

ARIS SUMMARY SHEET

District Geologist, Prince George

Off Confidential: 94.12.06

ASSESSMENT REPORT 23321

MINING DIVISION: Omineca

PROPERTY: Cygnet-Swan

LOCATION: LAT 56 29 00 LONG 125 30 00

          UTM 10 6262463 346045

          NTS 094C05E 094C06E

CLAIM(S): R 1-16, Swan 2, Swan 5, Swan 8-10, Swan 12-14

OPERATOR(S): Cominco

AUTHOR(S): Rhodes, D.

REPORT YEAR: 1993, 42 Pages

KEYWORDS: Devonian, Rosella Formation, Boya Formation, Argillaceous limestones  
Limestones, Mudstones, Siltstones, Quartzites, Sphalerite, Galena  
Pyrite, Barite

WORK

DONE: Geological, Geochemical

GEOL 4500.0 ha

Map(s) - 5; Scale(s) - 1:500, 1:2500, 1:10 000

SILT 23 sample(s); ME

SOIL 641 sample(s); ME

Map(s) - 6; Scale(s) - 1:10 000, 1:2500

RELATED

REPORTS: 21434, 22811

MINFILE: 094C 073, 094C 074, 094C 141

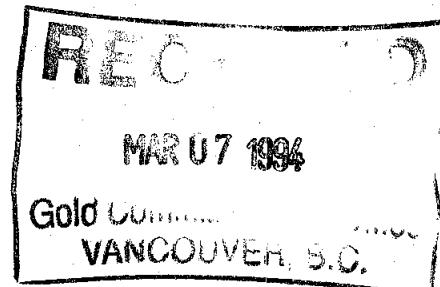
COMINCO LTD.

EXPLORATION

WESTERN DISTRICT

NTS 94-C-5,6

LOG #	APR 05 1994	RD.
ACTION.		
FILE NO:		



**1993 ASSESSMENT REPORT**

**CYGNET/SWAN PROPERTY**

**SWAN 1-14, Nell 1-10, R 1-16 and Rap 17**

Record No's 308212 -308216 incl., 316185 - 316193 incl.  
308237 - 308244 incl., 308219 - 308244 incl., 312616

Mesilinka R. to Swannell R.

Omineca Mining Division

LATITUDE: 56°29'

LONGITUDE: 125°30'

**CLAIMS OWNED BY STRATABOUND MINERALS CORP.**

**FILMED**

**OPERATOR: COMINCO LTD.**

**G E O L O G I C A L   B R A N C H  
A S S E S S M E N T   R E P O R T**

MARCH, 1994

D. RHODES  
SENIOR GEOLOGIST

**23,321**

## TABLE OF CONTENTS

	<u>Page</u>
1. SUMMARY .....	1
2. LOCATION AND ACCESS .....	1
3. TENURE .....	1
4. HISTORY .....	2
5. 1993 WORK .....	2
A. Objectives .....	2
B. Work .....	2
6. GEOLOGY .....	2
A. General .....	3
B. Detailed Geology .....	5
i) Rain Area Geology .....	5
ii) Knoll Area Geology .....	5
iii) Swan Area Geology .....	6
iv) Gilliland Tuff .....	6
C. Mineralization .....	6
7. GEOCHEMISTRY .....	8
8. CONCLUSIONS AND RECOMMENDATIONS .....	3
REFERENCES .....	3

## APPENDICES

Appendix 1 Statement of Expenditures

Appendix 2 Geochemical Analyses

Appendix 3 Statement of Qualifications

FIGURES (within body of Report)

Figure 1 CLAIM LOCATION MAP SHOWING OLD RAIN, KNOLL AND SWAN GRIDS

Figure 2 SWAN/CYNET PROPERTY CLAIMS ON GEOLOGY MAP (FERRI ET AL 1993B)

Figure 3 PANORAMIC PHOTOGRAPHIC VIEW OF RAIN RIDGE WITH GEOLOGY SHOWN

PLATES (within pouches)

	SCALE
Plate 93-1A CYGNET PROPERTY - GEOLOGY EAST HALF	1,10,000
Plate 93-1B CYGNET PROPERTY - GEOLOGY WEST HALF	1:10,000
Plate 93-2A CYGNET PROPERTY - EAST HALF - GEOCHEMISTRY VALUES AND CLAIM LOCATION	1:10,000
Plate 93-2B CYGNET PROPERTY - WEST HALF - GEOCHEMISTRY VALUES AND CLAIM LOCATION	1:10,000
Plate 93-3A CYGNET PROPERTY - EAST HALF - GEOCHEMISTRY SAMPLE LOCATIONS	1:10,000
Plate 93-3B CYGNET PROPERTY - WEST HALF - GEOCHEMISTRY SAMPLE LOCATIONS	1:10,000
Plate 4 CYGNET PROPERTY - "SWAN GRID" GEOLOGY	1:2,500
Plate 5 CYGNET PROPERTY - "SWAN GRID" ZINC SOIL GEOCHEMISTRY CONTOURS	1:2,500
Plate 6 CYGNET PROPERTY - "SWAN GRID" LEAD SOIL GEOCHEMISTRY CONTOURS	1:2,500
Plate 7 GEOLOGY AND SAMPLING RESULTS "RAIN" TRENCH SOUTH SHOWING	1:500
Plate 8 GEOLOGY AND SAMPLING RESULTS "SWAN" TRENCH NORTH EXTENSION OF MAIN SHOWING AREA	1:500 1:100

**COMINCO LTD.**

**EXPLORATION  
NTS. 94-C-3**

**WESTERN DISTRICT  
MARCH, 1994**

**ASSESSMENT REPORT - 1993  
SWAN/CYGNET PROPERTY - CLAIMS SWAN 1-14, NELL 1-10  
RAP 17 AND R 1-16**

**1. SUMMARY**

The Swan property (known as Cygnet in Cominco records) encompasses three areas of Cambrian to Devonian carbonates and lesser shales (the Swan, Knoll and Rain) lying along 12 kilometres of northwest trending geological strike separated from each other by fault displacement. Recent mapping has highlighted the presence of Devonian basaltic to rhyolitic pyroclastics referred to as the Gilliland Tuff.

Cominco 1992 work included a detailed soil geochemical and mapping grid on the Swan area, contour soil geochemistry and recce geology on the Rain, Knoll and Gilliland Tuff areas with a regional stream silt program covering the property. Work on the Rain and Knoll areas showed high geochemistry associated with apparently structural controlled Pb/Zn mineralization with the hosting stratigraphy being confined down dip and along strike by faults. Work on the Swan showed high lead, zinc geochemistry along strike of known showings that also appear to be structurally controlled, however some possibility exists for more significant sulphide accumulations. Interesting sphalerite and barite mineralization was found associated with bituminous dolomite interbeds in typical Devonian siliceous mudstones. A silt from the stream draining this area is anomalous in Cu, Zn and Ag. In addition a few silts and soils are anomalous in Cu, Pb, Zn, Ag on the western edge of the Swan 9 claim and may indicate mineralization in the Gilliland Tuff or in overlying stratigraphy, to the west, off the claims.

**2. LOCATION AND ACCESS**

The Swan/Cygnet property is located some 45 km. north of the Par property (Lat. 56°28', Long. 125°30'- see Fig 1 & 2). The claims lie within the Lay Range between the Mesilinka and Swannell Rivers. Access to most of the property is by helicopter with the southeastern most portion being reachable by a 1.5 km. hike from a rough 4x4 road off of the all season Omineca Mining access road.

**3. TENURE**

The Swan comprises 43 claims totalling 239 units. The claims were optioned by Cominco Ltd. from Stratabound Minerals Corp.. This report describes work undertaken by Cominco Ltd in the period July 20 - 27, 1993. Expenditures in 1993 totalled \$67,200. Details are given in Appendix 1. Details of the tenure are tabulated on the following page.

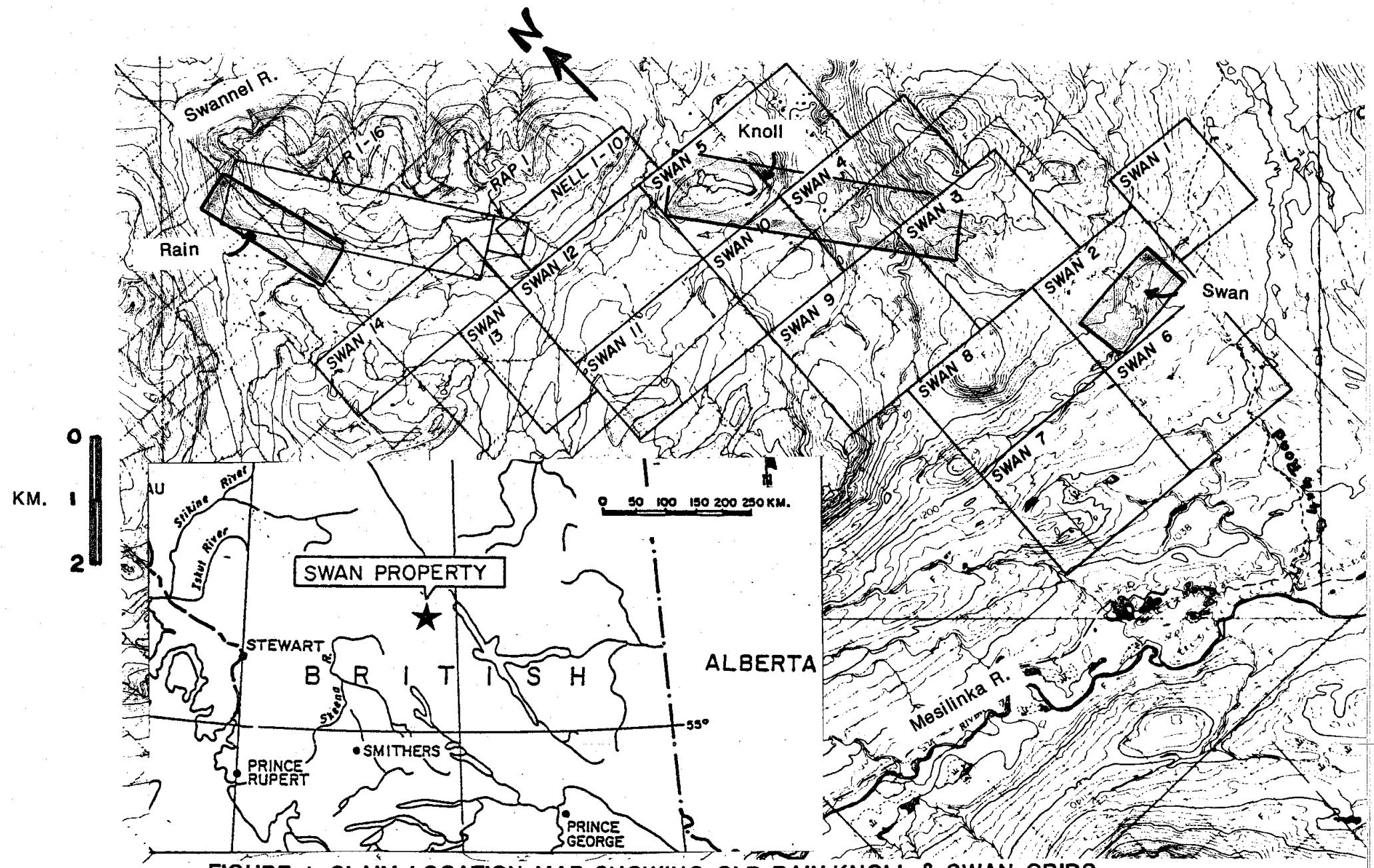
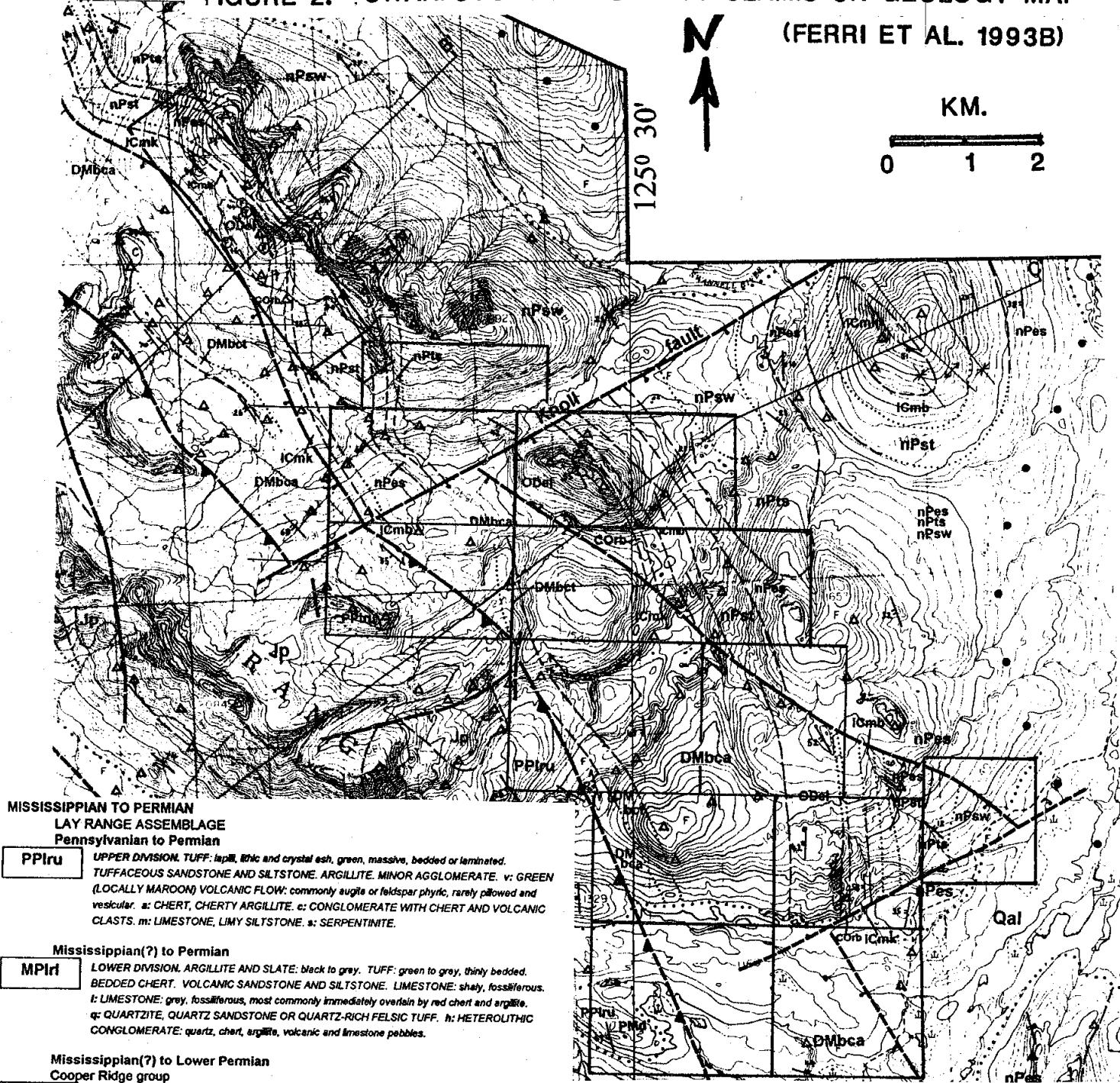


FIGURE 2: SWAN/CYGNET PROPERTY CLAIMS ON GEOLOGY MAP

(FERRI ET AL. 1993B)



**CAMBRIAN**  
Lower Cambrian  
ATAN GROUP  
MOUNT KISON FORMATION

**ICmk** LIMESTONE: grey to white and mottled, recrystallized, thin, wavy, indistinct and discontinuous bedding, slightly argillaceous and may be dolomitized, generally well bedded at bottom and more massive towards top.

**MOUNT BROWN FORMATION**

**ICmb** SANDSTONE, IMPURE QUARTZITE: grey brown to maroon, moderately to thickly bedded.  
INTERLAYERED WITH SILTSTONE AND PHYLLITE: dark grey to grey green, thinly to thickly bedded.  
MINOR LIMESTONE NODULES.

**NEOPROTEROZOIC**  
INGENIKA GROUP  
STELKUZ FORMATION

**nPst** PHYLLITE, SCHIST AND IMPURE QUARTZITE: green-grey, crenulated. LIMESTONE: white, honey coloured to bluish-grey, clean with thin micaceous partings. PHYLLITE, SLATE AND SILTSTONE: dark blue-grey to black, graphitic, locally contains biotite and garnet.

**ESPEE FORMATION**

**nPes** LIMESTONE: locally dolomitic, dark grey, grey to white mottled, thinly to moderately bedded, locally white marble.

**TSAIDZ FORMATION**

**nPts** SLATE, PHYLLITE: greenish grey to grey. INTERLAYERED WITH LIMESTONE TO CALCAREOUS PHYLLITE: both thinly bedded. LIMESTONE: blue-grey, impure and laminated. LESSER SANDSTONE, SILTSTONE: green-grey, feldspathic wacke; locally contains biotite.

**SWANNELL FORMATION**

<b>CLAIM NAME</b>	<b>TENURE NO</b>	<b>UNITS</b>	<b> DUE DATE</b>
-------------------	------------------	--------------	------------------

Swan 1	308212	12	March 17/96
Swan 2	308213	16	March 16/97
Swan 3	308214	16	March 16/96
Swan 4	308215	15	March 18/96
Swan 5	308216	18	March 19/97
Swan 6	316185	16	Feb. 17/97
Swan 7	316186	20	" "
Swan 8	316187	20	" "
Swan 9	316188	20	Feb. 18/97
Swan 10	316189	9	Feb. 19/97
Swan 11	316190	15	" "
Swan 12	316191	15	Feb. 20/97
Swan 13	316192	8	" "
Swan 14	316193	12	" "
Nell 1-10 incl. 308235-36 incl. 10 March 19/97			
Rap 17	312616	1	Aug. 16/97
R1-16 incl. 308219-34 incl. 16 March 19/97			

#### 4. HISTORY

The area was prospected in the 1960's by Cominco Ltd. ( A.B. Mawer) whose work discovered most of the known showings. Some of the showings were subsequently trenched by ABM. During 1972 SEREM Ltd. carried out a regional Pb/Zn stream sediment geochemical program throughout the Omineca Mountains. This led to the staking of 3 small properties (Swan, Burn-now Knoll, and Rain). In 1973 SEREM conducted programs of line cutting, soil geochemistry, geological mapping, trenching and ground geophysical (horizontal shootback EM) surveys on each property and in 1974 drilled 13 holes (2,155 feet) on the Rain property. No assessment was filed and the properties were allowed to lapse. The present Swan property covers most of the 3 old properties. In 1992 the area was mapped at 1:50,000 scale by F. Ferri and crew of the B.C. Geological Survey. Limited silt sediment sampling and analysis was undertaken as part of this program.

#### 5. 1993 WORK

##### A. Objectives

The objectives of the 1993 work were to: i) Examine and assess the known showing areas. ii) Examine and assess the mapped areas of Gilliland Tuff on the Swan property for any mineral potential.

##### B. Work

Cominco 1993 work included a detailed soil geochemical and mapping grid on the Swan and contour soil geochemistry and recce geology on the Rain, Knoll and Gilliland Tuff areas. A regional silt sampling program was also undertaken on the property.

Work on the Swan grid (Plate 4,5,6) consisted of blazing and flagging a one kilometre topofil and compass controlled base line at a 055° bearing and subsequently running geochemical sample lines at 100 metre intervals to the "north" (325°) and "south" (145°) of the base line for 500 metres taking samples every 50 metres. The geochemical lines were subsequently geologically mapped. The grid was designed to cover an area along strike from the old showings and trenches in which previous work had shown high soil geochemical values in lead and zinc.

Work on the other areas of the Swan claims (Plates 1-3) consisted of geological traverses designed to provide as much data as possible within a limited time frame and soil geochemical traverses designed to provide adequate sampling of any down slope dispersion from known showings or favourable strata. Two areas of old trenching on the Rain and Swan claims (Plate 7 & 8 resp.) were also mapped in detail and resampled.

In total the geochemical sampling produced: 254 soil samples on the Swan Grid; 387 soil samples on the rest of the Swan property and 23 silt samples on the Swan property.

## 6. GEOLOGY

### A. General

The general geology of the Swan and Rap claims consists of sedimentary rocks ranging in age from upper Proterozoic through to upper Devonian that lie within the Cassiar Terrane a portion of the ancestral North American continental margin displaced by movement on the Tintina Fault. Plates 1A and 1B show the geology mapped on the Swan at a 1:10,000 scale. Recent mapping by Ferri (1993a,b) has defined a number of new stratigraphic units. There is some controversy about some of the unit definitions and also about the need in some instances for new terminology inasmuch as there are some considerable similarities between these lithologies and those of previously defined units in the McDame area (Gabrielse 1963). Consequently in the geological mapping the older names for much of the stratigraphy have been used with the more recent names of Ferri (1993a,b) presented in brackets. This practice is continued within the text of this report. Figure 2 shows the geology of the Swan area taken from Ferri (1993b) with the outline of the claims superimposed.

The stratigraphic column accompanying the geologic maps describes most of the rocks encountered by Cominco to date in the Swan area. Most of the stratigraphic column is composed of carbonates with lesser shales that are often relatively indistinguishable from each other and commonly lack age-diagnostic fossils. The generally heavily forested and till covered nature of the country also results in a low percentage of outcrop and few continuous stratigraphic sections. Consequently mapping often results in some geological uncertainties. Certain lithologies and stratigraphic units are however particularly diagnostic and have been relied on extensively in the mapping. They include:

- i) the presence of well indurated somewhat micaceous quartzites below a thick carbonate section generally indicates the Boya (Mount Brown) Fm of the Atan Group (Lower Cambrian)
- ii) a thin (5-10m) horizon of limestone nodules in a sericitic mudstone matrix is identifiable over a wide area at the top of the Boya (Mount Brown) Fm and at the base of the Rosella Fm. (Mount Kison). This unit is often recessive but where present clearly defines the top of the Boya (Mount Brown) Fm.
- iii) the Rosella (Mount Kison) Fm. is composed of an assortment of carbonates ranging from very light coloured, textureless limestones and their dolomitized equivalents to variably argillaceous limestones and calcareous shales often bioturbated and oolitic. They resemble to varying degrees carbonates in the underlying Proterozoic and overlying Silurian (middle Ordovician to lower Devonian?) Sandpile (Echo Lake) Group. Occasionally, however, throughout the section Archaeocyathids are recognized that clearly define the carbonates as Rosella (Mount Kison) Fm.
- iv) the Sandpile (Echo Lk) Gp is a thick succession of bedded dolomites or less commonly limestones in which no diagnostic fossils have been found to date in the Swan area. Portions

of the stratigraphy display characteristics typical of peritidal sequences including fenestral, cryptalgal and oncologic/oolithic textures that seem to be unique to the Sandpile (Echo Lake) Gp. Accompanying and seemingly related to the algal features are peculiar silica ribs and irregular forms that also are confined to the Sandpile (Echo Lk.) Gp.

v) Black, fetid carbonates distinguish parts of the lower Devonian McDame (Otter Lakes) group and are clearly identifiable as such by the presence of two hole crinoids, amphipora, stromatoporoids and Devonian corals.

vi) the lower part of the Earn (Big Creek) Gp. is characterized by flaggy, planar laminated, very siliceous, distinctly blue-grey weathering mudstones not only on the Cassiar Platform but throughout the Selwyn Basin.

vii) Ferri has recognized a succession of basaltic to rhyolitic tuffs and agglomerates with some intercalated mudstones and limestones in the upper part of the Earn (Big Creek) Gp. that were formerly grouped with the allochthonous Lay Range Assemblage of the Slide Mountain Terrane. These rocks are recognizable as a distinctive unit on the Swan property.

The time/stratigraphic relationships at i) the base of the Sandpile (Echo Lk.) Gp. and ii) at the base of the Earn Gp. are not well understood.

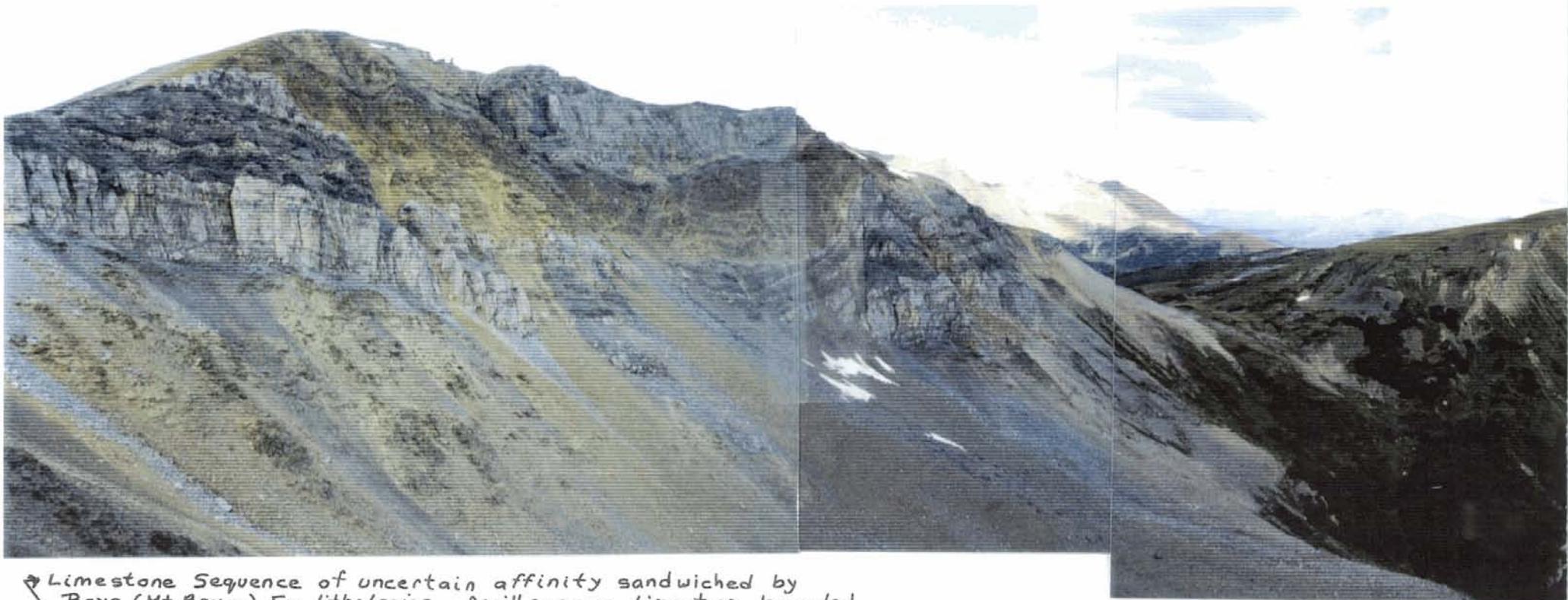
The Silurian (Middle Ordovician to Lower Devonian?) Sandpile (Echo Lk.) Gp. lithologies lie on Lower Cambrian Rosella (Mt. Kison) Fm. carbonates and extend upwards to the upper Devonian to Mississippian Earn (Big Creek) Gp.. This represents a substantial time span for a dominantly shallow water carbonate succession. Elsewhere, regionally, the Sandpile (Echo Lk.) Gp. lies immediately above rocks of disparate but often younger age than on the Swan property including Ordovician strata (as indicated by graptolites) and Middle Cambrian strata (as indicated by trilobites). This data suggests that there is a significant disconformity between Sandpile (Echo Lake) Gp. and underlying rocks. Such a time/depositional gap may be explainable by i) an unconformity or ii) regional thrusting.

The Earn Group lies above the Sandpile (Echo Lk.) Gp. rocks on most of the property. The contact of these two rocks is mapped as a normal fault in much of the area however in some instances it is mapped as a conformable contact (west of the Swan Grid). The geology here seems peculiar inasmuch as the lower Devonian McDame (Otter Lk.) Gp. carbonates appear to be absent and the Sandpile (Echo Lk.) Gp. appears much thinner than normal. Evidence regionally suggests that there may be an unconformity at the base of the McDame (Otter Lk.) Gp.. with some substantial facies variations in the McDame Fm. marking a tectonic differentiation of the former regionally extensive, Sandpile (Echo Lk.) Gp. carbonate platform rocks into localized basinal and platformal settings. Such an unconformity and lithofacies variations may explain some of the relationships on the Swan property.

## B. Detailed Geology

### i) Rain Area Geology

Plate 1B presents the geological mapping undertaken on the Rain. The Rain geology consists of a thin interval of Rosella (Mt. Kison) Fm. carbonates exposed along the high point of a prominent ridge line and forming a dip slope that falls away to the southwest from the ridge line. On the backside (ie northeast side) of the ridge an excellent section of underlying Boya (Mt Brown) Fm is exposed overlying upper Proterozoic sediments of the Ingenika Gp.. The Rosella (Mt. Kison) Fm. consists of a thin interval (5-10 m.) of black argillaceous, thinly bedded and platy limestones succeeded by about 30 to 40 metres of lighter grey burrowed



Limestone Sequence of uncertain affinity sandwiched by  
Boya (Mt Brown) Fm. lithologies. Argillaceous limestone bounded  
by cleaner limestones - Thrust emplaced wedge? Unusual limestone  
within Boya Fm.?

Uppermost Boya (Mt. Brown) Fm.  
Distinctive nodular Limestone

Very irregular contact appears  
to cross cut bedding in underlying  
Limestone unit - Thrust Fault?

