31  | 5   | 31   | 3.04 | 24  | 5   | ND  | 2   | 59  | .3   | 5   | 2   | 104 | .02 | .079 | 3   | 14  | .06 | 610  | .01 | 10  | .88  | .01 | .17 | 1   | 13409 |
| L49+00N 46+00E     | 21  | 21  | 24  | 152 | .1  | 25  | 4   | 26   | 2.49 | 23  | 5   | ND  | 1   | 46  | .2   | 4   | 2   | 131 | .01 | .052 | 3   | 12  | .05 | 873  | .01 | 10  | .76  | .01 | .13 | 1   | 8462  |
| L49+00N 46+25E     | 21  | 26  | 19  | 130 | .4  | 22  | 4   | 26   | 2.08 | 20  | 5   | ND  | 1   | 45  | .2   | 4   | 4   | 111 | .03 | .070 | 4   | 12  | .05 | 1020 | .01 | 8   | .70  | .01 | .13 | 1   | 11622 |
| L49+00N 46+50E     | 22  | 31  | 18  | 131 | .8  | 27  | 4   | 24   | 2.36 | 26  | 6   | ND  | 2   | 48  | 1.0  | 5   | 3   | 112 | .03 | .077 | 4   | 13  | .05 | 1004 | .01 | 8   | .81  | .01 | .14 | 1   | 13653 |
| L49+00N 46+75E     | 21  | 29  | 27  | 144 | 1.2 | 30  | 5   | 27   | 2.49 | 25  | 5   | ND  | 2   | 56  | 1.0  | 4   | 2   | 128 | .01 | .053 | 4   | 12  | .05 | 644  | .01 | 8   | .82  | .01 | .18 | 1   | 14644 |
| L49+00N 47+00E     | 20  | 24  | 24  | 185 | 1.6 | 31  | 6   | 55   | 2.65 | 22  | 5   | ND  | 2   | 55  | .2   | 3   | 2   | 122 | .03 | .064 | 7   | 17  | .10 | 840  | .01 | 4   | 1.13 | .01 | .15 | 1   | 11000 |
| L49+00N 47+25E     | 34  | 22  | 74  | 103 | .7  | 17  | 5   | 40   | 2.68 | 29  | 6   | ND  | 1   | 134 | .2   | 4   | 2   | 142 | .03 | .070 | 8   | 15  | .05 | 484  | .01 | 9   | .77  | .01 | .18 | 1   | 38733 |
| L49+00N 47+50E     | 25  | 21  | 28  | 160 | .4  | 32  | 4   | 38   | 2.22 | 20  | 5   | ND  | 1   | 44  | .2   | 4   | 2   | 171 | .01 | .043 | 3   | 12  | .05 | 763  | .01 | 8   | .76  | .01 | .14 | 1   | 2573  |
| L49+00N 47+75E     | 25  | 32  | 33  | 198 | .7  | 40  | 5   | 30   | 3.40 | 35  | 5   | ND  | 3   | 71  | .2   | 7   | 2   | 158 | .02 | .084 | 3   | 14  | .06 | 643  | .01 | 9   | 1.08 | .02 | .18 | 1   | 3709  |
| L49+00N 48+00E     | 23  | 33  | 28  | 193 | .9  | 35  | 6   | 48   | 2.51 | 16  | 5   | ND  | 1   | 63  | .4   | 2   | 2   | 107 | .03 | .072 | 7   | 15  | .07 | 762  | .01 | 8   | 1.08 | .01 | .16 | 1   | 8256  |
| L49+00N 48+25E     | 19  | 26  | 35  | 237 | .6  | 45  | 7   | 48   | 3.21 | 23  | 5   | ND  | 1   | 79  | .2   | 3   | 3   | 123 | .03 | .072 | 6   | 16  | .05 | 782  | .01 | 7   | .94  | .02 | .17 | 1   | 6632  |
| L49+00N 48+50E     | 24  | 22  | 31  | 131 | .8  | 30  | 6   | 82   | 2.00 | 14  | 5   | ND  | 2   | 41  | .8   | 2   | 2   | 145 | .07 | .072 | 9   | 21  | .08 | 987  | .01 | 9   | .92  | .01 | .14 | 1   | 20175 |
| STANDARD C/CB-1200 | 19  | 62  | 38  | 135 | 7.3 | 70  | 32  | 1050 | 3.96 | 41  | 20  | 7   | 39  | 52  | 18.7 | 14  | 21  | 59  | .52 | .087 | 38  | 59  | .93 | 186  | .08 | 34  | 2.00 | .07 | .14 | 10  | 2228  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*  |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm  |
| L49+00N 48+75E     | 39  | 31  | 33  | 130  | .5  | 24  | 3   | 25   | 2.01 | 13  | 5   | ND  | 4   | 113 | 1.0  | 3   | 2   | 166 | .02  | .058 | 5   | 12  | .05 | 601  | .01 | 9   | .84  | .02 | .21 | 1   | 2390 |
| L49+00N 49+00E     | 50  | 72  | 51  | 123  | .7  | 58  | 2   | 39   | 2.12 | 18  | 5   | ND  | 1   | 141 | 2.1  | 5   | 2   | 283 | .50  | .086 | 6   | 20  | .09 | 942  | .01 | 8   | .83  | .02 | .20 | 1   | 3007 |
| L49+00N 49+25E     | 26  | 41  | 29  | 185  | .9  | 38  | 4   | 56   | 2.86 | 17  | 5   | ND  | 2   | 54  | 1.7  | 6   | 2   | 138 | .14  | .055 | 7   | 15  | .12 | 807  | .01 | 7   | 1.18 | .02 | .19 | 1   | 2035 |
| L49+00N 49+50E     | 9   | 27  | 33  | 148  | 2.2 | 20  | 2   | 27   | 2.03 | 7   | 5   | ND  | 1   | 48  | .5   | 3   | 2   | 133 | .05  | .082 | 8   | 17  | .05 | 326  | .01 | 8   | .91  | .01 | .18 | 1   | 1155 |
| L49+00N 49+75E     | 22  | 21  | 24  | 92   | .5  | 12  | 1   | 23   | 3.73 | 17  | 5   | ND  | 2   | 25  | .2   | 5   | 2   | 172 | .04  | .061 | 3   | 14  | .07 | 286  | .01 | 13  | 1.09 | .04 | .36 | 1   | 1394 |
| L49+00N 50+00E     | 26  | 32  | 61  | 206  | 1.2 | 50  | 5   | 66   | 4.67 | 17  | 5   | ND  | 1   | 203 | .5   | 4   | 2   | 170 | .07  | .087 | 7   | 16  | .05 | 155  | .01 | 10  | .67  | .03 | .34 | 1   | 1492 |
| L47+00N 39+00E     | 47  | 36  | 61  | 538  | .2  | 76  | 5   | 39   | 2.32 | 20  | 5   | ND  | 1   | 39  | .9   | 14  | 2   | 223 | .02  | .049 | 6   | 16  | .04 | 770  | .01 | 11  | .54  | .01 | .10 | 1   | 2351 |
| L47+00N 39+25E     | 21  | 26  | 42  | 337  | 1.4 | 46  | 4   | 69   | 2.54 | 23  | 5   | ND  | 2   | 19  | 1.5  | 9   | 2   | 210 | .08  | .098 | 6   | 23  | .12 | 1172 | .01 | 14  | 1.12 | .01 | .13 | 1   | 3100 |
| L47+00N 39+50E     | 27  | 23  | 47  | 264  | .7  | 48  | 3   | 36   | 1.87 | 14  | 5   | ND  | 2   | 35  | .3   | 6   | 2   | 189 | .02  | .028 | 8   | 16  | .05 | 548  | .01 | 9   | .75  | .01 | .09 | 1   | 1566 |
| L47+00N 39+75E     | 33  | 33  | 49  | 445  | .5  | 63  | 4   | 66   | 2.16 | 18  | 5   | ND  | 2   | 29  | 1.9  | 7   | 2   | 186 | .06  | .063 | 6   | 15  | .07 | 1361 | .01 | 10  | .74  | .01 | .12 | 1   | 7575 |
| L47+00N 40+00E     | 61  | 41  | 69  | 469  | .6  | 100 | 5   | 40   | 2.29 | 23  | 5   | ND  | 1   | 32  | 1.8  | 12  | 2   | 243 | .04  | .058 | 5   | 17  | .03 | 1025 | .01 | 12  | .55  | .01 | .13 | 1   | 3913 |
| L47+00N 40+25E     | 21  | 19  | 28  | 197  | 1.0 | 32  | 3   | 35   | 1.40 | 10  | 5   | ND  | 1   | 23  | 2.2  | 7   | 2   | 174 | .06  | .041 | 8   | 18  | .05 | 1095 | .01 | 12  | .80  | .01 | .11 | 1   | 2325 |
| L47+00N 40+50E     | 41  | 28  | 111 | 349  | 1.0 | 57  | 2   | 19   | 1.74 | 15  | 5   | ND  | 1   | 22  | .9   | 26  | 2   | 385 | .03  | .040 | 6   | 21  | .04 | 531  | .01 | 12  | .63  | .01 | .10 | 1   | 1236 |
| L47+00N 40+75E     | 43  | 28  | 87  | 345  | .5  | 59  | 3   | 29   | 2.24 | 26  | 5   | ND  | 1   | 51  | 1.0  | 12  | 2   | 248 | .02  | .052 | 7   | 19  | .05 | 982  | .01 | 8   | .85  | .01 | .11 | 1   | 4125 |
| L47+00N 41+00E     | 26  | 23  | 29  | 249  | .5  | 43  | 4   | 39   | 1.93 | 16  | 5   | ND  | 2   | 35  | .6   | 7   | 2   | 167 | .03  | .037 | 6   | 14  | .06 | 1075 | .01 | 9   | .79  | .01 | .13 | 1   | 8953 |
| L47+00N 41+25E     | 27  | 43  | 50  | 285  | .3  | 49  | 5   | 64   | 2.46 | 15  | 5   | ND  | 1   | 53  | 1.1  | 5   | 2   | 126 | .04  | .060 | 6   | 14  | .05 | 898  | .01 | 10  | .79  | .01 | .14 | 1   | 3015 |
| L47+00N 41+50E     | 30  | 37  | 53  | 260  | .1  | 45  | 4   | 35   | 2.02 | 13  | 5   | ND  | 1   | 27  | 1.5  | 6   | 2   | 137 | .01  | .048 | 9   | 15  | .04 | 716  | .01 | 8   | .78  | .01 | .11 | 1   | 2036 |
| RE L47+00N 42+75E  | 33  | 33  | 452 | 1092 | 2.5 | 105 | 4   | 38   | 4.50 | 35  | 5   | ND  | 6   | 34  | 1.7  | 14  | 2   | 425 | .23  | .495 | 7   | 52  | .11 | 916  | .01 | 11  | 2.04 | .01 | .14 | 1   | 2194 |
| L47+00N 41+75E     | 39  | 49  | 64  | 307  | .4  | 50  | 4   | 39   | 3.61 | 20  | 5   | ND  | 1   | 45  | 1.0  | 7   | 2   | 184 | .03  | .062 | 6   | 13  | .04 | 796  | .01 | 10  | .68  | .01 | .14 | 1   | 4332 |
| L47+00N 42+00E     | 25  | 24  | 39  | 244  | .1  | 40  | 3   | 23   | 1.95 | 15  | 5   | ND  | 1   | 36  | .5   | 6   | 2   | 167 | .02  | .038 | 6   | 11  | .03 | 925  | .01 | 8   | .55  | .01 | .11 | 1   | 4164 |
| L47+00N 42+25E     | 32  | 24  | 68  | 306  | .1  | 53  | 3   | 23   | 1.99 | 17  | 5   | ND  | 1   | 36  | .5   | 8   | 2   | 215 | .01  | .038 | 5   | 13  | .04 | 862  | .01 | 8   | .58  | .01 | .12 | 1   | 5143 |
| L47+00N 42+50E     | 25  | 22  | 59  | 296  | .7  | 49  | 4   | 50   | 1.98 | 13  | 5   | ND  | 1   | 26  | .8   | 7   | 2   | 158 | .05  | .061 | 8   | 16  | .05 | 1051 | .01 | 10  | .73  | .01 | .10 | 1   | 2866 |
| L47+00N 42+75E     | 35  | 35  | 479 | 1152 | 2.6 | 109 | 4   | 41   | 4.71 | 39  | 5   | ND  | 7   | 35  | 1.6  | 17  | 3   | 439 | .24  | .517 | 8   | 54  | .12 | 945  | .01 | 11  | 2.09 | .01 | .14 | 1   | 2155 |
| L47+00N 43+00E     | 16  | 26  | 56  | 391  | 1.8 | 64  | 3   | 49   | 1.81 | 10  | 5   | ND  | 1   | 17  | 4.3  | 8   | 2   | 132 | .12  | .059 | 9   | 25  | .05 | 386  | .01 | 8   | .71  | .01 | .08 | 1   | 1105 |
| L47+00N 43+25E     | 31  | 31  | 137 | 1568 | .1  | 87  | 6   | 358  | 3.07 | 24  | 5   | ND  | 1   | 24  | 6.3  | 11  | 2   | 349 | .38  | .071 | 9   | 33  | .19 | 1857 | .01 | 8   | 1.46 | .01 | .11 | 1   | 3003 |
| L47+00N 43+50E     | 35  | 78  | 455 | 6888 | 1.6 | 487 | 7   | 649  | 2.78 | 19  | 5   | ND  | 1   | 66  | 36.9 | 8   | 2   | 212 | 1.55 | .110 | 8   | 35  | .36 | 789  | .01 | 9   | 1.49 | .02 | .10 | 1   | 2208 |
| L47+00N 43+75E     | 58  | 25  | 101 | 550  | .1  | 70  | 3   | 59   | 1.86 | 13  | 5   | ND  | 1   | 35  | 2.4  | 7   | 2   | 227 | .10  | .038 | 6   | 18  | .07 | 776  | .01 | 7   | .91  | .01 | .10 | 1   | 2321 |
| L47+00N 44+00E     | 61  | 27  | 44  | 355  | .9  | 82  | 3   | 47   | 1.90 | 16  | 5   | ND  | 1   | 24  | .6   | 13  | 2   | 408 | .03  | .037 | 9   | 24  | .06 | 1040 | .01 | 6   | .97  | .01 | .09 | 1   | 5039 |
| L47+00N 44+25E     | 137 | 68  | 73  | 829  | .4  | 125 | 5   | 117  | 2.56 | 32  | 5   | ND  | 4   | 12  | 3.2  | 39  | 3   | 879 | .12  | .053 | 9   | 46  | .11 | 285  | .02 | 12  | .96  | .02 | .10 | 1   | 1697 |
| L47+00N 44+50E     | 107 | 46  | 39  | 626  | .1  | 221 | 6   | 61   | 2.43 | 33  | 5   | ND  | 1   | 8   | .6   | 10  | 2   | 701 | .03  | .047 | 7   | 42  | .06 | 363  | .01 | 10  | .90  | .01 | .09 | 1   | 1526 |
| L47+00N 44+75E     | 25  | 29  | 30  | 491  | .1  | 59  | 4   | 50   | 3.16 | 29  | 5   | ND  | 2   | 74  | .6   | 5   | 2   | 368 | .03  | .077 | 6   | 22  | .12 | 649  | .01 | 8   | 1.30 | .02 | .19 | 1   | 4753 |
| L47+00N 45+00E     | 13  | 18  | 35  | 162  | .4  | 31  | 4   | 25   | 1.64 | 10  | 5   | ND  | 2   | 58  | .2   | 5   | 2   | 105 | .02  | .038 | 7   | 15  | .06 | 361  | .01 | 7   | .94  | .03 | .16 | 1   | 2052 |
| L47+00N 45+25E     | 35  | 49  | 56  | 487  | .5  | 107 | 7   | 43   | 3.78 | 30  | 5   | ND  | 3   | 79  | .7   | 11  | 2   | 232 | .01  | .076 | 7   | 17  | .05 | 533  | .01 | 9   | .83  | .03 | .18 | 1   | 2066 |
| L47+00N 45+50E     | 15  | 20  | 21  | 174  | .1  | 25  | 3   | 23   | 1.87 | 14  | 5   | ND  | 1   | 44  | .3   | 4   | 2   | 121 | .01  | .036 | 6   | 9   | .04 | 434  | .01 | 7   | .70  | .02 | .14 | 1   | 1349 |
| L47+00N 45+75E     | 9   | 27  | 38  | 250  | .4  | 60  | 7   | 37   | 2.74 | 12  | 5   | ND  | 1   | 72  | .6   | 4   | 2   | 94  | .04  | .057 | 8   | 15  | .05 | 467  | .01 | 8   | .84  | .02 | .16 | 1   | 1681 |
| L47+00N 46+00E     | 17  | 48  | 24  | 128  | 1.2 | 27  | 3   | 31   | 2.08 | 14  | 5   | ND  | 2   | 50  | 1.4  | 4   | 2   | 135 | .03  | .070 | 7   | 19  | .10 | 1006 | .01 | 7   | 1.62 | .02 | .13 | 1   | 2111 |
| L47+00N 46+25E     | 14  | 19  | 19  | 118  | .2  | 14  | 2   | 18   | 1.50 | 12  | 5   | ND  | 1   | 37  | .3   | 3   | 2   | 114 | .03  | .039 | 6   | 11  | .04 | 876  | .01 | 8   | .68  | .01 | .12 | 1   | 3229 |
| STANDARD C/CB-1200 | 18  | 62  | 39  | 133  | 7.6 | 75  | 31  | 1057 | 3.96 | 42  | 18  | 7   | 40  | 53  | 18.8 | 14  | 19  | 58  | .49  | .084 | 40  | 60  | .93 | 184  | .08 | 34  | 1.95 | .08 | .17 | 11  | 2209 |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.





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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V    | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|------|-----|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm  | %   | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm   |
| L47+00N 46+50E     | 18  | 23  | 29  | 187  | .3  | 26  | 5   | 29   | 2.49 | 17  | 5   | ND  | 6   | 92  | .2   | 3   | 2   | 132  | .04 | .053 | 4   | 12  | .05 | 625  | .01 | 4  | .73  | .01 | .12 | 1   | 12493 |
| L47+00N 46+75E     | 37  | 24  | 26  | 187  | .3  | 24  | 5   | 31   | 2.36 | 25  | 5   | ND  | 2   | 69  | .5   | 4   | 2   | 221  | .03 | .045 | 3   | 11  | .05 | 629  | .01 | 8  | .71  | .01 | .14 | 1   | 3245  |
| L47+00N 47+00E     | 52  | 295 | 26  | 142  | .7  | 147 | 13  | 474  | 4.69 | 86  | 8   | ND  | 1   | 181 | 3.8  | 4   | 2   | 951  | .48 | .203 | 2   | 19  | .09 | 839  | .01 | 2  | 1.03 | .01 | .14 | 1   | 5043  |
| L47+00N 47+25E     | 187 | 73  | 43  | 149  | .9  | 30  | 10  | 310  | 4.30 | 84  | 6   | ND  | 1   | 134 | 1.2  | 10  | 3   | 437  | .20 | .157 | 3   | 19  | .07 | 676  | .01 | 8  | .96  | .01 | .17 | 1   | 16586 |
| L47+00N 47+50E     | 46  | 56  | 29  | 164  | .6  | 28  | 5   | 49   | 2.60 | 41  | 5   | ND  | 1   | 66  | .9   | 5   | 2   | 177  | .05 | .087 | 4   | 15  | .10 | 737  | .01 | 7  | .97  | .01 | .17 | 1   | 2085  |
| L47+00N 47+75E     | 34  | 28  | 19  | 149  | .2  | 20  | 3   | 32   | 1.68 | 16  | 5   | ND  | 1   | 42  | .5   | 2   | 2   | 101  | .04 | .052 | 3   | 9   | .04 | 542  | .01 | 7  | .53  | .01 | .13 | 1   | 1686  |
| L47+00N 48+00E     | 42  | 47  | 27  | 175  | .4  | 26  | 6   | 194  | 2.22 | 32  | 5   | ND  | 1   | 74  | 2.0  | 4   | 3   | 163  | .37 | .080 | 6   | 17  | .13 | 991  | .01 | 5  | .87  | .01 | .15 | 1   | 2414  |
| RE L47+00N 49+25E  | 19  | 26  | 21  | 145  | .9  | 20  | 5   | 36   | 2.93 | 19  | 5   | ND  | 1   | 44  | .4   | 5   | 2   | 114  | .04 | .062 | 3   | 12  | .05 | 458  | .01 | 6  | .82  | .02 | .18 | 1   | 1603  |
| L47+00N 48+25E     | 22  | 26  | 21  | 178  | .4  | 22  | 4   | 27   | 1.78 | 12  | 5   | ND  | 1   | 55  | 1.8  | 3   | 2   | 82   | .22 | .056 | 4   | 9   | .06 | 596  | .01 | 6  | .51  | .01 | .13 | 1   | 1520  |
| L47+00N 48+50E     | 38  | 102 | 20  | 245  | .7  | 43  | 7   | 79   | 3.02 | 18  | 7   | ND  | 1   | 51  | 3.9  | 7   | 2   | 90   | .25 | .108 | 4   | 12  | .09 | 655  | .01 | 3  | .91  | .01 | .14 | 1   | 1678  |
| L47+00N 48+75E     | 21  | 69  | 34  | 525  | 2.3 | 46  | 12  | 72   | 8.28 | 21  | 5   | ND  | 2   | 41  | 1.0  | 8   | 2   | 162  | .03 | .196 | 2   | 15  | .05 | 381  | .01 | 6  | .93  | .01 | .15 | 1   | 1348  |
| L47+00N 49+00E     | 17  | 27  | 26  | 202  | .9  | 12  | 5   | 31   | 3.71 | 16  | 5   | ND  | 2   | 29  | .4   | 6   | 2   | 213  | .03 | .063 | 4   | 16  | .07 | 360  | .01 | 4  | 1.32 | .02 | .19 | 1   | 1296  |
| L47+00N 49+25E     | 19  | 27  | 20  | 150  | 1.0 | 21  | 5   | 35   | 3.02 | 19  | 5   | ND  | 1   | 45  | .5   | 6   | 2   | 117  | .04 | .062 | 3   | 14  | .05 | 488  | .01 | 6  | .85  | .02 | .18 | 1   | 1584  |
| L47+00N 49+50E     | 27  | 24  | 33  | 173  | .9  | 19  | 5   | 23   | 3.51 | 26  | 5   | ND  | 1   | 66  | .8   | 7   | 2   | 204  | .05 | .096 | 3   | 13  | .05 | 321  | .01 | 8  | .72  | .04 | .25 | 1   | 1647  |
| L47+00N 49+75E     | 26  | 25  | 29  | 137  | .5  | 23  | 4   | 30   | 2.12 | 19  | 5   | ND  | 1   | 62  | 2.0  | 8   | 2   | 89   | .23 | .064 | 4   | 14  | .07 | 438  | .01 | 9  | .52  | .03 | .19 | 1   | 1657  |
| L47+00N 50+00E     | 31  | 22  | 40  | 105  | .9  | 26  | 7   | 65   | 2.32 | 22  | 5   | ND  | 3   | 53  | .6   | 7   | 2   | 116  | .03 | .066 | 5   | 16  | .08 | 432  | .01 | 8  | 1.05 | .02 | .23 | 1   | 1872  |
| L46+00N 39+00E     | 18  | 18  | 22  | 191  | .3  | 27  | 5   | 45   | 1.74 | 9   | 5   | ND  | 1   | 19  | .3   | 2   | 2   | 141  | .02 | .037 | 7   | 14  | .04 | 654  | .01 | 6  | .74  | .01 | .08 | 1   | 1882  |
| L46+00N 39+25E     | 17  | 19  | 17  | 205  | 1.9 | 31  | 4   | 28   | 1.45 | 7   | 5   | ND  | 2   | 11  | .3   | 3   | 2   | 149  | .02 | .025 | 7   | 15  | .05 | 473  | .01 | 7  | .82  | .01 | .07 | 1   | 1370  |
| L46+00N 39+50E     | 21  | 20  | 25  | 223  | 6.6 | 32  | 5   | 31   | 1.96 | 11  | 5   | ND  | 1   | 43  | .4   | 3   | 2   | 148  | .02 | .037 | 5   | 12  | .04 | 706  | .01 | 5  | .67  | .01 | .09 | 1   | 2328  |
| L46+00N 39+75E     | 26  | 29  | 38  | 340  | 2.6 | 60  | 5   | 31   | 1.85 | 17  | 5   | ND  | 2   | 36  | .5   | 8   | 2   | 183  | .02 | .033 | 4   | 17  | .04 | 1091 | .01 | 7  | .63  | .01 | .09 | 1   | 4573  |
| L46+00N 40+00E     | 23  | 63  | 191 | 676  | 1.7 | 105 | 8   | 165  | 1.93 | 19  | 5   | ND  | 3   | 38  | 7.3  | 8   | 2   | 133  | .39 | .141 | 7   | 25  | .09 | 2052 | .01 | 13 | .51  | .01 | .12 | 1   | 8653  |
| L46+00N 40+25E     | 217 | 81  | 132 | 1032 | .7  | 221 | 9   | 59   | 3.33 | 43  | 7   | ND  | 1   | 19  | 5.8  | 25  | 2   | 529  | .18 | .085 | 6   | 33  | .06 | 753  | .01 | 8  | .82  | .01 | .09 | 1   | 1984  |
| L46+00N 40+50E     | 53  | 29  | 38  | 367  | .4  | 76  | 6   | 31   | 1.95 | 21  | 5   | ND  | 1   | 32  | .7   | 8   | 2   | 224  | .04 | .040 | 4   | 15  | .04 | 950  | .01 | 6  | .65  | .01 | .10 | 1   | 3438  |
| L46+00N 40+75E     | 45  | 39  | 76  | 425  | .5  | 73  | 7   | 46   | 2.79 | 34  | 5   | ND  | 1   | 58  | 1.3  | 14  | 2   | 281  | .04 | .067 | 4   | 17  | .05 | 830  | .01 | 7  | .72  | .01 | .13 | 1   | 7171  |
| L46+00N 41+00E     | 161 | 167 | 156 | 1046 | 3.8 | 184 | 10  | 52   | 4.06 | 51  | 5   | ND  | 2   | 33  | 3.0  | 67  | 2   | 1052 | .04 | .083 | 5   | 50  | .05 | 643  | .01 | 8  | .94  | .01 | .12 | 1   | 2017  |
| L46+00N 41+25E     | 24  | 42  | 45  | 319  | 1.3 | 58  | 11  | 189  | 2.89 | 13  | 5   | ND  | 1   | 61  | 3.8  | 4   | 2   | 120  | .26 | .050 | 5   | 17  | .14 | 1136 | .01 | 7  | .81  | .01 | .15 | 1   | 2636  |
| L46+00N 41+50E     | 22  | 25  | 40  | 200  | .9  | 34  | 7   | 108  | 2.60 | 7   | 5   | ND  | 1   | 39  | .8   | 2   | 2   | 81   | .30 | .034 | 3   | 11  | .10 | 1269 | .01 | 11 | .69  | .01 | .11 | 1   | 3269  |
| L46+00N 41+75E     | 23  | 25  | 30  | 239  | .8  | 39  | 5   | 33   | 1.68 | 10  | 5   | ND  | 1   | 25  | .4   | 4   | 2   | 166  | .06 | .049 | 4   | 16  | .06 | 777  | .01 | 10 | .90  | .01 | .09 | 1   | 2154  |
| L46+00N 42+00E     | 22  | 23  | 40  | 226  | .3  | 39  | 5   | 36   | 1.92 | 11  | 5   | ND  | 1   | 43  | .6   | 4   | 3   | 155  | .04 | .041 | 6   | 14  | .05 | 953  | .01 | 5  | .72  | .01 | .11 | 1   | 4981  |
| L46+00N 42+25E     | 27  | 21  | 34  | 234  | .3  | 39  | 5   | 30   | 1.74 | 14  | 5   | ND  | 1   | 24  | .5   | 5   | 2   | 179  | .04 | .030 | 5   | 12  | .04 | 698  | .01 | 8  | .54  | .01 | .08 | 1   | 1976  |
| L46+00N 42+50E     | 24  | 31  | 34  | 191  | .2  | 37  | 6   | 48   | 1.87 | 10  | 5   | ND  | 1   | 17  | .5   | 2   | 2   | 165  | .05 | .035 | 6   | 14  | .04 | 568  | .01 | 7  | .74  | .01 | .08 | 1   | 1680  |
| L46+00N 42+75E     | 30  | 16  | 35  | 214  | .1  | 43  | 4   | 27   | 1.46 | 14  | 5   | ND  | 1   | 24  | .3   | 5   | 2   | 186  | .02 | .022 | 6   | 11  | .04 | 1017 | .01 | 6  | .48  | .01 | .09 | 1   | 3992  |
| L46+00N 43+00E     | 37  | 24  | 57  | 326  | .4  | 52  | 5   | 23   | 2.01 | 19  | 5   | ND  | 1   | 39  | .3   | 8   | 2   | 215  | .02 | .040 | 4   | 12  | .03 | 888  | .01 | 5  | .45  | .01 | .11 | 1   | 6599  |
| L46+00N 43+25E     | 41  | 34  | 67  | 351  | .4  | 68  | 5   | 27   | 1.91 | 12  | 5   | ND  | 1   | 26  | .4   | 8   | 2   | 235  | .05 | .056 | 4   | 21  | .04 | 358  | .01 | 5  | .71  | .01 | .09 | 1   | 1274  |
| L46+00N 43+50E     | 33  | 30  | 36  | 199  | .7  | 37  | 5   | 41   | 1.47 | 8   | 5   | ND  | 1   | 24  | 1.4  | 5   | 2   | 159  | .11 | .047 | 9   | 21  | .04 | 1595 | .01 | 7  | .71  | .01 | .06 | 1   | 6100  |
| L46+00N 43+75E     | 44  | 40  | 144 | 360  | .5  | 53  | 6   | 78   | 1.79 | 9   | 5   | ND  | 1   | 27  | 4.6  | 4   | 2   | 232  | .54 | .038 | 11  | 20  | .05 | 1161 | .01 | 2  | .73  | .01 | .07 | 1   | 1956  |
| L46+00N 44+00E     | 80  | 43  | 229 | 625  | .9  | 83  | 4   | 44   | 1.72 | 22  | 6   | ND  | 1   | 16  | 3.4  | 7   | 2   | 379  | .24 | .051 | 4   | 22  | .06 | 529  | .01 | 5  | .86  | .01 | .09 | 1   | 1340  |
| STANDARD C/CB-1200 | 20  | 60  | 39  | 136  | 7.5 | 70  | 32  | 1047 | 3.96 | 41  | 18  | 7   | 41  | 52  | 18.0 | 14  | 21  | 61   | .49 | .087 | 38  | 60  | .93 | 183  | .08 | 34 | 2.03 | .06 | .14 | 11  | 2221  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.





| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe    | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | Li  | Ba*    |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|--------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %     | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm    |
| L46+00N 44+25E     | 104 | 24  | 181 | 258 | .7  | 50  | 4   | 44   | 2.02  | 11  | 5   | ND  | 2   | 10  | 1.2  | 4   | 2   | 335 | .04 | .039 | 13  | 25  | .04 | 336  | .02 | 9   | .67  | .01 | .06 | 1   | 991    |
| L46+00N 44+50E     | 98  | 40  | 28  | 546 | 1.0 | 129 | 4   | 33   | 2.13  | 21  | 5   | ND  | 1   | 14  | 1.1  | 30  | 2   | 609 | .05 | .045 | 10  | 36  | .06 | 957  | .01 | 9   | .83  | .01 | .09 | 1   | 2421   |
| L46+00N 44+75E     | 171 | 51  | 66  | 656 | .8  | 264 | 7   | 79   | 2.57  | 25  | 5   | ND  | 1   | 6   | 1.0  | 7   | 2   | 578 | .03 | .063 | 8   | 42  | .06 | 185  | .01 | 9   | .93  | .01 | .08 | 1   | 1600   |
| L46+00N 45+00E     | 45  | 26  | 56  | 332 | .8  | 78  | 3   | 20   | 1.70  | 21  | 5   | ND  | 1   | 38  | .5   | 10  | 2   | 409 | .01 | .035 | 7   | 20  | .04 | 460  | .01 | 6   | .71  | .02 | .14 | 1   | 1842   |
| L46+00N 45+25E     | 11  | 17  | 16  | 123 | .5  | 27  | 3   | 26   | 1.27  | 6   | 5   | ND  | 1   | 15  | .2   | 2   | 2   | 108 | .01 | .041 | 10  | 19  | .06 | 875  | .01 | 6   | 1.05 | .01 | .10 | 1   | 2131   |
| L46+00N 45+50E     | 17  | 23  | 34  | 181 | .4  | 35  | 3   | 23   | 2.11  | 15  | 5   | ND  | 1   | 64  | .2   | 2   | 2   | 104 | .01 | .046 | 5   | 11  | .04 | 561  | .01 | 6   | .65  | .02 | .17 | 1   | 13666  |
| L46+00N 45+75E     | 15  | 28  | 31  | 250 | .3  | 43  | 4   | 24   | 2.82  | 17  | 5   | ND  | 2   | 74  | .3   | 2   | 2   | 136 | .01 | .052 | 5   | 11  | .04 | 475  | .01 | 7   | .74  | .03 | .17 | 1   | 1724   |
| L46+00N 46+00E     | 16  | 26  | 41  | 201 | .6  | 37  | 4   | 27   | 2.45  | 14  | 5   | ND  | 1   | 70  | .3   | 2   | 2   | 133 | .02 | .059 | 6   | 13  | .04 | 496  | .01 | 8   | .71  | .01 | .17 | 1   | 1701   |
| L46+00N 46+25E     | 16  | 17  | 23  | 139 | .5  | 23  | 3   | 30   | 1.95  | 11  | 5   | ND  | 1   | 61  | .2   | 2   | 2   | 126 | .01 | .038 | 5   | 12  | .05 | 746  | .01 | 7   | .78  | .02 | .15 | 1   | 3761   |
| L46+00N 46+50E     | 15  | 19  | 21  | 131 | .7  | 21  | 2   | 32   | 1.37  | 14  | 5   | ND  | 1   | 77  | .4   | 2   | 2   | 115 | .04 | .048 | 4   | 10  | .04 | 1035 | .01 | 8   | .68  | .01 | .15 | 1   | 28096  |
| L46+00N 46+75E     | 19  | 40  | 54  | 203 | .4  | 40  | 2   | 13   | 2.13  | 38  | 5   | ND  | 2   | 358 | .7   | 3   | 2   | 116 | .07 | .077 | 2   | 13  | .06 | 1135 | .01 | 7   | .94  | .01 | .14 | 1   | 141062 |
| L46+00N 47+00E     | 18  | 14  | 24  | 76  | .2  | 12  | 2   | 22   | 1.06  | 8   | 5   | ND  | 1   | 58  | .3   | 2   | 2   | 112 | .03 | .045 | 7   | 14  | .05 | 724  | .01 | 8   | .68  | .01 | .13 | 1   | 3611   |
| L46+00N 47+25E     | 16  | 18  | 20  | 108 | .4  | 17  | 2   | 42   | 1.27  | 6   | 5   | ND  | 1   | 16  | .4   | 2   | 2   | 113 | .08 | .056 | 7   | 15  | .04 | 513  | .01 | 8   | .63  | .01 | .11 | 1   | 1319   |
| L46+00N 47+50E     | 19  | 19  | 20  | 96  | .6  | 18  | 3   | 53   | 2.02  | 11  | 5   | ND  | 1   | 43  | .3   | 2   | 2   | 153 | .05 | .055 | 8   | 18  | .05 | 558  | .01 | 7   | .84  | .01 | .18 | 1   | 3884   |
| L46+00N 47+75E     | 16  | 12  | 15  | 89  | .4  | 14  | 2   | 48   | 1.40  | 5   | 5   | ND  | 1   | 17  | .3   | 2   | 2   | 137 | .08 | .052 | 10  | 19  | .05 | 419  | .01 | 7   | .82  | .01 | .11 | 1   | 1274   |
| L46+00N 48+00E     | 22  | 20  | 23  | 185 | .6  | 24  | 3   | 24   | 2.14  | 15  | 5   | ND  | 1   | 44  | .4   | 3   | 2   | 118 | .01 | .042 | 4   | 11  | .05 | 533  | .01 | 6   | .78  | .02 | .17 | 1   | 1668   |
| L46+00N 48+25E     | 19  | 26  | 23  | 198 | .8  | 19  | 2   | 26   | 3.10  | 30  | 5   | ND  | 2   | 51  | 1.0  | 8   | 2   | 123 | .03 | .071 | 4   | 12  | .06 | 386  | .01 | 10  | .88  | .04 | .29 | 1   | 1552   |
| L46+00N 48+50E     | 26  | 34  | 26  | 199 | .8  | 17  | 2   | 24   | 3.43  | 22  | 5   | ND  | 1   | 38  | .6   | 6   | 2   | 146 | .05 | .085 | 5   | 17  | .07 | 444  | .01 | 10  | 1.08 | .03 | .23 | 1   | 1369   |
| L46+00N 48+75E     | 10  | 32  | 15  | 151 | .9  | 16  | 2   | 22   | 1.84  | 11  | 5   | ND  | 1   | 21  | .6   | 3   | 2   | 118 | .01 | .080 | 5   | 18  | .08 | 686  | .01 | 7   | 1.49 | .01 | .15 | 1   | 1611   |
| L46+00N 49+00E     | 16  | 60  | 24  | 193 | 1.3 | 21  | 2   | 34   | 3.95  | 29  | 5   | ND  | 3   | 38  | 1.3  | 11  | 2   | 171 | .02 | .088 | 4   | 19  | .09 | 246  | .01 | 7   | 1.65 | .03 | .28 | 1   | 1910   |
| L46+00N 49+25E     | 12  | 19  | 22  | 126 | .6  | 22  | 3   | 24   | 1.63  | 12  | 5   | ND  | 1   | 53  | .3   | 2   | 2   | 108 | .02 | .047 | 5   | 13  | .05 | 661  | .01 | 7   | .87  | .02 | .14 | 1   | 1711   |
| L46+00N 49+50E     | 15  | 26  | 25  | 168 | 1.2 | 28  | 3   | 32   | 2.02  | 15  | 5   | ND  | 1   | 64  | .9   | 4   | 2   | 103 | .02 | .080 | 6   | 14  | .05 | 587  | .01 | 7   | .84  | .02 | .16 | 1   | 1493   |
| L46+00N 49+75E     | 19  | 22  | 32  | 242 | .6  | 29  | 4   | 32   | 2.70  | 18  | 5   | ND  | 1   | 74  | .6   | 7   | 2   | 124 | .02 | .058 | 6   | 12  | .05 | 422  | .01 | 6   | .78  | .03 | .19 | 1   | 1240   |
| L46+00N 50+00E     | 15  | 16  | 20  | 105 | .2  | 17  | 2   | 20   | 1.26  | 12  | 5   | ND  | 1   | 38  | .4   | 4   | 2   | 97  | .04 | .027 | 5   | 10  | .05 | 401  | .01 | 6   | .72  | .01 | .11 | 1   | 1172   |
| L45+00N 39+00E     | 40  | 25  | 35  | 335 | .6  | 55  | 4   | 31   | 1.56  | 15  | 5   | ND  | 1   | 8   | .8   | 8   | 2   | 208 | .02 | .043 | 5   | 19  | .04 | 423  | .01 | 10  | .64  | .01 | .07 | 1   | 3647   |
| RE L46+00N 49+25E  | 16  | 20  | 27  | 133 | .8  | 24  | 3   | 25   | 1.69  | 14  | 5   | ND  | 1   | 55  | .3   | 2   | 2   | 116 | .02 | .050 | 6   | 14  | .05 | 671  | .01 | 7   | .89  | .02 | .14 | 1   | 1653   |
| L45+00N 39+25E     | 33  | 46  | 136 | 840 | 1.8 | 127 | 10  | 305  | 2.29  | 20  | 5   | ND  | 1   | 41  | 8.8  | 8   | 2   | 169 | .64 | .117 | 9   | 24  | .09 | 1299 | .01 | 15  | .71  | .01 | .14 | 1   | 3028   |
| L45+00N 39+50E     | 54  | 42  | 70  | 361 | .6  | 57  | 4   | 34   | 2.01  | 17  | 5   | ND  | 1   | 29  | 3.0  | 4   | 2   | 177 | .15 | .063 | 7   | 17  | .06 | 848  | .01 | 10  | .83  | .01 | .13 | 1   | 2003   |
| L45+00N 39+75E     | 49  | 42  | 47  | 346 | .6  | 66  | 8   | 80   | 2.87  | 17  | 5   | ND  | 1   | 12  | .6   | 3   | 2   | 191 | .02 | .062 | 3   | 17  | .05 | 310  | .01 | 12  | .87  | .01 | .11 | 1   | 1833   |
| L45+00N 40+00E     | 45  | 49  | 62  | 371 | .5  | 75  | 8   | 89   | 3.00  | 21  | 5   | ND  | 1   | 17  | .9   | 3   | 2   | 145 | .05 | .042 | 2   | 15  | .05 | 486  | .01 | 10  | .92  | .01 | .15 | 1   | 2196   |
| L45+00N 40+25E     | 43  | 40  | 74  | 324 | 1.1 | 55  | 7   | 67   | 2.93  | 16  | 5   | ND  | 2   | 24  | 2.1  | 2   | 2   | 141 | .02 | .044 | 5   | 14  | .04 | 418  | .01 | 9   | .76  | .01 | .17 | 1   | 4070   |
| L45+00N 40+50E     | 41  | 36  | 51  | 294 | .6  | 50  | 6   | 68   | 2.82  | 16  | 5   | ND  | 2   | 22  | 1.3  | 2   | 2   | 151 | .03 | .053 | 5   | 13  | .05 | 560  | .01 | 10  | .75  | .01 | .13 | 1   | 1905   |
| L45+00N 40+75E     | 28  | 43  | 89  | 206 | 1.2 | 43  | 5   | 73   | 2.69  | 12  | 5   | ND  | 1   | 134 | 2.9  | 2   | 2   | 104 | .41 | .078 | 7   | 20  | .12 | 1515 | .01 | 9   | .86  | .01 | .19 | 1   | 4069   |
| L45+00N 41+00E     | 74  | 97  | 44  | 370 | 1.3 | 68  | 6   | 33   | 10.03 | 69  | 5   | ND  | 2   | 108 | 2.4  | 2   | 2   | 91  | .19 | .170 | 4   | 12  | .07 | 323  | .01 | 8   | .86  | .02 | .29 | 1   | 3946   |
| L45+00N 41+25E     | 25  | 20  | 33  | 199 | .7  | 34  | 4   | 38   | 1.73  | 14  | 5   | ND  | 1   | 20  | .7   | 2   | 2   | 147 | .02 | .027 | 7   | 12  | .04 | 707  | .01 | 6   | .74  | .01 | .11 | 1   | 1845   |
| L45+00N 41+50E     | 27  | 39  | 33  | 201 | .3  | 36  | 6   | 64   | 2.83  | 12  | 5   | ND  | 1   | 22  | .7   | 2   | 2   | 139 | .04 | .035 | 7   | 13  | .05 | 875  | .01 | 9   | .81  | .01 | .13 | 1   | 2618   |
| L45+00N 41+75E     | 32  | 22  | 34  | 225 | .5  | 45  | 4   | 36   | 1.85  | 15  | 5   | ND  | 1   | 22  | .8   | 2   | 2   | 150 | .04 | .028 | 4   | 11  | .04 | 999  | .01 | 8   | .58  | .01 | .12 | 1   | 2655   |
| STANDARD C/CB-1200 | 18  | 61  | 40  | 134 | 7.3 | 77  | 31  | 1058 | 3.96  | 42  | 19  | 8   | 39  | 52  | 19.0 | 13  | 21  | 57  | .52 | .085 | 39  | 60  | .93 | 183  | .09 | 33  | 1.94 | .08 | .17 | 10  | 2204   |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



