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## GEOCHEMICAL AND GEOLOGICAL REPORT

## **ON THE**

## COREY PROPERTY

Skeena Mining Division, British Columbia NTS 104B/8W & 9W Latitude: 56 °27' N Longitude: 130 °25'W



PART\_\_\_OF\_2

Prepared for Ambergate Explorations Inc. Kenrich Mining Corp. 504 - 455 Gran GildEuGLL OGICAL BRANCH Vancouver ABSSESSMENT REPORT

Prepare by 22,881

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#### **INTRODUCTION**

The Corey property is located within, what is commonly known as, the "Golden Triangle" of northwestern British Columbia. This area hosts numerous, significant precious and/or base metal deposits and occurrences. The recently discovered, polymetallic Eskay Creek deposit, which is owned by Homestake Canada and Placer Dome, has a probable mining reserve of 1.19 million tons which grade 1.91 oz/ton gold and 85.5 oz/ton silver. The Corey property is situated, approximately, 12 km south of the Eskay Creek deposit. Immediately north of the Corey property is the Unuk property which is controlled by Granges Inc., Springer Resources and Cove Resources. The Unuk property underwent considerable exploration during 1991, but has since been idle due to litigation. Granges had reported drill results of up to 1.21 oz/ton gold and 13.38 oz/ton silver over 13.1 feet. The Corey is partially underlain by strata similar to that which hosts the Eskay Creek deposit and the Unuk property's mineralization. To the east of the Corey property are Placer's Kerr deposit and Newhawk Mines Ltd.'s West and Snowfields zones. The Kerr deposit has published reserves of 66 million tons grading 0.86% copper and 0.01 oz/ton gold. Reserves at the West zone are at 0.826 million tons of 0.45 oz/ton gold.

During 1992, the Corey property underwent varying degrees of exploration by Kennecott Canada Inc., Inco Exploration and Technical Services Inc. and Homestake Canada Ltd. In addition, a large number of silt, rock and soil samples, previously collected from the Corey property, were reanalyzed by Placer Dome and Kenrich Mining Corp. The author was engaged by Kenrich and Ambergate to compile a report on this work. The target was economic mineralization similar to the Eskay Creek deposit.

#### 1. Location, Access, Physiography and Climate

The Corey property is situated in northwestern British Columbia, approximately 70 km north of the town of Stewart (Figure 1). The property is centred upon  $56^{\circ} - 27'$  North latitude and  $130^{\circ} - 25'$  West longitude. This is within the 104B/8W and 9W NTS map sheets.

Access is by helicopter from the Tide Lake airstrip (32 km to the southeast) or from the Bob Quinn Lake airstrip (56 km to the north). A newly constructed road, paralleling the Iskut River, extends from Bob Quinn Lake to Volcano Creek. In the near future, this road will be extended to the Eskay Creek deposit.

#### Access throughout the property is via helicopter

The majority of the property lies on the east side of the Unuk River and ranges in elevation from 250 m along Unuk River to 2363 m at the Unuk Finger. Numerous cliffs and very deeply incised drainages typify the western side of the property. The west flowing Sulphurets Creek is the major drainage and it cuts through the northern half of the property.

Treeline is transitional at, approximately, the 1,200 m elevation. The lower slopes are covered by stands of mature spruce and a thick undergrowth of alder and devil's club. A number of the elevated valleys are occupied by glaciers, while patches of semi-permanent snow are found on north-facing slopes. Talus cover and a thin veneer of poorly developed soil are common along the upper mountain slopes.



The climate is typified by cold, snowy winters and warm, wet summers. Snow accumulations at higher elevations normally exceed 5 metres, whilst 1 to 2 metres occur along the Unuk River valley.

2. **Property Status** (Figure 3)

The property consists of 64 contiguous mineral claims (782 units), which includes 5 reverted crown grants. The claims are located within the Skeena Mining Division, B.C. and have recently been grouped (Appendix 9). Their status is summarized as follows:

	TABLE	1:	Claim Status		
Claim Name	Record	No. of Linits	Date of Record	Extury Date	Owner
	1				
Corey 1	251446	20	June 25, 1986	Tune 25, 1006	Kenrich & Ambergate
Corey 2	251440	20	June 25, 1986	June 25, 1996	Kenrich & Ambergate
Corey 3	251447	20	June 25, 1986	June 25, 1990	Kenrich & Ambergate
Corey 4	251448	20	June 25, 1986	June 25, 1996	Kenrich & Ambergate
Corey 5	251449	20	June 25, 1980	June 25, 1990	Kanrich & Ambargata
Corey 5	251450	20	June 25, 1960	June 25, 1990	Kennich & Ambergate
Corey 6	251451	20	June 25, 1980	June 25, 1990	Kenrich & Ambergate
Corey /	251452	20	June 25, 1980	Julie 25, 1990	Kennich & Ambergate
Corey 8	251453	20	1  June 25, 1980	June 25, 1990	Kenrich & Ambergate
Corey 10	251/14	12	Feb. 11, 1987	Feb. 11, 1997	Kenrich & Ambergaie
Corey 11	251715	4	reb. 11, 1987	red. 11, 1997	Kenrich & Ambergale
Corey 12	251716	4	Feb. 11, 1987	Feb. 11, 1997	Kenrich & Ambergate
Corey 14	251717	12	Feb. 11, 1987	Feb. 11, 1997	Kenrich & Ambergate
Corey 15	251718	16	Feb. 11, 1987	Feb. 11, 1997	Kenrich & Ambergate
Corey 16	251719	18	Feb. 11, 1987	Feb. 11, 1997	Kenrich & Ambergate
Corey 18	251720	20	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 19	251721	20	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 20	251722	16	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 21	251723	4	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 22	251724	4	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 23	251725	16	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 24	251726	16	Feb. 11, 1987	Feb. 11, 1997	Kenrich & Ambergate
Corey 25	251727	4	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 26	251728	4	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 27	251729	16	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 28	251730	16	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 29	251731	8	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate



	TABLE	1:	Claim Status	(continued)	
Claim Name	Record	No. of Units	Date of Record	Exmins Date	Owner
					V HUC
Corey 30	251732	8	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 31	251733	16	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 32	251734	20	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 33	251735	20	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 34	251736	20	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 35	251737	20	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 36	251738	14	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 37	251739	14	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 38	251740	12	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 39	251741	12	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 40	251742	12	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 41	251743	12	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 42	251744	5	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 43	251745	4	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 44	251746	20	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Corey 45	251747	10	Feb. 11, 1987	Feb. 11, 1996	Kenrich & Ambergate
Tine 1	252211	18	Feb. 10, 1989	Feb. 10, 1997	Kenrich & Ambergate
Ginger 1	301766	20	June 26, 1991	June 26, 1996	Kenrich & Ambergate
Ginger 2	301767	20	June 26, 1991	June 26, 1996	Kenrich & Ambergate
Candy 1 Fr.	303817	1	Sept. 10, 1991	Sept. 10, 1997	Kenrich & Ambergate
DEL-1	308909	8	April 16, 1992	April 16, 1996	Kenrich & Ambergate
DEL-2	308910	5	April 16, 1992	April 16, 1996	Kenrich & Ambergate
Cumberland (L265)	251492	1	Aug. 01, 1986	Aug. 01, 1997	Kenrich & Ambergate
Silver Pine (L266)	251493	1	Aug. 01, 1986	Aug. 01, 1997	Kenrich & Ambergate
Middlesex (L267)	251494	1	Aug. 01, 1986	Aug. 01, 1997	Kenrich & Ambergate
Ziphis (L268)	251495	1	Aug. 01, 1986	Aug. 01, 1997	Kenrich & Ambergate
Ougma (L269)	251496	1	Aug. 01, 1986	Aug. 01, 1997	Kenrich & Ambergate
Sul 1	251348	20	Feb. 28, 1986	Feb. 28, 1997	Kenrich
Sul 2	251349	20	Feb. 28, 1986	Feb. 28, 1997	Kenrich
Unuk 20	251377	20	Feb. 28, 1986	Feb. 28, 1997	Kenrich
Nica 1	252209	12	Sept. 10, 1988	Sept. 10, 1997	Ambergate
Nica 2	252210	16	Sept. 10, 1988	Sept. 10, 1997	Ambergate
Dee 1	253609	5	Feb. 18, 1990	Feb. 18, 1997	Kenrich
Dee 2	253610	4	Feb. 18, 1990	Feb. 18, 1997	Kenrich
Dee 3	253611	3	Feb. 18, 1990	Feb. 18, 1997	Kenrich
Dee 4	253612	4	Feb. 18, 1990	Feb. 18, 1997	Ambergate
Dee 5	253613	8	Feb. 18, 1990	Feb. 18, 1997	Ambergate
Dee 6	253614	4	Feb. 18, 1990	Feb. 18, 1997	Ambergate



#### 3. History of Exploration

The earliest exploration in the region appears to have been carried out by prospectors during the late 1800's. Mineral claims were first staked in the area of the present day Corey property by H. W. Ketchum in 1898. The Unuk River Mining and Dredging Company acquired the property in 1900 and excavated two adits on the Cumberland claim.

Only limited exploration was carried out within the region until the 1960's when the search for porphyry copper passed through the area. This was led by Newmont Mining Corporation who discovered a number of base and precious metal mineral occurrences, especially near the headwaters of Sulphurets creek.

Following a dramatic increase in precious metal prices in the late 1970's, regional exploration intensified until 1981.

During 1986, Catear Resources Ltd. staked the Corey 1 to 8 claims and carried out a program of rock and silt geochemistry and prospecting. This work apparently resulted in the discovery of the C-10 mineral occurrence. At this time Skelly Resources Ltd. staked the Sul 1&2 and Unuk 20 claims.

During 1987, the property was optioned to Bighorn Development Corp. who subsequently staked an additional 516 claim units. A program of property-wide silt, soil and rock geochemistry and prospecting and detailed evaluation was completed. The detailed work consisted of geological mapping, 49 metres of trenching and 590 metres of diamond drilling in six holes at the Cumberland prospect. The drilling, apparently, was done in two drill fans (-45, -60 and -70), with the first fan being underneath an old adit and the second, 50 to 100 feet along strike, to the south. During this period, Bel Pac Industries Ltd. acquired the Sul 1&2 and Unuk 20 claims.

During 1988, Bighorn carried out a program of follow-up silt sampling and prospecting and completed 647 metres of diamond drilling in six holes on the C-10 prospect. At this time, Kenrich Mining Corp. (nee Farquest Energy Corp.) optioned the Sul 1&2 and Unuk 20 claims. In addition, Ambergate Explorations Inc. (nee Nica Ventures Inc.) acquired the Nica 1 claim.

In 1989, Kenrich and Ambergate conducted linecutting, geological mapping, soil and silt sampling, magnetometer and VLF surveys on the Unuk 20 and Nica 1 claims, and a silt program on the Sul 1&2 claims.

During 1990, Ambergate drilled 86.0 metres in two diamond drill holes on the Nica 1 claim. Kenrich drilled seven diamond drill holes, totaling 486.4 metres, on the Unuk 20 claim.

In 1991, Placer Dome Inc. optioned the Sul 1&2, Nica 1 and Unuk 20 claims from Kenrich and Ambergate. An exploration program of geological mapping, soil and silt sampling, linecutting and surface geophysics (Mag, VLF-EM and limited I.P.) was completed. Placer also evaluated the potential of the Cumberland and C-10 prospect. Their work consisted of soil and rock geochemical, geological mapping and geophysical (VLF-EM and I.P.) surveys.

#### 1992 Work Program Summary

4.

The 1992 work was completed over two different portions of the Corey property.

The eastern portion of the property (Sul 1&2, Unuk 20 and Nica 1 claims) was under option to Placer Dome Inc. They carried out geochemical, geophysical and diamond drilling surveys which are described in a separate report by Placer.

The rest of the Corey property underwent varying degrees of exploration by Kennecott Canada Inc., Inco Exploration and Technical Services Inc. and Homestake Canada Ltd. This work consisted of geochemical sampling and geological mapping. In addition, Placer Dome Exploration Limited and Kenrich Mining Corp. completed a re-analysis of 1,104 geochemical samples, previously collected from the Corey property. Kenrich's consulting geologist, Dave Trueman, oversaw and/or organized much of this work (Trueman's qualifications found in Appendix 1).

#### **GEOLOGY**

#### 1. <u>Regional Geology</u> (Figure 4)

The general Unuk River area lies within the Intermontane tectono-stratigraphic belt - one of five, parallel, northwest/southeast trending belts which comprise the Canadian Cordillera. This belt of Permian to Middle Jurassic volcanic and sedimentary rocks defines the Stikinia/Stikine terrane. This is bounded on the west by the Coast Plutonic Complex and overlapped on the east and north by younger sediments of the Bowser Basin. The belt has been intruded by at least four episodes of plutonic rocks, from Late Triassic to Oligocene-Miocene.

The immediate Unuk River area is underlain by island arc rocks which have been intruded by plutonic rocks of Tertiary and Jurassic age. Volcanic and sedimentary rocks of the Stuhini Group, Triassic age, form the base of this island arc terrane. Stratigraphically overlying the Stuhini is the Hazelton Group (Jurassic). The Hazelton Group consists of four geologic formations. The Unuk River Formation's volcanic and sedimentary strata form the base of the Hazelton. Overlying this are sediments and intermediate to felsic volcanics of the Betty Creek Formation. These are in turn overlain by felsic rocks of the Mount Dilworth Formation, which is an extensive marker unit in the region. Dacitic to rhyolitic flows, tuffs, breccias and pyroclastic rocks dominate this formation. At the top of the Hazelton are mafic volcanic flows and breccias with interbedded sediments of the Salmon River Formation. The Salmon River and Mount Dilworth formations are the hosts for the Eskay Creek deposit. The Hazelton Group is overlain by the Bowser Lake Group.

#### 2. Property Geology

Reconnaissance mapping performed by Homestake Canada Ltd. and Kennecott Canada Inc. in the northwestern portion of the property revealed a structurally complex sequence of sediments and basic to felsic volcanics. The strata, generally, dips moderately to steeply to the east but field observations indicate some of the bedding has been overturned. Lineation measurements in this area revealed a shallow to moderate angle of stretching (S.E. to N.E.). In this portion of the property, north of Sulphurets creek, the stratigraphic units, from east to west, are described as follows:

#### John Peaks Pluton (Jurassic)

The only exposure observed was a biotitic granodiorite.

#### Sediments and Metasediments

These include epiclastics, mudstones, wackes and minor amounts of limestone and phyllite. Locally, the sediments are described as black, cherty and/or banded. A small wedge of plagioclasehornblende porphyritic monzodiorite was observed within this unit. Weak Kspar and propylitic alteration was noted.



#### Intermediate to Felsic Volcanics

These volcanics are, generally, pale green to black dacites to rhyolites. They include dacitic heterolithic tuffs and felsic debris flows and breccias. Minor amounts of Kspar and quartz-sericite-pyrite alteration was observed. Interbedded and locally foliated sediments were also noted within this sequence. The sediments include mudstone, siltstone, chert pebble conglomerate and fine-grained, cherty rocks.

#### Sediments

A narrow band of sediments was observed on the east side of a north-northwest trending fault structure. These include mudstone, argillite and silty to sandy sediments.

#### Mafic Volcanics

These are described as andesitic to basaltic volcanics which are commonly pillowed and/or brecciated. A few narrow quartz veins and exposures of dacitic fragmentals, andesitic dykes and siltstone/argillite were also observed. This unit is cut by a second, prominent north-northwest trending fault with a few associated, intrusive exposures of feldspar porphyry.

#### Intermediate Volcanics

Andestic to dacitic volcanics dominate this unit. Monolithic dacite breccias and mudstone were also observed.

South of Sulphurets creek, the Homestake mapping revealed that most of the exposures east of Mandy creek consist of andesitic to dacitic volcanics. These include chloritic schist and chloritic lithic tuff with interbedded argillite and mudstone. A few small felsic tuff exposures and mafic dykes were also noted. A number of narrow quartz veins are found in this area. To the west and south of Mandy creek, pillowed basalts and flow breccias dominate. A number of exposures of chert were also mapped. Further south is the Lee Brant Stock (Tertiary age) which is reported to consist of granite and granodiorite. Several, associated diorite and lesser aplite dykes were found within the surrounding metasediments and metavolcanics. The metasedimentary rocks consist of schist, marble and amphibolite. Locally, pillow structures, intense propylitic alteration and narrow quartz veins were observed.

#### 3. Mineralization

No new, significant mineralization was discovered during the course of the limited 1992 field programs. Homestake observed only minor amounts of pyrite.

#### **GEOCHEMISTRY**

#### 1. <u>Sampling</u>

A total of 1,597 geochemical samples were collected and/or analyzed during the 1992 field season.

Inco Exploration and Technical Services Inc. collected 6 grab/chip samples from the Cumberland occurrence.

Kennecott Canada Inc. collected 1 silt and 36 grab rock samples from the Corey property. The majority of these samples were taken north of Sulphurets creek.

Homestake Canada Ltd. collected 194 rock, 86 silt, 83 heavy mineral concentrate and 87 moss mat samples during the course of their investigation. The majority of the rock samples are grabs, although a few chip and two old drill core samples were also taken.

Placer Exploration Limited and Kenrich Mining Corp. re-analyzed 719 silt, 28 soil and 357 rock samples, which were collected during the 1987 and 1988 field seasons.

#### 2. <u>Analysis</u>

The Inco samples were sent to Acme Laboratories of Vancouver for fire assay preparation-atomic absorption finish gold, a 35 element ICP package and whole rock analysis. The samples were also sent to Activation Laboratories Ltd. of Ontario for a 35 element neutron activation analysis.

Kennecott sent their samples to International Plasma Laboratory Ltd. of Vancouver. Thirty-five of the rock samples and the silt sample's analysis consisted of 30 element ICP  $\pm$  fire assay preparationatomic absorption finish gold. Twenty-one of these rock samples underwent whole rock analysis. A grab sample from the Cumberland Showing was assayed for copper, lead, zinc, silver and gold.

Homestake sent their samples to Bondar Clegg & Co. Ltd. of North Vancouver for preparation and analysis. A total of 101 rock samples were analyzed by gold and silver fire assaying (30 gram samples), 5 element (Cu, Pb, Zn, Mo & Hg) ICP and 2 element (Sb & As) neutron activation. Another ninety-three rock samples underwent whole rock analysis. The 86 silt, 83 heavy mineral concentrate and 87 moss mat samples' analyses consisted of fire assay preparation-atomic absorption finish gold and silver, 5 element (Cu, Pb, Zn  $\pm$  Mo) ICP, 2 element (Sb & As) neutron activation and a cold vapour AA for Hg.

Placer had the 1,104 sample pulps sent from Loring Laboratories Ltd. of Calgary to the Placer Dome Research Centre for analysis. The samples' analyses consisted of gold determinations (10.0 grams digested with aqua regia and determined by graphite furnace A.A.) and a 27 element (Ag, Mo, Cu, Pb, Zn, As, Sb, Cd, Ni, Co, Mn, Bi, Cr, V, Ba, W, Be, La, Sr, Ti, Al, Ca, Fe, Mg, K, Na & P) ICP package.

#### 3. Description and Discussion of Results

#### i) Inco's Program (Figure 6)

The six rock sample results revealed that significant values are, apparently, restricted to the immediate, Cumberland showing area. The better gold, silver and lead results were obtained from the massive sulphide mineralization, while the laminated sulphides carry the highest zinc, copper and lead values. The massive barite returned significant silver, zinc and lead and anomalous gold results. The altered host rock carries anomalous gold, silver, zinc, lead, copper and barite.

#### ii) Kennecott's Program (Figures 7 and 8)

The only significant results were obtained from samples collected from the Cumberland showing. A grab sample from the massive sulphides returned 0.188 oz/t gold, 7.27 oz/t silver, 1.26 % copper, 7.38 % lead and 17.45 % zinc. The samples collected to the north and south of the Cumberland returned results at background levels.

iii) Homestake's Program (Maps 25-27)

The only significant rock sample results were obtained from the Cumberland showing. Sample number 62305, a 1.2 metre chip which included 30 cm of massive sulphide, returned 0.392 oz/t gold, 5.29 oz/t silver and significant lead and zinc values.

The silt, moss mat and heavy mineral concentrate results revealed numerous, single and multi-element anomalies. Anomalous values were deemed to be those in excess of 100 ppb Au, 2 ppm Ag, 100 ppm As, 10 ppm Sb and 450 ppm Zn. It should noted that the majority of the Au anomalies were obtained from the moss mat and heavy mineral samples. In general, the results indicate five areas of interest. These areas are described as follows:

#### 1) Northwestern portion of the property

Several single element Au, Sb, As and Zn anomalies were returned from this area. In addition, coincident Au-Ag-Sb-Zn (#199), Au-Ag-Zn (#308) and As-Sb (#300) anomalies are present.

#### 2) Southwest of Mount Madge

Ag (#315 and 311), Au (#313) and Au-As-Sb (#310) anomalies were obtained from creeks draining this area.

#### 3) East of Mount Madge

Numerous single element Au, As, Sb and Zn anomalies and two Au-Zn anomalies (#162 and 147) were returned from this area.

4) Elgar Showing Area

A number of Au, Sb, Au-Ag (#190), Au-Sb (#188) and Sb-Zn (#203) anomalies were obtained from creeks draining this area.

#### 5) Lower Mandy Creek Area

Samples (#192-195) collected from this area returned anomalous values in Au  $\pm$  As.

#### iv) Placer's and Kenrich's Program (Maps 1-24)

a) Silt Sample Results

Results from the previously collected silt samples identified four general areas of anomalous, multi-element values (see Figure 5). These areas are as follows:

#### 1) Northwestern portion of the property

Scattered anomalous values in gold (to 225 ppb), silver (1 to 8 ppm), arsenic (134 to 256 ppm), molybdenum (to 50 ppm), lead (to 36 ppm), zinc (to 565 ppm) and cadmium (to 4.1 ppm) were obtained from the creeks draining this area.

#### 2) Southwest of Mount Madge

The two small creeks which are located west of Mount Madge and drain into the Unuk River display numerous anomalous values in barium and/or silver (to 8.1 ppm), arsenic (to 178 ppm), lead (to 60 ppm), zinc (to 543 ppm) and cadmium (to 3.4 ppm). Further south, several of the creeks draining into the Unuk River displayed scattered, anomalous values in gold (to 1,292 ppb), antimony (to 40 ppm), bismuth (to 9 ppm) and lead (to 41 ppm).

#### 3) The Area of the Elgar Showing

One of the creeks draining the area of this showing displayed a large number of multielement anomalies. These include antimony (to 18 ppm), molybdenum (to 40 ppm), lead (to 35 ppm), zinc (to 677 ppm), cadmium and barium. Three anomalous gold values (to 790 ppb) were also obtained from a creek to the northeast of the Elgar showing.

#### 4) East of Mount Madge

Most of the creeks draining this area returned anomalous values in gold (to 680 ppb), as well as some in arsenic (to 130 ppm), bismuth (to 9 ppm), zinc (to 738 ppm), cadmium (to 4.3 ppm) and barium.

In addition to the above areas, numerous multi-element anomalies were obtained from the vicinity of the C-10 showing. These include gold (to 1,500 ppb), silver (to 5.1 ppm), arsenic (to 311 ppm), molybdenum (to 29 ppm), copper (to 5,619 ppm), lead (to 83 ppm), zinc (to 518 ppm), cadmium (to 3.5 ppm) and barium.

#### b) Rock Sample Results

The majority of anomalous rock sample results are from areas of known mineralization. These showings include the Silver Creek, the C-10, the Tet, the Mandy Glacier and the GFJ (see Figure 5). The samples from the C-10 showing returned anomalous values in Au and/or Ag  $\pm$  As, Sb, Bi, Cu, Cd. The highest gold result was 5,440 ppb. In the Silver Creek area, anomalous results in Ag and Sb  $\pm$  Pb, Zn, Cd were obtained. Anomalous values in Au, Ag, Sb, Bi, Cu, Pb  $\pm$  Zn, Cd were returned from the Tet showing. The highest gold result was 3,775 ppb. The samples from the GFJ showing returned anomalous values in Au, Sb and Pb  $\pm$  As, Bi, Cu, Cd, Zn. The best gold result was 57,460 ppb. A sample from the area of the Mandy Glacier showing returned anomalous Au, Ag, Bi and Cu values. The gold result was 31,874 ppb.

In addition to the above showings, three other areas of interest were revealed. To the northeast of the GFJ showing, two samples from a gossan returned anomalous values in Au, Ag, Bi  $\pm$  Pb. The best result was 55,000 ppb Au. To the north of the GFJ, three anomalous values in Au, As  $\pm$  Sb were obtained. The highest gold was 2,450 ppb. The third area of interest is southwest of Mount Madge where two samples returned anomalous, up to 6,052 ppb, gold values. A few scattered, single element Ba, Sb, Pb and Zn anomalies were also returned from other parts of the property, south of Sulphurets creek.

#### c) <u>Silver Creek Grid</u> (Figures 9 and 10)

Rock and soil sample results are at background levels for gold. The soil samples' silver results revealed several anomalous values on the north end of the grid. Values of up to 7.7 ppm Ag were received. The only significant rock result was from sample number 18007 which returned 3,473 ppm Ag.



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#### **CONCLUSIONS**

The reconnaissance mapping completed by Homestake and Kennecott, in the northwestern portion of the Corey property, appears to confirm the MDRU's recent geological interpretation. The MDRU believes that the prospective "Eskay Creek strata", which consist of basaltic and minor amounts of sedimentary rocks of the Salmon River Formation and felsic volcanics of the Mt. Dilworth Formation, traverse, north-south, through the property.

Although the preliminary, exploration work performed by Homestake, Kennecott and Inco did not reveal any, significant rock sample results, the presence of very prospective strata and the lack of detailed exploration over such a large property indicate a need for further work. This is quite evident when reviewing the results obtained from samples collected from creeks draining the Corey property.

The re-analysis of the previously collected silt samples by Placer Dome revealed 4 areas which require follow-up work. Numerous single and multi-element anomalies were obtained from creeks which drain these areas. Two of these areas are not, as yet, know to host any significant mineralization. The silt-moss mat-heavy mineral concentrate sampling program conducted by Homestake generally confirmed the values obtained by Placer. The Homestake results also indicate one additional area of interest. Results from the limited number of samples collected in the southern portion of the property are at background levels.



#### **RECOMMENDATIONS**

It is recommended that the Corey property be subjected to an exploration program that would focus, primarily, on the prospective Eskay Creek strata. This program must take into account preliminary, high elevation snow cover and should include:

- 1. completion of a compilation of all available data on prepared topographic base maps (1:10,000 and 1:5,000).
- 2. helicopter reconnaissance over the entire property in order to establish possible landing spots for crew put-outs and pick ups. This will help to determine possible traverses during the field program.
- 3. establishment of a grid in northwest portion of the property (north of Sulphurets creek) to provide control for geological and geochemical surveys. This work should cover the prospective Eskay Creek strata.
- 4. follow-up of all unexplained, sediment anomalies obtained by Placer Dome and Homestake. These include the northwest portion of the property (as described above), the area southwest of the Mount Madge, the area east of Mount Madge, the Elgar showing area and the lower portion of Mandy Creek. This work should include contour and creek traverse prospecting, geological mapping and geochemical sampling. Strategically placed control-base lines should be contemplated in the areas below treeline.
- 5. prospecting, geological mapping and silt sampling of the prospective Eskay Creek strata in the southern half of the property. This should be done later in the field season when the snow cover is gone.
- 6. prospecting and mapping in the area of all known mineralization, including possible mesothermal vein and porphyry targets.
- 7. prospecting and mapping of any unexplored portions of the property, as time and budget restraints permit.
- 8. a provision made for trenching of any showings which might be discovered during the above program.

Respectively submitted,

Rex Pegg, P. Eng., BASc



#### **BIBLIOGRAPHY**

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- Placer Dome Exploration Limited (1992): Compilation of results from re analysis of geochemical samples previously collected from the Corey property.

#### APPENDIX 1 : STATEMENT OF QUALIFICATIONS

I, REX STEPHEN PEGG, of #1 - 410 Mahon Avenue in the District of North Vancouver in the Province of British Columbia, do hereby certify that:

- 1. I am a graduate of the University of Toronto, BASc. (1976) in Geological Engineering (Exploration option) and have practiced my profession continuously since graduation.
- 2. I have over 16 years of experience in exploration for precious and base metals in the Canadian Cordillera.
- 3. I am a member in good standing of the Association of Professional Engineers of British Columbia.
- 4. I am an independent consulting geologist with an office at #800 900 West Hastings Street, Vancouver, British Columbia.
- 5. I am the author of the report entitled "Geochemical and Geological Report on the Corey Property, Skeena Mining Division, British Columbia", dated May 5, 1993.
- 6. Although I have not visited the property, I am familiar with the regional geology and the geology of nearby properties.
- 7. I do not own or expect to receive any interest (direct, indirect or contingent) in the property described herein nor in the securities of either Kenrich Mining Corp. or Ambergate Explorations Inc., in respect of services rendered in the preparation of this report.
- 8. I consent to and authorize the use of the attached report and my name in the Companys' Statement of Material Facts or other public document.

Dated at Vancouver, British Columbia this 5th day of May, 1993

Respectfully submitted,

Rex S. Pegg, BASc., P.Eng.

#### STATEMENT OF QUALIFICATIONS

I, DAVID L. TRUEMAN, of the City of Vancouver, in the Province of British Columbia, Canada, do hereby certify that:

- 1) I am a graduate from the University of Manitoba with a B.Sc. (1970), M.Sc. (1971) and Ph.D. (1980).
- 2) I have practised my profession in the mining business for approximately 30 years. My experience includes academic, government and industry and includes geological, geophysical and geochemical exploration of precious and base metal, rare metal and industrial mineral deposits, project initiation, mine production, metallurgical research, project feasibility and project finance.
- 3) I am a Professional Engineer and have been registered in the Province of Manitoba since 1973.
- 4) I acted as a consultant for Kenrich Mining Corp. and Ambergate Explorations Inc. with regards to the 1992 Corey property work.

mbia, Canada this, 5th day of May, 1993.
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Att D.L. MAN
ATPLIEMAN /
- All Chings
David L. Trateman, Ph.D., R.Eng.
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Dated at Vancouver, British Columbia, Canada this, 5th day of May, 1993.

#### **APPENDIX 2 : <u>SUMMARY OF FIELD PERSONNEL</u>**

1. Kennecott Canada Inc.

S. Bishop, Geologist Aug K. Curtis, Geologist June H. Smit, Geologist June

August 13 & 15, 1992 June 23 - 25, 1992 June 23 - 25 and August 13 & 15, 1992

2. Inco Exploration and Technical Services Inc.

J. Morin, Geologist	August 20, 1992
D. Slauenwhite, geologist	August 20, 1992

3. Homestake Canada Ltd. (48 man days from July 15 to Aug. 31, 1992)

John Belamy, geologist Carl Edmunds, geologist Paul Jones, prospector Dave Kuran, geologist Henry Marsden, geologist Ken Rye, geologist

A CALLAND CONTRACT CONTRACT 1. Sec. 1.

## **APPENDIX 3 : <u>STATEMENT OF EXPENDITURES</u>**

## 1. Kennecott Canada Inc.

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i) Labour			
H. Smit	2.5 days @ \$ 450/day		\$ 1,125.00
K. Curtis	1.5 days @ \$ 450/day		<b>\$</b> 675.00
S. Bishop	1.0 days @ \$ 450/day		\$ 450.00
ii) Transportation			
truck	735 km @ \$ 0.32/km		\$ 235.00
gas			<b>\$</b> 104.00
helicopter	3.5 hrs. @ \$ 850/hr.		\$ 2,975.00
iii) Room & Board 8 m	an days @ \$ 150/ day		\$ 1,200.00
iv) Geochemical Analysi	is		
rocks	36 samples @ \$ 20 each		<b>\$</b> 720.00
silts	1 samples @ \$ 20 each		\$ 20.00
		Sub Total:	\$ <u>7,504.00</u>
Inco Exploration and Te	echnical Services Inc.		
i) Labour	<b></b>		¢ 500.00
J. MORINI I G	ay $(a)$ \$500/day		\$ 500,00
D. Sladeliwi	nie 1 day @ \$300/day		\$ 500.00
ii) Helicopter ( Stewart t	to the property, return )		\$ 1,887.21
iii) Room & Board 2 m	an days @ \$80/day		<b>\$</b> 160.00
iv) Geochemical Analys	is		
rocks	6 samples @ \$ 35.03 each		\$ 210.18
		Sub-Tota	1: \$ <u>3,257.39</u>
Homestake Canada Ltd.			
i) Labour	48 man days @ \$ 400/day		\$19,200.00
ii) Helicopter	5 hrs. @ \$ 850/hr		\$ 4,250.00
iii) Room & Board 48	man days @ \$ 70/day		<b>\$</b> 3,360.00

	iv) Geochemical Analysis		
	whole rock	93 @ \$ 40.50 each	\$ 3,766.50
	rock	101 @ \$22.60 each	\$ 2,282.60
	silts	86 @ \$17.85 each	\$ 1,535.10
	moss mats	87 @ \$ 17.85 each	\$ 1,552.95
	heavy minerals	83 @ \$ 17.85 each	\$ 1,481.55
		Sub-Total:	\$ <u>37,428.70</u>
4.	Placer Dome Exploration Limite	2 <u>d</u>	
	i) Portion of the packing and ha	ndling of pulps (Calgary to Vancouver)	\$ 2,599.00
	ii) Geochemical Analysis (27 ele	ement ICP)	
	1,104 samp	les @ \$ 6.34 each	\$ 6,999.36
	iii) Portion of the consulting fee	s (plotting and evaluation of results)	\$ 7,904.21
		Sub-Total:	\$ <u>17,502.57</u>
5.	Kenrich Mining Corp.		
	i) Portion of the packing and ha	ndling of pulps (Calgary to Vancouver)	\$ 5,339.00
	ii) Portion of the consulting fees	(plotting and evaluation of results)	\$ 4,007.50
	iii) Consulting fees (Dave Truer	nan, P.Eng 44.55 days @ \$330/day)	\$14,700.00
		Sub-Total	\$ <u>24,046.50</u>
6.	Compilation and Report Writing		\$ <u>8,000.00</u>

GRAND TOTAL: \$97,739.16

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APPENDIX 4

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Sample Locations, Descriptions and Results - Inco Exploration

## DESCRIPTION OF SAMPLES AND CHEMICAL ANALYSES

	Au pob	Ag DDM	Zn pom	Pb ppm	Cu ppm	Ba pom
RX051237	Cumberla	nd showing:	adit porta fine grain 2% sulp carbonate	al; grab sample ned massive inten- phide stringers and large patcl	of light grey crmediate volca associated volca nes of fine grad	green very anic with ~ with quartz ined chlorite
	2430	17.2	32747	2504	2072	40347
RX051238	Cumberla sulphide	nd showing: a	dit portal; chip	sample across 4	0 cm of weathe	ered massive
	6030	114.5	231000	99999	10319	114421
RX051239	Cumberla	nd showing:	adit port: laminated	al; chip sample 1 sulphides	across 50 cm	of distinctly
	3350	99.8	239000	1691	13814	290980
RX051240	Cumberla	and showing:	adit port barite	al; chip sample	across 50 cm	of massive
	1156	91.4	149000	78236	6901	341939
RX051241	Cumberla	and prospect:	grab sar quartz co	nple of andesi ollected about 6	te with 15% 2+50 N and 1	chalcedonic 50 m SW of
	75	0.9	1390	163	142	2510
RX051242	Cumberla	and prospect:	grab sar collected	nple of andesit l on base line	te/basalt aqua about 300	gene breccia m south of
	44	2.2	2180	1036	174	1811



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ME MELYT ..... LA. TOKANA LTL.

GEOCHEMICAL ANALYSIS CERTIFICATE

Inco Expl. & Tech. Services PROJECT 60500-80001 File # 92-2779 Page 1 2690 - 666 Burrard St., Vancouver BC V6C 2X8 Submitted by: MARK SLAUENWHITE

CAMPIER	Mo	<u> </u>	Dh	7.0	<b>A</b> a	N4	<u> </u>	Mo	Fa	<b>A</b> .		<u>Au</u>	Th Sr		Sb	Rí V	<b>.</b>	p	1.	Cr.	Ma	84	T1	A1	Na	r		7-	Sn	¥	Nb	8.	Se.	Au*
JANFLER	DDM DDM	200	000	DDM	DOM	DDM	200	DDM		DDB		DOM	ADG ROG	pro-	Dom I	DDM DDM	. X	x	DDM	DOM		DDM	*	*	*	X	200	en Domen	DDM	D DR	DOR D		94 DØ	sob
																											PP 1							<b></b>
RX 051220	1	59	28	188	2.9	6	6	660	5.06	4	5	ND	1 391	.2	2	2 632	1.21	.011	2	23	2.33	355	. 30	8.47	. 90	3.24	5	6	1	7	3	1 21	.1	64
RX 051221	156	304	4386	129	12.1	12	31	209	2.38	4	5	ND	1 889	.2	2	3 500	.94	.077	2	12	1.24	721	. 50	8.03	1.29	3.29	7	10	1	18	1	1 37	.7	25
RX 051222	1	126	- 4	70	2.9	9	23	545	3.67	34	5	ND	2 129	.4	2	2 408	1.01	.038	2	17	.05	254	. 59	11.09	2.28	8.11	8	3	1	8	1	1 37	.6	14
RX 051223	1	249	31	249	3.8	75	89 2	2620	9.14	5	5	ND	1 204	.2	2	2,211	2.51	.068	- 4	213	2.65	144	. 50	8.58	2.22	3.50	2	2	1	17	1	1 32	.1	156
RX 051224	1	33	12	80	.2	45	26 1	556	5.95	4	5	ND	1 308	.2	2	2 300	6.77	.042	- 4	200	4.72	1066	. 38	7.80	2.38	.24	2	8	1	13	1	1 33	.2	51
RX 051225	1	53	9	95	. 6	44	12 1	1251	5.59	- 4	5	ND	1 298	.2	2	2 233	4.83	.119	10	80	2.69	6385	.49	7.23	1.63	1.68	2	20	2	24	2	1 24	.6	5
RX 051226	1	825	4	52	.2	9	21	375	5.19	4	5	ND	1 17	.2	2	2 194	. 12	.065	3	40	2.39	374	. 22	7.18	. 26	2.97	2	9	1	3	1	1 16	.2	10
RX 051227	1	17	31	36	.2	8	1	375	.80	13	5	ND	15 57	.2	2	2 3	.41	.008	43	10	.11	1351	.08	6.74	2.96	3.98	2	69	1	11	12	22	.8	3
RX 051228	1	30	511	205	3.9	22	12 3	1882	5.04	6578	5	ND	1 350	.9	36	2 121	15.79	.066	5	39	1.03	764	.14	7.68	.08	3.92	2	15	1	11	1	1 11	.9	304
RX 051229	1	471	99999	39034	83.1	33	22	447	15.97	79	5	ND	3 14	340.3	162	10 95	.33	.051	2	2	. 59	262	. 18	4.92	.06	2.53	2	8	1	5	1	6 B	.1	48
														_													_	_	_				_	-
RX 051230	1	128	199	303	1.4	23	17	926	5.43	7	5	ND	3 246	.8	11	2 231	1.00	. 142	9	43	1.90	544	.51	8.80	1.11	5.36	2	8	1	10		1 17	.3	5
RX 051231	16	301	422	2437	7.4	23	12 1	005	9.53	104	5	ND	3 104	22.7	18	6 131	1.44	.059	4	29	.89	179	.27	6.47	.31	3.03	5	9	1		1	1 11	.5	25
RX 051232	1	36	29	121	. 3	96	27 1	069	6.35	403	5	ND	1 403	.2	Z	2 193	3.23	.264	32	152	4.11	1493	.84	8.14	2.54	2.41	2	42	1			1 20		
	1	1633	6885	38076	49.4	24	55 2	475	17.37	820	5	ND	1 126	432.7	40	30 40	4.17	.009		1		240	.02	2.20	. 19	1.07			-		2	• J	.,	12
	1	45	51	489	.9	171	43 2	804	5.90	8	5	ND	2 1/0	1./	2	3 203	0.40	.084	¢	334	0.41	100	. 40	0.24	4.4/	1.33	3	**	•	**	"	1 31	• •	16
LOREY		••		**	~	12	•	110	1 83	2				2	2	2 42	.04	.008	11	50	. 63	903	. 13	1.93	.03	. 59	2	10	1	4	1	1 6	. 5	6
	1	31	18	03 83		14		110	6 59	3 20	5	ND	2 312	.2	2	2 316	5.82	.115	;	136	5.15	206	.51	7.17	2.38	.69	2	10	1	16	i	1 41	.2	9
KA US1230		2072	22 9604	19747	17.2	15	13 1	046	7.77	234	5	ND	2 12	122.0	10	3 233	1.36	. 160	5	1	2.64	1868	1.15	6.41	.09	3.56	70	73	1	39	8	1 21	.3 2	430
RK 031237	40	10310	00000	00999	114.5	17	7	683	9.19	88	5	3	3 14	1098.0	88	2 53	.18	.018	2	1	.20	194	.06	. 57	.04	.12	2	5	1	3	1	1 3	.0 6	030
BY 051239	28	13814	1691	99999	99.8	11	i	331	7.36	152	5	ND	1 24	1058.6	80	8 15	.03	.004	2	1	. 02	156	.01	.20	.03	.01	2	1	2	1	1	1	.2 3	350
AA UJIEJJ							-				-			-																			·	
BX 051240	10	6901	78236	99999	91.4	13	1	202	4.43	47	5	ND	1 24	575.8	79	2 10	.06	.003	2	1	.06	174	.01	. 19	.04	.01	2	1	1	1	1	1	.3 1	156
RX 051241	1	142	163	1390	.9	263	53 1	193	6.30	5	5	ND	1 224	4.2	2	2 236	6.40	.039	2	561	7.88	2009	. 53	7.64	1.36	1.09	2	38	1	19	1	1 36	.0	75
RX 051242	1	174	1036	2180	2.2	213	50 1	141	6.10	4	5	ND	1 169	8.6	2	2 248	6.93	.030	2	429	6.17	1378	. 52	7.60	2.09	.25	2	29	1	20	1	1 37	. 2	44
RX 051243	27	110	71	1160	.7	26	3	437	2.46	11	5	ND	2 244	5.2	2	4 180	2.32	.064	13	45	1.13	3868	. 46	7.31	1.21	3.97	2	55	3	35	6	1 21	.6	7
RX 051244	8	60	663	6439	1.2	11	5 4	611	6.37	37	10	ND	1 525	15.9	4	2 100	21.57	.042	3	12	2.47	202	. 12	2.03	. 10	.06	17	20	1	11	1	15	.4	6
RX 051245	1	17	106	215	.2	7	1	178	1.20	18	5	ND	4 71	1.0	2	29	.35	.010	25	18	. 30	2273	.14	6.53	2.43	4.34	2	23	1	11	13	1 2	.2	13
RE RX 051241	1	133	128	1271	.7	269	53 1	208	6.36	- 14	5	ND	1 227	3.4	2	2 239	6.27	.039	2	557	7.69	1880	.54	7.63	1.37	1.05	2	39	1	18	1	1 36	.6	103
RX 051246	2	26	18	96	. 3	26	14	522	4.34	18	5	ND	2 135	.2	2	2 101	2.82	.016	7	37	3.51	688	. 34	7.25	1.70	1.69	2	39	1	12	1	1 20		
RX 051247	2	16	- 44	240	.2	8	1	181	.97	7	5	ND	2 77	. 5	2	2 33	.67	.050	25	50	. 16	2725	.06	6.29	2.40	4.48	2	22	1		•	2 1		
RX 051248	36	49	113	311	.2	25	7	507	3.27	129	5	ND	1 148	1.0	2	2 67	1.87	.026	11	34	3.05	1489	.23	6.79	1.41	1.84	2	<b>P1</b>	1	'	č	2 10	•¥	3
												_		_					•		26			13	01		•				1	,		,
RX 051249	7	13	16	43	.2	4	1 1	279	.42	7	5	ND	1 233	,2	2	2 1	14.94	.010	2		.23	320	.01	- 15	1 24	01	-	21		16	;	1 10	1	,
RX 051250	5	31	24	70	.4	47	20	649	6.15	85	5	ND	1 121	.2	3	2 /0	3.39	.009	•	27	3.35	520	.20	7.19	1.69	1 2 02	-	15		20	÷	1 16		10
RX 051251	1	92	10	209	.9	11	9	937	6.38	36	5	ND	1 276	.3	2	2 187	.64	. 128	3	8	1.72	3/0	. 35	9.00	2.00	2.92	-	15		3		1 12		29
RX 051252	13	137	- 4	81	.7	6	7	362	6.60	17	5	ND	1 108	.2		2 196	.23	.12/	-		1.45	031	. 35	10.04	1.79			17		-	•	1 16		100
RX 051253	40	178	160	57	2.9	7	7	442	5.36	81	5	ND	29	.2	13	6 201	.29	.114	3	7	1.17	1010	. 30	ő.y/	.02	9.98	11	17	+	•		1 13	• *	130
					_	_	_				_			-		0 000			~		60	1176	40	10 60	67	6 36	•	17	•	3	1	1 17	.7	60
RX 051254	5	158	4	71	.8	6	2	348	6.22	19	5	NO	1 18	.2	•	2 224	12 26	.13/	2	20	. 90	421	. 40	3.40	2.30	40.40	•	*/	1	13	,	1 8	.8	3
RX 051255	1	19	6	42	.2	6	31	326	1.82	9	5	UN T	1 354	.2	2	22 52	14.JO 20	122	30	20 60	.00	240	.08	2.06	- 10	17	10	Ă	15	7		1 5	.5	497
STANDARD HFC/AU-R	19	66	42	129	6.6	92	45 )	274	4.59	40	21		00 66	0.13	10	~~ 04	. 58	. 123		00	. 37							-			<u> </u>		1.7 - 4	
											_				-							40 M					850			10.1	CACU			

ICP - .500 GRAM SAMPLE IS DIGESTED WITH 10ML HCLO4-HNO3-HCL-HF AT 200 DEG. C TO FUMING AND IS DILUTED TO 10 ML WITH DILUTED AQUA REGIA. THIS LEACH IS PARTIAL FOR MAGNETITE, CHROMITE, BARITE, OXIDES OF AL, ZR & MN AND MASSIVE SULFIDE SAMPLES. AU DETECTION LIMIT BY ICP IS 3 PPM. AS, CR, SB SUBJECT TO THE LOST OF VOLATILIZATION DURING HCLO4 FUMING.

AU\* ANALYSIS BY ACID LEACH/AA FROM 20 GN SAMPLE. Samples beginning 'RE' are duplicate samples. - SAMPLE TYPE: ROCK

- SIGNED BY DATE RECEIVED: AUG 25 1992 DATE REPORT MAILED:

		the detector	<u></u>	
	No. 40 10 10 10 10 10 10 10 10 10 10 10 10 10	· · · · · · · · · · · · · · · · · · ·	MON	TIME
ALME	ANALITICAL	LADURA	IUKILƏ	وم الالاسلام
	N 1 1 1 1 1 7 7 7 7 7 1 1 1 1 1 1 1 1 1	0.252575757575757	アンジェンシュ	20 <del>23 2003</del> 20

834 E. haalINGa af. VANLOUVER B.C. VOA IND FAUNE(004)253-3158 FAX(604)253-1110

Page 1

WHOLE ROCK ICP ANALYSIS

Inco Expl. & Tech. Bervices PROJECT 60500-80001 File # 92-2779 2690 - 666 Burrard St., Vancouver BC V6C 2X8 Submitted by: MARK SLAUENWHITE

	1								- 3-6		0-207	D.s.	<b>6</b>	7-		6-	6-	7.0	<u> </u>		Nb		101	ĊI M	
SAMPLE#	\$102	AL203	Fe203	MgC	CaO	Nazo	K20	1102	P205		Crzus	88	LU	2R			<u>ər</u>	21	Le		RO	10	LUI	30M •	
	×	<u> </u>	X	<u>X</u>		*	X	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		<u> </u>	*	ppm	ppm		<u>sppn</u> e	ppm	ppm	ppm	ppii		ppm	рри		^	_
PX 051220	28.26	12.66	6.95	2.24	1.49	.90	2.60	.33	.02	.06	.005	229157	28	103	23	106	3861	23	20	5	9	20	4.9	99.86	
BY 051220	1/2 17	12 40	3 46	1 24	8 85	1 37	2 75	65	14	02	002	184414	205	73	25	108	2819	22	20	10	5	20	3.0	99.84	
KA UJIZCI	57 00	31 77	1.54	1 1/	432	2 24	6 3/	76	08	់កំខ	002	2562	64	78	8 K	23	134	65	20	10	5	20	3.9	99.99	
KX UD1222	127.00	21.3/	4/ 37	7 00		2 01	3 70		14		072	1841	205	237	70	86	252	72	44	10	17	20	4.8	99.90	
RX U51223	40.07	19.02	14.21	3.90	87.74 1917	3.01	3.17	.07	. 10		072	1071	205	45	276	25	227	44	20	8842 ·	5	20	1 0	00 01	
RX 051224	53.46	16.13	8.84	6.79	8.03	3.37	.13	•01	.14	Ç, ÇV	.032	1240	2	63	80.4	23	331	44	27			20	1.7	//.//	
			A /7	7 00				1 00	70	×.2	017	7127	5	78	20	24	331	127	41	25	21	20	25	00.04	
RX 051225	57.48	14.69	8.45	3.88	0.33	2.21	1.20	1.00	.30		.013	7/4	707	70	844	2/	251	97	62	8 6	17	20	5 1	00 06	
RX 051226	61.83	16.92	7.62	3.04	, ZU		3.24	.70	• If		.005	(40	171	20			E/	177			11	20	7.1	00 06	
RX 051227	77.26	12.71	.81	.15	8, <b>4</b> 5	3.92	5.90	.10	.02	- 14	.002	1224	Ž	21	\$\$ <b>.</b> ]		24	133	24		46	20	12.0	00.95	
RX 051228	33.88	16.25	8.17	1.56	19.75	.15	4.53	.50	.17	.55	.005	1501	2	220	<u></u>	10	404	94 407	02		12	20	14.0	77.0J	
RX 051229	37.95	9.61	23.88	.88	.40	.08	2.74	.30	.11	.06	.003	895	345	38625		25	- 17	105	62		10	20	11.1	92.13	
										88.88						••			~~			20		00.00	
RX 051230	55.50	19.29	7.91	2.85	1.34	1.45	5.83	.66	.33	<b>21</b> 2	.002	2917	78	438	893 (	21	208	00	22		16	20	4.0	99.9U	
RX 051231	58.42	12.26	14.31	1.38	1.83	.36	3.03	.39	. 16	<b>.12</b>	.002	1191	244	2403	8 <b>2</b> 18	15	107	87	24		14	20	0.0	<b>YY.03</b>	
RX 051232	48.51	16.33	10.47	6.54	4,35	3.64	2.69	1.39	.68	, 15	.024	1724	52	160	91	25	425	157	141	20	21	20	4.7	99.90	
	35.47	4.83	31.20	.48	6,32	.24	.62	.04	.04	34	.003	371	841	43244	27	55	134	39	66		5	20	8.7	95.87	
	44.80	11.74	8.49	12.66	7.96	1.95	1.62	.63	.23	.36	.050	239	7	644	140	36	178	85	36	10	15	20	9.2	99.88	
COKEY				-						\$\$C\$															
•	190.40	3.52	2.75	-90	12	.05	.47	.20	.04	.01	.006	697	5	53	9	5	10	78	28	7	5	20	1.4	99.99	
	48 01	13.87	10.54	11.00	8.56	3.38	.24	.80	.31	13	.024	457	45	200	56	35	322	65	20	<b>314</b>	5	20	2.0	99.93	
T BY 051227	42 41	12 08	10.82	4.35	1 79		3.74	1.61	.42	214	-002	40347	1012	34417	16	30	37	152	89	60	20	20	5.7	95.39	
BY 051238	3 43	1 00	13 46	30	27	.05	.05	.08	.03	.08	.007	114421	2869	187266	24	61	339	23	20	5	5	20	16.1	78.12	
RA 051250	1 17	1.00	0 33	01	<u> </u>	05	.05	.01	.01	04	.005	290980	3703	115696	24	127	2001	5	21	88 S .	5	20	12.1	87.59	
	1.13		7.33							1258				•••											
BY 051240	81	32	5.12	.05	.09	.05	-05	.01	.01	.D2	.006	341939	1428	115493	37	154	2048	5	20	S. 5	5	20	7.7	87.10	
DV 051240	44 04	17 00	8.87	16.18	7 81	1.70	1.22	.81	.11	.15	.103	2510	89	1556	208	44	224	31	20	16	14	20	4.1	99.71	
DV 051247	16 53	16 35	R 07	12 77	A 61	2.79	.07	.82	.08	×15	.079	1811	105	2135	175	41	173	21	31	817	17	20	3.7	99.56	
KA 051242	40.00	16 12	7 48	2 08		1 48	3 86	-64	.17	06	.009	3955	59	1276	29	7	233	110	27	31	13	20	5.6	99.83	
RA UJ1243	77 /4	/ 20	40.24	1 07	20 25	1/	05	18	13	22	002	2615	30	7255	819	5	627	70	20	9	5	20	10.1	98.98	
RX U51244	31.40	4.20	10.20	4.07	<b>7</b>	. 14	.0,	. 10	. 13		1006	2015				-		• -							
	74 35	43 04	4 20	1.9	20	2 05	5 17	18	02	ິກຊິ	.002	2125	5	215	10	5	62	212	72	66	7	20	.8	99.96	
KX UJ1243	10.23	12.00	0.00	15 10	332	1 71	1 08	A1	10	816).	103	2303	72	1211	204	42	218	38	20	<b>15</b>	12	20	4.1	99.77	
RE KX U51241	147.10	14.03	9.04	13.17		2 40	4 70	.01	. 10	842	003	1080	5	100	27Å	11	131	105	20	21	5	20	3.9	99.99	
RX 051246	62.30	12.91	0.C	3.70	2. <u>2</u>	2.10	1.10	15		8.2	.00.	25/1	ś	234	877	5	68	195	46	<u>851</u>	6	20	1.1	100.02	
RX 051247	77.45	11.26	.97	.30		2.01	4.41	. 15	. ! !	842	-004	4//2	75	247	83 A	ś	128	112	44	ň¢®	5	20	3.6	99.96	
RX 051248	68.52	12.21	4.27	4.71	2.45	1.55	1.75	.49	.07	- 00	.002	1446	22	203	8 <b>. E W</b>		120	112				F	310		
					888.3		<b>A</b> 5			88 Q	003	71	6	24	28 P	5	216	33	20	<b>.</b>	5	20	16.3	100.21	
RX 051249	63.92	.37	.47	.45	10.44	.05	.05	.01	.02	.12	.002	1025	2	20	22	17	111	7/	20	20	Ę	20	4.4	00.00	
RX 051250	61.19	12.83	8.41	5.15	4.36	1.44	1.41	.49	.01	<b>00</b>	.002	1023	2	21/	29	4	270	20	20	×7	17	20	4 4	00.05	
RX 051251	154.30	19.63	9.44	2.91	.93	5.58	5.24	.48	.50	414	.002	2005	22	214 425	- See See See See See See See See See Se	C F	407	27	20		17	20	5 0	40 00	
RX 051252	55.17	19.62	9.27	2.45	<b>8435</b>	2.13	4.91	.51	.29	S.N.S.	.002	705	97		88 <b>-</b> 2	7	107	20	20		44	20	5.2	A0 00	
RX 051253	61.16	17.02	7.40	1.96	.38	.05	5.86	.41	.23	. 05	.002	1289	118	40		2	10	22	20		10	20	3.5	77.70	
																-	40	74	30		47	20		00 07	
RX 051254	55.84	20.70	8.34	1.67	.29	.09	6,38	.54	.28	.05	.002	1564	83	42	88 Ú	Ž	18	31	20		11	20	2.7	77.7/	
RX 051255	57.15	6.89	3.07	1.13	16.96	2.85	1.05	. 18	. 12	17	.003	4622	5	14	13 A	2	360	34	20	212 12	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	20	7.0	100.01	
STANDARD SO-4	69.15	10.20	3.44	.93	1.48	1.29	2.04	.55	.21	<b>. 07</b>	.006	805	22	92	88 <b>25</b> 8	5	199	507	23	<u> </u>	14	_20	10.4	100.00	_

.200 GRAN SAMPLES ARE FUSED WITH 1.2 GRAM OF LIBO2 AND ARE DISSOLVED IN 100 MLS 5% HNO3.

Samples beginning 'RE' are duplicate samples - SAMPLE TYPE: ROCK

DATE RECEIVED: AUG 25 1992 DATE REPORT

SIGNED BY

# ACTIVATION LABORATORIES LTD

_4423 ×
4449
21-SEP-92
08-SEP-92
92-2779
514

INCO-VANCOUVER INCO EXPLORATION & TECH. SERV. INC. 2 90-666 BURRARD STREET VANCOUVER, BRITISH COLUMBIA VAC 2X8 A TN: PHIL RUSE

ACTLABS

CERTIFICATE OF ANALYSIS

TAA package, elements and detection limits:

DA	5.	PPB	AG	5.	PPM	AS	2.	PPM	BA	100.	PPM
"R	1.	PPM	CA	1.	8	CO	5.	PPM	CR	10.	ppm
S	2.	PPM	FE	0.02	*	HF	1.	PPM	EG	1.	PPM
IR	5.	PPB	MO	5.	PPM	· NA	500.	PPM	NI	50.	PPM
RB	30.	PPM	SB	0.2	PPM	SC	0.1	PPM	SE	5.	PPM
N	0.01	8	SR	0.05	*	TA	1.	PPM	TH	0.5	PPM
ú	0.5	PPM	W	4.	PPM	ZŅ	50.	PPM	LA	1.	PPM
CE	3.	PPM	ND	5.	PPM	SM	0.1	PPM	EU	0.2	PPM
Έ	0.5	PPM	YB	0.05	PPM .	LU	0.05	PPM			

CERTIFIED BY :

Pages Total of

Activation Laboratories Ltd. Work Order: 4449 Report: 4423

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Sample description	AU	λG	AS	ВА	BR	CA	C0	CR	CS	FB	HF	ĦG	IR	ю	NA	NI	RB	SB	SC	SE	6N	SR	ТА	TH
	PPB	PPN	PPM	PPM	PPH	8	PPN	PPM	PPH	t	PPH	PPM	PPB	PPM	PPM	PPM	PPM	PPM	PPM	PPN		•	Pra	rra
RX-051220	66	<5	51	70000	<1	<1	6	25	<2	4.64	<0.5	<1	<5	<5	6910	<50	76	1.0	18	<5	<0.02	0.53	_ <1	<0.5
RX-051221	25	<5	91	40000	<1	<1	22	12	<2	2.66	<0.5	<1	<5	71	10000	<50	43	1.9	29	<2	<0.02	0.44	4	1.7
RX-051222	13	<5	79	1800	<1	<1	20	16	<2	2.93	2.0	<1	<5	<5	15500	<50	80	3.8	35	< 5	<0.02	<u.05< td=""><td>3</td><td>0.9</td></u.05<>	3	0.9
RX-051223	153	<5	26	1800	<1	<1	72	190	- 4	0.15	3.2	<1	<5	<5	20600	<50	54	1.3	36	<5	<0.03	<0.05	<1	1.5
RX-051224	<5	<5	<2	1000	<1	6	22	210	<2	5.39	2.2	<1	<5	<5	22600	<50	<30	0.7	32	<5	<0.02	<0.05	<1	1.0
RX-051225	<5	<5	3	6300	<1	4	13	76	<2	5.37	4.1	<1	<5	<5	16400	<50	<30	1.6	24	<5	<0.02	<0.05	<1	2.2
RX-051226	14	<5	3	590	<1	<1	19	30	<2	4.76	1.7	<1	<5	<5	2580	<50	40	0.4	25	9	<0.02	<0.05	<1	2.9
RX-051227	<5	<5	11	1000	<1	<1	<5	<10	<2	0.72	4.1	<1	<5	INT	28200	<50	<30	1.1	2.6	<5	<0.02	<0.05	<1	18
RX_051228	313	<5	40000	1400	<2	<5	12	38	5	5.39	2.5	<1	<5	<5	1820	<50	<100	74	13	<5	<0.03	<0.05	<1	2.9
RX-051229	179	110	B50	750	<1	<1	23	17	4	15.2	1.8	<1	<5	<5	571	<50	<30	130	7.5	24	<0.03	<0.05	<1	2.2
PX-051330	<5	<5	15	2500	<1	<1	16	34	6	4.77	2.9	<1	<5	<5	9970	<50	120	5.6	19	<5	<0.02	<0.05	<1	4.2
EX 051231	30	5	240	940	<1	2	13	24	4	8.26	1.9	<1	<5	12	2560	<50	61	12	9.8	<5	<0.01	<0.05	<1	2.1
RA-031431	11	~5	560	1600	<1	5	28	160	4	5.91	3.2	<1	<5	<5	25100	<51	110	3.0	19	<5	<0.03	<0.05	<1	3.1
KA-VJIZJZ	469	83	2500	590	<1	6	55	<10	<2	18.5	<0.5	<1	<5	<5	1740	<50	100	51	4.1	21	<0.06	<0.06	<1	<0.5
	16	<5	13	<100	<1	7	36	360	4	6.15	1.3	<1	<5	<5	15300	<50	68	0.6	31	<5	<0.02	<0.05	<1	<0.5
COREY	-			600	-1	~1	~5	36	<2	1.75	1.1	<1	<5	<5	<500	<50	<30	1.1	5.9	<5	<0.01	<0.05	<1	0.9
		<5		900		~ ~	26	150	1	6.49	2.1	<1	<5	<5	25100	<55	<30	1.5	40	<5	<0.03	<0.05	<1	2.2
	y	<>	13	<100	1	2	16	-10		7.35	10	<1	<5	12	1020	260	69	11	22	<5	<0.03	<0.05	<1	4.7
RX-D51237	1/50	100	360	33000	~1	-1	10	~10	-2	R.99	<1.0	29	<5	43	<500	<130	<30	83	2.5	140	<0.07	<0.10	<1	<0.5
RX-051238	1090	100	110	61000	~1	~1	10	~10	-2	7.47	<1.0	<2	<5	<5	<500	<120	<30	95	0.2	<5	<0.10	<0.13	<1	<0.5
RX-051239	4700	120	6302	00000	×1	~~		110		,														
DV 051340	1570	1 30	4502	80000	<1	<1	<5	23	<2	4.27	<1.0	<2	<5	<5	<500	<90	<30	75	0.9	<5	<0.06	<0.08	<1	<0.5
RE-051240	43	<5	13	2000	<1	7	41	750	2	6.11	2.0	<1	<5	<5	13200	<50	<30	0.8	34	<5	<0.02	<0.05	<1	0.6
A-051242	61	<5		1500	<1	2	44	610	<2	6.56	1.6	4	<5	<5	22600	<50	<30	1.5	39	<5	<0.02	<0.05	<1	<0.5
BY 051243	157	<5	25	3700	<1	4	5	49	5	2.76	5.5	<1	<5	21	12600	<50	130	3.8	22	<5	<0.02	<0.05	<1	4.9
RX-051244	7	<5	70	2100	<1	23	7	13	<2	6.61	1.3	<1	· <5	13	1040	<50	<30	3.8	5.6	<5	<0.01	<0.05	<1	0.9
DY-051745	10	-5	21	2000	<1	<1	<5	17	<2	1.21	9.9	<1	<5	<5	24500	<50	79	1.2	2.2	<5	<0.02	<0.05	<1	10
RY_051246	<5	<5	25	880	<1	<1	14	45	3	4.35	4.5	<1	<5	<5	16700	<50	69	2.0	20	<5	<0.02	<0.05	<1	5.1
RX-051240	<5	<5	24	2200	<1	<1	<5	49	<2	0.92	9.3	<1	<5	<5	23300	<50	80	2.5	1.4	<5	<0.02	<0.05	- 4	12
NA-VJ1247	~5	-5	110	1400	<1	3	7	36	4	2.96	5.3	<1	<5	25	12000	<50	70	2.3	16	<5	<0.01	<0.05	<1	4.4
RX-051249	<5	<5	13	<100	<1	16	<5	<10	<2	0.47	<0.5	<1	<5	6	<500	<50	<30	2.2	0.8	<5	<0.01	<0.05	<1	<0.5
		-15	140	1000	<1	3	18	32	3	5.95	4.0	<1	<5	<5	11700	<50	48	3.1	18	<5	<0.02	<0.05	<1	3.9
KX-U31230	10	~5	10	1700	-1	<1	11	<10	2	6.49	2.1	<1	<5	7	28800	<50	120	4.4	17	<5	<0.02	<0.05	<1	1.8
KK-051251	10	<0	23	820	21	<1	 A	14	4	6.45	1.6	<1	<5	17	16900	<50	130	5.8	17	<5	<0.02	<0.05	<1	2.1
KX-U51252	704		140	2000	~1	~1	12	16	14	B.57	3.0	<1	<5	72	707	150	260	16	26	19	<0.02	<0.05	<1	3.1
KX-UJ1234	147	< 3 	700	2700	~1	21		23	16	10.1	3.3	<1	<5	9	1370	<50	360	8.2	33	<5	<0.02	<0.05	1	3.4
RX-051254	14/	<3	30	2100	~*	~*								-								-0 OF		
RX-051255	12	<5	24	6100	<1	21	<5	32	<2	3.08	<0.5	<1	<5	<5	36000	<50	<30	2.8	14	<5	<0.02	<0.00	<1 	0.9
RX-051256	<5	<5	87	37000	<1	24	27	96	9	3.47	7.6	<1	<5	<5	12800	150	80	6.4	29	<5	<0.02	<0.05	<1	2.0
RX-051257	<5	<5	49	83000	<1	29	38	73	13	7.62	<0.5	<1	<5	<5	23600	270	86	22	30	<5	<0.04	0,44	<1	<0.5

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Activation Laboratories Ltd. Work Order: 4449

(96)

Report: 4423

Sample description	U	W	sn 🛛	LA	CE	ND	<b>B</b> M	EU	TB	YB	LU	Maor
	PPM	PPM	PPM	PPN	PPM	PPN	PPH	PPH	PPM	PPN	PPN	9
RX-051220	6.7	21	158	5	10	<5	0.3	0,9	<0.5	0.93	<0.05	30.00
RX-051221	9.2	31	155	7	11	<5	1.0	1.3	1.0	2.29	0.32	30.00
RX-051222	<0.5	9	194	8	22	10	2.5	1.3	0.9	1.52	0.28	30.00
RX-051223	2.9	- 4	<50	9	24	17	2.3	1.9	<0.5	2.82	0.43	30.00
RX-051224	<0.5	<4	<58	6	12	<5	1.8	0.8	<0.5	1.73	0.29	30.00
RX-051225	2.1	<4	150	14	32	14	3.8	1.4	<0.5	3.70	0.63	30.00
RX-051226	1.0	<4	89	9	22	10	2.2	0.7	0.6	2.98	0.37	30.00
RX-051227	6.8	<4	110	47	79	29	3.1	0.8	<0.5	1.56	0.20	30.00
RX-051228	<1.6	<9	282	10	21	18	1.6	1.0	<0.5	1.55	0.24	30.00
RX-051229	<0.5	<4	42300	4	<3	<5	0.6	0.5	<0.5	1.10	0.22	30.00
RX-051230	<0.5	<4	254	14	31	12	2.7	0.6	1.1	2.42	0.34	30.00
RX-051231	1.3	<4	2440	6	11	<5	1.2	0.5	<0.5	1.01	0.14	30.00
RX-051232	<0.5	<4	227	39	73	32	5.6	2.0	<0.5	2.24	0.39	30.00
	<1.0	<4	46300	14	22	10	1.7	<0.2	<0.5	1.38	0.14	30.00
	<0.5	<4	459	10	22	12	2.4	1.3	<0.5	1.43	0.28	30.00
COREY				17	18	14			-0.5	2.01	0.34	30.00
	<0.5	<4	63	13	17		2 6	1 5	<0.5	2.16	0.33	30.00
	<0.5	<4	73	25	43	20	4.6	1.9	<0.5	6.14	1.01	30.00
RX-051237	5.0	< 4	30100	43	20		0.2	-0.2	<0.5	<0.25	<0.05	30.00
RX-051236	<1.2	<42	31000	, y	20	~5	<0.1	<0.2	<0.7	<0.39	<0.06	30.00
RX-051239	<1.8	<44	39000	2	~ 5		~~~1					
RX-051240	<1.2	<41	49000	6	18	<5	<0.1	<0.2	<0.5	<0.25	<0.05	30.00
RX-051241	<0.5	<4	1450	3	8	5	1.9	0.9	<0.5	2.63	0.41	30.00
RX-051242	<0.5	<4	2610	2	8	<5	1.7	1.0	<0.5	3.21	0.51	30.00
RX-051243	7.7	<4	1410	20	36	19	4.7	1.4	1.0	6.19	0.87	30.00
RX-051244	13	<4	8080	5	16	10	1.1	0.5	<0.5	1.42	0.21	30.00
RX-051245	4.3	<4	293	32	71	28	7.6	1.9	2.1	13.0	1.97	30.00
RX-051246	5.0	<4	175	12	28	14	3.1	1.1	<0.5	4.38	0.74	30.00
RX-051247	3.6	<4	304	37	81	27	B.5	2.0	1.9	10.5	1.54	30.00
RX-051248	8.5	<4	326	14	33	13	3.0	0.7	<0.5	4.50	0.75	30.00
RX-051249	1.3	<4	60	2	3	<5	0.3	<0.2	<0.5	0.41	0.06	30.00
RX-051250	4.7	<4	<b>9</b> 9	10	22	10	2.9	0.9	<8,5	4.05	0.63	30.00
RX-051251	<0.5	<4	302	8	14	<5	1.6	0.9	<0.5	2.02	0.30	30.00
RX-051252	1.8	<4	202	7	16	<5	1.5	0.7	0.8	1.67	0.30	30.00
RX-051253	<0.5	28	137	7	17	<5	1.5	0.9	<0.5	1.79	0.35	30.00
RX-051254	2.0	23	130	8	16	9	1.6	0.7	<0.5	2.63	0.43	30.00
RX-051255	<0.5	<4	<50	10	21	<5	3.3	1.5	1.5	3.45	0.41	30.00
RX-051256	3.0	<4	602	19	34	<5	4.0	2.3	<0.5	4.63	0.67	30.00
RX-051257	<0.7	<4	11500	12	24	<5	2.2	1.8	<0.5	3.09	0.34	30.00

### **APPENDIX 5**

## Geology, Sample Locations, Descriptions and Results - KENNECOTT CANADA




COREY JUNE SAMPLES - ALL GRABS UNE 24' CUMBORIAND SHOWING - MAIN ZONE, IN FRONT IKA - 001 ZKL - 002 IKL - 003 EAST SIDE OF MAN SX LENS THG - 001 LOWER AST , ALT VOLC ; i - FRACT ; \_ PY, Sph, gal, Cpy CUMBERCOND HL -002 10 M ABOUT L. ADIT' ALT VOLC' FRACT ; PY, PSTDIO% P; BETWOON UP ! LOW. ADIT; EAST SIDE OF LUSSIN ; PYRITIC VOLCS ; FRACT ; WEATH. HL -003 HL -004 SAME - LESS PYRITIC (3%) VOLC 17 146 -005 (15 m CHIPS Anova Ridlet ; NE - comm- SE OF C-10 H6-006 +1- CARB- CITE ALT VOUCS ; DISS PY; 1+4 -007 JUNE 25: IHG - 008\_ N, SIDE OF SULPH. CR. - 60.2m WiDE OTZ POD : 15% Find Py - BLACK, GRAPHITIC SEDS . 2% PY' SULPME STA 009 010 - GAEY, SILICEOUS SODS/TURE : 5% PY 011 - LAPILLI TUAF ' Some SILI Wous AMALS' 3%, (012) - GRANDUC 013 2 @3580, SMAL CROOK W. BLACK ARCILLITE , It 44 42 FRACT 014 ) at UNUK AMUTE (SOT MAD) 1 70 3 % Py IKL OOU N. SIDE OF SULPH. CR BLACK , GRAPHITTLE SONS' 26.64 GROY, SILICODUS, FIND GROWN SOD/TUFF, MINDR VOLC FRAMS BLACK, GRAPHITIC SODS: 2617 005 •/ 006



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2036 bia S Vancouver, B.C. Canada V5Y 3E1 Phone (604) 879-7878 Fax (604) 879-7898

Report: 9200426 R Kenne	cott Canada	Inc.	·		Proje	ct; None	Given			Pag	e lof	-1	Sectio	n Tof	٢
Sample Name	Туре	Si02 %	T i 02 <b>%</b>	A1203 %	Fe203 %	Mg0 %	CaO Z	Na20 <b>%</b>	к20 %	MnO %	BaO <b>%</b>	P205 <b>%</b>	101 <b>X</b>	Total X	
IHL 002) BELOW IHL 003 CUMBERLAND IHL 004 SHOWING IHL 010) NORTH OF IHL 0115 SUL PHURETS	Rock Pulp Rock Pulp Rock Pulp Rock Pulp Rock Pulp	52.15 43.96 49.88 62.99 58.49	2.23 2.28 2.13 1.17 1.17	15.28 12.77 15.61 14.64 14.62	10.32 15.53 13.74 8.23 8.89	1.49 0.95 3.37 1.80 2.53	4.97 1.68 3.92 0.73 2.22	2.21 1.87 4.74 2.97 2.80	4.50 4.84 0.68 2.38 2.03	0.09 0.04 0.21 0.02 0.08	1.97 1.48 0.12 0.16 0.17	0.55 0.48 0.56 0.43 0.38	4.76 11.24 4.95 4.72 5.95	100.52 97.12 99.91 100.24 99.33	
IKL 002 CUMBERLAND IKL 003 J IKL 005> N. OF CILL PHURETS	Rock Pulp Rock Pulp Rock Pulp	45.91 48.25 63.21	2.07 2.21 1.19	14.63 13.99 15.26	11.41 14.36 7.73	3.79 4.75 1.62	2.18 6.24 0.97	0,13 1.70 4.60	4.74 3.72 1.36	0.14 0.22 0.02	1.67 1.70 0.17	0.48 0.22 0.51	5.42 2.63 4.56	92.57 99.99 101.20	

Minimum Detection Maximum Detection Method	0.01 100.00 WRock sclosufficient Samo	0.01 100.00 WRock	0.01 100.00 WRock stimate/	0.01 100.00 WRock 1000 %=	0.01 100.00 WRock Estimate	0.01 100.00 WRock %	0.01 100.00 WRock	0.01 100.00 WRock	0,01 100,00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 GeoSp	0.01 105.00 WRock
=No Test ReC=ReCheck ins	s≈Insufficient Samp	le m=r:	st mate/	1000 %-	ESCHARG	~							



2035 Solumbia Succite, Vancouver, B.C. Canada V5Y 3E1

Phone (604) 879-7878 Fax (604) 879-7898

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iPL Report: 9200425 T Project: None Giver	Kenr	ecott	Canada	i Inc.					0	In: J lut: J	un 3 ul 0	0, 1992 3, 1992	1	19 Ro	xck	P	age	1 of	1	Cert	Sect ified	ion 1 BC Ass	of 1 ayer	_!	$\langle \langle \rangle$	21	- Davi	id Chiu
Sample Name Ag ppm	Cu ppm	РЬ ррл	Zn ppm	As ppm	Sb ppm	Hg ppm	Мо ррт	TI B PPm PP	i C m pp	λd Co na ppra	Ni ppm	Ba W ppm ppm	Cr ppm p	V ppm	Mn ppm	La ppm	Sr ppm	Zr ppm	Sc ppm	Ti X	۸۱ ۲	Ca Z	Fe X	Mg Z	K 2	Na Z	Р <b>Х</b>	
IHG         001         ADIT         R         9.5           IHL         002         BEZOWR         3.9           IHL         003         HAIN         25.9           IHL         004         ANIT         R         0.1           IHG         005         8         1.1	974 16 86 13 439	2264 63 2037 19 5	6943 278 623 263 73	23 123 406 <	< 25 36 7 <	< < < < < <	5 9 16 3 26	< 2000 < 2000 < 2000 < 2000 < 2000 < 2000	< 16. < 0. <	4 31 < 48 2 29 < 36 < 24	12 38 6 8 9	3516 @1.8% < @1.3% < 934 < 1003 17	42 2 61 2 22 2 11 1 26 1	215 204 212 184 1 161	700 605 296 378 469	16 19 15 22 6	285 310 663 90 186	97 123 103 151 31	21 26 19 24 14	0.94 @1.2 <b>%</b> @1.2 <b>%</b> @1.1% 0.27	6.81 8.43 6.87 8.54 10.45	1.63 3.24 1.10 2.52 0.85	11.18 6.15 8.95 7.96 5.34	1.48 1.20 0.76 2.73 1.75	1.76 3.94 4.17 0.63 3.69	2.35 1.59 1.34 3.42 1.62	0.17 0.24 0.21 0.24 0.11	
IHG 006         (C-IO         R         1.2           IHG 007         R         0.1         R         0.1           IHG 009         N         of         R         0.3           IHL 010         SULPH         R         0.1	785 76 7 62 3	< 9 65 15 7	79 169 9 119 66	11 131 28 13	6 7 60 <	< < < < < <	12 4 55 8 4	< < < < <		< 20 < 20 < 25 < 10 < 17	9 11 21 11 4	992 < 1818 < 1530 < 427 < 1463 <	26 1 50 1 79 98 1 43 1	176 190 27 138 133	616 819 159 469 138	5 5 2 9 13	225 201 17 146 179	23 30 24 101 119	14 18 5 10 17	0.27 0.30 0.16 0.21 0.62	10.03 8.69 1.57 6.16 7.63	0.79 1.14 0.58 0.28 0.47	5.58 5.47 6.95 9.19 4.89	2.25 2.26 0.13 0.63 1.43	2.21 2.45 1.46 0.91 2.00	3.02 1.90 0.03 2.67 2.04	0.11 0.12 0.02 0.10 0.18	
IHL 01]       CK.       R       0.2         ING 012(2.3.14655       R       0.2         IHG 013       S.2.78       0.6         IHG 014       S.2.98       0.7         IKL 002       No. 9.2       8       0.7	7 04.07 30 14 3610	6 312 16 5 475	110 854 217 55 @4.3%	451 42 114 21	12 < 8 14	< < < < <	3 24 4 5 10	~ ~ ~ ~	< 2.	< 28 < 163 3 8 < 5 2m 38	6 65 10 4 11	1514 479 986 658 3475	24 1 115 2 129 171 20 2	130 253 89 45 219 1	540 226 370 234 132	15 5 9 10 14	184 26 70 44 26	119 25 100 93 79	17 7 12 8 23	0.63 0.13 0.22 0.15 01.3%	7.93 2.66 6.91 5.87 8.31	1,45 0,20 0,23 0,18 1,64	5.38 13.06 2.63 3.30 8.35	2,06 0.94 0.49 0.28 3.46	1.75 0.83 1.97 1.78 4.52	1.96 0.05 2.56 2.15 0.12	0.16 0.17 0.03 0.06 0.24	
IKL 003.) IL. (~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	100 11 8 397	102 10 12 9	291 103 73 21	7 11 27	7 10 8 5	< < < <	3 7 5 29	~ ~ ~ ~		< 70 < 9 < 19 < 6	39 5 5 12	€1.5% < 1027 < 1428 < 481 5	74 3 59 1 59 1 85 1	376 1 76 115 192	424 438 159 40	3 8 14 4	124 167 370 141	94 123 110 67	40 ( 19 ( 18 ( 10 (	01.1% 0.42 0.62 0.23	7.37 8.80 7.96 4.28	3.85 0.40 0.62 0.34	8.02 3.08 4.58 1.10	3,72 1.88 1.28 0.20	3.17 2.31 1.15 1.21	1.19 1.67 3.15 1.04	0.09 0.03 0.22 0.04	
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#### INTERNATIONAL PLASMA LABORATORY LTD.

