ARIS SUMMARY SHEET

District Geologist, Kamloops Off Confidential: 94.12.24

ASSESSMENT REPORT 23116 MINING DIVISION: Kamloops

PROPERTY: Ashton
LOCATION: LAT 50 15 00 LONG 121 23 00
UTM 10 5567458 615260
NTS 092I03W 092I06W
CLAIM(S): Rebecca 1-6,Rachel 1-4,Sheryl,Mellisa
OPERATOR(S): Kingston Res.
AUTHOR(S): Smith, S.W.
REPORT YEAR: 1993, 41 Pages
COMMODITIES
SEARCHED FOR: Copper
KEYWORDS: Triassic,Mount Lytton Complex,Spences Bridge Group,Limestones
Diorites,Andesites,Epidote,Magnetite
WORK
DONE: Geophysical,Geochemical,Geological
IPOL 9.9 km
Map(s) - 2; Scale(s) - 1:5000
SOIL 158 sample(s) ;ME
Map(s) - 1; Scale(s) - 1:5000
RELATED
REPORTS: 02532,02533,23028

Filmed

KINGSTON RESOURCES LTD

NTS: 92I/3W/6W

November 10, 1993

ASSESSMENT REPORT

GEOCHEMICAL SAMPLING AND GEOPHYSICAL SURVEY

ON THE

ASHTON PROPERTY

(REBECCA 1-6, SHERYL, MELLISA AND RACHEL 1-4 CLAIMS)

KAMLOOPS MINING DIVISION

LATITUDE: 50° 15'N LONGITUDE: 121° 25'W

REPORT BY

S.W. SMITH

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KINGSTON RESOURCES LTD

NTS: 92I/3W/6W **November, 1993**

ASSESSMENT REPORT-ASHTON PROPERTY

SUMMARY

The Ashton property is a porphyry copper prospect located 15 km east of Lytton, BC. The second phase of field work in 1993, consisting of geochemical soil sampling and IP survey, outlined a zone 500 by 500 m of coincidental anomalous copper in soils and high chargeability that together with data from previous owners and government mapping indicates that the Ashton property not only covers an area with known skarn alteration/mineralization, but also has excellent potential for porphyry style mineralization similar to the world class orebodies found in the Highland Valley area, 40 km to the northeast.

INTRODUCTION

The Ashton property is a porphyry copper prospect located 15 km east of Lytton, BC, on the southeast side of the Thompson River, with good road access from the Trans Canada Highway (Figure 1). The first recorded work in the area of the property was in the late 1960's when geochemical surveys and trenching found copper mineralization. The Rebecca 1 to 6 and Sheryl claims were staked in 1989-90 and Magnetometer and VLF-EM surveys were performed. Kingston optioned the property from Sylvia Apchkrum in April 1992. Kingston Resources staked the Rachel 1 to 4 claims in July, 1992. From June 8 to 15, 1993, Kingston's field work consisted of chaining and flagging 11.1 km of grid lines, geochemical sampling, prospecting and mapping on the property. This work is documented in the assessment report by the author, dated September 20, 1993. Due to favourable results further work was initiated: from July 5-7, 4.2 line km of IP survey; from July 20-27 the expansion of the grid by 6.9 line km and further soil sampling (158 samples); and from August 4-9, 1993 a further 5.7 line km of IP survey were performed.

LOCATION AND ACCESS

The claims of the Ashton property are located in the Kamloops Mining Division approximately 15 km east of Lytton, BC, on the southwest side of the Trans Canada Highway. The claims are centred on Latitude 50^0 15'N and Longitude 121^0 23'W (Figure 2). Access to the property from the highway is less than 2 km along the Nicoamen River Forest Service Road, an all weather gravel road, which crosses through the property.

PHYSIOGRAPHY

The property is situated along the southeast side of the Thompson River which at this point turns and flows east to join the Fraser River at Lytton. The majority of the claims are situated on steep northerly and westerly facing slopes where elevations range from 1000' to 3800' above sea level.

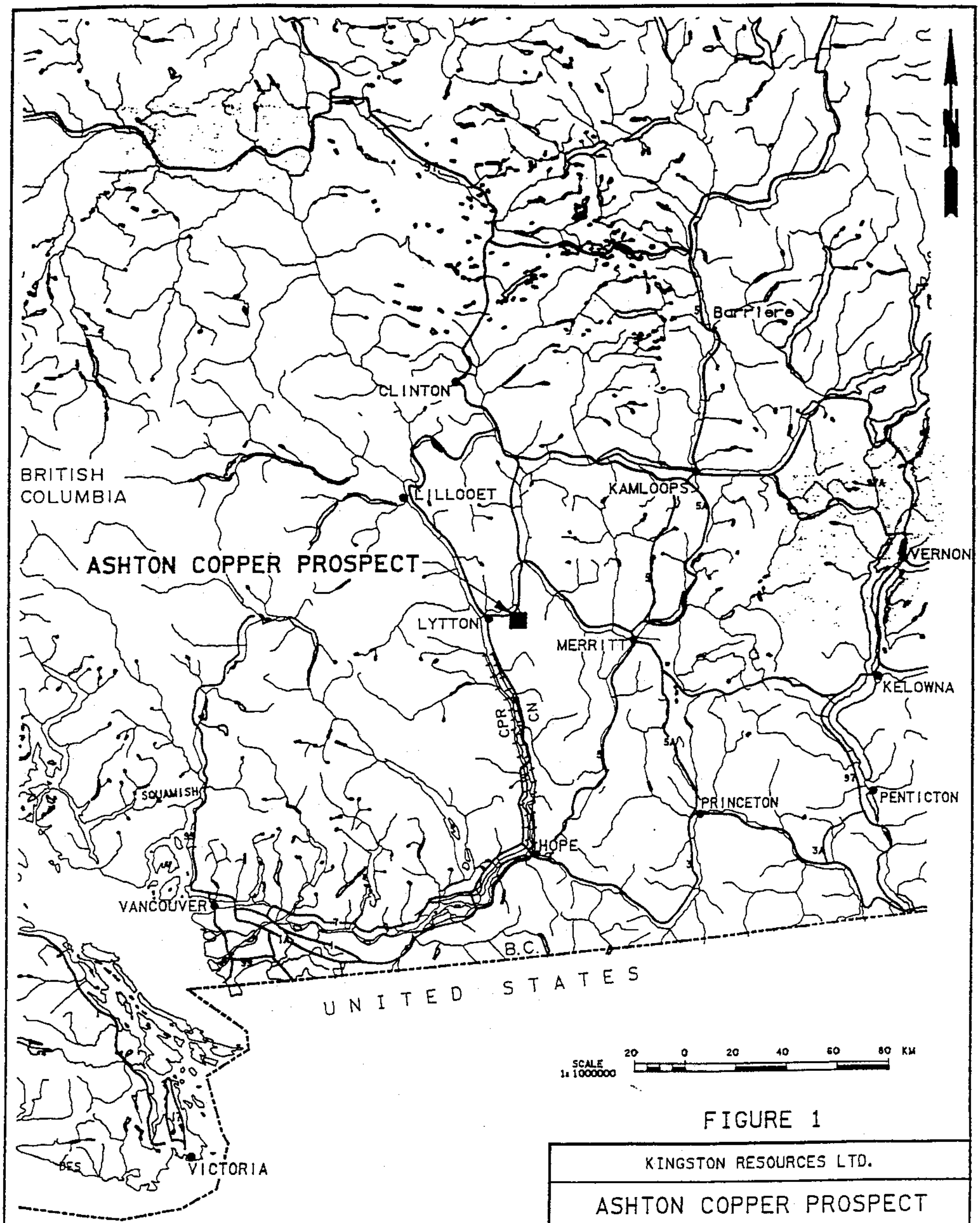
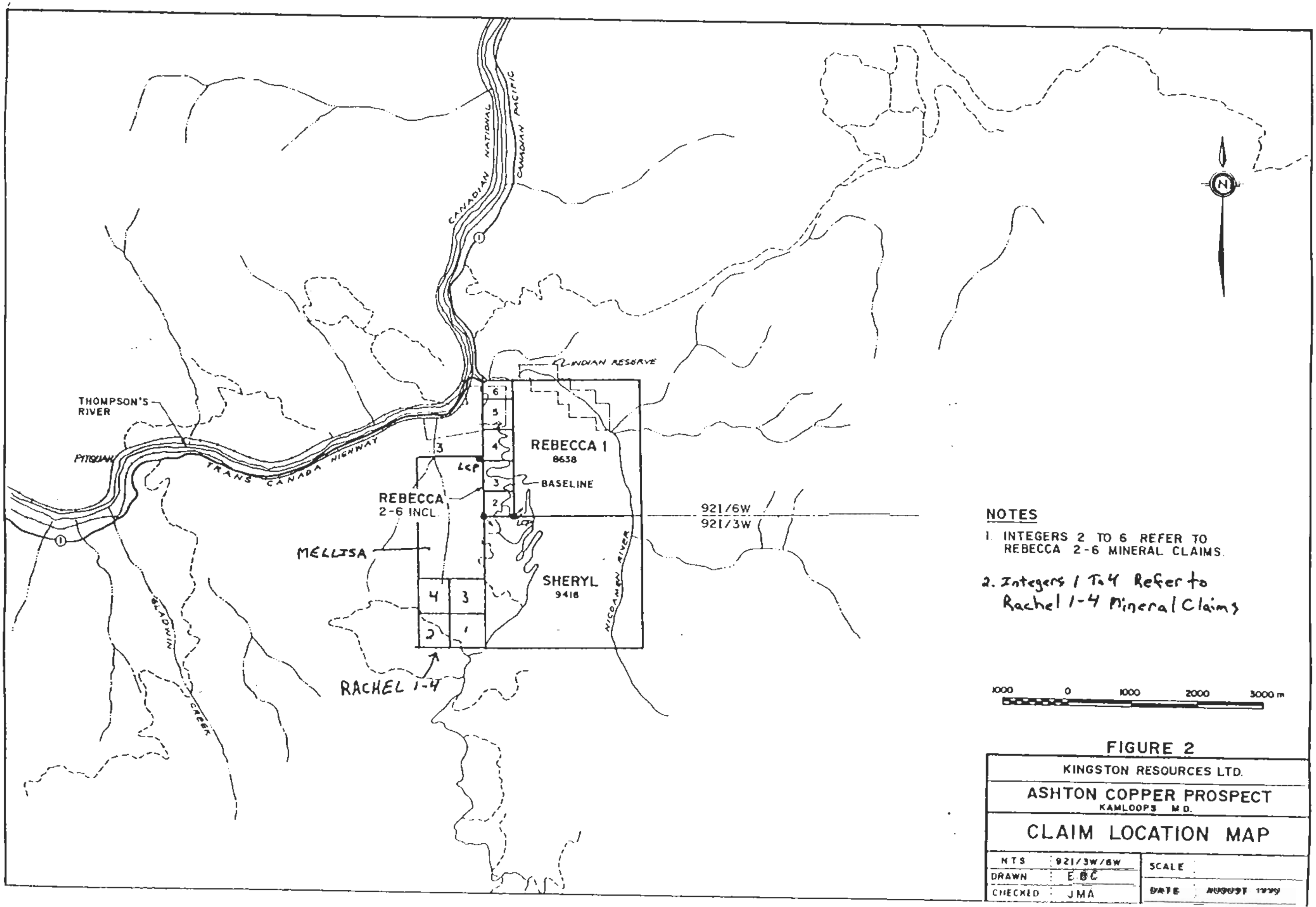


FIGURE 1

KINGSTON RESOURCES LTD.
ASHTON COPPER PROSPECT
GENERAL LOCATION MAP



CANADIAN NATIONAL
CANADIAN PACIFIC
INDIAN RESERVE
THOMPSON'S RIVER
PITQUAH
TRANS CANADA HIGHWAY
REBECCA 1
8638
BASELINE
LCP
REBECCA
2-6 INCL.
MELLISA
SHERYL
9416
NICOAMEN RIVER
BLADWIN CREEK
RACHEL 1-4
92I/6W
92I/3W
NOTES
1. INTEGERS 2 TO 6 REFER TO REBECCA 2-6 MINERAL CLAIMS.
2. Integers 1 To 4 Refer to Rachel 1-4 Mineral Claims
1000 0 1000 2000 3000 m
FIGURE 2
KINGSTON RESOURCES LTD.
ASHTON COPPER PROSPECT
KAMLOOPS M.D.
CLAIM LOCATION MAP
NTS 92I/3W/6W
DRAWN E.B.C.
CHECKED JMA
SCALE
DATE AUGUST 1999

Snow and rainfall appear to be quite light with summer weather being very hot and dry. Forest cover varies from thinly covered rocky slopes to thick dense regrowth areas where logging was done in the 1960's. Spruce, pine, balsam and hemlock typical of the somewhat dry, hot climate between Lytton and Ashcroft are present.

PROPERTY AND OWNERSHIP

The property consists of 53 claim units recorded in the Kamloops Mining Division. The Rebecca and Sheryl claims were optioned from Sylvia Apchkrum by Kingston Resources Ltd. in April 1992. The Rachel claims were staked for Kingston Resources Ltd. in July 1992. The Mellisa claim was staked by the author on July 1, 1993. Current due dates are listed below, these dates are subject to acceptance of all assessment work submitted.

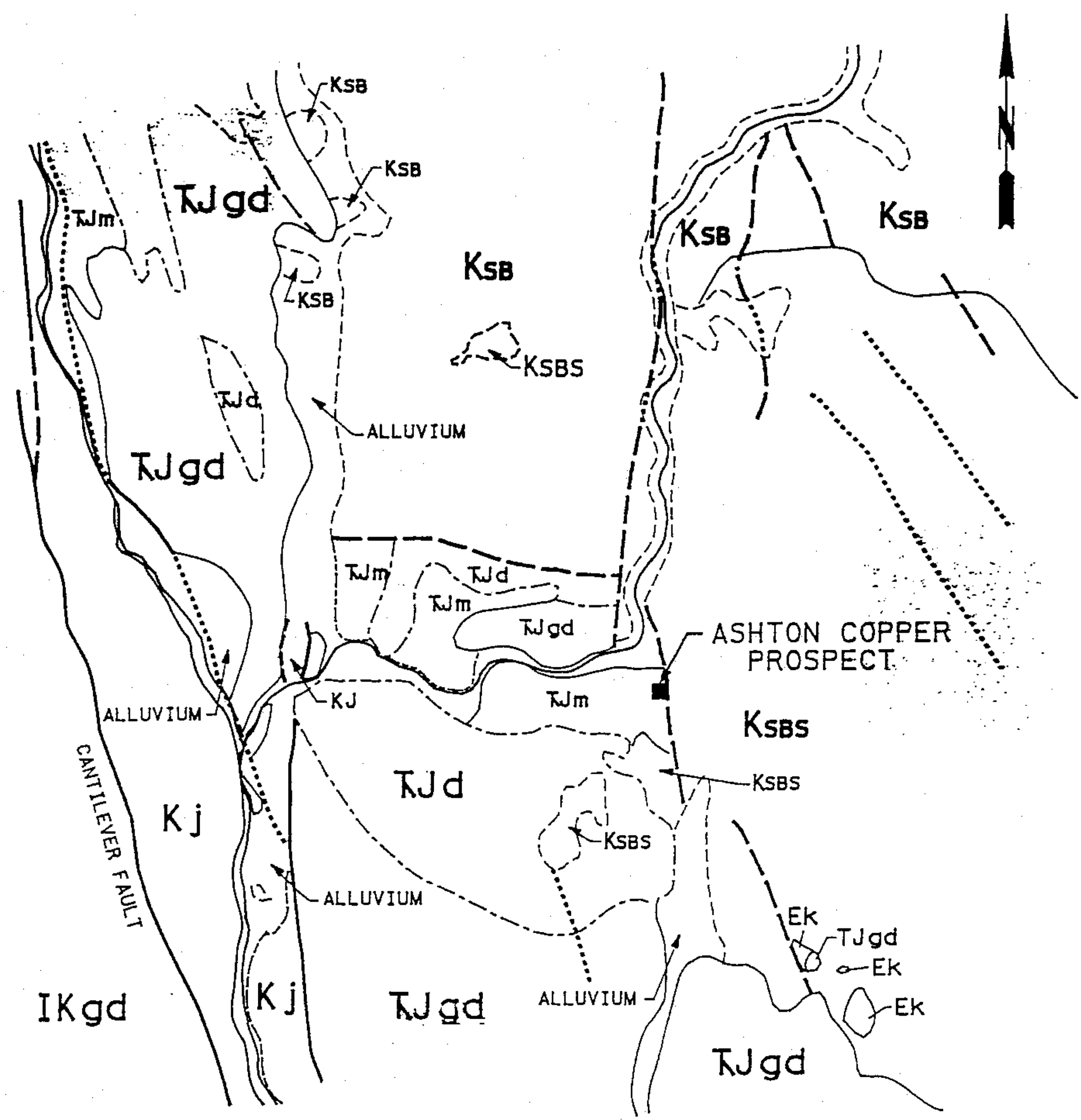
Claim Name	Record Number	No. of Units	Due Dates
Rebecca 1	218569	16	June 21, 1996
Rebecca 2	218570	1	June 20, 1996
Rebecca 3	218571	1	June 20, 1996
Rebecca 4	218572	1	June 20, 1996
Rebecca 5	218573	1	June 20, 1996
Rebecca 6	218574	1	June 20, 1996
Sheryl	219338	20	June 09, 1996
Rachel 1	311562	1	July 17, 1996
Rachel 2	311563	1	July 17, 1996
Rachel 3	311564	1	July 17, 1996
Rachel 4	311565	1	July 17, 1996
Mellisa	318692	8	July 1, 1996

HISTORY AND PREVIOUS WORK

The Ashton property covers an area that has seen little work filed for assessment. The property was covered by the Fil and T claims in 1969, when a geochemical soil survey for copper outlined a large zone (700 by 400 m) of anomalous copper (>200 ppm Cu). Follow up trenching of this zone located significant copper mineralization (35'of 0.73% Cu). Details of this work is documented in BC Mines assessment reports by J.W. Antal (#2532) and A.A. Burgoyne (#2533). In 1989-1990 the Rebecca 1 to 6 and Sheryl claims were staked. In 1990 VLF-EM and Magnetometer surveys were carried out on the Rebecca claims, these surveys are detailed by J.M. Ashton in his assessment report dated June 20, 1990.