## Teck Exploration (BC) PROJECT 1715 FILE # 92-2519

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| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe    | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V    | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*    |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|------|-----|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|--------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %     | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm  | %   | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm    |
| L45+00N 42+00E     | 21  | 12  | 23  | 147 | .3  | 24  | 3   | 30   | 1.34  | 10  | 5   | ND  | 7   | 13  | .2   | 2   | 3   | 128  | .02 | .025 | 7   | 11  | .04 | 401  | .01 | 4  | .69  | .01 | .08 | 1   | 1410   |
| L45+00N 42+25E     | 24  | 15  | 25  | 124 | .3  | 21  | 4   | 32   | 1.64  | 13  | 5   | ND  | 2   | 14  | .2   | 3   | 5   | 121  | .02 | .029 | 6   | 12  | .05 | 435  | .01 | 5  | .89  | .01 | .11 | 1   | 2025   |
| L45+00N 42+50E     | 23  | 20  | 27  | 175 | .5  | 29  | 5   | 41   | 2.08  | 13  | 5   | ND  | 3   | 19  | .6   | 3   | 3   | 141  | .01 | .030 | 7   | 13  | .06 | 334  | .01 | 6  | 1.00 | .01 | .09 | 1   | 1433   |
| L45+00N 42+75E     | 24  | 10  | 17  | 40  | .8  | 10  | 1   | 18   | .69   | 3   | 5   | ND  | 1   | 7   | .2   | 2   | 4   | 59   | .02 | .022 | 3   | 10  | .05 | 277  | .01 | 7  | .84  | .01 | .11 | 1   | 1927   |
| L45+00N 43+00E     | 21  | 98  | 81  | 440 | .6  | 118 | 32  | 885  | 12.37 | 11  | 5   | ND  | 3   | 22  | 2.5  | 2   | 2   | 47   | .12 | .046 | 12  | 23  | .14 | 1431 | .01 | 3  | 1.74 | .01 | .07 | 1   | 3835   |
| L45+00N 43+25E     | 53  | 38  | 99  | 511 | .7  | 91  | 7   | 107  | 3.09  | 23  | 5   | ND  | 1   | 19  | 1.1  | 11  | 2   | 456  | .03 | .064 | 6   | 26  | .07 | 354  | .01 | 5  | 1.04 | .01 | .09 | 1   | 1406   |
| L45+00N 43+50E     | 65  | 31  | 119 | 493 | 1.4 | 90  | 4   | 96   | 1.80  | 17  | 5   | ND  | 1   | 8   | 1.9  | 20  | 2   | 314  | .11 | .069 | 4   | 24  | .04 | 308  | .01 | 12 | .53  | .01 | .09 | 1   | 1183   |
| L45+00N 43+75E     | 35  | 26  | 100 | 277 | .5  | 47  | 4   | 118  | 2.33  | 26  | 5   | ND  | 1   | 8   | 1.0  | 11  | 2   | 235  | .04 | .077 | 5   | 24  | .06 | 168  | .01 | 7  | .79  | .01 | .07 | 1   | 944    |
| L45+00N 44+00E     | 232 | 94  | 153 | 835 | 1.6 | 108 | 6   | 34   | 4.87  | 103 | 9   | ND  | 2   | 21  | 2.7  | 60  | 3   | 1488 | .06 | .121 | 4   | 47  | .06 | 799  | .01 | 15 | .99  | .01 | .13 | 1   | 2075   |
| L45+00N 44+25E     | 173 | 72  | 78  | 947 | .9  | 274 | 7   | 99   | 2.95  | 57  | 10  | ND  | 1   | 10  | 8.0  | 32  | 2   | 1072 | .04 | .049 | 4   | 38  | .05 | 741  | .01 | 9  | .96  | .01 | .10 | 1   | 2185   |
| L45+00N 44+50E     | 133 | 80  | 43  | 938 | .9  | 267 | 7   | 39   | 2.60  | 50  | 5   | ND  | 1   | 15  | 4.8  | 50  | 3   | 1364 | .04 | .052 | 3   | 44  | .05 | 625  | .01 | 19 | .91  | .01 | .15 | 1   | 1922   |
| L45+00N 44+75E     | 32  | 36  | 48  | 138 | 1.4 | 34  | 5   | 10   | 5.56  | 21  | 5   | ND  | 3   | 102 | .7   | 6   | 2   | 194  | .02 | .077 | 3   | 25  | .04 | 56   | .01 | 4  | .81  | .21 | .24 | 1   | 4227   |
| L45+00N 45+00E     | 18  | 22  | 37  | 230 | .8  | 44  | 5   | 33   | 2.69  | 19  | 5   | ND  | 2   | 54  | .3   | 4   | 2   | 152  | .02 | .072 | 5   | 16  | .05 | 639  | .01 | 6  | .91  | .02 | .15 | 1   | 2480   |
| L45+00N 45+25E     | 9   | 41  | 30  | 230 | .6  | 63  | 10  | 64   | 3.46  | 19  | 5   | ND  | 3   | 18  | .3   | 4   | 2   | 100  | .01 | .072 | 2   | 14  | .06 | 316  | .01 | 6  | .98  | .01 | .14 | 1   | 1925   |
| L45+00N 45+50E     | 13  | 33  | 32  | 146 | 1.0 | 30  | 7   | 85   | 3.61  | 13  | 5   | ND  | 1   | 57  | .6   | 2   | 2   | 107  | .03 | .085 | 8   | 22  | .13 | 525  | .01 | 3  | 1.51 | .02 | .16 | 1   | 8378   |
| L45+00N 45+75E     | 13  | 20  | 35  | 168 | .6  | 29  | 5   | 36   | 2.05  | 12  | 5   | ND  | 2   | 67  | .4   | 3   | 2   | 102  | .03 | .054 | 6   | 16  | .06 | 728  | .01 | 9  | .85  | .01 | .17 | 1   | 7033   |
| L45+00N 46+00E     | 16  | 26  | 43  | 284 | 1.0 | 62  | 6   | 32   | 3.47  | 24  | 5   | ND  | 1   | 193 | .5   | 6   | 2   | 101  | .02 | .106 | 5   | 15  | .05 | 527  | .01 | 8  | .82  | .01 | .22 | 1   | 3417   |
| L45+00N 46+25E     | 9   | 25  | 25  | 144 | .5  | 30  | 6   | 82   | 2.52  | 12  | 5   | ND  | 1   | 62  | .2   | 2   | 2   | 97   | .03 | .049 | 9   | 16  | .06 | 627  | .02 | 6  | .82  | .01 | .14 | 1   | 3230   |
| L45+00N 46+50E     | 10  | 17  | 27  | 118 | 1.2 | 24  | 5   | 57   | 1.96  | 15  | 5   | ND  | 1   | 64  | .2   | 2   | 2   | 88   | .03 | .050 | 6   | 14  | .06 | 810  | .01 | 4  | .76  | .01 | .13 | 1   | 4895   |
| L45+00N 46+75E     | 14  | 35  | 38  | 255 | .7  | 48  | 8   | 55   | 3.39  | 27  | 5   | ND  | 4   | 148 | 1.0  | 5   | 2   | 119  | .04 | .087 | 5   | 16  | .07 | 206  | .01 | 6  | .94  | .03 | .22 | 1   | 29420  |
| RE L45+00N 46+25E  | 9   | 24  | 31  | 145 | .5  | 30  | 6   | 83   | 2.60  | 11  | 5   | ND  | 1   | 62  | .3   | 2   | 2   | 99   | .03 | .050 | 8   | 16  | .06 | 640  | .02 | 7  | .83  | .01 | .14 | 1   | 3353   |
| L45+00N 47+00E     | 11  | 9   | 32  | 76  | .3  | 15  | 3   | 42   | 1.40  | 8   | 5   | ND  | 1   | 61  | .3   | 2   | 2   | 106  | .02 | .032 | 6   | 12  | .05 | 656  | .01 | 8  | .73  | .01 | .11 | 1   | 120256 |
| L45+00N 47+25E     | 55  | 12  | 57  | 117 | .8  | 47  | 5   | 35   | 3.18  | 40  | 5   | ND  | 1   | 150 | .2   | 5   | 2   | 251  | .03 | .078 | 7   | 16  | .04 | 134  | .01 | 6  | .54  | .02 | .24 | 1   | 51328  |
| L45+00N 47+50E     | 15  | 6   | 9   | 236 | .5  | 6   | 1   | 7    | .37   | 5   | 5   | ND  | 1   | 10  | .3   | 2   | 3   | 92   | .02 | .016 | 2   | 9   | .03 | 499  | .01 | 8  | .46  | .01 | .09 | 1   | 2007   |
| L45+00N 47+75E     | 12  | 7   | 7   | 51  | .6  | 14  | 3   | 15   | .68   | 2   | 5   | ND  | 2   | 12  | .2   | 2   | 4   | 78   | .01 | .025 | 4   | 10  | .04 | 876  | .01 | 10 | .55  | .01 | .09 | 1   | 1949   |
| L45+00N 48+00E     | 27  | 27  | 27  | 72  | .7  | 15  | 4   | 24   | 2.09  | 12  | 5   | ND  | 1   | 62  | .4   | 3   | 2   | 140  | .02 | .057 | 4   | 16  | .05 | 336  | .01 | 7  | .80  | .01 | .23 | 1   | 2065   |
| L45+00N 48+25E     | 16  | 18  | 18  | 103 | .6  | 17  | 5   | 43   | 1.95  | 14  | 5   | ND  | 1   | 32  | .2   | 3   | 2   | 113  | .02 | .037 | 6   | 16  | .06 | 452  | .01 | 5  | 1.00 | .01 | .14 | 1   | 1765   |
| L45+00N 48+50E     | 36  | 25  | 28  | 139 | .4  | 19  | 5   | 27   | 2.95  | 32  | 5   | ND  | 1   | 43  | .2   | 2   | 2   | 105  | .02 | .065 | 4   | 18  | .07 | 312  | .01 | 7  | 1.10 | .03 | .26 | 1   | 1347   |
| L45+00N 48+75E     | 17  | 32  | 20  | 175 | .9  | 20  | 5   | 36   | 3.14  | 20  | 5   | ND  | 2   | 37  | .5   | 8   | 2   | 167  | .01 | .058 | 4   | 14  | .06 | 389  | .01 | 4  | .97  | .02 | .20 | 1   | 1425   |
| L45+00N 49+00E     | 9   | 16  | 16  | 113 | .8  | 15  | 3   | 25   | 1.50  | 7   | 5   | ND  | 1   | 14  | .5   | 3   | 2   | 134  | .02 | .052 | 4   | 15  | .07 | 424  | .01 | 7  | 1.26 | .01 | .17 | 1   | 1431   |
| L45+00N 49+25E     | 12  | 13  | 20  | 115 | .6  | 16  | 3   | 21   | 1.90  | 9   | 5   | ND  | 1   | 31  | .3   | 3   | 2   | 134  | .02 | .054 | 3   | 16  | .07 | 361  | .01 | 6  | 1.11 | .02 | .17 | 1   | 1347   |
| L45+00N 49+50E     | 8   | 18  | 18  | 118 | .8  | 16  | 4   | 39   | 1.92  | 9   | 5   | ND  | 1   | 32  | .4   | 2   | 2   | 113  | .02 | .046 | 5   | 14  | .06 | 371  | .01 | 6  | .98  | .01 | .16 | 1   | 1389   |
| L45+00N 49+75E     | 14  | 24  | 29  | 221 | 1.1 | 27  | 6   | 43   | 3.01  | 14  | 5   | ND  | 1   | 67  | .8   | 8   | 2   | 145  | .01 | .059 | 7   | 16  | .06 | 418  | .01 | 8  | .98  | .02 | .19 | 1   | 1406   |
| L45+00N 50+00E     | 19  | 28  | 22  | 45  | .7  | 12  | 3   | 20   | 1.30  | 6   | 5   | ND  | 1   | 122 | .2   | 3   | 2   | 128  | .02 | .048 | 4   | 15  | .05 | 607  | .01 | 7  | .80  | .02 | .14 | 1   | 1881   |
| L43+00N 50+00E     | 9   | 17  | 33  | 164 | 1.0 | 25  | 4   | 39   | 2.81  | 17  | 5   | ND  | 1   | 30  | .2   | 2   | 2   | 89   | .03 | .065 | 5   | 16  | .06 | 367  | .01 | 3  | 1.02 | .01 | .17 | 1   | 1771   |
| L43+00N 50+25E     | 7   | 18  | 26  | 148 | .7  | 20  | 4   | 36   | 2.30  | 11  | 5   | ND  | 1   | 31  | .4   | 2   | 2   | 91   | .03 | .054 | 6   | 15  | .07 | 321  | .01 | 4  | 1.11 | .01 | .15 | 1   | 1533   |
| L43+00N 50+50E     | 6   | 18  | 22  | 124 | .3  | 22  | 3   | 19   | 1.50  | 8   | 5   | ND  | 2   | 20  | .3   | 2   | 2   | 78   | .01 | .074 | 6   | 21  | .08 | 330  | .01 | 5  | 1.50 | .01 | .13 | 1   | 1579   |
| STANDARD C/CB-1200 | 19  | 57  | 39  | 132 | 7.6 | 70  | 32  | 1043 | 3.96  | 42  | 21  | 7   | 40  | 52  | 17.7 | 14  | 20  | 57   | .51 | .087 | 38  | 59  | .92 | 183  | .08 | 33 | 2.02 | .06 | .14 | 11  | 2185   |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm   |
| L43+00N 50+75E     | 8   | 28  | 30  | 187  | 1.2 | 42  | 4   | 45   | 2.28 | 15  | 5   | ND  | 3   | 25  | .8   | 2   | 2   | 95  | .02  | .080 | 5   | 18  | .07 | 322  | .01 | 6  | 1.26 | .01 | .17 | 1   | 1487  |
| L43+00N 51+00E     | 7   | 30  | 46  | 230  | 1.7 | 49  | 4   | 46   | 3.09 | 19  | 5   | ND  | 2   | 24  | .7   | 2   | 2   | 90  | .02  | .082 | 5   | 18  | .08 | 294  | .01 | 5  | 1.19 | .01 | .18 | 1   | 1453  |
| L43+00N 51+25E     | 6   | 23  | 29  | 175  | .5  | 37  | 4   | 29   | 2.10 | 15  | 5   | ND  | 2   | 15  | .5   | 2   | 2   | 99  | .01  | .056 | 5   | 18  | .08 | 231  | .01 | 5  | 1.32 | .01 | .15 | 1   | 1283  |
| L43+00N 51+50E     | 5   | 23  | 40  | 175  | 1.4 | 34  | 4   | 44   | 2.41 | 16  | 5   | ND  | 2   | 29  | .5   | 2   | 2   | 83  | .02  | .050 | 5   | 18  | .11 | 225  | .01 | 6  | 1.24 | .01 | .18 | 1   | 1344  |
| L43+00N 51+75E     | 5   | 27  | 22  | 252  | .3  | 49  | 4   | 64   | 2.58 | 13  | 5   | ND  | 2   | 16  | .5   | 2   | 2   | 73  | .02  | .042 | 3   | 10  | .05 | 184  | .01 | 7  | .68  | .01 | .18 | 1   | 1441  |
| L43+00N 52+00E     | 7   | 21  | 24  | 160  | .8  | 32  | 4   | 35   | 1.74 | 11  | 5   | ND  | 2   | 12  | .3   | 3   | 2   | 101 | .01  | .041 | 7   | 18  | .05 | 226  | .01 | 10 | 1.01 | .01 | .14 | 1   | 1067  |
| L43+00N 52+25E     | 12  | 21  | 32  | 189  | .2  | 39  | 4   | 27   | 2.00 | 18  | 5   | ND  | 2   | 48  | .4   | 2   | 2   | 102 | .01  | .041 | 4   | 13  | .05 | 749  | .01 | 11 | .80  | .02 | .14 | 1   | 10704 |
| L43+00N 52+50E     | 10  | 11  | 22  | 34   | .2  | 9   | 1   | 6    | .58  | 5   | 5   | ND  | 1   | 39  | .3   | 2   | 2   | 51  | .02  | .017 | 2   | 9   | .03 | 569  | .01 | 14 | .43  | .01 | .12 | 1   | 1999  |
| L43+00N 52+75E     | 6   | 17  | 27  | 49   | .7  | 12  | 1   | 13   | .78  | 6   | 5   | ND  | 2   | 25  | .4   | 2   | 2   | 64  | .04  | .035 | 5   | 14  | .03 | 1886 | .01 | 15 | .76  | .01 | .11 | 1   | 5187  |
| L43+00N 53+00E     | 15  | 30  | 30  | 102  | 1.2 | 21  | 1   | 17   | 1.34 | 16  | 5   | ND  | 2   | 92  | 1.0  | 2   | 2   | 124 | .05  | .068 | 5   | 17  | .05 | 1167 | .01 | 15 | .86  | .02 | .18 | 1   | 3869  |
| L43+00N 53+25E     | 34  | 23  | 26  | 164  | 1.7 | 22  | 2   | 11   | 2.28 | 15  | 5   | ND  | 2   | 128 | .9   | 3   | 2   | 141 | .02  | .055 | 4   | 14  | .05 | 409  | .01 | 13 | .74  | .02 | .29 | 1   | 1058  |
| L43+00N 53+50E     | 51  | 33  | 50  | 255  | 1.1 | 41  | 2   | 11   | 4.39 | 37  | 5   | ND  | 2   | 107 | 1.1  | 2   | 2   | 152 | .03  | .067 | 3   | 22  | .05 | 77   | .01 | 13 | .68  | .03 | .57 | 1   | 1561  |
| L43+00N 53+75E     | 32  | 52  | 35  | 444  | 2.4 | 77  | 5   | 28   | 2.02 | 24  | 5   | ND  | 1   | 71  | 2.0  | 10  | 2   | 270 | .04  | .066 | 9   | 32  | .05 | 455  | .01 | 12 | .90  | .01 | .15 | 1   | 1099  |
| L43+00N 54+00E     | 19  | 81  | 40  | 1740 | 5.9 | 241 | 14  | 304  | 3.54 | 39  | 5   | ND  | 4   | 34  | 29.1 | 12  | 2   | 274 | 1.39 | .327 | 28  | 69  | .17 | 731  | .01 | 10 | 2.12 | .01 | .13 | 1   | 1197  |
| L43+00N 54+25E     | 192 | 101 | 37  | 1085 | .7  | 339 | 14  | 55   | 4.99 | 45  | 6   | ND  | 3   | 47  | 2.6  | 14  | 2   | 682 | .03  | .099 | 17  | 43  | .07 | 229  | .01 | 16 | 1.04 | .01 | .19 | 1   | 686   |
| L43+00N 54+50E     | 39  | 35  | 22  | 279  | .8  | 57  | 4   | 27   | 2.35 | 16  | 5   | ND  | 1   | 82  | .4   | 5   | 2   | 168 | .03  | .080 | 8   | 19  | .05 | 245  | .01 | 15 | .75  | .01 | .16 | 1   | 676   |
| L43+00N 54+75E     | 39  | 34  | 24  | 433  | .7  | 73  | 5   | 33   | 2.08 | 18  | 5   | ND  | 1   | 40  | 1.5  | 6   | 2   | 206 | .03  | .042 | 8   | 22  | .05 | 173  | .01 | 11 | .74  | .01 | .13 | 1   | 676   |
| L43+00N 55+00E     | 32  | 36  | 31  | 310  | .5  | 57  | 4   | 27   | 1.82 | 16  | 5   | ND  | 2   | 98  | 1.0  | 4   | 2   | 209 | .02  | .065 | 10  | 27  | .09 | 237  | .01 | 15 | 1.36 | .01 | .15 | 1   | 800   |
| L43+00N 55+25E     | 80  | 80  | 24  | 882  | .4  | 237 | 13  | 49   | 3.31 | 25  | 6   | ND  | 2   | 64  | 3.5  | 3   | 2   | 306 | .06  | .113 | 15  | 29  | .07 | 305  | .01 | 10 | 1.16 | .01 | .14 | 1   | 1046  |
| L43+00N 55+50E     | 27  | 54  | 34  | 389  | .5  | 68  | 4   | 43   | 2.16 | 21  | 5   | ND  | 2   | 83  | 3.9  | 4   | 2   | 213 | .07  | .113 | 10  | 27  | .08 | 626  | .01 | 13 | 1.00 | .01 | .17 | 1   | 1365  |
| L43+00N 55+75E     | 30  | 55  | 39  | 554  | .9  | 91  | 6   | 37   | 2.33 | 20  | 5   | ND  | 2   | 102 | 11.2 | 6   | 2   | 224 | .78  | .145 | 22  | 27  | .14 | 726  | .01 | 10 | .91  | .01 | .16 | 1   | 1392  |
| L43+00N 56+00E     | 51  | 68  | 34  | 738  | .6  | 138 | 9   | 64   | 3.17 | 32  | 5   | ND  | 2   | 102 | 3.9  | 6   | 2   | 284 | .13  | .124 | 12  | 28  | .07 | 676  | .01 | 17 | .92  | .01 | .19 | 1   | 1470  |
| L42+00N 50+00E     | 9   | 23  | 32  | 186  | .7  | 33  | 3   | 34   | 2.61 | 14  | 5   | ND  | 1   | 20  | .4   | 2   | 2   | 98  | .04  | .074 | 7   | 16  | .06 | 267  | .01 | 6  | 1.01 | .01 | .13 | 1   | 1374  |
| RE L43+00N 55+25E  | 84  | 81  | 28  | 936  | .5  | 255 | 13  | 51   | 3.56 | 28  | 5   | ND  | 2   | 66  | 3.7  | 4   | 2   | 323 | .06  | .120 | 15  | 31  | .07 | 317  | .01 | 11 | 1.22 | .01 | .14 | 1   | 1033  |
| L42+00N 50+25E     | 9   | 35  | 32  | 268  | .7  | 51  | 4   | 48   | 3.19 | 15  | 5   | ND  | 1   | 35  | .8   | 2   | 2   | 99  | .06  | .102 | 6   | 18  | .09 | 291  | .01 | 5  | 1.25 | .01 | .16 | 1   | 1539  |
| L42+00N 50+50E     | 9   | 32  | 36  | 200  | 2.3 | 41  | 4   | 26   | 2.82 | 18  | 5   | ND  | 2   | 42  | .5   | 2   | 2   | 97  | .02  | .097 | 6   | 19  | .07 | 306  | .01 | 6  | 1.30 | .01 | .19 | 1   | 1605  |
| L42+00N 50+75E     | 7   | 25  | 34  | 174  | 1.4 | 35  | 3   | 34   | 2.40 | 14  | 5   | ND  | 2   | 26  | .4   | 2   | 2   | 97  | .02  | .070 | 6   | 19  | .08 | 279  | .01 | 6  | 1.44 | .01 | .17 | 1   | 1511  |
| L42+00N 51+00E     | 7   | 27  | 29  | 216  | .7  | 43  | 5   | 42   | 2.61 | 13  | 5   | ND  | 2   | 33  | .4   | 2   | 2   | 108 | .04  | .082 | 6   | 20  | .09 | 271  | .01 | 7  | 1.47 | .01 | .19 | 1   | 1316  |
| L42+00N 51+25E     | 8   | 27  | 46  | 233  | 1.1 | 42  | 5   | 43   | 2.48 | 14  | 5   | ND  | 2   | 46  | .2   | 2   | 2   | 85  | .01  | .056 | 5   | 16  | .06 | 472  | .01 | 8  | .99  | .01 | .19 | 1   | 2092  |
| L42+00N 51+50E     | 6   | 21  | 24  | 161  | .7  | 30  | 4   | 26   | 1.80 | 13  | 5   | ND  | 2   | 23  | .2   | 3   | 2   | 91  | .02  | .046 | 4   | 16  | .07 | 283  | .01 | 9  | 1.13 | .01 | .16 | 1   | 1423  |
| L42+00N 51+75E     | 21  | 37  | 52  | 193  | .7  | 44  | 3   | 19   | 2.71 | 27  | 5   | ND  | 3   | 338 | .2   | 3   | 2   | 99  | .02  | .085 | 3   | 15  | .03 | 344  | .01 | 13 | .61  | .03 | .20 | 1   | 34402 |
| L42+00N 52+00E     | 6   | 18  | 16  | 125  | 1.0 | 26  | 3   | 39   | 1.48 | 6   | 5   | ND  | 2   | 12  | .4   | 2   | 2   | 97  | .01  | .029 | 7   | 17  | .06 | 288  | .01 | 7  | 1.05 | .01 | .13 | 1   | 1259  |
| L42+00N 52+25E     | 28  | 27  | 34  | 287  | .9  | 55  | 4   | 28   | 2.27 | 19  | 5   | ND  | 3   | 71  | .3   | 3   | 2   | 196 | .01  | .039 | 5   | 18  | .06 | 383  | .01 | 12 | .95  | .01 | .18 | 1   | 1099  |
| L42+00N 52+50E     | 6   | 10  | 20  | 33   | .2  | 8   | 1   | 5    | .42  | 3   | 5   | ND  | 2   | 34  | .2   | 2   | 2   | 82  | .01  | .014 | 2   | 10  | .04 | 528  | .01 | 16 | .67  | .01 | .15 | 1   | 1305  |
| L42+00N 52+75E     | 7   | 14  | 20  | 98   | 1.2 | 20  | 2   | 17   | .96  | 8   | 5   | ND  | 1   | 20  | .2   | 2   | 2   | 99  | .01  | .021 | 2   | 11  | .05 | 221  | .01 | 12 | .79  | .01 | .13 | 1   | 1130  |
| L42+00N 53+00E     | 19  | 23  | 28  | 161  | .9  | 34  | 3   | 23   | 1.58 | 11  | 5   | ND  | 2   | 70  | .3   | 2   | 2   | 122 | .01  | .037 | 4   | 14  | .04 | 405  | .01 | 10 | .68  | .01 | .17 | 1   | 1361  |
| L42+00N 53+25E     | 7   | 39  | 14  | 73   | 1.6 | 17  | 2   | 10   | .97  | 5   | 5   | ND  | 1   | 54  | .4   | 2   | 2   | 66  | .02  | .040 | 4   | 12  | .03 | 629  | .01 | 9  | .67  | .01 | .11 | 1   | 1937  |
| STANDARD C/CB-1200 | 18  | 56  | 39  | 127  | 6.9 | 70  | 30  | 1021 | 3.96 | 39  | 18  | 7   | 35  | 53  | 18.8 | 18  | 19  | 54  | .50  | .087 | 36  | 57  | .90 | 190  | .08 | 35 | 1.96 | .08 | .16 | 12  | 2187  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg   | Ba   | Ti  | B   | Al   | Na  | K   | W  | Ba*   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|------|-----|-----|------|-----|-----|----|-------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %    | ppm  | %   | ppm | %    | %   | %   | %  | ppm   |
| L42+00N 53+50E     | 12  | 22  | 39  | 193  | 1.7 | 35  | 6   | 35   | 2.34 | 13  | 5   | ND  | 6   | 141 | .3   | 2   | 2   | 93  | .01  | .058 | 3   | 15  | .04  | 603  | .01 | 13  | .78  | .02 | .17 | 2  | 20523 |
| L42+00N 53+75E     | 14  | 46  | 23  | 56   | 2.6 | 18  | 2   | 10   | 1.29 | 6   | 5   | ND  | 2   | 127 | .2   | 2   | 2   | 113 | .02  | .047 | 2   | 15  | .04  | 673  | .01 | 11  | .74  | .01 | .17 | 1  | 2313  |
| L42+00N 54+00E     | 8   | 22  | 19  | 53   | .4  | 12  | 1   | 9    | .74  | 7   | 5   | ND  | 1   | 53  | .2   | 2   | 3   | 84  | .03  | .036 | 2   | 12  | .03  | 708  | .01 | 11  | .57  | .01 | .12 | 1  | 1926  |
| L42+00N 54+25E     | 7   | 15  | 18  | 118  | 1.0 | 22  | 4   | 21   | 1.28 | 7   | 5   | ND  | 1   | 24  | .3   | 2   | 2   | 91  | .01  | .035 | 5   | 17  | .06  | 1188 | .01 | 8   | 1.06 | .01 | .12 | 1  | 2822  |
| L42+00N 54+50E     | 15  | 18  | 22  | 129  | 3.0 | 27  | 3   | 15   | 1.12 | 8   | 5   | ND  | 1   | 68  | .2   | 4   | 2   | 125 | .01  | .037 | 3   | 15  | .05  | 549  | .01 | 9   | .82  | .01 | .14 | 1  | 1330  |
| L42+00N 54+75E     | 26  | 20  | 39  | 276  | 2.2 | 41  | 7   | 21   | 3.59 | 16  | 5   | ND  | 4   | 142 | 1.2  | 13  | 2   | 158 | .01  | .059 | 4   | 15  | .05  | 153  | .01 | 8   | .89  | .03 | .38 | 1  | 1392  |
| L42+00N 55+00E     | 12  | 14  | 24  | 110  | 1.2 | 19  | 2   | 16   | 1.26 | 7   | 5   | ND  | 2   | 58  | .6   | 3   | 2   | 127 | .01  | .029 | 2   | 13  | .05  | 332  | .01 | 13  | .84  | .01 | .17 | 1  | 1186  |
| L42+00N 55+25E     | 46  | 42  | 39  | 433  | 1.3 | 86  | 7   | 39   | 2.51 | 23  | 5   | ND  | 2   | 112 | 1.1  | 10  | 2   | 321 | .03  | .083 | 8   | 24  | .06  | 407  | .01 | 8   | .83  | .01 | .16 | 1  | 1076  |
| L42+00N 55+50E     | 54  | 68  | 67  | 1007 | 1.7 | 157 | 9   | 34   | 2.79 | 63  | 5   | ND  | 3   | 169 | 4.0  | 25  | 2   | 625 | .07  | .121 | 12  | 42  | .08  | 430  | .01 | 11  | 1.20 | .01 | .12 | 1  | 978   |
| L42+00N 55+75E     | 23  | 35  | 41  | 615  | .4  | 90  | 6   | 26   | 1.84 | 28  | 5   | ND  | 1   | 74  | 3.1  | 8   | 2   | 285 | .07  | .070 | 9   | 31  | .08  | 264  | .01 | 9   | .98  | .01 | .09 | 1  | 752   |
| L42+00N 56+00E     | 40  | 61  | 25  | 627  | .8  | 129 | 9   | 62   | 2.68 | 26  | 5   | ND  | 1   | 43  | 3.6  | 8   | 2   | 325 | .31  | .295 | 14  | 39  | .08  | 318  | .01 | 13  | 1.02 | .01 | .14 | 1  | 999   |
| L41+00N 50+00E     | 157 | 47  | 38  | 1699 | .7  | 364 | 27  | 99   | 6.93 | 75  | 5   | ND  | 4   | 19  | 2.9  | 21  | 5   | 571 | .03  | .110 | 7   | 26  | .08  | 91   | .01 | 5   | 1.09 | .01 | .07 | 1  | 580   |
| L41+00N 50+25E     | 19  | 25  | 25  | 222  | .4  | 43  | 4   | 37   | 1.42 | 12  | 5   | ND  | 1   | 47  | 2.4  | 3   | 2   | 146 | .46  | .047 | 15  | 20  | .14  | 285  | .01 | 5   | .97  | .01 | .08 | 1  | 1041  |
| L41+00N 50+50E     | 39  | 55  | 32  | 805  | 1.5 | 113 | 10  | 181  | 2.14 | 25  | 5   | ND  | 1   | 42  | 8.6  | 10  | 2   | 482 | .61  | .177 | 19  | 37  | .14  | 735  | .01 | 8   | 1.01 | .01 | .12 | 1  | 1488  |
| L41+00N 50+75E     | 31  | 38  | 22  | 446  | .5  | 74  | 5   | 54   | 1.26 | 12  | 5   | ND  | 1   | 24  | 7.0  | 5   | 2   | 401 | .18  | .063 | 17  | 26  | .09  | 605  | .01 | 7   | .86  | .01 | .09 | 1  | 1285  |
| L41+00N 51+00E     | 68  | 70  | 26  | 1917 | 2.5 | 319 | 8   | 205  | 1.64 | 36  | 6   | ND  | 2   | 51  | 21.8 | 18  | 2   | 934 | 1.17 | .127 | 21  | 42  | .20  | 723  | .01 | 11  | .88  | .01 | .15 | 1  | 1454  |
| L41+00N 51+25E     | 24  | 40  | 15  | 855  | 1.3 | 125 | 4   | 60   | 1.09 | 12  | 5   | ND  | 1   | 37  | 13.6 | 5   | 2   | 283 | .80  | .061 | 14  | 32  | .15  | 869  | .01 | 5   | .70  | .01 | .09 | 1  | 1657  |
| L41+00N 51+50E     | 77  | 53  | 28  | 1084 | 1.8 | 271 | 9   | 163  | 1.33 | 33  | 5   | ND  | 4   | 65  | 9.9  | 13  | 2   | 569 | 4.47 | .121 | 16  | 22  | 2.24 | 222  | .01 | 15  | .42  | .01 | .12 | 1  | 917   |
| L41+00N 51+75E     | 14  | 17  | 18  | 188  | .4  | 33  | 3   | 19   | 1.04 | 7   | 5   | ND  | 1   | 35  | .9   | 3   | 2   | 130 | .10  | .040 | 2   | 14  | .07  | 325  | .01 | 11  | .74  | .01 | .12 | 1  | 1238  |
| L41+00N 52+00E     | 18  | 25  | 27  | 223  | .9  | 40  | 4   | 18   | 1.64 | 11  | 5   | ND  | 1   | 74  | 1.2  | 3   | 2   | 145 | .03  | .053 | 3   | 18  | .06  | 433  | .01 | 9   | .92  | .01 | .16 | 1  | 1151  |
| L41+00N 52+25E     | 31  | 64  | 44  | 1277 | 1.5 | 204 | 13  | 118  | 2.84 | 31  | 5   | ND  | 2   | 41  | 10.1 | 14  | 2   | 428 | .41  | .262 | 16  | 49  | .21  | 471  | .01 | 16  | 1.66 | .01 | .10 | 1  | 981   |
| L41+00N 52+50E     | 22  | 40  | 40  | 615  | .6  | 80  | 6   | 55   | 2.19 | 15  | 5   | ND  | 1   | 81  | 5.1  | 6   | 3   | 247 | .09  | .144 | 10  | 32  | .09  | 884  | .01 | 9   | 1.32 | .01 | .16 | 1  | 1630  |
| L41+00N 52+75E     | 27  | 38  | 35  | 523  | .8  | 80  | 6   | 33   | 2.04 | 17  | 5   | ND  | 1   | 63  | 2.4  | 7   | 2   | 230 | .03  | .083 | 7   | 27  | .07  | 605  | .01 | 11  | .99  | .01 | .14 | 1  | 1298  |
| L41+00N 53+00E     | 26  | 46  | 38  | 658  | .7  | 88  | 9   | 181  | 2.39 | 19  | 5   | ND  | 1   | 95  | 5.3  | 7   | 2   | 237 | .48  | .153 | 10  | 29  | .11  | 915  | .01 | 9   | 1.02 | .01 | .16 | 1  | 1660  |
| L41+00N 53+25E     | 13  | 73  | 21  | 926  | 4.4 | 361 | 5   | 361  | 1.56 | 14  | 5   | ND  | 1   | 166 | 36.1 | 6   | 2   | 180 | 2.46 | .174 | 8   | 26  | .26  | 1085 | .01 | 13  | 1.00 | .01 | .10 | 1  | 2721  |
| L41+00N 53+50E     | 16  | 47  | 32  | 438  | 1.9 | 73  | 5   | 70   | 1.59 | 11  | 5   | ND  | 1   | 151 | 9.2  | 5   | 2   | 174 | 1.03 | .107 | 9   | 22  | .15  | 1079 | .01 | 8   | .88  | .01 | .15 | 1  | 1762  |
| L41+00N 53+75E     | 20  | 15  | 15  | 199  | .5  | 40  | 3   | 26   | .87  | 7   | 5   | ND  | 1   | 26  | 1.2  | 4   | 2   | 159 | .15  | .036 | 11  | 18  | .07  | 240  | .01 | 8   | .55  | .01 | .08 | 1  | 944   |
| RE L41+00N 52+75E  | 26  | 35  | 33  | 472  | .6  | 74  | 6   | 29   | 1.87 | 15  | 5   | ND  | 1   | 58  | 2.2  | 6   | 3   | 217 | .03  | .075 | 7   | 26  | .07  | 550  | .01 | 13  | .94  | .01 | .13 | 1  | 1327  |
| L41+00N 54+00E     | 87  | 40  | 30  | 390  | .7  | 129 | 3   | 30   | 1.39 | 24  | 5   | ND  | 1   | 10  | 1.2  | 10  | 2   | 812 | .06  | .035 | 11  | 39  | .07  | 142  | .01 | 8   | .76  | .01 | .09 | 1  | 710   |
| L41+00N 54+25E     | 47  | 28  | 29  | 405  | .5  | 83  | 7   | 105  | 3.12 | 33  | 5   | ND  | 4   | 61  | 1.4  | 7   | 2   | 490 | .43  | .127 | 12  | 37  | .27  | 234  | .01 | 4   | 1.44 | .01 | .13 | 1  | 1103  |
| L41+00N 54+50E     | 13  | 23  | 29  | 245  | .7  | 59  | 7   | 35   | 3.56 | 15  | 5   | ND  | 1   | 18  | .3   | 3   | 2   | 127 | .18  | .114 | 5   | 19  | .07  | 402  | .01 | 6   | 1.09 | .01 | .13 | 1  | 1664  |
| L41+00N 54+75E     | 11  | 33  | 33  | 166  | 1.0 | 33  | 6   | 44   | 2.58 | 13  | 5   | ND  | 1   | 25  | .7   | 2   | 2   | 102 | .03  | .094 | 5   | 20  | .08  | 589  | .01 | 4   | 1.26 | .01 | .16 | 1  | 2003  |
| L41+00N 55+00E     | 12  | 35  | 39  | 289  | 3.7 | 64  | 9   | 59   | 5.32 | 21  | 5   | ND  | 3   | 49  | .9   | 2   | 3   | 107 | .03  | .133 | 5   | 24  | .12  | 372  | .01 | 6   | 1.63 | .01 | .15 | 1  | 1673  |
| L41+00N 55+25E     | 8   | 24  | 31  | 195  | 1.1 | 35  | 6   | 28   | 2.52 | 11  | 5   | ND  | 1   | 25  | .7   | 2   | 2   | 104 | .02  | .078 | 5   | 19  | .08  | 266  | .01 | 5   | 1.42 | .01 | .15 | 1  | 1394  |
| L41+00N 55+50E     | 8   | 25  | 35  | 201  | .5  | 40  | 6   | 42   | 2.62 | 15  | 5   | ND  | 1   | 49  | .5   | 2   | 2   | 101 | .01  | .049 | 5   | 18  | .07  | 288  | .01 | 4   | 1.22 | .01 | .15 | 1  | 1455  |
| L41+00N 55+75E     | 11  | 18  | 21  | 119  | .5  | 26  | 4   | 23   | 2.22 | 14  | 5   | ND  | 2   | 92  | .2   | 3   | 2   | 85  | .01  | .054 | 2   | 12  | .04  | 810  | .01 | 7   | .61  | .01 | .11 | 1  | 28733 |
| L41+00N 56+00E     | 10  | 14  | 42  | 87   | .7  | 23  | 3   | 15   | 1.82 | 14  | 5   | ND  | 2   | 211 | .2   | 4   | 2   | 56  | .01  | .053 | 2   | 11  | .03  | 291  | .01 | 10  | .47  | .02 | .17 | 1  | 77320 |
| STANDARD C/CB-1200 | 19  | 57  | 38  | 130  | 7.4 | 69  | 32  | 1042 | 3.96 | 41  | 21  | 7   | 40  | 52  | 19.1 | 14  | 21  | 57  | .52  | .087 | 38  | 60  | .93  | 191  | .08 | 34  | 2.01 | .06 | .14 | 10 | 2221  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V    | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|------|------|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm  | %    | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm   |
| L40+00N 50+00E     | 7   | 17  | 33  | 118  | .4  | 23  | 4   | 22   | 1.89 | 9   | 5   | ND  | 6   | 26  | .2   | 2   | 2   | 86   | .02  | .064 | 6   | 17  | .06 | 273  | .01 | 4  | 1.16 | .01 | .12 | 1   | 1356  |
| L40+00N 50+25E     | 8   | 19  | 30  | 120  | 1.5 | 23  | 4   | 18   | 1.88 | 12  | 5   | ND  | 3   | 25  | .2   | 2   | 2   | 87   | .01  | .086 | 4   | 19  | .06 | 892  | .01 | 5  | 1.22 | .01 | .14 | 1   | 2323  |
| L40+00N 50+50E     | 7   | 22  | 32  | 147  | .5  | 27  | 5   | 20   | 1.86 | 11  | 5   | ND  | 2   | 36  | .2   | 2   | 2   | 89   | .01  | .069 | 4   | 17  | .06 | 1053 | .01 | 5  | 1.15 | .01 | .15 | 1   | 3130  |
| L40+00N 50+75E     | 6   | 16  | 27  | 127  | .4  | 22  | 3   | 14   | 1.47 | 11  | 5   | ND  | 2   | 18  | .2   | 2   | 2   | 85   | .01  | .047 | 4   | 15  | .06 | 255  | .01 | 7  | 1.05 | .01 | .14 | 1   | 1591  |
| L40+00N 51+00E     | 7   | 22  | 24  | 113  | .4  | 23  | 4   | 24   | 1.58 | 10  | 5   | ND  | 1   | 37  | .3   | 2   | 2   | 78   | .02  | .050 | 4   | 15  | .05 | 385  | .01 | 6  | .93  | .01 | .13 | 1   | 1595  |
| L40+00N 51+25E     | 16  | 25  | 76  | 213  | 2.4 | 39  | 6   | 34   | 2.23 | 14  | 5   | ND  | 3   | 59  | .4   | 2   | 2   | 103  | .01  | .057 | 4   | 18  | .04 | 596  | .01 | 13 | .94  | .01 | .20 | 1   | 5226  |
| L40+00N 51+50E     | 11  | 29  | 40  | 180  | 2.7 | 44  | 7   | 26   | 1.87 | 14  | 5   | ND  | 3   | 50  | .4   | 2   | 2   | 102  | .01  | .053 | 4   | 18  | .04 | 454  | .01 | 13 | 1.10 | .01 | .13 | 1   | 1759  |
| L40+00N 51+75E     | 9   | 17  | 40  | 73   | 1.8 | 21  | 3   | 17   | 1.00 | 7   | 5   | ND  | 2   | 87  | .2   | 2   | 2   | 81   | .01  | .037 | 3   | 14  | .04 | 1235 | .01 | 13 | .78  | .01 | .13 | 1   | 7712  |
| L40+00N 52+00E     | 9   | 19  | 40  | 144  | 1.1 | 31  | 5   | 28   | 1.61 | 10  | 9   | ND  | 2   | 78  | .4   | 2   | 2   | 92   | .01  | .051 | 4   | 14  | .05 | 871  | .01 | 15 | .92  | .01 | .15 | 1   | 3373  |
| RE L40+00N 53+25E  | 24  | 35  | 23  | 229  | 1.0 | 46  | 5   | 20   | 2.21 | 17  | 6   | ND  | 3   | 117 | .8   | 5   | 2   | 185  | .02  | .086 | 4   | 21  | .06 | 535  | .01 | 10 | 1.03 | .01 | .17 | 1   | 1443  |
| L40+00N 52+25E     | 8   | 18  | 32  | 72   | .4  | 23  | 3   | 13   | .97  | 5   | 5   | ND  | 2   | 77  | .2   | 2   | 2   | 94   | .01  | .033 | 2   | 14  | .05 | 927  | .01 | 16 | .83  | .01 | .12 | 1   | 7029  |
| L40+00N 52+50E     | 7   | 15  | 18  | 94   | 1.0 | 19  | 4   | 20   | .94  | 5   | 7   | ND  | 1   | 17  | .3   | 2   | 2   | 73   | .01  | .039 | 7   | 17  | .04 | 612  | .01 | 12 | .81  | .01 | .10 | 1   | 1631  |
| L40+00N 52+75E     | 19  | 23  | 25  | 186  | .8  | 34  | 3   | 16   | 1.19 | 10  | 6   | ND  | 1   | 91  | .7   | 3   | 4   | 154  | .02  | .073 | 4   | 20  | .07 | 407  | .01 | 14 | 1.04 | .01 | .16 | 1   | 1119  |
| L40+00N 53+00E     | 27  | 34  | 25  | 302  | 1.7 | 56  | 4   | 20   | 1.75 | 17  | 5   | ND  | 1   | 84  | .9   | 4   | 2   | 210  | .01  | .051 | 4   | 18  | .06 | 320  | .01 | 11 | .83  | .01 | .12 | 1   | 930   |
| L40+00N 53+25E     | 25  | 35  | 24  | 239  | 1.1 | 45  | 5   | 22   | 2.29 | 22  | 9   | ND  | 3   | 119 | 1.0  | 5   | 2   | 194  | .02  | .089 | 4   | 21  | .06 | 517  | .01 | 11 | 1.05 | .01 | .18 | 1   | 1455  |
| L40+00N 53+50E     | 27  | 40  | 32  | 455  | .4  | 83  | 6   | 24   | 1.77 | 16  | 5   | ND  | 1   | 44  | 1.2  | 5   | 2   | 200  | .04  | .058 | 8   | 28  | .05 | 247  | .01 | 11 | .76  | .01 | .10 | 1   | 878   |
| L40+00N 53+75E     | 12  | 17  | 20  | 160  | .1  | 26  | 2   | 15   | .78  | 7   | 5   | ND  | 1   | 35  | .8   | 2   | 2   | 150  | .03  | .044 | 11  | 21  | .06 | 188  | .01 | 10 | .82  | .01 | .08 | 1   | 878   |
| L40+00N 54+00E     | 39  | 31  | 24  | 328  | .9  | 68  | 6   | 26   | 2.00 | 11  | 5   | ND  | 1   | 26  | .5   | 2   | 2   | 178  | .01  | .043 | 8   | 17  | .05 | 131  | .01 | 11 | .75  | .01 | .10 | 1   | 669   |
| L40+00N 54+25E     | 28  | 21  | 25  | 282  | .5  | 56  | 4   | 25   | 1.42 | 13  | 14  | ND  | 2   | 26  | .5   | 5   | 2   | 197  | .01  | .032 | 7   | 17  | .05 | 158  | .01 | 9  | .72  | .01 | .10 | 1   | 804   |
| L40+00N 54+50E     | 11  | 13  | 19  | 132  | .9  | 20  | 3   | 25   | .99  | 3   | 5   | ND  | 1   | 27  | .6   | 2   | 2   | 129  | .03  | .048 | 12  | 19  | .09 | 209  | .01 | 7  | .93  | .01 | .10 | 1   | 1035  |
| L40+00N 54+75E     | 30  | 28  | 26  | 270  | .6  | 51  | 5   | 57   | 2.00 | 18  | 5   | ND  | 1   | 35  | 1.1  | 3   | 2   | 302  | .07  | .100 | 13  | 29  | .14 | 303  | .01 | 7  | 1.14 | .01 | .10 | 1   | 1022  |
| L40+00N 55+00E     | 39  | 34  | 43  | 333  | .2  | 70  | 4   | 43   | 1.61 | 21  | 5   | ND  | 2   | 32  | 1.1  | 5   | 2   | 464  | .04  | .065 | 13  | 35  | .10 | 203  | .01 | 6  | 1.13 | .01 | .09 | 1   | 887   |
| L40+00N 55+25E     | 44  | 58  | 39  | 391  | .4  | 95  | 4   | 23   | 1.67 | 20  | 5   | ND  | 2   | 15  | 2.0  | 9   | 2   | 516  | .11  | .146 | 18  | 39  | .06 | 245  | .01 | 7  | .78  | .01 | .09 | 1   | 865   |
| L40+00N 55+50E     | 61  | 125 | 20  | 2312 | 7.1 | 271 | 8   | 127  | 1.97 | 54  | 12  | ND  | 3   | 72  | 33.1 | 35  | 3   | 1122 | 1.54 | .575 | 25  | 84  | .18 | 618  | .01 | 26 | 1.14 | .01 | .24 | 1   | 1315  |
| L40+00N 55+75E     | 60  | 108 | 23  | 601  | 2.0 | 137 | 5   | 22   | 1.40 | 32  | 11  | ND  | 2   | 31  | 7.6  | 38  | 2   | 1068 | .60  | .277 | 21  | 118 | .09 | 207  | .01 | 10 | .96  | .01 | .11 | 1   | 500   |
| L40+00N 56+00E     | 84  | 39  | 48  | 527  | .7  | 142 | 7   | 60   | 2.61 | 32  | 5   | ND  | 4   | 35  | 1.5  | 11  | 2   | 774  | .09  | .080 | 16  | 49  | .14 | 212  | .01 | 6  | 1.62 | .01 | .10 | 1   | 887   |
| L38+00N 43+00E     | 40  | 20  | 46  | 325  | .4  | 57  | 5   | 28   | 1.72 | 16  | 5   | ND  | 2   | 36  | .5   | 8   | 3   | 225  | .04  | .036 | 4   | 14  | .04 | 742  | .01 | 8  | .56  | .01 | .10 | 1   | 2693  |
| L38+00N 43+25E     | 29  | 15  | 50  | 200  | .6  | 35  | 4   | 20   | 1.17 | 9   | 9   | ND  | 2   | 28  | .2   | 6   | 2   | 196  | .02  | .025 | 5   | 13  | .04 | 1393 | .01 | 8  | .73  | .01 | .08 | 1   | 8788  |
| L38+00N 43+50E     | 34  | 30  | 56  | 394  | .6  | 67  | 8   | 62   | 2.50 | 14  | 5   | ND  | 2   | 39  | .7   | 6   | 3   | 197  | .07  | .073 | 4   | 16  | .07 | 979  | .01 | 9  | .74  | .01 | .11 | 1   | 6224  |
| L38+00N 43+75E     | 39  | 33  | 67  | 470  | .3  | 76  | 10  | 58   | 3.20 | 23  | 5   | ND  | 2   | 43  | .8   | 7   | 2   | 177  | .04  | .074 | 5   | 16  | .08 | 986  | .01 | 7  | .81  | .01 | .11 | 1   | 6103  |
| L38+00N 44+00E     | 24  | 21  | 34  | 214  | .5  | 38  | 4   | 28   | 2.30 | 18  | 5   | ND  | 3   | 49  | .3   | 4   | 2   | 194  | .01  | .049 | 3   | 16  | .05 | 752  | .01 | 5  | .88  | .01 | .13 | 1   | 9973  |
| L38+00N 44+25E     | 30  | 24  | 57  | 310  | .4  | 57  | 6   | 31   | 2.78 | 17  | 5   | ND  | 3   | 85  | .3   | 4   | 2   | 202  | .01  | .058 | 3   | 13  | .04 | 523  | .01 | 5  | .75  | .02 | .14 | 1   | 3400  |
| L38+00N 44+50E     | 18  | 76  | 45  | 468  | .7  | 67  | 11  | 168  | 7.43 | 25  | 5   | ND  | 2   | 36  | .8   | 4   | 2   | 140  | .02  | .181 | 2   | 17  | .07 | 900  | .01 | 12 | 1.19 | .01 | .16 | 1   | 3590  |
| L38+00N 44+75E     | 27  | 20  | 45  | 211  | .6  | 37  | 6   | 40   | 2.44 | 14  | 5   | ND  | 2   | 47  | .2   | 4   | 2   | 154  | .01  | .042 | 3   | 13  | .05 | 576  | .01 | 2  | .84  | .01 | .11 | 1   | 45416 |
| L38+00N 45+00E     | 20  | 78  | 35  | 309  | 1.4 | 85  | 7   | 39   | 3.68 | 15  | 6   | ND  | 2   | 72  | 1.4  | 3   | 5   | 132  | .07  | .090 | 3   | 18  | .07 | 1123 | .01 | 9  | 1.39 | .01 | .17 | 1   | 4823  |
| L38+00N 45+25E     | 39  | 31  | 58  | 153  | .7  | 30  | 4   | 22   | 2.35 | 36  | 5   | ND  | 3   | 252 | .2   | 5   | 2   | 164  | .10  | .083 | 3   | 15  | .04 | 279  | .01 | 12 | .61  | .01 | .17 | 1   | 79156 |
| L38+00N 45+50E     | 37  | 16  | 35  | 79   | .4  | 15  | 4   | 50   | 1.37 | 11  | 5   | ND  | 2   | 140 | .3   | 4   | 2   | 175  | .09  | .067 | 11  | 21  | .07 | 1415 | .01 | 7  | .88  | .01 | .10 | 1   | 3706  |
| STANDARD C/CB-1200 | 19  | 58  | 39  | 131  | 7.5 | 69  | 32  | 1051 | 3.96 | 43  | 17  | 7   | 39  | 53  | 18.4 | 14  | 21  | 59   | .52  | .087 | 38  | 60  | .93 | 186  | .08 | 35 | 2.01 | .06 | .14 | 11  | 2185  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