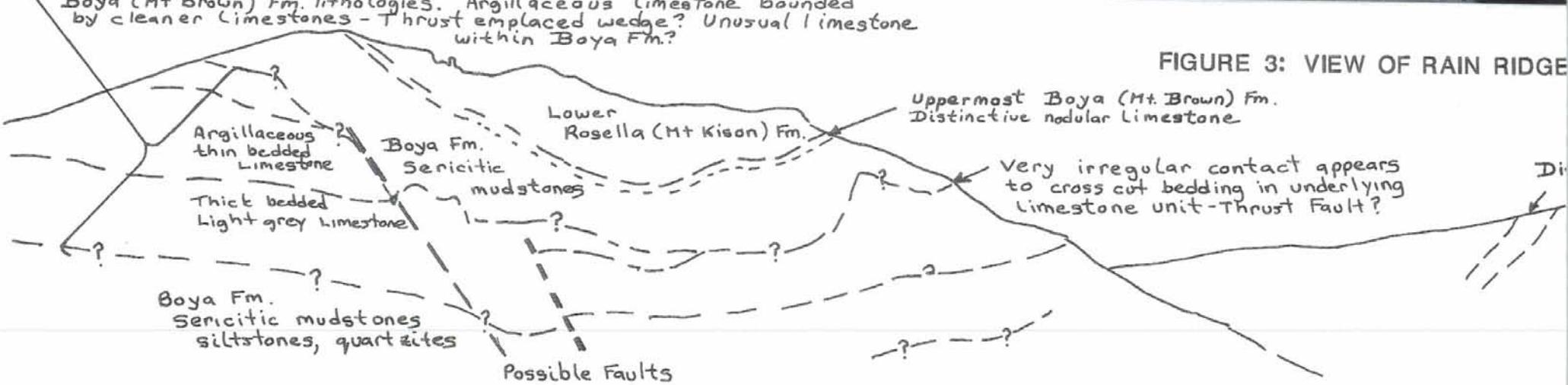


FIGURE 3: VIEW OF RAIN RIDGE WITH GEOLOGY SHOWN

FIGURE 3: VIEW OF RAIN RIDGE

limestones that periodically have lenses of moderately fossiliferous carbonate with some carbonate clasts. Archaeocyathids are evident in some of these fossiliferous areas. Patches of coarsely dolomitized carbonate occur in the burrowed lithology and may reflect differential dolomitization of more permeable areas including the fossiliferous hash lenses. These dolomitized lenses weather a distinctive orange red. While no sulphides were recognized in the dolomites except low on the slope around old Cominco/Serem trenches anomalous soil geochemistry may indicate that there are low levels of anomalous lead,zinc in the dolomites (see mineralization, geochemistry below).

The Rain section has been highlighted by a photograph and discussion by Ferri (1993a). Figure 3 duplicates Ferri's photograph of the back (eastern) side of the Rain ridge but places a different interpretation on the geology. No Sandpile (Echo Lk) Gp. rocks are believed to be present because: i)Archaeocyathids occur in the ridge top carbonate and ii) the distinctive nodular limestone marker at the top of the Boya (Mt Brown) Fm underlies this limestone. As a consequence of this all of the section below the ridge top limestone is believed to be part of the Boya Fm, however there is an interval of limestones within this section that is not typical of Boya. This limestone can also be traced on the southwest slope of the ridge and seems to be a continuous stratigraphic unit. The sericitic mudstone that overlies this limestone shows variable thicknesses and a seemingly discordant contact with the underlying limestone. Similarly the limestone itself shows very variable thicknesses in what seems to be a well bedded lithology. It is possible that the limestone is bounded by low angle faults that have introduced a slice of Rosella (Mt. Kison) Fm. into the Boya (Mt Brown) Fm. If this is so then it marks an earlier structural event than the subsequent Laramide deformation that has folded and faulted the limestone as a stratigraphic entity.

At the foot of the hill and generally not well exposed are black, siliceous mudstones of the Earn Gp.. Some pebbles appear to be present in the mudstones in the trench mapping and may be diamictites marking a debris flow. Considerable stratigraphic section is missing between the Earn (Big Creek) Gp. and the Rosella (Mt Kison) Fm and the contact is believed to be a fault which is also the interpretation shown by Ferri.

A number of trenches expose mineralization toward the base of the southwest slope of the hill. The best of these was mapped and sampled by Bruce Mawer and is shown in Plate 7.

### ii) Knoll Area Geology

The Knoll geology is shown on Plate 1A . The Knoll consists of a very prominent 300 metre high hill elongate in a northwest direction. The northeast side is very steep while the southwest side is of somewhat gentler slope that is close to a dip slope. The upper portion of the hill is dominated by a dolomite that is 60 to 100 % silicified into a blue grey, chert-like rock. Remnant patches and areas of dolomite confirm the original carbonate character of the rock and also show fenestral and cryptalgal laminae characteristic of the Sandpile ( Echo Lk.) Gp. The silicified Sandpile lithologies overlie lighter limestones and dolomites that are thought to probably be Rosella (Mt Kison) Fm. though no archaeocyathids were identified. In the stream valley on the northwest side of the Knoll quartzites were mapped that may be Boya (Mt. Brown) Fm or perhaps older quartzites.

### iii) Swan Area Geology

Plate 1A portrays the geology of the Swan area at a 1:10,000 scale while Plate 4 shows more detailed mapping at a scale of 1:2500. The geology consists of north trending stratigraphy dipping at 40 to 50° to the west. Light coloured limestones of the Rosella (Mt. Kison) Fm. with some shaly carbonates overlie quartzites and sericitic mudstones of the Boya

(Mt Brown) which in turn overlie carbonates and clastics of the Ingenika Gp. Overlying the Rosella (Mt. Kison) carbonates are dolomites that are intensely silicified with 20 to 100 % blue grey to white quartz replacing the carbonate. Unlike the Knoll these carbonates show no textures typical of the Sandpile (Echo Lk.) Gp. They are tentatively mapped as Sandpile Gp. because of their silicified character but it is possible that they are silicified Rosella (Mt. Kison Fm.). Locally the Rosella Fm. limestones are dolomitized to medium grained dolomite with patches of ferroan carbonate. This dolomitization is most common proximal to areas of faulting and is often found in association with mineralization (see below).

#### iv) Gilliland Tuff

Plates 1A and B show the geology encountered along several traverses designed to criss cross this volcanic unit as mapped by Ferri. The rocks encountered ranged from agglomerate through lapilli tuff to ash tuff and crystal tuffs. Compositionally the rocks range from basalts to rhyolites. Some limestones and shales interbed with the volcanics which sometimes show a degree of sedimentary reworking. Appendix 2 presents a number of whole rock determinations on samples of the volcanics along with multi-element ICP analysis.

### C. MINERALIZATION

Numerous mineralized showings occur on the Swan claims. For the most part they lie in the Rosella (Mt Kison) Fm. and are generally associated with dolomite and ferroan carbonate altered limestones. They commonly seem to be adjacent to faults and consist of veins, stockworks and more irregular replacement of dolomite by dominantly sphalerite, lesser galena plus or minus pyrite and barite. Some of the more significant showings are discussed below:

i) RAIN - Mineralization occurs associated with a restricted part of Rosella (Mt. Kison) Fm. stratigraphy on the lower elevations of the southwest facing dip slope. There is some suggestion that the favourable stratigraphy is particularly fossiliferous with fossil hash zones including Archaeocyathids showing up in several of the trenches. The stratigraphy is offset by several faults normal to the bedding. The showings cover a strike length of 1.5km. Bruce Mawer describes the showings as "stratabound ferrodolomite zones in part controlled by the cross cutting faults. The best zone (south Rain) was drilled by Serem along a strike length of approximately 800 metres. Along this strike length the surface has scattered mineralized float of barite-smithsonite-galena with grey silica some of which has good grade. Plate 7 presents a map of the best trench as drawn by Bruce Mawer with assays from a number of chip samples.

ii) KNOLL - Several showings occur on the northwest face of the Knoll. The most prominent consists of a 10x 15 m. area of Rosella (Mt. Kison) Fm. carbonates cut by a number of irregular barite + galena with minor sphalerite and smithsonite veins up to 0.5m. wide. Some of the veins are located along a fault along which the rock is brecciated and dolomitized. The veins comprise 50-95% white barite 1-4% fine to medium grained galena and 1-2% orange, brown sphalerite. A semi-continuous chip sample over 3.5 m. of the best mineralized interval (WR 93-046) assayed 2.2% lead 3.0% zinc and 39.9 g/t silver. Lower on the slope an outcrop of ankeritic and calc spar rich Rosella limestone reported to host 1-2% disseminated sphalerite analyzed from a grab sample of the best 40 cm. of mineralization 1.3% lead and 17.2% zinc (ICP - WR 93-044). On the southeast face of the Knoll float of dolomitized Rosella hosts disseminated sphalerite, galena and variable barite.

iii) CRAG - The Crag is a small rugged hill about two kilometres southeast of the Knoll. Bruce Mawer reports the mineralization to consist of scattered ferrodolomite zones in Rosella (Mt Kison) Fm. limestone, with weak sphalerite-galena mineralization in outcrop and in the hand

trenches. The mineralization is very erratic and low grade.

SWAN - Numerous showings are present most of which appear to be stringers, veins, disseminations and occasionally more massive replacement patches of sphalerite with lesser galena and sometimes pyrite in Rosella (Mt Kison) limestones altered to ferrodolomite. Most appear to be close to faults. Bruce Mawer cleaned out, sampled and mapped one old hand trench approximately 2-300 metres north of the "Main" showing. Plate 8 is a map of the trench with the chip sample assays. Bruce Mawer describes the mineralization as "patchy but high grade (50 cm. of massive sphalerite) with other stringers of sphalerite over 6.0m. of exposed ferrodolomite. This zone appears to be controlled in part by converging fault structures and may be limited".

The lead zinc anomaly on the 1993 grid lies in an area where one large outcrop shows stringers of sphalerite - galena mineralization however the talus covered slope shows numerous pieces of limestone and dolomite showing stringers, disseminations and stylolite controlled sphalerite/galena. In addition numerous pieces of higher grade oxidized float are present such that Bruce Mawer comments " there is more float material on the talus slope than can be envisioned as coming from the small showings located in outcrop above - there is a possibility of additional mineralization beneath the talus."

#### BARITE AREA

A day was spent by Bruce Mawer investigating an area of barite veins reported by Serem in the Devonian southeast of Knoll. The description below stems from this work. Interesting showings occur in the basal part of the Earn (Big Creek) Group where there are several thick (4-10 m.) interbeds of dark grey, medium to coarse crystalline bituminous or argillaceous dolomite (some fossil hash) in black, fissile, siliceous black mudstone and siltstone. Barite is present as medium to coarse crystalline masses sometimes bladed and appears to fill or replace dolomite breccia accompanied by some pyrite and trace sphalerite. Approximately four metres stratigraphically above the barite there is a sphalerite enriched bituminous dolomite about 30-40 cm. thick. The sphalerite is disseminated, lumpy and patchy and appears to be controlled in part by a bedded fault along the upper part of the creek.

Although Ferri et al maps this as (Earn Gp. Big Creek Gp.(1993), it could be a more argillaceous phase of the (McDame) Otter Lake Fm.

#### 7. GEOCHEMISTRY

##### Method

The soil sampling lines were run along preselected elevations and samples were taken at 100 metre intervals along the lines. At each sample location a small pit was dug with a shovel and a 300 gram sample of the B soil horizon was retrieved and placed in a kraft paper bag. The bag was annotated with the grid coordinates and notes were taken of the colour, nature and surroundings of the sample and sample site.

Silt samples were taken by landing the helicopter close to sites preselected on the topographic maps, locating areas of fines in or adjacent to the stream bed and, using a trowel, filling kraft paper bags with the fines. The heavily vegetated and often deeply incised streams prevented access to some sites.

All the samples were shipped to Cominco's Exploration and Research Laboratory at 1482 E. Pender St. in Vancouver. There the samples were dried, sieved and a 1 gram portion of the -

80 mesh fraction was extracted. This sample was subsequently digested by reverse aqua regia and presented to the ICP. machine for analysis of a 27 element suite.

### Results

The soil and silt analyses are presented in Appendix 2. The values for copper, lead, zinc and silver are plotted on Plates 2A, 2B, 5 and 6. Very high lead (100 - 5000ppm) zinc (200 - 5000 ppm) and silver (0.4 - 15 ppm.) in soil values are found in association with the known mineralization on the Rain and the Knoll. The limited soil cover and the carbonate nature of the bedrock in this environment fix the metals close to source and the metal values particularly of lead and silver are more likely to be an accurate reflection of the grade in bedrock than in other geomorphic and geological environments. Consequently it is thought that most of the anomalous geochemistry can be attributed to the known mineralization.

On the Rain, contour soils give anomalous values that are in part upslope of the known mineralization. This may represent glacial dispersion or it is possible that the gossanous weathering dolomitized lenses higher on the hill carry some anomalous but low amounts of lead and zinc.

On the Swan detailed grid a well defined coincident lead (500-8000ppm) and zinc (1000-8000ppm) anomaly covers a roughly circular area of 200 to 300 metres in diameter. The mineralization in the area has been described above and there is a broad talus sheet in this area that shows sufficient mineralized float to suggest that some mineralization may be concealed beneath the talus.

Soil sampling traverses were taken criss crossing the mapped occurrences of Gilliland Tuff. The northern samples did not return any anomalous results but moderately anomalous values for copper, lead, zinc and silver are evident in scattered samples from the soil traverses on Swan 8 and 9 claims.

Silt anomalies were taken on the Swan property by helicopter to provide a broad, unbiased assessment of the potential. A number of planned sites were not accessible because of steep valleys and thick bush however in general sufficient samples were acquired to provide a good overview. Anomalous silt samples were encountered in several areas. They include i) a drainage on the eastern edge of Swan 12 ii) three anomalous silts from drainages near the southern boundary of Swan 9 and an anomalous silt in Swan 3 upstream from the Devonian barite, sphalerite mineralization described above.

### 8. CONCLUSIONS

It is concluded that most of the Swan property showings have a significant structural control and while locally high grade are unlikely to have sufficient combination of grade, continuity and size as to make an economic ore body. The Swan grid geochemical anomaly overlies in large part talus that might mask significant mineralization although the vein, stringer and replacement character of mineralized float in the talus is not encouraging.

The occurrences of sphalerite and barite in Devonian sedimentary rocks may have potential for more stratabound mineralization though again there appears to be some association with faulting.

The anomalous stream silts and occasional soils on claims Swan 8 and 9 in the vicinity of the Gilliland Tuff outcrops suggests some potential for mineralization within this unit or perhaps in younger stratigraphy to the west.

## REFERENCES

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## **APPENDIX I**

**STATEMENT OF  
TOTAL EXPENDITURES SWAN 1-14,RAP 17,NELL1-10,R1-16**

**PERIOD JULY 20 - JULY 27**

GEOLOGY

Salaries	\$18,518
Contract	2,700
Expense Accts.	2,695
Supplies	<u>271</u>
	\$24,184

## GEOCHEMISTRY

Analyses	\$6,767
Supplies	<u>253</u>
	7,020

## **TRANSPORTATION**

Helicopter	\$19,838
Fixed Wing	1,319
Vehicle	1,935
Fuel	494
<u>Freight</u>	<u>233</u>

## **DOMICILE AND CAMP COSTS**

11.481

## DRAFTING AND REPRODUCTION

696

**TOTAL** \$ 67 200

**APPENDIX II**

**GEOCHEMICAL ANALYSIS**

CYGNET--WD

JOB V 93-0432S

Report date 23 AUG 1993

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	
S9329780	222751*14 2B 41	20	284	1611	<.4	16	214	11	9	73	1.85	<2	20	<5	<5	24	<2	<2	89	8	6	1572	1.47	.01	.94	8.30	.01	.05
S9329781	222752*14 2B341	10	6	128	<.4	<2	117	1	4	27	2.02	<2	34	<5	<5	52	<2	<2	9	<2	<2	63	.31	<.01	1.38	.19	.01	.03
S9329782	222753*14 1B231	3	17	382	<.4	13	100	2	3	26	1.36	<2	25	<5	5	26	<2	<2	34	28	16	96	.15	.02	.99	4.63	.01	.02
S9329783	222754*14 2B 31	27	<4	114	<.4	4	166	<1	11	49	2.75	<2	36	<5	<5	62	<2	<2	11	2	2	381	.76	.05	1.96	.30	.02	.03
S9329784	222755*14 2B 31	12	5	66	<.4	<2	82	<1	9	27	2.08	<2	32	<5	5	57	<2	<2	10	<2	<2	278	.62	.04	1.20	.41	.01	.04
S9329785	222756*14 2B 31	12	7	113	<.4	<2	80	1	14	23	2.20	<2	32	<5	<5	52	<2	<2	13	<2	<2	789	.40	.03	1.01	.43	.01	.05
S9329786	222757*14 1B431	12	9	84	<.4	<2	121	<1	10	50	1.88	<2	34	<5	<5	42	<2	<2	8	2	3	359	.58	.03	1.40	.33	.01	.04
S9329787	222758*14 2B 41	28	25	173	<.4	4	185	<1	13	73	1.79	<2	25	<5	5	35	<2	<2	25	10	12	1526	1.39	.01	1.05	4.30	.01	.05
S9329788	222759*12 2B343	28	84	392	<.4	3	213	2	13	61	2.30	<2	51	<5	6	47	<2	<2	23	8	4	992	2.25	.01	1.48	3.62	.01	.07
S9329789	222760*14 2B 32	8	74	1005	<.4	3	857	7	10	34	4.36	<2	46	<5	<5	58	<2	<2	13	14	8	1608	1.67	.03	1.63	2.62	.01	.04
S9329790	222761*14 2B342	6	30	329	<.4	<2	79	1	10	22	2.15	<2	36	<5	<5	51	<2	<2	7	<2	<2	309	.44	.05	1.13	.24	.01	.03
S9329791	222762*14 2B 32	15	88	872	<.4	<2	127	2	11	53	3.38	<2	40	<5	6	48	<2	<2	9	11	9	760	.54	.03	1.67	.64	.01	.04
S9329792	222763*14 2B 31	8	104	650	<.4	6	125	4	11	57	2.79	<2	40	<5	<5	43	<2	<2	11	8	7	680	.31	.03	1.66	.67	.01	.02
S9329793	222361* 211B	13	60	298	<.4	<2	522	1	12	24	2.27	<2	24	<5	7	35	<2	<2	17	2	2	906	.43	.03	1.13	.90	.01	.03
S9329794	222362* 212B	7	97	242	<.4	<2	327	1	13	13	2.66	<2	16	<5	<5	28	<2	<2	8	<2	<2	1371	.18	<.01	.86	.34	.01	.05
S9329795	222363* 212Y 2	11	26	192	<.4	<2	245	1	17	27	3.50	<2	24	<5	<5	33	<2	<2	9	<2	<2	605	.49	.02	1.30	.34	.01	.05
S9329796	222364* 212B	28	33	253	<.4	4	408	2	22	47	3.43	<2	27	<5	<5	20	<2	<2	22	5	4	1812	.67	<.01	1.52	.92	.01	.03
S9329797	222365* 212B 21	9	25	110	<.4	5	199	<1	17	15	3.63	<2	17	<5	<5	29	<2	<2	24	<2	<2	1062	.20	<.01	.89	.78	.01	.05
S9329798	222366* 212B	11	69	336	<.4	<2	363	1	18	25	2.73	<2	34	<5	<5	26	<2	<2	14	<2	3	584	.45	<.01	1.18	.44	.01	.08
S9329799	222367* 3 K 3	23	33	191	<.4	<2	3407	3	57	109	10.56	2	29	<5	7	26	<2	<2	55	4	2	27623	.41	<.01	.67	1.87	.01	.02
S9329800	222368* 3 K 3	77	32	210	<.4	3	2196	2	14	130	2.71	<2	100	<5	<5	35	<2	<2	50	23	11	627	.70	.01	1.99	2.51	.01	.06
S9329801	222369* 212B	108	27	113	<.4	2	1458	2	13	104	1.94	<2	56	<5	<5	42	<2	<2	26	37	22	317	.64	.03	1.21	1.18	.01	.05
S9329802	222370* 211B 2	13	9	92	<.4	<2	555	<1	8	47	1.65	<2	26	<5	6	39	<2	<2	14	<2	<2	256	.70	.01	1.04	.46	.01	.06
S9329803	222371* 2 2B	3	16	42	<.4	<2	64	<1	4	7	1.48	<2	15	<5	5	27	<2	<2	48	<2	6	46	.18	.01	.76	.53	.01	.06
S9329804	222372* 211B 2	3	18	31	<.4	<2	49	<1	5	9	2.32	<2	15	<5	<5	19	<2	<2	11	<2	14	93	.23	<.01	.93	.15	<.01	.04
S9329805	222373* 212B	19	21	48	<.4	<2	121	<1	14	46	2.25	<2	36	<5	<5	33	<2	<2	35	7	16	631	.61	.02	1.46	.63	.01	.06
S9329806	222374* 212B	17	34	73	<.4	11	209	<1	14	40	2.27	<2	40	<5	6	30	<2	<2	20	4	8	526	.59	.01	1.38	.45	.01	.06
S9329807	222801* 212B	21	120	82	<.4	15	222	<1	13	58	2.17	<2	36	<5	<5	35	<2	<2	10	2	3	353	.80	.02	1.20	.41	.01	.05
S9329808	222802* 212R	11	54	119	<.4	<2	323	<1	14	36	2.61	<2	36	<5	<5	49	<2	<2	13	2	3	822	.46	.02	1.30	.52	.01	.05
S9329809	222803* 211B	67	81	147	<.4	6	244	<1	24	117	3.48	<2	42	<5	5	38	<2	<2	27	15	12	868	1.65	.02	1.25	1.77	.01	.08
S9329810	222804* 212B 2	28	18	146	<.4	<2	163	<1	19	58	2.89	<2	55	<5	<5	47	<2	<2	14	5	6	1210	.73	.02	1.61	.37	.01	.12
S9329811	222805* 222G	65	9	68	<.4	<2	90	<1	16	78	2.59	<2	38	<5	9	41	<2	<2	43	7	10	495	1.41	.02	1.35	1.08	.02	.08
S9329812	222806* 222B	91	71	160	<.4	11	514	1	17	62	3.50	<2	34	<5	<5	18	<2	<2	33	12	6	636	.56	<.01	1.24	1.40	.01	.05

LAB NO.	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K	
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm												
S9329813	222807* 222B	20	59	127	<.4	4	210	<1	17	31	4.04	<2	21	<5	5	22	<2	<2	16	16	15	776	.29	<.01	.92	.83	.01	.07	
S9329814	222808* 222B	6	48	90	<.4	<2	159	<1	23	19	2.97	<2	24	<5	7	33	<2	<2	13	<2	2	1818	.28	.02	.91	.37	.01	.08	
S9329815	222809* 221B 2	20	114	202	<.4	<2	391	1	24	33	3.12	<2	26	<5	<5	28	<2	<2	12	3	3	1644	.40	.02	1.03	.52	.01	.09	
S9329816	222810* 222B	12	129	542	<.4	3	281	1	19	30	3.44	<2	34	<5	6	46	<2	<2	10	<2	<2	612	.50	.02	1.32	.41	.01	.05	
S9329817	222811* 21B	9	30	385	<.4	5	414	4	11	15	2.31	<2	21	<5	<5	41	<2	<2	11	<2	2	329	.34	.02	.98	.65	.01	.04	
S9329818	222812* 222B	11	122	362	<.4	<2	616	4	19	33	2.98	<2	33	<5	<5	58	<2	<2	13	2	2	1049	.58	.03	1.48	.68	.01	.07	
S9329819	222813* 221B 2	6	739	258	<.4	<2	310	2	10	17	1.91	<2	19	<5	<5	40	<2	<2	8	<2	2	801	.33	.01	.87	.35	.01	.10	
S9329820	222814* 222B 2	4	20	179	<.4	4	264	2	7	10	1.87	<2	13	<5	5	25	<2	<2	5	<2	<2	196	.18	<.01	.70	.20	.01	.06	
S9329821	222815* 222B	15	16	125	<.4	<2	927	<1	15	43	2.20	<2	25	<5	6	35	<2	<2	18	2	2	1034	.51	.01	1.08	.56	.01	.11	
S9329822	222816* 221B	9	251	1436	<.4	<2	550	21	15	47	2.63	<2	34	<5	6	43	<2	<2	11	2	2	3	1288	.56	.01	1.21	.58	.01	.05
S9329823	222817* 221B 2	3	25	24	<.4	<2	357	<1	3	9	1.31	<2	12	<5	<5	31	<2	<2	15	<2	2	79	.15	.01	.40	.25	.01	.08	
S9329824	222818* 223B 2	74	71	350	<.4	10	623	3	19	64	3.06	<2	32	<5	<5	17	<2	<2	44	7	5	965	.58	<.01	1.18	1.64	.01	.05	
S9329825	222819* 222B	13	82	536	<.4	<2	233	1	26	55	4.05	<2	42	<5	<5	54	<2	<2	10	2	2	1190	.80	.03	1.81	.33	.01	.04	
S9329826	222820* 3 K 3	110	25	208	<.4	2	442	1	7	62	1.52	<2	49	<5	5	17	<2	<2	96	5	3	489	.85	<.01	.75	4.26	.02	.03	
S9329827	222821* 222B	10	33	296	<.4	3	310	1	21	49	3.36	<2	57	<5	<5	50	<2	<2	16	<2	2	972	.73	.03	1.32	.50	.01	.05	
S9329828	222822* 221B 2	40	149	142	<.4	<2	227	<1	28	83	3.38	<2	50	<5	<5	46	<2	<2	16	8	12	1012	1.40	.01	1.60	.94	.01	.06	
S9329829	222823* 221B	19	9	69	<.4	<2	129	<1	11	53	2.06	<2	44	<5	6	40	<2	<2	29	7	16	301	.93	.03	1.49	.60	.01	.03	
S9329830	222824* 221B 2	14	32	52	<.4	3	70	<1	,22	42	3.60	<2	26	<5	<5	26	<2	<2	28	3	8	351	.57	.02	1.52	.37	.01	.02	
S9329831	222825* 221B 2	25	57	189	<.4	6	149	<1	28	128	4.00	<2	80	<5	<5	59	<2	<2	18	<2	<2	959	1.59	.04	1.65	.38	.01	.05	
S9329832	2228241* 222B	7	150	376	<.4	<2	288	1	16	20	2.43	<2	27	<5	5	28	<2	<2	13	<2	2	1106	.27	<.01	.88	.38	.01	.09	
S9329833	2228242* 221B	17	276	624	<.4	<2	224	1	18	59	2.69	<2	51	<5	<5	43	<2	<2	14	5	4	884	.78	.02	1.34	.53	.01	.14	
S9329834	2228243* 221B 21	9	136	1094	<.4	3	315	3	14	27	2.56	<2	20	<5	7	27	<2	<2	7	<2	3	735	.38	.02	.93	.46	.01	.05	
S9329835	2228244* 221B 21	7	752	2158	<.4	<2	393	8	13	25	2.76	<2	16	<5	6	25	<2	<2	11	11	10	1576	.39	.02	1.02	1.25	.01	.04	
S9329836	2228245* 221B 21	8	177	482	<.4	<2	207	1	11	35	1.85	<2	20	<5	5	17	<2	<2	5	6	6	199	.41	<.01	1.16	.40	<.01	.04	
S9329837	2228246* 221B	9	55	156	<.4	<2	82	2	9	53	2.35	<2	27	<5	<5	36	<2	<2	14	10	8	833	2.29	.01	1.14	3.09	.01	.03	
S9329838	2228247* 222B	15	10	110	<.4	6	110	1	13	78	2.56	<2	43	<5	<5	49	<2	<2	10	<2	<2	226	.92	.01	1.47	.48	.01	.04	
S9329839	2228248* 222B 2	8	27	206	<.4	5	96	1	12	29	2.78	<2	33	<5	<5	56	<2	<2	10	2	3	270	.52	.03	1.63	.64	.01	.03	
S9329840	2228249* 221B 2	15	104	703	<.4	11	169	2	23	134	3.38	<2	54	<5	<5	45	<2	<2	10	2	3	1323	1.59	.03	1.85	.43	.01	.03	
S9329841	2228250* 233B 2	33	269	668	<.4	4	743	4	9	44	2.02	<2	40	<5	<5	19	<2	<2	57	6	3	227	.88	<.01	.88	2.73	.01	.03	
S9329842	2228251* 233B 2	21	220	837	<.4	7	287	2	7	47	1.51	<2	38	<5	5	21	<2	<2	76	6	3	142	1.29	<.01	.81	2.75	.01	.03	
S9329843	2228252* 222B 2	9	20	39	<.4	10	79	<1	11	40	7.54	<2	34	<5	7	40	<2	<2	15	14	8	1651	.59	.03	1.35	.79	.01	.02	
S9329844	2228253* 222B	16	12	46	<.4	<2	118	<1	11	37	7.92	<2	46	<5	6	40	<2	<2	13	10	8	1649	.60	.03	1.54	.51	.01	.02	
S9329845	2228254* 222B	11	9	76	<.4	<2	72	<1	11	28	2.40	<2	39	<5	<5	41	<2	<2	20	2	6	325	.70	.03	1.38	.48	.01	.04	
S9329846	2228255* 222B	4	8	49	<.4	<2	79	<1	6	13	2.00	<2	23	<5	<5	43	<2	<2	7	<2	6	102	.35	.03	1.13	.24	.01	.03	
S9329847	2228256* 222B	16	13	51	<.4	<2	102	<1	11	23	2.77	<2	34	<5	<5	50	<2	<2	21	4	8	369	.42	.02	1.61	.60	.01	.03	
S9329848	2228257* 222B 2	15	20	42	<.4	2	47	<1	11	19	3.26	<2	19	<5	<5	27	<2	<2	17	13	32	379	.19	.02	1.06	.35	.01	.03	