REGIONAL GEOLOGY

The Ashton property lies in the southwestern part of the Intermontaine Belt. Figure 3 shows the regional geology of the area (Monger, 1989). The property straddles the boundary between the



LEGEND

FAULT

INFERRED FAULT

SCALE 1: 200000

4 0 4 8 km

LATE CRETACEOUS

IKgd -GRANODIORITE, QUARTZ MONZONITE

SPENCES BRIDGE GROUP

KsB -FELSIC, MAFIC FLOWS AND SANDSTONE -SHALE

KsBs -MAFIC VOLCANICS -CONGLOMERATE

EARLY AND MIDDLE CRETACEOUS

JACKASS MOUNTAIN GROUP

KJ SANDSTONE, ARGILLITE, CONGLOMERATE

TRIASSIC AND/OR JURASSIC

TJd -DIORITE, AMPHIBOLITE MT. LYTTON COMPLEX

TJgd -GRANODIORITE, QUARTZ MONZONITE MT. LYTTON BATHOLITH

TJm -LAYERED OF ROCK, AMPHIBOLITE, MYLONITE MT. LYTTON BATHOLITH

FIGURE 3

KINGSTON RESOURCES LTD.

ASHTON COPPER PROSPECT

REGIONAL GEOLOGY

MODIFIED AFTER J. W. H. MONGER GSC MAP 42-1989 older (Upper Triassic) Mount Lytton Complex on the west and the younger (Middle and Upper Cretaceous) aged Spences Bridge Group on the east.

The Mount Lytton Complex has been interpreted by Monger to be part of the roots of the Late Triassic Nicola arc. The complex is fault bounded, on the west by the Fraser River fault system and on the east by normal faults along the Thompson River. The Mount Lytton Pluton that is part of the complex has been age dated at 212 +/- 1 Ma (Parrish and Monger, 1992) which is very close to some dates reported from the central Guichon Batholith, which is located about 40 km to the northeast and contains the world class Highland Valley ore bodies. Parrish and Monger interpret the Mount Lytton and Guichon Creek bodies to be part of the Upper Triassic magmatic arc complex that characterizes Quesnellia terrane, but state that they were probably emplaced at different structural levels, as suggested by their contrasting settings.

The Middle and Upper Cretaceous Spences Bridge Group unconformably overlies and is in fault contact with the older Mount Lytton Complex. In the area of the property the Spences Bridge Group is relatively unaltered and consists of intermediate, locally felsic and mafic flows and pyroclastics along with sandstone, shale and conglomerate.

PROPERTY GEOLOGY

The property geology described here was mapped by the author in a previous report dated September 20, 1993.

On the east half of the property the rocks are typical reddish coloured andesitic flows and pyroclastics, typical of the Spences Bridge Group. The boundary between these volcanics and the older Triassic rocks was not seen, but it is believed that they either; unconformably overlie the older rocks, or are separated from them by steep dipping northerly trending faults that would be associated with the normal faults along the Thompson River to the north.

The rocks mapped in on the west side of the property are believed to be part of the Mount Lytton Complex (Personal Communication, Monger, 1993). These rocks were found to be a series of interbedded limestone and volcanic sediments with intrusive plugs or dykes of fine grained diorite.

The limestone varies from a clean white crystalline variety with a massive appearance to a thinly bedded grey silty variety. The limestone beds were noted to be from .5 to 5 m thick. Interbedded with the limestone was fine to medium grained green volcanic tuff that was much wider in width. The volcanics were commonly limy. Locally these rocks were very strongly altered and fractured, with the strongest alteration seen in the vicinity of the old trenches in the northwestern portion of the Sheryl claims.

The diorite noted on the property was dark grey/black and fine to medium grained with an intrusive appearance. It contained moderate to strongly disseminated magnetite and appeared to be from plugs or dykes associated with the Mount Lytton intrusives. Neither Antal or Burgoyne make reference to the diorite intrusions.

ALTERATION

Alteration on the property is varied, from relatively no alteration of the younger Spences Bridge Group on the east half of the property to locally very strong alteration within the Mount Lytton Complex on the west side. Alteration is strongest in prevalent north-south trending shear zones and at the contact between the diorite and the interbedded volcanics and limestone. Hydrothermal alteration of the volcanics was seen on a wide scale causing bleaching and quartz/carbonate veining within them. Epidote is the most common alteration mineral. Locally the diorite is so strongly altered that only epidote and magnetite can be seen. Secondary chlorite and calcite are also quite prevalent throughout the complex. The propylitic alteration (epidote, chlorite +/- pyrite) identified in the volcanics and diorite points to the property being in a porphyry style system.

In the main trench from 1969, which appears to be strongly sheared, the limestone is completely altered to thin bands of calc-silicate rock showing a strong skarn assemblage of garnet, epidote, calcite and chlorite with magnetite/hematite, pyrite and disseminated chalcopyrite/malachite. Interbedded with this is completely altered volcanics with a strong pyrite and magnetite/hematite content that is very strongly oxidized.

STRUCTURAL GEOLOGY

The general trend of the Spences Bridge Group on the property appears to be north-south and was noted at one outcrop to dip to the west at 50^0, but it is not known if this is constant overall. The interbedded volcanics and limestone were noted to generally strike between 100 and 150^0 and dip 70^0 to the southeast to near vertical. The exception to this is found at the main trench where the dip appears vertical but the strike is north-south (this may be due to the shearing).

MINERALIZATION AND GEOCHEMISTRY

In 1969, Antal states he took samples for 270 feet across the main trench. Results varied from 37 feet of 0.05% to 35 feet of 0.73% copper, this trench although not resampled was examined and the strongest mineralization appears to be disseminated chalcopyrite and malachite in calc-silicate rock, although malachite staining was noted in the altered volcanics and diorite.

During expansion of the 1993 grid, 3 grab samples and 21 chip samples from outcrops were taken. They were assayed for 30 elements by ICP at Eco-Tech Laboratories Ltd. in Kamloops, the results are in Appendix II, and the sample locations are plotted on Map 1. No significant gold and silver values were reported. The highest assays for copper were from 3 continuous 1 m chip samples which averaged 0.57% in a 5 m wide calc-silicate band with finely disseminated chalcopyrite and abundant malachite staining that was exposed in a logging cut 150 m northeast of the main trench.

As described in the September 20, 1993 report a new grid was chained and flagged in across 11.1 line km. From July 20 to 27, 1993 this grid was expanded by 6.9 line km to the southwest. One hundred and fifty eight soil samples were taken at 50 m intervals on lines that were 100 m apart. The expanded grid is shown on Map 2. All samples were taken from the "B" horizon at depths from 10 to 25 cm and then analyzed for a 30 element Inductively Coupled Plasma (ICP) analysis at Eco-Tech Laboratories Ltd. in Kamloops. The techniques are given in Appendix III and the results are listed in Appendix II.

Copper varied from 28 to 1438 ppm and was strongly anomalous across the southwest portion of the grid on lines 46 to 50N. A strong north-south anomalous trend through the middle of the grid from line 49N to line 60N (1100 m) was outlined in the previous report and this continues through the expanded grid from line 45N to 49N. This trend, open to the north and south is in line with the main trench from 1969 and may be partially due to down slope dispersion.

GEOPHYSICS

Two phases of induced polarization/resistivity survey (IP) survey were performed on the Ashton property from July 5 to 7 (4.2 line km) and August 4 to 9, 1993 (5.7 line km). The survey was conducted by Lloyd Geophysics Inc. A total of 9.9 line km of survey were completed. The pole dipole array was used for the survey, with an "a" spacing of 50 m and "n" separations of 1 to 4. The current electrode was to the west of the receiving electrodes on all survey lines (array heading east). The pseudosections are in Appendix VI and plan maps showing chargeability and resistivity are shown on Maps 2 and 3, in pocket.

A Huntec EDA IP-6 receiver and MK2 Model 7500 transmitter were used on the IP survey. Readings were taken in the time domain using a 2 second current pulse.

The chargeability contour plan (10 point triangular filter) on Map 2, shows a circular anomalous zone in the southwest portion of the grid that measures approximately 500 by 500 m (>10.0 msec). This correlates with the zone of high copper values identified in the soil, this zone of chargeability high is open to the north between 100 and 200W on line 5000N.

The resistivity contour plan (10 point triangular filter) on Map 3, shows a zone of high resistivity that trends in a north northwest direction. This higher resistivity may be the result of silicification of the underlying rocks and associated with alteration. The center of the high resistivity correlates with the chargeability high.

CONCLUSIONS

Field work in 1993 together with data from previous owners and government mapping indicates that the Ashton property not only covers an area with known skarn alteration/mineralization, but also has excellent potential for porphyry style mineralization.

The association between the Mount Lytton and Guichon Batholiths and the presence of porphyry style propylitic alteration, along with the coincidental zone of anomalous copper identified in soils and the circular chargeability high, makes it highly probable that copper-rich intrusive phases similar to those in the Guichon Batholith have also formed in intrusions in the Mount Lytton Complex. This gives the Ashton property excellent potential to host a large tonnage low grade porphyry copper orebody similar to those in the Highland Valley area of the Guichon Batholith.

RECOMMENDATIONS

Recommendations for the Ashton property are listed below:

1. Detail mapping of the expanded grid.

2. Drill testing of the coincidental copper in soil and IP anomalies.

Dated at Vancouver, British Columbia,
this 9 day of November 1993.

Scott W. Smith, P. Geol.

APPENDIX I

EXPENDITURES FROM GEOCHEMICAL SAMPLING AND IP SURVEY ON ASHTON PROPERTY

Between July 5 and August 9, 1993

Planning, trip preparation:		
	S.W. Smith (geologist) 1 day @ $400/day	$ 400.00
Salaries:	S.W. Smith (geologist) 3 days @ $400/day	1,200.00
	B. Forseille (technician) 6 days @ $300/day	1,800.00
Transportation:		
	Truck Rental	400.00
	Gas	169.14
	Highway toll	20.00
Meals and Accomadation:		
	Motel	303.60
	Restaurant	108.22
	Groceries	88.75
Field Supplies:		246.47
Assays:		
	185 soils (30 element ICP)	1,014.36
	24 rock (30 element ICP)	310.30
IP survey (9.9 line km)		16,301.16
Report Writing:		
	S.W. Smith (geologist) 4 days @ $400/day	1,600.00
	Drafting and reproduction	412.52
	TOTAL	**$ 24,374.52**

APPENDIX II

ASSAY/GEOCHEMICAL RESULTS

ECO-TECH LABORATORIES LTD.
10041 EAST TRANS CANADA HWY.
KAMLOOPS, B.C. V2C 2J3
PHONE - 604-573-5700
FAX - 604-573-4557

AUGUST 9, 1993

WESTORE ENGINEERING ETK 93-224
703-1112 W. PENDER
VANCOUVER, B.C.
V6E 2S1

ATTENTION: SCOTT SMITH

L45N - 51N

VALUES IN PPM UNLESS OTHERWISE REPORTED

158 SOIL SAMPLES RECEIVED JULY 28, 1993
PROJECT #: ASHTON

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1	- 45N 0 + 00	.2	3.03	40	34	15	<5	3.54	1	18	4	69	3.85	.06	<10	.91	1119	<1	.01	5	510	2	<5	<20	94	.13	10	63	<10	12	145
2	- 45N 0 + 50E	.2	3.38	35	10	15	<5	3.68	1	16	8	102	4.32	.12	<10	.70	1220	2	.01	11	440	26	5	<20	108	.14	<10	73	<10	12	242
3	- 45N 1 + 00E	<.2	3.88	40	6	55	<5	2.34	1	21	13	99	3.86	.09	<10	.67	861	<1	.01	13	800	18	<5	<20	83	.12	<10	73	<10	9	219
4	- 45N 1 + 50E	.2	3.02	25	6	50	<5	1.89	2	16	13	66	3.28	.05	<10	.61	798	<1	.01	21	300	28	5	<20	62	.12	10	71	<10	10	157
5	- 45N 2 + 00E	<.2	3.58	25	4	50	<5	1.37	1	23	55	286	4.27	.05	<10	.94	466	<1	.01	27	110	4	<5	<20	69	.15	<10	153	<10	11	90
6	- 45N 2 + 50E	<.2	2.22	20	4	45	<5	.92	<1	15	10	50	2.22	.06	<10	.42	570	<1	.02	12	530	4	<5	<20	45	.09	<10	62	<10	5	171
7	- 45N 3 + 00E	<.2	4.25	35	6	70	<5	1.34	1	29	20	292	4.54	.10	<10	.99	487	<1	.02	27	440	4	<5	<20	72	.17	<10	170	<10	9	127
8	- 45N 3 + 50E	<.2	4.21	35	6	35	<5	1.67	1	41	9	541	6.20	.08	<10	1.24	535	<1	.02	20	210	6	<5	<20	104	.22	<10	288	<10	10	103
9	- 45N 4 + 00E	<.2	3.06	50	4	20	<5	2.69	<1	32	8	416	5.20	.06	<10	1.00	766	<1	.01	14	440	2	<5	<20	120	.17	<10	208	<10	11	120
10	- 45N 4 + 50E	<.2	2.68	20	14	5	<5	2.18	1	9	9	23	2.15	.07	<10	.89	376	<1	<.01	3	410	<2	<5	<20	116	.08	<10	71	<10	7	56
11	- 45N 5 + 00E	<.2	2.20	30	8	25	<5	1.75	<1	15	6	273	3.62	.05	<10	1.31	733	<1	.01	5	990	<2	<5	<20	72	.09	<10	102	<10	10	77
12	- 45N 0 + 50W	<.2	2.49	40	52	15	<5	3.05	<1	17	4	79	3.56	.05	<10	.91	1046	<1	.01	5	750	<2	<5	<20	67	.15	<10	64	<10	12	130
13	- 45N 1 + 00W	<.2	2.43	90	24	30	<5	1.76	<1	23	8	189	3.14	.07	<10	.66	755	<1	.01	10	1070	2	<5	<20	70	.10	<10	66	<10	9	82
14	- 45N 1 + 50W	<.2	3.16	50	24	25	<5	2.20	1	16	6	122	3.22	.12	<10	.77	707	<1	.01	5	1240	2	<5	<20	79	.12	<10	63	<10	11	65
15	- 45N 2 + 00W	<.2	1.90	30	10	25	<5	2.16	<1	9	4	36	2.83	.05	<10	.43	689	<1	.01	3	320	<2	<5	<20	45	.09	<10	40	<10	8	68
16	- 45N 2 + 50W	<.2	2.21	55	24	40	<5	2.98	1	14	12	64	3.21	.17	<10	.88	1308	<1	.01	12	2160	16	5	<20	63	.06	<10	49	<10	14	440
17	- 45N 3 + 00W	<.2	2.29	100	8	35	<5	1.38	<1	14	9	60	3.08	.09	<10	.63	695	<1	.01	10	1050	12	<5	<20	29	.07	<10	69	<10	15	124
18	- 45N 3 + 50W	<.2	4.07	60	8	45	<5	1.80	<1	22	11	224	6.21	.26	<10	1.17	941	<1	.01	10	350	4	<5	<20	57	.05	<10	165	<10	26	192
19	- 45N 4 + 00W	<.2	2.95	230	8	90	<5	1.42	<1	18	11	91	5.02	.33	<10	.86	709	<1	.01	13	720	12	<5	<20	53	.04	<10	91	<10	21	144
20	- 45N 4 + 50W	<.2	3.38	35	8	75	<5	1.37	<1	23	34	93	4.62	.53	<10	1.59	729	<1	.04	47	770	10	<5	<20	76	.16	<10	96	<10	14	124
21	- 45N 5 + 00W	<.2	2.59	40	4	90	<5	.89	<1	15	26	55	4.15	.25	<10	.97	409	<1	.02	25	340	4	<5	<20	109	.06	<10	116	<10	11	94
22	- 45N 5 + 50W	<.2	2.75	20	4	65	<5	1.11	<1	20	28	164	4.76	.25	<10	1.00	451	<1	.03	22	550	2	<5	<20	92	.11	<10	166	<10	11	72
23	- 45N 6 + 00W	<.2	3.59	5	2	50	<5	1.08	<1	15	28	61	3.16	.09	<10	1.06	417	<1	.06	12	270	2	<5	<20	76	.04	<10	96	<10	3	38
24	- 45N 6 + 50W	<.2	2.84	10	4	55	<5	1.18	<1	20	33	81	4.18	.21	<10	1.21	470	<1	.04	22	630	2	<5	<20	105	.12	<10	130	<10	9	56
25	- 45N 7 + 00W	<.2	2.58	5	4	65	<5	.93	<1	20	35	103	3.86	.22	<10	.98	639	<1	.04	21	300	2	<5	<20	93	.14	10	117	<10	11	53