2036 Columbia Street Vancouver, B.C. Canada V5Y 3E1 Phone (604) 879-7878 Fax (604) 879-7898

Report: 9200424 R	Kennecott Canada	Inc.	<u></u>	Project	: None Giv	en	Page	T OF T
Sample Name	Туре	Cu Z	РЬ <b>х</b>	Zn X	Ag oz/st	Au oz/st		
IKA 001	Rock	1.26	7.38	17.45	7.27	0.188	CUMBERLAND	SHOWING

 Minimum Detection
 0.01
 0.01
 0.01
 0.01
 0.02

 Maximum Detection
 100.00
 100.00
 100.00
 1000.00
 1000.00

 Method
 Assay
 Assay
 Assay
 FAGrav
 FAGrav

 --=No
 Test
 ReC=ReCheck
 ins=Insufficient
 Sample
 m=Estimate/1000
 %=Estimate
 %

### KENNECOTT CANADA INC. ISKUT PROJECT GRAB SAMPLES AUGUST 1992

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SAN	1PLE	TYPE	PROPERTY	NORTH	LOCATION EAST	(UIM) ELEVA ïeet	TION meters	ANALYSIS	REMARKS
02	399	rock	Corey	6263590	410760	3980		ICP	altd seds
<b>92</b>	400	rock	Corey	6263600	410790	3960		WR	rhyolite
)2	401	rock	Corey	6263610	410890	3980		WR	basalt
02	402	rock	Corey	6262870	411270	4350	)	WR	rhyolite
02	403	rock	Corey	6262920	411320	4450		WR	dacite
22	404	rock	Corey	6263120	411260	4400	ł	WR	dacite
)2	405	rock	Corey	6263180	411290	4450		WR	dacite
02	406	rock	Corey	6263300	411200	4220	l i i i i i i i i i i i i i i i i i i i	ICP	bas brxx; lmst
72	407	rock	Corey	6264840	411120	4000	l i	WR	rhyolite
)2	414	rock	Corey	6265320	411000	3740	)	WR	rhy; py
02	415	rock	Corey	6265240	410700	3180	l .	WR	volc/sed; py
02	416	rock	Corey	6265190	410600	3180	)	ICP	shale
02	417	rock	Corey	6265230	410530	3180	)	WH	basalt
02	418	silt	Corey	6265040	410550	3300	)	ICP	
02	419	rock	Corey	6264930	410540	3360	1	WR	dac; py
02	420	rock	Corey	6265420	410320	3060	)	WR	dac; po
$\mathfrak{I}\mathfrak{I}\mathfrak{I}\mathfrak{I}\mathfrak{I}\mathfrak{I}\mathfrak{I}\mathfrak{I}\mathfrak{I}\mathfrak{I}$	421	rock	Corey	6265660	410080	3060	)	WR	basalt

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	Sample Name		лл ppb	Ag ppa	Cu ppm	РЬ Ррм	Zn ppm	As (xxm	Sb ppm	fig tixysj	Мо р(ж	66ui 1.1	Bi ppn	Cd ppm	Co ppm	N i Ppre	Ba ppm	₩ PJ vn	Cr Ppm	V Ppm	Mri Pipril	la ppon	Sr Ppm	7т ррпа	Sc: ppm	li T	AI Z	Ca Z	Fe Z	Hg Z	K Na X Z
e sit	02412 02414 02415 02416 02417	r R R R R R R R	3 < 4 9 3	< 0.3 0.7 <	31 7 4 24 51	< 8 5 3 <	45 7 186 46	\$ 25 19 <	* * * * *	< < < < < <	2 4 7 12 3	V V V V	~ ~ ~ ~ ~	< < ( 0.4	28 2 7 3 24	40 3 5 86 40	2 50 41 51 64	× × × × ×	23 103 32 25 108	36 4 33 28 122	284 83 144 138 698	2	32 3 28 4 15	1 1 1 <	< ( 1 ( 3 ( 2 ( 7 (	0.03 0.01 0.01 0.02 0.02	3.22 0.21 1.0/ 0.46 3.00	1.22 0.03 0.49 0.06 1.24	3.54 ( 0.85 ( 4.72 ( 3.06 ( 4.11 2	2.32 0.02 0. 0.87 0. 0.21 0. 2.75	< 0.23 02 0.07 07 0.07 08 0.03 < 0.08
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з <b>г</b> [*	07418 A	5	12_	0,1	31	9	233	12	*	۲	5	24	<	1.1	22	39	.86	۲	38	641	1701 .	8	. 16	2	40	.04	: <b>1.</b> 73	0.34	5.32),	.04 0.0	13 0:03
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Sample Name	1	Au đạti '	Ag ppm	Cu ppm	РЬ ррм	Zn ppm	As ppm	Sb ppm	ppm PDm	Ho f ppnepp	1 Bi n ppw	Cd PPm	Co ppm	Ni ppra p	Ba xon pp	н С xn pp	n ppr	/ Mu 1 ppm	La ppn	Sr ppm	Zr ppm	Sc ppm	li Z	۸۱ ۲	Ca Z	fe Z	Mg X	Х	Na Z	
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02403 02404 02405 02406	(R'R'R	3	<ul> <li>v.5</li> <li></li> <li></li></ul>	- - 	< 7 <		, 81 5	~ ~ ~	~ ~ ~	2 51 4	< < <	< 0.4	5 7 29	4	52 18 53	< 19 < 64 < 100	9 14 5 20 3 65	1090 52 1138	9	18 5 89	2	50 10 50	.03 .01 .02	1 47 0 21 1 26	0.96 0.11 10/	4.07 4.86 4.21	0.51 0.05 1.26	0.09 0.05 0.03	0.05 0.07 0.04	
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2036 Colu... Vancouver, B.L. Canada V5Y 3E1 Phone (604) 879-7878 Fax (604) 879-7898

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Sample Name         Type         Si02         Ti02         A1203         Fe203         Mg0         Ca0         Na20         K20         Mn0         Ba0         P205         L0I         Total           02400         Rock Pulp         69.02         0.30         16.60         1.52         0.07         0.26         7.30         3.27         <0.01         0.28         0.08         0.94         99.64           02401         Rock Pulp         69.02         0.30         16.60         1.52         0.07         0.26         7.30         3.27         <0.01         0.28         0.08         0.94         99.64           02401         Rock Pulp         47.06         0.86         19.40         8.03         6.57         11.30         3.00         0.27         0.11         0.01         0.66         3.09         99.76           02402         Rock Pulp         76.34         0.22         11.99         2.51         0.09         0.11         6.32         0.45         <0.01         0.05         0.05         1.36         99.49           02403         Rock Pulp         70.02         0.80         13.23         4.75         1.10         0.49         4.14         2.24         0.01 </th <th>Report: 9200692 R</th> <th>Kennecott Canada</th> <th>Inc.</th> <th></th> <th></th> <th>Proje</th> <th>ct: 05-3</th> <th>385</th> <th></th> <th></th> <th>Pag</th> <th>e 1 of</th> <th>1</th> <th>Sectio</th> <th>n 1 of</th>	Report: 9200692 R	Kennecott Canada	Inc.			Proje	ct: 05-3	385			Pag	e 1 of	1	Sectio	n 1 of
O2400         Rock Pulp         69.02         0.30         16.60         1.52         0.07         0.26         7.30         3.27         <0.01	Sample Name	Туре	S i 02 7	T 102 X	A 1203 X	Fe203 <b>%</b>	Mg0 <b>%</b>	CaO X	Na20 %	к20 <b>%</b>	Mn0 <b>%</b>	8a0 <b>%</b>	P205 <b>X</b>	L01 <b>X</b>	Total X
D2400         Rock Pulp         69.02         0.30         16.60         1.52         0.07         0.26         7.30         3.27         <0.01         0.28         0.08         0.94         99.64           D2401         Rock Pulp         47.06         0.86         19.40         8.03         6.57         11.30         3.00         0.27         0.11         0.01         0.06         3.09         99.76           D2402         Rock Pulp         76.34         0.22         11.99         2.51         0.09         0.11         6.32         0.45         <0.01		n .; P *		: e:									• ••	-	
12400Rock Pulp $69.02$ $0.30$ $16.60$ $1.52$ $0.07$ $0.26$ $7.30$ $3.27$ $<0.01$ $0.28$ $0.08$ $0.94$ $99.64$ 12401Rock Pulp $47.06$ $0.86$ $19.40$ $8.03$ $6.57$ $11.30$ $3.00$ $0.27$ $0.11$ $0.01$ $0.06$ $3.09$ $99.76$ 12402Rock Pulp $76.34$ $0.22$ $11.99$ $2.51$ $0.09$ $0.11$ $6.32$ $0.45$ $<0.01$ $0.26$ $0.24$ $3.29$ $100.57$ 2403Rock Pulp $70.02$ $0.80$ $13.23$ $4.75$ $1.10$ $0.49$ $4.14$ $2.24$ $0.01$ $0.26$ $0.24$ $3.29$ $100.57$ 2404Rock Pulp $65.18$ $0.96$ $14.11$ $6.51$ $0.96$ $1.90$ $3.99$ $3.91$ $0.16$ $0.26$ $0.35$ $2.32$ $100.61$ 2405Rock Pulp $69.04$ $0.62$ $11.53$ $7.24$ $0.15$ $0.25$ $5.36$ $1.94$ $0.01$ $0.20$ $0.25$ $3.55$ $100.14$ 2407Rock Pulp $72.26$ $0.29$ $12.46$ $4.03$ $0.35$ $0.46$ $2.90$ $4.98$ $0.07$ $0.21$ $0.03$ $1.43$ $99.47$															
02403         Rock Pulp         70.02         0.80         13.23         4.75         1.10         0.49         4.14         2.24         0.01         0.26         0.24         3.29         100.57           02403         Rock Pulp         65.18         0.96         14.11         6.51         0.96         1.90         3.99         3.91         0.16         0.26         0.35         2.32         100.61           02404         Rock Pulp         65.18         0.96         14.11         6.51         0.96         1.90         3.99         3.91         0.16         0.26         0.35         2.32         100.61           02405         Rock Pulp         69.04         0.62         11.53         7.24         0.15         0.25         5.36         1.94         0.01         0.20         0.25         3.55         100.14           02407         Rock Pulp         72.26         0.29         12.46         4.03         0.35         0.46         2.90         4.98         0.07         0.21         0.03         1.43         99.47           02407         Rock Pulp         72.26         0.29         12.46         4.03         0.35         0.46         2.90         0.92         0	02400 02401 02402	Rock Pulp Rock Pulp Rock Pulp	69.02 47.06 76.34	0.30	16.60 19.40 11.99	1.52 8.03 2.51	0.07 6.57 0.09	0.26 11.30 0.11	7.30 3.00 6.32	3.27 0.27 0.45	<0.01 0.11 <0.01	0,28 0.01 0.05	0.08 0.06 0.05	0.94 3.09 1.36	99.64 99.76 99.49
	02402 02403 02404 02405 02407	Rock Pulp Rock Pulp Rock Pulp Rock Pulp	70.02 65.18 69.04 72.26	0.80 0.96 0.62 0.29	13.23 14.11 11.53 12.46	4.75 6.51 7.24 4.03	1.10 0.96 0.15 0.35	0.49 1.90 0.25 0.46	4.14 3.99 5.36 2.90 3.05	2.24 3.91 1.94 4.98	0.01 0.16 0.01 0.07	0.26 0.26 0.20 0.21	0.24 0.35 0.25 0.03	3.29 2.32 3.55 1.43	100.57 100.61 100.14 99.47
	02415 02417 02419 02420 02421	Rock Pulp Rock Pulp Rock Pulp Rock Pulp Rock Pulp	46.23 66.32 66.03 47.25	1.04 1.03 0.80 2.50	19.52 11.59 10.59 13.76	9.35 6.27 7.54 14.95	7.25 0.22 1.53 7.22	7.62 0.49 3.04 8.37	3. 19 0. 32 2. 32 2. 03	0.17 8.70 2.95 0.61	0.15 0.03 0.08 0.22	0.02 0.87 0.20 0.08	0.10 0.49 0.38 0.47	4.39 3.09 4.76 2.84	99.03 99.42 100.22 100.30

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Minimum Detection Maximum Detection	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0.01 100.00 WRock	0,01 100,00 GeoSp	0.01 105.00 WRock
Method H. Tost Rof Dofhork	- WRock - Tasa Insofficient - Sam	WKOCK ple_m-F	wкоск st/1000	WROCK X-Est X	MROCK Mara No	Est	MROCK	MACCK	AROCK	MNOCK	HILOCK	Geoop	moor

**APPENDIX 6** 

Sample Locations, Descriptions and Results - HOMESTAKE CANADA

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### Homestake Corona 1992 Assay Results Kenrich Corey Claims

62301       Cuadratical Zase       -0.001       0.024       114       9       129       2       3.6       -0.2       -0.01         62302       Cuadratical Zase       -0.001       -0.02       173       5       77       -1       2.4       0.6       -0.01         62303       Cites (Cites and Section 2)       173       15       164.0       80.02       0.01       1.02       7.15       2.4       0.6       -0.01         62303       Cites (Cites and Section 2)       1.5       1.6       1.6       1.6       1.6       1.2       2.5       2.2       1.7       5.2       -0.2       0.08         62304       Addrets matrix mathems in 5.4       0.047       1.53       3.485       7.500       2.0000       99       7.7       1.2       2.4       0.6       2.7       7.6       2.7       6.6       0.022       2.1       1.5       2.6       0.02       2.6       6.4       312       1.5       5.0       9.4       1.0       0.2       2.6       6.4       312       1.5       5.0       9.4       1.0       0.02       1.6       1.6       1.6       1.6       0.0       0.2       2.1       1.6       1.0       0.2	ICC #	Description	Au	Ag	Cu	Pb	Zn	Mo	As	Sb	Ha
62302       Charlented Zase       -0.001       -0.02       173       5       77       -1       2.4       0.8       -0.01         62305       Charlented Zase       -0.01       -0.02       121       6       22       17       5.2       -0.2       0.08         62305       Mail. Insk y a maximu mightle g = p       0.032       5.23       4.21       7.16       16.40       6000       2000       42       2.12       2.8       7.16       15.40       6000       2000       42       2.12       2.8       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       2.4       7.1       2.4       4.4       0.0       0.0       0.0       2.2       7.1       5.1       7.1       7.1       1.6       1.6       7.7       6.2       0.0       0.0       2.4       1.6       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0       0.0	62301	Cumberland Zone	-0.001	0.04	114	9	129	2	3.8	-0.2	-0.01
62000       Camberdad Zase       -0.01       -0.02       212       6       22       17       5.2       -0.2       0.08         62004       CITK (Sinch) F & printers       0.129       7.16       1440       9603       20000       47       615       147       12.98       20000       47       161       142       455       716       140       20000       42       110       24.46       71       10000       20000       42       110       24.46       71       128       20       718       140       716       140       2000       42       128       20       718       140       2000       42       128       10       24.46       1128       10       24.46       2000       20       42       67       60.002       20       11       22       2.4       10       42.6       10       42.6       10       42.6       10       42.6       14.5       20.003       10       42.6       10       42.6       10.02       12.6       10.02       12.6       10.02       10       10       10.02       10.02       10.02       10.02       10.02       10.02       10.02       10.02       10.02       10.02       10.02	62302	Cumberiand Zone	-0.001	-0.02	173	5	77	-1	2.4	0.8	-0.01
62306       Mail: Simple mainter with 3% grintingen 1.2m dig       0.129       7.16       1640       8003       20000       47       618       147       12.88         62305       Mail: Sim digs of simple maintered with 3% grintingen 1.2m dig       0.047       1.83       9455       7660       2000       42       218       22.67       8.128         62305       Mail: Sim digs of simple maintered with 3% grintingen 1.2m dig       0.047       1.83       9455       7660       2000       42       218       22.67       8.128         62305       Andrikes zame       0.0301       -0.02       55       164       612       1       40       8.2       0.041         62310       Cumberland Zame       0.022       0.44       167       22.4       167       0.026         62405       Paile winks: Vi-470.024 (bit winks, wink and hang dry ry       -0.001       -0.02       5       15       123       2       2.4       1.7       0.035         62405       Paile winks: Vi-470.024 (bit winks, wink and hang dry ry       -0.001       -0.02       5       10       55       11       2.5       0.057       112       2       1.6       0.057       115       2.2       4       1.7       0.026 <td< td=""><td>62303</td><td>Cumberland Zone</td><td>-0.001</td><td>-0.02</td><td>212</td><td>8</td><td>22</td><td>17</td><td>5.2</td><td>-0.2</td><td>0.036</td></td<>	62303	Cumberland Zone	-0.001	-0.02	212	8	22	17	5.2	-0.2	0.036
62305       Multi Line help Jamanice majkette gr-12       0.392       5.29       4267       10000       20000       91       129       101       22.482         62306       Advecter; 18 miniger jut Line hip       0.049       1.75       655       1       40       62.004         62306       Advecter; 18 miniger jut Line hip       0.049       1.77       65       1       40       62.041         62306       Advecter; 18 miniger jut Line hip       0.022       0.06       67       157       655       1       40       62.041         62311       Camberiand Zaes       -0.02       40       167       7252       10       52       2.4       4.6       0.022         62404       Finite Vid-001       Manitic finite fragmental Marked, 1% gryn kruite       -0.001       -0.02       5       15       123       2       2.4       1.7       0.076         62404       Finite Vid-002, Vid-01, Wid-Nicete       -0.001       -0.02       5       10       53       7       11       2.0       0.116         62404       Finite Vid-02, Vid-01, Wid-Nicete Advecte       -0.001       -0.02       30       7       6       -1       0.0       0.0       0.0       0.0       0.0 <td>62304</td> <td>QSTR; 60cm chip 3% py stringers</td> <td>0,129</td> <td>7.16</td> <td>1640</td> <td>8903</td> <td>20000</td> <td>47</td> <td>618</td> <td>147</td> <td>12.982</td>	62304	QSTR; 60cm chip 3% py stringers	0,129	7.16	1640	8903	20000	47	618	147	12.982
62306       Austratic matter markened with 3% grantsgras 1.2m.chp       0.047       1.83       76500       20000       42       216       26.7         62307       Austratic markened model 1.2m.chp       0.093       0.077       1423       2047       20000       39       777       9       2.747         62308       Austratic markened model 1.2m.chp       0.093       0.072       0.1       68       175       655       1       40       9.2       0.041         62308       Camberstad Zone       0.002       0.1       68       175       652       2       67       6       0.052         62403       Doubstad Zone       0.002       0.1       68       175       652       1       122       16       2.4       1.6       0.052         62403       Doubstad Xu-2000       Austratic folds fragmental Markod, 1% pyrhothe       -0.001       -0.02       5       1       1       2.4       1.6       0.052         62403       Doubstad Xu-2000       Austratic folds fragmental Markod, 1% pyrhothe       -0.001       -0.02       10       -2       4       6       1.6       0.025         62403       Moditaces Multian Markod Pyrhothe       -0.001       -0.02       10	62305	Msul; 1.2m chip .3m massive sulphides gn-sp	0.392	5.29	4267	10000	20000	91	128	101	24.945
62307       Austake: 1% winsper yr Lac Alp       0.093       0.77       1423       2047       20000       39       777       9       2.747         62306       Austake: 1% winsper yr Lac Alp       0.002       55       64       312       1       52       6.4       0.022         62301       Camberiand Zone       0.002       55       64       312       1       62       6.4       0.022         62301       Camberiand Zone       0.002       16       222       1003       2.4       168       10       6.424         62404       Fibic Netark: VM-021 Mode Auk Infa gly ary p       -0.001       -0.02       16       5       5       115       60       9.4       0.057         62404       Fibic Netark: VM-021 Mode Auk Infa gly ary p       -0.001       -0.02       10       -2       11       6       19       0.9       0.555         62405       Fibic Netarity Mode Interface Multi and In	62306	Andesite; massive unsheared with 5% qtz stringers 1.2m chip	0.047	1.63	3455	7690	20000	42	216	26.7	3,128
62308       Austriker umkernikel Liz nåp       0.002       0.06       67       157       655       1       40       9.2       0.041         62309       Causkutsad Zose       0.002       0.1       68       175       624       2       67       6       0.022         62311       Causkutsad Zose       0.02       0.44       167       2521       123       2       2.4       1.7       0.042         62401       Datas, VAI-001 Maintic fails fagasstal Mached, 16 pythosts       -0.001       -0.02       5       15       123       2       2.4       1.7       0.074         62405       National waters Weil Topic Mache, table fagasstal Mached, 16 pythosts       -0.001       -0.02       5       10       33       7       10       2.4       1.5       0.9       0.8       6.2571         62407       Maidtoor Machee VM-0.001 Mainton Mathemather Pythop       -0.001       -0.02       21       15       61       2       16       1.5       0.92       0.025       0.02       16       61       2.5       1.6       0.2       16       0.5       0.025       0.025       1.6       1.5       0.025       0.025       0.025       0.025       0.025       0.025       <	62307	Andesite; 1% stringer py 1.2m chip	0.093	0.77	1423	2047	20000	39	777	9	2.747
26230 Cumberland Zone       -0.001       -0.02       55       64       312       1       52       6.4       0.022         02310 Cumberland Zone       0.02       0.11       68       175       6221       1905       2.4       168       10       0.42         02410 Cumberland Zone       0.02       0.01       -0.02       5       15       123       2.4       1.6       0.02         02410 Total vices       -0.001       -0.02       4       4       4.4       4.4       0.9       0.03         02420 Total vices       -0.001       -0.02       5       15       50       9.4       0.571         02400 Total vices       -0.001       -0.02       5       10       53       7       11       2       0.18         02423 Total vices       -0.001       -0.02       5       15       61       10       0.8       3.5       11       2       0.18       1.5       0.00       0.8       2.5       0.55       2.0       0.55       0.55       0.25       0.55       0.55       0.55       0.55       0.55       0.55       0.55       0.55       0.55       0.55       0.55       0.55       0.55       0.55 <t< td=""><td>62308</td><td>Andesite; unmineralized 1.2m chip</td><td>0.002</td><td>0.06</td><td>87</td><td>157</td><td>655</td><td>1</td><td>40</td><td>9.2</td><td>0.041</td></t<>	62308	Andesite; unmineralized 1.2m chip	0.002	0.06	87	157	655	1	40	9.2	0.041
62310       Cumberland Zone       0.002       0.1       68       175       624       2       67       6       0.022         62311       Cumberland Zone       0.002       0.48       167       252       1905       2.4       10.042         62403       Ficks investic VM - 021, Vicks, North ack taket rone, linessite       -0.001       -0.02       5       15       123       2       2.4       1.7       0.074         62404       Ficks investics, VM - 021, Vicks by, North ack taket rone, linessite       -0.001       -0.02       5       10       53       7       11       2       0.118         62405       Ficks investics, VM - 023, Vicks by, North ack taket rone, linessite       -0.001       -0.02       10       -2       41       6       19       0.9       0.835         62627       Moditory, North Cold Mark investion and interves with and interves w	62309	Cumberland Zone	-0.001	-0.02	55	64	312	1	52	6.4	0.029
62311       Cumberland Zane       0.02       0.48       167       2281       1905       2.4       168       10       0.02         62430       Deck       Month expl. Mid fing shy wy       -0.001       -0.02       5       15       123       2.4       1,7       0.0074         62405       Fields webank; VM - 005, Keb, breads & aber rane, lineonie       -0.001       -0.02       5       10       53       7       11       2       0.157         62405       Fields webank; VM - 005, Keb, breads & aber rane, lineonie       -0.001       -0.02       5       10       53       7       11       2       0.157         62405       Midden rane, VM - 005, Bields aber rane, lineonie       -0.001       -0.02       10       -2       41       6       19       0.9       0.685         62626       Middens; Multi Able systee rane, lineonie with seminater systee       -0.001       -0.02       21       15       52       3       3.3       0.053         62626       Widtheor, isket skie sprite prints is for the state systee       -0.001       -0.02       2       12       20       5       2.2       0.073         62626       Yelk systee systee skie statestatestatesystee       -0.001       -0.02       3	62310	Cumberland Zone	0.002	0.1	68	175	624	2	67	6	0.062
62403       Decket VM-001 binktic fabit fragmate al Mached, 1% prynotite       -0.001       -0.02       5       15       123       2       2.4       1,7       0.074         62404       Fids: weizes: VM-002, NS chip, hore Ad, ald frag dy vy       -0.001       -0.02       4       4       64       4       2.4       0.9       0.005         62405       Fids: weizes: VM-002, NS chip, hore Ad, ald frag dy vy       -0.001       -0.02       5       10       53       7       11       2       0.116         62405       Fids: Weizes: VM-002, NS chip, hore Ad, ald frag dy vy       -0.001       -0.02       10       -2       41       6       19       0.9       0.53         62405       Fids: Wides: WM-002, NS chip, hore Add S-4% Met pryte       -0.001       -0.02       21       15       61       2       18       0.03       0.033       0.063       0.032       0.02       15       92       3.5       5.2       2.079       0.07       0.022       16       26       10       1.5       10       1.5       1.5       1.5       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6       1.6	62311	Cumberland Zone	0.02	0.48	167	2521	1905	24	168	10	0.424
62404       Febs wearset; VM-C02, EW deb, North and, kild frag flav yr yr       -0.001       -0.02       4       4       64       4       2.4       0.9       0.025         62405       Febs wearset; VM-C02, Ko the, hords of the dates zone, linnonho       -0.001       -0.02       5       10       53       7       11       2       0.157         62406       Febs wearset; VM-C02, Ko the, hords of the dates zone, linnonho       -0.001       -0.02       39       17       69       -1       16       0.0       0.033         62628       Modinace; Model kiles and statures wears we by the       -0.001       -0.02       39       17       69       -1       16       0.033       0.033         62628       Modinace; Model Mich the parket we by the       -0.001       -0.02       36       15       92       3       5.5       2.2       0.073         62630       Modinace; Iolial Mich is chargeneabled by the by prite profestion 4       -0.001       -0.02       3       9       11       6       0.02       17       16       2.5       13       17       1.907         62650       NG Hisper polythyr, disclasting parket mark in fasture and stature and statu	62403	Dacite; VM-001 bimictic felsic fragmental bleached, 1% pyrthotic	-0.001	-0.02	5	15	123	2	2.4	1.7	0.074
62405       Peick volenais: VM-020, XNC dap, mercia & sheer ran, lineoise       -0.001       -0.06       3       5       31       15       50       9.4       0.577         62406       Riyoline VM-020, Xolinetia matrose vha (Jimany ja rans, 5-10% dias pry the       -0.001       -0.02       10       -2       41       6       19       0.9       0.835         62627       Muditore; tack sitkoor with or with 3-14% Mby synthe       -0.001       -0.02       21       15       61       2       18       0.7       0.003         62628       Muditore; isolating the rain matrix-to print       -0.001       -0.02       4       15       64       2       18       0.7       0.003         62629       Felick Venasit: interciate matrix shorts in the prints in the print prints in the print prints in the prints in	62404	Felsic volcanic; VM-002, E/W chip, North end, altd frag shy w/ py	~0.001	-0.02	4	4	64	4	2.4	0.9	0.085
62406         Rkyolite; VA-02, Michiga, Maf any Myr-po         -0.001         -0.02         5         10         53         7         11         2         0.118           62407         Mudiose; Wa-03, folder aduntoze wikh J-48 Mole pyrite         -0.001         -0.02         39         17         69         -1         16         1.5         0.008           62628         Mudiose; lacet listic information aduntose wikh J-48 Mole pyrite         -0.001         -0.02         21         15         61         2         18         0.003           62628         Mudiose; lacet listic information aduntose with Mandar pyrite         -0.001         -0.02         4         19         68         2         10         1.5         0.025           62630         Mudiose; laud listic information dyrite         -0.001         -0.02         3         16         22         5.5         2.2         0.079           62646         ORS, magy quart whis it factures, distanted pyrite         -0.001         -0.02         3         16         25         13         1.7         0.25           62647         ORS, magy quart whis it factures, distanted pyrite         -0.001         -0.02         3         7         16         25         13         1.7         0.26	62405	Felsic volcanic; VM-002, N/S chip, breccia & shear zone, limonite	~0.001	0.06	3	5	31	15	50	9.4	0.571
62407       Muditains; VM-03, foliated instance with 214% bits pyrite       -0.001       -0.02       10       -2       41       6       19       0.0       0.02         62627       Muditains; Morting with anality pyrite       -0.001       -0.02       21       15       61       2       18       0.7       0.003         62628       Muditains; Morting with anality pyrite       -0.001       -0.02       21       15       61       2       18       0.7       0.003         62628       Muditains; Morting with anality pyrite       -0.001       -0.02       14       15       74       9       30       33       0.003         62626       Cirk, Malay parage warkt with, Mole hyprite prinotite 1%       -0.001       -0.02       2       12       20       5       18       17       1.97         62666       Cirk, Nagy ourit with in facture, distancied pyrite       -0.001       -0.02       3       9       11       6       20       2.7       0.073         62826       Cirk, Nagy ourit with in facture, distancie system       -0.001       -0.02       3       9       11       6       0.4       0.8       0.452       2.5       18       17       0.02       5       18       17	62406	Rhyolite; VM-002,N/S chip, altd fing w/py-po	-0.001	-0.02	5	10	53	7	11	2	0.118
62627       Muditas: Match alkicov initional muditas view has 1 - 4% Nets pyrite       -0.001       -0.02       29       17       69       -1       16       1.5       0.003         62622       Muditas: Match is functional with a main be pyrite       -0.001       -0.02       21       15       61       2       18       0.7       0.003         62623       Muditas: Match is functional main be pyrite       -0.001       -0.02       24       19       68       2       10       1.5       0.003         62630       Muditas: Induct for the Match anguage mark to pyrite is pyrite to 1%       -0.001       -0.02       36       15       92       3       5.5       2.2       0.005         62646       OER, waggy quark tyrks to alse       -0.001       -0.02       3       16       26       4       10       2.9       0.572         62646       OER, waggy quark tyrks to alse       -0.001       -0.02       3       7       16       25       3       1.7       0.497         62646       OER, waggy quark tyrks to alse       -0.001       -0.02       3       7       16       25       1.1       -0.20       0.488       6       -1       1.2       0.048       0.292       1.4       0.5	62407	Mudstone; VM-003, foliated mudstone with (21mm) py lenses, 5-10% diss py	-0.001	-0.02	10	-2	41	· 6	19	0.9	0.635
626228         Muditors: notionally fractured with seni manie pyrite         -0.001         -0.02         21         16         61         2         16         01         2         10         15         0.027           026229         Field	62627	Mudstone; black siliceous siltstone/mudstone with 3-4% blebs pyrite	~0.001	-0.02	39	17	69		16	1.5	0.049
0       0.001       -0.02       4       19       68       2       10       1.5       0.023         026230       Multiones (blait oblate instances with shudaar pyrke       -0.001       0.02       14       15       74       9       30.3       0.033         02630       Multiones (blait oblate instances with shudaar pyrke       -0.001       -0.02       36       15       74       9       30.3       0.33       0.033         02630       Multiones (blait oblate instantes) explore (standal stantes)       -0.001       -0.02       2       12       20       5       18       17       1.307         02666       0287       yellow stated, quarts pyrite tose       0.002       -0.02       3       9       11       6       20       2.7       0.407         02822       Argilles w 2-3 % pr. 3m ekp       -0.001       -0.02       8       17       1.4       0.6       0.168         028224       Argilles w 2-3 % pr. 3m ekp       metaboxet oblatel oblater (standal stantes)       -0.001       -0.02       8       17       5.2       2.1       -0.2       0.449       0.049       0.049       0.022       1.1       0.20       0.449       0.041       0.02       7.1       5.9	62628	Mudstone; moderately fractured with semi massive pyrite	-0.001	-0.02	21	15	61	2	18	0.7	0.033
62250       Multioner, foliationer, distance and multioners with abundant pyrite       -0.001       0.002       14       15       74       9       30       0.025         622531       Multiones, full whe opgrave guart with abundant pyrite       -0.001       -0.02       36       15       92       3       5.5       2.2       0.051         622650       CSF, takipar porphyny, disseminated pyrite       0.002       -0.02       3       16       26       4       10       2.9       0.512         622650       CSF, takipar porphyny, disseminated pyrite       0.002       -0.02       3       16       26       4       10       0.29       0.512         622650       CSF, takipar porphyny, disseminated pyrite       -0.001       -0.02       3       7       16       25       13       1.7       0.262         622823       Argillice V-3 Sign 71 an chip       -0.001       -0.02       8       17       52       3       2.1       -0.2       0.489       62/225       8       158       3       6.1       2.8       0.046         622825       Pirk phynite Mowtarskie ( <i 7<="" sign="" td="">       -0       0.001       -0.02       6       8       48       2       -1       0.2       0.011</i>	62629	Feisic Volcanic: precipited pyritic feisic fragmental	-0.001	-0.02	4	19	68	2	10	15	0.027
62231       Mudrons: Multi white opaque quarts white. Moles prysite prytholite 1%       -0.001       -0.02       36       15       52       3       5.5       5.2       0.070         622655       037. Magg quarts while Matemained prythe       -0.001       -0.02       3       16       26       4       10       2.9       0.512         622657       037. Magg quarts while Matemained prythe       0.003       -0.02       3       9       11       6       20       2.7       0.407         622625       C37. yellow ritheol. quarts pryth output states       -0.001       -0.02       3       7       16       25       13       1.7       0.225         622627       Capille w 2-3 % pry: an chip       -0.001       -0.02       8       17       52       3       2.1       -0.2       0.489         622625       2-3% Por- pin a carboanted DHUT wheaks; prin       -0.001       -0.02       5       8       156       3       6.1       2.6       0.44         622627       DHUT; folianed vaice (3 % pry)       -0.001       -0.02       7       15       99       6       -1       1.0       0.001         622625       Applies (4 % pry)       -0.001       -0.02       74       3 <td>62630</td> <td>Mudstone: foliated felsics and fractured mudstones with abundant pyrice</td> <td>-0.001</td> <td>0.02</td> <td>14</td> <td>15</td> <td>74</td> <td>ā</td> <td>30</td> <td>3.3</td> <td>0.053</td>	62630	Mudstone: foliated felsics and fractured mudstones with abundant pyrice	-0.001	0.02	14	15	74	ā	30	3.3	0.053
62665       037. (https://securits.tot.gr/me.secu	62631	Mudstone: bull white organic quartz veins, blebs pyrite pyritotize 1%	-0.001	-0.02	36	15	92	3	55	2.2	0.079
62666       QSP, vago quarta visus in factures, discuilanted pyrite       0.003       -0.02       3       16       26       4       10       2.9       0.012         62666       QSP, valow stalesd, quartz pyrite zoae       0.002       -0.02       3       9       11       6       20       2.7       0.407         62822       Argille w1-3.% pyrite zoae       -0.001       -0.02       3       9       11       6       20       2.7       0.407         62822       Argille w1-3.% pyrite zoae       -0.001       -0.02       4       8       14       7       1.4       0.6       0.168         62822       Argille w1-3.% pyrite zoae       -0.001       -0.02       5       8       158       3       6.1       2.6       0.489         62825       2-3% Pore pit is carboanted DHLT victuality grab       -0.001       -0.02       6       8       48       2       9.1       1.7       0.058         62825       2-3% Pore pit is carboanted DHLT victuality grap       -0.001       -0.02       7       5       77       2       -1       0.3       0.011         62825       Argibrobite 1.% py       -0.001       -0.02       77       5       77       2	62665	OSP. feldspar porphyry, disseminated pyrite	-0.001	-0.02	2	12	20	5	18	17	1 907
62867       OSP, yellow stated, quartz pyrke zoac       0.002       -0.02       3       9       11       6       20       2.7       0.401         62867       OSP, yellow stated, quartz pyrke zoac       0.002       -0.02       3       7       16       25       13       1.7       0.2865         62822       Argille wf 2-3% pyr 3 an chip       -0.001       -0.02       8       17       52       3       2.1       -0.2       0.469         62825       2.3% pr 3 yn cindowatot DILT wokank: grab       -0.001       -0.02       5       8       158       3       6.1       2.8       0.469         62825       Pag byrk flow(strukhe; (<1% pr)	62666	OSP, vuery quartz veins in fractures, disseminated rorite	0.003	-0.02	3	16	26	4	10	29	0.512
G2202       Argille w/ 2-3% py 3m chip       -0.001       -0.002       3       7       16       25       13       1.7       0.266         G2202       Argille w/ 2-3% py 3m chip       -0.001       -0.002       4       8       14       7       1.4       0.6       0.186         G2202       Argille w/ 2-3% py 3m chip       -0.001       -0.002       8       17       52       3       2.1       -0.00       0.02         G2202       Argille w/ 2-3% py 3m chip       -0.001       -0.02       5       8       158       3       6.1       2.6       0.046         G2202       PLT1: folined vok (3%p)       -0.001       -0.02       6       8       48       2       9.1       17       0.031         G2205       Amphitolite; 1-3% py       -0.001       -0.02       74       3       27       2       -1       0.8       0.011         G2205       Amphitolite; 1% py magnetic       -0.001       -0.02       74       3       27       2       -1       -0.2       0.011         G2205       Amphitolite; 1% py magnetic       -0.001       -0.02       71       3       3.7       1.48       12       1.0.3       0.0.01	62667	OSP, vellow stained, quartz nyrite zone	0.002	-0.02	3		11	6	20	2.5	0.407
62923       Argilke w/2-3% pr; 3m chp       -0.001       -0.02       4       8       14       7       1.4       0.01       0.02         62923       Argilke w/2-3% pr; 3m chp       -0.001       -0.02       8       17       52       3       2.1       -0.2       0.486         62924       Argilke w/2-3% pr; 3m chp       -0.001       -0.02       8       17       52       3       2.1       -0.2       0.486         62925       Piag phyrit howharuise; (-15% pr)       -0.001       -0.02       7       15       99       6       -1       1.2       0.059         62925       Mais volkmin-1-2% po la Incurso of pillow rim.Boat       -0.001       -0.02       74       3       27       2       -1       -0.2       0.011         62955       Anghibolic; 15% pr       -0.001       -0.02       77       5       77       2       -1       -0.2       0.011         62955       Anghibolic; 15% pr       -0.001       -0.02       74       3       27       2       -1       -0.2       0.011         62956       Maiko volkmis; 3% pr       -0.001       -0.02       71       2       2       2       0.011       -0.2       0.011	62922	Arrillite w/ 2-3% ov: 3m chip	-0.001	-0.02	. 3	7	16	25	13	17	0.265
62224       Argilia wi 2-3% pri 3 a chip       -0.001       -0.02       8       17       52       3       2.1       -0.2       0.489         62222       2-3% Porp is achoanted DHLT volensit; grab       -0.001       -0.02       5       8       156       3       6.1       2.6       0.0489         62222       PLLT; foliated vic (3% pr)       -0.001       -0.02       5       8       158       3       6.1       2.6       0.0489         62227       PLLT; foliated vic (3% pr)       -0.001       -0.02       6       8       48       2       9.1       1.7       0.031         625954       Mathibulie; 1-3% pr       -0.001       -0.02       64       4       38       2       -1       -0.2       0.011         625955       Amphbolie; 1% pr magnetic       -0.001       -0.02       57       5       77       2       -1       -0.2       0.011         625954       Anglikoukaca-3ra chip is contact with malis.       -0.001       -0.02       8       14       11       5       26       5       0.027         625956       Anglikoukaca-3ra Chip       -0.001       -0.02       8       14       11       5       0.26       1.52	62923	Araillite w/2~3% ov: 3m chip	~0.001	-0.02	Ă	8	14	7	14	0.6	0.186
62925       2-3% Pro-py in carbonated Dill. vokank; grab       -0.001       -0.02       5       8       158       3       6.1       2.6       0.046         62925       Pag phyric flow/intrushe; (c1% py)       -0.001       -0.02       7       15       99       6       -1       1.2       0.031         62925       Dill.T; (biata vok (3%py)       -0.001       -0.02       6       8       48       2       9.1       1.7       0.031         62955       Amphilolite; 1-3% py       -0.001       -0.02       6       8       48       2       9.1       0.7       0.031         62955       Amphilolite; 1-3% py       -0.001       -0.02       74       3       27       2       -1       -0.2       0.011         62955       Amphilolite; 1-3% py       -0.001       -0.02       11       2       4       -1       -1       0.3       -0.011         62957       Aplite; 1% py       -0.001       -0.02       8       14       11       5       26       5       0.027         62989       Matic vokanic; 5% dis py       -0.001       -0.02       8       14       11       5       26       5       0.027	62924	Areillac w/2-3% rw 3m chin	-0.001	-0.02	Å	17	52	3	21	-0.2	0.100
62226       Plag byth flowiktruske; (-15k pt)       -0.001       -0.02       7       15       99       6       -1       1.2       0.031         62227       PLILT; follated vok (3%p)       -0.001       -0.02       6       8       48       2       9.1       1.7       0.031         62955       Amphibolite; 1-3% py       intrustes of plaws flowing: 1-3% py       -0.001       -0.02       74       3       2.7       2       -1       -0.2       0.011         62955       Amphibolite; 1+3% py       -0.001       -0.02       74       3       2.7       2       -1       -0.2       0.011         62957       Amphibolite; 1+9 yr angotic       -0.001       -0.02       57       5       77       2       -1       -0.2       0.011         62958       Mudstone: 3 a chai at constet with mafks.       -0.001       -0.02       8       14       11       5       26       5       0.027         62989       Mudstone: 1-2% py       -0.001       -0.02       6       6       38       19       26       2       1.792         62990       Mudstone: 1-2% py       rth mafks.       -0.001       -0.02       7       2       22       24 <t< td=""><td>62925</td><td>2-396 Pa-rw in cathonated DHI T volcanic: erab</td><td>-0.001</td><td>-0.02</td><td>5</td><td>8</td><td>158</td><td>ă</td><td>£.1 6 1</td><td>2.6</td><td>0.403</td></t<>	62925	2-396 Pa-rw in cathonated DHI T volcanic: erab	-0.001	-0.02	5	8	158	ă	£.1 6 1	2.6	0.403
Carbon Control       Contro       Control       Control<	62926	Plae nhurin flow/intructure (~1% m)	-0.001	-0.02	7	15	99	6	_1	1 2	0.040
Construction       Constructin       Constructin       C	62927	DHI T: foliated work (3 there)	-0.001	-0.02	, A	· A	48	ž	01	17	0.033
62955       Amphibolist: 1-3% py       -0.001       -0.02       74       3       27       2       -1       -0.2       0.011         62956       Amphibolist: 1% py magnetic       -0.001       -0.02       57       5       77       2       -1       -0.2       0.011         62957       Aplits: 1% py magnetic       -0.001       -0.02       57       5       77       2       -1       -0.2       0.011         62957       Aplits: 1% py magnetic       -0.001       -0.02       8       14       11       5       6       5       0.027         62989       Malit: volkanist: 5% dis py       -0.001       -0.02       8       14       11       5       6       0.02       1.792         62989       Malit: volkanist: 5% dis py       -0.001       -0.02       21       7       10       24       20       2.8       1.431         62990       Mudstones: 1-2% py stingers       -0.001       -0.02       7       2       22       24       29       4.5       1.522         62993       DHLT; oldy qtz-py(20%)       -0.001       -0.02       7       16       33       42       21       29.8       2.866       6       6299	62954	Matic volcanic - 1 - 2% no in fractures of nillow rim, float	-0.001	0.02	84	Ă	38	5	-1	0.8	0.031
Capabilicite: 1% py       Angibicite: 1% py       Co.001       -0.02       17       5       77       2       -1       -0.2       C0.011         C2957       Aplite: 1% py       -0.001       -0.02       11       2       4       -1       -1       0.3       -0.01         C2957       Aplite: 1% py       -0.001       -0.02       11       2       4       -1       -1       0.3       -0.01         C2958       Maltic one link at contact with mafies.       -0.001       -0.02       8       14       11       5       26       5       0.027         C2988       Malticone: a thip at contact with mafies.       -0.001       -0.02       6       6       38       19       26       2       1.792         C2990       Muditone: 1-2% py timgers       -0.001       -0.02       6       6       38       19       26       2       1.792         C2990       Muditone: 1-2% py timgers       -0.001       -0.02       7       2       22       24       29       4.5       1.522         C2990       DHLT; typ atteration: 2-3% py; 1m chip.       -0.001       -0.02       7       16       33       42       21       29.8       2.866	62955	Annhibolite: 1-3% m	-0.001	~0.02	74	3	27	5	-1	-0.3	0.011
Capara Applies, 16 py       -0.001       -0.002       01       0.002       01       0.001       -0.001         62979       DHLT; silicous w(2% py       -0.001       -0.002       8       14       11       5       26       5       0.027         62988       Mudstone - 3m chip at contact with mafies.       -0.001       -0.02       8       14       11       5       26       5       0.027         62988       Mudstone - 3m chip at contact with mafies.       -0.001       -0.02       6       6       38       19       26       2       1.792         62989       Mudstone; 1-2% py stringers       -0.001       -0.02       21       7       110       24       20       2.8       1.431         62999       Mudstone; 1-2% py stringers       -0.001       -0.02       7       2       22       24       29       4.5       1.522         62993       DHLT; poddy qtz - py(20%)       -0.001       -0.02       3       -2       9       12       26       3.1       0.376         62994       DHLT; poddy qtz - py(20%)       -0.001       -0.02       7       16       33       42       21       29.8       2.866         62994	62956	Amphibolite: 196 py	-0.001	-0.02	57	š	77	2	-1	-0.2	0.011
Correct Indig       -0.001       -0.002       11       2       -1       -1       -1       0.03       -0.001         C62970       DHLT; siliccous w/ 2% py       -0.001       -0.002       8       14       11       5       26       5       0.027         62980       Mudstone-3m chip at contact with malics.       -0.001       -0.002       23       7       148       12       10       1.2       0.436         62980       Mudstone; 1% py       -0.001       -0.002       6       6       38       19       26       2       1.792         62990       Mudstone; 1-2% py stringers       -0.001       -0.002       21       7       110       24       20       2.8       1.431         62991       Mudstone; 1-2% py stringers       -0.001       -0.002       7       2       22       24       29       4.5       1.522         62992       DHLT; poddy qtz-py(20%)       -0.001       -0.002       7       16       33       42       21       29.8       2.866         62995       DHLT, oddy qtz-py(20%)       -0.001       -0.002       3       479       7       19       5.5       0.074         64870       Mudstone; s	62957	Anlite: 16 m	-0.001	-0.02	11	2		_1	-1	-0.2	-0.01
Carrier Direct, introders in Dry       Direct, introders in Dry       11       0       20       0       0.027         Carrier Direct, introders in Dry       marking at contact with marks.       -0.001       -0.002       23       7       148       12       10       1.2       0.436         Carrier Direct, introders in Dry       Muditone: 1-2% py stringers       -0.001       -0.002       21       7       110       24       20       2.8       1.431         Carrier Direct, includes in Log in Contact, it is py       -0.001       -0.002       21       7       110       24       20       2.8       1.431         Carrier Direct, includes in Log in Contact, it is py       -0.001       -0.002       27       2       22       24       29       4.5       1.525         Carrier Direct, include in Line Contact       -0.001       -0.002       7       16       33       42       21       29.8       2.866         Carrier Direct, is point at its py       -0.001       -0.002       7       16       33       42       21       29.8       2.866         Carrier Direct, is py in a contact with margine       -0.001       -0.002       2       9       9       4       14       8.7       1.002	62979	DHI T elipsone w/2% ou	~0.001	-0.02	8	14	11	-1	26	0.5	0.01
62000       Multional - Julting at context with minick.       0.001       -0.02       20       7       140       12       10       1.2       0.430         62030       Multionar: 5% dis py       -0.001       -0.02       6       6       38       19       26       2       1.792         62990       Mudstone: 1-2% py stringers       -0.001       -0.02       46       14       81       52       50       4.4       1.151         62992       DHLT; QSP alteration; 2-3% py; 1n chip.       -0.001       -0.02       7       2       22       24       29       4.5       1.522         62994       DHLT; poddy qtz-py(20%)       -0.001       -0.02       3       -2       9       12       26       3.1       0.376         62995       DHLT- qsp alteration       -0.001       -0.02       7       16       33       42       21       29.8       2.866         62995       DHLT- qsp alteration       -0.001       -0.02       32       3       479       7       19       5.5       0.074         64870       Mudstone; 20cm gauge zone parallel to bedding, whithin arguilke       -0.001       -0.02       110       2       89       5       3.8       <	62988	Mudetone - 3m ship at contact with mafire	-0.001	-0.02	23	7	148	12	10	1 2	0.027
62900       Mudstone; 1% py       -0.001       -0.02       21       7       110       24       20       2.8       1.1/92         62991       Mudstone; 1-2% py stringers       -0.001       -0.02       21       7       110       24       20       2.8       1.1/92         62992       DHLT; QSP alteration; 2-3% py; 1m chip.       -0.001       -0.02       46       14       81       52       50       4.4       1.151         62992       DHLT; QSP alteration; 2-3% py; 1m chip.       -0.001       -0.02       3       -2       9       12       26       3.1       0.376         62994       DHLT; poddy qtz-py(20%)       -0.001       -0.02       3       -2       9       12       26       3.1       0.376         62995       DHLT; poddy qtz-py(20%)       -0.001       -0.02       2       9       9       4       14       8.7       5       0.074         64870       Mudstone; 20cm gauge zone parallel to bedding, whin argilike       -0.001       -0.02       110       2       89       5       3.8       2.4       0.062         64871       Felic Volcank; sidd in to felic fragmental with vaggy py zones       -0.001       -0.02       71       -2       <	62089	Madestolic - Sal chip at contact while matics,	-0.001	-0.02	20	, 6	- 170	10	20	1.2	1 700
62350       Individue, 1-3% py       -0.001       -0.02       21       1       10       24       20       2.5       1.431         62991       Mudstone, 1-2% py stringers       -0.001       -0.02       46       14       81       52       50       4.4       1.151         62992       DHLT; QSP alteration; 2-3% py; 1m chip.       -0.001       -0.02       7       2       22       24       29       4.5       1.522         62993       DHLT; poddy qtz-py(20%)       -0.001       -0.02       3       -2       9       12       26       3.1       0.376         62994       DHLT; poddy qtz-py(20%)       -0.001       -0.02       7       16       33       42       21       29.8       2.866         62995       DHLT- qsp alteration       -0.001       -0.02       2       9       9       4       14       8.7       1.002         64870       Mudstone; side in to felsic fragmental with vagy py zones       -0.001       -0.02       3       479       7       19       5.5       0.074         64871       Felsic Volcank; side in to felsic fragmental with vagy py zones       -0.001       -0.02       110       2       89       5       3.8	62000	Muditores = 100 ms py	-0.001	-0.02	21	7	110	19	20	2	1.792
62551       Hullstone, 1-2% py stragers       -0.001       -0.02       40       14       51       52       50       4.4       1.151         62992       DHLT; OSP alteration; 2-3% py; 1m chip.       -0.001       -0.02       7       2       22       24       29       4.5       1.522         62993       DHLT; poddy qiz-py(20%)       -0.001       -0.02       7       2       22       24       29       4.5       1.522         62994       DHLT; poddy qiz-py(20%)       -0.001       -0.02       7       16       33       42       21       29.8       2.866         62995       DHLT- qsp alteration       -0.001       -0.02       3       479       7       19       5.5       0.074         64870       Mudstone; 20cm gauge zone parallel to bedding, within argilike       -0.001       -0.02       32       3       479       7       19       5.5       0.074         64871       Febic Volcank; sild int to feisic fragmental with wagy pry zones       -0.001       -0.02       110       2       89       5       3.8       2.4       0.062         64877       AMPHIBOLITE, black apmhibolite tuff, quartz sweats, semi massive po       -0.001       -0.002       71       -2	62991	Mudstones, < 170 py	-0.001	-0.02	21	14	91	24 50	20	2.0	1.431
62593       DHLT; Qor attended, 2-36 py, in thip.       -0.001       -0.02       7       2       22       24       29       4,5       1.522         62993       DHLT; poddy qt2-py(20%)       -0.001       -0.02       3       -2       9       12       26       3,1       0.376         62994       DHLT; poddy qt2-py(20%)       -0.001       -0.02       7       16       33       42       21       29.8       2.866         62995       DHLT- qsp alteration       -0.001       -0.02       2       9       9       4       14       8.7       1.002         64870       Mudstone; 20cm gauge zone parallel to bedding, within argillke       -0.001       -0.02       32       3       479       7       19       5.5       0.074         64871       Febic Volcanic; 3id in to feisic fragmental with 'uggy prones       -0.001       -0.02       110       2       89       5       3.8       2.4       0.062         64877       AMPHIBOLITE, black spinhibolitic tuff, quartz sweats, seni massive po       -0.001       -0.02       71       -2       65       3       1.7       -0.2       0.022         64880       MIGMATTTE, black with white banded migmatite, mal       -0.001       -0.02	62002	DLT T: OSP alteration: 2 - 26 mr 1 m ab -	-0.001	-0.02	-40	2	22	02		4.4	1.101
62333       DHL1; poddy qt2-py(20%)       -0.001       -0.02       3       -2       9       12       20       3.1       0.378         62994       DHLT; poddy qt2-py(20%)       -0.001       -0.02       7       16       33       42       21       29.8       2.866         62995       DHLT- qsp alteration       -0.001       -0.02       2       9       9       4       4       8.7       1.002         64870       Mudstone; 20cm gauge zone parallel to bedding, within argilike       -0.001       -0.02       32       3       479       7       19       5.5       0.074         64870       Mudstone; 20cm gauge zone parallel to bedding, within argilike       -0.001       -0.02       32       3       479       7       19       5.5       0.074         64871       Febic Volcanic; idd in to feisic fragmental with vaggy py zones       -0.001       -0.02       110       2       89       5       3.8       2.4       0.062         648877       AMPHIBOLITE, sight with white banded migmatife, mail       -0.001       -0.02       71       -2       65       3       1.7       -0.2       0.022         64880       MIGMATTTH, black with white banded migmatife, mal       -0.001       -0.02<	62003	Diff. Ti noddu sta	-0.001	-0.02	,	2	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	10	29	4.5	1.522
62594DHL1; polay ql2 - py(20%)-0.001-0.0271633422129.62.686 $62995$ DHLT- qsp alteration-0.001-0.022994148.71.002 $64870$ Mudstone; 20cm gauge zone parallel to bedding, within argilike-0.001-0.023234797195.50.074 $64871$ Febic Volcanic; 3id in to febic fragmental with vaggy py zones-0.001-0.023128953.82.40.062 $64876$ AMPHIBOLITE, suphibolite tuff, quartz sweats, semi massive po-0.001-0.0271-26531.7-0.20.022 $64880$ MIGMATTTE, black with white banded migmatite, mal-0.001-0.0271-26531.7-0.20.022 $64886$ QSSP, quartz sericite pyrite schist/ruff, quartz vein-0.001-0.028420536757.80.183 $64887$ QSSP, rusty white/grey quartz flooded sericite/schist, py, cpy0.0020.0263443.11.30.064	62004	DILLT; poddy qtz-py(20%)		-0.02	37	-2	30	12	20	3.1	0.376
-0.001 $-0.02$ $2$ $3$ $4$ $14$ $6.7$ $1.002$ 64870Mudstone; 20cm gauge zone parallel to bedding, wikin argilike $-0.001$ $-0.02$ $32$ $3$ $479$ $7$ $19$ $5.5$ $0.074$ 64871Febic Vokanic; 3id in to felsic fragmental with vaggy py zones $-0.001$ $-0.02$ $310$ $2$ $89$ $5$ $3.8$ $2.4$ $0.062$ 64876AMPHIBOLITE, amphibolite tuff, quartz sweats, semi massive po $-0.001$ $-0.02$ $71$ $-2$ $65$ $3$ $1.7$ $-0.2$ $0.022$ 64887MIGMATTTH, black with white banded migmatite, mal $-0.001$ $-0.02$ $71$ $-2$ $65$ $3$ $1.7$ $-0.2$ $0.022$ 64880MIGMATTTH, black with white banded migmatite, mal $-0.001$ $-0.02$ $201$ $4$ $49$ $1$ $-1$ $1.1$ $0.01$ 64885VOLCANIC TUFF, breeciated tuff with pyrite matrix $-0.001$ $-0.02$ $84$ $20$ $53$ $6$ $75$ $7.8$ $0.183$ 64886QSSP, quartz sericite pyrite schist/rafi, quartz vein $-0.001$ $-0.02$ $6$ $3$ $4$ $4$ $3.1$ $1.3$ $0.064$	62005	DHLT; poddy qt2-py(20%)	-0,001	-0.02	,	0		42	21	29.0	2,000
64870Horizone: Joint guige toole paradic to be definit, which arguine $-0.001$ $-0.02$ $32$ $3$ $479$ $7$ $19$ $5.5$ $0.074$ 64871Felic Vokanic; sild int to felic fragmental with vaggy py zones $-0.001$ $-0.02$ $110$ $2$ $89$ $5$ $3.8$ $2.4$ $0.062$ 64876AMPHIBOLITE, amphibolite uif, quartz sweats, semi massive po $-0.001$ $-0.02$ $110$ $2$ $89$ $5$ $3.8$ $2.4$ $0.062$ 64877AMPHIBOLITE, black symbibolite, py/po opidote $-0.001$ $-0.02$ $71$ $-2$ $65$ $3$ $1.7$ $-0.2$ $0.022$ 64880MIGMATTIE, black with white banded migmatite, mal $-0.001$ $-0.02$ $201$ $4$ $49$ $1$ $-1$ $1.1$ $0.01$ 64885VOLCANIC TUFF, breecisted tuff with pyrite matrix $-0.001$ $-0.02$ $14$ $6$ $20$ $22$ $174$ $145$ $28.388$ 64886QSSP, quartz sericite pyrite schist/ruff, quartz vein $-0.001$ $-0.02$ $6$ $3$ $4$ $4$ $3.1$ $1.3$ $0.064$	64970	Drift I ~ dsp alteration	-0.001	-0.02	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	9	470	4	14	8.7	1.002
64871Perise Volcane; sid mt to feisic fragmental win Viggy py zones $-0.001$ $-0.02$ $110$ $2$ $89$ $5$ $3.8$ $2.4$ $0.062$ $64876$ AMPHIBOLITE, smphibolite tuff, quartz sweats, semi massive po $-0.001$ $0.06$ $249$ $-2$ $110$ $3$ $13$ $6.6$ $0.024$ $64877$ AMPHIBOLITE, black spmhibolite, py/po epidote $-0.001$ $-0.02$ $71$ $-2$ $65$ $3$ $1.7$ $-0.2$ $0.022$ $64880$ MIGMATTIE, black with white banded migmatite, mal $-0.001$ $-0.02$ $201$ $4$ $49$ $1$ $-1$ $1.1$ $0.01$ $64885$ VOLCANIC TUFF, breecisted tuff with pyrite matrix $-0.001$ $-0.02$ $14$ $6$ $20$ $22$ $174$ $145$ $28.388$ $64886$ QSSP, quartz sericite pyrite schist/ruff, quartz vein $-0.001$ $-0.02$ $64$ $20$ $53$ $6$ $75$ $7.8$ $0.183$ $64887$ QSSP, rusty white/grey quartz flooded sericite/schist, py, cpy $0.002$ $0.02$ $6$ $3$ $4$ $4$ $3.1$ $1.3$ $0.064$	64071	Mudsione, 20cm gauge zone paradei to bestamy, wiism arginke	-0.001	~0.02	32	3	4/9	ć	19	5.5	0.074
C+G/GAMPTHEOLITE, superconte tuit, quartz sweats, semi massive po $-0.001$ $0.06$ $249$ $-2$ $110$ $3$ $13$ $6.6$ $0.024$ $64877$ AMPHIBOLITE, black spinholdite, py/po opidote $-0.001$ $-0.02$ $71$ $-2$ $65$ $3$ $1.7$ $-0.2$ $0.022$ $64880$ MIGMATTIE, black with white banded migmatite, mal $-0.001$ $-0.02$ $201$ $4$ $49$ $1$ $-1$ $1.1$ $0.01$ $64885$ VOLCANIC TUFF, breecisted tuff with pyrite matrix $-0.001$ $-0.02$ $14$ $6$ $20$ $22$ $174$ $145$ $28.388$ $64886$ QSSP, quartz sericite pyrite schist/tuff, quartz vein $-0.001$ $-0.02$ $84$ $20$ $53$ $6$ $75$ $7.8$ $0.183$ $64887$ QSSP, rusty white/grey quartz flooded sericite/schist, py, cpy $0.002$ $0.02$ $6$ $3$ $4$ $4$ $3.1$ $1.3$ $0.064$	64070	reise vokanic; suo mi to teisie tragmental wan vuggy py zones	-0.001	-0.02	110	2	55	5	3,8	2.4	0.062
64871AMPHIBOLITE, black spinsholde, py/p6 epside $-0.02$ $71$ $-2$ $63$ $3$ $1.7$ $-0.2$ $0.022$ 64880MIGMATTIE, black with white banded migmatite, mal $-0.001$ $-0.02$ $201$ $4$ $49$ $1$ $-1$ $1.1$ $0.01$ 64885VOLCANIC TUFF, breecisted tuff with pyrite matrix $-0.001$ $-0.02$ $14$ $6$ $20$ $22$ $174$ $145$ $28.388$ 64886QSSP, quartz sericite pyrite schist/tuff, quartz vein $-0.001$ $-0.02$ $84$ $20$ $53$ $6$ $75$ $7.8$ $0.183$ 64887QSSP, rusty white/grey quartz flooded sericite/schist, py, cpy $0.002$ $0.02$ $6$ $3$ $4$ $4$ $3.1$ $1.3$ $0.064$	64070	AMPHIBOLITE, amphibolite tuit, quanz sweats, semi massive po	-0.001	0.06	249	-2	110	3	13	6,6	0.024
04000 MIGMATTIB, black with white banded migmatife, mal       -0.001       -0.02       201       4       49       1       -1       1,1       0,01         64885       VOLCANIC TUFF, breecisted tuff with pyrite matrix       -0.001       -0.02       14       6       20       22       174       145       28.388         64886       QSSP, quartz sericite pyrite schist/tuff, quartz vein       -0.001       -0.02       84       20       53       6       75       7.8       0.183         64887       QSSP, rusty white/grey quartz flooded sericite/schist, py, cpy       0.002       0.02       6       3       4       4       3.1       1.3       0.064	040//	AMTHIBULITE, MACK SPIENDOUSE, PY/PO CPXIOTE	-0.001	~0.02	/1	-2	65	3	1.7	-0.2	0.022
04000 VOLCANIC TUFF, breecisted tuff with pyrite matrix       -0.001       -0.02       14       6       20       22       174       145       28.388         64886       QSSP, quartz sericite pyrite schist/tuff, quartz vein.       -0.001       -0.02       84       20       53       6       75       7.8       0.183         64887       QSSP, rusty white/grey quartz flooded sericite/schist, py, cpy       0.002       0.02       6       3       4       4       3.1       1.3       0.064	04880	MIGMATTIE, black with white banded migmatite, mai	-0.001	-0.02	201	4	49	1	-1	1.1	0.01
04880   QSSP, quartz sericite pyrite schist/ruff, quartz vein.       -0.001       -0.02       84       20       53       6       75       7.8       0.183         64887   QSSP, nusty white/grey quartz flooded sericite/schist, py, cpy       0.002       0.02       6       3       4       4       3.1       1.3       0.064	04885	VOLCANIC TUFF, brecciated tuff with pyrite matrix	-0,001	-0.02	14	6	20	22	174	145	28.388
0400/ USSP, nusty white/grey quartz flooded serie#e/sehist, py, cpy   0.002 0.02 6 3 4 4 3.1 1.3 0.064	04886	QSSF, quantz sericite pyrite schist/tuff, quartz vein	0.001	~0.02	84	20	53	6	75	7.8	0.183
	64887	QSSP, rusty white/grey quartz flooded seric#c/schist, py, cpy	0,002	0.02	6	3	4	4	3,1	1.3	0.064

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### Homestake Corona 1992 Assay Results Kenrich Corey Claims

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ICC #	Description	Au	Ag	Cu	Pb	Zn	Mo	As	Sb	Hg
64888	DACITE, flow Breccia, siliceous volcanic black py matrix, dark green fragments	-0.001	-0.02	25	6	126	5	6.4	1.4	0.045
64889	QSS, pink/brown weathered, moderately foliated green sericite schist/tuff	-0.001	0.04	92	3	85	1	5.8	4.7	0.047
64896	QPS, quariz/pyrite/sericite alteration zone, honeycomb froath carbonate blades	0.008	0.42	50	342	287	2	352	31.5	3.472
64897	METAVOLCANIC, with 2% disseminated py, po at intrusive contact	0.002	0.04	196	93	312	4	17	1.9	0.058
64898	QVN, rusty pyritic breeciated quartz vein	0.025	0. <del>9</del> 7	185	6	61	21	5	1.1	0.044
72625	QVNS; bull white translucent quartz veins within andesite/diorite	-0.001	-0.02	3	10	42	5	-1	-0.2	0.033
72630	METAVOLCANIC, black baaded rusty heavy, py/pa	0.001	0.06	141	5	91	17	10	1.8	0.03
72641	Spring; white precipitate from dry creek on rusty metasiltstone	-0.001	0.05	32	12	127	10	8.4	4	0.058
72642	Mafie Volcanic; shear zone in green ves volcanic flow and f gr mass bi volc	-0.001	-0.02	50	16	130	12	16	2.6	0.028
72643	Mudstone; (HW) silicified in vic. of footwall diabase dyke	-0.001	-0.02	26	10	133	6	1.7	1.2	0.081
72644	MSUL; HG lense of sulphides, pyrite, trace chalcopyrite	0.001	-0.02	184	13	43	19	-1	0.7	0.011
72645	QSP; 5-7% disseminated pyrite	0.004	0.12	15	3	56	3	26	4.1	0.231
72646	Mudstone; pyritic	-0,001	-0.02	43	21	290	70	14	7.1	0.3
72649	QACV; siderite carbonate vein	-0.001	-0.02	-1	9	35	1	1.8	-0.2	0.011
72650	QCV: 20-25cm, parallel to foliation, mafic rust, host metamorphic unit	-0.001	0.08	21	3	10	1	-1	-0.2	-0.01
72651	Andesite; footwall metamorphic rock, foliated	-0.001	0.04	824	-2	1712	3	6.8	~0.2	0.03
72652	QVN; pyritic vuggy quartz vein, trace chalcopyrite	0.002	0.08	832	-2	793	5	4	1.4	0.168
72653	Andesite; footwall metamorphic rock, foliated	-0.001	0.04	145	-2	72	3	3.6	0.8	-0.01
72654	QBXVN: pyritic, trace chalcopyrite, malachite, azurite	-0.001	0.22	1579	7	4921	2	19	0.7	0.051
72655	Aplite: pyritic aplite dyke	-0.001	0.04	9	3	18	2	2.6	-0.2	-0.01
72657	Wacke: black cakareous equisranular w/ blobs pyrite, pyrthotite	0.001	-0.02	30	15	86	7	6.4	1.1	0.07
72658	Mudstone: cross cutting pyritic veinlets	-0.001	-0.02	22	13	41	8	29	2.2	0.067
72659	Felsic Volcanic; debris flow, chlorite, frats in bk sil py matrix	-0.001	~0.02	9	14	41	6	20	3.8	0.131
72660	Felsic Volcanic; debris flow, black siliceous pyritic matrix	0.001	-0.02	10	23	190	6	23	2,9	0.429
72661	Fragmental volcanic; 3m clay altered bleached bad pmictic dbf, po fragments	0.001	0.03	7	12	86	7	3,8	1.1	0.032
72662	Mudstone; szn 1m wide m py w/ sed matrix. Breccia zone, fining south	-0.001	-0.02	7	7	79	8	25	2.6	0.085
72663	QVN; py quartz lense 3mx 15m within wacke host	0.001	0.03	7	24	11	9	66	7.8	0.52
72664	Chert; propyi altd, fractd sediments, 5% diss py.	-0.001	0.02	9	25	25	11	247	14	0.621
72670	DHLT; altd felsic fragmental, strongly foliated	-0.001	0.12	4	3	74	4	28	3.7	0.162
80365		-0.001	-0.02	11	15	38	26	1.6	1.7	0.198
80366		-0.001	-0.02	41	13	121	19	11	3.4	0.274
80367		-0.001	0.04	103	18	148	5	45	7.9	0.104
80368		-0.001	-0.02	2	2	10	-1	~1	-0.2	0.015
80372		0.001	-0.02	17	15	49	5	70	3.1	0.031
80374		~0.001	0.05	19	13	77	6	53	- 5.1	0.03 į
80375		-0.001	0.04	71	13	154	2	18	3.4	0.024
80376		-0.001	-0.02	74	3	72	2	18	1.7	0.019
80377		0.001	0.22	37	57	31	8	54	14	0.117
80378		0.001	0.02	12	12	64	3	42	2	0.03
80901	Rhyolite; BMBX with 1% pyrite	-0.001	-0.02	9	11	42	6	28	3.3	0.035
80902	QVN; dyke cutting bk mtx wt fragmental rhyolite	-0.001	-0.02	3	79	151	2	2.3	0.7	0.096
80903	Rhyolite; fractured pale green with pyrite and pyrthotite	-0.001	-0.02	6	4	111	3	4	0.8	0.04
80904	Rhyolite; polyithic black matrix with remnant box work	-0.001	~0.02	5	7	50	5	4.4	1.6	0.06
80905	Wacke; gy- gn ispathic i grd wacks with pyrrhotite blebs	-0.001	0.02	5	7	83	4	7.4	1	0.063
80906	Mudstone; with pyrite lenses and fracture filling	-0.001	-0.02	16	11	48	4	27	2,8	0.169
80907	Rhyolite; E92-47 monolithic fragmental with disseminated pyrite	0.002	0.06	3	6	127	1	-1	0.7	D.036)
80908	Rhyolite; fractd mlithic fragmental with po-py	-0.001	0.06	23	13	150	3	1.7	1	0.025
80909	Dacise; grey/blue DHLT with pyrthotise	-0.001	-0.02	4	5	105	3	6.8	0.6	0.023
80910	Mudstone; pyritic fractured grey silicified sediment	-0.001	0.08	21	9	113	4	30	6.5	0.12

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ICC # Description	Au	Ag	Cu	Pb	Zn	Мо	As	Sb	Hg	AI203
64777 DACITE, rusty siliceous magnetic grey fractured ash tuff	-5	0.7	161	2	68	2	2.1	0.6	0.013	16.13
64778 DACITE bk gy felsic layer with pyrite bands	-5	0.6	91	3	68	2	7.9	0.5	0.028	12.78
64779 ANDESITE pale green vesicular intermediate flow	-5	0.8	35	-2	89	2	22	3.2	0.024	16.7
64780 ANDESITE pale apple green mottled volcanic flow at contact with situtone	-5	0.7	67	-2	76	3	-1	0,9	0.027	15.16
64781 CONGLOMERATE 40cm ispar porphyry boulder cgi, host black siliceous mud	5	0.8	67	2	95	2	1.5	0.6	0.02	18.86
64782 Mafic Volcanic; mega vesicular pillow, pillow flow unit	-5	0.7	35	3	89	3	1.4	0.5	0.019	16,19
64783 Matic Volcanic; white grey fine grained flow/pillow unit	5	0.7	62	3	95	2	3.3	0.5	0.015	14.42
64784 FELDSPAR PORPHYRY massive coarse grained	-5	0.3	61	5	58	3	2.6	0.6	0.011	15.52
64785 DACITE wish/felsic feldspar phyric volcanic flow	-5	0.7	62	5	92	4	-1	0.9	0.03	15.65
64785 ANDESITE It gn ispar augite pphyry intermediate volcanic flow, blebs po	-5	0.7	61	-2	55	3	-1	0.8	0.015	18.88
64787 ANDESITE sy m gr. intermediate any augite porphyry pillow unit	-5	0.6	18	-2	85	2	2	0.5	0.013	15.63
64788 ANDESITE pale grey intermediate pillow unit	-5	0.6	23	3	87	2	2.5	0.5	0.015	14.36
64789 ANDESITE Bx; w- gy broken pillow unit, qtz phenos & argillite frags, po	-5	1.2	13	-2	29	2	3.7	5.8	0.167	14.43
64790 DACITE grey felsic volcanic, angular fragmental, black siliccous matrix	-5	0.4	58	-2	110	3	1.4	0.2	0.022	14.35
64791 DACITE pale green grey, pyroxene/sugite porphyry dacite tull/flow?	-5	0.9	41	4	96	4	1.3	0.7	0.016	15.76
72684 DACITE, dacite/thyodacite layers with quartz filled tension pashes	-5	-0.2	1	29	71	1	2.3	0.9	0.106	8.8
72685 RHYODACITE, weakly foliated ispar porph. rhyodacite, cc alteration	-5	-0.2	<b>~</b> 1	15	49	2	1.4	1.1	0.015	9.73
72686 DACITE, weakly ioliated ispar porph. thyodacite, cc alteration	-5	-0.2	4	4	132	2	2.4	1.7	0.486	16.16
72687 DACITE, fresh ga fspar pphyry fragmental, schistose, eu pyrite	-5	-0.2	1	4	38	1	3.6	1.4	0.118	14.08
72690 SEDIMENT, black argilite with pyrite laminae, Fe stained	-5	-0.2	20	14	55	13	22	3	0.364	15.78
73677 AMPHIBOLITE, bk ry wi banded & siliceous w fracture pyrite	22	-0.2	103	4	17	5	2.6	-0.2	-0.01	14.2
73686 DACITE, gn m gr bjotite diorite/quartz diorite, weak chlorite alteration	-5	0.3	13	2	137	3	3	1.5	0.059	15.83
73687 Chert; fractid ga-gy cherty sediment with weak k-spar alteration	-5	0.3	28	15	100	3	6.6	1.6	0.038	19.36
73688 Wacke; fract'd gn wacke with malic fragments	-5	0.3	30	8	110	4	8.8	0.9	0.057	18.2
73689 Wacke;*******	-5	0.3	62	. 4	50	3	11	1.1	0.04	19.23
73690 DACITE, p gy f gr int to felsic fspar astal lithic tuff, dissd py/po <1%	-5	0.2	6	-2	136	4	2	0.5	0.041	15.23
73691 ANDESITE, pale grey feldspar porphyry volcanic, disseminated po	-5	0.2	4	-2	100	4	7.3	1.7	0.063	14.86
73692 DACITE, foliated vesicular stretched dacke pillow unit	-5	0.6	9	4	131	4	6.6	2	0.113	14.14
73693 ANDESITE, intermediate green banded tuff	-5	0.3	37	-2	77	3	3	-0.2	0.014	18.02
73694 Chert; banded cherty black and white sediment	-5	0.5	39	3	289	9	1.4	0.6	0.115	11.78
73695 RHYOLITE, saliceous felsic stretched welded tuff, strongly foliated	10	-0.2	8	~2	165	2	1.7	1	0.104	13.84
80362 Dacite tuff. Dark grey feldspar phyric tuff. Silicified with patchy pyrite.	-5	-0.2	3	15	13	4			0.051	13.6
80363 Betty Ck., Eskay Member equivalent. Foliated, silicified monomictic grey tuff.	6	-0.2	5	16	91	2			0.109	12.8
80364 Felsic tuff. Sil, hem tuff with fgr siliceous and feklspar phyric fragments.	-5	-0.2	8	7	39	5			0.134	13.33
80369 Salmon river basalt. Mixed pillow basalt and flow breccia.	6	0.2	71	4	53	4			0.02	10.52
80370 Salmon River chert. Black cherty sediments.	120	2.4	14	16	18	6			0.077	16.89
80371 Salmon River basalt. Fine grained basalt and flow breecha.	-5	0.3	45	9	64	6			0.011	15.44
80373 Basalt sill. Fine grained sill or dyke	6	0.6	23	7	161	5			0.02	14.88
80379 Dacite sill? Grey green, sugary breccia to aphanitic flow?	-5	-0.2	111	3	15	2			0.018	15.54
80380 Siliceous sill? Fine grained, very siliceous in silicified siltstone, chert.	-5	0.3	17	2	126	5			0.024	13.11
80381 Altered intrusive. Siliceous, fgr monzonite/diorite with ser-chl-py and mt.	-5	-0.2	1	6	36	-1			0.014	13.41
80382 Basalt sill.	10	0.5	6	3	123	4			0.018	14.02

#### Homestake Corona 1992 Whole Rock Results Kenrich Corey Claims

ICC #	Description	Au	Ag	Cu	Pb	Zn	Mo	As	Sb	Hg	A1203
KR92-003		-5	-0.2	67	6	123				-0.010	13.82
KR92-004	H Contraction of the second seco	-5	-0.2	59	4	107	2			0.010	15.53
E-27b	Mafic intrusive; 30% fspar 40% chlz'd hbls.	-5	0.6	9	12	130	3	8.7	1.7	0.07	15.31
E-28	Andeshic tuff/wacke; v. simm. to East Ridge member	5	-0.2	31	~2	86	-1	1	0.8	0.017	17.2
E-30	DHLT- dark matrix breccia; possible bx dyke	-5	0.3	9	11	92	2	7.2	0.6	0.023	12.17
E-32	DHLT-creaulated with 7% py	-5	0.3	4	5	136	-1	1.8	0.8	0.187	13.83
E-33	Dacitic tuff; felspar phyric; 2-5% py.	-5	0.4	5	11	30	10	16	2.3	0.13	13.35
E-34	Argilite with some fossils & pyrite (2%)	-5	0.4	8	8	37	4	23	2.2	2.615	14.58
E-35	DHLT; sil'n & seri'z. 2-3% py	) ~5	0.2	3	12	11	6	11	2.2	0.205	13.62
E-36	Massive Basaltic flow/intrusive	-5	0.2	23	4	70	-1	-1	0.7	0.017	14.39
E-37	Mafic flow; feldspar phyric; amygdular	-5	0.4	43	-2	86	-1	-1	-0.2	0.031	18.96
E-38	Mafic pillow flow top	-5	0.3	49	~2	76	1	1.9	0.7	0.03	15.79
E-39	Mudstone; interbedded with the pillowed basalts.	-5	0.5	29	4	83	2	1.2	0.4	0.073	10.07
E-41	Mafic volcanic; pillowed.	-5	0.5	66	-2	91	1	2.7	0.9	0.022	14.74
E-42	Dacitic monomictic tuff-fragmental.	-5	-0.2	49	-2	83	-1	- t	1.1	0.019	14.7
E-43	Intermediate pillowed volcanics.	-5	0.5	48	4	96	-1	4.5	2.4	0.023	16.1
E-45	Fragmental intrusive; polymictic dk mtx bx.	-5	0.4	49	14	86	2	35	1.6	0.458	15.53
E-47	DHLT; welded.	5	0.6	26	17	85	4	12	1,8	0.021	14.09
E-48	DALT; ash and Japilli tuffs.	-5	0.4	13	18	80	4	5.4	1.7	0.063	13.03
E-49	Rhyolite; welded fragmental.	-5	0.3	1	15	109	3	5.7	1.4	0.075	13.52
E-50	Rhyolite; ser and 1-2% py brd.	-5	-0.2	3	14	76	4	6.9	1,8	0.048	12.61
E-51	Fragmental; dark mix, rholite clasts, monolikhic	) -5	0.5	7	15	118	4	5.6	1.1	0.159	14.84
E-54	Rhyolite Bx; grey; wekled lapilli tulf w/ mafic fiamme	10	0.5	9	18	115	2	10	1.2	-0.01	13.59
E56	Mafic intrusive	-5	0.6	57	. 9	75	5	7.2	1,8	0.01	15.78
E-58	Mudstone; thinly bedded a minated	-5	0.2	4	4	16	4	2.3	0.5	0.015	11.91
E-59	Mafic voles; pillowed west facing	-5	0.6	33	4	68	4	7.9	3.4	0.02	19.58
E92-341	Gabbro; HBL-plag magnetite	~5	0.2	11	4	82	-1	-1	8,0	-0.01	15.86
E92~358a	Felsic volcanic; QSP altered DHLT	-5	-0.2	-1	4	23	-1	2.4	1,3	0.2	15.34
E92-359	Fspar Porphyry; 'Premier-type'	-5	~0.2	4	17	19	2	10	3.3	0.935	14.62
E92-403	QSP altered DHLT	-5	0.4	6	(	12	4	18	3	0.411	10.90
E92-407	DHLT; sheared with 1-2% po		0.2	-1	-2	147	3 E	1	-0.2	0,360	14.90
E92-409b	DHILT; crenulated	~5 5	0.4	8	4	104	5	2.9	3.4	0.300	17.40
1292-4090	DHLT; creaulated		0.3	*	-2	124	-1	67	4,0	0.400	12.76
E92-428	Lithic wacke	-5	-0.2	2	9		-1	0.7	2.4	0.101	12 70
1292-42/	Rhyolae	-5	-0.2	2	3	124	-1	0.0	2.1	0.231	14.66
E92-425	Highly foliated matic volcanic	-5	-0.2	1		95	J 4	2.3	1.0	0.231	14.00
E92-424a	Massive Ispar phyric intermediate flow	-5	0.2	*	3	193		20	1.2	0.07	12 22
102-4240	intermediate volcanic tragmental	-5	-0.2	4 E	22	30		2.3	0.0	0.071	19.12
03/74	KHYOLITE pale green materalization fractured myolite	-5	-0.2	21	18	110	-1	0.0	0.0	0.071	16 52
03775	RHYOLITE now banded weakly k-spar altered myolike	-5	~0.2	∠ I 10	10	150		22	2.7	0.000	17.67
03//0	RHYOLITE tod py,"non-pyritic section", dacide to augue porphry	-5	-0.2	10	14	100	-1	152	2.7	0.021	15.62
63///	DACITE salutied dacate tragmental with blebs pyrmotife 3%	14 E	-0.2	20	14	40	_1	-1	0.2	0.043	16.02
03//8	DIOKITE mega tekispar porphyry diorae	-5	-0.2	42	4	407	-1	-1	- V.Z A B	0.021	10.2
64/52	SCHINT, totated sericite schist, py	-5	0.0	21 170	3 6	131	ے 1	10	-0.2		10.01
64/53	DACITE, pale green weakly welded ash tuti, quartz vens	-0	0.0	170	0	- 50 E	-1	1.8	0.2	-0.01	19.65
64758	FELSTIE, white imed grained felsic intrusive, specular hematike, cpy, py		U.3 4	4	3	460	2	1.3		0.013	10.00
64/65	DACITE, flow breccia, siliceous, black pyritic matrix, dark green fragments	[ ~ <u>p</u>	1	10	4	109	4	3	ס.ן לה	0,020	14 00
64771	DACITE, rusty siliceous magnetic grey fractured ash tuff	-5	0.6	59	3	23	2	1.0	0.7	0,010	10.00
64772	ANDESITE, welded polylithic lapill/flow bx, grey frags, dark matrix, hematite	-5	0.5	16	10	142	3	14	2.3	0.037	15.05
64773	DIORITE, pale green altered white and black quartz diorite	-5	U.4	2	6	125	3	3. ا م م	1.3	0.030	10.90
64776	ANDSEITE, green feidspar crystal lithic tuff	) _5_	0.3		6	44	2	4.4	1,8	-0.01	10.96

Au analyses in PPB; other metals and Trace Elements in PPM and Major Oxides in %

### Homestake Corona 1992 Whole Rock Results Kenrich Corey Claims

1CC #	CaO	Fe2O3	K20	LOI	MgO	MnO	Na2O	P2O5	SiO2	TiO2	Total	BaO	Cr2O3	Nb	Y	Zr
KR92-003	9.64	13.08	2.55	3.66	5.28	0.20	2.85	0.17	46.62	2.02	99,98	0.08	0.01	7	44	114
KR92-004	9.07	14.11	1.66	2.69	5.91	0.23	2,66	0,16	45.88	1.86	99.80	0.03	0.01	6	42	105
E-27b	5.4	8,95	2.21	2.51	2.12	0.17	3,03	0.44	55.96	1.18	97.47	0.189	0.01	-5	37	121
E-28	0.63	7.62	4.08	3.42	2.04	0.09	1,66	0,09	61.03	0.73	98.75	0.157	-0.01	10	30	141
E-30	0,15	3,13	0.68	1.12	0.43	0,03	5,91	0.1	76.75	0,38	100.91	0.044	0.02	17	61	421
E-32	3,62	9.21	3.02	4.03	1.88	0.21	2.72	0.66	58.32	1.05	98,76	0.215	-0.01	9	46	140
(E-33	0,05	7.13	2.59	3.84	0.44	0.01	3.4	0,12	67.93	0,8	99,93	0.269	-0.01	16	26	246
E-34	0,23	5.44	3.59	7.37	1,68	0.02	0.77	0.15	64.62	0,94	99.69	0.301	-0.01	13	31	232
E−35	-0,01	5.6	4.84	3.03	0.19	-0.01	3.77	0.21	68.17	0.83	100.67	0.403	0.01	18	31	254
E~36	13,76	10	-0.05	4.4	9.15	0,15	0.11	0.05	47,15	0.88	100.09	0.003	0.05	16	20	59
E-37	8,25	10.1	0.29	4.51	6.41	0.16	3,43	0.09	45.59	1.45	99.3	0.019	0.04	-5	31	99
E~38	10.39	10.5	0.36	2.77	7.26	0.19	2,54	0,14	46,55	1.38	97.92	0.019	0.03	5	30	92
E-39	4.73	9.08	0.21	5.62	4.91	0,06	0.22	0,08	65.56	0.54	101.1	0.012	0.01	-5	10	106
E-41	13	11.41	0.05	3.04	5.45	0.2	2.85	0.17	48.89	1.67	101,46	0.011	0.03	9	39	98
E-42	10.36	10.61	0.43	3.08	5.39	0.14	1.5	0.14	52.54	1.42	100.35	0.023	0.02	8	34	121
E-43	6.83	12.62	0.4	4.3	6.66	0,18	3,78	0.24	45.12	1.7	97.98	0.018	0.03	8	39	126
E-45	3.84	4.86	3.98	5.93	3.64	0.02	1.44	0,18	<b>59.9</b> 5	0.72	100.25	0.165	-0.01	11	40	200
E-47	1.1	7,05	2.4	3.03	1.14	0.14	2.4	0.17	67.16	0.77	99.53	0.084	-0.01	14	49	229
E-48	1.21	3.2	4.89	2.94	0.09	0.07	2.49	0.1	72.71	0.32	101.33	0.258	0.02	24	84	506
(E-49	0.37	3.77	3.83	0.83	0.18	0,06	3.8	0.05	72.33	0.31	99.27	0.224	-0.01	29	106	489
E-50	0.22	1.75	3.45	0.64	0.13	0.03	4.23	0.03	77.59	0.3	101.28	0.269	0.03	20	54	508
E-51	0.89	5.8	3.02	2.29	1.18	0.1	3.37	0.11	66.36	0,54	98.65	0.149	-0.01	11	26	83
E-54	1.09	5.71	3.37	1.93	1.33	0.08	3,93	0.12	68.92	0.43	100.67	0.154	0.02	24	19	329
E-56	6.71	9.99	0.13	5.96	10.23	0.17	2.24	0.11	48.04	1.13	100.57	0.044	0.04	5	57	84
E-58	8.66	3.2	0.17	3.63	1.81	0.03	1,35	0.27	67.65	0,38	99,1	0.016	0.02	10	42	142
E-59	9,17	10.02	0.14	3.51	6.24	0.16	3.04	0.07	46.54	1.13	99.66	0.028	0.03	7	30	71
E92-341	4.74	9,99	3.39	-0.05	2.85	0.17	3.99	0.43	55.71	1.29	98.62	0.181	0.03	12	35	113
E92-358a	1.82	4,51	4.15	-0.05	0.45	0,28	5,83	0.65	66.75	1.14	101.07	0.127	0.03	15	41	217
E92-359	0.21	7,02	6.18	-0.05	0,38	0,01	2,96	0.22	65.45	1.06	98.49	0.345	0.03	19	25	268
E92-403	1,16	5.16	1.88	3.75	0.53	-0.01	5.58	0.45	64.3	1.1	100.2	0.325	-0.01	19	45	261
E92-407	2.21	6,87	3.76	2.6	1.08	0,27	4.29	0.48	62.11	1.12	100.02	0.246	0.01	10	59	232
E92-409b	1,03	9	5.4	2.52	0.79	0.28	3.6	0,51	59.18	1.18	99.12	0,183	-0.01	18	53	195
E92-409a	0.73	13,89	2.1	3.61	2.74	0.09	3,46	0.54	53.21	1.47	99,5	0.134	-0.01	5	45	190
E92-428	0.06	0,51	4.38	0.33	0.03	-0.01	4.73	0,13	74.13	0.22	98.53	0.23	0.02	19	43	306
E92-427	0.07	0.4	4.88	0.48	0.05	~0.01	3.85	0.1	76.84	0.24	99,97	0.265	0.01	13	49	286
E92-425	1.28	7.78	4.33	1.61	1.12	0.17	3,51	0.38	62.72	1	98.82	0.253	-0.01	15	55	216
E92-424a	1.02	6.91	4.11	1.61	0,87	0.07	3,56	0.43	65.1	1.08	99,95	0.269	-0.01	9	52	250
E92-424b	2.56	7.13	2.61	3.42	2.01	0.13	3.47	0,37	61.86	0.93	98.12	0.313	-0.01	24	49	232
63774	0.3	3,73	3.98	1.79	0,58	0.1	4.45	0,14	/1.51	0,3	100.19	0,156	0.02	19	10	115
63775	4.08	5,66	1.01	1.13	2.83	0.11	4.86	0.26	62.63	0.58	99.8	0.14	-0.01	23	<i>'6</i>	392
63776	0.71	12.8	0.47	3.8	4.36	0.11	4,94	0,27	51.59	1.76	98.41	0.033	-0.01	17	78	206
63777	2.12	4.7	3.59	2.99	0.51	0.02	5.62	0.37	62.14	1.03	99.02	0.302	0.01	21	51	190
63778	11	11,58	0.34	3.15	7.09	0.18	2.27	0,13	45.22	1.4	98.62	0.015	0.04	-5	36	90
64752	0.74	4.07	1.36	2.61	3.83	0.03	3.39	0.05	69.47	0.57	99,78	0.158	-0.01	9	49	287
64753	5.71	5.87	0.25	5	3.29	0.12	7.48	0,58	52.99	0.62	99.15	0.059	-0.01	7	51	117
64758	0.87	2.41	0.38	1.28	0.11	0.02	7,26	0.07	73.2	0.06	99.34	0.02	0.01	49	20	975
64765	3.83	8,69	2.14	3.47	4	0.09	3.47	0.71	54.47	2.09	99.67	0,115	-0.01	14	51	177
64771	7.05	11.88	0.63	1.01	5.41	0.21	4.53	0.18	50.88	1.85	98.05	0.013	-0.01	9	46	152
64772	5,58	8.35	2.37	4.9	2.81	0.11	2.01	0.49	56.98	1.06	97.83	0.181	-0.01	11	34	135
64773	1.36	6.07	4.6	1.78	1.59	0.09	3.52	0.39	62.82	1.06	99.47	0.243	-0.01	23	46	225
64776	9.87	9,68	1.72	2.83	7,88	0.19	2.03	0.05	46.31	0.83	97.45	0.081	0.03	10	56	299