## Teck Exploration (BC) PROJECT 1715 FILE # 92-2519

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| SAMPLE#             | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | U   | Ba*   |
|---------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|-------|
|                     | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm   |
| L38+00N 45+75E      | 23  | 60  | 29  | 250 | .8  | 68  | 5   | 31   | 2.65 | 20  | 5   | ND  | 4   | 104 | 6.0  | 3   | 3   | 121 | .24  | .101 | 5   | 18  | .10 | 1555 | .01 | 12  | 1.25 | .02 | .18 | 1   | 4834  |
| L38+00N 45+80E SILT | 27  | 73  | 28  | 504 | .9  | 112 | 9   | 177  | 3.32 | 29  | 7   | ND  | 2   | 126 | 7.0  | 6   | 2   | 96  | .45  | .085 | 4   | 13  | .11 | 527  | .01 | 10  | .81  | .02 | .20 | 1   | 12232 |
| L38+00N 46+00E      | 18  | 19  | 31  | 177 | .2  | 31  | 3   | 25   | 1.85 | 15  | 5   | ND  | 1   | 49  | .4   | 33  | 2   | 118 | .03  | .047 | 4   | 11  | .04 | 717  | .01 | 9   | .66  | .02 | .15 | 1   | 2508  |
| L38+00N 46+25E      | 18  | 24  | 30  | 215 | .4  | 37  | 4   | 25   | 2.03 | 13  | 5   | ND  | 1   | 57  | 1.2  | 4   | 3   | 119 | .05  | .060 | 3   | 13  | .05 | 725  | .01 | 10  | .76  | .01 | .17 | 1   | 2073  |
| L38+00N 46+50E      | 31  | 26  | 52  | 253 | .8  | 43  | 3   | 41   | 2.67 | 20  | 5   | ND  | 1   | 60  | 1.1  | 8   | 3   | 226 | .05  | .079 | 4   | 18  | .07 | 864  | .01 | 10  | 1.00 | .02 | .18 | 1   | 5404  |
| L38+00N 46+75E      | 20  | 19  | 23  | 167 | .3  | 30  | 3   | 17   | 1.86 | 13  | 5   | ND  | 1   | 69  | .5   | 3   | 2   | 84  | .09  | .042 | 3   | 9   | .05 | 723  | .01 | 8   | .53  | .02 | .16 | 1   | 3281  |
| RE L38+00N 48+00E   | 33  | 30  | 54  | 177 | 1.9 | 42  | 3   | 22   | 2.70 | 28  | 5   | ND  | 1   | 181 | 1.2  | 10  | 2   | 168 | .35  | .120 | 5   | 17  | .06 | 367  | .01 | 10  | .80  | .03 | .29 | 1   | 3302  |
| L38+00N 47+00E      | 44  | 34  | 37  | 283 | 2.6 | 77  | 6   | 525  | 3.61 | 49  | 5   | ND  | 2   | 226 | 2.5  | 3   | 2   | 154 | 1.26 | .117 | 5   | 21  | .29 | 682  | .01 | 8   | 2.09 | .02 | .24 | 1   | 3198  |
| L38+00N 47+25E      | 22  | 13  | 26  | 113 | .1  | 20  | 3   | 37   | 1.85 | 14  | 5   | ND  | 1   | 247 | .5   | 2   | 2   | 98  | .10  | .049 | 7   | 15  | .04 | 427  | .01 | 8   | .64  | .01 | .11 | 1   | 1244  |
| L38+00N 47+50E      | 24  | 17  | 18  | 140 | .1  | 28  | 4   | 38   | 1.61 | 10  | 5   | ND  | 1   | 62  | 1.0  | 2   | 2   | 97  | .51  | .061 | 8   | 16  | .08 | 1120 | .01 | 8   | .96  | .01 | .14 | 1   | 1566  |
| L38+00N 47+75E      | 25  | 22  | 34  | 148 | .4  | 28  | 3   | 29   | 2.18 | 18  | 5   | ND  | 2   | 78  | .6   | 5   | 2   | 100 | .11  | .085 | 3   | 13  | .05 | 535  | .01 | 12  | .74  | .02 | .24 | 1   | 1433  |
| L38+00N 48+00E      | 37  | 30  | 58  | 184 | 2.0 | 43  | 3   | 24   | 2.79 | 30  | 5   | ND  | 1   | 185 | 1.2  | 11  | 2   | 174 | .38  | .127 | 5   | 14  | .06 | 305  | .01 | 10  | .81  | .03 | .30 | 1   | 3053  |
| L38+00N 48+25E      | 13  | 14  | 23  | 120 | .7  | 20  | 2   | 58   | 1.33 | 7   | 5   | ND  | 1   | 28  | .3   | 2   | 2   | 102 | .12  | .054 | 5   | 14  | .07 | 410  | .01 | 9   | .89  | .01 | .16 | 1   | 1369  |
| L38+00N 48+50E      | 17  | 22  | 26  | 140 | .1  | 28  | 2   | 19   | 1.57 | 13  | 5   | ND  | 1   | 51  | .2   | 3   | 2   | 117 | .03  | .045 | 2   | 12  | .05 | 364  | .01 | 6   | .80  | .01 | .13 | 1   | 23440 |
| L38+00N 48+75E      | 7   | 16  | 24  | 119 | .4  | 22  | 2   | 18   | 1.36 | 8   | 5   | ND  | 1   | 28  | .3   | 2   | 2   | 79  | .06  | .054 | 6   | 15  | .06 | 524  | .01 | 6   | .95  | .01 | .19 | 1   | 1667  |
| L38+00N 49+00E      | 10  | 25  | 37  | 194 | .4  | 35  | 4   | 34   | 2.47 | 15  | 5   | ND  | 2   | 65  | .3   | 3   | 2   | 86  | .05  | .067 | 5   | 12  | .06 | 384  | .01 | 6   | .83  | .02 | .18 | 1   | 1411  |
| L38+00N 49+25E      | 8   | 22  | 33  | 171 | .4  | 28  | 3   | 19   | 1.86 | 12  | 5   | ND  | 1   | 47  | .4   | 2   | 2   | 88  | .03  | .062 | 5   | 14  | .06 | 427  | .01 | 6   | .94  | .01 | .17 | 1   | 1399  |
| L38+00N 49+50E      | 7   | 22  | 26  | 183 | .4  | 36  | 4   | 44   | 1.90 | 11  | 5   | ND  | 1   | 29  | .8   | 4   | 2   | 86  | .09  | .072 | 6   | 17  | .05 | 384  | .01 | 6   | .92  | .01 | .15 | 1   | 1303  |
| L38+00N 49+75E      | 6   | 23  | 19  | 212 | .8  | 35  | 4   | 36   | 1.82 | 8   | 5   | ND  | 1   | 18  | .4   | 2   | 2   | 81  | .07  | .079 | 5   | 15  | .07 | 458  | .01 | 5   | 1.11 | .01 | .16 | 1   | 1303  |
| L38+00N 50+00E      | 6   | 28  | 18  | 288 | .8  | 34  | 3   | 44   | 2.02 | 10  | 5   | ND  | 1   | 11  | 1.1  | 2   | 2   | 89  | .10  | .080 | 4   | 17  | .07 | 409  | .01 | 5   | 1.19 | .01 | .14 | 1   | 1361  |
| L38+00N 50+25E      | 14  | 23  | 25  | 96  | .6  | 16  | 2   | 13   | 1.06 | 9   | 5   | ND  | 1   | 55  | .3   | 2   | 2   | 62  | .02  | .043 | 3   | 11  | .03 | 426  | .01 | 7   | .77  | .01 | .12 | 1   | 4100  |
| L38+00N 50+50E      | 10  | 16  | 25  | 107 | .5  | 20  | 3   | 36   | 1.28 | 6   | 5   | ND  | 1   | 35  | .2   | 2   | 2   | 93  | .02  | .031 | 5   | 12  | .05 | 216  | .01 | 7   | .75  | .01 | .11 | 1   | 851   |
| L38+00N 50+75E      | 5   | 28  | 27  | 246 | .3  | 46  | 6   | 61   | 2.71 | 9   | 5   | ND  | 1   | 23  | .7   | 2   | 2   | 113 | .04  | .064 | 7   | 18  | .07 | 227  | .01 | 7   | 1.12 | .01 | .12 | 1   | 1085  |
| L38+00N 51+00E      | 7   | 28  | 26  | 163 | 1.0 | 31  | 4   | 30   | 1.98 | 7   | 5   | ND  | 1   | 21  | .4   | 2   | 2   | 101 | .01  | .065 | 6   | 20  | .07 | 303  | .01 | 9   | 1.31 | .01 | .18 | 1   | 1107  |
| L38+00N 51+25E      | 43  | 44  | 40  | 102 | 2.3 | 23  | 2   | 14   | 6.72 | 40  | 5   | ND  | 3   | 163 | 1.8  | 13  | 2   | 160 | .01  | .112 | 3   | 18  | .05 | 37   | .01 | 11  | .80  | .04 | .84 | 1   | 2296  |
| L38+00N 51+50E      | 39  | 36  | 24  | 127 | .7  | 27  | 3   | 27   | 2.50 | 24  | 5   | ND  | 1   | 69  | .6   | 5   | 2   | 203 | .09  | .080 | 7   | 21  | .06 | 565  | .01 | 11  | .93  | .01 | .21 | 1   | 1515  |
| L38+00N 51+75E      | 25  | 27  | 24  | 174 | .5  | 30  | 2   | 17   | 2.62 | 20  | 5   | ND  | 1   | 78  | .5   | 9   | 2   | 151 | .02  | .077 | 5   | 17  | .05 | 525  | .01 | 11  | .85  | .01 | .25 | 1   | 1361  |
| L38+00N 52+00E      | 29  | 25  | 17  | 194 | .1  | 40  | 3   | 23   | 1.58 | 14  | 5   | ND  | 1   | 19  | .3   | 5   | 2   | 159 | .01  | .048 | 6   | 19  | .05 | 261  | .01 | 9   | .82  | .01 | .14 | 1   | 1500  |
| L38+00N 52+25E      | 24  | 30  | 22  | 143 | .5  | 32  | 2   | 13   | 1.92 | 15  | 5   | ND  | 1   | 148 | .7   | 3   | 2   | 154 | .03  | .108 | 9   | 20  | .04 | 401  | .01 | 10  | .70  | .01 | .18 | 1   | 877   |
| L38+00N 52+50E      | 23  | 38  | 23  | 198 | .2  | 42  | 2   | 17   | 1.48 | 15  | 5   | ND  | 1   | 72  | 1.2  | 6   | 2   | 157 | .15  | .075 | 7   | 20  | .07 | 394  | .01 | 9   | .78  | .01 | .15 | 1   | 970   |
| L38+00N 52+75E      | 47  | 59  | 30  | 278 | .2  | 58  | 3   | 24   | 2.35 | 29  | 5   | ND  | 1   | 61  | 1.0  | 7   | 2   | 223 | .02  | .063 | 9   | 22  | .06 | 336  | .01 | 7   | .90  | .01 | .15 | 1   | 851   |
| L38+00N 53+00E      | 21  | 16  | 11  | 115 | .3  | 23  | 2   | 25   | .98  | 10  | 5   | ND  | 1   | 12  | .2   | 2   | 2   | 114 | .03  | .028 | 15  | 19  | .04 | 115  | .01 | 9   | .59  | .01 | .07 | 1   | 675   |
| STANDARD C/CB-1200  | 18  | 60  | 38  | 132 | 7.6 | 75  | 31  | 1060 | 3.96 | 41  | 18  | 8   | 39  | 52  | 18.8 | 15  | 22  | 57  | .49  | .084 | 39  | 60  | .93 | 183  | .08 | 34  | 1.94 | .08 | .17 | 10  | 2136  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.

AA

SEEP GRID

## GEOCHEMICAL ANALYSIS CERTIFICATE

Teck Exploration (BC) PROJECT 1715 File # 92-2640 Page 1

350 - 272 Victoria St., Kamloops BC V2C 2A2 Submitted by: RANDY FARMER

AA

| SAMPLE#            | Mo  | Cu  | Pb  | Zn  | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm   |
| L70+00N 55+00E     | 36  | 24  | 35  | 308 | .7  | 54  | 6   | 44   | 1.75 | 13  | 5   | ND  | 9   | 8   | .3   | 6   | 2   | 224 | .02 | .025 | 7   | 15  | .04 | 143  | .01 | 5  | .63  | .01 | .07 | 2   | 1358  |
| L70+00N 55+25E     | 41  | 27  | 39  | 360 | .4  | 67  | 6   | 41   | 1.99 | 14  | 5   | ND  | 2   | 13  | .2   | 8   | 2   | 246 | .03 | .030 | 6   | 13  | .04 | 182  | .01 | 6  | .63  | .01 | .08 | 1   | 1377  |
| L70+00N 55+50E     | 27  | 18  | 22  | 207 | .3  | 38  | 3   | 33   | 1.22 | 12  | 5   | ND  | 1   | 7   | .5   | 6   | 2   | 158 | .01 | .017 | 7   | 12  | .04 | 125  | .01 | 4  | .51  | .01 | .06 | 1   | 1141  |
| L70+00N 55+75E     | 27  | 18  | 23  | 204 | .4  | 33  | 4   | 50   | 1.33 | 7   | 5   | ND  | 1   | 10  | .8   | 5   | 2   | 148 | .11 | .025 | 9   | 12  | .04 | 278  | .01 | 8  | .48  | .01 | .06 | 1   | 1281  |
| L70+00N 56+00E     | 21  | 21  | 28  | 194 | .4  | 34  | 3   | 37   | .91  | 6   | 5   | ND  | 1   | 18  | 3.3  | 3   | 2   | 160 | .17 | .019 | 7   | 15  | .04 | 675  | .01 | 3  | .48  | .01 | .07 | 1   | 1723  |
| L70+00N 56+25E     | 10  | 19  | 10  | 105 | .1  | 19  | 2   | 18   | .45  | 2   | 5   | ND  | 1   | 25  | 3.4  | 2   | 2   | 108 | .50 | .011 | 13  | 18  | .03 | 467  | .01 | 6  | .36  | .01 | .04 | 1   | 1250  |
| L70+00N 56+50E     | 18  | 17  | 22  | 264 | .3  | 35  | 3   | 27   | 1.09 | 7   | 5   | ND  | 1   | 37  | 3.1  | 3   | 2   | 171 | .21 | .029 | 6   | 13  | .06 | 1201 | .01 | 7  | .55  | .01 | .12 | 1   | 16630 |
| L70+00N 56+75E     | 25  | 19  | 26  | 219 | .6  | 41  | 5   | 33   | 1.59 | 8   | 5   | ND  | 1   | 30  | .5   | 5   | 2   | 157 | .03 | .032 | 5   | 12  | .04 | 814  | .01 | 7  | .54  | .01 | .10 | 1   | 5190  |
| L70+00N 57+00E     | 27  | 17  | 15  | 193 | .1  | 38  | 3   | 24   | 1.07 | 6   | 5   | ND  | 1   | 9   | .3   | 4   | 2   | 191 | .05 | .018 | 6   | 12  | .04 | 167  | .01 | 10 | .43  | .01 | .07 | 1   | 1092  |
| L70+00N 57+25E     | 23  | 14  | 20  | 153 | .1  | 29  | 3   | 20   | .97  | 5   | 5   | ND  | 1   | 12  | .2   | 2   | 2   | 176 | .01 | .014 | 4   | 11  | .04 | 204  | .01 | 7  | .56  | .01 | .07 | 1   | 1068  |
| L70+00N 57+50E     | 32  | 14  | 26  | 224 | .3  | 48  | 3   | 27   | 1.31 | 11  | 5   | ND  | 1   | 15  | .4   | 5   | 2   | 236 | .01 | .022 | 3   | 12  | .04 | 182  | .01 | 5  | .55  | .01 | .08 | 1   | 1036  |
| L70+00N 57+75E     | 29  | 35  | 30  | 225 | .2  | 51  | 4   | 19   | 1.30 | 12  | 5   | ND  | 1   | 29  | .5   | 7   | 2   | 229 | .03 | .026 | 3   | 14  | .04 | 621  | .01 | 13 | .61  | .01 | .11 | 1   | 1806  |
| L70+00N 58+00E     | 25  | 19  | 32  | 206 | .2  | 34  | 4   | 23   | 1.45 | 10  | 5   | ND  | 1   | 28  | .2   | 5   | 2   | 184 | .03 | .023 | 2   | 10  | .04 | 246  | .01 | 10 | .53  | .01 | .11 | 1   | 1459  |
| L70+00N 58+25E     | 23  | 14  | 18  | 184 | .2  | 34  | 4   | 43   | 1.51 | 7   | 5   | ND  | 2   | 9   | .2   | 3   | 2   | 194 | .01 | .017 | 9   | 13  | .04 | 144  | .01 | 3  | .64  | .01 | .06 | 1   | 1048  |
| L70+00N 58+50E     | 47  | 43  | 47  | 300 | .4  | 56  | 5   | 38   | 2.92 | 25  | 5   | ND  | 4   | 18  | .2   | 9   | 2   | 363 | .02 | .054 | 5   | 26  | .08 | 238  | .01 | 7  | 1.15 | .01 | .10 | 1   | 1550  |
| L70+00N 58+75E     | 31  | 36  | 37  | 323 | .3  | 59  | 6   | 27   | 2.31 | 21  | 5   | ND  | 2   | 40  | 1.4  | 8   | 2   | 171 | .02 | .061 | 2   | 12  | .04 | 926  | .01 | 8  | .55  | .01 | .11 | 1   | 5855  |
| L70+00N 59+00E     | 28  | 31  | 36  | 228 | .3  | 41  | 4   | 18   | 1.72 | 15  | 5   | ND  | 2   | 34  | .4   | 6   | 3   | 149 | .01 | .046 | 2   | 12  | .03 | 833  | .01 | 6  | .51  | .01 | .11 | 1   | 4037  |
| L70+00N 59+25E     | 58  | 60  | 51  | 526 | .4  | 110 | 11  | 132  | 3.62 | 30  | 6   | ND  | 3   | 55  | 1.2  | 11  | 2   | 243 | .08 | .141 | 7   | 22  | .10 | 767  | .01 | 9  | .87  | .01 | .13 | 1   | 2848  |
| L70+00N 59+50E     | 49  | 40  | 48  | 336 | .5  | 66  | 6   | 33   | 3.06 | 48  | 5   | ND  | 1   | 56  | 2.0  | 6   | 2   | 225 | .04 | .097 | 4   | 22  | .04 | 711  | .01 | 7  | .67  | .01 | .14 | 1   | 2004  |
| L70+00N 59+75E     | 47  | 47  | 34  | 180 | 1.1 | 65  | 7   | 146  | 2.60 | 43  | 7   | ND  | 2   | 163 | 1.6  | 11  | 2   | 169 | .41 | .057 | 2   | 11  | .09 | 745  | .01 | 11 | .36  | .01 | .17 | 1   | 2950  |
| L70+00N 60+00E     | 57  | 43  | 76  | 224 | 2.4 | 79  | 6   | 24   | 3.07 | 34  | 6   | ND  | 1   | 286 | 3.1  | 11  | 2   | 178 | .46 | .084 | 2   | 8   | .04 | 250  | .01 | 5  | .38  | .02 | .27 | 1   | 2702  |
| L70+00N 60+25E     | 30  | 28  | 34  | 327 | 1.0 | 57  | 5   | 35   | 2.21 | 20  | 5   | ND  | 1   | 55  | 1.6  | 6   | 2   | 152 | .06 | .059 | 2   | 10  | .04 | 679  | .01 | 9  | .45  | .01 | .15 | 1   | 2051  |
| L70+00N 60+50E     | 32  | 49  | 32  | 420 | .5  | 69  | 6   | 52   | 2.24 | 27  | 5   | ND  | 1   | 49  | 1.6  | 7   | 2   | 183 | .14 | .064 | 2   | 11  | .05 | 766  | .01 | 9  | .47  | .01 | .14 | 1   | 2598  |
| L70+00N 60+75E     | 38  | 22  | 28  | 271 | .2  | 58  | 5   | 29   | 1.63 | 13  | 5   | ND  | 1   | 26  | .9   | 6   | 2   | 236 | .04 | .035 | 4   | 13  | .04 | 220  | .01 | 7  | .56  | .01 | .09 | 1   | 899   |
| L70+00N 61+00E     | 63  | 59  | 39  | 618 | .3  | 150 | 8   | 70   | 2.41 | 32  | 5   | ND  | 2   | 40  | 3.6  | 8   | 3   | 438 | .16 | .102 | 6   | 23  | .07 | 801  | .01 | 12 | .82  | .01 | .13 | 1   | 2252  |
| L70+00N 61+25E     | 28  | 20  | 34  | 199 | .6  | 31  | 4   | 24   | 1.77 | 13  | 5   | ND  | 1   | 31  | .8   | 4   | 2   | 206 | .04 | .040 | 4   | 14  | .06 | 866  | .01 | 13 | .86  | .01 | .13 | 1   | 1925  |
| L70+00N 61+50E     | 30  | 24  | 34  | 248 | .3  | 46  | 5   | 34   | 2.59 | 26  | 5   | ND  | 2   | 54  | .7   | 5   | 3   | 235 | .03 | .087 | 2   | 17  | .06 | 628  | .01 | 6  | 1.02 | .01 | .15 | 1   | 1655  |
| L70+00N 61+75E     | 19  | 12  | 35  | 150 | .2  | 25  | 5   | 61   | 1.88 | 8   | 5   | ND  | 2   | 22  | 2.5  | 4   | 2   | 165 | .04 | .028 | 7   | 14  | .06 | 340  | .02 | 8  | .73  | .01 | .11 | 1   | 1132  |
| L70+00N 62+00E     | 22  | 16  | 20  | 106 | .2  | 18  | 3   | 23   | 1.35 | 8   | 5   | ND  | 1   | 16  | 1.0  | 2   | 3   | 90  | .09 | .030 | 3   | 11  | .05 | 272  | .01 | 13 | .77  | .01 | .12 | 1   | 914   |
| L70+00N 62+25E     | 53  | 19  | 22  | 283 | .1  | 58  | 4   | 22   | 1.47 | 14  | 5   | ND  | 1   | 32  | .5   | 12  | 3   | 229 | .02 | .027 | 3   | 9   | .03 | 173  | .01 | 9  | .48  | .01 | .09 | 1   | 828   |
| L70+00N 62+50E     | 49  | 24  | 15  | 358 | .1  | 86  | 4   | 24   | 1.45 | 15  | 6   | ND  | 1   | 21  | 1.4  | 33  | 2   | 202 | .08 | .029 | 3   | 11  | .04 | 206  | .01 | 9  | .40  | .01 | .09 | 1   | 948   |
| L70+00N 62+75E     | 68  | 27  | 13  | 415 | .3  | 105 | 7   | 62   | 1.64 | 20  | 5   | ND  | 3   | 9   | 1.3  | 23  | 2   | 314 | .05 | .021 | 5   | 11  | .05 | 57   | .01 | 9  | .35  | .01 | .04 | 1   | 610   |
| L70+00N 63+00E     | 101 | 30  | 19  | 648 | 1.1 | 194 | 7   | 30   | 1.81 | 30  | 5   | ND  | 1   | 12  | 5.1  | 18  | 2   | 897 | .14 | .029 | 5   | 36  | .08 | 194  | .01 | 12 | .90  | .01 | .12 | 1   | 797   |
| RE L70+00N 62+25E  | 58  | 19  | 25  | 311 | .1  | 63  | 4   | 21   | 1.53 | 18  | 5   | ND  | 1   | 32  | .9   | 14  | 2   | 261 | .02 | .027 | 3   | 11  | .04 | 166  | .01 | 10 | .49  | .01 | .09 | 1   | 829   |
| L70+00N 63+25E     | 47  | 16  | 17  | 152 | .1  | 40  | 2   | 17   | 1.15 | 7   | 5   | ND  | 1   | 41  | 1.0  | 5   | 3   | 138 | .03 | .024 | 4   | 10  | .04 | 190  | .01 | 15 | .51  | .01 | .10 | 1   | 786   |
| L70+00N 63+50E     | 66  | 26  | 28  | 630 | .4  | 131 | 5   | 40   | 1.61 | 30  | 5   | ND  | 1   | 7   | 3.7  | 13  | 2   | 487 | .07 | .031 | 6   | 28  | .07 | 96   | .01 | 9  | .61  | .01 | .09 | 1   | 754   |
| L70+00N 63+75E     | 47  | 48  | 31  | 726 | .6  | 170 | 7   | 46   | 2.06 | 22  | 5   | ND  | 2   | 21  | 4.7  | 10  | 6   | 422 | .59 | .191 | 10  | 73  | .11 | 189  | .01 | 11 | 1.03 | .01 | .13 | 1   | 788   |
| STANDARD C/CB-1200 | 20  | 60  | 41  | 138 | 7.4 | 74  | 32  | 1067 | 3.96 | 42  | 22  | 7   | 40  | 53  | 19.1 | 14  | 20  | 61  | .50 | .086 | 38  | 61  | .94 | 183  | .08 | 33 | 2.03 | .07 | .14 | 10  | 2293  |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: SOIL BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP.  
 Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 18 1992 DATE REPORT MAILED: Aug 24/92 SIGNED BY: C. Leong, J. Wang; CERTIFIED B.C. ASSAYERS