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
26 -	46N 0 + 00	<.2	3.25	30	4	35	<5	1.55	<1	29	10	251	4.16	.07	<10	.75	468	<1	.01	12	190	6	<5	<20	82	.11	<10	160	<10	7	79
27 -	46N 0 + 50E	<.2	4.32	30	6	55	<5	2.17	1	25	15	222	4.18	.10	<10	.75	731	<1	.01	14	250	12	<5	<20	108	.15	<10	128	<10	10	144
28 -	46N 1 + 00E	<.2	3.73	15	4	60	<5	1.52	<1	28	21	329	5.09	.12	<10	.89	650	<1	.02	23	180	8	<5	<20	73	.17	<10	200	<10	11	110
29 -	46N 1 + 50E	<.2	3.53	40	2	60	<5	1.37	<1	28	21	308	4.90	.13	<10	.89	555	<1	.01	20	180	16	<5	<20	68	.15	<10	181	<10	8	112
30 -	46N 2 + 00E	<.2	3.74	25	6	55	<5	1.60	1	61	15	1151	7.23	.15	<10	1.55	706	<1	.02	30	390	4	<5	<20	62	.09	<10	289	<10	11	90
31 -	46N 2 + 50E	<.2	3.36	20	4	80	<5	1.35	<1	28	31	336	5.41	.10	<10	1.09	581	<1	.02	25	200	10	<5	<20	75	.16	<10	222	<10	14	86
32 -	46N 3 + 00E	<.2	2.56	15	4	60	<5	1.12	<1	16	23	91	3.64	.21	<10	.59	655	<1	.01	18	380	6	<5	<20	59	.14	<10	119	<10	8	121
33 -	46N 3 + 50E	<.2	3.26	30	8	55	<5	1.58	<1	38	16	768	6.63	.16	<10	1.28	704	<1	.02	18	270	2	<5	<20	63	.12	<10	305	<10	9	86
34 -	46N 4 + 00E	<.2	2.49	45	4	20	<5	2.71	<1	14	10	103	4.06	.08	<10	.62	983	<1	<.01	10	370	6	<5	<20	67	.10	<10	61	<10	11	123
35 -	46N 4 + 50E	<.2	2.84	245	8	45	<5	1.43	<1	51	14	418	6.66	.14	<10	.94	703	<1	.01	34	680	6	5	<20	42	.09	<10	143	<10	11	168
36 -	46N 5 + 00E	<.2	1.54	25	4	170	<5	.74	<1	10	5	26	2.37	.05	<10	.35	455	<1	.01	6	490	4	<5	<20	26	.05	<10	36	<10	22	62
37 -	46N 0 + 50W	<.2	3.66	15	2	5	<5	2.50	1	14	<1	319	1.85	.11	<10	.41	150	<1	.03	4	190	2	<5	<20	78	.02	<10	87	<10	1	20
38 -	46N 1 + 00W	<.2	4.20	10	2	10	<5	3.00	1	16	<1	45	1.50	.12	<10	.36	137	<1	.03	<1	240	4	<5	<20	104	.02	<10	53	<10	2	15
39 -	46N 1 + 50W	.2	4.38	25	8	25	<5	2.03	3	58	12	279	6.89	.10	<10	1.64	399	<1	.03	19	360	16	5	<20	115	.19	<10	357	<10	6	91
40 -	46N 2 + 00W	<.2	2.12	60	20	140	25	.86	<1	48	28	263	3.91	.17	<10	.80	371	11	.02	<1	580	42	<5	<20	20	.12	<10	211	90	<1	58
41 -	46N 2 + 50W	<.2	2.66	55	16	35	<5	1.30	<1	22	10	113	3.10	.07	<10	.77	463	<1	.02	12	470	8	<5	<20	52	.15	<10	83	<10	9	97
42 -	46N 3 + 00W	<.2	2.06	35	20	60	<5	1.49	<1	15	9	78	2.57	.16	<10	.73	721	<1	.01	7	1550	6	<5	<20	81	.11	<10	61	<10	9	80
43 -	46N 3 + 50W	.4	2.30	45	12	35	<5	1.45	1	16	12	92	2.93	.08	<10	.67	633	<1	.02	10	1240	16	<5	<20	56	.11	<10	62	<10	8	323
44 -	46N 4 + 00W	<.2	1.93	70	30	105	<5	4.19	5	10	13	62	2.40	.14	<10	.55	1572	<1	.01	11	3910	12	<5	<20	101	.04	<10	35	<10	11	484
45 -	46N 4 + 50W	<.2	3.19	20	4	185	<5	1.48	<1	9	7	28	2.75	.33	10	.45	579	<1	.02	5	300	14	<5	<20	464	.05	<10	55	<10	12	75
46 -	46N 5 + 00W	<.2	3.02	5	8	240	<5	1.46	<1	11	14	56	3.19	.53	<10	.59	445	<1	.01	11	440	12	<5	<20	509	.06	<10	69	<10	12	93
47 -	46N 5 + 50W	<.2	2.82	15	4	85	<5	1.47	<1	18	31	74	3.81	.14	<10	1.31	536	<1	.04	24	650	8	<5	<20	136	.08	<10	112	<10	13	77
48 -	46N 6 + 00W	<.2	2.09	5	4	75	<5	1.95	<1	19	42	61	4.02	.09	<10	1.26	538	<1	.07	28	730	4	<5	<20	129	.15	<10	157	<10	12	52
49 -	46N 6 + 50W	<.2	2.87	10	6	75	<5	1.20	<1	23	39	98	4.74	.31	<10	1.24	600	<1	.04	29	670	8	<5	<20	105	.17	<10	160	<10	13	74
50 -	46N 7 + 00W	<.2	2.72	10	4	80	<5	.69	<1	17	38	45	4.51	.32	<10	1.26	615	<1	.02	18	580	8	<5	<20	76	.14	<10	116	<10	11	69

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
51	- 47N 0 + 00	<.2	5.05	30	6	80	<5	2.23	2	32	18	334	4.20	.16	<10	.85	784	<1	.02	24	820	20	<5	<20	104	.17	<10	140	<10	11	152
52	- 47N 0 + 50E	<.2	4.48	30	6	60	<5	1.64	1	30	18	376	5.05	.11	<10	.90	674	<1	.02	21	140	24	<5	<20	73	.18	<10	204	<10	11	131
53	- 47N 1 + 00E	<.2	4.31	260	8	70	<5	1.60	<1	35	15	601	5.94	.21	<10	1.36	718	<1	.02	30	290	12	5	<20	65	.15	<10	241	<10	10	132
54	- 47N 1 + 50E	<.2	4.39	40	6	70	<5	1.61	1	39	19	671	7.01	.16	<10	1.35	754	<1	.03	25	180	12	<5	<20	81	.18	<10	335	<10	13	103
55	- 47N 2 + 00E	<.2	3.55	30	4	60	<5	1.41	<1	38	31	434	6.38	.11	<10	1.05	477	<1	.02	28	120	12	<5	<20	74	.20	<10	324	<10	10	81
56	- 47N 2 + 50E	<.2	3.88	20	32	285	15	1.42	<1	50	54	374	5.68	.33	<10	1.02	724	19	.03	26	440	84	<5	<20	77	.19	<10	317	190	7	94
57	- 47N 3 + 00E	<.2	5.49	25	8	60	<5	1.84	1	55	21	1006	6.82	.25	<10	1.46	618	<1	.03	31	260	14	<5	<20	152	.19	<10	343	<10	7	90
58	- 47N 3 + 50E	<.2	4.87	20	6	60	<5	1.70	1	51	29	583	7.52	.16	<10	1.85	612	<1	.07	27	180	8	<5	<20	123	.19	<10	385	<10	8	71
59	- 47N 4 + 00E	<.2	3.49	30	6	45	<5	2.02	<1	32	12	336	6.31	.08	<10	.94	559	<1	.02	18	230	10	<5	<20	98	.23	<10	345	<10	9	90
60	- 47N 4 + 50E	<.2	3.09	25	6	45	<5	1.03	1	22	10	130	4.06	.06	<10	.86	432	<1	.03	13	140	10	<5	<20	46	.15	<10	169	<10	8	150
61	- 47N 5 + 00E	<.2	3.85	40	6	40	<5	1.93	1	35	1	151	4.77	.12	<10	1.08	432	<1	.01	3	300	10	<5	<20	105	.11	<10	214	<10	7	70
62	- 47N 0 + 50W	<.2	4.65	30	6	55	<5	1.97	2	36	18	308	4.42	.13	<10	.88	844	<1	.02	22	720	20	<5	<20	88	.17	<10	216	<10	9	146
63	- 47N 1 + 00W	<.2	4.33	20	4	25	<5	2.23	1	37	7	765	3.41	.17	<10	.80	442	<1	.01	13	540	16	<5	<20	112	.08	<10	157	<10	4	77
64	- 47N 1 + 50W	<.2	4.83	30	6	45	<5	1.96	1	56	14	1151	6.83	.14	<10	1.37	656	<1	.02	24	390	24	<5	<20	126	.27	<10	399	<10	11	110
65	- 47N 2 + 00W	<.2	5.09	40	8	45	<5	2.14	1	55	23	520	7.48	.12	<10	1.67	630	<1	.03	26	500	20	<5	<20	124	.29	<10	386	<10	14	115
66	- 47N 2 + 50W	<.2	4.69	45	10	60	<5	1.82	<1	58	32	354	7.07	.09	<10	1.49	654	<1	.04	21	490	16	<5	<20	108	.23	<10	305	<10	12	120
67	- 47N 3 + 00W	<.2	4.76	35	8	45	<5	2.27	1	44	32	561	7.46	.13	<10	1.46	510	<1	.03	21	300	22	<5	<20	142	.29	<10	404	<10	16	105
68	- 47N 3 + 50W	<.2	3.91	35	6	50	<5	1.72	<1	46	26	491	6.52	.13	<10	1.18	676	<1	.03	20	380	22	<5	<20	98	.22	<10	327	<10	11	126
69	- 47N 4 + 00W	<.2	4.23	30	8	50	<5	1.64	<1	41	29	450	7.19	.08	<10	1.26	483	<1	.02	20	240	26	<5	<20	115	.26	<10	390	<10	12	118
70	- 47N 4 + 50W	<.2	2.24	30	20	140	<5	2.59	2	26	12	263	2.48	.17	<10	.46	2206	<1	.02	9	5050	10	<5	<20	142	.05	<10	66	<10	7	288
71	- 47N 5 + 00W	<.2	3.70	30	14	35	<5	2.28	1	20	12	107	4.27	.16	<10	1.06	539	<1	.01	7	290	14	<5	<20	99	.13	<10	101	<10	13	104
72	- 47N 5 + 50W	<.2	3.36	5	6	95	<5	1.36	<1	24	46	103	4.71	.20	<10	1.35	692	<1	.06	33	280	10	<5	<20	120	.17	<10	140	<10	17	75
73	- 47N 6 + 50W	<.2	3.06	5	14	90	<5	1.00	<1	20	44	52	4.72	.24	<10	1.07	521	<1	.05	22	470	10	<5	<20	92	.15	<10	153	<10	9	68
74	- 47N 7 + 00W	<.2	2.32	5	6	90	<5	.81	<1	14	28	33	3.17	.33	<10	.60	769	<1	.03	17	500	10	<5	<20	62	.13	<10	76	<10	8	92
75	- 48N 0 + 00	<.2	3.85	10	4	130	<5	1.41	<1	28	48	146	5.56	.16	<10	1.63	578	<1	.06	42	430	12	<5	<20	154	.18	<10	198	<10	22	67

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
76	48N 0 + 50E	<.2	4.39	20	6	75	<5	1.58	1	36	34	348	6.95	.35	<10	1.52	774	<1	.05	27	410	10	<5	<20	100	.18	<10	332	<10	13	91
77	48N 1 + 00E	.6	3.57	25	6	55	<5	1.75	2	33	24	336	5.98	.17	<10	1.85	767	<1	.06	37	420	8	5	<20	126	.14	10	280	<10	12	76
78	48N 1 + 50E	<.2	3.57	20	4	75	<5	1.28	1	29	17	448	5.49	.23	<10	1.07	663	<1	.02	21	110	8	<5	<20	61	.15	<10	255	<10	10	99
79	48N 2 + 00E	<.2	3.82	20	4	75	<5	1.31	1	31	34	437	7.31	.13	<10	1.38	387	<1	.06	24	160	4	<5	<20	126	.18	<10	437	<10	13	54
80	48N 2 + 50E	.2	3.64	15	6	50	<5	1.22	3	24	32	133	5.67	.14	<10	.84	718	<1	.03	32	110	<2	<5	<20	80	.18	50	252	<10	12	97
81	48N 3 + 00E	<.2	3.83	15	4	45	<5	1.41	<1	53	1	1438	11.65	.10	<10	3.47	646	<1	.05	31	220	<2	<5	<20	80	.29	20	896	<10	14	74
82	48N 3 + 50E	<.2	3.43	25	10	60	<5	1.24	1	25	11	377	5.18	.43	<10	.93	626	<1	.03	20	460	6	<5	<20	70	.10	<10	218	<10	6	127
83	48N 4 + 00E	<.2	3.13	30	8	55	<5	1.12	1	39	11	395	5.54	.20	<10	1.09	519	<1	.02	24	360	6	<5	<20	63	.15	<10	231	<10	6	154
84	48N 4 + 50E	<.2	3.77	35	6	55	<5	1.08	1	54	8	1534	5.87	.12	<10	1.70	544	<1	.02	28	360	4	<5	<20	74	.20	<10	339	<10	6	134
85	48N 5 + 00E	<.2	3.58	100	8	45	<5	1.85	1	41	10	591	7.04	.10	<10	1.86	781	<1	.01	23	490	4	5	<20	87	.20	<10	351	<10	17	96
86	48N 0 + 50W	<.2	5.01	35	6	85	<5	1.70	2	36	21	434	4.98	.20	<10	1.07	613	<1	.02	25	520	12	<5	<20	96	.19	<10	201	<10	12	125
87	48N 1 + 00W	<.2	4.74	30	4	80	<5	1.88	2	34	16	314	3.89	.15	<10	.88	672	<1	.02	20	450	18	<5	<20	96	.16	<10	147	<10	12	146
88	48N 1 + 50W	<.2	4.11	30	4	50	<5	1.41	1	39	18	257	4.47	.15	<10	1.07	476	<1	.02	17	470	10	<5	<20	79	.12	<10	208	<10	6	93
89	48N 2 + 00W	<.2	3.52	30	4	35	<5	1.39	1	32	6	128	3.56	.16	<10	.75	331	<1	.01	8	310	6	<5	<20	85	.09	<10	132	<10	7	55
90	48N 2 + 50W	<.2	4.53	40	8	30	<5	1.79	3	54	9	410	5.73	.16	<10	1.20	759	<1	.03	24	750	2	<5	<20	145	.22	20	262	10	11	126
91	48N 3 + 00W	<.2	3.63	25	8	40	<5	1.82	1	32	11	224	5.23	.13	<10	.96	425	<1	.02	12	460	6	<5	<20	119	.24	<10	265	<10	12	68
92	48N 3 + 50W	<.2	3.72	35	6	50	<5	1.65	2	68	3	235	6.60	.16	<10	1.24	559	<1	.02	9	470	2	<5	<20	142	.31	<10	403	<10	15	155
93	48N 4 + 00W	<.2	3.53	30	8	45	<5	1.85	1	59	3	193	5.32	.29	<10	1.06	646	<1	.02	8	750	2	<5	<20	144	.21	<10	305	<10	10	140
94	48N 4 + 50W	<.2	2.46	35	8	70	<5	1.44	1	28	14	131	2.95	.14	<10	.67	1069	<1	.02	15	2010	8	<5	<20	83	.11	<10	107	<10	7	209
95	48N 5 + 00W	<.2	3.67	30	24	65	<5	2.09	2	23	15	105	3.77	.33	<10	1.27	853	<1	.01	10	2290	6	5	<20	115	.12	<10	94	<10	12	207
96	48N 5 + 50W	<.2	2.41	15	8	90	<5	1.25	1	23	38	77	3.99	.36	<10	1.47	623	<1	.05	32	990	6	<5	<20	114	.15	<10	118	<10	15	75
97	48N 6 + 00W	<.2	2.54	10	6	85	<5	1.00	<1	20	38	76	3.91	.33	<10	1.37	534	<1	.04	28	500	4	5	<20	91	.14	<10	108	<10	12	62
98	48N 6 + 50W	<.2	2.81	10	6	90	<5	.96	1	23	41	78	4.40	.43	<10	1.51	758	<1	.03	27	550	4	<5	<20	84	.15	<10	114	<10	13	67
99	48N 7 + 00W	<.2	3.31	10	6	95	<5	.93	1	22	46	84	4.53	.42	<10	1.41	542	<1	.03	30	630	4	<5	<20	103	.16	<10	122	<10	16	62
100	49N 0 + 50W	<.2	4.10	20	6	90	<5	1.43	1	34	27	664	5.48	.20	<10	1.53	528	<1	.04	31	310	2	<5	<20	107	.17	<10	241	<10	11	73