	CaO	Fe2O3	K20	LOI	MgO	MnO	Na2O	P2O5	SiO2	TiO2	Total	BaO	Cr2O3	Nb	Y	Zr
64777	8.44	13.8	0.62	2.08	6.86	0.21	2.78	0.18	45.71	1.99	98.81	0.016	0.01	6	49	146
64778	1.82	7.18	1.57	3.4	3.7B	0.06	1.97	0.27	65.79	0.87	99,55	0.07	-0.01	-5	38	91
64779	5.35	10,55	0.34	5.98	4.87	0.17	5.51	0,39	45.83	1.62	97.32	0.013	-0.01	12	37	148
64780	8.22	11.3	0.52	3.57	5.98	0.17	3.13	0.18	47.47	1.73	97.52	0.071	0.03	7	43	113
64781	6.04	12.35	0.48	5.26	6.98	0.24	2.79	0.13	46	1.62	100.79	0.017	0.03	9	40	96
64782	5.41	10.63	0.57	5.11	6.13	0.24	4.62	0.33	46,92	1.53	97.74	0.045	-0.01	16	38	142
64783	10.59	10.96	0.34	4.71	7.48	0.2	4.1	0.18	45.11	2.05	100.2	0.023	0.04	-5	38	98
64784	15.75	9,98	0.38	4.05	6.82	0.17	1.82	0.16	44.43	1.44	100.57	0.02	0.04	7	31	81
64785	10.5	13.57	0.6	3.15	6.11	0.21	2.25	0.2	46.53	2.07	100.9	0.033	0.02	-5	43	124
64786	11.11	9.47	1.05	3.31	5.59	0.18	2.61	0,12	43.68	1.26	97,43	0.126	0.04	7	32	65
64787	7.05	11.21	0,5	3.32	5.74	0.16	4.22	0.23	50.76	1.73	100.59	0.038	0.01	9	46	105
64788	9.47	12.35	1.63	4.89	6.31	0.24	3.02	0.21	44.13	1.81	98,73	0.31	-0.01	9	43	110
64789	0.86	4.15	9.03	1.85	0.51	0.08	0.31	0.6	66.81	1.18	100.54	0.727	-0.01	9	35	111
64790	8.29	8.29	0.38	3.27	4.03	0.13	2.99	0.2	55.04	1.58	98.61	0.017	0.04	6	39	104
64791	5.33	11.94	1.24	3.72	6.47	0.21	4.11	0,12	47.11	1.48	97.54	0.051	0.01	15	39	83
72684	1.59	1.3	3.91	1.28	0.14	0.09	2.29	0.07	80.44	0.17	100.35	0.191	0.07	-5	49	246
72685	0.87	2.38	4	1.26	0.23	0.16	2.51	0.04	78.35	0.23	100,13	0.299	0.06	13	72	316
72686	1.31	5.23	4.71	2.45	0.76	0.15	4.14	0.43	62.95	1.16	99.71	0.276	-0.01	20	48	256
72687	0.12	4.44	3.68	1.28	0.56	0.11	3.82	0.08	69.28	0.44	98.05	0.167	-0.01	21	70	396
72690	0.88	5	2.29	4.86	1.73	0.04	3.01	0.21	64.15	0.83	98. <del>9</del> 4	0.163	-0.01	7	33	141
73677	3.79	6.67	0.39	0.75	3.46	0.07	4.37	0.21	64.98	0.88	99,81	0.017	0.02	8	28	147
73686	1.02	7.14	4.33	2.56	2.37	0.16	2.81	0.34	61.1	1	98,88	0.224	-0.01	18	54	211
73687	1.54	4,91	5.85	2.05	0.83	0.05	2.62	0.1	60.92	0.73	99.32	0.363	-0.01	13	30	185
73688	0.79	8.2	3	3.59	1.85	0.09	2.3	0.05	60,77	0.73	99.72	0.149	-0.01	10	25	171
73689	2.84	5.99	3.5	4.74	1,51	0.15	1.96	0.17	58.16	0.84	99.28	0.192	-0.01	11	15	164
73690	2.9	8.39	3.54	3.89	2.09	0.19	3.03	0.49	57.63	1.15	98,71	0.182	-0.01	15	32	169
73691	2.72	8.83	3.16	4.1	2.83	0.26	2.4	0,55	57.71	1.18	98,79	0.195	-0.01	16	46	200
73692	4.25	12.34	2.04	5.56	3.54	0.31	2.13	0,54	52,5	1.17	98,63	0.109	-0.01	16	47	164
73693	4.85	8.33	1.29	3.68	6.47	0.09	4.02	0,13	50,84	0.98	98.81	0.081	0.03	11	39	112
73694	0.78	3.72	3.32	1.76	0.95	0.04	3.07	0,17	73.25	0.39	99,36	0.125	-0.01	~5	39	153
73695	1.94	4.5	4.6	2.16	0.88	0.08	2.65	0.47	66.41	0.97	98.8	0.298	-0.01	16	39	127
80362	0.13	1.53	5.67	1.4	0.07	-0.01	3.56	0,08	72.46	0.23	99.01	0.264	0.02	12	32	276
80363	1.26	3.88	4.9	2.25	0.53	0.04	3.37	0.21	68.96	0.74	99.23	0.266	0.02	21	65	279
80364	1.29	4.23	4.95	1.27	0.69	0.05	3.44	0.23	70.61	0.77	101.13	0.25	0.02	17	51	241
80369	0.51	1.99	2,39	2.18	0.6	0.02	2.52	0.08	78.14	0.42	99.59	0.203	0.02	~5	33	100
80370	12.03	8	0.26	5.03	5.68	0.1	1.72	-0.03	49.09	0.62	<del>99</del> .48	0.007	0.05	5	19	128
80371	3.09	6.92	4.08	4.55	2.69	0.12	2.9	0.49	57.16	1.17	99,04	0.431	-0.01	22	79	494
80373	4.59	5.75	-0.05	4.77	2.51	0.06	7.78	0.1	58,9	0.51	99,85	0.004	-0.01	12	19	308
80379	4.6	5.82	-0.05	2.22	2.54	0.06	7.75	0.12	60.66	0.51	99,82	0.004	~0.01	7	50	183
80380	1.08	1.75	4.25	3.23	0.19	0.04	3.7	0,39	72.47	0.19	100.46	0.064	-0.01	9	43	126
80381	0.26	10.96	6.63	1.34	3	0.07	0.15	0.27	62.29	0.89	99.49	0.223	-0.01	12	11	172
80382	8.34	14.21	0.73	3,38	6.1	0,23	2.33	0,38	46,53	2.3	98,69	0.108	0.03	34	25	388

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KR92003 KR92004 Kr Kr Cumberland core; BH3@294'; mafic flow Cumberland core; BH3@202' mafic flow

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### Homestake Corona 1992 Stream Sediment Results Kenrich Corey Claims

	Description	Au	Ag	Cu	Pb	Zn	Mo	As	Sb	Ha
72623	sit	5	2.2	51	21	571		69	10	0.183
72624	moss mat	-5	2.4	48	11	395	5	59	9	0.13
72626	silt	-5	0.6	35	19	283		54	6.1	0.254
72627	moss mat	12	0.7	33	9	213	5	36	6	0.224
72628	süt	12	0.5	41	17	311		110	14	0.196
72629	moss mat	-5	0.7	42	8	245	4	96	11	0.182
72631	moss mat	5	0.2	41	8	111	3	87	~5	0.115

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#### International Corona Unuk Silt Program

NO.         ppb         ppb         ppb         ppb         ppb         ppm         ppm <th>SAMPLE</th> <th>Au</th> <th>. Au</th> <th>Au</th> <th>Ag</th> <th>Ag</th> <th>Ag</th> <th>Cu</th> <th>Cu</th> <th>Cul</th> <th>Pb</th> <th>Pb</th> <th>РЫ</th> <th>Zn</th> <th>Zn</th> <th>Zn</th> <th>As</th> <th>As</th> <th>As</th> <th>Sb</th> <th>/ Sb</th> <th>Sh</th> <th>Ha</th> <th>Ha</th> <th>Ha</th>	SAMPLE	Au	. Au	Au	Ag	Ag	Ag	Cu	Cu	Cul	Pb	Pb	РЫ	Zn	Zn	Zn	As	As	As	Sb	/ Sb	Sh	Ha	Ha	Ha
Sitt         Moss         Conc         Sitt         Moss <th< td=""><td>NO,</td><td>քքե</td><td>ppb</td><td>ppb</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>PPm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>maa</td><td>nom</td><td>%</td><td>~ ~</td><td>%</td></th<>	NO,	քքե	ppb	ppb	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	PPm	ppm	ppm	ppm	maa	nom	%	~ ~	%
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		Silt	Moss	Conc	Silt	Moss	Conc	Silt	Moss	Conc	Sät	Moss	Conc	Silt	Moss	Conc	Silt	Moss	Conc	Silt	Moss	Conc	Silt	Moss	Conc
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	261	56		38	0.3	-1	0.1	105	-1	105	13	~1	12	85	-1	79	8.5	-1	8.6	0.8	-1	1	0.005	-1	0.005
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	262	18	-1	25	0.3	<u>-1</u>	0.2	105	-1	97	11	-1	13	108	-1	112	12	-1	15	1.4	-1	1.1	0.005	-1	0.022
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	263	23	15	82	0.3	0.2	0.2	115	105	99	14	5	12	111	98	92	9.3	10	11	1	2	0,1	0.014	0.011	0.005
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	264	51	33	20	0.2	-1	-1	40	30	34	13	8	11	64	42	66	3.2	2	4.1	0.9	2	0.9	0.033	0.029	0.005
<b>249. 2 8 6 0.3 0.3 -1 3.4 35 2.5 15 9 11 138 176 141 44 59 3.3 9.1 9 5.1 0.122 0.123 0.191 171 15 16 15 16 0 17 15 16 0 2 1.1 0.005 0.013 0.016 177 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 10 0.1 17 175 175 10 1.1 100 176 177 175 10 0.1 177 175 10 0.1 177 175 177 111 10023 -1 10027 177 117</b>	265	-1	36	-1	-1	1	-1	-1	49	1	-1	77	-1	-1	65	-1	1	2	-1	-1	2	-1	-1	0.018	-1
<b>271 2 8 6 0.3 0.3 -1 34 35 25 15 9 11 138 176 149 44 59 33 3.4 9 5.1 0.122 0.123 0.109 17 13 0.0 2 1.1 0.062 0.013 0.016 0.017 0.017 0.016 0.017 0.017 0.016 0.017 0.017 0</b>																									
$\begin{array}{cccccccccccccccccccccccccccccccccccc$				/			**				-	•	· <del>-</del> -						· • • •	••••	-		*	•	•• •• • • •
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	. 417	2	۲.	- <b>P</b>	0,3	0,3	-1.	34	<u>35</u>	25	15	9	н.	198	176	149	44	59	33	8.1	9	5.	0.122	0.123	0.101
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$																	-				•				
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	271	15	16	13	0.4	0.3	-1	113	101	114	10	6	8	101		106	10	17	 13 <b>i</b>	0.9	2	ंचित	0.005	0.013	0.016
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	272	10	46	12	0.6	0.5	-1	212	184	73	20	12	12	97	75	58	11	5	7.3	-0.4	2	0.0	0.036	0.041	0.015
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	273	10	·1	8	0,3	-1	-1	108	-1	91	14	~1	9	- 92	-1	85	10	-1	9.4	0.7	-1-	11	0.023		0.021
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	274	6	2	28	0.4	0.5	-1	45	47	42	12	7	9	477	497	286	14	2	12	3.1	2	3	0.27	0.328	0.216
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	275	7	15	10	-1	0.3	-1	103	78	62	7	3	7	95	72	84	3,2	2	5.8	0.8	2	0.9	0.018	0.03	0.021
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	276	10	15	518	-1	0.2	1.7	67	67	59	3	1	4	46	42	56	2,6	2	4	0.1	2	0.1	0.015	0.024	0.018
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	277	2	39			0.2	-1	27	19	-1	1	5	-1	39	40	-1	2	2	-1	0,1	2	-1	0,005	0.005	-1
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	278	<u> </u>	7		0.1	0.2		8	11	1	7	4	-1	51	40	-1	4,4	2	-1	0.1	2	-1	0.021	0.015	-1
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	2/9	<u></u>	58		7 		<u>_</u> -1	141	138	106		1	4	55	36	47	1.4	2	-1	0.1	2	01	0.038	0.03	0.016
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	300		16	10	0.3	0.5	0.2		42	38	14	12	14	183	219	186	113	106	95	_14	11	13	0.11	0.193	0.13
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	301		<u> </u>	- <u>-</u> 8	0,4		0.2		-1	41	14		14	176	-1	167	86	-1	91	11		12	0.128		0.154
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	302		<u> </u>		0.3	0.3	<u>1 </u> _	33	35	-1	16	9	1	182	166	1	66	66	1	2.7	2	-1	0.151	0.166	-1
$\begin{array}{c c c c c c c c c c c c c c c c c c c $		10	2		0.6	0.5	0.3	30		- 28	24	16	19	271	175	231	20	13	28	2.7	2	3	0.171	0.12	0.138
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	305	2	10	100	0.5	0.4		40	51	28	18	12	12	310	275	196	226	218	84	5,4	2	5	0.162	0.166	0.088
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	306	2			0.2	0.3		4/	30	3/	13	8	12	18/	156	174	18	14	15	2.4	2	2.5	0,149	0.14	0.121
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	307		2		~1	0.5		29	28		14			151	147	- 1	21	18	-1	2.6	2	-1	0,186	0.186	1
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	308	2			31		0.8	102	48	- 20	10	¥		761	94	103	13	15	16	1.5	2	2.8	0.058	0.069	0.063
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	309	15	18		0.3	03		44	57	37	10				26	69	- 48	- 19	41	4.5	- 10	5,8	0.357	0.148	0.077
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	310	42	133	-1	0,8	0.9	-1	91	89		23	13		161	127		81	126					0.040	0.057	0.021
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	311	18	-1	-1	4.7	-1	-11	69	-1	-1	24	-1		227			63	-1		4 2			0.007	0.102	
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	312	36	43	324	0.2	0.3	-1	49	38	31	11	7	10	- 90	65	71		16	83	0.1			0.034		0.026
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	313	7	173	16	0.2	0.3	0.2	76	79	72	13	11	13	120	106	122	19	33	20	14		—ř:	0.012	0.022	0.020
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	314	2	-1	2	0.1	-1	-1	1	~1	7	1	-1	6	31	-1	41	1.2	-1	1.4	0.1		- 01	0.005		0.005
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	315	26	52	51	0,5	0.4	0.2	79	98	70	18	16	14	165	184	154	112	80	74	3.3	2	2.2	0.054	0.081	0.049
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	316	27	37		0,3	0.2	-11-	101	108	-1	15	12	-1	190	144	- 1	47	64	-11	2.6	2	-11	0.038	0.067	-11
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	317		12	14	0.2	0.1		40	48	33	10	4	8	64	58	51	4.1	8	2.3	0.1	2	0.1	0.014	0.024	0.014
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	318			- 2		-1	!			18	7	4	6	48	36	67	2.5	9	4.9	0.1	2	0.1	0.011	0.019	0.011
	320		-1	2		~	-11-	-1	2	1	3	2	4	27	36	32	-1	2	1	0.1	2	0.1	0.005	0.01	0.005
	- 020			٤		-1	<u></u> 1	-1	-1	-1	7	1	6	41	-1	45	1.3	-1	2	0.1	1	0.1	0.005	-1	0.005

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### International Corona Unuk Silt Program

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SAMPLE	Au	Au	Au	Ag	Ag	Ag	Cu	Cu	Cu	Pb	Pb	Pb	Zn	Zn	Zn	As	As	As	Sb	Sb	Sb	Ho	Ho	
NO.	ppb	ррь	ppb	Ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	%
	Silt	Moss	Conc	Silt	Moss	Conc	Silt	Moss	Conc	Silt	Moss	_ Conc	Silt	Moss	Conc	Silt	Moss	Conc	Silt	Moss	Conc	Silt	Moss	Conc
143	15	-1	12	1.3	-1	1.3	195	-1	166	55	-1	57	331	<u>-1</u>	307	51	-1	48	12	1	11	0.041	-1	0.051
144	10	31	30	0.8	1.8	1	103	118	91	27	41	39	591	411	560	29	27	35	5.7	7	5.8	0.027	0.042	0.022
								·		· · ·		`			-			,						
				·									···· = `											
147	42	204	11	!_	<u>1,1</u>	$-\frac{1.1}{2}$	. 101	<u> 95</u>	102	49	44	46	691	326	633	30	42	41	5.7	2	5.4	0,031	0.031	0.02
148	27	!	94			- 0,4			118	21		21	138		87			11	1	1	1.9	0.013	1	0.023
149	63	-1	1(1	<u> </u>			312					- 25	15/	-1	87	4.6	-1	6.2	0.6	1	0.1	0.005	1	0.005
150	61	129	1	1	8.0	<u></u>	282	326		26	26		331	290		10	8	!	1.8	2	<u>'</u>	0.005	0.02	-1
151	23	-1	5]	0.3				-1	<u>•/</u>		-1		450	405		12	-1		2		<u>1.0</u>	0.005		0.01
152	69	19	1	0.4	0.4		147	40	-1	10	10	-1	400	405	100	10	10	- 1	3.3	2		0.014	0,02	- 1
153	58	-1	1477	0.4	-1	0.4	474	-1	144	10		20	110		100	14	-1		2.6	~1	1.4	0.024		0.022
154	92		380	0.0			100		105	12			90		104	43			3.0		4.1	0.013		0.005
155				0.5		- 0.7			100	16			120		102				5.0	- 1		0.042		
150	42	<u> </u>		0.0			115		104	10			120			40		- 62	3.9			0.154		0 150
159	- 45	138	75	0.0		0.4	126	131	113	22	20	26	205	209	186	36	22	33	9.3	8	0.4	0.154	0.082	0.139
150	15			0.0	-1	1 3	182	1	137	26	-1		186	-1	139	32	-1	18	8.9	-1	5.6	0.05	-1	0.032
160	21	19	9	0.7	07	- 07	123	115	102	19	18	25	211	173	194	27	32	27	12	11	12	0.055	0.073	0.053
161	50	18	73	0.9	0.3	1.4	131	132	174	36	15	49	212	141	220	144	30	271	4.9	5	71	0 334	0 135	0 433
162	90	143	-1	1	1	-1	235	160	-1	42	23	-1	544	542	-1	85	58	-11	10	7	-1	0.349	0.304	-1
163	12	-1	348	0.2	-1	0.2	72	-1	64	10	-1	23	88	-1	87	10	-1	24	2.1	-1	1.9	0.038	-1	0.06
179	-1	19	-1	-1	0.2	-1	-1	51	-1	-1	9		-1	83		1	16	-11	-1	2	-11	-1	0.057	-1
180	30	-1	-1	0.4	-1	-1	150	-1	-1	29	-1	-1	145	-1	-1	19	- 1	-1	2	-1	-1	0.063	-1	-1
181	12	-1	-1	0.2	-1	-1	46	-1	-1	27	-1	-1	149	-1	-1	19	-1	-1	2.6	-1	-1	0.113	-1	-1
182	11	-1	9	0.4	<u> </u>	0.4	71	-1	64	47	-1	33	162	-1	141	25	-1	25	4.2	1	3.7	0.191	1	0.172
183	33	35	34	1.2	1.3	1.2	168	177	124	39	47	54	273	247	220	33	29	33	5.6	6	5.8	0.06	0.104	0.058
184	12	12	2	0,3	0.4	0.3	154	147	114	38	30	33	240	193	206	42	37	30	3.5	2	3	0.06	0.082	0.041
185	2	7		0.4	0.6	0.4	64	66	81	19	17	18	540	449	473	31	49	25	5.4	7	4.7	0.782	0.904	0.754
186	21	135	-1	0.4	0.6		121	162	-1	23	24		272	234	-1	32	57	-1	3.9	2	1	0.043	0.107	- 1
	<u> </u>	26	- 1000	0.0	0.5	<u>!</u>	149	150	-1	21	18	-1	211	144	-11		34	-1	3.4	2	-1[	0.08	0.062	-1
188	25		1238	0.0	0.7				82	29	26	52	199	228	165	60	51	80	<u>1</u>	2	9.4	0.165	0.194	0.205
100		183	664	1.1	<u> </u>		155	180	200	23	-1		224	- 1				75	5.7	<u>1</u>	5.6	0.161	-1	0,156
101	50	188		1.5	17		150	160	100		40		1127	1251	1	90	40		9.3		9.4	0.247	0.244	0.199
102	1300	1982	282	12	0.8		07	80	87	20	32		1137	1201	120	265	144		8.3	<u> </u>		0.427	0.351	
193	91	-1	154	1.2	-1	1 2	104	-1	81	25			100	-1	1471	200		201	3.1		3.8	0.080	0.003	- 0.079
194	76	1727	260	0.5	0.9	0.0	88	74	78	15	18	22	112	96	109	76	116	158	3.0		3.5	0.055	0.001	0.047
195	81	153	79	0.8	2.1	0.9	121	127	90	23	25	18	139	139	113	58	74	48	84		6.2	0.001	0.001	0.000
196	61	88	-1	0.6	1.5		128	104	-1	24	22		183	108	-1	62	40	-1	5.4	8	-1	0.095	0.105	t
197	15	15	-1	0.8	0,5	-1	53	47	-1	10		-1	221	158		27	33		2.7	. 2		0.094	0.128	
198	9	6	-1	50	48	50	151	117	133	248	164	174	780	481	624	160	102	170	118	75	166	0.238	.0.233	0.122
199	54	129	17	1.2	1.4	3.2	105	104	73	19	16	16	788	586	510	57	62	52	16	13	13	0.125	0,14	0,121
200	7	6	-1	0,3	-1	-1	79	105	-1	8	8	-1	107	106	-1	14	18	-1	1.2	2	-11	0.097	0.098	
201	85	106	309	0.8	0.9	1.8	162	238	127	28	27	27	251	170	193	58	60	46	7.4	6	7.9	0.198	0.272	0.135
202	9	-1	8	0.4	-1	0.3	52	-1	51	26	-1	30	123	-1	114	20	-1	19	2.4	-1	2.8	0,15	-1	0,128
203	32	39	-1	1.2	1.7	-1	153	179	1	29	29	-1	491	453	-1	35	47	-1	10	16	-11	0.144	0.245	1
204	39	36	-1	0.6	0.5	-1	140	138	-1	21	18	-1	120	121	-1	55	41	-1	4.1	2	-1	0,073	0.15	
205	8	64	101	1	1.1	1.2	75	70	68	32	25	29	194	177	151	71	71	62	12	13	11	0.193	0.249	0.155
206	60	-1	212	0.4	1	0.7	67	-1	89	14	-1	20	120	-1	122	52	-1	160	3.6	~1	3.8	0.054	1	0.08 1
207	210	-1	95	1.2	-1	1.3	109	-1	101	24	-1	27	265	-1	212	111	-1	149	8.8	~1	7.5	0,12	-1	0.11

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APPENDIX 7

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Sample Results and Silver Creek Grid Sketches - Placer Dome Exploration Limited





**Geochemical Analysis** 

Project/Venture:	1P	Geol:	K TROCIUK	Date Received:	JULY 30, 1992	Page	1	of	7
Area:	COREY	Lab Project No.:	D2469	Date Completed:	AUG 12, 1992	Attn:	K TROC	JUK	
Remarks:							S HOF	MAN	
Au - 10.0 g sample digest	ed with Agun Regin and determined by Graphite Furr	nace A.A. (D.L. 1 PPB)					J KOW	ALCHUK	
ICP - 0.5 g sample digeste	ad with 4 ml Agus Regis at 100 Deg. C for 2 hours.						E KIMU	ŘA –	

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Au - 10.0 g sample digested with 4 ml Aqua Regia and occumined by Glaphite Furnice A.A. (D.L. 1995) ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are sarely dissolved completely with this acid dissolution method.

SAMPLE	1	g	Mo	Cu	© Pb	Zn	As	Sb	Cd	Ni	Co	Mn	Bi	Cr V	Ba	W	Be	ta	Sr	Π	Al	<u>Ca</u>	Fe	Mg	ĸ	Na	P
No.	P	m	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm ppm	ррт	ppm	ppm	ppm	ppm	%	%	<u>    %     </u>	%	*	<u>%</u>	_%	<u>%</u>
AE-88-1	0	1	2	17		35	7	<5	<0.1	12	7	200	2	103 52	125	<5	0.3	16	41	0.11	0.72	0.47	2.25	0.49	0, 19	0.06	0.11
AE-88-2	<	0.1	1	- 14	a	38	5	<5	<0.1	11	7	223	2	135 50	131	<5	0.3	18	47	0.13	0.73	0.55	2.53	0.49	0.22	0.07	0.12
AE-88-3	0	1	- 4	10		37		<5	<0, 1	12	6	243	2	149 6	134	⊲5	0.3	19	52	0.15	0.79	0.64	2.90	0.52	0.23	0.08	0, 14
AE-68-4	0	1	2	14		42	- 5	<5	<0. 1	13	8	271	~2	180 6	155	<5	0.4	21	51	0.16	0.84	0.58	2.77	0.55	0.27	0.08	0.13
AE685	<	0.1	<1	11		40	ব	- 5	<0.1	12	7	276	<2	120 67	137	<5	0.4	20	34	0, 13	0.86	0.48	3.02	0.51	0.24	0.05	0.13
		- 1									1					]		1									1
AE-68-6		0.1	2	<b>t</b> 2	7	43	ব	-65	<0.1	11	7	382	2	111	150	< 5	0.5	18	35	0.13	1.02	0.42	2.75	0.55	0.24	0.04	0.12
AE88-7	0	.1	2	9	5	35	<5	<5	<0.1	10	6	248	2	120 4.	135	<5	0.3	15	32	0.11	0.74	0.37	2.13	0.48	0.23	0.05	0.09
AE-88-8	0	1	<1	10		42	්	ব	<0.1	11	7	347	2	132 52	152	<5	0.4	16	33	0.13	0.96	0.45	2.61	0.59	0.27	0.05	0, 12
AE-68-9	0		<1	11	2	36	්	<5	<0.1	10	5	207	2	104	125	<5	0.2	13	- 43	0.12	0.78	0.50	2.06	0.53	0.22	0.06	0.11
STD-P1	0	3	66	26	52	150	19	4	0.2	34	5	584	2	125 3	180	<5	0.4	8	- 87	0.11	1.11	0.93	2.34	0.87	0.38	0.07	0.09
	1															í											
AF-88-13	0	2	6	27		177	29	8	0.2	35	11	798	2	91 60	95	<5	0.6	10	22	0.07	1.78	0.42	4.12	1.08	0.12	0.04	0.06
AE-88-14	0	2	5	27	<u></u>	188	24	5	0.4	37	12	871	<2	85 63	100	5	0.6	11	25	0.08	1.88	0.45	4.41	1.16	0.12	0.05	0.09
AF-88-15	o	1	5	27	12	180	25	<5	0.3	37	12	759	2	78 64	98	<5	0.7	12	25	0.08	1.81	0.44	4.27	1.15	0.11	0.05	0.08
AE-88-16	0	2	3	26	13	184	22	7	0.4	37	12	624	~	77 64	103	<5	0.7	12	28	0.07	1.81	0.43	4.27	1.15	0.11	0.04	0.09
AE-88-17	- l õ	7		29	12	196	26	8	0.4	35	13	814	2	75 60	91	<5	0.7	12	28	0.07	1.71	0.42	3.95	1.01	0.10	0.05	0.07
AL-00-17	1	'' [						-																		1	
AE_88-18		0.1	7	32	- 11	175	26	<5	0.2	37	12	8 12	2	72 6	92	<5	0.6	11	22	0.06	1.89	0.37	4.48	1.15	0, 10	0.03	0.08
AF_88-23		<b>*</b> ]		23		97	4	-5	<0.1		9	773	2	55 48	123	<5	0.6	13	27	0.08	1.71	0.42	4.77	1.12	0.13	0.03	0, 12
AE_88_28	0		5	28		137	5	- 6	<0.1	42	10	933	2	80 53	120	<5	0.6	11	22	0.04	1.71	0.38	4.48	1.07	0.12	0.03	0,12
AE-88-28	1 õ		<1	24		136	-5	- 65	<0.1	43	11	1001		60 54	88	- 5	0.6	10	17	0.05	1.83	0.34	4.73	1.12	0, 10	0.02	0.11
AE_88_28*				22		138	ත්	đ	<0.1	43	11	991	2	59 53	86	_ ব্য	0.6	9	16	0.04	1.60	0.33	4.69	1.10	0.09	0.02	0.11
~c-00e0	ľ	·•	- 1					~					-														
AF-88-29	0	2	<1	31		139	6	<5	0.1	44	11	1016	~2	72 51	108	<5	0.8	13	22	0.04	1.79	0.37	4.63	1.11	0, 12	0.03	0.12
AE-88-30	0	2	<1	29		164	12	< 5	0.4	42	11	\$139	2	54 54	95	5	0.7	11	21	0.03	1.64	0.37	4.71	1.04	0.09	0.02	0.12
AE_88_31	- i	<b>7</b>	<1	27	11	142	<5	<5	<0.1		11	1025	2	73 54	117	্ ব	0.7	11	20	0.04	1.73	0.33	4.57	1.06	0.12	0.03	0.11
AF-88-32	lõ	2	<1	26	<b>∞</b> ,	153	7	<5	0.1	43	11	1131	2	52 54	110	<5	0.7	10	19	0.03	1.66	0.33	4.65	1.05	0.09	0.02	0.12
AF-88-33	l õ	31		29		167	8	6	0.2		11	1144	2	75 54	138	<5	0.7	12	22	0.04	1.75	0.35	4.70	1.05	0.14	0.03	0.12
	· · ·	1	- 1				-								1												
AF-88-34	0	2	- 4	28		262	6	ব	0.3	45	10	1171	2	65 5	130	্ৰ 🕹	0.7	11	21	0.04	1.76	0.35	4.76	1.07	0.13	0.03	0.12
AE-88-35	0	3	<1	32		203	10	ব	0.5	49	11	1451	2	73 57	149	ব	0.7	12	23	0.04	1.87	0.36	5.39	1.11	0.14	0.03	0.13 (
AE-88-40		5		41		199	11	-65	0.6	29	12	1116	~2	57 57	142	<5	0.7	14	38	0.08	1.83	0.43	5.35	1.12	0.15	0.04	0.13
AE-88-41	Ō	2		33		188	7	<5	0.4	2.024	10	895	2	53 54	115	5	0.6	13	30	0.07	1.77	0.44	5.24	1.11	0.13	0.03	0.14
AE_88_41*	ō	2	- <1	33		185	8	<5	0.3	23	10	887	2	52 53	116	<5	0.6	12	30	0.08	1.75	0.45	5.22	1.09	0, 13	0.03	0.14
		·-	- ''	Ψu																							
AF-88-42	n	1	6	36		166	6	- 6	0.4	22	10	829	2	55 50	110	<5	0.6	13	31	0.06	1.61	0.39	4.66	1.01	0.13	0.04	0.12
AF_88-71			11	138		81	6	6	<b>d</b> 0.1	37	17	535	2	82 10	110	9	0.5	8	40	0, 19	2, 18	0.64	5.22	1.45	0.43	0.13	0.11
			21	107		427	23	- 6	3.4	65	16	744	2	1 10 68	314	<5	0.5	10	34	0.03	1.21	0.39	4.21	0.96	0.15	0.02	0.13
AH_88_2		1	22	118		510	25	- 6	4.3	74	18	851	2	82 70	213	<5	0.5	10	33	0.03	1.19	0.38	4.31	0.94	0, 15	0.02	0.13
AU_88_3			23	110	47	463	20	4	3.6	66	16	738	ā	73 6	231	<5	0.4	9	33	0.04	1. 16	0.40	4.31	0.98	0.12	0.01	0.13
00-00-0	'	~ I											-														
AN_88_4	- I •	a	17	118	90	472	26	6	3.8	73	16	808	2	82 6	335	্ৰ	0.4	10	32	0.03	1.17	0.35	4.31	0.94	0.14	0.01	0.13
AU_46_5		11		113		462	21	- 6	3.5	6	15	743	ā	97 7	227	6	0.4	9	35	0.03	1.23	0.45	4.35	1.00	0.15	0.01	0.13
		11	23	130		561	27	- A	4.3	82	10	875	ā	89 70	275	6	0.5	10	36	0.04	1.30	0.42	4.80	1.04	0, 15	0.02	0.14
AU 49 7		1	20	111		452	21	- 25	3.4	65	1	717	0	91 70	250	6	0.5	9	34	0.04	1.21	0.42	4.29	1.00	0.14	0.02	0.13
			40	111	4.5	مدر	-		33		15	703	2	90 B	251	പ	0.4		<u>.</u>	0.04	1, 19	0.41	4.23	0.98	0.14	0.01	0, 13
Art-00-/-		•	TAL I	~~~	<b>100</b>	+++0	1 14		0.0				~		1	~											
1 L					0.00003333					0000000000000			1		.1	L			n dia amin'ny d								استجمعت ا

Geochemical Analysis

Project/Venture: Area:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2469	Date Received: Date Completed:	JULY 30, 1992 AUG 12, 1992	Page Attn:	2 K TRO	of CIUK	7
Remarks:							S HOF	FMAN	
Au - 10.0 g sample d	gested with Aqua Regin and dete	mined by Gaphile Furnace A.A. (D.L. 1 PPB)					J KOW	ALCHUK	
ICP - 0.5 n sample di	cented with 4 ml Agus Regis at 1	00 Deg. C for 2 hours.					E KIML	JR <b>A</b>	

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ICP -0.5 g mample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are marely dissolved completely with this acid dissolution method.

SAMPLE	Ag	Mo	Çu	Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	N.	Ba	Ŵ	Be	ها	Si	TI	AI I	On	Fe	Mg	K	Na	P
No.	ppm	ppm	ppm	pom	ppm	.ppm	ppm	ppm	ррпт	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	<b>%</b>	- %	- %	76	*	- 26	
AH-68-8	1.4	27	132	20	533	26	<5	4.2	76	20	934	2	84	73	236	17	0.5	10	35	0.03	1.24	0.40	4.76	0.98	0.13	0.01	0.14
AH-88-10	1.3	27	132	21	505	24	5	4.0	π	18	921	2	116		266	5	0.5	8	39	0.03	1.40	0.46	5, 15		0.10	0.02	0.15
AH-88-11	1.2	25	119	17	459	21	<5	3.6	72	17	863	2	81	66	201	<5	0.4	7	- 33	0.02	1.21	0.40	4.63	100	0, 12	0.01	0.13
AH~68-12	1.1	22	124	25	645	24	<5	6.8	82	24	1467	~	69	- 39	221	- 5	0.4	9	54	<0.01	0.74	0.26	3.61	0.45	0,11	0.01	0.10
AH-68-13	1.3	30	128	20	514	28	4	4.3	78	19	936	~2	75	73	194	ব	0.6	9	36	0.02	1.20	0.41	4.81	0.95	0, t2	0.01	0.16
AH-88-14	0.9	17	178	25	727	28	ব	9.8	122	42	3592	2	98	30	248	<5	0.4	10	29	0.01	0.70	0.20	3.41	0.36	0.08	0.01	0.07
AH-68-15	0.7	3	73	15	127	24	6	<0.1	27	15	757	3	44	61	104	<5	0.3	6	22	0.01	1.67	0.43	5.24	1.38	0.07	<0.01	0.13
AH-88-16	0.6	2	74	15	170	25	6	<0.1	28	14	769	2	63		140	<5	0.3	- 4	25	0.02	1.80	0.49	5.34		0, 13	0.02	0, 13
AH-68-17	07	2	73		139	26	<5	<0.1	25	14	778	2	42		95	<5	0.3	5	21	0.01	1.70	0.42	5.29		0.06	<0.01	0.14
AU -02 - 17*	0.7		76		140	27	-5	<0.1	25	14	784	0	43	63	94	<5	0.3	5	21	0.01	1.73	0.42	5.44	1.43	0.08	<0.01	0.14
AU-99-11-	0.7	ľ										-															
44.88.48	0.0	<u>ہ</u> ا	76		120	24	5	<0.1	25	15	793	2	47	70	109	17	0.4	8	24	0.02	1.85	0.46	5, 15	1.48	0.08	0.01	0.14
AH-08-10	0.0		77		140	22		-11	25	21	1110	0	58	86	161	5	0.5	ġ	25	<0.01	2.54	0.45	6.36	1.91	0.14	0.01	0.16
	0.0				143	71		-01	24	91	1007	0	54	66	208	4	0.6		28	<0.01	2.17	0.42	6.26	1.46	0, 15	0.01	0.13
AH-00-20	0.5				120	76		-01		20	A15	- 3	57		249	5	0.6			<0.01	2.01	0.44	6.26	1.30	0.17	0.01	0,13
AH-66-21	0.5			10	142	112		-0.1		21	1066		51		202	5	0.6		24	<0.01	2.78	0.44	6.71	2.03	0.14	<0.01	0.16
AH-68-22	0.4	2	<b>0</b> 0	ĸ	142	112	~3	<0.1		- "		~			EVE	~	0.0	-				•					
444 449 779					125	-6		-01		23	1220	0	51	20	311	<5	0.5		32	<0.01	3.13	0.63	7.08	2.40	0, 15	0.01	0.17
AH-08-23	0.4		00		492			10.1		18	877	2	98	70	205	-5	0.4	Å	95	0.02	1.26	0.42	4.61	0.00	0,14	0.02	0.14
AH-00-29	1.3		120		402	20		0.0		42	1100				87		0.0	14		0.13	184	0.40	8.04		0.18	0.16	0.10
AR-88-50	0.2				124	17		<0.1	100 S.		1180	~			72		0.0	16		0.16	176	0.42	4 81		0 15	0.17	0.00
AR-88-51	0.1	2	20		11/	12		<0.1			540		-		174		0.0			0.00	0.95	0.77	2.28	0.85	0.36	0.06	0.08
STD-P1	0.2	61	26		146	20	\ <b>~</b> >	0.1		•	300	~		- 41	174		0.4			0.00	0.00	4.67	2.20		0.00		4.44
											074		20	40	<b>6</b> 0			17	48	0.10	128	0.45	5.61	0.82	0.16	0.12	0.07
AH~85-02	<0.1	1 3	20		140	55		0.2							80					0.17	108	0.58	5.26	1 90	0.16	0 17	0 11
AR-68-53	<0.1	2	34	<b>K</b>	106			<0.1	e	14	002	~	30	10	00		0.9		40	0.17	1.00	0.40	5.03		0.10	0.15	0.10
AR-88-54	<0.1	3	42		93	10		<0.1	2	10	060	~	3/				1.0			0.17	1.04	0.40	4.04		0.14	0 13	0.10
AR~68-55	<0.1	2	46		94			<0.1		15	880	2			67		1.0	14		0.10	9.07	0.97	5 38		0,14	0.34	0.00
AR-68-57	<0.1	3	26		86		9	<0.1		10	000	~		•	5/	~	1.0			0.20	£.07	0.02	0.00		0.10	0.04	0.00
	1				400					47		-					1 10	1 44		0.18	101	0.58	5.45		0.14	0.18	0.00
AR~88-60	<0.1	3	23		102	•	<b>~</b>	<0.1	100 <b>F</b>	"	004	4	00		00					0,10	1.01	0.00	4.95		0.11	0.00	0.00
AR-68-62	<0.1	1	26	10	83		6	<0.1		9	703	2		<b>30</b>	01	9	0.6	1 🟅	30	0.07	1.01	0.30	4.62	4.00	0.11		0.00
AR-68-64	< 0.1	2	24		78	<5	6	<0.1	35	9	768	2	32		51	<0	0.4		20	0.08	1.03	1.00	4.03		0.07	0.04	0.11
AR~88-74	0.5	3	75	12	107	46	45	<0.1	100	17	1062	2	37	<b>S</b>	63	0	0.3	3	10	0.02	2.08	1.00	Ci.0	LOI	0.12		0.10
AR~88-74*	0.5	2	75	10	110	44	4	<0.1	19	18	1077	~2	38		62	< >	0.3	3	60	0.02	2.08	1.70	0.18	10/	0,12	[ 0.01]	U. 10
· · · ·		1				1						_				-		- 1			0.00	ا ممد ا				المما	0.40
AR8878	0.3	3	103	91	127	21	5	<0.1	23	20	1143	2	41		90	<5	0.4	7	•3	0,02	2.08	0.96	6,22	1.62	0.11	0.01	0.16
AR-68-79	0.1	1	90	13	117	19	45	<0.1	24	20	1130	<2	47	<b>8</b> 8	102	<5	0.5	9		0.02	2.09	0.96	0, 16	1.61	0,14	0.01	U. 16
AR6880	0.4	3	87	12	113	21	5	<0.1	24	19	1094	2	44	85	111	<5	0.5	8	<b>6</b> 2	0.01	2.03	0.91	6.06	1.57	0,13	0.01	0.15
AR-66-63	0.2	2	86	13	113	15	j <5	<0.1	23	19	1069	2	46	84	101	, <5	0.4	7	57	0.02	2.04	0.82	5.94	1.58	0, 15	0.01	0.15
AR-86-84	0.3	1 1	90	10	84	23	<5	<0.1	19	18	1018	2	36	76	111	<5	0.3	5	59	0.03	1.70	1.83	4.92	1.36	0.20	0.01	0, 15
						1	ł									1	1										• • -
AR-66-65	1.6	20	99	59	4 19	25	13	3.0	53	13	632	2	65	33	173	<5	0.4	8	17	0.01	0.70	0.23	3.61	0.50	0.11	0.01	0.10
AR-88-86	1.9	37	135	35	489	24	1 11	3.6	89	17	687	6	71	48	188	<5	0.5	9	27	0.01	0.92	0.36	4.46	0.76	0.12	0.01	0.12
AR-88-87	1.6	30	110	29	429	20	18	3.3	73	14	575	3	68	41	169	<5	0.4	8	23	<0.01	0.79	0.30	3.64	0.67	0, 10	<0.01	0.10
AR-88-88	1.5	36	124	29	433	21	14	3.2	86	16	594	3	62	47	177	<5	0.4	8	23	0.01	0.85	0.27	4.13	0.71	0.10	0.01	0.11
AR-88-85*	1.6	38	125	25	436	21	10	3.2	87	15	588	2	62	48	175	<5	0.3	7	22	0.01	0.85	0.26	4.11	0.70	0.10	0.01	0.11
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		<u> </u>						_		_		_	_						_								

Geochemical Analysis

Project/Venture:	1P	Geol:	K TROCIUK	Date Received:	JULY 30, 1992	Page	3 of	
Area:	COREY	Lab Project No.:	D2469	Data Completed:	AUG 12, 1992	Attn:	K TROCIUK	
Remarks:							<b>S HOFFMAN</b>	
Au - 10.0 g sample o	ligested with Aqua Regia and deb	smined by Gaphite Furnace A.A. (D.L. 1 PPB)					J KOWALCH	Ж
ICP - 0.5 a sample d	ligested with 4 ml Agus, Regis at 1	00 Deg. C for 2 hours.					E KIMURA	

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All - 10.0 g sample digested with 4 ml Aqua Regia at 00 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are tarely dissolved completely with this acid dissolution method.

SAMPLE	Ag	Mo	Cu	Pb 🛛	Zn	As	Sb	Cd	M	8	Mn	Bi	Cr	<b>Y</b>	Ba	W	Be	LA	<b>- 8</b> (	n	A	Ca	Fe	Ma	ĸ	Na	P
No.	ррп	n ppm	ppm	o ppm:	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<b>%</b>	%	<u>%</u>	%		%	%	%
AR-88-89	0.5	7	89	17	139	15	<5	0.2	41	18	$\overline{m}$	2	59	101	116	<5	0.6	10	39	0.04	1.64	0.55	4.82	1.48	0.09	0.01	0. 15
AR6690	0.4	8	87	2	119	14	- 5	<0.1	35	18	783	<2	56	103	- 93	< 5	0.5	9	37	0.04	1.67	0.54	4.80	1.49	0.08	0.01	0.15
AR-88-91	1.3	36	123	28	507	27	10	4.3	75	15	615	2	38	36	86	<5	0.4	7	25	<0.01	0.68	0.31	3.73	0.56	0.05	<0.01	0.11
AR-88-92	0.6	6	95	<b>H</b>	139	16	6	0.2	41	18	776	<2	60	94	117	<	0.6	9	35	0.03	1.59	0.49	4.67		0.06	0.01	0, 15
AR-88-93	0.8	11	100	13	216	15	<5	1.4	47	18	8 19	2	65	96	118	<5	0.5	8	38	0.04	1.61	0.61	4.88	1.40	0, 10	0.01	0.14
																i I											
AR-86-94	1.7	40	190	18	598	- 33	<5	8.8	95	29	1305	2	78	38	321	<5	0.5	9	28	<0.01	0.89	0.31	4.11	0.63	0.09	0.01	0.14
DL88192	0.2	4	33	7	201	- 34	- 5	0.7	36	14	1128	2	61	62	102	<5	0.7	9	19	0.05	1.76	0.35	5. 12	1.07	0.10	0.05	0, 10
DL-86-193	0.3	6	34	5	204	36	ব	0.6	37	13	1071	2	62	58	89	<5	0.7	9	19	0.04	1.73	0.37	4.85	1.11	0.09	0.04	0.00
DL-88-197	0.4	4	76	5	138	40	6	0.1	20	18	882	2	34	46	46	<5	0.3	4	168	<0.01	1.54	2.85	5.36	1.07	0.07	0.01	0, 15
DL-68-197*	0.4	4	79	7	144	30	<5	<0.1	20	17	886	2	34	45	46	<5	0.3	3	188	<0.01	1.53	2.86	5.32	1.07	0.07	0.01	0.15
			í .																								
DL-88-198	0.8	3	125	17	161	75	ব	<0.1	29	25	872	3	45	49	38	্ৰ	0.4	7	192	<0.01	1.52	2.95	7.25	1.05	0.12	0.01	0.13
DL-65-199	0.5	2	127	19	188	82	୍ ଏ <u>।</u>	0.1	30	26	898	3	44	49	36	<5	0.3	4	199	<0.01	1.57	3.05	7.71	1.05	0, 12	0.02	0.14
DL-66-201	0.5	1	131	18	171	70	<5	0.2	31	27	902	2	31	50	37	<5	0.4	7	184	<0.01	1.47	2.94	7.21	1.03	0.07	0.01	0.15
DL88-203	0.5	<1	100	13	152	49	්	<0.1	25	22	941	2	40	51	47	ব	0.4	7	220	<0.01	1.61	3.32	6.51	1.11	0.10	0.01	0.14
DL-85-204	0.4	1 1	105	12	143	56	<5	0.1	25	20	883	<2	30	47	39	্ৰ 🕹	0.4	6	182	<0.01	1.45	2.87	6, 16	1.02	0.07	0.01	0.15
					!																						
DL-88-224	0.3	4	85	10	116	28	6	<0.1	54	17	787	2	87	85	63	<5	0.6	11	49	0.07	1.73	0.48	4.49		0.16	0.07	0.13
DL68225	0.2	5	80	12	98	20	4	<0.1	48	16	744	2	81	62	56	<5	0.6	9		0.06	1.58	0,44	4.38	1.36	0.14	0.05	0, 12
DL88226	0.1	4	81	14	100	21	<5	<0.1	47	15	768	2	63	66	61	<5	0.6	8	48	0.07	1.68	0.42	4.51	1.42	0.15	0.05	0.13
DL88227	0.1	5	81	12	97	18	<5	<0.1	48	15	791	~2	61	64	- 58	<5	0.6		53	0.06	1.66	0.40	4.37	1.40	0.13	0.04	0.13
DL-88-227*	0.1	2	80	13	95	16	<5	<0.1	47	15	772	2	61	62	56	<5	0.5	8	50	0.05	1.62	0.39	4.26	1.37	0.13	0.04	0.12
																1											
DL-86-228	0.5	5	114	19	109	18	<5	<0.1	51	17	806	2	78	65	86	<5	0.6	11	61	0.05	1.62	0.33	4.38		0.12	0.04	0.11
DL-85-229	0.3	4	104	17	111	15	<5	<0.1	52	17	797	2	67	64	81	5	0.6	10	65	0.05	1.62	0.34	4.37		0.11	0.04	0.11
DL-88-230	0.2	5	97	15	107	15	<5	<0.1	51	16	783	2	70		80	্ৰ	0.6	10	63	0.05	1.62	0.35	4.30	1.42	0, 12	0.04	0.11
DL-88-231	0.1	5	106	16	113	12	- 5	<0.1	51	17	782	2	74	69	76	<5	0.6	12	54	0.05	1.71	0.36	4.52	1.49	0, 10	0.04	0. 12
DL-88-232	0.3	6	105	17	113	16	<5	<0.1	52	17	787	2	71	67	78	<5	0.6	12	57	0.05	1.71	0.35	4.40	1.50	0.11	0.04	0.12
		4	<b>I</b> 1													[							I				i
DL-88-233	0.3	4	96	17	111	12	- 5	<b>&lt;</b> 0.1	49	16	749	2	72	<b>\$5</b>	74	4	0.6	10	53	0.05	1.65	0.34	4.24		0.10	0.04	0.11
DL86234	0.3	4	92	10	112	- 14	<5	<0.1	50	15	755	2	77	65	82	(3)	0.5	9	59	0.04	1.70	0.33	4.18	1.50	0.11	0.04	0.11
DL88235	0.1	3	90	15	107	- 14	<5	<0.1	49	15	776	2	85	66	83	<5	0.5	9	58	0.05	1.70	0.35	4.25	1.51	0.11	0.04	0.12
DL-88-236	0.2	3	92	16	91	- 14	්	<0.1	27	15	820	2	60	75	81	<5	0.6	8	\$3	0.06	1.54	0.44	4.34	1.14	0.15	0.04	0, 13
STD-P1	0.2	59	25	56	147	19	4	0.1	37	7	572	2	108	34	182	<5	0.5	8	71	0.08	0.96	0.72	2.32	0.90	0.35	0.05	0.00
	1	1	1		1											1 1										1	
DL-66-237	0.2	2	102	10	<b>9</b> 3	15	ব্য	<0.1	27	16	866	∕2	59	78	85	5	0.6	9	34	0.07	1.61	0.48	4.40	1 18	0.17	0.04	0.13
DL88238	0.1	5	106	15	95	25	්	<0.1	27	18	820	<2	60	80	99	5	0.9	14	41	0.07	1.54	0.53	4.06	1.07	0.20	0.04	0, 13
DL88239	0.1	1	100	13	105	22	<5	<0.1	30	19	870	2	56	. <b>82</b>	90	্ ব	0.9	15		0.07	1.59	0.48	4.37		0.16	0.04	0.13
DL-86-240	0.1	4	120	17	107	25	5	<0.1		19	950	6	55	71	83	<5	0.8	11		0.05	1.54	0.47	4.89	1.10	0, 16	0.03	0, 16
DL-86-241	0.3	2	108	14	102	19	<5	<0.1	27	18	896	5	57		90	্ ব্য	0.7	10	24	0.07 [	1.81	0.50	4.78	3.31	0.22	0.03	0. 15
						i l		f							÷												
DL-88-242	<0.	1 4	60	12	119	30	4	<0.1	25	19	1311	3	54	ात	87	<5	1.0	11	60	0.12	1.71	0.62	4.41	12	0. 13	0. 10	0.11
JP8827	<0.	1 3	56		74	<5	<5	<0.1	28	14	425	2	55		3 15	⊲	0.5	4	22	0.07	1.67	0.84	3.87	1.24	0.26	0.03	0.14
JP-68-30	<0.	1 <1	19		33	<5	<5	⊲0.1	18	6	2 19	2	49	46	78	⊲	0.2	12	25	0.04	0.55	0.44	2.47	0.48	0.13	0.02	0, 15
JP-68-32	<0.	1 2	23	2	44	<5	<5	<0.1	24	7	277	3	106	51	1 16	<5	0.2	14	41	0.07	0.76	0.49	2.70	0.61	0.20	0.05	0, 14
JP-68-32*	<0.	1 2	22		46	<5	<5	<0.1	24	7	269	2	109	50	114	<5	0.2	13	40	0.07	0.75	0.49	2.65	0.61	0.20	0.05	0.14
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**Geochemical Analysis** 

	Projec Aria: Roma: Au — 1	tVentur 1ks: 10.0 g at	e: Imple d	gested	1P COREY with Aq	un Reg	in and c	<b>Sotermi</b>	ned by (	Gaphik	Furnac	Geol: Lab Pro	oject No [D.L. 1 F	.: РРВ)	k troc D2469	SIUK		Date R Date C	eceived omplete	: id:	JULY 30 AUG 12	), 1992 , 1992	,	Page Attn:	4 K TROC S HOFI J KOW	of XUK FMAN ALCHUK	7 (
	юр N.B. Т	0.5 g sa he majo	mple di roxide (	geste d element	with 4 m 18, Ba, B	al Aqua ie, Cr, L	Hegia # a and V	ut 100 E Valie Ri	leg. Cit rely dis	or 2 hou solved	ini. complei	tely with	n this ac	id disso	dution r	nethod										на	
SAMPLE	Ag	Mo	Cu	Pb	Zn	As	Şb	Cd	N	Co	Mn	Bì	Cr	V	Ba	W	Be	La	Şr	Ti	A	Qa .	Fe	Mg	K	Na	P
No.	ppm	Ppm.	ppm	ppm	ppm	ppm	ppm	ppm	ppm	PPm.	ppm	ppm	ppm 53	- ppm	ppm	ppm	ppm 0.2	ppm 14	E DOUR	70	70	70	70		70	70	70
JP88-33	0.1	2	26	Ľ	41	<5		<0.1	22		242	2	- 53		100		0.3	14		0.05	0.64	0.92	2.42	0.00	0.10	0.02	0.13
JP8834	<0.1	3			30	0	6	<0.1	20		230	3	122	24	109	7	0.3	15	35	0.00	0.00	0.30	2.34		0.18	0.00	0.00
JP-68-36	<0.1	6	29	2	3/		9	0.1	20		210	0	09	02	9/ 75		0.4	10	20	0.06	0.03	0.37	2.01	A 14	0.17	0.04	0.08
JP-68-38	<0.1	< <u>1</u>	20		33			<0.1	2		192	3	**		75		0.5	12		0.04	0.51	0.35	2.14		0.12	0.01	0.11
JP68-39	<0.1	" P	24	*	30	<∞	~ ~	<0.1	20	•	270	3	09		89	<0	0.3	13		0.05	0.05	0.37	2.43	0.00		0.04	0.08
					97			-		<b>.</b>	202		55	57	82	-	04	14	00	0.04	0.57	0.36	2 45	0.48	0 13	0.00	0 11
JP-00-41	<0.1		20		37						200	2	107		100	~	0.4		3.4	0.06	0.64	0.44	3 19	047	0.17	0.04	0 11
JP00-43		12	20		34						201		48		85	-5	0.3	12	so	0.05	0.60	0.34	2.09	0.50	0.14	0.02	0.10
JP-00-40	0.1		21		37					i i	108		45		81	5	0.2	11	27	0.05	0.57	0.34	2.08	0 49	0.13	0.01	0.10
JF-00-45-	0.1									45	374		47		118	7	0.4			0.06	1 10	0.02	2 85	A 86	0.15	0.03	0 10
JP-08-40	<0.1	2	57		3,	<0	~	<b>~</b>			214	~	-1		,,,,	· ·		, J		0.00	1.10	0.02				0.00	0.10
IP_88_47	<01	2	61	,	36	<5	6	-0.1	25	16	328	3	65	67	138	8	0.5	6	62	0.09	1.36	1.01	3.22	1.67	0.20	0.04	0,10
JP-88-48	0.1	1 2	57	2	33	<5	<5	<0.1	25	17	294	2	77	65	131	9	0.4	6	56	0.08	1.25	1.03	3.24	0.95	0.17	0.05	0.10
JP-88-49	0.4		63		133	<5	- 65	0.5	25	16	328	4	77	66	142	7	0.5	7	64	0.09	1.37	1.01	3.16	1.07	0.21	0.04	0.10
10-00-50	0.3		56		63	<5	<5	<0.1	23	16	279	0	64	59	134	6	0.4	5	57	0.07	1.21	1.02	2.99	0.92	0.16	0.04	0,10
JP_88-51	0.1		67		65	5	5	<0.1	25	19	314	6	55	67	130	9	0.5	6	61	0.08	1.34	1.02	3.29	1.06	0.20	0.03	0,10
		<sup>•</sup>										-						_									
JP-88-52	0.3	2	64	<1	54	<5	<5	<0.1	26	18	317	2	74	67	124	<5	0.5	6	69	0.09	1.41	1.27	3.34	1.09	0.20	0.05	0, 10
JP-88-53	0.1	2	68	5	46	<5	<5	<0.1	25	17	344	2	72	70	131	<5	0.4	5	68	0.10	1.49	1.09	3.39	1.16	0.24	0.04	0, 10
JP-88-54	0.1	2	65	2	36	<5	<5	<0.1	23	16	278	2	51	64	114	<5	0.4	4	61	0.08	1.30	1.13	3.28	1.02	0.20	0.03	0.10
JP-88-54*	0.1	1	63		34	<5	<5	<0.1	22	16	275	2	50	64	112	<5	0.3	3	59	0.08	1.29	1.12	3.24	1.02	0.20	0.03	0.10
JP6855	<0.1	4	70		42	<5	<5	<0.1	26	17	335	2	70	74	134	5	0.5	6	63	0, 10	1.45	1.05	3.51	1, 15	0.25	0.04	0, 10
																										1	
JP-88-56	0.1	4	68	<1	41	<5	<5	<0.1	28	19	314	2	69	75	127	9	0.4	5	64	0, 10	1.45	1, 16	3.56	<b>1.15</b>	0.23	0.04	0.11
JP88-57	<0.1	2	64		45	<5	<5	<0.1	26	17	332	5	76	71	135	<5	0.5	8	60	0, 10	1.40	0.99	3.38		0.23	0.04	0, 10
JP6858	<0.1	5	73		46	<5	<5	<0.1	25	20	292	4	49	72	118	6	0.5	7	67	0.09	1.39	1.46	3.42	1.11	0.24	0.03	0, 10
JP-~6859	0.1	1	Π		39	<5	<5	<0.1	28	21	346	4	66		139	<5	0.4	5	72	0.12	1.66	1.25	3.75	1.27	0.30	0.04	0.10
JP-68-67	<0.1	4	82	7	75	<5	<5	<0.1	28	17	468	3	74	79	334	<5	0.8	8	79	0, 10	1.98	0.68	3.64	1.28	0.30	0.03	0.11
						-					420			BE	205	-		7	100	0.00	1.60		3.81		0.21	0.00	0 +2
JP-88-71	<0.1	1 1	00		04		6	<0.1			922	2	6		460	<b>4</b> 5	0.0			0.00	1.00	<b>7.00</b>	3.01		0.31	0.03	0.12
JP68-72	<0.1	3	4/	. Sł	50	0		<0.1	<u> </u>	10	333	4	69	60	100	69	0.5	5		0.09	1.30	1.02	4.00	1.00	0.24	0.04	0.13
JP-68-74	0.1		63			<5		<0,1	29		440	~	00		300	<0	0.7	5		0.10	1.00	1.82	3.80		0.32	0.04	0.13
JP-68-74	0.1	2	62		70		0	<0.1	20	10	434	°.	79		307	<3	0.0		110	0.10	1.01	1.00	3.09		0.31	0.03	0.12
JP8875	<0.1	3	68	1000 <b>/</b>	12			<0.1		"	421	~	13		393	20	0.7	•	100	0.09	1.02		4, IJ	1.50	0.31	0.04	0, 13
10-68-76			57		79	-	a	41	31	17	368	0	83	95	376	4	0.6	7	89	0.08	1.69	0.83	4, 14	1 10	0.25	0.05	0.14
IP-68-79	201	3	40	15	101	23	6	40.1	1	14	711	0	47	50	126	<5	0.4	10	40	0.02	1.59	0.72	4.30	1.11	0.11	0.01	0.13
1P_88			30	12	93	17		40.1	1	12	006	0	36	45	86	5	0.4	9	31	0.01	1.50	0.58	3.98	1.06	0.07	<0.01	0.12
IP_68_61	0.0	2	43	ű	116	21	6			13	660	0	56		113	<5	0.4	10		0.01	1.64	0.83	4.05	123	0.11	0.01	0.12
JP-88-82			54		243	25		0.6		14	735	0	46	53	122	<5	0.3	9	26	0.01	1.68	0.44	4.37	123	0.10	0.01	0.13
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### PLACER DOME RESEARCH CENTRE Geochemical Analysis

Project/Venture: Area:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2469	Date Received: Date Completed:	JULY 30, 1992 AUG 12, 1982	Page Attn:	5 of K TROCIUK S HOEFMAN		7
Remarks: Au - 10.0 g eample digested	with Aqua Regia and determined by Graphite Furn	ace A.A. (D.L. 1 PPB)					J KOWALCH	UK	

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ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours.

N.B. The major oxide elements, Ba, Be, Cr, La and W are rarely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Mo	Cu	Pb	Žn	As	Sb	Cq		Co	Mn	Bij	Cr	¥	Ba	w	Be	LA	স	<b>"</b>	~		re .		- D	1988. 97	
No.		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	76	70	70	70		70	- 701	~
JP-88-92		0.4	2	53	<1	129	- 14	4	<0.1	22	23	1080	3	37	75	203	୍ଷ	0.3	2	DI	<0.01	1.70	1.01	0.01	2.71	0.14	-0.01	0.15
JP-88-93		0.2	<1	60	2	124	<5	ব্য	<0.1	21	21	1162	4	35	89	160		0.4	2		<0.01	2.00	0.00	4.94		0.10	0.01	0 13
JP-68-109		<0.1	1	27	2	131	<5	<5	<0.1	15	9	795	2	51	51	110		0.5			0.00	1.73	0.45	4.04		0.10	0.00	0.13
JP88110		<0.1	3	43	8	129	<5	୍	<0. 1	16	10	795	2	39	50	115	0	0.5			0.06	1.00	0.41	9.09		0.08	0.00	0.10
JP-88-111		0.1	6	27	6	151	<5	(5)	<0.1	18	10	817	~2	60	48	114	4	0.5	10	51	0.06	1.67	0.40	4.04	100	0.11	0.04	0.12
IP-88-112	1	0.1	5	29	5	147	6	ব	<0.1	19	10	825	5	41	48	1 19	්	0.5	10	35	0.06	1.60	0.39	4.60	1.07	0.00	0.04	0.12
IP_88_113		01	5	34	7	168	- 5	<5	0.2	21	10	862	- 4	55	51	105	<5	0.6	11	- 30	0.06	1.76	0.41	5.09	1.10	0,10	0.03	0.13
JP-88-114		<0.1	5	32		158	<5	ব	<0.1	19	10	811	~ 2	46	- 52	90	<5	0.5	10	27	0.06	1.68	0.41	5.04		0.06	0.03	0.13
eTD_P1		0.3	61	26	49	147	21	<5	0.1	34	6	581	~ ~	115	33	176	ব	0.4	6	78	0.09	1.01	0.83	2.29	0.87	0.35	0.06	0.06
40 - 40		-01	3	35	7	161	4	<5	0.2	20	9	794	2	50	48	93	ත්	0.5	12	25	0.04	1.60	0.37	4.76	1.01	0.10	0.02	0.12
JF-00-120			•																			•						
10 00 101		-01	4	35	7	169	9	<5	0.3	21	9	814	2	53	48	89	ব	0.6	12	25	0.04	1.60	0.36	4.74	1.02	0.11	0.02	0.12
JP-00-121		201	3	35	7	167	9	- 6	0.3	21	10	807	2	51	48	95	<5	0.6	12	28	0.05	1.60	0.37	4.75	1.02	0.11	0.03	0.12
JP-00-122		-0.1	2	30	7	156	9	<5	0.1	20	9	786	<2	50	45	87	<5	0.5	11	24	0.04	1.57	0.34	4.63	1.01	0.08	0.02	0.12
JP-00-123		20.1		200		160	7	-	<0.1	20	9	765	~2	46	46	93	්	0.5	11	26	0.05	1.57	0.35	4.69	1.02	0.10	0.03	0.12
JP-68-12/		20.1	- -	24		93	7	-5	<0.1	28	11	1128	~2	46	62	79	<5	2.8	14	45	0.13	1.55	0.47	7.35	1.06	0.10	0.12	0.08
JP-68-131		~~.	~	<b>•</b> •			•														1							
10.00_1310		-01	10	24	•	96	6	ব	<0.1	29	12	1166	2	47	63	80	<5	2.9	- 14	46	0.13	1.59	0.49	7.50	1.09	0.11	0.12	0.08
JF-00-131		20.1	1	7		46	4	- 6	<0.1	10011	7	305	~2	93	46	150	6	0.5	19	66	0.09	0.80	0.52	2.54	0.58	0.19	0.05	0.14
	- I	-0.1	-1			42	<5	6	<0.1	50	6	270	2	80	48	140	7	0.4	19	61	0.08	0.75	0.51	2.57	0.56	0.17	0.04	0.15
18-00-2	- í	<0.1		Ĭ		34	4	6	<0.1		6	223	2	44	38	1 18	<5	0.4	17	50	0.06	0.61	0.40	1.96	6.49	0.14	0.02	0.13
18-68-3		<0.1	-1				-5	6	<0.1	11	7	273	2	92	42	142	<5	0.4	14	53	0.08	0.75	0.34	2.20	0.57	0.16	0.04	0.08
18-00-4		<b>VU.1</b>	~'	ľ			~	-					_									1						
TD 88 5		0.1	3	ء ا	10	53	<5	6	<0.1	13	8	327	2	96	53	168	5	0.5	20	63	0.12	0.93	0.49	2.65	0.64	0.23	0.06	0.11
10-00-0		<0.1	-1			37	-5	6	<0.1		7	254	2	82	42	150	<5	0.4	15	56	0.09	0.74	0.36	2, 16	0.56	0.20	0.04	0.09
18-50-0		<0.1				35	-	- 5	<0.1	10	7	242	2	82	43	145	්	0.3	14	53	0.08	0.70	0.36	2.21	6.52	0.21	0.04	0.06
10-00-/		<0.1	-1		,	30	- 6	6	<0.1	11	6	217	2	108	65	115	<5	0.3	17	52	0.08	0.60	0.48	3.02	0.42	0.16	0.05	0.12
10-00-4		<0.1		1 10		34	6	6	<0.1	14	7	235	2	121	55	130	ব	0.3	17	55	0.10	0.72	0.55	2.62	0.50	0.20	0.07	0. 13
10-00-12		<0.1	3	*			-	-																				
TD 00 101		~0.1	Ι.	13		35	ব	6	<0.1		7	238	2	124	55	132	ব	0.3	17	56	0.10	0.73	0.55	2.65	0.50	0.21	0.07	0, 13
		0.1		35		194	19	6	1.1		9	1041	2	65	42	110	ব	0.7	12	22	0.04	1.39	0.32	4.34	0.75	0.15	0.05	0.09
10-00-14 TD 00 45		0.1		20		181	18	đ	0.7	35	8	1099	2	69	42	111	<5	0.7	11	20	0.03	1.43	0.30	4.46	6.77	0.15	0.04	0.09
10-00-00		0.2		94		105	10	6	0.8	36	9	1151	2	58	43	108	5	0.7	11	21	0.04	1.49	0.33	4.62	0.79	0.14	0.04	0.10
TD 40 40		0.1		32		187	18	đ	0.5		8	936	4	76	45	115	<5	0.8	12	19	0.03	1.57	0.31	4.73	6.84	0.17	0.04	0, 10
10-00-10		0.3	`'	‴			~		<b>.</b> -		1							1				L				1		
TD 00 00		0.9		97		157	11	5	0.1		7	702	0	75	45	98	<5	0.7	11	10	0.03	1.54	0.27	4.60	0.84	0.16	0.03	0.09
18-55-20		U.Z		4		110		تم ا		20	5	517	2	62	42	86	<5	0.6	10	14	0.03	1.54	0.22	3.83	0.81	0.11	0.03	0.07
18-68-21		< 0.1	1 1			50		ہ ا	-	20	10	350	0	45	56	Π	<5	0.3	6	34	0.07	1.26	0.53	2.87	0.70	0.21	0.05	0.09
18-66-62		<0.1	1							20	12	420	0	77	67	109	<5	0.3	5	44	0.10	1.58	0.63	3.26	0.80	0.29	0.07	0.09
18-66-63		<0.1	2	1 32							10	356	0	57	64	89	<5	0.3	7	40	0.08	1.33	0.56	3.13	0.67	0.22	0.06	0.10
16-58-65		<0.1	<sup>2</sup>	1 43		<b>30</b>	- <sup>-</sup>	<sup>س</sup> ا	<sup>~</sup> '''		1	~~~		"								1						i
							-	1	6.		11	371	0	60	86	91	ব	0.3	7		0.08	1.39	0.59	3.22	0.69	0.24	0.06	0,10
TB-68-65"		<0.1	?	40		30		1 7		95	1 11	361	0	74	63	99	<5	0.3	8	48	0.09	1.43	0.64	2.87	0.68	0.25	0.07	0.09
16-58-66		0.3	0	1 51						97	1	358	0	94	62	96	8	0.4	10	53	0.09	1.34	0.73	2.86	0.66	0.22	0.08	0.09
18-88-88		0.2	1 1	43	CT C	47					10	311	0	90	60	83	6	0.3	9	81	0.08	1.18	0.74	2.74	0.57	0.19	0.08	0.00
18-68-89		<0.1		34				<u> </u>			19	1061	10	121	73	318	6	0.6	7	20	0.07	2.02	0.60	6.05	1.70	0.14	0.02	0.12
TD-68-1		3.8	5	146		013	1 1/8	'l °	3.2				1 ~	"'		1	1 -											L
			1	1		3	L	L		10000000	3				AAAAAGS 25.20				-									

Geochemical Analysis

Project/Venture: Aren:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2469	Date Received: Date Completed:	JULY 30, 1992 AUG 12, 1992	Page Attn:	6 K TROCI	of UK
Berna rica:							S HOFF	MAN
Au - 10.0 a semple dia	ested with Agus Regis an	determined by Graphite Furnace A.A. (D.L. 1 PPB)					J KOWA	LCHUK

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E KIMURA

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Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB) ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are sarely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Mo	Сц	Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	¥ I	Ba	w	Be	LA	- 51	n	A	Ca	Fe	Mg	K	Nel	<u>۲</u>
Na.		ppm	ppm	ppm	pom	ppm	ppm	ppm	ppm	P.P.C.S	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm.	%	<u>%</u>	%	%		%	_%	<u>*</u>
TD-68-2		3.3	5	117	53	543	173	14	3.4	72	20	2092	- 4	118	76	263	<5	0.7	9	22	0.07	2.08	0.62	6.09	1.14	0.14	0.02	0.13
TD684	F	2.4	5	96	43	430	133	11	2.5	62	19	1974	~2	101	71	199	<5	0.6	6	25	0.06	1.99	0.61	5.60	1.84	0.12	0.02	0.13
TD885		1.4	4	85	34	332	96	12	1.8	55	21	1798	~2	89	$\overline{n}$	160	<5	0.8	8	•1	0.08	2.11	0.73	5.33	2.15	0.13	0.02	0.15
TD-68-6	1	1.5	3	86	38	371	117	<5	21	58	20	18 18	~ 2	97	72	176	<5	0.7	7	30	0.07	2.01	0.63	5.28	1.96	0.13	0.02	0.13
TD-68-7		1.7	5	69	38	370	111	12	2.2	62	21	1963	2	104	76	167	<5	0.7	7	\$0	0.07	2.12	0.64	5.51	2.04	0.13	0.02	0.13
	I		Í																								F	
TD-68-7*		18	4	84		372	110	11	2.1	<b>60</b>	20	1957	2	100	73	159	<5	0.7	7	28	0.07	2.04	0.62	5.45	1.96	0, 13	0.02	0.13
TD_88_8		11	3	68	26	193	56	<5	0.9	33	18	12 19	2	62	53	118	<5	0.7	12	22	0.03	1.60	0.37	4.15	1.00	0.08	0.02	0.07
TD_68_9		14	5	77		262	62	و	12	50	19	1522	2	91	58	146	<5	0.8	12	27	0.05	2.03	0.51	5, 10	1.65	0.11	0.02	0.10
TD-68 - 10		1 9	5			209	50	-5	0.6		18	1448	0	77	63	238	4	0.8	10	48	0.05	1.95	0.56	5.06	1.81	0.12	0.02	0.11
						48.1	93	-5	0.4		16	1043	0	102		134	<5	0.6	A	888. A	0.06	2.00	0.74	4.64	1.66	0.14	0.03	0.10
10-00-12	1	0.0	<b>°</b>	~				<b>∼</b>	V.4			~~~	-			~~~	~		-				••••					
						181	39		05		17	1 184	0		RR	135	-5	0.6		33	0.08	1.99	0.64	4.72	1 70	0.13	0.03	0.10
10-00-13		0.7		50		101	30		0.0			1050	~	103		129		0.5	7	90	0.08	2 00	0.64	471	1 73	0 13	0.03	0.10
10-06-14	1	0.7		53	GL	104	21		0.3		20	720	۲ v	205	503	70		0.5	5		0.17	2.85	0.02	5 10	271	0.16	0.04	0.08
TD-66-19		0.2	2	60	•	128		6	<0.1	100	1 <u>~</u>	708	y y	200		72	10	0.5			0.10	2.00	0.02	5.00		0.17	0.04	0.00
TD-68-16		0.2	1	61		122	0		<0.1			121	4	192		/0	<0	0.5	1		0.10	2.00	0.60	5.20		0.10	0.04	0.00
TD-68-17		0.2	3	63		127	8		<0, 1		23	741	¥.	1/2			<9	0.5	Ð		0.17	2.18	0.83	J. 10		0. 18	0.04	0.00
	ļ											570									0.00	104	0.04	2 20		0.24	0.00	أممه
STD-P1		0.2	64	26	S 51	147	20		<0,1		<u> </u>	5/3	4	115		1/1	<0	0.4	5		0.10	1.04	0.04	2.30		0.30	0.00	0.00
TD-88-16		0.1	<1	62		124	6	<b>S</b>	<0.1	<b></b>	22	701	~	1/4	() <b>1 1</b>	79	13	0.5	0		0.15	2.01	0.65	4.04	i an	0.17	0.04	0.04
TD68 - 19		0.1	2	58		115	11	[ <5	<0.1	78	21	653	2	155	96	87	<5	0.5	6		0.15	2.48	0.84	4.72	7.15	0.18	0.04	0.09
TD88 -20		<0.1	5	70	10	107	10	্ ব	<0.1		22	667	4	131		85	<5	0.8	9		0.14	2.1/	0.81	4.50		0.16	0.04	0.10
TD6821		0.1	<1	11	<1	39	ক	ব	<0.1		6	256	~2	45	40	111	<5	0.4	15		0.06	0.55	0.42	2.14		0. 18	0.02	0.12
				1								_	-				_											
TD-88-21A		0.4	<1	59	5	99	8	ব	<0.1	68	18	631	~	140	2	79	<5	0.6	6		0.15	2.21	0.83	4.61	1.57	0, 17	0.04	0.00
TD-88-22		0.3	2	66	7	101	11	6	<0, 1	63	20	656	2	129	\$3	63	<5	0.7	8	35	0.14	2.13	0.82	4.57		0, 19	0.04	0,10
TD8823	1	<0.1	3	25	<1	36	⊲5	<5	<0.1	22	8	256	4	81	121	97	<5	0.4	17	59	0.07	0.67	0.75	5.65	0.44	0.17	0.06	0.15
TD-68-24		0.2	1	41	2	36	්	4	<0.1	28	10	227	~2	64	60	146	<5	0.3	11	52	0.07	0.88	0.65	2.95	0.64	0.28	0.04	0.14
TD-68-25		<0.1	<1	17	<1	34	<u>්</u>	- 5	<0.1	18	6	243	2	81		75	ব	0.3	16	53	0.06	0.46	0.66	7.59	0.26	0,13	0.05	0, 15
TD8825*		<0.1	<1	16	<1	33	<u>්</u>	- 6	<0.1	17	6	237	2	79	162	74	<5	0.2	15	52	0.06	0.44	0.65	7.50	0.27	0.13	0.05	0, 15
TD-88-25A	1	<0.1	l <1	l 11	2	39	ব্য	<5	<0.1		6	290	2	67	40	119	<5	0.3	19	36	0.06	0.64	0.93	2.31	0.50	0.19	0.04	0.17
TD-86-26	ļ	0.2	<1	18	2 <b>21</b>	28	< গ	<5	<0.1	16	5	197	~2	73	104	81	7	0.2	12	49	0.06	0.51	0.56	5.07	0.30	0.14	0.05	0.11
TD-68-27		0.1	2	18	<1	27	ব	- ব	<0.1	15	6	182	<2	58	101	68	6	0.3	14	46	0.04	0.43	0.52	4.99	0.27	0.12	0.03	0.13
TD-68-28		0.1	<1	17	<1	25	ব	<5	<0.1	15	5	174	<2	57	91	68	<5	0.2	12	47	0.04	0.46	0.57	4.58	0.28	0.11	0.04	0.14
				1 "																								
TD_88_29		<0 \$	21	21	•	27	ক	ক	<0.1	15	6	183	2	56	65	70	<5	0.3	12	41	0.05	0.54	0.56	3.27	0.36	0.14	0.04	0.14
TD-88-30	I	0 1		21		26	6	6	<01	17		177	4	43	105	63	<5	0.1	10	38	0.04	0.46	0.53	5.25	0.28	0.11	0.03	0, 13
TO		-01		ي ا		24			-01	45	5	169	0	57	74	83	<5	0.1	8	48	0.05	0.49	0.47	3.80	0.31	0.14	0.04	0,10
TD_00_22				44		26		1			,	167	0	42	107	58	<5	0.1	10		0.03	0.40	0.48	5.33	0.25	0.10	0.03	0,13
10-00-02		0.1				24					, a	142	0	52			1 .	0.1			0.05	0.48	0.48	2.35	0.000	0.14	0.04	0.11
10-00-33		Ų. 1		en [		-	l ∽	<b>1</b>			J	176	~	~~		I "		<b>•••</b>	<b>"</b>			0.10	00					
			<u>ہ</u> ا			~	-				•	444	~	50		76	-*	0.2	14	4.5	0.05	0.47	045	221	0 20	0 13	0.04	0.10
10-08-33*		0.1		10		2	<0	8	<0.1	10		191	N N	32		10		-0.4			0.00	0.47	0.50	2.61	0.40	0.10	0.05	0.11
10-68-35		0.1	2	42	2	36		9	<0.1			200	2	02		80	<0			-	0.07	0.97	0.02	0.00	0.40	0.13	0.00	0.00
TD6836		<0.1	1 7	27	<1	30	୍	୍ଷ	<0.1	<u> </u>	3	208	2	60	21		<0	<0.1			0.07	0.03	0.40	2.00		0.14	0.00	0.00
TD-68-37		0.1	5	31	<b>*1</b>	33	_ ব	6	<0.1	<b>1</b>	4	229	2	83		62		<0.1			0.08	0.80	4.70	2.03	0.01	0.10	0.00	0.00
TD-88-39		<0.1	<1	61	<1	59	<5	<b> </b> ⊲5	<0.1	24	12	4 16	~2	53	76	170	<5	<0.1	<1		0.08	1.41	1.78	3.60	1.47	0.30	0.05	0.10
			L	L		1			L		i		L	L			L	L			l		L					

### PLACER DOME RESEARCH CENTRE Geochemical Analysis

1P COREY	Geol: Lab Project No.:	K TROCIUK D2469	Date Received: Date Completed:	JULY 30, 1992 AUG 12, 1992	Page Attn:	7 of K TROCIUK S HOFFMAI	4
with A sure Descin and determined by Omnibite Furre						J KOWALCH	<b>IUK</b>

Remarks: Au  $\sim$  10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB)

ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours.

Project/Venture: Area; ١

N.B. The major oxide elements, Be, Cr, La and W are marely dissolved completely with this acid dissolution method.