AB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	
329849	222358* 211B 2	8	9	46	<.4	<2	48	<1	6	16	2.26	<2	26	<5	<5	43	<2	<2	8	<2	4	101	.40	.03	1.24	.19	.01	.04	
329850	222087*24 2B 32	8	53	141	<.4	<2	135	<1	17	173	3.41	<2	57	<5	<5	17	<2	<2	37	5	3	248	1.72	<.01	.98	.75	<.01	.02	
329851	222088*24 2G 31	20	17	110	.4	<2	150	<1	9	94	1.99	<2	46	<5	5	16	<2	<2	54	6	3	336	.80	<.01	.77	1.46	<.01	.02	
329852	222089*24 2G 32	32	27	79	.5	3	187	1	26	179	2.80	<2	48	<5	<5	18	<2	<2	65	16	12	922	1.97	<.01	.97	2.19	<.01	.02	
329853	222090*24 2R 31	16	33	77	<.4	<2	74	<1	16	102	5.80	<2	42	<5	<5	23	<2	<2	3	<2	2	448	1.36	<.01	.96	.04	<.01	.01	
329854	222091*24 2B 31	4	9	17	<.4	4	79	<1	1	7	1.27	<2	22	<5	<5	22	<2	<2	6	<2	<2	22	.07	<.01	.81	.09	<.01	.01	
329855	222092*24 2G 31	11	17	58	<.4	<2	153	<1	12	33	2.78	<2	24	<5	6	13	<2	<2	29	2	2	315	.40	<.01	.70	.25	<.01	.03	
329856	222093*24 2G 31	7	17	46	<.4	<2	239	<1	7	10	2.10	<2	11	<5	<5	9	<2	<2	40	<2	<2	319	.13	<.01	.69	.80	<.01	.02	
329857	222094*24 2B 31	4	13	22	<.4	<2	103	<1	1	9	1.90	<2	22	<5	5	28	<2	<2	3	<2	2	24	.12	<.01	.81	.03	<.01	.01	
329858	222095*24 2K 32	27	13	274	<.4	28	303	.1	31	341	4.70	<2	37	<5	<5	19	<2	<2	12	6	2	1895	3.28	<.01	.73	.14	<.01	.02	
329859	222096*24 1B 31	16	15	88	<.4	26	202	<1	14	96	4.03	<2	42	<5	<5	21	<2	<2	7	<2	<2	332	1.40	<.01	.77	.10	<.01	.02	
329860	222097*24 2B232	12	14	112	<.4	12	407	<1	8	34	2.72	<2	18	<5	5	16	<2	<2	17	2	<2	134	.46	<.01	.77	.39	<.01	.02	
329861	222098*24 3Y 31	9	12	46	<.4	<2	78	<1	5	20	3.19	<2	23	<5	5	16	<2	<2	3	<2	<2	194	.35	<.01	.97	.02	<.01	.02	
329862	222099*24 2B 31	25	26	113	<.4	<2	200	<1	38	186	4.13	<2	30	<5	<5	13	<2	<2	7	<2	<2	1092	2.05	<.01	.73	.10	<.04	.02	
329863	222100*24 1B 31	3	7	13	<.4	<2	91	<1	1	6	1.49	<2	11	<5	<5	13	<2	<2	<2	<2	<2	70	.07	<.01	.55	.01	<.01	.02	
329864	222101*24 1G231	9	16	25	<.4	<2	45	<1	7	15	1.91	<2	11	<5	7	9	<2	<2	5	<2	<2	310	.16	<.01	.37	.05	<.01	.01	
329865	222102*24 2B 31	3	6	16	<.4	<2	75	<1	3	22	1.25	<2	14	<5	<5	14	<2	<2	2	<2	<2	113	.15	<.01	.73	.02	<.01	.01	
329866	222103*24 2B 31	14	14	53	<.4	2	166	<1	10	38	2.47	<2	21	<5	<5	18	<2	<2	12	<2	<2	405	.50	<.01	.74	.10	<.01	.02	
329867	222301*	4	23	66	130	<.4	5	469	1	8	25	3.25	<2	8	<5	5	9	<2	<2	129	7	7	907	1.36	<.01	.37	4.83	.01	.02
329868	222302*	4	55	21	371	<.4	13	67	4	28	230	2.88	6	24	<5	<5	18	<2	<2	31	9	2	1501	2.49	<.01	.67	.51	<.01	.02
329869	222303*	4	58	20	239	.4	<2	504	4	38	354	2.93	<2	28	<5	6	19	<2	<2	34	8	3	1428	3.91	<.01	.68	.53	<.01	.03
329870	222304*	4	14	35	96	<.4	<2	333	<1	19	175	2.27	<2	14	<5	<5	6	<2	<2	29	5	8	567	1.76	<.01	.63	.74	<.01	.02
329871	222305*	4	53	22	233	<.4	12	361	2	30	255	2.82	2	18	<5	<5	15	<2	<2	40	8	3	939	3.04	<.01	.46	.81	<.01	.02
329872	222306*	4	37	11	125	<.4	8	172	<1	34	324	2.96	<2	31	<5	<5	10	<2	<2	44	6	2	682	4.46	<.01	.41	.82	<.01	.02
329873	222307*	4	50	16	558	1.2	18	216	10	29	429	3.13	<2	50	<5	<5	18	<2	<2	40	8	2	367	3.04	<.01	.33	.79	<.01	.01
329874	222308*	4	50	14	164	<.4	14	355	1	39	398	3.39	<2	54	<5	<5	16	<2	<2	43	8	2	842	5.14	<.01	.52	.85	<.01	.02
329875	222309*	4	32	15	105	<.4	8	130	<1	29	250	2.85	<2	21	<5	6	8	<2	<2	119	7	7	633	3.32	<.01	.40	1.63	<.01	.02
329876	222310*	4	33	11	105	<.4	24	133	<1	35	374	3.03	<2	36	<5	<5	10	<2	<2	32	5	4	620	5.10	<.01	.43	.52	<.01	.01
329877	222311*	4	30	7	73	<.4	9	102	<1	43	525	3.24	<2	50	<5	<5	20	<2	<2	16	5	<2	941	6.37	<.01	.51	.35	<.01	.02
329878	222312*	4	48	12	137	<.4	<2	198	2	26	158	3.42	<2	48	<5	6	36	<2	<2	38	13	4	1504	1.27	<.01	.99	.84	<.01	.02
329879	222313*	4	32	9	74	<.4	15	180	<1	18	170	2.14	<2	47	<5	<5	20	2	<2	21	6	3	456	1.65	<.01	.64	.34	<.01	.02
329880	222314*	4	69	12	263	<.4	14	237	4	26	177	3.99	<2	50	<5	<5	31	<2	<2	47	18	9	3659	1.38	<.01	.74	.93	<.01	.05
329881	222315*	4	160	26	1090	<.4	61	560	22	41	360	4.11	3	118	<5	<5	49	<2	<2	65	120	70	1356	1.41	.01	1.85	1.25	<.01	.06
329882	222316*	4	104	10	283	<.4	8	163	5	20	252	2.59	<2	90	<5	<5	36	<2	<2	84	17	6	2040	1.14	<.01	1.02	1.95	<.01	.05
329883	222317*	4	24	107	1453	<.4	7	276	12	8	67	1.58	<2	54	<5	5	23	<2	<2	153	5	3	484	1.67	.01	.77	2.88	<.01	.02
329884	222318*	4	51	18	135	<.4	5	560	<1	23	75	4.12	<2	78	<5	<5	62	<2	<2	28	12	8	2843	.63	<.01	1.85	.37	<.01	.09

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	
S9329885	222319*	4	146	15	506	2.6	5	621	20	6	232	.85	4	53	<5	11	15	<2	<2	253	14	4	83	.45	<.01	.50	2.91	.01	.05
S9329886	222320*	4	44	27	464	<.4	15	296	1	41	351	2.70	<2	86	<5	6	29	<2	<2	27	6	3	996	3.65	<.01	.68	.56	.01	.02
S9329887	222198*22	2G231	42	7	68	<.4	<2	109	<1	17	88	2.21	<2	64	<5	<5	46	<2	<2	13	6	4	405	1.17	.02	1.36	.58	.01	.05
S9329888	222199*24	2B231	26	4	42	<.4	11	72	<1	13	85	2.23	<2	44	<5	<5	46	<2	<2	12	<2	2	190	1.29	.03	1.48	.36	.01	.03
S9329889	222200*24	2B231	6	9	99	<.4	5	92	<1	5	12	1.77	<2	23	<5	<5	42	<2	<2	11	<2	3	95	.31	<.01	1.05	.18	.01	.04
S9329890	222601*25	1B241	18	4	32	<.4	<2	122	<1	15	32	2.05	<2	37	<5	5	41	<2	<2	15	3	3	508	.64	.02	1.33	.44	.01	.04
S9329891	222602*25	2B241	11	6	39	<.4	<2	64	<1	10	18	1.65	<2	26	<5	<5	45	<2	<2	11	<2	2	214	.40	.03	1.00	.28	.01	.04
S9329892	222603*25	2B241	6	6	49	<.4	4	88	<1	6	14	1.30	<2	22	<5	<5	33	<2	<2	11	<2	<2	150	.40	.01	.97	.26	.01	.04
S9329893	222604*21	2G352	33	47	1745	<.4	17	610	15	9	120	1.51	<2	79	<5	<5	25	<2	<2	36	7	3	493	1.80	.01	.82	3.56	.02	.04
S9329894	222605*24	2G231	3	<4	28	<.4	<2	77	<1	1	2	.40	<2	7	<5	<5	21	<2	<2	10	<2	2	135	.03	<.01	.33	.21	.01	.01
S9329895	222606*25	1G241	30	7	37	<.4	<2	93	<1	11	42	2.28	<2	49	<5	<5	51	<2	<2	11	2	2	207	.92	.03	1.46	.29	.01	.05
S9329896	222607*25	1Y241	20	8	50	<.4	<2	72	<1	9	34	2.68	<2	42	<5	<5	70	<2	<2	12	<2	<2	175	.76	.05	1.45	.36	.01	.03
S9329897	222608*25	2B241	27	7	56	<.4	<2	121	<1	13	47	2.85	<2	48	<5	14	53	<2	<2	11	2	2	181	.80	.03	1.74	.27	.01	.03
S9329898	222609*22	2G341	27	7	78	<.4	<2	112	<1	15	55	2.56	<2	53	<5	8	58	<2	<2	15	2	2	432	1.15	.03	1.69	.46	.01	.04
S9329899	222610*22	1G131	48	68	2907	<.4	<2	962	19	12	194	2.13	<2	103	<5	5	39	<2	<2	46	9	4	500	1.39	.01	1.28	3.22	.02	.05
S9329900	222611*24	3B231	11	384	1438	<.4	<2	278	9	20	56	3.35	<2	55	<5	<5	46	<2	<2	13	2	2	1646	.81	.02	1.78	.76	.01	.05
S9329901	222612*22	3B231	19	649	1151	<.4	3	116	7	21	88	3.62	<2	74	<5	<5	51	<2	<2	9	4	3	1093	.96	.02	2.29	.33	.01	.04
S9329902	222613*22	1G131	45	35	341	<.4	<2	198	<1	17	100	2.54	<2	52	<5	6	45	<2	<2	17	9	5	459	1.28	.01	1.46	.62	.02	.04
S9329903	222614*22	2G231	43	58	329	<.4	<2	253	1	17	89	2.62	<2	56	<5	7	50	<2	<2	17	5	4	446	1.18	.03	1.64	.77	.02	.06
S9329904	222615*22	2N231	13	384	1059	<.4	<2	247	10	21	46	4.17	<2	44	<5	<5	57	<2	<2	6	<2	2	1114	.58	.03	1.27	.34	.01	.07
S9329905	222616*22	2B231	12	778	3213	.5	<2	276	31	8	12	2.86	<2	14	<5	7	27	<2	<2	14	8	5	3198	.63	.01	.61	2.48	.01	.02
S9329906	222617*22	3B232	28	3657	5432	4.0	37	854	23	14	31	3.80	<2	22	<5	12	37	<2	<2	41	16	12	2320	1.27	.01	.98	3.59	.01	.04
S9329907	222618*23	2B231	18	1425	3808	2.3	14	1470	24	12	45	3.83	<2	30	<5	<5	37	<2	<2	37	15	9	1838	2.69	<.01	1.10	4.46	.01	.04
S9329908	222619*23	2B131	9	81	496	<.4	12	264	2	9	41	2.61	<2	29	<5	<5	38	<2	<2	24	16	9	2142	1.19	.02	1.51	3.21	.01	.09
S9329909	222620*23	2B132	7	351	390	<.4	<2	128	2	5	30	2.01	<2	18	<5	6	31	<2	<2	15	12	9	1757	1.75	.01	.89	3.58	.01	.03
S9329910	222621*24	2R131	5	53	928	<.4	<2	141	4	9	30	3.05	<2	29	<5	7	49	<2	<2	12	25	13	2889	.62	.02	1.68	1.45	.01	.02
S9329911	222622*24	2Y231	21	13	136	<.4	17	123	<1	16	86	2.97	<2	48	<5	<5	54	<2	<2	11	4	4	364	.93	.02	2.42	.50	.01	.03
S9329912	222623*24	2B231	13	34	207	<.4	<2	132	1	15	84	3.28	<2	48	<5	<5	51	<2	<2	17	11	7	1545	1.59	.02	2.93	2.70	.01	.03
S9329913	222624*25	2B231	24	105	96	<.4	<2	220	<1	21	62	3.71	<2	39	<5	<5	64	<2	<2	18	3	3	291	.88	.04	1.94	.46	.01	.03
S9329914	222625*25	2B232	19	120	102	<.4	2	142	<1	19	56	4.21	<2	38	<5	5	52	<2	<2	21	3	6	460	.65	.03	1.63	.47	.01	.02
S9329915	222626*25	2B231	16	28	125	<.4	<2	130	<1	21	93	3.18	<2	61	<5	<5	59	2	<2	13	<2	<2	314	1.22	.03	1.40	.29	.01	.03
S9329916	222627*25	2B231	29	30	54	<.4	4	103	<1	23	99	2.97	<2	50	<5	5	50	<2	<2	20	2	4	362	1.12	.03	1.67	.42	.02	.03
S9329917	222628*25	2G231	45	10	59	<.4	<2	250	<1	20	84	3.03	<2	66	<5	<5	55	<2	<2	36	5	4	510	1.46	.03	2.01	.91	.02	.07
S9329918	222629*22	2B231	29	23	90	<.4	2	218	<1	21	82	2.84	<2	53	<5	<5	41	<2	<2	17	4	8	627	1.03	.02	1.38	.35	.01	.07
S9329919	222630*22	2B231	20	11	43	<.4	<2	72	<1	13	47	2.22	<2	42	<5	7	44	<2	<2	16	2	3	288	.74	.04	1.41	.35	.01	.09
S9329920	222631*24	2B231	8	29	115	<.4	<2	104	<1	12	27	2.22	<2	28	<5	<5	24	<2	<2	34	3	7	213	.41	.01	1.20	.36	.01	.04

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K	
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	%	%	%	
S9329921	222632*24	1B231	11	17	72	<.4	<2	98	<1	11	30	2.16	<2	37	<5	<5	38	<2	14	<2	3	219	.54	.03	1.27	.36	.01	.05	
S9329922	222633*24	1Y231	21	25	52	<.4	<2	244	<1	17	35	2.94	<2	35	<5	<5	28	<2	<2	16	5	11	859	.62	.01	1.36	.53	.01	.08
S9329923	222634*24	2B231	18	32	34	<.4	3	40	<1	7	13	1.58	<2	10	<5	<5	8	<2	<2	14	32	76	477	.16	<.01	.57	.79	<.01	.03
S9329924	222635*22	2B231	19	47	117	<.4	<2	158	<1	16	56	2.28	<2	37	<5	<5	39	<2	<2	13	2	3	327	.87	.03	1.35	.40	.01	.07
S9329925	222636*24	1B231	18	106	428	<.4	<2	452	3	28	26	2.85	<2	25	<5	<5	28	<2	<2	25	3	4	3478	.45	.02	1.34	1.02	.01	.06
S9329926	222637*24	2G 31	96	83	236	<.4	<2	661	1	21	75	3.94	<2	47	<5	7	25	<2	<2	27	10	5	870	.72	<.01	1.48	1.01	.01	.05
S9329927	222638*24	2G231	70	87	257	<.4	<2	715	<1	19	64	3.92	<2	50	<5	9	28	<2	<2	28	8	4	488	.63	<.01	1.45	1.12	.01	.04
S9329928	222639*24	1B231	19	94	346	<.4	<2	354	1	23	40	2.92	<2	34	<5	<5	35	<2	<2	14	<2	2	661	.54	<.01	1.35	.57	.01	.12
S9329929	222640*24	1B231	25	22	75	<.4	5	257	<1	23	58	3.99	<2	31	<5	5	28	<2	<2	9	2	2	281	.64	.01	1.87	.29	.01	.04
S9329930	222641*24	1B231	14	26	127	<.4	5	408	1	19	19	4.13	<2	23	<5	9	22	<2	<2	7	<2	2	429	.38	<.01	1.35	.22	<.01	.08
S9329931	222642*24	2B231	32	57	395	<.4	16	816	2	17	70	2.86	<2	55	<5	<5	49	<2	<2	23	11	6	776	.86	.01	1.50	.76	.01	.08
S9329932	222643*24	2B231	9	28	170	<.4	5	238	2	9	30	2.50	<2	32	<5	<5	52	<2	<2	11	<2	2	177	.48	.02	1.04	.34	.01	.10
S9329933	222644*24	2B231	34	23	98	<.4	4	934	1	19	120	2.31	<2	43	<5	5	50	<2	<2	22	2	3	575	1.28	.01	1.57	.68	.01	.11
S9329934	222645*25	2B131	19	15	203	<.4	8	399	2	11	47	2.16	<2	36	<5	<5	43	<2	<2	16	2	4	247	.80	.02	1.29	.32	.01	.05
S9329935	222646*24	2B231	17	23	249	<.4	5	341	7	10	48	1.55	<2	26	<5	<5	31	<2	<2	15	<2	4	464	.34	<.01	.91	.33	.01	.05
S9329936	222647*25	2N121	33	14	50	<.4	13	103	<1	12	50	3.23	<2	45	<5	<5	43	<2	<2	33	6	12	509	.73	.03	1.86	.52	.01	.08
S9329937	222648*25	2B121	24	21	59	<.4	9	73	<1	11	37	4.41	<2	46	<5	<5	54	<2	<2	19	2	7	282	.56	.04	1.83	.37	.01	.05
S9329938	222649*24	2B122	43	27	50	<.4	15	52	<1	17	47	3.21	<2	24	<5	<5	13	<2	<2	101	16	38	456	.65	<.01	1.30	1.78	<.01	.02
S9329939	222650*25	2B231	10	45	30	<.4	<2	52	<1	13	19	4.66	<2	16	<5	<5	11	<2	<2	12	4	13	398	.17	<.01	1.49	.21	<.01	.02
S9329940	222651*25	2B231	40	23	42	<.4	<2	155	<1	19	63	3.73	<2	53	<5	<5	31	<2	<2	13	5	20	221	.48	.01	2.06	.36	.01	.04
S9329942	222652*25	2G231	16	8	57	<.4	<2	100	<1	10	35	2.23	<2	39	<5	<5	51	<2	<2	17	2	4	195	.80	.05	1.65	.55	<.01	.03
S9329942	222653*24	3B231	20	102	81	<.4	5	136	<1	18	80	5.71	<2	59	<5	<5	68	<2	<2	13	7	6	417	1.01	.08	-2.11	.66	<.01	.02
S9329943	222654*24	3K123	108	6	56	<.4	12	517	<1	4	38	.34	<2	12	<5	<5	4	<2	<2	101	7	17	1310	.52	<.01	.38	5.47	.02	<.03
S9329944	222655*24	2B231	35	60	299	<.4	21	167	<1	19	35	4.04	<2	43	<5	<5	77	<2	<2	12	2	3	813	1.09	.09	2.08	.49	<.01	.08
S9329945	222656*24	2B232	11	56	366	<.4	5	292	1	15	32	3.82	<2	43	<5	<5	54	<2	<2	12	<2	2	644	.61	.03	1.51	.43	<.01	.05
S9329946	222657*24	2B231	10	30	159	<.4	7	159	1	21	40	3.09	<2	49	<5	<5	63	<2	<2	14	<2	2	901	.63	.03	1.13	.51	<.01	.08
S9329947	222658*24	2B231	21	27	100	<.4	8	261	<1	16	37	3.14	<2	46	<5	<5	47	<2	<2	17	<2	3	618	.66	.02	1.62	.61	<.01	.05
S9329948	222659*24	2B 31	37	313	625	<.4	12	434	6	20	80	3.08	<2	42	<5	<5	38	<2	<2	20	9	6	1046	.78	.01	1.34	.76	<.01	.07
S9329949	222660*24	2G 32	33	314	670	<.4	32	711	4	21	69	3.05	<2	41	<5	<5	35	<2	<2	21	14	9	1043	.66	<.01	1.38	.92	<.01	.08
S9329950	222661*24	2B 31	16	95	186	<.4	12	283	<1	16	56	3.33	<2	53	<5	<5	50	<2	<2	10	<2	2	422	.61	.02	1.21	.27	<.01	.07
S9329951	222662*23	2R231	7	181	435	<.4	5	454	3	16	29	2.70	<2	36	<5	<5	44	<2	<2	10	<2	2	1260	.31	.01	1.08	.42	<.01	.13
S9329952	222663*23	1Y231	21	389	1250	.7	<2	934	5	11	41	2.05	<2	15	<5	<5	14	<2	<2	51	5	4	470	1.58	<.01	.54	5.09	<.01	.08
S9329953	222664*24	2B231	24	557	2082	.5	18	432	6	18	68	3.06	<2	43	<5	<5	43	<2	4	19	12	8	1107	.87	.01	1.32	1.15	<.01	.09
S9329954	222665*24	1G341	25	202	509	<.4	7	377	5	13	72	2.69	<2	42	<5	5	48	<2	<2	12	15	10	423	.64	<.01	1.36	.76	<.01	.10
S9329955	222666*24	2B 31	21	120	401	<.4	9	1418	12	18	40	2.68	<2	39	<5	<5	53	<2	<2	13	3	4	762	.48	.01	1.45	.64	<.01	.05
S9329956	222667*24	3B 32	16	117	305	<.4	16	1082	5	15	34	2.68	<2	41	<5	<5	56	<2	<2	13	2	3	826	.46	.01	1.54	.49	<.01	.04

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	No	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K		
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	%	%			
S9329957	222668*24	2G 31	21	190	271	<.4	12	1290	2	13	65	2.34	<2	34	<5	<5	45	<2	<2	20	5	5	747	.63	<.01	1.58	.81	.01	.09	
S9329958	222669*24	2B 31	12	36	306	<.4	8	364	3	11	37	2.42	<2	26	<5	<5	40	<2	<2	8	<2	5	1243	.43	.01	1.12	.38	.01	.05	
S9329959	222670*22	2B 31	8	81	162	<.4	11	613	<1	17	148	2.66	<2	35	<5	<5	27	<2	<2	12	4	3	240	1.66	<.01	.87	.86	.01	.02	
S9329960	222671*22	3G231	10	97	198	.4	4	998	1	11	123	1.20	<2	17	<5	<5	10	<2	<2	61	7	4	385	5.09	<.01	.35	7.97	.01	.02	
S9329961	222672*22	2B132	1	161	410	<.4	8	1533	1	2	11	.39	<2	<4	<5	<5	4	<2	<2	58	3	2	610	8.79	<.01	.10	15.50	.01	.02	
S9329962	222673*23	2B121	<1	1218	1181	1.3	<2	1892	8	1	7	.57	<2	<4	<5	<5	17	4	<2	<2	66	3	2	849	9.39	<.01	.05	19.50	.01	.01
S9329963	222674*22	2G131	9	371	803	.7	7	961	3	4	19	1.04	<2	<4	<5	<5	5	<2	<2	41	4	3	584	5.28	<.01	.16	10.54	.01	.02	
S9329964	222675*24	1G232	13	162	392	<.4	9	1154	2	8	20	2.25	<2	<4	<5	<5	9	<2	<2	12	5	4	287	.73	<.01	.77	2.02	.01	.01	
S9329965	222676*22	2G231	9	159	279	<.4	10	479	2	6	17	1.86	<2	<4	<5	<5	7	<2	<2	15	6	8	297	1.82	<.01	.63	3.49	.01	.02	
S9329966	222677*24	2G231	6	30	78	<.4	4	63	<1	4	12	.98	<2	<4	<5	<5	3	<2	<2	14	2	4	236	2.24	<.01	.27	4.10	<.01	.01	
S9329967	222678*24	2B231	3	174	353	<.4	8	65	3	2	17	.68	<2	<4	<5	<5	6	<2	<2	20	3	3	547	4.75	<.01	.19	8.92	.01	.01	
S9329968	222679*24	2G231	7	97	136	.4	17	237	1	4	14	1.17	<2	<4	<5	<5	10	<2	<2	33	9	11	508	3.78	<.01	.26	7.55	.01	.04	
S9329969	222680*24	2G231	5	799	418	.6	7	41	5	3	22	1.08	<2	<4	<5	<5	9	<2	<2	28	6	9	455	4.56	<.01	.20	8.33	.01	.02	
S9329970	222681*23	2B231	<1	134	353	.4	6	30	4	<1	39	.36	<2	<4	<5	<5	4	<2	<2	49	4	3	658	9.23	<.01	.08	15.92	.01	.01	
S9329971	222682*24	1B231	4	306	618	<.4	7	133	7	8	21	2.95	<2	<4	<5	<5	26	<2	<2	15	18	14	1678	.22	<.01	1.05	1.67	<.01	.01	
S9329972	222683*24	2B231	10	1678	1621	1.4	7	371	22	10	63	4.58	<2	<4	<5	<5	30	<2	3	48	29	32	2600	.79	<.01	1.60	1.73	.01	.03	
S9329973	222684*24	2B231	7	746	2421	1.6	<2	179	22	4	76	2.72	<2	<4	<5	<5	24	<2	4	43	12	9	2860	5.09	<.01	.38	9.33	.01	.01	
S9329974	222685*24	1Y231	<1	92	224	<.4	<2	28	1	3	16	.52	<2	<4	<5	<5	10	<2	<2	46	5	5	573	8.92	<.01	.19	15.58	.01	.01	
S9329975	222686*24	2B231	6	3585	4965	12.3	33	1942	61	4	22	2.24	<2	<4	<5	<5	20	<2	15	45	6	6	1475	6.06	<.01	.45	10.63	.01	.01	
S9329976	222687*22	2B231	9	2148	1184	3.6	9	679	23	1	8	1.32	<2	<4	<5	<5	8	<2	<2	36	6	4	1658	9.30	<.01	.10	16.57	.02	.02	
S9329977	222688*23	2G142	9	446	947	1.2	13	463	8	6	17	1.72	<2	<4	<5	<5	7	<2	<2	37	6	12	723	4.46	<.01	.26	8.22	.01	.02	
S9329978	222689*23	2B231	4	1009	2642	5.3	16	716	17	3	21	2.00	<2	<4	<5	<5	14	<2	5	53	11	15	1566	7.04	<.01	.31	12.13	.01	.01	
S9329979	222690*23	2B231	1	1043	1122	2.3	9	393	17	1	10	1.21	<2	<4	<5	<5	9	<2	<2	38	8	5	2084	9.47	<.01	.14	16.59	.02	<.01	
S9329980	222691*23	2B231	8	2357	4683	15.2	<2	427	16	7	28	3.95	<2	<4	<5	<5	46	<2	<2	15	13	13	2533	1.00	<.01	.95	2.20	<.01	.01	
S9329981	222692*23	2G231	38	30	132	.8	5	158	<1	1	25	.84	<2	<4	<5	<5	93	<2	<2	42	17	10	234	3.37	<.01	.28	7.24	.01	.06	
S9329982	222693*23	1B231	6	84	176	<.4	9	1457	1	6	21	1.55	<2	<4	<5	<5	48	<2	<2	9	8	8	414	.48	<.01	.98	.90	<.01	.01	
S9329983	222694*23	2B 32	6	2082	2278	4.5	<2	235	35	5	15	3.46	<2	<4	<5	<5	17	<2	<2	45	20	23	4707	6.21	<.01	.47	11.34	.02	.01	
S9329984	222695*22	2B 32	6	1304	3538	6.8	14	210	32	6	34	3.75	<2	<4	<5	<5	19	<2	<2	24	24	19	3264	5.69	<.01	.88	9.79	.01	.01	
S9329985	222696*22	2B232	3	1788	1802	6.8	<2	228	18	1	6	1.98	<2	<4	<5	<5	13	<2	<2	34	8	5	2301	8.67	<.01	.25	15.31	.02	<.01	
S9329986	222697*22	1B 31	5	1067	3424	6.0	<2	245	34	4	30	4.15	<2	<4	<5	<5	27	<2	<2	26	26	15	3590	6.51	<.01	.70	11.27	.01	<.01	
S9329987	222698*22	1Y231	6	207	333	<.4	10	127	1	9	28	2.42	<2	<4	<5	<5	32	<2	<2	9	4	5	539	.29	<.01	.81	.42	<.01	.01	
S9329988	222699*22	1B231	4	256	589	<.4	6	87	4	8	34	1.87	<2	<4	<5	<5	23	<2	<2	19	12	10	881	2.49	<.01	.67	4.58	<.01	.01	
S9329989	222700*22	1B231	6	62	140	.4	11	56	2	3	35	.82	<2	<4	<5	<5	15	<2	<2	23	8	7	323	2.13	<.01	.62	3.80	.01	.01	
S9329990	222901*24	3B231	3	91	406	<.4	5	58	6	3	12	.98	<2	<4	<5	<5	14	<2	<2	16	11	5	1324	.57	<.01	.71	2.27	<.01	.01	
S9329991	222902*23	2B131	2	57	127	<.4	11	54	2	1	7	.69	<2	<4	<5	<5	10	<2	<2	13	7	4	410	.46	<.01	.33	1.76	<.01	<.01	
S9329992	222903*24	2B231	4	89	252	<.4	<2	145	<1	5	17	1.60	<2	<4	<5	<5	20	<2	<2	7	2	6	194	.14	<.01	.51	.51	<.01	.01	