## Teck Exploration (BC) PROJECT 1715 FILE # 92-2640

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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*  |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm  |
| L70+00N 64+00E     | 48  | 55  | 39  | 1080 | 2.1 | 171 | 9   | 174  | 2.12 | 22  | 5   | ND  | 5   | 44  | 9.9  | 11  | 2   | 283 | 1.12 | .333 | 27  | 76  | .20 | 423  | .01 | 14  | 1.36 | .01 | .14 | 2   | 1051 |
| L70+00N 64+25E     | 62  | 37  | 28  | 857  | .5  | 159 | 8   | 116  | 2.11 | 24  | 5   | ND  | 2   | 23  | 11.1 | 13  | 2   | 300 | .59  | .078 | 12  | 33  | .12 | 283  | .01 | 10  | 1.01 | .01 | .11 | 2   | 990  |
| L70+00N 64+50E     | 67  | 36  | 18  | 549  | .2  | 125 | 5   | 45   | 2.01 | 23  | 5   | ND  | 1   | 11  | 4.4  | 13  | 2   | 253 | .14  | .045 | 10  | 23  | .05 | 184  | .01 | 9   | .66  | .01 | .11 | 1   | 928  |
| L70+00N 64+75E     | 47  | 57  | 36  | 349  | .3  | 97  | 9   | 85   | 3.43 | 25  | 5   | ND  | 2   | 28  | 2.2  | 2   | 2   | 99  | .10  | .071 | 5   | 17  | .05 | 184  | .01 | 13  | .60  | .01 | .18 | 1   | 917  |
| L68+00N 55+00E     | 43  | 59  | 14  | 168  | .2  | 74  | 11  | 123  | 4.74 | 21  | 5   | ND  | 1   | 8   | .5   | 2   | 2   | 79  | .05  | .050 | 3   | 12  | .06 | 270  | .01 | 12  | .90  | .01 | .10 | 1   | 3181 |
| L68+00N 55+25E     | 51  | 47  | 42  | 281  | .9  | 110 | 22  | 134  | 5.27 | 14  | 5   | ND  | 3   | 41  | .2   | 3   | 2   | 56  | .01  | .045 | 3   | 14  | .05 | 496  | .01 | 12  | .91  | .01 | .17 | 1   | 3861 |
| L68+00N 55+50E     | 38  | 28  | 14  | 271  | .2  | 50  | 6   | 49   | 2.44 | 16  | 5   | ND  | 1   | 6   | .3   | 4   | 2   | 154 | .03  | .030 | 5   | 10  | .04 | 158  | .01 | 12  | .62  | .01 | .08 | 1   | 1602 |
| L68+00N 55+75E     | 41  | 22  | 21  | 178  | .2  | 31  | 3   | 33   | 1.45 | 13  | 5   | ND  | 1   | 15  | .6   | 4   | 2   | 124 | .13  | .022 | 5   | 8   | .04 | 334  | .01 | 11  | .48  | .01 | .08 | 1   | 1719 |
| L68+00N 56+00E     | 139 | 106 | 88  | 457  | .5  | 63  | 3   | 26   | 2.92 | 35  | 5   | ND  | 2   | 19  | 8.6  | 44  | 2   | 457 | .17  | .055 | 9   | 27  | .03 | 813  | .01 | 12  | .53  | .01 | .09 | 1   | 1511 |
| L68+00N 56+25E     | 68  | 24  | 107 | 378  | .1  | 66  | 3   | 22   | 1.77 | 15  | 5   | ND  | 1   | 18  | .5   | 10  | 2   | 258 | .05  | .028 | 5   | 15  | .04 | 160  | .01 | 10  | .63  | .01 | .05 | 1   | 1068 |
| L68+00N 56+50E     | 57  | 27  | 105 | 356  | .1  | 69  | 4   | 25   | 1.71 | 15  | 5   | ND  | 1   | 18  | .7   | 11  | 2   | 237 | .01  | .027 | 6   | 14  | .03 | 131  | .01 | 9   | .54  | .01 | .08 | 1   | 1095 |
| L68+00N 56+75E     | 49  | 28  | 72  | 367  | .1  | 69  | 3   | 29   | 1.66 | 18  | 5   | ND  | 1   | 10  | .5   | 12  | 2   | 337 | .01  | .023 | 6   | 15  | .04 | 138  | .01 | 6   | .59  | .01 | .07 | 1   | 1009 |
| L68+00N 57+00E     | 43  | 18  | 37  | 294  | .1  | 56  | 2   | 22   | 1.23 | 15  | 5   | ND  | 1   | 7   | .3   | 11  | 3   | 428 | .01  | .018 | 9   | 20  | .06 | 161  | .01 | 5   | .82  | .01 | .05 | 1   | 974  |
| L68+00N 57+25E     | 63  | 17  | 17  | 235  | .3  | 83  | 3   | 58   | .94  | 22  | 5   | ND  | 4   | 5   | 1.4  | 11  | 2   | 457 | .03  | .020 | 7   | 30  | .09 | 277  | .01 | 9   | .90  | .01 | .10 | 1   | 1246 |
| L68+00N 57+50E     | 22  | 11  | 11  | 156  | .2  | 29  | 1   | 12   | .85  | 7   | 5   | ND  | 1   | 7   | .3   | 5   | 2   | 178 | .01  | .017 | 8   | 12  | .04 | 185  | .01 | 8   | .66  | .01 | .07 | 1   | 1111 |
| L68+00N 57+75E     | 19  | 12  | 7   | 119  | .1  | 20  | 1   | 12   | .81  | 4   | 5   | ND  | 1   | 5   | .2   | 2   | 2   | 129 | .01  | .015 | 5   | 8   | .03 | 253  | .01 | 6   | .43  | .01 | .06 | 1   | 1150 |
| L68+00N 58+00E     | 31  | 17  | 24  | 230  | .2  | 43  | 2   | 36   | 1.25 | 9   | 5   | ND  | 1   | 17  | .2   | 5   | 2   | 186 | .04  | .020 | 4   | 11  | .05 | 203  | .01 | 9   | .48  | .01 | .08 | 1   | 1305 |
| L68+00N 58+25E     | 23  | 14  | 19  | 169  | .1  | 35  | 2   | 51   | 1.53 | 7   | 5   | ND  | 2   | 18  | .5   | 4   | 2   | 157 | .04  | .019 | 9   | 12  | .04 | 212  | .04 | 8   | .45  | .01 | .06 | 1   | 1167 |
| L68+00N 58+50E     | 28  | 13  | 9   | 183  | .1  | 44  | 2   | 19   | .93  | 8   | 5   | ND  | 1   | 6   | .8   | 6   | 2   | 169 | .04  | .015 | 4   | 9   | .03 | 134  | .01 | 11  | .35  | .01 | .07 | 1   | 843  |
| L68+00N 58+75E     | 30  | 21  | 21  | 263  | .1  | 47  | 3   | 22   | 1.64 | 15  | 5   | ND  | 1   | 21  | .4   | 8   | 2   | 228 | .02  | .028 | 3   | 10  | .04 | 1008 | .01 | 12  | .52  | .01 | .12 | 1   | 3674 |
| L68+00N 59+00E     | 27  | 18  | 24  | 218  | .1  | 43  | 3   | 32   | 1.67 | 12  | 5   | ND  | 2   | 23  | .5   | 7   | 2   | 196 | .01  | .025 | 6   | 12  | .04 | 244  | .01 | 11  | .69  | .01 | .10 | 1   | 1053 |
| L68+00N 59+25E     | 33  | 38  | 52  | 521  | .3  | 80  | 9   | 151  | 2.99 | 27  | 5   | ND  | 2   | 47  | 1.2  | 9   | 2   | 297 | .09  | .168 | 4   | 22  | .07 | 904  | .01 | 14  | 1.29 | .01 | .15 | 1   | 3772 |
| L68+00N 59+50E     | 62  | 52  | 38  | 670  | 1.5 | 123 | 7   | 75   | 3.62 | 32  | 6   | ND  | 3   | 99  | 3.7  | 17  | 2   | 164 | .30  | .106 | 7   | 15  | .06 | 897  | .01 | 12  | .47  | .01 | .20 | 1   | 3099 |
| L68+00N 59+75E     | 48  | 56  | 37  | 625  | 1.2 | 136 | 13  | 212  | 2.73 | 24  | 5   | ND  | 1   | 61  | 4.4  | 14  | 2   | 156 | .26  | .072 | 6   | 14  | .07 | 1184 | .01 | 10  | .45  | .01 | .14 | 1   | 3687 |
| L68+00N 60+00E     | 57  | 56  | 38  | 534  | .6  | 114 | 16  | 196  | 2.91 | 26  | 5   | ND  | 1   | 58  | 4.2  | 15  | 2   | 172 | .16  | .080 | 7   | 14  | .06 | 966  | .01 | 13  | .45  | .01 | .16 | 1   | 3247 |
| L68+00N 60+25E     | 30  | 38  | 25  | 400  | .3  | 71  | 5   | 62   | 2.30 | 18  | 5   | ND  | 1   | 42  | 2.8  | 6   | 2   | 159 | .10  | .073 | 5   | 11  | .04 | 980  | .01 | 12  | .51  | .01 | .13 | 1   | 2932 |
| L68+00N 60+50E     | 34  | 36  | 24  | 480  | .5  | 88  | 5   | 33   | 2.47 | 19  | 5   | ND  | 1   | 36  | 3.1  | 8   | 2   | 160 | .08  | .064 | 5   | 12  | .04 | 1074 | .01 | 14  | .49  | .01 | .14 | 1   | 3034 |
| L68+00N 60+75E     | 27  | 62  | 25  | 552  | .9  | 154 | 9   | 126  | 1.96 | 18  | 5   | ND  | 2   | 69  | 7.2  | 8   | 2   | 160 | .56  | .080 | 5   | 12  | .09 | 1124 | .01 | 14  | .50  | .01 | .13 | 1   | 5950 |
| L68+00N 61+00E     | 29  | 26  | 23  | 308  | .4  | 59  | 3   | 26   | 1.84 | 16  | 5   | ND  | 1   | 33  | 1.5  | 6   | 2   | 164 | .06  | .047 | 3   | 11  | .04 | 789  | .01 | 11  | .53  | .01 | .15 | 1   | 1999 |
| L68+00N 61+25E     | 72  | 99  | 29  | 4586 | .5  | 787 | 41  | 689  | 5.89 | 62  | 5   | ND  | 2   | 121 | 15.5 | 10  | 2   | 354 | 2.09 | .100 | 5   | 15  | .35 | 571  | .01 | 17  | .51  | .01 | .15 | 2   | 2037 |
| L68+00N 61+50E     | 27  | 20  | 20  | 255  | .3  | 49  | 3   | 31   | 1.54 | 11  | 5   | ND  | 1   | 32  | 2.0  | 5   | 2   | 171 | .08  | .035 | 5   | 12  | .05 | 565  | .01 | 17  | .68  | .01 | .12 | 1   | 1580 |
| L68+00N 61+75E     | 33  | 17  | 18  | 247  | .2  | 48  | 3   | 24   | 1.53 | 9   | 5   | ND  | 1   | 20  | 2.1  | 7   | 2   | 188 | .04  | .032 | 5   | 12  | .05 | 993  | .01 | 14  | .64  | .01 | .11 | 1   | 2580 |
| L68+00N 62+00E     | 53  | 19  | 16  | 470  | .1  | 102 | 3   | 29   | 1.32 | 16  | 5   | ND  | 1   | 18  | 2.1  | 9   | 2   | 370 | .13  | .023 | 2   | 16  | .05 | 400  | .01 | 12  | .47  | .01 | .13 | 1   | 1287 |
| L68+00N 62+25E     | 31  | 19  | 21  | 307  | .6  | 141 | 3   | 66   | 1.51 | 10  | 5   | ND  | 1   | 39  | 6.8  | 7   | 2   | 205 | .70  | .027 | 5   | 16  | .07 | 999  | .01 | 9   | .67  | .01 | .10 | 1   | 2239 |
| RE-L68+00N-61+25E  | 60  | 94  | 27  | 4383 | .6  | 733 | 39  | 643  | 5.70 | 57  | 5   | ND  | 1   | 113 | 15.7 | 8   | 2   | 333 | 1.98 | .095 | 4   | 13  | .34 | 572  | .01 | 14  | .50  | .01 | .14 | 1   | 2086 |
| L68+00N 62+50E     | 81  | 52  | 20  | 1831 | .1  | 427 | 8   | 204  | 1.93 | 23  | 5   | ND  | 1   | 48  | 11.4 | 7   | 2   | 329 | 1.50 | .085 | 11  | 22  | .12 | 336  | .01 | 13  | .59  | .01 | .08 | 1   | 1190 |
| L68+00N 62+75E     | 84  | 32  | 21  | 497  | .1  | 191 | 5   | 39   | 1.81 | 23  | 5   | ND  | 1   | 11  | 2.5  | 8   | 2   | 358 | .21  | .035 | 7   | 22  | .07 | 332  | .01 | 8   | .71  | .01 | .11 | 1   | 1181 |
| STANDARD-C/CB-1200 | 19  | 60  | 37  | 139  | 7.3 | 76  | 32  | 1113 | 4.16 | 42  | 19  | 7   | 37  | 52  | 19.1 | 14  | 19  | 61  | .50  | .089 | 40  | 63  | .91 | 183  | .09 | 35  | 1.95 | .08 | .16 | 11  | 2244 |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.





## Teck Exploration (BC) PROJECT 1715 FILE # 92-2640

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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm   |
| L68+00N 63+00E     | 78  | 30  | 19  | 487  | .1  | 159 | 4   | 38   | 1.74 | 20  | 5   | ND  | 3   | 10  | 4.5  | 7   | 2   | 294 | .22  | .037 | 8   | 22  | .05 | 248  | .01 | 9  | .59  | .01 | .12 | 1   | 1261  |
| L68+00N 63+25E     | 63  | 27  | 11  | 384  | .5  | 123 | 3   | 27   | 1.44 | 13  | 5   | ND  | 1   | 17  | 4.0  | 7   | 2   | 257 | .54  | .023 | 7   | 17  | .04 | 244  | .01 | 8  | .47  | .01 | .07 | 1   | 1011  |
| L68+00N 63+50E     | 66  | 35  | 29  | 616  | .1  | 156 | 5   | 55   | 2.09 | 22  | 5   | ND  | 1   | 26  | 5.3  | 8   | 2   | 392 | .77  | .042 | 14  | 24  | .07 | 263  | .01 | 6  | .89  | .01 | .07 | 1   | 979   |
| L68+00N 63+75E     | 48  | 14  | 14  | 335  | .1  | 87  | 3   | 27   | 1.29 | 11  | 5   | ND  | 1   | 16  | 2.2  | 6   | 2   | 268 | .49  | .026 | 7   | 16  | .05 | 170  | .01 | 6  | .55  | .01 | .06 | 1   | 925   |
| L68+00N 64+00E     | 25  | 10  | 11  | 159  | .1  | 43  | 2   | 20   | .76  | 6   | 5   | ND  | 1   | 13  | 1.8  | 3   | 2   | 140 | .32  | .019 | 10  | 12  | .04 | 170  | .01 | 6  | .45  | .01 | .08 | 1   | 995   |
| L68+00N 64+25E     | 52  | 67  | 16  | 571  | 1.9 | 214 | 7   | 345  | 1.88 | 27  | 5   | ND  | 1   | 70  | 12.8 | 8   | 2   | 306 | 3.24 | .137 | 31  | 39  | .25 | 417  | .01 | 16 | .64  | .01 | .09 | 1   | 1212  |
| L68+00N 64+50E     | 31  | 20  | 11  | 422  | .3  | 74  | 4   | 66   | 1.74 | 12  | 5   | ND  | 1   | 22  | 5.2  | 5   | 2   | 208 | .64  | .033 | 9   | 20  | .10 | 325  | .01 | 6  | .72  | .01 | .08 | 1   | 1223  |
| L68+00N 64+75E     | 63  | 35  | 14  | 620  | 1.8 | 144 | 11  | 199  | 2.22 | 25  | 5   | ND  | 1   | 36  | 7.6  | 14  | 2   | 210 | 1.04 | .061 | 14  | 20  | .07 | 471  | .01 | 9  | .78  | .01 | .14 | 1   | 1395  |
| L68+00N 65+00E     | 29  | 23  | 7   | 185  | .3  | 56  | 3   | 33   | 1.14 | 9   | 5   | ND  | 1   | 29  | 4.1  | 6   | 2   | 123 | .82  | .024 | 7   | 13  | .06 | 385  | .01 | 10 | .51  | .01 | .07 | 1   | 1104  |
| L66+00N 55+00E     | 46  | 19  | 31  | 332  | .2  | 75  | 2   | 15   | 1.14 | 17  | 5   | ND  | 1   | 9   | .5   | 20  | 2   | 265 | .03  | .015 | 10  | 13  | .02 | 129  | .01 | 7  | .32  | .01 | .05 | 1   | 1028  |
| L66+00N 55+25E     | 41  | 27  | 21  | 450  | .4  | 65  | 4   | 41   | 2.50 | 14  | 5   | ND  | 1   | 8   | .7   | 6   | 2   | 293 | .08  | .032 | 8   | 12  | .04 | 116  | .01 | 7  | .72  | .01 | .06 | 1   | 1000  |
| L66+00N 55+50E     | 22  | 13  | 13  | 114  | .2  | 19  | 2   | 30   | 1.11 | 5   | 5   | ND  | 1   | 7   | .6   | 2   | 2   | 83  | .07  | .016 | 6   | 9   | .04 | 261  | .01 | 8  | .67  | .01 | .07 | 1   | 1673  |
| L66+00N 55+75E     | 41  | 30  | 20  | 264  | .2  | 44  | 4   | 54   | 2.66 | 21  | 5   | ND  | 2   | 6   | .5   | 8   | 2   | 191 | .01  | .030 | 5   | 10  | .03 | 149  | .01 | 9  | .63  | .01 | .08 | 1   | 1776  |
| L66+00N 56+00E     | 34  | 24  | 29  | 273  | .1  | 45  | 4   | 36   | 1.64 | 15  | 5   | ND  | 1   | 7   | .6   | 9   | 2   | 161 | .02  | .023 | 7   | 10  | .03 | 127  | .01 | 10 | .54  | .01 | .06 | 1   | 1449  |
| RE L66+00N 57+25E  | 17  | 11  | 7   | 92   | .4  | 18  | 2   | 21   | .75  | 4   | 5   | ND  | 1   | 3   | .6   | 4   | 2   | 85  | .02  | .014 | 10  | 11  | .01 | 113  | .01 | 6  | .24  | .01 | .04 | 1   | 832   |
| L66+00N 56+25E     | 54  | 27  | 24  | 543  | .4  | 113 | 5   | 18   | 1.74 | 18  | 5   | ND  | 1   | 3   | .8   | 19  | 2   | 279 | .01  | .025 | 3   | 16  | .03 | 85   | .01 | 7  | .52  | .01 | .07 | 1   | 963   |
| L66+00N 56+50E     | 26  | 37  | 40  | 339  | 2.3 | 82  | 9   | 215  | 5.00 | 21  | 5   | ND  | 2   | 7   | 1.0  | 7   | 2   | 184 | .03  | .165 | 15  | 33  | .11 | 427  | .01 | 7  | 1.29 | .01 | .07 | 1   | 1840  |
| L66+00N 56+75E     | 160 | 54  | 191 | 3377 | .9  | 504 | 16  | 2912 | 8.61 | 46  | 5   | ND  | 1   | 29  | 36.9 | 9   | 2   | 624 | .16  | .060 | 15  | 47  | .14 | 1699 | .01 | 8  | 2.93 | .01 | .05 | 1   | 3654  |
| L66+00N 57+00E     | 50  | 16  | 31  | 334  | .2  | 63  | 2   | 68   | 1.34 | 12  | 5   | ND  | 1   | 4   | 1.1  | 10  | 2   | 226 | .01  | .019 | 6   | 10  | .03 | 103  | .01 | 6  | .39  | .01 | .04 | 1   | 749   |
| L66+00N 57+25E     | 19  | 11  | 10  | 96   | .5  | 19  | 2   | 24   | .78  | 3   | 5   | ND  | 1   | 3   | .5   | 3   | 2   | 91  | .02  | .014 | 10  | 11  | .02 | 116  | .01 | 7  | .24  | .01 | .04 | 1   | 819   |
| L66+00N 57+50E     | 69  | 26  | 59  | 435  | .5  | 92  | 2   | 31   | 1.54 | 19  | 5   | ND  | 1   | 14  | .7   | 20  | 2   | 477 | .01  | .023 | 8   | 18  | .04 | 241  | .01 | 9  | .59  | .01 | .06 | 1   | 1181  |
| L66+00N 57+75E     | 52  | 15  | 30  | 255  | .5  | 59  | 2   | 23   | 1.18 | 13  | 5   | ND  | 2   | 6   | .4   | 8   | 2   | 241 | .02  | .016 | 11  | 14  | .04 | 164  | .01 | 8  | .54  | .01 | .06 | 1   | 1031  |
| L66+00N 58+00E     | 21  | 14  | 19  | 150  | .2  | 25  | 2   | 14   | .93  | 7   | 5   | ND  | 1   | 28  | .3   | 4   | 2   | 115 | .01  | .016 | 4   | 8   | .03 | 1562 | .01 | 7  | .45  | .01 | .08 | 1   | 47669 |
| L66+00N 58+25E     | 31  | 15  | 54  | 242  | .1  | 46  | 3   | 34   | 2.11 | 14  | 5   | ND  | 1   | 24  | 2.7  | 5   | 2   | 291 | .01  | .036 | 7   | 18  | .06 | 1220 | .01 | 7  | .91  | .01 | .09 | 1   | 9565  |
| L66+00N 58+50E     | 30  | 13  | 31  | 191  | .4  | 37  | 2   | 17   | 1.14 | 10  | 5   | ND  | 2   | 23  | .3   | 8   | 2   | 176 | .08  | .019 | 6   | 10  | .03 | 862  | .01 | 9  | .46  | .01 | .10 | 1   | 3032  |
| L66+00N 58+75E     | 24  | 13  | 25  | 141  | .1  | 28  | 2   | 17   | 1.24 | 7   | 5   | ND  | 1   | 35  | .2   | 3   | 2   | 153 | .03  | .021 | 4   | 10  | .03 | 1009 | .01 | 10 | .53  | .01 | .10 | 1   | 4183  |
| L66+00N 59+00E     | 16  | 13  | 10  | 109  | .8  | 23  | 3   | 18   | .81  | 7   | 9   | ND  | 2   | 7   | .7   | 4   | 2   | 112 | .01  | .021 | 5   | 11  | .03 | 440  | .01 | 11 | .42  | .01 | .10 | 1   | 1346  |
| L66+00N 59+25E     | 36  | 21  | 48  | 368  | .1  | 56  | 3   | 43   | 1.97 | 17  | 5   | ND  | 1   | 25  | .7   | 4   | 2   | 249 | .04  | .039 | 3   | 10  | .03 | 419  | .01 | 11 | .45  | .01 | .08 | 1   | 1336  |
| L66+00N 59+50E     | 37  | 32  | 107 | 458  | .2  | 73  | 4   | 64   | 3.33 | 32  | 5   | ND  | 3   | 45  | 1.9  | 10  | 2   | 274 | .09  | .186 | 5   | 17  | .04 | 981  | .01 | 12 | .72  | .01 | .14 | 1   | 13874 |
| L66+00N 59+75E     | 31  | 23  | 29  | 330  | .6  | 56  | 3   | 22   | 1.80 | 18  | 6   | ND  | 2   | 27  | 1.1  | 9   | 2   | 201 | .02  | .035 | 3   | 11  | .03 | 1236 | .01 | 12 | .50  | .01 | .13 | 1   | 8052  |
| L66+00N 60+00E     | 37  | 82  | 43  | 563  | .7  | 113 | 12  | 180  | 2.67 | 23  | 7   | ND  | 2   | 54  | 5.2  | 11  | 2   | 145 | .23  | .082 | 6   | 12  | .05 | 1197 | .01 | 10 | .47  | .01 | .13 | 1   | 5437  |
| L66+00N 60+25E     | 81  | 117 | 143 | 530  | 1.1 | 110 | 11  | 229  | 4.34 | 58  | 9   | ND  | 2   | 128 | 6.8  | 15  | 2   | 235 | .30  | .112 | 5   | 15  | .05 | 1199 | .01 | 10 | .54  | .01 | .17 | 1   | 3605  |
| L66+00N 60+50E     | 48  | 86  | 79  | 456  | .6  | 94  | 5   | 87   | 4.19 | 36  | 5   | ND  | 2   | 60  | 2.2  | 11  | 2   | 172 | .05  | .115 | 6   | 15  | .03 | 798  | .01 | 11 | .54  | .01 | .13 | 1   | 2511  |
| L66+00N 60+75E     | 101 | 45  | 70  | 108  | 1.3 | 44  | 1   | 29   | 5.51 | 26  | 5   | ND  | 4   | 149 | .5   | 7   | 2   | 60  | .32  | .046 | 2   | 6   | .04 | 73   | .01 | 14 | .22  | .02 | .75 | 1   | 1726  |
| L66+00N 61+00E     | 24  | 20  | 29  | 283  | .2  | 46  | 3   | 30   | 1.81 | 13  | 5   | ND  | 1   | 30  | 3.6  | 6   | 2   | 153 | .05  | .031 | 3   | 9   | .03 | 734  | .01 | 11 | .45  | .01 | .14 | 1   | 1861  |
| L66+00N 61+25E     | 31  | 28  | 46  | 345  | .5  | 57  | 3   | 33   | 2.52 | 23  | 5   | ND  | 2   | 54  | 2.8  | 8   | 2   | 170 | .05  | .083 | 4   | 11  | .04 | 607  | .01 | 11 | .52  | .01 | .15 | 1   | 2135  |
| L66+00N 61+50E     | 37  | 47  | 46  | 426  | .4  | 83  | 4   | 62   | 2.64 | 26  | 5   | ND  | 2   | 47  | 2.6  | 9   | 2   | 224 | .07  | .073 | 4   | 14  | .04 | 738  | .01 | 12 | .59  | .01 | .16 | 1   | 2459  |
| STANDARD C/CB-1200 | 18  | 63  | 39  | 131  | 7.4 | 73  | 32  | 1044 | 3.96 | 41  | 17  | 7   | 38  | 52  | 18.5 | 15  | 20  | 56  | .52  | .085 | 39  | 59  | .92 | 183  | .08 | 34 | 1.93 | .08 | .16 | 10  | 2249  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca  | P    | La  | Cr  | Mg  | Ba   | Ti  | B   | Al   | Na  | K   | W   | Ba*   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|------|-----|-----|------|-----|-----|-----|-------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %   | %    | ppm | ppm | %   | ppm  | %   | ppm | %    | %   | %   | ppm | ppm   |
| L66+00N 61+75E     | 25  | 20  | 27  | 221  | .3  | 36  | 5   | 28   | 1.74 | 15  | 5   | ND  | 7   | 34  | 1.5  | 4   | 2   | 177 | .12 | .041 | 4   | 12  | .05 | 412  | .01 | 15  | .61  | .01 | .13 | 2   | 1304  |
| L66+00N 62+00E     | 29  | 16  | 28  | 233  | .1  | 44  | 4   | 20   | 1.57 | 15  | 5   | ND  | 2   | 34  | 3.2  | 5   | 2   | 187 | .05 | .031 | 3   | 13  | .04 | 360  | .01 | 12  | .45  | .01 | .15 | 1   | 1281  |
| L66+00N 62+25E     | 31  | 19  | 19  | 406  | .4  | 72  | 5   | 50   | 1.87 | 14  | 5   | ND  | 1   | 15  | 5.1  | 4   | 2   | 228 | .09 | .036 | 7   | 20  | .07 | 494  | .01 | 10  | .61  | .01 | .11 | 1   | 1423  |
| L66+00N 62+50E     | 49  | 39  | 30  | 802  | .8  | 189 | 12  | 258  | 2.92 | 37  | 5   | ND  | 2   | 30  | 9.4  | 8   | 2   | 337 | .87 | .052 | 15  | 56  | .26 | 1301 | .01 | 10  | 1.21 | .01 | .11 | 1   | 2578  |
| L66+00N 62+75E     | 68  | 23  | 13  | 420  | .1  | 121 | 5   | 37   | 1.63 | 20  | 5   | ND  | 1   | 9   | 1.5  | 5   | 2   | 367 | .06 | .024 | 4   | 19  | .05 | 167  | .01 | 10  | .48  | .01 | .08 | 1   | 789   |
| L66+00N 63+00E     | 72  | 22  | 13  | 428  | .1  | 127 | 5   | 20   | 1.45 | 18  | 5   | ND  | 1   | 5   | 1.9  | 8   | 2   | 435 | .05 | .022 | 2   | 19  | .04 | 143  | .01 | 13  | .43  | .01 | .09 | 1   | 810   |
| L66+00N 63+25E     | 58  | 18  | 14  | 377  | .1  | 110 | 4   | 22   | 1.35 | 15  | 5   | ND  | 1   | 4   | 1.6  | 8   | 2   | 455 | .04 | .018 | 4   | 19  | .04 | 133  | .01 | 13  | .43  | .01 | .09 | 1   | 799   |
| L66+00N 63+50E     | 72  | 29  | 22  | 444  | .1  | 128 | 7   | 47   | 2.38 | 17  | 5   | ND  | 1   | 11  | 1.2  | 7   | 2   | 264 | .04 | .035 | 5   | 15  | .04 | 100  | .01 | 12  | .47  | .01 | .10 | 1   | 798   |
| L66+00N 63+75E     | 228 | 76  | 83  | 1244 | .1  | 481 | 12  | 59   | 3.80 | 103 | 10  | ND  | 4   | 25  | 1.5  | 29  | 2   | 834 | .11 | .112 | 5   | 57  | .09 | 249  | .01 | 12  | 1.38 | .01 | .17 | 1   | 1039  |
| L66+00N 64+00E     | 82  | 59  | 24  | 502  | .1  | 126 | 8   | 22   | 2.59 | 28  | 5   | ND  | 2   | 9   | .8   | 7   | 2   | 164 | .03 | .032 | 3   | 13  | .04 | 135  | .01 | 13  | .56  | .01 | .11 | 1   | 867   |
| L66+00N 64+25E     | 132 | 35  | 21  | 674  | .1  | 152 | 7   | 24   | 2.42 | 28  | 5   | ND  | 1   | 12  | 1.9  | 23  | 2   | 314 | .04 | .040 | 5   | 14  | .04 | 107  | .01 | 5   | .47  | .01 | .09 | 1   | 826   |
| L66+00N 64+50E     | 66  | 31  | 23  | 418  | .3  | 97  | 8   | 79   | 2.22 | 23  | 5   | ND  | 3   | 16  | 1.9  | 12  | 2   | 209 | .08 | .038 | 5   | 15  | .08 | 138  | .01 | 9   | .48  | .01 | .12 | 1   | 854   |
| L66+00N 64+75E     | 48  | 41  | 21  | 243  | .1  | 56  | 6   | 42   | 2.31 | 14  | 5   | ND  | 2   | 19  | .6   | 5   | 2   | 100 | .08 | .034 | 6   | 11  | .04 | 164  | .01 | 8   | .44  | .01 | .12 | 1   | 884   |
| L66+00N 65+00E     | 42  | 25  | 19  | 170  | .2  | 36  | 4   | 26   | 2.13 | 12  | 5   | ND  | 2   | 11  | .9   | 4   | 2   | 100 | .02 | .028 | 5   | 11  | .04 | 191  | .01 | 7   | .60  | .01 | .13 | 1   | 791   |
| L64+00N 55+00E     | 53  | 26  | 49  | 431  | .4  | 89  | 4   | 28   | 1.62 | 24  | 5   | ND  | 1   | 9   | 1.3  | 30  | 2   | 540 | .05 | .033 | 15  | 25  | .05 | 180  | .01 | 10  | .60  | .01 | .06 | 1   | 813   |
| L64+00N 55+25E     | 53  | 19  | 28  | 362  | .1  | 85  | 4   | 33   | 1.68 | 16  | 5   | ND  | 1   | 7   | .9   | 15  | 2   | 396 | .05 | .019 | 19  | 16  | .04 | 131  | .01 | 7   | .49  | .01 | .05 | 1   | 872   |
| L64+00N 55+50E     | 77  | 26  | 28  | 487  | .3  | 138 | 4   | 23   | 1.68 | 31  | 5   | ND  | 2   | 5   | .7   | 28  | 2   | 611 | .01 | .024 | 31  | 32  | .06 | 154  | .01 | 9   | .65  | .01 | .06 | 1   | 1009  |
| L64+00N 55+75E     | 34  | 23  | 18  | 275  | .1  | 49  | 6   | 63   | 1.82 | 10  | 5   | ND  | 1   | 10  | .6   | 6   | 2   | 179 | .08 | .032 | 8   | 13  | .06 | 168  | .01 | 10  | .47  | .01 | .08 | 1   | 1298  |
| L64+00N 56+00E     | 33  | 48  | 28  | 394  | .6  | 55  | 6   | 73   | 2.76 | 28  | 5   | ND  | 1   | 99  | 3.9  | 3   | 2   | 79  | .23 | .087 | 2   | 10  | .05 | 784  | .01 | 11  | .40  | .01 | .14 | 1   | 2096  |
| L64+00N 56+25E     | 37  | 34  | 39  | 434  | .4  | 76  | 5   | 27   | 2.56 | 29  | 5   | ND  | 1   | 43  | 1.3  | 9   | 2   | 265 | .05 | .058 | 3   | 16  | .05 | 943  | .01 | 11  | .62  | .01 | .13 | 1   | 5568  |
| L64+00N 56+50E     | 31  | 22  | 32  | 360  | .1  | 67  | 5   | 23   | 1.64 | 23  | 5   | ND  | 1   | 27  | .8   | 6   | 2   | 291 | .04 | .033 | 2   | 15  | .06 | 1413 | .01 | 15  | .66  | .01 | .12 | 1   | 12889 |
| L64+00N 56+75E     | 63  | 26  | 34  | 370  | .1  | 97  | 5   | 31   | 1.56 | 21  | 5   | ND  | 1   | 19  | .9   | 14  | 2   | 448 | .04 | .027 | 9   | 20  | .05 | 765  | .01 | 11  | .54  | .01 | .09 | 1   | 2388  |
| L64+00N 57+00E     | 76  | 23  | 31  | 413  | .1  | 117 | 4   | 30   | 1.56 | 17  | 5   | ND  | 1   | 10  | .9   | 16  | 2   | 534 | .03 | .024 | 13  | 24  | .06 | 410  | .01 | 14  | .59  | .01 | .07 | 1   | 1468  |
| L64+00N 57+25E     | 37  | 21  | 31  | 351  | .1  | 61  | 5   | 29   | 1.76 | 14  | 5   | ND  | 1   | 30  | 1.3  | 5   | 2   | 272 | .03 | .023 | 4   | 16  | .06 | 1062 | .01 | 10  | 1.03 | .01 | .10 | 1   | 4412  |
| L64+00N 57+50E     | 43  | 21  | 26  | 272  | .1  | 57  | 4   | 21   | 1.57 | 14  | 5   | ND  | 1   | 22  | .4   | 8   | 2   | 316 | .04 | .030 | 5   | 13  | .04 | 316  | .01 | 14  | .53  | .01 | .09 | 1   | 1158  |
| L64+00N 57+75E     | 27  | 9   | 7   | 139  | .2  | 36  | 2   | 16   | .65  | 7   | 5   | ND  | 2   | 4   | .5   | 7   | 2   | 164 | .02 | .010 | 15  | 9   | .02 | 184  | .01 | 9   | .24  | .01 | .03 | 1   | 812   |
| L64+00N 58+00E     | 97  | 32  | 114 | 585  | .1  | 148 | 6   | 33   | 2.44 | 40  | 5   | ND  | 3   | 20  | .5   | 18  | 2   | 818 | .03 | .089 | 9   | 30  | .06 | 1243 | .01 | 14  | .89  | .01 | .10 | 1   | 4657  |
| L64+00N 58+25E     | 72  | 18  | 71  | 325  | .1  | 64  | 3   | 19   | 1.42 | 16  | 5   | ND  | 2   | 11  | .4   | 13  | 2   | 344 | .02 | .021 | 5   | 16  | .04 | 175  | .01 | 11  | .49  | .01 | .05 | 1   | 847   |
| L64+00N 58+50E     | 67  | 20  | 22  | 225  | .7  | 42  | 3   | 22   | 1.06 | 9   | 5   | ND  | 1   | 5   | 2.3  | 12  | 2   | 212 | .07 | .017 | 8   | 18  | .03 | 158  | .01 | 13  | .32  | .01 | .04 | 1   | 899   |
| RE L64+00N 57+50E  | 46  | 21  | 20  | 287  | .1  | 59  | 4   | 24   | 1.60 | 16  | 5   | ND  | 1   | 22  | .7   | 9   | 2   | 332 | .04 | .030 | 5   | 15  | .04 | 328  | .01 | 15  | .56  | .01 | .10 | 1   | 1077  |
| L64+00N 58+75E     | 24  | 12  | 12  | 179  | .7  | 40  | 3   | 26   | 1.01 | 8   | 5   | ND  | 1   | 5   | .5   | 6   | 2   | 189 | .03 | .017 | 10  | 12  | .03 | 159  | .01 | 10  | .40  | .01 | .04 | 1   | 789   |
| L64+00N 59+00E     | 34  | 19  | 17  | 262  | .5  | 47  | 3   | 19   | 1.09 | 7   | 5   | ND  | 1   | 3   | .3   | 10  | 2   | 211 | .01 | .020 | 5   | 12  | .03 | 91   | .01 | 8   | .36  | .01 | .05 | 1   | 840   |
| L64+00N 59+25E     | 20  | 11  | 11  | 190  | 1.1 | 38  | 3   | 22   | 1.00 | 7   | 5   | ND  | 1   | 4   | .7   | 7   | 2   | 125 | .02 | .014 | 6   | 13  | .03 | 146  | .01 | 9   | .42  | .01 | .04 | 1   | 868   |
| L64+00N 59+50E     | 37  | 24  | 22  | 252  | .1  | 48  | 6   | 37   | 1.79 | 12  | 5   | ND  | 1   | 11  | .5   | 6   | 2   | 169 | .02 | .025 | 6   | 13  | .04 | 190  | .01 | 12  | .57  | .01 | .07 | 1   | 1439  |
| L64+00N 59+75E     | 23  | 14  | 14  | 117  | .4  | 19  | 3   | 21   | 1.07 | 6   | 5   | ND  | 1   | 17  | .6   | 3   | 2   | 85  | .02 | .018 | 6   | 10  | .03 | 198  | .01 | 13  | .56  | .01 | .08 | 1   | 1339  |
| L64+00N 60+00E     | 22  | 18  | 14  | 148  | .4  | 26  | 4   | 43   | 1.46 | 7   | 5   | ND  | 1   | 7   | .3   | 4   | 2   | 126 | .02 | .017 | 7   | 10  | .04 | 158  | .01 | 10  | .53  | .01 | .06 | 1   | 1992  |
| L64+00N 60+25E     | 38  | 16  | 59  | 182  | .5  | 32  | 6   | 69   | 2.25 | 13  | 5   | ND  | 1   | 10  | 2.0  | 5   | 2   | 97  | .04 | .031 | 6   | 12  | .04 | 370  | .01 | 13  | .61  | .01 | .10 | 1   | 2373  |
| STANDARD C/CB-1200 | 20  | 60  | 43  | 138  | 7.3 | 73  | 32  | 1074 | 3.96 | 42  | 20  | 7   | 39  | 53  | 19.3 | 15  | 21  | 60  | .50 | .086 | 39  | 60  | .94 | 184  | .09 | 35  | 1.93 | .07 | .14 | 11  | 2244  |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V    | Ca   | P    | La  | Cr  | Mg  | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*  |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|------|------|------|-----|-----|-----|------|-----|----|------|-----|-----|-----|------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm  | %    | %    | ppm | ppm | %   | ppm  | %   | %  | %    | %   | %   | ppm | ppm  |
| L64+00N 60+50E     | 70  | 84  | 51  | 554  | 1.4 | 76  | 11  | 214  | 6.86 | 62  | 5   | ND  | 9   | 104 | 5.1  | 11  | 2   | 196  | .22  | .243 | 3   | 19  | .05 | 785  | .01 | 11 | .62  | .01 | .15 | 1   | 3416 |
| L64+00N 60+75E     | 76  | 129 | 45  | 535  | 1.4 | 102 | 13  | 265  | 5.49 | 46  | 6   | ND  | 7   | 104 | 7.2  | 12  | 2   | 146  | .44  | .158 | 4   | 19  | .09 | 702  | .01 | 11 | .93  | .01 | .20 | 1   | 2365 |
| L64+00N 61+00E     | 35  | 32  | 37  | 295  | .4  | 55  | 6   | 45   | 2.06 | 25  | 5   | ND  | 3   | 45  | 2.4  | 8   | 3   | 185  | .05  | .048 | 4   | 13  | .04 | 436  | .01 | 14 | .51  | .01 | .14 | 1   | 1459 |
| RE-L64+00N 62+25E  | 20  | 7   | 10  | 136  | .1  | 29  | 2   | 26   | .88  | 5   | 5   | ND  | 1   | 10  | 1.0  | 4   | 2   | 276  | .07  | .014 | 6   | 15  | .04 | 271  | .01 | 11 | .44  | .01 | .11 | 1   | 969  |
| L64+00N 61+25E     | 39  | 35  | 46  | 374  | .5  | 69  | 4   | 35   | 2.34 | 25  | 5   | ND  | 1   | 69  | 1.5  | 9   | 2   | 225  | .05  | .060 | 2   | 14  | .04 | 723  | .01 | 11 | .56  | .01 | .16 | 1   | 3018 |
| L64+00N 61+50E     | 29  | 24  | 23  | 275  | .4  | 46  | 4   | 55   | 1.90 | 13  | 5   | ND  | 1   | 36  | 1.3  | 5   | 2   | 172  | .12  | .047 | 6   | 13  | .05 | 391  | .01 | 15 | .53  | .01 | .13 | 1   | 1319 |
| L64+00N 61+75E     | 23  | 13  | 21  | 181  | .2  | 32  | 3   | 32   | 1.57 | 10  | 5   | ND  | 1   | 21  | 1.6  | 6   | 2   | 189  | .05  | .025 | 7   | 13  | .04 | 333  | .01 | 11 | .50  | .01 | .12 | 1   | 1201 |
| L64+00N 62+00E     | 24  | 11  | 15  | 157  | .1  | 32  | 2   | 18   | .96  | 8   | 5   | ND  | 1   | 11  | 1.1  | 5   | 2   | 281  | .03  | .018 | 4   | 13  | .04 | 244  | .01 | 15 | .48  | .01 | .11 | 1   | 970  |
| L64+00N 62+25E     | 20  | 9   | 7   | 127  | .1  | 28  | 1   | 23   | .83  | 6   | 5   | ND  | 1   | 9   | 1.1  | 3   | 2   | 265  | .07  | .014 | 5   | 13  | .04 | 262  | .01 | 10 | .42  | .01 | .10 | 1   | 1011 |
| L64+00N 62+50E     | 22  | 10  | 13  | 169  | .1  | 34  | 3   | 32   | 1.15 | 6   | 5   | ND  | 1   | 14  | 1.5  | 4   | 2   | 242  | .05  | .018 | 6   | 16  | .04 | 242  | .01 | 12 | .47  | .01 | .10 | 1   | 1082 |
| L64+00N 62+75E     | 27  | 10  | 18  | 194  | .1  | 41  | 2   | 27   | 1.21 | 9   | 5   | ND  | 1   | 15  | 1.9  | 5   | 2   | 268  | .10  | .018 | 5   | 14  | .05 | 222  | .01 | 14 | .43  | .01 | .10 | 1   | 940  |
| L64+00N 63+00E     | 21  | 10  | 17  | 170  | .1  | 33  | 3   | 57   | 1.32 | 6   | 5   | ND  | 2   | 10  | 4.1  | 4   | 2   | 231  | .07  | .015 | 11  | 17  | .05 | 215  | .04 | 8  | .53  | .01 | .09 | 1   | 1000 |
| L64+00N 63+25E     | 50  | 16  | 13  | 249  | .1  | 73  | 2   | 29   | 1.12 | 11  | 5   | ND  | 1   | 7   | 3.2  | 8   | 2   | 397  | .12  | .021 | 7   | 19  | .05 | 131  | .01 | 17 | .45  | .01 | .10 | 1   | 771  |
| L64+00N 63+50E     | 30  | 10  | 6   | 146  | .1  | 48  | 2   | 24   | .85  | 3   | 5   | ND  | 1   | 5   | 1.0  | 4   | 2   | 226  | .06  | .009 | 7   | 12  | .04 | 82   | .01 | 12 | .41  | .01 | .07 | 1   | 831  |
| L64+00N 63+75E     | 42  | 11  | 6   | 158  | .1  | 62  | 2   | 27   | .89  | 6   | 5   | ND  | 1   | 6   | 1.1  | 5   | 2   | 164  | .08  | .013 | 7   | 12  | .04 | 87   | .01 | 12 | .36  | .01 | .08 | 1   | 851  |
| L64+00N 64+00E     | 87  | 29  | 18  | 507  | .1  | 163 | 6   | 54   | 2.23 | 24  | 5   | ND  | 1   | 9   | 2.3  | 10  | 2   | 389  | .06  | .039 | 5   | 20  | .07 | 150  | .01 | 11 | .56  | .01 | .13 | 1   | 1061 |
| L64+00N 64+25E     | 62  | 29  | 19  | 482  | .3  | 111 | 7   | 58   | 2.24 | 21  | 5   | ND  | 1   | 18  | 1.8  | 9   | 2   | 175  | .17  | .045 | 6   | 21  | .07 | 276  | .01 | 11 | .55  | .01 | .12 | 1   | 1563 |
| L64+00N 64+50E     | 202 | 45  | 25  | 1261 | .1  | 397 | 12  | 85   | 3.34 | 75  | 5   | ND  | 2   | 8   | 1.1  | 22  | 2   | 715  | .05  | .037 | 4   | 35  | .06 | 213  | .01 | 15 | .58  | .01 | .14 | 1   | 1070 |
| L64+00N 64+75E     | 94  | 24  | 27  | 191  | .3  | 49  | 6   | 43   | 2.58 | 21  | 5   | ND  | 2   | 18  | .3   | 4   | 3   | 112  | .04  | .029 | 2   | 10  | .04 | 188  | .01 | 12 | .47  | .01 | .19 | 1   | 911  |
| L64+00N 65+00E     | 35  | 15  | 31  | 78   | .3  | 22  | 3   | 23   | 1.71 | 9   | 5   | ND  | 2   | 37  | .3   | 3   | 2   | 78   | .07  | .033 | 4   | 10  | .05 | 274  | .01 | 13 | .46  | .02 | .22 | 1   | 1021 |
| L62+00N 55+00E     | 56  | 16  | 92  | 542  | 1.2 | 111 | 5   | 201  | 3.63 | 14  | 5   | ND  | 2   | 14  | 4.8  | 10  | 3   | 533  | .11  | .022 | 14  | 26  | .06 | 555  | .01 | 2  | .85  | .01 | .06 | 1   | 1322 |
| L62+00N 55+25E     | 75  | 26  | 85  | 499  | .3  | 107 | 5   | 47   | 2.02 | 19  | 5   | ND  | 1   | 34  | 4.0  | 12  | 2   | 276  | .10  | .031 | 8   | 18  | .03 | 371  | .01 | 12 | .43  | .01 | .08 | 1   | 1362 |
| L62+00N 55+50E     | 55  | 23  | 47  | 395  | .3  | 86  | 5   | 34   | 1.72 | 17  | 5   | ND  | 1   | 14  | 1.6  | 17  | 2   | 347  | .03  | .028 | 13  | 18  | .04 | 223  | .01 | 11 | .43  | .01 | .08 | 1   | 1301 |
| L62+00N 55+75E     | 84  | 32  | 41  | 476  | .5  | 131 | 6   | 73   | 1.94 | 22  | 5   | ND  | 3   | 12  | 4.3  | 14  | 3   | 403  | .06  | .030 | 18  | 23  | .06 | 423  | .01 | 13 | .57  | .01 | .08 | 1   | 1695 |
| L62+00N 56+00E     | 81  | 90  | 38  | 5637 | 2.4 | 498 | 5   | 72   | 1.74 | 43  | 5   | ND  | 1   | 80  | 36.8 | 37  | 2   | 799  | 1.59 | .094 | 25  | 44  | .13 | 646  | .01 | 13 | .69  | .01 | .12 | 1   | 2463 |
| L62+00N 56+25E     | 148 | 183 | 30  | 2794 | 3.9 | 393 | 15  | 259  | 1.97 | 111 | 8   | ND  | 1   | 118 | 60.8 | 53  | 5   | 2455 | 1.55 | .185 | 72  | 90  | .12 | 997  | .01 | 27 | 1.01 | .01 | .21 | 1   | 2191 |
| L62+00N 56+50E     | 32  | 22  | 27  | 428  | .3  | 68  | 4   | 44   | 1.19 | 12  | 5   | ND  | 1   | 14  | 4.4  | 10  | 3   | 295  | .15  | .027 | 11  | 20  | .05 | 305  | .01 | 18 | .51  | .01 | .06 | 1   | 1341 |
| L62+00N 56+75E     | 42  | 25  | 27  | 550  | .4  | 92  | 5   | 47   | 1.51 | 14  | 5   | ND  | 1   | 14  | 3.0  | 12  | 4   | 278  | .14  | .030 | 9   | 18  | .06 | 377  | .01 | 15 | .55  | .01 | .07 | 1   | 1654 |
| L62+00N 57+00E     | 59  | 46  | 57  | 725  | .5  | 127 | 8   | 55   | 2.30 | 29  | 5   | ND  | 1   | 33  | 6.1  | 17  | 5   | 364  | .33  | .118 | 12  | 22  | .06 | 1183 | .01 | 16 | .60  | .01 | .12 | 1   | 3341 |
| L62+00N 57+25E     | 52  | 25  | 61  | 413  | .2  | 79  | 5   | 26   | 1.66 | 18  | 5   | ND  | 1   | 12  | 1.2  | 10  | 2   | 269  | .06  | .029 | 5   | 14  | .04 | 387  | .01 | 10 | .46  | .01 | .08 | 1   | 1695 |
| L62+00N 57+50E     | 20  | 10  | 21  | 163  | .2  | 31  | 4   | 40   | 1.34 | 4   | 5   | ND  | 2   | 12  | 4.4  | 4   | 2   | 135  | .14  | .014 | 12  | 11  | .04 | 243  | .02 | 11 | .36  | .01 | .06 | 1   | 1001 |
| L62+00N 57+75E     | 66  | 29  | 40  | 446  | .2  | 91  | 5   | 25   | 2.16 | 28  | 5   | ND  | 1   | 30  | 2.3  | 13  | 7   | 371  | .14  | .028 | 3   | 14  | .04 | 274  | .01 | 18 | .48  | .01 | .11 | 1   | 1193 |
| L62+00N 58+00E     | 195 | 50  | 176 | 719  | .6  | 161 | 7   | 29   | 3.98 | 62  | 5   | ND  | 2   | 42  | 3.2  | 51  | 6   | 1231 | .19  | .046 | 5   | 31  | .05 | 512  | .01 | 13 | .57  | .01 | .14 | 1   | 1807 |
| L62+00N 58+25E     | 52  | 24  | 41  | 347  | .3  | 68  | 5   | 36   | 1.80 | 18  | 5   | ND  | 2   | 14  | 3.2  | 12  | 2   | 313  | .06  | .020 | 9   | 15  | .04 | 353  | .01 | 12 | .49  | .01 | .09 | 1   | 1485 |
| L62+00N 58+50E     | 89  | 20  | 27  | 596  | .1  | 132 | 4   | 48   | 1.75 | 52  | 5   | ND  | 2   | 14  | 7.0  | 37  | 2   | 1102 | .09  | .035 | 37  | 47  | .08 | 392  | .01 | 13 | .67  | .01 | .14 | 1   | 2039 |
| L62+00N 58+75E     | 41  | 20  | 33  | 300  | .4  | 56  | 5   | 29   | 1.81 | 14  | 5   | ND  | 2   | 22  | 1.2  | 13  | 2   | 312  | .11  | .033 | 9   | 14  | .04 | 628  | .01 | 13 | .40  | .01 | .10 | 1   | 1726 |
| L62+00N 59+00E     | 54  | 23  | 16  | 220  | .2  | 39  | 5   | 28   | 2.73 | 22  | 5   | ND  | 2   | 14  | 1.3  | 6   | 2   | 236  | .09  | .033 | 5   | 11  | .04 | 214  | .01 | 13 | .45  | .01 | .10 | 1   | 1083 |
| STANDARD C/CB-1200 | 19  | 56  | 40  | 135  | 7.3 | 70  | 32  | 1045 | 3.96 | 42  | 18  | 7   | 38  | 52  | 18.6 | 15  | 19  | 58   | .52  | .088 | 36  | 60  | .93 | 182  | .08 | 34 | 1.97 | .07 | .14 | 10  | 2275 |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