$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	SAMPLE	A	Mo	Ċu	<b>Pb</b>	Zn	As	Sb	Cd	NI NI	Co	Mn	Bi	Cr	<b>. Y</b>	Ba	w	Be			11	<b>N</b>	Cal	10	. M9	<b>N</b>		<u> </u>
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	No			l ppm		DOM	ppm	ppm	ppm	pom	ppm	ppm	ppm	ppm	ppm	mqq	ppm	ppm	ρρπ	ppm	<u>%</u>	- %	<u>%</u>	<u>%</u>		%	- 20-	- *
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	TD_88 -40			1 5	5 41	54	4	7	<0.1	20	10	445	2	60	73	184	<5	<0.1	<1	53	0.08	1.46	2.09	3.40	1.17	0.29	0.05	0.00
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	10-00-40	<0	1 3	6	4	61	<5	<5	<0.1	24	10	399	~	63	69	168	<5	<0.1	<1	57	0.09	1.43	1.79	3.46	1.03	0.33	0.07	0.10
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	TD_88_42	0.2				58	<5	6	<0.1	23	9	414	~ ~	62	69	189	<5	<0.1	<1	60	0.09	1.47	1.77	3.45	1.07	0.33	0.07	0.10
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	TD-88-43	0.5		5	2	55	<5	6	<0.1	21	6	375	2	49	61	157	<5	<0.1	<1		0.08	1.32	1.92	3, 19	0.96	0.29	0.00	0.00
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	TD_88_44	0.5			5	61	<5	6	<0,1	24	13	404	2	61	71	187	<5	<0.1	<1	60	0.09	- 1.44	1.79	3.75	1.05	0.32	0.07	0, 10
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10-00 -44		' I `	1 -																		ļ					l	
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	TD_88 -44+	ا ام		l s	3	59		ব	<0.1	24	13	394	4	- 60	69	185	<5	<0.1	<1	59	0.09	1.43	1.78	3.74	103	0.31	0.07	0,10
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	TD_88-45	6			1 10	64	ব	(	<0.1	28	15	4 19	2	57	77	167	8	0.5	7	59	0.07	1.29	1.90	3.07		0,31	0.04	0.10
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	TD-88-46			1 5	8	60	<5	- 6	<0.1	25	- 14	4 18	2	46	72	154	6	0.3	3	57	0.07	1.28	1,96	3.04	1.117	0.30	0.04	0.10
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	TD_88_47			5 6	1	61	<5	6	<0.1	26	15	404	2	60	78	197	<5	0.3	3	62	0.08	1.38	2.07	3.21		0.31	0.05	0.10
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	TO -89 -49					61	<5	ব	<0.1	28	15	444	2	69	80	190	<5	0.3	3	70	0.09	1.45	2.07	3.41		0.32	0.07	0, 10
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10-00-40	~	'  "	1 *		1											1											
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	TT - 88 - 40		•   ;	rl 5	8	61	ব	_ ব্য	<0.1	27	14	415	2	76	77	189	<5	0.3	3	70	0.09	1.44	2.43	3.17		0.32	0.07	0.10
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	TD -00 -40			5 5	7	62	<5	6	<0.1	27	15	418	2	67	79	164	<5	0.5	6		0.08	1.41	2.57	3, 10	1.11	0,30	0.06	0,10
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	10-00-00				1	62	<5	6	<0.1	29	16	429	2	72	82	194	6	0.5	7	70	0.08	1.42	2.40	3.24		0.31	0.06	0,10
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	10-00-01					63	<5	6	<0.1	27	14	415	2	62	77	187	<5	0.4	5		0.08	1.37	2,46	3, 16		0.30	0.05	0.10
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	TD 49 59			1 .	3 3	91	6	6	<0.1	27	15	629	2	65	97	77	<5	0.8	9	165	0.03	1.82	1.45	4.18	1.52	0.13	0.02	0.16
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	10-60-03		"  '	'l -			-	1 ~													1							
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	TD	[ [ ] ]	, j	ป่อ	3	80	< ব	ি ব	<0.1	27	15	816	2	64	95	77	<5	0.8	10	163	0.03	1.77	1.43	4.12	1.47	0.13	0.02	0,15
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	10-00-00*				a 🔆 👘	89	6	<5	<0.1	26	15	791	2	60	93	73	19	6.0	11	166	0.03	1,72	1.37	3,96	1.45	0.12	0.02	0.15
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	10-00-04				2	66	<5	6	<0.1	24	13	795	2	64	95	73	<5	0.6	7	<b>141</b>	0.03	1.83	1, 10	4.12	1.55	0.14	0.02	0.15
ID=88-57       Cli       Cli <thcli< th="">       Cli       Cli       &lt;</thcli<>	10-00-00			:l 5	1	86	4	6	<0.1	24	13	762	2	60	94	67	<5	0.6	8	146	0.03	1.77	1.32	4.05	1.46	0.13	0.02	0.15
ID=68-57       C0.1       3       96       9       87       C5       C5       C0.1       25       15       772       C2       56       96       72       C5       0.8       12       144       0.03       1.73       1.24       3.86       1.45       0.12       0.02       0.15         TD=68-56       0.1       2       104       9       91       5       7       0.1       26       16       801       -2       56       96       95       72       <5       0.8       12       144       0.03       1.73       1.24       3.86       1.45       0.12       0.02       0.15         TD=68-50       0.1       2       104       9       91       5       7       0.1       28       16       801       <2       56       96       69       <5       0.7       11       125       0.03       1.71       1.11       3.86       1.44       0.12       0.02       0.15         TD=68-61       0.1       1       7       <1       31       <5       <5       195       <2       91       77       <5       0.2       17       30       0.04       0.50       0.49 <t< td=""><td>10-00-00</td><td></td><td></td><td></td><td>7</td><td>81</td><td>6</td><td>&lt;5</td><td>&lt;0.1</td><td>23</td><td>13</td><td>767</td><td>2</td><td>59</td><td>\$3</td><td>84</td><td>&lt;5</td><td>0.7</td><td>10</td><td>162</td><td>0.03</td><td>1.77</td><td>1.49</td><td>3.82</td><td>1.50</td><td>0, 12</td><td>0.02</td><td>0.14</td></t<>	10-00-00				7	81	6	<5	<0.1	23	13	767	2	59	\$3	84	<5	0.7	10	162	0.03	1.77	1.49	3.82	1.50	0, 12	0.02	0.14
TD-88-58       c0.1       3       96       9       87       c5       c3       c0.1       25       15       772       c2       59       96       72       c5       0.8       12       144       0.03       1.73       1.24       3.86       145       0.12       0.02       0.15         TD-88-69       0.1       2       104       9       91       5       7       c0.1       26       16       901       c2       58       96       69       c5       0.7       11       125       0.03       1.76       0.94       4.06       148       0.12       0.02       0.15         TD-88-60       0.2       c1       92       7       84       c5       c5       0.1       23       13       764       c2       58       96       69       c5       0.6       10       137       0.03       1.71       1.11       3.86       144       0.12       0.02       0.15         TD-88-61       c0.1       1       7       c1       31       c5       c5       c0.1       9       5       195       c2       91       72       95       c5       0.2       17       30       0.0	10-00-0/	``	.	ין י		1	-	-																				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	TD_88_58			ه اه	6	87	ব	ব	<0.1	25	15	772	< 2	59	95	72	<5	0.8	12	144	0.03	1.73	1.24	3.89		0.12	0.02	0.15
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	TD 88 -50		<b>.</b>	10		91	5	7	<0.1	26	16	801	2	58	96	69	<5	0.7	11	125	0.03	1.76	0.94	4.06		0.12	0.02	0.15
ID-66-00       0.2       1       7       c1       31       c5       c5       195       c2       91       72       95       c5       0.2       16       42       0.07       0.54       0.47       3.12       0.39       0.14       0.05       0.14         TD-68-61       c0.1       1       8       c1       34       c5       c5       195       c2       91       72       95       c5       0.2       16       422       0.07       0.54       0.47       3.12       0.39       0.14       0.05       0.14         TD-68-62       c0.1       1       8       c1       34       c5       c5       195       c2       91       72       95       c5       0.2       17       30       0.04       0.50       0.49       3.35       0.39       0.11       0.01       0.17         6TD-P1       0.3       59       27       52       147       20       c5       0.2       90       8       545       c2       109       34       163       c5       0.4       7       69       0.08       0.94       0.74       2.09       0.83       0.33       0.05       0.48       0.05 <td>TO -00 -00</td> <td></td> <td></td> <td></td> <td>0</td> <td>84</td> <td>&lt;5</td> <td>6</td> <td>&lt;0.1</td> <td>23</td> <td>13</td> <td>764</td> <td>⊲</td> <td>58</td> <td>92</td> <td>68</td> <td>&lt;5</td> <td>0.6</td> <td>10</td> <td>137</td> <td>0.03</td> <td>1.71</td> <td>1.11</td> <td>3.86</td> <td></td> <td>0.12</td> <td>0.02</td> <td>0.15</td>	TO -00 -00				0	84	<5	6	<0.1	23	13	764	⊲	58	92	68	<5	0.6	10	137	0.03	1.71	1.11	3.86		0.12	0.02	0.15
ID=66       Cl       I       B       Cl       34       C5       C5       189       C2       40       80       77       C5       0.2       17       30       0.04       0.50       0.49       3.35       0.39       0.11       0.01       0.17         TD=66<-62       C0.1       1       6       5       189       C2       40       80       77       c5       0.2       17       30       0.04       0.50       0.49       3.35       0.39       0.11       0.01       0.17         6TD=P1       0.3       59       27       52       147       20       c5       0.2       30       6       545       c2       100       34       163       c5       0.4       7       69       0.08       0.94       0.74       2.09       0.83       0.33       0.05       0.06         1D=68<-63       <0.11       2       10       5       28       c5       c5       c0.1       9       6       149       c2       56       57       73       19       0.3       17       30       0.05       0.42       0.35       0.38       1.00       0.02       0.11       0.02       0.11	TD-88-81			1 -	7	31	<5	<5	<0.1	9	5	195	2	91	72	95	<5	0.2	16	42	0.07	0.54	0.47	3.12	0.33	0.14	0.05	0.14
BTD-P1       0.3       59       27       52       147       20       45       0.2       30       6       545       <2       100       34       163       <5       0.4       7       89       0.08       0.94       0.74       2.09       0.453       0.33       0.05       0.08         BTD-P1       0.3       59       27       52       147       20       45       0.2       30       6       545       <2	TD -88 -62			il	6 21	34	<5	6	<0.1		5	189	<2	40	80	177	<5	0.2	17	50	0.04	0.50	0.49	3.35	(1996) 1997	0.11	0.01	0.1/
8TD-P1         0.3         59         27         52         147         20         c5         0.2         90         6         545         c2         109         34         163         c5         0.4         7         89         0.08         0.94         0.74         2.09         0.85         0.33         0.05         0.05         0.05         0.05         0.42         0.35         2.35         0.31         0.00         0.02         0.11           TD-88-65         <0.1	1D-00 -04	``	^'	1	-							1						1										
TD-68-63       <0.1       2       10       5       28       <5       <5       <0.1       9       6       149       <2       56       57       73       19       0.3       17       30       0.05       0.42       0.35       2.35       0.31       0.10       0.02       0.11         TD-68-63       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1       <0.1	PTD-P1		3 5	ol 2	7 8	147	20	ব	0.2	30	6	545	( 2	109	34	163	⊲5	( 0.4	1 7		0.06	0.94	0.74	2.09	2003).«	0.33	0.05	0.06
TD-68-65         <0.1         <1         7         2         36         <5         <5         <0.1         4         217         <2         53         33         103         7         0.2         13         18         0.06         0.56         0.38         1.70         0.44         0.17         0.03         0.11           TD-68-65         <0.1	TD_88_63			2 1	0	28	<5	්	<0.1	9	6	149	2	56	57	73	19	0.3	17	<b>SO</b>	0.05	0.42	0.35	2.35	0.31	0.10	0.02	0.11
TD-58-68 <0.1 <1 4 2 33 <5 <5 <0.1 4 3 183 <2 37 26 92 <5 0.1 12 13 0.05 0.49 0.35 1.39 0.40 0.15 0.01 0.12 113 0.05 0.49 0.35 1.39 0.40 0.15 0.01 0.12 0.12 0.15 0.01 0.15 0.01 0.15 0.01 0.12 0.15 0.01 0.01	TD_88 -65		1 -	1	7	36	<5	6	<0.1		4	217	2	53	33	103	7	0.2	13	18	0.06	0.56	0.38	1.70	0.44	0.17	0.03	0.11
	TD-88_68		5il 2	il		33	<5	6	<0.1		3	183	2	37	26	92	<5	0.1	12	13	0.05	0.49	0.35	1.39	0.40	0,15	0.01	0.12
	TD-08-70		31 D		5	33	4	്ക്	<0.1		4	191	2	42	23	93	<5	0.1	12	15	0.06	0.52	0.37	1.35	0.42	0.16	0.02	0.12
	10-00-10		~~  ``	1	-	1	1 ~	1	1		1	[	[	[			[	[										
	TD		<u> </u>	1	4	32	<5	<5	<0.1		4	185	~	41	22	91	<5	0.1	11		0.06	0.50	0.35	1.30		0, 15	0.02	0.11

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E KIMURA

### **Geochemical Analysis**

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Project/Venture: Area:	COREY 1P	Geol: Lab Project No.:	K TROCIUK D2445 DEFMAN	Date Received: Date Completed:	JULY 22, 1992 AUG 11, 1992	Page Attn:	1 of K TROCIUK S HOFFMAN	4
Hernarks:	PULP SAMPLES FROM LORING LABS	RESULTS TO K THOUGH AND TO S IN					010011000	•
Au - 10.0 g sample (	digested with Aqua Regia and determine	d by Graphite Furnace A.A. (D.L. 1 PPB)					J KOWALCH	IUK
ICP = 0.5 a sample o	figested with 4 ml Agua Regia at 100 De	1 C for 2 hours.					E KIMURA	

ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Ba, Cr, La and W are sarely dissolved completely with this acid dissolution method.

bc         pen	SAMPLE	7	Ag M	lo	Cu	Pb	Zn	As	Sb	Cd	Ni	Co	Mn	Bi	Cr	્યજ્ઞ	Ba	w	Be	LA	Sr	n	A	Ca	Fe	Mg	ĸ	Na	P
Act-as-10         0.2         c1         4         16         c1         7         5         25         7         35         100         45         100         45         100         45         100         45         100         45         100         45         100         45         100         45         100         1	No.	P	pm pj	pm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	_ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<u>%</u>	%	<b>%</b>	<u>%</u>	%	%	%	%
Act-as-11       0.3	AE-88-10		.2	<1	4	16	41	<5	<5	<0.1	17	5	257	<2	71	33	110	<5	0.1	12	35	0.06	0,69	0.38	1.96	0.50	0.12	0.04	0.08
Act-ast-12       Q.2       <1       T       S1       S3       C       C       C       S1       C       S1       C       S1       C       S1       S2       C       S1       S1       S2       S2       S1       S1 <t< td=""><td>AE-88-11</td><td>0</td><td>.3</td><td>&lt;1</td><td>17</td><td>22</td><td>192</td><td>24</td><td>8</td><td>0.2</td><td>39</td><td>10</td><td>798</td><td>3</td><td>58</td><td>62</td><td>82</td><td>&lt;5</td><td>0.4</td><td>8</td><td>22</td><td>0.08</td><td>1.95</td><td>0.45</td><td>4.36</td><td>1.25</td><td>0.10</td><td>0.04</td><td>0.09</td></t<>	AE-88-11	0	.3	<1	17	22	192	24	8	0.2	39	10	798	3	58	62	82	<5	0.4	8	22	0.08	1.95	0.45	4.36	1.25	0.10	0.04	0.09
Act-as-10       c.0.1       c.1	AE-88-12	10	.2	<1	12	13	139	20	<5	<0.1	30	7	591	<2	54	54	69	<5	0.3	6	21	0.07	1.63	0.40	3.66	0.99	0.09	0.04	0.07
Act-Ba-20       0.1       1       15       72       91       < 55       < 50       0.1       14       87       70       4       20       67       11       20       0.4       11       20       0.4       11       20       0.4       11       20       0.4       10       0.1       0.01       0.03       0.01       0.03       0.01       0.03       0.01       0.03       0.01	AE-88-19	<	0.1	<1	15	10	90	6	<5	<0.1	13	8	742	3	28	48	104	<5	0.4	12	25	0.07	1.70	0.40	4.61	1.15	0, 10	0.03	0.13
Act-ab-2:         0.1         <1         15         6         94         7         c5         0.1         15         6         97         4         27         46         101         c5         0.0         1.5         6         10         c5         0.0         1.5         6         10         6         22         23         0.00         1.6         0.4         4.7         1.51         0.03         0.1           Act-ab-2.4         0.2         2         177         11         35         5         5         6         0.1         4.58         8.73         4.2         22         0.0         1.70         0.44         4.71         1.10         0.03         0.1         0.03         0.1         0.04         0.02         0.01         0.03         0.01         0.03         0.01         0.03         0.01	AE88-20	6	1	1	15	12	91	<5	<5	<0.1		8	760	4	30	47	114	<5	0.4	11	26	0.07	1.73	0.40	4.61	1.17	0.11	0.03	0, 13
Act-8a-21       0.1       ct       11       0.0       0.1       ct       11       0.0       0.3       0.1       0.1       ct       11       0.0       0.3       0.1         Act-8a-22       0.2       1       11       19       5       c5       0.1       16       8       88       877       c2       20       0.0       170       0.46       4.77       100       0.00       0.01         Act-8a-27       0.2       2       171       111       190       5       c5       0.1       34       4 58       22       50       52       60       10       20       100       100       0.00       2.01       0.00       0.00       0.01       100       0.00       100       0.00       0.00       0.00       0.01       0.00	//2		·	·																									
Act-as2       0.1       c.t       m       11       98       c.t       c.t       1       15       8       818       6       2       20       101       100       11       100       0.1       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.11       0.03       0.01       0.11       0.03       0.01       0.11       0.03       0.01	AE-99-21			~1	15	10	94	7	<5	<0.1	14	8	767	4	27	46	101	<5	0.4	12	23	0.08	1.68	0.41	4.71	1.11	0, 10	0.03	0.13
$ \begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 1 \\ 3 \\ 3 \\ 4 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 4 \\ 5 \\ 5$	AE-99-22			21	10	3 A A	95	<5	<5	<0.1	15	8	8 18	6	28	50	118	<5	0.4	12	31	0.07	1.79	0.45	4.73	1.20	0.11	0.03	0.13
$ \begin{array}{c} Ac = 3 = -7 \\ AC = 3 = -7 \\ STD = P1 \\ \hline \begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	AE-00-22			<b>`</b>	17	3834 (	197	5	<5	0.3	16	8	773	2	27	43	107	<5	0.5	12	25	0.08	1.67	0.41	4.45	1.11	0.11	0.03	0, 12
Act-os-C1         O.5         61         24         54         139         75         0.1         54         4         555         -2         106         33         104         -5         0.3         7         11         0.0         0.06         2.20         0.26         0.35         0.06         0.48           Act-os-C2         1.4         10         113         112         121         13         0.6         11         6         57         140         122         51         1.0         16         35         0.01         182         -5         0.5         9         100         0.04         1.83         4.31         1.02         0.17           Act-os-C6         1.0         9         96         156         1.0         166         77         140         122         177         0.44         1.62         2.0         1.46         1.40         1.02         0.1         0.02         1.11         0.22         0.21         1.40         1.40         1.02         0.11         0.22         0.21         1.46         1.40         0.13         0.02         0.17         1.11         0.22         1.42         1.40         1.40         1.40         1.40<	AE-00-24		2		17		136	5	<5	<0.1		8	839	2	50	52	89	<5	0.5	10	20	0.04	1.72	0.36	4.24	1.10	0,10	0.03	0.11
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$				~			120	10	-5	0.1		Ă	558	2	108	33	164	<5	0.3	7	B1	0.10	1.04	0.86	2.20	0.86	0.35	0.06	0.08
AE=88-48       0.4       0       73       90       918       73       0.1       210       0.50       4.86       1.50       0.51       0.00       0.41       0.51       0.00       0.41       0.51       0.00       0.51	SID-P1	_   <sup>u</sup>	.3	ויי	24		105	13	~~	0.1		•	~~	4					0.0						2.20		•••••		
Ac-Ba-Ba       0.4       B       73       90       97       0.0       47       16       45       95       10							100	40	-5			21	004	5	71	140	120	5	10	16	37	0 13	2 19	0.50	4 88	1 83	0.15	0.06	0.14
AL=08-02       1.4       10       13       14       15       15       15       16       17       18       16       16       17       18       16       16       17       18       16       16       17       18       16       16       17       18       16       16       17       18       16       17       18       16       17       18       16       17       18       17       18       17       18       17       18       17       18       17       18       17       18       17       18       17       18       16       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16       11       16	AE-88-48		•			IU.	180	17	10	0.4	24	46	954	3	50	·····	182	-5	0.4	B	75	0.02	1.38	1.83	4 31	1 12	0 12	0.02	0.15
AE=88-56       10       3       36       66       67       63       60       64       66       64       67       74       76       75       9       100	AE-88-52		•	10	113		212	10	10	0.0		16	860	Ă	54	103	185		0.5	ő	100	0.04	1.69	224	4.37	1.57	0 14	0.02	0.18
AE=88-36       0.7       5       94       10       0.0       0.7       44       10       0.7       14       -7       144       -7       146       -7       94       150       -7       94       170       1144       -7       144       -7       94       155       -50       0.50       9       0.04       155       2.34       4.47       144       0.10       0.11       0.20       0.17       0.11       0.10       0.11       0.10       0.11       0.10       0.11       <	AE-88-56		.0	a	90	0	100	10	40	0.7	<b>40</b>	10	000	7	40		150		0.5		102	0.04	1.60	231	A 16		0.14	0.00	0.17
AE=88-61       0.9       8       90       16       189       19       19       10       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       22       17       18       17       18       22       17       18       17       18       17       18       22       17       18       18       17       18       22       17       18       17       18       22       17       18       18       11       10       14       10       18       23       15       0.5       15       0.5       115       0.04       1.55       2.55       0.5       115       0.04       1.55       2.55       0.5       115       0.04       1.55       2.55       15       0.61       115       2.24       2.24       2.24       2.24       2.24       2.24       2.24       2.24       2.24 <th< td=""><td>AE68-58</td><td></td><td>.7</td><td>5</td><td>94</td><td>13</td><td>166</td><td>20</td><td>10</td><td>0.6</td><td></td><td>10</td><td>04/</td><td>•</td><td>40</td><td></td><td>100</td><td></td><td>0.5</td><td></td><td>104</td><td>0.04</td><td>1.61</td><td>2.34</td><td>4.10</td><td></td><td>0.13</td><td>0.02</td><td>0.19</td></th<>	AE68-58		.7	5	94	13	166	20	10	0.6		10	04/	•	40		100		0.5		104	0.04	1.61	2.34	4.10		0.13	0.02	0.19
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	AE-88-61	10	.9 }	8]	99	16	189	19	0	0.7	<b>1</b>	1/	1 140	~	• *	<u></u>	100	< 2	0.5		<b>111</b>	0.04	1.01	2.04	4.47		0.10	0.02	0.13
AL=88=62       0.6       6       97       14       0.6       15       0.1       15       0.21       17       0.5       1.5       0.5       1.6       0.7       0.8       0.7       0.5       1.5       0.5       0.7       0.7       0.7       1.55       0.5       1.0       0.4       40       15       834       3       48       100       193       c5       0.5       7       115       0.04       1.55       2.3       0.13       0.27       0.5       8       0.15       0.13       0.22       0.17         AE=88=65       0.8       5       90       12       172       18       5       0.6       45       15       841       3       49       95       144       <5       0.6       11       0.65       0.6       0.1       0.13       0.22       0.13       0.23       0.13       0.22       0.17         AE=88-67       0.8       3       99       14       177       12       16       0.5       5       0.1       18       c5       0.4       1.11       0.04       1.81       2.21       1.80       0.31       0.02       0.13       0.22       0.13 <t< td=""><td></td><td></td><td>_</td><td></td><td></td><td></td><td>400</td><td></td><td>1</td><td></td><td></td><td>17</td><td>890</td><td></td><td>47</td><td>6</td><td>155</td><td>أيرا</td><td>0.6</td><td>12</td><td>107</td><td>0.04</td><td>1.62</td><td>228</td><td>4 20</td><td>140</td><td>0 14</td><td>0.02</td><td>0 17</td></t<>			_				400		1			17	890		47	6	155	أيرا	0.6	12	107	0.04	1.62	228	4 20	140	0 14	0.02	0 17
AE=88-63       0.7       4       67       44       159       16       c3       0.3       40       15       624       23       63	AE8862		.8	8	95	14	162	20	14	0.8	<b>.</b>	17	002	~		2	170	~	0.0	12		0.04	1.65	2.31	4.06		0.17	0.02	0.18
AE=88-64 AE=88-65       0.8       6       92       20       158       16       10       0.4       40       15       634       3       46       100       133       <5       0.5       7       105       0.04       158       1.53       0.52       0.4       4.50       1.53       0.52       0.6       4.27       158       634       47       90       136       <5       0.5       180       0.04       1.56       2.40       1.54       0.13       0.02       0.64       155       2.40       1.54       0.13       0.02       0.64       1.55       2.26       4.22       1.54       0.13       0.02       0.64       1.55       2.24       4.22       1.54       0.13       0.02       0.64       1.55       2.24       4.21       1.54       0.13       0.02       0.64       1.55       2.54       0.04       1.55       0.04       1.56       0.04       1.56       0.04       1.56       0.24       4.24       1.54       0.13       0.02       0.67       0.168       0.25       4.14       0.24       0.13       0.02       0.67       0.57       0.57       0.57       0.57       0.57       0.57       0.57       0.57 <td>AE88-63</td> <td>0</td> <td>.7</td> <td>4</td> <td>87</td> <td>14</td> <td>159</td> <td>16</td> <td></td> <td>0.5</td> <td><b>4</b>0</td> <td>15</td> <td>821</td> <td>~</td> <td>4/</td> <td>99</td> <td>100</td> <td>&lt;0</td> <td>0.5</td> <td>0</td> <td></td> <td>0.04</td> <td>1.00</td> <td>2.01</td> <td>4.00</td> <td></td> <td>0.13</td> <td>0.02</td> <td>0.10</td>	AE88-63	0	.7	4	87	14	159	16		0.5	<b>4</b> 0	15	821	~	4/	99	100	<0	0.5	0		0.04	1.00	2.01	4.00		0.13	0.02	0.10
AE-88-65       0.8       4       66       92       169       19       45       0.8       4       47       99       146       5       0.6       1.03       2.28       4.22       1.59       0.20       0.66         AE-88-65*       0.8       5       90       127       18       0.14       177       21       7       0.7       46       16       855       42       47       99       146       55       0.66       11       96       0.04       1.58       2.28       4.24       151       0.13       0.02       0.16         AE-88-72       0.4       <13       91       13       171       12       6       0.5       42       14       0.33       2.2       4.6       91       155       <5       0.4       6       100       0.24       101       0.02       0.17         AE-88-72       0.4       <13       34       10       102       <5       <5       <1       24       20       65       41       0.3       6       33       0.13       1.00       0.51       3.67       1.01       0.38       0.66       0.1       0.25       4.4       107       107       10	AE-68-64	0	.8	6	92	20	158	16	10	0.4	40	15	834	3	48	100	193	<0	0.5	<u>'</u>	115	0.04	1.07	2.40	9.20	100	0.13	0.02	0.17
AE-88-65*       0.8       5       90       12       172       18       5       0.6       15       91       15       91       14       c5       0.5       105       0.04       1.50       2.56       4.24       1.51       0.14       0.02       0.16       0.04       1.50       2.56       4.24       1.51       0.14       0.12       0.16       0.04       1.50       2.56       4.24       1.51       0.14       0.12       0.16       0.04       1.50       2.56       4.24       1.51       0.12       0.14       0.12       0.16       0.04       1.56       2.56       0.64       64 <th66< th="">       66       65<td>AE8865</td><td>0</td><td>.8</td><td>4</td><td>89</td><td>12</td><td>169</td><td>19</td><td>&lt;5</td><td>0.6</td><td>42</td><td>15</td><td>836</td><td>4</td><td>4/</td><td>20</td><td>138</td><td></td><td>0.5</td><td></td><td>100</td><td>0.04</td><td>1.09</td><td>2.20</td><td>9.02</td><td></td><td>0.13</td><td>0.02</td><td>0,10</td></th66<>	AE8865	0	.8	4	89	12	169	19	<5	0.6	42	15	836	4	4/	20	138		0.5		100	0.04	1.09	2.20	9.02		0.13	0.02	0,10
AE-88-67       0.8       3       99       14       177       21       7       0.7       46       16       855       <2       47       91       148       <5       0.6       11       96       0.04       1.55       2.28       4.13       1.45       0.14       0.02       0.17         AE-88-72       0.4       <1       91       13       171       12       6       0.5       <42       148       33       <2       46       91       156       <5       0.4       6       156       0.4       6       105       0.44       1.15       0.13       0.00       0.17       0.00       0.02       0.18       0.02       0.18       0.02       0.17       0.02       0.17       0.02       0.17       0.02       0.17       0.02       0.17       0.02       0.17       0.02       0.17       0.02       0.17       0.02       0.17       0.03       0.3       1.01       0.36       0.03       0.31       1.01       0.36       0.03       0.11       0.13       1.57       0.57       3.79       0.90       0.31       0.05       0.33       0.41       0.47       0.18       0.06       0.13       0.22	AE-88-65*	0	.8	5	90	12	172	18	5	0.6	45	15	841	3	49	୍ଟ୍ର	144	<>	0.5	6	TUD	0.04	1.00	2.30	4.24	1.04	U, 14	0.02	0.10
AE-88-67       0.8       3       99       14       177       21       7       0.7       42       16       653       42       41       91       148       c3       0.04       1.58       2.26       4.13       1.43       1.43       1.43       1.43       1.43       1.41       0.02       0.18         AE-88-72       0.3       3       91       13       171       12       6       0.5       42       41       0.22       46       91       156       c5       0.41       1.1       90       0.55       4.14       0.93       0.02       0.41       1.1       1.90       0.55       4.1       0.02       0.18       0.00       0.51       3.67       1.11       1.90       0.55       3.71       0.66       0.12       1.11       1.50       0.51       3.67       1.01       0.02       0.18       0.00       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13       0.06       0.13 <td></td> <td>0.04</td> <td>1 50</td> <td></td> <td></td> <td></td> <td>0.14</td> <td>0.00</td> <td>0 17</td>																						0.04	1 50				0.14	0.00	0 17
AE=88-70       0.7       3       91       13       171       12       6       0.5       24       14       833       <2       46       91       156       <5       0.4       6       105       0.4       10       0.13       0.13       0.02       0.18       0.02       0.18       0.02       0.19       0.13       0.10       0.02       0.16       0.17       0.06       0.12       1.60       0.51       3.67       1.01       0.03       0.06       0.12       1.60       0.51       3.67       1.01       0.36       0.06       0.12       1.60       0.51       3.67       1.01       0.36       0.06       0.12       1.60       0.50       3.49       0.89       0.31       0.06       0.12       1.60       0.50       3.49       0.89       0.31       0.06       0.12       1.60       0.50       3.49       0.89       0.31       0.06       0.12       1.60       0.50       3.49       0.89       0.31       0.06       0.12       1.60       0.50       3.49       0.89       0.31       0.06       0.12       1.60       0.50       1.10       0.17       0.11       0.31       0.57       0.57       0.57       0.50 <td>AE-88-67</td> <td></td> <td>.8</td> <td>3</td> <td>99</td> <td></td> <td>177</td> <td>21</td> <td>7</td> <td>0.7</td> <td>46</td> <td>16</td> <td>855</td> <td>&lt;2</td> <td>47</td> <td><u> </u></td> <td>148</td> <td></td> <td>0.0</td> <td>11</td> <td>90</td> <td>0.04</td> <td>1.00</td> <td>2.20</td> <td>4, 13</td> <td></td> <td>0.14</td> <td>0.02</td> <td>0.17</td>	AE-88-67		.8	3	99		177	21	7	0.7	46	16	855	<2	47	<u> </u>	148		0.0	11	90	0.04	1.00	2.20	4, 13		0.14	0.02	0.17
AE-88-72       0.4       <1       81       11       90       5       <5       0.1       24       20       619 $<<       58       57       146       14       0.3       6       41       0.12       1.69       0.35       0.4       0.4       0.4       0.4       0.10       0.2       c5       <51       0.1       26       <50       0.1       23       17       548       <2       54       79       117       7       0.3       6       37       0.12       1.50       0.55       3.49       0.59       0.31       0.06       0.12         AE-88-74       0.2       5       69       6       65       <0.1       25       16       518       <2       65       87       110       8       0.3       7       41       0.13       1.57       0.57       3.79       0.90       0.31       0.06       0.1         AE-88-77       0.1       3       23       <5       <5       <0.1       13       7       256       266       857       70       0.2       12       38       0.09       0.75       0.54       3.54       0.14       0.05       0.14       0.02       0.22 $	AE-88-70	0	.7	3	91	13	171	12	6	0.5	42	14	833	<2	46	91	156	<5	0.4	6	105	0.04	1.61	2.41	4.24	1.51	0.13	0.02	0,18
AE=88-73       0.3       3       84       10       102	AE-88-72		.4	<1	81	11	90	5	<5	<0.1	24	20	619	<2	58	97	148	14	0.3	6	41	0.12	1.69	0.56	4.14	0.99	0.37	0.06	0,12
AE=88-74       0.2       4       72       7       84       6       <5       <0.1       23       17       548       <2       54       79       117       7       0.3       6       37       0.12       1.56       0.50       3.49       0.39       0.31       0.00       0.12         AE=88-75       0.1       3       23       <5       <5.5       <0.1       125       16       518       <2       65       87       110       8       0.33       7       41       0.13       1.57       0.57       3.79       0.90       0.31       0.06       0.13         AE=88-76       0.6       2       122       7       54       <5       <0.1       14       7       256       <2       66       88       7       0.2       12       37       0.90       0.75       0.57       3.19       0.47       0.17       0.06       0.13       0.47       0.18       0.06       0.14       0.72       0.57       3.19       0.47       0.17       0.50       0.13       0.47       0.17       0.51       0.10       0.51       0.10       0.51       0.11       0.22       1.22       1.22       1.23       1	AE-88-73	10	.3	3	84	10	102	<5	<5	<0.1		19	625	<2	58	85	129	8	0.3	6	39	0.13	1.80	0.51	3.67	1.01	0.36	0.06	0.12
AE-88-75       0.2       5       69       6       83       <5       <5       0.1       25       16       518       <2       65       87       110       8       0.3       7       41       0.13       1.57       0.57       3.79       0.90       0.31       0.00       0.13         AE-88-76       0.1       3       22       37       <5       <5       <5       <0.1       14       7       256       <2       59       88       88       7       0.2       12       38       0.09       0.75       0.54       3.54       0.47       0.18       0.05       0.14         AE-88-77       0.6       2       112       7       24       0.1       22       22       1291       <2       36       89       73       <0.2       12       37       0.09       0.75       0.47       0.18       0.02       2.99       1.32       6.32       1.48       0.02       2.29       1.32       6.32       1.68       0.22       2.46       1.44       6.51       1.07       0.57       0.79       0.90       0.71       0.50       0.02       2.29       1.32       6.32       1.57       0.76       0.22<	AE-88-74	0	.2	4	72	7	84	6	<5	<0.1	23	17	548	<2	54	79	117	7	0.3	6	37	0.12	1.56	0.50	3.49	0.69	0.31	0.05	0, 12
AE-88-75       0.2       5       69       6       83       <5       <5       10       25       10       8       0.3       7       41       0.13       1.3       0.37       0.04       0.37       0.04       0.37       0.04       0.37       0.04       0.37       0.04       0.37       0.04       0.13       0.37       0.22       15       65       57       0.1       13       7       254       <2       59       88       88       7       0.2       12       38       0.09       0.75       0.54       3.54       0.47       0.18       0.05       0.14         AE=88-77       0.6       2       112       7       124       33       10       <0.1       22       22       1291       <2       36       893       74       <5       0.2       2.3       1.34       6.51       1.91       0.05       0.13         AR=88-67       0.6       2       112       7       124       33       10       <0.1       223       23       1325       4       36       93       74       <5       0.2       23       1.34       6.51       1.91       0.05       0.11       0.02       0.		1						_												_				0.57					0.40
AE=88-76       0.1       3       23       c1       35       c5       c5       c0.1       13       7       254       c2       59       88       88       7       0.2       12       38       0.09       0.72       0.57       3.61       0.47       0.18       0.05       0.14         AE=88-77       0.6       2       112       7       124       33       10       -0.1       22       22       22       37       0.09       0.75       0.56       0.54       3.54       0.47       0.18       0.05       0.13         AR=88-67*       0.6       4       107       9       129       34       c5       c0.1       23       23       1325       4       36       93       74       c5       0.2       3       49       0.02       2.39       1.34       6.51       1.91       0.15       0.02       0.17         AR-88-72       0.5       1       107       11       140       28       c5       1271       6       42       117       80       c5       0.7       13       50       0.02       2.46       1.14       6.30       1.86       0.14       0.02       0.17	AE88-75		.2	5	69	6	83	<5	<5	<0.1	25	16	518	<2	65	87	110	8	0.3		<b>1</b>	0.13	1.5/	0.5/	3.79	0.80	0.31	0.06	0.13
AE-68-77 $<0.1$ 3       24       2       37 $<5$ $<5$ $<0.1$ $14$ 7 $258$ $<2$ $66$ $82$ $66$ $62$ $12$ $37$ $0.5$ $0.6$ $2$ $112$ $7$ $124$ $33$ $10$ $0.1$ $22$ $22$ $1291$ $<2$ $36$ $893$ $73$ $<5$ $0.2$ $23$ $1.32$ $6.32$ $183$ $0.14$ $0.02$ $0.75$ $0.54$ $3.54$ $6.47$ $0.07$ $0.09$ $0.75$ $0.54$ $3.54$ $6.47$ $0.02$ $0.29$ $1.32$ $6.32$ $185$ $0.14$ $0.02$ $0.17$ AR-88-67* $0.5$ 1 $107$ $11$ $40$ $28$ $<5$ $0.1$ $23$ $23$ $1325$ $4$ $36$ $93$ $74$ $<5$ $0.2$ $3$ $49$ $0.02$ $2.39$ $1.34$ $6.51$ $1.91$ $0.16$ $0.17$ $0.65$ $0.7$ $13$ $60$ $0.22$ $2.39$ $1.34$ $6.51$ <	AE8876	0	1	3	23	<b>≪</b> 1	35	<5	<5	<0.1	13	7	254	2	59	88	88	7	0.2	12	38	0.09	0.72	0.57	3.81	0.47	0.18	0.05	0.14
AR-68-67 AR-88-67*       0.6       2       112       7       124       33       10       <0.1       22       22       129       34       <5       0.2       2       48       0.02       2.29       1.32       6.32       1.83       0.14       0.02       0.17         AR-88-67*       0.6       4       107       9       129       34       <5       <0.1       23       23       1325       4       36       93       74       <5       0.2       3       49       0.02       2.39       1.34       6.51       1.91       0.15       0.02       0.17         AR-88-72       0.5       1       107       11       140       28       <5	AE-88-77		0.1	3	24	2	37	<5	<5	<0.1	14	7	258	<2	66	82	86	<5	0.2	12	37	0.09	0.75	0.54	3.54	0.47	0.17	0.05	0.13
AR-88-67*       0.6       4       107       9       129       34       <5 $<0.1$ 23       23       1325       4       36       93       74       <5       0.2       3       49       0.02       2.39       1.34       6.51       1.91       0.15       0.02       0.11         AR-88-75       1.5       1       107       11       140       28       <5	AR-88-67	0	.6	2	112	7	124	33	10	<0.1	22	22	1291	2	36	89	73	<5	0.2	2	48	0.02	2.29	1.32	6.32	1.83	0.14	0.02	0,17
AR-88-72       0.5       1       107       11       140       28       <5       <0.1       28       25       1271       6       42       117       80       <5       0.7       13       50       0.02       2.48       1.14       6.30       1.95       0.14       0.02       0.18         AR-88-75       1.5       <1       844       4       135       21       <5       <0.1       24       19       1200       6       38       102       85       <5       0.3       6       48       0.02       2.27       1.18       5.88       1.78       0.14       0.02       0.16         AR-88-76       1.2       <1       93       6       133       26       <5       <0.1       25       22       1186       7       37       96       113       <5       0.4       7       48       0.02       2.29       1.06       6.17       1.70       0.14       0.01       0.17         AR-88-77       0.4       3       89       6       129       21       <5       21       151       14       114       4       73       66       174       <5       0.7       12       0.7	AR8867*		.6	4	107	9	129	- 34	<5	<0, 1	23	23	1325	4	36	93	74	<5	0.2	3	49	0.02	2.39	1.34	6.51	1.91	0,15	0.02	0.17
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																		1											
AR-88-75       1.5       <1       84       4       135       21       <5       <0.1       24       19       1200       6       38       102       85       <5       0.3       6       48       0.02       2.27       1.18       5.88       1.78       0.14       0.01       0.16         AR-88-76       1.2       <1       93       6       133       26       <5       <0.1       26       21       1120       8       37       93       99       <5       0.4       7       38       0.02       2.27       1.18       5.88       1.63       0.13       0.02       0.17         AR-88-77       0.4       3       89       6       129       21       <5       <0.1       25       22       1186       7       37       96       113       <5       0.4       7       48       0.02       2.29       1.06       6.17       1.70       0.14       0.01       0.17         DL-88-176       1.0       4       55       7       499       58       <5       2.1       51       1357       5       59       58       163       <5       0.7       11       19       0.05	AR-88-72	0	.5	1	107	<b>3</b> (1)	140	28	<5	<0.1	28	25	1271	6	42	117	80	<5	0.7	13	50	0.02	2.46	1.14	6.30	1.95	0.14	0.02	0, 18
AR-88-76       1.2       <1       93       6       133       26       <5       <0.1       26       21       1120       8       37       93       99       <5       0.4       7       38       0.02       2.21       0.71       6.08       1.63       0.13       0.02       0.17         AR-88-77       0.4       3       89       6       129       21       <5       <0.1       25       22       1186       7       37       96       113       <5       0.4       7       48       0.02       2.29       1.06       6.17       1.70       0.14       0.01       0.17         DL-88-176       1.0       4       55       7       499       58       <5       2.8       52       15       1357       5       59       58       163       <5       0.7       11       19       0.05       1.81       0.48       6.14       0.95       0.14       0.03       0.13       0.02       0.17         DL-88-176       1.0       4       55       7       499       58       <52       15       1357       5       59       58       163       <57       11       19       0.05	AR-88-75	1	.5	<1	84	4	135	21	<5	<0.1	24	19	1200	6	38	102	85	<5	0.3	6	48	0.02	2.27	] 1.18	5.88	1.78	0.14	0.01	0.16
AR-88-77       0.4       3       89       6       129       21       c5       c0.1       25       22       1186       7       37       96       113       c5       0.4       7       48       0.02       2.29       1.06       6.17       1.70       0.14       0.01       0.17         DL-88-174       0.5       3       44       10       431       53       c5       2.1       51       14       1141       4       73       68       174       c5       0.7       12       21       0.07       2.07       0.54       5.86       113       0.17       0.04       0.12         DL-88-176       1.0       4       55       7       499       58       c5       2.8       52       15       1357       5       59       58       163       c5       0.7       11       19       0.05       1.81       0.48       6.14       0.95       0.14       0.03       0.13         DL-88-176       0.8       5       56       6       417       70       c5       1.8       55       15       1455       6       55       64       180       c5       0.7       10       20	AR-88-76	1	.2	<1	93	6	133	26	<5	<0.1	26	21	1120	8	37	93	99	<5	0.4	7	38	0.02	2.21	0.71	6.08	1.63	0.13	0.02	0, 17
DL-88-174       0.5       3       44       10       431       53       <5       2.1       51       14       1141       4       73       68       174       <5       0.7       12       21       0.07       2.07       0.54       5.86       1.13       0.17       0.04       0.12         DL-88-176       1.0       4       55       7       499       58       <5       2.8       52       15       1357       5       59       58       163       <5       0.7       11       19       0.05       1.81       0.48       6.14       0.95       0.14       0.03       0.13         DL-88-176       0.8       5       56       6       417       70       <5       1.8       55       15       1455       6       55       64       180       <5       0.7       10       20       0.07       2.02       0.55       6.35       14       0.03       0.13         DL-88-190       0.2       3       25       3       224       31       <5       1.1       43       11       1491       5       52       48       139       0.7       13       19       0.04       1.67	A9-88-77		4	3	89	6	129	21	<5	<0.1	25	22	1186	7	37	96	113	<5	0.4	7	48	0.02	2.29	1.06	6.17	1.70	0.14	0.01	0, 17
DL-88-176       1.0       4       55       7       499       58       <5       2.8       52       15       1357       5       59       58       163       <5       0.7       11       19       0.05       1.81       0.48       6.14       0.95       0.14       0.03       0.13         DL-88-178       0.8       5       56       6       417       70       <5       1.8       55       6       55       64       180       <5       0.7       11       19       0.05       1.81       0.48       6.14       0.95       0.14       0.03       0.13         DL-88-190       0.2       3       25       3       224       31       <5       1.1       43       11       1491       5       52       48       139       <5       0.7       13       19       0.04       1.67       0.33       4.72       0.87       0.14       0.03       0.13         DL-88-194       <0.1       <1       23       5       0.6       41       13       1255       5       60       65       111       <5       0.7       11       21       0.08       1.96       0.49       4.79       1.42<	DI -88-174	Ì	5	3	44	10	431	53	<5	2.1	51	14	1141	4	73	68	174	<5	0.7	12	21	0.07	2.07	0.54	5.86	1.13	0.17	0.04	0.12
DL-88-176       1.0       4       55       7       499       58       <5       2.8       52       15       1357       5       59       58       163       <5       0.7       11       19       0.05       1.81       0.48       6.14       0.95       0.14       0.03       0.13         DL-88-178       0.8       5       56       6       417       70       <5       1.8       55       64       180       <5       0.7       10       20       0.07       2.02       0.55       6.35       1.40       0.12       0.03       0.13         DL-88-190       0.2       3       25       3       224       31       <5       1.1       43       11       1491       5       52       48       139       <5       0.7       13       19       0.04       1.67       0.33       4.72       0.87       0.14       0.03       0.10         DL-88-194       <0.1       <1       23       5       217       36       <5       0.6       42       13       1255       5       60       65       111       <5       0.7       11       21       0.09      1.97       0.49       4.81 </td <td></td> <td>_   `</td> <td>·~  </td> <td>1</td> <td></td> <td></td> <td></td> <td>· ·-</td> <td></td>		_   `	·~	1				· ·-																					
DL-88-178         0.8         5         56         8         417         70         <5         1.8         55         15         1455         6         55         64         180         <5         0.7         10         20         0.07         2.02         0.55         6.35         1.40         0.12         0.03         0.13           DL-88-190         0.2         3         25         3         224         31         <5	01-88-176		.01	4	55	7	499	58	<5	2,8	52	15	1357	5	59	58	163	<5	0.7	11	19	0.05	1.81	0.48	6.14	0.95	0.14	0.03	0, 13
DL-88-190         0.2         3         25         3         224         31         <5         1.1         43         11         1491         5         52         48         139         <5         0.7         13         19         0.04         1.67         0.33         4.72         0.87         0.14         0.03         0.10           DL-88-194         <0.1	01-88+178		A	5	56	R	417	70	<5	1.8	55	15	1455	6	55	64	180	<5	0.7	10	20	0.07	2.02	0.55	6.35	1.10	0, 12	0.03	0.13
DL-88-194         <0.1         <1         23         5         217         36         <5         0.6         41         13         1255         5         60         65         111         <5         0.7         11         21         0.08         1.96         0.49         4.79         1.42         0.13         0.05         0.10           DL-88-194*         <0.1	01-88-190		2	3	25		224	31	<5	1.1	43	11	1491	5	52	48	139	<5	0.7	13	19	0.04	1.67	0.33	4.72	0.87	0.14	0.03	0,10
DL-88-194* <0.1 1 23 3 217 33 <5 0.6 42 13 1255 6 60 65 111 <5 0.7 11 21 0.09 1.97 0.49 4.81 1.13 0.13 0.05 0.09	DI -88 - 194		1	-1	23		217	36	<5	0.6	41	13	1255	5	60	65	111	<5	0.7	11	21	0.08	1.96	0.49	4.79	1.12	0.13	0.05	0, 10
	01 -88 - 104*		0.1	1	23		217	33	6	0.6	40	13	1255	6	60	65	111	<5	0.7	11	21	0.09	1.97	0.49	4.81	1.13	0.13	0.05	0.09
	00-104		· · ·	1				~~		0.0				-										1					

#### PLACER DOME RESEARCH CENTRE Geochemical Analysis

Geol:

	K TROCIUK	Date Received:	JULY 22, 1992	Page	2	of
ect No.:	D2445	Date Completed:	AUG 11, 1992	Attn:	K TROC	IUK
ND TO SH	KOFFMAN				S HOFF	MAN

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Area: Remarks:

Project/Venture:

Lab Proj PULP SAMPLES FROM LORING LABS. RESULTS TO K TROCIUK AND TO S HOFFMAN

Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB)

COREY

1P

ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are rarely dissolved completely with this acid dissolution method.

bc         pen	SAMPLE		Ag	Mo	Cu	РЬ	Zn	As	SD	Cđ	S.M.S	ço	Mn	191	Or I		Da	**	De		્ય	<b>.</b>	~		~ ~ ~	Mi H	â	~	۳ مر
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	No.		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	_ppm	ppm	ppm	_ppm	ppm	- 76	76	70	70		20	-70-1	70
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	DL-88-195		0.1	3	39	12	226	41	<5	0.9	46	17	1144	7	63	73	115	<5	1.1	18	24	0.08	2.05	0.49	4,00	1.10	0.12	0.04	0.09
µr=0-16         10         4         73         6         477         3         76         21         777         3         100         65         230         68         10         230         68         100         230         68         100         230         68         100         230         68         100         230         68         100         230         68         100         230         68         100         230         68         100         68         220         100         210         230         68         68         230         68         68         230         68         68         230         68         68         230         68         68         230         68         68         230         68	DL-88-196		0.1	<1	28	7	210	34	<5	0.4	42	13	1043	2	58	66	95	<0	0.6	8	21	0.09	1.97	0.50	4.70	1.10	0.13	0.05	0.09
jr=88-19         0.5         <1         0.2         9         214         0.2         0.7         72         77	JP-68-18		1.0	4	73	8	417	40	<5	2.3	76	21	1747	3	110	87	240	<5	0.4	8	20	0.10	2.39	0.57	6.30	1.87	0.13	0.02	0.12
µr=0-20         0.8         1         71         9         369         43         5         2.1         77         21         776         24         716         24         100         12         238         0.85         1.0         1.0         1.0         1.0         1.0         1.0         0.00	JP-88-19	1	0.5	<1	62	9	214	92	<5	0.7	72	17	1734	4	107	64	234	<5	0.5	12	13	0.08	2.16	0.41	4.64	1.66	0.10	0.03	0.07
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP88-20	1	0.8	1	71	Ð	389	43	5	2.1	77	21	1736	2	111	69	252	<5	0.5	10	22	0.11	2.36	0.55	6.05	1.87	0. 12	0.02	0.11
jr-ad-22         10         1         71         15         400         48         6         6         175         20         756         6         96         20         55         10         22         0.0         2.3         0.01         0.21         0.00			1		1											886.X													
Important         Important <t< td=""><td>10-98-22</td><td></td><td>1.0</td><td>1 1</td><td>71</td><td>13</td><td>400</td><td>48</td><td>6</td><td>2.1</td><td>75</td><td>20</td><td>1756</td><td>6</td><td>108</td><td>89</td><td>220</td><td>&lt;5</td><td>0.5</td><td>10</td><td>22</td><td>0.10</td><td>2.38</td><td>0.61</td><td>6.21</td><td>1.86</td><td>0.13</td><td>0.02</td><td>0.12</td></t<>	10-98-22		1.0	1 1	71	13	400	48	6	2.1	75	20	1756	6	108	89	220	<5	0.5	10	22	0.10	2.38	0.61	6.21	1.86	0.13	0.02	0.12
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	IP-98-23		12	-1	77		343	38	6	1.7	143	29	1752	2	215	94	183	<5	0.5	9	21	0.13	2.84	0.60	6.22	2.71	0.10	0.03	0.10
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	ID-00-23		10		67	Ā	376	40	<5	2.1	82	21	1677	3	1 19	89	203	<5	0.4	9	18	0.11	2.45	0.59	6.16	1.96	0.13	0.02	0.12
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	JF-00-24		0.0		65	Ā	362	38	<5	17	81	20	1595	0	120	91	204	<5	0.5	9	18	0.12	2.48	0.61	6.24	2.05	0.12	0.02	0.11
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP~00-25		0.8			888 - Y	2002	44	-5	10	8	21	1625	2	121	94	209	<5	0.5	9	18	0.12	2.57	0.63	6.39	2.12	0.13	0.02	0.12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP-88-25*	ł	0.9	ין	00		309	44		1.0		- '	IUZU				200					0.12			••••		••••=		
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $									-	2.1		20	1727		118	01	150	<5	0.5	10	21	0.09	2.43	0.54	6.01	2.04	0.11	0.02	0.12
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP-88-26		0.9		15	<u> </u>	.307		40	2.1	<u> </u>	22	1747	S V	424	05	203	-5	0.5	10	50	0 11	2 59	0.56	6.40	2 20	0.12	0.02	0.12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP-88-28		0.9	6	/8	CI CI	3/2	49	<5	2.0	<u> </u>	24	004	~		20	200	~5	0.5	10	25	0.00	0.66	0.51	2.82	0.55	0.16	0.04	0.12
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP8829		<0.1	3	19	ಿಂದ	46	5	<5	<0.1	00 <b>6</b> 6		204	~	0.5				0.4	10		0.00	0.00	0.57	5.81		0.10	0.02	0.10
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP8830		0.7	7	77	12	333	53	<5	1.6	(6	19	1638	6	110	60	231	<0	0.5	17	2ª	0.10	2.04	0.57	0.64		0.17	0.00	0.10
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP88-31		<0.1	5	23	6	45	6	<5	<0.1	23	9	277	~2	73	28	100	<5	0.4	17	30	0.10	0.72	0.50	£.00		Ų. 17	0.04	0.11
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $		1		1	1 1													-		45			0.74	0.55			0.40	0.04	A 11
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP8835		<0.1	2	25	3	40	<5	<5	<0.1	- 22	8	270	<2	72	80	90	<5	0.2	15		0.10	0.71	0.55	3.02	0.21	0.10	0.04	0.11
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP		< 0.1	9	25	3	43	<5	<5	<0.1	24	8	274	<2	75	91	98	<5	0.2	1/	<b>40</b>	0,10	0.73	0.00	3.80	<b>1.</b>	0.10	0.04	0, 13
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP88-40	1	< 0.1	5	22		39	<5	<5	<0.1	21	7	250	<2	64	69	92	<5	0.2	13	36	0.10	0.70	0.54	3.02	0.51	0.17	0.04	0.11
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP68-42	1	<0.1	6	22	4	41	<5	<5	<0.1	23	8	264	2	70	47	113	<5	0.2	12	39	0.10	0.78	0.52	2.25	0.61	0.19	0.04	0.11
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	STD-P1		0.2	64	27	50	144	20	<5	0.2	37	7	578	<2	122	38	182	<5	0.5	9	90	0.12	1, 12	0.98	2, 19	0.86	0.38	0.07	0.09
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				1					ļ																				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP88-44	1	0.1	3	37	6	48	9	5	0.2	27	12	282	2	67	79	103	6	0.7	23	44	0.09	0.74	0.55	3.13	0.56	0.17	0.04	0.13
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP-88-60		0.1	<1	11	×<1	37	<5	<5	<0.1	18	5	209	2	53	73	67	7	0.2	14	50	0.10	0.75	0.63	3.00	0.43	0.12	0.04	0. 14
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	JP-88-61		0.2	2	19	5	35	<5	<5	<0.1	29	7	212	2	64	48	66	<5	0.3	11	56	0.08	0.97	0.68	2.05	0.53	0.11	0.06	0.10
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	IP-88-62		0.2	5	24	3	41	<5	<5	<0.1	43	9	251	3	68	77	60	5	0.3	12	49	0.09	1.09	0.79	3.10	0.71	0.12	0.07	0.11
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	ID. 00 - 63		-01	1 -1	3		25	<5	<5	<0.1	8	4	155	2	47	41	62	<5	0.4	12	82	0.08	0.69	0.67	1.72	0.33	0.09	0.03	0.10
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JF -00 -05		~~	`'	۲ I			~~	-																				
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	1D		-01	-1	2		30	<5	<5	<0.1	10	5	198	2	50	80	59	<5	0.3	18	79	0.11	0.71	0.88	3.29	0.37	0.09	0.04	0.17
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JF-00-04	]	201			5	26	-5	-5	-01		4	171	0	60	61	62	<5	0.3	15	80	0.10	0.67	0.78	2.55	0.32	0. 10	0.05	0.13
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP-68-65	1	<0.1				20	~5		-0.1			176		AI	50	66	<5	0.3	14	<b>B4</b>	0.10	0.71	0.80	2.50	0.33	0.10	0.05	0.13
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	JP-88-00		<0.1				50	-5		-0.1		17	384		56	103	177	<5	0.8	3	1 18	0.15	1.54	7.95	4.59	128	0.30	0.03	0.11
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP88-69		<0.1		~~		52	5				16	403		55	108	177	<5	0.0	4	123	0.15	1.59	7.95	4.63	132	0.31	0.03	0.11
JP-88-70	JP		<0.1	2	• •		- 24	<5		<0.1			400		~			~	0.0			0.10							•••••
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $									-				477	ار			220		44	11	110	0 14	192	4.85	4 45		0.34	0.04	0.12
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP8870	1	<0.1	3	65	5	70	<3	5	<0.1		20	4//	• •		<u> </u>	247	ہ ا	놂		1.10	0.14	1.02	4 03	3 72	4 477	0.34	0.05	0 12
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP8873	J	<0.1	] 7	54	<1	68	<5	<5	<0.1	29	15	440	~	04		34/	 		3		0.14	1.01	7.50	4.04	1 20	0.04	0.00	0.15
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP~88-78		<0.1	1	53	5	74	<5	<5	<0.1	32	15	431	2	/2		309	<0	0.5	4	92	0.12	1.00	1.05	4.04		0.20	0.00	0.13
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP8864	ł	<0.1	2	53	15	129	20	7	<0.1	22	13	$\overline{m}$	4	48	- BU	147	<0	0.5	ษ	00	0.03	1.76	1.00	4.20		0.10	0.02	0.13
JP-88-86       0.1       7       48       14       115       17       <5       <0.1       20       13       697       <2       45       54       146       <5       0.3       6       47       0.03       1.72       0.94       4.24       1.23       0.15       0.02       0.13         JP-88-87       0.1       2       46       17       125       16       <5	JP8885	l I	<0.1	3	53	15	128	20	্ ব	<0.1	21	14	758	4	49	60	153	<5	0.5	9	63	0.03	1.79	1.30	4.27	1.20	0.17	0.02	0.13
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	•		4											1				_											
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	JP8886	1	0.1	7	48	14	115	17	<5	<0.1	20	13	697	2	45	54	146	<5	0.3	6	47	0.03	1.72	0.94	4.24	1.23	0.15	0.02	0.13
JP-88-95       <0.1       3       21       6       148       <5       <5       <0.1       14       9       729       <2       34       46       115       <5       0.5       9       26       0.09       1.67       0.48       4.35       1.05       0.13       0.03       0.13         JP-88-97       <0.1       <1       27       10       126       8       <5       <0.1       32       11       784       <2       52       51       89       <5       0.7       9       20       0.06       1.79       0.34       4.20       1.06       0.13       0.04       0.10         JP-88-97*       <0.1	JP-88-87		0.1	2	48	17	125	16	<5	<0.1	19	11	720	<2	45	55	154	<5	0.3	6	62	0.03	1.73	1.31	4, 19	1:24	0, 16	0.02	0, 13
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	JP8895		<0.1	3	21	6	148	<5	<5	<0.1	14	9	729	2	34	46	115	<5	0.5	9	26	0.09	1.67	0.48	4.35	1.05	0.13	0.03	0.13
JP-88-97* <0.1 2 28 9 125 8 <5 <5 <5 52 89 <5 0.7 10 21 0.06 1.77 0.34 4.18 1.05 0.13 0.04 0.10	JP8897	1	<0.1	<1	27	10	126	8	<5	<0.1	32	11	784	2	52	51	89	<5	0.7	9	20	0.06	1.79	0.34	4.20	1.06	0.13	0.04 [	0, 10
	IP-88-97*		<0.1	2	28	9	125	8	<5	<0.1	33	11	783	2	52	52	89	<5	0.7	10	21	0.06	1.77	0.34	4, 18	1.05	0.13	0.04	0.10
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J KOWALCHUK

K At- 1

E KIMURA

Geochemical Analysis

COREY	Geol:	K TROCIUK	Date Received:	JULY 22, 1992	Page	3	of	5
1P	Lab Project No.:	D2445	Date Completed:	AUG 11, 1992	Attn:	K TROC	JUK	
PULP SAMPLES FROM LORING LABS. RESULTS TO K 1		S HOFI	MAN					
ligested with Agua Regia and determined by Graphite Furr	BCOA.A (D.L. 1 PPB)	)				J KOW	ALCHUK	
licested with 4 ml Agus Regis at 100 Deg. C for 2 hours.	•					E KIMU	RA	

Project/Venture:

Area:

Remarks:

Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB) ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are rarely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	y.	Ba	w	Be	لما	ଃ		A	Ca	Fe	Mg	K	Na	P
No.		ppm	ppm	ppm	ppm	ppm	ppm	ррт	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<u>%</u>	%	%	%	*	%	<u>%</u>	<u>%</u>
JP8898		0.2	2	29	23	125	5	<5	<0.1	33	11	818	- 4	51	53	82	<5	0.7	11	19	0.05	1.87	0.32	4.42	1.13	0.12	0.03	0.10
JP-88-99		0.3	4	30	9	135	6	ব	<0.1	24	9	792	2	45	56	100	<5	0.5	11	29	0.06	1.82	0.42	4,00	1.07	0.12	0.03	0.12
JP~-88-100		0.2	5	34	9	137	- 11	<5	0.1	26	11	807	<2	44	58	97	<5	0.6	14	28	0.06	1./8	0.40	4.63	1.00	0.11	0.03	0.12
JP-88-101		0.2	4	24	12	140	6	<5	<0.1	16	11	807	<2	36	56	1 16	<5	0.7	16		0,10	1.85	0.48	5.09	3. 18	0,12	0.03	0.14
JP-88-102		0.2	4	25		121	<5	<5	<0.1	88 ST	10	768	<2	- 33	54	110	<5	0.5	12	35	0.09	1.77	0.48	4.71	1.10	0.10	0.03	0.13
JP-88-103		0.5	6	28	7	308	<5	<5	0.7	22	12	792	<2	35	60	118	<5	0.7	14	35	0.11	1.75	0.49	4.91	1.10	0.11	0.04	0.13
JP-88-104		0.3	3	18	4	120	<5	<5	<0.1	39	8	741	<2	54	51	100	<5	0.5	9	20	0.04	1.64	0.38	4.07	1.04	0. 10	0.02	0.11
JP-88-105		0.1	2	24	6	149	<5	<5	<0.1	52	9	1005	<2	64	56	112	<5	0.6	9	21	0.03	1.87	0.36	4.51	1.15	0.11	0.03	0.12
JP-88-106		0.2	3	29	13	168	<5	<5	<0,1	65	10	1000	2	73	65	126	<5	0.7	10	23	0.04	2.21	0.40	5.23	1.40	0.12	0.03	0.13
JP-88-106*		0.2	3	28	i i i i	166	<5	<5	<0.1	63	10	991	2	71	63	122	<5	0.6	10	23	0.03	2.14	0.39	5.05	1.36	0.12	0.03	0.13
							-										1 1				' î		i i			- 1	1	
IP-88-107		<0.1	<1	38	17	164	<5	<5	0.4	55	15	1142	- 4	66	69	131	<5	1.1	20	26	0.05	1.95	0.37	4.73	1.19	0. 13	0.03	0.11
JP-88-108		<0.1	<1	22	7	141	<5	<5	<0.1	43	10	939	~2	59	58	105	5	0.6	10	21	0.05	1.82	0.39	4.42	1.14	0, 12	0.03	0.12
IP-88-115		0.1	21	31	12	166	<5	<5	<0.1	21	10	866	<2	40	57	120	<5	0.5	12	36	0.10	1.93	0.51	5.14	1, 19	0.14	0.04	0.14
1D_00_117		0.1	2	33	A	192	<5	<5	0.2	23	10	948	<2	40	55	118	<5	0.5	12	35	0.08	1.95	0.48	5.17	1.20	0.14	0.04	0.13
JP-00-117		~0.1	5	35	01	182	-65	ব	0.2	24	12	883	2	40	61	117	<5	0.7	15	36	0.10	1.92	0.49	5.26	1.18	0.13	0.04	0.14
JF -00 - 118		<b></b>	- <b>-</b>	~		· · · ·			•				-	5														I
ID. 00 -124		<01	-1	28		172	<5	- 5	0.2	21	10	825	2	38	52	97	<5	0.6	14	27	0.07	1.79	0.43	4.77	1.10	0.12	0.02	0.13
10, 92 - 125		0 1		32	12	199	<5	<5	0.3	24	11	9 18	2	42	57	117	<5	0.6	13	34	0.09	1.96	0.48	5, 18	1.21	0, 14	0.04	0.14
JP 40 125		-01	-1	33	8 W G	197	<5	<5	0.3	25	12	931		40	60	119	<5	0.7	14	36	0.09	1.90	0.48	5.21	1.17	0.13	0.04	0.14
JP -00 = 120	Ì	<0.1		42		431	65	<5	0.7	77	8	583		32	77	61	<5	0.7	7	42	0.13	1.78	0.47	4.83	1.25	0.11	0.09	0.09
JP-00-100		~01	50	42	8	434	66	<5	0.8	78	8	588	-4	32	78	60	<5	0.7	7	42	0.14	1.80	0.47	4.91	1.27	0.11	0.09	0.09
ur -00 - 100		~ •				,	•-							Ë														I
TB_99_10		<01	<1 <1	32	6	80	<5	<5	<0.1	15	11	308	2	64	67	153	7	0,5	15	47	0.12	0.94	0.58	2.80	0.61	0.30	0.05	0.13
TR. 09 _ 12		0.2		37	27	215	13	<5	0.8	39	10	1100	2	49	47	122	<5	0.7	10	23	0.06	1.78	0.39	4.81	0.93	0.16	0.04	0.12
10-00-10 TR. 00-17		0.2	5	39		209	13	4	0.7	42	11	1129	5	51	48	125	<5	0.8	11	24	0.06	1.83	0.41	4.93	0.98	0.15	0.05	0,12
TD-00-1/		0.2	-1	35		188	10	-5	0.5	36	9	904	5	49	45	113	<5	0.7	11	21	0.05	1.72	0.36	4.61	0.91	0.15	0.04	0.11
TB_88_22		0.0	3	24	10	142	5	<5	0.1	34	8	652	2	53	46	96	<5	0.7	11	17	0.04	1.84	0.27	4.12	0.94	0.13	0.03	0.09
10-00-22		0.1	Ŭ				-				_		_															
TB_88_23		0.1	3	18	6	181	<5	<5	0.3	49	14	2072	3	59	60	121	<5	0.9	9	25	0.06	2,15	0.38	5. 18	1.15	0.11	0.06	0.10
TR-08-24		0.1	7	16	2	168	<5	<5	0.1	40	14	1927	3	58	55	127	ব্য	0.8	7	25	0.06	2.01	0.41	5.02	1.12	0.10	0.05	0.10
TD-00-24		0.2		14		174	<5	5	0.2	51	14	2142	2	57	60	151	<5	0.9	8	30	0.07	2.10	0.44	5.15	1.23	0.11	0.07	0.11
TR. 00-20		0.2	2	20		160	~5	-	0.1	58	16	1832	0	66	65	144	⊲5	0.9	11	27	0.05	2.25	0.43	5.39	1.34	0.12	0.04	0,13
etb_01		0.3	67	28	57	156	20	6	0.3	38	7	684	0	121	38	195	<5	0.7	8	95	0.12	1.13	1.00	2.34	0.97	0.41	0.07	0.09
310-61		0.0	°'	20				<b></b>		je 👫	'		-										1					
T0. 00. 07		0.1	4	50		130	16	اجه ا	<0.1		21	1362	0	40	89	113	<5	1.1	21	84	0.22	2.53	0.78	5.88	170	0.21	0.20	0.13
TR 00 00		0.1		20		106	40	ایتر	201		20	1362	2	34	87	107	5	0.8	15	97	0.27	2.56	0.89	5.85	181	0.22	0.27	0.13
10-00-20		0.1	1. 21	30		120			-	200	16	1256	2	90	77	98	- 5	0.8	14	76	0.21	2.41	0.76	5.78	1.62	0.20	0.19	0.12
10-00-29		0.1		37		100	ية: عدر		-0.1			854	2	38	79	86	6	0.7	11	25	0,10	1.85	0.43	5.17	112	0, 12	0.05	0.12
10-68-30		0.2		3/		207	~0				13	961	2		87	108	5	0.7	10	54	0.18	2.43	0.68	5.73	156	0.17	0.15	0.13
18-88-31		U.2	'	1 <sup>40</sup>		201	<0					~ '	~	~		.~~	- <b>-</b>											
		~ ~				007	Æ		-01	20	12	1080		45	87	119	5	0.8	13	37	0.13	2.48	0.57	6.50	1.49	0.17	0.06	0,15
16-88-32		0.2	3	*/		20/	<0 -			20	10	856		30	67	91	<5	0.0	10	27	0.09	1.86	0.43	5, 15	1.12	0.13	0.05	0.12
18-88-33		0.1	3	3/		109	5			5		0.14	N Y	200		60		0.0 A 0	10	ីទំ	0.10	1.89	0.45	5.22		0, 13	0.05	0.12
115-88-34		0.1	3	39	5	102	0				10	010		45	74	105		0.0	11	ail	0 10	2.06	0.48	5.56	123	0.16	0.06	0.13
18~88-35		0.1	6	39		601	<0			<b>3</b> 1		910	× ×		74	100		0.4	10	00	0 10	198	0.45	5.42	1 18	0.15	0.05	0.12
TB-88-35*		0.1	3	36		161	5		<0.1	*0	יי	000	~~	<b>~</b> 3		100	~	0.0		<b>. 7</b>	V. 10		0.70	0.72		~ •	~~~	0.12
						1			L				L.,	6	$\sim \sim $		<b>ل</b>		l	94000993					unicessite dis			

### PLACER DOME RESEARCH CENTRE Geochemical Analysis

Project/Venture: Area:	COREY 1P	Geol: Lab Project No.:	K TROCIUK D2445	Date Received: Date Completed:	JULY 22, 1992 AUG 11, 1992	Pa <i>ge</i> Attn:	4 K TROCI	of UK	5					
Remarks:	PULP SAMPLES FROM LORING LABS.		SHOFF	MAN .										
Au - 10.0 g sample	Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB)													

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ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Ba, Cr, La and W are rarely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Mo	Cu	Pb j	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	8¥.	Ba	l w j	Be	LA 🛞	ST		A	ua	re N	8 <b>3</b> 1	2	- nai	- <b>5</b>
No,		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррт	ppm	ррп	ppm	ppm	ppm	ppm	ppm	ppm r	ppm	<u>~~~</u>	- %	0.29	4 71	70	70	- 70-	-71
TB-8836		< 0.1	5	37	6	139	<5	<5	<0.1	27	10	751	2	38	64	86	<5	0.6	1		0.08	1.75	0.30	1.50	0.07	0.12	0.00	0.10
TB88-37		0.1	6	31	5	128	<5	<5	<0.1	24	9	718	<2	36	59	82	<	0.5		20	0.09	1.00	0.30	7.50		0.10	0.04	0.10
TB-88-38		0.1	<1	26	2	86	<5	<5	<0.1	15	9	757	2	28	57	112	<5	0.4	9 S		0.13	1.70	0.52		101	0.12	0.05	0.12
TB-88-39		<0.1	5	26	<1	90	<5	<5	<0.1	15	10	769	<2	30	55	113	<5	0.4	9	45	0.12	1.73	0.52	4.44	1.02	0.12	0.001	0.12
TB-88-40		<0.1	3	24	<1	94	<5	<5	<0.1	15	9	741	<2	28	50	124	<5	0.4	8	50	0.11	1.64	0.50	4, 10	1.00	0.12	0.05	0.11
																					1							
TB-88-41		0.2	3	19	7	123	13	<5	<0.1	24	9	889	2	- 38	53	84	<5	0.9	16	31	0.10	1.96	0,40	4,45	1.12	0,14	0.05	0.09
TB-88-51		0.2	3	22		103	16	<5	<0.1	25	8	663	~2	42	57	86	<5	0.6	13	27	0.08	1.88	0.36	4.20	1.07	0.13	0.05	0.08
TB-88-52		< 0.1	11	6	9	123	6	<5	<0.1	18	6	1292	<2	29	32	85	<5	0.6	10	24	0.04	1.59	0.31	4.39	u.a/	0.11	0.05	0.08
TB-88-53		<0.1	13	10	7	89	79	<5	<0.1	12	9	536	<2	26	68	68	<5	1.0	12	52	0.15	2.25	0.62	3.66	0.14	0.10	0.12	0.11
TR-88-53*		<0.1	13	11	9	92	80	<5	<0.1	14	10	540	2	28	72	72	<5	1.1	15 💮	56	0.15	2.28	0.66	3.69	0.84	0.10	0.13	0.11
							1																					
TB88-59		0.3	7	24	3	104	<5	<5	<0.1	27	19	1076	<2	37	88	90	<5	0.9	14	115	0.33	2.36	1.13	5.50	1.66	0.22	0.40	0.11
TB-88-60		1.0	10	76	13	466	8	<5	3.3	66	15	1107	<2	46	48	128	<5	0.4	11	58	0.06	1.40	1.30	3.99	1.04	0.14	0.02	0.10
TB-88-61		0.9	5	144	1	157	17	<5	<0.1	63	23	1139	2	93	1 16	70	<5	0.5	7	33	0.21	2.63	0.60	5.67	1.96	0.11	0.10	0.10
TB-88-63		1.3	, B	65	20	317	16	<5	2.4	57	14	8 18	2	45	43	93	<5	0.5	11	51	0.05	1.26	1.11	4.26	0,95	0.13	0.02	0.09
TB-88-64		12	10	83	21	431	17	6	2.9	64	17	1048	<2	47	50	123	<5	0.5	12 🖉	60	0.06	1.39	1.32	4.32	1.05	0.15	0.02	0.11
10-00-04	. 1													}	68-2 C		J J				1							
TB_88-65		1.1	7	71	10	371	13	<5	2.3	55	14	973	<2	51	49	138	<5	0.4	11	62	0.06	1.38	1.40	3.83	1.06	0.14	0.02	0.10
TB-88-67		1.0	8	71	12	350	8	<5	2.1	53	13	950	<2	49	48	129	<5	0.4	12 💮	62	0.06	1.40	1.39	4.04	1.07	0, 15	0.02	0.11
TR_88_68	i 1	1.5	7	92	17	534	11	6	3.5	71	18	1240	<2	43	50	136	<5	0.4	11 🛞	66	0.06	1.38	1.51	4,21	1.05	0,16	0.02	0.12
TB_88_60	ļ	0.8	3	88	17	609	10	7	4.3	80	19	1343	2	57	51	159	<5	0.4	10 🛞	63	0.06	- 1.44	1.44	4.08	1.08	0.17	0.02	0.11
TB-88-69*		0.8	8	87	17	596	9	<5	4.2	79	19	1329	<2	56	50	153	<5	0.4	10	62	0.06	1.42	1.41	4.03	1.07	0.17	0.02	0.11
1.0-00-00		0.0	•																		1	1						
18-88-70	1	0.7	6	76	19	270	17	5	1.6	45	14	740	2	55	49	129	<5	0.6	14	62	0.05	1.29	1.41	4.03	0.96	0,13	0.02	0.10
TB-88-71		1.0	5	61	13	236	9	<5	1.3	43	11	768	2	43	46	125	<5	0.4	8	57	0.06	1.29	1.30	3,74	0.99	0.13	0.02	0.10
TB-88-72		0.8	6	61	15	213	13	<5	1.2	42	11	686	2	54	48	132	<5	0.3	8	36	0.06	1.36	0.77	3.94	110.1	0,13	0.02	0.10
TB-88-73		1.0	7	81	17	496	18	7	3.5	69	18	1163	2	48	52	130	<5	0.5	13 🛞	60	0.06	1.38	1.31	3.99	1.01	0.14	0.02	0.11
TB-88-74		0.5	9	82	16	532	25	7	3.8	71	18	1206	2	48	51	132	<5	0.5	11	65	0.06	1.43	1.43	4.10	1.04	0.14	0.02	0.11
			_	1									í –	( {			1 1					[	[				[	
TB-88-75	[	0.4	5	66	19	258	15	4	1.5	47	12	806	<2	50	50	135	<5	0.4	11	64	0.06	1.41	1.42	4, 10	1.05	0,15	0.02	0.11
TR-88-76		0.6	9	77	17	403	15	<5	2.8	58	15	991	< 2	47	51	145	<5	0.4	10	61]	0.07	1.41	1.31	4.07	104	0.15	0.02	0.11
TB-88-77		0.6	12	80	19	604	17	8	4.2	77	19	1274	<2	46	46	112	<5	0.4	9	57	0.05	1.39	1.28	4.23	101	0,13	0.02	0.10
TB-88-78	1	0.8	8	73	14	446	15	<5	3.1	64	15	1081	⊲	44	48	132	<5	0.4	9	62	0.06	1.38	1.36	3.90	1.03	0,14	0.02	0.11
TB-88-78*		0.9	7	76	16	452	13	5	3.1	65	16	1115	2	45	49	132	<5	0.4	9	63	0.06	1.41	1.40	4.01	1.05	0.14	0.02	0.11
1													1															
TR-88-79		0.9	10	102	34	559	44	8	4.7	85	25	1157	2	49	56	87	<5	0.9	19	61	0.05	1.37	1.23	4,94	0.98	0.14	0.02	0.10
TR_88-80		0.7	6	77	17	473	15	<5	3.5	63	15	1086	2	45	48	138	<5	0.4	9	63	0.06	1.38	1.42	3.80	1.02	0,14	0.02	0.11
TB-88-81		0.9	7	91	15	695	15	<5	5.6	86	20	1422	2	41	51	151	<5	0.4	9 🖉	66	0.06	1.41	1.49	3,74	1.03	0,14	0.02	0.12
TD_88_03		0.7	9	107	60	511	150	<5	3.4	76	19	1930	4	107	81	259	<5	0.6	8	22	0.09	2.25	0.69	5.88	1.89	0.13	0.02	0.13
10-00-00		0.0	3	62	22	207	43	<5	0.8	55	19	1222	2	86	n	181	<5	0.6	9 🖉	42	0, 10 }	2,19	0.74	4.82	08.1	0, 14	0.03	0.12
10-00-01		v. •		l –									ł	1								1						
TD-08_64		<01	6	7	7	47	<5	<5	<0.1	11	6	298	3	63	43	130	<5	0.3	17 🕅	34	0.12	0.77	0.55	2, 16	0.58	0.22	0.05	0.13
10-00-04		201	3	1		28	<5	<5	<0.1	7	4	201	< 2	53	30	103	<5	0.1	10	26	0.09	0.58	0.43	1.58	0.43	0.18	0.04	0.10
TD_00_07	1 1	201	4			31	<5	<5	<0.1	8	4	223	2	64	34	115	<5	0.2	12 🕅	31	0.11	0.65	0.52	1.79	0.48	0.21	0.05	0.12
TD-00-07		201		1 7	a	42	<5	<5	<0.1	11	6	3 19	2	62	53	167	<5	0.2	14 🕅	34	0.12	0.85	0.56	2.64	0.64	0.24	0.04	0.12
00-00-12		0.3	85	2	50	135	19	<5	<0.1	33	5	536	< 2	114	31	170	<5	0.4	4	83	0.11	1.02	0.92	2.23	0.82	0.35	0.06	0.06
910-F1	t I	0.0	50	<sup>20</sup>		<b>~</b>			1		Ī															1		L
# Geochemical Analysis

Project/Venture:	COREY	Geol :	K TROCIUK	Date Received:	JULY 22, 1992	Page	5	of	
Area:	1P	Lab Project No.:	D2445	Date Completed:	AUG 11, 1992	Attn:	K TROC	IUK	
Remarks:	PULP SAMPLES FROM LORING I	ABS. RESULTS TO K TROCIUK AND TO S H	DEFMAN	-			S HOFF	MAN	
Au — 10.0 g sample	e digested with Aqua Regia and deter	mined by Gaphite Furnace A.A. (D.L. 1 PPB)					J KOW/	LCHUK	
ICP - 0.5 g sample	digested with 4 ml Aqua Regia at 10	0 Deg. C for 2 hours.					E KIMU	RA	
N.B. The major oxid	ie elements, Ba, Be, Cr, La and War	a rarely dissolved completely with this acid dis	solution method						

SAMPLE		Ag	Мо	Cu	Pb	Zn	As	Sb	Cd	Ní	Co	Mn	Bi	Cr	SV 🛛	Ba	W	Be	La	Sr	Ti	AI	Ca	Fe	Mg	K	Na	P
No.		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррт	ррт	ppm	ppm	ррт	ppm	%	%	%	%	5	%	%	<b>%</b>
TD-88 -73		0.2	<1	8	4	49	<5	<5	<0.1	12	7	359	2	64	51	170	<5	0.4	18	35	0.12	0.86	0.51	2.52	0.65	0.25	0.04	0.11
TD-8876		0.3	1	7	6	52	<5	<5	<0.1	12	7	368	2	53	49	159	<5	0.4	16	34	0.12	0.86	0.51	2.57	0.67	0.27	0.04	0.12
TD-88 ~78		<0.1	6	5	2	45	<5	<5	<0.1	<b>***1</b> 1	7	327	2	63	57	154	<5	0.4	17	34	0.11	0.77	0.45	2.80	0.59	0.25	0.04	0.11
TD8879	1 1	<0.1	<1	6	3	51	<5	<5	<0.1	12	8	356	2	57	51	165	<5	0.3	17	31	0.11	0.86	0.46	2.66	0.66	0.26	0.04	0.12
TD-88 ~82	1	<0.1	<1	2	3	42	<5	<5	<0,1	9	5	3 19	2	61	45	148	<5	0.2	15	27	0.11	0.77	0.41	2.46	0.56	0.28	0.04	0.11
TD8883		<0.1	<1	3	<1	37	<5	<5	<0.1	31	5	266	2	61	78	103	<5	0.2	18	29	0. 10	0.63	0.59	3.62	0.49	0. 18	0.04	0,16
TD-88 ~84		0.1	<1	1	<1	34	<5	<5	<0.1	i t	- 4	239	2	49	25	1 18	<5	0.2	10	24	0.08	0.63	0.35	1.54	0.48	0.20	0.04	0.08
TM-88~2		<0.1	<1	2	<1	37	<5	<5	<0.1	8	- 4	209	2	57	34	128	<5	0.2	8	34	0.09	0.67	0.33	1.74	0.43	0.21	0.04	0.08
TM-88~3		<0.1	<1	4	<1	40	<5	<5	<0.1	15	5	240	2	71	125	85	<5	0.2	22	32	0.11	0.57	0.71	5.07	0.38	0, 16	0.04	0.21
STD-P1		0.2	61	27	52	155	20	<5	0.1	35	6	590	~	114	35	178	<5	0.4	7	83	0.11	1.05	0.89	2.30	0.87	0.38	0.06	0.08
TM-88~5		<0.1	<1	16	5	42	<5	<5	<0.1	17	9	250	2	74	109	98	6	0.6	24	36	0.11	0.61	0.52	4, 19	0.38	0, 16	0.04	0, 13
TM88~-6		<0.1	<1	4 💥	2	33	<5	<5	<0.1	9	4	198	2	61	55	96	10	0.2	14 🛛	28	0.10	0.58	0.41	2.41	0.38	0.16	0.04	0, 10
TM-88~7		<0.1	1	6	6	43	<5	<5	<0.1	41	6	250	Q	73	52	1 18	10	0.4	17	31	0, 12	0.77	0.41	2.32	0.46	0. 19	0.04	0.11
TM-88~10	{ }	<0.1	<1	- 4 😹	81)	46	<5	<5	<0.1	10	6	241	~2	70	53	138	<5	0.3	16	32	0.13	0.74	0.39	2.38	0.54	0.23	0.04	0.10
TM-88~15		<0.1	1	5	2	42	<5	<5	<0.1	11	6	258	2	60	57	96	<5	0.3	19	28	0.09	0.60	0.53	2.69	0.45	0.17	0.04	0.14
TM-88~16		<0.1	- 4	4	<1	39	<5	<5	<0.1	8	5	254	2	60	36	113	<5	0.3	15	28	0.09	0.63	0.42	1.86	0.47	0, 18	0.04	0. 10
TM-88~20		0,6	4	13 💮	6	214	73	7	0.9	32	11	1669	2	58	46	120	<5	0.5	10	25	0.05	1.68	0.34	4.33	0.94	0.14	0.05	0.07
TM-88~21		0.6	- 4	30 🛞	12	267	114	<5	0.7	31	13	1320	2	51	41	129	<5	0.6	11	31	0.05	1.65	0.39	4.87	0.87	0, 16	0.06	0.08
TM-88~22		0.4	5	30 🛞	୍ରା	271	- 88	<5	0.4	31	12	1062	2	61	44	177	<5	0.6	10	29	0.04	1.78	0.34	4.82	0.86	0.22	0.06	0.09
TM-88-22*		0.4	<1	28	7	269	84	<5	0.4	29	11	1058	2	60		169	<5	0.6	8	28	0.03	1.70	0.33	4.62	0.82	0.21	0.06	80.0
TM68 ~-27		<0.1	- 4	41	6	149	20	<5	0.2	40	16	1010	2	55	65	89	5	1.1	20	26	0.05	2.03	0.35	5.04	121	0.14	0.05	0.11
TM-88-27*		<0.1	2	38 🛞	5	146	18	<5	<0.1	38	12	998	2	50	62	85	<5	0.7	12	21	0.05	1.96	0.33	4.95	1 17	0.13	0.04	0.10

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Geochemical Analysis

F	Project/Venture: Vai:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2497	Date Received: Date Completed:	JULY 22, 1992 AUG 18, 1992	Page Atin:	1 K TRO	of	2
F	Remarks:							S HOFE	MAN	
	u - 10.0 g ample digester	d with Aqua Regia and determined by Graphite Furra	ace A.A. (D.L. 1 PPB)					J KOW	ALCHUK	
	CD - 0.5 a comple dicester	with 4 mil Arus Begin at 100 Deg. C for 2 hours						EKIMU	RA	

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ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are tarely dissolved completely with this acid dissolution method.