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %		
S9329993	222904*24	2B231	2	51	111	<.4	10	50	<1	2	6	.84	<2	8	<5	<5	15	<2	5	<2	2	54	.09	<.01	.43	.28	<.01	.01		
S9329994	222905*24	2B231	3	369	702	<.4	<2	95	2	5	18	2.93	<2	14	<5	<5	20	<2	<2	7	22	25	544	.25	.01	1.72	.44	<.01	.02	
S9329995	222906*24	2B231	5	365	4243	1.3	19	487	.40	8	15	4.95	<2	11	<5	<5	17	<2	<2	13	11	9	2729	2.06	<.01	.82	4.08	<.01	.02	
S9329996	222907*24	2B231	6	221	324	<.4	2	116	3	6	16	1.52	<2	7	<5	<5	9	<2	<2	11	7	7	318	.65	<.01	.50	1.61	<.01	.02	
S9329997	222908*24	2B231	3	124	393	<.4	12	82	5	3	11	1.25	<2	10	<5	<5	17	<2	<2	12	6	4	658	.21	<.01	.48	1.13	<.01	.01	
S9329998	222909*24	2B231	6	452	338	<.4	15	193	5	13	18	1.34	<2	10	<5	<5	18	<2	<2	13	9	12	1066	.49	<.01	.40	1.40	<.01	.01	
S9329999	222910*24	2B131	3	121	44	<.4	5	53	<1	4	14	1.30	<2	9	<5	<5	12	<2	<2	6	3	6	142	.17	<.01	.46	.50	<.01	.02	
S9330000	222911*24	1B131	4	1072	124	<.4	6	77	<1	4	19	1.29	<2	11	<5	<5	20	<2	<2	7	7	5	1308	.42	<.01	.58	1.12	<.01	.02	
S9330001	222874*14	2B 31	13	16	59	<.4	2	80	<1	14	52	3.71	<2	46	<5	<5	69	<2	<2	9	<2	7	375	.48	.01	.95	.13	.01	.02	
S9330002	222875*14	2B 31	14	15	51	<.4	<2	78	<1	15	64	4.79	<2	46	<5	<5	73	<2	<2	7	<2	5	809	.59	.01	.89	.11	<.01	.02	
S9330003	222876*12	2B 32	35	11	68	<.4	<2	151	<1	30	250	4.67	<2	63	<5	<5	63	<2	<2	16	<2	2	503	3.65	.01	1.35	.25	.01	.04	
S9330004	222877*14	1B 31	21	15	69	<.4	<2	58	<1	11	32	3.63	<2	11	<5	<5	11	<2	<2	8	3	18	259	.25	<.01	.63	.12	<.01	.15	
S9330005	222878*12	2B232	40	26	104	<.4	11	235	<1	33	48	4.14	<2	11	<5	<5	9	<2	<2	19	7	25	2961	.30	<.01	.52	.43	<.01	.10	
S9330006	222879*12	2B 32	22	17	95	<.4	9	109	<1	24	33	3.63	<2	12	<5	<5	11	<2	<2	14	8	38	1279	.32	<.01	.71	.32	<.01	.14	
S9330007	222880*12	1B 31	13	19	78	<.4	20	134	<1	13	20	3.97	<2	14	<5	<5	24	<2	<2	13	3	13	1705	.28	.01	.86	.13	<.01	.11	
S9330008	222881*12	2B 32	8	6	54	<.4	<2	27	<1	4	14	2.64	<2	4	<5	<5	11	<2	<2	3	<2	17	81	.05	<.01	.36	.01	<.01	.01	
S9330009	222882*12	1B 33	13	7	38	<.4	3	59	<1	3	14	1.32	<2	8	<5	<5	11	<2	<2	7	2	9	134	.07	<.01	.17	.08	.01	.02	
S9330010	222883*12	3B 32	23	13	78	<.4	4	76	<1	48	282	3.65	<2	78	<5	<5	20	<2	<2	10	3	6	860	3.63	<.01	.55	.24	.01	.03	
S9330011	222884*12	2B 32	30	10	69	<.4	6	23	<1	9	30	3.34	<2	8	<5	<5	9	<2	<2	3	4	18	103	.09	<.01	.39	.02	<.01	.03	
S9330012	222885*12	1B431	6	171	156	<.4	11	383	<1	8	12	2.24	<2	12	<5	<5	9	<2	<2	9	4	4	20	121	.37	<.01	1.25	.80	<.01	.07
S9330013	222887*12	2B232	57	24	98	<.4	17	82	<1	36	70	4.67	<2	12	<5	<5	9	<2	<2	13	29	113	1000	.38	<.01	.73	.27	<.01	.07	
S9330014	222888*13	2B 31	27	22	98	<.4	8	91	<1	17	29	3.13	<2	6	<5	<5	8	<2	<2	8	4	17	504	.12	<.01	.47	.20	<.01	.04	
S9330015	222889*12	3B 32	9	475	702	<.4	12	898	5	7	19	2.42	<2	11	<5	<5	14	<2	<2	14	6	7	731	1.25	<.01	.94	3.20	<.01	.02	
S9330016	222890*12	2G 31	8	80	162	<.4	18	202	<1	7	17	2.01	<2	10	<5	<5	9	<2	<2	14	6	8	452	1.67	<.01	.71	3.26	<.01	.02	
S9330017	222891*12	2B 32	18	103	211	<.4	7	253	1	10	24	2.29	<2	8	<5	<5	8	<2	<2	22	5	10	393	1.64	<.01	.31	3.59	<.01	.03	
S9330018	222892*12	2B 32	24	140	242	<.4	3	713	1	18	155	2.73	<2	22	<5	<5	11	<2	<2	34	9	10	721	4.74	<.01	.46	5.80	<.01	.02	
S9330019	222893*12	1B 41	20	13	84	<.4	<2	181	<1	21	51	3.14	<2	4	<5	<5	5	<2	<2	105	6	19	752	.17	<.01	.18	1.13	<.01	.04	
S9330020	222894*14	2B 31	3	148	200	<.4	7	167	2	6	9	1.45	<2	8	<5	<5	11	<2	<2	11	7	6	543	.42	<.01	.49	1.60	<.01	.01	
S9330021	222895*14	2B 32	<1	1202	548	1.2	15	60	7	2	12	1.07	<2	5	<5	<5	20	<2	<2	37	9	7	1288	7.63	<.01	.32	13.70	.01	.01	
S9330022	222896*14	2B 31	3	87	164	<.4	5	474	1	4	12	2.31	<2	13	<5	<5	24	<2	<2	9	<2	5	120	.15	<.01	.81	.55	<.01	.01	
S9330023	222897*14	2B 32	6	196	566	<.4	6	216	6	8	26	3.12	<2	14	<5	<5	26	<2	<2	20	21	14	4589	2.64	.01	.89	6.14	.01	.01	
S9330024	222898*14	2B 31	5	361	363	<.4	7	1649	3	6	12	2.41	<2	11	<5	<5	18	<2	<2	13	10	10	631	.15	<.01	.78	.96	<.01	.01	
S9330025	222900*12	2G341	18	107	193	<.4	<2	158	<1	13	22	2.08	<2	4	<5	<5	5	<2	<2	82	7	16	452	.35	<.01	.29	2.32	<.01	.07	
S9330026	222951*12	2B 31	13	755	621	1.3	<2	616	5	16	104	3.34	<2	33	<5	<5	20	<2	<2	33	22	27	1490	1.67	<.01	.94	2.66	<.01	.02	
S9330027	222952*14	2B341	5	438	666	<.4	3	744	5	13	55	4.37	<2	33	<5	<5	32	<2	<2	17	8	11	1580	.38	<.01	1.38	.66	<.01	.02	
S9330028	222953*14	2B342	6	475	548	.8	3	393	4	9	31	3.68	<2	23	<5	<5	37	<2	<2	19	6	8	698	.17	<.01	1.08	.53	<.01	.02	

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg ppm	Ti %	Al %	Ca %	Na %	K %
S9330029	222954*14 2B 31	5	104	108	<.4	6	271	1	32	140	4.31	<2	43	<5	<5	21	<2	<2	19	2	6	834	1.18	<.01	.81	.71	<.01	.03
S9330030	222955*14 2B 31	17	67	108	<.4	12	91	<1	21	149	5.15	<2	49	<5	<5	27	<2	<2	13	2	8	375	.96	<.01	.75	.33	<.01	.03
S9330031	222956*14 2B 31	9	27	75	<.4	<2	70	<1	11	94	3.25	<2	34	<5	<5	23	<2	<2	16	<2	6	199	.89	<.01	.62	.30	<.01	.01
S9330032	222957*14 2B 31	11	29	123	<.4	<2	288	1	64	471	5.53	<2	163	<5	<5	21	<2	<2	19	2	3	1634	4.81	.01	.64	.54	<.01	.02
S9330033	222958*14 2B 31	7	27	76	<.4	<2	97	<1	38	244	4.22	<2	55	<5	<5	23	<2	<2	8	<2	7	697	2.83	<.01	.60	.14	<.01	.02
S9330034	222959*14 2B 31	7	20	79	<.4	91	89	<1	16	117	3.38	<2	38	<5	<5	38	<2	<2	6	<2	6	242	1.26	<.01	.69	.12	<.01	.02
S9330035	222960*14 2B 31	14	20	75	<.4	10	198	<1	10	68	2.20	<2	29	<5	<5	30	<2	<2	40	<2	6	265	.29	<.01	.52	.73	<.01	.01
S9330036	222961*14 2B 31	8	34	141	<.4	7	249	1	7	19	2.89	<2	20	<5	<5	15	<2	<2	10	<2	7	239	.14	<.01	.48	.40	<.01	.02
S9330037	222962*14 2B 31	8	585	1571	4.2	5	530	6	5	21	3.40	<2	15	<5	<5	22	<2	<2	16	10	11	424	.29	<.01	.80	.68	<.01	.02
S9330038	222963*14 2B 31	4	319	775	1.1	14	286	2	4	21	2.39	<2	17	<5	<5	27	<2	<2	8	4	8	215	.25	<.01	.97	.34	<.01	.02
S9330039	222964*14 1B341	12	164	255	.8	5	112	1	10	20	1.78	<2	5	<5	<5	6	<2	<2	44	6	19	567	.12	<.01	.27	.49	<.01	.02
S9330040	222965*14 2B231	7	99	241	<.4	2	226	1	5	11	1.78	<2	4	<5	<5	4	<2	<2	46	7	8	347	.07	<.01	.26	.36	<.01	.07
S9330041	222966*14 1B 31	13	200	596	1.0	18	507	1	7	35	1.93	<2	11	<5	<5	8	<2	<2	37	8	7	90	.73	<.01	.38	1.49	<.01	.02
S9330042	222967*14 2B 31	21	35	77	<.4	29	26	<1	5	17	3.59	<2	4	<5	<5	11	<2	<2	<2	<2	3	164	.05	<.01	.52	.01	<.01	.02
S9330043	222968*14 2G342	13	103	219	.4	<2	1778	7	8	17	2.00	<2	5	<5	<5	5	<2	<2	44	5	3	980	.38	<.01	.40	3.06	<.01	.01
S9330044	222912*24 2B231	13	11	92	<.4	4	200	<1	6	10	1.73	<2	11	<5	<5	34	<2	<2	13	2	5	80	.22	<.01	1.05	.20	.01	.07
S9330045	222913*14 2B 31	33	12	73	<.4	13	322	<1	9	26	2.28	<2	18	<5	<5	32	<2	<2	37	9	8	265	.45	.01	1.07	.61	.01	.04
S9330046	222914*24 2G231	39	13	99	.6	13	421	1	11	27	2.55	<2	18	<5	<5	35	<2	<2	42	11	8	486	.46	.01	1.20	.79	.01	.04
S9330047	222915*14 3B 31	35	11	108	1.2	18	343	<1	6	25	2.13	<2	16	<5	<5	30	<2	<2	30	7	8	171	.42	.01	1.05	.50	.01	.04
S9330048	222916*24 2K231	92	19	164	.8	3	1219	3	13	65	4.25	<2	35	<5	<5	71	<2	<2	41	29	25	1182	.59	.01	2.63	.68	.01	.08
S9330049	222917*14 K 31	59	10	76	.5	<2	885	2	7	32	2.01	<2	19	<5	<5	35	<2	<2	120	13	10	728	.49	.01	1.15	2.11	.01	.04
S9330050	222918*22 3G342	30	17	111	.4	4	894	<1	10	24	3.08	<2	20	<5	<5	54	<2	<2	60	5	8	484	.46	<.01	1.49	1.09	.01	.06
S9330051	222919*14 2B 31	18	9	69	<.4	10	456	<1	6	17	1.90	<2	14	<5	<5	39	<2	<2	24	4	7	122	.34	<.01	1.20	.41	.01	.03
S9330052	222321* 211B	51	23	103	<.4	15	118	<1	18	80	2.79	<2	75	<5	<5	64	<2	<2	18	8	5	488	1.18	.09	1.68	.68	.02	.12
S9330053	222322* 411Y 2	23	35	159	<.4	<2	177	<1	15	57	3.11	<2	58	<5	<5	72	<2	<2	17	3	3	258	.88	.06	2.22	.52	.02	.05
S9330054	222323* 412Y 5	55	26	124	<.4	27	149	<1	19	93	3.16	<2	69	<5	<5	66	<2	<2	19	12	8	511	1.17	.08	1.84	.74	.02	.09
S9330055	222324* 212B 2	16	26	239	<.4	15	167	<1	14	44	3.49	<2	56	<5	<5	77	<2	<2	14	2	3	242	.80	.08	2.09	.41	.01	.04
S9330056	222325* 313B 2	15	198	1366	<.4	8	442	25	16	57	3.11	<2	52	<5	<5	52	<2	<2	47	6	6	1912	.61	.03	1.73	3.27	.01	.06
S9330057	222326* 212B 5	30	138	588	<.4	7	132	2	23	98	4.31	<2	53	<5	<5	65	<2	<2	32	9	8	1611	2.05	.04	2.50	3.12	.02	.03
S9330058	222327* 212Y 4	23	22	59	<.4	24	63	<1	12	61	2.57	<2	42	<5	<5	54	<2	<2	21	2	3	273	1.13	.04	1.48	.59	.02	.03
S9330059	222328* 211G 2	2	10	112	<.4	<2	250	1	2	7	.61	<2	20	<5	<5	18	<2	<2	21	<2	3	46	.27	<.01	.68	.36	.01	.06
S9330060	222329* 212Y	47	15	81	<.4	2	115	<1	16	78	2.81	<2	60	<5	<5	54	<2	<2	23	4	4	531	1.44	.04	1.67	.51	.01	.05
S9330061	222330* 212B	13	8	74	<.4	4	67	<1	8	24	2.80	<2	42	<5	<5	65	<2	<2	12	<2	3	147	.50	.05	1.44	.26	.01	.04
S9330062	222331* 212B	17	8	73	<.4	<2	123	<1	11	32	2.41	<2	45	<5	<5	65	<2	<2	20	2	3	246	.82	.05	1.55	.49	.01	.05
S9330063	222332* 222G	37	6	60	<.4	8	105	<1	13	55	2.69	<2	63	<5	<5	63	<2	<2	19	3	4	301	1.25	.05	1.81	.44	.01	.05
S9330064	222333* 222B	16	6	54	<.4	8	89	<1	9	25	2.11	<2	39	<5	<5	56	<2	<2	18	2	4	235	.65	.04	1.46	.44	.01	.07

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	X	La	Mn	Mg	Ti	Al	Ca	Na	K	
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	%	%	%	%												
S9330065	222334* 222Y	24	5	53	<.4	3	72	<1	10	35	2.37	<2	46	<5	<5	59	<2	<2	18	2	3	312	.89	.05	1.53	.45	.01	.06	
S9330066	222335* 221B	16	4	33	<.4	11	74	<1	8	26	2.02	<2	40	<5	<5	48	<2	<2	21	3	4	177	.74	.06	1.35	.56	.01	.03	
S9330067	222336* 222B	19	225	775	<.4	16	292	<1	18	62	3.96	<2	61	<5	<5	51	<2	<2	12	2	5	304	.89	.01	1.93	.28	.01	.08	
S9330068	222337* 221B	43	19	129	<.4	8	294	<1	21	61	5.67	<2	61	<5	<5	44	<2	<2	12	2	4	204	.98	.01	2.89	.21	.01	.05	
S9330069	222338* 222B	39	315	836	<.4	10	768	7	19	88	3.08	<2	46	<5	<5	47	<2	<2	17	13	9	1117	.91	.01	1.47	.74	.01	.06	
S9330070	222339* 433B 3	42	18	274	<.4	<2	754	13	2	43	.23	<2	27	<5	<5	3	<2	<2	164	2	<2	278	.64	<.01	.16	6.55	.01	.02	
S9330071	222340* 222B 22	12	166	723	<.4	24	305	3	21	66	3.17	<2	50	<5	<5	45	<2	<2	31	3	4	883	1.06	.03	1.47	.91	.01	.11	
S9330072	222777*14 2B 31	5	143	460	<.4	13	83	1	6	14	1.77	<2	20	<5	<5	31	<2	<2	17	3	7	521	.49	.02	.97	1.36	.01	.03	
S9330073	222778*14 2B341	22	308	978	<.4	3	667	7	15	68	3.05	<2	40	<5	<5	56	<2	<2	17	13	11	1179	1.22	.02	1.60	1.55	.01	.06	
S9330074	222779*14 2B342	13	814	8704	<.4	13	856	28	16	42	4.50	<2	29	<5	<5	48	<2	<2	12	8	8	819	.38	<.01	1.67	1.03	.01	.05	
S9330075	222780*14 1B341	8	1233	8654	1.2	2	769	36	12	15	4.20	<2	19	<5	<5	45	<2	<2	20	10	12	884	.15	<.01	1.18	2.62	.01	.04	
S9330076	222781*13 3B 42	17	1199	5824	2.5	9	1053	49	9	8	1.69	<2	9	<5	<5	24	<2	<2	53	8	6	3007	.21	.01	.51	7.08	<.01	.02	
S9330077	222782*14 2B 32	26	1018	3327	.7	<2	2184	12	25	78	4.44	<2	47	<5	<5	59	<2	<2	36	9	7	1490	1.15	.03	1.59	1.45	.01	.05	
S9330078	222783*14 2B 31	13	143	577	<.4	9	269	1	19	42	4.12	<2	54	<5	<5	6	74	<2	<2	29	3	4	308	.75	.04	1.75	.64	.01	.04
S9330079	222784*14 3B 32	25	202	880	<.4	14	942	4	19	38	3.05	<2	35	<5	<5	31	<2	<2	57	7	7	4216	.51	<.01	1.41	1.52	.01	.04	
S9330080	222785*14 3B341	16	288	654	<.4	5	411	2	16	37	3.08	<2	36	<5	<5	38	<2	<2	44	8	7	786	1.18	<.01	1.27	2.22	.01	.06	
S9330081	222786*1 3 3	25	<4	6089	<.4	7	615	<1	1	46	.27	<2	4	<5	<5	3	<2	<2	134	<2	<2	74	.46	<.01	.12	5.09	.01	.02	
S9330082	222787*14 3B 43	37	30	366	.4	<2	631	2	4	17	.45	<2	7	<5	<5	10	<2	<2	167	<2	<2	784	.62	<.01	.37	6.06	.01	.02	
S9330083	222788*14 2B 31	56	21	186	<.4	<2	380	<1	29	128	3.35	<2	53	<5	<5	69	<2	<2	27	5	3	785	1.19	.04	1.83	1.26	.02	.08	
S9330084	222789*11 2G 41	78	139	1474	<.4	4	544	5	18	102	2.92	<2	139	<5	<5	75	<2	<2	28	11	6	310	1.30	.03	2.21	.69	.02	.05	
S9330085	222790*14 1B 41	29	7	56	<.4	17	124	<1	13	47	2.73	<2	52	<5	<5	60	<2	<2	19	2	3	274	.97	.04	1.60	.41	.01	.06	
S9330086	222791*14 2B 41	8	8	34	<.4	15	54	<1	4	13	2.19	<2	29	<5	<5	80	<2	<2	13	<2	2	83	.31	.06	1.11	.36	.01	.03	
S9330087	222792*14 2B431	7	7	47	<.4	21	52	<1	5	11	2.48	<2	31	<5	<5	74	<2	<2	12	<2	3	116	.37	.07	1.19	.34	.01	.03	
S9330088	222793*14 1B 31	33	8	50	<.4	21	140	<1	14	42	4.14	<2	37	<5	<5	62	<2	<2	17	4	6	628	.68	<.01	1.82	.61	.01	.06	
S9330089	222794*14 1B 31	24	8	58	<.4	11	119	<1	11	30	2.44	<2	37	<5	<5	45	<2	<2	23	3	5	158	.72	.02	1.76	.54	.01	.04	
S9330090	222795*14 1B 31	20	4	40	<.4	4	87	<1	9	30	2.30	<2	40	<5	<5	56	<2	<2	17	2	5	203	.84	.04	1.56	.45	.01	.06	
S9330091	222796*14 1B341	22	13	159	<.4	10	80	<1	8	23	2.41	<2	38	<5	<5	79	<2	<2	30	3	5	203	.66	.08	1.66	.71	.02	.06	
S9330092	222178*2212B231	32	10	93	<.4	6	83	<1	10	33	2.86	<2	39	<5	<5	54	<2	<2	21	2	5	191	.57	.05	1.49	.44	.01	.06	
S9330093	222179*22 2B131	27	6	63	<.4	11	113	<1	10	28	2.41	<2	37	<5	<5	65	<2	<2	21	2	5	183	.53	.04	1.65	.44	.02	.05	
S9330094	222180*22 2B231	31	8	126	<.4	20	112	<1	16	44	4.84	<2	72	<5	<5	91	<2	<2	16	2	4	221	.81	.07	2.66	.33	.02	.08	
S9330095	222181*22 2B231	26	9	51	<.4	8	92	<1	11	34	2.93	<2	41	<5	<5	67	<2	<2	17	2	6	152	.54	.05	1.82	.39	.01	.06	
S9330096	222182*22 2B231	25	5	82	<.4	22	90	<1	9	32	2.72	<2	52	<5	<5	68	<2	<2	20	2	6	152	.70	.04	1.92	.45	.02	.06	
S9330097	222183*22 2B 32	59	6	114	<.4	11	176	<1	23	77	3.58	<2	90	<5	<5	82	<2	<2	31	6	6	1232	1.20	.07	2.43	.80	.02	.09	
S9330098	222184*22 2B231	36	13	107	<.4	12	103	<1	17	70	2.94	<2	69	<5	<5	70	<2	<2	27	3	4	448	1.05	.10	1.94	.61	.02	.11	
S9330099	222185*23 2G131	78	13	60	<.4	13	94	<1	17	78	2.82	<2	63	<5	<5	67	<2	<2	30	10	7	460	1.16	.10	1.80	.83	.03	.12	
S9330100	222186*23 2G131	29	38	397	<.4	12	139	<1	14	64	2.91	<2	52	<5	<5	60	<2	<2	25	5	6	461	.62	.06	2.01	.69	.02	.09	

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K	
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	%	%	%		
S9330101	222187*24	2B231	39	9	107	<.4	15	150	<1	12	59	3.17	<2	63	<5	<5	79	<2	<2	20	3	3	211	1.02	.09	2.44	.50	.02	.05
S9330102	222188*23	2B132	28	80	1998	<.4	16	259	5	10	95	4.29	<2	37	<5	<5	47	<2	<2	45	8	5	2519	5.19	.02	1.19	10.68	.01	.07
S9330103	222189*24	1B231	53	53	830	.5	68	132	1	16	128	2.76	<2	30	<5	7	39	<2	<2	59	9	5	779	1.79	.03	1.30	12.95	.04	.05
S9330104	222190*24	2B231	36	17	147	<.4	16	193	<1	17	69	3.02	<2	71	<5	<5	82	<2	<2	28	3	3	415	1.19	.10	2.39	.85	.03	.07
S9330105	222191*22	1B231	57	13	134	<.4	18	106	<1	18	95	2.90	<2	45	<5	<5	68	<2	<2	22	4	3	442	1.53	.09	1.72	.84	.03	.04
S9330106	222192*22	2G232	42	44	105	<.4	3	151	<1	19	83	3.30	<2	45	<5	6	50	<2	<2	32	17	9	777	1.82	.03	1.64	2.38	.02	.07
S9330107	222193*24	2G231	27	42	578	<.4	4	334	1	17	112	3.35	<2	90	<5	<5	67	<2	<2	25	8	6	572	1.76	.07	2.31	1.40	.03	.10
S9330108	222194*22	2B231	31	25	145	<.4	<2	239	<1	19	76	2.81	<2	61	<5	<5	63	<2	<2	21	4	4	710	1.11	.09	1.69	.82	.02	.11
S9330109	222195*23	3B122	13	16	260	<.4	6	211	1	7	18	1.19	<2	13	<5	<5	24	<2	<2	27	13	10	2615	1.89	.01	.50	5.08	.01	.04
S9330110	222196*23	2B231	48	16	140	<.4	15	241	<1	16	70	2.82	<2	43	<5	<5	56	<2	<2	21	10	7	762	1.37	.04	2.11	1.61	.02	.09
S9330111	222197*24	2B31	68	7	148	<.4	22	183	<1	21	105	3.36	<2	74	<5	<5	70	<2	<2	27	11	7	719	1.31	.08	2.04	1.00	.03	.20
S9330112	222501*4113B133	62	10	162	<.4	7	179	1	28	262	3.72	<2	63	<5	<5	46	<2	<2	39	13	5	1005	3.14	.03	1.33	.81	.01	.05	
S9330113	222502*4112B342	35	4	71	<.4	<2	118	<1	44	480	3.61	<2	108	<5	<5	39	<2	<2	23	5	2	635	6.25	.03	.89	.48	.02	.02	
S9330114	222503*4222B241	29	6	86	<.4	<2	167	<1	56	512	5.09	<2	86	<5	<5	40	<2	<2	13	2	2	904	6.74	.02	1.07	.26	.01	.04	
S9330115	222504*452GB141	86	7	88	<.4	<2	908	<1	55	579	4.63	<2	100	<5	<5	50	<2	<2	21	11	6	1093	5.40	.03	1.26	.42	.02	.04	
S9330116	222505*4522B141	55	6	65	<.4	5	284	<1	42	515	4.45	<2	89	<5	<5	46	<2	<2	30	7	3	799	6.68	.02	1.15	.33	.01	.03	
S9330117	222506*4522B132	30	4	80	<.4	28	167	<1	41	388	4.97	<2	72	<5	<5	57	<2	<2	14	2	<2	643	5.59	.02	1.04	.26	.01	.06	
S9330118	222507*4522B142	17	8	119	<.4	<2	214	<1	59	324	7.03	<2	86	<5	<5	56	<2	<2	17	2	<2	1455	3.61	.02	.97	.34	.02	.04	
S9330119	222508*4522B132	18	5	99	<.4	<2	155	<1	69	536	5.97	<2	84	<5	<5	43	<2	<2	12	<2	<2	1441	7.78	.02	.93	.27	.01	.04	
S9330120	222509*4113B121	49	6	68	<.4	<2	68	<1	56	743	4.19	<2	92	<5	<5	30	<2	<2	15	4	2	962	9.42	.02	.67	.37	.01	.02	
S9330121	222510*452GB132	27	5	62	<.4	7	77	<1	42	463	4.48	<2	79	<5	<5	46	<2	<2	21	3	2	578	6.49	.03	.98	.36	.01	.03	
S9330122	222511*4521B132	24	6	93	<.4	<2	105	<1	53	412	5.96	<2	108	<5	<5	69	<2	<2	14	2	<2	930	6.10	.05	1.34	.29	.02	.03	
S9330123	222512*4521B142	142	5	115	<.4	41	235	<1	38	182	7.26	<2	200	<5	<5	176	<2	<2	8	5	<6	733	3.07	.11	3.52	.23	.01	.02	
S9330124	222513*4522B132	24	4	89	<.4	<2	80	<1	48	526	5.32	<2	124	<5	<5	38	<2	<2	9	<2	<2	742	7.06	.02	1.04	.23	.01	.04	
S9330125	222514*4223G242	57	7	84	<.4	<2	115	<1	46	336	4.37	<2	107	<5	<5	61	<2	<2	17	5	3	1160	4.63	.03	1.33	.39	.02	.04	
S9330126	222515*4523B132	46	6	94	<.4	11	98	<1	56	449	5.49	<2	100	<5	<5	73	<2	<2	17	3	2	1061	6.36	.03	1.50	.32	.02	.03	
S9330127	222516*452GB242	36	<4	78	<.4	26	67	<1	43	466	4.70	<2	137	<5	<5	55	<2	<2	16	4	2	829	5.93	.04	1.26	.39	.02	.03	
S9330128	222517*4222B242	33	6	90	<.4	<2	92	<1	65	495	5.68	<2	136	<5	<5	56	<2	<2	13	4	2	1129	5.51	.03	1.29	.30	.02	.05	
S9330129	222518*4522B132	56	5	88	<.4	<2	81	<1	68	610	4.67	<2	118	<5	<5	45	<2	<2	13	6	3	1346	6.34	.03	1.17	.34	.02	.03	
S9330130	222519*4522B132	16	<4	92	<.4	<2	67	<1	77	791	7.78	<2	117	<5	<5	29	<2	<2	9	2	<2	1498	9.59	.02	.69	.23	.01	.02	
S9330131	222520*452GB242	39	4	76	<.4	10	97	<1	57	663	4.72	<2	116	<5	<5	41	<2	<2	18	4	<2	859	7.62	.03	1.22	.38	.02	.03	
S9330132	222521*4223B142	53	16	138	<.4	14	260	1	36	127	4.02	3	62	<5	<5	60	<2	<2	24	5	3	2249	1.29	<.01	1.41	.27	.01	.05	
S9330133	222522*442GB241	120	27	390	3.2	43	88	1	12	128	5.73	81	16	<5	<5	32	<2	<2	19	6	4	306	.07	<.01	.50	.25	.01	.04	
S9330134	222523*4422B243	33	6	141	<.4	10	190	3	55	247	5.21	<2	102	<5	<5	77	<2	<2	34	<2	2	1784	3.00	.05	1.01	.54	.02	.05	
S9330135	222524*4112B243	44	4	71	<.4	<2	57	<1	46	556	3.85	<2	161	<5	<5	41	<2	<2	27	5	2	717	7.93	.02	.80	.61	.01	.02	
S9330136	222525*4421B241	38	4	72	<.4	29	66	<1	21	124	4.35	<2	131	<5	<5	91	<2	<2	26	2	2	538	2.26	.07	1.62	.29	.02	.03	