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| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V    | Ca   | P    | La  | Cr  | Mg   | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba   |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|-----|-----|-----|------|-----|-----|------|------|------|-----|-----|------|------|-----|----|------|-----|-----|-----|------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm  | %    | %    | ppm | ppm | %    | ppm  | %   | %  | %    | %   | %   | ppm | ppm  |
| L62+00N 59+25E     | 138 | 163 | 349 | 3543 | 1.9 | 354 | 13  | 280  | 2.27 | 53  | 5   | 2   | 8   | 69  | 37.9 | 60  | 4   | 341  | 1.69 | .031 | 3   | 15  | .07  | 463  | .01 | 7  | .28  | .01 | .09 | 2   | 1488 |
| L62+00N 59+50E     | 142 | 90  | 200 | 1690 | 1.3 | 181 | 13  | 216  | 5.36 | 62  | 13  | ND  | 3   | 96  | 7.7  | 26  | 2   | 432  | .93  | .073 | 4   | 19  | .11  | 843  | .01 | 6  | .83  | .01 | .14 | 1   | 2150 |
| L62+00N 59+75E     | 58  | 67  | 93  | 849  | .6  | 98  | 10  | 89   | 3.53 | 33  | 5   | ND  | 3   | 46  | 6.2  | 13  | 2   | 226  | .23  | .082 | 4   | 16  | .06  | 1156 | .01 | 8  | .61  | .01 | .16 | 1   | 3090 |
| L62+00N 60+00E     | 43  | 45  | 37  | 538  | .3  | 99  | 6   | 42   | 2.49 | 32  | 5   | ND  | 2   | 53  | 3.2  | 9   | 2   | 330  | .16  | .096 | 3   | 17  | .05  | 908  | .01 | 14 | .54  | .01 | .15 | 1   | 3570 |
| L62+00N 60+25E     | 34  | 59  | 29  | 493  | .6  | 92  | 10  | 77   | 2.27 | 21  | 5   | ND  | 2   | 58  | 7.1  | 8   | 2   | 205  | .24  | .065 | 4   | 16  | .07  | 1220 | .01 | 11 | .68  | .01 | .14 | 1   | 5251 |
| L62+00N 60+50E     | 45  | 66  | 34  | 1028 | .7  | 203 | 13  | 207  | 2.36 | 30  | 5   | ND  | 1   | 92  | 8.4  | 9   | 5   | 211  | 1.84 | .106 | 5   | 14  | .57  | 718  | .01 | 13 | .47  | .01 | .15 | 1   | 4509 |
| L62+00N 60+75E     | 30  | 29  | 25  | 258  | .8  | 46  | 4   | 33   | 1.69 | 13  | 5   | ND  | 1   | 27  | 2.7  | 7   | 4   | 183  | .13  | .050 | 5   | 15  | .07  | 411  | .01 | 18 | .63  | .01 | .14 | 1   | 1138 |
| L62+00N 61+00E     | 39  | 26  | 26  | 357  | .4  | 72  | 5   | 33   | 2.05 | 22  | 5   | ND  | 1   | 38  | 1.5  | 8   | 2   | 228  | .05  | .046 | 2   | 12  | .04  | 552  | .01 | 13 | .41  | .01 | .15 | 1   | 1678 |
| L62+00N 61+25E     | 35  | 22  | 30  | 293  | .5  | 66  | 5   | 68   | 1.72 | 15  | 5   | ND  | 4   | 26  | 3.2  | 6   | 3   | 246  | .17  | .033 | 5   | 16  | .10  | 532  | .01 | 15 | .66  | .01 | .14 | 1   | 1370 |
| L62+00N 61+50E     | 42  | 21  | 23  | 307  | .1  | 72  | 5   | 25   | 1.63 | 19  | 5   | ND  | 1   | 28  | 2.7  | 8   | 3   | 271  | .07  | .025 | 3   | 13  | .04  | 311  | .01 | 11 | .43  | .01 | .12 | 1   | 1065 |
| L62+00N 61+75E     | 26  | 16  | 22  | 212  | .5  | 47  | 4   | 30   | 1.51 | 9   | 5   | ND  | 1   | 25  | 2.1  | 5   | 2   | 208  | .15  | .026 | 6   | 14  | .07  | 455  | .01 | 14 | .62  | .01 | .11 | 1   | 1204 |
| L62+00N 62+00E     | 44  | 34  | 22  | 395  | .6  | 96  | 6   | 46   | 2.31 | 32  | 5   | ND  | 2   | 32  | 2.1  | 9   | 5   | 318  | .18  | .037 | 2   | 15  | .06  | 823  | .01 | 8  | .56  | .01 | .14 | 1   | 2477 |
| L62+00N 62+25E     | 44  | 24  | 21  | 349  | .3  | 79  | 6   | 47   | 2.17 | 26  | 5   | ND  | 1   | 30  | 1.5  | 9   | 2   | 382  | .09  | .046 | 4   | 18  | .06  | 422  | .01 | 10 | .66  | .01 | .13 | 1   | 1163 |
| L62+00N 62+50E     | 54  | 20  | 19  | 364  | .3  | 88  | 5   | 25   | 1.82 | 18  | 5   | ND  | 1   | 18  | 3.6  | 10  | 4   | 326  | .14  | .033 | 4   | 16  | .05  | 241  | .01 | 10 | .45  | .01 | .13 | 1   | 974  |
| L62+00N 62+75E     | 76  | 65  | 28  | 804  | 1.2 | 263 | 10  | 135  | 2.21 | 33  | 5   | ND  | 3   | 64  | 7.6  | 13  | 2   | 662  | 2.02 | .044 | 11  | 31  | .29  | 570  | .01 | 16 | 1.11 | .01 | .12 | 1   | 1317 |
| L62+00N 63+00E     | 186 | 100 | 16  | 1639 | 2.2 | 597 | 15  | 247  | 2.24 | 55  | 5   | ND  | 1   | 135 | 19.7 | 29  | 2   | 812  | 4.85 | .060 | 8   | 26  | .18  | 615  | .01 | 35 | .60  | .01 | .15 | 2   | 1457 |
| L62+00N 63+25E     | 231 | 76  | 19  | 1019 | .7  | 517 | 20  | 371  | 3.10 | 48  | 5   | ND  | 6   | 81  | 5.9  | 11  | 2   | 574  | 2.92 | .067 | 7   | 24  | .95  | 442  | .01 | 20 | .51  | .01 | .16 | 1   | 1442 |
| L62+00N 63+50E     | 113 | 47  | 13  | 742  | .7  | 289 | 11  | 134  | 2.06 | 34  | 5   | ND  | 3   | 27  | 3.8  | 9   | 2   | 515  | .39  | .026 | 7   | 26  | .13  | 395  | .01 | 13 | .68  | .01 | .14 | 1   | 1317 |
| L62+00N 63+75E     | 319 | 306 | 42  | 4716 | 4.2 | 934 | 16  | 273  | 2.57 | 161 | 26  | ND  | 14  | 206 | 43.5 | 82  | 2   | 2950 | 5.20 | .151 | 35  | 87  | 1.00 | 445  | .01 | 29 | .95  | .01 | .27 | 1   | 1834 |
| L62+00N 64+00E     | 190 | 83  | 67  | 1265 | .8  | 444 | 16  | 291  | 3.09 | 60  | 7   | ND  | 7   | 113 | 9.9  | 17  | 2   | 560  | 1.90 | .085 | 10  | 28  | .77  | 473  | .01 | 19 | .50  | .01 | .18 | 1   | 1454 |
| L62+00N 64+25E     | 193 | 76  | 70  | 1001 | .1  | 400 | 11  | 92   | 3.12 | 50  | 5   | ND  | 3   | 18  | 3.7  | 15  | 2   | 812  | .22  | .021 | 7   | 30  | .11  | 303  | .01 | 13 | .63  | .01 | .12 | 1   | 1049 |
| L62+00N 64+50E     | 63  | 32  | 35  | 435  | .7  | 87  | 6   | 40   | 2.42 | 18  | 5   | ND  | 2   | 63  | 4.6  | 8   | 2   | 238  | .24  | .048 | 7   | 14  | .08  | 416  | .01 | 13 | .57  | .01 | .18 | 1   | 1086 |
| L62+00N 64+75E     | 59  | 40  | 34  | 204  | .8  | 71  | 12  | 285  | 4.11 | 24  | 5   | ND  | 2   | 49  | 2.9  | 3   | 3   | 136  | .28  | .071 | 6   | 15  | .11  | 644  | .01 | 11 | .90  | .01 | .22 | 1   | 1288 |
| L62+00N 65+00E     | 52  | 27  | 25  | 180  | .8  | 57  | 8   | 99   | 3.16 | 20  | 5   | ND  | 3   | 33  | 2.4  | 6   | 2   | 142  | .15  | .057 | 4   | 13  | .08  | 325  | .01 | 13 | .62  | .01 | .24 | 1   | 1074 |
| L60+00N 55+00E     | 112 | 17  | 38  | 385  | .1  | 190 | 6   | 28   | 1.90 | 34  | 5   | ND  | 1   | 11  | .8   | 16  | 2   | 251  | .03  | .024 | 6   | 16  | .04  | 154  | .01 | 6  | .42  | .01 | .07 | 1   | 884  |
| L60+00N 55+25E     | 89  | 31  | 16  | 335  | .1  | 89  | 5   | 27   | 1.86 | 14  | 5   | ND  | 1   | 11  | 6.3  | 9   | 2   | 213  | .16  | .023 | 12  | 23  | .03  | 204  | .01 | 12 | .24  | .01 | .05 | 1   | 985  |
| L60+00N 55+50E     | 79  | 33  | 80  | 430  | .2  | 96  | 5   | 28   | 1.95 | 19  | 5   | ND  | 1   | 19  | 3.2  | 16  | 2   | 300  | .06  | .031 | 11  | 16  | .03  | 273  | .01 | 10 | .32  | .01 | .08 | 1   | 1275 |
| RE-L62+00N 64+75E  | 59  | 39  | 35  | 200  | .8  | 74  | 13  | 287  | 4.08 | 23  | 5   | ND  | 2   | 48  | 2.4  | 5   | 2   | 140  | .27  | .070 | 6   | 16  | .11  | 637  | .01 | 13 | .91  | .01 | .22 | 1   | 1313 |
| L60+00N 55+75E     | 51  | 26  | 64  | 772  | 1.0 | 94  | 6   | 414  | 2.62 | 20  | 5   | ND  | 1   | 15  | 15.3 | 12  | 2   | 481  | .11  | .055 | 12  | 29  | .11  | 446  | .02 | 10 | 1.07 | .01 | .09 | 1   | 1426 |
| L60+00N 56+00E     | 88  | 32  | 84  | 445  | .6  | 109 | 5   | 61   | 2.20 | 23  | 5   | ND  | 3   | 16  | 1.9  | 29  | 2   | 527  | .04  | .033 | 17  | 24  | .04  | 169  | .02 | 9  | .46  | .01 | .08 | 1   | 1073 |
| L60+00N 56+25E     | 88  | 21  | 40  | 446  | .1  | 154 | 5   | 38   | 2.01 | 29  | 5   | ND  | 2   | 12  | 3.8  | 14  | 2   | 472  | .07  | .029 | 37  | 23  | .05  | 433  | .01 | 14 | .56  | .01 | .09 | 1   | 1957 |
| L60+00N 56+50E     | 26  | 11  | 20  | 203  | .1  | 37  | 4   | 63   | 1.59 | 9   | 5   | ND  | 2   | 15  | 3.8  | 4   | 2   | 190  | .08  | .020 | 13  | 15  | .05  | 238  | .03 | 14 | .50  | .01 | .09 | 1   | 1046 |
| L60+00N 56+75E     | 43  | 29  | 49  | 249  | .1  | 43  | 4   | 24   | 2.73 | 22  | 5   | ND  | 2   | 20  | .7   | 6   | 2   | 258  | .05  | .057 | 6   | 11  | .04  | 298  | .01 | 10 | .53  | .01 | .14 | 1   | 1628 |
| L60+00N 57+00E     | 27  | 15  | 19  | 178  | .7  | 46  | 4   | 23   | 1.64 | 14  | 5   | ND  | 1   | 7   | 1.6  | 6   | 2   | 176  | .03  | .028 | 7   | 17  | .04  | 220  | .01 | 9  | .59  | .01 | .09 | 1   | 1211 |
| L60+00N 57+25E     | 39  | 22  | 22  | 281  | .1  | 55  | 4   | 19   | 1.58 | 16  | 5   | ND  | 1   | 22  | 1.0  | 8   | 2   | 281  | .02  | .024 | 4   | 12  | .04  | 939  | .01 | 14 | .52  | .01 | .11 | 1   | 2904 |
| L60+00N 57+50E     | 35  | 17  | 20  | 227  | .2  | 46  | 3   | 19   | 1.38 | 10  | 5   | ND  | 1   | 14  | .7   | 7   | 3   | 250  | .03  | .021 | 4   | 12  | .04  | 322  | .01 | 12 | .51  | .01 | .09 | 1   | 1170 |
| L60+00N 57+75E     | 39  | 46  | 43  | 3083 | .5  | 294 | 8   | 131  | 1.80 | 22  | 5   | ND  | 1   | 62  | 14.8 | 10  | 2   | 352  | 1.05 | .050 | 8   | 18  | .13  | 743  | .01 | 13 | .57  | .01 | .11 | 5   | 2311 |
| STANDARD C/CB-1200 | 20  | 58  | 42  | 131  | 7.6 | 75  | 32  | 1056 | 3.96 | 42  | 18  | 7   | 39  | 53  | 18.8 | 15  | 19  | 60   | .50  | .084 | 38  | 60  | .94  | 186  | .08 | 35 | 2.01 | .07 | .14 | 10  | 2262 |

Sample type: SOIL. Samples beginning 'RE' are duplicate samples.



AA ANALYTICAL

## Teck Exploration (BC) PROJECT 1715 FILE # 92-2640

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AA ANALYTICAL

| SAMPLE#            | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn   | Fe    | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca    | P    | La  | Cr  | Mg   | Ba   | Ti  | B  | Al   | Na  | K   | W   | Ba*  |
|--------------------|-----|-----|-----|------|-----|-----|-----|------|-------|-----|-----|-----|-----|-----|------|-----|-----|-----|-------|------|-----|-----|------|------|-----|----|------|-----|-----|-----|------|
|                    | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm  | %     | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %     | %    | ppm | ppm | %    | ppm  | %   | %  | %    | %   | %   | ppm | ppm  |
| L60+00N 58+00E     | 62  | 49  | 77  | 904  | .3  | 122 | 7   | 135  | 2.41  | 23  | 12  | ND  | 4   | 22  | 13.6 | 18  | 2   | 432 | .25   | .077 | 12  | 23  | .04  | 623  | .01 | 13 | .57  | .01 | .13 | 1   | 2411 |
| L60+00N 58+25E     | 36  | 26  | 50  | 395  | .5  | 65  | 3   | 26   | 1.60  | 18  | 8   | ND  | 3   | 28  | 3.6  | 11  | 2   | 236 | .17   | .034 | 5   | 13  | .04  | 973  | .01 | 13 | .45  | .01 | .16 | 1   | 2111 |
| L60+00N 58+50E     | 32  | 17  | 29  | 397  | .2  | 58  | 3   | 35   | 1.41  | 14  | 7   | ND  | 2   | 22  | 3.3  | 7   | 2   | 216 | .22   | .049 | 7   | 12  | .05  | 528  | .01 | 13 | .47  | .01 | .11 | 1   | 1600 |
| L60+00N 58+75E     | 38  | 18  | 19  | 255  | .2  | 51  | 3   | 27   | 1.40  | 12  | 6   | ND  | 2   | 16  | .7   | 9   | 2   | 207 | .03   | .024 | 4   | 9   | .04  | 331  | .01 | 11 | .45  | .01 | .10 | 1   | 1164 |
| L60+00N 59+00E     | 38  | 32  | 29  | 378  | .2  | 74  | 4   | 31   | 2.15  | 21  | 5   | ND  | 2   | 38  | 1.2  | 9   | 2   | 197 | .08   | .070 | 4   | 13  | .04  | 894  | .01 | 11 | .50  | .01 | .15 | 1   | 3490 |
| L60+00N 59+25E     | 32  | 45  | 31  | 658  | .6  | 104 | 6   | 91   | 1.97  | 20  | 5   | ND  | 2   | 59  | 5.6  | 9   | 2   | 178 | .66   | .068 | 5   | 13  | .07  | 1131 | .01 | 9  | .45  | .01 | .13 | 1   | 4692 |
| L60+00N 59+50E     | 57  | 45  | 23  | 785  | .8  | 195 | 7   | 204  | 1.36  | 26  | 12  | 2   | 6   | 116 | 6.0  | 12  | 2   | 307 | 6.59  | .160 | 15  | 20  | 2.82 | 415  | .01 | 19 | .41  | .02 | .17 | 1   | 1909 |
| L60+00N 59+75E     | 45  | 49  | 44  | 2729 | 1.2 | 678 | 67  | 2337 | 10.62 | 16  | 7   | ND  | 1   | 223 | 5.7  | 7   | 2   | 115 | 1.38  | .074 | 6   | 9   | .15  | 371  | .01 | 19 | .34  | .01 | .11 | 1   | 1302 |
| L60+00N 60+00E     | 59  | 58  | 166 | 1130 | 1.2 | 126 | 10  | 308  | 3.07  | 30  | 6   | ND  | 2   | 40  | 11.3 | 15  | 2   | 191 | .50   | .111 | 8   | 15  | .08  | 1091 | .01 | 12 | .47  | .01 | .12 | 1   | 2053 |
| L60+00N 60+25E     | 37  | 43  | 29  | 516  | .6  | 106 | 8   | 204  | 3.01  | 29  | 5   | ND  | 2   | 49  | 3.8  | 10  | 2   | 224 | .60   | .155 | 5   | 15  | .19  | 1053 | .01 | 14 | .58  | .01 | .19 | 1   | 2986 |
| L60+00N 60+50E     | 37  | 31  | 36  | 409  | .5  | 78  | 5   | 126  | 2.72  | 27  | 5   | ND  | 1   | 50  | 1.3  | 9   | 2   | 202 | .13   | .060 | 3   | 11  | .05  | 760  | .01 | 14 | .53  | .01 | .15 | 1   | 1936 |
| L60+00N 60+75E     | 29  | 24  | 27  | 275  | .4  | 47  | 3   | 31   | 1.78  | 17  | 5   | ND  | 2   | 28  | 1.2  | 7   | 2   | 182 | .03   | .042 | 5   | 10  | .05  | 388  | .01 | 12 | .60  | .01 | .14 | 1   | 1106 |
| L60+00N 61+00E     | 21  | 12  | 20  | 157  | .1  | 31  | 2   | 24   | 1.06  | 8   | 5   | ND  | 2   | 26  | 1.6  | 5   | 2   | 131 | .08   | .020 | 6   | 10  | .05  | 176  | .01 | 12 | .47  | .01 | .09 | 1   | 660  |
| L60+00N 61+25E     | 26  | 15  | 12  | 161  | .1  | 35  | 2   | 24   | 1.09  | 9   | 6   | ND  | 2   | 13  | 1.5  | 6   | 2   | 173 | .05   | .021 | 7   | 11  | .04  | 150  | .01 | 16 | .45  | .01 | .09 | 1   | 663  |
| L60+00N 61+50E     | 40  | 21  | 15  | 216  | 1.1 | 56  | 4   | 36   | 1.47  | 14  | 6   | ND  | 2   | 12  | 1.2  | 7   | 2   | 231 | .07   | .022 | 8   | 13  | .04  | 111  | .01 | 14 | .42  | .01 | .09 | 1   | 750  |
| L60+00N 61+75E     | 34  | 25  | 35  | 321  | .1  | 50  | 4   | 36   | 2.01  | 13  | 5   | ND  | 1   | 38  | 3.7  | 5   | 2   | 147 | .32   | .035 | 5   | 10  | .06  | 335  | .01 | 12 | .46  | .01 | .09 | 1   | 960  |
| L60+00N 62+00E     | 50  | 36  | 88  | 612  | .4  | 86  | 5   | 48   | 2.92  | 21  | 7   | ND  | 3   | 48  | 1.9  | 11  | 2   | 157 | .05   | .056 | 7   | 12  | .04  | 220  | .01 | 13 | .42  | .01 | .12 | 1   | 1134 |
| L60+00N 62+25E     | 26  | 25  | 857 | 4672 | 1.3 | 207 | 35  | 775  | 3.47  | 19  | 5   | ND  | 2   | 86  | 25.7 | 13  | 2   | 272 | 3.43  | .634 | 21  | 32  | .17  | 300  | .01 | 20 | 1.56 | .01 | .15 | 1   | 804  |
| L60+00N 62+50E     | 58  | 12  | 17  | 141  | .1  | 28  | 2   | 15   | 1.15  | 10  | 5   | ND  | 1   | 6   | .8   | 2   | 2   | 123 | .11   | .018 | 4   | 8   | .04  | 104  | .01 | 18 | .56  | .01 | .07 | 1   | 745  |
| L60+00N 62+75E     | 31  | 23  | 35  | 343  | .1  | 56  | 4   | 90   | 2.45  | 12  | 5   | ND  | 1   | 7   | 1.0  | 4   | 2   | 148 | .02   | .038 | 7   | 11  | .04  | 80   | .01 | 11 | .55  | .01 | .07 | 1   | 821  |
| L60+00N 63+00E     | 18  | 30  | 51  | 554  | .8  | 63  | 6   | 95   | 2.91  | 18  | 5   | ND  | 2   | 41  | 1.9  | 11  | 2   | 161 | .14   | .062 | 3   | 12  | .07  | 219  | .01 | 15 | .77  | .01 | .17 | 1   | 1119 |
| RE L60+00N 62+00E  | 41  | 38  | 80  | 577  | .1  | 76  | 5   | 43   | 2.74  | 19  | 5   | ND  | 2   | 47  | 2.1  | 7   | 2   | 147 | .04   | .052 | 6   | 11  | .03  | 222  | .01 | 11 | .43  | .01 | .11 | 1   | 1171 |
| L60+00N 63+25E     | 25  | 15  | 18  | 727  | .2  | 61  | 4   | 62   | 1.27  | 11  | 5   | ND  | 2   | 18  | 4.6  | 6   | 2   | 144 | .39   | .021 | 10  | 11  | .06  | 243  | .01 | 8  | .45  | .01 | .08 | 1   | 986  |
| L60+00N 63+50E     | 28  | 26  | 27  | 1362 | .5  | 112 | 9   | 335  | 1.52  | 18  | 5   | ND  | 1   | 42  | 7.3  | 9   | 2   | 315 | 1.39  | .063 | 10  | 22  | .07  | 363  | .01 | 8  | .83  | .01 | .07 | 1   | 914  |
| L60+00N 63+75E     | 44  | 34  | 27  | 1500 | .5  | 158 | 5   | 79   | 1.68  | 21  | 5   | ND  | 2   | 32  | 4.3  | 12  | 2   | 257 | .87   | .042 | 9   | 19  | .08  | 307  | .01 | 11 | .60  | .01 | .09 | 1   | 1195 |
| L60+00N 64+00E     | 54  | 51  | 49  | 1751 | .8  | 258 | 6   | 138  | 1.92  | 24  | 5   | ND  | 2   | 52  | 9.8  | 12  | 2   | 216 | 1.45  | .078 | 9   | 16  | .28  | 375  | .01 | 13 | .45  | .01 | .13 | 1   | 1399 |
| L60+00N 64+25E     | 84  | 62  | 47  | 1805 | .4  | 273 | 7   | 145  | 1.85  | 26  | 5   | ND  | 3   | 70  | 11.6 | 13  | 2   | 233 | 2.24  | .074 | 7   | 14  | .70  | 471  | .01 | 13 | .39  | .01 | .12 | 1   | 1679 |
| L60+00N 64+50E     | 62  | 56  | 52  | 1117 | .5  | 186 | 8   | 146  | 2.07  | 24  | 5   | ND  | 1   | 50  | 9.0  | 11  | 2   | 253 | 1.23  | .074 | 9   | 16  | .33  | 513  | .01 | 10 | .45  | .01 | .11 | 1   | 1707 |
| L60+00N 64+75E     | 66  | 309 | 25  | 2418 | .7  | 577 | 105 | 954  | 8.56  | 14  | 30  | ND  | 12  | 75  | 26.9 | 5   | 3   | 145 | 1.26  | .089 | 10  | 43  | .13  | 407  | .01 | 12 | 2.14 | .01 | .11 | 1   | 1166 |
| L60+00N 65+00E     | 5   | 78  | 2   | 416  | .3  | 266 | 38  | 2160 | 4.47  | 5   | 6   | ND  | 1   | 613 | 6.0  | 2   | 2   | 20  | 12.22 | .024 | 5   | 6   | 6.44 | 588  | .01 | 2  | .61  | .02 | .03 | 1   | 1093 |
| STANDARD C/CB-1200 | 20  | 60  | 39  | 135  | 7.5 | 79  | 32  | 1079 | 3.96  | 42  | 21  | 7   | 39  | 53  | 19.2 | 13  | 21  | 59  | .50   | .087 | 40  | 61  | .90  | 183  | .09 | 35 | 1.94 | .08 | .17 | 11  | 2201 |

Sample description (if any) see duplicate samples

ACME ANALYTICAL LABORATORIES LTD.

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## GEOCHEMICAL ANALYSIS CERTIFICATE



Teck Exploration (BC) PROJECT 1715 File # 92-2723

350 - 272 Victoria St., Kamloops BC V2C 2A2 Submitted by: RANDY FARMER

| SAMPLE#   | Mo  | Cu  | Pb  | Zn   | Ag  | Ni   | Co  | Mn  | Fe   | As  | U   | Au  | Th  | Sr  | Cd   | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg   | Ba   | Ti  | B   | Al  | Na  | K   | W   | Ba*   |
|-----------|-----|-----|-----|------|-----|------|-----|-----|------|-----|-----|-----|-----|-----|------|-----|-----|-----|------|------|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-------|
|           | ppm | ppm | ppm | ppm  | ppm | ppm  | ppm | ppm | %    | ppm | ppm | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | %    | %    | ppm | ppm | %    | ppm  | %   | ppm | %   | %   | %   | ppm | ppm   |
| M45249    | 44  | 71  | 92  | 1637 | 1.2 | 207  | 7   | 157 | 1.86 | 27  | 5   | ND  | 2   | 73  | 15.1 | 17  | 2   | 385 | .82  | .096 | 11  | 23  | .12  | 990  | .01 | 13  | .58 | .01 | .16 | 2   | 5622  |
| M45250    | 63  | 76  | 43  | 8923 | .6  | 1004 | 5   | 88  | 1.66 | 24  | 5   | ND  | 1   | 84  | 39.2 | 8   | 2   | 318 | 2.63 | .102 | 7   | 18  | .37  | 352  | .01 | 15  | .51 | .01 | .11 | 1   | 1119  |
| M45293    | 23  | 32  | 16  | 930  | .5  | 163  | 7   | 186 | 1.33 | 12  | 5   | ND  | 3   | 66  | 7.6  | 7   | 2   | 140 | 4.47 | .126 | 14  | 14  | 1.80 | 415  | .01 | 16  | .40 | .01 | .14 | 1   | 2776  |
| M45301    | 74  | 127 | 27  | 5005 | 1.0 | 897  | 13  | 215 | 2.46 | 42  | 5   | ND  | 2   | 132 | 20.4 | 17  | 2   | 306 | 4.90 | .134 | 10  | 23  | .90  | 416  | .01 | 20  | .51 | .01 | .20 | 1   | 1703  |
| RE M45293 | 26  | 32  | 18  | 908  | .5  | 165  | 7   | 191 | 1.37 | 13  | 5   | ND  | 3   | 68  | 7.4  | 6   | 2   | 145 | 4.59 | .131 | 14  | 14  | 1.83 | 429  | .01 | 16  | .41 | .01 | .14 | 1   | 2247  |
| M45302    | 14  | 38  | 33  | 478  | .6  | 66   | 7   | 117 | 1.97 | 13  | 5   | ND  | 3   | 53  | 3.8  | 5   | 2   | 43  | .43  | .066 | 7   | 9   | .17  | 659  | .01 | 9   | .52 | .01 | .13 | 1   | 33823 |
| M45303    | 8   | 42  | 25  | 273  | .6  | 65   | 8   | 172 | 2.09 | 8   | 5   | ND  | 2   | 71  | 2.4  | 2   | 2   | 41  | .62  | .061 | 5   | 12  | .24  | 941  | .01 | 10  | .70 | .01 | .12 | 1   | 8751  |
| M45304    | 10  | 36  | 24  | 422  | .6  | 70   | 7   | 140 | 1.90 | 12  | 5   | ND  | 3   | 67  | 3.5  | 3   | 2   | 44  | .60  | .061 | 6   | 9   | .20  | 1051 | .01 | 8   | .60 | .01 | .13 | 1   | 21326 |

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 3ML 3-1-2 HCL-HNO3-H2O AT 95 DEG. C FOR ONE HOUR AND IS DILUTED TO 10 ML WITH WATER.  
 THIS LEACH IS PARTIAL FOR MN FE SR CA P LA CR MG BA TI B W AND LIMITED FOR NA K AND AL. AU DETECTION LIMIT BY ICP IS 3 PPM.  
 - SAMPLE TYPE: MOSS MAT BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP.  
 GEOCHEM BA ANALYSIS BY WHOLE ROCK ICP. Samples beginning 'RE' are duplicate samples.

DATE RECEIVED: AUG 22 1992 DATE REPORT MAILED: *Aug 27/92* SIGNED BY: *C. Long* D. TOYE, C. LEONG, J. WANG; CERTIFIED B.C. ASSAYERS



Teck Exploration (BC) PROJECT 1715 FILE # 92-2518

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| SAMPLE#   | Mo  | Cu  | Pb  | Zn   | Ag  | Ni  | Co  | Mn  | Fe   | As  | U   | Au  | Th  | Sr  | Cd  | Sb  | Bi  | V   | Ca   | P    | La  | Cr  | Mg  | Ba  | Ti  | B   | Al  | Na  | K   | W   | Ba*  |
|-----------|-----|-----|-----|------|-----|-----|-----|-----|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
|           | ppm | ppm | ppm | ppm  | ppm | ppm | ppm | ppm | %    | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | ppm | %    | %    | ppm | ppm | %   | ppm | %   | ppm | %   | %   | %   | ppm | ppm  |
| M45211    | 20  | 65  | 29  | 714  | .9  | 334 | 5   | 229 | 2.19 | 21  | 6   | ND  | 1   | 175 | 2.9 | 4   | 2   | 113 | 1.07 | .087 | 3   | 13  | .15 | 269 | .01 | 16  | .50 | .02 | .20 | 1   | 8188 |
| M45212    | 26  | 73  | 37  | 1119 | .9  | 303 | 12  | 393 | 3.62 | 29  | 5   | ND  | 2   | 219 | 8.5 | 4   | 2   | 120 | .85  | .128 | 4   | 17  | .16 | 122 | .01 | 13  | .80 | .03 | .25 | 1   | 9380 |
| M45251    | 37  | 80  | 30  | 775  | .9  | 232 | 12  | 262 | 3.18 | 22  | 7   | ND  | 1   | 137 | 9.4 | 8   | 2   | 159 | .93  | .127 | 4   | 17  | .14 | 460 | .01 | 18  | .77 | .01 | .21 | 1   | 2126 |
| RE M45212 | 26  | 72  | 36  | 1107 | 1.0 | 281 | 13  | 373 | 3.57 | 26  | 7   | ND  | 2   | 208 | 8.4 | 5   | 2   | 120 | .80  | .125 | 4   | 15  | .15 | 148 | .01 | 11  | .78 | .02 | .25 | 1   | 9918 |

Sample type: MOSS MAT. Samples beginning 'RE' are duplicate samples.  
 BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP.