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
101-	49N 1 + 00W	<.2	3.53	10	4	130	<5	1.09	1	25	45	108	4.48	.22	<10	1.42	535	<1	.05	41	600	4	<5	<20	146	.19	<10	125	<10	20	69
102-	49N 1 + 50W	<.2	3.33	10	4	90	<5	.95	1	22	27	84	3.84	.33	<10	.87	574	<1	.02	27	480	12	<5	<20	74	.15	<10	116	<10	10	114
103-	49N 2 + 00W	<.2	4.84	25	8	80	<5	1.58	2	35	21	291	4.54	.21	<10	1.11	624	<1	.02	23	520	12	<5	<20	96	.19	<10	172	<10	11	129
104-	49N 2 + 50W	<.2	2.45	20	2	40	<5	1.27	<1	17	12	283	2.93	.10	<10	.73	203	<1	.01	14	240	2	<5	<20	74	.06	10	120	<10	4	36
105-	49N 3 + 00W	<.2	2.92	20	6	60	<5	1.78	1	31	32	243	5.98	.15	<10	1.10	507	<1	.04	23	510	2	<5	<20	112	.22	<10	367	<10	12	61
106-	49N 3 + 50W	<.2	4.63	30	6	70	<5	1.56	1	41	21	249	5.50	.20	<10	1.17	438	<1	.03	20	430	4	5	<20	112	.21	<10	266	<10	10	77
107-	49N 4 + 00W	<.2	3.25	25	4	35	<5	1.45	1	40	6	123	4.19	.15	<10	.90	417	<1	.02	7	300	4	<5	<20	77	.11	<10	215	<10	4	60
108-	49N 4 + 50W	<.2	4.10	30	8	45	<5	2.04	1	47	8	326	5.49	.16	<10	1.19	481	<1	.02	28	420	4	<5	<20	128	.19	<10	279	<10	9	95
109-	49N 5 + 00W	<.2	3.24	30	12	60	<5	1.93	1	42	13	322	4.51	.17	<10	1.06	694	<1	.02	21	2230	2	<5	<20	141	.12	<10	199	<10	6	128
110-	49N 5 + 50W	<.2	2.53	20	8	70	<5	1.82	1	21	26	90	3.48	.40	<10	1.21	670	<1	.04	22	740	4	<5	<20	125	.12	<10	109	<10	10	100
111-	49N 6 + 00W	<.2	2.15	5	4	100	<5	.80	<1	19	33	50	3.34	.47	<10	.88	892	<1	.03	22	580	4	<5	<20	83	.14	<10	86	<10	11	83
112-	49N 6 + 50W	<.2	2.50	10	6	95	<5	.73	1	20	38	50	3.70	.47	<10	1.13	761	<1	.03	27	390	6	<5	<20	78	.15	<10	93	<10	13	78
113-	49N 7 + 00W	<.2	2.44	10	4	100	<5	.66	<1	17	34	36	3.31	.33	<10	.87	635	<1	.03	20	310	4	<5	<20	62	.15	<10	84	<10	10	84
114-	50N 0 + 00E	<.2	4.30	15	4	70	<5	1.26	1	33	39	176	5.64	.20	<10	1.66	508	<1	.06	20	150	2	5	<20	83	.09	<10	238	<10	11	54
115-	50N 0 + 50W	1.2	4.59	15	6	80	<5	1.29	2	37	55	370	6.30	.32	<10	1.66	841	<1	.04	38	170	2	<5	<20	80	.08	20	324	<10	14	87
116-	50N 1 + 00W	<.2	3.78	50	6	40	<5	2.25	1	33	20	716	7.06	.29	<10	1.43	699	<1	.02	23	550	<2	<5	<20	114	.18	10	343	<10	12	97
117-	50N 1 + 50W	<.2	4.73	25	6	105	<5	1.52	2	33	37	407	6.38	.23	<10	1.33	570	<1	.04	36	380	2	<5	<20	130	.22	10	270	<10	16	91
118-	50N 2 + 00W	<.2	3.62	20	6	85	<5	1.45	2	27	35	339	5.87	.25	<10	.98	568	<1	.03	31	1010	<2	<5	<20	128	.18	20	327	<10	11	91
119-	50N 2 + 50W	<.2	3.60	10	6	120	<5	1.30	1	26	60	173	5.47	.27	<10	1.47	614	<1	.04	44	580	2	<5	<20	140	.20	20	205	<10	20	68
120-	50N 3 + 00W	<.2	3.01	10	4	115	<5	1.05	1	21	47	63	4.13	.27	<10	.98	574	<1	.05	32	290	2	<5	<20	128	.22	10	119	<10	20	74
121-	50N 3 + 50W	<.2	3.53	15	6	110	<5	1.25	1	25	51	104	4.70	.52	<10	1.27	751	<1	.04	42	440	<2	<5	<20	151	.22	10	124	<10	21	75
122-	50N 4 + 00W	<.2	3.17	5	8	100	<5	1.16	1	26	41	145	4.81	.70	<10	1.00	833	<1	.04	31	520	<2	<5	<20	115	.23	10	170	<10	17	87
123-	50N 4 + 50W	<.2	3.45	10	6	95	<5	1.13	1	26	42	178	5.42	.47	<10	1.02	737	<1	.04	29	340	2	<5	<20	110	.23	10	213	<10	16	99
124-	50N 5 + 00W	<.2	3.29	15	6	60	<5	1.82	<1	31	53	184	5.82	.25	<10	1.39	646	<1	.09	33	610	<2	<5	<20	195	.24	10	279	<10	15	69
125-	50N 5 + 50W	<.2	3.12	10	14	155	<5	1.96	1	36	62	158	4.93	.35	<10	1.67	623	3	.13	41	900	36	<5	<20	236	.24	<10	217	80	18	63

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
126-	50N 6 + 00W	<.2	3.01	15	8	65	<5	2.85	1	31	42	136	5.23	.23	<10	2.08	686	<1	.09	41	800	<2	<5	<20	197	.19	<10	207	<10	13	62
127-	50N 6 + 50W	<.2	3.62	10	6	110	<5	1.23	1	24	49	97	4.88	.28	<10	1.47	572	<1	.04	42	530	<2	<5	<20	149	.19	10	137	<10	21	68
128-	50N 7 + 00W	<.2	2.80	10	6	95	<5	.78	1	15	34	38	3.46	.43	<10	.81	571	<1	.04	28	390	2	<5	<20	77	.17	10	81	<10	13	106
129-	51N 0 + 50W	<.2	3.70	5	4	140	<5	1.13	1	24	47	73	4.51	.30	<10	1.15	715	<1	.05	40	380	2	<5	<20	131	.22	<10	126	<10	21	90
130-	51N 1 + 00W	<.2	2.89	5	4	105	<5	1.14	1	21	48	73	4.13	.48	<10	.94	787	<1	.05	33	310	2	<5	<20	122	.23	<10	118	<10	18	104
131-	51N 1 + 50W	<.2	3.36	15	6	120	<5	1.16	1	23	56	103	4.83	.38	<10	1.18	600	<1	.04	45	500	<2	<5	<20	146	.22	10	154	<10	21	76
132-	51N 2 + 00W	<.2	4.14	30	10	65	<5	1.86	1	36	28	544	6.99	.45	<10	1.38	589	<1	.04	28	440	<2	<5	<20	109	.19	10	385	<10	11	87
133-	51N 2 + 50W	<.2	3.04	15	6	85	<5	1.07	2	20	36	85	4.21	.40	<10	.82	584	<1	.03	27	420	4	<5	<20	86	.21	<10	156	<10	14	110
134-	51N 3 + 00W	<.2	3.68	10	6	90	<5	1.29	2	23	37	171	4.82	.45	<10	.94	595	<1	.03	31	400	2	<5	<20	108	.21	10	189	<10	16	93
135-	51N 3 + 50W	<.2	3.17	10	4	100	<5	1.34	1	24	49	134	4.89	.25	<10	1.44	662	<1	.06	40	740	<2	<5	<20	153	.22	10	163	<10	17	67
136-	51N 4 + 00W	<.2	3.12	10	6	100	<5	1.16	1	23	47	106	4.79	.24	<10	1.17	628	<1	.05	33	340	<2	<5	<20	122	.21	10	175	<10	18	65
137-	51N 4 + 50W	<.2	3.15	10	6	125	<5	.86	1	22	66	60	4.61	.38	<10	1.68	781	<1	.03	41	430	<2	<5	<20	97	.18	10	113	<10	18	77
138-	51N 5 + 00W	<.2	2.92	20	6	65	<5	1.65	<1	28	33	252	5.53	.22	<10	1.45	656	<1	.05	31	470	<2	<5	<20	148	.20	10	258	<10	15	77
139-	51N 5 + 50W	<.2	2.27	10	4	30	<5	1.47	<1	19	29	133	2.98	.12	<10	1.10	370	<1	.04	26	400	<2	<5	<20	123	.08	30	104	<10	8	45
140-	51N 6 + 00W	<.2	2.20	10	4	40	<5	.90	1	10	14	35	2.63	.48	<10	.54	446	<1	.01	14	1020	<2	<5	<20	69	<.01	20	55	<10	9	76
141-	51N 6 + 50W	<.2	2.72	10	6	75	<5	1.12	1	21	40	68	4.41	.48	<10	1.46	703	<1	.05	33	870	<2	<5	<20	115	.16	20	122	<10	16	69
142-	51N 7 + 00W	<.2	3.04	10	8	115	<5	1.64	1	21	48	58	4.26	.54	<10	1.73	764	<1	.06	42	1070	<2	<5	<20	212	.15	10	101	<10	17	70
143-	57N 0 + 00E	<.2	3.95	20	4	60	<5	1.16	1	22	26	119	5.00	.56	<10	1.02	602	<1	.03	19	550	<2	<5	<20	89	.17	30	189	<10	13	82
144-	57N 0 + 50E	<.2	3.29	10	6	65	<5	.86	1	16	22	54	3.52	.47	<10	.71	508	<1	.03	20	430	<2	<5	<20	77	.17	10	95	<10	12	91
145-	57N 1 + 00E	<.2	2.69	5	4	75	<5	.92	1	16	35	40	3.43	.53	<10	.76	784	<1	.04	28	430	<2	<5	<20	99	.19	20	86	<10	13	94
146-	57N 1 + 50E	<.2	3.11	10	10	85	<5	1.21	1	21	48	62	4.16	.54	<10	1.12	592	<1	.05	35	550	<2	<5	<20	131	.22	20	116	<10	17	68
147-	57N 2 + 00E	<.2	2.81	10	6	80	<5	1.42	1	22	52	77	4.87	.21	<10	1.36	536	<1	.07	39	870	<2	<5	<20	177	.24	30	180	<10	18	64
148-	57N 2 + 50E	<.2	3.17	10	12	100	<5	1.13	1	23	51	79	4.66	.57	<10	1.27	617	<1	.06	43	360	<2	<5	<20	151	.23	20	121	<10	22	79
149-	57N 3 + 00E	<.2	4.21	15	10	65	<5	1.98	1	49	33	342	7.63	.30	<10	2.35	784	<1	.08	31	310	<2	<5	<20	136	.17	30	373	<10	12	79
150-	57N 3 + 50E	<.2	3.16	45	8	45	<5	2.22	1	34	19	522	6.28	.30	<10	1.45	717	<1	.03	26	420	<2	<5	<20	149	.20	20	311	<10	14	113

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
151-	57N 4 + 00E	<.2	3.53	45	12	35	<5	2.30	2	39	11	632	6.75	.32	<10	1.58	965	<1	.02	24	300	<2	<5	<20	151	.23	30	331	<10	14	168
152-	57N 4 + 50E	<.2	3.25	40	14	40	<5	1.89	1	27	31	457	5.65	.48	<10	1.40	546	<1	.03	36	410	<2	<5	<20	162	.21	30	235	<10	20	100
153-	57N 5 + 00E	<.2	2.15	10	24	75	<5	5.43	1	21	22	215	3.46	.37	<10	1.08	762	<1	.02	37	1770	<2	<5	<20	203	.06	10	113	<10	10	99
154-	57N 5 + 50E	<.2	2.82	5	6	35	<5	1.73	1	22	21	171	3.89	.19	<10	1.33	400	<1	.04	25	440	<2	<5	<20	138	.12	30	163	<10	7	47
155-	57N 6 + 00E	<.2	2.76	5	12	50	<5	1.42	1	27	47	44	4.90	.54	<10	1.62	625	<1	.07	61	850	<2	<5	<20	159	.31	10	96	<10	25	82
156-	57N 6 + 50E	<.2	2.92	5	6	70	<5	1.11	1	25	55	45	4.69	.40	<10	1.71	628	<1	.08	61	510	<2	<5	<20	180	.27	20	98	<10	22	68
157-	57N 7 + 00E	<.2	3.52	10	4	60	<5	1.18	1	29	58	52	5.31	.30	<10	2.41	584	<1	.10	85	380	<2	<5	<20	165	.28	20	103	<10	24	65
158-	47N 6 + 00W	<.2	3.22	5	4	90	<5	1.17	1	25	45	102	5.41	.20	<10	1.80	698	<1	.05	34	620	<2	<5	<20	133	.15	10	144	<10	13	68

QC/DATA:

Repeat #:

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1-	45N 0+00	.2	3.00	40	36	20	<5	3.37	2	19	4	73	3.78	.06	<10	.90	1080	<1	.01	6	520	2	5	<20	92	.12	10	63	<10	11	147
39-	46N 1+50W	<.2	4.24	25	6	25	<5	1.92	1	55	11	260	6.23	.10	<10	1.44	383	<1	.03	7	340	14	<5	<20	98	.14	10	289	<10	6	82
77-	48N 0+50E	<.2	3.24	30	4	60	<5	1.55	<1	31	22	319	5.36	.17	<10	1.68	704	<1	.06	29	410	6	<5	<20	120	.13	10	254	<10	11	70
115-	50N 0+50W	<.2	4.81	45	4	80	<5	1.34	2	38	57	388	6.62	.38	<10	1.73	6865	<1	.04	36	160	2	<5	<20	78	.09	10	339	<10	15	87
153-	57N 5+00E	<.2	2.29	15	24	80	<5	5.37	1	22	25	216	3.87	.39	<10	1.13	790	<1	.02	39	1770	<2	5	<20	204	.07	20	135	<10	10	101
STANDARD 1991:		1.2	1.96	65	4	115	<5	1.79	<1	21	67	83	3.92	.42	<10	.96	720	<1	.02	24	650	18	5	<20	61	.12	20	83	<10	9	73
STANDARD 1991:		1.0	1.61	65	4	110	<5	1.40	<1	19	57	79	3.34	.41	<10	.95	615	<1	.02	21	630	20	5	<20	59	.11	<10	72	<10	8	63