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K
		ppm	%	ppm	ppm	ppm	ppm	ppm	ppm																			
S9330137	222526*4222B242	157	9	101	<.4	32	173	<1	26	123	4.06	<2	92	<5	<5	84	<2	<2	165	15	8	1303	1.77	.03	2.01	1.66	.02	.06
S9330138	222527*442GB242	45	9	101	<.4	14	89	<1	9	59	3.27	<2	49	<5	<5	28	<2	<2	50	9	4	247	.82	<.01	1.48	.79	.01	.06
S9330139	222528*4422B241	25	30	81	<.4	47	165	<1	13	39	3.46	<2	31	<5	<5	21	<2	<2	20	8	12	961	.29	<.01	1.07	.33	.01	.07
S9330140	222529*442GB241	83	10	89	<.4	6	79	<1	30	175	3.34	<2	62	<5	<5	42	<2	<2	14	6	5	747	2.58	.04	.98	.33	.01	.05
S9330141	222530*4222B2341	28	6	92	<.4	12	137	<1	15	113	2.91	<2	128	<5	<5	91	<2	<2	21	<2	2	291	1.60	.02	1.09	.30	.01	.04
S9330142	222531*4422B243	144	20	218	<.4	37	199	1	30	98	5.04	3	61	<5	<5	73	<2	<2	25	19	12	947	1.47	.02	1.66	.42	.01	.09
S9330143	222532*422KB143	50	9	104	<.4	22	122	<1	33	269	4.05	<2	181	<5	<5	64	<2	<2	27	7	4	741	3.56	.02	1.30	.41	.02	.04
S9330144	222533*4223B142	44	14	81	<.4	28	250	<1	7	70	2.14	<2	54	<5	<5	62	<2	<2	54	8	10	233	.44	<.01	1.27	1.04	.02	.04
S9330145	222534*4222B241	85	9	94	<.4	15	155	<1	42	295	4.73	<2	131	<5	<5	79	<2	<2	25	11	6	1006	3.38	.04	2.04	.51	.02	.06
S9330146	222535*432GB122	49	24	80	<.4	15	284	<1	8	31	2.10	<2	53	<5	<5	37	<2	<2	11	<2	8	335	.22	<.01	.68	.10	.01	.04
S9330147	222536*422BK243	68	28	108	<.4	15	461	1	9	77	2.06	<2	38	<5	<5	20	<2	<2	79	11	9	856	.38	<.01	1.03	1.39	.01	.08
S9330148	222537*4222B232	34	42	95	<.4	10	152	<1	13	35	3.33	<2	30	<5	<5	26	<2	<2	14	3	11	994	.59	<.01	1.41	.19	.01	.06
S9330149	222538*4323B121	22	25	95	<.4	8	260	<1	3	8	1.80	<2	12	<5	<5	13	<2	<2	23	2	8	138	.07	<.01	.79	.29	.01	.06
S9330150	222539*4323B232	40	19	102	<.4	11	211	<1	26	79	3.25	<2	80	<5	<5	50	<2	<2	17	2	5	1488	.89	.02	1.11	.28	.02	.07
S9330151	222540*4322B132	29	17	109	<.4	11	286	1	30	61	2.98	<2	134	<5	<5	68	<2	<2	34	3	3	1755	.51	.04	1.05	.51	.02	.07
S9330152	222541*4422G231	13	5	36	<.4	5	72	<1	3	8	1.19	<2	39	<5	<5	48	<2	<2	21	<2	5	73	.28	.05	.93	.36	.02	.03
S9330153	222542*4422B232	14	4	67	<.4	10	137	<1	12	61	3.13	<2	103	<5	<5	79	<2	<2	17	<2	2	235	1.06	.06	1.28	.38	.02	.03
S9330154	222543*4422B241	19	5	89	<.4	12	537	<1	15	83	3.22	<2	114	<5	<5	74	<2	<2	21	<2	3	357	1.50	.06	1.09	.34	.02	.04
S9330155	222544*4422B131	32	12	145	<.4	8	602	<1	4	23	2.15	<2	19	<5	<5	36	<2	<2	20	<2	6	62	.05	<.01	.56	.12	.01	.05
S9330156	222545*411GB232	113	12	244	.8	35	617	2	30	419	4.47	<2	133	<5	<5	49	<2	<2	78	22	11	3197	2.26	.01	1.87	1.38	.02	.11
S9330157	222546*422GB231	62	9	70	<.4	20	86	<1	28	204	2.84	<2	88	<5	<5	43	<2	<2	23	5	6	617	3.16	.03	1.01	.44	.02	.09
S9330158	222547*442RB241	15	6	78	<.4	9	164	<1	12	46	3.12	<2	96	<5	<5	90	<2	<2	18	2	3	207	1.06	.06	1.41	.40	.02	.04
S9330159	222548*4222B231	12	13	60	<.4	6	205	<1	5	13	1.72	<2	19	<5	<5	43	<2	<2	16	2	24	295	.07	<.01	.55	.25	.01	.07
S9330160	222549*4422B231	17	5	25	<.4	11	223	<1	<1	2	.70	<2	8	<5	<5	39	<2	<2	4	<2	18	<5	.03	<.01	.49	<.01	<.01	.05
S9330161	222550*4112G141	76	14	271	<.4	35	195	2	25	155	3.59	2	56	<5	<5	45	<2	<2	46	16	10	2356	1.54	.03	1.07	.81	.02	.10
S9330162	222551*4422B242	42	14	84	<.4	15	107	<1	25	123	3.46	<2	107	<5	<5	58	<2	<2	20	5	6	774	1.74	.03	1.38	.39	.02	.14
S9330163	222552*4422B231	20	19	63	<.4	9	146	<1	7	35	2.92	<2	47	<5	<5	59	<2	<2	13	3	5	148	.65	<.01	1.32	.23	.01	.08
S9330164	222553*4422B341	71	21	166	.5	13	744	1	24	91	3.24	<2	89	<5	<5	64	<2	<2	31	12	11	1656	1.08	<.01	1.88	.45	.02	.14
S9330165	222554*4222B231	9	10	34	<.4	<2	87	<1	1	5	.92	<2	13	<5	<5	28	<2	<2	9	<2	8	24	.08	<.01	1.04	.11	.01	.06
S9330166	222555*4422B231	8	10	29	<.4	<2	108	<1	1	4	.85	<2	9	<5	<5	22	<2	<2	8	<2	7	9	.06	<.01	.93	.12	.01	.06
S9330167	222556*4422B231	11	14	45	<.4	<2	50	<1	2	7	1.09	<2	8	<5	<5	21	<2	<2	7	2	9	85	.09	<.01	1.07	.07	.01	.07
S9330168	222557*4422B231	15	20	58	<.4	<2	129	<1	7	18	1.84	<2	24	<5	<5	30	<2	<2	12	3	7	240	.37	<.01	1.03	.23	.01	.09
S9330169	222558*4422B231	15	20	70	<.4	6	100	<1	6	16	2.85	<2	30	<5	<5	64	<2	<2	13	2	8	134	.46	.03	1.31	.25	.02	.05
S9330170	222559*442RB241	126	16	209	<.4	<2	84	<1	6	48	3.37	3	16	<5	<5	80	<2	<2	12	2	4	50	.06	<.01	.66	.03	.01	.08
S9330171	222560*4422B231	53	11	254	<.4	17	224	1	15	66	3.09	<2	70	<5	<5	123	<2	<2	42	5	7	218	.97	.03	1.79	.47	.02	.06
S9330172	222561*4422B241	23	6	165	<.4	<2	233	3	13	89	3.30	<2	74	<5	<5	101	<2	<2	30	5	4	249	1.76	.06	1.53	.61	.02	.06

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %	Tl %	Al %	Ca %	Na %	K %
S9330173	222562*4421B341	23	9	204	.8	8	194	3	5	30	2.89	3	87	<5	<5	126	<2	<2	56	5	5	94	.45	.03	1.56	.60	.02	.09
S9330174	222563*442RB341	11	6	118	<.4	<2	99	1	13	28	2.84	<2	62	<5	<5	75	<2	<2	22	2	3	858	.55	.08	1.31	.51	.02	.06
S9330175	222564*4422B241	36	65	105	<.4	<2	154	<1	34	100	3.64	<2	70	<5	<5	70	<2	<2	41	26	83	572	.92	.05	2.24	.70	.02	.09
S9330176	222565*4423B241	18	31	94	<.4	3	238	<1	19	67	3.09	<2	54	<5	<5	42	<2	<2	31	5	17	470	1.40	.05	1.51	.69	.02	.10
S9330177	222566*4422B231	20	19	256	1.0	16	500	3	7	33	2.11	4	17	<5	<5	41	<2	<2	17	3	15	163	.16	<.01	.92	.20	.01	.10
S9330178	222567*4422B232	11	23	150	<.4	<2	640	1	9	17	2.41	<2	16	<5	<5	21	<2	<2	36	3	11	579	.22	<.01	.87	.54	.01	.17
S9330179	222568*4322B232	19	46	182	<.4	4	709	1	20	40	2.47	<2	30	<5	<5	22	<2	<2	28	6	16	3533	.57	<.01	1.45	.60	.01	.15
S9330180	222569*4322B123	31	53	363	.7	24	1947	1	28	28	2.06	<2	16	<5	<5	12	<2	<2	81	9	7	6313	.30	<.01	1.01	1.78	.01	.16
S9330181	222570*4322B232	18	32	307	<.4	<2	646	2	24	47	2.46	<2	38	<5	<5	32	<2	<2	71	5	6	5230	.54	.03	1.44	1.28	.01	.21
S9330182	222571*4223B231	61	6	212	<.4	11	140	6	20	96	2.99	<2	72	<5	<5	70	<2	<2	42	4	3	558	1.01	.07	1.69	1.04	.02	.10
S9330183	222118*24 2N 31	84	13	151	.7	23	305	<1	10	51	4.16	4	32	<5	<5	32	<2	<2	10	4	8	188	.67	<.01	1.56	.08	.01	.08
S9330184	222119*24 3G231	73	10	65	12.6	<2	988	<1	3	22	2.60	4	65	<5	<5	33	<2	<2	17	3	9	18	.23	<.01	1.53	.12	.01	.06
S9330185	222120*24 3B 31	86	19	176	<.4	23	213	<1	13	45	5.34	11	38	<5	<5	60	<2	<2	14	4	3	616	.53	<.01	1.13	.16	.01	.08
S9330186	222121*24 2B 31	45	15	86	<.4	8	335	<1	5	29	2.93	4	49	<5	<5	90	<2	<2	9	2	5	112	.43	<.01	1.37	.10	.01	.08
S9330187	222122*24 2B 32	44	9	81	<.4	16	120	<1	3	20	1.74	3	33	<5	<5	53	<2	<2	13	2	8	132	.11	<.01	.82	.19	.01	.06
S9330188	222123*24 3B 31	57	23	109	<.4	43	201	<1	17	93	5.26	2	120	<5	<5	99	<2	<2	10	2	4	703	1.48	<.01	1.64	.17	.01	.08
S9330189	222124*24 3B 31	80	17	167	<.4	38	451	<1	18	87	4.60	2	97	<5	<5	73	<2	<2	15	5	6	701	1.35	<.01	1.55	.29	.01	.09
S9330190	222125*24 3B 31	31	12	81	<.4	5	256	<1	5	35	3.08	<2	73	<5	<5	84	<2	<2	8	2	7	169	.54	<.01	1.75	.15	.01	.08
S9330191	222126*24 3B 31	34	18	89	.9	3	312	<1	7	54	5.50	<2	68	<5	<5	48	<2	<2	7	2	3	76	.74	<.01	1.92	.10	.01	.04
S9330192	222127*24 3B 31	32	16	91	<.4	30	161	<1	6	31	4.18	2	50	<5	<5	73	<2	<2	9	2	4	83	.61	<.01	1.78	.13	.01	.06
S9330193	222128*24 2Y 31	24	13	102	<.4	12	147	<1	7	33	4.12	2	62	<5	<5	78	<2	<2	5	<2	4	244	.62	<.01	2.02	.05	.01	.05
S9330194	222129*24 1G 31	45	28	127	<.4	9	641	<1	21	68	3.96	<2	40	<5	<5	17	<2	<2	48	9	8	607	.78	<.01	1.63	.65	.01	.07
S9330195	222130*22 2G 31	32	17	107	.5	4	202	<1	11	48	2.51	3	36	<5	<5	28	<2	<2	23	7	6	574	.43	<.01	1.18	.19	.01	.07
S9330197	222132*22 2G 31	36	18	157	1.0	9	48	<1	7	42	3.51	5	28	<5	<5	33	<2	<2	44	9	2	902	11.42	.02	1.34	.83	.01	.02
S9330198	222133*24 2B 31	12	10	74	<.4	<2	89	<1	4	20	2.03	6	36	<5	<5	36	<2	<2	12	4	4	359	.58	<.01	1.53	.21	.01	.04
S9330199	222134*24 2B 31	20	15	102	.5	4	47	<1	19	149	3.65	2	108	<5	<5	39	<2	<2	16	4	3	615	2.45	<.01	1.65	.30	.01	.05
S9330200	222135*21 3G 31	63	18	219	<.4	24	190	1	7	93	3.74	10	47	<5	<5	47	<2	<2	30	12	4	339	1.50	<.01	1.96	.44	.01	.05
S9330201	222136*22 2G 31	50	9	116	<.4	3	83	<1	42	415	4.20	<2	110	<5	<5	46	<2	<2	36	7	3	763	5.46	.05	1.58	.72	.01	.03
S9330202	222137*22 2G 41	53	20	126	<.4	15	130	<1	20	142	3.20	<2	87	<5	<5	24	<2	<2	35	8	6	604	1.37	<.01	1.12	.56	.01	.06
S9330203	222138*22 2B 31	22	12	108	<.4	22	459	<1	17	140	3.84	<2	58	<5	<5	54	<2	<2	5	3	6	260	1.84	<.01	1.96	.06	.01	.04
S9330204	222139*22 3B231	57	21	134	<.4	<2	172	<1	36	193	5.42	3	58	<5	<5	35	<2	<2	16	3	3	913	2.73	<.01	1.18	.21	.01	.04
S9330205	222140*22 3G 32	23	8	101	<.4	<2	145	1	30	211	3.97	<2	74	<5	<5	42	<2	<2	35	4	2	722	2.68	.03	1.24	.74	.01	.04
S9330206	222141*24 2B 31	16	6	71	<.4	<2	197	<1	26	162	4.58	<2	86	<5	<5	80	<2	<2	13	<2	3	503	2.40	.04	1.57	.19	.01	.04
S9330207	222142*24 2G 31	37	6	97	<.4	2	239	<1	35	434	3.84	<2	89	<5	<5	41	<2	<2	27	6	2	613	5.21	.04	1.16	.42	.01	.03
S9330208	222143*24 2G 31	51	9	233	.5	32	487	<1	39	379	4.17	<2	69	<5	<5	30	<2	<2	51	9	3	909	4.75	.02	1.00	.48	.01	.03

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K	
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm		
S9330209	222144*24	2G 31	72	10	183	1.2	26	212	<1	22	212	3.26	<2	29	<5	<5	15	<2	<2	26	9	6	451	2.42	.01	.58	.26	.01	.03
S9330210	222145*24	2G 31	45	21	114	<.4	20	105	<1	22	151	5.09	<2	46	<5	6	31	<2	<2	7	<2	3	609	1.96	<.01	.78	.09	.01	.03
S9330211	222146*24	2B 31	20	12	58	1.9	18	88	<1	7	53	3.45	2	86	<5	<5	95	<2	<2	6	<2	5	299	.47	<.01	1.14	.06	.01	.03
S9330212	222147*24	2B 31	19	15	84	<.4	26	108	<1	11	48	4.38	3	60	<5	<5	66	<2	<2	6	<2	2	773	.69	<.01	1.27	.13	.01	.06
S9330213	222148*24	2B 31	14	10	85	<.4	6	212	<1	55	743	4.80	<2	66	<5	<5	23	<2	<2	6	<2	2	1456	9.02	<.01	.50	.09	<.01	.03
S9330214	222149*24	2B 31	22	11	78	<.4	38	125	<1	9	57	3.71	3	52	<5	<5	51	<2	<2	5	<2	4	548	.76	<.01	1.20	.07	<.01	.04
S9330215	222150*24	2G231	64	26	90	<.4	18	166	<1	2	24	3.18	5	16	<5	<5	46	<2	<2	19	<2	6	118	.05	<.01	.53	.09	<.01	.05
S9330216	222151*24	2B 31	11	14	27	<.4	5	169	<1	1	6	1.12	<2	17	<5	<5	59	<2	<2	16	<2	6	35	.08	<.01	.92	.01	<.01	.05
S9330217	222152*24	2B 31	11	13	38	<.4	12	125	<1	2	15	2.02	<2	34	<5	<5	61	<2	<2	6	<2	7	46	.32	<.01	1.37	.05	.01	.04
S9330218	222153*24	2B 31	30	10	71	<.4	14	1564	<1	24	128	3.32	<2	25	<5	<5	38	<2	<2	10	<2	6	1049	.83	<.01	.83	.10	<.01	.07
S9330219	222154*24	2B 31	22	10	79	<.4	<2	55	<1	10	58	3.73	2	37	<5	<5	56	<2	<2	6	2	3	536	.86	.02	1.60	.12	<.01	.03
S9330220	222155*24	3B 32	26	11	69	<.4	<2	108	<1	8	39	3.18	2	30	<5	<5	78	<2	<2	14	2	2	359	.50	.02	1.03	.26	<.01	.03
S9330221	222035*24	2B 32	10	13	50	<.4	<2	123	<1	6	20	2.45	<2	19	<5	<5	15	<2	<2	9	2	19	132	.42	<.01	1.54	.31	<.01	.04
S9330222	222036*24	2B 31	7	8	35	<.4	<2	111	<1	3	11	1.63	<2	13	<5	<5	14	<2	<2	7	<2	17	141	.26	<.01	1.15	.26	<.01	.07
S9330223	222037*24	2B 31	15	12	60	<.4	10	69	<1	7	21	2.36	<2	18	<5	<5	14	<2	<2	7	<2	15	371	.37	<.01	1.50	.10	<.01	.03
S9330224	222038*24	2B 31	14	11	53	<.4	3	41	<1	7	24	2.29	<2	15	<5	<5	14	<2	<2	12	4	26	188	.54	<.01	1.49	.13	<.01	.07
S9330225	222039*24	2B 32	10	9	56	<.4	<2	66	<1	4	17	2.16	<2	19	<5	<5	18	<2	<2	7	2	14	206	.40	<.01	1.24	.15	<.01	.13
S9330226	222040*24	3B 31	14	16	54	<.4	6	50	<1	6	17	3.15	<2	16	<5	<5	16	<2	<2	6	3	14	371	.37	<.01	1.50	.10	<.01	.03
S9330227	222041*24	2B 31	17	14	74	<.4	6	72	<1	7	23	3.56	<2	25	<5	<5	24	<2	<2	15	2	6	449	.48	<.01	1.71	.24	<.01	.04
S9330228	222042*24	2G 31	14	19	52	<.4	<2	40	<1	5	20	3.30	<2	22	<5	<5	18	<2	<2	10	2	8	209	.34	<.01	1.17	.12	<.01	.03
S9330229	222043*24	2G 32	19	31	109	<.4	14	86	<1	8	34	2.27	<2	24	<5	<5	21	<2	<2	188	21	35	526	1.10	<.01	1.32	6.43	<.01	.04
S9330230	222044*24	3G342	14	64	98	<.4	<2	96	<1	10	31	3.88	<2	37	<5	<5	26	<2	<2	19	10	24	1061	.48	<.01	1.54	.31	<.01	.05
S9330231	222045*22	2B 31	17	23	46	<.4	<2	82	<1	9	24	2.83	<2	12	<5	<5	12	<2	<2	29	12	34	605	.37	<.01	1.92	.39	<.01	.04
S9330232	222046*23	2G 32	16	59	92	<.4	12	107	<1	7	32	2.35	<2	22	<5	<5	24	<2	<2	290	16	20	803	1.19	<.01	1.00	7.87	<.01	.04
S9330233	222047*24	3G341	21	85	104	<.4	21	134	<1	9	53	3.39	<2	34	<5	<5	28	<2	<2	76	24	37	848	1.04	<.01	1.18	2.15	<.01	.04
S9330234	222048*24	3G 31	23	87	107	<.4	<2	114	<1	11	49	3.20	<2	30	<5	<5	29	<2	<2	110	19	30	784	1.69	<.01	1.20	4.00	<.01	.04
S9330235	222049*24	3G 32	25	86	214	<.4	7	199	1	12	32	2.78	2	17	<5	<5	27	<2	<2	162	42	57	2173	.95	<.01	.78	4.94	<.01	.05
S9330236	222050*23	3G341	24	153	215	<.4	5	268	<1	9	44	3.61	<2	30	<5	<5	32	<2	<2	109	22	27	1473	1.41	<.01	1.26	4.32	<.01	.04
S9330237	222051*23	2G 31	19	160	172	.6	12	185	<1	7	38	2.55	<2	16	<5	<5	19	<2	<2	211	13	16	1165	1.96	.01	.76	13.70	<.01	.03
S9330238	222052*23	2B 31	16	212	284	.4	4	360	<1	7	30	3.38	<2	21	<5	<5	27	<2	<2	115	16	22	1530	2.71	<.01	1.02	7.64	<.01	.04
S9330239	222053*23	2B 31	8	270	240	.7	<2	413	<1	4	19	2.54	<2	12	<5	<5	24	<2	<2	149	9	11	1863	6.03	<.01	.52	14.94	<.01	.02
S9330240	222054*22	2B 31	5	194	218	.4	<2	302	<1	2	10	1.39	<2	5	<5	<5	10	<2	<2	175	4	4	949	7.96	<.01	.28	17.50	<.01	.01
S9330241	222055*22	2B 31	2	235	409	.5	<2	238	1	1	9	1.19	<2	5	<5	<5	10	<2	<2	173	4	4	931	8.82	<.01	.22	19.63	<.01	.01
S9330242	222056*22	2G231	6	324	493	.7	<2	471	2	3	11	1.49	<2	10	<5	<5	16	<2	<2	225	12	11	1436	6.54	<.01	.41	16.58	<.01	.02
S9330243	222057*22	2G231	10	741	309	1.0	4	1026	1	4	16	2.18	<2	13	<5	<5	20	<2	<2	183	16	16	1670	5.39	<.01	.57	13.39	<.01	.03
S9330244	222058*22	2B 31	4	184	320	.5	<2	418	1	2	10	1.62	<2	6	<5	<5	10	<2	<2	139	6	7	964	6.07	<.01	.29	14.92	<.01	.01

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm											
S9330245	222059*22 2B 31	8	207	239	.7	<2	341	1	3	15	2.70	<2	11	<5	<5	18	<2	<2	102	12	12	2078	4.79	<.01	.49	10.36	.01	.02
S9330246	222060*22 2B 31	7	249	279	<.4	13	238	1	3	17	1.96	<2	13	<5	<5	19	<2	<2	97	13	11	1642	5.87	<.01	.59	13.26	.01	.03
S9330247	222061*22 2B 32	18	1055	805	1.1	<2	487	3	7	35	3.38	<2	27	<5	<5	32	<2	<2	98	25	22	2420	4.44	<.01	1.06	10.32	.01	.04
S9330248	222062*22 2B 31	10	216	176	<.4	<2	241	<1	4	25	1.69	<2	18	<5	<5	20	<2	<2	100	13	13	1110	4.10	<.01	.62	11.58	.01	.03
S9330249	222063*24 2B 31	10	280	249	.5	<2	369	1	5	28	1.53	<2	19	<5	<5	20	<2	<2	97	8	8	971	7.37	<.01	.49	12.63	.01	.01
S9330250	222064*22 2G 231	18	195	247	<.4	9	329	1	8	37	2.79	<2	26	<5	<5	30	<2	<2	88	21	25	1256	1.69	<.01	1.02	4.58	.01	.04
S9330251	222065*24 2G 31	11	111	86	<.4	10	234	<1	5	29	1.62	<2	13	<5	<5	14	<2	<2	240	9	13	430	3.40	<.01	.57	15.15	.01	.02
S9330252	222066*24 2G 32	18	188	130	<.4	11	395	1	10	62	2.87	<2	36	<5	<5	30	<2	<2	128	16	21	732	1.17	<.01	1.31	4.65	.01	.03
S9330253	222067*24 2G 31	15	75	70	<.4	14	317	<1	7	39	2.47	<2	22	<5	<5	26	<2	<2	74	14	16	863	5.09	<.01	.83	8.69	.01	.02
S9330254	222068*24 2G 31	14	45	67	<.4	12	270	<1	5	33	2.41	<2	18	<5	<5	24	<2	<2	72	14	17	683	5.20	<.01	.76	9.14	.01	.03
S9330255	222069*24 2B 31	13	25	49	<.4	<2	181	<1	7	28	2.02	<2	11	<5	<5	12	<2	<2	57	9	19	533	3.41	<.01	.73	6.05	.01	.04
S9330256	222070*24 2B 31	19	52	70	<.4	19	342	<1	8	40	3.94	<2	18	<5	<5	25	<2	<2	35	23	24	2344	3.89	<.01	1.12	6.37	.01	.03
S9330257	222071*24 2B 31	16	19	56	<.4	<2	167	<1	15	39	2.60	<2	17	<5	<5	10	<2	<2	32	6	21	890	2.60	<.01	.99	3.86	.01	.05
S9330258	222235*14 K 42	21	44	133	<.4	<2	140	<1	7	45	3.04	<2	32	<5	<5	26	<2	<2	50	34	59	852	.56	<.01	1.63	1.03	.01	.05
S9330259	222236*14 3B 42	20	108	159	<.4	<2	129	<1	6	38	2.59	<2	21	<5	<5	21	<2	<2	150	13	21	592	2.79	<.01	.99	9.36	.01	.04
S9330260	222237*14 1B 42	10	115	104	<.4	<2	667	<1	4	28	2.19	<2	15	<5	<5	19	<2	<2	142	13	15	689	4.88	<.01	.61	13.49	.01	.02
S9330261	222238*14 2B 41	13	70	141	<.4	<2	179	<1	7	31	3.61	<2	42	<5	<5	33	<2	<2	30	8	17	308	.45	<.01	1.68	.77	.01	.05
S9330262	222239*14 3B 42	13	446	482	.5	16	292	1	5	27	4.67	<2	25	<5	<5	40	<2	<2	68	27	29	2179	3.62	<.01	.93	7.28	.01	.03
S9330263	222240*14 3B 42	19	236	349	.6	<2	412	1	6	40	5.19	<2	34	<5	<5	42	<2	<2	46	26	24	746	2.03	<.01	1.23	4.77	.01	.04
S9330264	222241*13 3G 41	20	182	228	<.4	14	356	<1	8	41	3.67	<2	23	<5	<5	29	<2	<2	59	19	26	1392	4.36	<.01	.90	6.93	.01	.02
S9330265	222242*14 2B 42	17	579	693	<.4	7	712	2	10	44	7.03	<2	40	<5	<5	88	<2	<2	53	26	25	6382	2.62	<.01	1.40	4.68	.01	.03
S9330266	222243*14 1B 42	2	208	219	<.4	<2	156	<1	2	14	1.51	<2	10	<5	<5	18	<2	<2	95	7	7	966	9.56	<.01	.38	16.41	.01	<.01
S9330267	222244*14 2B 41	2	167	195	.4	<2	173	<1	1	10	1.23	<2	5	<5	<5	10	<2	<2	124	4	4	752	9.67	<.01	.26	19.39	.01	.01
S9330268	222245*14 2B342	1	256	507	.5	11	230	2	1	8	1.35	<2	6	<5	<5	11	<2	<2	101	5	4	1339	9.76	<.01	.22	17.38	.01	.01
S9330269	222246*14 2B342	3	660	905	.6	8	544	3	2	11	1.83	<2	7	<5	<5	19	<2	3	99	7	5	1464	9.70	<.01	.28	17.01	.01	.01
S9330270	222247*14 2B 41	1	554	993	.6	10	251	4	2	10	1.80	<2	8	<5	<5	20	<2	4	83	8	6	1651	9.75	<.01	.30	16.93	.01	.01
S9330271	222248*14 2B342	1	554	572	.8	<2	612	2	2	13	1.26	<2	7	<5	<5	15	<2	<2	123	5	4	981	9.55	<.01	.22	16.74	.01	.01
S9330272	222249*14 2B 42	7	738	1065	.8	11	499	4	4	20	3.00	<2	19	<5	<5	37	<2	2	84	14	12	2413	7.47	<.01	.70	13.03	.01	.02
S9330273	222251*14 2B 33	6	455	647	.9	<2	482	3	2	14	2.33	<2	11	<5	<5	23	<2	<2	137	10	9	1535	8.52	<.01	.39	15.39	.01	.01
S9330274	222252*14 2B 42	15	883	1215	1.3	<2	1272	7	7	34	6.72	<2	30	<5	<5	66	<2	<2	72	27	21	5290	5.09	<.01	1.10	8.73	.01	.03
S9330275	222253*14 2B 42	7	519	465	.7	<2	478	2	2	15	1.91	<2	12	<5	<5	27	<2	<2	157	12	9	1627	8.26	<.01	.48	16.22	.01	.02
S9330276	222254*14 2G 42	2	705	527	.9	2	649	1	2	12	2.17	<2	17	<5	<5	41	<2	<2	117	19	13	1099	8.74	<.01	.55	15.41	.01	.01
S9330277	222255*14 3G342	15	915	1085	.5	21	2279	3	9	45	5.25	<2	39	<5	<5	79	<2	<2	52	32	23	2126	3.44	<.01	1.45	5.45	.01	.04
S9330278	222256*14 3G 42	20	1262	1452	.7	15	2188	6	10	43	6.40	<2	47	<5	<5	94	<2	<2	37	36	25	3208	1.70	<.01	1.54	3.34	.01	.05
S9330279	222257*14 1B 42	9	203	278	<.4	<2	1402	<1	4	26	1.53	<2	16	<5	<5	20	<2	<2	135	8	8	423	6.73	<.01	.55	13.85	.01	.02
S9330280	222258*14 3B 43	17	514	404	<.4	14	1118	1	9	43	4.08	<2	34	<5	<5	52	<2	<2	58	40	42	1130	1.37	<.01	1.38	2.86	.01	.05