# SILTS AND FE-SEEPS



Teck Exploration (BC) PROJECT 1715 FILE # 92-2518

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| SAMPLE#    | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Ba*<br>ppm |
|------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|------------|
| ST45215    | 75        | 99        | 28        | 1451      | 1.1       | 356       | 22        | 467       | 3.51    | 32        | 9        | ND        | 2         | 117       | 15.1      | 14        | 2         | 263      | 1.05    | 126    | 11        | 21        | .19     | 631       | .01     | 17       | .81     | .01     | .16    | 1        | 3279       |
| ST45216    | 78        | 72        | 20        | 801       | .7        | 255       | 13        | 217       | 2.34    | 25        | 11       | ND        | 2         | 93        | 8.4       | 7         | 2         | 211      | 2.06    | .079   | 9         | 16        | .77     | 687       | .01     | 16       | .46     | .01     | .12    | 1        | 3480       |
| ST45218    | 29        | 59        | 13        | 446       | .7        | 94        | 6         | 159       | 1.48    | 17        | 6        | ND        | 2         | 80        | 6.0       | 5         | 2         | 150      | 1.03    | .067   | 8         | 13        | .33     | 683       | .01     | 14       | .43     | .01     | .12    | 1        | 3732       |
| RE ST45216 | 74        | 69        | 19        | 734       | .6        | 240       | 12        | 206       | 2.17    | 25        | 6        | ND        | 2         | 88        | 7.7       | 6         | 2         | 202      | 1.98    | .075   | 8         | 13        | .75     | 712       | .01     | 17       | .43     | .01     | .12    | 1        | 3443       |

Sample type: SILT. Samples beginning 'RE' are duplicate samples.  
BA\* .2 GM SAMPLE FUSED WITH 1.2 GM LIBO2, ANALYSIS BY ICP.



Teck Exploration (BC) PROJECT 1715 FILE # 92-2641

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| SAMPLE#            | Mo<br>ppm | Cu<br>ppm | Pb<br>ppm | Zn<br>ppm | Ag<br>ppm | Ni<br>ppm | Co<br>ppm | Mn<br>ppm | Fe<br>% | As<br>ppm | U<br>ppm | Au<br>ppm | Th<br>ppm | Sr<br>ppm | Cd<br>ppm | Sb<br>ppm | Bi<br>ppm | V<br>ppm | Ca<br>% | P<br>% | La<br>ppm | Cr<br>ppm | Mg<br>% | Ba<br>ppm | Ti<br>% | B<br>ppm | Al<br>% | Na<br>% | K<br>% | W<br>ppm | Ba*<br>ppm | Hg<br>ppb |
|--------------------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|-----------|---------|-----------|----------|-----------|-----------|-----------|-----------|-----------|-----------|----------|---------|--------|-----------|-----------|---------|-----------|---------|----------|---------|---------|--------|----------|------------|-----------|
| ST45221            | 33        | 53        | 18        | 2072      | .7        | 211       | 17        | 415       | 3.21    | 21        | 5        | ND        | 2         | 59        | 9.5       | 10        | 2         | 126      | .37     | .073   | 12        | 12        | .10     | 521       | .01     | 4        | .92     | .01     | .10    | 2        | 3327       | 80        |
| ST45271            | 254       | 25        | 12        | 2453      | .8        | 718       | 150       | 18716     | 17.19   | 311       | 5        | ND        | 48        | 238       | 9.2       | 5         | 6         | 35       | 1.49    | .190   | 5         | 8         | .08     | 647       | .01     | 2        | .43     | .01     | .06    | 1        | 3100       | 100       |
| RE S45225          | 23        | 18        | 2         | 1002      | .1        | 101       | 40        | 873       | 37.78   | 2         | 5        | ND        | 7         | 28        | 28.3      | 2         | 9         | 5        | .20     | .019   | 2         | 3         | .02     | 61        | .01     | 2        | .41     | .01     | .01    | 1        | 151        | 5         |
| - ST45273          | 47        | 35        | 6         | 4283      | .2        | 389       | 107       | 1793      | 33.34   | 33        | 10       | ND        | 7         | 138       | 8.5       | 2         | 6         | 18       | .74     | .055   | 2         | 4         | .06     | 332       | .01     | 2        | .28     | .01     | .03    | 1        | 1476       | 60        |
| - S45225           | 22        | 18        | 2         | 1021      | .1        | 101       | 41        | 781       | 38.28   | 2         | 5        | ND        | 8         | 29        | 26.8      | 2         | 9         | 5        | .20     | .019   | 2         | 3         | .02     | 76        | .01     | 2        | .42     | .01     | .01    | 1        | 160        | 5         |
| - S45230           | 34        | 30        | 2         | 3699      | .1        | 287       | 88        | 1068      | 37.54   | 2         | 11       | ND        | 8         | 66        | 46.4      | 4         | 6         | 64       | .57     | .019   | 3         | 8         | .05     | 208       | .01     | 8        | 1.03    | .01     | .03    | 3        | 750        | 60        |
| - S45231           | 19        | 30        | 11        | 4076      | .3        | 416       | 153       | 2352      | 30.66   | 2         | 5        | ND        | 6         | 76        | 11.7      | 2         | 2         | 69       | .41     | .026   | 2         | 6         | .04     | 446       | .01     | 2        | .46     | .01     | .10    | 2        | 1928       | 105       |
| - S45234           | 112       | 19        | 2         | 12967     | .1        | 1770      | 520       | 9333      | 37.90   | 34        | 5        | ND        | 19        | 210       | 4.9       | 2         | 5         | 11       | 1.66    | .025   | 2         | 11        | .03     | 195       | .01     | 2        | .06     | .01     | .01    | 1        | 329        | 15        |
| - S45240           | 13        | 23        | 2         | 279       | .4        | 125       | 43        | 11271     | 29.03   | 33        | 5        | ND        | 37        | 413       | 6.8       | 2         | 4         | 23       | 4.38    | .110   | 3         | 9         | .18     | 1370      | .01     | 2        | .15     | .01     | .02    | 1        | 3184       | 60        |
| STANDARD C/CB-1200 | 18        | 58        | 39        | 128       | 6.9       | 70        | 31        | 1040      | 3.96    | 38        | 17       | 7         | 37        | 52        | 16.9      | 15        | 19        | 56       | .48     | .083   | 36        | 58        | .88     | 187       | .08     | 35       | 1.88    | .07     | .16    | 10       | 2075       | 1600      |

Sample type: SILT. Samples beginning 'RE' are duplicate samples.

Fe-Seep

**APPENDIX IV**  
**Analytical Procedures**





**ACME ANALYTICAL LABORATORIES LTD.**

**Assaying & Trace Analysis**

852 E. Hastings St., Vancouver, B.C., Canada V6A 1R6

Telephone: (604) 253-3158 Fax: (604) 253-1716

**Geochemical Methods  
Acme Analytical Laboratories Ltd.**

Soil Preparation: Dry soil or silt sample up to 1 Kg  
at 60 deg.C and sieve to -80 mesh.

Rock Preparation: Rocks or cores are crushed to -  
3/16" and 250 gm is split out. This split is  
pulverized using a ring mill pulverizer to 99% -100  
mesh.

ICP Analysis: 0.50 gm sample is digested with 3ml 3-  
1-2 HCL-HNO3-H2O at 95 deg.C for one hour and is  
diluted to 10ml with water. This leach is partial for  
Mn, Fe, Sr, Ca, P, La, Cr, Mg, Ba, Ti, B, W and limited  
for Na, K, Al.

Gold Analysis (Fire Geochem): 10 gm is ignited at 600  
deg.C for 4 hours and fused with F.A. flux. The dore  
bead is dissolved in Aqua Regia and analysed by ICP.

|                        |       |
|------------------------|-------|
| Detection limit for Au | 1 ppb |
| Pt                     | 3 ppb |
| Pd                     | 3 ppb |
| Rh                     | 3 ppb |

\*\* Larger sample - on special request.



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**GOLD & SILVER BY FIRE ASSAY**

1 A.T is mixed in dry reagent flux with 1 Ag inquart and fused at 1000 deg C for 45 to 60 mins. The resulting Ag bead from cupellation is dissolved in aqua-regia. Au is analyzed by ICP. High Ag is obtained from the difference between the bead weight and the Au value. Wet acid leach Ag will also perform to obtain low grade Ag and to check Ag value obtained by fire assay. The procedure for wet acid Ag is same as below.

**ASSAY FOR CU, PB, ZN AND AG**

In 250 ml volumetric flask, 1 g sample is digested in 60 ml of aqua-regia for one hour and diluted to 250 ml. analyzed by ICP.

**WHOLE ROCK ANALYSIS**

0.2 g fused with LiBO<sub>2</sub>, dissolved in 100 ml dilute acid, analysed by ICP. This procedure is also the same for total BA.

## **APPENDIX V**

### **Rock Sample Descriptions**

| SAMPLE NUMBER | LOCATION COMMENT                                            | SAMPLE DESCRIPTION                                                                                                                                                                                                                                                                                            |
|---------------|-------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 45201         | Nod Grid - just SE of L48N, 47+50E, ele. 1500m, along creek | ≈60cm chip thru weakly rusty Poker Chip black shale, HW of nodular barite zone, no visible pyrite, non-calcareous, non-siliceous, S <sub>1</sub> 122/85NE (cleavage at high angle to bedding as noted from pencil rods)<br>ran: 2685 ppm Ba                                                                   |
| 45202         | SW of Nod Grid, along creek, ele. 1405m                     | 1.0m chip same as 45201 plus: weakly graphitic, good bedding, likely Pregnant? shale, S <sub>0</sub> 160/32SW, S <sub>1</sub> 118/80SW, L <sub>1</sub> 28+300<br>ran: 5848 ppm Ba                                                                                                                             |
| 45203         | SW of Nod Grid, along creek, ele. 1350m                     | 1.0m chip thru weak-moderately rusty Poker Chip shale with local Porcellanite bands, weak-moderately graphitic, S <sub>0</sub> 142/30SW, S <sub>1</sub> 120/85NE<br>ran: 2766 ppm Ba                                                                                                                          |
| 45204         | West of Nod Grid, along creek, ele. 1125m                   | 1.0m chip thru moderately rusty Poker Chip black shale, local concretions, S <sub>1</sub> 110/75SW<br>ran: 2656 ppm Ba                                                                                                                                                                                        |
| 45205         | South of Nod Grid, Central claims, along creek, ele. 1300m  | 1.0m chip thru moderately rusty Poker Chip with Porcellanite bands, weakly graphitic, S <sub>0</sub> 130/35SW<br>ran: 908 ppm Zn, 13.1 ppm Cd, 235 ppm V, 1192 ppm Ba                                                                                                                                         |
| 45206         | Nod Grid, just off L44N, 47+00E, ele. 1600m                 | 1.2m chip thru Nodular Barite; spherulitic barite nodules up to 4mm diameter (2mm mode), nodules circular to ellipsoid and often in discontinuous wavy bands along bedding, ± narrow ≤3mm shale bands, overall more barite than shale matrix and bands, S <sub>0</sub> 105/55NE<br>ran: 296658 ppm Ba (29.7%) |
| 45207         | Nod Grid, just off L44N, 47+00E, ele. 1600m                 | Same as 45206 plus: 1.0m chip thru Nodular Barite; more shale matrix and bands than nodular barite, S <sub>0</sub> 110/70NE<br>ran: 19410 ppm Ba                                                                                                                                                              |
| 45208         | Nod Grid, just off L44N, 46+50E, ele. 1585m                 | 1.0m chip thru Poker Chip shale, in footwall of nodular barite zone, S <sub>0</sub> 120/72NE<br>ran: 4430 ppm Ba                                                                                                                                                                                              |
| 45209         | Nod Grid, just off L44N, 46+75E, ele. 1592m                 | 1.0m chip thru Poker Chip shale, in footwall of nodular barite zone, closer to zone than 45208<br>ran: 4671 ppm Ba                                                                                                                                                                                            |
| 45210         | Nod Grid, 3m north of L44N, 47+75E, ele. 1615m              | 1.0m chip thru weakly siliceous, slightly silty Poker Chip shale, in hanging wall of nodular barite zone, bedding and cleavage not measureable<br>ran: 1569 ppm Ba                                                                                                                                            |

| SAMPLE NUMBER | LOCATION COMMENT                                                  | SAMPLE DESCRIPTION                                                                                                                                                                                                                |
|---------------|-------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 45213         | NE of B/L of Nod Grid, between L50N & 44N ele. 1385m              | 1.0m chip thru weakly rusty Poker Chip shale, no visible sulphides, along creek, S <sub>0</sub> 130/58SW                                                                                                                          |
| 45214         | NE of B/L of Nod Grid, between L44N & 50N, ele. 1375m             | 1.0m chip thru weakly rusty black Porcellanite (POR), just below sample 45213 along creek, S <sub>0</sub> 140/45SW                                                                                                                |
| 45217         | NE of B/L of Nod Grid, between L44N & 50N, ele. 1455m             | 1.0m chip thru locally moderately rusty Poker Chip shale (PCP), along creek, slightly warped bedding, S <sub>0</sub> 112/30SW, S <sub>1</sub> 100/60SW, L <sub>1</sub> 10→280<br>ran: 236 ppm Zn, 2.46% Fe, 2629 ppm Ba           |
| 45220         | South of 1616 peak, ele. 1275m                                    | 1.0m chip thru weak to moderately rusty PCP, trace disseminated pyrite, S <sub>0</sub> 160/40NE, S <sub>1</sub> 140/60NE, strong cleavage (rods), along creek<br>ran: 2754 ppm Ba                                                 |
| 45223         | South of 1616 peak, ele. 1418m                                    | 1.0m chip thru weakly rusty Pregnant shale (PR), beds 0.5cm-7cm wide (mode 2-5cm), mesoscopic fold 40→200, S <sub>0</sub> 110/35SW, along creek                                                                                   |
| 45224         | South of 1616 peak, ele. 1790m                                    | 1.0m chip thru weakly rusty PCP, S <sub>0</sub> 160/60SW, S <sub>1</sub> 130/40NE, ≈50m downstream from iron seep<br>ran: 3538 ppm Ba                                                                                             |
| 45227         | Along bank of Bowerhenney Creek, south of Seep Grid ele. 1185m    | 1.0m chip thru moderately rusty POR, beds 1-4cm wide, wavy folded, S <sub>0</sub> 135/60SW, bedding roughly parallel to axial plane of tight to isoclinal folds<br>ran: 10.3 ppm Cd, 174 ppm V                                    |
| 45228         | Upper Bowerhenney Creek tributary, North of Seep Grid, ele. 1370m | 1.0m chip thru moderate to strongly rusty POR with local PR beds, beds 1-4cm strongly folded in variable directions, local quartz-carbonate veinlets up to 2cm wide, no visible pyrite<br>ran: 1051 ppm Zn, 7.3 ppm Cd, 143 ppm V |
| 45229         | Just downstream from #45228, ele. 1330m                           | 1.0m chip thru moderately rusty POR/PR? (mostly POR), locally strongly graphitic, trace pyrite, S <sub>0</sub> 140/80SW                                                                                                           |
| 45232         | Seep Grid, along Bowerhenney Creek ele. 1190m                     | 50cm chip thru PR shale, contains laminated pyrite (up to 0.5cm) and disseminated pyrite, beds 1-5cm, S <sub>0</sub> 140/50SW<br>ran: 4.10% Fe                                                                                    |
| 45233         | Seep Grid, along Bowerhenney Creek ele. 1178m                     | 1.0m chip thru weakly laminated and disseminated pyrite in PR shale, just upstream from iron seep & waterfall, S <sub>0</sub> 010/50E                                                                                             |

[illegible]

| SAMPLE NUMBER | LOCATION COMMENT                                                                        | SAMPLE DESCRIPTION                                                                         |
|---------------|-----------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------|
| 45252         | at main fork in upper Bowerheney Ck, south of Nod Grid.                                 | Grab of porcellanite with trace pyrite and blue stain on fractures.                        |
| 45253         | Near main fork in upper Bowerheney Ck, @ 1435m elevation on west branch. Nod Grid area. | Grab of nodular barite horizon in laminated shale. Ran: 135160ppm Ba.                      |
| 45254         | Nod Grid L44N - 43+25E                                                                  | Grab of rusty pregnant shale, trace Py on fractures. Ran: 224ppm Zn.                       |
| 45255         | Nod Grid BL50E - 48+50N                                                                 | Grab of thick bedded, siliceous shale (Pregnant Shale) with graphitic partings.            |
| 45256         | Nod Grid 49+25N - 50+50E                                                                | Grab of rusty black porcellanite with trace disseminated Py.                               |
| 45257         | Nod Grid L48N - 47+25E                                                                  | 1.0m chip of rusty, laminated black shale. Haring wall to nodular barite, ran: 7848ppm Ba. |
| 45258         | Nod Grid hand trench A SE                                                               | Chip from 0.5m to 1.1m, poker chip shale. Footwall to nodular barite, ran: 1707ppm Ba.     |
| 45259         | Nod Grid hand trench A SE                                                               | Chip 1.1 to 2.1m, poker chip shale. Footwall to nodular barite, ran: 1830ppm Ba.           |
| 45260         | Nod Grid hand trench A SE                                                               | Chip 2.1 to 3.2m, poker chip shale. Footwall to nodular barite, ran: 1337ppm Ba.           |
| 45261         | Nod Grid hand trench A SE                                                               | Chip 4.2 to 5.2m, poker chip shale. Footwall to nodular barite, ran 2124ppm Ba.            |
| 45262         | Nod Grid hand trench A SE                                                               | Chip 5.2 to 6.2m, poker chip shale. Footwall to nodular barite, ran: 2734ppm Ba.           |
| 45263         | Nod Grid hand trench A SE                                                               | Chip 6.2 to 7.2m, nodular barite. Ran: 302714ppm Ba.                                       |
| 45264         | Nod Grid hand trench A SE                                                               | Chip 7.2 to 8.2m, nodular barite. Ran: 314099ppm Ba.                                       |
| 45265         | Nod Grid hand trench A SE                                                               | Chip 8.2 to 9.4m, nodular barite, trace Py. Ran: 244827ppm Ba.                             |
| 45266         | Nod Grid hand trench A SE                                                               | Chip 9.4 to 10.2m, nodular barite, trace Py. Ran: 183598ppm Ba.                            |
| 45267         | Nod Grid hand trench A NW                                                               | Chip 5.4 to 7.4m, poker chip shale, NE side of nodular barite (HW). Ran: 4026ppm Ba.       |
| 45268         | Nod Grid hand trench A NW                                                               | Chip 7.4 to 9.4m, poker chip shale, NE side of nodular barite (HW). Ran: 2008ppm Ba.       |

| SAMPLE NUMBER | LOCATION COMMENT                                             | SAMPLE DESCRIPTION                                                                                                                                                                         |
|---------------|--------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 45269         | Nod Grid hand trench A NW                                    | Chip 9.4 to 11.4m, poker chip shale, NE side of nodular barite (HW). Ran: 1923ppm Ba.                                                                                                      |
| 45270         | Nod Grid hand trench A NW                                    | Chip 11.4 to 14.2m, poker chip shale, NE side of nodular barite (HW). Ran: 2959ppm Ba.                                                                                                     |
| 45272         | Longwalk Ck. 1220m elev.                                     | 1.0m chip, rusty dark grey shale with mm scale Py laminations. Includes 10cm fault zone. Ran: 3303ppm Ba.                                                                                  |
| 45275         | Bowerheney Ck., second side Ck south of heli-pad 1080m elev. | 1.0m chip across rusty fault zone which separates porcellanite to the west from bioclastic limestone to the east. Ran: 1787ppm Pb, 2028ppm Zn, 4.3ppm Ag, 6.8ppm Cd, 164ppm V, 3736ppm Ba. |
| 45276         | Same as 45275, but at 1100m elev.                            | Grab from black, graphitic porcellanite with fracture and breccia matrix fill Py. Ran: 209ppm Zn.                                                                                          |
| 45283         | Creek traverse, north side of Warneford River. 1210m elev.   | Composite grab over 0.5m of nodular barite hosted by poker chip shale. Ran: 111579ppm Ba.                                                                                                  |
| 45284         | Same as 45283, at 1040m elev., at junction with main ck.     | Grab of distinctly laminated shale with sparse barite nodules and trace Py. Ran: 19907ppm Ba.                                                                                              |
| 45286         | Same as 45283, at 980m elev. in main ck.                     | Grab of distinctly laminated unit with Ba nodules and minor disseminated Py. Ran: 48153ppm Ba.                                                                                             |
| 45288         | Same as 45283, at 960m elev. in main ck.                     | Grab of Pregnant shale with Ba nodules and minor Py, also blue powder on fracture surfaces. Ran: 19271ppm Ba.                                                                              |
| 45289         | Near 45283, at 1145m elev.                                   | Grab of 30cm x 30cm float boulder of massive to veiny barite. Ran: 484714ppm Ba.                                                                                                           |
| 45290         | Ridge traverse north of Warneford River, 1187m elev.         | 0.5m chip of massive barite in silty shale (distinctly laminated unit?). Ran: 392204ppm Ba.                                                                                                |
| 45291         | 25m downhill from 45290.                                     | Grab of nodular to laminated and massive barite hosted by DL? Ran: 183547ppm Ba.                                                                                                           |
| 45292         | Same as 45290, at 1170m elev.                                | 1.0m chip through nodular to massive and laminated barite with minor Py (Poker Chip shale host?). Ran: 189699ppm Ba.                                                                       |



## **APPENDIX VI**

### **Soil Sample Descriptions**

1.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |        | 1715          |           | SAMPLER |      | DOUG NIKIRY |         |                  |
|------------|---------------|--------------|------------|------------------|--------|---------------|-----------|---------|------|-------------|---------|------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOUR | PARTICLE SIZE | FRAGMENTS |         |      | SLOPE       | SEEPAGE | COMMENTS         |
|            |               |              |            |                  |        |               | %         | ROUND   | COMP |             |         |                  |
| L38+00m    | 50+00E        | 15           | 5          | BM               | DB     |               |           |         |      | 15°S        |         |                  |
| "          | 50+25E        | 20           | 10         | BM               | DB     |               |           |         |      | 15°S        |         |                  |
| "          | 50+50E        | 20           | 10         | BM               | LB     |               |           |         |      | 15°E        |         |                  |
| "          | 50+75E        | 20           | 10         | BM               | LB     |               |           |         |      | 10°E        |         |                  |
| "          | 51+00E        | 20           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                  |
| "          | 51+25E        | 30           | 10         | BM               | LB     |               |           |         |      | 35°E        |         |                  |
| L38+00m    | 51+50E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         | SHALE % @ 51+50E |
| "          | 51+75E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                  |
| "          | 52+00E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                  |
| "          | 52+25E        | 20           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                  |
| "          | 52+50E        | 30           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                  |
| "          | 52+75E        | 20           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                  |
| L38+00m    | 53+00E        | 30           | 10         | BM               | LB     |               |           |         |      | 30°E        |         |                  |
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2.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |        | 1715          |           | SAMPLER |      | DOUG NIKIRK |         |                                         |
|------------|---------------|--------------|------------|------------------|--------|---------------|-----------|---------|------|-------------|---------|-----------------------------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOUR | PARTICLE SIZE | FRAGMENTS |         |      | SLOPE       | SEEPAGE | COMMENTS                                |
|            |               |              |            |                  |        |               | %         | ROUND   | COMP |             |         |                                         |
| L40+00N    | 50+00E        | 30           | 10         | BM               | DB     |               |           |         |      | 10°E        |         |                                         |
| "          | 50+25E        | 40           | 10         | BM               | DB     |               |           |         |      | 40°E        |         |                                         |
| "          | 50+50E        | 30           | 10         | BM               | LB     |               |           |         |      | 40°E        |         |                                         |
| "          | 50+75E        | 30           | 10         | BM               | DB     |               |           |         |      | 40°E        |         |                                         |
| "          | 51+00E        | 20           | 10         | BM               | DB     |               |           |         |      | 40°E        |         |                                         |
| "          | 51+25E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                                         |
| L40+00N    | 51+50E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                                         |
| "          | 51+75E        | 20           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                                         |
| "          | 52+00E        | 20           | 10         | BM               | DB     |               |           |         |      | 25°E        |         |                                         |
| "          | 52+25E        | 20           | 10         | BM               | DB     |               |           |         |      | 25°E        |         |                                         |
| "          | 52+50E        | 30           | 10         | BM               | DB     |               |           |         |      | 25°E        |         |                                         |
| "          | 52+75E        | 20           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                                         |
| L40+00N    | 53+00E        | 20           | 10         | BM               | DB     |               |           |         |      | 25°NE       |         |                                         |
| "          | 53+25E        | 30           | 10         | BM               | DB     |               |           |         |      | 20°NE       |         |                                         |
| "          | 53+50E        | 20           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                                         |
| "          | 53+75E        | 20           | 10         | BM               | DB     |               |           |         |      | 10°E        |         |                                         |
| "          | 54+00E        | 20           | 10         | BM               | LB     |               |           |         |      | 10°E        |         |                                         |
| "          | 54+25E        | 30           | 10         | BM               | LB     |               |           |         |      | 20°E        |         |                                         |
| L40+00N    | 54+50E        | 20           | 10         | BM               | LB     |               |           |         |      | 10°E        |         |                                         |
| "          | 54+75E        | 20           | 10         | BM               | MB     |               |           |         |      | 10°E        |         |                                         |
| "          | 55+00E        | 20           | 10         | BM               | DB     |               |           |         |      | —           |         |                                         |
| "          | 55+25E        | 30           | 10         | BM               | DB     |               |           |         |      | 10°E        |         |                                         |
| "          | 55+50E        | 30           | 10         | BM               | BL     |               |           |         |      | 10°W        |         | CROSS CREEK @ 55+45E<br>9% IN CREEK BED |
| "          | 55+75E        | 20           | 10         | BM               | DB     |               |           |         |      | —           |         |                                         |
| L40+00N    | 56+00E        | 20           | 10         | BM               | LB     |               |           |         |      | —           |         |                                         |
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| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |        | 1715          |           | SAMPLER |      | DOUG NIKIRK |         |                      |
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| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOUR | PARTICLE SIZE | FRAGMENTS |         |      | SLOPE       | SEEPAGE | COMMENTS             |
|            |               |              |            |                  |        |               | %         | ROUND   | COMP |             |         |                      |
| L43100N    | 50+00E        | 20           | 10         | BM               | DB     |               |           |         |      | —           |         |                      |
| "          | 50+25E        | 20           | 10         | BM               | LB     |               |           |         |      | —           |         |                      |
| "          | 50+50E        | 20           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                      |
| "          | 50+75E        | 20           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                      |
| "          | 51+00E        | 20           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                      |
| "          | 51+25E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                      |
| L43100N    | 51+50E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         | % @ 51+45E           |
| "          | 51+75E        | 30           | 10         | AM               | DB     |               |           |         |      | 35°E        |         |                      |
| "          | 52+00E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                      |
| "          | 52+25E        | 40           | 10         | BM               | DB     |               |           |         |      | 35°E        |         |                      |
| "          | 52+50E        | 20           | 10         | BM               | BL     |               |           |         |      | 35°E        |         |                      |
| "          | 52+75E        | 20           | 10         | BM               | DB     |               |           |         |      | 30°E        |         |                      |
| L43100N    | 53+00E        | 20           | 10         | BM               | DB     |               |           |         |      | 10°E        |         | CROSS CREEK @ 52+95E |
| "          | 53+25E        | 20           | 10         | BM               | LB     |               |           |         |      | 15°E        |         |                      |
| "          | 53+50E        | 30           | 10         | BM               | LB     |               |           |         |      | 20°E        |         |                      |
| "          | 53+75E        | 30           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                      |
| "          | 54+00E        | 40           | 10         | BM               | DB     |               |           |         |      | 20°E        |         |                      |
| "          | 54+25E        | 30           | 10         | BM               | LB     |               |           |         |      | 20°E        |         |                      |
| L43100N    | 54+50E        | 40           | 10         | BM               | LB     |               |           |         |      | 20°E        |         |                      |
| "          | 54+75E        | 30           | 10         | BM               | LB     |               |           |         |      | 20°E        |         |                      |
| "          | 55+00E        | 30           | 10         | BM               | LB     |               |           |         |      | 15°E        |         |                      |
| "          | 55+25E        | 30           | 10         | BM               | DB     |               |           |         |      | 10°E        |         |                      |
| "          | 55+50E        | 30           | 10         | BM               | DB     |               |           |         |      | 10°E        |         |                      |
| "          | 55+75E        | 40           | 10         | BM               | DB     |               |           |         |      | 10°E        |         |                      |
| L43100N    | 56+00E        | 30           | 10         | BM               | DB     |               |           |         |      | 10°E        |         |                      |
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| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |        | 1715          |           | SAMPLER |      | DOUG NIKIRK |         |          |
|------------|---------------|--------------|------------|------------------|--------|---------------|-----------|---------|------|-------------|---------|----------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOUR | PARTICLE SIZE | FRAGMENTS |         |      | SLOPE       | SEEPAGE | COMMENTS |
|            |               |              |            |                  |        |               | %         | ROUND   | COMP |             |         |          |
| L46+00N    | 46+75E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°N        |         |          |
| "          | 47+00E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°N        |         |          |
| "          | 47+25E        | 20           | 10         | TALUS FINES      | MD     |               |           |         |      | 15°N        |         |          |
| "          | 47+50E        | 30           | 10         | BM               | MB     |               |           |         |      | 15°N        |         |          |
| "          | 47+75E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°N        |         |          |
| "          | 48+00E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°N        |         |          |
| "          | 48+25E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°N        |         |          |
| L46+00N    | 48+50E        | 20           | 10         | BM               | MD     |               |           |         |      | 15°N        |         |          |
| "          | 48+75E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°N        |         |          |
| "          | 49+00E        | 20           | 10         | BM               | LB     |               |           |         |      | —           |         |          |
| "          | 49+25E        | 20           | 10         | BM               | MB     |               |           |         |      | 5°E         |         |          |
| "          | 49+50E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°W        |         |          |
| "          | 49+75E        | 20           | 10         | BM               | MB     |               |           |         |      | 15°W        |         |          |
| L46+00N    | 50+00E        | 20           | 10         | BM               | MB     |               |           |         |      | —           |         |          |
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|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      |             |         |          |
|            |               |              |            |                  |        |               |           |         |      | </          |         |          |

"NOD GRID"

7

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER DOUG NIKIRK |      |       |         |                     |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|---------------------|------|-------|---------|---------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                     |      | SLOPE | SEEPAGE | COMMENTS            |
|            |               |              |            |                       |        |               | %         | ROUND               | COMP |       |         |                     |
| L4B+00N    | 39+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | —     |         | CROSS CREEK @ 39+15 |
| "          | 39+25E        | 40           | 10         | BM                    | DB     |               |           |                     |      | 10°W  |         |                     |
| "          | 39+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | —     |         |                     |
| "          | 39+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | —     |         |                     |
| "          | 40+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | —     |         |                     |
| "          | 40+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | —     |         |                     |
| L4B+00N    | 40+50E        | 30           | 10         | BM                    | LB     |               |           |                     |      | 15°E  |         |                     |
| "          | 40+75E        | 30           | 10         | BM                    | DB     |               |           |                     |      | 30°E  |         | CROSS CREEK @ 40+75 |
| "          | 41+00E        | 30           | 10         | BM                    | DB     |               |           |                     |      | —     |         |                     |
| "          | 41+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°W  |         |                     |
| "          | 41+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°W  |         |                     |
| "          | 41+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 30°W  |         |                     |
| L4B+00N    | 42+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 30°W  |         |                     |
| "          | 42+25E        | 10           | 5          | BM                    | LB     |               |           |                     |      | 20°W  |         |                     |
| "          | 42+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°W  |         |                     |
| "          | 42+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°W  |         |                     |
| "          | 43+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°W  |         |                     |
| "          | 43+25E        | 10           | 5          | BM                    | LB     |               |           |                     |      | 10°W  |         |                     |
| L4B+00N    | 43+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |                     |
| "          | 43+75E        | 30           | 10         | BM                    | MB     |               |           |                     |      | 15°N  |         |                     |
| "          | 44+00E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 15°N  |         |                     |
| "          | 44+25E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 15°N  |         |                     |
| "          | 44+50E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 5°E   |         |                     |
| "          | 44+75E        | 30           | 10         | BM                    | LB     |               |           |                     |      | 5°E   |         |                     |
| L4B+00N    | 45+00E        | 30           | 10         | BM                    | DB     |               |           |                     |      | 5°E   |         |                     |
| "          | 45+25E        | 20           | 10         | BM                    | DB     |               |           |                     |      | —     |         |                     |
| "          | 45+50E        | 20           | 10         | BM                    | MB     |               |           |                     |      | —     |         |                     |
| "          | 45+75E        | 20           | 10         | BM                    | MB     |               |           |                     |      | —     |         |                     |
| "          | 46+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°W  |         |                     |
| "          | 46+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°W  |         |                     |
| L4B+00N    | 46+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°W  |         |                     |



8.

[illegible]

9.

[illegible]

10.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER DOUG NIKIRK |      |       |         |          |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|---------------------|------|-------|---------|----------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                     |      | SLOPE | SEEPAGE | COMMENTS |
|            |               |              |            |                       |        |               | %         | ROUND               | COMP |       |         |          |
| L52100N    | 47+50E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°W  |         |          |
| "          | 47+75E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°W  |         |          |
| "          | 48+00E        | 15           | 10         | BM                    | DB     |               |           |                     |      | 15°W  |         |          |
| "          | 48+25E        | 10           | 5          | BM                    | DB     |               |           |                     |      | 15°W  |         |          |
| "          | 48+50E        | 20           | 10         | BM                    | DB     |               |           |                     |      | 10°W  |         |          |
| L52100N    | 48+75E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 20°W  |         |          |
| "          | 49+00E        | 10           | 5          | BM                    | LB     |               |           |                     |      | 20°W  |         |          |
| "          | 49+25E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°NW |         |          |
| "          | 49+50E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| "          | 49+75E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| L52100N    | 50+00E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| "          | 50+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| "          | 50+50E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| "          | 50+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| "          | 51+00E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| L52100N    | 51+25E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 15°N  |         |          |
| "          | 51+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°NE |         |          |
| "          | 51+75E        | 15           | 10         | BM                    | OB     |               |           |                     |      | 20°NE |         |          |
| "          | 52+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 25°NE |         |          |
| "          | 52+25E        | 20           | 10         | BM                    | OB     |               |           |                     |      | 25°N  |         |          |
| L52100N    | 52+50E        | 15           | 10         | BM                    | LB     |               |           |                     |      | 20°NE |         |          |



12/

NOT GRID L 45+00N, L 54+00N, L 49+00N

| 1992       |                  | SOIL SAMPLES |            | PROPERTY PROJECT 1715            |        |               |           | SAMPLER G. MAY |       |       |                                                                                           |                                        |
|------------|------------------|--------------|------------|----------------------------------|--------|---------------|-----------|----------------|-------|-------|-------------------------------------------------------------------------------------------|----------------------------------------|
| SAMPLE NO. | GRID LOCATION    | DEPTH (cm)   | THICK (cm) | HORIZON                          | COLOUR | PARTICLE SIZE | FRAGMENTS |                |       | SLOPE | SEEPAGE                                                                                   | COMMENTS                               |
|            |                  |              |            |                                  |        |               | %         | ROUND          | COMP  |       |                                                                                           |                                        |
| L45+00N    | 46+75E           | 35           | 10         | BH                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
|            | 47+00E           | 30           | 10         | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
|            | 25               | 20           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           | (*) NODULAR BARITE O/C?                |
|            | 50               | 25           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 75               | 20           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 48+00E           | 20           | 10         | BM                               | MB     |               |           |                | SL/ha | -     |                                                                                           |                                        |
|            | 25               | 30           | 10         | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
| L45+00N    | 50               | 30           | 10         | BM                               | MB     |               |           |                | SL/ha | -     |                                                                                           |                                        |
|            | 75               | 30           | 10         | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
|            | 49+00E           | 30           | 10         | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
|            | 25               | 30           | 10         | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
|            | 50               | 30           | 10         | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
|            | 75               | 30           | 10         | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
| L45+00N    | 50+00E           | 30           | 10         | BM/C1                            | LB     |               |           |                | SL/ha | -     |                                                                                           |                                        |
| L54+00N    | 45+00E           | 30           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 50               | 30           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 46+00E           | 30           | 10         | BM                               | LB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 50               | 30           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 47+00E           | 30           | 10         | BM                               | LB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 50               | 20           | 5          | BM                               | LB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 48+00E           | 25           | 5          | BM                               | LB     |               |           |                | SL/ha | →     |                                                                                           |                                        |
| L54+00N    | 50               | 30           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           |                                        |
|            | 49+00E           | 30           | 10         | BM                               | MB     |               |           |                | SL/ha | →     |                                                                                           | "poker chip" O/C.                      |
|            | 50               | 30           | 10         | BM                               | MB     |               |           |                |       | →     |                                                                                           | shale O/C some (2m) staining (surface) |
|            | 50+00E           | 30           | 10         | BM                               | MB     |               |           |                | SL/ha | -     |                                                                                           |                                        |
|            | 50               | 25           | 10         | BM                               | MB     |               |           |                | SAND  | →     |                                                                                           |                                        |
|            | 51+00E           | 35           | 10         | BM                               | MB     |               |           |                | SL/ha | -     |                                                                                           | O/C                                    |
|            | 30               | 25           | 5          | BM                               | MB     |               |           |                |       | -     |                                                                                           |                                        |
| L54+00N    | 52+00E           | 25           | 10         | BM                               | MB     |               |           |                | SL/ha | →     |                                                                                           | O/C shale                              |
| L44+00N    | 50+00E to 56+00E |              |            | GRAVITY SURVEY LINE - NO SAMPLES |        |               |           |                |       |       | 50+45E "poker chip" O/C<br>~ 51+00E to ~ 54+150 ~ 50m SE<br>of line = O/C in creek (mini) |                                        |

NOD GRID L 45100N

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER G. MAY |       |       |         |          |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|----------------|-------|-------|---------|----------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                |       | SLOPE | SEEPAGE | COMMENTS |
|            |               |              |            |                       |        |               | %         | ROUND          | COMP  |       |         |          |
| L 45100N   | 39400E        | 35           | 10         | Bm                    | MB     |               |           |                |       | →     |         |          |
|            | 25            | 35           | 10         | Bm                    | DB     |               |           |                | CL    | →     |         | CREEK    |
|            | 50            | 35           | 10         | Bm                    | MB     |               |           |                |       | -     |         |          |
|            | 75            | 35           | 10         | Bm                    | MB     |               |           |                | SL    | -     |         |          |
|            | 40400E        | 35           | 10         | Bm                    | LB     |               |           |                |       | →     |         |          |
|            | 25            | 35           | 10         | Bm                    | LB     |               |           |                |       | →     |         |          |
|            | 50            | 35           | 10         | Bm                    | LB     |               |           |                |       | →     |         |          |
|            | 75            | 40           | 10         | Bm                    | DB     |               |           |                |       | →     |         |          |
|            | 41400E        | 25           | 10         | Bm                    | MB     |               |           |                | SL    | →     |         |          |
|            | 25            | 25           | 10         | Bm                    | MB     |               |           |                | SL/CL | →     |         |          |
|            | 50            | 25           | 10         | Bm                    | MB     |               |           |                |       | →     |         |          |
|            | 75            | 25           | 10         | Bm                    | LB     |               |           |                |       | →     |         |          |
|            | 42400E        | 25           | 10         | Bm                    | LB     |               |           |                |       | -     |         |          |
|            | 25            | 20           | 10         | Bm                    | LB     |               |           |                |       | -     |         |          |
|            | 50            | 20           | 10         | Bm                    | LB     |               |           |                |       | -     |         |          |
|            | 75            | 20           | 10         | Bm                    | LB     |               |           |                |       | -     |         |          |
| L 45100N   | 43400E        | 30           | 10         | Bm                    | OB     |               |           |                |       | -     |         |          |
|            | 25            | 30           | 10         | Bm                    | DB     |               | 60        |                | CL    | -     |         |          |
|            | 50            | 25           | 10         | Bm                    | DB     |               |           |                |       | →     |         |          |
|            | 75            | 25           | 10         | Bm                    | MB     |               | 60        |                | SL/CL | →     |         |          |
|            | 44400E        | 25           | 10         | Bm                    | MB     |               |           |                |       | →     |         |          |
|            | 25            | 55           | 10         | Bm                    | MB     |               |           |                |       | →     |         |          |
|            | 50            | 45           | 10         | Bm?                   | DB     |               |           |                |       | →     |         |          |
|            | 75            | 35           | 10         | Bm                    | MB     |               |           |                |       | →     |         |          |
|            | 45400E        | 25           | 10         | Bm                    | MB     |               |           |                |       | →     |         |          |
|            | 25            | 20           | 10         | Bm                    | OB     |               |           |                |       | →     |         |          |
|            | 50            | 25           | 10         | Bm                    | MB     |               |           |                | SL/CL | →     |         |          |
|            | 75            | 25           | 10         | Bm                    | MB     |               |           |                |       | -     |         |          |
|            | 46400E        | 35           | 10         | Bm                    | MB     |               |           |                |       | -     |         |          |
|            | 25            | 35           | 10         | Bm                    | MB     |               |           |                | SL/CL | -     |         |          |
| L 45100N   | 46450E        | 30           | 10         | Bm                    | MB     |               |           |                |       | -     |         |          |

$24700\text{ N}, 24900\text{ N}$ 

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER G. MAY |       |         |              |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|----------------|-------|---------|--------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                | SLOPE | SEEPAGE | COMMENTS     |
|            |               |              |            |                       |        |               | %         | ROUND          |       |         |              |
| L47100N    | 49+00E        | 20           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 25            | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 50            | 25           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 75            | 25           | 10         | Bm?                   | MB     |               |           |                | -     |         |              |
| L47100N    | 50+00E        | 25           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
| L49100N    | 45+00E        | 25           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 25            | 25           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 50            | 25           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 75            | 30           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 46+00E        | 25           | 10         | Bm                    | MB     |               |           |                | -     |         | CREEK 45+50E |
|            | 25            | 25           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 50            | 30           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 75            | 25           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
| L49100N    | 47+00E        | 25           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 25            | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 50            | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 75            | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 48+00E        | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 25            | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 50            | 10           | 5          | Bm                    | LB     |               |           |                | -     |         |              |
|            | 75            | 10           | 5          | Bm                    | LB     |               |           |                | -     |         |              |
|            | 49+00E        | 10           | 5          | Bm                    | MB     |               |           |                | -     |         |              |
|            | 25            | 20           | 10         | Bm                    | MB     |               |           |                | -     |         |              |
|            | 50            | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
|            | 75            | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |
| L49100N    | 50+00E        | 20           | 10         | Bm                    | LB     |               |           |                | -     |         |              |

15.