NOTE: < = LESS THAN
> = GREATER THAN

ECO-TECH LABORATORIES LTD.
FRANK J. PEZZOTTI, A.Sc.T.
B.C. Certified Assayer

SC93/KAMISC

Chip samples

ECO-TECH LABORATORIES LTD.
10041 EAST TRANS CANADA HWY.
KAMLOOPS, B.C. V2C 2J3
PHONE - 604-573-5700
FAX - 604-573-4557

WESTORE ENGINEERING ETK 93-234
703-1112 W. PENDER STREET
VANCOUVER, B.C.
V6E 2S1

ATTENTION: SCOTT SMITH

AUGUST 10, 1993

VALUES IN PPM UNLESS OTHERWISE REPORTED

16 ROCK SAMPLES RECEIVED JULY 28, 1993

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1 -	R/C 2- 1	<.2	4.68	10	6	45	5	4.81	<1	28	65	33	6.11	.03	<10	1.80	964	1	.18	26	610	<2	10	<20	154	.06	<10	227	<10	7	55
2 -	R/C 2- 2	<.2	4.90	20	8	50	<5	4.89	<1	34	61	42	7.11	.03	<10	2.00	940	1	.19	27	490	<2	10	<20	175	.11	<10	273	<10	7	61
3 -	R/C 2- 3	<.2	5.86	10	6	60	<5	5.27	<1	30	75	2292	6.67	.02	<10	.88	651	1	.50	29	190	<2	10	<20	224	.05	<10	277	<10	1	55
4 -	R/C 2- 4	<.2	5.49	10	6	70	<5	5.64	<1	36	56	1374	8.26	.02	<10	1.06	860	<1	.38	29	130	<2	<5	<20	178	<.01	<10	312	<10	<1	71
5 -	R/C 2- 5	<.2	3.78	10	6	45	<5	5.68	<1	33	47	122	7.87	.01	<10	1.00	988	<1	.22	28	220	<2	5	<20	119	<.01	<10	303	<10	1	63
6 -	R/C 2- 6	<.2	2.27	20	8	30	<5	9.20	<1	27	26	54	5.90	.02	<10	.97	1195	<1	.02	18	350	<2	5	<20	89	<.01	<10	238	<10	4	63
7 -	R/C 2- 7	<.2	3.33	10	10	80	<5	2.31	<1	122	10	315	>15	<.01	<10	1.95	531	<1	.09	12	220	<2	10	<20	70	.23	20	1752	<10	<1	83
8 -	R/C 2- 8	<.2	3.80	10	8	55	<5	4.27	<1	58	<1	198	10.25	<.01	<10	1.81	796	<1	.15	7	200	<2	10	<20	127	.24	<10	799	<10	9	56
9 -	R/C 3- 1	<.2	3.00	10	6	70	<5	3.01	<1	47	5	571	9.71	.04	<10	1.74	731	<1	.09	29	220	<2	15	<20	82	.10	<10	721	<10	12	49
10 -	R/C 3- 2	<.2	3.43	10	6	55	<5	4.48	<1	41	9	477	7.98	.03	<10	2.80	1005	<1	.03	30	170	<2	15	<20	57	.05	<10	517	<10	10	55
11 -	R/C 3- 3	<.2	2.37	10	6	45	<5	3.01	<1	41	14	584	8.14	.04	<10	1.58	762	<1	.05	32	260	<2	5	<20	57	.14	<10	557	<10	13	48
12 -	R/C 3- 4	<.2	3.41	10	6	60	<5	3.28	<1	37	86	235	6.99	.03	<10	2.16	872	<1	.07	37	50	<2	5	<20	99	.10	<10	460	<10	11	57
13 -	R/C 3- 5	<.2	2.27	5	6	35	<5	3.22	<1	15	144	129	3.14	.02	<10	1.40	633	<1	.09	15	430	<2	5	<20	70	.06	<10	65	<10	10	38
14 -	S/R 93- 6	.4	2.62	10	8	20	<5	2.07	<1	25	10	3293	1.85	.03	<10	.77	205	<1	.14	15	20	2	5	<20	102	.04	<10	37	<10	2	33
15 -	S/R 93- 7	<.2	3.11	10	6	35	<5	1.95	<1	31	16	248	6.36	.01	<10	.73	184	<1	.26	5	940	<2	5	<20	134	.08	<10	361	<10	5	27
16 -	S/R 93- 8	<.2	4.48	10	8	55	<5	2.67	<1	42	49	644	9.63	.01	<10	.94	322	<1	.33	31	180	<2	<5	<20	259	.13	<10	757	<10	1	45

QC/DATA:

Repeat #:

ET#	DESCRIPTION	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1 -	R/C 2- 1	<.2	4.55	10	6	45	<5	4.67	<1	27	60	33	5.95	.03	<10	1.74	940	<1	.18	26	580	<2	5	<20	151	.06	<10	222	<10	7	53
STANDARD 1991:		1.2	1.79	70	6	110	<5	1.64	<1	18	60	78	3.68	.32	<10	.89	648	<1	.02	22	640	14	5	<20	62	.11	<10	75	<10	11	66

NOTE: < = LESS THAN

SC93/WESTORE

ECO-TECH LABORATORIES LTD.
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B.C. Certified Assayer

ECO-TECH LABORATORIES LTD.
10041 EAST TRANS CANADA HWY.
KAMLOOPS, B.C. V2C 2J3
PHONE - 604-573-5700
FAX - 604-573-4557

JULY 9, 1993

WESTORE ENGINEERING ETK 93-170
703 - 1112 W. PENDER
VANCOUVER, B.C.
V6E 2S1

ATTENTION: SCOTT SMITH

VALUES IN PPM UNLESS OTHERWISE REPORTED

8 ROCK SAMPLES RECEIVED JULY 2, 1993
PROJECT #: ASHTON 93-2

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
1	- R/C 1-1	10	<.2	1.21	20	2	10	<5	1.02	<1	18	23	607	2.11	<.01	<10	1.03	292	1	.03	13	50	8	5	<20	32	.08	<10	65	<10	5	29
2	- R/C 1-2	5	.2	1.37	195	6	15	<5	1.20	<1	22	50	1605	1.89	<.01	<10	.42	247	3	.06	17	220	10	<5	<20	32	.04	<10	23	<10	3	169
3	- R/C 1-3	5	.2	1.32	60	36	15	<5	1.09	<1	14	48	1760	1.57	<.01	<10	.44	327	1	.05	18	180	10	<5	<20	26	.03	<10	27	<10	2	106
4	- R/C 1-4	10	.6	1.24	70	4	10	<5	.94	<1	15	44	4791	2.21	<.01	<10	.52	394	2	.04	14	510	8	<5	<20	24	.05	<10	30	<10	4	151
5	- R/C 1-5	20	.6	1.35	65	2	15	<5	.73	<1	23	48	5767	2.83	<.01	<10	.44	432	2	.02	8	550	8	<5	<20	29	.06	<10	31	<10	5	65
6	- R/C 1-6	25	.8	1.11	60	2	15	<5	.54	<1	22	49	5569	3.15	<.01	<10	.34	402	4	.02	7	510	6	<5	<20	25	.06	<10	18	<10	6	66
7	- R/C 1-7	30	<.2	1.37	25	4	15	<5	.75	<1	21	35	1595	2.50	.01	<10	.73	282	2	.04	8	100	10	<5	<20	32	.07	<10	44	<10	4	35
8	- R/C 1-8	20	<.2	2.84	<5	4	40	<5	1.45	<1	34	15	1180	5.38	.03	<10	.95	233	1	.23	26	30	14	<5	<20	275	.08	<10	281	<10	2	34

QC DATA

ET#	DESCRIPTION	AU (ppb)	AG	AL(%)	AS	B	BA	BI	CA(%)	CD	CO	CR	CU	FE(%)	K(%)	LA	MG(%)	MN	MO	NA(%)	NI	P	PB	SB	SN	SR	TI(%)	U	V	W	Y	ZN
REPEAT #:																																
1	- R/C 1-1		<.2	1.19	20	4	15	<5	1.01	<1	17	23	589	2.06	<.01	<10	1.01	286	1	.03	12	60	8	5	<20	32	.08	<10	63	<10	5	29
STANDARD 1991 -			1.2	1.42	75	4	140	<5	1.40	<1	17	50	79	3.15	.29	<10	.83	610	<1	.01	22	580	22	5	<20	51	.07	<10	59	<10	8	70

NOTE: < = LESS THAN

ECO-TECH LABORATORIES LTD.
FRANK J. PEZZOTTI, A.Sc.T.
B.C. Certified Assayer

SC93/KAMMISC#1

Eco·Tech
LABORATORIES LTD.

ASSAYING
GEOCHEMISTRY
ANALYTICAL CHEMISTRY
ENVIRONMENTAL TESTING

10041 E. Trans Canada Hwy., R.R. #2, Kamloops, B.C. V2C 2J3 Phone (604) 573-5700
Fax (604) 573-4557

JULY 13, 1993

CERTIFICATE OF ASSAY ETK 93-170

WESTORE ENGINEERING
703-1112 W. PENDER STREET
VANCOUVER, B.C.
V6E 2S1

ATTENTION: SCOTT SMITH

SAMPLE IDENTIFICATION: 8 ROCK SAMPLES RECEIVED JULY 2, 1993
PROJECT #: 93-2

ET#	Description	CU (%)
4-	R/C 1-4	.52
5-	R/C 1-5	.59
6-	R/C 1-6	.60

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APPENDIX III

ANALYTICAL METHODS

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Fax (604) 573-4557

METHODOLOGY

a) Gold - Geochemical — Fire Assay - A.A.

A 10.000 gram sample is fire assayed by conventional fire assay procedures. The resulting bead is dissolved in 3ml aqua regia and is analyzed for gold by Atomic Absorption.

Minimum Reportable Concentration: 5 (pbb)

b) 30 Element ICP — Aqua Regia Digestion

A one gram sample* is digested with a 6ml mixture of HCL, HNO_3, H_2O in a ratio of 3:2:1. The digestion is carried out at 95°C for two hours. The digested sample is made up to 20ml with distilled water and analyzed by ICP.

Minimum Reportable Concentration:

a) Aqua Regia Digestion

Ag	0.2 ppm	Cu	1 ppm	Pb	2 ppm
Al*	0.01%	Fe*	0.01%	Sb	5 ppm
As	5 ppm	K*	0.01%	Sn	20 ppm
B*	2 ppm	La	10 ppm	Sr*	1 ppm
Ba*	5 ppm	Mg*	0.01%	Ti*	0.01%
Bi	5 ppm	Mn*	1 ppm	U*	10 ppm
Ca*	0.01%	Mo	1 ppm	V	1 ppm
Cd	1 ppm	Na*	0.01%	W*	10 ppm
Co	1 ppm	Ni	1 ppm	Y	1 ppm
Cr*	1 ppm	P*	10 ppm	Zn	1 ppm

Dissolution of elements marked by an asterisk may not be complete.
* 2 gram sample can be used at no extra charge

Copper Assay

A 2g sample is digested in a 200ml phosphoric flask with HNO_3, HCl. The digestion is carried out on a hot plate for 2 hours. The sample is bulked up with distilled water and analysed for copper by Atomic Absorbtion. The minimum reportable concentration is <0.01%.

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Fax (604) 573-4557

Quality control

a) Sample Preparation

Random Duplicate samples are split from each shipment and introduced in each suite of samples sent to the laboratory for analysis. No less than one sample in forty is re-split. Each sample is assigned a unique lab number and barcode to be read by the barcode reader at the weigh station. A second person checks the lab number assignment for accuracy.

b) Weighing Stations

Each balance is calibrated twice during each shift using N.B.S. referenced weights. Samples are identified prior to weighing by use of a barcode reader. The sample identification, sample weight and analysis required is automatically captured by computer.

c) Fire Lab

Separate fusion pots are used for Assay, Rock Geochem and Soil Geochem. The pots are catalogued and are not reused until the assay is completed. Pots which were used for samples containing high or anomalous gold values are discarded at the end of each day. All flux mixtures are tested for purity before use.

d) Analysis

Samples are analyzed from test tube racks containing forty test tubes. Each rack will contain thirty-seven samples, (one of which may be a blind duplicate re-split form the bucking facility), one blank, one soil standard and one duplicate sample. Approximately 25 Can Met and several in-house standards are routinely used by our laboratory. As a minimum, a full 10% of all samples analyzed are quality control samples. In addition to the quality control analyses, check analyses are routinely performed to verify data for anomalous samples.

ASSAYING
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Fax (604) 573-4557

The samples are analyzed in the following order:

Test Tube	Contents
#40	Soil Standard (CanMet or In-House) to verify instrument calibration and sample digestion.
#1	Reagent Blank to check for reagent contamination and instrument zero.
#2 to #38	Analysis of samples.
#39	Sample Duplicate.
#40	Soil Standard and Recalibration.

Quality Control Data Assessment

Each element analyzed in the soil standards has an individual statistical plot of standard deviation for the analysis. Upper and lower warning limits are set at ±2 standard deviations. The analysis is considered to be out of control and is stopped when the value exceeds ±3 standards deviations. If the nature of the problem cannot be determined, the entire block of samples is re-analyzed. The results for duplicate and blind duplicate pairs must fall within our tolerance limits for precision of geochemical analysis as outlined below:

Average Value	Precision
1 to 2 times detection limit	± 100%
3 to 4 " "	± 60%
5 to 6 " "	± 40%
7 to 10 " "	± 25%
11 to 100 " "	± 15%
> 100 " "	± 10%

APPENDIX IV

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VLF-EM and Magnetic Survey of the Burgoyne Group of Mineral Claims. Assessment Report.

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Smith, S.W., 1993:
Geological Mapping and Geological Sampling on the Ashton Property; Kingston Resources Ltd.

APPENDIX V

STATEMENT OF QUALIFICATIONS

I, Scott W. Smith, of 845 East 31st Avenue, Vancouver, BC, V5V 2X2, declare:

1. I am a Professional Geologist, residing at the above address.
2. I graduated from the University of Alberta with a Bachelor of Science (Spec. Geology) degree in 1988.
3. I have been practising my profession as a geologist for five years.
4. I am a member in good standing with the Association of Professional Engineers, Geologists and Geophysicists of Alberta.
5. This report is based on my personal field examination of the property.

Dated at Vancouver, British Columbia,
this 9 day of November 1993.

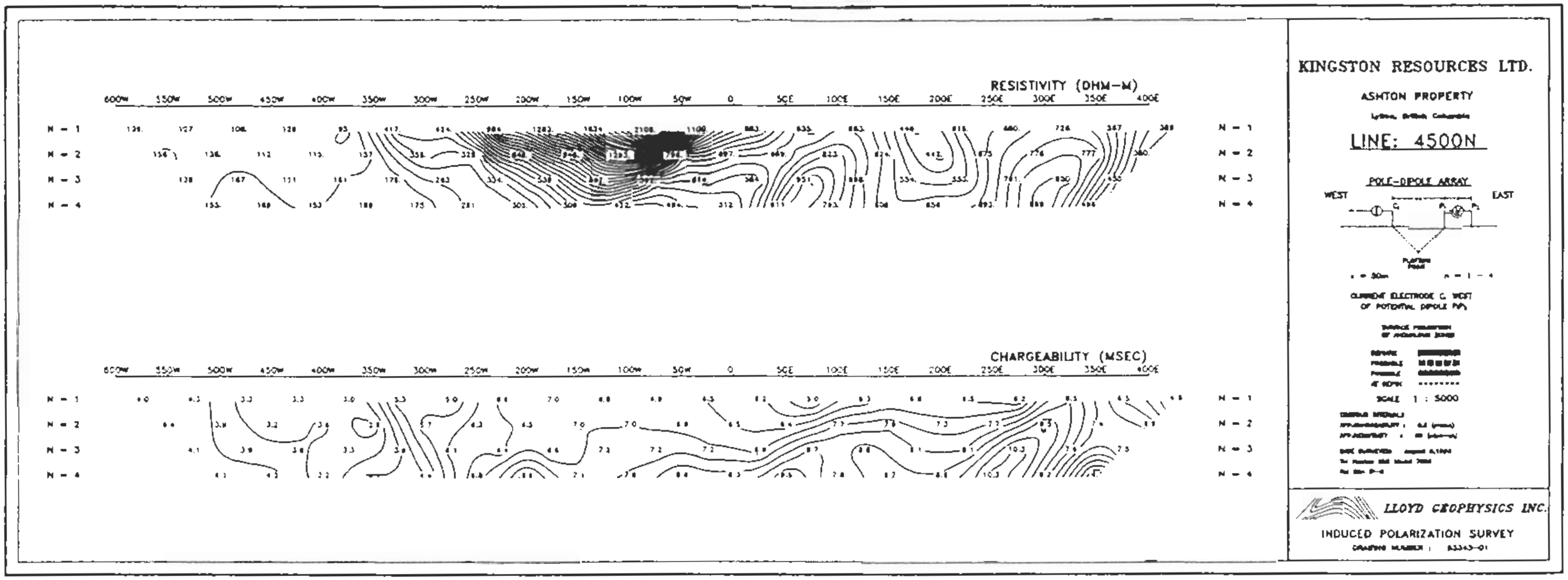
[signature]

Scott W. Smith, P. Geol.