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SAMPLE		Ag	Mo	Cu	Pb	Zn	As	Sb	Cď	NI	Co	Mn	-Bi	Cr	V	Ba	Ŵ	Be	ta 🛛	Sr	Π	A I	Ca	Fe	Mg	ĸ	Na	P
Na.	[	ppm	ppm	ppm	ppm	ppm	mgq	ppm	ppm	ppm	ppm	ppm	ppm	_ppm	ppm	ppm	ppm	ppm	ppm	ppm	<u>%</u>	<u>%</u>	- 26-1	_%		- *	-*	-
AE-88-25		<0.1	<1	17	14	112	7	<5	<0.1	39	8	783	5	52	43	89	<5	0.5	10	16	0.03	1.60	0.34	4.18	105	0.08	0.02	0.11
AE-43	1	<0.1	2	25	15	148	8	- 6	0.4	18	11	766	5	34		91		0.6	14		0.07	1.0/	0.43	4.01		0.00	0.02	0.13
AE49		0.2	1	88		118	17	8	0.3	36	15	856	4	46		138	<0	0.5	8	(ID)	0.04	1.07	2.78	4.20		0.13	0.02	0.15
AE-50		3.0	23	132	58	758	27	17	6.7	126	16	721	6	47	<b>24</b>	153	<0	0.3	4	90	<0.01	0.53	0.87	3.03		0.05	<0,01	0.14
AE51		0.1	2	82	18	106	15	<5	0.2	30	15	836	2	44	104	143	<>>	0.5		122	0.04	1.72	2.40	4.46	- LOI	0,11	0.02	U. 10
{ }																	_				[						[	
AE-53		<0.1	2	- 81	17	116	11	<5	0.3	31	13	770	2	44	91	129	<5	0.4	7	90	0.03	1.55	2.00	4.02	1.20	0.10	0.02	0.16
AE-54		0.3	4	88	20	139	20	6	0.7	38	16	808	3	42	84	146	<5	0.5	9	100	0.03	1.51	2.30	4, 16	S. Andrewski, S. A.	0,11	0.02	0.1/
AE55		0.1	3	85	17	119	12	6	0.3	34	15	832	4	43	<b>\$</b> 2	163	<5	0.4		- 11A	0.04	1.00	2.50	4.36	1.07	0,12	0.02	0.10
AE57		0.2	3	91		151	18	<5	0.6	39	14	843	- 4	43	80	134	<5	0.4	7		0.03	1.61	2.48	4.23	1.49	0. 12	0,02	0.16
AE~57*		0.2	3	87	13	152	16	<5	0.6	39	15	846	3	43	81	134	<5	0.4	7	98	0.04	1.61	2.51	4.26	1.49	0.12	0.02	0.16
												1																
AE-59		1.0	6	102	20	155	30	13	1.3	46	20	806	7	45	<b>92</b>	139	<5	1.1	20		0.03	1.45	2.19	3.86	1.30	0.13	0.02	0.15
AE-60		0.9	4	95	20	164	19	7	0.8		15	807	4	42	<b>90</b>	152	(~)	0.5	8		0.03	1.52	2.15	4.1/		0.12	0.02	0.10
AE-66	]	0.7	4	101	18	176	19	8	0.8	42	16	- 841	2	41	83	162	<5	0.5	8	. IU-	0.04	1.58	2.39	4.36		0.13	0.02	0.19
AE69		0.7	4	91	21	139	13	6	0.4	36	14	791	5	41	96	168	<5	0.5	7	<u> </u>	0.03	1.58	2.40	4.26		0.11	0.02	0.17
AR~88-56	1	0.2	4	57	14	100	14	6	0.2	29	18	771	7	41]	<b>95</b>	70	] <5∣	1.1	19	55	0, 15	1.90	0.64	4.59	1.33	0, 13	0,10	0.13
1													_											6 00				
AR-58	1	0.3	5	32	14	118	10	4	<0.1	28	21	1578	3	30	78	$\pi$	<ol> <li><ol> </ol></li> <li><ol> <li><ol> </ol></li> </ol> </li> <li><ol> <lo><ol> </ol></lo></ol></li> <lo><ol> <lo><ol> <lo><ol> <lo><ol> </ol></lo> <lo><ol> <lo><ol> <lo><ol> </ol> </lo></ol></lo></ol></lo></ol></lo></ol></lo></ol></lo></ol></li> <lo><ol> <lo><ol> <lo><ol> <lo><ol> <lo><ol> </ol> </lo></ol></lo></ol></lo></ol></lo></ol></lo></ol></li> <lo><ol> <lo><ol> </ol> </lo></ol></lo></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol></li></ol>	1.0	18	61	0.21	2.02	0.73	0.82		U. 10	0.22	0.11
AR-61		<0.1	8	25	13	102	9	< গ	<0.1	25	14	7 19	- 4	31	75	61	<3	0.9	13	D/	0.17	1./5	0.64	4.76		0, 14	0.15	0.06
AR63	- 1	0.1	3	32	B	83	-5	<5	<0.1	15	11	773	4	24	51	96	<5	0.4	10		0,08	1.62	0.49	4.50	1.81	0.10	0.03	0.12
AR-65		0.1	4	23	10	107	18	୍ୟ	<0.1	24	14	780	5	30	74	56	<5	0.8	11	53	0,16	2.10	0,66	4.85		0.12	0.14	0,10
AR-65*		0.1	4	24	11	106	19	<5	<0.1	25	13	768	3	30	75	57	<5	0.8	12	54	0.16	2.12	0.67	4.89		0. t2	0.14	0.10
																						4.74		4 87		0.14	0.01	
AR-66		<0.1	( 3	14		109	6	<	<0.1	2	16	1001	~2	29	69	12	<0	0.8	9	DI	0.20		0.001	4.0/		0.14	0.21	0.101
AR-68		0.4	1	113	23	146	35	<5	0.6	30	30	1298	3	39	108	12	<0	1.0	18	20	0.03	2.31	1.31	0.3/		0.14	0.02	0.10
AR-69	·	0.1	<1	87	13	116	22	<5	<0.1	23	22	1253	6	34	TUT	65	<0	0.4	0	60	0.02	2.29	1.74	0.04		0.15	0.01	0.13
AR-70		<0.1	<1	100	16	129	22		<0.1	2	23	1340	5	34	RU6		<0	0.3	5		0.02	0.37	1.50	4.00		0.13	0.02	0.10
AR-71		0.1	<1	93		120	26	<b>_</b>	<0.1	23	21	12/0	3	33	1.0	09	~	0.3			0.02	2.37	1.00	0.22		0. 14	0.01	0.10
40.70				70		114	85		-		21	1120	0	30	104	75	-5	0.3	5	74	0.03	2.21	1.89	5.95	1.70	0, 15	0.02	0.17
AH-/3		0.4			-	120	30			26	20	4141	2	34		101	<5	0.6	10	47	0.02	2.12	104	5.85	1.57	0.14	0.02	0.15
AH-81		<0.1		80		130	22		-0.1	60	21	1001	2	32	AA	110	-5	0.3	5	38	0.02	2.16	0.86	6.09	1.61	0.14	0.01	0.15
AH-62		<0.1	[ ]			120	20		0.1	5	20	871	2	29	57	48	45	0.3		166	0.02	1.65	274	5.86	1.14	0.14	0.02	0.13
DL-88-112		<0.1				12/	30		0.1		20	692	· •	100		173	-5	04	7	RD	0 10	1.01	0.89	2 27	0.83	0.36	0.06	0.06
SID-P1		0.2	8	24		161	10	( <sup>~</sup>	0.2		°		-	, ~~				<b>۳</b> . ۳	1 1							0.00		
01 - 171		0.4		74		400	74	7	3.2	57	22	1257	8	51	73	133	<5	1.4	26	27	0.06	1.75	0.49	5.83	0.99	0.11	0.02	0.11
01-175		0.7		53		415	80	1	2.2	A	14	1163	Ă	44	60	114	<5	0.6	10	17	0.06	1.86	0.46	5.93	1.08	0.10	0.02	0.11
		0.7				225	24	-	1.7	63	14	1018	0	57	78	179	<5	0.7	10	45	0.05	1.71	0,73	4.62	1.32	0, 12	0.04	0.13
DL-190		0.2		85		459	75		23	55	14	2147	3	45	64	154	<5	0.7	10	23	0.06	2.04	0.58	6.42	1.12	0.12	0.03	0.12
01 492		0.0		74		174	20		0.6	79	20	838	5	127	191	96	<5	0.8	12	32	0.22	2.82	0.89	5.45	2.37	0.12	0.04	0.09
UL- 102		0.2	<b>1</b>	1 1			20	· ~ ا			1 -			l ~ .		1	[	1	-							_,		
DI 183		<01	•	87	,	163	5	6	<0.1	79	28	842	3	134	121	100	<5	0.6	5	32	0.24	3.03	0.95	5.60	2.54	0.13	0.04	0.09
01-194		0.1	1	67		179	10	<5	<0.1	85	30	900	2	146	124	118	<5	0.6	5	34	0.26	3.23	0.96	5.78	2.67	0.14	0.04	0.08
	•	0.3	2	31		190	36	6	0.8	38	10	1072	5	40	47	110	<5	0.7	12	20	0.05	1.61	0.34	4.59	0.85	0.12	0.04	0.10
01-200		0.4		1 111	24	166	85	4	0.4	30	25	912	3	29	54	36	<5	0.3	5	190	0.02	1.71	2.81	7.06	1.17	0.13	0.02	0.14
DL-200*		04	1	110	23	169	85	6	0.6	34	27	911	7	33	59	37	<5	0.5	9	181	0.02	1.74	2.78	6.89	1.19	0,13	0.02	0.14
02-200		0.4	I .	1			-	-			1	• • •																
					a constantine de la c						_																	

Project/Venture:	1P	Geol:	K TROCIUK	Date Received:	JULY 22, 1992	Page	2	of	2
Area:	COREY	Lab Project No.:	D2497	Date Completed:	AUG 18, 1992	Attn:	K TROC	<b>NUK</b>	
Romarks:							<b>S</b> HOFF	MAN	
Au - 10.0 g sample di	gested with Aqua Regia and det	ermined by Graphite Furnace A.A. (D.L. 1 PPB)					J KOWA	LCHUK	
ICP - 0.5 g sample di	gested with 4 mi Aqua Regia at	100 Deg. C for 2 hours.					E KIMUI	RA	

N.B. The major oxide elements, Ba, Be, Cr, La and W are sarely dissolved completely with this acid dissolution method

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SAMPLE	Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	Ni	Co	Mn	Bi	Cr	Y	Ba.	W	Be			ן וד	A ]	Qu	Fe	Mg ]	ĸ	Na	P
No.	ррп	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррт	ppm	ppm	ppm p	pm	*	-%	%	<u>%</u>	*	<u>%</u>	_%	<u>%</u>
DL-202	0.4	5	118	19	172	85	<5	0.5	31	27	965	7	33	60	42	<5	0.5	2		0.02	1.77	3,10	6.74	1.18	0,14	0.02	0.14
DL-205	0.4	6	114	21	171	86	<5	0.5	30	26	938	6	29	56	37	0	0.3	2	197	0.02	1.74	2.97	6.82	1.10	0.13	0.02	0,15
DL206	0.3	4	79		139	24	<5	0.4	2	17	901	6	28	32	60	3	0.3	5		0.02	1.0/	2.92	5.08	1-15	0.13	0.02	0.14
DL-207	0.4	5	118	26.	155	69	<5	0.6	32	28	904	10	31	08	40		0.0		100	0.02	1.04	2.61	5.00		0.131	0.02	0,10
DL206	0.4	4	87	20	143	38	7	0.3		19	962	8	30	37	- 50	S	0.3	•		0.02	1.01	3.11	<b>0.04</b>	1.20	0.14	0.02	U. 13
					457	50					000	7			46	-	0.01		103	<b>~</b> ~	1 69	2 03	5.88		0 13	0.01	0 14
06-209	0.1	</td <td></td> <td></td> <td>13/</td> <td>30</td> <td>a</td> <td>0.4</td> <td></td> <td>20</td> <td>024</td> <td></td> <td>20</td> <td></td> <td>- 40 54</td> <td></td> <td>0.3</td> <td></td> <td></td> <td>0.02</td> <td>173</td> <td>2.01</td> <td>5 50</td> <td>4.7</td> <td>0.14</td> <td>0.02</td> <td>0 14</td>			13/	30	a	0.4		20	024		20		- 40 54		0.3			0.02	173	2.01	5 50	4.7	0.14	0.02	0 14
DL-210	0.2	3	110	10	150	37		0.2		26	016	12	32	85	43		0.4		IR4	0.03	1.74	2.58	6 79		0.15	0.02	0.15
	0.3	. 5	110		38			0.0		R	236	6	45		116	6	0.2	16	51	0.09	0.70	0.57	2.47	0.50	0.16	0.03	0.14
10-00-00					36	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		0.2		5	235		12	4.4	110		0.2	15	50	0.09	0.65	0.53	2 35	0.48	0.16	0.03	0.14
10-00-00-	<0.	'  `'	10			~		0.2		Ŭ	200	-															
TR-11	<0	1 <1	1 11	7	32	<5	<	<0.1	11	6	198	4	49	48	100	<5	0.3	15	41 (	0.08	0.58	0.48	2.22	8.41	0.15	0.03	0.11
TB-42	<0	1 7	33	22	163	37	<5	0.8	33	19	852	4	37	61	99	<5	1.6	29	31 0	0.06	1.91	0.36	5.63	1.14	0.10	0.05	0.06
TB-43	0.1	10	24	20	164	20	<5	<0.1	22	13	724	7	30	37	95	<5	1.1	18	30	0.05	1.69	0.40	6.11	0.94	0.13	0.05	0.10
TB-44	0.1	4	30	15	119	<5	ব	<0.1	20	10	765	4	28	55	82	<5	0.5	11	28	0. 10	1.60	0.44	4.57	0.99	0. 10	0.03	0.11
TB-45	<0.	1 6	21	12	101	12	<5	<0.1	23	12	644	4	37	69	69	<5	0.7	11	44	0. 15	1.77	0.58	4.54	1.19	0.13	0.11	0.07
												[ ]				{	1 1				- (						-
TB46	<0.	1] 6	21	15	122	15	<5	<0.1	25	14	807	3	31	78	- 61	<5	0.9	13	52	0.18	1.94	0.65	5.01	134	0.12	0.15	0.07
TB-47	<0.	1 9	79	15	331	27	<5	1.7	59	23	776	5	69	110	80	<5	0.8	11	38	0.18	2.41	0.96	5.26	1.54	0.13	0.05	0.09
TB-48	8.0	7	74	- 34	330	16	<5	1.3	58	21	718	5	89	114	90	<5	0.5	6	35	0.21	2.47	1.04	5.17	1.62	0,15	0.06	0.09
T8-50	<0.	1 5	21	36	157	33	<5	<0.1	21	15	1038	2	49	65	109	<5	0.9	15		0.23	2.20	0.88	5.18	1.37	0.19	0.22	0.12
STD-P1	0.2	58	25	54	145	20	<5	0.3	30	6	595	~	125	33	1/9	<0	0.4	•		0.11	1.05	0.94	2.3/	0.67	0.38	0.00	0.06
	1		1 494					10		-	000	<u>ہ</u>			170		1 1 5	24		0 14	2 10	157	4.81		0.76	0.04	0 14
18-54	0.3	1 '	131					1.0		30	1017			1.10	404				54	0 15	2 38	171	5.02		0.05	0.04	0.15
18-55	0.4	3	103		110	11		<0.1		05	1077				217		0.4		59	0.14	243	1 60	5.30		0.61	0.03	0.15
10-00	0.5		111		113	14		-0.1	57	24	1086			111	230	-5	0.3		61	0.15	2.47	1.87	5.31		0.91	0.04	0.16
10-0/ T0_60	0.5		85	15	95	17	-5	-11	21	19	1137	3	52	101	243	<5	0.3	5	65	0.12	2.41	2.06	4.79	1.83	0.69	0.05	0.15
10-30	0.5	1	1 ~		-		~					} -				-											
TB-50	0.5	2	95		96	14	<5	<0.1	22	22	1013	5	53	103	218	<5	0.3	4	55	0.14	2.32	1.68	4.82	1.84	0.81	0.05	0,14
TB-60	0.4	5	89	13	104	12	5	<0.1	21	19	1034	5	54	103	271	<5	0.3	4	58	0. 13	2.33	1.76	4.86	1.81	0.77	0.05	0, 15
TB-61	0.3	1 4	16	14	118	8	<5	<0.1	12	7	661	3	39	24	131	<5	0.6	13	22	0.04	1.58	0.36	4.77	0.88	0.19	0.05	0, 12
TB-64	0.7	5	53	13	68	<5	<5	<0.1	30	13	406	4	85	87	106	6	0.3	9	50	0.13	1.66	0.88	3.79	0.82	0.29	0.10	0.11
TB-64*	0.6	6	52	13	64	<5	<5	<0.1	29	13	396	2	83	85	105	8	0.3	9	48	0.12	1.62	0.85	3.70	0.79	0.26	0.09	0.11
1 1	1	1	1				1 1									1	1										
TB67	0.3	1	39		58	7	<5	<0.1	34	12	362	2	85	65	95	ব্য	0.4	10	53	0.11	1.42	0,90	2.81	0.73	0.22	0.10	0.09
TD-74	0.1	<1	9		38	<5	<5	<0.1		5	248	2	95	36	139	7	0.2	14 🔛	37	0.11	0.67	0.50	2.02	0.50	0.23	0.06	0.10
TM-88-01	0.1	3	25	12	43	13	<5	0.6	15	11	253	4	104	46	147	6	0.9	22	46	0.11	0.75	0.44	1.81	0.45	0.22	0.06	0.06
TM-04	<0.	1 1	11		44	<5	<5	<0.1		6	273	4	99	53	143	<5	0.3	16	40	0.14	0.82	0.55	2.61	0.51	0.23	0.06	0.13
TM-12	0.1	<1	6	6	44	<5	<5	<0.1	10	5	276	2	106	46	157	<5	0.3	15	<b>*</b>	U. 15	0.84	0.48	2.42	0.80	0.26	0.05	0.11
			1 .			- 1						~			100	-	0.0	40	-	0 15	0.72	0.69	200	0.50	0.22	0.00	0 12
TM 13	0.1	<1	6	<u> </u>	30	(5)		<0.1	10	5	242		100	35	133		0.3		20	0.10	0.72	0.53	2.00	0.55	0.23	0.06	0.10
TM-14	<0.	1] <1	2		41			<0.1		6	206	3	001		125		0.4	20		0.12	0.00	0.50	21/	0.50	0.22	0.00	0.13
TM-14*	<0.	1 <1		Distance D	38	<0	< 3	<0.1	1933 S.L.	<b>&gt;</b>	204	2	₩/		121	<0	0.2		30.a.d	0.11	0.04	0.35	2.13	8084-ALA	0.4	0.00	0.13

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Geochemical Analysis

Project/Venture: Area: Remarks:	COREY 1P	Geol: Lab Project No.:	K TROCIUK D2446	Date Received: Date Completed:	JULY 22, 1992 AUG 11, 1992	Page Attn:	1 K TROC S HOFF	of IUK MAN	
Au - 10.0 g sample di ICP - 0.5 g sample di N.B. The major oxide e	gested with Aqua Regia and gested with 4 ml Aqua Regia elements, Ba, Be, Cr, La and	determined by Graphite Furnace A.A. (D.L. 1 PF at 100 Deg. C for 2 hours. Ware rarely dissolved completely with this acid	<sup>9</sup> B) I dissolution method				j kowa E kimui	ALCHUK RA	

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No.         Open         Den         Den <thden< th="" th<=""><th>SAMPLE</th><th></th><th>Ag</th><th>Mo</th><th>Cu</th><th>Pb</th><th>Zn</th><th>As</th><th>Sb</th><th>Cd</th><th>Ni</th><th>Co</th><th>Mn</th><th>Bi</th><th>Cr</th><th>V  </th><th>Ba</th><th>W</th><th>Be</th><th>La</th><th>S SI</th><th>ΤI</th><th>AI</th><th>Qa</th><th>Fe</th><th>Mg</th><th>к</th><th>Na</th><th>P</th></thden<>	SAMPLE		Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	Ni	Co	Mn	Bi	Cr	V	Ba	W	Be	La	S SI	ΤI	AI	Qa	Fe	Mg	к	Na	P
AR-Ba-01.       0.6       2       4       41       13       6       -5       -6.01       7       2       2       65       -7       100       -5       -6.01       0.7       0.03       0.06       0.01       0.03       0.06       0.01       0.03       0.06       0.01       0.05       0.01       0	No.		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррп	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	%	%	<b>%</b>	<u>%</u>	%	%
Act-act-1       0.4       5       42       14       101       45       7       0.1       11       210       200       13       45       0.5       12       200       13       45       0.5       11       480       0.5       220       0.03       0.01       0.02       0.00 <td>AR-88-01</td> <td></td> <td>0.8</td> <td>2</td> <td>14</td> <td>14</td> <td>13</td> <td>8</td> <td>&lt;5</td> <td>&lt;0.1</td> <td>7</td> <td>2</td> <td>58</td> <td>2</td> <td>128</td> <td>7</td> <td>170</td> <td>&lt;5</td> <td>0.2</td> <td>5</td> <td>5</td> <td>&lt;0.01</td> <td>0.07</td> <td>0.05</td> <td>1.07</td> <td>0.03</td> <td>0.05</td> <td>&lt;0.01</td> <td>0.01</td>	AR-88-01		0.8	2	14	14	13	8	<5	<0.1	7	2	58	2	128	7	170	<5	0.2	5	5	<0.01	0.07	0.05	1.07	0.03	0.05	<0.01	0.01
Act-act-Ac-2       c0.1       2       33       9       61       c3       c4       c4 <thc4< th="">       c4       c4</thc4<>	AE-88-44-1		0.4	5	42	1	101	<5	7	<0.1	<b>3</b> 1	25	865	~2	62	129	31	<5	0.4	6	7	0.23	2.60	0.93	6.81	2.03	0.02	0.04	0.08
AE-68-63-3         AE-68-64-73-2         Col. 1         4         33         6         12         Col. 1         9         30         100         9         100         100         7         4         7         100         50         Col. 1         4         7         100         30         30         6         100         100         0.00	AE88442		< 0.1	2	33	9	61	<5	<5	<0.1	19	11	498	2	90	93	6	<5	0.7	6	6	0.21	2.86	2.63	4.59	0.91	<0.01	<0.01	0.07
ALC-88-6-1       c.0.1       3       33       6       8       c.5       8       c.1       32       18       79       4       7       17       17       24       27       124       27       124       27       124       27       124       27       124       17       16       17       17       17       17       17       17       17       17       17       17       17       17       17       17       17       18 <td>AE-88-45-3</td> <td></td> <td>&lt; 0.1</td> <td>4</td> <td>35</td> <td>6</td> <td>129</td> <td>&lt;5</td> <td>&lt;5</td> <td>&lt;0.1</td> <td>31</td> <td>30</td> <td>1 199</td> <td>7</td> <td>45</td> <td>205</td> <td>50</td> <td>&lt;5</td> <td>0.4</td> <td>5</td> <td></td> <td>0.33</td> <td>3.41</td> <td>1.91</td> <td>8.63</td> <td>1.90</td> <td>0.02</td> <td>0.03</td> <td>0, 14</td>	AE-88-45-3		< 0.1	4	35	6	129	<5	<5	<0.1	31	30	1 199	7	45	205	50	<5	0.4	5		0.33	3.41	1.91	8.63	1.90	0.02	0.03	0, 14
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	AE-88-46-1		<0.1	3	33	6	84	<5	8	<0.1	32	16	797	4	74	1 10	15	<5	0.4	4	~~7	0.24	2.72	1.53	5.97	1.79	0.01	0.03	0.08
AL=Be-T-2       Col.1       45       Col.1       55       72       110       115       Col.1       55       72       110       115       Col.1       55       72       120       0.00<																					\$\$\$\$C.;								
BK-88-00       <0.1       7       74       7       74	AE-88-47-2		<0.1	- 4	35	11	115	<5	<5	<0.1	55	32	1190	8	58	136	54	<5	0.5	5	7	0.22	3.04	0.87	6.57	2.09	0.03	0.04	0.10
BK-88-40       cl.1       5       4       6       7       26       cl.1       4       7       7       100       1.33       0.07       0.14       0.04       0.00       0.08       1.33       0.07       0.14       0.04       0.01       0.13       0.01       1.30       0.01       1.30       0.01       1.30       0.01       1.30       0.01       0.00       0.08       0.01       0.00       0.08       0.01       0.00       0.08       0.01       0.00	BK-88-39		<0.1	7	74	7	42	<5	<5	<0.1	12	8	571	~2	49	60	142	<5	0.1	- 4	17	0.11	1.53	0.62	3.04	1, 12	1.05	0.04	0.09
BK-88-41       24       7       286       2       50       13       c5       0.1       14       13       0.04       121       0.39       581       127       0.38       0.01	BK-88-40		<0.1	5	4	6	7	26	<5	<0.1	4	<1	59	~2	57		72	<5	<0.1	4	7	<0.01	0.20	0.09	1.33	0.07	0.14	0.04	<0.01
STD-P1       0.3       67       28       511       156       19       c5       0.1       37       6       580       c2       124       37       186       c5       5       7       83       0.11       1.7       0.05       2.40       0.91       0.41       0.06       0.06         BK-88-42       0.04       1       467       c5       c5       44       60       85       c5       0.6       12       23       0.06       201       0.28       6.96       182       0.11       0.01       0.33         BK-88-42       0.0       2       41       161       211       122       14       160       17       17       15       55       33       52       2       7       0.11       140       0.03       0.22       0.00       0.03       0.03       0.02       2.00       0.03       0.01       0.04       0.03       0.05       0.01       0.02       2.05       0.05       0.05       0.06       0.01       0.02       0.05       0.01       0.02       0.05       0.01       0.02       0.05       0.01       0.02       0.05       0.01       0.02       0.05       0.01       0.01	BK-88-41	- 1	2.4	7	258	2	50	13	<5	<0.1	18	12	322	<2	39	58	66	<5	0.1	4	-13	0.04	1.21	0.39	5.81	1.27	0.26	0.02	0.18
BK-88-41A BK-88-42         0.9         2         105         27         B7         57         45         0.1         122         5         44         93         85         45         0.6         12         23         0.08         201         0.28         5.99         112         0.11	STD-P1		0.3	67	26	51	156	19	<5	0.1	37	6	589	<2	124	37	188	<5	0.5	7	93	0.11	1.17	0.95	2.40	0.91	0.41	0.08	0.08
BK-88-41A         0.9         2         105         27         87         67         63         64         103         65         65         12         23         0.06         21         23         0.06         21         0.23         0.06         211         0.01         0.17         0.02         0.41           BK-88-43         3.0         2         41         11         124         141         124         141         124         141         124         141         124         141         124         141																													
BK-88-42       0.4       1       46       9       146       <5       <5       0.1       <1       1       0.05       123       0.34       1.00       0.17       0.02       0.1       0.10       0.03       0.2       0.41       161       0.11       11       0.05       0.25       0.03       0.25       0.03       0.22       0.04       0.03       0.02       0.04       0.03       0.02       0.01       0.01       0.03       0.02       0.05       0.01       0.01       0.03       0.02       0.04       0.02       0.04       0.03       0.02       0.04       0.01       0.03       0.02       0.04       0.01       0.03       0.05       <	BK-88-41A		0.9	2	105	27	87	67	<5	<0.1	20	11	1282	5	44	93	85	<5	0.6	12	23	0.08	2.01	0.26	5.99	1.92	0.11	0.01	0.13
BK-88-43       3.0       2       41       19       2       6.7       6       71       56       28       59       -55       0.1       -11       15       0.00       0.71       0.28       0.41       0.38       0.22       20       0.01       0.11       0.01       0.01       0.01       0.01       0.01       0.01       0.02       0.21       1.11       0.11       0.01       0.01       0.01       0.01       0	BK-88-42		0.4	1	46	9	148	<5	<5	0.3	9	2	746	~2	43	43	52	<5	0.1	<1	<b>3311</b>	0.05	1.23	0.34	2.94	1.09	0.17	0.02	0.14
BK-88-44       0.7       4       63       14       186       0.49       c       c       11       121       124       3       71       58       33       c       50       21       17       0.01       1.44       0.37       6.52       1.00       0.01       0.44       0.37       6.52       1.00       0.01       0.03         BK-88-46       0.1       5       16       9       14       12       c5       c5       0.1       22       15       c5       c0.1       c4       0.02       c2       15       c5       c0.1       c4       0.03       0.05 <th< td=""><td>BK-88-43</td><td></td><td>3.0</td><td>2</td><td>41</td><td>18 1</td><td>241</td><td>142</td><td>&lt;5</td><td>&lt;0.1</td><td>16</td><td>7</td><td>819</td><td>4</td><td>50</td><td>28</td><td>59</td><td>&lt;5</td><td>0.1</td><td>&lt;1</td><td>15</td><td>0.08</td><td>0.71</td><td>0.28</td><td>6.14</td><td>0.36</td><td>0.22</td><td>&lt;0.01</td><td>0.18</td></th<>	BK-88-43		3.0	2	41	18 1	241	142	<5	<0.1	16	7	819	4	50	28	59	<5	0.1	<1	15	0.08	0.71	0.28	6.14	0.36	0.22	<0.01	0.18
BK-88-45       10.0       2       382       10       10.0       2       382       10       10.0       2       382       10       11       1       12       13       15       16       9       10.0       20       0.05	BK-88-44		0.7	- 4	63	14	186	0.49%	<5	<0.1	22	18	4987	3	71	58	33	<5	0.2	2		0.01	1.94	0.37	6.92	1.00	0.15	<0.01	0, 10 [
BK-88-46 BK-88-46A         0.4         3         114         3         23         <5         <5         <0.1         4         10         102         <2         50         20         27         <5         <0.1         2         17         0.00         0.53         0.16         2.04         0.28         0.05 <t< td=""><td>BK-88-45</td><td></td><td>10.0</td><td>2</td><td>382</td><td>10</td><td>1086</td><td>96</td><td>&lt;5</td><td>6.1</td><td>11</td><td>1</td><td>243</td><td>- 4</td><td>72</td><td>23</td><td>15</td><td>&lt;5</td><td>&lt;0.1</td><td>&lt;1</td><td>5</td><td>&lt;0.01</td><td>0.48</td><td>0.26</td><td>5.90</td><td>0.21</td><td>0.06</td><td>&lt;0.01</td><td>0.03</td></t<>	BK-88-45		10.0	2	382	10	1086	96	<5	6.1	11	1	243	- 4	72	23	15	<5	<0.1	<1	5	<0.01	0.48	0.26	5.90	0.21	0.06	<0.01	0.03
BK-88-46       0.4       3       184       3       23       c5       c5       c5       c5       20       27       c5       c1       12       17       0.66       0.33       0.16       2.04       0.28       0.05 <th0.05< th=""> <th0.05< th=""> <th0.01< td=""><td>l  </td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>_</td><td>_</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th0.01<></th0.05<></th0.05<>	l																_	_											
BK-8B-46A       0.1       5       16       9       14       12       <       <       14        15       16       9       14       12       <       <       14       15       16       9       14       12         14       15       16       9       14       15       251       45       65       3       35       35       25       36       45       36       45       0.26       133       277       0.45       0.11       0.00       0.05       0.01       0.05	BK-88-46		0.4	3	184	3	23	<5	<5	<0.1		10	102	2	50	20	27	<5	<0.1	2		0.06	0.53	0.16	2.04	0.28	0.05	0.05	0.05
BK-88-47       3.8       5       670       33       25       46        5       209       40       10       208       3.6       0.68       0.62       1       57       0.01       0.19       2.08       3.6       0.68       0.60       0.01       0.02       13       291       7       148       70       <5       8.6       23       5       391       <2       60       22       71       <5       0.2       2       44       0.01       0.25       1.33       2.81       0.45       0.11       <0.01       0.05       1.88       0.03       0.07       <0.01       0.02       1.33       2.81       0.45       0.11       <0.01       0.05       1.88       0.03       0.07       <0.01       0.02       1.33       2.81       0.44       0.41       1.48       11       4.4       5       1.55       1.220       <2       93       14       76       7       0.4       8       9       0.01       0.13       0.05       1.88       0.03       0.07       <0.10       0.05       1.88       0.03       0.07       <0.10       0.05       1.00       0.05       1.00       0.05       1.01       0.01	BK-88-46A		0.1	5	16	₽	14	12	<5	<0.1	9	- 4	146	<2	22	15	41	<5	0.2	<1	409	<0.01	0.32	12.30	0.48	0.33	0.01	0.02	0.03
BK-88-46       5.1       12       291       10       1160       71       <5       8.6       23       5       335       <2       61       21       71       <5       0.2       22       44       <0.01       0.28       1.33       2.77       0.45       0.11       <0.01       0.06         BK-88-469       0.3       <13       291       71       it       65       0.2       23       75       0.41       15       15       120       22       76       46       141       <5       0.3       13       111       <0.01       0.33       4.00       0.45       0.11       <0.01       0.05       188       0.00       0.07       <0.01       0.05       188       0.03       0.07       <0.01       0.05       188       0.00       0.07       <0.01       0.05       188       0.00       0.07       <0.01       0.05       188       0.01       0.00       0.05       1.08       0.01       0.00       0.06       0.01       0.05       0.07       <0.01       0.05       0.05       0.07       <0.01       0.05       0.05       0.07       <0.01       0.05       0.07       0.01       0.00       0.01       0.00<	BK-88-47	-	3.8	5	670	13	2519	46	<5	20.9	40	8	256	3	93	12	36	<5	0.2	1	57	<0.01	0.19	2.08	3.46	0.38	0.06	<0.01	0.02
BK-88-49       0.3       <1       3       291       7       1148       70       <5       8.2       23       5       391       <2       60       22       72       <5       0.2       2       44       <0.01       0.25       1.33       2.81       0.45       0.11       <0.00         BK-88-49       0.3       <1       34       20       103       00       <5       0.4       14       6       66       <2       93       14       76       7       0.4       8       9       <0.01       0.13       0.05       188       0.03       0.07       <0.01       0.02         BK-88-51       0.3       <1       77       3       109       <5       <5       <0.1       23       24       1804       230       66       635       <5       0.5       67       0.01       1.53       4.40       4.84       112       0.18       0.01       0.10         BK-88-52       0.4       <16       70       <5       <5       <0.1       20       20       462       6       50       111       55       10.8       3       275       1.32       6.54       1.17       0.08       0.1	BK-88-48		5.1	12	291	10	1160	71	<5	8.6	23	5	385	<2	61	21	71	<5	0.2	2	- 44	<0.01	0.26	1.33	2.77	0.45	0.11	<0.01	0.05
BK-88-49       0.3       <1       34       20       103       10       <5       0.4       14       6       86       <2       93       14       76       7       0.4       8       9       -0.01       0.13       0.05       1.88       0.03       0.07       <0.01       0.02         BK-88-50       0.4       1       48       11       194       <5       <5       <0.1       155       122       <2       76       48       141       <5       0.3       3       111       <0.01       1.53       4.40       4.84       112       0.13       0.05       1.88       0.01       0.00       0.00       0.00       0.00       0.00       0.01       0.01       1.53       4.40       4.84       11       15       122       0.1       1.53       1.40       0.64       0.55       0.55       6.57       0.51       0.53       0.51       0.50       1.42       0.11       2.5       0.01       0.15       0.01       0.13       0.05       1.44       0.66       0.01       1.10       0.01       1.53       1.41       0.16       1.30       0.65       5.41       1.17       0.53       0.275       1.32 <t< td=""><td>BK-88-48*</td><td></td><td>4.9</td><td>13</td><td>291</td><td>7</td><td>1148</td><td>70</td><td>&lt;5</td><td>8.2</td><td>23</td><td>5</td><td>391</td><td>~2</td><td>60</td><td>22</td><td>72</td><td>&lt;5</td><td>0.2</td><td>2</td><td>44</td><td>&lt;0.01</td><td>0.25</td><td>1.33</td><td>2.81</td><td>0.45</td><td>0.11</td><td>&lt;0.01</td><td>0.05</td></t<>	BK-88-48*		4.9	13	291	7	1148	70	<5	8.2	23	5	391	~2	60	22	72	<5	0.2	2	44	<0.01	0.25	1.33	2.81	0.45	0.11	<0.01	0.05
BK-88-49       0.3       <1							400		-	~ ~		_					70					-0.01	0 12	0.05	1 00		0.07	-0.01	0.02
BK = 88 - 50       0.4       1       1       1       14       13       12       24       160       40       42       17       6.3       5.1       17       0.3       5       17       0.3       5       17       0.3       1.42       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.50       1.32       3.17       6.47       0.5       0.5       0.5       0.5       1.17       0.5       0.5       0.5       1.17       0.5       0.5       0.5       1.17       0.3       5       14       0.16       1.30       0.65       5.44       0.89       0.66       0.08       0.13       0.5       1.47       0.10       0.72       0.71       0.12       0.55       1.32       0.54       1.17       0.10       0.71       0.12       0.66       0.08       0.13       0.55       1.31<	BK-88-49		0.3	<1	34	20	103	10	<0	0.4		0	00	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	83				0.4	0		-0.01	1.52	0.00	1.00		0.07	0.01	0.02
BK-88-51       0.3       <1       77       3       109       <5       <5       101       23       23       180       22       30       60       635       <53       63       53       63       635       63 <td>BK-88-50</td> <td></td> <td>0.4</td> <td>1</td> <td>48</td> <td></td> <td>194</td> <td>&lt;0</td> <td>&lt;5</td> <td>&lt;0.1</td> <td>CI CI</td> <td>15</td> <td>1220</td> <td>~</td> <td>/0</td> <td><b>40</b></td> <td>141</td> <td>&lt;0</td> <td>0.3</td> <td>3</td> <td></td> <td>&lt;0.01</td> <td>1.53</td> <td>4.40</td> <td>9.04</td> <td></td> <td>0,10</td> <td>0.01</td> <td>0.10</td>	BK-88-50		0.4	1	48		194	<0	<5	<0.1	CI CI	15	1220	~	/0	<b>40</b>	141	<0	0.3	3		<0.01	1.53	4.40	9.04		0,10	0.01	0.10
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	BK-88-51	1	0.3	<1	11	<u> </u>	109	<5	<5	<0.1	23	24	1804	2	30	00	030	<0	0.5	6	47	0.01	1.42	0.17	5.00		1 12	0.00	0.15
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	BK-88-52		0.4	<1	121	2	73	12	<0	<0.1	18	21	401	5	02 51	121	77	12	0.3	5		0.21	1.04	0.54	5.00	0.80	1.12	0.08	0.13
BK-88-54       0.3       6       76       2       51       <5       <0.1       20       20       462       6       50       111       55       10       0.8       3       25       0.10       2.75       1.32       6.54       1.17       0.80       0.17       0.12         BK-88-55       0.3       17       520       2       36       <5       <0.1       15       20       539       4       45       136       55       23       0.6       4       41       0.12       2.75       2.25       4.01       0.72       0.71       0.20       0.17         BK-88-56       0.1       16       174       6       30       <5       <5       <0.1       113       8       276       4       81       113       83       <5       0.4       4       37       0.12       2.00       1.23       3.05       0.77       0.69       0.16       0.13         BK-88-57       0.1       177       173       2       2       8       173       83       <5       0.4       33       37       0.13       2.04       1.24       3.07       0.77       0.70       0.16       0.13	BK-68-53		0.2	29	98	4	10	<5	<0	<0.1	••	21	324	3	51	114		13	0.5	3		0.10	1.50	0.03	0.44		0.00	0.00	V. 13
BK-88-55       Co.1       25       Co.1       15       20       539       4       45       136       55       23       0.6       4       41       0.12       2.75       2.25       4.01       0.72       0.71       0.20       0.17         BK-88-56       0.1       16       174       6       30       c5       c5       c0.1       13       8       276       4       81       113       83       c5       0.4       4       37       0.12       2.00       1.23       3.05       0.75       0.69       0.16       0.13         BK-88-57*       0.1       17       13       7       278       4       83       115       84       c5       0.4       3       37       0.12       2.00       1.23       3.05       0.75       0.69       0.16       0.13         BK-88-58       0.2       1       7.35	RK_89_54		03	6	76	•	51	-5	-5	-01	20	20	462	6	50		55	10	0.8	3	25	0.10	2.75	1.32	6.54	1.17	0.80	0.17	0.12
BK-88-56       0.3       17       520       2       36       45       40       69       57       0.6       4       51       0.12       2.69       1.75       6.50       0.62       0.85       0.23       0.19         BK-88-57       0.1       16       174       5       30       45       40.1       113       82       276       4       81       113       83       45       0.4       4       37       0.12       2.00       1.23       3.05       0.75       0.69       0.16       0.13         BK-88-57*       0.1       17       13       7       276       4       83       115       84       45       0.4       3       37       0.13       2.04       1.24       3.07       0.77       0.70       0.16       0.13         BK-88-58       0.2       4       12       16       50       6.5       0.1       6       1       735       42       58       5       57       45       0.4       20       10       40.01       0.27       1.00       2.26       0.04       0.11       0.04       0.02         BK-88-59       0.2       4       12       16 <th< td=""><td>BK-00-54</td><td></td><td>~0.1</td><td>25</td><td>204</td><td></td><td>46</td><td>~5</td><td>~5</td><td>-0.1</td><td></td><td>20</td><td>539</td><td>Ā</td><td>45</td><td>136</td><td>55</td><td>23</td><td>0.6</td><td>Ă</td><td></td><td>0.12</td><td>2.75</td><td>2.25</td><td>4.01</td><td>0.72</td><td>0.71</td><td>0.20</td><td>0.17</td></th<>	BK-00-54		~0.1	25	204		46	~5	~5	-0.1		20	539	Ā	45	136	55	23	0.6	Ă		0.12	2.75	2.25	4.01	0.72	0.71	0.20	0.17
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	DK-00-00		0.1	20	520	5	40	~	~5	-0.1	17	38	341	5	44	109	69	57	0.6		51	0.12	2.69	1.75	6.50	0.62	0.65	0.23	0.19
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	DK-00-30 DK-99-57		0.3	16	174	R	30	~5	~5	-01		a l	276	Ă	81	113	83	<5	0.4	4	37	0.12	2.00	1.23	3.05	0.75	0.69	0.16	0.13
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	DK-00-57			17	174	Š	30	-5	-5	-11		7	278	Å	83	115	84	<5	0.4	3	37	0.13	2.04	1.24	3.07	0.77	0.70	0.16	0.13
BK-88-58       <0.1       3       10       2       17       <5       <5       <1       735       <2       58       5       57       <5       0.4       20       10       0.01       0.27       1.00       2.26       0.04       0.11       0.04       0.02         BK-88-59       0.2       4       12       16       50       6       <5       0.1       6       2       189       <2       85       7       34       9       0.3       12       6       <0.01       0.27       1.00       2.26       0.04       0.01       0.027       0.06       1.36       0.06       0.03       0.02         BK-88-60       0.2       7       10       10       33       <5       <5       <0.1       8       2       129       <2       32       7       93       <5       0.4       11       15       <0.01       0.42       0.27       3.93       0.15       0.20       0.05       0.01       0.22       0.01       0.42       0.27       3.93       0.15       0.20       0.05       0.01       0.27       0.01       0.42       0.27       3.93       0.15       0.20       0.05       0.01	01-00-01-	1		. "					~			1	2/5														1	1	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	DK_00_50	f	-01		10		17	-	~	-01	R	1	735	0	58	<b>F</b>	57	<5	0.4	20	10	<0.01	0.27	1.00	2.26	0.04	0.11	0.04	0.02
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	DK-00-30	1	0.0		10	10	50	~		0.1	A		189	0	85		34	9	0.3	12	8	<0.01	0.31	0.06	1.36	0.05	0.08	0.03	0.02
BK-88-61       0.2       3       70       <1       339       6       <5       1.6       104       33       917       <2       237       160       105       <5       56       0.07       4.02       2.70       6.21       4.07       0.03       0.05       0.06         BK-88-61       0.2       1       16       1       103       109       <5       <0.1       18       5       522       4       33       15       70       <5       0.4       10       10       0.06       1.29       0.45       9.15       1.01       0.15       0.02       0.11         BK-88-70       <0.1       2       12       118       <5       <0.1       18       5       522       4       33       15       70       <5       0.4       10       10       0.06       1.29       0.45       9.15       1.01       0.15       0.02       0.11         BK-88-71       <0.1       2       12       118       <5       <0.1       100       4       605       <2       30       9       110       <5       0.6       26       8       <0.01       1.23       0.29       3.88       0.75       0.1	9K_89_60		0.2	7	10	10	33	-5	-5	-0.1	R	2	129	0	32	<b>7</b>	93	<5	0.4	11	15	<0.01	0.42	0.27	3.93	0.15	0.20	0.05	0,10
BK-88-70       <0.1       18       16       1       103       109       <5       <0.1       18       5       522       4       33       15       70       <5       0.4       10       10       0.06       1.29       0.45       9.15       1.01       0.15       0.02       0.11         BK-88-70       <0.1	BK_88_61		0.2		70		330	~~~ R	-5	1.8	104	33	917	0	237	160	105	<5	0.3	5	56	0.07	4.02	2.70	6.21	4.07	0.03	0.05	0.06
BK-88-71       <0.1       2       12       118       <5       <5       <0.1       10       4       605       <2       30       9       110       <5       0.6       26       8       <0.01       1.23       0.29       3.88       0.75       0.16       0.01       0.05         BK-88-72       <0.1       10       8       3       28       35       6       <0.1       12       4       123       <2       39       39       69       <5       0.3       8       17       0.04       0.71       0.22       5.97       0.48       0.10       0.05       0.16         BK-88-73       0.4       11       37       7       104       7       <5       0.2       19       4       557       <2       58       70       63       <5       0.4       13       23       0.02       1.31       1.64       4.57       1.03       0.09       0.02       0.27	BK-00-01		-0.1	19	16		103	109	-5	-0.1	IR I	5	522	4	33	15	70	<5	0.4	10	10	0.06	1.29	0.45	9.15	101	0.15	0.02	0.11
6K-88-71       <0.1       2       12       12       118       <5       <5       <0.1       10       4       605       <2       30       9       110       <5       0.6       26       8       <0.01       1.23       0.29       3.88       0.75       0.16       0.01       0.05         6K-88-72       <0.1       10       8       3       28       35       6       <0.1       12       4       123       <2       39       39       69       <5       0.3       8       17       0.04       0.71       0.22       5.97       0.48       0.10       0.05       0.16         6K-88-73       0.4       11       37       7       104       7       <5       0.2       19       4       557       <2       58       70       63       <5       0.4       13       23       0.02       1.31       1.64       4.57       1.03       0.09       0.02       0.27	DK-00-70		- 0.1	"	.0		,		~~			J		•															,
BK-88-72       <0.1       10       8       3       28       35       6       <0.1       12       4       123       <2       39       59       <5       0.3       8       17       0.04       0.71       0.22       5.97       0.48       0.10       0.05       0.16         BK-88-73       0.4       11       37       7       104       7       <5	8K-88-71	- 1	-01		12	12	118	<5	5	<b>c</b> 0.1	10		605	0	30		110	<5	0.6	26	8	<0.01	1.23	0.29	3.88	0.75	0,16	0.01	0.05
BK-88-73 0.4 11 37 7 104 7 <5 0.2 19 4 557 <2 58 70 63 <5 0.4 13 23 0.02 1.31 1.64 4.57 1.03 0.09 0.02 0.27	BK_88_72	- I	201	10	, <u>2</u>		28	35		-0.1	12		123	0	39	39	69	<5	0.3	8	17	0.04	0.71	0.22	5.97	0.48	0.10	0.05	0.16
	BK_89_73		04	11	37		104	7	<5	0.2	19		557	0	58	70	63	<5	0.4	13	23	0.02	1.31	1.64	4.57	1.03	0.09	0.02	0.27
IRK_88_74 I I 2.3 I 11 31/00051 68 35 <5 0.4 002 0.14 2970 <2 115 0052 58 <5 0.3 5 0.245 <0.01 0.46 4.83 4.21 0.225 0.08 0.02 0.14	BK-88-74	1	23	11	31	5	69	35	<5	0.4	14	2	970	0	115	52	58	<5	0.3	5	246	<0.01	0.46	4.83	4.21	0.25	0.08	0.02	0.14
BY 8 74 24 7 29 4 69 36 5 0.3 14 1 971 2 118 51 56 5 0.2 4 249 0.01 0.45 4.94 4.25 0.24 0.08 0.02 0.14	BK-88-74*		24	7	29		69	36	- 6	0.3		1	971	2	118	51	56	<5	0.2	4	249	<0.01	0.45	4.94	4.25	0.24	0.08	0.02	0.14
	DR-00-14		*·· •	· '	20				~~					_		s -													

Project/Venture: Area:	COREY 1P	Geol: Lab Project No.:	K TROCIUK D2446	Date Received: Date Completed:	JULY 22, 1992 AUG 11, 1992	Page Attn:	2 of K TROCIUK	4
Remarks:							SHOFFMAN	
Au - 10.0 g sample digeste	d with Aqua Regia and determined by Graphite Furne twith 4 ml Agua Regia at 100 Deg. C for 2 bours	ace A.A. (D.L. 1 PPB)					J KOWALCHUK E KIMURA	

ICP ~ 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Ba, Cr, La and W are rarely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Mo	Çu	⊘РЬ	Źn	As	Sb	Cd	NI NI	Co	Mo	Bi	Cr	1990 - A.	Ba	w	Be	ίa.	୍ୟ		A	Ca	<b>F0</b>	MO	~	Na	۳ «
No.		ppm	ррт	ppm	ppm	ppm	ррт	ppm	ppm	ppm	ррт	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	%	%		%	<b>%</b>	*
BK-88~75		1.1	48	146	21	1030	11	<5	3.8	270	25	540	3	111	204	95	<5	0.7	11	31	0.15	1.84	1.34	5.41	0.94	0.09	0.04	0.08
BK-88-76		0.7	22	56	12	314	24	<5	2.5	27	5	612	~	60	109	41	8	0.4	3	24	0.11	1.27	0.41	5.09	0.42	0.19	0.03	0.08
BK-88-77	- 1	0.8	20	42	15	218	235	<5	1.5	34	6	251	~	43	26	57	<5	0.3	6	8	0.03	0.56	0.15	5.39	0.21	0.17	<0.01	0.06
BK-88-78		0.7	29	409	5	151	<5	<5	<0.1	44	10	597	8	117	221	109	<5	0.5	6	15	0.18	1.75	0.32	6.28	0,95	0.16	0.02	90.0
BK-88-79		4.8	11	384	5	78	18	<5	<0.1	20	14	928	2	59	113	113	<5	1.0	4	61	0, 18	2.82	0.81	5.64	1.50	1.46	0.14	0.14
DV 00 00		0.2		201	,	20	-5	<5	<0.1	<b>7</b>	2	197	2	44	13	40	<5	0.5	12	7	<0.01	0.60	0.11	2.29	0.20	0.22	0.01	0.03
DK-00-00		0.2	1 7	201	8 S .	120	-5	-5	-01	100 A 1	5	729	a	72	87	695	<5	0.2	4	3	0.21	2.28	0,14	4.23	1.80	1.61	0.03	0.08
BK-66-61		<0.1		32	2 C	50		~5	~0.1		10	358	2	115	<b>11</b>	350	<5	0.2	1	12	0.24	1.67	0.41	4.44	1.30	0.95	0.07	0, 10
BK-88-82		0.2		105					-0.1	100 for		254		88	<u></u>	206	<5	0.2	<1	66	0.05	1.15	0.54	1.82	0 37	0.29	0.09	0.07
BK-88-83		<0.1	2	67	2	23	<0	<3	<0.1	14		0.54				204		0.2	1		0.05	1 15	0.54	181	0.36	0.29	0.09	0.07
BK-88-83*		<0.1	3	66	ಿತಿ	29	<>	<>	<0.1	12	- 1	330	~~	8		204		0.2	`'		0.00	1. 10	0.04	1.01		0.20		0.01
											_		_			42.4		0.7			-0.01	0.28	0.14	3 57	0.40	0 17	0.03	0.09
BK-88-84		0.1	5	21	8	32	12	<5	<0.1	13	6	246	~~	48		131	° °	0.7	13	10	<0.01	0.30	0.14	0.07		0.17	0.00	0.00
BK-88-85		<0.1	2	5	7	95	<5	<5	<0, 1	9	5	599	<2	97	34	42		0.3	5	2	<0.01	0.90	0.30	2.00		0.00	0.03	0.09
BK-88-86		0.2	2	6	6	36	<5	<5	<0.1	9	<1	131	_ <2	40	2	92	<5	0.2	6	2	0.21	0.10	0, 13	4.10	<b>CU.U</b> 1	0.10	0.03	0, 13
BK-88-87		0.1	21	3	5	11	10	<5	<0.1	7	<1	23	<2	40		173	<5	<0.1	3	7	0.13	0.19	<0.01	4.40	0.01	0.14	0.03	0.08
BK-88-88		0.1	4	3	6	31	6	<5	<0.1	5	<1	77	~2	37		141	<5	0.2	9	23	<0.01	0.66	0.16	3.63	0.44	0.26	0.05	0.13
			Į																		I I							
BK-88-89		0.2	4	5	7	1 19	<5	<5	<0.1	11	9	1784	2	48	-47	61	<5	0.4	9	60	0.01	0.89	1.54	4.97	0.32	0.17	0.02	0.14
BK-88-90		0.1	3	11	2	215	<5	<5	<0.1	14	11	982	<2	25	20	121	<5	0.4	11	40	<0.01	1.09	0.42	6.02	0,45	0.20	0.02	0.20
BK-98-01		01	Â	6		24	14	<5	<0.1	10	2	110	<2	45	8	109	<5	0.3	7	20	<0.01	0.23	0.03	5.63	0.02	0.25	0.02	0.12
DK-00-31		-01	1	7		307	<5	<5	<0.1	9	2	482	2	31	15	120	<5	0.4	12	56	<0.01	1.31	1.67	4.45	0.80	0.17	0.03	0.16
BK-00-92				<b></b>		152	20	-5	-01	35	5	594	0	116	34	180	<5	0.4	6	85	0.10	1.08	0.88	2.36	0.88	0.37	0.07	0.08
ISID-P1		0.2	~	~~		JJZ	×۳	~	-0.1		Ŭ																	
			۰ ا	- I		,	-5	-5	-01	e a company	-1	21	0	31		184	<5	02	7	18	<0.01	0.21	0.04	2.89	0.02	0.25	0.04	0.09
BK-88-93		0.3	2	10	0		<5		<0.1			21	2	20		40.4		0.3	+2	19	-0.01	0.23	0.21	2 18	0.05	0 19	0.04	0.11
BK-88-94		<0.1	5	8	J.	16	9	<0	<0.1	2	2	55	~~		°,			0.5	12		-0.01	0.02	0.00	22.45	n 72	0.02	-0.01	0.02
8K-68~94A		4 16.0	<1	1970	427	74	4.16%	74	1.1	64	78	10105	2290	44	2002 I		<0				<0.01	0.00	0.00	22.90		0.02		0.02
BK8894B		260.0	2	1754	243	88	2.51%	60	1.7	64	77	15394	1519	40		6	<2	0.1	2	1999 P.	<0.01	0.04	0.00	23.01	ill work of	0.01	0.07	0.03
BK-68-95		4.3	7	53	19	15	21	<5	<0.1	8	3	443	41	101		54	<5	0.2	8		<0.01	0.13	0.01	2.32		0.09	0.03	0.01
1				ł													L _					0.47						0.00
BK-88-96		1.7	<1	20	19	54	16	<5	0.2	8	3	380	6	82		69	<5	0.2	6		<0.01	0.17	0.08	1.34	<b>n'n</b> 5	0.09	0,03	0.02
BK-88-97		1.9	<1	54	<1	101	<5	<5	<0.1	35	19	718	~2	170	240	10	<5	0.3	4	3	0.36	2.34	0.45	8.71	1.95	0.04	0.02	0,12
BK8898		1.4	<1	23	8	69	5	<5	<0.1	16	3	498	2	61	105	24	<5	0.2	4	3	0.20	0.99	0.10	4,17	1.09	0.05	0.02	0.07
BK-88-99		1.5	. A	41	6	134	8	<5	<0.1	19	2	667	2	61	86	37	<5	0.2	6	6	<0.01	2.74	0.14	7.49	3.47	0, 10	<b>&lt;</b> 0.01	0. 19
81 -88 -90*		1.5	9	43	7	135	5	<5	<0.1	20	2	673	2	64	86	38	<5	0.2	6	6	<0.01	2.79	0.14	7.55	3.52	0, 10	<0.01	0.20
00-00-00				l			Ī										1											
				444		74	14	6	-01	27	20	835	0	48	117	39	<5	0.7	13	29	0.12	2.09	0.57	5.58	1.89	0.05	0.02	0.19
86-88-100		0.3		114		20						708		65	10	68	<5	0.1	5	14 1	0.03	0.81	2.12	2.33	0.72	0.10	0.02	0.07
BK-88-101		0.2	2	53		30		< 3	-0.1			177		74		. 24			3		0.05	0.60	0 17	1.57	048	0.05	0.03	0.04
BK-88-102		0.3	<1	16	12	25	28	2	<0.1		2		2			29		1			-0.01	0.67	0.50	5 30	0.20	0 12	0.06	0.32
BK-88-103		<0.1	13	8	20	37	29	<5	<0.1	10	2	105	<2	32	20	19	<0	0.2		000	0.01	0.07	0.00	4 19		0.12	0.00	0.02
BK-88-104		<0.1	8	32	∴ <1	57	6	8	<0.1	22	9	506	~2	66	23	130	<5	0.3	3	203	<0.01	0.20	0.00	-, 13		0.00	0.01	0.00
																	L _					4.00	1					0.45
BK-88-105		<0.1	5	13	2	56	26	7	<0.1	13	7	528	<2	92	30	43	<5	0.3	12	52	<0.01	1.33	1.25	3.63	0.77	0.04	0.01	0.15
BK-88-106		4.8	105	16	62	65	84	18	<0.1	18	<1	33	<2	65	34	53	<5	<0.1	2	5	0.20	0.30	0.06	1.57	0.27	0.10	<0,01	0.06
BK-88-107		0.4	9	46	10	76	<5	<5	<0.1	24	5	484	2	53	32	109	<5	<0.1	4	17	0.10	1.21	0.31	4.00	1, 10	0.07	0.02	0,10
BK-AA-MA		0.4	A A	95	21	51	<5	<5	<0.1	28	44	354	5	75	144	38	<5	0.3	2	5	0.08	2.03	0.44	8.93	1.46	0.54	0.04	0, 14
01-00-100+		0.3		000		53	<5	<5	<0.1	29	46	365	2	75	148	37	<5	0.3	3		0.08	2.06	0.44	9.28	1.49	0.55	0.04	0.14
DIV-00-100-		0.3	<b>°</b> ا	~~		1 ~	<u>~</u> ا		1		1		- 1					1										
			1		10000700044	1	L	[	·	1 - COCCES 2 - C		L						-										

Geochemical Analysis

Project/Venture: Area:	COREY 1P	Geol: Lab Project No. :	K TROCIUK D2446	Date Received: Date Completed:	JULY 22, 1992 AUG 11, 1992	Page Attn:	3 K TROC	of IUK	
Remarks:							S HOFF	MAN	
Au - 10 0 a sample dige	sted with Aque Regis	and determined by Gaphite Furnace A.A. (D.L. 1 PPB)					J KOW/	LCHUK	

E KIMURA

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Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB) ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are rarely dissolved completely with this acid dissolution method.

SAMPLE	Ag	Mo	Cu	Pb	Zn	As	Sb	Cđ	N.	Co	Mn	Bi	Cr	્યું	Ba	w	Be	La St	1 U	A	Ca	61	<b>. M</b> 9	ĸ	Na	P
Na	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm ppm	%	<u>%</u>	<u>%</u>	%	<b>%</b>	%	%	%
BK-88-109	0.5	3	109	<1	45	<5	<5	<0.1	24	19	375	~2	55	105	55	<5	0.4	6 16	0.10	1.58	0.98	6. 13	101	0.54	0.11	0.18
BK-68-110	0.5	<1	14	12	185	17	<5	0.6	224	10	398	<2	95	90	43	<5	0.3	5 2	0.08	1.32	0.53	4.94	0.75	0.51	0.08	0.10
BK88111	0.2	<1	20	2	45	<5	<5	<0.1	18	11	352	~2	62	59	46	<5	0.2	5 17	0.11	1.03	0.44	3.39	0.66	0.47	0.09	0.11
BK-68-112	10.0	3	119	25	1263	8	<5	6.3	17	12	592	9	77	97	35	6	0.3	3 2	0.11	1.46	0.63	5.89	0.79	0.29	0.02	0.12
BK-88-113	1.4	5	292	59	663	<5	<5	1.6	13	16	1132	6	75	94	72	<5	0.5	3 29	0,14	3.18	1.44	4.70	L 18	0.91	0.13	0.09
		_							8888C					0 (g. 29) 												
BK_88_114	0.4		148		71	6	-5	<b>c</b> 0 1	10	18	634	0	91	105	125	ব	0.7	4	0.13	4.09	2.35	4.22	0.97	0.88	0.27	0,10
DK-00-14	0.4		101		71	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	-5	-01	2847	18	497	0	64	107	170	6	0.2	4	0.20	3.03	1.46	4.66	80 Y 1	0.97	0.21	0.14
DK-00-110	0.0	`;	240		457	24		29	200	17	453	100	A	84	72	131	0.5	4	0.12	2.92	167	4 88	0.84	0.47	0.17	0 12
DK-00-10	2.0		240		-07			-01	20	25	161	~	55	40	40	-5	0.3	3	0.08	2.08	1 49	4 34	0.29	0 19	0 19	0 14
8K-88-11/	0.7		238		21	0		-0.1		20	100	~	50		44		0.0		0.00	2.00	1.50	4 38	0.70	0,10	0.10	0.14
BK-88-117"	0.7	4	235	9	27	<3	<>	<0.1		20	юU	2	- 33		41		0.3		0,00	2.00	1.00	4.00		V. 13	0.18	V. 14
						_						_				ا ا			0.40	0.07	4 00			0.54	0.04	0 40
BK-88-118	0.6	<1	55	5	89	<5	<5	<0.1	18	15	4/9	3	5/	98	37		0.5	1	0.10	2.0/	1.33	4.40		0.01	0.21	0.10
BK-88-119	1.5	4	281	245	469	<5	<5	1.4	26	21	701	12	55	<b>94</b>	46	<0	0.5	3 22	0.14	2.11	1.42	6.22	<b>U.5</b>	0.70	0.21	0.11
BK-88-120	1.4	<1	89	20	87	<5	<5	<0.1	15	16	339	<2	49	ः 59	36	<5	0.3	3 38	0.08	2.55	1,49	5.23	0.53	0.33	0.21	0.11
BK-88-121	0.2	1	68	7	48	<5	<5	<0.1	14	- 4	310	<2	39	21	70	<5	0.2	8 14	0.08	1.05	0.21	2.81	1.04	0, 10	0.02	0.09
BK-88-122	1.2	4	118	5	51	<5	<5	<0.1	16	6	307	<2	39	16	65	<5	0.3	8	0.04	0.87	0.30	3, 19	0.86	0.17	0.02	0.15
				<u> </u>					ŶŰ.				ŀ													
BK-88-123	0.1	<1	95	<b>*</b> 1	49	<5	<5	<0.1	13	9	914	2	30	33	77	<5	0.5	9 229	<0.01	0.41	3.22	3.62	0.85	0.09	0.05	0, 16
DL-88-179	0.5	<1	21	9	296	15	<5	0.3	18	2	343	4	65	11	32	<5	0.5	5 11	<0.01	0.78	0.15	4.50	0.25	0, 10	0.01	0.08
DI -88 - 18 1	0.3	1	138	< I	84	<5	<5	<0.1	21	30	570	2	27	83	16	ব	0.5	4 30	0,12	1.56	1.21	5.77	1.21	0.04	0.07	0.29
01-88-185	0.2	37	81	2	30	<5	<5	<0.1	35	13	171	2	60	54	50	<5	0.3	3 77	0,10	0.81	0.70	3.14	0.38	0.28	0.11	0.10
DI -88 - 185*	0.2	34	80		29	<5	<5	<0.1	35	13	167	~2	59	52	48	<5	0.3	3 74	0.09	0.78	0.68	3.06	0.37	0.28	0.11	0.10
	0.2	· · ·												889 S						1						
N -98-196	02	7	117		112	6	<5	<0.1	55	16	602	4	181	151	217	9	0.5	4 219	0.20	2.38	1.58	4.02	1.30	1, 18	0.11	0.11
0 99 197	0.2	.	84		34	~	-5	-01		18	265	3	66	51	49	<5	6.0	3 226	0.08	1.53	3.03	2.82	0.39	0.39	0.27	0.18
	0.2		1 1 1		27	~5	-5	~01		23	166	6	37	17	10	-5	0.2	6	0.06	0.78	138	3 19	0.23	0.03	0 10	0.34
UL-00-100	0.2		020		21			~0.1		25	101	2	31	65	88	~5	0.3	A	0.10	1 10	1 14	4 10	Sec.	0.11	0.10	0.22
UL-00-109	0.3		200	8 A.	122	79	42	0.1	5.0	8	350	4	57	27	21	-5	0.3	7 75	-0.01	0.39	153	6 16	0 19	0.08	0.03	0.50
DL-86-212	0.U	2			HOZ 1	10	13	0.1			- 350				£, 1	<sup>~</sup>	0.0			0.00		0, 10		0.00	0.00	0.00
			404					-0.4	OF	40	765				24	~	0.2		-0.01	0.66	0.68	7.01	054	0.00	0.00	0.97
DL88-213	0,1	5	104		119	04		<0.1			703		-0		24		0.2		0.01	0.00	0.00	0.00	0.05	0.08	-0.02	0.27
DL-88-214	0.5	4	15	12	61	11	<3	<0.1		2	440	•	30	17	07	<0 -	0.4	O K	0.02	0.04	0.10	0.00	0.00	0.20	<0.01	0.10
DL-88-215	0.2	5	11	13	80	13	<5	<0.1	11		492	4	29	8	80	9	0.3	2	0.02	0.37	0.20	0.91		0.20	<0.01	0.19
DL88216	0.2	<1	10	···· 6	110	<5	<5	<0.1		81	1031	~2	391	<u></u>	129	<0	0.3	9	0.02	1.14	0.00	0.00		0,20	0.03	0.25
STD-P1	0.2	59	27	43	147	19	<5	0.1	35	6	572	<2	109	30	168	S	0.4	5 80	0.10	0.97	0.86	2.27	<b>U.1</b> 22	0.34	0.06	0.08
		1	1																							
DL-88-217	0.4	3	15	10	84	<5	<5	<0.1	12	10	529	<2	30	24	110	12	0.3	10 34	0.02	0.64	0.63	4.26	0.23	0.16	0.03	0.25
DL-86-218	0.2	<1	5	9	95	<5	<5	<0.1	7	5	1521	<2	59	27	65	<5	0.2	6 4	0.01	0.74	1, 10	3.50	0.29	0.09	0.02	0.14
DL88219	0.3	12	14	18	48	15	<5	<0.1	15	7	587	2	23	10	30	<5	0.6	7	<0.01	1.13	0.17	8.47	0.69	0.24	<0.01	0.12
DL-88-220	0.8	11	48	98	59	47	5	<0.1	14	7	154	3	33	14	39	⊲5	0.3	7	<0.01	1.00	0.14	7.49	0.68	0.09	0.01	0. 10
DL-88-221	<0.1	<1	10	<1	91	<5	<5	<0.1	15	28	1036	2	95	92	69	<5	0.2	2	0.08	2.81	0.36	6.90	3.59	<0.01	0.02	0.06
					- 1															Ì						
01-88-222	0.1	1 1	a 1		19	8	<5	<0.1	6	2	43	2	61	5	62	പം	0.2	7	0.04	0.15	<0.01	2,10	0.04	0.12	0.03	0.01
01-99-223	0.1				46	A	5	<0.1	<b>A</b> 1	10	487	0	110	150	118	6	0.2	2 1BE	0.01	1.10	2.26	3.89	0.76	0.08	<0.01	0.16
UL-00-220	0.1		50		30		ا <sub>ح</sub> م	201		17	340	3	20	95	42	<u> </u>	0.3	2	0,19	1.09	0.59	4.69	0.83	0.06	0.05	0.08
UDD 49.0	0.1		60		20					20	359		82	87	22		0.2	<1 00 C	0.13	196	1.07	4.72	160	0.04	0.08	0.09
Jrn-66-2	0.2	_	1 2		50	~ 3				20	260				24		0.2		0.13	105	1 06	4 66	1 86	0.04	0.00	0.00
JPK-66-2"	0.2	2	1 79		28	<3	< 3	<0.1	100 <b>* *</b>	20	332		02		<u>ב</u> ו	~	V.2	``	1 0.10	1.00	1.00	7.00		0.04	0.00	0.08
1 ]			l				[	L	13888300							[			4		5 I		1.409.000			

# Geochemical Analysis

Project/Venture:	COREY	Geol:	K TROCIUK	Date Received:	JULY 22, 1992	Page	4	of	4
Area:	1 <del>P</del>	Lab Project No.:	D2446	Date Completed:	AUG 11, 1992	Attn:	K TROCI	UK	
Remarks:							S HOFFN	AAN	
Au - 10.0 g sample d	igested with Aqua Regia and deter	mined by Graphite Furnace A.A. (D.L. 1 PPB)					J KOWA	LCHUK	
ICP = 0.5 g comole di	cested with 4 ml Acue Begin at 10	0 Derr. C for 2 hours					EKIMUR	IA	

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ICP - 0.5 g sample digested with 4 ml Aqua Rega at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are marely dissolved completely with this acid dissolution method.

SAMPLE	Ag	Мо	Cu Pb	Zn	As	Sb	Cd	(NI)	Со	Mn	BI	Cr	< <b>V</b> ()	Ba	W	Be	La	Sr	Ti	A	Ca	Fe	Mg	K	Na	P
No.	ppm	ppm	ppm ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррт	ppm	%	%	%	%	~ %	%	%	<u>%</u>
JPR-88-3	0.6	6	41 2	609	<5	<5	<0.1	27	5	4 15	2	39	21	48	<5	0.3	9	<u>کي</u>	0.07	0.81	0.05	6.79	0,40	0. 14 (	0.01	0.05
T8-88-1	< 0.1	<1	51	163	<5	<5	<0.1	62	22	797	2	56	70	28	<5	0.2	- 4	32	0.14	3.41	3, 13	4.65	1.56	0.03	0, 19	0.07
T8-88-2	< 0.1	<1	73 <1	89	<5	<5	<0.1	53	30	611	<2	55	79	41	<5	0.3	6	8811	0.20	2.17	1.37	4.76	1.58	0.03	0.03	0.06
TB-88-3	0.2	<1	185 <1	45	<5	<5	<0.1	26	15	451	2	68	79	5	<5	0.2	- 4	ેંે 20	0.21	1.83	Q.67	6.80	×1.37	0.01	0.02	0.06
TB884	0.3	1	21 <1	152	76	6	0.9	17	4	637	2	39	15	62	<5	0.4	3	1 16	<0.01	0.63	3.73	2.58	0,27	0.11	0.02	0.03
TB-88-5	<0.1	2	34 <1	95	<5	<5	<0.1	35	19	758	~2	53	91	29	<5	0.2	5	10	0.13	2.81	0.54	5.37	2.22	0.02	0.05	0.07
TB886	<0.1	<1	48 <1	93	<5	<5	<0.1	100	28	663	<2	131	65	18	<5	0.2	7	25	0.11	3.03	1.14	5.76	2.09	0.02	0, 10	0.15
TB-88-7	0.1	<1	48 <1	96	<5	<5	<0.1	97	30	860	<2	192	88	13	<5	0.2	6	12	0.15	2.97	1.74	6.12	2.55	0.02	0.03	0.14
TB-88-8A	0.2	<1	62 <1	176	<5	<5	<0.1	25	13	1029	< 2	31	63	33	<5	0.5	6	10	0.12	3.67	1.01	7.01	2.46	0.04	0.01	0. 13
TB-88-8A*	0.2	2	61 <1	179	<5	<5	<0.1	25	13	1034	<2	31	62	32	<5	0.4	6	9	0.11	3.74	0.98	7.19	2.53	0.04	0.01	0.13
TB-88-88	0.2	3	66 <1	155	<5	<5	<0.1	23	11	1026	~	31	70	37	<5	0.6	6	12	0.17	3.76	1, 18	6,98	2.39	0.04	0.01	0.13
TB-88-9	< 0.1	4	66 <1	62	<5	<5	<0.1	180	29	556	2	368	50	10	<5	0.2	3	<b>12</b>	0.13	2.69	2.39	4.14	2.49	0.03	0, 10	0.06
TB-88-10	< 0.1	2	22 <1	98	<5	<5	<0.1	73	32	958	2	129	116	14	<5	0.3	5	7 🔅 🏹	0.22	3.15	1.08	6.79	2.59	0.01	0.02	0.08
TB-88-11	<0.1	5	82 <1	80	<5	<5	<0.1	126	30	769	2	213	74	12	<5	0.3	- 4	5 🔅	0.18	3,35	1.11	4.97	3.27	0.02	0.02	0.05
TB88-12	0.2	10	66 2	73	8	ব	<0.1	23	13	779	2	80	138	16	<5	0.6	5	83	0.09	1.58	3.44	5.51	1.73	0.06	0.02	0.12
TB8813	0.1	5	110 <1	69	5	<5	<0.1	22	24	1020	2	38	259	41	<5	0.4	7	274	0.04	2.37	4.48	5.76	1.95	0.07	0.02	0. 19
TB-88-14	<0.1	2	13 <1	94	<5	<5	<0.1	16	24	904	2	135	×133	34	<5	0.2	- 4	>>> 8	0.12	3.42	0.49	6.13	4,10	0.01	0.02	0.06
TB-88-15	<0.1	- 4	6 14	10	<5	<5	<0.1		<1	51	<2	42	8	70	<5	0.1	13	9	0.04	0, 19	0.07	1.63	0.07	0.09	0.04	0.01
TB-88-16	9.0	3	231	350	<5	<5	0.6	20	16	634	<2	43	122	31	<5	0.6	2	39	0.10	3.36	1.86	6.40	1.02	0.66	0. 19	0.12
TB-88-16*	9.0	4	229 3	343	<5	<5	0.5	20	16	624	5	42	118	30	<5	0.6	2	ંં 36	0.09	3.25	1.78	6.15	0.98	0.63	0.18	0, 12

**Geochemical Analysis** 

Project/Venture;	1P	Geol:	K TROCIUK	Date Received:	JULY 22, 1992	Page	1	of
Area:	COREY	Lab Project No.:	D2440	Date Completed:	AUG 5, 1992	Attn:	K TROC	NUK
Remarks:							<b>1 KOM</b>	LACHUK
Au - 10.0 g samole	digested with Agus Regis and	determined by Graphite Furnace A.A. (D.L. 1 PPB)					E KIMU	RA

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Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB)

ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are rarely dissolved completely with this acid dissolution method.

SAMPLE	Au	Ag .	Mo	Cu	∞ Pb	Zn	As .	Sb	Çq	N	Co	Mn	Bi	Cr		Ba	w	Be	L.R.	ા શાળ		AI I	Ca	1-e	Mg	К	Na	۲
Na	ppb	ppm	ppm	ррт	ppm	ppm	ppm	ppm	ppm	ppm	_ppm	ррт	ppm	ppm	ppm	_ppm	ppm	ppm	ppm	ppm	%	<u>%</u>	<u>    %     </u>	%	- %	_%	<u>%</u>	<u>%</u>
BJS-1		0.1	6	32	<b>8813</b>	66	24	<5	<0.1	23	17	645	2	21	23	56	୍ୟ	0.5	6		<0.01	1.04	0.12	4.52	0.37	0.02	<0.01	0.09
BJS-2	1	<0.1	3	34	11	77	41	<5	<0.1	20	22	977	3	21	23	51	< ත	0.4	7	31	<0.01	0.91	0,12	5.95	0.38	0.02	<0.01	0.12
BJS-3	1	< 0.1	4	32	88 <b>1</b> 4	85	41	<u>୍</u> ଟ	<0.1	18	26	1948	2	14	22	45	< ব	0.6	10	24	<0.01	0.78	0.31	5.99	0.46	0.02	<0.01	0.11
8.15-4		<01	1	25	12	104	13	6	<0.1	20	12	970	2	15	26	80	<5	0.6	12	36	<0.01	1.34	0.32	5.02	0.64	0.02	<0.01	0.13
DIC 5		201		21		70	1 7		-01	8 W 7	16	1003	2	15	25	154	6	0.6	11	26	0.02	1.05	0.20	4.63	0 57	0.02	0.01	0.09
000-0		<b>CO.1</b>	! '	21		14	! '		<b>NO. 1</b>		10	1000	~			101		0.0	••		V.V.		0.20			0.02		
	J							ا ر													0.00	9.00	0.70	200		0.02		0.00
CG-101		8.4	3	55	12	285	35	୍ଦ	0.7	W/	24	1129	~	150	P/	30	<0	0.8	10	21	0.00	3.63	0.78	3.89		0.03	0.01	0.00
DL-01		0.4	<1	80	16	111	18	<5	<0.1	<b>0</b> 0	18	769	3	33	ಾ	45	<ol> <li>&lt;0</li> </ol>	U.6	10	್ಷಾಗಂ	0.07	1.09	0.33	4.72		0.09	0.00	0.10
DL-02		0.5	<1	129	20	138	27	<5	<0, 1	35	24	1062	3	27		49	୍ଷ	0.5	9	24	0.04	1.79	0.35	5.23	101	0.06	0.04	0, 13
DL-03		0.7	<1	129	15	116	36	9	<0, 1	30	20	556	6	22	35	57	<5	0.4	7	32	<0.01	1.45	0.69	4.69	0.89	0.05	<0.01	0.13
STD-P-1		0.2	59	27	61	150	19	6	0.2	36	6	578	<2	111	33	179	<5	0,4	6	~77	0.09	1.01	0.80	2.26	0.85	0.37	0.06	0.08
						1				3 (1) (s.,																		1
DI04		4.1	5	150		738	72	- 5	4.3	59	38	2947	6	28	66	42	- 6	0.9	11	45	0.02	1.76	0.62	7.39	1.20	0.06	0.02	0.17
				126	38 A S	172	72		30	36	24	1213	2	22	52	36	<5	04	8		0.01	129	3.49	6.65	0.98	0.06	0.02	0.16
		1.0		407	**	075			12	28	20	1127	6	22	- RA	53	-5	0.3		66	0.02	145	0.91	8 45	1 12	0.06	0.02	0.18
DL-00		1.0		107		210			1.0		20	1107						0.0		400	-0.01	1.40	2.04	6 07		0.00	0.01	0.10
DL07		0.6	<1	115	8 8 V	216	53	<0	0.8	20	24	665	2	20		20	<3	0.3	0	100	<0.01	1.40	2.94	0.27		0.05	0.01	0.15
DL08		0.6	<1	159	<b>8815</b>	169	195	<⊅	0.2	<b>1</b>	- 34	860	4	21	45	21	C	0.3	6	187	<0.01	1.40	3.01	1.87		0.05	<0.01	Ų, 13
	1	ł	1											1			1									!		
DL-10		0.2	<1	18	38 <b>8</b> 1	22	<5	< 5	<0.1	13	5	127	2	20	66	49	< গ	0.1	13	38	0.02	0.34	0.56	3.16	0.24	0.09	0.01	0,18
DL-11		0.3	1	90	3	39	<5	<5	<0.1	40	18	243	<2	55	71	133	<5	0.2	5	48	0.08	1.10	0.56	3.43	0.81	0.39	0.03	0.12
DL 12		NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS
DI 13		0.2	3	19	2 - C - C - C - C - C - C - C - C - C -	24	<5	<5	<0,1	15	5	130	<2	22	BO	41	<5	0.1	13	32	0.02	0.34	0.60	3.74	0.24	0.09	0.02	0.19
DI - 13*		0.2	2	20		22	ব	<5	<0.1	15	5	127	2	22	79	42	6	0.1	13	33	0.02	0.35	0.62	3,66	0.25	0.10	0.02	0.20
	· ·		-														1			2000-200								1
		-01	-1	.7		20	-5		-01	10	6	158	0	27	1 19	50	6	0.2	15	37	0.02	0.35	0.60	5, 18	0 24	0.08	0.01	0 19
DL-14		<b>CO.</b>							~~ 1		~	464				44		0.0	40		0.02	0.49	0.64	4 04	0 20	0.00	0.02	0.10
DL-15		<0.1	3	20		21		<2	<0.1			104	~~	24		400		0.2		20	0.00	1.07	1.04	9.00	4 00	0.03	0.02	0.15
DL-16		<0.1	<1	56		40	< <u>•</u>		<0.1		15	310	~	32		133	<0	0.3			0.09	1.27	1.21	0.20	0.00	0.27	0.02	0,10
DL-20	ļ	0.1	2	60	2	54	<5	<∞	<0.1	32	22	376	<2	42	<u> </u>	152		0.2		10	0.07	1.24	0.40	3.82	0.63	0.26	0.03	0.09
DL-21		< 0.1	<1	55	7	80	<5	<5	0.2	28	12	412	<2	43	58	117	<5	0.4	4	29	0.09	1.35	0.42	2.62	0.86	0.17	0.04	0.07
	1				99 - CARA ( 1																							
DL-22		0.5	<1	64	8 8 8	47	<5	<⊅	<0.1	24	17	303	2	31	63	133	<5	0.2	1	24	0.07	1.08	0.51	3.28	0.77	0.26	0.03	0.12
DL-23		<0.1	<1	84	<b>0</b> 10	65	<5	<5	<0, 1	35	19	431	2	50	82	171	<5	0.4	3	25	0, 12	1.71	0.50	3.80	<b>L 14</b>	0.37	0.04	0, 13
DL-24		<0.1	<1	58		41	<5	<5	<0.1		14	300	2	29	55	80	<5	0.4	3	12	0.08	1.31	0.26	2.71	0.66	0.17	0.02	0.09
DI -25		0.2	2	110		71	7	_ ব	<0.1	36	23	484	2	41	106	115	<5	0.2	2	31	0.07	1.24	0.52	4.68	0.90	0.39	0.04	0.11
DI		0.2	2	108	<b>K</b>	70	- 65	ক্র	<0.1		21	470	2	40	101	115	<5	0.2	2	31	0.07	1.21	0.49	4.46	0.88	0.39	0.03	0.11
			-			1	-										-		_									1
	ł			l			46	ا ير ا	A 4		20	384	ام ا	30	00 g 1	62	17	0.5	R	36	0.06	124	0.81	4.17	0.80	0.32	0.05	0.10
UL-20		0.4		90		20	01 مر ا		V. I		20	400			8874	100	<u>"</u>	0.3			0.00	1 20	0.00	3.65	0.80	0.02	0.05	0.00
DL-27		0,4	<1	96	8.80 C	()	CD	<	<0.1		23	400	~~	•••		100		0.3		<b>20</b>	0.00	1.50	0.50	3,03		0.23	0.00	0.09
DL-28		0.3	2	91		111	10	<	0.1		25	506	~	54		135		0.3	3	30	0.09	1.52	0.09	4.51		0.42	0.04	0.12
DL-29		0.3	] 3	80	12	99	5	⊲5	<0.1	50	23	590	2	66	HOO	204	<0	0.4	4	28	0,10	1,66	0.54	4.26	141	0,47	0.03	0.12
0S-1	ł	1.2	1 1	166	19	193	71	୍ ଏ	0.3	32	22	1272	<2	43	62	- 36	୍	0.3	4	19	0.03	1.76	0,45	5.02	1.58	0.05	0.01	0.16
	[			ļ –																								1
DS-2	]	1.1	1 1	151	19	184	78	പ	<0.1	34	23	1143	5	42	63	30	<5	0.3	3	18	0.03	1.75	0.46	5.61	1.61	0.05	0.01	0.16
DS-3	1 · ·	0.4	3	61		145	50	- 6	<0.1	22	16	1043	0	29	52	41	<5	0.3	4	20	0.04	1.45	0.53	4.08	1.33	0.08	0.02	0, 18
08-4			1	145		107	107		0.2	200	25	1355	0	31	55	42	<5	0.2	4	21	0.05	1.59	0.62	5.67	1 47	0,15	0.01	0.20
00-4		1.0	1 21	124		100	426	ام <sup>~</sup> ا	-0.1		27	1201		20	40	33	6	0.2		10	0.04	145	0.60	6.02	1.34	0.14	0.01	0.20
03-0		1.2		134		170	407	_	~~.1		21	1205		20		35		0.2		<b></b>	0.04	1 50	0.60	6 04	1 30	0 14	0.01	0.20
DS-5*		1.2	2	136	60	170	127	اه ا	0.1	30	26	1323	~~		20 P L	30	<b>1</b>	0.2	3		0.04	1.50	0.00	0.04	1000 C	0.14	0.01	0.20
	<u> </u>	I	L	l		L		1						l	2000 M.	L,	I		L	0.02045			└╌╦╴╾┯┛		000000000	لسممح		

Geochemical Analysis

Project/Venture: Area: Remarke:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2440	Date Received: Date Completed:	JULY 22, 1992 AUG 5, 1992	Page Attn:	2 K TROCI	of IUK
residence,							J KOWL	ACHUK

Au = 10.0 g sample digested with Aqua Regia and determined by Gaphite Furnace A.A. (D.L. 1 PPB) ICP = 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours.