NOD GRID

L 47+00N

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               | SAMPLER G. AM |  |       |         |          |  |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|---------------|--|-------|---------|----------|--|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS     |  | SLOPE | SEEPAGE | COMMENTS |  |
| L47+00N    | 41+25E        | 35           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 30           | 10         | DM                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 75            | 30           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 42+00E        | 30           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 25            | 25           | 10         | DM                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 25           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 75            | 30           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
|            | 43+00E        | 25           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
|            | 25            | 25           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 25           | 10         | Bm?                   | DB     |               |               |  | 1/2   |         |          |  |
|            | 75            | 25           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 44+00E        | 25           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 25            | 25           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 25           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 75            | 25           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 147+00N       | 45+00E       | 30         | 10                    | Bm     | GB            |               |  | 1/2   |         |          |  |
|            | 25            | 25           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 25           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 75            | 25           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 46+00E        | 30           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |
|            | 25            | 25           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 25           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 75            | 25           | 10         | Bm                    | LB     |               |               |  | 1/2   |         |          |  |
|            | 47+00E        | 45           | 10         | Bm?                   | DB     |               |               |  | 1/2   |         |          |  |
|            | 25            | 45           | 10         | Bm?                   | DB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 30           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
|            | 75            | 25           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
|            | 48+00E        | 25           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
|            | 25            | 20           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
|            | 50            | 50           | 10         | Bm                    | DB     |               |               |  | 1/2   |         |          |  |
| L47+00N    | 48+75E        | 20           | 10         | Bm                    | MB     |               |               |  | 1/2   |         |          |  |

⊗ NOODLE AIR BAKITE float (local)



NOD GRID

L 50+00N, L 47+00N

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |       |               |           | SAMPLER G. MAY |        |       |         |               |
|------------|---------------|--------------|------------|-----------------------|-------|---------------|-----------|----------------|--------|-------|---------|---------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOR | PARTICLE SIZE | FRAGMENTS |                |        | SLOPE | SEEPAGE | COMMENTS      |
| L 50+00N   | 45+00 E       | 30           | 10         | Bm                    | MB    |               |           |                |        | -     |         | CREEK 44+95 E |
|            | 25            | 30           | 10         | Bm                    | MB    |               |           |                |        | SW    |         |               |
|            | 50            | 30           | 10         | Bm                    | MB    |               |           |                |        | -     |         |               |
|            | 75            | 20           | 5          | Bm                    | MB    |               |           |                |        | -     |         |               |
|            | 46+00 E       | 20           | 10         | Bm                    | LOB   |               |           |                |        | -     |         |               |
|            | 25            | 20           | 10         | Bm                    | MB    |               |           |                |        | -     |         |               |
|            | 50            | 20           | 10         | Bm                    | GR    |               |           |                |        | -     |         |               |
|            | 75            | 20           | 10         | Bm                    | LB    |               |           |                | 50/100 | -     |         |               |
|            | 47+00 E       | 20           | 10         | Bm                    | LB    |               |           |                | 50/100 | -     |         |               |
|            | 25            | 30           | 10         | Bm                    | LB    |               |           |                | 50/100 | -     |         |               |
|            | 50            | 20           | 10         | Bm                    | LOB   |               |           |                |        | -     |         |               |
|            | 75            | 20           | 10         | Bm                    | MB    |               |           |                | 50/100 | -     |         |               |
|            | 48+00 E       | 20           | 10         | Bm                    | MB    |               |           |                |        | -     |         |               |
|            | 25            | 15           | 5          | Bm                    | MB    |               |           |                | 50/100 | -     |         |               |
|            | 50            | 15           | 5          | Bm                    | LB    |               | 50        |                | 50/100 | -     |         |               |
|            | 75            | 20           | 5          | Bm                    | LB    |               | 50        |                | 50/100 | -     |         |               |
|            | 49+00 E       | 15           | 5          | Bm                    | LB    |               | 65        |                | 50/100 | -     |         |               |
|            | 25            | 20           | 5          | Bm                    | GB    |               | 50        |                | 50/100 | -     |         |               |
|            | 50            | 20           | 5          | Bm                    | LOB   |               |           |                |        | -     |         |               |
|            | 75            | 20           | 5          | Bm                    | LOB   |               | 60        |                | 50/100 | -     |         |               |
| L 50+00N   | 50+00 E       | 15           | 5          | Bm                    | LOB   |               | 60        |                | 50/100 | -     |         |               |
| L 47+00N   | 39+00 E       | 35           | 10         | Bm                    | MB    |               |           |                |        | SW    |         |               |
|            | 25            | 35           | 10         | Bm                    | MB    |               |           |                |        | -     |         |               |
|            | 50            | 35           | 10         | Bm                    | GB    |               |           |                |        | -     |         |               |
|            | 75            | 35           | 10         | Bm                    | MB    |               |           |                |        | -     |         | CREEK 39+85 E |
|            | 40+00 E       | 35           | 10         | Bm                    | MB    |               |           |                |        | -     |         |               |
|            | 25            | 25           | 10         | Bm                    | LB    |               |           |                |        | -     |         |               |
|            | 50            | 25           | 10         | Bm                    | LB    |               |           |                |        | -     |         |               |
|            | 75            | 35           | 10         | Bm                    | MB    |               |           |                |        | SW    |         | O/C scale     |
| L 47+00N   | 41+00 E       | 35           | 10         | Bm                    | MB    |               |           |                |        | SW    |         |               |

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |        | 1715          |           | SAMPLER |      | G. MAY |         |                            |
|------------|---------------|--------------|------------|------------------|--------|---------------|-----------|---------|------|--------|---------|----------------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOUR | PARTICLE SIZE | FRAGMENTS |         |      | SLOPE  | SEEPAGE | COMMENTS                   |
|            |               |              |            |                  |        |               | %         | ROUND   | COMP |        |         |                            |
| L 91+00N   | 56+00E        | 60           | 10         | Bm               | GP     |               |           |         |      | SW     |         | crack ~ 15 meters to South |
|            | 75            | 35           | 10         | Bm               | GP     |               |           |         |      | SW     |         |                            |
|            | 50            | 35           | 10         | Bm               | GP     |               |           |         |      | -      |         |                            |
|            | 25            | 35           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 55+00E        | 35           | 10         | DM               | MB     |               |           |         |      | -      |         |                            |
|            | 75            | 35           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 50            | 25           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 25            | 25           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 54+00E        | 25           | 10         | DM               | MB     |               |           |         |      | -      |         |                            |
|            | 75            | 25           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 50            | 25           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 25            | 25           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 53+00E        | 30           | 10         | Bm               | MB     |               |           |         | CL   | -      |         |                            |
| L 91+00N   | 75            | 30           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 50            | 30           | 10         | Bm               | MB     |               |           |         | CL   | -      |         |                            |
|            | 25            | 30           | 10         | C1?              | DGR    |               |           |         |      | -      |         |                            |
|            | 52+00E        | 30           | 10         | C1?              | DGR    |               |           |         |      | -      |         |                            |
|            | 75            | 35           | 10         | Bm               | MB     |               | 50        |         | 2/m  | -      |         |                            |
|            | 50            | 35           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 25            | 25           | 10         | Bm               | BM     |               |           |         |      | -      |         |                            |
|            | 51+00E        | 30           | 10         | Bm               | MB     |               |           |         |      | -      |         |                            |
|            | 75            | 20           | 10         | DM               | LB     |               |           |         |      | -      |         |                            |
|            | 50            | 20           | 10         | Bm               | CB     |               |           |         | 2/m  | -      |         |                            |
|            | 25            | 30           | 10         | Bm               | MB     |               | 50        |         | 2/m  | -      |         |                            |
| L 91+00N   | 52+00E        | 20           | 5          | Bm               | MB     |               |           |         | 2/m  | -      |         | ridge                      |

NOD GRID 2 44+00N

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER G. MAY |        |       |         |                    |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|----------------|--------|-------|---------|--------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                |        | SLOPE | SEEPAGE | COMMENTS           |
|            |               |              |            |                       |        |               | %         | ROUND          | COMP   |       |         |                    |
| L 44100N   | 42+75E        | 20           | 10         | Bm                    | M/B    |               |           |                | 54/100 | ->    |         |                    |
|            | 43+00E        | 25           | 10         | Bm                    | M/B    |               |           |                | 54/100 | ->    |         |                    |
|            | 25            | 25           | 10         | Bm                    | D/B    |               |           |                |        | ->    |         | CREEK 43+20E       |
|            | 50            | 30           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |
|            | 75            | 30           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |
|            | 44+00E        | 25           | 10         | Bm                    | C/B    |               |           |                |        | ->    |         |                    |
|            | 25            | 25           | 10         | Bm                    | D/B    |               |           |                | 54/100 | ->    |         |                    |
|            | 50            | 20           | 10         | Bm                    | D/B    |               |           |                |        | ->    |         |                    |
|            | 75            | 25           | 10         | Bm                    | D/B    |               |           |                |        | ->    |         |                    |
|            | 45+00E        | 30           | 10         | Bm                    | M/B    |               |           |                | 66/100 | ->    |         |                    |
|            | 25            | 30           | 10         | ?                     | G/R    |               | 80        |                | 54/100 | ->    |         |                    |
|            | 50            | 30           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |
|            | 75            | 30           | 10         | Bm                    | M/B    |               | 75        |                | 54/100 | ->    |         |                    |
|            | 46+00E        | 30           | 10         | Bm?                   | M/B    |               |           |                | 54/100 | ->    |         |                    |
| L 44+00N   | 25            | 30           | 10         | Bm?                   | M/B    |               |           |                | 54/100 | ->    |         | very fine talus    |
|            | 50            | 25           | 10         | Bm                    | D/B    |               |           |                | 54/100 | ->    |         | very fine talus    |
|            | 75            | 25           | 10         | Bm                    | D/B    |               |           |                | 54/100 | ->    |         |                    |
|            | 47+00E        | 20           | 10         | Bm                    | DGR    |               |           |                |        | ->    |         |                    |
|            | 25            | 25           | 10         | C 2                   | L/B    |               |           |                | 54/100 | ->    |         |                    |
|            | 50            | 20           | 10         | Bm                    | D/B    |               |           |                | 54/100 | ->    |         | "poker chip" talus |
|            | 75            | 10           | 5          | Bm                    | D/B    |               |           |                | 66     | ->    |         |                    |
|            | 48+00E        | 10           | 5          | Bm                    | O/B    |               | 50        |                | 54/100 | ->    |         |                    |
|            | 25            | 25           | 10         | Bm                    | D/B    |               |           |                |        | -     |         |                    |
|            | 50            | 20           | 10         | Bm                    | D/B    |               | 50        |                | 54/100 | ->    |         |                    |
|            | 75            | 35           | 10         | Bm                    | D/B    |               |           |                |        | ->    |         |                    |
|            | 49+00E        | 25           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |
|            | 25            | 25           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |
|            | 50            | 25           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |
|            | 75            | 25           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |
| L 44+00N   | 50+00E        | 25           | 10         | Bm                    | M/B    |               |           |                |        | ->    |         |                    |

NOD GRID L 44+00N

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER G. MAY |        |         |                         |  |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|----------------|--------|---------|-------------------------|--|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                | SLOPE  | SEEPAGE | COMMENTS                |  |
|            |               |              |            |                       |        |               | %         | ROUND          |        |         |                         |  |
| L 44+00N   | 35+00 E       | 25           | 10         | Bm                    | OB     |               | 40        |                | 50/100 | NE →    |                         |  |
|            | 25            | 20           | 10         | Bm                    | OB     |               | 60        |                | 50/100 | →       |                         |  |
|            | 50            | 20           | 10         | Bm                    | MB     |               | 25        |                | 50/100 | →       |                         |  |
|            | 75            | 25           | 10         | Bm                    | MB     |               | 25        |                | 50/100 | →       | clumpy talus            |  |
|            | 36+00 E       | 25           | 10         | Bm                    | OB     |               |           |                | 50/100 | →       |                         |  |
|            | 25            | 25           | 10         | Bm                    | MB     |               |           |                |        | -       |                         |  |
|            | 50            | 30           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 75            | 35           | 10         | Bm                    | DB     |               |           |                | CL     | →       |                         |  |
|            | 37+00 E       | 35           | 10         | Bm                    | GR     |               |           |                |        | →       | 36+60 draw              |  |
|            | 25            | 30           | 10         | Bm                    | LB     |               |           |                |        | →       |                         |  |
|            | 50            | 30           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 75            | 30           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 38+00 E       | 25           | 10         | Bm                    | MB     |               |           |                | CL     | →       |                         |  |
|            | 25            | 25           | 10         | Bm                    | MB     |               |           |                | CL     | →       |                         |  |
|            | 50            | 25           | 10         | Bm                    | MB     |               |           |                | CL     | →       |                         |  |
|            | 75            | 25           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
| L 44+00N   | 39+00 E       | 25           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 25            | 25           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 50            | 25           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 75            | 25           | 10         | Bm/CL                 | GB     |               |           |                |        | →       |                         |  |
|            | 40+00 E       | 25           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 25            | 25           | 10         | Bm                    | MB     |               |           |                | 50/100 | →       |                         |  |
|            | 50            | 25           | 10         | Bm                    | MB     |               |           |                |        | →       |                         |  |
|            | 75            | 25           | 10         | Bm                    | MB     |               |           |                | 50/100 | →       |                         |  |
|            | 41+00 E       | 25           | 10         | Bm                    | LB     |               |           |                |        | →       |                         |  |
|            | 25            | 25           | 10         | Bm                    | LB     |               |           |                |        | →       |                         |  |
|            | 50            | 25           | 10         | Bm                    | LOB    |               |           |                |        | →       |                         |  |
|            | 75            | 25           | 10         | Bm                    | LOB    |               |           |                |        | -       |                         |  |
|            | 42+00 E       | 15           | 5          | Bm                    | MB     |               |           |                |        | -       | Ridge                   |  |
|            | 25            | 15           | 5          | Bm                    | MB     |               |           |                |        | -       |                         |  |
| L 44+00N   | 50            | 20           | 10         | Bm                    | MB     |               |           |                |        | →       | scale pit. "power chip" |  |

o/c solitious charity scale  
STK ~ 3550 DIP ~ 72° W



2.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |       |               | 1715 |           | SAMPLER |      |       | DOUG NIKIRK |                                      |
|------------|---------------|--------------|------------|------------------|-------|---------------|------|-----------|---------|------|-------|-------------|--------------------------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOR | PARTICLE SIZE | %    | FRAGMENTS | ROUND   | COMP | SLOPE | SEEPAGE     | COMMENTS                             |
| L60+00N    | 60+00E        | 30           | 10         | BM               | DB    |               |      |           |         |      | 35°W  |             |                                      |
| "          | 60+25E        | 20           | 10         | BM               | MB    |               |      |           |         |      | 35°W  |             |                                      |
| "          | 60+50E        | 20           | 10         | BM               | LB    |               |      |           |         |      | 35°W  |             |                                      |
| "          | 60+75E        | 20           | 10         | BM               | LB    |               |      |           |         |      | 30°NW |             |                                      |
| "          | 61+00E        | 20           | 10         | BM               | LB    |               |      |           |         |      | 25°NW |             |                                      |
| L60+00N    | 61+25E        | 20           | 10         | BM               | LB    |               |      |           |         |      | 30°N  |             |                                      |
| "          | 61+50E        | 30           | 10         | BM               | LB    |               |      |           |         |      | 30°N  |             |                                      |
| "          | 61+75E        | 30           | 10         | BM               | LB    |               |      |           |         |      | 30°N  |             |                                      |
| "          | 62+00E        | 30           | 10         | BM               | MB    |               |      |           |         |      | 35°N  |             |                                      |
| "          | 62+25E        | 20           | 10         | BM               | DB    |               |      |           |         |      | 35°N  |             | 1/2 @ 62+20E                         |
| L60+00N    | 62+50E        | 30           | 10         | BM               | LB    |               |      |           |         |      | 35°N  |             |                                      |
| "          | 62+75E        | 30           | 10         | BM               | LB    |               |      |           |         |      | 35°N  |             |                                      |
| "          | 63+00E        | 20           | 10         | BM               | LB    |               |      |           |         |      | 35°N  |             |                                      |
| "          | 63+25E        | 40           | 10         | BM               | LB    |               |      |           |         |      | 38°N  |             |                                      |
| "          | 63+50E        | 30           | 10         | BM               | DB    |               |      |           |         |      | 45°N  |             |                                      |
| L60+00N    | 63+75E        | 30           | 10         | BM               | DB    |               |      |           |         |      | 45°N  |             |                                      |
| "          | 64+00E        | 30           | 10         | BM               | DB    |               |      |           |         |      | 45°N  |             |                                      |
| "          | 64+25E        | 20           | 10         | BM               | DB    |               |      |           |         |      | 45°N  |             | 1/2 @ 64+40E                         |
| "          | 64+50E        | 20           | 10         | BM               | DB    |               |      |           |         |      | 45°N  |             |                                      |
| "          | 64+75E        | 20           | 10         | BM               | DB    |               |      |           |         |      | —     |             | 1/2 @ 64+75E<br>CROSS CREEK @ 64+80E |
| L60+00N    | 65+00E        | 10           | 5          | BM               | MB    |               |      |           |         |      | 40°S  |             | 1/2 @ 65+00E                         |





4.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |        | 1715          |           | SAMPLER |      | DOUG NIKIRK |         |                                              |
|------------|---------------|--------------|------------|------------------|--------|---------------|-----------|---------|------|-------------|---------|----------------------------------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOUR | PARTICLE SIZE | FRAGMENTS |         |      | SLOPE       | SEEPAGE | COMMENTS                                     |
|            |               |              |            |                  |        |               | %         | ROUND   | COMP |             |         |                                              |
| L62+00N    | 60+00E        | 20           | 10         | BM               | MB     |               |           |         |      | 35°SE       |         |                                              |
| "          | 60+25E        | 20           | 10         | BM               | MB     |               |           |         |      | 30°E        |         |                                              |
| "          | 60+50E        | 30           | 10         | BM?              | DB     |               |           |         |      | —           |         | CROSS CREEK @ 60+50E<br>SAMPLE TAKEN 5M EAST |
| "          | 60+75E        | 20           | 10         | BM               | MB     |               |           |         |      | 35°W        |         |                                              |
| "          | 61+00E        | 20           | 10         | BM               | MB     |               |           |         |      | 35°W        |         |                                              |
| L62+00N    | 61+25E        | 20           | 10         | BM               | LB     |               |           |         |      | 35°W        |         |                                              |
| "          | 61+50E        | 20           | 10         | BM               | LB     |               |           |         |      | 25°W        |         |                                              |
| "          | 61+75E        | 20           | 10         | BM               | LB     |               |           |         |      | 30°S        |         |                                              |
| "          | 62+00E        | 20           | 10         | BM               | LB     |               |           |         |      | 35°S        |         |                                              |
| "          | 62+25E        | 20           | 10         | BM               | LB     |               |           |         |      | 35°S        |         |                                              |
| L62+00N    | 62+50E        | 30           | 10         | BM               | LB     |               |           |         |      | 35°S        |         |                                              |
| "          | 62+75E        | 20           | 10         | BM               | LB     |               |           |         |      | 35°S        |         | % @ 62+75E                                   |
| "          | 63+00E        | 10           | 5          | TALUS FINE       | BL     |               |           |         |      | 35°S        |         | % @ 63+00E                                   |
| "          | 63+25E        | 5            | 5          | TALUS FINE       | BL     |               |           |         |      | 35°S        |         | % @ 63+25E                                   |
| "          | 63+50E        | 20           | 10         | BM               | LB     |               |           |         |      | 35°S        |         |                                              |
| L62+00N    | 63+75E        | 5            | 5          | TALUS FINE       | BL     |               |           |         |      | 35°S        |         | % @ 63+75E                                   |
| "          | 64+00E        | 30           | 10         | BM               | DB     |               |           |         |      | 35°S        |         |                                              |
| "          | 64+25E        | 20           | 10         | BM               | MB     |               |           |         |      | 30°W        |         |                                              |
| "          | 64+50E        | 20           | 10         | BM               | LB     |               |           |         |      | 30°W        |         |                                              |
| "          | 64+75E        | 20           | 10         | BM               | MB     |               |           |         |      | 30°W        |         | % @ 64+65E                                   |
| L62+00N    | 65+00E        | 20           | 10         | BM               | LB     |               |           |         |      | 35°W        |         | % @ 65+00E                                   |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            |                  |        |               |           |         |      |             |         |                                              |
|            |               |              |            | </               |        |               |           |         |      |             |         |                                              |

# "SEEP GRID"

5.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER DOUG NIKIRK |      |       |         |                      |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|---------------------|------|-------|---------|----------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                     |      | SLOPE | SEEPAGE | COMMENTS             |
|            |               |              |            |                       |        |               | %         | ROUND               | COMP |       |         |                      |
| L64400N    | 55+00E        | 20           | 16         | BM                    | LB     |               |           |                     |      | 10°E  |         |                      |
| "          | 55+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°E  |         |                      |
| "          | 55+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°E  |         |                      |
| "          | 55+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 30°E  |         | BOTTOM OF GULLY      |
| "          | 56+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°E  |         |                      |
| L64400N    | 56+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°E  |         |                      |
| "          | 56+50E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 10°E  |         |                      |
| "          | 56+75E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 10°E  |         |                      |
| "          | 57+00E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 10°E  |         |                      |
| "          | 57+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 10°E  |         |                      |
| L64400N    | 57+50E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 25°E  |         |                      |
| "          | 57+75E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 25°E  |         |                      |
| "          | 58+00E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 25°E  |         |                      |
| "          | 58+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 25°E  |         |                      |
| "          | 58+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 25°E  |         |                      |
| L64400N    | 58+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 35°E  |         |                      |
| "          | 59+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 35°E  |         |                      |
| "          | 59+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 35°E  |         |                      |
| "          | 59+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 35°E  |         |                      |
| "          | 59+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 40°E  |         |                      |
| L64400N    | 60+00E        | 20           | 10         | BM                    | MB     |               |           |                     |      | 40°E  |         |                      |
| "          | 60+25E        | 20           | 10         | BM                    | DB     |               |           |                     |      | 40°E  |         |                      |
| "          | 60+50E        | 20           | 10         | BM                    | DB     |               |           |                     |      | 40°E  |         | CROSS CREEK @ 60+55E |
| "          | 60+75E        | 5            | 5          | TALL FINESS           | DB     |               |           |                     |      | 40°W  |         | %C @ 60+75E          |
| "          | 61+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 40°W  |         |                      |
| L64400N    | 61+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 25°W  |         |                      |
| "          | 61+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 25°W  |         |                      |
| "          | 61+75E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 15°W  |         |                      |
| "          | 62+00E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 20°W  |         |                      |
| "          | 62+25E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 25°W  |         |                      |
| L64400N    | 62+50E        | 20           | 10         | BM                    | LB     |               |           |                     |      | 30°W  |         |                      |

6.

[illegible]

# "SERP GRID"

7.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT |       | 1715          |           | SAMPLER |       | DOUG NIKIRK |                            |
|------------|---------------|--------------|------------|------------------|-------|---------------|-----------|---------|-------|-------------|----------------------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON          | COLOR | PARTICLE SIZE | FRAGMENTS |         | SLOPE | SEEPAGE     | COMMENTS                   |
|            |               |              |            |                  |       |               | %         | ROUND   | COMP  |             |                            |
| L68+00N    | 55+00E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 55+25E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 55+50E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 55+75E        | 10           | 5          | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 56+00E        | 20           | 10         | BM?              | DB    |               |           |         |       | 20°E        |                            |
| L68+00N    | 56+25E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 56+50E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 56+75E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 57+00E        | 20           | 10         | BM               | LB    |               |           |         |       | 10°E        |                            |
| "          | 57+25E        | 20           | 10         | BM               | LB    |               |           |         |       | 10°E        |                            |
| L68+00N    | 57+50E        | 20           | 10         | BM               | LB    |               |           |         |       | 15°E        |                            |
| "          | 57+75E        | 20           | 10         | BM               | LB    |               |           |         |       | 15°E        |                            |
| "          | 58+00E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 58+25E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 58+50E        | 20           | 10         | BM               | LB    |               |           |         |       | 25°E        |                            |
| L68+00N    | 58+75E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°E        |                            |
| "          | 59+00E        | 20           | 10         | BM               | LB    |               |           |         |       | 25°E        |                            |
| "          | 59+25E        | 30           | 10         | BM               | LB    |               |           |         |       | 30°E        |                            |
| "          | 59+50E        | 20           | 10         | BM?              | DB    |               |           |         |       | 40°E        |                            |
| "          | 59+75E        | 20           | 10         | BM               | DB    |               |           |         |       | 40°E        |                            |
| L68+00N    | 60+00E        | 20           | 10         | BM               | MB    |               |           |         |       | 40°E        |                            |
| "          | 60+25E        | 20           | 10         | BM               | MB    |               |           |         |       | 35°W        | CROSS CREEK @ 60+20E       |
| "          | 60+50E        | 20           | 10         | BM               | MB    |               |           |         |       | 35°W        |                            |
| "          | 60+75E        | 20           | 10         | BM               | DB    |               |           |         |       | 35°W        |                            |
| "          | 61+00E        | 20           | 10         | BM               | LB    |               |           |         |       | 30°W        |                            |
| L68+00N    | 61+25E        | 20           | 10         | BM               | DB    |               |           |         |       | 30°W        | CROSS SMALL CREEK @ 61+25E |
| "          | 61+50E        | 20           | 10         | BM               | LB    |               |           |         |       | 30°W        |                            |
| "          | 61+75E        | 20           | 10         | BM               | LB    |               |           |         |       | 30°W        |                            |
| "          | 62+00E        | 20           | 10         | BM               | LB    |               |           |         |       | 25°W        |                            |
| "          | 62+25E        | 20           | 10         | BM               | LB    |               |           |         |       | 20°W        |                            |
| L68+00N    | 62+50E        | 30           | 10         | BM               | DB    |               |           |         |       | 20°W        |                            |

8.

[illegible]

"SEEP GRID"

9.

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER G. MAY |      |       |         |                 |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|----------------|------|-------|---------|-----------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                |      | SLOPE | SEEPAGE | COMMENTS        |
|            |               |              |            |                       |        |               | %         | ROUND          | COMP |       |         |                 |
| L66+00W    | 55+00E        | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 25            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 50            | 10           | 35         | Bm                    | Lb     |               |           |                |      | →     |         |                 |
|            | 75            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         | clay            |
|            | 56+00E        | 10           | 26         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 25            | 10           | 30         | Bm                    | Mb     |               | 30        |                |      | →     |         | soil holes      |
|            | 50            | 10           | 30         | Bm                    | Mb     |               |           |                |      | →     |         | some rusty soil |
|            | 75            | 10           | 35         | Bm                    | OB     |               |           |                |      | →     |         |                 |
|            | 57+00E        | 10           | 20         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 25            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 50            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 75            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 58+00E        | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 25            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
| L66+00W    | 50            | 10           | 35         | Bm                    | Lb     |               |           |                |      | →     |         |                 |
|            | 75            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 59+00E        | 10           | 35         | ?                     | BR     |               | 90        |                |      | →     |         | tal             |
|            | 25            | 10           | 35         | Bm                    | DB     |               |           |                |      | →     |         |                 |
|            | 50            | 10           | 35         | Bm                    | DB     |               |           |                |      | →     |         |                 |
|            | 75            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 60+00E        | 10           | 25         | Bm                    | DB     |               |           |                |      | →     |         |                 |
|            | 25            | 10           | 25         | Bm                    | DB     |               |           |                |      | →     |         | soil holes      |
|            | 50            | 10           | 25         | Bm                    | Mb     |               |           |                |      | →     |         | CRACK           |
|            | 75            | 10           | 25         | Bm                    | Mb     |               |           |                |      | →     |         | soil/gravel     |
|            | 61+00E        | 10           | 25         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 25            | 10           | 35         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 50            | 10           | 25         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 75            | 10           | 25         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 62+00E        | 10           | 25         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
|            | 25            | 10           | 25         | Bm                    | Mb     |               |           |                |      | →     |         |                 |
| L66+00W    | 62+50E        | 10           | 30         | Bm                    | Mb     |               |           |                |      | →     |         |                 |

'SEEP GRID'

| 1992       |               | SOIL SAMPLES |            | PROPERTY PROJECT 1715 |        |               |           | SAMPLER G. M. H. Y |      |       |         |              |
|------------|---------------|--------------|------------|-----------------------|--------|---------------|-----------|--------------------|------|-------|---------|--------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm) | HORIZON               | COLOUR | PARTICLE SIZE | FRAGMENTS |                    |      | SLOPE | SEEPAGE | COMMENTS     |
|            |               |              |            |                       |        |               | %         | ROUND              | COMP |       |         |              |
| L6600N     | 62+75E        | 10           | 25         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 63+00E        | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 25            | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 50            | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 75            | 10           | 30         | Bm                    | OB     |               |           |                    |      | →     |         |              |
|            | 64+00E        | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 25            | 10           | 35         | Bm                    | M/B    |               | 40        |                    |      | →     |         | soil/talus   |
|            | 50            | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 75            | 10           | 35         | Bm                    | LB     |               |           |                    |      | →     |         |              |
| L6600W     | 65+00E        | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            |               | Depth        | Thick      |                       |        |               |           |                    |      |       |         |              |
| L7000W     | 55+00E        | 10           | 35         | Bm                    | M/B    |               |           |                    |      |       |         |              |
|            | 25            | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 50            | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 75            | 10           | 25         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 56+00E        | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 25            | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 50            | 10           | 25         | Bm                    | LB     |               |           |                    |      | →     |         |              |
|            | 75            | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 57+00E        | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 25            | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 50            | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 75            | 10           | 30         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 58+00E        | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 25            | 10           | 20         | Bm                    | LB     |               |           |                    |      | -     |         | BENCH        |
|            | 50            | 10           | 30         | Bm                    | OB     |               |           |                    |      | -     |         |              |
|            | 75            | 10           | 35         | Bm                    | GB     |               |           |                    |      | →     |         |              |
|            | 59+00E        | 10           | 35         | Bm                    | DB     |               |           |                    |      | →     |         |              |
|            | 25            | 10           | 35         | Bm                    | M/B    |               |           |                    |      | →     |         |              |
|            | 50            | 10           | 35         | Bm                    | DB     |               |           |                    |      | →     |         | CREEK 59+65E |
| L7000W     | 59+75E        | 10           | 35         | Bm                    | GR     |               | 40        |                    |      | →     |         | soil/talus   |

11.

| 1992       |               | SOIL SAMPLES |                                | PROPERTY PROJECT |        |               |           | SAMPLER <u>G. M. N. 7</u> |      |       |         |              |
|------------|---------------|--------------|--------------------------------|------------------|--------|---------------|-----------|---------------------------|------|-------|---------|--------------|
| SAMPLE NO. | GRID LOCATION | DEPTH (cm)   | THICK (cm)                     | HORIZON          | COLOUR | PARTICLE SIZE | FRAGMENTS |                           |      | SLOPE | SEEPAGE | COMMENTS     |
|            |               |              |                                |                  |        |               | %         | ROUND                     | COMP |       |         |              |
| L70100N    | 60+00E        | 10           | 20                             | Bm               | GR     |               | 40        |                           |      | →     |         | soil/talus   |
|            | 25            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 50            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 75            | 10           | 35                             | Bm               | MB     |               |           |                           |      | -     |         |              |
|            | 61+00E        | 10           | 35                             | Bm               | MB     |               |           |                           |      | -     |         | 61+05E CREEK |
|            | 25            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 50            | 10           | 35                             | Bm               | LB     |               |           |                           |      | →     |         |              |
|            | 75            | 10           | 25                             | Bm               | MB     |               | 60        |                           |      | →     |         | soil/talus   |
|            | 62+00E        | 10           | 30                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 25            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
| L70100N    | 50            | 10           | 25                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 75            | 10           | 30                             | Bm               | MB     |               | 30        |                           |      | →     |         | soil/talus   |
|            | 63+00E        | 10           | 70                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 25            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 50            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 75            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 64+00E        | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 25            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            | 50            | NO           | SAMPLE - Gully thick A horizon |                  |        |               |           |                           |      | →     |         | CREEK        |
|            | 75            | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
| L70100N    | 65+00E        | 10           | 35                             | Bm               | MB     |               |           |                           |      | →     |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
|            |               |              |                                |                  |        |               |           |                           |      |       |         |              |
| </         |               |              |                                |                  |        |               |           |                           |      |       |         |              |



## **APPENDIX VII**

### **Gravity Survey Specifications and Procedures**

**Instrumentation:**

A Lacoste & Romberg gravity meter, serial #371, was utilized for the gravity measurements. Pertinent meter variables are summarized below.

**Meter #371:**

| Range: | Value:  | Interval: |
|--------|---------|-----------|
| 4600   | 4836.25 | 1.05173   |
| 4700   | 4941.42 | 1.05168   |

**Additional Survey Equipment:**

- 1 Compaq portable computer
- 1 GDD Instrumentation Hydrostatic level

**Field Procedures, Gravity:**

All gravity readings were taken in a loop procedure to allow for correction of instrument drift. Temporary field bases were established as required to expedite the survey.

The gravity meters' sensitivity was set prior to the commencement of the survey and checked regularly as the survey progressed. All gravity readings were taken to the 1/100th of a milligal. Due to the extreme topography and close station spacing inner terrain corrections were not taken. The large intrinsic errors of the terrain correction would likely mask the local anomalies in this scale of survey. Five percent of the gravity stations were repeated on a random basis as an additional check on data quality. The average repeat difference was .05 milligals. The daily ties and repeatability of gravity measurements prove the overall integrity of the gravity surveying.

**Field Procedures, Surveying:**

A GDD hydrostatic level was used to obtain the gravity station elevations. The GDD level determines differential levels between two sensor ends. Using a 'leapfrog' technique elevations along and between lines can be determined. The advantage of this system is that line of sight is not required to conduct the survey. The disadvantage is that traverse closures exceed the normal closures of an optical survey by several factors. To minimize elevation inaccuracies each gravity station was occupied twice in a closed survey loop.

---

**DATA REDUCTION:**

---

The gravity readings were converted to milligals and corrected for: instrument height, earth tides, drift between base ties and adjusted to the local base value. The results are listed as Observed Gravity. Using elevations derived from the GDD hydrostatic level, the Observed Gravity values were then corrected to Bouguer Gravity using the following formula:

$$Gb = Gobs + tc - Gl + (.30845 * h) - ((.04186 * h) * d)$$

where:

*Gb* = Bouguer\_Gravity

*Gobs* = Observed\_Gravity

*Gl* = latitude\_correction

*tc* = total\_terrain\_correction

*h* = station\_elevation

*d* = density

The latitude correction was calculated as

$$1.307 * \sin^2 * \text{latitude}(\text{mgals/mile North/South})$$

Line and station positions were used to geometrically derive North-South distances.

To ensure the most accurate elevations possible from the GDD level, the following adjustments were made to the raw field readings. The loop misclosure was prorated throughout the survey traverse, then the two individual readings made at each gravity station were meaned. I feel that these measures contributed substantially to the accuracy of the elevation survey and the overall viability of the entire gravity survey.

---

**SUMMARY:**

---

There were no problems with either the gravity survey logistics or gravity data integrity throughout the course of this gravity survey. The high accuracy of the gravity measurements, as indicated by the base ties and repeats yields a reliable gravity data set from which exploration decisions may be based.

## FIELD PROCEEDURE

### Elevations

The survey was conducted using a GDD electronic level to measure elevation differences between stations. The electronic level consists of a fluid filled plastic hose and two pressure sensors to measure hydraulic pressure within the fluid. The system is sensitive to temperature changes and therefore must be used in differential mode and frequently zeroed. In this survey, a point near camp was chosen as the zero point and all measurements on the grid referenced to this point. Proceedure is for the lead operator to take a reading at a piont, mark the point, and continue on. When the rear operator reaches this point, the elevation difference is taken and the proceedure repeated.

### Gravity.

The survey utilized a Lacoste & Romberg G meter. A base station was set near camp (same as elevation) and all data was read in a looping proceedure from this point. Data was corrected for G meter daily drift, converted to observed gravity using the correction factors for the particular meter and reduced to Bouguer gravity using the formula

$$GBouguer = G_{observed} + (0.30845 * \text{elevation}) - (0.04188 * \text{elevation} * \text{density})$$
  
-Latitude corr+tidal corr+Terrain correction

where

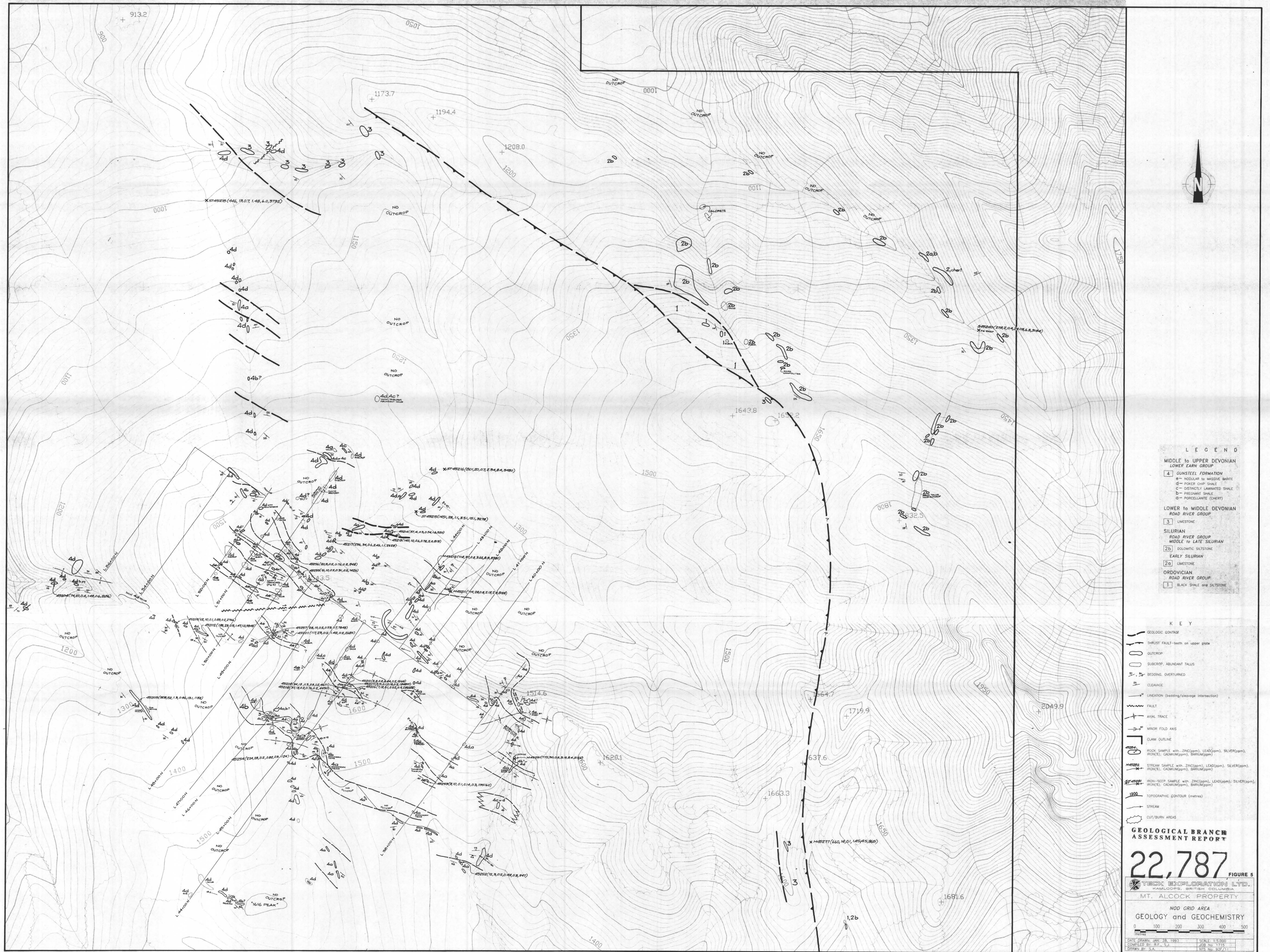
Latitude correction =  $1.307 \sin^2 \phi$  mgal/mile

Tidal correction is taken from GSC tide tables

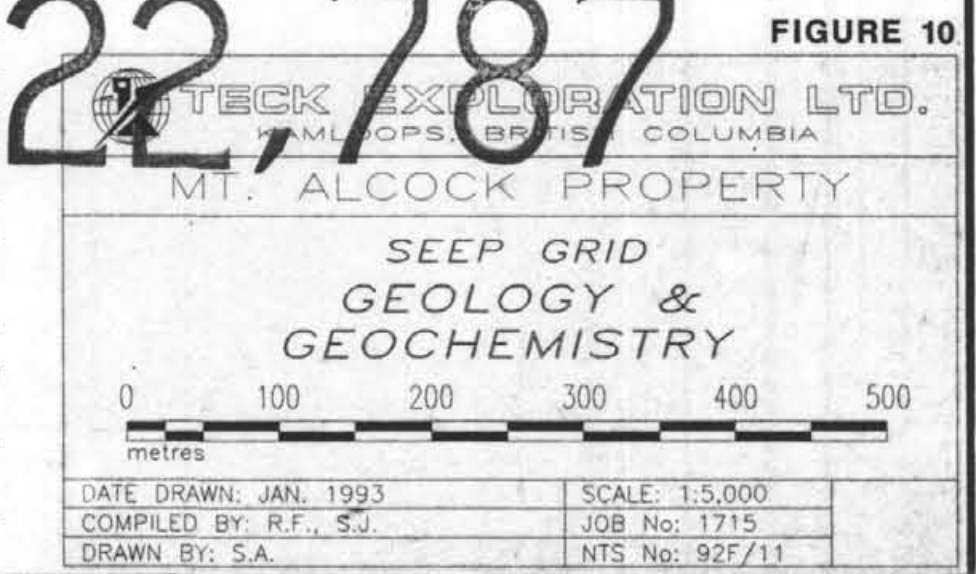
Terrain is visually estimated and corrected using Hammer charts.