APPENDIX VI

IP SURVEY

PSEUDOSECTIONS



RESISTIVITY (OHM-M)
CHARGEABILITY (MSEC)
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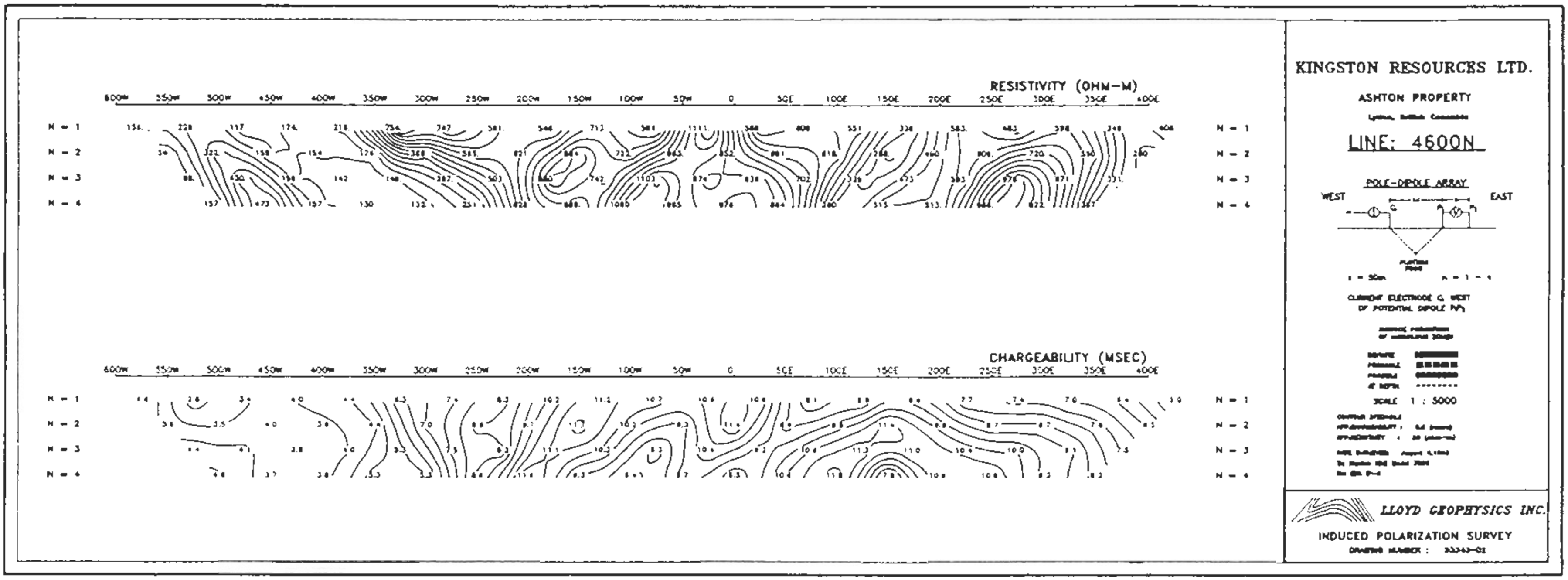
N = 1
N = 2
N = 3
N = 4
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
LINE: 4500N
POLE-DIPOLE ARRAY
WEST
EAST
SCALE 1 : 5000
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY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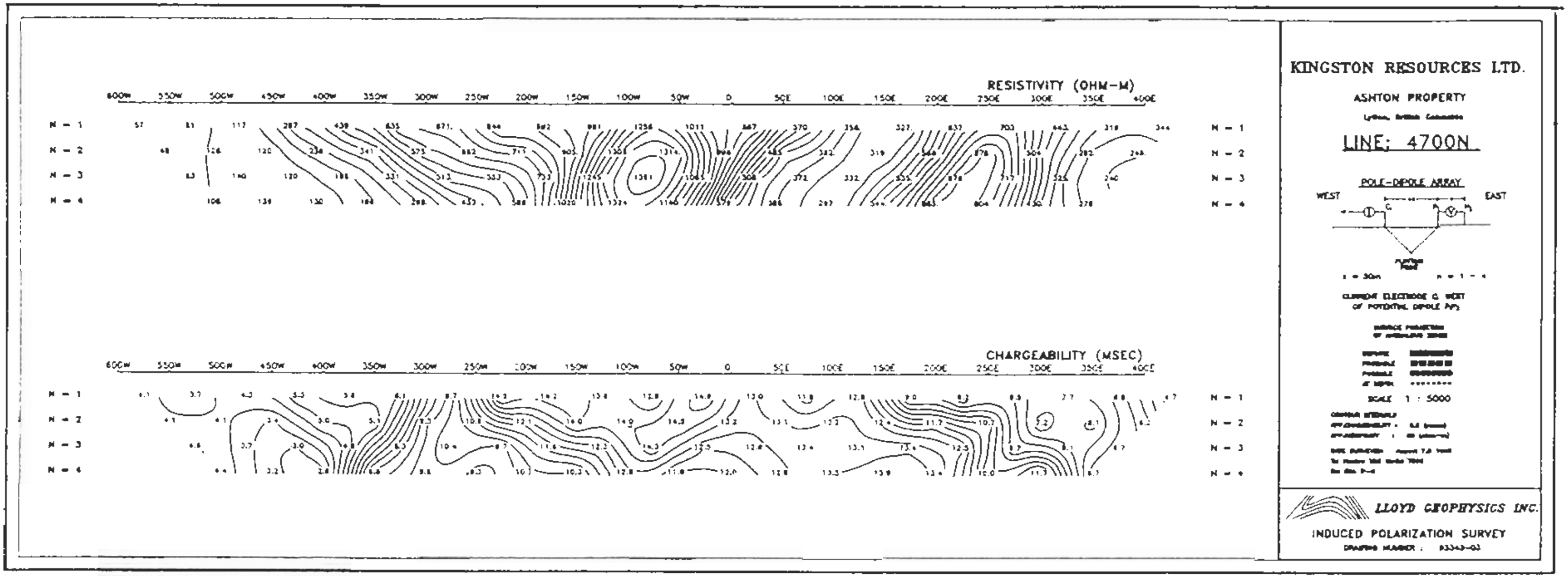
INDUCED POLARIZATION SURVEY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ASHTON PROPERTY
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EAST
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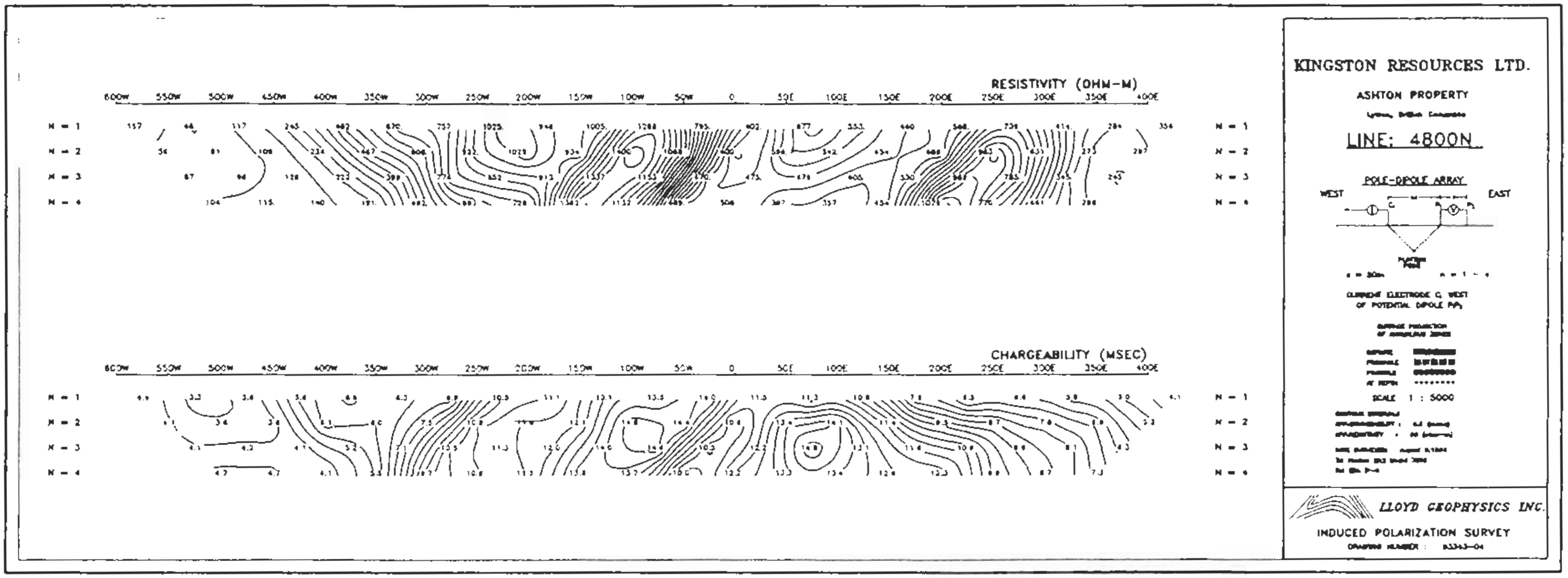
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY



RESISTIVITY (OHM-M)
CHARGEABILITY (MSEC)
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ASHTON PROPERTY
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POLE-DIPOLE ARRAY
WEST
EAST
CURRENT ELECTRODE C WEST OF POTENTIAL DIPOLE
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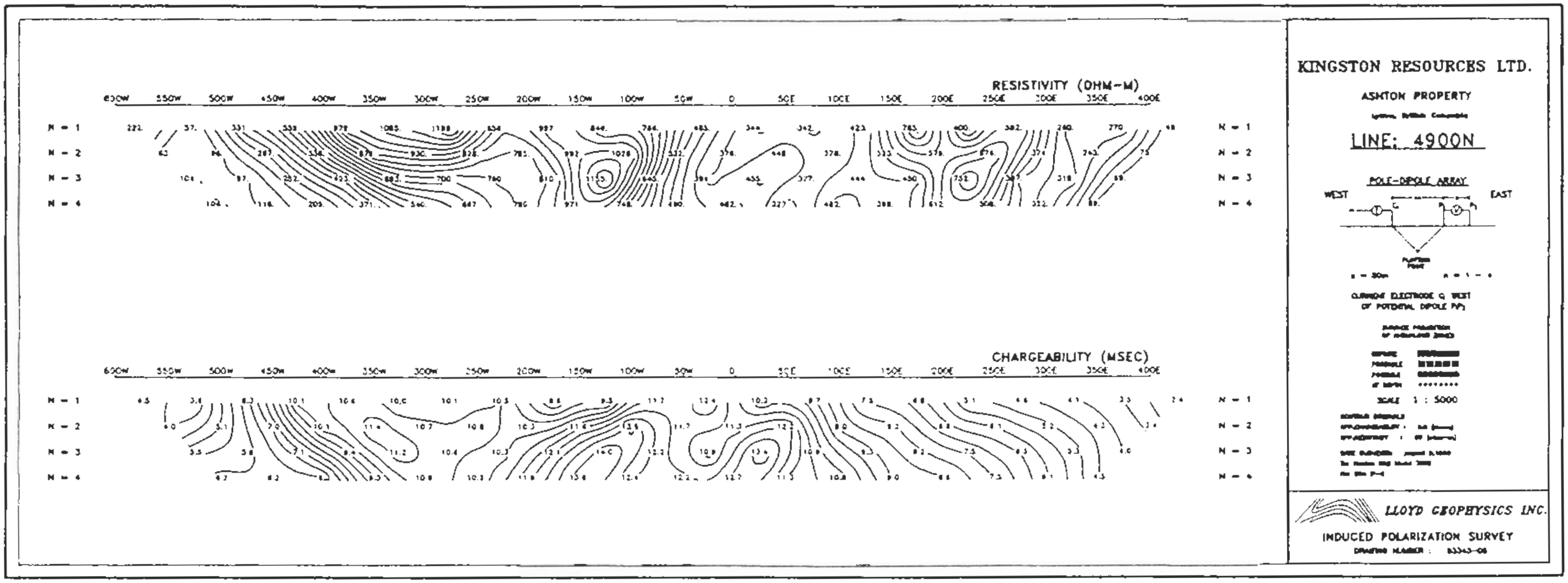
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY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CHARGEABILITY (MSEC)
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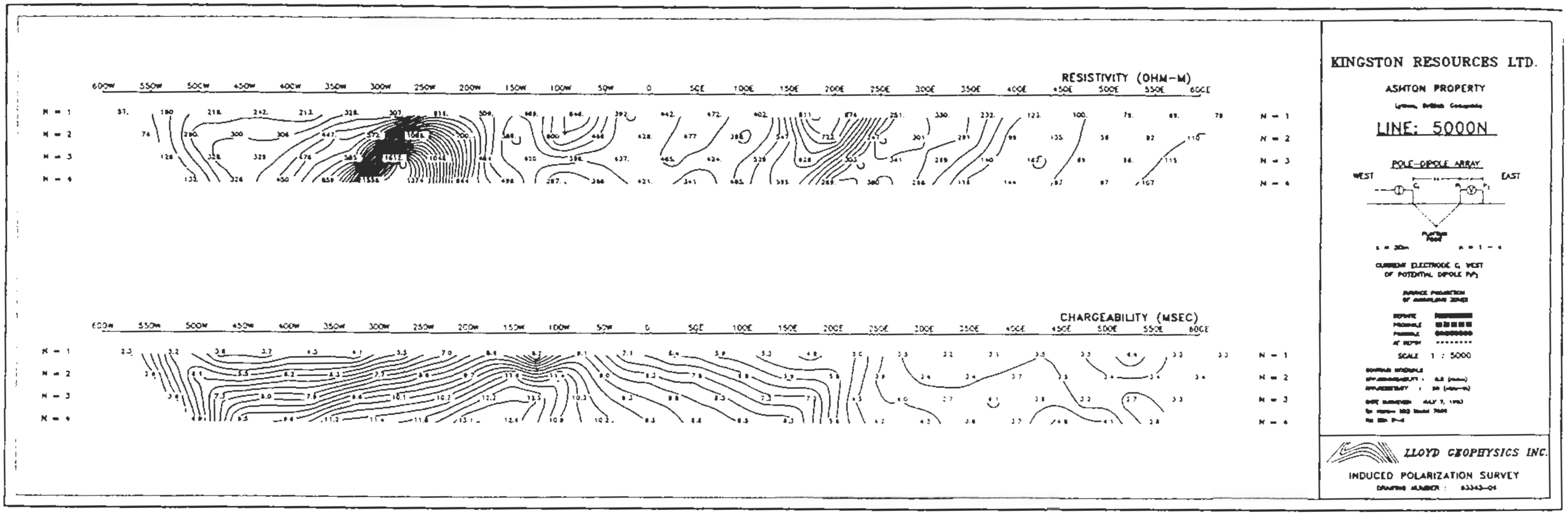
N = 1
N = 2
N = 3
N = 4
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
LINE: 4900N
POLE-DIPOLE ARRAY
WEST
EAST
SCALE 1 : 5000
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY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N = 2
N = 3
N = 4
CHARGEABILITY (MSEC)
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
LINE: 5000N
POLE-DIPOLE ARRAY
WEST
EAST
SCALE 1 : 5000
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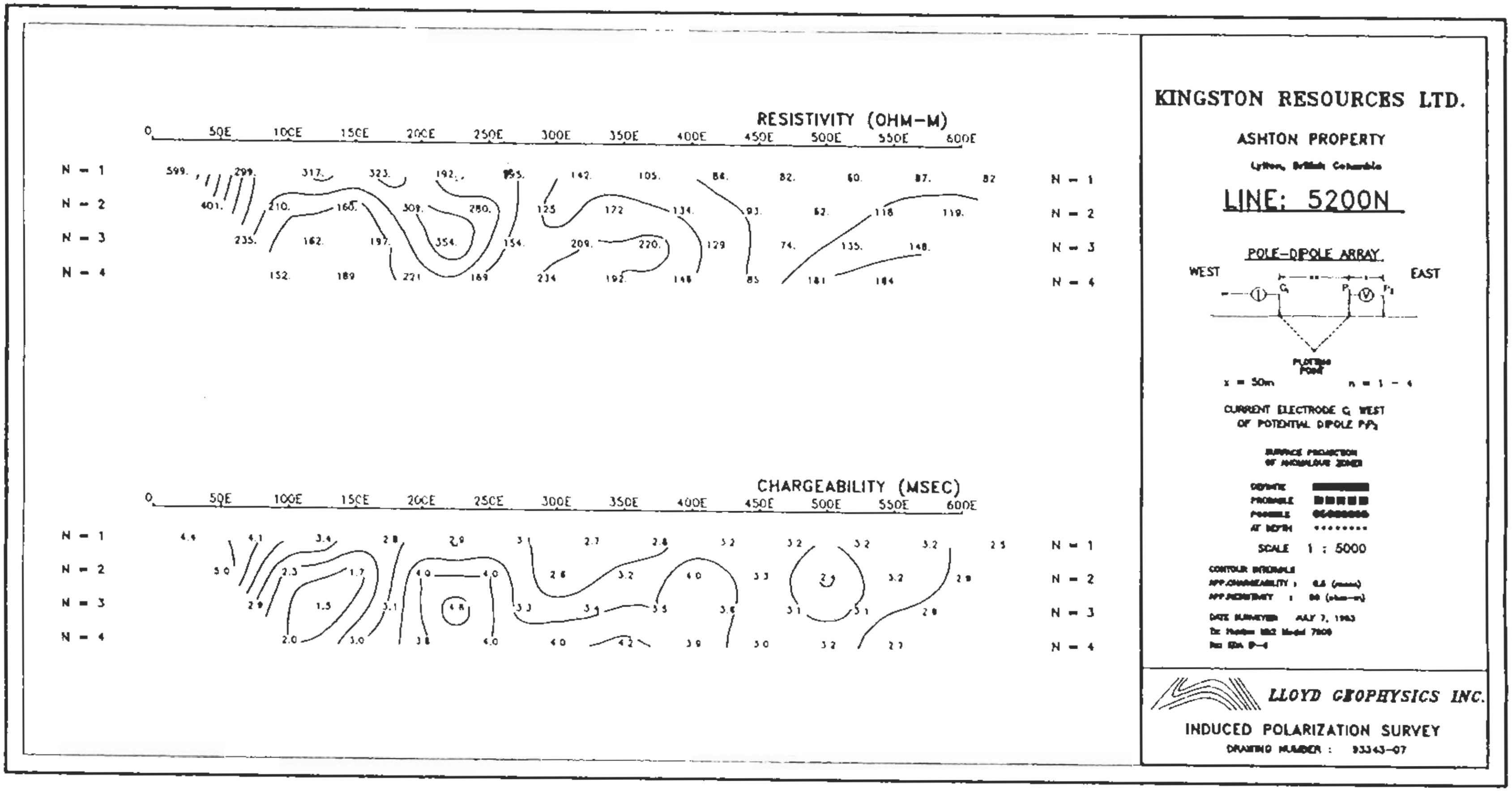
INDUCED POLARIZATION SURVEY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CHARGEABILITY (MSEC)
0 50E 100E 150E 200E 250E 300E 350E 400E 450E 500E 550E 600E
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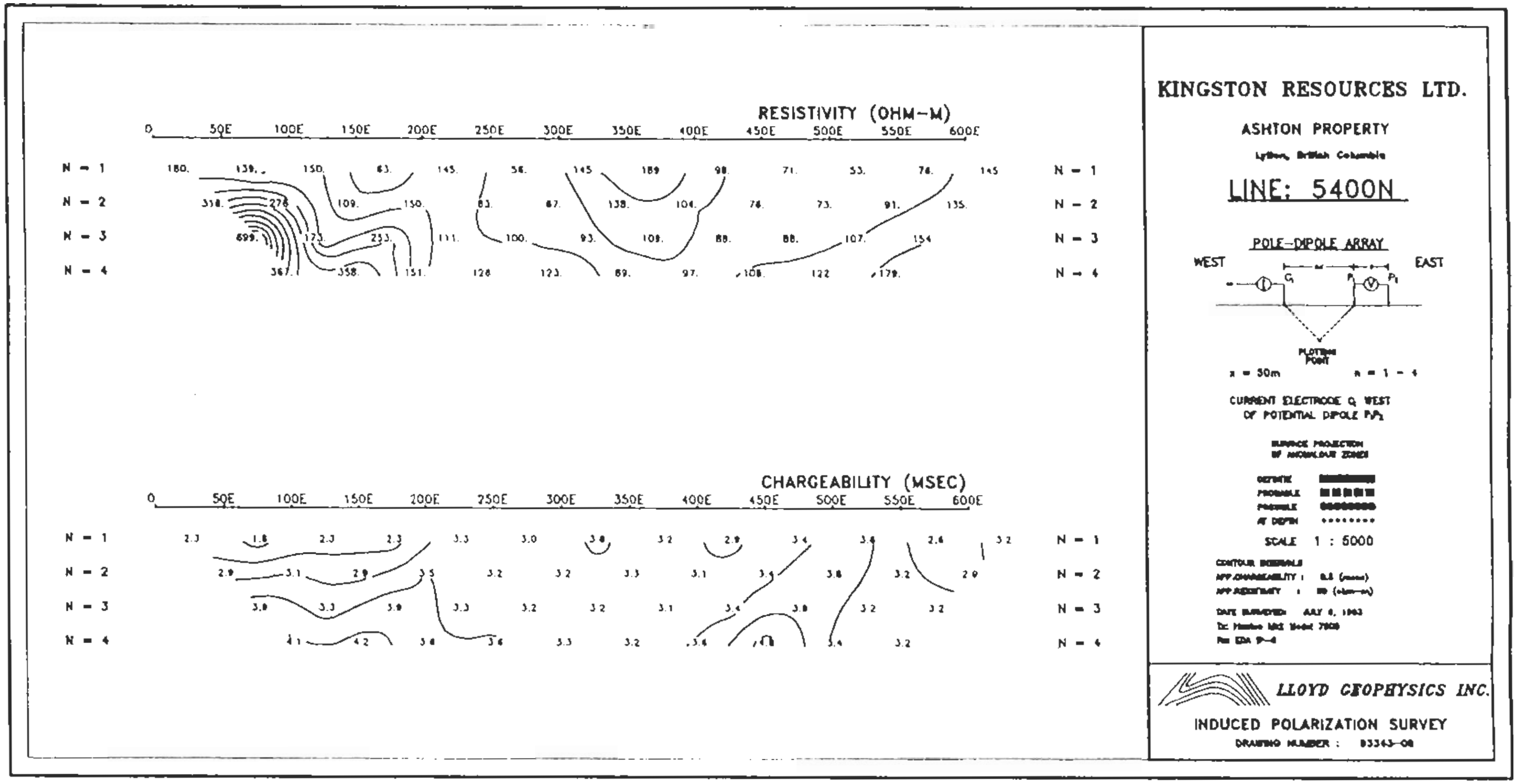
N = 2
N = 3
N = 4
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
Lytton, British Columbia
LINE: 5200N
POLE-DIPOLE ARRAY
WEST
EAST
x = 50m
n = 1 - 4
CURRENT ELECTRODE C1 WEST
OF POTENTIAL DIPOLE P1P2
SCALE 1 : 5000
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY
DRAWING NUMBER : 93343-07