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N.B. The major oxide elements, Ba, Be, Cr, La and W are marely dissolved completely with this acid dissolution method

SAMPLE	Au	Ag	Mo	Cu	₩Pb .	Zn	As	Sb	Çq	N	Co	Mn	Bi	Cr	V	Ba	W	Be	La	Sr	Π	A	Ca	Fe	∭Ma⊗	K	Na	P
Na	ppb	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	DOM	nog	pom	mag	DDM	Dom	8	96				e la	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
DS-6		1.3	3	168	18	192	83	<5	<0.1	32	24	1202	2	39	61	32	10	0.3	5		0.03	1.67	0.30	5 57	1 52	0.04		70
(EH-10		0.8	4	113		125	18	<5	<0.1	55	23	1028	2	63	72	97	<5	0.6	ě		0.16	104	0.68	4 07	07	0.07	0.01	0.10
EH-11		0.8	3	98	9	103	19	<5	<0.1	39	20	977	~2	52	67	53	6	0.3	e e	21	0.03	1.83	0.55	4.80		0.05	0.01	0.10
EH 12		0.7	3	86	7	103	12	<5	<0.1	58	22	947	2	88	76	38	<5	0.3	Ă	<b>17</b>	0.03	2.25	0.00	5.00		0.05	0.01	0.10
EH-13		24	7	173	18	235	74	<5	0.2	29	24	1322	2	32	76	59	-5	0.3		40	0.02	2.20	0.40	0.00		0.04	0.02	0.14
J								~					-	~		~	~	0,0	- T		0.02	2.31	0.48	0.33		0.04	0.02	0.17
ES-1		0.8	6	38	13	43	24	<5	<0.1		3	238	0	64	57	12	~	0.2										
ES-2		0.1	2	59	12	92	36	-5	601		15	817				20		0,3			0.11	2,15	0.04	4,34	0.46	0.04	0.01	0.05
ES-3		<0.1	3	37	9	112	14		-01	56	14	552		80	33	<u>44</u>		0.5	2	<u> </u>	0.09	2.1/	0,16	3.98	1.50	0.04	0.03	0.05
ES-4		3.0		23	14	104		~~~	-0.1	25		215		55	60	23	<0	0.0		ÇI 💭	0.08	1.73	0.36	3,47	1.47	0.06	0.03	0.06
FS-4*		3.0		23	16	104						210			01	21	<3	0.8		UI	0. 10	1.59	0.47	4,10	0.46	0.04	<0.01	0.04
		0.0	Ň	~		~~	- <b>-</b> 1		~0.1	e	ິ	215	~	- 24 [	<b>B</b> 1	28	<5	0,8	9	10	0.09	1.59	0.47	4.11	0.46	0.04	<0.01	0.04
FS-5		0.1	1	43		128			~	~			-	~														
ES-6		0.1				120	25		<0.1	BU	10	567	~~	82	83	36	9	1,0	11	29	0. 16	2.05	0.45	4,14	171	0.08	0.09	0.05
ES-7		0.2		67		164	30	<3	<0.1	91	23	/81	~2	178	83	36	<5	0,5	5	22	0.08	2.61	0.46	4.43	2.44	0.07	0.04	0.07
CO_8		0.2			2	104	39	< 3	0.1	D.1	2/	920	~2	94 [	113	102	<5	0.7	9	44	0.14	2.55	0.70	4.87	1.83	0.16	0.10	0, 10
C3-0		0.3	<1	12	0	115	19	<5	0.1	46	21	560	<2	67 [	76	78	<5	0.7	7	24	0.08	2.18	0.42	3.45	1.04	0.10	0.03	0.07
C3-8		_U.1	3	80	8	188	12	6	0.3	37	26	557	<2	50	68	101	<5	0.7	7	18	0.09	1.60	0.29	3.58	0.96	0.14	0.04	0.08
0140-1			اء ا				_	_											1		I							
		0.3	5	138		137	<5	<5	0.1	41	23	827 į	~	48	103	166	<5	0.8	7	67	0.14	2.04	0.73	4.82	1.48	0.57	0.03	0.15
GWS-2		1.6	2	1 19	21	187	34	<5	0.2	101	29	1391	<2	1 10	90	60	<5	1.1	14	29	0.11	3.23	0.46	4.94	2.04	0.09	0.05	0.13
GWS-0		1.1	2	104	7	153	19	<5	<0.1	152	42	1237	<2	208	113	31	<5	0.6	7	22	0.10	3.64	0.50	6.28	3.55	0.04	0.03	0.09
GWS-4		1.0	5	95	18	274	61	6	0.5	88	27	1837	2	95	69	445	<5	0.7	8	32	0.11	2.67	0.39	5.94	1.93	0.08	0.08	0.12
SID-P1		0.3	58	25	51	152	19	8	0.2	35	. 5	531	2	1 10	30	172	<5	0.4	5	70	0.08	0.98	0.79	2.32	0.84	0.37	0.05	0.08
	1						1										1	- 1										
GMR-2	1	0.5	4	46	7	375	20	<5	0.6	78	19	721	~2	88	55	128	10	0.7	7	23	0.09	2.14	0.45	4.36	1.96	0.06	0.08	0.07
GW5-6		0.2	1	39	10	160	47	<5	<0.1	65	17	841	~2	98	44	40	<5	0.8	9	13	0.09	1.80	0.28	3.62	140	0.06	0.05	0.04
GWS-7		0.2	2	74	13	125	57	6	<0.1	105	28	1035	<2	151	80	32	<5	0.8	9	32	0.13	3.23	0.40	4.58	270	0.07	0.11	0.04
GWS-8		0.1	4	28	12	95	10	<5	<0.1	34	11	321	2	33	45	159	<5	1.4	14	88 H I	0.03	1.71	0.18	3.52	0 76	0.04	0.01	0.04
GWS9		<0.1	2	21	6	106	26	<5	<0.1	34	14	668	2	29	59	53	<5	0,8	10	36	0.12	1.43	0.51	3.72	1 25	0.08	0.12	0.04
0.110											I					[											v	0.00
GW5-10	1	0.1	3	22	7	110]	12	<5	0.4	28	- 11	1068	2	29	42	86	<5	0.9	11	18	0.06	1.25	0.28	3.42	0.68	0.04	0.04	0.07
GW5-11		0.1	3	21	8	124	20	6	0.2	29	11	598	~2	29	46	67	<5	0.9	9	21	0.06	1.32	0.33	3 18	0.7.1	0.06	0.06	0.07
GWS-12		0.2	2	26	13	87	9	<5	<0.1	26	11	825	2	27	43	43	<5	0.6	7	14	0.06	1.41	0.19	3.37	0 70	0.05	0.05	0.06
GWS-13	- 1	0.1	- 4	32	12	110	15	5	0.4	25	11	8 16	2	28	42	40	<5	1.0	12	11	0.04	1.65	0.22	341	0.50	0.04	0.00	0.07
GWS-13*		0.1	1	33	17	113	18	7	0.4	26	13	8 10	2	28	43	42	<5	1.1	12	10	0.04	1.70	0.23	3 52	0.60	0.04	0.02	0.00
	- 1		[				- 1									- 1	I									0.04	V. V2	v
GWS-14	[	0.2	4	59	13	161	20	9	0.4	31	13	834	2	33	76	59	9	1.0	12	28	10.00	148	0.43	3.84	0.08	0.00	0.05	0.11
GWS-15		0.2	4	67	15	150	23	- 14	0.3	32	14	865	2	34	80	69	<5	1.1	14	20	0.04	1 50	0.43	4.00	0.07	0.00	0.00	0.11
GW\$-16		0.3	6	37	15	164	11	7	0.3	24	11	883	4	26	58	48	<5	13	17	22	0.07	1.60	0.70	1.00	0.70	0.00	0.03	0.12
GWS-17		0.3	4	26	12	144	<5	<5	0.2	22	12	518	2	24	56	44	<5	1 1	15	40	0.15	1.00	0.23	2.60	0.73	0.05	0.04	0.09
GWS-18	I	0.5	3	26	10	110	<5	5	0.1	25	14	965	-	25	50	51	-5	13	15		0.16	1.70	0.50	3.00	u.o/	0.09	0.14	0.08
								1					-			<b>•</b> '	~	1.0	<b>'</b> '		0. 10	1.48	0.52	3.65	1.05	0.10	0.15	0.08
GWS-19		0.4	3	22	6	151	<5	6	0.2	25	- 14Ì	704	- 21		50	أعم	أعر				<b>~</b> ~					1		I
GWS-20		0.3	2	18	5	71	<5	-5	40.1	20	13	736	2	20		40	<0	0.9	12	49	0.19	1.43	0.60	3.98	L 15	0.11	0.19	0.07
GWS-21		0.4	-	22		297	-5	7	-	000	- 22	1100	2	20	20 T	30	<0	0.(	8	3/	0.15	1.20	0.45	3.51	1.00	0.09	0.14	0.05
GWS-22	1	1.6	22	140	18	473	20	14	3.4		10	800				23	<0	11	ਿੱ		0.13	2.27	0.59	8.09	0.74	0.08	0.13	0.08
GWS-22*		1.4	22	141	10	478	201		37	70		842			00	<b>*</b>	<0	0.4	2	34	0.02	1.04	0.48	4.40	0.84	0.05	0.01	0.13
						ן"יי	~	- ''l	· · /	10	שי	043	4	ູຈາ		- 47	<5	0,4	5	37	0.02	1.07	0.49	4.62	0.86	0.05	<0.01	0. 14
				B	********			i	8					8	XXX-378	1	]		P	- K.S.	1	Ì		8		1	1	

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E KIMURA

**Geochemical Analysis** 

Project/Venture: Area;	1P COREY	Geol: Lab Project No.:	K TROCIUK D2440	Date Received: Date Completed:	JULY 22, 1992 AUG 5, 1892	Page Attn;	3 of K TROCIUK	
Remarks:							<b>J KOWLACHUR</b>	•
	a directed with Arris	egis and determined by Garphite Furnace A.A. (D.L. 1 PPB)					E KIMURA	

Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB) ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are sarely dissolved completely with this acid dissolution method.

SAMPLE	Au	Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	<b>. Y</b> .	Ba	w	Be	لعا	୍ୟ	n	A	Ca	Fe	Mg	K	Na	
No.	ppb	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<b>P</b> Pm	<b>ppm</b>	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	_%	<u>%</u>	_%		~%	<u>%</u>	- *	<u>%</u>
GWS-23		0.5	4	69	14	127	55	<5	<0.1	20	13	691	<2	24	45	34	<5	0.2	2	48	0.01	1.37	0.95	5.27	1.05	0.02	<0.01	0.14
GWS-24	1	1.1	19	154	18	677	33	7	4.8	88	19	887	2	30	56	58	<5	0.2	1	33	0.02	1.06	0.42	4.57	0.83	0.03	<0.01	0.14
GWS-25	1	NSS	NSS	NSS	NSS	NSS.	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS	NSS
GWS-26		0.4	4	70	13	99	25	<5	<0.1	22	10	649	~2	28	51	60	<5	0.2	3	24	0.03	1, 19	0.44	3.36	0.79	0.03	0.01	0.11
GWS-27		0.3	3	73	22	139	30	6	0.3	34	13	674	2	38	51	49	<5	0.6	6	37	0.05	1.34	0.54	3. 18	0.87	0.05	0.02	0.09
																1					1	1					1	- 1
GWS-28		0.3	5	96		162	23	9	0.7		17	648	2	35	61	41	<5	0.5	8	42	0.04	1.27	0.47	3.37	0.98	0.11	0.01	0. 12
GWS-29		03	<1	100	22	166	25	8	0.4	29	15	711	2	33	62	45	<5	0.5	6	40	0.04	1.39	0.72	3.28	1.10	0.17	<0.01	0.16
GWS-30		13	<1	109		200	23	7	0.4	52	15	969	2	42	46	60	<5	0.3	<1	94	0.03	1.71	1.06	4.09	L 16	0.03	0.01	0.10
GWS_31	ĺ	19	a	120	ts.	266	46	8	1.4	59	14	963	2	35	45	83	<5	0.2	1	26	0.02	1.14	0.40	4.03	0.85	0.02	<0.01	0.11
OWE_314		1.8		110	16	265	48	Ē	12	5A	14	950	0	35	45	86	<5	0.2	1	26	0.02	1.13	0.41	4.07	0.84	0.02	<0.01	0, 12
0110-01-		1.0		110				Ŭ					-															
0146 22				64		35	-5	-5	-0.1	77	17	244	0	105	70	192	6	0.3	11	53	0.09	1.24	0.57	3.22	1.10	0.46	0.02	0.14
040-02		0.2		25		24	~	-5	-01	7	7	247	0	24	36	134	<5	0.2	19	54	0.06	0.75	0.60	2.14	0.56	0.17	0.02	0.20
000-24		0.2		23		20	~~~		<0 1	13		164	2	24	58	79	<5	0.3	22	41	0.04	0.48	0.65	2.77	0.35	0.10	0.01	0.24
0110-04		0.1				16	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		-0.1	<b></b>		127	2	20	75	60	<5	0.3	17	39	0.03	0.37	0.46	3.47	0.27	0.11	0.01	0.16
GWS-05		0.1		- 22		10	~	3	~		, , , , , , , , , , , , , , , , , , ,	130		201	AA	73	-5	0.3	27	38	0.03	0.41	0.72	2.11	0.30	0.09	0.01	0.29
GWS-36		0,1	<1	8		ю	- 3	-0	×0.1		°		~	~	<u> </u>		~	0.3	- 1				V 2			0.00		0.20
OW9-97		-01	-1	+2	, s	15	-5	-5	<0.1	18	7	127	0	22	137	32	<5	0.2	19	27	0.02	0.21	0.55	6.25	0.14	0.06	0.01	0.21
GWS-39		0.7	2	97		17	-5	-5	40.1	14	13	169	a	29	60	72	<5	0.2	10	21	0.04	0.62	0.48	3.05	0.42	0.13	0.02	0.13
GW3-30		0.2	<u>د</u>	40		45	~5		-		7	120	3	24	TAD	31	-5	0.2	18	22	0.02	0.21	0.45	6.73	0.13	0.06	0.01	0.16
GWS-39		0,1		12		17		5	-0.1			138	2	24	171	20	- R	0.2	19	25	0.02	0.18	0.53	7.62	0 13	0.06	0.01	0.21
GWS-40		0.1		10			6	9	<0.1			126		27	SER.	26		0.2	40	57	0.00	0.17	0.51	7 34	A 11	0.05	0.01	0.20
GWS-40*		10.1	ן י>	12		01	<b>~</b> 3		<b>CO.</b> 1			130	~	~		20	~	<b>v</b> .e	~		0.00	v	0.01	1.04		0.00	0.01	0.20
				- 25		- 26	~	-	-0.1		7	172	0	24	45	44	<5	0.2	13	26	0.02	0.49	0.45	2.24	0.36	0.07	0.01	0.14
GWS-41		0,1		20								100		2.1	40	45		0.2	19	22	0.04	0.40	0.57	2 32	0.24	0.08	0.02	0.20
GWS-42		0.2	1	12		20	<b>G</b>	6	<b>CO. 1</b>			166	۲ v	21	76	28		0.2	25	20	0.02	0.28	0.63	3.35	0.22	0.05	0.01	0.25
GWS-43		0.1	2	10		23	<0					152	N X	26		20		0.0	28	23	0.02	0.23	0.76	5.46	0 18	0.04	0.01	0.31
GWS-44		0.1	3	10		20	<		-0.1		Å	166	2 4	22		27	7	0.0	27	23	0.02	0.29	0.74	4.02	0.24	0.05	0.01	0.30
GWS-45		<0,1	<1	11		20			<b>NO. 1</b>		v	~~	~				· ·	<u>۲. ۲</u>				0.20		1.04				0.00
0.000 4.0		-01	-1	10		02	~	-5	-01		5	144	-2	23	80	35	<5	02	21	22	0.03	0.34	0.56	3.03	0.29	0.06	0.01	0.21
GWS-40		<0.1					3				7	477	2			30	-5	0.2	+1	200	0.02	0.47	0.43	3 11	0.35	0.06	0.01	0 14
GWS-47		<0.1	4	20		20	<b>9</b>	<5	<0.1		- 4	102	N V		422	20		0.2	11		0.02	0.36	0.14	5.90	0.27	0.05	-0.01	0 12
GWS-48		<0.1	<1	21		21	<0	<0	<0.1			103	S A	27		67		0.2	18		0.02	0.67	0.54	2.07	0.45	0.00	0.01	0 10
GWS-49		<0,1	<1	14		41	<0	<0	<0.1		2	204	4			474		0.2	7	70	0.00	1.00	0.74	2.01	0.01	0.30	0.01	0.00
STD-P1		0.3	57	26	48	143	21	<∞	<0, 1	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	2	263	~	102	<b>.</b>	1/4	<0	0.4	[ 1		0.00	1.00	0.74	£.20	0.01	0.08	0.00	0.00
]																49	1 +0		<u>م</u>		ا مرما	0.80	0.20	471	0.63	0.04	0.04	0 10
GWS-50		1.3	3	161	36	226	- 39	14	0.7	CP CP	19	0/2	4	23		-0	12	0.4		~	0.02	0.00	0.20	3.47		0.04	0.01	0.00
GWS-51		2.5	12	111		223	28	10	1.5	62	14	404	2		~~	34		0.3			0.01	1.45	0.25	4.50		0.04		0.00
GW\$-52		0.6	1	113	12	173	25	<5	0.4		1/	836	V V	34			<0				0.02	1.40	0.43	4.00		0.03		0.14
GWS-53		0.9	14	133	17	403	32	<5	3.1	64	20	1146	~~	32	24 24	63	<0	0.0	1 🎽	CO.	0.02	1.10	0.41	5.30		0.01	0.01	0.14
GWS54		0.3	<1	158	15	106	36	<5	<0.1	25	20	937	2	24	₩¥	63	<3	0.8	f 9	100 sta	0.07	1.74	0.47	<b>3. 1</b> 8	P D	Ų.28	0.02	U. 13
{				5				۔ ۱	1								-	1	_ ۱		0	4 50	0.00			A 4F		A 44
GWS-55		0.1	1	104	9	101	25	<5	<0,1	43	18	8 19	4	30	66	50	<5	0.6	8	28	0.07	1.59	0.42	4.44	L 10	0,15	0.03	0.14
GWS-56	•••	0.2	2	86	12	113	19	<5	<0.1	47	17	838	2	34	54	34	<5	0.6	10	42	0.07	1.52	0.35	4.14	1.20	0,09	0.05	0.10
GWS-57		1.3	2	142	17	554	72	5	2.2	60	29	1847	4	24	65	48	<5	0.8	10	46	0.06	1.71	0,60	8.40	7.1	0, 10	0.06	0.18
GWS58	l	<0.1	1	87	7	69	7	্ব	<0.1	32	18	501	<2	36	75	120	ļ <5	Į 0.3	⁴	52	0.07	1.22	1.55	3.72	1.01	0.28	0.03	0.11
GWS-58*		0.1	<1	88	4	68	6	<5	<0.1	32	17	514	~2	35	74	126	<5	0.3	4	52	0.07	1.26	1.58	3.66	1.05	0.29	0.03	0,11
						L			L				L				L	L	I				L					

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Project/Venture:	1P	Geol;	K TROCIUK	Date Received;	JULY 22, 1992	Page	4	of	8
Area:	COREY	Lab Project No.:	D2440	Date Completed:	AUG 5, 1992	Attn:	K TRO	CIUK	
Remarks:				·			J KOW	LACHUK	
Au - 10.0 g sample	e digested with Aqua. Regia and determ	ined by Graphite Furnace A.A. (D.L. 1 PPB)					E KIM	JRA	
ICP = 0.5 a sample	digested with 4 ml Agus Regis at 100	Deg C for 2 hours							

ICP - 0.5 g sample digested with 4 mi Aqua Regia at 100 Deg. C tor 2 nours. N.B. The major oxide elements, Ba, Ba, Cr, La and W are rarely dissolved completely with this acid dissolution method.

SAMPLE	Au	Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	NI	Co	Mn	Bi	Cr	X I	Ba	w	Be	LA []]		ן ת	A	ି ଦଣ 🏻	Fe	Mg	- K	Na	P
Na	ppb	ppm	<u>ppm</u>	ppm	ppm	ppm	ррт	ppm	ppm	ppm	ppm	_ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm p	<u>m</u> ]	<u>×</u>	<u>%</u>	<u>_%</u>	<u>%</u>	*	%	%	*
GWS59		0.2	3	79	B	63	6	<5	<0.1	33	18	452	2	40	85	132	<5	0.4	6	54 (	) 80.C	1.29	1.07	3.93	1.02	0.29	0.04	0.11
GWS-60	i i	0.4	<1	41		40	<5	ব্য	<0, 1	23	12	296	2	35	64	80	<5	0.3	10	32 (	0.05	0.87	0.49	3.07	0.69	0, 13	0.02	0.10
GWS-61		1.3	j 14	122		446	- 34	6	3.2	82	25	1172	- 4	29	71	540	<5	0.9	19 🛞	51 (	D. 14	1.68	0.49	5.31	1.13	0,11	0.10	0.14
GWS62		2.7	41	205	64	837	53	49	7.8	88	29	1364	~2	21	38	99	<5	0.6	11	23 (	0.02	0.82	0.27	5.51	0.58	0.05	0.01	0.14
GWS-63		1.7	28	159	- 77	583	46	24	4.7	75	23	986	2	21	34	111	<5	0.6	11	22 (	0.02	0.71	0.25	4.97	0.49	0.04	0.02	0.12
			Į –	{																								
GWS-64		2.3	36	194	79	768	52	34	6,9	88	26	1261	- 4	21	37	113	<5	0.5	10 📖	23 (	0.02	0.80	0.27	5.46	0.56	0.05	0.01	0.14
GWS-65		0.8	10	114	47	204	41	ব	0.9	62	19	8 19	3	30		59	<5	0.4	9	40 0	0.02İ	1, 10	0.45	4.61	0.97	0.07	<0.01	0.13
GWS-66		0.3	L 5	94		153	23	8	0.5	57	18	909	2	63	82	96	<5	0.5	9	103 0	3.04 l	1.48	2.36	4.28	1.44	0.11	0.01	0.22
GWS67		1.0	6	88	25	422	22	5	3.1	57	16	1003	2	25	45	69	<5	0.5	14	81 (	0.04 l	1.22	1.76	4.26	0.92	0.09	0.01	0.15
GWS-67*		0.9	7	86	23	4 19	19	5	3.0	55	15	993	2	23		65	<5	0.5	14	81 (	0.04	1, 19	1.72	4, 19	0.90	0.09	0.01	0.15
				11				Ī			[]																	
HCS-1		0.1	4	69	14	90	16	- 61	<0.1	27	17	763	0	36		55	ا م	0.4	g 🕅	23 (	2.04	1.55	0.38	4.76	<b>11</b> 8	0.05	0.00	0 13
HCS-2		0.2	5	72	17	B4	44	- 6	<0.1	24	16	003	0	29	<b>1</b>	46	-5	0.5	11	32 0	007	1.41	0.43	4 25	1.12	0.06	0.04	0.13
HCS-3		0.1	3	70	23	79	18	-5	<0.1	97	18	719	0	35	8 T.	62	-5	0.5	10	22 0	104	149	0.35	4 76		0.05	0.02	0.13
HCS-4		-01	3	80		74	16		-01	25	17	678		31	50	80	-	0.5			1 02	1.58	0.81	4.80		0.05	-0.01	0.10
HCS-5		-01		87	- 16	70	21		-0.1		16	710		34	70	50		0.5	10	37	0.02	1.00	0.01	4.00		0.00	0.01	0.10
1100-0				. "					<b>CO.</b> 7			1.00	¥.	~		39		0.0		88 I		1.40	0.00	4.25		0.00	0.01	0.14
HCS_6		0.2	5	68		83	12		-01	100 Ha	14	874	2	22	60	82	-5	0.5	44	าลได	أدمد	1 90	0.01	4 17		0.08	0.04	0.15
HCS-7		0.1	اي ا	24	17	136	17		-01		12	1000		17	5	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		0.0	45	24	100	1.00	0.01	5.07	0.00	0.00	0.01	0.13
		0.1		28		110	18		~ 1		12	1/10.9		10		82	-6	0.0		24		0.07	0.02	3.07	0 70	0.00	0.03	0.13
HCS_0		0,1	5	43	22	170	10				10	12 10	<u> </u>	23	201	65		0.7			1.001	1.50	0.20	5.40	0.70	0.08	0.08	0.07
HCS_0*		0.2		42		168	14			2	10	1108	-	20		67	<0 -6	0.0				1.00	0.54	5.12	1.20	0,11	0,10	0.10
100-0		V.E	] 7	<b>*</b>			, m				"	1 1 1 1 1 1 1 1						0.7		34 `	. <b>19</b>	1.40	0.53	9.02		0, 11	0.10	0.09
HCS-10		0.8	2	38	-	194	5	-5	-01		201	074	-	25	60	60		10	25	47 0	n 46	172	0.54	4.04	4.74	0 10	0.17	0.00
HC8_11		0.5	5	77	40	143	16	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	0.1	70	26	875	~	07			-5	1.0				240	0.04	4.00	1 60	0.10	0.17	0.08
HCS-12		0.0	5	21	46		R	اتم ا	-0.1		201	1001	-	21	00	57		1.0	40			1.02	0.82	4.00	1.00	0.12	0.06	0.06
HCS_13		0.1		49	14	111	42				21	060	×,	20		40		1.0			0.20	170	0.07	4.20	0.04	0.11	0.21	0.00
HCS_14		0.2		<b>1</b>	17	116	52	~		66	12	711		40		50		0.8	10	19	200	1.78	0.20	4.40	0.00	0.00	0.05	0.00
		0.1	1	<b>''</b>	<u> </u>		U.S.		-0.1		· *			· ~	20 <b>7</b> 9	~		0.7	· · · · ·	¥ `	.uz	1.05	0.24	3.73		0.04	0.01	0.10
HCS-15		0.1	l ,	26	- 12	مما	225	ه ا	-	30		707		34	Bal	50	ا مر	0.0	45	<u></u>	امەر	160	0.50	3.67	0.02	0.06	0.04	0.09
		0.4		20		101	25	, š	1 4	<b>1</b> 0	10	1657		20	<b>11</b>	87	-5	1.0		52	0.07	1.67	0.00	4.45		0.00	0.00	0.00
HC6. 17		0.4	]			101	40		1.3		12	1007	X V	20		0/	<0	1.0		23	.07	1.07	0.34	4.40	0.04	0.07	0.00	0.09
HCS-18		0.3				240	43		1.2			1797		21	88 <b>3</b>		<0 -5	0.9			.04	1.40	0.30	4.40	0.05	0.00	0.03	0.10
HCC_188		0.1		30		240	40		47		12	1700	N V	20	8875	101		0.8				1.55	0.33	3.03	0.10	0.07	0.02	0.12
10.0-10		0.7	<pre>4</pre>			278		"	1.7		<b>1</b> 3	1108	~~	20			<0	0.9	••	881	J.US	1.48	0.32	4.80	U.00	0.07	0.02	0.12
HC9_10		0.1				120	•		~ ~			1104	ا م	~		أرج	ام ا		<b>1</b> 0	20	<u></u>	4 EE		2 05			0.07	0.00
		-04	1 22			108	45	ارت ا	0.4			1445	3	3.	80° 1	14		U.8	14			1.00	0.34	3.03	0.84	0.03	0.07	0.08
100-20		<b>₹</b> 0,1	1 1	28		114	10		0,4	200 C		704		201			6	1.0		<u>مع</u> (	.00	1.40	0.33	3.07	U.04	0.03	0.00	0.07
109-21		0,1		30	39 20			40	-0.1	33		/01	<u> </u>	34	21		<3	1.2				1.75	0.35	3.60	U.84	0.07	0,10	0.08
103-22		<0.1		34		474	44		<0.1			021	9	20	04		6	0.0		28 0		1.42	0.44 (	3.71	<u>u.a</u> (	0.00	0.04	0.12
HCS-23		0,1	( ¥	<b>4</b> 2	ાગ	1/4	11	טי ן	0.5	33	22	\$20	3	24	01	57	<>	0.8	13 👸	20	າເເສ	1.45	0.39	4.81	0.94	0.06	0.05	0.10
1000 04							-	أمدا									ا ہے ا		- <b>.</b> [33	S .	امہ	1	l				0.00	A 40
100-24	<i></i>	0,1		3/		02	5	13	<0.1	18	12	729	4	Nor Contract of Co	<u> </u>	69	3	U.5		#2  (	1.00	1.55	0.45	4.64	103	0.041	0.03	0.12
105-20		<0.1	2	20	<b>10</b>	113	<0		<v. 1<="" td=""><td>() <sup>30</sup></td><td>10</td><td>044</td><td>~</td><td>30</td><td><b>D</b>0</td><td>80</td><td>&lt;2</td><td>0.9</td><td>L 72</td><td>20 (</td><td>.09  </td><td>1.51</td><td>0.40</td><td>3.91</td><td>0.83</td><td>0.06</td><td>0.06</td><td>0.09</td></v.>	() <sup>30</sup>	10	044	~	30	<b>D</b> 0	80	<2	0.9	L 72	20 (	.09	1.51	0.40	3.91	0.83	0.06	0.06	0.09
105-20		0,1	2	20	<b>T</b>	106	<0	<3	<0.1	a	<b>G</b> I	1693	2	20	<b>46</b> ]	86	<0	0.9	12	30 0	roal	1.49	0.36	4.49	0.81	0.05	0.07	0.08
HC3-2/		0.3		38		143	01	10	0.2	37	15	EPUT	5	30	49	55	<b>S</b>	U.8	<u> </u>	ାଧା (	1.00	1.73	0.33	5.00	1, 10	0.04	0.04	0.11
SID-P1		0.2	66	27	56	145	20	6	0.2	37	6	577	~	121	<b>34</b>	177	<5	0.5	7	64 (	111	1.07	0.91	2.29	0.86	0.37	0.07	0.08
	ليستعد	L	1	نــا			L	ليــــــا	L		L	I	ل	ئى						<u></u>	_1		<u>i</u>			1		

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Project/Venture: Area:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2440	Date Received: Date Completed:	JULY 22, 1992 AUG 5, 1992	Page Attn:	5 K TROC	of IUK	8
Remarks:							1 KOWL	ACHUK	
Au - 10.0 g sample	e digested with Aqua. Regia and de	ermined by Graphite Furnace A.A. (D.L. 1 PPB)					E KIMU	RA	

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ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are sarely dissolved completely with this sold dissolution method.

SAMPLE	Au	Ag	Mo	Cu	РЬ	Zn	As	Sb	Cd	NI	Co	Min	BI	Cr	Y	Ba	W	Bø	إعفا	Sr	ן ת	AI	Ca	Fe	Mg	- K [	Na	P
No.	ppb	ppm	_ppm	ррлт	ppm	ppm	ppm	ppm	ppm	ррт	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	_%	<u>%</u>	<u>%</u>	<u>%</u>	- %	<u>%</u>	<u>%</u>	%
HC\$-28	t l	0.9	2	107	10	174	19	5	0.5	39	16	774	2	39	80	127	<5	0.4	8	44	0.06	1.56	0.63	4, 19	1.28	0.12	0.02	0.16
HCS-29		0.7	3	109	11	168	18	<5	0.4	38	17	771	6	38	67	122	্ৰ 🕹	0.5	8	47	0.07	1.57	0.68	4,49	1.31	0.12	0.02	0.16
HCS-30		0.6	5	120	13	191	17	7[	0.7	45	18	859	8	43	85	124	<5	0.5	9	51	0.07	1.61	0.64	4.45	1.44	0.10	<0.01	0.16
HCS-31		0.1	<1	127	÷**9	78	<5	<5	<0.1	18	20	815	5	23	105	312	<5	0.7	8	67	0.13	1.94	1.09	4.24	1.55	0.68	0.02	0.22
HCS-32		<0.1	1	117		69	8	<5	<0.1	19	19	817	8	24	104	215	< গ	0.8	7	70	0.11	1.60	1.00	4.94	1.40	0.60	0.01	0.21
	]			• •								• • •	_															
HC8-33		04	-1	80		118	10	-5	02		11	639	3	31	71	60	~	0.3	7		0 10	1 37	0.50	3.85	0.01	0.04	0.03	0.00
UC8_34		9.5		166		253	16	19	97	- <b>1</b> 00		443	5	48	200 A 2	32		0.3		42	-0.01	1 14	0.00	4 17	1.10	0.00	-0.01	0.00
103-34		0.0	10	114		355	30	-5	-0.1		47	770	, s	27	20	70		0.0			0.00	1 2 2	1.45	4.40		0.00	0.01	0.15
100-00		0.4		114			00		CU. 1			110	5			10		0.7			0.00	1.02	1.40	4.05		0.10	0.01	0.10
10.3-30		0.2	10	140	000 P		20	8	<u, i<="" td=""><td><b>Option</b></td><td>31</td><td>870</td><td>5</td><td>204</td><td>္ကားမွာ</td><td>N I</td><td>6</td><td>0.5</td><td></td><td>1 <b>4 7</b></td><td>0.10</td><td>2.70</td><td>0.43</td><td>4.84</td><td>2.01</td><td>0.44</td><td>0.05</td><td>0.09</td></u,>	<b>Option</b>	31	870	5	204	္ကားမွာ	N I	6	0.5		1 <b>4 7</b>	0.10	2.70	0.43	4.84	2.01	0.44	0.05	0.09
ן ויי-טוצן		0,3	60	20		147	<b>U</b> T	ୖ	0.2	- 30	4	5/9	כ		30	1/1	<b>○</b>	0.5	8	S 18	ן טר. ט	1.05	0.86	2.31	0.87	0.38	0.06	0.08
[													_															
]HCS-37 ]		0.6	13	215	(1) (1) (1) (1) (1) (1) (1) (1) (1) (1)	214	37	8	<0.1		64	1589	5	59	121	173	12	0.8	12	26	0.24 ]	3.22	0,41	5,52	1.83	0.68	0.08	0.13
HCS-38		0,4	22	226	32	204	35	9	<0.1	48	69	1804	- 4	63	143	200	24	0.8	12	20	0.23	3.28	0.32	5.40	1.89	0.73	0.05	0.12
HCS-39		0.3	10	125	25	122	13	11	<0.1	47	26	756	- 4	55	106	153	) 8]	0.8	12	36	0.19	2.50	0.40	4.99	1.46	0.45	0.07	0.12
HCS-40		0.3	12	101	15	106	7	<5	<0.1	105	19	530	2	73	71	100	ব	0.5	8	17	0.13	2.03	0.24	4,41	1.80	0.30	0.03	0.10
HCS-41		0,1	1	61	2	81	8	<5	<0.1	46	15	4 16	2	46	75	96	<5	0.5	11	<b>1</b>	0.12	1.73	0.57	3,52	1.05	0.25	0.04	0.14
1											i l						ļ										· · · · · ·	
HCS-42		<0.1	2	38	<b>1</b>	41	<5	5	<0.1	17	11	279	2	29	105	81	্ৰ ব	0.3	17	32	0.07	0.76	0.64	4,49	0.51	0.17	0.03	0.21
HCS-43		0.1	2	57	10	71	12	<5	<0.1	31	15	375	<2	41	78	100	<5	0.3	8	42	0.10	1.59	0.63	3.73	0.83	0.28	0.05	0.14
HCS-44		<0.1	2	29	80 Ce 1	41	5	5	<0.1	7	10	268	2	28	72	75	< ব	0.3	13	37	0.07	0.85	0.66	3.24	0.52	0,16	0.03	0, 19
HCS-45		<0.1	2	32	88 M (	34	<5	<5	<0.1	13	8	236	0	26	83	59	8	0.3	12	38	0.08	0.70	0.67	3 55	040	0.12	0.03	0.20
HCS-45*		0.1	2	31		33	<5	<5	<0.1		8	227	2	27		58	21	0.2	13	37	0.06	0.66	0.69	3.84	0.38	0 12	0.03	0.21
		••••	-								-			-										4.41		<i>v</i>		U. <u>.</u> ,
HCS-46A		0.4	<1	22	5	31	10	7	0.4	13	7	170	2	22	12	55	6	0.6	21	63	0.05	0.68	0.79	1 73	0 36	0.08	0.02	0 19
HCS-46B		04	8	20		38	<5		-0.1	45		231	0	28		57	10	0.2	20	886 I.S.	0.07	0.75	0.80	3 32	0.45	0.11	0.03	0.28
HC8-47		4.8		147		70	-5	~~	~		1 1	304	~			74		0.2	5	000 TE	0.10	0.53	0.08	4 /10	<b>1</b>	0.11	0.00	0.10
1100 41		10	2	444		144	<b>E</b> 4		0.4			467		104		81		4.4	10		0.15	0.07	0.00	0.72	4 40	0.10	0.11	0, 12
1100-10		1.0 1.5							0.0		21	931		107		01				01	0.13	0.04	0.4/	0.73		0.00	0.00	0.12
ILC9-49		1,9	<1 <1	**	88 C	- 04	¥	l 'I	0.2		•	201	~~	115				8. 1	10	0<	0.24	0.92	0.75	U.04	2.23	0.13	0.19	0.12
404-50		20	-1	88		#5	44		0.2			200		07	nn.	52		00	42		0 12	0.20	0.50	0.08		0.00	0.07	0.10
1103-00		2.0						ائد ا	-0.4			70				50		0.8	10	· · · ·	0.15	0.30	0.00	0.80		0.00	0.07	0.10
HC5-51		0.3	<1	44			19	<b>C</b> 0	<0.1		2	10	2	00	14 <u>4</u>	30	6	0.9	13	<b>04</b>	0.30	0.34	1.00	1.04	1.00	0,18	0.34	0.11
HC5-52		0.8	<1	78		04	40	8	0.1		, and the second s	1036	~~	94	108	81	<b>Q</b>	0.9	12		0.16	0.69	0.69	1.25	1./0	0,10	0,12	0,13
HC5-53		1.0	<1	112		61	5	<ol> <li>S</li> </ol>	<0, 1	50	12	379	~2	200	120	60	6	0.7	9	40	0.21	1.34	0.86	2.02	2,15	0.08	0.07	0.11
HCS-53*		0.9	<1	111	6	58	<5	<5 5	<0.1	49	11	372	2	192	1 19	56	ি ক	0.6	8	37	0.20	1.29	0.81	1.99	2.18	0.08	0.07	0.10
							_										l I											
HCS-54	!	0.7	[ <1]	86	15	139	77	<5	<0.1	81	25	1167	2	103	90	62	<5	0.8	11	38 [	0.11	2.90	0.80	4.27	171	0.07	0.05	0.11
HCS~55		1.2	3	94	30	176	107	8	0.2	68	28	1591	<2	90	107	65	6	1.1	15	33	0.12	2.92	0.67	4.68	1.52	0.08	0.06	0.14
HCS-56	l	0.6	3	53	24	137	244	9	<b>&lt;</b> 0. †	65	25	1225	2	108	155	47	ব	1.2	17	38	0.18	3.56	0.88	5.00	1.50	0.08	0.09	0.12
HCS-57		1,0	3	65	23	152	96	6	<0.1	53	14	780	<2	73	104	53	ସ	1.4	17	22	0.13	2.46	0.56	4.30	1.00	0.06	0.04	0,10
HCS-58		1.6	<1	109	22	196	51	8	0.1	72	27	1282	2	84	107	64	<5	0.9	11	38	0.20	2,74	0.63	5,11	1.87	0,10	0.13	0.11
HCS-59	l	0.3	39	367	a an	122	5	<5	⊲0,1	31	19	866	10	41	169	163	75	0.7	5	18	0.24	3.10	0.37	8.60	2.14	1.27	0.04	0.20
HCS-60	1.11	0.1	25	330		96	<5	<5	<0.1	27	12	561	4	47	152	104	51	0.5		16	0.20	2.47	0.29	7.41	175	0.96	0.02	0.16
HCS-61		0.2	35	295		1 100	<5	- K	×0 ×	20	i iil	590	R	أمها		15.2	50	0.5			0.21	2.56	0.34	8 11	1 84	102	0.04	0.18
Luce_en		0.1		327		74	7	اير ا	-0.1		51	405	7	35	000	50	110	04		25	0.14	100	0.58	8.63	1 17	0.57	0.07	0.16
100-02		0.1	1.1	904		1 5		ام <sup>ح</sup> ا	-0.1			404	<b>'</b>		00 CO	40				<u>یک کہ ا</u>		1.00	0.00	0.00		0.0/	0.00	0.10
nua-02-		0.2	14	324		13		•	<u, 1<="" td=""><td></td><td>-0</td><td>401</td><td></td><td>33</td><td>ಿಕಿಂ</td><td> /</td><td></td><td>0.4</td><td>3</td><td>88 <b>°</b> 1</td><td>0.14</td><td>1.01</td><td>0.94</td><td>0.4/</td><td>- H K</td><td>0.55</td><td>0.00</td><td>0.14</td></u,>		-0	401		33	ಿಕಿಂ	/		0.4	3	88 <b>°</b> 1	0.14	1.01	0.94	0.4/	- H K	0.55	0.00	0.14
	Ļ	L		L	200 - 200 - 20 - 200 - 20	أسرب المرا			_					L	96.260.00		است. ما	L		2 2075 5			L.		100000000			ليبيني

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Project/Venture:	1₽	Geol;	K TROCIUK	Date Received:	JULY 22, 1992	Page	6	of	8
Area:	COREY	Lab Project No.:	D2440	Date Completed:	AUG 5, 1992	Attn:	K TROC	IUK	
Remarks:							J KOWI	ACHUK	
Au – 10.0 g sampi	e digested with Aque, Regis and deter	mined by Graphite Furnace A.A. (D.L. 1 PPB)					E KIMU	RA	

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ICP - 0.5 g sample digested with 4 ml Aqua Regia and determined by Glaphite Fundoe X.A. (O.E. FFFB) ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are tarely dissolved completely with this acid dissolution method.

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MA         PP         PP<	SAMPLE	Au	Ag	Mo	Cu	Pb	Zn	As	Sb	Cđ		Co	Mn	BL	Cr	¥.	Ba	W	Be	LA	ଁ ହା	ินไ	- AL [	Cal	Fe	i Mg	K	Na	P
HCS=A3         L2         L3         L2         L3         L2         L3         3         L3 <thl< td=""><td>No.</td><td>ppb</td><td>ppm</td><td>ppm</td><td>ррп</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>1mqq</td><td>ppm 🖉</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ppm</td><td>ррт</td><td>ppm</td><td>%</td><td>%</td><td>%</td><td>%</td><td>~ % ~</td><td>_ % ]</td><td>%</td><td>%</td></thl<>	No.	ppb	ppm	ppm	ррп	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	1mqq	ppm 🖉	ppm	ppm	ppm	ppm	ррт	ppm	%	%	%	%	~ % ~	_ % ]	%	%
HGB-44         Li2         3         36         12         36         12         36         12         36         12         36         12         36         12         36         12         36         12         36         12         36         12         36         16         55         65         65         65         65         66        66         66	HCS-63		0.3	12	436		108	<5	ు	<0.1	34	63	444	4	30	75	31	180	0.6	5	21	0.11	1.43	0.54	8.56	0.85	0.48	0,04	0.11
HC3-65       22       20       407       20       20       40       12       45       60       42       12       45       60       42       12       45       60       42       12       45       60       42       12       45       60       42       50       62       63       85       46       45       60       42       10       65       60       62       63       85       64       65       60       63       65       60       65       60       65       60       65       60       65       60       65       60       65       65       65       65       65       65       65       65       65       65       65       65       66       65	HCS-64	) 1	1.2	) 3	295	18	302	< 5	<5	0.8	26	35	1224	7	37	130	450	6	0.4	4	21	0.16	2.25	0.39	6.43	1.78	1, 17	0.03	0.13
HOG-R0         Q.01         1         10         6         80         9         Cd.         Q.1         2         10         Q.0         Q.2         31         BS         40         S5         Q.1         11         Q.00         Q.00         Q.01         Q.11          HCS-H0A         Q.2         C1         BS         D.1         BS         D.1         BS         D.1         BS         D.1         D.1 <thd.1< th=""> <thd.1< th=""></thd.1<></thd.1<>	HCS-65		2.2	20	407	29	234	33	6	1.2	36	26	687	5	21	50	21	<5	0.5	9	37	0.04	1.00	0.91	8.21	0.79	0.06	0.01	0.13
HCS-47       0.1       2       65       6       9       9       45       6.1       21       14       55       6.1       21       14       55       6.1       21       14       55       6.1       57       67       23       15       640       45       100	HCS-66	[ ]	<01	1	70		60	9	<5	<0.1	9.94	15	604		33	65	44	<5	0.7	12		0.07	1.38	1.03	4.05		0.08	0.01	0.14
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	HC9_67		0.1	2	65		60	10	-5	-01	88 <b>5</b> 4	14	558	0	31	<b>85</b>	40	<5	0.6	50	885	0.07	129	0.94	4.51	4.00	0.06	0.01	0.15
HCS-BAB         0.1         4         600         55         11         55         5         5         11         90         477         2         33         65         44         45         0.5         900         14         0.70         120         130         0.65         110         150         110         100         100        100         100 <t< td=""><td></td><td></td><td>0.1</td><td>· ^</td><td>~</td><td></td><td>~</td><td></td><td>~</td><td></td><td></td><td></td><td>~~~</td><td>-</td><td>- <b>*</b> •</td><td></td><td></td><td>~</td><td>v</td><td></td><td></td><td></td><td></td><td></td><td>4.91</td><td></td><td>v</td><td>0.01</td><td>0.10</td></t<>			0.1	· ^	~		~		~				~~~	-	- <b>*</b> •			~	v						4.91		v	0.01	0.10
$ \begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 $					400		440	15	_			47	667		a 4 🕅	ar I	40					0.00	- 4 4 4	0.70	4 00		0.05	0.00	0.40
Trace-sum         Color	100-00		0.1				400	10		<b>NO. 1</b>		10	701		40		40		0.8	17		0.00	1.77	0.70	9.20		0.00	0.05	0.10
$ \begin{array}{c} \begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	HUS-09A		0.2	!</td <td>- <b>20</b></td> <td></td> <td>102</td> <td>19</td> <td><b>°</b></td> <td>0.1</td> <td>4</td> <td>12</td> <td>721</td> <td></td> <td>30</td> <td><b>9</b>2</td> <td></td> <td>60</td> <td>0.5</td> <td>10</td> <td>ಿಂದ</td> <td>0.05</td> <td>1.12</td> <td>0.51</td> <td>3.82</td> <td>0.94</td> <td>0.05</td> <td>0.02</td> <td>0.14</td>	- <b>20</b>		102	19	<b>°</b>	0.1	4	12	721		30	<b>9</b> 2		60	0.5	10	ಿಂದ	0.05	1.12	0.51	3.82	0.94	0.05	0.02	0.14
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	HC3-098		0.3		111		105	20	8	0.0	20 × 0	20	00/		29		32	6	0.4	•	8 8 P	0.05	1.10	0.90	4,40	₩.#/A	0.07	0.01	0.15
HGS-70*       0.3       <17       0.1       11       0.3       19       c5       0.1       0.6       670       c2       31       622       64       65       0.4       8       39       0.64       1.00       0.56       0.56       0.77       0.6       0.57       0.58       0.57       0.48       0.44       0.57       0.48       0.44       0.57       0.48       0.44       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.46       0.57       0.56       0.52       0.77       0.46       0.57       0.56       0.57       0	HCS-70		U.3		70		105	19	3	<0.1		11	670	Z	31	<b>P3</b>	47	<3	0.4	v	880 L	0.05	1. 14	0.57	3.96	0.000	0.05	0.01	0.14
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	HCS-70*		0.3	<1	70		103	19	<5	<0.1	<b>30</b>	10	679	< 2	31	62	46	<5	0.4	8	್ಷಿತಿ	0.04	1.09	0.56	3.88	0.87	0.05	0.01	0, 14
HGS-71       0.4       6       72       22       121       20       9       0.2       26       11       860       22       31       60       53       22       0.4       8       44       0.77       1.46       0.44       0.06       0.03       0.12         HCS-73       0.2       67       20       12       34       62       45       64       37       33       22       66       57       65       10       16       63       0.22       1.77       0.44       0.06       0.03       0.02       0.02       0.02       0.02       0.03       0.04       0.06       0.03       0.04       0.00       0.06       0.00       0.01       0.00       0.01       0.00       0.01       0.00       0.01       0.00       0.01       0.01       0.01       0.01       0.02       0.02       0.02       0.02       0.02       0.02       0.01       0.01       0.01       0.01       0.02       0.02       0.02       0.01       0.01       0.02       0.02       0.02       0.02       0.02       0.03       0.01       0.01       0.01       0.00       0.00       0.01       0.01       0.01       0.01       0																					88 C							·	
HGS-72       0.1       7       67       12       130       12       45       0.4       14       55       0.2       0.55       0.27       0.06       0.05       0.27       0.06       0.05       0.27       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.10       0.06       0.07       0.02       0.06       0.07       0.06       0.07       0.07       0.07       0.07       0.07       0.06       0.07       0.07       0.02       0.07	HCS-71		0.4	6	72	12	121	20	8	0.2	26	11	560	2	31	60	53	22	0.4	8		0.07	1. 19	0.77	3.48	0.94	0.05	0.03	0, 12
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	HCS-72		0.1	7	67	12	138	12	<5	0.5	45	9	483	2	65 🛛	56	88	- 5	0.4	8	40	0.06	0.93	0.55	3.27	0.76	0.04	0.02	0. 12
HCS-74       0.2       11       30       18       136       55       6       0.1       21       14       10       21       23       21       23       21       23       21       23       21       23       21       23       21       23       21       23       21       23       21       23       21       23       21       23       21       23       21       23       23       20       21       20       21       20       20       20       20       20       20       20       20       20       21       20       20       20       20       20       21       20       21       21       21       21       21       21       21       21	HCS-73		0.2	16	20	12	84	82	<5	<0.1	24.	15	713	3	22	69	57	<5	1.0	15	53	0.22	1.72	0.64	4.09	1.13	0.09	0.19	0.09
HCS-75       0.1       9       41       70       182       77       27       21       46       59       c5       10       34       0.07       1.42       0.41       4.83       0.08       0.04       0.03       0.12         HCS-76       0.2       10       16       6       109       11       c5       0.1       45       9       431       c2       38       39       106       c5       1.0       10       16       0.02       1.52       0.23       1.48       0.04       0.02       0.06       0.02       1.52       0.23       1.45       0.03       0.44       0.03       0.14       0.02       1.00       17       29       9       102       c2       21       11       22       55       0.6       17       0.22       0.03       0.44       0.03       0.15       0.03       0.16       0.33       10.13       10.13       10.13       10.13       10       10       12       11       1076       c2       28       38       131       15       0.23       0.33       10.20       10.33       10.20       10.33       10.20       10.23       10.20       10.20       10.20       10.20	HCS-74		0.2	11	30	18	136	55	6	<0.1	21	14	1 193	<2	22	51	111	<5	1.1	19	<b>41</b>	0.10	1.97	0.53	4.56	1.02	0.06	0.07	0, 10
HCS-76       0.2       10       18       5       100       11       -5       -0.1       45       9       431       -2       38       38       100       -15       1.52       0.23       4.18       0.00       0.02       0.00       0.02       1.52       0.23       4.18       0.00       0.02       0.00       0.03       3.44       0.46       0.00       0.02       0.03       3.44       0.46       0.02       0.03       3.44       0.46       0.02       0.03       3.44       0.46       0.02       0.02       0.03       3.44       0.46       0.02       0.02       0.03       3.44       0.46       0.02       0.02       0.03       3.44       0.46       0.02       0.02       1.52       0.03       3.44       0.47       0.2       4.3       3.3       1076       c2       2.83       131       105       1.40       0.42       2.25       0.66       0.60       0.10       0.07       1.33       44       4       1020       2.5       133       2.35       1.65       0.7       12       1.40       0.42       2.25       0.66       0.60       0.30       0.66       0.30       0.66       0.30       0.66	HCS-75		0, 1	9	41	10	182	13	<5	0.5	26	11	776	2	21	48	59	<5	0.5	10	34	0.07	1.42	0.41	4.83	0.93	0.04	0.03	0, 12
HCS-76       0.2       10       16       8       100       11       c5       0.1       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       11       10       10       11       10       0.02       1.52       0.03       1.45       0.03       0.46       0.00       0.02       0.02       0.02       0.02       0.02       0.02       0.02       0.02       0.02       0.02       0.02       0.02       0.03       1.45       0.73       0.04       0.02       0.02       0.03       1.45       0.73       0.04       0.02       0.02       0.03       1.45       0.03       1.55       0.03       0.05       0.03       0.06       0.02       0.02       0.03       0.04       0.02       0.02       0.03       0.06       0.02       0.03       0.06       0.03       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06			•											1									1						]
HCS-77       0.1       9       35       9       5       0.2       25       10       913       -2       47       37       77       72       -65       0.6       6       17       0.22       1.30       0.30       3.44       0.60       0.04       0.02       0.08         HCS-79       0.1       10       17       12       94       -5       -65       -65       -65       -65       -66       13       28       0.33       1.46       0.27       0.08       0.38       0.70       0.22       0.03       0.04       0.02       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.02       0.08       0.70       0.22       0.07       0.34       0.06       0.02       0.08       0.70       0.21       110       18       31       0.1       16       0.31       0.12       0.10       0.06       0.01       0.07       0.02       1.0       18       31       0.1       10       10       18       31       0.1       10       12       10       10       10       10       10       10       10       10       10       10       10	HCS-76		0.2	) 10]	18	8	109	11	<5	<0.1	45	9	431	<2	38 🔯	38	108	<5	1.0	10	18	0.02	1.52	0.23	4.18	0.69	0.03	0.02	0.06
HCS-78       0.1       7       29       9       113       9       6       0.1       42       16705       -2       34       38       79       -25       0.7       6       15       0.03       145       0.27       381       0.73       0.04       0.02       0.08         STD-P1       0.2       58       26       54       141       20       -5       0.3       32       11       176       -2       28       38       131       -5       1.0       16       31       0.12       1.4       0.06       0.06         HCS-80       0.1       4       26       12       136       15       -5       0.3       32       11       1076       -2       28       38       131       -5       1.0       16       31       0.12       1.40       0.42       3.25       0.66       0.03       3.00         HCS-82       0.2       3       31       12       136       14       15       0.5       0.1       140       0.5       0.1       0.5       0.3       3.00       0.03       0.07       12       12       0.00       14       4.5       0.16       0.33       0.30       <	HCS-77		0.1	9	35		128	9	5	0.2	53	10	913	2	47	37	72	<5	0.6	8	17	0.02	1.30	0.30	3.44	0,80	0.04	0.02	0.09
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	HCS-78		0.1	7	29	9	113	9	6	0.1	42	\$6	1705	<2	34 🖗	38	79	<5	0.7	9	<b>15</b>	0.03	1.45	0.27	3.81	0.73	0.04	0.02	0.09
STD-P1       0.2       58       26       54       441       20       <55       0.3       36       6       568       <2       111       22       165       <5       0.4       6       72       0.00       0.63       0.79       2.25       0.79       0.34       0.06       0.06         HCS-80       0.1       3       44       8       12       136       15       <55	HCS79		<0.1	10	17	12	94	<5	<5	<0.1	32	9	402	4	31	42	44	<5	0.8	13	29	0.13	1.80	0.38	3, 15	0.73	0.08	0.12	0.10
HCS-80       0.1       3       H4       6       120 $< d_5$ $d_5$ 0.3       3.2       11       1076 $< d_2$ 28       38       131 $< d_5$ 10       16       31       0.12       140       0.42       3.25       0.66       0.0       0.0         HCS-81       0.2       4       26       12       138       15 $< d_5$ 0.3       3.5       6       667 $< d_2$ 32       42       61 $< d_5$ 0.7       12       14       0.03       1.57       0.24       3.73       0.77       0.06       0.03       0.06       0.0       0.06       0.00       0.06       0.00       0.06       0.01       0.06       0.01       0.06       0.01       0.06       0.01       0.06       0.01       0.05       0.03       0.02       0.77       13       31       0.61       111       123       22       20.83       21       75       66       55       <5       0.66       8       22       0.06       8.8       22       2.64       132       32       0.10       14       0.52       0.16       0.21       0.44       4.55       0.33 <th< td=""><td>STD-P1</td><td></td><td>0.2</td><td>58</td><td>26</td><td>54</td><td>141</td><td>20</td><td>&lt;5</td><td>0.3</td><td>36</td><td>. 6</td><td>568</td><td>2</td><td>111</td><td>28</td><td>165</td><td>&lt;5</td><td>0.4</td><td>6</td><td>72</td><td>0.09</td><td>0.93</td><td>0.79</td><td>2.25</td><td>0.79</td><td>0.34</td><td>0.06</td><td>0.08</td></th<>	STD-P1		0.2	58	26	54	141	20	<5	0.3	36	. 6	568	2	111	28	165	<5	0.4	6	72	0.09	0.93	0.79	2.25	0.79	0.34	0.06	0.08
HCS=80       0.1       3       14       6       100       45       31       0.12       140       0.42       325       0.66       0.00       0.07         HCS=81       0.2       4       26       12       138       15       45       0.3       325       16       66       7       12       14       0.03       157       0.26       0.05       0.05       0.05       0.05       0.05       0.05       0.05       0.05       0.05       0.05       0.05       0.05       0.06       0.06       0.07       12       14       0.03       157       0.24       3.75       0.77       0.05       0.05       0.05       0.06       0.06       0.06       0.06       0.07       12       22       0.06       0.07       12       14       14       0.02       0.05       0.05       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.06       0.07       0.07       0.05       0.05       0.06       0.06       0.06       0.07       0.07       0.05       0.03       0.02       0.06       0.06       0.07       0.06       0.07				1 1										1								]	1	1				1	
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	HCS-80		0.1	3	14	8	120	<5	- 5	0.3	32	11	1076	2	28 🖉	38	131	<5	1.0	16	31	0.12	1.40	0.42	3.25	0.66	0.06	0,10	0.07
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	HCS-81		0.2	4	26	12	138	15	<5	0.3	35	8	687	2	32	42	81	<5	0.7	12	3414	0.03	1.57	0.24	3.73	0.77	0.05	0.03	0.08
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	HCS-82		0.2	3	31	12	165	21	8	0.6	40	11	1109	ā	31	43	63	<5	0.7	12	17	0.04	1.49	0.29	4.16	0.78	0.05	0.03	0.09
HCS-44       0.6       1       111       23       228       23        53       22       175       96       55       <5       0.6       8       22       0.14       3.14       0.52       6.16       2.24       0.05       0.04       0.10         HCS-85       0.7       3       31       39       61       233       <5	HCS-83		0.5	<1	141	25	138	23	<5	<0.1	57	34	1803	2	67	121	222	<5	0.7	12	22	0.09	3.32	0.50	6.71	2 35	0.06	0.03	0.15
HCS-85 $0.7$ $3$ $31$ $99$ $61$ $233$ $c5$ $c0.1$ $20$ $8$ $562$ $c2$ $64$ $193$ $211$ $c5$ $0.7$ $10$ $32$ $0.10$ $223$ $0.79$ $4.55$ $0.33$ $0.00$ $0.07$ $0.44$ $4.57$ $1.41$ $0.04$ $0.02$ $0.12$ HCS-86 $1.0$ $1$ $633$ $223$ $c5$ $0.2$ $4.0$ $18$ $755$ $c2$ $79$ $82$ $62$ $50.6$ $6$ $211$ $0.06$ $1.79$ $0.44$ $4.57$ $1.41$ $0.04$ $0.02$ $0.12$ HCS-88 $0.2$ $2$ $52$ $66$ $21$ $0.66$ $1.79$ $0.46$ $4.46$ $1.55$ $0.5$ $0.51$ $4.47$ $1.52$ $0.05$ $0.43$ $1.47$ $0.04$ $0.66$ $21$ $0.06$ $1.33$ $0.46$ $4.46$ $1.55$ $0.5$ $0.11$ $0.63$ $0.51$ $0.51$ $0.51$ $0.51$ $0.52$ $0.51$ $0$	HCS-84		0.6		111	23	228	23	<5	0.6	132	32	1288		175	96	55	<5	0.6	8	22	0.14	3.14	0.52	6.16	2 84	0.05	0.04	0.10
$\begin{array}{c c c c c c c c c c c c c c c c c c c $				'					~	••••				-						Ť									•
HCS-B6       1.0       1       63       14       120       23       c5       0.2       40       18       755       c2       54       85       40       c5       0.4       8       20       0.06       1.78       0.44       4.57       1.41       0.04       0.02       0.18         HCS-B7       0.6       3       63       23       129       34       c5       0.1       57       19       935       c2       79       82       62       c5       0.5       6       21       0.08       2.19       0.44       4.49       1.55       0.05       0.04       0.10         HCS-88       0.2       2       52       17       104       36       c5       c0.1       445       18       756       c2       59       901       44       c5       0.5       7       40       0.18       0.03       0.51       4.47       120       0.06       0.15       0.06         HCS-89       0.1       c1       88       8       155       5       c5       c0.1       143       35       1012       c2       222       003       69       c5       0.5       8       32       0.2	HCS-85		07	1 3	31	10	61	233	-55	<b>Ø</b> 1	્રિઝો	В	562	0	64	193	21	<5	0.7	10	32	0.10	2 23	0.79	4.55	6 33	0.03	600	0.07
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			10		83		120	23	1.5	0.2		18	755	2	64	2	40	-5	0.4	A	8 Poo	0.06	1 70	0.44	4.57		0.04	0.02	0.12
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	HCS_87		0.6		63		120	34	~	0.2		10	035		70	600	62		0.5	6	8 5 I	0.00	2 10	0.44	4.40	1 66	0.04	0.02	0.12
$\begin{array}{cccccccccccccccccccccccccccccccccccc$			0.0		62		103	25				19	764		67	6	42	-5	0.5	ž	8 K 1	0.00	100	0.50	4.92	145	0.00	0.04	0.10
HCS-88       0.2       c1       34       10       63       c3       c4.1       47       10       72       c2       c3       b1       c4       c5       0.5       7       80       0.6       0.5       0.6       0.5			0.2	-1	52		404	20	~	<b>1</b>		10	700		50	404		-5	0.5		88. A	0.10	2.02	0.50	4.33	1.40	0.03	0.15	0.00
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	ncs-00-		V.2	ויין						~~. 1		19	102	~	<b>.</b>			<u> </u>	0.5	· · · ·		0.10	2.00	0.31	7,7/		0.09	0.10	0.00
$\begin{array}{c c c c c c c c c c c c c c c c c c c $			<u>-</u>				400			~ ~		05	10.40	~	~~~							0.04	3 00		6 70				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	100 00		0.1	<u>^</u> ]	00		100	0	3	<0.1	14-3	33	1012	<u> </u>	222	000	03	<del>ده</del> بر	0.5	6	202	0.21	3.33	0.91	<b>p.70</b>	0.00	0.00	0.09	0.08
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	103-90		0.3		39		30/	43	6	1.9		13	010	~	30	<u> </u>	02	<3	U.(	IU 10	10	0.02	1, 16	0.34	4.18	u.03	0.04	0.02	0.08
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	HCS-91		0.2	< <u>'</u>	29	2	/0	0		<0.1	<b>11</b>	13	343	~	60	93	60	<5	0.5	12	28	0.08	1.21	0.57	4,30	0.97	0.11	0.02	0.14
HCS-93       8.1       <1       68       16       187       43       12       0.7       84       22       1073       <2       90       76       79       <5       0.7       10       30       0.08       1.92       0.59       4.70       1.76       0.06       0.02       0.12         HCS-94       0.3       2       54       2       69       <5	HCS-92		0.8	<1	65	15	265	42	8	1.3		22	1250	<2	103	80	79	<5	0.6	9	24	0.08	2.07	0.48	5.50	1.79	0.05	0.01	0.11
HCS-94       0.3       2       54       2       69       <5 $<5$ $<0.1$ $32$ $17$ $403$ $<2$ $41$ $97$ $230$ $<5$ $0.5$ $5$ $62$ $0.10$ $1.59$ $0.83$ $4.60$ $1.13$ $0.24$ $0.03$ $0.13$ ML-01 $0.5$ 1 $106$ $8$ $97$ $18$ $7$ $<0.1$ $22$ $22$ $903$ $<2$ $31$ $96$ $150$ $<5$ $0.4$ $6$ $44$ $0.09$ $1.89$ $1.63$ $4.47$ $1.56$ $0.83$ $4.60$ $1.56$ $0.24$ $0.03$ $0.13$ ML-02 $0.5$ 4 $133$ $16$ $119$ $65$ $7$ $<0.1$ $24$ $23$ $1151$ $<2$ $26$ $73$ $61$ $<5$ $0.3$ $5$ $0.03$ $2.02$ $1.73$ $5.93$ $1.57$ $0.12$ $<0.01$ $0.9$ $2.15$ $6.12$ $1.52$ $0.14$ $<0.01$ $0.9$ $2.15$ $6.12$ $1.52$ $0.14$	HCS-93		8. 1	<1	68	<b>36</b>	187	43	12	<b>Q.7</b>	64	22	1073	<li>2</li>	90	76	79	<5	0.7	10	<b>30</b>	0.08	1.92	0.59	4.70	176	0.06	0.02	0, 12
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $																									i				
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	HCS-94		0.3	2	54	2	69	<5	<5	<0.1	32	17	403	<2	41	97	230	<5	0.5	5	62	0.10	1.59	0.83	4.60	1.13	0.24	0.03	0.13
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	ML-01	•••	0.5	1	106	<b></b> 6	97	18	7	<0.1	22	22	903	2	31	86	150	<5	0.4	6	44	0.09	1.89	1.63	4.47	1.56	0.58	0.02	0, 15
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	ML-02		0.5	4	133	16	119	65	7	<0.1	24	23	1151	2	26 🔯	73	61	<5	0.3	6	51	0.03 (	2.02	1.73	5.93	1.57	0.12	<0.01	0, 19
ML-03 <sup>4</sup> 0.2 1 121 11 114 84 7 <0.1 23 28 1457 <2 24 83 50 <5 0.3 5 70 0.03 1.99 2.15 6.18 1.50 0.14 <0.01 0.18	ML-03		0.3	1	123		118	81	<5	<0.1	24	26	1466	2	25	84	54	<5	0.3	5	70	0.03	2.03	2, 15 ]	6.12	1.52	0, 14	<0.01	0, 18
	ML-03*		0.2	1	121	1	114	84	7	<0.1	23	28	1457	<2	24 🖗	83	50	<5	0.3	5	70	0.03	1.99	2.15	6, 18	1.50	0.14	<0.01	0, 18
															<sup>®</sup>						R. 2. 9								{

**Geochemical Analysis** 

Project∕Venture: Area:	1P COREY	Geol: Lab Project No.:	K TROCIUK 02440	Date Received: Date Completed:	JULY 22, 1992 AUG 5, 1992	Page Attn:	7 K TROCI	of
Remarks:							JKOWL	ACHUK
	digested with Ague Be	ain and determined by Graphite Furnace A.A. (D.L. 1 PPB)					E KIMUP	łA

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Au - 10.0 g sample digested with Aqua Regia and determined by Graphite Furnace A.A. (D.L. 1 PPB) ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, 8a, Be, Cr, La and W are rarely dissolved completely with this acid dissolution method.

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SAMPLE	Au	Âg	Mo	Cu	Pb	Zn	As	Sb	Cd	NI	Co	- Mn j	BI	Cr		Ba	ן אין	Be	של	SI SI	11	A	Ca	FO	Mg	ĸ	Na	P
No.	ppb	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррт	ppm	ppm	ppm	ppm	ppm	ppm	%	<u>%</u>	_%	- %	<b>%</b>	<u>%</u>	- *	_%
ML-04		0.3	2	84	3	96	17	<5	<0.1	28	15	1038	2	25	42	70	<5	<0.1	<1	54	0.02	1.31	1.31	5.02	0.91	<b>0</b> . 10 [	<0.01	0.20
ML-05		0.2	<1	87	<1	67	22	<li>&lt;1</li>	<0.1	16	12	368 ]	(2)	17	38	59	<5	<0.1	<1	53	0.04	0.81	1.29	3.29	0.57	0.29	0.01	0.11
ML-06		0.3	2	97	18	121	53	5	<0.1	35	20	738	6	27	37	24	<5	<0, 1	<1	135	0.01	1.25	2,13	5.65	0.89	0.05	<0.01	0.15
MS-01		0.3	3	107	11	197	91	-5	<0.1	35	22	1488	5	44	98	61	<5	<0.1	<1	15	<0.01	2.61	0.47	6, 13	2.29	0.04	<0.01	0.17
MS-02		1.5	3	310	12	174	133	< 5	<0.1	30	12	925	5	51	84	33	<5	<0.1	<1	10	0.01	1.64	0.37	4,40	1,57	0.03	0.01	0.12
			-																				1					
MS-03		04	2	83	31	142	63	7	<0.1		10	575	6	71	86	- 90	<5	<0.1	<1	13	<0.01	2.13	0.32	3,98	2.04	0.02	0.01	0, 10
MS-04		11	5	209	20	177	147	-	<0.1	26	22	1027	5	36	67	29	<5	<0.1	<1	8	0.01	1.57	0.29	5,40	1.34	0.03	0.01	0.13
MS-05		<01	i i	39		104	62	-5	<0.1	59	20	783	4	91	87	29	<5	0.3	<1	44	0.18	2.15	0.56	4.43	1.87	0, 10	0.20	0.06
MS-06		04		55		92	114	<5	<0.1	58	17	846	7	95	89	18	<5	<0.1	<1	41	0.15	2.47	0.63	4, 19	1.99	0.09	0.14	0.06
MG-06#		0.2	1 1	55		89	111		-01	55	16	839	6	89	87	17	<5	<0.1	<1	39	0.14	2.42	0.59	4.23	1.96	0.08	0,13	0.06
M0-00		0.2		~				~					-															
10-07		-0.4		52		- 20	17	-5	-01	46	14	291	0	73	36	A	<5	ا مع	6	55	<0.01	2.29	1.08	1.78	1.18	0.05	0.02	0.02
MS-01		<0.1	) ໍ່	400	10	124	40		-0.1	0.9	3.1	14 14		144	75	27	<5	0.3	5	27	0.06	2.77	0.55	5 30	2 47	0.05	0.02	0.07
MS-00		0.0		102	in in	129	43 22		0.3	8	24	1021		145	70	40	-5	0.4	5	14	0.06	2.37	0.33	4.82	2 14	0.06	0.02	0.08
MS-US		<0.1				115			-0.1		47	764		01	76	20	-5	0.4	1 7		0.10	198	0.36	421	474	0.07	0.03	0.07
MS-10		<0.1	8	44	2	115	<b>C</b> 3	8	<0.1	20	10	15020			10	65		1.0	1 20	100	-0.01	5 23	0.17	8.38	0.63	0.02	-0.01	0 12
\$1-A		3.2	29	5619	83	518	1 15	<0	3.5	00 <b>00</b>	243	10038	~		ю		~5		~		20.01	0.23	0.17	0,50		0.02	~0.01	0.12
											25	0650	~		36	81	-5	0.3		20	001	148	0.38	0 11	1 24	0.03	-0.01	0.17
555-1		4.9	16	404		400	¥4 10	<i>u</i>	1.3			2002	v s	20		20		0.0			-0.01	2 17	1 44	8.04	1 02	0.04	-0.01	0 18
SSS-2		0.6	5	136	12	124	16		<0.1		23	1097	~			29		0.2			-0.01	2.10	0.44	6.05	4 76	0.04	-0.01	0.16
SSS-3		0.7	5	132	33	236	40	<b>a</b>	0.2	20	29	2068	~	23	Da	01	<0	0.3	2		<0.01	2.10	1.72	6.05		0.03	-0.01	0,10
SSS-4		0.5	4	114	7	235	15	<	<0.1	33	24	1106	~2	42	60	33		0.2	3	24	<0.01	2.15	1.73	5,80		0.04	0.01	0.10
SSS-4*		0.4	3	111	Þ	235	14	< 5	<0.1	33	- 24	10/5	~2	42		33	< ~	0.2	•	•4	<0.01	2.13	1.74	3,80	1.50	0.04	20.01	0.17
			[	{								1000						1				1 00				0.02		0.12
\$\$\$-5		1.3	2	186	33	3/5	90	9	1.8	30	21	1909	~	20	00	00	13	0.5			0.02	1.02	0.23	0,08		0.00	-0.01	0.10
SSS-6		0.7	7	344	40	417	311	10	2.7	47	59	2860	5	28	69	118	<5	0.5		01	0.00	1.90	0.18	9,57		0.02	<0.01	0.10
SSS-7		1.1	4	167	29	295	100	<5	1.4	21	25	1812	2	25		61		0.4		લ	0.02	1.07	0.20	6, 10	1.14	0.03	<0.01	0.13
SS\$8		0.4	3	105	13	209	32	<5	0.9	41	18	858	2	49	75	53	<0	0.2	10	19	0.03	0.98	0.52	4,60	0.18	0.00	0.01	0.10
SSS-9		0.3	1 1	64	9	93	55	6	0.2	22	14	734	<2	28	<b>5</b> 1	42	<>	0.2	0	24	0.02	1.25	0.82	4, 10	<del>.</del>	0.00	<0.01	0.17
	1		{										-				-	1	۱ <u> </u>		1	4.04				0.00		
SSS-10		0.3	1	53	8	81	22	<5	<0.1	22	11	646	4	29		35	<	0.2	<u> </u>	20	0.02	1.21	0.80	3,02		0.00	<0.01	0.14
SSS-11	F	0.3	2	68		108	34	ব	0.3	23	13	734	<2	29	51	48	<5	0.2	1 1	- <b>2</b> 5	0.02	1.29	0.60	4, 10	TOS	0.06	<0.01	0.10
SSS-12	{	0.3	2	56	11	83	39	7	0.2	21	13	725	~	27	48	45	<5	0.3	í 9	39	0.02	1.17	1.20	3,83	0.90	0.08	<0.01	0.18
SSS-13		0.8	4	89	14	114	74	ଏ	0.3	43	19	1014	2	46	59	44	<5	0.3	8	- 39	0.03	1.48	1.21	4,69	1.26	0.06	<0.01	0.20
STD-P1	1	0.3	58	26	52	146	23	6	0.4	35	6	571	2	101	33	168	<5	j 0.4	1 7	73	0.08	0.96	0.74	2.22	0.84	0.34	0.05	0.08
1	1	1	1	1				1	1								)	1	Ì									!
SSS-14	1	1.5	1	76	9	109	46	<5	<0.1	25	17	980	2	32	55	50	<5	0.3	6	23	0.02	1.41	0.67	4.40	1.16	0.07	<0.01	0.20
SSS-15		0.9	1	131	20	164	107	<5	0.5	28	24	1316	2	27	55	52	<5	0.4	10	23	0.04	1.36	0.58	5.22	1.22	0, 12	0.01	0.21
SSS-16	1	1.0	2	162	19	184	85	5	0.4	33	25	1222	<2	37	67	37	<5	0.5	11	22	0.03	1.61	0.45	5,59	1.44	0.04	0.01	0, 18
SSS-17		0.9	3	211	20	214	62	<5	0.7	32	30	14 15	2	35	74	44	<5	0.6	11	18	0.04	1.64	0.32	5.79	1.55	0.04	0.01	0, 15
SSS-18		1.0	3	164	17	184	85	<5	0.5	31	23	1248	2	35	62	36	<5	0.4	8	22	0.03	1.54	0.47	5.25	1.36	0.04	0.01	0,18
}	}	1	1	1		]	1	Ì	1								1	1	1									
SSS-19		1.2	<1	161	29	169	183	5	0.2	32	30	1348	2	24	49	43	<5	0.2	5	21	0.04	1.33	0.58	6,68	1.21	0, 12	0.01	0.20
SSS-20	• •	0.5	1	90	12	117	53	ব	0.2	27	18	981	2	34	58	67	<5	0.1	6	19	0.05	1.29	0.55	4.33	1, 10	0.16	0.02	0, 16
555-21		0.3	1	78	31	158	17	6	0.6	59	22	763	2	68	75	109	<5	0.4	6	33	0.08	2.24	0.68	4.45	1.42	0.14	0.03	0.10
555-22		0.2	1 2	92	13	112	19	6	<0.1	72	21	925	2	96	68	69	<5	0.3	8	23	0.04	1.98	0.46	4.81	1.94	0.05	0.02	0.11
999-22*		0.2		6	1	113	19	6	0.2	72	22	929		97	70	70	<5	0.4	(8	23	0.05	2.03	0.45	4.92	1.99	0.05	0.02	0.12
000-ec	1	) v.e	] '	1 ~			"						_				-			1885								
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Geochemical Analysis

Project/Venture: Area:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2440	Date Received: Date Completed:	JULY 22, 1992 AUG 5, 1992	Page Atto:	8 K TROCI	of JK
Remarks:							JKOWLA	CHUK
	strained with Association and statements of his Committee Frame							Δ

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Au — 10.0 g sample digested with Aqua Regis and determined by Graphite Furnace A.A. (D.L. 1 PPB) ICP — 0.5 g sample digested with 4 ml Aqua Regis at 100 Deg. C for 2 hours. N.B. The major oxide elements, Be, Be, Cr, La and W are rarely dissolved completely with this sold dissolution method.

SAMPLE	Âu I	Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	V	Ba	W	Be	La	Sr	īπ [	A	Cal	Fe	Mg	- K T	Na	PŢ
No.	ppb	PPm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm.	ppm 🔤	mqq	ppm	ppm	ppm	ppm	ppm	%	%	%	<u>%</u>	%	_%_	_%_	%
SSS-23		0.6	<1	91	7	102	13	<5	<0.1	45	22	1059	2	59	81	54	<5	0.4	11	21	0.05	2.02	0.49	5.13	1.85	0.04	0.01	0.16
SSS-24	1	0.7	2	102	7	117	12	6	<0, 1	62	26	1081	<2	84	<b>D</b> 7	47	<5	0.6	14 ]	22	0.05	2.40	0.48	5.70	2.29	0.04	0.02	0.14
SSS-25	[	2.4	5	139	14	181	37	<5	0.1	60	28	1381	<2	72	99	65	<5	0.5	9	24	0.06	2.76	0.49	6.67	2.55	0.04	0.02	0,14
555-26	l	1.1	5	105	13	145	29	<5	<0.1	51	22	1195	<2	64 💮	88	<b>6</b> 8 (	<5	0.5	10	23	0.05	2.23	0.48	5.70	1.98	0.05	0.01	0.14
SSS-27		0.3	2	76	6	105	75	<5	0.3	34	18	796	<2	45	59	57	<5	0.4	11	53	0.06	1.22	1.38 į	4.22	1.01	0.08	0.02	0.15
	i																	1					1					
125N-00E	1	0.4	5	29	9	31	5	<5	<0.1	6	3	127	<2	14	164	30	<5	0.1	4	7	0.32	0.42	0.05	2.32	0.07	0.03	0.01	0.03
L25N-05E		0.9	12	42	18	192	18	8	0.7	29	43	1409	2	26	148	67	<5	1.0	12	8	0.18	2.02	0, 12	7.64	0.41	0.04	0.01	0.08
125N-10E	l	2.4	11	55	22	477	15	<5	2.6	47	32	1919	<2	33 💹	90	122	<5	1.7	27	20	0.05	2.94	0.46	6.41	0.76	0.06	<0.01	0.13
L25N-15E	1	1.2	6	45	11	179	13	<5	1.4	21	5	313	2	23	61	76	<5	0.5	11	17	0.06	1.51	0.20	5.74	0.30	0.04	0.02	0.08
125N-15E*	[	1.2	8	47	10	182	13	<5	1.4	23	5	307	2	25	61	79	<5	0.5	10	18	0.06	1.60	0.21	5.79	0.31	0.04	0.02	0.08
	1		_				1									)	1											
125N-20E		1.1	8	81	10	367	7	7	<0.1	30	9	538	2	21	58	- 44	9	1.3	13	5	0.04	2.59	0, 10	10.39	0.39	0.04	<0.01	0.08
125N-25E		1.8	6	60	17	224		<5	0.4	28	64	644	<2	27	76	104	<5	1.7	15	15	0.02	3.62	0,16	7.66	0.17	0.04	<0.01	0.08
125N-30E		1.9	11	23	13	131	13	<5	0.2	13	- 4	194	~	17 💹	89	78	<5	0.4	8	11	0.10	1.33	0, 16	5.17	0.09	0.04	<0.01	0.05
150N-00E		3.7	8	114	42	1512	- 44	13	13.0	115	67	3282	2	33 💹	85	114	<5	2.4	- 44	18	0.03	3.76	0.49 [	8.50	0.63	0.04	<0.01	0.12
150N-5E	1	1.6	2	20	6	65	6	<5	0.5	13	7	274	2	16	51	48	<5	0.3	7	33	0.23	0.92	0.47	2.91	0.39	0.07	0.08	0.06
	1	,	-	-																								
150N-10E	ļ	0.8	2	36	34	211	<5	<5	2.6	22	- 14	1566	2	20	43	99	<5	1.2	18	47	0.11	2.44	0.84	3.44	0.27	0.05	0.05	0.08
150N-15E	- 1	2.4	8	90	32	694	25	8	6.3	64	48	2630	<2	22	47	112	<5	1.9	27	28	0.02	2.79	0.69	9.23	0.40	0.05	<0.01	0.14
150N-20E		1.8	8	82	28	541	15	8	5.8	60	50	2554	~	22	53	- 90	<5	1.7	24	11	0.03	2.38	0.29	8.10	0.45	0.05	<0.01	0.11
150N-25E		1.4	7	100	38	569	41	15	7.0	67	27	3258	<2	14	17	218	<5	1.2	27	25	<0.01	0.98	0.38	7.52	0. 18	0.07	<0.01	0.10
150N-25E*		1.4	8	102	43	565	42	15	7.2	68	27	3203	~2	13	17	220	<5	1.2	27	25	<0.01	0.99	0.39	7.55	0, 18	0.07	<0.01	0.10
	· {		Ĩ																				1				1	1
150N-30E		2.0	15	108	17	1902	38	6	29.9	64	26	12776	<2	16	72	255	6	0.7	16	10	<0.01	0.95	0.22	7.00	0.39	0.02	<0.01	0.11
175N-00E	í	9.0	7	121	56	1420	46	5	9.5	89	32	2147	~2	38	67	92	<5	2.1	42	26	0.04	3.69	0.71	6.50	0.51	0.03	<0.01	0.10
175N-5E		6.0	11	84	17	401	18	<5	2.8	34	23	1047	2	31	73	76	<5	1.5	24	26	0.04	2.88	0.59	6.14	0.27	0.02	0.01	0.12
175N-10E		10.0	13	120	54	998	43	9	9.0	88	68	3214	<2	37	98	- 99	<5	2.1	37	S 12	0.03	3.56	0.25	8.86	0.75	0.04	<0.01	0.12
175N-15E		3.7	5	51	19	454	16	6	3.0	36	20	1695	2	26	57	- 95	<5	1.5	22	27	0.04	2.66	0.82	5.25	0.45	0.05	<0.01	<b>0.10</b> [
			_						1																			
175N-20E		1.1	15	73	29	307	38	9	0.4	33	12	512	2	20	51	87	<5	1.2	19	3	0.05	2.77	0.05	7.04	0.30	0.03	<0.01	0.04
175N-25E		1.5	5	20	7	80	11	<5	<0.1	10	3	17	2	18	93	41	<5	0.5	8	10	0.14	1.37	0,16	3.99	0.09	0.03	<0.01	0.04 ]
175N-30E		0.4	6	24	B	104	8	<5	<0.1	21	5	226	2	25	124	53	<5	0.4	7	10	0.24	1.98	0,10	7.07	0.46	0.03	0.02	0.04
STD-P1		0.2	61	27	48	152	20	6	<0.1	34	5	_ 548	2	111	37	172	<5	0.4	- 8	83	0, 10	1.07	0.85	2.32	0.89	0.37	0.06	0.08

**Geochemical Analysis** 

Project/Venture:	1P	Geologist: KIBOCIUK	Date Received:	JULY 22, 1992	Page	1 of
Area:	COREY	Lab Project No.: (D2499)	Date Completed:	AUGUST 20, 1992	Attn:	K TROCIUK
Remarks:		$\bigcirc$				S HOFFMAN

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J KOWALCHUK

E KIMURA

Au - 10.0 g sample digested with Aqua Regia and determined by Giaphite Furnace A.A. (D.L. 1 PPB)

ICP - 0.5 g sample digested with 4 mt Aqua Regia at 100 Deg. C for 2 hours.

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N.B. The major oxide elements, Ba, Be, Cr, La and W are marely dissolved completely with this acid dissolution method.