Data is reduced nightly and presented as profiles



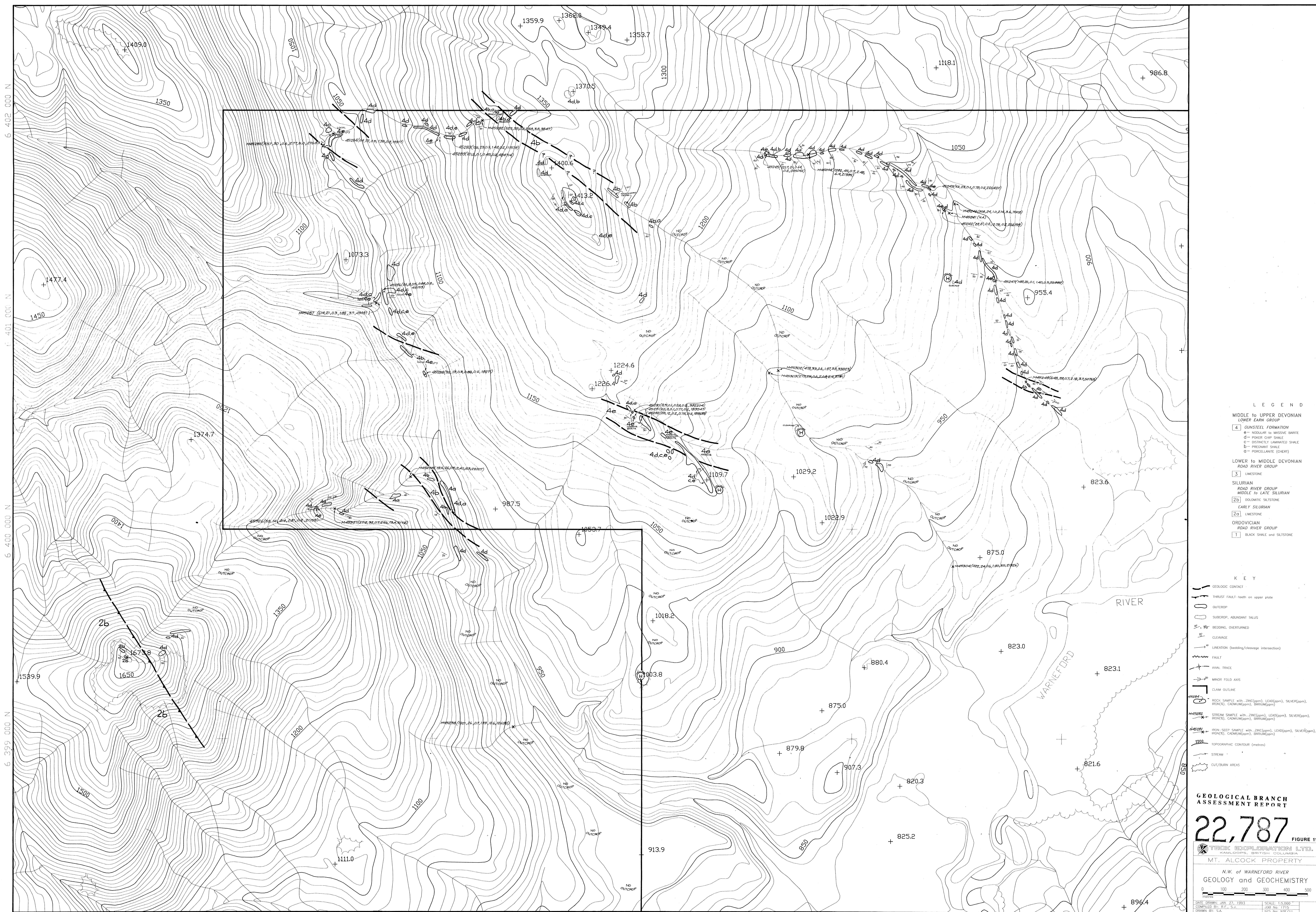








6 402 000 N  
6 401 000 N  
6 400 000 N  
6 399 000 N



- LEGEND**
- MIDDLE to UPPER DEVONIAN  
LOWER EARN GROUP
- 4 GLENSTEEL FORMATION
- 4a - NODULAR to MASSIVE BARITE
  - 4b - FOLKER CHIP SHALE
  - 4c - DISTINCTLY LAMINATED SHALE
  - 4d - PREGNANT SHALE
  - 4e - PORCELLANITE (CHERT)
- LOWER to MIDDLE DEVONIAN  
ROAD RIVER GROUP
- 3 LIMESTONE
- SILURIAN  
ROAD RIVER GROUP  
MIDDLE to LATE SILURIAN
- 2b DOLOMITE/SILTSTONE
- 2a Limestone
- ORDOVICIAN  
ROAD RIVER GROUP
- 1 BLACK SHALE and SILTSTONE

- KEY**
- GEOLOGIC CONTACT
  - THRUST FAULT - teeth on upper plate
  - OUTCROP
  - SUBCROP, ABUNDANT TALUS
  - BEDDING, OVERTURNED
  - CLEARANCE
  - LINEATION (bedding/clearance intersection)
  - FAULT
  - AXIAL TRACE
  - MINOR FOLD AXIS
  - CLIMB OUTLINE
  - ROCK SAMPLE with ZINC(ppm), LEAD(ppm), SILVER(ppm), IRON(ppm), CADMIUM(ppm), BISMUTH(ppm)
  - STREAM SAMPLE with ZINC(ppm), LEAD(ppm), SILVER(ppm), IRON(ppm), CADMIUM(ppm), BISMUTH(ppm)
  - IRON-SEED SAMPLE with ZINC(ppm), LEAD(ppm), SILVER(ppm), IRON(ppm), CADMIUM(ppm), BISMUTH(ppm)
  - TOPOGRAPHIC CONTOUR (metres)
  - STREAM
  - OUT/BURN AREAS

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

**22,787** FIGURE 11

**THECK EXPLORATION LTD.**  
KALAGORP, BRITISH COLUMBIA

MT. ALCOCK PROPERTY

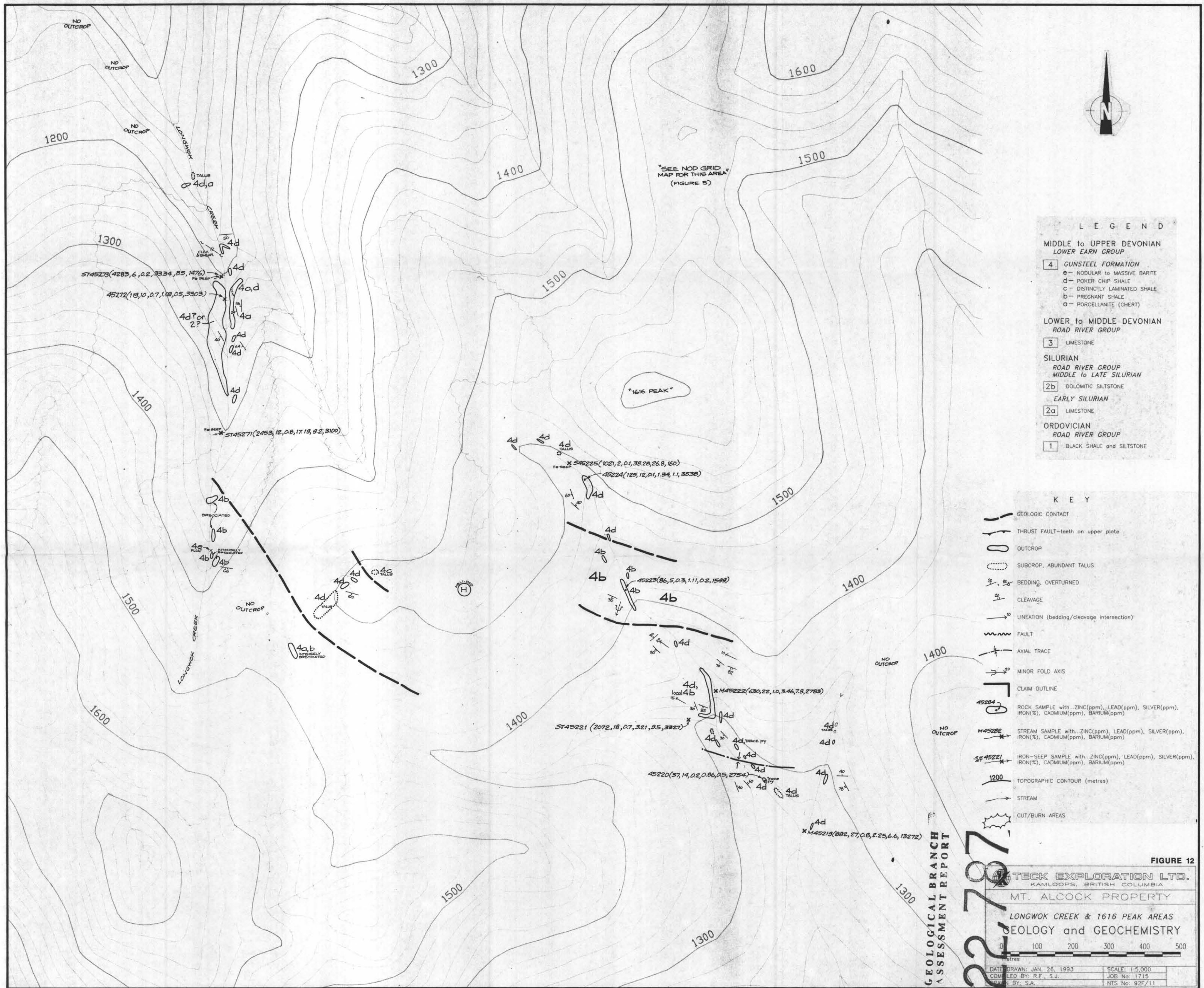
N.W. of WARNEFORD RIVER  
GEOLOGY and GEOCHEMISTRY

0 100 200 300 400 500

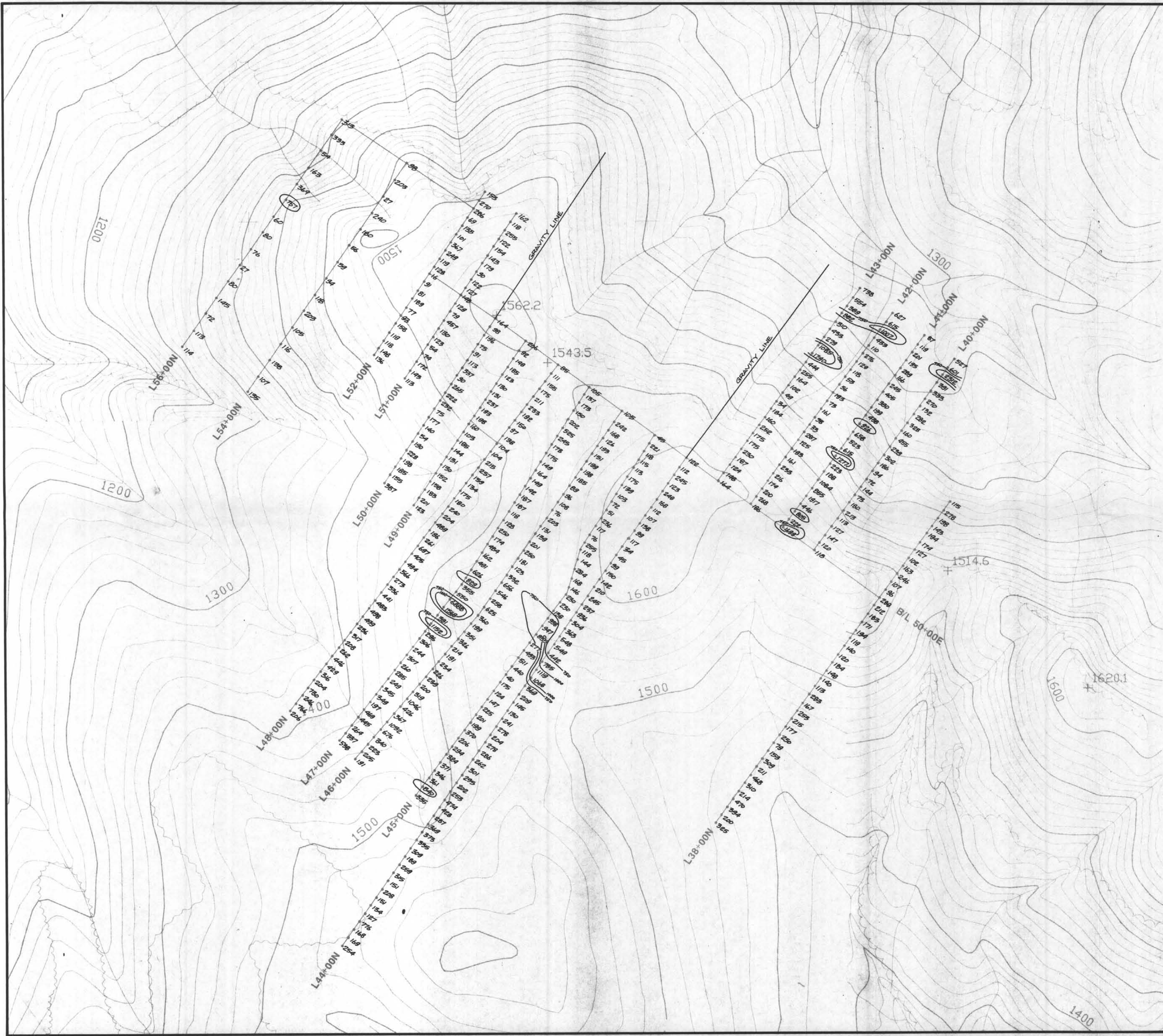
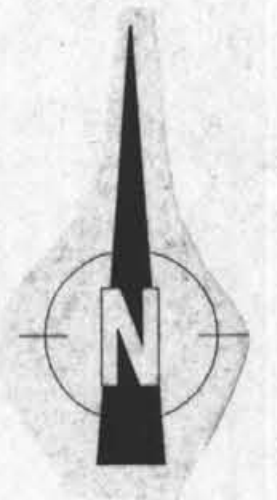
DATE DRAWN: JAN 27, 1993  
COMPILED BY: R.F. S.J.  
DRAWN BY: S.A.

SCALE: 1:5,000  
JOB No. 1715  
DATE: Nov. 9/87/11



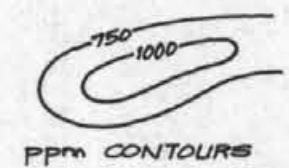






GEOLOGICAL BRANCH  
ASSESSMENT REPORT

22,787



TECK EXPLORATION LTD.  
KAMLOOPS, BRITISH COLUMBIA

MT. ALCOCK PROPERTY

NOD GRID  
Soil Geochemistry  
Zn(ppm)

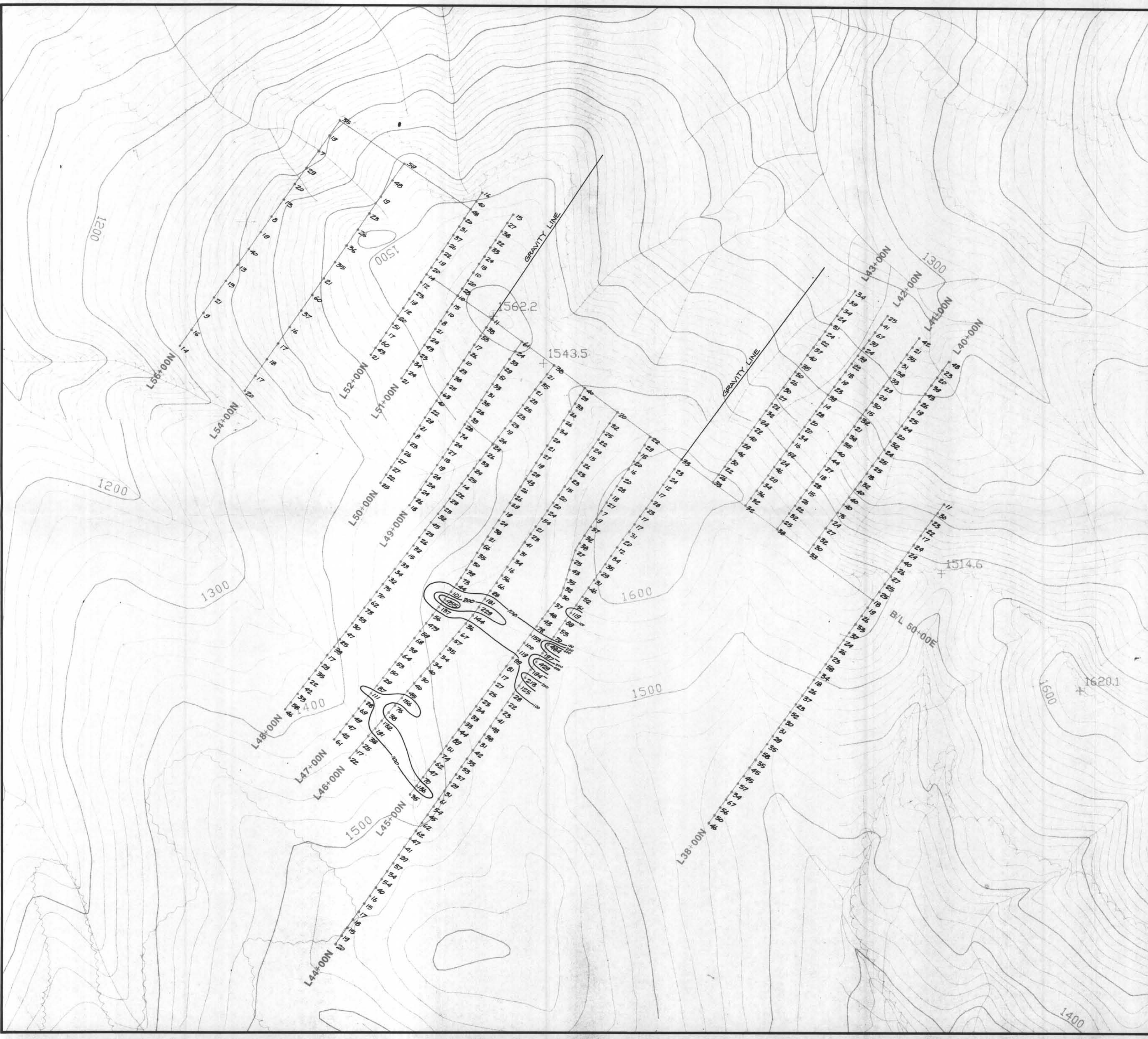
0 100 200 300 400 500  
metres

DATE DRAWN: JAN. 1993  
COMPILED BY: R.F., S.J.  
DRAWN BY: S.A.

SCALE: 1:5,000  
JOB No: 1715  
NTS No: 92F/11

FIGURE 13







GEOLOGICAL BRANCH  
ASSESSMENT REPORT

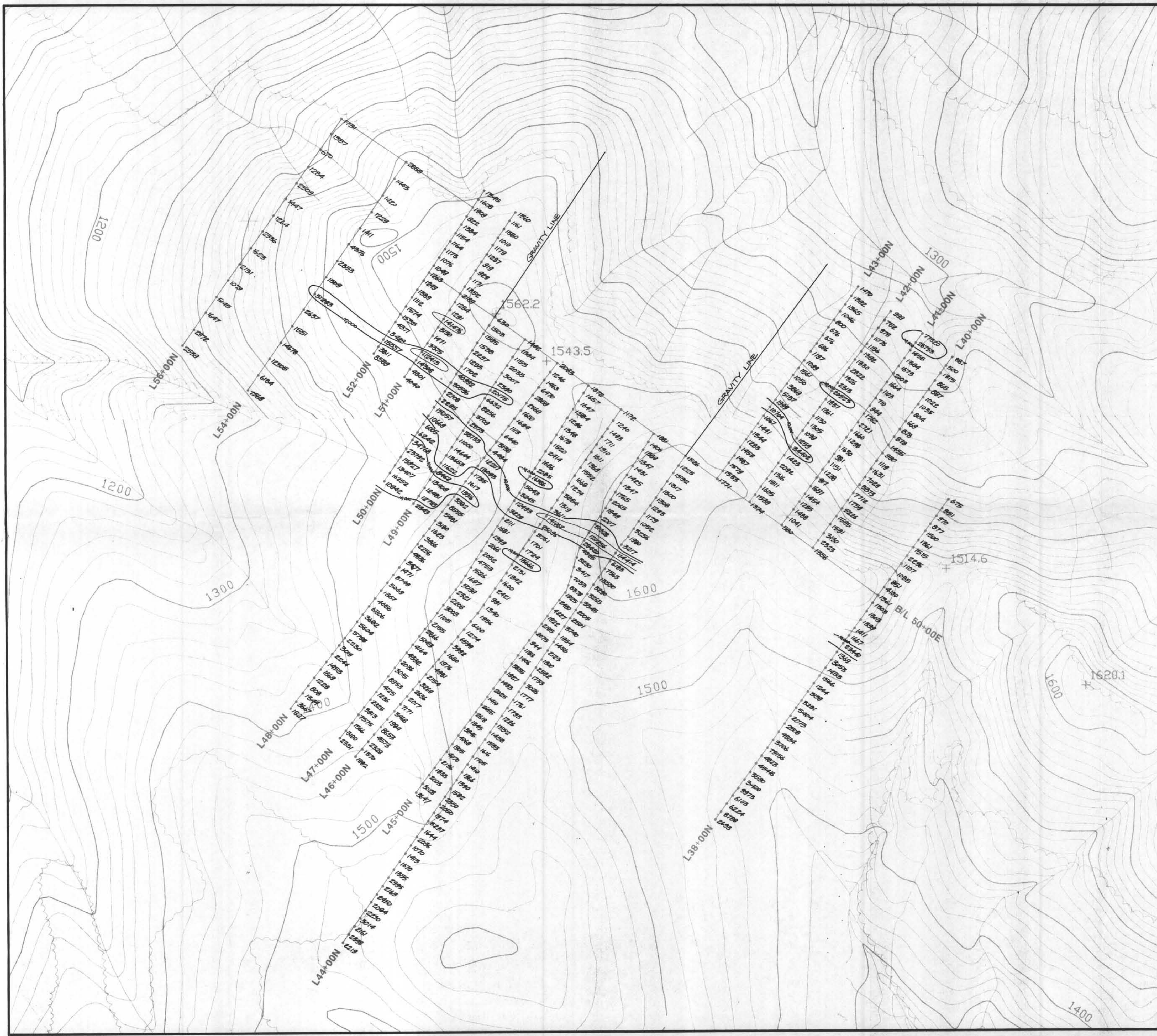
22,787



FIGURE 14

|                                                                                                                                                  |                |
|--------------------------------------------------------------------------------------------------------------------------------------------------|----------------|
|  <b>TECK EXPLORATION LTD.</b><br>KAMLOOPS, BRITISH COLUMBIA |                |
| MT. ALCOCK PROPERTY                                                                                                                              |                |
| NOD GRID<br>Soil Geochemistry<br>Pb(ppm)                                                                                                         |                |
|                                                             |                |
| DATE DRAWN: JAN. 1993                                                                                                                            | SCALE: 1:5,000 |
| COMPILED BY: R.F., S.J.                                                                                                                          | JOB No. 1715   |
| DRAWN BY: S.A.                                                                                                                                   | NTS No. 92F/11 |





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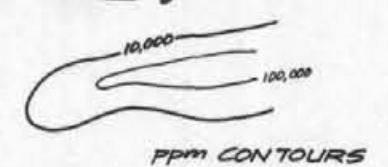
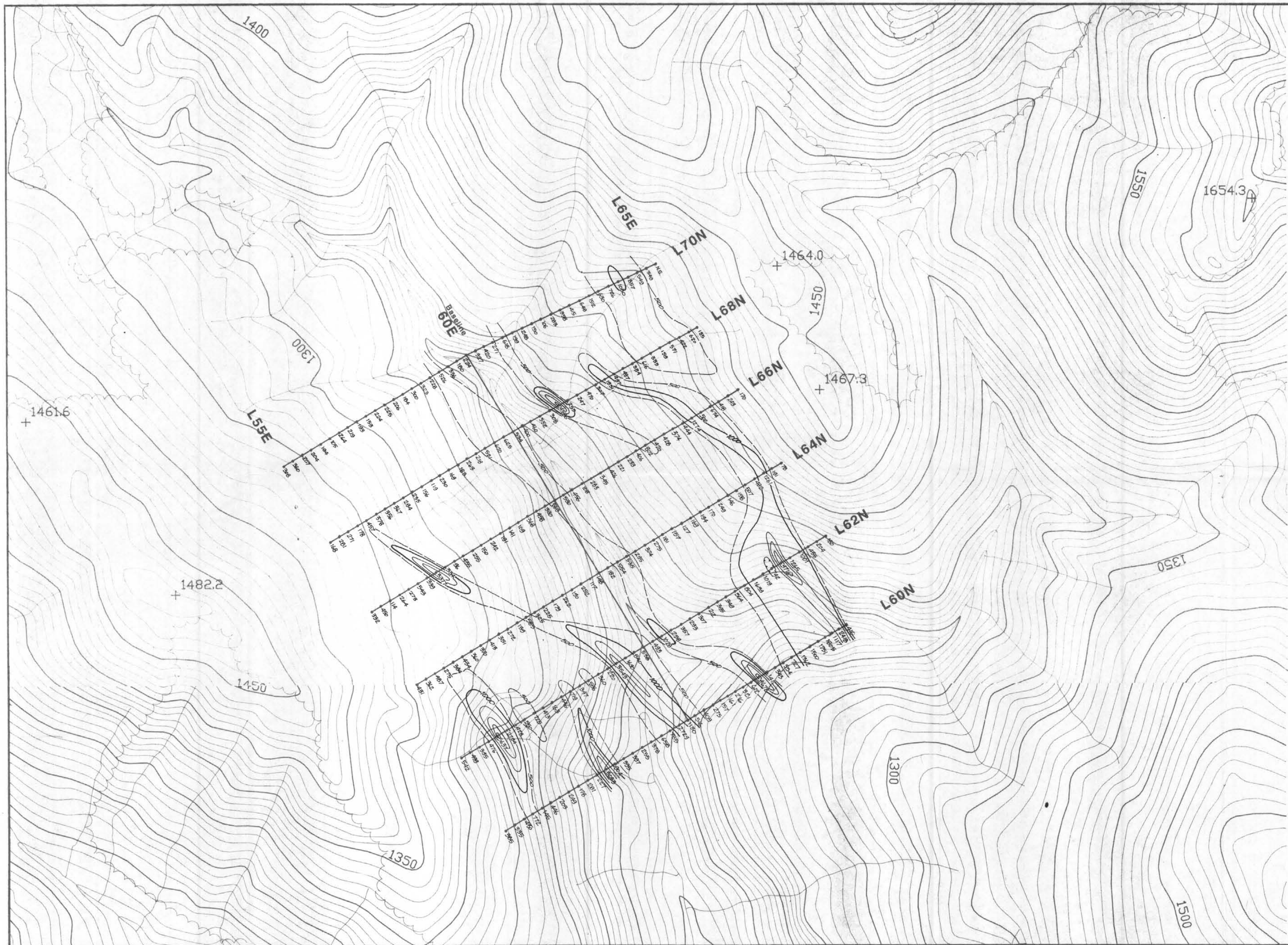


FIGURE 15

|                                                                   |                                                  |
|-------------------------------------------------------------------|--------------------------------------------------|
| <b>TECK EXPLORATION LTD.</b><br>KAMLOOPS, BRITISH COLUMBIA        |                                                  |
| MT. ALCOCK PROPERTY                                               |                                                  |
| NOD GRID<br>Soil Geochemistry<br>Ba(ppm)                          |                                                  |
| 0 100 200 300 400 500<br>metres                                   |                                                  |
| DATE DRAWN: JAN. 1993<br>COMPILED BY: R.F. S.J.<br>DRAWN BY: S.A. | SCALE: 1:5,000<br>JOB No: 1715<br>NTS No: 92F/11 |





GEOLOGICAL BRANCH  
ASSESSMENT REPORT

22,787

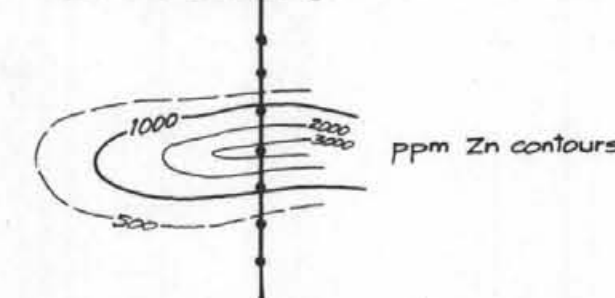


FIGURE 16

**TECK EXPLORATION LTD.**  
KAMLOOPS, BRITISH COLUMBIA

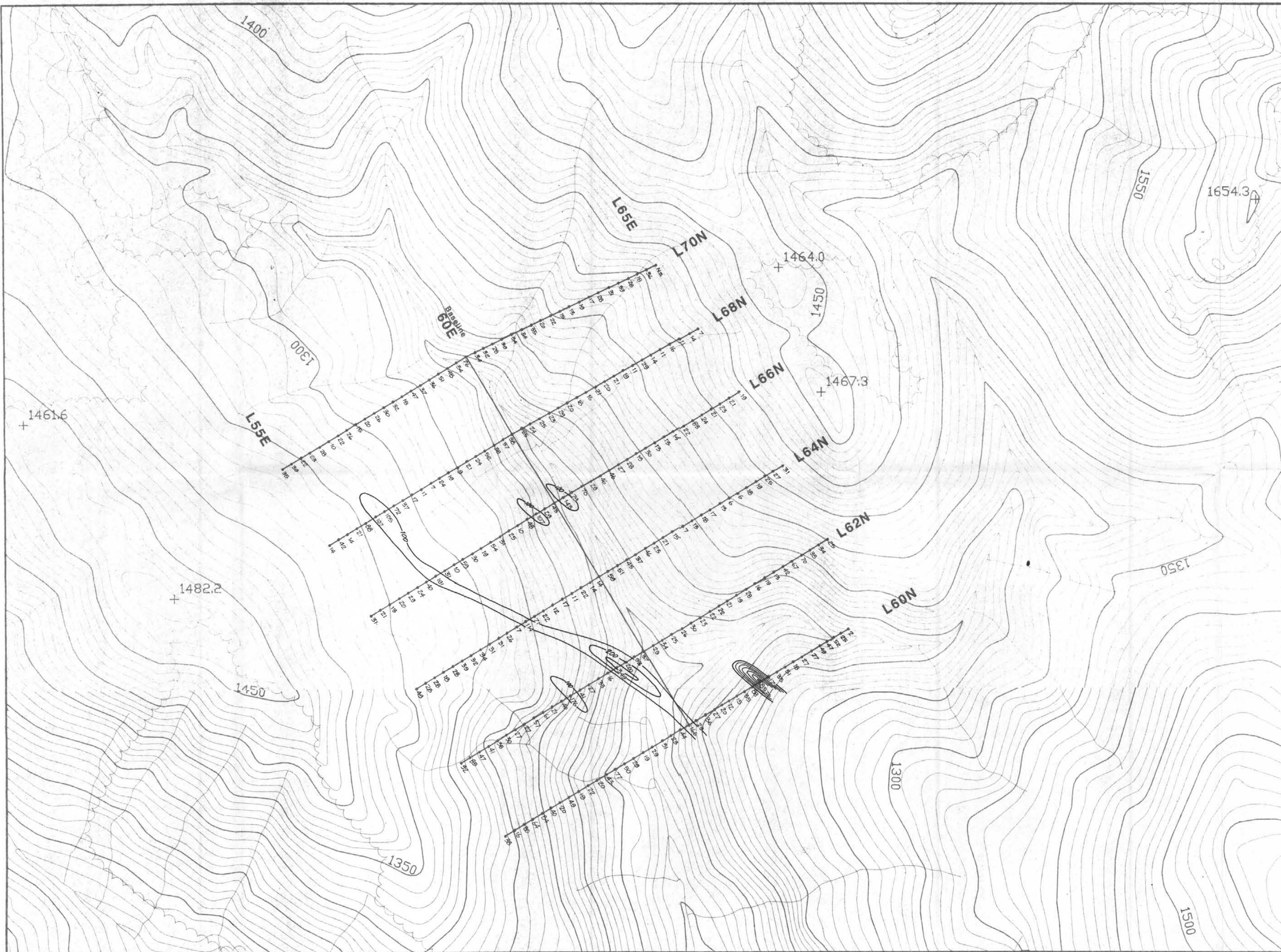
MT. ALCOCK PROPERTY

**SEEP GRID**  
Soil Geochemistry  
Zn(ppm)

0 100 200 300 400 500  
metres

|                         |                |
|-------------------------|----------------|
| DATE DRAWN: JAN. 1993   | SCALE: 1:5,000 |
| COMPILED BY: R.F., S.J. | JOB No: 1715   |
| DRAWN BY: S.A.          | NTS No: 92F/11 |





GEOLOGICAL BRANCH  
ASSESSMENT REPORT

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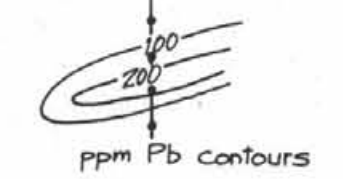

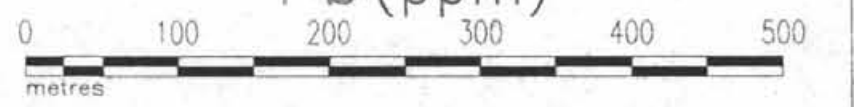
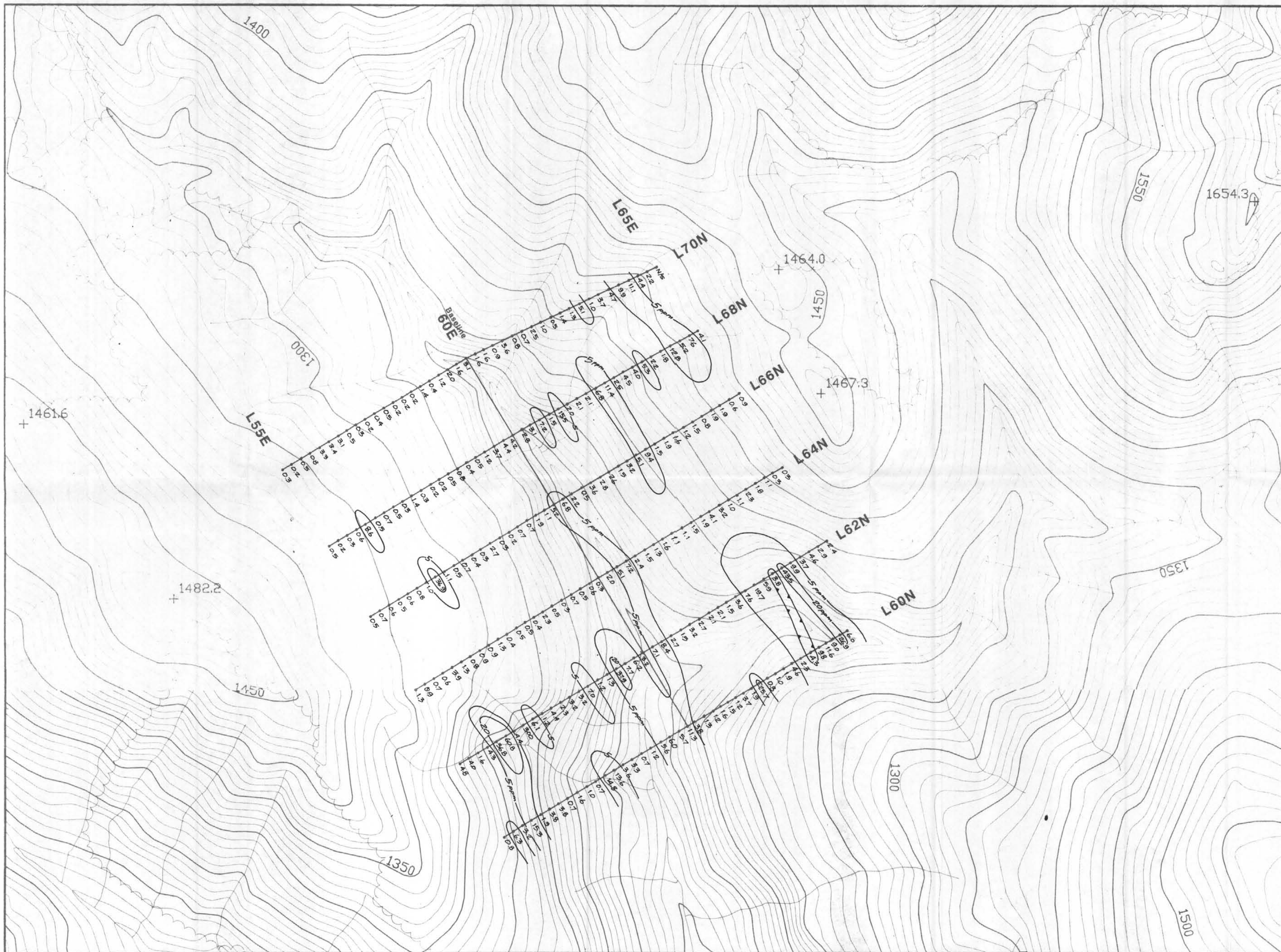


FIGURE 17

|                                                                                                                                                  |                                                  |
|--------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------|
|  <b>TECK EXPLORATION LTD.</b><br>KAMLOOPS, BRITISH COLUMBIA |                                                  |
| MT. ALCOCK PROPERTY                                                                                                                              |                                                  |
| <b>SEEP GRID</b><br>Soil Geochemistry<br>Pb(ppm)                                                                                                 |                                                  |
|                                                             |                                                  |
| DATE DRAWN: JAN. 1993<br>COMPILED BY: R.F., S.J.<br>DRAWN BY: S.A.                                                                               | SCALE: 1:5,000<br>JOB No: 1715<br>NTS No: 92F/11 |





GEOLOGICAL BRANCH  
ASSESSMENT REPORT

22,787

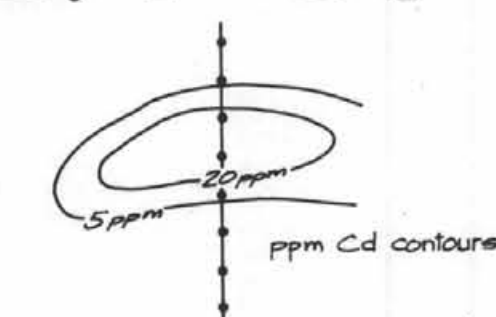


FIGURE 18

**TECK EXPLORATION LTD.**  
KAMLOOPS, BRITISH COLUMBIA

MT. ALCOCK PROPERTY

**SEEP GRID**  
Soil Geochemistry  
Cd(ppm)

0 100 200 300 400 500  
metres

DATE DRAWN: JAN. 1993  
COMPILED BY: R.F., S.J.  
DRAWN BY: S.A.

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