RESISTIVITY (OHM-M)
CHARGEABILITY (MSEC)
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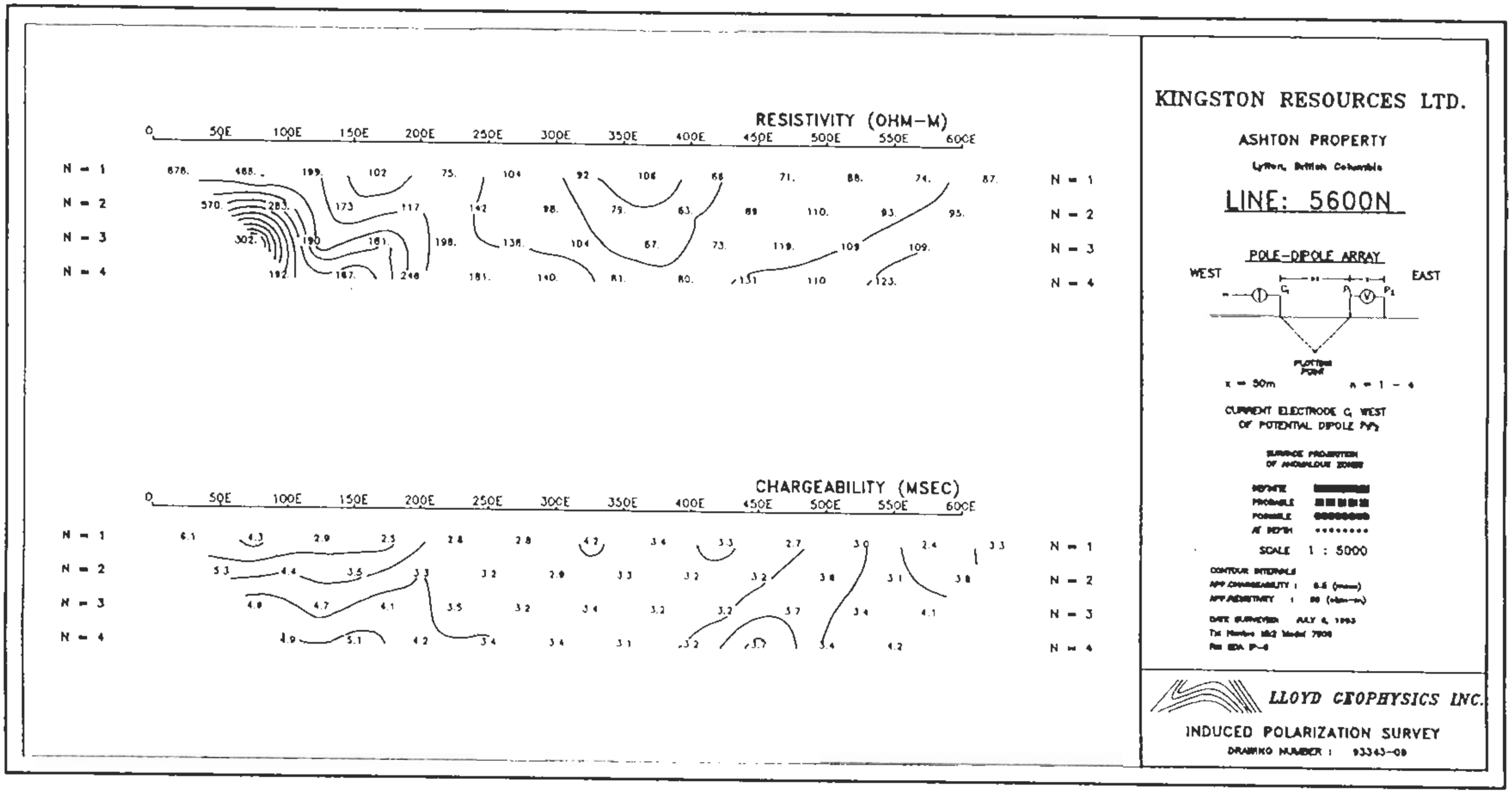
N = 1
N = 2
N = 3
N = 4
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
LINE: 5400N
POLE-DIPOLE ARRAY
WEST
EAST
PLOTTING POINT
a = 50m
n = 1 - 4
SCALE 1 : 5000
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY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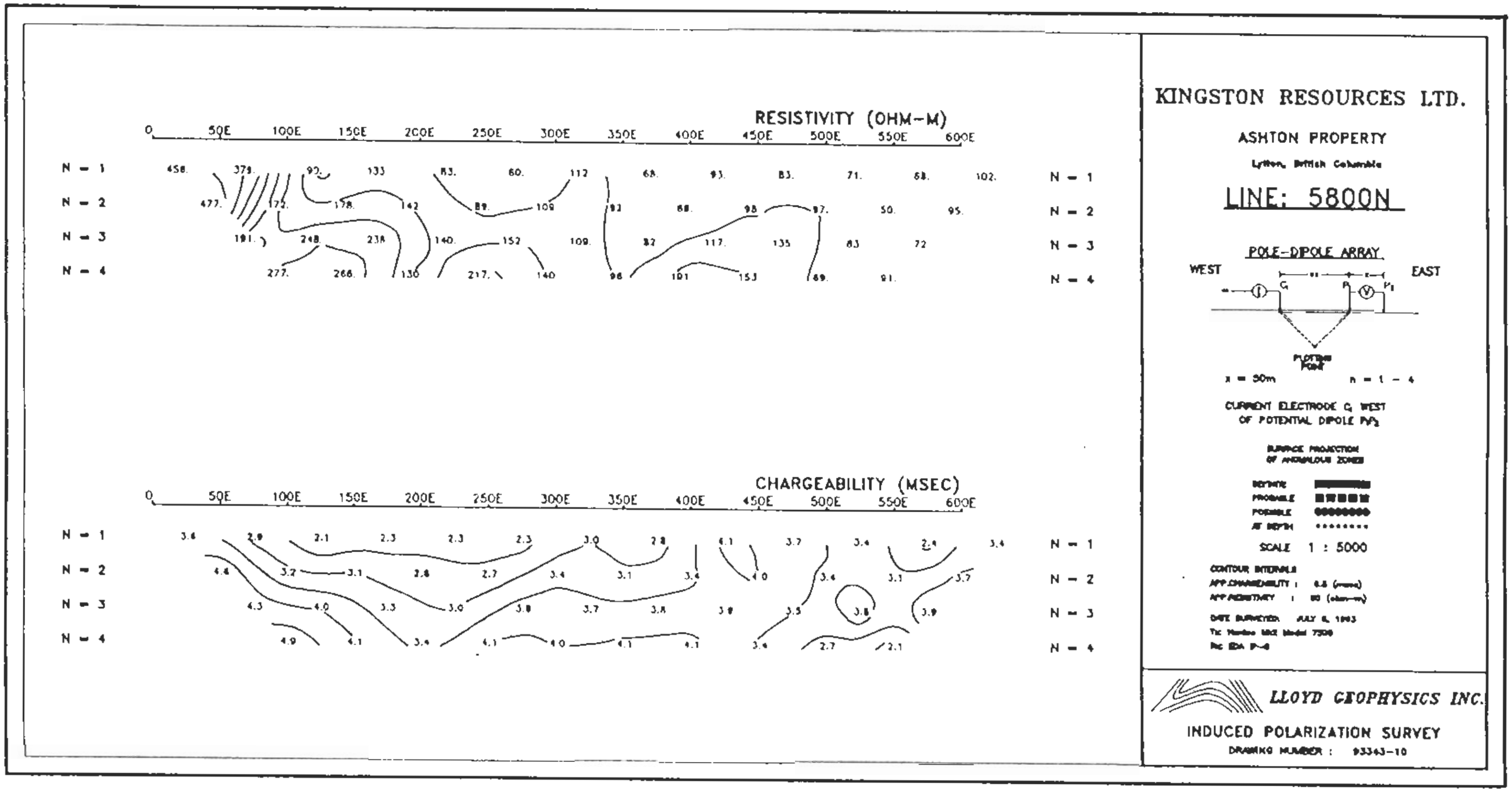
CHARGEABILITY (MSEC)
0 50E 100E 150E 200E 250E 300E 350E 400E 450E 500E 550E 600E
N = 1
N = 2
N = 3
N = 4
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
LINE: 5600N
POLE-DIPOLE ARRAY
WEST
EAST
SCALE 1 : 5000
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY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CHARGEABILITY (MSEC)
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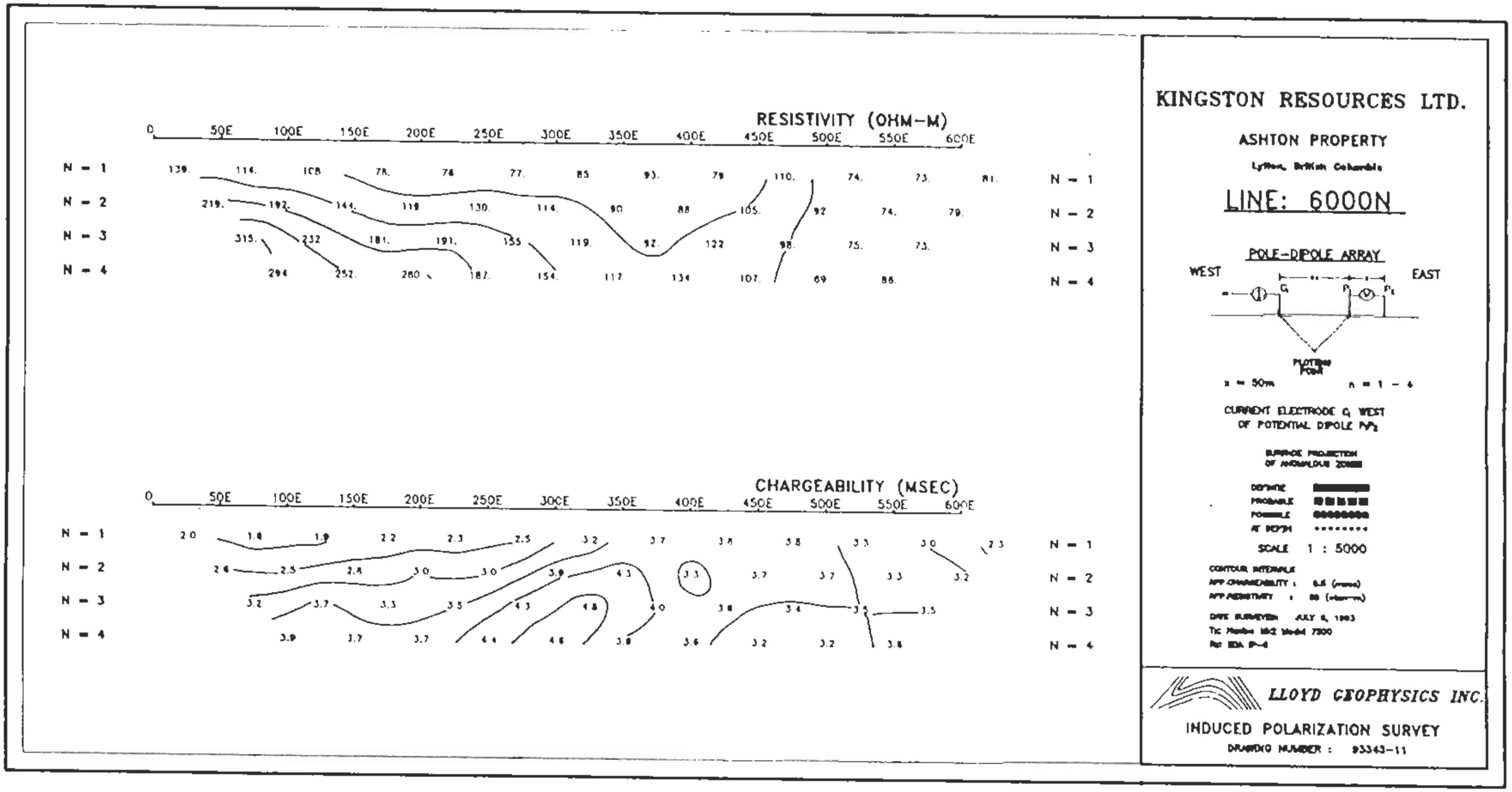
50E
100E
150E
200E
250E
300E
350E
400E
450E
500E
550E
600E
N = 1
N = 2
N = 3
N = 4
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
LINE: 5800N
POLE-DIPOLE ARRAY
WEST
EAST
SCALE 1 : 5000
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY
93343-10