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SAMPLE		Ag	Mo	Cu	Pb	Zn	As	Şb	Çq	XNC.	Co	Mn	Bi	Cr	V	Ba	W	Be	La	Sr	П	A	8	Fe	≪ Mg∛	K	Na	P
Na.		ppm	ppm	ррт	ppm	ррт	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	opm	ppm	ppm	ppm	ppm	%	%	%	%	ે %ે	%	%	_%
18 10 1		760.0	1	1.43%	. 188	153	3.76%	0.29%	2.3	34	3	292	762	50	<1	<1	<5	0.1	1	<u></u> 1	<0.01	0.03	0.01	17.89	0.02	0.02	<0.01	0.03
18 102		3.6	3	96	2	35	101	7	<0.1	114	47	235	13	97	30	<1	<5	0.1	1	2 2	0.12	2.52	2.72	7.39	1, 16	<0.01	<0.01	0.04
18 103	1	9.0	<1.	82	6	32	0.58%	<5	<0.1	21	- 4	1062	15	20	<b>~1</b>	19	<5	0.1	2	<b></b> 1	<0.01	0, 19	0.03	7, 18	0.02	0.17	<0.01	0.01
18 104		0.4	<1	61	1	78	56	<5	0.2	125	20	553	<2	185	62	<1	<5	0.3	3	1992-4	0.16	1.81	1.39	4.25	1.59	<0.01	0.04	0.04
18 105		4.4	26	50	58	65	207	9	<0.1	25	15	707	8	81	85	32	<5	0.1	2	×85	<0.01	1.68	0, 16	9.81	1.09	0.07	<0.01	0.08
																				28 Q.								
18 106		0.6	8	37	6	52	11	<5	<0.1	19	7	291	2	16	24	50	<5	0.1	2	<u> 888</u> 4	0.05	1.34	0, 19	6.07	1.29	0, 19	0.03	0. 12
18 107	ł	1.0	<1	38	16	313	6	<5	1.6	10	6	763	~2	89	2	54	<5	0.1	2	18	0.03	0.77	0.57	2.70	0.48	0, 10	0.02	0.06
18 108		0.6	3.	122	4	84	63	<5	0.3	52	15	516	~2	<b>95</b> [	×44	<1	<5	0.3	6	10	0.17	2.69	0, 19	5.33	83,40	0.02	<0.01	0.04
18 109	1	0.4	3	70	17	68	95	6	0.2	69	- 14	409	2	192	<b>119</b>	21	<5	0.3	- 4	8 C 🔸	0,18	1.72	0, 15	5.44	222	0.04	0.01	0.05
18 109 *		0.5	· 2	68	15	87	93	<5	0.2	68	13	395	2	190	117	18	<5	0.2	3	ి 3	0.17	1.68	0.14	5.36	2.20	0.04	0.01	0.05
															20.					6 1 A. I								
18110		0.3	3	26	9	97	57	<5	0.6	88	15	610	2	269	180	- 44	<5	0.4	7	3. A.A.	0.38	2.51	0.34	6, 18	3.16	0.09	0.01	0.06
18111		0.3	<1	79	2	- 44	<5	<5	0.3	15	19	227	2	18	84	25	<5	0.3	- 4	8	0.21	1.36	0.80	3.80	0.97	0.07	0.05	0. 12
18112		0.5	13	74	5	464	11	<5	5.1	34	10	306	2	46	89	76	<5	0.4	5	1884	0.07	1.05	0, 19	4.78	0.60	0.25	0.03	0.07
18113	1	0.7	3	61	5	81	27	<5	0.8	27	12	295	2	62	123	54	<5	0.4	9	14	0, 10	1.76	1.72	4.57	1.29	0.09	0.05	0.61
18114	1	0.2	2	91	5	34	31	<5	0.6	15	11	244	2	42	90	54	ব	0.6	11	51	0.07	0.73	0.46	3.47	0.42	0.36	0.03	0.10
· ·	1																											
18115		<0.1	4	33	1	16	<5	<5	0.2	7	<1	43	2	33	68	151	<5	0.3	6	32	0.03	0.33	0.03	4.27	0. 16	0.37	<0.01	0,10
18116		0.1	3	22	13	106	51	<5	0.6	103	27	604	2	209	121	19	<5	0.2	2	2	0.17	2.02	0, 19	4.93	2.84	0.04	0.01	0.03
18117		0.8	3	60	10	117	16	<5	1.7	55	13	576	~2	60	64	57	<5	0.2	- 4	18	0.10	1.94	2.01	3.60	L29	0.07	0.11	0.10
18118		3.1	6	1260	34	254	124	24	<0.1	60	9	259	39	77	102	7	<5	0.2	3	2 2	0.16	1.02	0.13	22.24	0.66	0.03	0.02	0.08
18118*	I	3.0	4	1254	35	256	129	21	<0.1	59	8	257	42	79	101	6	<5	0.2	2	2	0.15	1.01	0.11	21.64	0.64	0.03	0.01	0.08
															289 (X.)		1			1000					848 A.			
18119		1.7	10	90	15	486	32	<5	6.5	52	13	1003	5	73	<b>13 1</b>	25	<5	0.7	16	2012	0.07	0.92	0.87	6.23	ି ୦.69	0.08	0.02	0, 17
18 120		0.7	3	112	13	48	65	15	0.5	15	22	1335	~2	20	53	64	<5	0.6	8	ुं 433	0.02	1.29	7,44	4.58	0.72	0.24	0.01	0.17
18 12 1	1	1.8	4	79	3	1039	293	41	4.5	26	22	730	- 4	54	128	32	<5	0.6	10		0.12	1.39	0.78	5.54	1.39	0.05	0.02	0, 15
18 122	}	9.0	7	40	7	509	35	13	2.2	32	5	26659	- 24	47	45	- 27	<5	0.3	6	30	<0.01	0.64	0.38	15.46	1.37	0.09	<0.01	0.08
18 123		55.0	8	165	×1	590	39	36	2.9	39	9	35926	43	31	53	- 34	<5	0.3	6	<b>41</b>	<0.01	0.49	0.41	18.30	1.62	0.05	0.01	0.07
																_				1846 - I								
18506	1	290.0	2	1.04%	2894	277	612	290	14.7	55	98	1171	3398	63	∰ <b>\$</b> \$	5	125	<0.1	2	<u>⊚</u> ⊗2	<0.01	0.03	0.02	17.07	0.06	0.02	<0.01	0.03
18507		7.0	5	356	25	135	3.62%	46	0.6	41	11	31962	65	21	20	8	<5	0.2	5	<u> </u>	<0.01	0, 10	0.23	19,47	L30	0.04	<0.01	0.03
18508		2.5	11	309	16	883	0.89%	9	5.3	25	28	19090	32	- 4	31	97	<5	0.3	5	23	0.04	0.73	0.60	10.29	0.96	0.58	<0.01	0.22
18509	1	16.0	5	929	504	106	1.12%	25	0.2	39	23	30 192	182	16	15	28	13	0.1	4	<u></u>	<0.01	0.04	0.30	19.73	1.56	0.02	<0.01	0.03
18509*		17.0	4	942	105	101	1.12%	25	0.3	40	23	30342	182	17	15	28	14	0.1	5	B	<0.01	0,04	0.31	19.80	1.61	0.02	0.01	0.03
	1		1										_ 1				]											
185 10		9.0	3	579	31	139	8.28%	73	0.4		43	8399	58	35	11 I	18	<5	0.3	6	3	<0.01	0.11	0.07	19.34	0.27	0.06	<0.01	0.03
1940 1		53.0	1	75	26	164	0.34%	76	1.0		3	4807	5	153	7	15	<5	<0.1	3	5	<0.01	0.12	0.05	4.72	0, 16	0.05	<0.01	0.01
19402		3.1	23	964	3	- 44	437	15	0.7	19	16	1353	6	34	27	52	<5	0.7	9	43	0.03	0.60	4.22	6.09	0.37	0.24	0.01	0.07
19403		3.8	62	116	100	355	310	17	0.9	33	35	415	23	42	11	16	<5	0.3	7	20	0.01	0.21	2.01	16.65	0.11	0.12	<0.01	0.04
19404		0.6	13	53		73	42	11	0.9		5	1264	~2	9	16	41	<5	0.2	2	15 1	<0.01	0.24	9.52	2.63	0.56	0.13	0.02	0.03
1			l																								]	
19405		0.5	2	106	13	67	<5	27	<0.1	36	80	953	8	65	53	23	<5	0.2	5	142	0.01	1.79	2.34	9.97	1.04	0.04	0.02	0.12
19406	· ·	1.6	3	61	6	110	19	<5	<0.1	18	17	1487	7	30	49	33	<5	0.2	3	48	0.04	1.53	1.73	6.71	(1,48)	0,16	0.01	0.13
19407		0.6	<1	24	68	76	47	5	0.5	9	5	40	2	26	3	- 44	<5	<0.1	2	7	<0.01	0.19	0.15	2.20	0.03	0.17	<0.01	0.04
19408		0.9	1	74	12	44	7 19	30	0.3	17	13	246	2	40	14	59	<5	0.1	3	26	<0.01	0.65	0.88	4.27	0.41	0.17	0.01	0.08
STD-P1	1	0.2	58	27	50	147	21	5	0.8	35	6	590	<2	96	32	177	<5	0.4	7	76	0.10	0.99	0.86	2.35	0,83	0.37	0.06	0.08
	1				888-Q.										###C>}			1		899 A. A.	1							

NOTE: "02" CONVERTED -> ppm FOR CU, PB, ZN, AS, SB. (22/Aug/92)

Geochemical Analysis

Project/Venture:	1P	Geologist:	K TROCIUK	Date Received:	JULY 22, 1992	Page	2 of	8
Area:	COREY	Lab Project No.:	D2499	Date Completed:	AUGUST 20, 1992	Attn:	K TROCIUK	
Remarks:							S HOFFMAN	
Au - 10.0 g sample di	gested with Agus Regis and deter	mined by Gmphite Furnace A.A. (D.L. 1 PPB)					J KOWALCHU	ĸ

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ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are rarely dissolved completely with this acid dissolution method.

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SAMPLE	Ag	Mo	Cu	<b>Pb</b>	Zn	As	Sb	Cđ	NI.	Co	Mn	Bi	Cr V	Ba	W	Bø	LA	Sr	Ti	AI	Ôa,	Fa	Md	ĸ	Na	P
Na	ppm	ppm	mqq	mqq	mqq	ppm	mqq	<b>p</b> pm	ppm	mqq	ppm	mqq	ppm ppm	ppm	mqq	ppm	mqq	mqq	%	%	%	%		%	%	_%_
19409	1.1	3	31	75	66	109	<5	0.6	<b>S</b> 3	6	1216	2	31 4	9 94	<5	0.4	10	24	0.09	0.88	0.33	3.75	0.55	0.22	0.02	0, 16
19410	0.8	2	178	<b>1</b>	86	283	<5	0.6	18	13	9524	5	66 88 1	8 53	<5	0.2	3	54	0.01	0.40	1.24	6, 10	0.52	0.21	<0.01	0.07
19411	2.4	5	165	80 B	42	70	<5	<0.1	47	325	404	15	45 5	2 12	< 5	0.1	3	B	0.04	0.80	0.27	14,14	9.67	0,16	0.01	0.11
194 12	4.2	4	423	9	92	112	16	0.2	37	13	3 1932	43	32	8 42	<5	0.1	5	8	<0.01	0.15	0.30	19, 14	1.35	0,08	<0.01	0.04
194 13	2.5	2	64	111	87	60	<5	0.1	26	8	676	9	45	8 10	1 <5	<0.1	<1	<b>11</b>	0,10	0.31	0.14	10,11	0.09	0.33	0.01	0.08
\ {	ļ	i ا					ι I				}				{	}						. 1				ł
19414	1.4	3	97	13	38	19	<5	0.4	22	14	897	<2	161 2	5 17	<5	<0.1	<1	9	0.02	0.65	0.37	3,36	0.62	0.05	<0.01	0.01
194 15	26.0	14	482	×844	41	455	9	<0.1	42	149	202	34	36 2	) g	5	<0.1	2	11	<0.01	0.24	0.23	16.04	0 15	0.14	<0.01	0.06
194 16	1.2	5	162	×1	95	2318	15	<0.1	40	19	40794	45	35 2	0 7	<5	0.1	6	17	<0.01	0.26	0.13	19,99	072	0.02	<0.01	0.03
194.17	0.4	2	90	<b>X</b> <1	61	18	<5	<0.1	26	21	368	7	52	0 11	<5	0.2	2		0.15	2.76	0.89	7.56	1 73	0.02	0.01	0.06
194 17 *	04	5	84	× 1	61	19	<5	<01	26	21	372	5	51 10	9 11	<5	0.2	2	· 🏼 🧿	0.15	2 75	0.87	7 30	171	0.02	0.01	0.06
							1 1					I		ŝ,	~~	, <u>, , , , , , , , , , , , , , , , , , </u>	_	****						0.00		0.00
104.18	0.7		42	>>© •	90	<5	<5	0.5	28	14	566	4	R2 12	5 37	6	0.6	11		0.15	240	0.73	5 AQ	6	0.05	0.03	0.10
104 19	0.7	16	11		264	14	32	0.0	50	3	29070	63	<1 M	536	5	0.4	22	RQ	-0.01	0.04	0.67	25.00	<b>1</b> 14	0.00	-0.01	0.03
19420	0.2		140		A1	124	14	0.0	28	i i	20527	19		25	25	0.2	3	RA	-0.01	0.05	2.88	14 18	4 27	0.01	0.01	0.00
19420	0.0		115	30 a.	51	-5		~0.1	<b>1</b>	21	A12	7	72	6 46		0.2			0.01	0.00	1.00	7 10	A 78	0.03	0.01	0.02
19421	0.5				80	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		0.1		۲ (۲	814		40 40	5 03		0.7		24	0.13	1.00	1.24	7.10	V./0	0.00	0.13	0.10
19422	0.5	) '						V.2		1 1	1 0 1			်] ခ်၊		) V.E	<b>–</b>	- <b>-</b>	0.07	1.20	0.40	9,03	0.13	0.00	0.07	0.00
10473	1 0 1	7	61		18	14	41	0.8	1990 - A	20	400	80	1 10	୍ମ 1 ୨୨	1.5	0.5	6		0.03	0.60	0.62	2 2 1	0.01	0.14	0.001	0.04
10420	1 3 3	1 20	3088		45		انه ا	-0.0	344	280	180	70	45	il a		0.3	l e		0.00	0.05	0.02	40.45	0.40	0.17	0.05	0.04
10424	17	20	3300			2409	20	-0.1	<b>1</b>	200	20405	20				0.0	5		-0.02	0.41	0.20	15 05		0.00	0.02	0.00
19423			12	<u>.</u>	121	4000	23	0.1		22	55700	20						220	<0.01	0.51	0.20	10,00	2.00	0.02	<0.01	0.02
19420	1.0		129	88 - L	101	2020	27	0.7		20	53280	17		280			0	0.00	<0.01	0.4/	0.20	10.84	0.30	0.04	0.01	0.03
18420-	1.0		118		123	3025	23	0.0	00 <b>**</b>	21	155775	3		1 202	°	0.1	0	- 36 I	<0.01	0.45	0.27	10,41	0.30	0.04	0.01	0.03
10427	0.8		54		152	976	37	03	47	10	54213	64	16 2	8 1 1A	6	0.3	14	73	-0.01	0.20	0.28	22.28		0.01	-0.01	0.02
19428	67.0		2055	1814	3633	2531	839	387	27	25	11991	99	56	4 32	65	0.5	10	23	-0.01	0.11	0.06	12 4 1	0.00	0.05	-0.01	0.02
19429	77.0	1 21	2448	14 1	136	2579	215	0.2	28	43	4004	1788	73		308	01	2		-0.01	0.03	0.02	12.71	0.02	0.00	-0.01	0.02
19430	35	10	1845	34 e	59	43	18	<01		761	269	53	63	Š Ř	11	01			-0.01	0.05	0.02	10.02	200	0.02	-0.01	0.02
19431	0.0	10	802		20	17	5	04		89	498	Â	76	5 27	15		-1	74	0.03	0.03	2.86	3 11	0.44	0.03	0.01	0.02
	0.0	`'		20 M				0.4	898 e					8		· · · ·			0.00	V.20	2.00	0.11		0, 11	0.02	0.02
19432	3.4	5	272	×1	83	52	16	<0.1	37	127	153	44	53 5	5 6	87	0.3	2	· · · · · ·	0.07	0.78	0.12	19.48	n 12	107	0.02	0.04
19433	17	22	2682		23	<5	<5	<01	88	253	145	13	59 2	1 14	35	02	2		0.03	0.44	0.25	11 13	0.22	0.16	0.03	0.03
19434	15	136	1893	1 × 1	25	<5	<5	<0.1	833	128	160	11	107 2	1 12	425	0.1	2	7	0.03	0.26	0.50	0.80	0.45	0.12	0.00	0.05
19435	18.0	5	79	23	949	284	21	52	143	27	12776	15	220 11	1 46	6	0.5	-		-0.01	3 27	0.24	13 44		0.07	-0.01	0.03
STD-P1	0.3	66	25	50	150	21	6	0.9	39	6	589	2	101	7 173	6	0.5	6	77	0.00	102	0.83	2.35	0.02	0.37	0.06	0.00
	0.0	1			1		-	0.0	886 C	-		~		्रि					0.00		0.00	2.00		0.07	0.00	0.00
19436	1 1 1	1 a	74	a an	100	<5	13	0.6	184	34	705	0	325	1 10	6	0.0	10		0.21	3.06	1 33	541	4.45	0.04	0.01	0.06
19437	5840	a a	0.52%	0.84 %	2020	0.15%	1.15%	22.6	8	7	20236	75	36	8 4	25	0.4			<0.01	0.69	0.06	22 91	ីស	0.04	-0.01	0.00
19438	83.0	1 5	187	124	1686	31	217	12.5	110	20	3712	3	222	18 18	6	0.6	3		0.07	2 94	0.00	5.62	2 4 1	0.01	0.01	0.04
19439	1 149		1.33%	18 14	2344	644	1.72 %	51.0		7	20830	120	31	1 10	25		5		-0.01	0.27	0.05	10.02	0.31	0.05	-0.01	0.07
19440	160 0	ג ו ג	330	457	0.85%	207	601	57.6	132	30	15 158	21	94	8 12	1 3	1.0	Ř		-0.01	1 18	0.00	0.82		0.00	-0.01	0.04
		ľ			/			00				- '			l ~ ~		l I				0.07	0.02		v. 10	-0.01	0.04
19441	1680	1 1	1711	682	1031	1.33%	0.34 9	13.2	109	23	377 14	80	10 2	୍ଗ ପା ୨	1 05	0.2	5		001	0.14	0 10	22 88	075	0.00	10.01	0.03
19442	5640		0.74%	2480	3297	0.23 %	0.90	44.3			37957	90	21		1 6	0.3	, š	55	20.01	0.32	0.14	21.57	0.70	0.02	-0.01	0.00
19443	132 0	1 - 1	108	10 1	4350	395	363	28.3	213	42	16420	19	105		1 25	17	3		-0.01	1.35	0.37	1108	1 20	0.00	-0.01	0.04
10444	310	1		20	120	34	21	10	17	4	837	0	41	A 12		0.2	5		-0.01	1.30	0.22	4.52	0.82	0.13	0.01	0.00
10444	30.0		50	27	110	30	20	0.0			812		34	5 IU 8 III		0.2			-0.01	1.00	0.23	4.44	0.00	0.00	0.00	0.10
	30.0	`'	<b>"</b>		, "°		<b></b>	v.9		3	1 ~~~	<u> </u>		č <sup>13</sup>		{ v.z	Ĵ		~0.01	1.20	0.23	יי. <del>י</del>		0.00	0.00	0, 13
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Project/Venture:	1P	Geologist:	K TROCIUK	Date Received:	JULY 22, 1992	Page	3	of	8
Area:	COREY	Lab Project No.:	D2499	Date Completed:	AUGUST 20, 1992	Attn:	K TROCI	UK	
Remarks:							SHOFFN		
Au - 10.0 g sample digested	i with Aqua Regia and determined by Graphi	te Furnace A.A. (D.L. 1 PPB)					J KOWAL	CHUK	
ICP - 0.5 g sample digested	with 4 ml Aqua Regia at 100 Deg. C for 2 ho	XUF8.					EKIMUR	A	
N.B. The major oxide elemen	ts, Ba, Se, Cr, La and W are rarely dissolved	completely with this acid disso	lution method						
						12:14:1			

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SAMPLE	Ag	Mo	Cu	PD	Zn	As	SD	Ca	<b>IN</b>	60	MG	ы		1 <b>V</b>	- ber	"	Da	- 14	ु भ	" [	~		r v			~	~
No.	ppm	_ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	opm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<u> </u>	%	%	<u>%</u>	~ % ~	<u>%</u>	- %	<u>*</u>
19445	60.0	3	122	45	111	38	149	1.2	127	30	1591	5	140	98	- 34	<5	0.7	4	217	<0.01	1.25	7.75	5, 19	2.38	0.04	0.01	0.04
19446	20.0	1	1333	12	77	8	41	0.1	51	88	3310	136	42	16	26	681	0.2	3	93	0.02	0.44	1.76	16,62	0.58	0.24	0.01	0.03
19447	13.0	2	467	12	181	<5	26	0.2	30	12	5992	27	92	76	157	23	0.3	3	15	0.10	2.30	0.33	10.01	1.39	0.44	<0.01	0.06
19448	3.0	2	401	- 11	163	21	11	0.5	24	22	1609	16	15	29	62	24	0.3	10	14	0.03	0.83	0.51	7.80	0.61	0.52	<0.01	0.16
19449	6.0	11	2368		86	<5	16	0.2	29	30	864	17	107	32	31	<5	0.1	3	31	0.01	1.44	0.35	8,46	1_25	0. 17	0.01	0.04
19450	263.0	5	4.30%	828	581	1.00%	241	7.5	38	30	12032	1879	34	8	10	366	0.1	4	4	<0.01	0.06	0.11	17.78	0.60	0.03	<0.01	0.05
19451	3.2	2	583	13	116	145	23	0.5	21	11	168 14	46	67	10	39	9	0.2	3	17	<0.01	0.22	0.37	9.06	1.01	0.20	0.01	0.10
19452	6.0	3	330	6	142	115	21	0.6	30	21	28295	45	100	13	18	5	0.1	5	9	<0.01	0.26	0.22	12.43	1.05	0.04	0.01	0.04
19453	68.0	6	1.08%	189	413	2.02%	59	4.3	41	15	29521	288	19	13	27	26	0.1	5	22	<0.01	0.03	0.14	20.77	0.78	0.03	<0.01	0.03
10453	66.0	5	1089	190	415	2 02 9	57	44	42	17	30485	293	19	13	27	28	0.1	5	23	<0.01	0.03	0.14	21.27	0.79	0.03	<0.01	0.03
18435	00.0	l .	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		4.0	<b></b>											••••	-									
10454	300	1 .1	1 1 14 14		248	0.479	33	25	48	7	39007	38	3	23	19	<5	0.3	10	5	<0.01	0.02	0.30	25,13	1.86	<0.01	<0.01	0.03
10455	20.0		3610		70	2689	25	-01		17	23850	46	43	7	34	247	<0.1	2	10	<0.01	0.04	0.04	18.02	0.14	0.04	<0.01	0.02
19455	20.0		80 10		54	464	50			30	0.92		86	87	42	-5	0.1	2	12	0.12	2.12	0.72	5.46	1.90	0.30	0.02	0.06
19456	0.8				5	40		-0.1			412			127	46	-	0.1	3		0.23	2.24	0.39	9.13	1.83	0.11	0.01	0.09
19457	0.9	<1	002		82	10	10	<0.1	00	120	4.00				40	-5	0.1			0.03	242	0.07	23.16	្លាំណ៍	0.12	-0.01	0.08
19456	15.0	2	2022	ಿಂ	1/3	445	30	<0.1		320	2400	25			-		0.1	· ·	820	0.00	6. TE	0.07	20.00	88. A.S.	V. 12		0.00
			0.000		494			~ 1		97	1304		46	100	57		0.2	ه ا	1 - A	0.05	2 46	\$ 72	1100	1.9.1	0.27	0.01	0.20
19459	1 11		230		104	<3	ີ	<0.1			1007	2	22	454	54	-5	0.2	5		0.05	2.47	2.50	10 23	2 04	0.22	0.02	0.29
19460	1.1	<1	200	Р	231	<0	3	<0.1	20		1092		23				0.2			0.00	1.27	0.00	15 70	87. A	0.16	-0.01	0.07
19461	3.8	1 1	2029	S 1	135	<0	8	<0.1	~	14	29002	13	21	<u>عي جو</u>	40				66	-0.01	1.40	1 22	804	0.04	0.10	-0.01	0.04
19462	3.8	5	140		2.1/9	6/2	ני ו	104.3		12	6294		107		475					0.01	1.40	0.85	2.66	0.00	0.10	0.06	0.00
STD-P1	0.2	62	26	<b>49</b>	153	21	•	Ų.9		1 1	012	~	107	30	1/5	<3	0.5	°		0.10	1.00	0.00	2.00	0.00	0.30	0.00	0.00
					404					26	20750	~~~~			57	-5	0.5	41		0.02	154	0.53	11.00	1 12	0.20	10.05	0.05
19463	111	3	4/2				10	0.0		35	20150	174		5	45	+ 120	0.0			0.02	0.05	0.15	5 04	0.57	0.33	-0.01	0.08
19464	49.0	20	387	232/	6.50%	849	16	000.4		"	8112	1/4		<b>9</b> 2	40	1130	0.2	1 5		0.00	1.09	2.10	20.25	0.81	0.00	-0.01	0.04
19465	3.8	2	1219	40	1142	104	"	7.4		302	1003	42	10	20	19	20	0.3			-0.03	1.00	2.00	5 10	0.07	0.00	-0.01	0.04
(BJR-1	0.2		33	23	299	28		1.9			400		22	С	39		0.1			0.01	0.12	0.06	7 62	0.02	0.00	20.01	0.02
BJR-2	<0.1	<1	37	×	96	40	<0	0.3	•	38	00	ຸ	-0			~	<0.1	'			0.12	0.00	7.02		0.02	~~~	0.02
	-0.	,	42		713	79		24			208	7	70	a and	95	8	02		37	<0.01	0.12	0.03	3,15	0.04	0.06	<0.01	0.01
	1				402	40		24		1 7	264		54		37	5	0.2	Å	L Г.	<0.01	0.20	0.03	3 16	0.04	0.22	<0.01	0.02
	1.0		17	دع 55	170	224	70	8.9		1 1	63		04		67	5	<0 1	2	l 🖾 🖌	0.02	0.14	0.02	3.03	0.02	0.23	<0.01	0.01
	0.0	"		10	3/0	200	<b>'</b> °	0.2		1	829		23	<b>2</b> 2	80	65	0.3	Å	260	<0.01	1.33	7,10	2.87	0.64	0.20	0.02	0.11
		2	80	40	82	10		0.7			822		21	21	70	-5	0.3	1 7	257	<0.01	1.24	8.85	2.73	0.61	0.19	0.02	0.10
DLH-0-	0.1		80	<b>P</b>	~	, 's	°	0.0			044	~				<b>—</b>	0.0	1 .	120.0								
	0.5	_				<u>م</u> ا	44				200		أمعا	18 - A	44	-5	0.5	12	17	0.02	1.09	0.17	2.34	0.84	0.08	0.04	0.05
	0.5		302	10	16			0.0	1000	2	763	2	28	20 m	30		0.2		100.14	0.06	0.46	2.64	3.14	0.22	0.10	0.02	0.12
	0.8		302		140			0.0		30	1174	1	49	220	121	1.5	0.7		1	0.23	4.83	1.38	6.67	2.50	2.56	0,13	0.18
GS-49	0.8	3	1 101		140	<0	<b>S</b>	0.1		1	11/0	<b>4</b>	90		87		0.2		28 1	20.01	0.20	3.77	3.61		0.08	0.01	0.03
GS-50	1.5	3	137		141	33	1 1	1.3		1 7	1004		27	<b>1</b>	404		0.0		<b>1</b>		0.52	0.15	342	0.30	0.00	-0.01	0.05
GS-51	1.5	2	64		103	10	•	1.2		i ¥	314	~	- 34		124	~~	0.5	•		<b>~~</b> .~'	0.00	0.10	0.72	0.00	V. 12		0,00
										1 -	400	-			40	-	0.2		<b>.</b>	0 12	0.76	041	3.00	1.01	0 10	0.03	0 12
GS~52	1.1	15	75	12	58	116	<5	0,5	22	1 1	438	2	30				0.3	1 1	L	0.12	0.70	0.1	255	0.52	0.10	-0.01	0.10
GS-53	1.0	18	64	<b>1</b>	108	23	13	1.0	e v	1	100		46	<b>B</b>	69		0.2	1	<b>1000</b>		0.05	2.65	1.00	0.00	0.08	-0.01	0.00
GS-54	0.8	5	22	29	80		<5	1.3	1980 <b>14</b>	5	786		81	0		<5	0.1		200	0.01	0.08	2.05	6.70	0.00	0.00	0.01	0.00
GS-55	1.3	4	167	43	52	25	8	0.5	42	34	1765	5	12	<b>53</b>	89		0.8	9	108	<0.01	0.41	1,98	5.76	2.40	0.20	0.02	0.23
GS-55*	1.4	5	172	47	52	] 23	7	0.5	100044	34	1772	6	11	- 54	99	) <s< td=""><td>0.7</td><td>) <b>°</b></td><td>]<b>∏</b>712</td><td>&lt;0.01</td><td>0.42</td><td>8.25</td><td>8.03</td><td>2.40</td><td>0.20</td><td>0.02</td><td>0.24</td></s<>	0.7	) <b>°</b>	] <b>∏</b> 712	<0.01	0.42	8.25	8.03	2.40	0.20	0.02	0.24
			L		<u> </u>	1		L		L	<u> </u>	1	L	343	L	J	L		<u>1997.</u>	1	L	<u>ا</u>	L	1997 O.M. 19			i

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Project/Venture:	1P	Geologist:	K TROCIUK	Date Received:	JULY 22, 1992	Page	4	of	8
Area:	COREY	Lab Project No.:	D2499	Date Completed:	AUGUST 20, 1992	Attn:	K TROC	IUK	
Remarks:							S HOFF	MAN	
Au - 10.0 g sample digested	I with Aqua Regia and determined by Graphite Furre	ICO A.A. (D.L. 1 PPB)					J KOW/	<b>LCHUK</b>	
ICP - 0.5 g sample digested	with 4 ml Aqua Regia at 100 Deg. C for 2 hours.						E KIMU	RA	
N.B. The major oxide elemen	ts, Ba, Be, Cr, La and W are rarely dissolved compl	etely with this acid disc	olution method.						

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SAMPLE	<b>i</b> '	Ag	Мо	Cu 🎇	Pb	Zni	- As	Sb	Çd	N	Co	Mn	84	Cr		Be.	i w i	8e	لما	ંક	ותן	A	04	Fe	<b>Ma</b>	- K	Na	P
Na	L	ppm	ppm	ppm 🛐	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<b>%</b>	%	<b>%</b>	%	8	<u>%</u>	%	<u>%</u>
GS-56		1.0	5	222		- 99	<5	11	<0, 1	22	23	972	8	24	214	163	<5	0.6	7	41	0.23	3.56	1.21	6. 15	1.06	1.64	0.12	0, 18
GS-57		7.0	8	43	847	159	- 32	10	1.8	11	7	147	~2	92	27	89	<5	0.5	8	<b>41</b>	0.02	0.43	0.25	2.16	0.12	0.24	0.01	0.09
GS-58	1	3.7	- 54	1758 🛞	<b>*1</b>	43	8	16	<0.1	85	231	225	23	65	39	15	<5	0.5	6	- 25	0.05	0.95	0.93	12,92	0.12	0.07	0.01	0.07
GS-59	i '	0.4	3	24	23	7	12	<5	0.5		4	29	~	49	2	87	<5	<0.1	8	<b></b> 5	<0.01	0.10	0.02	1. 18	<0.01	0.17	0.03	0.01
GS-60		0.6	3	23	8	6	15	<5	0.3		<1	36	<2	43	3	114	<5	0.1	6		<0.01	0.12	0.02	2.39	<0.01	0.19	0.05	0.03
															× * *													
GS61		0.2	- 4	9	6	93	27	8	0.2	9	5	463	2	21	16	165	<5	0.3	8	32	<0.01	1.01	0.39	5.69	0.33	0.22	0.04	0.24
GS62	1	2.0	2	4 📖	1847	2207	<5	<5	9.6	3	- 4	278	<2	64	2	12	<5	<0.1	2	34	<0.01	0.14	0.44	1.20	0.08	0.02	0.04	0.07
GS-63	1 '	0.3	9	8	37	113	16	10	0.1	11	5	139	3	15	18	72	<5	0.2	5	<b>1</b>	<0.01	1.45	0.40	6.47	0.67	0.20	0.05	0.23
GS-64		0.4	8	14 🕅	14	107	21	<5	<0, 1	11	8	559	2	26	34	64	<5	0.2	5	93	<0.01	1.37	1.03	6.66	0.82	0.10	0.05	0.23
STD-P1		0.3	66	25	48	152	19	8	0.7	34	6	553	~2	103	34	176	<5	0.4	6	82	0, 10	1.03	0.84	2.22	0.86	0.37	0.06	0.06
GS-65		0.4	3	11	522	223	ব্য	<5	1.4	5	3	160	5	103	9	11	<5	0.2	5	16	<0.01	0.22	0.26	1.09	0.09	0.02	0.03	0.03
GS-66	]	0.4	<1	14 🔯	2	60	<5	<5	<0, 1		2	426	2	136	22	53	<5	<0.1	1	- 29	<0.01	1, 19	0.21	3.57	0.53	0.07	0.03	0.08
GS-67		<0.1	11	8 🛞	2	37	11	7	<0.1	10	<1	91	<2	18	20	98	<5	0.2	3	24	<0.01	1.13	0.29	7.24	0.44	0.26	0.04	0.26
GS-68		0.1	11	16	<1	121	<5	11	<0.1	12	9	420	5	11	24	20	<5	0.2	3	44	<0.01	1.72	0.70	8.72	0.88	0.15	0.04	0, 19
GS-69		.0.1	11	11		47	<5	7	<0.1	9	2	207	5	4	16	109	<5	0.3	4	57	<0.01	1.40	0.81	6.46	0.56	0.31	0.02	0.33
GS-70		<0.1	4	5	<1	18	15	6	<0, 1	6	<1	101	5	24	5	91	<5	0.1	5	8	<0.01	0.52	0.12	4.62	0.19	0.25	0.04	0, 13
GS-71		0.1	3	7	<b>(1</b> )	14	<5	<5	<0.1	4	<1	96	2	29	9	82	<5	<0.1	6	3 13	0.01	0.46	0.15	3.07	0, 17	0.17	0.04	0, 12
GS-72		<0.1	2	20	13	52	<5	10	0.3	3	<1	29	2	31	2	54	<5	0.3	16	2	<0.01	0.22	<b>&lt;0.01</b>	1.73	0.01	0, 15	0.02	0.02
GS-73		<0.1	<1	6	7	1	21	7	0.5	3	<1	14	3	63	2	93	<5	<0.1	8	3	<0.01	0.17	<0.01	0.78	<0.01	0.11	0.04	<0.01
QS-73*	•	<0.1	2	5	6	<1	17	ব্য	0.4	1	<1	15	2	62	<1	89	<5	<0.1	6	1	<0.01	0, 14	<0.01	0.64	<0.01	0.11	0.04	<0.01
GS-74		0.1	6	11	25	19	69	8	0.6	9	4	39	4	31		121	<5	0.5	13		<0.01	0. 19	0.02	2.58	0.03	0.13	0.03	0.03
G\$75	1	< 0.1	2	4	811	19	24	<5	0.4		<1	28	2	46		93	<5	0.1	8	12	<0.01	0.11	<0.01	1.75	<0.01	0.14	0.03	0.02
GS78		< 0.1	6	11	16	10	7	5	0.8	6	3	52	2	75	8	107	<5	0.4	12	9	<0.01	0.15	0.02	0.53	0,01	0.14	0.03	< 0.01
GS-77		<0.1	5	9 🕅	17	45	9	<5	0.6	8	3	65	2	46	8	45	<5	0.3	8	10	<0.01	0.19	B0.0	2.75	0.06	0.07	0.04	0.03
GS-78		0.1	6	5		13	12	7	0.5	5	<1	74	2	102	1	40	<5	<0.1	4	3	<0.01	0,09	0.01	1.52	<0.01	0.06	0.02	<0.01
GS-79		0.3	68	4	17	17	16	ব	0.4	1	<1	47	2	36	2	52	<5	0.1	6	<b>11</b>	<0.01	0, 13	0.12	2.92	0.01	0.11	0.02	0.02
GS-80		0.2	14	7 🕅	5	69	14	7	0.3	10	7	280	2	26		69	<5	0.2	6	66	<0.01	0.85	0.76	5.50	0.38	0, 16	0.04	0.26
GS-61	l I	0.1	5	4 ₩	10	25	21	11	0.3	6	<1	94	2	31	10	87	<5	0.2	8	11	0.02	0.21	0.04	3.62	0.03	0.15	0.03	0.09
GS-62		0.1	2	2	6	- 11	13	7	0.4		<1	27	2	42	3	165	<5	<0.1	5	10	<0.01	0.13	<0.01	2,14	<0.01	0, 19	0.05	0.05
G\$-82*		0.1	3	4	7	12	17	শ্	0.5	5	<1	31	2	43	5	162	<5	0.1	6	1	<0,01	0.13	0.01	2.14	0.01	0. 19	0.05	0.05
GS-83		<0.1	9	18	14	41	24	<5	0.7	15	12	518	2	27	15	133	<5	0.7	16	35	<0.01	0.55	0.20	3.27	0.26	0.24	0.04	0. 13
GS-84	1	0.1	1	3	<b>31</b>	7	<5	<5	0.6	3	<1	103	2	133	2	6	<5	<0.1	1	26	<0.01	0.03	0.30	0.37	0.01	0.01	<0.01	<0.01
GS-85		<0.1	4	33 🕅		40	<5	<5	0.5	10	6	1130	2	91	14	19	<5	0.1	3	243	<0.01	0.68	2.85	2.63	0.53	0.03	0.02	0.02
GS-86		<0.1	3	7 💹		32	5	<5	0.8	5	3	408	2	151	6	16	<5	0.2	5	53	<0.01	0.09	0.81	0.46	0.05	0.03	<0.01	0.02
GS-87		0.1	4	178		40	11	8	0.6	24	10	707	4	102	25	35	<5	0.3	5	271	<0.01	0.91	2.87	2.36	0.80	0.07	0.01	0.04
GS-68		<0.1	5	59	4	37	<5	<5	0.7	8	6	644	2	89	12	12	<5	0.1	2	305	<0.01	0.35	3.82	1.47	0.28	0.03	0.01	0.02
GS-89		<0.1	6	108 🕺	7	18	<5	<5	0.5	16	8	971	2	75	11	15	<5	0.1	2	<b>49</b> 1	<0.01	0.26	4.98	2.26	0.23	0.03	0.01	0.04
GS-90	{	<0.1	3	58		20	8	<5	0.5	18	7	559	2	102	13	58	<5	0.1	4	226	<0.01	0.56	2.52	1.91	0.39	0.13	0.01	0.06
GS-91		0.1	- 4	37 🕺	3	18	<5	<5	0.5	10	4	299	3	94	28	38	<5	.0.1	2	47	<0.01	0.63	0.73	1.77	0.46	0.07	0.03	0.07
GS-91*		0.1	2	37	2	18	ব	<5	0.4	1	4	300	3	96	28	39	<5	<0.1	2	48	<0.01	0.65	0.72	1.79	0.46	0.07	0.03	0.07
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Project/Venture:	1 <del>P</del>	Geologist:	K TROCIUK	Date Received:	JULY 22, 1992	Page	5	of	8
Area:	COREY	Lab Project No.:	D2499	Date Completed:	AUGUST 20, 1992	Attn:	K TROC	UK	
Remarks:							S HOFFI	MAN	
Au - 10.0 a sample digested	t with Agua Regia and determined by Graphite Furm	ace A.A. (D.L. 1 PPB)					J KOWA	LCHUK	
ICP - 0.5 o sample digested	with 4 ml Agua Regia at 100 Deg. C for 2 hours.	•					E KIMUF	A.	
N.B. The major oxide elemen	ts, Be, Cr, La and Ware rarely dissolved comp	letely with this acid dis	solution method						
Ag Mo Cu Ph	70 As Sh Cd Ni Co Mn	BI Cr	Ba W Ba	La Sr 1	Al Ca Fe	Ma	K	Na	P

SAMPLE		Ag	Мо	Cu Pl	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	V	Ba	w	6e	ما	ୢଽ	π	A	Ca	Fe	Mg	K	Na	P
No.		ppm	ppm	ppm pp	n ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	*	%	<b>%</b>	*	~~~	- %	<b>%</b>	<u>%</u>
G\$-92		0.2	10	60	9 112	38	9	<0.1	28	16	1009	4	19	14	78	<5	0.3	5	10	<0.01	1.06	0.15	7.58	0.26	0.14	<0.01	0.10
GS-93		0.1	30	29	3 42	<5	<5	<0,1	13	3	142	4	15	B	57		0.2			0.03	0.32	0.05	5.00	0.03	0, 18	<0.01	0.06
GS-94		0.8	2	47	0 59	33	9	<0,1	13	7	320	6	28	29	48	<0	<0.1	1	10	<0.01	1.40	0.14	3.00	0.80	0.10	0.02	0.11
GS-95		0.2	1	33	1 71	<5	<5	0.2	8	6	345	3	56	35	47	<0	<0.1			<0.01	1.12	0.62	3.32	0.64	0.06	0.03	0.00
GS-96		0.5	1	39	7 51	9	8	<0.1	11	10	365	5	71	32	80	<5	<0.1	י	21	<0.01	1.09	0.42	4.09	U.71	0.13	0.02	0, 14
					*											i _	l	_							A 07		
GS-97	1 1	0.3	2	48	9 145	13	10	0.5	12	12	470	3	92	32	83	<5	0.3	8	55	<0.01	0.98	0.58	2.25	0.81	0.07	0.01	0.05
GS-96	.	0.1	2	6 1	1 12	8	5	0.7		2	31	2	63	5	67	<0	0.2	10		<0.01	0.15	<0.01	0.60	0.04	0.08	0.03	0.02
GS-99		<0.1	2	<1	0 5	6	9	0.5	2	<1	10	<2	51		66	<5	<0.1	יי ן	SS 3	<0.01	0.09	<0.01	0.60	<0.01	0.10	0.03	<0.01
GS-100		2.0	12	6 📖	6 44	35	19	<0.1	<b>9</b>	<1	<1	2	31	<b>1</b>	64	<5	0.1	4	l	<0.01	0.14	<0.01	5.81	<0.01	0, 15	0.03	0.02
GS-100*		2.0	12	6	3 43	35	23	<0,1	8	<1	<1	2	30	<1	62	<5	0.1	4		<0.01	0.14	<0.01	5.49	<0.01	0.15	0.02	0.01
l						l	Į.	Į																			
GS-101		<0.1	4	18	0 92	14	7	1.1	13	8	218	3	94	15	49	7	1.1	19	33	<0.01	0.81	0.29	2.04	0.47	0.13	<0.01	0.01
GS-102		<0.1	5	16	5 91	7	6	0.4	13	10	1068	5	55	34	102	<5	0.5	14	633	<0.01	2.04	3.19	4.46	1.23	0.06	0.01	0.1/
GS~103		<0.1	8	18	6 150	5	<5	0.5	14	17	1420	9	13	37	110	<5	0.8	17	103	0.02	1.84	2.27	6.43	0.52	0.13	0.02	0.26
GS-104		0.1	3	8	8 91	<5	<5	0.2	10	7	835	7	75	17	89	<5	0.2	7	438	<0.01	1.86	2.56	4.38	L 17	0.07	<0.01	0.14
GS-105		.0.3	6	9	7 36	16	<5	<0.1	23	4	306	5	29	13	25	<5	<0.1	4	54	<0.01	0.45	0.53	6.26	0.25	0.02	0.04	0.11
{					20 20	{	<b>\</b>	ļ –										{ _				{					
GS-106		0.4	<1	75	1 52	6	<5	0.2	10	10	494	<2	80	13	32	<5	0.1	2	8	<0.01	0.52	0.12	3.67	0.21	0.06	0.02	0.07
GS-107		0.8	2	54	1 53	59	<5	0.2	12	12	691	5	72	35	80	<5	0.1	2	76	<0.01	1.09	1, 12	3.60	0.68	0.09	0.02	0.10
GS-108		1.0	<1	37	2 122	66	<5	<0.1	12	5	341	4	18	18	79	<5	<0.1	4	9	<0.01	0.45	0,17	5.39	0, 17	0.23	<0.01	0.19
GS-109		0.9	3	196	3 444	29	<5	1.4	17	12	504	7	20	48	40	<5	0.2	2	10	0.09	1.35	0.29	7.56	0.90	0.18	<0.01	0.16
STD-P1		0.3	64	24	9 153	20	7	0.7	36	6	563	2	99	34	174	<5	0.4	6	83	0.10	1.03	0.86	2.31	0.86	0.35	0.06	0.08
1	1 1	1	۱.			1	1	1					1 1		1	1	1	1	<b>N</b>	1	1	1				] ]	
GS-110	l i	1.4	19	255	<b>4</b> 80	14	<5	0.4	12	9	483	7	12	34	50	<5	0.3	6	10	0.07	1.09	0.27	4.50	1.20	0.15	0.02	0.12
G\$-111		1.6	<1	23	2 93	48	<5	<0.1	13	3	271	4	18	35	85	<5	<0.1	2	7	0.12	0.74	0.11	6.52	0.69	0.15	0.02	0, 15
KK79	!	0.7	<1	57	0 76	39	<5	0.3	25	18	406	4	26	41	56	<5	0.1	3	19	0.10	0.85	0.92	4.25	0,65	0.21	0.01	0, 16
KK80	[	12.0	<1	66 2	4 465	134	11	0.2	26	10	747	12	24	11	37	<5	0.1	2	31	0.04	0.26	1.21	10.15	0.04	0.25	0.01	0.13
KK-81		1.1	4	37	109	34	<5	0.3	14	7	161	4	16	9	53	<5	<0.1	2	30	0.08	0.23	0.99	4.26	0.02	0.24	0.01	0.14
										1		[				_	1		1222							ا مم ا	
KK-82	Į –	0.5	2	32	25 88	35	<5	0.2	15	6	299	3	38	13	104	<5	0.1	2	22	0.05	0.69	0.45	3.87	0.42	0.20	0.01	0.18
KK83		0.6	2	68	5 92	45	<5	0.5	33	16	1061	7	38	31	89	<5	0.2	2	101	0.06	1.21	2.68	4.42	0.95	0.18	0.01	0.15
KK-84		0.5	2	49	4 92	21	<5	0.2	20	15	953	5	14	61	64	<5	0.1	3	83	0.05	0.64	2.46	3.99	0.37	0.19	0.02	0.16
KK65		0.5	<1	243	7 85	27	<5	0,8	13	9	470	⊲2	52	9	78	<5	<0.1	!	46	<0.01	0.24	0.70	1.96	0,17	0.14	0.02	0.13
KK-85*	1	0.5	1	245	4 85	28	<5	0.8	13	9	464	2	53		80	<5	<0.1	1	47	<0.01	0.24	0.69	1.97	0.17	0.14	0.02	0.13
	l l					1	1	1		:					· ·				1230								1
KK-86		1.4	5	48	7 37	47	<5	<0.1	12	6	537	<2	1 11	14	81	<5	0.1	4	81	<0.01	0.26	0.67	4.93	0.06	0.29	0.01	0.27
KK87		1.1	4	137	7 75	25	7	<0.1	21	16	1016	<2	14	83	96	<5	0.1	4	57	0.05	1.69	1.63	7.72	1,39	0,14	0.01	0.18
KK-88		60.0	4	1.20%	2 200	1012	51	<0.1	49	34	352 19	4 13	3	13	8	<5	<0.1	5	22	<0.01	0.07	0.10	25.70	0.69	0.02	<0.01	0.04
KK-89		9.0	<1	95 📖	£ 49	7.69 9	55	<0,1	47	110	12143	30	39	13	22	<5	<0.1	6	29	<0.01	0.45	0, 10	16.55	0.60	0.06	<0.01	0.02
KK-90		3.7	5	676	2 231	651	<5	1.0	10	2	3495	26	62	<b>*</b> 1	25	<5	<0.1	2	3	<0.01	0.45	<0.01	5.18	0.18	0.03	0.03	<0.01
	1	{	1									l I				1			1888 B								i
KK-91		1.4	<1	849	1 94	56	11	<0.1	136	79	673	10	61	136	33	<5	<0.1	1	10	0.27	2.36	0.35	11.39	1.61	0.11	<0.01	0.08
KK-92		4.9	<1	1063	5 77	7	<5	<0.1	51	6	572	13	40	143	66	<5	0.1	2	25	0.42	1.66	0.28	12.53	0.98	0.17	<0.01	0.06
KK-93		0.7	1	85	4 7	6	8	<0.1	15	7	933	< 2	18	60	88	<5	0.1	<1	8817	0.08	1.72	0.39	4.60	1.38	0.22	0.02	0.16
KK-94		2.4	<1	462	6 55	16	<5	<0.1	43	24	474	11	24	118	101	<5	<0.1	1	20	0.35	1.24	0.54	12.98	0.73	0.21	0.01	0.07
KK-94*		2.4	<1	462	10 54	i <b>] 17</b>	<5	<0.1	44	25	468	8	26	118	106	<5	0.3	4	22	0.34	1.21	0.54	12.74	0,72	0.20	0.01	0.07
	1				10 A							L		SSS:-	1		<u> </u>		120	1							<u> </u>

# Geochemical Analysis

Project/V	enture: 1P	Geologist:	K TROCIUK	Date Received:	JULY 22, 1992	Page	6	of	8
Area:	COREY	Lab Project No.:	D2499	Date Completed:	AUGUST 20, 1992	Attn:	K TROC	IUK	
Remarks:							S HOFF	MAN	
Au - 10.0	) g sample digested with Aqua Regla and determined by G	isaphite Furnace A.A. (D.L. 1 PPB)	1				J KOWA	LCHUK	
ICP - 0.5	g sample digested with 4 ml Aqua Regia at 100 Deg. C fo	r 2 hours.					E KIMU	RA	
N.B. The	major oxide elements, Ba, Be, Cr, La and W are rarely disa	olved completely with this acid dis	solution method.						

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SAMPLE		Ag	Mo	Cu	Pb	Zn	As	SP	Cq	<b>N</b>	Co	Mn	BI	Cr	<b>V</b>	Ba	l w	Be	لقا	ૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢૢ		A	Ca	re	⊗ Mg ≥	N I	Na	P
No.		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррпі	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<u>×</u>	%	<b>%</b>	<u>%</u>	<b>%</b>	<u>%</u>	%	<u>%</u>
KK-95		1.6	<1	29	54	47	49	<5	0.5		6	260	- 4	15	28	97	<5	0.4	7	U	0.12	0.46	0.25	3.09	0.13	0.25	0.01	0,16
KK-96		1.2	5	215	7	3178	59	9	13.8	35	26	1854	19	20	85	17	<5	0.2	2	•	0.05	3.08	0.30	12.57	2.48	0.09	0.01	0.15
KK-97		0.3	8	12	10	48	43	<5	0.5	6	1	61	4	52	4	86	<5	0.2	9	8	<0.01	0.23	0.04	1.94	0.05	0.21	0.04	<0.01
KK-08		0.5	7	7	11	24	35	9	0.4	5	<1	43	2	37	2	105	<5	0.1	9		<0.01	0, 13	0.01	2.17	0.02	0, 18	0.03	0.01
KK-00		0.7					34		0.2		21	28	- 2	47	2	106	6	0.2	6		<0.01	0, 19	<0.01	2.42	<0.01	0.25	0.03	<0.01
VV-93		0.7	ଁ	<b>-</b>		1 '	<b>~</b>	~					-			,			- T									
														~					10		المصا	0.40	ا مم	101		0.22	0.05	0.00
KK-100	]	0.2	3	11	21	1 1	1 41	<0	0,0		3	4/	~2	20	8 <b>.</b> .	104		0.3		l	-0.01	0.10	0.02	1.01		0.20	0.00	-0.01
KK-101		0.1	5	11	1	13	47	<5	0,5		3	49	~2	42	3	117		0.3	1 1		<0.01	0.10	0.01	1.09	<b></b>	0.17	0.04	<0.01
KK-102		<0.1	2	3		7	6	<5	0,5	3	<1	67	~2	125		90	<b>S</b>	<0.1	5		<0.01	0.13	0.01	0.52	<u.u1< td=""><td>0.11</td><td>0.03</td><td>&lt;0.01</td></u.u1<>	0.11	0.03	<0.01
KK-103		0.1	3	1	3	8	20	<5	0.4	3	<1	15	<2	65		127	<5	<0.1	1 7	1988 <b>•</b>	<0.01	0.13	<0.01	0.90	<0.01	0, 14	0.02	<0.01
KK-103*	Í	0.1	4	<1	5	8	19	5	0.4	3	<1	17	<2	69	1	132	<5	<0.1	7	4	<0.01	0.13	<0.01	0.98	<0.01	0, 14	0.02	<0.01
								1																		. /		
KK-104		0.6	່ 5	່ ອ່	137	34	62	<5	0.6	6	1	) 38	2	60	3	55	<5	0.3	9	12	<0.01	0.22	<0.01	2.24	0.02	0.18	0.05	0.01
KK-105		0.9	1	33		144	116	14	0,5	22	4	22273	16	133	11	17	<5	0.3	9	5	<0.01	0.04	0.13	9.53	0.97	0.01	<0.01	0.02
KK 106		04	24	16	6	34	84	11	0.4	13	4	364	5	65		27	<5	0.5	12	8	<0.01	0.17	0.02	4.59	0.04	0, 15	0.03	<0.01
KK-107	1	0.4		4		11	35	الحم ا	0.3		- 1	130	0	77		36	<5	0.2	5		<0.01	0.18	<0.01	2.97	0.02	0.14	0.04	<0.01
		0.4			5	11	27		0.3	à	21	54		68		38	-5	0 1	5		20.01	0 15	0.02	2.81	0.01	0.12	0.03	<0.01
NN- NO	i i	. 0.3	''	· ·			<b>-</b>	<sup>~</sup>	0.0			<u>ا ۳</u>	~	~		~												
KK 400	1 '	1		440		207	54	1 47	27		45	246	14	97		17	-5	ا م	) 🦻	132	-0 01	0.61	346	11.09	0.47	0, 19	ിരന്നി	0.06
KK-109		0.3	00			307	150		2.1		1.0	97	17					0.4			-0.01	0.17	0.40	12.26	0.00	0.12	0.03	0.01
KK-110		0.1	42	22	<b>*</b> 1	38	150	10	<0.1	-	<1	37	10	4.3	<u> </u>	-		0.2		2	-0.01	0.17	0.04	1.20		0.12	0.00	0.01
KK-111	1	Q. 1	<1	5		18	13	<5	0.4	•	<1	36	<2	40	ž		<0	0.3		2	<0,01	0.31	0.05	1.00	0.02	0.31	0.02	0.02
KK-112		1.7	28	30	65	87	145	16	<0, 1	<b>2</b> 2	4	56	26	21	3	3	<0	0.2	3		<0.01	0.1/	<0.01	17.73	0.02	0.10	<0.01	0.02
KK-112*	1	1.7	31	30	66	119	144	15	<0.1	33	4	58	27	22	3	2	<5	0.2	3	2	<0.01	0.18	<0.01	16, 12	0.02	0.201	<0.01	0.02
	1	1	1 '	1			1	1 1				1				۱	1 _	1	Ì.				1					
KK-113		0.1	<1	11	6	76	1699	<5	<0.1	<b>19</b>	8	11134	7	111	40	42	<5	0.1	3	(V)	<0.01	1.77	0.70	7.53	0.00	0.01	<0.01	0.02
KK-114		9.0	2	64	58	97	1.51%	23	<0.1	35	24	26516	53	61	34	11	592	<0.1	4	92	<0.01	1.60	0.50	12.03	0.73	<0.01	<0.01	0.03
KK-115	1	0.3	2	25	2	118	0.37 %	7	<0.1	37	12	50705	29	36	24	22	16	<0.1	7	97	<0.01	0.82	0.29	18.23	0.78	0.02	<0.01	0.02
KK-116		1.1	1	91		105	0.57 %	<5	<0.1	32	16	28164	18	68	25	50	<5	0.1	4	50	<0.01	0.94	0, 16	15.45	0.64	0.08	<0.01	0.03
KK-117		0.5	3	72	3	100	0.30%	11	<0.1	42	9	38139	39	14	24	- 33	<5	<0.1	5	40	<0.01	0.59	0.24	23,17	1.33	0.05	<0.01	0.03
	1	1	1	1			1	1 '			1	}	1	1 1			1	1	]		6		1			1		
KK-118		1.4	2	45		78	0.319	< 5	<0.1	26	3	10511	15	25	17	325	<5	0.2	5	26	<0.01	1. 18	0.25	16.00	0.40	0.18	0.01	0.11
KK	i i	1.8	4	69	2	226	143	9	0.1	41	9	42003	41	21	13	81	<5	<0,1	8	37	<0.01	0,17	0.24	23.15	1.02	<0.01	<0.01	0.03
KK-120		0.4	1 <1	15	5	29	0.82%	<5	0.3	17	13	6216	2	177	12	21	<5	0.1	5	84	<0.01	0.40	0.69	4.13	0.19	0.01	0.01	0.02
KK-121		13	1	30	<b>,</b>	83	0.40%		<01	26	14	323 18	14	61	23	40	<5	<0.1	5	131	<0.01	0.92	0.18	11.74	0.43	0.02	<0.01	0.02
	1	1 1 2		27	50	149	23	<u>ہ</u> ۔ ا	0.5	35	5	611	0	98	31	174	<5	0.3	4	ВО	0.10	1.00	0.84	2.23	0.86	0.35	0.06	0.08
SID-FI	1	0.2	5	[ •'		1	1 -	<b></b>			1 -	1	-	1			1 ~	1	1									
KK 107			- 1	0.0		100	0.000			40	12	5 1200	42	42	21	20	5	0.3	14		40.01	0.32	040	17.48	1 13	0.02	0.01	0.03
NN-122	1	0.2		80		404	1 40 0				1 24	33005		45	20	20		0.4	1 11	70	40.01	103	0.21	15.86	0.80	0.04	<0.01	0.03
KK-123	[	0.5	8	39		124	1.127	10	<b>«</b> 0.1	<b>1</b>		20200	34	10	Contraction of the second	- 33			"			0.74	0.22	10 17	1 10	0.02	-0.01	0.03
KK-124	1	0.4	5	64	1	92	0.2/9	22	<0,1	<b>40</b>		32309	43	34		21	<ul> <li>&lt;3</li> <li>&lt;3</li> </ul>	0.3	2		-0.01	0.14	0.22	10.11		0.02	0.01	0.00
KK - 125	1	2.0	5	28	10	126	1.749	35	<0,1	39	23	23307	- 32	14	ĸ	53	<b>S</b>	0.2	1 1		<0.01	0.01	0.29	0, 12	u.o/	0.12	0.01	0.00
KK-126	1	0.4	6	27	1	99	0.36%	4 28	<0.1	40	9	37021	49	10	15	62	<⁵	0.1	]. <b>⊺</b>		<0.01	0.50	0.26	21.36	14	0.02	<0.01	0.04
	1		1									1			i an				1 .				0.00	10.00			-	0.02
KK-127		166.0	9	885	1081	78	27.39	q 375	<0.1	40	1096	855	143	9	1	8	1. 14	<0.1	2	20	<0.01	0.15	0.82	18.83	0.05	<0.01	<0.01	0.03
KK-128		3.3	2	41	41	36	1.849	<b>4 30</b>	0.1	14	23	5980	20	114	3	9	<5	<0.1	2	- 1888 F	<0.01	0.08	0.03	6.36	0.10	<0.01	<0.01	<0.01
KK-129	1	534.0	3	1,10%	634	707	6.47%	0.38%	19.8	83	70	5557	152	73	7	4	10	<0.1	3		<0.01	0.04	0.12	15.93	0.20	<0.01	<0.01	0.03
KK-130		13.0	8	0.37%	20	149	5.66%	63	1,1	27	20	14285	33	60	16	22	<5	0.2	4	1	<0.01	0.85	0.13	13.36	0.59	0.24	<0.01	0.05
KK-130*	1	13.0	A	0.379	21	150	5.66 9	6 51	1.0	27	19	14087	32	59	16	22	<5	0.2	5	1	<0.01	0.84	0.13	13, 15	0.59	0.24	<0.01	0.05
	1	1	<b>آ</b> ا	1			1	1			1								1	<b>1</b> 8880	1							

	Project/Venture: Area:		1P COREY	,						Geolog Lab Pro	jist; oject No.:	+ : C	( TROC )2499	IUK		Date R Date C	eceived omplete	: ad;	JULY 22 AUGUS	2, 1992 ST 20, 19	992	Page Attn:	7 K TRO	of CIUK	8
	Remarks: Au - 10.0 g sam ICP - 0.5 g sam N.B. The major o	ple digested ple digested xide element	with Aq with 4 m s, Ba, B	un Regi ni Aqua ie, Cr, Li	a and d Regia a a and W	etermine t 100 De 'are pare	ad by G ag. C fo aly diss	imphite r 2 hou solved	Furnac ns. complet	a A.A. ( toly with	(D.L. 1 Pl	PB) d dissol	ution n	nethod									s hof J kow E kimi	FMAN /ALCHU! JRA	ĸ
Т	Ag Mo	Cu Pb	Zn	As	Sb	Cd	Ni Ni	Co	Mn	BI	Cr	SV	Ba	W	8e	La	Sr	П	A	Ča.	Fe	Mg	K	Na	P
	ppm ppm	ppm ppm	ppm	ppm	ppm	ppm 🛛	ppm	ppm	ppm	ppm	ppm 3	ppm	ppm	ppm	ppm	рргп	ppm	%	%	%	%	<b>%</b>	%	%	%

SAMPLE		An	Ha	Cu	<b>Ph</b>	7n	A.	Sh	64	SSS MRSS	60	Mn	E AL	0	≪v~-	Be	W T	Be		27 <b>0</b> - 27		AL		E.	10 May 1	K	No	b
No		000	000	0.000		0.000	0000	000			000	0000		007	0.000	000		0.0			<u></u>	2		α.	8 <b>.</b> .	n. ex	1 Vel.	
KK-131	-	26.0	1	0.539		132	0 709	90		00	10	10600	35	4 4 0	<b>PP</b>	200	PP0			- ppen		0.00		70	0.20	0.02	70	0.00
KK 129		12.0		110		102	5 00 0	00	0.8			10033	64	20	i an	20		0.1	]	S	-0.01	0.00	0.00	8.38	0.32	0.03	<0.01	0.02
NN 102		13.0				105	7.45.00	07	1.8	40	44	10342	04	30		10	<0	<0.1	5	23	0.01	0.00	0.17	17.49	USJ	0.04	<0.01	0.05
KK-133		0.0	<1	02	30	42	1.1070	40	<0.1	<b>DU</b>	112	5123	- 34	40		14	<0	0.2	4	37	<0.01	0.42	0.64	15.29	0. TØ	0.05	<0.01	0.02
KK-134	1	2.9	<1	167	24	39	1.30%	16	<0.1	21	20	8073	16	50	<b>15</b>	55	<5	0.3	6	<b>31</b>	<0.01	0.75	0.76	9.91	0.32	0.27	<0.01	0.07
KK-135		5.2	5	25	35	61	6.50%	50	<0.1	52	120	30744	49	31	19	21	<5	0.2	6	29	≪0.01	0.37	0.18	19.01	0.49	0.04	<0.01	0.02
				]					ſ											38747								1
KK-136		94.0	7	3.12%	262	169	1.02%	146	1.2	46	47	20320	986	33	15	11	6	0.2	7	22	<0.01	0.21	0.11	19.96	0.57	0.03	<0.01	0.04
KK137		3.5	6	219	25	119	4.11%	69	0.2	43	29	31458	63	- 34	13	21	<5	0.2	9	26	<0.01	0.10	0.25	19.21	1.34	0.06	<0.01	0.03
KK-138	- I ·	126.0	9	2.28%	445	520	0.48%	91	5.4	45	51	19275	624	39	25	17	<5	0.2	7	<b>3</b> 41	0.01	0.40	0.28	21.03	0.51	0.21	<0.01	0.09
KK-139		2.0	3	189		62	0.31%	7	0.5	19	6	144 12	20	100	10	30	<5	0.1	5	27	<0.01	0.21	0.11	8.95	0.41	0.03	<0.01	0.02
KK-139*	1	20	2	185		62	0.31%	7	0.3	10	5	146 12	22	106		30	-5	<b>20 1</b>	3	ି 🧟	-0.01	0.22	0.11	0 12		0.03	-0.01	0.02
			· -	1			1		0.0		Ĭ		-				~~		Ŭ			0.44	, v.,,	·		0.00	~0.01	1
KK-140	1	26.0	8	0 75 %	55	202	1049	28	14	20	<b>1</b> 0	25602	71	98		40	-5	0.2	A	6	0.01	0.84	0.15	14 15	A BA	0.04	-0.01	0.03
KK-141		165.0		1811	650	71	1549	47	0.4		03	3605	682	07		12	-5	0.4			-0.01	0.12	0.10	17.06	0.07	0.07	-0.01	0.00
	,	122.0	2	0.59%	350	157	2 389	61	0.4		143	040	520	90		12		0.7				0.15	0.03	17.80	0.01	0.00	<0.01	0.03
		20.0		0.00 /	0.00	107	2.00 /		0.4	ಿಂದ	140	040	328	440		0		0.2	1		0.01	0.05	<0.01	20.03	0.03	<0.01	<0.01	0.03
KK-143		8.0		323	203	01	0.117	0	0.2			732	35	110	<b></b>	65	<>	0.4	8	૾ૻ૽ૻ	<0.01	0.43	0.10	1.27	0, 18	0, 19	<0.01	0.07
KK-144		56.0	24	0.36%	961	488	6.78%	490	7,9	52	49	19397	203	31		13	<5	0,1	7	8C1•	<0.01	0,10	0.12	22.26	0.62	0,06	<0.01	0.04
KK-145	'	100.0	1/	0.51%	367	1191	7.82%	255	21.0	97	37	28 122	123	18	<b>1</b> 1	16	<5	0.1	8	30	<0.01	0.16	0.13	21.83	0.63	0.09	<0.01	0.04
KK-146		8.0	8	304	285	661	2.76%	125	9.8	- 40	18	33435	61	20	1983 <b>1</b> 4	15	144	0.1	8	- <b>8</b>	<0.01	0, 10	0.21	19.82	1.60	0.06	<0.01	0.04
KK-147	. 1	12.0	- 4	136	508	4 14	4.09%	68	5.1	43	34	19073	51	44	10	22	<5	0.2	7	<b>X 12</b>	<0.01	0.17	0.16	15.38	0.70	0,14	<0.01	0.05
KK 148		3.0	5	52	152	136	0.89%	28	0.5	33	13	28892	37	65	15	19	55	0.1	7	24	<0.01	0.05	0.19	16.74	<b>%111</b>	0.02	<0.01	0.04
KK 148*	· [	2.9	4	50	151	134	0.89%	27	0.5	32	12	27898	- 38	62	14	18	52	<0.1	7	23	<0.01	0.05	0.19	16.26	1.06	0.02	<0.01	0.04
KK-140			2		466	70	1100	~				1020	97	~		40						0.07				0.00		
		8.0	2		60	10	11.07	82				1030	31	89		10	<5	0.5	14		<0.01	0.07	0.02	11.50	0.03	0.03	<0.01	0.02
KK-150		3.2	4	80	<b>2</b> 1	3399	1436	16	15.3	20	13	869	11	19	ిల	- 30	<>	0.4	9	33	0.09	0.52	0.51	7,60	0.26	0.36	<0.01	0.12
KK-151		3.7	2	46	88	56	1/86	8	0.7	19	14	515	9	42	16	43	<5	0.5	10	31	<0.01	0, 16	0.14	4.20	0.04	0.25	<0.01	0.05
KK-152		2.0	1	221	50	95	189	8	<0.1	20	6	539	11	18	52	97	<5	0.1	4	33	0.01	0.94	0.40	10.32	0.50	0.24	0.01	0.25
KK-153		2.2	1	52		20	116	<5	<0.1	25	17	129	9	21	27	17	<5	0.1	3	20	0.12	0.23	0.50	8. 16	0.04	0.22	<0.01	0.21
KK-154		2.1	4	239		444	119	<5	0.7	29	18	2038	3	21	98	19	<5	0.2	4	13	0.06	2.85	0.30	13.99	1.40	0, 13	<0.01	0.14
KK-155	1	11	<1	71	28	148	1168	18	<0.1	37	10	304.17	20	49	18	21	<5	0.1	7	43	<0.01	0.36	0.04	16 40	n 4a	0.05	-0.01	0.03
KK-156		11	4	1 19		80	0.48%	36	<01		13	38283	48	17	<b>10</b>	10	-5	01	7	20	0.01	0.18	0.18	21 04	0 97	0.02	-0.01	0.03
KK-157		21	1	59		38	80	9	-01	15	4	770		12	20 A 5	80	-5	01	i i	20	0.18	0.46	0.28	7 45	8731	0.23	-0.01	0.00
KK-157*	l l	22	- 1	59	AR.	37	70		-01	15		760		12		70	~5	0.1	3	20	0.19	0.45	0.20	7 28	8.30	0.20	-0.01	0.20
						•••		-	~~				ľ				~		Ŭ		<b>•</b> ••••	0.40	0.20	7.00		V.EU	~0.01	0.20
KK-158		47.0	4	2.06%		101	677	21	00	24	10	15827	63	16	10	14	31	0.4	14	34	0.01	0.08		17 55	0.04	0.04	0.04	0.04
KK-159		40.0	13	168 4		87	363	21	0.5	35	 А	22139	42	11		0	45	0.0	6	See.	-0.01	0.05	0.00	10.52	867	0.04	0.01	0.04
KK-460	1			397			6 22 94		0.5	1 - Sec.	່ກ	14070	37	30				0.5			-0.01	0.00	0.00	15.00		0.04		0.04
KK 161		7.7		1000	900	202	1 1 22 2	50	1.0		22	5744	444	- V-C - A-C		32		0.3			-0.01	0.17	0.11	14.10		0, 15	0.01	0.00
		10.0	2	0584	300	200	1.22 7	10	1.0		20	3/44	444	82	CI 😳	CI CI		0.4				0.06	0.02	11,53	0.00	0.05	0.01	0.03
INA- NC		10.0	. J	2001		100	0.31%	12	<0.1	<b>1000</b>	8	21311		20		3	<3	0.1	4		<0.01	0.02	0.02	19.09	0.09	0.03	0.01	0.02
KK-163		35.0	4	3371	345	579	1.61%	100	4,6	34	17	21378	304	43	11	14	772	0.1	4	27	<0.01	0.05	0.06	16.29	0 18	0.05	0.01	0.03
KK-164	13	314.0	2	1.63%	1214	864	9.67%	208	8.8	32	32	423	1286	48	6	5	21	<0.1	3		<0.01	0.05	<0.01	18.65	0.01	0.06	0.01	0.04
KK-164A	le	304.0	3	2.78%	1856	945	7.44%	298	13.1	32	30	56	2490	40	<b>6</b>	3	<5	<0.1	2	88 A	<0.01	0.02	<0.01	19.53	<0.01	0.04	<0.01	0.05
KK-165	[ `	4.5	∣ <1	235	42	32	934	ත්	0.9		2	2811	7	138	8 B	6	11	<0.1	1	18 A 1	<0.01	0.06	0.02	2.69	0.03	0.04	0.01	0.01
STD-P1		0.2	68	26	5.59	150	28	<5	10	20		559	3	105	36	179	7	0.5	7	82	0 10	103	0.86	2 28	0.84	0.36	0.04	0.09
	1	~~	~	<sup>-</sup>			<b></b>	~~			ľ	~~~				114	'		'I			1.00	0.00	£.20		0.00	0.00	0.00
					100 CO.		•		L	Proc.26020000	·						I	L			<u>د</u>		l		Second State of the			

Project/Venture:	1P	Geologist:	K TROCIUK	Date Received:	JULY 22, 1992	Page	8	of	8
Area:	COREY	Lab Project No.:	D2499	Date Completed:	AUGUST 20, 1992	Attn:	K TROO	CIUK	
Remarka:							S HOFF	MAN	
Au - 10.0 g sample dig	ested with Aqua Regia and det	ermined by Graphite Furnace A.A. (D.L. 1 PPB)					J KOW.	ALCHUK	
ICP - 0.5 g sample dig	ested with 4 ml Aqua Regia at	100 Deg. C for 2 hours.					E KIMU	RA	
N.B. The major oxide el	ements, Ba, Ba, Cr, La and Wa	tre rarely dissolved completely with this acid diss	borttem notulo						
-									

SAMPLE		10	Мо	Cu	Pb	Zn	As	Sb	Cd	N	Co	Mn	BI	Cr	V	Ba	W I	Be	La	Sr (	Π	A	Ca l	Fe	Mg	K	Na	P
<u>No.</u>	Р	om	ppm	ppm	ppm	ppm	ppm	_ppm	ppm	ppm.	ppm	<b>p</b> pm	ppm	ppm	ppm	ppm	ppm	ppm	ррт	ppm	%	%	%	%	ૢૢૢૢૢૢ	%	<b>%</b>	%
KK-166	8	5.0	<1	1.48 %	3 19	349	1.43%	35	5.4	35	15	12497	389	51	4	12	<5	<0.1	<1	10	<0.01	0.03	0.03	15.51	0.08	<0.01	<0.01	0.03
KK-167	1 10	.7	<1	148	<1	111	159	10	0.1	45	27	2505	11	53	92	54	<5	0.2	2	<b>8884</b> 1	0.02	3.88	1.40	6.77	3.19	0.00	<0.01	0.08
KK 168		.9	5	106	<1	67	112	18	0.5	33	7	27287	44	18	22	44	<5	0.1	3	18	<0.01	0,13	0.52	15.43	2.20	0.07	<0.01	0.06
KK-169	1 1	.8	<1	38		50	1.64 %	34	0.2	25	3	19938	30	57	10	6	<5	<0.1	1	3	<0.01	0.09	0.09	12.75	0.56	<0.01	<0.01	0.02
KK-170	1 1	.8	<1	37	<1	48	1.63%	20	0.2	23	2	17352	25	73	8	3	<5	<0.1	<1	2	<0.01	0.10	0.07	11.09	0.49	<0.01	<0.01	0.02
KK-171	10	3.0	<1	33	43	102	4. 18 %	45	0.1	28	11	6261	49	60	5	5	<5	<0, 1	16	2	<0.01	0.05	0.01	12.05	0.08	0.02	<0.01	0.03
KK-172		0	<1	44	73	317	3.11%	56	0.6	24	10	5771	27	44	2	14	<5	0.1	3	3	<0.01	0.18	<0.01	10.97	0.02	0.12	<0.01	0.08
KK-173		.8	<1	79	2	30	486	6	0.3	10	18	451	4	95	7	47	<5	<0.1	<1	B	<0.01	0.29	0.18	3.02	0.09	0.07	0.03	0.07
KK-174	2	1.0	4	365	89	465	3.61%	74	2.9	33	11	23740	56	16	7	34	< 5	<0.1	3	1	<0.01	0.26	0,17	16.09	0.69	0.11	<0.01	0.06
KK-174*	21	I.O [	2	366	- 89	469	3.61%	76	3.2	33	11	23434	57	17	8	34	<5	0.1	2	7	<0.01	0.26	0.17	15.94	0.71	0.11	<0.01	0.06
KK-175	20	3.0	5	499	91	628	7.36%	177	3.8	48	25	21213	75	22	17	30	7	0.3	8	14	<0.01	0.61	0.13	19.66	0.60	0.10	<0.01	0.05
KK-176	0	.7	2	92	<b>11</b>	45	221	8	0.3	18	19	1280	6	38	107	44	<5	0.2	7	65	0.14	0.95	1.91	4.82	0.86	0,10	0.02	0.28
KK-177		.3	<1	75	15	157	498	<5	0.9	19	13	988	4	16	31	43	<5	0.2	7	844	<0.01	0.72	0.42	4.33	0.32	0.26	<0.01	0.15
KK-178	1	.0	<1	83	43	89	125	6	<0.1	19	3	1089	12	26	114	88	<5	0.1	3	38 <b>-</b> 7	0.09	1.65	0.17	8.01	1.52	0.11	<0.01	0.17
KK-179	0	.6	<1	54	13	50	70	8	0.3	12	3	353	6	32	20	75	<5	0.2	4	42	0.13	0.39	2.78	5.02	0,10	0,18	0.02	0.13
KK-180	0	.5	8	58	14	99	91	<5	<0.1	19	8	664	9	20	65	60	<5	0.1	4	15	0.11	1.39	0.42	7.06	1.43	0,16	0.01	0, 19
KK-181		.4	7	677	29	329	128	<5	1.3	18	8	210	10	21	26	23	<5	0.1	5	1	0.08	0.49	0.32	7.19	0.16	0.23	<0.01	0.18
SSR-1	0	.1	<1	48	2	47	5	<5	0.4	59	23	313	7	59	82	45	<5	0.2	2	24	0.13	1.42	1.17	3.12	0.74	0.08	0.16	0.11
SSR-2		1	<1	141		54	5	<5	0.2	17	10	528	7	25	139	171	<5	0.3	4	19	0.23	1.71	0.97	4.91	0.96	0.31	0.10	0.13
SSR-2*	0	.1	<1	136	3	53	7	7	0.3	16	10	529	9	25	136	169	<5	0.3	3	10	0.22	1.67	0.93	4.79	0.94	0.31	0.10	0.13
SSR-3	0	.1	4	16	8	50	<5	<5	0.5	106	18	291	6	179	48	213	<5	0.2	з	48	0,13	3.34	1.65	2.20	1.57	0,44	0.22	0.03
SSR-4	<	0.1	3	69	2	36	1	<5	0.4	19	12	203	6 (	34	70	91	<5	0.1	4	38 k 4	0.12	1.02	0.39	3.61	0.80	0.16	0.05	0.00
SSR-5		0.1	10	48	4	85	1	<5	1.1	29	6	120	3	34	51	135	<5	0.1	4	10	0.14	0.75	0.47	2.50	0.47	0.18	0.06	0.08
SSR-6	1 10	3	10	18	14	116	29	9	1.4	15	3	922	2	75	28	14	<5	0.2	5	835	0.03	0.61	2.94	1.82	0.23	0.08	0.03	0.03
SSR-7	3	.4	9	1453	16	53	352	18	0.3	47	21	559	46	26	44	14	8	0.2	3	24	0.06	1.39	0.71	18.11	0.71	0.68	0.01	0.09
STD-P1	0	.3	67	25	52	145	22	6	0.8	34	6	598	4	106	34	171	<5	0.4	7	83	0, 10	1.04	0.89	2.35	0.82	0.33	0.06	0.08

Geochemical Analysis

Project/Venture:	1P	Geol:	K TROCIUK	Date Received:	JULY 22, 1992	Page	1	of	1
Area:	COREY	Lab Project No.:	D2498	Date Completed:	AUG 18, 1992	Attn:	K TROCH	UK	
Remarks:							S HOFFN	IAN	
Au - 10.0 g anmple digested	with Aqua Regia and determined by Graphite Furna	ce A.A. (D.L. 1 PPB)					J KOWAL	CHUK	
ICP - 0.5 g sample digested	with 4 mi Aqua Regia at 100 Deg. C for 2 hours.						E KIMUR	A	
N.B. The major oxide element	ta, Ba, Be, Cr, La and W are mirely dissolved comple	etely with this acld disc	solution method						

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SAMPLE	1	Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	Ni	Co	Mn	Bi	Çr	Y	Ba	W	Be	Le St	Π	A	Ca	Fe	Mg	K	Na	P
No.		ppm	ppm	ррт 🛞	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	_ppm	ppm	ppm	ppm ppm	%	%	%	%	%	%	%	%
19466		<0.1	<1	55	2	106	Ĝ	<5	Q. 1	21	19	569	2	43	152	17	<5	0.4	6 32	0.33	0.93	1.15	7.97	0.83	<0.01	0.04	0.13
GS-112		0.1	5	93 🛛	17	150	25	8	1.0	25	18	744	4	60	75	37	<5	1.0	25 17	0.16	1.70	0.34	5.20	1.59	<0.01	0.04	0.10
GS-113		<0.1	<1	45 📓	9	120	8	- 5	0,1	8	10	2111	2	43	15	135	<5	0.4	15	<0.01	1.38	0.36	5.27	0.96	0.18	0.03	0.15
GS-114	- 1	0.1	8	5	2	11	7	<5	0.2	5	3	13	2	39		164	<5	0.2	7 12	<0.01	0.21	0.02	4.81	<0.01	0.21	0.05	0.11
GS-115		0.1	2	42	5	10	6	<5	0.1	3	3	<1	⊲	40	3	102	<5	0.3	7 16	0.15	0.10	0.12	3.50	<0.01	0.17	0.04	0.10
KK-181		0.2	4	42	13	227	7	⊲5	1.6	16	9	222	2	66	106	18	<5	0.6	7 10	0.11	3.10	3.25	4.23	1.07	<0.01	<0.01	0.13
KK-182		1.4	2	22	3	146	8	6	1.0	11	6	2379	2	- 36	39	42	<5	0.2	4 7	0.08	0.55	7.07	2.90	0.31	0.10	0.02	0.07
KK-183		1.0	2	17	41	39	35	ব	0.1	5	1	46	~	82	25	53	<5	0.1	5 5	<0.01	0.68	0, 12	2.65	0.16	0.12	<0.01	0.08
KK-184		0.2	3	86	•	191	24	7	0.9	86	13	3756	2	21	15	52	<5	0.6	7 312	<0.01	1.15	4.79	4.66	0.42	0.15	0.01	0.07
STD-P1		0.2	62	25	52	155	20	ব	0.3	35	7	569	~	112	35	175	<5	0.5	9 86	0.11	1.02	1.11	2.36	0.82	0.36	0.06	0.08
KK-185		1.7	7	59	8	140	40	<5	0.9	37	6	1442	2	82	17	41	<5	0.4	7 23	<0.01	0.51	1, 18	4.15	0.23	0.14	<0.01	0.07
KK-186		0.1	3	30	9	88	<5	<5	≪0.1	\$6	- 4	463	- 4	81	67	8	<5	0.2	3	0, 18	1.23	0.27	4.10	1.05	0.02	0.06	0.06
KK 188		0.2	5	9	12	44	19	<5	<0.1	9	3	167	~ 2	30	7	159	<5	0.3	11 10	0.04	0.75	0.50	4.96	0.45	0.27	0.03	0.21
KK-189		<0.1	- 4	10	8	12	14	<5	0.2	8	3	199	2	88	11	48	7	0.3	13	<0.01	0.25	0.08	1.93	0.07	0.04	0.07	0.03
KK-190		<0.1	3	8	8	35	10	<5	<0.1	8	3	409	2	36	7	100	<5	0.3	10 45	0.01	0.61	1.60	4.50	0.43	0.17	0.04	0.13
KK-191		<0.1	3	6	8	25	29	<5	<0.1	13	<1	71	5	49	5	70	<5	0.2	4 10	0.10	0.23	0.07	7.33	0.03	0.25	0.03	0.11
KK-191*		<0.1	3	5	8	25	29	<5	<0.1	12	<1	67	6	48	5	69	<5	0.2	4	0.10	0.22	0.06	7.26	0.02	0.25	0.03	0.11

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Project/Venture:	COREY	Geol:	K TROCIUK	Date Received:	JULY 22, 1992	Page	1	of	2
Area:	1P	Lab Project No.:	02447	Date Completed:	AUG 11, 1992	Attn:	_K TRO	CIUK	
Remarks:							S HOF	FMAN	
Au - 10.0 g sample dig	pested with Aqua Regia and o	letermined by Graphite Furnace A.A. (D.L. 1 PPB)					<b>J KOW</b>	ALCHUK	
ICP - 0.5 g sample dig	ested with 4 ml Aqua Regia a	t 100 Deg. C for 2 hours.					E KIMU	IRA	
N.B. The major oxide el	lements, Ba, Ba, Cr, La and V	/ are minely dissolved completely with this acid dis	solution method						