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Hn	Mg	Tl	Al	Ca	Na	K
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm												
S9330281	222259*14 3B433	20	1070	485	1.1	18	1533	1	8	50	3.95	<2	38	<5	<5	66	<2	<2	71	22	21	762	1.75	.01	1.18	3.09	.01	.03
S9330282	222260*14 2G542	15	176	214	<.4	12	284	<1	7	44	3.36	<2	45	<5	<5	29	<2	<2	65	24	31	233	.44	<.01	1.36	1.01	.01	.03
S9330283	222261*14 3G541	11	56	83	<.4	<2	302	<1	6	31	2.65	<2	33	<5	<5	25	<2	<2	81	11	16	175	.40	<.01	1.54	1.14	.01	.04
S9330284	222262*13 2G432	13	45	64	<.4	<2	195	<1	5	26	2.29	<2	15	<5	<5	20	<2	<2	95	13	16	485	3.64	<.01	.80	7.42	.01	.04
S9330285	222263*14 3B432	7	14	99	<.4	3	152	<1	3	12	1.59	<2	20	<5	<5	15	<2	<2	41	2	9	260	.19	<.01	.72	1.15	<.01	.05
S9330286	222264*14 1B432	4	11	52	<.4	2	215	<1	2	11	1.96	<2	26	<5	<5	17	<2	<2	13	<2	12	124	.28	<.01	.98	.37	<.01	.05
S9330287	222265*14 1B342	4	7	27	<.4	<2	93	<1	1	6	1.01	<2	19	<5	<5	10	<2	<2	9	<2	18	<5	.22	<.01	1.47	.18	<.01	.05
S9330288	222266*14 1B343	3	7	21	<.4	<2	51	<1	1	4	.88	<2	14	<5	<5	9	<2	<2	10	<2	11	<5	.15	<.01	1.03	.09	<.01	.04
S9330289	222267*14 2B343	6	7	22	<.4	<2	59	<1	2	7	1.47	<2	9	<5	<5	9	<2	<2	10	<2	8	122	.07	<.01	.94	.03	<.01	.06
S9330290	222268*14 2B342	12	17	47	<.4	4	58	<1	4	14	1.96	<2	16	<5	<5	19	<2	<2	9	<2	10	197	.05	<.01	.60	.12	<.01	.05
S9330291	222269*14 2B342	9	11	38	<.4	2	102	<1	4	12	1.86	<2	18	<5	<5	16	<2	<2	9	<2	11	168	.08	<.01	.65	.12	<.01	.05
S9330292	222270*14 2G232	4	8	22	<.4	5	102	<1	1	5	1.04	<2	19	<5	<5	10	<2	<2	15	<2	10	77	.14	<.01	.85	.34	<.01	.05
S9330293	222271*13 2B233	6	11	25	<.4	<2	212	<1	3	5	1.18	<2	12	<5	<5	12	<2	<2	16	2	9	472	.06	<.01	.87	.40	<.01	.07
S9330294	222272*13 2B342	13	79	57	<.4	<2	103	<1	9	31	2.76	<2	41	<5	<5	20	<2	<2	13	2	7	315	.52	<.01	1.14	.19	<.01	.05
S9330295	222273*14 K 41	11	442	115	<.4	10	674	<1	7	33	3.30	<2	59	<5	<5	41	<2	<2	47	11	16	203	.49	<.01	1.61	.95	<.01	.04
S9330296	222274*14 3B 42	10	93	129	<.4	8	265	<1	6	25	2.64	<2	41	<5	<5	21	<2	<2	27	8	15	206	.30	<.01	1.17	.51	<.01	.06
S9330297	222275*14 2B 42	9	18	41	<.4	4	325	<1	2	12	1.89	<2	18	<5	<5	12	<2	<2	30	2	13	163	.11	<.01	.80	.73	<.01	.04
S9330298	222276*14 2G232	22	21	60	<.4	9	157	<1	13	23	2.81	<2	6	<5	<5	6	<2	<2	38	5	13	466	.30	<.01	.66	1.06	<.01	.07
S9330299	222277*14 2B341	12	49	87	<.4	<2	190	<1	6	28	2.43	<2	50	<5	<5	20	<2	<2	25	2	10	469	.31	<.01	.68	.69	<.01	.05
S9330300	222278*14 2B341	12	80	77	<.4	5	423	<1	5	24	2.75	<2	48	<5	<5	32	<2	<2	31	7	13	279	.33	<.01	1.44	.83	<.01	.07
S9330301	222279*14 2B341	14	111	70	<.4	10	291	<1	7	25	2.78	<2	48	<5	<5	36	<2	<2	20	2	9	157	.31	<.01	1.34	.38	<.01	.04
S9330302	222280*13 2B341	19	113	82	<.4	5	237	<1	8	36	2.70	<2	19	<5	<5	24	<2	<2	183	10	15	866	-2.11	<.01	.83	8.23	<.01	.08
S9330303	222281*13 2B341	13	106	62	<.4	<2	161	<1	5	26	1.74	<2	11	<5	<5	13	<2	<2	455	7	11	490	1.79	<.01	.48	18.29	<.01	.03
S9330304	222283*14 2B 42	7	52	85	<.4	<2	262	<1	4	15	2.33	<2	22	<5	<5	6	<2	<2	34	4	13	302	.20	<.01	1.26	.74	<.01	.05
S9330305	222284*14 1Y231	2	4	13	<.4	<2	36	<1	1	2	1.27	<2	<4	<5	<5	5	<2	<2	2	<2	13	73	.01	<.01	.35	<.01	<.01	.03
S9330306	222285*13 2G231	6	9	21	<.4	<2	196	<1	2	10	1.07	<2	6	<5	<5	5	<2	<2	25	3	8	588	.04	<.01	.54	.59	<.01	.04
S9330307	222286*14 2G341	16	47	116	<.4	2	109	<1	5	28	2.31	<2	12	<5	<5	10	<2	<2	42	16	32	173	.15	<.01	.87	.85	<.01	.07
S9330308	222287*14 2B341	13	18	57	<.4	4	53	<1	7	23	2.98	<2	21	<5	<5	13	<2	<2	8	3	29	192	.39	<.01	1.34	.07	.01	.05
S9330309	222288*14 2B 41	7	12	41	<.4	10	69	<1	3	12	2.28	<2	11	<5	<5	15	<2	<2	10	<2	25	73	.16	<.01	1.24	.30	.01	.04
S9330310	222289*24 2G 31	4	5	13	<.4	<2	55	<1	1	3	.51	<2	9	<5	<5	6	<2	<2	6	<2	28	18	.05	<.01	1.11	.02	.01	.04
S9330311	222290*14 2B 41	12	10	45	<.4	<2	39	<1	5	17	2.84	<2	19	<5	<5	14	<2	<2	6	2	22	161	.31	<.01	1.10	.03	.01	.05
S9330312	222291*14 2B 41	15	17	53	<.4	<2	44	<1	11	26	2.65	<2	15	<5	<5	10	<2	<2	7	4	48	467	.26	<.01	1.08	.05	<.01	.04
S9330313	222292*24 2R 31	10	8	31	<.4	<2	47	<1	3	12	2.27	<2	16	<5	<5	17	<2	<2	5	<2	13	118	.13	<.01	.90	.04	.01	.05
S9330314	222293*14 2B341	12	9	38	<.4	<2	50	<1	5	16	2.38	<2	13	<5	<5	11	<2	<2	8	2	14	140	.18	<.01	.96	.06	.01	.07
S9330315	222294*24 2B 31	10	10	39	<.4	<2	93	<1	6	19	2.83	<2	25	<5	<5	15	<2	<2	8	2	14	101	.26	<.01	1.13	.09	.01	.06
S9330316	222401*24 2B 31	15	13	57	<.4	11	31	<1	6	13	5.25	<2	29	<5	<5	31	<2	<2	8	<2	6	274	.55	<.01	1.88	.05	.01	.05

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %
S9330317	222402*14 1B231	11	9	42	<.4	<2	57	<1	5	12	2.64	<2	15	<5	<5	19	<2	<2	6	<2	9	293	.19	<.01	.97	.04	.01	.07
S9330318	222403*2122B 31	18	<4	11	<.4	109	26	<1	3	8	1.43	<2	<4	<5	<5	7	<2	<2	<2	16	147	<.01	<.01	.27	<.01	<.01	.02	
S9330319	222404*14 1B341	18	8	40	<.4	<2	17	<1	4	12	2.20	<2	6	<5	<5	14	<2	<2	3	<2	12	223	.03	<.01	.63	.02	<.01	.03
S9330320	222405*24 2B 31	14	10	44	<.4	9	56	<1	5	14	2.78	<2	13	<5	<5	15	<2	<2	5	<2	20	113	.11	<.01	.99	.04	<.01	.05
S9330321	222406*14 2B341	9	7	27	<.4	13	31	<1	3	9	2.01	<2	10	<5	<5	14	<2	<2	5	<2	14	129	.11	<.01	.71	.08	<.01	.04
S9330322	222407*24 3B 32	8	13	33	<.4	12	58	<1	5	9	1.80	<2	10	<5	<5	9	<2	<2	10	2	16	222	.13	<.01	.64	.10	.01	.06
S9330323	222409*24 1B 31	8	7	24	<.4	<2	89	<1	3	5	1.54	<2	5	<5	<5	9	<2	<2	3	<2	15	416	.03	<.01	1.08	.02	.01	.07
S9330324	222410*14 3B 43	17	142	313	<.4	11	219	1	18	67	4.29	<2	55	<5	<5	41	<2	<2	99	16	21	1496	.53	<.01	1.43	2.49	.01	.09
S9330325	222411*23 3B 33	25	207	395	<.4	23	222	<1	15	69	3.18	<2	26	<5	<5	24	<2	<2	107	12	15	1045	.54	<.01	1.17	3.49	.01	.10
S9330326	222412*14 3B432	12	23	57	<.4	69	284	<1	16	16	2.21	<2	14	<5	<5	12	<2	<2	69	2	7	996	.14	<.01	.59	1.30	.01	.10
S9330327	222413*24 2B 31	19	22	76	<.4	<2	94	<1	18	26	3.77	<2	19	<5	<5	11	<2	<2	9	<2	8	662	.47	<.01	1.46	.05	.01	.11
S9330328	222414*14 2B342	14	20	58	.5	<2	315	<1	18	17	2.99	<2	13	<5	<5	12	<2	<2	6	<2	6	6075	.05	<.01	.85	.04	.01	.07
S9330329	222415*24 2B 31	13	20	52	<.4	<2	125	<1	12	16	2.65	<2	11	<5	<5	11	<2	<2	7	2	10	889	.11	<.01	.81	.07	.01	.07
S9330330	222416*14 2B342	11	16	53	<.4	3	227	<1	7	15	2.46	<2	9	<5	<5	12	<2	<2	11	<2	16	846	.10	<.01	.67	.19	.01	.07
S9330331	222417*24 3K 42	14	255	74	<.4	3	525	<1	6	23	2.54	<2	14	<5	<5	22	<2	<2	46	22	24	1445	.58	<.01	.62	3.06	<.01	.03
S9330332	222418*13 3B242	11	176	215	.6	2	493	<1	2	9	.47	<2	5	<5	<5	9	<2	<2	355	8	11	893	2.69	<.01	.13	13.49	<.01	.03
S9330333	222419*24 3K 43	18	487	746	<.4	6	1554	6	7	22	.99	<2	10	<5	<5	15	<2	2	200	11	12	1534	.48	<.01	.39	5.73	.01	.04
S9330334	222420*14 2B341	20	8512	2113	10.2	33	16902	12	12	50	2.95	47	21	<5	17	88	<2	13	272	27	21	1729	1.45	<.01	1.18	4.23	<.01	.05
S9330335	222421*14 3B341	18	207	186	<.4	<2	2025	1	6	16	.95	2	6	<5	<5	9	<2	<2	70	5	5	665	.15	<.01	.30	2.30	<.01	.02
S9330336	222422*14 2G232	15	92	45	.8	<2	832	<1	4	13	.99	<2	6	<5	<5	7	<2	<2	41	9	13	180	.09	<.01	.28	.59	<.01	.05
S9330337	222423*14 3B342	29	43	159	<.4	<2	755	13	8	21	1.03	2	8	<5	<5	9	<2	<2	53	2	5	1050	.05	<.01	.23	.86	<.01	.04
S9330338	222424*14 2B341	20	193	149	<.4	7	696	2	9	16	1.92	<2	16	<5	<5	23	<2	<2	46	10	10	1061	.10	<.01	.49	.99	<.01	.03
S9330339	222425*14 2G 31	19	251	65	.5	6	1354	1	8	34	1.69	<2	28	<5	<5	18	<2	<2	57	16	14	321	.47	<.01	.61	1.53	<.01	.02
S9330340	222426*14 2B342	6	92	49	<.4	5	319	<1	4	15	2.15	<2	32	<5	<5	32	<2	<2	19	3	6	280	.16	<.01	.79	.50	<.01	.02
S9330341	222427*14 2G 41	9	68	35	<.4	9	285	<1	5	14	1.49	<2	13	<5	<5	15	<2	<2	216	14	20	1000	.30	<.01	.51	4.89	<.01	.02
S9330342	222428*14 2G341	9	104	118	<.4	8	1035	1	8	20	1.49	<2	16	<5	<5	21	<2	<2	50	14	16	1219	2.19	<.01	.57	4.30	<.01	.03
S9330343	222429*14 2B453	8	26	37	<.4	<2	165	<1	2	9	1.63	<2	7	<5	<5	7	<2	<2	12	4	11	46	.17	<.01	.94	.27	<.01	.02
S9330344	222430*13 2B342	12	64	224	<.4	<2	102	4	9	28	1.39	<2	9	<5	<5	9	<2	<2	202	12	16	1019	.21	<.01	.64	4.89	<.01	.04
S9330345	222431*14 2B341	4	49	60	<.4	6	102	<1	6	13	1.57	<2	9	<5	<5	11	<2	<2	95	15	10	706	.20	<.01	.54	1.99	<.01	.02
S9330346	222432*14 2B341	4	28	40	<.4	<2	155	<1	7	22	1.96	<2	17	<5	<5	11	<2	<2	55	13	16	621	.17	<.01	.96	1.12	<.01	.02
S9330347	222433*13 3G 43	7	79	155	<.4	8	185	1	7	21	2.25	<2	18	<5	<5	35	<2	<2	187	20	26	1667	.41	<.01	1.02	5.07	<.01	.02
S9330348	222434*13 2B 42	4	17	63	<.4	<2	151	<1	1	8	1.22	<2	6	<5	<5	11	<2	<2	125	7	9	1445	6.69	<.01	.16	12.99	.01	.02
S9330349	222435*14 2B342	13	13	58	<.4	<2	46	<1	2	15	1.77	<2	8	<5	<5	19	<2	<2	5	<2	3	52	.16	<.01	.64	.29	<.01	.01
S9330350	222436*13 2G232	24	50	66	.6	15	205	<1	<1	15	1.72	10	7	<5	<5	93	<2	<2	32	<2	19	<5	.03	<.01	.42	.03	<.01	.04
S9330351	222437*13 2G 41	24	44	30	1.5	6	243	<1	1	8	1.58	9	9	<5	<5	60	<2	<2	35	2	29	185	.02	<.01	.38	.02	<.01	.05
S9330352	222438*13 2G341	7	19	27	2.6	<2	102	<1	<1	6	.70	4	6	<5	<5	39	<2	<2	11	<2	8	34	.02	<.01	.34	.04	<.01	.08

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	X	La	Mn	Mg	Ti	Al	Ca	Na	K
		ppm	%	ppm	ppm	ppm	ppm	ppm	ppm																			
S9330353	222439*14 2B41	13	32	39	<.4	.5	112	<1	1	11	.94	2	11	<5	51	<2	<2	22	<2	9	18	.03	<.01	.46	.04	<.01	.02	
S9330354	222440*14 2B231	6	20	16	.5	5	44	<1	<1	7	.46	<2	7	<5	69	<2	<2	8	<2	5	<5	.01	<.01	.33	<.01	<.01	<.01	
S9330355	222441*14 2B341	1	5	7	<.4	<2	46	<1	<1	1	.10	<2	7	<5	45	9	<2	<2	5	<2	7	<5	.01	<.01	.52	.02	<.01	.01
S9330356	222442*14 2B341	5	9	21	<.4	4	31	<1	1	7	1.21	<2	18	<5	<5	40	<2	<2	5	<2	6	26	.07	<.01	.54	.04	<.01	.02
S9330357	222443*14 2B341	11	32	39	.8	<2	79	<1	<1	12	.84	<2	13	<5	<5	64	<2	<2	45	<2	10	<5	.01	<.01	.60	.01	<.01	.02
S9330358	222444*14 2B341	5	18	36	<.4	3	188	<1	2	10	.65	<2	25	<5	<5	18	<2	<2	8	<2	5	99	.10	<.01	.48	.11	<.01	.01
S9330359	222445*14 2B341	7	92	55	<.4	7	364	<1	2	13	1.16	<2	43	<5	<5	33	<2	<2	9	<2	4	75	.18	<.01	.74	.08	.01	.02
S9330360	222446*14 2B341	3	22	28	<.4	<2	129	<1	1	4	.46	<2	20	<5	<5	13	<2	<2	6	<2	4	57	.05	<.01	.57	.04	<.01	.01
S9330361	222447*14 2B341	4	39	44	<.4	3	138	<1	2	13	.94	<2	30	<5	<5	32	<2	<2	9	<2	4	32	.26	<.01	.86	.08	<.01	.01
S9330362	222448*14 2B341	6	20	35	<.4	<2	42	<1	<1	12	.86	<2	10	<5	<5	32	<2	<2	6	<2	6	17	.04	<.01	.64	.02	<.01	.01
S9330363	222449*14 2B341	10	14	68	<.4	<2	310	<1	12	101	3.13	<2	90	<5	<5	40	<2	<2	9	<2	4	269	.85	.01	1.35	.10	.01	.03
S9330364	222450*14 2B41	19	11	112	<.4	<2	200	<1	97	758	7.21	<2	115	<5	<5	25	<2	<2	5	<2	<2	2227	10.09	<.01	.76	.14	<.01	.03
S9330365	222451*14 2B341	5	9	43	<.4	<2	361	<1	8	58	1.18	<2	73	<5	<5	21	<2	<2	9	<2	3	124	.72	<.01	.99	.12	.01	.02
S9330366	222452*14 2B341	17	42	225	<.4	2	693	1	14	264	2.83	<2	90	<5	<5	27	<2	<2	14	<8	4	565	1.10	.01	1.10	.57	<.01	.06
S9330367	222453*14 2B41	22	66	129	<.4	<2	386	1	46	148	4.62	<2	121	<5	<5	43	<2	<2	8	<2	3	2710	.85	.02	.99	.19	<.01	.05
S9330368	222454*14 2B341	10	20	107	<.4	<2	215	<1	17	176	2.98	<2	82	<5	<5	25	<2	<2	8	<2	2	295	2.20	<.01	.85	.17	<.01	.02
S9330369	222455*14 2B341	9	8	61	<.4	<2	315	<1	13	156	2.43	<2	76	<5	<5	25	<2	<2	6	<2	2	219	1.75	<.01	.94	.11	<.01	.02
S9330370	222456*14 1B341	4	5	44	<.4	<2	183	<1	7	60	1.42	<2	53	<5	<5	18	<2	<2	5	<2	2	104	.78	<.01	.69	.11	<.01	.02
S9330371	222457*14 2B341	8	14	69	<.4	<2	263	<1	49	501	5.00	<2	69	<5	<5	30	<2	<2	5	<2	<2	1133	7.53	<.01	.72	.13	<.01	.02
S9330372	222458*14 2B341	8	12	60	<.4	21	168	<1	21	191	2.74	<2	49	<5	<5	20	<2	<2	4	<2	<2	451	2.64	<.01	.55	.09	<.01	.02
S9330373	222459*14 2B341	15	7	59	<.4	<2	652	<1	16	169	1.53	<2	37	<5	<5	14	<2	<2	14	<3	2	426	1.59	<.01	.60	.17	.01	.04
S9330374	222460*14 2B341	24	15	138	<.4	<2	449	<1	20	215	3.75	<2	73	<5	<5	26	<2	<2	11	<7	4	823	1.36	<.01	1.04	.20	<.01	.06
S9330375	222461*14 1B341	3	<4	17	<.4	<2	94	<1	2	16	.44	<2	16	<5	<5	12	<2	<2	5	<2	2	76	.21	<.01	.50	.11	<.01	.01
S9330376	222462*14 2B341	7	10	58	<.4	<2	151	<1	24	212	2.40	<2	29	<5	<5	18	<2	<2	5	<2	<2	488	2.91	<.01	.49	.07	<.01	.03
S9330377	222463*14 1B341	31	18	69	<.4	<2	155	<1	81	727	3.99	<2	57	<5	<5	18	<2	<2	6	<3	2	1218	6.97	<.01	.70	.12	<.01	.02
S9330378	222464*14 2B341	17	20	91	<.4	<2	112	<1	55	574	4.12	<2	60	<5	<5	19	<2	<2	7	<3	<2	966	7.49	<.01	.58	.14	<.01	.02
S9330379	222465*14 2B341	16	16	102	<.4	9	388	<1	35	414	3.53	<2	73	<5	<5	20	<2	<2	9	<3	2	529	5.16	<.01	.80	.28	<.01	.02
S9330380	222466*14 2B342	7	19	44	<.4	5	128	<1	6	63	1.72	<2	57	<5	<5	28	<2	<2	8	<2	2	232	.71	<.01	.72	.15	<.01	.02
S9330381	222467*14 2B341	3	9	27	<.4	<2	114	<1	2	21	1.11	<2	34	<5	<5	23	<2	<2	5	<2	3	38	.26	<.01	.79	.06	<.01	.01
S9330382	222468*14 2B341	7	17	45	<.4	<2	92	<1	5	55	2.50	<2	57	<5	<5	49	<2	<2	5	<2	2	118	.54	<.01	.88	.10	<.01	.01
S9330383	222469*14 2B341	9	18	62	<.4	7	120	<1	10	100	2.47	<2	54	<5	<5	44	<2	<2	8	<2	2	319	.94	<.01	.68	.18	<.01	.02
S9330384	222470*14 2B341	9	17	56	<.4	<2	336	<1	6	60	1.56	<2	44	<5	<5	37	<2	<2	13	<2	3	101	.61	<.01	.93	.26	.01	.02
S9330385	222471*14 2B341	9	25	67	<.4	2	409	<1	13	59	1.85	<2	41	<5	<5	25	<2	<2	15	<2	5	326	.62	<.01	.82	.54	<.01	.04
S9330386	222472*14 2B341	7	34	75	<.4	9	168	<1	6	66	2.53	<2	66	<5	<5	45	<2	<2	9	<2	3	162	.70	.01	.87	.19	<.01	.02
S9330387	222473*14 2B341	6	38	77	<.4	<2	163	<1	5	38	2.19	<2	40	<5	<5	19	<2	<2	9	<2	4	39	.41	<.01	.81	.13	<.01	.02
S9330388	222474*14 2Y341	7	24	62	<.4	<2	55	<1	7	66	3.13	<2	47	<5	<5	26	<2	<2	4	<2	4	193	.73	<.01	1.07	.05	<.01	.01

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Tl	Al	Ca	Na	K	
		ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	%	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	ppm	
59330389	222851*14	2B 31	15	16	128	<.4	3	645	1	13	40	2.40	<2	37	<5	45	<2	19	2	2	521	.54	.02	1.07	.83	.01	.05		
59330390	222852*14	X 42	83	44	68	<.4	<2	1082	1	14	44	2.18	<2	33	<5	<5	21	<2	<2	74	20	8	2007	.37	<.01	1.31	1.92	.01	.04
59330391	222853*14	2B 32	6	23	117	<.4	3	524	1	5	11	1.41	<2	11	<5	<5	26	<2	<2	12	<2	3	386	.14	<.01	.51	.58	.01	.04
59330392	222854*14	2B 31	10	32	213	<.4	7	490	1	12	30	2.39	<2	24	<5	<5	45	<2	<2	8	<2	2	430	.47	<.01	1.21	.38	.01	.10
59330393	222855*14	2B 32	10	69	325	<.4	2	878	5	10	29	2.50	<2	28	<5	<5	56	<2	<2	12	<2	2	392	.56	<.01	1.17	.49	.01	.05
59330394	222856*14	2B 32	9	52	267	<.4	4	469	6	14	32	2.05	<2	20	<5	<5	31	<2	<2	10	<2	2	1320	.44	<.01	.77	.43	.01	.07
59330395	222857*14	2B 32	7	51	247	<.4	9	192	1	13	20	2.83	<2	24	<5	<5	48	<2	<2	9	<2	2	494	.40	<.01	.88	.34	.01	.05
59330396	222858*14	2B 31	10	123	636	<.4	<2	432	4	15	24	2.96	<2	28	<5	<5	49	<2	<2	11	<2	3	1379	.39	<.04	1.04	.66	.01	.09
59330397	222859*14	2B 32	6	95	233	<.4	7	300	1	15	13	2.33	<2	18	<5	<5	34	<2	<2	9	<2	2	956	.20	<.02	.66	.33	.01	.09
59330398	222860*14	2B 31	29	84	229	<.4	<2	354	1	22	35	3.09	<2	18	<5	<5	21	<2	<2	21	<2	3	2115	.29	<.01	.99	.84	<.01	.15
59330399	222861*14	2B 32	22	25	98	<.4	<2	119	<1	15	16	3.93	<2	16	<5	<5	17	<2	<2	5	<2	3	395	.25	<.01	1.04	.18	<.01	.05
59330400	222862*14	2B 31	8	21	121	<.4	5	142	<1	8	18	2.05	<2	27	<5	<5	55	<2	<2	10	<2	2	169	.42	<.03	1.09	.28	.01	.03
59330401	222863*14	2B 32	6	81	293	<.4	<2	292	4	11	15	2.41	<2	17	<5	<5	39	<2	<2	12	<2	2	437	.24	<.01	.67	.37	.01	.04
59330402	222864*14	2B 32	16	138	329	.6	8	104	2	13	55	3.03	<2	31	<5	<5	42	<2	<2	23	10	10	1980	4.14	<.02	1.62	7.03	.01	.03
59330403	222865*14	2B341	14	86	449	<.4	<2	191	1	23	57	3.64	<2	50	<5	<5	61	<2	<2	11	<2	3	1264	.64	<.05	1.52	.50	<.01	.06
59330404	222866*11	2G 43	60	251	1709	<.4	10	599	14	8	79	1.67	<2	72	<5	<5	35	<2	9	46	11	7	353	.65	<.01	.98	1.80	<.01	.04
59330405	222867*14	2B 31	46	49	96	<.4	22	332	<1	24	69	5.58	<2	46	<5	<5	60	<2	<2	55	13	8	1286	.90	<.05	1.63	1.01	<.01	.03
59330406	222868*14	2B 32	25	26	98	<.4	<2	104	1	16	29	3.14	<2	20	<5	<5	22	<2	<2	95	10	26	3076	.34	<.02	1.11	1.11	.01	.04
59330407	222869*14	2B 32	19	17	36	<.4	<2	31	<1	8	26	3.21	<2	26	<5	<5	41	<2	<2	17	2	7	173	.55	<.05	1.38	.38	.01	.02
59330408	222870*14	3B 43	58	<4	16	<.4	<2	106	<1	3	30	.37	<2	5	<5	<5	2	<2	<2	729	12	12	1184	.16	<.01	.37	6.93	<.01	.02
59330409	222475*14	2B341	6	24	81	<.4	<2	193	<1	6	60	2.27	<2	43	<5	<5	19	<2	<2	9	<2	4	109	.60	<.01	1.02	.12	<.01	.01
59330410	222476*14	2B342	7	35	131	<.4	15	615	<1	13	102	2.38	<2	28	<5	<5	24	<2	<2	13	<2	4	264	1.26	<.01	.67	.34	<.01	.02
59330411	222477*14	2B341	2	18	32	<.4	9	117	<1	1	4	1.00	<2	12	<5	<5	9	<2	<2	4	<2	7	63	.06	<.01	.70	.04	<.01	.01
59330412	222478*14	2B341	4	20	31	<.4	5	198	<1	4	7	1.08	<2	6	<5	<5	4	<2	<2	16	2	4	236	.09	<.01	.46	.36	<.01	.02
59330413	222479*14	2B341	4	59	81	<.4	<2	256	<1	2	14	1.92	<2	28	<5	<5	22	<2	<2	7	<2	3	26	.18	<.01	.75	.07	<.01	.02
59330414	222480*14	2B341	4	8	11	<.4	<2	86	<1	<1	2	.63	<2	9	<5	<5	4	<2	<2	2	<2	5	.03	<.01	.76	<.01	<.01	<.01	
59330415	222481*14	2B341	2	9	12	<.4	<2	58	<1	<1	1	.38	<2	13	<5	<5	4	<2	<2	3	<2	2	.45	.03	<.01	.74	.01	<.01	.01
59330416	222764*14	1B 31	28	11	70	<.4	<2	135	<1	11	41	2.33	<2	41	<5	<5	54	<2	<2	13	<2	2	322	.68	<.03	1.36	.49	.01	.07
59330417	222765*14	2B 31	22	50	58	<.4	4	78	<1	13	61	2.25	<2	31	<5	<5	43	<2	<2	25	6	6	457	.90	<.03	1.42	.84	.02	.03
59330418	222766*14	2B342	14	17	78	<.4	7	116	<1	10	23	2.87	<2	31	<5	<5	65	<2	<2	13	<2	2	365	.43	<.06	1.27	.40	<.01	.09
59330419	222767*14	2B 31	41	9	44	<.4	11	65	<1	12	85	2.07	<2	33	<5	7	39	<2	<2	12	2	2	199	1.20	<.03	1.19	.32	<.01	.06
59330420	222768*14	2B341	12	6	72	<.4	<2	59	<1	7	22	3.25	<2	44	<5	5	78	<2	<2	9	<2	<2	161	.48	<.05	1.62	.25	<.01	.04
59330421	222769*14	2B 31	16	8	87	<.4	5	153	<1	22	26	2.85	<2	43	<5	<5	67	<2	<2	22	<2	3	1682	.50	<.02	1.27	.42	<.01	.06
59330422	222770*14	2B 31	16	7	42	<.4	<2	90	<1	6	20	1.54	<2	27	<5	<5	37	<2	<2	11	<2	2	151	.53	<.01	1.20	.27	<.01	.03
59330423	222771*14	2B431	17	<4	36	<.4	8	88	<1	6	22	1.70	<2	34	<5	<5	42	<2	<2	13	<2	2	202	.52	<.02	1.12	.32	<.01	.03
59330424	222772*14	2B 31	8	5	32	<.4	<2	60	<1	4	13	1.34	<2	22	<5	<5	33	<2	<2	10	<2	2	113	.39	<.02	.85	.25	<.01	.03