RESISTIVITY (OHM-M)
CHARGEABILITY (MSEC)
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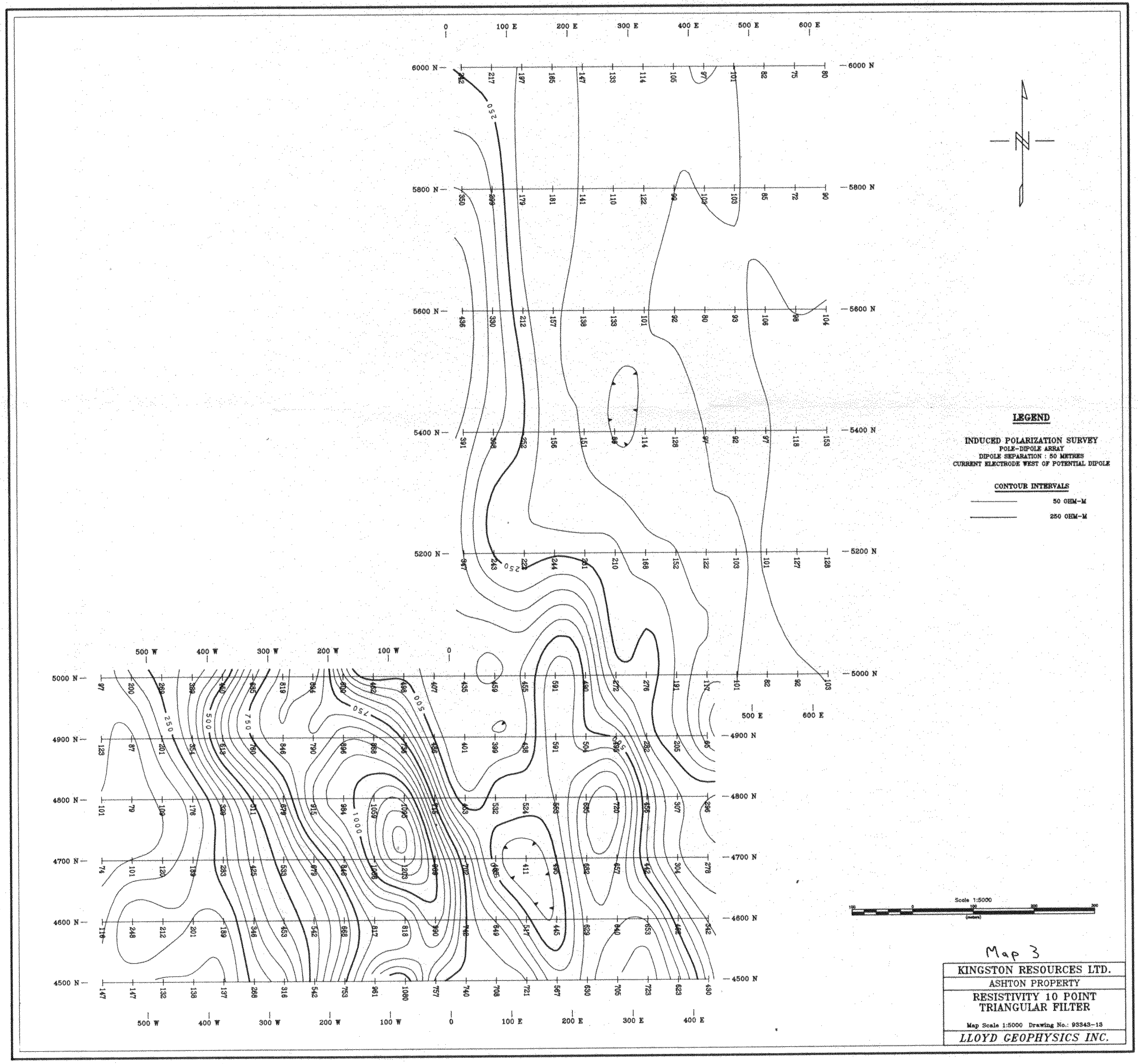
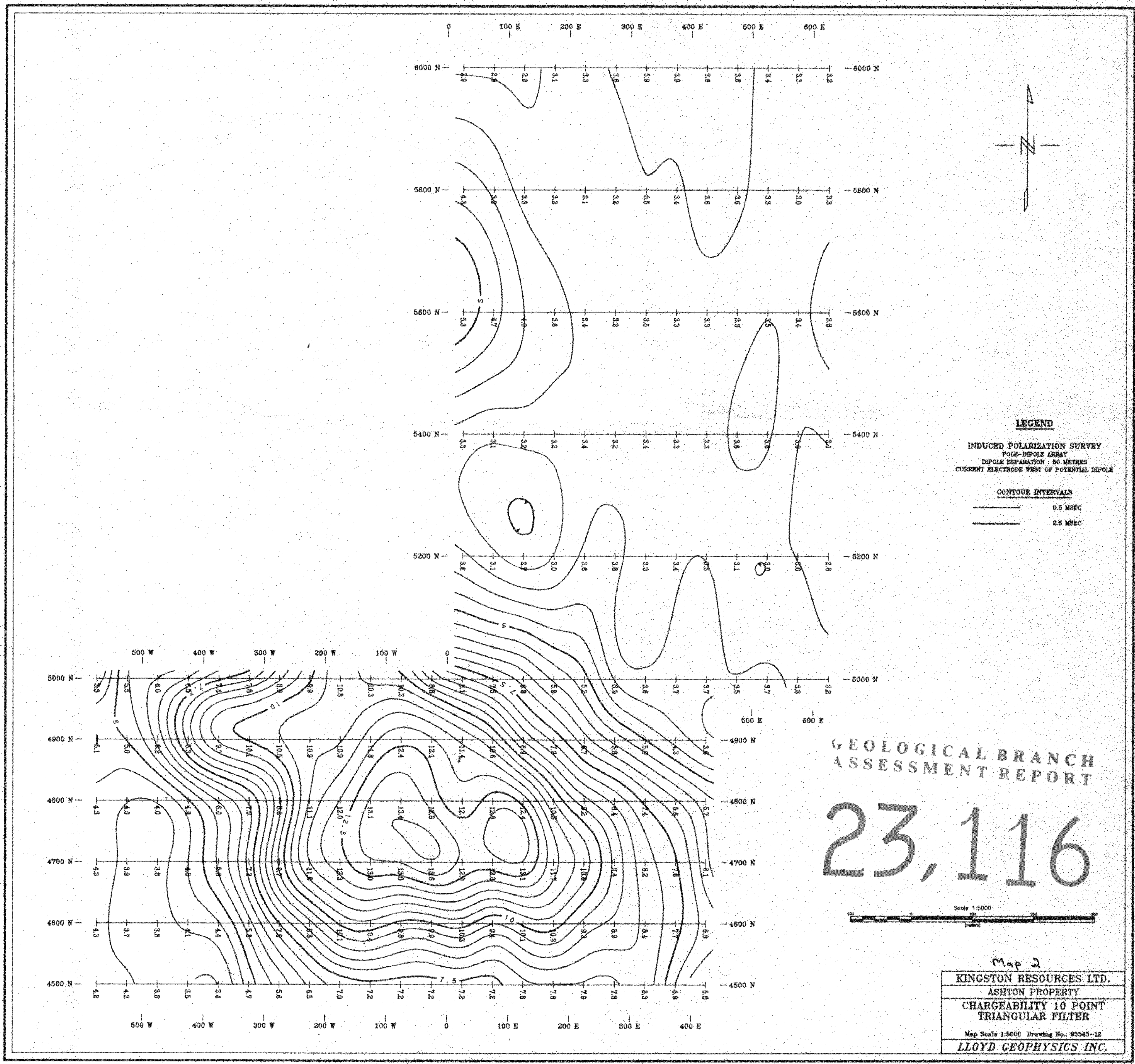
N = 2
N = 3
N = 4
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
LINE: 6000N
POLE-DIPOLE ARRAY
WEST
EAST
CURRENT ELECTRODE C1 WEST OF POTENTIAL DIPOLE P1P2
SCALE 1 : 5000
LLOYD GEOPHYSICS INC.
INDUCED POLARIZATION SURVEY
DRAWING NUMBER : 93343-11


6000 N
5800 N
5600 N
5400 N
5200 N
5000 N
4900 N
4800 N
4700 N
4600 N
4500 N
500 W
400 W
300 W
200 W
100 W
0
100 E
200 E
300 E
400 E
500 E
600 E
LEGEND
INDUCED POLARIZATION SURVEY
POLE-DIPOLE ARRAY
DIPOLE SEPARATION : 50 METRES
CURRENT ELECTRODE WEST OF POTENTIAL DIPOLE
CONTOUR INTERVALS
50 OHM-M
250 OHM-M
Scale 1:5000
Map 3
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
RESISTIVITY 10 POINT TRIANGULAR FILTER
Map Scale 1:5000 Drawing No.: 93343-13
LLOYD GEOPHYSICS INC.


0
100 E
200 E
300 E
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500 E
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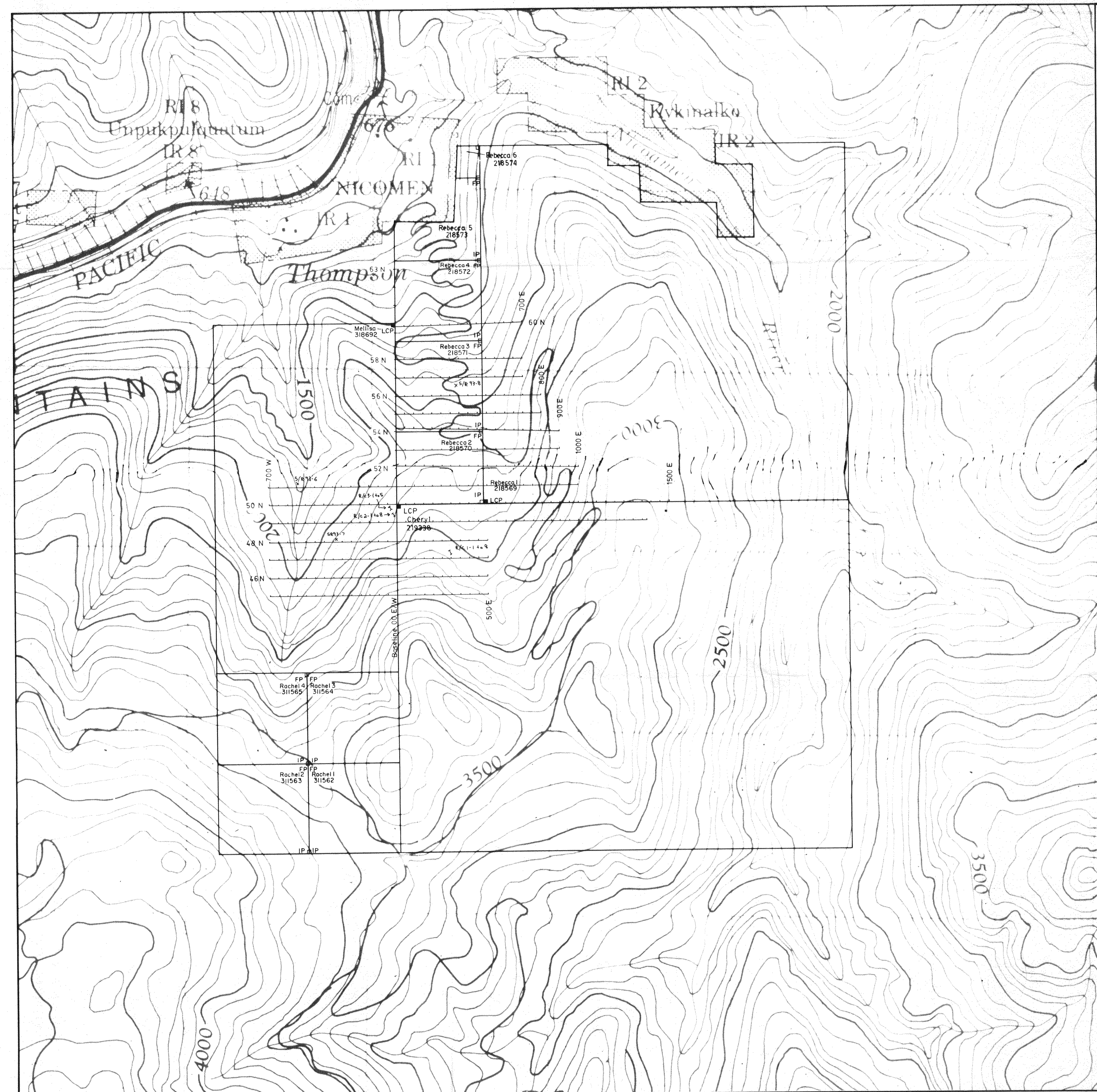
5000 N
4900 N
4800 N
4700 N
4600 N
4500 N
500 W
400 W
300 W
200 W
100 W
LEGEND
INDUCED POLARIZATION SURVEY
POLE-DIPOLE ARRAY
DIPOLE SEPARATION : 50 METRES
CURRENT ELECTRODE WEST OF POTENTIAL DIPOLE
CONTOUR INTERVALS
0.5 MSEC
2.5 MSEC
GEOLOGICAL BRANCH
ASSESSMENT REPORT
23,116
Scale 1:5000
Map 2
KINGSTON RESOURCES LTD.
ASHTON PROPERTY
CHARGEABILITY 10 POINT
TRIANGULAR FILTER
Map Scale 1:5000 Drawing No.: 93343-12
LLOYD GEOPHYSICS INC.



LEGEND

- ■ Legal Corner Post
- □ Initial Post/Final Post
- Claim Boundaries
- Rebecca1 218569 — Claim Name & Tenure Number
- Highway
- Allseason Gravel Road
- x S/R93-6 Rock-grab sample
- R/C1-1 to 8 Rock-chip sample (8 continuous samples in interval)

GEOLOGICAL BRANCH
ASSESSMENT REPORT

23,116

SCALE 1:10000

0 100 200 300 500 1000
METRES

KINGSTON RESOURCES LTD.

Ashton Property Kamloops M.D.

Grid + Sample Location

Drawn By:	Scale: 1:10000
Checked By:	NTS: 92I/3W/6W
Date:	Map No.: 1