SAMPLE	T	Ag	Mo	Cu Pt	Zr	As	Sb	Çq	Ni	Co	Мл	Bì	Cr	<b>V</b>	Ba	W	Be	La .	Sr	ותן	A	Ca	Fe	Mg	ĸ	Na	P
No.		pm	ppm	ppm ppr	n pp	n ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	<b>%</b>	%	%	*	%	%	%
42075		0.5	2	5	4	0 9	<5	<0.1	<1	<1	421	<2	118	I	109	<5	0.2	7	62	<0.01	0.23	1.97	0.29	0.01	0.22	0.01	0.01
42076		0.2	<1	<1	0	9 <5	<5	<0.1	<1	<1	235	<2	105	<b></b> 1	98	8	0.4	13	24	<0.01	0.26	0.86	0.14	<0.01	0.27	<0.01	<0.01
42077		D.2	2	33 6	2 3	4 <5	<5	<0.1	<1	<1	378	<2	103	<1	96	6	0.4	10	32	<0.01	0.23	1.37	0.14	<0.01	0.25	<0.01	<0.01
42078		).2	<1	35 8	4	4 13	<5	0.1	× <1	<1	4 16	⊲	84	2	60	6	0.3	11	41	<0.01	0, 12	1.56	0.14	<0.01	0.15	0.01	<0.01
42079		0.6	2	64 22	5 13	9 27	<5	0.1	13	18	2079	~2	42	56	73	<5	0.2	2	221	<0.01	1.93	8.28	4.82	1.62	0.18	0.01	0.12
1 1		· · ·	_							1		1 1	i l			1				}	្រ	1				1 1	1
42080		hal	3	63	7 10	3 23	<5	<0.1	17	19	1538	2	43	73	74	<5	0.2	2	147	<0.01	2.28	5.39	5.81	1.88	0, 16	0.02	0.13
42089			2	56	7 0	9 254	<5	28	202	15	19582	16	50	22	73	<5	0.2	3	37	<0.01	0.60	0.83	10.63	109	0.26	<0.01	0.12
42000			2	50	2 č	0 30	-5	-0.1		18	13737	14	52	37	43	6	04	Ă	75	<0.01	122	1 75	0.80	4.04	0.25	-0.01	0 14
42090		57	10	20		2 12			43		3657		81	10	88	-5	0.5	7	78	-0.01	0.62	2.55	4 04	0.69	0.20	0.02	0.05
42091			12	20				-0.1			5007				105		0.0	, i	60	0.40	100		0.07		0.20	0.02	0.00
SID-P1	- 1	ມສຸ	62	20 00	2 14	5 20	< 3	0.2	32	1 1	301	ଁ		ಿ	103	<5	0.5	•	<b>.</b>	0.10	1.02	0.94	2.21	u.pa	0.35	0.00	0.00
	1 I.		-		S .													_			0.07		4 00				0.00
42092		0.2	5	23	<b>4</b> 1	4 6	6	<0.1			1073	~	94	- 18	89	<5	0.5	a	123	<0.01	0.67	3.24	1.80	UAZ	0, 19	0.02	0,04
42093		0.6	3	62	3 5	6 9	8	<0.1	14	20	1832	~2	30	41	83	<5	0.3	4	199	<0.01	1./5	5.87	5.22	1.28	0.18	0.02	0.14
42094		D.6	3	72	8 16	4 9	7	<0.1	17	22	1308	<2	31	51	92	<5	0.4	6	171	<0.01	1.82	4.89	5.24	1.38	0. 18	0.02	0.14
42095		).5	3	80	7 15	9 7	6	<0.1	18	21	1351	<2	25	<b>71</b>	87	<5	0.5	7	177	<0.01	2.26	5.61	5.81	1.73	0, 16	0.02	0.14
42096		).4	3	67	7 12	9 8	<5	<0.1	SS 15	20	1516	<2	26	49	82	<5	0.5	6	205	<0.01	1.98	6.49	4.97	1.52	0, 17	0.01	0.14
- j					÷		1							880).									i				
42097		).5	1	53	0 9	3 11	5	<0.1	15	18	1267	<2	26	42	77	<5	0.4	4	164	<0.01	1.93	5.21	5.00	1.45	0,19	0.01	0.14
42100		0.7	2	63	9 1	5 13	9	<0.1	14	17	2443	~2	22	36	51	<5	0.3	4	223	<0.01	1.67	7.29	4.73	1,35	0, 13	0.01	0.13
42101		1.5	2	62	5 16	8 31	<5	0.2	17	19	3345	2	29	35	79	<5	0.4	5	179	<0.01	1.54	5.67	5.38	1.34	0.23	0.01	0.14
42102		),7	1	50	2 4	1 30	6	1.7	21	18	2831	2	35	53	84	<5	0.4	3	196	<0.01	1.88	5.86	4.94	1.54	0. 19	0.02	0, 12
42102*	- 10	D.6	2	52	3 44	5 31	7	1.6	20	17	2823	2	34	52	81	<5	0.4	3	193	<0.01	1.82	5.66	4.76	1.49	0.19	0.02	0.12
					8																1						
42103		).4	5	14	0 6	2 12	<5	<0.1	10	10	1576	2	27	38	62	<5	0.3	5	181	<0.01	1.68	5.91	3.37	1.25	0.17	0.02	0.10
42104	- I I	0.2	3	18	<b>i</b> (	6 6	<5	<0.1	11	12	1279		27	33	97	<5	0.4	7	110	<0.01	1.51	3.79	3.48	0.99	0.23	0.02	0.10
42105		22	3	25	3 7	2 8	<5	<0.1	14	17	1601	2	29	30	63	<5	0.4	8	151	<0.01	1.13	5.11	3.96	0.85	0, 16	0.01	0.12
42106		3	Ă	23	al s	4 16	5	<0.1	27	22	1674		55	53	64	<5	0.4	6	132	<0.01	1.78	4.43	6.35	143	0.24	0.01	0.13
42107			5	16 5		9 55	<5	<0.1	20	30	1492	6	59	24	42	<5	0.3	7	135	<0.01	0.97	4.06	8.41	0.70	0.24	0.01	0.12
12101		~~	v		8			,				-						-								0.0.1	
42100		na İ	7	109	1	7 23	6	0.4	17	16	1334	5	107	52	70	<5	0.4	8	74	<0.01	1.83	2.21	4.92	131	0, 18	0.01	0.12
42110			ŕ	230		3 20	-5	52		12	2525		54	47	87	-5	0.3	â	102	-0.01	191	5.50	5 27	1 06	0.25	0.01	0 15
42110			0	1 10		6 23	~	2.4		12	1592		40	26	82		0.3		174	-0.01	1 30	3.67	3.08	0.01	0.26	0.01	0.11
10110		<u> </u>	0	1 10		7 23		4.1	14	12	501		48	5.	67		0.0	5	00	-0.01	1 32	0.72	4 28	0.02	0.27	-0.01	0.11
42112			0	119				1.1			501		40	21	69	~5	0.2	, i	20	-0.01	1 38	0.72	4.20	0.82	0.27	-0.01	0.11
42112-	- 1	7.8	•		X 20	~ ~	< 3				302	~	~0		00	<0	V. 1	-		~0.01	1.50	0.00	7.73	0.00	0.29	<b>~</b> 0.01	
	[		_			= _ ~					0004				74			_			4 77	4.04	E 000		0.04	0.01	0.00
42113		1.5	5	97	9 6	5 64	<0	2.5	15	17	2061	~~	61	- 44	/1	<0	0.3	6	1/6	<0.01	1.//	4.04	5.09	1.10	0.21	0.01	0.12
42114		L1	6	101	9 9	43	<0	4.0	13	CT C	2181	~~	40		88	<0	0.3	4	108	<0.01	2.00	4.88	4.75	1.20	0.24	0.01	0,14
42115		1.0	5	105	6 59	8 47	7	2.7	15	16	2971	2	22	49	83	<5	0.6	10	220	<0.01	1.86	6.54	4.49	1.10	0.22	0.01	0.13
42116		1.0	4	99	1 80	3 60	11	3.9	16	16	2369	2	38	55	83	<5	0.4	7	165	<0.01	1.98	5.06	4.90	1.25	0.23	0.01	0, 14
42117		1.0	5	190	7 67	2 62	12	2.8	20	23	1992	4	41	66	82	<5	0.5	9	123	<0.01	2.40	3.55	6.25	1.59	0.24	0.01	0, 15
						1																					
42119		).6	3	99	2 42	9 39	<5	1.8	15	21	1421	4	40	32	74	<5	0.4	7	105	<0.01	1.40	3,30	4.80	0.89	0.26	0.01	0.11
42 120		1.4	5	129	8 34	7 86	<5	1.7	15	16	1757	3	48	25	75	<5	0.3	6	125	<0.01	1.38	3.07	5.02	0.92	0.31	0.01	0.13
42133		).6 İ	6	68 12	0 44	4 22	7	1.8	14	16	3320	2	58	38	103	<5	0.3	5	397	<0.01	1.54	10.46	4.58	1.03	0.20	0.01	0.11
42135		3.3	4	86	8 16	9 25	9	0.4	16	18	2379	2	58	43	72	<5	0.5	7	253	<0.01	1.89	8.03	4.52	1.43	0.18	0.01	0,14
42135*		<b>5</b>	Á	80	7 16	7 24	8	0.4	14	16	2340	2	57	41	70	<5	0.4	5	251	<0.01	1.84	8.03	4.32	1.39	0.18	0.01	0,13
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**Geochemical Analysis** 

Project/Venture:	COREY	Geol:	K TROCIUK	Date Received:	JULY 22, 1992	Page	2	of	2
Area:	1P	Lab Project No.:	D2447	Date Completed:	AUG 11, 1992	Attn:	K THOO	JUK	
Remarks:							SHOFF	MAN	
Au — 10.0 g sample di	igested with Aqua Regia and o	letermined by Gaphite Furnace A.A. (D.L. 1 PPB)					JKOWA	ALCHUK	
ICP - 0.5 g sample di	gested with 4 ml Aqua Regia a	at 100 Deg. C for 2 hours.					E KIMU	KA	
N.B. The major oxide (	elements Re. Be. Cr. La and V	V are parely dissolved completely with this acid dis	solution method						

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Ňa P Bi Cr Y 8a W Be لعا Sr Π A G Fe Mg κ Co Mn Sb Cd Ni SAMPLE Мо Cu Pb Zn As Ag % % % % % % 96 % ppm ppm mqq ppm ppm ppm ppm ppm ppm ppm ppm рот ppm ppm ppm DDM ppm DDM DDM No. 0.01 3.12 6.19 6.78 2.47 0.08 0.02 0.13 32 26 1939 2 74 174 43 8 0.4 5 208 70 153 15 <5 <0.1 <1 42139 0.5 1 0.15 204 42 <5 161 0.01 3.42 5.45 7.61 2.67 0.08 0.02 30 29 1970 <2 49 0.3 33 <5 <0.1 2 56 <1 187 42140 0.3 0.16 0.02 0.14 74 71 <5 1.90 7.16 5.46 1.49 2 49 0.4 209 < 0.01 18 19 2 17 2 114 10 <5 <0.1 2441 0.3 42141 1.30 0.22 0.01 0.15 50 <5 114 < 0.01 1.53 3.88 6.24 14 <5 <0.1 22 24 1342 2 50 44 0.4 6 42142 0.4 1 18 2 87 72 <0.01 1.51 6.95 5.75 1.25 0.21 0.01 0.13 22 19 2077 2 62 49 <5 0.4 7 230 16 <5 <0.1 2 10 4 88 42143 1.0 1.56 0.22 0.02 0.16 59 63 <5 0.3 5 112 < 0.01 1.87 3.69 6.03 <5 <0.1 21 26 1309 2 49 96 20 0.8 2 183 2 42144 40 56 <5 141 <0.01 1.59 4.54 6.03 1.39 0.22 0.01 0.17 2 48 0.2 4 <5 <0.1 22 26 1304 98 21 0.6 4 133 î 1 1 42145 1.20 0.21 0.01 0.16 42 55 <5 148 <0.01 1.45 5.27 6.01 19 2 57 0.2 4 2 98 2 72 5 <5 <0.1 23 1371 42146 0.7 38 60 <5 <0.01 1.39 4.90 5.43 1.20 0.21 0.02 0,16 57 0.3 5 141 3 88 79 7 <5 <0.1 20 20 1350 4 11 0.4 42147 1.17 0.21 0,15 37 59 <5 0.3 5 137 < 0.01 1.34 4.79 5.26 0.01 19 20 1337 56 76 <5 <0.1 4 0.4 4 86 13 8 42147\* 0.20 65 <5 153 < 0.01 1.55 5.20 5.53 141 0.01 0.14 2 56 46 0.4 5 7 9 <0.1 20 24 1529 84 42148 0.6 4 161 <1 56 1.73 4.13 6.68 1.52 0.21 0.01 0.16 <5 5 126 < 0.01 <2 63 51 0.3 <5 <0.1 23 24 1370 0.2 3 36 <1 90 11 42149 171 0.18 0.01 0.13 2 53 62 93 <5 0.3 4 242 < 0.01 2.17 8.34 4.95 2 54 <1 327 10 <5 1.0 17 19 1738 0.3 42153 66 96 <5 70 < 0.01 2.61 3.22 5.97 2.11 0.21 <0.01 0.16 22 875 <2 46 0.3 4 10 <5 <0.1 21 3 66 <1 114 42 154 0.4 0.12 0.01 79 88 72 <5 0.3 3 154 < 0.01 2.66 6.06 5.83 2.47 0.14 25 1677 2 3 63 99 17 <5 <0.1 36 42155 0.5 9 53 <5 280 < 0.01 3.52 9.15 6.54 3 29 0.06 0.01 0.10 159 0.5 3 <5 <0.1 56 30 2026 2 119 101 14 42159 0.3 1 40 <1 57 65 <5 145 < 0.01 1.59 5.86 4.87 1.29 0.17 0.01 0.10 0.4 4 <5 19 20 1351 <2 61 9 61 12 68 24 <0.1 42 163 1.1 1.76 0.22 < 0.01 0.14 20 23 2 44 56 75 <5 0.3 31 87 < 0.01 2.11 3.88 5.63 84 23 <5 <0.1 1164 3 65 7 0.9 42164 58 <5 < 0.01 2.14 6.54 5.26 1.76 0.13 0.01 0.12 2 56 89 0.3 3 179 <5 18 19 1677 90 122 11 <0.1 42167 1.0 4 20 33 2.26 0.89 0.36 0.06 0.08 172 <5 76 0.09 1.02 0.96 33 553 2 114 0.4 6 61 27 53 149 19 <5 0.1 5 STD-P1 0.2 212 <0.01 1.74 6.96 4.97 1.23 0.20 0.01 0.13 26 44 89 <5 0.3 4 17 20 1351 2 64 2 87 13 <5 <0.1 42176 0.5 4 <5 <5 51 91 1.67 5.81 4.62 1.23 0.18 0.01 0,12 5 182 <0.01 14 19 1286 ~2 32 0.4 6 51 16 83 17 <5 <0.1 42181 0.4 52 43 1.52 0.23 0.14 2.93 6.93 0.01 21 31 1583 5 43 63 0.4 7 97 0.02 1.95 152 9 <5 <0.1 8 24 5 42 190 0.3 37 61 <5 0.2 5 72 <0.01 2.05 2.15 6,75 1.46 0.26 <0.01 0,15 18 18 1557 5 5 22 142 29 <5 <0.1 0.2 16 42191 51 1.66 5.84 1.72 0.20 < 0.01 0.14 35 94 <5 0.3 6 40 < 0.01 2.15 4 82 11 134 16 <5 <0.1 21 26 866 0.8 BK88R-124 176 <0.01 2.13 5.88 5.33 1.70 0.19 <0.01 0.14 1621 2 53 93 <5 0.3 4 17 25 33 66 96 <5 <0.1 19 BK88R-125 0.5 4 8 8 30 <5 0.3 7 83 <0.01 0.25 2.65 0.68 0.17 0.08 0.03 0.01 151 5 11 8 <5 0.1 5 3 949 2 9 9 BK88R-126 < 0.1 55 <5 0.24 3.43 0.53 0.11 0.13 0.03 <0.01 768 2 130 7 0.3 9 129 <0.01 3 3 5 **t**2 18 5 <5 <0.1 7 BK88R-127 < 0.1 2 72 1,59 0.28 <0.01 0.09 0.03 < 0.01 <5 <0.1 60 < 0.01 0.08 406 <2 176 6 3 < 0.1 5 6 21 9 <5 <5 0.1 1 BK88R-128 <5 0.09 1.60 0.31 <0.01 0.09 0.03 <0.01 2 172 3 73 0.1 7 61 <0.01 24 9 <5 <5 0.2 3 1 410 BK88R-128\* < 0.1 6

Project/Venture;	1P	Geol:	K TROCIUK	Date Received:	JULY 30, 1992	Page	1	of	7
Area:	COREY	Lab Project No.:	D2470	Date Completed:	AUG 18, 1992	Attn:	K TROO	CIUK	
Remarks:							S HOF	FMAN	
Au – 10.0 g sample dig	jested with Aqua Regia and deter	mined by Graphite Furnace A.A. (D.L. 1 PPB)					J KOW	ALCHUK	
ICP - 0.5 g sample dig	ested with 4 ml Aqua Regia at 10	0 Deg. C for 2 hours.					E KIMU	RA	

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ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are sarely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Мо	Cu	Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr 💦	V S	Ba	W	Be	5	ŝ	m	AI	Ca	Fe	Mg	ĸ	Na	Ρ
Na.		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<b>ppm</b>	ppm	ppm	ppm	ppm p	pm .	ppm	ppm	ppm	ррт	ppm	%	%	%	<b>%</b>	<b>%</b>	%	%	<u>%</u>
42194		0.6	<1	- 74	18	645	27	<5	2.5	15	12	2619	<2	19 💮	69	89	<5	0.2	2	185	<0.01	2.40	5.52	5.36	1.68	0.27	0.01	0. 14
42195		0.5	1	68	48	396	41	15	2.1	21	17	2291	<2	32 📖	71	107	8	1.1	20	173	<0.01	2.08	4.81	4.40		0.29	0.01	0.13
42 197		0.7	<1	70	36	758	46	<5	3.3	<b>15</b>	12	2416	~2	18 🔛	56	65	<5	0.2	<1	193	<0.01	2.34	5.22	5.59	1.73	0.27	0.01	0, 13
42200	-	0.5	<1	42	× 101	548	146	<5	1.9	20	20	2548	2	22	69	87	<5	0.2	<1	137	<0.01	2.71	4.78	6.05	<b>1.90</b>	0.28	0.01	0.14
42201		1.4	<1	79	35	445	202	<5	1.6	14	18	2552	< 2	10	31	62	<5	0.2	<1	371	<0.01	1.46	6.00	5.46	1.02	0.30	<0.01	0.13
42202		1.3	1	46	198	577	59	5	1.8	<b>15</b>	16	3360	2	13	66	73	<5	0.2	<1	211	<0.01	2.68	6.64	5.85	1.90	0.26	<0.01	0, 13
42203		1.1	3	76	125	620	82	7	2.4	7	19	2439	<2	14	58	89	<5	0.5	7	142	<0.01	2.37	4.66	5.66	1.59	0.33	0.01	0.15
42204		2.3	1	71	187	484	41	ব	2.1	24	17	3588	2	22	51	68	<5	0.3	1	189	<0.01	2.20	6.04	6.02		0.30	0.01	0, 13
42205		0.8	<1	47	37	552	49	<5	2.2	54	32	3543	2	68 📖	138	39	<5	0.4	2	150	0.01	3.75	4.12	8.06	2.83	0, 19	0.02	0.12
STD-P1		0.2	61	25	50	146	20	<5	0.2	32	3	575	2	112	31	159	<5	0.4	8	85	0.11	1.06	0.93	2.27	0.82	0.35	0.06	0.07
								[			_					Í												
42206		0.6	5	30	7	223	33	10	<b>&lt;</b> 0.1	31	26	4653	4	- 35 📖	106	47	<5	0.5	5	119	0.04	2.27	3.41	6.38		0.26	0.02	0.14
42216		0.1	ã	75		89	15	- 6	0.4	148	39	1173		273	140	32	<5	1.1	17	119	0.28	3.02	3.82	5.21	3.57	0.05	0.04	0.07
42217		<0.1	- Ă	63		59	<5	<5	<0.1	1 16	32	829		204	11	14	<5	0.3	- 4	74	0.24	2.90	1.87	4.72	3.49	0.06	0.04	0.07
42218		<0.1	Å	62		43	-6	6	<0.1	111	29	630	2	208	76	13	<5	0.3	4	82	0.27	2.28	2.90	3.67	2.66	0.05	0.04	0.06
42219		<0.1	4	78		52	<5	- 5	<0.1	117	30	703	2	235	82	13	<5	0.3	3	59	0.31	2.55	2.60	4.12	2.87	0.06	0.04	0.06
											•••				98				-									
42220		<0.1	4	75	× 7	61	<5	<5	<0.1	126	34	721	2	221	83	20	<5	0.5	9	61	0.30	2.37	3.02	4, 10	247	0.07	0.04	0.07
42221	1	<0.1	2	73	<1	56	<5	⊲5	<0.1	136	33	714	2	217	77	- 14 ]	< ১	0.3	4	53	0.34	2.42	3.88	3.98	1977 I	0.06	0.04	0.07
42222		<0.1	3	64		49	<5	ব	<0.1	122	31	678	2	18 1	79	13	<5	0.3	3	84	0.31	2.36	4.84	3.93	246	0.05	0.04	0.06
42223		<0.1	2	74	3 S	58	<5	6	<0.1	111	31	699	2	138	69	19	<5	0.2	4	54	0.26	2.67	1.72	4.39	2.85	0.09	0.04	0.07
42223*		<0.1	4	73		58	<5	6	<0.1	110	30	694	~2	136	69	19	<5	0.2	4	53	0.26	2.64	1.68	4.41	2 83	0.09	0.04	0.07
													_				-											
42224		<0.1	3	48	10	97	11	9	0.3	800 F31	25	621	~2	108	73	40	-5	1.0	26	<b>60</b>	0.18	1.84	2.73	3.79	Sec. 77	0.05	0.05	0, 14
42225		<0.1	2	11	<b>***</b> 2	106	<5	্ৰ	<0.1	21	14	535	2	50	45	28	<5	0.4	23	119	0.16	1.65	1.99	3.55	1 38	0.06	0.04	0.20
42226		<0.1	2	14	<1	104	15	5	<0,1	19	12	548	2	47	47	33	<5	0.3	22	104	0.17	1.62	2.59	3.71	1:35	0.06	0.04	0, 19
42227		< 0.1	3	10	8 <b>4</b> 1	107	9	<5	<0.1	18	12	541	2	51	48	36	<5	0.4	22	113	0.18	1.63	3.25	3.72	134	0.06	0.04	0.20
42228		<0.1	3	63		83	<5	- 5	<0.1	112	31	731	2	187	88	15	<5	0.4	7	66	0.27	2.44	2.57	4.41	2.74	0.03	0.05	0.08
		1																										]
42229	1	<0.1	- 4	82	7	68	<5	8	<0.1	101	32	738	2	148	89	18	<5	0.6	12	60	0.25	2.52	1.96	4.36	2.78	0.05	0.04	0.07
42230		<0.1	1	82	<1	67	<5	< 5	<0.1	114	32	784	<2	167 🞆	91	13	<5	0.3	5	60	0.28	2.76	2.25	4.64	3.06	0.06	0.05	0.07
42231		<0.1	4	80	2	70	<5	9	<0.1	133	33	790	2	185	88	16	<5	0.3	5	63	0.29	2.92	2.51	4.71	3.32	0,06	0.05	0.07
42232		<0.1	4	72	<1	56	<5	6	<0.1	131	31	7 19	2	269 🞆	79	13	<5	0.3	- 4	82	0.26	2.48	6.14	3.96	2.87	0.07	0.04	0.06
42232*		< 0.1	4	75	2	58	7	6	<0.1	125	32	714	2	256	79	14	<5	0.6	8	83	0.22	2.34	5.96	3.93	2.83	0.07	0.04	0.07
	1																											
42233		<0.1	7	102	. 6	68	8	6	0.4	175	40	717	3	439	82	32	<5	1.0	19	59	0.24	2.49	3.25	3.84	2.92	0.11	0.04	0.07
42234		<0.1	4	74	<1	56	<5	- 5	<0.1	150	30	760	2	425	75	19	<5	0.3	3	53	0.22	2.45	5.91	3.91	274	0.10	0.03	0.06
42235		0.1	4	82	2	63	<5	ব	<0.1	157	34	771	2	425	78	21	<5	0.3	3	61	0.28	2.53	5.55	3.96	2 88	0.10	0.04	0.06
42237		<0.1	1	77		56	<5	- 5	<0.1	143	31	740	2	235	74	25	<5	0.3	2	51	0.32	2.33	4.29	3.57		0.13	0.04	0.06
42238	1	0.1	3	68		60	<5	<5	<0.1	156	34	7 18	2	241	76	19	<5	0.3	2	57	0.34	2.36	5.17	3.62	2 57	0.09	0.04	0.06
	1												_ <b>_</b> [															
42246	1	0.1	4	88	18	45	<5	a	0.1	550	32	559	2	276	62	24	<5	0.6	8	2	0.24	2,10	4.34	2.81	231	0.10	0.04	0.05
42248		<0.1	2	=0		49	4	6	<0.1	163	29	580	2	288	60	19	<5	0.2	2	43	0.28	2.33	3,59	3.06	2.02	0.11	0.03	0.05
42249		<01	3	74	2	46	ক	6	<0.1	193	31	597	2	300	61	18	<5	0.2	2	33	0.26	2.43	3.29	3.26	2.70	0.11	0.03	0.05
42250		0.3	3	67		52	4	ای ا	<b>40</b> .1	179	32	659	2	298	67	16	6	0.2	3	2	0.27	2.77	2.72	3.62		0.10	0.04	0.06
42250*		0.4	4	71		54	6	6	<0.1	175	33	651	0	293	70	20	<5	0.4	7		0.27	2.68	2.73	3.52	303	0.10	0.03	0.06
		~ ~		''				~~			~								-									0.00
L					a service de la constante de la constante de la constante de la constante de la constante de la constante de la			·					· · · · ·							e oorayóa							I	

Project/Venture: Area:	1P COREY	Geol: Lab Project No.:	K TROCIUK D2470	Date Received: Date Completed:	JULY 30, 1992 AUG 18, 1992	Page Attn:	2 of K TROCIUK	7
Remarks:							SHOFFMAN	
Au - 10.0 g ample digested	I with Aqua Regia and determined by Graphite Furm	ICO A.A. (D.L. 1 PPB)					J KOWALCHUK	
ICP - 0.5 g sample digested	with 4 mi Aqua Regia at 100 Deg. C for 2 hours.						E KIMUKA	

N.B. The major oxide elements, Ba, Be, Cr, La and W are marely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	N	Co	Mn	81	Cr	<b>V</b>	Ba	w	80		<b>\$</b>		~	Cal	ne	. PM	- <u>N</u>	Na	۳ ~
Na		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	mqq	ppm	ppm	ppm	ppm	ppm	ppm	ppm p	ppm	*	-*		<u>%</u>		- 200	- 204	70
42251		<0.1	1	90	11	69	7	<5	0.6	102	37	715	3	159	88	29	<5	1.2	23	50	0.22	2.28	2.65	3.97		0.06	0.04	0.0/
42252		<0.1	<1	65	2	- 44	ব	<5	<0.1	160	28]	558	~2	299	66	29	<5	0.2	3	20	0.22	2.25	2.8/	3.15	2.04	0.21	0.04	0.05
42253		0.1	1	73	2	42	<5	<5	<0.1	159	28	576	2	290	61	31	<5	0.2	2	20	0.19	2.23	4.44	3.16	2.45	0.24	0.04	0.05
42254		<0.1	<1	78	2	41	<5	<5	<0.1	164	27	531	<2	270	52	36	<5	0.2	2	22	0.19	2.25	2.53	3.07	2.5/	0.23	0.04	0.05
42255		<0.1	<1	88	7	42	<5	- 6	<0.1	186	- 30	538	~2	279	52	31	<5	0.3	4	21	0, 19	2.20	2.50	3.08	2.49	0.19	0.03	0.05
42256		<0.1	<1	76		44	<5	<5	<0.1	166	29	503	2	272	48	27	<5	0.3	3 🛞	25	0, 16	2.05	2.80	2.81	2.35	0.15	0.03	0.05
42257		0.1	<1	78		39	<5	<5	<0.1	154	27	427	~2	228	36	24	<5	0.2	2	20	0.15	1.76	2.76	2.63		0.10	0.02	0.04
42258		0.1	<1	69		38	<5	<5	<0.1	149	25	485	2	260	4	16	<5	0.2	2	24	0.13	1.93	3.03	2.72	2.15	0.09	0.03	0.04
42259		<0.1	<1	73		44	<5	<5	<0.1	155	28	564	2	287	59	6	<5	0.2	2	42	0.17	2.07	4.45	3.04	2.40	0.04	0.03	0.04
42250+		<0.1	1	74		44	45	6	<0.1	157	29	561	2	285	60	7	<5	0.4	4	42	0.17	2.06	4.31	3.01	2.39	0.05	0.03	0.04
422.00		~~					~	-					_										I				1	
10000		0.1	-1	84	,	46	-65	<5	<0.1	194	33	556	~	302	\$7	8	6	0.2	4	15	0.16	2.57	1.37	3.33	2.62	0.05	0.04	0.03
10001						43		Ā	<0.1	168	28	500	a	247	38	5	<5	0.1	2	17	0.16	2.34	1.97	3.00	2.50	0.04	0.03	0.03
40060		-01				46		ایم ا	<01	182	33	591	ā	260	42	3	<5	0.2	2	19	0.18	2.56	2.55	3.37	2.84	0.04	0.03	0.03
42202		0.1				50			-0.1	201	35	606	0	328	52	15	<5	0.4	6	18	0.17	2.69	1.80	3.45	2.80	0.11	0.04	0.04
42203		0,1	3	60					<0.1	184	30	558	3	282		14	<5	0.2	2	18	0.19	2.53	2.58	3.25	2.53	0.17	0.04	0.03
42264		0.2	<1	16	1000 <b>6</b>		<0	~3	×0. I		33	~~	, v	2					- 100									
		- 0.4				50	-		-0.1		34	- 608	0	317	52	+2	<5	0.2	2	7	0.23	2.80	1.92	3.63	2.88	0.12	0.04	0.04
42260		<0.1				30			-0.1	103	30	581		200	20 M	14	<5	0.1		17	0.22	2.59	1.36	3.40	2 60	0.13	0.03	0.04
42266		<0.1		<b>00</b>		40	3	<u> </u>	-0.1		30	515	5	202		10	~~	0.1		10	0.20	2.45	1.36	3.18	2.37	0.17	0.04	0.03
42267		<0.1	<1	88		42	<5		<0,1		30	310		202	72	10		0.1		20	0.22	2.88	2.65	4.21	100	0.11	0.03	0.04
42268		<0.1	1	86		56	<5		<0.1		30	570		110		196	~	0.5		89	0 11	1 11	0.80	2.33	0.85	0.37	0.07	0.08
STD-P1		0.2	64	20	<b>D</b> 1	139	20	<b>S</b>	0.2	3/	•	3/0	<b>~</b>	1.9		100	<b>∼</b>	0.5	<b>`</b> ]		<b>v</b>			2.00		0.01	0.01	
														444		16	-	0.4	7	90	0.21	2 16	2 94	4.00	2 31	0 10	0.03	0.06
42269		<0.1	Z	"		50	<0		<0.1			600		199	20			0.7			0.25	101	2.87	3 42	1 92	0.06	0.03	0.06
42270		<0.1	2	64		56	8		<0.1		20	000		100	00		~	1.0	4		0.10	2.08	2.50	1 70	2.08	0.00	0.03	0.06
42271		<0.1	4	85		60	75	11	0.3		30	607		141	DK S	20	-	1.0		5	0.10	104	2 14	3.55		0.12	0.02	0.05
42272		<0.1	2	55		48	<	୍	<0.1		21	028	4	143		13		0.2			0.20	0.00	3.57	A 14		0.10	0.02	0.05
42273		<0.1	2	64		30	<0	(	<0.1		29	/32	~	10/		20		0.2	' 🞆		0.20	2.20	0.07	4. 14		0.20	v	0.00
											-			170		-		0.0	1 🕅		0.22	2 58	4 77	4 73	285	0.06	0.03	0.05
42274		<0.1	3	69	<b>1</b>	59	<5	0	<0.1	00	30	848		1/8		3	<0 - 5	0.2	` <u>'</u>	67	0.22	2.00	5.00	4.50	2 6 9	0.00	0.00	0.00
42275		<0.1	2	60	<b>*1</b>	62	<5	୍ଷ	<0.1	56	29	869	2	1/4	TUG		<0	0.5		21	0.23	2.01	0.80	4.09		0.04	0.03	0.00
42276		<0.1	<1	61	<1	51	<5	<5	<0.1	51	27	784	2	157	86	7	69	0.2	<1		0.23	2.10	4.08	4.04	2.18	0.12	0.03	0.00
42277		<0.1	<1	68	<1	58	<5	<5	<0.1	56	30	793	2	167	78	13	<0	0.2	2 × 10	4	0.22	2.00	2.04	4.00		0.23	0.02	0.00
42277*		<0.1	<1	66	<1	59	<5	<5	<0.1	57	30	790	<2	167	11	13	<3	0.2	2	<b>~</b>	0.21	2.00	2.81	4.04	211	0.23	0.02	0,00
1		1	Ì										]															
42278		<0.1	3	82	8	62	19	20	0.5	68	36	709	4	138	84	38	<5	1.2	24	38	0.17	2,16	2.76	3.60	2.12	0.20	0.02	0.06
42279		<0.1	4	71	2	49	<5	8	<0.1	60	28	595	2	133	65	22	<5	0.3	4	21	0.18	2.05	1.82	3.66	1.98	0,23	0.02	0.06
42280		<0.1	2	68	2	49	- 5	6	<0.1	61	26	575	2	120	54	28	<5	0.2	3 🛞	17	0. 18	2.00	1.80	3.58	1.95	0.26	0.02	0.05
42281		<0.1	3	69		54	<5	<5	<0.1	65	28	714	2	135	57	46	<5	0.2	3	16	0.21	2.34	1.82	4.07	2.28	0.37	0.03	0.05
42282	÷	<0.1	3	70		60	6	9	<0.1	66	32	734	2	137	74	37	<5	0.5	9	21	0.25	2.36	2.03	4.04	2.25	0.27	0.03	0.05
			ľ				1																					
42283		<0.1	4	72	2	65	6	1 11	<0.1	68	34	841	2	161	89	33	<5	0.2	2	15	0.23	2.78	2.38	4.76	2.66	0.33	0.03	0.05
42284		201	3	65		60	ക	6	<0.1	73	29	781	2	146	73	54	<5	0.2	2	15	0.22	2.50	2.06	4.33	2.38	0.48	0.03	0.05
42285		201		1 20	3	56	6	6	<0.1	81	31	666	2	148	56	43	<5	0.2	2	14	0.25	2.35	1.14	4.09	2.33	0.36	0.03	0.05
4/298				77		65	6	a	40.1	64	27	583	2	117	59	47	<5	0.3	4	14	0.22	2.14	0.89	3.75	2.11	0.37	0,03	0.05
46200				1 77		55			-01	64	28	582	0	116	58	47	<5	0.2	2	13	0.22	2,18	0.82	3.79	2.14	0.38	0.03	0.05
42200 *		<0.1	<sup>2</sup>	1 "			1 - 2	<b>1</b>					-	1														
		I		1	10000000000	<u> </u>		L	<u> </u>	100000 CC 000			L															

Project/Venture:	1P	Geol:	K TROCIUK	Date Received:	JULY 30, 1992	Page	3	of	7
Area:	COREY	Lab Project No.:	D2470	Date Completed:	AUG 18, 1992	Attn:	K TROC	IUK	
Remarks:							S HOFF	MAN	
Au - 10.0 g sample digested	I with Aqua Regia and determined by Graphite Furne	ace A.A. (D.L. 1 PPB)					J KOWA	TCHICK	
ICP - 0.5 g sample digested	with 4 ml Aqua Regia at 100 Deg. C for 2 hours.						E KIMUF	<b>A</b>	
			- 1						

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N.B. The major oxide elements, Ba, Be, Cr, La and Ware sarely dissolved completely with this acid dissolution method.

SAMPLE		B Mo	Cu	Pb	Zn	As	Sb	Cq	N	Co	Mn	BI	Cr	V	Ba	w	Be	عا	Sr	Π	A	Oa	Fe	Mg	ĸ	Na	P
No.	PF	m ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	<u>%</u>	_%_	<u>%</u>	%	%	%	%	%
42287	<	0.1 <b>  &lt;</b> 1	68		58	<5	<5	<0.1	63	26	633	<2	108	62	35	<5	0.2	1	21	0.20	2.32	1.65	4.11	2.56	0, 19	0.03	0.05
42268	0.	1   <1	63	2	66	4	<5	<0.1	67	26	701	~2	123	60	21	<5	0.2	<1	21	0.18	2.64	1.64	4.35	2.96	0. 14	0.03	0.05
42289	<	\. <b>1</b>   '	1 60		50	<5	<5	<0.1	57	23	574	<2	110	51	22	<5	0.2	1		0.16	2.14	1.35	3.59	2.34	0. 14	0.03	0.05
42290	<	). <b>1</b>   ·	1 62	3	52	<5	- 5	<0.1	56	24	574	~2	111	53	25	<5	0.2	<1	20	0.18	2.13	2.14	3.58	2.27	0.17	0.03	0.05
42291	<	.1 <1	1 73	2	57	<5	<5	<0.1	63	26	664	2	114	61	18	<5	0.2	<1	26	0.17	2.35	2.70	4.01	2.58	0. 13	0.03	0.05
1										1																- 1	
42292	0.	5   3	73		96	7	<5	<0.1	17	20	1516	2	19	60	79	<5	0.2	1	178	<0.01	2.28	7.00	5.51	1.83	0.16	0.01	0.14
42293	0.	1 <1	68	2	120	-5	<5	<0.1	18	17	1560	2	24	71	63	<5	0.2	1	180	<0.01	2.49	7.12	5.65	2.04	0, 13	0.01	0.13
42294	0.	1 1	69		100	<5	<5	<0.1	15	18	1238	2	20	61	72	<5	0.2	<1	192	<0.01	2.19	7.09	5.18	1.84	0.14	0.01	0.13
42295	<	1	72	1	44	<5	<5	<0.1	169	29	524	2	230	\$7	16	<5	0.2	<1	27	0.16	2.27	3.15	3.17	2.80	0.09	0.02	0.05
42295*	<		74	2	45	4	<5	<0.1	170	30	525		232	47	16	<5	0.2	<1	27	0.16	2.28	3.14	3.18	2.80	0.09	0.02	0.05
42296	<	1 <1	66	2	47	⊲5	ব	<0.1	154	28	565	2	249	47	23	<5	0.2	4	16	0,14	2.34	1.49	3.24	2.67	0.12	0.02	0.05
42298	0		79	5	61	11	9	0.3	167	35	611	5	291	65	25	6	0.9	18	37	0.17	2.33	2.78	3.25	2.69	0.08	0.03	0.05
42299	<		61		53	<5	6	<0.1	165	31	687	2	324	71	5	<5	0.3	4	37	0.18	2.47	3.80	3.68	2.95	0.02	0.03	0.05
42300	<	1 <1	67	2	44	<5	-65	<0.1	180	30	567		307	62	5	<5	0.2	3	32	0.18	2.22	3.33	3.25	2.50	0.02	0.03	0.05
42301	10		71		39	6	<5	<0.1	161	27	485		249	46	14	<5	0.2	2	25	0.15	1.96	2.49	2.81	2.25	0.08	0.03	0.04
12001		.   .	1			-	~					_						-									
42304		<b>u</b> l 3	1 72	iller.	46	<5		40.1	184	29	587	2	283	54	20	<5	0.2	2	32	0.17	2.25	3.85	3.15	2.58	0.11	0.03	0.05
42305			62	~1	40	<5	6	<0.1	140	26	538	2	247	52	17	<5	0.4	5	39	0.16	1.86	6.01	2.61	2.076	0.08	0.03	0.04
42308					37	-5	- 5	01		26	528	0	249	51	15	<5	0.2	1	49	0.15	1.80	6.95	2.64	200	0.09	0.03	0.05
42307			48		32		-5	-01	106	21	443	2	206	4	15	-5	0.2	1	87	0 18	175	3 77	2 29	1.92	0.07	0.02	0.03
42307					30			-01	120	23	456		212		11	-5	0.2	1	38	0.18	179	3.81	2.34		0.07	0.02	0.03
72307		···   `'	'I ~~		~	, J	~	<b>~v</b> . <b>,</b>				~				~		•		0.10			2.04				0.00
42308	1.0	• •			40		12	-01	205	34	613	0	301	58	15	<5	0.3	4	34	0.19	2.30	3.83	3.36	2 8 1	0.10	0.03	0.05
42300					47	25	10	0.5	454	34	578	2	250	83	20	10	10	16	30	0.15	1.82	6.00	2 70	• •	0.04	0.02	0.05
42309			78		35	11		0.5		20	403		270		5		0.2	3		0.17	170	4 78	2 73		0.03	0.02	0.05
42311					40			-01	105	33	876		329	50	š	-5	0.2	3	37	0 19	2.60	4 14	3.54	2.01	0.03	0.03	0.04
423 12			82			7	~	0.2	107	33	680		310	5.8	7	-5	0.2	2	20	0.19	2 70	3.86	3 66		0.05	0.03	0.04
100 14		· '	'  <b>'</b> ~		<b>~</b>	<b>'</b>	~	V.2		~		-			· '	~		-		· · · ·			0.00				0.04
42313			20		40		-	-01	100	33	662	0	321	82	7	-5	0.2	2	35	0 18	3.01	2 82	3.83		0.06	0.03	0.04
42314					40	Ē	7	0.2	205	35	618		308		10	-5	0.4	7	9.9	0.10	2.87	2 22	3 59		0.04	0.03	0.04
42314					51	~		-0.1	-	35	671		314		5		0.7	2	37	0.20	2.00	2.37	3.88		0.03	0.00	0.04
123 13			70		5	3			200	30	660		373				0.2	4 9		0.20	3 11	2.07	3.00	3 00	0.00	200	0.04
423 10					140			0.0			570		114		170		0.2	6	82	0.11	1.00	0.00	2 20		0.00	0.02	0.04
	10	- 04	" <b>"</b>			21	~	0.0		°	378	~				~	0.4			0.11	1.00	0.00	2.20		0.04	0.00	0.00
109.17						-		-		20			200			_	0.5			0.17	0.00	2.00	3 77		0.07	امم	0.04
4231/	0.	5 5	<u>۲</u>		32	<0	2	<0.1	eu/	30	671		280	22	- 12	<0 5	0.0			0.1/	2.03	2.00	3.11		0.07	0.03	0.04
423 16	<		80		39	<0	2	<0.1	101	30	500		243	2/		<0	0.3	2		0.10	2.34	3.03	3.01	6.CH	0.04	0.02	0.03
423 19	<		<b>94</b>		49	11		0.4	10.3	35	000	~	202		19	6	0.9	16	00	0.16	2.4/	2.20	3, 13	2.00	0.04	0.03	0.04
42320	0.	!! !			01	0	~	<0.1	200	40	804	2	401	840	2		0.4	3		0.28	3.50	3,40	4.01		0.03	0.05	0.04
42321	0.	ין י	83	<b>1</b>	43	<5	5	<0.1	1/2	30	202	~	291	, en	Ð	-	0.2	2	P1	0.21	2.62	3.22	3.43	a.up	0.04	0.03	0.03
1						-																<u></u>					0.00
42323	<		1 74		43	0	9	<0.1	1/2	30	01/	~2	200			0	0.2	1		0.20	2.41	3./5	3.30	2.81	0.04	0.04	0.03
42324	<	u <1	85		48	<9	0	<0.1	100	32	000	~~~	313		3	<0	0.3	2		0.22	2.91	3.09	3.79	0.00	0.03	0.03	0.04
42326	0.		89		48	-	<	<0.1	193	33	010	2	331	01		0	0.4	4		0.23	2.09	2.03	3.56	3.10	0.04	0.03	0.03
42327	<		85		43	49	4	<0.1	1/5	29	203	~~~	260	<b></b>	5	S	0.2	1		0,18	2.00	2.36	3.37		0.04	0.03	0.03
42327*	<	ul 3	1 84 J	<b>1</b>	43	4	- 40	<0.1	175	30	560	< <	291	ā1	5	<5	0.2	2	22	0, 18	2.62	2.43	3.41	2.86	0.04	0.03	0.03
					l																						

Project/Venture:	1P	Geol:	K TROCIUK	Date Received:	JULY 30, 1992	Page	4	of	7
Area:	COREY	Lab Project No.:	D2470	Date Completed:	AUG 18, 1992	Attn:	K TROC	HUK	
Remarks:							S HOFE	FMAN	
Au - 10.0 g sample	digested with Aqua Regia and determi	ned by Graphite Furnace A.A. (D.L. 1 PPB)					J KOW	ALCHUK	
ICP - 0.5 g sample	digested with 4 ml Aqua Regia at 100 [	Deg. C for 2 hours.					EKIMU	RA	
N.B. The major oxide	elements, Ba, Ba, Cr, La and Ware m	rely dissolved completely with this acid dis	solution method						

Π A **Ca** Fe 1.6 SAMPLE Мо Cu Pb Zn As Sb Ćď N Co Mn BI Ĉr Ba W 80 La Sr ĸ Na Ag % % % % 96 % % % ppm ppm ppm ppm ppm ppm ppm ppm ppm ppm ppm DOM ppm DDM DDM DOM No. ppm ppm ppm <5 31 591 à 265 55 10 ģ 0.6 9 4 0.23 2.87 4.08 3.53 3.25 0.04 0.03 0.03 42328 \$ **Ø**.1 0.1 <1 86 51 172 ර 2 156 85 6 <5 2 31 0.32 2.48 5.20 4.44 2.61 0.04 0.03 0.06 42330 0.1 <1 76 59 <5 <0.1 60 27 805 0.2 71 2 175 93 3 <5 0.2 2 24 0.28 2.96 2.39 4.89 3.44 0.04 0.02 0.06 12332 54 <5 ත <0.1 62 31 847 < 0.1 <1 8 16 <5 14 0.03 54 32 850 2 160 80 8.0 0.26 2.49 5.18 4.24 274 0.03 0.06 42333 0. t 2 74 ź 63 7 . <0.1 4. 7 <⊅ ⊲5 <0.1 175 32 537 2 224 55 5 <5 0.2 <1 55 0.19 2.36 5.80 3.25 2.94 0.04 0.04 0.03 42334 <0.1 <1 59 41 582 263 9 <5 <1 41 0.18 2.97 5.21 3.63 6 E.Y 0.09 0.02 0.03 70 <5 <0.1 179 33 2 66 0.2 42335 < 0.1 <1 79 6 26 49 5 <5 17 0.21 0.05 42336 <1 69 5 42 45 <5 <0.1 162 506 2 270 0.1 <1 2.61 1.84 3.44 3 17 0.02 0.03 < 0.1 ර 56 28 1073 2 185 134 4 <5 0.3 2 30 0.16 3.20 7.58 5.24 3.84 0.02 0.02 0.05 2 64 <5 <0.1 42338 < 0.1 <1 64 <5 25 **c**5 143 3 3 0.21 3.97 4.26 0.03 0.02 42339 < 0.1 <1 63 3 70 <5 <0.1 61 28 1069 2 215 0.3 3.49 5.82 0.06 2 71 ් 6 <0.1 59 28 1068 2 211 142 <5 0.2 1 24 0.21 3.48 3.91 5.81 4.21 0.02 0.02 0.06 42339\* <0.1 3 65 2 ත් 7 49 0.22 2.39 4.76 2.57 0.04 0.03 0.05 42342 <0.1 2 64 58 <5 11 <0.1 57 27 873 2 166 107 11 0.5 3.97 2 2 72 ත් 58 31 932 <2 196 110 9 <⊅ 0.3 4 31 0.32 2.71 3.12 4.62 2.74 0.06 0.03 0.07 42343 <0.1 70 3 4 <0.1 14 <5 769 4 40 0.25 2.29 67 55 4 ත් <0.1 63 27 2 153 86 0.3 4.44 3.85 2.36 0,10 0.03 0.05 42344 < 0.1 82 21 **6** 15 43 0.23 42345 <0.1 2 84 55 12 10 0.2 63 32 646 3 136 0.8 1.98 3.04 3.41 2.5 0.07 0.03 0.06 26 673 2 136 82 9 <5 0.3 4 43 0.18 2.26 3.35 3.74 2.53 0.06 0.03 0.05 52 <5 61 42346 < 0.1 1 53 3 <5 <0.1 đ <0.1 27 743 2 147 12 <⊅ 0.3 4 44 0.22 2.30 3.06 3.89 2.4 0.06 0.02 0.06 42347 <0.1 2 63 55 Ō 61 86 1 2 81 73 4 <5 <0.1 73 34 1059 2 207 143 8 <5 0.4 4 51 0.27 3.08 3.54 5.33 3.52 0.03 0.03 0.07 42348 <0.1 3 8 <5 3 124 0.20 3 40 13 <5 <0.1 43 20 874 2 123 104 0.4 1.79 10.80 3, 19 1.95 0.05 0.03 0.04 42349 44 2 < 0.1 **ර** 128 9 7 63 0.28 2.84 0.03 42350 <0.1 3 73 4 66 ⊲5 <5 <0.1 64 30 953 2 163 0.5 2.64 4.43 4.61 0.03 0.06 2 ⊲5 <5 <0.1 64 30 958 2 164 126 6 <5 0.4 3 62 0.27 2.67 4.42 4.67 2.89 0.02 0.03 0.06 42350\* 3 68 64 < 0.1 36 988 7 <5 6 38 0.31 3.23 2.83 0.05 0.03 0.07 42351 < 0.1 3 84 <1 84 <⊅ <5 <0.1 83 2 213 139 0.4 5.41 113 8 <5 4 31 0.32 2.84 0.07 5 141 67 ත් ⊲5 <0, 1 75 34 836 <2 192 0.3 2.65 2.32 4.72 0.04 0.06 42352 0.5 5 5 74 32 812 204 123 5 <5 0.3 4 35 0.35 2.56 1.62 4.71 2.66 0.03 0.04 0.06 <1 71 <5 <5 <0.1 42353 0.1 71 3 π 89 <5 0.5 9 148 0.03 2.35 42354 0.6 4 101 101 17 <5 <0.1 28 32 1421 3 42 4.84 5.79 1.70 0.18 0.02 0.15 22 22 1367 28 78 90 <5 0.3 4 149 0.01 2.54 4.80 6.06 0.17 0.02 0.15 42355 5 71 3 106 <5 <5 <0,1 3 0.2 24 14 10 23 111 184 <0.01 2.27 5.54 5.73 1.65 0.23 0.01 0,16 42356 0.2 3 71 8 103 7 7 <0.1 22 50 <5 0.3 4 96 5 84 133 6 ත් <0.1 22 22 1424 8 26 81 <5 0.3 4 180 <0.01 2.72 5.48 6.11 0.20 0.01 0.16 42357 7 0.3 107 <5 21 23 1702 28 80 0.4 5 210 0.01 2.69 6.95 5.58 0.17 0.01 0.15 69 113 13 <0.1 5 42358 1.5 1 28 6 <5 5 68 57 109 11 4 <0.1 21 22 1480 2 29 89 81 0.3 4 193 <0.01 2.64 6.10 5.92 1.95 0,15 0.02 0,16 42359 2.2 86 77 <5 103 20 21 1475 2 28 0.3 3 187 <0.01 2.59 5.91 5.70 1 10 0.14 0.02 0.15 42359\* 2.2 4 65 55 11 <5 <0.1 74 7 10 <0.1 22 24 1680 25 81 73 <5 0.4 7 148 <0.01 2.52 5.88 6.05 1.87 0.13 0.01 0.15 42360 0.6 4 103 4 83 79 <5 4 00 2 03 0.17 5 89 11 ٥ <0.1 25 27 1315 8 30 0.2 <0.01 2.64 3.70 6.51 0.01 0.16 42361 0.7 8 105 5 71 5 20 1467 23 81 85 <⊅ 0.3 5 1 19 <0.01 2.14 4.95 5.55 1.80 0.20 0.01 0.17 42362 0.4 7 86 14 <0.1 23 4 25 32 58 93 <5 0.8 13 42363 0.3 5 71 14 88 24 18 <0.1 25 1714 5 164 <0.01 1.95 6.17 4.64 8 K Y 1 0.19 0.01 0.12 2 25 28 ⊲5 <0.1 6 1074 2 41 14 76 <5 0.3 8 123 <0.01 0.57 3.96 1.19 0.34 0.19 0.01 0.03 11 9 6 42365 < 0.1 83 <⊅ 12 <0.01 0.28 2.30 0.09 0.21 0.01 42366 0.1 2 14 19 7 <5 <0.1 3 2 726 2 46 3 0.3 60 0.31 <0.01 7 55 <5 3 5 50 76 <5 <0.1 21 22 1085 2 32 32 0.2 BR <0.01 1.37 3.17 5.58 1.15 0.24 <0.01 0.13 42369 1.3 14 264 50 70 <5 42370 7 62 7 89 80 5 <0.1 22 22 1299 2 27 0.3 6 26 <0.01 1.88 3.72 5.46 1.60 0.20 0.01 0.14 0.6 63 <5 5 99 13 8 <0.1 23 21 1488 27 110 0.3 154 <0.01 2.80 5.19 7.05 2.04 0.13 0.01 0.15 42372 66 2 3 4 0.4 37 184 <5 0.5 27 152 20 <5 <0.1 559 2 115 37 9 87 0,12 1.13 1.00 2.46 0.84 0.37 0.06 0.06 STD-P1 0.3 65 50 6

	Project/Venture: Area: Bemarka:	1P COREN	r					Geol: Lab Pro	oject No.:	K TROC 02470	XUK		Date Re Date Ce	sceived: pmplete	d:	JULY 3 AUG 16	0, 1992 1, 1992		Page Atin:	5 K TROC 8 HOF	of XUK MAN	7
	Au - 10.0 g sample d ICP - 0.5 g sample d N.B. The major oxide	igested with Aq igested with 4 r elements, Ba, f	un Regin ni Aqua F 3e, Cr, La	and dete legia at 1 and W a	ermined by G 100 Deg. C fo ure murely diss	ina.phite ir 2 hour iolved o	Furna.c rs. complet	e A.A. (	(O.L. 1 PPB) h this acid diss	olution r	nethod									j kow. E kimu	ALCHUN RA	C
1	Ag Mo Cu	Pb Zn	As	Sb	Cd NI	Co	Mn	Bi	Cr V	Ba	W	Be		Sr	Π	A	Ca	Fe	Mg	K	Na	P
	mag mag mag	ppm ppm	ppm	ppm (	ppm ppm	рргп	ppm	ppm	ppm ppm	ppm	ppm	ppm	ppm	ppm	%	%	<b>%</b>	<b>1 %</b>		<b>%</b>	%	%

SAMPLE	Ag	Mo	Cu Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	Y	Ba	w	Be		Sr	П	AI	Ca	Fe	Mg	K	Na	P
No.	ppm	ppm	ppm ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррт	ppm	ppm	ppm	ppm	ppm	ppm	%	%	%	%	*	%	%	%
42373	0.5	2	56 7	64	26	୍ <u>ସ</u>	<0.1	16	15	2133	~2	29	73	58	<5	0.2	3	358	<0.01	1,69	11.45	4.73	1.33	0.10	0.02	0.10
42374	0.7	4	85 3	92	9	<5	<0.1	25	27	1140	~2	- 34	122	60	<5	0.7	11	139	<0.01	2.73	5.34	8.51	2.34	0.13	0.02	0.15
42375	0.7	1	72 6	106	5	<5	<0. 1	18	20	1321	2	26	98	56	< ব	0.4	5	169	<0.01	2.24	6.33	5.61	1.79	0.13	0.02	0.13
42376	0.4	1	62 1	112	<5	<5	<0.1	16	21	1175	~	23	121	47	<5	0.2	2	136	<0.01	2.53	5.31	6.28	2.04	0, 10	0.02	0.13
42377	0.9	1	88 4	103	<5	<5	<0.1	19	18	t226	2	24	104	54	<5	0.2	2	128	<0.01	2.49	5.40	6, 18	1.97	0, 12	0.02	0.12
																									- 1	
42378	0.7	2	73 3	88	<5	<5	<0.1	18	23	1619	2	26	91	58	<5	0.2	1	192	<0.01	2.08	7.88	5.82	1.63	0.12	0.02	0.12
42370	0.6	1 2	65 7	103	9	<5	<0.1	19	20	1447	2	21	67	67	<5	0.4	6	163	<0.01	1.88	6.10	5.58	1.44	0.14	0.01	0.12
42380	0.9	1 4	55 2	102		<5	<0.1	15	18	1603	2	10	49	61	<5	0.3	2	181	<0.01	1.68	6.42	5.78	1.48	0.16	0.01	0.14
42381	0.6	1	55	95	18	-65	<0.1	16	19	3680	4	10	54	61	<5	0.3	2	133	<0.01	1.77	4.91	6.44	1.63	0.15	0.01	0.15
ETD_P1	0.3		26 49	146	19	6	<0.1	32	4	558	2	109	35	172	<5	0.4	7	77	0.11	1.00	0.90	2.31	0.81	0.35	0.06	0.08
SID-FI	0.0	<b>–</b>																			1					
10206	1 1 3	,		150	6	-5	<0.1	23	23	3278	2	14	61	71	<5	0.7	10	168	<0.01	2.02	6.43	7.44	2.11	0, 19	0.01	0.15
42300	20	5	85 21	498		6	0.7	22	17	11138	2	13	29	36	<5	0.3	2	100	<0.01	1.38	3.87	9,47	1.24	0, 19	<0.01	0.14
42307	0.6	3	87 21	140	11		<0.1	23	24	2041	2	17	60	75	<5	0.9	15	207	<0.01	2.14	8.77	5.92	1.72	0.18	0.01	0.14
42390	0.5		53	104	- 5	5	<0.1	17	18	1959	2	13	71	56	<5	0.4	4	232	<0.01	2.42	9.26	6.09	1.94	0.12	0.01	0.13
42308	0.5		254	131	- 65	- 6	<0.1	108	26	1077		210	151	135	<5	0.5	9	118	0.04	3.09	3.84	5.90	3.24	0.05	0.02	0.11
42380	0.0	`'			~	~					_															
42300	1 10	6 21	318 21	192	- 5	୍ୟ	<0.1	36	22	996	2	35	140	40	<5	0.2	7	22	<0.01	4.03	0.50	7.94	3 75	0.07	0.01	0.18
42403	0.6	1 21	4671 762	414	<5	-5	<0.1	51	19	1132	224	48	105	51	<5	0.2	- 4	70	0.01	27.72	1.77	5.83	2.37	0.09	0.03	0.20
42400	0.5		283 21	138	- 6	୍ୟ	<0.1	31	22	1450	2	31	128	49	<5	0.2	5	121	<0.01	3.44	3.06	7.06	2.80	0.08	0.02	0.16
42404	0.5		A 18	176	- 65	-5	<0.1	34	23	1441	2	37	135	49	<5	0.3	6	78	<0.01	3.40	1.80	6.88	3.06	0.07	0.02	0.17
42405	0.0		A11	168		- 5	<0.1	31	22	1434		33	130	43	<5	0.2	4	73	<0.01	3.36	1.76	6.71	3.01	0.06	0.02	0.16
42400-		`'			~						-															
42408	1 07	1 7	200 6	50	7	ব	<0.1	5	14	278	2	26	25	42	<5	0.2	5	9	<0.01	0.89	0.29	4.54	0.63	0.22	<0.01	0.13
42407		1 .	108 3	51	12	-6	<0.1	13	14	4 16	3	17	13	39	<5	0.2	4	22	<0.01	0.73	0.75	4.79	0.47	0.28	<0.01	0.12
42407	1.0	5	A11 0	53	17	-5	<0.1	1	13	948	0	21	16	45	<5	0.2	3	96	<0.01	0.83	2.67	4.24	0.63	0.27	<0.01	0.11
42400	1.0		1090 15	86	37	12	<0.1	18	16	1854	6	22	31	69	<5	0.6	12	133	<0.01	1.47	2.93	4.17	1.34	0.25	0.01	0.11
42400	80	1 5	2030 12	115	42	ত্র	0.4	13	11	1376	4	19	14	41	<5	0.2	5	147	<0.01	0.73	3.33	4.02	0.52	0.26	0.01	0.11
727 10		1																								l
42411	20		1702 8	277	30	_ ⊲	<0.1	13	11	621	3	15	20	113	<5	0.2	7	57	<0.01	1.50	1.29	3.46	1.07	0.30	0.01	0.14
424 12	24	1 2	1378	78	37	- 5	<0.1		10	856	6	16	17	100	<5	0.2	6	97	<0.01	1.28	1.93	3.17	0.87	0.27	0.01	0.13
424 12			2300	54	38	A	<0.1	12	11	942	2	16	14	73	<5	0.2	4	158	<0.01	0.88	2.96	3.26	0.56	0.26	0.01	0.11
404.14	3.5		2037	50	46	പ്	<0.1	2	11	689	3	17	17	80	<5	0.3	7	106	<0.01	0.87	2.02	2.97	0.47	0.29	0.01	0.12
424 14 1	3.6		2048	49	43	đ	<0.1	11	10	682	0	15	13	77	<5	0.2	4	102	<0.01	0.81	1.97	2.89	0.44	0.28	0.01	0.11
747 19	0.0	"		<b>1</b>																						1
10415	7.	1	4131 40	79	71	-	<b>4</b> 1 1	4	19	1080	3	16	23	65	<5	0.3	5	183	<0.01	1.28	2.94	4.78	0.84	0.24	0.02	0.12
424 10	7.0		5278	10	35	2	20.1		12	532	5	21	26	57	6	0.2	5	32	<0.01	1.65	0.84	4.79	1.50	0.23	0.01	0.13
424 70	7.0		225	30	-5	5	-0.1		14	501	õ	25	11	23	<5	0.2	3	57	<0.01	0.71	1.84	4.81	0.69	0.18	0.01	0.11
4241/	0.0		395				<0.1		14	858	0	22	14	23	6	0.2	3	76	<0.01	0.73	2.63	4.91	0.70	0, 19	0.01	0.11
424 18	0.9		205	40	~		0.1		17	680		28	10	34	-5	0.6	10	87	<0.01	0.61	3.13	4.49	0.58	0.18	0.01	0.11
424 19	0.0	°		<b>~</b>	•	•	0.2		[ "	~~~	<b>~</b>	- 1		<u>٦</u>		1										1
		1 -	457		العمر	ا مر	-		14	782	0	25	•	26	6	0.2	2	54	<0.01	0.37	2.07	4.69	0.63	0, 18	0.01	0.11
42420	0.4			20					1 12	834	2	23	<b>n</b>	33	-5	0.2	2		<0.01	0.42	3.06	4.15	0.88	0.18	0.01	0.11
42421	0.4			50	~		-0.1	47	14	782	2	22	<u> </u>	33	6	0.2	3	75	<0.01	0.57	2.84	4.24	0.84	0.17	0.01	0.12
42422	0.5		2000	57	<0 _				16	815		22		20	6	0.2	3	79	<0.01	0.43	3.11	4.48	0.73	0.17	0.01	0.11
42423	0.8		301		5	<b>1</b>	-0.1		10	1010		24		31		0.2	l ă	25	-0.01	0.47	3.15	4.52	0.77	0.18	0.01	0.12
42423*	0.8	2	3/6 <1		- 1	•	<0.1	P	<b>"</b>	0 19	<sup>3</sup>	-	*	31	<b>1</b>	0.3					<sup>~</sup>	4.042		<b>.</b>		
				1		L			1	L.,,	L	L	x x	<b>.</b>	L				1							

Project/Venture:	1P	Geol:	K TROCIUK	Date Received:	JULY 30, 1992	Page	6	of	7
Areat	COREY	Lab Project No.:	D2470	Date Completed:	AUG 16, 1992	Attn:	K TROC	IUK	
Remarks:							S HOFF	MAN	
Au - 10.0 g aample digest	ed with Aqua Regia and determined by Graphite Fu	mace A.A. (D.L. 1 PPB)					J KOW/	ALCHUK	
ICP - 0.5 g sample digeste	d with 4 ml Agua Regia at 100 Deg. C for 2 hours.						E KIMU	RA	

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ICP - 0.5 g sample digested with 4 ml Aqua Regia at 100 Deg. C for 2 hours. N.B. The major oxide elements, Ba, Be, Cr, La and W are sarely dissolved completely with this acid dissolution method.

SAMPLE		Ag	Mo	Cu	Pb	Zn	As	Sb	Cd	N	Co	Mn	Bi	Cr	Y	Ba		Be	LA	Sr	п	A	Ca	Fe	Mg	K	Na	P
No.		ppm	pom	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	pom	ppm	%	%	%	_%		_%_	%	%
42424		0.1	<1	172	<1	61	<5	ଏ	<0.1	15	14	538	2	26	12	26	( < 5	0.3	4	57	<0.01	0.71	2.31	5.30	0.82	0.16	0.01	0.12
42425		0.3	3	162		58	27	10	<0.1	20	20	624	<2	28	28	40	7	0.8	- 14	84	<0.01	0.67	3.09	5.20	070	0.15	0.01	0.11
42426		0.1	<1	88	<1	44	්	<5	<0.1	13	13	727	<2	27	10	35	-5	0.2	2	78	<0.01	0.67	3.32	4.67	0.91	0. 19	0.01	0.11
42427		0.2	2	62	880 H	35	<⊅	ব	<0.1	2012	12	997	4	24	11	32	<5	0.2	2	t28	<0.01	0.51	5.20	4.48	0.63	0, 16	0.01	0.10
42428		0.4	4	26		38	<5	<10	<0.1	500	12	675	2	22	10	26	ත	0.2	2	118	<0.01	0.55	4.35	6.06	0.55	0.14	0.01	0, 10
								1																				
42429		03	4	56	<b>1</b>	38	7	ব	<0.1	13	12	862	2	26	10	19	- 5	0.2	2	116	<0.01	0.58	4.43	4.93	0.56	0.16	0.01	0, 10
42430		0.7	i i	41	3	40	12	<5	<0.1	13	13	1269	2	28	12	21	6	0.3	5	96	<0.01	0.36	3.85	4.16	0.23	0.17	<0.01	0.11
42431		07	i i	45		49	6	- 6	<0.1	12	13	17 16	2	27	9	15	ব	0.2	2	105	<0.01	0.39	4.27	4.96	0.31	0.15	<0.01	0.10
42432		0.7	1	38		53	-65	<5	<0.1	12	13	1393	2	27	9	13	6	0.2	1	94	<0.01	0.41	3.64	4.76	0.32	0.16	<0.01	0.11
42422		0.7		37		55	~		-0.1		12	1404	0	28	•	13	6	0.2	2	2	<0.01	0.41	3.70	4.68	0.32	0.16	<0.01	0.11
76796		0.7	l .	<b>, ,</b>		~~	~	ľ			-		-						-									••••
40400		0.2		45		-	~	~	-01		18	640	ĸ	20	20	27	ച	04	7		-0.01	0.98	248	4.59	0.99	0.17	0.01	0 12
42438		0.2					~		-0.1			657	ň	22	10 To	24		0.2	2	KG	-0.01	1.04	2 10	4 45		0.16	0.01	0.12
42440		0.2	1	49		60	~		-0.1		12	034		25	19	36	-5	0.2	2		-0.01	1 11	3.49	4.32		0.17	0.01	0.11
42442		u 1	9	40		000	<0		SU. 1		10	4374	~	23	20 C	30		0.2			-0.01		2.74	5 12		0.15	0.01	0.12
42443		0.5	0	44		200	10	<0	1.0			1071	~~	~~~~	<b>CD</b>	40		0.2	-		-0.01	1.1	3.74	- 3. 12 A 20		0,10	0.01	0.12
42444		0.4	7	1 103		121	10		<0.1		24	137.1	4	22	45	31	<0	0.2	<b>4</b>		<0.01	1.91	3.53	0.30		U. 14	0.01	U. 13
	Į											1005								400				# 70		0.15		
42446		1.4		[ 11]		926	<b>0</b> 9	0	3.3		30	1090	B	39		38	8	0.3	2	124	<0.01	2.48	4.20	0.70		0,10	0.01	0.14
42447		0.5	1 7	56		3/5	43	4	0.9	<b>6</b> U	31	2410	3	89	TU I	- 34	8	0.4	Z	ICA	<0.01	3.52	0.28	0.97		0.10	0.01	0.11
42448		7.0	8	87		653	58	9	2.4	26	24	2581	2	31	46	46	<0	0.3	<1	150	<0.01	2.44	5.11	6.67		0.16	0.01	0.14
42449		1.2	5	56	21	236	9	ব	<0.1		42	1864	<2	127	133	40	0	0.4	2	163	<0.01	3.96	5.32	6.15		0.07	0.01	0.06
STD-P1		0.3	64	27	53	154	19	<5	0.2	35	6	587	⊲	118	37	163	୍	0.5	7	<b>P2</b>	0.11	1.15	0.94	2.29		0.36	0.07	0.08
			_	i																								
TM-9		<0.1	2	31		58	8	6	0.3	20	13	348	8	113		153	9	1.0	32		0.1/	0.96	0,49	3.10	S. Sanitard	0.24	0.08	0.10
TM-11	· ·	<0.1	1	17	3	55	5	9	0.1	17	12	327	3	107	62	176	<5	0.7	26		0.17	0.91	0.49	2.60	0.00	0.28	0.06	0.09
TM-17		<0.1	1	9	8 <b>*</b> 1	43	<5	<5	<0.1	<b>10</b>	5	279	2	101		127	- 5	0.3	19	39	0.13	0.73	0.53	1.90	Sec.	0.22	0.07	0.11
TM 18		<0.1	1	9		44	<5	4	<0.1		6	316	2	122		139	୍ୟ	0.3	25	46	0.16	0.79	0.72	2.38	الشنشقا	0.24	0.06	0, 15
TM-19		0.1	<1	8	8 <b></b>	40	- 5		<0.1		6	269	2	91	49	115	<5	0.3	26		0.15	0.67	0.78	2.53		0.20	0.06	0, 18
	{																_											
TM-23		0.1	1	38		118	9	8	<0.1	38	14	1168	2	72	74	123	<5	1.0	17	33	0.10	1.87	0.45	4.59	1.03	0.17	0.06	0, 10
TM-24		<0.1	2	36		116	<5	<5	<0.1	38	14	1025	4	71	75	124	්	1.0	16	33	0.10	1.91	0.46	4.65	1.00	0.18	0.06	0, 10
TM-25		0.1	3	23	2	110	ব	8	<0.1	37	15	7 12	2	65	74	98.	<5	0.9	- 14	75	0.23	2.24	0.82	4.81	1.32	0.21	0.27	0.08
TM-26		0.1	2	36	2007	148	6	<⊅	<0.1	39	14	1091	2	63	56	96	්	0.8	- 14	22	0.05	2,10	0.35	5.14	1.14	0.17	0.05	0.11
TM26*		0.1	3	36		151	7	<5	<0.1	38	14.	1061	3	62	55	95	- 5	0.8	13	21	0.05	2.07	0.34	5.10	1.13	0.17	0.05	0.10
			]								] ]							]										
TM-30		0.6	7	109	12	204	14	6	0.6	50	17	907	2	74	97	263	<5	0.6	12	52	0.10	1.73	0.64	4.35	1.40	0, 16	0.02	0.13
TM-31		0,8	7	109	12	195	15	<5	0.6	48	17	942	<2	71	97	272	<5	0.5	11	49	0.10	1.76	0.64	4.45	1.45	0,16	0.02	0, 13
TM-32		1.0	9	128	13	252	19	10	1.1	<b>59</b>	21	1099	2	73		286	ব	0.6	12	55	0.10	1.80	0.66	4.72	1.43	0, 17	0.02	0.14
TM-33		0.8	8	121		225	21	9	0.8	53	19	1009	2	74	100	294	<5	0.6	12	57	0.12	1.83	0.72	4.64	×1.45	0, 19	0.02	0.14
TM-34		0.7	5	90		148	14	7	0.3	39	17	792	<2	85	94	252	ব	0.6	- 14	52	0.11	1.73	0.75	4.13	128	0.20	0.04	0, 13
						1															{					:		
TM-35		0.8	5	115		191	19	<5	0.5	45	19	931	~2	69		269	<5	0.5	11	56	0.12	1.88	0.82	4.66	1.42	0.21	0.03	0, 15
JP88-83		0.4	2	56		131	20	- 6	<0.1	21	13	835	<2	54	62	170	<5	0.4	9	69	0.04	1.82	1.22	4.61	1.26	0.21	0.02	0.12
JP-96		0.1	3	37		120	6	6	<0.1	20	12	833	3	46		131	ব	0.5	11	41	0.14	1.85	0.60	5.07	1.05	0.15	0.04	0.12
JP-115		0.2		35		157	9	6	0.1	21	11	869	2	45	54	135	- 5	0.5	12	36	0.11	1.75	0.50	4.84	1.04	0.16	0.04	0,12
JP-116*		0.2		38		161	Ă	6	0.2	22	12	872	2	47	57	140	6	0.6	13	37	0.11	1.78	0.52	4.92	1.08	0, 16	0.04	0.12
		v		‴ ا			Ŭ						-															
1		<u> </u>				r i		h		second second	• • • • •			· · · · · · · · · · · · · · · · · · ·	شيت بتبديت		أسبب وسعومي و							_				

JP - 118 JP - 128 JP - 129 JP - 130 JP - 132

	MPLE Ag Mo Cu					un Regi ni Aqua ie, Cr, L	h and c Regin s a and V	letermir it 100 E Vare m	ved by G leg. C fa rely disa	ìnaphile Ir 2 hou Iroived	) Furna.c Ins. complet	Geol: Lab Pro is A.A. ( toly with	pject No (D.L. 1 I n this ac	k: PPB) sid disso	K TROC D2470 plution r	CIUK method		Date R Date C	eceive ompiet	1: ed:	JULY 30 AUG 18	), 1992 , 1992		Page Altn:	7 K TROC S HOFF J KOW E KIMU	of HUK MAN ALCHUN IRA	7
SAMPLE	Ag	Mo	Cu		Zn	As	Sb	Cd	N.	Co	Mn	Bi	Cr	X.	Ba	W	Be	La	Sr	TI	A	On I	Fe	Ma	K	Na	Ρ
No.	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ррпз	%	%	%	%	<b>%</b>	%	~ ∞	%
1 18	0.2	6	46	13	173	12	12	0.7	28	15	851	8	56	66	136	\$	1.1	23	38	0.09	1.77	0.47	4.72	1.04	0.15	0.04	0.12
128	0.2	6	28		159	8	<5	<0.1		11	737	- 4	64	60	114	5	0.8	17	32	0.09	1.79	0.43	4.34	0.99	0.16	0.07	0.08
129	0.1	4	27	3	116	9	0	<0.1	25	10	594	5	51	50	93	<5	0.8	16	26	0.06	1.71	0.33	4.56	0.91	0.14	0.05	0.09
130	0.1	3	28		130		5	<0.1	27	- 14	940	5	50	80	89	<5	0.9	13	63	0.17	2.32	0.71	5.22	1.44	0. 19	0.17	0.10
132	0.1	7	16	9	103	32	4	<0.1	23	11	667	5	50	83	86	4	0.7	11	46	0.12	2.12	0.59	5.26	1.42	0.15	0.11	0.12
134	1 1.0	4	61		417	17	4	1.6	30	17	901	9	62	88	144	<5	0.5	9	21	0, 10	1.83	0.49	5.34	1.05	0.20	0.06	0.09
56 - T1	422.0	5	4 18	578	2210	1050	753	16.7	80	9	31748	47	39	25	6	<5	0.3	5	5	<0.01	0.31	0.29	18.23	1.82	0.04	0.01	0.03
58 - T2	27.0	2	50	81	44 12	251	1 18	35.6	190	- 44	11010	9	150	63	9	<u> </u> ସ	1.3	3	K	<0.01	1.97	1.48	9, 10	1.87	0.16	[⊲0.01]	0.05
<b>18 13</b>	20.0	4	48		4276	232	125	34.3	184	41	7380	6	184	79	9	5	1.6	2	27	<0.01	2.55	3.33	7.82	2.56	0.16	<0.01	0.05

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				8				30.030 AS			1	18					0.0303	336	1	1		268869999			1
JP-134	1.0	- 4	61 41	417	17	ব্য	1.6	30	17	901	9	62	68	- 144	<5	0.5	9	친 0.1	Ю 1.8	3 0.49	5.34	1.05	0.20	0.06	0.09
KK-86-T1	422.0	5	4 18 578	2210	1050	753	16.7	60	9 3	1748	47	39	25	6	<5	0.3	5	5 <0.(	1 0.3	1 0.29	18.23	1.82	0.04	0.01	0.03
KK~68 - T2	27.0	2	50 81	44 12	251	118	35.6	190	44 1	1010	9	150	63	9	-5	1.3	3	14 <0.0	)1 1.9	7 1.48	9.10	1.87	0.16	<0.01	0.05
KK68 T3	20.0	- 4	48 13	4276	232	125	34.3	<b>114</b>	41 1	7380	6	184	79	9	ব	1.6	2	27 <0.0	)1 2.5	5 3.33	7.82	2.56	0.16	<0.01	0.05
KK-88-T3*	20.0	2	42 12	4264	230	123	33.6	178	39 7	366	5	177	76	9	ර	1.5	2	28 <0.(	01 2.4	4 3.30	7.60	2.44	0.15	<0.01	0.05
KK-88-14	45.0	2	96 23	1121	394	123	5.1	182	41 1	674	7	184	80	14	12	1.4	9	18 <0.(	)1 2.3	1 2.27	8.70	1.97	0.20	<0.01	0.04
KK-68-T5	1044.0	<b>4</b>	10 15 34 12	963	1480	2907	7.3	56	6 4	)407	46	14	15	<1	ර	0.1	5	5 <0.0	0.0	6   0.24	20.94	1.87	0.02	<0.01	0.03
TD-68-66	1.3	<1	18 41	19	7	40	<0.1		5	767	~2	84	32	142	<5	0.2	13	37 0.	1 0.7	2 0.46	2.17	0.55	0.24	0.06	0.09
TD-68-77	0.3	1	13 5	32	4	8	<0.1	2	6	342	~2	117	51	181	<5	0.3	18	7 0.	5 0.9	0 0.54	2.80	0.64	0.29	0.06	0.11
TD8880	0.2	<1	9	21	ব	6	<0.1	13	7	358	2	94	58	193	<5	0.3	21	50 0.	6 0.9	4 0.63	3.18	0.69	0.31	0.06	0.14
TD-68-81	<0.1	8	17 9	34	ব	18	<0.1	15	8	493	2	97	58	176	<5	0.5	23	13 0.	5 0.8	6 0.55	3.02	0.61	0.28	0.06	0.11
TD8881*	<0.1	3	20 212	44	<5	17	<0.1		9	527	2	<u>93 </u>	57	168	্হ	0.5	24	12 0.	4 0.8	1 0.53	2.93	0.59	0.26	0.05	0.11

**Geochemical Analysis** 

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		ProjectA Area: Remarks Au - 10. ICP - 0.5 N.B. The	/enture: 0:gsamp 5:gsamp amajoro	ole diges le diges xlde eler	SAMPLE ted with A ted with 4 nents and	1P COR 104 B08 S WERE Qua Peç mi Aqua Ba, Be,	YRBCCE 104809 ANALYZE giaand de Regiaat Cr, Laan	D 3 TIM termine 100 Deg d Wane	ESFOR/ d by A.A. J. C for 2 i rarely dis	NU. SEE (D.L.5 Pi hours. solved co	PROJEC PB) ompletel	( L CTP1608. ly with this	Seologis Ab Proje ASY FO acid di	t: ect No.: R MORE ssolution	AU BESU	3 SHEV D1608 JLTS			Date Re Date Co	calved; mpletad;		OCT 8, 11 NOV 7, 11	99 1 99 1		Page Attn:	1 G SHEVC JKOWAL E KIMUR R HODG:	of HENKO CHUK A SON	١
SAMPLE	Au	Ag	AI	As	Ba	Be	Bi	Ca	Cd	Co	Cr	Cu	Fe	ĸ	্ৰা	Mg	Mn	Mo	Ne	Ni	P	Pb	Sb	Sr	Tì		W	Zn
No.	ppb	ррт	. %	ppm	ppm	ppm	ррт	%	ρpm	opm	ppm	ppm	%	%	ppm	%	ppm	ppm	<b>%</b>	ppm	%	ppm	ppm :	ppm	*	ppm	ppm	ppm
B2329	<5	0.3	1.36	8	82	<1	2	0.51	13	13	7	45	527	0.05	्राउ	0.67	876	7	0.02	21	0.15	14	<5	40	0.06	51		232
82331-	25	0.4	1.64	51	84	<1	<2	0.61	0.6	215	22	52	4.53	0.07	<u> </u>	0.95	973	6	0.02	31	0.15	21	<5	37	0.06	62	<10	183
B2333	<5	0.3	1.58	13	131	<1	<2	041	0.9	17	33	55	4.59	0.05	14	0.87	1739	3	0.02	53	0.12	16	<5	22	0.03	51	<10	174
B2335	<5	0.2	2.32	68	159	<1	<2	0.97	13	19	25	63	5.12	0.05	- 1 <b>7</b>	0.82	1694	6	0.03	33	0.11	16	7	51	0.06	70	<10)	248
82337-	130	0.5	1.64	56	155	<1	<2	0.62	1.1	22	14	100	5.53	0.05	종극박	0.72	1444	3	0.02	40	0.12	32	6	44	0.02	39	<10	248
62339	<5	0.3	2.24	198	102	<1	<2	1.19	18	22	34	45	5.37	0.05	13	0.90	1821	2	0.04	54	80.0	15	26	31	0.14	100	<10	277
B2341	<5	0.6	2.49	322	87	<1	<2	1.27	1.3	21	38	71	6.00	0.06	13	1,10	1350	2	0.04	48	0.12	29	33	34	0.13	100	<10	266
87786 -	<5	2.4	1.82	81	156	<1	<2	0.59	4.0	19	9	91.	6.83	0.09	12	0.77	1935	4	0.01	69	0.13	22	14	18	0.04	51	<10	520
B7788-	20	0.1	4 20	17	7.1	<1	<2	2.19	a0	41	74	<u>66</u>	5.98	0.06	6	2.54	1139	<1	0.03	73	0.08	12	<5	41	031	130	<10	146
STD-AU8-P1	250	0.2	1.14	21	163	<1	2	0.98	0.3	8	109	26	2.00	031	9	0.88	589	44	90.0	34	80.0	55	<5	77	D.11	25	<10	144
87790-	30	20	1.55	28	156	<1	<2	08.0	3.3	18	14	81	5.85	0.05	14	88.0	1336	18	0.01	56	0.12	21	<5	26	0.05	57	14	527
B/792-	20	0.4	1.93	28	98	<1	<2	1.24	0.3	21	19	81	5.37	0.08	13	1.71	1379	3	0.01	24	0,18	34	<5	101	0.04	95	<10	165
87792*		0.5	1.95	34	103	<1	<2	1.25	04	21	21	82	545	80.0	14	1.72	1395	3	0.01	25	0.19	33	<5	101	0.04	97	<10	167

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# PLACER DOME RESEARCH CENTRE

Geochemical Analysis

	Project/Venture: Area: Permarks: Au – 10.0 g sample digested ICP – 0.5 g sample digested N.B. The major oxide element SAMPLE Au Ag AI As							termined 100 Deg d Ware i	by A.A. C for 2 rarety dis	(D.L.5.P. hours. solvedice	PB) ompletel	C L ywith this	∂eologis ab Proje ackof di	t: act No.: ssolution	method.	G SHEVO	CHENKO		Date Received: Date Completed:		OCTOBE	778, 1991 7730, 199	1	Page Attn:	1 G SHEVC J KOWAL E KIMUR/ R HODGS	of HENKO CHUK A SON	1
SAMPLE	Au	Ag	AI	As	Ba	Be	Bi	Ca	Cd	Co	Cr	Cu	Fe	К	ंष्ट्रा	Mg	Mn	Mo	Na Ni	P	РЪ	Sb	Sr	ਾ	<u>v</u>	W	Zn
No.	ррь	ppm	%	ppm	ppm	ррт	ppm	%	ppm	pom.	ppm	ррл	<u>%</u>	<u>%</u>	ppm	%	ppm	ppm	% ppm	*	ppm	ppm			<b>p</b> pm	_ppm	
82330	<5	0.3	1.54	15	147	<1	<2	0.49	8.0	12	12	41	4.66	0.05	्र 12	0.94	934	5	0.03	0.13	13	< 5	53	0.00	33	<10	1/0
B2332	<5	0.1	1.59	15	76	<1	<2	0.45	0.3	9	9	12	4.58	0.04	15	0.79	1756		0.04	0.10	16	<5	30	0.05	34	<10	120
B2334	<5	0.2	1.67	11	152	<1	<2	0.67	12	. 15	30	33	4 27	0.07	13	0.80	1895	3	0.04 40	0.13	13	<5	38	000	20	<10	180
82336	<5	02	2.02	55	139	<1)	<2	0.98	1.3	16	29	43	4 29	0.04	14	0.71	1570	3	0.04 25	0.10	15	្រំ	28	00/		<10	212
82338	<5	0.2	1.58	55	132	<1	<2	0.67	60	20	21	79	4.90	0.05	9	0.78	1377	1	6003 Sa	0.10	- 24	< 2	51	ULA	39	<10	<u> ط</u>
B2340	-5	0.3	1.72	134	79	<1	<2	1.67	13	18	36	39	4.05	0.05	10	0.67	17 19	2	0.04 31	0.10	9	5	42	60.0	77	<10	193
B2342	-5	04	1.75	256	70	<1	<2	2.18	13	15	43	45	3.43	0.05		0.58	1693	3	0.02 30	0.12	16	14	52	0.05	61	<10	179
B7785	<5	10.	1.77	68	188	<1	<2	0.52	4.1	18	10	89	6.37	0.08	ે મો	0.76	2031	5	0.02 50	0.13	ম	7	19	003	48	<10	کلک
B7787	<5	<0.1	4.15	32	75	<1	<2	1.79	80	44	75	89	6.13	0.06	5	2.53	1351	<1	0.03 72	80.0	6	<5	44	0.25	124	<10	168
87787	NSS	<0.1	4.19	41	65	<1	<2	1.84	0.5	45	78	89	6,18	0.06	4	2.63	1307	<1	0.03 72	0.08	7	<5	42	0.24	123	<10	157
					1.101	I			- F	2 A. S.					4 C - 1									~~ <u>~</u>			
87789 -	<5	0.3	149	33		<1	<2	0.56	3.8	18	20	75	521	0.05	15	0.90	147 1	19	0.01 81	0.12	24	<5	29	0.05	57	11	065
B7791 -	<5	0.5	1.91	30	85	<1	<2	0.84	a.o	50	24	80	4.94	80.0	· 12	1.74	1379	<1	0.01 23	0.15	35	<5	84	0.03	92	<10	163
STD-AU8-P1	235	0.3	1.10	20	183	<1	<2	0.93	03		116	26	227	0.33	. 10	0.84	600	44	0.06 31	0.08	55	<5	93	0,11	40	<10	140

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