LAB NO	FIELD NUMBER	Cu	Pb	Zn	Ag	As	Ba	Cd	Co	Ni	Fe	Mo	Cr	Bi	Sb	V	Sn	W	Sr	Y	La	Mn	Mg	Ti	Al	Ca	Na	K
		ppm	%	ppm	ppm	ppm	ppm	ppm																				
S9330425	222773*14 2B341	16	5	56	<.4	11	97	<1	12	29	2.06	<2	33	<5	<5	43	<2	<2	14	2	3	349	.54	.02	1.27	.35	.01	.03
S9330426	222774*14 2B 32	12	14	120	<.4	<2	183	<1	8	30	2.95	<2	36	<5	<5	73	<2	<2	12	<2	2	195	.63	.04	1.42	.54	.01	.03
S9330427	222775*14 2B 31	14	11	79	<.4	7	121	<1	9	61	2.12	<2	32	<5	<5	43	<2	<2	10	<2	2	150	.65	<.01	1.12	.39	.01	.04
S9330428	222776*14 1B 31	13	47	218	<.4	6	98	1	11	68	2.98	<2	40	<5	<5	52	<2	2	13	5	4	375	.86	.03	1.92	.97	.01	.04
S9330429	222359* 222X 1	13	25	61	<.4	2	296	<1	13	30	2.33	<2	34	<5	<5	31	<2	<2	17	3	8	406	.61	.01	1.46	.48	.01	.05
S9330430	222360* 212Y	35	54	125	<.4	8	184	<1	15	48	2.98	<2	35	<5	<5	37	<2	<2	14	2	4	373	.74	.02	1.34	.41	.01	.06
S9330431	222072*24 2B 31	19	17	63	<.4	5	192	<1	6	55	3.18	<2	25	<5	<5	26	<2	<2	5	<2	<2	157	.60	<.01	.87	.07	<.01	.01
S9330432	222073*24 3B 31	33	13	59	<.4	25	85	<1	5	27	4.16	<2	18	<5	<5	18	<2	<2	5	<2	2	173	.19	<.01	.61	.07	<.01	.01
S9330433	222074*24 2G 31	117	18	173	<.4	43	157	<1	6	55	3.42	2	11	<5	<5	25	<2	<2	21	5	3	174	.09	<.01	.61	.38	<.01	.01
S9330434	222075*24 3B 31	63	17	105	<.4	42	191	<1	14	96	3.33	<2	20	<5	<5	18	<2	<2	18	3	3	569	.82	<.01	.62	.26	<.01	.02
S9330435	222076*24 2G 31	80	19	118	<.4	30	429	<1	44	287	3.67	<2	25	<5	<5	13	<2	<2	23	7	5	928	3.43	<.01	.66	.29	<.01	.01
S9330436	222077*24 2G 41	68	18	325	1.1	23	771	1	21	141	2.84	<2	27	<5	<5	14	<2	2	40	12	4	835	.95	<.01	.82	.52	<.01	.01
S9330437	222078*24 2G 31	31	9	85	<.4	6	358	<1	17	166	2.59	<2	70	<5	<5	23	<2	2	20	3	3	267	1.75	<.01	.78	.29	.01	.01
S9330438	222079*24 2G 31	71	11	89	<.4	<2	219	<1	32	358	2.98	<2	26	<5	<5	21	<2	2	20	6	2	679	3.79	<.01	.77	.33	.01	.01
S9330439	222080*24 2B 31	12	20	73	<.4	6	689	<1	17	102	3.79	<2	38	<5	<5	26	<2	<2	5	<2	<2	352	1.15	<.01	.91	.06	<.01	.03
S9330440	222081*24 2B 31	12	13	72	<.4	<2	274	<1	14	102	3.15	<2	67	<5	<5	45	<2	<2	6	<2	<2	266	1.35	<.01	.91	.09	.01	.01
S9330441	222082*24 2G 31	18	8	80	<.4	8	259	<1	25	296	3.16	<2	64	<5	<5	20	<2	<2	13	2	<2	459	4.17	<.01	.67	.19	<.01	.02
S9330442	222083*24 2G 31	44	9	177	.7	<2	382	1	17	232	3.16	<2	89	<5	<5	28	<2	2	17	17	8	493	2.17	<.01	1.28	.27	.01	.01
S9330443	222084*24 2B 31	27	18	72	<.4	21	150	<1	21	141	3.53	<2	43	<5	<5	27	<2	<2	8	<2	<2	556	1.73	<.01	.80	.11	<.01	.01
S9330444	222085*24 1K 31	37	20	89	<.4	15	207	<1	12	96	2.73	<2	30	<5	<5	21	<2	<2	60	11	12	273	2.16	<.01	.63	3.04	<.01	.01
S9330445	222086*24 2B 31	59	66	110	.4	2	462	<1	22	170	2.97	<2	63	<5	<5	24	<2	<2	25	10	7	466	1.81	<.01	.84	.49	<.01	.01
S9330446	222104*24 1G 31	6	6	25	<.4	6	175	<1	3	29	1.16	<2	19	<5	<5	16	<2	<2	2	<2	2	72	.29	<.01	.69	.02	<.01	.01
S9330447	222105*24 1G 31	8	9	49	<.4	3	242	<1	8	53	2.15	<2	32	<5	<5	25	<2	<2	8	<2	<2	222	.72	<.01	.76	.09	<.01	.01
S9330448	222106*24 2B231	18	23	117	<.4	<2	161	<1	13	64	3.85	<2	54	<5	<5	31	<2	<2	13	<2	<2	305	.72	<.01	.94	.34	<.01	.01
S9330449	222114*24 2B 31	19	12	108	<.4	19	162	<1	4	20	2.77	5	31	<5	<5	38	<2	<2	9	3	2	175	.23	<.01	.76	.10	<.01	.01
S9330450	222115*24 2B 31	11	9	53	<.4	<2	170	<1	2	13	1.80	<2	21	<5	<5	21	<2	<2	7	2	3	<5	.41	<.01	1.22	.08	<.01	.01
S9330451	222116*24 2G 31	21	13	100	<.4	5	237	1	8	39	2.47	3	81	<5	<5	40	<2	<2	24	5	3	373	.48	<.01	.64	.41	.01	.02
S9330452	222117*24 3B 31	41	11	44	.5	<2	158	<1	7	46	3.60	<2	92	<5	<5	50	<2	<2	6	<2	<2	175	1.06	<.01	1.40	.10	.01	.01
S9330453	222826* 221B 2	20	46	159	<.4	5	222	<1	24	93	3.55	<2	69	<5	<5	68	<2	<2	21	2	2	373	1.26	.04	1.83	.38	.01	.04
S9330454	222827* 221B 2	25	48	82	<.4	5	84	<1	30	154	4.14	<2	62	<5	<5	42	<2	<2	23	2	5	426	1.84	.03	1.46	.35	.01	.03
S9330455	222871*14 K 43	49	<4	20	<.4	<2	112	<1	2	38	.30	<2	8	<5	<5	2	<2	<2	554	17	21	301	.12	<.01	.45	6.90	.01	.01
S9330456	222872*14 2B 42	6	38	35	<.4	10	53	<1	6	12	2.35	<2	11	<5	<5	8	<2	<2	163	18	37	545	.09	<.01	.71	1.50	<.01	.02
S9330457	222873*14 2B 41	10	10	44	<.4	9	50	<1	9	22	2.31	<2	28	<5	<5	53	<2	<2	26	<2	4	205	.51	.04	1.34	.37	.01	.05

I=insufficient sample X=small sample E=exceeds calibration C=being checked R=revised  
 If requested analyses are not shown, results are to follow

## ANALYTICAL METHODS

ICP PACKAGE : 0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

GYGNET-WD

Job V 93-0428R

Report date 22 OCT 1993

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	Ba(4) ppm	Pb(1) %	Zn(1) %	Ag(1) g/t	Ag(1) oz/t
R9305650	WR93-046	18	E16700	E24300	41.3	E185432	2.17	2.96	39.90	1.164
R9305651	WR93-047	110	E39900	E40000	82.9	E188601	4.75	4.15	86.03	2.509
R9305681	NR-93-36	13	2110	6840	2.6	233		0.73		
R9305682	NR-93-37	9	5030	3840	5.6	E23275	0.59		6.77	0.197
R9305683	NR-93-38	18	3590	E16800	5	292		1.62	6.90	0.201
R9305684	NR-93-39	7	3860	1850	5.1	168			6.83	0.199
R9305685	NR-93-40	16	369	E17100	1.4	20		1.65		
R9305686	NR-93-41	10	8760	E18700	11.3	E27961	0.94	1.62	11.77	0.343

I=insufficient sample X=small sample E=exceeds calibration C=being checked R=revised

If requested analyses are not shown, results are to follow

ANALYTICAL METHODS

- Cu Aqua Regia decomposition / AAS
- Pb Aqua Regia decomposition / AAS
- Zn Aqua Regia decomposition / AAS
- Ag Aqua Regia decomposition / AAS
- Ba(4) X-Ray fluorescence / pressed pellet
- Pb(1) Assay
- Zn(1) Assay
- Ag(1) Fire assay, lead collection / Gravimetric finish
- Ag(1) Fire assay, lead collection / AA finish (low level) 1/2 A.T.

CYGNET-WD

Job V 93-0455R

Report date 22 OCT 1993

LAB NO	FIELD NUMBER	SiO <sub>2</sub>	TiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	FeO	MnO	MgO	CaO	Na <sub>2</sub> O	K <sub>2</sub> O	P <sub>2</sub> O <sub>5</sub>	Ba	LOI
		%	%	%	%	%	%	%	%	%	%	%	%	%
R9305847	WR93-063	84.01	0.18	2.87	1.57	0.05	1.69	2.63	0.01	0.79	0.04	0.30	4.81	98.95
R9305848	W93-053B	48.46	2.26	13.35	14.61	0.22	6.34	7.85	2.92	0.08	0.23	0.01	3.58	99.91
R9305849	W93-065	67.87	0.63	15.07	4.52	0.06	3.11	0.65	2.32	2.33	0.13	0.15	3.11	99.95
R9305850	W93-053A	59.05	0.90	14.44	9.70	0.22	3.29	5.31	3.71	1.07	0.20	0.04	1.93	99.86
R9305851	W93-057	81.57	0.36	9.28	2.47	0.03	0.41	0.18	2.82	1.50	0.05	0.06	1.33	100.06
R9305852	W93-055	69.57	0.58	13.61	3.47	0.05	1.17	1.69	1.76	4.15	0.15	0.16	3.68	100.04
R9305853	W93-053C	50.04	2.41	13.50	13.46	0.20	5.23	5.58	3.29	0.05	0.42	0.01	5.30	99.49
R9305854	S93-723-1	47.32	2.63	15.18	15.41	0.03	9.12	0.75	0.11	1.42	0.50	0.15	6.56	99.18
R9305855	S93-723-2	73.16	0.63	14.42	1.76	0.04	0.64	0.35	2.72	3.50	0.17	0.14	2.09	99.62
R9305856	S93-723-2A	71.96	0.65	14.20	2.92	0.02	0.77	0.28	1.47	4.25	0.17	0.39	2.61	99.69
R9305857	S93-723-3	58.78	2.18	14.01	10.95	0.08	4.33	0.44	3.96	0.73	0.24	0.18	3.15	99.03
R9305858	S93-723-3A	47.35	2.36	14.65	12.83	0.14	5.53	4.31	3.61	0.88	0.30	0.42	6.93	99.31
R9305859	S93-723-4	48.21	2.29	14.40	11.99	0.10	6.67	3.81	0.78	2.46	0.32	0.88	7.43	99.34
R9305860	S93-723-4A	46.77	2.50	14.55	12.30	0.15	7.32	3.98	1.45	1.85	0.34	0.56	7.83	99.60

I=insufficient sample X=small sample E=exceeds calibration C=being checked R=revised

If requested analyses are not shown ,results are to follow

## ANALYTICAL METHODS

FeO determined by acid digestion /volumetric. LOI determined gravimetrically

Other elements by Li borate fusion/XRF . Where no FeO value shown 'Fe<sub>2</sub>O<sub>3</sub>' is total Fe as Fe<sub>2</sub>O<sub>3</sub>

CYGNET-WD

JOB V 93-0455R

Report date 22 OCT 1993

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %	
R9305847	WR93-063	24	4	21	<.4	6	612	<1	2	6	.77	<2	91	<5	<5	3	<2	<2	402	2	5	354	.91	<.01	.18	1.95	<.01	.10	
R9305848	W93-053B	77	<4	47	<.4	<2	25	<1	31	27	5.68	<2	32	<5	<5	149	9	<2	31	14	2	884	2.38	.39	2.86	1.32	.04	<.01	
R9305849	W93-065	7	14	68	<.4	20	111	<1	6	12	2.76	<2	65	<5	<5	11	<2	<2	9	12	33	252	1.63	.05	2.07	.27	.02	.16	
R9305850	W93-053A	161	4	64	<.4	13	38	<1	14	5	3.42	<2	44	<5	<5	102	<2	<2	43	7	3	578	1.15	.14	1.68	1.21	.13	.12	
R9305851	W93-057	8	16	24	<.4	<2	.93	<1	3	8	1.32	<2	148	<5	<5	3	<2	2	6	2	25	152	.11	<.01	.40	.04	.04	.21	
R9305852	W93-055	4	12	15	<.4	5	157	<1	3	5	1.09	<2	38	<5	<5	2	<2	<2	17	6	9	245	.09	<.01	.35	1.22	.01	.40	
R9305853	W93-053C	19	<4	44	<.4	<2	14	<1	26	23	7.23	<2	40	<5	<5	174	<2	<2	57	21	3	1088	2.90	.15	3.35	2.08	.02	<.01	
R9305854	S93-723-1	41	<4	213	<.4	<2	203	<1	17	75	8.54	<2	120	<5	<5	13	117	<2	<2	41	9	13	<5	4.70	<.01	5.21	.43	<.01	.16
R9305855	S93-723-2	6	16	51	<.4	2	158	<1	6	6	.42	<2	55	<5	<5	<2	<2	<2	13	6	15	311	.03	<.01	.32	.29	.02	.35	
R9305856	S93-723-2A	8	20	39	<.4	3	463	<1	3	5	.82	<2	95	<5	<5	2	<2	2	11	6	20	77	.04	<.01	.48	.13	.02	.54	
R9305857	S93-723-3	47	<4	80	<.4	<2	219	<1	19	70	6.08	<2	141	<5	<5	140	<2	<2	10	5	11	173	2.52	.04	3.01	.25	.04	.09	
R9305858	S93-723-3A	90	<4	91	<.4	22	227	<1	32	86	7.07	<2	137	<5	<5	186	<2	<2	80	7	9	833	3.09	.02	3.57	2.91	.02	.05	
R9305859	S93-723-4	78	4	88	<.4	4	350	<1	32	80	6.55	<2	98	<5	<5	121	<2	<2	56	7	11	604	3.41	<.01	3.72	2.58	<.01	.18	
R9305860	S93-723-4A	83	<4	87	<.4	50	258	<1	31	80	6.53	<2	116	<5	<5	8	132	<2	<2	73	7	10	900	3.67	<.01	3.88	2.66	.01	.15

I=insufficient sample X-small sample E-exceeds calibration C-being checked R=revised

If requested analyses are not shown ,results are to follow

## ANALYTICAL METHODS

ICP PACKAGE :0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

CYGNET-WD

Job V 93-0428R

Report date 22 OCT 1993

LAB NO	FIELD NUMBER	SiO <sub>2</sub>	TiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	FeO	MnO	MgO	CaO	Na <sub>2</sub> O	K <sub>2</sub> O	P <sub>2</sub> O <sub>5</sub>	Ba	LOI
		%	%	%	%	%	%	%	%	%	%	%	%	%
R9305649	WR93-044	0.13	0.04	0.35	2.53	0.13	7.98	12.57	1.52	0.05	0.06	7.02	31.83	64.21
R9305652	WR93-048	57.42	0.01	0.05	0.38	0.02	8.07	13.72	0.09	0.02	0.07	0.19	19.74	99.78
R9305653	WR93-049	59.20	0.81	19.66	7.47	0.07	1.32	0.25	0.33	5.61	0.11	0.22	4.69	99.74
R9305654	WR93-054	64.57	0.77	15.83	5.51	0.02	3.51	0.26	1.13	3.30	0.12	0.16	4.58	99.76
R9305655	WR93-055	70.30	0.65	14.15	3.86	0.04	1.46	0.34	0.91	4.98	0.16	0.20	2.85	99.90
R9305656	WR93-056	97.96	0.04	0.51	0.55	0.01	0.01	0.15	0.01	0.05	0.01	0.02	0.32	99.64
R9305657	WR93-059	87.18	0.26	4.46	3.01	0.02	0.94	0.18	0.11	0.93	0.06	0.40	1.92	99.47
R9305658	WR93-063	88.78	0.17	2.99	1.56	0.08	0.81	1.13	0.06	0.86	0.04	0.33	2.46	99.27
R9305659	WR93-064	77.37	0.54	9.33	3.92	0.01	0.80	0.13	0.07	2.42	0.09	0.98	3.22	98.88
R9305660	WR93-052	80.58	0.45	7.30	3.51	0.02	1.15	0.17	0.07	2.09	0.05	0.72	2.84	98.95
R9305678	NR-93-33	0.22	0.01	0.25	0.20	0.02	0.38	54.51	0.01	0.06	0.01	0.01	43.55	99.23
R9305679	NR-93-34	0.22	0.01	0.23	1.57	0.09	16.94	33.73	0.02	0.05	0.05	0.44	46.01	99.36
R9305680	NR-93-35	6.33	0.09	2.59	1.59	0.06	18.03	27.32	0.05	0.63	0.06	0.01	42.48	99.24
R9305687	NR-93-42	0.21	0.02	0.24	1.23	0.10	19.96	30.58	0.03	0.04	0.04	0.02	47.06	99.53

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If requested analyses are not shown ,results are to follow

## ANALYTICAL METHODS

FeO determined by acid digestion /volumetric. LOI determined gravimetrically

Other elements by Li borate fusion/XRF .Where no FeO value shown 'Fe<sub>2</sub>O<sub>3</sub>' is total Fe as Fe<sub>2</sub>O<sub>3</sub>

CYGNET-WD

Job V 93-0428R

Report date 22 OCT 1993

LAB NO	FIELD NUMBER	Cu ppm	Pb ppm	Zn ppm	Ag ppm	As ppm	Ba ppm	Cd ppm	Co ppm	Ni ppm	Fe %	Mo ppm	Cr ppm	Bi ppm	Sb ppm	V ppm	Sn ppm	W ppm	Sr ppm	Y ppm	La ppm	Mn ppm	Mg %	Ti %	Al %	Ca %	Na %	K %
R9305649	WR93-044	54	1335172400	3.1	8	86	1111	<1	2	1.35	<2	<4	<5	<5	<2	<2	<2	72	<2	<2	738	4.91	<.01	.01	8.38	<.01	<.01	
R9305652	WR93-048	6	585	611	1.1	4	1094	5	<1	2	.19	<2	60	<5	<5	<2	<2	40	<2	<2	98	4.75	<.01	<.01	9.70	<.01	<.01	
R9305653	WR93-049	20	264	326	.4	<2	907	2	18	40	4.29	<2	19	<5	<5	4	<2	<2	21	2	23	659	.37	<.01	.79	.11	.01	.24
R9305654	WR93-054	20	56	146	<.4	<2	220	<1	4	32	3.08	2	45	<5	5	18	<2	<2	9	2	9	102	1.50	<.01	1.83	.11	.01	.17
R9305655	WR93-055	5	99	149	<.4	12	421	<1	4	8	1.28	<2	47	<5	<5	2	<2	<2	10	5	10	249	.08	<.01	.41	.18	.01	.37
R9305656	WR93-056	3	33	45	<.4	2	150	<1	<1	6	.35	<2	208	<5	<5	<2	<2	<2	2	<2	<2	52	.02	<.01	.03	.03	<.01	<.01
R9305657	WR93-059	40	32	101	<.4	6	491	<1	6	35	1.88	<2	108	<5	<5	15	<2	<2	21	<2	11	201	.44	<.01	.68	.06	<.01	.08
R9305658	WR93-063	12	13	34	<.4	12	565	<1	2	9	.82	<2	101	<5	6	2	<2	<2	185	<2	3	665	.38	<.01	.15	.86	<.01	.09
R9305659	WR93-064	55	15	132	.9	27	1056	<1	5	32	2.37	<2	69	<5	5	10	<2	<2	17	2	16	65	.04	<.01	.40	.02	<.01	.18
R9305660	WR93-052	41	35	629	1.2	24	781	3	5	61	2.12	<2	71	<5	7	22	<2	<2	11	2	20	75	.25	<.01	.50	.03	<.01	.18
R9305678	NR-93-33	1	30	53	<.4	2	42	<1	<1	<1	.08	<2	<4	<5	<5	<2	<2	<2	1499	<2	<2	96	.18	<.01	<.01	36.65	<.01	<.01
R9305679	NR-93-34	<1	36	384	.4	7	1259	1	<1	<1	.78	<2	4	<5	<5	3	<2	<2	42	2	<2	527	9.61	<.01	.01	21.49	.01	<.01
R9305680	NR-93-35	<1	5	6	<.4	6	12	<1	1	4	.79	<2	5	<5	<5	2	<2	<2	57	6	3	386	10.10	<.01	.08	17.90	.02	.04
R9305687	NR-93-42	<1	17	832	.4	19	180	4	<1	1	.60	<2	<4	<5	<5	<2	<2	<2	35	<2	<2	610	11.22	<.01	.01	21.48	.01	<.01

I=inufficient sample X-small sample E=exceeds calibration C=being checked R=revised

If requested analyses are not shown ,results are to follow

## ANALYTICAL METHODS

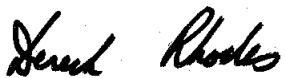
ICP PACKAGE :0.5 gram sample digested in hot reverse aqua regia (soil,silt) or hot Aqua Regia(rocks).

### APPENDIX III

#### STATEMENT OF QUALIFICATIONS

I, Dereck Rhodes, of the District of North Vancouver, in the Province of British Columbia make oath and say:

1. THAT I am a geologist residing at 2514 Bronte Road, North Vancouver, British Columbia with a business address at 700-409 Granville Street, Vancouver, British Columbia.
2. THAT I graduated with a B.Sc in geology from McMaster University, Hamilton, Ontario in 1969.
3. THAT I have practised geology with Cominco Ltd. from June, 1969 to present.




Dereck Rhodes  
Senior Geologist

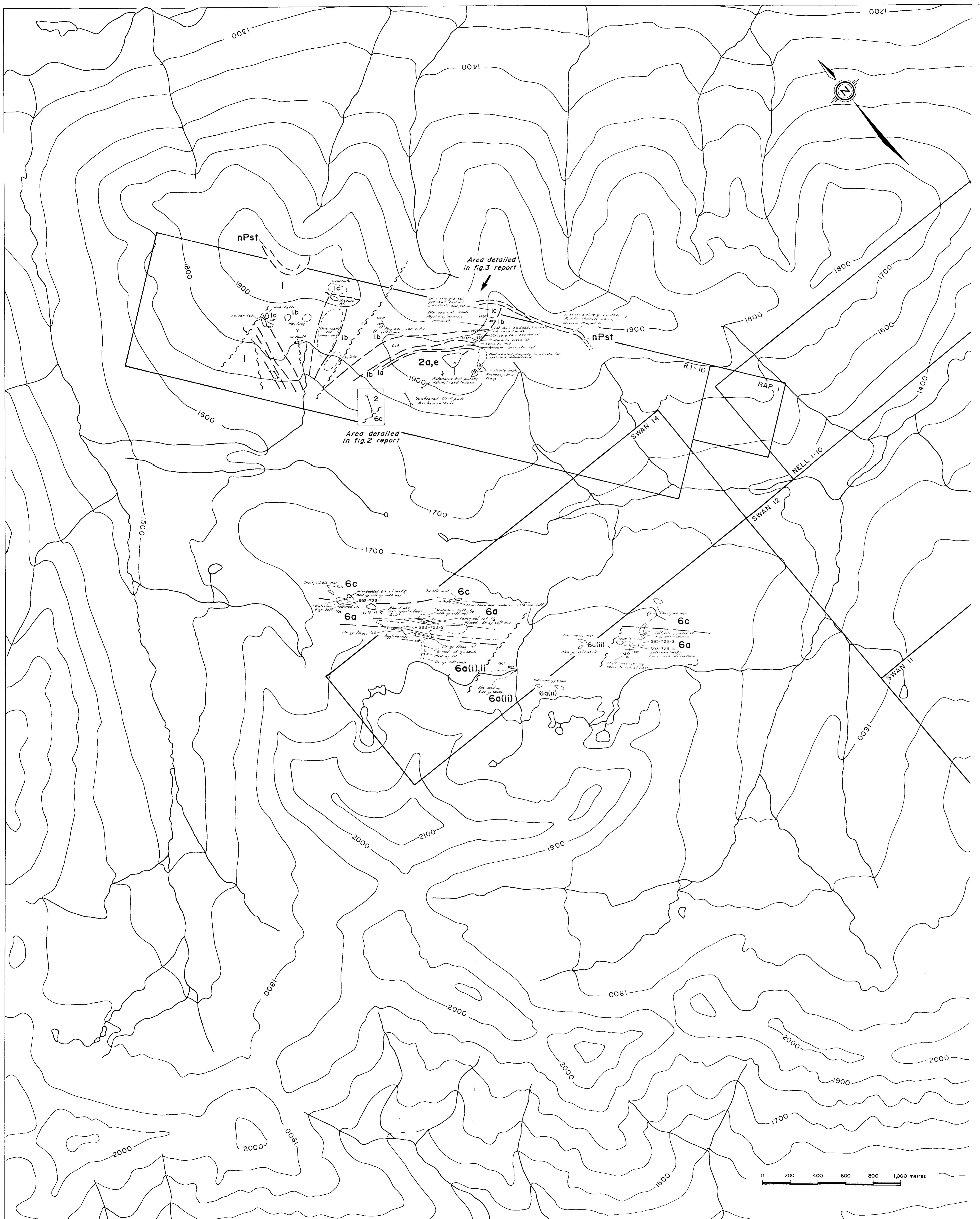
DR/dr

February 1994

23,321

GEOLOGICAL BRANCH  
ASSESSMENT REPORT





# GEOLOGICAL BRANCH ASSESSMENT REPORT

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1994 PAR LEGEND

(Older stratigraphic terminology is used with equivalent stratigraphic nomenclature defined by Ferri in brackets)

## **Upper Devonian - Lower Mississippian**

**EARN GROUP (BIG CREEK GP)**

- 6** Undifferentiated

**6a** GILLILAND TUFF - Andesitic to rhyolitic ash tuffs, crystal tuffs, lapilli tuffs, agglomerates and volcaniclestics.

6a(i) LIMESTONE dark grey, flaggy limestone interbedded or associated with volcanics

6a(ii) NON SILICEOUS MUDSTONES - soft, grey to dark grey mudstones interbedded with either volcanics or 6a(i) limestones.

**6b** LIMESTONES/DOLOMITES black, carbonaceous fetid limestones and/or dolomites, sometimes crinoidal that appear to be interbedded with 6c black siliceous mudstones.

**6c** BLACK, CARBONACEOUS, SILICEOUS SHALE AND MUDDY CHERT. Thin, planar bedded (0.5-10 cm), silver to blue-grey weathering, clinky sound when struck.

Middle Devonian

McDAME GROUP (OTTER LAKES GROUP)

- 5** (undifferentiated)

Early Silurian - Early Devonian

**SANDPILE GROUP (ECHO LAKE GROUP)**  
(lithologies not necessarily in stratigraphic order)

**4** (undifferentiated)

**4a** FINE-MEDIUM GRAINED, MOTTLED LIGHT-MEDIUM GREY AND GREENISH BUFF DOLOMITE  $\pm$  LIMESTONE. Bedding is generally indistinct, undulatory algal laminations locally, silica ribs and blobs are common and locally define bands (< 1.0 m) with up to 50% silica, dark grey ooids (1-2 mm) locally, may be fetid and crackle brecciated.

**4b** MEDIUM-COARSE CRYSTALLINE WHITE-LIGHT GREY DOLOMITE. Massive-medium bedded (10-20 cm), may have sucrosic or "salt and pepper" appearance, coarse grained sections typically lighter colour, occasional bituminous vugs or crackle network, locally zebra and fenestral texture, patchy silicification.

**4c** MEDIUM-DARK GREY, FINE-MEDIUM CRYSTALLINE DOLOMITE  $\pm$  LIMESTONE. Characterized by fenestral fabric defined by lenses and discontinuous laminations of white dolomite, faint fetid odour, locally oolitic bioturbated.

**4e** INTENSELY SILICIFIED DOLOMITE - rock composed of 60-100% silica nodding and replacing dolomite locally Sandpile lithologies evident elsewhere host carbonate of uncertain affinity.

**4f** DOLOMITE HOSTING SAND GRAINS - medium bedded, light to dark grey dolomites with 1-10% disseminated, well rounded quartz sand grains.

ATTAN GROUP

### **Lower Cambrian (to Middle Cambrian)**

#### **ROSELLA FORMATION (Mt. Kison F)**

Rosetta lithologies not necessarily in stratigraphic order.

- 2** (undifferentiated)

**2a** MEDIUM-DARK GREY, OOLITIC, ARGILLACEOUS LIMESTONE. Medium-thick bedded (10-50 cm) to nodular, variably argillaceous and carbonaceous,  $\pm$  (0.5 mm - 5.0 mm oolites), wavy to irregular partings and bedding surfaces,  $\pm$  bioturbated,  $\pm$  zebra texture,  $\pm$  rose-reddish colouration, Archeocyathids (up to 5.0 cm) locally.

**2b** MEDIUM-DARK GREY, OOLITIC, ARGILLACEOUS DOLOMITE. Dolomitized equivalent of unit 2a? Dolomite is fine-medium crystalline, medium to thick bedded, local oolitic beds consist of 10-80% rounded, black oolites interbedded with argillaceous beds.

**2c** MEDIUM GREY TO WHITE, FINE-MEDIUM CRYSTALLINE LIMESTONE AND/OR DOLOMITE. Predominantly fine crystalline, clean limestone with lesser fine-medium (sucrosic) grained dolomite. Massive to non-descript mottled texture; thin, indistinct wavy bedding and crinkly algal laminations; local dark grey argillaceous bands (<2 cm) and black bituminous fracture networks and stylolite seams; few Archeocyathids observed.

**2d** WHITE TO LIGHT GREY OR CREAM COLOURED, COARSELY RECRYSTALLIZED DOLOMITES  $\pm$  MINOR LIMESTONE. May represent a dolomitized and/or coarsely recrystallized equivalent of unit 2c. Light cream to light gray, coarse (2-10 mm) rhombic dolomite and minor calcite, minor argillaceous laminae or patches, no fossils observed.

**2e** VARIABLY CALCAREOUS TO NON-CALCAREOUS SHALE. Occurs in association with Unit 2. Appears to occur at the base of the Rosella as well as higher up in the Rosella stratigraphy. It may represent a more shaly end member of unit 2a, which also occurs at more than one stratigraphic position. The shale is dark grey-black, commonly fissile,  $\pm$  laminated, silty to muddy, and very calcareous to non-calcareous. Includes shales in upper portions of Rosella that have Salterellip (Area 3N) (L.C.) or trilobites of (Upper L.C.) (Area 3S). Similar shales and argillaceous limestones in apparent conformity with underlying Rosella Fm lithologies host trilobites dated as Middle Cambrian on Razorback Ridge. There are for the present included within the Rosella (Mt. Kison) Fm rather than the Razorback Fm as defined by Ferry.

Lower Cambrian

**BOYA FM (MOUNT BROWN FORMATION)**

(In 1993 map/report referred to as Transitional Phyllite Unit)

- Private Use)

1 BOYA FM (Undifferentiated)

1a INTERBANDED NODULAR LIMESTONE AND LIMY, SERICITIC MUDSTONE. Light green-grey, variably sericitic mudstone  $\pm$  siltstone interbanded with nodular, argillaceous limestone. Sericitic mudstone component is generally < 25%. Phyllitic appearance with increased sericite content.

1b LIGHT TO MEDIUM GREEN-GREY, VARIABLY CALCAREOUS, SERICITIC, PHYLLITIC MUDSTONE,  $\pm$  MINOR VOLCANIC TUFF,  $\pm$  MINOR SILTY SANDSTONE. Weathered outcrops and trench exposures are poorly indurated, have a very friable fibrous "woody" texture, and a wavy, crenulated and kinked foliation.

1c QUARTZITE - Quartz sandstones lesser siltstones

NEOPROTOSAURIC

NEOPROTEROZOIC  
INGENIKA GROUP

**nPst** PHYLLOLITE, SCHIST AND IMPURE QUARTZITE:  
green-grey, crenulated. LIMESTONE: white,  
honey coloured to bluish-grey, clean with thin  
micaceous partings. PHYLLOLITE, SLATE AND  
SILTSTONE: dark blue-grey to black, graphitic,  
locally containing biotite and garnet.


## Symbols


- | <u>Symbols</u> |                  |  |
|----------------|------------------|--|
|                | outcrop          |  |
|                | subcrop          |  |
| — — —          | defined contact  | 140° / 60°                               |
| - - - - -      | inferred contact | ▲ rock sample                            |
|                | fault            | * * x float, abundant rock chips in soil |
|                |                  | → ← trench                               |

# CYGNET PROPERTY

GEOLOGY

OMINECA M.D., B.C.





SYMBOLS

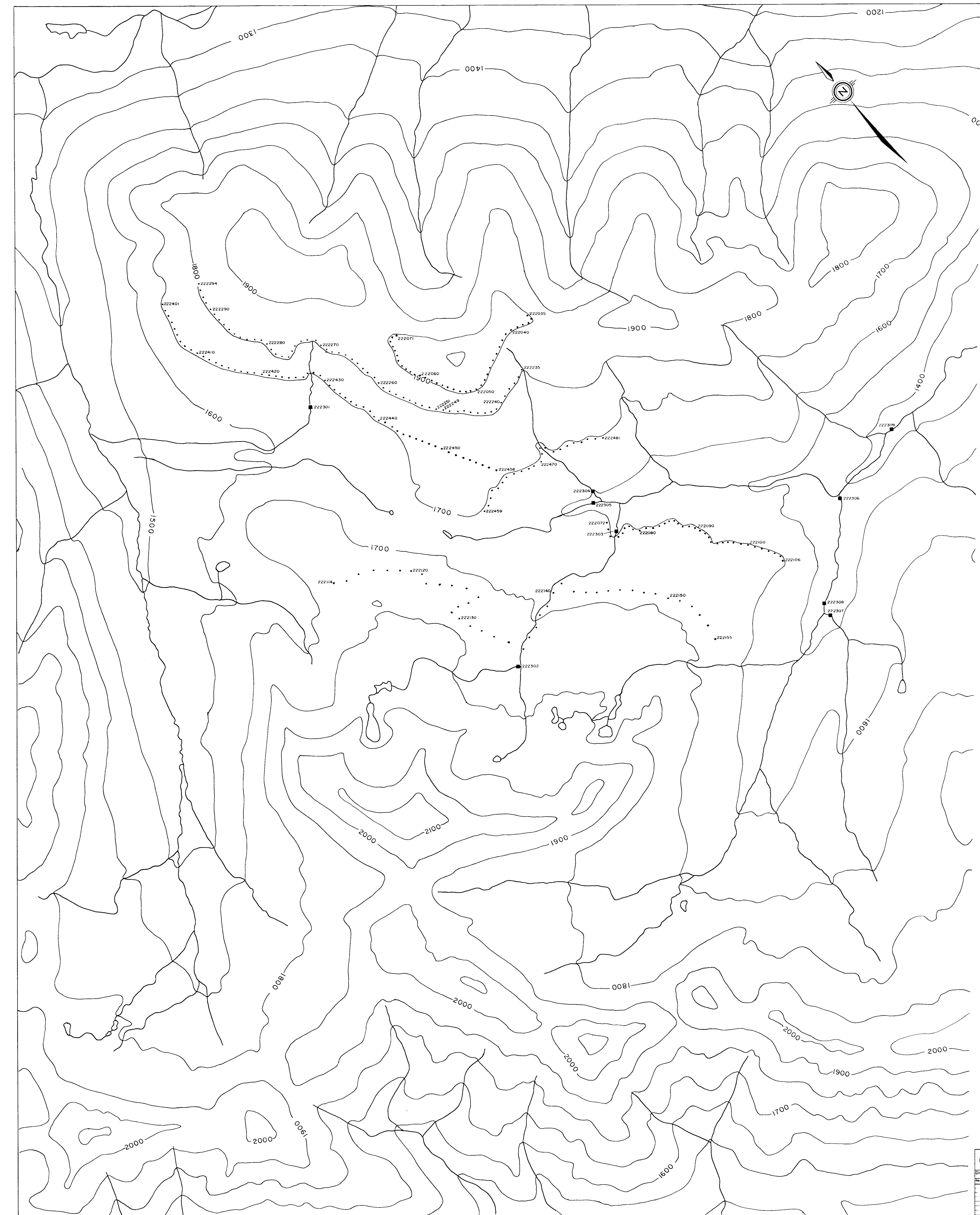
● Soil Sample Site  
■ Stream Sediment Site

GEOLOGICAL BRANCH  
ASSESSMENT REPORT

**23,321**

CYGNET PROPERTY		(EAST HALF)	R.T.C. 94 C/2/6,1/2
GEOCHEMISTRY SAMPLE LOCATIONS			
Drawn by	D.H.	Traced by	g.k.g
Revised by	Date	Revised by	Date
OMINECA M.D., B.C.			
Scale: 1 : 10,000		Date: NOVEMBER 1993	
Plate: 93-3a			





GEOLOGICAL BRANCH  
ASSESSMENT REPORT

**23,321**

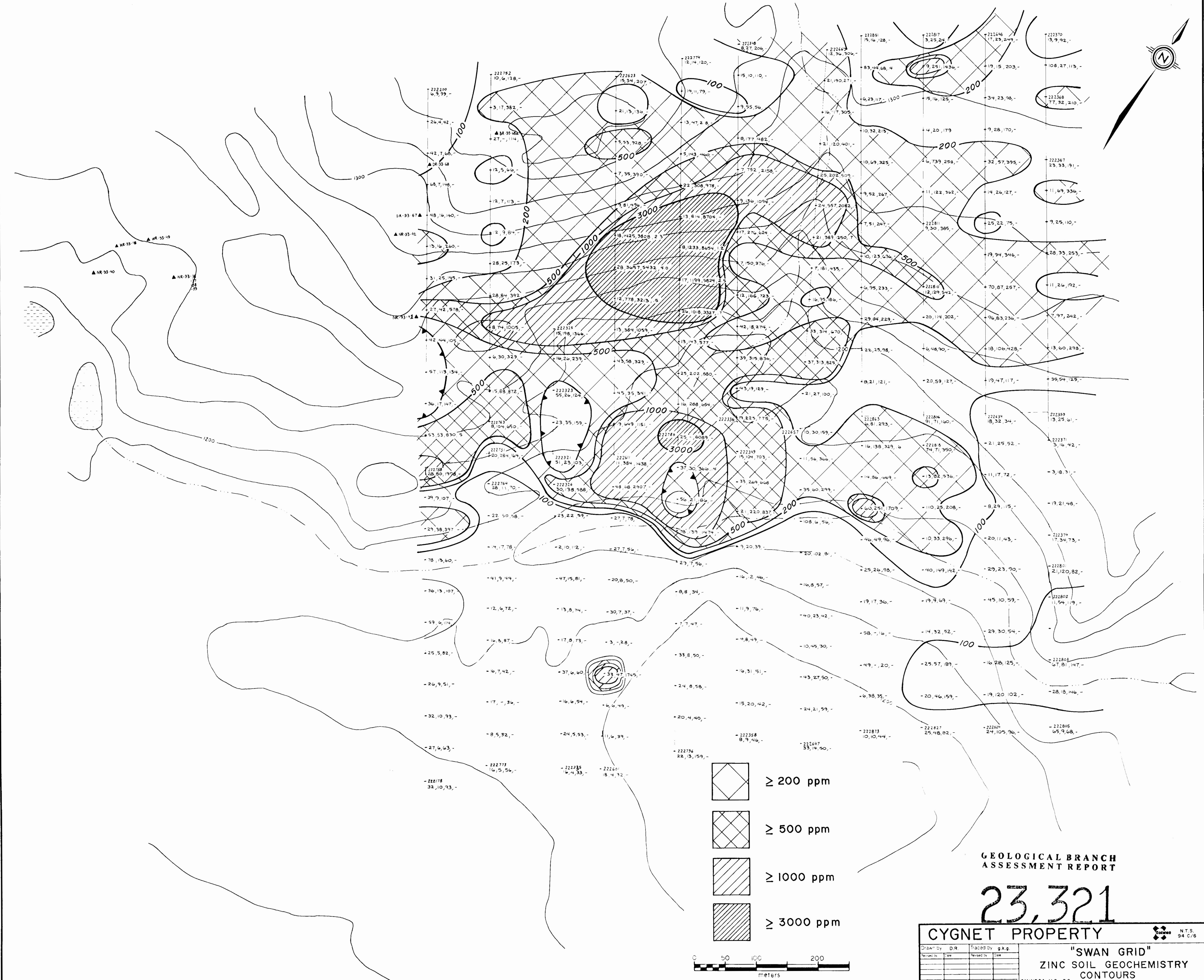
SYMBOLS

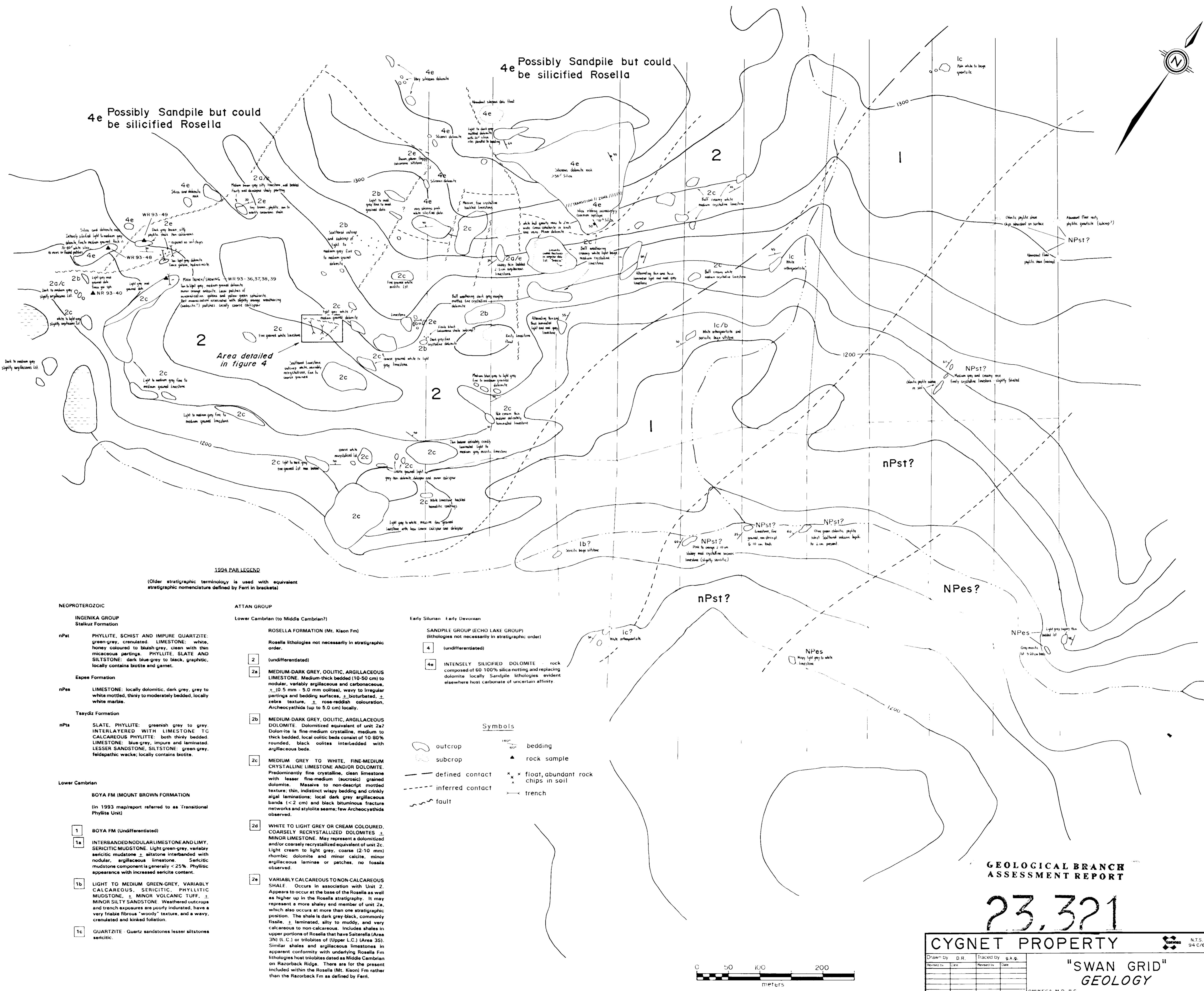
● Soil Sample Site

■ Stream Sediment Site

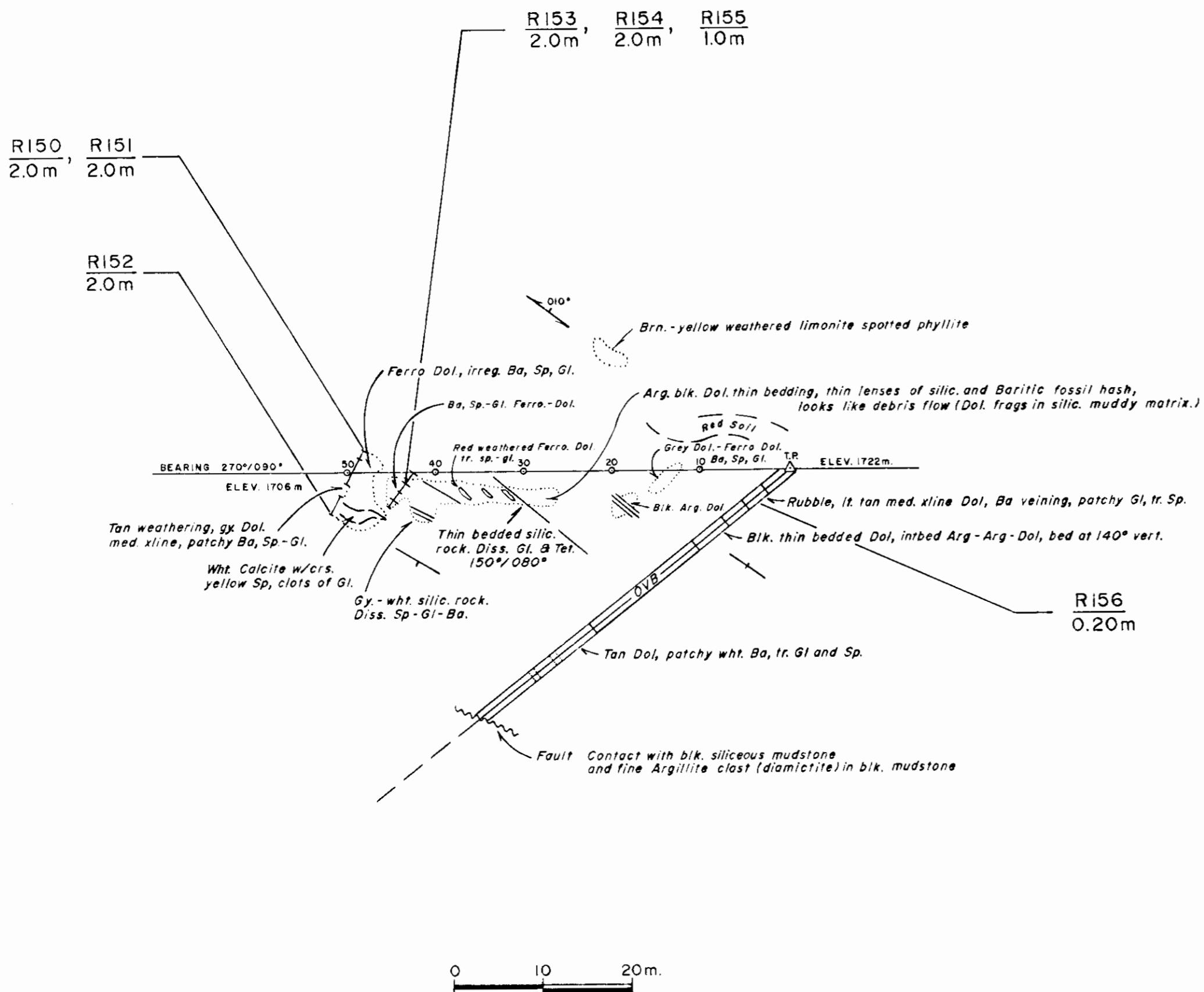
0 200 400 600 800 1,000 metres

CYGNET PROPERTY (WEST HALF)		N.T.S. 94 G/5,6/12													
Drawn by	D.R.	Traced by	g.k.g												
Revised by	Date	Revised by	Date												
<table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 25%;"> </td> <td style="width: 25%;"> </td> <td style="width: 25%;"> </td> <td style="width: 25%;"> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> </tr> <tr> <td> </td> <td> </td> <td> </td> <td> </td> </tr> </table>															
GEOCHEMISTRY SAMPLE LOCATIONS															
OMINECA M.D., B.C.		Scale: 1 : 10,000													
		Date: NOVEMBER 1993 Plate: 93-3b													









**ROCK GEOCHEM  
Analyses A.A.**

	Pb ppm	Zn ppm	Ag ppm
R150	4930	e 21,000	6.3
R151	1920	8210	2.4
R152	e 20,500	e 43,600	24.9
R153	8550	e 15,200	10.6
R154	e 10,100	e 43,700	14.4
R155	e 10,500	e 15,700	14.8
R156	e 15,700	e 73,400	20.4

e = exceeds calibration

**GEOLOGICAL BRANCH  
ASSESSMENT REPORT**

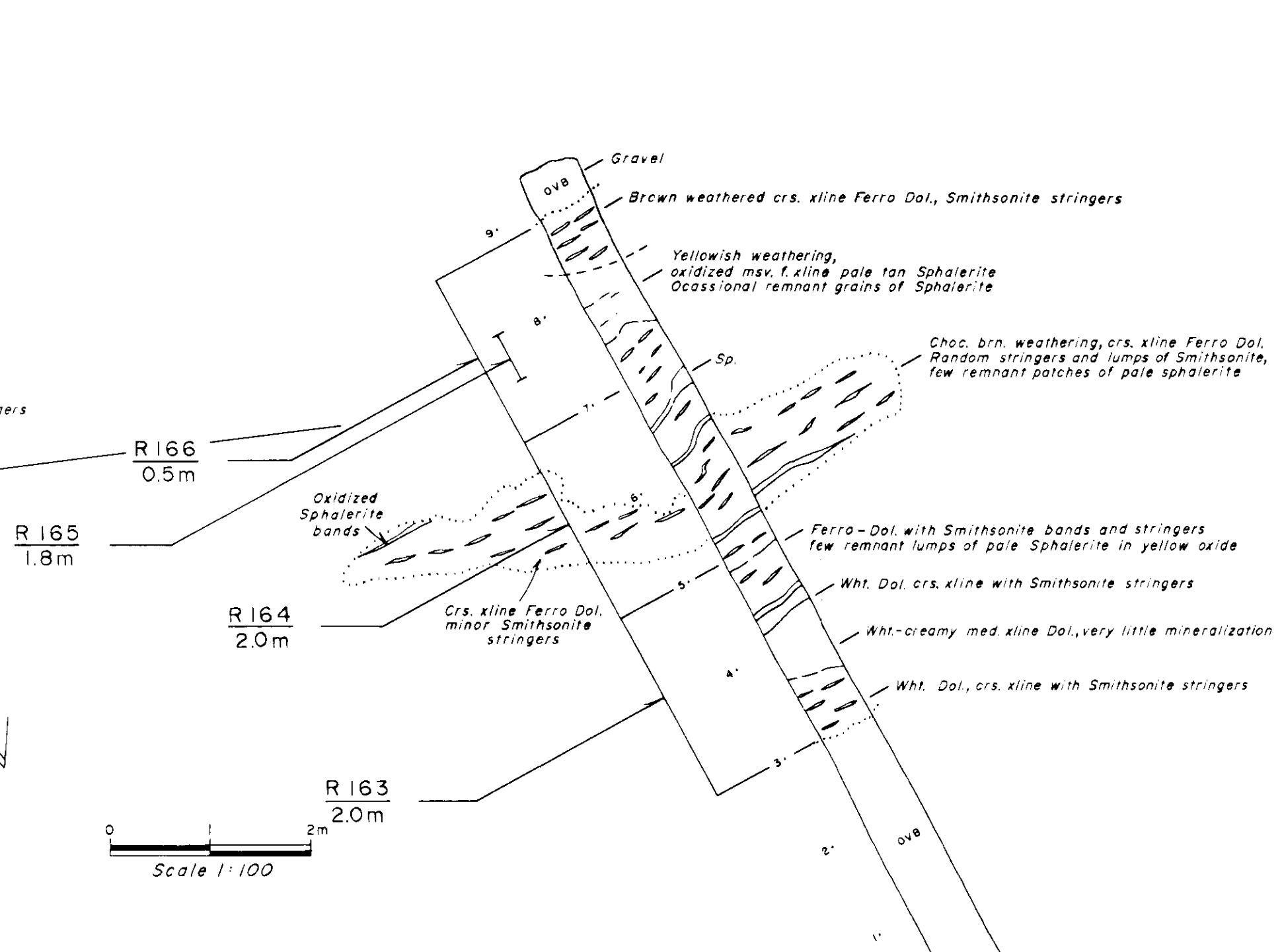
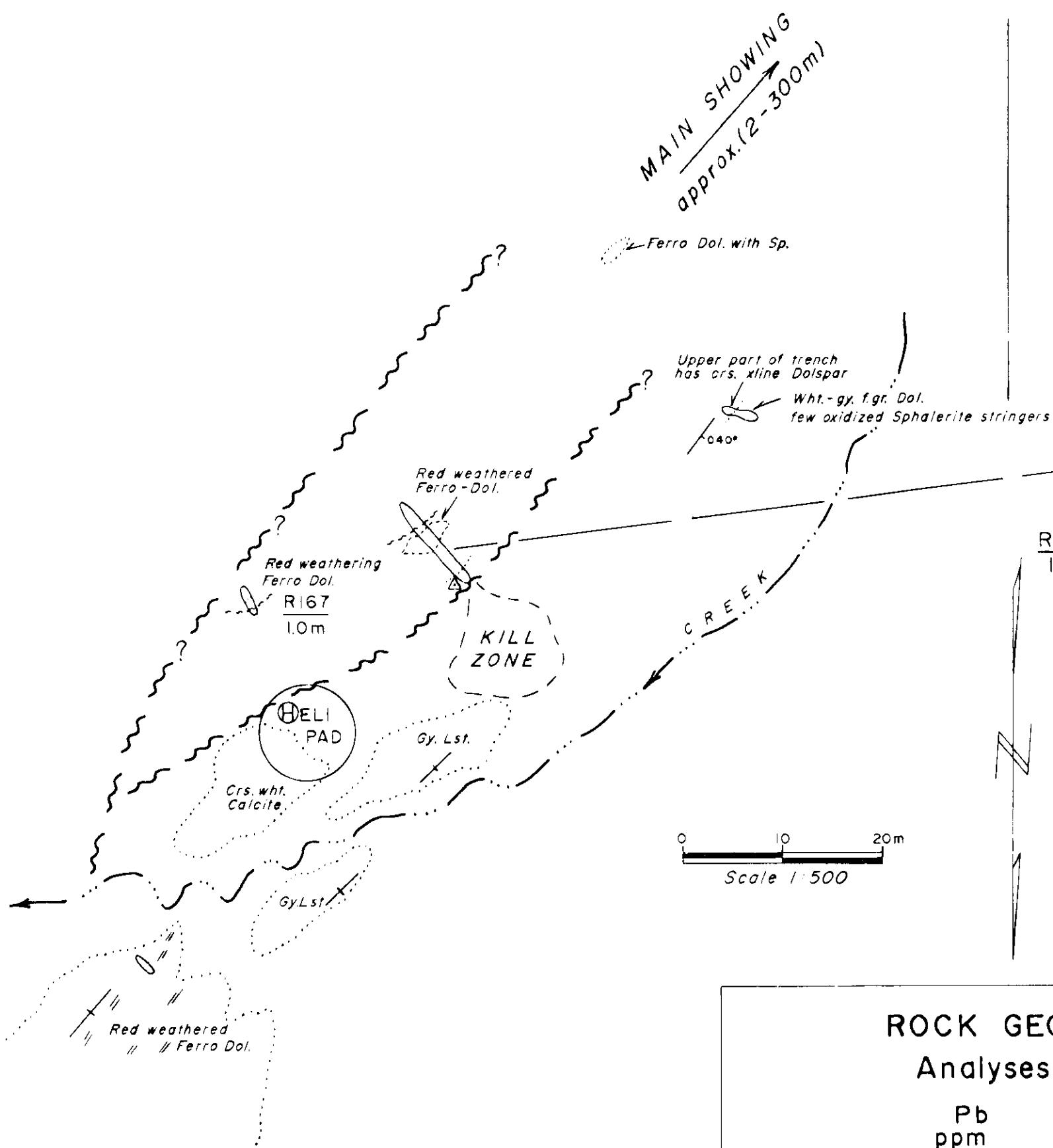
**23,321**

**CYNET PROPERTY**

Cominco N.T.S.  
94 C/6

**"RAIN" TRENCH  
South Showing**

Drawn by: A.B.M.	Traced by: g.k.g.		
Revised by	Date	Revised by	Date
OMINECA M.D., B.C.		Scale: 1 : 500 Date: JULY 1993 Plate: 93-7	



**ROCK GEOCHEM**  
Analyses A.A.

	Pb ppm	Zn ppm	Ag ppm
R163	1640	e128,000	28.0
R164	7490	e114,000	40.9
R165	2670	e170,500	46.4
R166	4830	e252,000	68.6
R167	6120	e95,200	38.5

e = exceeds calibration

**GEOLOGICAL BRANCH ASSESSMENT REPORT**  
**23,321**

**CYNET PROPERTY** N.T.S. 94 C/6

Drawn by: A.B.M.	Traced by: g.k.g.
Revised by: _____	Date: _____
Revised by: _____	Date: _____
OMINECA M.D., B.C.	Scale: _____
Date: JULY 1993	Plate: 93-8

**"SWAN" GROUP**  
N. Extension of "Main" Showing

#210-0640